On the Minimum Induced Drag of Wings -orThinking Outside the Box

Albion H. Bowers

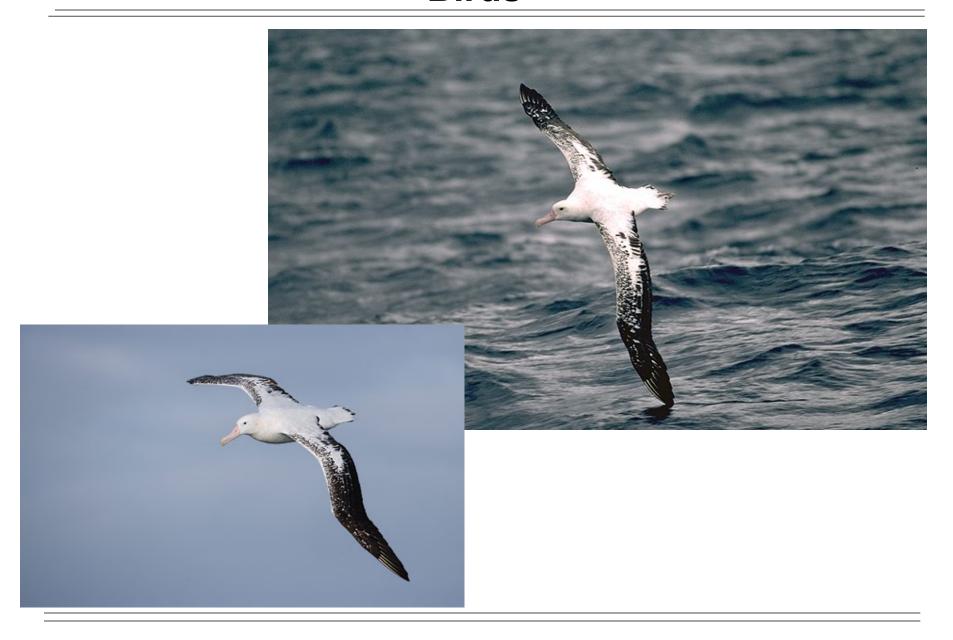
NASA Dryden Flight Research Center

04 Sep11

Introduction

- The History of Spanload
 Development of the optimum spanload
 Winglets and their implications
- Horten Sailplanes
- Flight Mechanics & Adverse yaw
- Concluding Remarks

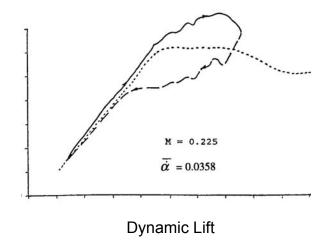
Birds



Bird Flight as a Model

or "Why don't birds have vertical tails?"

- Propulsion
 Flapping motion to produce thrust
 Wings also provide lift
 Dynamic lift birds use this all the time (easy for them, hard for us)
- Stability and Control
 Still not understood in literature
 Lack of vertical surfaces
- Birds as an Integrated System
 Structure
 Propulsion
 Lift (performance)
 Stability and control
- Wright dis-integrated the bird
- Its time to reintegrate bird-flight



Spanload Development

Ludwig Prandtl

Development of the boundary layer concept (1903)

Developed the "lifting line" theory

Developed the concept of induced drag

Calculated the spanload for minimum induced drag (1908?)

Published in open literature (1920)

Albert Betz

Published calculation of induced drag

Published optimum spanload for minimum induced drag (1914)

Credited all to Prandtl (circa 1908)

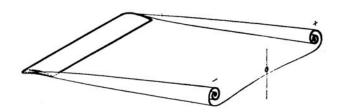
Spanload Development (continued)

- Max Munk
 General solution to multiple airfoils
 Referred to as the "stagger biplane theorem" (1920)
 Munk worked for NACA Langley from 1920 through 1926
- Prandtl (again!)
 "The Minimum Induced Drag of Wings" (1932)
 Introduction of new constraint to spanload
 Considers the bending moment as well as the lift and induced drag

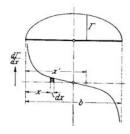
Practical Spanload Developments

- Reimar Horten (1945)
 Use of Prandtl's latest spanload work in sailplanes & aircraft Discovery of induced thrust at wingtips
 Discovery of flight mechanics implications
 Use of the term "bell shaped" spanload
- Armin Klein & Sathy Viswanathan
 Minimum induced drag for given structural weight (1975)
 Includes bending moment
 Includes shear

Prandtl Lifting Line Theory

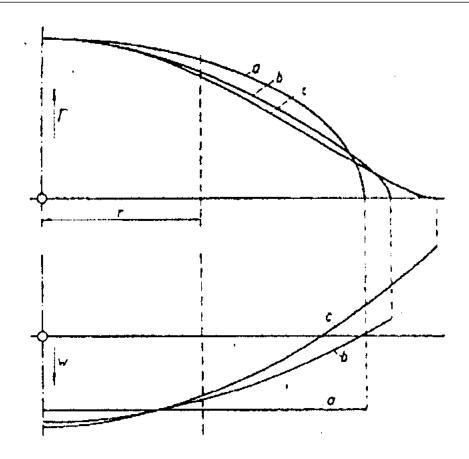


Prandtl's "vortex ribbons"



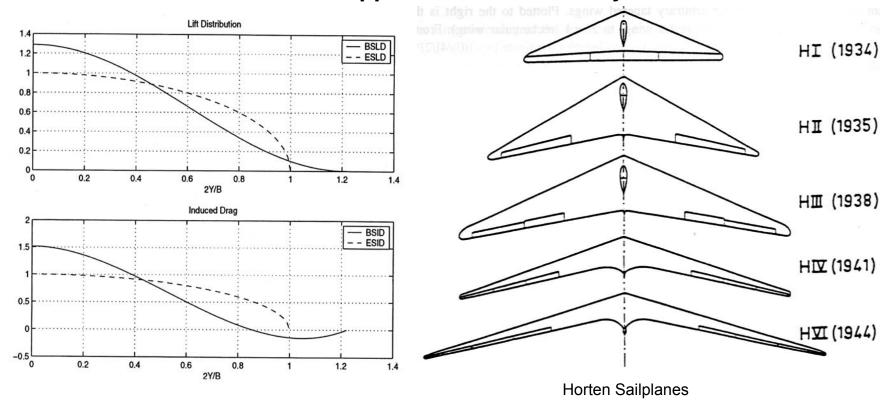
- Elliptical spanload (1914)
- "the downwash produced by the longitudinal vortices must be uniform at all points on the aerofoils in order that there may be a minimum of drag for a given total lift." y = c

Minimum Induced Drag & Bending Moment



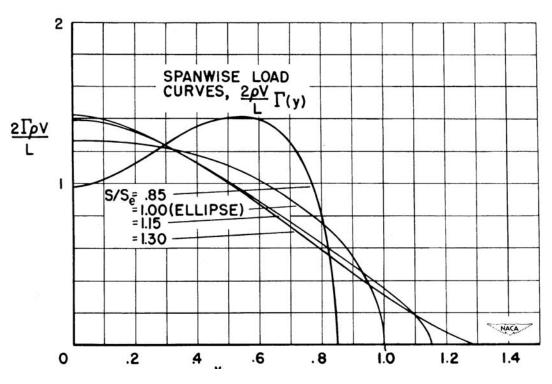
Prandtl (1932)
 Constrain minimum induced drag
 Constrain bending moment
 22% increase in span with 11% decrease in induced drag

Horten Applies Prandtl's Theory



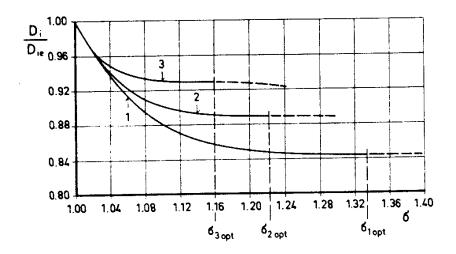
 Horten Spanload (1940-1955) induced thrust at tips wing root bending moment

Jones Spanload



- Minimize induced drag (1950)
 Constrain wing root bending moment
 30% increase in span with 17% decrease in induced drag
- "Hence, for a minimum induced drag with a given total lift and a given bending moment the downwash must show a linear variation along the span." y = bx + c

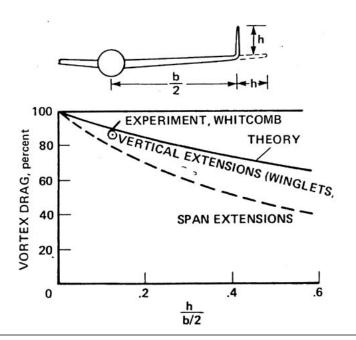
Klein and Viswanathan

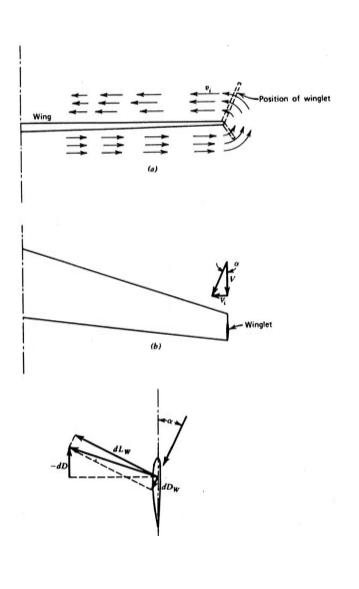


- Minimize induced drag (1975)
 Constrain bending moment
 Constrain shear stress
 16% increase in span with 7% decrease in induced drag
- "Hence the required downwash-distribution is parabolic." $y = ax^2 + bx + c$

Winglets

- Richard Whitcomb's Winglets
 - induced thrust on wingtips
 - induced drag decrease is about half of the span "extension"
 - reduced wing root bending stress





Spanload Summary

Prandtl/Munk (1914)

Elliptical

Constrained only by span and lift

Downwash: y = c

Prandtl/Horten/Jones (1932)

Bell shaped

Constrained by lift and bending moment

Downwash: y = bx + c

Klein/Viswanathan (1975)

Modified bell shape

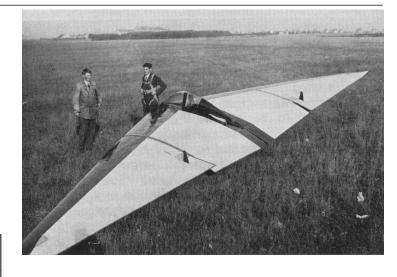
Constrained by lift, moment and shear (minimum structure)

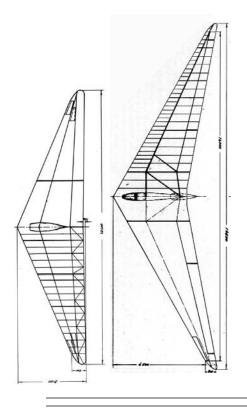
Downwash: $y = ax + bx + c^2$

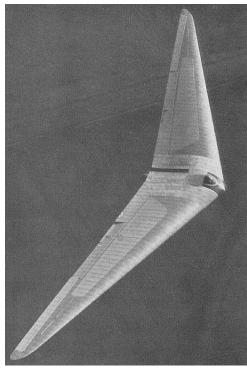
- Whitcomb (1975)
 - Winglets
- Summarized by Jones (1979)

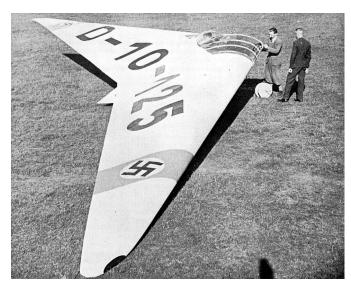
Early Horten Sailplanes (Germany)

- Horten I 12m span
- Horten II 16m span
- Horten III 20m span



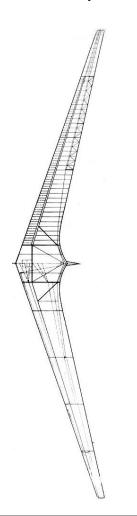


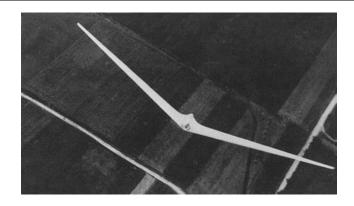


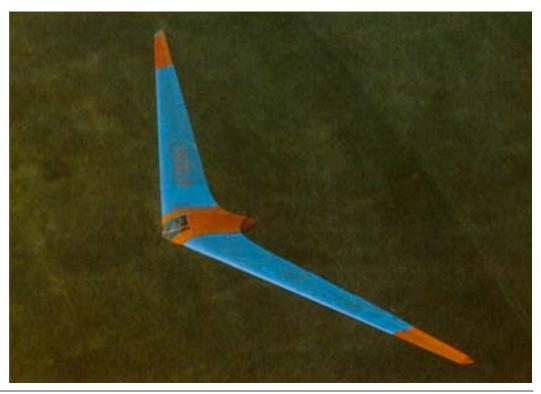


Horten Sailplanes (Germany)

- H IV 20m span
- H VI 24m span

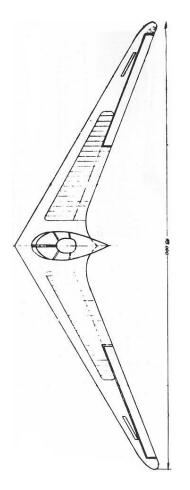


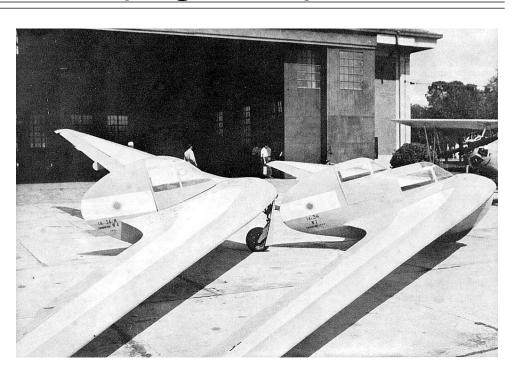




Horten Sailplanes (Argentina)

- H I b/c 12m span
- H XV a/b/c 18m span

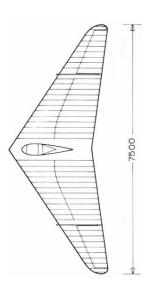


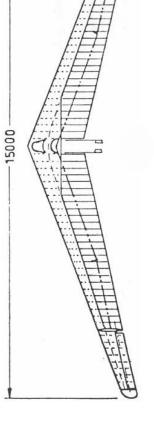


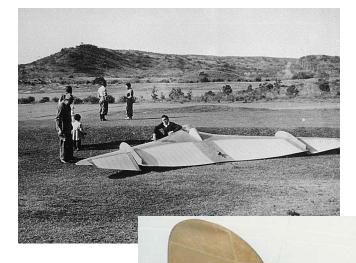


Later Horten Sailplanes (Argentina)

H Xa/b/c7.5m,10m, &15m











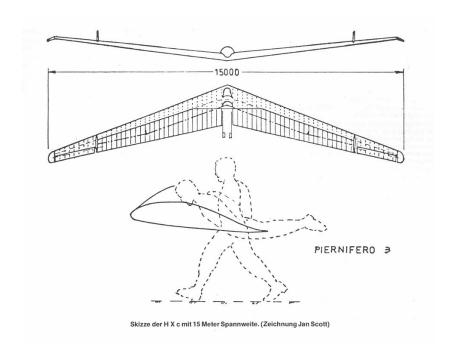
Bird Flight Model

- Minimum Structure
- Flight Mechanics Implications
- Empirical evidence
- How do birds fly?



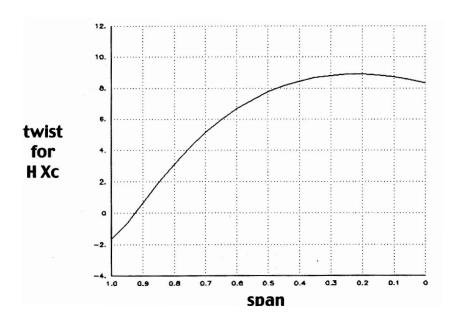
Horten H Xc Example

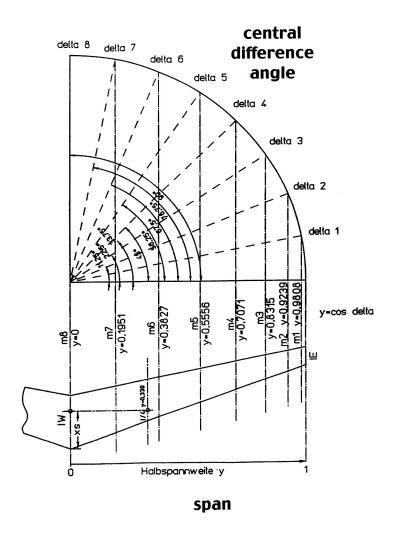
 Horten H Xc footlaunched ultralight sailplane 1950



Calculation Method

- Taper
- Twist
- Control Surface Deflections
- Central Difference Angle

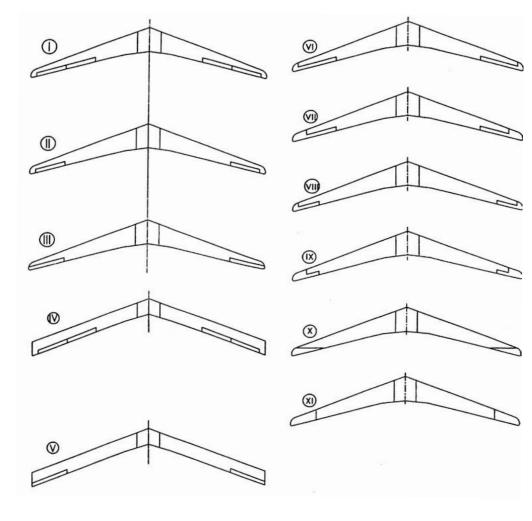




Dr Edward Udens' Results

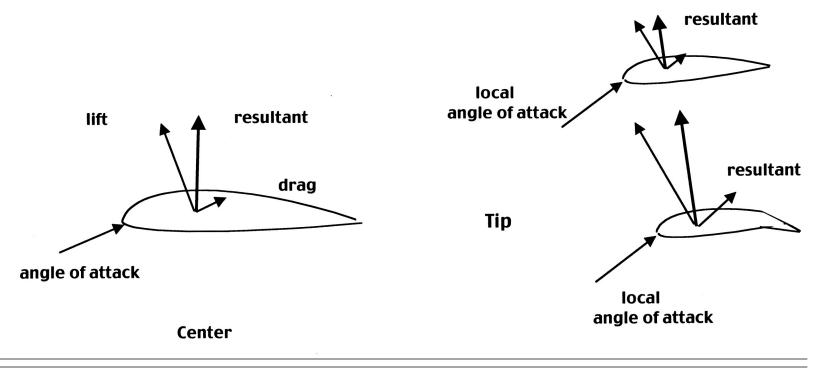
- Spanload and Induced Drag
- Elevon Configurations
- Induced Yawing Moments

Elevon	Config	Cn∂a	Spanload	
1	00	02070	bell	
H	.00	01556	bell	
Ш	.00)2788	bell	
IV	0	19060	elliptical	
V	0	15730	elliptical	
VI	.00	01942	bell	
VII	.00	02823	bell	
VIII	.00	04529	bell	
ΙX	.00	05408	bell	
X	.00	04132	bell	
ΧI	.00	05455	bell	



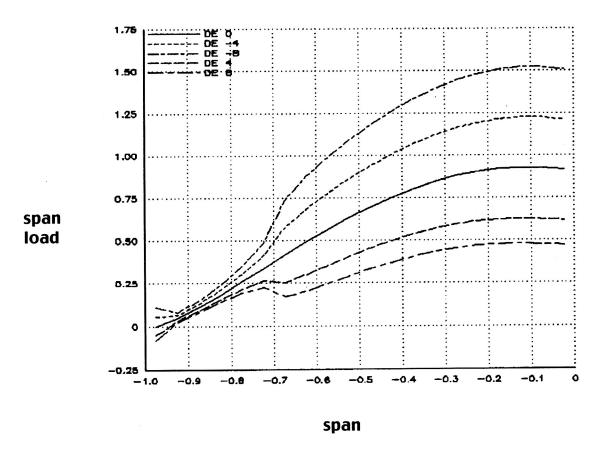
Horten H Xc Wing Analysis

- Vortex Lattice Analysis
- Spanloads (longitudinal & lateral-directional) trim & asymmetrical roll
- Proverse/Adverse Induced Yawing Moments handling qualities
- Force Vectors on Tips twist, elevon deflections, & upwash
- 320 Panels: 40 spanwise & 8 chordwise



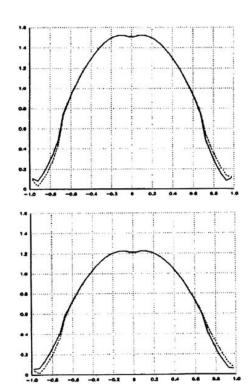
Symmetrical Spanloads

- Elevon Trim
- CG Location

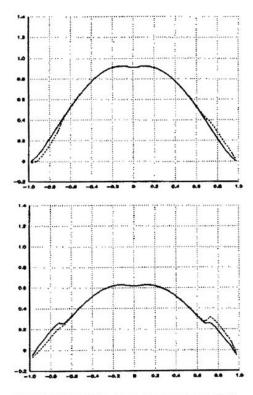


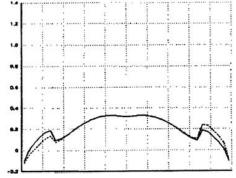
Asymmetrical Spanloads

- Cl∂a (roll due to aileron)
- Cn∂a (yaw due to aileron) induced component profile component change with lift
- Cn∂a/Cl∂a
- CL(Lift Coefficient)
 Increased lift:
 increased Cl
 increased Cn
 increased lift:
 decreased Cl
 decreased Cn
 increased Cn
 increased Cl
 increased Cn
 in



CL	Cl	Cn
.966	.01384	.00055
.774	.01384	.00037
.582	.01345	.00021
.390	.01384	.00003
.198	.01345	00015





Airfoil and Wing Analysis

- Profile code (Dr Richard Eppler)
- Flap Option (elevon deflections)
- Matched Local Lift Coefficients
- Profile Drag
- Integrated Lift Coefficients match Profile results to Vortex Lattice separation differences in lift
- Combined in MatLab

Performance Comparison

Max L/D: 31.9

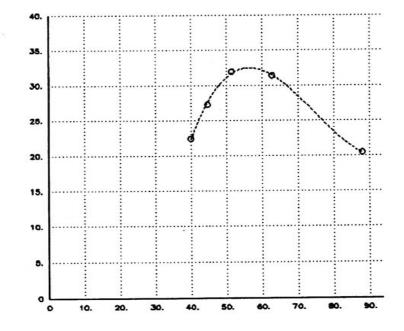
Min sink: 89.1 fpm

Does not include pilot drag

Prediicted L/D: 30

L/D

Predicted sink: 90 fpm



velocity

Horten Spanload Equivalent to Birds

- Bell Shaped Span Load is equivalent to bird span load (shear not considered in Horten designs)
- Flight mechanics are the same turn components are the same
- Both attempt to use minimum structure
- Both solve minimum drag, turn performance, and optimal structure with one solution

Concluding Remarks

- Birds as as the first model for flight
- Theortical developments independent of applications
- Applied approach gave immediate solutions, departure from bird flight
- Eventual meeting of theory and applications (applied theory)
- Spanload evolution (Prandtl/Munk, Prandtl/Horten/Jones, Klein & Viswanathan)
- Flight mechanics implications
- Hortens are equivalent to birds
- Thanks: Juliana Plumb, Dr Bob Liebeck, Nalin Ratnayake, Kia Davidson, Mike Allen, Walter Horten, Georgy Dez-Falvy, Rudi Opitz, Bruce Carmichael, R.T. Jones, Russ Lee, Phil Barnes, Dan & Jan Armstrong, Dr Phil Burgers, Ed Lockhart, Andy Kesckes, Dr Paul MacCready, Reinhold Stadler, Edward Udens, Dr Karl Nickel & Jack Lambie

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