

Variations in Cathodoluminescent Intensity of Spacecraft Materials Exposed to Energetic Electron Bombardment

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Abstract—Many contemporary spacecraft materials exhibit cathodoluminescence when exposed to electron flux from the space plasma environment. A quantitative, physics-based model has been developed to predict the intensity of the glow as a function of incident electron current density and energy, temperature, and intrinsic material properties. We present a comparative study of the absolute spectral radiance for several types of dielectric and composite materials based on this model which spans three orders of magnitude. Variations in intensity are contrasted for different electron environments, different sizes of samples and sample sets, different testing and analysis methods, and data acquired at different test facilities. Together, these results allow us to estimate the accuracy and precision to which laboratory studies may be able to determine the response of spacecraft materials in the actual space environment. It also provides guidance as to the distribution of emissions that may be expected for sets of similar flight hardware under similar environmental conditions.

Index Terms—cathodoluminescence, light emission, materials testing, electron flux, space environment effects

I. INTRODUCTION

Many highly disordered insulating materials used in spacecraft construction can exhibit electron-induced glow or cathodoluminescence when exposed to the space plasma environment [1]. Determinations of the absolute and relative cathodoluminescent intensity of spacecraft materials per incident electron flux are essential to predict and mitigate consequences for optical detection [2] and for stray light contamination in space-based observatories [1,3]. They also

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provide important information about the defect structure and electron transport properties of these materials [4-8].

Previous studies have focused on how the relative spectral radiance of cathodoluminescent materials varies with changes in environmental conditions, including electron energy, current density, absorbed power density, and temperature. This has led to the development of a quantitative, physics-based model to predict the intensity of glow as a function of incident electron current density and energy, temperature, and intrinsic material properties [1,3,7,9]. However, from a practical point of view, it is also important to develop an understanding of the variations of the cathodoluminescent intensity of diverse spacecraft materials exposed to energetic electron bombardment in both the space environment and space simulation studies. This is the focus of this paper.

We present results of ground-based measurements simulating space-induced cathodoluminescence from a wide variety of thin film dielectric and nanodielectric composite samples. Comparisons of the absolute spectral intensities per incident electron flux for these materials show three orders of magnitude variation. Variations in intensity are contrasted for different incident electron current densities and energies, different sample sizes and thicknesses, different testing and analysis methods, and data acquired at different test facilities. We also report on the variability of cathodoluminescence for a large set of similar epoxy samples exposed simultaneously to similar space-like monoenergetic electron flux conditions. The observed statistical fluctuations provide assessment of the instrumentation precision, the variation between samples, and the stochastic variations inherent to the material. The combined results of studies of numerous similar samples led to higher precision results that allow for quantification of additional materials properties.

II. MODEL OF CATHODOLUMINESCENT INTENSITY

The model developed for the observed electron-induced luminescence phenomenon is based on band theory of highly disordered insulating materials [3,7,10]. The observed luminescence occurs when an incident high energy, charged particle undergoes a series of inelastic collisions exciting valence band electrons into the conduction band. The excited electrons rapidly decay to localized (shallow trapped) states, with a mean binding energy ϵ_{ST} below the mobility edge. A final electron transition, from the short-lived shallow trap states to longer-lived deep trap states is the origin of the emitted photon. The model predicts that the overall luminescent intensity I_l scales with incident current density

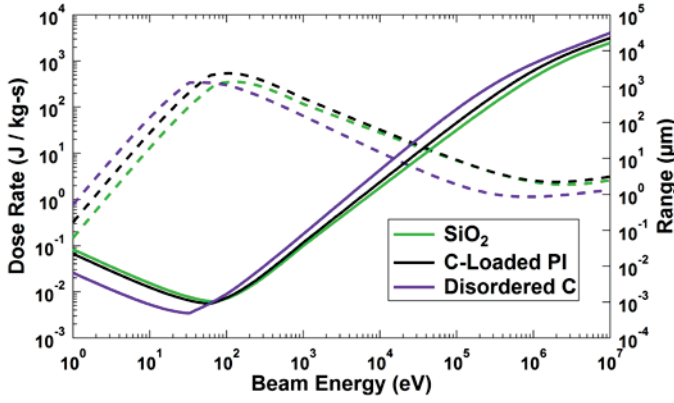


Fig. 1. Range (solid curves) and dose rate (dashed curves) of three disordered materials (SiO_2 , carbon-loaded polyimide, and graphitic amorphous carbon) as a function of incident electron energy using calculation methods and the continuous slow-down approximation described in Wilson *et al.* [14].

J_{inc} , incident beam energy E_{inc} , temperature T , and photon wavelength λ as

$$I_\gamma(J_{inc}, E_{inc}, T, \lambda) \propto \frac{\dot{D}(J_{inc}, E_{inc})}{\dot{D} + \dot{D}_{sat}} \left\{ \left[e^{-(\epsilon_{ST}/k_B T)} \right] \left[1 - e^{-(\epsilon_{ST}/k_B T)} \right] \right\} \times \left\{ \left[1 - A_f(\lambda) \right] \left[1 + \mathbb{R}_m(\lambda) \right] \right\}. \quad (1)$$

The dose rate \dot{D} (absorbed power per unit mass) is given by

$$\dot{D}(J_{inc}, E_{inc}) = \frac{J_{inc} E_{inc} [1 - \eta(E_{inc})]}{q_e \rho_m} \times \begin{cases} [1/L] & ; R(E_{inc}) < L \\ [1/R(E_{inc})] & ; R(E_{inc}) > L \end{cases}. \quad (2)$$

q_e is the electron charge, ρ_m is the mass density of the material, $\eta(E_b)$ is the contribution of backscattered yield, and L is the sample thickness. \dot{D}_{sat} is the material-dependent saturation dose rate. The exponential terms in Eq. (1) account for temperature dependence [3]. The last two λ -dependant terms correct for photon absorption within the luminescent material and reflection from any underlying coating [11]. A more detailed discussion of the model is given in [1]. This work focuses on the dependence of spectral radiance on J_{inc} , E_{inc} , and the range of the deposited electrons, $R(E_{inc})$.

The dependence of the spectral radiance on incident current density, J_{inc} , in Eq.(1) is through the dependence on dose rate; $I_\gamma(J_{inc}) \propto \dot{D}(J_{inc}) / [\dot{D}(J_{inc}) + \dot{D}_{sat}] \propto J_{inc} / [J_{inc} + J_{sat}]$. At low dose rates ($\dot{D} \ll \dot{D}_{sat}$), I_γ is linearly proportional to J_{inc} . At higher current densities ($\dot{D} \gg \dot{D}_{sat}$), saturation occurs when trap states fill, limiting the number of states electrons can decay into; I_γ approaches a constant material-specific saturation intensity. Such saturation effects, at increasing current densities and fixed incident energies, have been reported for disordered SiO_2 [3], nanodielectric carbon-loaded polyimide [9], cyrate ester/graphite fiber composites [12], and bisphenol/amine epoxy [1,13].

The energy dependence of the spectral radiance is more complicated, due to the energy-dependent penetration depth or range, $R(E_{inc})$, in Eq. (2). For nonpenetrating radiation—where the energy-dependent penetration depth or range, $R(E_{inc})$, is less than the film thickness L —all incident power is absorbed in the material. At low incident power, both \dot{D} and I_γ are linearly proportional to the incident energy and

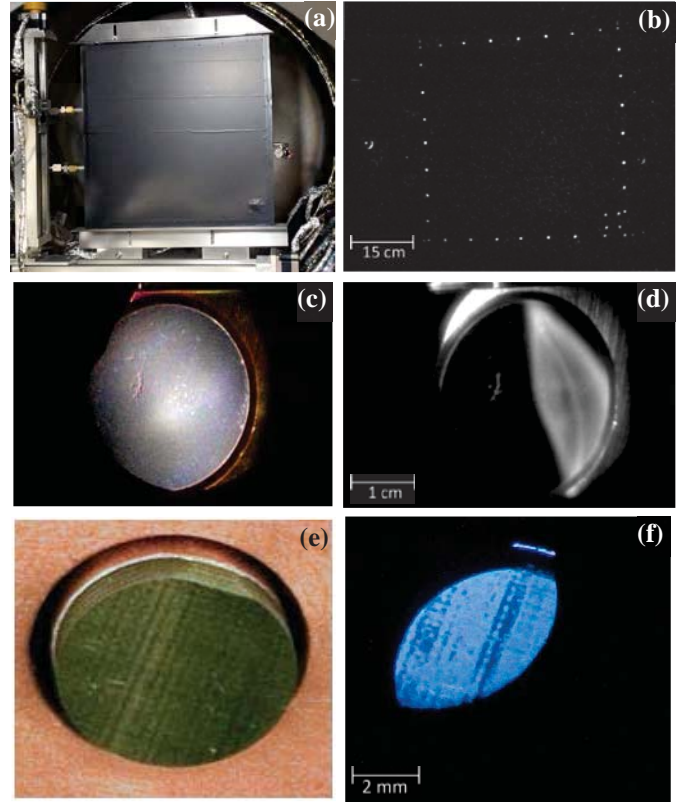


Fig. 2. Sample images in ambient light (left) and under electron bombardment (right) showing variations in sample composition, size and facility. (a-b) 41x41 cm sample of carbon-loaded polyimide mounted in the MSFC test chamber, with 36 epoxy glue dots luminescing under electron flux. (c-d) 2.5 cm diameter sample of thin disordered SiO_2 coating on Au-coated mirror mounted in the USU SEEM test chamber. (d) Image with the beam focus adjusted so that electrons impinge and cathodoluminescence is evident only on the right side of the sample. (e-f) 1 cm diameter sample of cyrate ester/graphite fiber composite at USU. Striations in the images result from the composite fiber structure of the material. (f) Image with the electron beam offset to the top left, limiting cathodoluminescence to this quadrant. (b) and (d) are CCD video frame images; all other images are SLR still color photographs.

power density, $(J_{inc} E_{inc} / q_e)$. At higher incident power, both \dot{D} and I_γ exhibit saturation effects for increasing energy and fixed current density. For penetrating radiation—where $R(E_{inc}) > L$ —the *absorbed* power is reduced by a factor of $[L/R(E_{inc})]$ [14] leading to a similar dependence for I_γ . Fig. 1 shows the range and dose for select disordered materials as functions of incident energy.

An energy-dependent correction to the incident flux, $J_{inc} [1 - \eta(E_{inc})]$, is also included in Eq. (2) to account for quasi-elastic backscattered electrons that do not deposit substantial energy; $\eta(E_{inc})$ is the backscattered electron yield [11]. For the most part, this correction is small and weakly dependant on energy. For biased samples, or when excess charge is stored in the trap states, a surface voltage V_s results and E_{inc} is replaced everywhere in Eqs. (1) and (2) by the landing energy, $(E_{inc} - q_e V_s)$.

III. CATHODOLUMINESCENT VARIATIONS

A. Experimental Test Methods and Facilities

Cathodoluminescence tests used well-characterized, uniform, large-area, approximately normal-incidence, monochromatic electron beams to irradiate tests samples. The

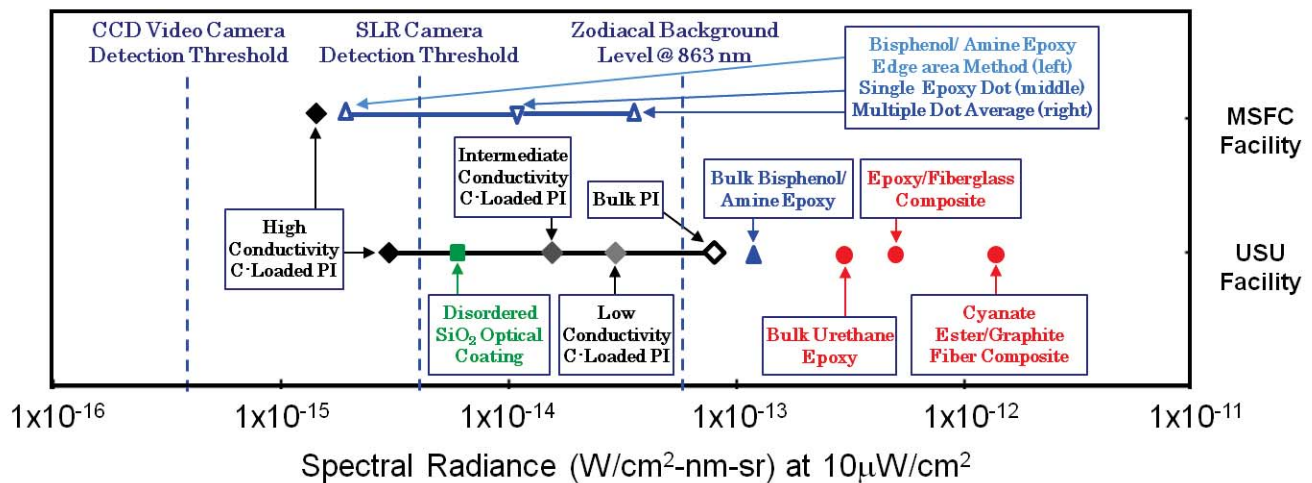


Fig. 3. Measured absolute cathodoluminescent intensities for ~ 10 keV electron bombardment scaled to $10 \mu\text{W}/\text{cm}^2$, representative of severe space environments. Data acquired using the CCD video camera (863 nm weighted central wavelength and 500 nm bandwidth). The materials shown—in approximate order of increasing intensity—are: three levels of decreasing carbon loading of polyimide from high to low conductivity and bulk polyimide (black squares); disordered SiO_2 optical coatings (green); neat bisphenol/amine and urethane epoxies (blue); and composite resin fiber materials including cyanate ester/ graphite fiber, urethane epoxy/carbon fiber, and epoxy/fiberglass composites (red). Measurements at the two test facilities are identified at right. Three data analysis methods are compared for bisphenol/amine samples; these range over more than two orders of magnitude, illustrating the need for well designed test methods. The spectral radiance for the zodiacal background stray light intensity at 863 nm is shown for comparison (dashed blue line) [17], as are the detection thresholds of the cameras at the MSFC facility [1].

samples were in high vacuum conditions, held at fixed temperatures that could be controlled to cryogenic levels. Results presented here used two optical detectors: (i) an image-intensified CCD video camera (Xybion, ISG-780-U-3; ~ 400 -900 nm bandwidth and 830 nm peak wavelength), and (ii) a single lens reflex CCD still camera (Canon, EOS Rebel XT DS126071; ~ 390 -650 nm bandwidth and 553 nm peak wavelength) [1]. The cameras were calibrated on an absolute scale using NIST traceable sources; their detection threshold sensitivities are noted in Fig. 3. In addition to the optical detectors, picoammeters measured current through the sample, monitored the mounting stage current, and measured beam currents.

Figure 2 shows some examples of materials tested and CCD video camera and SLR still camera color images of the cathodoluminescence. In Fig. 2(d) cathodoluminescence is evident only on the right side of the SiO_2 sample, where the beam has been focused. Figure 2(f) of a cyanate ester/graphite fiber composite sample shows a uniform circular electron beam offset to the top left, limiting cathodoluminescence to this quadrant.

Measurements were conducted at two independent facilities: the Environment Effects Laboratory at NASA Marshall Space Flight Center (MSFC) and the Space Environment Effects Materials (SEEM) test facility at Utah State University (USU).

USU testing uses a $\sim 1 \text{ m}^3$ ultrahigh vacuum chamber ($\sim 10^{-6}$ Pa) equipped with a high energy electron gun with a focused beam (5-30 keV at 0.1 -1000 nA/cm^2 flux) [15]. Temperatures from ~ 50 K to ~ 350 K were used for cathodoluminescence tests [16]. Samples from <1 cm to ~ 3 cm diameter were tested. Additional NIR-IR and mid-IR cameras and detectors, UV/Vis/NIR spectrometers, and electron emission measurement capabilities were used for some measurements [1].

MSFC testing used a larger $\sim 2 \text{ m} \times 1 \text{ m}$ diameter ultrahigh vacuum chamber ($\sim 10^{-6}$ Pa) able to accommodate large (up to 41×41 cm) flight samples. It is equipped with a high energy electron flood gun (1-100 keV at 1 -100 nA/cm^2 flux) with *in*

situ Faraday cups positioned on either side of the large sample to monitor the incident beam current (see Fig. 2(a)). Temperatures down to ~ 120 K were attained by mounting samples on an electrically-isolated liquid nitrogen reservoir.

Measurements at the two test facilities are identified separately in Fig. 3. Measurements for similar materials (bisphenol/amine and intermediate conductivity carbon-loaded polyimide samples) show agreement to within a factor of ~ 2 -3. This is reasonable agreement given the differences in sample materials, temperatures, test methods, instrumentation, and electron bombardment conditions for the different tests. However, it also serves as an indication of the uncertainties associated with ground-based testing.

B. Variations with Material

Figure 3 shows a comparison of measured absolute cathodoluminescent spectral radiances for different spacecraft materials, which spans approximately three orders of magnitude. These different results for varied current, keV electron bombardment have been linearly scaled to $10 \mu\text{W}/\text{cm}^2$ incident electron power densities, which is representative of severe space environments. The materials tested include: polyimide films, neat urethane and bisphenol/amine epoxy films; bulk and thin optical coatings of disordered SiO_2 ; several grades of commercially available high-conductivity carbon-loaded polyimide nanodielectric composites; cyanate ester and urethane epoxy resins in graphite fiber and fiberglass composites; and multilayer dielectric/conductor composites.

In general terms, we found that the relative cathodoluminescence for a given electron flux ranks from lowest to highest intensity for polyimide nanodielectric composites, disordered SiO_2 , bulk polyimide, bulk epoxy materials, and epoxy resin composites. Polyimide and carbon-loaded polyimide exhibit relatively weak cathodoluminescent intensities, with the intensity decreasing with carbon content. As a point of comparison, note that these absolute spectral

intensities for isolated samples exposed to electron fluxes comparable to solar wind intensities span the intensity of the zodiacal background in the visible and near infrared wavelength range (vertical dashed line of Fig. 3) [17]; this relative comparison of intensities to the zodiacal background is most important for space-based observatories, where the zodiacal background can be a significant source of external light contamination [1]. Also note that these measured intensities are greater than the scaled CCD video camera detection threshold.

Figure 4 shows three cathodoluminescence spectra typical of spacecraft materials which are all similar in the visible region, and exhibit multiple peaks indicative of multiple types of defects. The cynate ester [12] and SiO₂ [3] spectra were acquired at USU; the epoxy spectra is from a different facility [6].

C. Variation with Energy and Penetration Depth

The energy dependence of cathodoluminescence scales as a saturation function of the dose rate (see Eq. (1)) For nonpenetrating radiation, the dose rate (see Eq. (2)) scales linearly with energy with a small—usually negligible—correction term for the energy dependence of the electron backscatter yield. Figure 5 shows spectral radiance versus incident energy curves for two bulk materials—cynate ester/graphite fiber composite (red circle) [12], and bisphenol/amine epoxy (blue triangles) [13]—where the sample is thick enough that all the incident electrons are deposited. These increase linearly with energy at low incident power density, but reach saturation limits at higher power densities ($\sim 10^3 \mu\text{W}/\text{cm}^2$ for the cynate ester and $\sim 230 \mu\text{W}/\text{cm}^2$ ($\pm 70\%$) for bisphenol materials). The bisphenol data fit by the linear curve in Fig. 5 (blue triangles) does not show appreciable saturation, while other data (blue inverted triangles) shows significant saturation effects. Saturation of bisphenol/amine epoxy is also evident in Fig. 6 at lower power

densities. The saturated spectral radiance curve (blue curve, with a saturation power density of $360 \mu\text{W}/\text{cm}^2$ ($\pm 30\%$)) taken after the electron beam is turned on and after the sample has reached equilibrium deviates noticeably above $\sim 50 \mu\text{W}/\text{cm}^2$ from the linear spectral radiance curve (green curve) taken immediately after the electron beam is turned on and before saturation is reached.

For thin films, such as the $\sim 60 \text{ nm}$ SiO₂ optical coating in Fig. 5 (green curve), incident electrons above a threshold energy ($\sim 1.2 \text{ keV}$; see Fig.1) are able to penetrate all the way through the material. For energies above this penetrating dose rate power deposition decreases with increasing energy, so the spectral radiance also decreases. Radiance from thicker SiO₂ layers is found to increase linearly to higher energies and at higher dose rates exhibit saturation effects [4].

With composite materials, such as the carbon-loaded polyimide, the relationship between energy and cathodoluminescent intensity is more complicated. The black

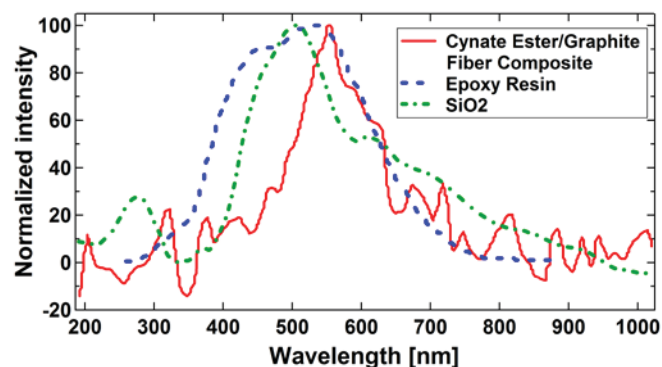


Fig. 4. Cathodoluminescent spectra of three highly disordered insulating materials. Materials shown are: cynate ester/graphite fiber composite (red solid curve) at $\sim 100 \text{ K}$ [12], epoxy resin at $\sim 295 \text{ K}$ (blue dashed curve) [6], and SiO₂-coated mirror at $\sim 269 \text{ K}$ (green dash-dotted curve) [3]. The spectra are normalized at maximum intensities and are not corrected for the wavelength-dependant relative detector sensitivity.

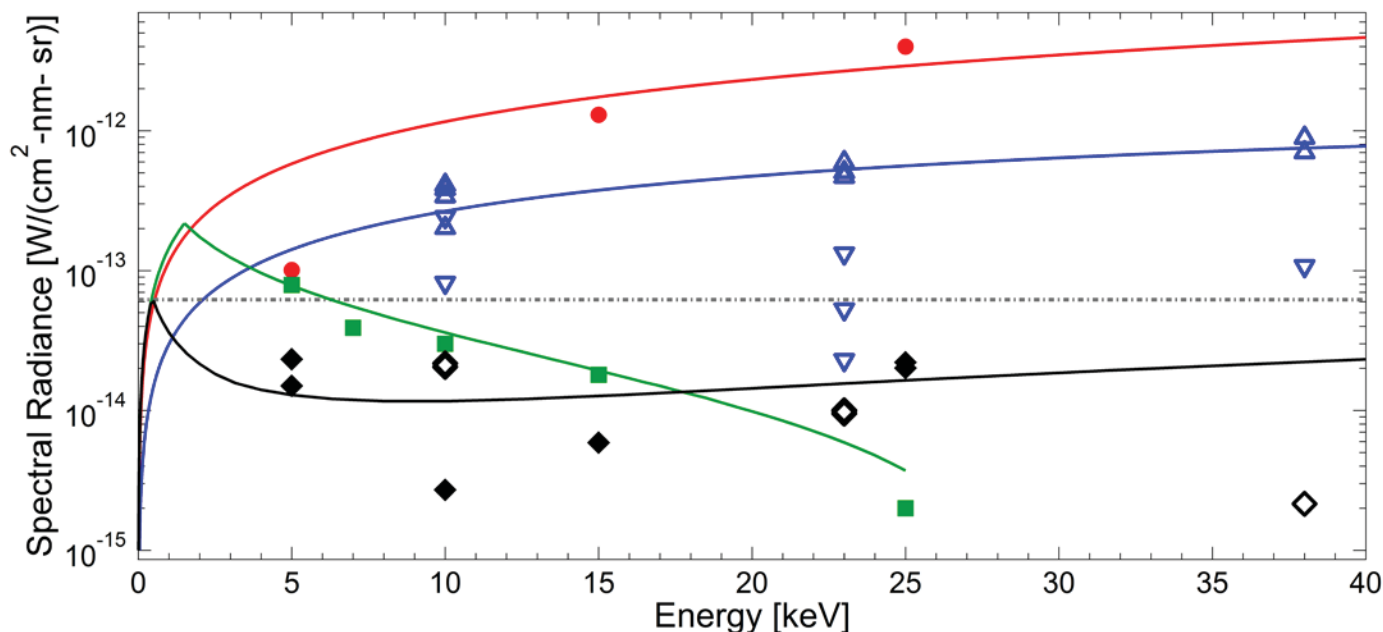


Fig. 5 Absolute cathodoluminescent spectral radiance versus incident electron energy of four materials, scaled to $10 \text{ nA}/\text{cm}^2$ electron current density. The plot shows data for SiO₂-coated mirror (green square) [3,4], carbon-loaded polyimide (black diamonds) [1,9], cynate ester/graphite fiber composite (red circle) [12], and bisphenol/amine epoxy (blue triangles) [1,13]. Data were taken with the CCD video camera at USU (solid symbols) and MSFC (open symbols). Fits are based on Eqs. (1) and (2). The approximate level of the zodiacal background stray light intensity at 863 nm is shown for comparison (dashed grey line) [17].

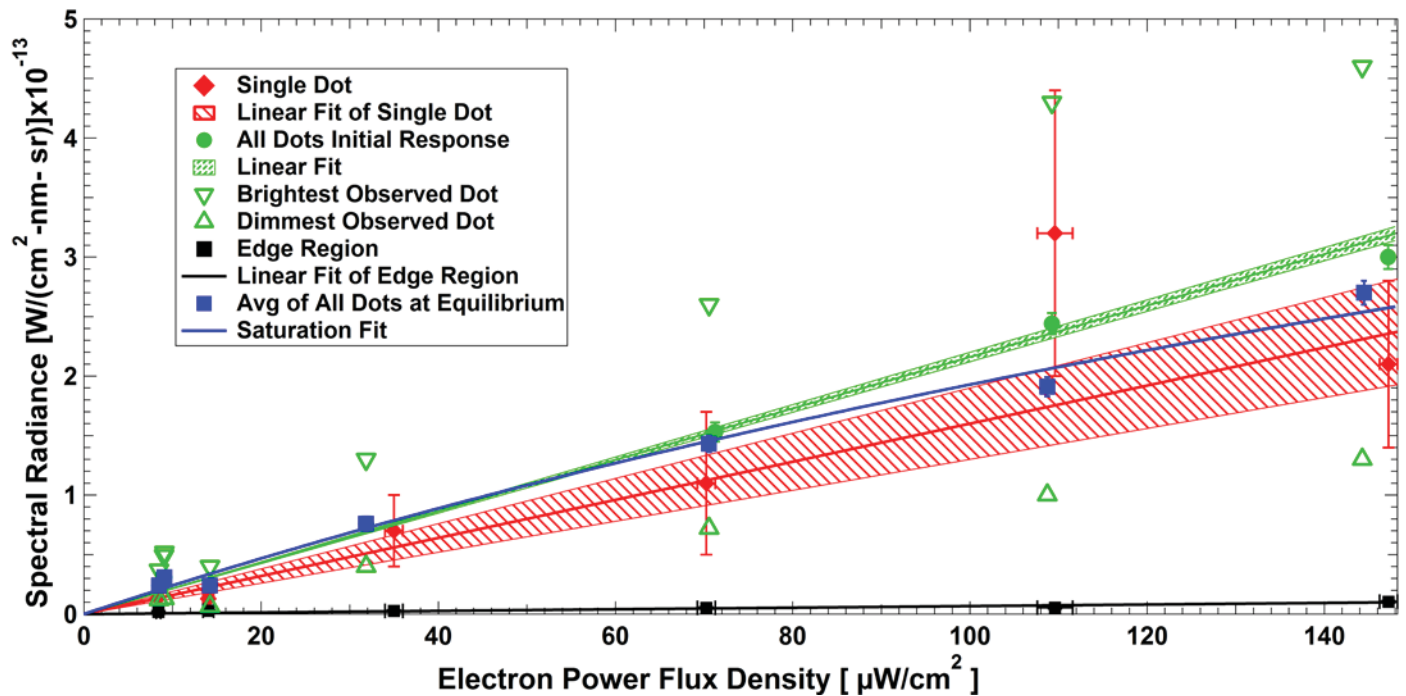


Fig. 6. Comparison of different methods to determine the absolute spectral radiance per incident electron power density as a function of incident electron energy for bulk bisphenol/amine epoxy samples. The slope of the linear fit, or conversion efficiency of high energy electron power to luminescent photon power, of 2.16×10^{-9} [W/(W-nm-sr)] ($\pm 2\%$) determined from the statistical analysis of 36 “glue dot” (green) is $\sim 35\%$ larger than from analysis of a single “glue dot” (red) and $\sim 32X$ larger than from using edge region analysis (black). The range of variations of the 36 sample data set is indicated by the $\sim \pm 5\%$ standard deviation (error bars) and $\sim \pm 60\%$ minimum to maximum range (green triangles). Errors for the spectral radiance and slope values for the linear fit of the single “glue dot” are $\sim 5X$ larger than for the analysis of all dots. Comparison for the multiple sample data set of green initial (unsaturated) and blue equilibrium (saturated) curves show saturation effect at higher dose rates. The fit for the saturated (blue) curve from Eq. (1) is of the form $I_{\nu} \propto \dot{D}/(\dot{D} + \dot{D}_{sat})$, with a proportionality constant of $9 \cdot 10^{-13}$ [W/(cm²nm²sr)] ($\pm 20\%$) and $D_{sat} = 1.5$ kGy/s ($\pm 30\%$) or $P_{sat} = 360$ μ W/cm².

curve in Fig. 5. is a linear superposition with $\sim 88\%$ of a penetrating curve (10 nm thickness, with ~ 350 eV penetration energy) that models thin polyimide layers above carbon particles and $\sim 12\%$ of a nonpenetrating curve (2 μ m thickness, with a penetration energy equal to the incident energy of ~ 10 keV) that models thick polyimide regions between the carbon particles. The relative surface areas of thin ($\sim 19\%$) and ($\sim 81\%$) thick polyimide regions determined with scanning electron microscopy are consistent with these estimates [18]. Even such a simple bimodal distribution of polyimide thicknesses predicts the relatively flat energy dependence of the spectral radiance curve observed at higher energies. A similar effect is seen qualitatively in Fig. 2(f) of the cynate ester/graphite fiber composite sample. Thicker regions of epoxy are lighter, while the thinner epoxy layers over graphite fibers are more intense and brighter blue in color.

D. Variations with Analysis Methods

Analysis of bisphenol/amine epoxy data taken at MSFC emphasizes the variation in results using three different analysis procedures [13]. Use of these different procedures to determine the absolute spectral radiance per incident electron power density as a function of incident electron energy, as shown in Fig. 6, produced results that differed by more than an order of magnitude.

The “edge region analysis” procedure defined a large square annular region that enclosed all 36 ~ 1 mm diameter “glue dot” regions of bulk epoxy as well as an $\sim 220X$ larger area of surrounding carbon-loaded polyimide (see Fig. 2(b)). As expected and seen in Fig. 3, the estimated spectral radiance

was much closer to that of carbon-loaded polyimide than bulk bisphenol/amine epoxy.

The “single dot analysis” procedure eliminated most of the contribution from carbon-loaded polyimide contamination by analyzing only a small region around a single epoxy dot. This procedure gives more accurate intensity results, but has a large statistical uncertainty since only ~ 15 pixels per frame comprising the single dot could be analyzed.

The most accurate results are obtained using the “multiple dot average” procedure. Data for all 36 epoxy dots individually are analyzed simultaneously using the single dot analysis; the statistical uncertainty is reduced by using the average value and associated standard deviation. As is readily apparent from Fig. 6, the multiple dot analysis results in much greater accuracy. Slopes of the linear fits in Fig. 6, or the spectral radiance per incident electron power density in [W/cm²-nm-sr] per [μ W/cm²], measure the conversion efficiency of high energy electron power to luminescent photon power. The slope of 2.16×10^{-9} [W/(W-nm-sr)] ($\pm 2\%$) from the statistical analysis procedure (green) is $\sim 35\%$ larger than from the single dot analysis (red) and $\sim 32X$ larger than from using edge region analysis (black). The multiple dot analysis result is the closest to the results measured at USU for a larger bulk sample, as shown in Fig. 2.

E. Variation of Similar Samples

Analysis multiple dots characterizes the variation between samples. The range of variations of the 36 sample data set is indicated by the $\sim \pm 5\%$ standard deviation (error bars) and $\sim \pm 60\%$ minimum to maximum range (triangles) shown in Fig.

6. The multiple dot analysis also results in much greater precision. Errors for the spectral radiance and slope values for the linear fit of the single dot procedure are $\sim 5X$ large than for the analysis with the multiple dot procedure.

When many samples are statistically analyzed, precise measurements can be made at low intensities and additional small effects can become apparent. It is evident from comparison of the curves and associated uncertainties in Fig. 6 that the saturation effects discussed in Sec. III.C at low dose rates would not be observable without the higher precision obtained with the multiple dot procedure. That is, the observed differences for the green unsaturated curve and blue saturated curve are greater than the uncertainties in the red single dot curve. The uncertainty in \dot{D}_{sat} was also reduced by more than a factor of 2.

IV. CONCLUSION

Cathodoluminescence is an important space environment-induced phenomenon to understand, especially in applications where extremely sensitive space-based optical detection is necessary. Measurements of the absolute spectral intensities per incident electron flux have been presented that confirm a quantitative, physics-based model to predict the intensity of the glow as a function of incident electron current density and energy, temperature, and sample thicknesses and composition. Comparisons for these materials show three orders of magnitude variation. For bulk nonpenetrating materials, spectral radiance increases with increasing incident electron power and flux. In thin films where electron penetration is possible, a linear relation is seen at low energies, but once penetration occurs intensity decreases with increasing energies. Composite materials, where both penetrating and nonpenetrating electrons effects were present, required a combination of these two effects in the model. Saturation effects at higher doses were observed and accurately modeled, for both penetrating and nonpenetrating electrons.

Statistical analysis of the observed statistical fluctuations of cathodoluminescence for a large set of similar epoxy samples exposed simultaneously to similar space-like monoenergetic electron flux conditions provided measures of both the instrumentation precision and the stochastic variations inherent to the material. The statistical analysis of the combined results of studies of numerous similar samples led to higher precision and accuracy results that allow for quantification of additional more subtle effects. Together, these results allow us to estimate the accuracy and precision to which laboratory studies may be able to determine the response of spacecraft materials in the actual space environment. It also provides guidance as to the distribution of emissions that may be expected for sets of similar flight hardware under similar environmental conditions.

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