

STEADY POTENTIAL SOLVER FOR UNSTEADY AERODYNAMIC ANALYSES

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Presentation Outline

- Description of flow solver, SFLOW
- Subsonic Calculations (Steady & Unsteady)
 - Compressor Cascade (10th Standard Configuration)
 - Turbine Cascade (4th Standard Configuration)
 - GE Low Speed Research Compressor
 - GE Low Speed Research Turbine
- Transonic Calculations (Steady)
 - Compressor Cascade (10th Standard Configuration)

Objective

Develop steady flow solver for use with LINFLO

- Compatible with LINFLO
- Composite Mesh
- Transonic Capability

Approach

- Steady flow potential equation written in nonconservative form
- Newton's Method
- Implicit, Least-Squares, Interpolation Method used to obtain finite difference expressions
- Matrix inversion routines from LINFLO

Differential Equations

Steady Flow

$$\begin{aligned} A^2 \nabla^2 \phi - (\gamma - 1) \nabla^2 \Phi \frac{\bar{D}\phi}{Dt} - \frac{\bar{D}^2 \phi}{Dt^2} - \nabla \phi \cdot \frac{\nabla(\nabla \Phi)^2}{2} \\ = -A^2 \nabla^2 \Phi + \nabla \Phi \cdot \frac{\nabla(\nabla \Phi)^2}{2} \end{aligned}$$

$$\frac{\bar{D}}{Dt} = \nabla \Phi \cdot \nabla$$

Unsteady Flow

$$A^2 \nabla^2 \phi - (\gamma - 1) \nabla^2 \Phi \frac{\bar{D}\phi}{Dt} - \frac{\bar{D}^2 \phi}{Dt^2} - \nabla \phi \cdot \frac{\nabla(\nabla \Phi)^2}{2} = 0$$

$$\frac{\bar{D}}{Dt} = i\omega + \nabla \Phi \cdot \nabla$$

Newton' Method

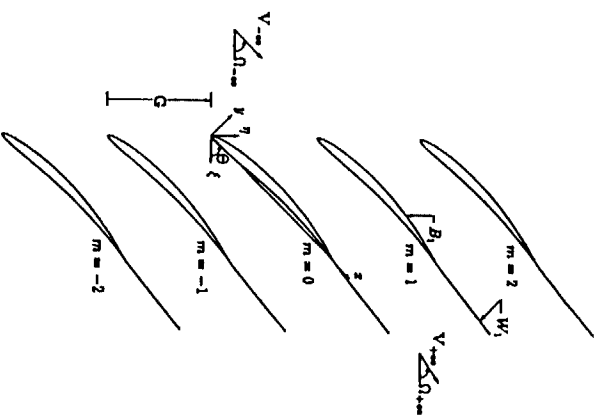
$$[A(\Phi)] \{\phi\} = \{b(\Phi)\}$$

$$\Phi(\bar{x})^{n+1} = \Phi(\bar{x})^n + \phi(\bar{x})^n$$

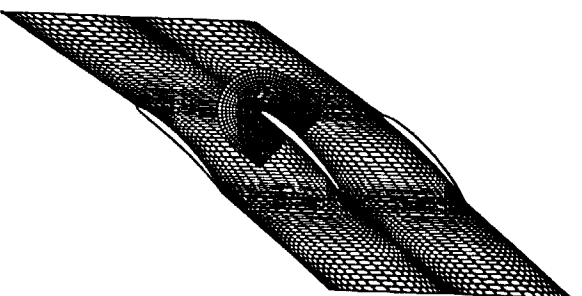
Convergence Criterion

$$|\phi(\bar{x})^n| < \epsilon$$

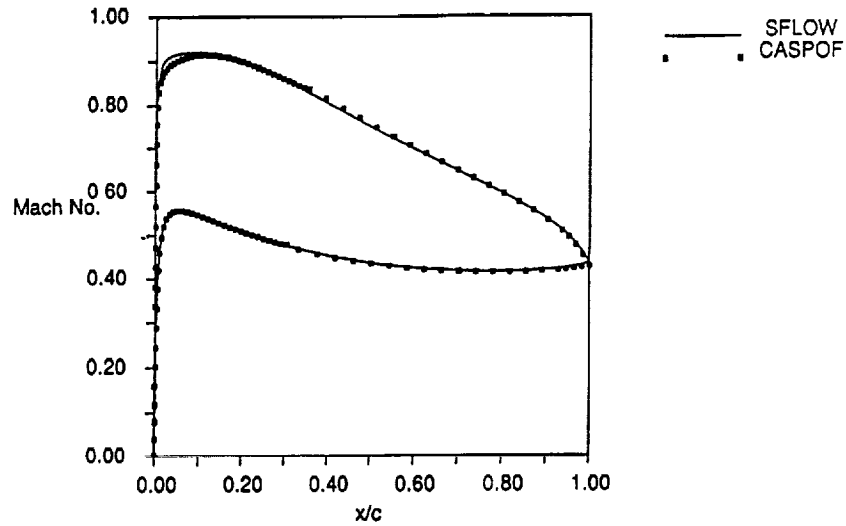
Cascade Geometry



Composite Mesh

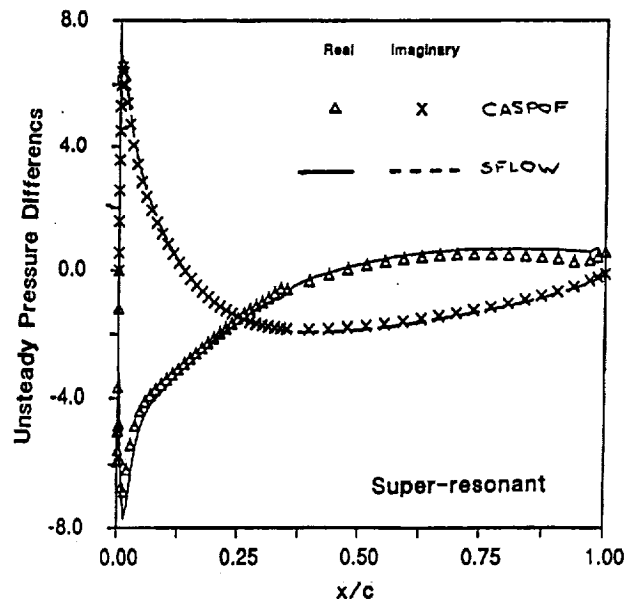


10th Standard Configuration, Subsonic Flow Conditions
 Steady Mach Number Distribution
 $M_{\infty} = 0.7, \Omega_{\infty} = 55 \text{ deg}$



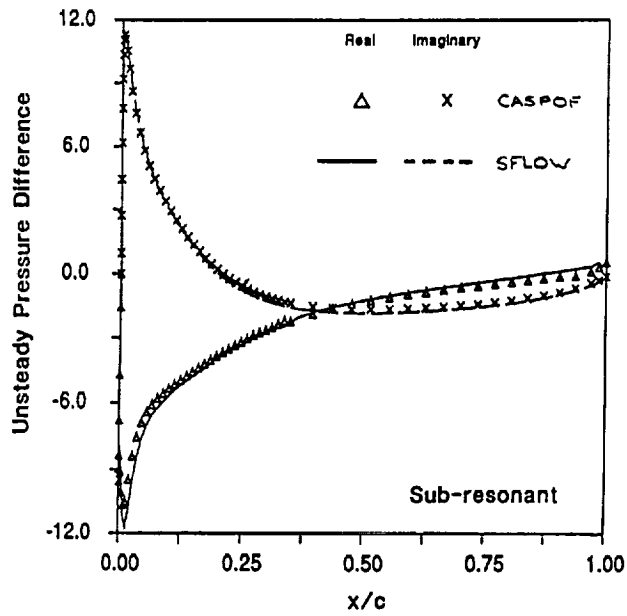
10th Standard Configuration, Subsonic Flow Conditions
 Unsteady Torsion Mode Response

$\alpha = 1.0, \omega = 0.24, \sigma = 30 \text{ deg}$

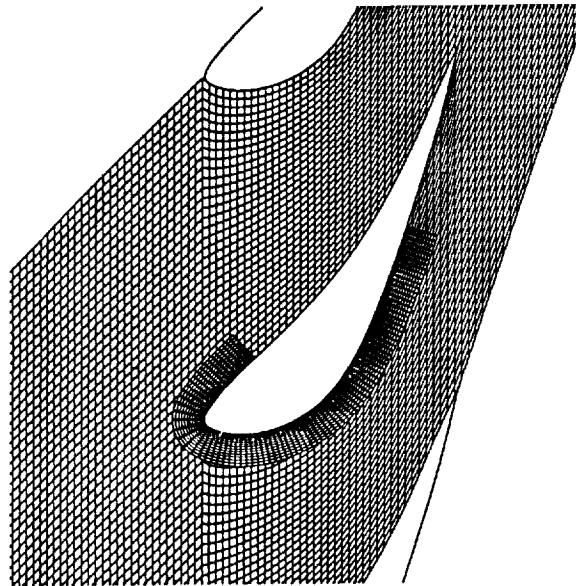


10th Standard Configuration, Subsonic Flow Conditions Unsteady Torsion Mode Response

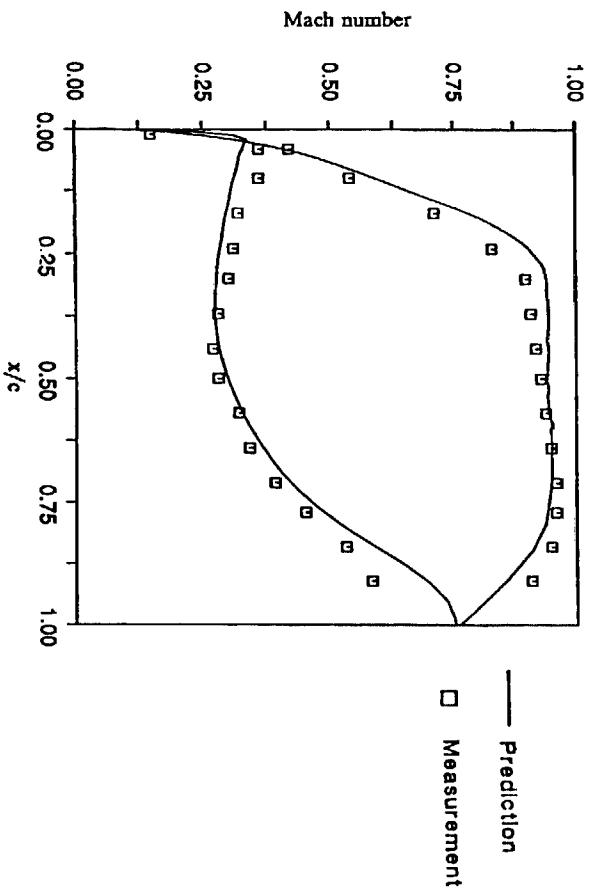
$\alpha = 1.0, \quad \omega = 0.24 \quad \sigma = 180 \text{ deg}$



Standard Configuration Number 4 Turbine Cascade Composite Mesh

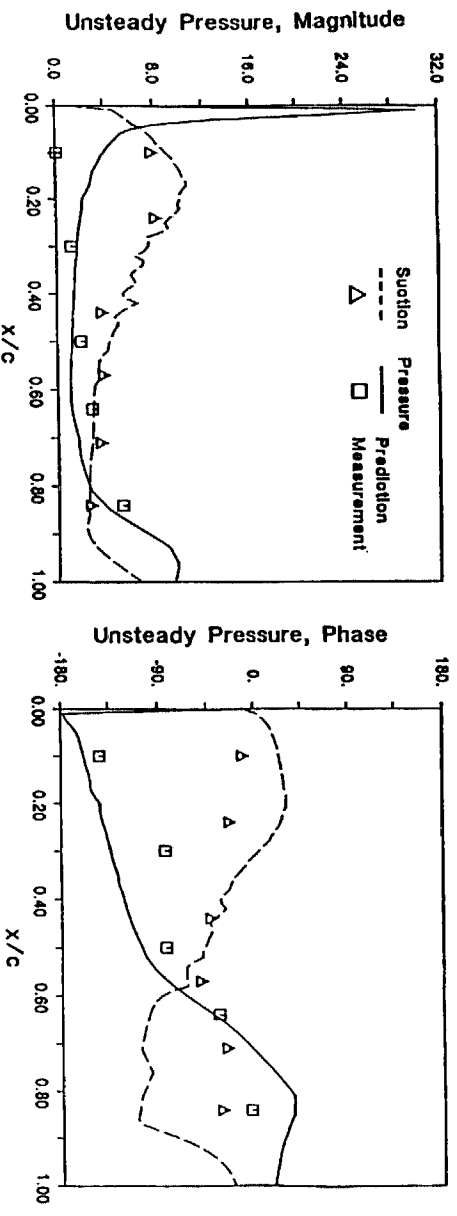


Standard Configuration Number 4 Steady Surface Mach Number Distribution



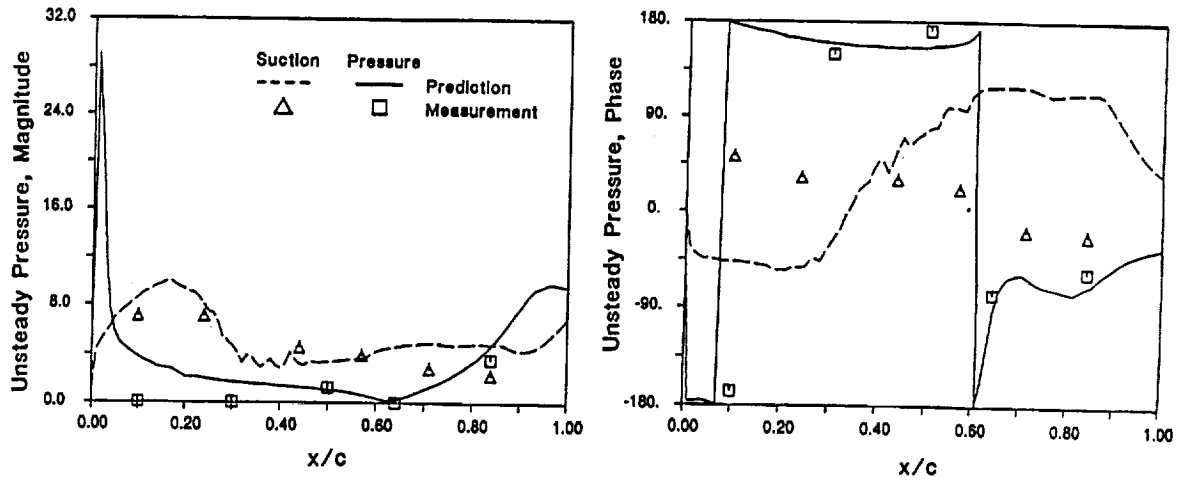
Standard Configuration Number 4 Unsteady Aerodynamic Response

$h = (0.0016, 0.0029)$, $\omega = 0.24$, $\sigma = -90$ Deg

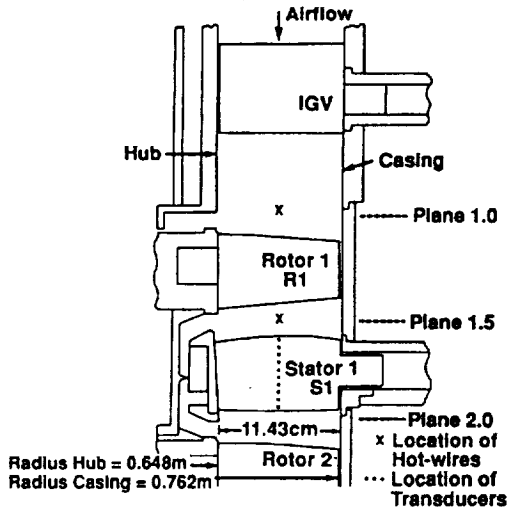


Standard Configuration Number 4 Unsteady Aerodynamic Response

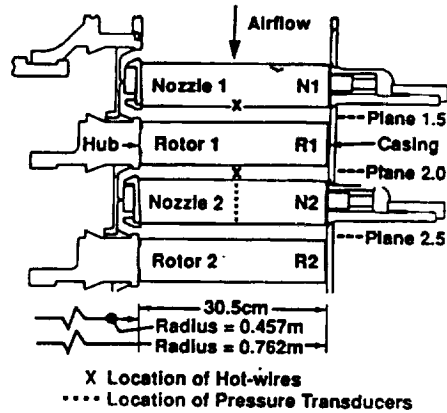
$h = (0.0016, 0.0029)$, $\omega = 0.24$, $\sigma = 90$ Deg



GE Low Speed Research Compressor & Turbine Configurations

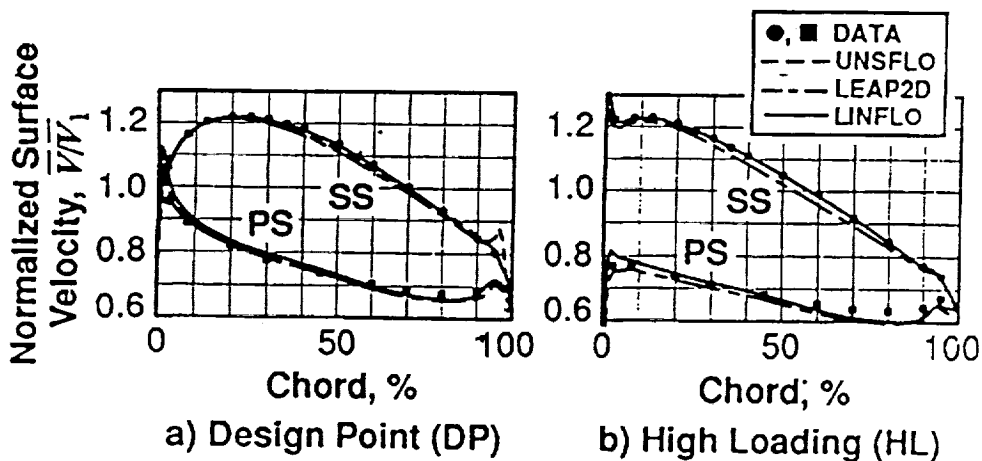


Compressor Test Rig

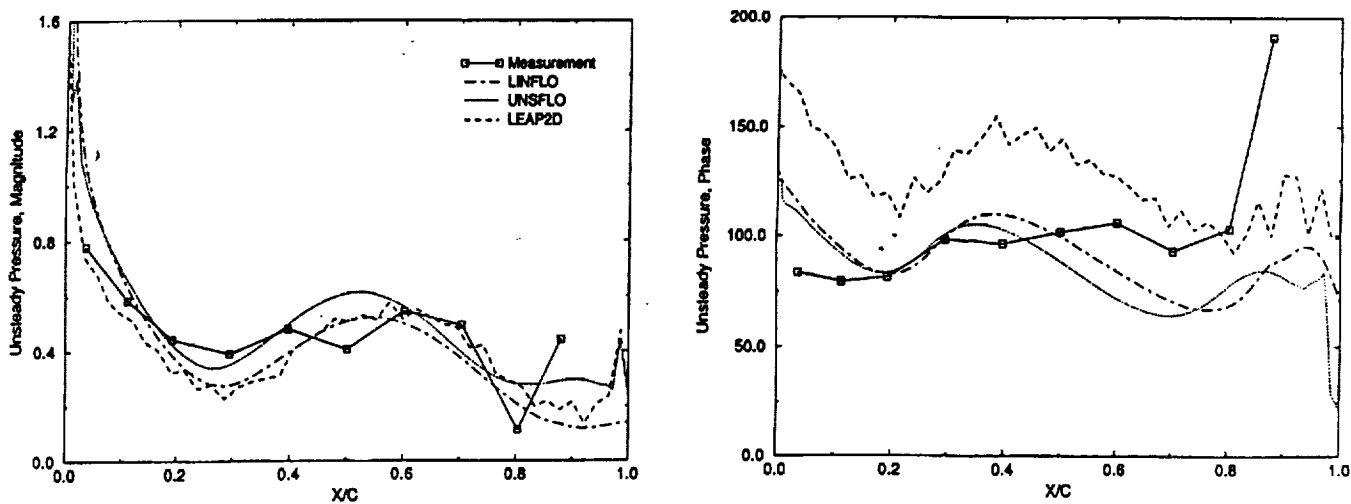


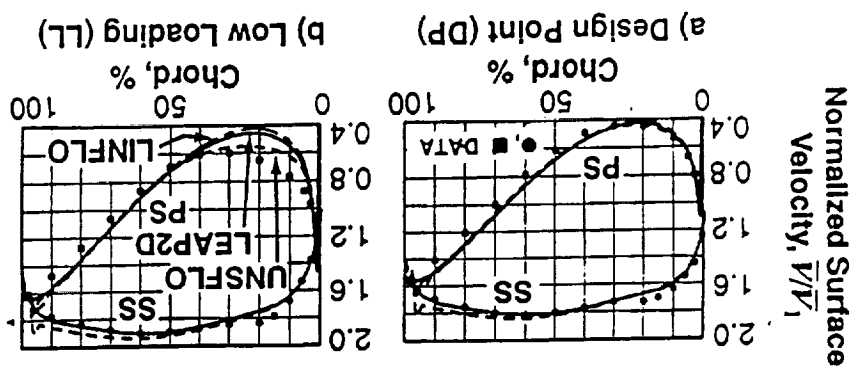
Turbine Test Rig

GE Low Speed Research Compressor Steady Blade Loading

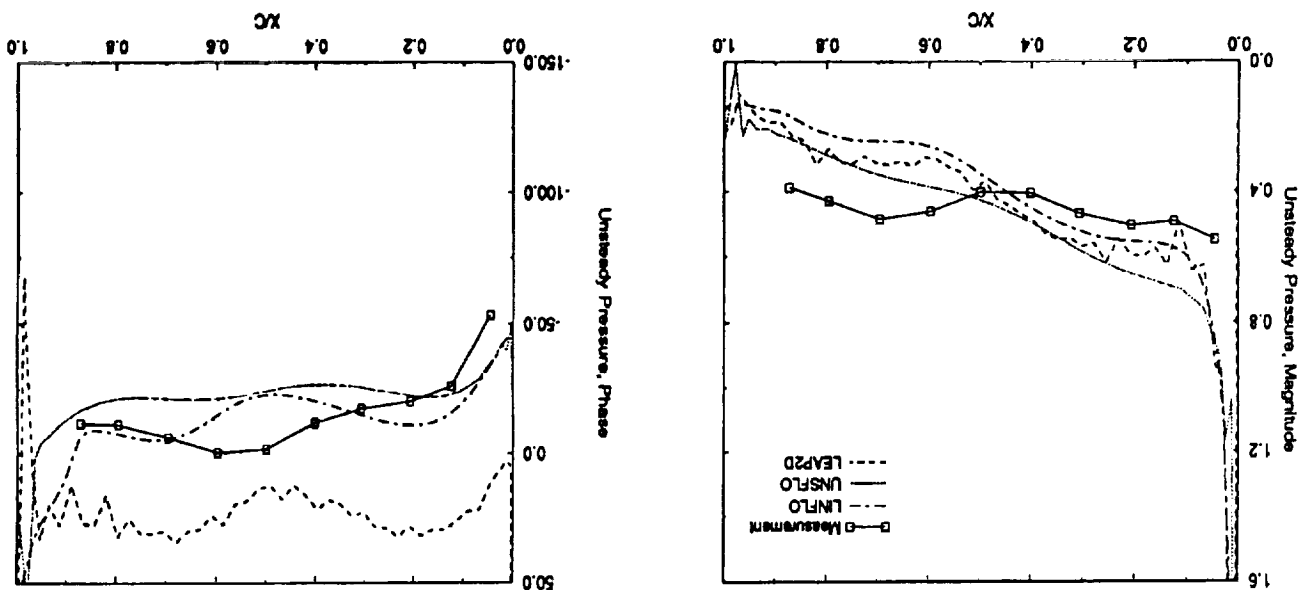


GE Low Speed Research Compressor Design Point, Suction Surface



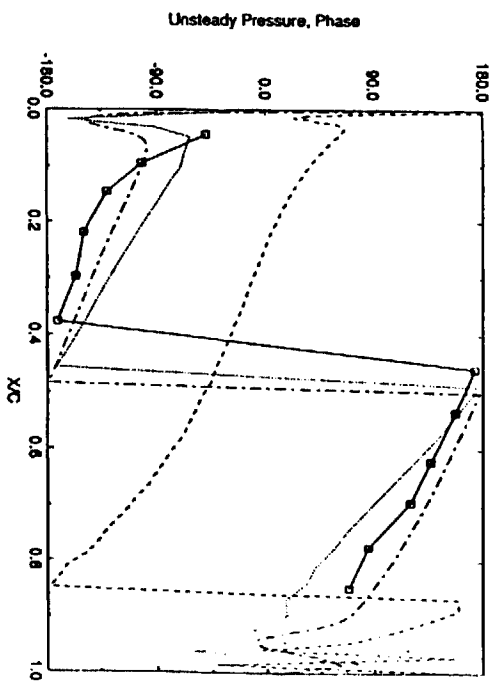
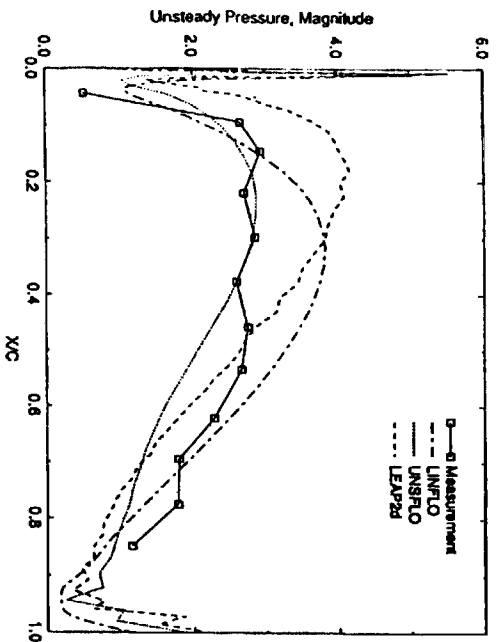


GE Low Speed Research Turbine
Steady Blade Loading

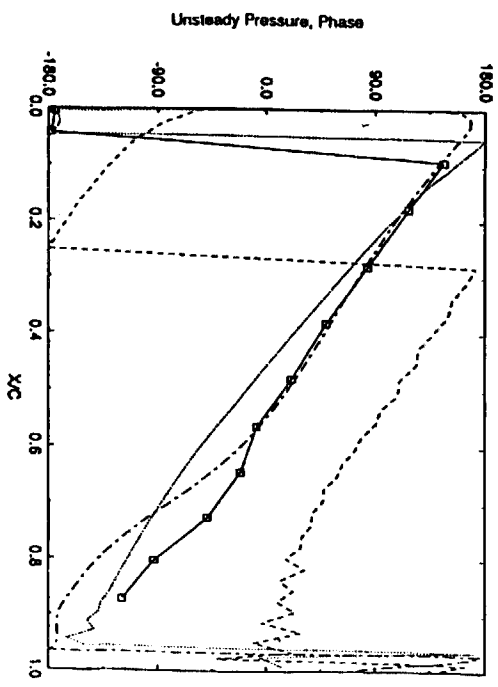
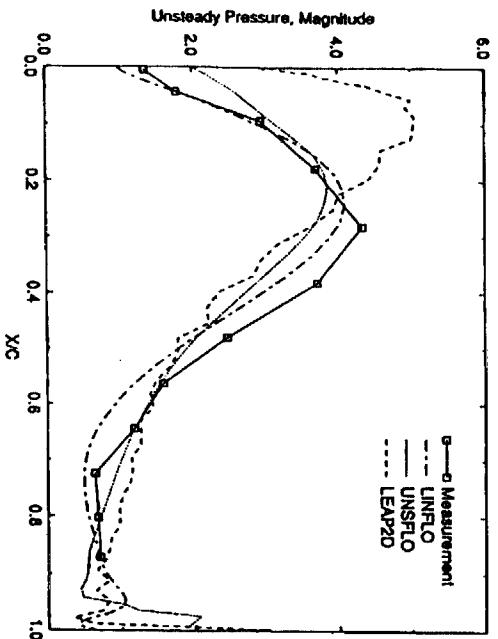


GE Low Speed Research Compressor
Design Point, Pressure Surface

GE Low Speed Research Turbine Design Point, Pressure Surface



GE Low Speed Research Turbine Design Point, Suction Surface



Transonic Flow Calculations

- Artificial viscosity added using rotated difference scheme of Jameson
- Dissipation coefficient based on local Mach number
- Modified Newton's method used to solve resulting equations

Modified Newton' Method for Transonic Flow Calculations

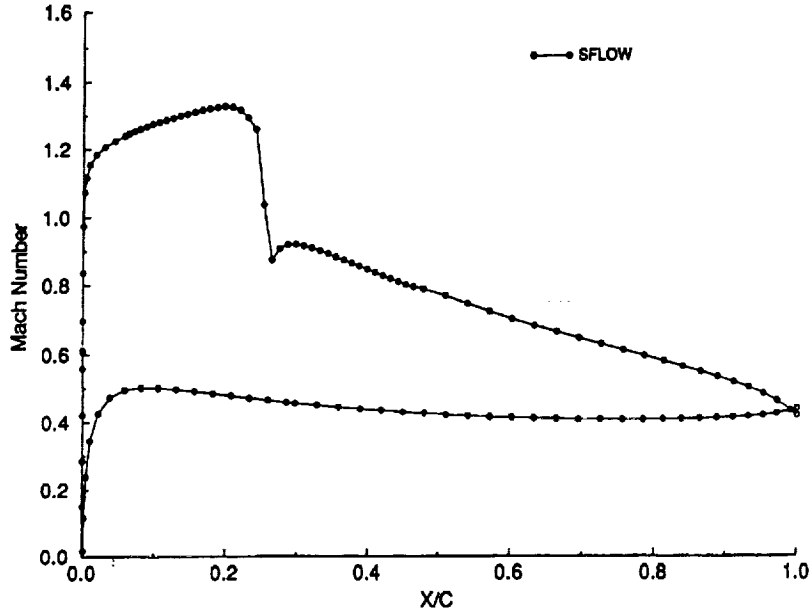
$$[A(\Phi)] \{\phi\} = \{b(\Phi)\}$$

$$\Phi(\bar{x})^{n+1} = \Phi(\bar{x})^n + \omega \phi(\bar{x})^n$$

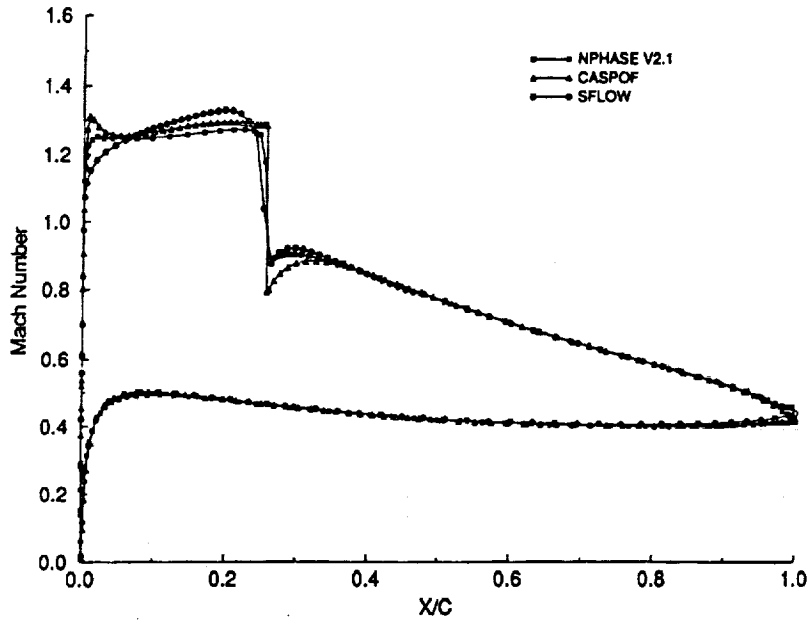
Convergence Criterion

$$|\phi(\bar{x})^n| < \varepsilon$$

10th Standard Configuration, Transonic Flow Conditions
 $M_\infty = 0.8$, $\Omega_\infty = 58$ deg.



10th Standard Configuration, Transonic Flow Conditions
Comparison with NPHASE & CASPOF Results
 $M_\infty = 0.8$, $\Omega_\infty = 58$ deg.



Summary

- 10th standard configuration predictions show good agreement with other flow solvers
- 4th standard configuration turbine predictions show good agreement with the magnitude of measured data, however there are some problems with phase near trailing edge on suction surface
- GE low speed research compressor and turbine predictions show reasonable agreement with magnitude and phase measurements
- Transonic solution progressing, needs better model for artificial viscosity near shock, and mesh clustering capability

