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Intelligence/Electronic Warfare (IEW) Direction-Finding and Fix Estimation Analysis Report Volume 2 TRAILBLAZER

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| This report contains an analysis of the direction finding (DF) and fix estimation algorithms in TRAILBLAZER. The TRAILBLAZER software analyzed is old and not currently used in the field. However, the algorithms here analyzed are used in other current IEW systems. The report examines the underlying algorithm assumptions (including unmodeled errors) and their appropriateness for TRAILBLAZER. Coding and documentation problems are then discussed. A detailed error budget is presented, in Appendix B. An extensive bibliography on fix estimation procuedres is contained in Appendix A. |  |

# U.S. ARMY INTELLIGENCE CENTER AND SCHOOL Software Analysis and Management System <br> INTELLIGENCE/ELECTRONIC WARFARE (JEW) DIRECTION-FINDING AND FIX ESTIMATION ANALYSIS REPORT VOLUME 2 TRAILBLAZER 

December 20, 1985



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## ABBREVIATIONS AND ACRONYMS

| ACM | Association for Computing Machinery |
| :--- | :--- |
| AGTELIS | Automated Ground Transportable Emitter Location and <br> Identification System |
| BETA | Battlefield Exploitation and Target Acquisition |
| DF | Direction Finding |
| DOD | Department of Defense |
| EEP | Elliptical Error Probability |
| ELINT | Electronic Intelligence |
| EOB | Enemy Order of Battle |
| GR | GUARDRAIL |
| IPF | Information Processing Facility |
| ITEP | Interim Tactical ELINT Processor |
| JPL | Jet Propulsion Laboratory |
| LOB | Line-of-Bearing |
| LOP | Line-of-Position |
| MCS | Master Control Station |
| MGRS | Military Grid Reference System |
| QUICKLOOR | An Airborne Non-Communication Emitter Location and |
|  | Identification System |
| RMS | Root-Mean-Square |
| RSS | Remote Slave Station |
| SNR | Signal-to-Noise-Ratio |
| TCATA | TRADOC Combined Arms Training Activity |
| TR | TRAILBLAZER |
| USAICS | U. S. Army Intelligence Center and School |
| USAMS | USAICS Software Analysis and Management System |
| UTM | Universal Transverse Mercator |

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## CONTENTS

1. INTRODUCTION ..... 1-1
1.1 PURPOSE ..... 1-1
1.2 BACKGROUND ..... 1-1
2. ASSUMPTIONS, RESTRICTIONS, SCOPE ..... 2-1
2.1 BRIEF DESCRIPTION OF RADIO DIRECTION-FINDING AND POSITION FIXING ..... 2-1
2.2 ASSUMPTIONS ..... 2-4
2.3 RESTRICTIONS ..... 2-5
2.4 SCOPE ..... 2-6
3. TRAILBLAZER DF FIX ESTIMATION ..... 3-1
3.1 A GENERAL DESCRIPTION OF TRAILBLAZER DF FIX ESTIMATION ..... 3-1
3.2 SIMPLIFIED DESCRIPTION OF TRAILBLAZER DF FIXING PROCESS ..... 3-4
3.3 DETAILED DESCRIPTION OF TRAILBLAZER FIXING ..... 3-11
3.4 FIX ESTIMATION ..... 3-11
3.5 FIX OPTIMIZATION ..... 3-17
3.6 FIX ERROR ELLIPSE COMPUTATION (CONFIDENCE REGION) ..... 3-23
3.7 COMPUTATIONAL AND OPERATIONAL OBSERVATIONS ..... 3-25
4. OBSERVATIONS AND CONCLUSIONS ..... 4-1
APPENDIXES
A.
A. 1 ANNOTATED REFERENCE LIST ..... A-1
A. 2 SCHAUM'S OUTLINE SERIES - SELECTED UNDERGRADUATE LEVEL OUTLINES ..... A-1
A. 3 INTRODUCTORY UNDERGRADUATE TEXTS ..... A-2
A. 4 SPECIALIZED REFERENCES ..... A-3
A. 5 MILITARY SYSTEMS AVAILABLE DOCUMENTATION ..... A-8
B. FIX ESTIMATION ERROR MODEL ..... B-1
C. TRAILBLAZER ERROR BUDGET ..... C-1
D. ALGORITHMS IN STANDARD FORM ..... D-1
E. DATA BASE ENTRIES FOR TRAILBLAZER ..... E-1
F. USAMS ALGORITHM ANALYSIS SERIES ..... F-1

## CONTENTS (Continued)

Figures
1-1. Overview - From All Sources Through the Cross Correlation Process ..... 1-3
2-1. Relative Location of Two Direction-Finding Stations ..... 2-2
2-2. Relative Location of Several Direction-Finding Stations ..... 2-3
3-1. TRAILBLAZER Deployment ..... 3-2
3-2. Normal Radio Range vs Antenna Height ..... 3-3
3-3. Set of Five LOBs Showing Intersections ..... 3-5
3-4. Set of LOBs Showing Intersections After LOB5 has been Removed ..... 3-6
3-5. Set of Five LOBs Showing "Ghost" or "Phantom" Intersections ..... 3-7
3-6. Determination of Supporting LOBs (Wild Bearing has been edited out) For Intersection 1-2 ..... 3-8
3-7. Determination of Supporting LOBs (Wild Bearing has been edited out) For Intersection 3-4 ..... 3-9
3-8. Flow of the TRAILBLAZER DF Fixing Algorithm ..... 3-12
3-9. Intersection Geometry ..... 3-14
3-10. Supporting LOB Geometry ..... 3-16
3-11. Fix Estimate Optimization, Part I ..... 3-19
3-11. Fix Estimate Optimization, Part II ..... 3-20
3-11. Fix Estimate Optimization, Part III ..... 3-21
3-11. Fix Estimate Optimization, Part IV ..... 3-22

# SECTION 1 <br> INTRODUCTION 

### 1.1 PURPOSE

This analysis focuses on illuminating the logical and mathematical structure of the location estimating algorithms found in the TRAILBLAZER system, and identifying the assumptions that must hold for these algorithms to give valid results. TRAILBLAZER is one of several current U. S. Army directionfinding systems. These systems use several lines-of-bearing to estimate the location of an enemy emitter. Such a location estimate is often called a "fix." Several general methods for direction finding and fix estimations, some with more mathematically rigorous foundations, some frankly empirical, are discussed in Intelligence/Electronic Warfare (IEW) Direction Finding and Fix Estimation Analysis Report, Volume 1, Overview. The TRAILBLAZER algorithms analyzed belong to that most interesting hybrid class of empirical algorithms with a strong mathematical flavor. Although the designer of such an algorithm of ten has a specific mathematical structure in mind, the empirical nature of the algorithm of ten leaves the analyst several possible mathematical interpretations. This richness of interpretation increases the understanding of just how well the algorithms function in various environments and how compatible they are with algorithms found in other systems.

### 1.2 BACKGROUND

This algorithm analysis effort is being performed by the Jet Propulsion Laboratory for the U. S. Army Intelligence Center and School as a research-type effort to increase the understanding of the hybrid mathematical/ empirical algorithms found in intelligence processing systems. Algorithm results from one system are frequently used as input data for another system. Understanding both the assumptions under which the algorithms work, and the assumptions their results satisfy, is crucial to understanding the overall system. This view of a metasystem of intelligence processing systems (see Figure l-1) is central to this algorithm analysis effort.

For purposes of these studies, "algorithm" means a set of rules for carrying out a single conceptual operation on a set of data. There are many types of algorithms necessary to the operation of the metasystem shown in Figure 1-1. Analyses reported on so far, listed in Appendix $E$, have focused on four of these: geographical transformation algorithms, self and crosscorrelation algorithms, and aggregation algorithms. Geographical transformation algorithms translate locations from one grid reference system to another. These algorithms appear in almost all systems, often as incoming data or report preparation functions. Self-correlation algorithms test if the entity referred to in a new report has already been recorded in the database that reflects the estimated enemy situation. Cross-correlation algorithms test if a sighted piece of equipment belongs to an already identified unit, or a lower echelon unit to a higher echelon one. Aggregation algorithms try to identify an artillery battery in a cluster of equipment, a division in a group of regiments, or like groupings. Several statistical issues arising particularly in the correlation algorithms, are analyzed in a companion set of technical memoranda.

Looking once more at Figure 1-1, note that the same intelligence function, hence algorithms performing that function, is of ten embedded in several intelligence processing systems. Some generic algorithms, such as the geographical transformation algorithms mentioned above, appear in almost all systems. Comparing these algorithms that perform the same function in different systems increases the understanding not only of what these algorithms actually do and how well they perform, but also increases the understanding of how a "good" algorithm would work and what it would look like. Such comparisons should lead to developing criteria for selecting algorithms for embedding in new or upgraded systems, and finally in the creation of a library of "good" algorithms from which the choice can be made. The development of these criteria and building such a library are two major goals of this algorithm analysis effort to which each analysis of an algorithm in an existing system contributes.

ALL SOURCE PROCESSING OVERVIEW
FROM ALL SOURCES THRU THE
CROSS CORRELATION PROCESS


Figure 1-1. Overview - From All Sources Through the Cross-Correlation Process

## SECTION 2

ASSUMPTIONS, RESTRICTIONS, SCOPE

BRIEF DESCRIPTION OF RADIO DIRECTION-FINDING AND POSITION FIXING

The purpose of radio direction-finding is to estimate or fix the position of selected emitters. Usually, the position estimate is accompanied by a confidence region reflecting measurement errors, propagation errors, and modeling errors.

Radio direction-finding (DF) requires that an emitter be viewed from at least two DF stations spaced far enough apart that their look angles intersect as close to 90 degrees as possible. However, $90^{\circ}$ is usually impossible under battlefield conditions. Figure 2-1 illustrates a simple situation of two DF stations.

The fix estimate is at the point of intersection of the two lines-of-bearing (LOBs) (Figure 2-1). Since there is only one point of intersection, we have insufficient information to estimate the fix uncertainty due to measurement, propagation, and modeling errors.

In a multiple DF station configuration, there are many intersections (Figure 2-2). A more accurate fix estimate may be obtained by evaluating the clustering of these intersections. Since each intersection is a simple fix estimate, the uncertainty can then be expressed as a confidence region surrounding this fix estimate. This uncertainty reflects:
(1) Random measurement errors in measuring the lines-of-bearing.
(2) Errors because of different radio propagation effects along the lines-of-bearing.
(3) Errors because of spherical or flat-Earth assumptions.
(4) Phantom or ghost intersections because of the presence of multiple emitters or hidden emitter reflectors.


Figure 2-1. Relative Location of Two Direction-Finding Stations


Figure 2-2. Relative Location of Several Direction-Finding Stations

Some standard assumptions are made in the following analyses:
(1) The lines-of-bearing are straight.
(2) The errors in the separate lines-of-bearing are independent.
(3) The errors in the lines-of-bearing are Normally (Gaussian) distributed with zero mean and fixed estimable variance.
(4) The emitter location estimate error is distributed as a bivariate Normal distribution.
(5) The sensor positions are known exactly.
(6) The transmitter location is fixed during the period of DF fixing.
(7) The sensors are properly sited, calibrated, and operated.

Assumption \#1 is reasonable for the systems considered in this report when the sensors are properly sited. However, this assumption is weak at frequencies below approximately 30 MHz because of the effects of atmospheric tilt.

Assumption \#2 is reasonable based on the systematic errors being accounted for in calibrations. This assumption is weak at frequencies below approximately 30 MHz when some stations are close enough to each other to be subjected to the same propagation effects.

Assumption \#3 is usual when considering measurements which are subject to random measurement error. There are biases in the measurements from navigation errors, errors in the calibration tables, interference, depression angle effects, etc; these biases may be removed. In the absence of specific
knowledge about these errors the normal assumption is reasonable. Distorting effects such as plinthing to account for wild bearings, skewedness because of low receiver signal-to-noise ratios, and distortions resulting from the sensors not uniformly surrounding the emitter can weaken or invalidate this assumption.

Assumption \#4 is necessary to allow confidence levels about the estimated emitter position to be computed. The qualifications on assumption 非3 also apply to \#4.

Assumption \#5 is reasonable based on the fact that any such position errors can be added to the emitter estimate uncertainty, if they are significant.

Assumption \#6 is necessary to the analyses of the systems considered in this report, and it is reasonable over the period required to obtain a single fix.

Assumption \#7 is reasonable in the absence of contradictory information.

## 2.3 <br> RESTRICTIONS

In addition to the assumptions discussed in section 2.2, this report does not consider the following effects:
(1) Geographic transformation, map projection effects, and grid reference system conversions (see UAA002 Analysis of Geographic Transformation Algorithms July 9, 1982 of this series of algorithm analysis reports).
(2) Propagation effects.
(3) Centroid effects and susceptibility to deception (meaconing, gated signal parameter techniques, etc.).
(4) Special problems associated with low-probability-of-intercept emitters (low SNR, spread-spectrum, time-frequency diversity, frequency agility, etc).
(5) Numerical computation and normal truncation effects.
(6) Combination of lines-of-bearing, or emitter location estimates and their confidence ellipses from different systems (these problems will be the subject of a future report in this series of algorithm analysis reports).
(7) Elimination of wild bearings and ghost intersections using hardware/software processing of target message internals.
2.4 SCOPE

This report covers the TRAILBLAZER system as documented in ROLM 1602 Extended Assembly Language listings, marked DSO:TBSYS.SV, generated on 2/25/82.

SECTION 3
TRAILBLAZER DF FIX ESTIMATION

## 3.1 <br> A GENERAL DESCRIPTION OF TRAILBLAZER DF FIX ESTIMATION

This analysis of the TRAILBLAZER DF Fixing System (a communication intelligence collection system (COMINT)) is based on the TRAILBLAZER AN/TSQ114, Operator's Manual TM 32-5811-022-10-1, and assembly language listings dated $2 / 25 / 82$. There are some questions as to whether the manual and the listing correspond to the same version of TRAILBLAZER, of which there are several.

TRAILBLAZER is a ground-based, computer-assisted COMINT DF Fixing System consisting of five sensors: two master control stations (MCC) and three remote slave stations (RSS). TRAILBLAZER can obtain relatively accurate fixes in the "normal fix mode" with as few as three operational sensors. Less reliable fixes (cuts) can be obtained in the "degraded fix mode" using multiple lines-of-bearing from each of only two sensors.

Figure 3-1 depicts the most desirable siting of the five stations of a TRAILBLAZER system. This layout allows for a maximum DF base line consistent with maintaining the required data-links between the sensors. Over flat terrain the penetration of the system is about 15 to 20 km .

Figure 3-2 indicates extended penetration ranges possible when the system is operated from elevated vantage points.

TRAILBLAZER's five sensors can obtain up to five lines-of-bearing (LOBs) simultaneously on a desired emitter(s) and place this set of LOBs in one of up to five available bins (arrays). Each bin may contain up to five sets of LOBs on same or different emitters. Wild LOBs may be edited (rejected) by one of the system operators based on actual content.

The system operates in a multifix (automatic) mode and in a single fix (manual) mode. Since the single fix mode amounts to the first pass in the multifix mode it will not be discussed separately.


Figure 3-1. TRAILBLAZER Deployment
From: U.S. Army Field Manual (FM 30-476),
Radio Direction-Finding, 8 April 1977


Figure 3-2. Normal Radio Range vs Antenna Height
From: U.S. Army Field Manual (FM 30-476), Radio Direction-Finding, 8 April 1977

The following description is based on obtaining a DF fix using one set of five LOBs in one bin (array). Since there are five LOBs, there can be up to 10 possible intersections of two LOBs.

$$
C_{r}^{n}=\frac{n!}{r!(n-r)!}
$$

is the number of combinations of $n$ things taking $r$ at a time.

Each of these intersections represents an initial fix candidate. The "best" intersection must be selected, and any obviously "wild" (extraneous) LOBs must be discarded (edited). Figure 3-3 represents a set of five LOBs with the intersections numbered for reference.

The first step is to edit any wild bearings. Since LOB from station five does not form any intersections near the cluster of the other intersections (see Figure 3-3), it will be edited from the set of LOBs as a wild bearing (Figure 3-4). "Ghost" or "phantom" intersections from the geometry of the LOBs should also be edited (Figure 3-5). These are inadvertent crossings of LOBs and not relevent to the fix estimation process.

Next, each of the remaining intersections is evaluated to choose the "best" one. The "best" intersection is determined by considering which intersection is best supported by the other LOBs. For a LOB to support a fix estimate the "exactness of the LOB" from the station to the estimated fix is determined. If the angular difference between the two LOBs is excessive (greater than 3 standard deviation (sigma) units in statistical terms*) the station's LOB is considered to be a wild bearing and is discarded. Otherwise, it is considered a supporting LOB. The number of supporting LOBs is noted for each intersection. The intersection with the greatest number of supporting LOBs is selected as the initial fix estimate. Figures 3-6 and 3-7 show how the supporting LOBs are determined.

[^0]

Five LOBs Showing Intersections


Set of LOBs Showing Intersections After LOBS has been Removed
3-4. Set of LOBs Showing Intersections After $L O B 5$ has been



Figure 3-6. Determination of Supp
For Intersection 1-2


Figure 3-7. Determination of Supp
For Intersection 3-4

The initial fix estimate is then optimized to obtain the "best" fix estimate. This optimization process uses a potential function (detailed below) as the objective function and is based on displacing the initial fix estimate systematically in four directions (north, west, south, east), and calculating the support for each displaced (trial) estimate and keeping the "best" one. This process is continued with steps decreasing in size until a "best" fix estimate is located.

The support of the trial "best" fix is calculated as the sum of the potential function weighted (which is a semi-normalized Gaussian-weighted) miss-angles between the actual LOBs and the computed LOBs to the trial location. The effect of the Gaussian weighting is to give more consideration to the LOBs associated with the smaller miss-angles.

Having found an optimized or "best" fix estimate, a "confidence" region is calculated. A "confidence" region is a region that is likely to contain the true emitter location for some percentage of all fixes on a given emitter ( $50 \%$ in the case of TRAILBLAZER).

The following description of TRAILBLAZER DF Fixing has been freely-adapted from the software comments. Differences between the actual code and the description of the algorithm will follow, along with comments on the methods used.

The TRAILBLAZER DF Fixing Algorithms are based mainly on heuristic and empirical reasoning, rather than purely mathematical/statistical techniques. The four main steps in the DF Fixing process are quite intermingled and relate to the following discussion as follows:
(1) Obtain initial fix estimates.
(2) Reject wild lines-of-bearing by manual screen editing and automatic rejection.
(3) Refine (optimize) the initial fix estimate.
(4) Establish a confidence region (elliptical error probable (EEP)) around the fix estimate.

### 3.3 DETAILED DESCRIPTION OF TRAILBLAZER FIXING

The TRAILBLAZER fix algorithm has been tailored specifically for operation with the LOB data produced by a ground-based DF network, consisting of a predetermined number of DF stations, whose locations remain invariant during the data collection process. The goal of this algorithm is its attempt to resolve multiple targets reliably, while at the same time avoiding ghosts, i.e., false targets arising from coincidental intersections of unrelated LOBs.

The TRAILBLAZER fix algorithm execution consists of three distinct processes or phases:
(1) Fix estimation (ESTMP Procedure) and wild bearing rejection (ESTMP and FINAL Procedures).
(2) Fix optimization (FPEAK Procedure).
(3) Computation of an error ellipse surrounding the established fix point (FINAL Procedure).

Figure 3-8 outlines the flow of the TRAILBLAZER DF fixing algorithm.
3.4 FIX ESTIMATION

The estimation process is the key to the fix algorithm. For an understanding of this process, the TRAILBLAZER LOB database structure must be explained. The LOB data are stored in sets of up to five LOBs, i.e., one LOB from each of five possible DF stations. A set of five LOBs results from a system response to a DF command (or from a single manual LOB entry sequence via the "demo" command). The assumption is made that to the best of the operator's judgment, the LOBs within a set are associated with a single emitter. Given that the LOBs within a set are collected simultaneously, this is a fair assumption.


Figure 3-8. Flow of the TRAILBLAZER DF Fixing Algorithm

The objective of the estimation process is to examine all possible intersections of pairs of LOBs in the same set and all other sets, and to select that intersection which has the largest number of other LOBs in the database that miss this intersection by less than some specified miss angle. The estimation process selects that intersection which lies within the largest or strongest cluster of intersecting LOBs. It also makes a gross check to prevent duplication of previous fixes in multifix processing (as discussed in intersection criterion (2) discussed below). This process is computationally efficient because:
(1) The number of DF stations is small. Therefore, the number of intersections to be examined per set is reasonable.
(2) The locations of the DF stations are fixed. Consequently, for miss angle computations at each intersection, there are at most only three other exact LOBs that need to be computed, since two are already used for the intersection.

Each possible intersection of two LOBs is calculated directly from the geometry indicated in Figure 3-9.

The calculated intersection is validity-checked by:
(1) Verifying a true intersection, i.e., $D_{1}$ and $D_{2}$ both positive.
(2) Verifying that the angular difference between the LOBs is sufficient $\mathrm{LOB}_{2}-\mathrm{LOB}_{1} \geq 0.6$ degree.
(3) Verifying that the minimum and maximum range limitations are not exceeded for either station, $0.5 \leq \mathrm{D}_{\mathrm{i}} \leq 100 \mathrm{~km}$.
(4) Verifying that the intersection does not fall within the error ellipse of any previously computed fix (in the multifix mode only).


Figure 3-9. Intersection Geometry

Supporting LOBs are calculated from all the available (unused in any previous fix optimization) LOBs over all the bins. These supporting LOBs are calculated as indicated in Figure 3-10 and must fall within 3 sigma of the actual intersection to be considered as supporting it. The actual value of sigma is confused in the available source code listings. It is stated to be 2 degrees in the source code comments, but assigned a value of 8 degrees in parts of the source code.

In order for an intersection to be a candidate for valid fix estimate, an intersection must satisfy the following criteria:
(1) The intersection is real, i.e., the absolute value of the difference between the LOBs is at least 0.6 degree and the directed LOB vectors must intersect. The source code does not verify that only forward-looking LOBs are considered for intersections. It is possible, in running the program, to allow reciprocal bearings and create "phantom" intersections. This, however, is unlikely because of the normal deployment geometry. Also, the intersection must be in the range of 0.5 to 100 km of the reporting stations. The source code implementation of intersection out of range fails and would loop infinitely because of an initialization problem.
(2) If this is not the first pass for fix processing, i.e., a multifix (as opposed to single fix) situation looking for multiple emitters, the intersection must fall outside the error ellipse of the immediately previous successful fix estimate (this is because all previous fix error ellipses are checked in the optimization process). This provides the capacity to resolve multiple targets.
(3.a) In the normal fix mode (as opposed to degraded) the intersection must be supported by LOBs from at least three stations. The supporting LOBs must be within a $\pm 3$ sigma miss angle of the three exact LOBs from their


Figure 3-10. Supporting LOB Geometry
stations to the intersection. Also the supporting LOBs belong to a set of LOBs not used in any previous fix optimization computation, and in which the majority of LOBs conform to this miss angle requirement.
(3.b) In the degraded fix mode, the intersection must be supported by more than one set of intersecting LOBs from two stations whose LOBs were used in the computation of the intersection. The supporting LOBs must be within $\pm 3$ sigma of the exact LOBs from their stations to the intersection. Furthermore, these LOBs must belong to a set of LOBs not used in any previous fix computations in which the majority of LOBs conform to this miss angle requirement. The degraded mode is used only if the estimation process for the normal fix fails to yield a valid estimate which would satisfy the three station criteria.
(5) Of all the possible intersections, this intersection is supported by the largest number of LOBs that meet the miss angle and set requirements mentioned in the above criteria.

The estimation process yields a "non-ghost" intersection which is the best fix estimate (lies within the strongest clustering of LOBs). Also in the multiple fix case, the best fixed estimate lies outside the error ellipse of the previous fix. In addition, by discarding invalid intersections, the amount of computations in subsequent estimations (in the multitude fix case) is considerably reduced. Thus, for the multiple fix case, the number of computations is reasonably bounded.

In the case of multiple target examination, once the fix mode has been degraded, it remains degraded for all subsequent passes. Also, failure to obtain a fix estimate in the degraded mode precludes further passes.

### 3.5 FIX OPTIMIZATION

The fix optimization process seeks to improve the fix estimate by finding that location which locally maximizes a multipeaked objective function. By the nature of the estimation process, the initial estimate should be fairly close to the optimum fix location. This process also performs a final check to eliminate the duplication of previous fixes in the multifix situation.

At the outset of the optimization process, an estimate is available along with the exact LOBs associated with it from each system station. Also available are the LOBs supporting this estimate as a valid fix estimate. Before beginning optimization, that portion of the database which supports a particular fix estimate is modified to include complete sets when a majority of the LOBs supported the estimate. This increases the potential number of peaks and ridges in the objective function.

The optimization is then performed by systematically searching for a local peak in the total objective function which is a potential function of the form

$$
\sum \sum \exp \left[-K a_{i j}^{2}(x, y)\right]
$$

where the outer sum is over the stations, the inner sum over the LOBs from each station and $a_{i j}$ is the miss angle between the actual and computed LOB (see Figure 5-8). This objective function is applied locally in each case by: (1) using the selected portion of the database, (2) using the fix estimate as an initial reference location, (3) using its associated set of exact LOBs, and (4) using the computed potential function for the point.

The peak searching scheme is a fairly conventional pattern search optimization method (Jacoby, 1972; Gill, 1980) but without a pattern step directed along the steepest gradient. The reference location is displaced by some step size (initially 16 screen raster (resolution) points) along the axes in the following four directions: $+Y,+X,-Y,-X$. Only one direction is considered at a time, generating a trial location. If one of these trial locations yields a higher value of the potential function, the trial location becomes the reference, an associated set of exact LOBs is determined, and a new trial location in the same direction is attempted. This peak search scheme continues until no further improvement in the same direction can be made and the process has been repeated in all directions. Figure 3-11, Parts I through IV illustrate the fix estimate optimization process. At this point, the step size is halved and the four directions are tried again. The procedure stops either when the step size becomes too small (currently less than one raster point in screen geometry), or after a maximum number of successful improvements have been made (currently 16). Under these restrictions the process is nondivergent, that is, it stops.

Although this algorithm always stops, and gives a value, it may not converge in the sense that the final location estimate is substantially closer to the location of the nearest local peak than was the starting value. One major cause is that the objective function itself may not be sharply peaked, and may even have ridges. Thus, since the optimization algorithm does not have a pattern step, and it does not rotate axes to take advantage of the gradient, it may climb very slowly. Three other factors compound this behavior.
(1) Angles are rounded to quarter degrees.


Figure 3-11.


Figure 3-11. Fix Estimate Optimization, Part II


Figure 3-11. Fix Estimate Optimization, Part III


Figure 3-11. Fix Estimate Optimization, Part IV
(2) Only the first four terms of the Taylor expansion for the exponential function are used in calculating the objective function.
(3) The algorithm terminates after, at most, 16 steps.

Therefore, as of ten occurs in purely empirical methods, the location estimate may be fairly inaccurate and thus not well-defined.

In the multifix situation (multiple passes), the final location (a result of peak searching), is checked to determine whether the emitter lies outside the error ellipses of all previous fixes. If not, this optimized fix is unacceptable and a new fix estimate must be obtained. Note that if this occurs, the selected portion of the local database that gave rise to this unacceptable optimized estimate is removed from further consideration.

If the final location is acceptable, what remains is the computation of the parameters in an error ellipse surrounding the optimized fix estimate. The data available at this point is: (1) a selected subset of the LOB database, (2) a final optimized fix location, (3) a set of exact LOBs to that location from all system stations, and (4) and the value of the potential function for that location. This procedure is satisfactory for ellipses with small eccentricity. However, it degrades with the higher eccentricity ellipses arising from emitter ranges that are large with respect to the sensors' baseline. Also, just as it is unclear that the best fix estimate is a measure of central tendency for a known bivariate distribution, it is equally unclear that the calculated ellipse reflects a related measure of dispersion. The statistical properties of these estimates is important because intelligence processing systems to which these values are input data assume they are the estimated mean and elliptical error probable from a bivariate normal distribution.

### 3.6 FIX ERROR ELLIPSE COMPUTATION (CONFIDENCE REGION)

The error ellipse computation serves a dual purpose. First, its computed parameters are used in the checks to prevent duplications of previous fixes. Second, it is part of the information describing a fix.

The parameters computed are:
(1) The ellipse orientation angle of the semimajor axis in radians. This is with respect to true north, and is defined as the mean of all LOB angles used.
(2) The ellipse semi-major axis is denoted: $a=s /\left(\operatorname{tau}_{E}\right)^{1 / 2}$, and semi-minor axis is denoted: $b=s\left(\operatorname{tau}_{E}\right)^{1 / 2}$, where $s$ is the ellipse size, and tau the ellipse axis ratio (semi-minor/semi-major).

In more detail, the size $s$ is directly proportional to the root-mean squared miss angle of all LOBs used in fix computation. It is also directly proportional to the mean (potential weighted) station to the target distance. It is inversely proportional to a weak function of a number of LOBs used. This dependence is and should be weak because the LOB errors in a ground-based system are primarily due to propagation path perturbation by terrain. These errors are not zero-mean and not uniformly distributed.

It should be noted that:
(1) The RMS miss angle is forced to be no less than the system instrument accuracy of two degrees. The actual value of the rms value is confused in the available source code listings from 2 to 8 degrees.
(2) The step size itself is forced to be at least 0.5 km .
(3) The step size is tripled when the fix mode is degraded. This is based on the consideration that with only two stations providing LOBs, there is no indication of the propagation path perturbation effect; hence, a twostation fix location is of questionable value.

The ellipse axis ratio semiminor/semimajor is defined as the mean absolute deviation of all LOBs used from the mean LOB vector, i.e., the ellipse orientation angle divided by 45 degrees.

Note that when these error ellipse parameters are used, they are used to ensure that a fix estimate does not duplicate a previously determined fix. The criterion employed requires that the fix estimate be outside the previous fix error ellipse.

### 3.7 COMPUTATIONAL AND OPERATIONAL OBSERVATIONS

The TRAILBLAZER fix algorithm involves a considerable amount of computation, particularly in the estimation process. The first fix estimate requires examination of every possible intersection in every set of LOBs. If in the first estimation, all invalid intersections are removed from future consideration, the amount of computation in subsequent estimations (in a multiple fix case) is considerably reduced. In addition, once an estimate is optimized, the size of the LOB database is reduced since a set of LOBs is used only once in computing a final fix location. The fix estimate is then removed from further consideration. Consequently, the amount of computation in a multiple fix case is reasonable.

Since the entire fix calculation methodology is highly empirical, numerical parameters must be chosen with care. There are two key parameters: (1) the allowable miss angle used in the estimation process (currently 3 sigma), and (2) the width constant for the potential function (currently ( $1 / 3$ sigma) ${ }^{2} / 2$ ). These parameters control the sensitivity (resolution) of the fix algorithm, and indirectly affect the error ellipse size (both the RMS miss angle and mean range are potential-weighted). If a change to these parameters is contemplated, the comments in the code recommend that their interrelationship remain reasonably the same. For example, the parameters to be changed should be multipliers of 3 sigma. For TRAILBLAZER, the current parameters give reasonable results according to the field test data (after removing obviously bad data attributed to hardware malfunctions, interference, operator mistakes, etc.). These results indicate that the error ellipse computed is about a 50 percent confidence ellipse. A considerable amount of testing and
field experience would be required in order to optimize the parameters, given the indeterminate character of LOB error statistics for ground-based DF. It should be emphasized that this is a highly empirical process.

In view of the capabilities of the TRAILBLAZER system for LOB set separation at collection time using bin assignments and subsequent LOB editing, the fix algorithm should be used in the single-fix or manual mode for best results. However, when no such separation has been made or is possible, or when the operator does not have the time for post-collection LOB editing, the fix algorithm may be used in the multifix or automatic mode with a reasonable expectation of comparable results.

## SECTION 4 <br> OBSERVATIONS AND CONCLUSIONS

It appears that the assembly language source code that this analysis was based on might not be the latest version. Most of the problems indicated in Section 3 with bold-type underlining could all be due to an early version of the software in transition. The fact the system is deployed and operating tends to support the feeling that the analyzed software was not the current version.

## APPENDIX A

## A. 1 <br> ANNOTATED REFERENCE LIST

The references listed in this appendix fall into two categories: (1) books on general mathematics, (2) books and articles on direction finding techniques. The general mathematics books are included to better acquaint users with the necessary mathematical and technical background. They include Schaum's outline series which provides good examples, some introductory undergraduate level references, and more specialized and advanced text and references.
A. 2 SCHAUM'S OUTLINE SERIES - SELECTED UNDERGRADUATE LEVEL OUTLINES

These outlines are valuable for obtaining an overview of selected subjects quickly. Explanatory text is developed along with fully solved examples in stand-alone, easily referenced blocks. The most current edition is not always referenced. The publisher is McGrawHill, New York.

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## APPENDIX B

FIX ESTIMATION ERROR MODEL

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## APPENDIX B

## CONTENTS

1.0 PURPOSE ..... B-5
2.0 SCOPE ..... B-5
3.0 POSITIONAL ERRORS OF A PLATFORM ..... B-6
3.1 FRAME OF REFERENCE ERRORS ..... B-6
3.1.1 Geodetic Errors ..... B-7
3.1.2 Geomagnetic Errors ..... B-7
3.1.3 Cartographic Errors ..... B-9
3.2 POSITION MEASUREMENT ERRORS ..... B-10
3.2.1 Inertial Navigation ..... B-10
3.2.2 Referenced Navigation ..... B-10
3.2.3 Doppler Navigation ..... B-12
4.0 ATTITUDE ERRORS ..... B-13
4.1 ATTITUDE COORDINATES ..... B-13
4.2 CORRELATION BETWEEN ATTITUDE AND POSITIONAL COORDINATES ..... B-13
5.0 ANTENNA ERRORS ..... B-14
6.0 INSTRUMENTATION ERRORS ..... B-15
7.0 ERROR TABULATION ..... B-15
TABULATION OF ERROR BUDGET ..... B-17
Figure 1. Geocentric Positional Coordinates ..... B-18
Figure 2. Attitude of the Platform ..... B-19
Figure 3. The Geoid and Latitude ..... B-20
REFERENCES ..... B-21

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## APPENDIX B

ERROR BUDGET
1.0

PURPOSE

The purpose of this appendix is to identify all of the various error components, in the most general case, when determining lines of bearings. These lines of bearing are used in subsequent fix estimations for emitters.

### 2.0 SCOPE

The essential assumptions of this document are: the emitter is not moving at the time the line of bearing is measured; the sensor may be in any position, from earthbound to a moving satellite.

The type of errors considered may be classified into several categories:
(1) Sensor platform position and orientation errors.
(2) Sensor attitude.
(3) Antenna errors.
(4) Instrumentation errors.
(5) Time.

The sensor platform postion and orientation errors may be referred to as "positional errors."

Errors due to propagation effects, site selection, varying aperture versus aspect effects, and operator errors are not considered in this document. Also, errors due to the choice of algorithms or numerical computations are not considered.

These error sources may be broadly classified into errors in the frame of reference and errors in position measurement. The former include errors which will be present regardless of a sensor platform's actual location or measurement thereof. These are largely the result of error or uncertainty in establishing the frame of reference for exchange of position information. Position measurement errors are those due to error or uncertainty in the methods and equipment used to determine platform location within the selected frame of reference.

The geocentric coordinates and references are:

| Latitude | $\phi$ | Phi |
| :--- | :--- | :--- |
| Longitude | $\lambda$ | Lambda |
| Altitude | $h$ |  |
| Orientaton of meridian plane (Direction of North) |  |  |

These coordinates are best described by the diagram in Figure 1. The geographic latitude is measured positive from the equator toward the North Pole in degrees. The geographic longitude is measured positive from the prime meridian at Greenwich toward the East in degrees. The altitude is measured from the mean sea level (the geoid) in meters and is positive in a direction away from the center of the earth. The physical sources of errors in these parameters will depend largely on the source of the data used to determine them.

### 3.1 FRAME OF REFERENCE ERRORS

Establishment of a frame of reference for exchange of position information on the earth involves seven major processes, all of which may introduce some error of uncertainty into any position reference within the selected framework.

Two of the seven processes are the province of geodesy, and involve measuring and representing the shape of the earth.

One process involves measurement of the actual shape of the earth independent of local variations in topography. This is typically most closely represented by mean sea level, i.e., sea level independent of variations due to lunar tides, and local gravitational anomalies. The resulting geometric figure, termed a geoid, becomes the basis for subsequent representations of the earth's surface. This figure is subject to error and uncertainty due to the measurement process and to changes in the actual shape of the earth over time.

The second process is the selection of a geometrical figure close to the geoid in shape, but simpler from the standpoint of mathematical and geometric manipulation, to be used as the basis of the mapping process in a given part of the world. The figure is generally based on a very nearly spherical ellipsoid which, because of its nearness to spherical shape, is of ten called a spheroid. Different spheroids are in use for different parts of the world both for historical reasons and because slightly differing ellipsoids best approximate the geoid over different parts of the earth. Different spheroids are typically defined by giving the radius at the equator and the flattening. The latter is defined as the difference between the radius at the equator and that at the pole divided by the radius at the equator. Selection of a spheroid introduces error as the selected figure is only an approximation to the geoid, and may vary from the geoid irregularly over the portion of the earth being mapped.

### 3.1.2 Geomagnetic Errors

Airborne platforms depend on a magnetic flux goniometer during initialization of the inertial platform. Field soldiers and mobile units often have to depend on magnetic compasses for determining bearings. Although this is one of the oldest means of taking bearings, it can be very inaccurate. The earth's magnetic field tends to align with the nearest magnetic pole. However,
the magnetic poles are about three kilometers from the geographic poles. Furthermore, the two poles, North and South, are not even symmetrically placed. And to complicate this, there are local variations over all the earth's surface. This angle that the compass makes with the grid lines of a military map is called the "declination" of the compass. The magnetic lines of force are not parallel to the earth's surface, except along the indefinite circle called the magnetic equator. The angle the magnetic field makes with a horizontal plane is called the dip angle or the magnetic inclination.

The declination at any one location does not remain the same year after year and changes somewhat over long periods of time. Besides these so-called secular changes, there are variations within the year and also small changes of angle throughout the day. Large erratic variations occur during "magnetic storms." These storms are of ten concurrent with the appearance of sun-spots. Variations from storms are infrequent enough and the other variations are sufficiently slow that it is practical to publish maps of countries and other large areas showing the magnetic declination. On these maps, points of equal magnetic declination are connected by lines. Each wiggly line is labeled with the amount and direction of the magnetic declination. These lines are called isogonic lines. The isogonic line of zero magnetic declination is indicated by a heavy line, and is called the agonic line. Maps of smaller area indicate the magnetic declination in their legend by an arrow pointing to the magnetic north and labeled with the value of the magnetic declination in degrees.

The National Space Technology Laboratory at the Naval Office in Bay Saint Louis, Mississippi has a world mathematical model of the earth's magnetic field. The model consists of an order 12 spherical harmonic series with time varying coefficients to take care of secular changes. The model is considered good for $\pm 5$ years. However, the model is incapable of describing anomalies smaller than about $1,100 \mathrm{~km}$, and has an inaccuracy of about $3,500 \mathrm{~km}$. The model is updated every five years from new satellite and aircraft survey data. Local anomalies will normally deviate a few degrees of arc from the earth's main field direction, but can deviate by tens of degrees in areas where the mineral magnetite is abundant and in polar regions. For accurate orientation using the earth's magnetic field, there is no good substitute for a local survey.

The remaining four processes introducing frame of reference errors fall into the province of cartography, i.e., the recording, measurement, and representation of geographic, topographic, and cultural features on the surface of the earth.

The first of these processes involves selection of one or more coordinate systems to be used to specify locations on the selected representation of a portion of the earth. In virtually all world reference systems, at least one of the coordinate frames used will apply to the selected spheroid, and the reference system used is in fact almost always the familiar geographic (latitude-longitude) coordinate system. Errors arise in this process due to errors in the measurements associated with selection of reference or registration points as bases of the coordinate system as well as in the measurement and computation involved in extending the coordinate frame from the base points through the area to be mapped.

The second process involves, in those cases where the final representation will be planar, a projection of all or a portion of the selected spheroid onto a plane according to some well defined set of mathematical and geodetic conventions. This step will of ten be followed by another iteration of the first step to select a reference system suitable for measurement and computation in the Euclidean plane. Errors arise in this process due to the distortion involved in the projection from the spheroid to the plane as well as in any subsequent registration and extension of the associated planar coordinate system.

The third process consists of the recording and measurement of surface features within the selected coordinate system(s). The errors inherent to this process include those associated with measurement of the features themselves, their relative locations, and their locations with respect to the coordinate systems selected.

The fourth process consists of the rendering of recorded features and associated coordinate systems into one or more forms that can be interpreted by people with a modicum of training and experience. Errors arise in this process due to distortions and simplifications imposed by the scale and resolution available in the final product, which in turn are governed in part by the current technology and in part by the limitations of the human perceptual system. A highway 10 meters in width, for example, if represented to scale on a $1: 250,000$ map, would be 0.04 millimeters wide and all but invisible to the naked eye.
3.2 POSITION MEASUREMENT ERRORS

### 3.2.1 Inertial Navigation

The four coordinates of position can be maintained by a suitably designed inertial platform. There will be essentially four type of errors with such systems:
(1) Errors in measurement and setting of initial position.
(2) Errors in platform measurement of inertial change.
(3) Errors in precision of computation of position from inertial change
(4) Cumulative errors in position, i.e., drift.

The basic component of most modern inertial navigation systems is the gyroscope. In addition to the familiar function of referencing direction (gyro compass), gyroscopes may be designed to measure rotations, to seek the local vertical, and to act as accelerometers.

### 3.2.2 Referenced Navigation

Referenced navigation systems are those that depend on beacons, or repeaters of known position or velocity. These may be classified by the geometry of the data processing:
(1) Hyperbolic (Decca, Loran, Omega, Satellite Aided Navigation.
(2) Circular (Sextant, Satellite Aided Navigation.
(3) Polar (TACAN).

The hyperbolic and the circular navigation systems are methods of triangulation. However, the hyperbolic method deals exclusively with the sides of the triangle, while the circular method deals with two sides and an angle. The polar method gives both a range and azimuth from the reference station.

Decca is a low frequency ( $70-130 \mathrm{kHz}$ ) hyperbolic system that triangulates by measuring the phase difference between signals from a master/slave pair of reference stations. The master/slave separation is 60 to 120 n .m. The useful range is about $240 \mathrm{n} . \mathrm{m}$. over water. Loran $A$ is medium frequency ( 2 MHz ) hyperbolic system that triangulates by measuring the time difference between receipt of pulses from two stations. The range of Loran $A$ is several hundred miles over water, but much reduced over land. Loran $C$ is a low frequency ( $90-110 \mathrm{kHz}$ ) version of Loran $A$ with considerably more range. OMEGA is a very low frequency hyperbolic system that triangulates by comparing the phase of signals from two beacons separated by a baseline of 5,000 to 6,000 miles. The coverage is world wide and may be used by submersibles.

Satellite-aided navigation has the most diverse possibility for use as a referenced system of navigation. The orbital elements and thus both the position and velocity of the satellite are accurately known. By combining such measurables as elevation angle, azimuth angle, ranges, difference in range, range sum, or doppler shift, fixes may be obtained that fit any of the listed categories in the first paragraph of this section. Methods that depend on measurement of the elevation angle of one or more satellites determine small circles on the earth's surface for fixes. Methods that determine distances lead to hyperbolic conic lattices for fixing.

TACAN is a UHF radio navigation system which provides both distance and bearing information of the aircraft relative to the selected ground beacon. The antenna system is the key to measuring the aximuth. The antenna system has a single, central element for transmission and reception. The parasitic elements are mounted on two concentric cylinders which rotate at fifteen
revolutions per second. The inner cylinder consists of a single parasitic element which causes a single cardioid polar pattern rotating at 15 rps. The outer cylinder has nine parasitic elements that superimpose nine lobs on the cardioid pattern. This gives an amplitude modulated signal with two frequency modulations of 15 Hz and 135 Hz . The transponder further emits bearing reference pulses as the peak of each lobe points East. When the lobe which coincides with the peak of the cardioid points East, a special "North" reference pulse code is transmitted. The airborne equipment measures the phase relationship of the maximum signal amplitude relative to the North reference pulses in order to determine the bearing of the aircraft relative to the beacon. The accuracy of the azimuth is in the order of magnitude of two degrees. The distance measuring part of TACAN equipment is like radar except that the return signal comes from a beacon used to produce strong artificial echoes. The beacon will respond to numerous simultaneous interrogations. To make this possible, the pulse repetition rate of the airborne transmitter is cause to jitter in a random manner. The receiver is allowed to recognize only those pulses received that follow the same jitter pattern and ignore all other. The slant range is determined to roughly 0.25 nautical miles under most conditions.

### 3.2.3 Doppler Navigation

Airborne Doppler is a SHF (micro-wave) system of navigation using the terrain or water below as a reference. Depending on the particular doppler system used, some or all of the following data can be made available to the crew:
(1) Component velocities and distances run, along, across, and perpendicular to the aircraft axes.
(2) Ground speed.
(3) Drift angle.
(4) Angle of attack.
(5) Height above terrain.

If True Air Speed, Pitch, and Heading Angles are available from such sources as an inertial system, then the following secondary data may be obtained.
(1) Wind speed and direction.
(2) Climb angle.
(3) Track angle.

The Doppler systems may have various configurations of antenna beams directed at different angles toward the earth. A two beam system may be used to measure ground speed and drift. A three beam system is basically sufficient to extract all three velocity components, but a four beam symmetrical arrangement is of ten used.
4.0 ATTITUDE ERRORS
4.1 ATTITUDE COORDINATES

The three attitude coordinates are:

| Roll Angle | $\alpha$ | alpha |
| :--- | :--- | :--- |
| Pitch Angle | $B$ | beta |
| Yaw Angle | $\gamma$ | gamma |

Figure 2 serves to define each of these angles. These are the standard Euler angles as defined by a "right hand" rule. However, it should be noted that the sign of these angles vary considerably throughout published literature. See Korn and Korn, reference 2, section 14.10-6, for a discussion of this coordinate system and the diverse choice of signs. In some aireborne systems these positional coordinates are limited by preset stops which may introduce non-linear errors.

### 4.2 CORRELATION BETWEEN ATTITUDE AND POSITIONAL COORDINATES

With a cursory examination of these six coordinates, it is apparent that errors in three of them will produce the larger errors. An error in yaw
angle alone will produce a divergence of the azimuth angle of bearing. This azimuth error will always be quite close in magnitude, but opposite in sign, to the Yaw error. Errors in longitude and latitude will produce an error in the position of the line of bearing as a function of the azimuth angle, but this does not effect the azimuth angle. If the azimuth angle is in the vicinity of zero or 180 degrees, an error of longitude will be reflected directly, and of nearly the same value, in the longitude of the fix estimations. At azimuth angles of 90 and 270 degrees, the line of bearing and consequently the fixes are unaffected by errors in longitude. The effects of errors in latitude are analogous in their effect but displaced by 90 degrees.

It is not so obvious that an error in the three remaining coordinates (altitude, roll, and pitch) should have any effect on the line of bearing. Indeed an error in altitude alone should only change the slant range and have no effect on the line of bearing. However, when coupled wih errors in roll and pitch, there is a definite mathematical relation or coupling. The significance of an error in altitude remains to be evaluated. Errors in roll and pitch (which have less effect on the error of the fix estimate than yaw, longitude, and latitude) directly cause errors in azimuth angle on the line of bearing.
5.0 ANTENNA ERRORS

Orientation with respect to the platform.
Difference between the mechanical axis and RF axis.
Beam width.

These first two antenna errors are directly related to the platform attitude coordinate errors. In fact the orientation of the antenna with respect to the platform and the difference between the mechanical axis and the RF axis are best described by Euler angles. If the axis defining these coordinates are chosen originally in coincidence, first order approximations will serve to considerably simplify the maze of trigonometric functions relating these angles. These three Euler angles can be identified as pitch, roll, and yaw. For small errors in these angles, the errors may be simply added to the corresponding platform angles. It should be noted at this point that the RF boresight error is a function of the radio frequency.

Beam width is always a function of the antenna geometry and frequency. A phased antenna system's beam width will vary considerably with change in aspect angle.
6.0 INSTRUMENTATION ERRORS

Bias (Systematic errors).
Noise (Random errors).

Bias errors, for example, are systematic errors such as boresite errors, parallax errors in instrument readings, and bezel errors. Bias errors are usually minimized by calibration procedures.

Noise errors are due to random phenomenon such as receiver noise. This noise normally produces random errors in bearings by increasing the region of uncertainty when determining the minima of a signal or the change in sign from the phase of a signal. There are many techniques of minimizing the effects of noise, depending on the source and nature of the noise (see Reference 5). In high frequency receivers, the receiver's "front end" is a high source of thermal noise, so the high gain required is usually obtained after heterodyning to a lower frequency or after further detection at the "rear end." Commonly, the band pass of filtering is reduced to the minimum that will not deteriorate the information content. The effect of impulse noise, such as noise emanating from electrical ignitions, can be minimized by amplitude clipping just above the signal level.

### 7.0 ERROR TABULATION

The sensor positional error is equally important in fixing, mobile, or airborne sensors. The attitude errors are most important in airborne sensors. The sensor geometric error refers to such errors as the difference between the geometric and RF axis of a direction-finding antenna, or even an optical tracker. Range is included with the geometric sensor errors for convenience only.

The specifications and tolerances will always include the units. The exact meaning of the specification and tolerance columns will depend on the instrument involved.

## TABULATION OF ERROR BUDGET

```
SYSTEM
COMPONENT
A/N NUMBER
MODEL
\begin{tabular}{|c|c|c|c|}
\hline & CLASSIFICATION & SPECS & TOLER \\
\hline 1. & Sensor Positional Errors & & \\
\hline a. & Longitude & & \\
\hline b. & Latitude & & \\
\hline c. & Altitude & & \\
\hline d. & Position (linear distance) & & \\
\hline 2. & Sensor Attitude Errors & & \\
\hline a. & Reference meridian (North) & & \\
\hline b. & Roll & & \\
\hline c. & Pitch & & \\
\hline d. & Yaw & & \\
\hline e. & Rates (TBD) & & \\
\hline 3. & Sensor Geometric Errors & & \\
\hline a. & Azimuth & & \\
\hline b. & Elevation & & \\
\hline c. & Range & & \\
\hline 4. & Instrument errors & & \\
\hline a. & Bias (systematic or secular errors) & & \\
\hline b. & Noise random errors & & \\
\hline
\end{tabular}
```


## References:

## NOTES:



Figure 1. Geocentric Positional Coordinates


Figure 2. Attitude of the Platform


Figure 3. The Geoid and Latitude

## REFERENCES

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APPENDIX C
TRAILBLAZER ERROR BUDGET

## Page intentionally left blank

TABULATION OF ERROR BUDGET
SYSTEM
COMPONENT
A/N NUMBER
MODEL

## References:

## NOTES:

APPENDIX D
ALGORITHMS IN STANDARD FORM

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Figure D-1. Illustration for Test Case for TRAILBLAZER Algorithm in Pascal

PROGRAM TRAILBLAZER(INPUT, OUTPUT, TRAILIN, TRAILOUT);

(*
This program/algorithm has been tailored specifically for operation with the LOB data produced by a ground-based DF NET, consisting of a small fixed number of DF stations, whose locations remain invariant during the data collection process.. The distinctive feature of this algorithm is its capacity to resolve reliably, multiple targets while at the same time avoiding GHOSTS, i.e. false targets arising from coincidental intersections of unrelated LOBS.

Original program written in "RCRM ASSEMBLEY LANGUAGE". Translated into PASCAL by Nick Covella, JUNE 1984.
; ;

CONST

| Shapefactor | $=3 ;$ |
| :--- | :--- |
| Pie | $=3.14159 ;$ |
| Radian | $=180 ;$ |
| Max | $=101 ;$ |
| Min | $=0.6 ;$ |
| Sigma | $=8 ;$ |

TYPE

Stations = RECORD

| Xcoord | REAL; (* | X-Location of any station. *) |
| :---: | :---: | :---: |
| Ycoord | REAL; (* | Y-Location of any station. *) |
| Theta | REAL; (* | Angle inputted from the user. *) |
| Alpha | REAL; ${ }^{*}$ | Calculated angle from input to TRUE NORTH *) |
| MissAngle | REAL; (* | Difference between the Alpha angle and the recalculated angle after an intersection has been found. *; |
| Semimajor | REAL; $<*$ | in kilometers *) |
| Semiminor | REAL; (* | in kilometers *) |
| Distance | REAL; (* | approx. distance from the staions to the object being "fixed". *) |
| Reflob | BOCLEAN: | (* indicates that an LOB has been attempted by the station. |
| Flag | BCOLEAN: | (* indicates that an intersection for this station has been calculated. *) |
| Orgin | INTEGER; | (* indicator for station manipulation *) |

END:

Data $\quad=$ RECORD

Xintercept : REAL;
Yintercept : REAL;
Support D-4 REAL;
Supportflag : ARRAYE
SupCountFlaq: INTEGER

Flag
: BODLEAN;

END;


UAR

| MissedAngle | $:$ REAL; |
| :--- | :--- |
| AStation | $:$ INTEGER; |
| BinNumber | $:$ INTEGER; |
| Index | $:$ INTEGER; |
| Intlosubscript | $:$ INTEGER; |
| IntPass | $:$ INTEGER; |
| Nmax | $:$ INTEGER; |
| Nother | $:$ INTEGER; |
| Nsame | $:$ INTEGER; |
| Col | $:$ INTEGER; |
| Stanumb | $:$ INTEGER; |
| Row | $:$ INTEGER; |
| Trailout | $:$ TEXT; |
| TrailIn | $:$ TEXT; |
| Intlo | $:$ Intlotype; |
| Lob | $:$ Lobtupe; |
| ID | $:$ Stations; |
| Table | $:$ TUT; |



BEGIN
WRITELN:' Entering CLEAR');
$I:=0$;
FOR BinNumber : $=1$ TO 5 DO
(* initialize the variables of the bins of each station. *)

D-5

Lobrec[Bininumber]. x́coord $:=00.000$;
Lobrec[BinNumber]. Ycoord $:=00.000$;
Lobrec[BinNumber]. Theta $:=000000 ;$
Lobrec[BinNumber]. Alpha $:=00.000 ;$
Lobrec[BinNumber]. MissAngle $:=00.000 ;$
Lobrec[BinNumber]. Semimajor : $=00$. 000;
Lobrec[BinNumber]. Semiminor $:=00.000$;
Lobrec[BinNumber]. Distance $:=00.000$;
Lobrec[BinNumber]. Refiob : $=$ FALSE;
Lobrec[BinNumber]. Flag := FALSE;
Lobrec[BinNumber]. Orgin $:=0$;
END:

FOR BinNumber $:=1$ TD 5 DO
BEGIN
$I:=I+1 ;$
FOR AStation $:=1$ TO 5 DO (* initialize the truth-table of the bins *)
BEGIN

| Tabletype[BinNumber, AStation]. Xintercept | $:=00.000 ;$ |
| :--- | :--- |
| Tabletype[BinNumber, AStation]. Yintercept | $:=00.000 ;$ |
| Tabletype[BinNumber, AStation]. Support | $:=00.000 ;$ |
| Tabletype[BinNumber, AStation]. SupCountFlag | $:=0 ;$ |
| Tabletype[BinNumber, AStation]. SupportFlag[I] | $=$ FALSE; |
| Tabletype[BinNumber,AStation]. Flag | $:=$ FALSE; |

## END;

END;
FOR Intlosubscript $:=1$ TO 5 DO (* intersection LOB array. *) Intloarray[Intiosubscript] : $=0$ i $\quad(*$ initialized to -1 in actuai program $x$ WRITELN: Leaving CLEAR');

END; :* PROCEDURE "CLEAR" *)

##  <br> PROCEDURE INELLIPSE (VAR Xefix : REAL; <br> VAR Yefix : REAL; <br> VAR Answer: BOOLEAN; <br> Table : TVT);


(4)

This procedure will insure that a fix estimate doesn't duplictate the last or any previous fix. INELLIPSE returns true in the boolean variable Ansuer if the fix estimate is in the ellipse determined by theprevious fixes.
*)
$V A R$
Valuel, Valueisqr, Value2, Value2sqr $: ~ R E A L ;$
Tempadd, Tempcos, Tempsin
Sum
Xeoord, Yeoord

| Semiminoraxis | : REAL; |
| :--- | :--- |

BEGIN
WRITELN(' Entering INELIIPSE');
(* get $x$ and $y$ coordinates of the center of the ellipse*)
(* get the cosine of the ellipse *)
Tempeos : = CaS( (Yefix * Pie) / Radian);
Tempsin : $=\operatorname{SIN}((X e f i x * P i e) / R a d i a n) ;$
Tempadd $:=$ Tempcos + Tempsini
Semimajoraxis : = Tempcos + Tempsin; (* JUST FOR ARGUEMENT *)
Value! : = Tempadd / Semimajoraxis;
ValueiSqr : = Valuel * Valuei;
Tenpeds : = CaS( (Xefix * Pie) / Radian);
TEmpsin: $=$ SiN( (Yefix * Pie) / Radian);
Tempadd : $=$ Tempcos - Tempsini
Seniminoraxis : = Tempcas + Tempsin: (* JUST FOR ARGUEMENT *)
Value2 : $=$ Tempadd / Semiminoraxis;
value2Sqr : = Value2 * Value2;
Sum : = Valueisqr + Value2Sqri
IF Sum $>2$ THEN
Answer : = TRUE $(*$ indicating that the estimate was probably different fram any other estimate *)
ELSE
Ansuer : = FALSE; (* indicating that the estimate already exists. *:
WRITELN(, Leaving INELLIPSE');
-END; (* PROCEDURE "INELLIPSE" *)

PROCEDURE MSCAN(VAR Lobrec : Lobtype);
 ©

This procedure searches all LOBS LOBS have been marked indicating that they have been used for a particular fix then they will be unmarked by this procedure.
*)
$\because A R$
BinNumber : INTEGER;
EEGIN

WRITELN(' Entering MSCAN');
FOR BinNumber : = 1 TO 5 DO (* check each BINSET to see which have been marked. Unmark those that have been marked. *;

```
IF Lobrec[BinNumber]. Flag \(=\) TRUE THEN Lobrec[BinNumber].Flag := FALSE;
```

WRITESN: Leaving MSCAN');
_ END; (* PROCEDURE "MSCAN" *)

```
    Reflob : INTEGER;
VAR Lobrec : Labtype;;
```


(*
This procedure accumlates counts of marked LOBS for each station in the counter NOTHER and NSAME. "SCNDB" is called by "FPOT" to perform missangle variance on a station besis.
*)

VAR
Sumvariance : REAL;
Sumpotential : REAL;
Temp1. Temp2. Temp3: REAL;
Exp
Potential
BinNumber
REAL;
REAL;
Sigma, Shapefactor : INTEGER; (* constants given in the progeam *)
$X$. $Y$ : INTEGER; (* Substitute variables for the parameters passed to this subroutine. *)
Scancitr : INTEGER; (* counter of marked LOBS *)

BEGIN
WRITELN(' Entering SCNDB' ${ }^{\prime}$;
$X:=$ Compcnt;
$Y:=$ Reflob;
Sumvariance: $=0$;
Sumpotential: $=0$;
Nother : $=0$;
Nsame : $=0$;
IF $X=1$ THEN
Scancntr : = Nother;
For BinNumber : = 1 TO 5 DO
IF Lobrec[BinNumber]. Reflob = FALSE THEN
BEGIN
Lobrec[BinNumber]. Flag := FALSE;
Scancntr : = Nsame; Nother : = 1;

END;
Lobrec[BinNumber]. Reflob: = TRUE;
WHILE Lobrec[BinNumber].Flag © TRUE DO
BEGIN

```
IF }X=1\mathrm{ THEN
    Scancntr := Scancontr + 1;
IF ((Scancitr = O) DR (X = O)) THEN
            MissedAngle := Scancntr - X (* LOB - reflob *);
IF MissedAngle == 0 THEN
            MissedAngle := - (MissedAngle);
                IF MissedAngle > Pie THEN
                        D-8
```

```
MissedAngle := (2 * Pie) - MissedAngle;
Sigma := 日;
Shapefactor:= 3;
Temp1 := Sigma * Shapefactor;
Temp2 := MissedAngle/ Temp1;
Exp:= ((SQR(Temp2)) / 2);
Temp3 := (((Exp * Exp)/2) + ((Exp * Exp * Exp)/6) + Exp + 1);
Potential := 1/Temp3;
SumPotential : = Sumpotential + Potential;
SumVariance := SumVariance + ((SOR(MissedAngle) * Potential);;
```

END;

END;

IF Nother $=0$ THEN
Scancntr : = Nother
ELSE
Scancntr : = Nsame;
WRITELN(, Leaving SCANDB');
END; (* PROCEDURE "SCANDB" *)

PROCEDURE XPREP! StIdent : Lobtype;
I : INTEGER;
Intx : REAL;
Inty : REAL;
VAR Computed : BOQLEAN);

(*
This procedure computes the LDB angle of the Intersection and returns the coordinates of theproper location in the vミriables Intx and Inty.
*)

UAR
Distancex : REAL;
Distancey : REAL;
TotalDist: REAL;

BEGIN

WRITELN(' Entering XPREP');

Distancex : = StIdent[I].Xeaord - Intx;
Distancey : = StIdent[I]. Ycoord - Inty;
TotalDist $:=\operatorname{SQRT}((S Q R(D i s t a n c e X))+(S Q R(D i s t a n c e Y))) ;$
IF (TotalDist © Min) THEN

BEGIN
WRITE:N(Trailout);
D-9
WRITELN(TrailOut, 'The distance from Station \#', StIdent[I]. Orgin:i; is te

WRITELN(Trailout);
Intx: $=00.000$;
Inty: $=00.000$;
Computed : = FALSE;
END;
IF (TotalDist $>$ Max) THEN
BEGIN

```
WR ITELN(TrailDut);
WRITELN{TrailOut, 'The distance from Station #',StIdent[II. Orgin:i: is ts
WRITELN(TrailOut, 'far to obtain a proper intersection.');
WRITELN(TrailOut);
Intx:= 00.000;
Inty:=00.000;
Computed := FALSE;
```

END;
WRITELN! ' Leaving XPREP';;

END; (* PRDCEDURE "XPREP" *)


i This procedure is called twice by "XSEC", once for each of the two stations involved in the computation of their LOB intersection. If the intersection is negative then no intersection is computed.

NOTE: The parameters of $I$ and $J$ contain the staion number of the two stations whose intersection is to be computed.
*)
VAR
Dx, Dy : REAL; (* Temporary variable for Di and D2. *)
Cosiner, SineI : REAL;
CosineJ, SineJ: REAL;
TempDist : REAL;
BEGIN
WRITELN( Entering XCOMP');
$D x:=X d i s t ;$
$D y:=$ Ydist;
IF (StIdent[I]. Alpha = StIdent[J]. Alpha) THEN

```
Intx:= 00.000;
```

Inty : = 00.000;
Computed : = FALSE;
WR ITELN(Trail口ut);
WRITE(Trailout, 'Station \#', StIdent[I]. Orgin:1, " and Station \#');
WRITE(Trail口ut, StIdent[J]. Orgin:1, ' have the same initial LOB');
WR ITELN(Trailout);
WRITELN(TrailOut, 'trajectory. . . No intersection possible.' ');
WRITELN(Trail0ut);

END
ELSE
BEEIN

```
CosineI := COS((iStIdent[I].Theta) * Pie) / Radiani;
CosineJ:= COS((<StIdent[U].Theta) * Pie) / Radiani;
SineI := SIN(((StIdent[I]. Theta) * Pie) / Radian);
Sinev := SIN(((StIdent[J]. Theta) * Pie) / Radian);
Xdist : = (( Dx * CosineJ) - (Dy * SineJ ));
Xdist := Xdist/SIN(<(StIdent[J].Theta - StIdent[I].Theta) * Pie)/ Radie:
Ydist := (( Dx * CosineI ) - ( Dy * SineI ));
Ydist := Ydist/SIN(((StIdent[J].Theta - StIdent[II.Theta) * Pie)/ Radia-
Computed : = True;
```

END;
IF (Computed $=$ TRUE) THEN
BEGIN

```
        Intx := StIdent[I]. Xcoord + (Xdist * SIN(((<StIdent[I]. Thetia)
                * Pie) ( Radian));)
        Inty : = StIdent[I]. Ycoord + (Xdist * COS((()StIdent[I]. Theta)
                        * Pie) / Radian)));
        Computed : = TRUE;
```

    END;
    IF ( $(A B S($ (StIdent[I].Alpha) - (StIdent[J]. Alpha)) $\leqslant=0.6)$ AND
(Computed $=$ TRUE)) THEN
BEGIN

```
WR ITELN(TrailOut);
WRITE(TrailDut,'The difference between the angles of Station #; ;
WRITEiTrailOut, StIdent[I]. Drgin:1,' and Station #',StIdent[J]. Orgin:1;;
WRITELN(TrailOut);
WRITELN(TrailOut,'is too small to obtain a proper intersection.');
WRITELN(TrailOut,'Station #',StIdent[I]. Orgin:1,' and Station #', StIdent[
WRITELN(TrailOut,'are not participating in the test data');
WRITELN(TrailOut);
Intx := 00.000;
Inty:= 00.000;
Computed := FALSE;
```

END:

## BEGIN

XPREP(StIdent, StIdent[I]. Orgin, Intx, Inty, Computed); XPREP(StIdent, StIdent[JJ. Orgin, Intx, Inty, Computed);

END;

WRITELN(' Leaving XCOMP');

END; (* PROCEDURE XCOMP *)


```
PROCELURE ILOBS(VAR AllStat : Lobtype; i*LOB's back to remaining stations
                                    which have inputted data into
                                    the database. *)
    Stident : Lobtype;
    Intx : REAL; (* possibly a VAR *)
    Inty : REAL; (* possibly a VAR *)
    StaNumb : INTEGER;
VAR Table : TVT);
```


(* This procedure completes the intersection file called "INTLO".
Reported LOBS are flagged and stored in "INTLO" as indexed by the
repective station numbers.
4)

VAR
AngleTheta : REAL; (* Angle formed by the fixed point back to eah station. *)
DistX : REALi (* distance between the fixed x-coord and the $x$-coord of the stations' position. *)
Disty : REAL; (* distance between the fixed y-coord and the $y$-coord of the stations' position. *)
Temp4 : REAL;
Temp 5 : REAL;
I, $J, K, N$ : INTEGER;
A, B : INTEGER;
SupportCount: INTEGER;
NewData : Lobtype;
BEGIN
WRITELN( Entering ILOBS');
$\mathrm{N}:=1$;
DistX : $=000000$;
Disty : $=000000$;
$K:=$ StaNumb;

FOR $J:=1$ TO StaNumb DO
IF ( (StIdent[J]. Reflob = TRUE) AND (StIdent[J].Flag = TRUE)) THEN
BEGIN

```
NewData[N]. Orgin := StIdent[J]. Orgin;
```

$N:=N+1 ; \quad$ D-12

## END

## ELSE

BEGIN
NewData［K］．Orgin ：＝StIdent［J］．Orgin；
$K:=K-1 ;$
END；

```
N:= 1;
K:=StaNumb;
```

WR ITELN(Trailout);
WR ITELN(TrailOut);
WFITELN(TrailOut);
WR ITELN(Trail口ut, 'The two stations participating in the intersection ,
WRITELNイTrail口ut,' calculations are:
WRITELN(Trailout,', Station \#, NewData[N]. Orgin:1);
WRITELN(TrailOut,' Station \#, NewData[N + 1]. Crgin: 1);
WRITELN(TrailOut);
WR ITELN(TrailOut,' The following information determines the back');
WR ITELN(TrailOut, 'LOB"s to:
A: = NewData[N]. Orgin;
$B:=N e w D a t a[N+1]$. Drgin;
$A:=$ NewData[A]. Orgin;
$B:=$ NewData[B]. Orgin;

CASE StaNumb DF

2 ：WRITELN（TrailOut，＇
3：WRITELN（TrailOut，＇Station \＃＇，NeuData［K］．Orgin：I）；

WR ITELN（Trailout，＇ WRITELNiTrailout，＇

END；
5：BEGIN
WR ITELN（TrailDut，＂ WRITELN（TrailDut，＂ WRITELN（Trailout，＇

No other station＇）；

7：BEGIN
，

Station \＃＇，NewData［k］．Orgin：1：；
Station \＃＇，NewData［K－i］．Orgin

END；

END；

```
WRITELN(TrailOut);
WR ITELN(TrailOut,'----------_----------------------------------------------------------
WR ITELN(TrailOut, '-------------------------------------------------------------------
```



```
WRITE!TrailGut, '----------For Intersecting Station"s ',NeuData[N]. Orgin:1,' Ar
WRITE(TrailOut,NewData[N + 1]. Orgin:1,'---------');
```

```
WRITELN\TrailOut,'
WRITELN(Trailout,
WRITELN(TrailOut);
WR ITELN(TrailOut);
WRITE{TrailOut, 'Intersecting coordinates for Station #',NewData[N]. Orgiri:1:
WRITE(TrailDut,' and Station #',NewData[N + 1]. Drgin:1,' is:');
WRITELN(TrailOut);
WRITELN(TrailDut);
WRITELN(TrailDut,'( (',Intx:6:3,',',Inty:6:3,')');
WRITELN(TrailOut);
SupportCount:= O;
FOR }\checkmark:=1 TO StaNumb DO
IF ((StIdent[J]. Reflob = TRUE) AND (StIdent[J].Flag = FALSE): THEN
BEGIN
Al1Stat[J].Flag:= StIdent[J].Flag;
WRITELN(TrailOut);
WRITELN(TrailDut,'X-coordinate',StIdent[J]. XEoord:6:3,' of 5tation #
                    StIdent[J]. Orgin:1);
WRITELN(TrailDut,'loaded into the system.');
WRITELN(TrailOut);
AllStat[\l]. Xcoord := StIdent[J]. Xcoord;
WRITELN(TrailOut, 'Y-coordinate', StIdent[u]. Ycoord:6:3,' of Stavien =
                            StIdent[J]. Orgin:1);
WRITELN(TrailOut,'loaded into the system.'';
WRITELN(TrailOut);
Alistat[\]. Ycoord := StIdent[v]. Ycoord;
DistX:= (Intx - AllStat[J].Xcoord); (* could be ABS *)
DistY : = (Inty - AllStat[J]. Ycoord); (* could be ABS *)
IF DistY = 00.000 THEN
    BEGIN
WRITELN(Trai lOut);
WRITELN\TrailOut,' This station can not exist at the location'y;
WRITELN(TrailOut,' 0f (',DistX:6:3,',',DistY:6:3,')');
WRITELN(TrailOut);
END
ELSE
```

```
BEGIN
```

BEGIN
IF ((DistY< 00.000) AND (DistX < 00.000)) THEN
BEGIN
AngleTheta := ARCTAN(Distx/DistY) * 180/Pie;
AngleTheta : = AngleTheta + 180.000;
IF AngleTheta < 00.000 THEN
AngleTheta }:=360.000 + AngleTheta;
END
ELSE
D-14

```
```

IF ((DistY < 00.000) AND (DistX > 00.000)) THEN

```
begin
```

Disty $:=00.000-$ Disty;
AngleTheta $:=$ ARCTAN(DistX/Disty) * 180/Pie;

```

END
ELSE
BEGIN
AngleTheta \(:=\operatorname{ARCTAN(DistX/Disty)} * 180 /\) Fie;
END;
```

WRITELN(TrailOut);
WRITELN(TrailOut,'The exact computed LOB angle is = ', AngleTheta:=
WRITELN(TrailOut);
Temp4:= ABS(StIdent[J]. Theta - AngleTheta);
StIdent[J]. MissAngle := Temp4;
AllStat[J]. MissAngle := StIdent[J]. MissAngle;
IF {Temp 4 \= 360. O} THEN
Temp4 := Temp4 - 360.0;
IF (Temp4<= (3 * Sigma)) THEN
BEGIN

```
    Temp \(5:=\) Temp4 * Temp4;
    Table[A, B]. Support : = TempS + Table[A,B]. Support;
    Table[B, A]. Support : = TempS + Table[B,A]. Support;
    Table[A, B]. SupportFlag[StIdent[J]. Orgin]: := TRUE;
    Table[B, A]. SupportFlag[StIdent[J]. Orgin] := TRUE;
    SupportCount := SupportCount +1 ;
    Table[A, B]. SupCountFlag : = SupportCount;
    END
ELSE

BEGIN
Table[A, B]. SupportFlag[StIdent[J]. Orgin] := FALSE;
Table[B, A]. SupportFlag[StIdent[J]. Orgin]: = FALSE;
 WRITE(TrailQut,' is greater than 3 sigma.' '); WRITELN(Trailout);

END;
WRITELN(TrailOut);
WRITELN(Trai iDut, 'Difference between the back LOB angle and the'; ; WRITE(Trailout, 'actual angle for Station \#', StIdent[J]. Orgin: 1 ; WRITE(Trailout,' = ', Temp4:6:3,'.');
WRITELN(Trailout);
WRITELN(Trailout);
D-15

END;
END
ELSE
IF ((StIdent[J].Reflob = TRUE) AND (StIdent[J].Flag = TRUE)) THEN
BEGIN
AllStat[J]. Xcoord \(\quad:=\) StIdent[J]. Xcoord;
AllStat[J]. Ycoord \(:=\) StIdent[J]. Ycoord;
AllStat[J]. Alpha \(:=\) StIdent[J]. Alpha;
AllStat[J]. Theta \(:=\) StIdent[J]. Theta;
AilStat[J]. Refiob \(:=\) StIdent[J]. Reflob;
AllStat[J]. Flag \(\quad:=\) StIdent[J]. Flag;
AllStat[J]. Missangle : = StIdent[J]. MissAngle;
AllStat[J]. Orgin \(:=\) StIdent[J]. Orgini
END
ELSE
BEGIN
\begin{tabular}{|c|c|}
\hline Allstat[J]. Xcoord & 00.000: \\
\hline Allistat[J]. Ycoord & \(=00.000\); \\
\hline Allstat[J]. Alpha & \(=00.000 ;\) \\
\hline AllStat[J]. Theta & \(=00.000 i\) \\
\hline Allstat[J]. Reflob & = FALSE; \\
\hline AllStat[J]. Fiag & = FALSE; \\
\hline AllStat[J]. Missangle & -00.000; \\
\hline AllStat[J]. Orgin & StIdent[J]. Orgin \\
\hline
\end{tabular}

END:
```

WRITELN(TrailOut, '------------------------------------------------------------
WRITELN\TrailGut,'-------------End Of Inputted Data---------------------
WRITE(TrailOut, '--------Far Intersecting Station"s ',NewData[N]. Orgin:1,
WRITE(TrailOut, NewData[N + 1]. Orgin:1, '--------');
WRITELN(TrailOut);
WRITELN(TrailOut,'
WRITELN(TrailOut);
WR ITELN(TrailOut);
WRITELN(TrailOut);
WRITELN(TrailOut);
WRITELN(TrailOut);
WRITELN(TrailOut);
WRITELN(' Leaving ILOBS');
Temp5 := 00.000;
END; (* PROCEDURE "ILOBS" *)

```

(*
This procedure uses the two LOBS to determine if there is an intersecton using the criteria for a valid fix estimate. intersecting coordinates are INTX and INTY. " XSEC" establishes a series of LOBS called INTLO from all stations to the intersection point.
*)

VAR
\(X\) : \(Y\) : REAL; (* Dummy variables for intx and Inty *)
Xdist
REAL; (* Distance of \(X 1-X 2\) *)
YdiEt
REAL; (* Distance of Y1 - Y2 *)
Listi, Liste : Intlotype; (* used for computing intercept coords. *)
AllStat : Lobtype; (* data structure that will contain all of the LOB's that return to station that did not attempt any LOB's. *)

BEGIN
WRITELN(' Entering XSEC');
\(x:=I n t x ;\)
\(Y:=I n t y ;\)
Xdist \(:=00.000\);
Ydist \(:=00.000\);
Intx : = 00.000;
Inty \(:=00.000\);

Xdist : = (StIdent[I]. Xcoord - StIdent[J]. Xcoord); (* could be ABS : ;
Ydist : \(=\) (StIdent[I]. Ycoord - StIdent[J]. Ycoord); (* could be ABS *)
XCDMP (I, J, Xdist, Ydist, StIdent, Intx, Inty, Computed);

IF (Computed = FALSE) THEN
BEGIN
```

WRITELN(TrailOut);
WRITELN(TrailOut,' No intersection found from this data using';;
WRITE(TrailDut,' Station \#',StIdent[I].Orgin:1,' and ');
WRITE(TrailOut,' Station \#',StIdent[J]. Drgin:1);
WRITELN(TrailDut);
WRITELN(TrailOut);

```

END;
```

WRITELN:' Leaving xSEC');

```
END: (* PRDCEDURE "XSEC" *)

Lob : Lobtype); D-17
```

    the test for validity ( i.e. > 0.6 ) then the corresponding value in
    the Truth table will be marked indicating that the intersection failed
    the validity test.
    *)
VAR
BinNumber : INTEGER;
AStation : INTEGER;
BEGIN

```
```

WRITELN(' Entering ZEXI');

```
WRITELN(' Entering ZEXI');
FOR BinNumber := 1 TO 5 DO
    FOR AStation := 1 TO 5 DO
        IF Table[BinNumber, AStation].Flag = TRUE THEN
                IF (ABS(Lob[BinNumber]. Xcoord - Lob[BinNumber].Ycoord)) > 0.6 THEM
                    Table[BinNumber,AStation].Flag := FALSE;
WRITELN(, Leaving ZEXI');
END; (* PRDCEDURE "ZEXI" *)
```


procedure reconvert ( Lobrec : Labtype;
VAR Starec : Lobtype);

```
<***************#*******************************************************************
(* This subroutine takes the data stored in "Lobrec"and places it in the
    original order in the data structure called "Starec".
*)
VAR
J : INTEGER;
Location : INTEGER;
```

BEGIN
WRITELN( Entering RECONVERT');
FOR Location : $=1$ TO 5 DO
EEGIN
$\checkmark \quad:=$ Lobrec[Location]. Orgini Starec[J]. Xcoord := Lobrec[Location]. Xcoord; Starec[J]. Ycoord $:=$ Lobrec[Location]. Ycoord; Starec[J]. Theta $:=$ Lobrec[Location]. Theta; Starec[J]. Alpha $:=$ Lobrec[Location]. Alpha; Starec[J]. Reflob $:=$ Lobrec[Location]. RefLob; Starec[J].flag $:=$ Lobrec[Location]. Flag;

END;
WRITELN(' Leaving RECONVERT');
END; \&* PROCEDURE "RECONVERT" *?

VAR Lobrec : Lobtype);


```
(* This subroutine takes the data stored in "Starec" and places it in a
    sequenced order starting in the first and subsequent cells of the data
    structure "Lobtype".
*)
```

VAR
J. $K$ : INTEGER;

Location : INTEGER;
BEGIN
WRITELN(' Entering CONVERT');
$\checkmark:=0$;
$k:=6$;
FOR Location := 1 TO 5 DO
IF StarectLocationl. Reflob $=$ TRUE THEN
BEGIN

```
J:= J + 1; (* index for Lobrec *)
Lobrec[J]. Xcoord := Starec[Location]. Xcoord;
Lobrec[J]. Ycoord := Starec[Location]. Ycoord;
Lobrec[J].Theta := Starec[Location]. Thetai
Lobrec[J].Alpha := Starec[Location].Alpha;
Lobrec[J].Reflob := Starec[Location].Reflob;
Lobrec[J].Flag := Starec[Location].Flag;
Lobrec[J]. Orgin := Location;
```

END

## ELSE

BEGIN


END;
WRITELN(' Leaving CONVERT');
END; (* PROCEDURE "CONVERT" *)



```
(* This procedure extracts the data from the database for use in
    computing the intersection of the LOB's from the BINSETS for each
        station. Parameter "Table" will contain truth-value assignments for
        valid intersections in the Binsets of each Station.
    *)
VAR
    I. J : INTEGER; (* index for the data structure LOBREC *)
    BinNumber : INTEGER;
    AStation : INTEGER;
    NextOne : INTEGER;
    MaxSupport : INTEGER;
    TempStation: INTEGER;
    LoopCntr : INTEGER;
    Location1: INTEGER;
    Location2 : INTEGER;
    Location3 : INTEGER;
    Location4 : INTEGER;
    X1 : REAL;
    Y1 : REAL;
    Intx : REAL;
    Inty : REAL;
    MinExactLob: REAL;
    Lobrec : Lobtypej
    AllStations : Lobtype; (* keeps track of the back LOB's to the
                                    stations whose intersection has not yet
                                    been calculated. *)
```

BEGIN
WR I TELN(.
Entering GAXI');
AStation : = 2;
TempStation : = AStation;
BinNumber : = 1;
$\operatorname{Intx}:=00.000$;
Inty $:=00.000$ i
CASE StaNumb OF
2: LoopCntr:=1;
3 : LoopCntr := 3;
4 : LoopCntr : = 6;
5 : LoopCntr: $=10$ i

END;

CONVERT(Starec, Lobrec);

WHILE Dspxi <= LoopCntr DO
BEGIN
IF TempStation $=$ StaNumb +1 THEN

BEGIN

```
AStation := AStation + 1;
TempStation : = AStation; D-20
BinNommon = = AinNlmmer + 1:
```

```
        Lobrec[BinNumber - 1].Flag:= FALSE;
```

END;
IF (iLobrec[BinNumber].Reflob = TRUE) AND (Lobrec[TempStation]. Reflob = TRUE)) THEN

BEGIN

XSEC(Lobrec, StaNumb, BinNumber, TempStation, Intx, Inty, Computed); END;

Location3 : = Lobrec[BinNumber]. Orgin;
Location4 $:=$ Lobrec[TempStation]. Orgini
IF Computed = FALSE THEN

## BEGIN

Table[Location3, Location4]. Flag: = FALSE;
Table[Location4, Location3]. Flag : = FALSE;

## END

ELSE
BEGIN

```
Table[Location3, Location4]. Xintercept := Intx;
Table[Location3, Location4]. Yintercept := Inty;
Table[Location4,Location3]. Xintercept := Intx;
Table[Location4,Location3]. Yintercept := Inty;
Table[Location3,Location4].Fiag : = TRUE;
Table[Location4, Location3].Fiag : = TRUE;
Lobrec[BinNumber]. Flag : = TRUE;
Lobrec[TempStation]. Flag : = TRUE;
ILOBS(AllStations,Lobrec, Intx, Inty,StaNumb,Table);
FOR I := 1 TO StaNumb DO
    IF Al1Stations[I].Flag = FALSE THEN
        BEGIN
            \:=Lobrec[I]. Orgin;
            Starec[J]. MissAngle := AllStations[I]. MissAngle;
            END;
    END:
```

Dspxi : $=D \operatorname{spxi}+1 ;$
TempStation : = TempStation + 1;
Lobrec[TempStation - 1].Flag : = FALSE;
END;

```
WRITELN(TrailDut,'This is the table that shows the relation of data');
WRITELN(TrailOut,'between any of the stations.');
WRITELN(TrailOut);
WRITE(TrailOut, '------------------------
WRITE(TrailOut,' ---m---');
WRITELN(TrailOut);
WRITE(TrailOut, 'Intersecting Stations Xintercept Yinter:-
WRITE(TrailDut,' Support');
WR ITELN(TrailOut);
WR ITE\TrailOut,'--------------------
WRITE(TrailOut,' ---m---');
WR ITELN(TrailOut);
MinExactLob:= 10000000000.000;
NextOne := 5i
MaxSupport := O;
FOR BinNumber := 1 TO 5 DO
    FGR TempStation := 1 TO 5 DO
```

BEGIN
WRITE(TrailGut, 'Station "', BinNumber: 1, ' Station \#', TempStation: i);
WRITE(Trailout, ' ');
WRITE(TrailOut, Table[BinNumber, TempStation]. Xintercept: 6: 3);
WRITE(TrailOut, ' ');
WRITE(TrailOut, Table[BinNumber, TempStation]. Yintercept: 6: 3);
WRITE (Trailout, ' , Table[BinNumber, TempStation]. SupCoumtFiag: $:$
WRITELN(Trailout);
IF ( ( (Table[BinNumber, TempStation]. SupCountFlag < NextOne: AND
(Table[BinNumber, TempStation].SupCountFlag > MaxSupport)) AND
(Table[BinNumber, TempStationd.Flag = TRUE)) THEN

## BEGIN

MaxSupport : = Table[BinNumber, TempStation]. SupCountFlag;
Location 1 : = BinNumber;
Locatione : = TempStation;

## END;

END;

FOR I : $=1$ TO 5 DO
BEGIN
WR ITELN(Trailout);
WR ITELN(Trailout,' $\qquad$
WR ITELN(TrailDut,' ' $\overline{\text { Station } \# ', ~ I: 1, ' ~ d a t a: ' ~ ') ; ~}$
WR ITELN(Trailout, '-_- --_-_(
WRITELN(Trailout);
WRITELN(TrailOut, ' X -coord = ', Starec[I]. Xcoord: 6: 3);
WR ITELN(Trailout, 'Y-coord
= ', Starec[I]. Ycoord: 6: 3);
WRITELN(Trailout,' Theta
= ',Starec[I]. Theta:6:3);
WRITELN(Trailout, 'Alpha= = Starec[I]. Alpha:6:3);
WRITELN(Trailout, 'Reflab= ', Starec[I]. Reflob);
WRITELN(Trailout, 'Flag $D-22=$ ', Starec[I]. Flag);
WR ITELN(Trailout, 'Semimajor = ', Starec[I]. Semimajor: 6: 3);


```
WRITELN(Trail口ut,'Distance = ',Starec[I].Distance:6:3);
WRITELN(TrailOut,'Orgin = ',Starec[I]. Orgin:2;;
```

WR ITELN(Trail口ut);

END；
WR ITELN（TrailOut，＇From the data submitted by each station and the data：； WRITELN（TrailOut，＇extracted from various calculations the best＂FIX＂＇）； WRITELN（Trailout，＇location of the object attempting to transmit is at：＇）； WRITELN（Trailout）；

WR ITE（Trailout，Table［Location1，Location2］．Yintercept：6：3，＇）＇；
WR ITELN（TrailOut）；
WR ITELN（TrailOut）；
WRITELN（TrailDut）；
WR ITELN（Trail口ut）；
WRITELN（Trailout）；
WFiTELN（＇Leaving GAXI＇）；
END；（＊PRDCEDURE＂GAXI＂＊）

PROCEDURE SUXI（VAR Dspxi ：INTEGER）；

（＊This procedure sets up the diplacement variable（parameter Dspxi ） and sets up the ability to extract data from the database through use of the displacement variable．
$* *$

BEGIN
WRITELN（＇Entering SUXI＇$) ;$
Dspxi ：$=1 ; \quad(*-1$ in actual progran＊）
WRITELN（＇Leaving SUXI＇）：
END；（＊PRDCEDURE＂SUXI＂＊）

PROCEDURE LMARK（VAR Table：TVT；
Lobrec ：Lobtype ）；

i火 This procedure marks LDBS acceptable for use in fix estimation．Marked LOBS for optimixed fix estimation are used by＂FPEAK＂to obtain a best fix．
＊）

VAR

BinNumber ：INTEGER；
I ：INTEGER；
BEGIN
WRITELN！＇
Entering LMARK＇）；
$I:=1$ ；

FOR BinNumber $:=1$ TO 5 DO

```
    IF ((Lobrec[BinNumber]. Xcoord = Lobrec[BinNumber + I]. Xcoord) AND
        (Lobrec[BinNumber].Ycoord = Lobrec[BinNumber + 1].Ycoord); THEN
        Table[AStation, BinNumber].Flag := TRUE;
    I := I + 1;
    WRITELN(' Leaving LMARK');
END; (* PRDCEDURE "LMARK" *)
```

VAR
Dspxi : INTEGER;
Computed : BOOLEAN;

```


```

PROCEDURE FIRSTPASS\Lobrec : Lobtype;

```
PROCEDURE FIRSTPASS\Lobrec : Lobtype;
    StaNumb : INTEGER;
    StaNumb : INTEGER;
    Table : TVT;
    Table : TVT;
    Intlo : Intlotype);
```

    Intlo : Intlotype);
    ```


```

(* This sub does whatever.

```
(* This sub does whatever.
*)
*)
BEGIN
WRITELN( Entering FIRSTPASS');
Computed : = FALSE;
SUXI(Dspxi);
GAXI(Table, Computed, Dspxi, Lobrec, StaNumb);
WRITELN(, Leaving FIRSTPASS');
END; (* PROCEDURE "FIRSTPASS" *)
```



```
PROCEDURE LOADDATA(VAR Lobrec : Lobtype;
VAR StaNumb : INTEGER);
(* This procedure prompts the user for input to the TRAILBLAZER program.
*)
VAR
Tempó : INTEGER;
StationCntr: INTEGER;
BEGIN
```

```
WRITELN("
```

WRITELN("
Entering LDADDATA');
Entering LDADDATA');
REPEAT
WRITELN(TrailOut);
WRITELN(TrailOut, ' How many stations will be reporting LOB"s');
WRITELN(TrailOut,' on the transmitting object.',);
READ(TrailIn,StaNumb);
WRITELN(TrailOut,StaNumb); D-24

```
```

Temp6:= StaNumb;
IF ( (Tempb }=\mathrm{ = 0) OF (Temp' }>=6)) THE
BEGIN
WRITELN(TraiIDut);
WRITELN('This value ',StaNumb:2,' is invalid');
WRITELN\&'Try again with a value from 1 to 5.');
WRITELN(TrailOut);
END;

```
```

UNTIL ((TempG > O) AND (TempG < 6));

```
UNTIL ((TempG > O) AND (TempG < 6));
REPEAT
EEGIN
Temps := Temp6 - 1;
REPEAT
REPEAT
WRITELN(TrailOut);
WRITELN(TrailOut, 'Input the Station that is "FIXING".');
READ(TrailIn, StationCntr);
WRITELN(TrailOut, StationCntr);
IF {(StationCntr <= 0) OR (StationCntr >= 6)) THEN
BEGIN
WRITELN(TrailOut);
WRITELN(TrailOut,'This value ', StationCntr'2,' is invalid';;
WRITELN(TrailOut,'Try again with value from 1 to 5.');
WRITELN(TrailOut);
END;
UNTIL ( (StationCntr \(>0\) ) AND (StationCntr < 6));
IF Lobrec[StationCntr]. Reflob = TRUE THEN
```


## BEGIN

WRITELN(Trailout);
WRITELN(TrailDut,' Station \#', StationCntr: 1, ' has already been');
 WRITELN(Trailout);

END:
UNTIL Lobrec[StationCntr]. Reflob = FALSE;

```
WR ITELN(TrailOut);
```

WR ITELN(Trailout, 'Input the x-coordinate of Station \#', StationCntr: 1);
READ (Trailin, Lobrec[StationCntr]. Xeoord);
WR ITELN(Trailout, Lobrec[StationCntr]. Xeoord: 6: 3);
WRITELN(Trailout);
D-25

READ(TrailIn, Lobrec[StationCntr]. Ycoord);
WRITELN(TrailOut, Lobrec[StationCntr]. Ycoord: 6: 3);
WR I TELN(TrailOut);
WRITELN(Trailout, 'Input the angle, in relation to true North, formed';;
WRITELN(TrailQut, 'by Station \#', StationCntr:1,' and the possible'); WRITELN(Trailout, 'location ( FIX) of the transmitting object');
READ(TrailIn, Lobrec[StationCntr]. Theta);
WR ITELN(Trail口ut, Lobrec[StationCntr]. Theta: 6: 3);
WR ITELN(TrailOut);
IF Lobrec[StationCntr]. Theta $>180.00$ THEN
Lobrec[StationCntr]. Theta : = Lobrec[StationCntr]. Theta - 360.00;
Lobrec[StationCntr]. Alpha : = 90-Lobrec[StationCntr]. Theta; Lobrec[Stationcntr].Reflob : = TRUE;
WR ITELN(Trail口ut);

END;

UNTIL (TempG $=0$ );
WRITELN(, Leaving .LDADDATA');
END; (* PRDCEDURE "LDADDATA" *)


| PROCEDURE ESTMP (Lobrec | : Lobtype; |
| ---: | :--- |
| IntPass | INTEGER; |
| Index | $:$ INTEGER; |
| Intlo | $:$ Intlotype; |
| Table | $:$ TVT); |


(*
This procedure is called by "HPFIX" to obtain abest fix estimate. A single fix or one of mutilplefixes in either the normal mode or the degraded mode may be requested.
"ESTMP" calls the following procedures and/or functions:
SUBS COMMENTS

1) GAXI : Extracts two Lines of Berings (LOBS) for computing intersection.
2) INELL : To determine and ensure that a fix estimate doesn't duplicate the last or any previous fix
3) LMARK : Marks LOBS acceptable for use in fix estimation.
4) MSCAN: Clears marks from database.
5) SCNDB : Accumulates counts of marked LDBS for each station.
6) SUXI : Sets up the ability to extract data from each station.
7) XSEC : Uses two LOBS to determine if there is an intersection using the criteria for a valid fix estimate.
8) ZEXI : Clears appropiate indicators when an intersection fails validity.
\#)
VAR
Dx. Dy : REAL; D-26

Xefix
REAL; (* $x$ coordinate of estimate *)
Yefix
REAL; (* y coordinate of estimate *)
Templefix : REAL; (* temporary variable for Xefix *)
Temnvefix



BEGIN

## WRITELN('

Entering ESTMP');

| Dx | $:=00.000 ;$ |
| :--- | :--- |
| Dy | $:=00.000 ;$ |
| Xefix | $:=00.000 ;$ |
| Yefix $:=00.000 ;$ |  |
| Nsame $:=0 ;$ |  |
| Nother $:=0 ;$ |  |
| Nmax $:=0 ;$ (* maximum LOB counter | $=*$ ) |

LOADDATA(Lobrec, StaNumb);
FIRSTPASS (Lobrec, StaNumb, Table, Intlo);

IF IntPass $>1$ THEN
BEGIN
INELLIPSE (Xefix, Yefix, Ansuer, Table);
TempXefix: = Xefix;
TempYefix : = Yefix;
IF Answer = TRUE THEN
BEGIN
ZEXI(Table, Lobrec);
CLEAR (Lobrec, Intlo, Table);
END
ELSE
LMARK(Table, Lobrec);
WHILE Index $>-1$ Do

```
        IF Lobrec[Bin].Flag = TRUE THEN
        BEGIN
                Cntfunction := 0;
                SCNDB(Cntfunction, Index,Lobrec);
            END
            ELSE
        Lobcounter := Lobcounter + 1;
        Index := Index - 1;
    END;
IF Nother =0 THEN
    BEGIN
        IF Made = TRUE THEN
        IF Nsame >= 4 THEN
            BEGIN
            Newcounter := Nsame + Nother;
            IF Nmax >= Newcounter THEN
                BEGIN
                    Nmax := Newcounter;
                    Xefix:= Intxi
                    Yefix:= Inty;
                    Nsame : = 0;
                    Nother := 0;
                    Newcounter := 0;
                END
                ELSE
                    BEGIN
                    ZEXI(Table, Labrec);
                    CLEAR(Lobrec,Intlo,Table);
                    Nsame := O;
                    Nother := 0;
                    Nmax := 0;
                    MSCAN(Lobrec);
                    END;
            END;
    END
ELSE
```

Newcounter : = Nsame + Nother;

```
IF Nmax \(\rangle=\) Newcounter THEN

BEGIN
Nmax : = Newcounter;
Xefix: = Intxi
Yefix: \(=\) Intyi
Nsame : \(=0\);
Nother : \(=0\);

\section*{END;}

END:
END;

WRITELN(' Leaving ESTMP');
END; (* PROCEDURE "ESTMP" *)



(* MAIN PRDGRAM*)
EEGIN
REWRITE(Trailout);
RESET(TrailIn);
WR ITELN(Trailout);
WR ITELN(Trailout);

WRITELN(TrailQut, '**** BEGINNING PROGRAM TRAILBLAZER ****');
 WR ITELN(Trailout); WR ITELN(TrailOut);

Index : = 0 ;
IntPass \(:=1 ;\) (* First pass through the system *)
CLEAR (Lob, Intlo, Table);
ESTMP(Lob, IntPass, Index, Intlo, Table);
WRITELN(TrailOut):
WR ITELN(TrailOut);

WR ITELN(TrailDut, '**** PROGRAM TRAILBLAZER COMPLETED ****');
 WR ITELN(TrailOut); WRITELN(Trailout):

END. (* MAIN PROGRAM "TRAILBLAZER" *)
```

**** BEGINNING PROGRAM TRAILBLAZER ****

```
```

    How many stations will be reporting LOB"s
    on the transmitting object.
        4
    Input the Station that is "FIXING".
1
Input the x-coordinate of Station \#1
10.000
Input the y-coordinate of Station \#1
18. }00
Input the angle, in relation to true North, formed
by Station \#l and the possible
location ( FIX) of the transmitting object
50.000

```
Input the Station that is "FIXING".
        2
Input the x-coordinate of Station \#2
    20. 000
Input the \(y\)-coordinate of Station \#2
    5. 000
Input the angle, in relation to true North, formed
by Station \#2 and the possible
location ( FIX) of the transmitting object
    33. 000
Input the Station that is "FIXING".
            3
Input the \(x\)-coordinate of Station \#3
    60.000
Input the \(y\)-coordinate of Station \(\# 3\)
    25. 000
Input the angle, in relation to true North, formed
by Station *3 and the possible
location ( FIX) of the transmitting object
\(-5.000\)

Input the \(x\)-coordinate of Station \#4
90.000

Input the \(y\)-coordinate of Station *4
25. 000

Input the angle, in relation to true North, formed by Station \#4 and the possible location ( FIX) of the transmitting object 312. 000

The two stations participating in the intersection calculations are:

Station \({ }^{*} 1\) Station \#2

The following information determines the back LOB"s to:

Station \#3
Station \#4
---------Beginning Of Inputted Data-
- -------For Intersecting Station"s 1 And

Intersecting coordinates for Station \#1 and Station \#2 is:
(50.525, 52. 005)

X-coordinate 60.000 of Station \#3
loaded into the system.
Y-coordinate 25.000 of Station \#3
loaded into the system.

The exact computed LOB angle is \(=\mathbf{- 1 9} 334\)

Difference between the back LOB angle and the actual angle for Station \(\# 3=14.334\).

X-coordinate 90.000 of Station \#4 loaded into the system.
_ Y-coordinate 25.000 of Station \#4
loaded into the system.
\[
\mathrm{D}-31
\]

The exact computed LOB angle is \(=\mathbf{- 5 5} .624\)

Difference between the back LOB angle and the
actual angle for Station \(\# 4=7.624\).


———————For Intersecting Station"s 1 And 2-

The two stations participating in the intersection calculations are:

Station \#1
Station \#3
The following information determines the back LOB"s to:

Station \#2
Station \#4
-

Intersecting coordinates for Station \#1 and Station \#3 is: (57.151, 57. 564)

X-coordinate 20.000 of Station \#2 loaded into the system.

Y-coordinate 5. 000 of Station \#2 loaded into the system.

The exact computed LOB angle is \(=35.252\)

Difference between the back LOB angle and the actual angle for Station \(\# 2=2.252\).

X-coordinate 90.000 of Station \#4
loaded into the system.
Y-coordinate 25. 000 of Station \#4 D-32 loaded into the sustem.

The exact computed LOB angle is \(=-45.249\)

Difference between the back LaB angle and the actual angle for Station *4 \(=2.751\).
-_---------E-End Df Inputted Data-
-------For Intersecting Station"s 1 And 3-

The two stations participating in the intersection calculations are:
\[
\begin{aligned}
& \text { Station } \# 1 \\
& \text { Station } \$ 4
\end{aligned}
\]

The following information determines the back LOB" 5 to:

Station \#2
Station \#3


Intersecting coordinates for Station \#1 and Station \#4 is:
(55. 434, 56. 124)

X-coordinate 20.000 of Station \#2
loaded into the sustem.
Y-coordinate 5. 000 of Station \(\#\)
laaded into the system.

The exact computed LOB angle is \(=34.726\)

Difference between the back LOB angle and the actual angle for station \(\# 2=1.726\).
\(X-c o o r d i n a t e ~ 60.000\) of Station \(\# 3\) loaded into the system.

Y-coordinate 25.000 of Station \#3 loaded into the system.

The exact computed \(L O B\) angle is \(=-8.346\)

Difference between the back \(L O B\) angle and the actual angle for Station \(\# 3=3.346\).
```

_-_----------End Of Inputted Data------------------
_-_-----_or Intersecting Station"s 1 And 4-----

```

The two stations participating in the intersection calculations are:

> Station \#2 Station \#3

The following information determines the back LOB"s to:

> Station \#1
> Station \#4
\(\qquad\)





Intersecting coordinates for Station *2 and Station \#3 is:
(56.793. 61.656)

X-coordinate 10.000 of Station \#1
loaded into the system.
Y-coordinate 18. 000 of Station \#1
loaded into the system.

The exact computed LOB angle is \(=46.986\)

Difference between the back \(L O B\) angle and the actual angle for Station \#1 = 3.014.

X-coordinate 90 OOO nf Gtatinn \#a
loaded into the system.
Y-coordinate 25.000 of Station \#4
loaded into the system.

The exact computed LOB angle is \(=-42.174\)

Difference between the back LOB angle and the actual angle for Station \(\# 4=5.826\).

--------For Intersecting Station"s 2 And 3-m--m-

The two stations participating in the intersection calculations are:

> Station \#2
> Station \(\# 4\)

The following information determines the back LOB"s to:

> Station \#1

Station \#3

Intersecting conrdinates for Station \(\# 2\) and Station \#4 is:
(54.024, 57.393)

X-coordinate 10.000 of Station \#1 loaded into the system.

Y-coordinate 18.000 of Station \#1 loaded into the system.

The exact computed LOB angle is \(=48.178\)

Difference between the bark LOB angle and the actual angle for Station \#1 = 1.8e2. \(\mathrm{D}-35\)
```

X-ronrdinate 60. OGO of Station \#3
loaded into the system.
Y-coordinate 25.000 of Station \#\#
loaded into the system.
The exact computed LOB angle is $=-10.452$
Difference between the back LOB angle and the actual angle for Station $\# 3=5.452$.

```
\(\qquad\)

The two stations participating in the intersection calculations are:

Station \#3
Station \#4
The following information determines the back LOB"s to:

Station \#1
Station \#2


Intersecting coordinates for Station \#3 and Station \#4 is:
(57.435. 54. 322)
\(X\)-coordinate 10.000 of Station \#1 loaded into the system.

Y-coordinate 18.000 of Station \#1 loaded into the system.

The exact computed LOB angle is \(=52.558\)
D-36
Difference between the back LDB angle and the
actual angle for Station \#1 = 2.558 .

X-coordinate 20.000 of Station \#2
loaded into the system.
- Y-coordinate 5. 000 of Station \#2
loaded into the system.

The exact computed \(L O B\) angle is \(=37.198\)

Difference between the back \(L O B\) angle and the actual angle for Station \#2 \(=4.198\).

This is the table that shows the relation of data between any of the stations.
\begin{tabular}{|c|c|}
\hline \multicolumn{2}{|l|}{Intersecting Stations} \\
\hline Station & \#1 Station \#1 \\
\hline Station & \#1 Station \#2 \\
\hline Station & \#1 Station \#3 \\
\hline Station & \#1 Station \#4 \\
\hline Station & \#1 Station \#5 \\
\hline Station & \#2 Station \\
\hline Station & \#2 Station \#2 \\
\hline Station & \#2 Station \#3 \\
\hline Station & \#2 Station \#4 \\
\hline Station & \#2 Station \#5 \\
\hline Station & \#3 Station \#1 \\
\hline Station & \#3 Station \#2 \\
\hline Station & \#3 Station \#3 \\
\hline Station & \#3 Station \#4 \\
\hline Station & \#3 Station \\
\hline Station & \#4 Station \#1 \\
\hline Station & \#4 Station \#2 \\
\hline Station & \#4 Station \#3 \\
\hline Station & \#4 Station \#4 \\
\hline Station & \#4 Station \#5 \\
\hline Station & \#S Station \# \\
\hline Station & \#5 Station \#2 \\
\hline Station & \#5 Station \#3 \\
\hline Station & \#5 Station \\
\hline & \\
\hline
\end{tabular}
\begin{tabular}{ccc} 
Xintercept & Yintercept & Support \\
\hline 0.000 & 0.000 & 0 \\
50.525 & 52.005 & 2 \\
57.151 & 57.564 & 0 \\
55.434 & 56.124 & 2 \\
0.000 & 0.000 & 0 \\
50.525 & 0.005 & 2 \\
0.000 & 61.656 & 0 \\
56.793 & 57.393 & 0 \\
54.024 & 0.000 & 0 \\
0.000 & 57.564 & 0 \\
57.151 & 61.656 & 0 \\
56.793 & 0.000 & 0 \\
0.000 & 54.322 & 0 \\
57.435 & 0.000 & 2 \\
0.000 & 57.124 & 0 \\
55.434 & 54.393 & 2 \\
54.024 & 0.000 & 0 \\
57.435 & 0.000 & 0 \\
0.000 & 0.000 & 0 \\
0.000 & 0.000 & 0 \\
0.000 & 0.000 & 0 \\
0.000 & 0.000 & 0 \\
0.000 & 0.000 & 0 \\
0.000 & & \\
0.000 & & \\
\hline
\end{tabular}
X-coord \(=10.000\)
Y-coord \(=18.000\)
Theta \(=50.000\)
Alpha \(=40.000\)
Reflob \(=\) TRUE
Flag \(=\) FALSE
Semimajor \(=0.000\)
Semiminor \(=0.000\)
Distance \(=0.000\)
Orgin \(=0\)

\begin{tabular}{|c|c|}
\hline Station \#3 & ta: \\
\hline X -coord & 60.000 \\
\hline Y-coord & 25. 000 \\
\hline Theta & -5. 000 \\
\hline Alpha & 95. 000 \\
\hline Reflob & TRUE \\
\hline Flag & TRUE \\
\hline Semimajor & 0. 000 \\
\hline Semiminar & 0.000 \\
\hline Distance & 0.000 \\
\hline Orgin & 0 \\
\hline
\end{tabular}


Station \(\overline{\text { Sata }}\) :
\(X\)-coord \(=0.000\)
\(Y\)-coord \(=0.000\)
Theta \(=0.000\)
Alpha \(=0.000\)
Reflob \(=\) FALSE
Flag \(=\) FALSE
Semimajor \(=0.000\)
Semiminor \(=0.000\)
Distance \(=0.000\)
Orgin \(=0\)
From the data submitted by each station and the data extracted from various calculations the best "FIX" location of the object attempting to transmit is at:
(50.525, 52.005)

APPENDIX E
DATA BASE ENTRIES FOR TRAILBLAZER

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PART I
TRAILBLAZER

\section*{table of contents}
1. Trailblazer Ouerview

ミ. Utilizes Analysis for HPFIXM
3. Attribute Report . . . . . . . . . . . . . . . . . . . ......................... . .

1. TRAILBLAZER Overview
```

1 TRAILBLAZER FRDCESS DESCRIPTION: TRAILBLAZER is a manned, ground-based direction finding system. The system functions by intercepting targets at the master control station (MCS) and providing at least two DF bearings from some combination of MCS and remote slave station (RSS) subsystems. Successful deployment of the system requires a line-of-sight (LOS) to the target area and to the other subsystems.

```

GYNONYM: AN/TSQ-114
2. Utilizes Analysis for HPFIXM

Utilizes Structure
COUNT LEVEL NAME

\begin{tabular}{|c|c|c|}
\hline COUNT & LEVEL & NAME \\
\hline 50 & 1.4.6.4 & TB_Fmset \\
\hline 51 & 1.4.6.5 & TB_Lmar \(k\) \\
\hline 52 & 1.4.6.5.1 & TB_Sclmk \\
\hline 53 & 1.4.6.6 & TB_Mkact \\
\hline 54 & 1.4.6.7 & TB_Fpot \\
\hline 55 & 1.4.6.7.1 & TB_Scndb \\
\hline 56 & 1.4.6.7.1.1 & TB_Ipot \\
\hline 57 & 1.4.6.7.2 & TB_Sqrt \\
\hline 58 & 1.4.6.8 & TB_Inell \\
\hline 59 & 1.4.6.9 & TB_Zexit \\
\hline 60 & 1.4.6. 10. & TB_Mscan \\
\hline 61 & 1.4.6.11. & TB_Zexi \\
\hline \(\pm 2\) & 1. 4.7 & TB_Groom \\
\hline \(\leq 3\) & 1. 4.8 & TB_Stcpy \\
\hline 64 & 1.4.7 & TB_Mkusd \\
\hline 65 & 1. 4. 10. & TB_Mclr \\
\hline 66 & 1. 4. 11. & TB_Svel1 \\
\hline 67 & 1.4.12. & TB_Odepy \\
\hline 68 & 1.4.12. 1 & TB_Mabin \\
\hline 67 & 1.4.12. 2 & TB_Mscan \\
\hline 70 & 1.4.12.3 & TB_Whbin \\
\hline 71 & 1.4.12.3.1 & TB_Lfin \\
\hline 72 & 1.4.12.4 & TE_Xigel1 \\
\hline 73 & 1.5 TB & Lamp \\
\hline 74 & 1.6 TB & Pchk \\
\hline 75 & 1.7 TE & Store \\
\hline
\end{tabular}

TRAILBLAZER

Utilizes MEtrix

Explanation of the Utilizes Matrix:
The rows are input pROCESS names, and the columns are PROCESSES UTILIZED by (or a SUBPART of) the rows.

*** Matrix empty for Rows il thru 15 and Columns 1 thru 15

Utilizes Mation


\section*{TRAILBLAZER}

Utilizes Matrix



\section*{Utilizes Matrix}

3. Attribute Report

REPORT SPECIFICATION:
1 tree-level \(H=\) 'TREE LEVEL' COL=14
2 mathematical-field \(H=\) 'MATHEMATICAL FIELD' COL=25
*** No SYSTEM-PARAMETERS
TREE LEVEL MATHEMATICAL F:EL
\begin{tabular}{|c|c|c|}
\hline TE_Atan2 & leaf & trigonometry \\
\hline TB_Cos & leaf & trigonometry \\
\hline T3_Dbcpy & middle & data_base_handiling \\
\hline TB_Estmp & middle & logical \\
\hline TB_Final & middle & multivariate_statistics \\
\hline TEFlobs & middle & logical \\
\hline TE Finnew & middle & optimization \\
\hline TR_Fmsam & leaf & optimization \\
\hline TB_Fmset & leaf & optimization \\
\hline TB_Fpeak & middle & optimizations \\
\hline TB_Fpot & middle & optimization \\
\hline TB_Gaxi & leaf & data_base_handiing \\
\hline TB_Groom & leaf & data_base_manipuiation \\
\hline TB_Hpfix & root & logical \\
\hline TB_Hpfixm & root & logical \\
\hline TE_Ilobs & middle & N/A \\
\hline TB_Inell & leaf & multivariate_statistucs \\
\hline TE_Ipot & leaf & optimization \\
\hline T3 Mabin & leaf & data_base_handling \\
\hline TBMkact & leaf & data_base_manioulation \\
\hline TBMscan & leaf & data_base_handling \\
\hline TB_Ddcpy & middle & N/A \\
\hline TB_Sclmk & leaf & data_base_handling \\
\hline TP_Scndb & middle & optimization \\
\hline T3_Sin & leaf & trigonometry \\
\hline TB_Stepy & leaf & data_base_handling \\
\hline TB_Suxi & leaf & data_base_manipulation \\
\hline TB_Svell & leaf & data_base_handling \\
\hline TP_whbin & middle & logical \\
\hline TB_Xeomp & leaf & trigonometry \\
\hline TB_Xprep & middle & N/A \\
\hline TB_xsec & middle & trigonometry \\
\hline TB_Zexi & leaf & data_base_handling \\
\hline
\end{tabular}
4.

TB＿HPFIX．MOD
TB＿FIXD TB＿．ENGU TB＿．DEGU TB＿．PTY TB＿GUIT TB＿DATSET TB＿DISF TB＿ESTAT TB＿HPFIX TB＿LAMP TB＿PCHK TB＿STORE
TB＿HPFIX
TB＿ESTAT
TB＿FORK
TB＿AUTCL
TB＿DBCPY
TB＿ESTMP
TB＿FINAL
TB＿FPEAK
TB＿GROOM
TE－MCLR
TB＿DOCPY
TB＿STCPY
TB＿SVELL
TB＿XYごL
TB＿DBCPY
TB＿．ENQU
TB－．DEGU
TB＿MEMR
TB＿ESTMP
TB＿．ENGU
TB＿．DEQU
TB＿FINAL
TB＿．ENQU
TB＿．DEQU
TB＿ATAN2
TB＿CDS
TB＿SIN
TB＿SQRT
TB＿FPEAK
TB＿．ENQU
TB＿．DEQU
TB＿GRODM
TB＿ODCPY TB＿XYELL TE＿MEMR
TB＿STEPY
TB＿．ENQU

51 52

> TB_DEQU
> TB_SVELL

1 TB_HPFIX.MOD
PROCESS DESCRIPTION: HPFIX is the main module for processing a fix command received from either operator. It computes, displays, and saves fix data as required by the \(f i x\) commands.

ZTEFIXD FROCESE DESCRIPTION:
FIXD is jumped to by COMRET to complete the task of processing the FIX command.

3 TB_ENGU
PROCESS
DESCRIPTION:
Entry point for. ENGU sustem call

4 TB_DEQU PRDCESS
DESCRIPTION:
Entry point for. DEQU system call.

5 TB_PTY
PROCESS

DESCRIPTIDN:
Entry for. PTY instruction call.
\(\therefore T B_{-}\)QUIT
PRDCESE
DESCRIPTION:
Entry point for GUIT instruction.

7 TB_DATSET
PROCESS
DESCRIPTIDN:
DATSET is called by \(F i x D\) when a fix has been successfully computed. It generates a formatted table of fix information
called the DATSET generated fix table.
```

BTB_DISF
PROCESS
DESCRIPTIDN:
DISF is called by FIXD to display each successfully calculated fix and by DISP when processing a DISPLAY command, or during display change processing to re-display fix information.

```
```

7 TB_ESTAT

```

PROCESS
DESCRIPTIGN:
The function of this moduie/proc is to queue error status messages for display on the AN/UYQ-10 and to assure that tie messages are displayed for three seconds. Any moduie may cali ESTAT whenever display of an error/status message is required.

10 TB_HPFIX
PRDCESE
DESCRIPTION:
HPFIX is called by FIXD to compute a fix and to provide ail fin information in a FIX DATA TABLE containing:
the fix point latitude
the fix point longitude
the fix ellipse orientation angle major axis relative to NORTH
the length in km of the fix error ellipse semi-major axis
the length in km of the fix error ellipse semi-minor axis
the display unit number
the LOB display header
the LOB's involved in the fix computation.

\section*{11 TB LAMP}

PROCESS
DESCRIPTION:
LAMP is called to program panel button lights. It combines the panel unit number and the desired function into a command wiori, and sends the command to the selected panel.

12 TEPCHK
PROCESS
DESCRIPTION:
This routine simply checks to see if the page currently on display has function which depend on the page, e. g. to see if the current page number is one which permits text editing.

13 TB_STORE
PROCESS

DESCRIPTIDN:
STDRE is called by COPTRET as a result of a STORE command arid bug FixD for earh fix in a multi-fix request. STORE saves the latest set of fin data in FIXO
\[
14
\]
\(\qquad\) FORK PROCESS

DESCRIPTIDN:
Entry point for. FORK system call.
```

\thereforeE TB_AUTCL
PROCES=

```

DESCRIPTIOH:
AUTCL is called by HPFIX before computing the first multi-fix, and by CLEAR to process the fix portions of the PURGE and DUNE commands or in response to the ELIM command where no specific fixes were specified.

1○ TB_DBCPY
PRDCESS

DESCRIPTION:
DBCPY is called by HPFIX to obtain a local copy of that part af the LOB database which is displayed and not removed. The giadas database referred to is DATAO/DATA1.

17 TB_ESTMP
PROCESS

DESCRIPTION:
ESTMP is called by HPFIX to obtain a best fix estimate for either a single fix or one of multiple fixes in either the normal or degraded mode.
:B TB_FINAL
PROCESS

DESCRIPTIDN:
FINAL is called by HPFIX, after an optimized fix point has been determined, to calculate the parameters of the error elifpses.

19 TB_FPEAK
PROCESS
DESCRIPTION
FPEAK is called by HPFIX to optimize the fix estimate
obtained from ESTMP.

こO TB_GROOM
PROCESS

DESCRIPTIDN:
GROOM is called by HPFIX to initialize the local database for fix computations or to re-initialize it if the fix mode has been degraded to reconsider rejected intersections.

21 TB_MCLR
PROCESS
DEECRIPTIDN:
MCLR is a globally available utility used to update the heacer text and draw the page border divider and/or graphics for a page on the appropriate AN/UYQ-10 display unit.

22 TB_ODCPY
PROCESS

DESCRIPTION:
ODCPY is called by HPFIX, after successful computation of a \(\hat{\mathrm{c}} \mathrm{ix}\). to store all fix related data in a file.

23 TB_STCPY
PROCESS

DESCRIPTION:
STCPY is called by HPFIX to store a local copy of station locations and screen geometry for use in fix computations.

24 TB_SVELL
PROCESS

DESCRIPTION:
SVELL is called by HPFIX to save fix and related ellipse parameters.

25 TB_XYZLL
PROCESS
DESCRIPTION:
XYZLL is called by HPFIX following completion of a successful fix. It takes \(X, Y\) screen coordinates and performs a translation and rotation to get \(X, Y\) coordinates relative to North being directly vertical. An inverse Gnomonic projection is the done to get the latitude and longitude of the point.

\section*{TRAILBLAZER}

DESCRIPTION:
MEMR services memory requests.

SYNONYM: TB_MEMR

O7 TB_ATANE
PROCESS

DESCRIPTION:
ATANE is a giobally avellable utility which determines the floating point radian angle whose tangent is \(X / Y\). \(X\) and \(y\) are double precision arguments supplied to the function

28 TE_COS
PROCESE
DESCRIPTION:
COS is a globally available utility which, passed an angie in floating point radians, calculates its cosine.

29 TB_SIN
PRDCESS

DESCRIPTION:
SIN is a globally available utility which, given an angle in floating point radians, calculates its sine.

30 TB_SQRT PROCESS DESCRIPTION:
SGRT is a globally available utility used to approximate the square root of an input argument.

\section*{APPENDIX F \\ USAMS ALGORITHM ANALYSIS SERIES}

1．Analysis of Geographic Transformation Algorithms JPL D－181

DTIC \＃ADA 129182
Dated：July 9， 1985

2．Correlation Algorithm Report
JPL D－182 UAA－003
DTIC \＃ADA 129181
Dated：September 15， 1982

3．Applications of Correlation Techniques for Battlefield Identification I

JPL D－179 UAA－006
Dated：June 1984

4．Cross－Correlation：Statistics，Templating，and Doctrine JPL D－184

DTIC 非ADA 155624
Dated：February 29， 1984

5．Intelligence Algorithm Methodology I
JPL D－183 UAA－004
DTIC 非ADB 078293
Dated：August 15， 1983

6．Intelligence Algorithms in Target Analysis and Planning （TAP）

JPL D－178 UAA－007
DTIC 非ADB 092402L
Dated：November 30， 1984
7. Intelligence Algorithm Methodology II: An Intelligence/Electronic Warfare (IEW) Tactical Sensors Model JPL D-185 UAA-008

Dated: 1985
8. Intelligence/Electronic Warfare (IEW) Direction-Finding and Fix Estimation Analysis Report
Volume 1, Overview
JPL-180, Vol. 1 UAA-001
9. Intelligence/Electronic Warfare (IEW) Direction-Finding and Fix Estimation Analysis Report

Volume 3, GUARDRAIL
JPL-180, Vol. 3 UAA-001
Dated: December 1985
10. A Non-Standard Probabilistic Position-Fixing Model

JPL D-186 UAA-009
Dated: June 1985
11. A Collection of Area of Interest (AOI) Algorithms JPL D-171 UAA-011

Dated: July 1985
12. Power of Statistical Tests Used in Correlation Techniques for Battlefield Identification

JPL D-2793 UAA-016
Formerly Technical Memorandum No. 5
Dated: August 1985
13. Testing and Combination of Confidence Ellipses: A Geometric Analysis
JPL D-2782
UAA-013
Formerly Technical Memorandum No. 2
Dated: August 5, 1985
14. Wild Bearings Analysis

JPL D-2783 UAA-014
Formerly Technical Memorandum No. 3
Dated: July 10, 1985
15. Collection and Analysis of Specific ELINT Signal Parameters JPL D-2781 UAA-012

Formerly Technical Memorandum No. 1
Dated: June 23, 1985
16. IEW Sensor Error Budget for DF Fix Estimations

Technical Memorandum No. 4
Dated: August 14, 1985
17. Confidence Ellipse Research Software

JPL D-2786 UAA-015
Technical Memorandum No. 6
Dated: August 8, 1985
18. The Power of Statistical Tests - Software

JPL D-2788 UAA-017
Technical Memorandum No. 7
Dated: December 2, 1985
19. Collection and Analysis of Specific Elint

Signal Parameters: Final Report
JPL D-2787 UAA-016
Technical Memorandum No. 8
Dated: December 9, 1985
20. Intelligence/Electronic Warfare (IEW) Direction-Finding and Fix Estimation Analysis Report

Volume 2, TRAILBLAZER
JPL D-180, Vol. 2 UAA-001
Dated: December 20, 1985```


[^0]:    * $\pm$ one sigma about the average value of the LOBs will usually contain about $\mathbf{6 8 \%}$ of all the LOBs. $\pm 3$ sigma corresponds to about $99.7 \%$.

