

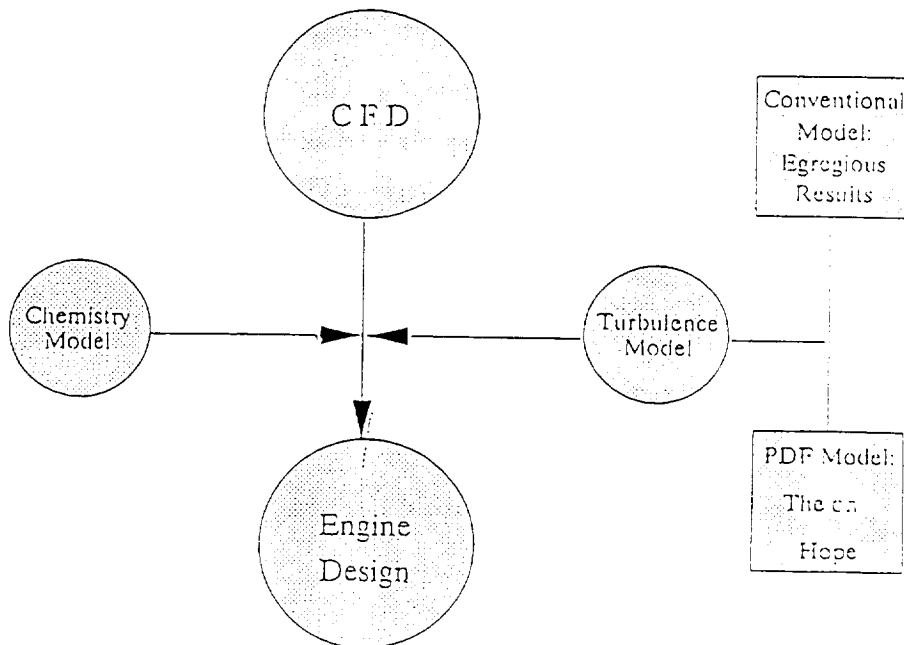
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OUTLINE

- . Motivation
- . PDF modeling of reactive flows
- . The Lewis PDF module
- . Validations and applications
- . Current research
- . Technology transfer

COMPUTATION OF TURBULENT COMBUSTION



GOVERNING EQUATIONS

$$\begin{aligned}
 \rho_{,t} + (\rho u_i)_{,i} &= 0 \\
 (\rho u_i)_{,t} + (\rho u_j u_i)_{,j} &= -p_{,i} + \tau_{ij,j} \\
 (\rho E)_{,t} + (\rho u_j E)_{,j} &= -q_{i,i} + \Phi \\
 (\rho Y_k)_{,t} + (\rho u_j Y_k)_{,j} &= (\rho D Y_{k,j})_{,j} + \omega_k
 \end{aligned}$$

$$A_{,t} \equiv \frac{\partial A}{\partial t}$$

$$A_{,j} \equiv \frac{\partial A}{\partial x_j}$$

CLOSURE PROBLEM:

$$\begin{aligned}
 u_i &= \bar{u}_i + u'_i, \\
 Y_i &= \bar{Y}_i + Y'_i,
 \end{aligned}$$

- $\overline{u'_i u'_j}$ — Turbulence Modeling
- $\overline{Y'_i u'_j}$ — Analogy of shear stress: diffusion model.
- $\overline{\rho w_i}$ — ???

$$\rho w_i = \rho w_i(Y_1, \dots, Y_n, T)$$

But in general:

$$\overline{\rho w_i} \neq \bar{\rho} w_i(\bar{Y}_1, \dots, \bar{Y}_n, \bar{T})$$

PDF Modeling of Turbulent Reactive Flows Current status

- Assumed PDF (Spalding, 1971; Gosman & Lockwood, 1973; ...)
 - ◇ Advantage: simple, fast.
 - ◇ Disadvantages: Need unique mixture fraction; assumed shape may not be real.
- Composition PDF (Pope, 1976; Dopazo & O'Brian, 1974)
 - ◇ Advantage: Reaction rate treated exactly; existing moment closure codes easily adapted.
 - ◇ Disadvantages: Turbulent diffusion needs model.
- Velocity-Composition joint PDF (Pope & Chen 1980, Pope 1981)
 - ◇ Advantage: Reaction rate treated exactly; no diffusion model needed.
 - ◇ Disadvantages: Models for velocity field relatively untried; Require more computer resource.

PDF Modeling of Turbulent Reactive Flows

- Objective:
 - ◇ Develop models that can accurately simulate finite rate chemical reactions in turbulent flows.
 - ◇ Develop and validate independent PDF modules.
 - ◇ Technology transfer.
- Criteria
 - ◇ Accuracy and robustness.
 - ◇ Practical in terms of today's computing power.
 - ◇ Easy integration with existing industry computational platform.

PDF Modeling of Turbulent Reactive Flows

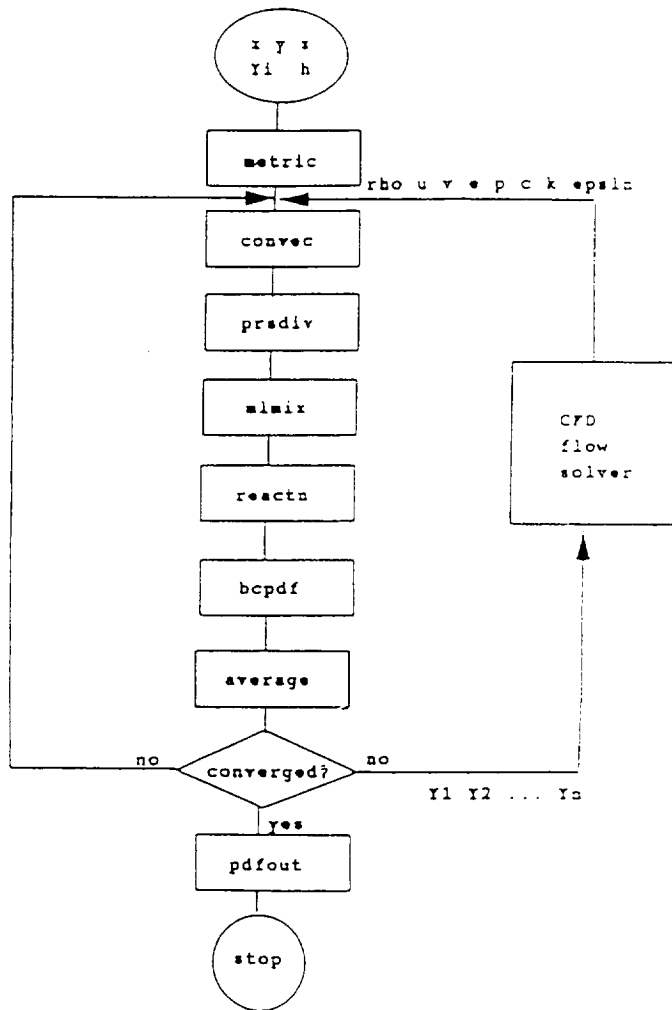
- Approach:
 - ◇ Joint pdf method for scalar compositions.
 - ◇ Moment closure schemes for velocity field.
 - ◇ Develop hybrid solver consisting of Monte Carlo method and finite-difference/finite-volume method.

PDF Modeling of Turbulent Reactive Flows

- Current status (Lewis)

$$\begin{aligned} & (\rho P)_{,t} + (\rho \langle u_j | Y_i, h \rangle P)_{,j} + (\rho w_j P)_{,y_j} \\ & = (D_i P)_{,j} + M(P) - (S_p P)_{,h}. \end{aligned}$$

- ◇ Continuous mixing model developed.
- ◇ Model for compressibility effect proposed.
- ◇ 2D and 3D Monte Carlo PDF module developed.
- ◇ Validation studies.
- ◇ Code released to industry during a workshop.



Validation Cases

- Scalar field in homogeneous turbulence.
- Oblique shock.
- 2D supersonic hydrogen combustor.
- Axisymmetric supersonic combustor.
- Piloted flame near extinction.

Scalar field in homogenous turbulence pdf compared with Gaussian distribution

Current model

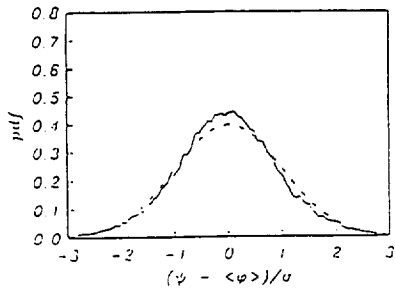


Figure 2. Asymptotic pdf distribution for a scalar in homogeneous turbulence. — present model; --- Gaussian.

Modified curl's model

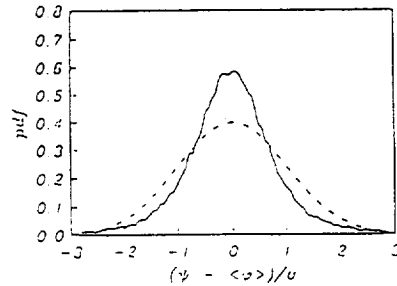
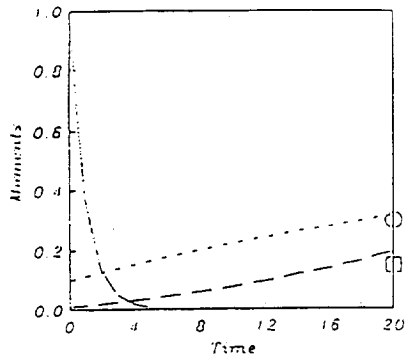


Figure 3. Asymptotic pdf distribution for a scalar in homogeneous turbulence. — modified Curl model; --- Gaussian.

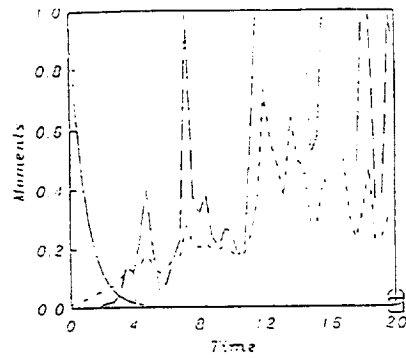
Scalar field in homogenous turbulence 3rd and 4th moments compared with Gaussian

Current model



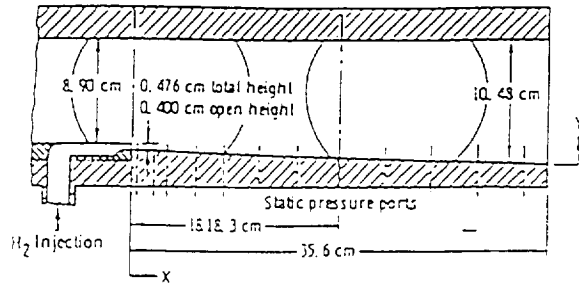
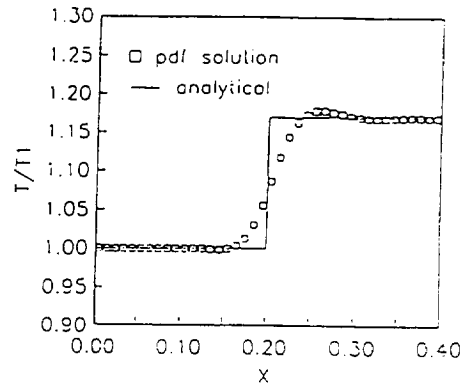
Evolution of moments from the present model. — standard deviation, ···· 0.1 x fourth central moment, --- 0.01 x sixth central moment, -·-· 0.1 x fourth moment for Gaussian distribution, □ 0.01 x sixth moment for Gaussian distribution.

Modified curl's model

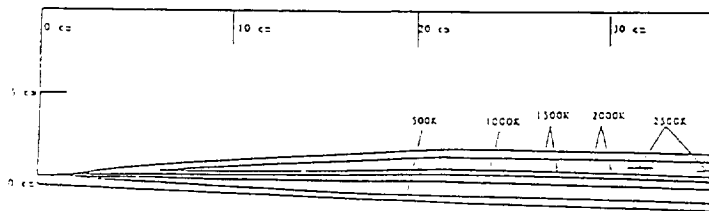


Evolution of moments from the modified Curl model. — standard deviation, ···· 0.01 x fourth central moment, --- 0.0001 x sixth central moment, -·-· 0.01 x fourth moment for Gaussian distribution, □ 0.0001 x sixth moment for Gaussian distribution.

Temperature across an oblique shock:
pdf solution compared with analytical
prediction.

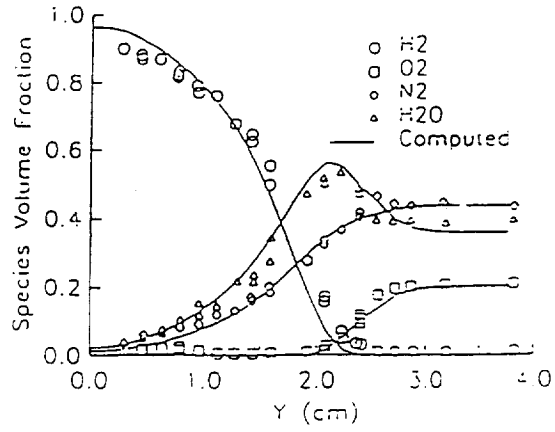


Supersonic hydrogen combustor
(Exp. Burrows & Kurkov, 1973)



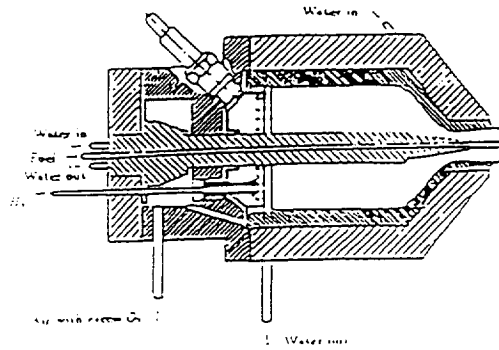
Temperature Contour (pdf solution)

Supersonic hydrogen combustor
 Mole fraction:
 pdf solution compared with exp. data

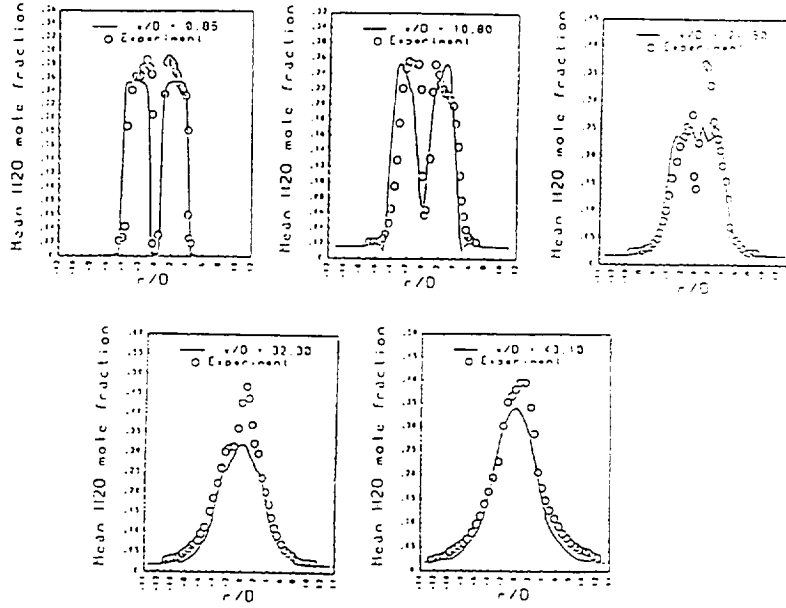


Coaxial burner: geometry and test condition
 (Exp. Cheng, et al. 1991)

Exit Conditions	Hydrogen Jet	Outer Jet	Ambient Air
Mach Number	1	2	0
Temperature, K	545	1250	300
Velocity, m/s	1780	1417	0
Pressure, MPa	.112	.107	.101
Mass Fraction			
Y_{H_2}	1.	0.	0.
Y_{O_2}	0.	.245	.233
Y_{N_2}	0.	.35	.737
Y_{H_2O}	0.	.175	.01

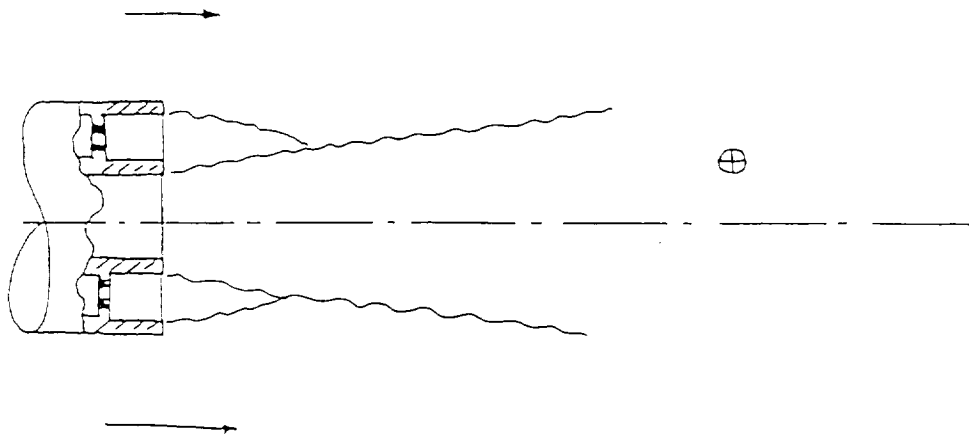


Mean H₂O mole fraction
 Coaxial burner
 pdf solution compared with exp. data

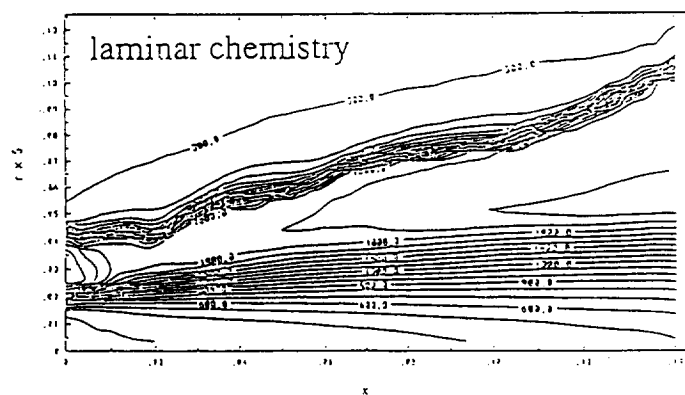
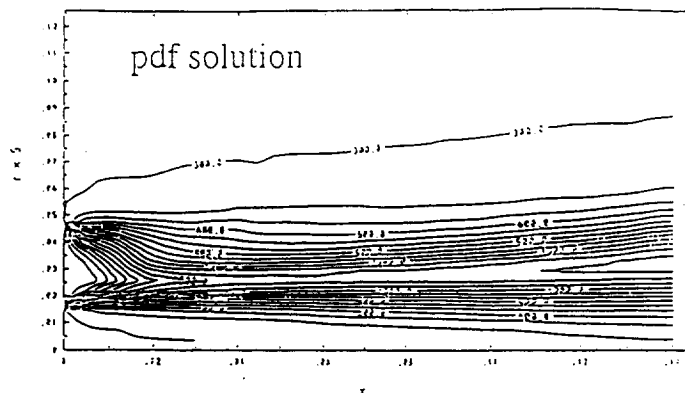


Piloted flame (Masri et al., 1994)

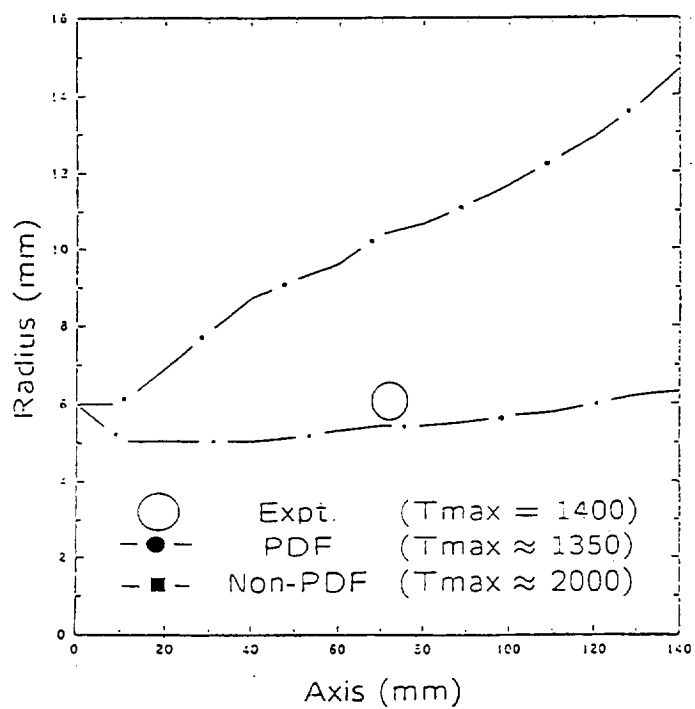
Fuel: 45% CO, 15% H₂, and 40% N₂
 Flame close to extinction



Piloted Flame
Mean Temperature



Piloted Flame
Flame Location



Current Projects

- ◇ Application of PDF module to emission predictions
- ◇ Incorporate general chemistry procedure.
- ◇ Incorporate spray models.
- ◇ Use parallel computing for the PDF module.

Collaboration with industry and technology transfer

- Features of independent pdf module:
 - ◇ Easily coupled with any existing industry flow codes.
 - ◇ Novel averaging scheme to reduce memory requirement.
 - ◇ General chemistry package.
 - ◇ Parallelized workstation version.
- Technology transfer: workshops
 - ◇ July, 1993; code released to 15 US institutions.
 - ◇ October, 1994.

