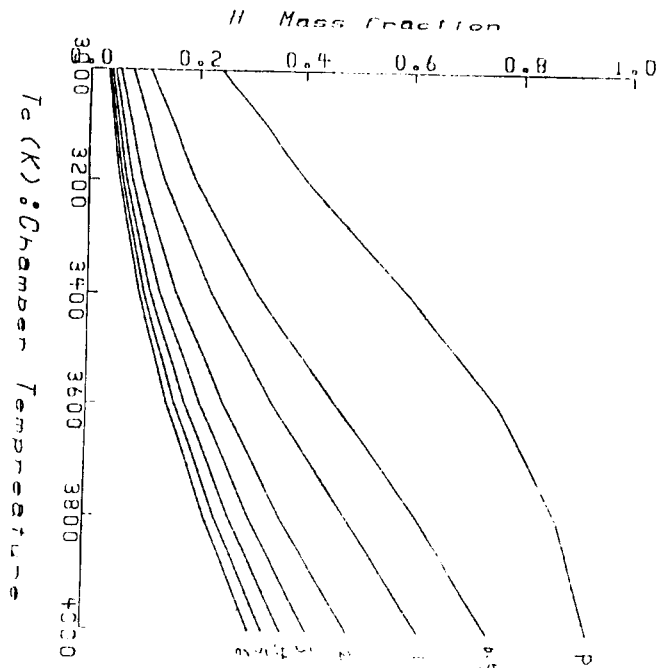


# COMPUTATIONAL FLUID DYNAMICS FOR NUCLEAR THERMAL PROPULSION

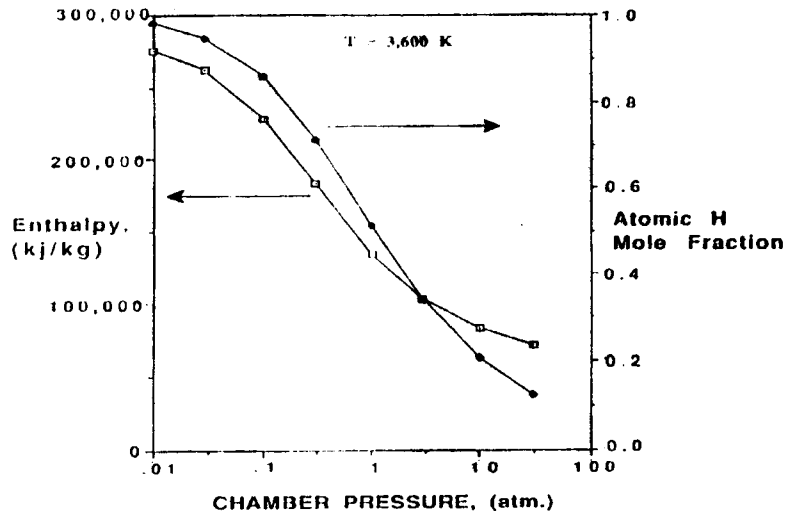
Presented to the  
Nuclear Propulsion Technical Interchange Meeting

October 21, 1992

Robert M. Stubbs  
Suk C. Kim



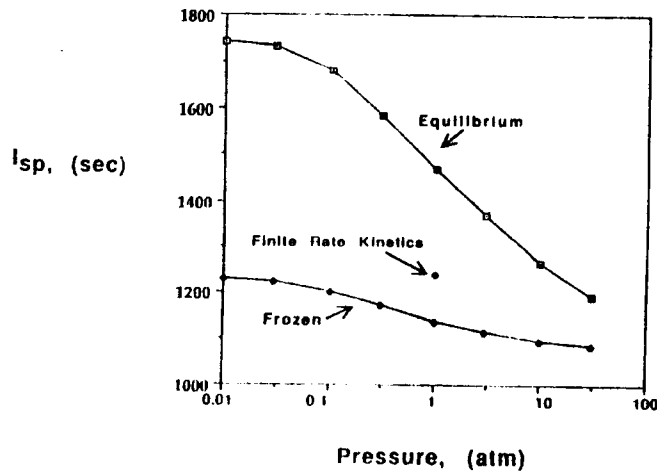
**SPECIFIC ENTHALPY OF HYDROGEN AND MOLE FRACTION OF H  
AS A FUNCTION OF CHAMBER PRESSURE  
AT A CHAMBER TEMPERATURE OF 3,600 K**



INTERNAL FLUID MECHANICS DIVISION

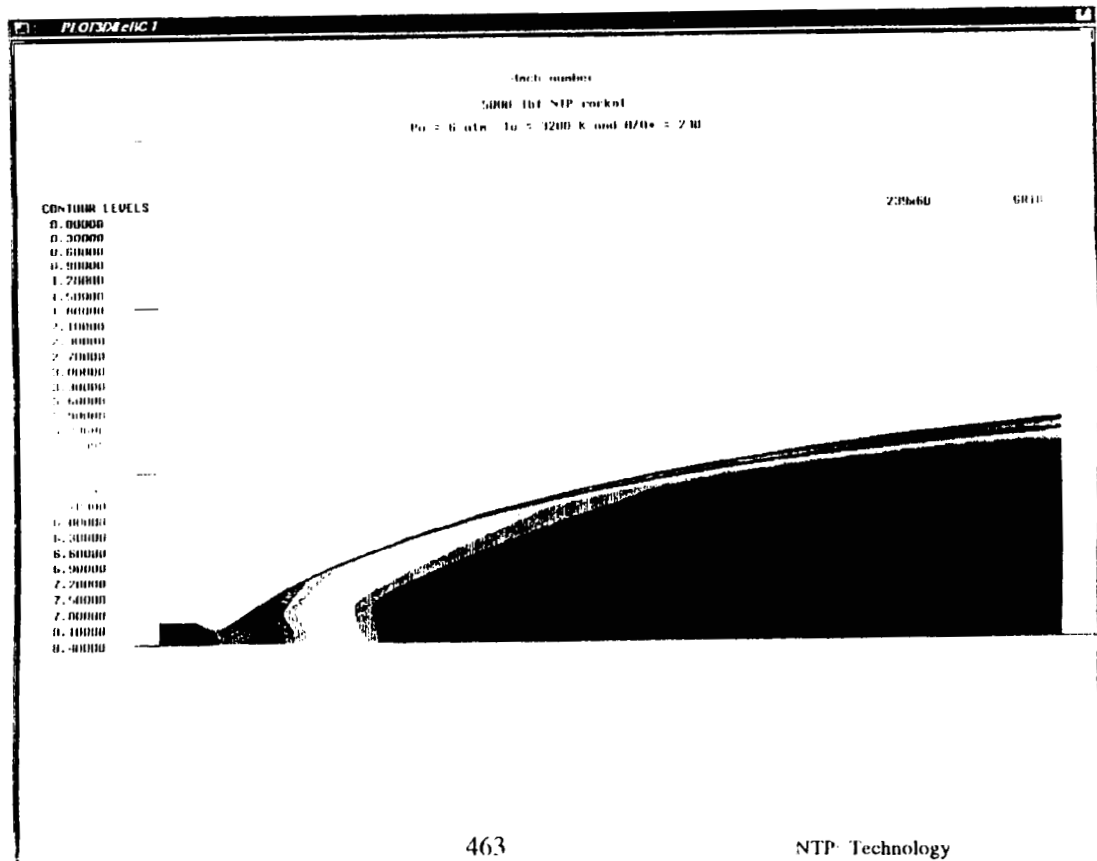
**SPECIFIC IMPULSE AS A FUNCTION OF CHAMBER PRESSURE**

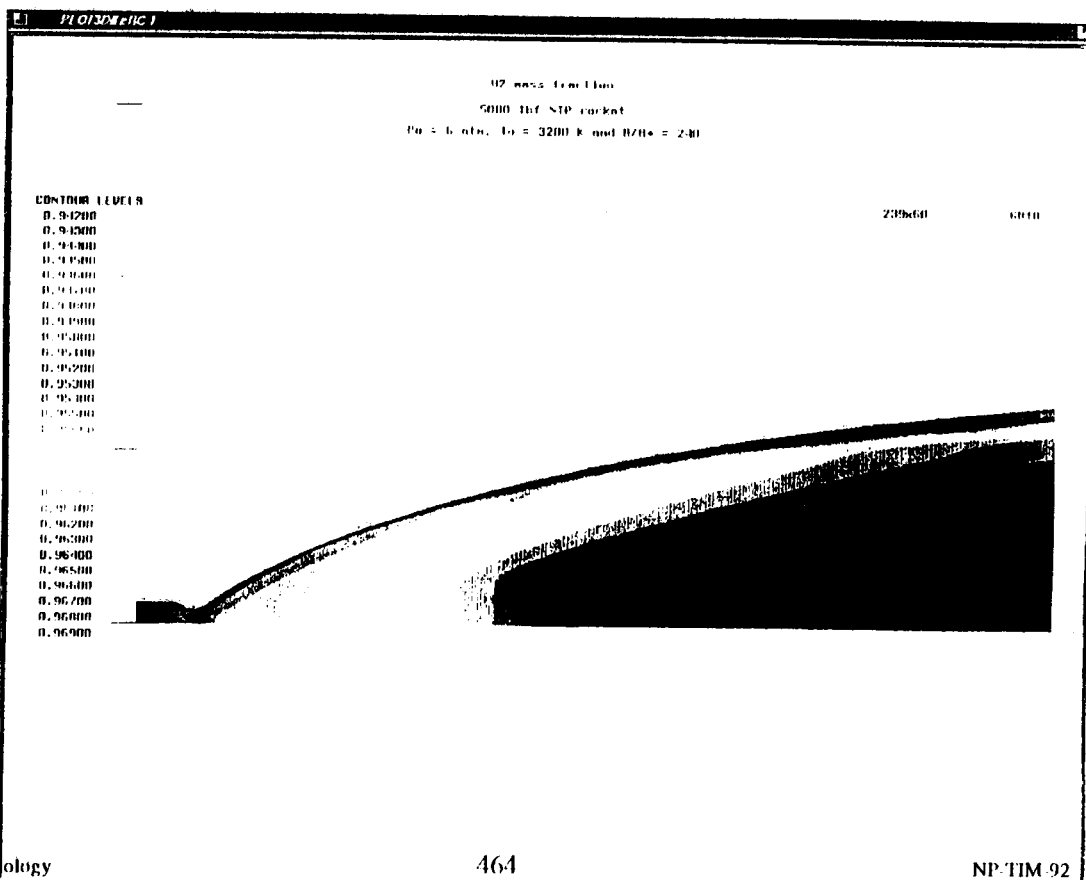
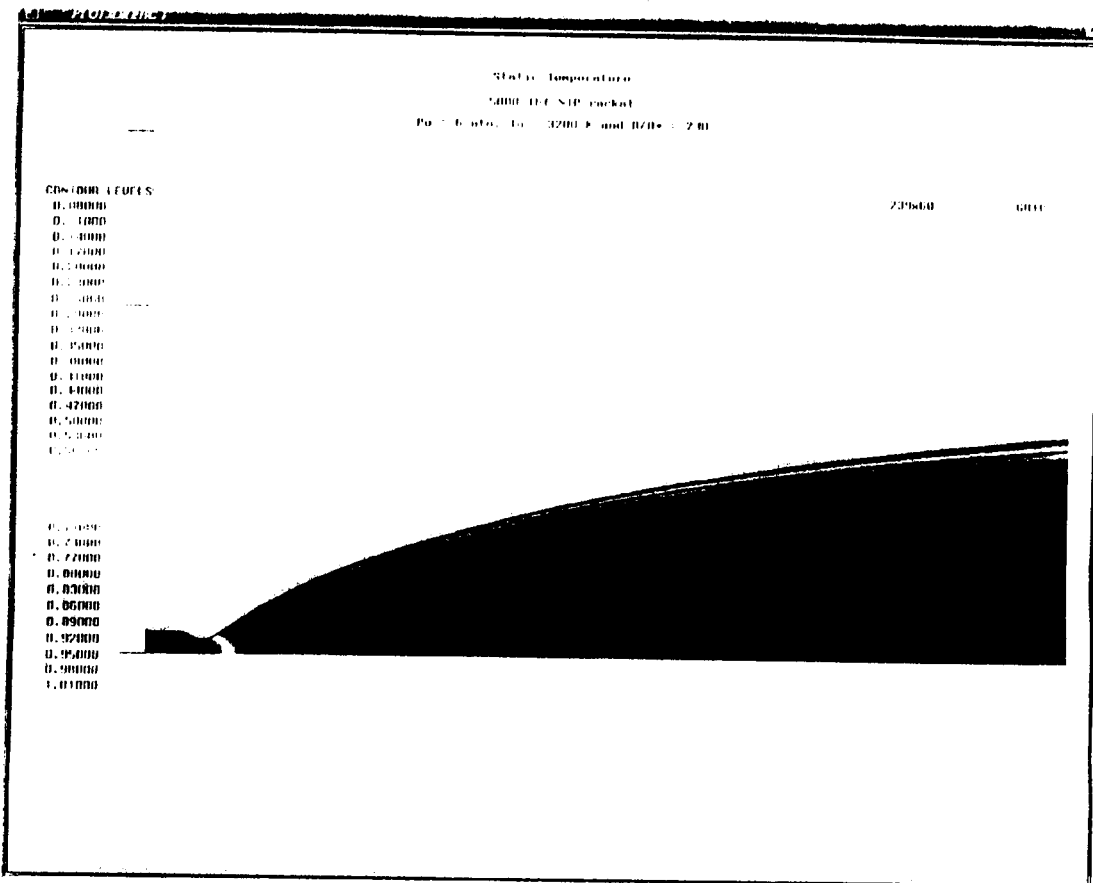
$T_c = 3,600 \text{ K}$



## RPLUS

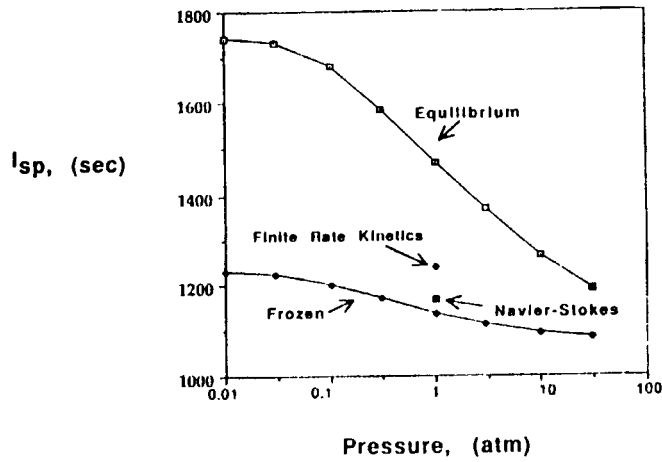
- DEVELOPED AT NASA-LEWIS
- A NAVIER-STOKES CODE WITH FINITE RATE CHEMICAL KINETICS CAPABILITY
  - LU-SSOR
  - 9 SPECIES, 18 REACTIONS, (H<sub>2</sub>, O<sub>2</sub> COMBUSTION SYSTEM)
  - 3-D, (ONLY 2-D AXISYMMETRIC REQUIRED HERE)





SPECIFIC IMPULSE AS A FUNCTION OF CHAMBER PRESSURE

$T_C = 3,600 \text{ K}$



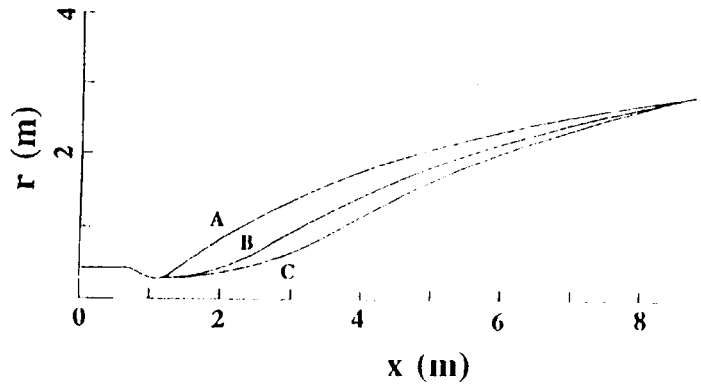
NASA

LEWIS RESEARCH CENTER

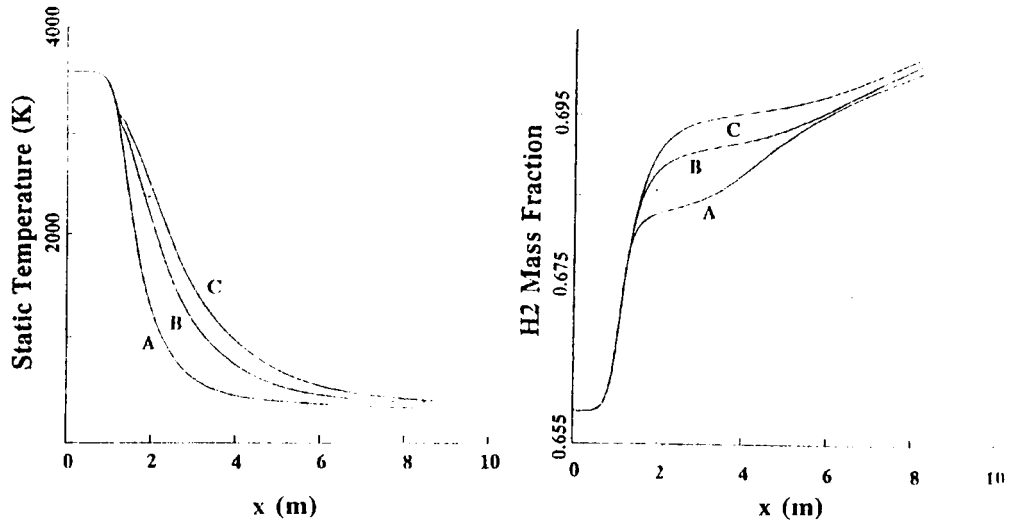
WALL CONFIGURATIONS OF NOZZLES "A", "B", AND "C"

ALL HAVE:

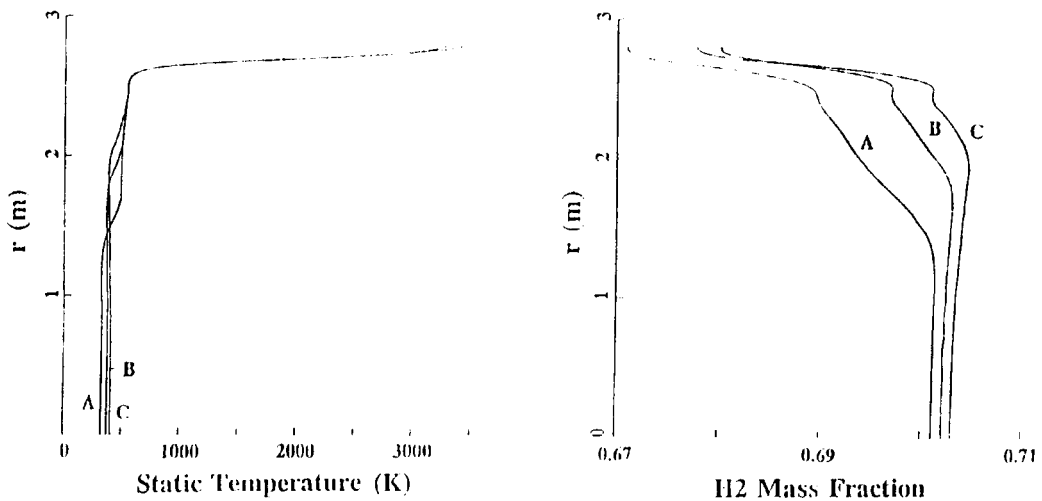
- $R_{\text{THROAT}} = 0.28 \text{ m}$
- $A_E/A_T = 100$
- THROAT TO EXIT LENGTH = 7.6 m

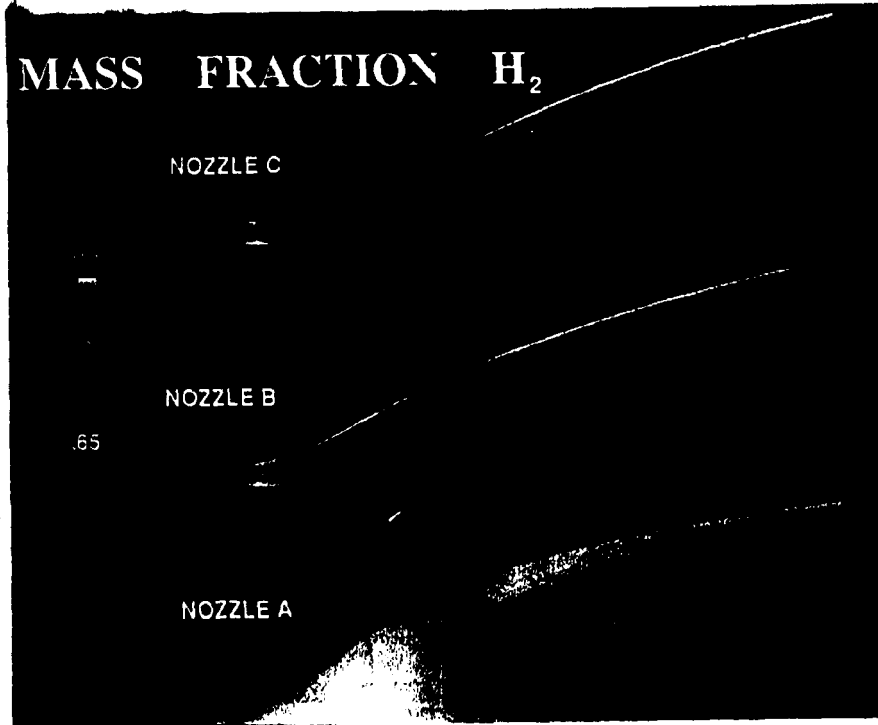


### Axial Distributions on the Centerlines



### Radial Distributions at the Exit





National Aeronautics and  
Space Administration  
  
Lewis Research Center

NASA

TABLE 4. Specific Impulse of NTP  
Nozzles which have been scaled  
to produce, at each Temperature,  
approximately equal Thrust.

$T_c$ , (K)	Isp, (lb <sub>f</sub> -s/lb <sub>m</sub> )		
	$P_c=10$ atm $r_t=0.28$ m	$P_c=1.0$ atm $r_t=0.8854$ m	$P_c=0.1$ atm $r_t=2.8$ m
2700	901.61	899.48	903.14
3200	1024.33	1037.21	1072.47
3600	1144.22	1183.39	1223.17

TABLE 5. Specific Impulse for variously sized NTP Nozzles with  $T_c=3600$  K,  $P_c=1.0$  atm.

Isp, (lb <sub>f</sub> -s/lb <sub>m</sub> )		
$r_t=0.28$ m	$r_t=0.8854$	$r_t=2.8$ m
1151.57	1183.39	1220.41

#### SUMMARY

- CFD SIMULATIONS PREDICT LOWER SPECIFIC IMPULSE VALUES FOR THE LOW PRESSURE NUCLEAR THERMAL ROCKET THAN ONE-DIMENSIONAL, INVISCID ANALYSES.
- THE LOW PRESSURE CONCEPT SHOWS MORE PROMISE AT HIGHER TEMPERATURES THAN AT LOWER TEMPERATURES, BECAUSE OF THE GREATER AMOUNT OF DISSOCIATION.
- SMALLER NOZZLES SHOW LARGER VISCOUS LOSSES, ESPECIALLY AT LOW PRESSURES; THEREFORE, PERFORMANCE GAINS ARE ASSOCIATED WITH LARGER NOZZLES.
- ADVANCED CFD CODES SUCH AS RPLUS (3D, NAVIER-STOKES, CHEMICAL KINETICS), WITH THEIR ABILITY TO SIMULATE REAL GAS EFFECTS, PROVIDE THE DESIGNER WITH POWERFUL TOOLS TO ANALYZE THE ENTIRE FLOW FIELD AND CALCULATE GLOBAL PERFORMANCE VALUES.