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COMPUTER PROGRAM FOR CALCULATING
SUPERSONIC FLOW ABOUT CIRCULAR,
ELLIPTIC, AND BIELLIPTIC CONES
BY THE METHOD OF LINES

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16. Abstract <p>This paper is a user's manual for a computer program which calculates the supersonic flow about circular, elliptic, and bielliptic cones at incidence and elliptic cones at yaw by the method of lines. The program is automated to compute a case from a known or easily calculated solution by changing the parameters through a sequence of steps. It provides information including the shock shape, flow field, isentropic surface properties, entropy layer, and force coefficients. A description of the program operation, sample computations, and a FORTRAN IV listing are presented.</p>					
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COMPUTER PROGRAM FOR CALCULATING SUPERSONIC FLOW

ABOUT CIRCULAR, ELLIPTIC, AND BIELLIPTIC CONES

BY THE METHOD OF LINES

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SUMMARY

This paper is a user's manual for a computer program which calculates the supersonic flow about circular, elliptic, and bielliptic cones at incidence and elliptic cones at yaw by the method of lines. The program is automated to compute a case from a known or easily calculated solution by changing the parameters through a sequence of steps. It provides information including the shock shape, flow field, isentropic surface properties, entropy layer, and force coefficients. A description of the program operation, sample computations, and a FORTRAN IV listing are presented.

INTRODUCTION

In reference 1 the so-called method of lines was developed for obtaining numerical solutions of general conical flow problems, that is, those gas dynamic problems in which the fluid properties do not vary along rays emanating from a common point in the flow. The method was applied to circular and elliptic cones and to the compression side of conical delta wings with shock attached at the sharp leading edges.

This paper describes a computer program which uses the method of reference 1 and which is specially designed for circular- and elliptic-cone problems. The program provides information including the shock shape, flow field, isentropic surface properties, entropy layer, and force coefficients. A program for the delta-wing problems is described in reference 2.

The present program has a built-in capability for three different, but related, cross sections: circular, elliptic, and "bielliptic." The bielliptic cross section is one composed of two ellipses with different axis ratios on the windward and leeward sides of the body.

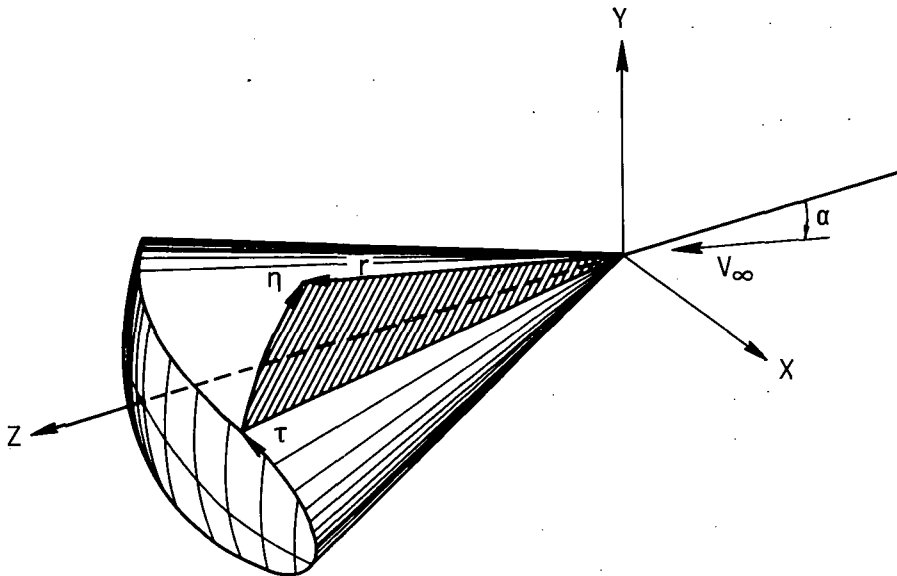
The mathematical method and coordinates are described very briefly, and the operation of the program is described in detail. A listing of the computer program is given in appendix A together with a list of the subroutines and a flow chart. Appendix B presents sample computations.

METHOD OF LINES

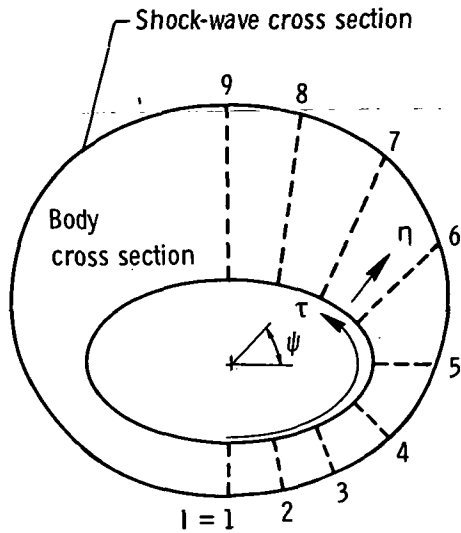
The flow equations are initially written in a body-oriented, orthogonal, conical coordinate system (r, η, τ) shown in sketch (a) where r is the distance along a conical ray, η is the angle measured from the body surface to the ray in a plane $\tau = \text{Constant}$, and τ is a measure of the arc length along the intersection of the body surface with a sphere of radius r centered at the body apex. Specifically, τ is determined by numerical integration on the unit sphere. The stream velocity vector V_∞ lies in the YZ-plane of symmetry, and the origin of the arc length τ is taken in the windward plane of symmetry. All computations are made in the right half-plane. The integration of the system of equations is facilitated by a coordinate transformation which maps the region bounded by the shock and the body into a rectangular domain as shown in sketch (b). The transformed variables are

$$\zeta = \frac{\eta}{\eta_s} \qquad \xi = \xi(\tau)$$

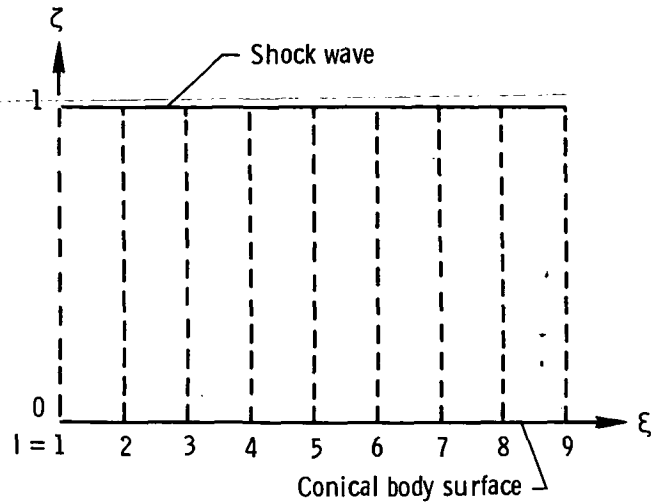
where $\eta = \eta_s(\tau)$ is the shock surface. Thus, $\zeta = 0$ on the body and $\zeta = 1$ on the shock. Also shown in sketch (b) is the cylindrical polar angle ψ ; in the windward symmetry plane $\psi = -\frac{\pi}{2}$, in the leeward symmetry plane $\psi = \frac{\pi}{2}$. For the elliptic cone at incidence the major axis lies in the XZ-plane and α is the angle of incidence, and for the elliptic cone at yaw the major axis lies in the YZ-plane and α is the angle of yaw.



Sketch (a)



Physical (τ, η) plane



Transformed (ξ, ζ) plane

Sketch (b)

The $\xi\zeta$ -plane is divided by N lines parallel to the ζ -axis; the line $I = 1$ is taken in the windward plane of symmetry and the line $I = N$ is in the leeward plane of symmetry. At each line the system of differential equations is reduced to a set of ordinary differential-difference equations by replacing the derivatives $\partial/\partial\xi$ by finite differences. The derivative of the Lagrange interpolation polynomial is used in this program with an equal number of lines on either side of the line at which $\partial/\partial\xi$ is computed; therefore, central differencing is obtained when the line spacing is equal. The system of equations is integrated simultaneously along each line $I = 1, \dots, N$. The differential equations along any line are coupled to those along the other lines through the finite-difference approximations for the cross derivatives $\partial/\partial\xi$. The equations are integrated by a fourth-order Runge-Kutta method. The accuracy of this method allows the use of relatively large integration steps. The integration step can generally be taken in increments of -0.1 from the shock to $\zeta = 0.1$ and in increments of -0.05 and -0.025 thereafter except in calculations where resolution of the entropy layer is sought.

The initial values for the system of equations are determined from the shock relations once the shock shape is specified, and the equations are integrated numerically from the shock to the body. An iterative process based on the Newton method is utilized to adjust the shock shape to satisfy the conditions of flow tangency on the body. Usually a very good estimate of the shock shape is required for a successful calculation. The exception is the circular cone at moderate incidence (relative to the cone semiapex angle); a tangent-cone approximation suffices for an initial estimate of the shock shape for this case. In order to obtain a good initial estimate of the shock shape for the

elliptic cone provision is made to proceed by a series of steps from a simpler case or a known solution. The procedure is completely automated for incrementing any one of the five parameters: free-stream Mach number, cone angle, angle of incidence, axis ratio, or ratio of specific heats.

PROGRAM OPERATION

Considerable flexibility has been built into the computer program in order to obtain converged solutions in a wide variety of cases. The solutions in many instances are very sensitive to the shock shape; consequently, they must be developed in incremental steps from a simpler or known solution. Instabilities can arise in some cases, and a change in some of the parameters involved will sometimes yield converged solutions. A number of parameters can be adjusted which can affect the convergence and computing time. Some discussion of these parameters is given with general recommendations for their values.

Incrementation of a Parameter

A good estimate of the shock shape is required for successful convergence for all cases other than the circular cone at small relative incidence, $\frac{\alpha}{\theta_0} < 0.5$, where θ_0 is the cone semiapex angle in the YZ-plane of symmetry. The built-in approximate shock (NREAD = 0) is satisfactory only for starting the computation of circular or nearly circular cones at small incidence. The elliptic-cone solutions and the circular-cone solutions at relatively large incidence can be constructed by changing the input parameters through a sequence of steps from a known or easily calculated solution, a new converged shock shape being obtained with each change of the input parameters¹ ($T, \alpha, \theta, M_\infty, \gamma$). An extrapolation routine is used to predict a new shock shape for the new input parameters.

The converged values of $\eta_{s,i}$ (where the subscript i is the line index) for the initial value of the parameter (PARAM) are used as the input values corresponding to a small variation (DPRAM1) of the input parameter. Thus, the input parameter is changed from its initial value (PARAM) to $\text{PARAM} + \text{DPRAM1}$. Typically, DPRAM1 is taken as 0.05 or 0.1 of the initial value of PARAM. Once the converged solution for this value of the parameter is obtained, the $\eta_{s,i}$ for a new value of the parameter, corresponding to the sum of the initial value of PARAM and DPRAM (where DPRAM is the regular increment), are computed by linear extrapolation. After three sets of converged $\eta_{s,i}$

¹The variables discussed in this section are further described in the section entitled "Input Description."

have been obtained corresponding to three values of the input parameter, a quadratic extrapolation is employed. The computations continue in increments of DPRAM up to the final value of PARAM (PARAMF) unless some difficulty is encountered which can cause the value of DPRAM to be halved. Some of these difficulties are discussed in the section entitled "Limitations." The computation is then restarted from the last converged value of PARAM once DPRAM has been halved. If DPRAM becomes less than DPRMIN the computation is terminated.

A convenient method for computing an elliptic cone is to increment T (INCRMT = 1) with the value of θ corresponding to the desired value for the elliptic cone. The computation for a circular cone would start with $\alpha = 0^\circ$ and NREAD = 0. Typical values of the increments would be DPRAM1 = -0.05 and DPRAM = -0.1 or -0.2. Once the computation has attained the final value of T , a second computation could be made for increasing angles of attack. In this computation the last converged $\eta_{s,i}$ values corresponding to $\alpha = 0^\circ$ would be read in (NREAD = 1 and NCNVRGB = 0). The incrementation would then be made on α ; thus, INCRMT = 2. Typical values of the α -increments might be DPRAM1 = 0.1 and DPRAM = 1.0 or 2.0.

It is possible, through a simple modification of the program, to increment two (or more) parameters simultaneously by establishing a functional relation between them. This procedure is followed in cases where only the final combination of values of parameters is of interest. For example, to compute an elliptic-cone flow field with $T = 0.6$ and $\alpha = 4.0^\circ$ one could take

```
T = 1., ALPHAD = 0., NREAD = 0, INCRMT = 1, NCNVRGB = 0,  
PARAM = 1., PARAMF = .6, DPRAM1 = -.05, DPRAM = -.1
```

and set

```
ALPHAD = 4.*(1.-PARAM)/(1.-PARAMF)
```

after card A1490 of the MAIN program.

Nonuniform Line Spacing

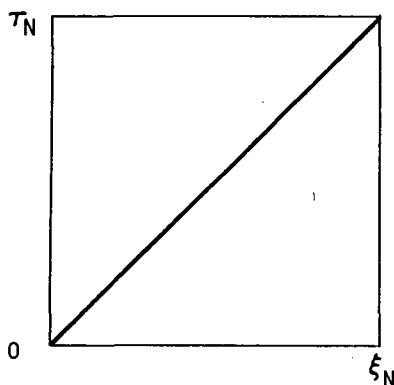
Included in the program are several options for obtaining a nonuniform line spacing. One option allows the user to select three regions around the right half-body so that in each region the physical line spacing is constant (equal $\Delta\tau$) but can differ from the spacing in the other two regions. This option is called when NSPACE = 2 and is described in the section entitled "Input Description."

The other options are continuous transformations between the physical arc length τ and the computational coordinate ξ . In these options the computations are carried out with equal increments $\Delta\xi$, whereas the physical spacing $\Delta\tau$ is stretched in various regions according to the option triggered by KTRANSF and the slope control parameter SLOPE (see section "Input Description"). The basic transformation is the following cubic polynomial relating τ to ξ :

$$\tau = \tau_0 + (\xi - \xi_0) \left[a + b(\xi - \xi_0)^2 \right]$$

where a is the slope control parameter $d\tau/d\xi$ at $\xi = \xi_0$ and has the FORTRAN name SLOPE and b and ξ_0 are constants which depend on the choice of a and τ_0 . There are three options, described as follows:

(1) KTRANSF = 1, identity transformation. This option gives $\tau = \xi$, that is, uniform line spacing in both the physical and computational planes (sketch (c)). With SLOPE = 1.0 as input, the program automatically uses $\tau_0 = \xi_0 = b = 0$. This option is the one which has been generally successful for most body shapes, as explained in reference 1.



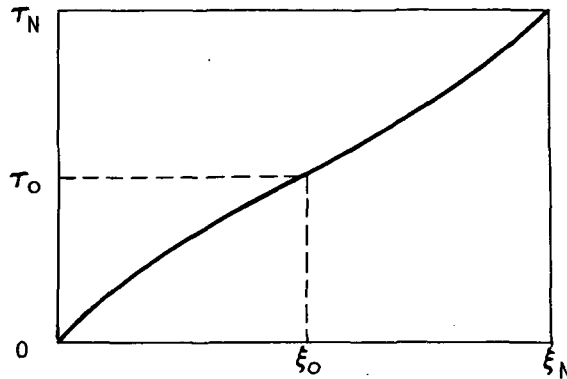
Sketch (c)

(2) KTRANSF = 2, high or low density of lines at $\psi = 0^\circ$. In this transformation option, τ_0 is the value of τ at $\psi = 0^\circ$, that is, $\tau_N/2$. Then ξ_0 and b are given by

$$\xi_0 = \frac{3\tau_0}{2a + 1}$$

$$b = \frac{1 - a}{3\xi_0^2}$$

which give $\frac{d\tau}{d\xi} = 1.0$ at both $\xi = 0$ and $\xi = \xi_N$. When $a = \text{SLOPE}$ is less than or greater than 1, the physical line spacing is more or less dense, respectively, near $\psi = 0^\circ$ than it is near the symmetry planes. Sketch (d) illustrates the transformation when $\text{SLOPE} < 1.0$. The user may typically employ $\text{SLOPE} < 1.0$ when calculating the flow over an elliptic cone with $T < 1.0$ in order to place relatively more lines in the region of large curvature. For the same reasons, $\text{SLOPE} > 1.0$ may be used for the elliptic cone with $T > 1.0$. Practical values of SLOPE range between 0.5 and 1.5.



Sketch (d)

(3) $\text{KTRANSF} = 3$, high or low density of lines at $\psi = 90^\circ$. In this option, the line spacing can be made more or less dense near the leeward symmetry plane, $\psi = 90^\circ$, by choosing $a = \text{SLOPE}$ less than or greater than 1, respectively. The parameters of the cubic polynomial are

$$\tau_0 = \xi_0 = 0$$

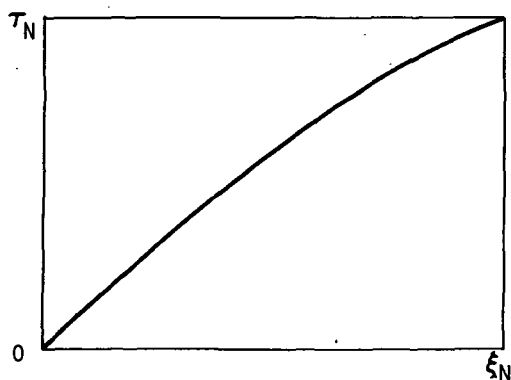
$$\frac{d\tau}{d\xi} = 1.0 \quad (\xi = 0)$$

$$b = \frac{a - 1}{3\xi_N^2}$$

where

$$\xi_N = \frac{3\tau_N}{2 + a}$$

This transformation is illustrated in sketch (e) for $\text{SLOPE} < 1.0$.



Sketch (e)

Input Description

The following list contains the program input variables, which are arranged according to order of presentation in the program.

<u>Input card</u>	<u>FORTTRAN variable</u>	<u>Description</u>
1	STMACH	Free-stream Mach number, M_∞
	GAMMA	Ratio of specific heats, γ
	T	Semiaxis ratio of the elliptic cone, b/a , where b is the semiaxis of the elliptic body in the YZ-plane of symmetry (which contains the velocity vector, sketch (a)) and a is the semiaxis in the XZ-plane of symmetry
	THETAD	The cone semiangle in the XZ symmetry plane, θ , degrees
	ALPHAD	Angle of attack, α , degrees
2	N	Number of lines. Line 1 is in the windward symmetry plane and line N is in the leeward symmetry plane. Must be an odd number to obtain force coefficients. Maximum allowed value is $N = 20$.

Input
card

FORTTRAN
variable

Description

2	M	Body selection trigger M = 0 for zero-incidence circular-cone solution M = 2 for circular, elliptic, and bielliptic cones
	NREAD	Trigger for reading in shock shape NREAD = 0 if the built-in approximate shock shape is to be used. This shock shape is satisfactory only for nearly circular cones at small incidence. NREAD = 1 when input shock shape is to be read in
	NSPACE	Line space trigger NSPACE = 1 for equal line spacing in the computational plane (equal $\Delta\xi$). The line spacing in the physical plane ($\Delta\tau$) can be made nonuniform by selection of the parameters KTRANSF and SLOPE. NSPACE = 2 gives piecewise constant line spacing in three segments with NA lines in the first segment, (NB-NA) lines in the second segment, and (N-NB) lines in the third segment. Set KTRANSF = 1 and SLOPE = 1.0. This option is not recommended. See input card 8 for further description.
	INCRMT	Trigger denoting which parameter on card 1 is to be incremented INCRMT = 1 increment T INCRMT = 2 increment ALPHAD INCRMT = 3 increment THETAD INCRMT = 4 increment STMACH INCRMT = 5 increment GAMMA
	IPRINT	Print trigger IPRINT = 1 full print including basic information for each trial shock shape, output heading, and zeta print blocks (flow-field data for each value of zeta) for intermediate and final computations

<u>Input card</u>	<u>FORTTRAN variable</u>	<u>Description</u>
2		IPRINT = 2 prints only ZETA = 0 block for all but the final (PARAMF) case in a series and full print for PARAMF
	NCNVRGB	<p>Start selection trigger</p> <p>NCNVRGB = 0 η_s values are found from the built-in approximate shock shape (with NREAD = 0) or are read in (NREAD = 1). See input card 9.</p> <p>NCNVRGB = 1 one set of converged η_s values are read in which correspond to PARAM1. The program uses those η_s values to start the calculation for PARAM.</p> <p>NCNVRGB = 2 two sets of converged η_s values are read in which correspond to PARAM1 and PARAM2. The program extrapolates these η_s values linearly to obtain η_s values to start the computation for PARAM.</p> <p>NCNVRGB = 3 three sets of converged η_s values are read in which correspond to PARAM1, PARAM2, and PARAM3. The program extrapolates these quadratically to obtain η_s values to start the computations for PARAM.</p>
	KTRANSF	<p>Continuous line spacing transformation trigger. (See section entitled "Nonuniform Line Spacing.")</p> <p>KTRANSF = 1 identity transformation in conjunction with SLOPE = 1 (see input card 4). Required for NSPACE = 2. The computational coordinate ξ is equal to the arc length τ.</p> <p>KTRANSF = 2</p> <p>If SLOPE < 1 the lines will be more dense in the region $\psi = 0^\circ$.</p> <p>If SLOPE > 1 the lines will be more dense in the windward and leeward symmetry planes.</p>

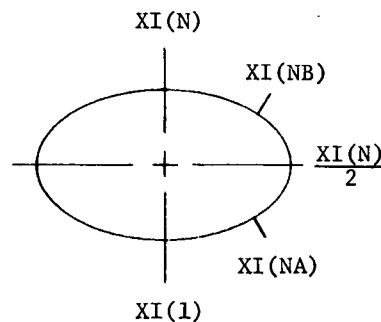
<u>Input card</u>	<u>FORTTRAN variable</u>	<u>Description</u>
2		<p>KTRANSF = 3</p> <p>If SLOPE < 1 the lines will be more dense in the leeward symmetry plane.</p> <p>If SLOPE > 1 the lines will be more dense in the windward symmetry plane.</p>
	NPLOT	<p>Punched card output to be used for plotting. (See section on "Output.")</p> <p>NPLOT = 0 no punched card output for plots</p> <p>NPLOT = 1 punched card output for plots</p>
	NPUNCH	<p>Punched card output for η_s</p> <p>NPUNCH = 0 no punched card output of η_s values</p> <p>NPUNCH = 1 punched card output of η_s values for each pivotal shock shape</p>
3	PARAM	<p>First value of STMACH, GAMMA, T, THETAD, or ALPHAD to be computed in a series, with the others held constant. (See definition of INCRMT.)</p>
	PARAMF	<p>Final value of PARAM to be computed</p>
	DPRAM1	<p>First small increment used with NCNVRGB = 0 or 1 to perturb the results obtained with PARAM. Program uses η_s values converged for PARAM to start the computations for PARAM = PARAM + DPRAM1. Successful convergence for this new value of PARAM gives the information needed for linear extrapolation to the next value of PARAM which is the sum of the original value of PARAM and DPRAM. If NCNVRGB \neq 0 or 1, DPRAM1 is a dummy input.</p>
	DPRAM	<p>Incremental value of parameter used after first increment DPRAM1. The magnitude of DPRAM must be greater than the magnitude of DPRAM1.</p>

<u>Input card</u>	<u>FORTTRAN variable</u>	<u>Description</u>	
3	DPRMIN	Minimum value allowed for DPRAM. If the program runs into trouble during a series of parameter incrementations, DPRAM is halved, possibly many times. DPRMIN prevents wasted machine time in hopeless cases.	
4	SLOPE	Continuous line spacing transformation parameter. (See section "Nonuniform Line Spacing.")	
	SLOPE	KTRANSF	Denser lines at
	1.0	1	
	<1.0	2	$\psi = 0^\circ$
	>1.0	2	$\psi = -90^\circ$ and $+90^\circ$
	<1.0	3	$\psi = +90^\circ$
	>1.0	3	$\psi = -90^\circ$
5	VTEST	Accuracy criterion on maximum normal velocity component at cone surface. Usually 10^{-3} suffices for three figures in shock shape and pressure distribution.	
	VTEST1	When the maximum magnitude of the normal velocity component on the surface VMAX lies between VTEST and VTEST1, a modified Newton method is incorporated, where the old Jacobian matrix of influence coefficients is used (ref. 1).	
6	M2E	Trigger for bielliptic cone computation. M2E = 0 for circular or elliptic cones M2E = 1 for bielliptic cone. It is necessary to set NSPACE = 1, KTRANSF = 1, and SLOPE = 1 for M2E = 1.	
7	TU	$\frac{b}{a}$, where b is the semiaxis in the leeward YZ (vertical) plane of symmetry and a is the semiaxis in the XZ (horizontal) plane of symmetry. TU is the axis ratio for the upper half of the bielliptic cone, and T is the axis ratio for the lower half. This card is read in only for M2E = 1.	

<u>Input card</u>	<u>FORTTRAN variable</u>	<u>Description</u>
8		This card is read in only when $\text{NSPACE} = 2$.
	NA	Number of lines equally spaced in first segment; must be an odd number to obtain force coefficients (sketch (f))
	NB	Line number at end of second segment; must be an odd number to obtain force coefficients

ANA $\frac{XI(NA)}{XI(N)/2}$

BNB $\frac{XI(NB)}{XI(N)/2}$



XI is arc length along contour.

Sketch (f)

9 This card is read in only if $\text{NREAD} = 1$ and $\text{NCNVRGB} = 0$.

ETAS(I) (I = 1, . . . , N) Values of η_s which are used to start the computations for PARAM. See input card 2 description for $\text{NCNVRGB} = 0$.

The use of previously converged results for starting a series of related computations provides an economical method of using the program. Input cards 10 to 18 are used for this purpose: input cards 10 and 11 are used when one converged case is read in ($\text{NCNVRGB} = 1$); input cards 12 to 14 are used with two converged cases ($\text{NCNVRGB} = 2$), and input cards 15 to 18 are used with three converged cases ($\text{NCNVRGB} = 3$). Thus, if one had previously converged elliptic-cone cases for $T = 0.8, 0.7$, and 0.6 , one could use those three sets of η_s values with $\text{NCNVRGB} = 3$ to predict the starting shock shape for some other value of T , say 0.5 . Hence the input would include $\text{INCRMT} = 1$, $\text{PARAM} = 0.5$, $\text{PARAM1} = 0.8$, $\text{PARAM2} = 0.7$, and $\text{PARAM3} = 0.6$.

<u>Input card</u>	<u>FORTRAN variable</u>	<u>Description</u>
10		This card and input card 11 are read in only if $NCNVRGB = 1$. See input card 2 description for $NCNVRGB = 1$.
	PARAM1	Value of PARAM corresponding to ETAS1(I)
11	ETAS1(I) (I = 1, . . . , N)	Values of η_s corresponding to PARAM1
12		This card and input cards 13 and 14 are read in when $NCNVRGB = 2$. See input card 2 description for $NCNVRGB = 2$.
	PARAM1	Value of PARAM corresponding to ETAS1(I)
	PARAM2	Value of PARAM corresponding to ETAS2(I)
13	ETAS1(I) (I = 1, . . . , N)	Values of η_s corresponding to PARAM1
14	ETAS2(I) (I = 1, . . . , N)	Values of η_s corresponding to PARAM2
15		This card and input cards 16, 17, and 18 are read in only when $NCNVRGB = 3$. See input card 2 description for $NCNVRGB = 3$.
	PARAM1	Value of PARAM corresponding to ETAS1(I)
	PARAM2	Value of PARAM corresponding to ETAS2(I)
	PARAM3	Value of PARAM corresponding to ETAS3(I)
16	ETAS1(I) (I = 1, . . . , N)	Values of η_s corresponding to PARAM1
17	ETAS2(I) (I = 1, . . . , N)	Values of η_s corresponding to PARAM2
18	ETAS3(I) (I = 1, . . . , N)	Values of η_s corresponding to PARAM3

Output

Among the first items printed are some of the input parameters (see section entitled "Input Description") and, in addition, some preliminary computed quantities and control parameters (described in the sections entitled "Auxiliary Definitions" and "Secondary Parameters") which are not input data but which can be readily changed within the program. Two sample computations are presented in appendix B.

Each pivotal (trial) shock shape and the resulting normal velocity components at the cone surface are printed out regardless of the print option. (The N-variations of the pivotal shock shape are not printed.) The following information is printed: ETAS(I), ETASP(I), CP(I) at shock, CP(I) at body, and V(I) at body for $I = 1, \dots, N$ from left to right. (CP is pressure coefficient and V is normal velocity component.) After the print of V(I) at the body, the quantities KCOUNT, VMAX, EPSIG, SPACER, VMXTEST, and DETERM are printed followed by DETA(I).

If IPRINT = 1 and a case has been converged (i.e., VMAX < VTEST), the full results are printed, starting on a new page, with much of the preliminary information repeated in an orderly fashion. This allows the printing for the preliminary iterations to be separated and discarded if desired. If IPRINT = 2, only the final converged case in a series is printed in full. For an explanation of full print, see sections "Summary Print Block" and "ZETA Print Blocks."

The arc length TAU(I) and the transformed coordinate XI(I) are printed between the summary print block and the zeta print blocks together with the body coordinates XO(I), YO(I) and the shock quantities ETAS(I) and ETASP(I).

Windward- and leeward-line zeta limits.- Following the ZETA = 0 print block are the limiting values of certain flow properties which are dependent upon the direction of approach to the nodal-point singularity as described in reference 1. For the elliptic cone with $T < 1$, a nodal point lies on the surface in both the windward and leeward symmetry planes. The values printed in the ZETA = 0 print block are the limits obtained by approaching the symmetry planes along the surface. The limits corresponding to an approach in the symmetry plane are tabulated under the headings "WINDWARD LINE ZETA LIMIT" and "LEEWARD LINE ZETA LIMIT." For the circular cone and the elliptic cone with $T > 1$, the windward stagnation point is a saddle point and all variables are continuous there, hence the values printed in WINDWARD LINE ZETA LIMIT and the ZETA = 0 print block are the same. For the elliptic cone with $T > 1$, a saddle point or a nodal point may lie on the surface in the leeward symmetry plane, depending upon the geometry and flow conditions. (The entropy function SBAR is printed under the heading labeled "S.")

Force coefficients.- After the windward-line and leeward-line zeta limits, the aerodynamic force and moment coefficients are printed as well as the center-of-pressure location. The quantities printed are coefficients of axial force (CZ), normal force (CY), drag (CD), lift (CL), moment about X-axis (CM), and the coordinates of the center of pressure (YBAR and ZBAR). The reference area for the force and moment coefficients is the base area.

Plots.- The program has a plot option trigger, NPLOT, which can be used to obtain punched card output for use in another program which, in turn, rearranges the cards in an order suitable for plotting cross-flow streamlines and the cross sections of the body and shock, as well as surface and shock pressure coefficients and surface quantities U, W, RHO, and CROSSM as functions of ψ . This second program is not included, however, because each different computer system has its own variations in plotting routines and requirements. It is hoped that the user can adapt the punched card output for these plots to his specific requirements.

Appropriate labels for the cards are punched at cards A1600 and A1610, and the body coordinates, polar angle ψ , and surface quantities are punched at cards A6020 to A6100 of MAIN program. The quantity NZETA punched at card A6020 in the MAIN program (computed at card L760 in subroutine PRINT) is a counter of the number of integration steps from the shock which is used in the plotting program. In subroutine PRINT, the polar angle and shock pressure coefficient are punched at cards L550 and L560. The coordinates of the shock and cross-flow streamlines are punched at cards L810 and L820.

Auxiliary Definitions

Several quantities appear in the printout of the preliminary iterations; some of these quantities can be useful in evaluating the sequence of iterations. Those quantities which have not been defined elsewhere are defined as follows:

<u>FORTRAN</u> <u>variable</u>	<u>Description</u>
AAST	Ratio of critical speed to free-stream speed
DETA	The correction applied to each value of η_s , $\Delta\eta$
DETERM	The determinant of the Jacobian, or influence coefficient, matrix. (This matrix is normalized so that the sum of squares of the elements of each row is 1.)
EPSIGMX	Maximum value allowed for EPSIG. This parameter has been used at times with EPSIG (see section "Secondary Parameters") computed within the program as some fraction of VMAX. This procedure is not recommended. Set in card A2080 of MAIN program.
EPSIGOM	Parameter for controlling step size during the numerical integration of the body geometry. Used in cards C540 and C550 in subroutine RUNKUT and set in card A580 in the MAIN program.

<u>FORTTRAN</u> <u>variable</u>	<u>Description</u>
EPSIVAR	Perturbation parameter. Changes η_s to $(1 + \text{EPSIVAR})\eta_s$ for each perturbation integration. Set in card A2090 of MAIN program and used in cards A8280, A8350, and A8370 of MAIN program.
ETASP	Derivative of the quantity η_s with respect to the arc length τ , $d\eta_s/d\tau$
INTCNT	Number of integration steps used to determine $\xi(N)/2$ in body geometry computation
KCOUNT	Total number of pivotal and variational integrations (see NCYCLE)
NCYCLE	Number of iteration cycles. The first cycle always consists of one pivotal (trial) and N variational integrations to generate the Jacobian matrix. Subsequent cycles may or may not include the N perturbation integrations. No perturbation runs are made when $V_{\text{MAX}} < V_{\text{TEST1}}$ (modified Newton computation) and the old Jacobian matrix is used to obtain the corrections $\Delta\eta$; in this case a cycle is one integration. When $V_{\text{MAX}} > V_{\text{TEST1}}$ one cycle consists of the pivotal integration and the N perturbation integrations required to generate a new Jacobian matrix.
PTINF	Free-stream total pressure referenced to product of free-stream density and square of free-stream velocity
RANGLE	Relative angle of incidence, α/θ_0 , where θ_0 is the cone semiapex angle in the vertical (YZ) plane of symmetry
VMAX	Maximum magnitude of normal velocity component on body surface
VMXTEST	Velocity test parameter, computed in cards A2600 and A2610 of the MAIN program and used in card A7860. If $V_{\text{MAX}} > V_{\text{MXTEST}}$ occurs during a parametric incrementation series, the increment is automatically halved. VMXTEST is computed as 0.5 of the minimum magnitude of the velocity component normal to the shock wave. This factor can be altered in card A2590 of the MAIN program as required.

FORTTRAN
variable

Description

XI Computational coordinate, ξ . The computational coordinate is related to the physical arc-length coordinate τ through the function $\xi = \xi(\tau)$. The function can be chosen to alter the line spacing in the arc-length variable τ . See KTRANSF and SLOPE in section entitled "Input Description."

Secondary Parameters

A number of parameters have been built into the program which control various computations. Those related to the size of the integration steps are as follows:

FORTTRAN
variable

Description

EPSIG Control parameter for triggering the extrapolation to the surface. When the G-function in the denominator of the equations for the zeta derivatives becomes smaller than EPSIG, the program extrapolates to obtain values of the normal velocity component at the surface. Used in cards J920 and J940 of subroutine EQNS and set in card A2060 of the MAIN program. Normal value is 10^{-3} . This parameter must be reduced in value when small integration steps are used near the body.

EPSINT, DSMAX, DSMIN Parameters used when integration step size is automatically varied. This option is not recommended. The program uses a preselected step variation by setting DSMIN=DSMAX at card K350 of subroutine RUNKUT2. The value of EPSINT is set in card A2100 of MAIN program and is used in cards K1300 and K1430 of subroutine RUNKUT2.

SPACER Sets the minimum distance between points to be used in the formula for extrapolation to body surface. Used in card K530 of subroutine RUNKUT2 and set in card A2070 of MAIN program. Recommended value is SPACER=EPSIG.

Summary Print Block

The notation used in the summary print block is as follows:

<u>FORTTRAN variable</u>	<u>Symbol</u>	<u>Description</u>
I		Line number
PSID		Arc tan (y_o/x_o), degrees
PSISD		Arc tan (y_s/x_s), degrees
XO, YO	x_o, y_o	Cartesian coordinates of body in plane $Z = 1$
XOBAR, YOBAR	\bar{x}_o, \bar{y}_o	Cartesian coordinates of body referenced to $x_{o,max}$
XS, YS	x_s, y_s	Cartesian coordinates of shock in plane $Z = 1$
XSBAR, YSBAR	\bar{x}_s, \bar{y}_s	Cartesian coordinates of shock referenced to $x_{o,max}$
ETAS	η_s	Value of η at shock, radians (see section on "Zeta Print Blocks" for description of η)
BETAD	β	Angle between free-stream velocity vector and tangent plane to shock, degrees
XI	ξ	Computational coordinate (see section on "Auxiliary Definitions")
CPSHOCK		Pressure coefficient at shock wave
CPBODY		Pressure coefficient at body surface

Zeta Print Blocks

The notation used in the zeta print blocks is as follows:

<u>FORTTRAN variable</u>	<u>Description</u>
ZETA	Independent variable, η/η_s ; $\xi = 1$ at shock and $\xi = 0$ on body surface.

<u>FORTTRAN variable</u>	<u>Description</u>
P	Pressure p referenced to product of free-stream density and square of free-stream velocity
P/ROASTSQ	Pressure referenced to product of free-stream density and square of critical speed
P/PTINF	Pressure referenced to free-stream total pressure
P/PINF	Pressure referenced to free-stream pressure
RHO	Density ρ referenced to free-stream density
U,V,W	u-, v-, w-components of velocity in r-, η -, τ -directions, respectively, referenced to critical speed
UC,VC,WC	Quasi-cylindrical velocity components in Z-direction, and directions normal and tangential to body contour in plane $Z = 1$, respectively, referenced to critical speed
VCC,WCC	Circular cylindrical velocity components normal and tangential to a circle in plane $Z = 1$, referenced to critical speed. UCC is same as UC.
VX,VY,VZ	Cartesian velocity components, referenced to critical speed
PSINOR	Arc tan (VX/VZ), degrees
THETNOR	Arc cos $VY/\sqrt{(VX)^2 + (VY)^2 + (VZ)^2}$, degrees
XBAR, YBAR	Cartesian coordinates referenced to $x_{o,max}$
XBHLD, YBHLD	Cartesian coordinates of cross-flow streamline (isentropes) that intersects the shock at line I, referenced to $x_{o,max}$
ETA	Angle measured in a plane normal to the body from a ray on surface to ray in field, η , radians
G	Function that appears as a factor in the denominator of most of the equations for the ζ -derivatives and which vanishes at the body (g in ref. 1, p. 12)

FORTTRAN
variable

Description

DEQNS	Function which is a factor in the denominator of the equations for the ζ -derivatives (D in ref. 1, p. 13). It vanishes when a line $\zeta = \text{Constant}$ becomes tangent to a conical characteristic. This tangency can occur only when regions of supersonic cross flow ($\text{CROSSM} \geq 1$) appear.
AM	Local Mach number, $\frac{\sqrt{U^2 + V^2 + W^2}}{a}$, where a is the speed of sound.
CROSSM	Cross-flow Mach number, $\frac{\sqrt{V^2 + W^2}}{a}$
SBAR	Entropy function, $\bar{S} = \log \left[\left(\frac{P}{P_{\text{INF}}} \right) \rho^\gamma \right]$
POROGAM	P/ρ^γ
PT/PTINF	Ratio of total pressure to free-stream total pressure
PT	Total pressure referenced to product of free-stream density and square of free-stream velocity
BERNOUL	Error in Bernoulli equation, $1 - \left(\frac{2\gamma}{\gamma - 1} \frac{p}{\rho} + u^2 + v^2 + w^2 \right) \frac{\gamma + 1}{\gamma - 1}$
DPDZ, DUDZ, DVDZ, DWDZ, DSBDZ	$\frac{dp}{d\zeta}, \frac{du}{d\zeta}, \frac{dv}{d\zeta}, \frac{dw}{d\zeta}, \frac{d\bar{S}}{d\zeta}$, respectively
PP, UP, VP, WP, SBARP	Finite-difference approximations for $\frac{\partial p}{\partial \tau}, \frac{\partial u}{\partial \tau}, \frac{\partial v}{\partial \tau}, \frac{\partial w}{\partial \tau}, \frac{\partial \bar{S}}{\partial \tau}$, respectively

Accuracy Control Parameters

The accuracy of the computations improves with increasing number of lines N and with increasing number of points NP in the cross-derivative approximation formula only within certain limitations. Instabilities arise for computations at low free-stream Mach numbers or for very flat (small T) elliptic cones, and the instabilities are

accentuated for the larger values of N . The integration step size, particularly near the body surface, can also influence the accuracy of the final results. Recommended values for computations to engineering accuracy (three to four figures) are given for the principal parameters.

<u>FORTTRAN</u> <u>variable</u>	<u>Description</u>
DS	<p>Integration step size from shock to body. Set in cards K420, K430, K440, and K450 of subroutine RUNKUT2. Recommended values are</p> <p>DS = -0.1 for $0.1 < ZETA \leq 1.0$</p> <p>DS = -0.05 for $0.05 < ZETA \leq 0.1$</p> <p>DS = -0.025 for $0.025 < ZETA \leq 0.05$</p> <p>DS = -0.0125 for $0 < ZETA \leq 0.025$</p>
N	<p>Number of lines</p> <p>For circular cones at small incidence ($RANGLE < 0.5$) or elliptic cones of moderate axis ratio ($1. \geq T \geq 0.7$) and small incidence, $N = 5$ to 11.</p> <p>For circular cones at large incidence ($RANGLE \geq 0.5$) and elliptic cones at any incidence, $N = 13$ to 19.</p>
NP	<p>Number of points used in computation of cross derivatives. Set in card A620 in MAIN program.</p> <p>NP = 3 for computations where computing time is a prime consideration</p> <p>NP = 5 for most computations. Larger values increase the computing time substantially with little change in the overall results. The accuracy with NP = 5 is noticeably better than with NP = 3.</p>
VTEST	<p>Convergence criterion on the maximum normal velocity component at the body surface</p> <p>VTEST = 10^{-3} to 10^{-4} for most cases</p> <p>VTEST = 5×10^{-3} for relatively flat elliptic cones ($T \leq 0.25$) where convergence is difficult</p>

FORTTRAN
variable

Description

VTEST1	Parameter for selection of regular or modified Newton method. The modified Newton method is used after all the normal velocity components on the body are less than VTEST1 VTEST1 = 0.01 to 0.05 for most cases VTEST1 = 0.001 for relatively flat ($T \lesssim 0.25$) elliptic cones
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The quantity DPRAM, which is the increment in the parameter being varied in the computations, can have a significant influence on the overall computing time. Values of this parameter can only be established on the basis of experience. For example, if the incrementation parameter is the angle of attack, DPRAM = 2.5 may suffice for circular cones at Mach numbers larger than 3, whereas the value of DPRAM required for an elliptic cone may be considerably smaller. The automatic incrementation routine has a built-in provision for reducing the size of the increment as required. See section on "Incrementation of a Parameter."

Entropy-Layer Computations

The values of some of the parameters must be changed in order for computations to be carried into the entropy layer. These computations have to be carried out in a sequence of steps by using the converged shock shape from one sequence as the input values for the next sequence of computations. The magnitudes of the quantities VTEST, EPSIG, SPACER, and DS must be reduced in stages. Setting SPACER=EPSIG is recommended for all computations. One satisfactory procedure has made use of a systematic step-size reduction (for example, a halving mode for DS) for values of ZETA less than 0.1 with EPSIG = 10.*VTEST. The quantity VTEST was then reduced in a sequence of computations, the first with VTEST = 10^{-4} , the second with VTEST = 10^{-6} , and so forth. The computation was continued in stages until VTEST was 10^{-10} .

Limitations

The computations may become very sensitive to the accuracy of the shock description, or fail completely, for the following conditions:

- (1) Angle of attack equal to or greater than the body apex half-angle in the vertical (YZ) plane of symmetry. Three factors contribute to the difficulty in obtaining a solution: (a) the shock wave on the leeward side approaches tangency with the free-stream Mach cone which is a singularity of the equations, (b) the cross flow becomes locally supersonic which signals the onset of embedded shock waves, and (c) the computed pressures in the

flow field or on the body become very small. The computations can often be continued to larger angles of attack by reducing the number of lines. Use can also be made of the option of altering the body shape on the leeward side to avoid some of the computational difficulties for cases where the flow on the windward side is of primary interest. For this option set $M2E = 1$ and $TU > T$ in the input. See section "Input Description."

(2) Very flat elliptic cone. The pressure gradients in the cross-flow direction became large as the axis ratio T becomes small, thus dictating a relatively large number of lines to construct the solution to good accuracy. However, instabilities arise for a large number of lines (ref. 1) and it becomes necessary to use fewer lines than would otherwise be desirable. Some roughness in the computed results will generally be evident when $T \lesssim \frac{1}{3}$ but this is dependent on the angle of attack. Computations for smaller T can be made for small angles of attack but the results will be more irregular. The maximum number of lines recommended is $N = 19$.

(3) Low Mach number. The computations become very sensitive to the accuracy of the shock shape at the low supersonic Mach numbers. If difficulty is encountered for $M_\infty < 2$, say, the solution can sometimes be obtained by reducing the number of lines. In general, the method fails for slender cones at low supersonic Mach numbers, a condition which produces a weak shock.

Special System Features

The program is written in FORTRAN IV for the Control Data 6000 series computer system. Some changes may be required for other systems. The word length of this computer is 60 bits, so double precision should be used on systems with 32- or 36-bit word lengths. Some seven-character variable names have been used in the program which may not be acceptable to other systems. At card A1330 a test is made on the input values of T and α . If they are exactly 1.0 and 0., respectively, the zero-incidence circular-cone solution (using only one line) is triggered. Some computers may not store an exact 1.0 or 0., even though they are inputs, hence an appropriate test would need to be substituted. The program requires a field length of 70 K_g to compile and execute on the CDC 6000 series computer system at Langley Research Center.

Langley Research Center,
National Aeronautics and Space Administration,
Hampton, Va., December 30, 1971.

APPENDIX A

PROGRAM LISTING, LIST OF SUBROUTINES, AND FLOW CHART

The computational program listing is given in this appendix together with a list of the subroutines and a flow chart.

Program Listing

The computational program listing is as follows:

```

AAST=SQRT((GAMMA-1.)/(GAMMA+.1))+2./((GAMMA+.1)*STMACH**2)      A 820
AASTO=AAST**2                                                    A 830
READ (5,135) N,M,NREAD,NSPACE,INCRMT,IPRINT,NCNVRGB,KTRANSF,NPLOT. A 840
INPUNCH.                                                         A 850
READ (5,134) PARAM,PARAMF,OPRAME,OPRAM,OPRNM                    A 860
READ (5,134) SLOPE                                              A 870
READ (5,134) VTEST,VTFCTI                                       A 880
IF M2E=0 USE REGULAR M*2 SOLUTION                                A 890
IF M2E=1 USE M*2 BODY WITH TWO ELLIPSES                         A 900
WHEN M2E=1, NSPACE MUST EQUAL ONE, KTRANSF=1, SLOPE=1          A 910
                                                                    A 920
                                                                    A 930
                                                                    A 940
                                                                    A 950
                                                                    A 960
                                                                    A 970
                                                                    A 980
                                                                    A 990
                                                                    A1000
                                                                    A1010
                                                                    A1020
                                                                    A1030
                                                                    A1040
                                                                    A1050
                                                                    A1060
                                                                    A1070
                                                                    A1080
                                                                    A1090
                                                                    A1100
                                                                    A1110
                                                                    A1120
                                                                    A1130
                                                                    A1140
                                                                    A1150
                                                                    A1160
                                                                    A1170
                                                                    A1180
                                                                    A1190
                                                                    A1200
                                                                    A1210
                                                                    A1220
                                                                    A1230
                                                                    A1240
                                                                    A1250
                                                                    A1260
                                                                    A1270
                                                                    A1280
                                                                    A1290
                                                                    A1300
                                                                    A1310
                                                                    A1320
                                                                    A1330
                                                                    A1340
                                                                    A1350
                                                                    A1360
                                                                    A1370
                                                                    A1380
                                                                    A1390
                                                                    A1400
                                                                    A1410
                                                                    A1420
                                                                    A1430
                                                                    A1440
                                                                    A1450
                                                                    A1460
                                                                    A1470
                                                                    A1480
                                                                    A1490
                                                                    A1500
                                                                    A1510
                                                                    A1520
                                                                    A1530
                                                                    A1540
                                                                    A1550
                                                                    A1560
                                                                    A1570
                                                                    A1580
                                                                    A1590
                                                                    A1600
                                                                    A1610
                                                                    A1620
                                                                    A1630
                                                                    A1640
                                                                    A1650
                                                                    A1660
                                                                    A1670
                                                                    A1680
                                                                    A1690
AAST=SQRT((GAMMA-1.)/(GAMMA+.1))+2./((GAMMA+.1)*STMACH**2)
AASTO=AAST**2
READ (5,135) N,M,NREAD,NSPACE,INCRMT,IPRINT,NCNVRGB,KTRANSF,NPLOT.
INPUNCH.
READ (5,134) PARAM,PARAMF,OPRAME,OPRAM,OPRNM
READ (5,134) SLOPE
READ (5,134) VTEST,VTFCTI
IF M2E=0 USE REGULAR M*2 SOLUTION
IF M2E=1 USE M*2 BODY WITH TWO ELLIPSES
WHEN M2E=1, NSPACE MUST EQUAL ONE, KTRANSF=1, SLOPE=1
READ (5,135) M2E
IF (M2E.EQ.1) READ (5,134) TU
KCONVT=0
NINP=1
NAN=1
ANA=1
BNB=1
NMI=1
NPI=1
IF (NSPACE.EQ.2) READ (5,144) NA,NR,ANA,BNB
NCNVGB=NCNVRGB
PRINT 137, N,M,NREAD,NSPACE,NP,NCNVGB
PRINT 145, NA,ANA,NR,BNB
PRINT 156, VTEST,VTFCTI
PRINT 160, SLOPE,KTRANSF
IF (M2E.EQ.0) PRINT 180, M2E
IF (M2E.EQ.1) PRINT 179, M2E,TU
IF (NCNVGB.EQ.0) AND (NREAD.EQ.0) GO TO 8
IF (NCNVGB.EQ.0) AND (NREAD.EQ.1) GO TO 3
IF (NCNVGB.EQ.1) GO TO 4
IF (NCNVGB.EQ.2) GO TO 5
IF (NCNVGB.EQ.3) GO TO 7
3 READ (5,152) (ETAS(1),I=1,N)
GO TO 8
4 READ (5,134) PARAM
READ (5,152) (ETAS(1),I=1,N)
DO 4 I=1,N
5 ETAS(1)=ETAS(1)
GO TO 8
6 READ (5,134) PARAM,PARAMF
READ (5,152) (ETAS(1),I=1,N)
GO TO 8
7 READ (5,134) PARAM,PARAMF,PARAM3
READ (5,152) (ETAS(1),I=1,N)
READ (5,152) (ETAS(2),I=1,N)
READ (5,152) (ETAS(3),I=1,N)
R DO 132 L=1,100
IF (WHLD.EQ.0) AND (M.EQ.2) AND (T.EQ.1) AND (ALPHAD.EQ.C) GO TO 9
GO TO 10
9 WHLDF=2
WHLDB=N
M=1
N=1
10 IF (OPRAM.LT.0) AND (PARAM.LT.PARAMF) PARAM=PARAMF
IF (OPRAM.GT.0) AND (PARAM.GT.PARAMF) PARAM=PARAMF
IF (OPRAM.EQ.PARAM) AND (NCNVGB.EQ.1) OPRAM=PARAM-OPRAM1
IF (OPRAM.EQ.PARAM) AND (NCNVGB.EQ.2) OPRAM=PARAM-OPRAM2
IF (OPRAM.EQ.PARAM) AND (NCNVGB.EQ.3) OPRAM=PARAM-OPRAM3
PRINT 138
SELECT REAL PARAMF
GO TO (11,12,13,14,15), INCRMT
11 TPADAM
GO TO 16
12 ALPHAD=PARAM
GO TO 16
13 THETA=PARAM
GO TO 16
14 STMACH=PADAM
GO TO 16
15 GAMMA=PADAM
GO TO 16
16 CONTINUE
PRINT 136, STMACH,GAMMA,T,THETA,ALPHAD
IF (NPLOT.EQ.1) PUNCH 152, STMACH,GAMMA,T,THETA,ALPHAD,SLOPE
IF (NPLOT.EQ.1) PUNCH 135, N,M,KTRANSF
PRINT 141, PPSIGOM
PRINT 154, AAST
PRINT 156, VTEST,VTFCTI
IF (M2E.EQ.0) PRINT 180, M2E
IF (M2E.EQ.1) PRINT 179, M2E,TU
PRINT 160, SLOPE,KTRANSF
THETA=THETA/RAD
ALPHAD=ALPHAD/RAD
PROGRAM MAIN(INPUT,OUTPUT,TAPE5=INPUT,PUNCH) A 10 C
CONICAL FLOW ABOUT ELLIPTIC CONES BY THE METHOD OF LINES WITH A 20 C
INCREMENTATION OF A PARAMETER A 30 C
COMMON F(3),DF(3),FC(3),DFC(3),AB1(3),AB2(3),AB3(3),AB4(3) A 60 C
COMMON FU(20,6),DFU(20,6),FUC(20,6),DFUC(20,6),B1(20,6),B2(20, A 70
16),B3(20,6),B4(20,6) A 80
COMMON SBAR(20),DSB(20),SBARP(20),DSBP(20),DSB2(20),DSB3(20),DSB A 90
14(20),X(20),XO(20),YO(20),A1(20),A2(20),A3(20),A4(20),A5(20),A6(2 A 100
20),A7(20),A8(20),AKR(20),GX(20),GY(20),GXX(20),GYY(20),GXY(20),ETA A 110
3(20),ETAS(20),ETASP(20),RFTAD(20),RHO(20),R(20),P(20),U(20),V(20), A 120
W(20),WP(20),UP(20),VP(20),WP(20),XS(20),YS(20),DUDZ(20),DPDZ(20), A 130
SDVZ(20),DWDZ(20),AM(20),S(20),ZETA1(20),ZETA2(20),ZETA3(20),ZETA4 A 140
6(20),DU1(20),DU2(20),DU3(20),DU4(20),DU1(20),DU2(20),DU3(20),DU4(2 A 150
70),DU1(20),DU2(20),DU3(20),DU4(20),G(20),PSID(20),DP1(20),DP2(20), A 160
BDP3(20),DPA(20),DEONS(20),CROSSM(20),POROGAM(20),O(20),OH(20),PS15 A 170
90(20),BERNOUL(20),XSRAM(20),YS9AR(20),RHOISEN(20),UISEN(20) A 180
COMMON XOBAR(20),YOBAR(20),XBAR(20),YBAR(20),TAU(20),G2B(20),DPDZE A 190
1X(20) A 200
COMMON KTRANSF,SLOPE A 210
COMMON AAST,B11,B12,B13,B21,B22,B23,NSPACE,P1,M,N,L1,T,THETA,R,GAMM A 220
1A,DX1,CON1,CON2,STMACH,AB,A11,A12,A13,A21,A22,A23,A31,A32,A33,ALPH A 230
2AR,N1,NDRIBG,M,H,K,S,IPRA,IRAD,NF,NLINES,EPSIG,NPRINT,SPACER,NEXTMAP, A 240
JPSIGOM,PPSINT,DFD,XIN,SI,OPM) A 250
COMMON /BLOCKN/ DNDX1,WP1,WP2,WP3,WP4 A 260
COMMON /ERROR/ ER(12),ERR(12),PLK(12) A 270
COMMON VCC(20),VCC(20),CPHOCK(20),CP1(20),SARHLD(20),XRHLD(20),YB A 280
1HL(20),UC(20),VC(20),WC(20),X(20),Y(20),THEINOR(20),PSINH(20), A 290
2OPRT(20),PTOPT(120),PT(120),POASTO(20),POPINF(20),CPHODY(20) A 300
DIMENSION DMOLD(20,20) A 310
COMMON /BLOCK1/ ISL,NCYCLF,INCOUNT,ISIGN A 320
COMMON /BLOCK2/ NA,NR,ANA,NR,M2E,TU A 330
COMMON /BLOCK6/ NFG A 340
COMMON BLOCK1 NEEDED IN MP,LRANGE,ERRV2 A 360
COMMON BLOCK2 NEEDED IN MP,LRG A 370
DATA (ER(1),I=1,12)/,3ER1,3HEH2,3HER3,3HER4,3HER5,3HER6,3HEH7,3HEH A 380
1R,3HER9,4HER10,4HER11,4HER12/ A 390
DATA (ER(1),I=1,12)/,4HER13,4HER14,4HEH15,4HER16,4HER17,4HER18,4HE A 400
190,4HER19,4HER20,4HER21,4HEH22,4HEH23,4HER24,4HER25,4HER26,4HE A 410
DATA (HLK(1),I=1,12)/,4HLK1,4HLK2,4HLK3,4HLK4,4HLK5,4HLK6,4HE A 420
1LK7,4HLK8,4HLK9,4HLK10,4HLK11,4HLK12/ A 430
DIMENSION STASO(20), VO(20), D(20,20), B(20,12), PIVOT(20), DETA(2 A 440
10), XREAL(20), YREAL(20), X(20), Y(20), ETAS(20), ETAS2(20), ETAS A 450
2(20), F1(20), F1(20), F2(20), F2(20), F3(20), F3(20), F4(20), F4(2 A 460
10),VALENCE(0,DEFIN) A 470
CALL DAYTIM (DATE) A 480
PRINT 139, IDATE A 490
PRINT 138 A 500
PRINT 139, IDATE A 510
PRINT 172 A 520
PRINT 173 A 540
PRINT 174 A 550
PADM=7,206770E1 A 560
P1=7,1815026E3 A 570
EPSIGOM=.001 A 580
PARAM=1.0 A 590
NDRIBG=1 A 600
ISL=1 A 610
M2E= A 620
NSPAC=NDP A 630
WHLDB= A 640
M=0 - ZERO-INCIDENCE (CIRCULAR CONE A 650
M=2 - CIRCULAR-ELLIPTEIC AND BI-ELLIPTIC CONES A 670
C INCRMT=1 INCREMENT T A 680
C INCRMT=2 INCREMENT ALPHA A 690
C INCRMT=3 INCREMENT THETA A 700
C INCRMT=4 INCREMENT STMACH A 710
C INCRMT=5 INCREMENT GAMMA A 720
C IPRINT=1 PRINTS CONVERGED VALUES FOR EACH PARAMETER A 730
C IPRINT=2 PRINTS CONVERGED VALUES ONLY FOR FINAL PARAMETER A 740
C (A) IDENTITY TRANSFORMATION, KTRANSF=1, SLOPE=1 A 750
C (R) HIGH DENSITY OF LINES AT LEADING EDGE, KTRANSF=2, SLOPE LT 1, A 760
C (C) HIGH DENSITY OF LINES AT NODAL POINT, KTRANSF=3, SLOPE LT 1, A 770
C A 780
1 READ (5,134) STMACH,GAMMA,T,THETA,ALPHAD A 790
IF (ENPFILE 5) 137,2 A 800
2 CONTINUE A 810

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APPENDIX A

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RANGLE=ALPHAR/ATAN(TAN(THETAR))
PRINT 167, RANGLE
A=PI*TAN(THETAR)**2
IF (M=EQ.1) A=PI/2.*TAN(THETAR)**2*(TU+T)
GAMX1=/GAMMA
AA1=/((GAMMA*STMACH**2)
PTINF=AA*(1.+(GAMMA-1)/2.*STMACH**2)**(GAMMA/(GAMMA-1.))
SINALP=SIN(ALPHAR)
COSALP=COS(ALPHAR)
C SELECTION OF BODY GEOMETRY #=0 - ZERO-INCIDENCE CIRCULAR CONE.
C #=2 CIRCULAR AND ELLIPTIC CONES
IF (L1.EQ.1.AND.M.EQ.2) THOLD=T
IF (L1.EQ.1.AND.M.EQ.2) THETHLD=THETAR
IF (L1.EQ.1.AND.M.EQ.2) EPSIMLD=EPSIGOM
IF (M.EQ.0) GO TO 18
IF (M.EQ.2.AND.L1.EQ.1) GO TO 19
IF (M.EQ.2.AND.L1.NE.1) GO TO 17
17 IF (ABS(THOLD-T).GT.1.E-05.OR.ABS(THETHLD-THETAR).GT.1.E-05) GO TO
    18
    GO TO 20
18 CALL RC
    IF (NCONVRG.EQ.0.AND.NREAD.EQ.0.AND.L1.EQ.1) GO TO 19
19 CALL APPROX
C INITIAL VALUES OF INTEGRATION PARAMETERS
20 J=0
    DE0=1.0
    NCRG=1
    NCONINT=0
    NCYCLE=1
    NPIV=0
    NPRINT=1
    ISIGM=500
    ISIGMA=500
    EPSIGM=.001
    EPSIGMA=.025
    NMAX=20
    INTSTEP=0
    NLNFS=N
A1700 CALL SHOCK (I)
A1710 UNDRHO=ABS(V1)*COS(CIGMA)*W1)*SIN(SIGMA)*.5
A1720 IF (I.FO.1) VMXTEST=UNDRHO
A1730 IF (I.GT.1.AND.UNDRHO.LT.VMXTEST) VMXTEST=UNDRHO
A1740 CP(1)=2.*(P(1)-1./GAMMA*STMACH**2)
A1750 IF (P(1).LT.0) GO TO 105
A1760 CRSHOCK(I)=CP(I)
A1770 26 CONTINUE
A1780 IF (7.LT.I-0) GO TO 27
A1790 GO TO 32
A1800 27 DO 29 I=1,N
A1810 I=I-1
A1820 I=I-2
A1830 IF (I.EQ.1) I=2
A1840 IF (I.FO.1) I=3
A1850 IF (I.FO.2) I=1
A1860 IF (I.FO.2) I=2
A1870 IF (SBAR(I).LT.SBAR(I=1).AND.SBAR(I=1).GT.SBAR(I=2)) GO TO 28
A1880 GO TO 29
A1890 28 J=I
A1900 J=I-1
A1910 J=I-2
A1920 29 CONTINUE
A1930 DENOM=(X(J)-X(J=1))*SBAR(J=2)-(X(J)-X(J=2))*SBAR(J=1)+(X
A1940 I(J=1)-X(I(J=2))*SBAR(J))
A1950 NUM=(X(I(J=1))*SBAR(J=2)-(X(I(J=2))*SBAR(J=1)+(X(I
A1960 I=1)-X(I(J=2))*SBAR(J))
A1970 XIST=.5*(NUM/DENOM)
A1980 IF (J.NE.2) GO TO 30
A1990 XIST=C
A2000 SBARMX=SBAR(J)
A2010 GO TO 31
A2020 30 CONTINUE
A2030 TERM1=(X(I=1)-X(I(J=1)))*(XIST-X(I=1))*SBAR(J=2)/(X(I(J=2))-X(I(J=1)
A2040 1)*(X(I(J=2))-X(I(J=1)))
A2050 TERM2=(X(I=2)-X(I(J=2)))*(XIST-X(I=2))*SBAR(J=1)/(X(I(J=1))-X(I(J=2)
A2060 1)*(X(I(J=1))-X(I(J=2)))
A2070 TERM3=(X(I=3)-X(I(J=3)))*(XIST-X(I=3))*SBAR(J)/(X(I(J=1))-X(I(J=2))*
A2080 1*(X(I(J=2))-X(I(J=1)))
A2090 SBARMX=TERM1+TERM2+TERM3
A2100 31 DGAM=AA*EXP(SBARMX)
A2110 32 IF (NPRINT.EQ.1.AND.NPIV.FO.0) GO TO 33
A2120 GO TO 34
A2130 33 PRINT 157, (ETASP(I),I=1,N)
A2580
A2590
A2600
A2610
A2620
A2630
A2640
A2650
A2660
A2670
A2680
A2690
A2700
A2710
A2720
A2730
A2740
A2750
A2760
A2770
A2780
A2790
A2800
A2810
A2820
A2830
A2840
A2850
A2860
A2870
A2880
A2890
A2900
A2910
A2920
A2930
A2940
A2950
A2960
A2970
A2980
A2990
A3000
A3010
A2140 PRINT 165, EPSIG, EPSIGM, SPACER, EPSIVAR, EPSINT
A2150 IF (NCONVRG.EQ.1.AND.L1.EQ.1) GO TO 132
A2160 IF (NCONVRG.EQ.2.AND.L1.EQ.1) GO TO 17
A2170 IF (NCONVRG.EQ.3.AND.L1.EQ.1) GO TO 18
A2180 132 COMPUTE INITIAL VALUES FOR INTEGRATION
A2190
A2200
A2210
A2220
A2230
A2240
A2250
A2260
A2270
A2280
A2290
A2300
A2310
A2320
A2330
A2340
A2350
A2360
A2370
A2380
A2390
A2400
A2410
A2420
A2430
A2440
A2450
A2460
A2470
A2480
A2490
A2500
A2510
A2520
A2530
A2540
A2550
A2560
A2570
A3020 PRINT 198, (CP(I),I=1,N)
A3030 34 IF (NDEBUG.EQ.0) PRINT 143, (I,U(I),P(I),V(I),W(I),I=1,N)
A3040
A3050 DUMMY INITIALIZATION OF EXTRAPOLATION PARAMETERS
A3060
A3070
A3080
A3090
A3100
A3110
A3120
A3130
A3140
A3150
A3160
A3170
A3180
A3190
A3200
A3210
A3220
A3230
A3240
A3250
A3260
A3270
A3280
A3290
A3300
A3310
A3320
A3330
A3340
A3350
A3360
A3370
A3380
A3390
A3400
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A3420
A3430
A3440
A3450
A3460
A3470
A3480
A3490
A3500
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APPENDIX A

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FUN(1.6)=SBAR(1)
DFUN(1)=DZETA
FUNC(1)=U(1)
36 CONTINUE
      INTEGRATE EQUATIONS FROM ZETA=1 TO ZETA=0
      DO 5A INTENT=1,100000
      CALL DERIVZ (DZETA,ND)
      IF (NEG.FO,0.0) GO TO 105
      IF (NEG.EQ,0.0) GO TO 105
37 IF (NPRINT.NE.2) GO TO 66
      NSB=1
      EPS1=5E-01
      SBTEST=1.E-08
      NSBCNT=0
      SBRCN=SBARMX
      DO 3R I=1,N
      ZFA=FUN(1.1)
      U(1)=FUN(1.2)
      P(1)=FUN(1.3)
      V(1)=FUN(1.4)
      W(1)=FUN(1.5)
      SBAR(1)=FUN(1.6)
      DZETA=DFUN(1.1)
      DUZ(1)=DFUN(1.2)
      DDZ(1)=DFUN(1.3)
      IF (ZETA.NE.0.0) DVZ(1)=DFUN(1.4)
      DWZ(1)=DFUN(1.5)
      DSBRZ(1)=DFUN(1.6)
38 CONTINUE
      UMW(1)
      RHO=RHOD(1)
      SW=SBAR(1)
      PORGAM=POROGAM(1)
      UL=U(N)
      RHL=RHOD(N)
      SL=SBAR(N)
      PORGAML=POROGAM(N)
      IF (T.FO.1.) PGAM=POROGAMW
      W(1)=0.
      W(N)=W(1)
      NTIMES=1
      IF (ZFA.NE.0.0) GO TO 62

      IF (W.FO.1) GO TO 62
      IF (W2.EQ.1) GO TO 42
CORRECT SURFACE QUANTITIES AT ZETA=0
      EPS1=EN1.E-05
      TERM1=(1.+2./((GAMMA-1.)*STNACH**2))/AASTSO
      FAC=(2.*GAMMA)/((GAMMA-1.)*AASTSO)
      IF (W.EQ.2.AND.T.GT.1.) GO TO 39
      ISIGNP=ISIGN+1
      LMT=1
      LMT=N
      GO TO 42
39 DO 40 I=1,NM1
      IF (W(1).GE.0.0.AND.W(1)+LT.0.0) GO TO 41
40 CONTINUE
      ISIGN=500
      ISIGNP=ISIGN+1
      LMT=1
      LMT=N
      GO TO 42
41 ISIGN=1
      ISIGNP=ISIGN+1
      LMT=1
      LMT=ISIGN
      ISIGNH=ISIGN
42 NPNHLD
      ISIGNH=ISIGN
      DO 43 I=LMT,1,LMT
      IF (Y(LT,1.) RHO(1)=P(1)/PGAM**GAMW
      IF (Y.EQ.1.) RHO(1)=P(1)/PORGAM**GAMW
      IF (Y.GT.1.AND.ISIGN.EQ.500) RHO(1)=P(1)/PORGAM**GAMW
      IF (Y.GT.1.AND.ISIGN.NE.500.AND.I.GE.1.AND.I.LE=ISIGN) RHO(1)=P(1)/PORGAM**GAMW
      IF (Y.GT.1.AND.ISIGN.NE.500.AND.I.GE.1.AND.I.LE=ISIGN) RHO(1)=P(1)/PORGAM**GAMW
      IF (Y.GT.1.AND.ISIGN.NE.500.AND.I.GE.1.AND.I.LE=ISIGN) RHO(1)=P(1)/PORGAM**GAMW
      U(1)=SORT(TERM1-FAC*P(1)/RHO(1)-W(1)**2)
43 CONTINUE
      RSH(1)=E-08
      NSTOP=0
      ISL=2
      GO TO 52
44 DO 44 I=LMT,1,LMT
      A3460
      A3470
      A3480
      A3490
      A3500
      A3510
      A3520
      A3530
      A3540
      A3550
      A3560
      A3570
      A3580
      A3590
      A3600
      A3610
      A3620
      A3630
      A3640
      A3650
      A3660
      A3670
      A3680
      A3690
      A3700
      A3710
      A3720
      A3730
      A3740
      A3750
      A3760
      A3770
      A3780
      A3790
      A3800
      A3810
      A3820
      A3830
      A3840
      A3850
      A3860
      A3870
      A3880
      A3890
      F(1)=TERM1-FAC*P(1)/RHO(1)-U(1)**2-UP(1)**2
      UISEN(1)=U(1)
45 CONTINUE
      JTFMD=0
      DO 4R J=LMT,1,LMT
      I=LMT,1
      JTFMD=1
      JTFMD=JTFMD+1
46 U(J)=1.+EPSIU)*UISEN(J)
      NPNHLD
      IF (ISIGN.NE.500.AND.NTIMES.EQ.1.AND.I.FO.ISIGN) NP=3
      IF (ISIGN.NE.500.AND.NTIMES.EQ.2.AND.I.FO.ISIGN+1) NP=3
      CALL LGRANGE (1, NP, N, NINES, NDEBUG, X(1), X(1)+X.Y, DYDX)
      IP(1)=GCR(1)+DYDX
      F(1)=TERM1-FAC*P(1)/RHO(1)-U(1)**2-UP(1)**2
      DFID(I,J)=(F(1)-F(1))/EPSIU*UISEN(J)
      DFID(I,TEMP)=DFID(I,J)
      IF (I.FO.LMT) GO TO 47
      I=1
      ITFMD=ITFMD+1
      GO TO 46
47 U(J)=UISEN(J)
48 CONTINUE
      IF (ISIGN.EQ.400) NXYZ=N
      IF (ISIGN.NE.400.AND.NTIMES.EQ.1) NXYZ=ISIGN
      IF (ISIGN.NE.400.AND.NTIMES.EQ.2) NXYZ=ISIGN
      ITFMD=0
      DO 49 I=LMT,1,LMT
      ITFMD=ITFMD+1
49 R(ITFMD,1)=F(1)
      CALL SIFD (DFIDU,NXYZ,2,1,DFTERM,PIVOT,NMAX,ISCALE)
      ITFMD=0
      DO 50 I=LMT,1,LMT
      ITFMD=ITFMD+1
50 U(1)=UISEN(1)+R(ITFMD,1)
      ITFMD=0
      DO 51 I=LMT,1,LMT
      ITFMD=ITFMD+1
      IF (RSH(1).ITFMD,1),GT,PPISFN) GO TO 52
51 CONTINUE
      GO TO 59
52 DO 53 I=LMT,1,LMT
      NPNHLD=0
      IF (ISIGN.NE.500.AND.NTIMES.EQ.1.AND.I.FO.ISIGN) NP=3
      A4340
      A4350
      A4360
      A4370
      A4380
      A4390
      A4400
      A4410
      A4420
      A4430
      A4440
      A4450
      A4460
      A4470
      A4480
      A4490
      A4500
      A4510
      A4520
      A4530
      A4540
      A4550
      A4560
      A4570
      A4580
      A4590
      A4600
      A4610
      A4620
      A4630
      A4640
      A4650
      A4660
      A4670
      A4680
      A4690
      A4700
      A4710
      A4720
      A4730
      A4740
      A4750
      A4760
      A4770
      IF (ISIGN.NE.400.AND.NTIMES.EQ.2.AND.I.FO.ISIGN+1) NP=3
      CALL LGRANGE (1, NP, N, NINES, NDEBUG, X(1), X(1)+X.Y, DYDX)
      IF (I.GE.2) I=I+DYDX
      IF (ISIGN.NE.400.AND.NTIMES.EQ.1) GO TO 54
      GO TO 58
54 DO 54 I=LMT,1,LMT
      IF (I.FO.1.) GF.FO.AND.(P(1)+LT.0.0) GO TO 56
55 CONTINUE
56 ISIGN=1
      ISIGNP=ISIGN+1
      IF (ISIGN=ISIGNH) 57,58,57
57 LMT=1
      LMT=ISIGN
      NTIMES=1
      GO TO 42
58 U(1)=U(1)
      N4STOP=NSTOP+1
      IF (N4STOP,GT,25) PRINT 166, N4STOP
      IF (N4STOP,GT,25) GO TO 59
      GO TO 44
59 DO 59 I=LMT,1,LMT
      W(1)=U(1)
      POROGAM(1)=P(1)/RHO(1)**GAMMA
      SBAR(1)=ALOG(GAMMA*STNACH**2/POROGAM(1))
      DENOM=ISIGNP/(GAMMA**P(1)/RHO(1))
      CRSCM(1)=ABS(W(1))/DENOM**AAST
      ASOFCMAM=FUN(1.3)/RHO(1)
      RUSO=U(1)**2+V(1)**2+W(1)**2
      AM(1)=SORT(AAST**2+RUSO/ASO)
      DENOM=1.+2./((GAMMA-1.)*STNACH**2)
      BERNUL(1)=1.-2.*GAMMA*FUN(1.3)/RHO(1)*((GAMMA-1.)*RUSO**AAST**2)
      I/JORNM
      ASOFCAMMA=FUN(1.3)/RHO(1)
      ASO=ASO/AASTSO
      WDA=U(1)**2+V(1)**2+W(1)**2
      DVZ(1)=CTAS(1)*((1.-WDA)*W(1)+U(1)**2.-WDA)
      DDPZ(1)=CTAS(1)*RHO(1)**2*AASTSO*AKR(1)
59 CONTINUE
      IF (LMT.FO.N) ISIGN=500
      IF (LMT.EQ.N) GO TO 41
      LMT=ISIGNP
      I=LMT
      IF (ISIGN.EQ.NM1,00,ISIGN.FO.N) GO TO 61
      NTIMES=2
      A4780
      A4790
      A4800
      A4810
      A4820
      A4830
      A4840
      A4850
      A4860
      A4870
      A4880
      A4890
      A4900
      A4910
      A4920
      A4930
      A4940
      A4950
      A4960
      A4970
      A4980
      A4990
      A5000
      A5010
      A5020
      A5030
      A5040
      A5050
      A5060
      A5070
      A5080
      A5090
      A5100
      A5110
      A5120
      A5130
      A5140
      A5150
      A5160
      A5170
      A5180
      A5190
      A5200
      A5210

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APPENDIX A

GO TO 42
ND=NDHLI)
KIGW=EQO
COMPUTE SPECIAL QUANTITIES FOR PRINTOUT
DO 70 I=1,N
IF (ZETA=EQ.O) FTA(I)=0.0
...
PUNCH 152, (XBAR(I),I=1,N)
PUNCH 152, (YBAR(I),I=1,N)
PUNCH 152, (PSID(I),I=1,N)
PUNCH 152, (CPODY(I),I=1,N)
PUNCH 152, (U(I),I=1,N)
PUNCH 152, (W(I),I=1,N)
PUNCH 152, (RHO(I),I=1,N)

APPENDIX A

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      NO 03 I=1,N
02 FTAS(I)=FTAS(I)
      GO TO 95
03 NO 04 I=1,N
      FTAS(I)=FTAS(I)
      FTAS(I)=FTAS(I)
04 FTAS(I)=FTAS(I)
      PARAM=PARAM2
      PARAM2=PARAM3
      DPARAM=DDPARAM
05 IF (DPRAM.LT.O.C.AND.PPARAM.DPRAM.LT.PPARAM) GO TO 96
      IF (DPRAM.GT.O.C.AND.PPARAM.DPRAM.GT.PPARAM) GO TO 96
      GO TO 97
06 PARAM=PARAMF
      GO TO 98
07 DPARAM=DDPARAM
08 COEFF1=(PARAM-PARAM2)/(PARAM-PARAM3)/(PARAM-PARAM1)
      COEFF2=(PARAM-PARAM1)/(PARAM-PARAM3)/(PARAM-PARAM1)
      COEFF3=(PARAM-PARAM1)/(PARAM-PARAM3)/(PARAM-PARAM1)
      COEFF4=(PARAM-PARAM1)/(PARAM-PARAM3)/(PARAM-PARAM1)
09 NO 09 I=1,N
      ETAS(I)=COEFF*ETAS(I)+COEFF2*ETAS2(I)+COEFF3*ETAS3(I)
      GO TO 132
      HEADING PRINTOUT FOR TAYLOR-MACCOLL
100 PRINT 148
      PRINT 136. STMACH,GAMMA,T.THETA,D.ALPHAD
      PRINT 141. EPSIGOM
      PRINT 137. N,M,NREAD,NSPACE,ND,NCNVRG
      PRINT 156. VTEST,VTEST1
      IF (M2.EQ.0) PRINT 180. M2E
      IF (M2.EQ.1) PRINT 179. M2E,TU
      PRINT 160. SLOPE,KTRANSF
      PRINT 153. KCOUNT,VMAX,EPSIG,SPACER,VMXTEST
      IF (DPRAM.LT.O.C.AND.PPARAM.NE.PPARAM) PRINT OUT ONLY AT ZETA=0
      IF (DPRAM.EQ.2.AND.PPARAM.NE.PPARAM) GO TO 37
      COMPLETE PRINT OUT FROM ZETA=1 TO ZETA=0
      GO TO 103
      HEADING PRINTOUT FOR M=2 BODY
101 CONTINUE
      PRINT 138
      PRINT 137. N,M,NREAD,NSPACE,ND,NCNVRG
      PRINT 165. NAL,NAN,NP,NR
      PRINT 136. STMACH,GAMMA,T.THETA,D.ALPHAD
      PRINT 167. RANGLE
      PRINT 165. EPSIG,EPSIGMX,SPACER,EPSIVAR,EPSINT
      PRINT 178. NCYCLE,VTEST,VTEST1,VMAX,AAST,PTRF
      PRINT 156. VTEST,VTEST1
      IF (M2.EQ.0) PRINT 180. M2E
      IF (M2.EQ.1) PRINT 179. M2E,TU
      PRINT 160. SLOPE,KTRANSF
      PRINT 153. KCOUNT,VMAX,EPSIG,SPACER,VMXTEST
      PRINT 140
      LPRINT=2
      CALL PRINT (NLINEP,LPRINT,ZETA,DZETA,NP,NPLOT,NZETA)
      IF (DPRAM.EQ.2.AND.PPARAM.NE.PPARAM) PRINT OUT ONLY AT ZETA=0
      IF (DPRAM.EQ.2.AND.PPARAM.NE.PPARAM) GO TO 37
      COMPLETE PRINT OUT FROM ZETA=1 TO ZETA=0
      GO TO 103
      VARIATION OF SHOCK DISTANCE FOR NEWTON-RAPHSON COMPUTATION OF SHOC
      NCOUNT - COUNTER OF PIVOTAL AND VARIATION INTEGRATIONS NCOUNT =1
102 NCOUNT=NCOUNT+1
      KCOUNT=KCOUNT+1
      NPIV=NPIV+1
      IF (NCOUNT.GT.1) GO TO 112
      PIVOTAL RUNS
103 DO 104 I=1,N
      VO(I)=FUN(I,4)
      IF (I.EQ.1) VMAX=ABS(VO(I))
      IF (ABS(VO(I)).GT.VMAX) VMAX=ABS(VO(I))
104 ETAS(I)=ETAS(I)
      A6980
      A6990
      A7000
      A7010
      A7020
      A7030
      A7040
      A7050
      A7060
      A7070
      A7080
      A7090
      A7100
      A7110
      A7120
      A7130
      A7140
      A7150
      A7160
      A7170
      A7180
      A7190
      A7200
      A7210
      A7220
      A7230
      A7240
      A7250
      A7260
      A7270
      A7280
      A7290
      A7300
      A7310
      A7320
      A7330
      A7340
      A7350
      A7360
      A7370
      A7380
      A7390
      A7400
      A7410
      A7420
      A7430
      A7440
      A7450
      A7460
      A7470
      A7480
      A7490
      A7500
      A7510
      A7520
      A7530
      A7540
      A7550
      A7560
      A7570
      A7580
      A7590
      A7600
      A7610
      A7620
      A7630
      A7640
      A7650
      A7660
      A7670
      A7680
      A7690
      A7700
      A7710
      A7720
      A7730
      A7740
      A7750
      A7760
      A7770
      A7780
      A7790
      A7800
      A7810
      A7820
      A7830
      A7840
      A7850
      IF (VMAX.GT.VMXTEST) GO TO 105
      IF (NPIV.EQ.2) GO TO 111
      IF (NPIV.EQ.1.AND.NPIV.EQ.1) PRINT 153. KCOUNT,VMAX,EPSIG,SPACER
      VMXTEST
      NSKIP=1 IS THE MODIFIED NEWTON METHOD (D(I,J) NOT RECOMPUTED)
      IF (NSKIP.EQ.1) GO TO 116
      IF (EPSIG.EQ.EPSIGMX) GO TO 111
      NCOUNT=0
      GO TO 21
      DECREASE PARAM INCREMENT AND RESTART FROM LAST CONVERGED SOLUTION
105 IF (NCNVRG.EQ.2) GO TO 106
      IF (NCNVRG.EQ.1) GO TO 107
      IF (NCNVRG.EQ.2) GO TO 109
      IF (NCNVRG.EQ.3) GO TO 110
106 PRINT 179
      STOP 777A
107 DPARAM=PARAM-DPRAM
      DPARAM=.5*DPRAM
      NO 108 I=1,N
      FTAS(I)=FTAS(I)
      GO TO 81
109 DPARAM=PARAM-DPRAM
      DPARAM=.5*DPRAM
      IF (DPRAM.LT.O.C.AND.DPRAM.GT.DPRMIN) STOP 7777
      IF (DPRAM.GE.O.C.AND.DPRAM.LT.DPRMIN) STOP 7777
      GO TO 86
110 DPARAM=PARAM-DPRAM
      DPARAM=.5*DPRAM
      IF (DPRAM.LT.O.C.AND.DPRAM.GT.DPRMIN) STOP 7777
      IF (DPRAM.GE.O.C.AND.DPRAM.LT.DPRMIN) STOP 7777
      GO TO 87
      DECREASE FTAS(I) VARIATION
111 ETAS(J+1)=ETAS(J+1)*(1+EPSIVAR)
      GO TO 21
      A7860
      A7870
      A7880
      A7890
      A7900
      A7910
      A7920
      A7930
      A7940
      A7950
      A7960
      A7970
      A7980
      A7990
      A8000
      A8010
      A8020
      A8030
      A8040
      A8050
      A8060
      A8070
      A8080
      A8090
      A8100
      A8110
      A8120
      A8130
      A8140
      A8150
      A8160
      A8170
      A8180
      A8190
      A8200
      A8210
      A8220
      A8230
      A8240
      A8250
      A8260
      A8270
      A8280
      A8290
      A8300
      A8310
      A8320
      A8330
      A8340
      A8350
      A8360
      A8370
      A8380
      A8390
      A8400
      A8410
      A8420
      A8430
      A8440
      A8450
      A8460
      A8470
      A8480
      A8490
      A8500
      A8510
      A8520
      A8530
      A8540
      A8550
      A8560
      A8570
      A8580
      A8590
      A8600
      A8610
      A8620
      A8630
      A8640
      A8650
      A8660
      A8670
      A8680
      A8690
      A8700
      A8710
      A8720
      A8730
      A8740
      A8750
      A8760
      A8770
      A8780
      A8790
      A8800

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APPENDIX A

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IF (NTERM.GF.N) GO TO 126
IF (NCNVRG.EO.O) STOP 6666
IF (NCNVRG.FO.1) GO TO 124
DPRM=DPDPRM+DPRM
DPRM=.5*DPRM
PARAM=PARAM+DPRM
GO TO 125
124 PARAM=PARAM-DPRM
DPRM=.5*DPRM
PARAM=PARAM+DPRM
GO TO 126
125 IF (NCNVRG.FO.2) GO TO 87
IF (NCNVRG.FO.3) GO TO 98
126 DO 127 I=1,N
127 FTAS(I)=ETAS(I)
GO TO 132
128 DO 129 I=1,N
129 DETA(I)=PI(I)
130 PRINT 150, (DETA(I),I),N)
J=0
NEXCY=NEXCY+1
NCNMT=0
NPIV=0
DO 141 I=1,N
131 ETAS(I)=ETAS(I)+DETA(I)
GO TO 21
132 CONTINUE
GO TO 11
133 CALL DRYTIM (IDATE)
PRINT 160, IDATE
STOP 010

174 FORMAT (A14,R)
135 FORMAT (A14)
136 FORMAT (8H STMACH=E16.8,2X,6HGAMMA=E16.8,2X,2HTF=E16.8,2X,7HTHETAD=
      I E16.8,2X,7HALPHAD=E16.8/)
137 FORMAT (2H N=12,2X,2HM=11,2X,6HNREAD=11,2X,7HNSPACE=11,2X,3HNPI=2,
      12X,7HNCNVRG=11)
138 FORMAT (1H1//)
139 FORMAT (2A10//)
140 FORMAT (/)
141 FORMAT (9H PPSIGOM=E16.8)
142 FORMAT (1X16.15/(A16,R))

48740 16.8,2X,6HPI=E16.8/)
48750 170 FORMAT (/5H M2F15.2X,3HTU=E16.8/)
48760 180 FORMAT (/5H M2F14/)
48770 SUBROUTINE RG
48780 R=10
48790 R=20
48800 R=30
48810 R=40
48820 R=50
48830 COMMON FUN1(20.5),DFUN(20.5),FUNC(20.5),DFUNC(20.6),B(120.6),B2(20.
      16),R1(20.6),R4(20.6)
48840 COMMON SBAR(20),DSEBZ(20),SBARR(20),DSR(20),DSB2(20),DSR3(20),DSR
      14(20),XI(20),XO(20),YO(20),A1(20),A2(20),A3(20),A4(20),A5(20),A6(2
      20),A7(20),A8(20),A9(20),G1(20),G2(20),G3(20),GY(20),GX(20),ETA
      2(20),FTAS(20),FTASPR(20),FBTAN(20),QH(20),Q(20),PI(20),MU(20),W(20),
      4W(20),PP(20),UP(20),VP(20),WP(20),XS(20),YS(20),ZETA(20),DPDZ(20),
      50VDZ(20),DWDZ(20),AM(20),S(20),ZETA1(20),ZETA2(20),ZETA3(20),ZETA4
      6(20),DU1(20),DU2(20),DU3(20),DU4(20),DU1(20),DU2(20),DU3(20),DU4(2
      7),DV1(20),DV2(20),DV3(20),DV4(20),S1(20),PS1(20),S2(20),DP2(20),
      8DP3(20),DP4(20),DEDN(20),CHOSM(20),PHOGAM(20),O1(20),O2(20),PS15
      9(20),SERNDK(20),XSEAR(20),YSEAR(20),HMOISEN(20),LMOISEN(20)
      COMMON XOBAR(20),YOBAR(20),XEAR(20),YEAR(20),TAU(20),GB2(20),DPDZE
      1X(20)
      COMMON KTOANSP,SLOPE
      COMMON AAST,R11,R12,R13,H21,R22,R21,NSPACE,PI,M,N,L1,T,THETAR,GA,M
      1A,DX,CON1,CON2,STMACH,AL,A11,A12,A13,A21,A22,A23,A31,A32,A33,ALPH
      2AR,N1,N2,FRUG,N,K,5,GM,NF,NL,NF3,PSIGON,PRINT,SPACE,NEXTRAP
      3
      EPSIGOM=PSIGON,DPD,XI,N1,CNPI
      4
      COMMON PERROB,SR(12),CRR(12),JUL(12)
      COMMON VCC(20),VCC(20),CPHOC(20),CP(20),SBARHL(20),XPHLD(20),YH
      5HLD(20),UC(20),VC(20),WC(20),VX(20),VY(20),THETNR(20),PSINUP(20),
      62POPI(20),PIODT(20),PT(20),PDA1(20),POPINF(20),CPHOY(20)
      COMMON /BLOCK2/ NA,NB,ANA,ENB,42P,TU
      DIMENSION IDATE(2)
      TITLE
      NTI=5E+1
      NF=2
      AB=ANITHETAR)
      NI=N+1/2
      RNDY=RELFCTIOM
      IF (M.EO.O) GO TO 1
      IF (W.FO.2) GO TO 2

49180 C
49190 C
49200 C
49210 TAYLOR-MACCOLL
49220 I=1
49230 XI(I)=0.0
49240 X(I)=0.0
49250 Y(I)=0.0
49260 Y(I)=0.0
49270 DIM(1+2*N)
49280 GY(1)=2*N
49290 GX(1)=2*N
49300 GY(1)=0.0
49310 IF (NDEBUG.EO.O) PRINT 46, I,X(I),Y(I),Y(I)
49320 IF (NDEBU.EO.O) PRINT 45, I,GX(I),GY(I),GX(I),GY(I)
49330 GO TO 36
49340 NSTEP=2
49350 C
49360 C CIRCULAR AND ELLIPTIC CONE - COMPUTATION OF XI(I)
49370 C
49380 NINT=1
49390 NQUAD=0
49400 F(1)=0.0
49410 F(2)=0.0
49420 DS=0.1*AB
49430 DF(1)=DS
49440 C
49450 C INTEGRATION WITH XO OR YO INDEPENDENT VARIABLE - NINT=1
49460 C INTEGRATION OVER XO - NCHANGE=1, VARIABLE STEP - NSTEP=2
49470 C
49480 XOO=0.0
49490 NCHANGE=1
49500 CFCW=AB/SQR(1.1+*2)
49510 CFCF=2*F2*AB/SQR(1.1+*2)
49520 DO 6 INTCNT=1,10000
49530 CALL DERIV (NINT,NCHANGE,NDEBUG,T,AB,F,DF,NF,XOO,XI4,SLOPE,BSLP,AS
      1L)
      IF (NCHANGE.EO.2.AND.ABS(F(11),LE,1.E-10) GO TO 7
      2
      CALL BUNKUT (NINT,NCHANGE,NSTEP,NDEBUG,T,AB,F,DF,FC,DFC,DS,ABI,AB2
      3,ABS,ABA,NF,EP SIGOM,NQUAD,XOO,XI4,SLOPE,BSLP,ASL)
      IF (INTCNT.EO.1) ORAB=DS/AR
      4
      IF (NDEBUG.EO.O) PRINT 47, INTCNT
      5
      IF (NCHANGE.EO.1.AND.ABS(CHECK1-F(11)),LE,1.E-07) GO TO 4
      6
      IF (NCHANGE.EO.1.AND.(F(1)+DF(1)),LE,CHECK1).AND.(CHECK1-(F(1)+DF(1)
      7),GE,-E-07) GO TO 6
      8
49180 C
49190 C
49200 C
49210 TAYLOR-MACCOLL
49220 I=1
49230 XI(I)=0.0
49240 X(I)=0.0
49250 Y(I)=0.0
49260 Y(I)=0.0
49270 DIM(1+2*N)
49280 GY(1)=2*N
49290 GX(1)=2*N
49300 GY(1)=0.0
49310 IF (NDEBUG.EO.O) PRINT 46, I,X(I),Y(I),Y(I)
49320 IF (NDEBU.EO.O) PRINT 45, I,GX(I),GY(I),GX(I),GY(I)
49330 GO TO 36
49340 NSTEP=2
49350 C
49360 C CIRCULAR AND ELLIPTIC CONE - COMPUTATION OF XI(I)
49370 C
49380 NINT=1
49390 NQUAD=0
49400 F(1)=0.0
49410 F(2)=0.0
49420 DS=0.1*AB
49430 DF(1)=DS
49440 C
49450 C INTEGRATION WITH XO OR YO INDEPENDENT VARIABLE - NINT=1
49460 C INTEGRATION OVER XO - NCHANGE=1, VARIABLE STEP - NSTEP=2
49470 C
49480 XOO=0.0
49490 NCHANGE=1
49500 CFCW=AB/SQR(1.1+*2)
49510 CFCF=2*F2*AB/SQR(1.1+*2)
49520 DO 6 INTCNT=1,10000
49530 CALL DERIV (NINT,NCHANGE,NDEBUG,T,AB,F,DF,NF,XOO,XI4,SLOPE,BSLP,AS
      1L)
      IF (NCHANGE.EO.2.AND.ABS(F(11),LE,1.E-10) GO TO 7
      2
      CALL BUNKUT (NINT,NCHANGE,NSTEP,NDEBUG,T,AB,F,DF,FC,DFC,DS,ABI,AB2
      3,ABS,ABA,NF,EP SIGOM,NQUAD,XOO,XI4,SLOPE,BSLP,ASL)
      IF (INTCNT.EO.1) ORAB=DS/AR
      4
      IF (NDEBUG.EO.O) PRINT 47, INTCNT
      5
      IF (NCHANGE.EO.1.AND.ABS(CHECK1-F(11)),LE,1.E-07) GO TO 4
      6
      IF (NCHANGE.EO.1.AND.(F(1)+DF(1)),LE,CHECK1).AND.(CHECK1-(F(1)+DF(1)
      7),GE,-E-07) GO TO 6
      8
143 FORMAT (1X,2H=14,2X,5HU(1)=E16.8,2X,5HP(1)=E16.8,2X,5HV(1)=E16.8,
      12X,5HW(1)=E16.8)
144 FORMAT (1X,2H=2F16.8)
145 FORMAT (4H NA=12,2X,6HANA=E16.8,2X,3HNB(12,2X,4HNBPE16.8/)
146 FORMAT (8H INTCNT=15,2X,6HNEXTRAP=11)
147 FORMAT (/4BX,5HZETA=E16.8/)
148 FORMAT (//29H ZERO-INDEPENDENCE CIRCULAR CONE//)
149 FORMAT (2H V(1)X(E16.8))
150 FORMAT (5H DETA(1)X(E16.8))
151 FORMAT (4H ETAS(1)X(E16.8))
152 FORMAT (A16.8)
153 FORMAT (8H KOUNT=15,2X,5HVMAX=E16.8,2X,6HPSIG=E16.8,2X,7HSPACER=
      1F16.8,2X,8HVMXTEST(E16.8))
154 FORMAT (6H AAST=E16.8/)
155 FORMAT (7H PARAM=E16.8,2X,2HM=11,2X,7HINCRMT=12,2X,7HNCYCLE=14)
156 FORMAT (7H VTEST=E16.8,2X,7HVTST1=E16.8)
157 FORMAT (4H FTASPR(E16.8))
158 FORMAT (15H CP(1) AT SHOCK/(E16.8))
159 FORMAT (16H CP(1) AT ZETA=0/(E16.8))
160 FORMAT (7H SLOPE=E16.8,2X,8HKTTRANSF=12)
161 FORMAT (13TH U VC RHO S POROGAM U
      2 DT,PTINF VC VX VY VZ
      3
162 FORMAT (/72H WINDW
      4
163 FORMAT (17H LEEMAR
      5
164 FORMAT (11E12.4)
165 FORMAT (/7H EPSIG=E16.8,2X,8HPSIGMX=E16.8,2X,7HSPACER=E16.8,2X,8H
      1FPSIVAR=E16.8,2X,7HPSINT=E16.8/)
166 FORMAT (//41H SURFACE VALUES ARE NOT CONVERGED, NSTOP=15//)
167 FORMAT (8H RANGL(E16.8))
168 FORMAT (18H NCYCLE=12,6H AT (2A10//)
169 FORMAT (20H A2617 COMPLETED AT (2A10//)
170 FORMAT (/35H NCNVRG=0 AND I CANNOT HALVE DPRAM//)
171 FORMAT (//44H SURFACE PROPERTIES NOT CORRECTED FOR M2E=1//)
172 FORMAT (//42H DAV15=RD0-A2617-APPLIED MECHANICS -9-8-69)
173 FORMAT (15H BERNIE KLUNKER)
174 FORMAT (93H CONICAL FLOW ABOUT ELLIPTIC CONES BY THE METHOD OF LIN
      1ES WITH INCREMENTATION OF A PARAMETER//)
175 FORMAT (1X(E16.8))
176 FORMAT (7H D(1+J))
177 FORMAT (8H DETERM=E16.8)
178 FORMAT (8H NCYCLE=12,2X,6HVMTEST=E16.8,2X,5HVMAX=E16.8,2X,5HAAST=E1

```

APPENDIX A

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      IF (NCHANGE.EQ.1.AND.(F(1)+DF(1)).LE.CHECK1.AND.CHECK1-(F(1)+DF(1))
1) LE.1-E-07) GO TO 3
      IF (NCHANGE.EQ.1.AND.(F(1)+DF(1)).GT.CHECK1) GO TO 3
      IF (NCHANGE.EQ.2.AND.(F(1)+DF(1)).LE.0.0.AND.ABS(F(1)+DF(1)).GT.1
1E-07) GO TO 6
      IF (NCHANGE.EQ.2.AND.(F(1)+DF(1)).LE.0.0.AND.ABS(F(1)+DF(1)).LE.1
1E-07) GO TO 5
      IF (NCHANGE.EQ.2.AND.(F(1)+DF(1)).GT.0.0) GO TO 5
3 DS=CHECK1-F(1)
  DF(1)=DS
  GO TO 6
C
C
C   INTEGRATION OVER Y0 - NCHANGE=2. VARIABLE STEP - NSTEP=2
C
4 NCHANGE=2
  F(1)=CHECK2
  DS=0.1*AB
  DF(1)=DS
  GO TO 6
5 DS=-F(1)
  CONTINUE
6 TAIMEF(2)
  IF (M2E.FQ.1.AND.NTIMES.EQ.1) TAUL=TAUNI
  IF (M2E.EQ.1.AND.NTIMES.EQ.2) TAUI=TAUNI
  TAUI(N)=2.*TAUNI
  IF (M2E.FQ.1.AND.NTIMES.EQ.2) TAUI(N)=TAUL+TAUI
  TAUI=TAUI(N)
  GO TO (8,9,10), KTRANS
8 TAUR=0.
  XIR=TAUR
  ASLP=TAUR
  ASLP=1.
  XINI=TAUNI
  XIN=2.*XINI
  XI(N)=XIN
  GO TO 11
9 TAUR=TAUNI
  ASLP=SLOPE
  XIR=.7*TAUR/(2.*SLOPE+1.)
  XINI=XIR
  XIN=2.*XINI
  XI(N)=XIN
  ASLP=(1.-SLOPE)/(2.*XIR+2)
  GO TO 11
10 TAUR=0.
  XIR=TAUR
  ASLP=1.
  XI(N)=3.*TAUNI/(2.*SLOPE)
  XIN=XI(N)
  ASLP=(SLOPE-1.)/(3.*XI(N)+2)
  XINI=5*XI(N)
11 XI(1)=0.0
  IF (M2E.NE.1) GO TO 12
  IF (M2E.FQ.1.AND.NTIMES.EQ.1) XIL=XINI
  IF (M2E.FQ.1.AND.NTIMES.EQ.2) XIL=XINI
  IF (M2E.FQ.1.AND.NTIMES.EQ.2) XI(N)=XIL*XII
  IF (M2E.FQ.1.AND.NTIMES.EQ.2) XI(N)=XIL*XIII
  NTIMES=2
  TAU=
  GO TO 2
12 IF (NDEBUG.EQ.0) PRINT 50, BLK(1),XIR,TAUR,XIN,SLOPE,ASLP,EQUAN,DT
  TAUXI=XI(1),XINI
  DPRINT 27, INTENT
  XI(NB)=AN*XINI
  XI(NB)=NB*XINI
  IF (NDEBUG.EQ.0) PRINT 30, XI(1),XI(NB),XI(NB),XINI,XI(N),TAUNI,TA
  UI(N),TAUR,TAUL,XII,XIL
  IF (NDEBUG.EQ.1) GO TO 13
  AA=XI(NB)/FLOAT(NB-1)
  ABB=XI(NB)-XI(NB)/FLOAT(NB-NA)
  AN=XI(N)-XI(NB)/FLOAT(NB-NA)
  IF (NDEBUG.EQ.0) PRINT 40, AA,ABB,AN
  DO 14 I=1,N
  IF (I.EQ.1) OR (I.EQ.NA) OR (I.EQ.NB) OR (I.EQ.N) GO TO 15
  IF (NDEBUG.EQ.1) GO TO 14
  IF (I.GT.1.AND.I.LT.NA) XI(I)=AA*FLOAT(I-1)
  IF (I.GT.NA.AND.I.LT.NB) XI(I)=XI(NB)+AA*FLOAT(I-NB)
  IF (I.GT.NB.AND.I.LT.N) XI(I)=XI(NB)+AN*FLOAT(I-NB)
15 TAUI(1)=TAUR*(XI(I)+Y0)/SLOPE+ASLP*(XI(I)-XIR)**2
  TAUI(2)=ASLP*(XI(I)-Y0)**2
  GPP(1)=1./TAUI
16 CONTINUE
  IF (NDEBUG.EQ.0) PRINT 38, XI(1),I=1,N
  IF (NDEBUG.EQ.0) PRINT 50, BLK(2),TAUI(1),I=1,N
  IF (NDEBUG.EQ.0) PRINT 50, BLK(3),GPP(1),I=1,N
C
C   CIRCULAR AND ELLIPTIC CONF - COMPUTATION OF X0(1)
C   INTEGRATION OVER XI - NINT=2, VARIABLE STEP SIZE - NSTEP=2

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APPENDIX A

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29 IF (NCHANGE.FO.1.AND.F(1).GT.XIL) DXI=XIL-F(1)  B2610  ILP1
IF (NCHANGE.EO.1.AND.F(1).GT.XIL) DXI=XIL-F(1)  B2620  DN A 1=2.NF
11.7-10) DXI=XIL-F(1)  B2630  AR2(1)=DS*NF(1)
DF(1)=DXI  B2640  4 F(1)=FC(1)+AP2(1)/2.
IF (NDEBUG.FO.2) PRINT 13. (1+AB2(1)+F(1)+F(1).NF)  B2650  IF (NDEBUG.FO.2) PRINT 13. (1+AB2(1)+F(1)+F(1).NF)
IF (NDEBUG.FO.2) PRINT 49. DVI  B2660  CALL DERIV (NINT,NCHANGE,NDEBUG.T,AB,F,DF,NF,XOO,XIR,SLOPE,BSLP,AS
70 CONTINUE  B2670  ILP)
GEOMETRIC PARAMETERS FOR CIRCULAR AND ELLIPTIC CONES  B2680  DN S 1=2.NF
31 IF (NDEBUG.FO.1) GO TO 33  B2690  AR3(1)=DS*NF(1)
DO 32 I=1,N  B2700  F(1)=FC(1)+AP2(1)
32 PRINT 40. I,XI(1)+XO(1)+Y(1)+TAU(1)  B2710  R2710
33 DO 34 I=1,N  B2720  IF (NDEBUG.FO.2) GO TO 34
IF (NDEBUG.FO.2) GO TO 34  B2730  CALL DERIV (NINT,NCHANGE,NDEBUG.T,AB,F,DF,NF,XOO,XIR,SLOPE,BSLP,AS
IF (NDEBUG.FO.2) T=TL  B2740  ILP)
IF (NDEBUG.FO.2) T=TL  B2750  DN A 1=2.NF
34 GX(1)=2.*AT**2*XO(1)  B2760  AR2(1)=DS*NF(1)
GY(1)=2.*AT**2  B2770  F(1)=FC(1)+1/6.*(AB1(1)+2.*AB2(1)+2.*AB3(1)+AH4(1))
GXV(1)=2.*AT**2  B2780  IF (NDEBUG.FO.2) PRINT 15. (1+AB4(1)+F(1)+F(1).NF)
GYV(1)=2.  B2790  IF (NDEBUG.FO.2) RETURN
GX(1)=2.  B2800  IF (NDEBUG.FO.2) RETURN
IF (NDEBUG.FO.2) PRINT 45. I,GX(1)+GY(1)+GXV(1)+GYV(1)  B2810  NO 7 1=2.NF
35 CONTINUE  B2820  IF (NDEBUG.FO.2) AND,APS(AHP(1)/DS)+LE.1+P-06) GO TO 7
IF (NDEBUG.FO.2) LIMIT=1  B2830  IF (NDEBUG.FO.2) AND,APS(AH(1)/DS)+LE.1+P-05) GO TO 7
DO 36 I=1,LIMIT  B2840  IF (NDEBUG.FO.2) AND,APS(AH(1)/DS)+LE.1+P-05) GO TO 7
A1(I)=XO(1)+XO(1)**2+YO(1)**2  B2850  IF (NDEBUG.FO.2) TEST=ABS(1.-ABS(1)/AP2(1))
A4(I)=XO(1)+GY(1)+YO(1)+GY(1)  B2860  IF (NDEBUG.FO.2) TEST=ABS(1.-ABS(1)/AP2(1))
A2(I)=GX(1)+GY(1)+2*AA(1)**2  B2870  IF (1.FO.2) TEST=MAX(1)
AA(I)=GX(1)+YO(1)+AA(1)  B2880  IF (TEST.GT.TEST) TEST=MAX(1)
A7(I)=XO(1)+GY(1)+YO(1)+GY(1)  B2890  7 CONTINUE
AB(I)=GY(1)+2*GX(1)+GX(1)**2+GY(1)**2+GX(1)*GY(1)+GY(1)*GX(1)  B2900  IF (TEST=MAX(1).G.FPSIGOM.AND,ABS(1)/DS.GT.DSMIN) GO TO 8
AKB(I)=AB(I)*A(1)/A2(1)**1.5  B2910  IF (TEST=MAX(1).G.FPSISOM) GO TO 9
PS(I)=57.295779*(A*TANP(YO(1)),XO(1))  B2920  RETURN
G(I)=1.0  B2930  9 DS=...
DP(1)=0.0  B2940  9 GO TO 9
IF (NDEBUG.FO.2) PRINT 41  B2950  IF (1.99NS).GT.DSMAY) RETURN
IF (NDEBUG.FO.2) PRINT 42. A1(1)+A2(1)+A3(1)+A4(1)+A5(1)+A6(1)+A7(1)+A8(1)+AKB(1)+PS(1)+G(1)+G(1)+PS(1)  B2960  NS=1.0
77 CONTINUE  B2970  NF(1)=DS
IF (NDEBUG.FO.2) T=TL  B2980  RETURN
RETURN  B2990
38 FORMAT (6H XI(1)/(R16.8))  B3000
39 FORMAT (5X,5HX(1),12X,6HX(IN),10X,6HX(INI),1X,5HX(IN  B3060
11+1)+5HTAUN(1)+6HTAUN(1)/E16.8)  B3070  FND
40 FORMAT (3H I=15+2X,6HX(1)=E16.8+2X,6HX(1)=E16.8+2X,6HY(1)=E16.8  B3080  SUBROUTINE DERIV (NINT,NCHANGE,NDEBUG.T,AB,F,DF,NF,XOO,XIR,SLOPE,B
1+2X,7HTAU(1)=F16.8)  B3100  ISLP,ASLP)
41 FORMAT (10H A1(1)FC.1)  B3110  C
42 FORMAT (11XE16.8)  B3120  C
43 FORMAT (11X)4E16.8)  B3130  C
44 FORMAT (4H IZ=15+2X,7HX(1Z)=E16.8+2X,7HX(1Z)=E16.8+2X,7HY(1Z)=E  B3140  C
116.8+2X,6HDF(1)=E16.8+2X,2HI=15)  B3150  C
45 FORMAT (3H I=14+2X,6HX(1)=E16.8+2X,6HY(1)=E16.8+2X,7HGXX(1)=E16.  B3160  C
8+2X,7HGY(1)=E16.8+2X,7HXY(1)=E16.8)  B3170  C
46 FORMAT (3H I=14+2X,6HX(1)=E16.8+2X,6HX(1)=E16.8+2X,6HY(1)=E16.8  B3180  C
1)  B3190  C
47 FORMAT (8H INTCNT=15)  B3200  C
48 FORMAT (4H AA=E16.8+2X,4HAB=E16.8+2X,3HAN=E16.8)  B3210  C
49 FORMAT (5H DXI=E16.8)  B3220  C
50 FORMAT (15H SUBROUTINE HG (1X)1A6/(BE16.8))  B3230  C
END  B3240-
SUBROUTINE RUNKUT (NINT,NCHANGE,NSTEP,NDEBUG,T,AB,F,DF,NF,FC,DFC,DS,A  C
1R1,AR2,AB3,ABA,NF,EP,EPISIGOM,NOUAD,XOO,XIR,SLOPE,BSLP,ASLP)  C 20
INTERGRATION FOR BODY GEOMETRY  C 30
DIMENSION F(NF), DF(NF), FC(NF), DFC(NF), AB1(NF), AB2(NF), AB3(NF)  C 40
1), AR4(NF)  C 70
IF (NDEBUG.FO.2) PRINT 10. NF,F(1),F(2),DF(1),DF(2)  C 80
FIXED STEP INTEGRATION - NSTEP=1, VARIABLE STEP INTEGRATION - NSTE  C 90
QUADRATURE - NOUAD=1, INTEGRATION - NOUAD=2  C 100
TESTMAX=.5*EPSIGOM  C 110
DSMAX=.02*AR  C 120
NS(NP)=F-.05  C 130
DO 1 I=1,NF  C 140
DFC(I)=DF(I)  C 150
1 FC(I)=F(I)  C 160
2 IF (NDEBUG.FO.2) PRINT 11. DS  C 170
DF(1)=DS  C 180
DO 3 I=2,NF  C 190
AB1(I)=DS*DFC(I)  C 200
3 F(1)=FC(1)+AB1(I)/2.  C 210
F(1)=FC(1)+DS/2.  C 220
IF (NDEBUG.FO.2) PRINT 12. (1+AB1(I)+F(1)+F(1).NF)  C 230
CALL DERIV (NINT,NCHANGE,NDEBUG.T,AB,F,DF,NF,XOO,XIR,SLOPE,BSLP,AS  C 240
14 FORMAT (1X,2HI=15+2X,6HR3(1)=E16.8+2X,5HF(1)=F16.8)  C 690
15 FORMAT (1X,2HI=15+2X,6HRA(1)=E16.8+2X,5HF(1)=F16.8)  C 700
FND  C 710-
SUBROUTINE DERIV (NINT,NCHANGE,NDEBUG.T,AB,F,DF,NF,XOO,XIR,SLOPE,B  C
ISLP,ASLP)  C 20
COMPUTE DERIVATIVES FOR BODY GEOMETRY INTEGRATION  C 30
DIMENSION F(NF), DF(NF)  C 40
GO TO (1,5), NINT  C 50
1 GO TO (2,3), NCHANGE  C 60
2 FRI=FSORT(AB**2-F(1)**2)  C 70
GX(1)=AT**2*F(1)  C 80
A1(1)=F(1)**2+FRI**2  C 90
GO TO 4  C 100
3 XOO(1)=1*FSORT(AB**2+2*F(1)**2)  C 110
FRI=FSORT(AB**2-XOO**2)  C 120
GX(1)=AT**2*XOO  C 130
A1(1)=XOO**2+2*F(1)**2  C 140
4 GY1=-2.*FRI  C 150
A2(1)=AB**2*2*AT**2  C 160
A1(1)=AB**2+GY1**2+AA1**2  C 170
IF (NCHANGE.EO.1) DF(2)=SORT(A2(1)/(A1+GY1))  C 180
IF (NCHANGE.EO.2) DF(2)=SORT(A2(1)/(A1+GX1))  C 190
IF (NDEBUG.EO.2) PRINT 6. NINT-T,AB,F(1)+F(2),FBI,GY1,GY1,A11,AA1  C 200
1A2(1)=DF(1)+DF(2)  C 210
RETURN  C 220
5 DURN=AR**2-F(2)**2  C 230
FRI=FSORT(ABS(QUAN))  C 240
GX(1)=AT**2*F(2)  C 250
GY1=2.*F(3)  C 260
A1(1)=F(2)**2+2*FBI**2  C 270
A2(1)=GX1**2+2*GY1**2+AA1**2  C 280
TAUX1=ASLP+3.*BSLP*(F(1)-XIR)**2  C 290
G2BI=1./TAUX1  C 300
DF(2)=A1*GY1/(SORT(A2(1)*G2BI))  C 310
DF(3)=A1*GX1/(SORT(A2(1)*G2BI))  C 320
IF (NDEBUG.EO.2) PRINT 6. NINT-T,AB,F(1)+GX1+GY1+A11+A21,AA1,F(1),F  C 330
1(2),F(3)+DF(1)+DF(2),DF(3)+T,DTAUX1,G2BI  C 340
RETURN  C 350
6 FORMAT (17H SUBROUTINE DERIV/115/(BE16.8))  C 410

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APPENDIX A

Table with 4 columns: Line number, Column 1, Column 2, Column 3. Contains code snippets for various mathematical and programming operations.

APPENDIX A

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A11=-Y0(1)*QUAN1+GX(1)*QUAN2      G 370
A12=-Y0(1)*QUAN1+GY(1)*QUAN2      G 380
A13=-QUAN1-AA(1)*QUAN2             G 390
A21=-QUAN1*(GY(1)+Y0(1)*AA(1))    G 400
A22=QUAN1*(GX(1)+Y0(1)*AA(1))    G 410
A23=QUAN1*AT(1)                   G 420
A31=Y0(1)*QUAN3+GX(1)*QUAN4      G 430
A32=Y0(1)*QUAN3+GY(1)*QUAN4      G 440
A33=QUAN3-AA(1)*QUAN4             G 450
IF (NDEBUG.EQ.0) PRINT 1, 1,QUAN1,QUAN2,QUAN3,QUAN4,QUAN5,A11,A12,
PHIR=ATAN2(GY(1),GX(1))           G 470
SINPHIR=SIN(PHIR)                 G 480
COSPHIR=COS(PHIR)                 G 490
R11=1+1/COSPHIR+1/2+CINPHIR        G 500
R12=2+1/COSPHIR+2/2+CINPHIR        G 510
R13=A31/COSPHIR+A32+CINPHIR        G 520
R21=-A11/SINPHIR+A12+COSPHIR       G 530
R22=-A21/SINPHIR+A22+COSPHIR       G 540
R23=-A31/SINPHIR+A32+COSPHIR       G 550
IF (NDEBUG.EQ.0) PRINT 1, 1,GY(1),GX(1),PHIR,SINPHIR,COSPHIR,B11,B
112,B13,B21,R22,B23               G 560
RTI=DM                             G 570
G 580
G 590
G 600
G 610
G 620
G 630
G 640
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APPENDIX A

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1 2X,4HP(1)=E16-B-2X,9HSBAP(1)=E16,B) I 640 DFORM(1)=(H#FIB/AAS1**2-(G1B/AAS1)**2-G1)**2/ASO J 870
END I 650- IF (INDEBUQ.EQ.0) PRINT 12, BLK(4),I,AM(1),CROSSM(1),POROGAM(1),S(1) J 880
SURROTIME FONS (DZETA) J 10 1)+UP(1),VP(1),WP(1),SBARP(1),FF+F1,F2,F3,QUAN,FIB,G1B,G(1),D J 890
COMPJF ZETA DFRIVATIVES J 20 ZFONS(1)=FUN(1,1) J 900
J 30 IF (NEVTRAP.D0.1) GO TO 9 J 910
J 40 IF ((G1),GT=EPS15,OR,DEONS(1),LT=EPS1G,AND,FUN(1,1),GE+.80) GO T J 920
J 40 10.6 J 930
COMMON F(3),DF(3),FC(3),DFC(3),AR1(3),AB2(3),AR3(3),AB4(3) J 60 IF (ABS(G(1)),LT=FPS16,OR,G(1),GT.0.) GO TO 7 J 940
COMMON FUN(20,6),DFUN(20,6),FUNC(20,6),DFUNC(20,6),B1(20,6),B2(20, J 70 IF (DEONS(1),GT.0.) GO TO 6 J 950
16),R1(20,6),R4(20,6) J 70 COMMON SBRV(20),DSBD(20),SBARP(20),DSD(20),NSB2(20),DSB3(20),DSB J 80
COMMON SBRV(20),DSBD(20),SBARP(20),DSD(20),NSB2(20),DSB3(20),DSB J 80 14(20),X1(20),X0(20),Y0(20),A1(20),A2(20),A3(20),A4(20),A5(20),A6(2 J 90
20),A7(20),A8(20),AK3(20),XK(20),GY(20),GX(20),SY(20),GX(20),ETA J 100 PRINT 13
3(20),ETAS(20),ETASP(20),LAD(20),RHO(20),R(20),P(20),U(20),V(20), J 110 RETURN
AM(20),PP(20),UP(20),VP(20),WP(20),XS(20),YS(20),DUD(20),DPU(20), J 120
DWD(20),DWD(20),AM(20),S(20),ZETA(20),ZETA(20),ZETA(20),ZETA(20), ZETA(20), J 130
A(20),DU1(20),DU2(20),DU3(20),DU4(20),DU1(20),DU2(20),DU3(20),DU4(2 J 140
70),DV1(20),DV2(20),DV3(20),DV4(20),PS1(20),DPI(20),DP2(20), J 150
ADP(20),DPA(20),DFON(20),CROSSM(20),POROGAM(20),O(20),OP(20),PS15 J 160
90(20),BERNDL(20),XSAR(20),YSAR(20),RHO(SFN(20),UISFN(20)) J 170
COMMON XGBAR(20),YGBAR(20),XGAB(20),YGBAR(20),TAU(20),GZB(20),DSDZ E J 180
1X(20) J 190
COMMON KTRANS,SLOPE J 200
COMMON AAS1,B11,R12,R13,B21,B22,B23,NSPACE,P1,M,N,L1,T,THETAR,GAMM J 210
14,DK1,CON1,CON2,STMACH,AS,A11,A12,A13,A21,A22,A23,A31,A32,A33,ALPH J 220
2AR,N1,INDEBUQ,H,K,SIGMA,HAD,HP,NLINES,EPSIG,MPRINT,SPACE,NEXTAP, J 230
3EPSICOM,EPSINT,DEO,XINI,SIGNP J 240
COMMON /BLOCKN/DWDX1,WP1,WP2,WP3,WP4 J 250
COMMON /ERROR/ ER(12),ERR(12),BLK(12) J 260
COMMON VCC(20),WCC(20),CPHOCK(20),CP(20),CRASHLD(20),XRHL(20),YB J 270
1HL(20),XIC(20),VCC(20),XIC(20),XK(20),VY(20),THETNOR(20),PSIN(20), J 280
2PROPT(20),P1OPT(20),P2(20),POAST(20),POPINF(20),CPRODY(20) J 290
COMMON /BLOCKS/ NFGP J 300
IF (INDEBUQ.F0.0) PRINT 1 J 310
NFXTAB=0 J 320
1 DO 10 I=1,N J 330
ANUM=2*FUN(1,1)*FAT(1) J 340
SURT=1/SORT(O(1)**2+4*FUN(1,1)*(-O(1))) J 350
IF (O(1),GE.0.0) ETA(1)=ANUM/O(1)+SORT(1) J 360
IF (O(1),LT.0.0) ETA(1)=ANUM/O(1)-SORT(1) J 370
IF (INDEBUQ.EQ.0) PRINT 12, BLK(1),I,ETAS(1),ETASP(1),ETA(1),ANUM,S J 380
1OR1,FUN(1,1),FUN(1,2),FUN(1,3),FUN(1,4),FUN(1,5),O(1),OP1(1),AKB(1 J 390
2),GAMMA,STMACH,AR,PP(1),UP(1),VP(1),WP(1),ZETA(1),ZETA2(1),ZETA3( J 400
3),ZETA4(1),DU1(1),DU2(1),DU3(1),DU4(1),DP1(1),DP2(1),DP3(1),DP4(1 J 410
4),DV1(1),DV2(1),DV3(1),DV4(1),DPI(1),DPI2(1),DPI3(1),DPI4(1),FUN(1,6) J 420
FIB=O(1)+2*O(1)*(-O(1))*FAT(1)/ETAS(1) J 430
G1B=FAT(1)*OP(1)*I*(-ETAS(1)/ETAS(1))-ETASP(1)*FIB/ETAS(1) J 440
CON1=5*ETA(1) J 450
CON2=COS(FAT(1)) PRINT 12, BLK(1),I,ETAS(1),ETASP(1),ETA(1),ANUM,S J 460
HCON2=AKR(1)*CON1 J 470
HK=CON1+AKB(1)*CON2 J 480
IF (ABS(H),GE.1.0F-07) GO TO 2 J 490
PRINT 12, ERR(1),I,FUN(1,1),ETAS(1),ETA(1),CON1,CON2,H,KHK J 500
STOP 120 J 510
2 TANSIG=FATSP(1)/H J 520
SIGMA=ATAN(TANSIG) J 530
BUSQ=FUN(1,2)**2*FUN(1,4)**2*FUN(1,5)**2 J 540
DENOM=EXP(FUN(1,6)) J 550
IF (INDEBUQ.EQ.0) PRINT 12, BLK(2),I,CON1,CON2,AKB(1),H,KHK,ETASP(1) J 560
1,TANSIG,SIGMA,BUSQ,GAMMA,STMACH,DENOM,FIB,G1B J 570
IF (ABS(DENOM),GE.1.0F-07,AND,FUN(1,3),GT.0.0) GO TO 3 J 580
PRINT 12, ERR(2),I,GAMMA,STMACH,TANSIG,SIGMA,BUSQ,DENOM,FUN(1,1),F J 590
1UN(1,2),FUN(1,3),FUN(1,4),FUN(1,5) J 600
NEGP=C
PRINT 14 J 620
RTURN J 630
3 RHO(1)=(GAMMA*STMACH**2*FUN(1,3)/DENOM)**1./GAMMA) J 640
DENOM=1+2./((GAMMA-1)*STMACH**2) J 650
BERNDL(1)=1-(2.*GAMMA*FUN(1,3)/(RHO(1)*(GAMMA-1))+BUSQ*AAST**2) J 660
1/DENOM J 670
IF (RHO(1),GE.1.E-10) GO TO 4 J 680
PRINT 12, ERR(3),I,BUSQ,DENOM,RHO(1),FUN(1,3) J 690
STOP 1203 J 700
4 ASO=GAMMA*FUN(1,3)/RHO(1) J 710
IF (INDEBUQ.EQ.0) PRINT 12, BLK(3),I,RHO(1),ASO J 720
IF (ASO,GT.1.E-20) GO TO 5 J 730
PRINT 12, ERR(4),I,RHO(1),FUN(1,3),BUSQ,ASO J 740
STOP 1204 J 750
5 AM(1)=SORT(AAST**2*PBUSQ/ASO) J 760
CROSSM(1)=SORT(AAST**2*(BUSQ-FUN(1,2)**2)/ASO) J 770
POROGAM(1)=FUN(1,3)/RHO(1)*GAMMA J 780
S(1)=ALOG(FUN(1,3)*GAMMA*STMACH**2/RHO(1)*GAMMA) J 790
FF=ETAS(1)*(HP(FUN(1,4)**2*FUN(1,5)**2)-FUN(1,5)*UP(1)) J 800
F1=ETAS(1)*(FUN(1,5)*PP(1)/RHO(1)+ASO*WP(1)**2+HP(FUN(1,2)-HK*FUN(1 J 810
1,4)) J 820
F2=ETAS(1)*(FUN(1,5)*VP(1)+HP(FUN(1,2)*FUN(1,4)+HK*FUN(1,5)**2) J 830
F3=ETAS(1)*(PP(1)/RHO(1)*AAST**2+FUN(1,5)*WP(1)+HP(FUN(1,2)*FUN(1 J 840
1,5)*HK*FUN(1,4)+FUN(1,5)) J 850
G(1)=HP(FUN(1,4)*FIB+FUN(1,5)*G1B J 860
```

APPENDIX A

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11 FORMAT (16H SUBROUTINE FONS) J1760
12 FORMAT (17H SUBROUTINE FONS (X1A6.15/(RE16.8)) J1760
13 FORMAT (18H DEGRS (5 NEGATIVE)) J1780
14 FORMAT (//23H CUCH-NEGATIVE PRESSURE//) J1790
      FNR J1800
SUBROUTINE RUNKUT2 (NS,NP) K 10
COMMON F(3),DF(3),FC(3),AB(3),AB2(3),AB3(3),AB4(3) K 20
COMMON FUN(20.6),DFUN(20.6),FUNC(20.6),DFUNC(20.6),B1(20.6),B2(20. K 30
16),B3(20.6),B4(20.6) K 40
COMMON SBAR(20),DSB2(20),SBARP(20),DSR1(20),DSB2(20),DSB3(20),DSB K 50
14(20),X1(20),X0(20),Y0(20),A1(20),A2(20),A3(20),A4(20),A5(20),A6(2 K 60
20),A7(20),AB(20),AKB(20),GX(20),GY(20),GXX(20),GYY(20),GXY(20),ETA K 70
3(20),ETAS(20),ETASP(20),ETATD(20),RHO(20),R(20),P(20),U(20),V(20), K 80
AW(20),VPP(20),VLP(20),VP(20),XPI(20),XS(20),YS(20),DUZ2(20),DPDZ(20), K 90
SDVDZ(20),DWDZ(20),AM(20),S(20),ZETA1(20),ZETA2(20),ZETA3(20),ZETA4 K 100
6(20),DUI(20),DUZ(20),DU3(20),DVA(20),DX1(20),DQZ(20),DW3(20),DW4(2 K 110
70),DVI(20),DV2(20),DV3(20),DVA(20),G(20),PS10(20),DPI(20),DP2(20), K 120
RDP3(20),DPA(20),DEGNS(20),CROSSM(20),POROGAM(20),G(20),OP(20),PS15 K 130
90(20),PERNOUL(20),XSBAR(20),YSBAR(20),RHO1(20),UISFN(20) K 140
COMMON XBAR(20),YBAR(20),XBAR(20),YBAR(20),TAU(20),G2R(20),OPDZE K 150
1X(20) K 160
COMMON KTRANSF,SLDOP K 170
COMMON AAST,B11,R12,R13,R21,R22,R23,NSPACE,P1,M,N,LI,T,TETAR,GAMM K 180
1A,NX1,CONI,CON2,STMACH,AB,A11,A12,A13,A21,A22,A23,A31,A32,A33,ALPH K 190
ZAR,ML,NEBUG,HE,HE,SI,OMA,RD,NE,NLINES,EPSIG,MPRINT,SPACER,NEXTWAP, K 200
3EPSIG,COX,EPISINT,EO,OXI,1,SIGNPI K 210
COMMON /BLOCKN/ DWX(1,YP1,YP2,WP3,WP4 K 220
COMMON /ERROR/ ER(12),ERR(12),BLK(12) K 230
COMMON VCC(20),VCC(20),CPHOCK(20),CP(20),SBARHLD(20),XRHLD(20),YB K 240
1HL(20),UC(10),VC(20),AC(20),VK(20),VY(20),THEINOR(20),PSINUR(20), K 250
2PDP1(20),PTOPT(1,20),PT(20),POASTSD(20),POPINF(20),CPRONY(20) K 260
COMMON /BLOCKA/ NEGR K 270
NDFRIG=1 K 280
IF (NDFRIG.NE.1) GO TO 2 K 290
PRINT 27 K 300
DO 1=1,N K 310
1 PRINT 28, 1,(NX,FUN(1,NX),DFUN(1,NX),NXF=1,NF) K 320
2 TESTMAX=5*EPSINT K 330
DSMIN=1 K 340
NSMIN=NSMIN K 350
IF (NSMIN.FO.DSMAX) NS=-DSMAX K 360
C (DSMIN,EO,DSMAX) GIVES A FIXED INTEGRATION STEP K 370
C K 380
      WRAWD(N) K 870
      DO 8=1,N K 880
      DO 7 NXF=1,NF K 890
      OFUNC(1,NXF)=DFUNC(1,NXF) K 860
      7 FUNC(1,NXF)=F(1,NXF) K 870
      8 CONTINUE K 880
      DO 10 I=1,N K 890
      10 DFUN(I)=DS K 900
      IF (NDFRUG.FO.0) PRINT 29, NS K 910
      DO 11 I=1,N K 920
      DO 11 NXF=1,NF K 930
      R1(1,NXF)=NS*DFUNC(1,NXF) K 940
      11 FUNC(1,NXF)=FUNC(1,NXF)+R1(1,NXF)/2. K 950
      DO 12 I=1,N K 960
      12 FUNI(1)=FUNC(1,1)+NS/2. K 970
      IF (NDFRUG.NE.0) GO TO 14 K 980
      DO 13 I=1,N K 990
      13 PRINT 30, 1,(NXF,B3(1,NXF),FUN(1,NXF),NXF=1,NF) K1000
      14 CALL DERIVE (DS,NP) K1010
      IF (NDFRUG.NE.0) RETURN K1020
      IF (NEGP.FO.0) RETURN K1030
      IF (NEXTWAP.FO.1) RETURN K1040
      DO 15 I=1,N K1050
      DO 15 NXF=1,NF K1060
      RP(1,NXF)=NS*DFUNC(1,NXF) K1070
      15 FUNI(1,NXF)=FUNC(1,NXF)+RP(1,NXF)/2. K1080
      IF (NDFRUG.NE.0) GO TO 17 K1090
      DO 16 I=1,N K1100
      16 PRINT 31, 1,(NXF,B2(1,NXF),FUN(1,NXF),NXF=1,NF) K1110
      17 CALL DERIVE (DS,NP) K1120
      IF (NEGP.FO.0) RETURN K1130
      IF (NEGP.FO.0) RETURN K1140
      IF (NEXTWAP.FO.1) RETURN K1150
      NCNT=0 K1160
      DO 19 I=1,N K1170
      FUNI(1)=FUNC(1,1)+DS K1180
      DO 19 NXF=1,NF K1190
      B3(1,NXF)=DS*DFUNC(1,NXF) K1200
      IF (ABS(B3(1,NXF)/DS)+LE+1.F-03) GO TO 18 K1210
      TESTARS(1)=B3(1,NXF)/B2(1,NXF) K1220
      NCNT=NCNT+1 K1230
      IF (NCNT.FO.1) TESTMAX=TEST K1240
      IF (TESTMAX.GT.TESTMAX) TESTMAX=TEST K1250
      18 FUNI(1,NXF)=FUNC(1,NXF)+B3(1,NXF) K1260
      IF (NDFRUG.FO.0) PRINT 32, 1,NXF,B3(1,NXF),FUN(1,NXF),TEST K1270
      19 CONTINUE K1280
      IF (NSMIN,EO,DSMAX) GO TO 20 K1290
      IF (TESTMAX.GT.EPSINT.AND.ARS(DS),GT,DSMIN) GO TO 24 K1300
      20 CALL DERIVE (DS,NP) K1310
      IF (NEGP.FO.0) RETURN K1320
      IF (NEGP.FO.0) RETURN K1330
      IF (NEXTWAP.FO.1) RETURN K1340
      DO 21 I=1,N K1350
      DO 21 NXF=1,NF K1360
      B4(1,NXF)=DS*DFUNC(1,NXF) K1370
      21 FUNI(1,NXF)=FUNC(1,NXF)+1./6.*(B1(1,NXF)+2.*B2(1,NXF)+2.*B3(1,NXF)+ K1380
      1PA(1,NXF)) K1390
      IF (NDFRUG.NE.0) GO TO 23 K1400
      DO 22 I=1,N K1410
      22 PRINT 33, 1,(NXF,B4(1,NXF),FUN(1,NXF),NXF=1,NF) K1420
      23 IF (TESTMAX.LE.(1+EPSINT)) GO TO 25 K1430
      RETURN K1440
      24 DS=4*DS K1450
      GO TO 9 K1460
      25 IF (NSMIN,EO,DSMAX) RETURN K1470
      IF (ABS(1.9*DS),GT,DSMAX) RETURN K1480
      DS=1.9*DS K1490
      DO 24 I=1,N K1500
      26 DFUN(1,1)=DS K1510
      RETURN K1520
      27 FORMAT (19H SUBROUTINE RUNKUT2) K1530
      28 FORMAT (3H 1=15/15H NXF=13.2X,11HFUN(1,NXF)=E16.8.2X,11HFUN(1,NXF K1560
      1)=1K.8) K1570
      29 FORMAT (4H DS=E16.8) K1580
      30 FORMAT (3H 1=15/15H NXF=13.2X,10HB1(1,NXF)=E16.8.2X,11HFUN(1,NXF)= K1590
      1E16.8) K1600
      31 FORMAT (3H 1=15/15H NXF=13.2X,10HB2(1,NXF)=E16.8.2X,11HFUN(1,NXF)= K1610
      1E16.8) K1620
      32 FORMAT (3H 1=13.2X,4HNXF=13.2X,10HB3(1,NXF)=E16.8.2X,11HFUN(1,NXF)= K1630
      1E16.8.2X,5HTEST=E16.8) K1640
      33 FORMAT (3H 1=15/15H NXF=13.2X,10HB4(1,NXF)=E16.8.2X,11HFUN(1,NXF)= K1650
      1E16.8) K1660
      END K1670
SUBROUTINE PRINT (ML,INEP1,LPRINT,ZETA,DZETA,NP,NPLOT,NZETA) L 10
COMMON F(3),DF(3),FC(3),AB(3),AB2(3),AB3(3),AB4(3) L 20
COMMON FUN(20.6),DFUN(20.6),FUNC(20.6),DFUNC(20.6),B1(20.6),B2(20.6) L 30

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APPENDIX A

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20 FORMAT (3X,1H1,6X,3H1A0,14X,2H1,14X,2H0,14X,2HY0,13X,4HETAS,11X, L1800 M 710  
15H1ASPP//16,6F16.6) L1810 M 720  
21 FORMAT (/) L1820 M 730  
22 FORMAT (14X,3H1=10X,4H1=20X,3H1=30X,3H1=40X,3H1=50X,3H1=60X,3H1=70 L1840 M 740  
1X,3H1=80X,3H1=90X,4H1=10/ ) L1850 M 750  
23 FORMAT (14X,4H1=118X,4H1=128X,4H1=138X,4H1=148X,4H1=158X,4H1=168X L1860 M 760  
1,4H1=178X,4H1=188X,4H1=198X,4H1=20/ ) L1870 M 770  
24 FORMAT (11X,17,1,10F12.4) L1880 C M 20  
25 FORMAT (14X,4H1=218X,4H1=228X,4H1=238X,4H1=248X,4H1=258X,4H1=268X L1890 C M 30  
1,4H1=278X,4H1=288X,4H1=298X,4H1=30/ ) L1900 C M 40  
26 FORMAT (14X,4H1=318X,4H1=328X,4H1=338X,4H1=348X,4H1=358X,4H1=368X L1910 C M 50  
1,4H1=378X,4H1=388X,4H1=398X,4H1=40/ ) L1920 C M 60  
27 FORMAT (14X,4H1=418X,4H1=428X,4H1=438X,4H1=448X,4H1=458X,4H1=468X L1930 C M 70  
1,4H1=478X,4H1=488X,4H1=498X,4H1=50/ ) L1940 C M 80  
28 FORMAT (5F16.8) L1950 C M 90  
29 FORMAT (/59X,19HSUMMARY PRINT BLOCK//) L1960 C M 100  
C M 110  
SUBROUTINE FMCDEFS (N,NA,NH,NSPACE,X1,A,M,AA,AAA,P,AB,AI,AA,GY,YO, L1970  
15INAI,P,COSALP,C2R) M 20  
COMPUTE FORCE AND MOMENT COEFFICIENTS M 30  
DIMENSION X1(N),PIN, A2(N),AI(N),AA(N),GY(N),YO(N),G2R(N) M 40  
IF (NSPACE.FD.1) GO TO 5 M 50  
SUM1=0.0 M 60  
SUM2=0.0 M 70  
SUM3=0.0 M 80  
NCOWS=1 M 90  
DX1=X1(NA)-X1(NA-1) M 100  
GO TO 11 M 110  
1 CONTINUE M 120  
2 CONTINUE M 130  
AINT=DX1/3.*SUM1 M 140  
AINT=DX1/3.*SUM2 M 150  
AINT=DX1/3.*SUM3 M 160  
SUM1=0.0 M 170  
SUM2=0.0 M 180  
SUM3=0.0 M 190  
NCOWS=2 M 200  
DX1=X1(NA)-X1(NA-1) M 210  
GO 2 1=NA,NB M 220  
GO TO 11 M 230  
3 CONTINUE M 240  
4 CONTINUE M 250  
AINT=DX1/3.*SUM1 M 260  
AINT=DX1/3.*SUM2 M 270  
AINT=DX1/3.*SUM3 M 280  
SUM1=0.0 M 290  
SUM2=0.0 M 300  
SUM3=0.0 M 310  
NCOWS=3 M 320  
DX1=X1(NA)-X1(NA-1) M 330  
GO 1 1=NA,N M 340  
GO TO 11 M 350  
5 CONTINUE M 360  
AINT=DX1/3.*SUM1 M 370  
AINT=DX1/3.*SUM2 M 380  
AINT=DX1/3.*SUM3 M 390  
GO TO (B,9), NSPACE M 400  
6 C2=0./AA*INT7 M 410  
CY=0./AA*INT8 M 420  
YBR=0./13.*AA*C2*INT9 M 430  
GO TO 10 M 440  
7 C2=0./AA*(AINT1+AINT4+AINT7) M 450  
CY=0./AA*(AINT2+AINT5+AINT8) M 460  
YBR=0./13.*AA*C2*(AINT3+AINT6+AINT9) M 470  
8 CDEFS=COSALP*CY*INAI M 480  
CL=CY*INAI*P*CY*COSALP M 490  
ZRAD=2./3. M 500  
CM=VARD*CY*ZRAD*CY M 510  
DDINT 14 M 520  
DDINT 12, C2,CY,CD,CL M 530  
DDINT 13, YBR,ZRAD,FM M 540  
RETURN M 550  
1) AAA=0(1)-AA M 560  
DENOM=SQRT(A2(11)+G2R(1)) M 570  
QUAN1=AAA*AA(1)*AI(1)/DENOM M 580  
QUAN2=AAA*GY(1)*AI(1)/DENOM M 590  
QUAN3=QUAN1*YN(1) M 600  
IF (MOD(1,2).F0.0) FACT=4.0 M 610  
IF (MOD(1,2).NE.0) FACT=2.0 M 620  
IF (1.EQ.01+OR.1.EQ.NA+OR.1.EQ.NB+OR.1.EQ.N) FACT=1.0 M 630  
SUM1=SUM1+FACT*QUAN1 M 640  
SUM2=SUM2+FACT*QUAN2 M 650  
SUM3=SUM3+FACT*QUAN3 M 660
```

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27 DETERM=DETERM*PIVOT
C
C DIVIDE PIVOT ROW BY PIVOT ELEMENT
C
      DO 20 L=1,N
      IF (IPIVOT(L)-1) 2R,20,30
28 A(IICOLU,L)=A(IICOLU,L)/PIVOT
29 CONTINUE
      IF (M) 32,30,30
30 DO 21 L=1,M
21 R(IICOLU,L)=R(IICOLU,L)/PIVOT
C
C REDUCE NON-PIVOT ROWS
C
      DO 30 L=1,N
      IF (L-IICOLU) 33,30,33
      T=A(L,IICOLU)
      DO 36 L=1,N
      IF (IPIVOT(L)-1) 34,36,36
34 A(L,L)+T*(L)-A(IICOLU,L)*T
35 CONTINUE
      IF (M) 38,36,36
36 DO 37 L=1,M
37 B(L,L)+T*(L)-B(IICOLU,L)*T
38 CONTINUE
39 RETURN
END
FUNCTION DIF (L,M,ND,VARI,VARD)
C
C THIS FUNCTION SUBPROGRAM FINDS THE DERIVATIVE AT A GIVEN POINT.
C L FOR THE DERIVATIVE X AND Y IN A GIVEN TABLE. THE N-POINT
C LAGRANGIAN FORMULA IS USED WHERE N IS ODD.
C
C L = INTEGER, THE POINT OF X AND Y AT WHICH DERIVATIVE IS FOUND
C N = INTEGER, 1-5, TO DETERMINE THE POINT FORMULA. N = N2+M1
C ND = INTEGER, THE NUMBER OF POINTS IN TABLE OF VARIABLES
C VARI = ARRAY OF INDEPENDENT VARIABLE. X, VARI(ND)
C VARD = ARRAY OF DEPENDENT VARIABLE. Y, VARD(ND)
C
C DIMENSION VARI(ND), VARD(ND), X(11), Y(11)
C
DIF=0.17770000000000000000
IF (M,LT,1) RETURN
N2=M+1

IF (M.GT,5.OR,N.GT,ND) RETURN
M1=M+1
M2=ND-M+1
K=L
IF (L,LT,M1.OR,N,GT,ND) GO TO 1
K=M1
IF (L,LT,M2) GO TO 1
K=L+ND-N
1 MX=L-K
      DO 2 J=1,N
      MJ=VARI(J)
      X(J)=VARI(MJ)
2 Y(J)=VARD(MJ)
      A=1.
      B=0.
      C=0.
      DO 4 J=1,N
      IF (J,GT,K) GO TO 4
      D=1.
      DO 3 I=1,N
      IF (I,GT,J) GO TO 3
      DAP=X(J)-X(I)
      CONTINUE
      TAY=X(J)-Y(I)
      BAP=V(J)-(D*T)
      A=AT
      C=AT+T
4 CONTINUE
      DIF=A*B+V(K)*C
      RETURN
      END

```

APPENDIX A

Subroutines

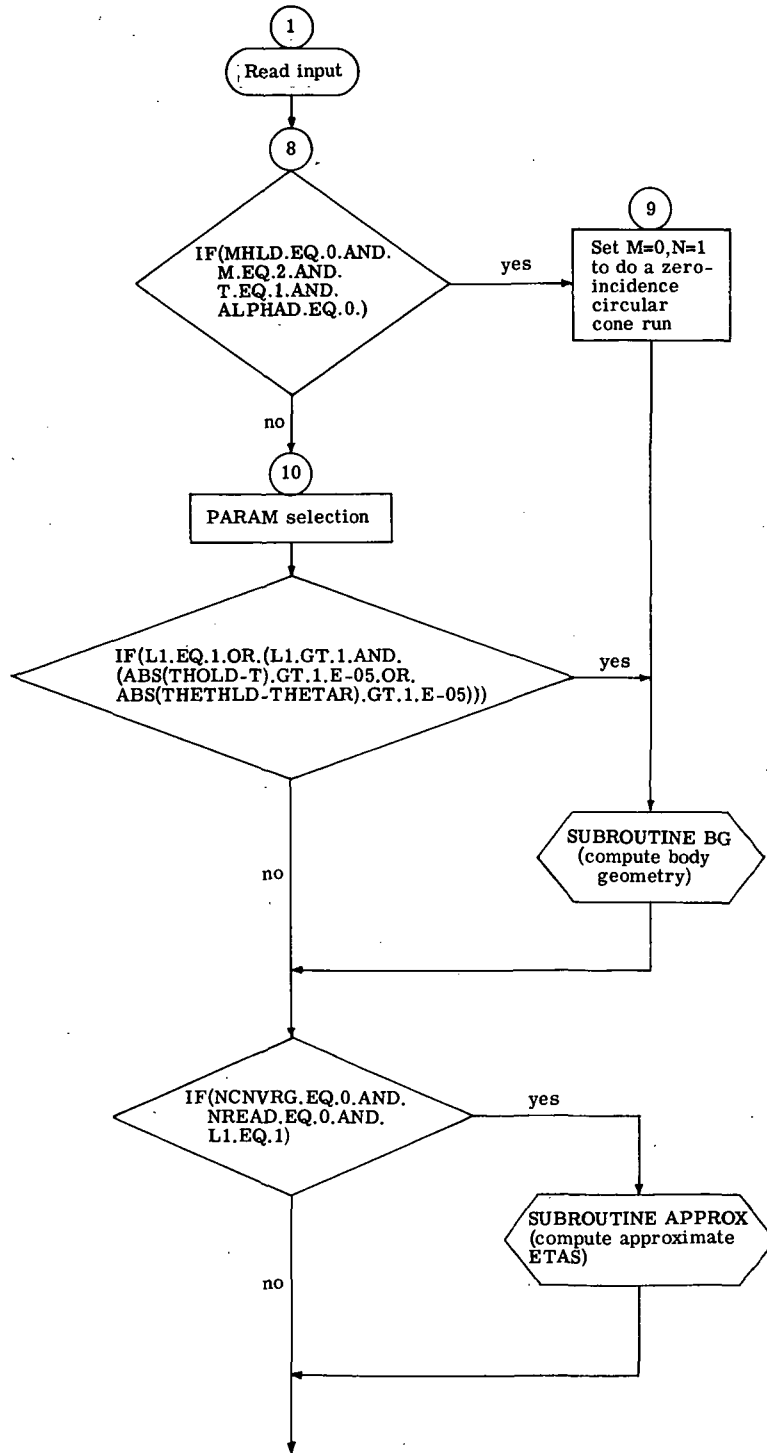
A list of the subroutines used in this program is presented.

<u>FORTTRAN name</u>	<u>Called by</u>	<u>Function</u>
BG	MAIN	Executive subroutine for computation of body geometry
RUNKUT	BG	Runge-Kutta integration for body geometry
DERIV	BG RUNKUT	Computation of derivatives for body-geometry integration
APPROX	MAIN	Computation of approximate shock shape for NREAD = 0
LGRANGE	MAIN DERIV2	Establishes line arrangement, accounts for symmetry where appropriate, for computation of XI derivatives for function DIF
DIRCOS	MAIN	Computation of direction cosines of R, ETA, TAU coordinates
SHOCK	MAIN	Computation of flow quantities behind shock
DERIV2	MAIN RUNKUT2	Executive subroutine for computation of derivatives for integration of equations
EQNS	DERIV2	Computation of zeta-derivatives for integration of equations
RUNKUT2	MAIN	Runge-Kutta integration of equations
PRINT	MAIN	Print instructions
FMCOEFS	MAIN	Computation of force and moment coefficients
SIMEQ	MAIN	Solution of simultaneous linear equations to evaluate corrections DELTA to the shock shape
DIF	LGRANGE	Computation of derivatives from the Lagrange formula

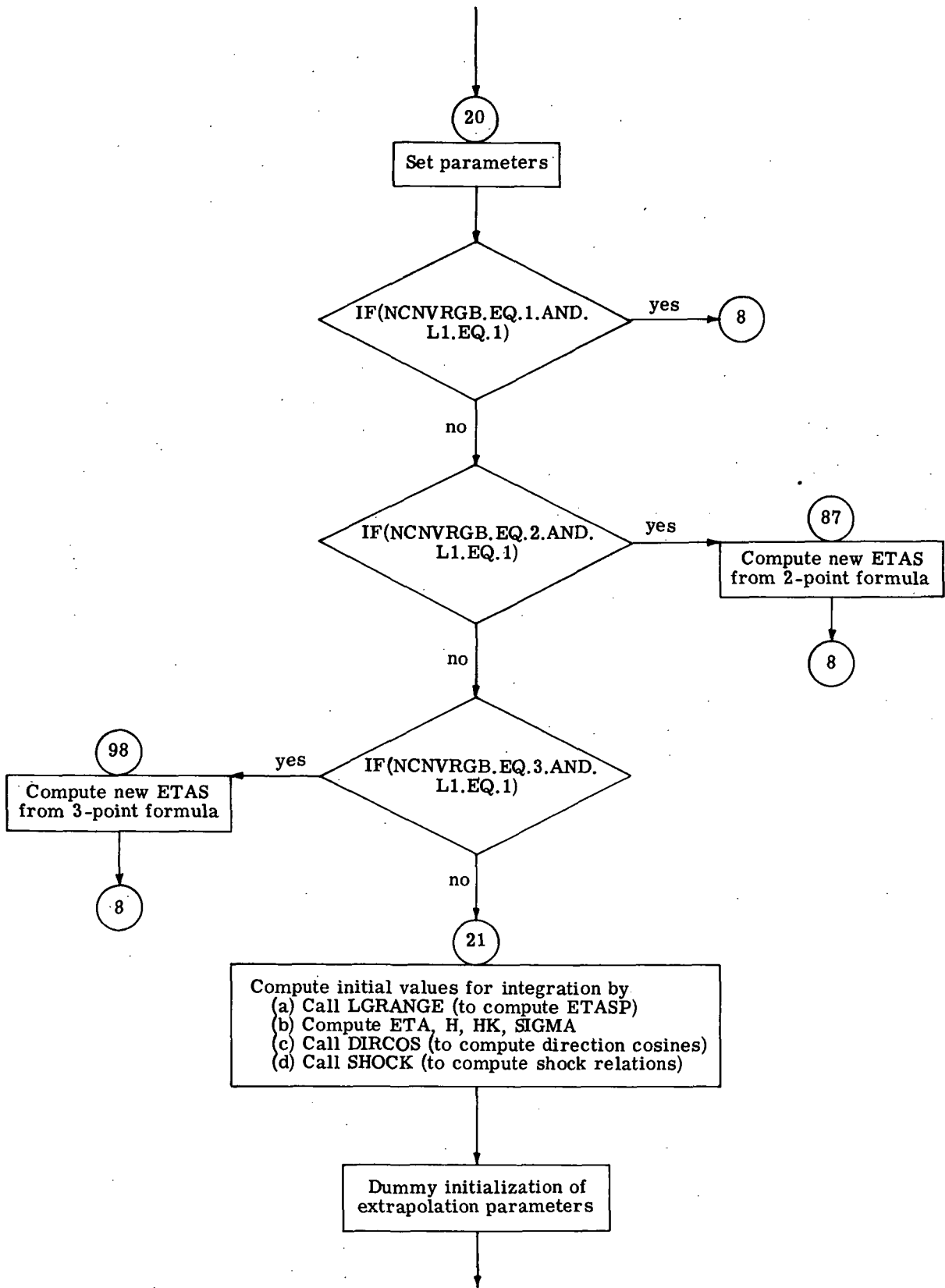
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Flow Chart

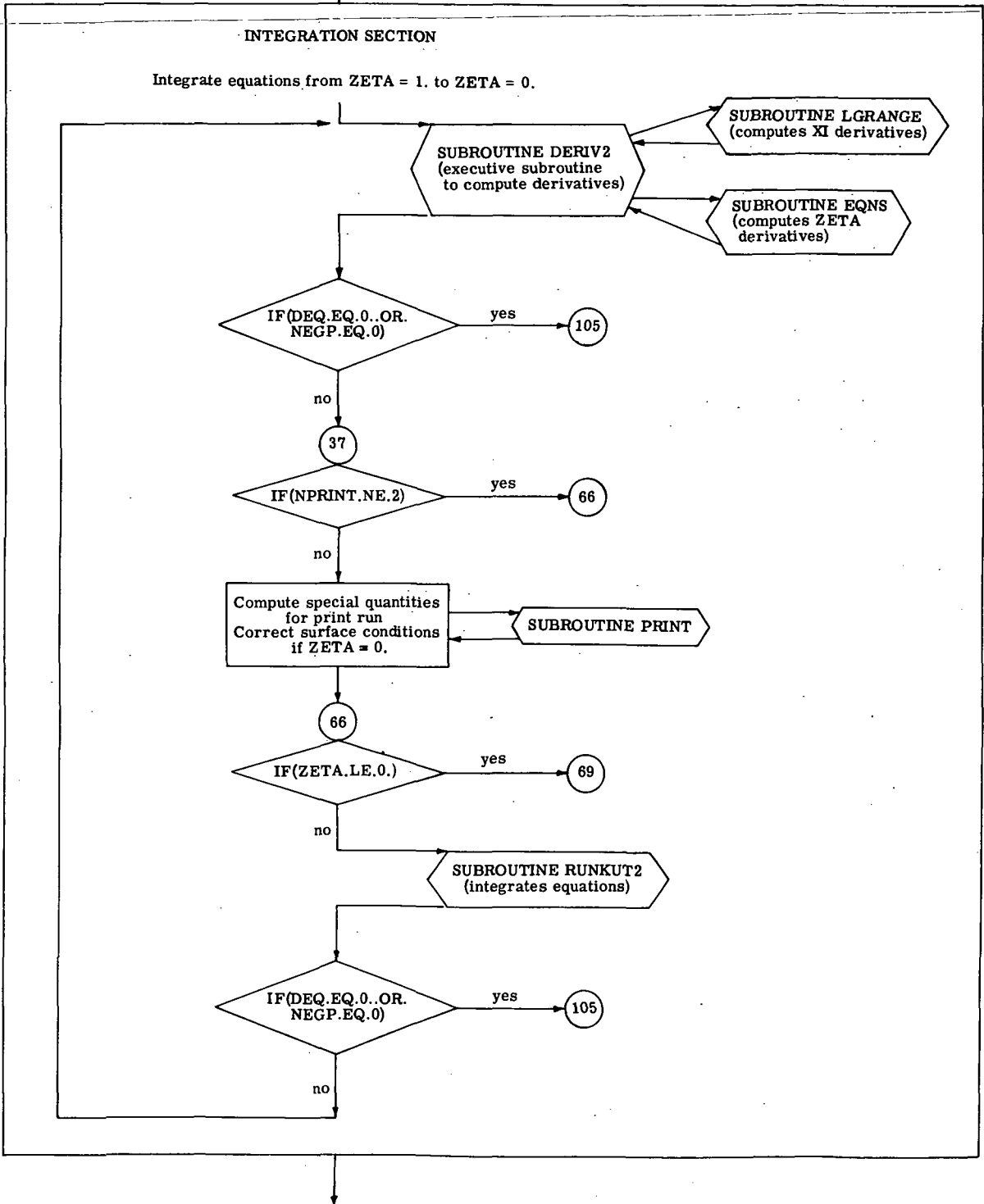
A flow chart of the computer program is given:



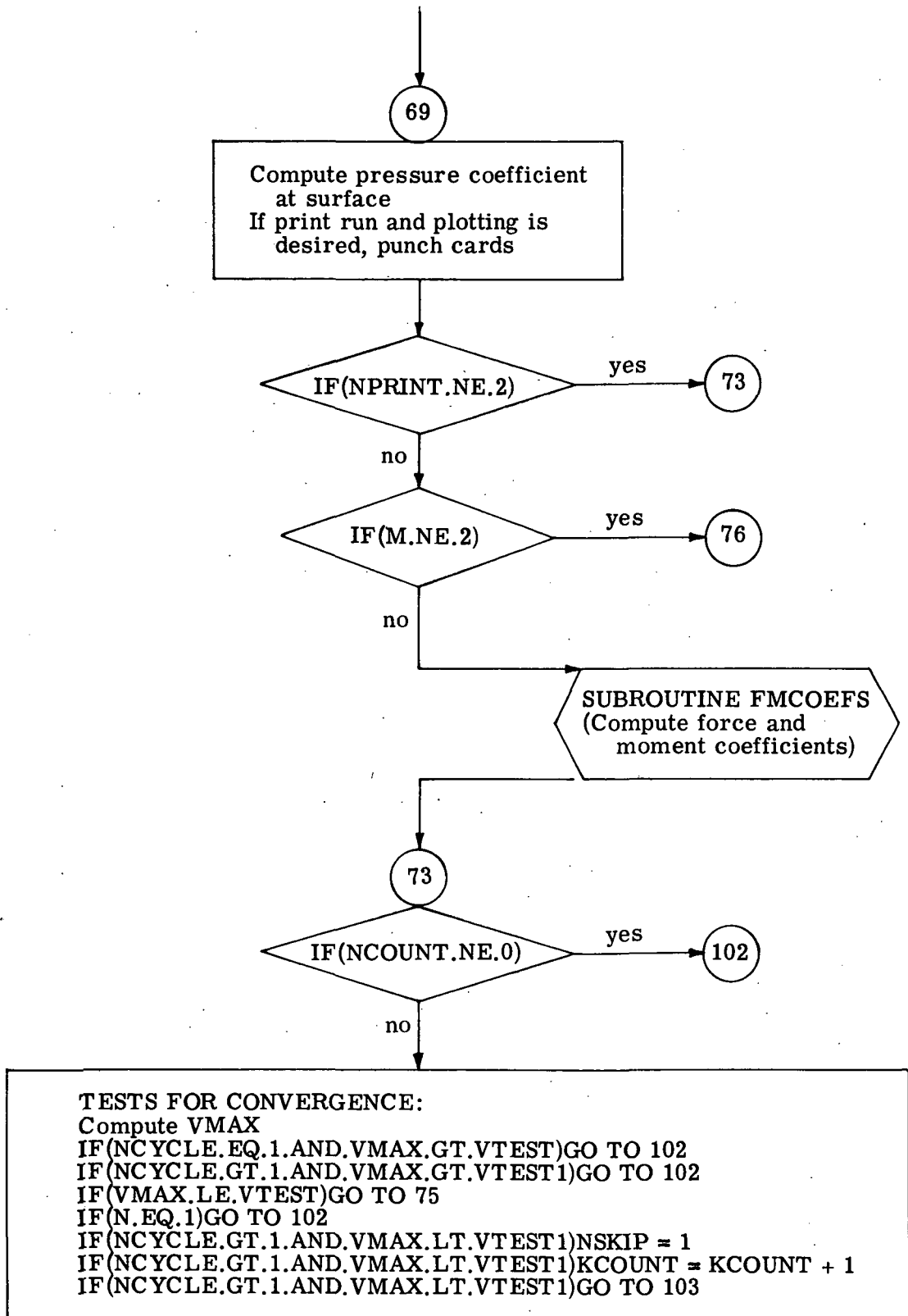
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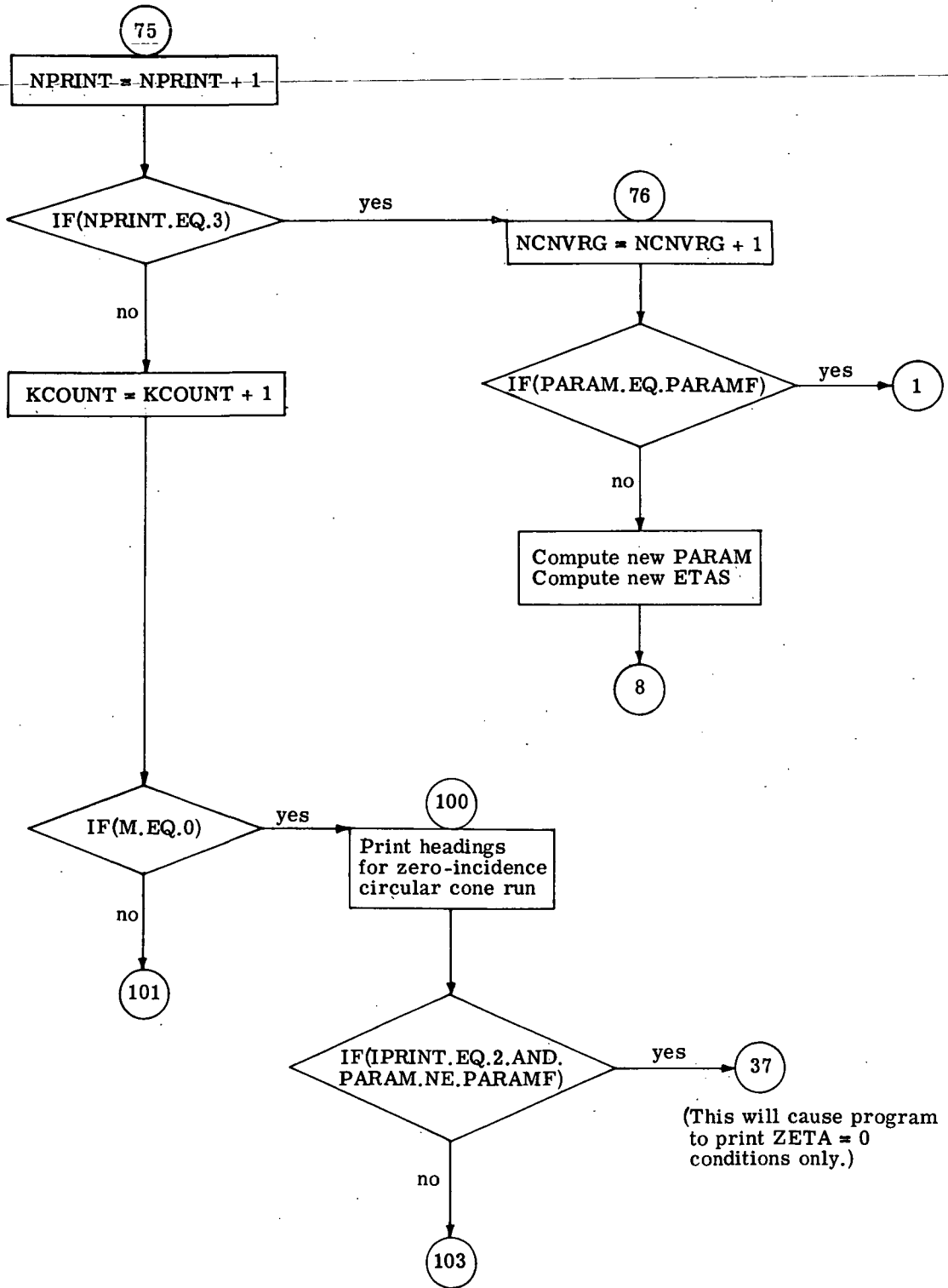
APPENDIX A



APPENDIX A



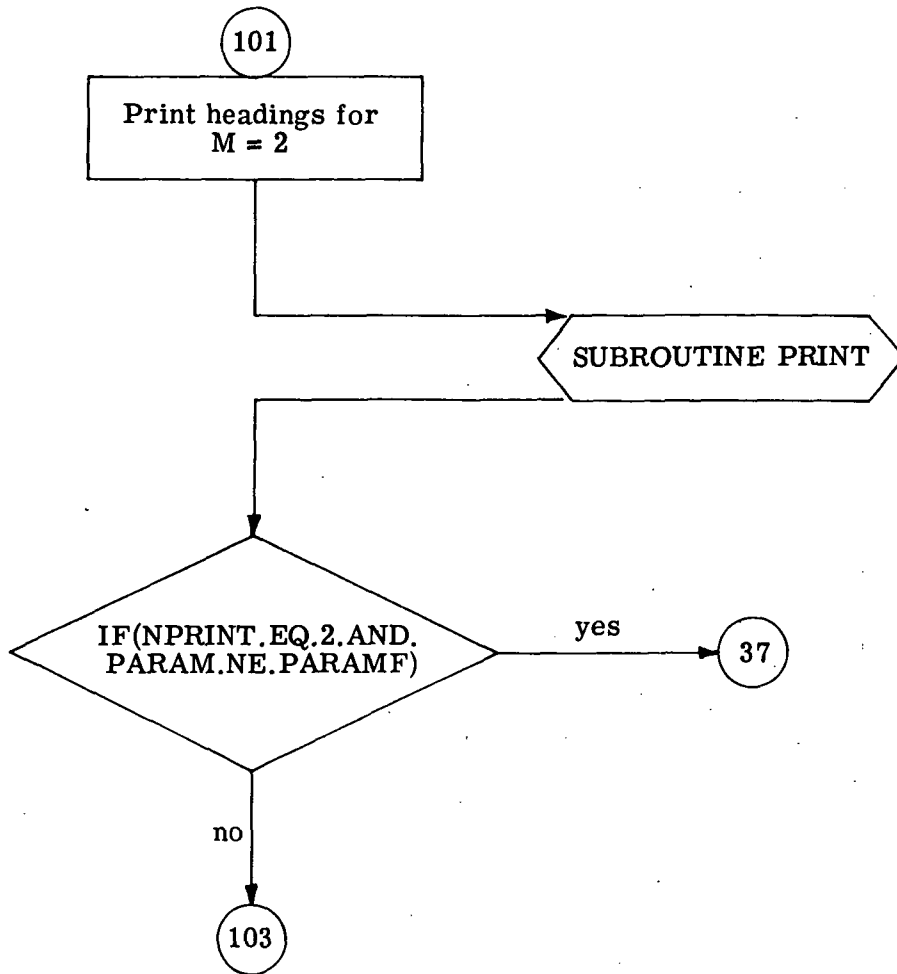
APPENDIX A



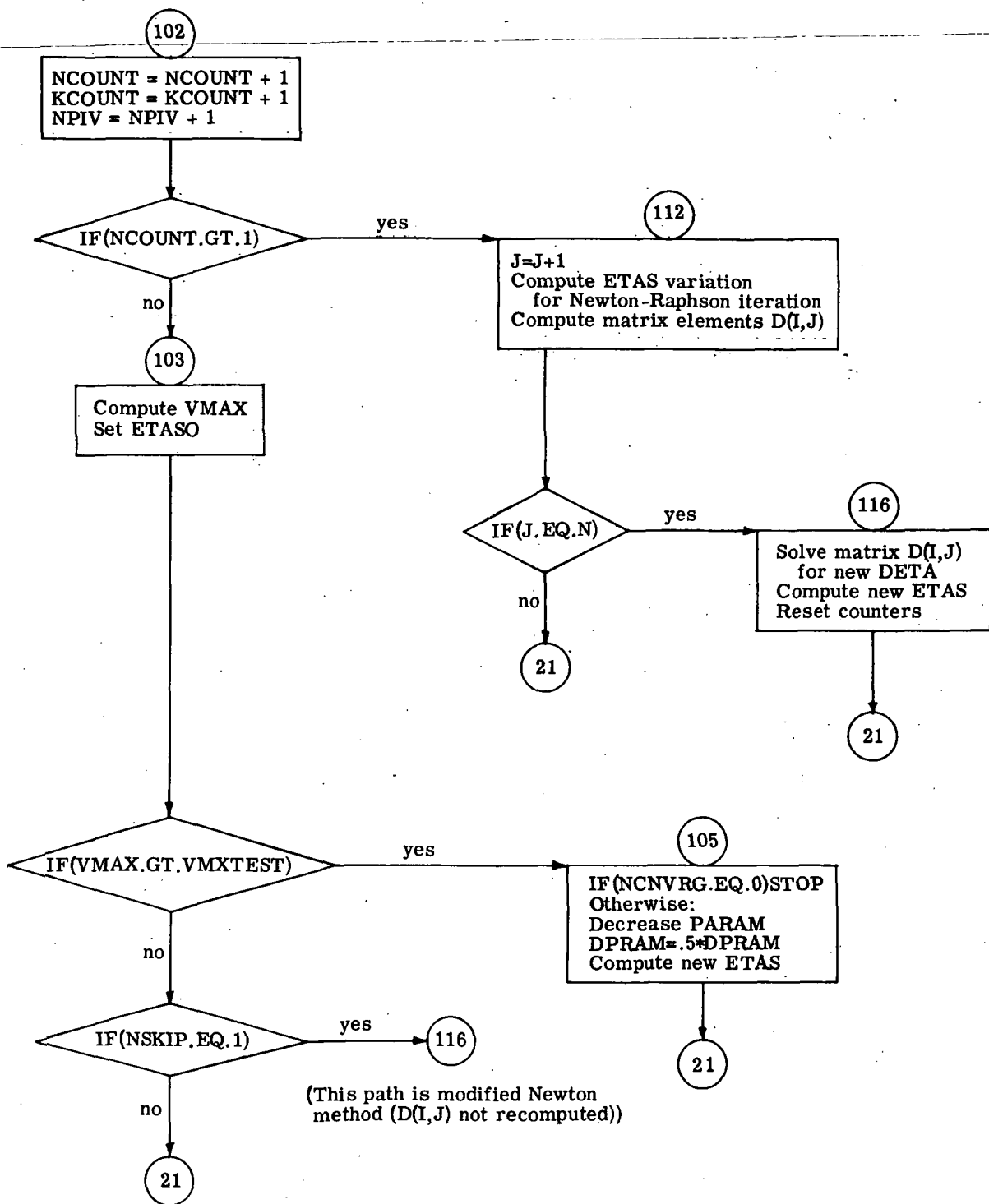
(This will cause program to print ZETA = 0 conditions only.)

(This will give a complete printout from ZETA = 1 to ZETA = 0)

APPENDIX A



APPENDIX A



APPENDIX B

SAMPLE COMPUTATIONS

Two computations are presented which illustrate the operation of the program. The first computation makes use of the built-in approximate shock shape to start the calculations for the zero-incidence circular cone after which T is decremented to obtain the solution for an elliptic cone with $T = 0.6$. The second solution uses the converged values of η_s for $T = 0.6$ to start computations which increment the angle of attack up to 4° . The central processor times, including compilation, for the first and second cases, respectively, were 171 seconds and 116 seconds on the CDC 6600.

Explanations of sections of the sample-computation output are provided at the end of this appendix. Circled numbers at the left side of each section indicate the appropriate explanatory note. These notes describe the first two sets of computations in the first case, the circular cone at zero incidence and the elliptic cone at zero incidence with $T = 0.95$. The printout for other values of the parameters is similar to that which is annotated.

The input for the first case is

<u>Input card</u>	<u>Description</u>
1	STMACH = 8.0, GAMMA = 1.4, T = 1.0, THETAD = 10.0, ALPHAD = 0
2	N = 9, M = 2, NREAD = 0, NSPACE = 1, INCRMT = 1, IPRINT = 2, NCNVRGB = 0, KTRANSF = 1, NPLOT = 0, NPUNCH = 1
3	PARAM = 1, PARAMF = .6, DPRAM1 = -.05, DPRAM = -.1, DPRMIN = -.05
4	SLOPE = 1.
5	VTEST = .001, VTEST1 = .03
6	M2E = 0

The input for the second case is

<u>Input card</u>	<u>Description</u>
1	STMACH = 8.0, GAMMA = 1.4, T = 0.6, THETAD = 10.0, ALPHAD = 0.
2	N = 9, M = 2, NREAD = 1, NSPACE = 1, INCRMT = 2, IPRINT = 2, NCNVRGB = 0, KTRANSF = 1, NPLOT = 0, NPUNCH = 0

APPENDIX B

<u>Input card</u>	<u>Description</u>
3	PARAM = 0., PARAMF = 4.0, DPRAM1 = 0.5, DPRAM = 2.0, DPRMIN = 0.5
4	SLOPE = 1.
5	VTEST = .001, VTEST1 = .03
6	M2E = 0
7	ETAS(I) values from first computation for T = 0.6

Input Cards for First Sample Case

```

80000000+01  14000000+01  10000000+01  10000000+02  00000000+00
 9   2   0   1   1   2   0   1   0   1
10000000+01  60000000+00 -50000000-01 -10000000+00 -50000000-01
1.
.001          .03
0

```

Conical Flow About Elliptic Cones by the Method of Lines

With Incrementation of a Parameter

```

N= 9  M=2  NREAD=0  NSPACE=1  NP= 5  NCONVRG=0
NA= 1  ANA= 0.          NB= 1  BNB= 0.

VTEST= 1.00000000E-03  VTEST1= 3.00000000E-02
SLOPE= 1.00000000E+00  KTRANSF= 1

M2E= 0

```

APPENDIX B

①
 STMACH= 8.0000000E+00 GAMMA= 1.4000000E+00 T= 1.0000000E+00 THETAD= 1.0000000E+01 ALPHAD= 0.
 EPSIGOM= 1.0000000E-C3
 AAST= 4.23895624E-01
 VTEST= 1.0000000E-03 VTEST1= 3.0000000E-02
 M2E= 0
 SLOPE= 1.0000000E+CC KTRANSF= 1
 RANGLE= 0.
 EPSIG= 1.0000000E-03 EPSIGM= 1.0000000E-03 SPACER= 1.0000000E-03 EPSIVAR= 1.0000000E-C8 EPSINT= 2.5000000E-02
 NCYCLE= 1 AT 08/04/71 14.22.56.

②
 ETAS
 5.50956561E-02
 ETASP
 0.
 CP(1) AT SHOCK
 5.03073752E-02
 CP(1) AT ZETA=0
 7.0761156E-02
 V
 1.47011292E-02
 KCOUNT= 1 VMAX= 1.47011292E-02 EPSIG= 1.0000000E-03 SPACER= 1.0000000E-03 VMXTEST= 1.1222428E-01
 DETA
 -2.97082582E-02
 NCYCLE= 2 AT 08/04/71 14.22.58.

③
 ETAS
 5.21258263E-02
 ETASP
 0.
 CP(1) AT SHOCK
 5.81257080E-02
 CP(1) AT ZETA=0
 5.84872446E-02
 V
 9.49271631E-05

④
 ZERO=INCIDENCE CIRCULAR CONE

⑤
 STMACH= 8.0000000E+00 GAMMA= 1.4000000E+00 T= 1.0000000E+00 THETAD= 1.0000000E+01 ALPHAD= 0.
 EPSIGOM= 1.0000000E-C3
 N=1 M=0 NRSAD=0 NSPACE=1 NP=5 NCHVRG=0
 VTEST= 1.0000000E-03 VTEST1= 3.0000000E-02
 M2E= 0
 SLOPE= 1.0000000E+CC KTRANSF= 1
 KCOUNT= 3 VMAX= 9.49271631E-05 EPSIG= 1.0000000E-03 SPACER= 1.0000000E-03 VMXTEST= 1.1222436E-01
 ZETA= 0.

	I=1	I=2	I=3	I=4	I=5	I=6	I=7	I=8	I=9	I=10
P	4.5404E-02									
P/RNASTSQ	2.5269E-01									
P/PTINF	4.1671E-C4									
P/PINF	4.0482E+00									
RHD	2.5686E+CC									
U	2.3046E+00									
V	9.4927E-C5									
W	0.									
UC	2.2696E+00									
VC	4.0020E-C1									
WC	6.8639E-16									
VCC	4.0020E-01									
MCC	0.									
VX	0.									
VY	-4.0020E-C1									
VZ	2.2696E+00									
PSINOR	0.									
THEYNOR	7.9592E+01									
XBAR	0.									
XBHLD	IIIII									
YBAR	-4.0020E+00									
YBHLD	IIIII									
ETA	0.									
G	-2.9708E-02									
DEQNS	5.6061E+CC									
AM	6.201E+00									
CROSSM	7.8230E-C3									
SBAR	8.2482E-02									
POROGAM	1.2120E-C2									
PT/PTINF	8.1367E-C1									
PT	8.8657E+01									
BERNDUL	2.0604E-1C									
DVDZ	2.4029E-C1									
DPDZ	-7.7589E-C5									
PP	0.									
UP	0.									
WP	0.									

⑥
 WINDWARD LINE ZETA LIMIT

U	PHG	S	POROGAM	UC	VC	WC	VX	VY	VZ	PT/PTINF
2.3046E+00	2.5686E+00	8.2482E-02	1.2120E-02	2.2696E+00	4.0020E-01	6.8639E-16	0.	-4.0020E-01	2.2696E+00	8.1367E-01

LEEWARD LINE ZETA LIMIT

U	PHC	S	POREGAM	UC	VC	WC	VX	VY	VZ	PT/PTINF
2.3046E+00	2.5686E+CC	8.2482E-02	1.2120E-02	IIIII	IIIII	IIIII	IIIII	IIIII	IIIII	IIIII

⑦

APPENDIX B

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```
STMACH= 8.0C00C0CCE+00 GAMMA= 1.4000000E+00 T= 1.0000000E+00 THETA0= 1.0000000E+01 ALPHAD= .0.
EPSIG0= 1.0000000E-C3
AAS1= 4.23899624E-01
VTEST= 1.0000000E-C3 VTEST1= 3.0000000E-02
MZE= C
SLOPE= 1.0000000E+00 KTRANSF= 1
RANGLE= 0.
INTCNT= 562
EPSIG= 1.0000000E-03 EPSIGX= 1.0000000E-03 SPACER= 1.0000000E-03 EPSIVAR= 1.0000000E-C8 EPSINT= 2.5000000E-02
MCYCLE= 1 AT 08/04/71 14.23.12.
ETAS
5.21258263E-02 5.21258263E-02 5.21258263E-02 5.21258263E-02 5.21258263E-02 5.21258263E-02 5.21258263E-02 5.21258263E-02
5.21258263E-02
ETASP
-1.70437284E-15 -1.78294202E-15 -5.61136102E-15 -3.14659334E-16 -3.14659334E-16 -3.14659334E-16 -3.14659334E-16 -3.14659334E-16
3.15981575E-15
CP(I) AT SHOCK
5.81257080E-02 5.81257080E-02 5.81257080E-02 5.81257080E-02 5.81257080E-02 5.81257080E-02 5.81257080E-02 5.81257080E-02
5.81257080E-02
CP(I) AT ZETA=0
6.84873446E-02 6.84873446E-02 6.84873446E-02 6.84873446E-02 6.84873446E-02 6.84873446E-02 6.84873446E-02 6.84873446E-02
6.84873446E-02
V
9.49271644E-05 9.49271634E-05 9.49271625E-05 9.49271625E-05 9.49271623E-05 9.49271621E-05 9.49271622E-05 9.49271613E-05
9.49271602E-05
```


APPENDIX B

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```

STMACH= 8.00000000E+00 GAMMA= 1.40000000E+00 T= 9.00000000E-01 THETA= 1.00000000E+01 ALPHAD= 0.
EPSIGM= 1.00000000E-03
AAST= 4.23895674E-01
VTEST= 1.00000000E-03 VTEST1= 3.00000000E-02
M2E= 0
SLOPE= 1.00000000E+00 KTRANSF= 1
RANGLE= 0.
INTCNT= 555
EPSIG= 1.00000000E-03 EPSIGM= 1.00000000E-03 SPACER= 1.00000000E-03 EPSIVAR= 1.00000000E-08 EPSINT= 2.50000000E-02
    
```

NCYCLE= 1 AT 08/04/71 14.24.02.

15

```

ETAS
5.21258263E-02 5.21258263E-02 5.21258263E-02 5.21258263E-02 5.21258263E-02 5.21258263E-02 5.21258263E-02 5.21258263E-02
5.21258263E-02
ETASP
2.85368974E-16 2.96575581E-15 -1.16880593E-14 -2.40433891E-15 2.20983018E-15 -6.65434544E-15 4.67522372E-15 -2.60524180E-15
-1.36253089E-14
CP(I) AT SHOCK
5.19854497E-02 5.27760493E-02 5.49302035E-02 5.71069656E-02 5.81257079E-02 5.71069656E-02 5.48302035E-02 5.27760493E-02
5.19854497E-02
CP(I) AT ZETA=0
6.3742661E-02 6.22910070E-02 6.47580514E-02 6.76538881E-02 6.90026268E-02 6.76538881E-02 6.47580514E-02 6.22910070E-02
5.13742660E-02
V
-1.29580395E-02 -1.01038641E-02 -2.26212560E-03 7.00722059E-03 1.12901814E-02 7.00722060E-03 -2.26212559E-03 -1.01038641E-02
-1.29580395E-02
KCOUNT= 5 VMAX= 1.29580395E-02 EPSIG= 1.00000000E-03 SPACER= 1.00000000E-03 VMXTEST= 1.12522436E-01
DETERM= 3.07170127E-01
    
```

16

```

DETA
1.89315963E-02 1.41672756E-02 2.60993148E-04 -9.01379894E-04 -1.38493720E-03 -9.01380635E-04 2.60994501E-04 1.41672706E-03
1.89315963E-02
NCYCLE= 2 AT 08/04/71 14.28.33.
    
```

17

```

ETAS
5.40186859E-02 5.35425539E-02 5.23868194E-02 5.12244464E-02 5.07408891E-02 5.12244457E-02 5.23868208E-02 5.35425534E-02
5.40186859E-02
ETASP
5.70737849E-16 -1.34483821E-02 -1.91180715E-02 -1.35862656E-02 -9.12009542E-09 1.35862647E-02 1.91180739E-02 1.34483862E-02
-1.72370963E-14
CP(I) AT SHOCK
5.33239299E-02 5.38191407E-02 5.50920708E-02 5.64933699E-02 5.71176935E-02 5.64933694E-02 5.50920718E-02 5.38191403E-02
5.33239299E-02
CP(I) AT ZETA=0
6.31159473E-02 6.36917425E-02 6.52111283E-02 6.69549602E-02 6.77559429E-02 6.69549596E-02 6.52111296E-02 6.36917421E-02
6.31159470E-02
V
2.37640844E-04 -2.58504529E-05 -3.03235054E-04 -7.95653304E-05 1.54874302E-04 -7.95735848E-05 -3.03222178E-04 -2.58922999E-05
2.37624468E-04
    
```


APPENDIX B

18

M=9 M=2 NREAD=3 NSPACE=1 NP=5 MCVRG=1
NA=1 ANA=0
STNACH= 8.0000000E+00 GAMMA= 1.4000000E+00 T= 9.5000000E-01 THETA0= 1.0000000E+01 ALPHA0= 0.
RANGLE= 0.
EPSIG= 1.0000000E-03 EPSIGM= 1.0000000E-03 SPACER= 1.0000000E-03 EPSIVAR= 1.0000000E-08 EPSINT= 2.5000000E-02
MCVCL= 2. VTEST= 1.0000000E-03 VMAX= 3.03235054E-04 AAST= 4.23895624E-01 PTINF= 1.08560472E+02
VTEST= 1.0000000E-03 VTEST1= 3.0000000E-02
MZE= 0
SLOPE= 1.0000000E+00 KTRANSF= 1
KCOUNT= 15 VMAX= 3.03235054E-04 EPSIG= 1.0000000E-03 SPACER= 1.0000000E-03 VMTEST= 1.12670063E-01

19

SUMMARY PRINT BLOCK

Table with columns I=1 to I=10 and rows for variables like PSID, PSISD, XD, YO, XOBAR, YOBAR, KS, YS, XSBAR, YSBAR, ETAS, BETAD, XI, CPSHOCK, CPBODY.

20

Table with columns I and rows for variables TAU, XI, XO, YO, ETAS, ETASP.

21

ZETA= 0.

Table with columns I=1 to I=10 and rows for variables P, P/ROASTSO, P/PTINF, RHO, U, V, W, UC, VC, WCC, WCC, VX, VY, VZ, PSINOR, THETNOR, XBAR, YBAR, YBHD, ETA, G, DEQNS, AM, CROSSM, SBAR, POROGAM, PT/PTINF, BERNOL, DWDZ, DPDZ, PP, UP, WP.

22

WINDWARD LINE ZETA LIMIT

Table with columns U, RHD, S, POROGAM, UC, VC, WC, VX, VY, VZ, PT/PTINF.

LEEWARD LINE ZETA LIMIT

Table with columns U, RHD, S, POROGAM, UC, VC, WC, VX, VY, VZ, PT/PTINF.

23

FORCE COEFFICIENTS

CZ= 6.53537194E-02 CW= 3.03431525E-10 CD= 6.53537194E-02 CL= 3.03431525E-10
YBAR= -8.83952681E-11 ZBAR= 6.66666667E-01 CM= -2.08064643E-10

APPENDIX B

```

STMACH= 8.00000000E+00 GAMMA= 1.40000000E+00 T= 9.00000000E-01 THEIAD= 1.00000000E+01 ALPHAD= 0.
EPSIGM= 1.00000000E-03
AAST= 4.2385624E-01
VTEST= 1.00000000E-03 VTEST1= 3.00000000E-02
MZE= C
SLOPE= 1.00000000E+00 KTRANSF= 1
RANGLE= C.
INTCNT= 549

EPSIG= 1.00000000E-03 EPSIGMX= 1.00000000E-03 SPACER= 1.00000000E-03 EPSIVAR= 1.00000000E-08 EPSINT= 2.50000000E-02

NCYCLE= 1 AT 08/04/71 14.29.23.
ETAS
5.59121456E-02 5.49592814E-02 5.26478126E-02 5.03230665E-02 4.93559519E-02 5.03230650E-02 5.26478153E-02 5.49592804E-02
5.59121456E-02
ETASP
-7.94559377E-15 -2.75714772E-02 -3.91953075E-02 -2.78541699E-02 -1.86977596E-08 2.78542009E-02 3.91953124E-02 2.75714487E-02
-3.91191428E-15
CP(I) AT SHOCK
4.36333337E-02 4.95002356E-02 5.18482708E-02 5.47163004E-02 5.61154345E-02 5.47162995E-02 5.18482727E-02 4.95003348E-02
4.66393337E-02
CP(I) AT ZETA=0
5.78802728E-02 5.98228886E-02 6.15368096E-02 6.51675153E-02 6.70626022E-02 6.51675142E-02 6.15368124E-02 5.88228875E-02
5.78802322E-02
V
-5.63894722E-05 -1.10763317E-03 -1.89480205E-03 -2.85522826E-04 1.04842179E-03 -2.85538879E-04 -1.89477585E-03 -1.10763680E-03
-5.64026022E-05
KCOUNT= 15 VMAX= 1.84480205E-03 EPSIG= 1.00000000E-03 SPACER= 1.00000000E-03 VMXTEST= 1.12822761E-01
DETERM= 2.80852110E-01
DETA
1.34247153E-04 1.96503280E-04 2.23596807E-04 7.34915189E-05 -3.26704956E-05 7.34936784E-05 2.23593524E-04 1.96503899E-04
1.34346843E-04
NCYCLE= 2 AT 08/04/71 14.34.45.
ETAS
5.50464927E-02 5.51557847E-02 5.28734094E-02 5.02965580E-02 4.93222814E-02 5.03365587E-02 5.28734088E-02 5.51557843E-02
5.50464924E-02
ETASP
-7.96468565E-15 -2.64764857E-02 -4.02441731E-02 -3.03485275E-02 7.69344303E-09 3.03485213E-02 4.02441625E-02 2.64764898E-02
-3.41545646E-15
CP(I) AT SHOCK
4.37320085E-02 4.36324350E-02 5.20123217E-02 5.47801497E-02 5.60918609E-02 5.47801501E-02 5.20128212E-02 4.96324348E-02
4.97320085E-02
CP(I) AT ZETA=0
5.79520091E-02 5.99605591E-02 6.17582348E-02 6.52534220E-02 6.69983733E-02 6.52534226E-02 6.17582341E-02 5.89605588E-02
5.79520090E-02
V
-1.93618346E-05 1.12209234E-06 2.74780192E-06 -5.90074459E-06 1.99749039E-07 -5.89223510E-06 2.74207456E-06 1.12796235E-06
-1.93494933E-06

```

APPENDIX B

N= 3 M=2 NREAC=1 NSPACE=3 NP= 5 NCVNRG=2
NA= 1 ANA= 0. NB= 1 RNB= 0.
STMACH= 8.0000000E+00 GAMMA= 1.40000000E+00 T= 9.0000000E-01 THETA= 1.0000000E+01 ALPHA= 0.
RANGE= 0.
EPSIG= 1.0000000E-03 EPSIGM= 1.0000000E-03 SPACER= 1.0000000E-03 EPSIVAR= 1.0000000E-08 EPSINT= 2.5000000E-02
NCYCLE= 2 VTEST= 1.0000000E-03 VMAX= 5.90074459E-06 AAST= 4.2389524E-01 PTINF= 1.08960426E+02
VTEST= 1.0000000E-03 VTEST1= 3.0000000E-02
MZE= 0
SLOPE= 1.0000000E+00 KTRANSF= 1
KCOUNT= 26 VPA= 5.90074459E-06 EPSIG= 1.0000000E-03 SPACER= 1.0000000E-03 VMHTEST= 1.12826425E-01

SUMMARY PRINT BLOCK

Table with 10 columns (I=1 to I=10) and 20 rows (PSID, PSISD, XD, YD, XDBAR, YDBAR, XS, YS, XSBAR, YSBAR, ETAS, BETAD, XI, CP5HCK, CP8DYY) showing numerical values for each parameter across the 10 iterations.

Table with 7 columns (I, TAU, XI, XD, YO, ETAS, ETASP) and 10 rows (1-10) showing numerical values for each parameter across the 10 iterations.

ZETA= 0.

Table with 10 columns (I=1 to I=10) and 30 rows (P, P/RJASTSO, P/PPTINF, P/PPTINF, RMD, U, V, W, UC, VC, WC, VCC, MCC, VX, VY, VZ, PSINDR, THEINDR, XBAR, YBAR, YBHLD, ETA, DEQNS, AN, CROSSM, SBAR, PORDDM, PT/PPTINF, BERNUL, DPZJ, PP, UP, WP) showing numerical values for each parameter across the 10 iterations.

WINDOW LINE ZETA LIMIT

Table with 10 columns (U, PFD, S, PORCGAM, UC, VC, WC, VX, VY, VZ, PT/PTINF) showing numerical values for each parameter.

LEEWARD LINE ZETA LIMIT

Table with 10 columns (U, PFD, S, PORCGAM, UC, VC, WC, VX, VY, VZ, PT/PTINF) showing numerical values for each parameter.

FORCE COEFFICIENTS

Cz= 6.22207376E-02 Cy= 3.45491588E-10 Cd= 6.22307576E-02 Cl= 3.45491988E-10
YBAR= -9.47652744E-11 ZBAR= 6.66666576E-01 Cm= -2.36275497E-10*

APPENDIX B

```

STMACH= 8.0000000E+00 GAMMA= 1.4000000E+00 T= 8.0000000E-01 THETAD= 1.0000000E+01 ALPHAD= 0.
EPSIGM= 1.0000000E-03
AAST= 4.23895624E-01
VTEST= 1.0000000E-03 VTEST1= 3.0000000E-02
MZE= 0
SLOPE= 1.0000000E+00 KTRANSF= 1
RANGLE= 0.
INTCNT= 534

EPSIG= 1.0000000E-03 EPSIGM= 1.0000000E-03 SPACER= 1.0000000E-03 EPSIVAR= 1.0000000E-08 EPSINT= 2.5000000E-02

NCYCLE= 1 AT 08/04/71 14.35.36.
ETAS
6.05045477E-02 5.89717562E-02 5.45233797E-02 4.89612558E-02 4.63900545E-02 4.89612658E-02 5.45233654E-02 5.89717579E-02
6.05045459E-02
ETASP
3.37880377E-15 -5.10888235E-02 -8.90699696E-02 -7.43350400E-02 1.27216364E-07 7.42348700E-02 8.90698825E-02 5.10889688E-02
6.45418027E-15
CP(I) AT SHOCK
4.01578326E-02 4.16406487E-02 4.57216855E-02 5.10011352E-02 5.39884539E-02 5.10011407E-02 4.57216750E-02 4.16406508E-02
4.01578313E-02
CP(I) AT ZETA=0
4.82123171E-02 4.97329155E-02 5.43519132E-02 6.11710440E-02 6.53961132E-02 6.11710500E-02 5.43518962E-02 4.97329198E-02
4.82123201E-02
V
-1.94853445E-03 2.33063061E-04 2.27762106E-03 9.19976049E-04 -1.02281102E-03 9.20089324E-04 2.27747291E-03 2.33050669E-04
-1.94844967E-03
KCOUNT= 27 VMAX= 2.27762106E-03 EPSIG= 1.0000000E-03 SPACER= 1.0000000E-03 VMXTEST= 1.13167277E-01
DETERM= 2.23930617E-01
DETA
7.47246962E-05 -9.24857545E-05 -2.15155374E-04 -1.38775937E-04 1.32280609E-05 -1.38785586E-04 -2.16141046E-04 -9.24865536E-05
7.47272115E-05
NCYCLE= 2 AT 08/04/71 14.40.43.
ETAS
6.05792724E-02 5.88792705E-02 5.43072244E-02 4.88224799E-02 4.64032826E-02 4.88224802E-02 5.43072244E-02 5.88792714E-02
6.05792724E-02
ETASP
4.22350471E-15 -5.41682213E-02 -8.94869352E-02 -7.17948767E-02 3.65661834E-09 7.17948755E-02 8.94869403E-02 5.41682271E-02
8.51495962E-15
CP(I) AT SHOCK
4.02064869E-02 4.16001473E-02 4.55810055E-02 5.08825033E-02 5.39979816E-02 5.08825039E-02 4.55810055E-02 4.16001480E-02
4.02064873E-02
CP(I) AT ZETA=0
4.97500934E-02 5.41536146E-02 6.09850818E-02 6.54544308E-02 6.09850820E-02 5.41536147E-02 4.97500942E-02
4.97500934E-02
V
3.63565881E-06 -4.13366731E-06 3.58628345E-06 -8.11127010E-06 -1.79487195E-06 -8.10913418E-06 3.58526017E-06 -4.12837365E-06
3.64161159E-06

```

APPENDIX B

N= 9 M=2 NREAC=1 ASPACE=1 NP= 5 NCVNRG=3
NA= 1 ANA= 0.
NB= 1 BNB= 0.

STNACH= 8.00000000E+00 GAMMA= 1.40000000E+00 T= 8.00000000E-01 THETA= 1.00000000E+01 ALPHAD= 0.

RANGL= 0.

EPSIG= 1.00000000E-03 EPSIGM= 1.00000000E-03 SPACEP= 1.00000000E-03 EPSIVAR= 1.00000000E-08 EPSINT= 2.50000000E-02

MCYCLE= 2 VTEST= 1.00000000E-03 VMAX= 8.11137010E-06 AAST= 4.23895624E-01 PTINF= 1.08960426E+02

VTEST= 1.00000000E-03 VTEST1= 3.00000000E-02

MZE= 0

SLJPE= 1.00000000E+00 KTRANSF= 1
KCOUNT= 37 VMAX= 8.11137010E-06 EPSIG= 1.00000000E-03 SPACER= 1.00000000E-03 VMXTEST= 1.13165686E-01

SUMMARY PRINT BLOCK

Table with 10 columns (I=1 to I=10) and 17 rows of numerical data representing various physical parameters.

Table with 7 columns (I, TAU, XI, XO, YO, ETAS, ETASP) and 9 rows of numerical data.

ZETA= 0.

Large table with 10 columns (I=1 to I=10) and 39 rows of numerical data, including parameters like P, R/RAJSTQ, P/PINF, etc.

WINDWARD LINE ZETA LIMIT

Table with 10 columns (U, FHC, S, POROGAM, UC, VC, WC, VX, VY, VZ, PT/PTINF) and 1 row of numerical data.

LEEWARD LINE ZETA LIMIT

Table with 10 columns (U, FHC, S, POROGAM, UC, VC, WC, VX, VY, VZ, PT/PTINF) and 1 row of numerical data.

FORCE CCEFFICIENTS

CZ= 5.58773043E-02 Cy= -1.15912119E-09 CD= 5.58773043E-02 CL= -1.15912119E-09
ZBAR= 2.7355976E-10 ZBAR= 6.66606667E-01 CM= 7.88C3212E-10

APPENDIX B

```

STARACH= 8.0000000E+00 GAMMA= 1.4000000E+00 T= 7.CCC0000E-01 THETAD= 1.0000000E+01 ALPHAD= 0.
EPSIGM= 1.0000000E-C3
AAST= 4.23895624E-01
VTEST= 1.0000000E-03 VTEST1= 3.0000000E-02
MZE= 0
SLDPE= 1.0000000E+00 KTRANSF= 1
RANGLE= 0.
INTCNT= 542
EPSIG= 1.0000000E-03 EPSIGX= 1.0000000E-03 SPACER= 1.0000000E-03 EPSIVAR= 1.0000000E-C8 EPSINT= 2.5000000E-02
MCYCLE= 1 AT 08/04/71 14.41.33.
ETAS
6.57490737E-02 6.32654550E-02 5.63592194E-02 4.73573333E-02 4.33702392E-02 4.73573290E-02 5.62552260E-02 6.32654586E-02
6.57490774E-02
ETASP
2.06221158E-15 -8.42162182E-02 -1.49100432E-01 -1.2505506E-01 -5.73739710E-08 1.25055883E-01 1.49100515E-01 8.42161740E-02
-4.08110428E-15
CP(1) AT SPOCK
3.25155250E-02 3.40934796E-02 3.88905924E-02 4.60771294E-02 5.18500397E-02 4.60771376E-02 3.88905977E-02 3.40934814E-02
3.25155273E-02
CP(1) AT ZETA=0
3.96779986E-02 4.10897283E-02 4.58533962E-02 5.50538919E-02 6.38243004E-02 5.50538906E-02 4.58534064E-02 4.10897298E-02
3.96779993E-02
V
1.06714185E-03 1.02872411E-04 -2.01853932E-03 -5.14720956E-04 -4.90439374E-04 -5.14773373E-04 -2.01846954E-03 1.02912137E-04
1.06711690E-03
RCOUNT= 38 VPAX= 2.01853932E-03 EPSIG= 1.0000000E-03 SPACER= 1.0000000E-03 VMXTEST= 1.13543428E-01
DETERM= 1.61954078E-01
DETA
6.42158948E-05 5.12949475E-C6 2.61804489E-04 6.90076870E-05 1.50031559E-04 6.90119831E-C5 2.61795682E-04 9.12565645E-06
6.42114645E-05
MCYCLE= 2 AT 08/04/71 14.46.44.
ETAS
6.58132896E-02 6.32745845E-02 5.66170239E-02 4.74263409E-C2 4.35202708E-02 4.74263410E-02 5.66170227E-02 6.32745843E-02
6.58132889E-02
ETASP
1.37480772E-15 -8.20542882E-02 -1.48541466E-01 -1.26412054E-01 2.58082281E-09 1.26412041E-01 1.48541463E-01 8.20542939E-02
-8.55287937E-15
CP(1) AT SPOCK
3.25549427E-02 3.40818064E-02 3.90488275E-02 4.61410855E-02 5.19556313E-02 4.61410854E-02 3.90488267E-02 3.40818063E-02
3.25549422E-02
CP(1) AT ZETA=0
3.96612636E-02 4.10207947E-02 4.60410509E-02 5.51670752E-02 6.39200737E-02 5.51670748E-02 4.60410498E-02 4.10207947E-02
3.96612633E-02
V
-1.65205243E-06 -2.87239876E-06 2.71192694E-06 -2.76495214E-06 -4.63137971E-07 -2.76422458E-06 2.70187141E-06 -2.87419557E-06
-1.65065455E-06

```

APPENDIX B

9 # 2 NREAD=1 NSPACE=1 NP= 5 MCVNRG=4
NA= 1 NHA= 0
STXACH= 8.00000000E+00 GAMMA= 1.40000000E+00 T= 7.00000000E-01 THETAD= 1.00000000E+01 ALPHAD= 0.
RANGLE= 0.
EPSIG= 1.00000000E-03 EPSIGX= 1.00000000E-03 SPACEP= 1.00000000E-03 EPSIVAR= 1.00000000E-08 EPSINT= 2.50000000E-02
MCYCLE= 2 VTST= 1.00000000E-03 VMAX= 2.87419557E-06 AAST= 4.22895624E-01 PTINF= 1.08960426F+02
VTST= 1.00000000E-03 VTST1= 3.00000000E-02
MZE= 0
SLJPE= 1.00000000E+00 KTRANSF= 1
KCOUNT= 48 VMAX= 2.87419557E-06 EPSIG= 1.00000000E-03 SPACER= 1.00000000E-03 VMXTEST= 1.13524119E-01

SUMMARY PRINT BLOCK

Table with 10 columns (I=1 to I=10) and multiple rows (PSID, X0, XOBAR, etc.) containing numerical values.

Table with 10 columns (I, XI, XO, YO, ETAS, ETASP) and 10 rows of numerical data.

ZETA= C.

Large table with 10 columns (I=1 to I=10) and many rows (P, P/ROASTSQ, etc.) containing numerical values.

WINDWARD LINE ZETA LIMIT

Table with 10 columns (U, RHO, POROGAM, UC, VC, WC, VX, VY, VZ, PT/PTINF) and 2 rows of numerical data.

LEEWARD LINE ZETA LIMIT

Table with 10 columns (U, RHO, POROGAM, UC, VC, WC, VX, VY, VZ, PT/PTINF) and 2 rows of numerical data.

FCRC CEFICIENTS

CZ= 4.93030902E-02 CV= 8.47105821E-10 CD= 4.93030902E-02 CL= 8.47105821E-10
YBAR= -1.76233989E-10 ZBAR= 6.66666667E-01 CM= -5.73426094E-10

APPENDIX B

```

-----
STMACH=--8.0000000E+0C-- GAMMA= -1.4000000E+0C--T= -6.CC00000E-01 THETAD=--1.0000000E+01--ALPHA= 0.
EPSIGM= 1.0000000E-03
AAST= 4.23895524E-01
VTEST= 1.0000000E-03 VTEST1= 3.C000000E-02
MZE= 0
SLJPE= 1.0000000E+0C KTRANSF= 1
RANGLE= 0.
INTCNT= 535

EPSIG= 1.0000000E-03 EPSIGM= 1.0000000E-03 SPACER= 1.0000000E-03 EPSIVAR= 1.0000000E-05 EPSINT= 2.5000000E-02

NCYCLE= 1 AT 08/04/77 14.47.36.
ETAS
7.17495442E-02 6.83417268E-02 5.98028079E-02 4.62081412E-02 4.06742459E-02 4.62081411E-02 5.98028037E-02 6.83417230E-02
7.17485258E-02
ETASP
-1.71669201E-16 -1.09969229E-01 -2.18635250E-01 -1.96022889E-01 4.96504407E-09 1.96022844E-01 2.18635213E-01 1.09969233E-01
-1.47248656E-14
CP(1) AT SHOCK
2.57185511E-02 2.71312239E-02 3.25938638E-02 4.02067556E-02 4.99642127E-02 4.02067547E-02 3.25938607E-02 2.71312217E-02
2.57185486E-02
CP(1) AT ZETA=0
3.18264032E-02 3.29667162E-02 3.78422765E-02 4.74111446E-02 6.22466445E-02 4.74111425E-02 3.78422712E-02 3.29667139E-02
3.18264008E-02
V
-5.9543570E-04 8.96580725E-04 -1.04556122E-03 1.06644452E-05 -3.11654826E-03 1.06655817E-05 -1.04559695E-03 8.96552226E-04
-5.95446112E-04
KCOUNT= 49 VMAX= 3.11654826E-03 EPSIG= 1.0000000E-03 SPACER= 1.0000000E-03 VMXTEST= 1.13901763E-01
DETERM= 1.02596375E-01
DETA
2.26749504E-04 -1.50012641E-04 3.04148110E-04 2.11108647E-05 3.96943556E-04 2.11107987E-05 3.04152947E-04 -1.50007970E-04
2.26753718E-04
NCYCLE= 2 AT 08/04/77 14.53.44.
ETAS
7.13752927E-02 6.81917142E-02 6.01069560E-02 4.62292520E-02 4.10711895E-02 4.62292519E-02 6.01069567E-02 6.81917151E-02
7.13752935E-02
ETASP
-2.97510361E-15 -1.09298212E-01 -2.16839878E-01 -1.95167423E-01 -3.06864049E-09 1.95167429E-01 2.16839998E-01 1.09298214E-01
-1.43085416E-14
CP(1) AT SHOCK
2.58497446E-02 2.70381576E-02 3.27478878E-02 4.02049007E-02 5.02404907E-02 4.02049007E-02 3.27478883E-02 2.70381581E-02
2.58497452E-02
CP(1) AT ZETA=0
3.19477657E-02 3.28410192E-02 3.79526754E-02 4.73487283E-02 6.25566225E-02 4.73487284E-02 3.79526765E-02 3.28410198E-02
3.19477661E-02
V
3.76248864E-06 -5.76764917E-07 -3.18456270E-06 -1.10974277E-06 8.35007932E-06 -1.11283905E-06 -3.17889150E-06 -5.69367358E-07
3.76567373E-06

```


APPENDIX B

ZETA = 5.CCCCCCOE-01

Table with 11 columns (I=1 to I=10) and rows of data points for variables P, P/ROASTSO, P/PTINF, RHO, U, V, W, VC, WC, VCC, MCC, XZ, VV, PSINOR, THE TNOR, XBAR, XBHL, YBAR, YBHL, ETA, G, DEQNS, AM, CROSSM, SBAR, PORDGAM, PT/PTINF, PT, BERNOUL, DPDZ, DUDZ, DWDZ, DSDZ, PP, UP, VP, WP, SBARP. Each row contains 11 numerical values corresponding to the columns.

ZETA = 8.00000000E-01

Table with 11 columns (I=1 to I=10) and rows of data points for variables P, P/ROASTSO, P/PTINF, RHO, U, V, W, VC, WC, VCC, MCC, XZ, VV, PSINOR, THE TNOR, XBAR, XBHL, YBAR, YBHL, ETA, G, DEQNS, AM, CROSSM, SBAR, PORDGAM, PT/PTINF, PT, BERNOUL, DPDZ, DUDZ, DWDZ, DSDZ, PP, UP, VP, WP, SBARP. Each row contains 11 numerical values corresponding to the columns.

APPENDIX B

	ZETA= 0.									
	I=1	I=2	I=3	I=4	I=5	I=6	I=7	I=8	I=9	I=10
P	2.7135E-02	2.7578E-02	3.0123E-02	3.4812E-02	4.2441E-02	3.4812E-02	3.0123E-02	2.7578E-02	2.7135E-02	
P/ROASTSQ	1.5701E-01	1.5348E-01	1.6764E-01	1.9374E-01	2.3619E-01	1.9374E-01	1.6764E-01	1.5348E-01	1.5101E-01	
P/PTINF	2.4904E-04	2.5310E-04	2.7645E-04	3.1949E-04	3.8951E-04	3.1949E-04	2.7645E-04	2.5310E-04	2.4904E-04	
P/PINF	2.4313E+CC	2.4710E+00	2.6990E+00	3.1192E+00	3.8027E+00	3.1192E+00	2.6990E+00	2.4710E+00	2.4313E+00	
RHO	1.8012E+00	1.8222E+00	1.9408E+00	2.1521E+00	2.4793E+00	2.1521E+00	1.9408E+00	1.8222E+00	1.8012E+00	
U	2.3266E+00	2.3255E+00	2.3204E+00	2.3144E+00	2.3094E+00	2.3144E+00	2.3204E+00	2.3255E+00	2.3266E+00	
V	3.7731E-06	-5.7667E-07	-3.1874E-06	-1.1091E-06	8.3500E-06	-1.1128E-06	-3.1789E-06	-5.6937E-07	3.7657E-06	
W	-1.3225E-13	-5.7929E-02	-1.0507E-01	-1.1609E-01	3.0585E-09	1.1609E-01	1.0507E-01	5.7929E-02	-4.1893E-13	
UC	2.3737E+CC	2.3121E+00	2.3054E+00	2.2919E+00	2.2743E+00	2.2919E+00	2.3054E+00	2.3121E+00	2.3737E+00	
VC	2.4478E-01	2.5280E-01	2.8057E-01	3.4036E-01	4.0102E-01	3.4036E-01	2.8057E-01	2.5280E-01	2.4478E-01	
WC	-1.3183E-13	2.2772E-02	4.0118E-02	3.6554E-02	3.0716E-09	-3.6554E-02	-4.0118E-02	-2.2771E-02	1.7807E-11	
VCC	2.4478E-01	2.4775E-01	2.6757E-01	3.2545E-01	4.0102E-01	3.2545E-01	2.6757E-01	2.4775E-01	2.4478E-01	
WCC	-1.3225E-13	-5.5216E-02	-9.3470E-02	-1.0612E-01	3.0585E-09	1.0612E-01	9.3470E-02	5.5216E-02	-4.1921E-13	
VX	-1.3225E-13	7.1792E-02	1.5593E-01	2.7610E-01	4.0102E-01	2.7610E-01	1.5593E-01	7.1791E-02	-2.8097E-11	
VY	-2.4478E-01	-2.4346E-01	-2.3667E-01	-2.0236E-01	3.0512E-09	2.0236E-01	2.3667E-01	2.4346E-01	2.4478E-01	
VZ	2.3737E+CC	2.3121E+00	2.3054E+00	2.2919E+00	2.2743E+00	2.2919E+00	2.3054E+00	2.3121E+00	2.3737E+00	
PSINDR	-3.2751E-12	1.7785E+00	3.8695E+00	6.8653E+00	1.0000E+01	6.8693E+00	3.8695E+00	1.7784E+00	-6.9480E-10	
THEINOR	8.3961E+01	8.3992E+01	8.4152E+01	8.4990E+01	9.0000E+01	8.4990E+01	8.4152E+01	8.3992E+01	8.3961E+01	
XBAR	0.	3.1552E-01	6.1784E-01	8.7723E-01	1.0000E+00	8.7723E-01	6.1784E-01	3.1552E-01	-6.9800E-11	
XHLD	0.	-6.9800E-11	-6.9800E-11	-6.9800E-11	-6.9800E-11	-6.9800E-11	-6.9800E-11	-6.9800E-11	-6.9800E-11	
YBAR	-5.0000E-01	-5.6935E-01	-4.7178E-01	-2.8805E-01	-1.8308E-01	2.8805E-01	4.7178E-01	5.6935E-01	6.0000E-01	
YHLD	-6.0000E-01	6.0000E-01	6.0000E-01	6.0000E-01	6.0000E-01	6.0000E-01	6.0000E-01	6.0000E-01	6.0000E-01	
ETA	0.	0.	0.	0.	0.	0.	0.	0.	0.	
G	-3.1464E-03	-3.1640E-03	-3.2556E-03	-3.3525E-03	-3.5262E-03	-3.3525E-03	-3.2556E-03	-3.1640E-03	-3.1464E-03	
DEQNS	5.5689E+00	5.6005E+00	5.6084E+00	5.6258E+00	5.6551E+00	5.6258E+00	5.6084E+00	5.6005E+00	5.5689E+00	
AM	6.7911E+00	6.7737E+00	6.6795E+00	6.5274E+00	6.3235E+00	6.5274E+00	6.6795E+00	6.7737E+00	6.7911E+00	
CROSSM	3.8803E-13	1.6870E-01	3.0214E-01	3.2700E-01	8.3748E-09	3.2700E-01	3.0214E-01	1.6870E-01	1.2228E-12	
SBAR	4.4571E-02	6.4571E-02	6.4571E-02	6.4571E-02	6.4571E-02	6.4571E-02	6.4571E-02	6.4571E-02	4.4571E-02	
POROGAM	1.1905E-02	1.1905E-02	1.1905E-02	1.1905E-02	1.1905E-02	1.1905E-02	1.1905E-02	1.1905E-02	1.1905E-02	
PT/PTINF	9.5525E-01	8.5093E-01	8.5093E-01	8.5093E-01	8.5093E-01	8.5093E-01	8.5093E-01	8.5093E-01	9.5525E-01	
PT	9.2717E+01	9.2717E+01	9.2717E+01	9.2717E+01	9.2717E+01	9.2717E+01	9.2717E+01	9.2717E+01	9.2717E+01	
BERNOUL	-2.3590E-12	9.3827E-11	-2.8993E-10	-1.1044E-10	-1.1603E-11	-1.1043E-10	9.3804E-10	-5.2885E-09	-2.3448E-12	
DVDZ	-2.5296E-01	-2.4611E-01	-2.3563E-01	-2.4399E-01	-2.8188E-01	-2.4399E-01	-2.3563E-01	-2.4611E-01	-2.5296E-01	
DPDZ	1.3845E-27	2.8193E-04	1.2057E-03	2.2823E-03	2.6963E-18	2.2823E-03	1.2057E-03	2.8193E-04	1.3912E-26	
PP	-4.2624E-16	2.4959E-02	6.3750E-02	1.3674E-01	-1.9696E-10	-1.3674E-01	-6.3750E-02	-2.4959E-02	-2.1771E-15	
UP	-1.3225E-13	-5.7929E-02	-1.0507E-01	-1.1609E-01	3.0585E-09	1.1609E-01	1.0507E-01	5.7929E-02	-4.1893E-13	
WP	-1.1248E+00	-1.0039E+00	-5.5985E-01	1.0039E+00	2.2445E+00	1.0039E+00	-5.5985E-01	-1.0039E+00	-1.1248E+00	

WINDWARD LINE ZETA LIMIT

U	RHC	S	POROGAM	UC	VC	WC	VX	VY	VZ	PT/PTINF
2.3307E+00	1.9617E+00	1.8312E-02	1.1367E-02	2.3178E+00	2.4521E-01	4.2057E-16	0.	-2.4521E-01	2.3178E+00	9.5525E-01

LEEWARD LINE ZETA LIMIT

U	RHO	S	POROGAM	UC	VC	WC	VX	VY	VZ	PT/PTINF
2.3307E+00	1.6617E+00	1.8312E-02	1.1367E-02	2.3178E+00	2.4521E-01	1.8258E-11	-2.8256E-11	2.4521E-01	2.3178E+00	9.5525E-01

FORCE COEFFICIENTS

CZ= 4.23665934E-02 CY= -1.11726977E-09 CD= 4.23665934E-02 CL= -1.11726977E-09
 YBAR= 1.45010171E-10 ZBAR= 6.6666567E-01 CM= 7.53108427E-10

APPENDIX B

Input Cards for Second Sample Case

```

80000000+01  14000000+01  60000000+00  10000000+02  00000000+00
 9   2   1   1   2   2   0   1   0   0
00000000+00  40000000+01  10000000+00  20000000+01  25000000+00
1.
.001          .03
  n
7.19752927E-02  6.81917142E-02  6.01069560E-02  4.62292520E-02  4.10711895E-02
4.62292519E-02  6.01069567E-02  6.81917151E-02  7.19752935E-02

```

Conical Flow About Elliptic Cones by the Method of Lines With Incrementation of a Parameter

```

N= 9  M=2  NREAD=1  NSPACE=1  NP= 5  NCVRG=0
NA= 1  ANA= 0.          NR= 1  BNB= 0.

VTEST= 1.00000000E-03  VTEST1= 3.00000000E-02
SLOPE= 1.00000000E+00  KTRANSF= 1

MZE= 0

```

```

-----
STACH= 8.00000000E+00  GAMMA= 1.40000000E+00  T= 6.00000000E-01  THETA= 1.00000000E+01  ALPHA= 0.
-----
EPSIGM= 1.00000000E-03
AAST= 4.23895624E-01
-----
VTEST= 1.00000000E-03  VTEST1= 3.00000000E-02
-----
RZE= C
-----
SLOPE= 1.00000000E+00  KTRANSF= 1
-----
RANGLE= 0.
-----
INTCNT= 335
-----
EPSIG= 1.00000000E-03  EPSIGM= 1.00000000E-03  SPACER= 1.00000000E-03  EPSIVAR= 1.00000000E-08  EPSINT= 2.50000000E-02
-----
NCYCLE= 1  AT  11/23/71  10.43.45.
-----
ETAS
7.19752927E-02  6.81917142E-02  6.01069560E-02  4.62292520E-02  4.10711895E-02  4.62292519E-02  6.01069567E-02  6.81917151E-02
7.19752935E-02
ETASP
-1.84558363E-16  -1.09298214E-01  -2.16839587E-01  -1.95167422E-01  -2.24633824E-09  1.95167429E-01  2.16839598E-01  1.09298213E-01
-1.87734140E-14
CP(1) AT SP0CK
2.58497446E-02  2.70381576E-02  3.27478878E-02  4.02045007E-02  5.02404908E-02  4.02049007E-02  3.27478884E-02  2.70381581E-02
2.58497451E-02
CP(1) AT ZETA=0
3.19477657E-02  3.28410192E-02  3.79526754E-02  4.73487282E-02  6.25566226E-02  4.73487284E-02  3.79526765E-02  3.28410198E-02
3.19477661E-02
V
3.76373538E-06  -5.76565892E-07  -3.18515018E-06  -1.11030199E-06  8.35045244E-06  -1.11252286E-06  -3.1752788E-06  -5.69227898E-07
3.76530080E-06

```

APPENDIX B

M= 9 N=2 NREAD=1 NSPACE=1 NP= 5 NCONV=0
NA= 1 NAA= G. NB= 1 NBD= G.

STMACH= 8.0000000E+00 EAMMA= 1.4000000E+00 T= 6.0000000E-01 THETA= 1.0000000E+01 ALPHA= 0.
EPSIG= 1.0000000E-03 EPSIGM= 1.0000000E-03 SPACER= 1.0000000E-03 EPSIVAR= 1.0000000E-08 EPSINT= 2.5000000E-02
NGCYCLE= 1 VTEST= 1.0000000E-03 VMAX= 8.35045244E-06 AAST= 4.23895624E-01 PTAFA= 1.08960426E+02
VTEST= 1.0000000E-03 VTEST1= 3.0000000E-02
MZE= C
SLOPE= 1.0000000E+00 KTRANSF= 1
KCOUNT= 1 VMAX= 8.25045244E-06 EPSIG= 1.0000000E-03 SPACER= 1.0000000E-03 VMXTEST= 1.13847636E-01

SUMMARY PRINT BLOCK

Table with 10 columns (I=1 to I=10) and multiple rows of numerical data for variables like PSID, PSISD, X0, Y0, X0BAR, Y0BAR, XS, YS, XSBAR, YSBAR, ETAS, BETAD, XI, CP5HOCK, CPBODY.

Table with 7 columns (I, TAU, XI, XC, Y0, ETAS, ETASP) and 9 rows of numerical data.

ZETA= 0.

Large table with 10 columns (I=1 to I=10) and many rows of numerical data for variables like P, P/ROASTSC, P/PTINF, P/PINF, RHD, U, V, W, WC, VC, WC, VCC, WCC, VX, VY, VZ, PSINDR, THE TNDR, XRHLD, YBAR, YRHLD, ETA, G, DEONS, AM, CROSSH, SRAR, PORUGAM, PT/PTINF, PT, BERNOUL, DWDZ, DPOZ, PPZ, UP, WP.

WINDWARD LINE ZETA LIMIT

Table with 10 columns (U, PHO, S, PORCGAM, UC, VC, WC, VX, VY, VZ, PT/PTINF) and 2 rows of numerical data.

LEEWARD LINE ZETA LIMIT

Table with 10 columns (U, PHO, S, PORCGAM, UC, VC, WC, VX, VY, VZ, PT/PTINF) and 2 rows of numerical data.

FORCE COEFFICIENTS

CZ= 4.23900661E-02 CV= -1.73145544E-09 CD= 4.23900661E-02 CL= -1.73145544E-09
YBAR= 3.03019755E-10 ZBAR= 6.66666667E-01 CM= 1.16714849E-09

APPENDIX B

```

SYMACH= 8.0000000E+00 GAMMA= 1.4000000E+00 T= 6.0000000E-01 THETAD= 1.0000000E+01 ALPHAD= 1.0000000E-01
EPSIGM= 1.0000000E-03
AAS= 4.23895624E-01
VTEST= 1.0000000E-03 VTEST1= 3.0000000E-02
MZE= 0
SLOPE= 1.0000000E+00 KTRANSF= 1
RANGLE= 1.65584572E-02
EPSIG= 1.0000000E-03 EPSTGMX= 1.0000000E-03 SPACER= 1.0000000E-03 EPSIVAR= 1.0000000E-08 EPSINT= 2.5000000E-02
NCYCLE= 1 AT 11/23/71 10.44.25.
ETAS
7.10752927E-02 6.81917142E-02 6.01069560E-02 4.62292520E-02 4.10711895E-02 4.62292519E-02 6.01069567E-02 6.81917151E-02
7.19752535E-02
ETASP
-1.84558363E-16 -1.09258214E-01 -2.16839987E-01 -1.95167422E-01 -2.24633824E-09 1.95167429E-01 2.16839998E-01 1.09298213E-01
-1.87734140E-14
CP(I) AT SPOCK
2.68649448E-02 2.80235122E-02 3.36347846E-02 4.08527973E-02 5.02402584E-02 3.95597530E-02 3.18672759E-02 2.60615452E-02
2.48440665E-02
CP(I) AT ZETA=0
3.31102988E-02 3.40260143E-02 3.91575001E-02 4.84372601E-02 6.25323730E-02 4.63263643E-02 3.67981562E-02 3.16693858E-02
3.07832291E-02
V
3.48546669E-03 3.04583404E-03 2.49925858E-03 1.50756657E-03 -2.87172450E-05 -2.02377997E-03 -2.59574138E-03 -3.13299132E-03
-3.54570000E-03
KCOUNT= 2 VMAX= 3.54570000E-03 EPSIG= 1.0000000E-03 SPACER= 1.0000000E-03 VMXTEST= 1.13847682E-01
DETERM= 1.01689119E-01
DETA
-5.52070562E-04 -5.05545334E-04 -3.92264699E-04 -2.15575846E-04 -1.94939215E-06 2.15562375E-04 3.56269468E-04 5.15607810E-04
5.69846920E-04
NCYCLE= 2 AT 11/23/71 10.49.34.
ETAS
7.14232221E-02 6.76861689E-02 5.97146913E-02 4.60132762E-02 4.10692401E-02 4.64448143E-02 6.05032262E-02 6.87073229E-02
7.25449404E-02
ETASP
-2.94372203E-15 -1.07817311E-01 -2.14194646E-01 -1.91571161E-01 3.98915366E-03 1.98842690E-01 2.19578685E-01 1.10926022E-01
-1.52228381E-14
CP(I) AT SPOCK
2.65427949E-02 2.77148372E-02 3.33618575E-02 4.06561636E-02 5.02414689E-02 3.97593277E-02 3.21421413E-02 2.63731177E-02
2.51712561E-02
CP(I) AT ZETA=0
3.27251379E-02 3.36315758E-02 3.87514139E-02 4.80592930E-02 6.25519315E-02 4.66378439E-02 3.71597108E-02 3.20650576E-02
3.11884848E-02
V
6.78013186E-05 6.01856081E-06 -2.52866966E-05 -1.56674581E-05 -1.25864189E-05 -1.58065137E-05 -1.77344153E-05 8.87268619E-06
4.81165288E-05

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APPENDIX B

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STMACH= 8.0000000E+00 GAMMA= 1.4000000E+00 T= 6.0000000E-01 THETA0= 1.0000000E+01 ALPHAD= 2.0000000E+00
EPSIGM= 1.0000000E-03
AAST= 4.23895624E-01
VTEST= 1.0000000E-03 VTEST1= 3.0000000E-02
MZE= C
SLOPE= 1.0000000E+00 RTRANSF= 1
RANGLE= 3.31169144E-01
EPSIG= 1.0000000E-03 EPSIGX= 1.0000000E-03 SPACER= 1.0000000E-03 EPSIVAR= 1.0000000E-08 EPSINT= 2.5000000E-02
NCYCLE= 1 AT 11/23/71 10.50.14.
ETAS
6.09338815E-02 5.80808075E-02 5.22616620E-02 4.19057351E-02 4.10322017E-02 5.05404994E-02 6.80323461E-02 7.85038713E-02
8.33682319E-02
ETASP
-1.51030047E-15 -7.96801622E-02 -1.63933172E-01 -1.23242202E-01 7.97831158E-02 2.68672648E-01 2.71613743E-01 1.41854379E-01
-2.08741818E-14
CP(1) AT SPOCK
4.05505760E-02 4.14322556E-02 4.59023081E-02 5.01421199E-02 5.11495725E-02 3.21161771E-02 2.14538340E-02 1.45792461E-02
1.31057107E-02
CP(1) AT ZETA=0
4.81018466E-02 4.91311747E-02 5.40674504E-02 6.11705403E-02 6.13298977E-02 3.17268117E-02 2.16482668E-02 1.74766251E-02
1.71248333E-02
V
-9.63702054E-03 -9.45577817E-03 -7.54535302E-03 -4.74592613E-03 7.63098167E-04 -1.10366227E-02 -1.22528208E-02 -1.42992494E-02
-1.55544168E-02
KCOUNT= 13 VMAX= 1.55544168E-02 EPSIG= 1.0000000E-03 SPACER= 1.0000000E-03 VMXTEST= 1.13673517E-01
DETERM= 9.12166681E-02
DETA
1.75709050E-03 1.71351465E-03 1.28641629E-03 9.17074509E-04 3.55273348E-04 1.08400409E-03 1.55115695E-03 2.12212091E-03
2.23271172E-03
NCYCLE= 2 AT 11/23/71 10.55.17.
ETAS
6.26909720E-02 5.97942222E-02 5.35480783E-02 4.28268096E-02 4.14274750E-02 5.16245035E-02 6.95835030E-02 8.06259522E-02
8.56009436E-02
ETASP
-7.73023930E-16 -8.41263462E-02 -1.71435501E-01 -1.32975789E-01 8.13865466E-02 2.80716053E-01 2.81299202E-01 1.48465087E-01
-1.83634631E-14
CP(1) AT SPOCK
4.17028240E-02 4.25910411E-02 4.68394346E-02 5.08683302E-02 5.14401036E-02 3.30088874E-02 2.24425036E-02 1.57254850E-02
1.42407628E-02
CP(1) AT ZETA=0
4.94614482E-02 5.05247370E-02 5.52865504E-02 6.20756138E-02 6.15937145E-02 3.35939129E-02 2.32453729E-02 1.91000738E-02
1.86581896E-02
V
1.49714339E-04 6.59535718E-05 -4.17424518E-05 -8.97677752E-05 -4.43872632E-05 -3.95666605E-04 -3.15906295E-04 -3.96441855E-05
5.56961220E-04

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APPENDIX B

N= 9 M=2 NREAD=1 NSPACE=1 NP= 5 NCAVRG=2
NA= 1 ANA= 0. AB= 1 BNB= 0.
STMACH= 8.0000000E+00 GAMMA= 1.4000000E+00 T= 6.C000000E-01 THETA= 1.0000000E+01 ALPHAD= 2.0000000E+00
RANGL= 3.3116914E-01
EPSIG= 1.0000000E-03 EPSIGPX= 1.0000000E-03 SPACER= 1.0000000E-03 EPSIVAR= 1.0000000E-08 EPSINT= 2.5000000E-02
NCVCL= 2 VTEST= 1.0000000E-03 VPAX= 5.56501220E-04 AAST= 4.23895624E-01 PTINF= 1.08560426E+02
VTEST= 1.0000000E-03 VTEST1= 3.0000000E-02
M2E= 0
SLOPE= 1.0000000E+00 MTRANSF= 1
KCOUNT= 23 VMAX= 5.56501220E-04 EPSIG= 1.0000000E-03 SPACER= 1.0000000E-03 VMATEST= 1.13619136E-01

SUMMARY PRINT BLOCK

Table with 10 columns (I=1 to I=10) and rows for parameters like PSID, PSISO, X0, XDBAR, YDBAR, XS, YS, XSBAR, YSBAR, ETAS, BETAD, XI, CPSHOCK, CPBODY.

Table with 7 columns (I, TAU, XI, XC, VD, ETAS, ETASP) and rows for parameters 1 through 9.

ZETA= 0.

Large table with 10 columns (I=1 to I=10) and rows for parameters P, P/PTINF, P/PINF, RHO, U, V, W, UC, VC, WCC, VCC, MCC, VX, VY, VZ, PSINDR, THEINCR, XBAR, XBMLD, YBAR, YRHLD, ETA, DEQNS, AM, CROSSM, SBAR, PDRGAP, PT/PTINF, BERNQUL, DDDZ, PP, UP, WP.

WINDWARD LINE ZETA LIMIT

Table with 10 columns (U, RHO, S, PORCAM, UC, VC, WC, VX, VY, VZ, PT/PTINF) and one row of data.

LEEWARD LINE ZETA LIMIT

Table with 10 columns (U, RHO, S, PORCAM, UC, VC, WC, VX, VY, VZ, PT/PTINF) and one row of data.

FORCE COEFFICIENTS

CZ= 4.33630484E-02 CY= 9.22434684E-02 CX= 4.65587041E-02 CL= 5.07547583E-02
YBAR= -1.58871219E-02 ZBAR= 6.66666667E-01 CM= -6.22284796E-02

APPENDIX B

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STMACH= 6.00000000E+00 GAMMA= 1.40000000E+00 T= 6.00000000E-01 THETA0= 1.00000000E+01 ALPHAD= 4.00000000E+00
EPSIG0= 1.00000000E-03
AAS1= 4.23895624E-01
VTEST= 1.00000000E-03 VTEST1= 3.00000000E-02
RZE= 0
SLOPE= 1.00000000E+00 KTRANSF= 1
RANGLE= 6.62338287E-01
EPSIG= 1.00000000E-03 EPSIGPX= 1.00000000E-03 SPACER= 1.00000000E-03 EPSIVAR= 1.00000000E-08 EPSINT= 2.50000000E-02
MCYCLE= 1 AT 11/23/71 10.56.03.
EYAS
5.71037891E-02 5.50043294E-02 4.96974454E-02 4.12550504E-02 4.26159149E-02 5.93018690E-02 8.23256429E-02 9.75278923E-02
1.03927039E-01
EYASP
1.02566007E-16 -6.83148663E-02 -1.41825391E-01 -9.12759147E-02 1.66148739E-01 3.91619215E-01 3.66148845E-01 2.01549240E-01
-2.75899443E-14
CP(1) AT SPOCK
6.23081671E-02 6.29350687E-02 6.50848005E-02 6.50554219E-02 5.51913507E-02 2.92340819E-02 1.55382225E-02 8.04002435E-03
6.19048647E-03
CP(1) AT ZETA=0
7.18671981E-02 7.29640045E-02 7.61385638E-02 7.81817104E-02 5.89847833E-02 1.98189549E-02 9.52996627E-03 8.22316664E-03
8.50866161E-03
V
3.13590376E-03 4.26116068E-03 3.13709417E-03 2.00123827E-03 4.51393242E-04 -1.07370231E-02 -1.14404335E-02 -8.64716521E-03
-3.33121244E-03
RCOUNT= 24 VMAX= 1.14404335E-02 EPSIG= 1.00000000E-03 SPACER= 1.00000000E-03 VMAXTEST= 1.11451068E-01
DETERM= 4.96810152E-02
DETA
-6.65642026E-04 -7.54603087E-04 -5.65569366E-04 -3.63084535E-04 -2.02071743E-04 3.47875098E-04 6.70528349E-04 1.09556953E-03
8.38465080E-04
MCYCLE= 2 AT 11/23/71 11.01.00.
EYAS
5.64401471E-02 5.42497263E-02 4.91318761E-02 4.09919658E-02 4.24138432E-02 5.96497441E-02 8.25561713E-02 9.86234618E-02
1.04765505E-01
EYASP
4.19457901E-16 -6.77022706E-02 -1.37829037E-01 -8.85720672E-02 1.72815243E-01 3.95888557E-01 3.73548308E-01 2.02441533E-01
-2.14165116E-14
CP(1) AT SPOCK
6.18116966E-02 6.23652044E-02 6.46460458E-02 6.47838567E-02 5.51927197E-02 2.96374577E-02 1.55580359E-02 8.55583128E-03
6.57651052E-03
CP(1) AT ZETA=0
7.13349532E-02 7.23141941E-02 7.56217879E-02 7.79172893E-02 5.93372194E-02 2.11254900E-02 1.05087409E-02 8.80368423E-03
8.99560551E-03
V
2.00708611E-05 1.03949796E-05 1.64161191E-07 7.28417927E-07 -4.44601693E-05 -5.55113121E-04 -2.81041930E-04 -1.03900309E-05
3.22546646E-04

```


APPENDIX B

Table with 11 columns (I=1 to I=10) and rows for ZETA = 9.C0C0C0C0E-01. Rows include parameters like P, P/ROASTSC, P/P/INF, RHO, U, V, W, UC, VC, WC, WCC, VX, VY, VZ, PSINOR, THETNCR, XBARD, XBHL, YBAR, YBHL, ETA, DEQNS, AM, CROSSM, SBAR, PDRGAM, PT/P/INF, BERNOLU, DPOZ, DDUZ, DVOZ, DWDZ, DSBDZ, UP, US, VP, WP, SBAPP.

Table with 11 columns (I=1 to I=10) and rows for ZETA = 8.C0C0C0C0E-01. Rows include parameters like P, P/ROASTSC, P/P/INF, RHO, U, V, W, UC, VC, WC, WCC, VX, VY, VZ, PSINOR, THETNCR, XBARD, XBHL, YBAR, YBHL, ETA, DEQNS, AM, CROSSM, SBAR, PDRGAM, PT/P/INF, BERNOLU, DPOZ, DDUZ, DVOZ, DWDZ, DSBDZ, UP, US, VP, WP, SBAPP.

APPENDIX B

Table with columns labeled I=1 to I=10 and rows containing alphanumeric codes and numerical values. Header: ZETA= 7.CCCCCCCC-01

Table with columns labeled I=1 to I=10 and rows containing alphanumeric codes and numerical values. Header: ZETA= 6.0000000E-01

APPENDIX B

Table with columns labeled I=1 to I=10 and rows labeled with parameters like P, P/ROASTSQ, P/P/PTINF, RHO, U, V, W, etc. The header indicates ZETA = 5.0000000E-01.

Table with columns labeled I=1 to I=10 and rows labeled with parameters like P, P/ROASTSQ, P/P/PTINF, RHO, U, V, W, etc. The header indicates ZETA = 4.0000000E-01.

APPENDIX B

ZETA= C.

	I=1	I=2	I=3	I=4	I=5	I=6	I=7	I=8	I=9	I=10
P	4.6829E-02	4.7318E-02	4.8971E-02	5.0119E-02	4.0759E-02	2.1583E-02	1.6348E-02	1.5521E-02	1.5659E-02	
P/ROASTSC	2.6061E-01	2.6333E-01	2.7254E-01	2.7852E-01	2.2683E-01	1.2012E-01	9.0982E-02	8.6546E-02	8.7144E-02	
P/PTINF	4.2578E-04	4.3427E-04	4.4944E-04	4.5957E-04	3.7407E-04	1.9808E-04	1.5004E-04	1.4272E-04	1.4371E-04	
P/PINF	4.1959E+00	4.2357E+00	4.3878E+00	4.4907E+00	3.6520E+00	1.9339E+00	1.4648E+00	1.3934E+00	1.4030E+00	
RHD	2.5918E+00	2.6109E+00	2.6757E+00	2.7244E+00	2.3469E+00	1.4903E+00	1.2221E+00	1.1792E+00	1.1851E+00	
U	2.3013E+00	2.3008E+00	2.2992E+00	2.2933E+00	2.3017E+00	2.3155E+00	2.3256E+00	2.3395E+00	2.3421E+00	
V	2.0078E-05	1.0095E-05	1.6232E-07	1.2888E-07	-4.4440E-05	-5.5511E-04	-2.8104E-04	-1.0390E-05	-3.2255E-04	
W	-1.3081E-13	-2.2237E-02	-2.9910E-02	8.2664E-03	1.6024E-01	2.7266E-01	2.2767E-01	1.1326E-01	-3.7501E-13	
UC	2.2885E+00	2.2865E+00	2.2757E+00	2.2679E+00	2.2667E+00	2.3032E+00	2.3222E+00	2.3282E+00	2.3290E+00	
VC	2.4214E-01	2.5001E-01	2.7745E-01	3.3680E-01	3.5964E-01	3.4149E-01	2.8233E-01	2.5455E-01	2.4673E-01	
WC	-1.3040E-13	5.7591E-02	1.1380E-01	1.9595E-01	1.6024E-01	1.1961E-01	8.1666E-02	3.2035E-02	1.7972E-11	
VCC	2.4214E-01	2.5568E-01	2.9870E-01	3.7242E-01	3.9964E-01	2.6249E-01	2.1310E-01	2.3273E-01	2.4673E-01	
WCC	-1.3081E-13	-2.1199E-02	-2.6609E-02	7.5566E-03	1.6024E-01	2.4903E-01	2.0241E-01	1.0766E-01	-3.9889E-13	
VX	-1.3081E-13	1.0539E-01	2.2125E-01	3.5438E-01	3.9946E-01	1.9770E-01	4.6529E-02	1.8385E-02	-2.8304E-11	
VY	-2.4214E-01	-2.3391E-01	-2.0242E-01	-1.0907E-01	1.6024E-01	3.1849E-01	2.9200E-01	2.5885E-01	2.4673E-01	
VZ	2.2885E+00	2.2865E+00	2.2757E+00	2.2679E+00	2.2667E+00	2.3032E+00	2.3222E+00	2.3282E+00	2.3290E+00	
PSINOR	-3.2751E-12	2.6391E+00	5.5433E+00	8.9355E+00	5.9899E+00	4.2634E+00	1.1479E+00	4.5245E-01	-6.9629E-10	
THETNCP	8.3960E+01	8.4165E+01	8.4949E+01	8.7280E+01	8.6018E+01	8.2149E+01	8.2878E+01	8.3728E+01	8.3953E+01	
XBAR	0.	2.1552E-01	6.1784E-01	8.7723E-01	1.0000E+00	8.7723E-01	6.1784E-01	2.1552E-01	-6.9800E-11	
XBHLD	0.	-6.9800E-11	-6.9800E-11	-6.9800E-11	-6.9800E-11	-6.9800E-11	-6.9800E-11	-6.9800E-11	-6.9800E-11	
YBAR	-6.0000E-01	-5.6935E-01	-4.7118E-01	-2.8855E-01	-1.8308E-01	-2.8805E-01	-4.7118E-01	-5.6935E-01	-6.0000E-01	
YBHL	-6.0000E-01	6.0000E-01	6.0000E-01	6.0000E-01	6.0000E-01	6.0000E-01	6.0000E-01	6.0000E-01	6.0000E-01	
ETA	0.	0.	0.	0.	0.	0.	0.	0.	0.	
G	-2.8906E-03	-2.8588E-03	-3.1299E-03	-3.1642E-03	-3.7544E-03	-4.4949E-03	-6.4499E-03	-2.2810E-03	-3.3450E-03	
DEQNS	5.5016E+00	5.5933E+00	5.6005E+00	5.6190E+00	5.6580E+00	5.6433E+00	5.6248E+00	5.6164E+00	5.6143E+00	
AM	6.1333E+00	6.1230E+00	6.0851E+00	6.0662E+00	6.2723E+00	6.9408E+00	7.2503E+00	7.3072E+00	7.2993E+00	
CROSSM	3.4964E-13	5.5176E-02	7.9208E-02	2.1818E-02	4.3561E-01	8.1170E-01	7.6520E-01	3.5935E-01	1.1688E-12	
SBAR	1.0093E-01	1.0093E-01	1.0093E-01	1.0093E-01	1.0093E-01	1.0093E-01	1.0093E-01	1.0093E-01	1.0093E-01	
PODOGAM	1.2346E-02	1.2346E-02	1.2346E-02	1.2346E-02	1.2346E-02	1.2346E-02	1.2346E-02	1.2346E-02	1.2346E-02	
PT/PTINF	7.7700E-01	7.7700E-01	7.7700E-01	7.7700E-01	7.7700E-01	7.7700E-01	7.7700E-01	7.7700E-01	7.7700E-01	
PT	8.4662E+01	8.4662E+01	8.4662E+01	8.4662E+01	8.4662E+01	8.4662E+01	8.4662E+01	8.4662E+01	8.4662E+01	
BERNOUL	-6.7175E-11	7.8354E-09	1.2754E-08	1.9943E-09	-1.5192E-08	-8.0709E-08	3.2243E-08	2.3383E-08	-1.7339E-08	
DVDZ	-2.3760E-01	-2.2756E-01	-2.4628E-01	-2.5687E-01	-2.6212E-01	-2.0704E-01	-1.6697E-01	-2.3043E-01	-2.9962E-01	
DPDZ	1.5304E-27	4.7353E-05	1.1011E-04	1.2971E-05	7.2349E-03	1.1250E-02	4.9221E-03	1.0007E-03	1.0676E-26	
PP	-2.1038E-15	2.1476E-02	4.2647E-02	-5.5851E-02	-2.9299E-01	-2.4071E-01	-3.4697E-02	6.0466E-04	-2.5336E-15	
UP	-1.3081E-13	-2.2237E-02	-2.9910E-02	8.2664E-03	1.6024E-01	2.7266E-01	2.2767E-01	1.1326E-01	-3.7501E-13	
WP	-4.8145E-01	-4.0016E-01	4.3141E-01	1.6717E+00	2.4849E+00	1.0715E+00	-1.7635E+00	-2.3430E+00	-1.8242E+00	

WINDARC LINE ZETA LIMIT

U	RHD	S	PORCGAM	UC	VC	WC	VX	VY	VZ	PT/PTINF
2.3024E+00	2.6097E+00	9.1142E-02	1.2226E-02	2.2896E+00	2.4223E-01	4.1546E-16	0.	-2.4223E-01	2.2896E+00	7.9624E-01

LEONARD LINE ZETA LIMIT

U	RHD	S	PORCGAM	UC	VC	WC	VX	VY	VZ	PT/PTINF
2.3496E+00	1.2730E+00	7.0168E-04	1.1169E-02	2.3366E+00	2.4720E-01	1.8407E-11	-2.8758E-11	2.4720E-01	2.3366E+00	9.9825E-01

FORCE COEFFICIENTS

CZ= 4.62736810E-02 CV= 1.86505024E-01 CD= 5.51708934E-02 CL= 1.82822818E-01
 YBAR= -3.00745746E-02 ZBAR= 6.66666667E-01 CM= -1.25728326E-01

APPENDIX B

Explanatory Notes

- ① Some input and auxiliary parameters. Only one line is used in this preliminary calculation for the zero-incidence circular cone.
- ② Computed values for first pivotal integration.
- ③ Change in shock shape.
- ④ New shock shape and computed values for second pivotal integration.
- ⑤ Input quantities, auxiliary quantities, and secondary quantities, beginning on a new page, for converged solution of circular cone at zero incidence.
- ⑥ Zeta print block at cone surface for circular cone at zero incidence.
- ⑦ Windward-line and leeward-line zeta limits or circular cone at zero incidence.
- ⑧ Repetition of input quantities, auxiliary quantities, and secondary quantities for circular cone at zero incidence. At this stage, the program takes the η_s -value just obtained from the $N = 1$ calculation and assigns it at all the lines. The problem is now reintegrated, using the full program logic, cross derivatives, and so on; of course, the shock shape satisfies the convergence criterion on the first integration.
- ⑨ Summary print block for circular cone at zero incidence.
- ⑩ Arc length and body coordinates at each of the lines.
- ⑪ Repetition of zeta print block at cone surface for circular cone at zero incidence
- ⑫ Repetition of windward-line and leeward-line zeta limits for circular cone at zero incidence.
- ⑬ Force and moment coefficients together with center-of-pressure location.
- ⑭ Input quantities, auxiliary quantities, and secondary quantities for $T = 0.95$ (PARAM + DPRAM1). The η_s -values from the zero-incidence circular cone are used to start the iteration for the zero-incidence elliptic cone with $T = 0.95$.
- ⑮ Input values of η_s from converged circular cone at zero incidence and computed values from first pivotal integration.
- ⑯ Change in shock shape.

APPENDIX B

- ①7 New shock shape and computed values for second pivotal integration.
- ①8 Input quantities, auxiliary quantities, and secondary quantities, beginning on a new page, for converged solution of elliptic cone with $T = 0.95$.
- ①9 Summary print block for elliptic cone with $T = 0.95$.
- ②0 Arc length and body coordinates at each line for elliptic cone with $T = 0.95$.
- ②1 Zeta print block at cone surface for elliptic cone with $T = 0.95$.
- ②2 Windward-line and leeward-line zeta limits on elliptic cone with $T = 0.95$.
- ②3 Force and moment coefficients together with center-of-pressure location for elliptic cone with $T = 0.95$.

REFERENCES

1. Klunker, E. B.; South, Jerry C., Jr.; and Davis, Ruby M.: Calculation of Nonlinear Conical Flows by the Method of Lines. NASA TR R-374, 1971.
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