

**WORKSHOP FOR CFD APPLICATIONS IN ROCKET PROPULSION****APRIL 20-22, 1993**

1995 117018

**PHASE II HGM AIR FLOW TESTS IN SUPPORT OF HEX VANE INVESTIGATION**

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4380-1  
p. 12

Following the start of SSME certification testing for the Pratt & Whitney Alternate Turbopump Development (ATD) High Pressure Oxidizer Turbopump (HPOTP), cracking of the leading edge of the inner HEX vane was experienced. The HEX vane, at the inlet of the oxidizer bowl in the Hot Gas Manifold (HGM), accepts the HPOTP turbine discharge flow and turns it toward the Gaseous Oxidizer Heat Exchanger (GOX HEX) coil. The cracking consistently initiated over a specific circumferential region of the hex vane, with other circumferential locations appearing with increased run time. Since cracking had not to date been seen with the baseline HPOTP, a fluid-structural interaction involving the ATD HPOTP turbine exit flowfield and the HEX inner vane was suspected.

As part of NASA contract NAS8-36801, Pratt & Whitney conducted air flow tests of the ATD HPOTP turbine turnaround duct flowpath in the MSFC Phase II HGM air flow model. These tests included HEX vane strain gages and additional fluctuating pressure gages in the turnaround duct and HEX vane flowpath area. Three-dimensional flow probe measurements at two stations downstream of the turbine simulator exit plane were also made. Modifications to the HPOTP turbine simulator investigated the effects on turbine exit flow profile and velocity components, with the objective of reproducing flow conditions calculated for the actual ATD HPOTP hardware. Testing was done at the MSFC SSME Dynamic Fluid Air Flow (Dual-Leg) Facility, at air supply pressures between 50 and 250 psia. Combinations of turbine exit Mach number and pressure level were run to investigate the effect of flow regime.

Information presented includes

- 1) Descriptions of turbine simulator modifications to produce the desired flow environment.
- 2) Types and locations for instrumentation added to the flow model for improved diagnostic capability.
- 3) Evaluation of the effect of changes to the turbine simulator flowpath on the turbine exit flow environment.
- 4) Comparison of the experimental turbine exit flow environment to the environment calculated for the ATD HPOTP.

**SSME ALTERNATE TURBOPUMP  
DEVELOPMENT PROGRAM**

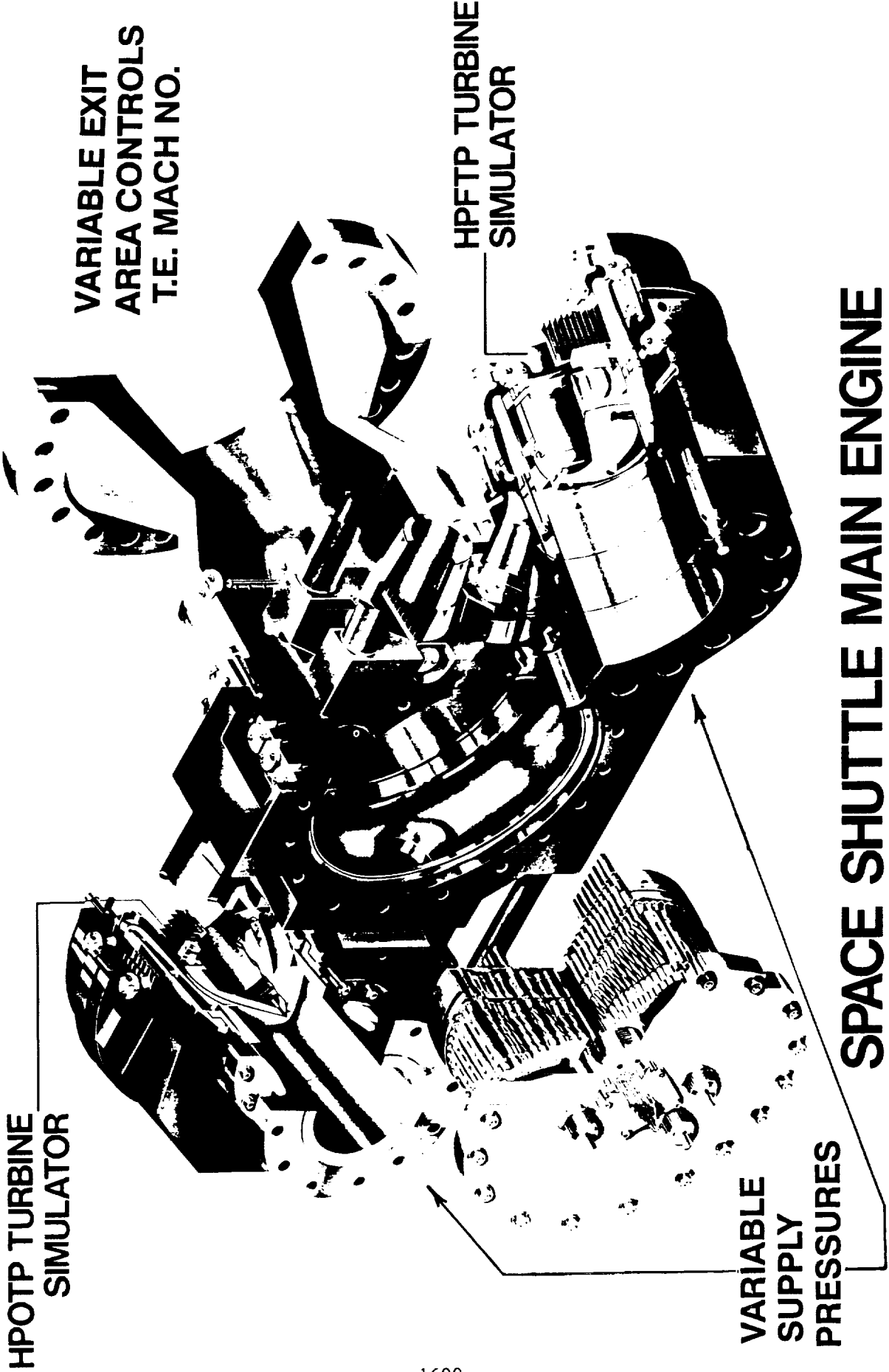
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**Marshall Space Flight Center  
April 20-22, 1993**

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West Palm Beach, Florida**

**HPOTP TURBINE  
SIMULATOR**



**VARIABLE EXIT  
AREA CONTROLS  
T.E. MACH NO.**

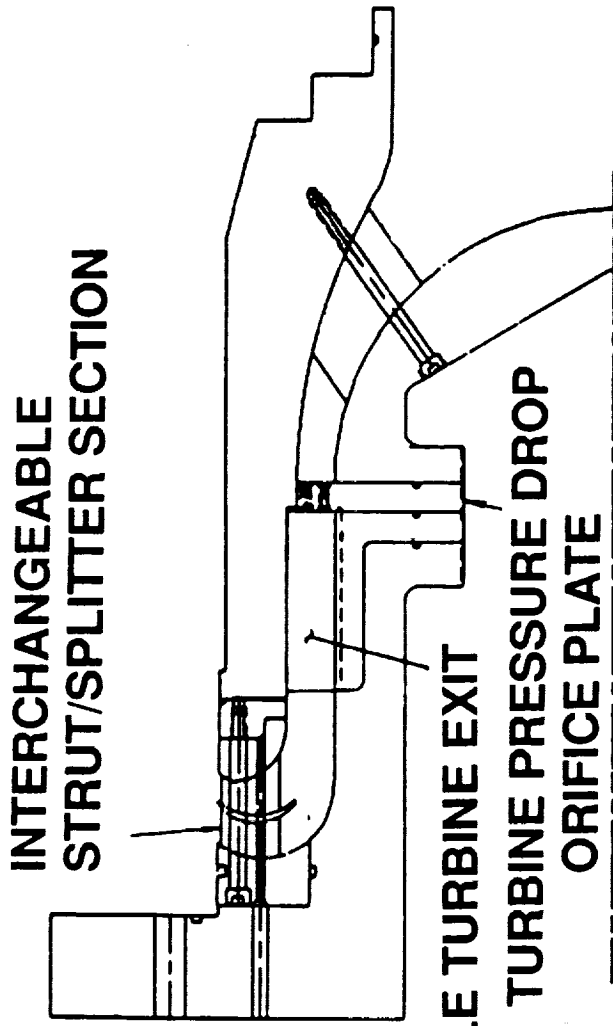
**HPFTP TURBINE  
SIMULATOR**

**VARIABLE  
SUPPLY  
PRESSURES**

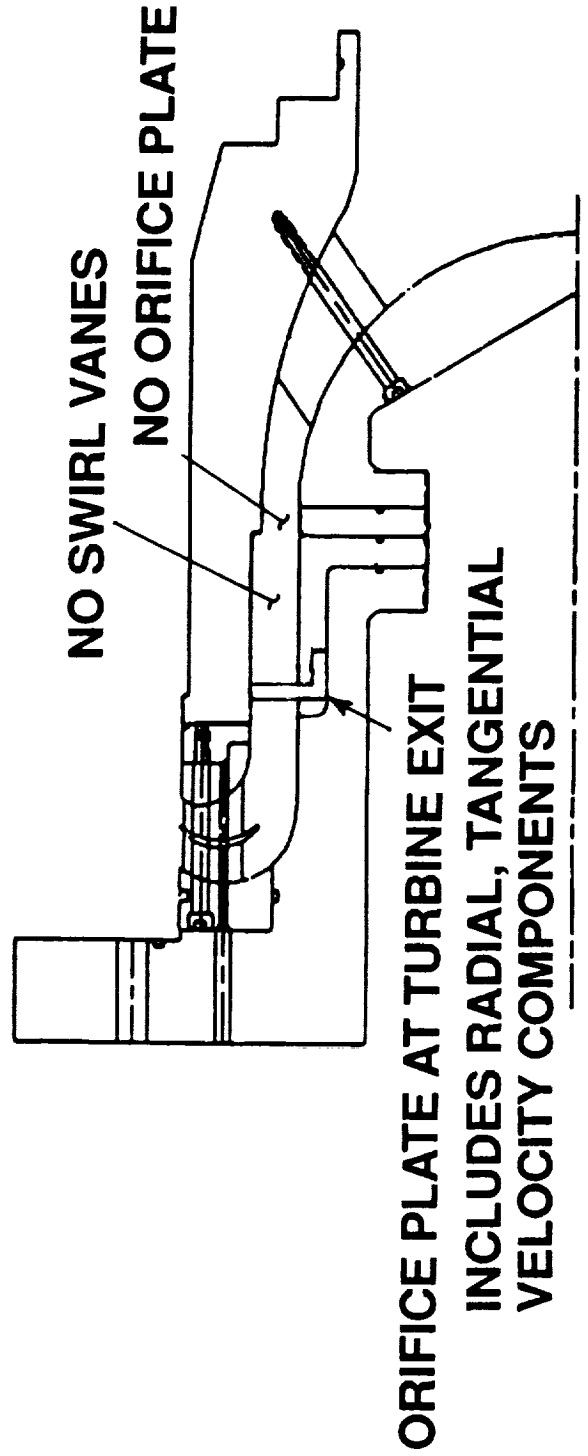
**SPACE SHUTTLE MAIN ENGINE  
EXPERIMENTAL AIR FLOW MODEL**

# TURBINE SIMULATOR/ORIFICE COMPARISON

## BASELINE



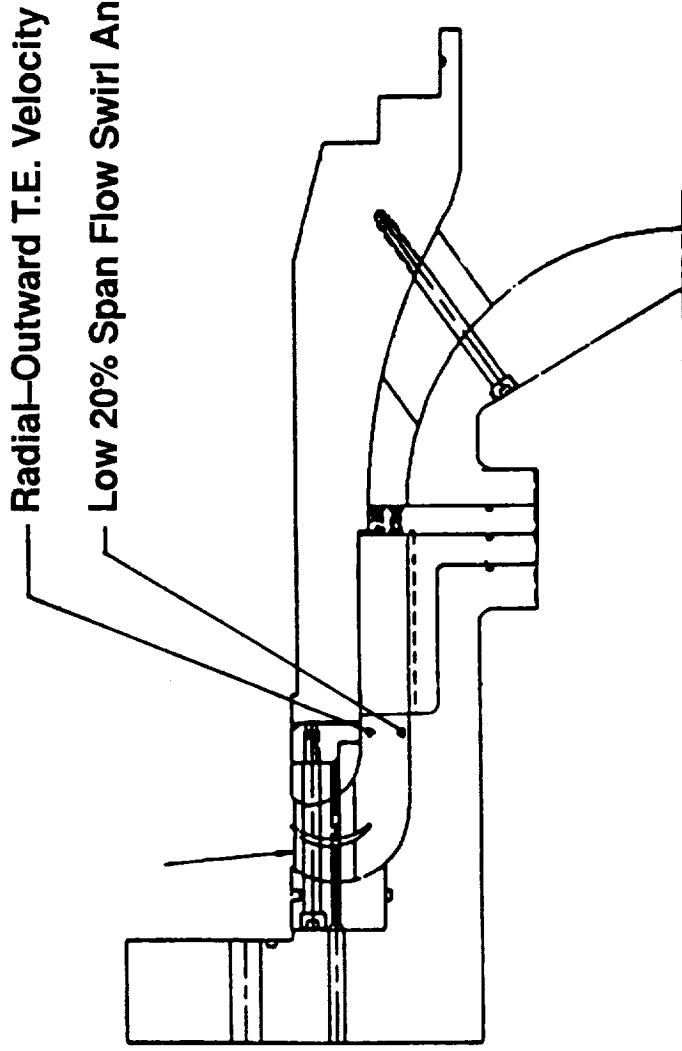
## MODIFIED



# FLOW MODEL/ENGINE FLOW CONDITION DIFFERENCES

*Model Tests Did Not Simulate Flow Of Final Turbine Design*

## ENGINE



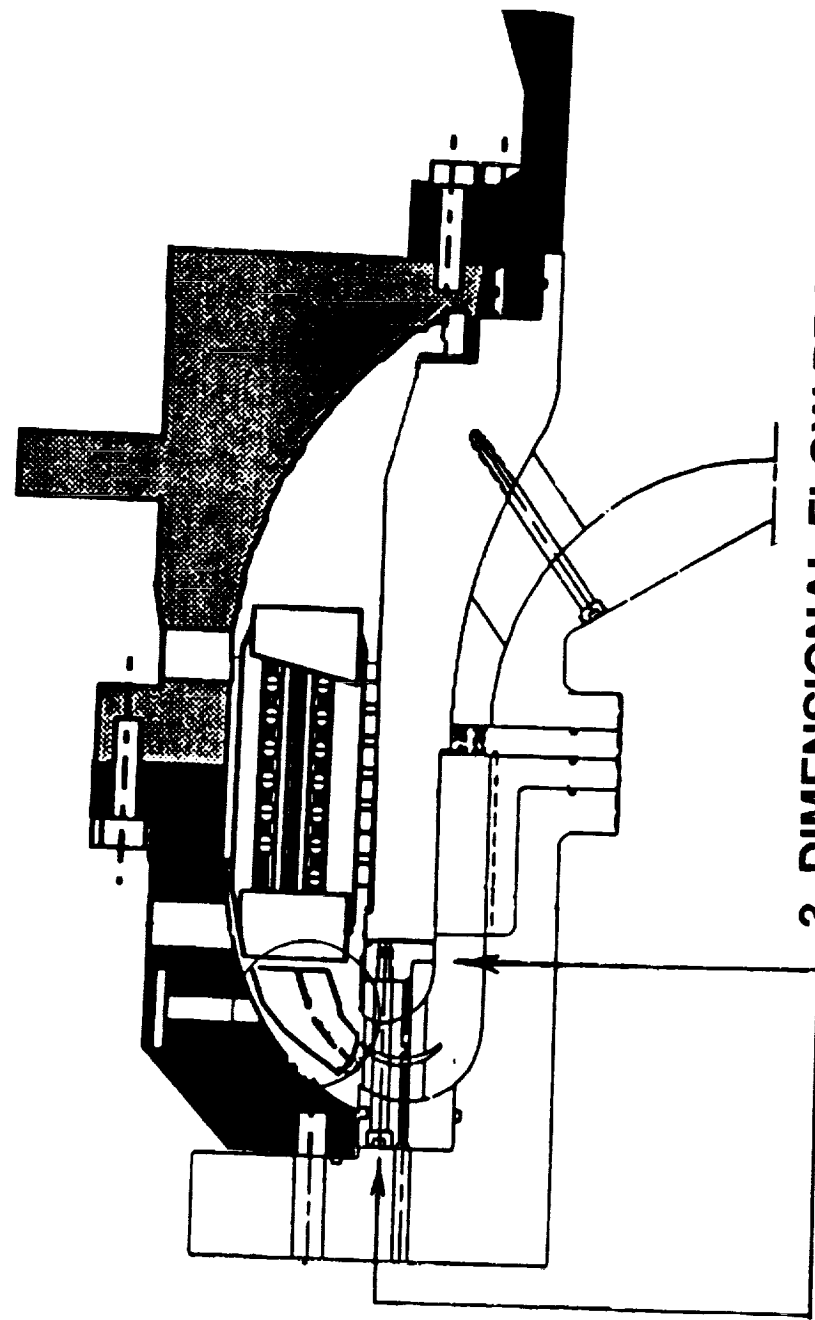
## FLOW MODEL

Radial Velocity Not Matched  
High 20% Span Flow Swirl Angle

# ADDITIONAL HPOTP/HGM INSTRUMENTATION

*Improve Definition Of Flow Environment, HEX Vane Response*

HEX VANE STRAIN GAGES  
FLUCTUATING PRESSURE TRANSDUCERS

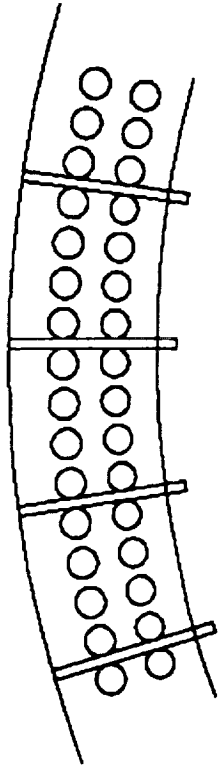


3-DIMENSIONAL FLOW PROBES

# VARIATIONS OF ORIGINAL ORIFICE PLATE

*Objective Was To Match ATD HPOTP Turbine Exit Flow Profile*

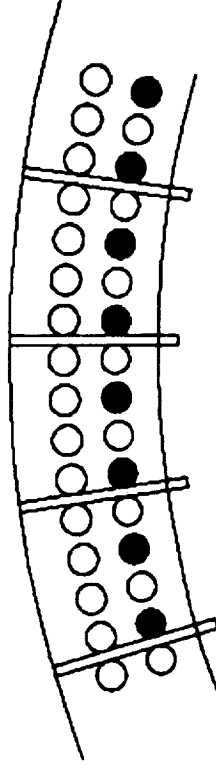
## ORIGINAL



17.7% POROSITY

AXIAL FLOW

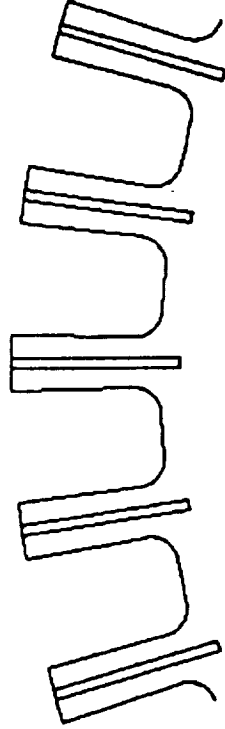
## 75% ORIGINAL



13.6% POROSITY

50% OF ID HOLES PLUGGED

## LARGE AREA



51.2% POROSITY

MATERIAL BETWEEN SWIRL  
VANES REMOVED

# AIR FLOW MODEL TEST CONDITION MATRIX

	Approx. Turbine Exit Mach Number									
	.04	.07	.10	.11	.13	.14	.15	.16		
50			O,L			L				O,L
100			O,L			L				O,L
150			O			L				O
200			O							
250	O	O	O,7	O	O	O,7	O	O	O,7	O

**O = Original Plate**

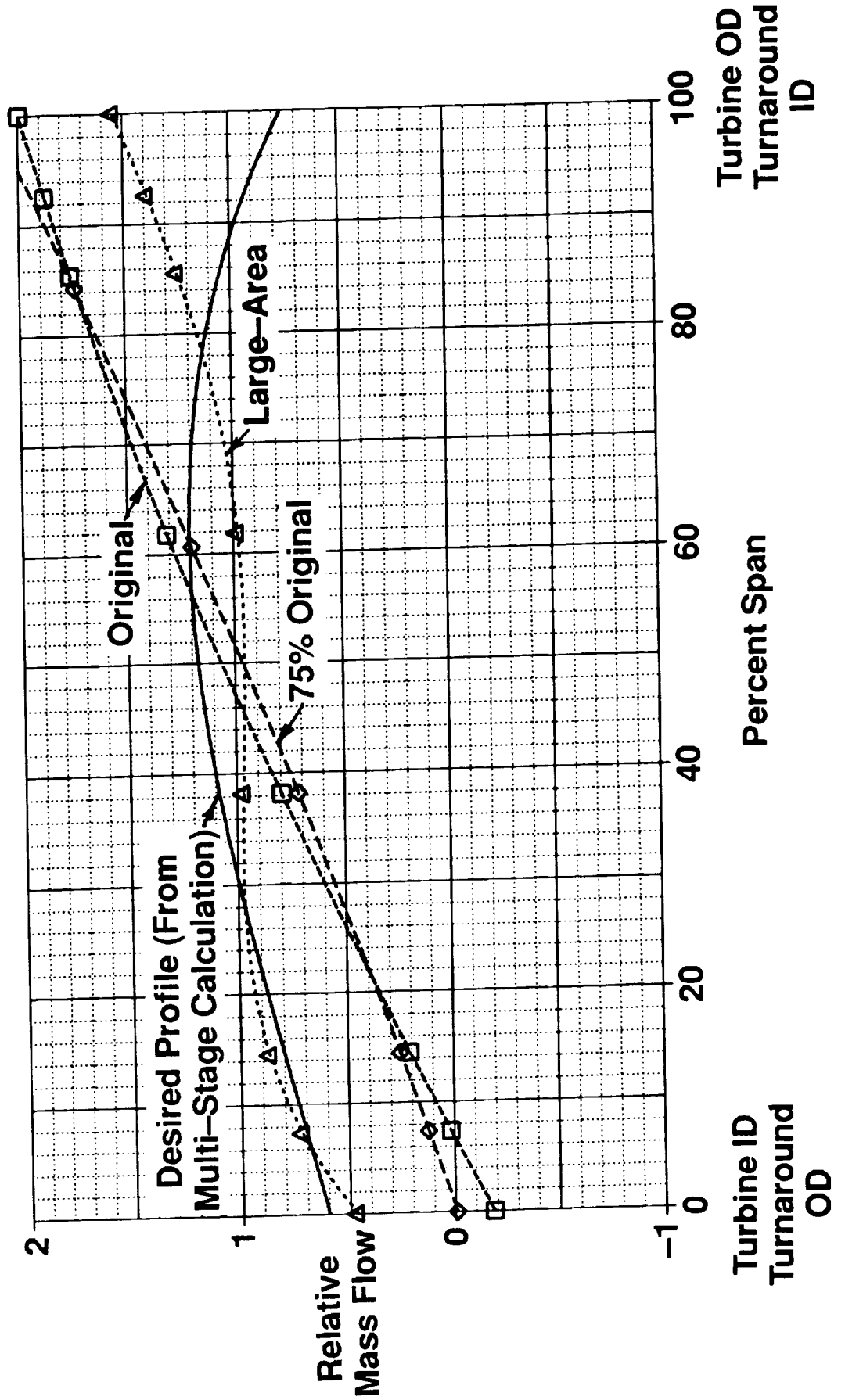
**7 = 75% Plate**

**L = Large-Area Plate**



# INITIAL ORIFICE PLATE REVISIONS RADIAL PROFILES

## Significant Variation in Mass Flow Profiles Obtained

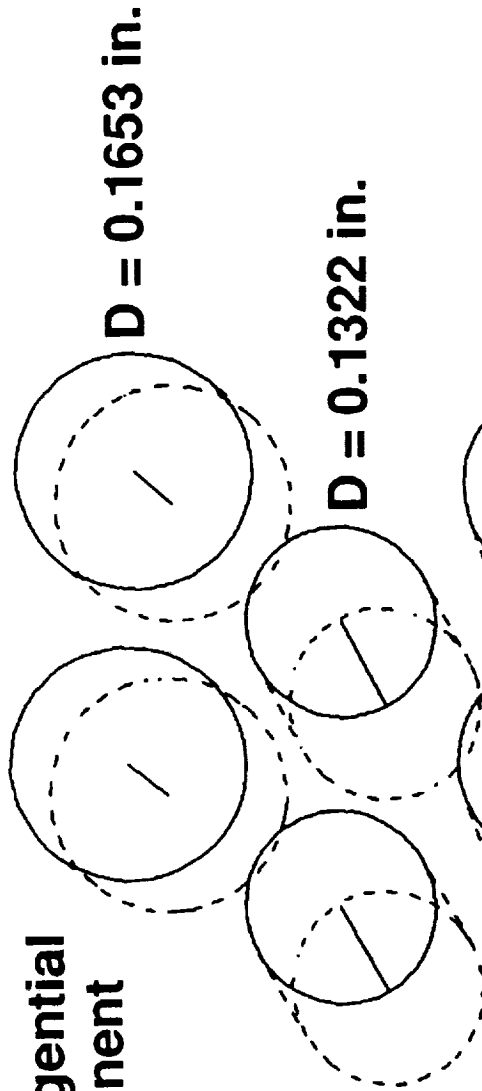


# NEW ORIFICE PLATE CONFIGURATION

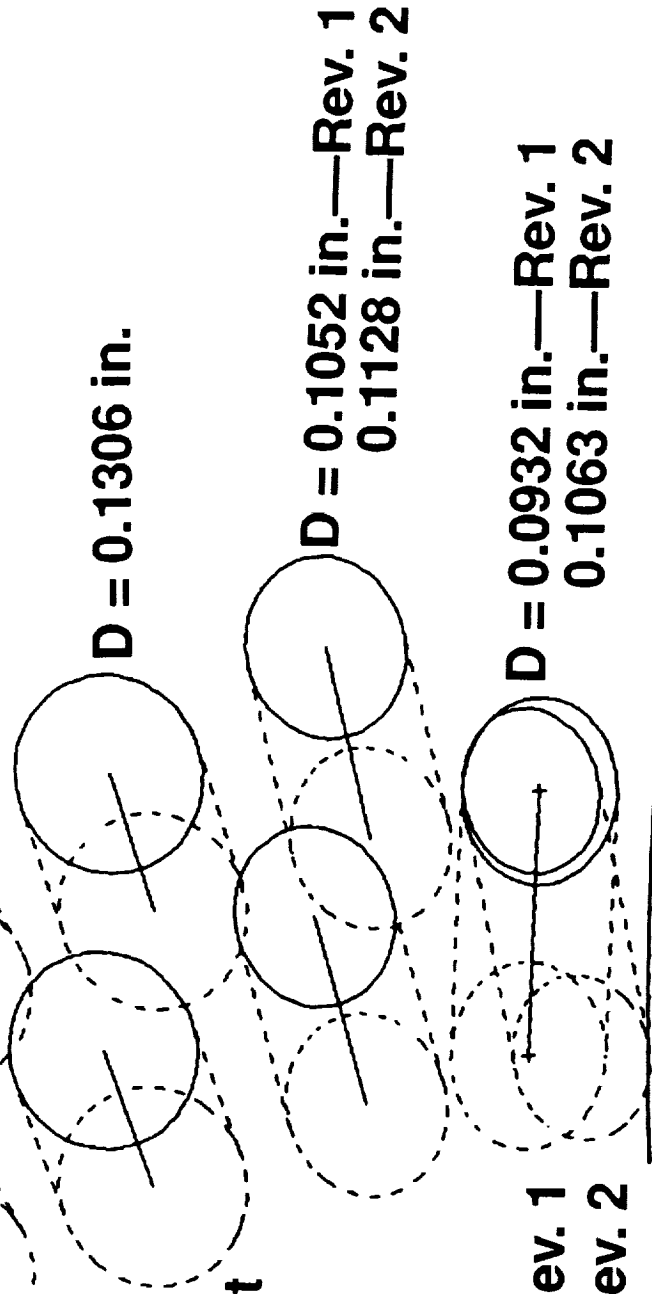
*To Match Turbine Exit Velocity Components And Mass Profile*

## VIEW LOOKING UPSTREAM

**Decreasing Tangential  
Velocity Component  
Toward OD**



**Increasing Radial  
Velocity Component  
Toward OD**

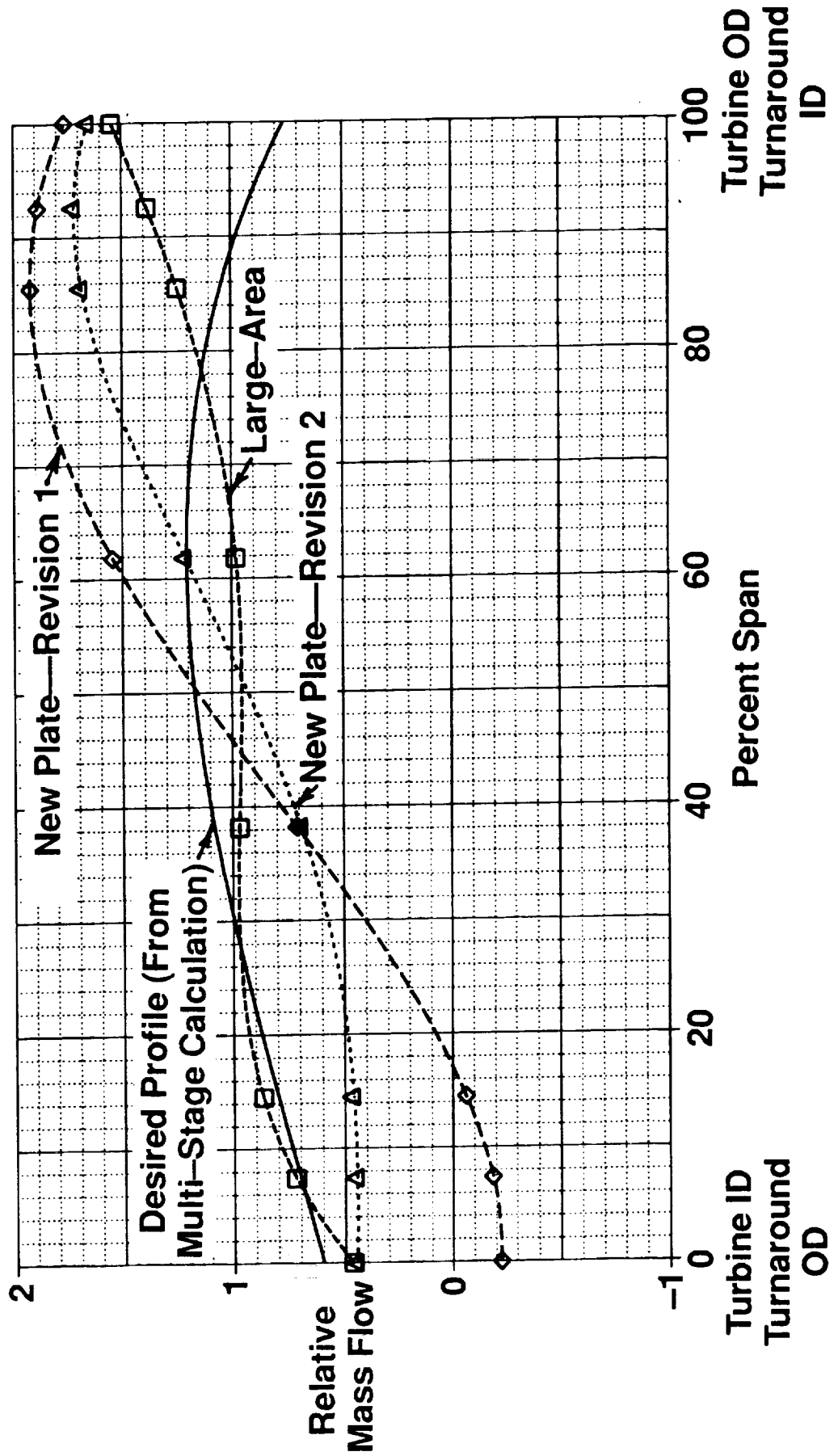


**Porosity = 38.0%, Rev. 1  
40.0%, Rev. 2**

**D = 0.1653 in.**  
**D = 0.1322 in.**  
**D = 0.1306 in.**  
**D = 0.1052 in.—Rev. 1  
0.1128 in.—Rev. 2**  
**D = 0.0932 in.—Rev. 1  
0.1063 in.—Rev. 2**

# REVISED HPOTP TURBINE SIMULATOR FLOW PROFILES

*Further Modification In Progress*



## **AIR FLOW TEST STATUS TO DATE**

- **Test Model Shows Ability To Study Complex Flow–Related Phenomena**
- **Contractor/Government Collaboration Vital In Rapid Response**
- **Accurate Evaluation Of Configuration Changes Requires Flow Conditions Closely Matching Actual Hardware**
- **Matching Of Flow Conditions Requires Careful Attention To Flowpath Details**
- **Continued Effort With Best Match Of Engine Environment**
- **HEX Vane Stress Level And Unsteady Pressure Analyses In Progress**