

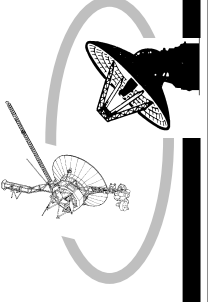
# Small Mercury Ion Clock for On-board Spacecraft Navigation\*

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**\*Research performed at the Jet Propulsion Laboratory, California Institute of Technology, under a contract with the National Aeronautics and Space Administration**

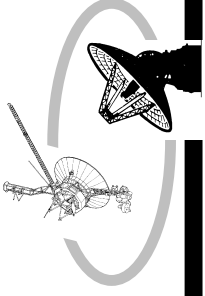




## Outline

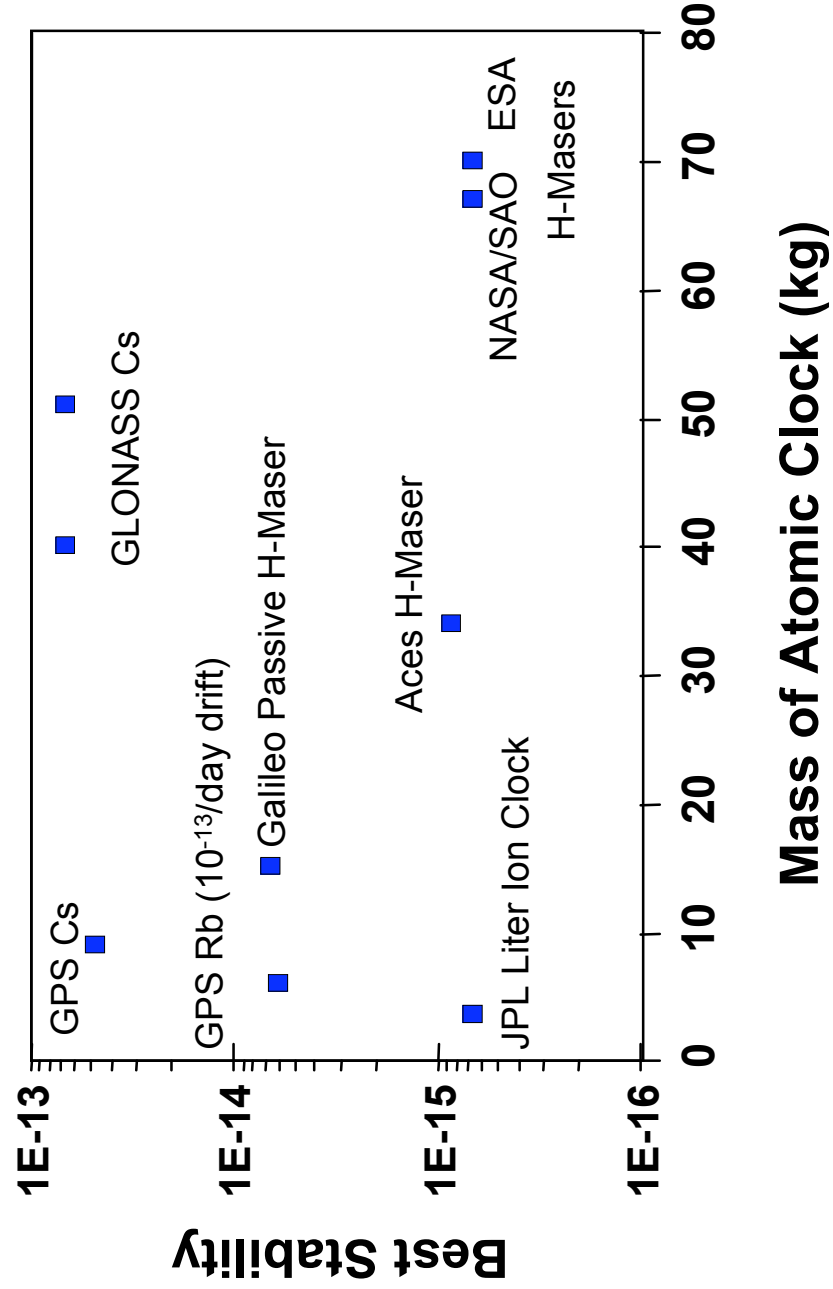
- Review of Ultra-Stable Space clock Mass vs Stability
- Laboratory Hg microwave Ion clock
  - Ion shuttling from 'Optical' trap to Microwave resonance trap;
  - $3 \times 10^{-16}$  'floor' with  $> 100 \times$  less drift than space Rb;
- Development of a One-Liter Hg Ion clock
  - Optical System Re-design;
  - Trap miniaturization, one piece brazed, no fasteners,...
  - Ultra-high Vacuum developed for getter pumping;
- Tests of Breadboard Liter clock Package
  - $5 \times 10^{-14}$  at 1 second;
  - 3x reduction buffer gas shift with Neon
- Summary

# Small Mercury Ion Clock for On-board Spacecraft Navigation



- JPL can use a small, reliable, high stability clock,  $\sim 10^{-14}$  to  $10^{-15}$  for deep space navigation
- Interplanetary S/C radio system components ( TWTA, USO,...) are 1-2 kg /2-3 liters

## Space-Based Clocks (LEO)

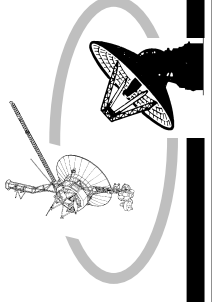


### How Large are Deep Space Craft ?

Voyager I	< 825 kg
Magellan (1989)	1035 kg
Ulysses (1990)	370 kg
Mars Observer ☹	1018 kg
Mars Global Surveyor	674 kg
Mars Pathfinder	570 kg
Cassini (1997)	2580 kg
Deep Space 1	373 kg
Mars Climate Orbiter ☹	388 kg
Stardust (1999)	300 kg
Mars Odyssey	376 kg
MER ( Rover 185 kg)	1013 kg ( r over + s/c)



# Over-view of Multi-pole Clock (1<sup>st</sup> design)



## No Lasers, Microwave Cavities, or Cryogenics

- ~20 years operational experience in 5 clocks,
- 3 linear traps,
- 2 shuttle from linear 4-pole to multi-pole
- All exceed  $10^{-15}$  stability

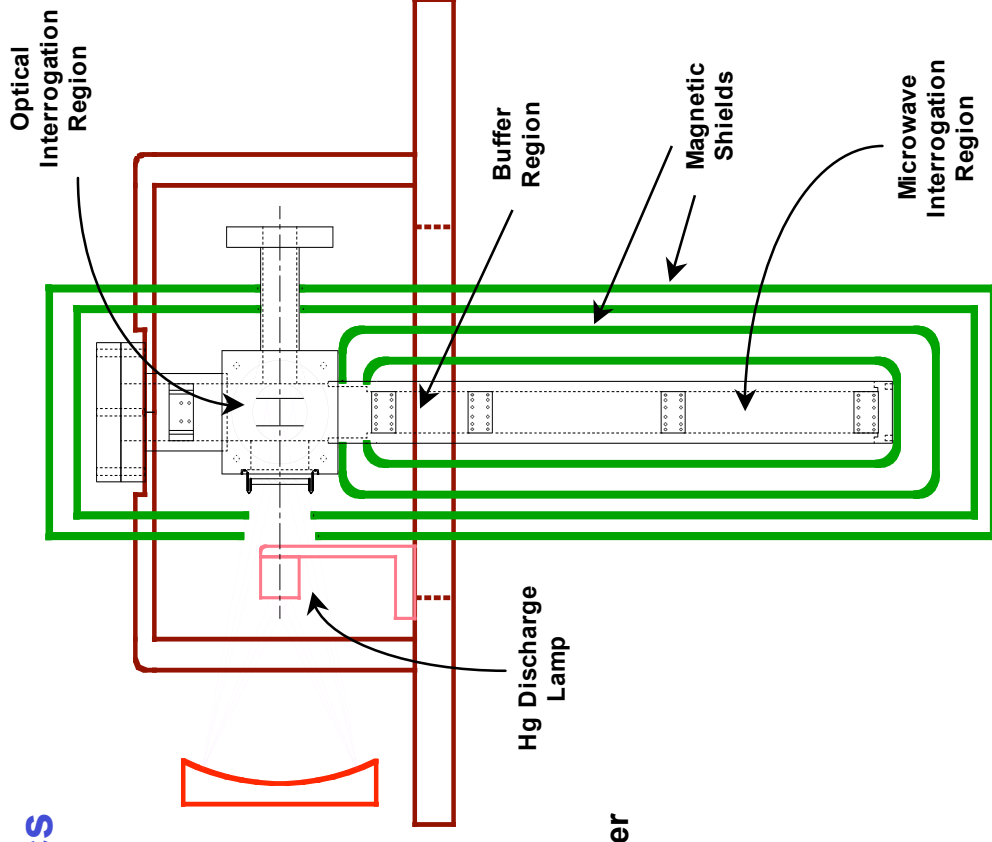
**Ions are Optically Pumped in a quadrupole trap**  
(optically open and ions are concentrated)

**40 Ghz Clock resonance in Multi-Pole trap, an RF trap with little or no radio frequency micromotion**  
(low ion density, low micro-motion, little space-charge number sensitivity)

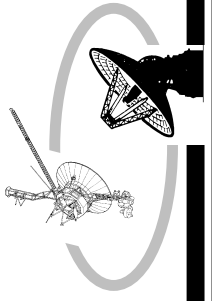
**Doppler-free for transverse k vector**

**Doppler broadened for axial k vector**

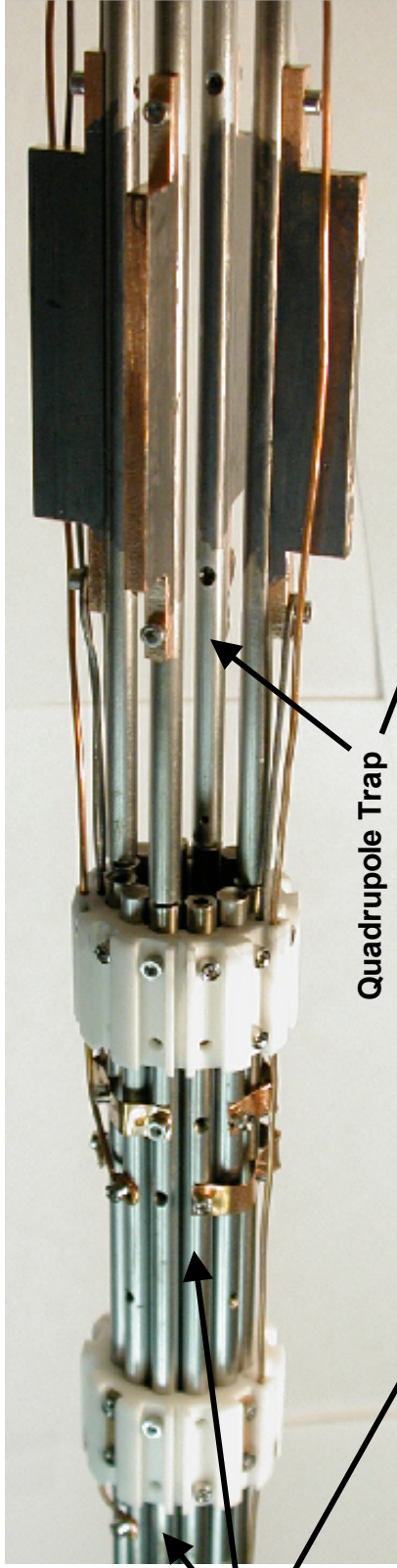
**Ions are shuttled between 4-pole and 12-pole**



**Hg Ion Frequency Standard**

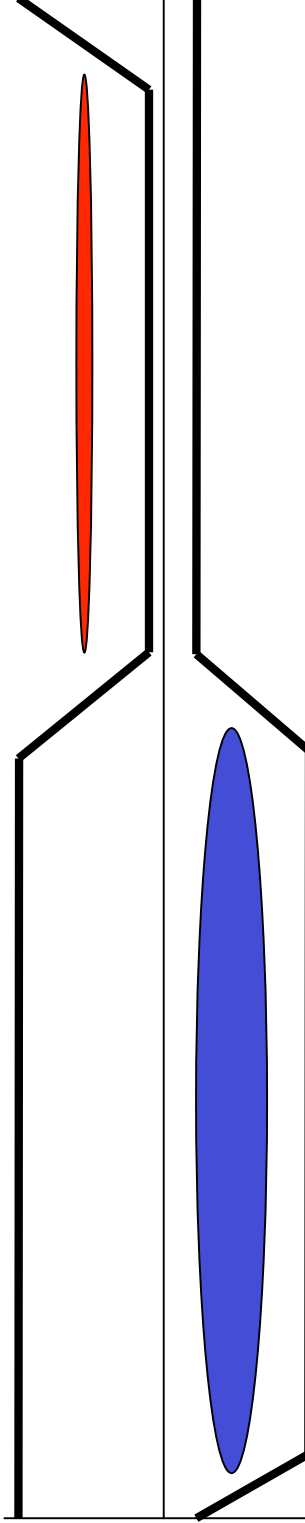
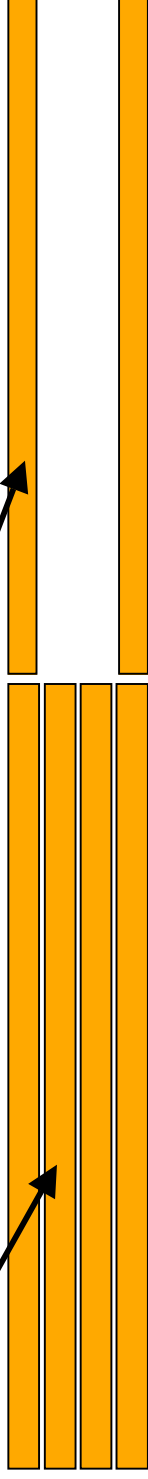


# Shuttling Ions from Quadrupole to 12-Pole (and back)



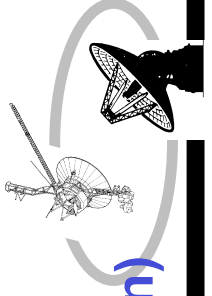
12-pole trap

Quadrupole Trap

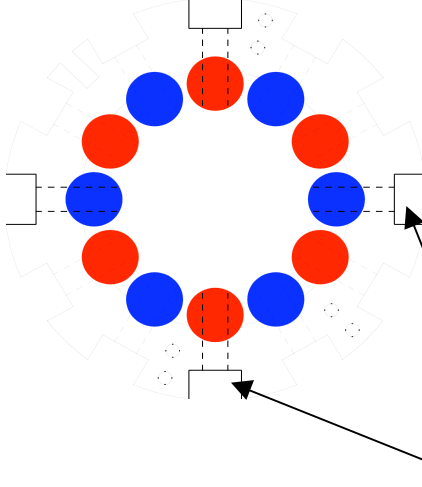
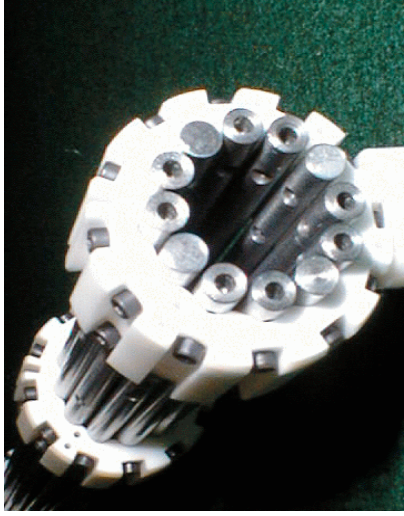


Trap Electrode  
DC Voltage along  
trap axis

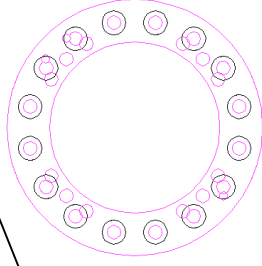
**~5,000,000 shuttles have been executed to date in USNO unit**



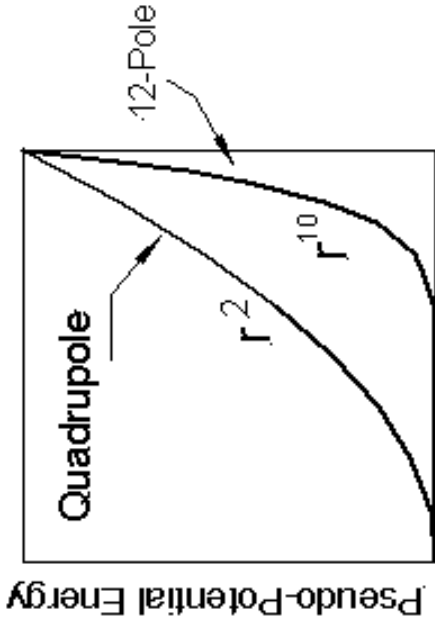
# Quadrupole vs Higher Pole (RF trap with little micro-motion in microwave region)



Laboratory 12-pole



Space-clock 16-pole  
60% external diameter  
100% internal diameter



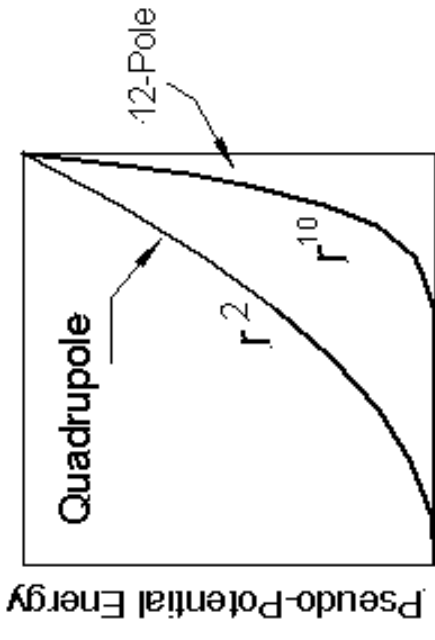
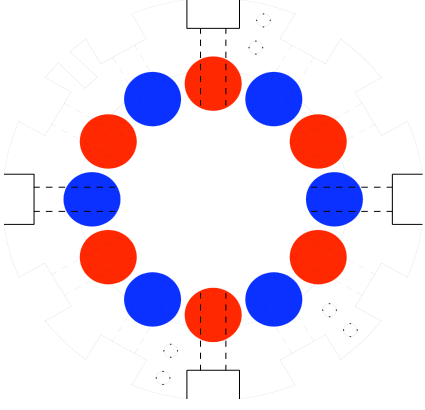
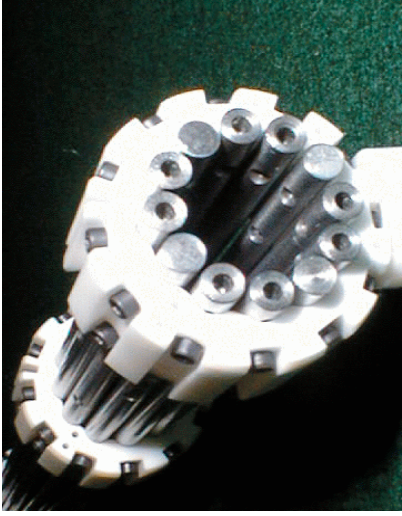
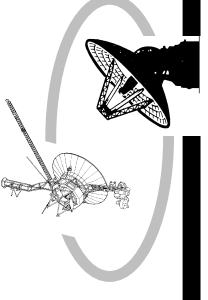
Pseudo-potential grows as  $R^{2k-2}$  for 2k rod electrodes

$$U_{pseudo} \propto R^{2k-2} \quad \overline{KE}_{transverse} = (k-1)\overline{U}_{pseudo} \quad (\text{Virial Theorem})$$

$$\overline{KE}_{m-motion} = \overline{U}_{pseudo} = \overline{KE}_{transverse} / (k-1)$$

RF Trap with very little RF micro-motion (k=2 quadrupole)

# Quadrupole vs Higher Pole (Well Depth)



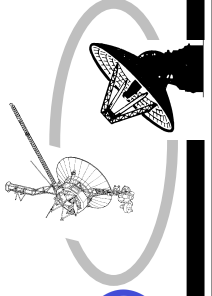
$$\eta = \frac{2q|\nabla E_0|}{m\Omega^2} = k(k-1) \frac{qU_0}{m\Omega^2 r_0^2} \hat{r}^{k-2} \leq 0.3 \equiv \eta_{\max}$$

Numerical trajectory; D. Gerlich, Adv. Chem. Phys. LXXXII (1992)

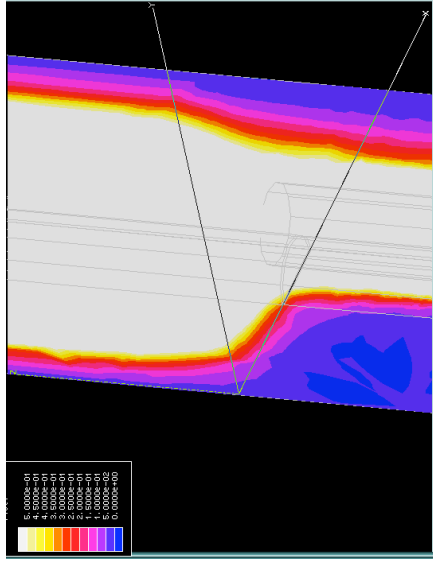
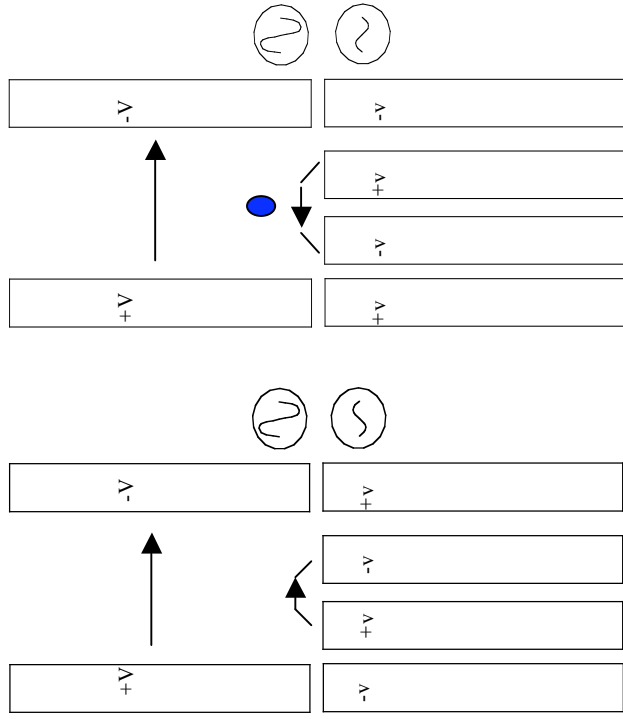
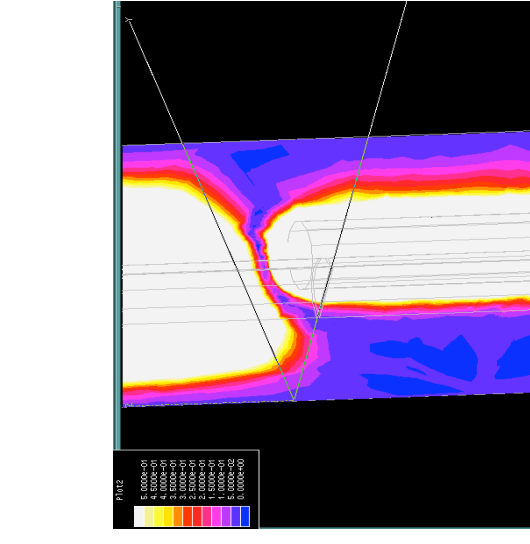
$$V_{k \gg 1}^*(R_{\max}) = \frac{m\Omega^2 r_0^2 \eta_{\max}^2}{k^2} \frac{1}{16}$$

Well depth diminishes with  $k^2$  unless frequency,  $\Omega$ , increases with  $k$





# Shuttling Ions from Quadrupole to 12-Pole (phase must change on co-linear rods at trap junction)



Opposite Phase on colinear electrodes produces good RF pseudopotential

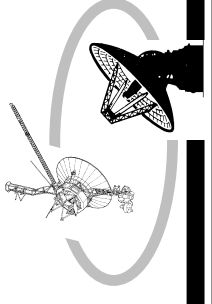
Same Phase on colinear electrodes produces a hole in the RF pseudopotential

- Problem: Joining a 4-pole to an arbitrary k-pole microwave resonance trap. Holes in the pseudo-potential cannot be avoided.
  - Can't use the higher pole traps where the lowest micro-motion is achieved.

## •Solution:

Operate the Higher pole trap at different frequency (e.g., ~2x higher). Holes open and close faster than ions can drift through.

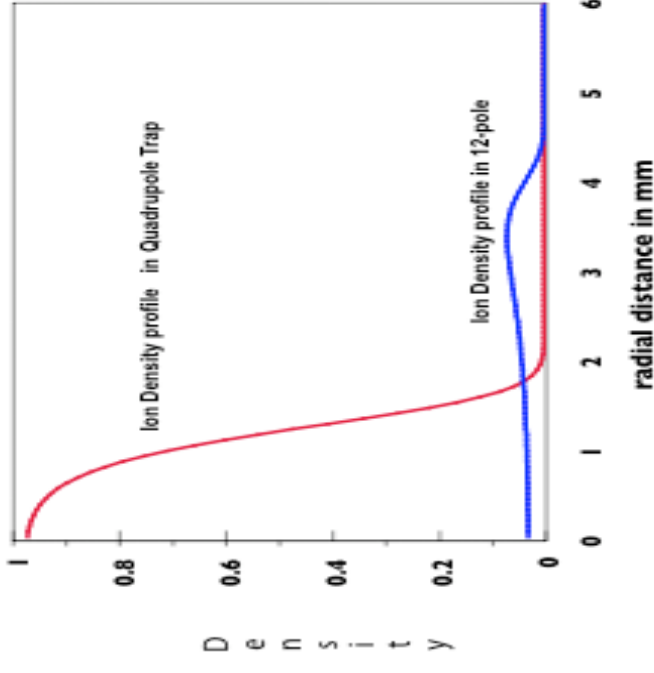
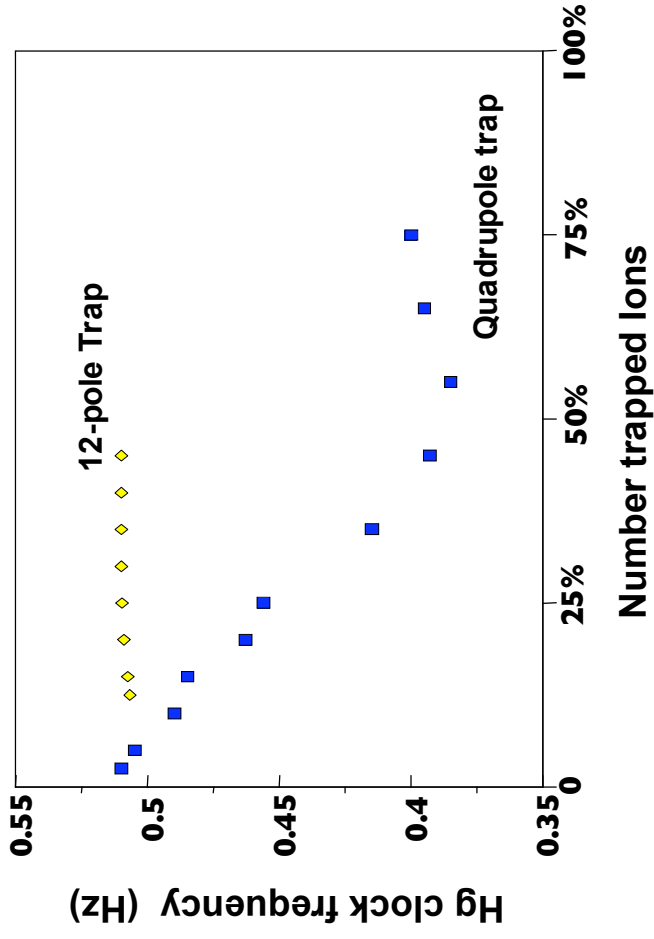
Well depth  $\sim \frac{\Omega^2}{k^2}$  can be preserved as k gets large.



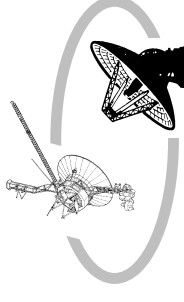
# Ion-number sensitivity is drastically reduced

Ion-number frequency pulling is at least 20x reduced from LITS quadrupole !

It doesn't behave like ion heating and 2nd-order Doppler frequency pulling !

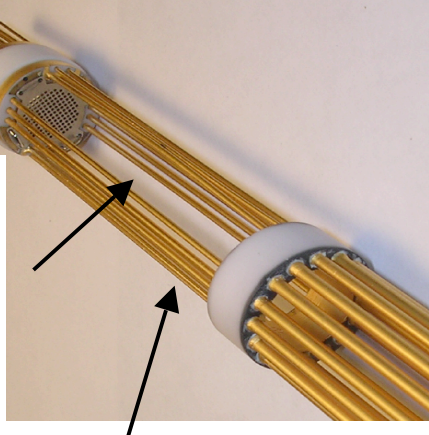


# Miniaturizing Ion Traps

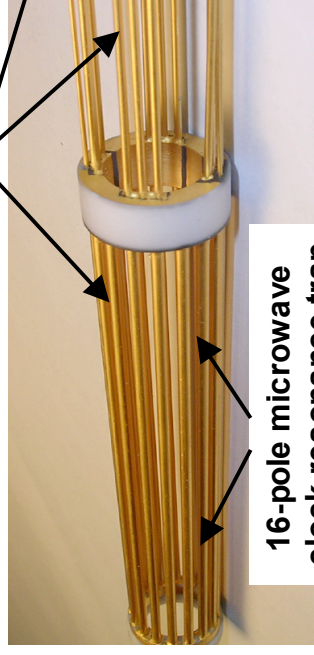


- State selection/optical interrogation in quadrupole; microwave clock resonance in higher multipole trap.
- Ion traps are brazed, “one piece” with metallized electrical interconnects; no screws, etc. used as fasteners.
- Non-magnetic parts required for high Q atomic resonance ( $Q \sim 3 \times 10^{11}$ ).
- 16-pole provides better isolation to stray external fields, for 0.056” moly rod size.
- 4-pole load trap has twice the well depth of the previous version; better ion load rates, higher SNR in clock resonance.

Quadrupole optical state selection trap

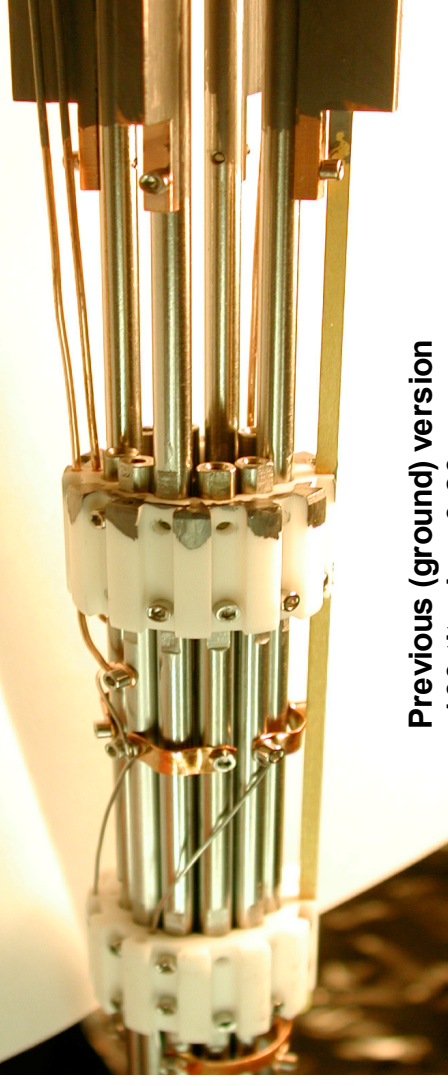


Gold plated Moly wires and rods



16-pole microwave clock resonance trap

>10x trap size reduction

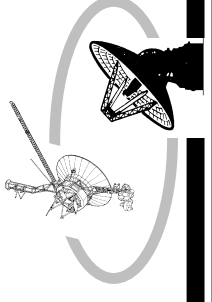


Previous (ground) version  
>100 titanium 0-80 screws

John Prestage

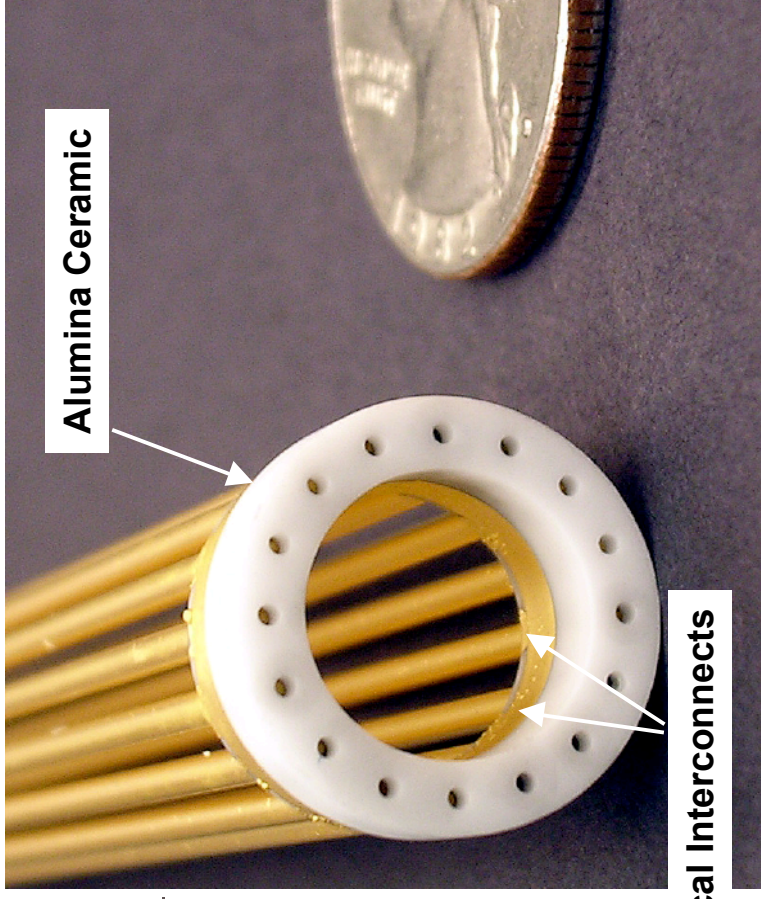
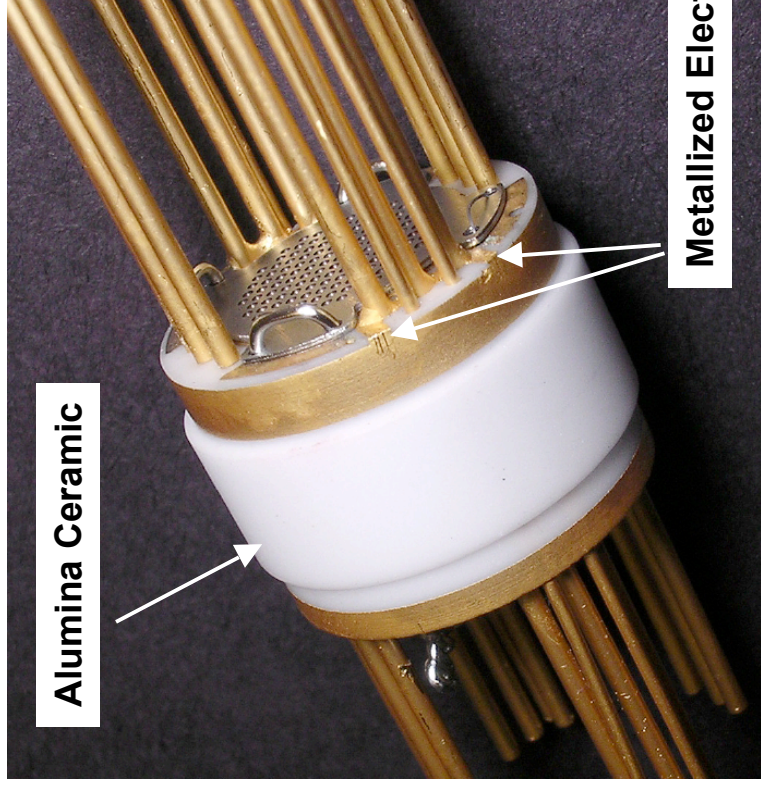
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## Full Trap Design, Fabrication Completed

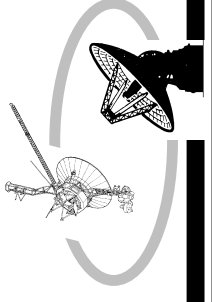
- 4 trap assemblies procured and delivered, 5<sup>th</sup> to be inspected for electrical connection integrity;
  - First 2 assemblies were “learning curve” fabrications, mechanical/magnetic/electrical problems
  - Remaining 3 are ready for clock tests.



John Prestage

April 2004

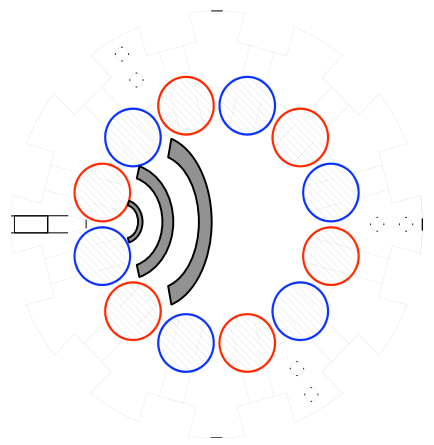
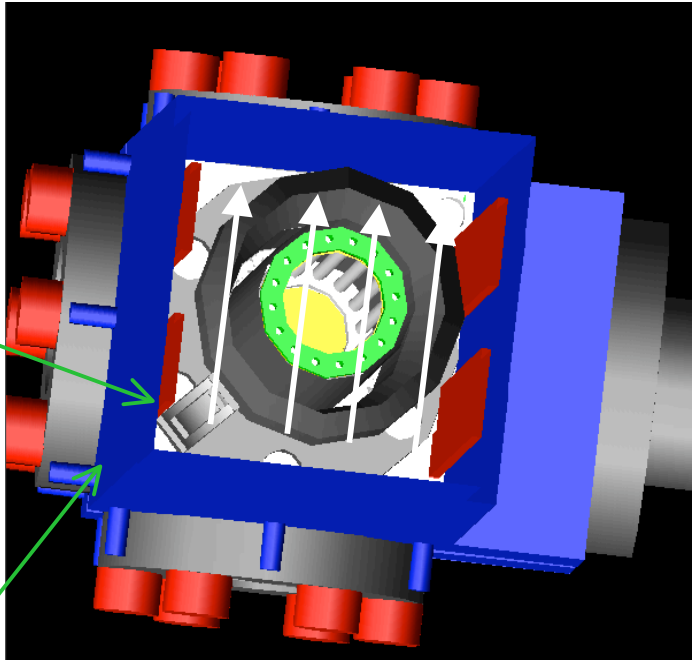
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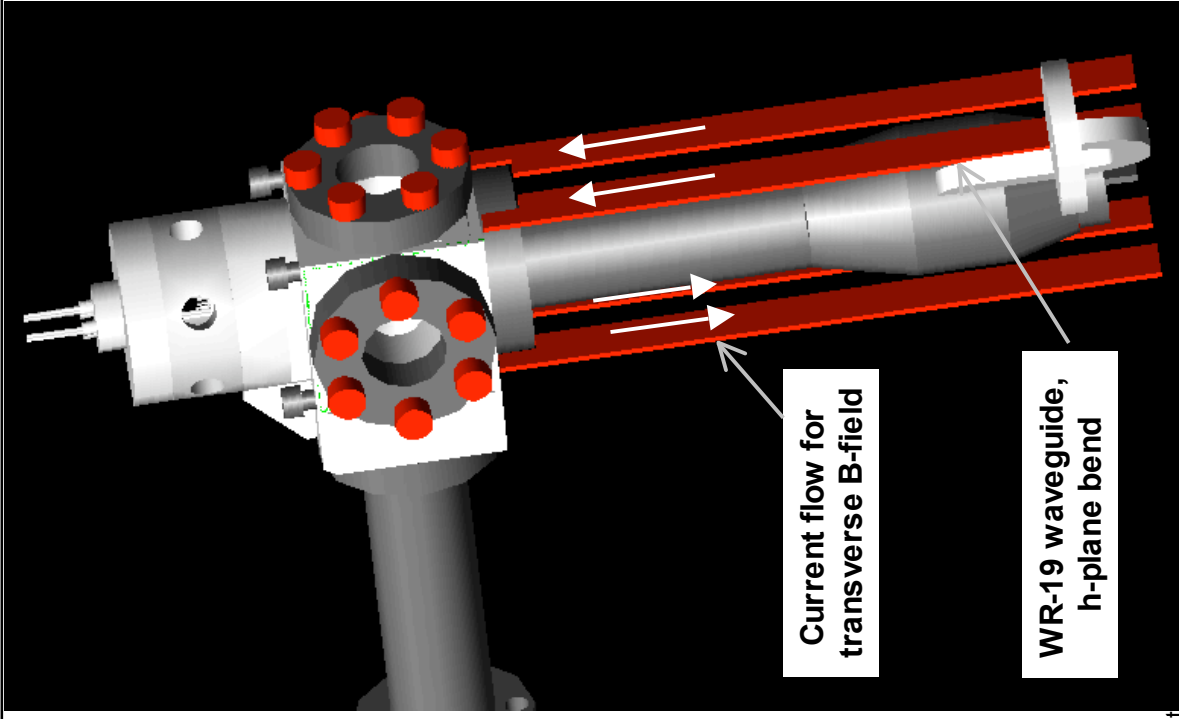
## Inner Shields, field coils, and WR-19 waveguide

Microwaves propagated trap axis avoids carrier suppression of 40.5 GHz

Inner magnetic shield square cross-section

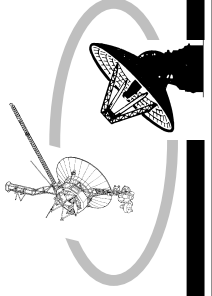


Doppler-free clock transition requires transverse  $k$  vector



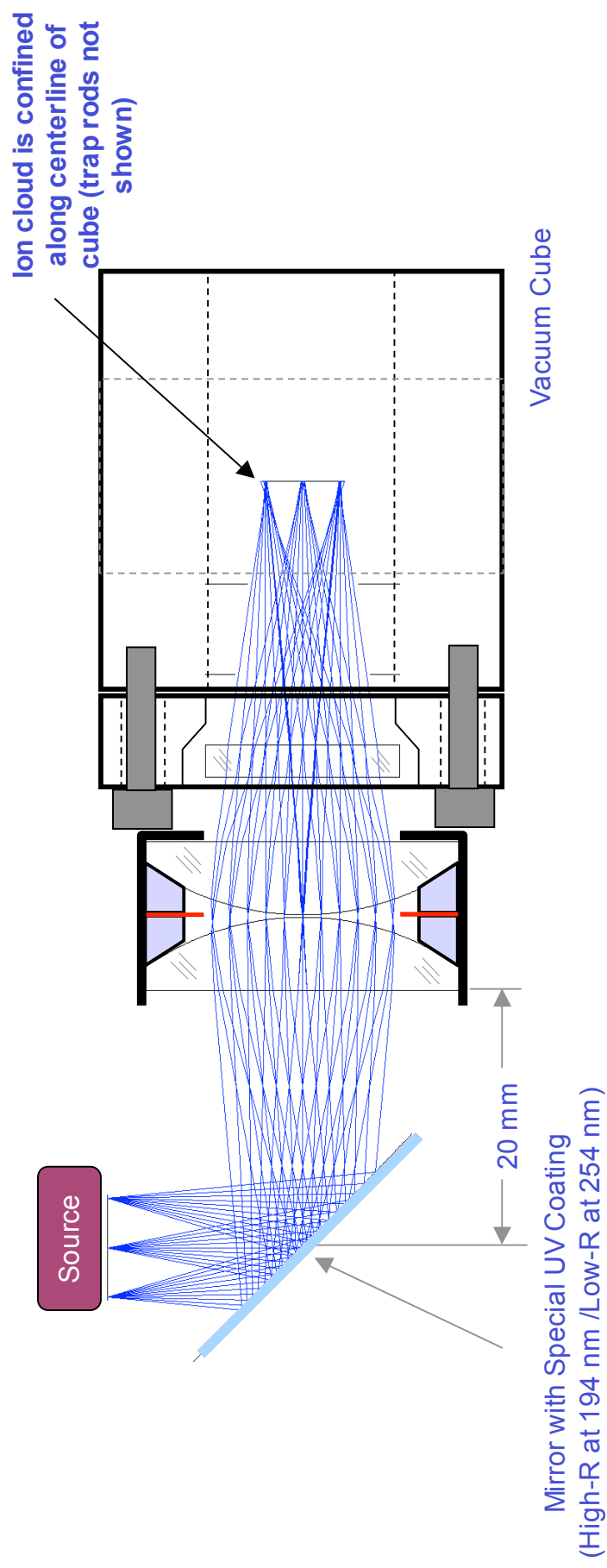
Current flow for transverse B-field

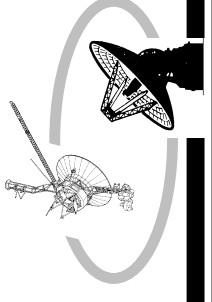
WR-19 waveguide, h-plane bend



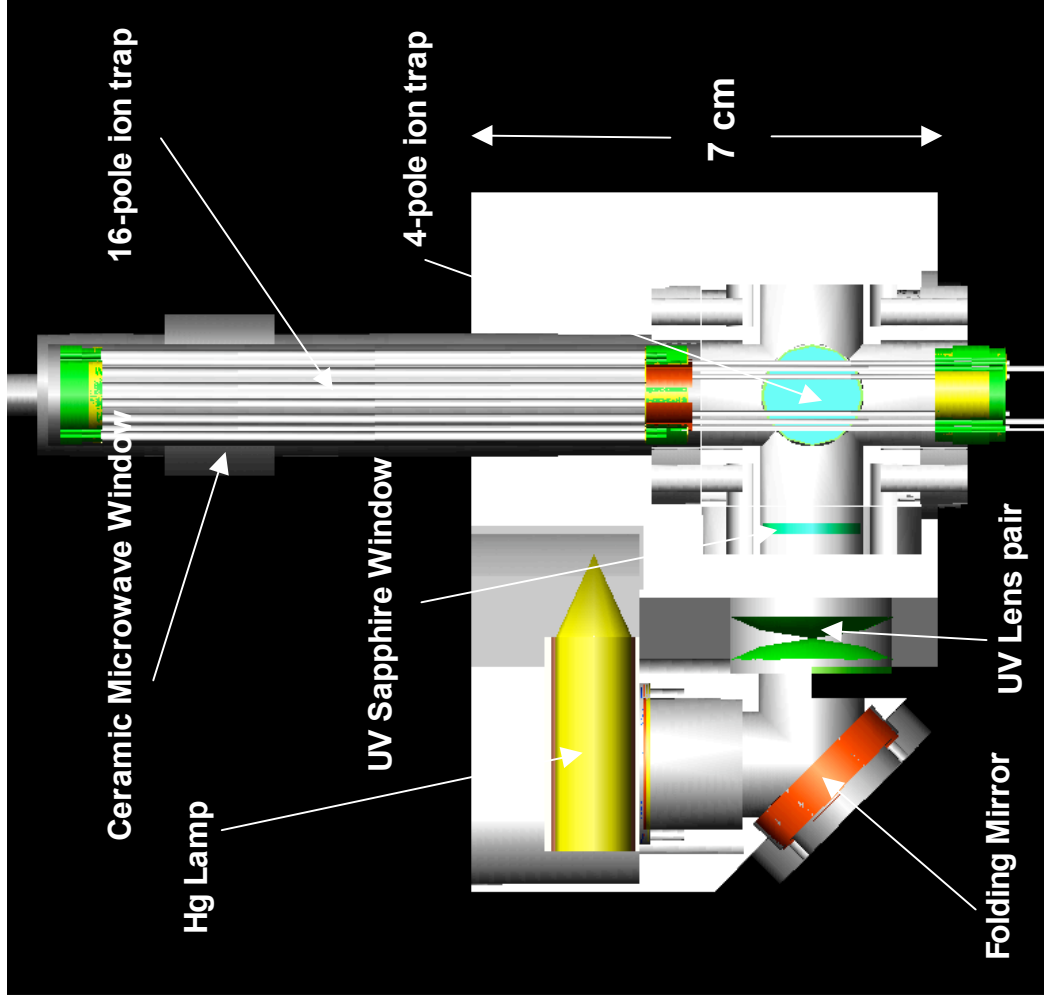
# Optical System - 2 lenses and 1 mirror

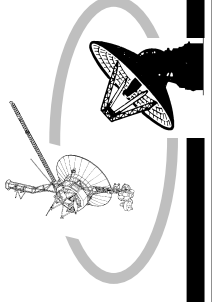
- Design Uses 3 identical optical arms, each with 2 lenses, an UV dichroic folding mirror, and a UV-grade sapphire vacuum window.
  - Ion fluorescence detection arms are oriented perpendicular to input light arm.
- Optics features:
  - UV-grade silica, 10-5 scratch-dig polish, antireflectance coated to <0.5% per surface.
  - Surface roughness is a source of stray light in the UV; laser optical polish used.
- Clock optical components are also used in semi-conductor photolithography (ArF 193 nm laser)





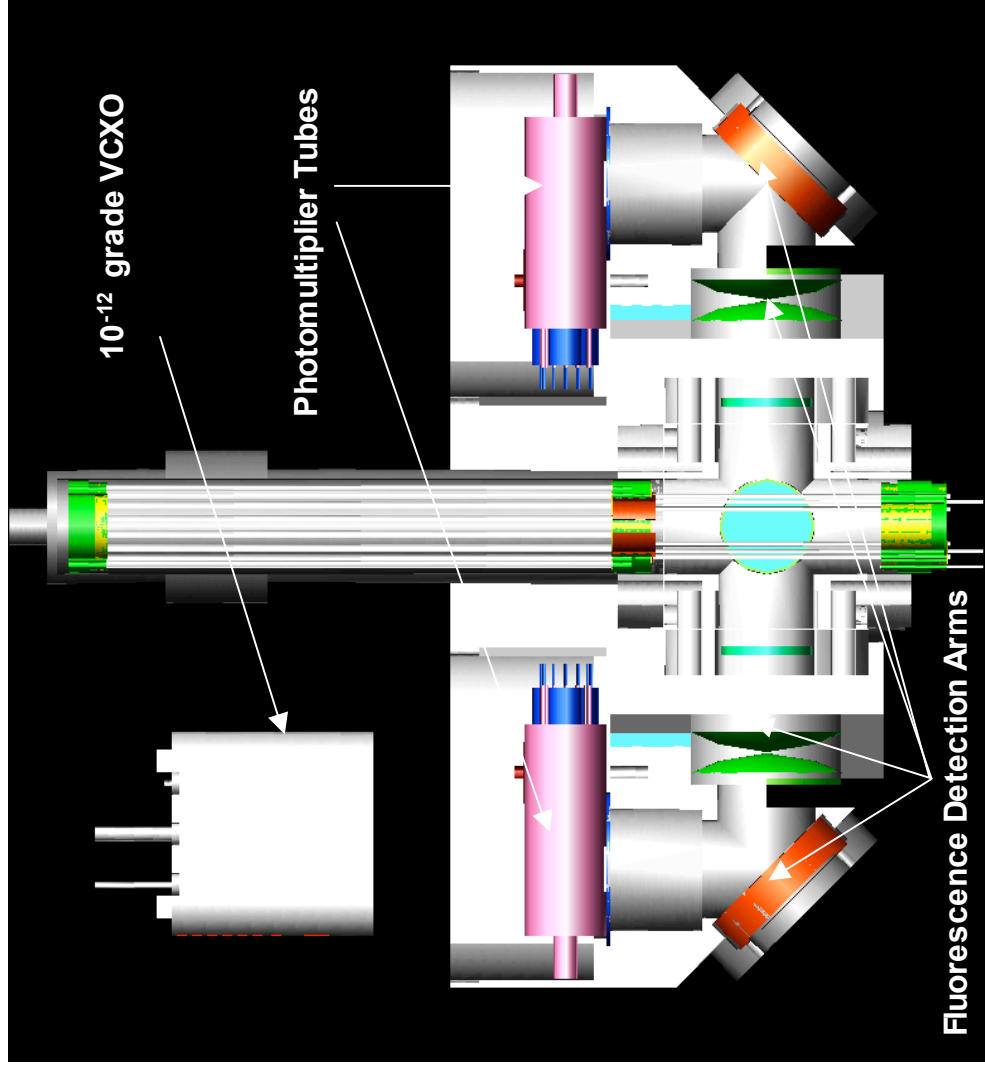
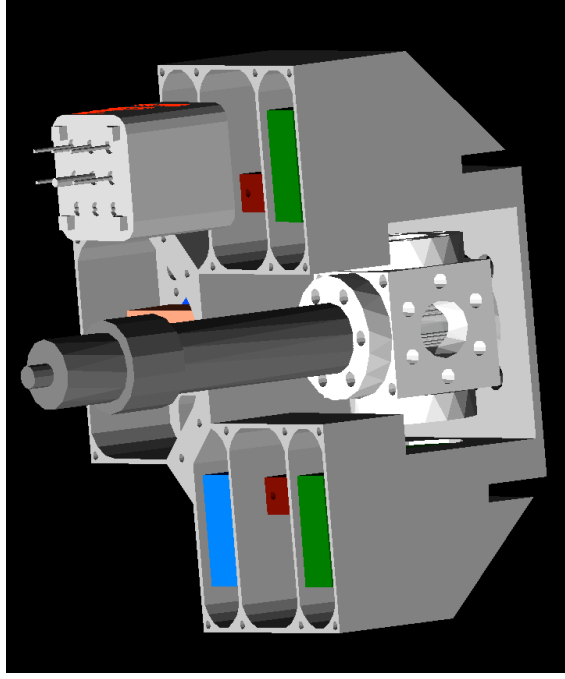
- **Optical Mount is single piece modular**
  - **can be tested for internal alignment without the ion trap**
- **Lamp resonator and exciter power electronics are integrated into module**
- **Sensitive detector electronics are isolated from lamp exciter power via RF-tight gasket compartments**



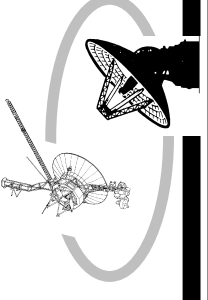


# Modular Compact Optical System

- UV light detectors with power supply, amp/discriminator chip are integrated into module.
- Isolated from RF power in lamp driver module with RF-tight compartments as shown below







## Packaged Optical Electronics - UV source and fluorescence detectors

Lamp Resonator  
with Hg lamp

High-Voltage supply for PMT

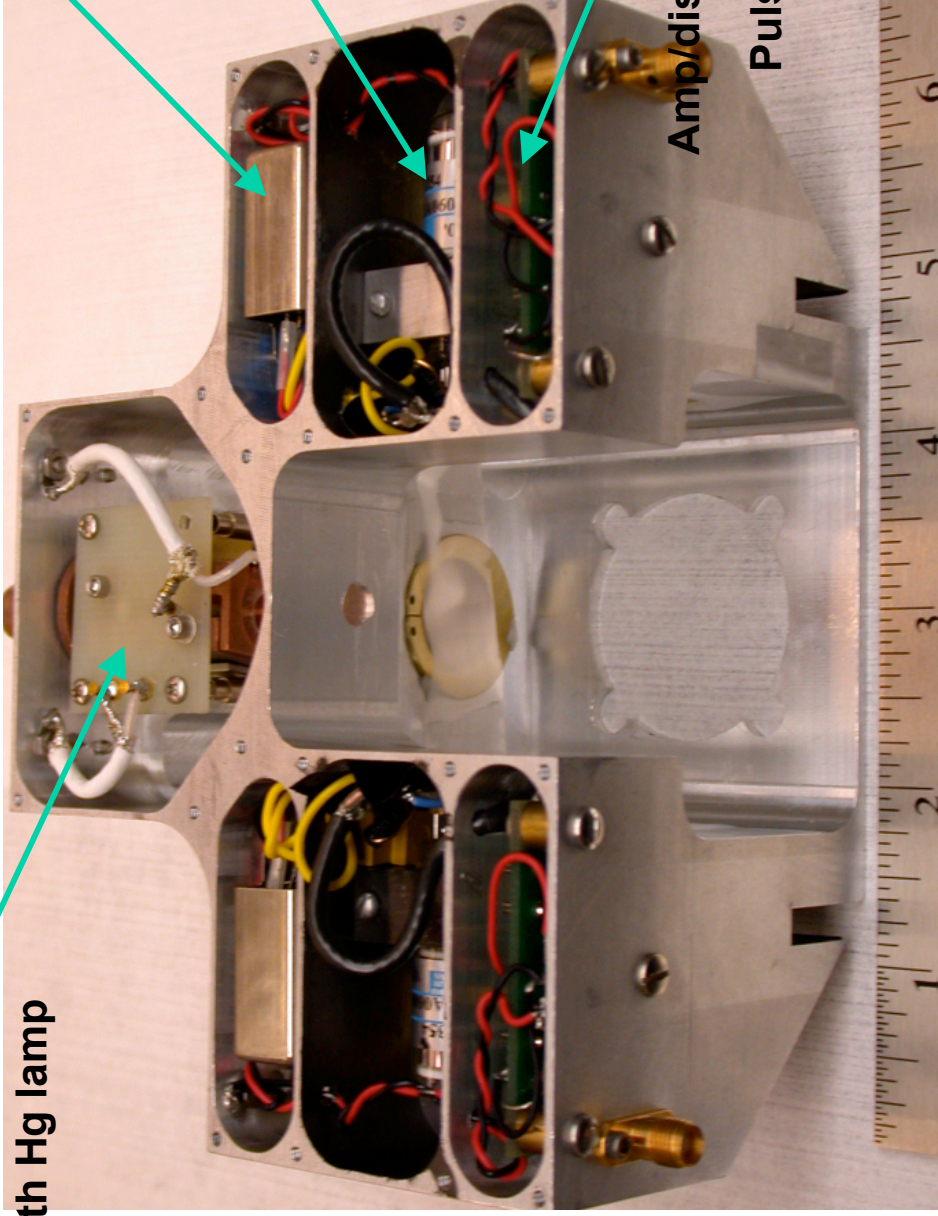
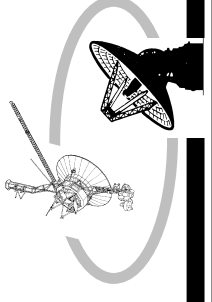


Photo-multiplier Tube  
(PMT) with base

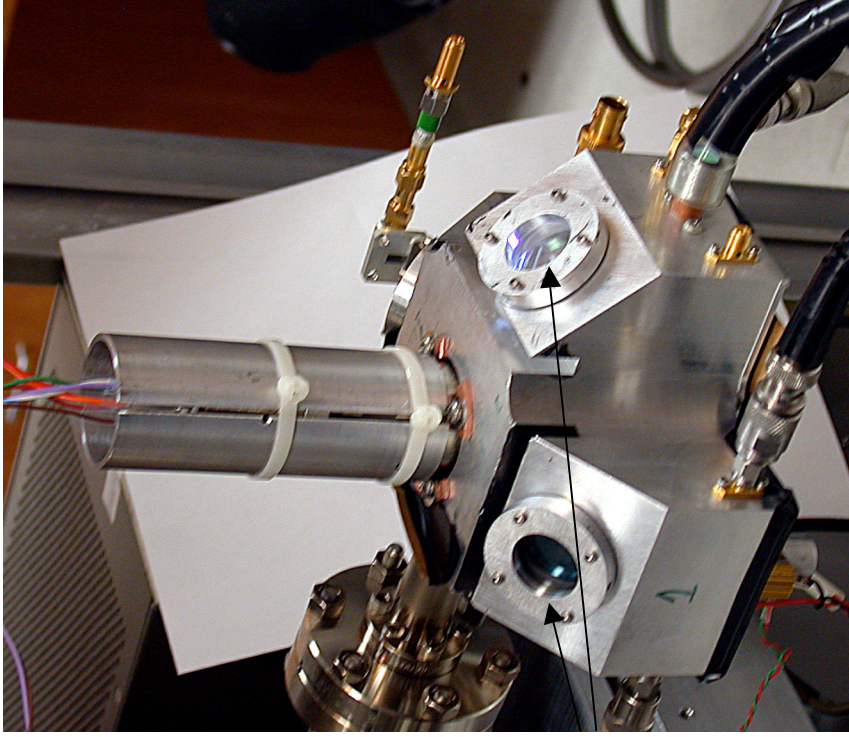
Amp/discriminator PC board

Pulse out to counter

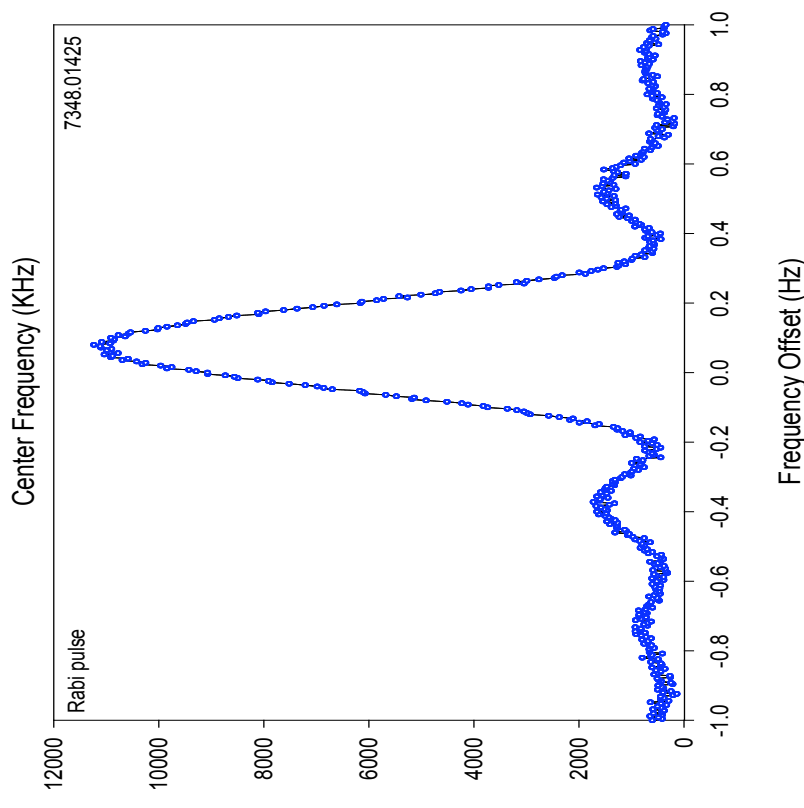
# Liter Hg Ion Clock, $10^{-13} \tau^{-1/2}$

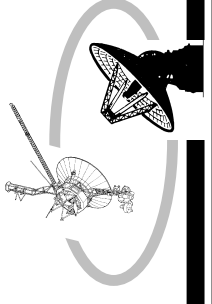


- Demonstrated short-term stability  $10^{-13} \tau^{-1/2}$ , as good as the 100x larger ground-based package.
- Line Q  $\sim 2 \times 10^{11}$  in the first measurement (shown at right)
- No magnetic shields yet installed



Folding Mirrors

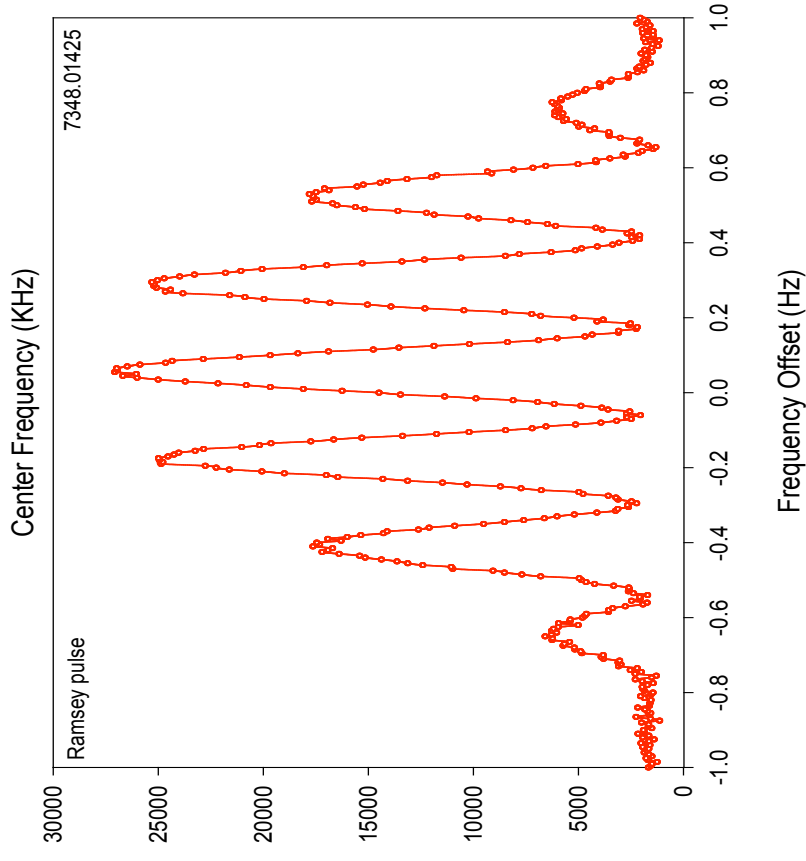
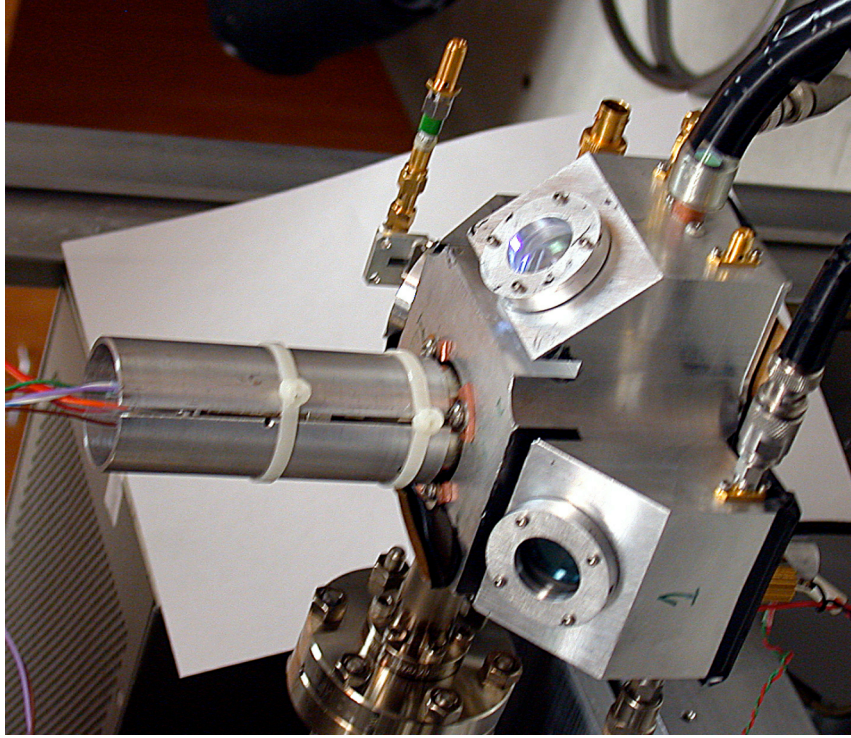


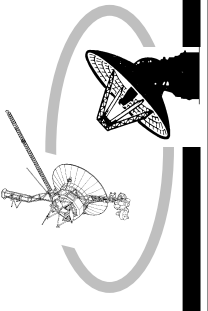


# Liter Hg Ion Clock, $10^{-13} \tau^{-1/2}$

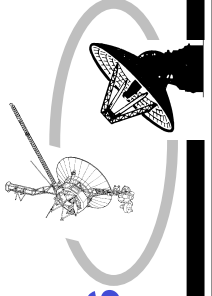
**JPL**

- $Q \sim 4 \times 10^{11}$  in measurements shown at right.
- No magnetic shields for these measurements.
- $Q \sim 10^{12}$  in later measurements.





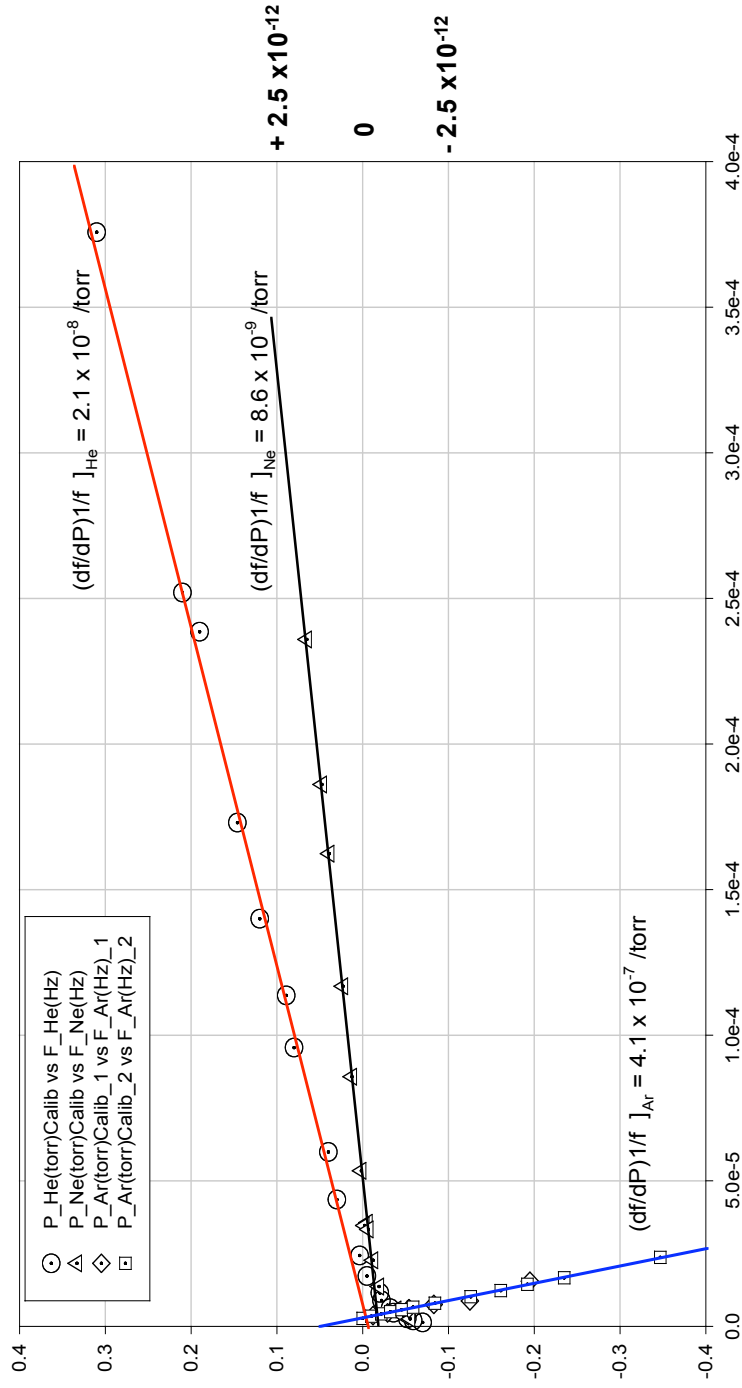
- **Replace mechanical pumping and buffer-gas flow system.**
  - Light, noble buffer gas required to cool ions to room temperature, increase number of captured/trapped ions.
  - UHV prepared, filled with buffer gas and getters, then sealed.
- **Getter pumping, bulk and surface getters (Benvenuti, et al, 1998)**
  - Consumes no mass, power, little volume.
  - Will not pump or otherwise consume buffer gas.
- **Requires UHV design and fabrication.**
  - 400 C Sapphire windows developed.
  - Low gas load field emitter filament employed.
  - Titanium vacuum jacket materials.
  - 400 C bake-out with sealed getters, filled to  $\sim 10^{-5}$  Torr with Ne buffer.



# Ion clock uses buffer gas to “cool” ions

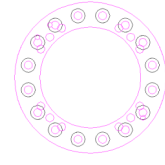


- Hg<sup>+</sup> clock uses ~ 10<sup>-5</sup> Torr “buffer” gas to cool ions to near room temperature; helium is traditionally used.
- Investigated neon and argon as substitutes; Found 3 times less clock frequency changes in neon than helium; 20x more in argon
- Additionally, neon pressure varies 5x less than helium for a 1 C temperature change
- Frequency pulling < 10<sup>-15</sup> per degree C temperature change !

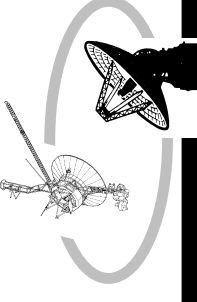


Calibrated Buffer Gas Pressure (torr)

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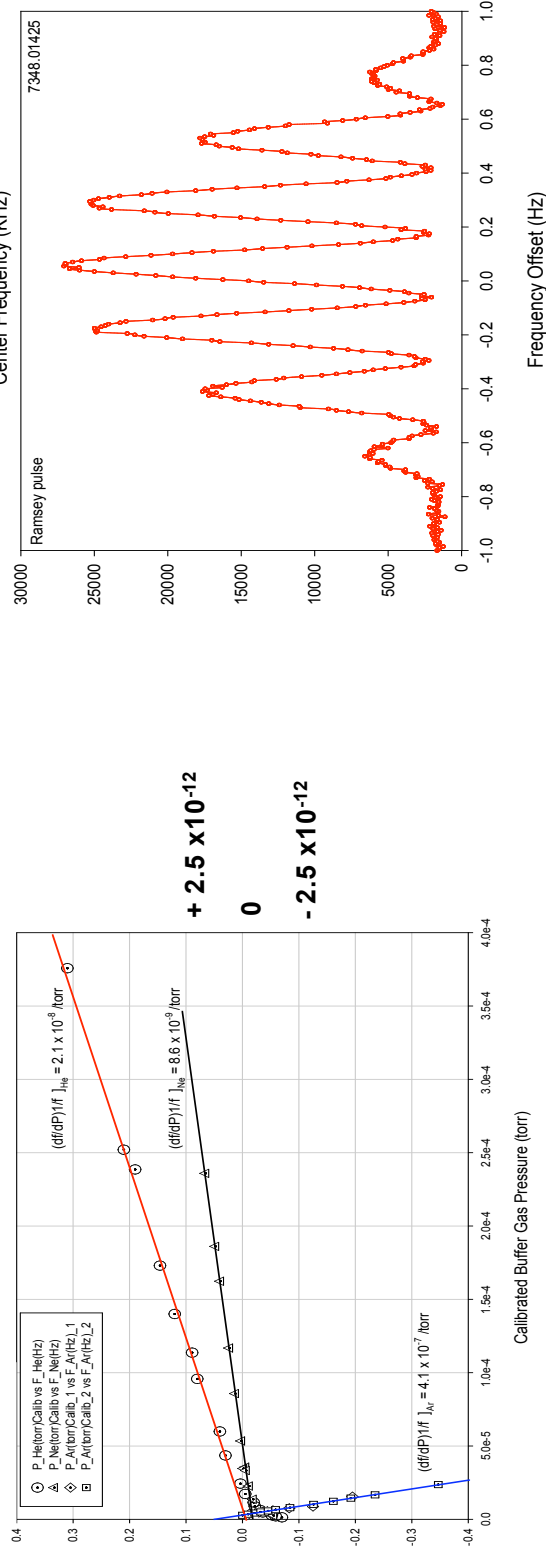


# Summary

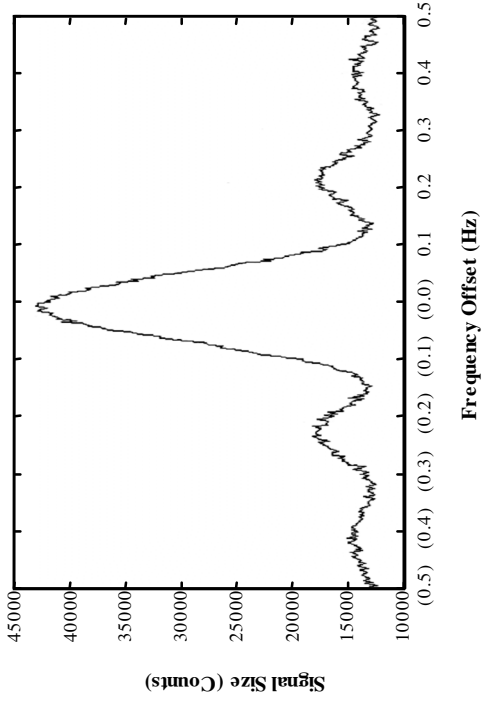
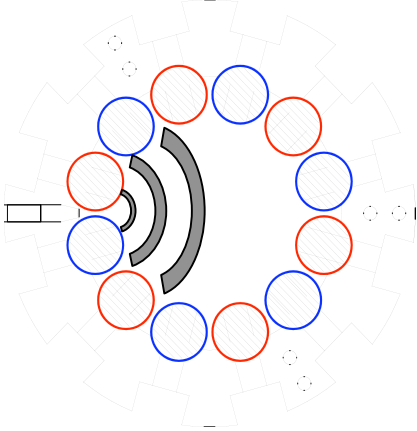
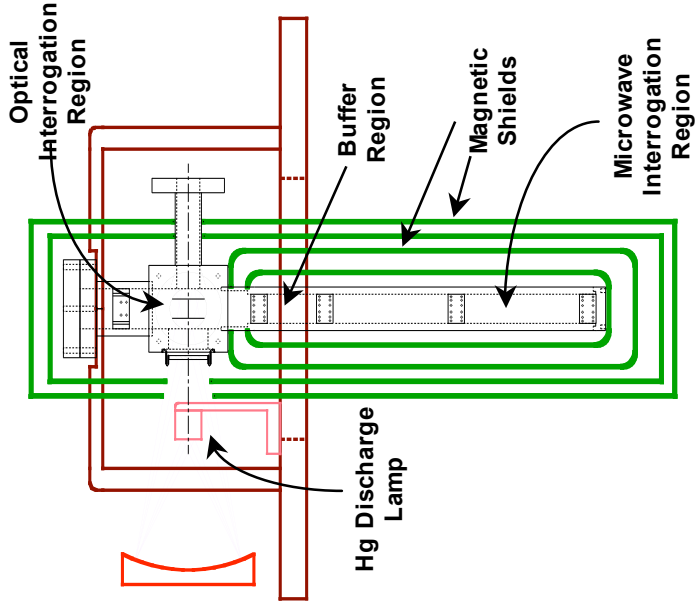
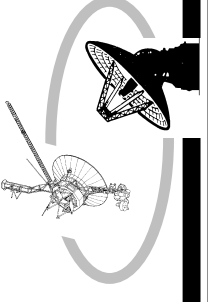


- Microgravity friendly, 1-g gravity friendly.
- $10^{-15}$  stability in a 1-2 liter package seems feasible.
- Demonstrated  $10^{-13} \tau^{-1/2}$  in ~ 1-liter physics package breadboard.
- Demonstrated 3x reduction in buffer gas shift by neon.

• Frequency pulling  $< 10^{-15}$  per degree C temperature change via buffer gas variations



# Doppler-free and doppler-broadened resonance in 12-pole trap

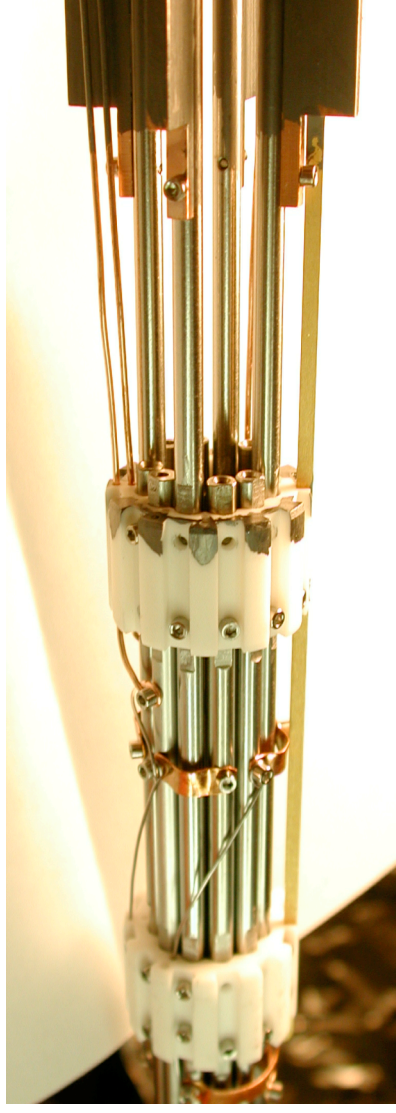


Doppler-free clock transition for transverse  $k$  vector propagation ( $\sim 100$  mHz)

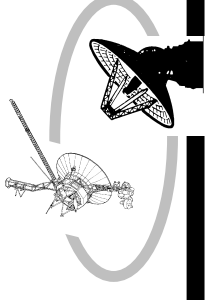
Propagation along the trap axis determines ion temperature; 1% width measure gives  $2 \times 10^{-15}$  2<sup>nd</sup> Doppler determination

$$\delta V_{Doppler} = 2 \frac{v_0}{c} \sqrt{\frac{2k_B T \ln 2}{m}}$$

$$= 35.6 \sqrt{\frac{T(K)}{300}} \text{ [kHz]}$$



## Ion clock redesign for space



- Small Ion Clock Approach and Heritage
  - No lasers, uwave cavities, cryogenics, atomic beams, etc.
  - Ions are electrically shuttled between separate optical and microwave traps.
    - Each trap is optimized for its task:
      - quadrupole for optical state selection;
      - multi-pole for microwave clock.
  - Very good stability shown in USNO Timescale running “open loop”
    - “Open loop” operation means no self-measurements of frequency offsets: Zeeman, ion temperature,... etc.
      - Fewer parts and procedures, produces stable output continuously
    - Ion clock is not so sensitive to temperature fluctuations
      - Measured *unshielded* temperature coefficient of few  $10^{-15}$  per C.
      - No bulky temperature isolation needed.

