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NASA DOEPOD NDE Capabilities Data Book

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Overview

This data book contains the Directed Design of Experiments for Validating Probability of Detection (POD) Capability of NDE Systems (DOEPOD) analyses of the nondestructive inspection data presented in the NTIAC, Nondestructive Evaluation (NDE) Capabilities Data Book [1]. DOEPOD is designed as a decision support system to validate inspection system, personnel, and protocol demonstrating 0.90 POD with 95% confidence at critical flaw sizes, a90/95. Although 0.90 POD with 95% confidence at critical flaw sizes is often stated as an inspection requirement in inspection documents, including NASA Standards [2], NASA critical aerospace applications have historically only accepted 0.978 POD or better with a 95% one-sided lower confidence bound exceeding 0.90 at critical flaw sizes, a90/95. (see Figure 11 of [3]).

The test methodology used in DOEPOD is based on the field of statistical sequential analysis founded by Abraham Wald,

"Sequential analysis is a method of statistical inference whose characteristic feature is that the number of observations required by the procedure is not determined in advance of the experiment. The decision to terminate the experiment depends, at each stage, on the results of the observations previously made. A merit of the sequential method, as applied to testing statistical hypotheses, is that test procedures can be constructed which require, on average, a substantially smaller number of observations than equally reliable test procedures based on a predetermined number of observations." A. Wald [4]

Details of the analysis methods used in DOEPOD are fully described in the DOEPOD [5] manual, and "Directed Design of Experiments for Validating Probability of Detection Capability of a Testing System" US Patent Serial Number: US 8,108,178. Additional details are available on the operation [6] [7] and proof property validation [7] of DOEPOD.

The critical importance of validating methodologies used for establishing POD have been highlighted [3] and this data book provides the DOEPOD validation of POD capabilities for NDE systems, materials, structures, and flaw types presented in the NTIAC, Nondestructive Evaluation (NDE) Capabilities Data Book [1].

The maximum likelihood estimation (MLE) method used in DOEPOD to estimate the probability of detection using a two parameter logit model (MLE-Logit) are identical to that used in NTIAC [1]. This MLE method was chosen as a verification of data integrity so that the MLE POD plots in NTIAC [1] and this data book are identical except where this data book provides a correction to NTIAC [1] analysis. Corrections to NTIAC [1] are indicated in the Errata listed at the end of this document. Other MLE-Logit methods may be used, and a simple grid search for maximizing parameters has been demonstrated [3] to be effective. The POD analysis methods of NTIAC [1] and a military handbook [8] use a predetermined number of observations.

It is noted here that the MLE-Logit POD curve fit plots shown in this data book and NTIAC [1] are not validated for implementation [3]. Internal and external validation of MLE-Logit POD estimates is required prior to implementation and initial guidance on validation procedures is provide elsewhere [3]. In contrast, if CASE 1, CASE 1+, CASE 1# identifications are identified by DOEPOD analyses of test data, then the system, personnel, and inspection protocol maybe considered for acceptance by engineering authority for implementation application on relevant systems

437 NTIAC data sets are analyzed by DOEPOD to yield a CASE identification for each data set. Possible CASE identifications are listed in Table 1. The reader is referred to the DOEPOD manual [5] for definitions of the parameters in Table 1, and for design of experiment instructions on how to proceed to validate systems and personnel inspection capability. The DOEPOD analysis highlights 72 NTIAC data sets has CASE 1, CASE 1+, or CASE 1# data sets all exhibit 0.978 POD or better with a 95% one-sided lower confidence bound exceeding 0.90 at critical flaw sizes and meet the historical NASA acceptance criteria when actions in Table 1 are addressed.

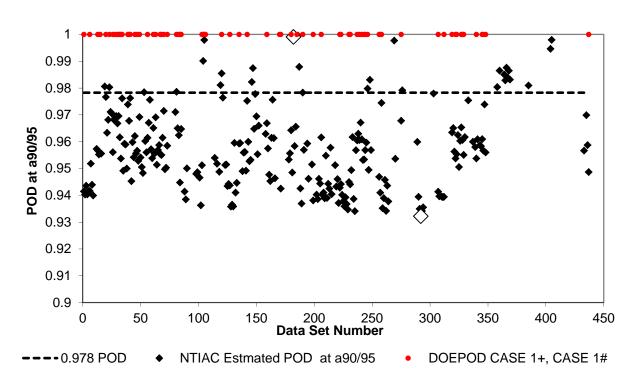
DOEPOD acronyms are defined at the end of this overview.

	Is 90/95 POD at X_{pod} reached? (i.e., lower confidence bound, X_{Best_LCL} , is equal to or greater than 0.9)	DOEPOD Analysis Summary and Recommendations
CASE 1	0	90/95 POD at X_{pod} has been reached. Actions: Address any false call warnings.
CASE 1+	0	90/95 POD at X _{pod} has been reached. Actions: Misses above Xpod need to be explained and resolved. Address any false call warnings.
CASE 1#	0	90/95 POD at X _{pod} has been reached. Actions: Further validation at flaw sizes greater than Xpod is required. Add large flaws. Address any false call warnings.
CASE 1*	0	90/95 POD at X _{pod} has been reached. Actions: Further validation at flaw sizes greater than Xpod is required. Add large flaws. Misses above Xpod need to be explained and resolved. Address any false call warnings.
CASE 2	0	90/95 POD at X_{pod} has been reached, however, there are an excessive number Misses above X_{pod} . Actions: Additional validation at identified flaw sizes is required. Add flaws per instructions.
CASE 4	0	90/95 POD at X_{pod} has not been reached. Actions: Increase number of flaws at $X_{\text{POH=1}}$ or X_{Best_LCL}
CASE 5	0	90/95 POD at X_{pod} has not been reached and there are Misses above X_{Best_LCL} . Actions: Increase the number of flaws at $X_{POH=1}$.
CASE 6	0	90/95 POD at X_{pod} has not been reached. The POH is fluctuating above X_{Best_LCL} and X_{poh} is greater than $X_L/3$. The inspection system is unstable for the flaw size range analyzed. Actions: Increase the flaw size range by a factor of two.
CASE 7	0	90/95 POD at X_{pod} has not been reached. The inspection system is unstable for the entire flaw size range analyzed. Actions: The inspection system may not be appropriate or increase the flaw size range by a factor of two.
SURVEY CASES	0	The optimized class width exceeds 1/3 XL and X_{pod} has not been reached. The class width optimization has determined that there is a class width for which the smallest X_{POH} =1 class length is identified. Actions: Add flaws at Survey/Optimum X_{POH}

Table 1

= NO

= YES



Logit-ML Estimated POD at a90/95

Figure 1. Logit-ML Estimated POD at critical flaw size, a90/95, from NTIAC (1997). Open diamonds refer to data sets each having 325 samples. The horizontal dashed line is the NASA minimum binomial estimated POD (0.978) accepted in practice at a flaw size, Xpod, for failure critical applications. DOEPOD analyses identified 72 (red disk) data NTIAC data sets that are classified as CASE 1+, or CASE 1# having estimated POD exceeding 0.978 at a flaw size, Xpod. Note that Xpod and a90/95 are flaw size inspection capability labelling designations for DOEPOD and NTIAC Data Books, respectively. Xpod and a90/95 do not necessarily refer to the same flaw size for the same data sets.

A top level summary of the DOEPOD analyses of the nondestructive inspection data presented in the NTIAC Data Book [1] is provide in Table 2. CASE 1+, CASE 1#, CASE 1*, and CASE 2 all exhibit at least one singular point where the one-sided lower 95% confidence bound on POD exceeds 0.90 at a critical flaw size and additional actions are needed per Table 2 instructions to complete the validation over a range of larger flaw sizes. CASE 4 data sets represent data sets that are similar to CASE 2 data sets, however additional data at selected flaws sizes is needed to move a CASE 4 data set to a CASE 2 data set. The CASE 5 data sets have excessive false negatives in the flaw size range tested, therefore data for larger flaw sizes is needed. CASE 6 data sets exhibit local instability over a portion of the flaw sizes tested, therefore data for larger flaw sizes is needed or the inspection system is inappropriate for the inspection required. CASE 7 data sets exhibit instability over the entire the flaw size range tested, therefore, therefor

inspection required.

CASE ID	Number of Data Sets	Action Needed
CASE 1+	2	Explain of observed false negatives
CASE 1#	71	Further validation at larger flaws. Add test specimens with larger flaws.
CASE 1*	80	Further validation at larger flaw. Add test specimens with larger flaws. Explain observed false negatives.
CASE 2	46	Add test specimens at identified flaw sizes to demonstrate POD to be monotonically increasing with flaw size
CASE 4	37	Increase amount of relevant data by adding test specimens at identified flaw sizes to establish acceptable POD
CASE 5	12	Add test specimens with increased flaw sizes to address excessive false negatives at smaller flaw sizes.
CASE 6	91	Add test specimens with flaw sizes at least twice as large to address local inspection system oscillation instability or utilize a different inspection system or method.
CASE 7	98	Add test specimens with flaw sizes at least twice as large to address global inspection system instability or utilize a different inspection system or method.

Table 2

A summary of the output of parameter values from the DOEPOD analysis of nondestructive inspection data and methods presented in the NTIAC Data Book [1] is listed in Table 3. The descriptions of the parameters in Table 3 are detailed in reference [5]. The data file name is in column 3 of Table 3 and is used to identify the companion DOEPOD analysis output file. The printouts of the DOEPOD analysis output files follow in alphabetic in order to facilitate location. The electronic DOEPOD analysis output files and a searchable summary of parameter values from the DOEPOD analysis (Table 3) are available in the companion CD-ROM entitled "NASA DOEPOD Nondestructive Evaluation (NDE) Capabilities Data Book" which may be obtained upon request from the publisher.

DOEPOD software is available from NASA by contacting Kathy A. Dezern, phone: 757.864.5704, email: <u>kathy.a.dezern@nasa.gov</u>

Example

As an illustrative example we examine the first data set A1001AL. The multi-parameter maximum likelihood analysis in the NTIAC NDE Capabilities Data Book indicates the inspection system to have a 0.94 POD with lower single-sided 95% confidence bound that exceeds 0.9 at 0.27" flaw size (column labeled "NTIAC 90/95 occurs at POD (inch)". In contrast, the NASA DOEPOD point estimate based method (no curve fitting) indicates that the acceptable capability of this inspection system is at or above the 0.61" flaws size (column labeled Xpod CLASSLENGTH) where 1.0 POD is estimated (column labeled POH or POD @Xpod) with a single-sided lower 95% confidence bound that exceeds 0.9 at 0.61" flaw size.

Examining the data analyses for A1001AL (page 20). There are five Misses (Xs) for the 72 flaws larger than the 0.27" flaw size yielding a 0.93 point estimate of POD for these grouped larger flaws with a single-sided lower 95% confidence bound of 0.83. The multi-parameter POD curve fit does not highlight these Misses as important. DOEPOD indicates that the POD capability for this system and for fracture critical inspections is at or above the 0.61" flaw size. Even then, DOEPOD analysis indicates [RED notes in chart] that additional large flaw data is needed to complete the validation before accepting the 0.61" flaw size capability of this inspection system, and that false call analysis is also required.

Accepting the 0.27" flaw size identified by multi-parameter maximum likelihood method as the detection capability of this inspection system for fracture critical inspections adds known risk as highlighted by the 0.93 point estimate of POD with a single-sided lower bound of 0.83 for the largest flaws. DOEPOD analysis indicates that the POD capability for this system and for fracture critical inspections is at or above the 0.61" flaw size.

DOEPOD DEFINITIONS

C _L	Class length, e.g., inspection parameter (length, depth, area, etc.)
C_{W}	Class width (width of the moving class; all flaws within the range C_L to C_L - $C_{W,}$ inclusively, are group together)
Hit	Flaw is detected
Miss	Flaw is not detected
MLE	Maximum Likelihood Estimate of POD using a two parameter statistical model. The MLE is included in DOEPOD as a user request for comparison. <i>The included method is that of the</i> NDE Capabilities Data Book, 3rd ed., Nov. 1997, NTIAC DB-97-02, DoD. <i>The use of MLE estimated POD is not recommend unless a full validation of the estimated POD is performed (see Generazio, E. R., Interrelationships Between Receiver/Relative Operating Characteristics Display, Binomial, Logit, and Bayes' Rule Probability of Detection Methodologies, NASA-TM-2014-21818, April 2014.</i>
Need	Add new samples to the existing specimen set in order to reach the number of samples required at the class length. Note that a single specimen may contain more than one flaw, so that "add samples" refers to "add flaws".
LCL	Lower confidence bound (value) of POH @ 95% confidence
Opt. X _{POH}	Optimum X_{POH} is identified for non-survey data sets. Optimum X_{POH} is the smallest class length and largest class width at which the minimum $X_{POH} = 1$ occurs. Optimum X_{POH} may be more aggressive than optional, X_{PODopt} , or X_{Best} _{LCL} , when the class width is constrained to the companion Optimum X_{POH} class width listed. DOEPOD does not force use of Optimum X_{POH} over X_{PODopt} or $X_{Best LCL}$ Stability has not been demonstrated at Optimum X_{POH} , therefore there is an additional risk that Optimum X_{POH} can not be satisfied to reach X_{POD}
РОН	Estimate of Probability of Hit (Number of Hits in Class Length/Total Number of Trials in Class Length)
POD	Probability of Detection (the true POD obtained if an infinite number of samples are used)
Signal Amplitude	Scalar amplitude output of NDE inspection system

Survey Data Sets	Survey Data Sets are data sets that have a sparce or disperse collection of samples. The moving class width optimization has identified this data set as having limited applications where the classwidth has exceeded $X_L/3$ and X_{POD} has not been reached. An alternate optimization of X_{POH} is used to provide guidance. The Survey Set is the recommended initial set for DOEPOD.
Survey X _{POH}	Survey X_{POH} is only identified for data sets determined to be Survey Data Sets. Survey X_{POH} is the smallest class length and largest class width at which the minimum $X_{POH} = 1$ class length occurs. Survey X_{POH} is the minimum class length at which X_{POD} may be achieved when the class width is constrained to the companion survey class width listed. Survey X_{POH} is utilized in all cases in which a Survey Set is identified by DOEPOD.
$X_{\text{Best LCL}}$	Class length exhibiting the maximum or "best" LCL. The best class length is determined by increasing the moving class width until a maximum LCL is obtained
X _i	Class length X at point "i"
X _L	Largest class length in entire data set
X _m	Class length near the mid-point between the largest and the smallest class lengths having no Misses
X _P	90/95 POD or greater is achieve, by grouping numbers of specimens, for the range X_P to X_L . X_P is only provided when X_{POD} has been identified.
	For inspector qualification, X_P cannot be less than the largest flaw Missed. The class width of flaw set used for inspector qualification is listed as Inspector Classwidth @ Xp in the charts. The flaw sizes used for inspector qualification range from Xp to (Xp - Classwidth @ Xp).
X _{POD}	Class length at which the lower confidence bound (value) is 0.90 (90/95 POD) @ 95% confidence.
X _{POH=1} , X _{POH}	Class length where there are no Misses above this class length, and $POH = 1$ above this class length.
X _{PODopt}	Optional existing smaller class length where X_{POD} may also be achieved if additional samples are added and Hits are identified.
X _S	Smallest class length in the data set
UCL	Upper confidence bound (value) of the false call rate @ 95% confidence

**Validated 90/95 POD has been reached at a classlength, X_{POD}. In order to achieve 90/95 POD for the class length range between X_{POD} and the largest class length in the data set, X_{L_2} inclusively, validation at a classlength near the mid-point and largest classlength is required^{ς}. If, in addition, there exists a class length, X_P, where 90/95 POD or greater exits for all class lengths in the range X_P to X_L , and $X_P = X_{POD}$, and there is a sufficient number and adequate range and distribution of classlengths greater than X_{POD} , then the validation extends from X_{POD} to X_{L} . When this occurs, validation at a classlength near the mid-point and largest classlength is satisfied. ^EWARNING: There are inspection systems that exhibit an oscillating or non-uniform POD. For example when the flaws are greater than the eddy current footprint, when large flaws are loaded to closure, or when the physics of the inspection processes changes modes over the flaw size range of interest. If flaws in these ranges or conditions are to be detected with a 90/95 POD, then samples in these ranges need to be included. When multiple base parameters are combined, e.g., (length)x(width) = area, and the combine parameter (e.g., area) is used as the class length, then 90/95 POD is only valid if the inspection technology has been validated to quantitatively measure each of the base parameters, or if the inspection technology is validated to guantitatively measure the new combine parameter. When all CASE 1 or CASE 1+ requirements are met, and the above warnings have been evaluated and the upper confidence bound of the false call rate is not excessive, then the inspection system is validated between X_{POD} and the largest class length X_L for the flaw types, materials, and structure of the test specimen set. Validated is defined here to be: "This confidence bound procedure has a probability of at least 0.95 to give a lower bound for the 90% POD point that exceeds true (unknown) 90% POD point. This is referred to as 90/95 POD, and for larger flaws in the evaluation range 90/95 POD is met or exceeded. DOEPOD SOFTWARE AND ANY ACCOMPANYING DOCUMENTATION IS RELEASED "AS IS". THE U.S. GOVERNMENT MAKES NO WARRANTY OF ANY KIND, EXPRESSED OR IMPLIED, INCLUDING, WITHOUT LIMITATION, ANY WARRANTIES OF MERCHANTABILITY AND FITNESS FOR A PARTICULAR PURPOSE. IN NO EVENT WILL THE U.S. GOVERNMENT BE LIABLE FOR ANY DAMAGES, INCLUDING ANY LOST PROFITS, LOST SAVINGS, OR OTHER INCIDENTAL OR CONSEQUENTIAL DAMAGES ARISING OUT OF THE USE, OR INABILITY TO USE THIS SOFTWARE OR ANY ACCOMPANYING DOCUMENTATION, EVEN IF INFORMED IN ADVANCE OF THE POSSIBILITY OF SUCH DAMAGES. THIS SOFTWARE MAY NOT BE MODIFIED, DISTRIBUTED, OR REPRODUCED.

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			Analysis CLASS- CLASS-	Best_LCL Best_LC L WIDTH	Best_LCL CLASS-										False Call	False Call	False Call	False Call	Length or Area per Inspection (in or in^2) =	False Call			NTIAC 90% POD occurs	NTIAC 90/95 occurs at POD (inch) XI	PO PC	DH or DD @ M	METHO
MATERIAL	STRUCTURE	FILE NAME		L WIDTH		XL#Xm	Xm # Xs 2	(s#Xici	Xicl # Xpoh	Xpoh #	2XL 2X	(L#Xss	Xss #		pt # UCL	Rate	Length (in)	Area (in^2)	(in or in^2) =	Opportunities False Calls	False Call Flag	MLE flag	at (inch)			bod	D
2219 AI T-87	plate	A1001AL.xis	6/4/15 5:14 PM CASE 1# 0.6100 0.2000 0.9050		0.979									0.5890	29						Warning: No false call analysis.		0.2	0.27	0.61	1.000	ET
2219 AI T-87	plate	A1001BL.XLS	6/4/15 5:16 PM CASE 2 0.3130 0.2000 0.9040		0.979	24 0.6460	29														Warning: No false call analysis.		0.185	5 0.25		0.961	ET
2219 AI T-87	plate	A1001CL.XLS	6/4/15 5:19 PM CASE 1* 0.3360 0.0570 0.9001		0.979	0.5430															Warning: No false call analysis.		0.3	0.41	0.496	1.000	ET
2219 AI T-87	plate	A1002AL.XLS	6/4/15 5:21 PM CASE 2 0.2980 0.0510 0.9001		0.979	22 0.4890	24														Warning: No false call analysis.		0.2	0.285		1.000	ET
2219 AI T-87	plate	A1002BL.XLS	6/4/15 5:22 PM CASE 1* 0.1080 0.0310 0.9001		0.979	0.3360															Warning: No false call analysis.		0.075	5 0.095	0.131	0.967	ET
2219 AI T-87	plate	A1002CL.XLS	6/4/15 5:25 PM CASE 1# 0.1530 0.0360 0.9001		0.979	0.5230								0 1520	29						Warning: No false call analysis.		0.275				ET
																					Warning: No false call	MLE Divergence Warning: Initial results					
2219 AI T-87	plate	A1003AL.XLS	6/4/15 5:27 PM CASE 1* 0.0760 0.0090 0.9077		0.610	0.2620															analysis.	listed.	0.055	0.065	0.096	1.000	ET
		A1003BL.XLS	6/4/15 5:30 PM CASE 1* 0.0830 0.0080 0.9001		0.610	0.2620															Warning: No false call	MLE Divergence Warning: Initial results		4 0.05	0.086	1.000	ET
2219 AI T-87	plate	A1003BL.XLS	6/4/15 5:30 PM CASE 1* 0.0830 0.0080 0.9001 6/4/15 5:34 PM CASE 1* 0.0830 0.0080 0.9001		0.610																analysis. Warning: No false call analysis.	listed.	0.04	1			ET
2219 AI T-87	plate					0.2620																	0.09		0.108	1.000	
2219 AI T-87	plate	A2002AL.XLS	6/4/15 5:36 PM CASE 7		0.5100						1.1000	29									analysis. Warning: No false call analysis.		0.29	++		-	ET
2219 AI T-87	plate	A2002BL.XLS	6/4/15 5:38 PM CASE 7	0.8609 0.2000	0.3720						1.1000	29				-					analysis. Warning: No faise call			──┼			ET
2219 AI T-87	plate	A2002CL.XLS	6/4/15 5:39 PM CASE 1* 0.4740 0.2000 0.9001		0.550																Warning: No false call analysis. Warning: No false call		0.095				ET
Ti 6Al4V	plate	A3001AL.XLS	6/4/15 5:40 PM CASE 1# 0.2250 0.0400 0.9001		0.407									0.2225	29						analysis. Warning: No false call		0.175	1			ET
Ti 6Al4V	plate	A3001BL.XLS	6/4/15 5:41 PM CASE 2 0.2650 0.0800 0.9001		0.407	70 57 0.3150	9																0.265	0.365		0.978	ET
Ti 6Al4V	plate	A3001CL.XLS	6/4/15 5:43 PM CASE 1# 0.2420 0.0420 0.9001		0.407	0.3550								0.2350	1						analysis. Warning: No false call analysis.		0.18	0.21	0.242	1.000	ET
Ti 6AJ4V	plate	A3003AL.XLS	6/4/15 5:43 PM CASE 7	0.8719 0.0270	0.2120						0.8140	29									Warning: No false call analysis.		0.275	0.36			ET
Ti 6AJ4V	plate	A3003BL.XLS	6/4/15 5:45 PM CASE 7	0.7411 0.0220	0.2470						0.8140	29									Warning: No false call analysis.		0.49				ET
Ti 6Al4V	plate	A3003CL.XLS	6/4/15 5:46 PM CASE 7	0.7942 0.0310	0.2470						0.8140	29									Warning: No false call analysis.		0.585				ET
SS AMS 355	hole	A400011.XLS	6/4/15 5:48 PMCASE 6	0.8190 0.0750		75 24			0.2	575 24	0.5150	29									analysis. Warning: No false call analysis.		0.12	0.185			ET
SS AMS 355	hole	A400013.XLS	6/4/15 5:49 PM CASE 1# 0.1031 0.0540 0.9001		0.257									0.1004	2						Warning: No false call		0.04		0.10314	1.000	ET
SS AMS 355	bole	A400014.XLS	6/4/15 5:50 PM CASE 6	0.6518 0.0070					0.1	559 28	0.5150	29									Warning: No false call analysis		0.095				ET
SS AMS 355	hole	A400014.XLS	6/4/15 5:51 PM CASE 5	0.5493 0.0030					0.0		0.0100	~~									Warning: No false call populatio		0.095				ET
SS AMS 355 SS AMS 355	hole	A400015.XLS	6/4/15 5:52 PM CASE 1# 0.1031 0.0540 0.9001	0.0493 0.0030	0.0579 0.257				0.0					0.1004	2						analysis. Warning: No false call analysis.		0.035		0.10214		ET
	noie	A500011.XLS	6/4/15 5:53 PM CASE 4	0.8855 0.0230				0.0	902 4 0.0		0.1803			0.1004	- 2						analysis. Warning: No false call		0.025		J.10314		ET
SS AMS 355	hole							0.0				29									analysis. Warning: No false call						
SS AMS 355	hole	A500013.XLS	6/4/15 5:55 PM CASE 6	0.7360 0.0050					0.0	339 27	0.0921	29			-	-					analysis. Warning: No false call analysis.		0.03				ET
SS AMS 355	hole	A500014.XLS	6/4/15 5:56 PM CASE 1# 0.0591 0.0180 0.9001		0.090									0.0579	2						analysis. Warning: No false call		0.03		0.05905	1.000	ET
SS AMS 355	hole	A500015.XLS	6/4/15 5:57 PM CASE 5	0.5493 0.0030		1 1			0.0	663 27						-					analysis. Warning: No false call		0.035	1			ET
SS AMS 355	hole	A500016.XLS	6/4/15 5:58 PM CASE 1# 0.0610 0.0250 0.9001		0.081									0.0587	3						analysis. Warning: No false call		0.03				ET
2024 AI T-37	lap splice	A6001A.XLS	6/4/15 5:59 PM CASE 1* 0.1140 0.0180 0.9001		0.812																		0.09			1.000	
2024 AI T-37	lap splice	A6001AR.XLS	6/4/15 6:00 PM CASE 1# 0.1140 0.0180 0.9001		0.812	0.2910								0.1060	3						analysis. Warning: No false call analysis.		0.09	0.095	0.114	1.000	ET
2024 AI T-37	lap splice	A6001B.XLS	6/4/15 6:01 PM CASE 1# 0.0940 0.0140 0.9001		0.812	0.2760								0.0930							Warning: No failse call	MLE Divergence Warning: Initial results	0.065	5 0.075	0.094	1.000	ET
2024 AI 1-37	lap splice	A0001B.ALS	6/4/15 6:01 PM CASE 1# 0.0940 0.0140 0.9001		0.812	20 0.2760								0.0930	-						analysis.	MLE Divergence Warning: Initial results listed.	0.065	0.075	0.094	1.000	
2024 AI T-37	lap splice	A6001C.XLS	6/4/15 6:03 PM CASE 1# 0.1140 0.0180 0.9001		0.812	0.2910								0.1060	3						Warning: No false call analysis.	Warning: Initial results listed.	0.085	0.09	0.114	1.000	ET
2024 AI T-37	lap splice	A6001D.XLS	6/4/15 6:04 PM CASE 1# 0.1280 0.0240 0.9050		0.812	0.3720								0.1270	1						Warning: No false call analysis.		0.105	0.115	0.128	1.000	ET
2024 AI T-37	lap splice	A6001E.XLS	6/4/15 6:05 PM CASE 1# 0.1280 0.0240 0.9050		0.812	0.3720								0.1270	1						Warning: No false call		0.095	5 0.1	0.128	1.000	ET
																					Warning: No false call	MLE Divergence Warning: Initial results listed.					
2024 AI T-37	lap splice	A6001F.XLS	6/4/15 6:06 PM CASE 1* 0.1200 0.0230 0.9050		0.812											-					analysis. Warning: No faise call	listed.	0.075		0.12		ET
2024 AI T-37	lap splice	A6001G.XLS	6/4/15 6:07 PM CASE 4	0.8666 0.0870				0.2													Warning: No false call analysis. Warning: No false call		0.16				ET
2024 AI T-37	lap splice	A6001GR.XLS	6/4/15 6:09 PM CASE 6	0.8707 0.0540	0.1920 0.812	20 27			0.3	220 24	1.6240	29									analysis.	MLE Divergence	0.16	0.185			ET
2024 AI T-37	lap splice	A6001H.XLS	6/4/15 6:11 PM CASE 1* 0.1310 0.0250 0.9001		0.812	0.3720															Warning: No false call	Warning: Initial results listed.	0.105	0.12	0.227	1.000	ET
2024 /011-37	iap spice	A000TH.ALS	64413 6.11 PM CASE 1 0.1310 0.0200 0.8001		0.012	0.3720															Warning: No false call	MLE Divergence Warning: Initial results listed.	0.103	0.12	0.221	1.000	- 61
2024 AI T-37	lap splice	A6001J.XLS	6/4/15 6:12 PM CASE 1# 0.1310 0.0250 0.9001		0.812	0.3720								0.1305	29						analunia	Warning: Initial results listed.	0.105	0.115	0.131	1.000	ET
2024 AI T-37	lap splice	A6001JR.XLS	6/4/15 6:13 PM CASE 1# 0.1280 0.0240 0.9050		0.812	0.3720								0.1230	2						Warning: No false call analysis.		0.095	0.11	0.128	1.000	ET
																					Warning: No false call	MLE Divergence Warning: Initial results listed					ET
2024 AI T-37	lap splice	A6002A.XLS	6/4/15 6:14 PM CASE 1# 0.0940 0.0140 0.9001		0.812						-			0.0930	1						analysis. Warning: No false call analysis.	listed.	0.075			1.000	
2024 AI T-37	lap splice	A6002B.XLS	6/4/15 6:15 PM CASE 2 0.1050 0.0180 0.9001		0.812	20 26 0.2910	26				_											MLE Divergeore	0.1	0.12		1.000	ET
2024 AI T-37	lap splice	A6002C.XLS	6/4/15 6:17 PM CASE 1* 0.1050 0.0180 0.9001		0.812	0.2910															Warning: No false call analysis.	MLE Divergence Warning: Initial results listed.	0.07	0.08	0.105	1.000	ET
2024 AI T-37	lap splice	A6002D.XLS	6/4/15 6:18 PM CASE 1* 0.1280 0.0240 0.9050		0.812																Warning: No false call analysis.		0.105				ET
2024 AI T-37	lap splice	A6002DR.XLS	6/4/15 6:19 PM CASE 1# 0.1540 0.0340 0.9077		0.812									0.1530	29						Warning: No false call analysis.		0.095	1			ET
101-101-01	Durde der		0.1040 0.0040 0.0077		0.012	0.3220								0.1000							Warning: No false call	MLE Divergence Warning: Initial results	0.095	0.11	0.104	1.000	
2024 AI T-37	lap splice	A6002E.XLS	6/4/15 6:20 PM CASE 1* 0.1310 0.0250 0.9001		0.812	0.3720															analysis.	warning: Initial results listed.	0.11	0.13	0.227		ET
2024 AI T-37	lap splice	A6002ER.XLS	6/4/15 6:21 PM CASE 1# 0.1860 0.0450 0.9001		0.812	0.3720								0.1840	29						Warning: No false call analysis.		0.11	0.125	0.186	1.000	ET
2024 AI T-37	lap splice	A6002F.XLS	6/4/15 6:22 PM CASE 7	0.8190 0.0710	0.2910						1.6240	29									analysis. Warning: No false call analysis.		0.2	0.265			ET
																					Warning: No false call	MLE Divergence Warning: Initial results					
2024 AI T-37	lap splice	A6002G.XLS	6/4/15 6:24 PM CASE 1# 0.1200 0.0230 0.9050		0.812	0.3720					-			0.1190	29						analysis.		0.095	5 0.105	0.12	1.000	ET
2024 AI T-37	lap splice	A6002H.XLS	6/4/15 6:25 PM CASE 1* 0.2220 0.0910 0.9001		0.812	0.3720															Warning: No false call analysis.	MLE Divergence Warning: Initial results listed.	0.12	0.135	0.222	0.978	ET
2024 AI T-37	lap splice	A6002HR.XLS	6/4/15 6:27 PM CASE 1* 0.1300 0.0250 0.9050		0.812																Warning: No false call analysis.		0.105	0.135			ET
2024 AI T-37	lap splice	A6002J.XLS	6/4/15 6:28 PM CASE 6		0.1270 0.812				0.2	760 24	1.6240	20									Warning: No false call		0.145		0.10		ET
2024 AI T-37 2024 AI T-37		A6003A.XLS	6/4/15 6:30 PM CASE 1* 0.1054 0.0190 0.9001		0.1270 0.812				0.2	24	1.0240	20									analysis. Warning: No false call		0.145		0.1054		ET
2024 ALT-37	lap splice	NUUUJALALO	014/10/0.30 PM CASE 1 0.1054 0.0190 0.9001		0.811	0.2910															analysis.	MLE Divergence Warning: Initial results	0.085	0.095	0.1054	1.000	C1
2024 AI T-37	lap splice	A6003B.XLS	6/4/15 6:31 PM CASE 1* 0.1141 0.0190 0.9050		0.811	0.2910															Warning: No false call analysis.		0.085	0.095	0.1141	1.000	ET
																					Warning: No false call	MLE Divergence Warning: Initial results listed.					
2024 AI T-37		A6003C.XLS	6/4/15 6:32 PM CASE 1* 0.0936 0.0150 0.9001		0.811						_										analysis. Warning: No false call populatio	listed.	0.065	1			ET
2024 AI T-37	lap splice	A6003D.XLS	6/4/15 6:34 PM CASE 1# 0.1054 0.0190 0.9001		0.811	0.2910								0.1030	1						analysis.		0.09	0.1	0.1054	1.000	ET

BOM ADM BOM BOM BOM BOM BOM BOM BOM BOM				Analysis		Xpod	Xpod CLASS-	1	0	Best_LCL	Best_LCL														False Call	Eales Call	False Call	Eales Call	Length or Area	Falsa Call			NTIAC 90% POD occurs	ITIAC 90/95	F	POH or POD @ METHO
	MATERIAL	STRUCTURE	FILE NAME	Date/Time	CASE ID	LENGTH	WIDTH	LCL	L Est_LC	WIDTH	LENGTH	XL X	L#Xm	n Xm #	Xs	Xs#XI	ci Xici	# Xpoh	Xpoh #	2XL 23	(L#Xss	Xss #	Xpodopt	Xpodopt #	UCL	Rate	Length (in)	Area (in^2)	(in or in^2) =	Opportunities	False Calls False Call Flag	MLE flag	at (inch)	POD (inch)	(P)	Cod D
	0004 417 07		100005 10 0	01445 0.05 50	0105.41	0.4000	0.0000					0.0447																			Warning: No false call	MLE Divergence Warning: Initial results	0.405	0.445	0.44505	0.070
																															analysis. Warning: No false call	listed.				
<																															Warning: No false call				0.1054	
															3																Warning: No false call					
	2024 AI 1-37	lap spilce	A0003H.ALS	0/4/15 0:39 PM	GRGE 2	0.1308	0.0250	0.900				0.8117	20 U	.3/19 2	5																anaysis.	MLE Divergence	0.14	0.165		1.000 ET
	2024 AI T-37	lap splice	A6003J.XLS	6/4/15 6:40 PM	CASE 1#	0.0982	0.0160	0.905	io			0.8117	c	.2910									0.0980	29							Warning: No false call analysis.	listed.	0.08	0.09	0.0982	1.000 ET
																															Warning: No false call	MLE Divergence Warning: Initial results				
																															analysis. Warning: No false call	listed.	0.08			
	2024 AI T-37	lap splice	A6004B.XLS	6/4/15 6:43 PM	CASE 1#	0.1140	0.0180	0.900	1			0.8120	C	0.2910				-					0.1070	3 3							analysis.	MLE Divergence	0.095	0.105	0.114	1.000 ET
	2024 AI T-37	lap splice	A6004BR.XLS	6/4/15 6:44 PM	CASE 1*	0.1050	0.0180	0.900	11			0.8120	C	.2910																		Warning: Initial results listed.	0.07	0.085	0.105	1.000 ET
	2024 AI T-37	lap splice	A6004C.XLS	6/4/15 6:46 PM	CASE 5				0.6070	0.0010	0.1140	0.8120	27					0.176	0 27												analysis.		0.14	0.165		ET
																															Warning: No faise call	MLE Divergence Warning: Initial results				
1 1										0.0010	0.0960		27					0.176	0 27													listed.	0.13			
																								3												
	2024 AI T-37	lap splice	A6004E.XLS	6/4/15 6:50 PM	CASE 1#	0.1310	0.0250	0.900	1			0.8120	C	0.3720									0.1305	5 29							analysis.	M E Diversore	0.11	0.125	0.131	1.000 ET
	2024 ALT-37	lan solice	A6004F XLS	6/4/15 6:52 PM	CASE 1*	0 1050	0.0180	0.900	1			0.8120		2910																	Warning: No false call analysis	Warning: Initial results listed	0.065	0.075	0 105	1.000 FT
		ap space																													Warning: No false call	MLE Divergence				
	2024 AI T-37																						0.1020	2								listed.				
																																	1			
Name Name Name Name Na	2024 AI T-37	lap splice	A6004H.XLS									0.8120																			analysis.					
	2024 AI T-37	lap splice	A6004J.XLS	6/4/15 6:57 PM	CASE 1#	0.1760	0.0390	0.900	1			0.8120	C	.3720									0.1710	3 3									0.105	0.12	0.176	1.000 ET
Image	STEEL 4340	plate		6/4/15 6:58 PM	CASE 7				0.5493	0.0040	0.0933									4.8060	29										waming: No faise call analysis.					
100 <td>STEEL 4340</td> <td>plate</td> <td>A7001BL.XLS</td> <td>6/4/15 7:00 PM</td> <td>CASE 7</td> <td></td> <td></td> <td></td> <td>0.6070</td> <td>0.0050</td> <td>0.0933</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>4.8060</td> <td>29</td> <td></td>	STEEL 4340	plate	A7001BL.XLS	6/4/15 7:00 PM	CASE 7				0.6070	0.0050	0.0933									4.8060	29															
<	STEEL 4340	plate	A7001CL.XLS						0.5493	0.0040	0.0933									4.8060	29										waming: No faise call analysis.					
1 1	STEEL 4340	plate	A7003AL.XLS	6/4/15 7:05 PM	CASE 7				0.6356	0.0630	0.3500									4.8060	29										analysis.					ET
m m	STEEL 4340	plate	A7003BL.XLS	6/4/15 7:07 PM	CASE 6				0.5493	0.0010	0.1960	2.4030	28					1.603	0 28	4.8060	29										analysis.					ET
	STEEL 4340	plate	A7003CL.XLS	6/4/15 7:09 PM	CASE 6				0.6878	0.0520	0.2480	2.4030	28					1.603	0 28	4.8060	29										analysis.					ET
	SS AMS 355	hole	A8001L.XLS	6/4/15 7:11 PM	CASE 1*	0.0218	0.0050	0.900	11			0.3425	C	0.1611																	Warning: No false call analysis.		0.025	0.03	0.04404	1.000 ET
	SS AMS 355	hole	A8002L.XLS									0.3425	C	0.1611									0.0145	5 29							Warning: No false call analysis.		0.01	0.015	0.01468	
1 1																															Warning: No false call	MLE Divergence Warning: Initial results				
A A																		_													analysis. Warning: No false call	listed.	0.01			
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mom mom mom mom mom mom mom </td <td>SS AMS 355</td> <td>hole</td> <td>A8005L.XLS</td> <td>6/4/15 7:23 PM</td> <td>CASE 1#</td> <td>0.0575</td> <td>0.0180</td> <td>0.910</td> <td>14</td> <td></td> <td></td> <td>0.3425</td> <td>C</td> <td>0.1694</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>0.0567</td> <td>7 29</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>analysis.</td> <td>M E Diversione</td> <td>0.03</td> <td>0.035</td> <td>0.05753</td> <td>1.000 ET</td>	SS AMS 355	hole	A8005L.XLS	6/4/15 7:23 PM	CASE 1#	0.0575	0.0180	0.910	14			0.3425	C	0.1694									0.0567	7 29							analysis.	M E Diversione	0.03	0.035	0.05753	1.000 ET
	SS AMS 355	hole	A8006L.XLS	6/4/15 7:24 PM	CASE 1#	0.0587	0.0190	0.905	0			0.3425	c	0.1694									0.0581	29								Warning: Initial results listed.	0.04	0.045	0.05873	1.000 ET
<td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>0.0020</td> <td>0.0650</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>0.080</td> <td>0 26</td> <td>0 1900</td> <td>29</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>Warning: No false call analysis</td> <td></td> <td>0.12</td> <td></td> <td></td> <td></td>										0.0020	0.0650							0.080	0 26	0 1900	29										Warning: No false call analysis		0.12			
matrix matrix matrix matrix <									0.8444				26					0.684	0 26	1 3680	29										analysis					
													26						0 26		29										Warning: No false call analysis		0.055	0.065		
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and bit bit bit bit bit bit bit bit bit bit bit bit bit bit bit bit bit bit bit bit bit< bit< bit< bit< bit< bit< bit< bit< bit< bit< bit< <td></td> <td>26</td> <td></td> <td></td> <td></td> <td></td> <td>0.076</td> <td>0 26</td> <td></td> <td>29</td> <td></td>													26					0.076	0 26		29															
													20						0 20		20										Warning: No false call		0.105	0.14		
Barry Algebra Barry Algebra Barry Algebra <th< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>29</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>Warning: No false call</td><td></td><td></td><td></td><td></td><td></td></th<>																					29										Warning: No false call					
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Part Part Part Part Part Part Part Part						0.0450	0.0500	0.000		0.0080	0.9430			4500						2.5420	29															
2104 169/269 0405 1498 0425 0405 1498 0425 040 0405 1498 0425 040<						0.9450	0.0560	0.905		0.0000	0.2670		100 1							2.2760	20										Warning: No false call					
1 1													20					1.000			29										analysis.					
219 A T MOM 4017 4 MOM 4 4019 7 MOM 6 4019 7 MOM 6 401 7 MOM 6												1.1880	20					1.188	26		23										Warning: No false call					
Control Cold Cold Cold Cold <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>29</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>Warning: No false call</td><td></td><td></td><td>0</td><td></td><td></td></t<>																					29										Warning: No false call			0		
21 A 1 7 A 102 M 6 401 7 5 2 P A 25 F 6 40 7 5 2 P A 5 F 9 A 9 A 9 A 9 A 9 A 9 A 9 A 9 A 9 A 9 A 9 A 9 A 9 A 9 A 9 A 9 A 9 A 9 A 9 A 9 A 9 A 9 A 9 A 9 A 9 A 9 A												4.4055						0.000			29										Warning: No false call					
2129 A 169/2219 webs 16 2401 5 20 PW CASE 1 2400 0 1000 1000 1000 0 1100 0 1100 0 11000 0																					29										Warning: No false call			0.74		
219 A 178 words w	2219 AL F-87/w2319	weld TFC	ACUU3(3)L.xls	6/4/15 7:50 PM	CASE 6			-	0.8666	0.2000	1.0760	1.4350	26					1.435	u 26	2.8700	29											MLE Divergence	0.75			ET
219 A 178 words w	2219 AI T-87/w2319	weld flush LFC	AD001(3)L.xls	6/4/15 7:52 PM	CASE 1*	0.3480	0.0290	0.905	10			1.5620	1	.1190																	Warning: No false call analysis.	Warning: Initial results listed.	0.105	0.13	0.348	1.000 ET
Part of the section				6/4/15 7:58 PM	CASE 1*	0.3480	0.0290	0.905	10			1.5620	1	.1190																	Warning: No false call analysis.		0.185	0.24	0.348	1.000 ET
2 3 3 5																															Warning: No false call	MLE Divergence Warning: Initial results				
Distribution Distribution <th< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>23</td><td></td><td></td><td></td><td></td><td></td><td></td><td>Warning: No false call</td><td>listed.</td><td>1</td><td></td><td></td><td></td></th<>																								23							Warning: No false call	listed.	1			
214 J 43 / 34 / 34 245 / 34	2219 AI T-87/w2319	weld flush TFC	AE001(3)L.xis	6/4/15 8:10 PM	CASE 1#	0.2350	0.0570	0.905	0			0.4950	C	0.3080									0.2240	8							artarysis.	MLE Divergence	0.185	0.23	0.235	1.000 ET
And bit And bit <t< td=""><td>2219 AI T-87/w2319</td><td>weld flush TFC</td><td>AE002(3)L.xls</td><td>6/4/15 8:11 PM</td><td>CASE 1#</td><td>0.2670</td><td>0.0850</td><td>0.905</td><td>10</td><td></td><td></td><td>0.4950</td><td>c</td><td>.3810 2</td><td>9</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>0.2530</td><td>29</td><td></td><td></td><td></td><td></td><td></td><td></td><td>Warning: No false call analysis.</td><td>Warning: Initial results listed.</td><td>0.2</td><td>0.23</td><td>0.267</td><td>1.000 ET</td></t<>	2219 AI T-87/w2319	weld flush TFC	AE002(3)L.xls	6/4/15 8:11 PM	CASE 1#	0.2670	0.0850	0.905	10			0.4950	c	.3810 2	9								0.2530	29							Warning: No false call analysis.	Warning: Initial results listed.	0.2	0.23	0.267	1.000 ET
State Both DA 2																															Warning: No fake call	MLE Divergence Warning: Initial results				
STEEL 430 Jate BiOTO XLS 64/15 81 2PM CASE 6 0 0.000 0.0							0.0570	0.905				0.4950	-	0.3080									0.1380	26							analysis.	listed.	0.005		0.235	
Since Aug parts Since Aug constraints con		plate						-					28								29										analunia					
STEEL 430 Jule Biolific DVLS 64/15 ±15 PM_OASE 6 0.210 2 0.210 2 0.400 0.200 2 0.400 0.210 2 0.400 2 0.400 0.400 2 0.400 0.4000 2 0 0.400 0 0 0	STEEL 4340	plate						-					28								29										analysis.		0.695			
STEEL 4340 plate B1001EULS 64/15.817 PMCASE 2 0.0500 0.0500 0.2340 2.4030 28 1 1.2270 28 4.6660 29 0 0.44 0.4 0.4 0.4 0.4 STEEL 4340 plate B1001CD.XLS 64/15.817 PMCASE 2 0.0600 0.0300 0.9001 0.2100 28 4.6660 29 0 0 0.44 0 0.47 <td< td=""><td>STEEL 4340</td><td>plate</td><td>B1001BD.XLS</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>28</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>29</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>analysis.</td><td></td><td></td><td></td><td></td><td></td></td<>	STEEL 4340	plate	B1001BD.XLS										28								29										analysis.					
	STEEL 4340	plate	B1001BL.XLS	6/4/15 8:17 PM	CASE 6				0.8719	0.0520	0.2340							1.227	0 28	4.8060	29												0.4			MT
STEEL 4340 plate B1001CLX.S 64/15.819.PM CASE 2 0.2340 0.0600 0.9001 2.400 24 16000 28 10 100 MT	STEEL 4340	plate	B1001CD.XLS												4																					0.978 MT
	STEEL 4340	plate	B1001CL.XLS	6/4/15 8:19 PM	CASE 2	0.2340	0.0630	0.900	11			2.4030	24 1	.6030 2	в																Warning: No false call analysis.		0.37			1.000 MT

*All lengths are in inches 13

Matrice <th></th> <th>STRUCTURE</th> <th></th> <th>Analysis Date/Time</th> <th></th> <th>Xpod CLASS-</th> <th>Xpod CLASS-</th> <th></th> <th>Best_LC</th> <th>Best_LCL CLASS-</th> <th>Best_LCL CLASS- LENGTH</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>Xici # Xnoh</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>Fal</th> <th>alse Call</th> <th>False Call</th> <th>False Call</th> <th>False Call</th> <th>Length or Area per Inspection</th> <th>False Call</th> <th></th> <th>_</th> <th></th> <th>NTIAC 90% POD occurs</th> <th>NTIAC 90/95 occurs at</th> <th>POH</th> <th>or @ ME</th> <th>етно</th>		STRUCTURE		Analysis Date/Time		Xpod CLASS-	Xpod CLASS-		Best_LC	Best_LCL CLASS-	Best_LCL CLASS- LENGTH							Xici # Xnoh							Fal	alse Call	False Call	False Call	False Call	Length or Area per Inspection	False Call		_		NTIAC 90% POD occurs	NTIAC 90/95 occurs at	POH	or @ ME	етно
		STRUCTURE			1	1	WIDTH	LCL	-	1		XL X	L#Xm	Xm #	Xs	XS #)	(ICI		1			(ss X	ss#Xp	odopt Xpod	opt # UC	UL	Kate	Length (in)	Area (in^2)	(in or in^2) =	Opportunities	False Calls	False Call Flag Warning: No false call	MLE flag	at (inch)	POD (inch) XP	Xpod		
<td< td=""><td></td><td>plate</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>0.0060</td><td>0.0603</td><td></td><td>28</td><td></td><td></td><td></td><td></td><td>0.156</td><td>3 26</td><td>0.4200</td><td>29</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>		plate								0.0060	0.0603		28					0.156	3 26	0.4200	29																		
	STEEL 4340	plate	B1003AL.XLS	6/4/15 8:22 PI	MCASE 2	0.2340	0.0590	0.900	1			2.4030	24 1.60	30 28	В																		analysis		0.26	0.465	1		
	STEEL 4340	plate	B1003BD.XLS	6/4/15 8:23 PI	MCASE 6				0.8813	0.0120	0.0663	0.2100	28					0.210	0 28	0.4200	29												warning: No faise call analysis.						MT
																																	Warning: No false call	MLE Divergence Warning: Initial results					1.1
	STEEL 4340	plate	B1003BL.XLS			0.00.0	0.0590	0.900	1				27 1.60	30 28	8																		analysis. Warning: No faire call	listed.		0.135	1.		
<td>STEEL 4340</td> <td>plate</td> <td>B1003CD.XLS</td> <td>6/4/15 8:26 PI</td> <td>MCASE 6</td> <td></td> <td></td> <td></td> <td>0.8813</td> <td>0.0120</td> <td>0.0663</td> <td>0.2100</td> <td>28</td> <td></td> <td></td> <td></td> <td></td> <td>0.156</td> <td>3 23</td> <td>0.4200</td> <td>29</td> <td></td> <td>0.045</td> <td></td> <td></td> <td></td> <td>MT</td>	STEEL 4340	plate	B1003CD.XLS	6/4/15 8:26 PI	MCASE 6				0.8813	0.0120	0.0663	0.2100	28					0.156	3 23	0.4200	29														0.045				MT
	STEEL 4340	plate	B1003CL.XLS	6/4/15 8:27 PI	MCASE 1*	0.2340	0.0590	0.900	11			2.4030	1.60	30																			analysis.		0.12	0.235	0.234 1	.000 1	MT
	SS AMS 355	hole	B2001.XLS	6/4/15 8:29 PI	MCASE 6				0.8190	0.0750	0.1752	0.2575	24					0.257	5 24	0.5150	29												Warning: No false call analysis.		0.115	0.175		1	MT
	SS AMS 355	hole	B2002.XLS	6/4/15 8:30 P	MCASE 1#	0.1031	1 0.0540	0.900	1			0.2575	0.19	29										0.1004	2								Warning: No false call analysis.		0.04	0.065 0	10314 1	.000	MT
																																		MLE Divergence					
	SS AMS 355	hole	B2003.XLS	6/4/15 8:31 PI	MCASE 5				0.3684	0.0010	0.0512	0.2575	28					0.063	4 27														analysis.	listed.	0.045	0.07			MT
																																	Warning: No false call	MLE Divergence Warning: Initial results					1.1
Bit Bit Bit Bit Bit		hole												_							29		_										analysis. Warning: No false call	listed.					
	SS AMS 355	hole											4	_			0.0902			0.1803	29												analysis.	-					
	SS AMS 355	hole	B4001L.XLS	6/4/15 8:36 PI	MCASE 5				0.4729	0.0010	0.0623	0.3425	28					0.082	1 26														analysis.		0.175	0.26			мт
	2219 AI T-87	plate	C1001AL.XLS	6/4/15 8:38 PI	MCASE 7				0.8609	0.0200	0.2610									1.9580	29														0.395	0.63			РТ
	2219 AI T-87	plate	C1001BL XLS	6/4/15 8:40 P	MCASE 6				0.8368	0.0850	0.3260	0.9790	28					0.610	0 22	1 9580	29												Warning: No false call analysis.		0.44	0.695			РТ
		elete					0.200	0.017					0.7	00										0.6270	20								Warning: No false call		0.215		0.520 1	000	пт
		plate						-	-																2.3								Warning: No false call						
		plate																																					
	2219 AI T-87	plate	C1002BL.XLS	6/4/15 8:47 PI	MCASE 1*	0.1080	0.0310	0.900	1			0.9790	0.34	20																			analysis.		0.08	0.105	0.261 0.	.967 F	PT
	2219 ALT-87	plate	C1002C1 X1 S	6/4/15 8:40 0	MCASE 1*	0.2000	0.054	0 0 000	1			0.9790	0.5	30																			Warning: No false call analysis	Warning: Initial results	0.11	0.145	0.508	000	PT
N N N N N N N N N N N N N N N N N N N		- Marce	STOULOL.ALS	0-+10 0.49 Pl	Gride (3.250	3.0010	0.000				0.0780	0.54																					MLE Divergence	0.11	0.140			<u> </u>
<td>2219 AI T-87</td> <td>plate</td> <td>C1003AL.XLS</td> <td>6/4/15 8:51 P</td> <td>MCASE 1*</td> <td>0.0830</td> <td>0.0080</td> <td>0.900</td> <td>11</td> <td></td> <td></td> <td>0.6100</td> <td>0.26</td> <td>20</td> <td></td> <td>Warning: No false call analysis.</td> <td>Warning: Initial results listed.</td> <td>0.02</td> <td>0.035</td> <td>0.086 1</td> <td>.000</td> <td>РТ</td>	2219 AI T-87	plate	C1003AL.XLS	6/4/15 8:51 P	MCASE 1*	0.0830	0.0080	0.900	11			0.6100	0.26	20																			Warning: No false call analysis.	Warning: Initial results listed.	0.02	0.035	0.086 1	.000	РТ
1 1	2219 AI T-87	plate	C1003BL XLS	6/4/15 8·56 P	MCASE 2	0 1020	0.0170	0 0 900	1			0.6100	0.26	20 10	1																		Warning: No false call		0.08	0.095	0.279 1	000	PT
m m		elote																															Warning: No false call						
		plate					0.013	0 0.500				0.0100	0.20	20																			Warning: No false call		0.00	0.07	0.000 0.		
1 1		plate								0.0520	0.5300			_						1.1000	29												analysis. Warning: No false call						
m m		plate											0.01											0.2880	28								analysis. Warning: No faire call				0.001		
	2219 AI T-87	plate	C2002CL.XLS	6/4/15 9:03 PI	MCASE 2	0.4740	0.2000	0.900	11			0.5500	0 0.49	60																					0.22	0.385	1		
1 1	Ti 6Al4V	plate	C3001AL.XLS	6/4/15 9:04 PI	MCASE 6				0.7942	0.0180	0.1940	0.4070	28					0.300	0 27	0.8140	29														0.705				РТ
m m	Ti 6AJ4V	plate	C3001BL.XLS	6/4/15 9:06 PI	MCASE 2	0.1950	0.0540	0.900	11			0.4070	0.30	00 17	7																		Warning: No false call analysis.		0.12	0.175	0.32 1	.000	РТ
	Ti 6Al4V	plate	C3001CL.XLS	6/4/15 9:07 P	MCASE 4				0.8768	0.0850	0.3250	0.4070	23				0.3250	6 0.324	0 7														Warning: No false call analysis.		0.14	0.325			PT
		- 1 - 4 -											40							0.0140													Warning: No false call						
and a		plate								0.0500								0.340	10 10	0.8140	20												Warning: No false call						
M M M M M <th<< td=""><td>Ti 6Al4V</td><td>plate</td><td>C3002BL.XLS</td><td>6/4/15 9:10 P</td><td>MCASE 2</td><td>0.1900</td><td>0.0530</td><td>0.900</td><td>1</td><td></td><td></td><td>0.4070</td><td>0.30</td><td>17</td><td>7</td><td></td><td></td><td></td><td>-</td><td></td><td>-</td><td></td><td>_</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>MLE Divergence</td><td>0.12</td><td>0.165</td><td>0.315 1.</td><td>.000 F</td><td><u>PT</u></td></th<<>	Ti 6Al4V	plate	C3002BL.XLS	6/4/15 9:10 P	MCASE 2	0.1900	0.0530	0.900	1			0.4070	0.30	17	7				-		-		_											MLE Divergence	0.12	0.165	0.315 1.	.000 F	<u>PT</u>
image image <th< td=""><td>Ti 6AI4V</td><td>plate</td><td>C3002CL XLS</td><td>6/4/15 9:11 P</td><td>MCASE 1#</td><td>0.2160</td><td>0.0340</td><td>0.900</td><td>1</td><td></td><td></td><td>0.4070</td><td>0.26</td><td>50</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>0 1300</td><td>15</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>Warning: No false call analysis.</td><td>Warning: Initial results listed.</td><td>0.08</td><td>0.1</td><td>0.216 1</td><td>000</td><td>рт</td></th<>	Ti 6AI4V	plate	C3002CL XLS	6/4/15 9:11 P	MCASE 1#	0.2160	0.0340	0.900	1			0.4070	0.26	50										0 1300	15								Warning: No false call analysis.	Warning: Initial results listed.	0.08	0.1	0.216 1	000	рт
		alata								0.1000	0.2250									0.9140	20												Warning: No false call		0.195	0.485			DT
image image <th< td=""><td></td><td>plate</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>0.1000</td><td>0.3250</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>0.8140</td><td>29</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>Warning: No false call</td><td></td><td></td><td></td><td></td><td></td><td></td></th<>		plate								0.1000	0.3250									0.8140	29												Warning: No false call						
MAM M		plate													8				-		-		_											-					
		plate					0.0520	0.905						18	8																		analysis. Warning: No faise call				1.		
Add <td>SS AMS 355</td> <td>hole</td> <td>C400011.XLS</td> <td>6/4/15 9:15 P</td> <td>MCASE 6</td> <td></td> <td></td> <td></td> <td>0.8074</td> <td>0.0730</td> <td>0.1752</td> <td>0.2575</td> <td>24</td> <td></td> <td></td> <td></td> <td></td> <td>0.257</td> <td>5 24</td> <td>0.5150</td> <td>29</td> <td></td> <td>analysis.</td> <td></td> <td>0.13</td> <td>0.195</td> <td></td> <td></td> <td></td>	SS AMS 355	hole	C400011.XLS	6/4/15 9:15 P	MCASE 6				0.8074	0.0730	0.1752	0.2575	24					0.257	5 24	0.5150	29												analysis.		0.13	0.195			
Add A	SS AMS 355	hole	C400012.XLS	6/4/15 9:16 PI	MCASE 5				0.5493	0.0070	0.0776	0.2575	28					0.085	8 27														warning: No faise call analysis.		0.085	0.12			РТ
Add A	SS AMS 355	hole	C400013.XLS	6/4/15 9:18 PI	MCASE 5				0.5493	0.0070	0.0669	0.2575	28					0.085	8 27														Warning: No false call analysis.		0.1	0.185			РТ
AND SUM S		bole											19				0 1929																Warning: No false call analysis		0.135				
Add <td></td> <td>hole</td> <td></td> <td>4</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>0.1803</td> <td>20</td> <td></td>		hole											4							0.1803	20																		
BAMES BAMES BAMES BAMES		hala																															Warning: No false call						
Abs A		1016											4																				warwiysis. Warning: No false call						
Solds de		hole					-	-		0.020			4				0.0902	4 0.090	12		29							_	_		+	-				0.12			
Teles de lise 2 Mais de 1982 Marie 1 10 1 10 10 10 10 10 10 10 10 10 10 10	SS AMS 355	hole						_													29														0.095				
Differe Differe <t< td=""><td>STEEL 4340</td><td>plate</td><td>C6001AL.XLS</td><td></td><td></td><td></td><td></td><td></td><td>0.7942</td><td>0.0100</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>1.603</td><td>0 28</td><td>4.8060</td><td>29</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>	STEEL 4340	plate	C6001AL.XLS						0.7942	0.0100								1.603	0 28	4.8060	29																		
Differe Differe <t< td=""><td>STEEL 4340</td><td>plate</td><td>C6001BL.XLS</td><td>6/4/15 9:30 PI</td><td>MCASE 6</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>28</td><td></td><td></td><td></td><td></td><td>1.603</td><td>0 28</td><td>4.8060</td><td>29</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>warning: No taise call analysis.</td><td></td><td></td><td></td><td></td><td></td><td></td></t<>	STEEL 4340	plate	C6001BL.XLS	6/4/15 9:30 PI	MCASE 6								28					1.603	0 28	4.8060	29												warning: No taise call analysis.						
Here General As a	STEEL 4340	plate	C6001CL.XLS	6/4/15 9:32 PI	MCASE 6				0.7942	0.0100	0.1153	2.4030	28					1.603	0 28	4.8060	29																		РТ
And And <td>STEEL 4340</td> <td>plate</td> <td>C6002AL XI S</td> <td>6/4/15 9:33 P</td> <td>MCASE 2</td> <td>0.250</td> <td>0.0700</td> <td>0.900</td> <td>1</td> <td></td> <td></td> <td>2,4030</td> <td>26 1.60</td> <td>30 28</td> <td>3</td> <td></td> <td>Warning: No false call analysis.</td> <td></td> <td>0.1</td> <td></td> <td>1</td> <td>.000</td> <td>PT</td>	STEEL 4340	plate	C6002AL XI S	6/4/15 9:33 P	MCASE 2	0.250	0.0700	0.900	1			2,4030	26 1.60	30 28	3																		Warning: No false call analysis.		0.1		1	.000	PT
TEEL 430 jule Column Colum Colum Colum <td></td> <td>Warning No false -</td> <td>MLE Divergence</td> <td></td> <td></td> <td></td> <td></td> <td></td>																																	Warning No false -	MLE Divergence					
VIECE 430 Deel 0 COURT 43 OPUID 5677 CASE Court 40 OPUID 677 Court 40 Court 40 Court 40 Court 40	STEEL 4340	plate	C6002BL.XLS	6/4/15 9:35 PI	MCASE 1*	0.0960	0.0400	0.900	11			2.4030	1.60	130																			warning: No taise call analysis.	listed.	0.06	0.08	0.18 1	.000	РТ
VIECE 430 Deel 0 COURT 43 OPUID 5677 CASE Court 40 OPUID 677 Court 40 Court 40 Court 40 Court 40																																	Warning: No false call	MLE Divergence Warning: Initial results					
TEEL 430 def Sold VLXS 64/15 S 27 M/GASE 2.00 0.00 0.00 2.00		plate							-					-					-					0.1940	11								analysis.	ISRd.					
TEEL 40 Add Conde Cal Add and and and and and and and and and a	STEEL 4340	plate	C6003AL.XLS												В												_	_	_										
TEEL 40 Add Conde Cal Add and and and and and and and and and a	STEEL 4340	plate	C6003BL.XLS									2.4030	24 1.60	30 28	в																		analysis.		0.155	0.255	1	.000	РТ
Alternational Alternational<	STEEL 4340	plate	C6003CL.XLS	6/4/15 9:40 PI	MCASE 1*	0.2340	0.0590	0.900	11			2.4030																					Warning: No false call analysis.		0.11	0.175	0.234 1	.000	РТ
TEEL 430 hole CPORL X5 64/15 94 PM CASE 5 V 0.640 0.700 0.840 0.700 0.840 0.700 0.840 0.840 0.700 0.840 0.840 0.700 0.840 0.840 0.700 0.840 0.840 0.700 0.840 0.840 0.700 0.840 0.840 0.700 0.840 0.840 0.700 0.840 0.840 0.700 0.840 0.840 0.700 0.840 0.840 0.700 0.840 0.840 0.700 0.840 0.840 0.700 0.840 0.700 0.700 0.840 0.700 0.700 0.840 0.700 0.700 0.840 0.700 0.700 0.840 0.700 0.700 0.840 0.700 0.700 0.840 0.700 0.700 0.840 0.700 0.700 0.840 0.700<																																	Warning: No fake coll	MLE Divergence Warning: Initial results					
TEEL 40 hole CV0X.X.S 64/15 9.3 PM CASE 4 V 0.84 0.07 0.719 0.800 0.729 0.800 0.927 V 0.910 1.992	STEEL 4340	hole	C7001L.XLS	6/4/15 9:41 P	MCASE 5		-		0.5493	0.0040	0.0738	0.3425	28					0.088	1 28														analysis.	listed.	0.215	0.36		4	РТ
All All <td>07551 (515</td> <td>h al a</td> <td>07000:</td> <td>0/4/17 5 5</td> <td></td> <td>Warning: No false call</td> <td>MLE Divergence Warning: Initial results</td> <td></td> <td></td> <td></td> <td></td> <td></td>	07551 (515	h al a	07000:	0/4/17 5 5																													Warning: No false call	MLE Divergence Warning: Initial results					
TEEL 40 Inde C700X.XS 64/15 947 MCASE 0 0.079 0.030 0.252 7 0.032 7 0.032 7 0.032 7 0.032 0.252 7 0.032 0.252 7 0.032 0.252 7 0.032 0.252 7 0.032 0.252 7 0.032 0.252 7 0.032 0.252 7 0.032 0.252 7 0.032 0.252 7 0.032 0.252 7 0.032 0.252 7 0.032 0.252 7 0.032 0.252 7 0.032 0.252 7 0.032 0.252 7 0.032 0.252 7 0.032 0.252 7 0.032 0.252 7 0.032 0.252 7 0.032	STEEL 4340	nole	C7002L.XLS	6/4/15 9:43 PI	MCASE 4		-	-	0.8444	0.0970	0.2131	0.3425	27				0.2131	11 0.199	2 13												+		analysis.	listed. MLE Divergence	0.35	0.58			21
219 AT 767 singer part 680(13).0.6 64/15.94.7M (ASE2 0.05 0.	STEEL 4340	hole	C7003I XI S	6/4/15 9·45 P	MCASE 4				0 7791	0.0930	0 2512	0.3425	27				0.2512	17 0.251	2														Warning: No false call analysis.	Warning: Initial results listed.	0.3	0.505			РТ
219 A T-77 shore and scale 64015 340 M CASE 7 0.278 0.078 0.057 0.080 0.478 0.789		etringer oon					0.00~	0.000		3.0000								0.20															Warning: No false call		0.075				
219 A T-77 shings parts (2002) Das (4/15 95 0 PM CASE 7) 0 0 0 73 0 00 0.453 0 0 0.453 0 0 0.453 0 0 0.453 0 0 0.453 0 0 0.453 0 0 0.453 0 0 0.453 0 0 0.453 0 0 0.453 0 0 0.453 0 0 0.453 0 0 0.453 0 0 0.453 0 0 0.453 0 0 0.453 0 0 0.453 0 0 0.453 0 0 0 0.453 0 0 0 0.453 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0																			1														anarysis. Warning: No false call			0.12			
213/11/0/ Sunger Jane Ox02(5)/0.5 0/41/03.0/07/04/04/07/04/04/07/04/04/07/04/04/07/04/04/07/04/04/07/04/04/07/04/04/07/04/04/07/04/04/07/04/04/07/04/04/07/04/04/04/04/04/04/04/04/04/04/04/04/04/							0.0050	0.905					23 0.57	90 17	9				1																				
213N T-87 jatinger panel [080023]Las 8/4/15.95 FM (CASE 2 0.2820 0.0880 0.0960 0.0840 28 0.4760 22 1000 PT							-			0.0030				-						0.1900	29											-							PT
	2219 AI T-87	stringer panel	C8002(3)L.xls	6/4/15 9:51 P	MCASE 2	0.2620	0.0680	0.905	i0			0.6840	26 0.4	60 23	3																		analysis.		0.395		1	.000	РТ

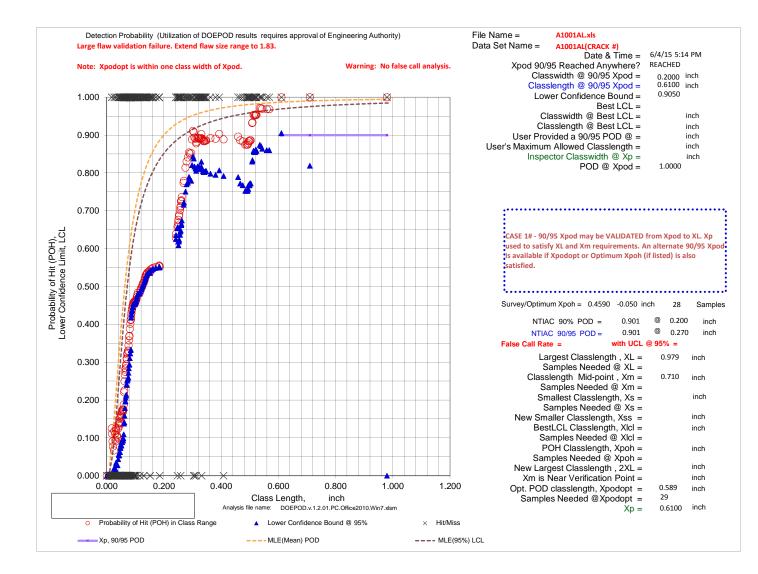
				Ameliate		Xpod	Xpod		Bes	LCL Best_L	CL											1 1			False Call	Eales Call	False Call	Eales Call	Length or Area per Inspection	False Call			NTIAC 90%	TIAC 90/95	5	POH or POD @ MI	ETHO
	MATERIAL	STRUCTURE	FILE NAME	Analysis Date/Time	CASE ID	LENGTH	WIDTH	LCL	L WID	TH LENGT	TH XL	XL	¥ Xm	Xm #	Xs	Xs#	Xici	Xici # Xpol	Хро	h#2XL	2XL	W Xss	Xss # 2	(podopt Xpodop	UCL	Rate	Length (in)	Area (in^2)	(in or in^2) =		False Calls False Call Flag	MLE flag	at (inch)	POD (inch)		Xpod	D
Image Image Image Image	2219 AI T-87	stringer panel	C8003(3)D.xls	6/4/15 9:53 PN	CASE 1#	0.0680	0.0090	0.9050	0		0.	0950	0.07	60										0.0665	29								0.095		0.068	1.000	PT
	2219 AI T-87	stringer panel	C8003(3)L.xls	6/4/15 9:54 PN	CASE 1#	0.5790	0.0130	0.9050	D		0.	6840	0.61	20										0.2910	20						Warning: No false call analysis.		0.405	0.665	0.579	1.000	PT
	2219 AI T-87/w2319			6/4/15 9:56 PN	CASE 7				0.8813	0.0180 0.6	900									2	.5420	29									analysis						PT
	2219 AI T-87/w2319	weld LOP	C9002(3)L.xls	6/4/15 9:57 PN	CASE 7				0.6070	0.0040 0.3	1450									2	.5420	29															PT
																						29									opolygic						
	2219 AI T-87/w2319	weld LOP	C9004(3)L.xls	6/4/15 10:03 PN	CASE 6				0.8931	0.0260 0.7	080 1.	2710	23					1.	2100	23 2.	.5420	29											0.005				PT
						0.1200	0.0210	0.9050					13 0.49	30 23																	Warning: No false call analysis.						
									0.7206	0.0060 0.1	000 1	1880 3	26					1	1880	26 2	3760	29															PT
						0.3240	0.0670	0 9050					0.54	00																	Warning: No false call analysis.		0.26	0.6	0.324		
<			CB001(3)L xls				0.0430	0.9050	0		1	4350	0.51	90																	Warning: No false call analysis		0.055	0.09	0.478	1 000	PT
																															Manian Madala and	MLE Divergence					
	2219 AI T-87/w2319	e weld TFC	CB002(3)L.xls																			_		0.2950	2						analysis.	listed.					
Martial Martia Martial Martial Martial Martial Martial Mar	2219 AI T-87/w2319	weld TFC	CB003(3)L.xls	6/4/15 10:09 PN	CASE 1*	0.3060	0.0330	0.9050	D		1.	4350	0.99	20								_									analysis.		0.21	0.345	0.498	1.000	PT
	0040 417 071-0040		00004/001	0/4/45 40 40 50	0.050	0.0000		0.0050																							Warning: No false call	MLE Divergence Warning: Initial result:	0.005	0.075		4 000	
	2219 AL 1-6//W2319	9 weid nush LPC	CC001(3)L.XIS	6/4/15 10:10 PN	CASE 2	0.0830	0.0230	0.9050			1.	5620 .	20 0.01	00 20																	ararysis.		0.005	0.075		1.000	PI
	2219 AI T-87/w2319	e weld flush LFC	CC002(3)L.xls	6/4/15 10:19 PM	CASE 1*	0.0830	0.0230	0.9050	D		1.	5620	1.11	90																	Warning: No false call analysis.		0.05	0.07	0.191	1.000	PT
																															Warning: No false call	MLE Divergence Warning: Initial results					
No.	2219 AI T-87/w2319	eld flush LFC	CC003(3)L.xls	6/4/15 10:24 PN	CASE 1*	0.0830	0.0230	0.9050	0		1.	5620	1.11	90																	analysis.	listed. MLE Divergence	0.04	0.065	0.191	1.000	PT
District Distrint District Distri	2219 AI T-87/w2319	weld flush TFC	CD001(3)L.xls	6/4/15 10:28 PN	CASE 1#	0.2350	0.0570	0.9050	D		0.	4950	0.30	80										0.1380	26							Warning: Initial results listed.	0.005		0.235	1.000	РТ
</td <td>2219 AI T-87/w2319</td> <td>e weld flush TFC</td> <td>CD002(3)L.xls</td> <td>6/4/15 10:29 PN</td> <td>CASE 4</td> <td></td> <td></td> <td></td> <td>0.8813</td> <td>0.0840 0.3</td> <td>1080 0.</td> <td>4950 3</td> <td>26</td> <td></td> <td></td> <td></td> <td>0.3080</td> <td>5 0.</td> <td>2970</td> <td>8</td> <td></td> <td>Warning: No false call analysis.</td> <td></td> <td>0.205</td> <td>0.725</td> <td></td> <td></td> <td>PT</td>	2219 AI T-87/w2319	e weld flush TFC	CD002(3)L.xls	6/4/15 10:29 PN	CASE 4				0.8813	0.0840 0.3	1080 0.	4950 3	26				0.3080	5 0.	2970	8											Warning: No false call analysis.		0.205	0.725			PT
			CD003(3)L.xis	6/4/15 10:30 PN	CASE 4				0.8666				26				0.3080	8 0.	3080												analysis.			0.31			PT
						0.0240	0.0060	0 9001					13 0.04	90 14																	Warning: No false call analysis.		0.03	0.04			
																															Warning: No faire call	MLE Divergence					
Part of the state Part of the state Part of the state	HAYNES 188 AMS 5	5 plate	CE011(6)L.xls	6/4/15 10:32 PN	CASE 2	0.1300	0.0190	0.9001	1		0.	3500 4	14 0.22	80 16													_				analysis.		0.115	0.155		1.000	PT
</td <td>HAVNES 188 AMS F</td> <td>Solate</td> <td>CE012(6)D vie</td> <td>6/4/15 10:33 PM</td> <td>CASE 14</td> <td>0.0100</td> <td>0.0020</td> <td>0.9120</td> <td></td> <td></td> <td></td> <td>0690</td> <td>0.02</td> <td>80</td> <td></td> <td>Warning: No false call</td> <td>MLE Divergence Warning: Initial result: lictud</td> <td>0.005</td> <td>0.01</td> <td>0.01</td> <td>1.000</td> <td>PT</td>	HAVNES 188 AMS F	Solate	CE012(6)D vie	6/4/15 10:33 PM	CASE 14	0.0100	0.0020	0.9120				0690	0.02	80																	Warning: No false call	MLE Divergence Warning: Initial result: lictud	0.005	0.01	0.01	1.000	PT
																															Warning: No false call	LINU.					
						0.0480	0.0100	0.9001			-	3500	0.13	70							4000	~									Warning: No false call		0.03	0.04	0.107		
																						29									Warning: No false call						
										0.0010 0.1				_						0.	.7000 :	29									analysis. Warning: No false call						
						0.1410	0.0110	0.9050				3500	0.25	00																	analysis. Warning: No false call		0.065	0.075	0.141		
MAX MAX MAX MAX MAX MAX MAX MAX <																						29									analysis. Warning: No false call						
										0.0180 0.1									_	0.	.7000 2	29			_	-											
Cond Cond Cond Cond Co									1 1		-								_						_	-					analysis. Warning: No false call						
bolic bolic <th< td=""><td></td><td></td><td></td><td></td><td></td><td>0.2600</td><td>0.0260</td><td>0.9001</td><td></td><td></td><td></td><td>3500</td><td>0.28</td><td>50</td><td></td><td></td><td></td><td></td><td>_</td><td></td><td></td><td></td><td></td><td>0.2580</td><td>29</td><td></td><td></td><td></td><td></td><td></td><td>analysis.</td><td></td><td>0.12</td><td>0.15</td><td>0.26</td><td></td><td></td></th<>						0.2600	0.0260	0.9001				3500	0.28	50					_					0.2580	29						analysis.		0.12	0.15	0.26		
conditional all all all all all all all all all												_										29									analysis.						
Normal and Solution and S									0.5293	0.0200 0.1	850		_							0	.7000	29															
MACHE MAME for Gebole Model Mode																																					
MANCH MANG						0.2620	0.0420	0.9001				3500	0.30	10																	analysis.				0.262		
Marcial Mar	HAYNES 188 AMS 5	5 plate																				29									analysis.						
MANDER MAN	HAYNES 188 AMS 5	5 plate	CE051(6)L.xls	6/4/15 11:07 PN	CASE 6				0.8768	0.0090 0.1	410 0.	3500 3	27					0.	2680	22 0.	.7000	29									analysis.		0.315	0.575			
while black b	HAYNES 188 AMS 5	5 plate	CE052(6)D.xls	6/4/15 11:09 PN	CASE 1+	0.0170	0.0020	0.9050	0		0.	0690	0.05	50																	analysis.		0.015	0.02	0.017	1.000	PT
Print Strates Print St	HAYNES 188 AMS 5	5 plate	CE052(6)L.xls	6/4/15 11:12 PN	CASE 1*	0.2460	0.0190	0.9001	1					30																	analysis.		0.07	0.085	0.246		
minimes discord distantines discord distantin	HAYNES 188 AMS 5	5 plate	CE061(6)D.xls	6/4/15 11:14 PN	CASE 2	0.0630	0.0090	0.9104	4		0.	0690 :	33 0.06	60 29																			0.04	0.055		1.000	PT
MANDER 1844/AB 4/2000 General (a) General (a) General (a) General (a) <td>HAYNES 188 AMS 5</td> <td>5 plate</td> <td>CE061(6)L.xls</td> <td>6/4/15 11:15 PN</td> <td>CASE 7</td> <td></td> <td></td> <td></td> <td>0.8829</td> <td>0.0940 0.2</td> <td>460</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>0.</td> <td>.7000</td> <td>29</td> <td></td> <td>0.185</td> <td>0.265</td> <td></td> <td></td> <td></td>	HAYNES 188 AMS 5	5 plate	CE061(6)L.xls	6/4/15 11:15 PN	CASE 7				0.8829	0.0940 0.2	460									0.	.7000	29											0.185	0.265			
MANES 1940 5. 2000 Color 0.00 Color 0	HAYNES 188 AMS 5	5 plate	CE062(6)D.xls	6/4/15 11:17 PN	CASE 1*	0.0180	0.0020	0.9001	1		0.	0690	0.05	50																	analysis.		0.015	0.02	0.018	1.000	PT
NAME OUTOR OUTOR OUTOR OU	HAYNES 188 AMS 5	5 plate	CE062(6)L.xls	6/4/15 11:20 PN	CASE 1*	0.0980	0.0180	0.9001	1		0.	3500	0.25	60																			0.07	0.09	0.105	1.000	PT
NUMES 188 MS glus CLOPICAL MUMES 188 MS glus MUES 188 MS glus MUES 188 MS glus <									0.8368	0.0050 0.0										0.	.1380	29									Warning: No false call analysis.		0.07				
NAMES 1848 1000 0 0411127 040 04	HAYNES 188 AMS 5	5 plate	CE071(6)L.xls	6/4/15 11:25 PN	CASE 6				0.7791	0.0060 0.2	480 0.	3500	27					0.	3470	28 0.	.7000	29									analysis.		0.31	0.455			PT
HANES BARS Genome Genom Genome Genome Genome Genome </td <td></td> <td></td> <td></td> <td></td> <td></td> <td>0.0220</td> <td>0.0050</td> <td>0.9050</td> <td></td> <td></td> <td></td> <td></td> <td>0.03</td> <td>50</td> <td></td> <td>Warning: No false call analysis.</td> <td></td> <td></td> <td></td> <td>0.022</td> <td></td> <td></td>						0.0220	0.0050	0.9050					0.03	50																	Warning: No false call analysis.				0.022		
HANES BARS Gentline <								0.9050	0		0.	3500	0.25	00																			0.075				
And binding										0.0010 0.0										0	.1380	29									Warning: No false call analysis.						
219 A F.4 6445 5113.8 M 5445 6.00 5.00 5.00 <td></td> <td>29</td> <td></td> <td></td> <td></td> <td></td> <td>_</td> <td></td>																						29					_										
219 AT 910 At		plate				0.0380	0.0040	0.9050		0.2		1780	0.14	10																	Warning: No false call		0.025	0.035	0.038		
219 ATC 3100 M 641 51140 M 640 640 640 640 <td></td> <td>niste</td> <td></td> <td>Warning: No false call</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>		niste																													Warning: No false call						
219 ATC 948 9498 A 6491 51142 M GAS 6493 6493 6498 <th< td=""><td></td><td>plate</td><td></td><td></td><td></td><td></td><td></td><td></td><td>1 1</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>Warning: No false call</td><td></td><td>0.09</td><td>1</td><td></td><td></td><td></td></th<>		plate							1 1																						Warning: No false call		0.09	1			
219 H 47 jake 0108 LX5 64/5 1162 PM QSE 1 0.130 0.303 0.309 0 0 0 0<		piate																													Warning: No false call		0.03				
219 AT 0100 X 0401 S114 SP (AS 0401 S114 SP (AS 0400 S114 SP (AS 040		plate																													analysis.						
219 H46 pade 0100L0L0 64/15 1156 PM (OSE 10 0.55) 0.000 0.001 0.000		plate									_														29						analysis. Warning: No false call		0.025				
219 Ar Ar plate Diox00xX 64/15 11:48 PM CASE 6 V 0.667 0.080 0.10 V 0.10 V 0.10 V <td></td> <td>plate</td> <td></td> <td></td> <td></td> <td>0.1530</td> <td>0.0360</td> <td>0.9001</td> <td>1 1</td> <td></td> <td></td> <td></td> <td>0.52</td> <td>30</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>0.1520</td> <td>29</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>analysis.</td> <td></td> <td>0.09</td> <td></td> <td>0.153</td> <td></td> <td></td>		plate				0.1530	0.0360	0.9001	1 1				0.52	30										0.1520	29						analysis.		0.09		0.153		
219 H 747 plate 01002LX5 64/15 1162 PM QSE1 0.500 0.600 0.607 0.678		plate								0.0080 0.0			28					0.	1490	28 0.	3560	29									analysis.		0.06				
2219 N1-67 pade D102/BUXS 64/15 1152 PM CASE 2 0.048 0.007 0.0790 27 0.499 24 0		plate							1																						analysis.		0.17		0.29		
2219 AT 57 plate D1028LXCS 64/151152 PM CASE 2 02900 0.0460 9.9001 0.9790 27 0.4890 24 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		plate				0.0.00			1																	-							0.02				
2219 A/T-67 plate 01002CD XLS 64/15 1154 PMCASE 11 0.0578 0.0110 0.0055 0.1178 0.1788 0.1778	2219 AI T-87	plate				0.2900	0.0490	0.9001	1		0.	9790	27 0.48	90 24																	analysis.		0.125	0.295		1.000	UT
	2219 AI T-87	plate	D1002CD.XLS	6/4/15 11:54 PM	CASE 1*	0.0570	0.0110	0.9050	D		0.	1780	0.11	70																	analysis.		0.025	0.04	0.105	1.000	UT

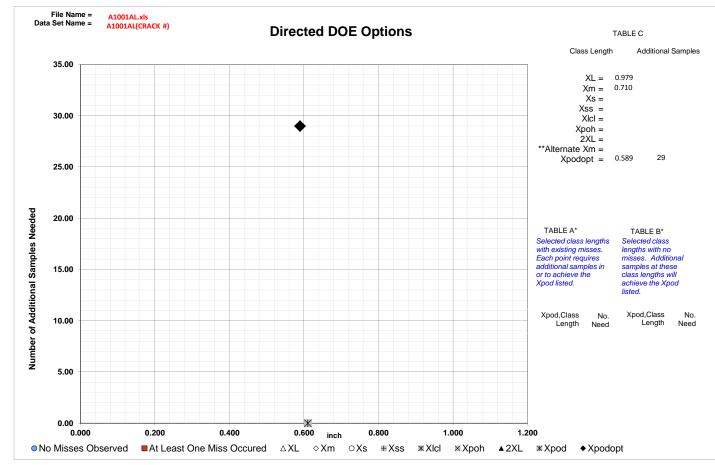
			Analysis	Xpod CLASS- CASE ID LENGTH	Xpod CLASS-	Best_LC C	Best_LCL B CLASS- C	Best_LCL CLASS-												Fa	alse Call	False Call	False Call	False Call	Length or Area per Inspection (in or in^2) =	False Call			NTIAC 90% NTI POD occurs occ	AC 90/95 urs at	PO	OH or DD @ METHO
MATERIAL	STRUCTURE					LV	WIDTH L	ENGTH XL	XL#Xm	Xm # Xs	Xs#X	(IcI X	cl# Xpoh	Xpoh	# 2XL	2XL# X	Kss	Kss # Xp	odopt Xp	odopt # U	CL F	Rate	Length (in)	Area (in^2)	(in or in^2) =	Opportunities	False Calls False Call Flag	MLE flag	POD occurs occ at (inch) POI		Р Хр	od D
2219 AI T-87	plate	D1002CL.XLS		CASE 1* 0.329				0.97																			Warning: No false call analysis. Warning: No false call		0.09	0.125		0.978 UT
2219 AI T-87	plate	D1003AD.XLS	6/4/15 11:57 PN	CASE 1# 0.038	0.0040 0.90	50		0.17	80 0.111	D									0.0375	29							analysis. Warning: No false call		0.015	0.02	0.038	1.000 UT
2219 AI T-87	plate	D1003AL.XLS		CASE 1# 0.102		01		0.61	00 0.262	D				_					0.1015	29							analysis.		0.055	0.07	0.102	1.000 UT
2219 AI T-87	plate	D1003BD.XLS	6/5/15 12:02 AM	CASE 1* 0.035	0.0030 0.90	77		0.17	80 0.110	D																	Warning: No false call analysis.		0.02	0.025	0.035	1.000 UT
2219 AI T-87	oloto	D1003BL.XLS	6/5/15 12:05 AM	CASE 1* 0.083	0.0080 0.90			0.61	00 0.262																		Warning: No false call	MLE Divergence Warning: Initial results	0.035	0.045	0.083	1.000 UT
2219 AI T-87	plate	D1003CD.XLS		CASE 2 0.046				0.01		12																	Warning: No false call	Land.	0.035	0.045		0.967 UT
22157011-07	plate	D1003CD.XL3	0.0/13 12.10 /0	CASE 2 0.040	0.0130 0.80			0.17	00 27 0.110	5 13																	anayaa.	MLE Divergence Warning: Initial results	0.055	0.05		0.507 01
2219 AI T-87	plate	D1003CL.XLS	6/5/15 12:12 AM	CASE 2 0.290	0.0490 0.90	01		0.61	00 18 0.380	0 17																	Warning: No false call analysis.	Warning: Initial results listed.	0.095	0.14		1.000 UT
2219 AI T-87	plate	D2002AD.XLS	6/5/15 12:13 AM	CASE 1* 0.036	0.0150 0.90	77		0.14	40 0.115	D																	Warning: No false call analysis.		0.025	0.04	0.094	1.000 UT
2219 AI T-87	plate	D2002AL.XLS	6/5/15 12:14 AM	CASE 1# 0.534	0.0600 0.90	01		0.55	00 0.538	D									0.2880	28							Warning: No false call analysis.		0.105	0.18	0.534	1.000 UT
2219 AI T-87	plate	D2002BD.XLS	6/5/15 12:15 AM	CASE 1* 0.036	0.0150 0.90	77		0.14	40 0.115	D																	Warning: No false call analysis.		0.03	0.045	0.094	1.000 UT
2219 AI T-87	plate	D2002BL.XLS	6/5/15 12:15 AM	CASE 1# 0.534	0.0600 0.90	01		0.55	00 0.538	D									0.2880	28							Warning: No false call analysis.		0.11	0.19	0.534	1.000 UT
2219 AI T-87	plate	D2002CD.XLS	6/5/15 12:16 AM	CASE 1* 0.036	0.0150 0.90	77		0.14	40 0.115	0																	Warning: No false call analysis.		0.02	0.03	0.046	1.000 UT
2219 AI T-87	plate	D2002CL.XLS	6/5/15 12:17 AM	CASE 1# 0.534	0.0600 0.90	01		0.55	00 0.538	D									0.4260	23							Warning: No false call analysis.		0.085	0.145	0.534	1.000 UT
Ti 6Al4V	plate	D3001AL.XLS	6/5/15 12:18 AM	CASE 1* 0.215	0.0350 0.90	01		0.40	0.265	D																	Warning: No false call analysis.		0.185	0.245	0.255	1.000 UT
Ti 6Al4V	plate	D3001BL.XLS		CASE 1# 0.300				0.40	70 0.345	D									0.2875	29							analysis. Warning: No false call analysis.		0.235	0.345		1.000 UT
Ti 6Al4V	plate	D3001CL.XLS		CASE 1# 0.250				0.40											0.2485	29									0.14	0.18		1.000 UT
Ti 6Al4V	plate	D3003AL.XLS	6/5/15 12:21 AM				0.0250	0.2350							0.8140	29											analysis. Warning: No false call analysis.		0.265	0.555		UT
																											Warning: No false call	MLE Divergence Warning: Initial results				
Ti 6Al4V	plate	D3003BL.XLS	6/5/15 12:22 AM					0.40		0								1	0.1760	15							analysis.	listed.	0.115	0.14		1.000 UT
Ti 6Al4V	plate	D3003CL.XLS		CASE 1* 0.216	0.0340 0.90			0.40		D																	Warning: No false call analysis. Warning: No false call		0.135	0.185	0.216	1.000 UT
SS AMS 355	hole	D4004.XLS	6/5/15 12:24 AM			0.4729		0.0512 0.25					0.0		28												Warning: No faise call analysis. Warning: No faise call		0.075	0.095		UT
SS AMS 355	hole	D5004.XLS	6/5/15 12:25 AM	CASE 4		0.8855	0.0230	0.0902 0.09	02 4			0.0902	4 0.0	902	0.1803	29											warning: No faise call analysis.		0.245	0.51		UT
STEEL 4340	plate	D6001AL.XLS	6/5/15 12:28 AM	CASE 6		0.8931	0.0800	0.2620 2.40	30 28				1.6	030 :	28 4.8060	29											analysis. Warning: No false call analysis.		0.4			UT
STEEL 4340	plate	D6001BL.XLS	6/5/15 12:30 AM	CASE 2 0.250	0.0700 0.90	01		2.40	30 27 1.603	28																	Warning: No false call analysis.		0.315			1.000 UT
STEEL 4340	plate	D6001CL.XLS	6/5/15 12:31 AM	CASE 6		0.8931	0.0800	0.2620 2.40	30 28				1.6	030 :	28 4.8060	29											Warning: No false call analysis.		0.33			UT
STEEL 4340	plate	D6003AL.XLS	6/5/15 12:33 AM	CASE 6		0.8368	0.0130	0.1183 2.40	30 28				1.6	030 :	28 4.8060	29											Warning: No false call analysis.		0.575			UT
STEEL 4340	plate	D6003BL.XLS	6/5/15 12:35 AM	CASE 6		0.8813	0.0680	0.2620 2.40	30 28				1.6	030 :	28 4.8060	29											Warning: No false call analysis.		0.43			UT
STEEL 4340	plate	D6003CL.XLS	6/5/15 12:37 AM	CASE 6		0.8813	0.0680	0.2620 2.40	30 28				1.6	030 :	28 4.8060	29											Warning: No false call analysis.		0.45			UT
SS AMS 355	hole	D7001L.XLS	6/5/15 12:39 AM	CASE 1# 0.083	0.0220 0.90	01		0.34	25 0.169	4									0.0738	3							analysis. Warning: No false call analysis.		0.115	0.155	0.08333	1.000 UT
SS AMS 355	hole	D7002L.XLS	6/5/15 12:40 AM	CASE 1# 0.066	3 0.0210 0.90	01		0.34	25 0.169	4									0.0659	1							Warning: No false call analysis.		0.105	0.165	0.06626	1.000 UT
SS AMS 355	hole	D7003L.XLS		CASE 1# 0.083				0.34		4									0.0782	4							Warning: No false call analysis.		0.065	0.075	0.08333	1.000 UT
2219 AI T-87	stringer panel	D8001(3)D.xls	6/5/15 12:42 AM				0.0020						0.0	730 :	26 0.1900	29											Warning: No false call analysis.		0.055	0.065		UT
2219 AI T-87		D8001(3)L.xls		CASE 2 0.164	0 0.0040 0.90			0.68		23																	Warning: No false call analysis.		0.34	0.51		1.000 UT
2219 AI T-87	stringer panel	D8002(3)D.xls		CASE 1* 0.044				0.09																			analysis. Warning: No false call analysis.		0.045	0.05		1.000 UT
2219 AI T-87	stringer panel	D8002(3)L.xls		CASE 1* 0.200				0.68																			Warning: No false call analysis.		0.22	0.255		1.000 UT
2219 AI T-87		D8003(3)D.xls		CASE 2 0.042				0.09																			Warning: No false call analysis		0.06	0.065		1.000 UT
2219 AI T-87		D8003(3)L.xls		CASE 2 0.276				0.68																			Warning: No false call		0.37	0.46		1.000 UT
2219 AI T-87/w2319	weld LOP	D9001(3)D.xis	6/5/15 12:52 AM		0.0030 0.80	0.6070	0.0010	0.1030	~0 13 0.305	20					0.3200	20											analysis. Warning: No false call analysis.		0.57	0.40		1.000 UT
2219 AI T-87/w2319	weld LOP	D9001(3)L.xls	6/5/15 12:54 AM			0.6070		0.3380							2.5420	20											Warning: No false call analysis.					UT
																25											Warning: No false call					
2219 AI T-87/w2319	weld LOP	D9002(3)D.xls	6/5/15 12:57 AN			0.6070		0.1030							0.3200	29											Warning: No false call analysis.		0.005			UT UT
2219 AI T-87/w2319	weld LOP	D9002(3)L.xls	6/5/15 12:59 AM	CASE 7		0.7169	0.0040	0.3410						_	2.5420	29												MLE Divergence Warning: Initial results	0.005			UT
2219 AI T-87/w2319	weld LOP	D9003(3)D.xls	6/5/15 1:02 AM	CASE 1* 0.063	0.0020 0.90	50		0.16	00 0.105	0																	Warning: No false call analysis.	listed.	0.005	0.015	0.104	1.000 UT
																											Warning: No false call	MLE Divergence Warning: Initial results				
2219 AI T-87/w2319		D9003(3)L.xls	6/5/15 1:19 AM		0.0170 0.90			1.27	10 0.846																		analysis. Warning: No false call analysis.	listed.	0.11	0.16	1.158	1.000 UT
2219 AI T-87/w2319		D9004(3)D.xls	6/5/15 1:32 AM			0.8444	0.0010	0.0440							0.3200	29											analysis. Warning: No false call analysis.					UT
2219 AI T-87/w2319	weld LOP	D9004(3)L.xls	6/5/15 1:33 AM			0.7791	0.0010	0.2940							1.5000	29											analysis. Warning: No false call					UT
2219 AI T-87/w2319	weld LOP	D9005(3)D.xls	6/5/15 1:36 AM				0.0030	0.1050							0.3200												analysis. Warning: No false call					UT
2219 AI T-87/w2319	weld LOP	D9005(3)L.xls	6/5/15 1:38 AM	CASE 6		0.7169	0.0040	0.3410 1.27	10 26				1.2	450 :	26 2.5420	29											analysis.	MLE Divergence				UT
2219 AI T-87/w2319	weld LOP	D9006(3)D.xls	6/5/15 1:40 AM	CASE 1# 0.097	0 0.0010 0.90	50		0.16	00 0.128	D									0.0940	20							Warning: No false call analysis.	MLE Divergence Warning: Initial results listed.	0.015	0.02	0.097	1.000 UT
																											Warning: No false call	MLE Divergence Warning: Initial results				
2219 AI T-87/w2319	weld LOP	D9006(3)L.xls	6/5/15 1:58 AM		0.0140 0.90			0.88	90 0.742	0																	Warning: No faise call	listed.	0.03	0.1	0.659	1.000 UT
2219 AI T-87/w2319		DA001(3)D.xls					0.0190	0.0930							0.4300												Warning: No false call analysis. Warning: No false call analysis.					UT
2219 AI T-87/w2319	weld LFC	DA001(3)L.xls	6/5/15 2:19 AM			0.8931		0.1650 1.69					1.6	-	26 3.3920							_					analysis.					UT
2219 AI T-87/w2319	weld LFC	DA002(3)D.xls	6/5/15 2:20 AN	CASE 6		0.6467	0.0110	0.0450 0.21	50 26				0.2	150	26 0.4300	29											Warning: No false call analysis. Warning: No false call					UT
2219 AI T-87/w2319	weld LFC	DA002(3)L.xls	6/5/15 2:21 AM	CASE 6		0.7791	0.0920	0.2570 1.18	80 26				1.1	880 :	26 2.3760	29											analysis.					UT
2219 AI T-87/w2319	weld LFC	DA003(3)D.xis	6/5/15 2:23 AM	CASE 2 0.087	0 0.0220 0.91	29		0.21	50 20 0.151	29																	Warning: No false call analysis.		0.145			1.000 UT
																											Warning: No false call	MLE Divergence Warning: Initial results				
2219 AI T-87/w2319		DA003(3)L.xls	6/5/15 2:24 AM		0 0.0520 0.91			1.69	60 17 0.560	11																	analysis. Warning: No false call peoplerin	isted.	0.35			1.000 UT
2219 AI T-87/w2319		DB001(3)D.xls	6/5/15 2:25 AM				0.0010	0.0400							0.4700												analysis. Warning: No false call		0.18			UT
2219 AI T-87/w2319		DB001(3)L.xls	6/5/15 2:27 AM				0.1000								2.8700	29											analysis. Warning: No false call					UT
2219 AI T-87/w2319		DB002(3)D.xls	6/5/15 2:28 AM					0.23		20																	analysis. Warning: No false call					1.000 UT
2219 AI T-87/w2319		DB002(3)L.xis	6/5/15 2:29 AN		0.0330 0.90	50		1.43	50 17 1.085	23																	analysis. Warning: No false call					1.000 UT
2219 AI T-87/w2319	weld TFC	DB003(3)D.xls	6/5/15 2:30 AM	CASE 6		0.7791	0.0010	0.0400 0.23	50 26				0.2	350	26 0.4700	29											analysis.					UT

MATERIAL STRUCTURE FILE NAME	Analysis Date/Time CASE	Xpod CLASS-	Xpod - CLASS- H WIDTH	Best_LC	Best_LCL Bes CLASS- CLA WIDTH LEN	ILCL ASS- NGTH XL	XI #	Xm Xm	ii Xs	Xs # X	ici Xici	If Xnoh	Xpoh #	2XI 2XI	I # Xss	Xss # Xnodont X	False Call	False Call Rate	False Call	False Call Area (in^2)	Length or Area per Inspection (in or in^2) =	False Call Opportunities	False Calls False Call Flag	PC	TIAC 90% NTL DD occurs occ (inch) POL	AC 90/95 ursat D (inch) XP	POH POD Xpod	or METHO D
2219 AI T-87/w2319 weld TFC DB003(3)L.xls				0.866		_	.4350 2	6					760 20	2.8700	29						(Warning: No false call analysis.		()	(UT
																							Warning: No false call	MLE Divergence Warning: Initial results				
2219 AI T-87/w2319 weld flush LFC DC001(3)D.xls				0 0.9050			.2760	0.2150				_	_					-					analysis. Warning: No false call	listed.	0.03			1.000 UT
2219 AI T-87/w2319 weld flush LFC DC001(3)L.xls				0 0.9050			.5620	1.1190										-					analysis. Warning: No false call	<u> </u>	0.18			1.000 UT
2219 AI T-87/w2319 weld flush LFC DC002(3)D.xls							.2760 2	6 0.2150	17			_	_					-					analysis. Warning: No false call		0.06	0.105		1.000 UT
2219 AI T-87/w2319 weld flush LFC DC002(3)L.xls 2219 AI T-87/w2319 weld flush LFC DC003(3)D.xls				0 0.9050			.5620	0.2150				-	-					-					analysis. Warning: No false call analysis		0.235		.895 1	1.000 UT
2219 AI T-87/w2319 weld flush LFC DC003(3)D.xis 2219 AI T-87/w2319 weld flush LFC DC003(3)L.xis							.5620	1.1190				-	-					-					Warning: No false call		0.045		.348 1	1.000 UT
2219 AI T-87/w2319 weld flush TFC DD001(3)D.xls			00 0.029	0.9050	9 0.0120	0.1150 0		0.1.1190				0.2	150 26	0.4300	20								Warning: No false call		0.165	0.235 0.	.346 1	UT
2219 AI T-87/w2319 weld flush TFC DD001(3)L.xis						0.2970 0		6				0.49	-	0.9900	29								Warning: No false call analysis.		0.64			UT
2219 AI T-87/w2319 weld flush TFC DD002(3)D.xls				0.866		0.1100 0		6				0.2		0.4300	29								Warning: No false call analysis		0.13			UT
2219 AI T-87/w2319 weld flush TFC DD002(3)E.xis	6/5/15 3:03 AM CASE 0			0.820		0.2390 0		6				0.4		0.9900	29								Warning: No false call analysis		0.13			UT
2219 AI T-87/w2319 weld flush TFC DD003(3)D.xls				0.315		0.0660	.4000 2					0.4	555 20	0.4300	29								Warning: No false call analysis		0.57			UT
2219 AI T-87/w2319 weld flush TFC DD003(3)Lxis	6/5/15 3:05 AM CASE 7			0.271		0.1780								0.9900	29								Warning: No false call analysis.		0.005			UT
IN 718 and HAYNES plate E1001AL.XLS	6/5/15 3:07 AM CASE 6			0.570		0.1900 0	.4220 2	8				0.42	220 28	0.8440	29								Warning: No false call analysis.					VT
IN 718 and HAYNES plate E1002ALXLS				0.716		0.3010 0		8				0.43	220 28	0.8440	29								Warning: No false call analysis.		0.595			VT
																							Warning: No false call	MLE Divergence Warning: Initial results listed.				
SS AMS 355 hole E2006.XLS	6/5/15 3:11 AM CASE 7	7		0.720	06 0.0180	0.0669								0.5150	29			-					analysis.		0.28	0.715		VT
2219 AI T-87 plate F10001AA.XL	6/5/15 3:13 AM CASE (в		0.651	0.0100	0.5273 0	.8091 2	8				0.80	091 28	1.6182	29								Warning: No false call analysis.	MLE Divergence Warning: Initial results listed.				RT
2219 AI T-87 plate F10001BA.XL	5 6/5/15 3:14 AM CASE 6				0.0100	0.5136 0						0.80		4.0400	~								Warning: No false call	MLE Divergence Warning: Initial results				RT
2219 AI T-87 plate F10001BA.XL 2219 AI T-87 plate F10001CA.XL			-	0.472		0.5136 0		°		\vdash		0.80	091 28	1.6182	29								analysis. Warning: No false call	isted.			-	RT
2219 AI T-87 plate F10001CA.XL 2219 AI T-87 plate F10002AA.XL			33 0.000	0.549	0.0050		.8091	0.6500						1.0182	28	0.5780	29						analysis. Warning: No false call		0.605	0.75 0.58		RT 1.000 RT
2219 AI T-87 plate F10002AA.XL				0 0.9001			.8091	0.0500								0.5780	28						Warning: No false call	t	0.605	0.585 0.67		0.970 RT
2219 AI 1-87 plate F100028A.XL				0 0.9001			1.8091 4		20														Warning: No false call		0.46	0.565 0.67		1.000 RT
2219 AI T-87 plate F10002CA.XL			33 0.000	0.894	9 0.3000	0.8091	1.0091 4		.0					1.6182	29								Warning: No false call		0.055	0.475	- '	RT
2219 AI T-87 plate F10003AA.XL			45 0.069	0.9001	0.3000		.8091	0.6000						1.0102	25								Warning: No false call		0.435	0.525 0.53	2222 1	1.000 RT
2219 AI T-87 plate F10003CA.XL							.8091	0.6833								0.5917	29						Warning: No false call analysis		0.505			1.000 RT
2219 AI T-87 plate F10601AD.XL			0.002	0.039	98 0.0040	0.0370		0.0000						0.0860	29	0.0511	2.5						Warning: No false call analysis.		0.128	0.000	0.0	RT
																							Warning: No false call	MLE Divergence Warning: Initial results listed.				
2219 AI T-87 plate F10601AL.XL	6/5/15 3:30 AM CASE 7	7	_	0.062	28 0.0020	0.2580			-				_	0.6840	29								analysis.	M E Diversione				RT
2219 AI T-87 plate F10601BD.XL	5 6/5/15 3:32 AM CASE 7	7		0.006	64 0.0010	0.0270								0.0860	29								Warning: No false call analysis.	Warning: Initial results listed.				RT
																							Warning: No false call	MLE Divergence Warning: Initial results				RT
2219 AI T-87 plate F10601BL.XL	6/5/15 3:33 AM CASE 7	7		0.012	27 0.0010	0.0600								0.6840	29								analysis.	listed. MLE Divergence				RT
2219 AI T-87 plate F10601CD.XL	6/5/15 3:35 AM CASE 7	7		0.012	0.0010	0.0190								0.0860	29								Warning: No false call analysis.	Warning: Initial results listed.				RT
2219 AI T-87 plate F10601CL.XL	6/5/15 3:35 AM CASE 7			0.012	0.0010	0.2590								0.6840									Warning: No false call	MLE Divergence Warning: Initial results				RT
2219 AI T-87 plate F10601CL.XL 2219 AI T-87 plate F10602AD.XL			30 0.011		0.0010		.0430 (0 0.0430						0.6840	29	0.0420							analysis. Warning: No false call pophysis	Isled.		0.055		1.000 RT
2219 AI T-87 plate F10602AD.XL 2219 AI T-87 plate F10602AL.XL			30 0.011		31 0.2000			0 0.0430			0.3420	2 0.34	420	0.6840	29	0.0420	28						Warning: No false call		0.04	0.055		RT RT
2219 AI T-87 plate F10602AL:XL						0.0430	1.3420	-			0.3420	2 0.3	420	0.0860	29								Warning: No false call		0.035	0.045		RT
2219 AI T-87 plate F10602BL.XL			90 0.200		0.0140		.9790	0.7100						0.0000	2.5	0.5370	29						Warning: No false call analysis		0.345		539 1	1.000 RT
2219 AI T-87 plate F10602CD.XL			30 0.011				1.0430	0 0.0430								0.0420	29						Warning: No false call analysis.		0.04	0.055		1.000 RT
2219 AI T-87 plate F10602CL.XL				0.893	0.2000	0.3420 0		2			0.3420	2 0.34	420	0.6840	29								Warning: No false call analysis.		0.13	0.185		RT
2219 AI T-87 plate F10603AD.XL				0.863		0.0430								0.0860	29								Warning: No false call analysis.		0.03	0.035		RT
2219 AI T-87 plate F10603AL.XL						0.3420 0	.3420	2			0.3420	2 0.34	420	0.6840	29								Warning: No false call analysis.		0.095	0.125		RT
2219 AI T-87 plate F10603BD.XL	6/5/15 3:45 AM CASE	1# 0.04:	30 0.011	0.9001		0	1.0430	0 0.0430								0.0420	29						Warning: No false call analysis.		0.025	0.025	1	1.000 RT
2219 AI T-87 plate F10603BL.XL	6/5/15 3:45 AM CASE	1# 0.28	70 0.200	0 0.9253		0	.3420	0.3145	0					0.6840	1	0.2830	29						Warning: No false call analysis.		0.11	0.155 0.	.287 1	1.000 RT
2219 AI T-87 plate F10603CD.XL	5 6/5/15 3:46 AM CASE	1# 0.04	30 0.011	0.9001			1.0430 (0.0430								0.0420	29						Warning: No false call analysis.		0.035	0.05	1	1.000 RT
2219 AI T-87 plate F10603CL.XL	6/5/15 3:47 AM CASE	4		0.893	0.2000	0.3420 0	.3420	2			0.3420	2 0.34	420	0.6840	29								Warning: No false call analysis.		0.14	0.205		RT
2219 AI T-87 plate F12201AD.XL	5 6/5/15 3:48 AM CASE 7	7		0.720	06 0.0660	0 1780								0.3560	20								Warning: No false call analysis	MLE Divergence Warning: Initial results listed				RT
plate r12201AD.XL	Granta a:46 AM CASE			0.720	0.0000	J.1780								0.3000	20								Warning: No false call	Isted. MLE Divergence Warning: Initial results listed.				
2219 AI T-87 plate F12201AL.XL				0.741			.9790 2	8				0.6		1.9580	29			_	-				Warning: No false call analysis. Warning: No false call	listed.				RT
2219 AI T-87 plate F12201BD.XL			-	0.687			.1780 2				0.1780	21 0.13		0.3560	29								Warning: No tase call analysis. Warning: No false call		0.14	0.17	-	RT
2219 AI T-87 plate F12201BL.XL				0.607		0.5350 0	.9790 2	8				0.6	100 28	1.9580	29								analysis. Warning: No false call		0.625			RT
2219 AI T-87 plate F12201CD.XL			-	0.621	1	0.1490							-	0.3560	29			-	-				analysis. Warning: No false call		0.185			RT
2219 AI T-87 plate F12201CL.XL			-	0.687		0.5430 0		8		\square		0.6		1.9580	29			-	-				analysis. Warning: No false call				_	RT
2219 AI T-87 plate F12202AD.XL			-	0.881			.1780	5			0.1780	5 0.13		0.3560	29			-					analysis. Warning: No false call		0.13	0.185		RT
2219 AI T-87 plate F12202AL.XL			-	0.860			.9790 2	8			0.5680	9 0.56	680					-					analysis. Warning: No false call		0.62			RT RT
2219 AI T-87 plate F12202BD.XL				0.873	9 0.0750	0.1490	.9790	0.7100						0.3560	29	0.5370		-					analysis. Warning: No false call		0.09	0.115		
2219 AI T-87 plate F12202BL.XL 2219 AI T-87 plate F12202CD.XL			90 0.200	0 0.9152 0.873	9 0.0750	0.1490	1.9790	0.7100						0.3560	~	0.5370	29						analysis. Warning: No false call		0.345	0.465 0.	.539 1	1.000 RT RT
2219 AI T-87 plate F12202CD.XL 2219 AI T-87 plate F12202CL.XL			-	0.873			.9790 2			\vdash		0.49		0.3560	29								analysis. Warning: No false call		0.125	0.185	-	RT
2219 AI T-87 plate F12202CL.XL: 2219 AI T-87 plate F12203AD.XL				0.472		0.1530 0		0				0.49		0.3560	29								analysis. Warning: No false call		0.605	0.1		RT
2219 AI T-87 plate F12203AD.XL 2219 AI T-87 plate F12203AL.XL				0.876		0.1060 0	2	0				0.13	/ 30 28	0.3560	29								analysis. Warning: No false call		0.08	0.1		RI
zzid ALT-67 prate F12203ALXL	D/D/10 4:08 AM CASE 1			0.886	0.3000	0.0100				I – I			-	1.2200	23			_	-		-		analysis.		0.285	0.3/5		KI

		E FILE NAME	Analysis Date/Time		Xpod CLASS- LENGTH	Xpod CLASS-	Best_LC	Best_LCL Be CLASS- CL WIDTH LE	st_LCL ASS-												False	Call Fals	ise Call Fa	alse Call Fal	e Call	Length or Area per Inspection (in or in^2) =	False Call			NTIA POD	C 90% NTIA occurs occu ch) POD	C 90/95 rs at	POH or POD @ METHO
MATERIAL 2219 AJ T-87	STRUCTUR	F12203BD.XLS	Î.					WIDTH LE		0.1780	0.1485	# Xs	xs #)	CICI X	lcl#Xp	ooh Xpo	h#/2XI	L 2XL#	XSS	Xss # Xpodopt 0.1180	Xpodopt # UCL	Rab	ste Le	ength (in) Are	a (in^2)	(in or in^2) =	Opportunities	False Calls	False Call Flag	MLE flag at (in	ch) POD	0.105 0.1	Xpod D 19 1.000 RT
2219 AI T-87	plate	F12203BL.XLS								0.6100	0.5680	25								0.5290	29							u v	narysis. Varning: No false call Inalysis.		0.305	0.41 0.5	
2219 AI T-87	plate	F12203CD.XLS	6/5/15 4:12 A				0.866	8 0.0670	0.1260		17					0.1780	17 (0.3560 29										V a	Varning: No false call inalysis.		0.055	0.065	RT
2219 AI T-87	plate	F12203CL.XLS	6/5/15 4:14 A			0 0.200				0.6100	0.5430									0.5185	29							V a	Varning: No false call inalysis.		0.3	0.415 0.5	
2219 AI T-87	plate	F20002AA.XLS	6/5/15 4:16 A	M CASE 4			0.651	8 0.0910	0.6545	0.6545	22			0.6545	22	0.6182	23	1.3091 29										a	Varning: No false call inalysis.				RT
2219 AI T-87	plate	F20002BA.XLS	6/5/15 4:17 A	M CASE 4			0.651	8 0.0910	0.6545	0.6545	22			0.6545	22	0.6182	23	1.3091 29										v a	Varning: No false call nalysis.				RT
2219 AI T-87	alata	F20002CA.XLS	6/5/15 4:18 A	MCARE 0			0.761	6 0.0370	0.5182	0.6545	27					0.5636	20	1 3091 29										W	Varning: No false call	MLE Divergence Warning: Initial results			RT
2219 AI T-87	plate	F20852AD.XLS							0.0440	0.0540	28					0.0540		0.1080 25										0	Varning: No false call inalistis	issue.			RT
2219 AI T-87	plate	F20852AL.XLS					0.549		0.3260									0.7680 29										Vi a	Varning: No false call inalysis.				RT
2219 AI T-87	plate	F20852BD.XLS	6/5/15 4:22 A	MCASE 7			0.493		0.0540									0.1080 25											Varning: No false call inalysis.		0.13		RT
2219 AI T-87	plate	F20852BL.XLS					0.549	3 0.0140	0.3840	0.3840	24			0.3840	24	0.3840		0.7680 29										a	Varning: No false call inalysis.				RT
2219 AI T-87	plate	F20852CD.XLS	6/5/15 4:23 A	M CASE 7			0.561	9 0.0120	0.0540									0.1080 29										a	Varning: No false call nalysis.		0.095		RT
2219 AI T-87	plate	F20852CL.XLS	6/5/15 4:24 A	M CASE 7			0.638	3 0.2000	0.3840									0.7680 29										a	Varning: No false call inalysis.		0.505		RT
2219 AI T-87	plate	F22202AD.XLS	6/5/15 4:25 A	MCASE 4			0.651	8 0.0200	0.1440	0.1440	22			0.1440	22	0.1360	23 (0.2880 29										-	Varning: No false call nalysis.		0.14	0.2	RT
2219 AI T-87	plate	F22202AL.XLS	6/5/15 4:27 A	MCASE 7			0.779		0.4920		_	_						1.1000 29										a	Varning: No false call inalysis.				RT
2219 AI T-87	plate	F22202BD.XLS	6/5/15 4:28 A				0.652		0.1440			_						0.2880 29											Varning: No false call inalysis. Varning: No false call		0.14	0.195	RT
2219 AI T-87	plate	F22202BL.XLS					0.605		0.4920									1.1000 29		+								a	varning: No false call nalysis. Varning: No false call				RT
2219 AI T-87	plate	F22202CD.XLS					0.769		0.1440									0.2880 29										a	nalysis. Varning: No false call		0.15		RT
2219 AI T-87	plate	F22202CL.XLS				-	0.741			0.5500	22					0.5500		1.1000 29								_		a	nalysis. Varning: No false call inalysis.				RT
Ti 6Al4V	plate	F30651AD.XLS	6/5/15 4:33 A				0.741		0.0510									0.2000 29										a V	nalysis. Varning: No false call		0.05	0.11	RT
Ti 6Al4V Ti 6Al4V	plate	F30651AL.XLS F30651BD.XLS					0.720		0.4070								_	0.8140 29											nalysis. Varning: No false call		0.255	0.41	RT
Ti 6Al4V	plate	F30651BD.XLS	6/5/15 4:35 A				0.741		0.0510									0.2000 29										a V	inalysis. Varning: No false call		0.05	0.095	RI
Ti 6Al4V	plate	F30651CD.XLS					0.774		0.4070									0.2000 25										a V	nalysis. Varning: No false call volusio		0.04	0.48	RT
Ti 6Al4V	niste	F30651CL.XLS					0.741		0.2500									0.8140 25											Varning: No false call inalysis.		0.225	0.325	RT
Ti 6Al4V	plate	E30653AD XLS	6/5/15 4:40 A				0.779			0 1000	28					0.1000		0.2000 25											Varning: No false call inalysis.		0.120	0.02.0	RT
Ti 6Al4V	plate	F30653AL.XLS					0.807		0.0910									0.8140 29											Varning: No false call nalvsis.				RT
Ti 6Al4V	plate	F30653BD.XLS	6/5/15 4:42 A				0.687	7 0.0040	0.0160	0.1000	28					0.1000		0.2000 29										W a	Varning: No false call inalysis.				RT
Ti 6Al4V	plate	F30653BL.XLS					0.741	1 0.0170	0.0840									0.8140 29										8	Varning: No false call inalysis.				RT
Ti 6Al4V	plate	F30653CD.XLS	6/5/15 4:45 A	M CASE 6			0.636	0 0.0130	0.0290	0.1000	28					0.1000	28 (0.2000 29										a	Varning: No false call nalysis.				RT
Ti 6Al4V	plate	F30653CL.XLS	6/5/15 4:46 A	M CASE 7			0.741	1 0.0750	0.3250									0.8140 29											Varning: No false call nalysis.		0.73		RT
Ti 6Al4V	plate	F32251AD.XLS	6/5/15 4:47 A	MCASE 6			0.549		0.2150		28					0.3200		0.7040 29										4 	Varning: No faise call inalysis. Varning: No faise call				RT
Ti 6Al4V	plate	F32251AL.XLS	6/5/15 4:49 A				0.549		0.2150	0.3520	28	_				0.3200		0.7040 29										a	varning: No false call nalysis. Varning: No false call				RT
Ti 6Al4V	plate	F32251BD.XLS	6/5/15 4:52 A				0.418		0.0970		_							0.1940 29										a	nalysis. Varning: No false call		0.115		RT
Ti 6Al4V	plate	F32251BL.XLS				_	0.248		0.3520									0.7040 29										a	nalysis. Varning: No false call				RT
Ti 6Al4V	plate	F32251CD.XLS					0.248		0.3520									0.7040 29										a	inalysis. Varning: No false call				RT
Ti 6Al4V Ti 6Al4V	plate	F32251CL.XLS	6/5/15 4:55 A				0.248		0.3520		28					0.3520		0.7040 29											nalysis. Varning: No false call				RT
Ti 6Al4V	plate	F32253AD.XLS					0.683		0.2250		28					0.3520		0.7400 25										a V	inalysis. Varning: No false call		0.605		RI
Ti 6Al4V	plate	F32253AL.ALS	6/5/15 4:58 A				0.683		0.2250		27					0.3520		0.7400 25										a V	inalysis. Varning: No false call		0.605		RT
Ti 6Al4V	niste	F32253BL.XLS					0.677		0.2470		27					0.3700		0.7400 25										W a	Varning: No false call inalysis.		0.365	0.695	RT
Ti 6Al4V	plate	F32253CD.XLS	6/5/15 5:01 A				0.741		0.0580		28					0.1030		0.2060 25										W	Varning: No false call inalysis.		0.18	0.000	RT
Ti 6Al4V	plate	F32253CL.XLS					0.607		0.2120							0.3700		0.7400 29										W	Varning: No false call inalysis				RT
STEEL 4340	plate	F40601A.XLS	6/5/15 5:04 A				0.549		0.0913				-					0.4960 29											Varning: No false call natysis.				RT
STEEL 4340	plate	F40601B.XLS	6/5/15 5:05 A	MCASE 7			0.529		0.0943									0.4960 29											Varning: No false call nalysis.				RT
STEEL 4340	plate	F40601C.XLS	6/5/15 5:06 A	MCASE 7			0.450	4 0.0070	0.1163									0.4960 29										Vi a	Varning: No false call inalysis.				RT
STEEL 4340	plate	F40603A.XLS	6/5/15 5:08 A				0.687		0.0943		28					0.1750		0.4960 29										v a	Varning: No false call inalysis. Varning: No false call		0.265		RT
STEEL 4340	plate	F40603B.XLS	6/5/15 5:09 A				0.687		0.0943		28					0.2480		0.4960 29										~	Varning: No false call inalysis. Varning: No false call		0.49		RT
STEEL 4340	plate	F40603C.XLS	6/5/15 5:10 A				0.716		0.0953		28					0.1750		0.4960 29		+									varning: No false call nalysis. Varning: No false call		0.265		RT
STEEL 4340	plate	F42501A.XLS	6/5/15 5:12 A				0.248		0.3300		28					1.6030		4.8060 29										a	varning: No false call varning: No false call				RT
STEEL 4340	plate	F42501B.XLS	6/5/15 5:13 A			-	0.134		0.4000		28					1.6030		4.8060 25											nalysis. Varning: No false call				RT
STEEL 4340	plate	F42501C.XLS	6/5/15 5:16 A				0.223		0.3300		28					1.6030	_	4.8060 29										a	nalysis. Varning: No false call				RT
STEEL 4340 STEEL 4340	plate	F42503A.XLS	6/5/15 5:17 A				0.794		0.3500		28					1.6030	28 4	4.8060 29										a V	inalysis. Varning: No false call		0.66		RT
STEEL 4340 STEEL 4340	plate	F42503B.XLS	6/5/15 5:20 A				0.761		0.3500		28					0.5320	28											a V	nalysis. Varning: No false call nalysis		0.66		RT
2219 AI T-87	weld LOP	F5001(3)D.xis	6/5/15 5:20 A				0.794		0.3500		26						28	0.3200 29										a V	natysis. Varning: No false call inalysis.		0.575		RT
2219 AI T-87	weld LOP	F5001(3)L.xls	6/5/15 5:22 A			0 0.058		0.0010		1.2100	1,1750																		Varning: No false call Inalysis.		0.10	1.1	
2219 AI T-87	weld LOP	F5002(3)D.xls	6/5/15 5:26 A				0.866	6 0.0010	0.0500		26					0.1600	26 (0.3200 29											Varning: No false call inalysis.				RT
2219 AI T-87	weld LOP	F5002(3)L.xls	6/5/15 5:28 A			0.049	0 0.9050			1.2100	0.8250	8																V a	Varning: No false call inalysis.			1.1	
																												W	Varning: No false call	MLE Divergence Warning: Initial results			
2219 AI T-87	weld LOP	F5003(3)D.xls	6/5/15 5:30 A	M CASE 2	0.0720	0.002	U 0.9050			0.1600	20 0.1050	8																a	inalysis.	listed. MLE Diverseore	0.005	0.005	1.000 RT
2219 AI T-87	weld LOP	F5003(3)L.xls	6/5/15 5:41 A	MCASE 2	0.6880	0.017	0.9050			1.2100	16 1.0790	14																V a	Varning: No false call nalysis.	Warning: Initial results listed.	0.005	0.005	1.000 RT

			Analysis CLASS- CLASS-	L	Best_LCL B CLASS- C	lest_LCL			1			1							5-1 0-II	5-1 0-II	5-1 0-II	F-1 0	Length or Area per Inspection	5-1 0-II				NTIAC 90% POD occurs	NTIAC 90/95	POH	or @ METHO
MATERIAL	STRUCTURE	FILE NAME	Analysis CLASS- CLASS- Date/Time CASE ID LENGTH WIDTH LCL	L Best_LC	WIDTH L	ENGTH	XL X	L#Xm	Xm #	Xs X:	s # Xici	Xici #	Xpoh	Xpoh #	2XL	2XL #	Xss	Xss # Xpodopt Xpodopt #		Rate					False Calls	False Call Flag	MLE flag		POD (inch)		
2219 AI T-87		F6001(3)D.xis	6/5/15 5:49 AM CASE 7	0.6070	0.0050	0.1780									0.430	0 29										Warning: No false call analysis.					RT
2219 AI T-87	weld LFC	F6001(3)L.xls	6/5/15 5:50 AM CASE 7	0.6070	0.0070	0.0790									2.376	0 29										Warning: No false call analysis.					RT
2219 AI T-87	weld LFC	F6002(3)D.xls	6/5/15 5:52 AM CASE 7	0.5709	0.0420	0.2150									0.430	0 29										Warning: No false call analysis.					RT
2219 AI T-87	weld LFC	F6002(3)L.xls	6/5/15 5:53 AM CASE 6	0.6070	0.0050	0.5030	1,1880	26					1.1	1880 26	2.376	0 29										Warning: No false call analysis.					RT
2219 AI T-87	weld LFC	F6003(3)D.xls	6/5/15 5:55 AM CASE 4	0.8666	0.0620	0.2150	0.2150	8			0	2150	8 0.3	2150	0.430	0 29										Warning: No false call analysis.					RT
2219 AI T-87	weld LFC	F6003(3)L.xls	6/5/15 5:56 AM CASE 4	0.8190	0.3000	1.1880	1.1880	14			1	.1880	14 0.9	9810 26	2.376	0 29										Warning: No false call analysis.					RT
2219 AI T-87	weld TFC	F7001(3)D.xis	6/5/15 5:58 AM CASE 4	0.6070	0.0420	0.2350	0.2350	23			0	.2350 2	23 0.1	2350	0.470	0 29										Warning: No false call analysis.					RT
2219 AI T-87	weld TFC	F7001(3)L.xls	6/5/15 5:59 AM CASE 6	0.6070	0.0130	0.2730	1,4350	26					12	4350 26	2.870	0 29										Warning: No false call analysis.					RT
2219 AI T-87	weld TFC	F7002(3)D.xis	6/5/15 6:01 AM CASE 4	0.6070	0.0420	0.2350	0.2350	23			0	.2350 2	23 0.1	2350	0.470	0 29										Warning: No false call analysis.					RT
2219 AI T-87	weld TFC	F7002(3)L.xls	6/5/15 6:03 AM CASE 6	0.6070	0.0130	0.2730	1.4350	26					1.	4350 26	2.870	0 29										Warning: No false call analysis.					RT
2219 AI T-87	weld TFC	F7003(3)D.xls	6/5/15 6:05 AM CASE 6	0.8190	0.0050	0.0480	0.2350	26					0.3	2350 26	0.470	0 29										Warning: No false call analysis.					RT
2219 AI T-87	weld TFC	F7003(3)L.xls	6/5/15 6:06 AM CASE 6	0.7933	0.0240	0.3060	1.4350	26					1.	4350 26	2.870	0 29										Warning: No false call analysis.					RT
2219 AI T-87	weld flush LFC	F8001(3)D.xls	6/5/15 6:08 AM CASE 4	0.8444	0.0610	0.2760	0.2760	11			0	.2760	11 0.3	2760	0.552	0 29										Warning: No false call analysis.					RT
																										Warning: No false call	MLE Divergence Warning: Initial results				
2219 AI T-87	weld flush LFC	F8001(3)L.xls	6/5/15 6:09 AM CASE 7	0.8739	0.6000	1.5620			_		_		_		3.124	0 29					-					analysis.	listed. MLE Divergence				RT
2219 AI T-87	weld flush LFC	F8002(3)D.xls	6/5/15 6:11 AM CASE 4	0.8931	0.0690	0.2760	0.2760	2			0	2760	2 0.3	2760	0.552	0 29										Warning: No false call analysis.	Warning: Initial results listed.	•			RT
2219 AI T-87	weld flush LFC	F8002(3)L.xls	6/5/15 6:12 AM CASE 4	0.8813	0.5000	1.5620	1.5620	5			1	.5620	5 1.5	5620	3.124	0 29										Warning: No false call analysis.					RT
2219 AI T-87	weld flush LFC	F8003(3)D.xls	6/5/15 6:15 AM CASE 4	0.8931	0.0690	0.2760	0.2760	2			0	.2760	2 0.3	2760	0.552	0 29										Warning: No false call analysis.					RT
2219 AI T-87	weld flush LFC	F8003(3)L.xls	6/5/15 6:17 AM CASE 1* 0.3530 0.0300 0.905	0			1.5620	1.1	190																	Warning: No false call analysis.				1.061 1	.000 RT
2219 AI T-87	weld flush TFC	F9000CD.XLS	6/5/15 6:18 AM CASE 7	0.5619	0.0120	0.0540									0.108	0 29										Warning: No false call analysis.		0.095			RT
																											MLE Divergence Warning: Initial results				
2219 AI T-87	weld flush TFC	F9001(3)D.xls	CASE 7											_	0.430	0 29											listed. MLE Divergence				RT
2219 AI T-87	weld flush TFC	F9001(3)L.xls	CASE 7												0.990	0 29											Warning: Initial results listed.				RT
																										Warning: No false call	MLE Divergence Warning: Initial results				
2219 AI T-87	weld flush TFC	F9002(3)D.xls	6/5/15 6:19 AM CASE 4	0.3684	0.0010	0.2150	0.2150	26			0	.2150 2	26 0.3	2150	0.430	0 29										analysis.	listed. MLE Divergence				RT
2219 AI T-87	weld flush TFC	F9002(3)L.xls	6/5/15 6:20 AM CASE 4	0.3684	0.0010	0.4950	0.4950	26			0	.4950 2	26 0.4	4950	0.990	0 29										Warning: No false call analysis.	Warning: Initial results listed.	0.56			RT
																										Warning: No false call	MLE Divergence Warning: Initial results				
2219 AI T-87	weld flush TFC	F9003(3)D.xls	6/5/15 6:21 AM CASE 4	0.3684	4 0.0010	0.2150	0.2150	26			0	.2150 2	26 0.3	2150	0.430	0 29										analysis.	listed. MLE Divergence				RT
2219 AI T-87	weld flush TFC	F9003(3)L.xls	6/5/15 6:22 AM CASE 4	0.3684	0.0010	0.4950	0.4950	26			0	.4950	26 0.4	4950	0.990	0 29										Warning: No false call analysis.	Warning: Initial results listed.	0.56			RT
2219 AI T-87	plate	G10003AA.XLS	6/5/15 6:23 AM CASE 7	0.8514	4 0.0930	0.6333									1.633	3 29										Warning: No false call analysis.		0.64			нт
2219 AI T-87	plate	G10003AD.XLS	6/5/15 6:25 AM CASE 4	0.8190	0.0490	0.1260	0.1780	28			0	.1260	14 0.1	1260												Warning: No false call analysis.		0.095			нт
2219 AI T-87	plate	G10003AL.XLS	6/5/15 6:26 AM CASE 1* 0.3220 0.0750 0.900	1			0.6100	0.5	350																	Warning: No false call analysis.		0.245	0.4	0.475 1	.000 HT
2219 AI T-87	plate	G10003BA.XLS	6/5/15 6:27 AM CASE 7	0.6532	0.2000	0.6833									1.618	2 29										Warning: No false call analysis.					нт
2219 AI T-87	plate	G10003BD.XLS	6/5/15 6:29 AM CASE 7	0.8074	4 0.0300	0.1260									0.356	0 29										Warning: No false call analysis.		0.105	0.17		HT
2219 AI T-87	plate	G10003BL.XLS	6/5/15 6:30 AM CASE 6	0.7794	0.0530	0.2950	0.6100	27					0.8	5680 23	1.220	0 29										Warning: No false call analysis.		0.46	0.63		нт
SS AMS 355	hole	G2001L.XLS	6/5/15 6:31 AM CASE 1# 0.0845 0.0260 0.900	1			0.2425	0.1	694									0.0774 2								Warning: No false call analysis.		0.075	0.1	0.08452 1	.000 HT



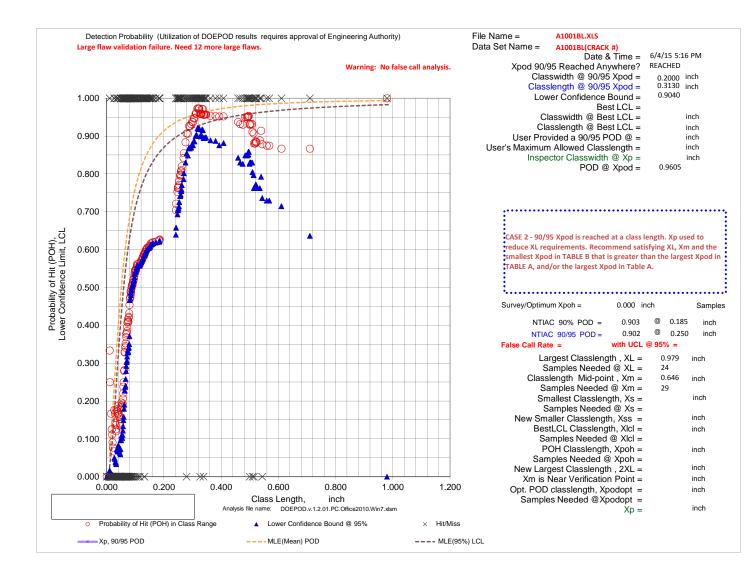


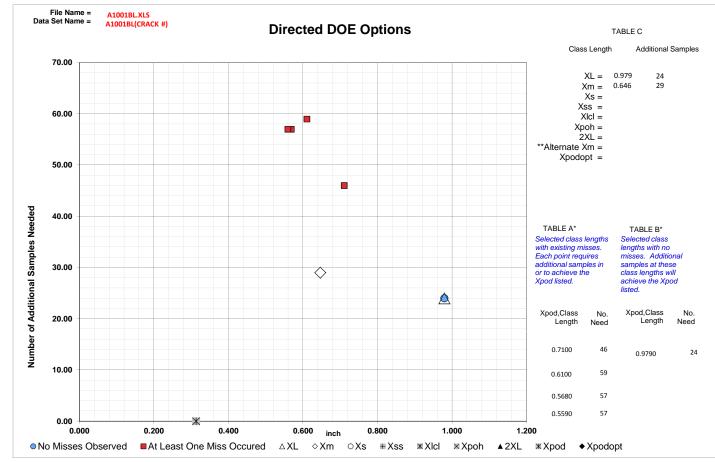
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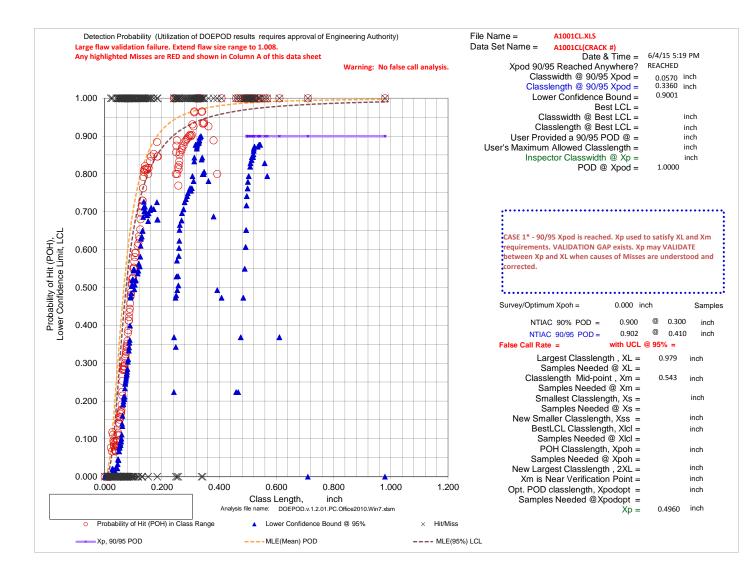


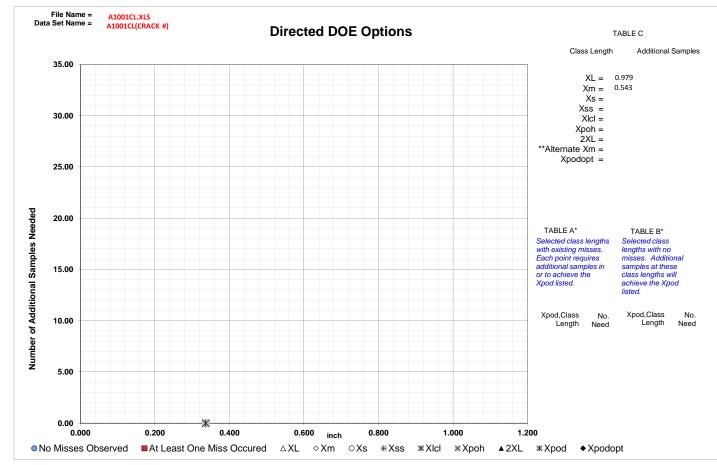
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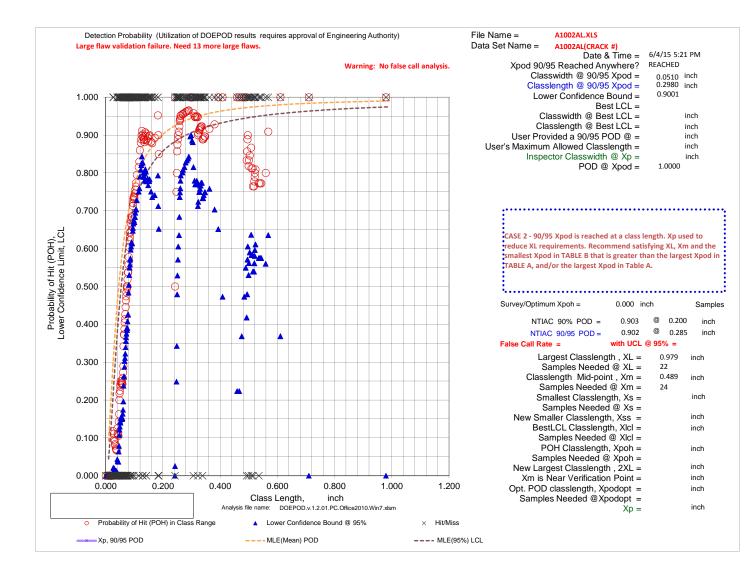


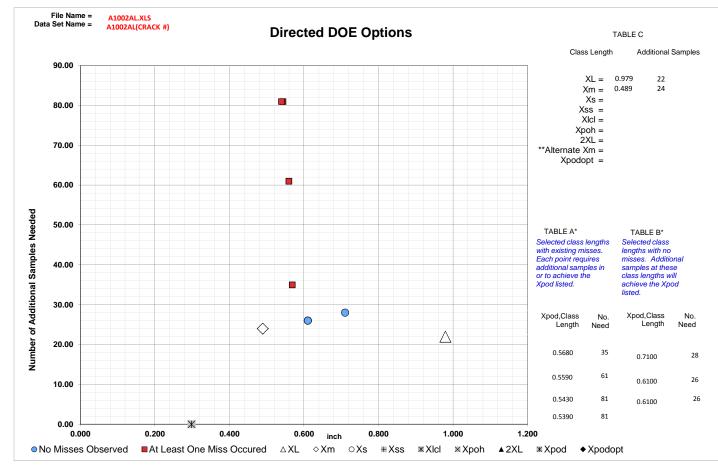
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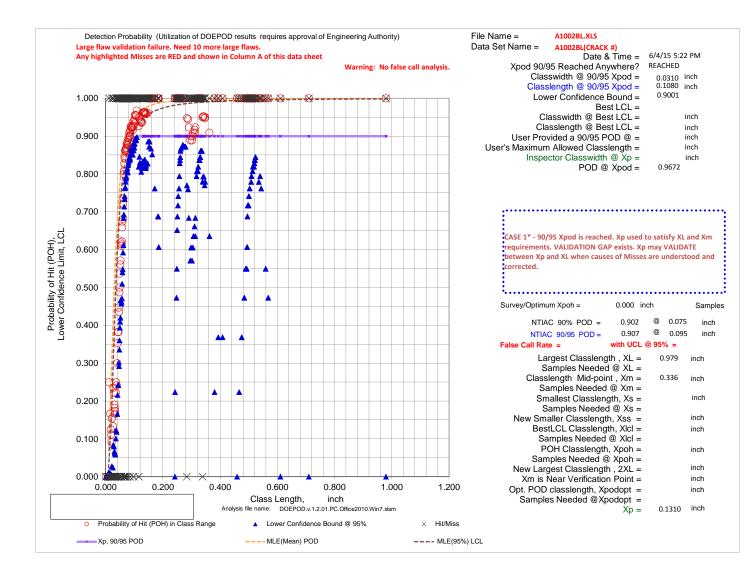


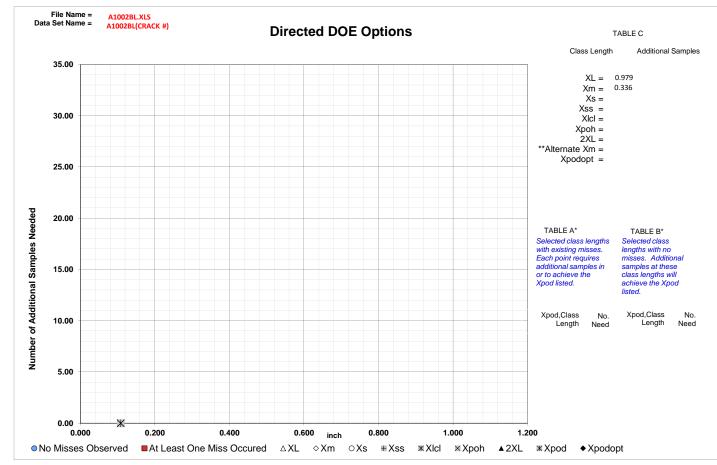
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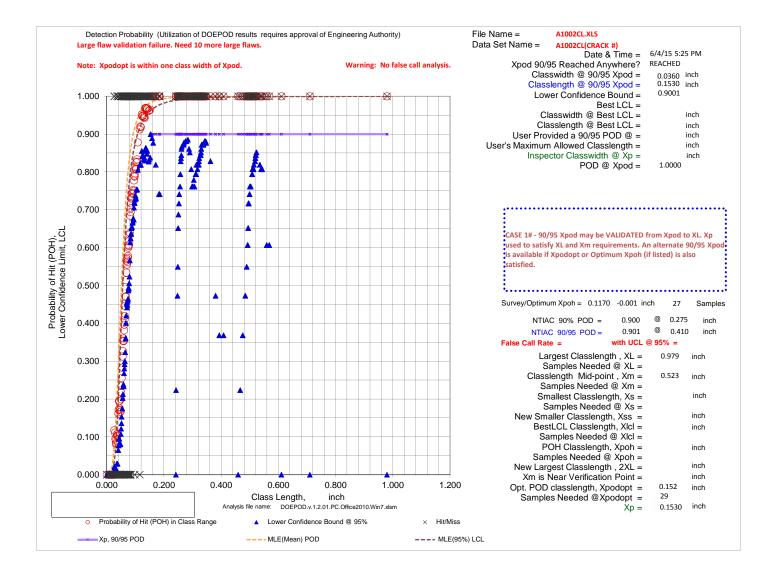


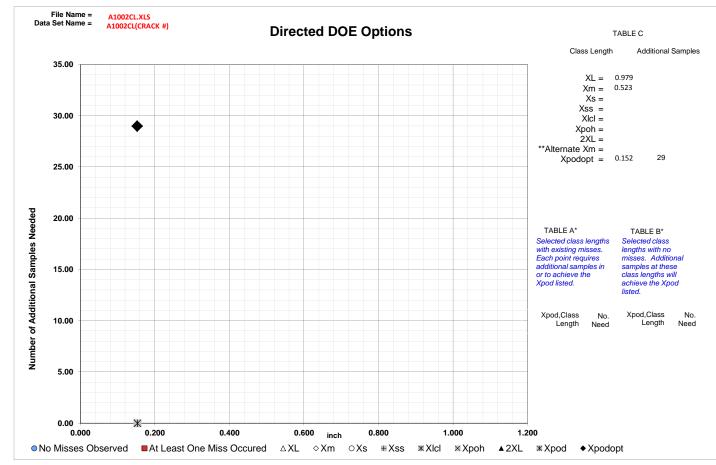
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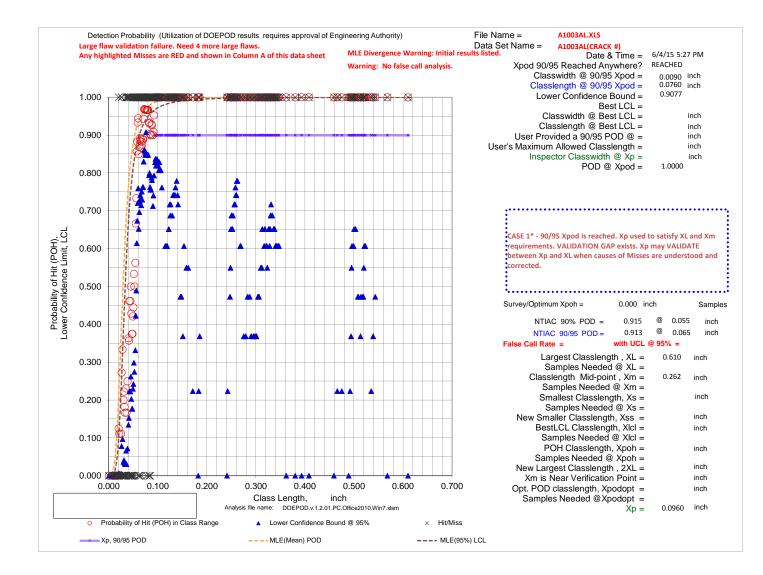


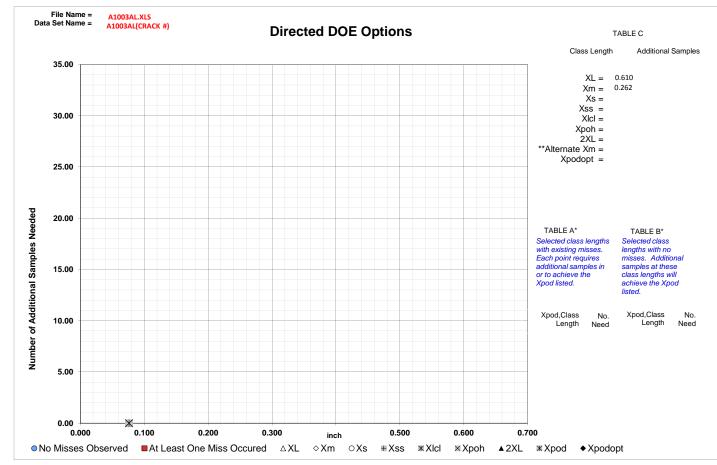
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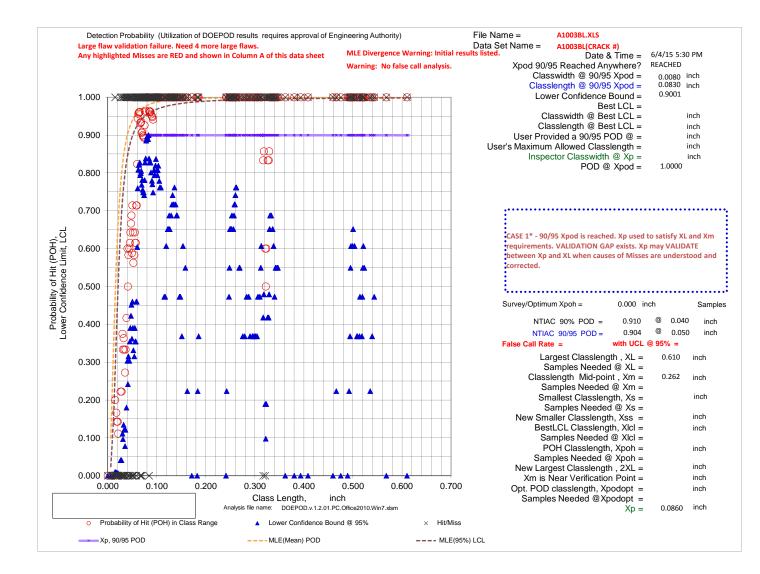


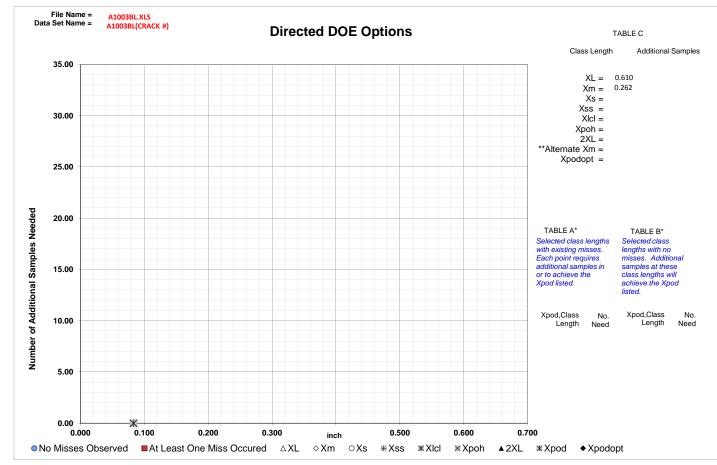
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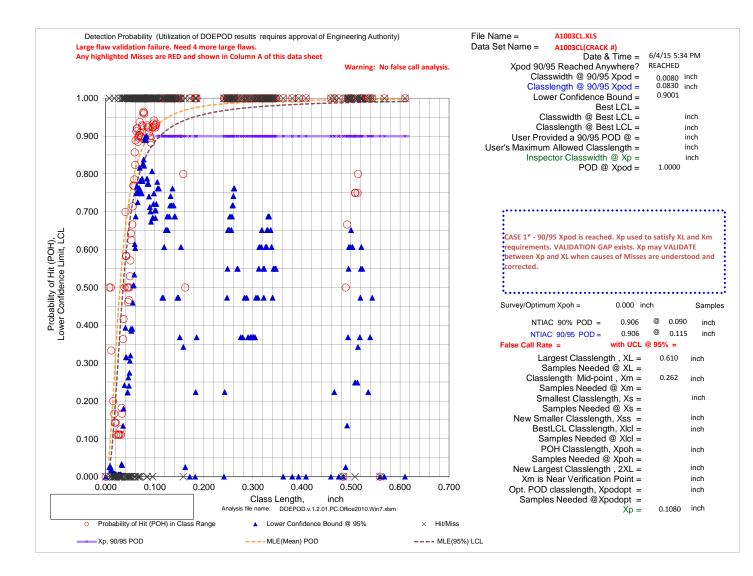


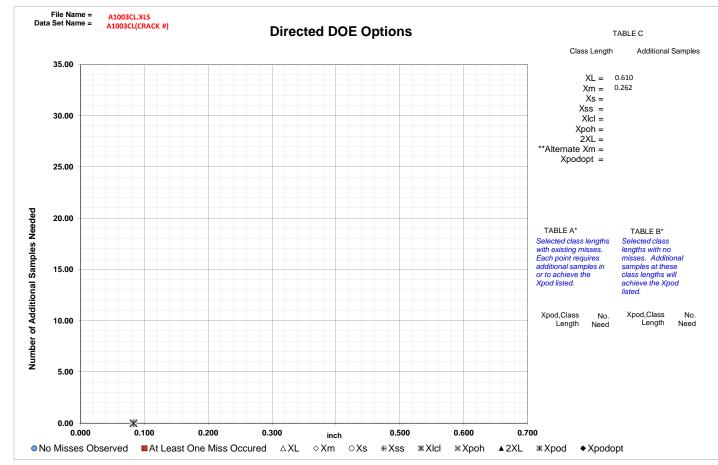
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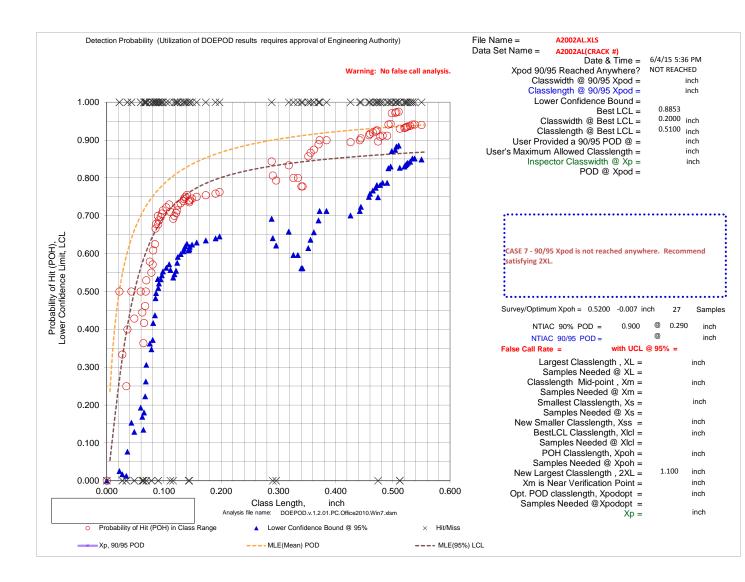


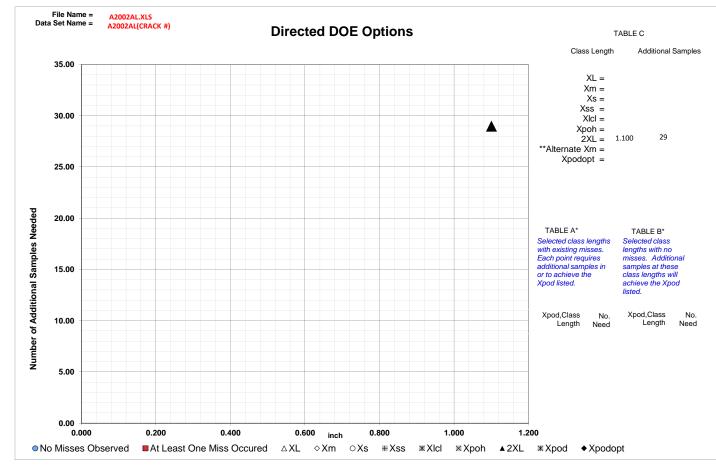
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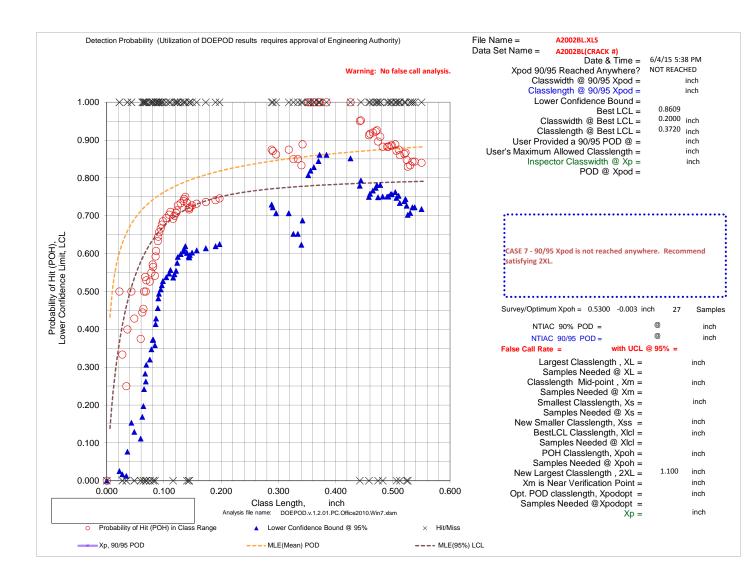


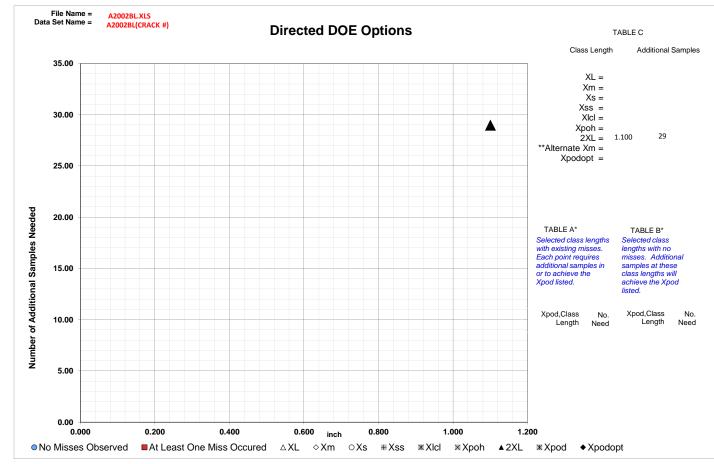
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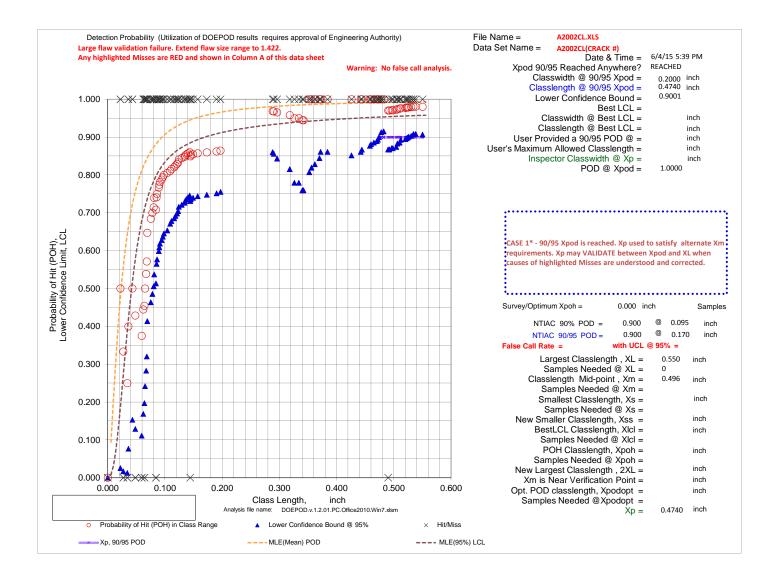


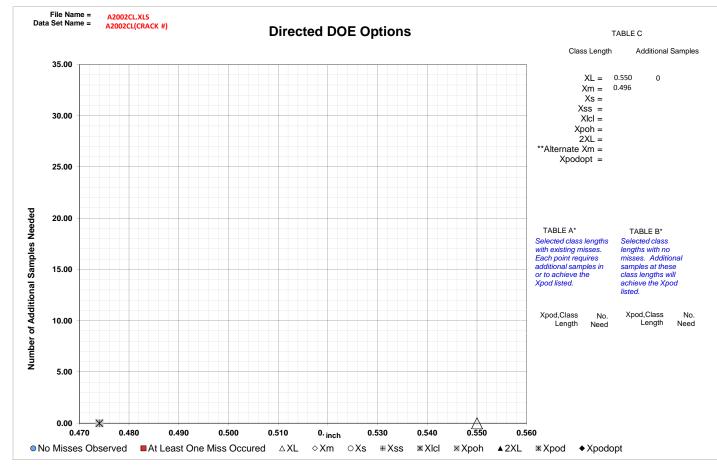
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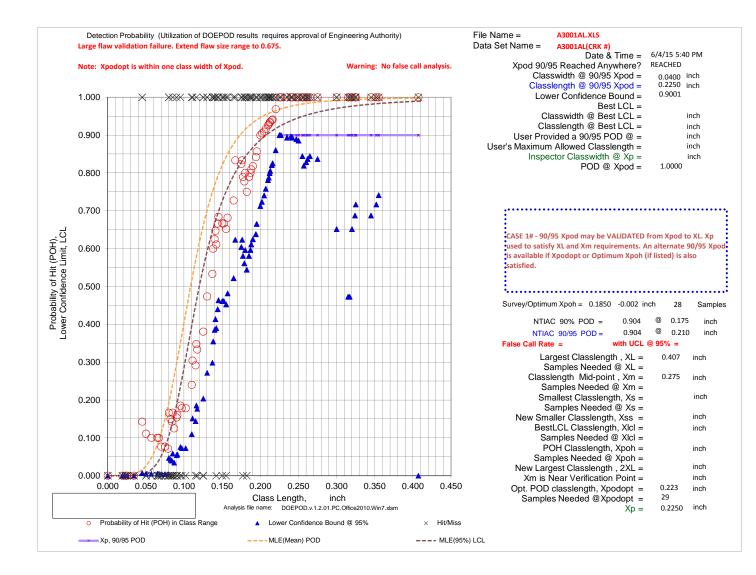


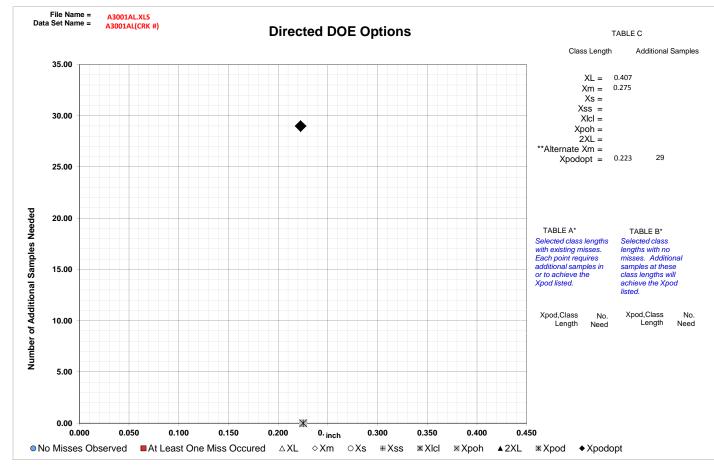
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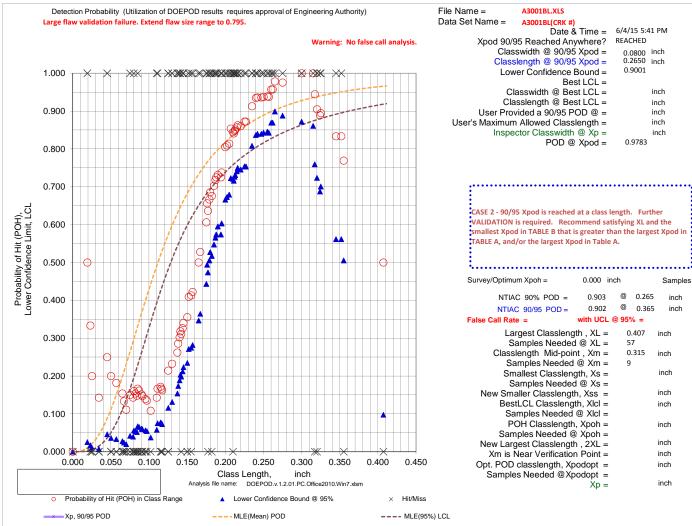


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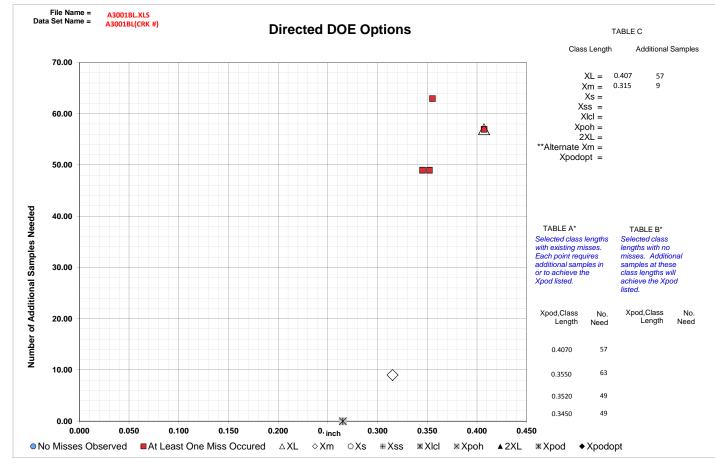
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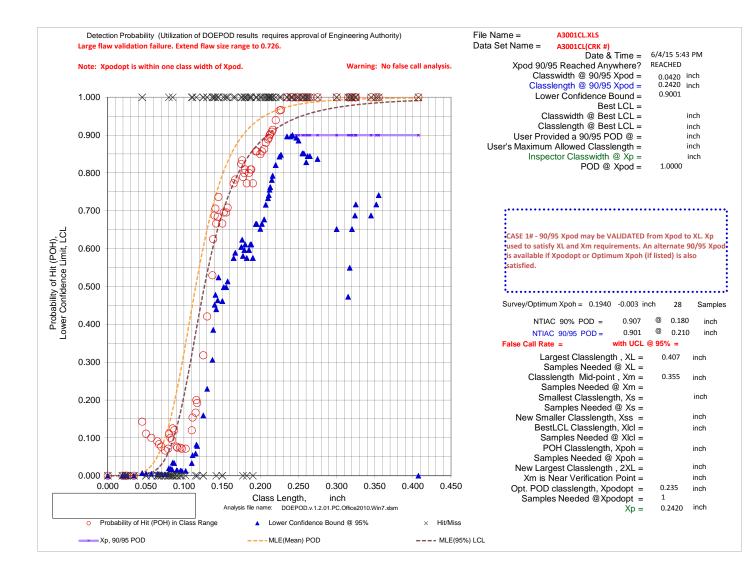


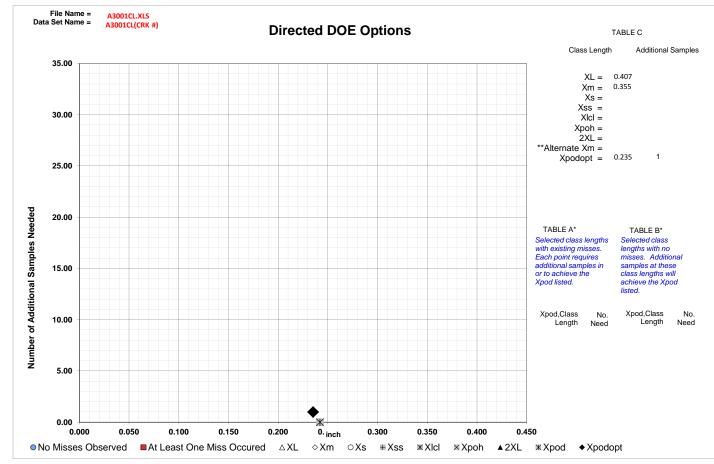
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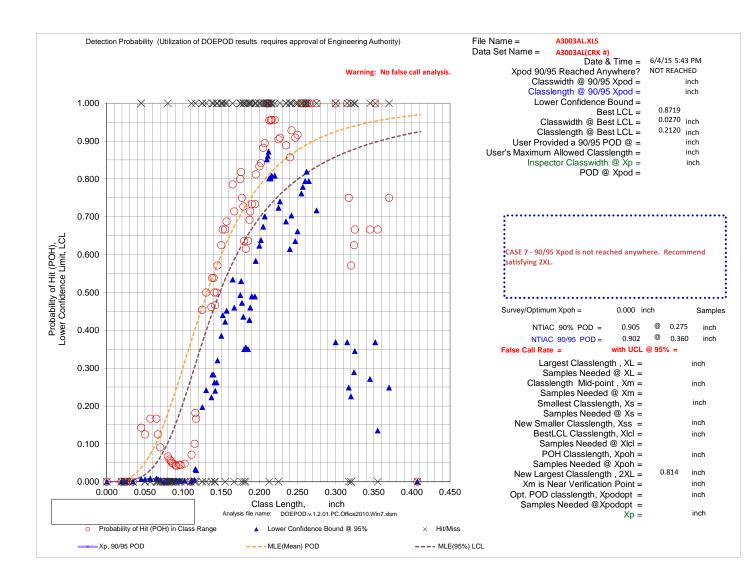


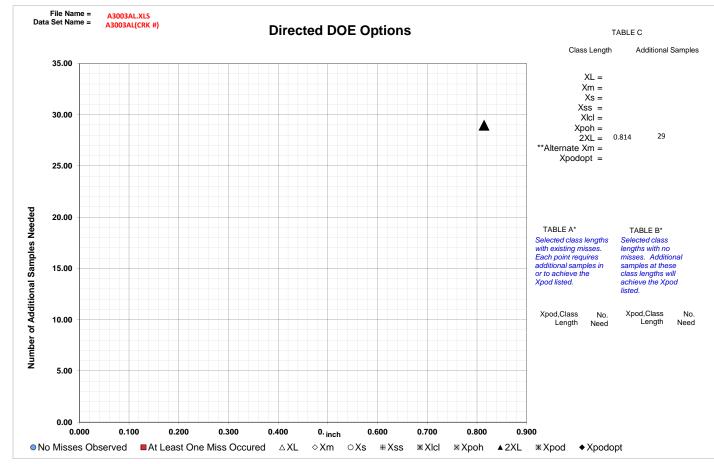
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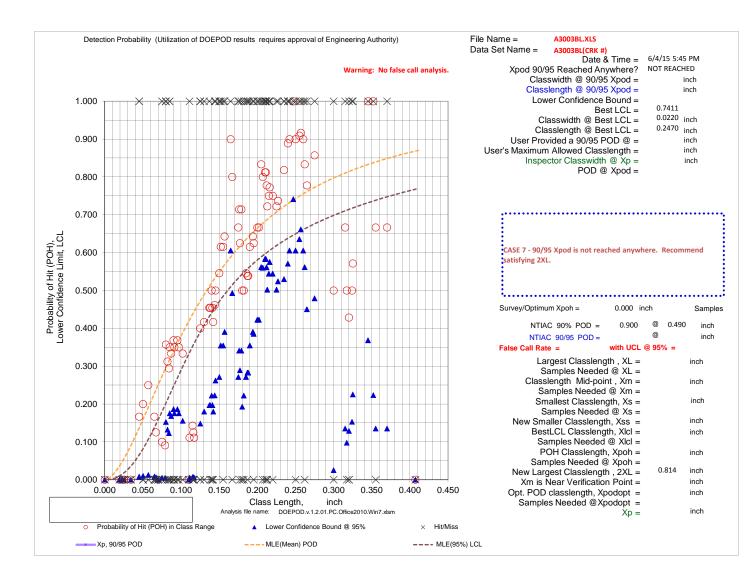


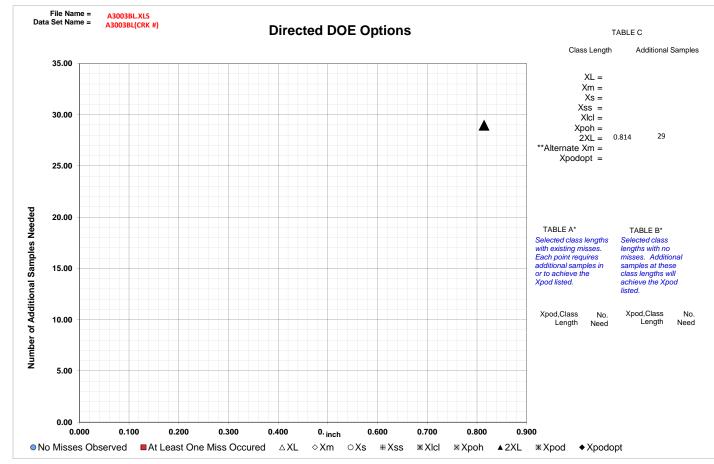
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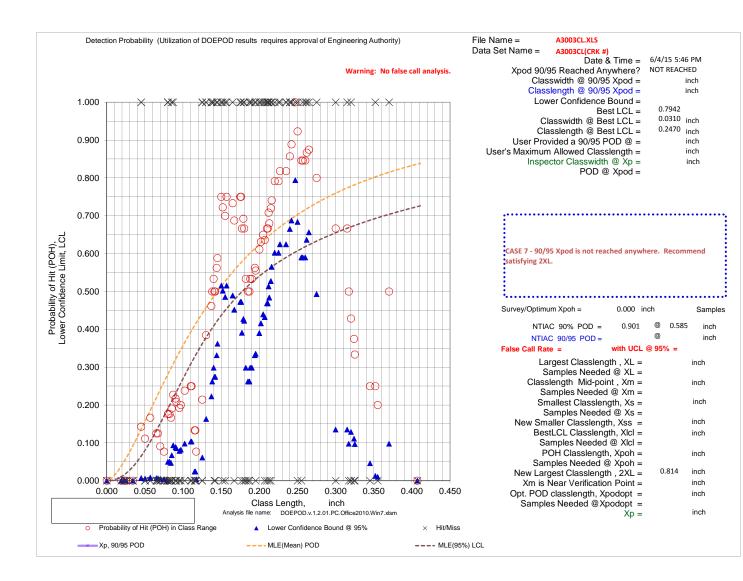


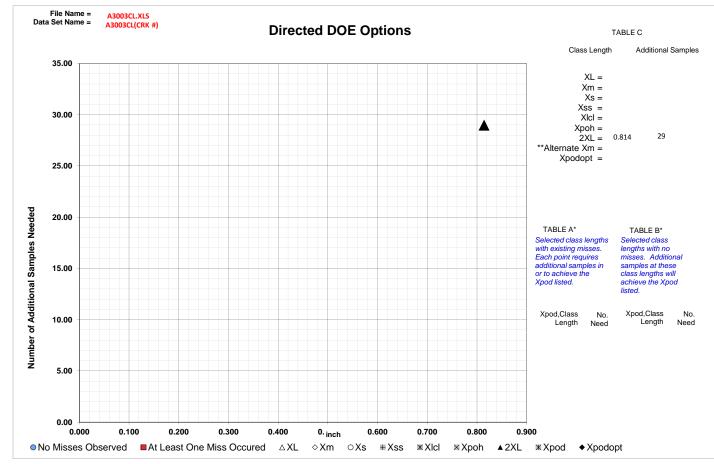
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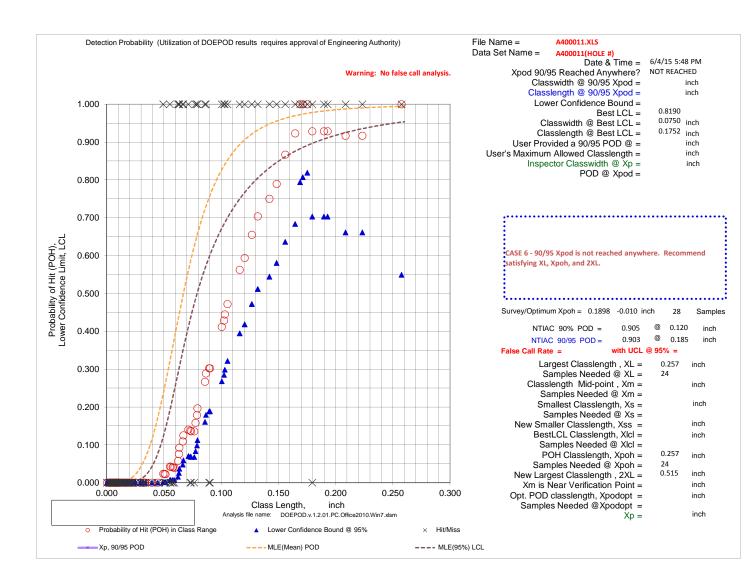


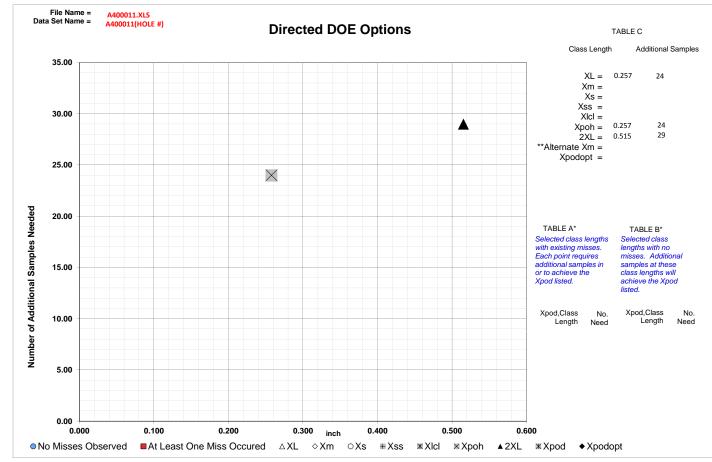
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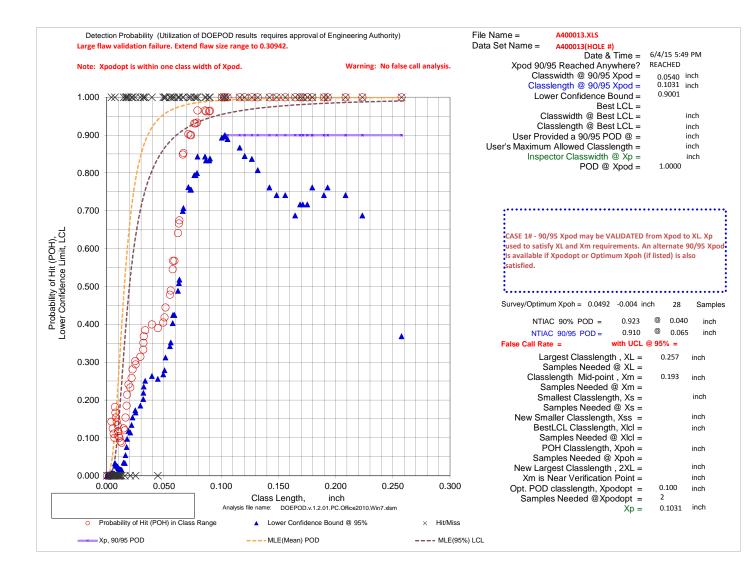


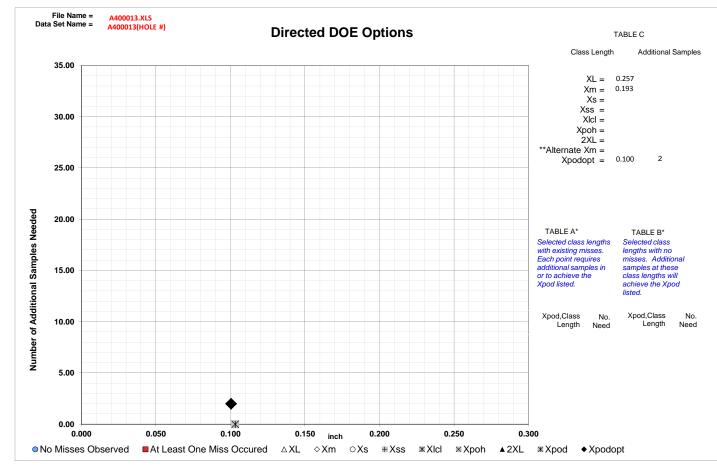
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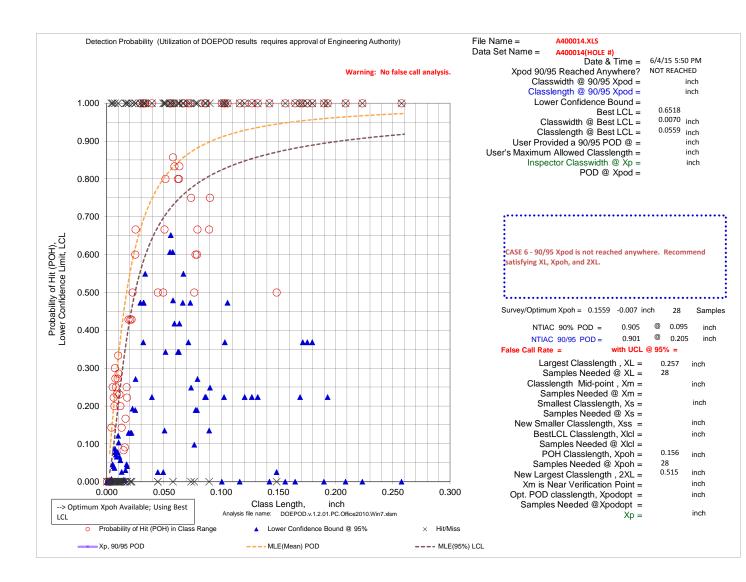


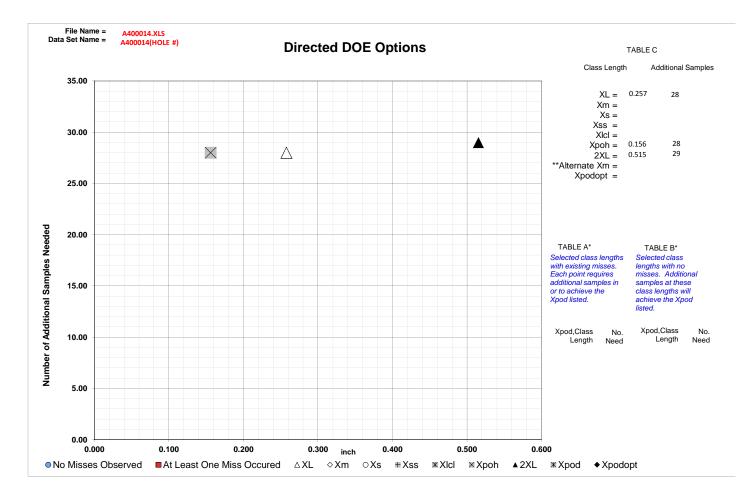
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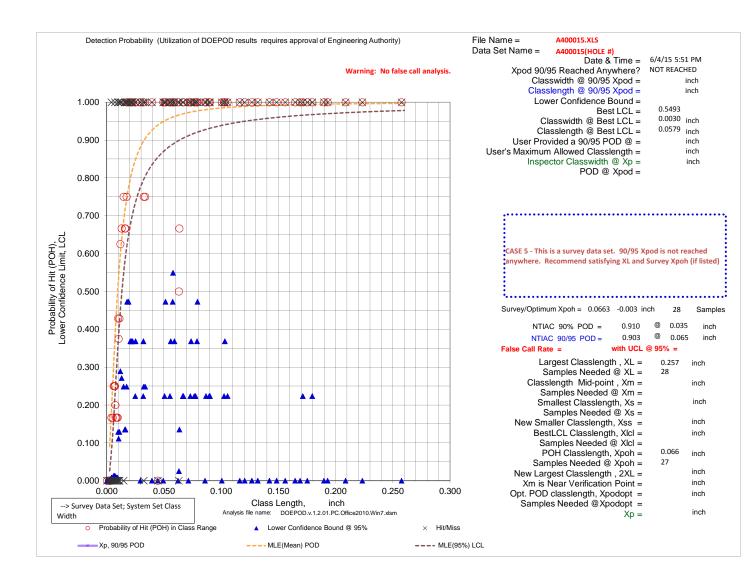


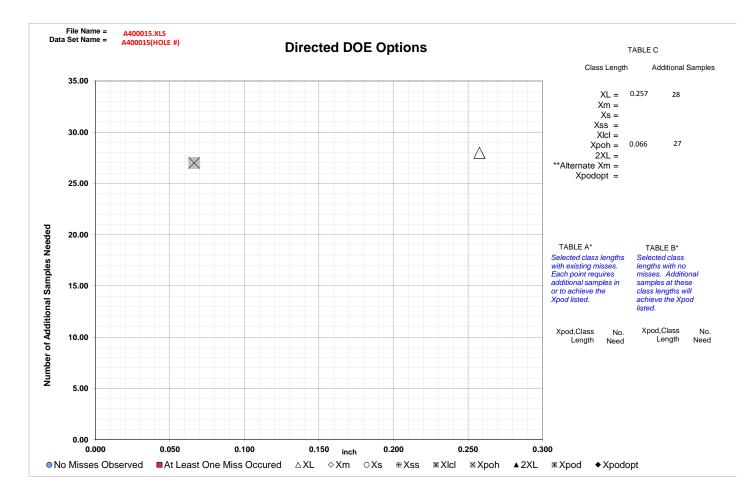
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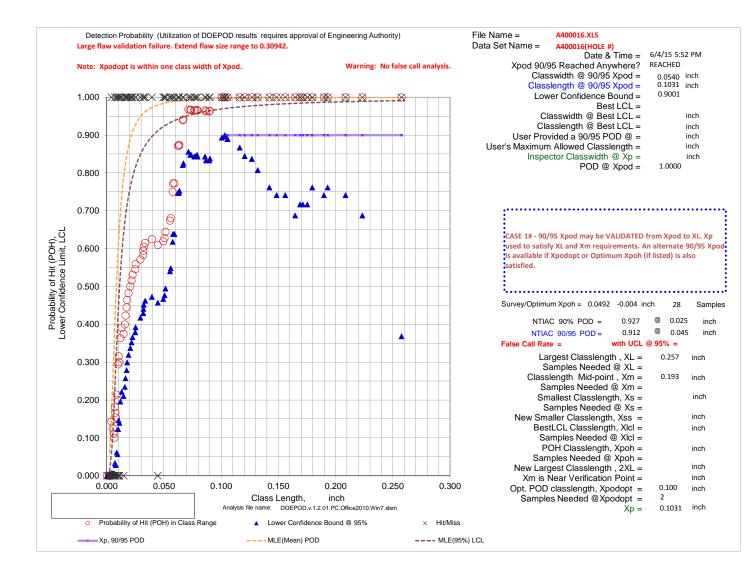


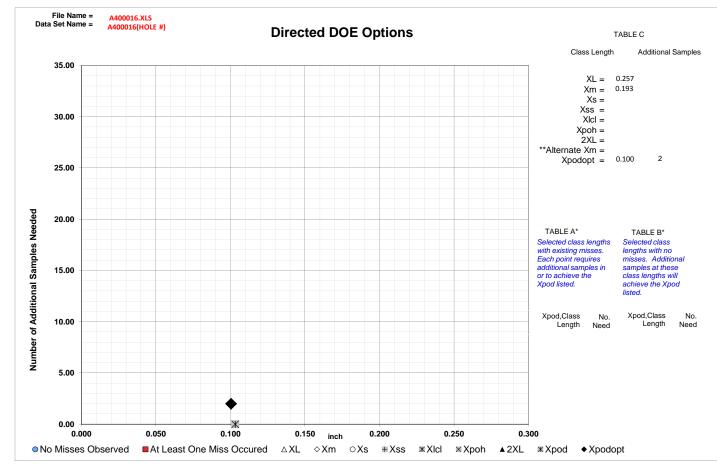
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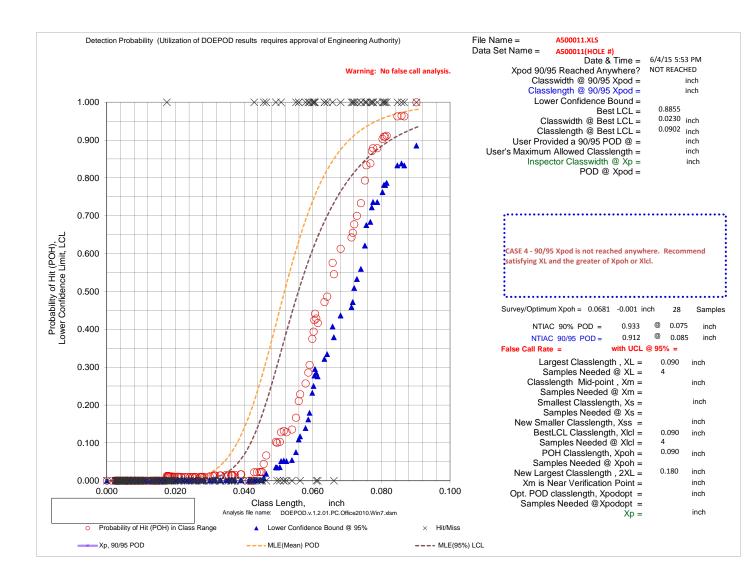


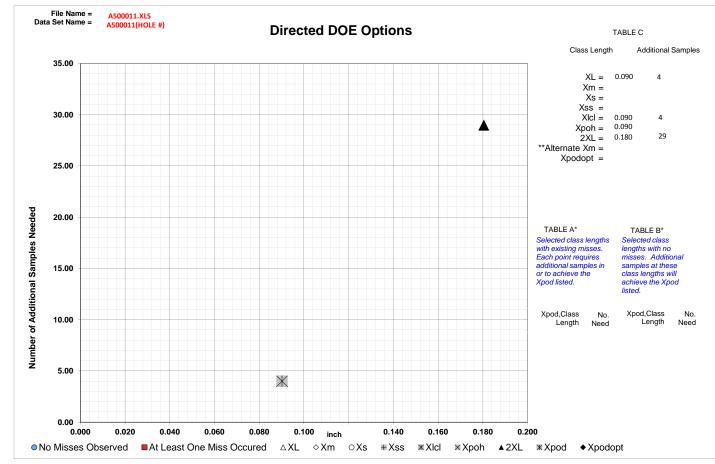
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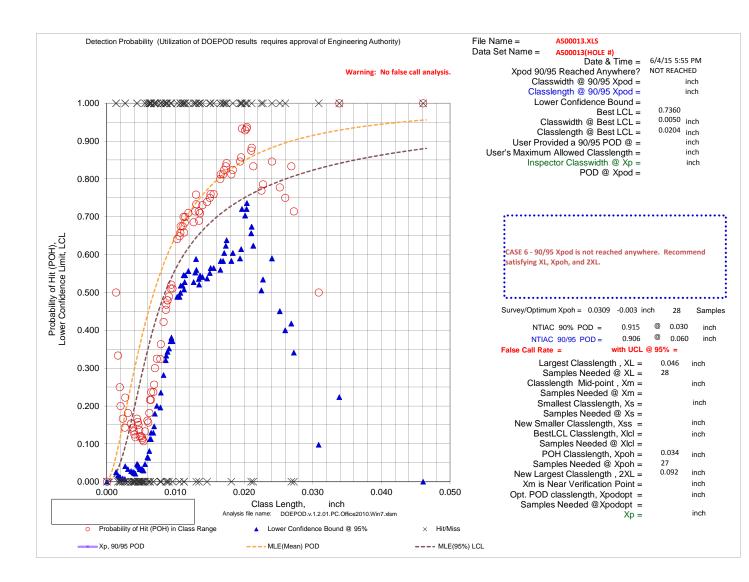


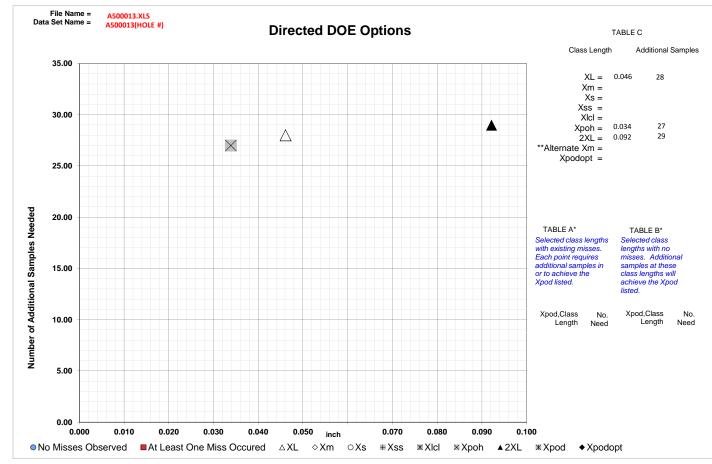
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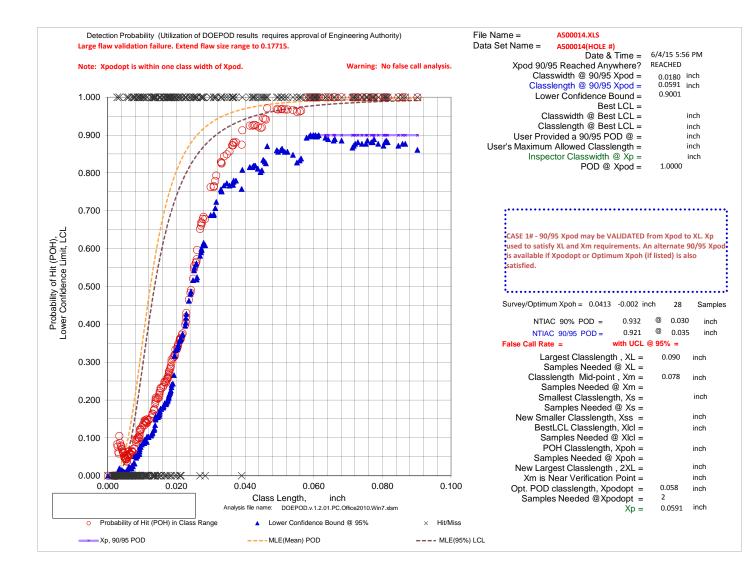


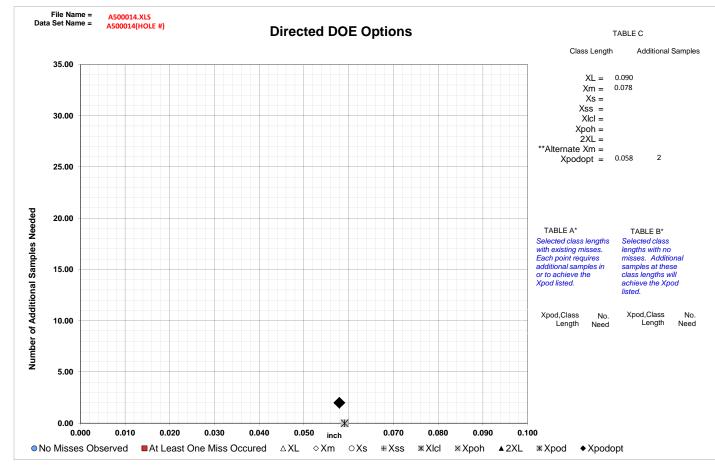
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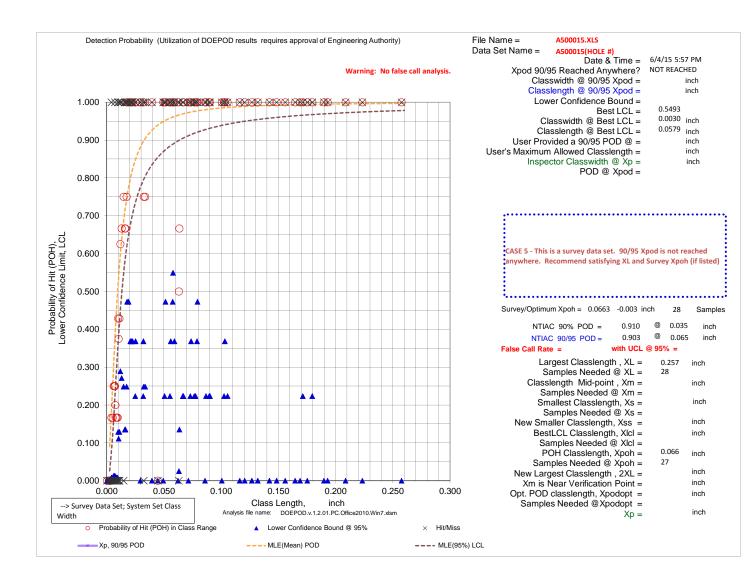


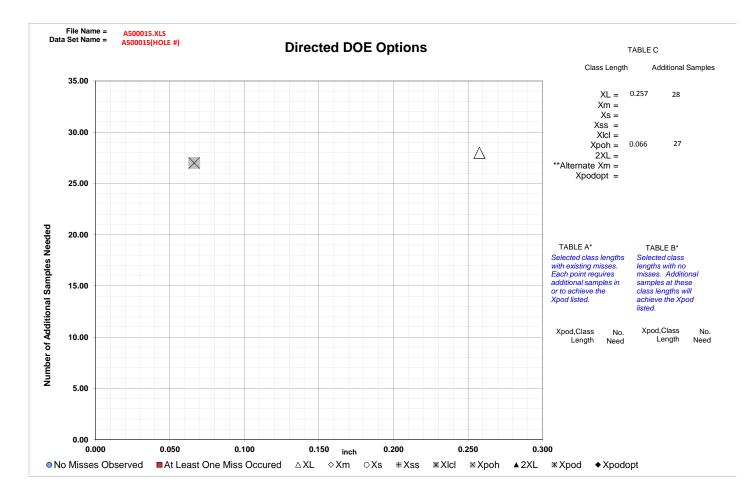
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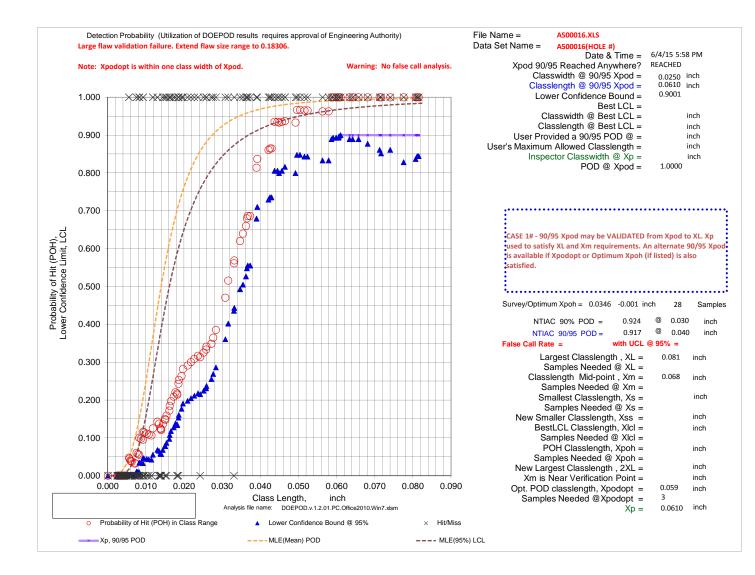


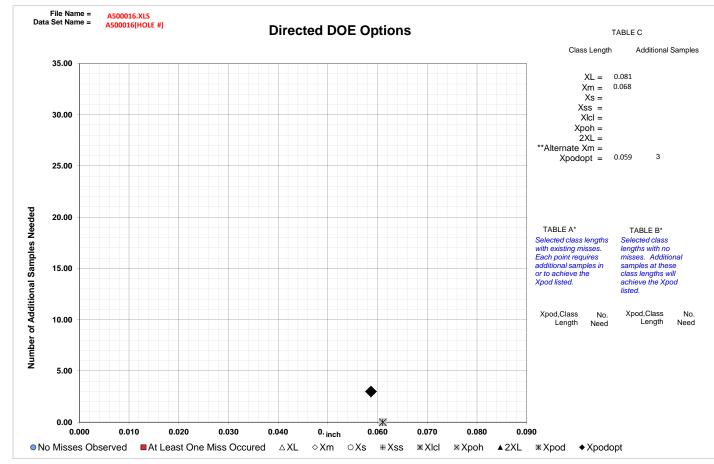
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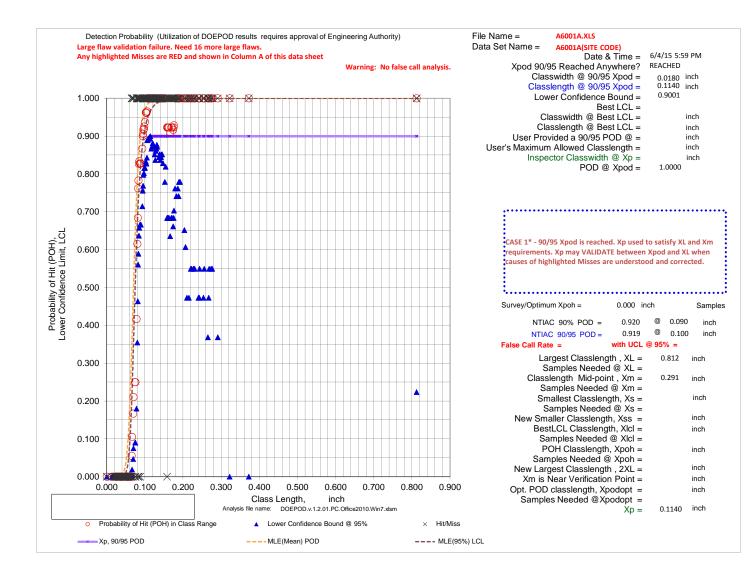


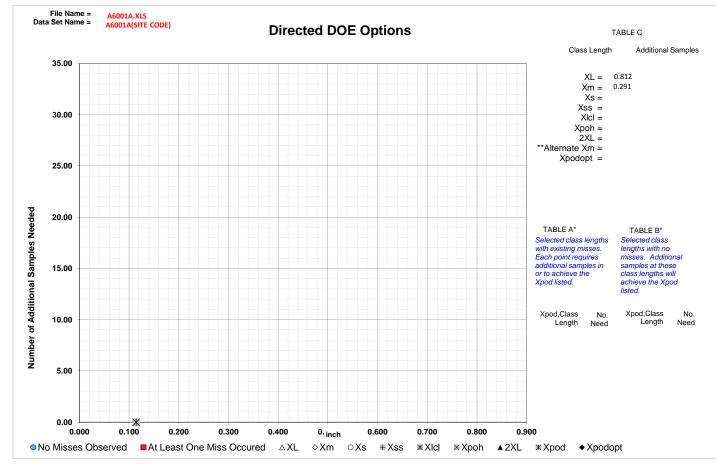
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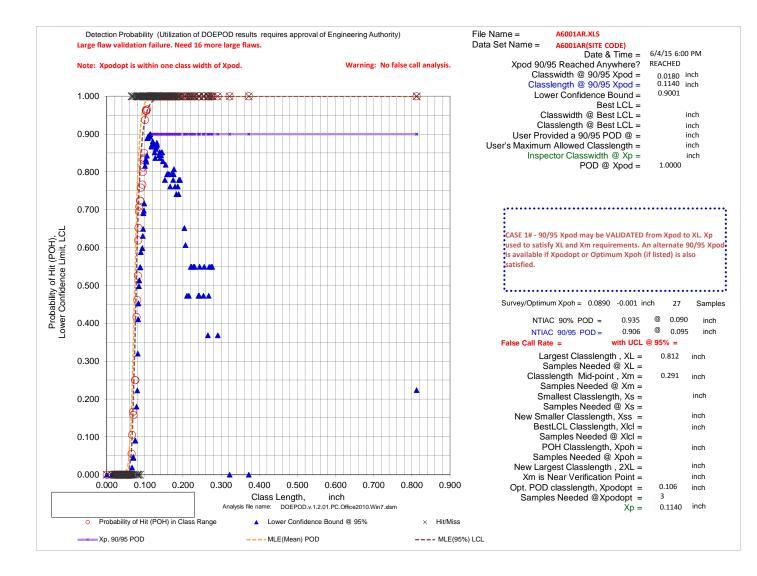


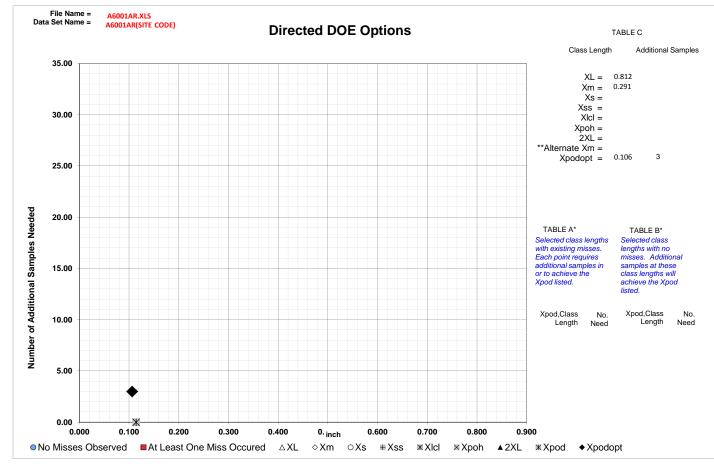
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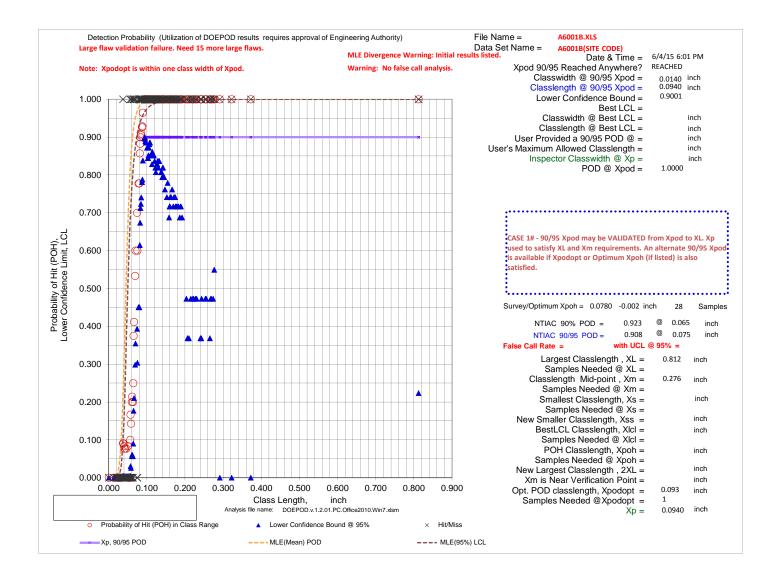


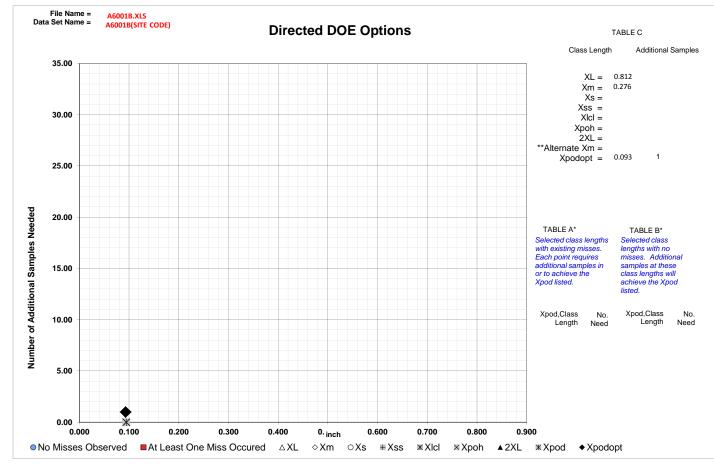
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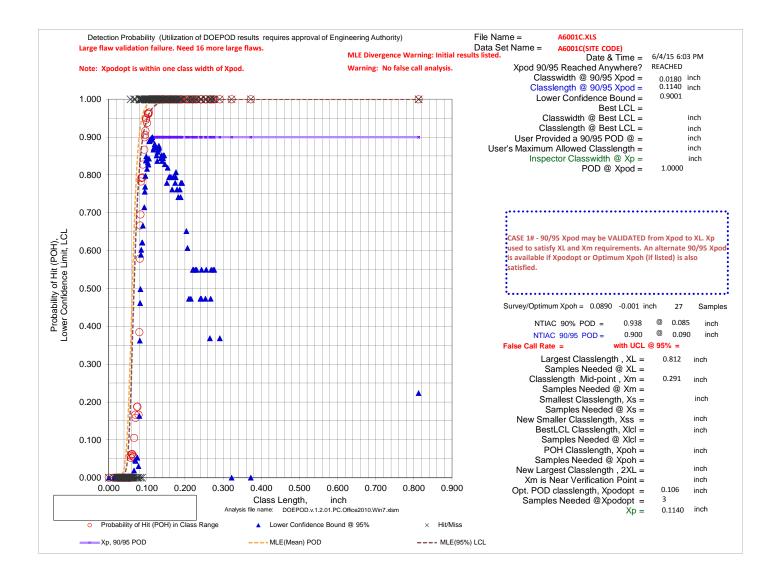


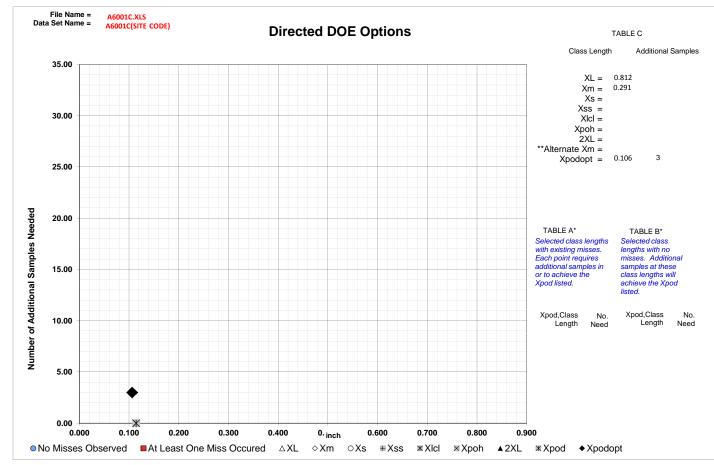
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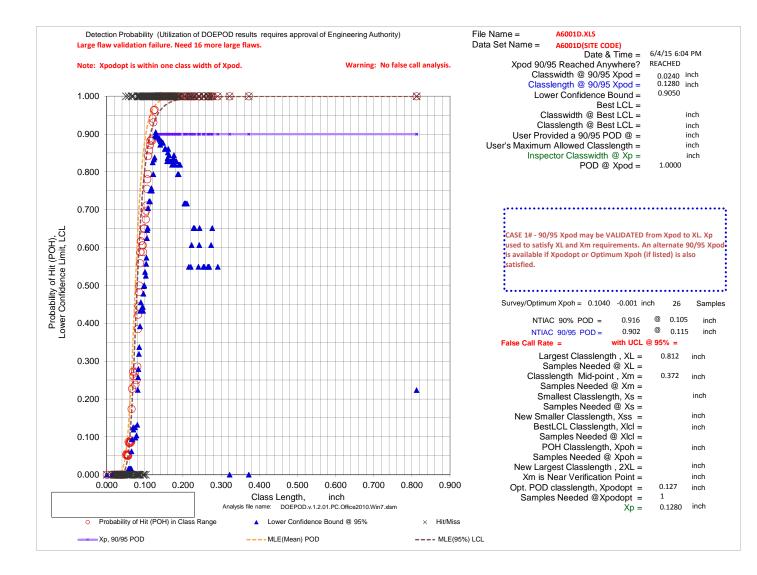


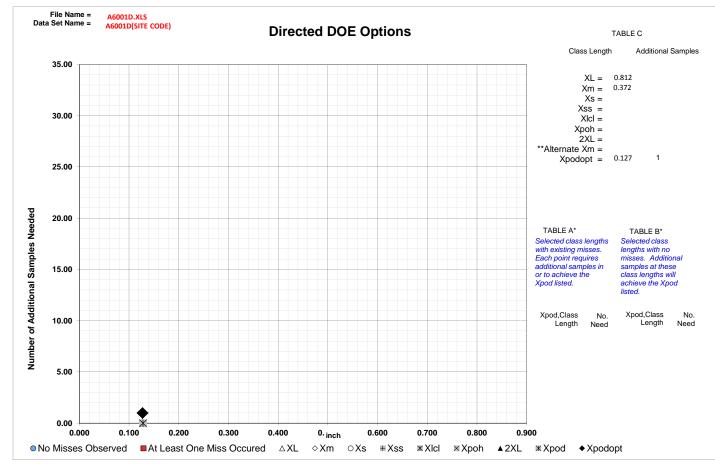
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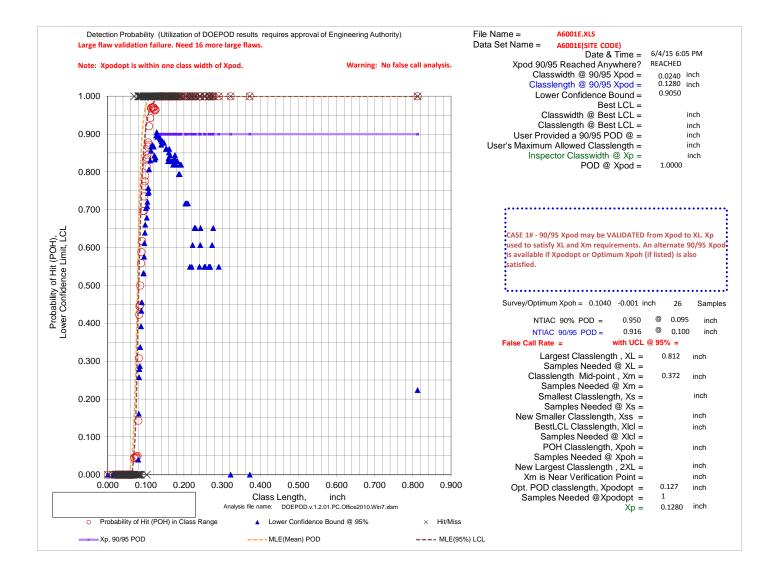


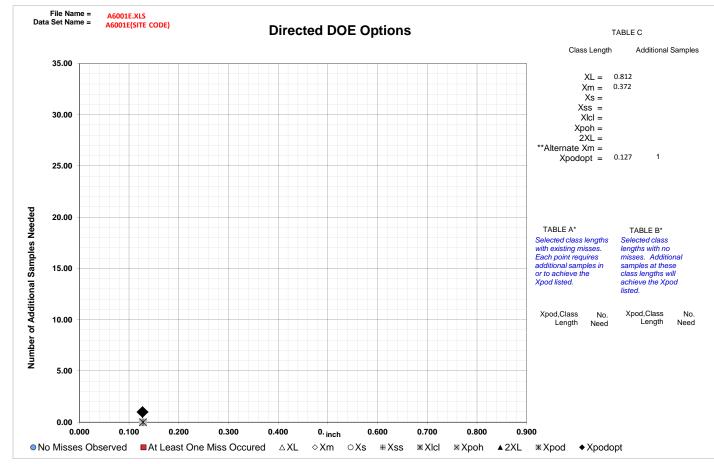
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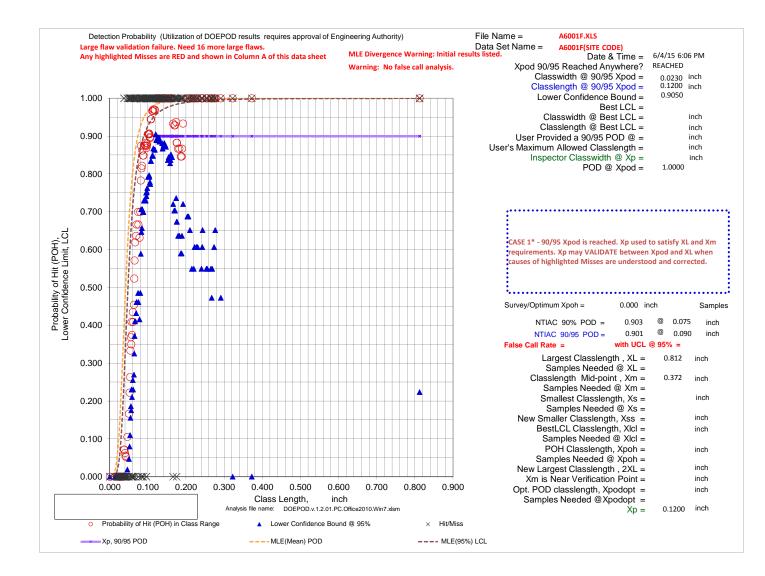


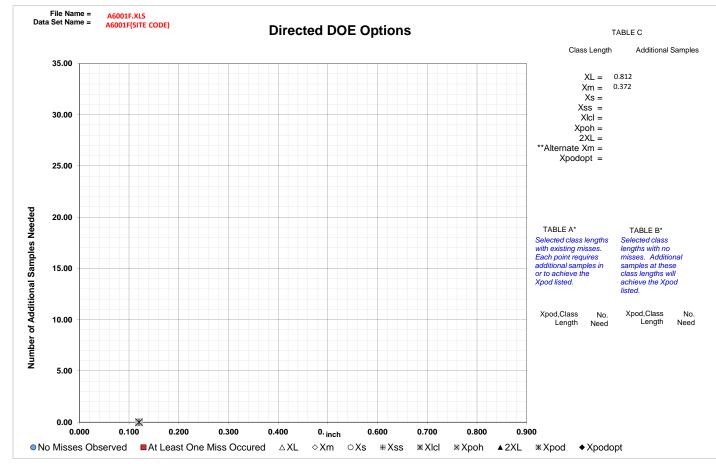
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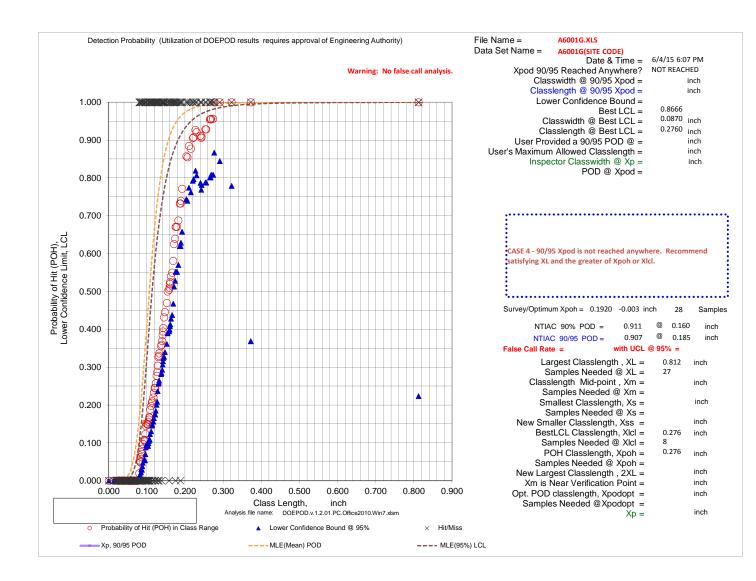


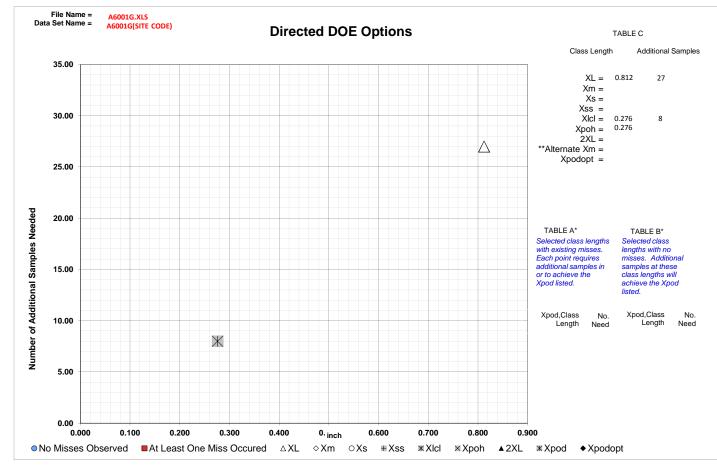
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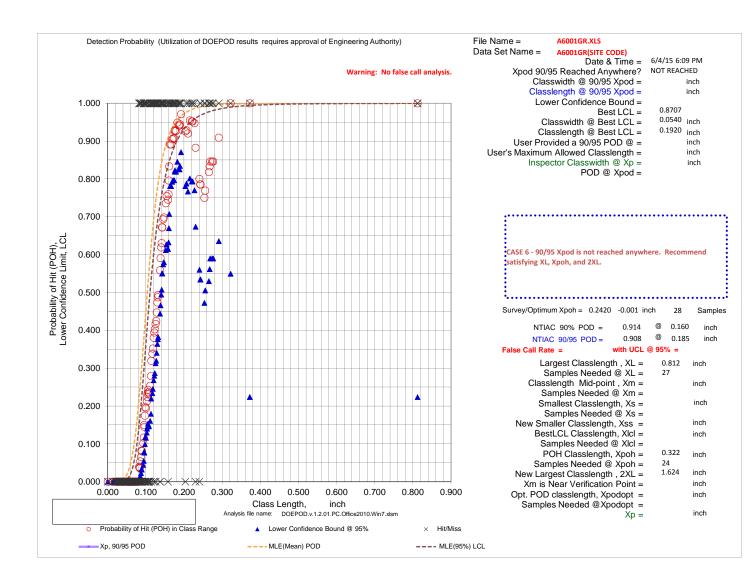


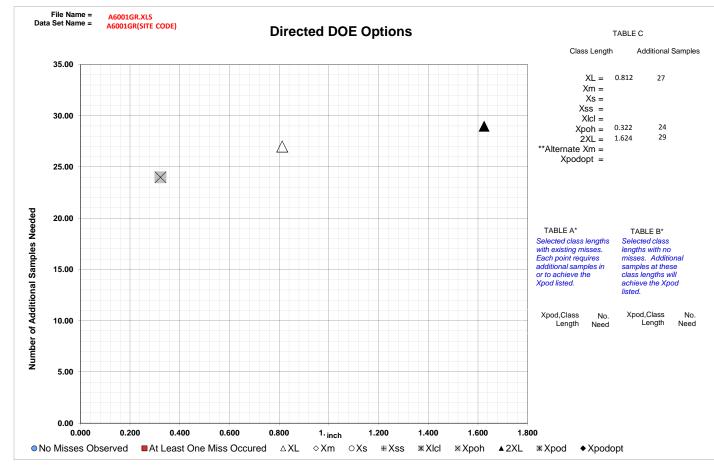
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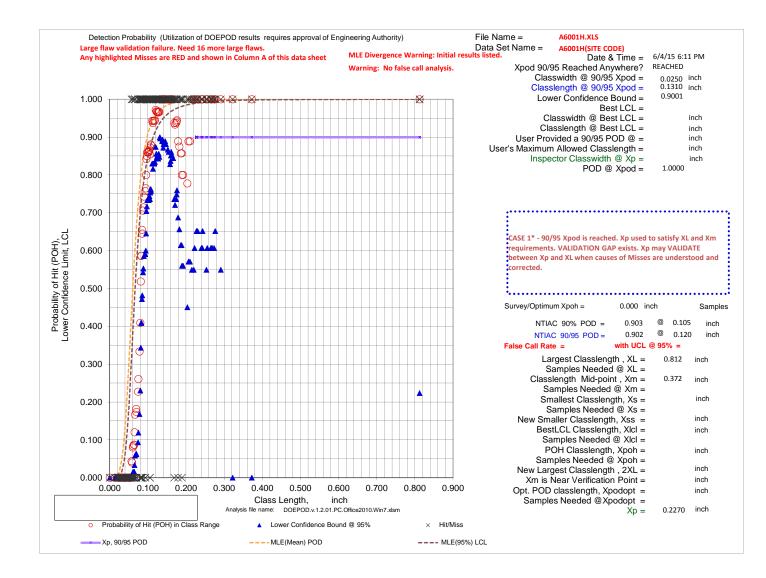


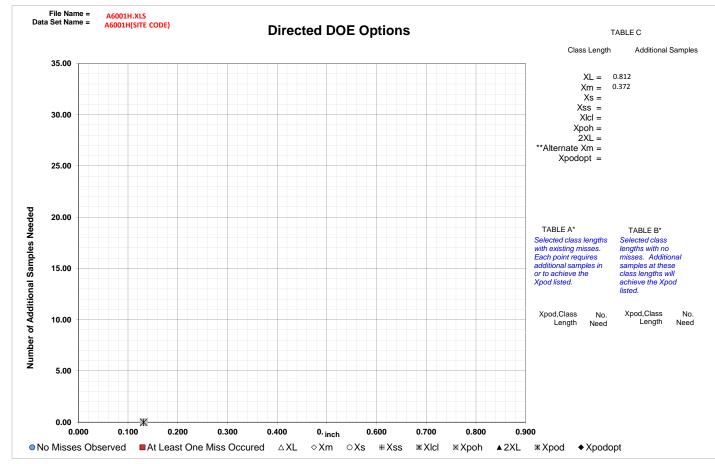
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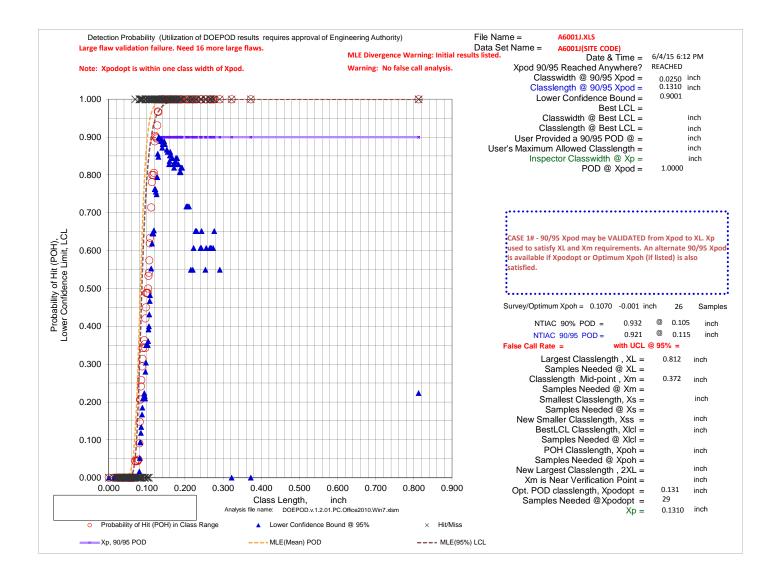


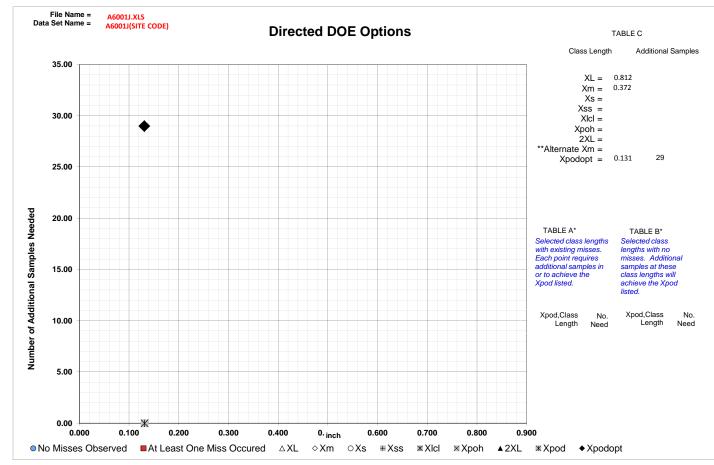
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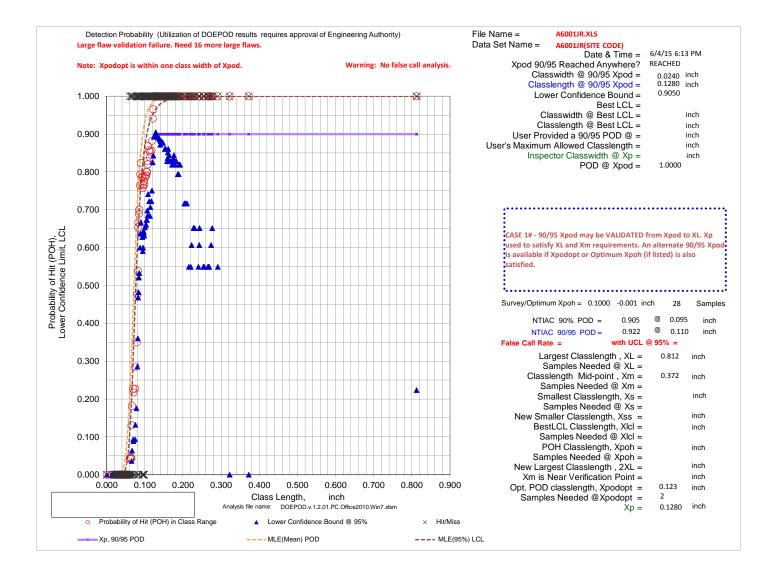


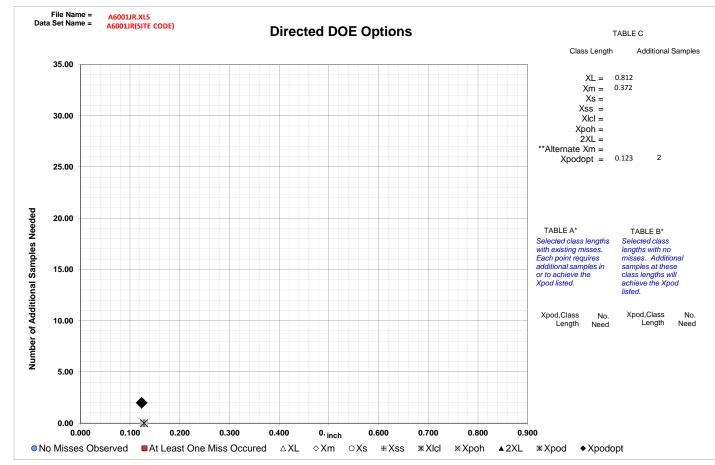
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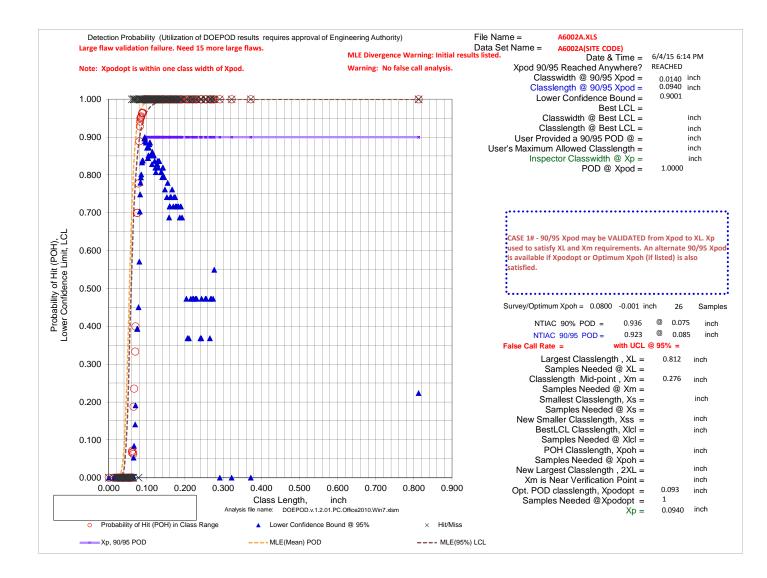


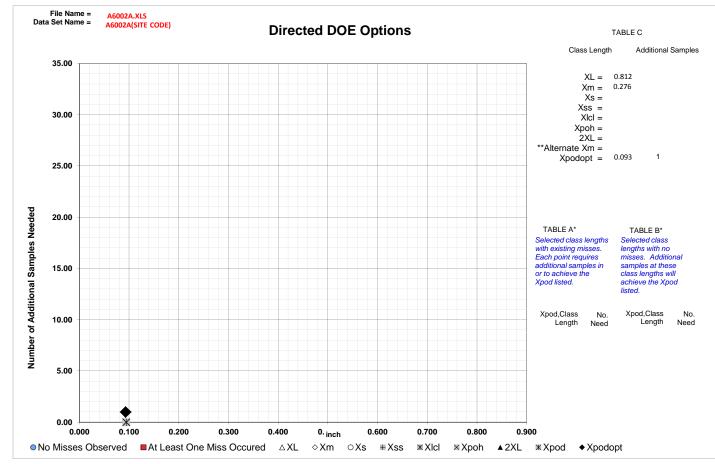
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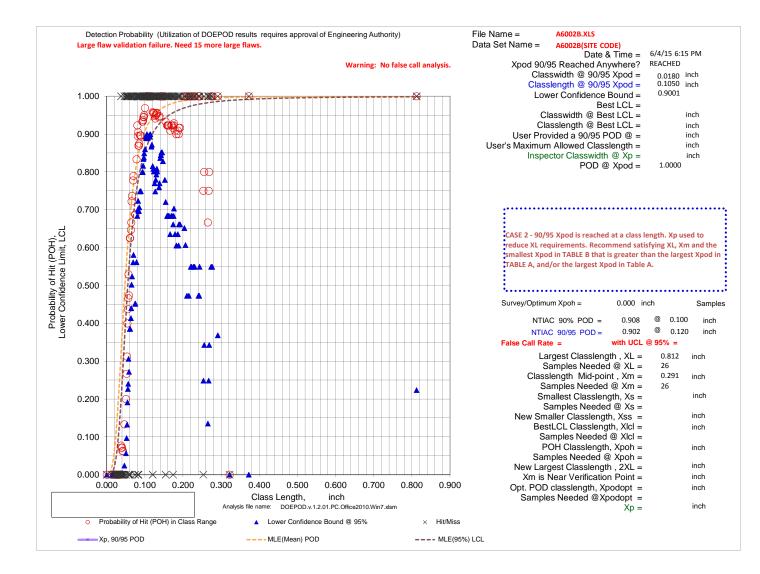


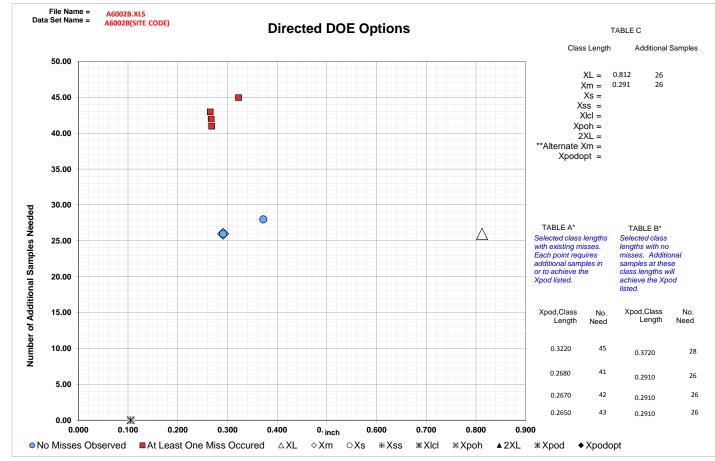
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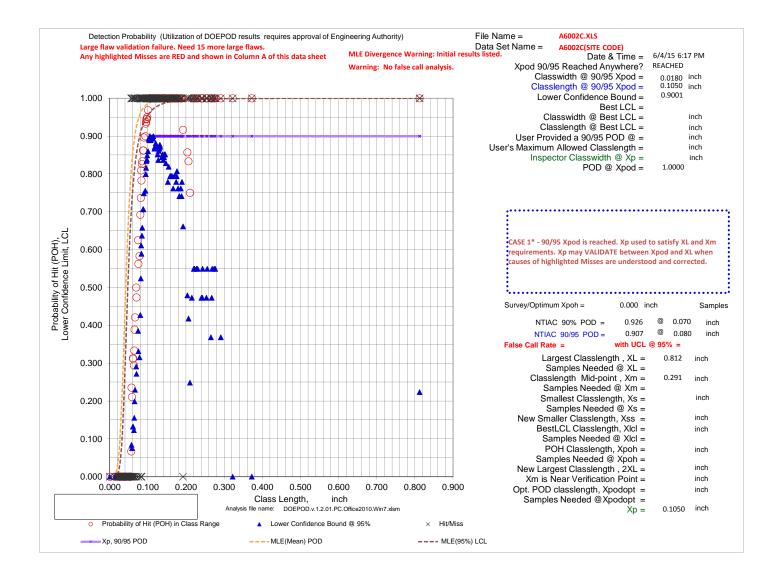


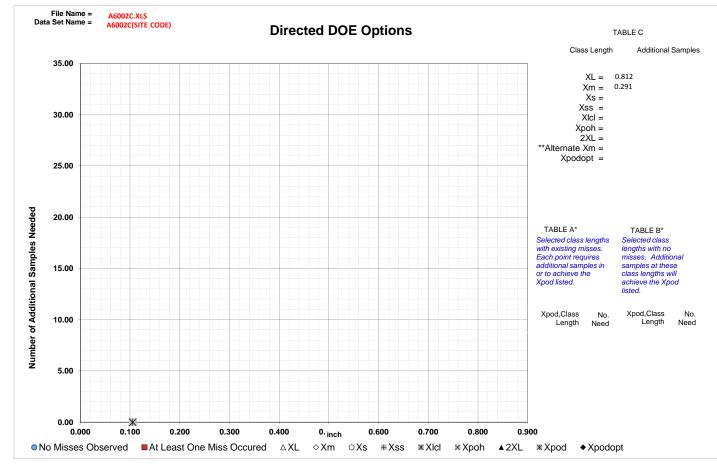
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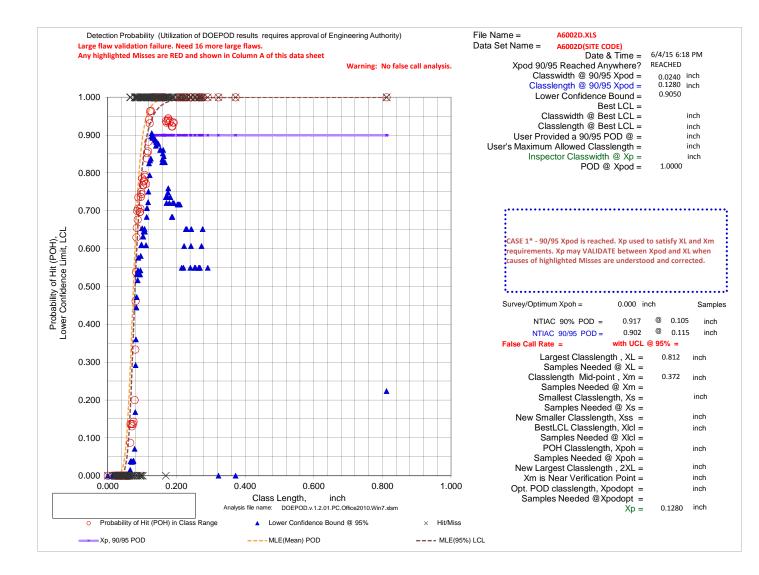


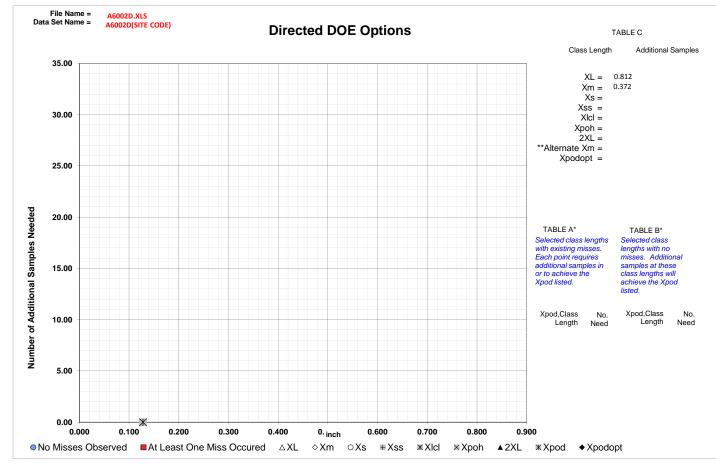
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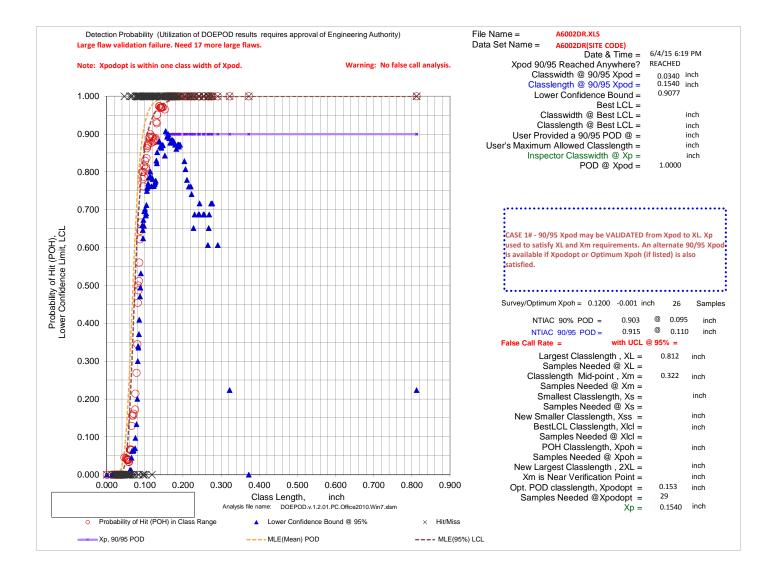


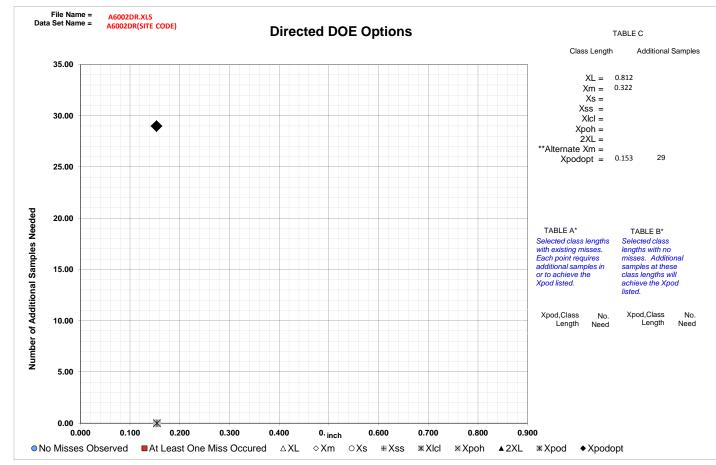
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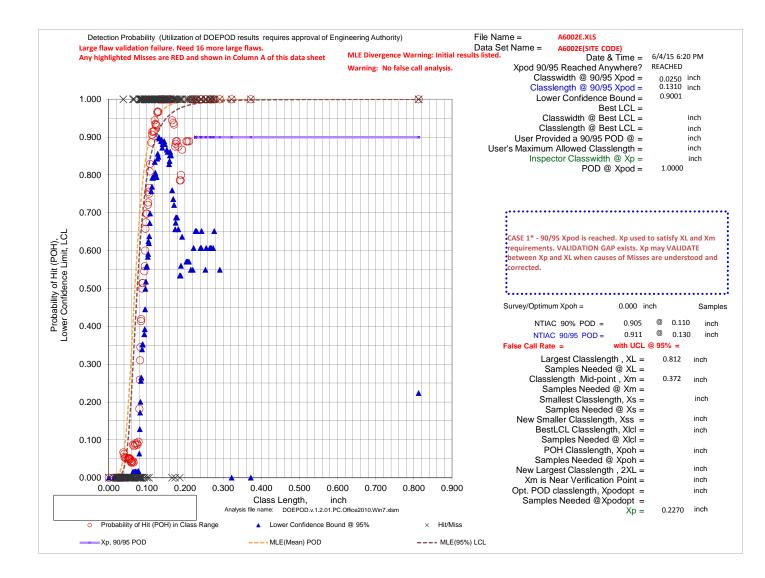


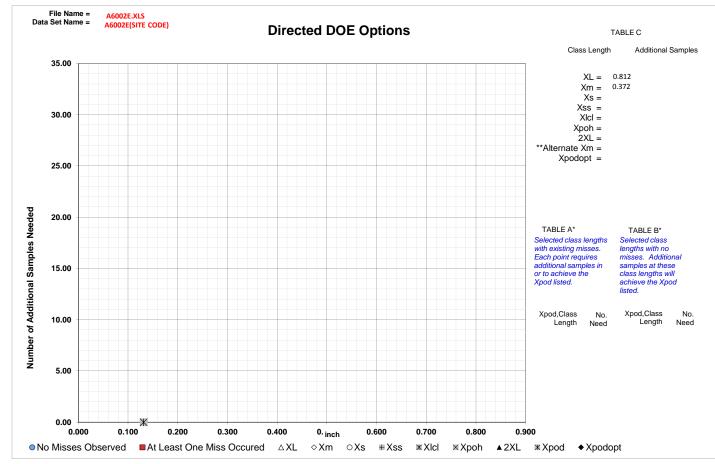
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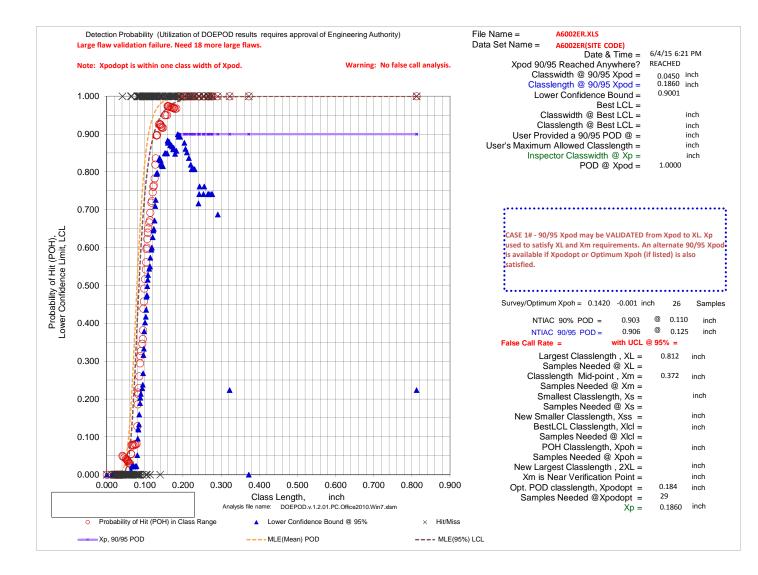


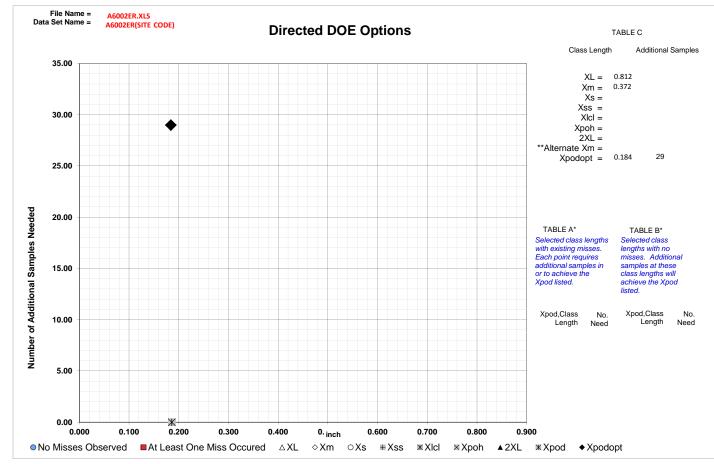
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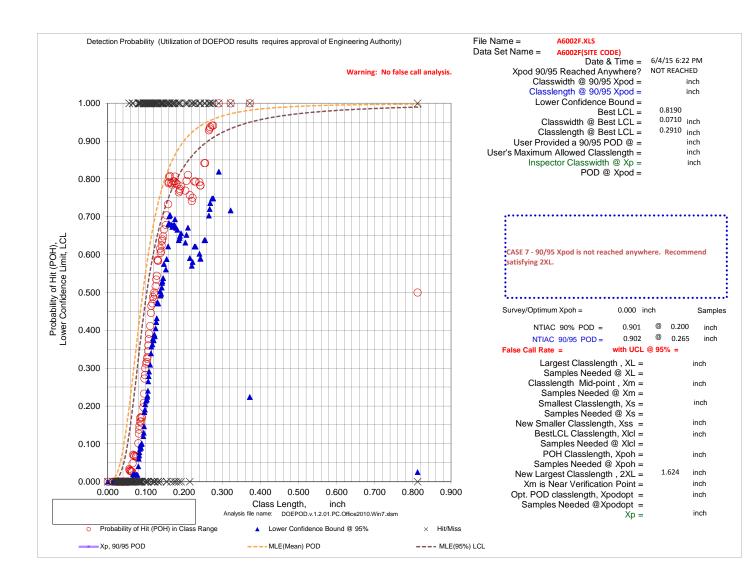


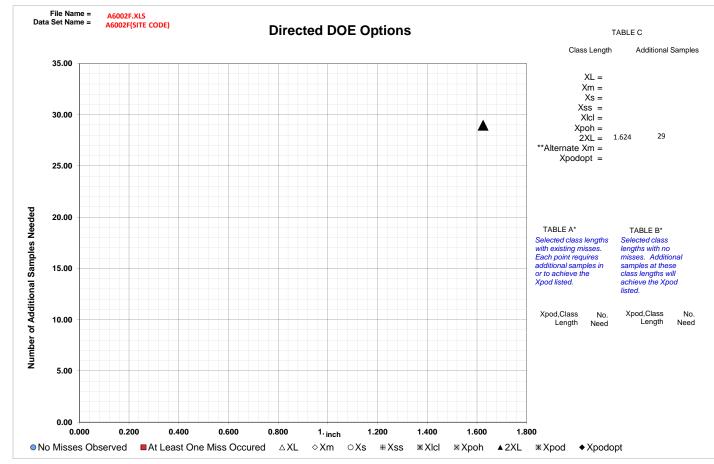
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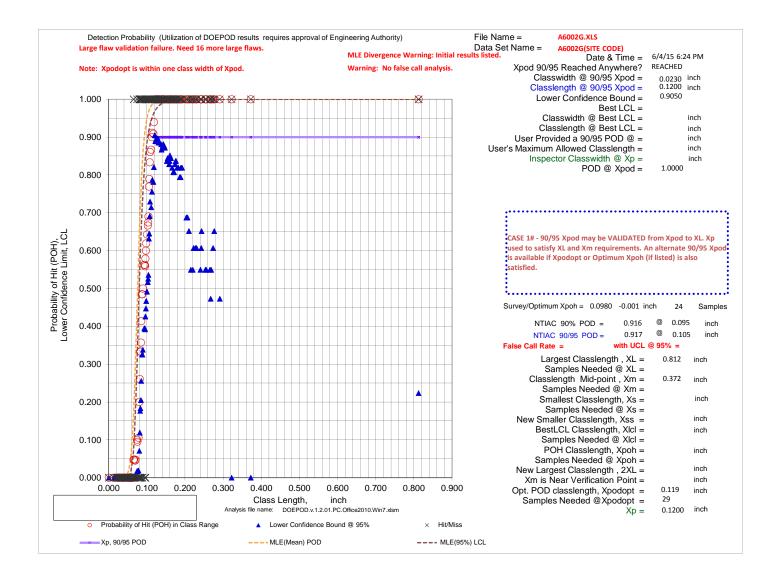


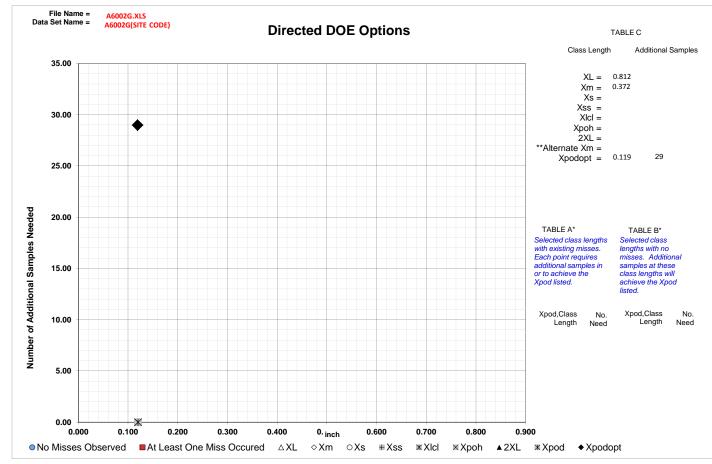
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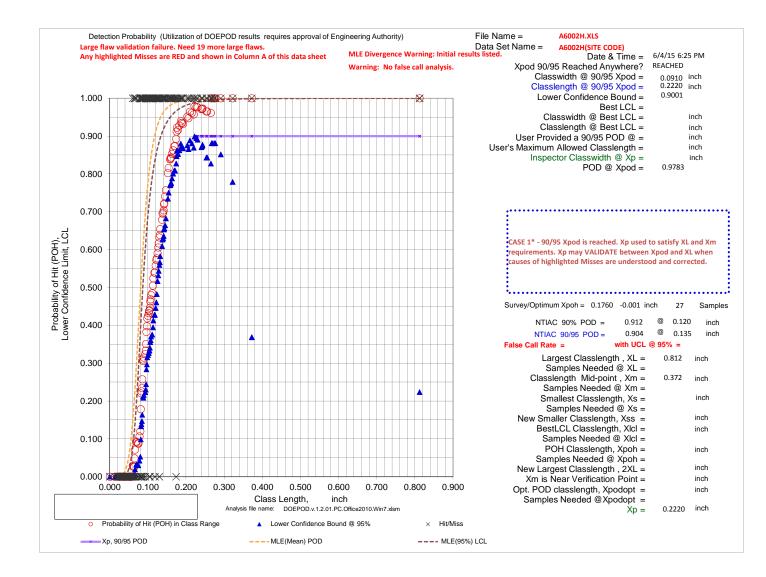


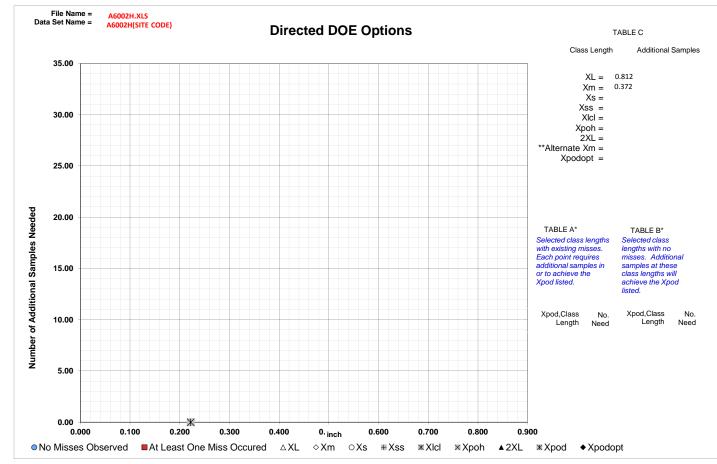
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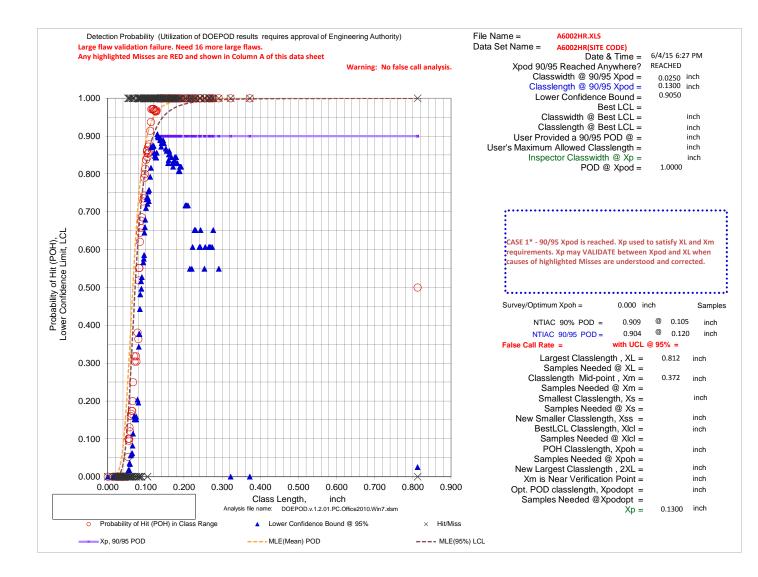


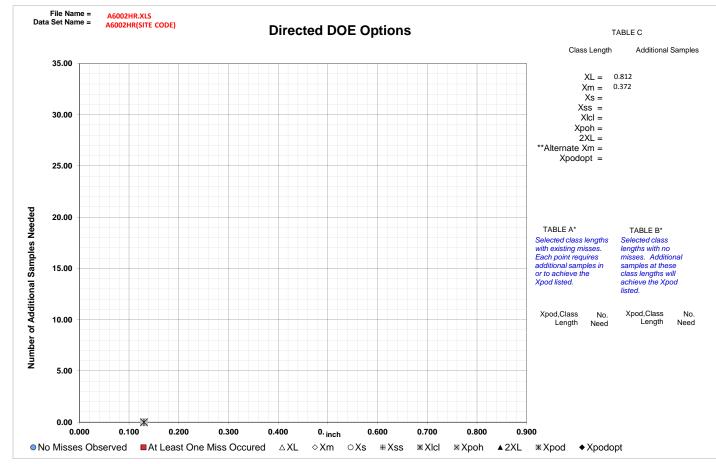
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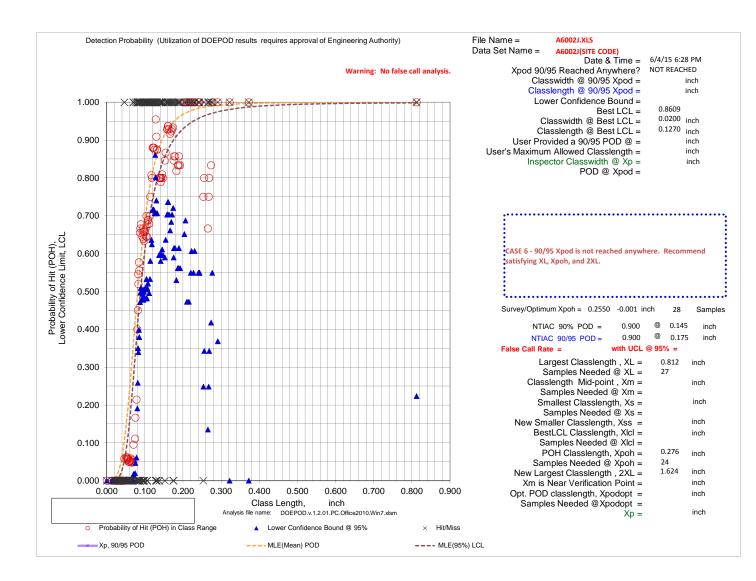


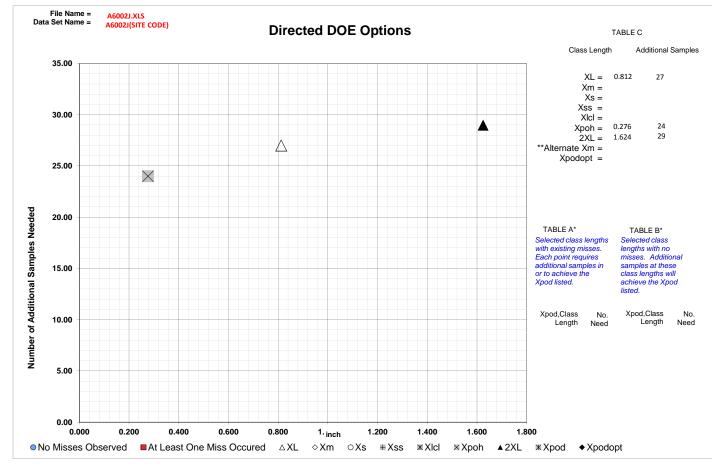
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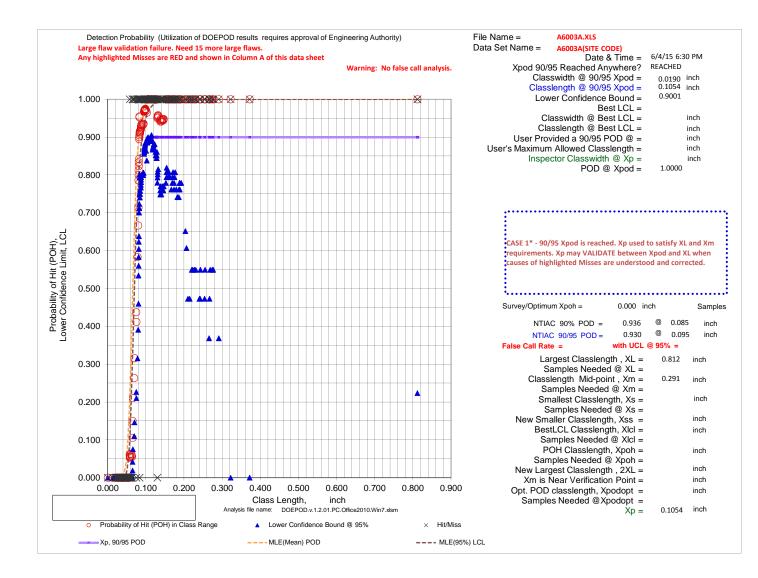


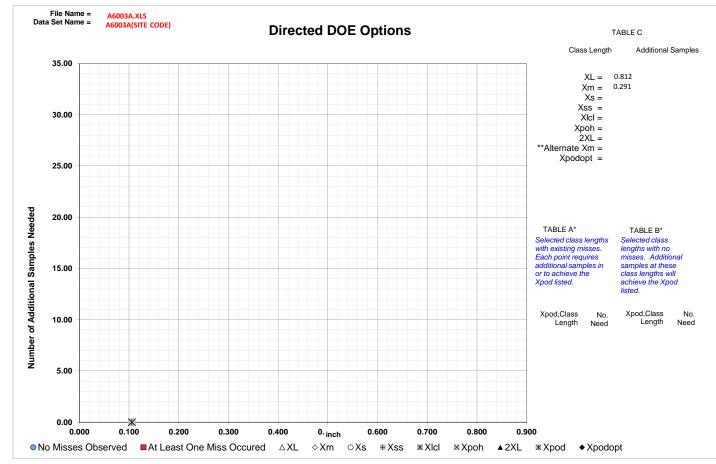
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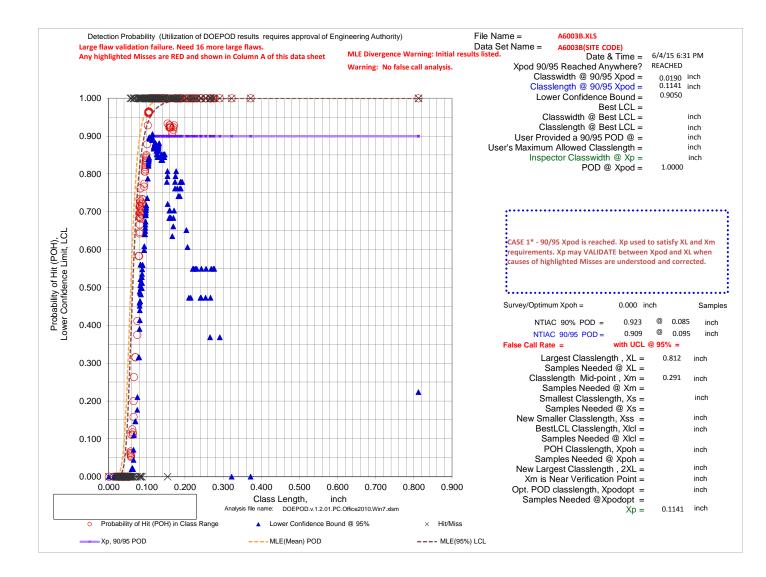


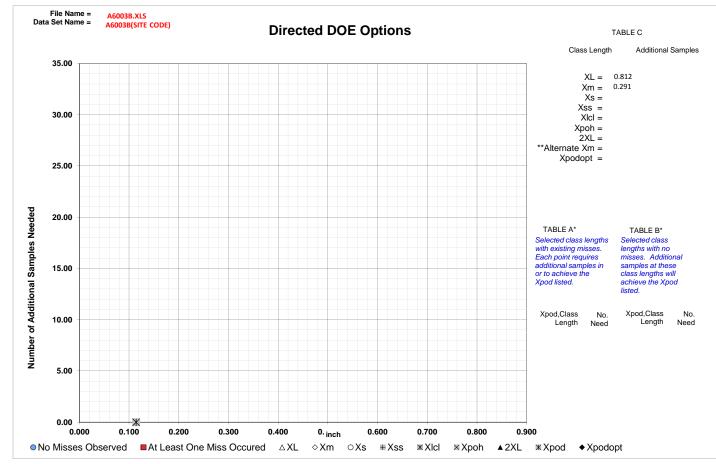
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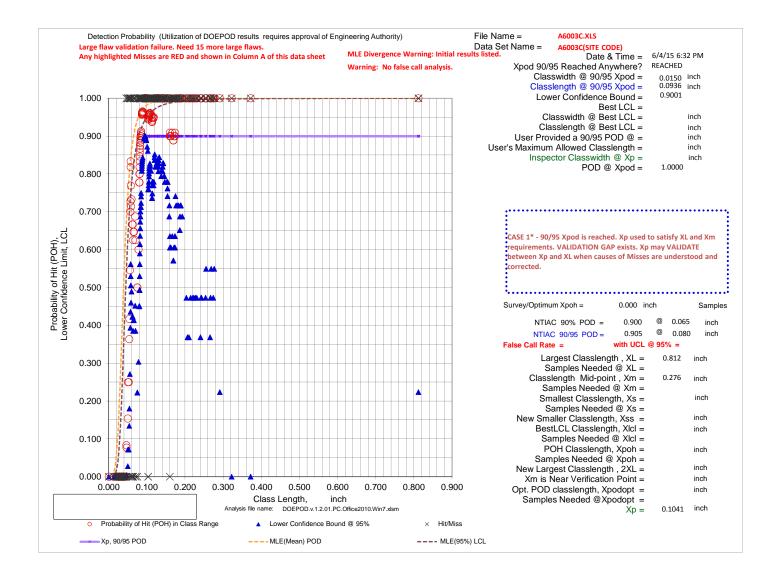


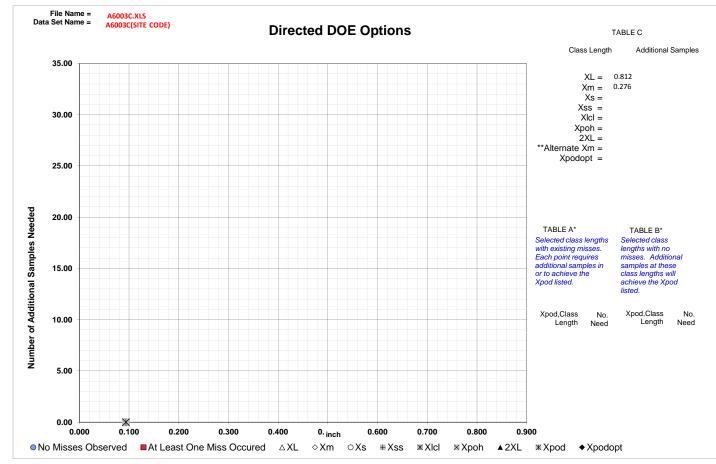
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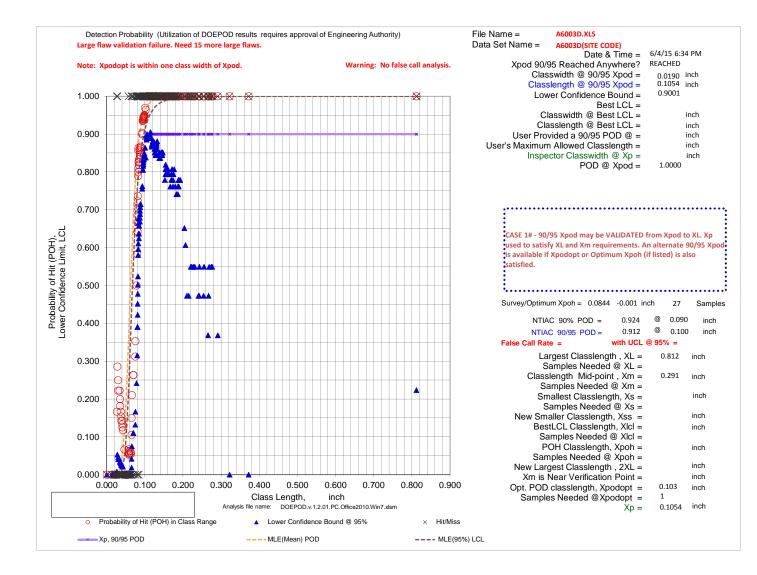


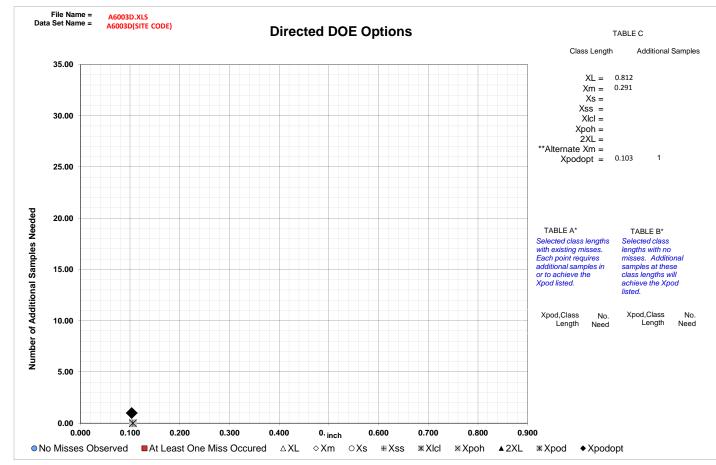
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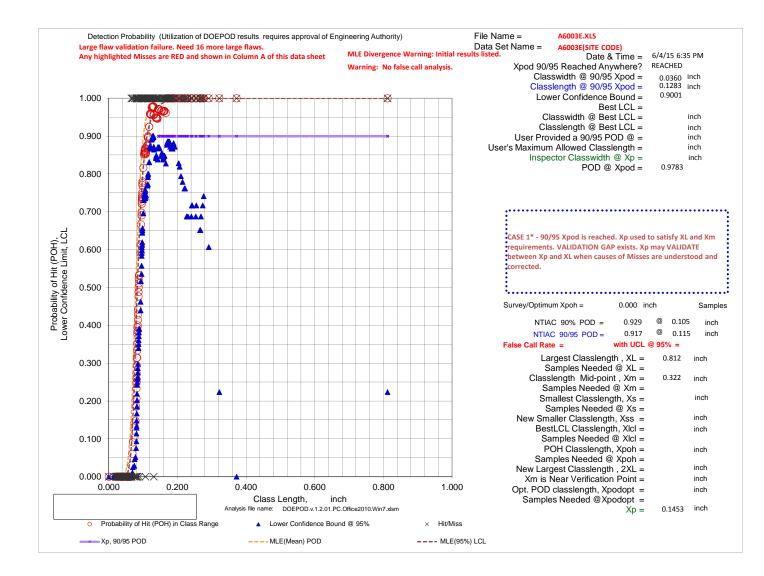


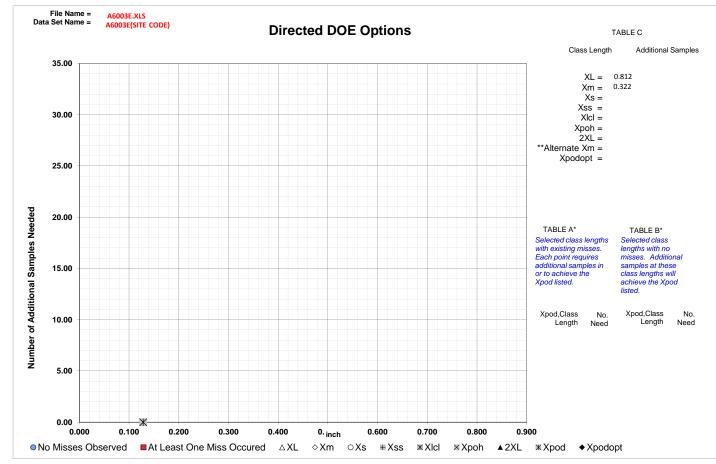
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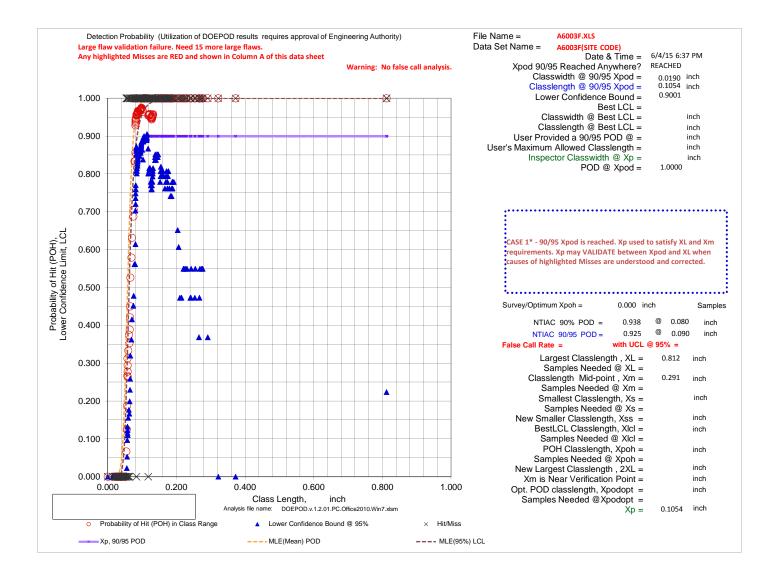


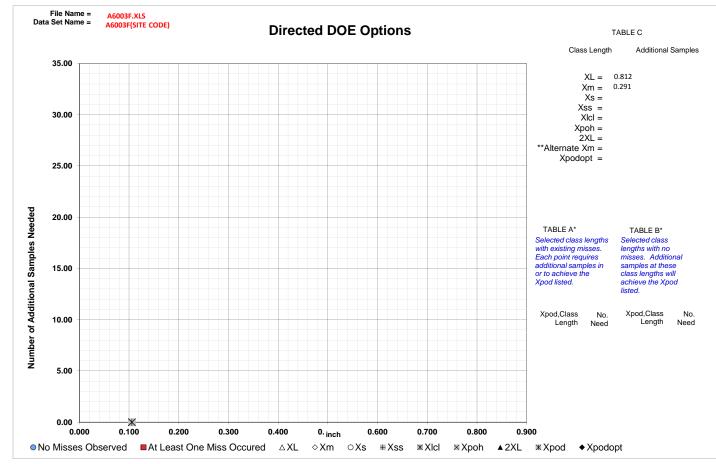
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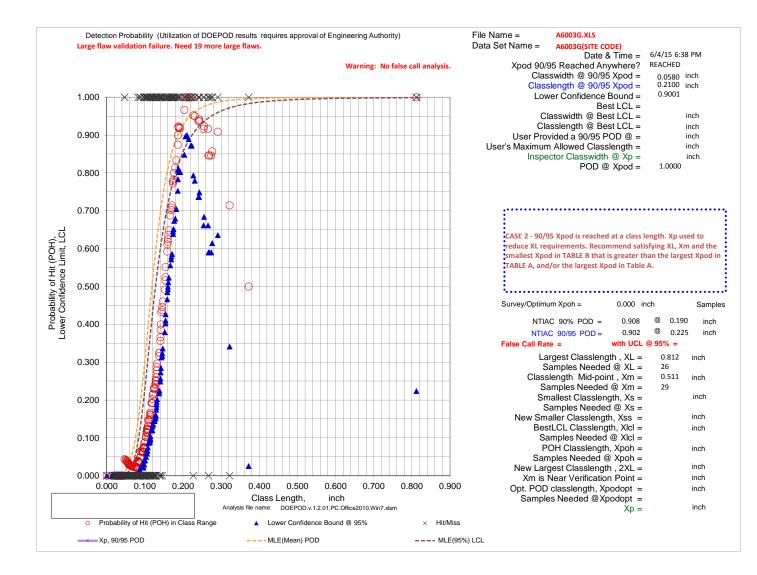


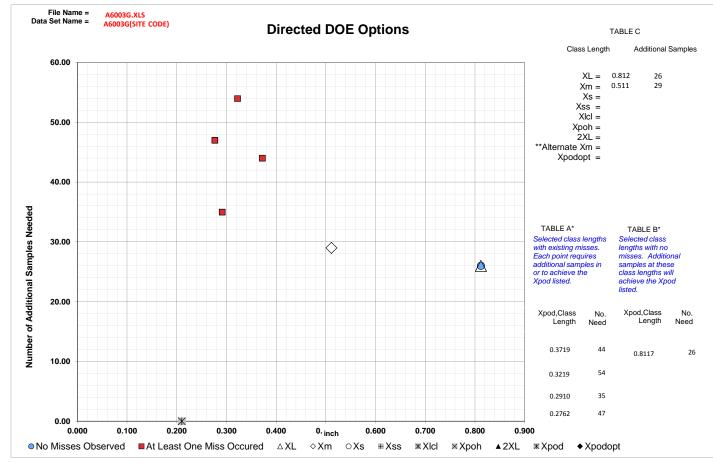
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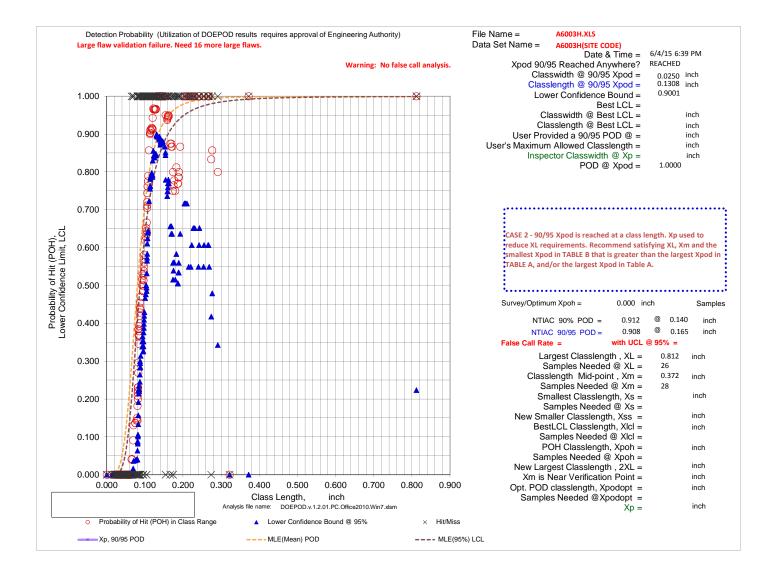


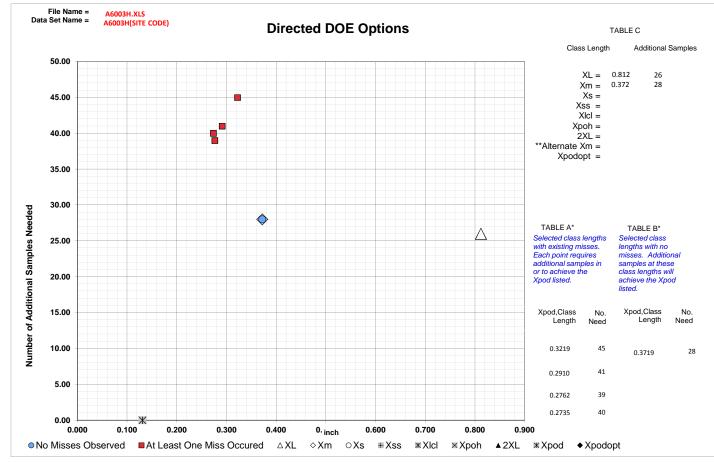
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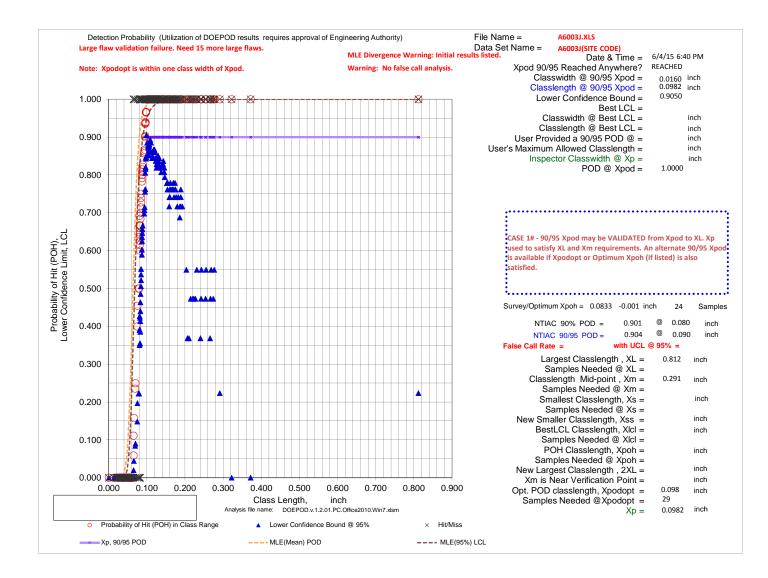


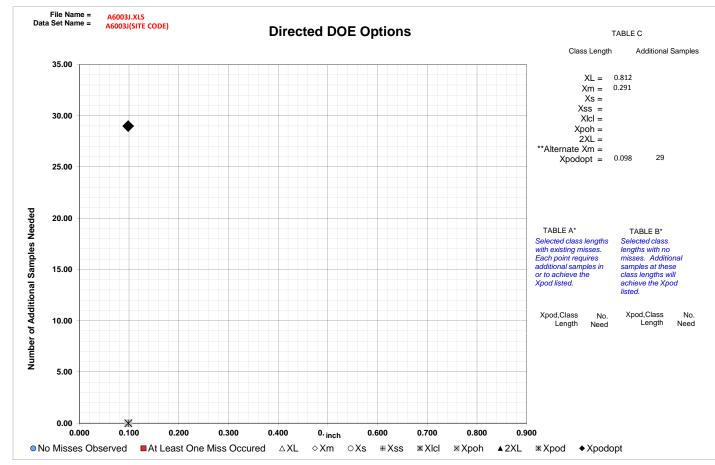
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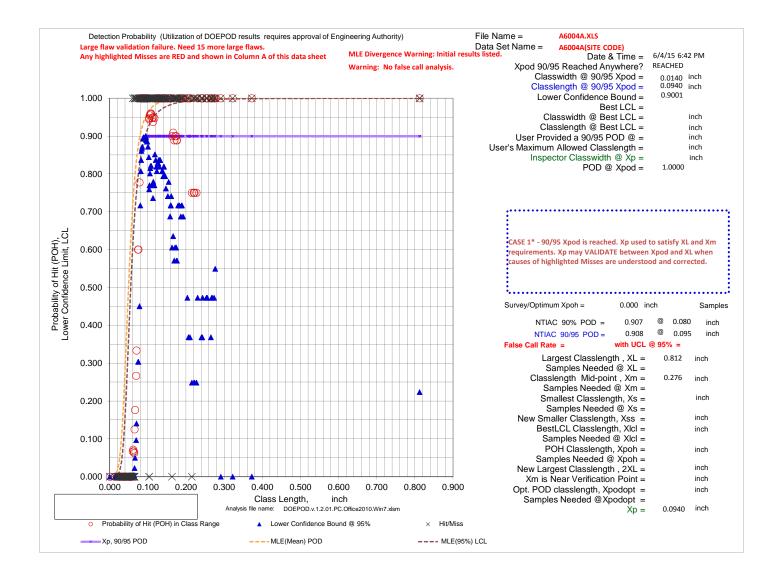


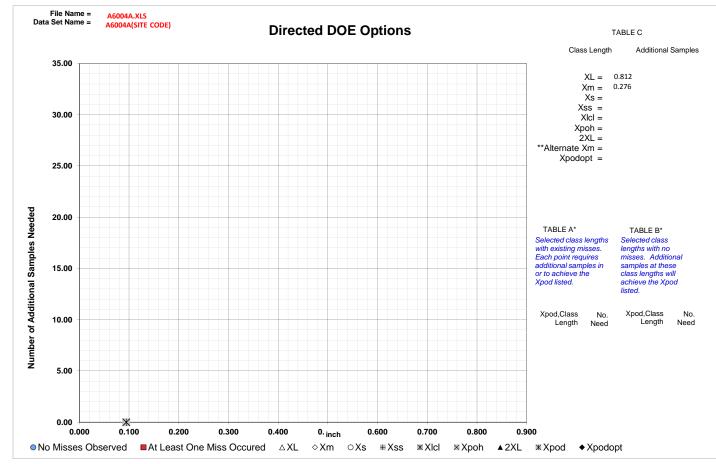
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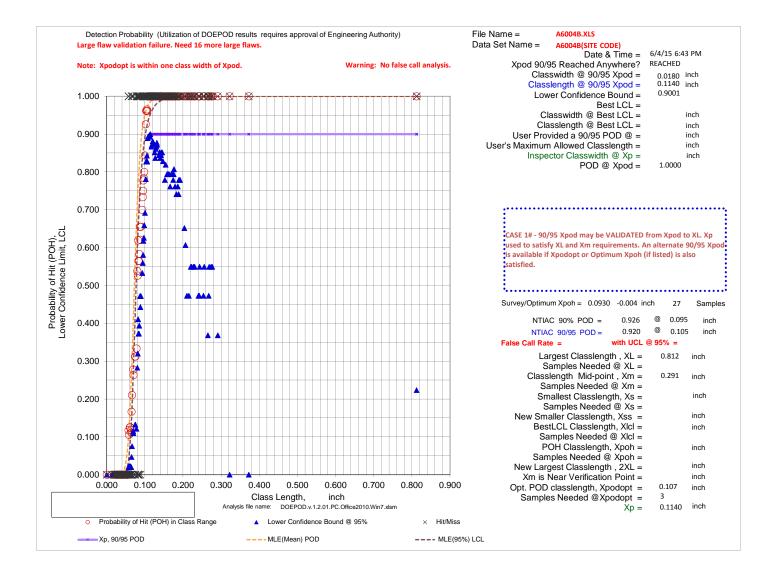


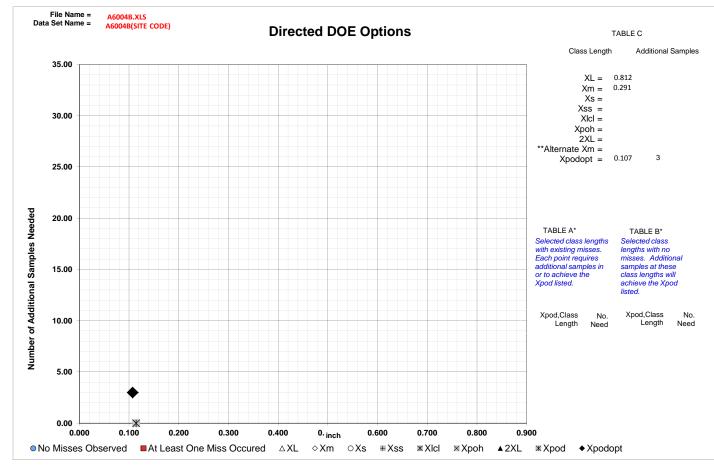
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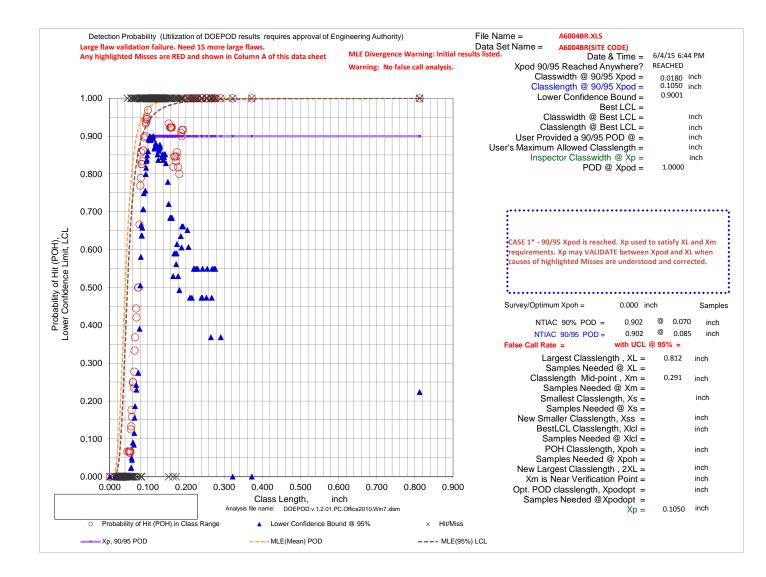


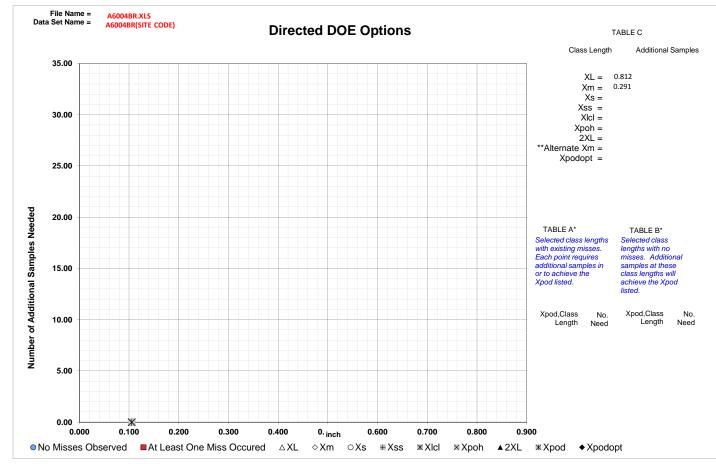
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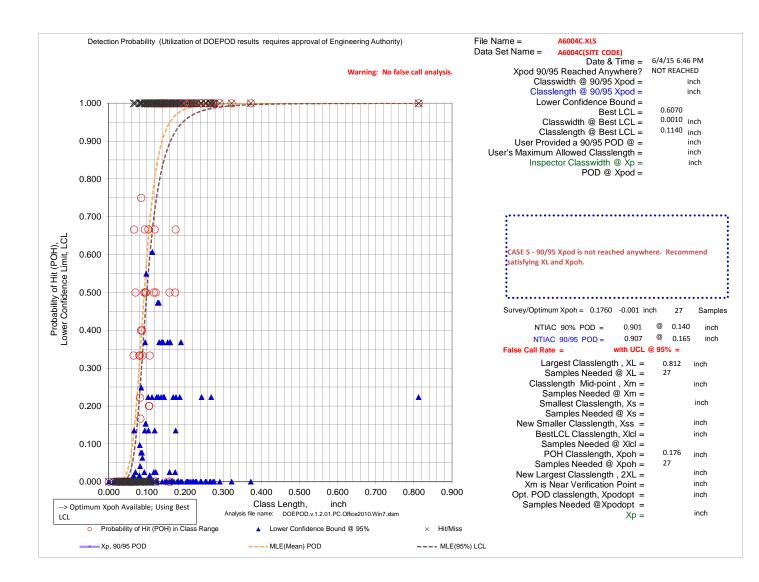


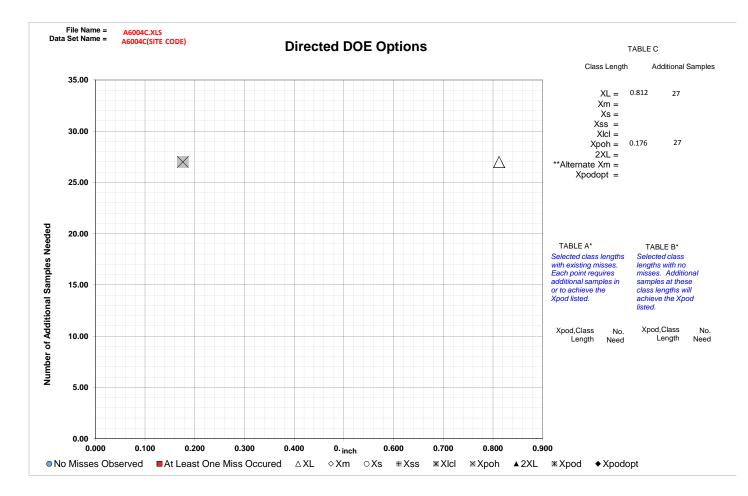
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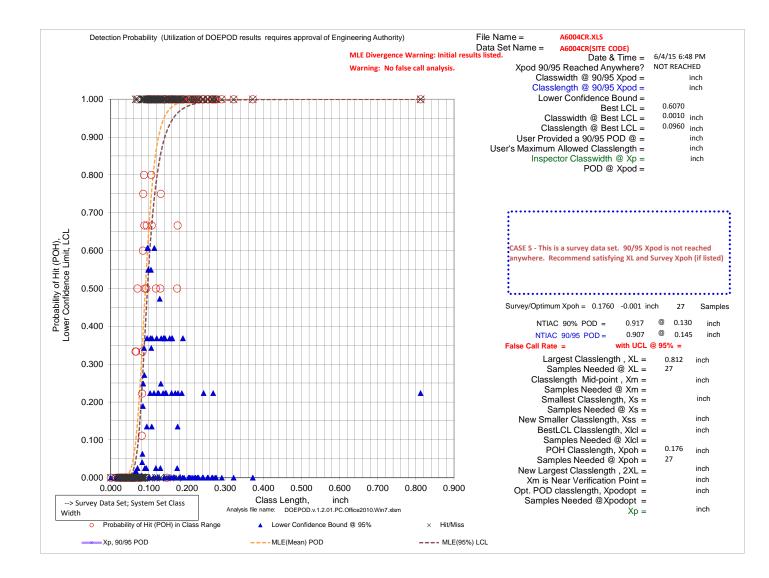


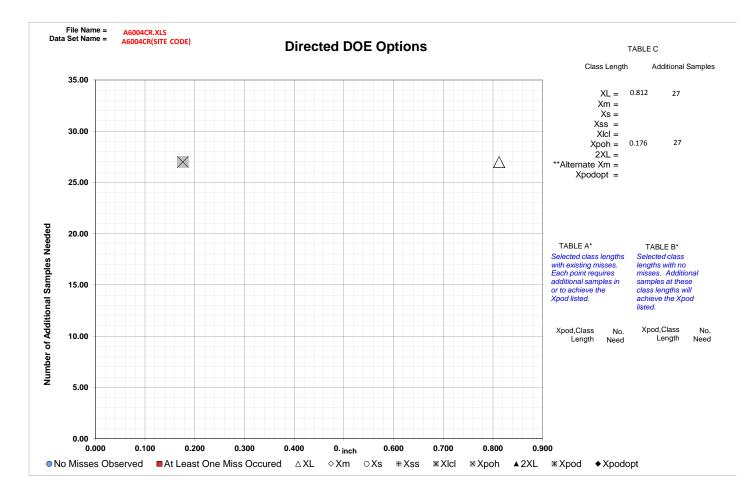
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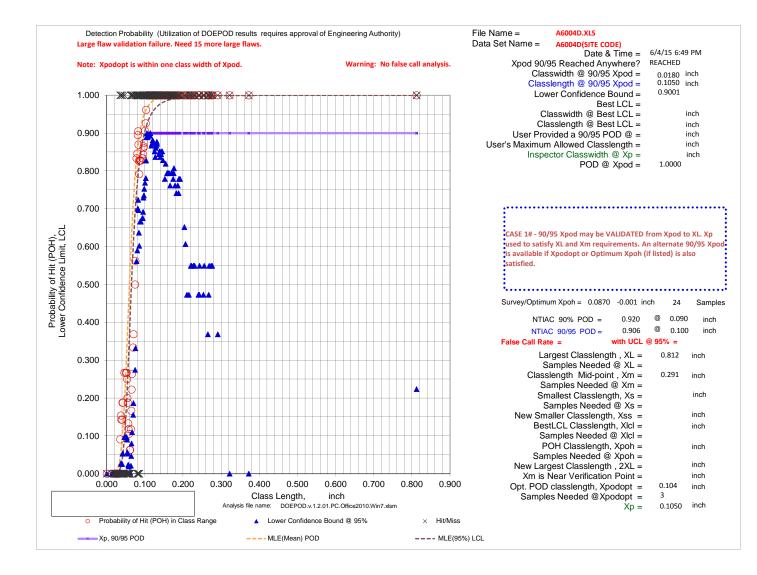


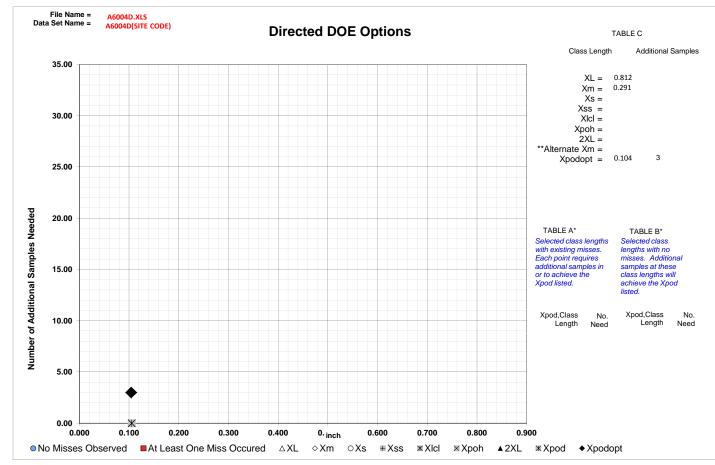
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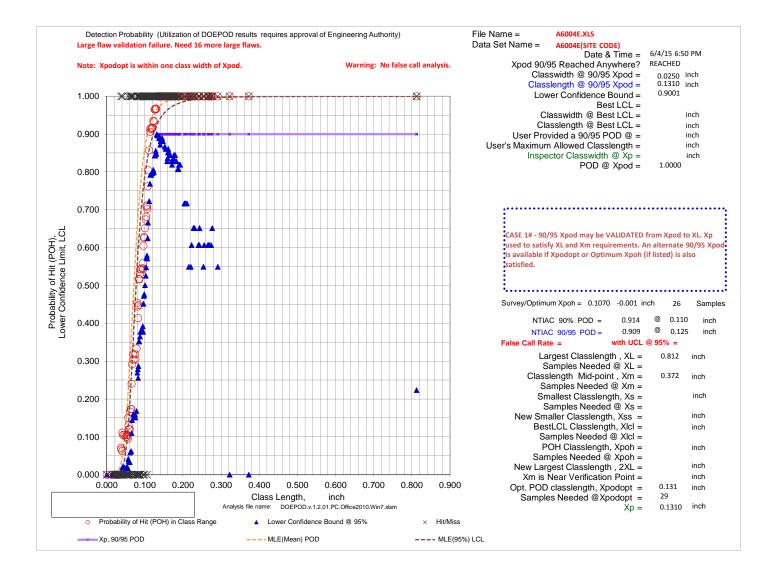


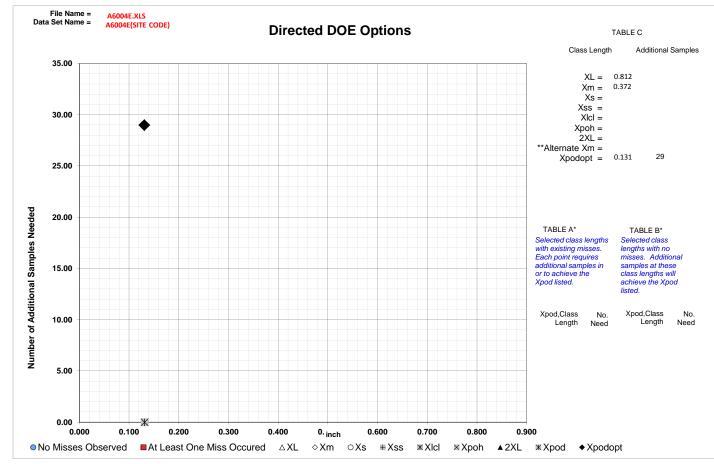
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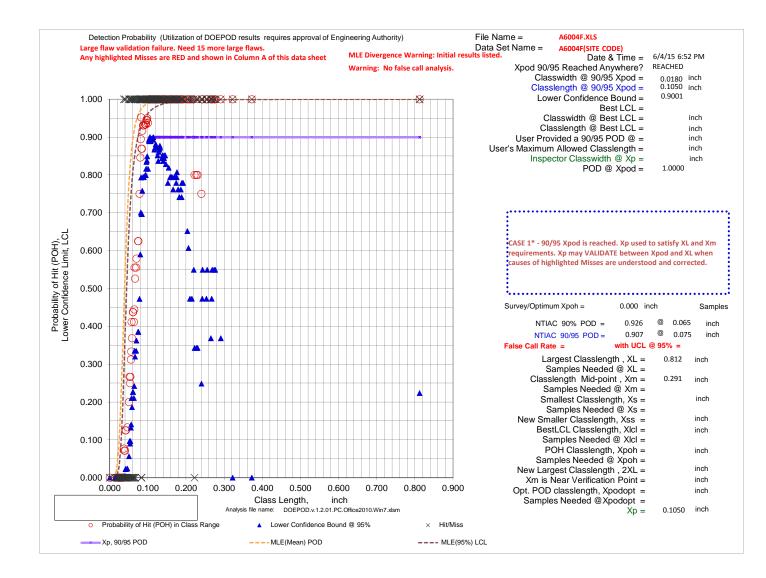


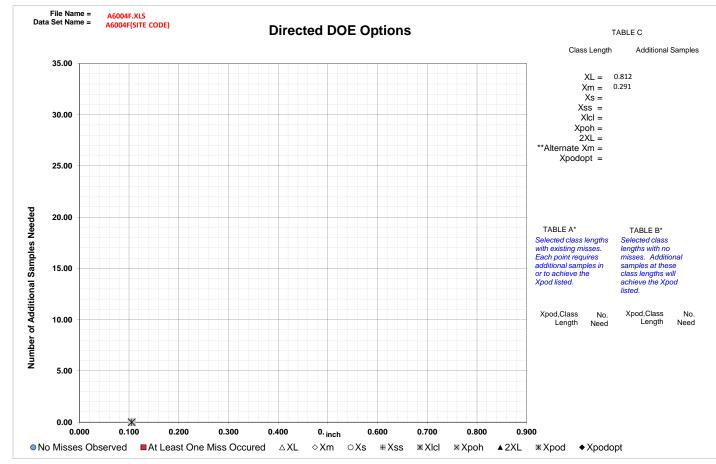
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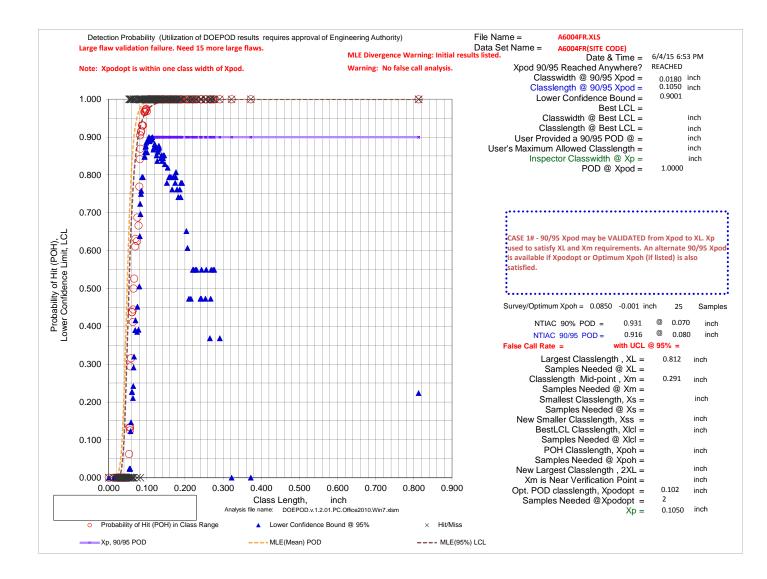


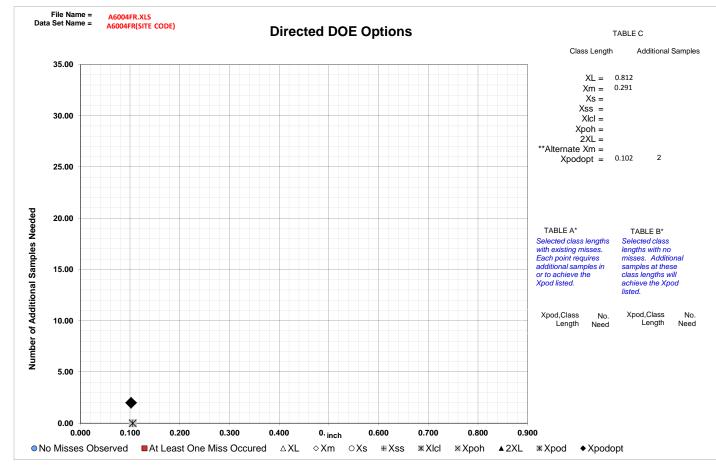
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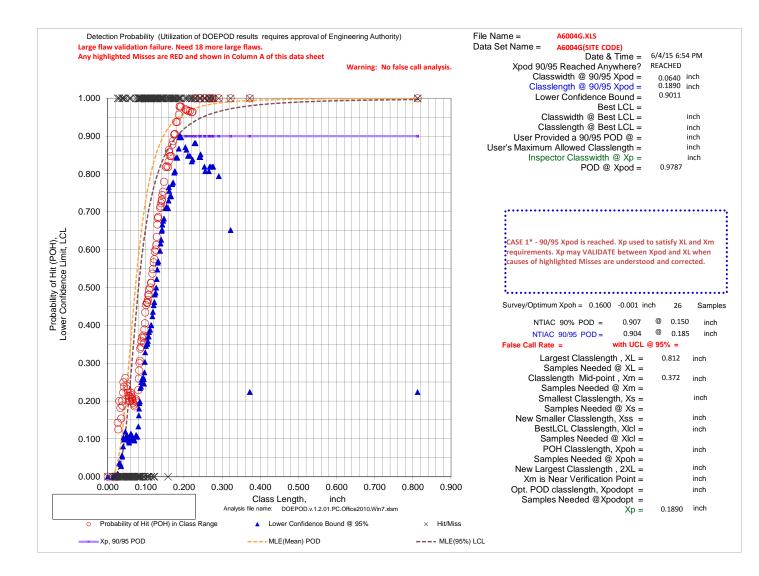


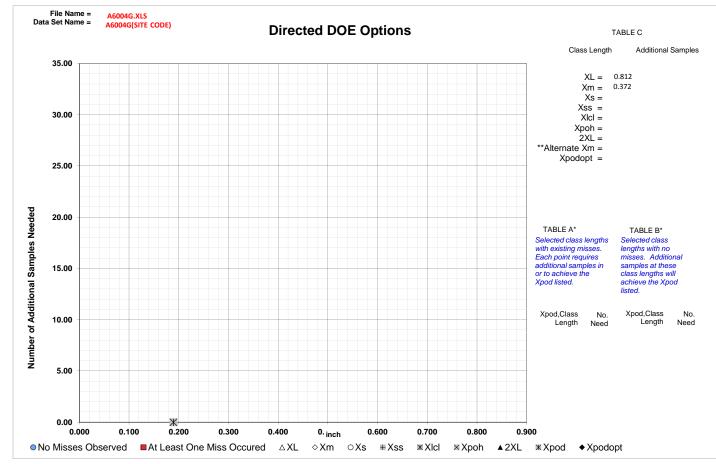
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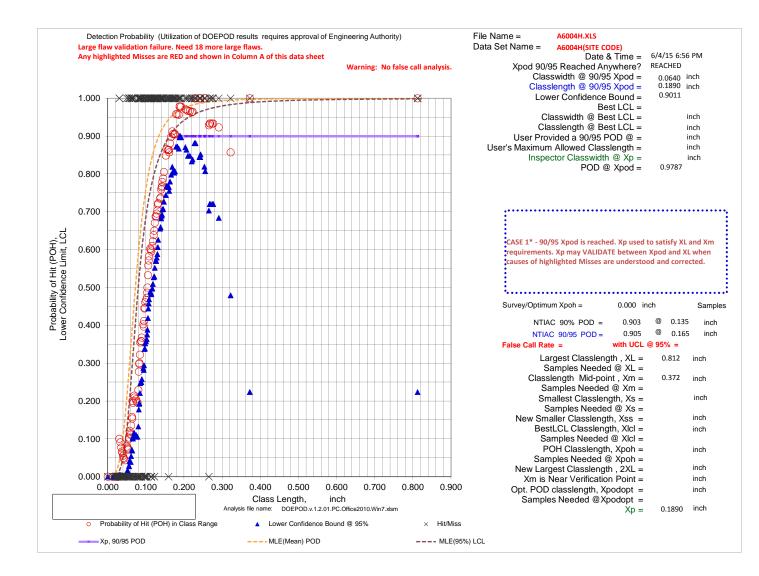


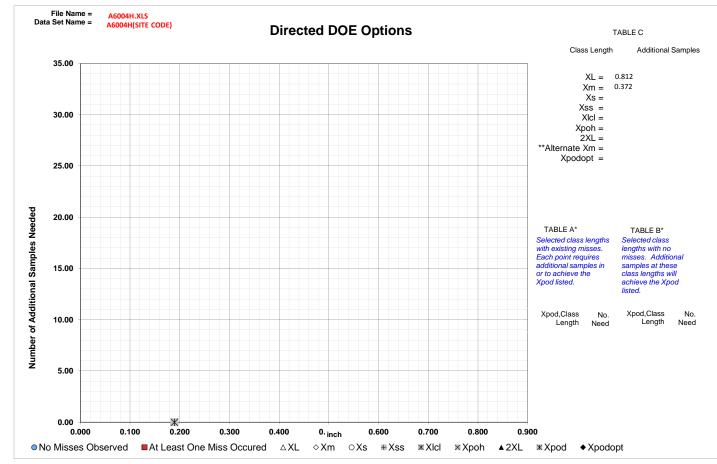
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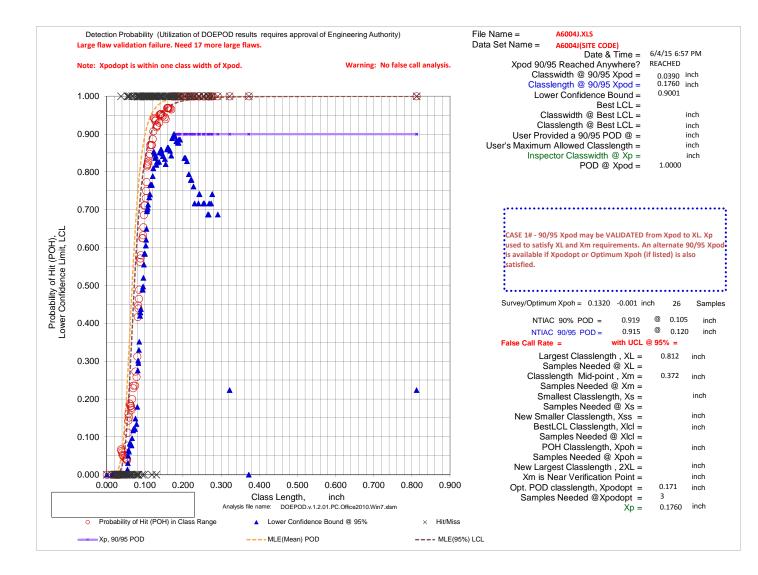


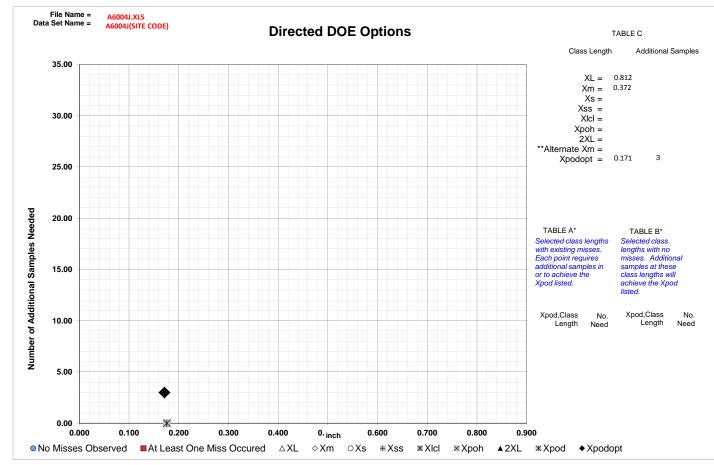
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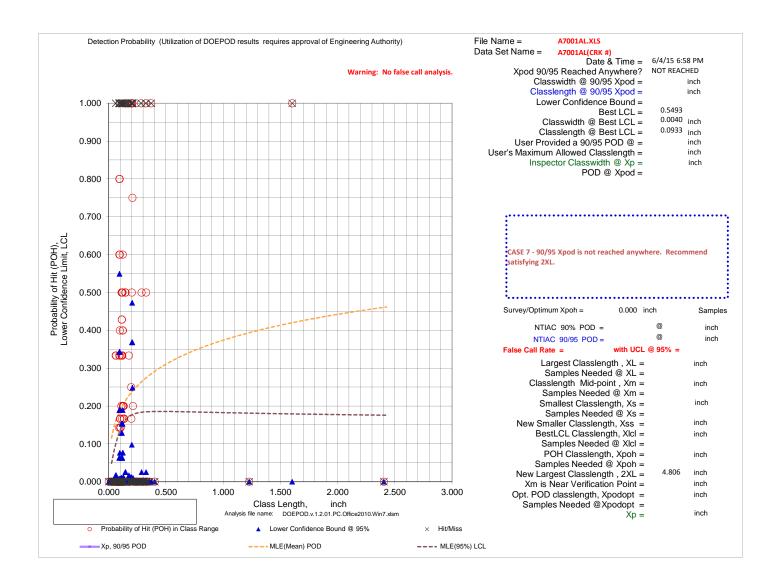


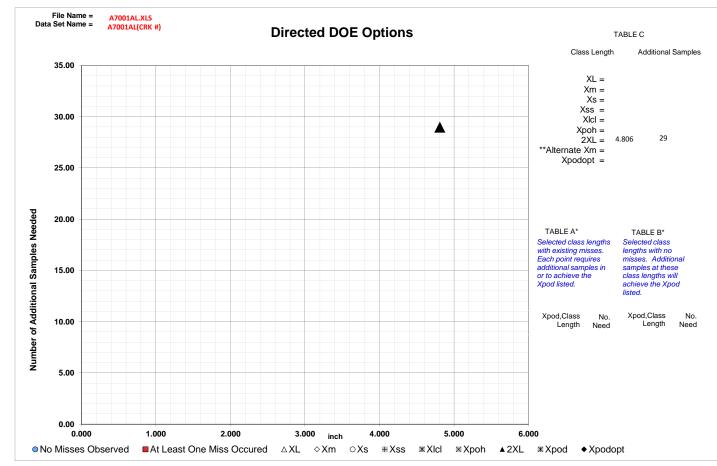
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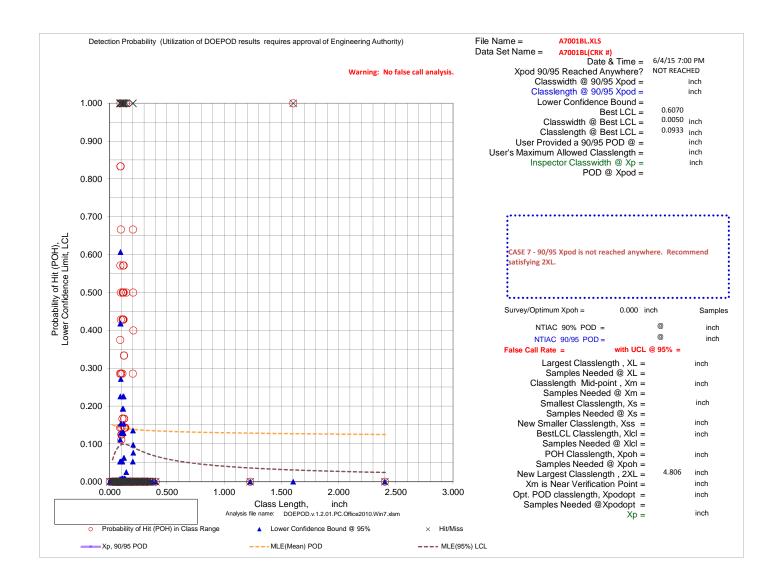


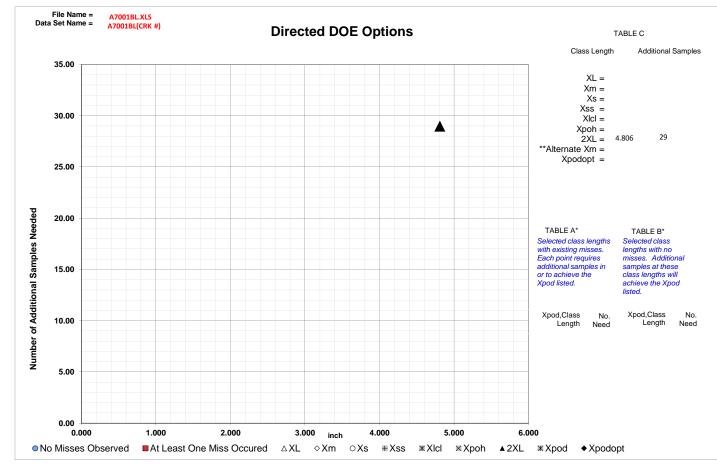
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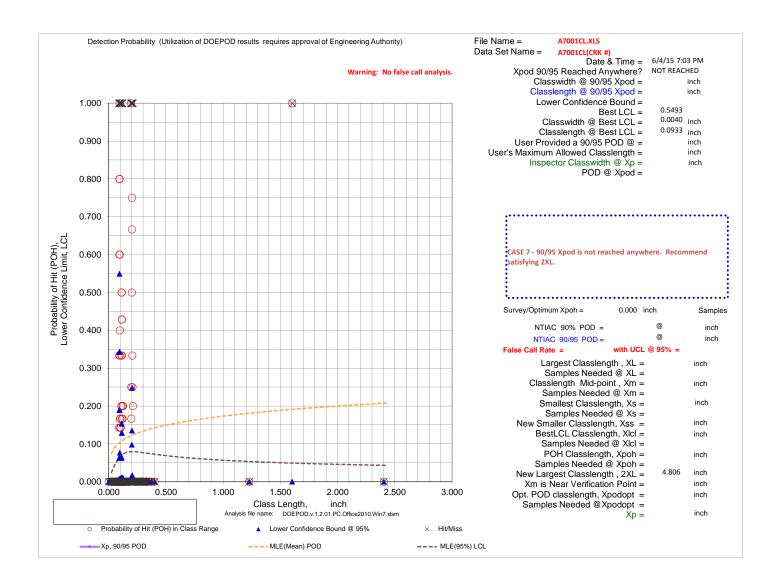


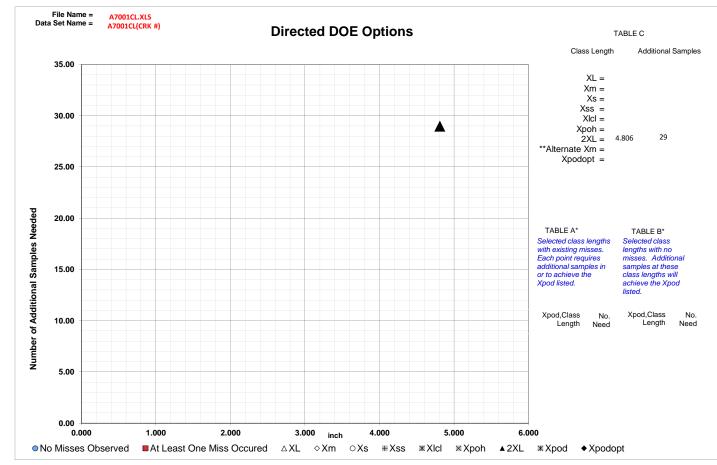
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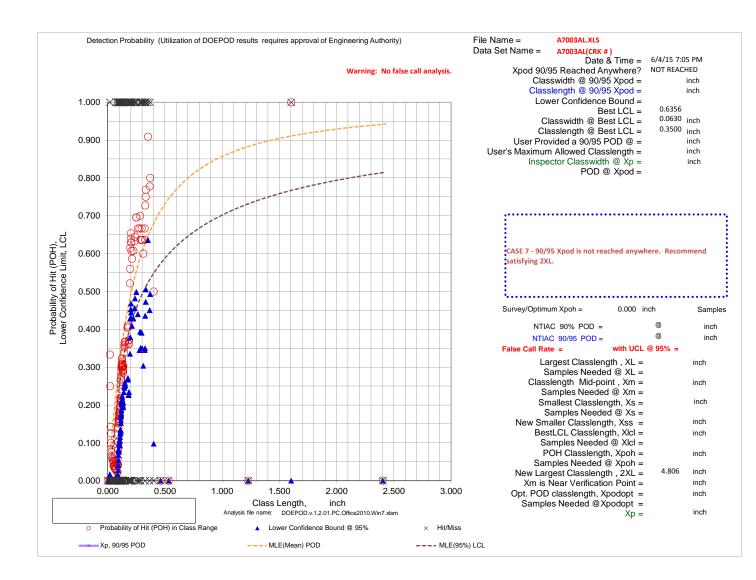


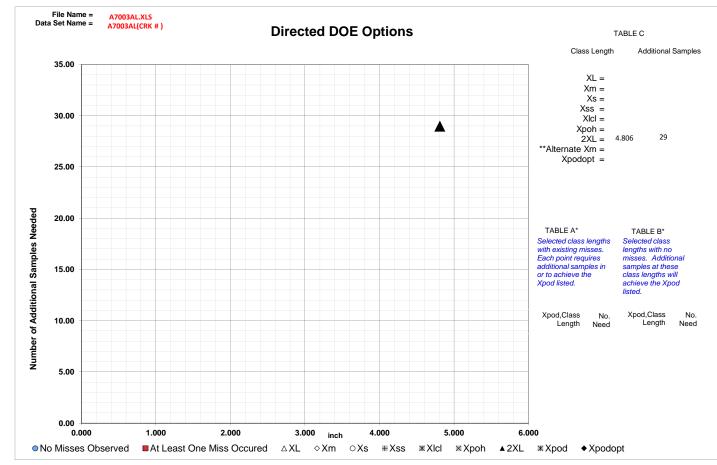
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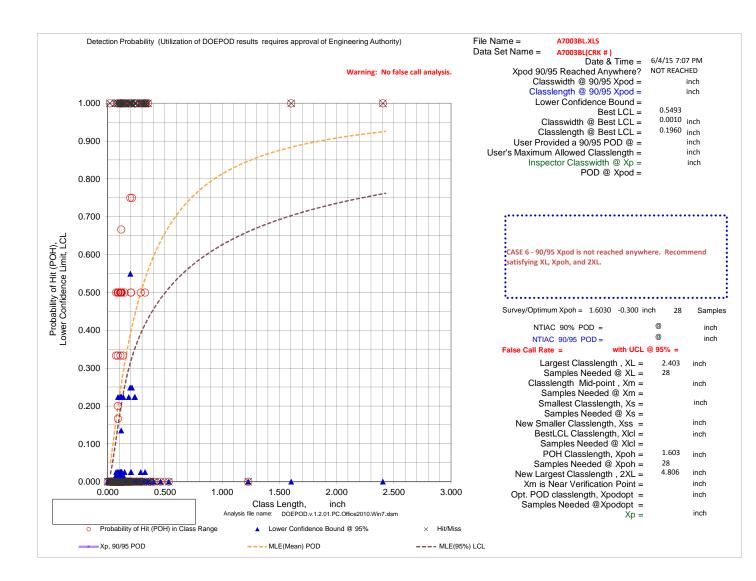


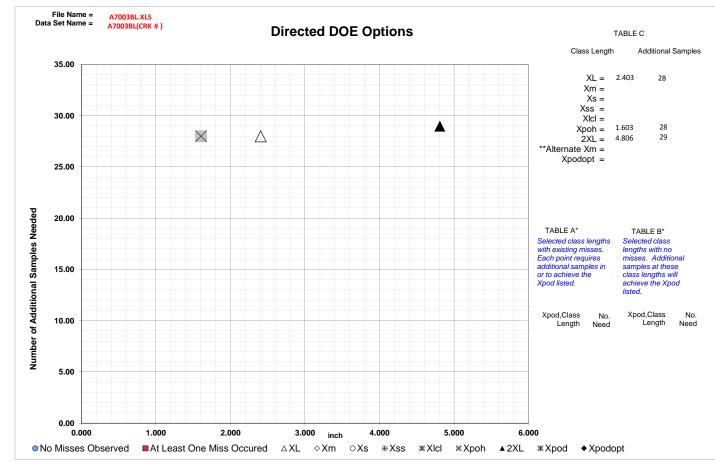
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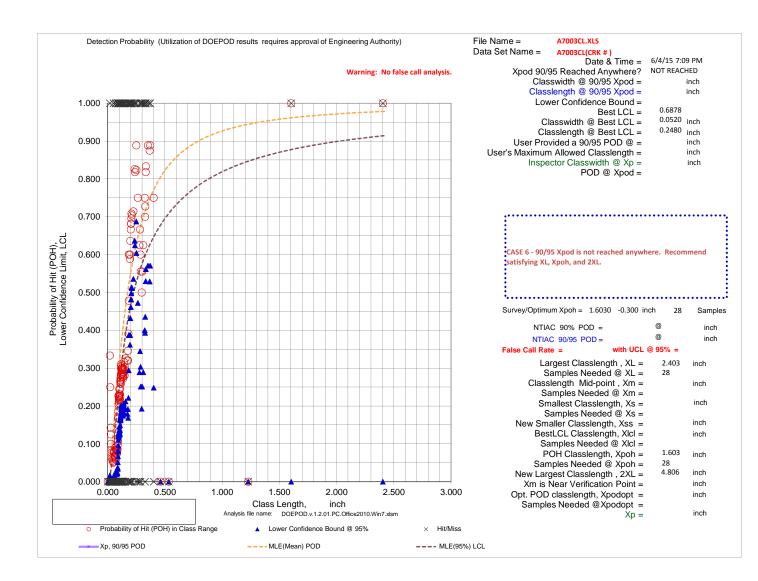


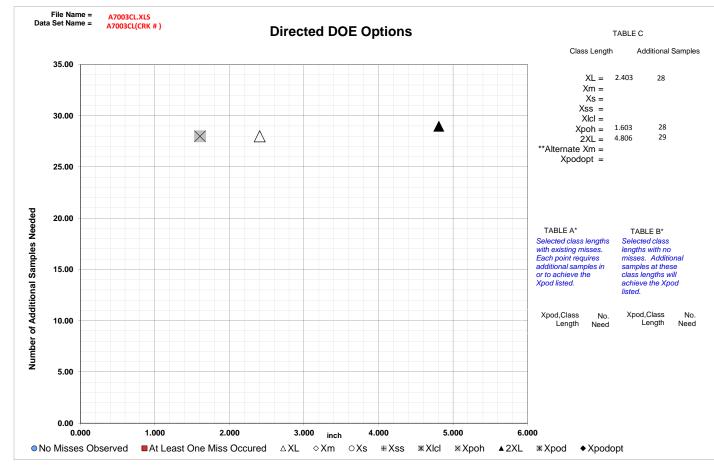
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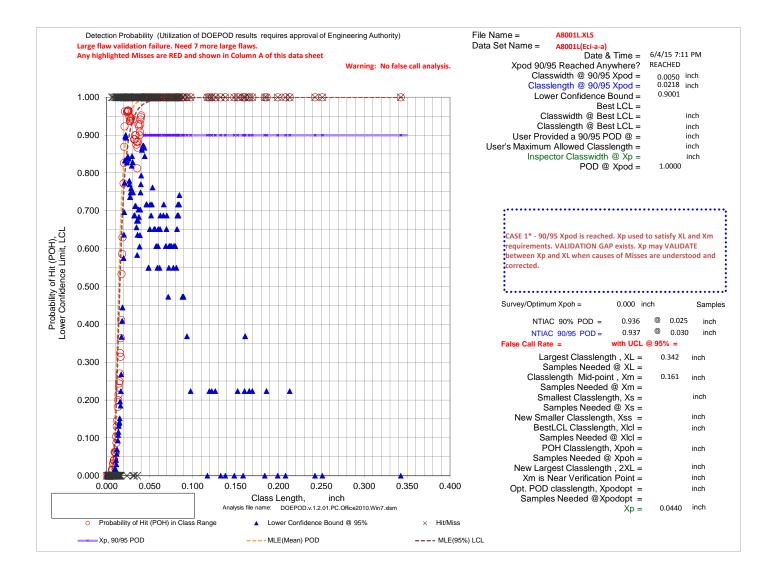


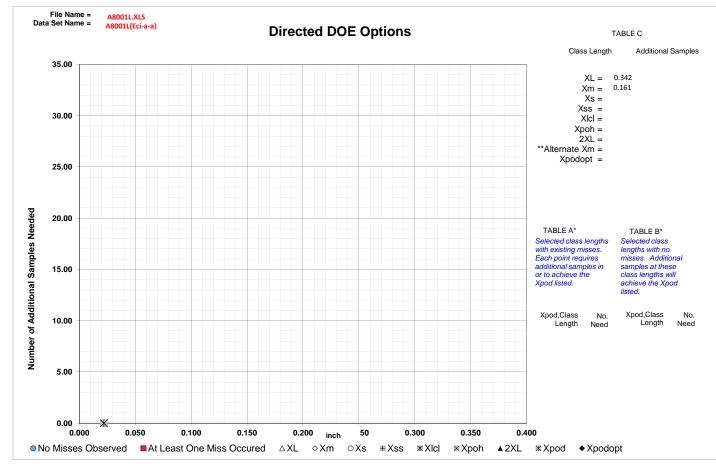
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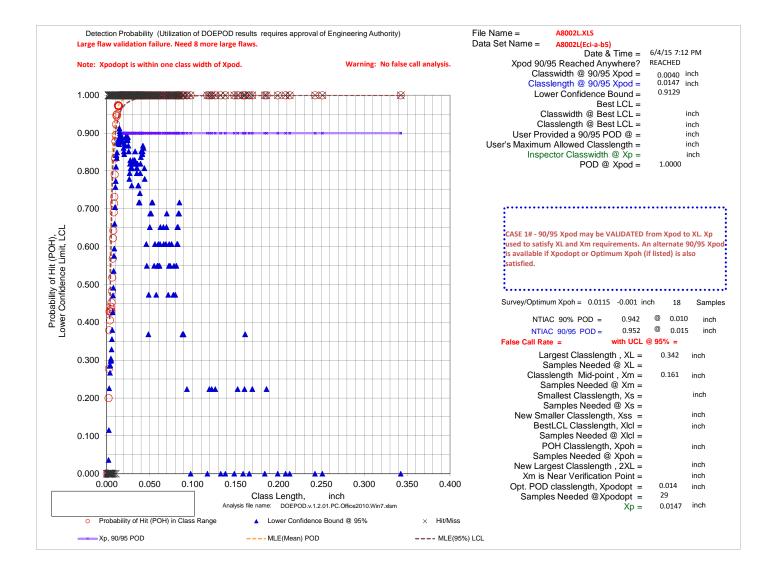


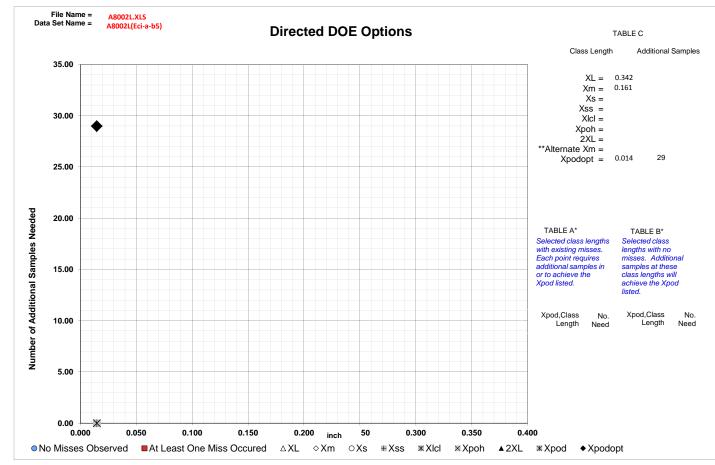
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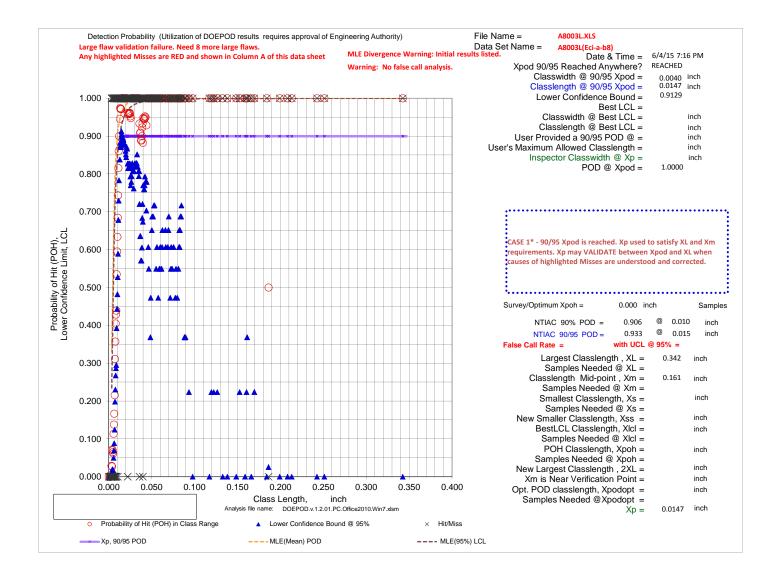


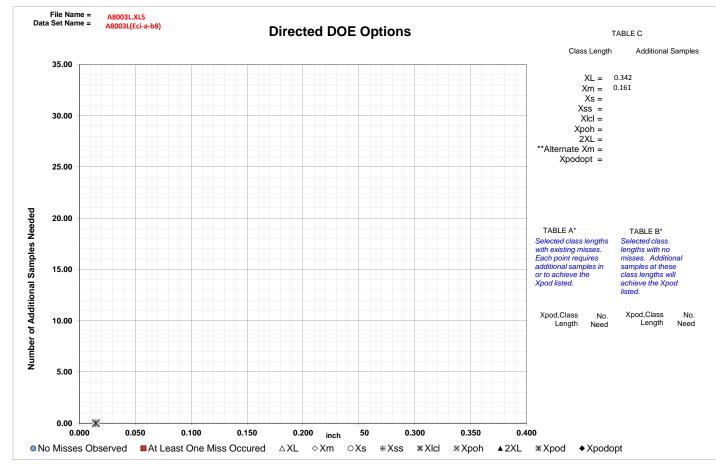
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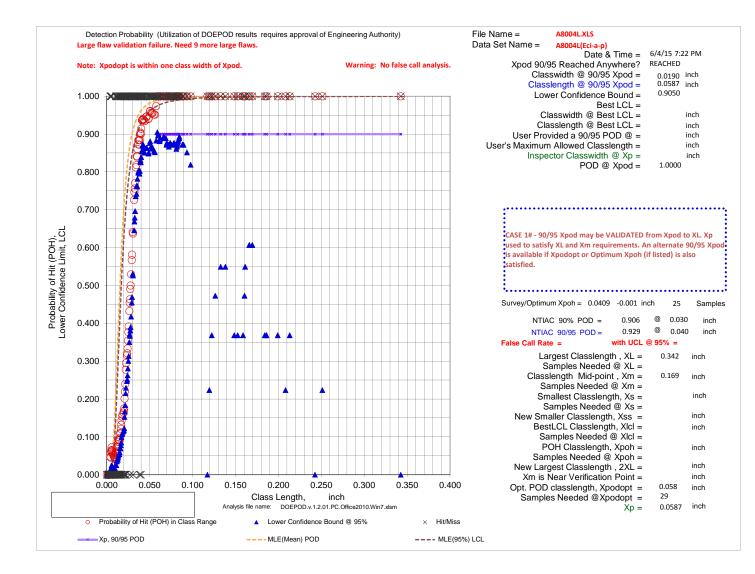


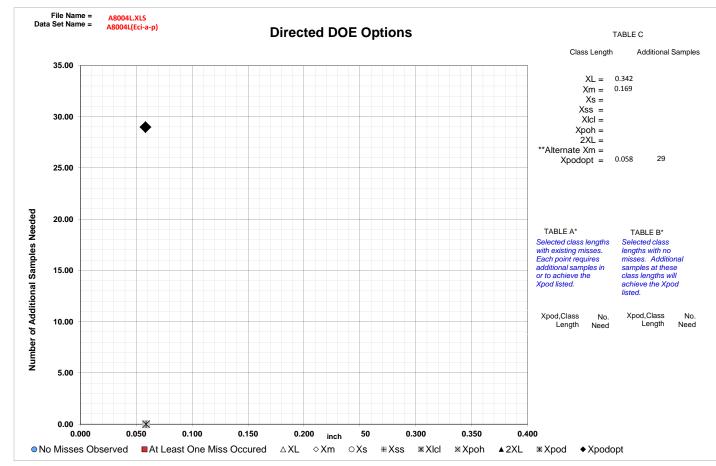
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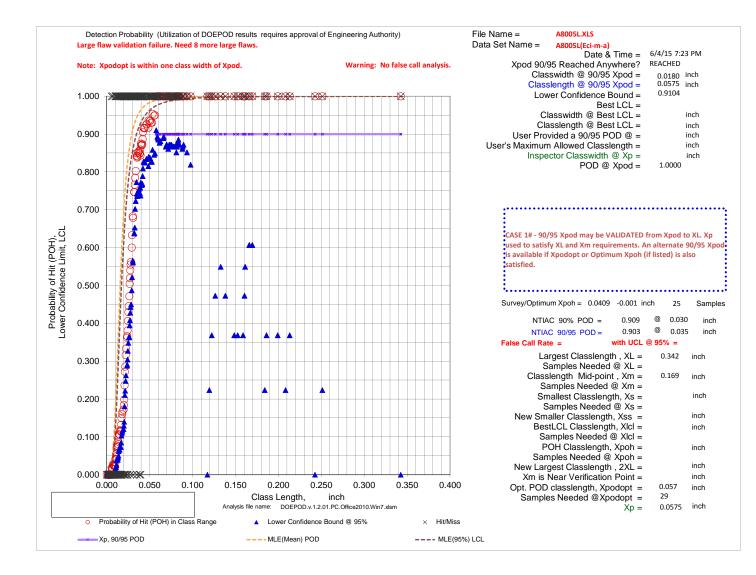


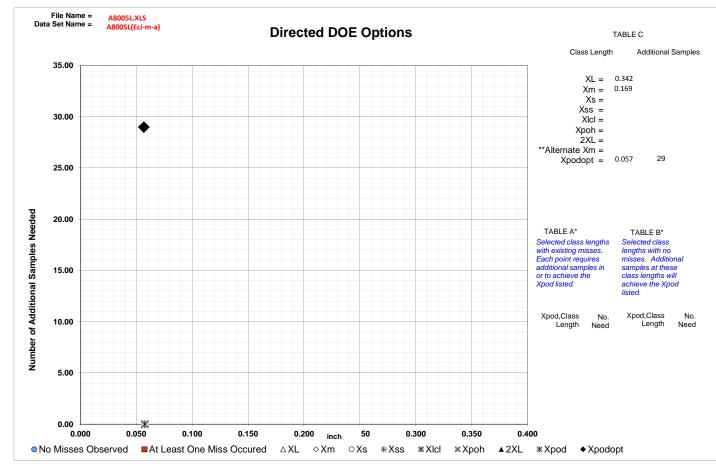
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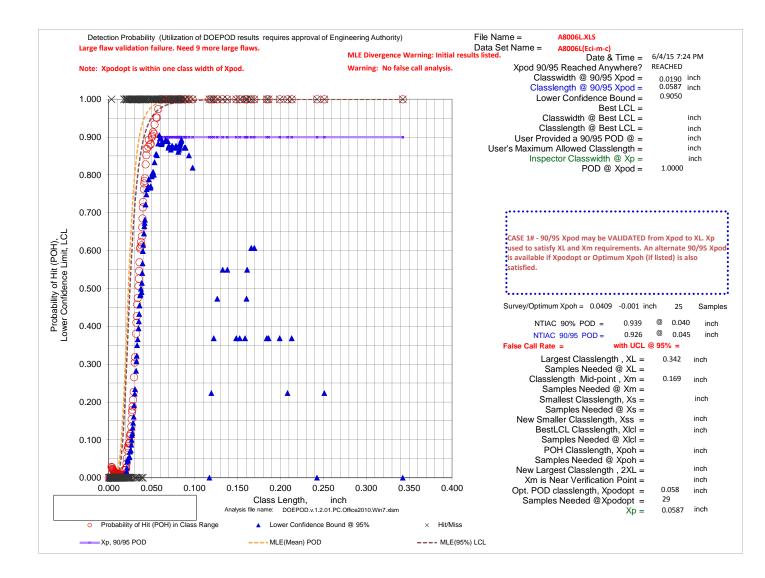


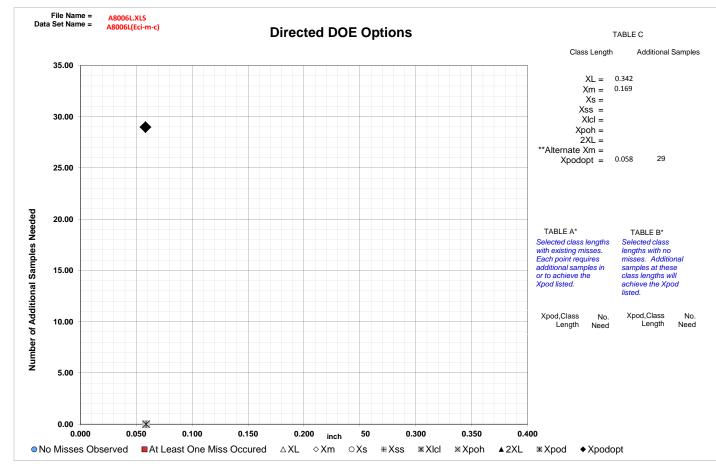
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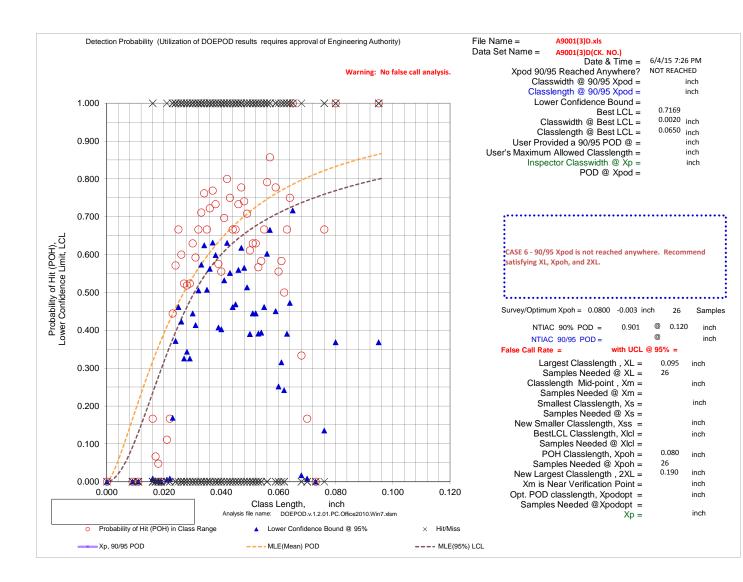


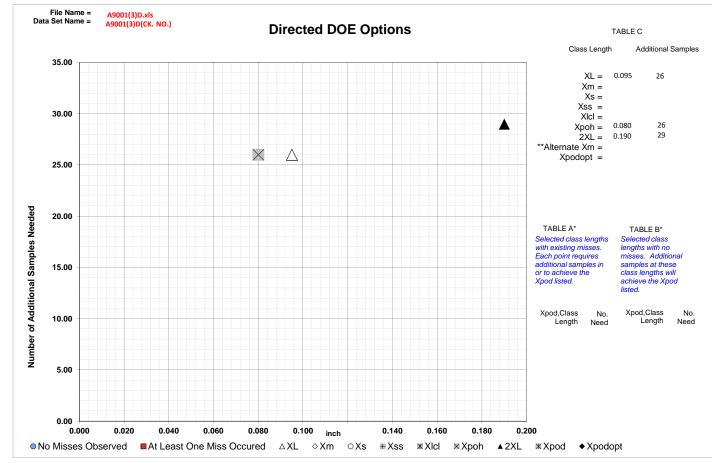
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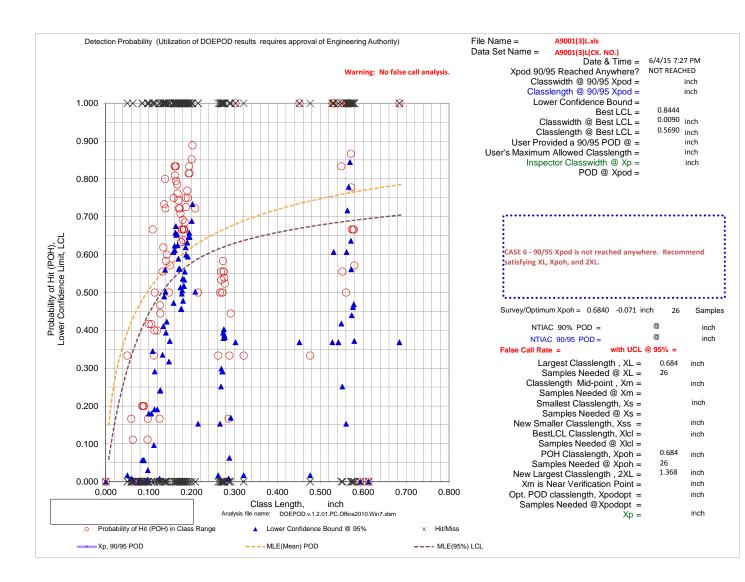


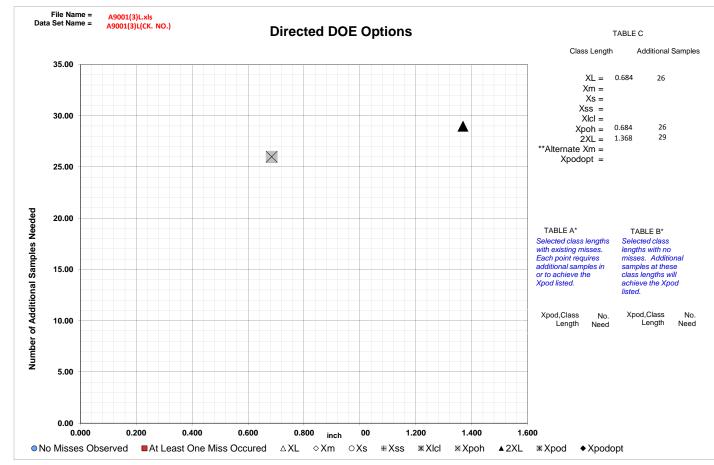
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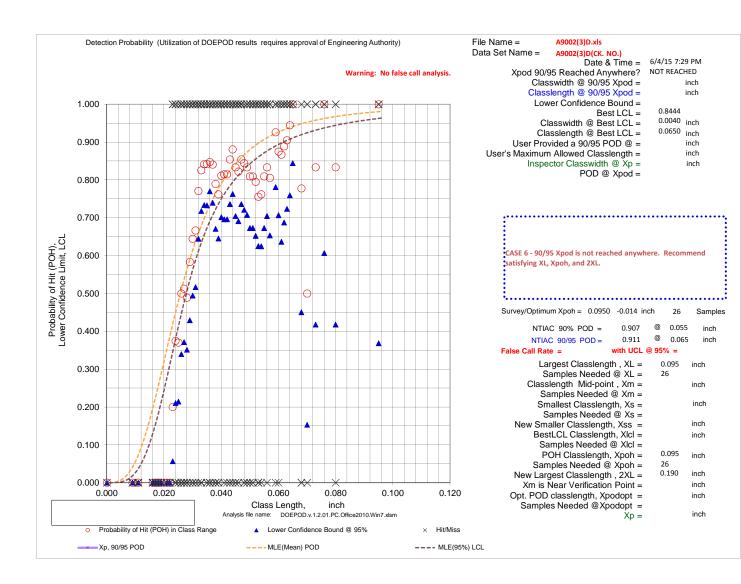


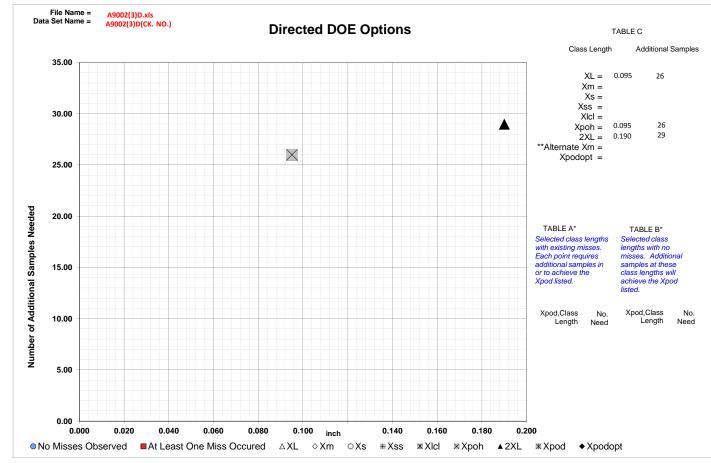
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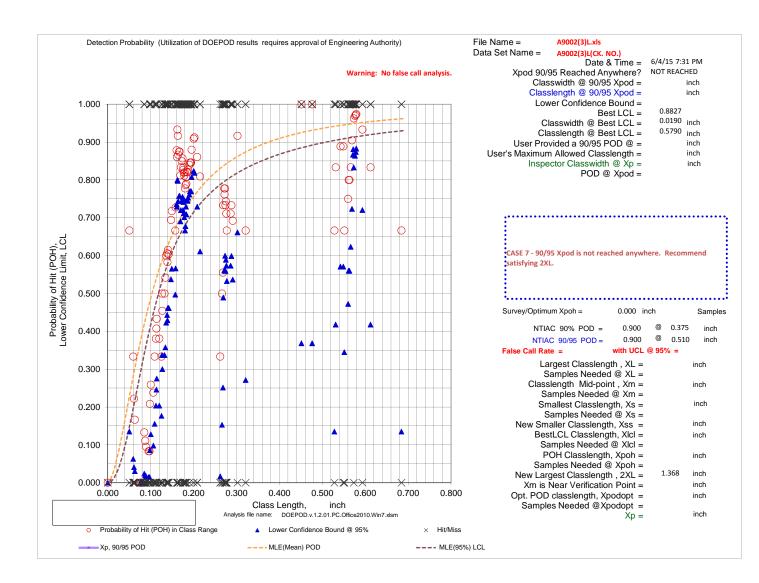


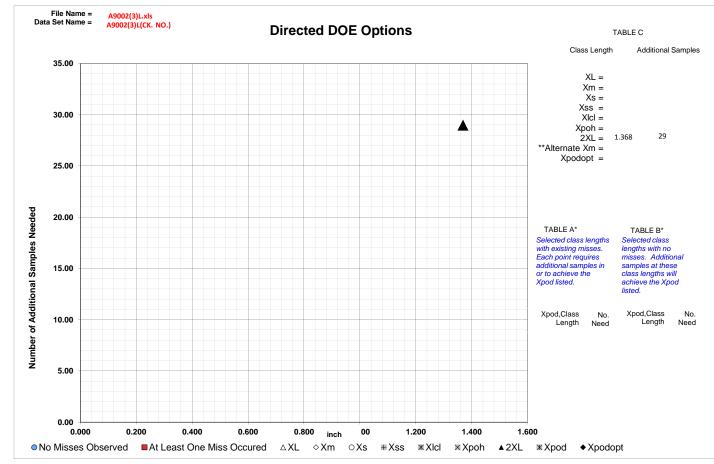
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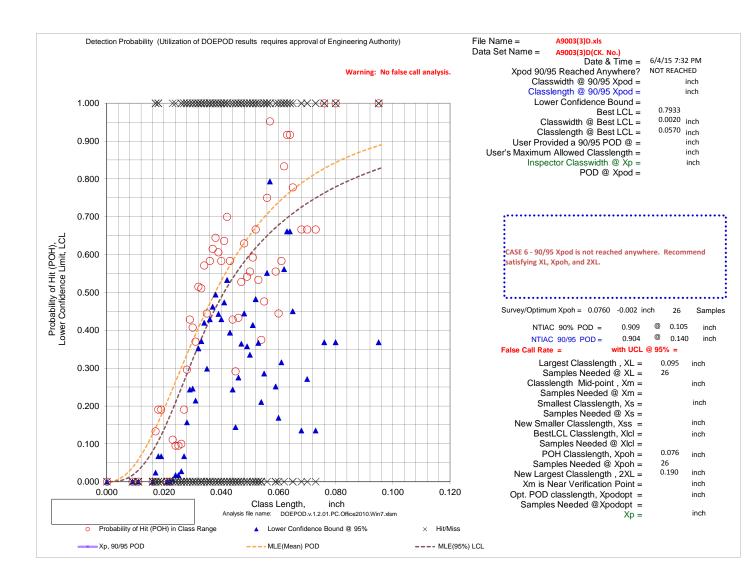


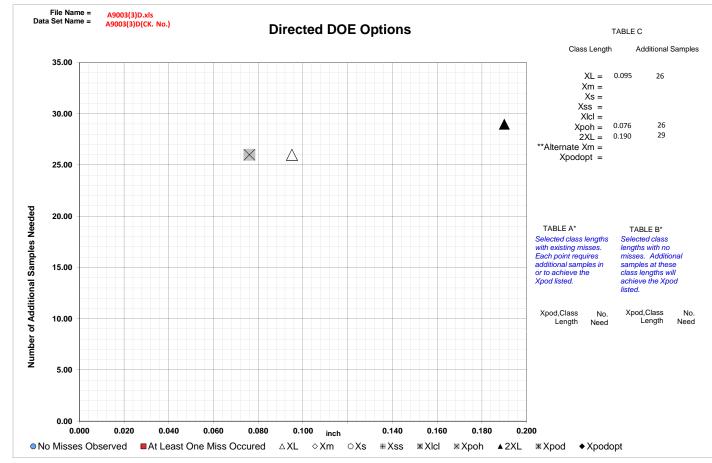
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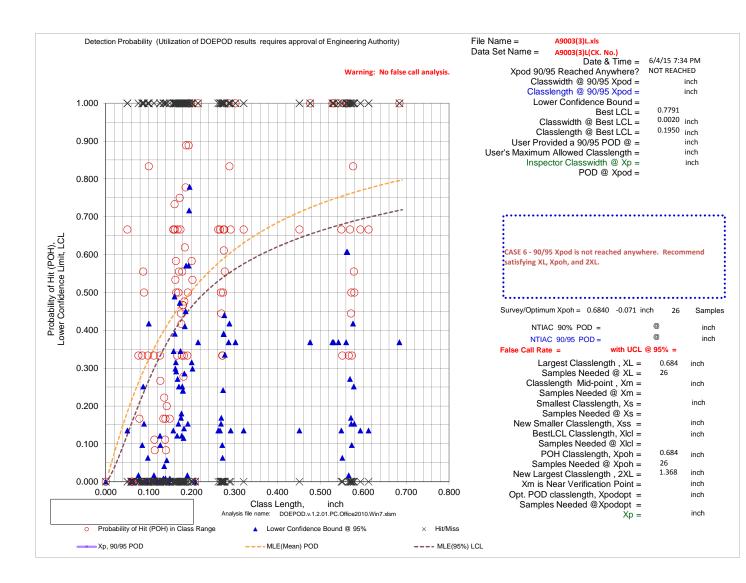


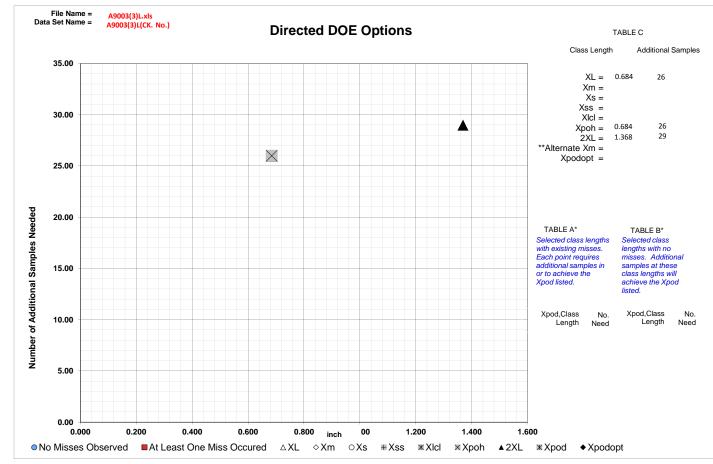
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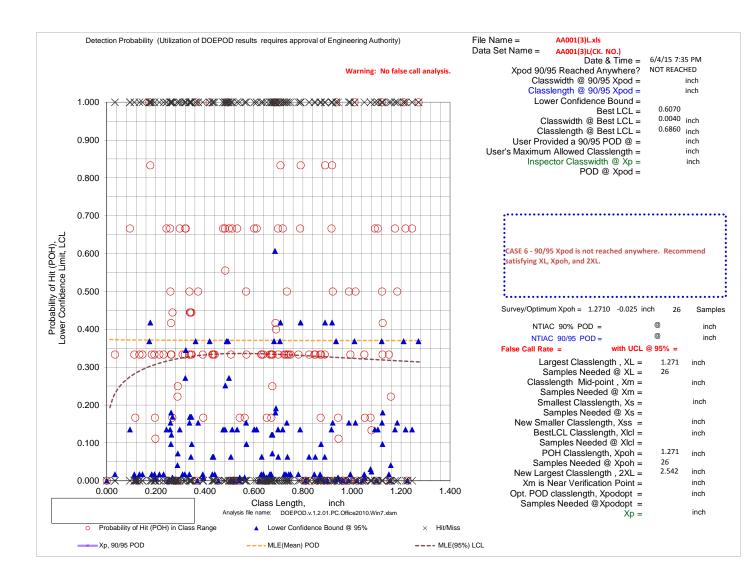


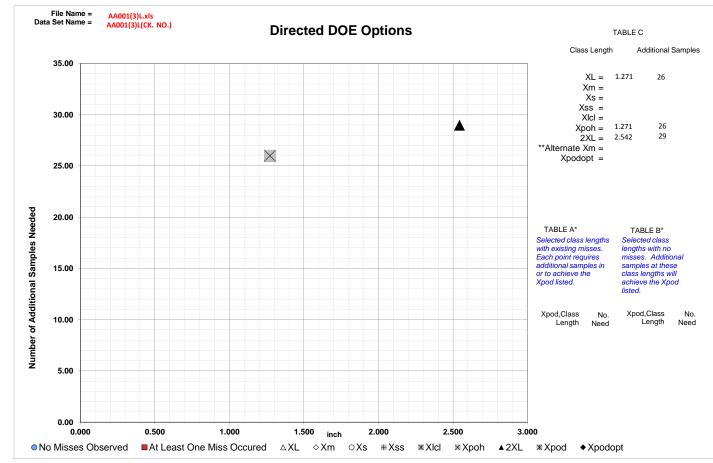
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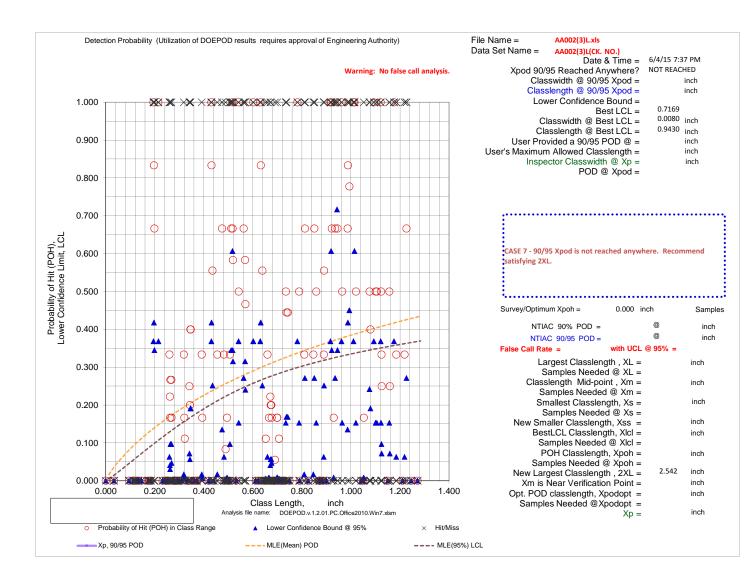


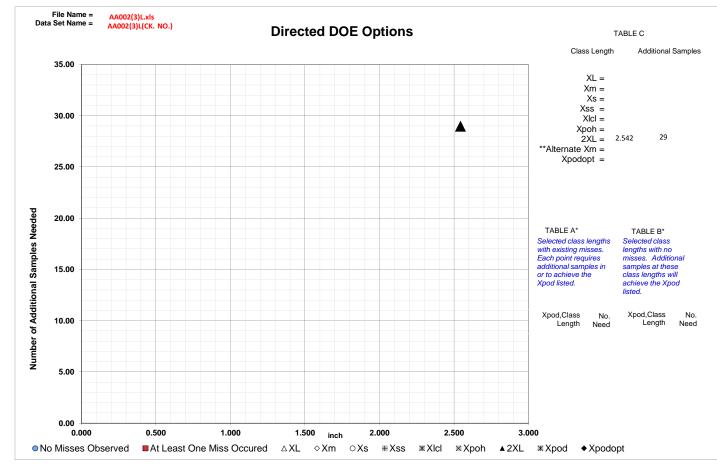
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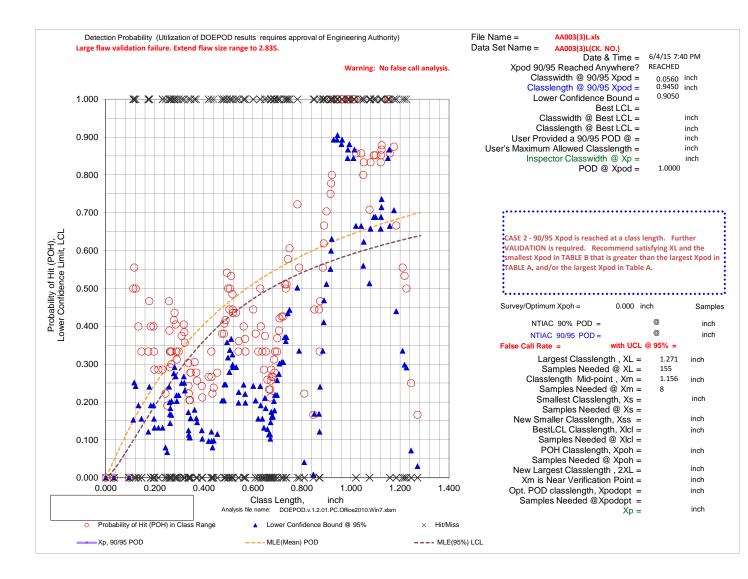


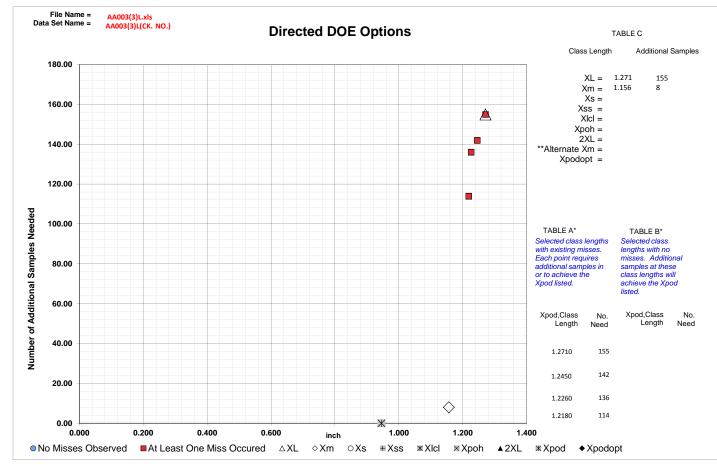
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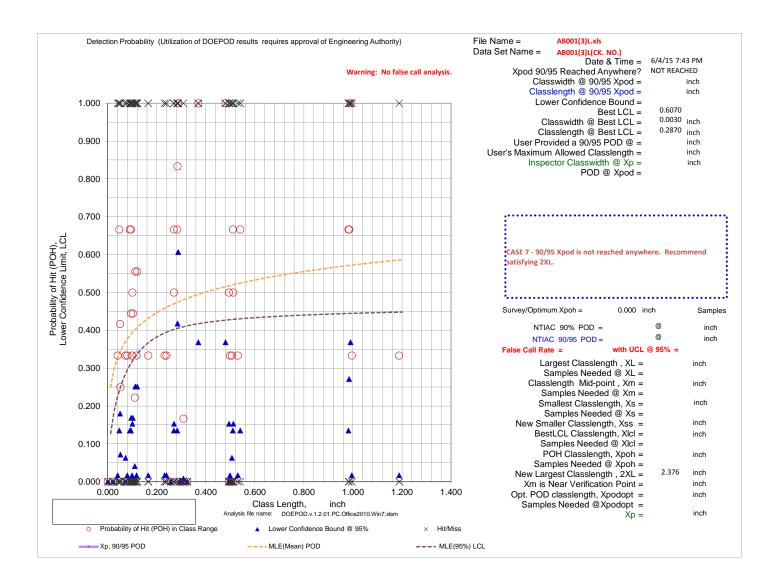


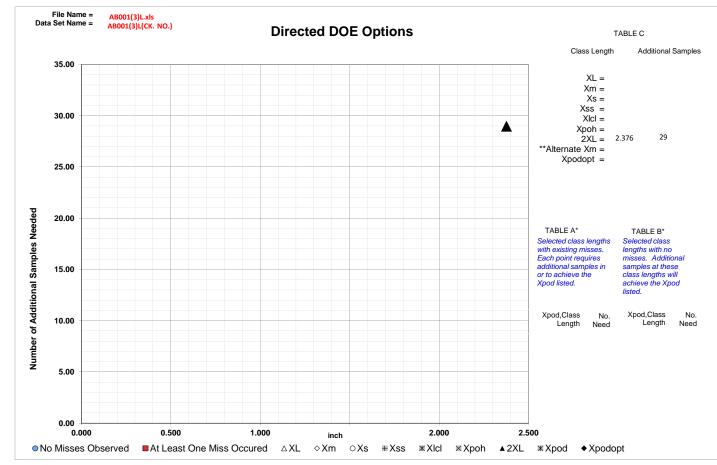
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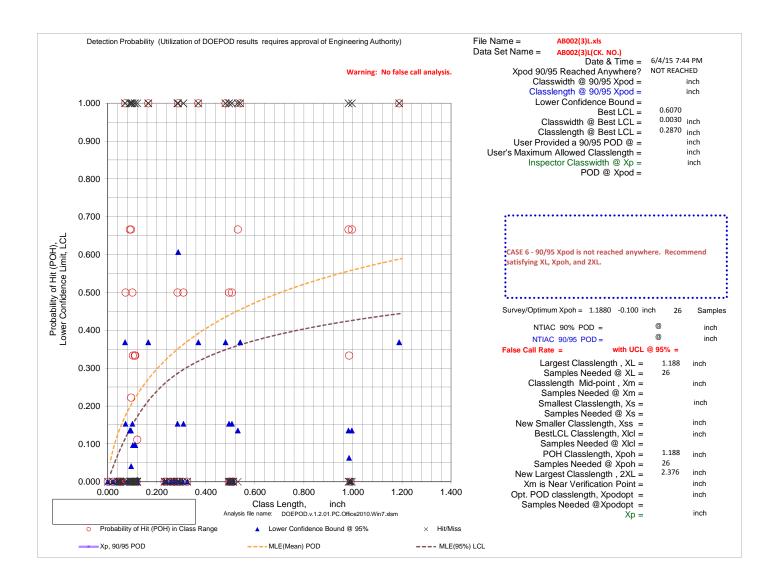


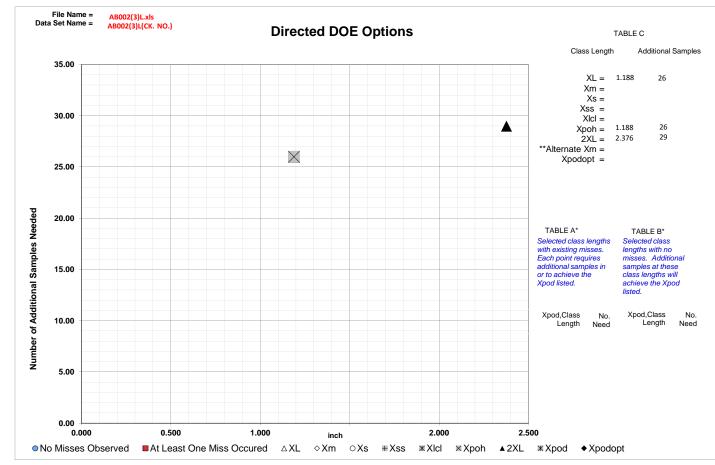
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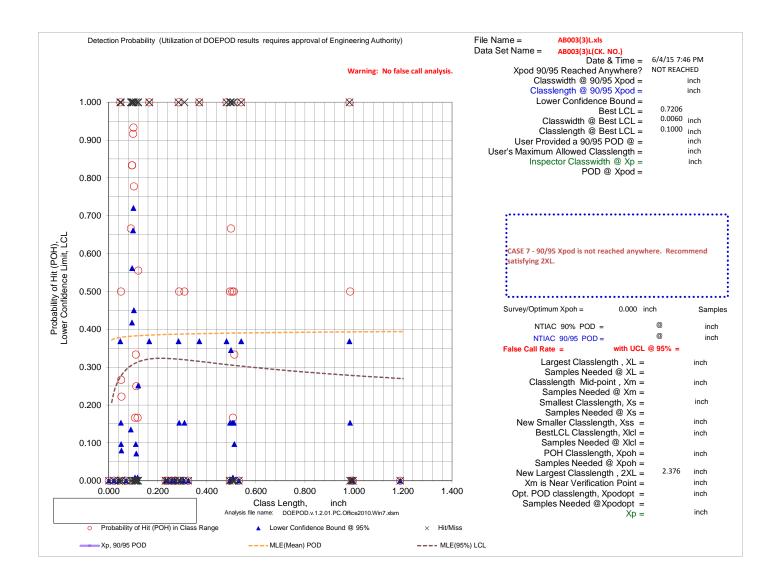


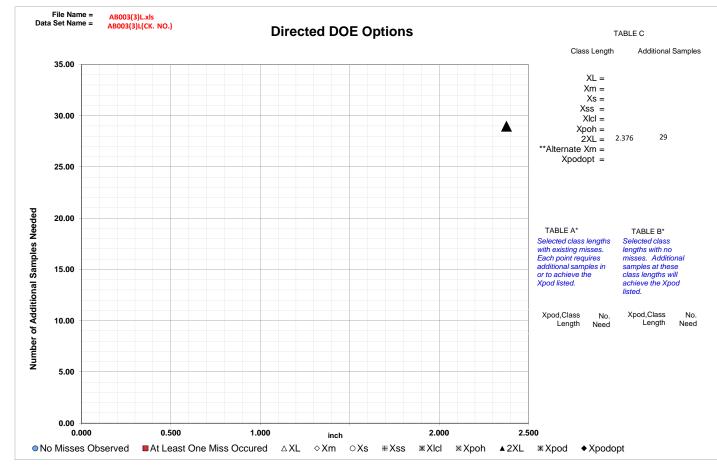
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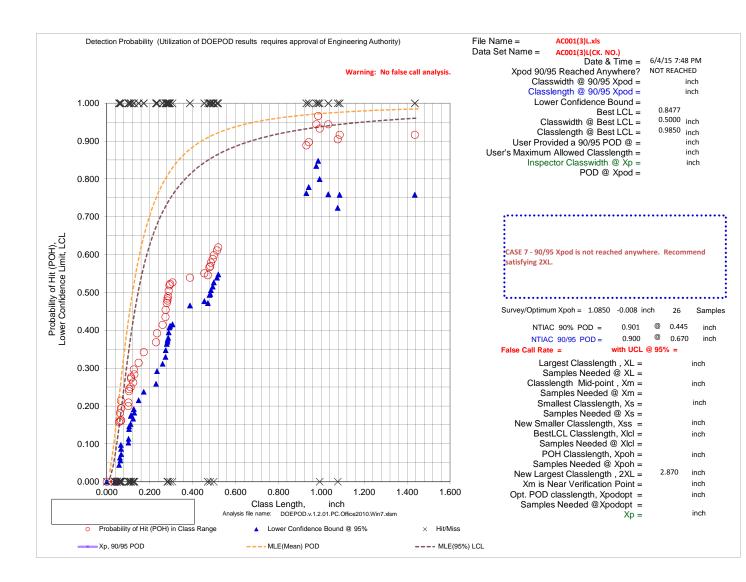


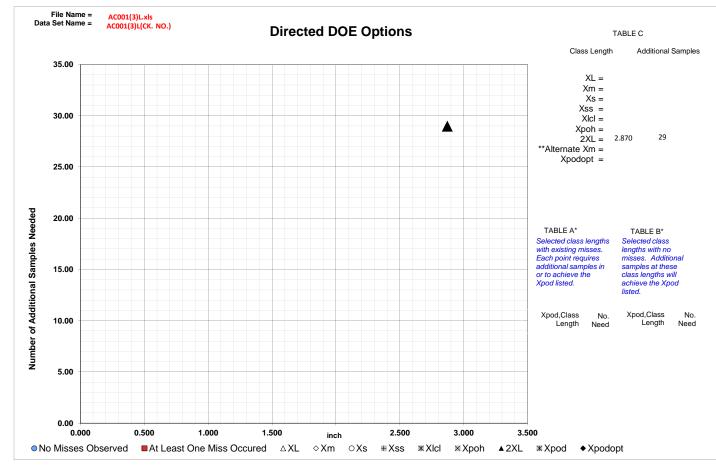
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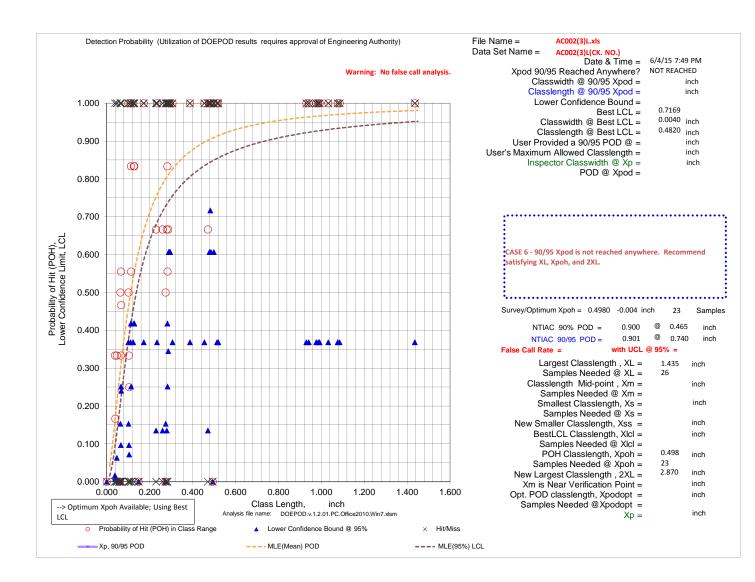


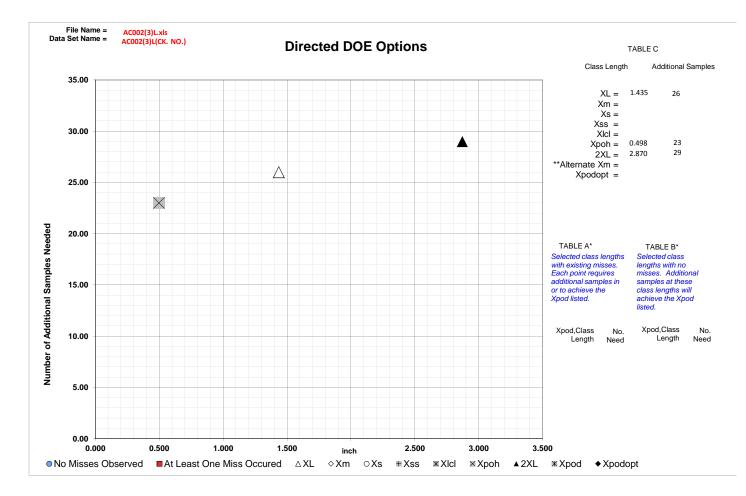
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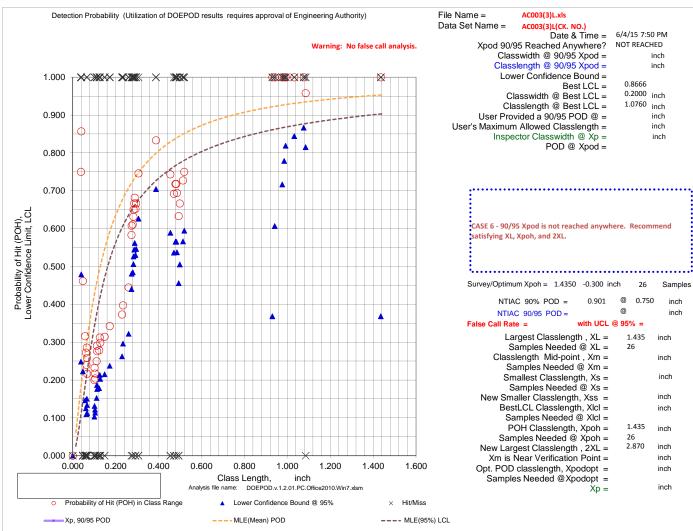


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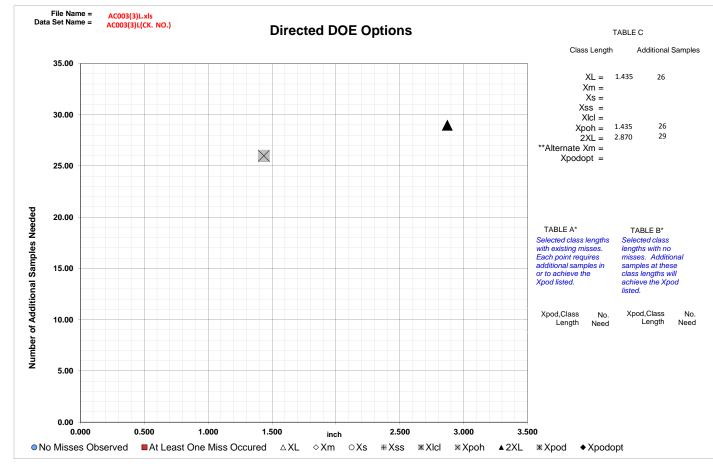
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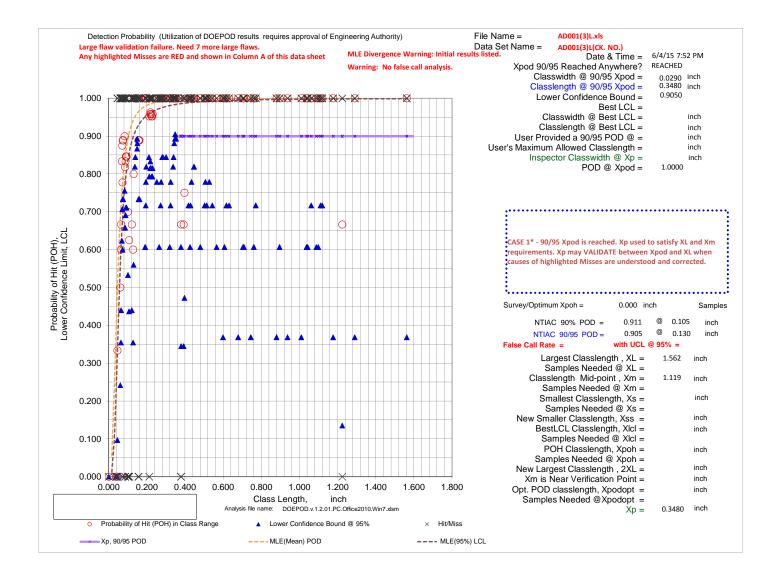


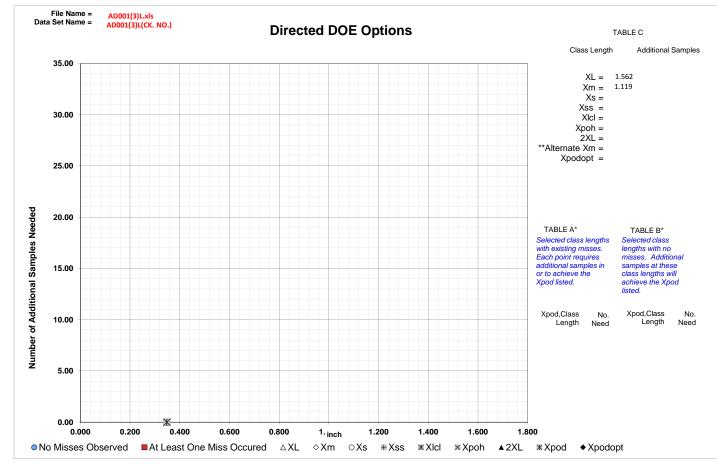
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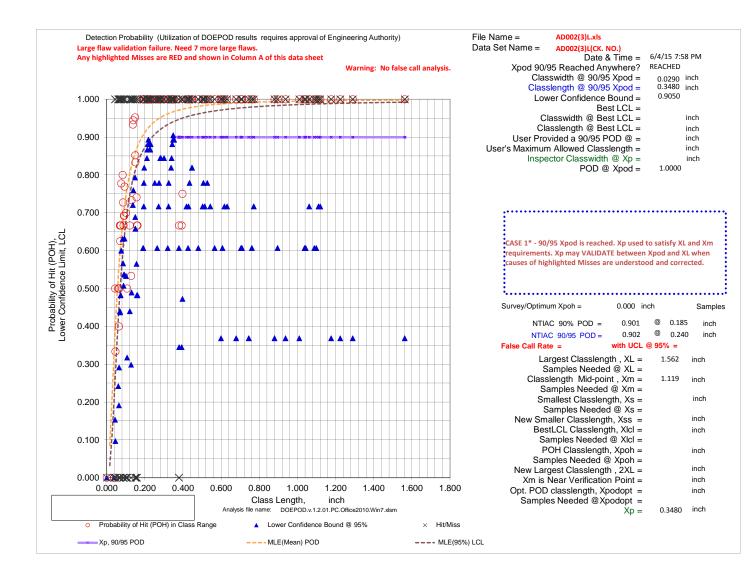


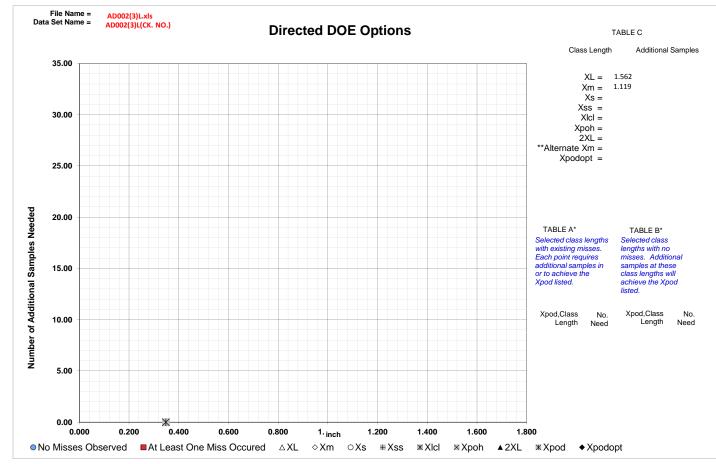
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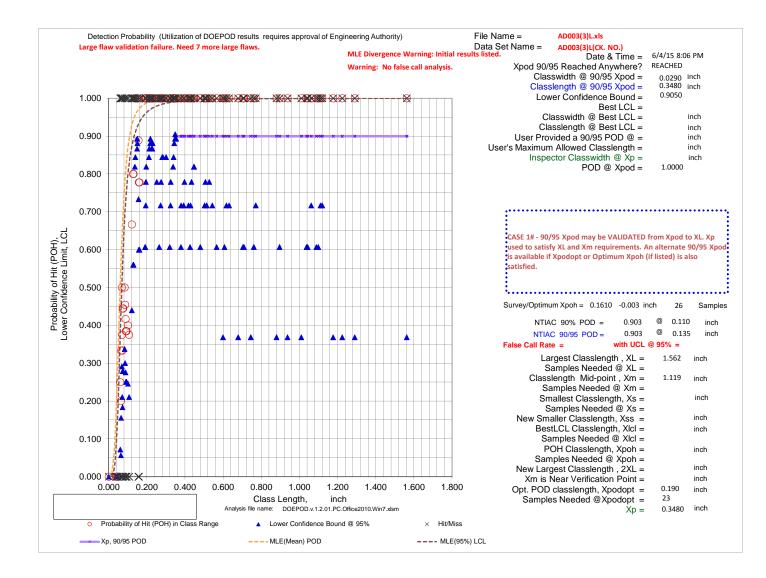


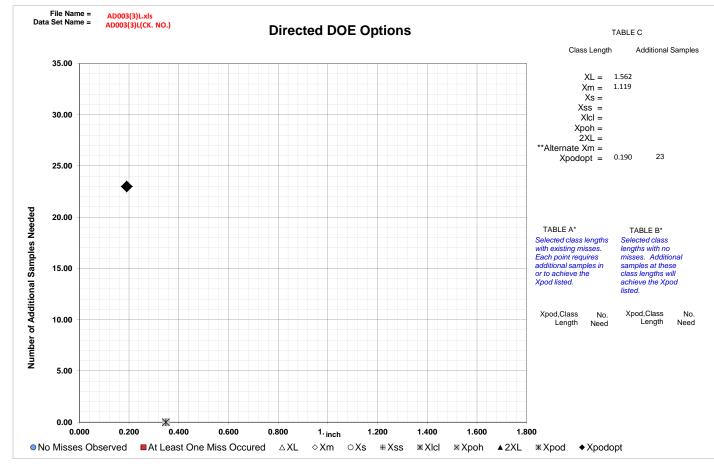
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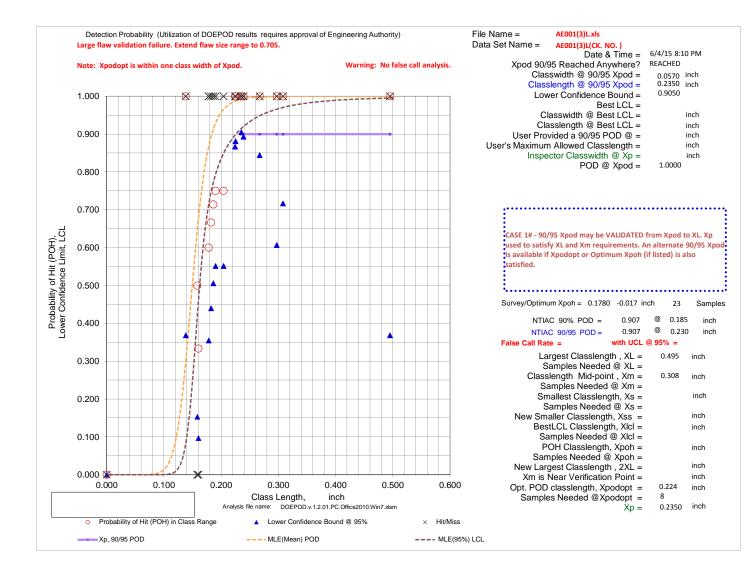


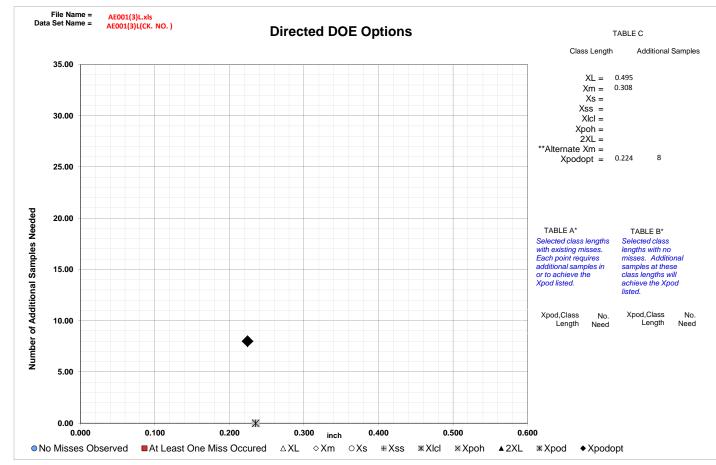
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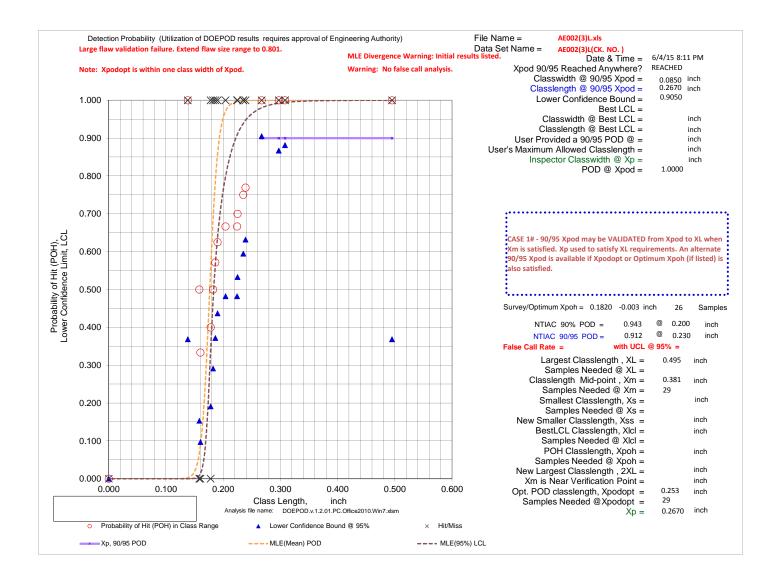


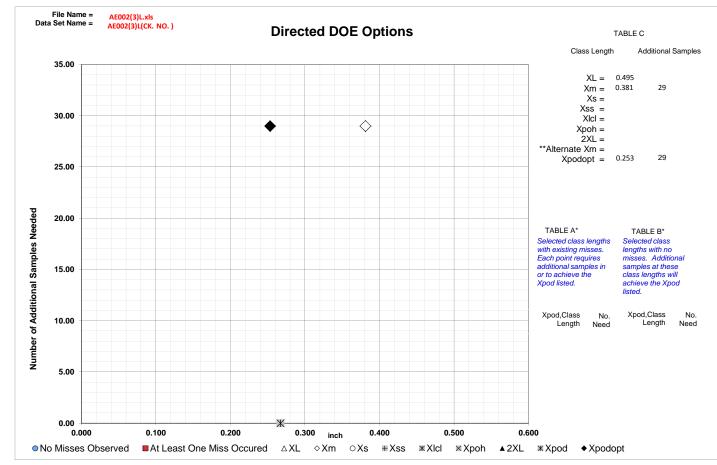
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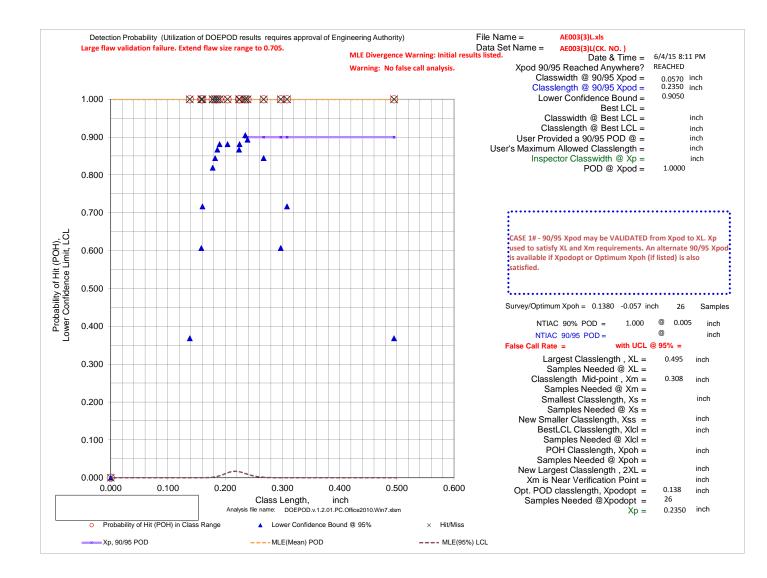


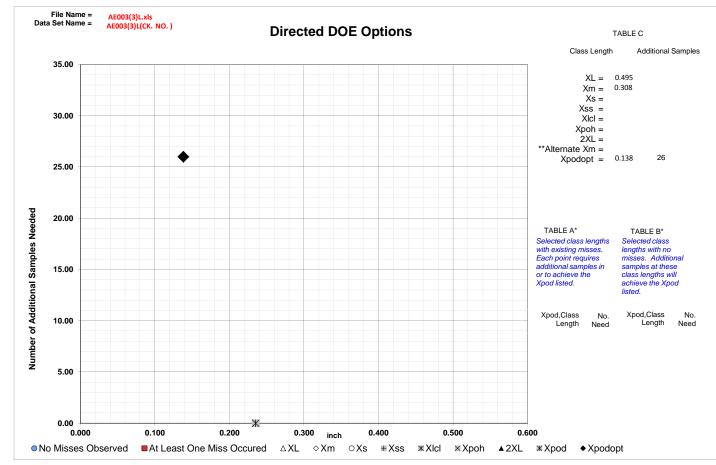
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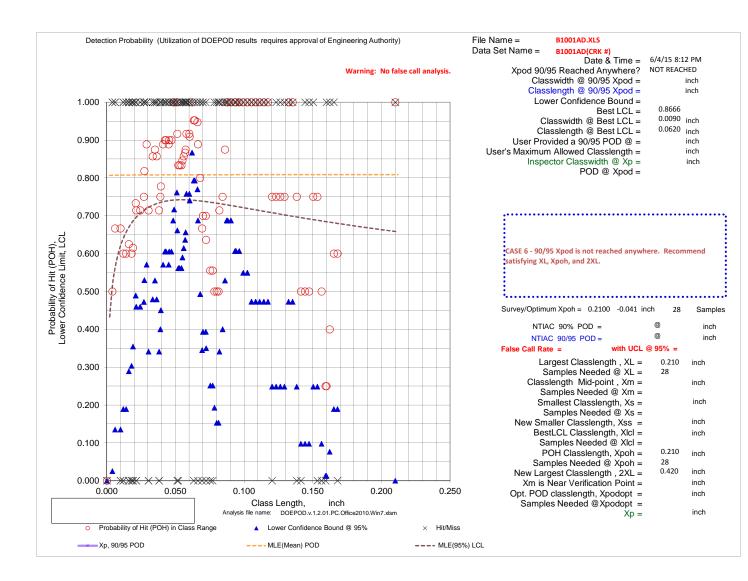


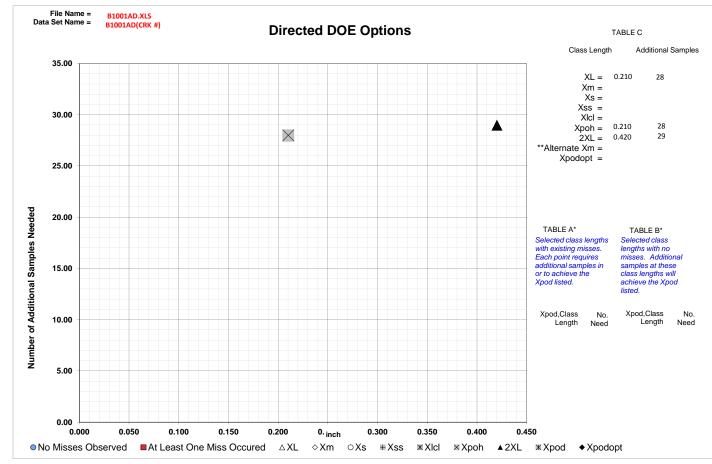
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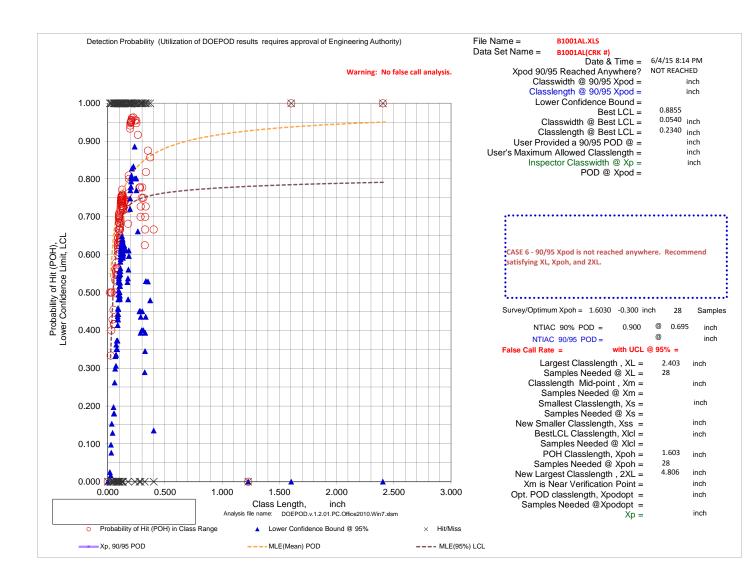


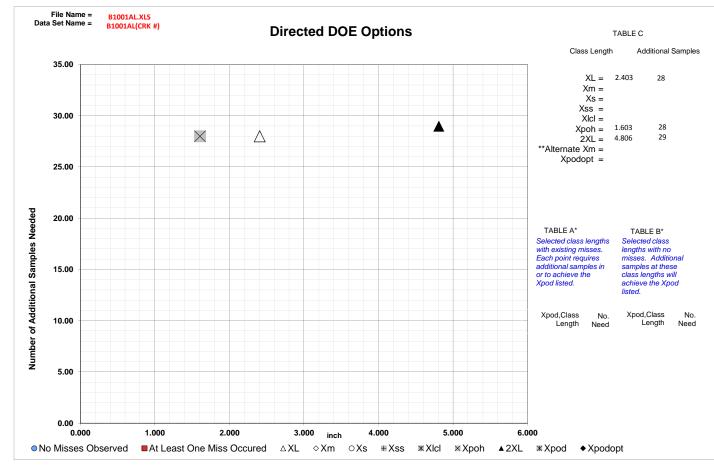
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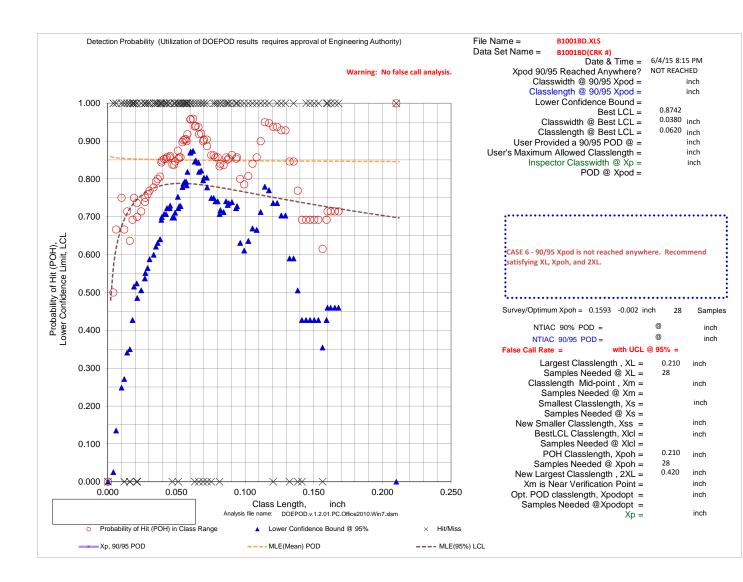


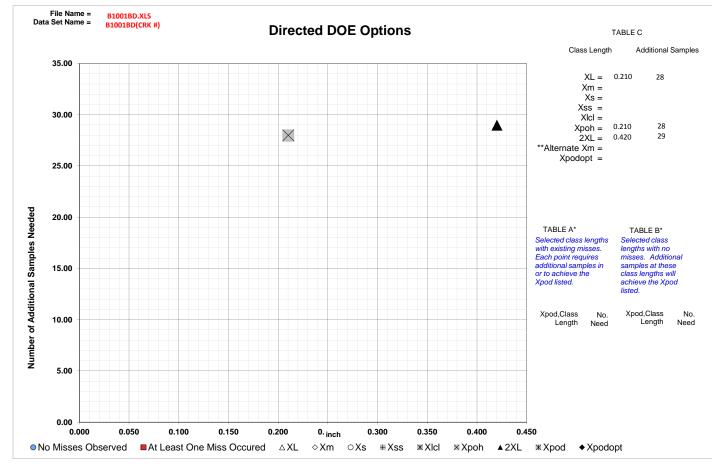
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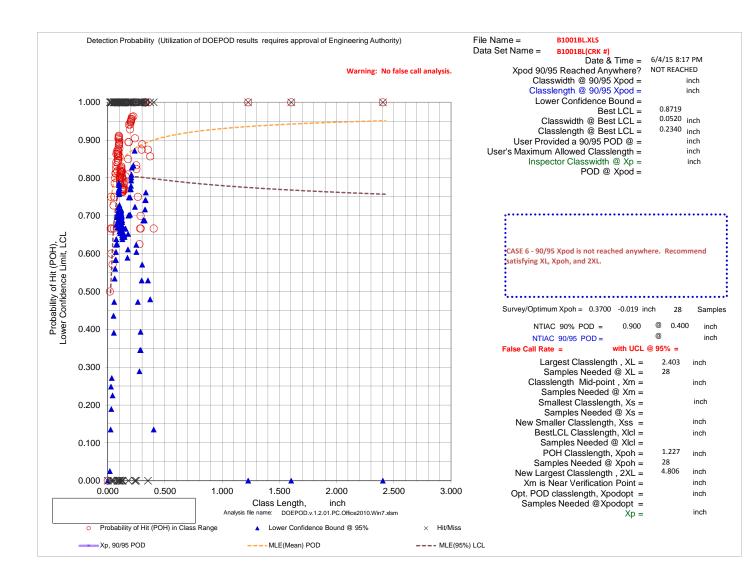


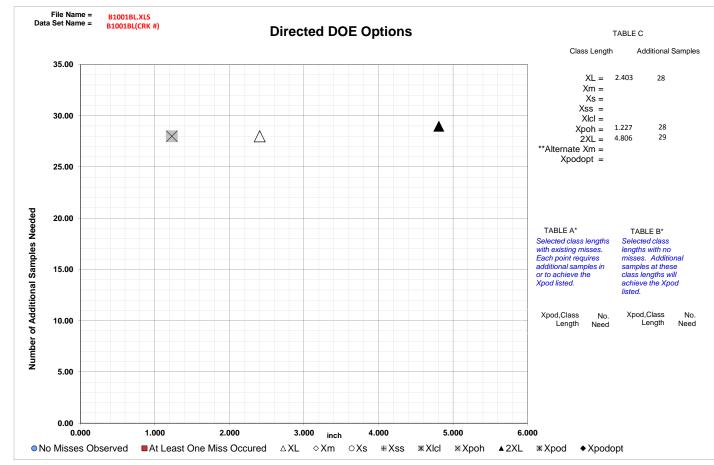
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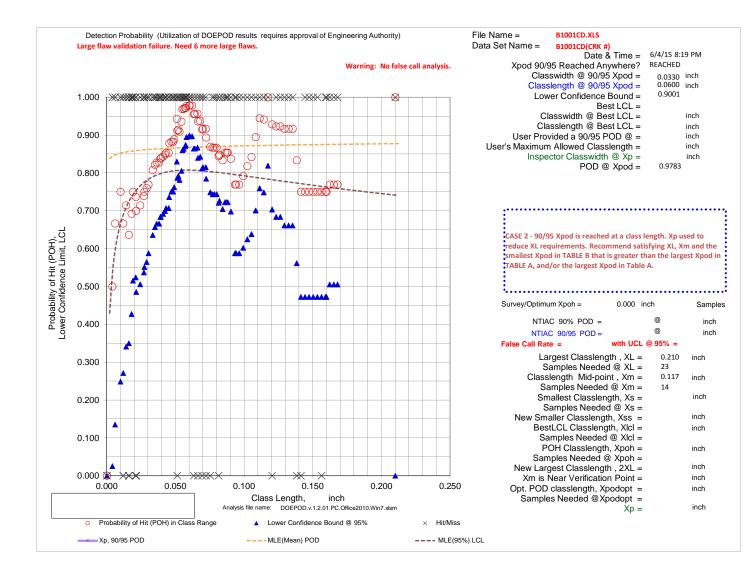


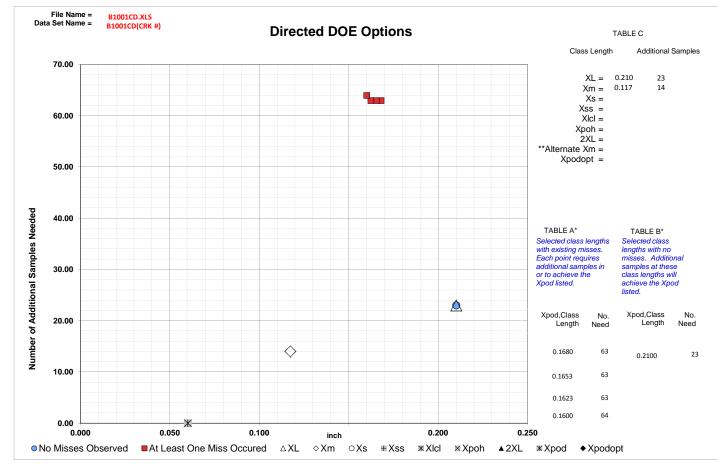
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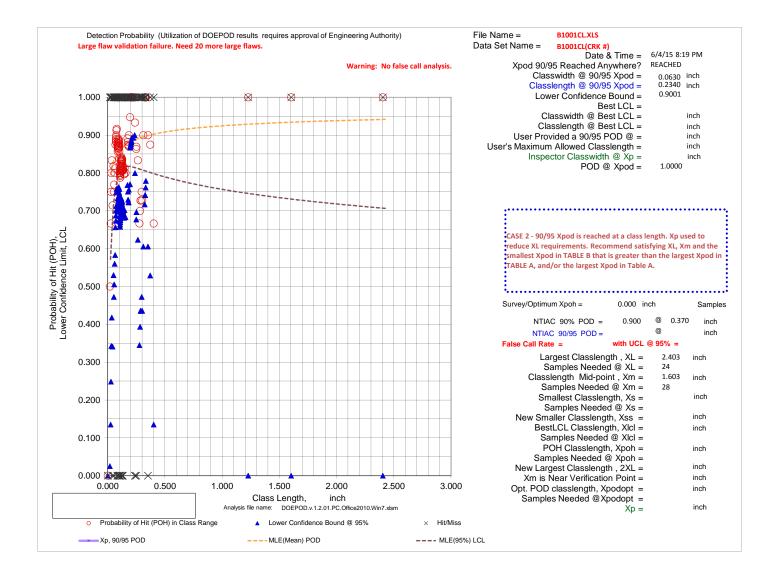


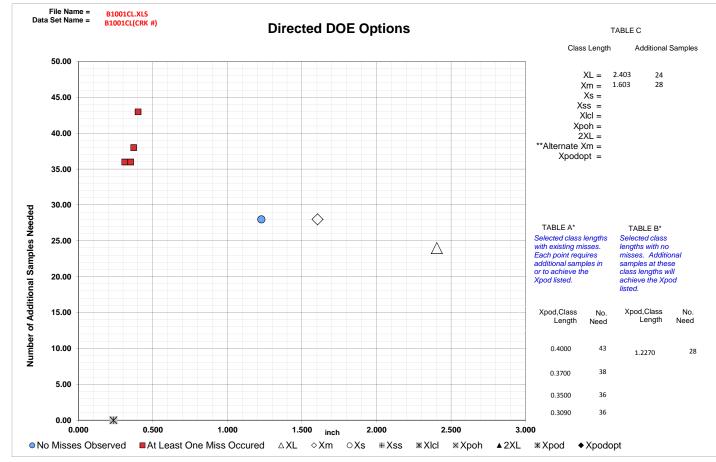
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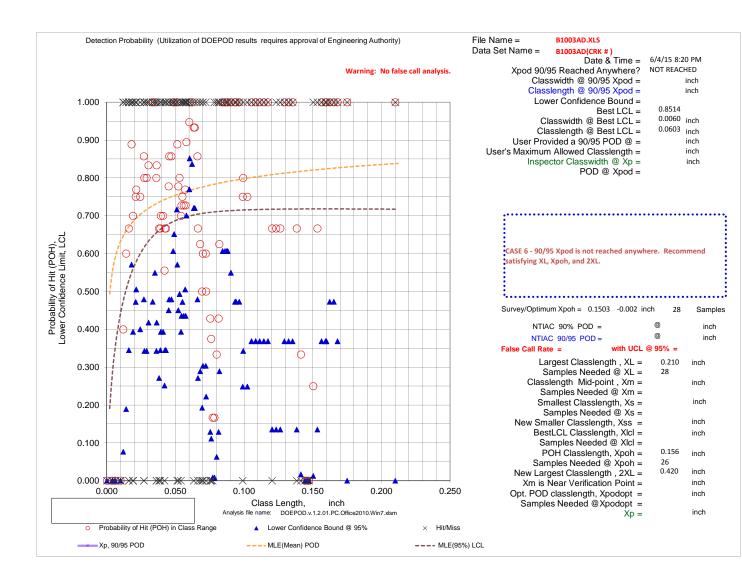


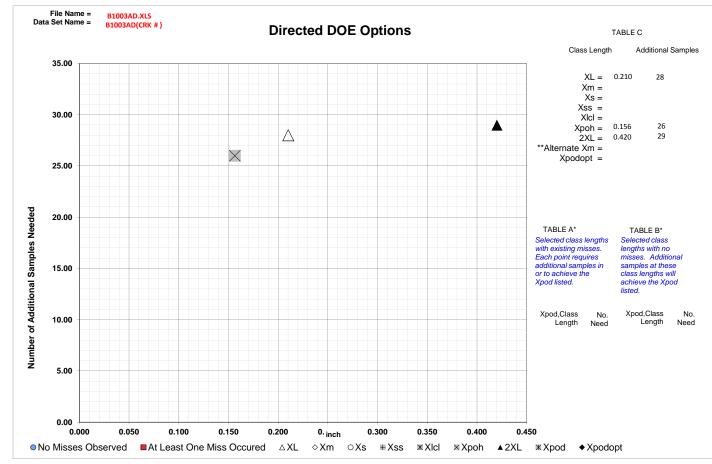
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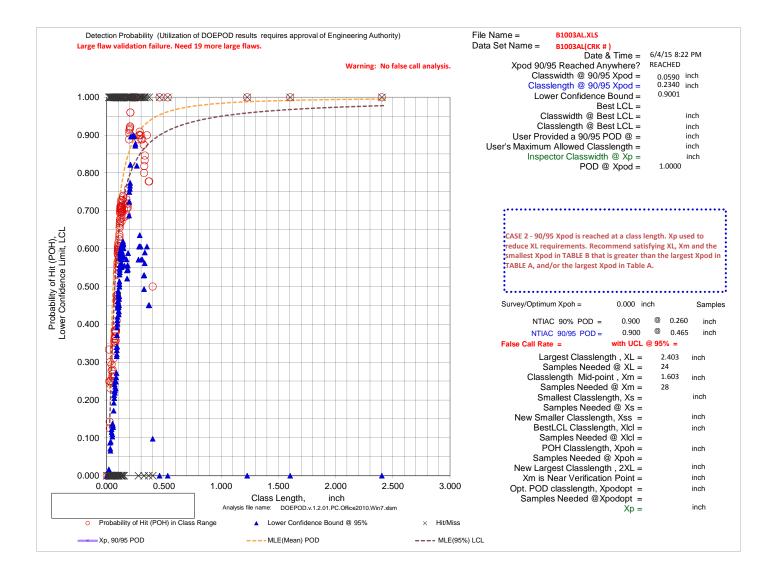


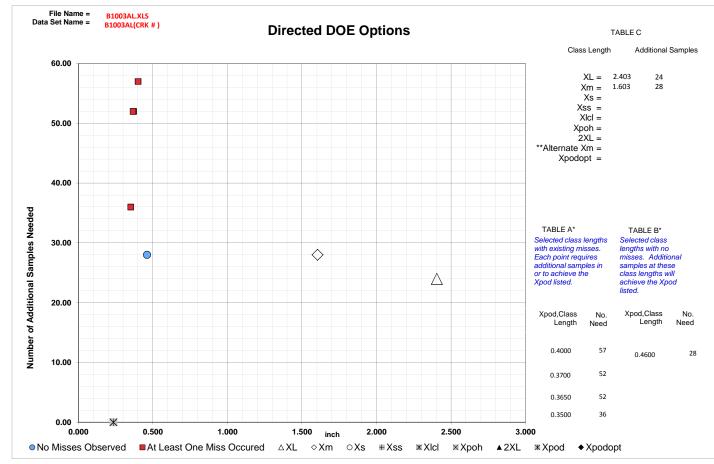
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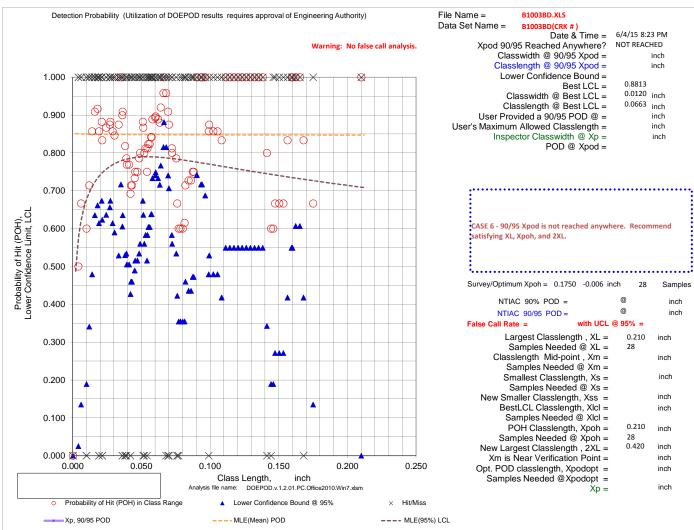


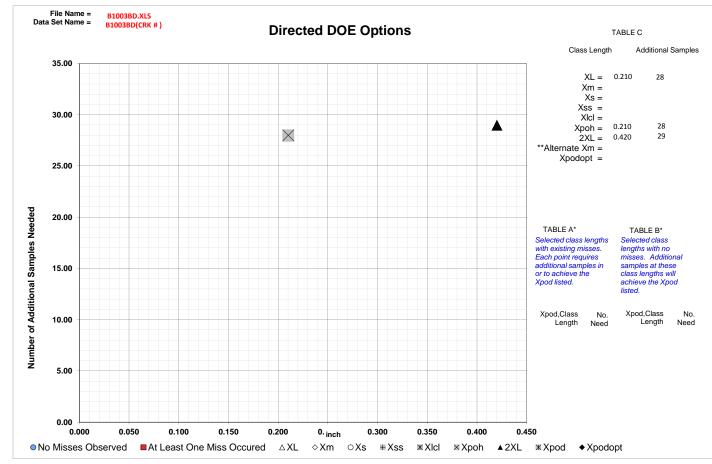
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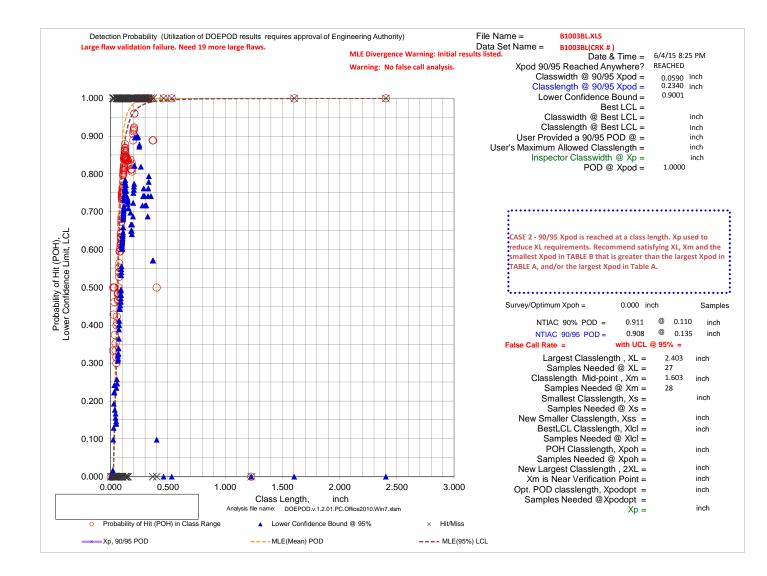


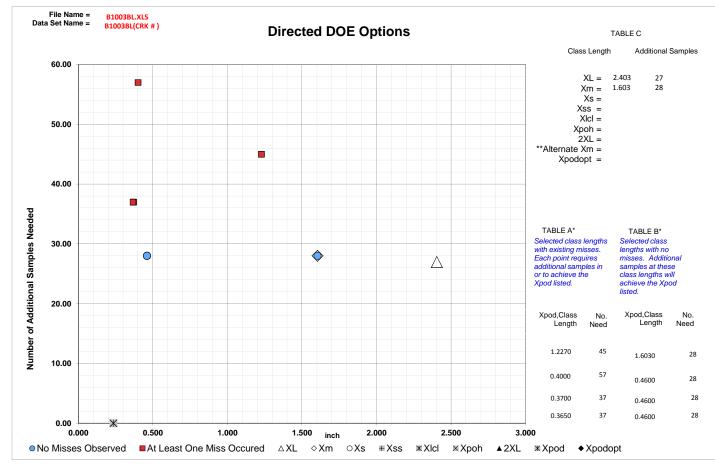
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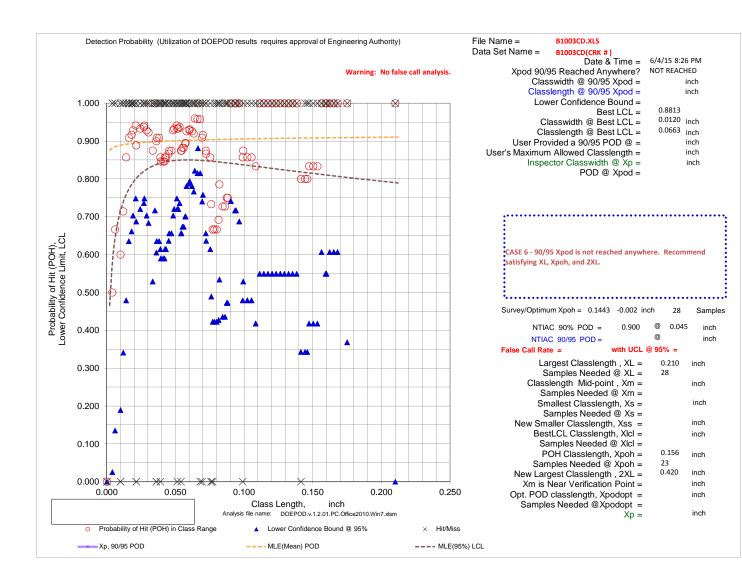


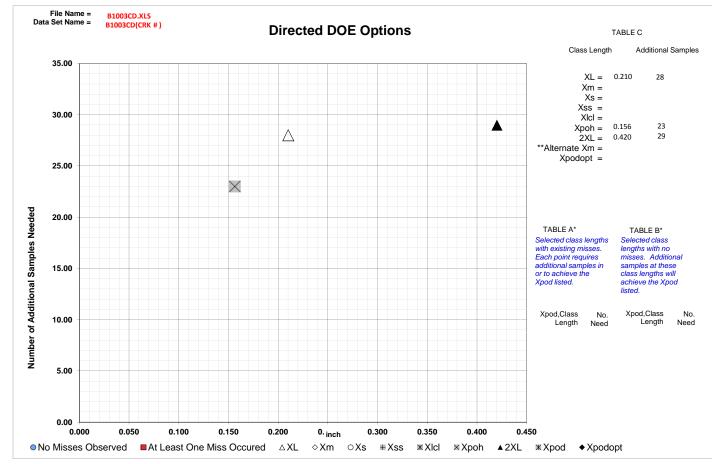
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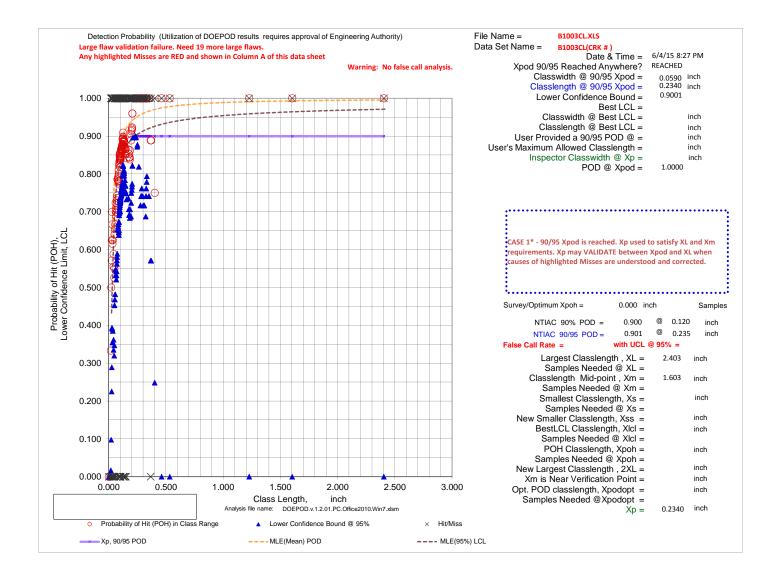


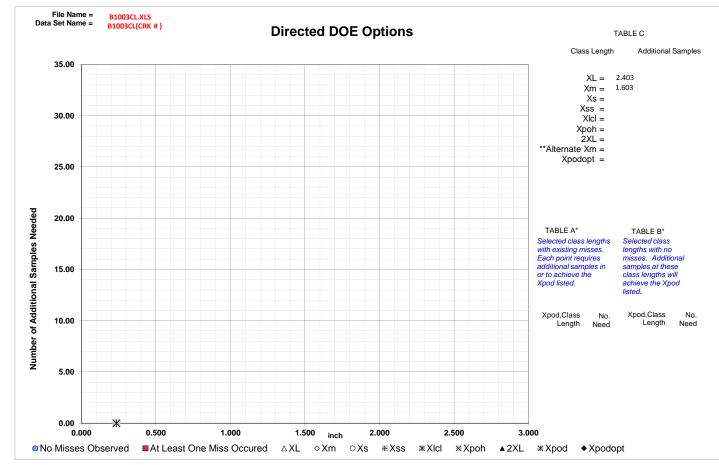
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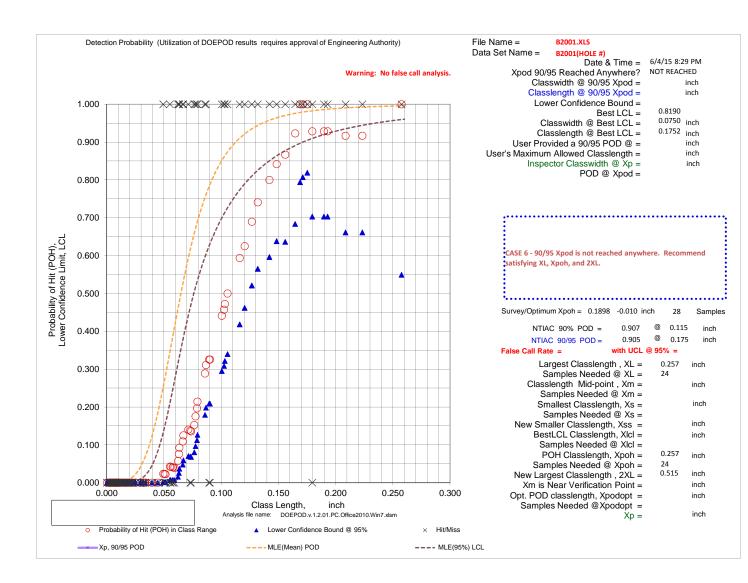


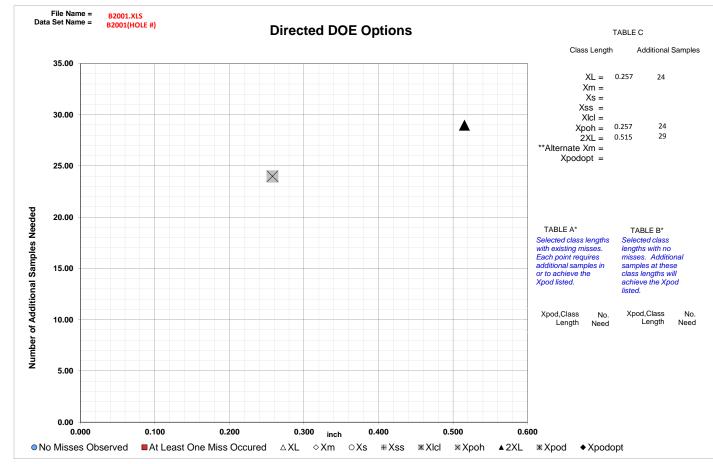
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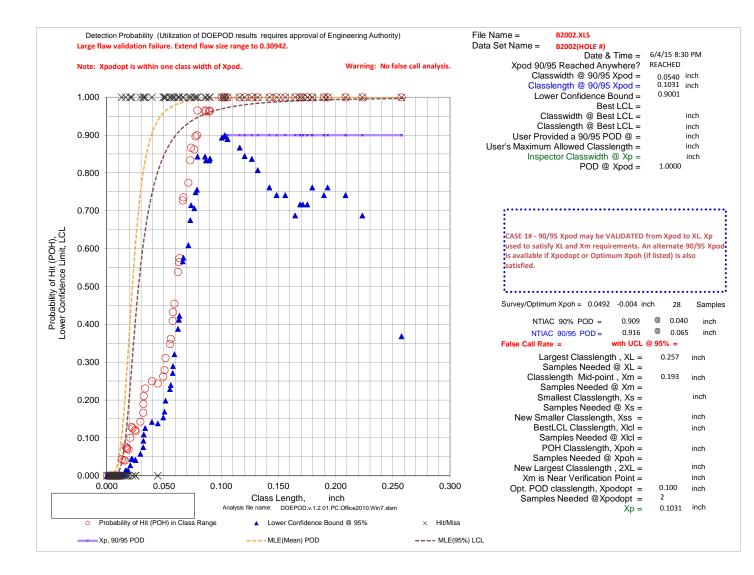


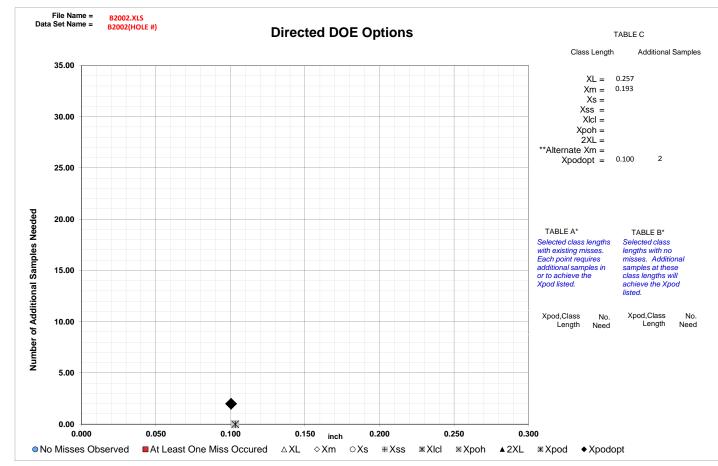
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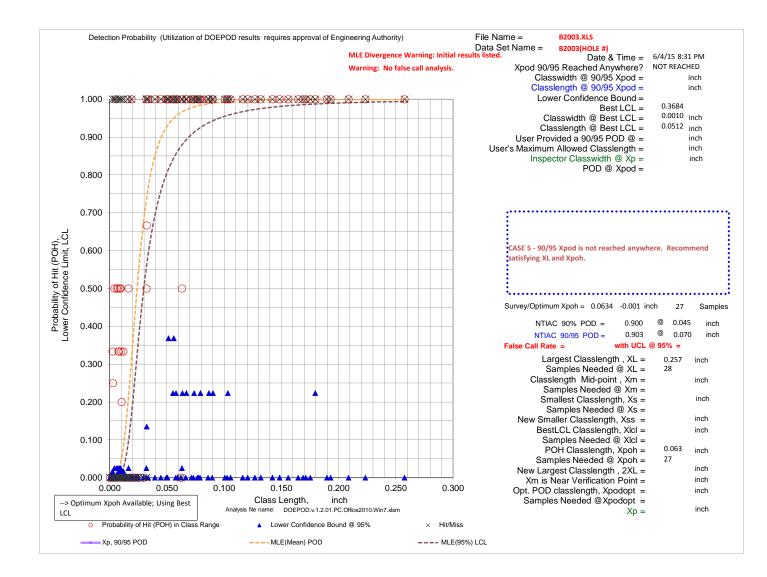


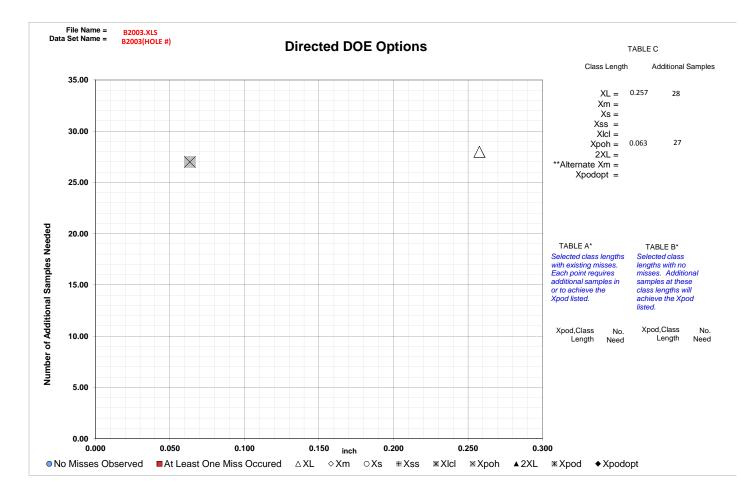
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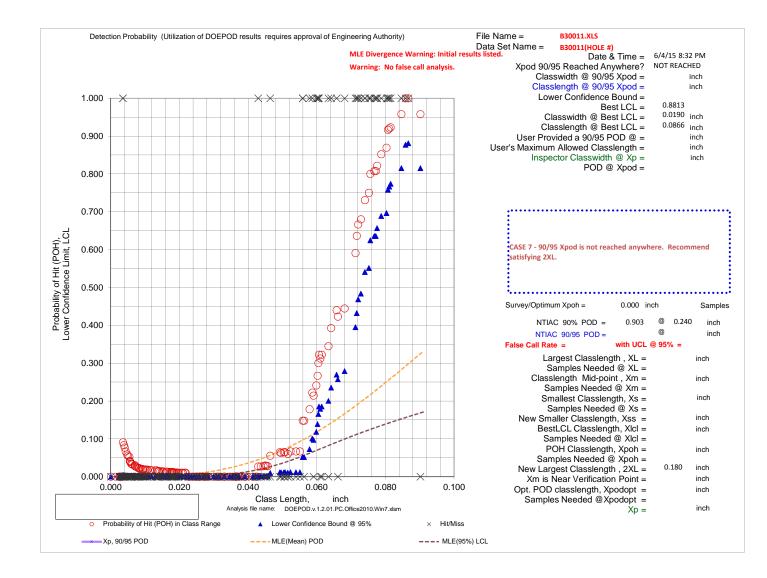


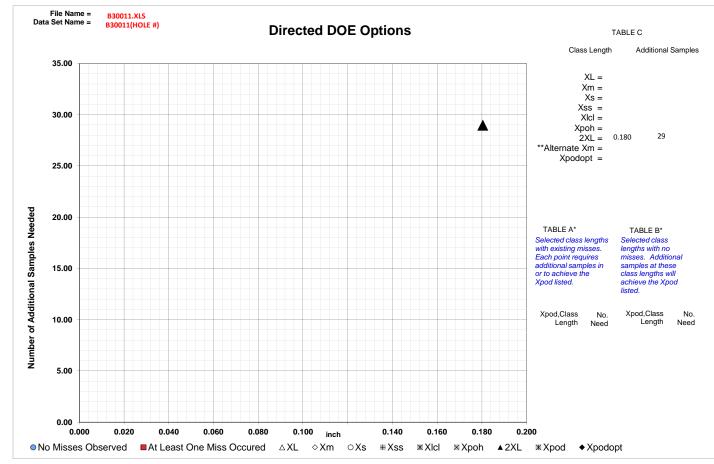
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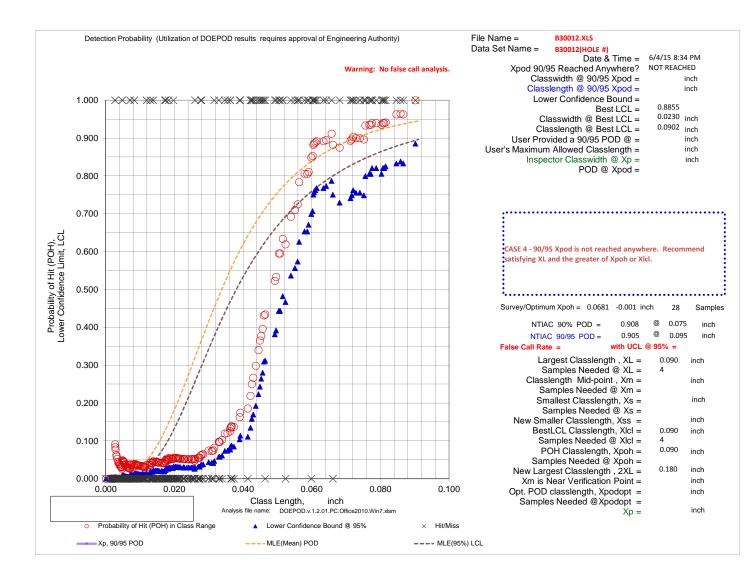


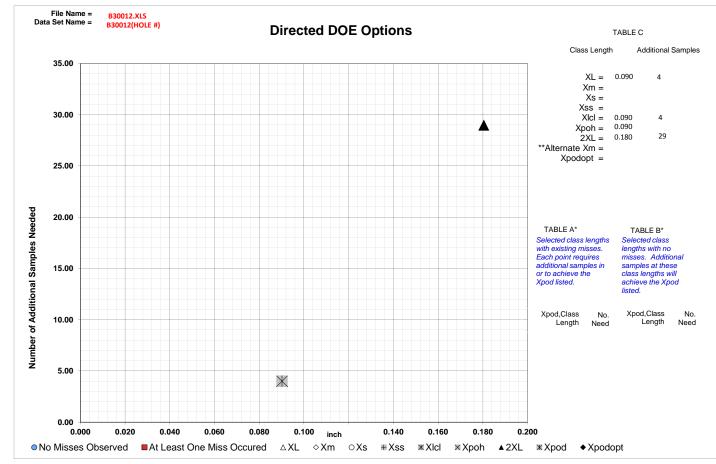
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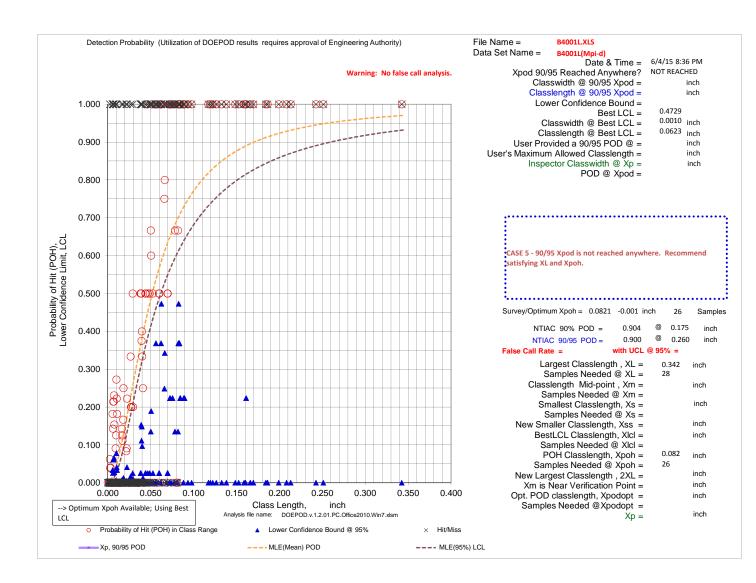


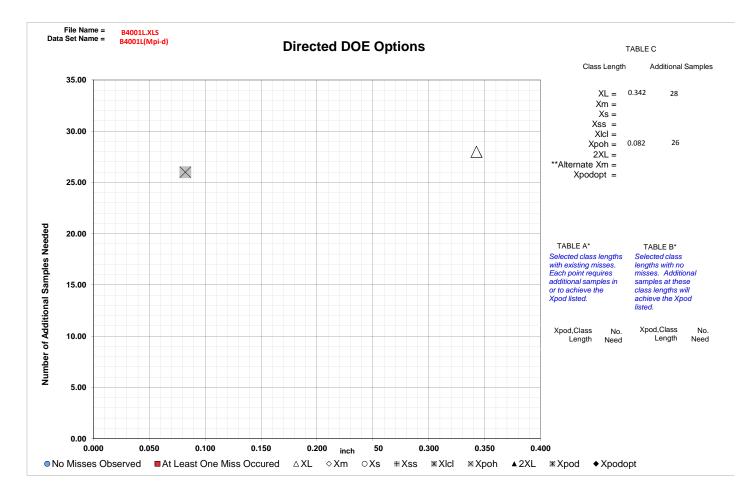
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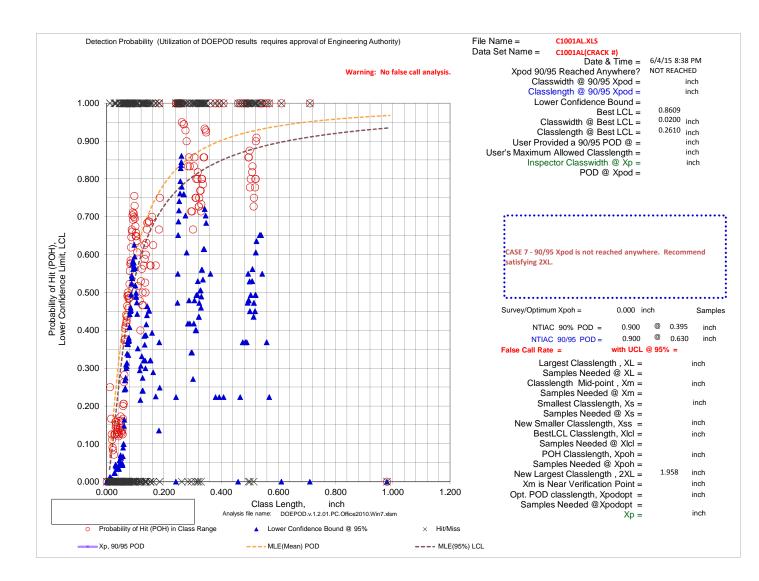


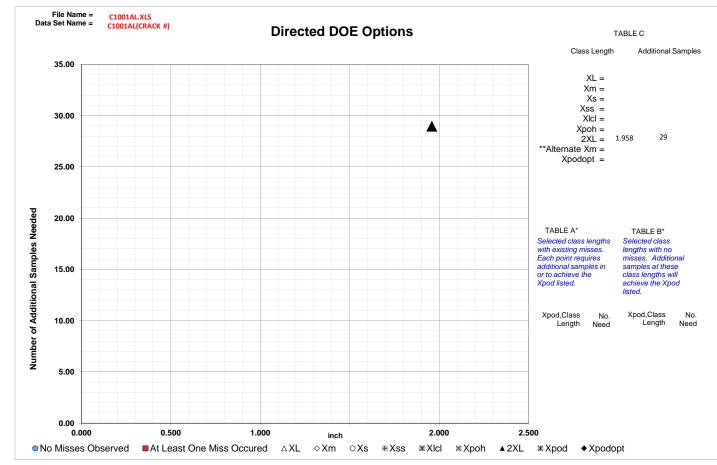
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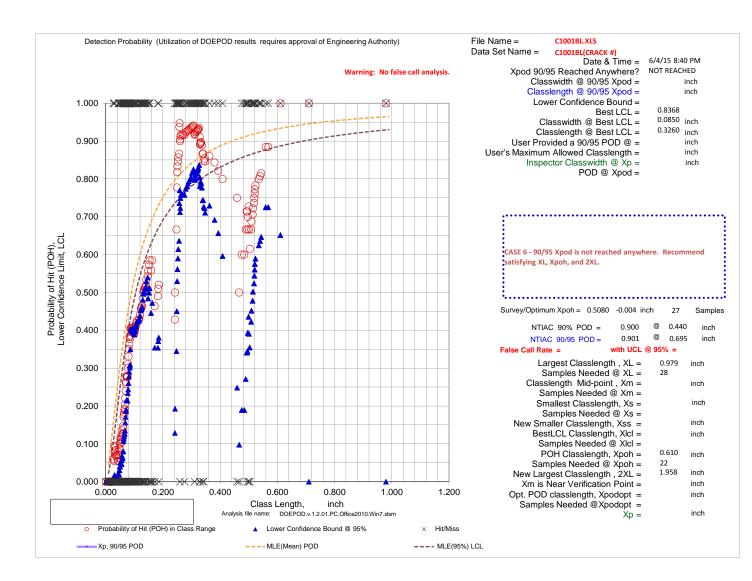


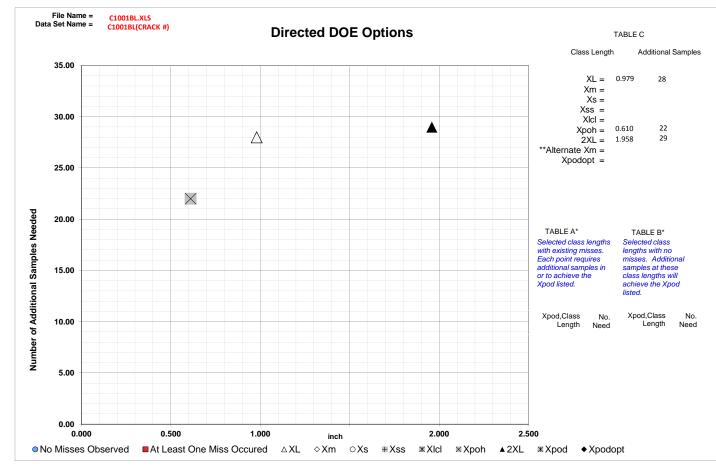
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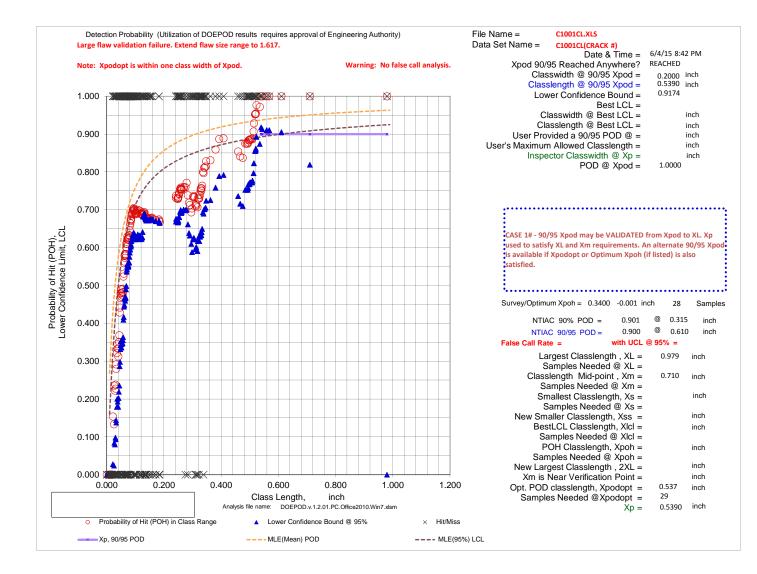


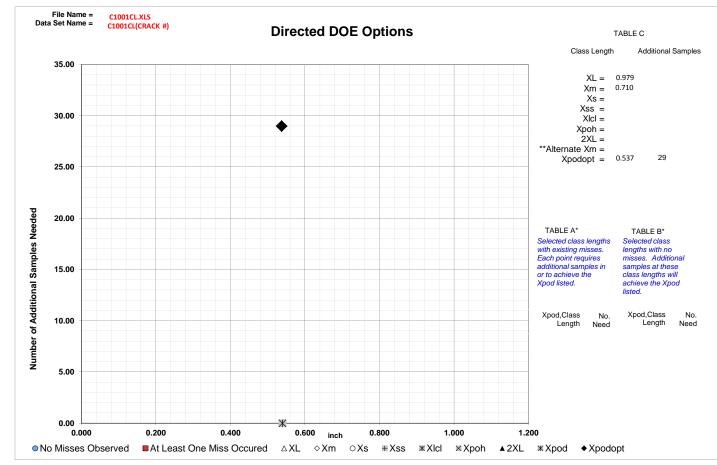
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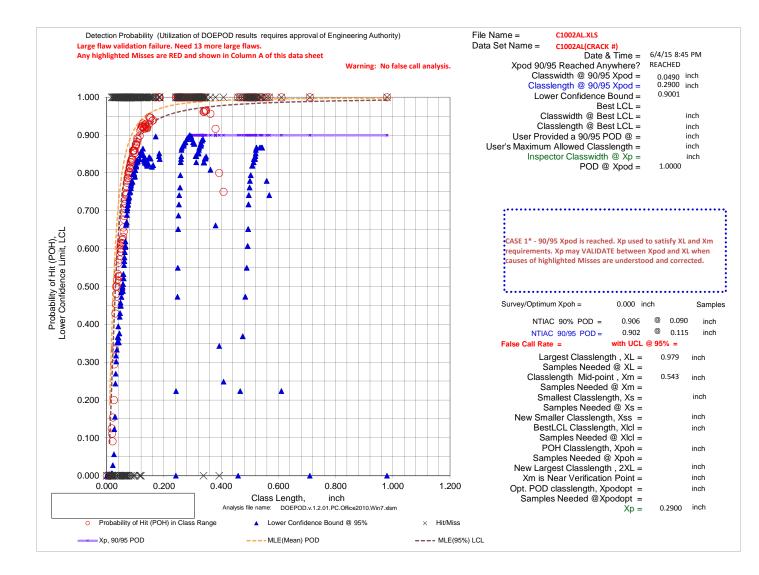


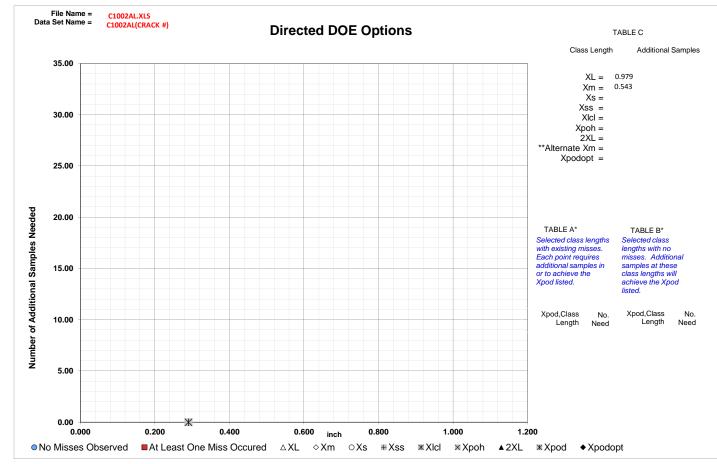
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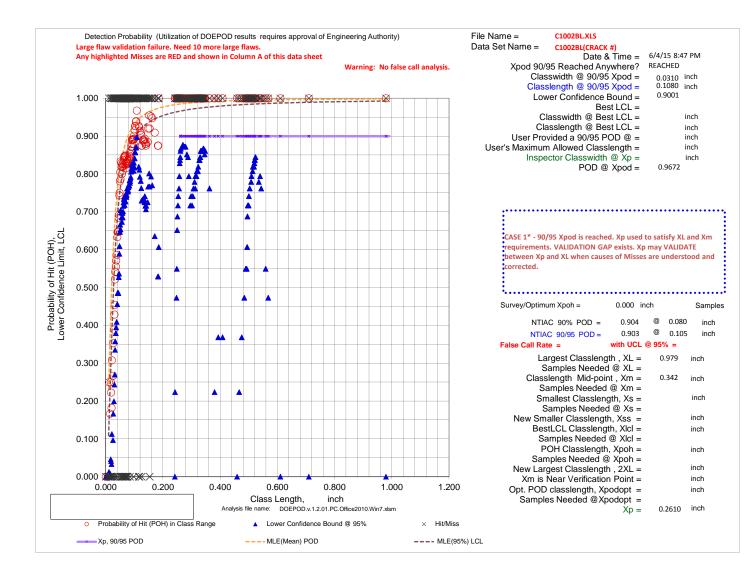


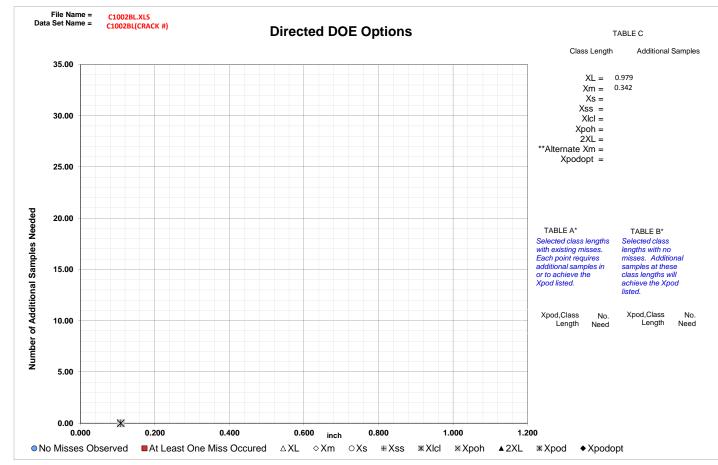
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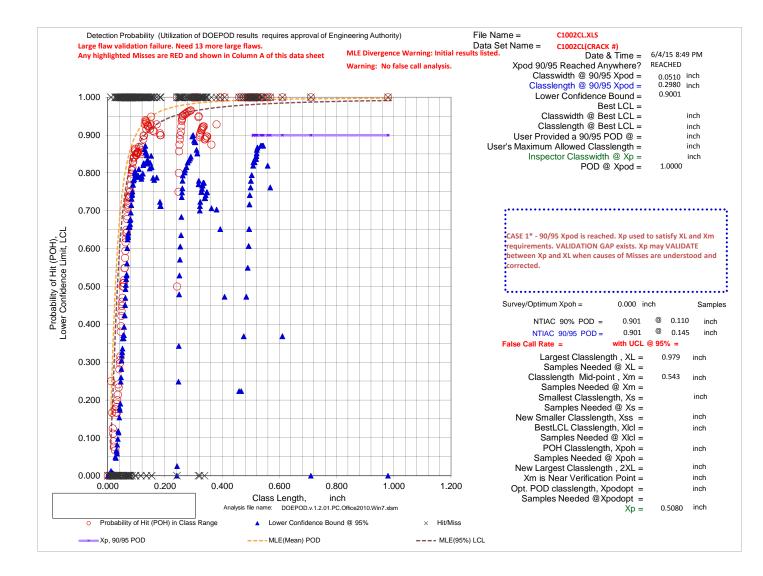


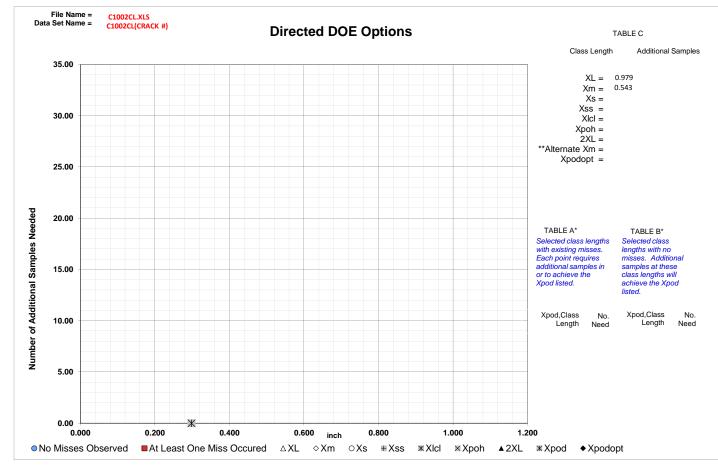
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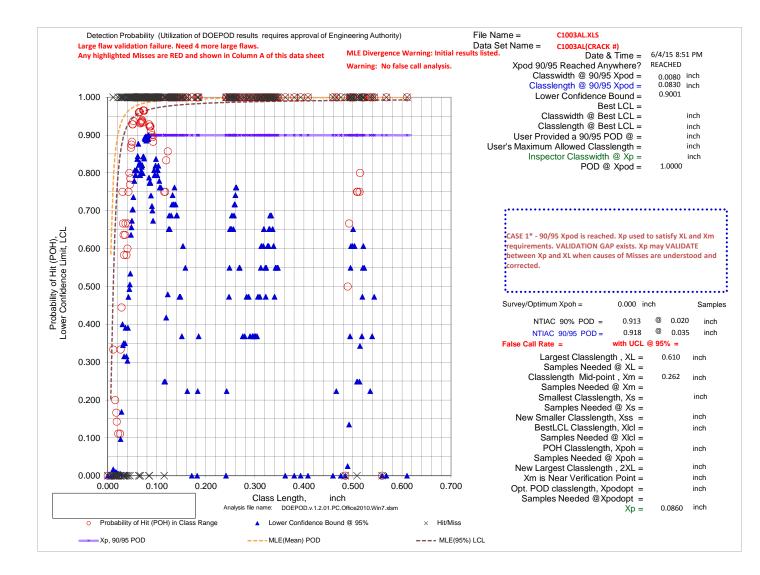


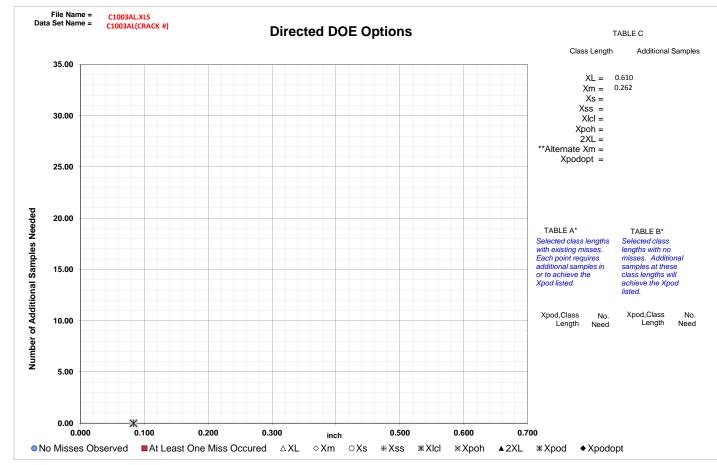
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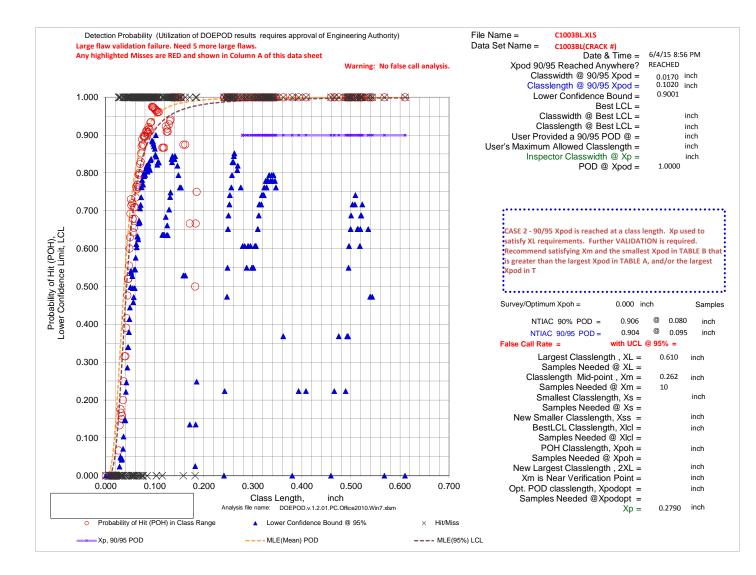


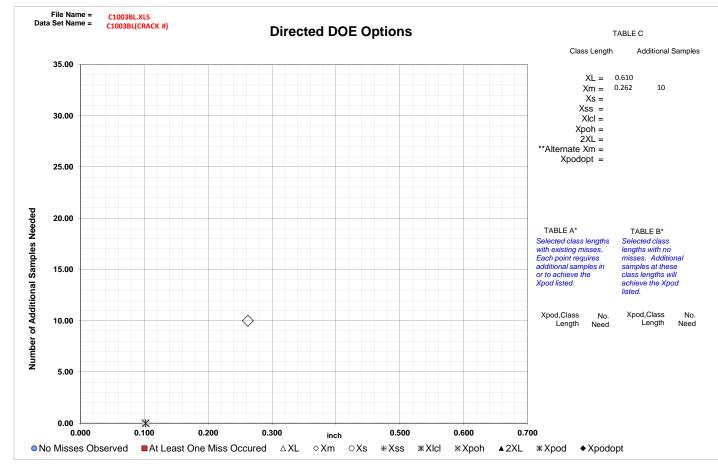
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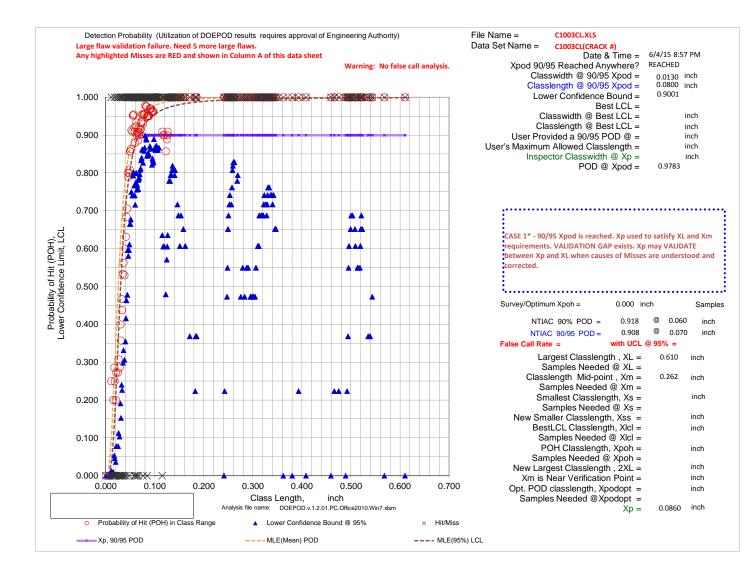


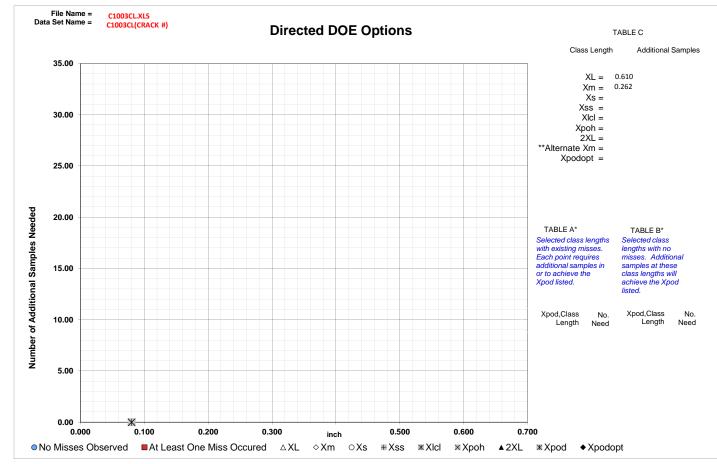
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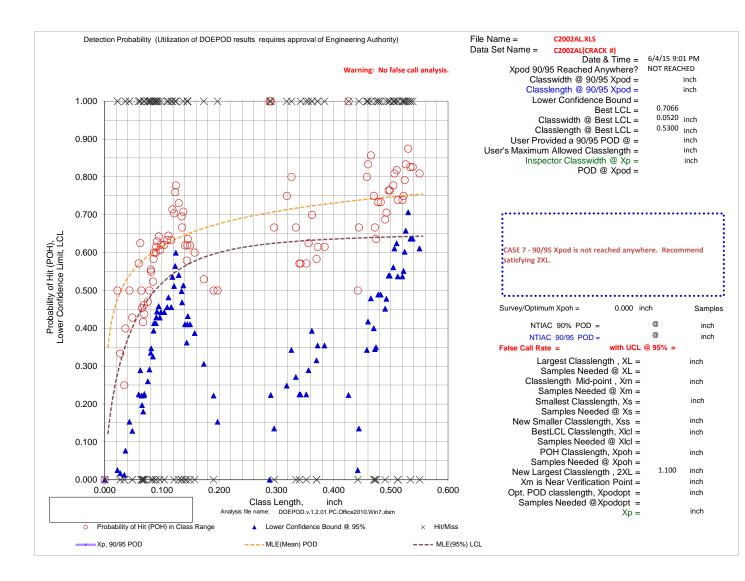


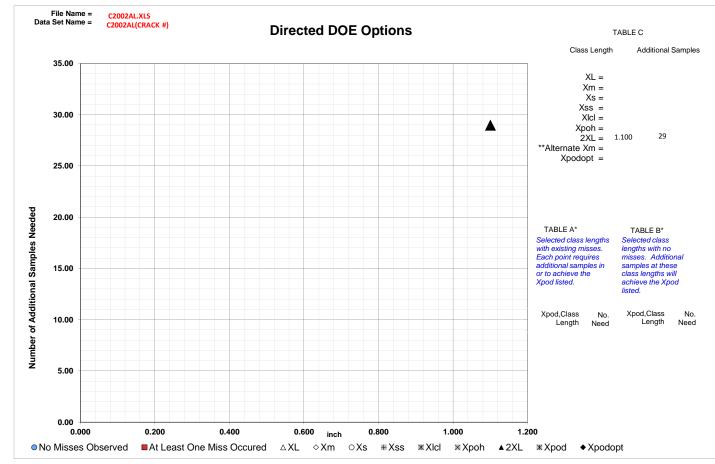
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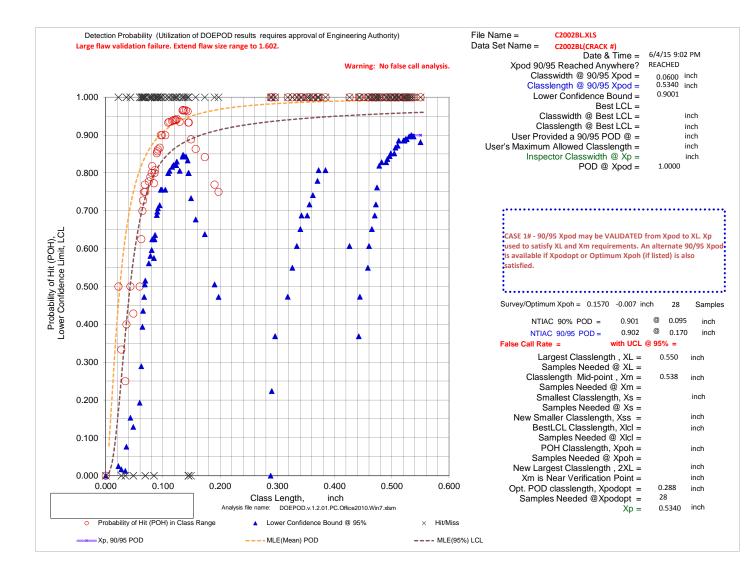


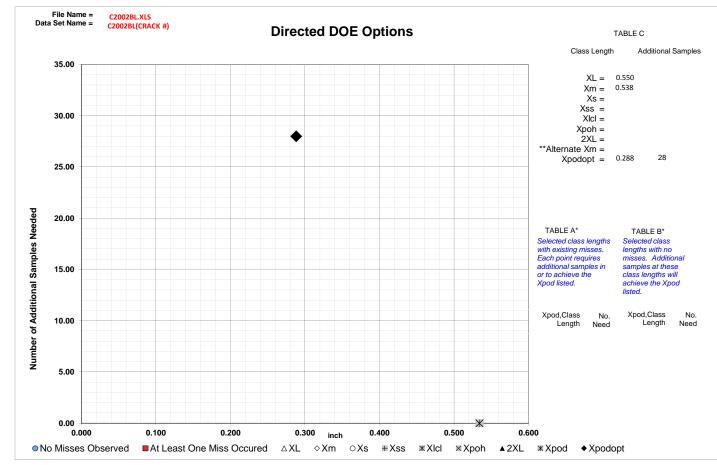
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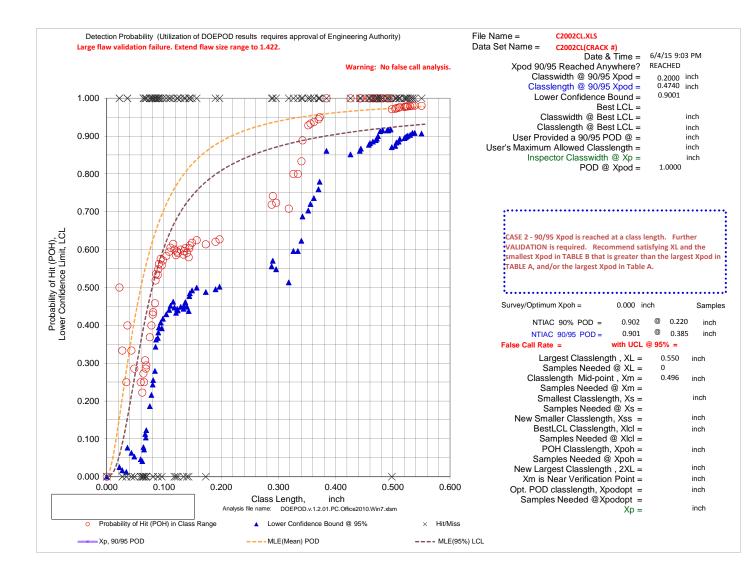


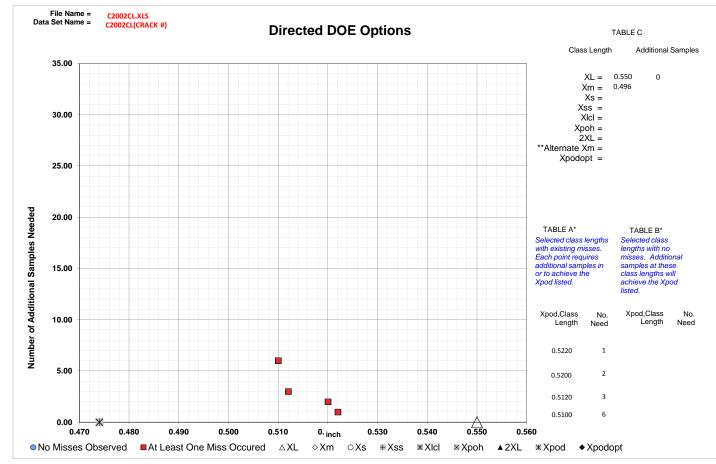
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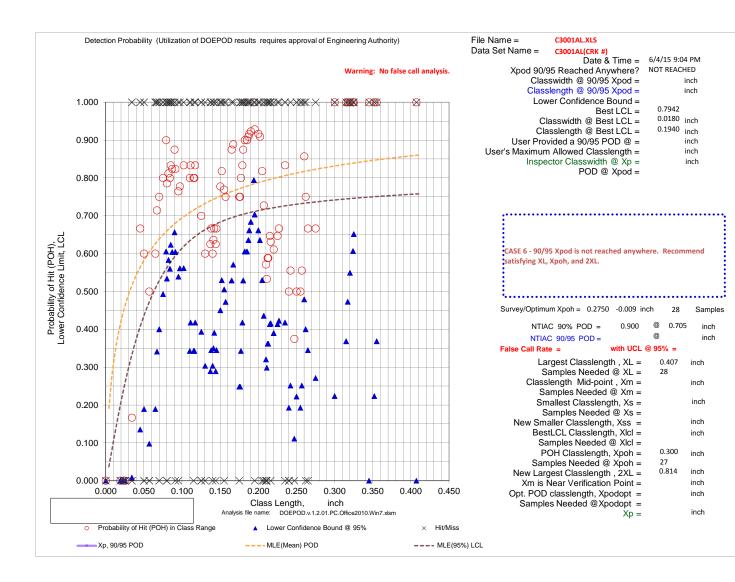


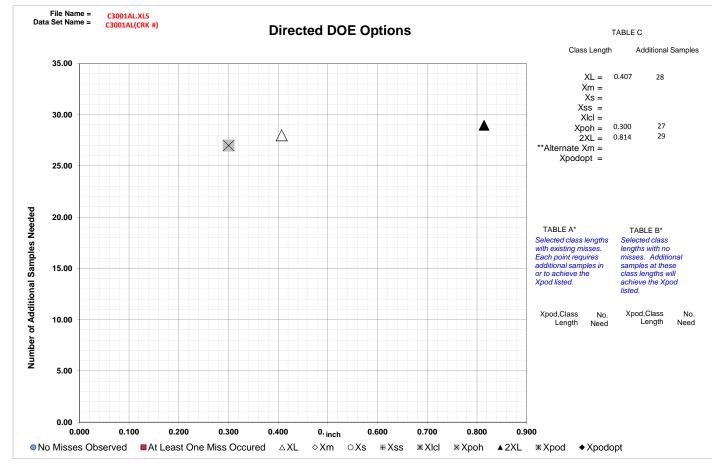
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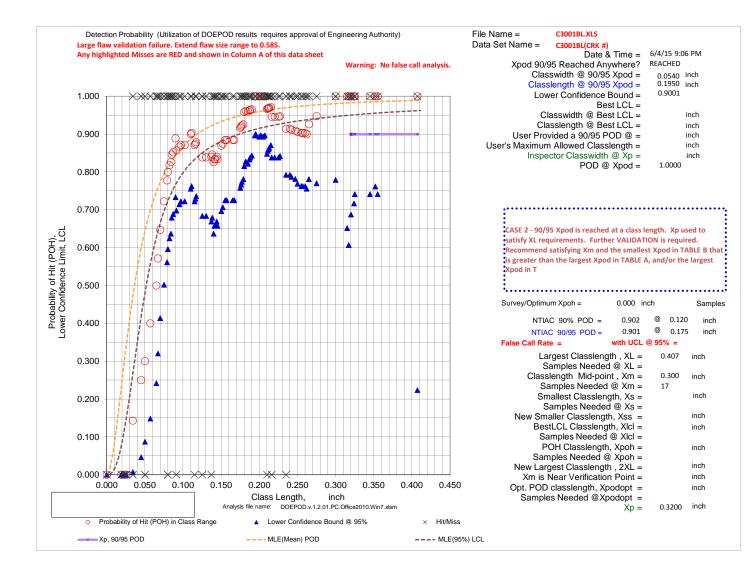


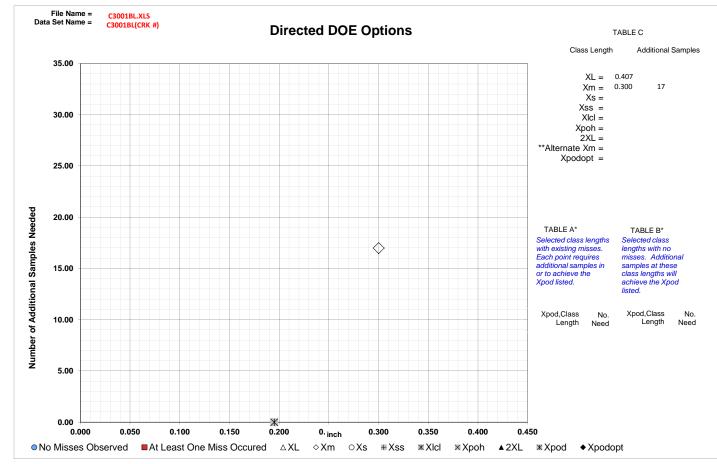
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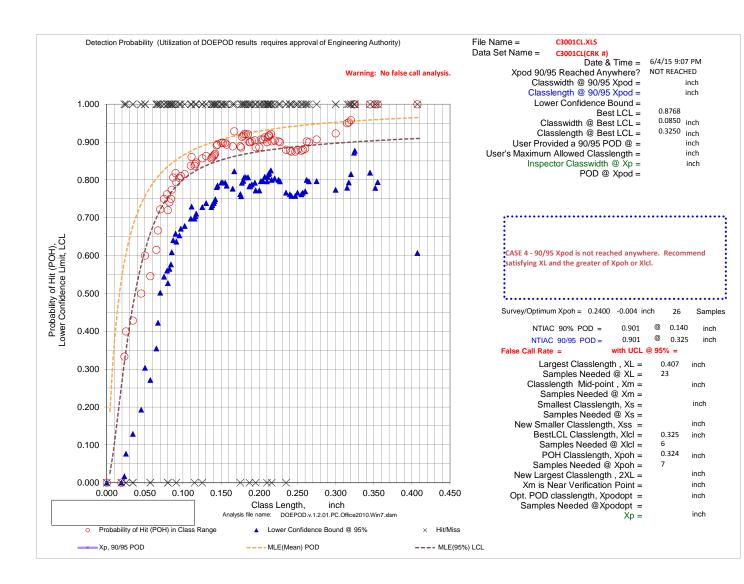


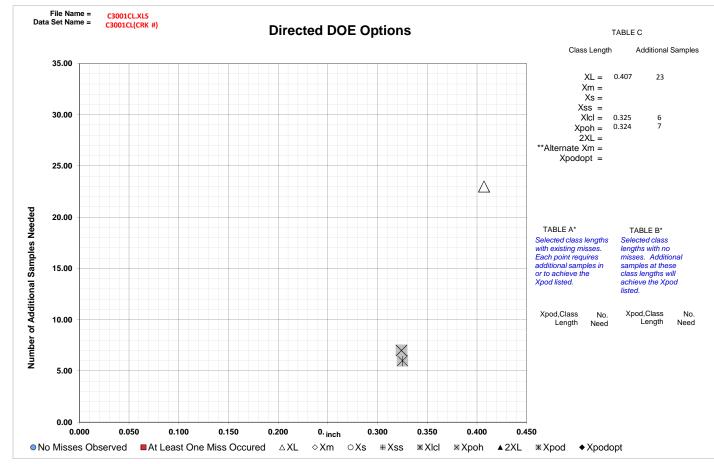
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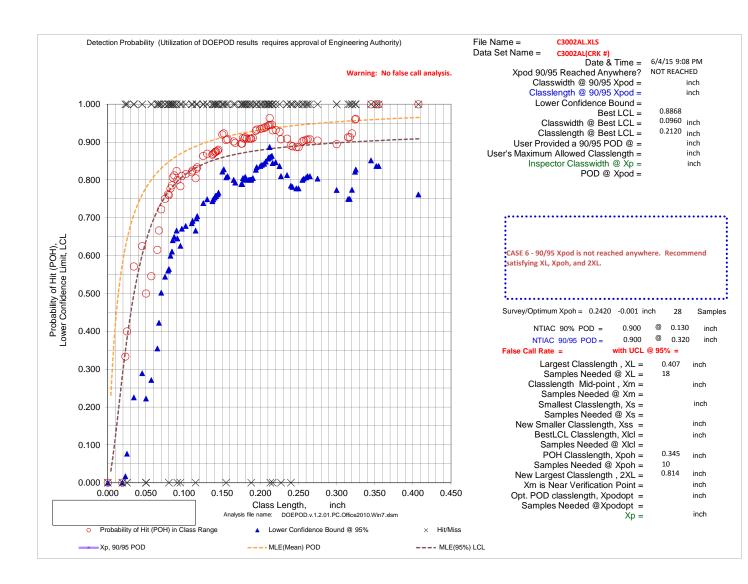


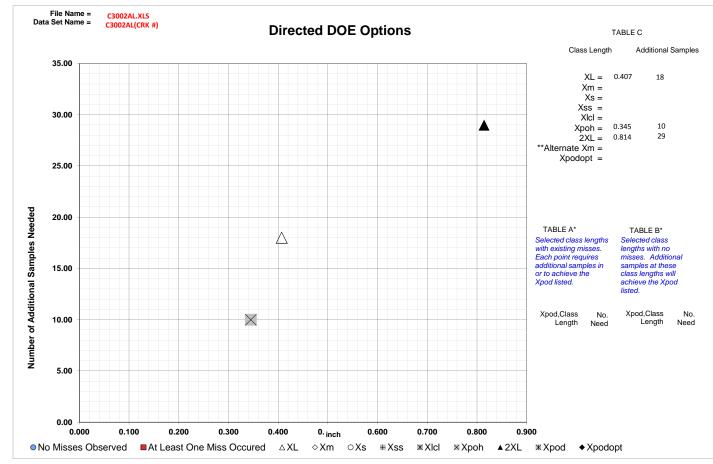
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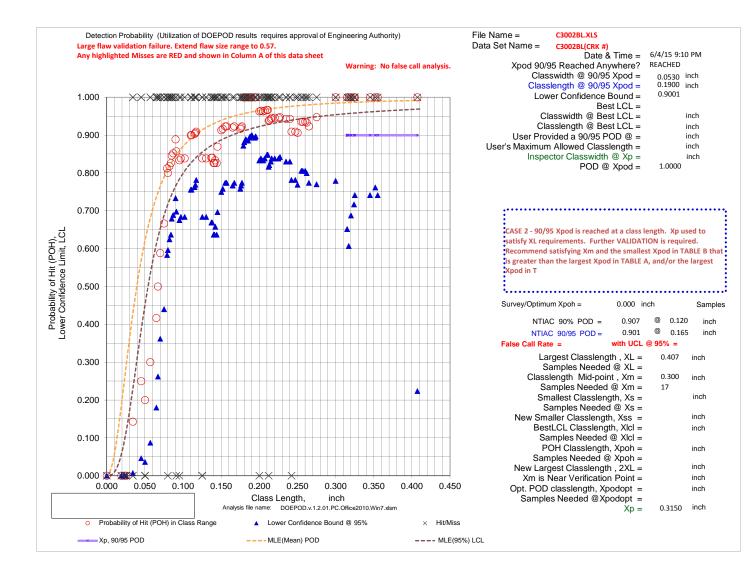


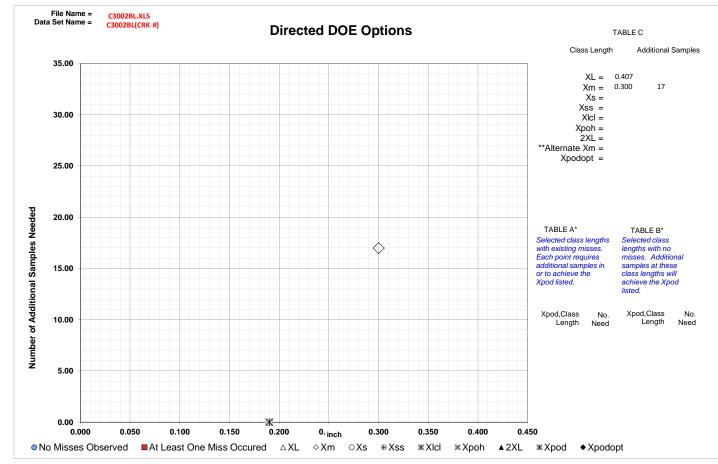
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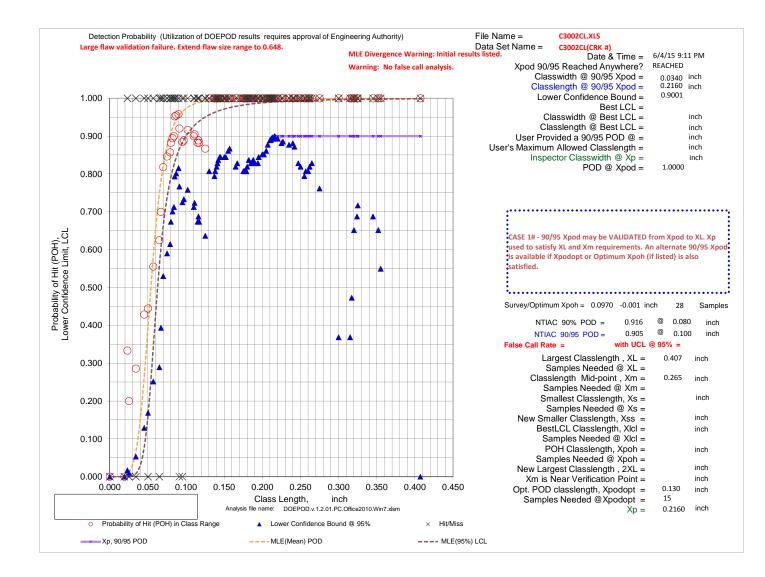


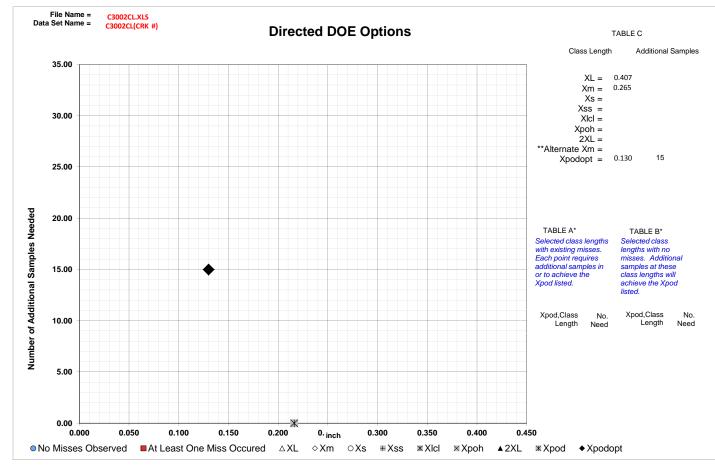
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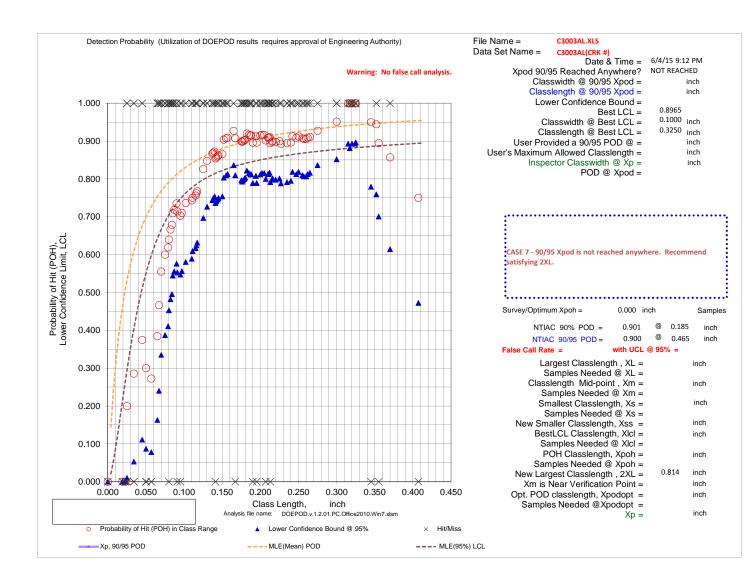


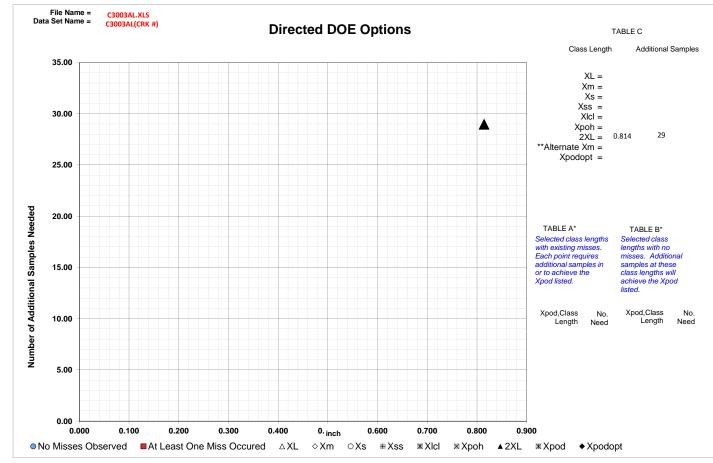
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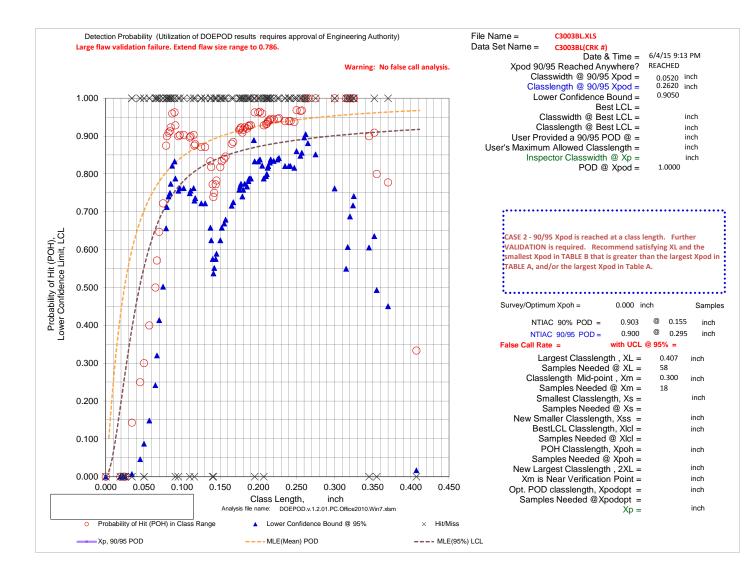


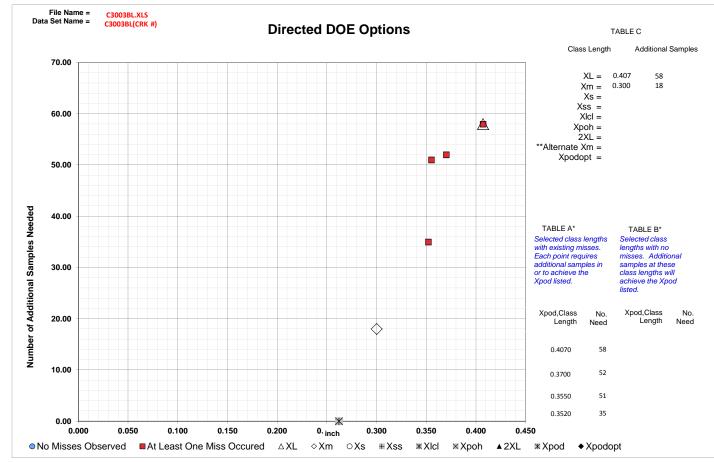
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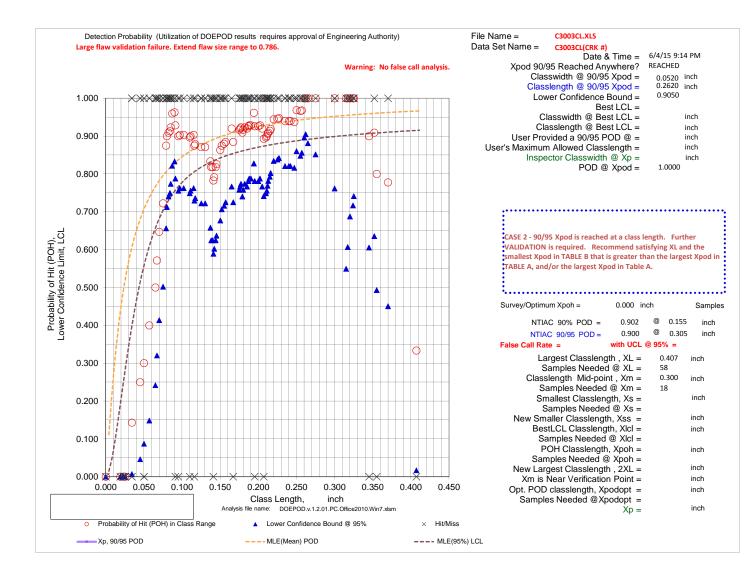


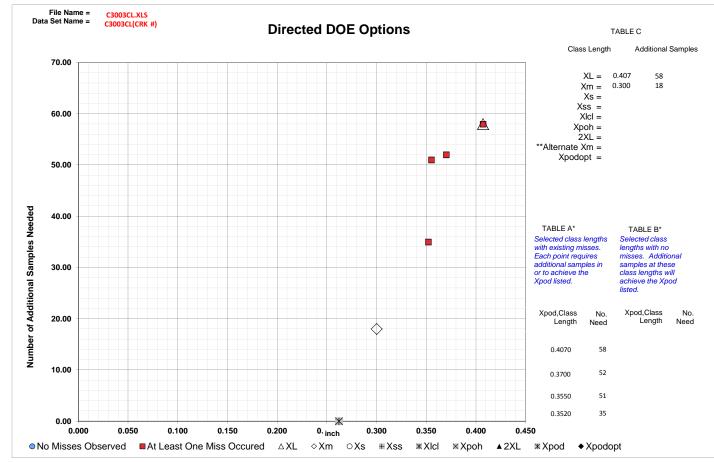
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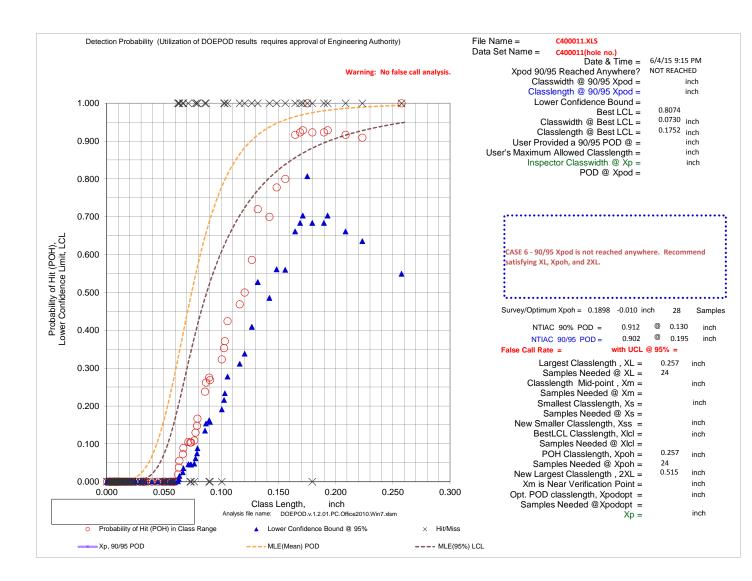


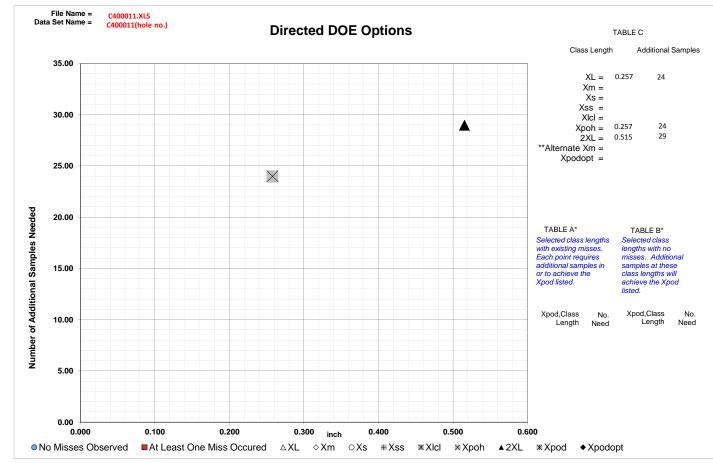
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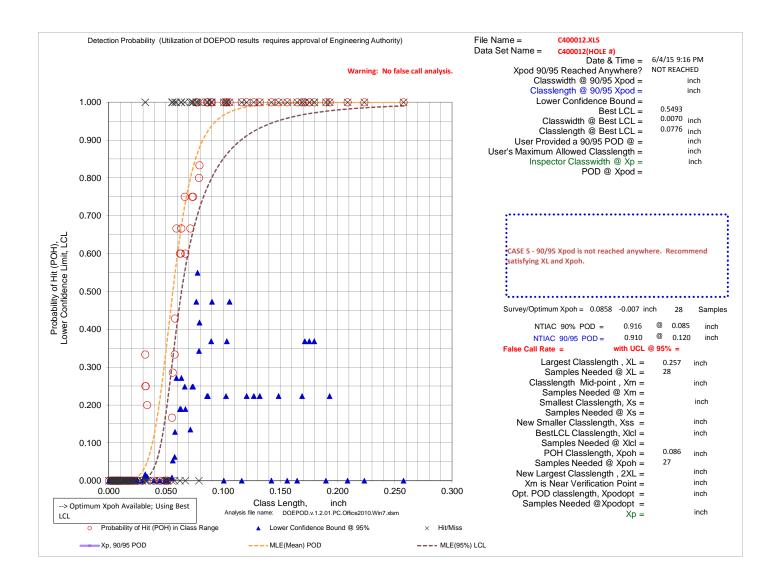


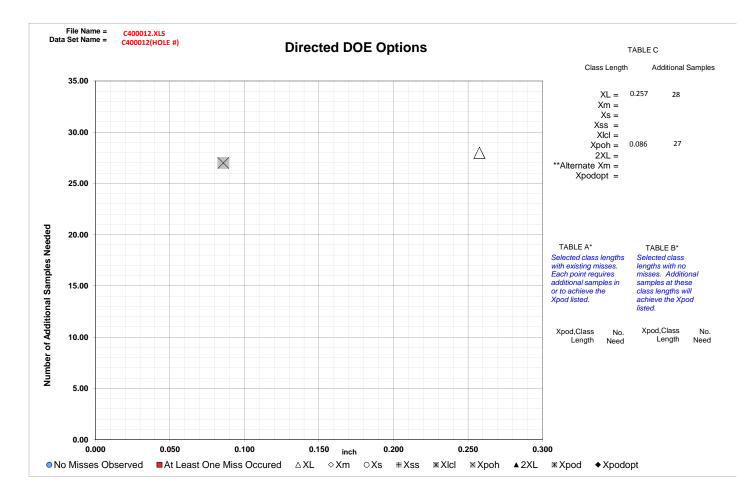
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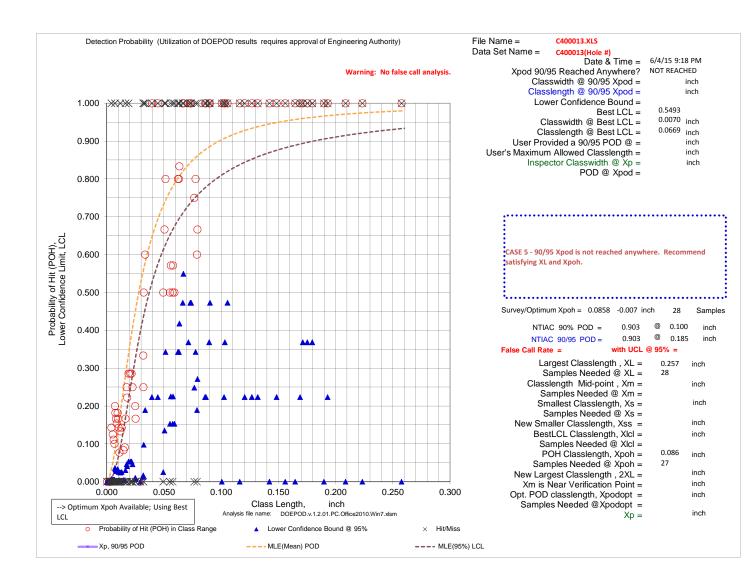


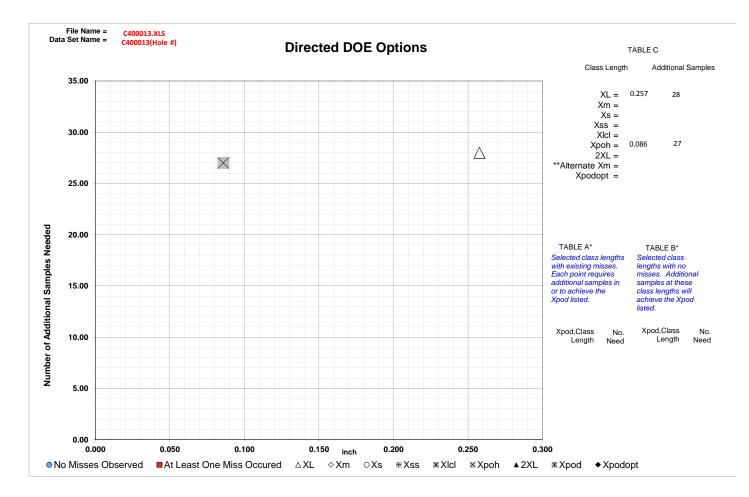
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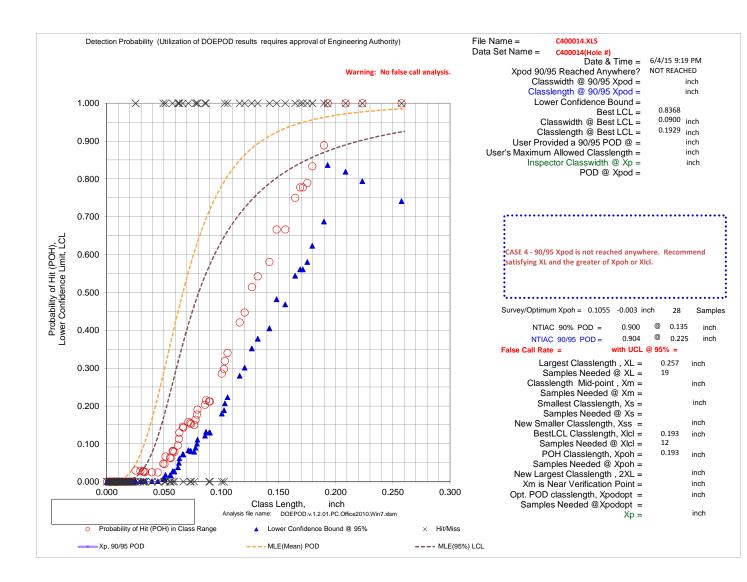


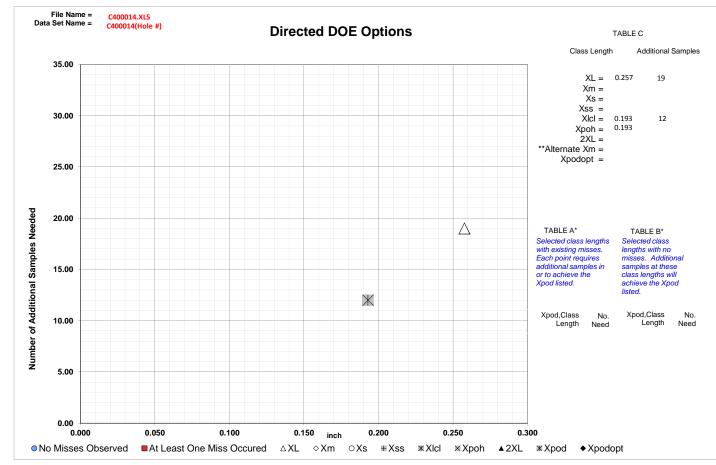
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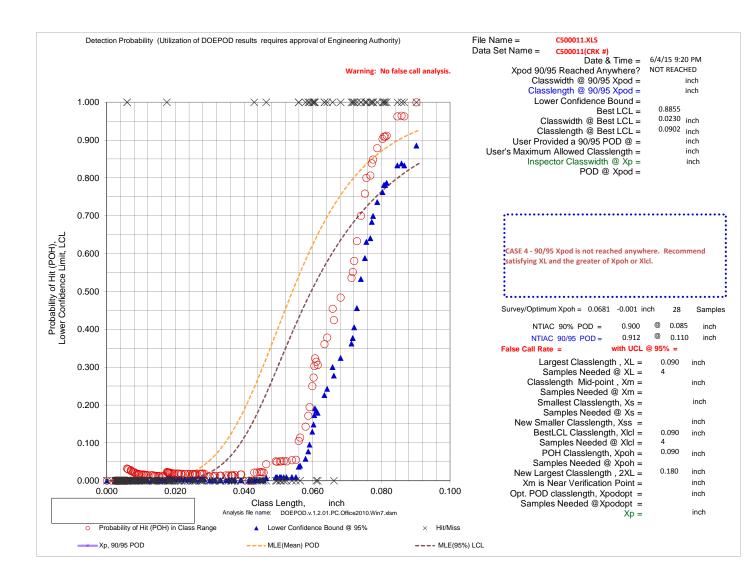


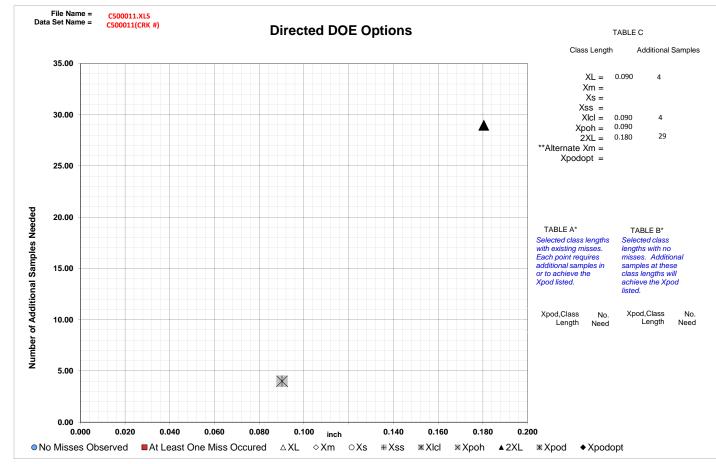
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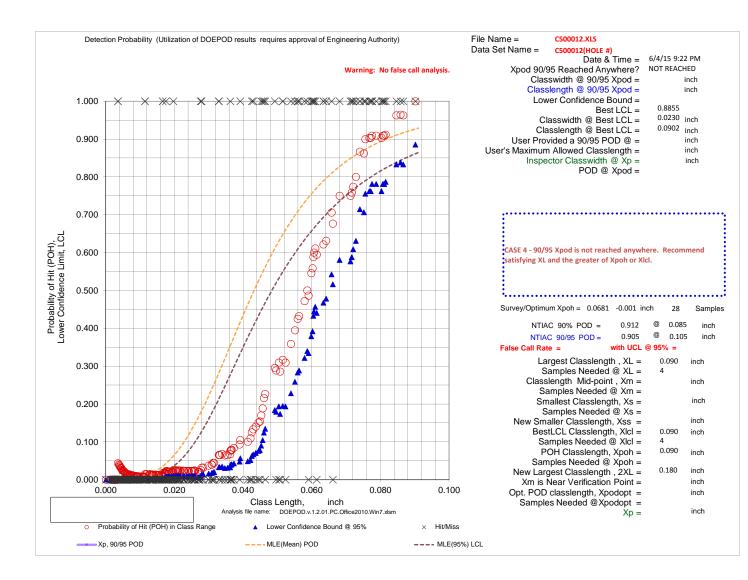


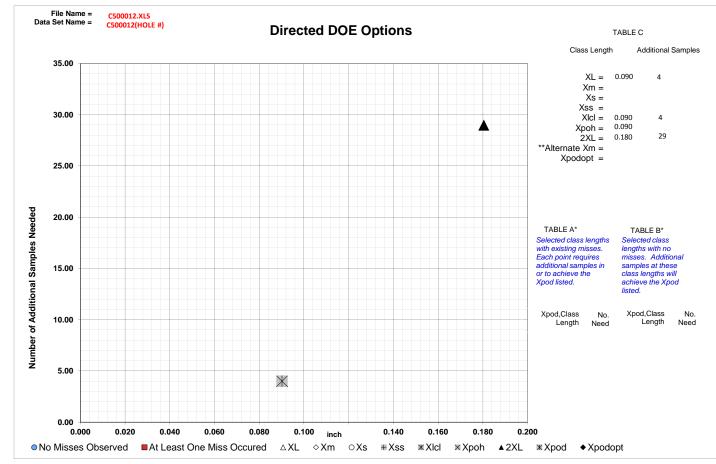
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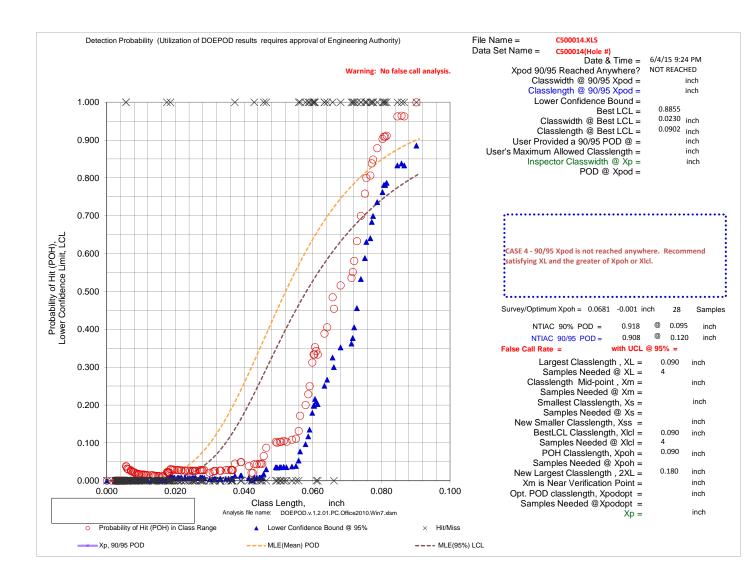


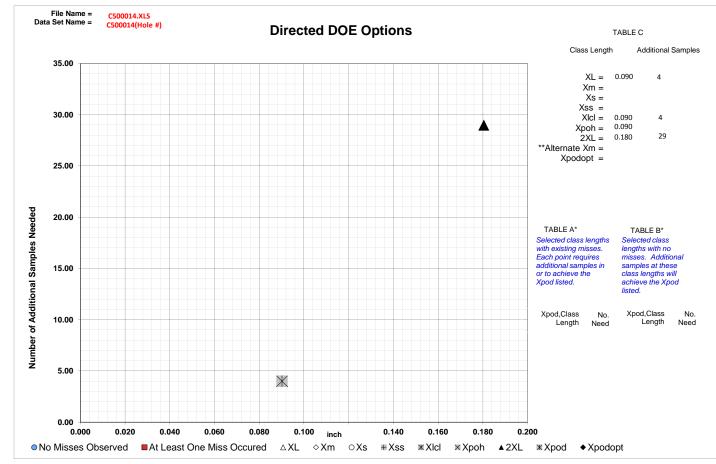
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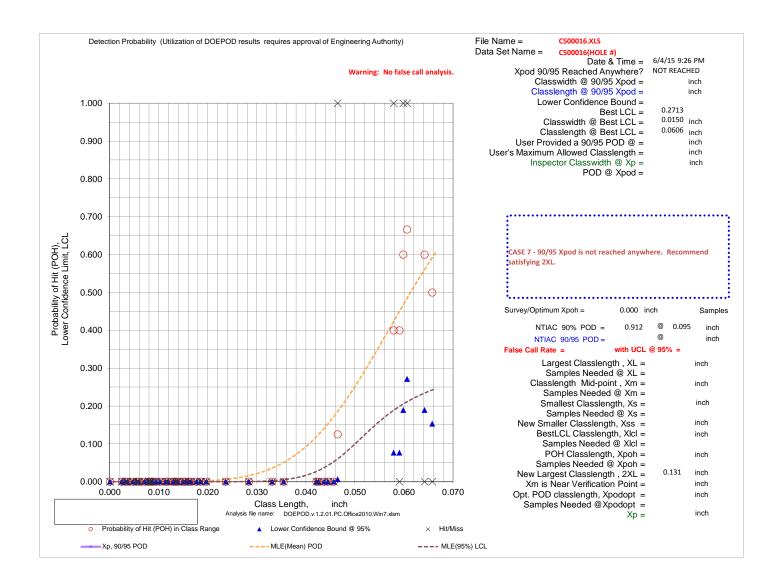


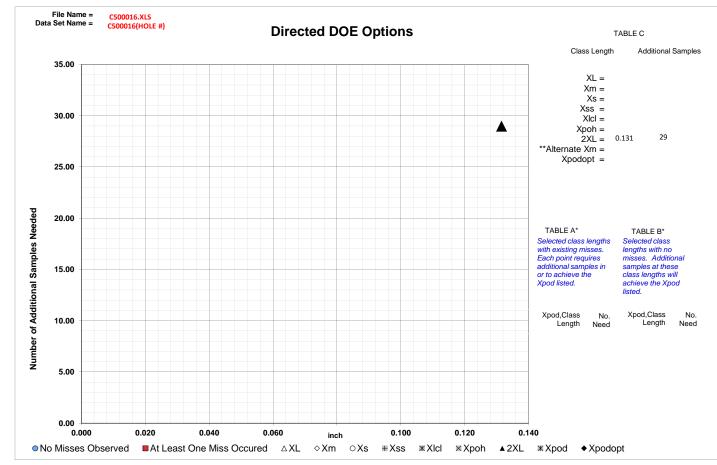
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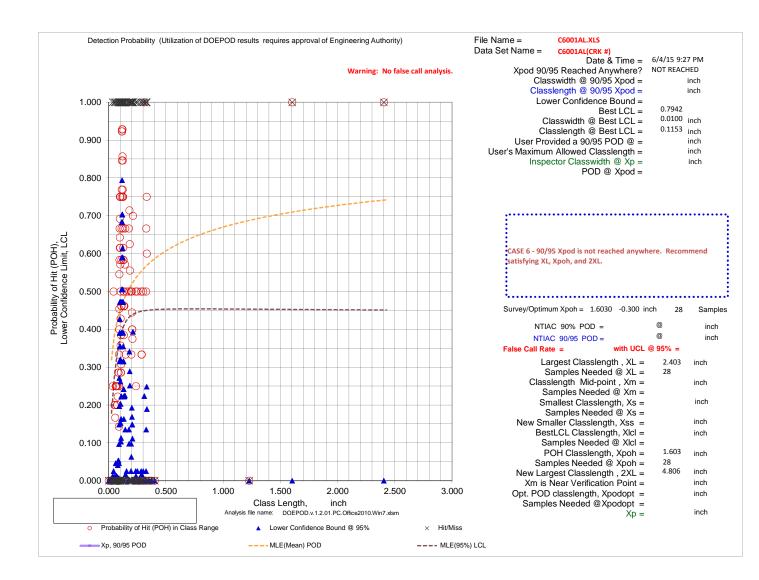


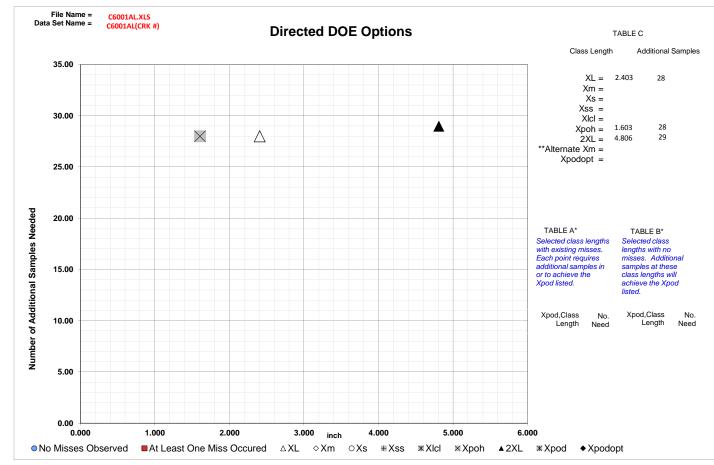
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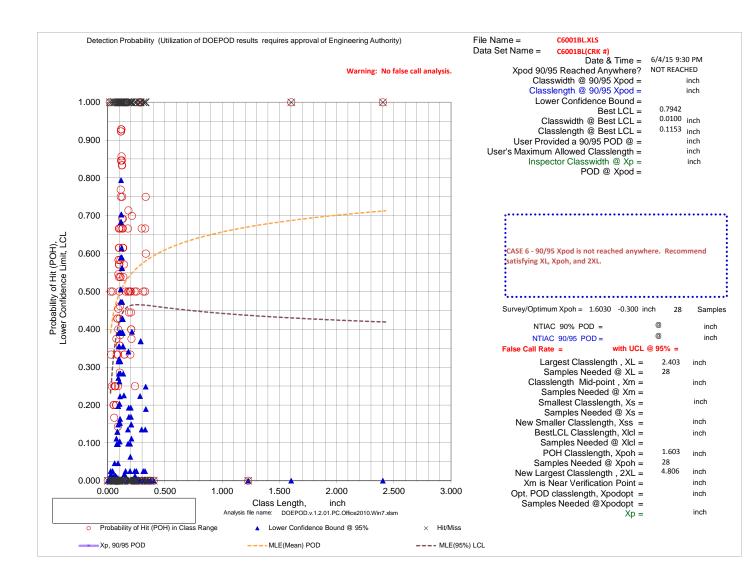


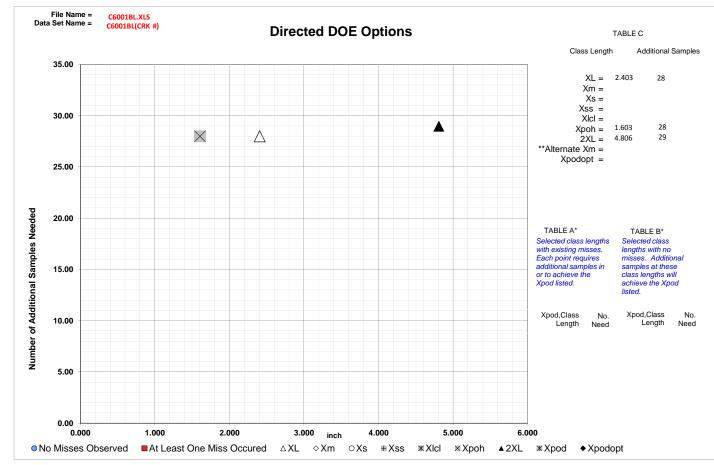
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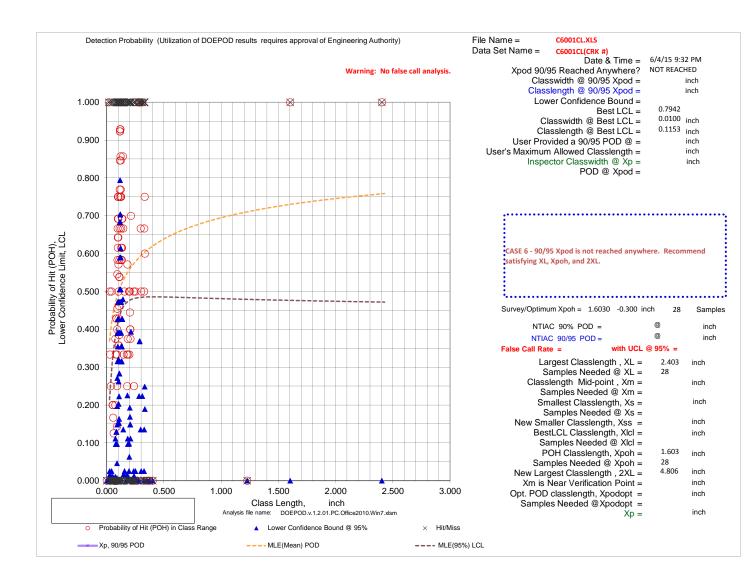


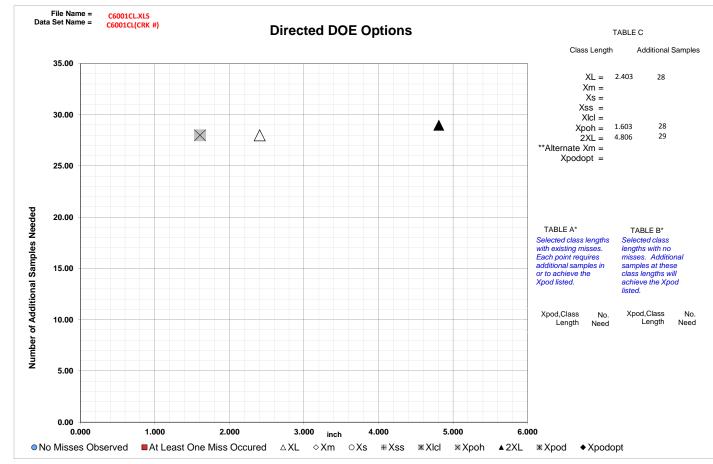
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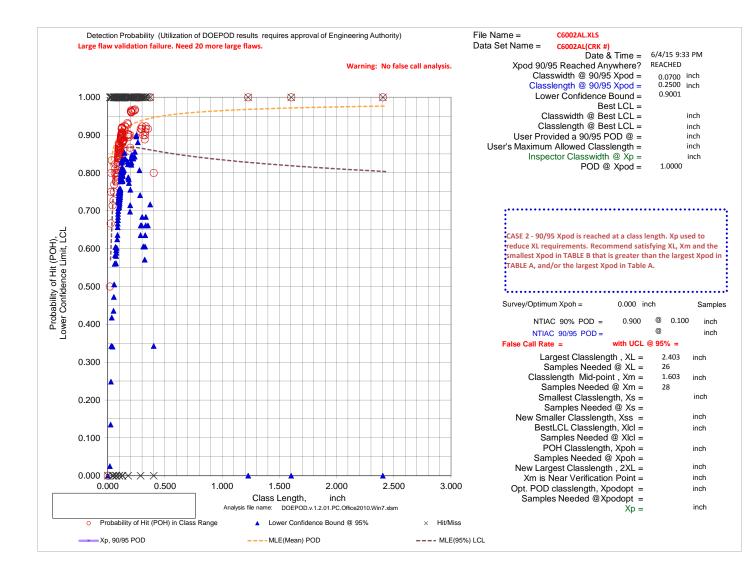


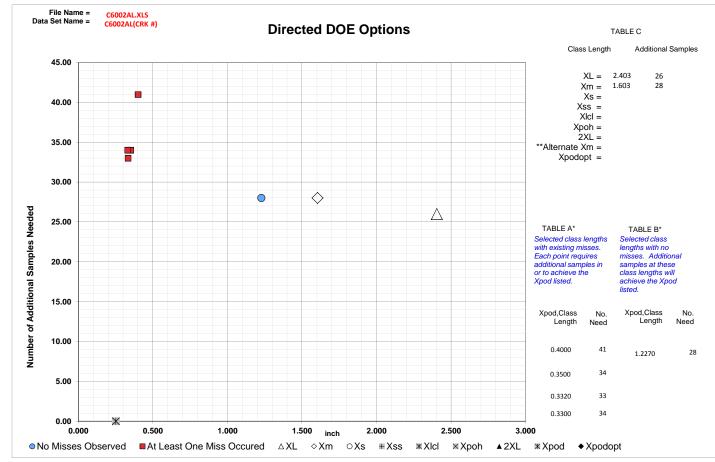
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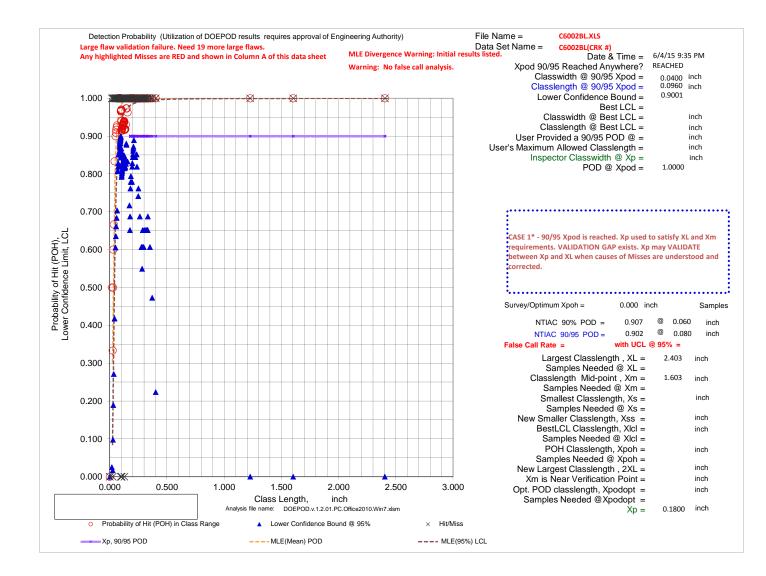


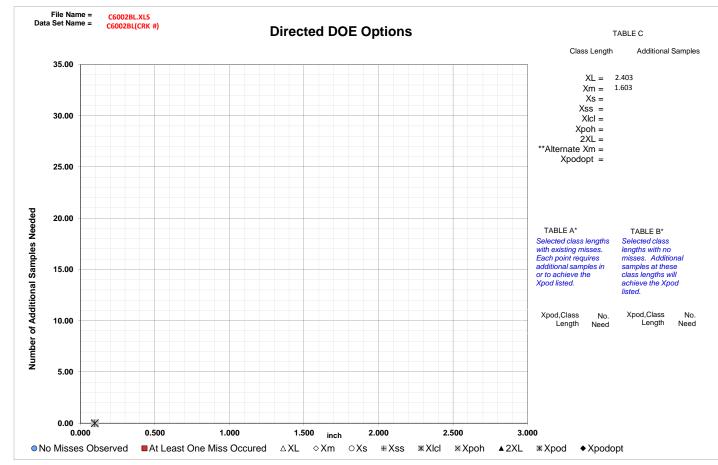
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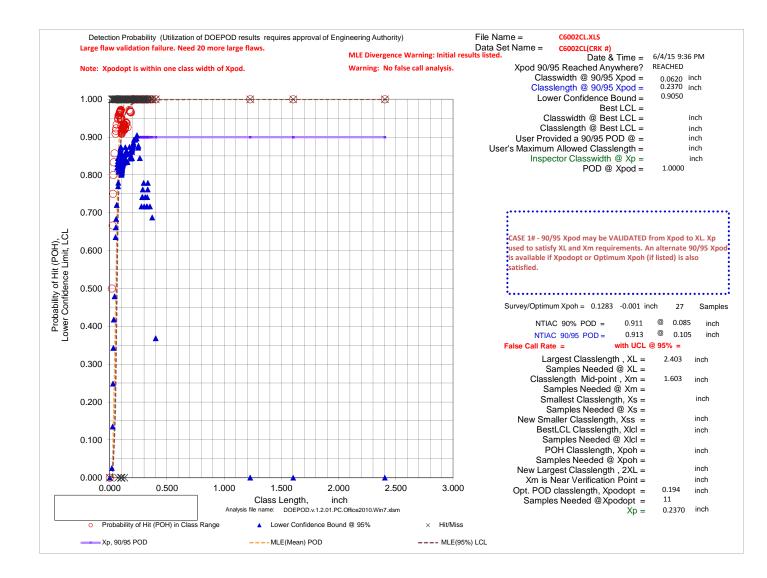


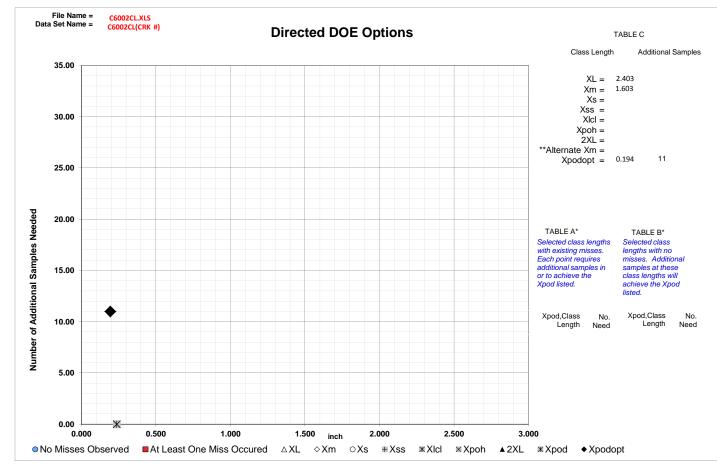
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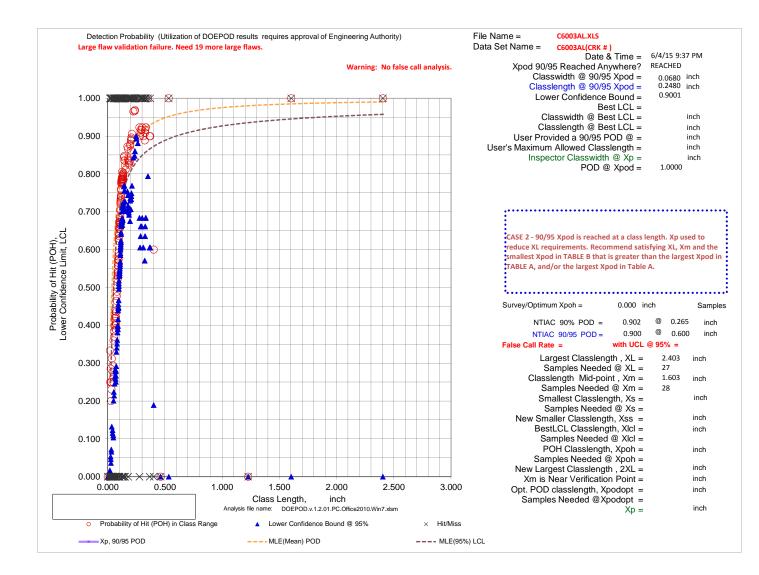


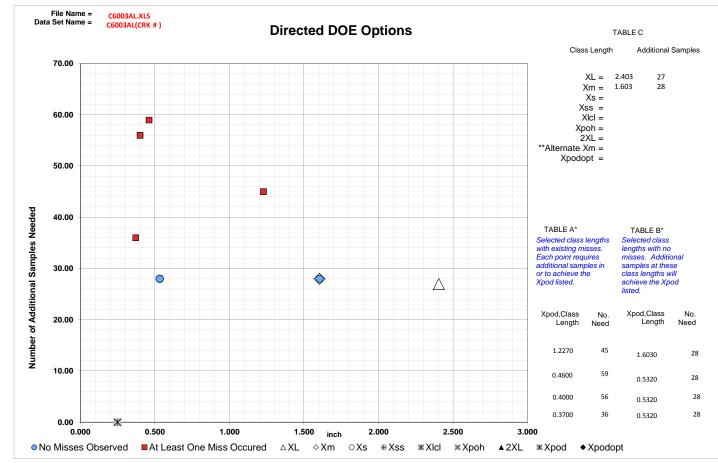
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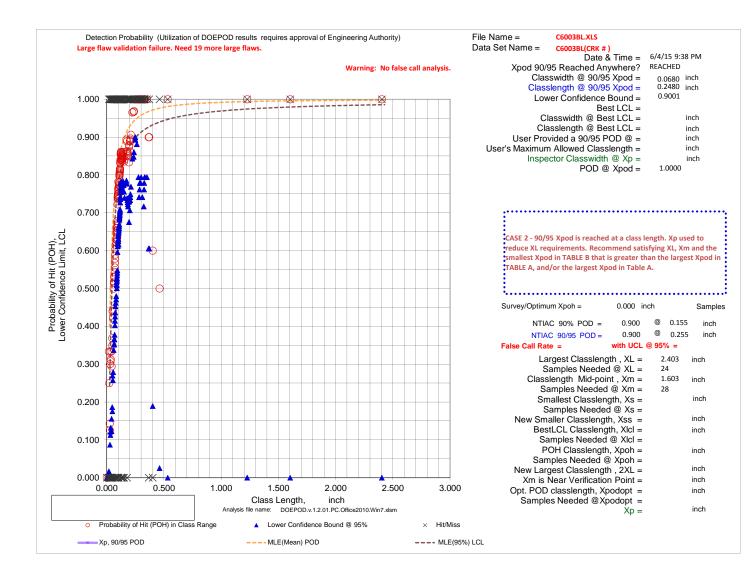


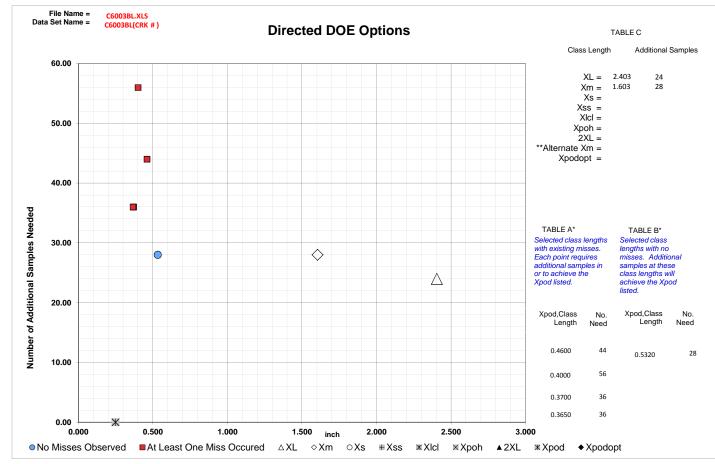
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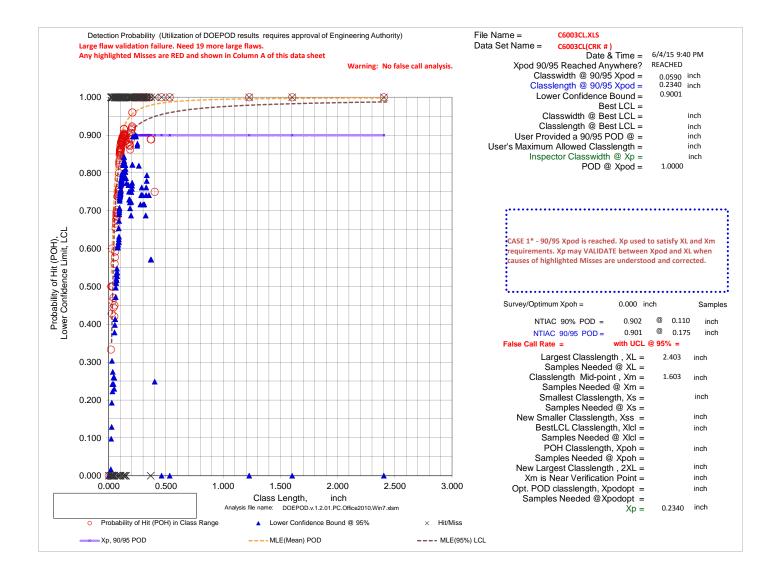


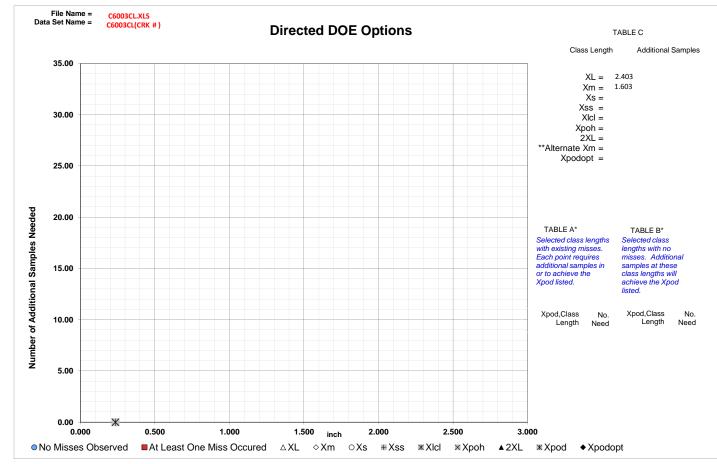
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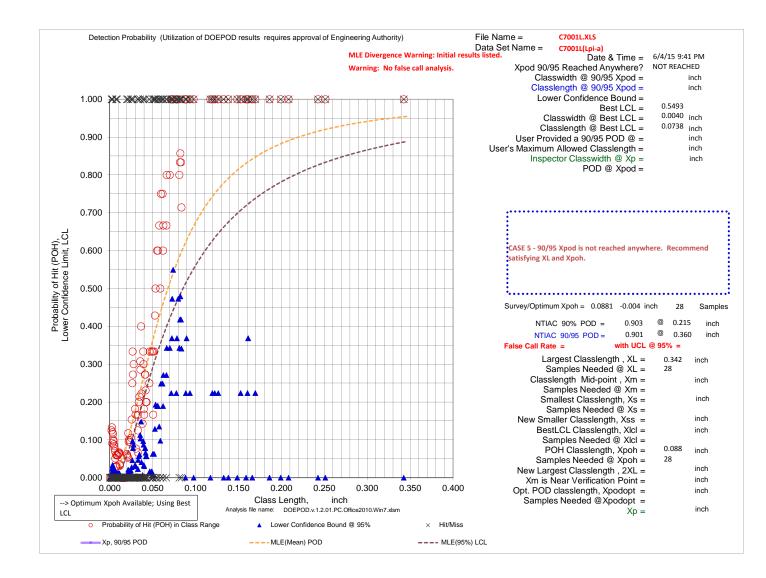


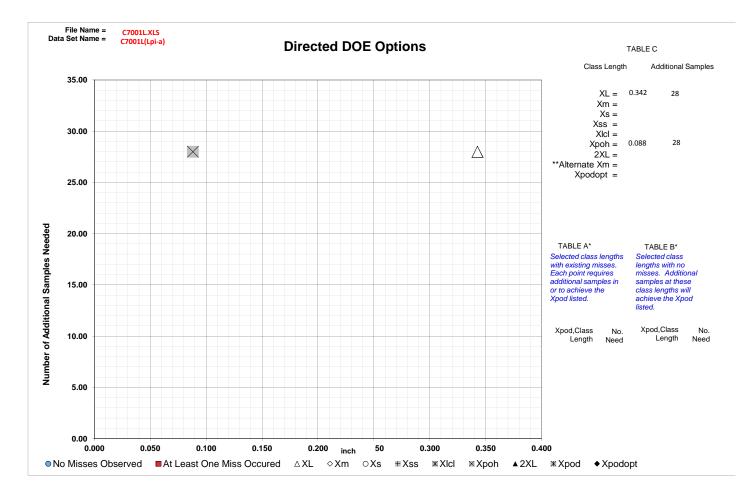
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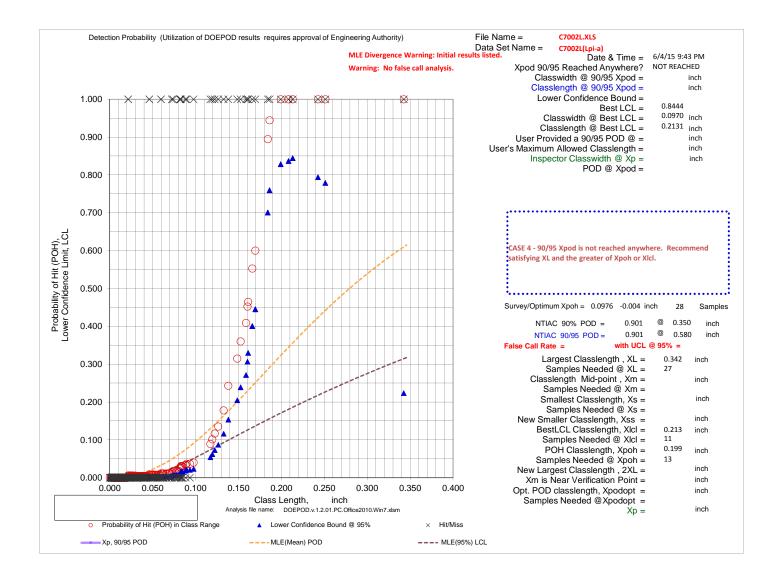


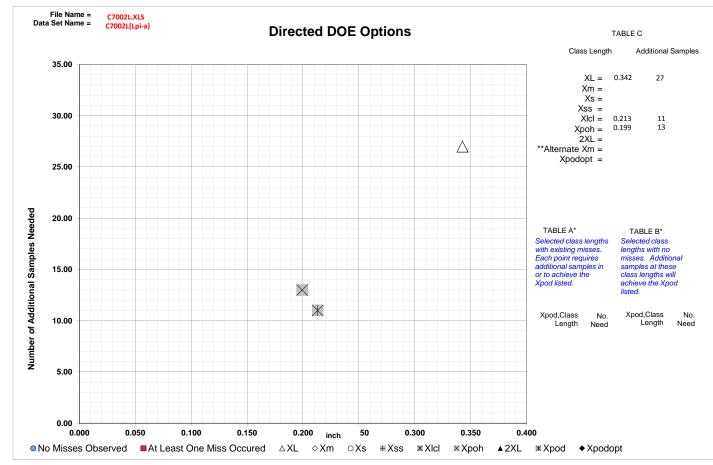
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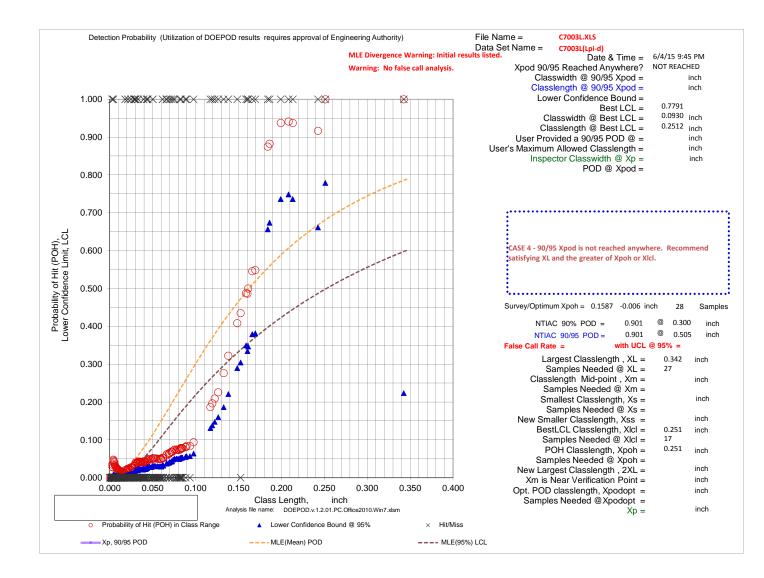


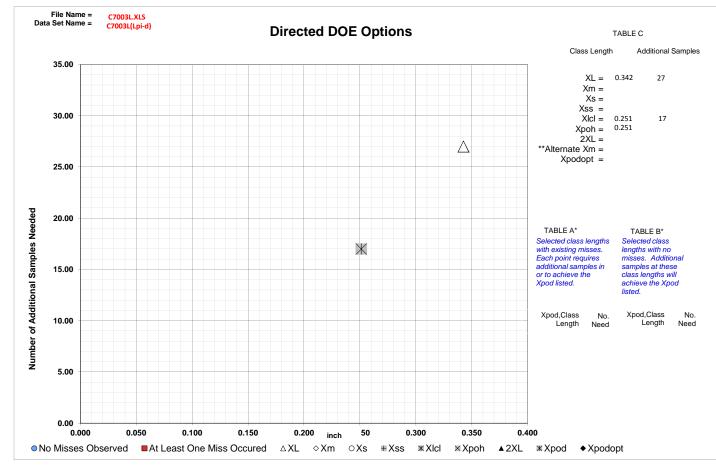
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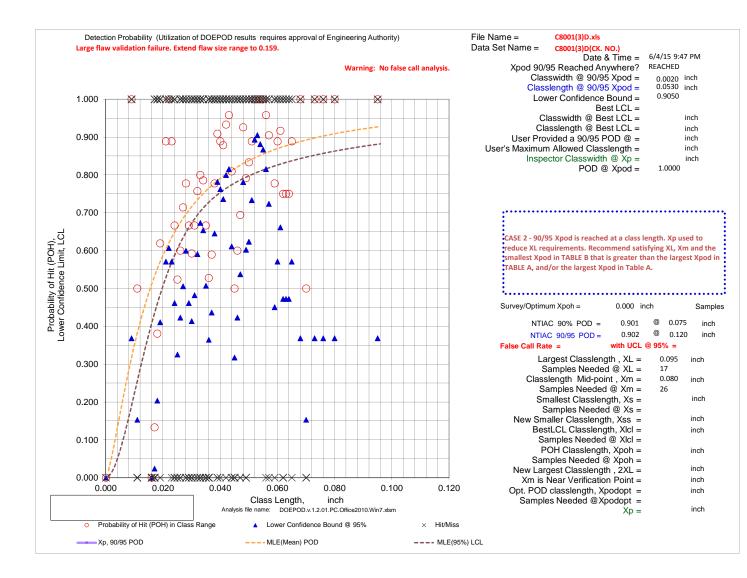


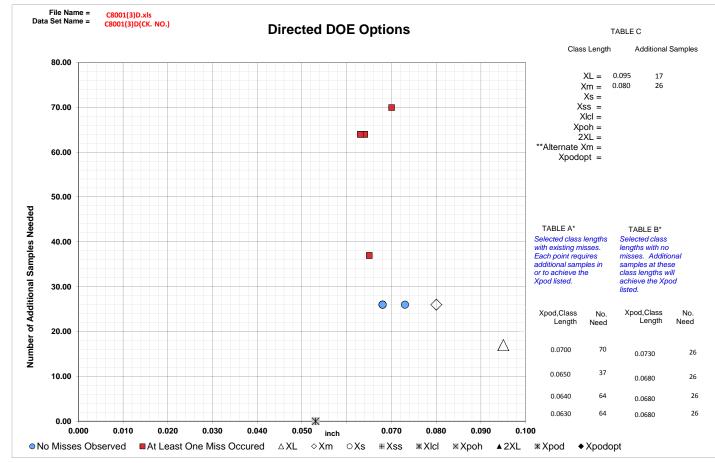
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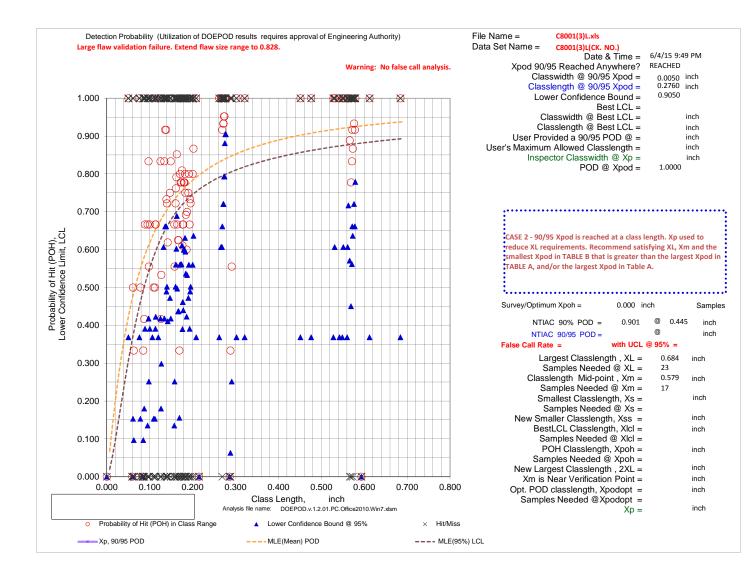


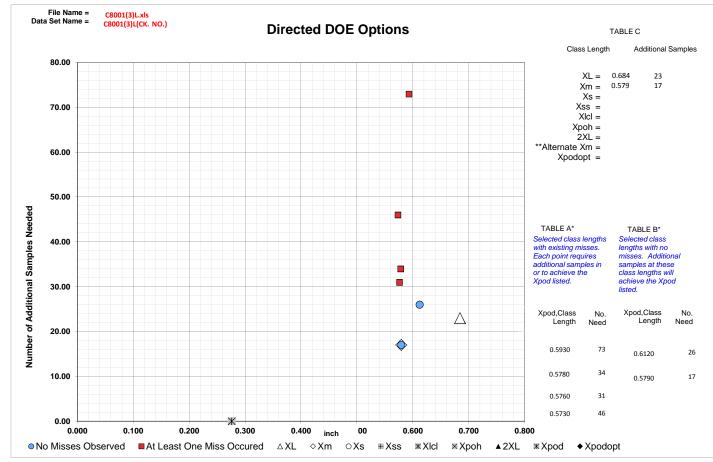
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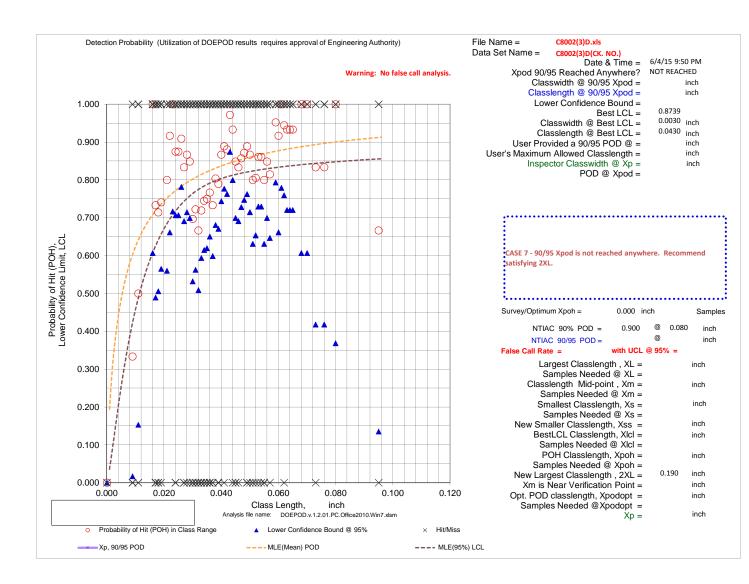


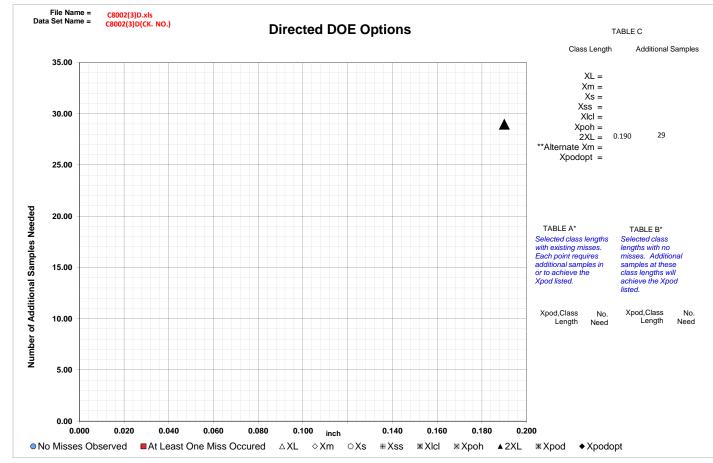
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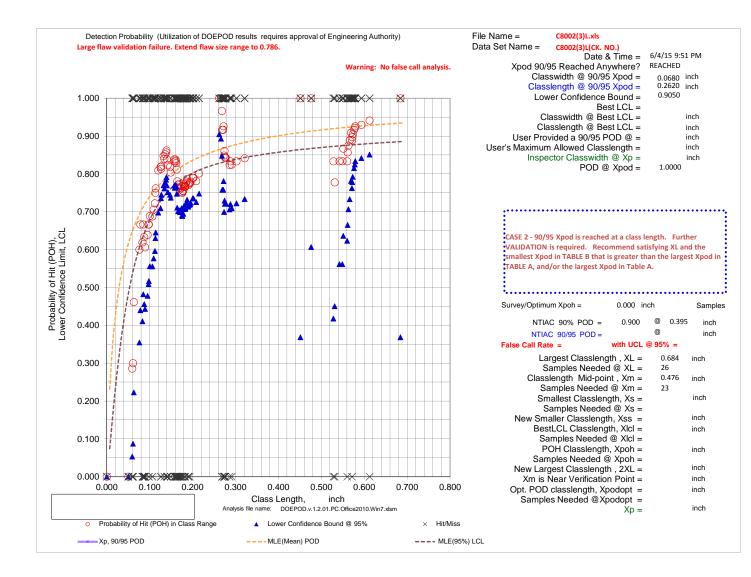


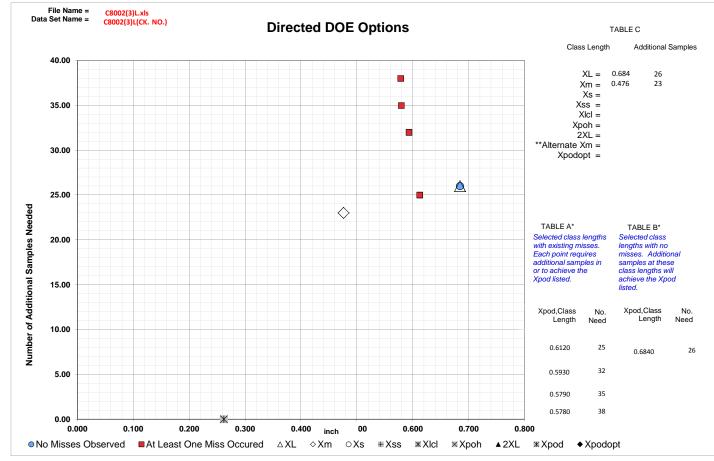
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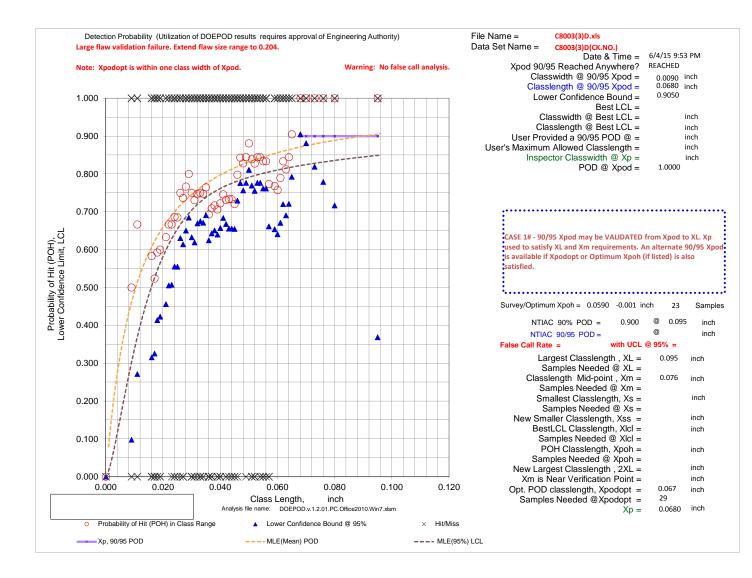


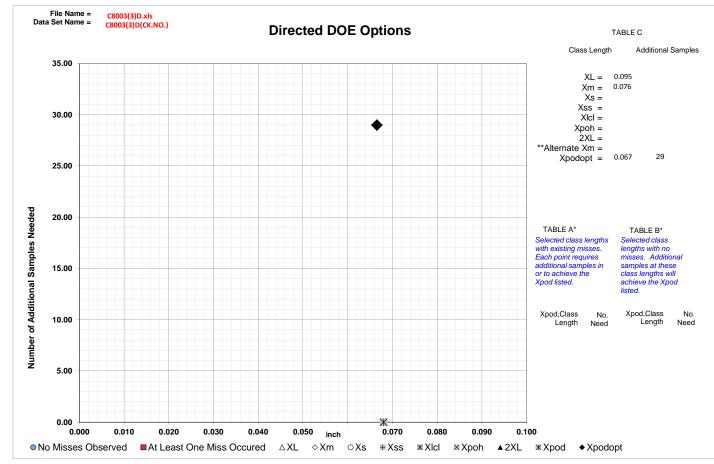
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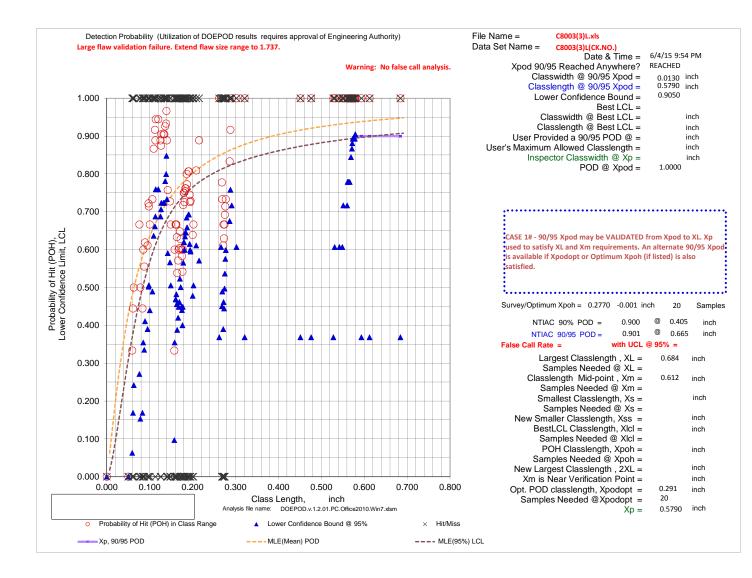


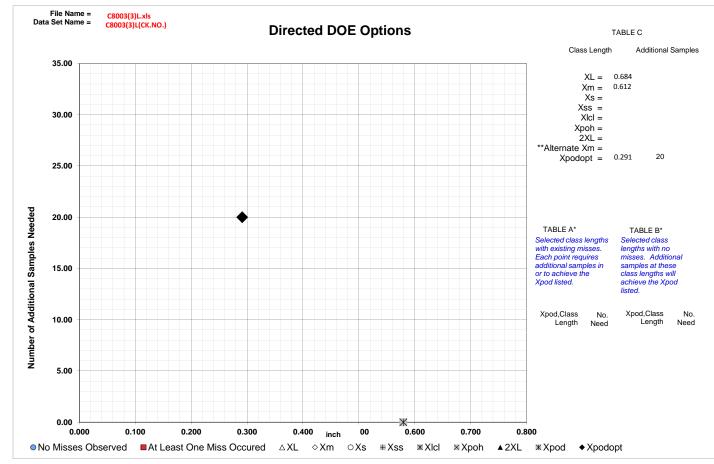
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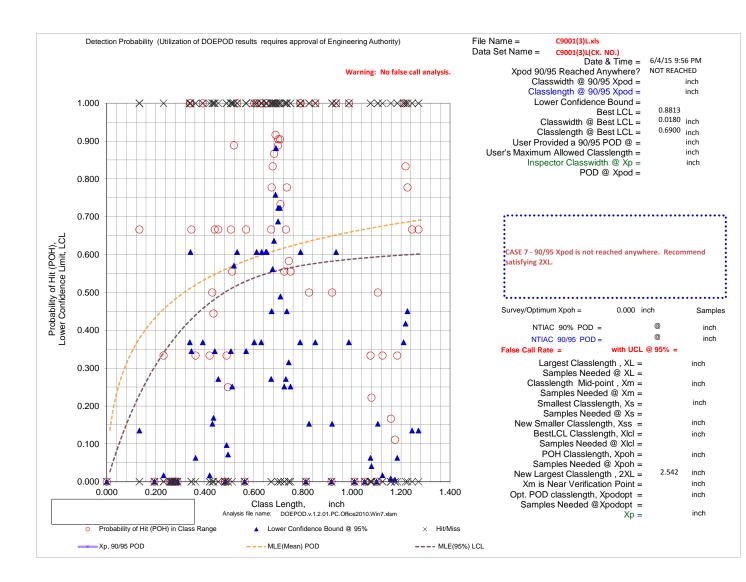


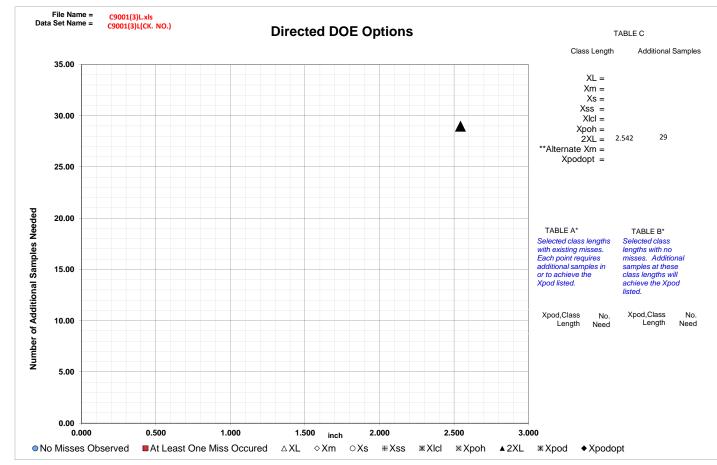
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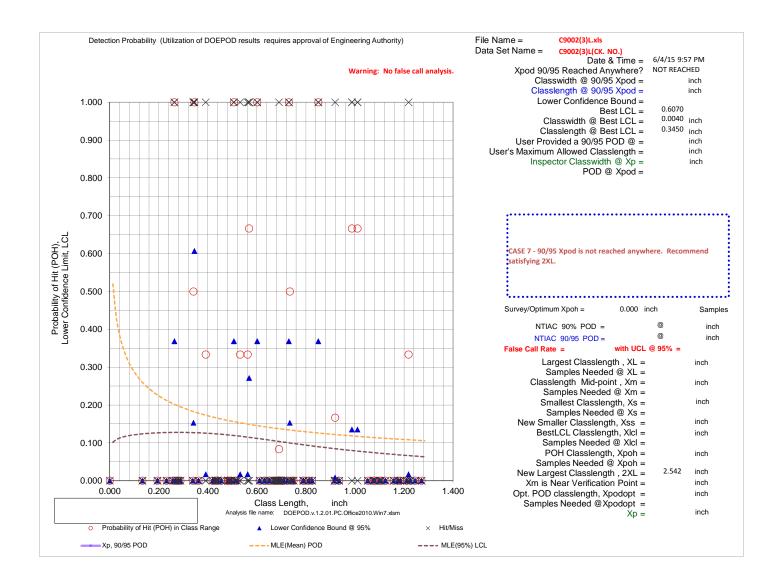


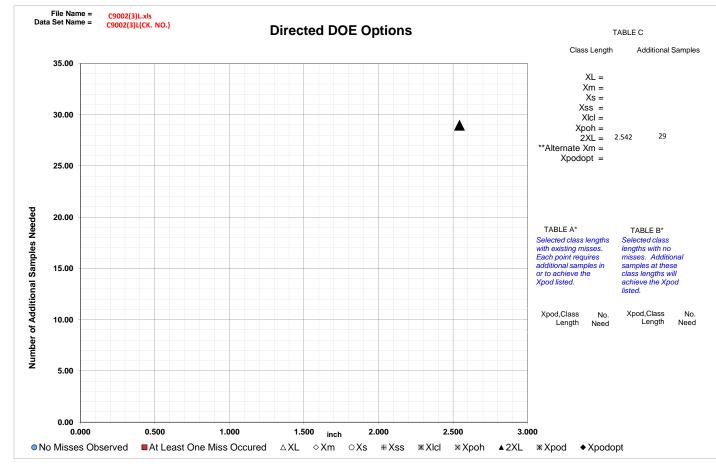
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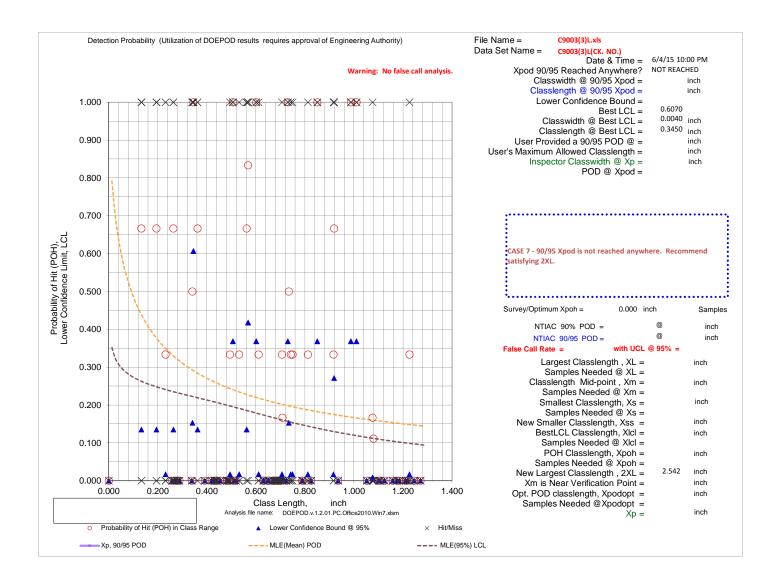


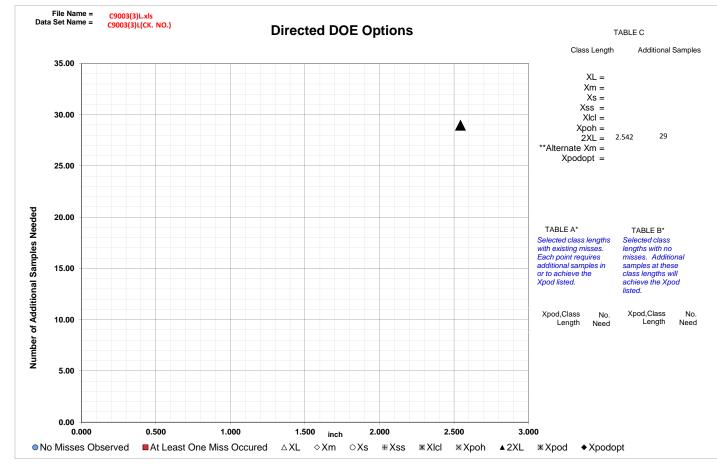
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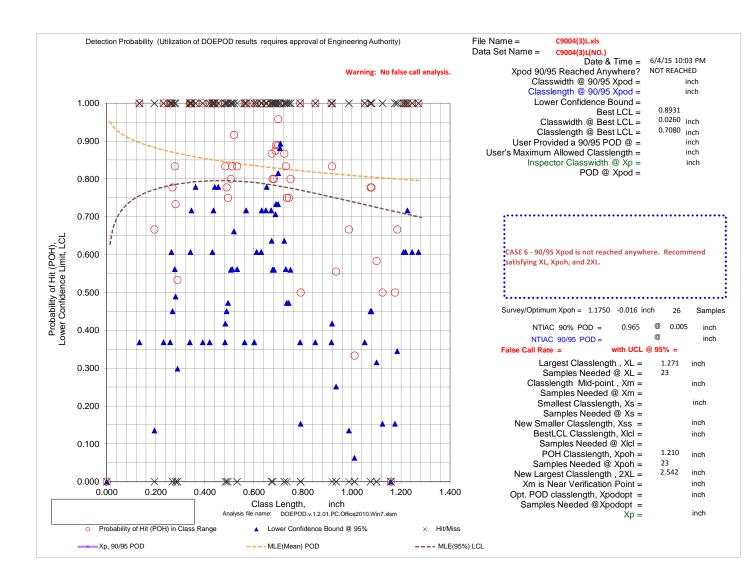


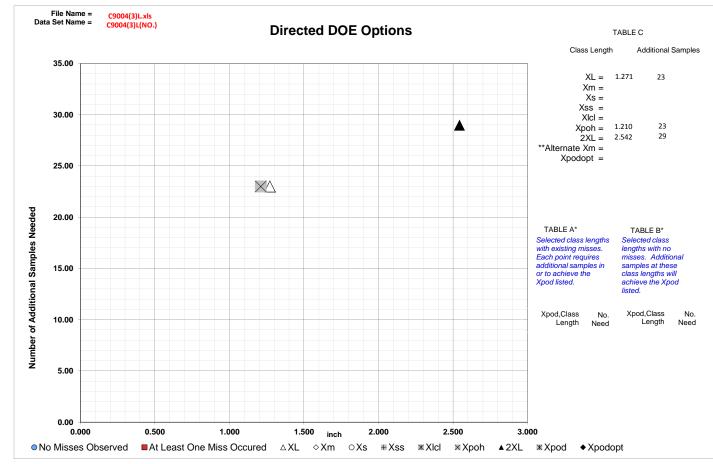
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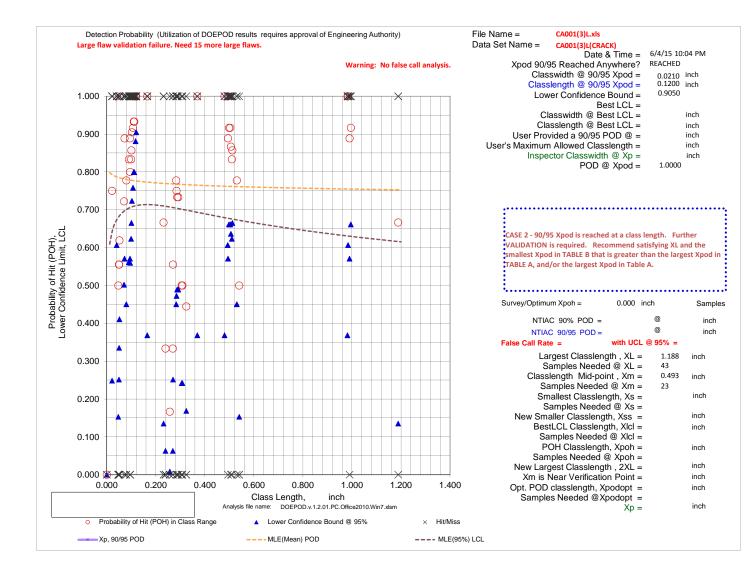


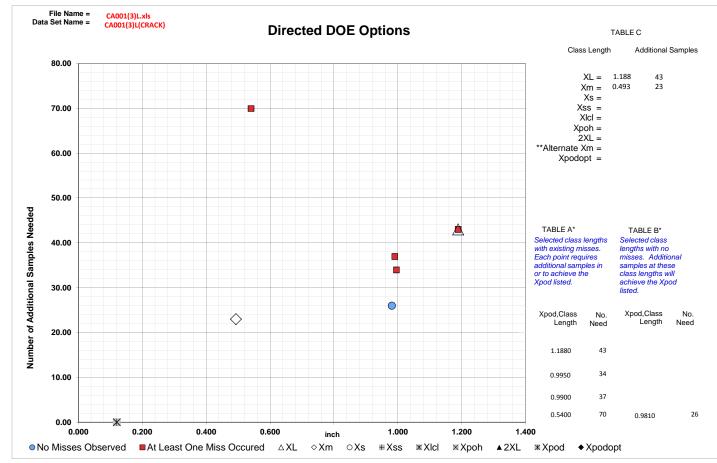
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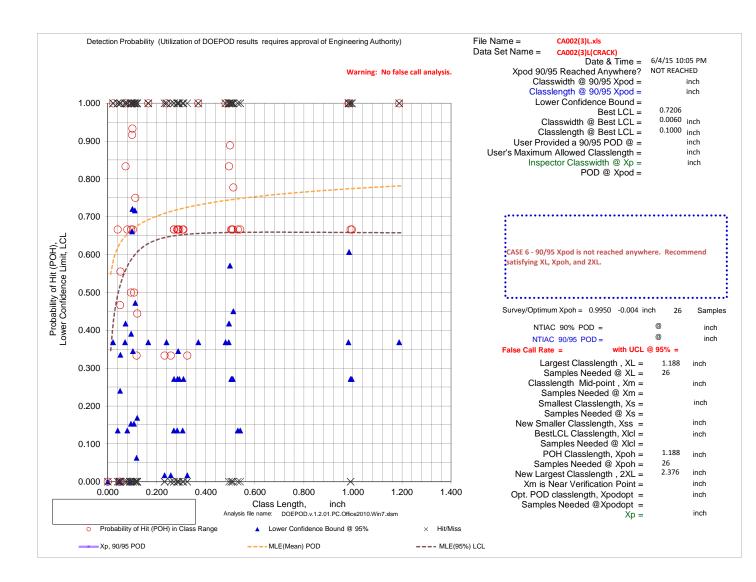


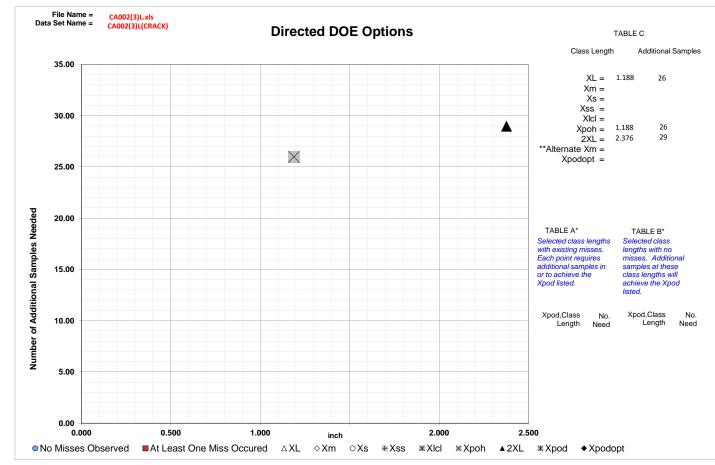
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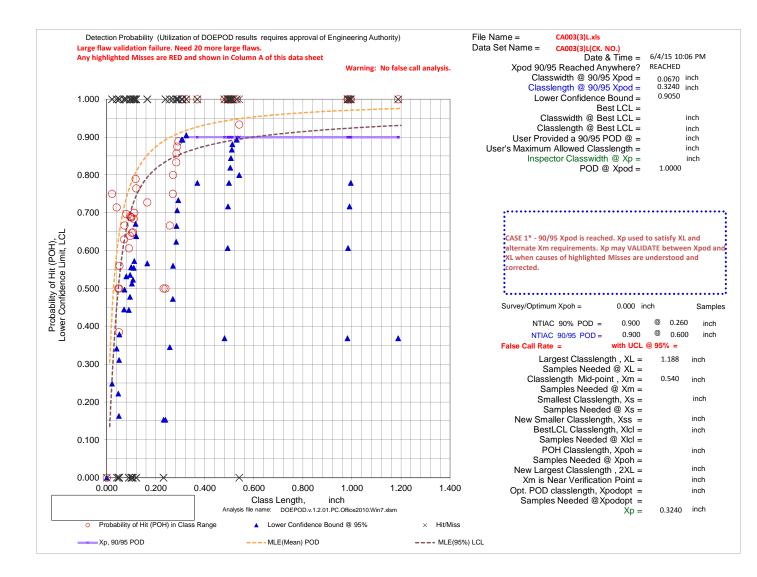


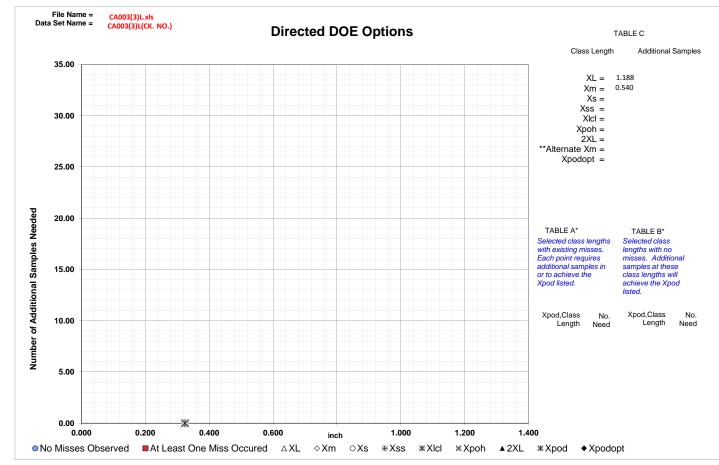
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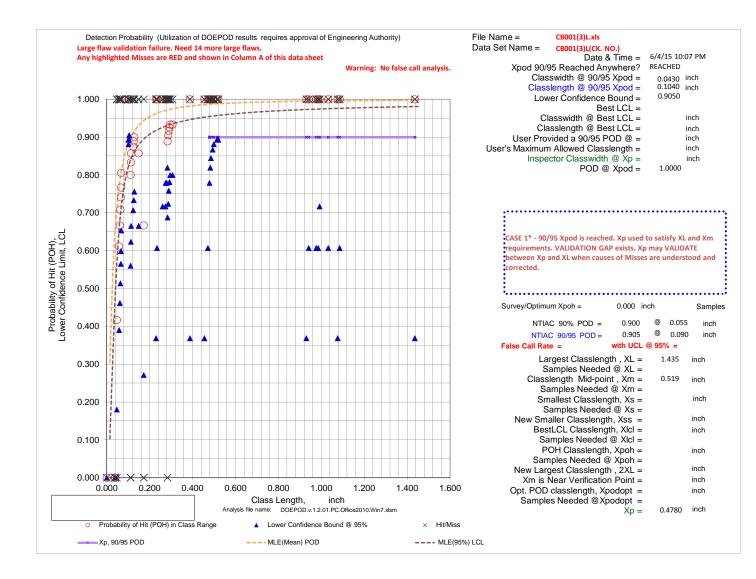


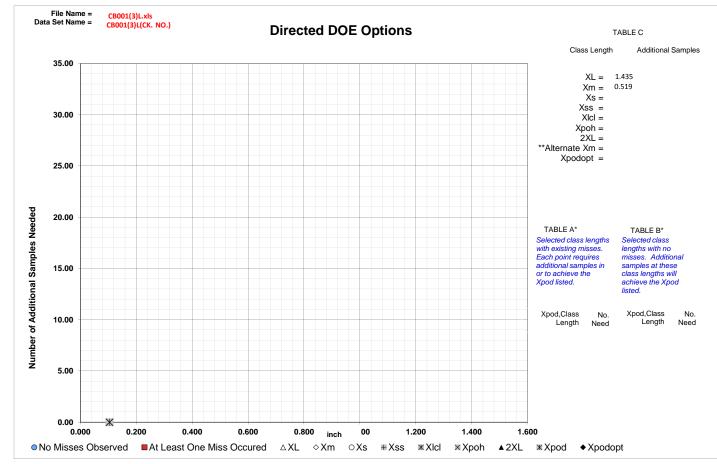
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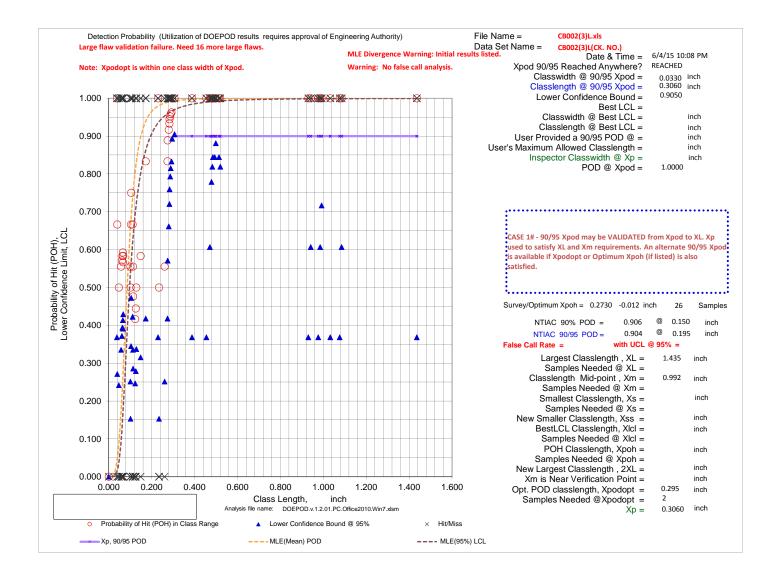


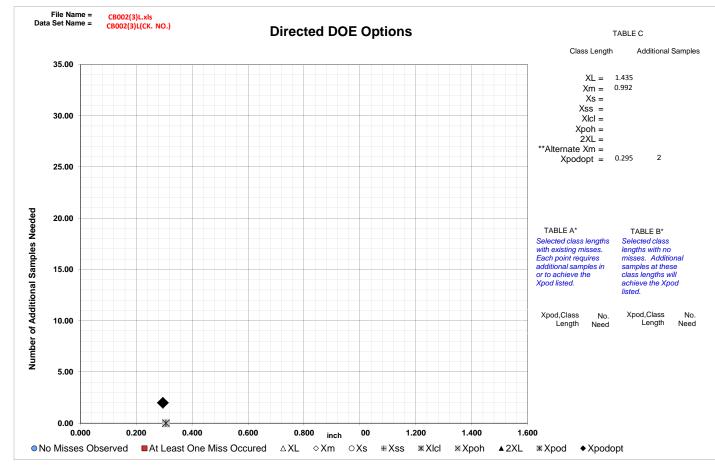
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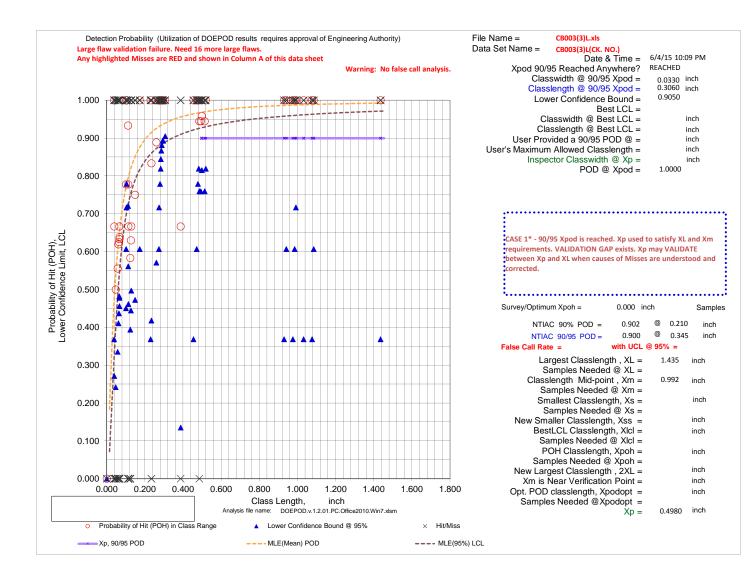


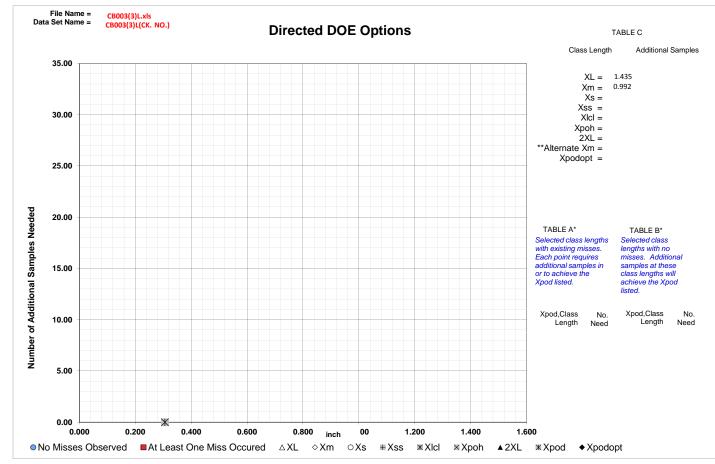
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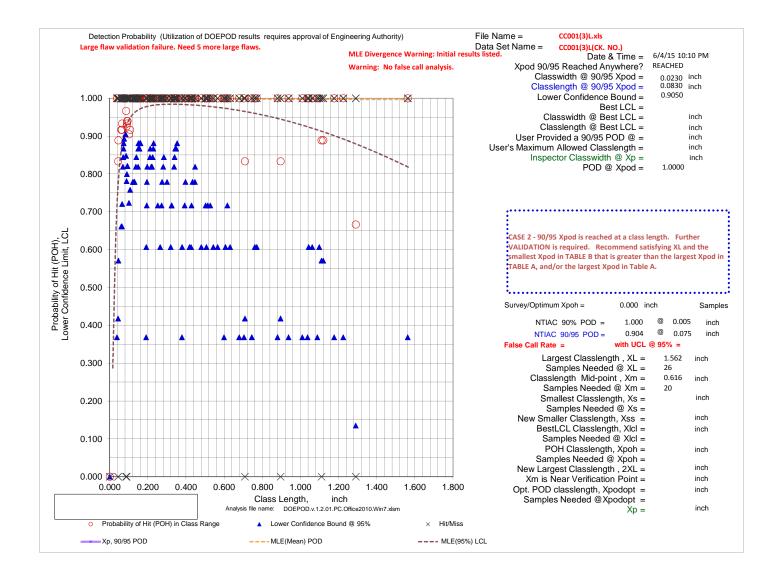


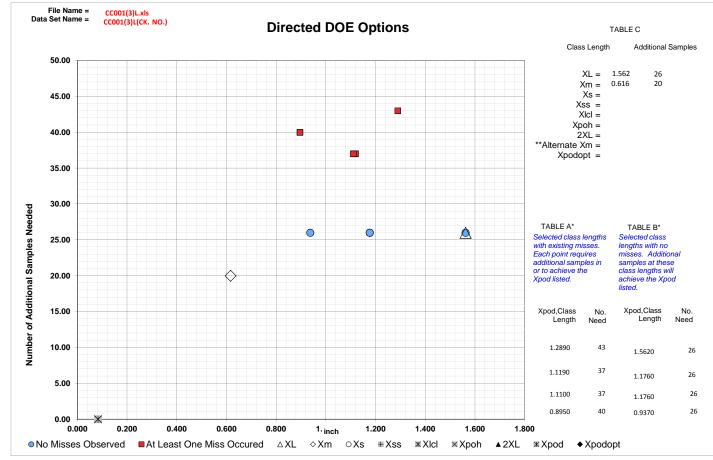
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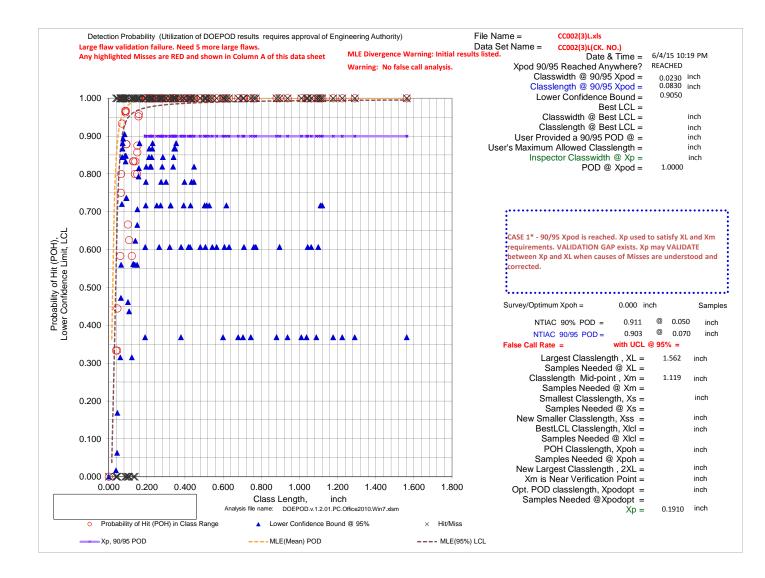


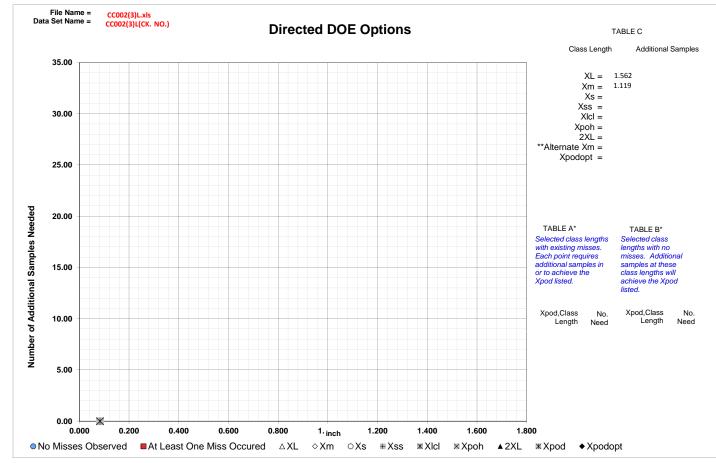
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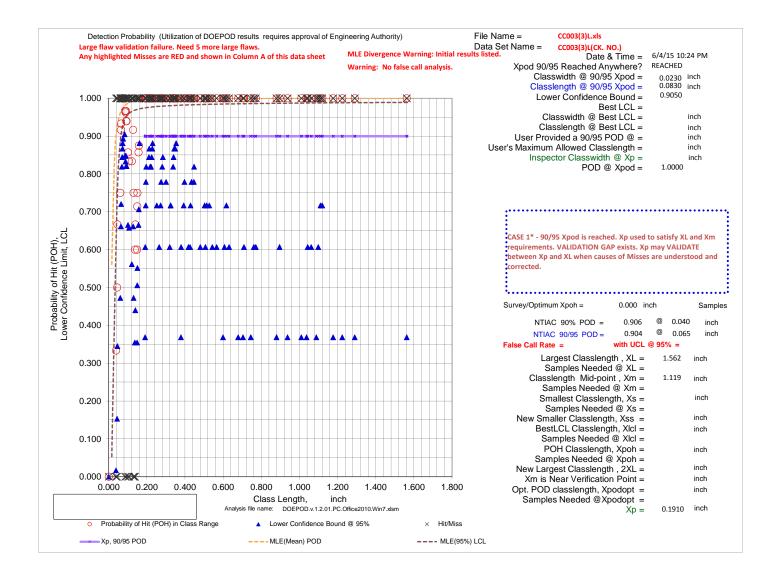


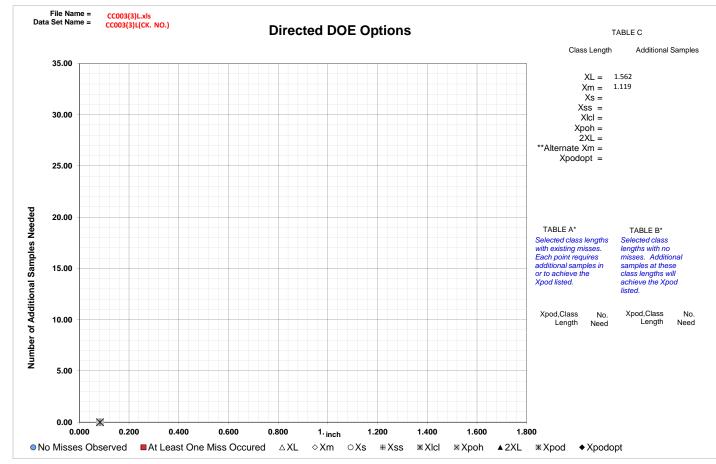
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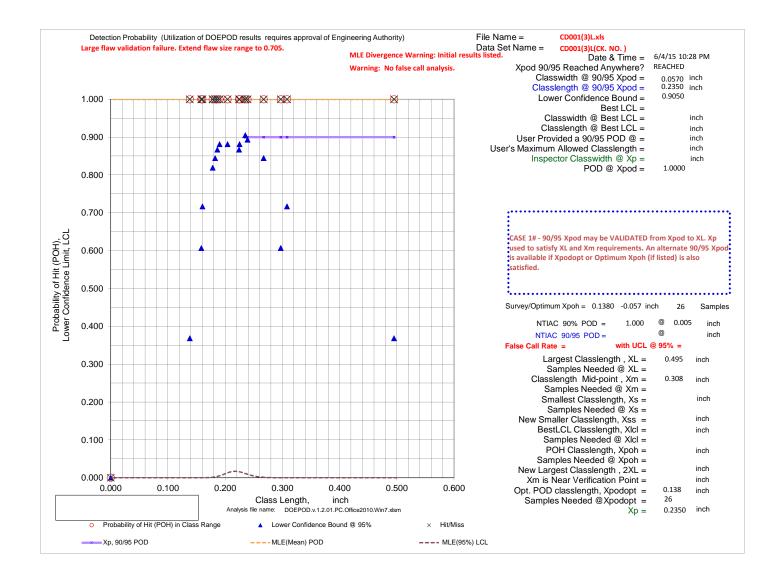


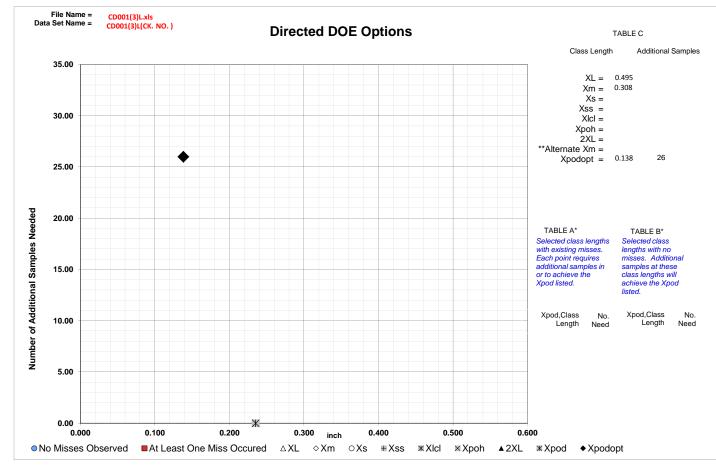
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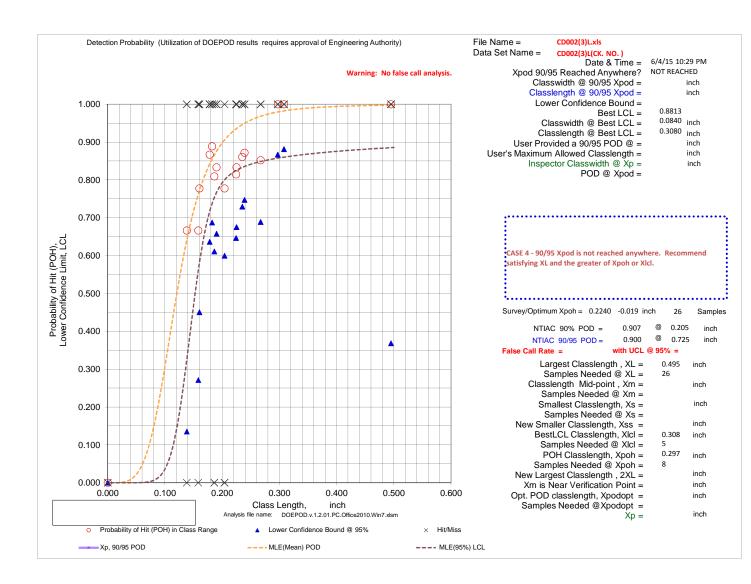


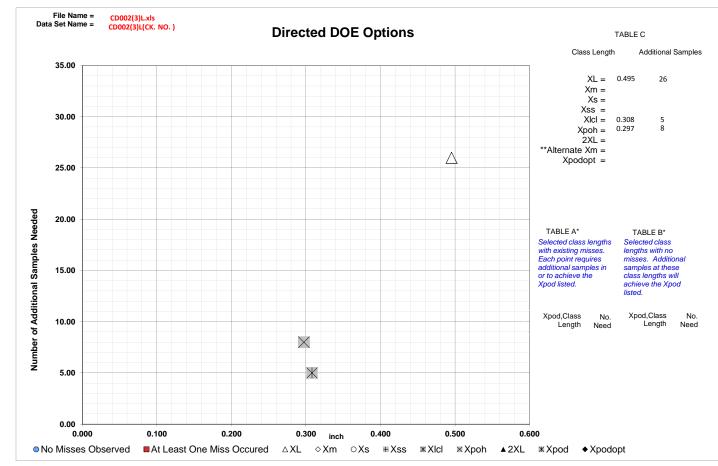
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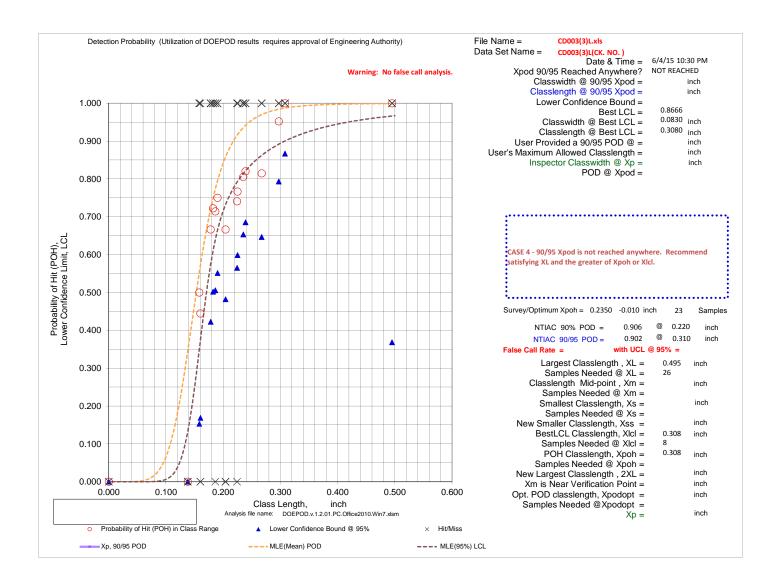


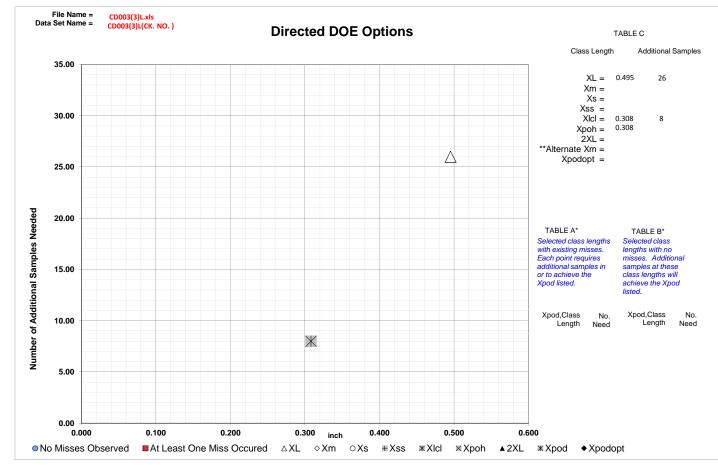
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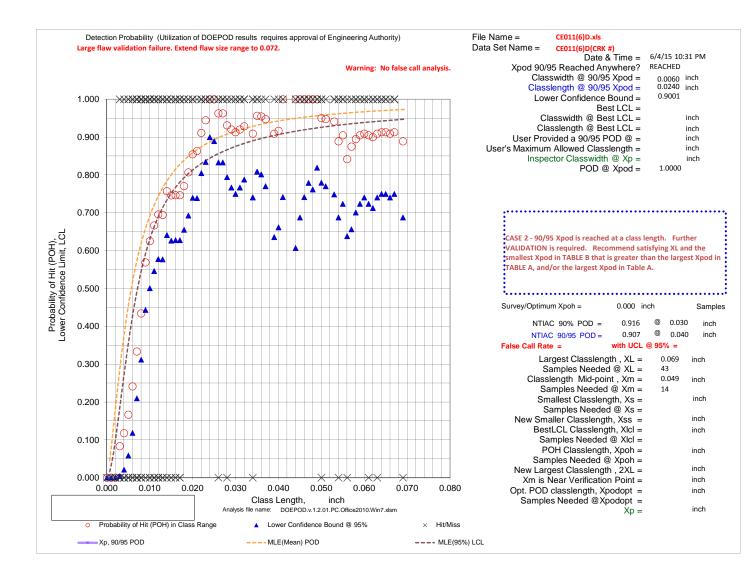


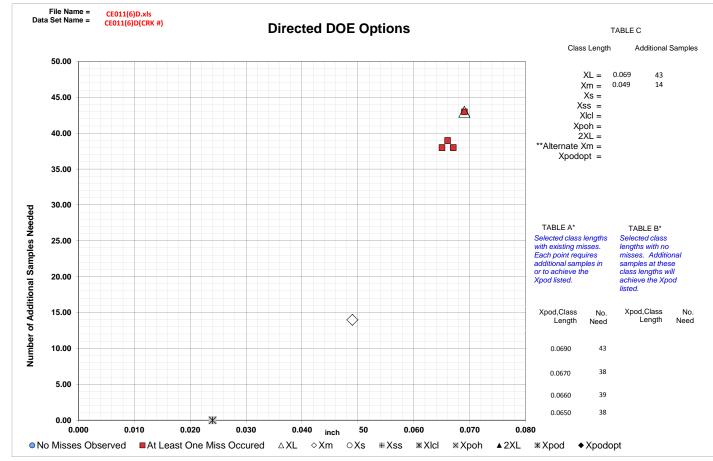
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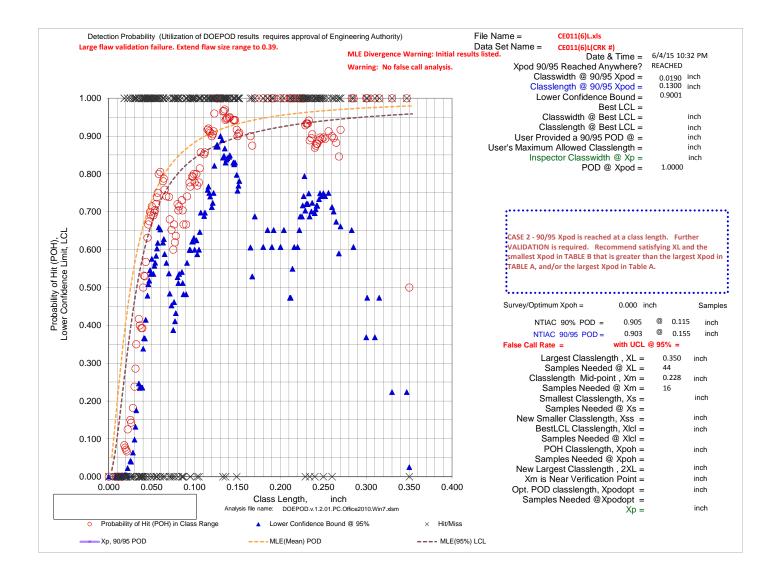


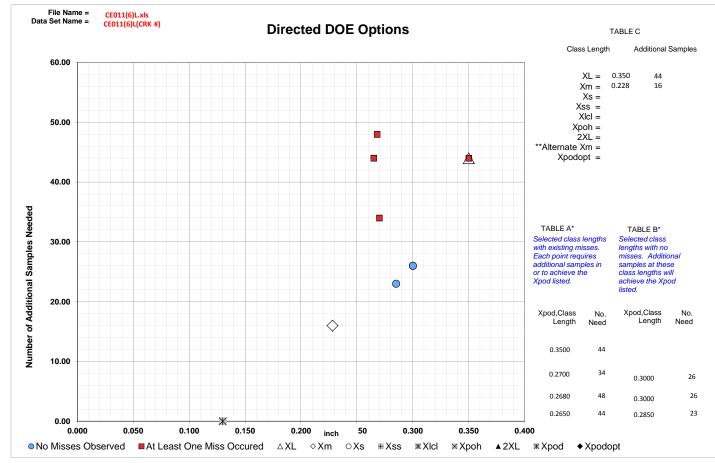
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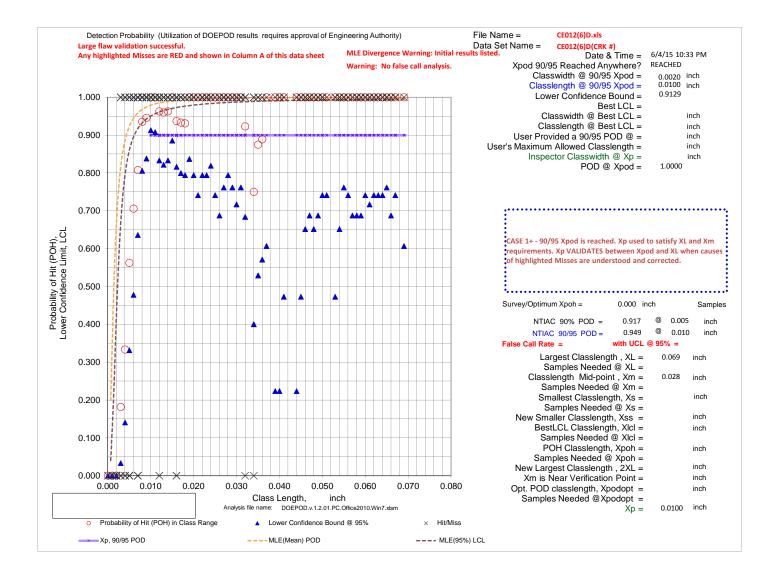


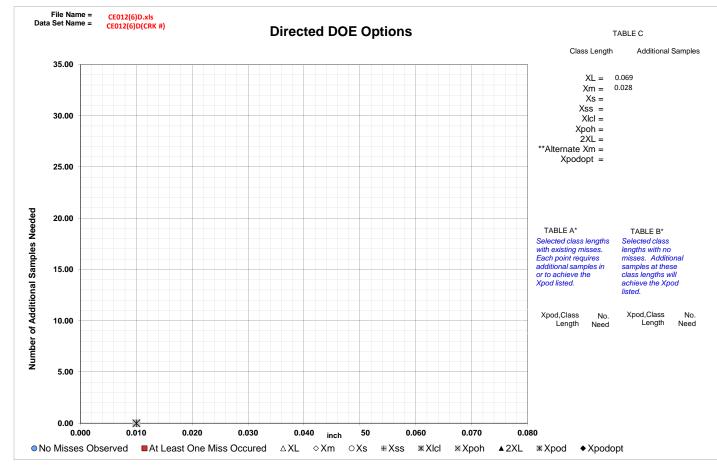
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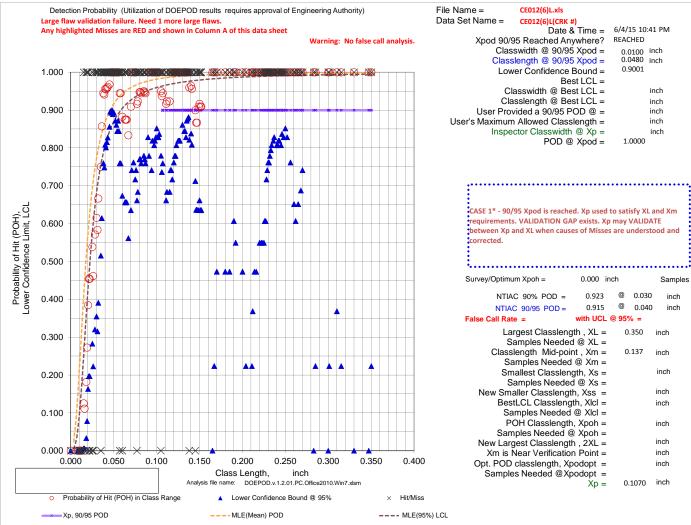


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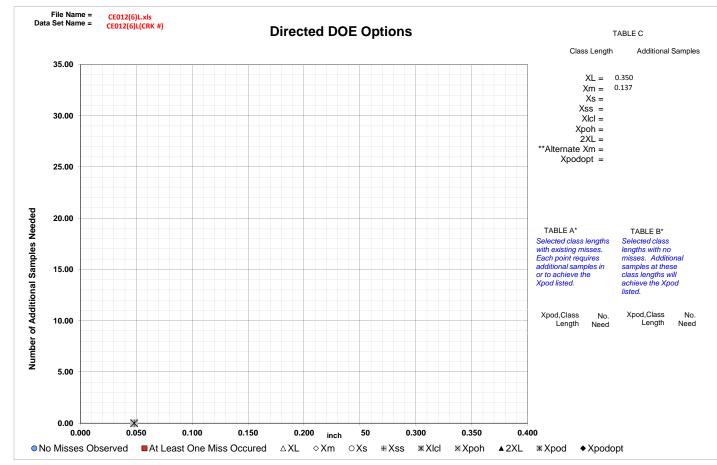
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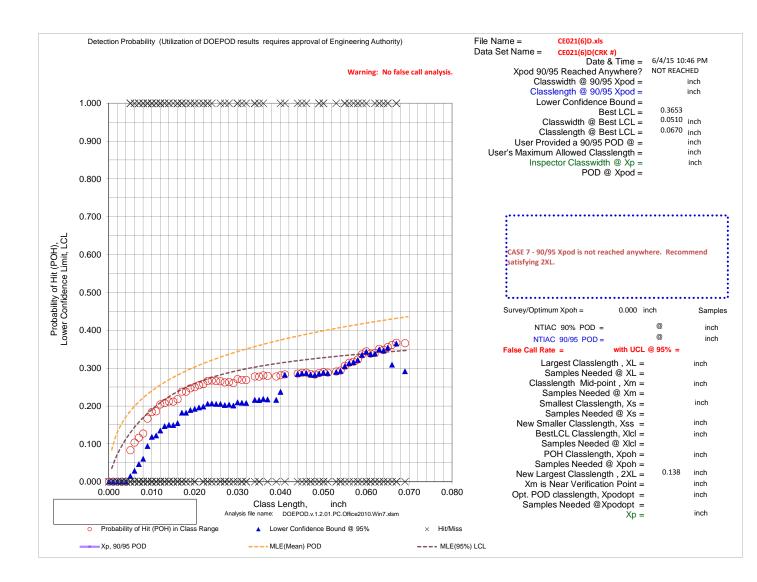


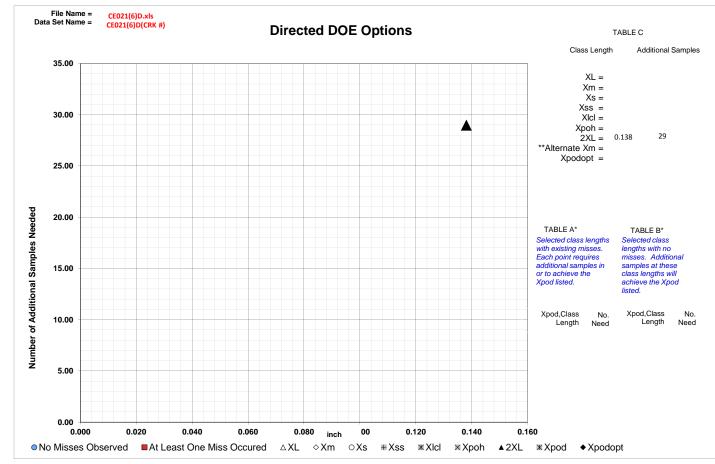
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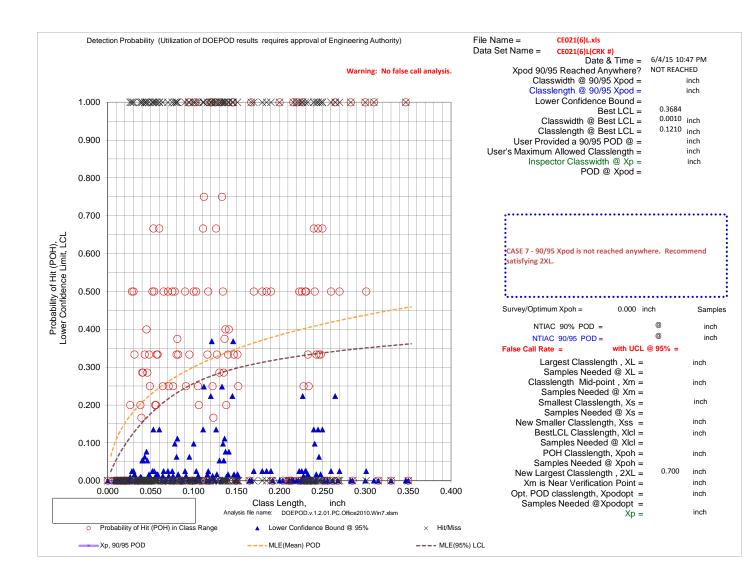


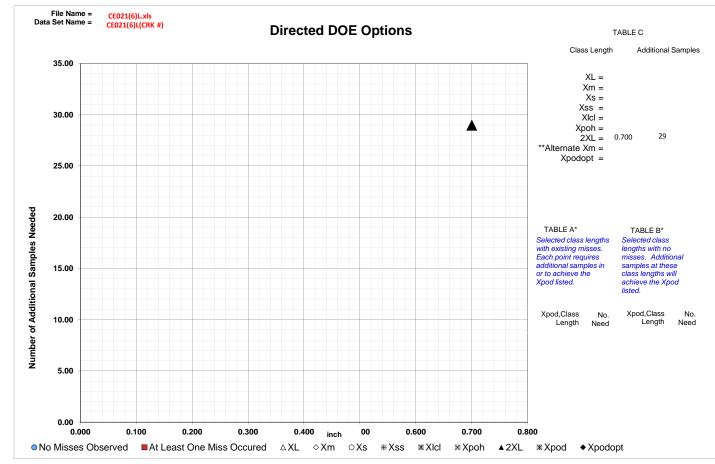
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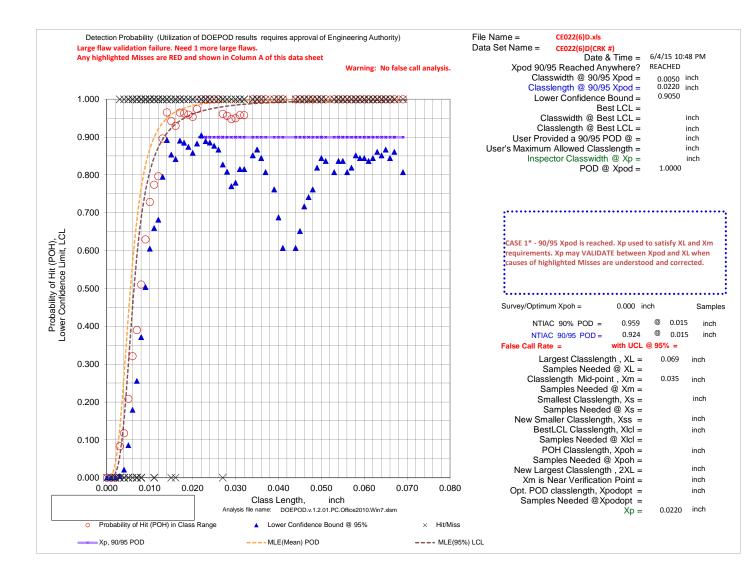


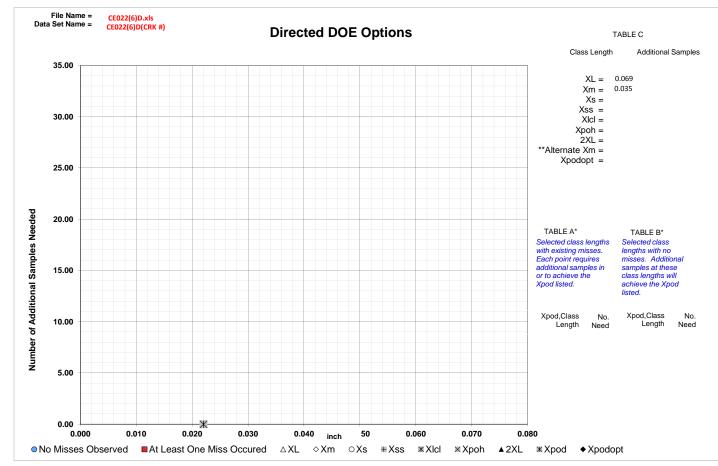
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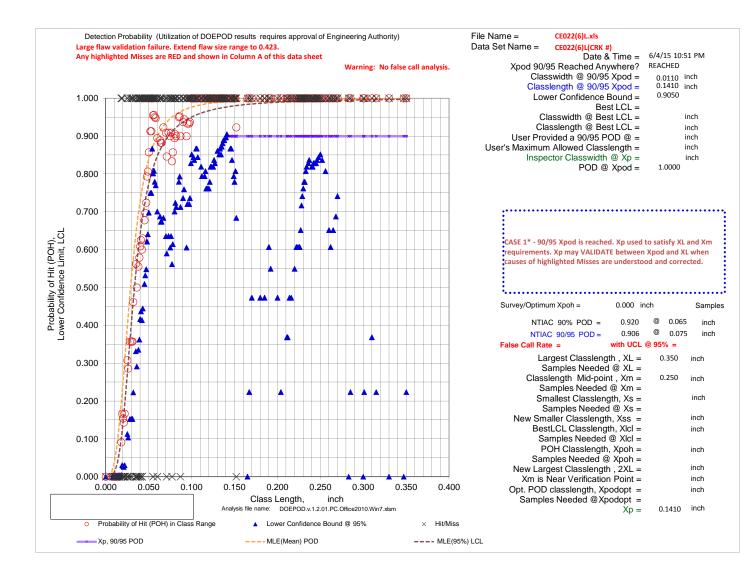


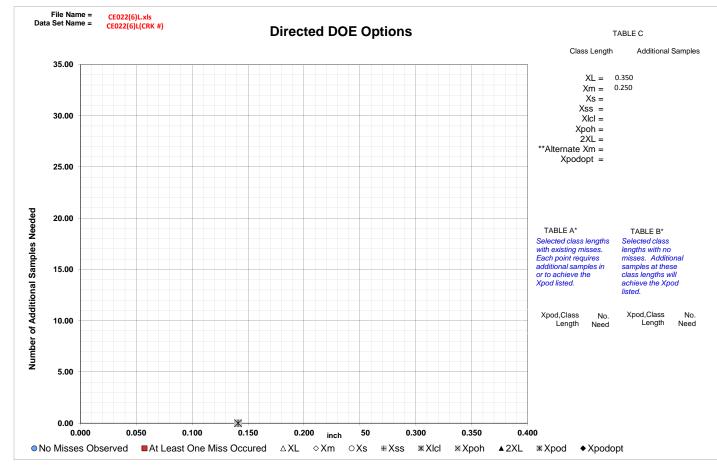
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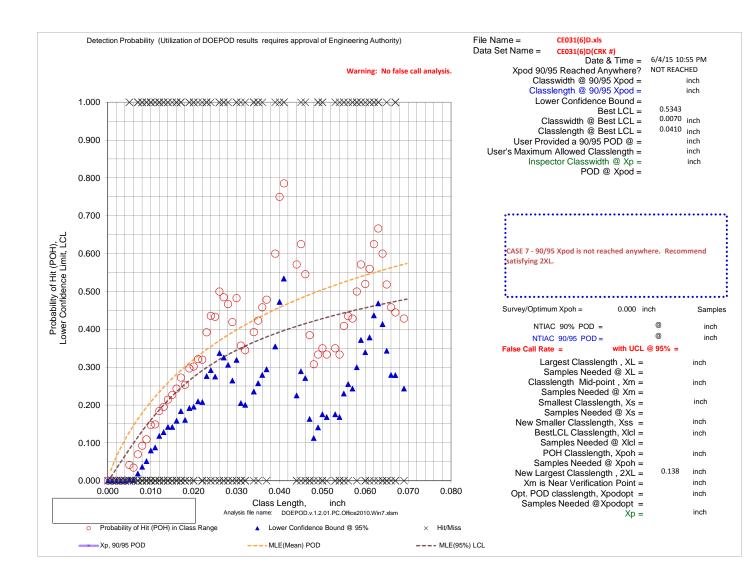


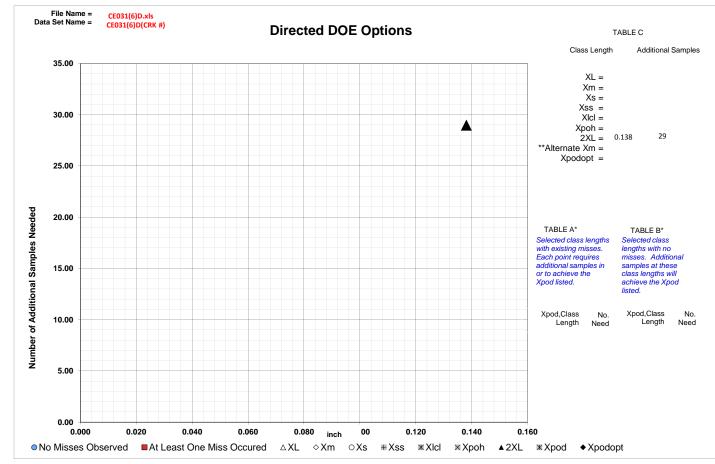
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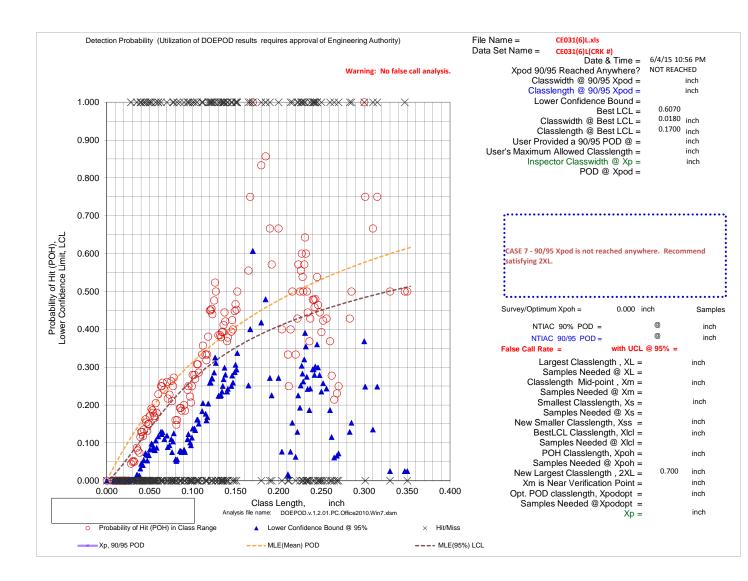


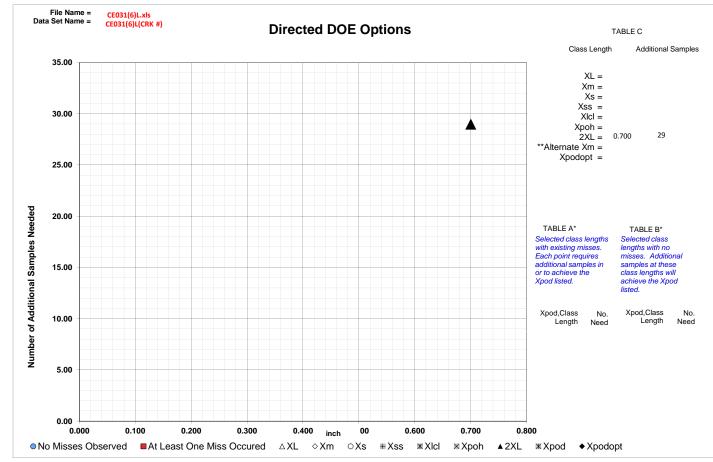
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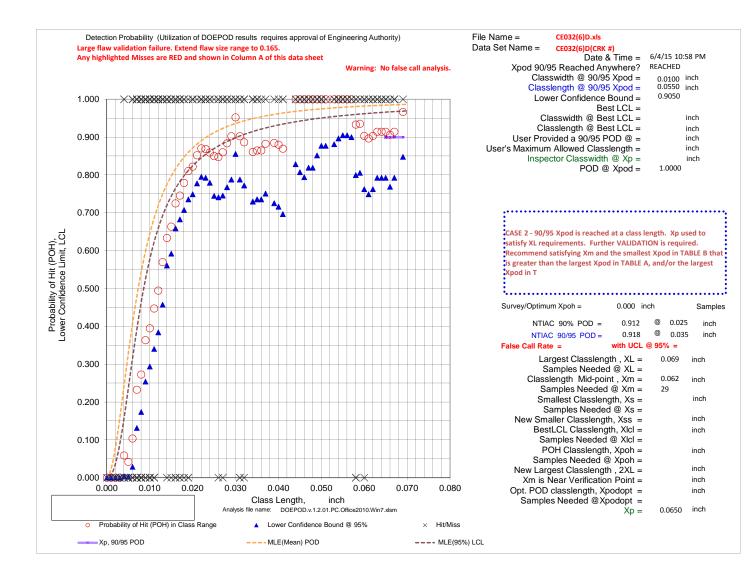


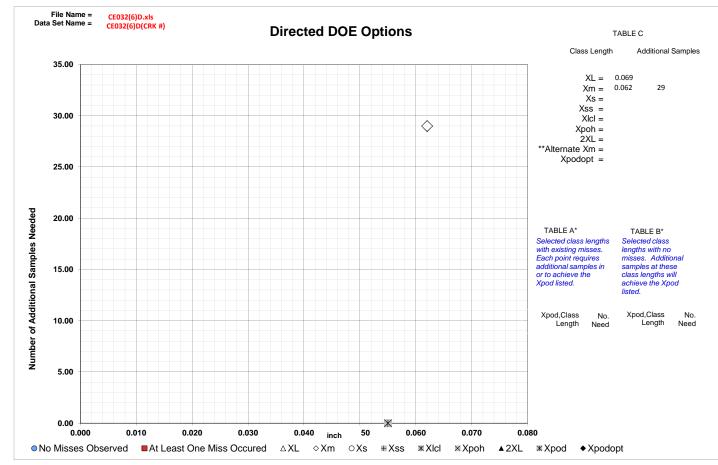
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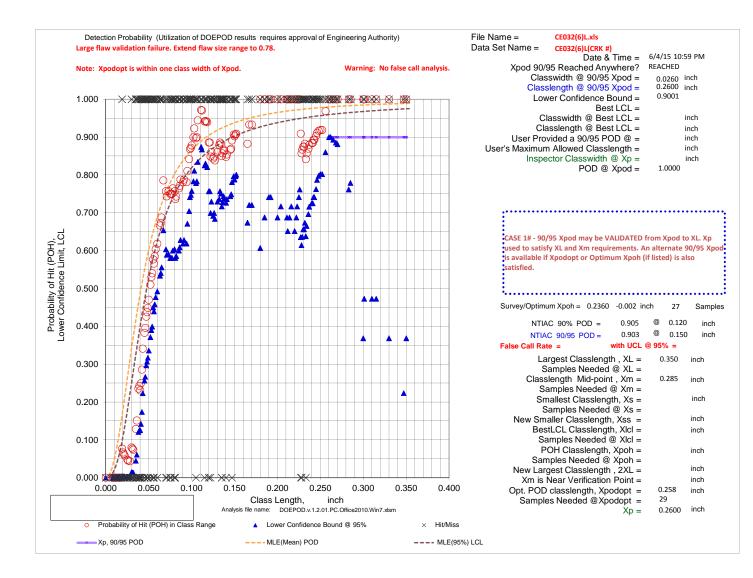


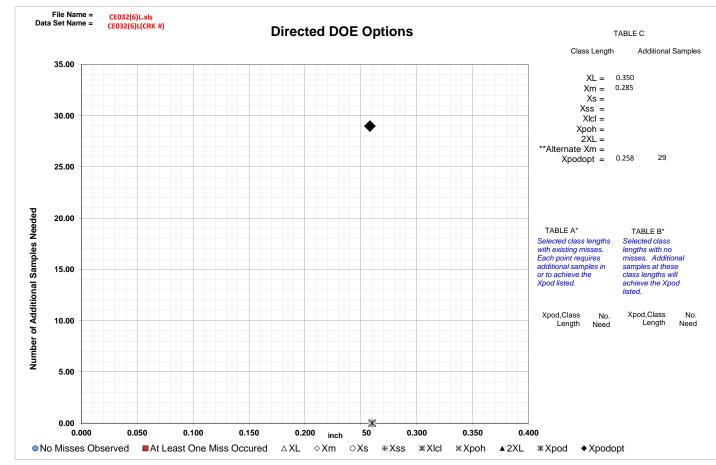
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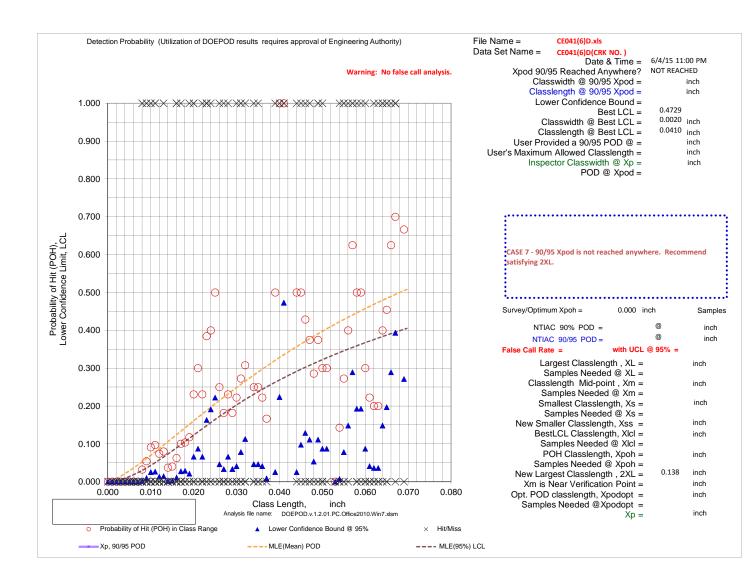


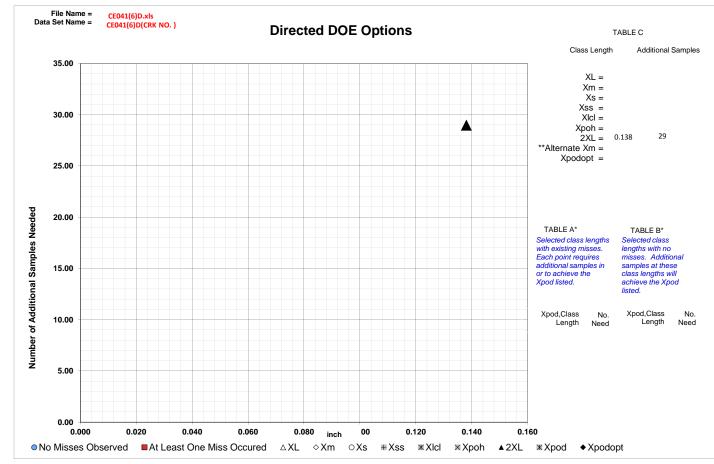
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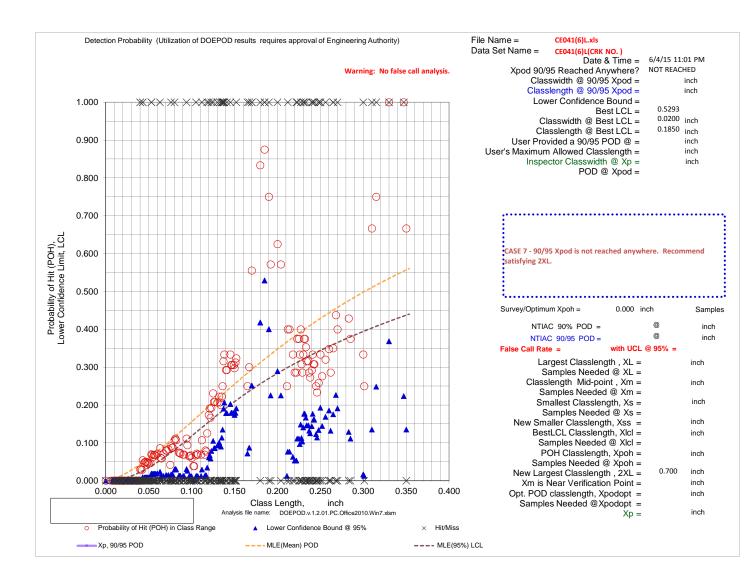


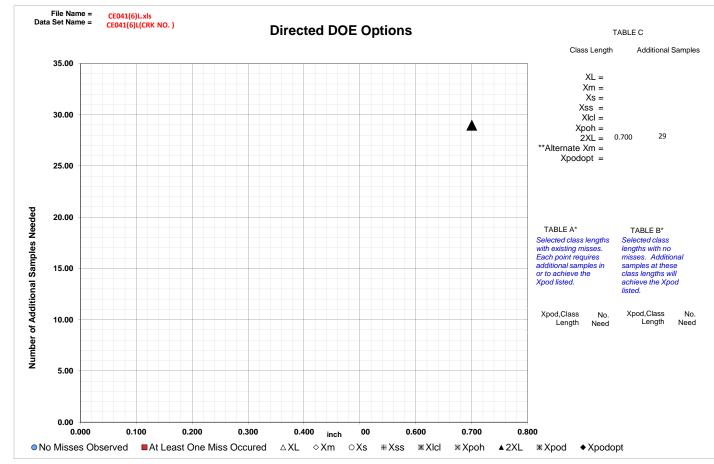
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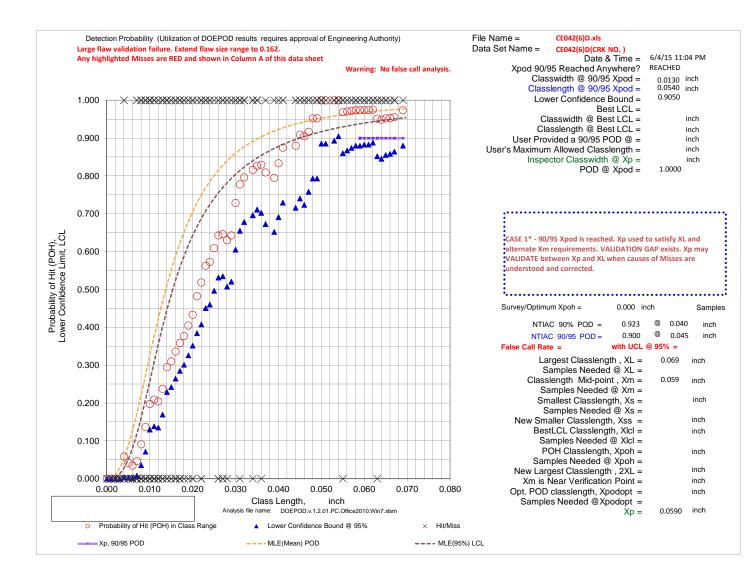


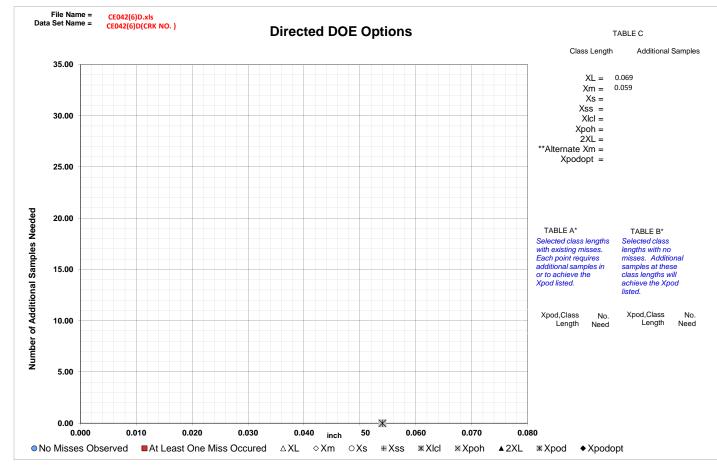
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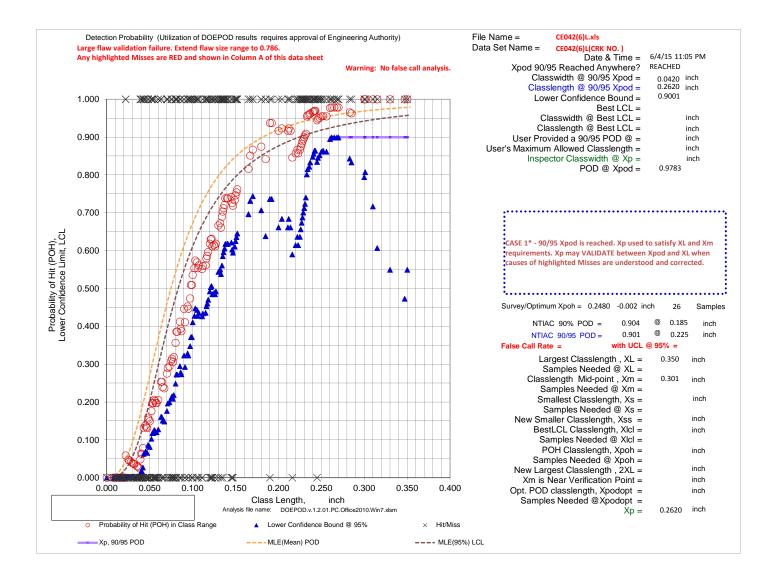


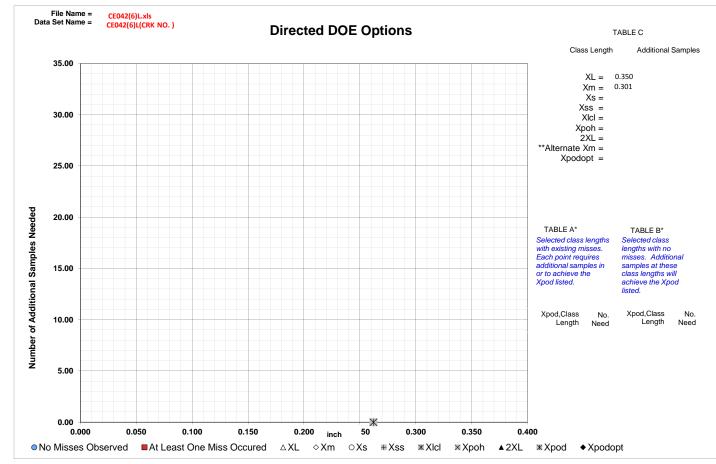
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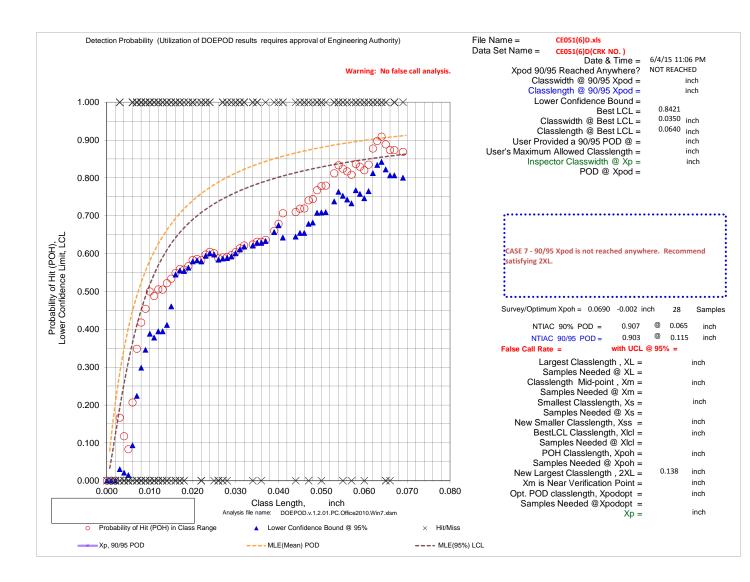


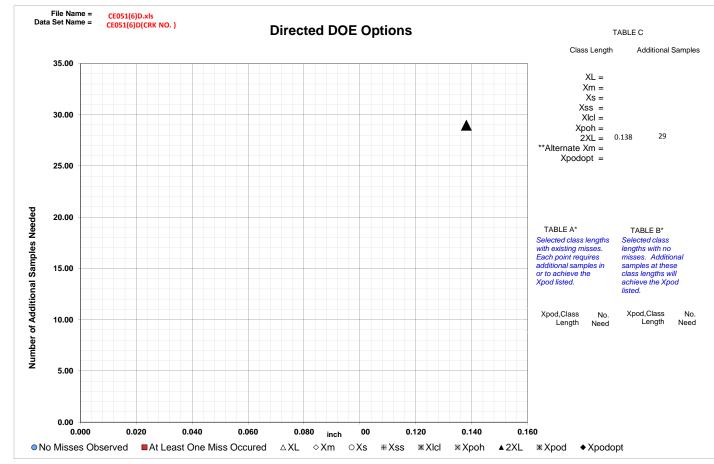
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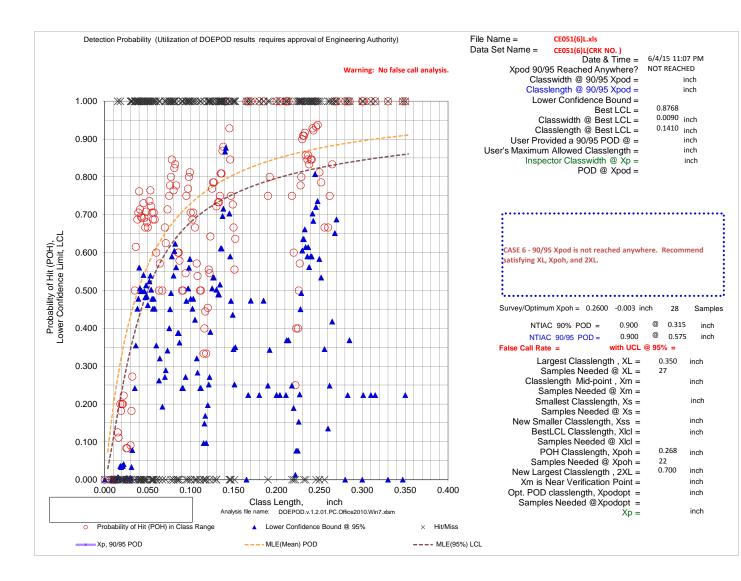


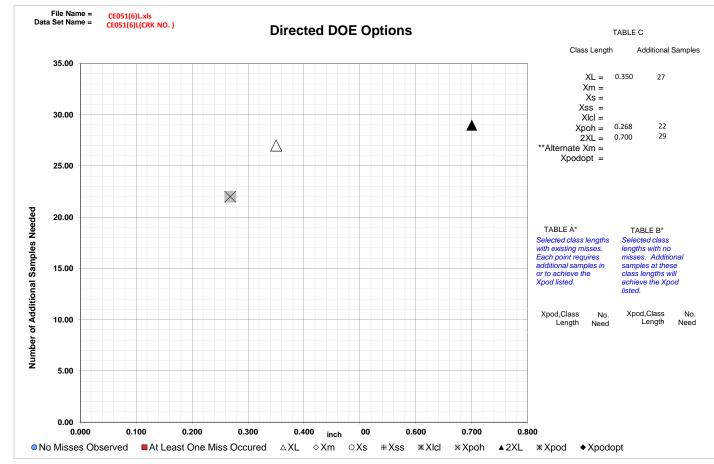
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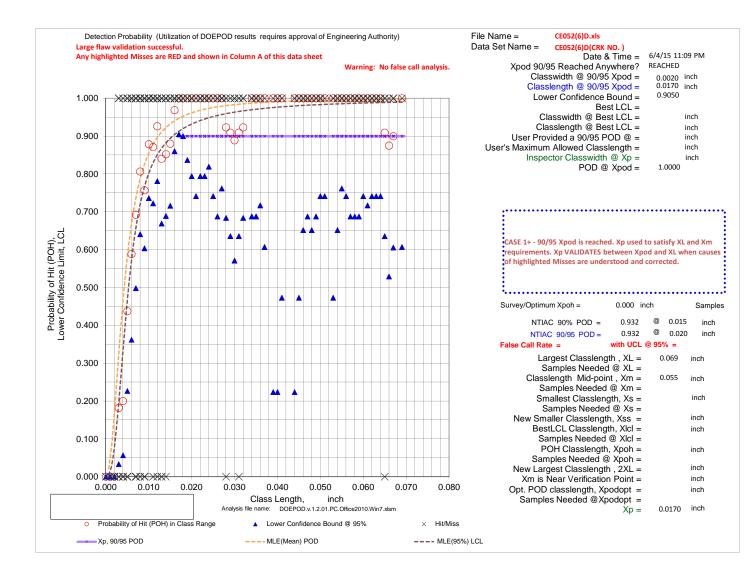


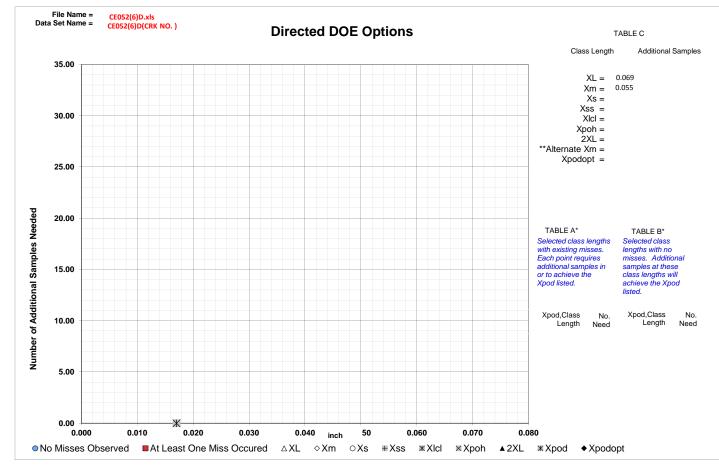
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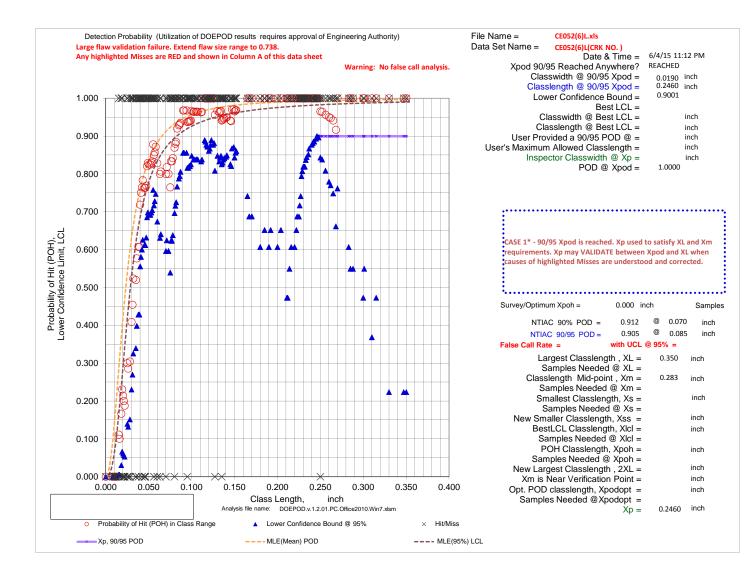


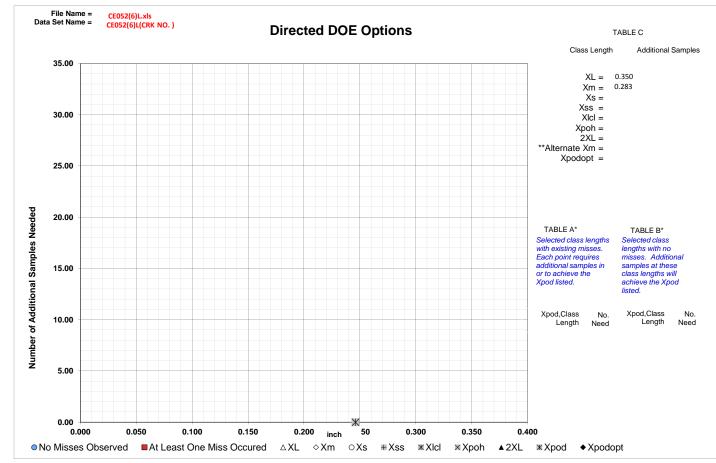
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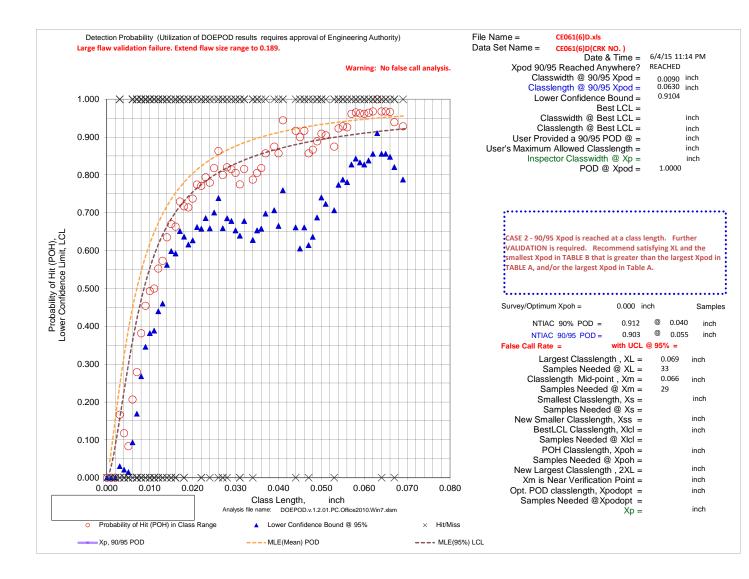


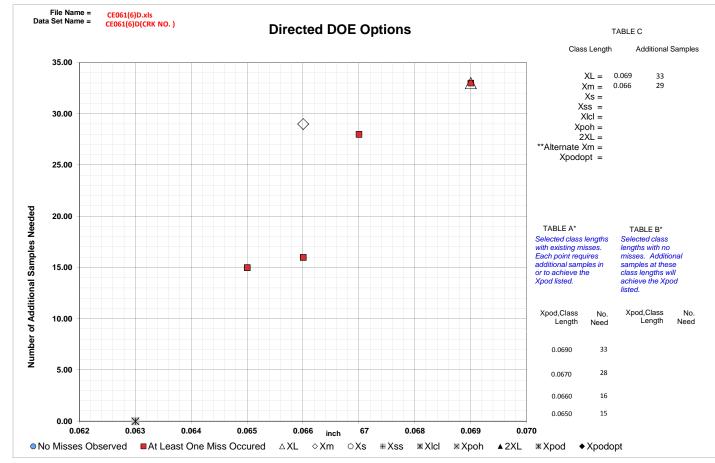
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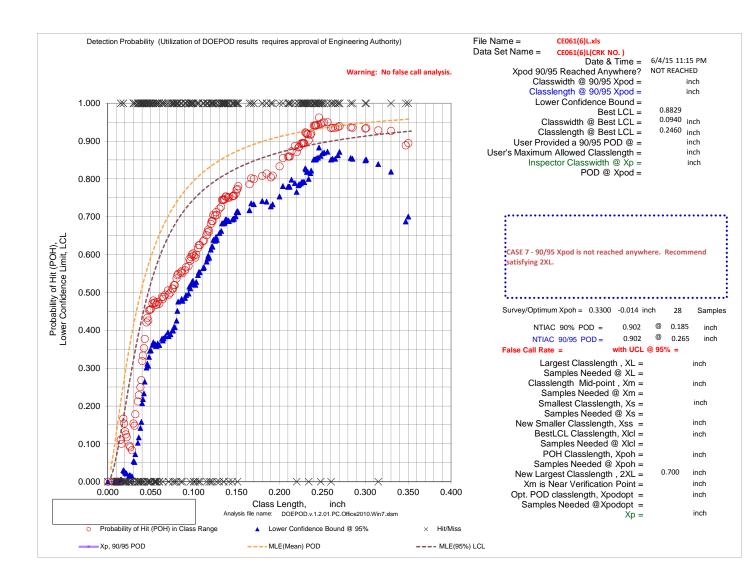


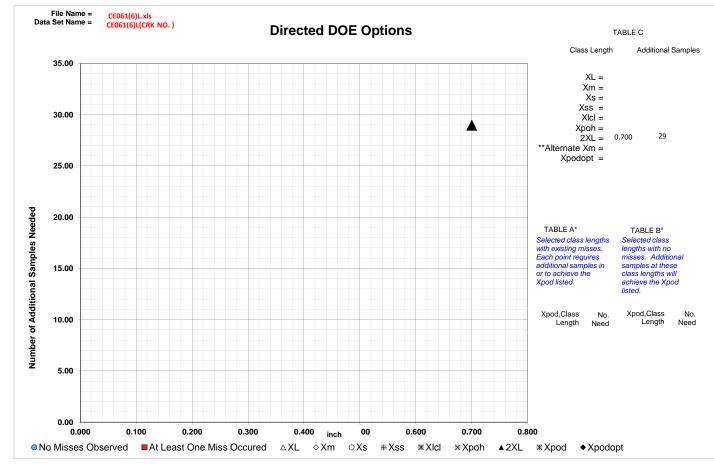
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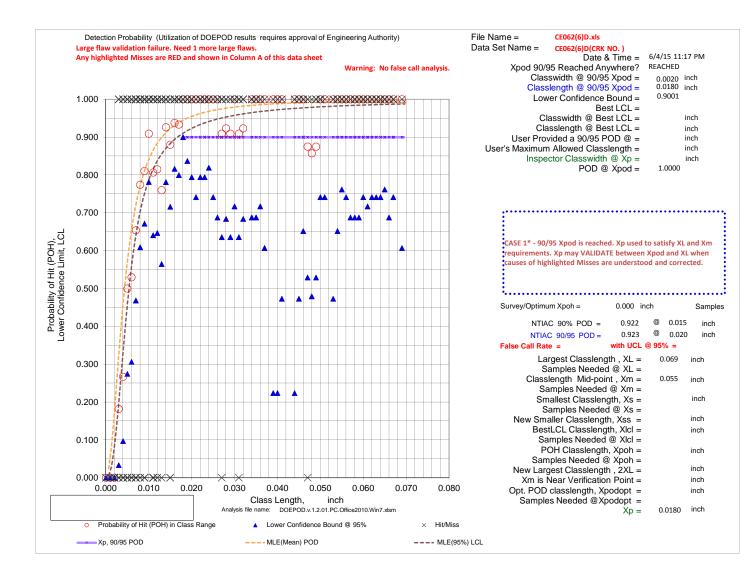


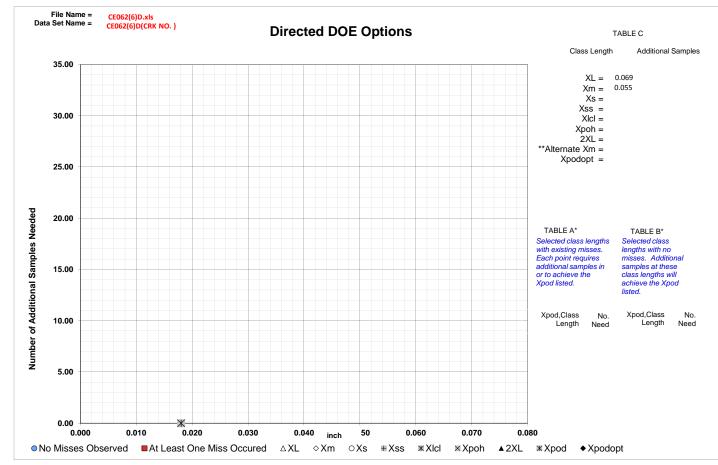
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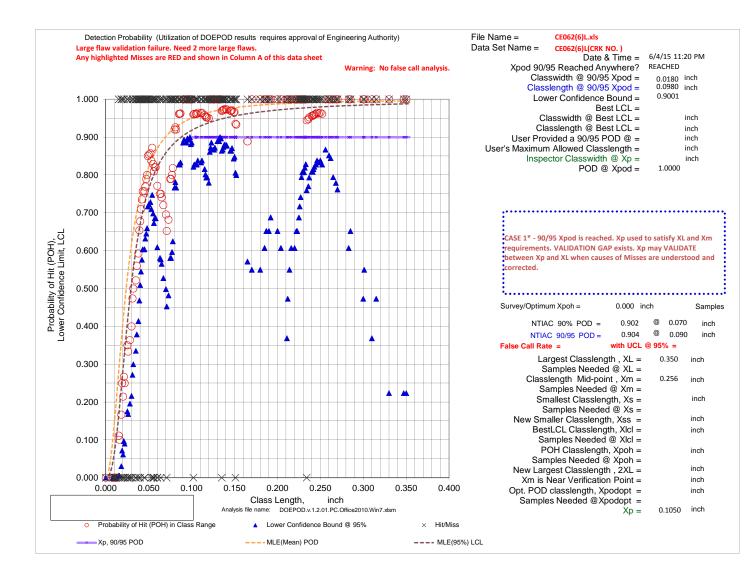


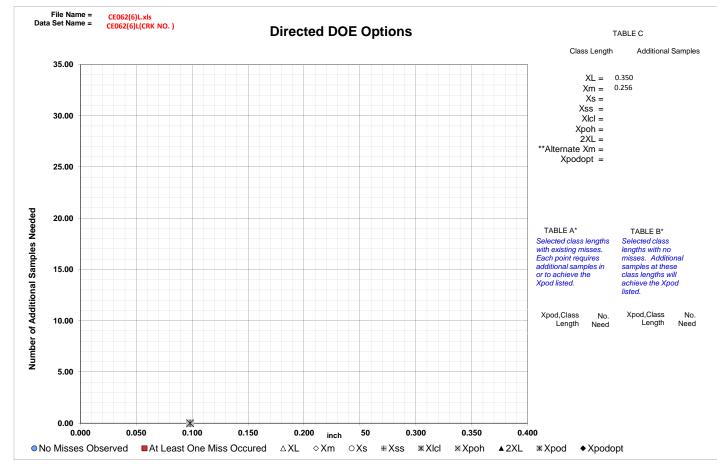
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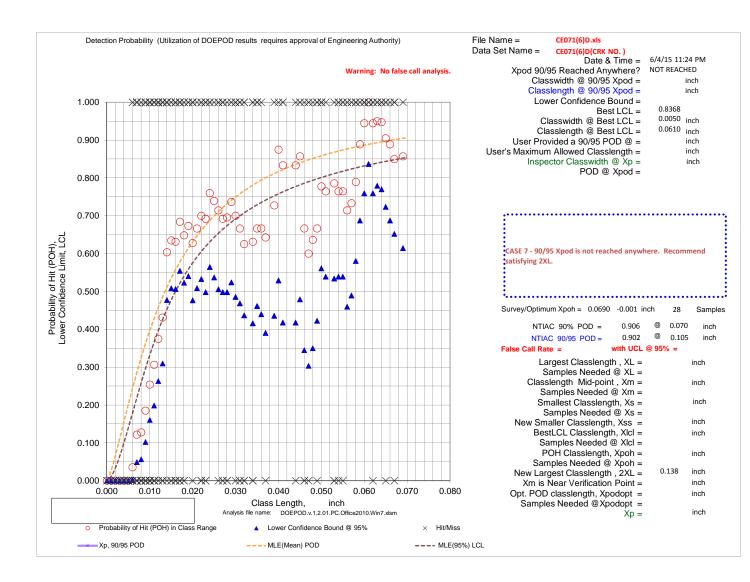


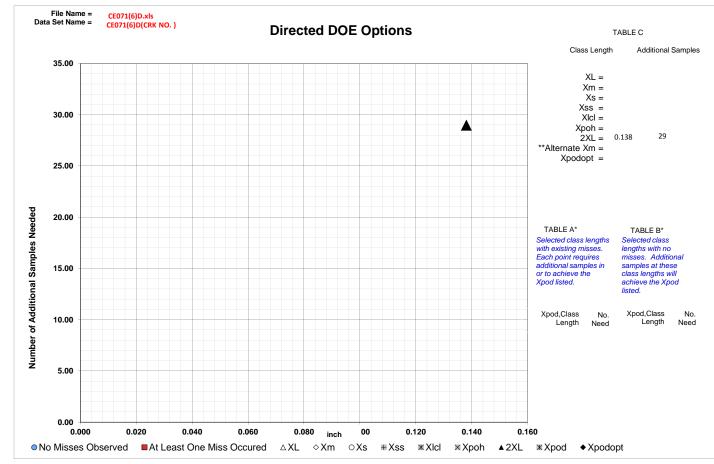
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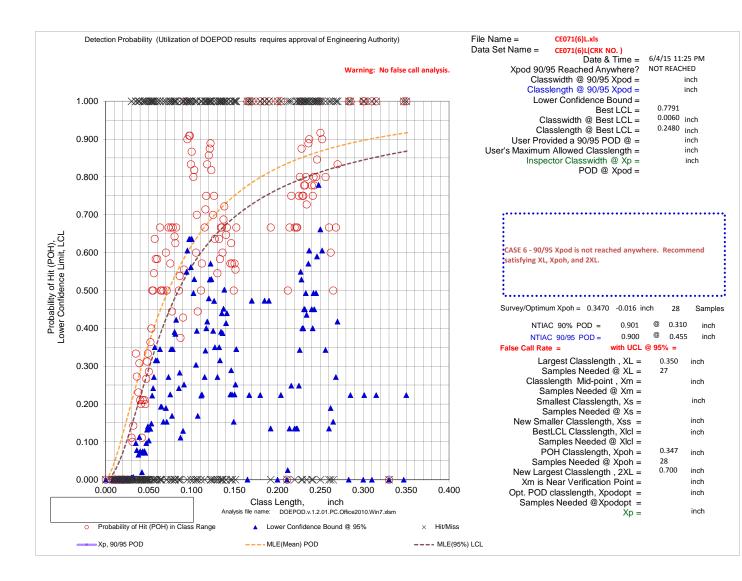


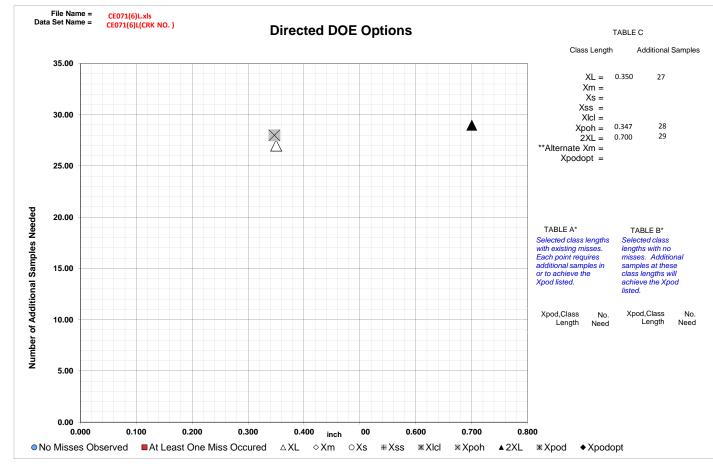
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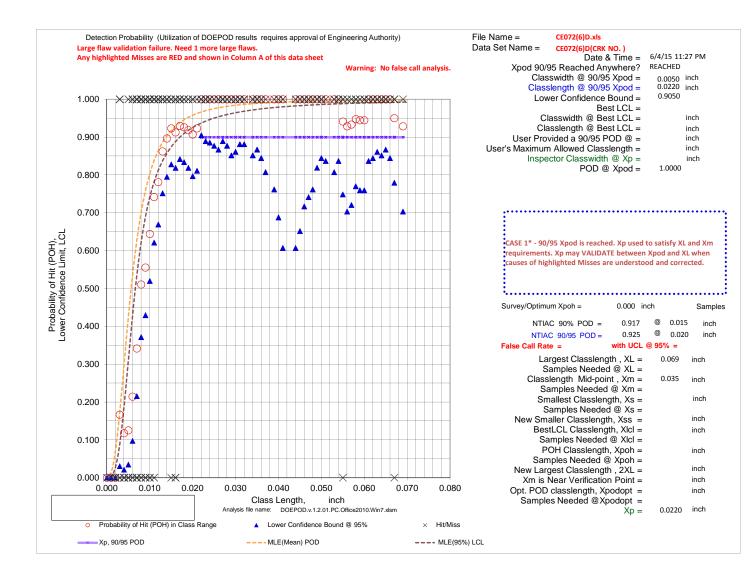


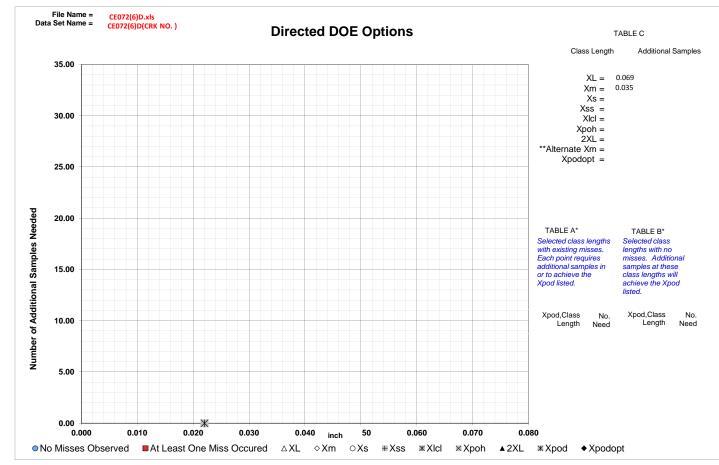
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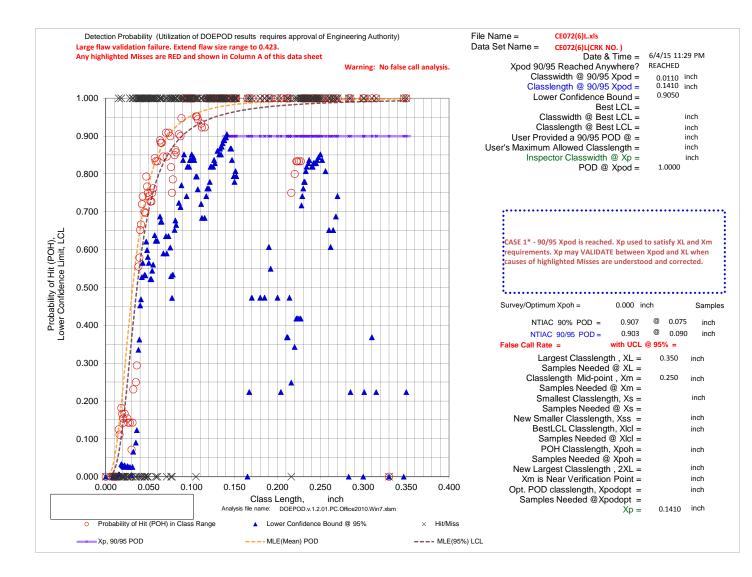


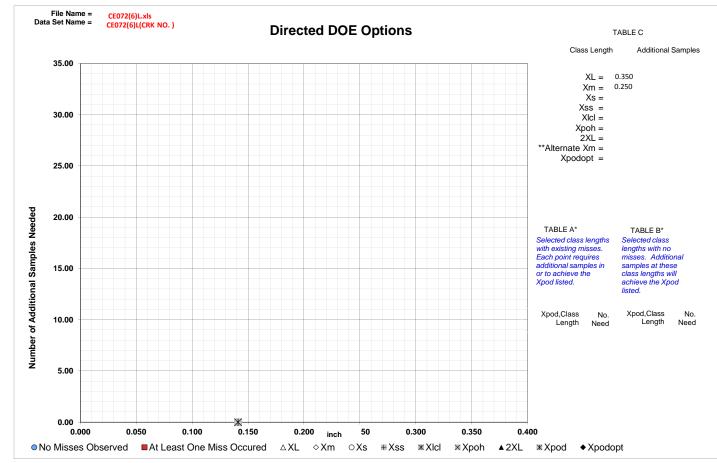
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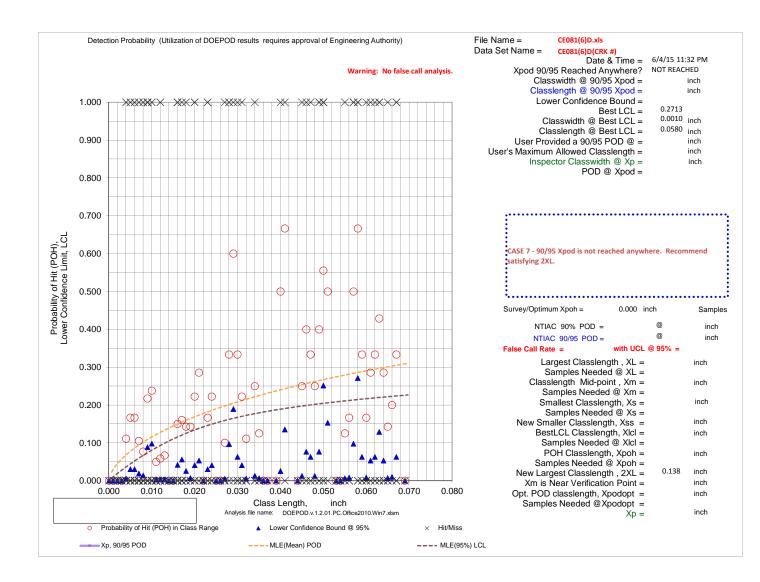


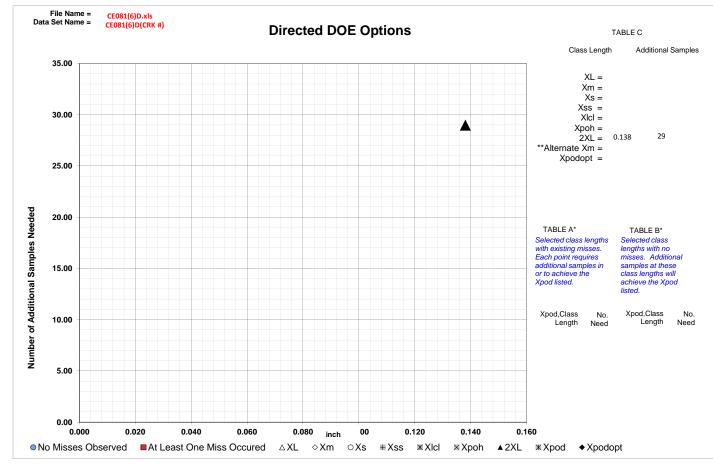
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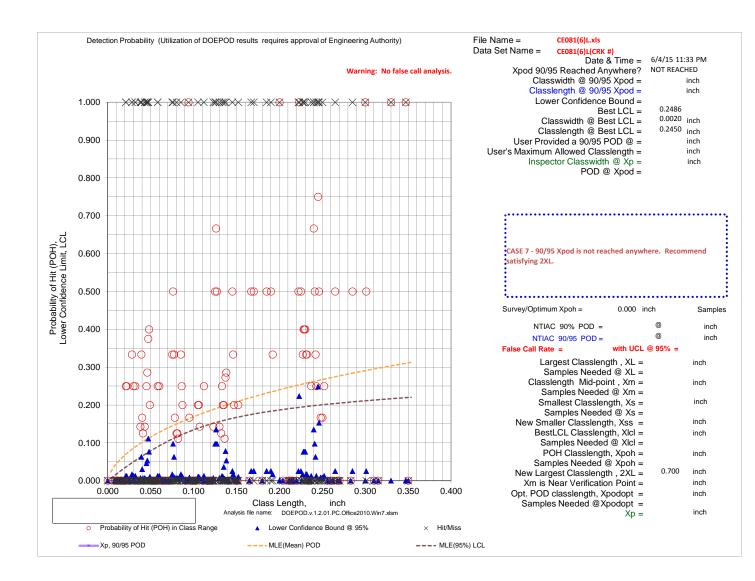


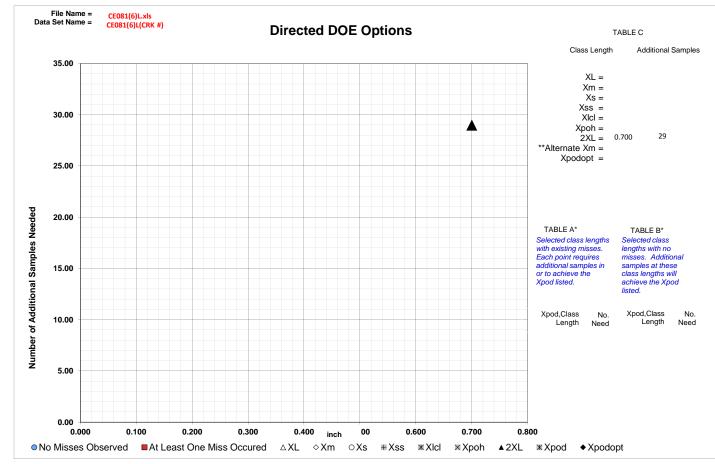
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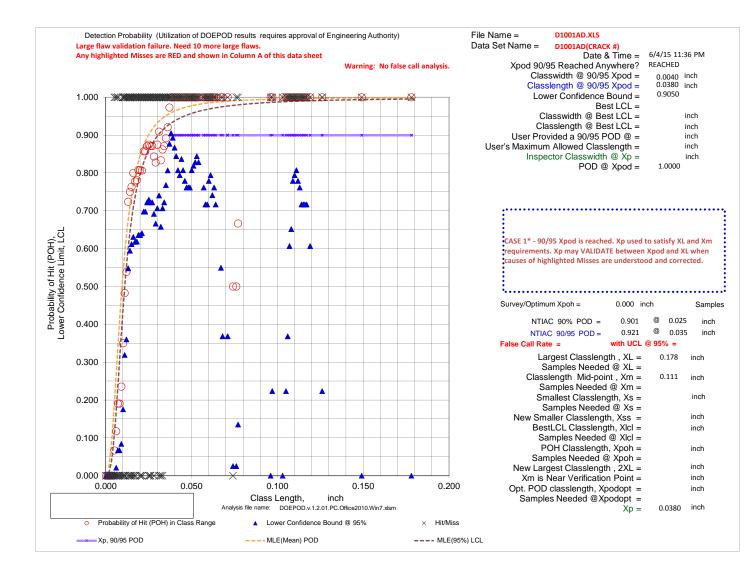


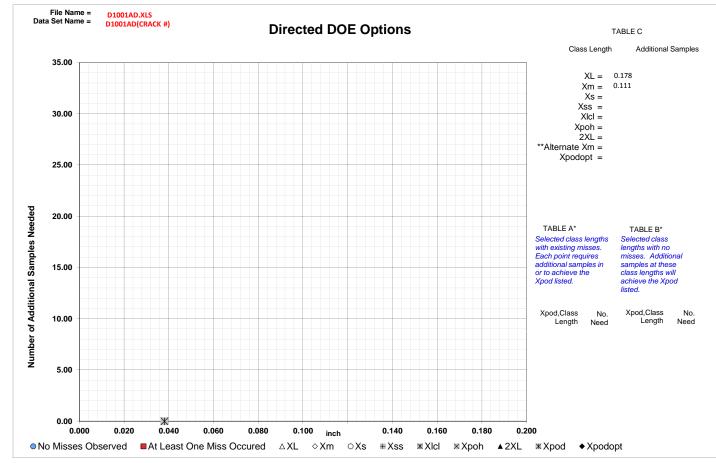
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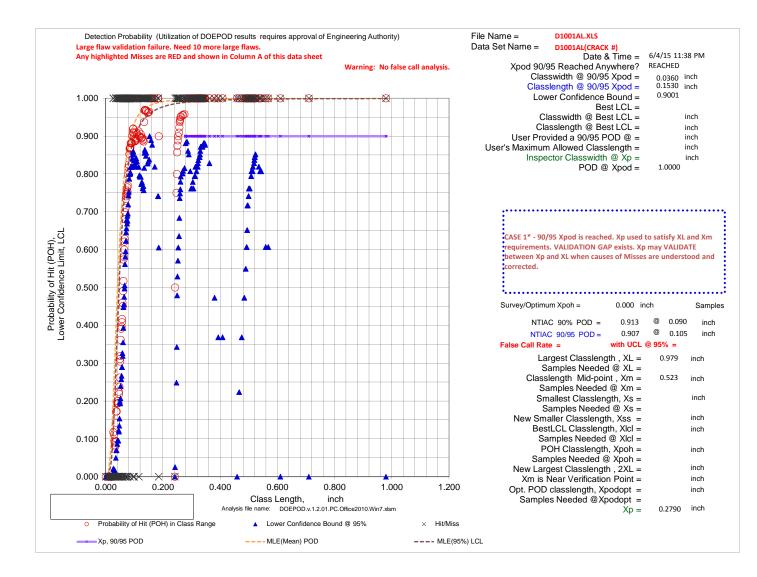


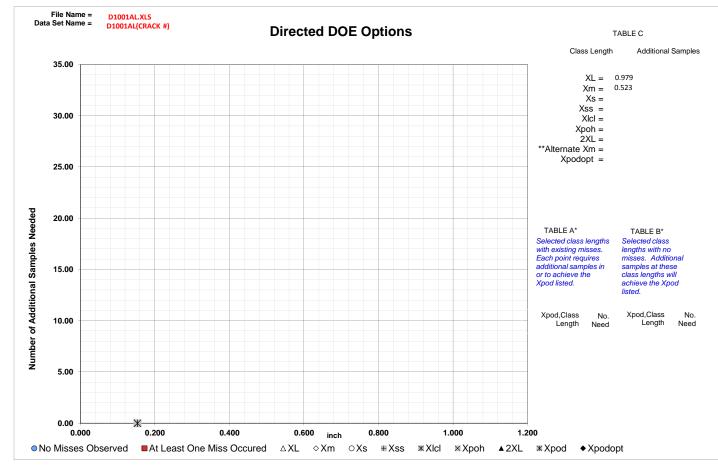
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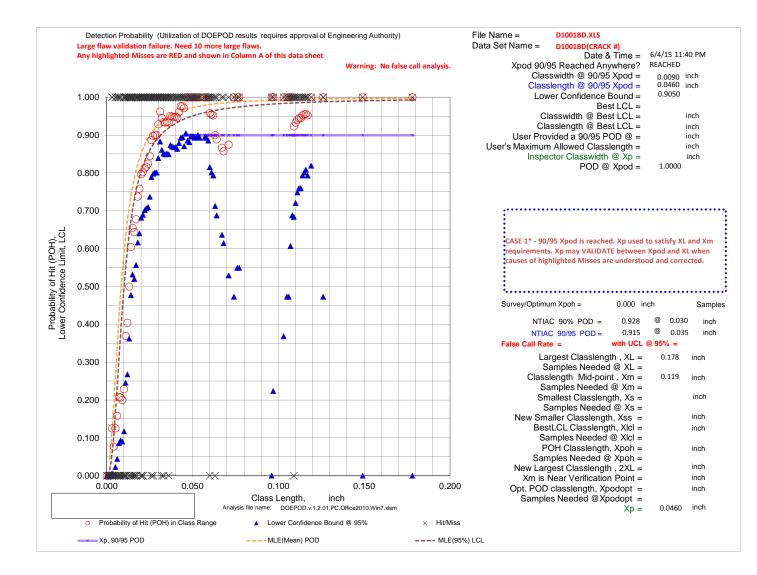


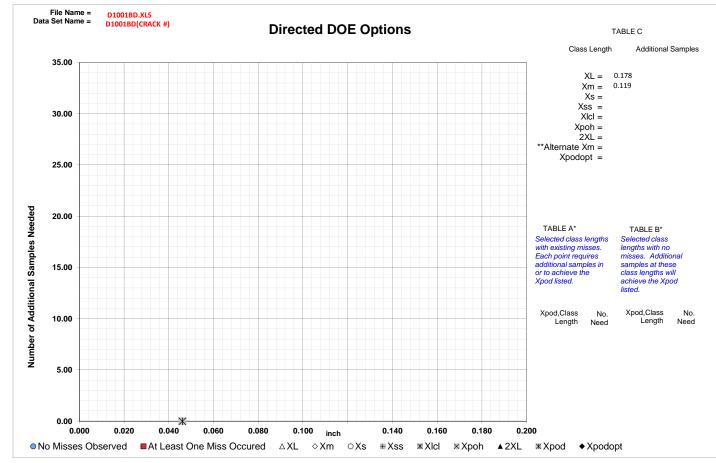
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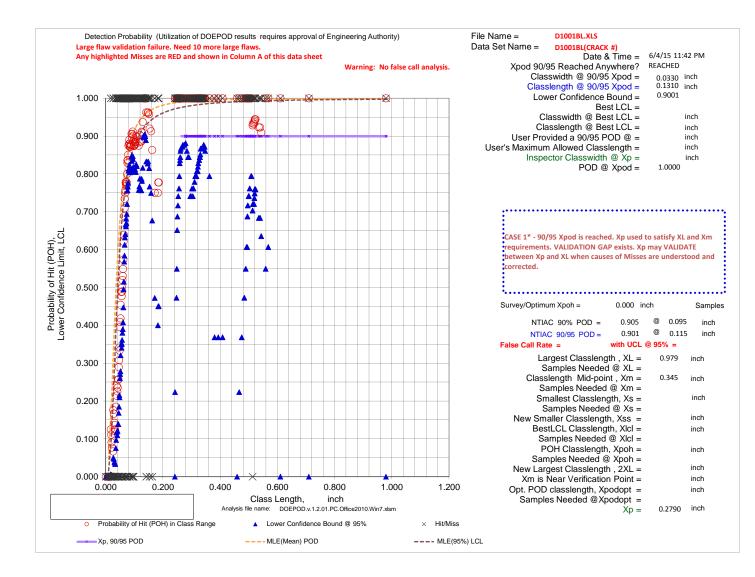


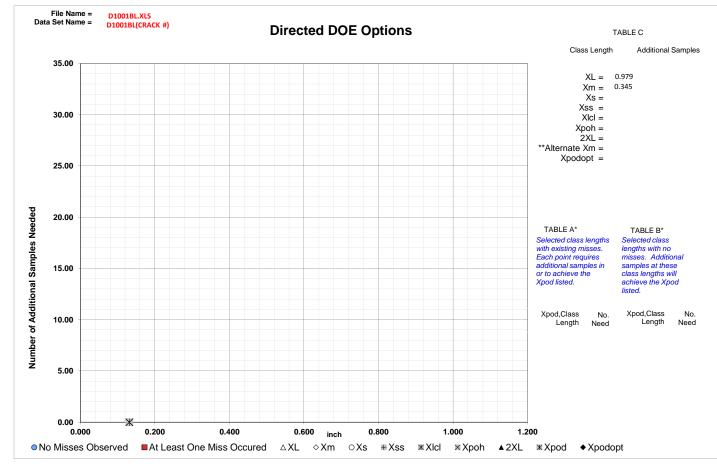
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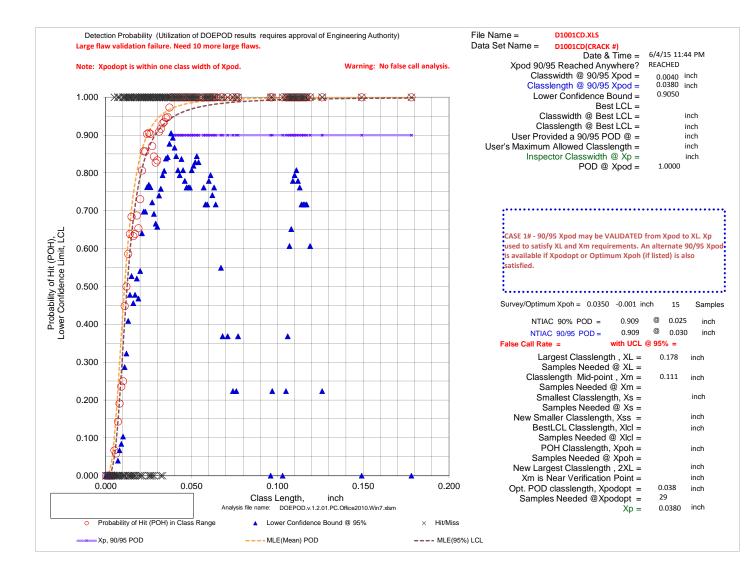


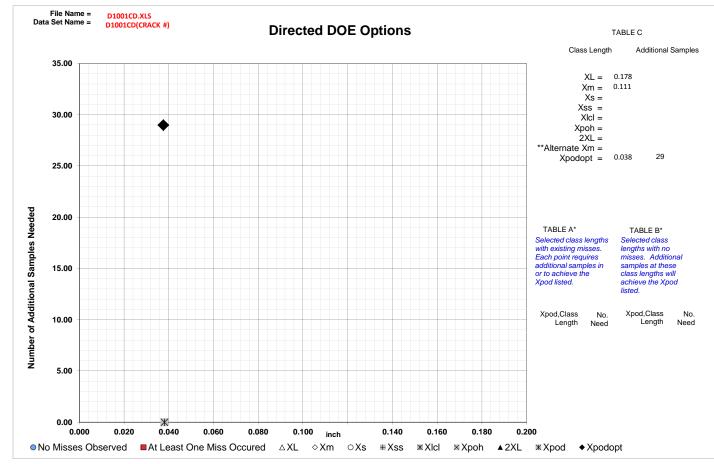
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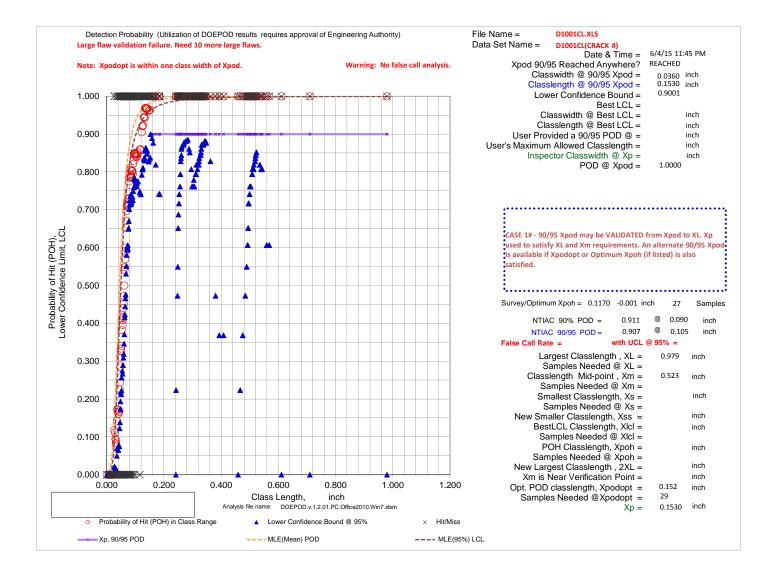


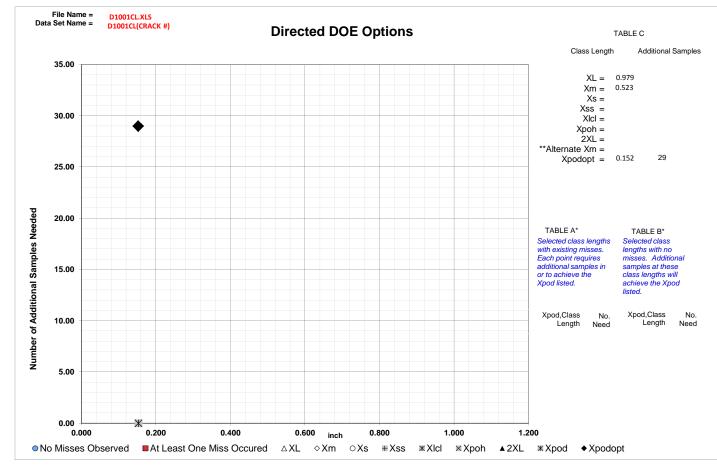
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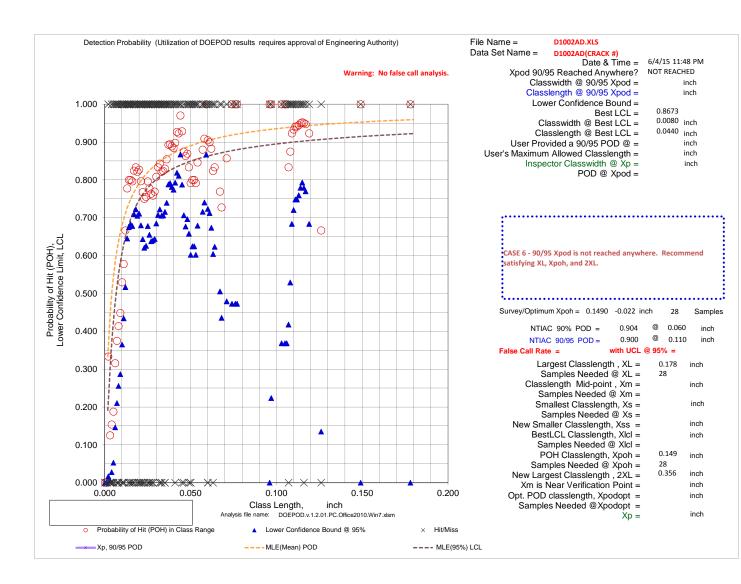


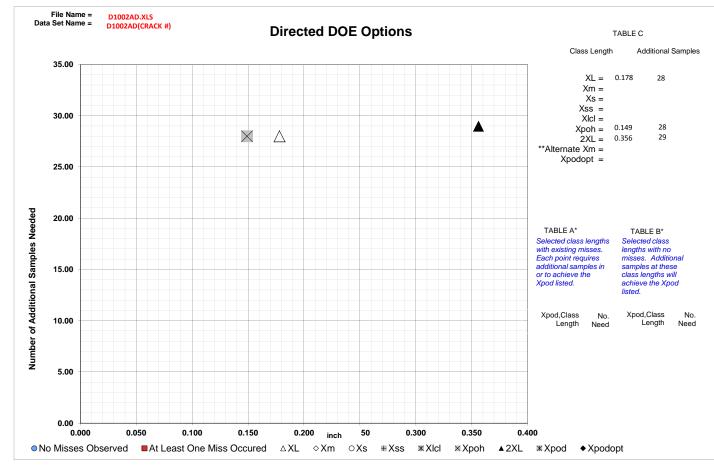
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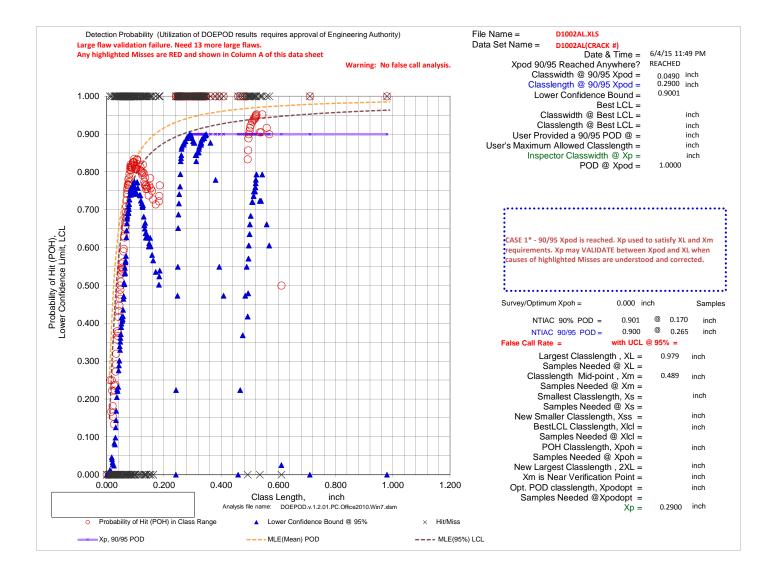


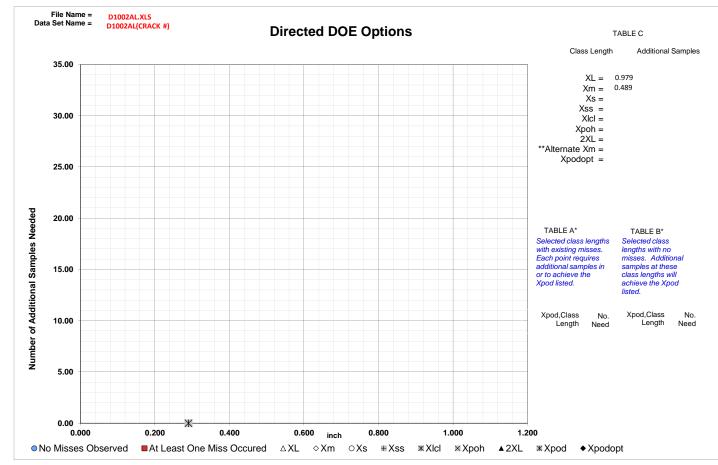
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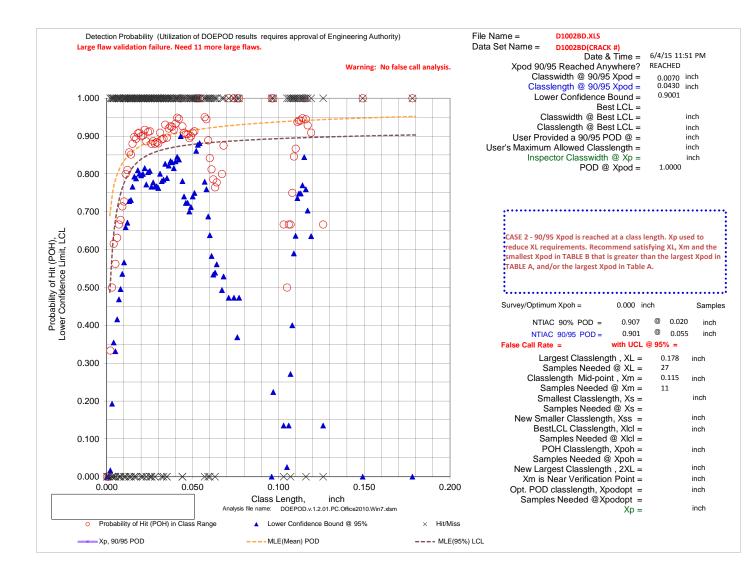


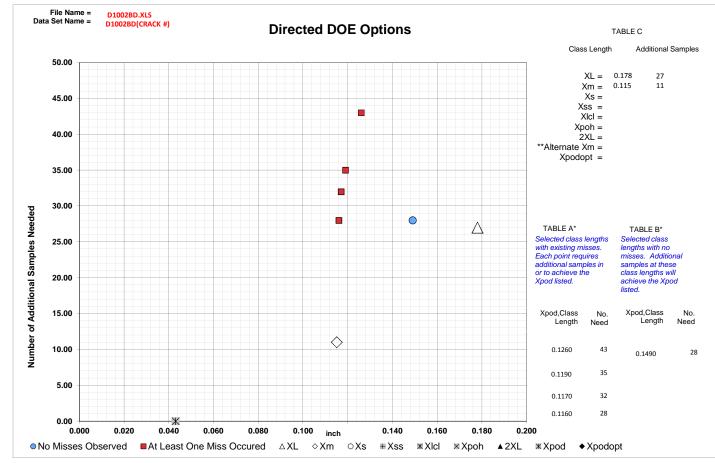
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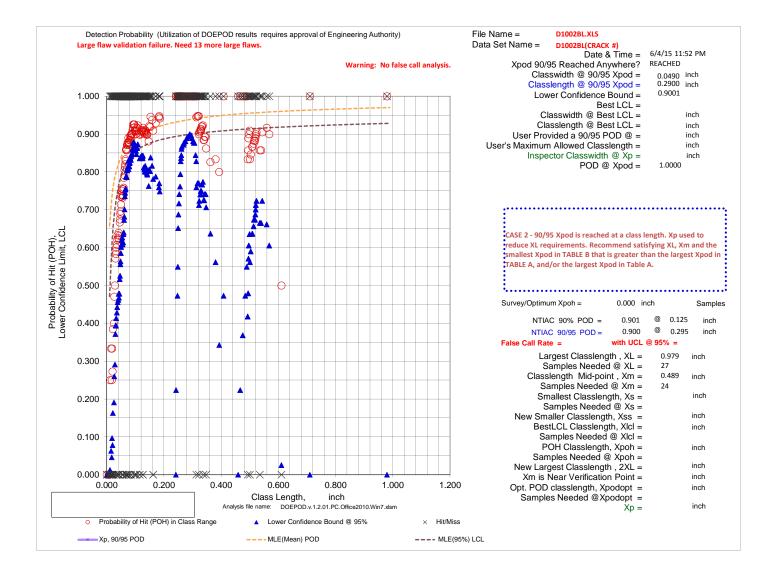


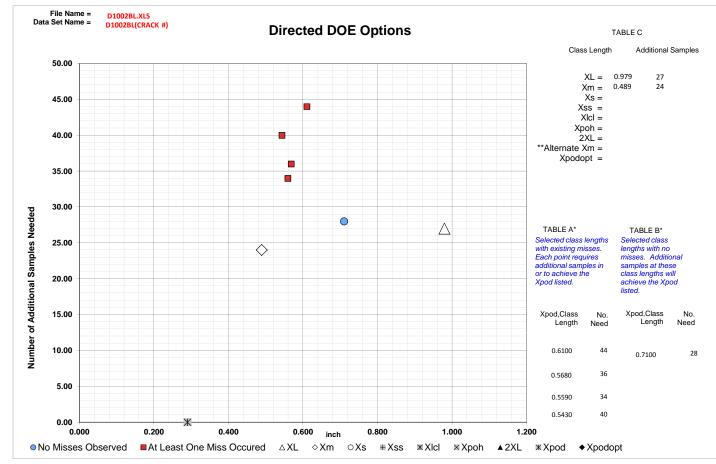
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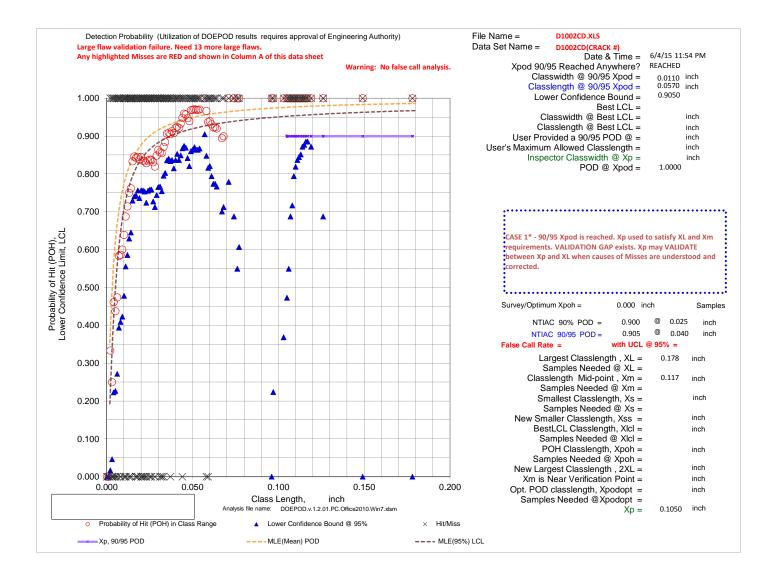


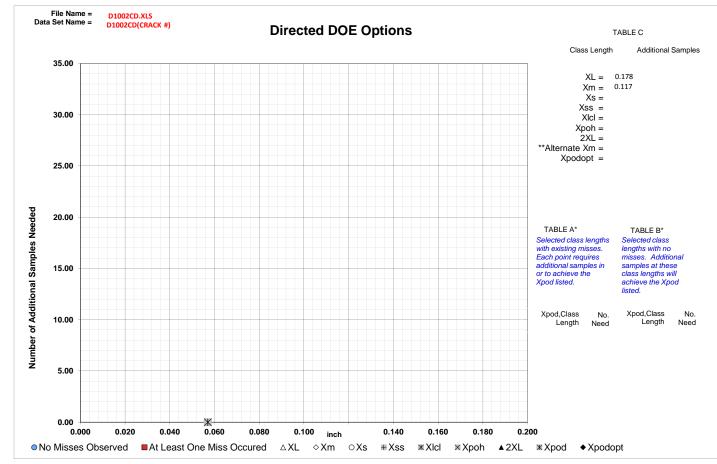
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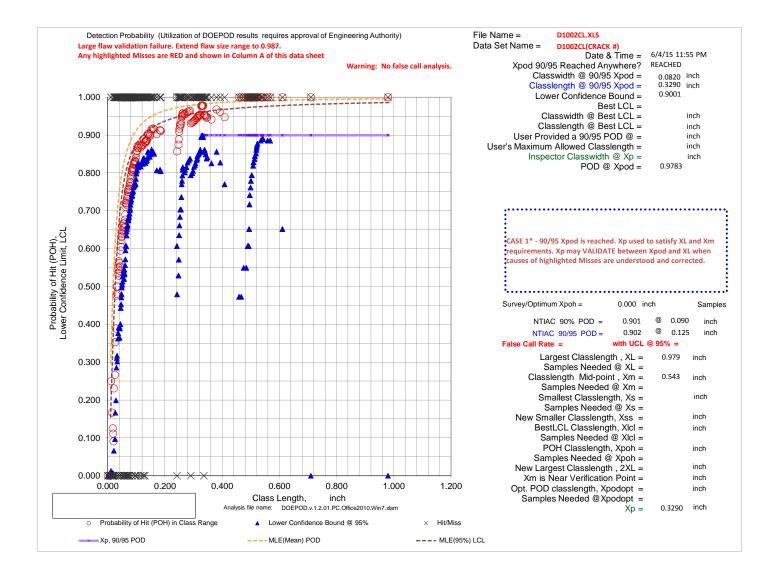


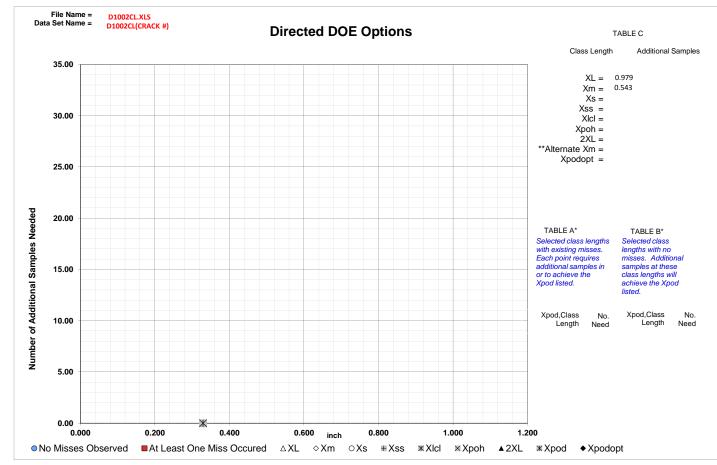
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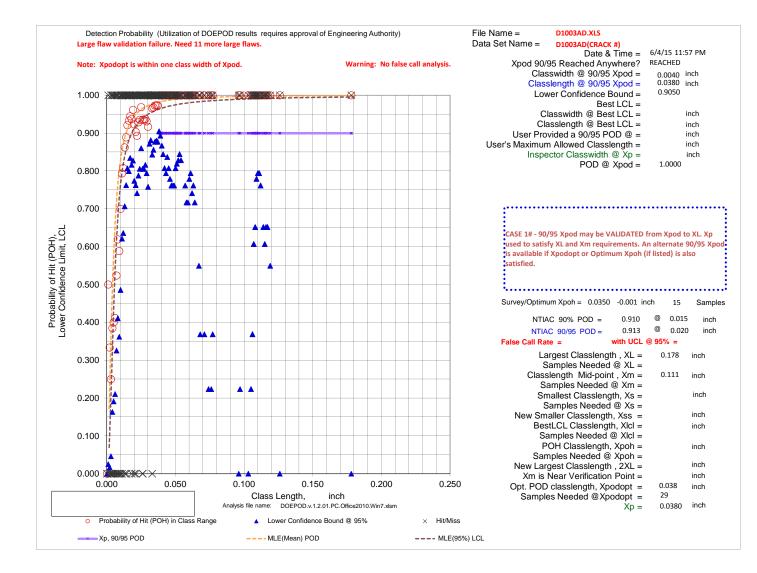


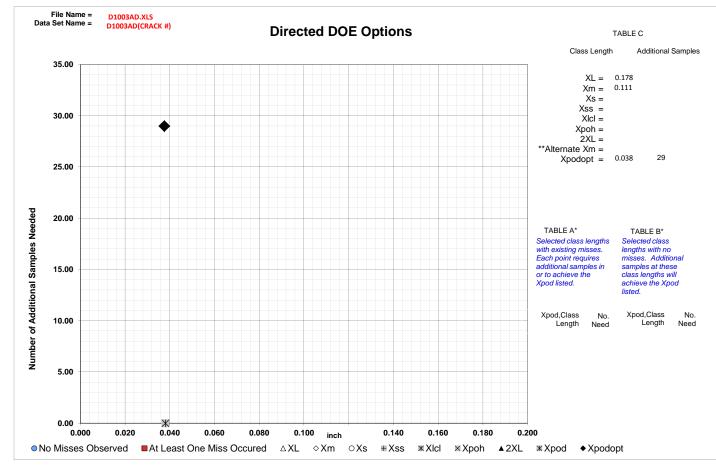
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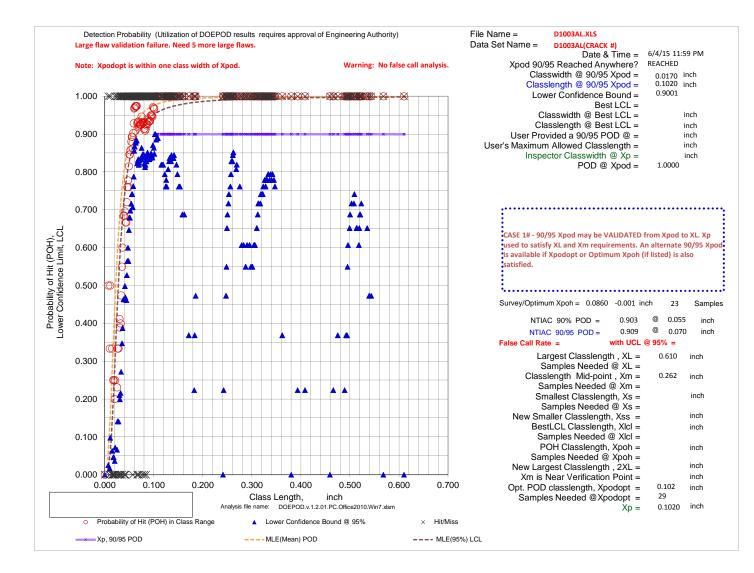


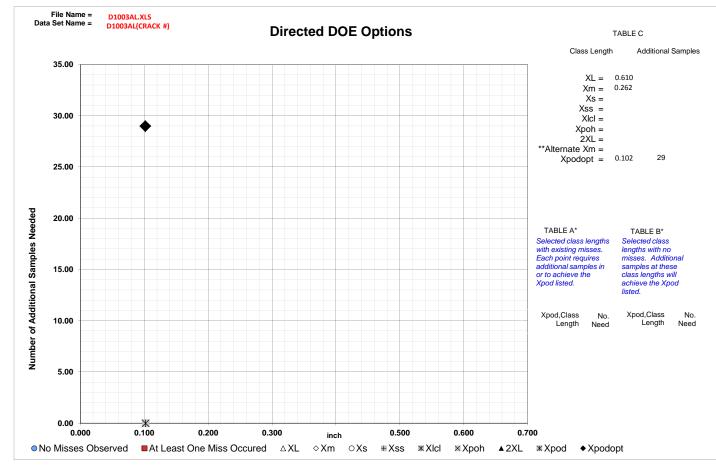
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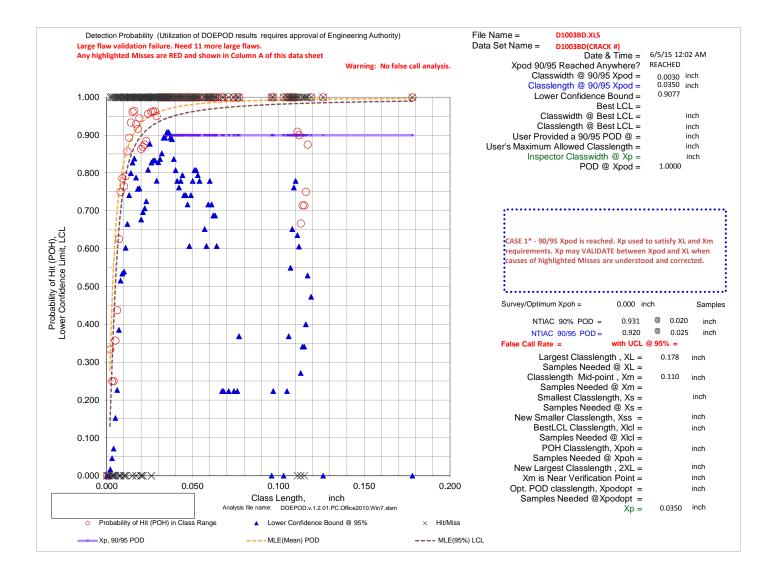


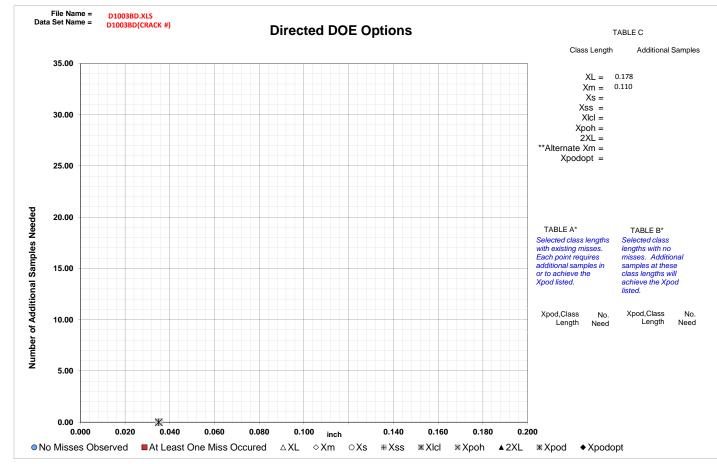
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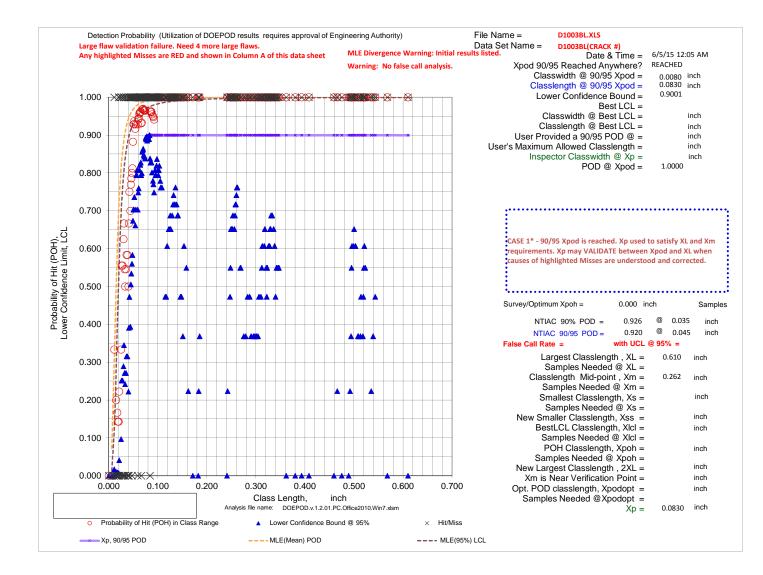


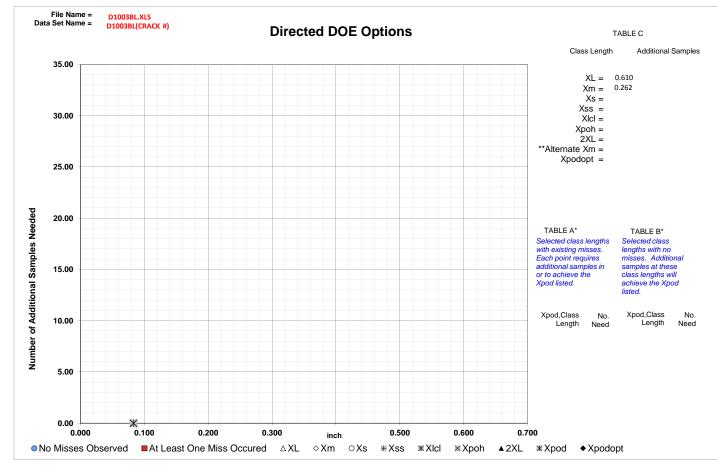
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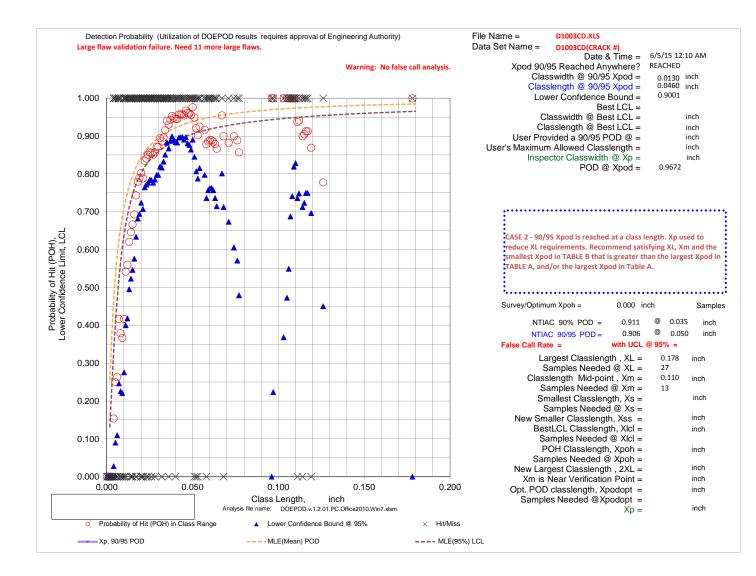


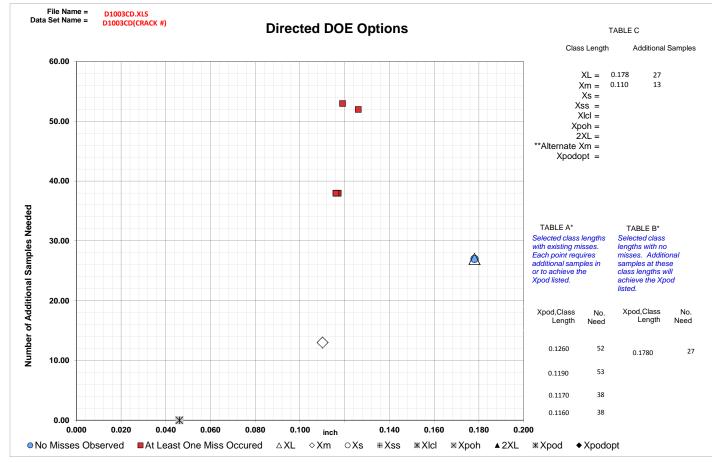
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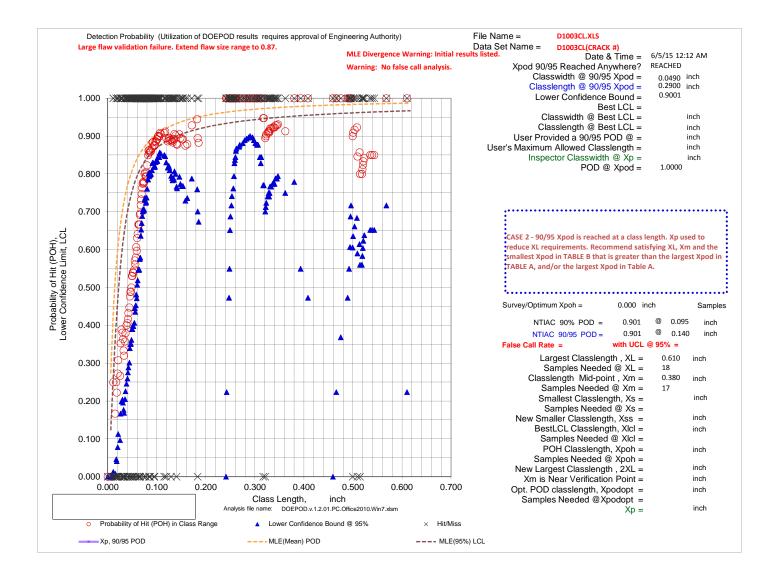


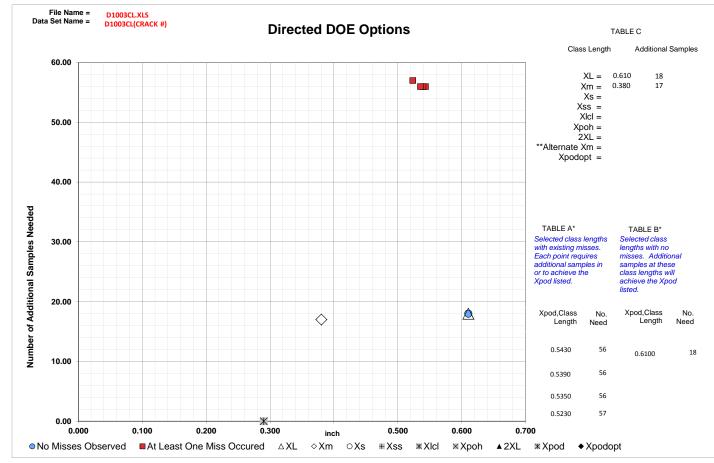
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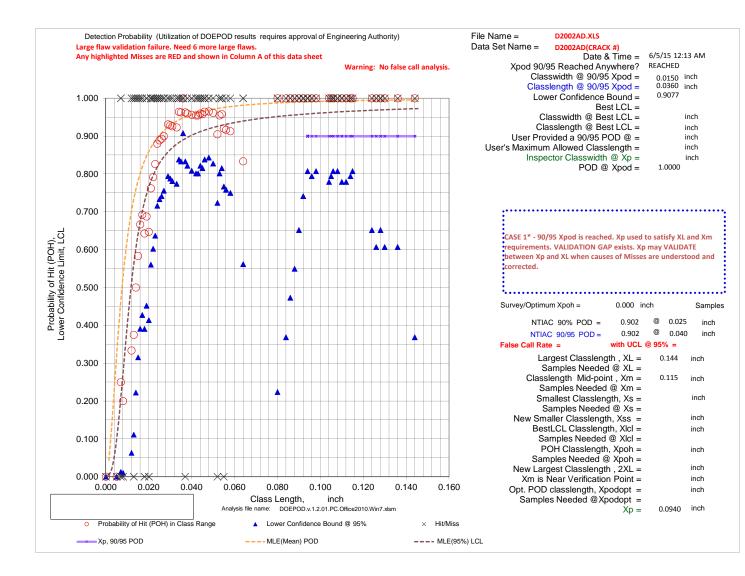


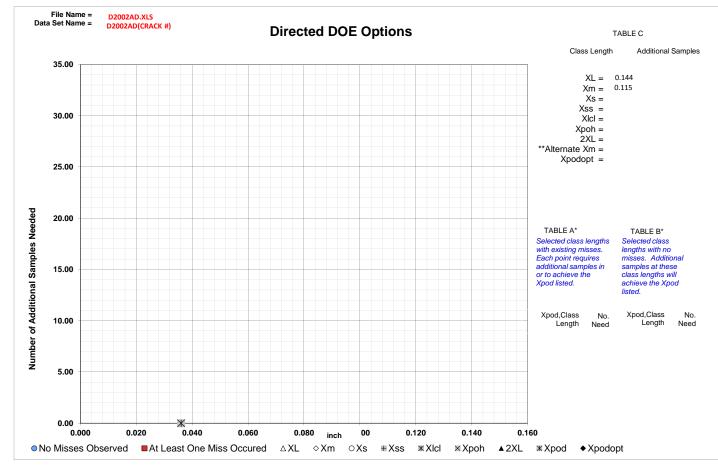
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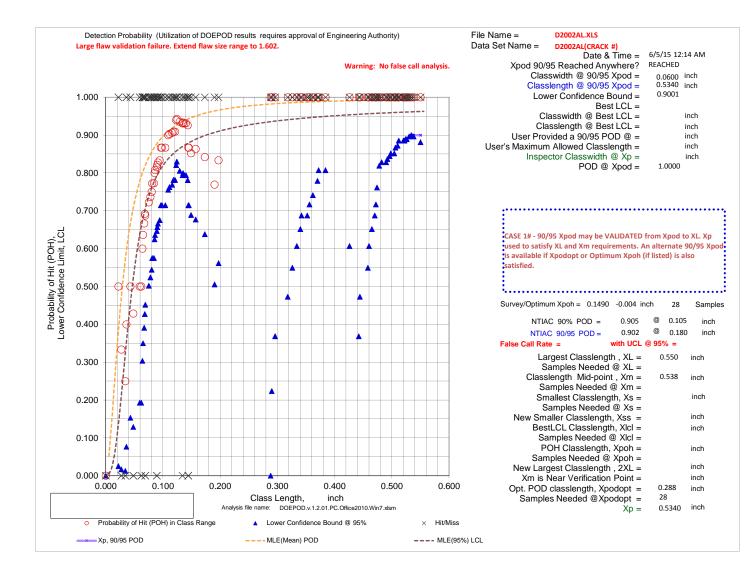


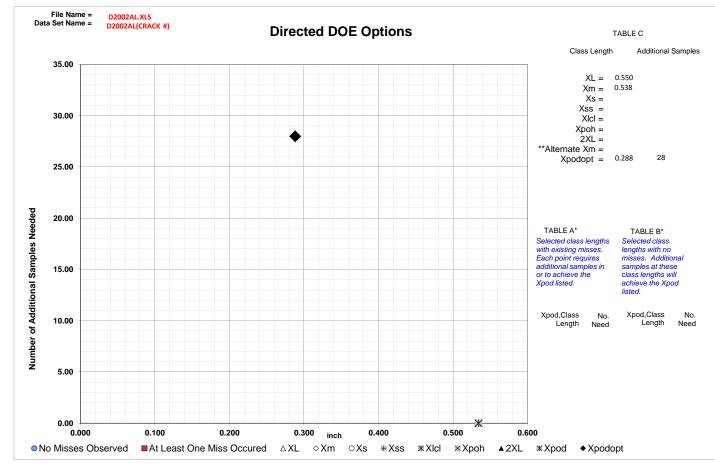
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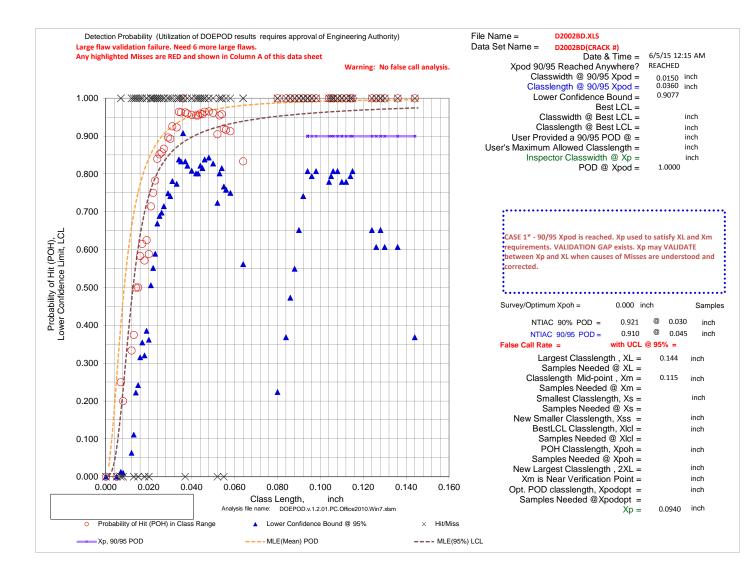


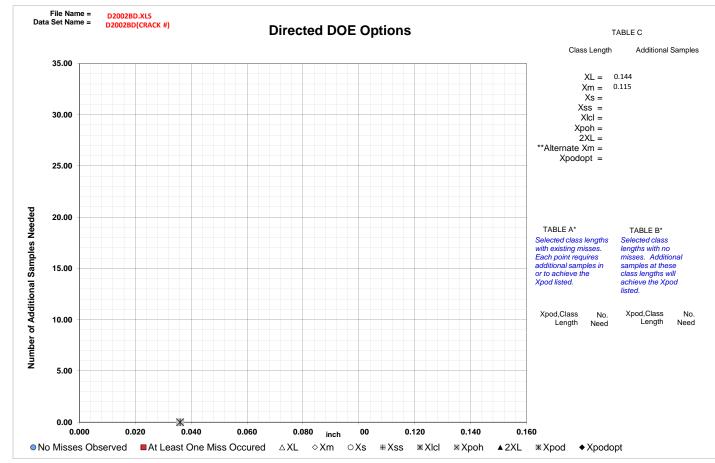
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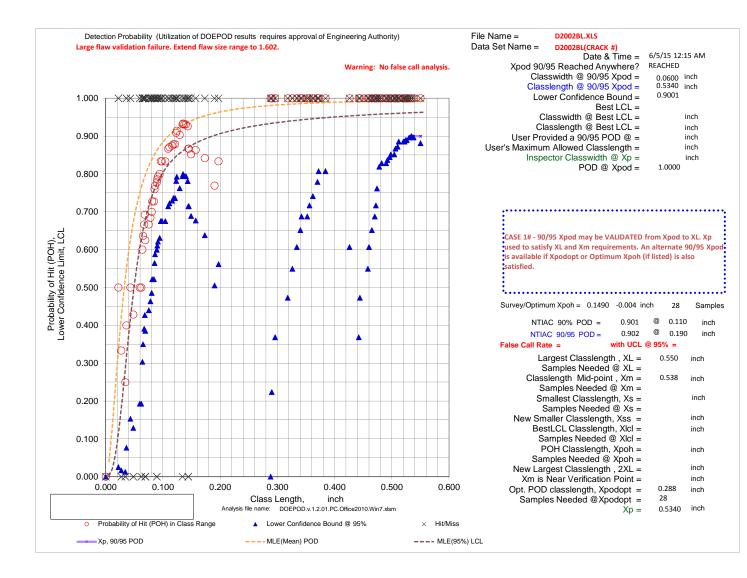


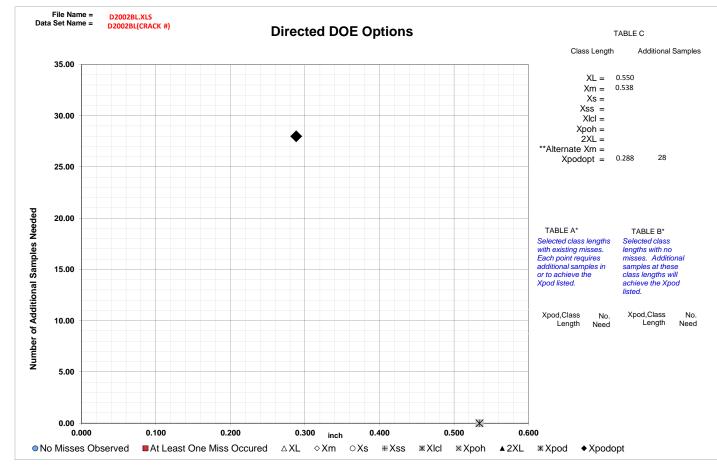
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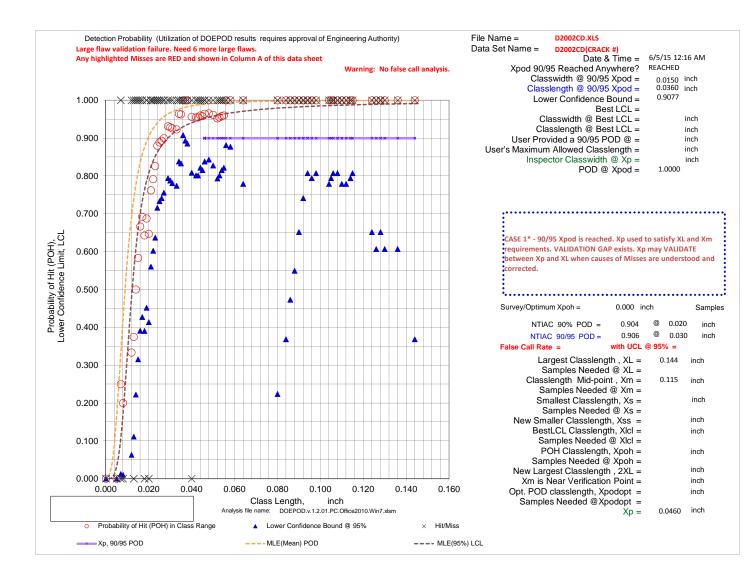


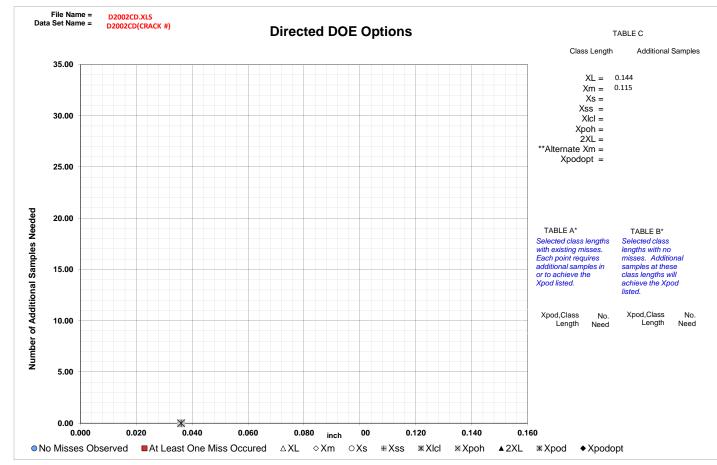
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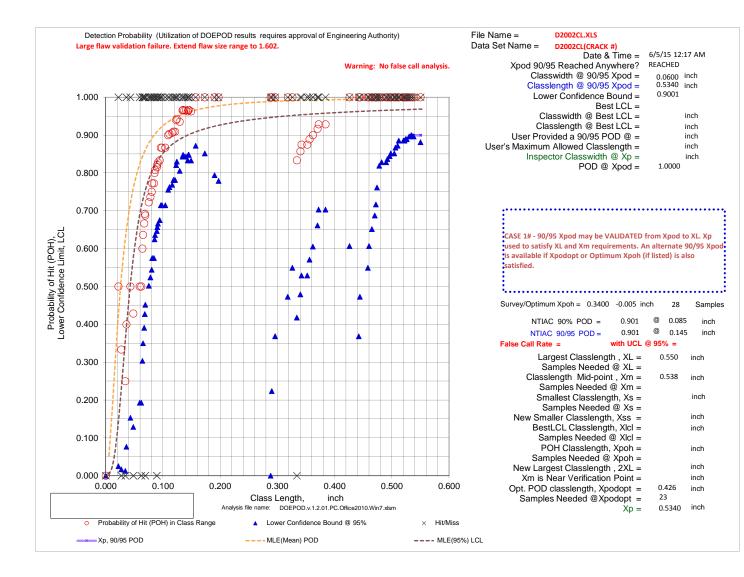


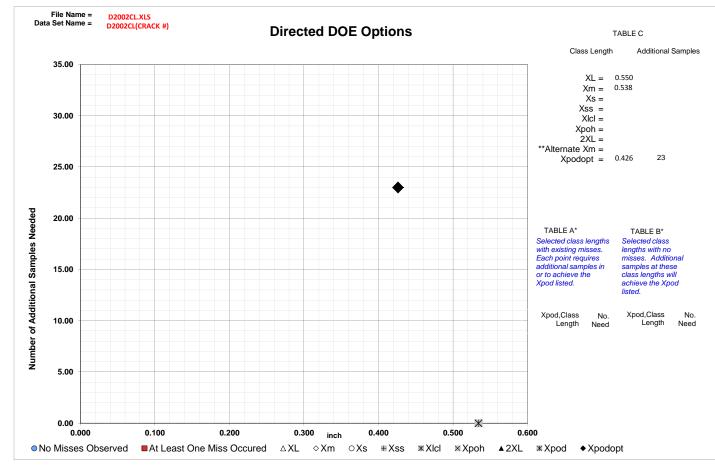
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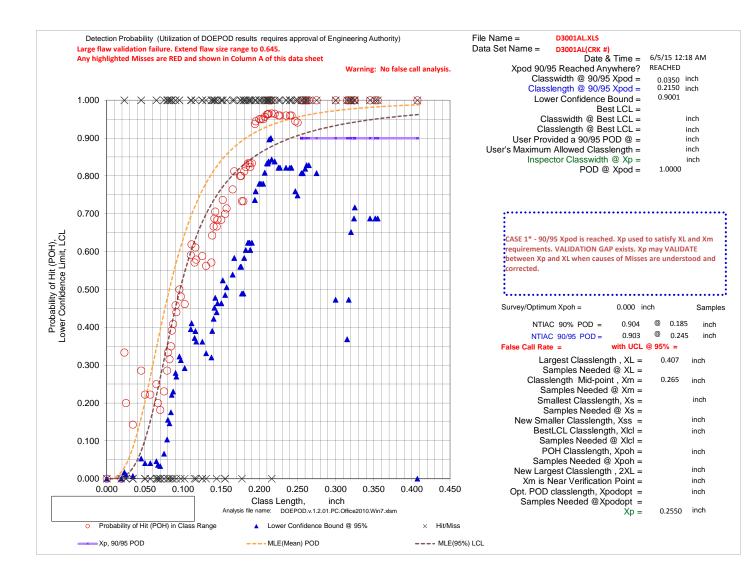


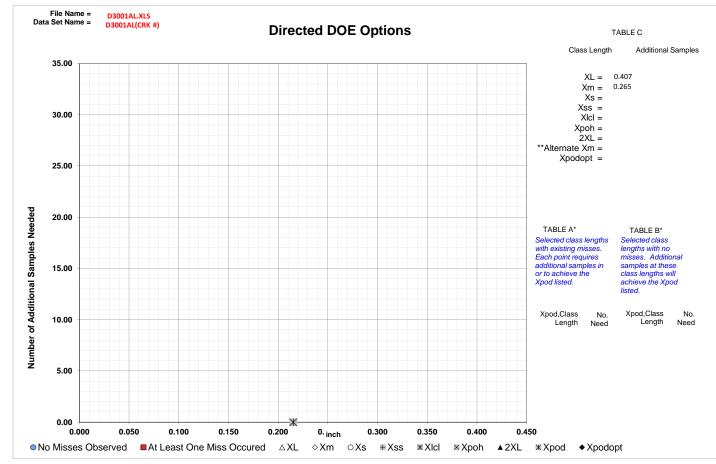
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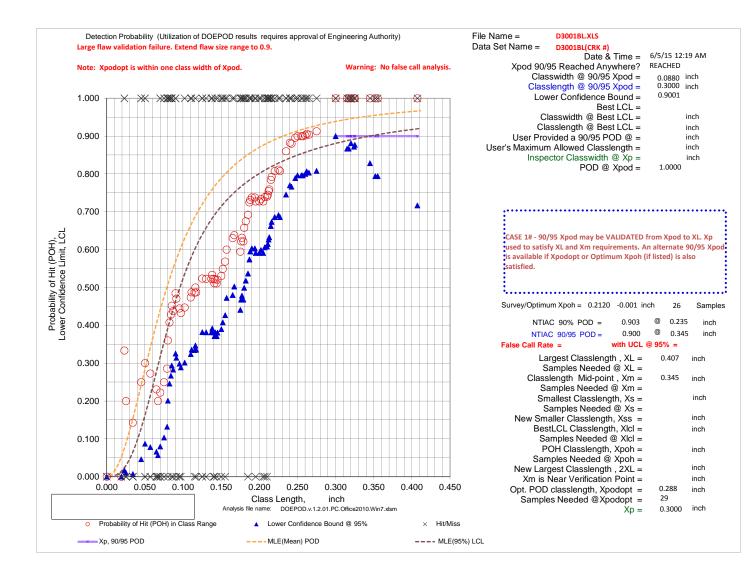


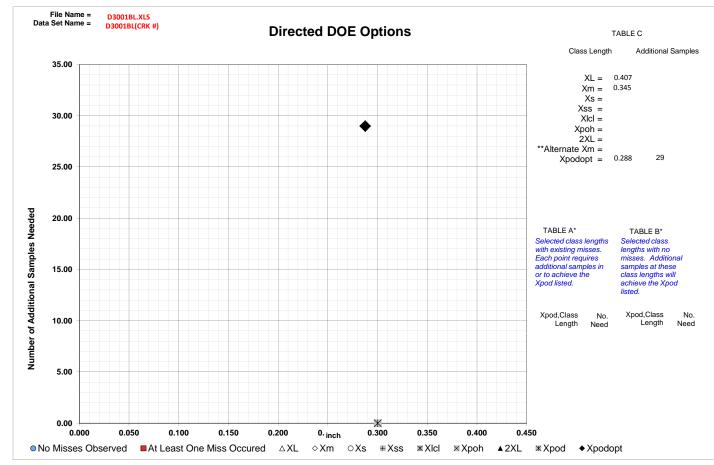
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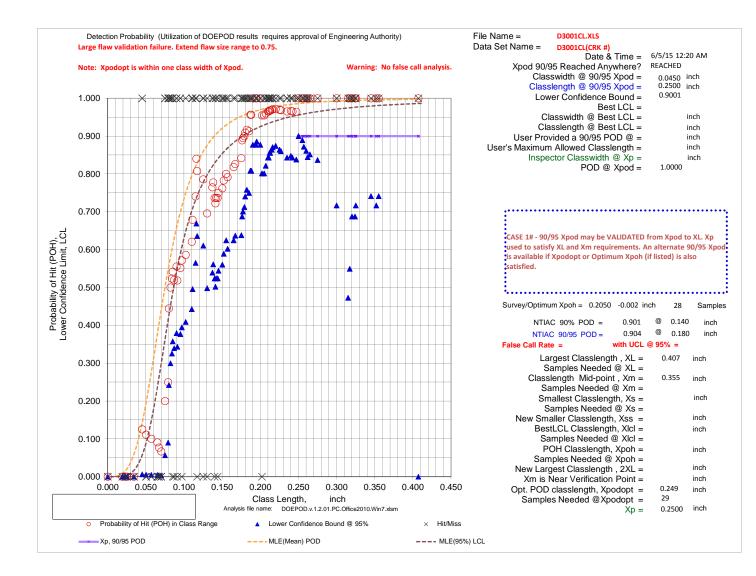


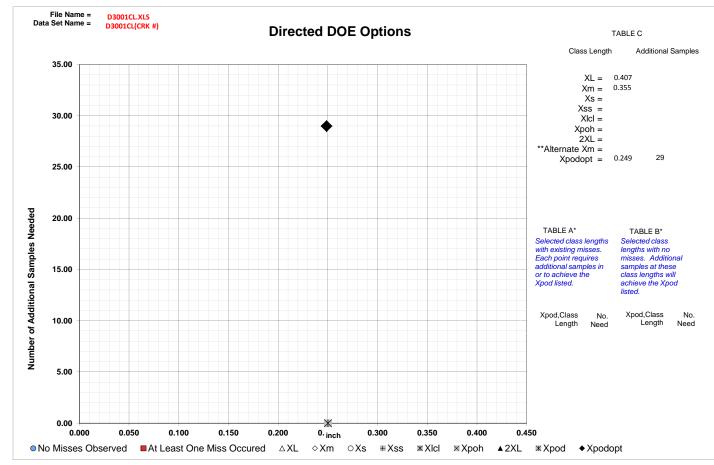
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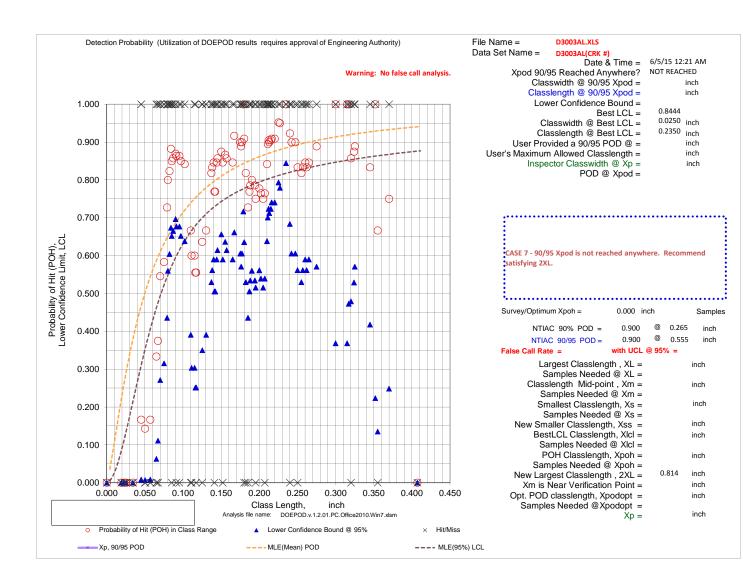


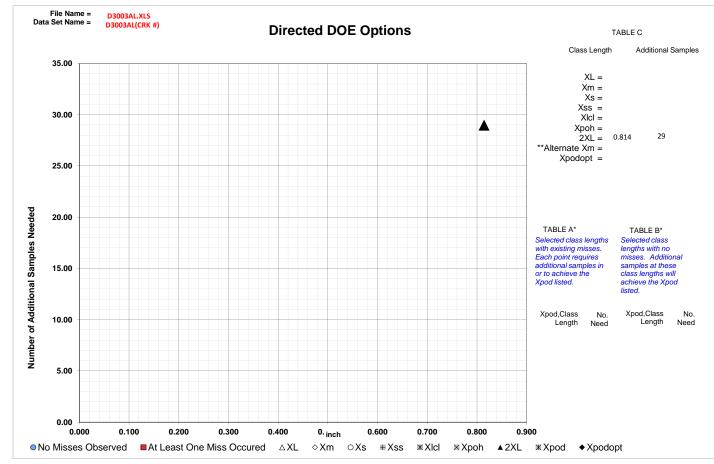
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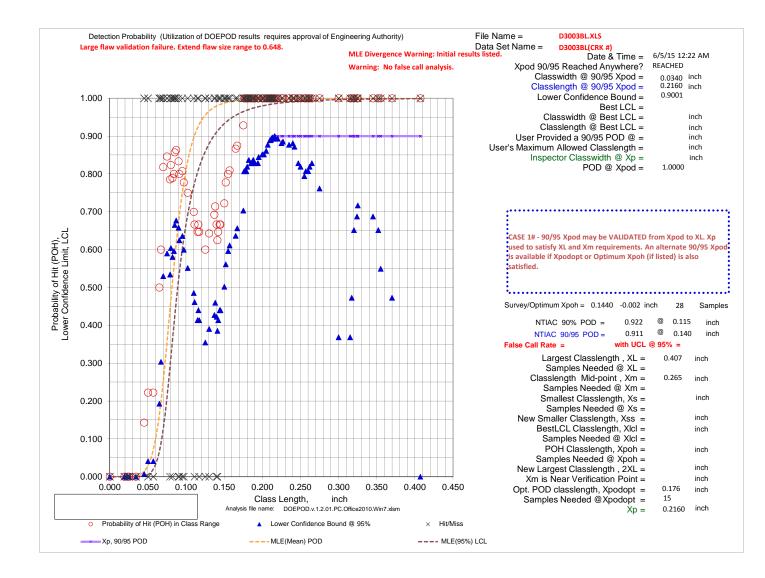


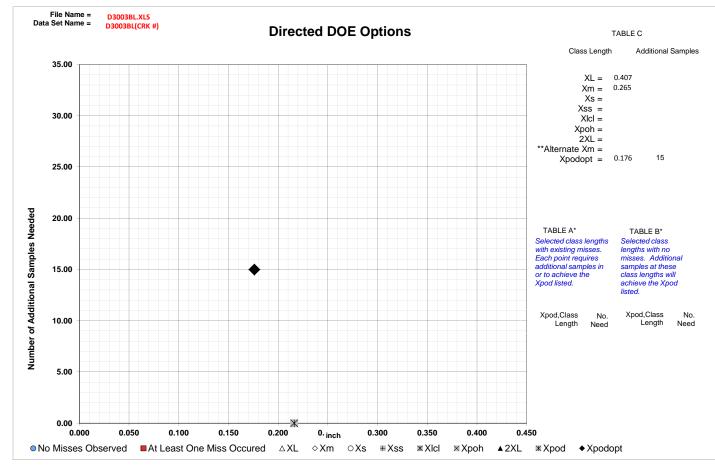
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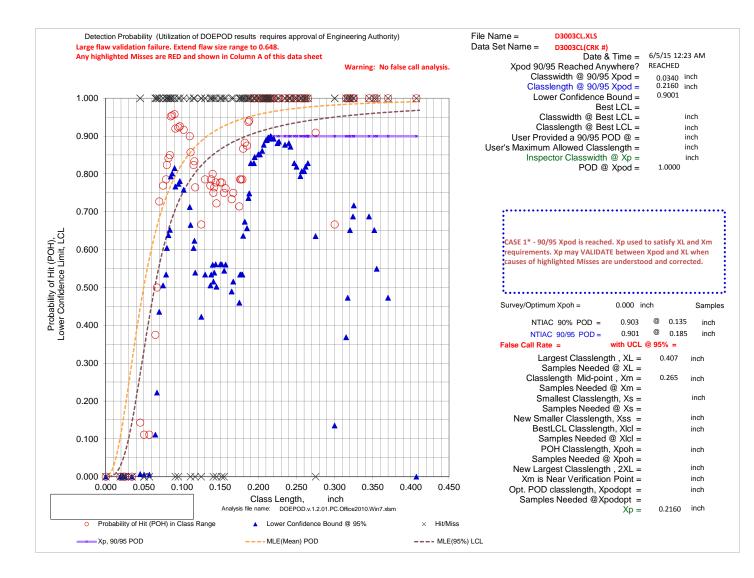


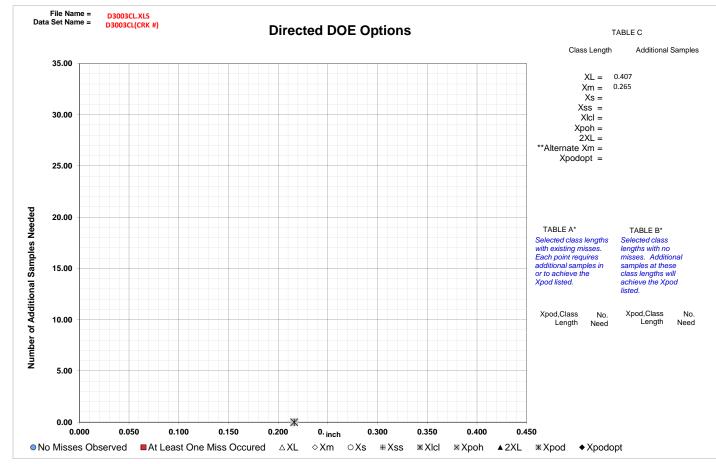
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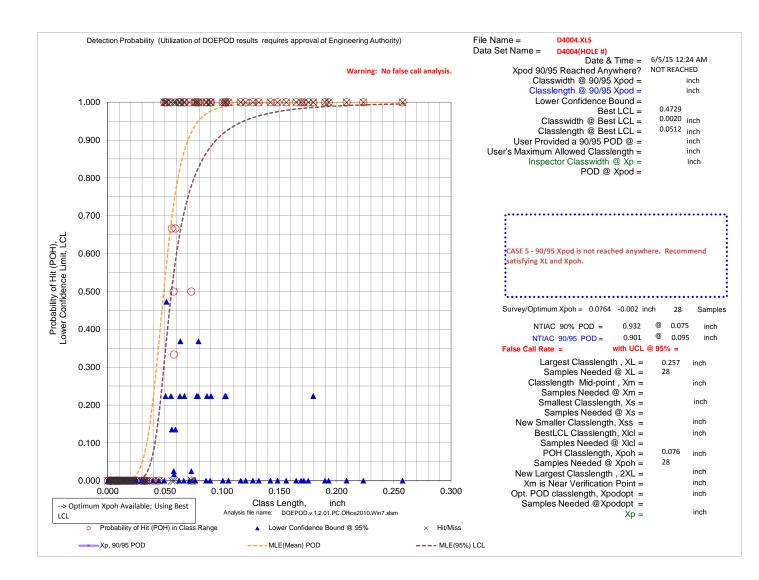


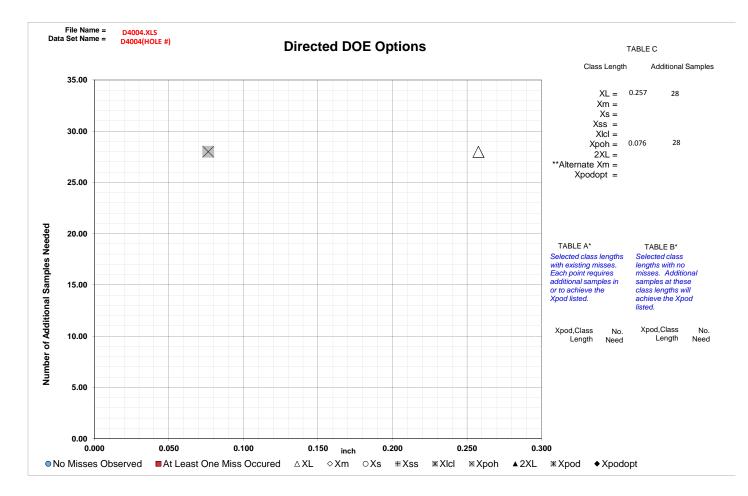
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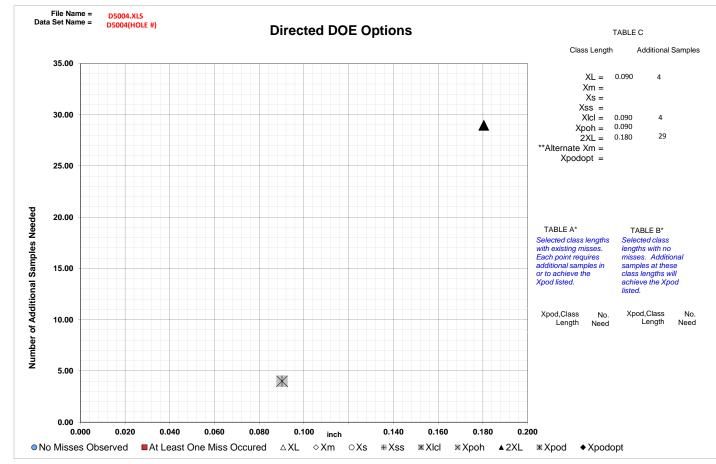
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	Detection Probability (Utilization of DOEPOD results requires approval of Engineering Authority) Warning: No false call analysis.														analysis.	File Name = D5004.XLS Data Set Name = D5004(HOLE #) Date & Time = Xpod 90/95 Reached Anywhere? Classwidth @ 90/95 Xpod =			6/5/15 12: NOT REAC			
Probability of Hit (POH), Lower Confidence Limit, LCL	1.000														Classlength @ 90/95 Xpod = in Lower Confidence Bound = Best LCL = 0.8855							
	0.900										0) (000 D				User's	C User Pro Maximu	Classwidth @ Bea lasslength @ Bea ovided a 90/95 P m Allowed Class ector Classwidth	st LCL = st LCL = OD @ = length = @ Xp =	0.0230 0.0902	inch inch inch inch inch
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	0.700									8												
	0.600									` ھر م					•••••			CASE 4 - 90/95 Xpod is not reached anywl satisfying XL and the greater of Xpoh or X				nmend
	0.500	0							6								Su	rvey/Optin	num Xpoh = 0.0681	-0.001 ir	nch 28	Samples
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		Class Length, inch Analysis file name: DOEPOD.v.1.2.01.PC.Office2010.Win7.xism Probability of Hit (POH) in Class Range Lower Confidence Bound @ 95% × Hit/Mis														Samp	ies ineeueu @Ap	Xp =		inch		
		robability of p, 90/95 PC	. ,	in Clas	s Range	Range A Lower Confidence Bound @ 95%									_	× Hit/Miss						

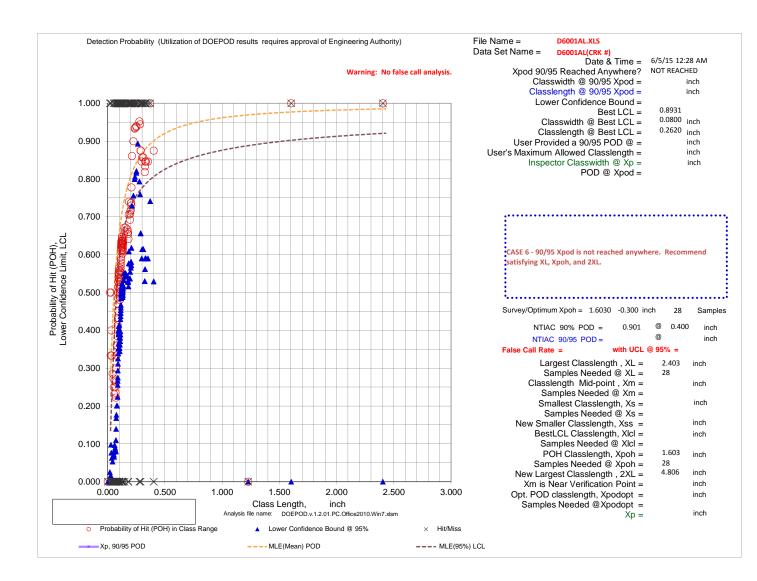


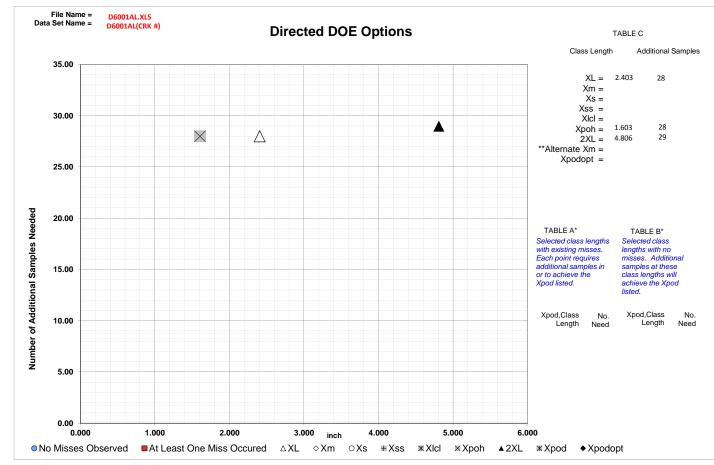
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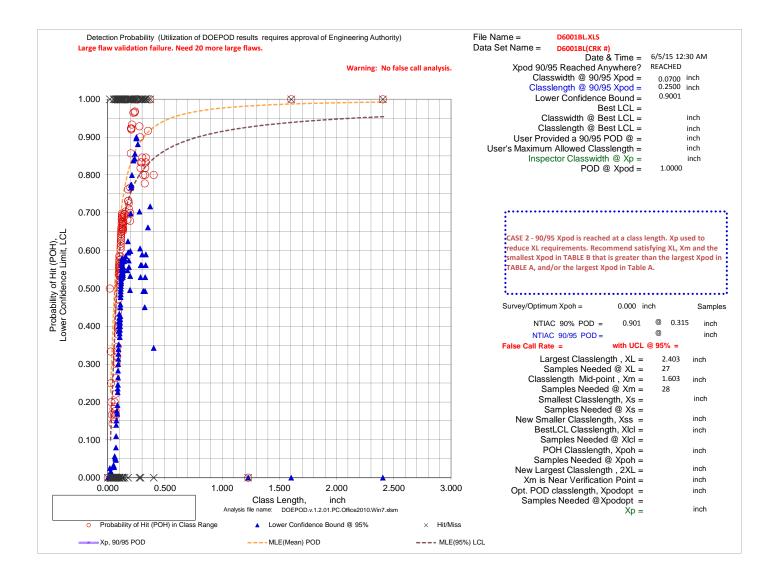


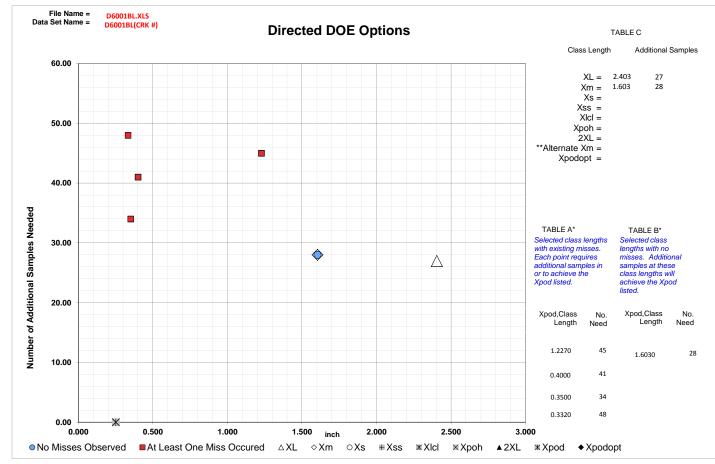
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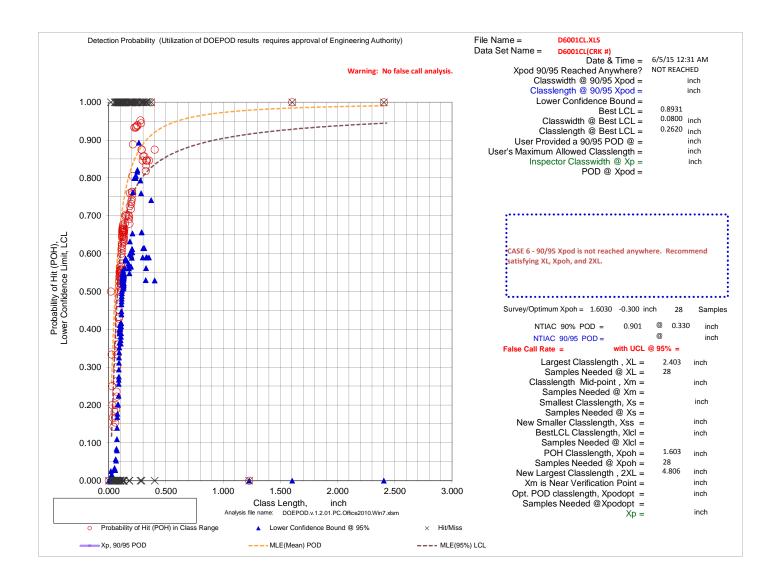


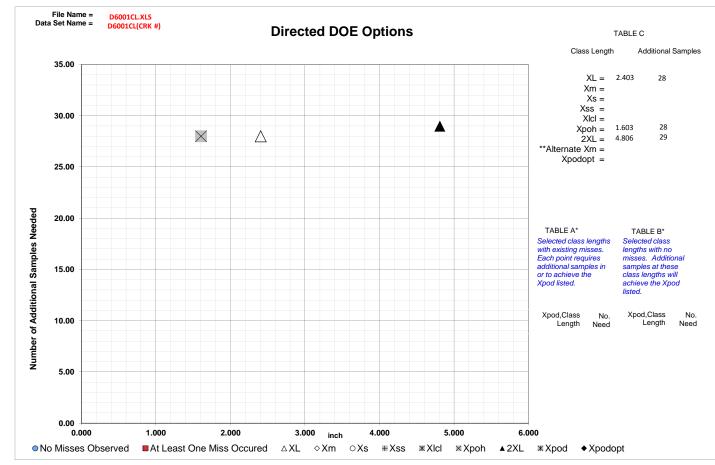
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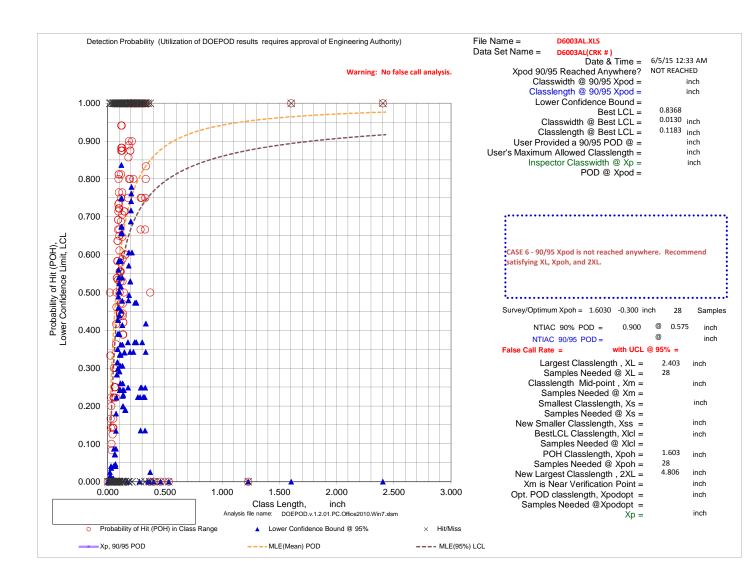


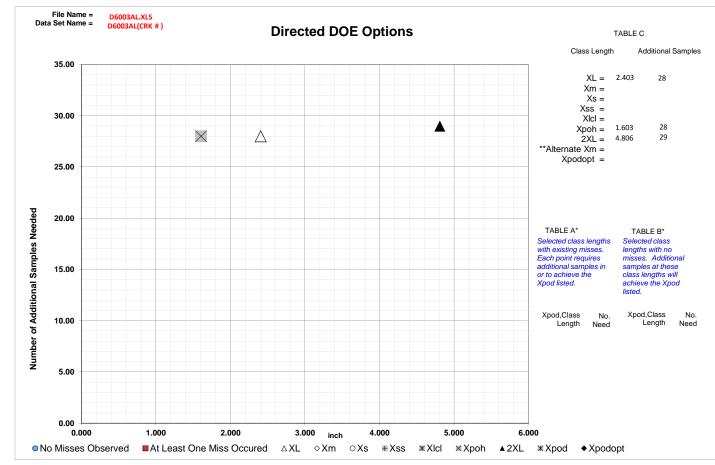
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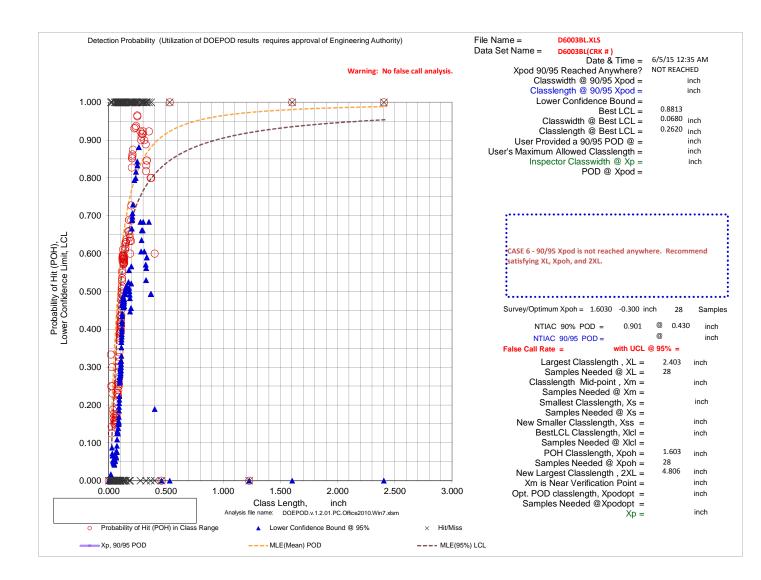


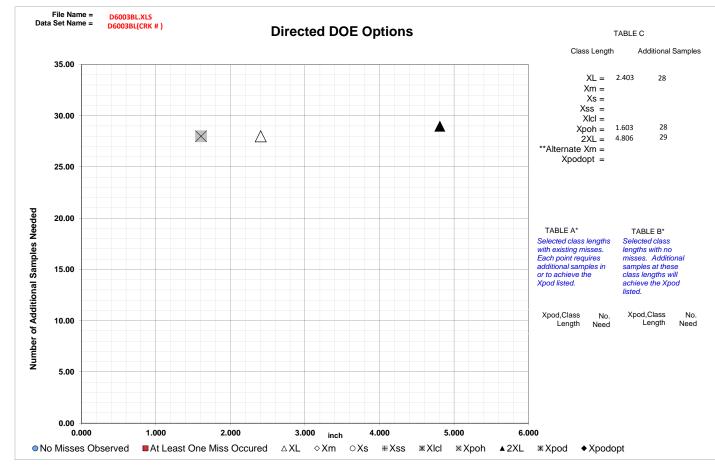
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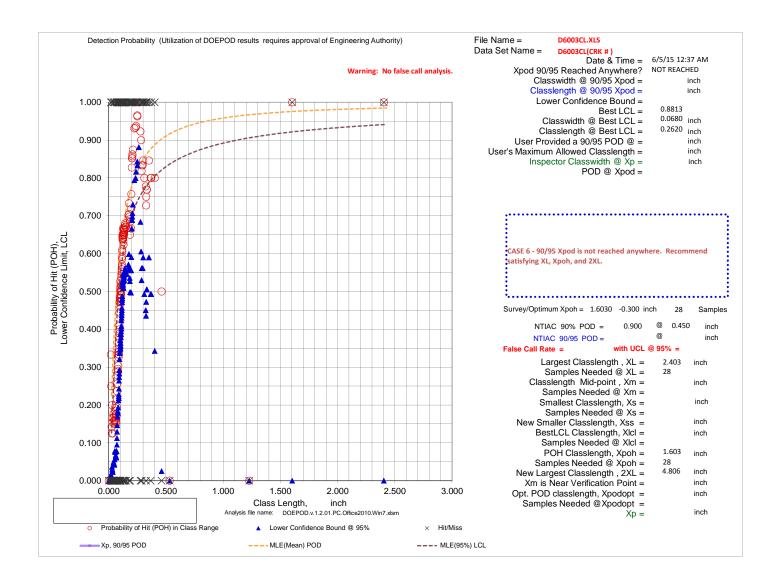


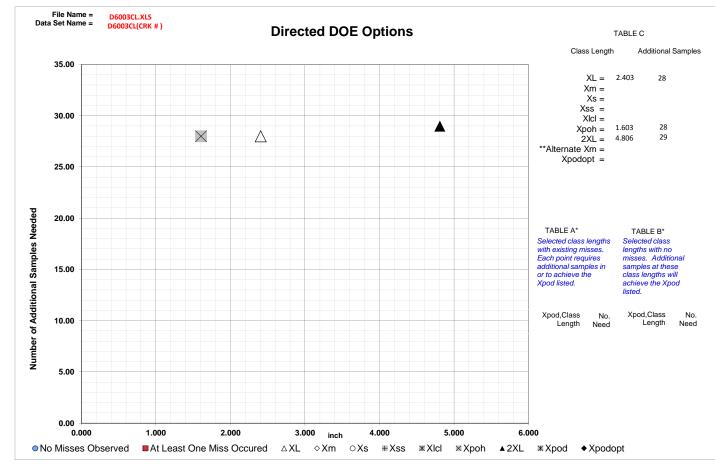
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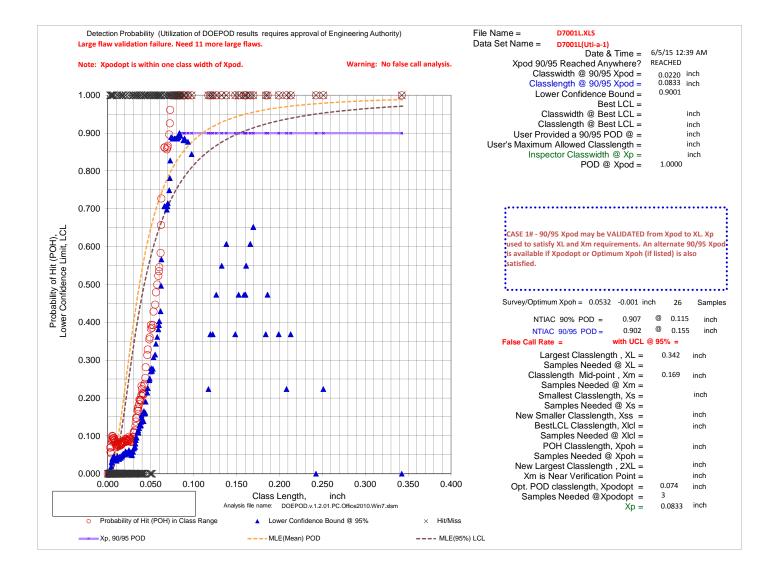


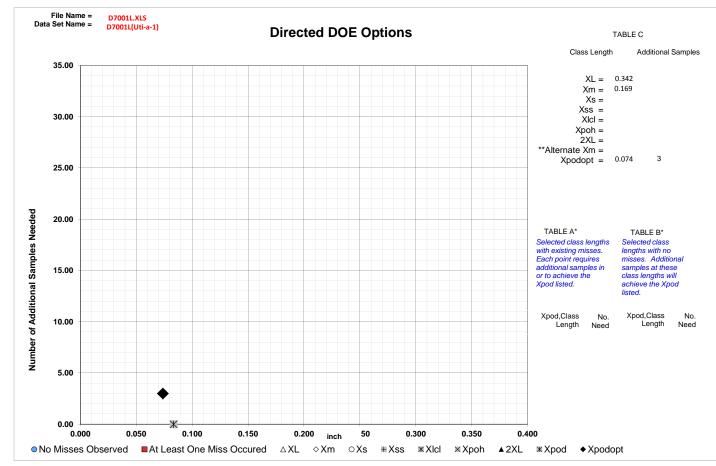
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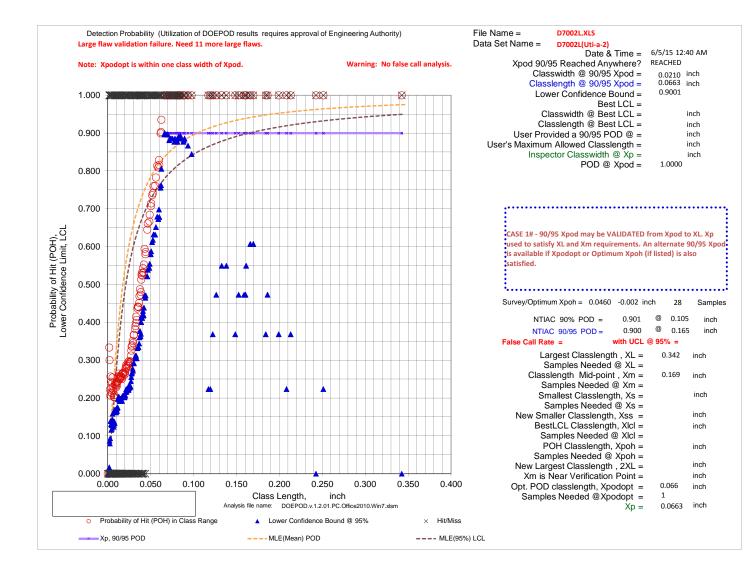


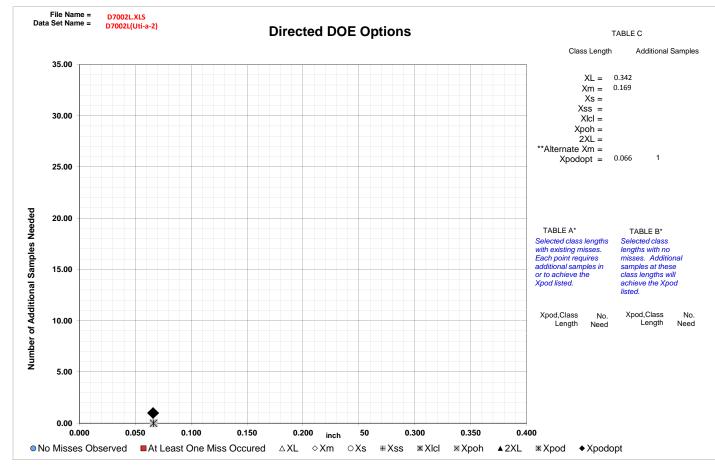
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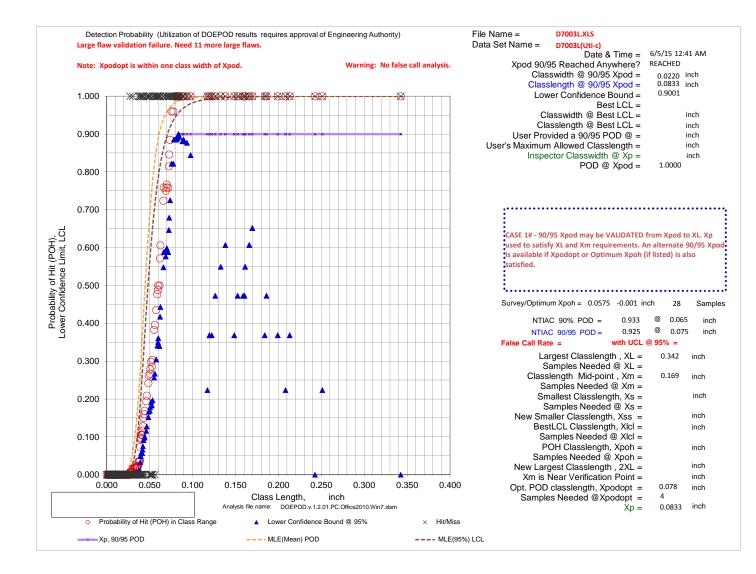


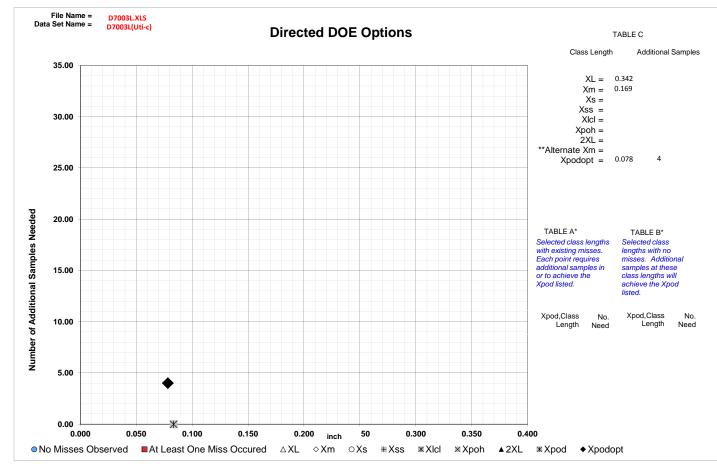
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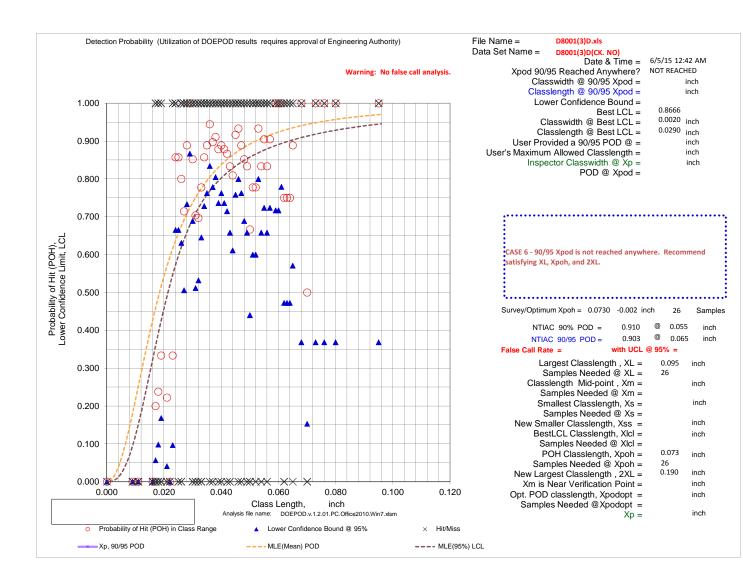


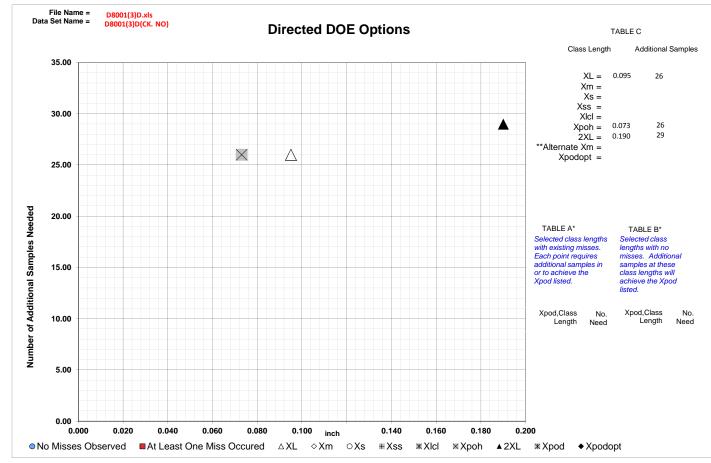
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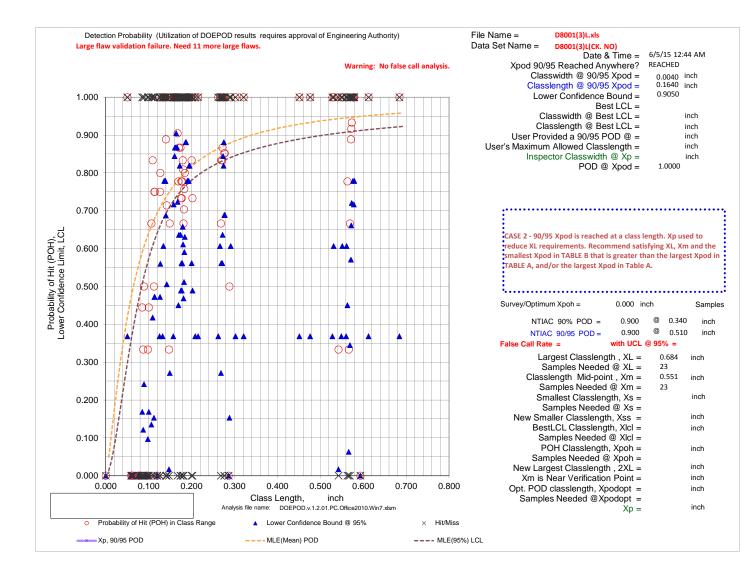


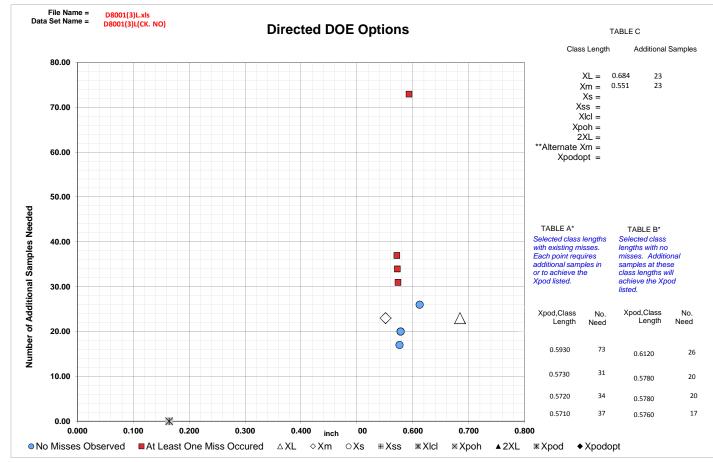
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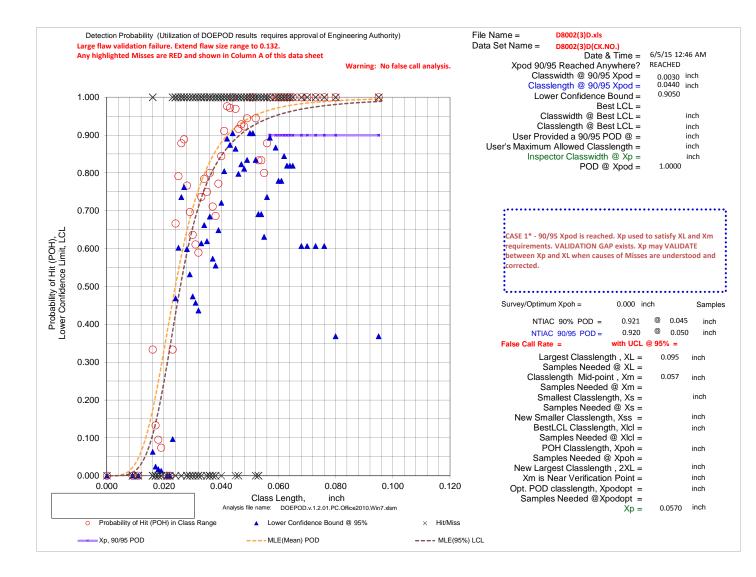


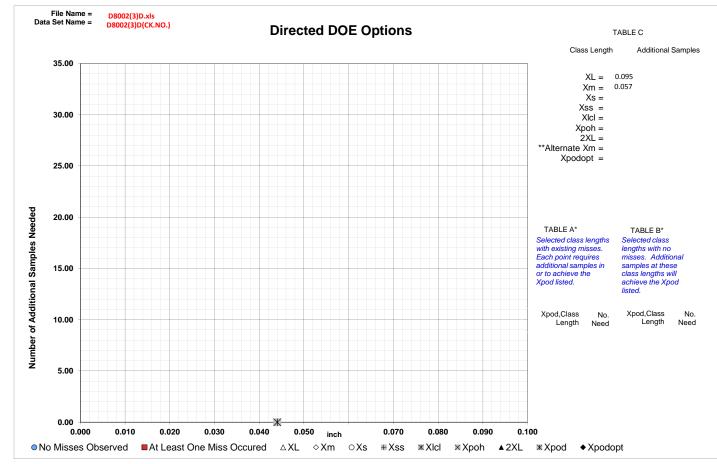
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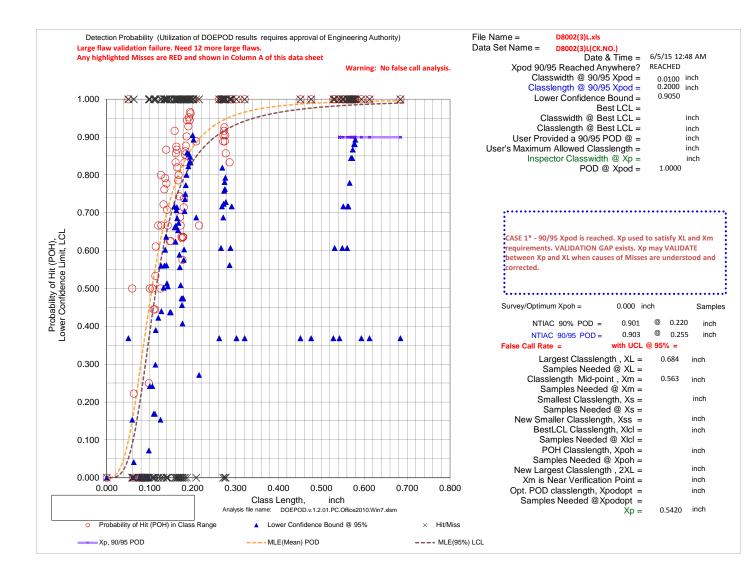


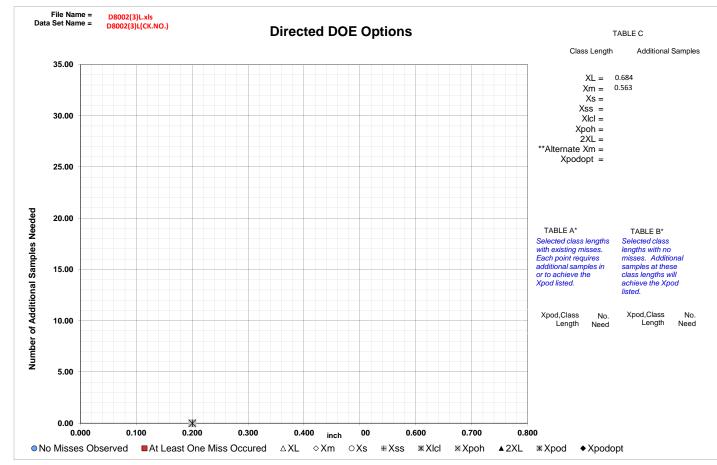
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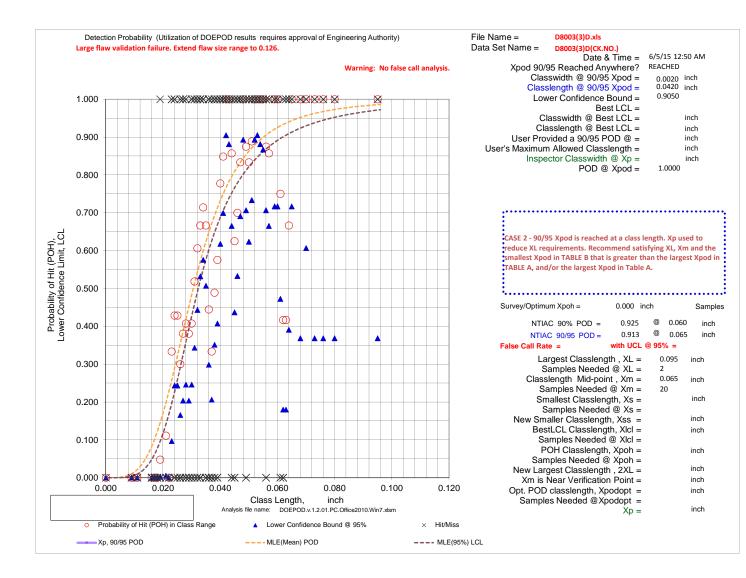


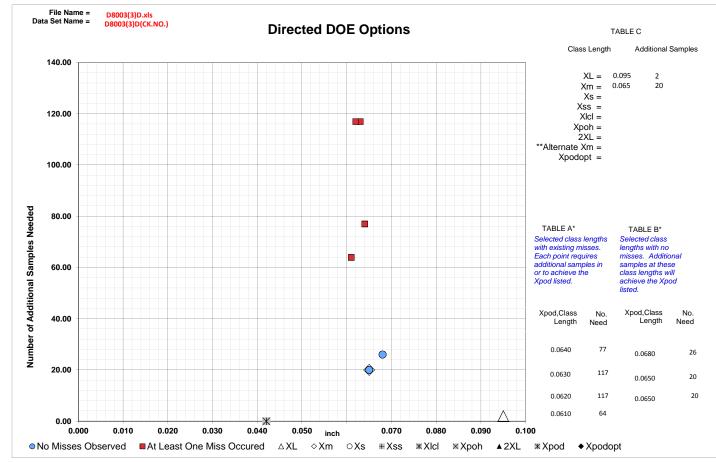
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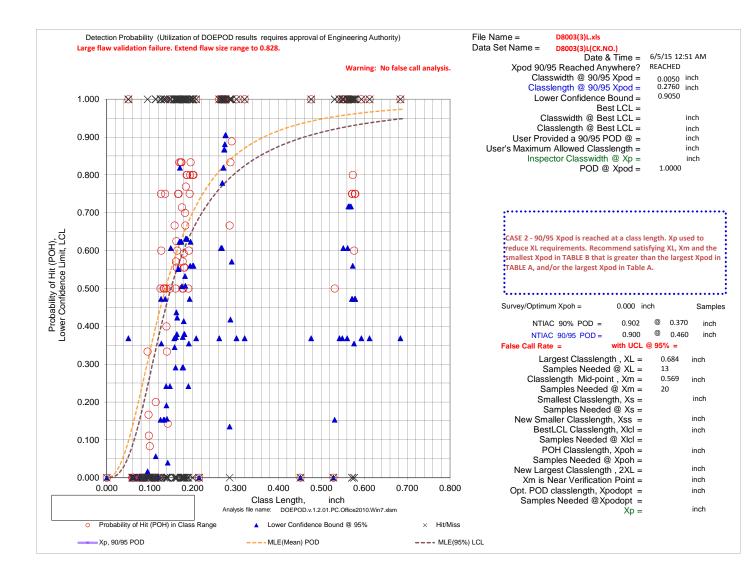


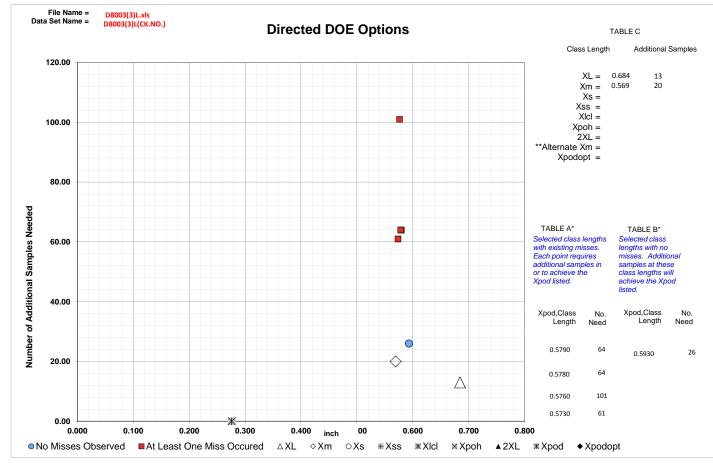
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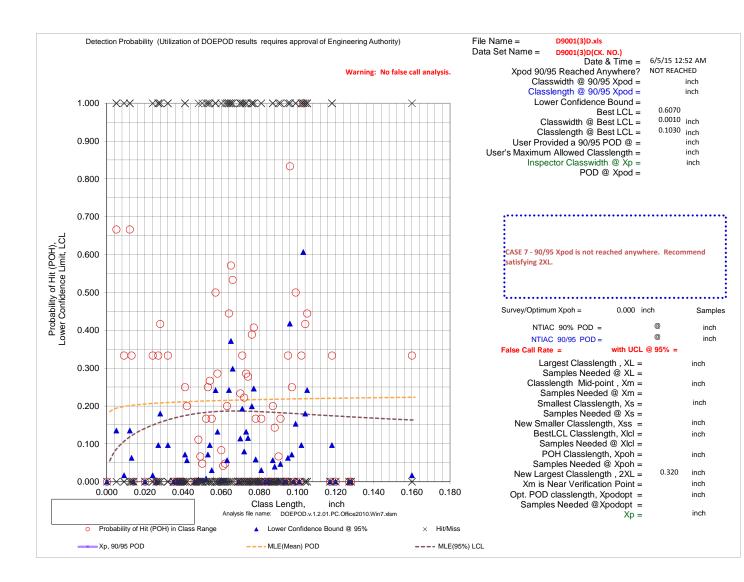


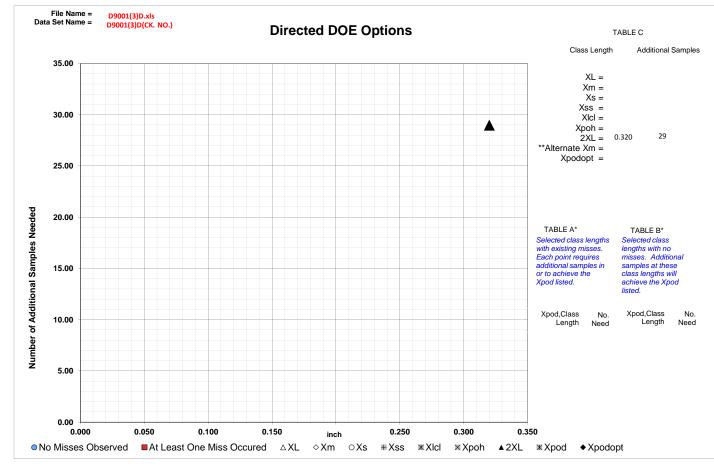
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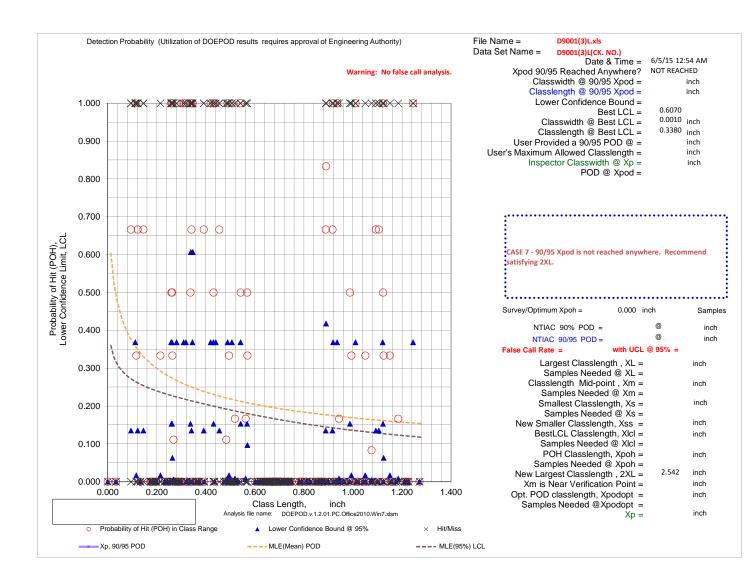


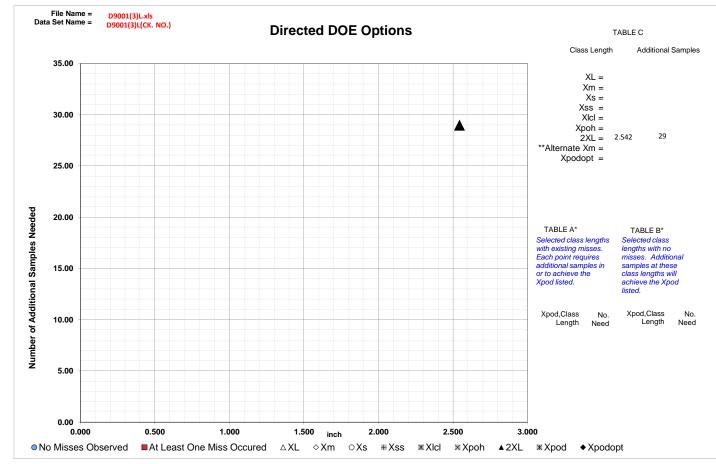
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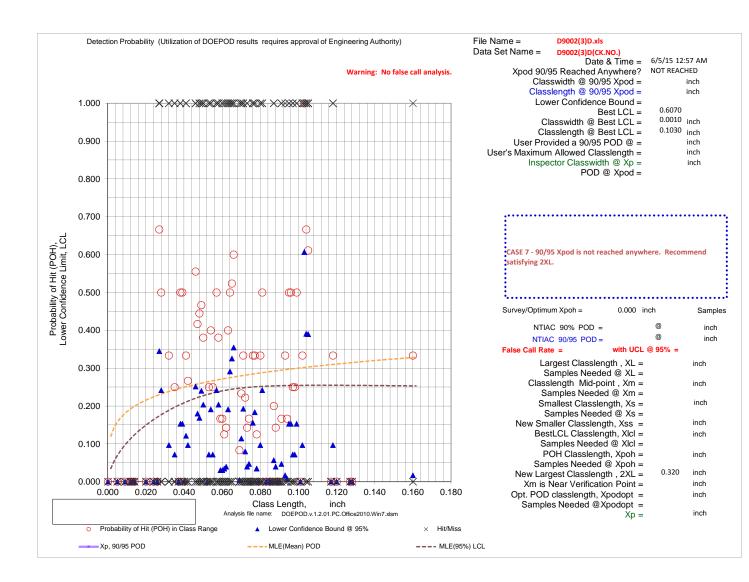


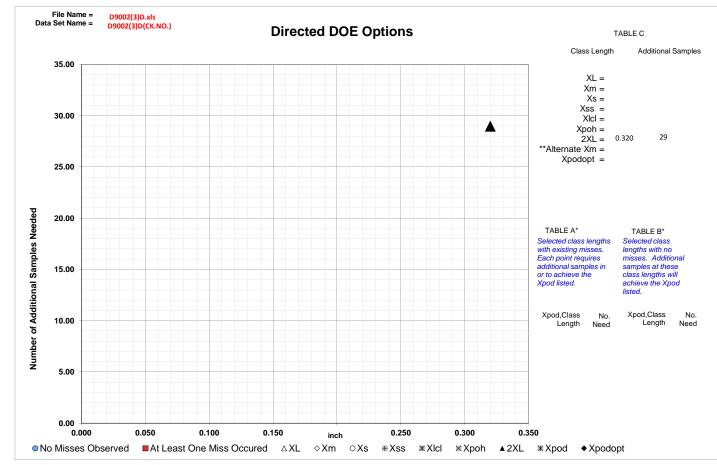
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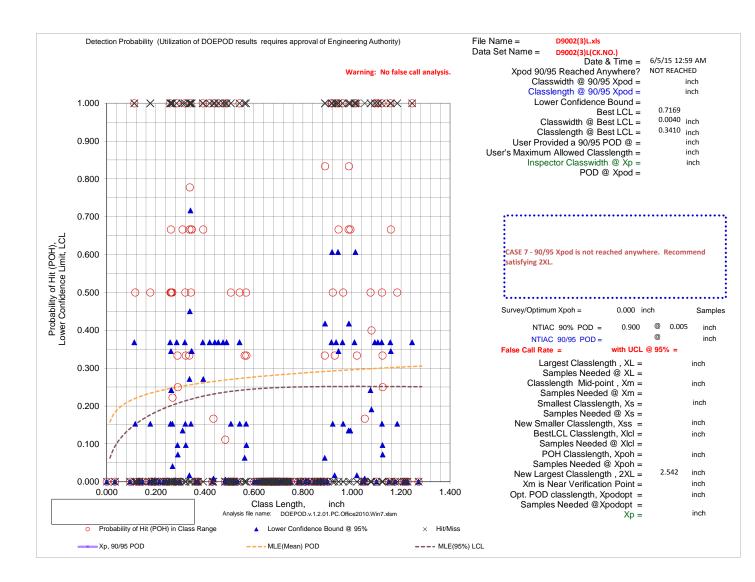


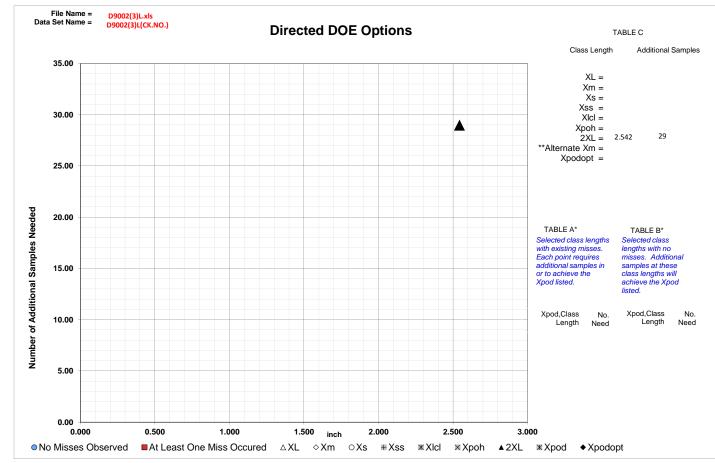
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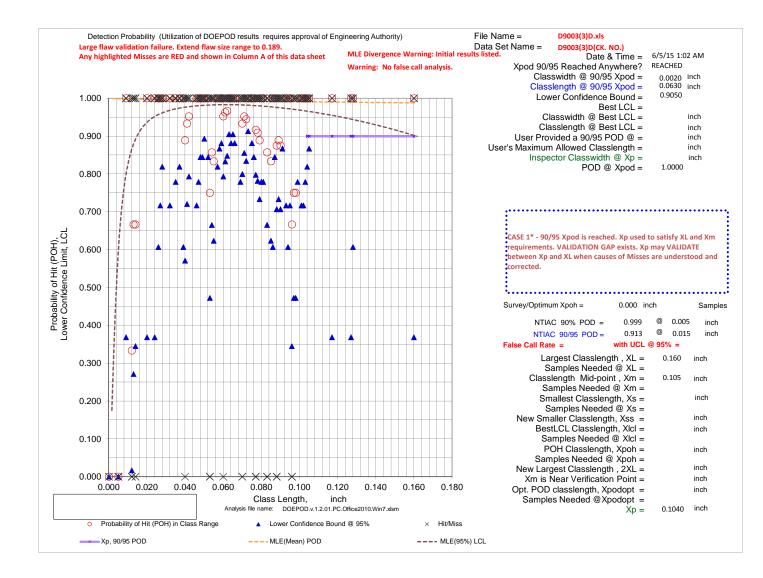


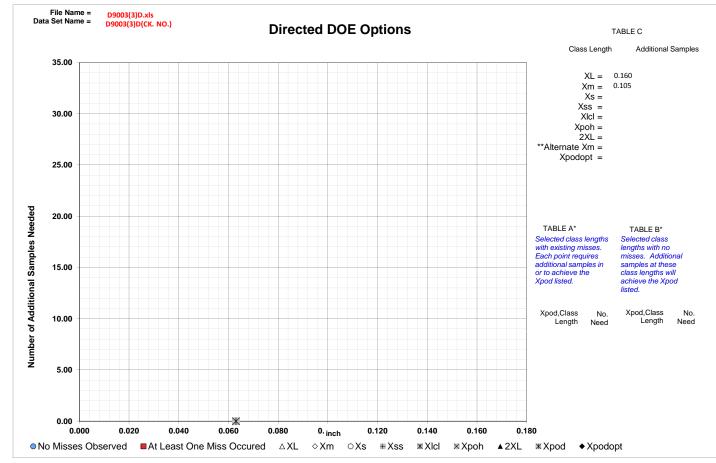
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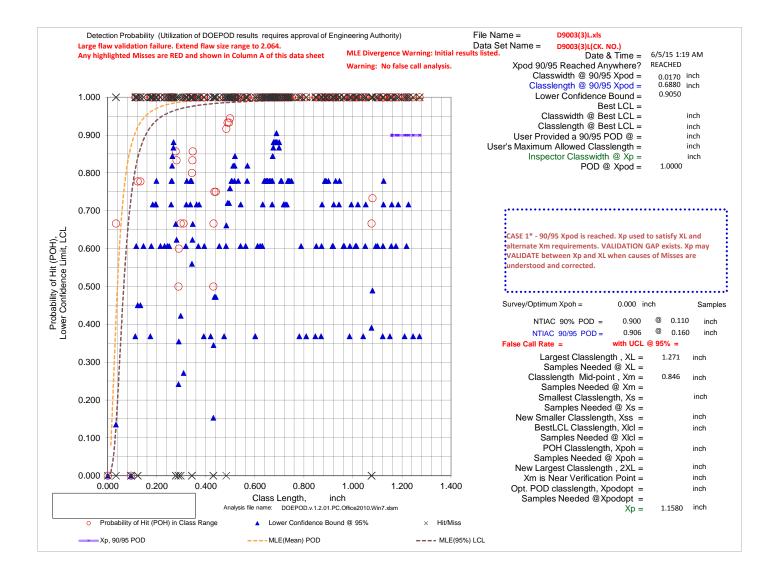


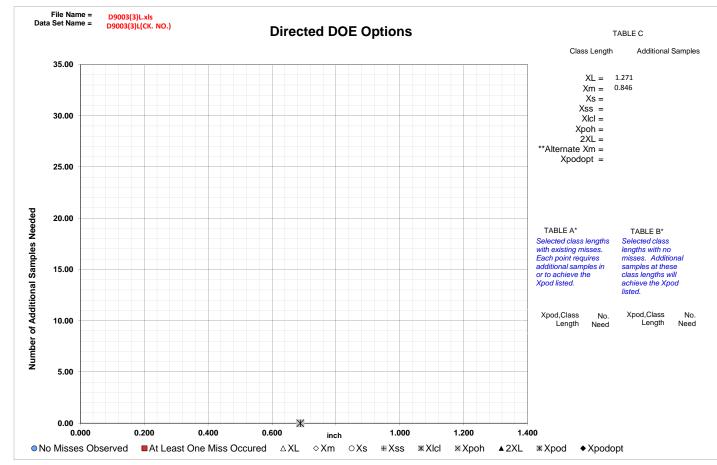
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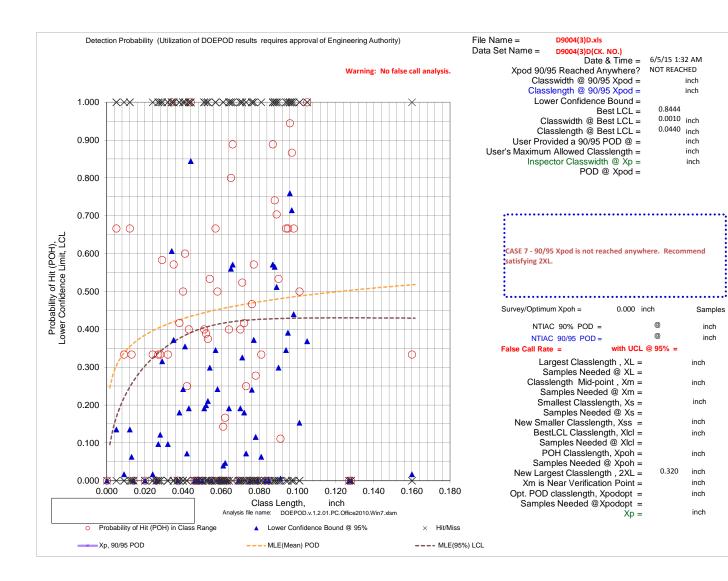


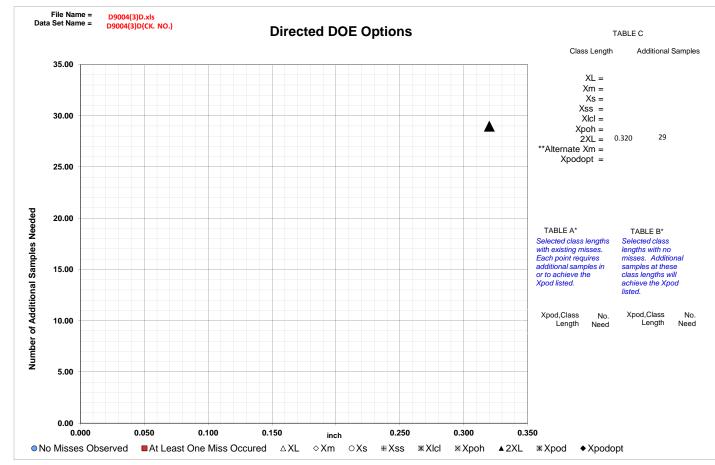
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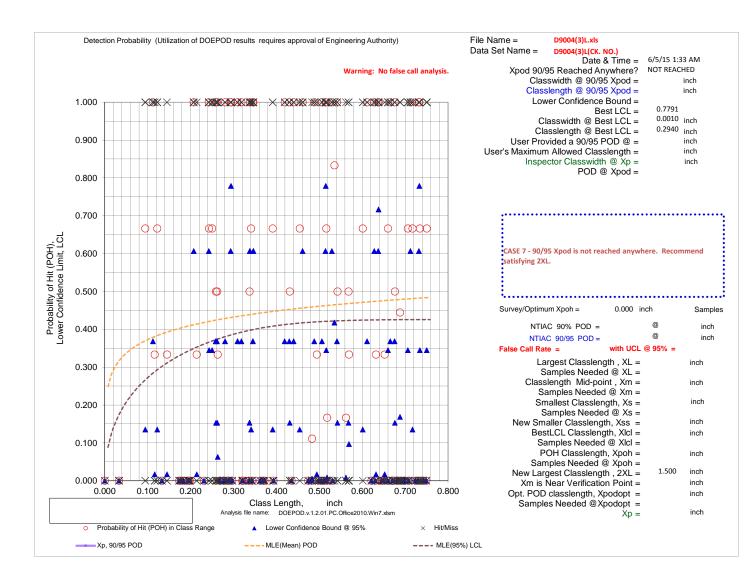


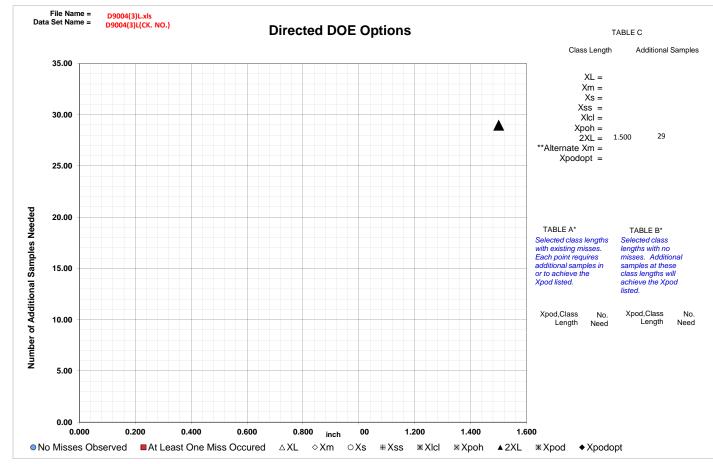
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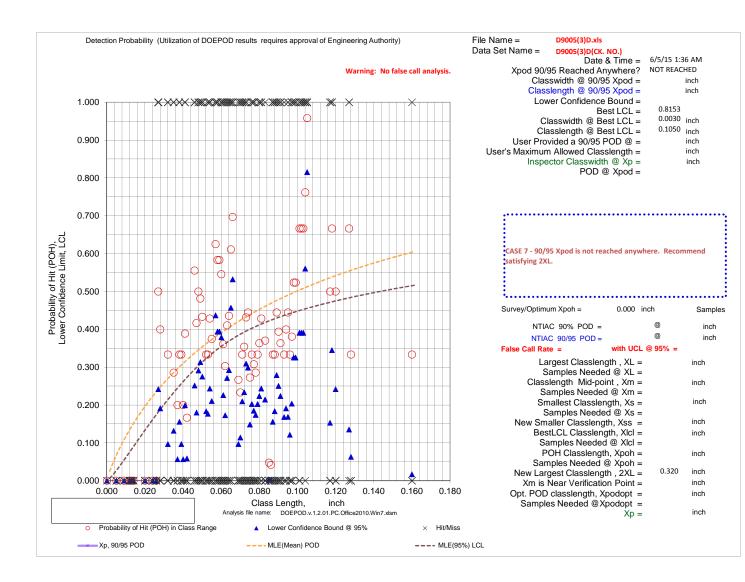


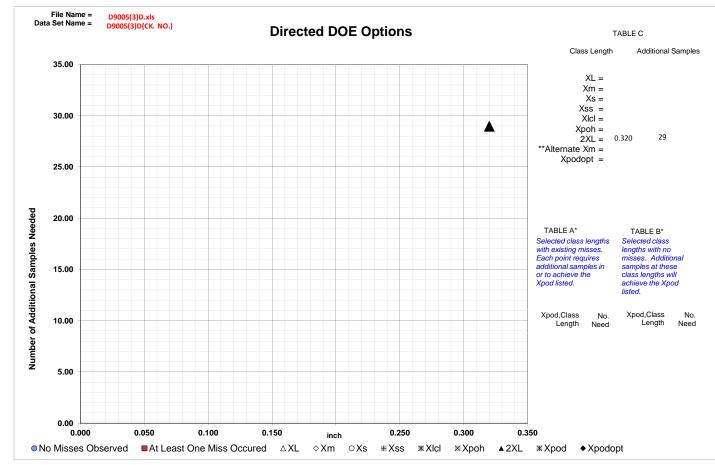
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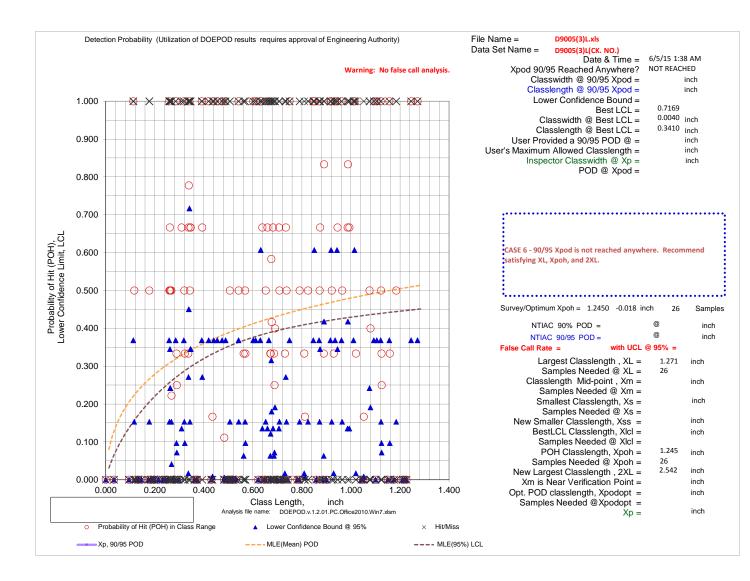


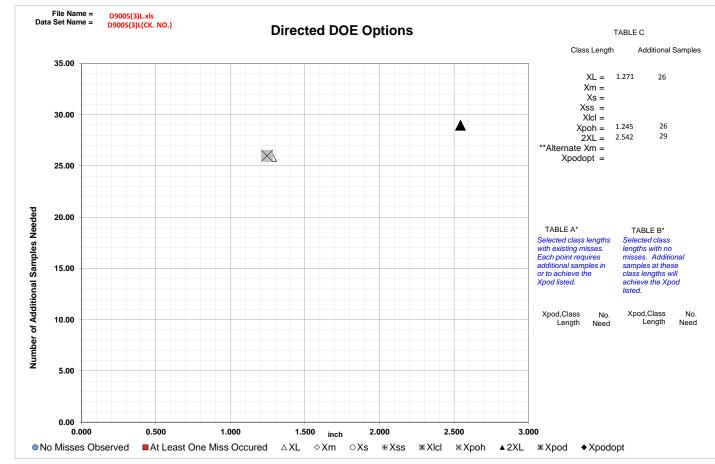
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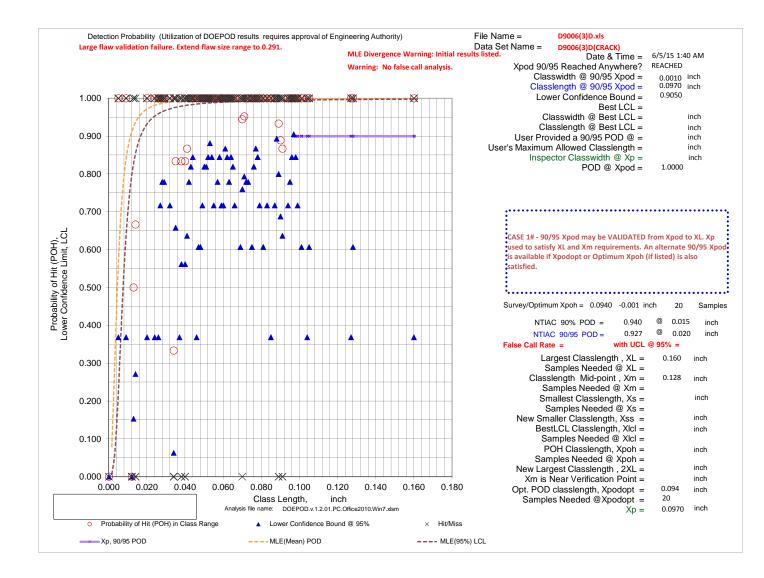


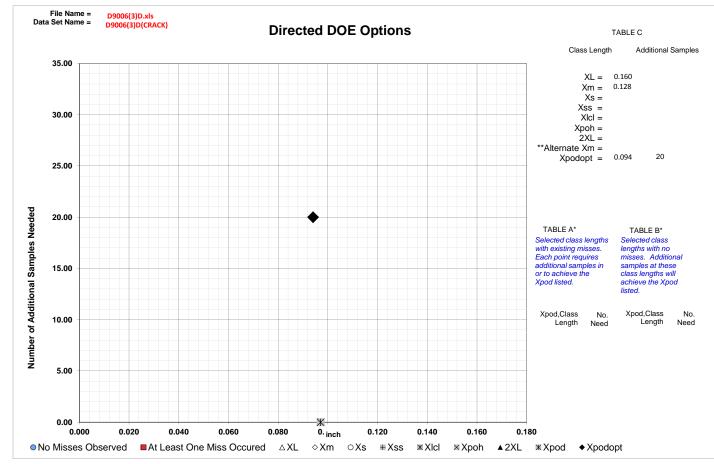
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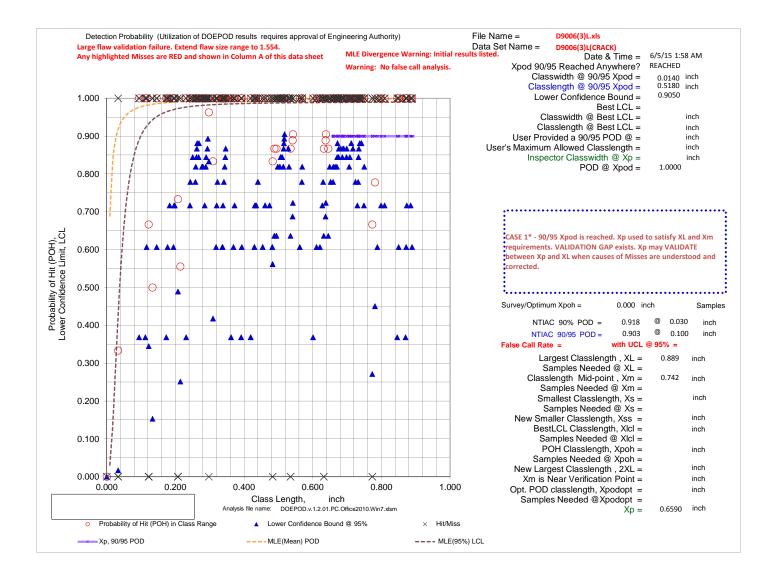


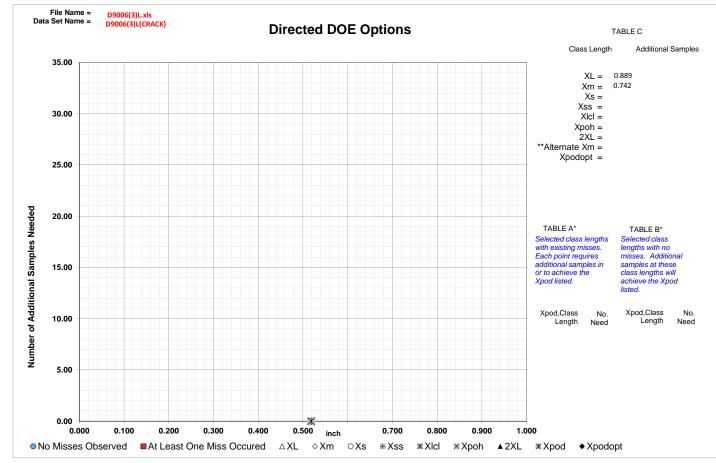
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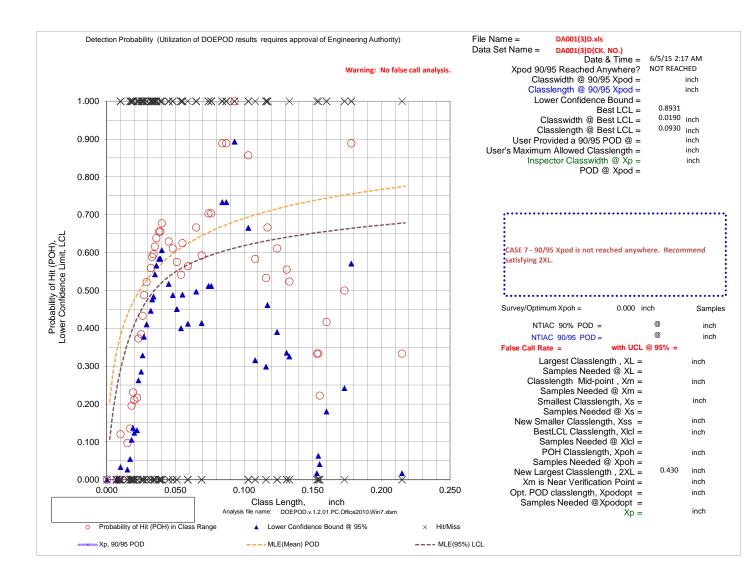


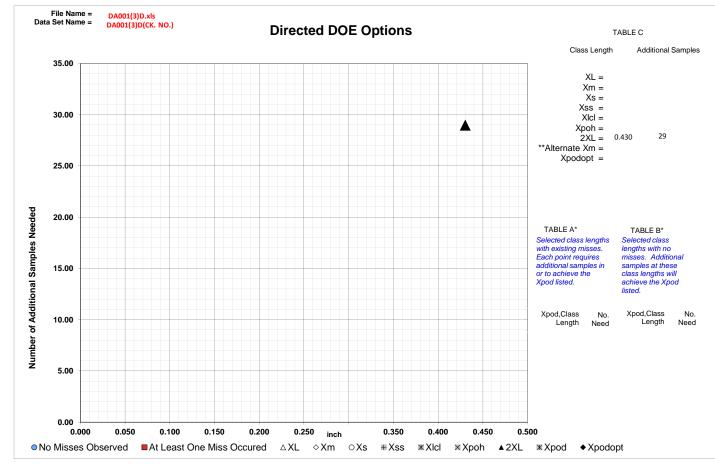
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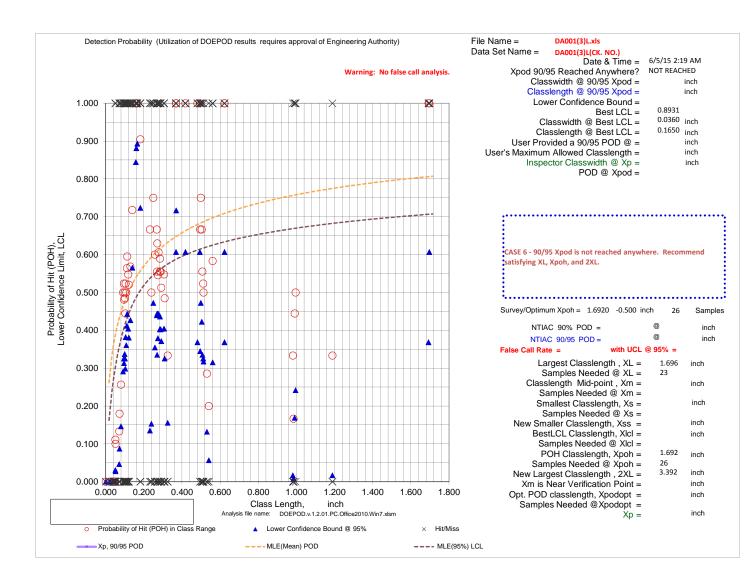


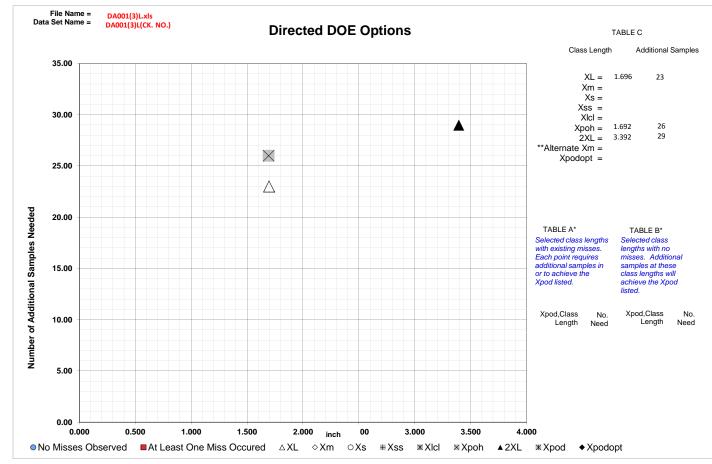
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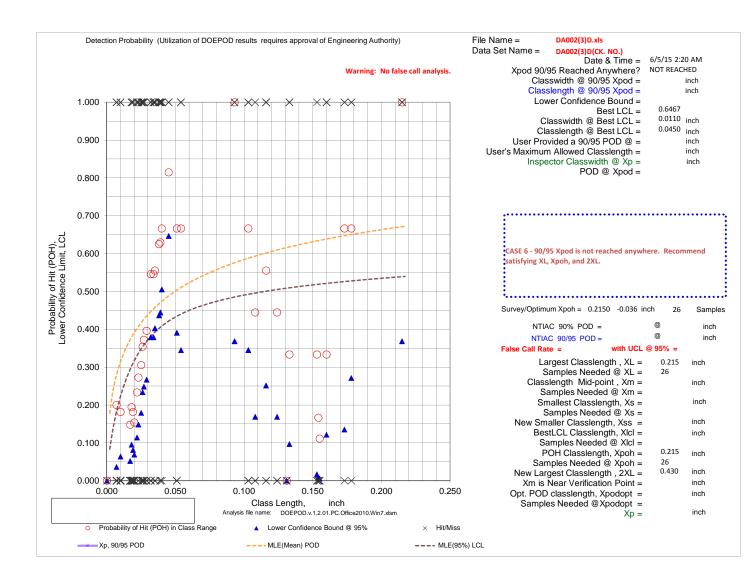


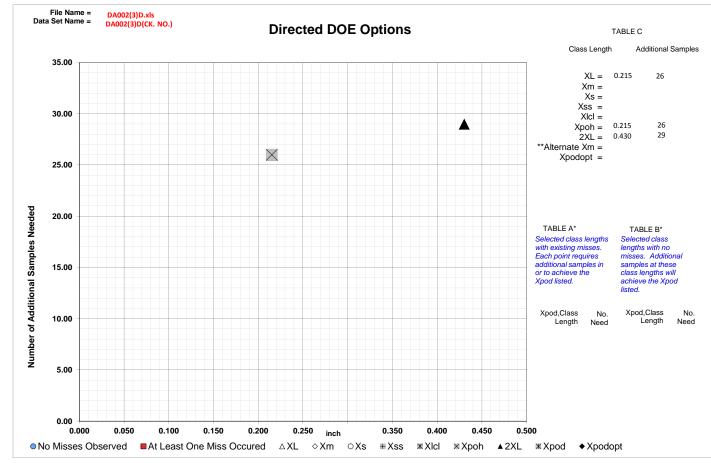
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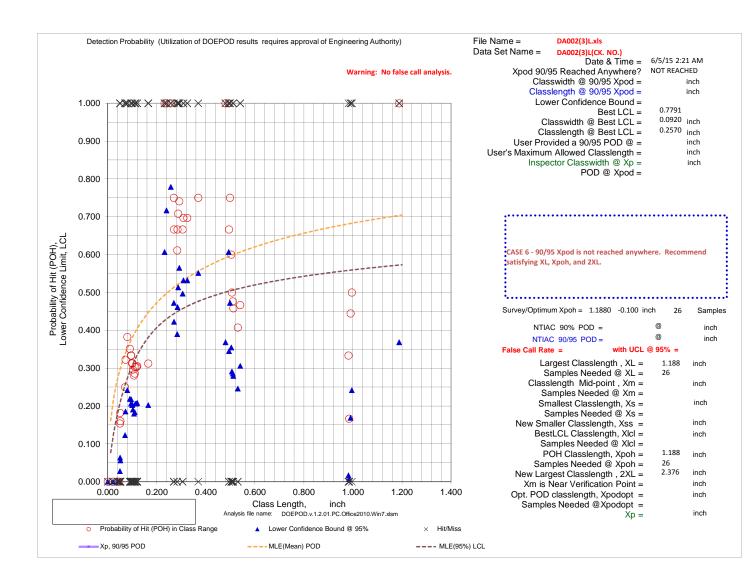


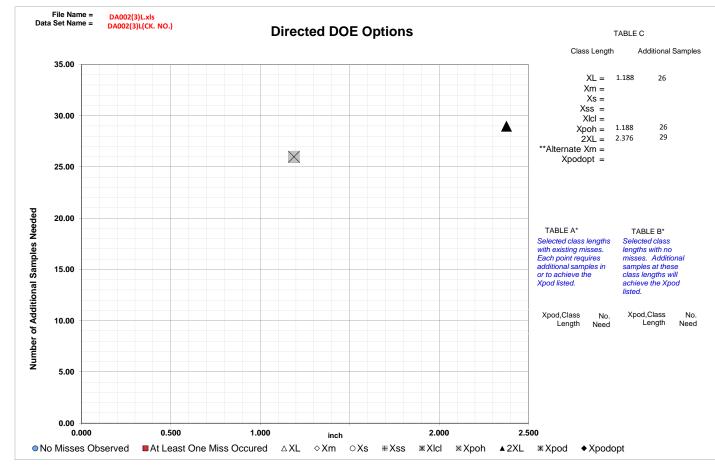
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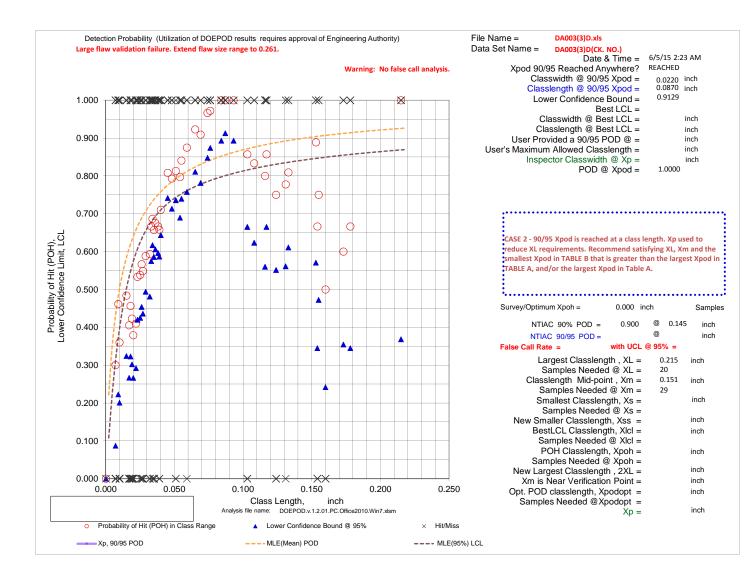


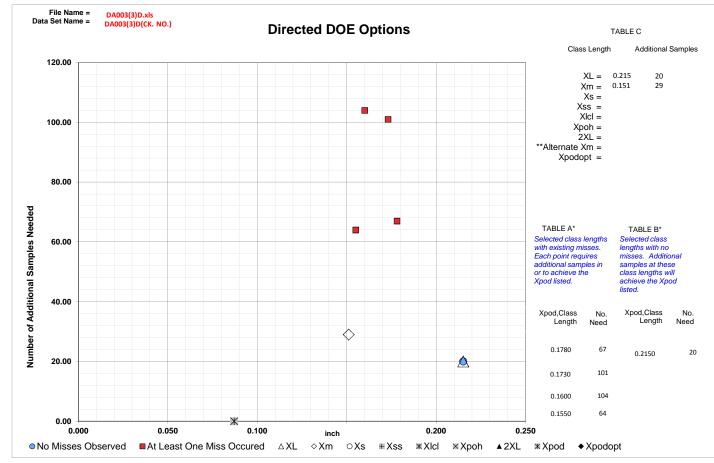
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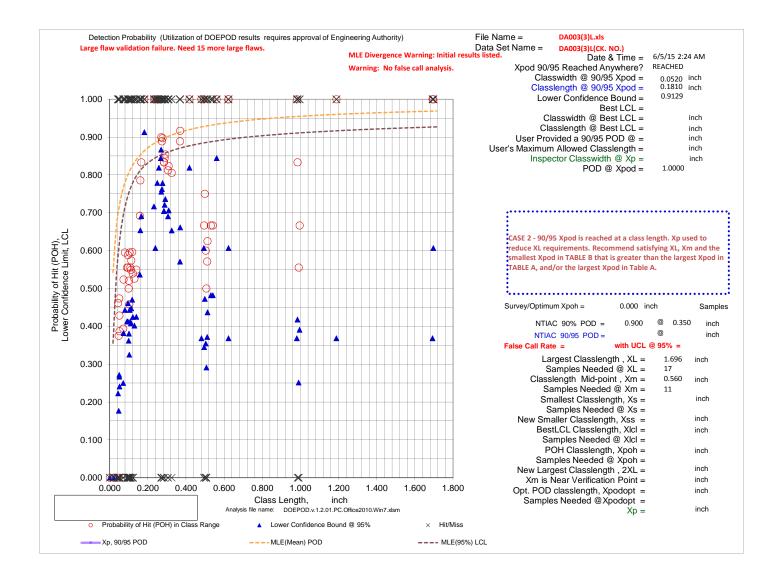


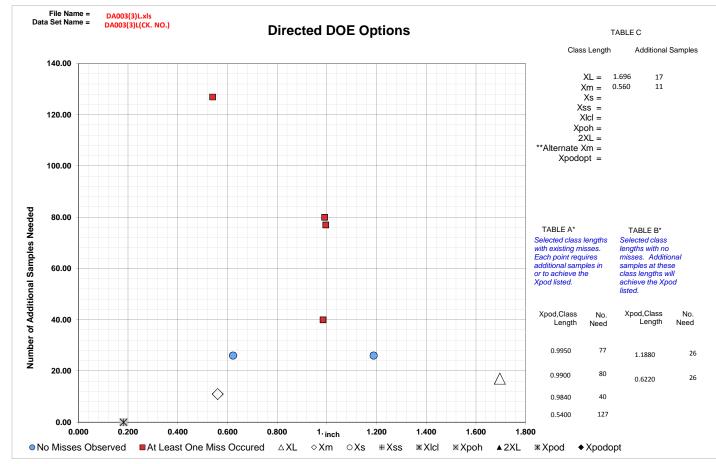
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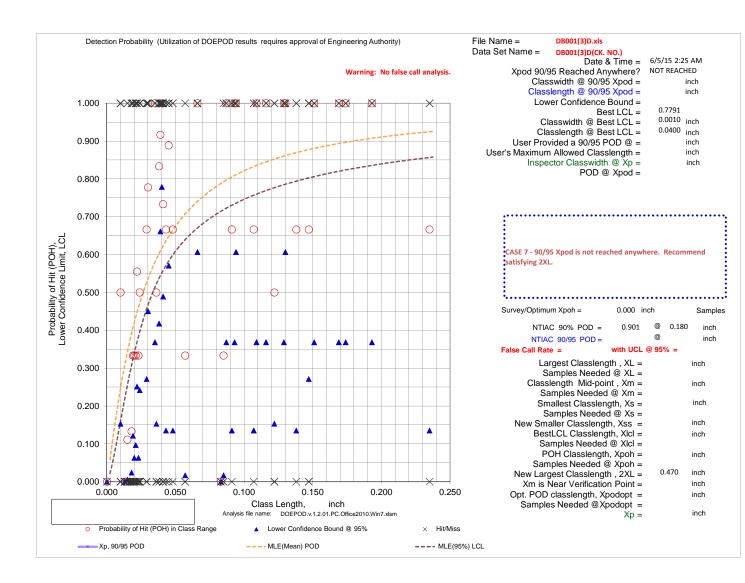


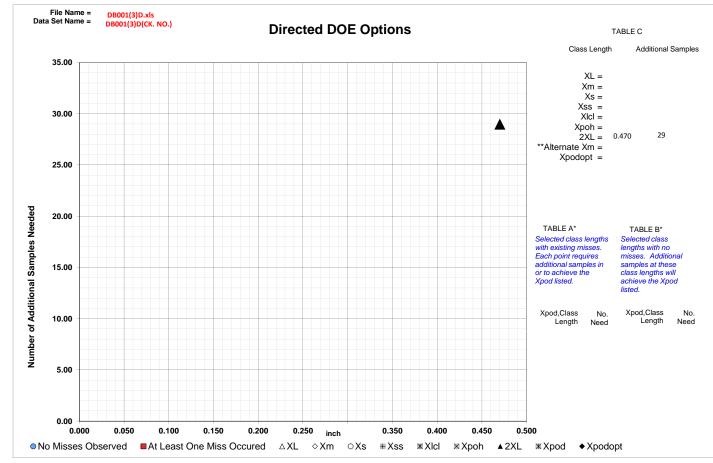
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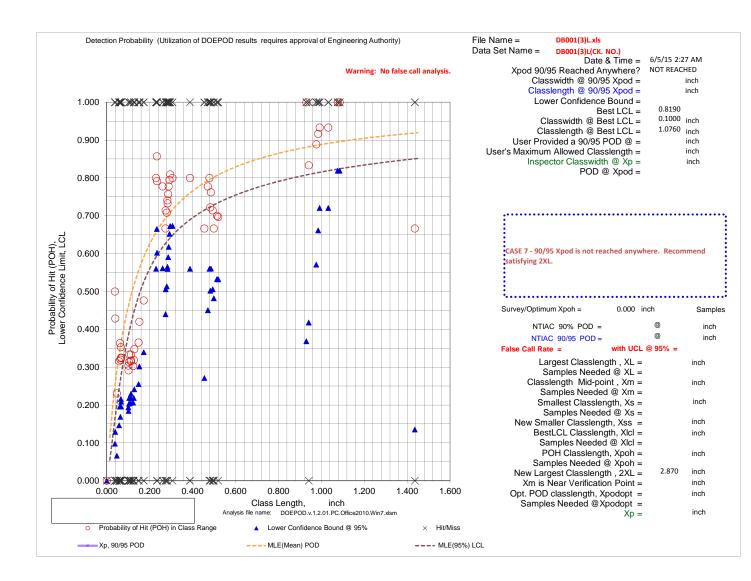


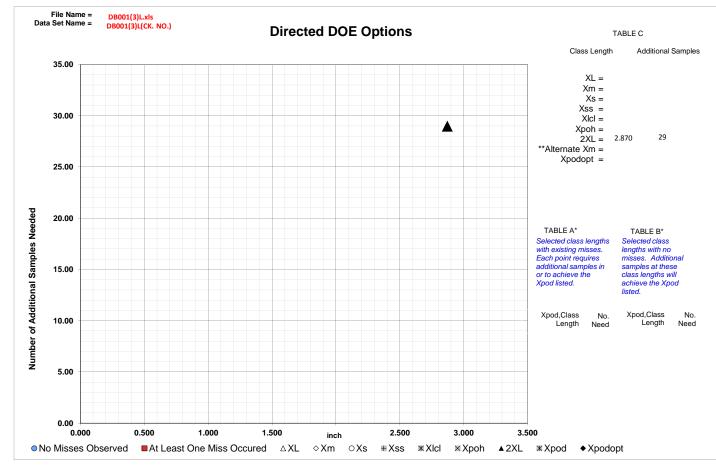
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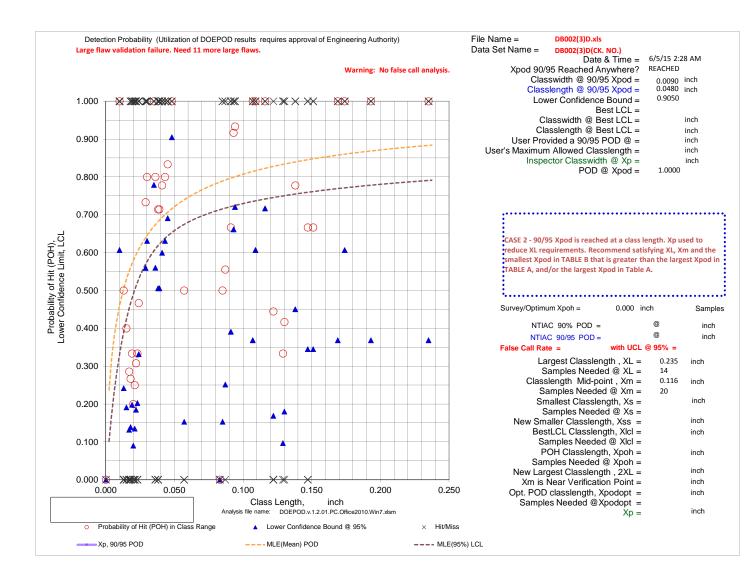


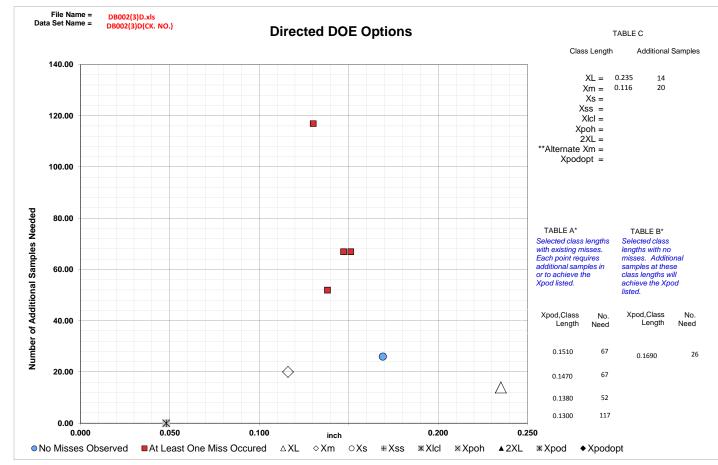
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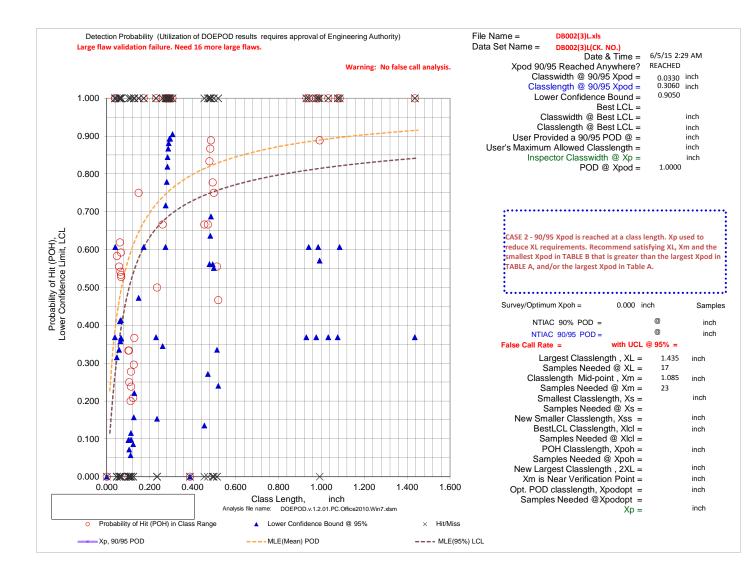


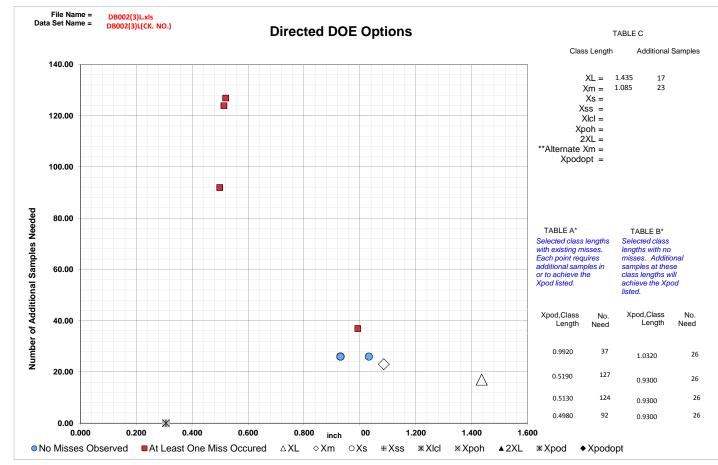
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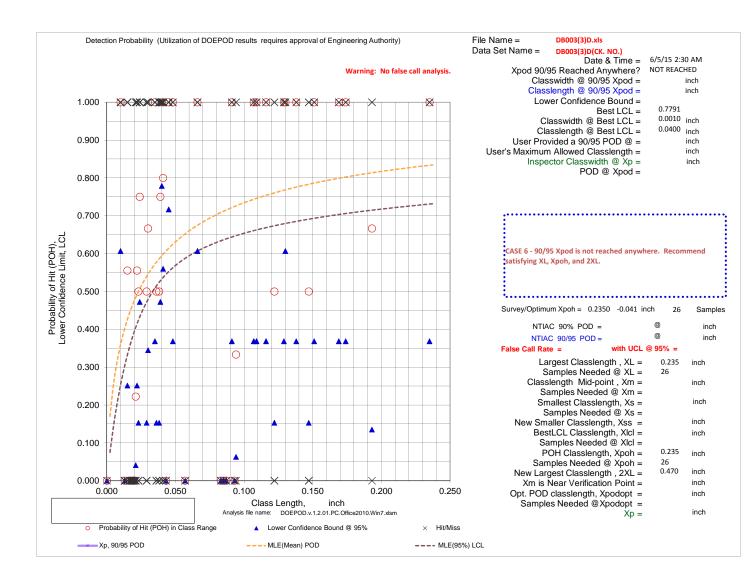


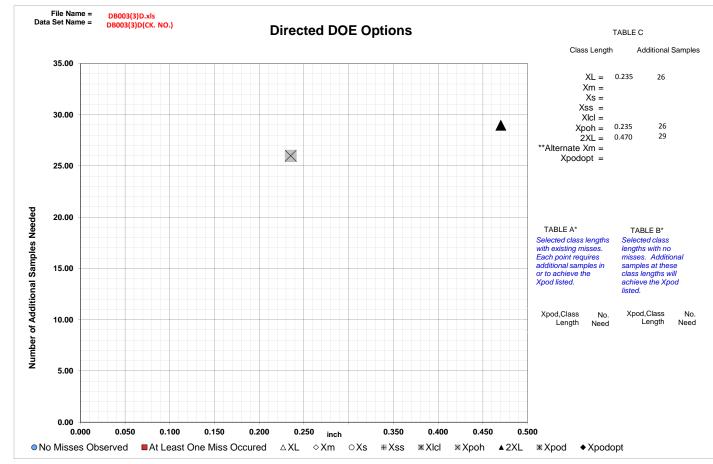
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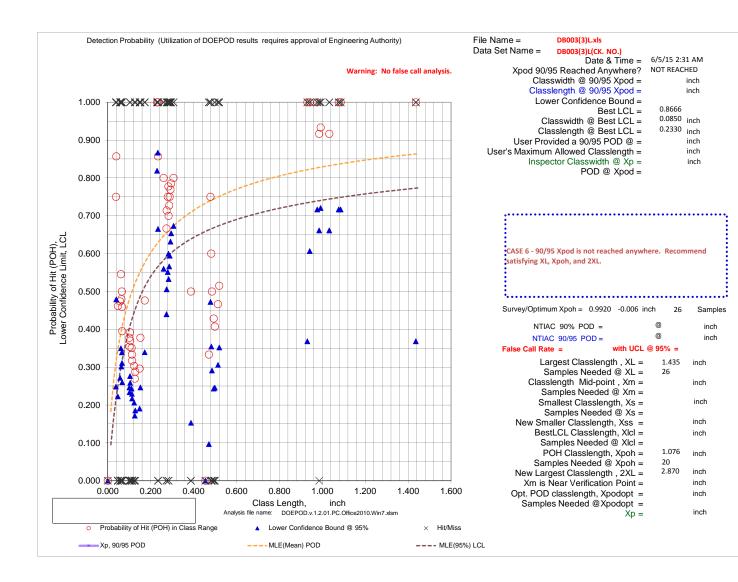


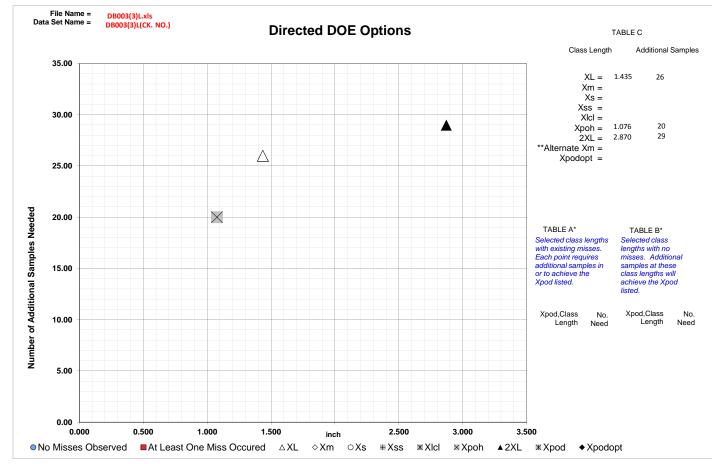
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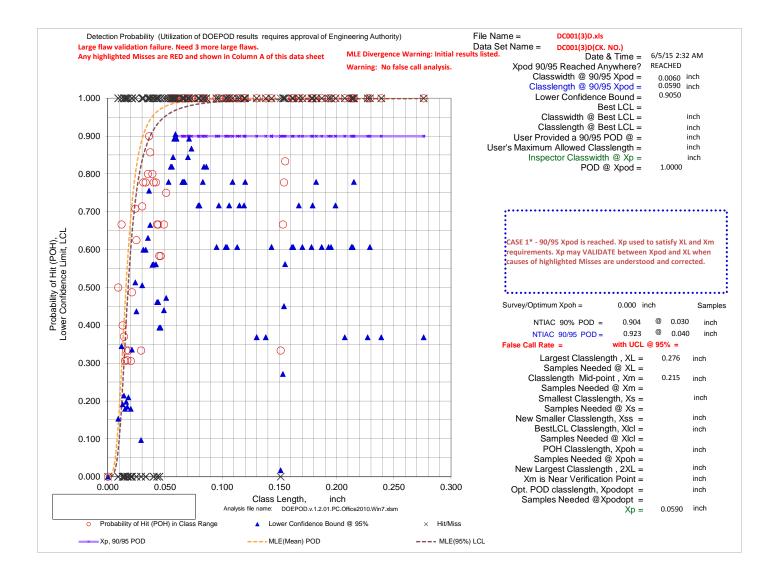


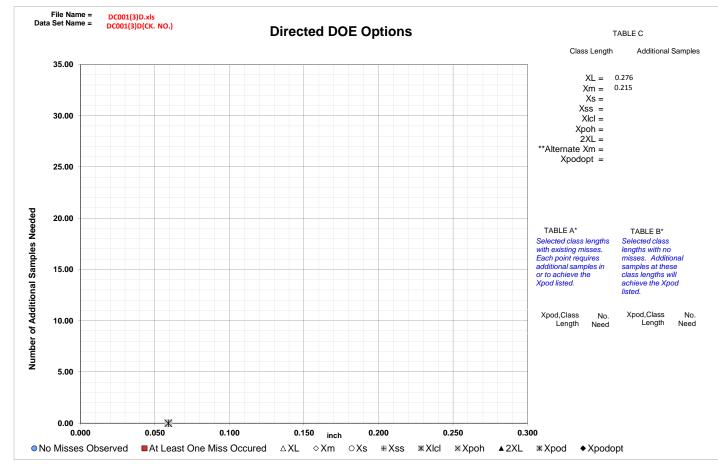
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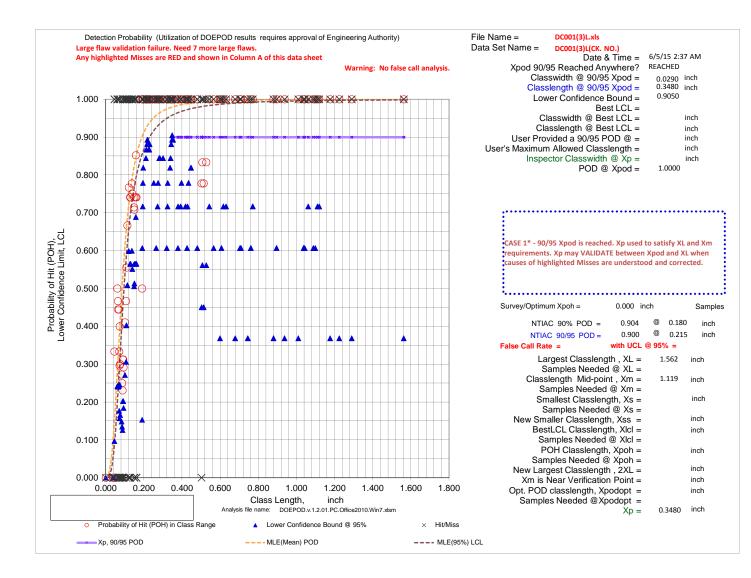


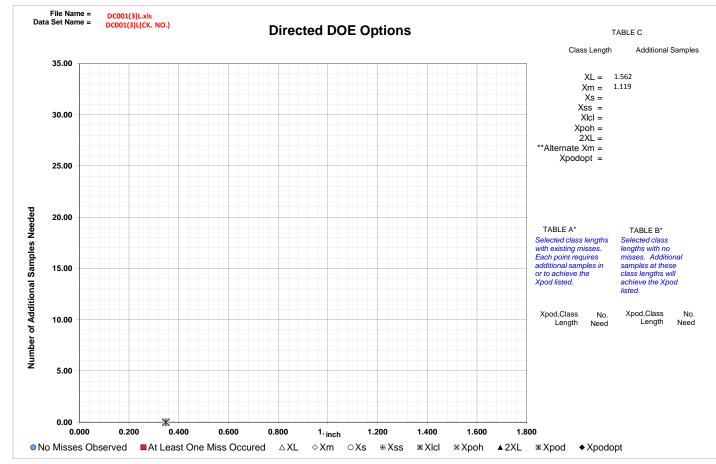
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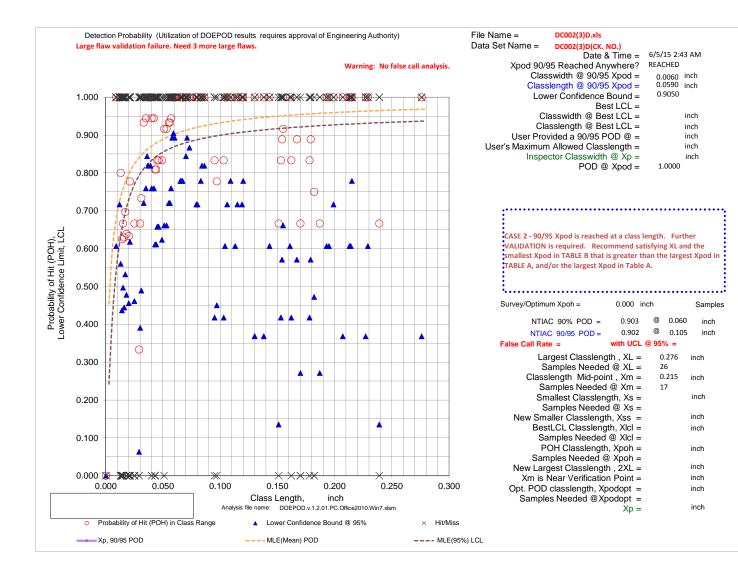


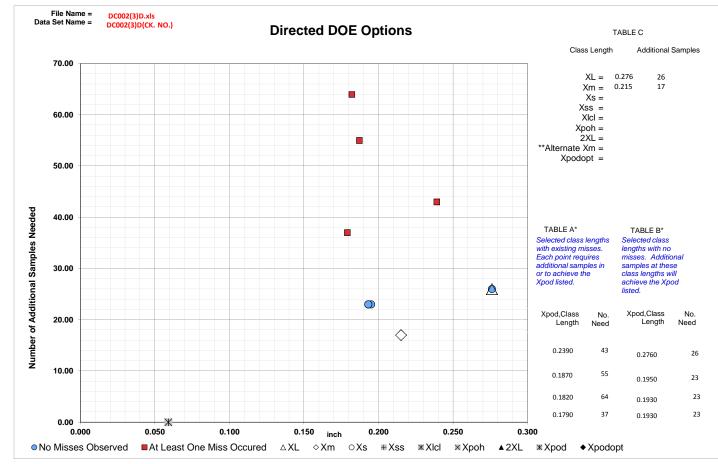
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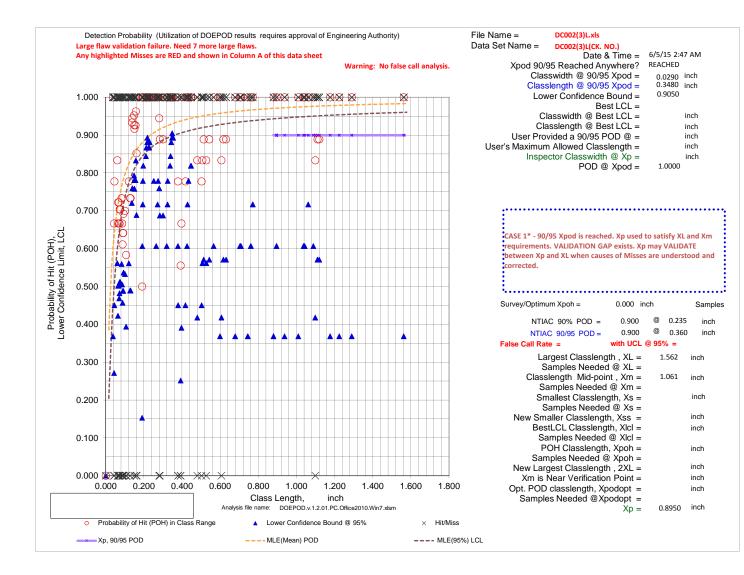


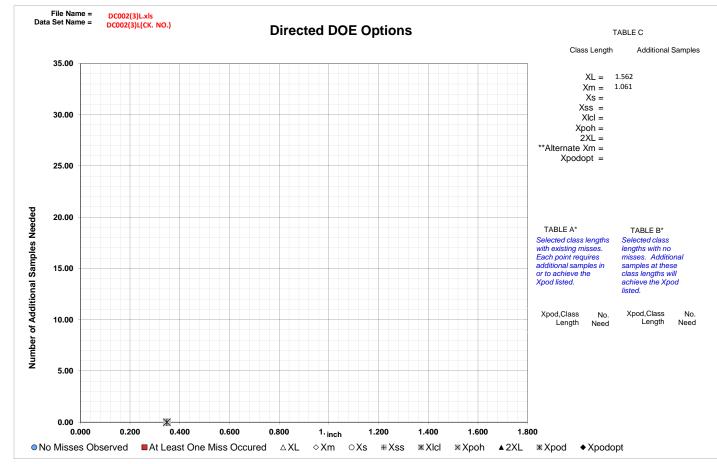
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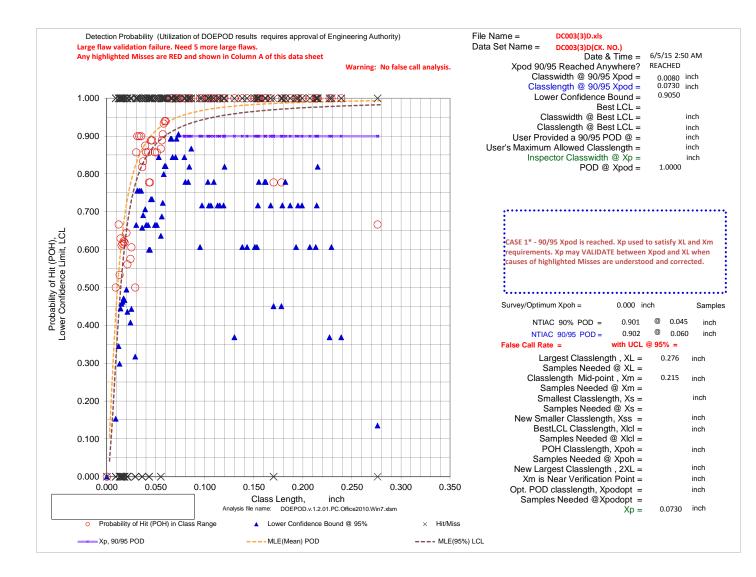


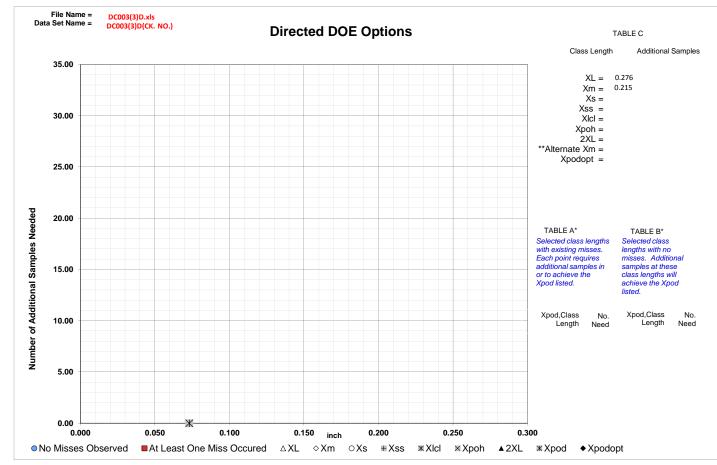
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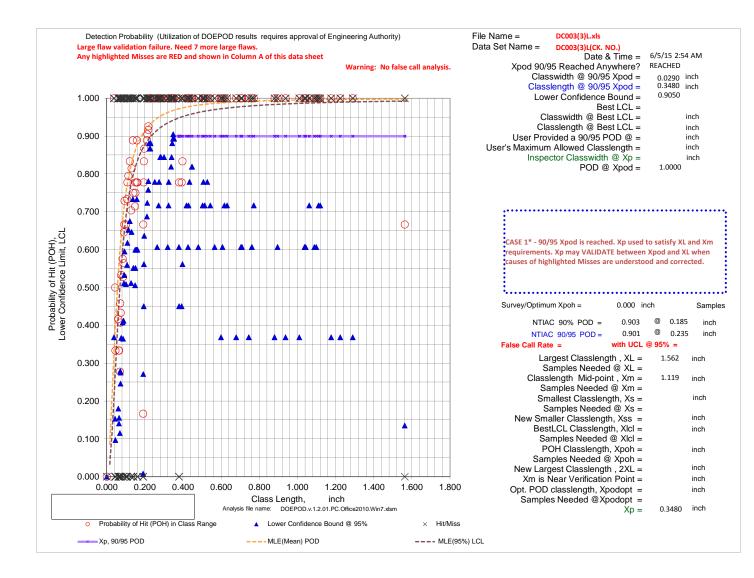


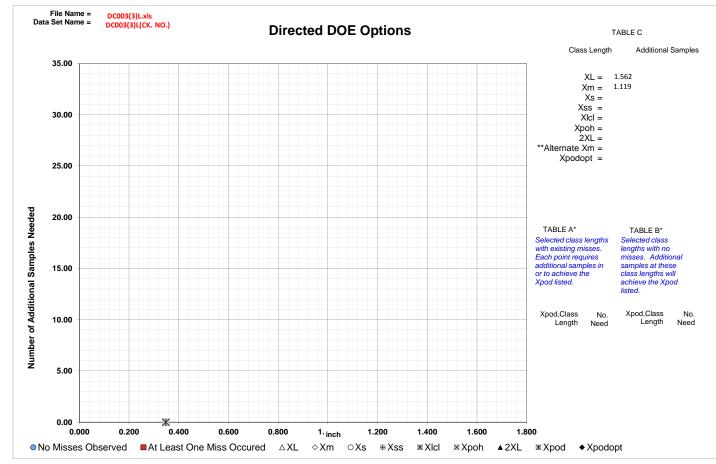
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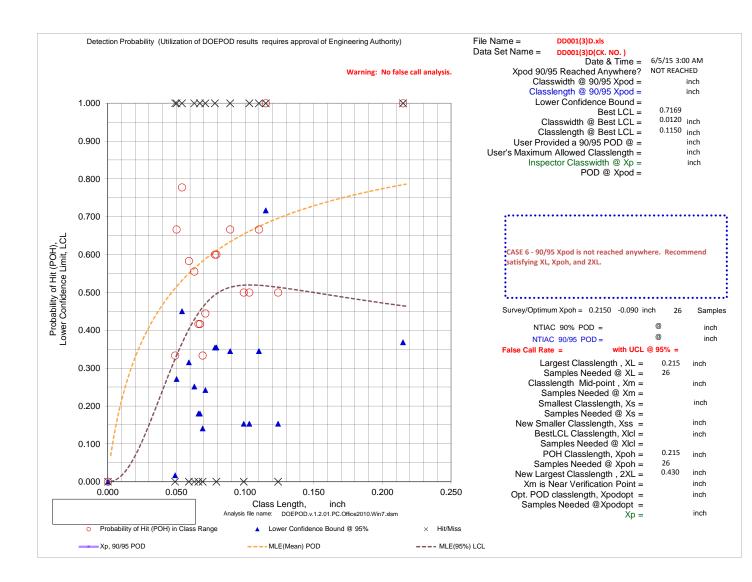


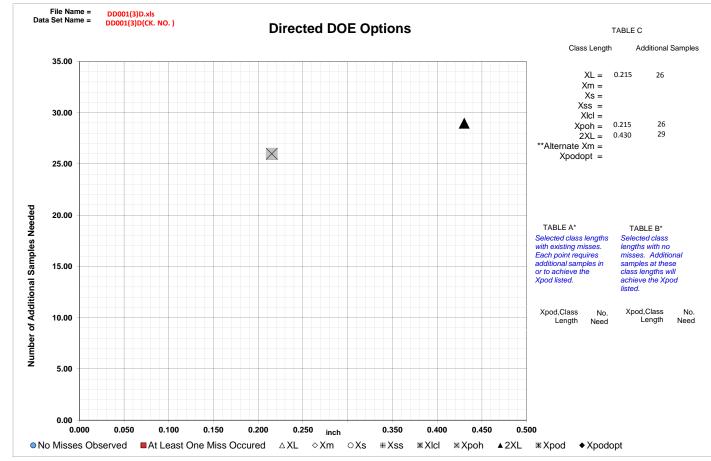
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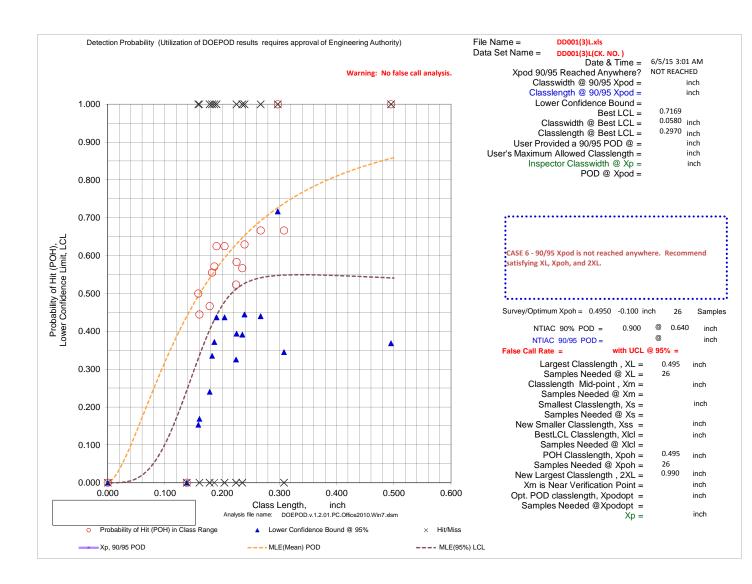


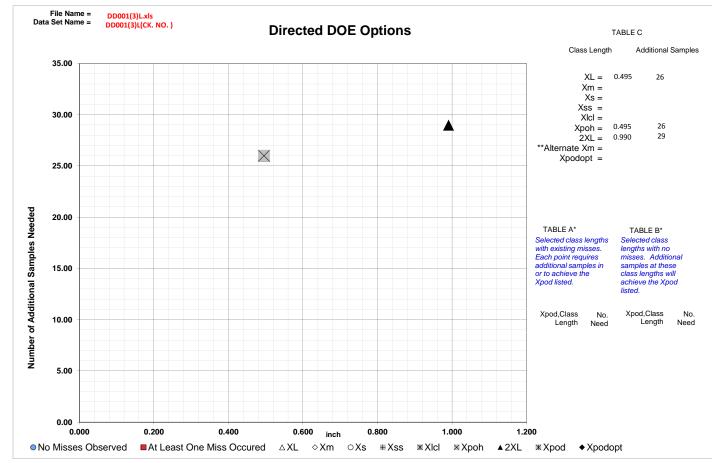
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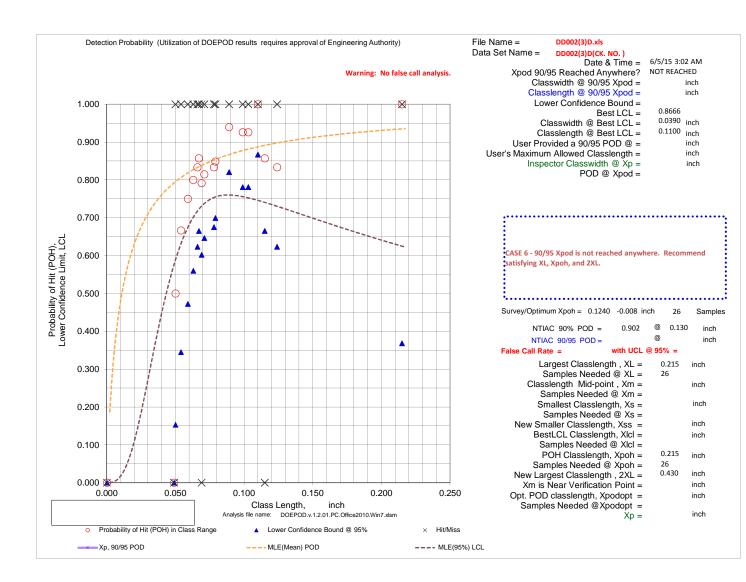


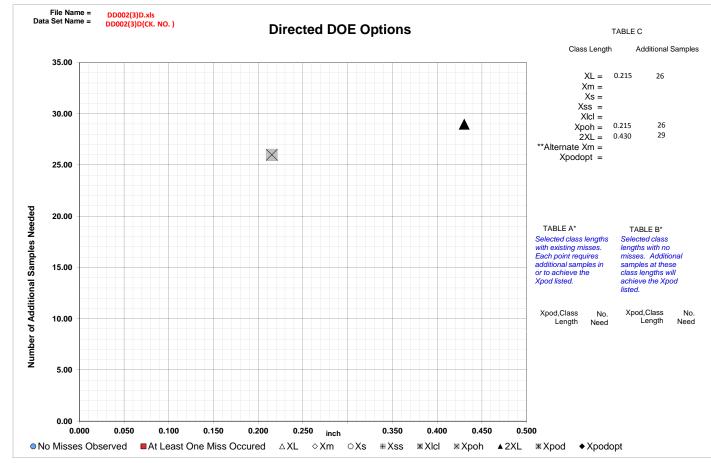
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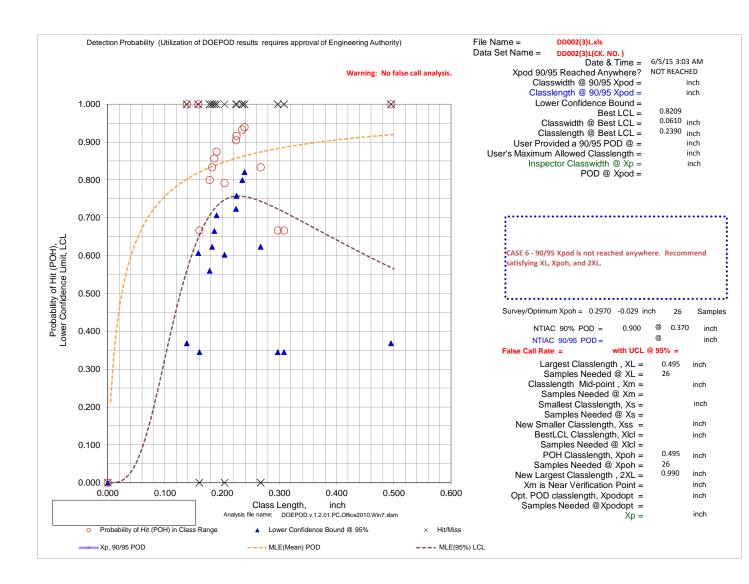


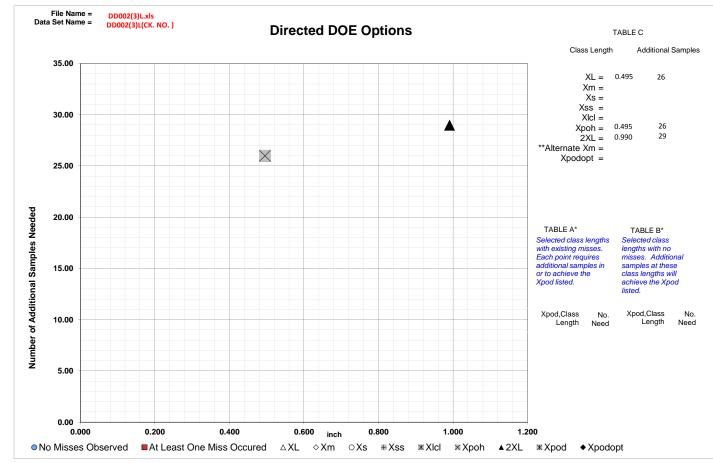
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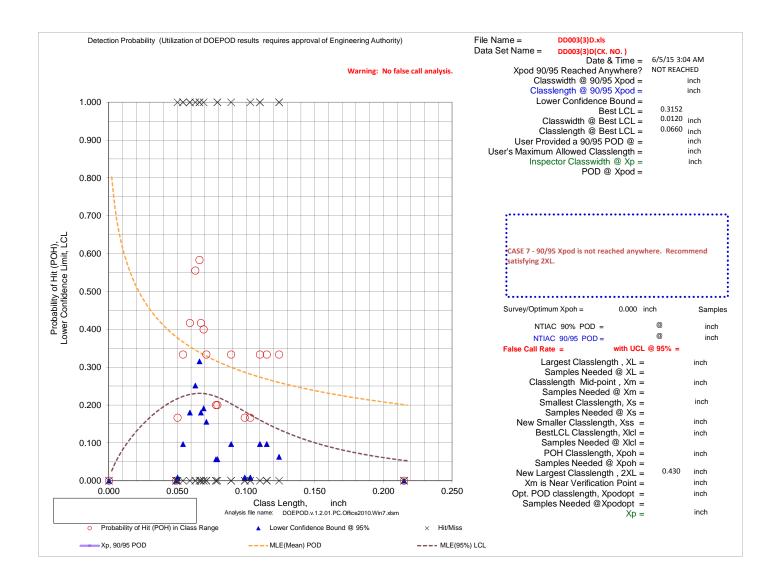


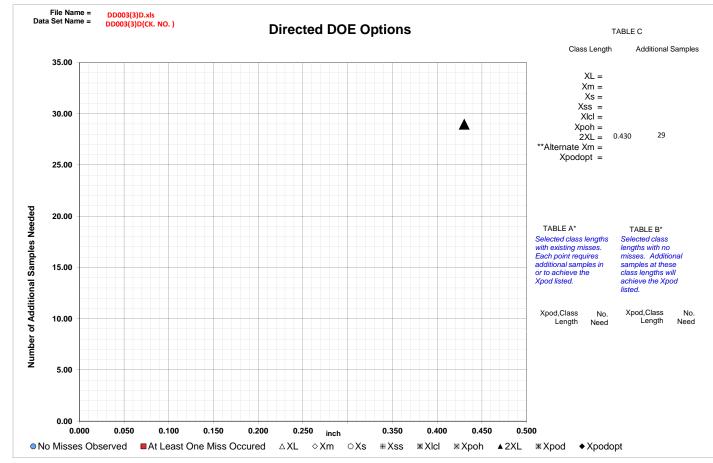
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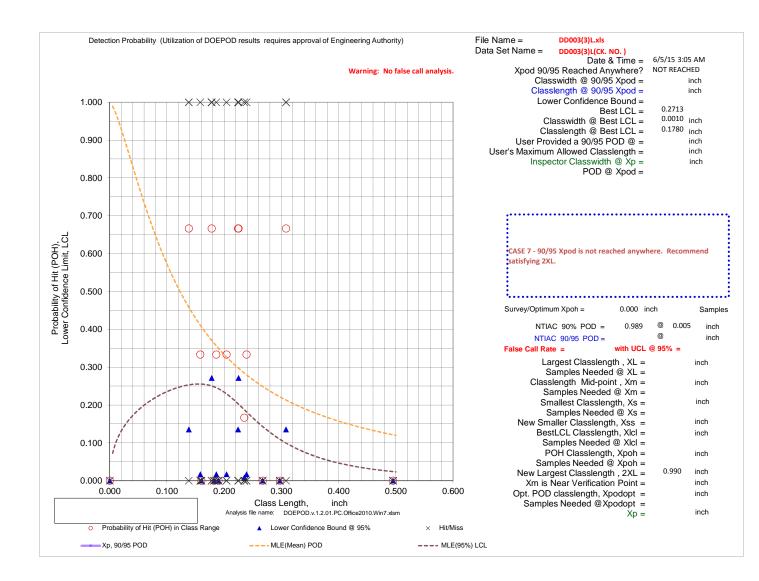


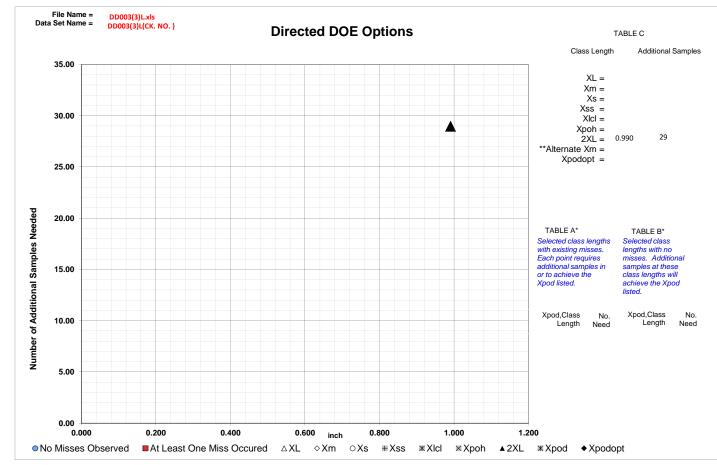
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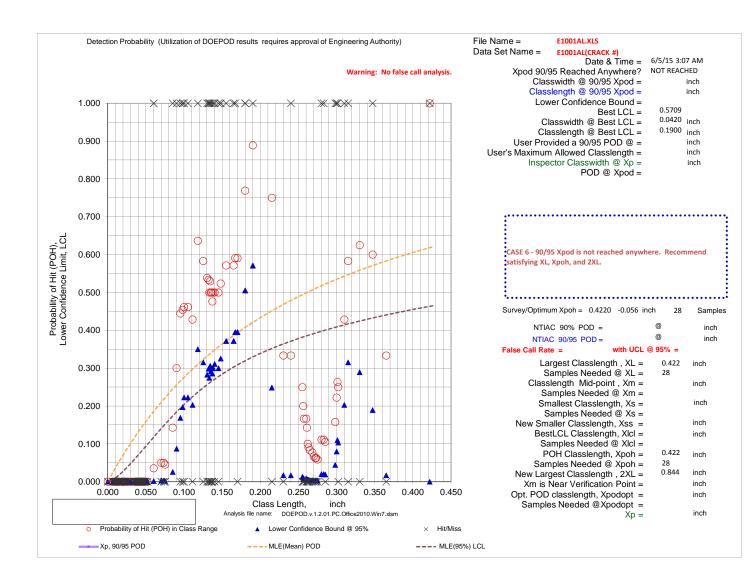


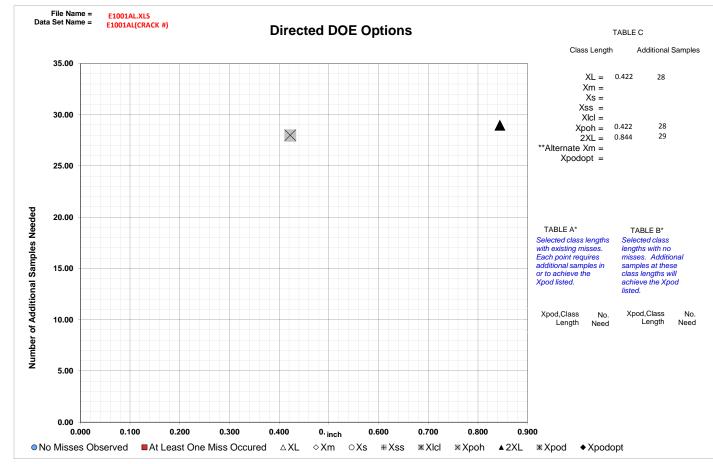
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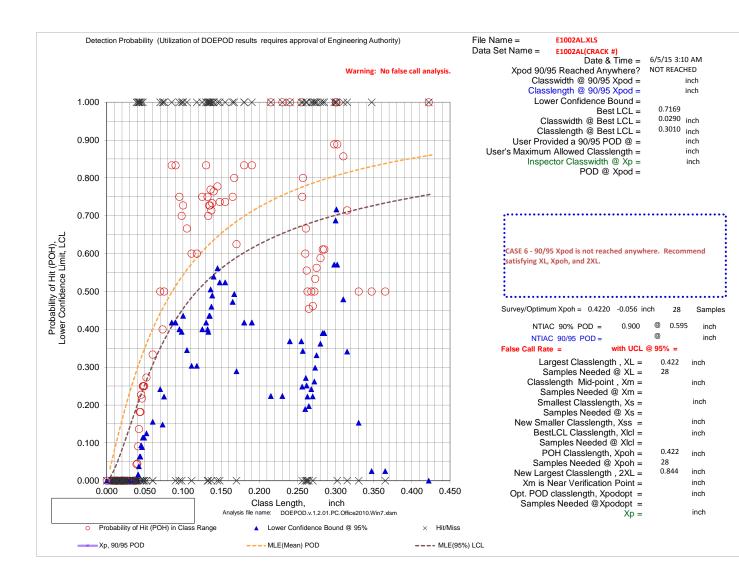


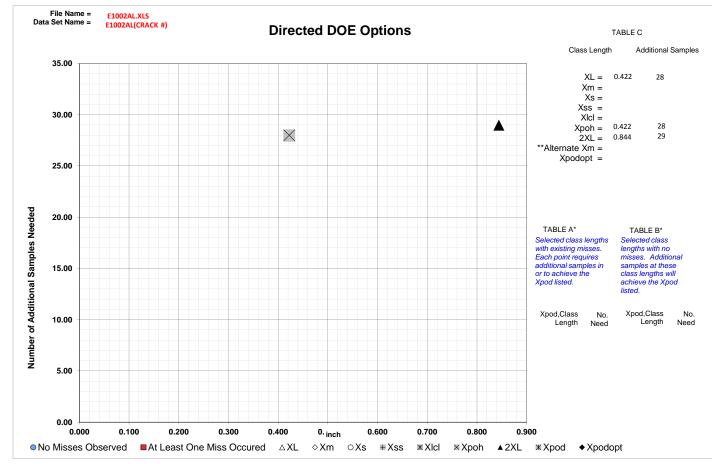
* Although Xpod appears to have been reached at a point, there are Misses at larger class lengths this indicates that the POH function may be oscillatory. This needs to be checked. The class lengths listed in Table A exhibited misses and resulted in LCL below 0.90. Only largest 4 class lengths are shown.

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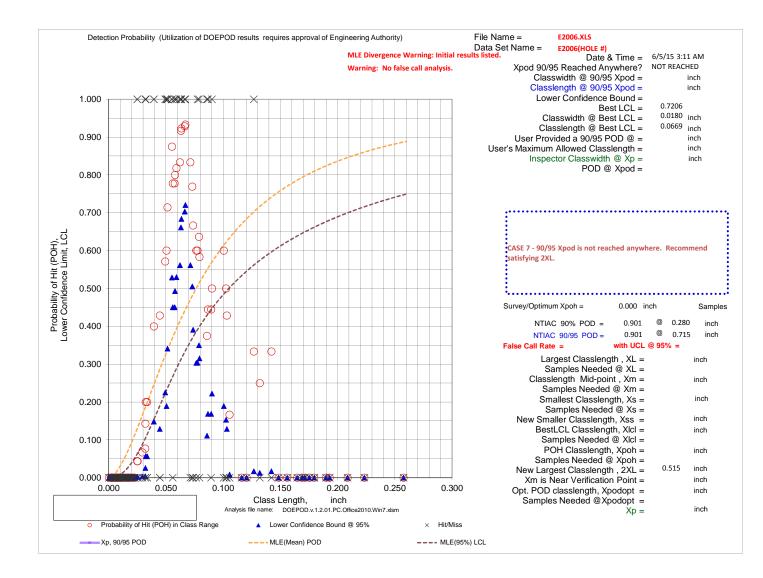


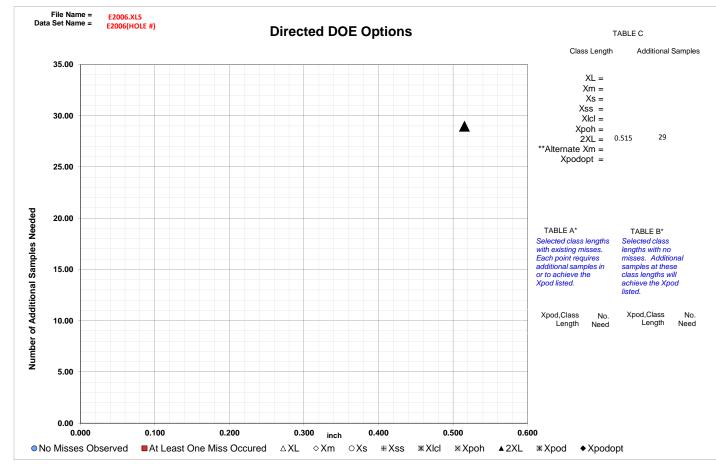
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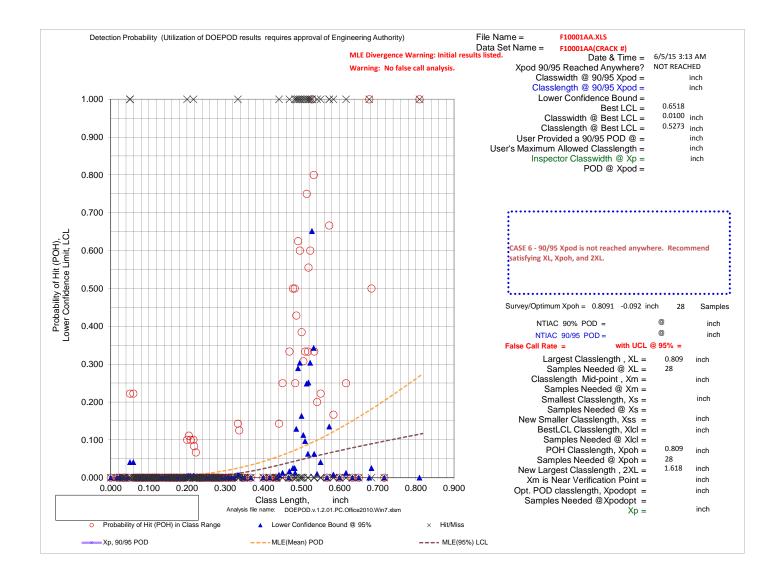


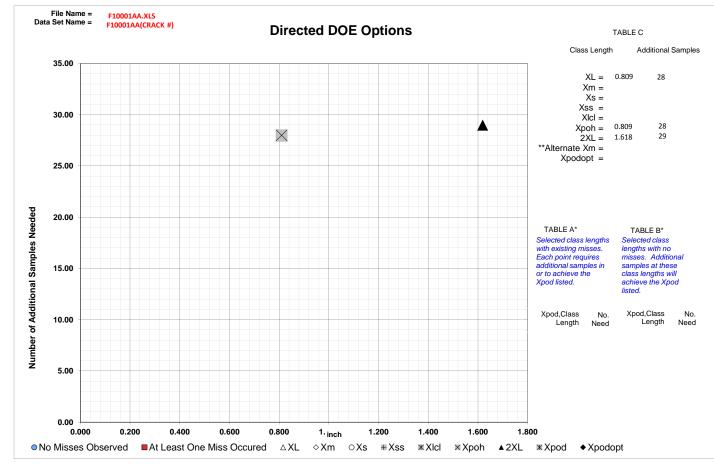
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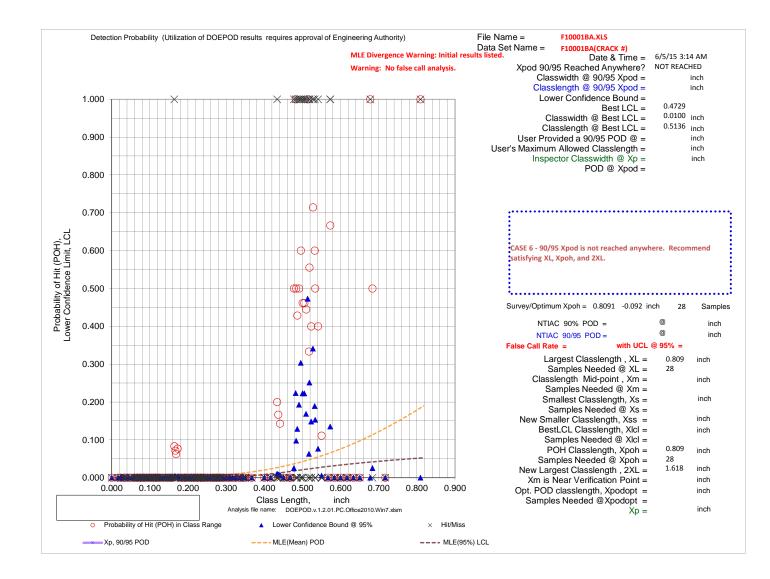


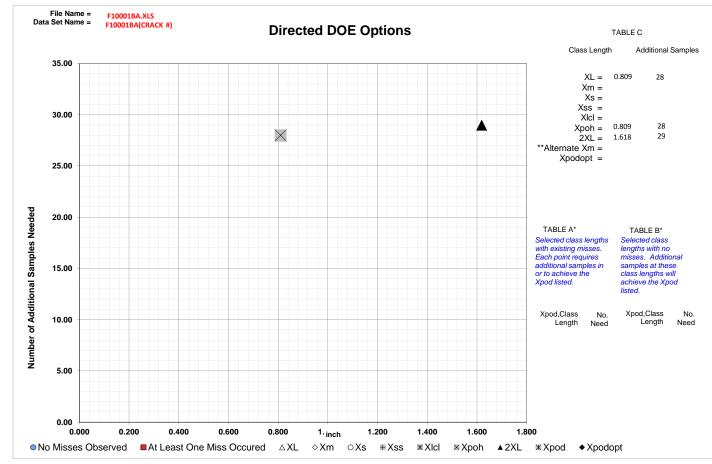
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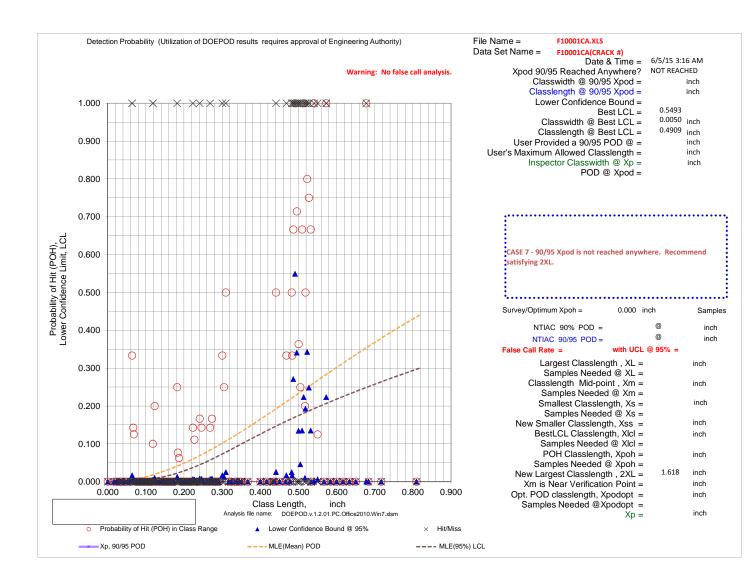


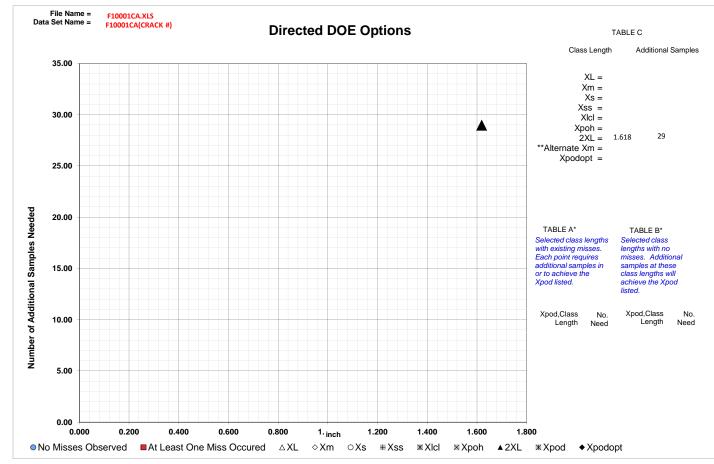
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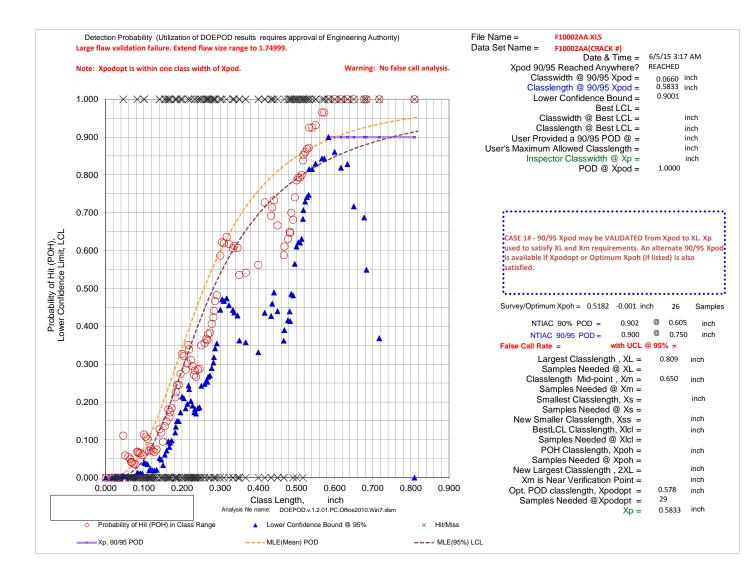


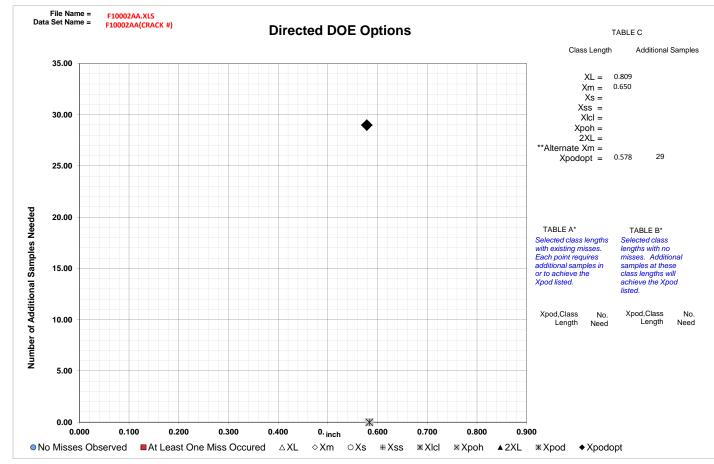
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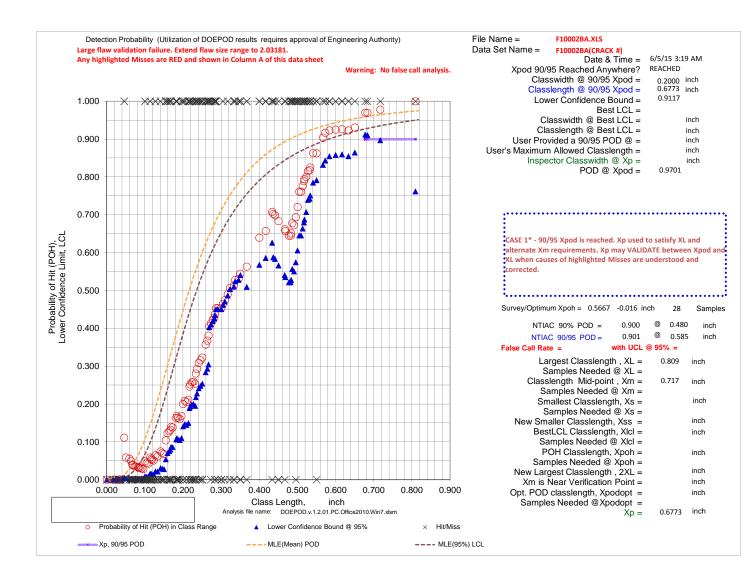


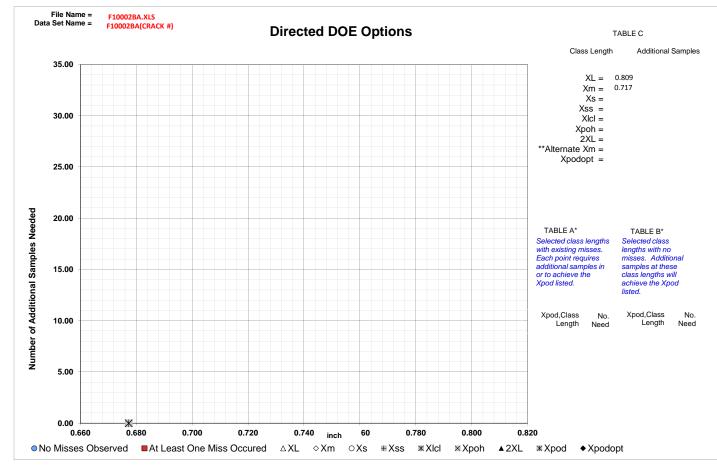
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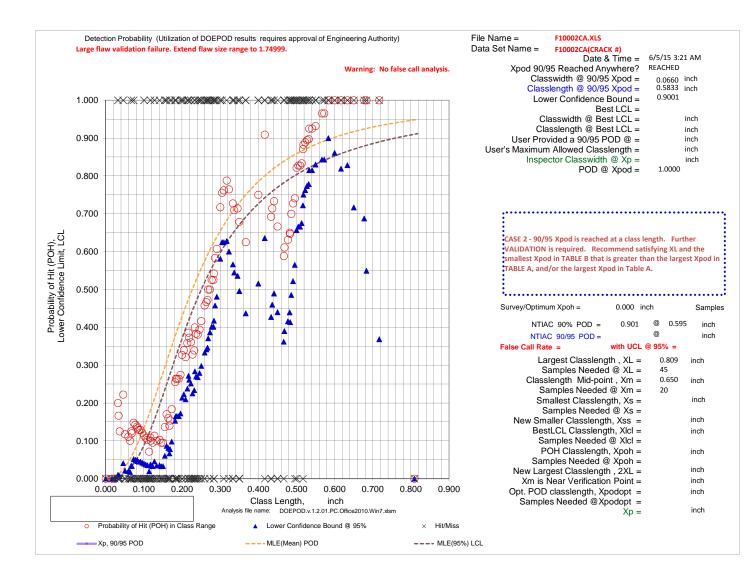


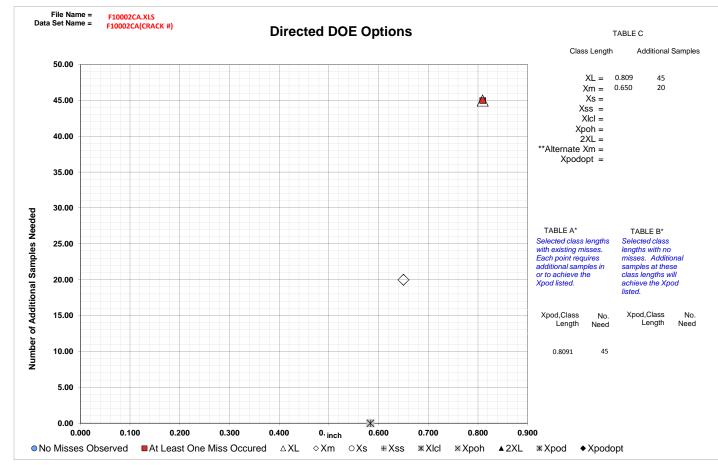
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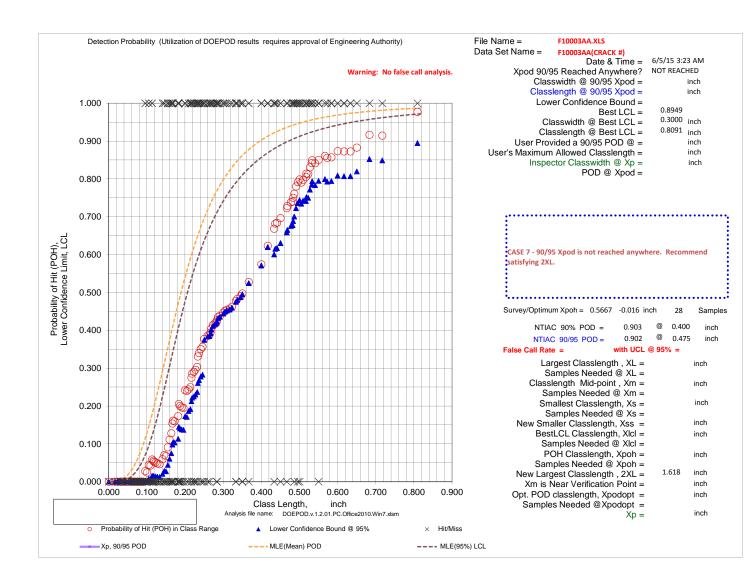


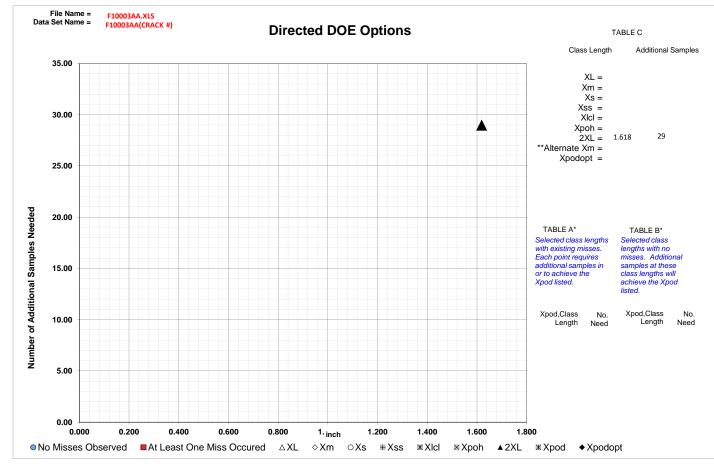
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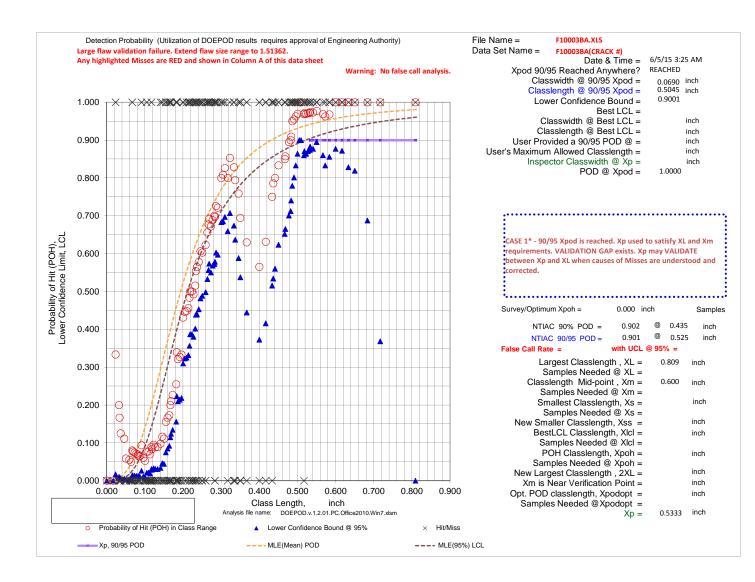


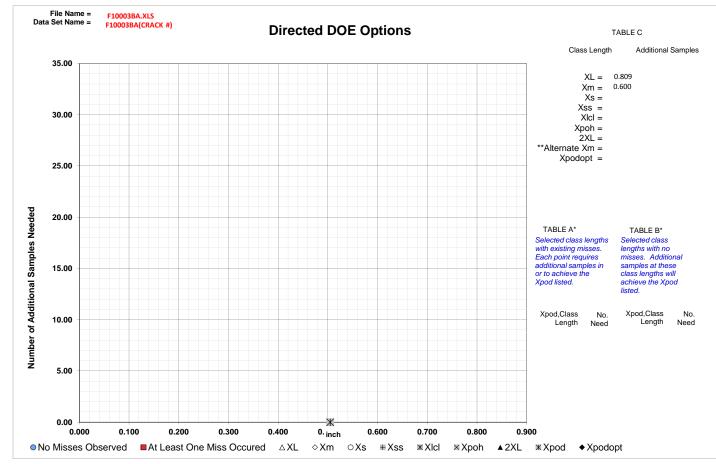
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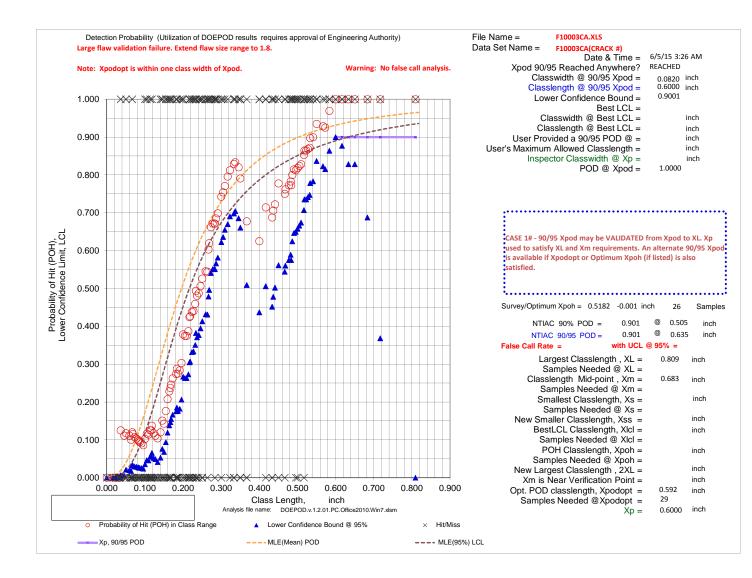


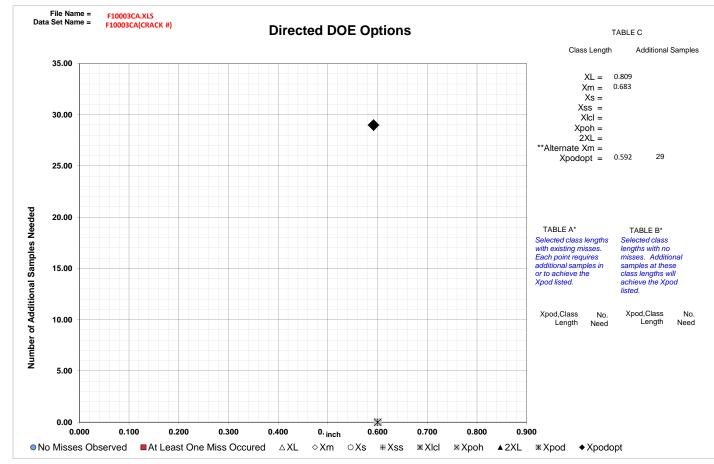
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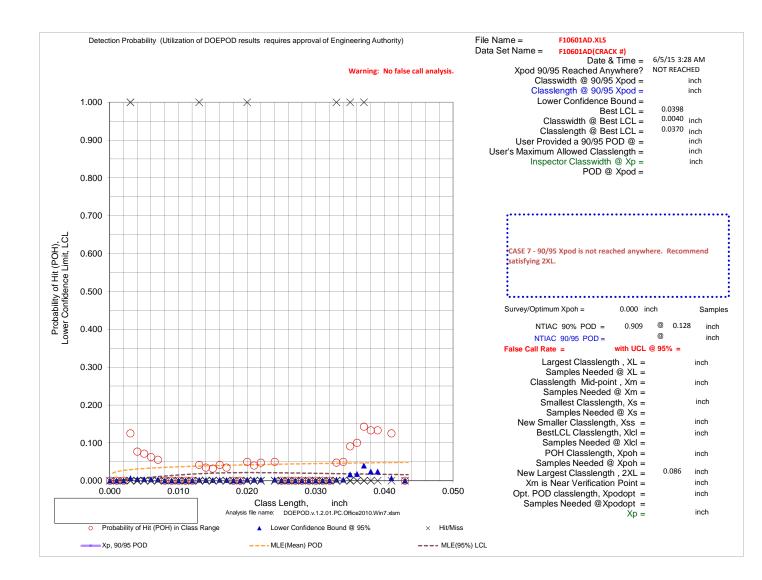


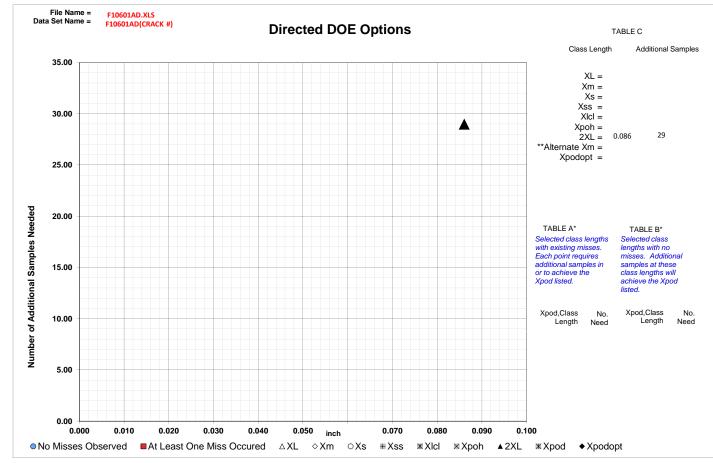
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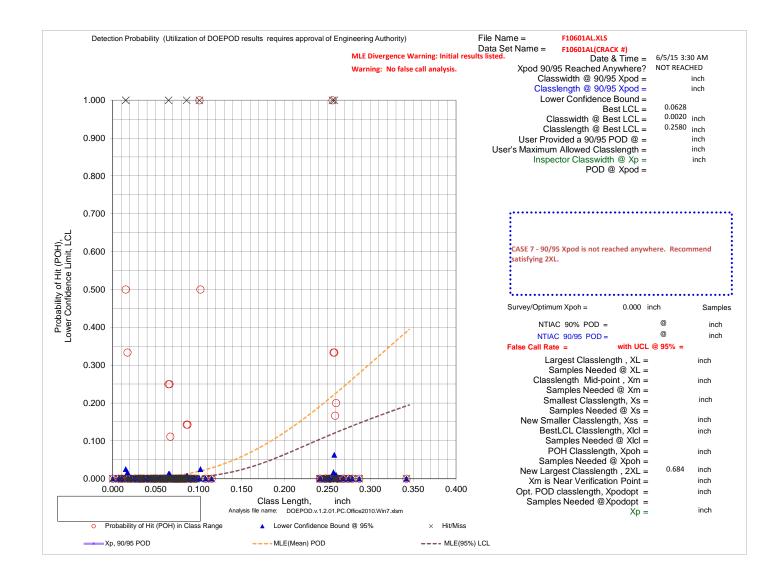


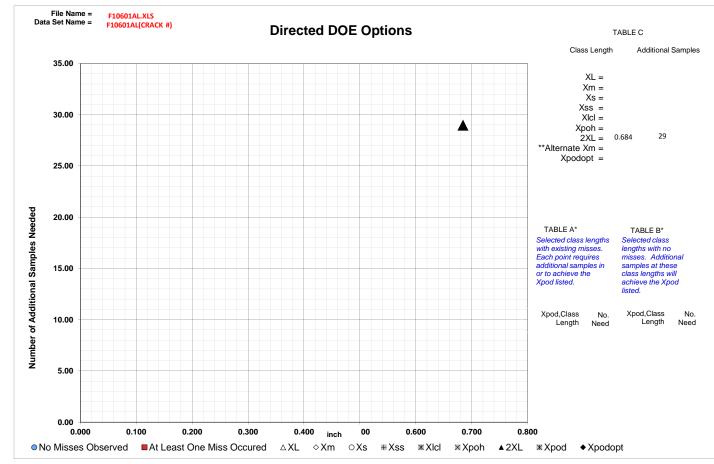
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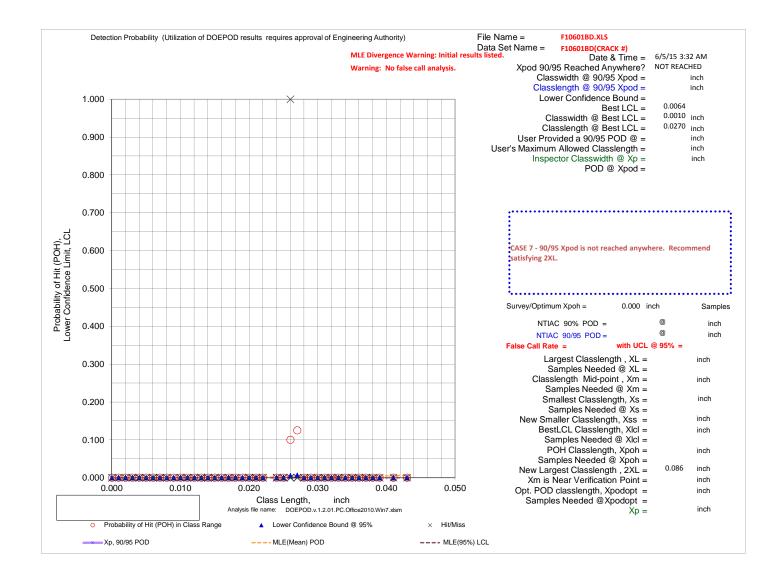


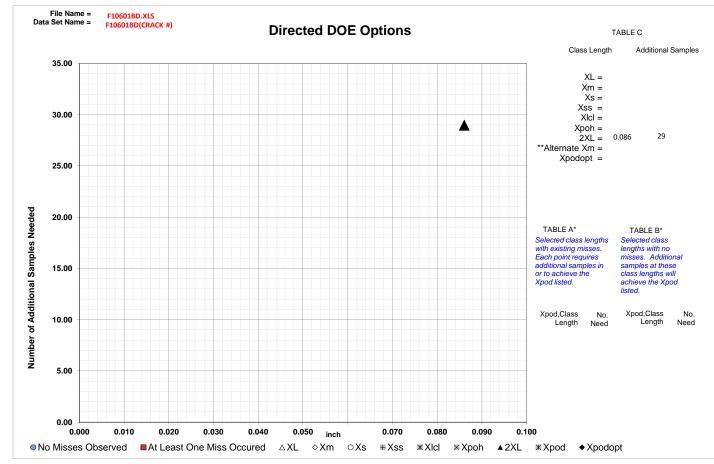
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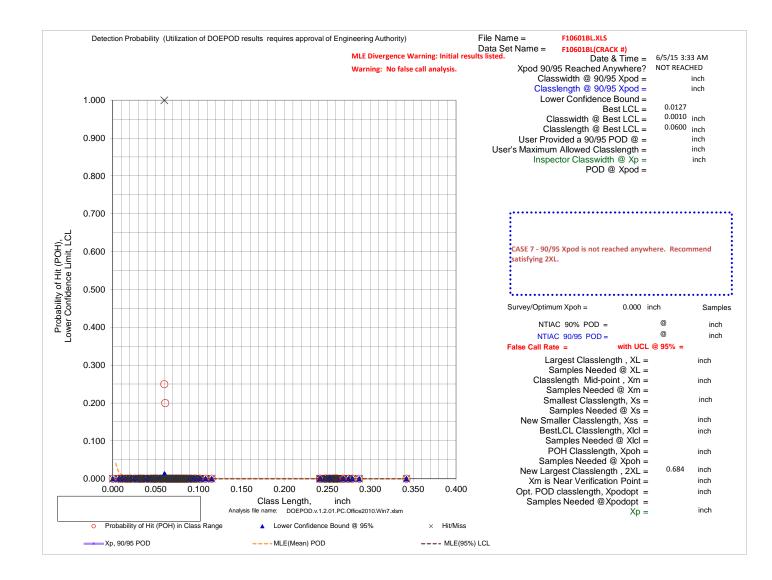


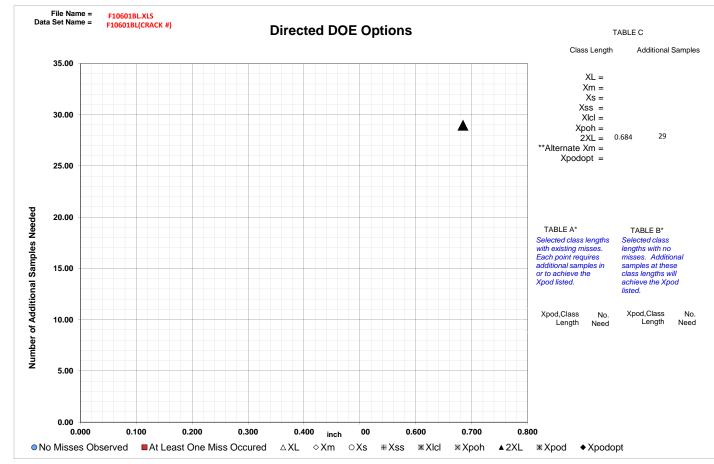
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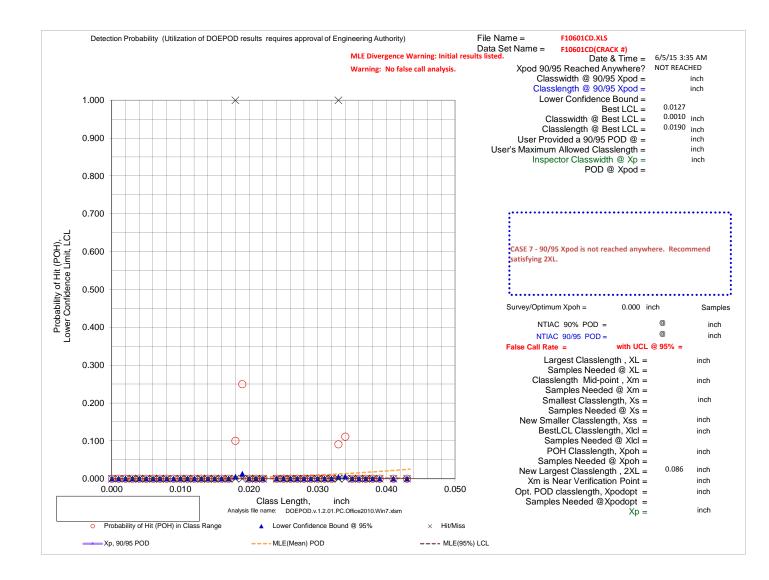


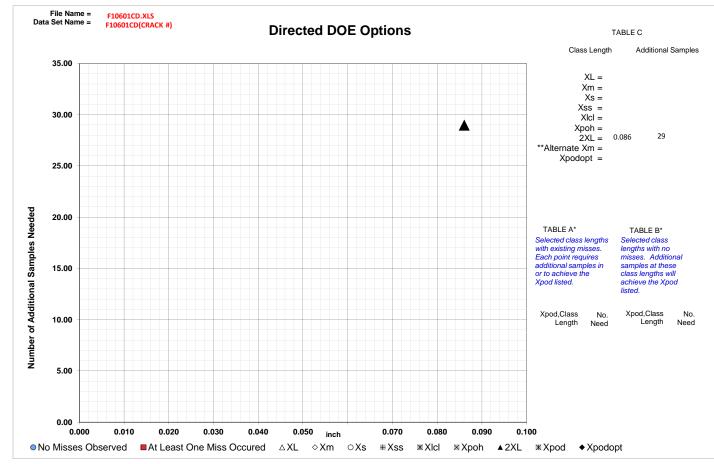
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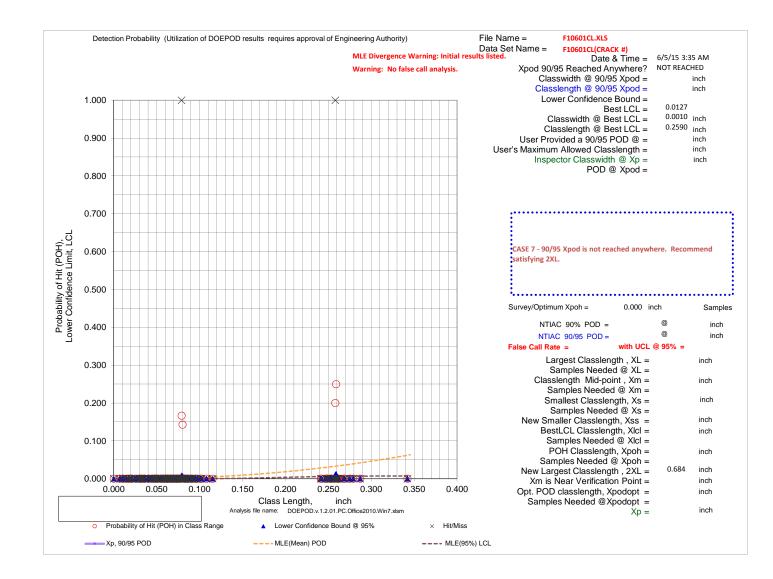


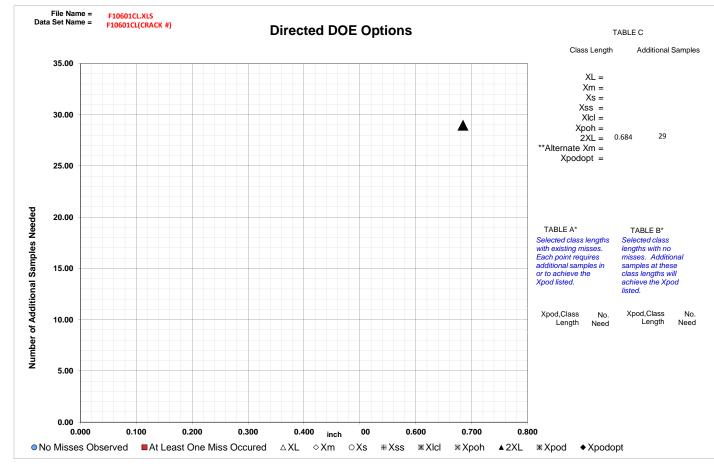
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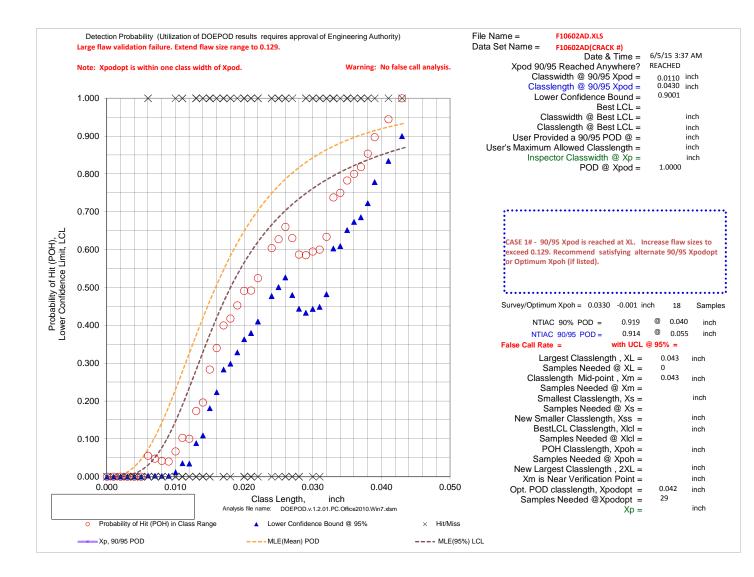


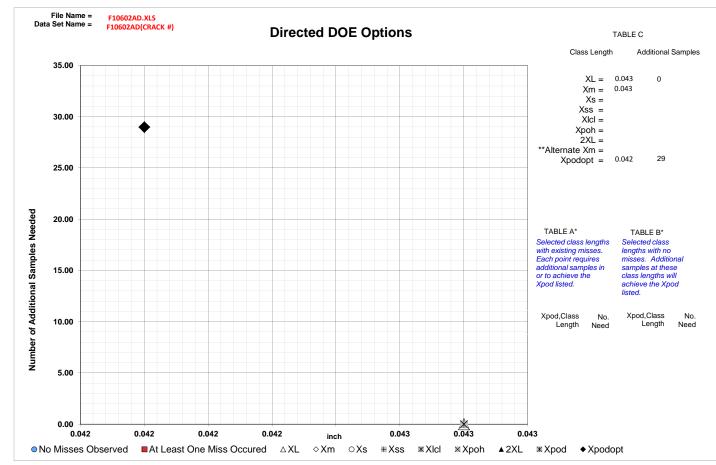
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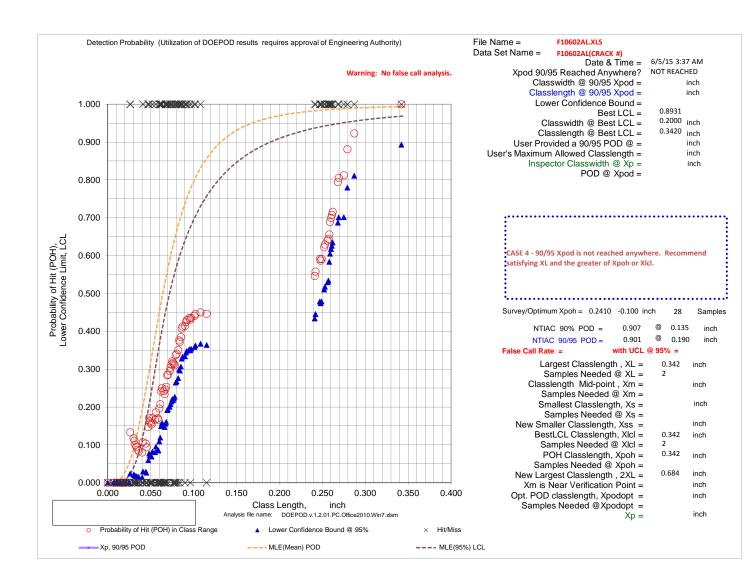


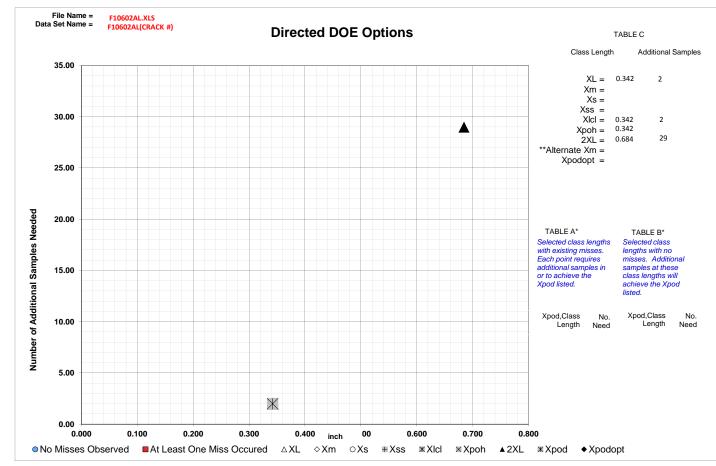
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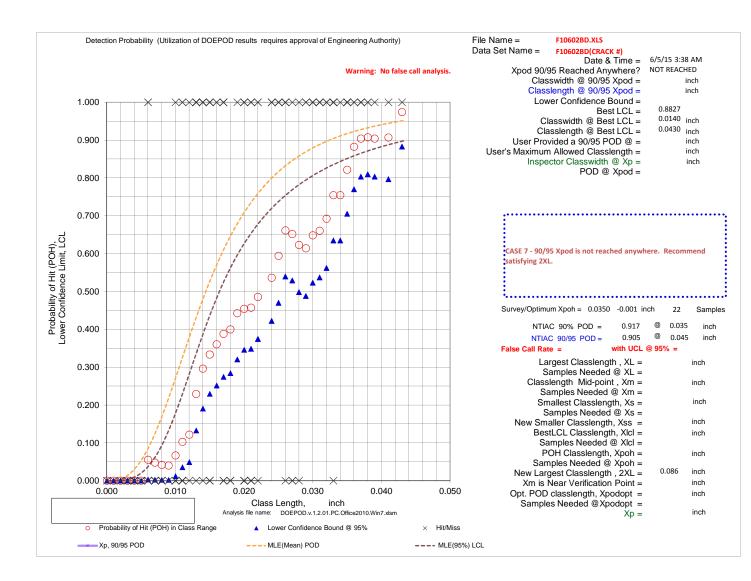


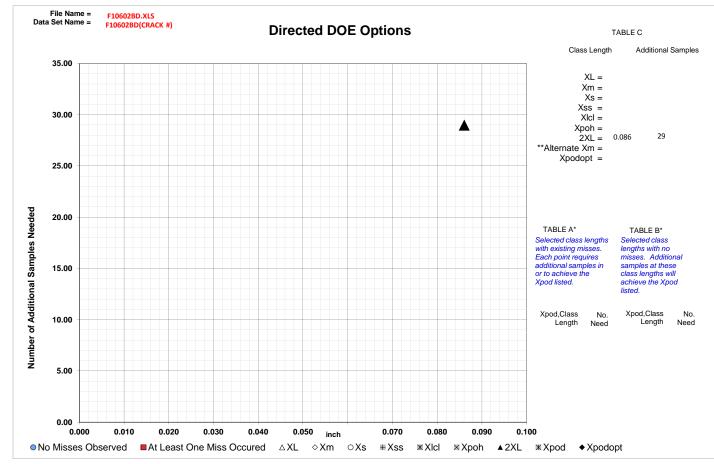
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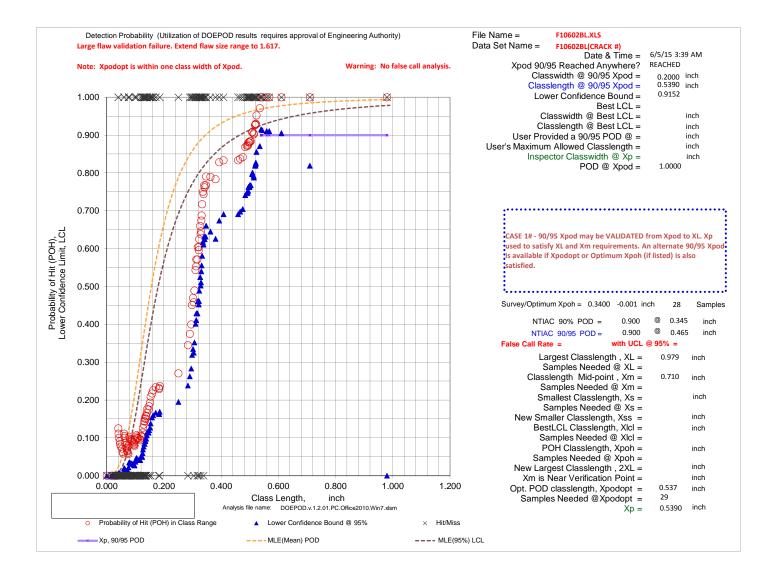


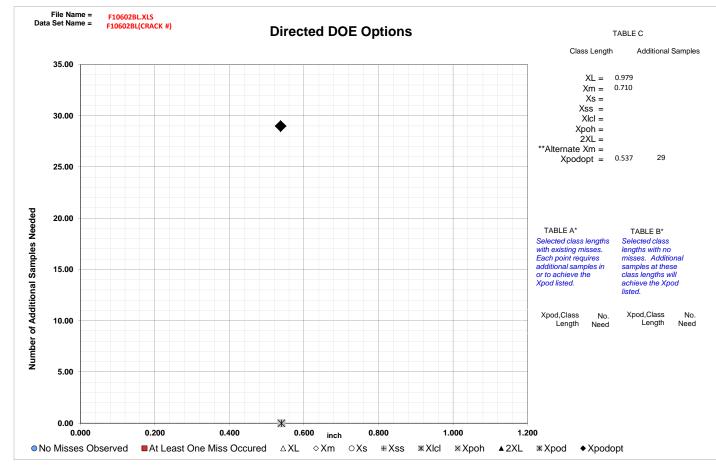
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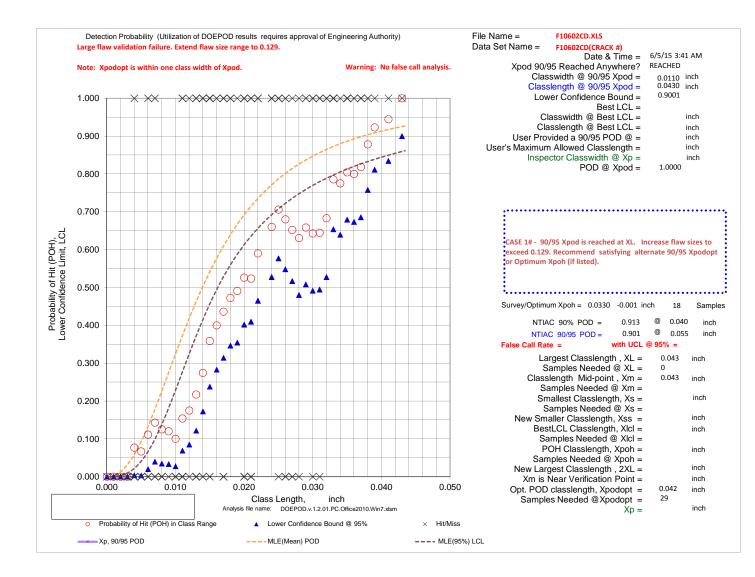


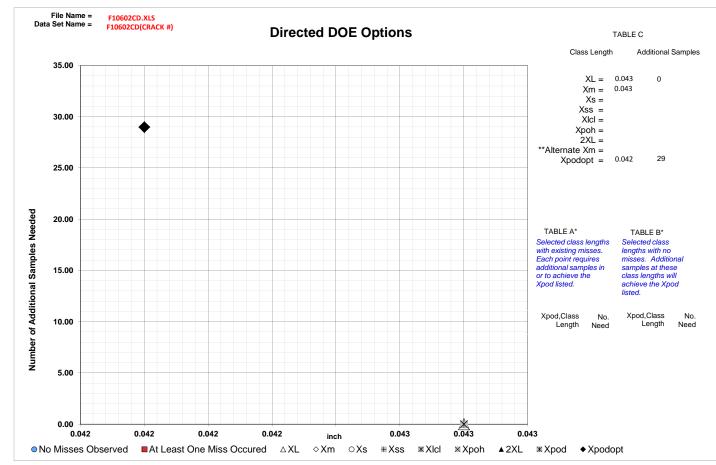
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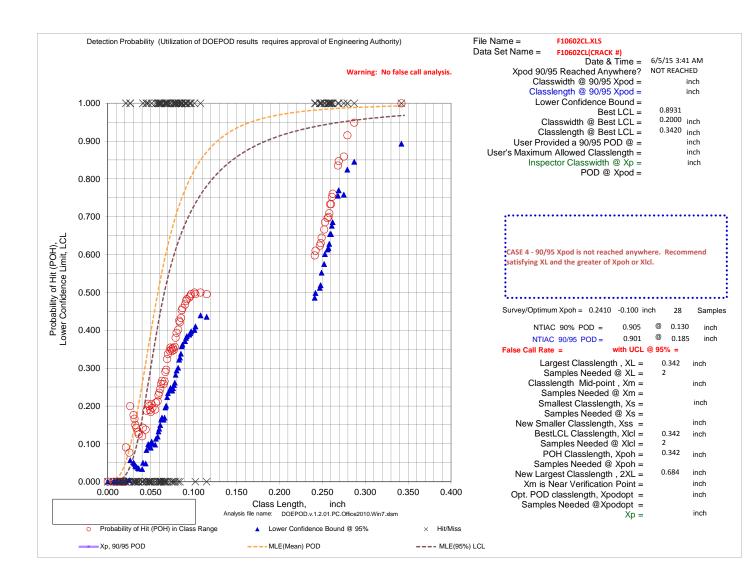


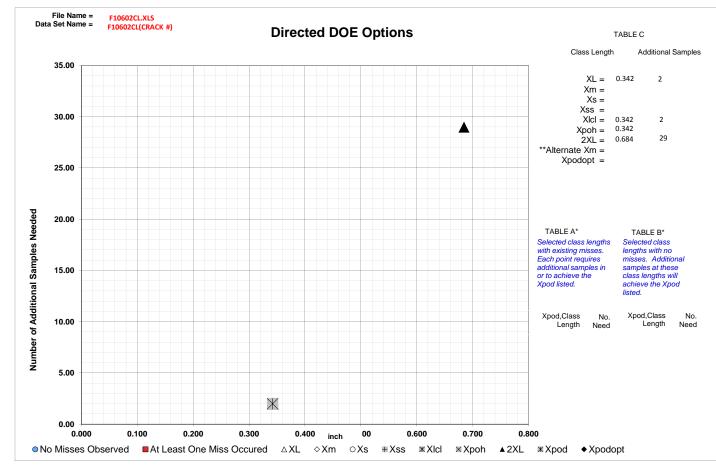
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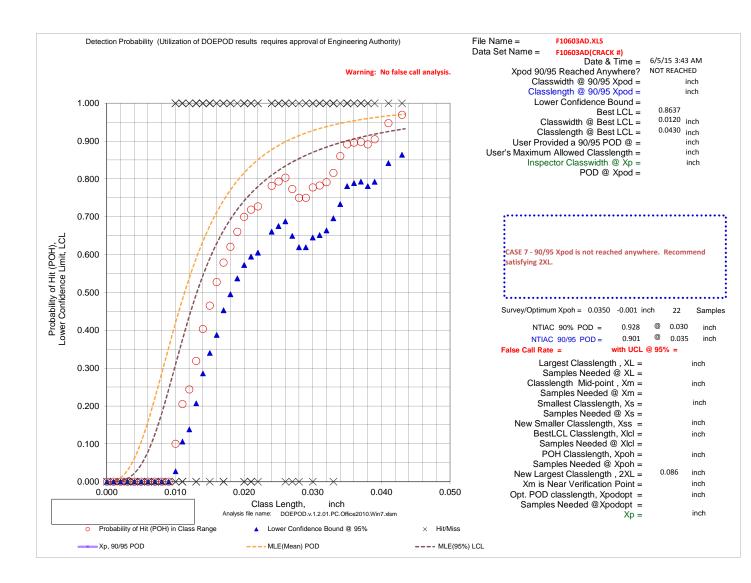


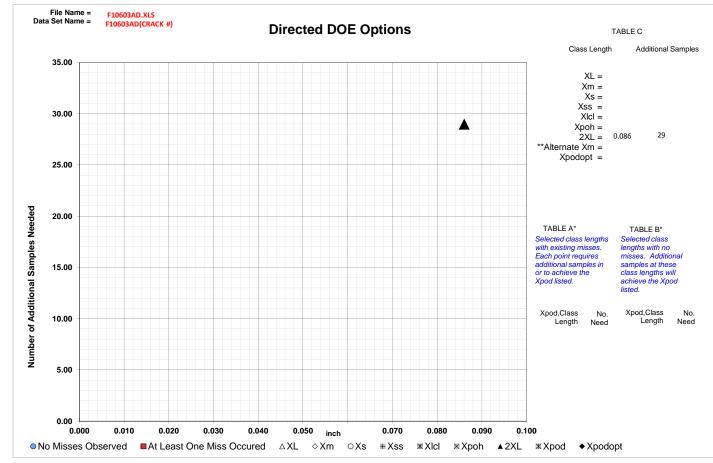
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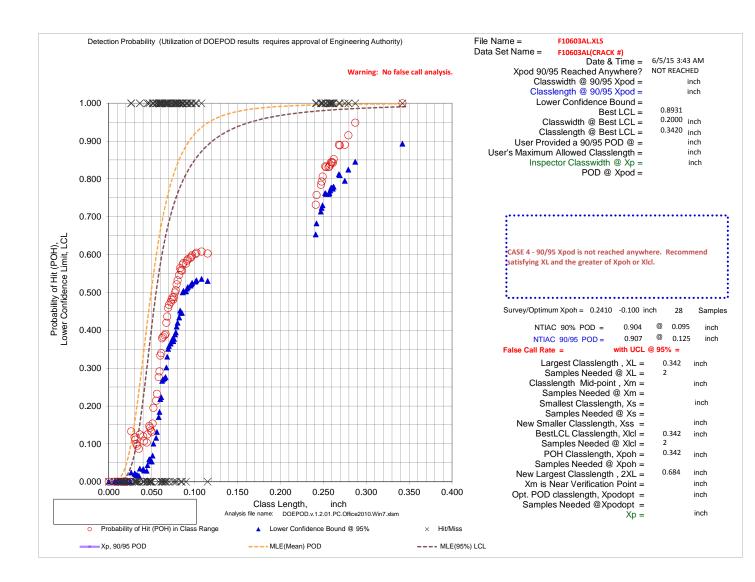


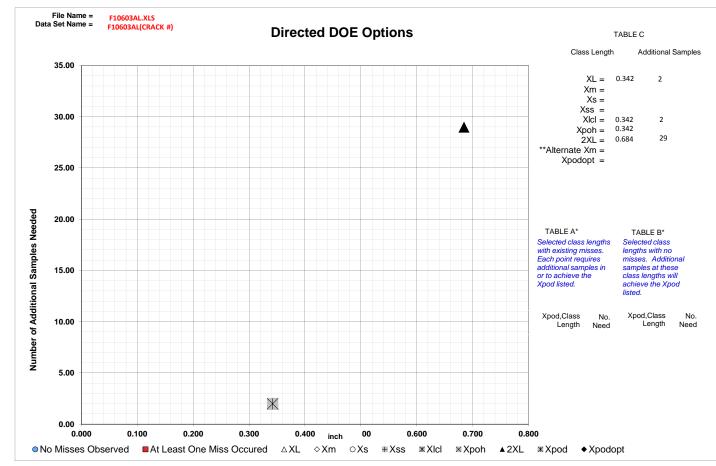
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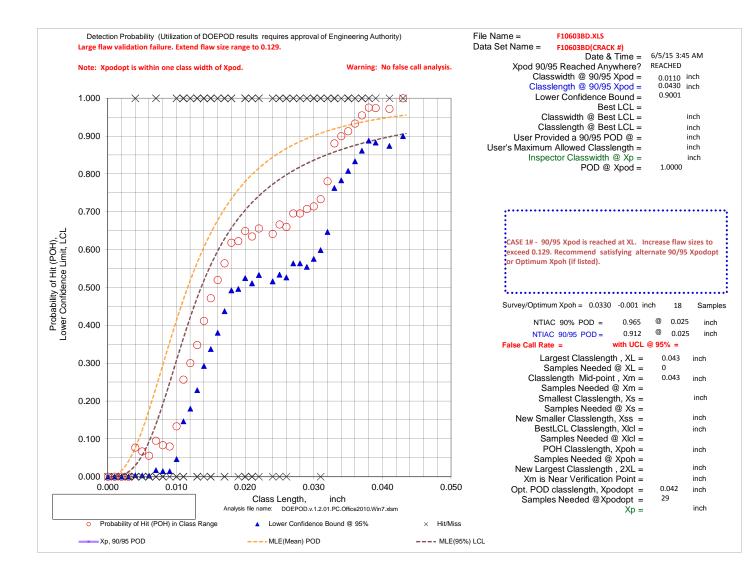


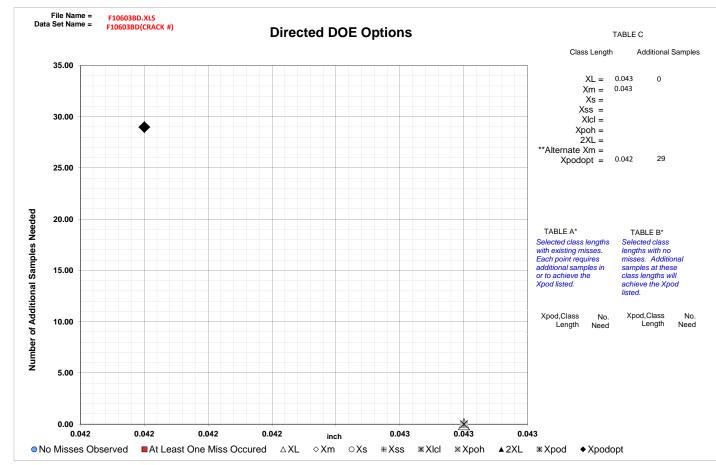
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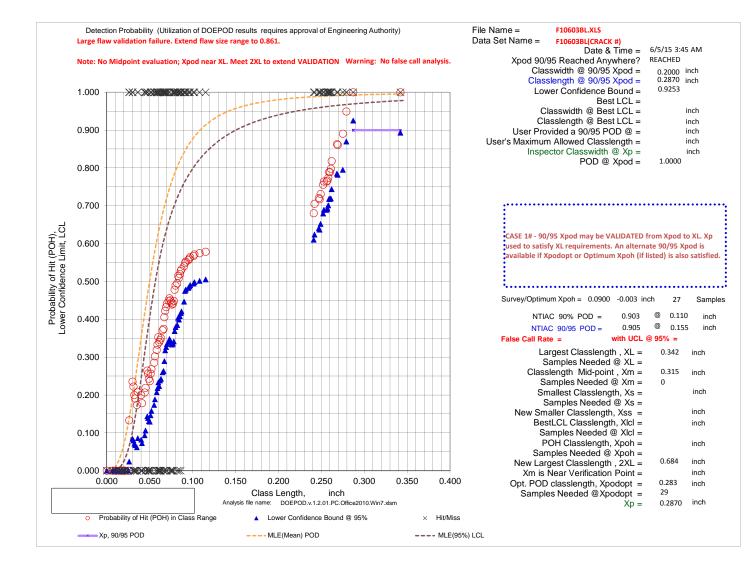


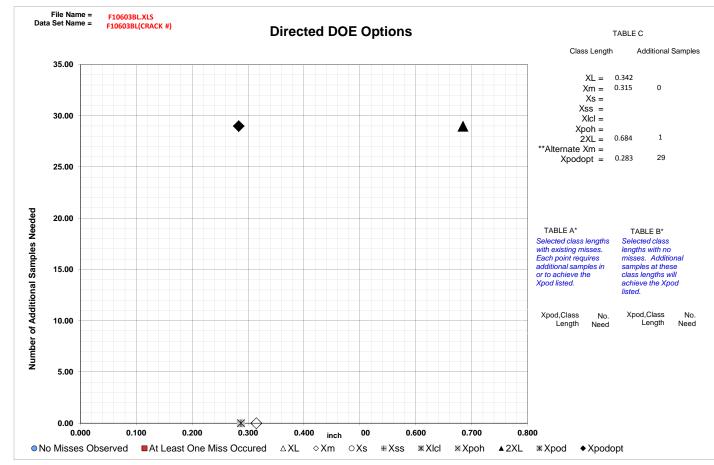
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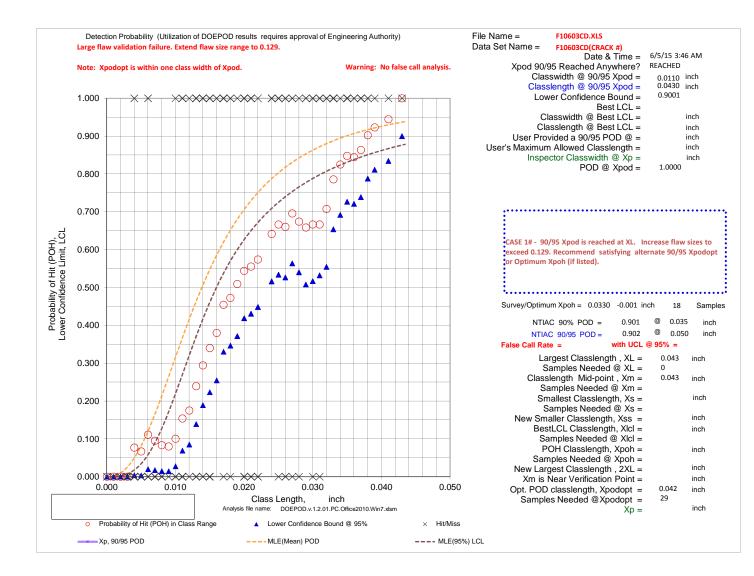


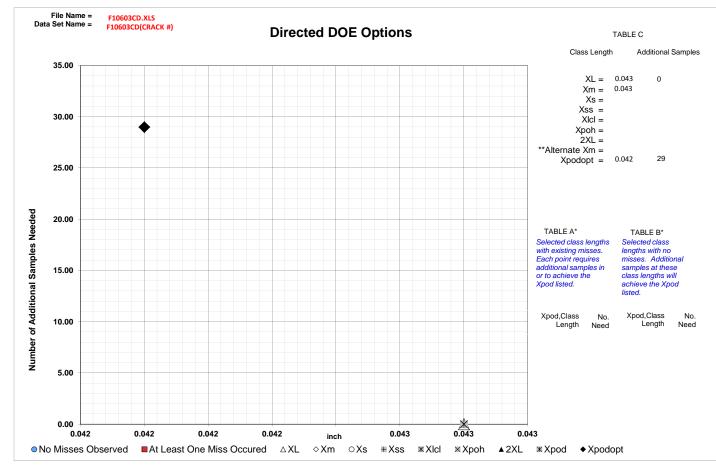
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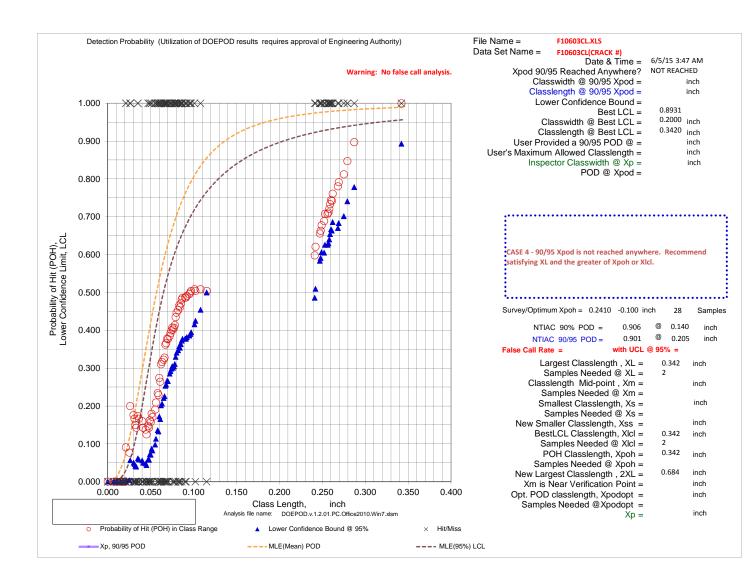


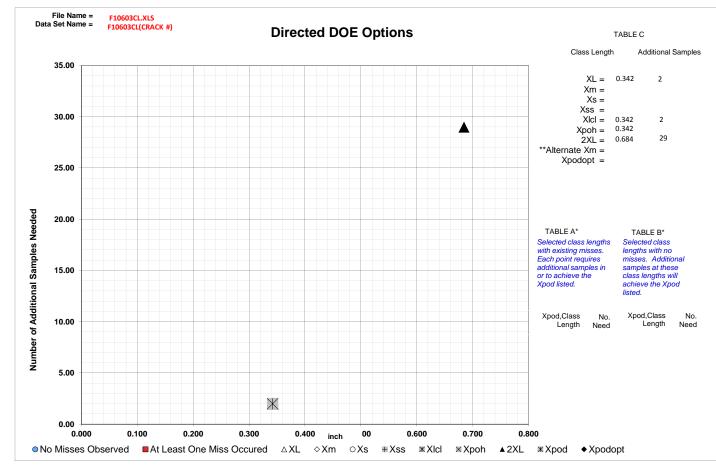
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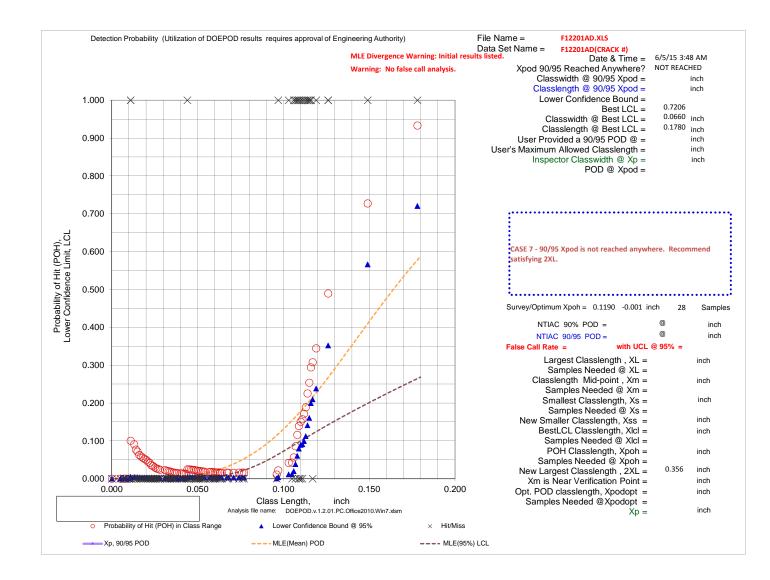


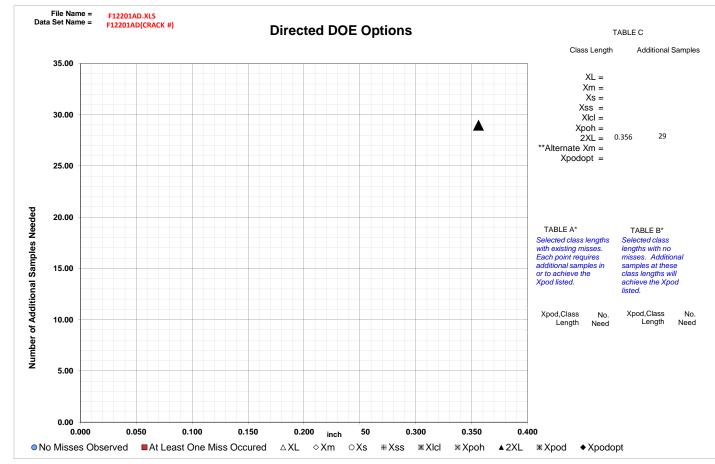
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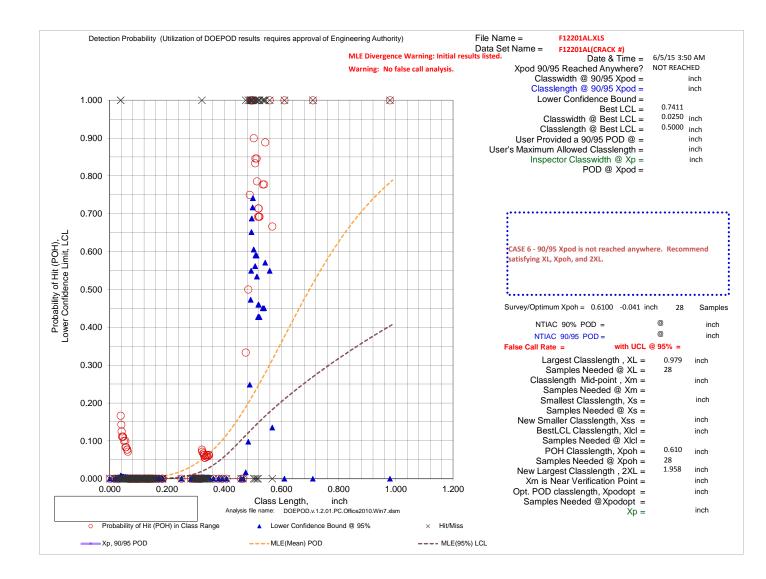


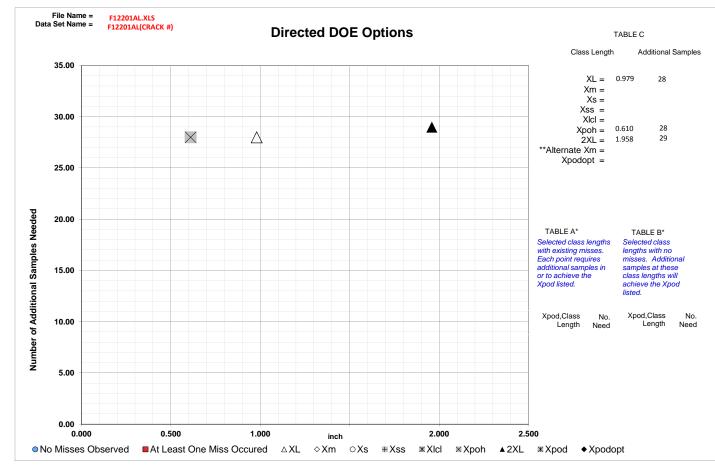
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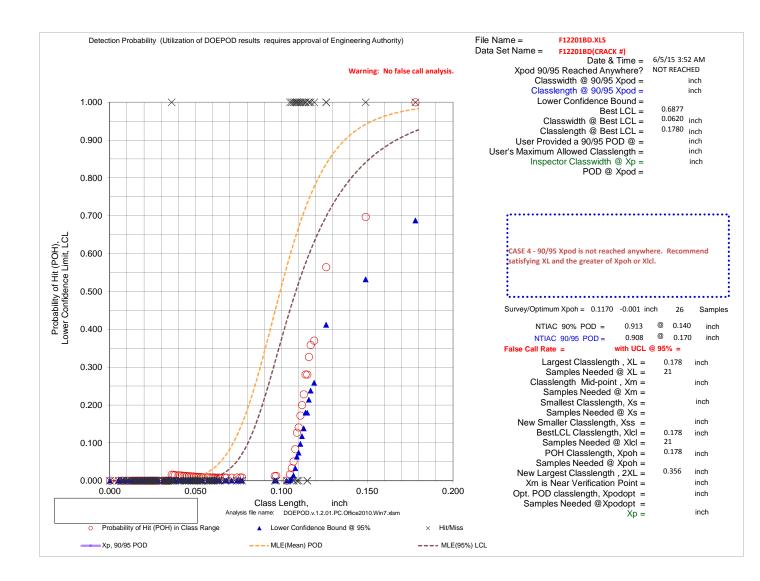


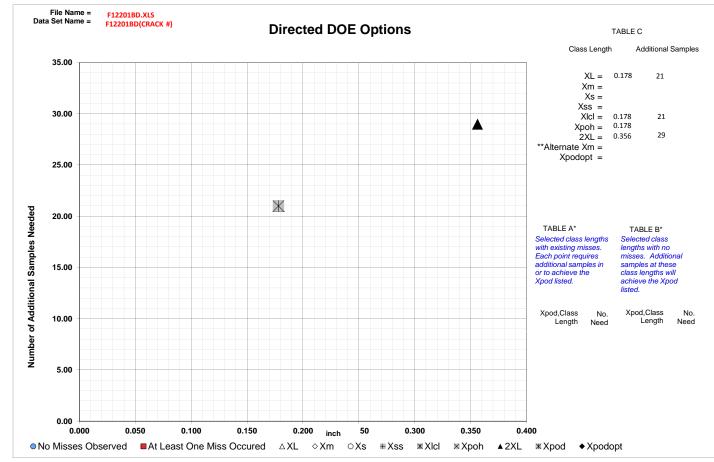
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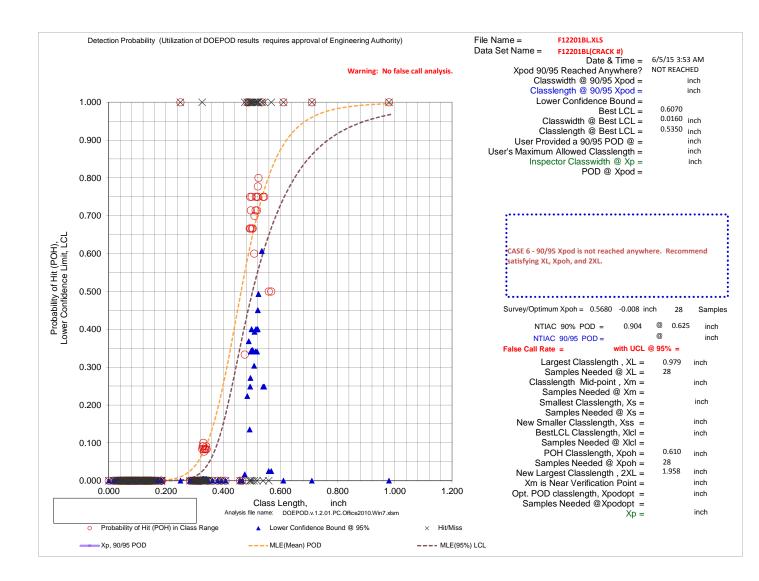


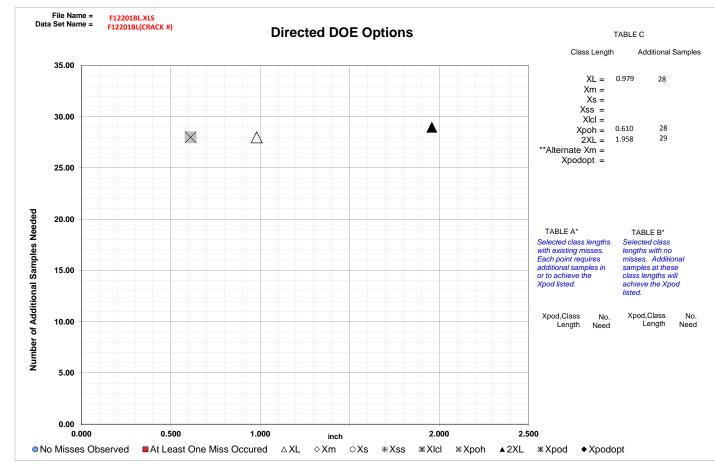
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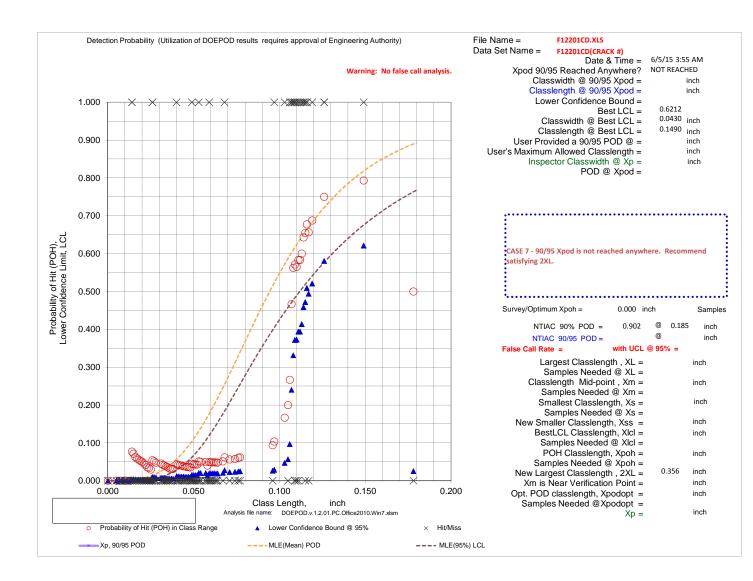


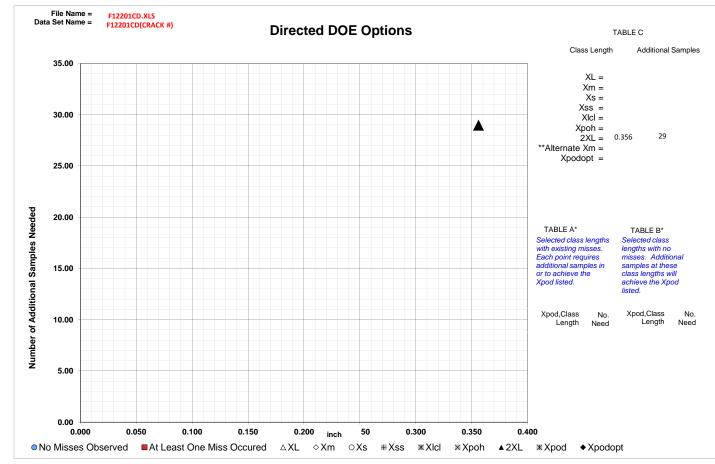
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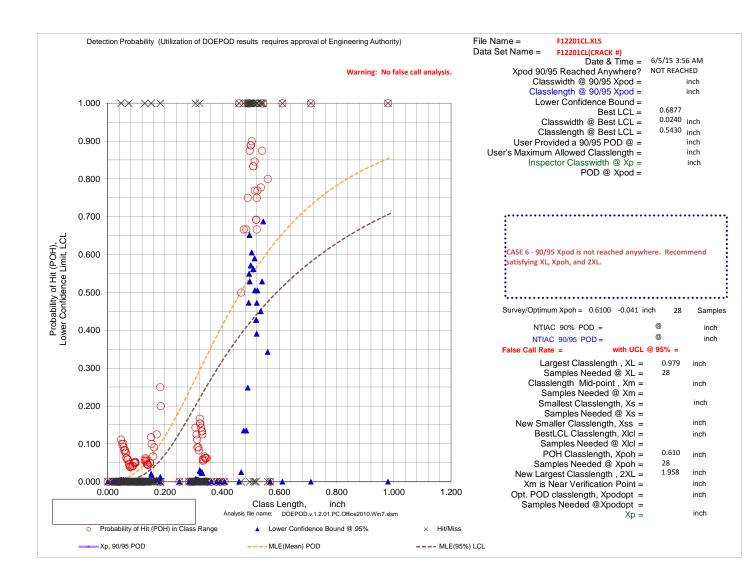


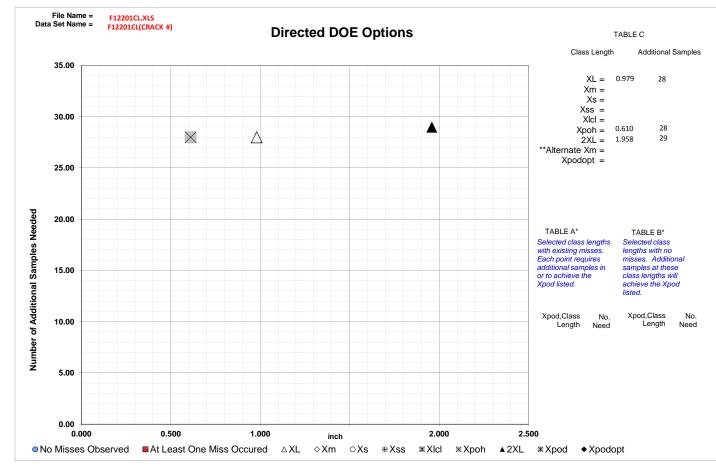
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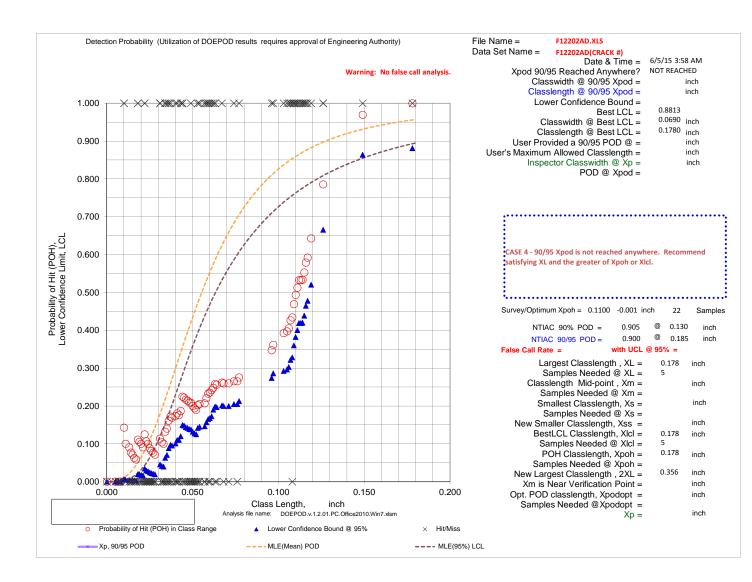


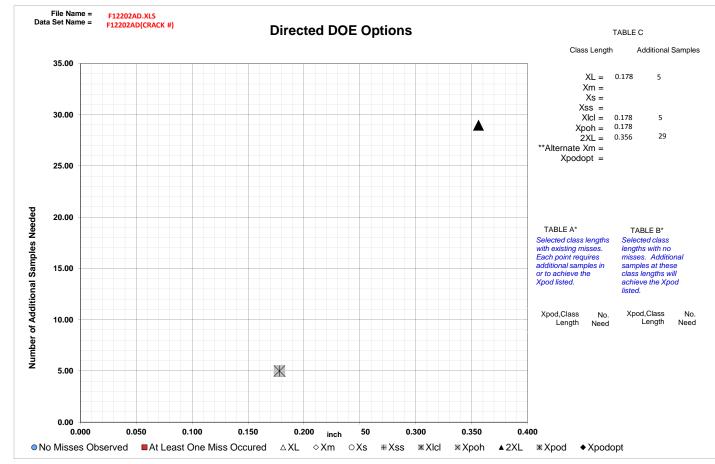
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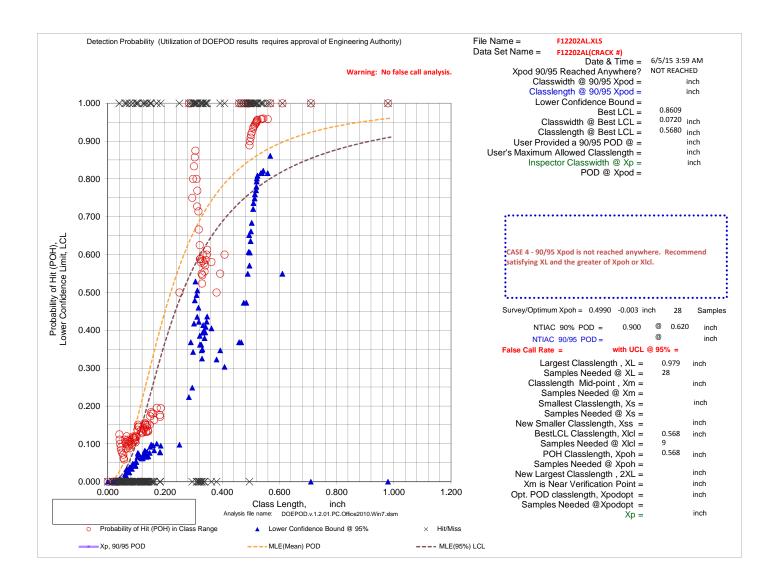


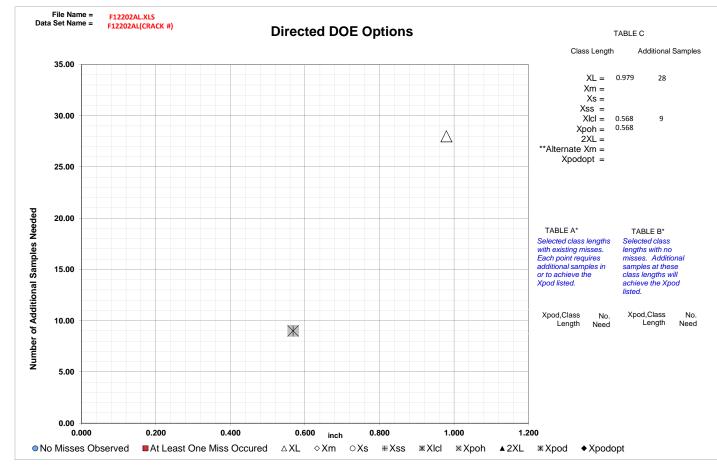
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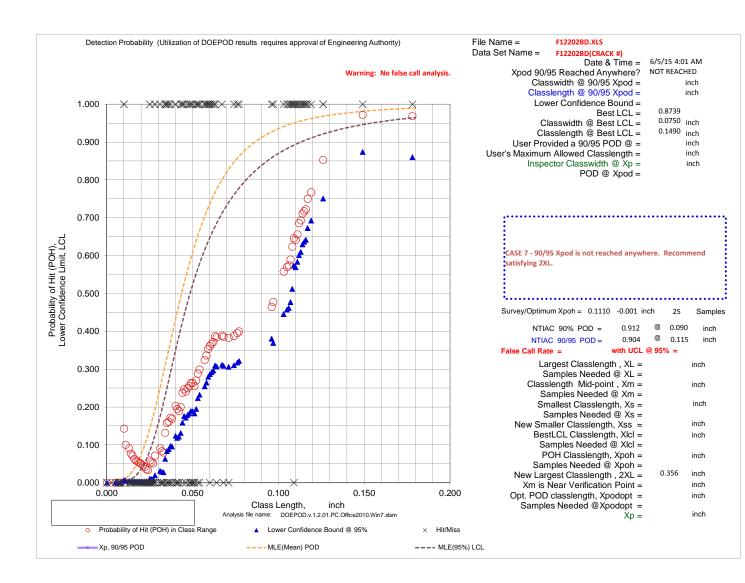


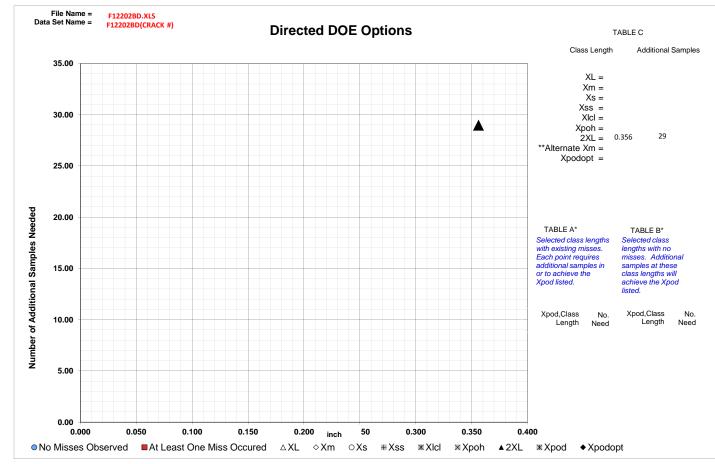
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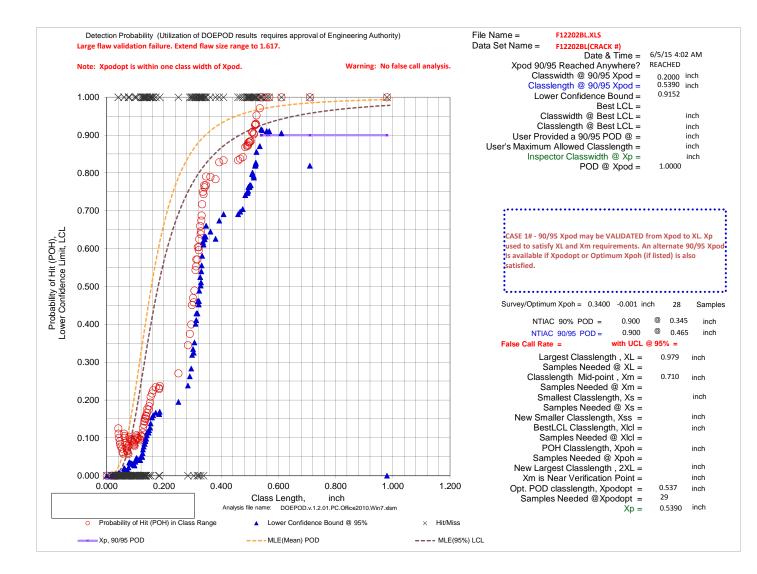


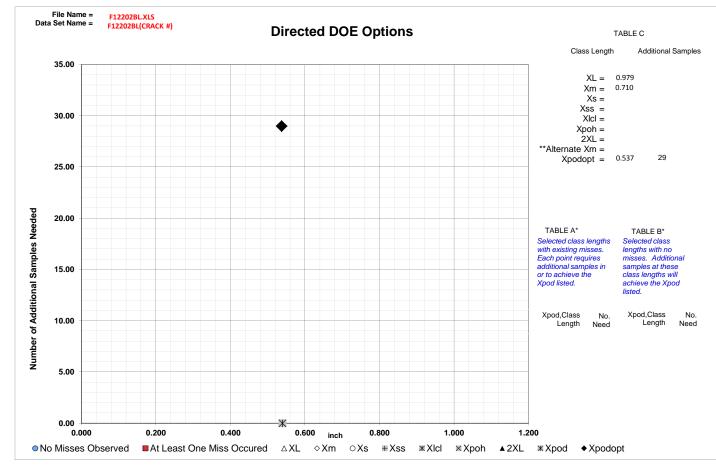
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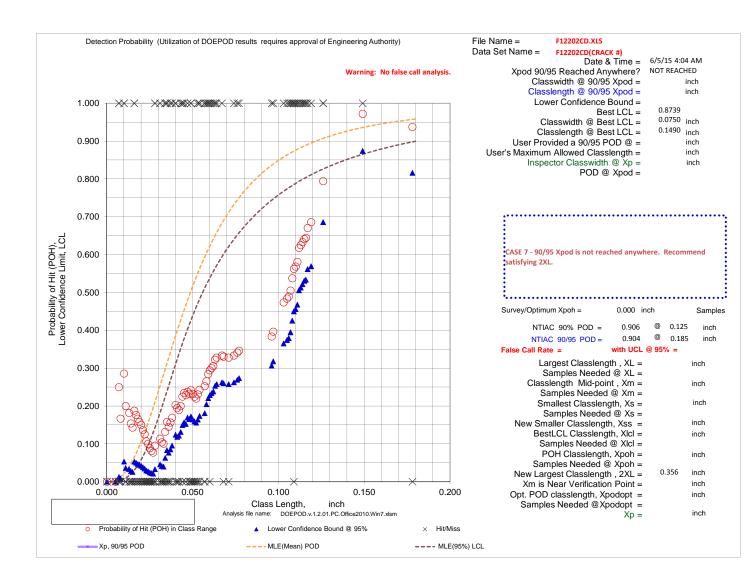


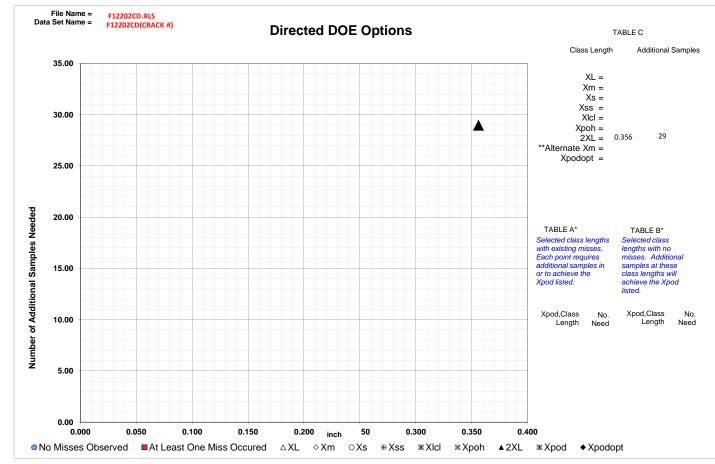
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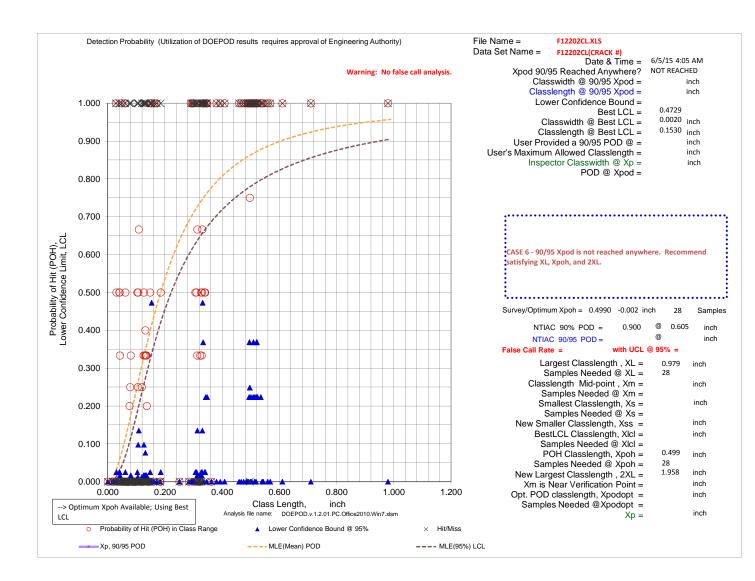


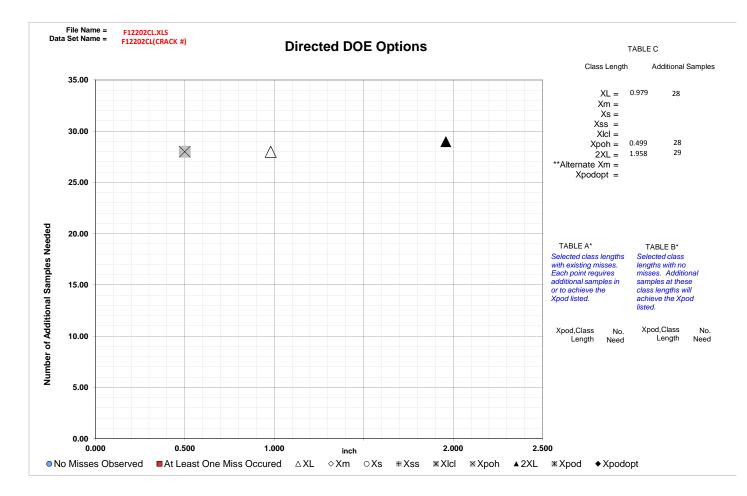
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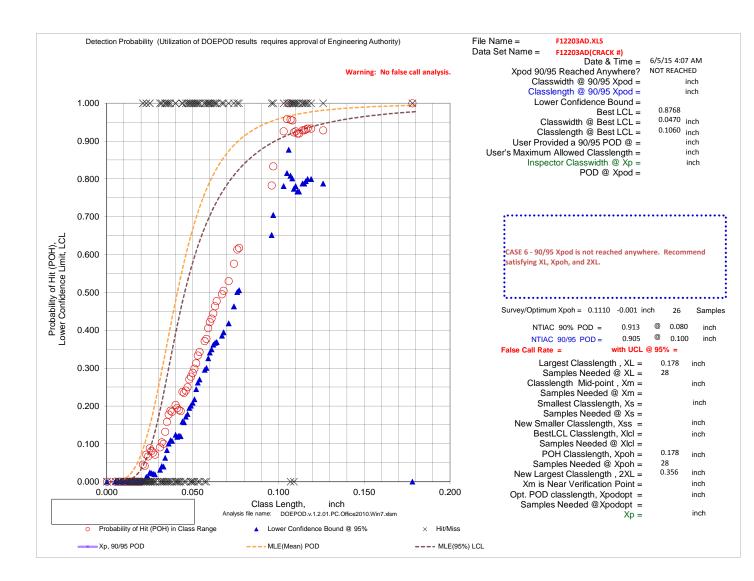


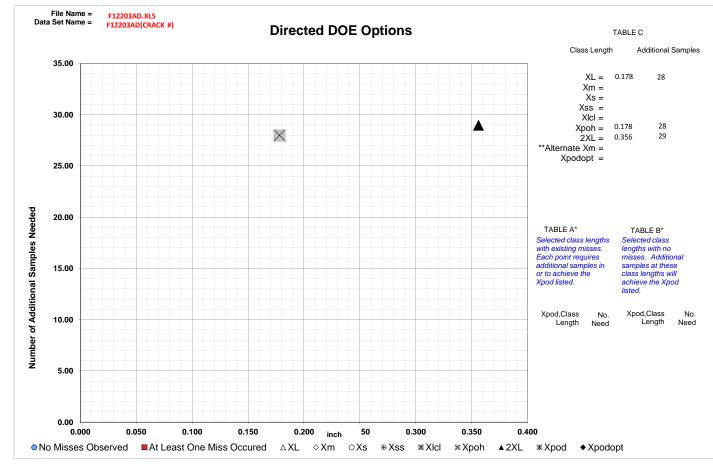
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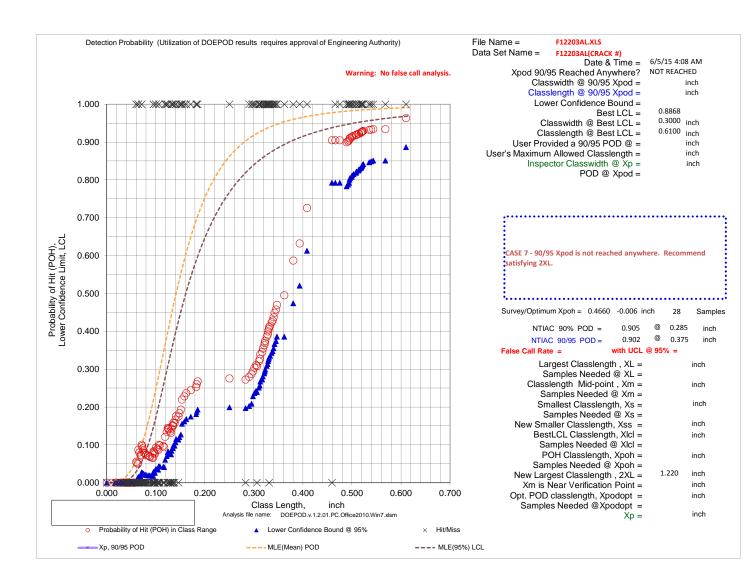


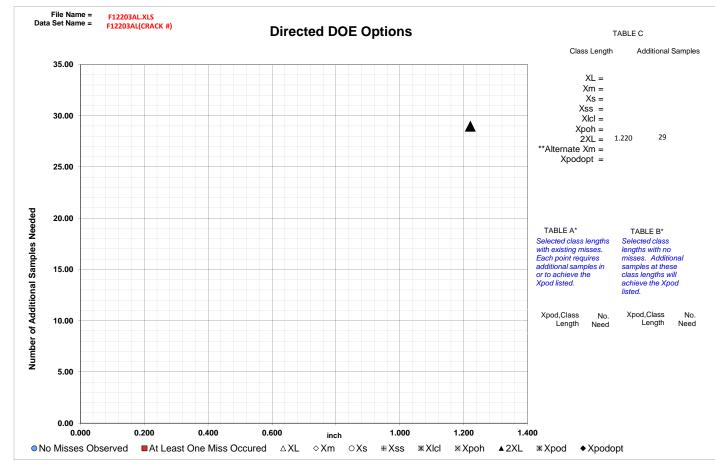
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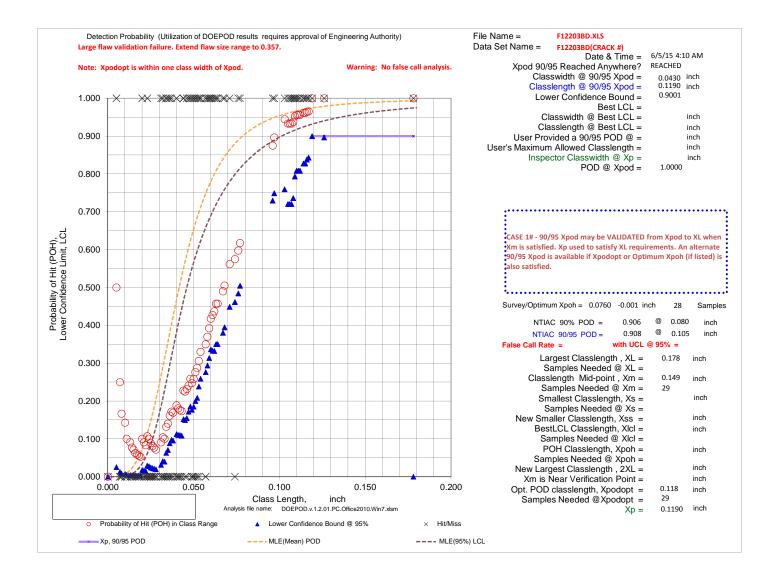


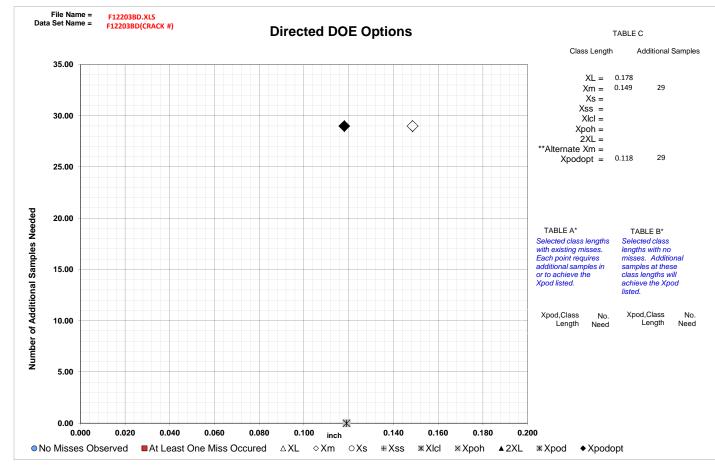
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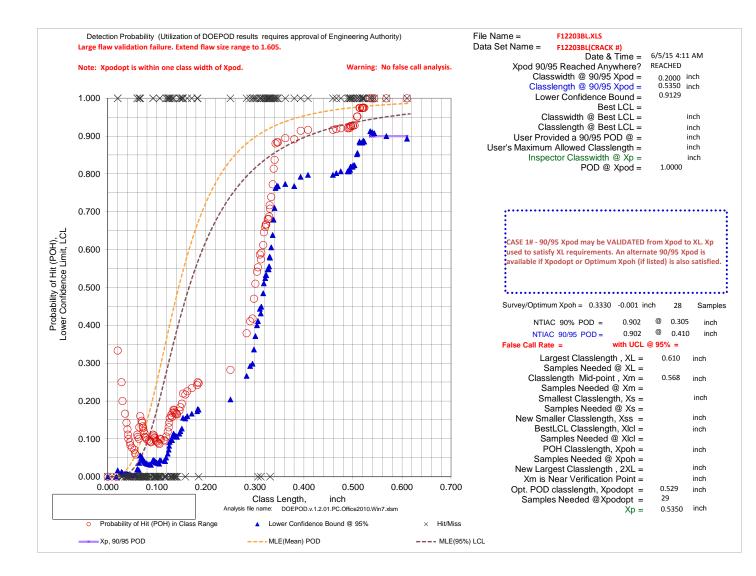


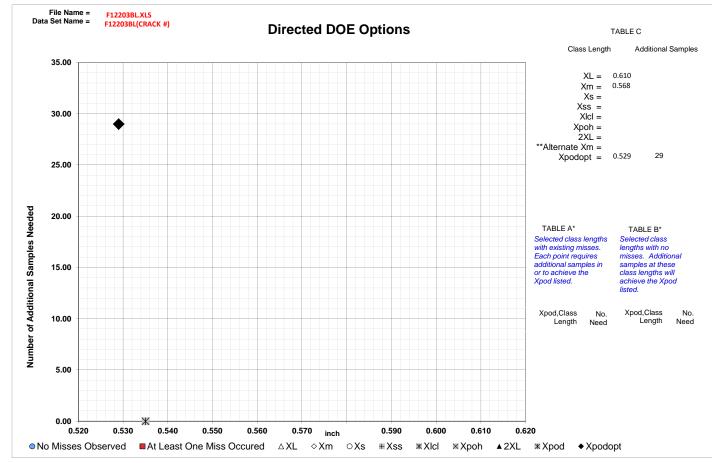
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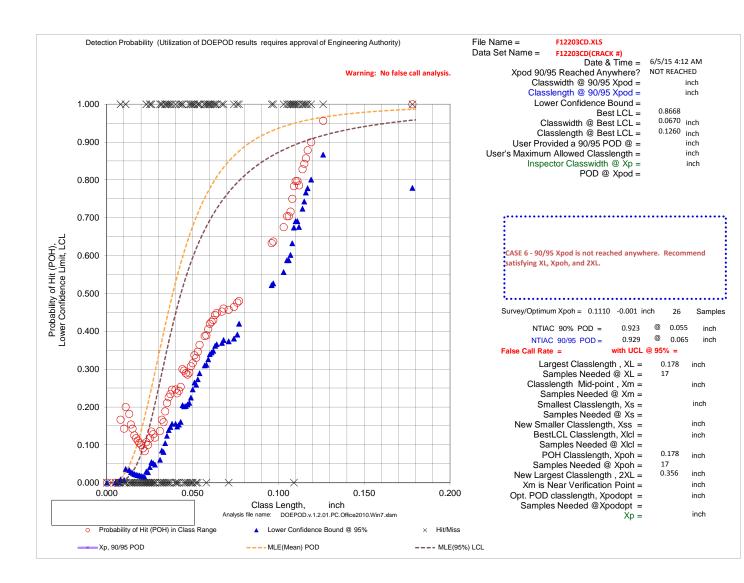


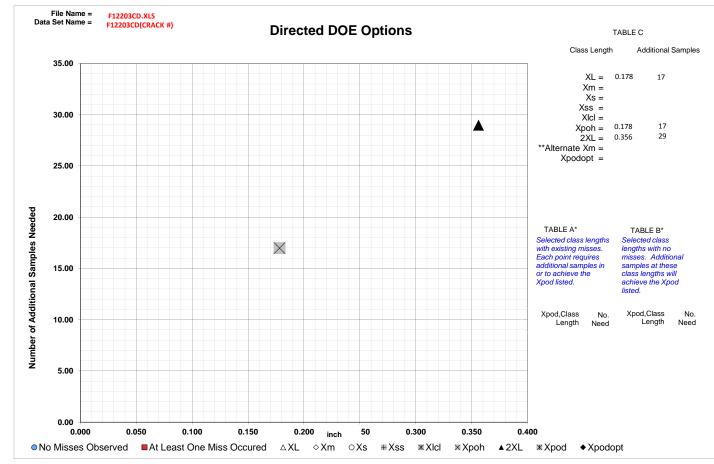
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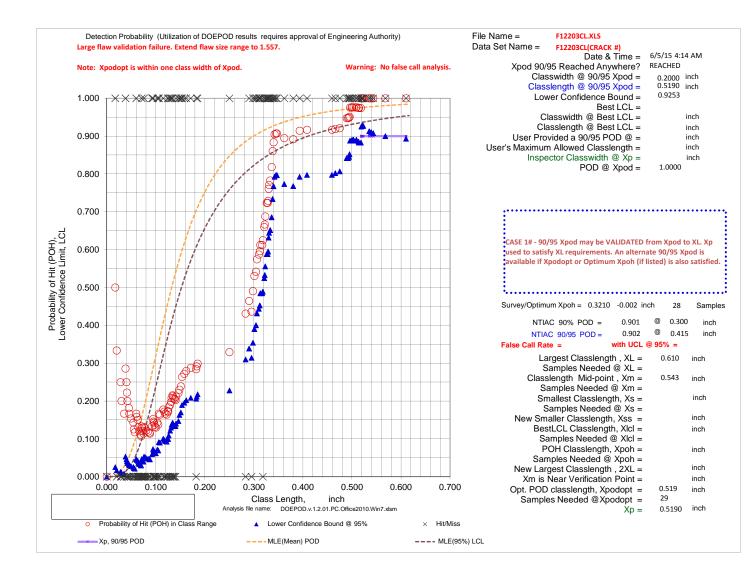


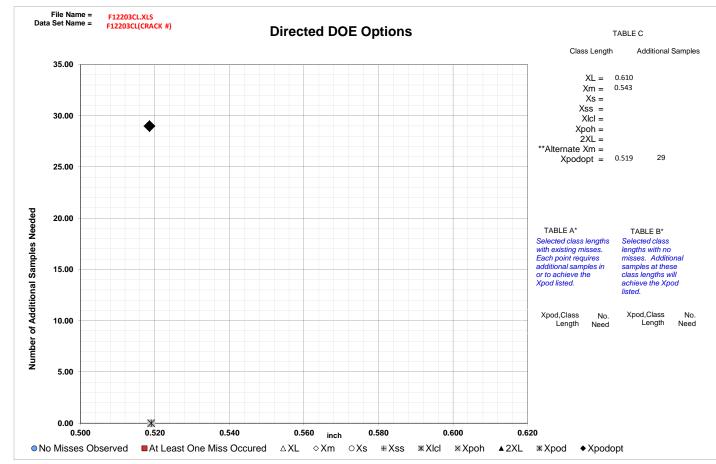
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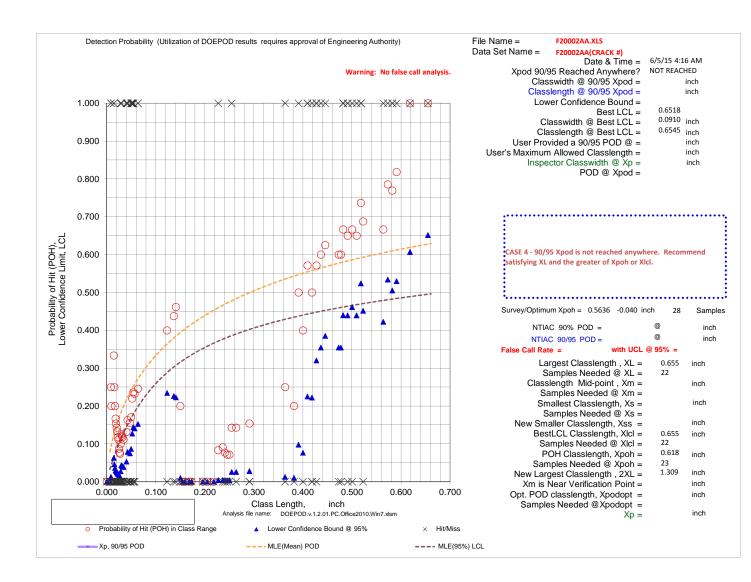


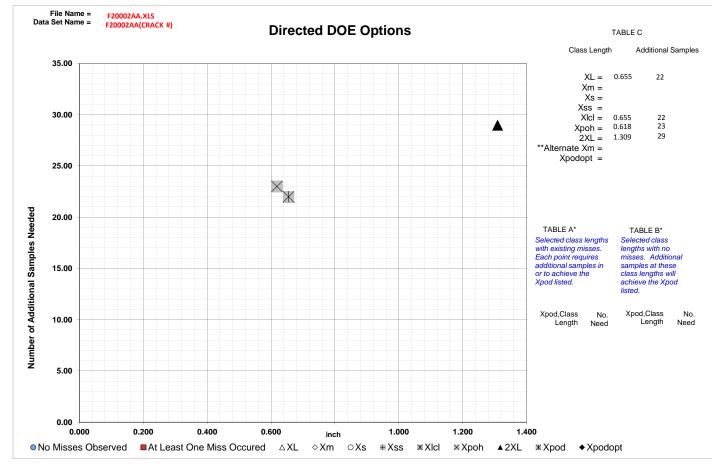
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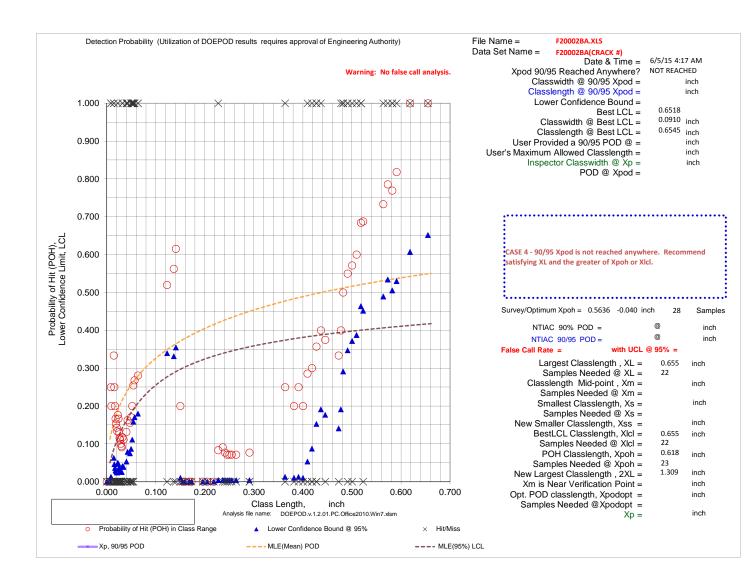


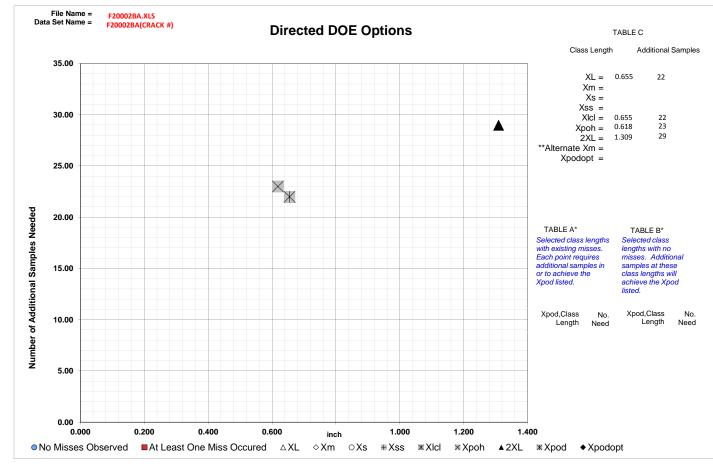
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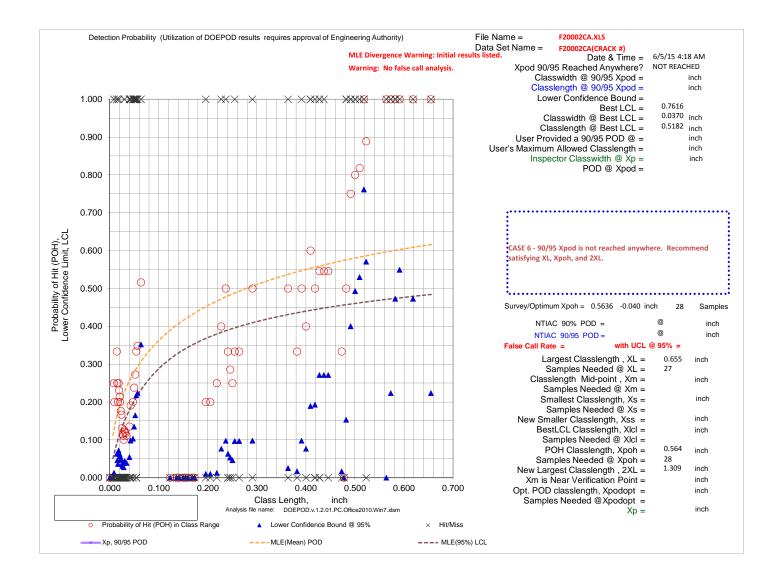


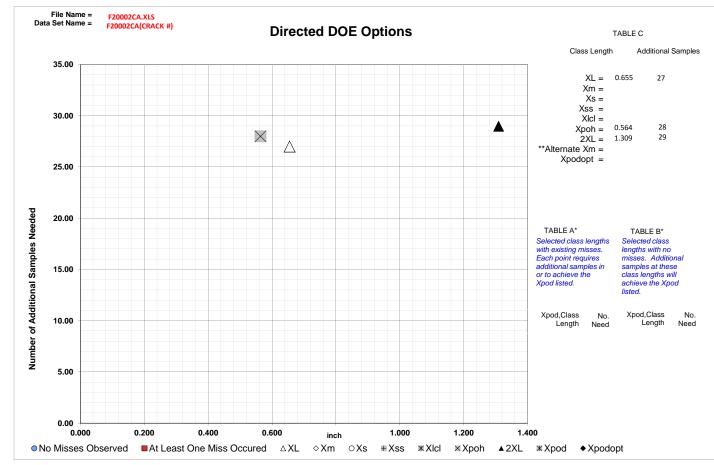
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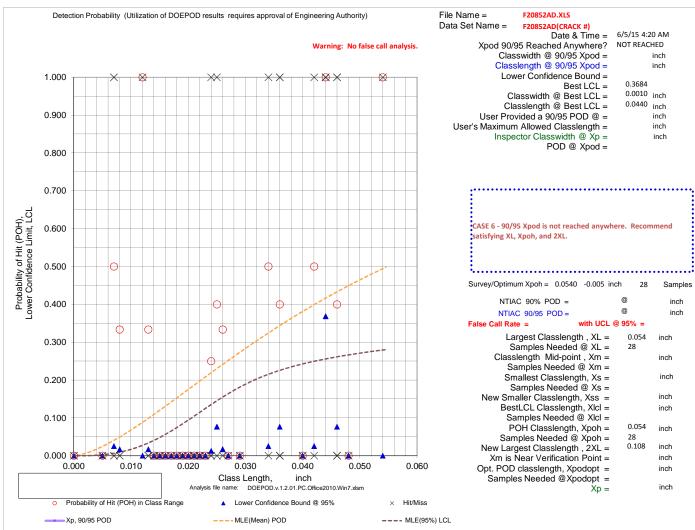


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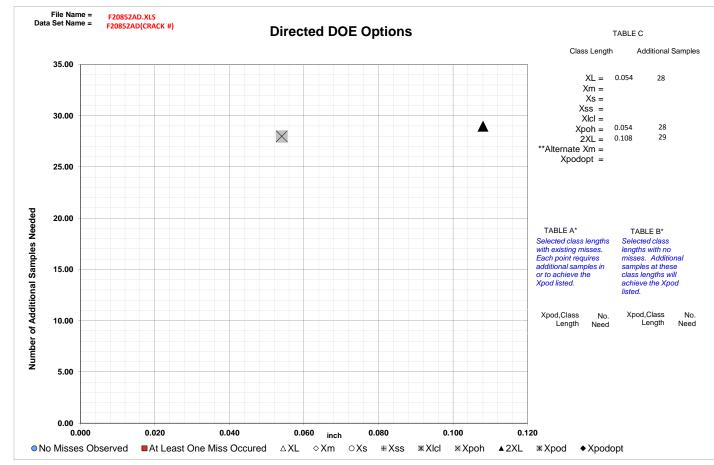
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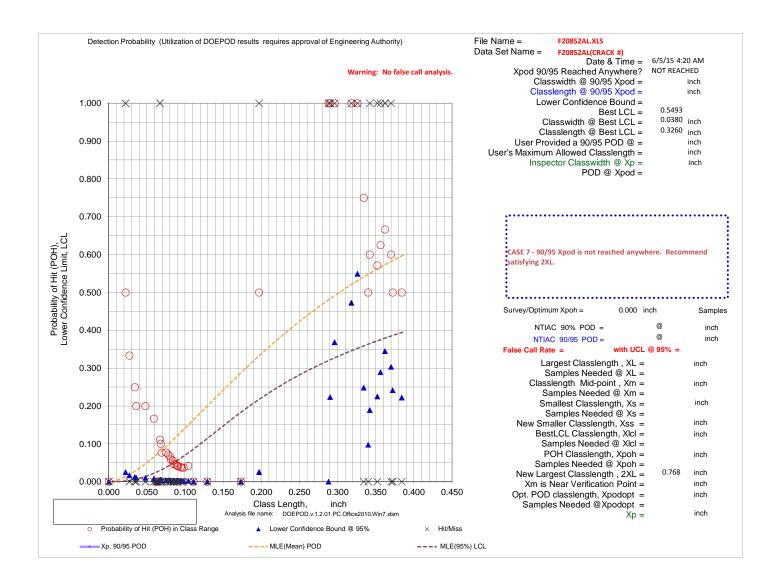


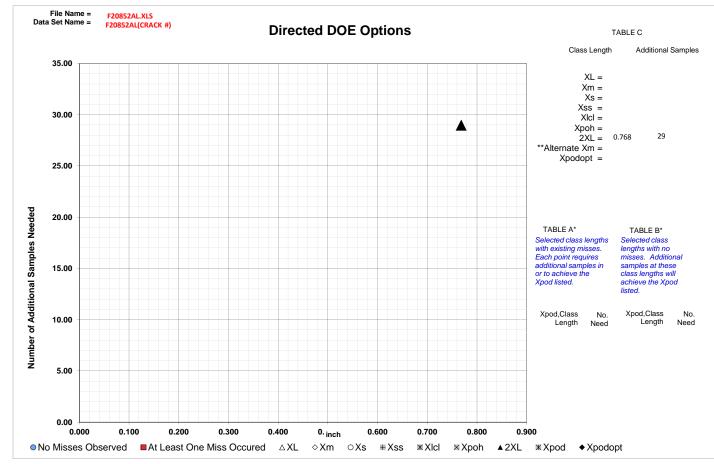
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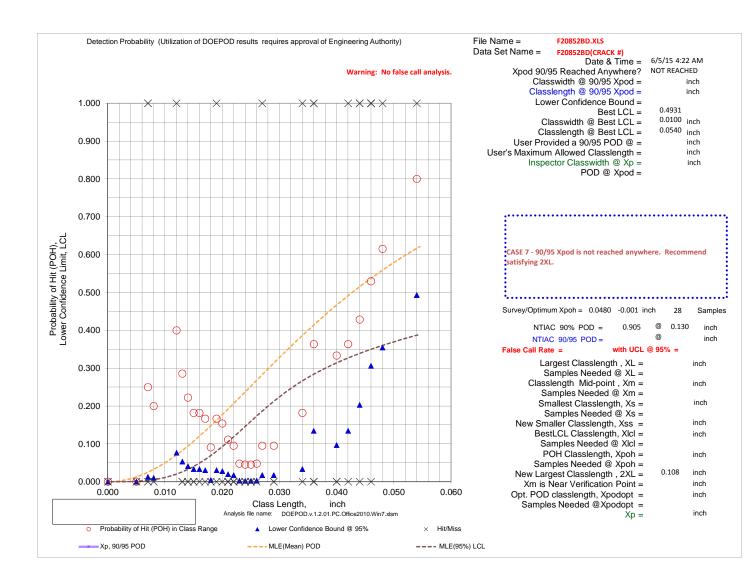


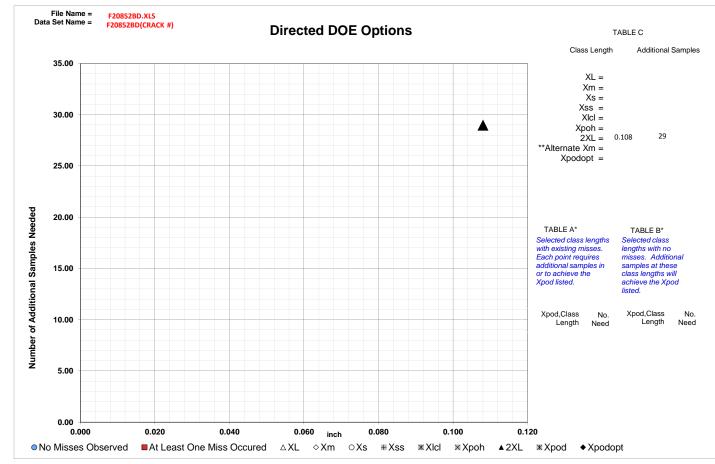
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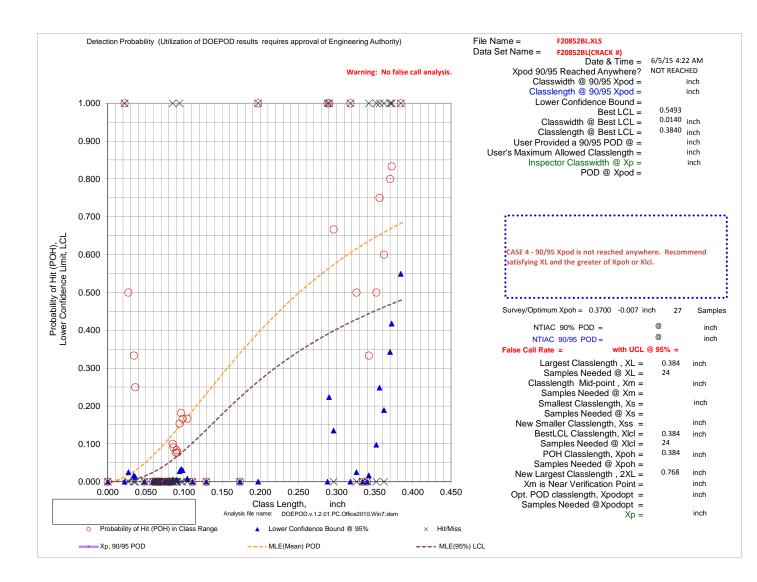


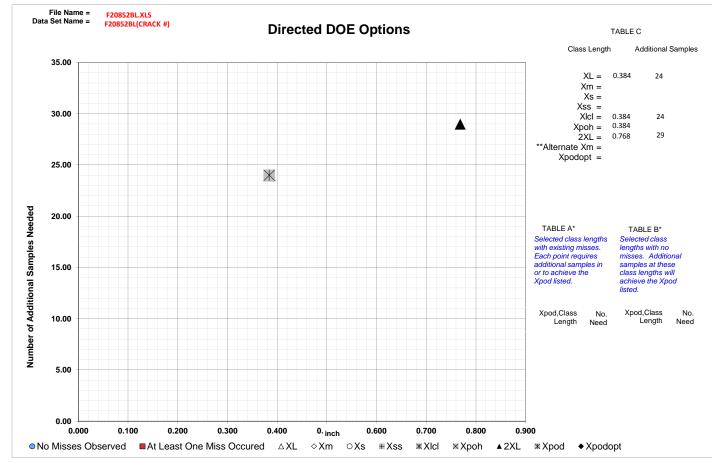
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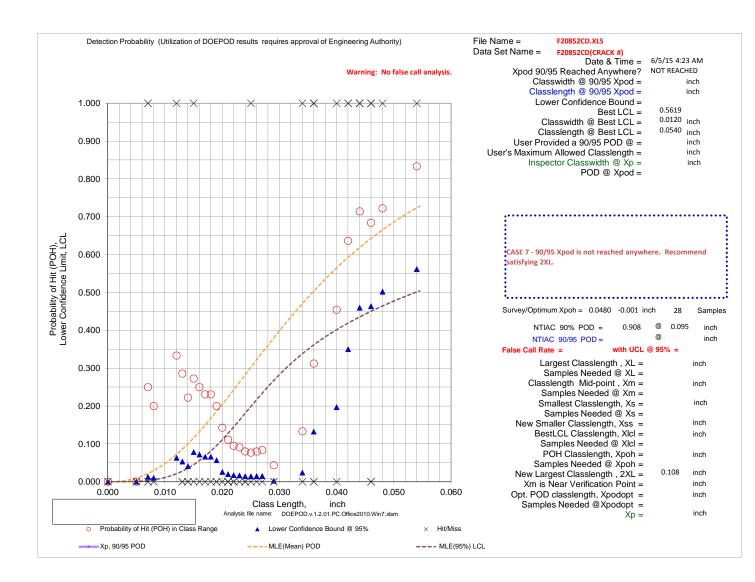


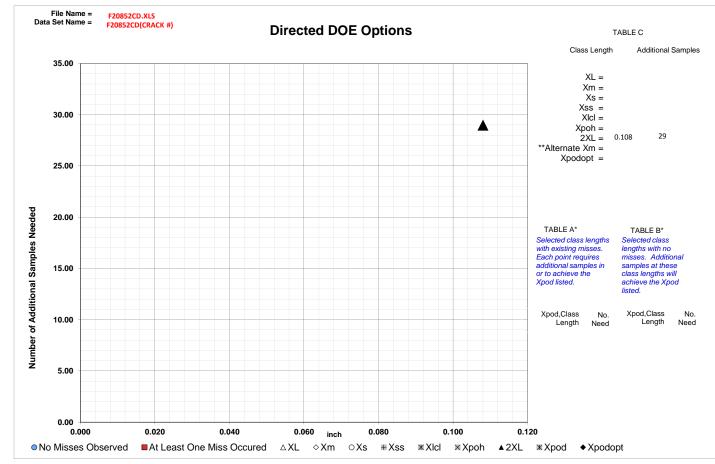
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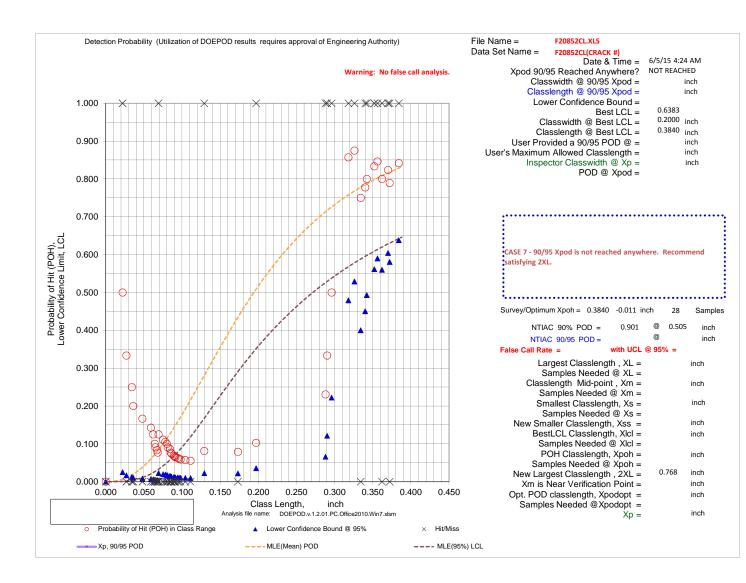


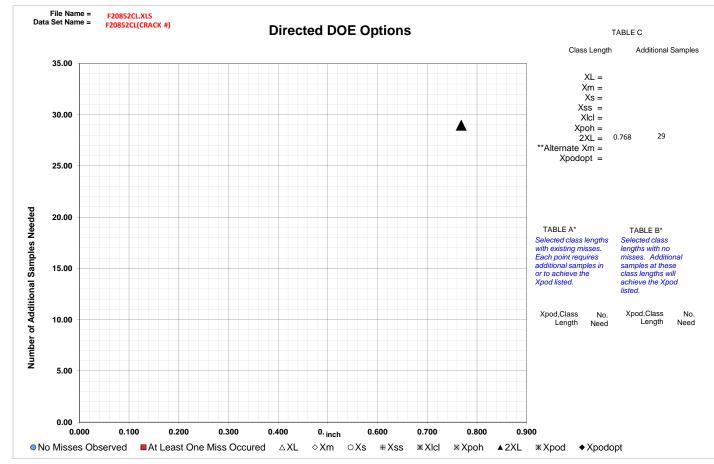
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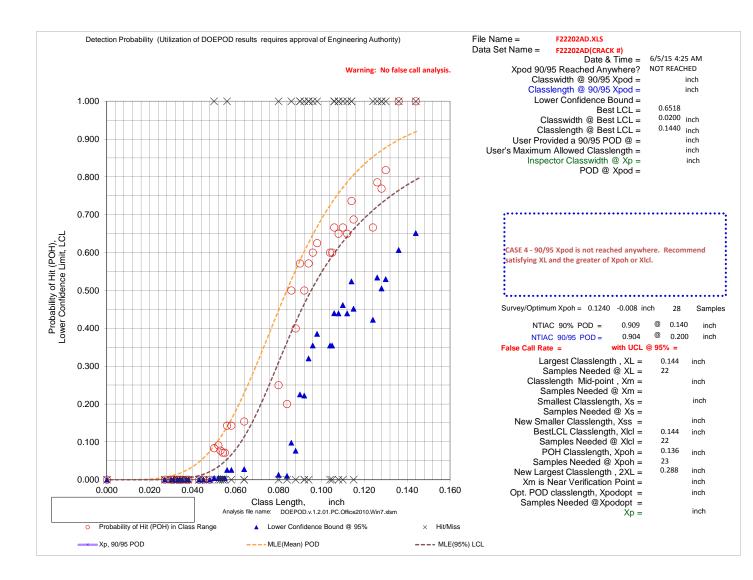


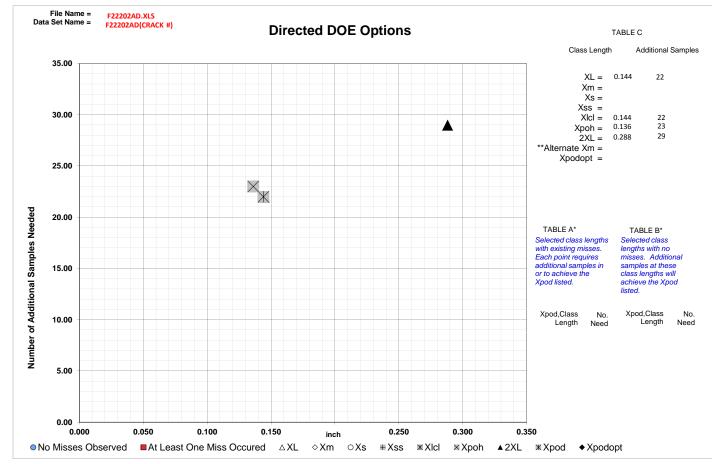
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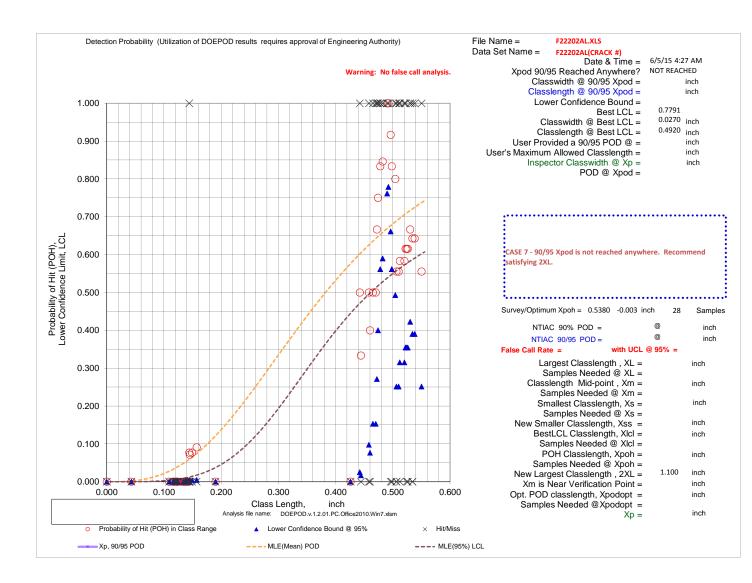


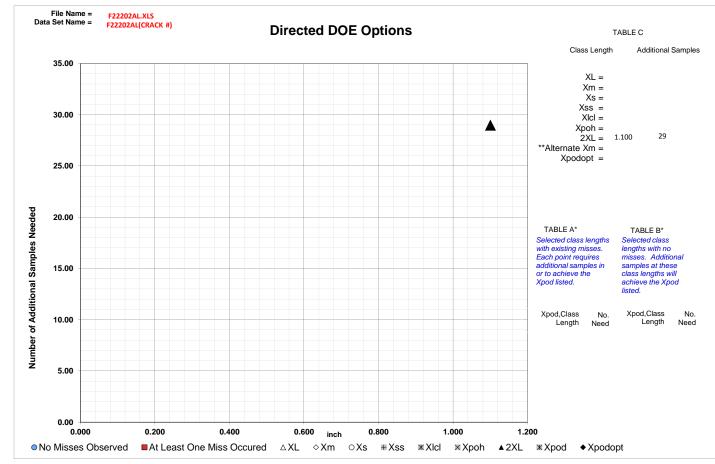
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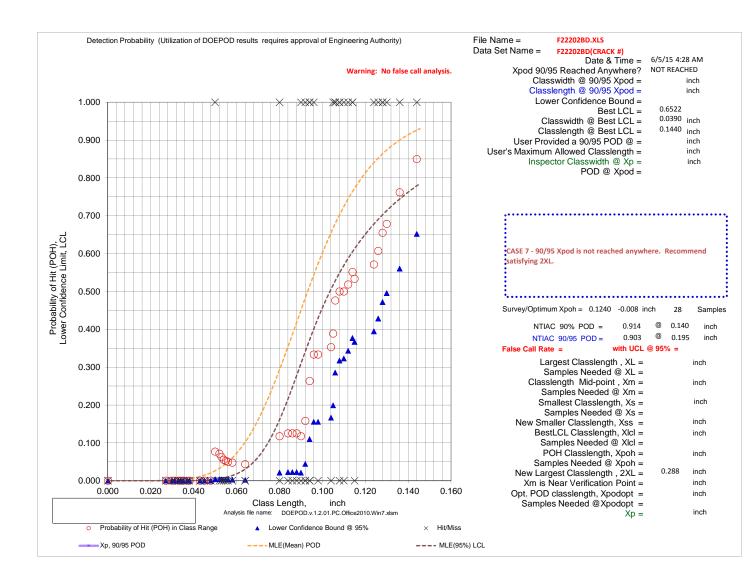


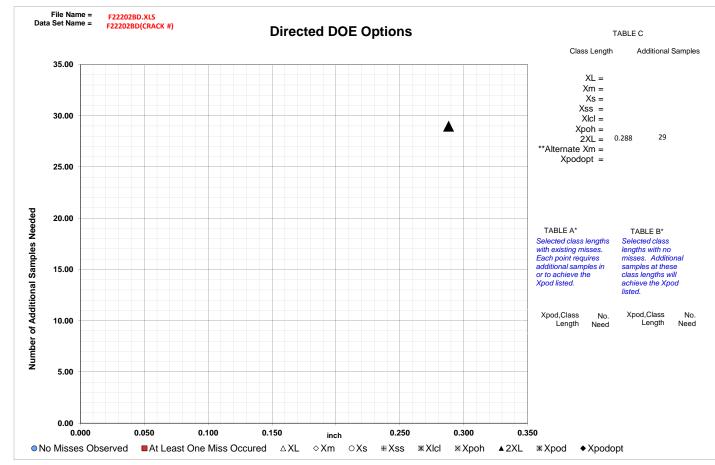
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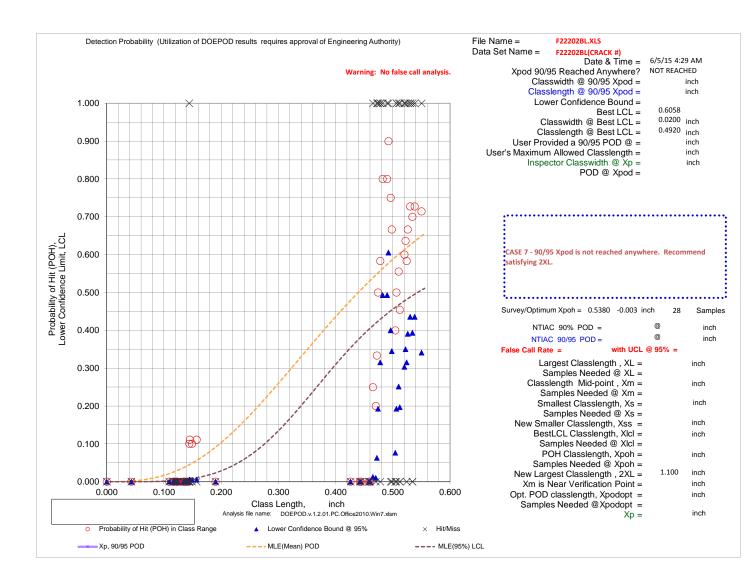


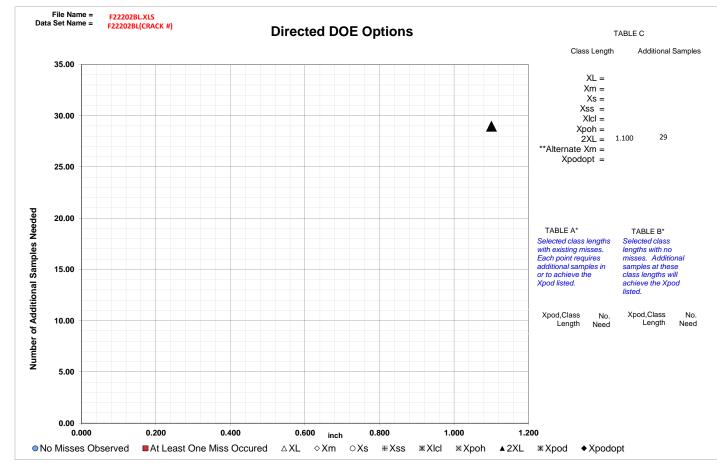
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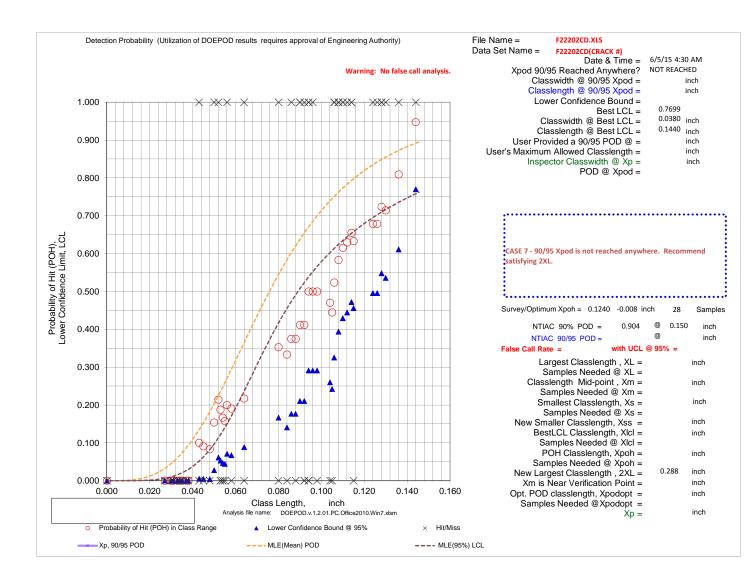


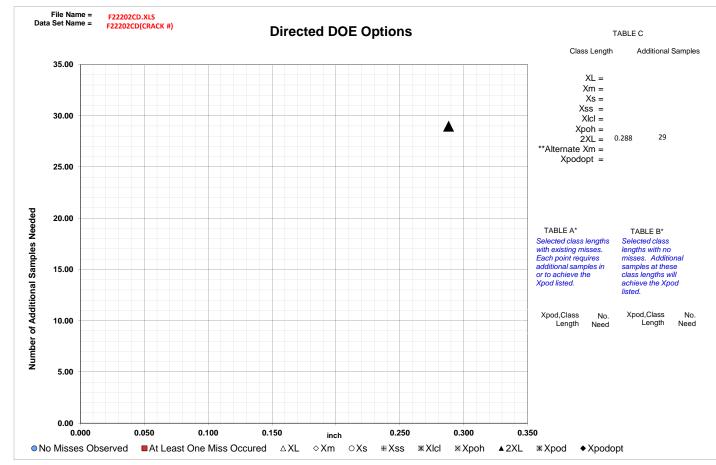
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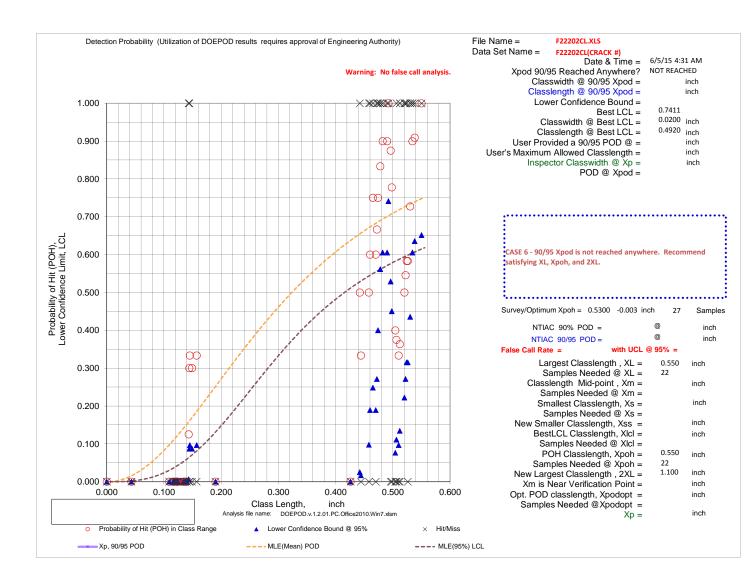


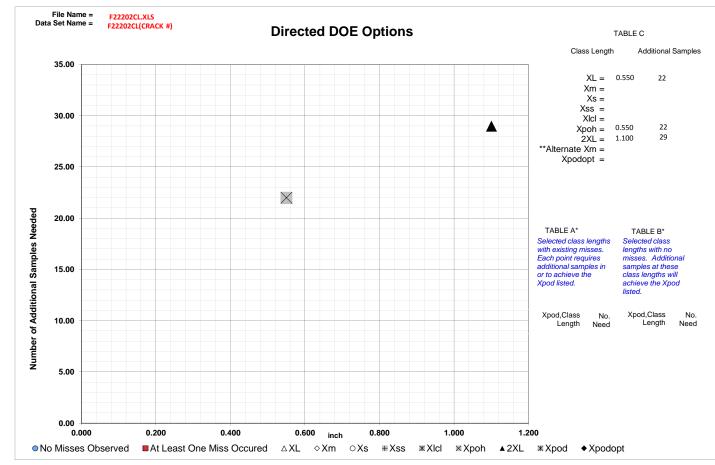
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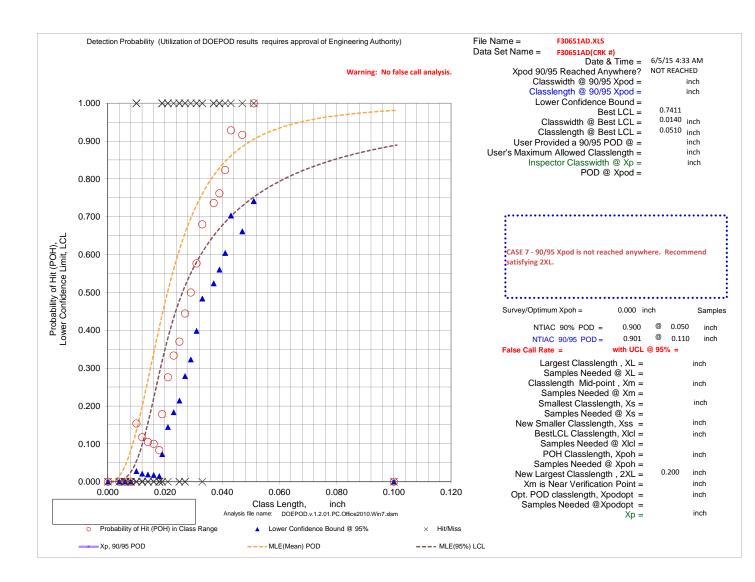


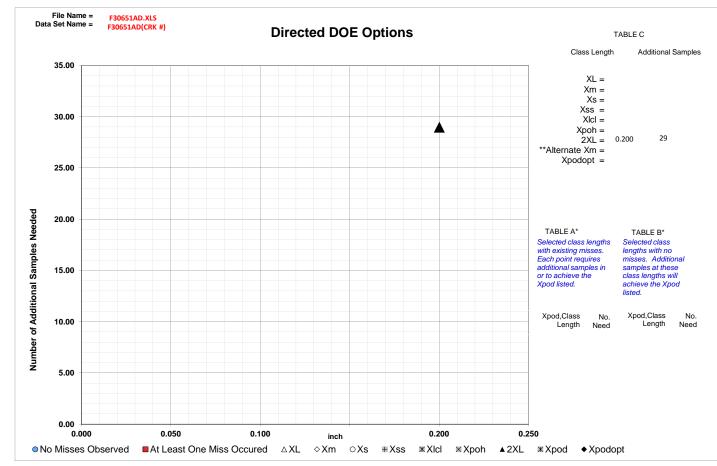
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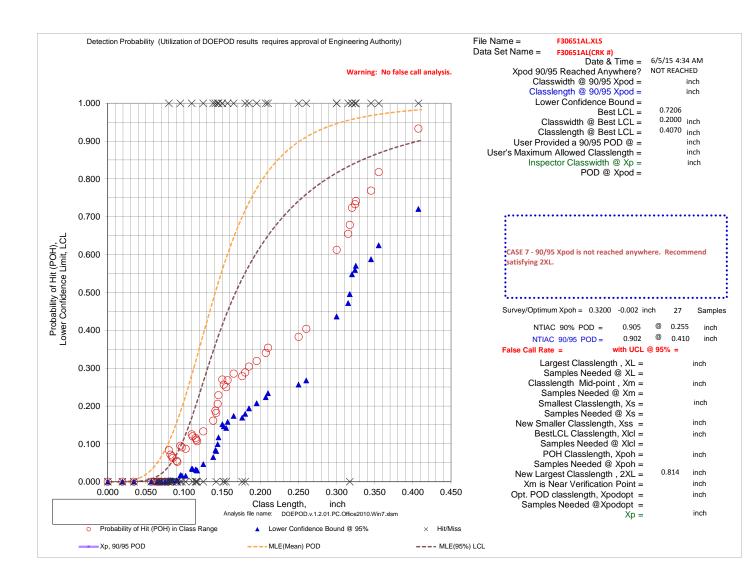


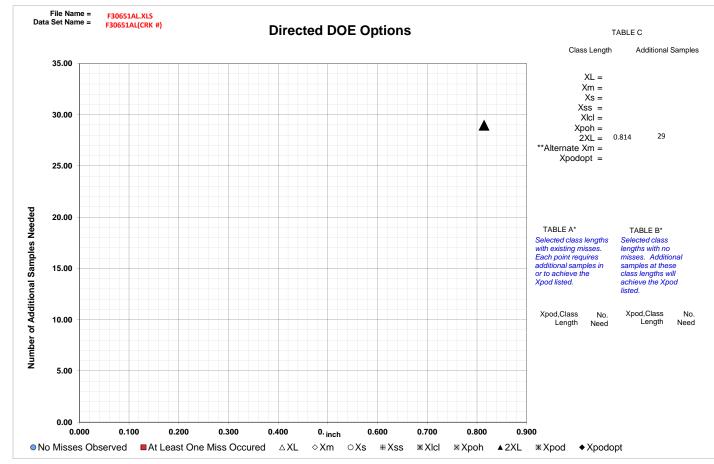
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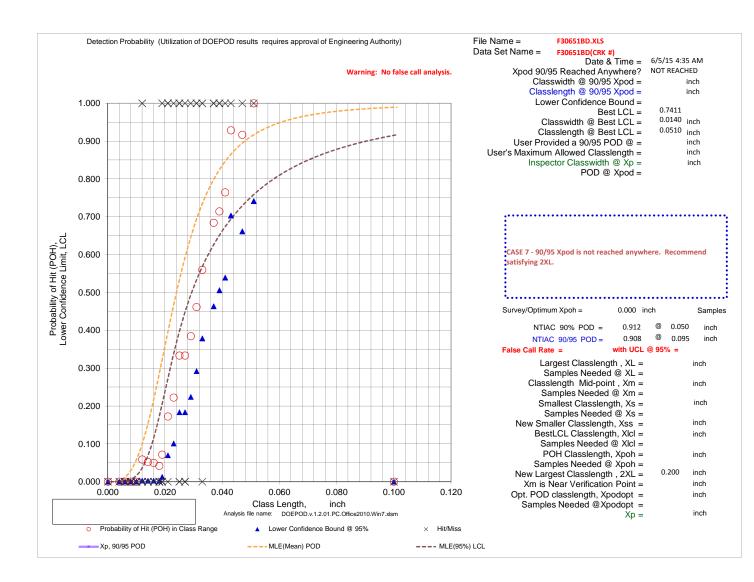


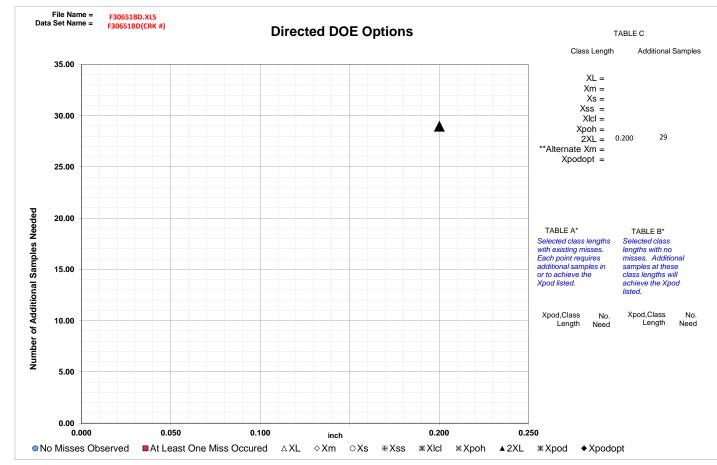
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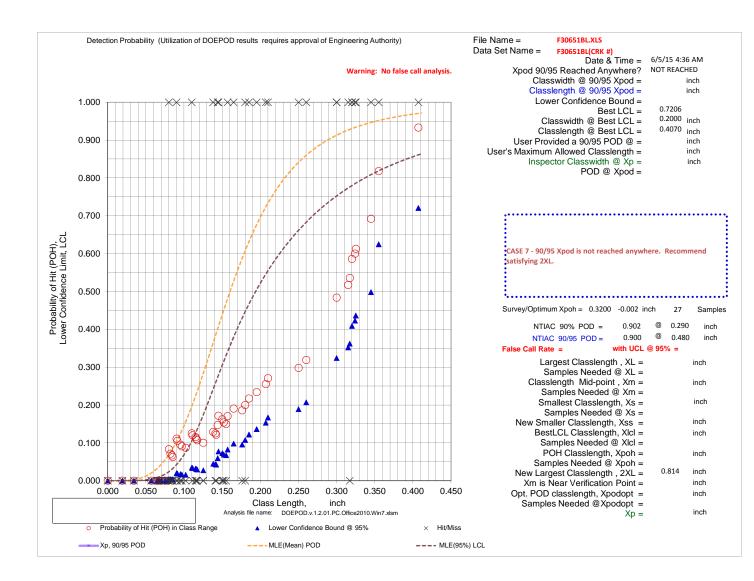


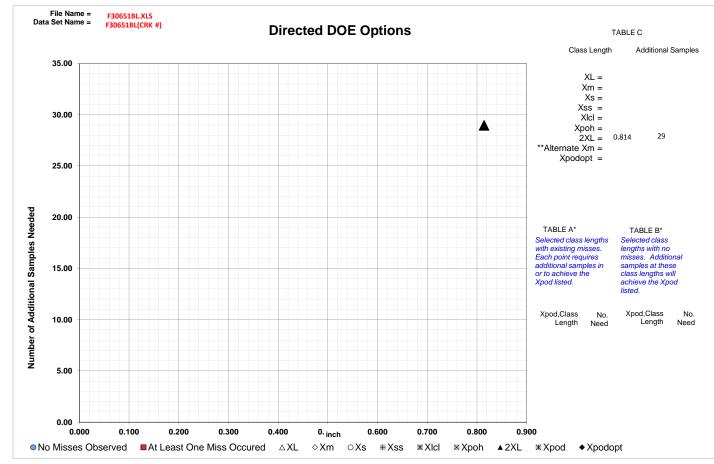
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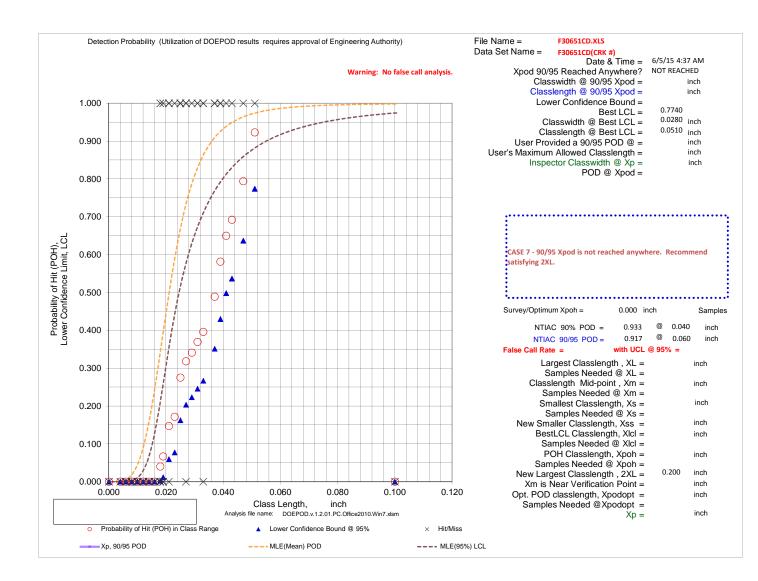


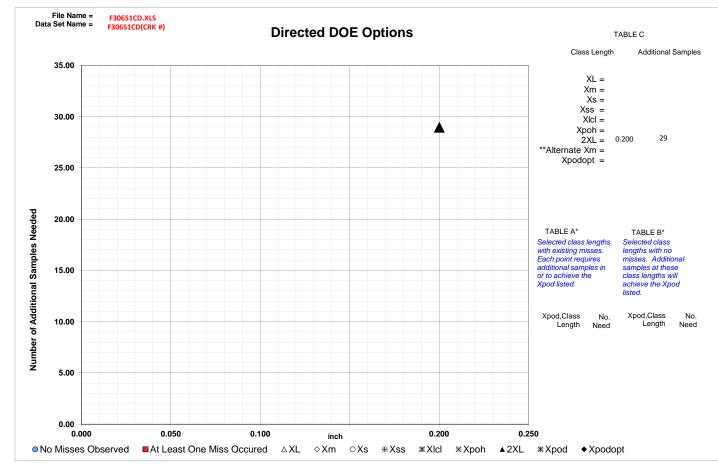
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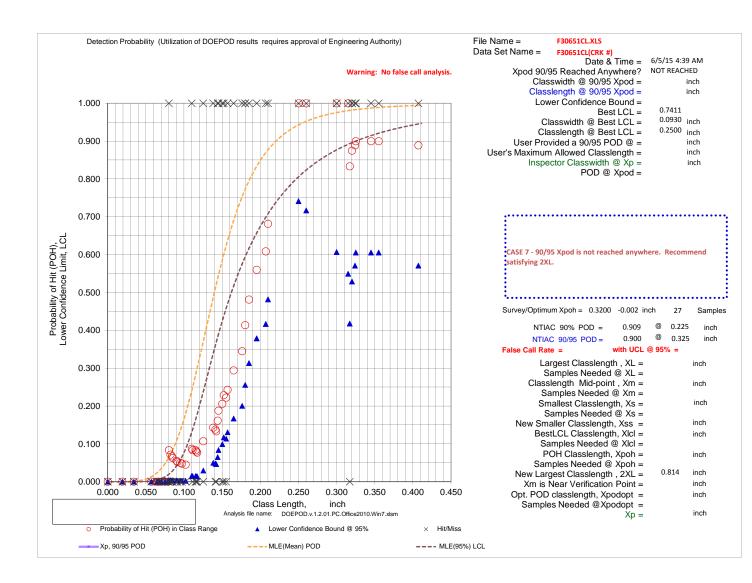


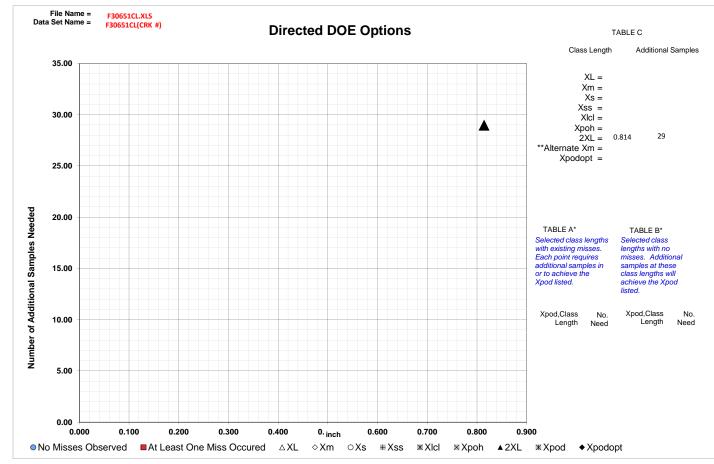
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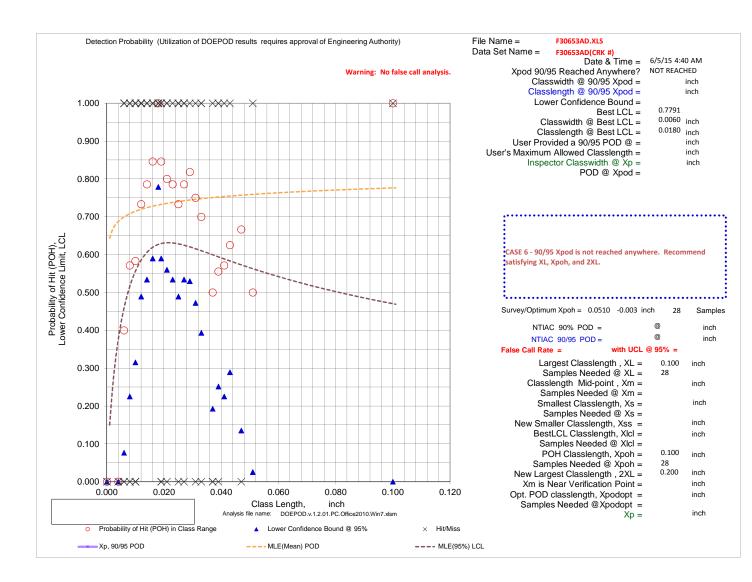


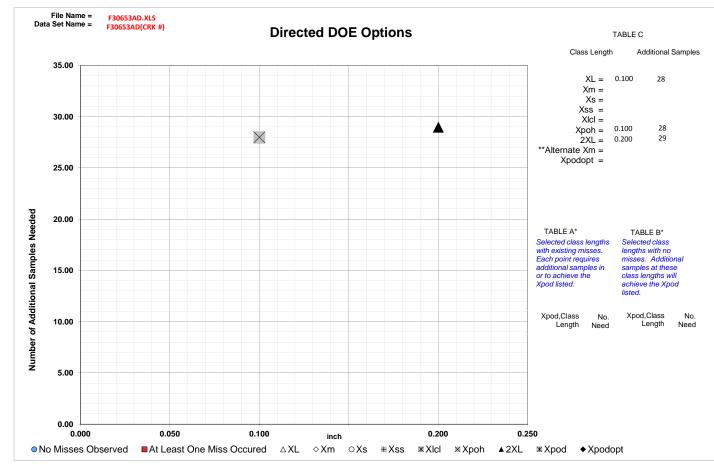
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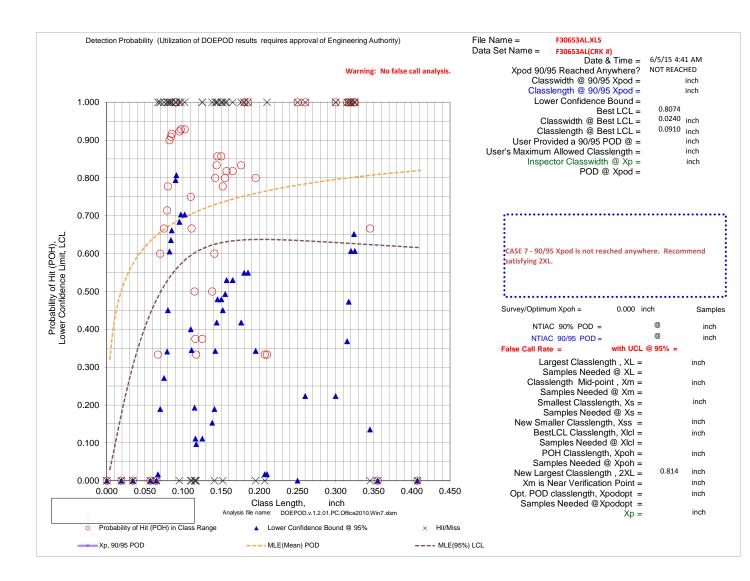


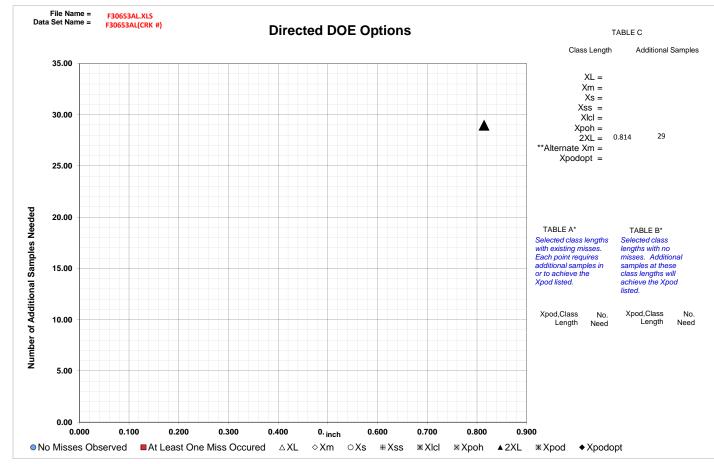
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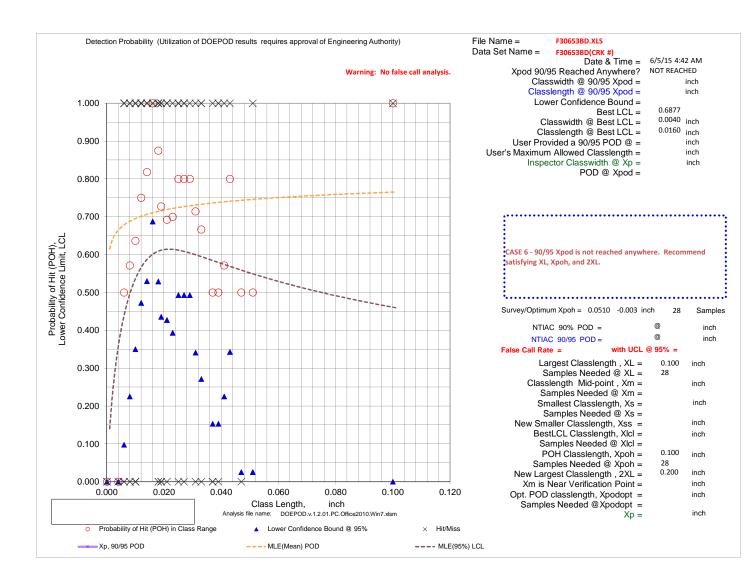


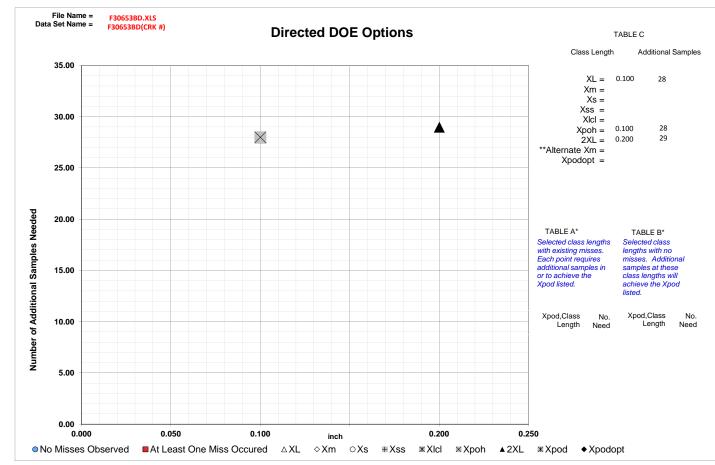
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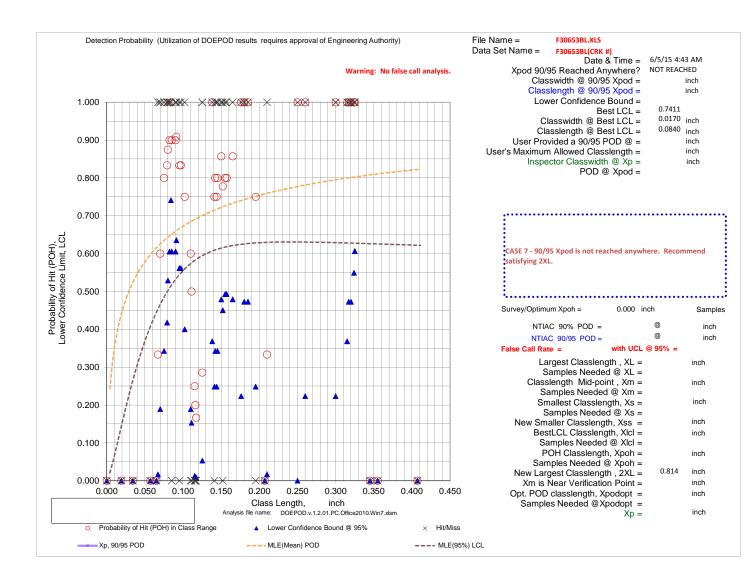


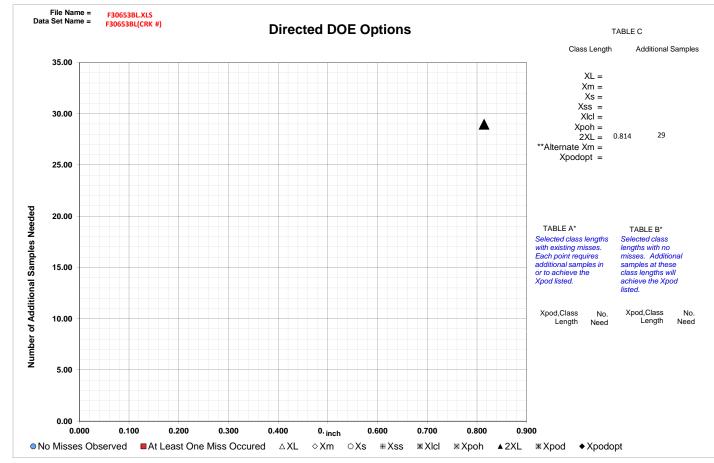
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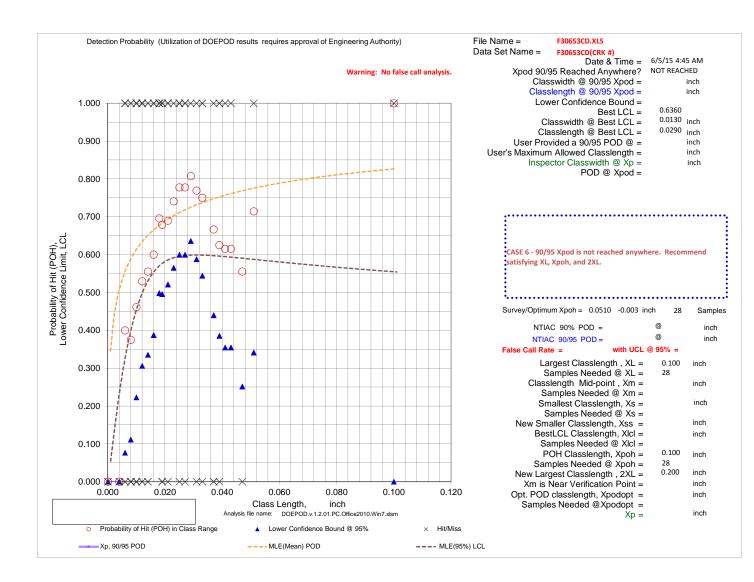


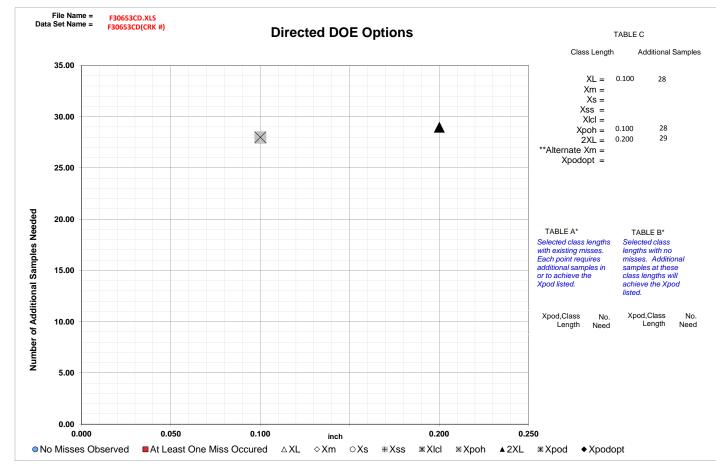
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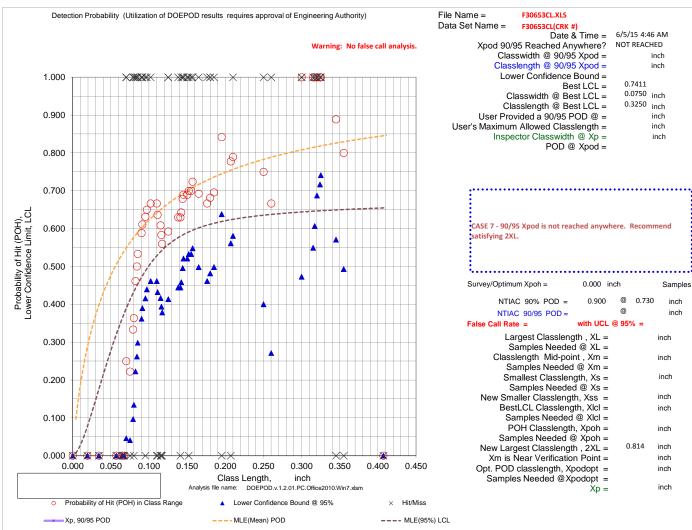


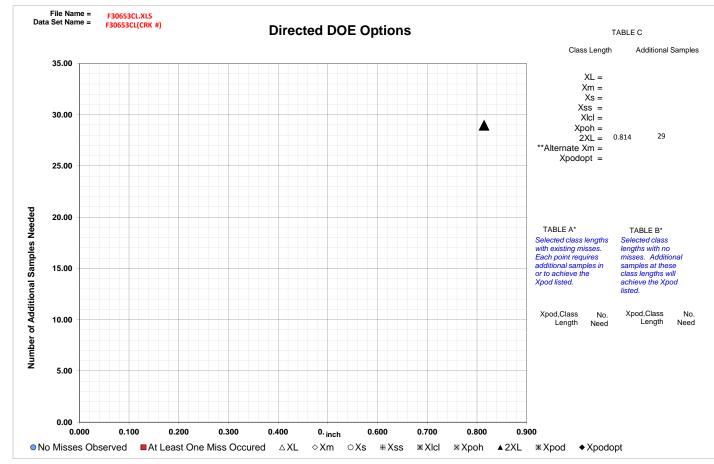
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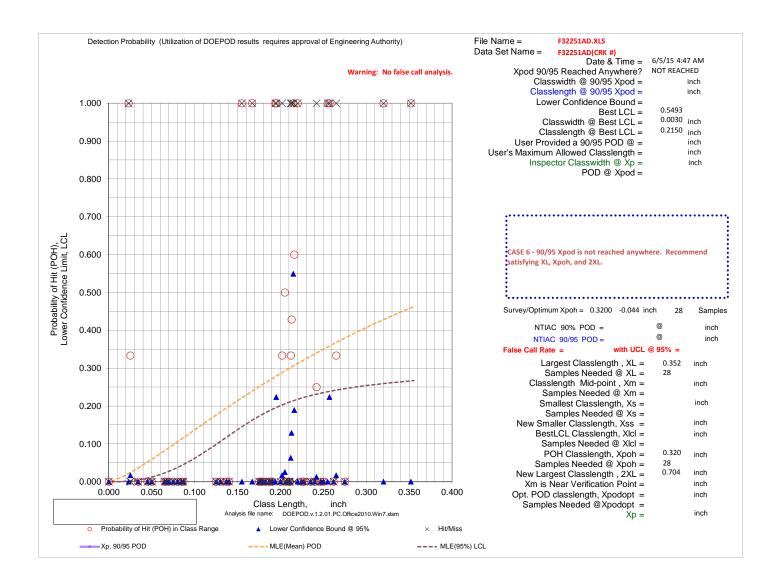


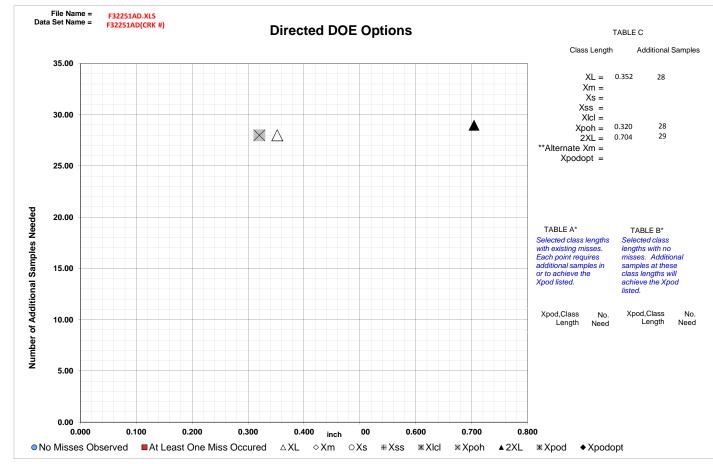
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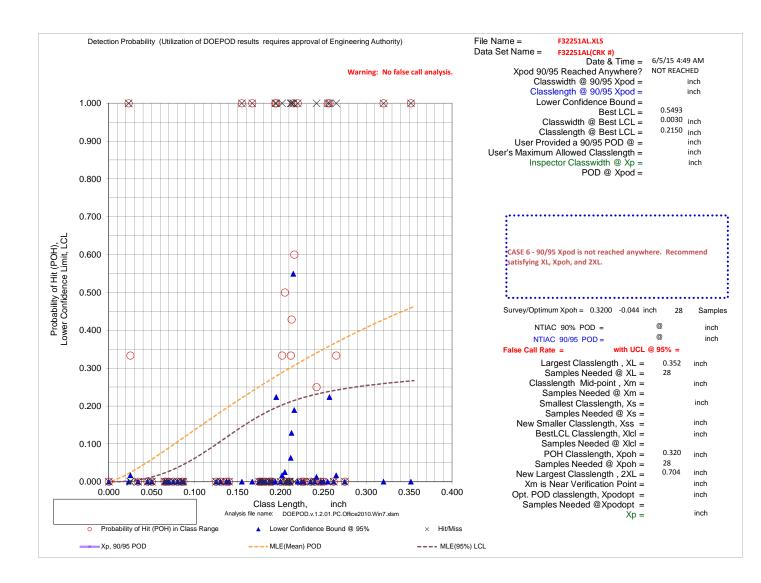


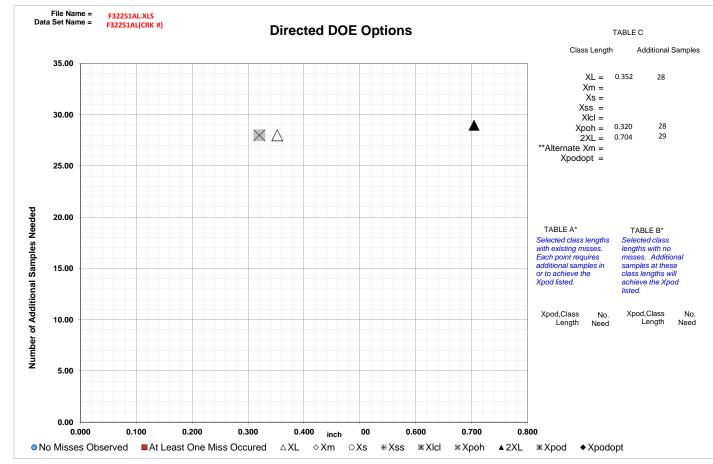
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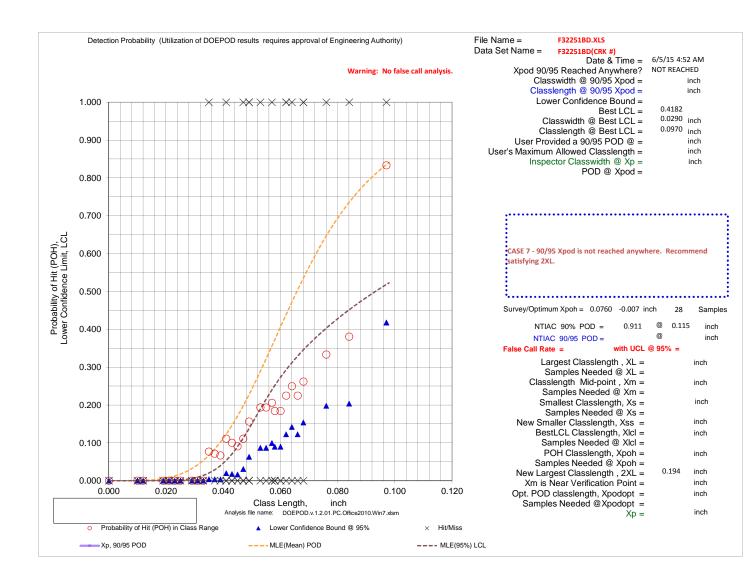


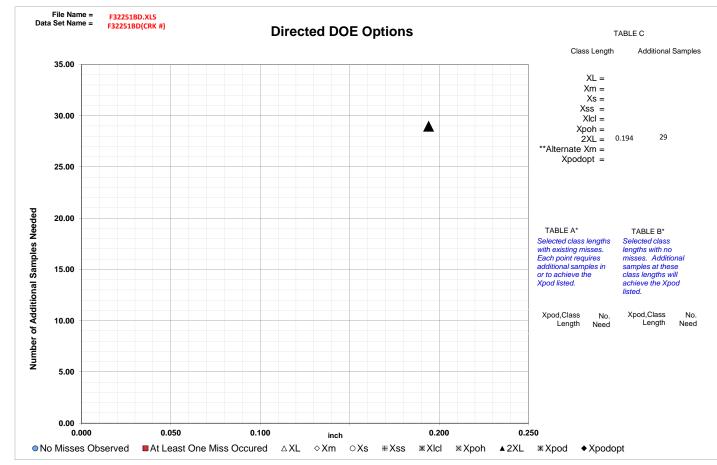
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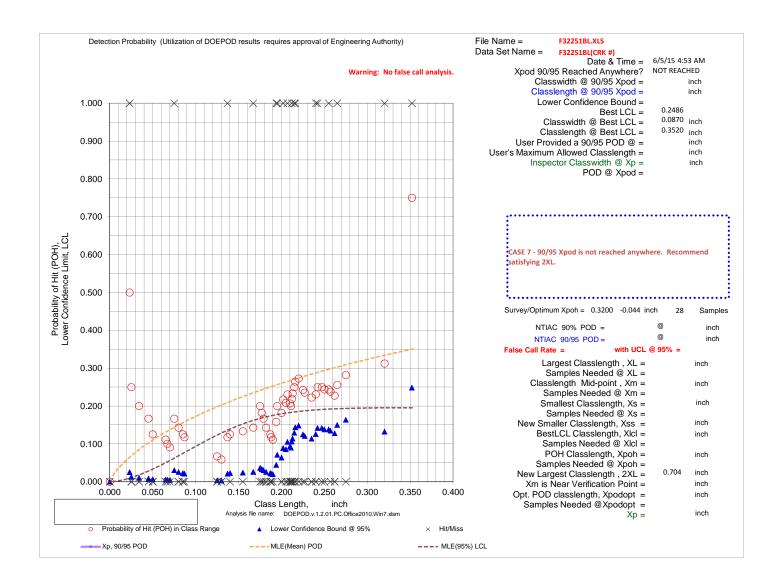


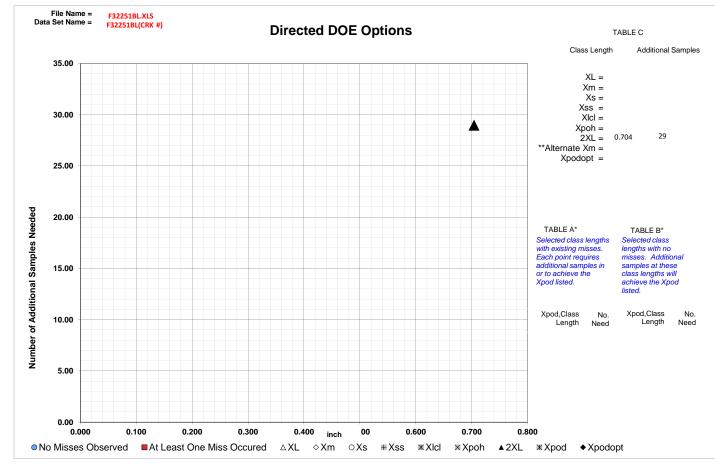
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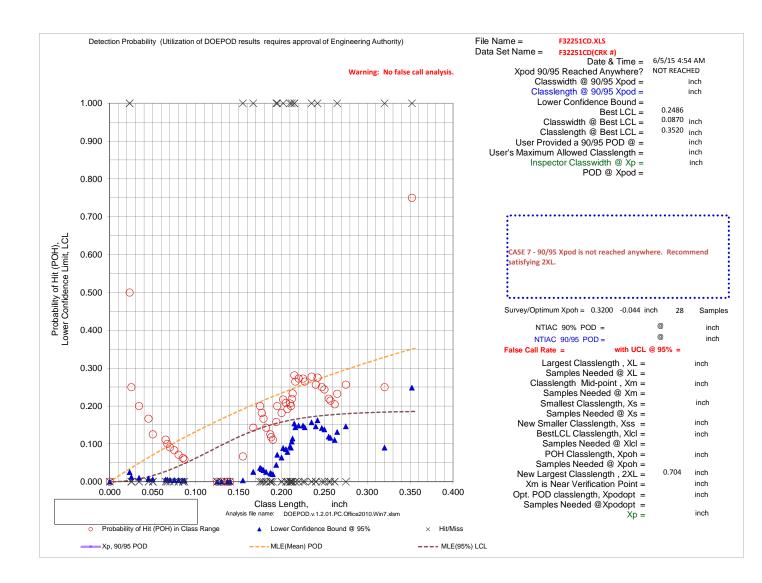


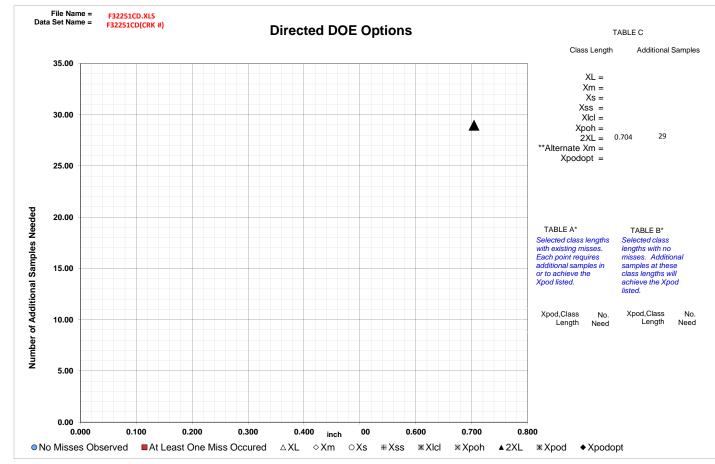
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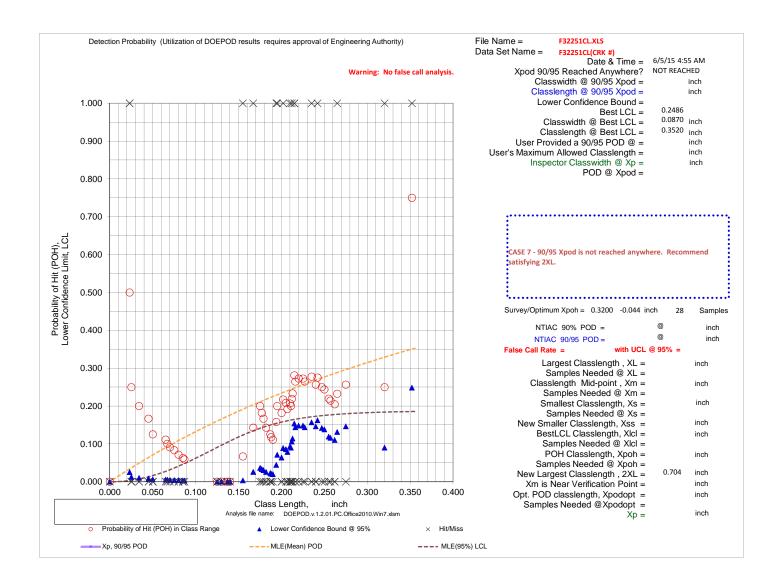


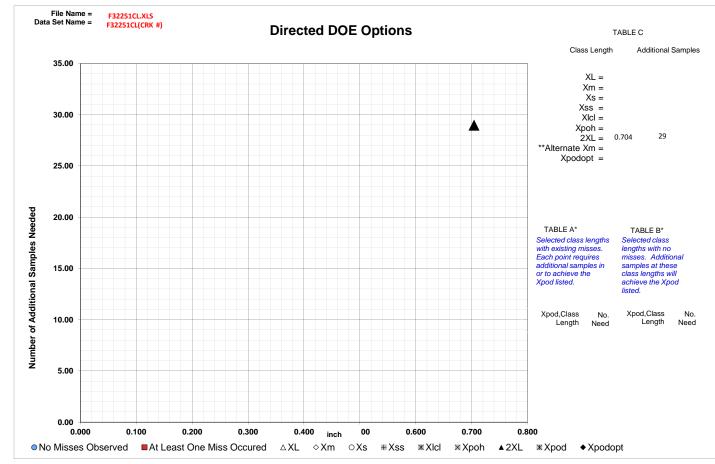
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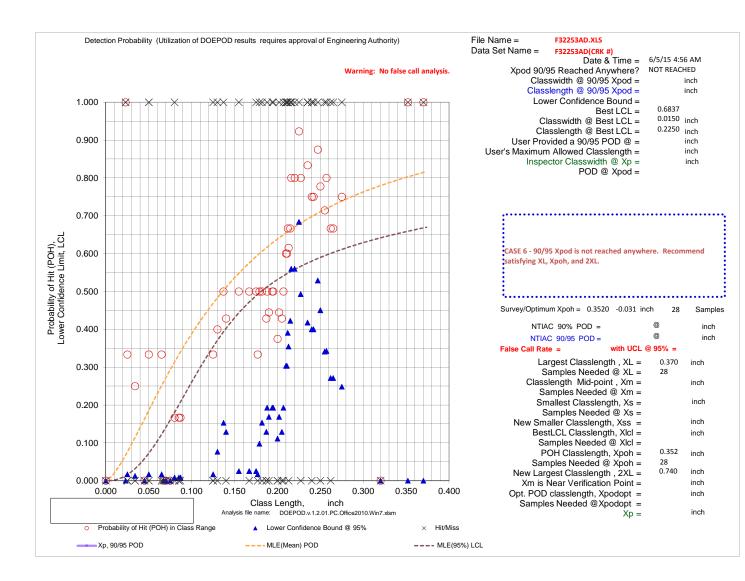


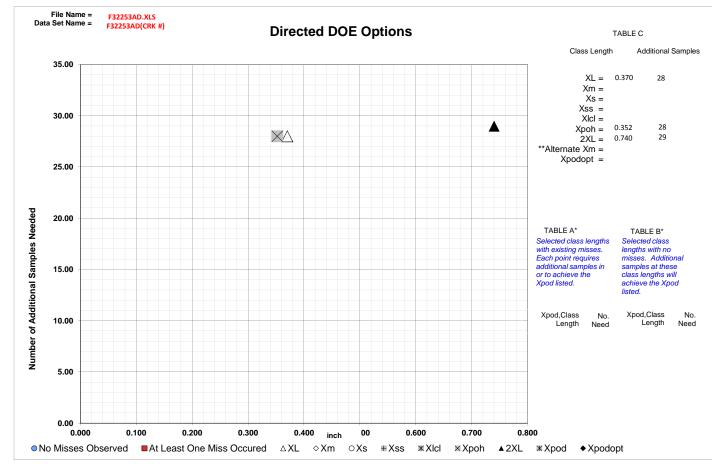
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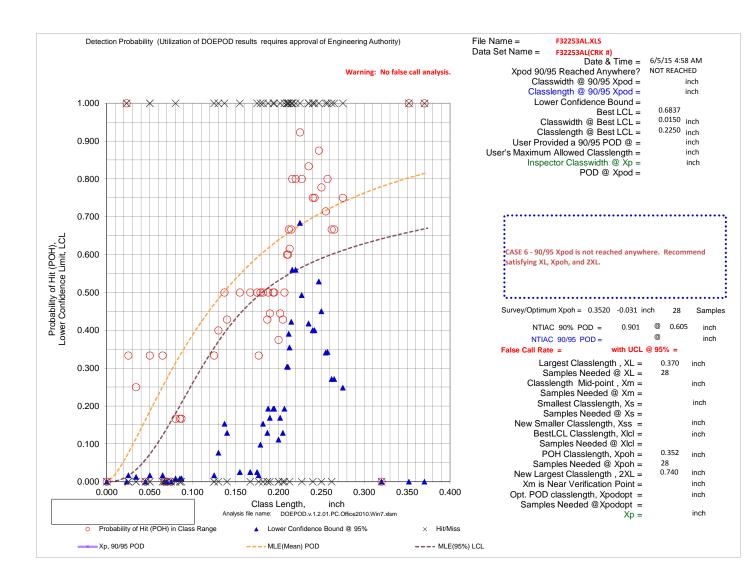


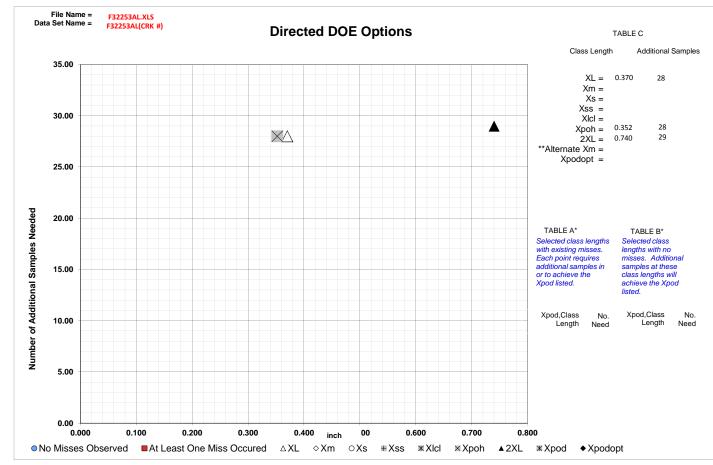
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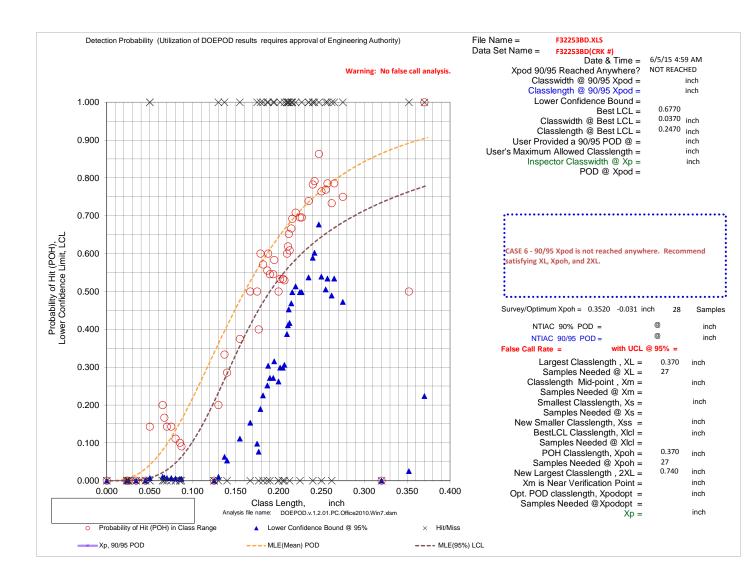


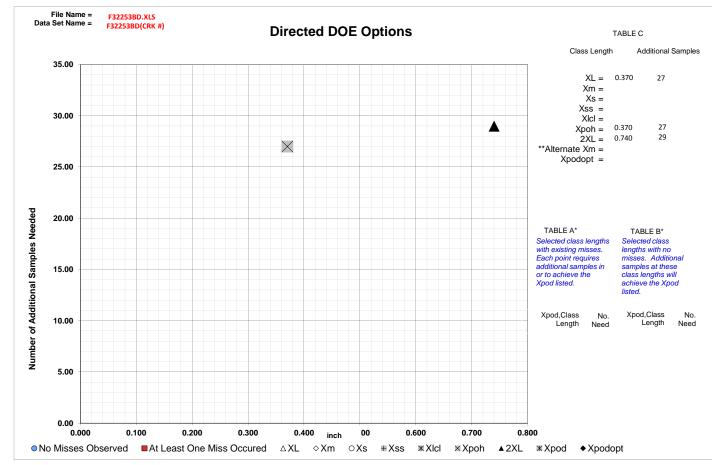
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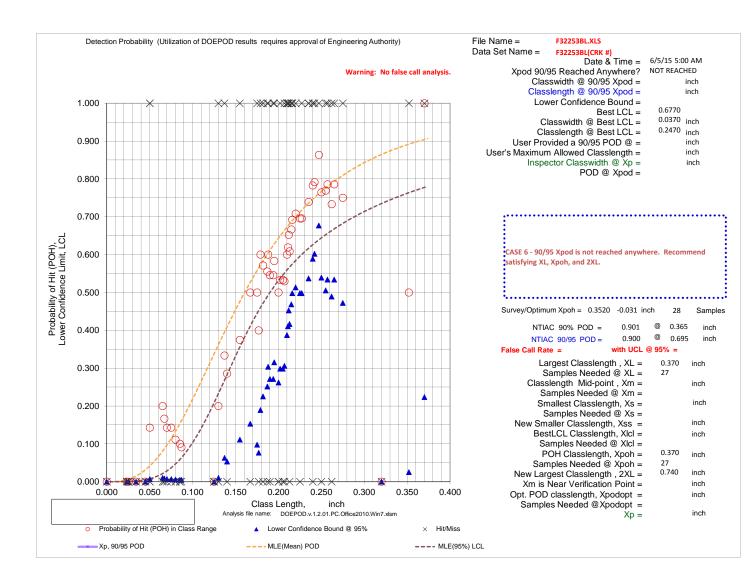


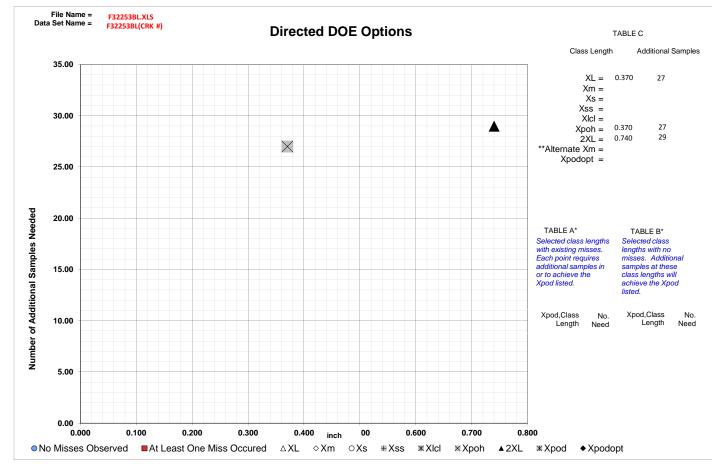
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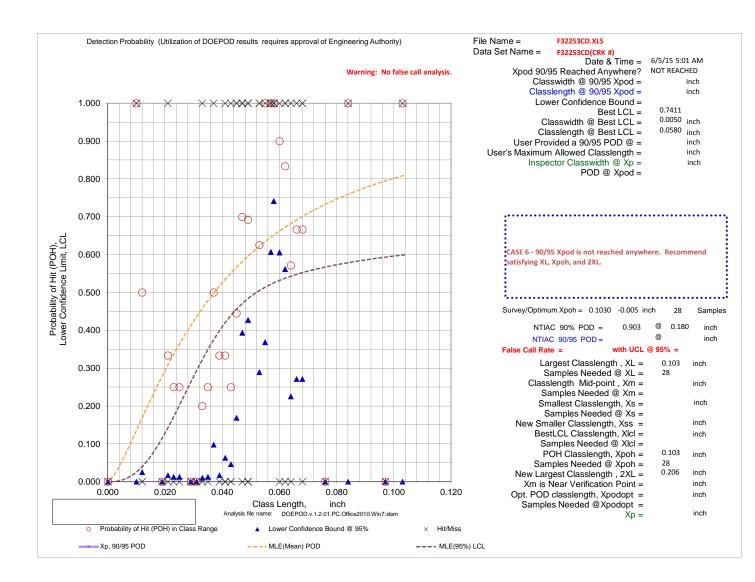


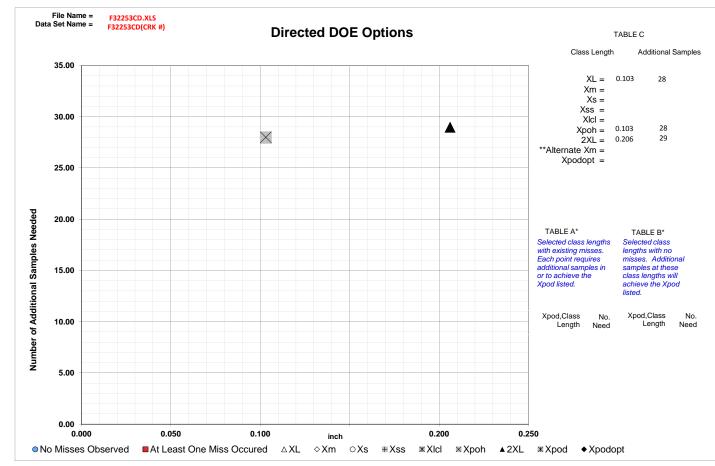
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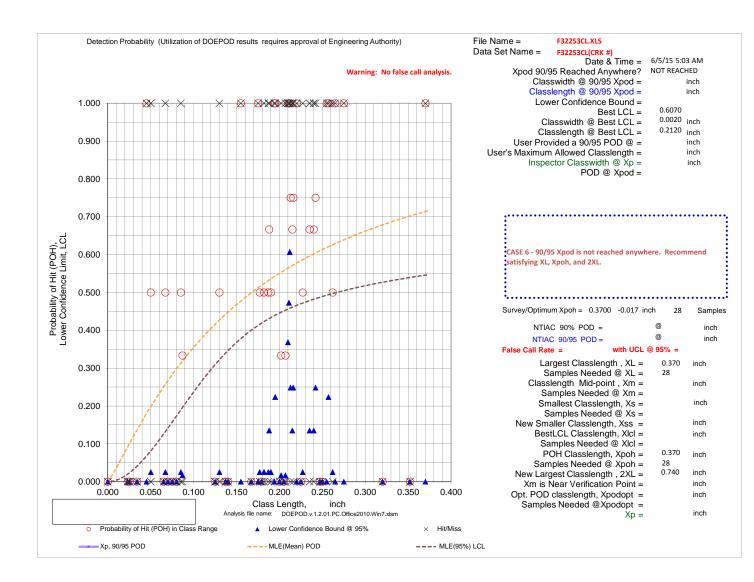


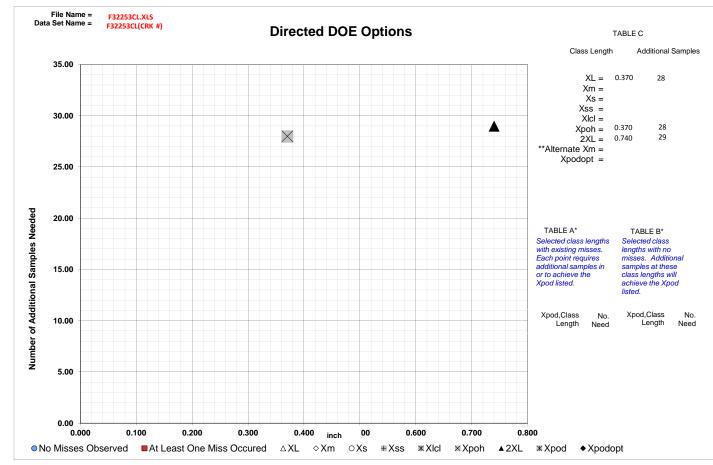
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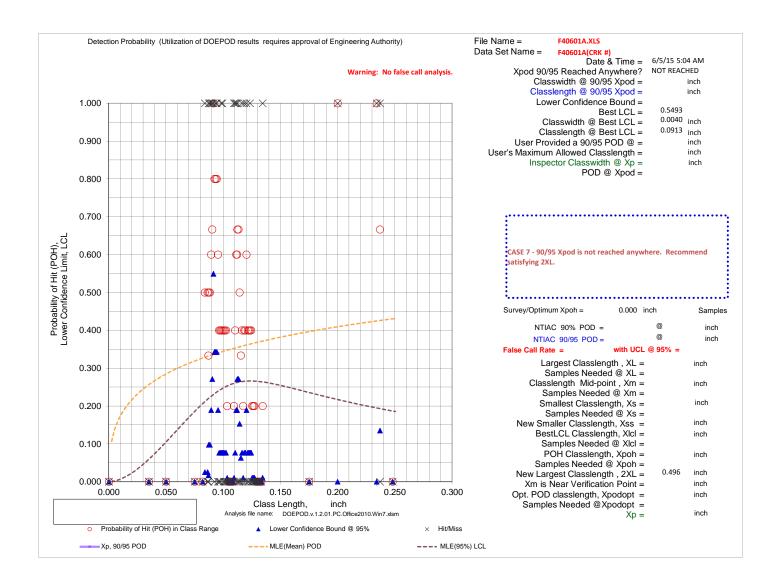


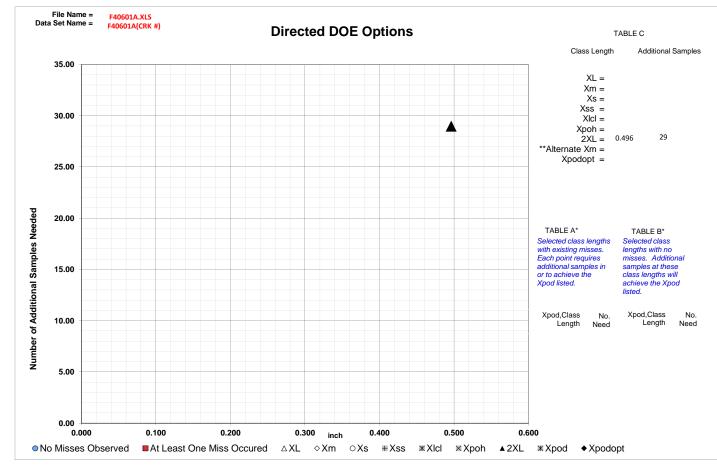
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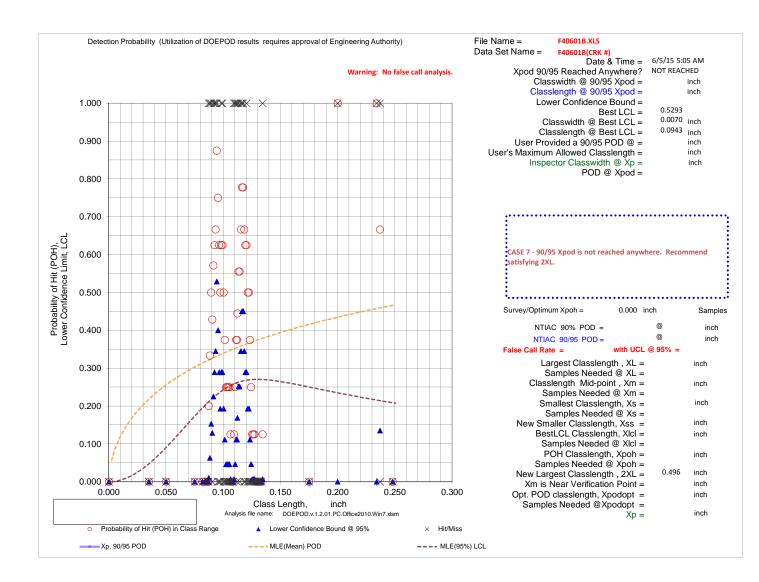


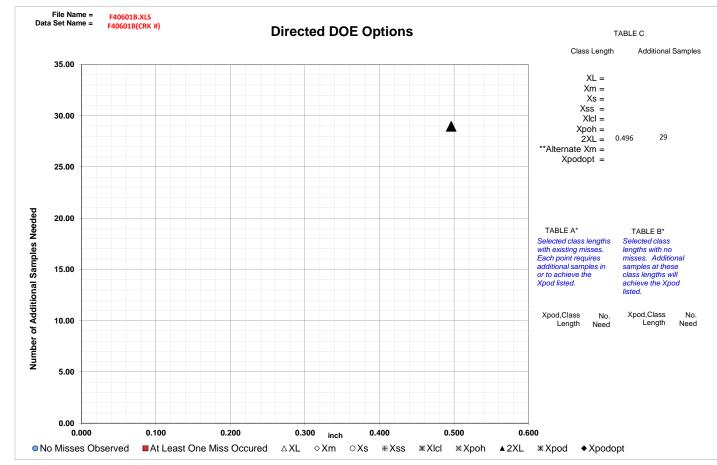
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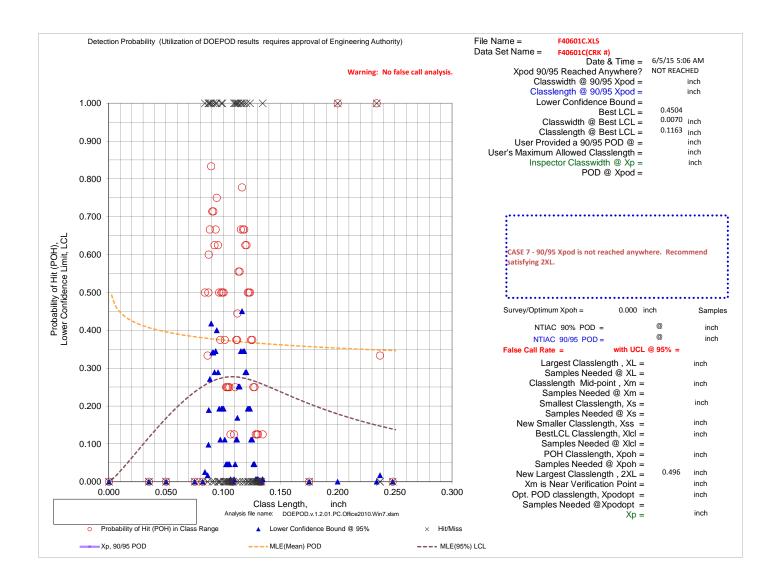


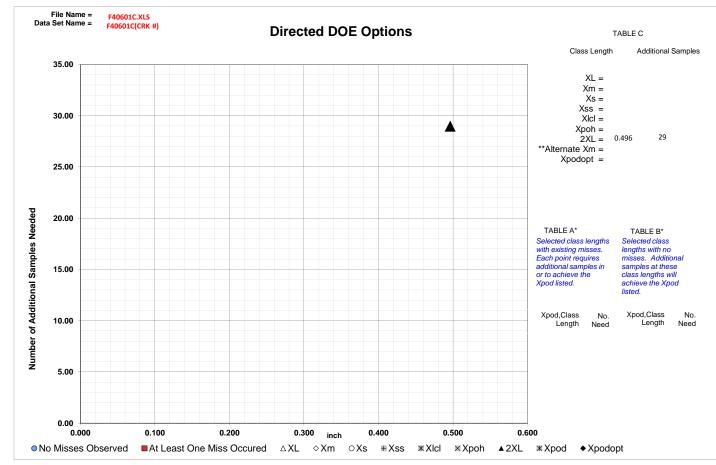
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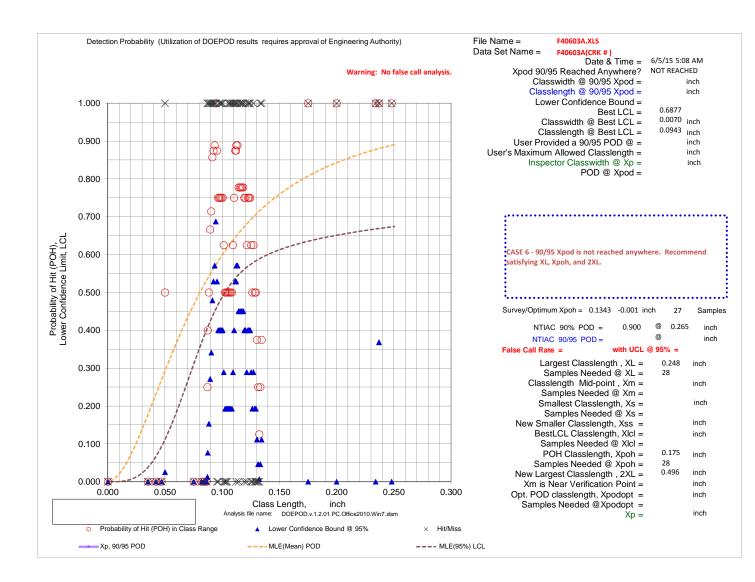


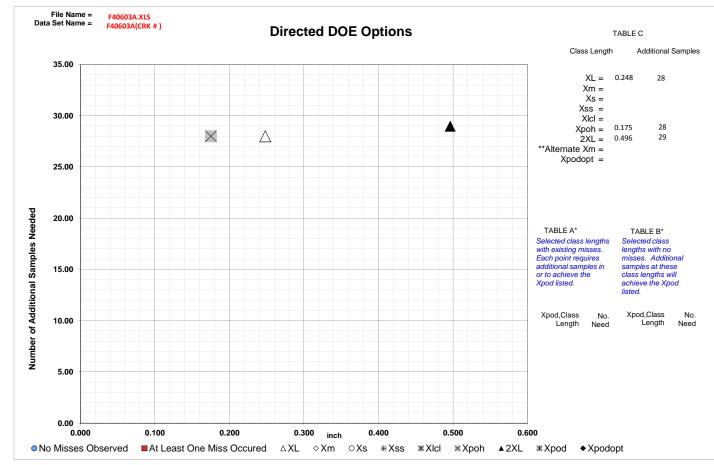
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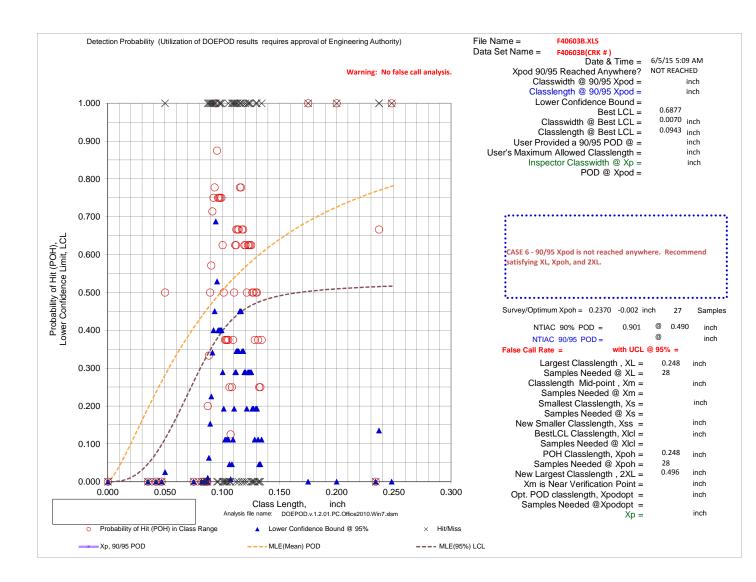


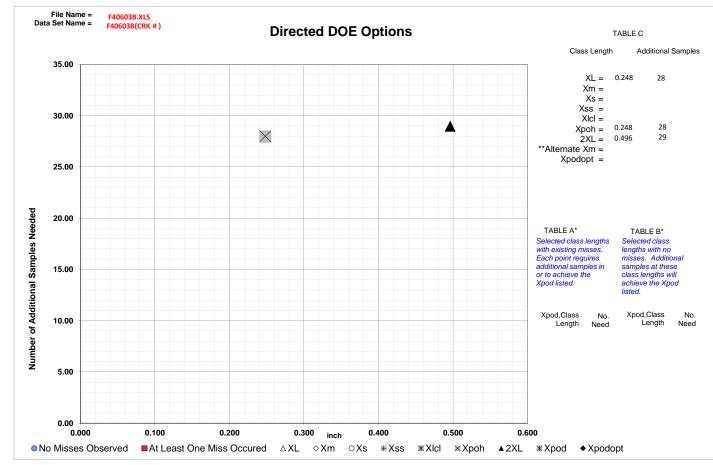
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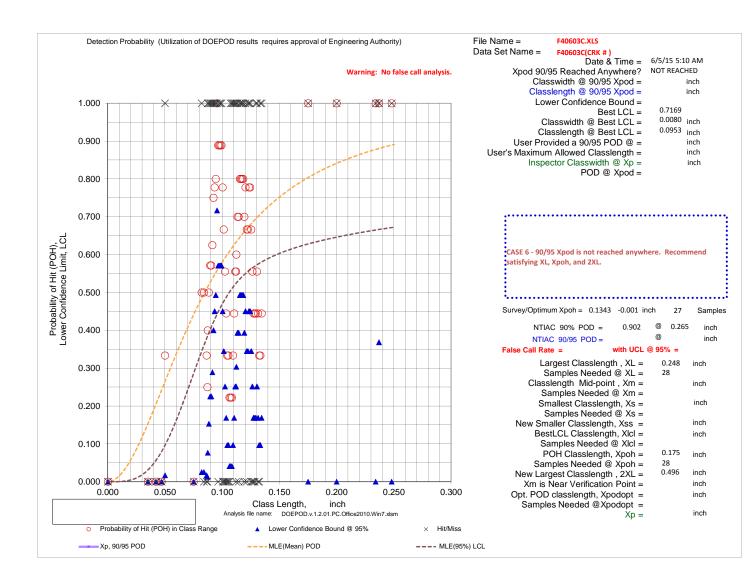


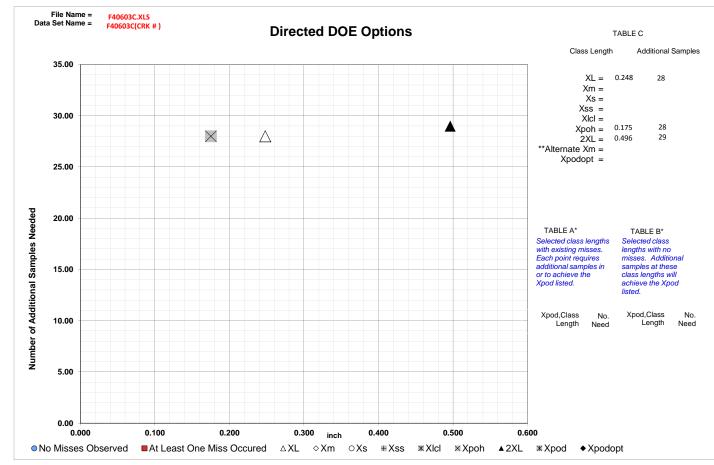
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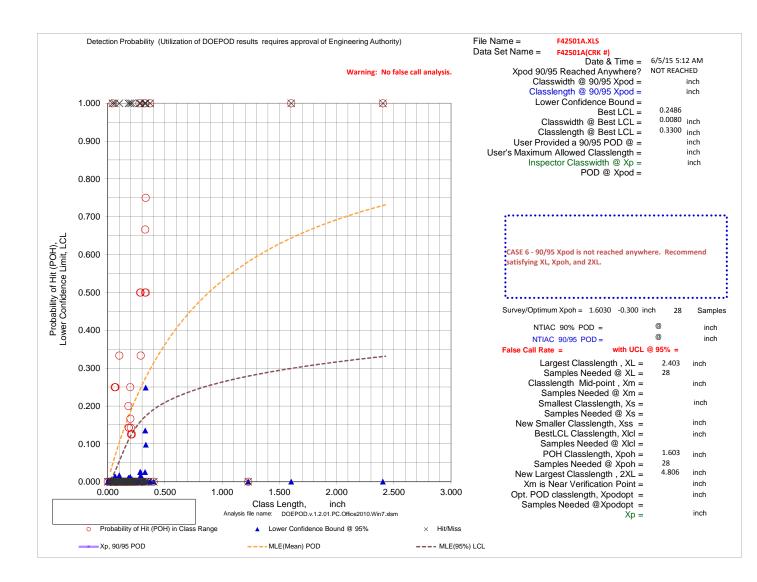


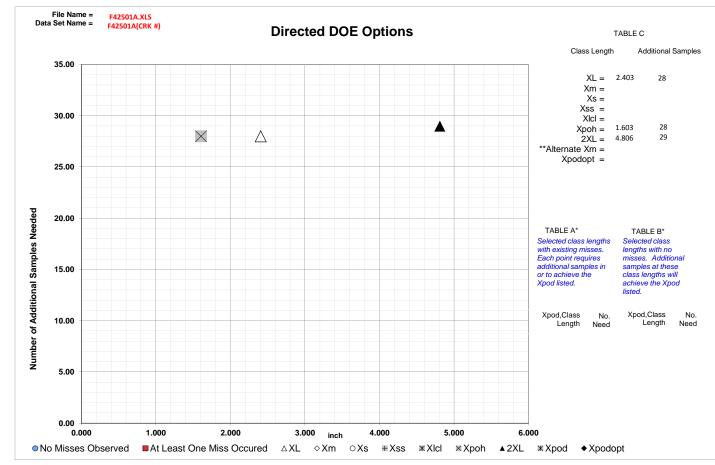
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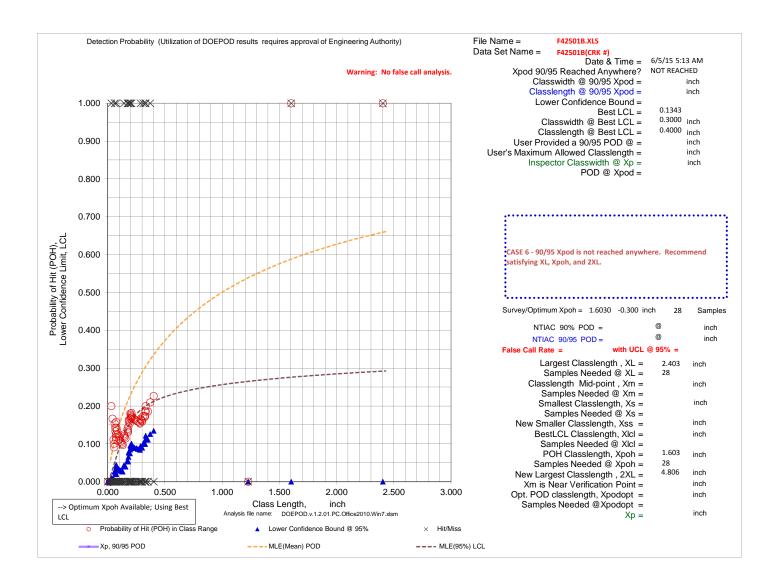


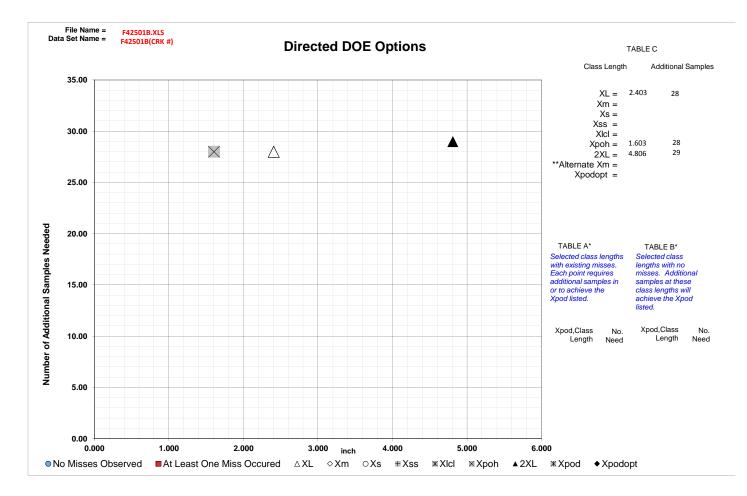
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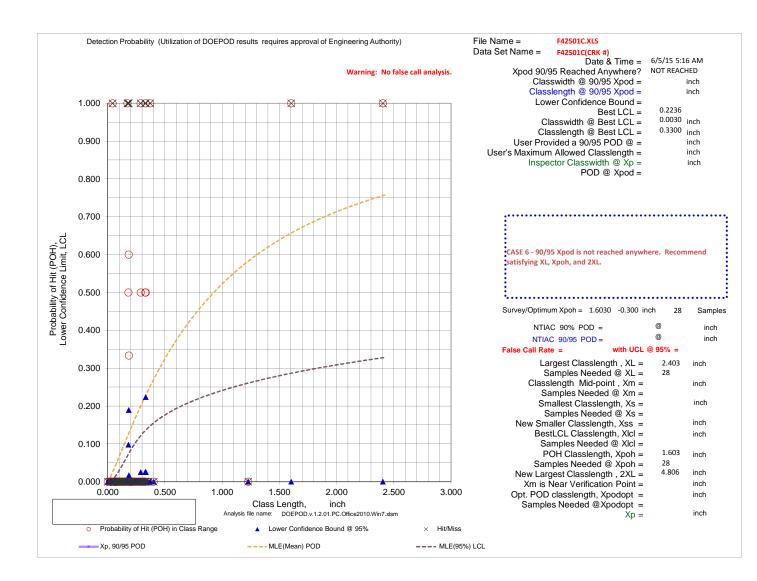


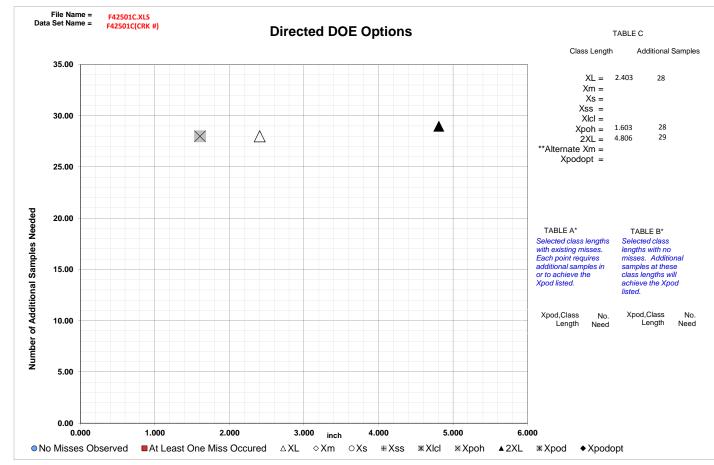
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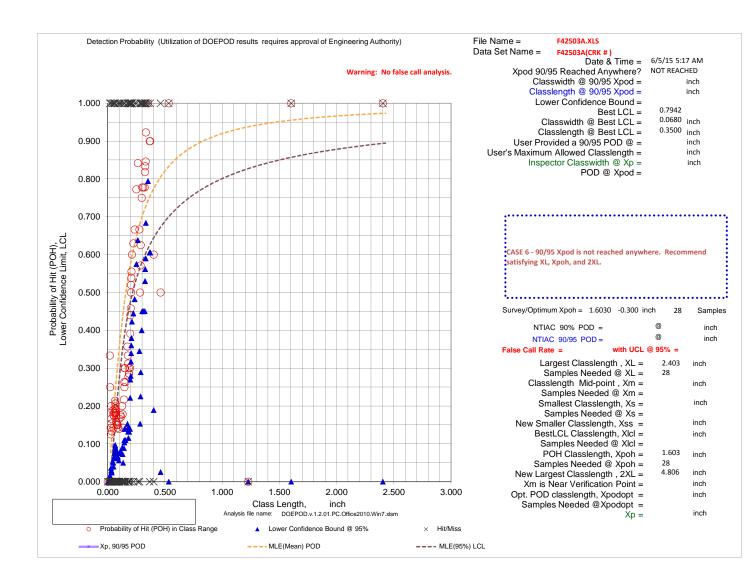


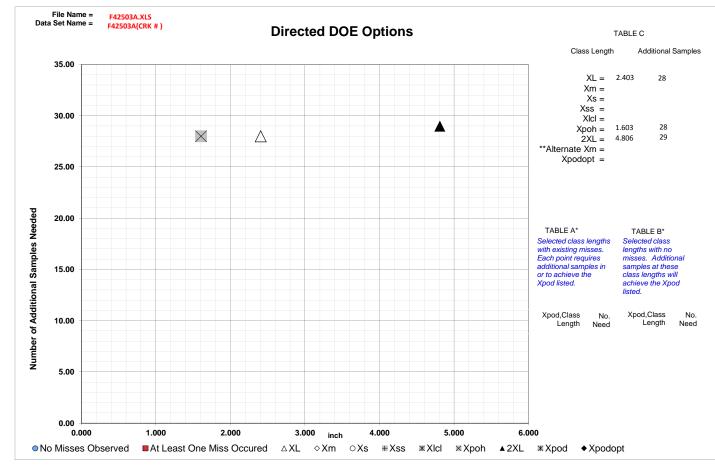
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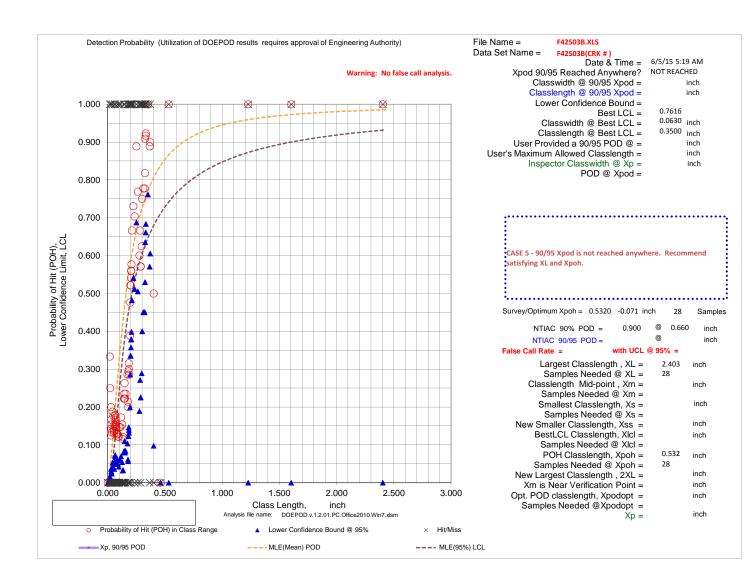


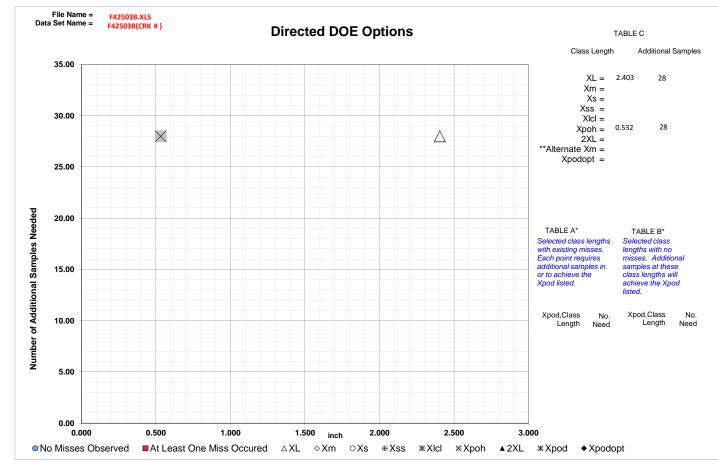
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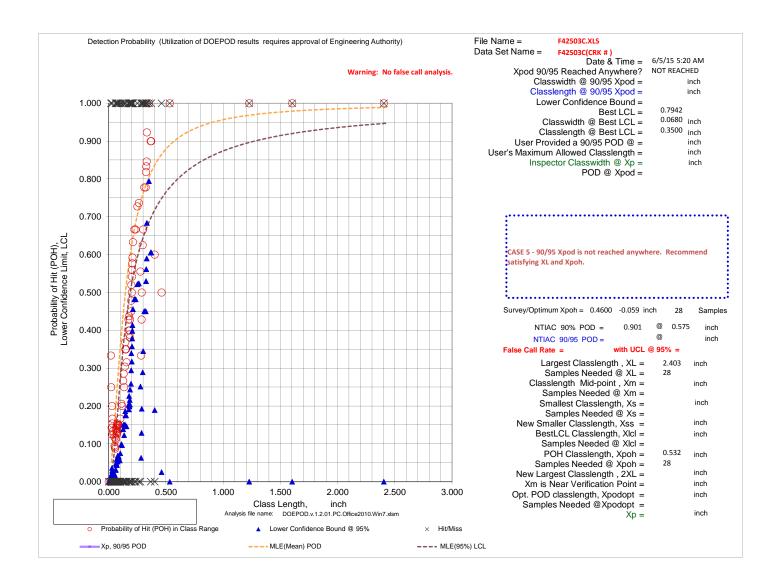


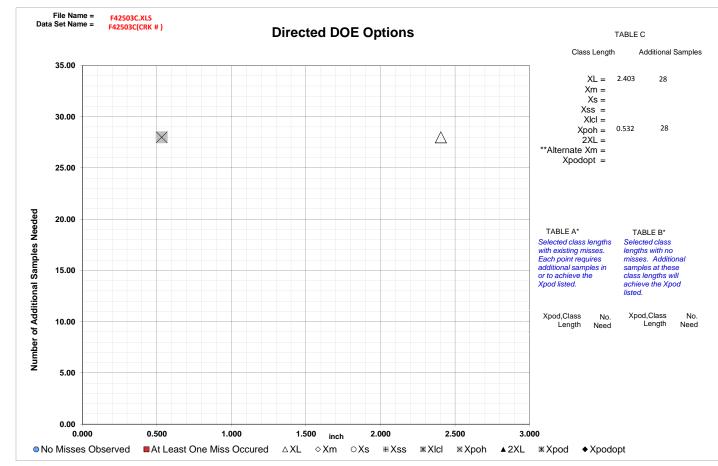
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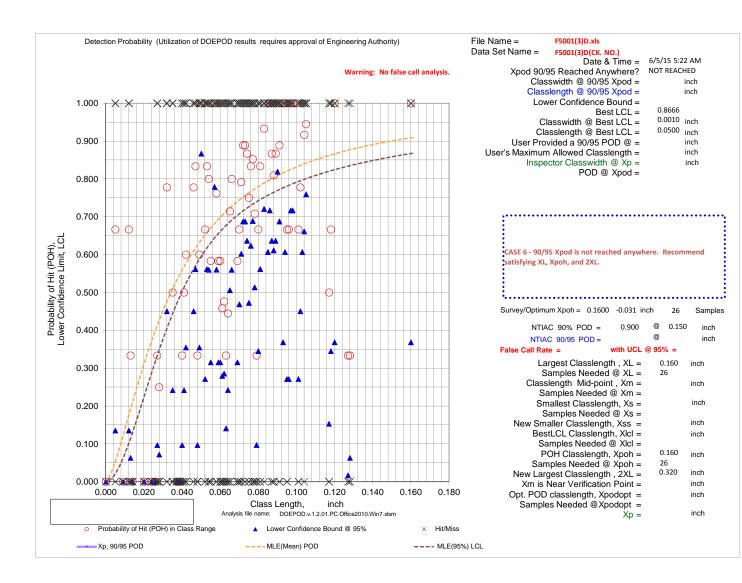


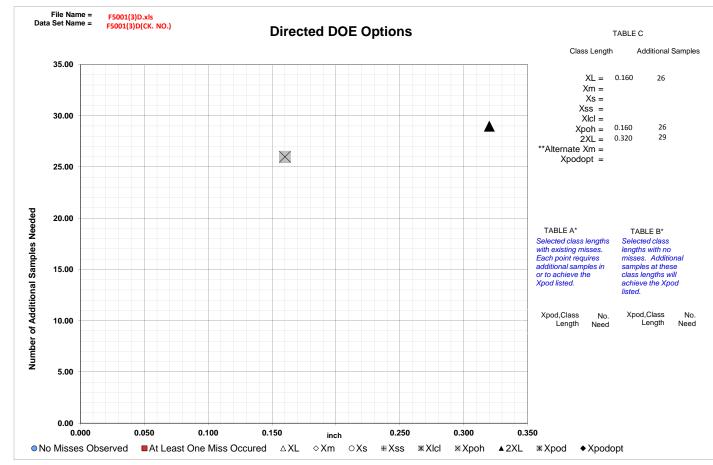
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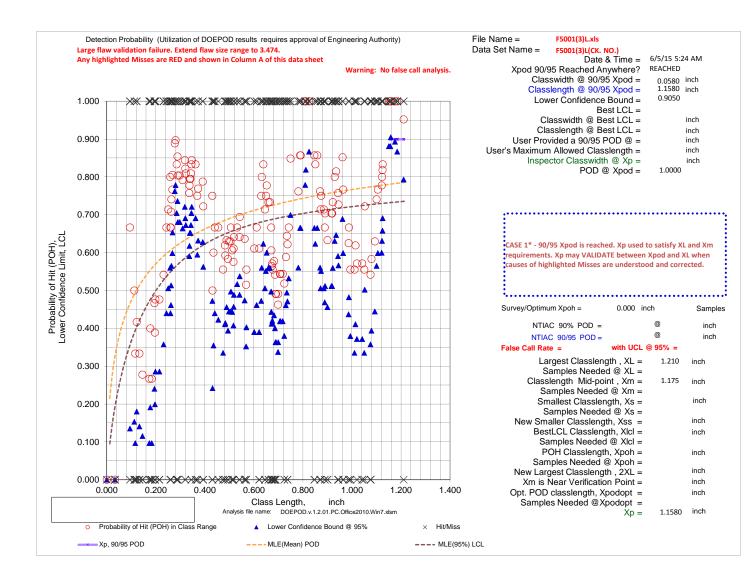


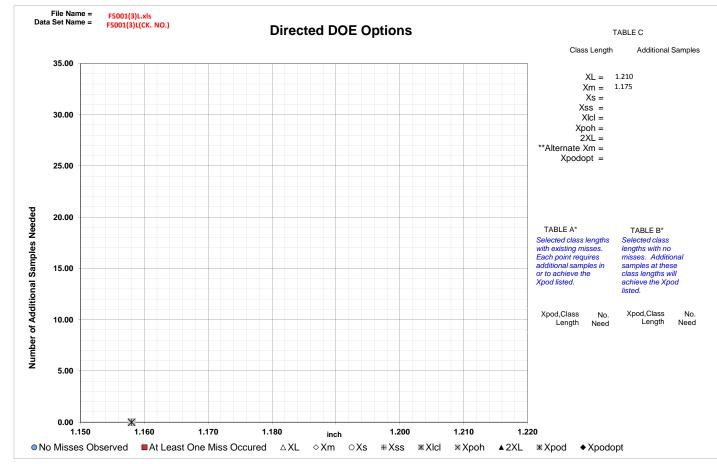
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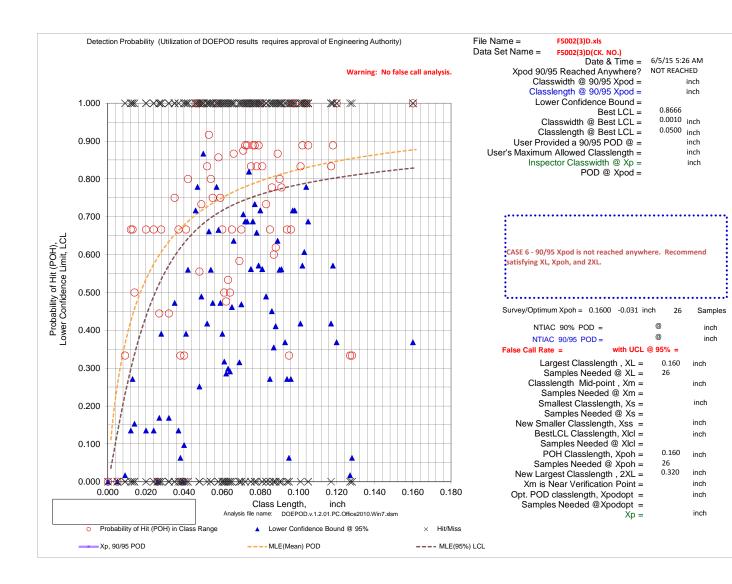


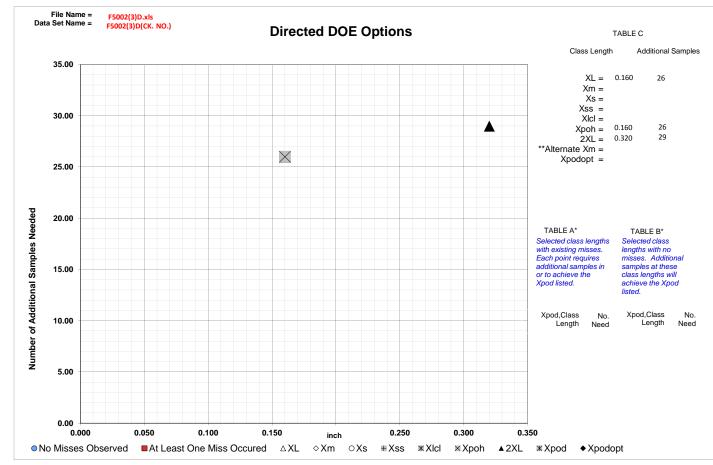
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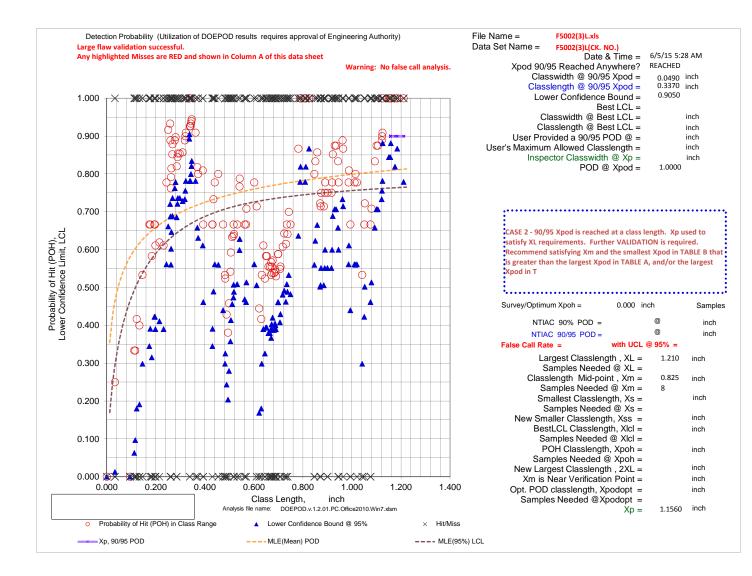


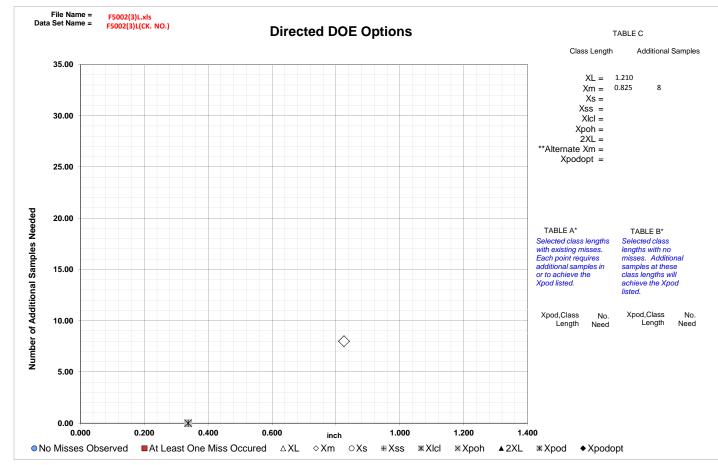
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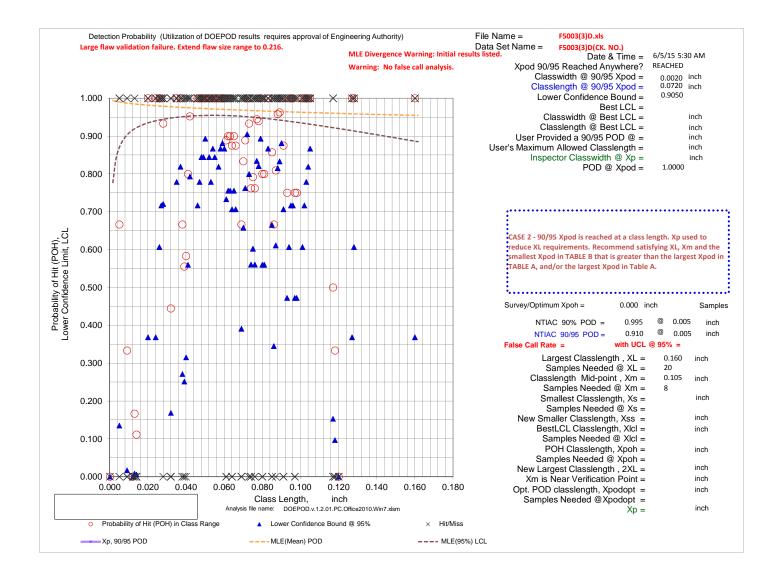


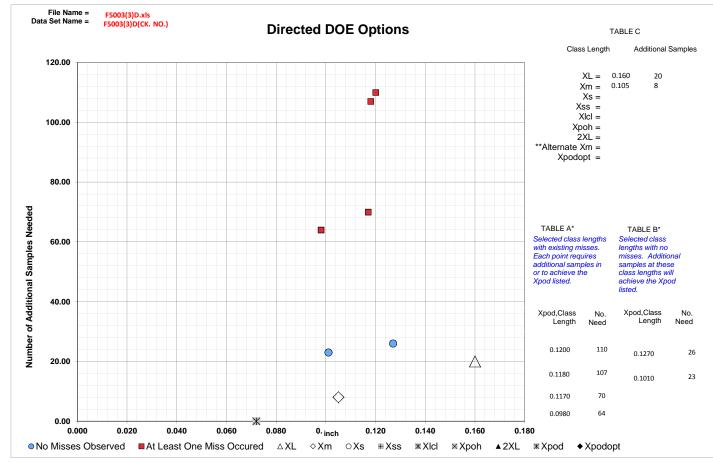
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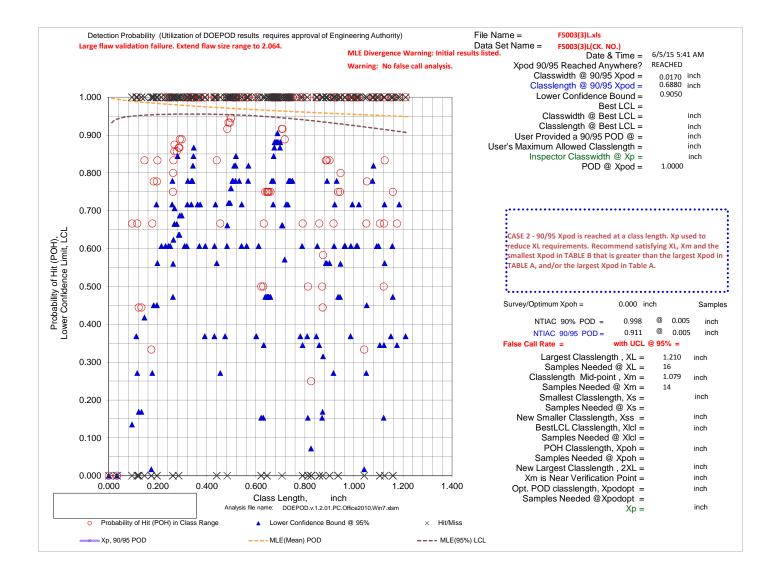


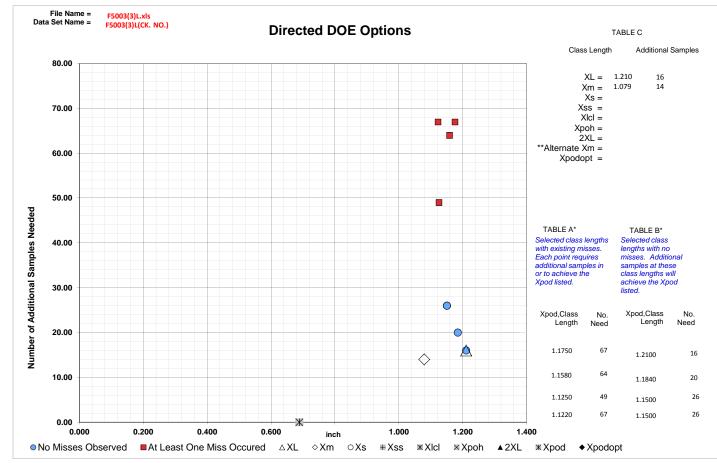
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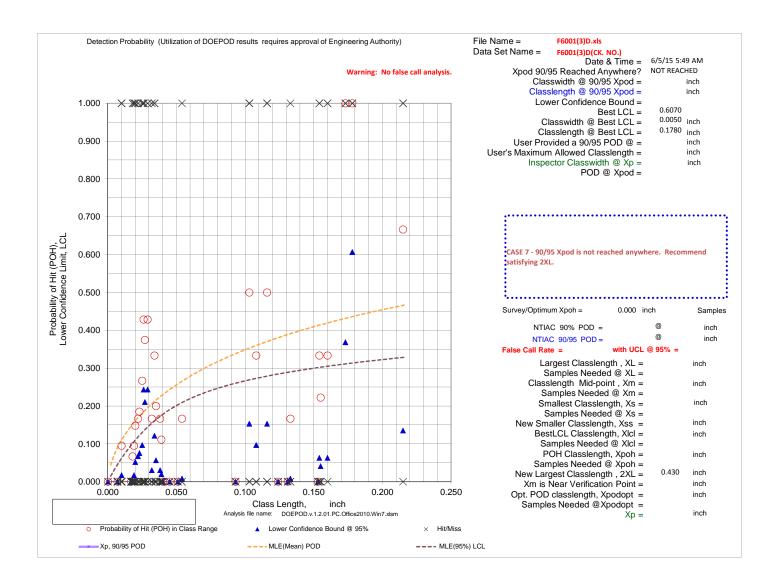


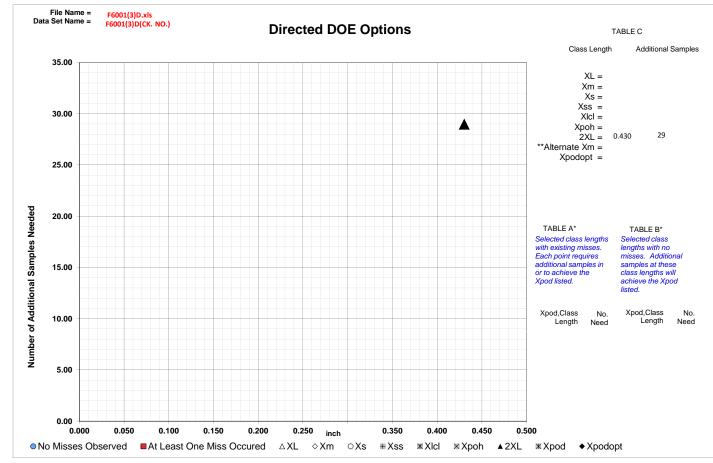
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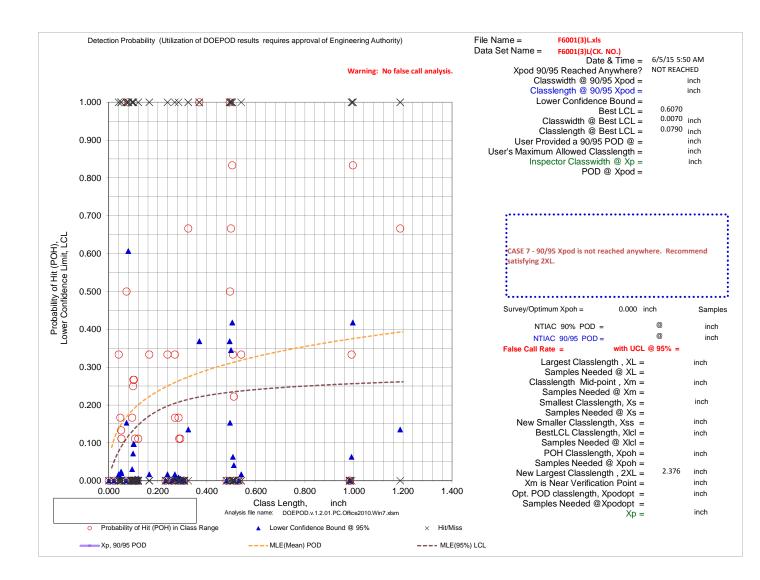


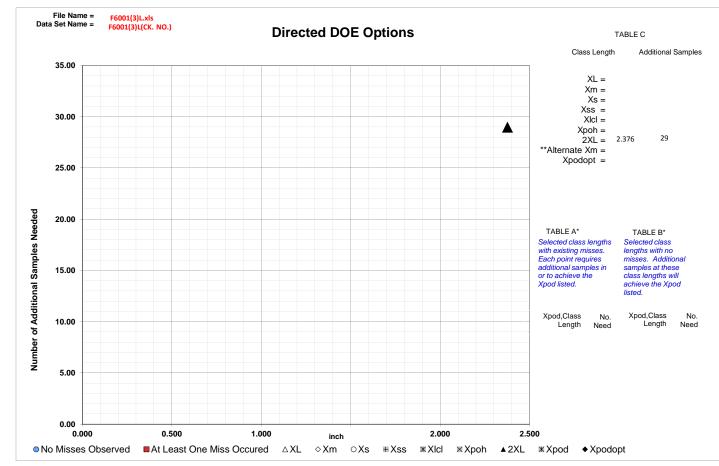
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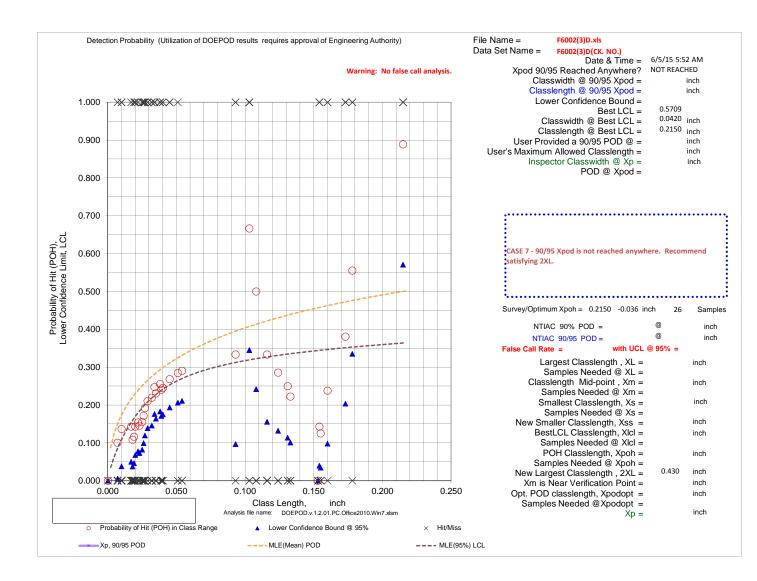


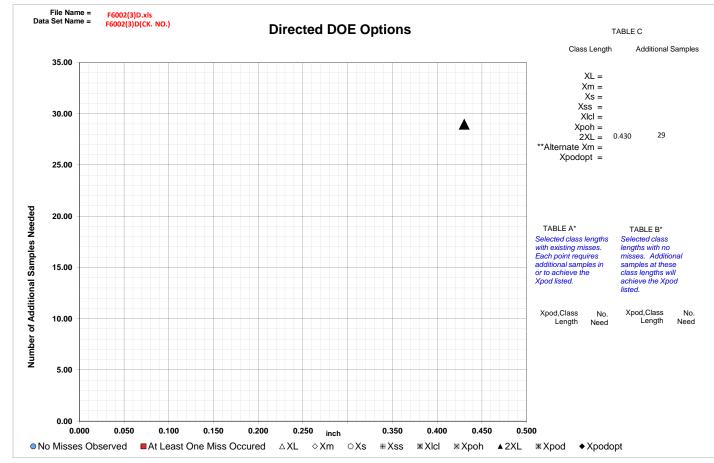
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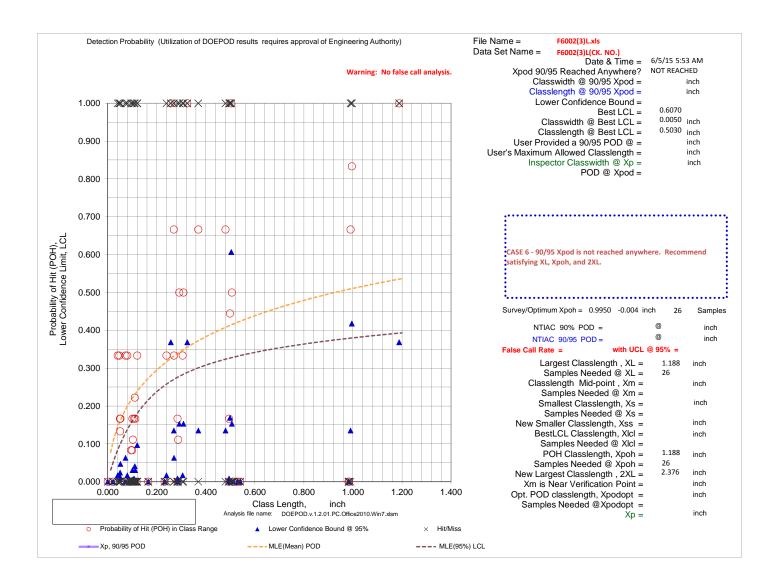


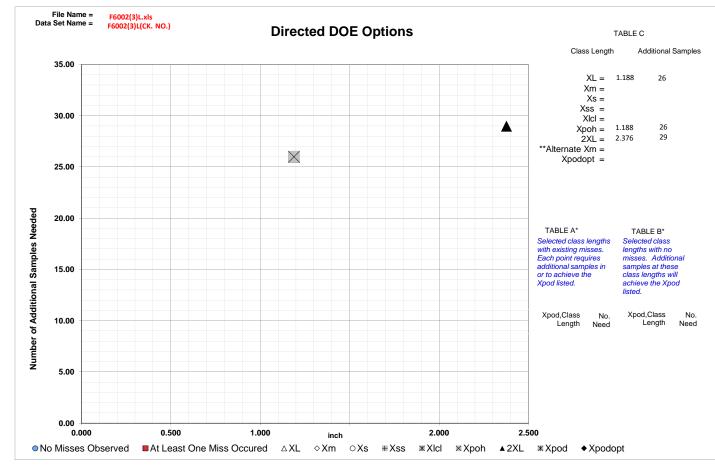
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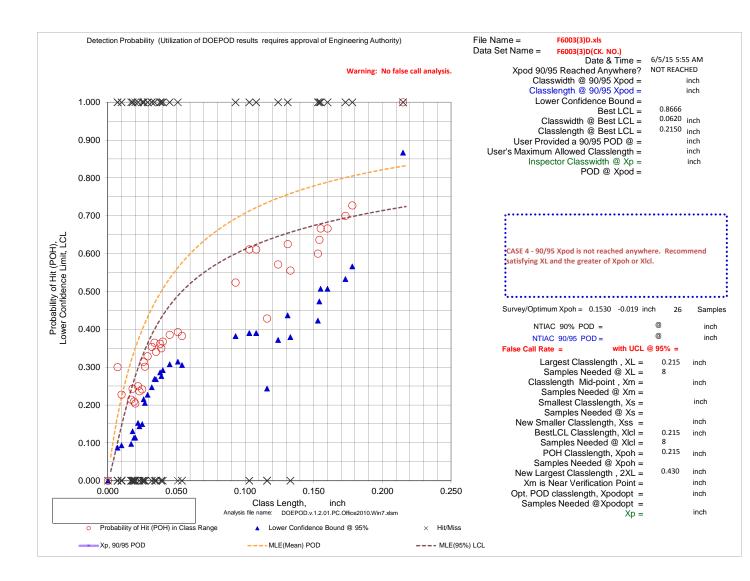


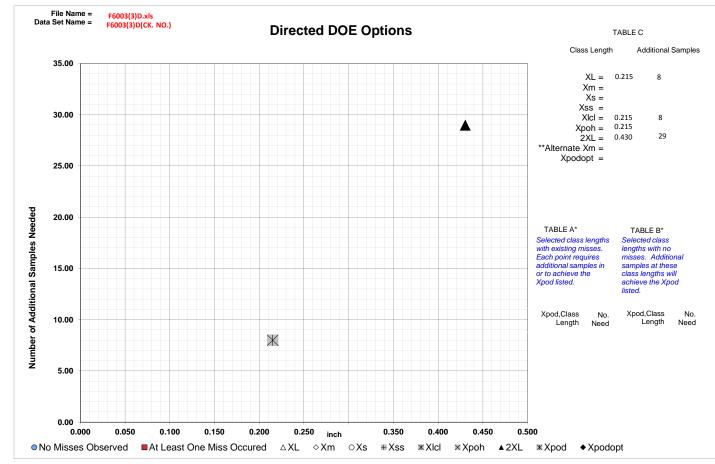
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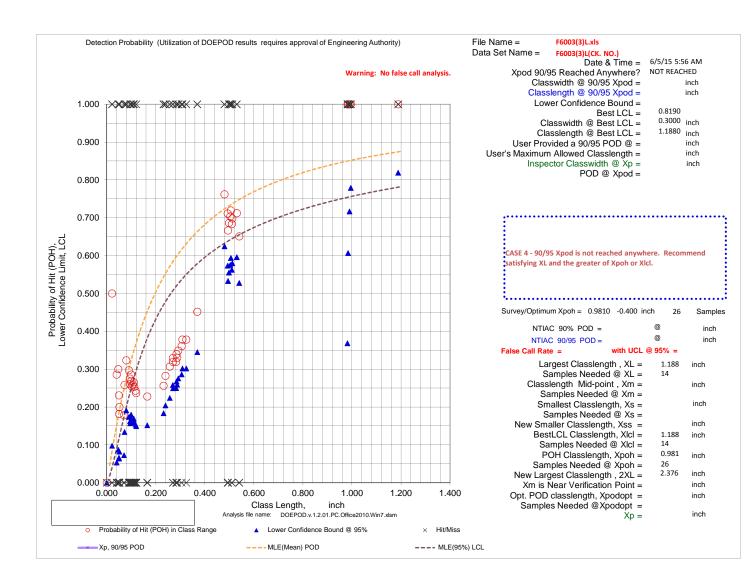


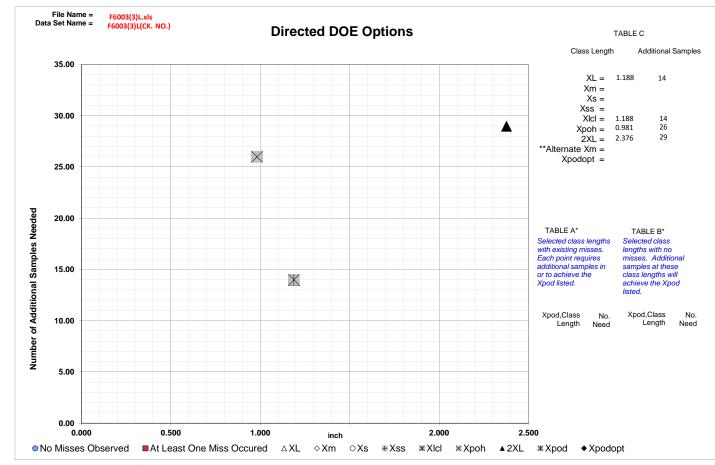
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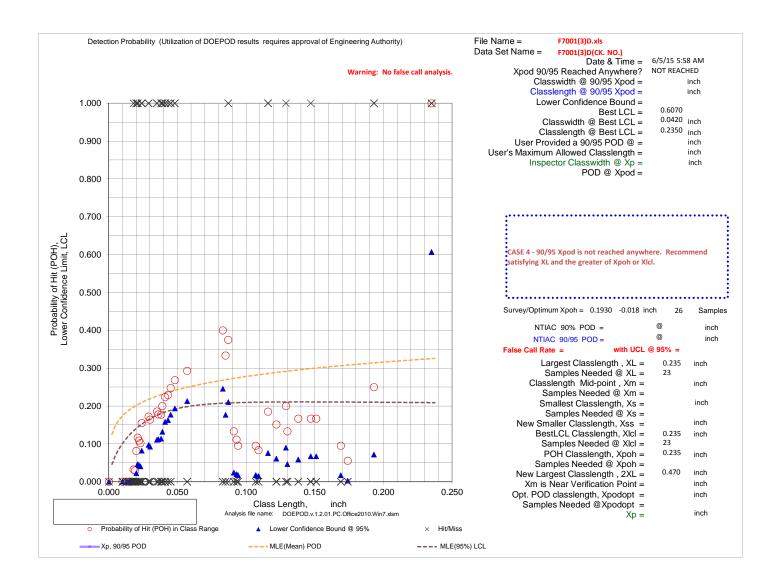


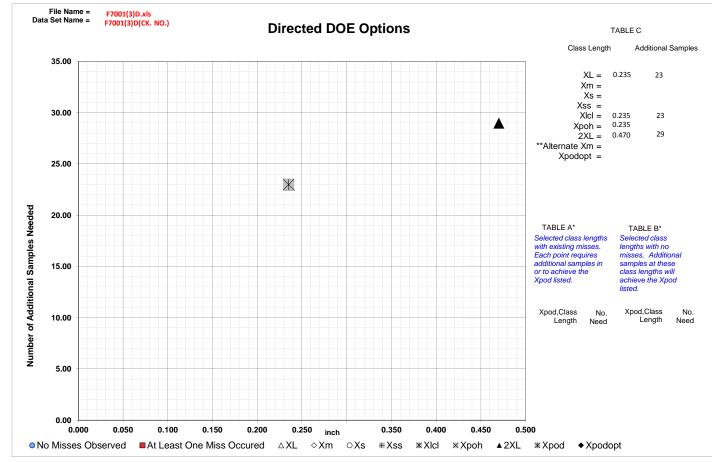
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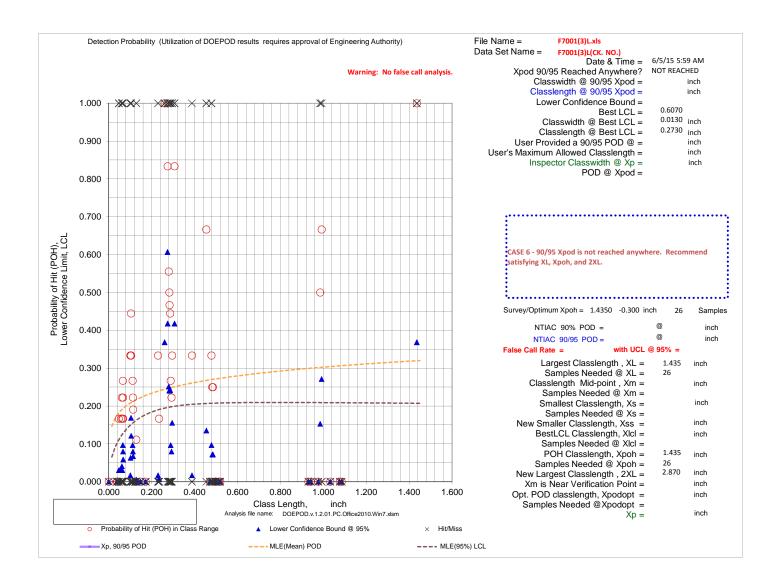


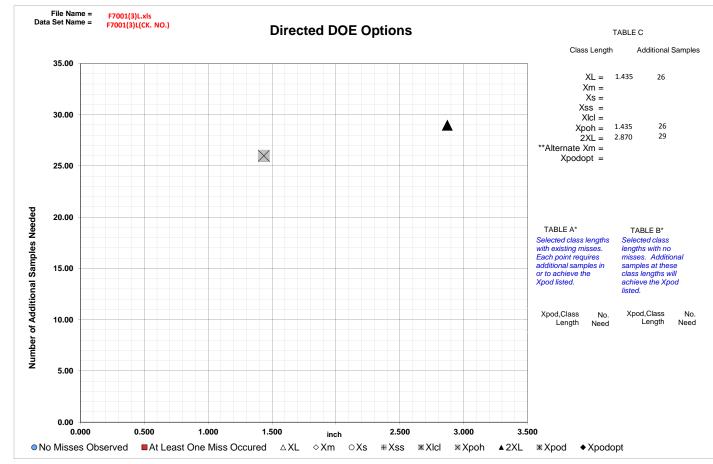
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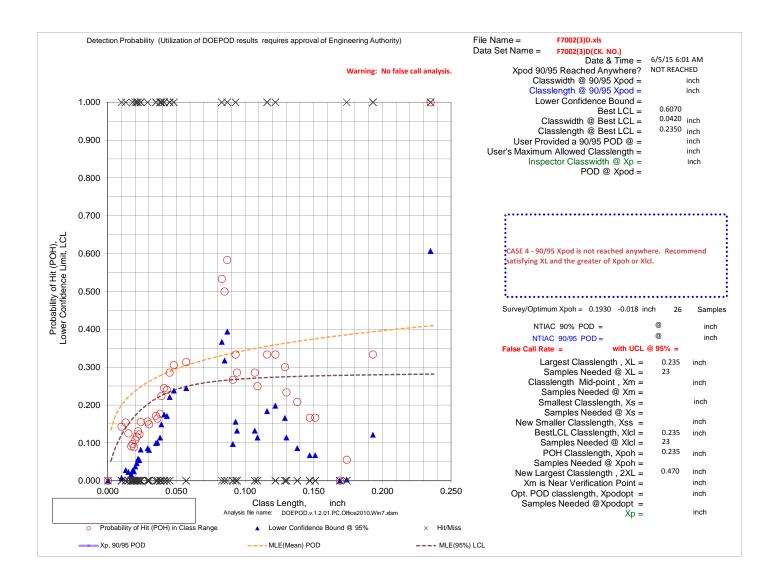


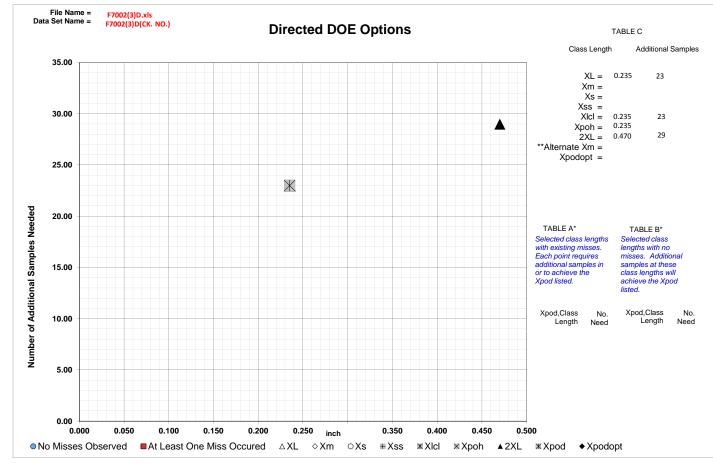
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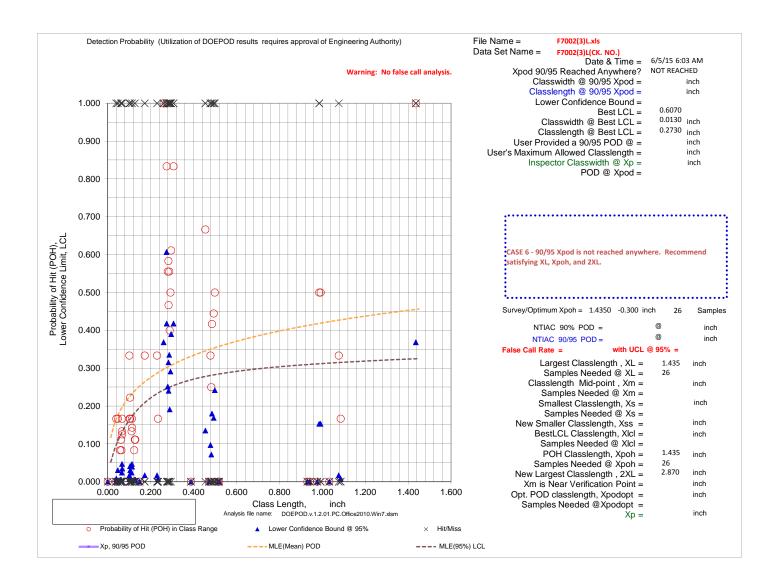


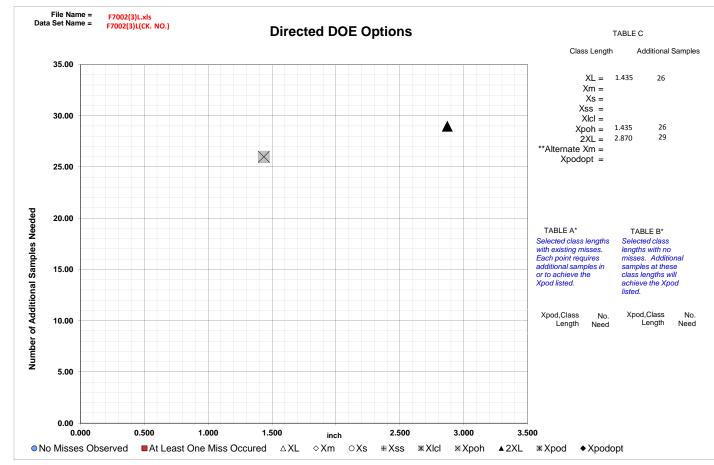
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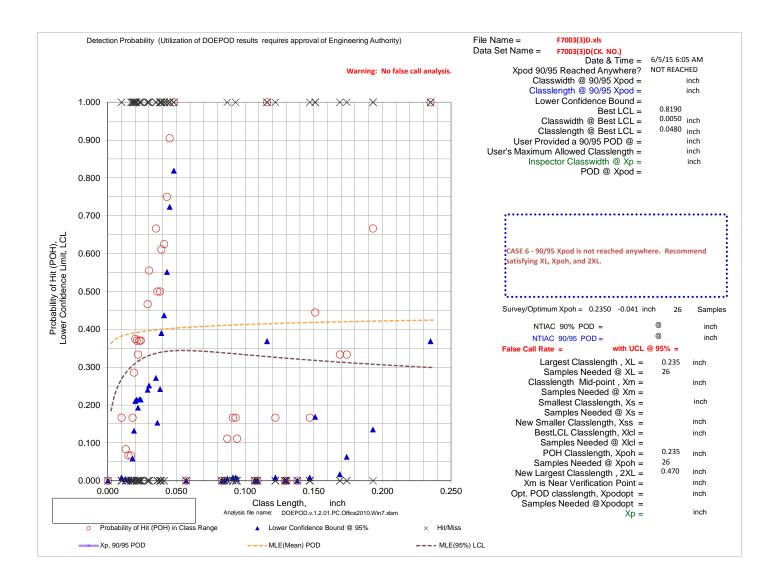


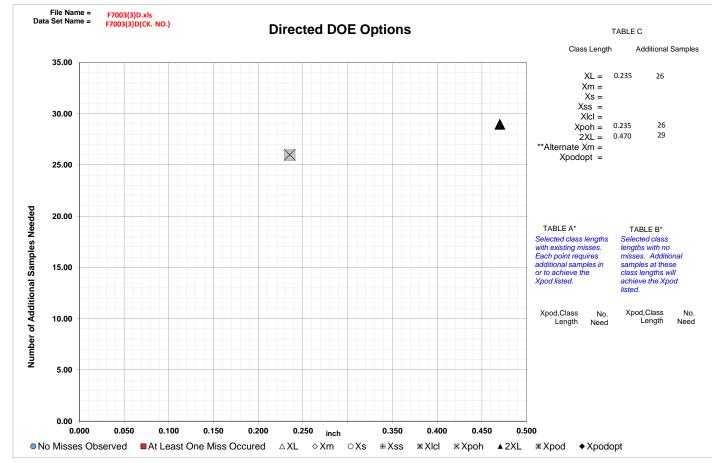
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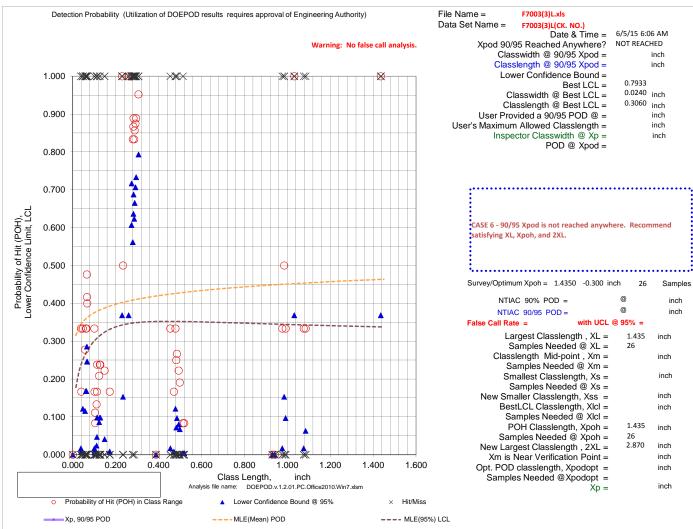


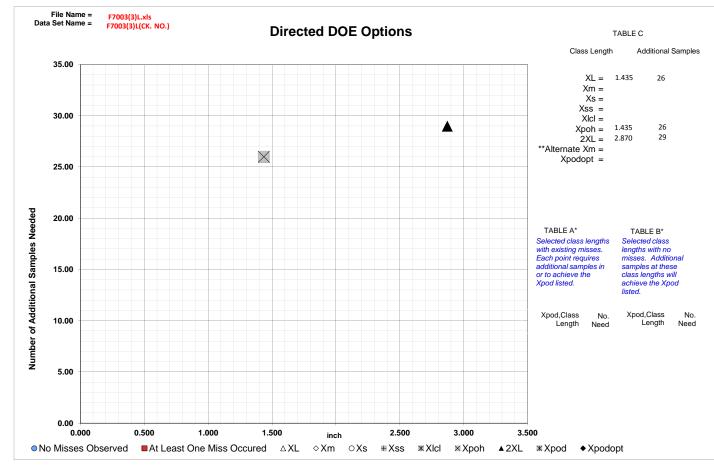
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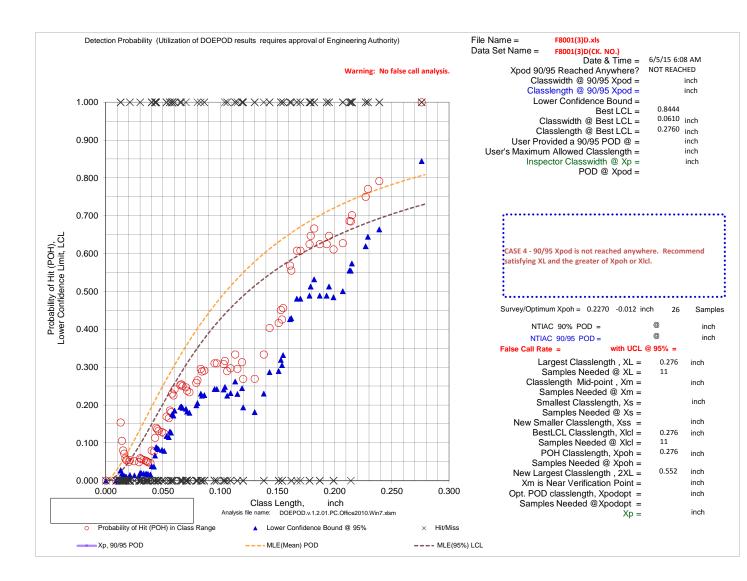


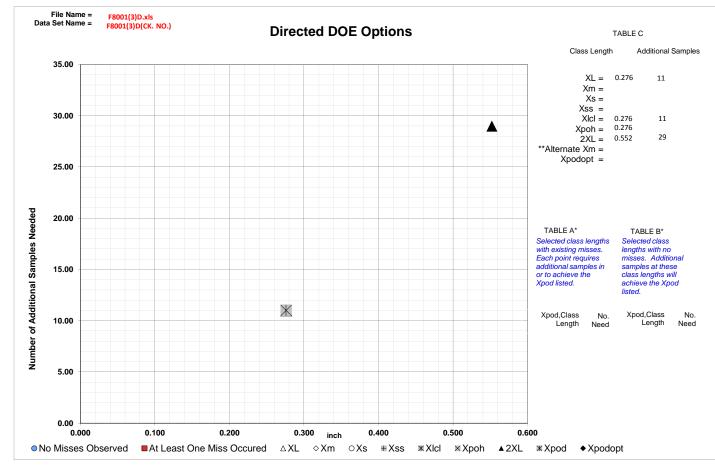
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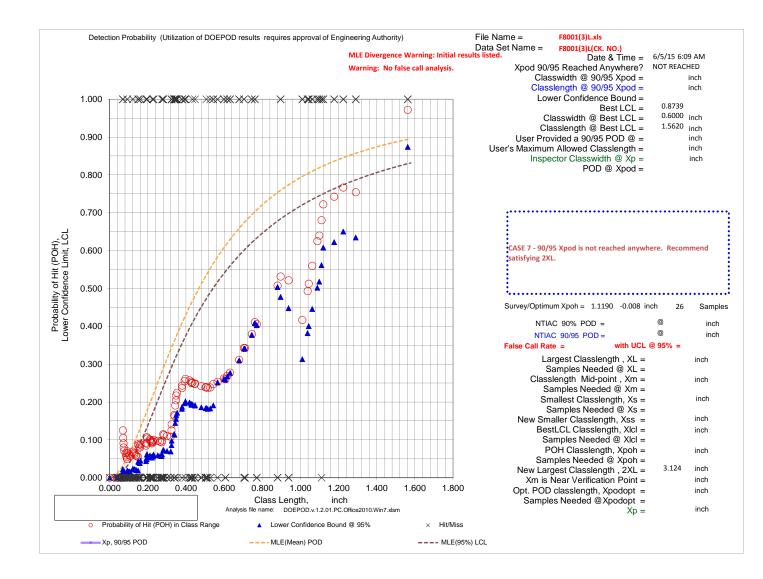


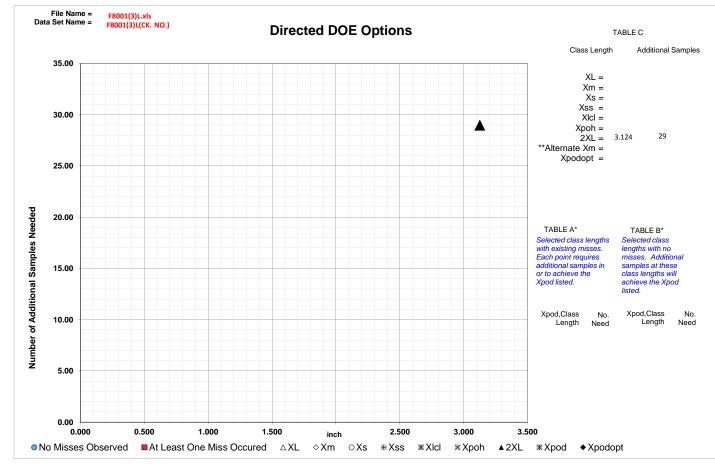
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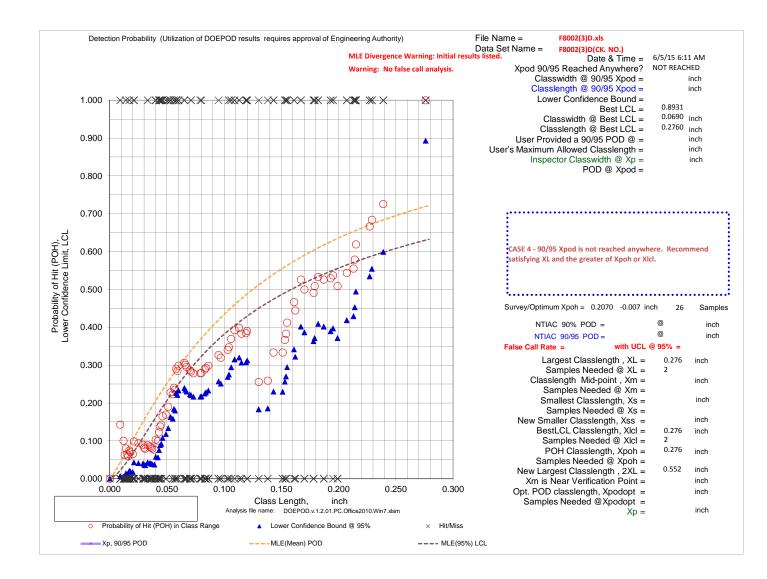


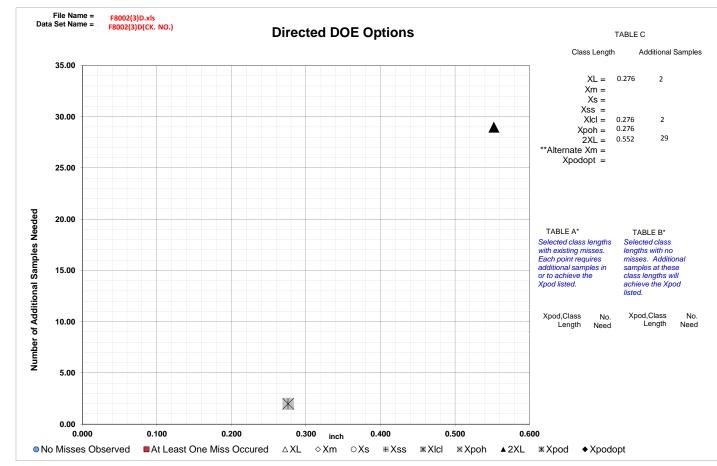
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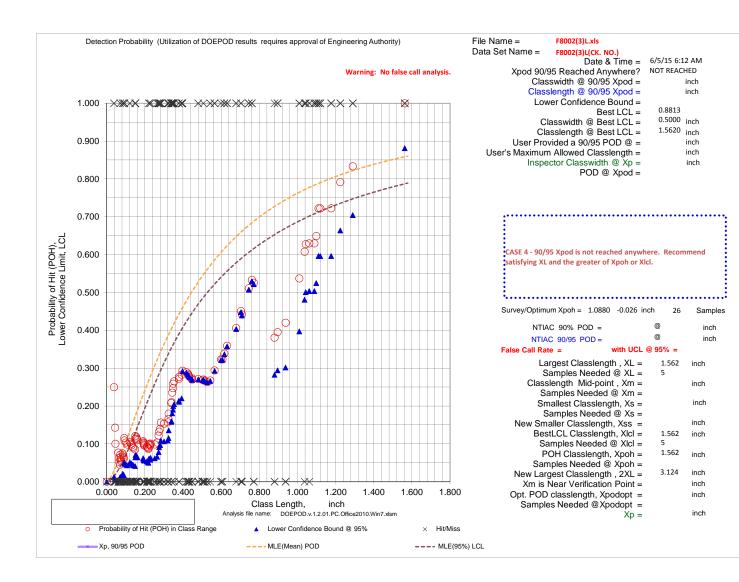


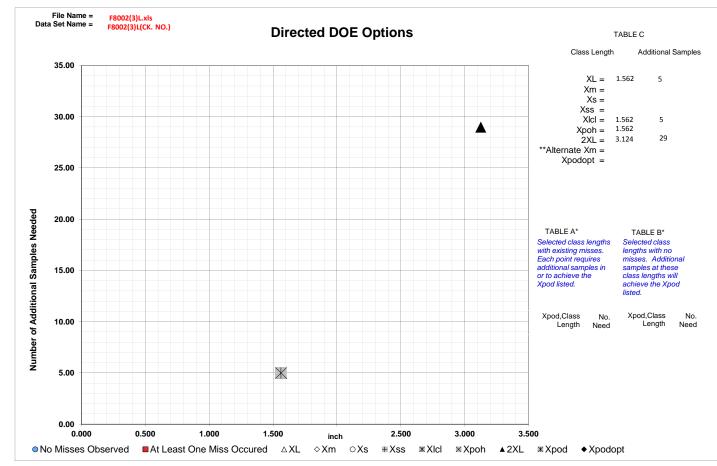
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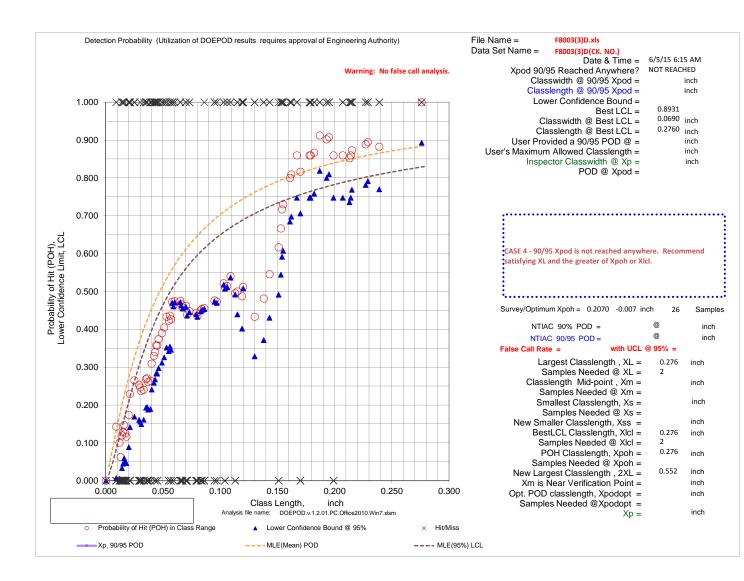


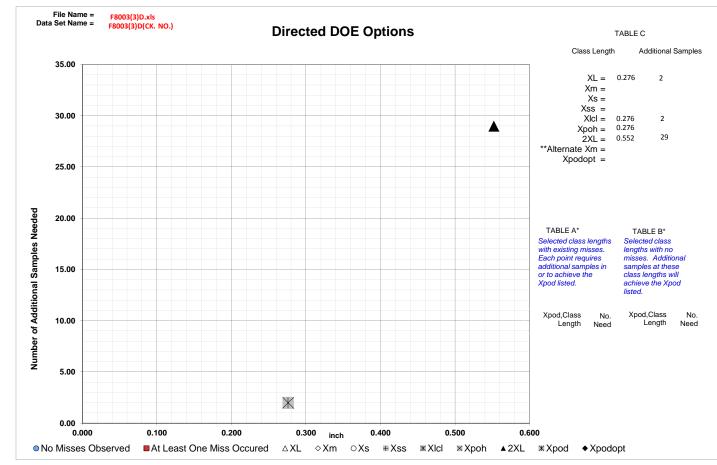
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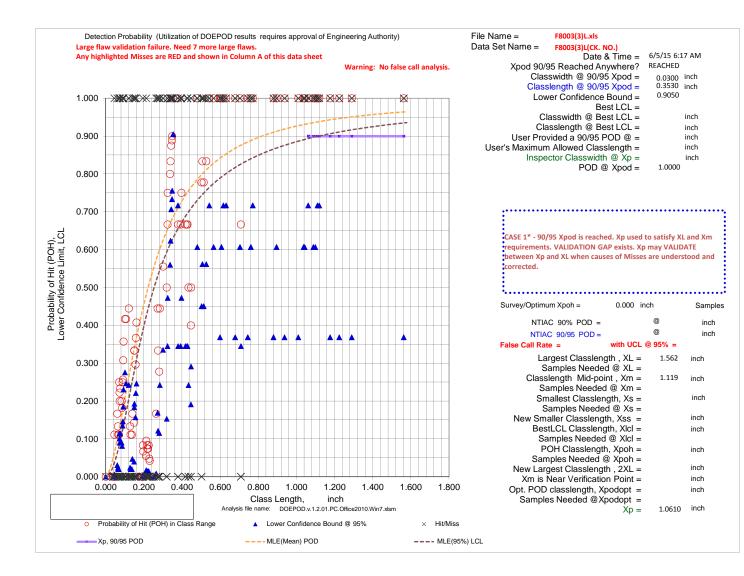


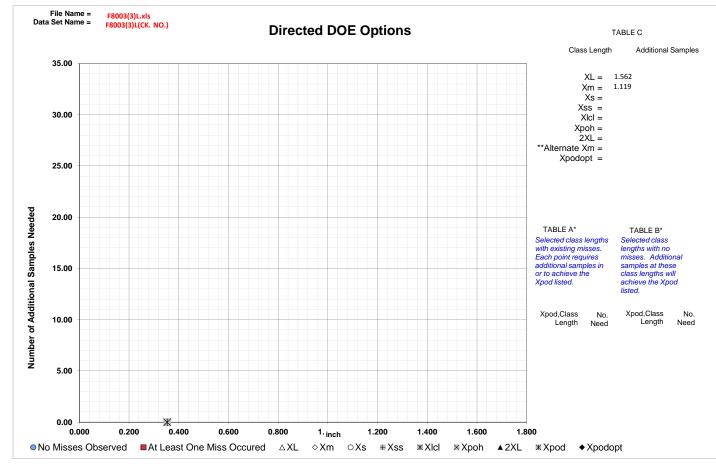
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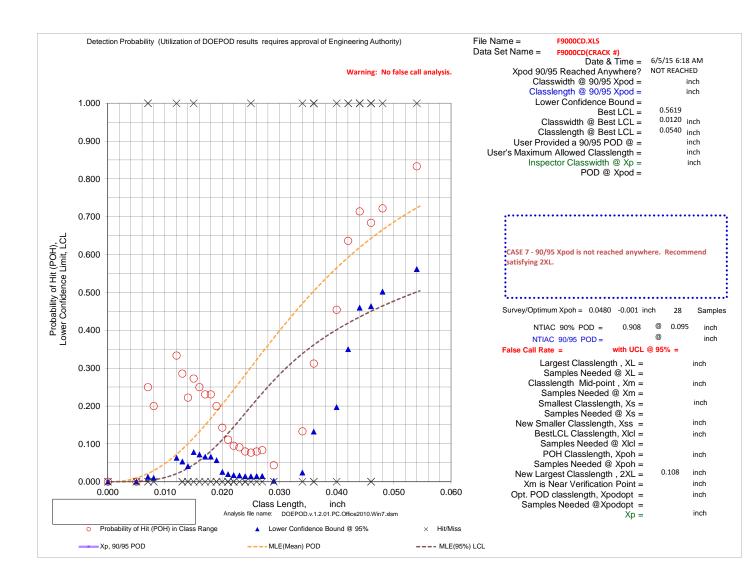


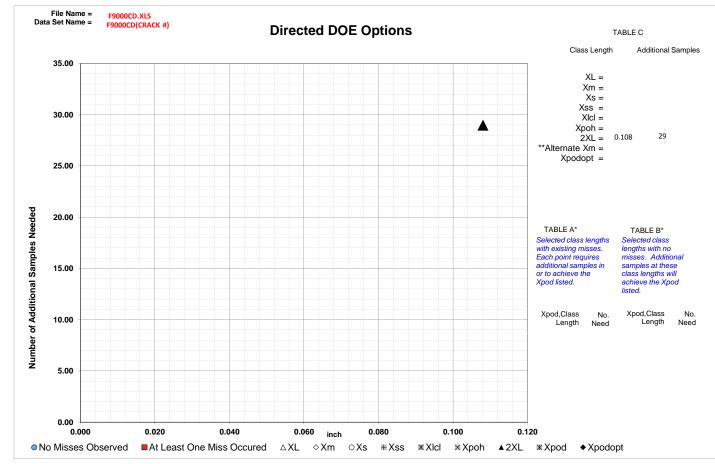
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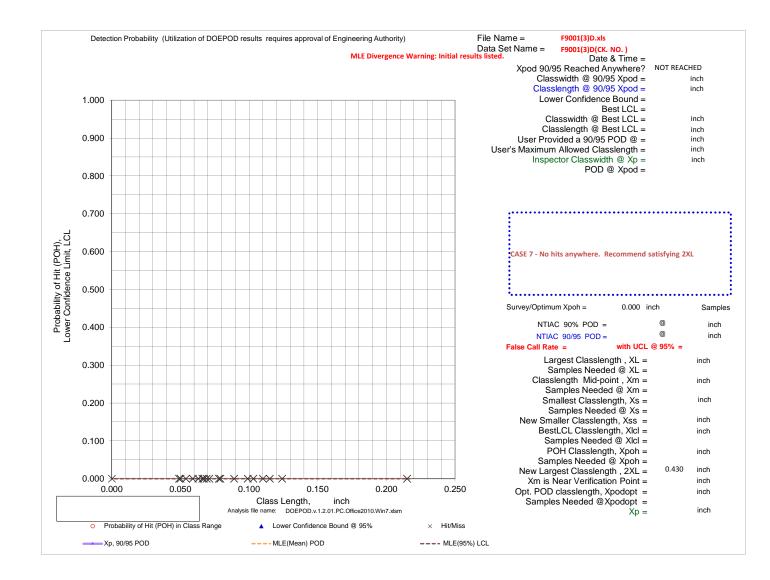


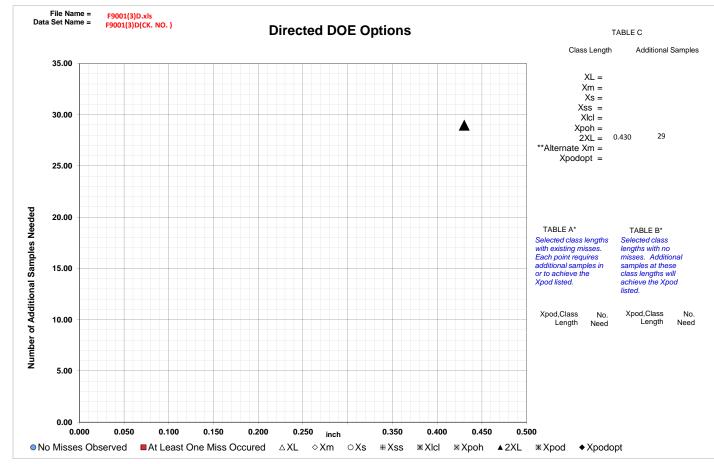
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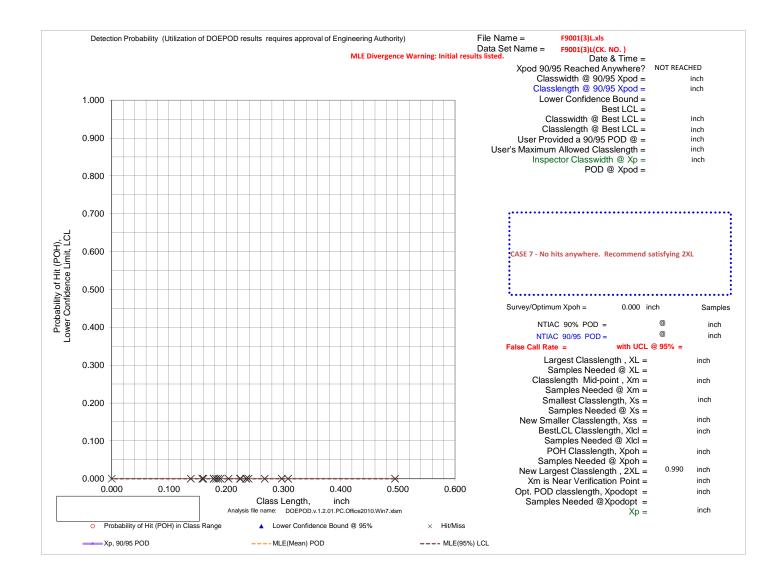


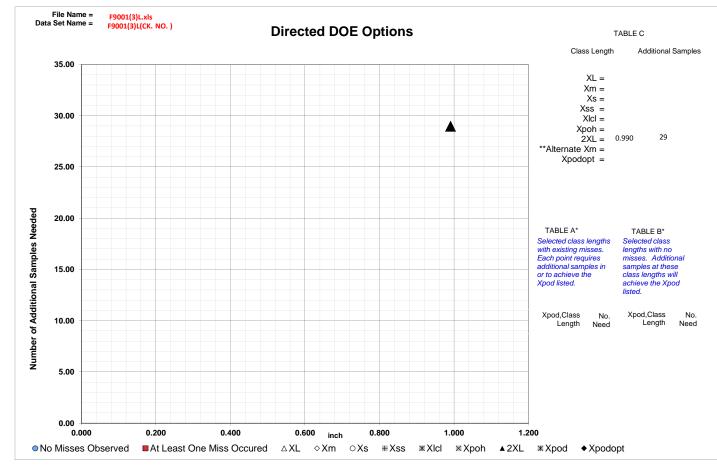
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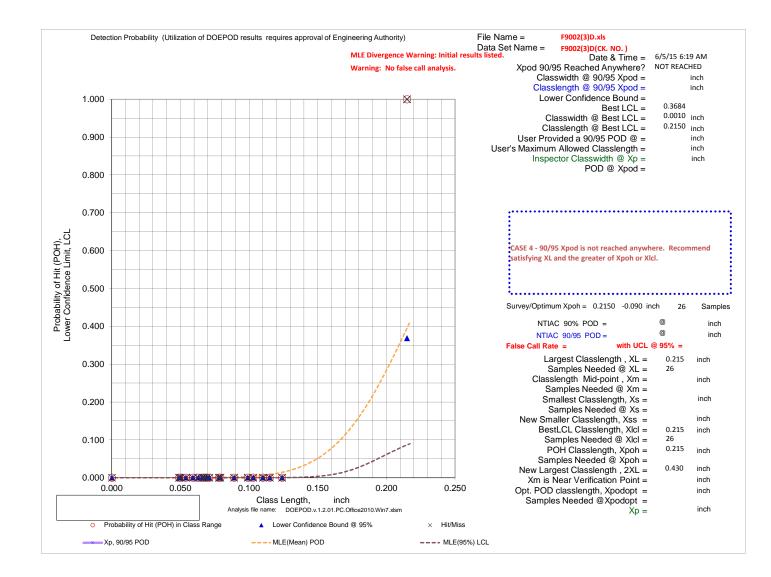


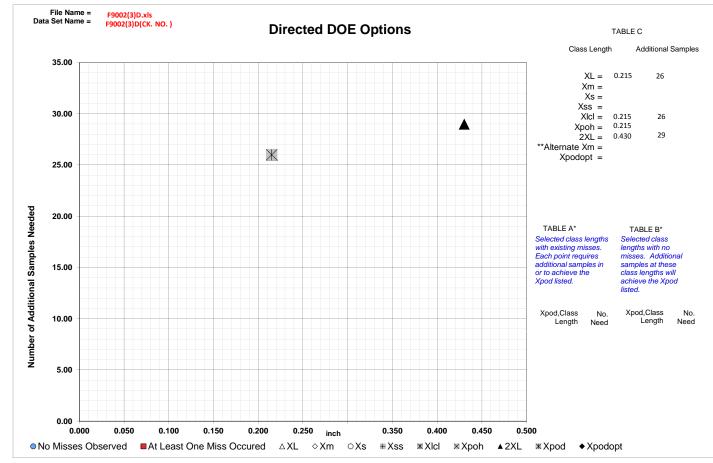
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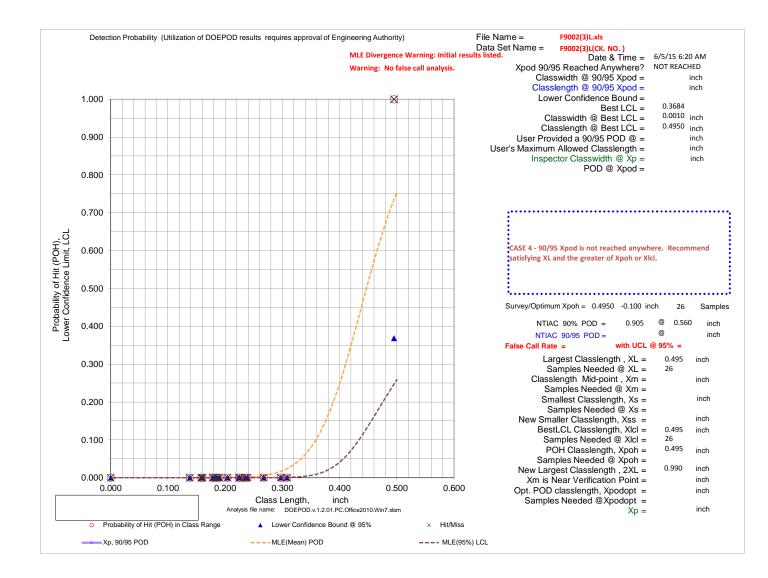


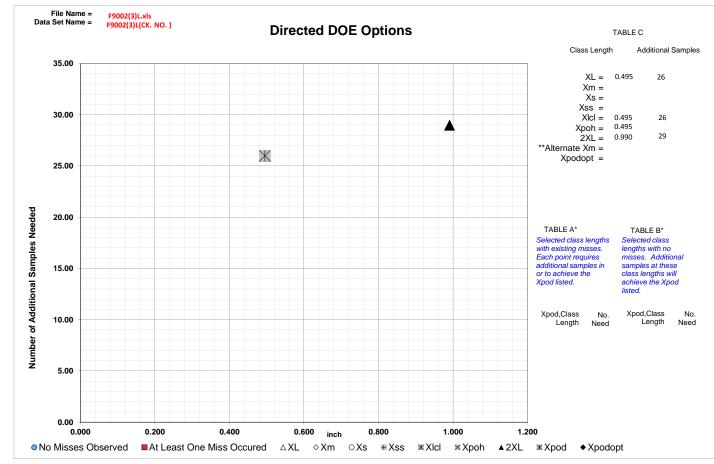
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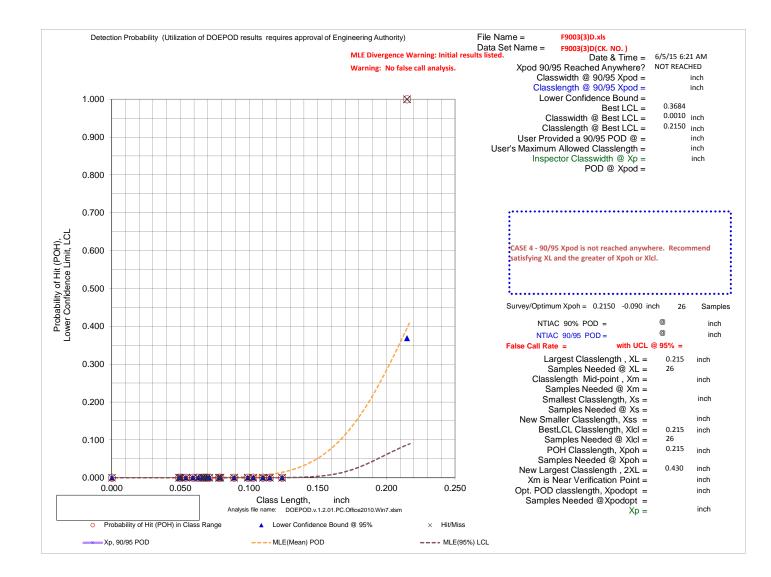


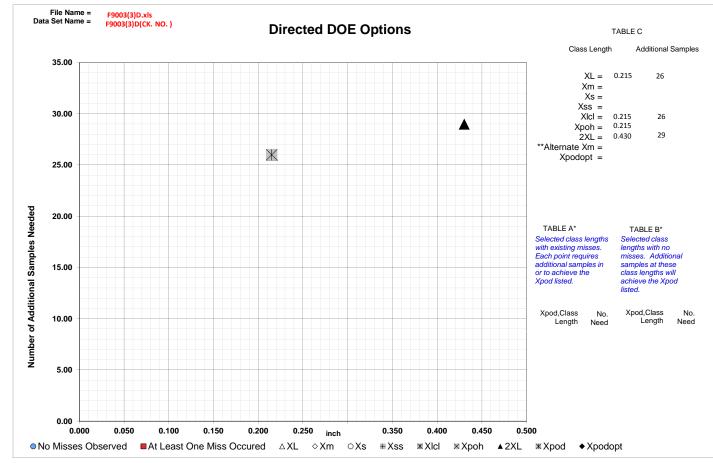
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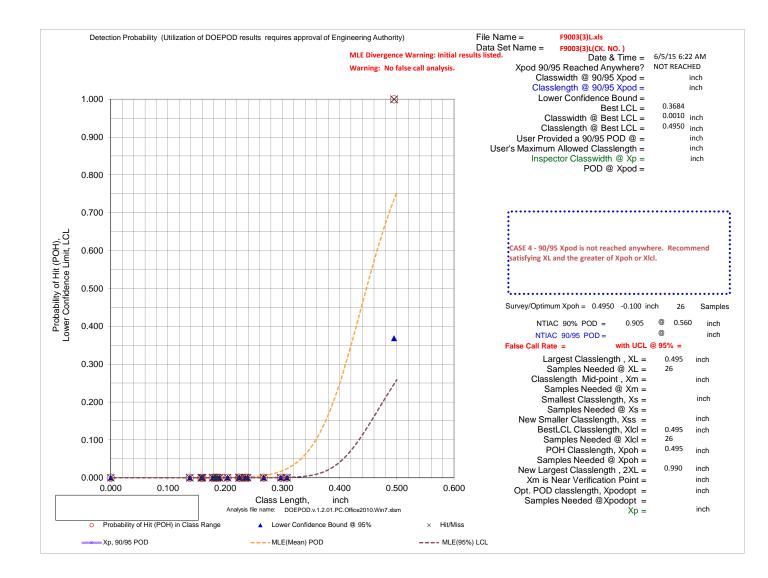


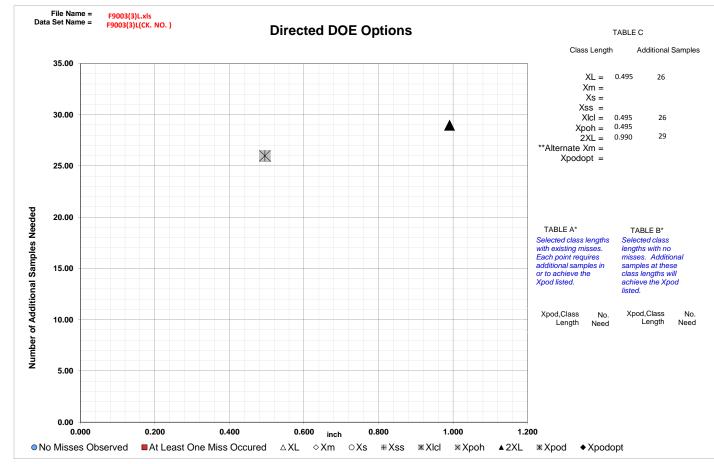
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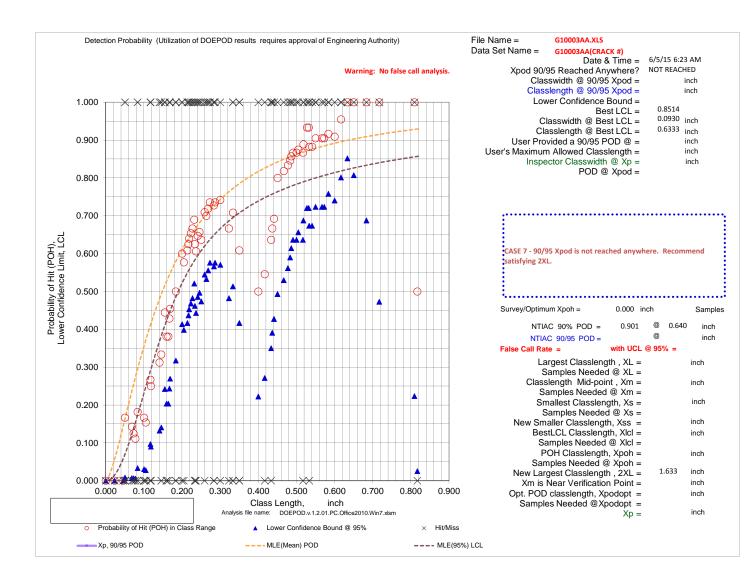


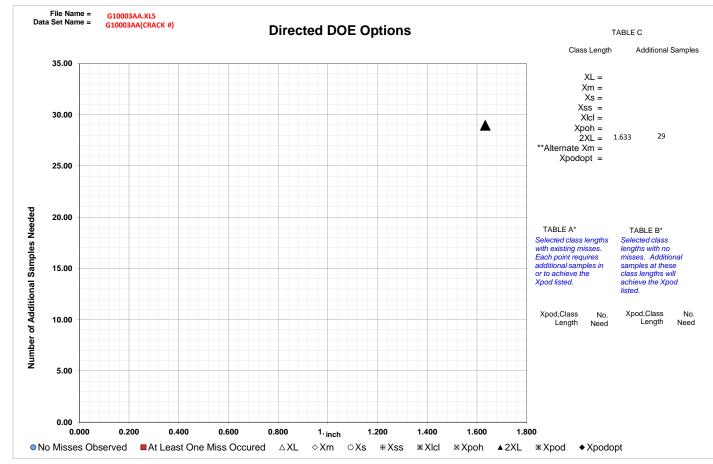
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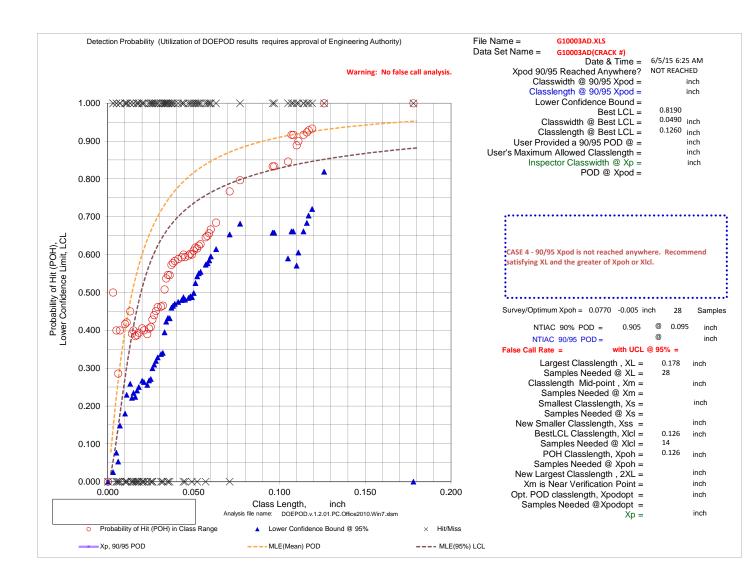


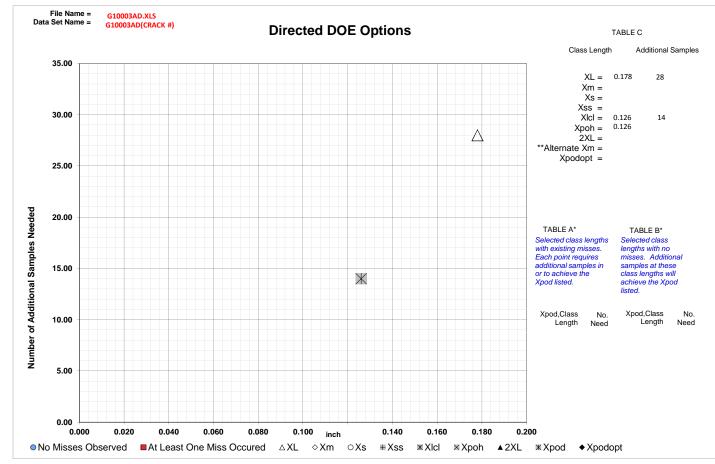
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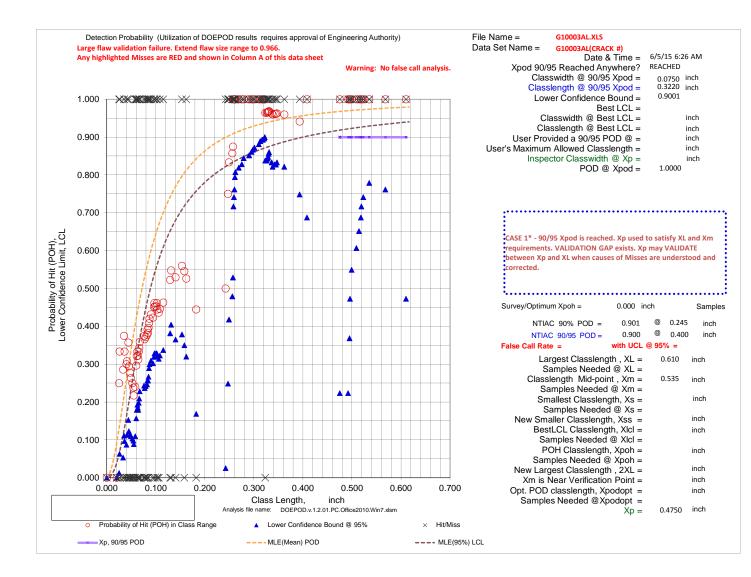


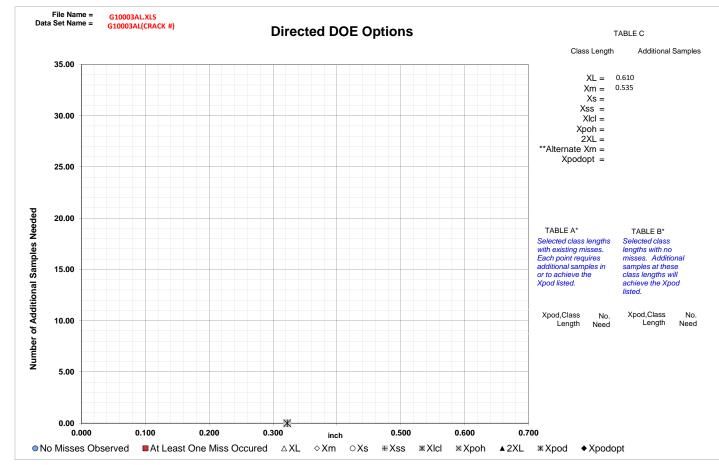
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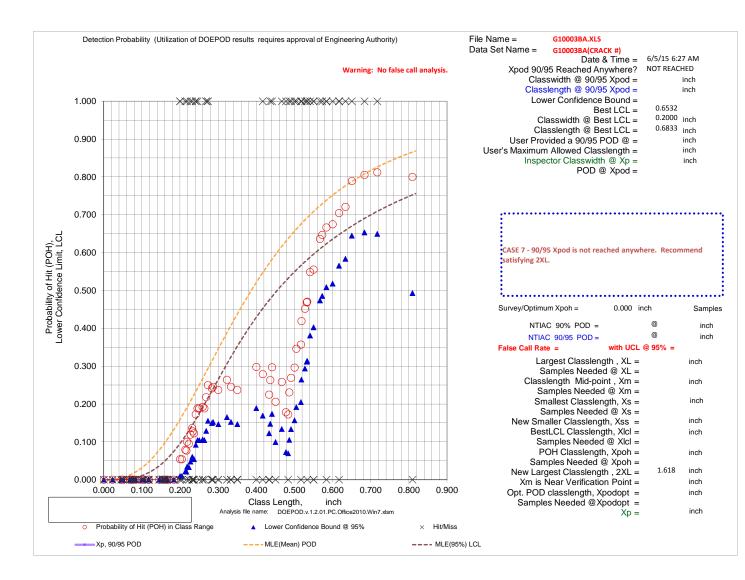


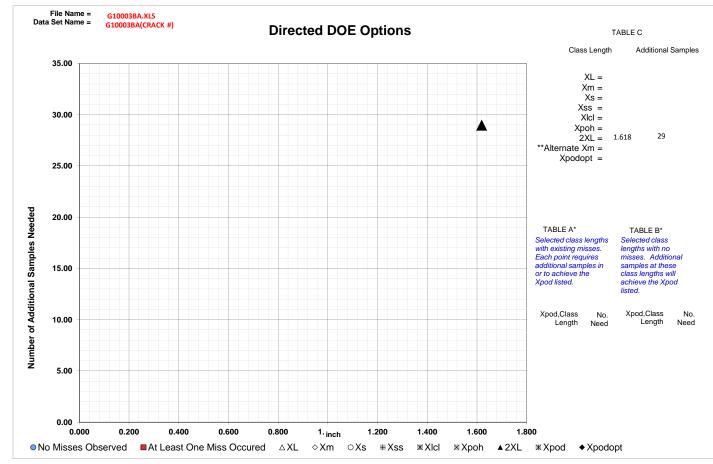
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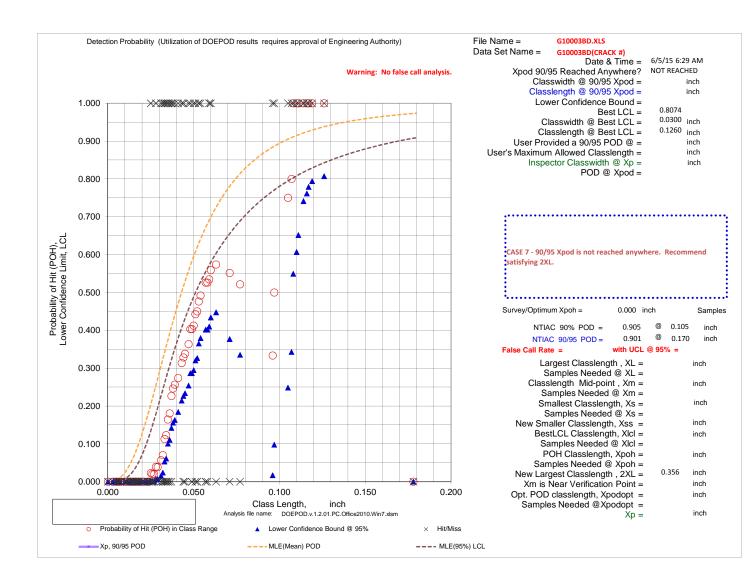


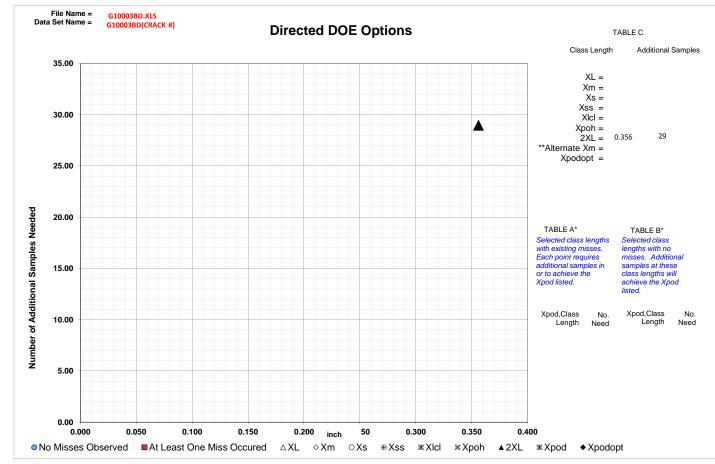
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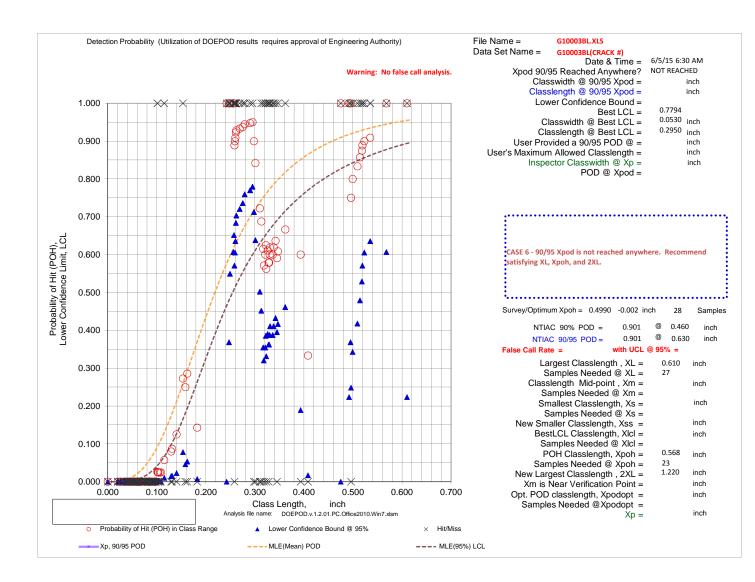


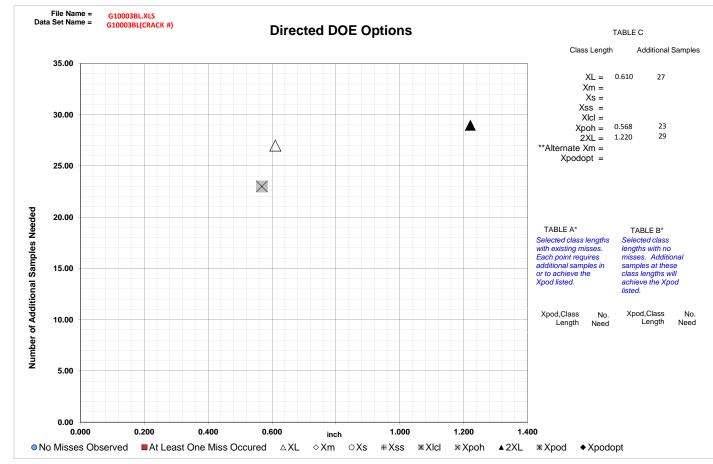
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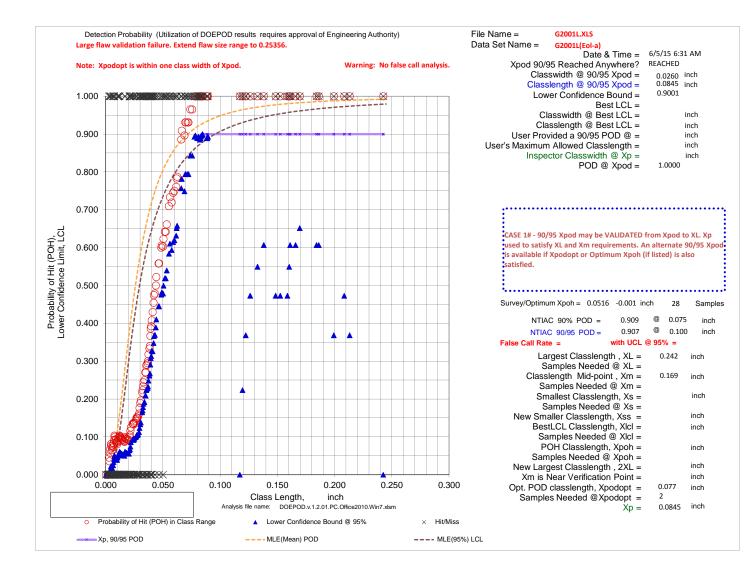


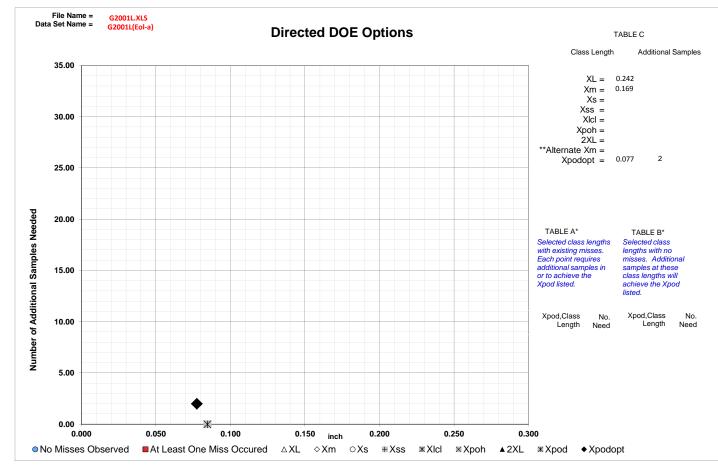
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Errata

NTIAC NDE Capabilities Book, 3rd Edition (November 1997) [NTIAC: DB-97-02]

DATA sets that do not appear to exist on the NTIAC CD:

B20011 (appears to be B2001) B20012 (appears to be B2002) B20013 (appears to be B2003)

G6001G (appears to be A6001G) G6001GR (appears to be A6001GR) G6002G (appears to be A6002G) G6003G (appears to be A6003G) G6004G (appears to be A6004G)

F40601AL (appears to be F40601A) F40601BL (appears to be F40601B) F40601CL (appears to be F40601C)

F40603AL (appears to be F40603A) F40603BL (appears to be F40603B) F40603CL (appears to be F40603C)

F42501AL (appears to be F42501A) F42501BL (appears to be F42501B) F42501CL (appears to be F42501C)

F42503AL (appears to be F42503A) F42503BL (appears to be F42503B) F42503CL (appears to be F42503C)

A4000(7) is listed in Mag Particle data index – should be B4000(7) with B4001L as the companion data set

DATA sets on the CD that are not listed in the index:

B1001AD (POD data not shown in book) B1001BD (POD data not shown in book) B1001CD (POD data not shown in book)

B1003AD (POD data not shown in book) B1003BD (POD data not shown in book) B1003CD (POD data not shown in book) B4001L (see above)

B2001 (appears to be the missing B20011 above) B2002 (appears to be the missing B20012 above) B2003 (appears to be the missing B20013 above)

There are an additional 18 data sets (grouped) and not listed in the index:

DB001(3)D (POD data not shown in book) DB001(3)L (POD data not shown in book) DB002(3)D (POD data not shown in book) DB002(3)L (POD data not shown in book) DB003(3)D (POD data not shown in book) DB003(3)L (POD data not shown in book)

DC001(3)D (POD data not shown in book) DC001(3)L (POD data not shown in book) DC002(3)D (POD data not shown in book) DC002(3)L (POD data not shown in book) DC003(3)D (POD data not shown in book) DC003(3)L (POD data not shown in book)

DD001(3)D (POD data not shown in book) DD001(3)L (POD data not shown in book) DD002(3)D (POD data not shown in book) DD002(3)L (POD data not shown in book) DD003(3)D (POD data not shown in book) DD003(3)L (POD data not shown in book)

DATA set duplicated:

F9000CD appears to be a duplicate identical to data file F20852CD

DATA Analysis integrity:

During validation of DOEPOD results on the entire NTIAC NDE Capabilities Book "DOEPOD(NTIAC)", some exceptions were noted in the results. There are 437 data sets and exceptions were identified in the 32 data sets listed below. The analysis results shown in the NTIAC NDE Capabilities Book, 3rd Edition (1997) [NTIAC: DB-97-02] for the data sets listed below are incorrect due to a data listing error. These data sets need to be re-run with data sorted.

A1001CL.XLS A1002CL.XLS

A9003(3)L.xls
AA003(3)L.xls
AC001(3)L.xls
CB003(3)L.xls
CE032(6)D.xls
F10601AD.XLS
F10601BD.XLS
F10601CD.XLS
F10602AD.XLS
F10602BD.XLS
F10602CD.XLS
F10603AD.XLS
F10603BD.XLS
F10603CD.XLS
F12201AD.XLS
F12201BD.XLS
F12201CD.XLS
F12202AD.XLS
F12202BD.XLS
F12202CD.XLS
F12203AD.XLS
F12203BD.XLS
F12203CD.XLS
F32251AD.XLS
F32251CD.XLS
F32253AD.XLS
F32253BD.XLS
F8002(3)L.xls
G10003BD.XLS
G10003BL.XLS

OTHER:

C8003(3)L.xls - sample #136 shows 3 trials with -1 in the HIT/MISS column C8003(3)D.xls - sample #136 shows 3 trials with -1 in the HIT/MISS column

C3002: Sample #16 shows 0.10" in depth. NASA CR 151098 pg 27. shows 0.010". Since the sample thickness is 0.063" this NTIAC entry is incorrect.

The primary and secondary scales on abscissa axes in Chart 1may be incorrect. Compare actual flaw sizes and inspection data on data sheets available in electronic distributions.

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13. SUPPLEMENTARY NOTES							
14. ABSTRACT							
This data book contains the Directed Design of Experiments for Validating Probability of Detection (POD) Capability of NDE Systems (DOEPOD) analyses of the nondestructive inspection data presented in the NTIAC, Nondestructive Evaluation (NDE) Capabilities Data Book, 3rd ed., NTIAC DB-97-02. DOEPOD is designed as a decision support system to validate inspection system, personnel, and protocol demonstrating 0.90 POD with 95% confidence at critical flaw sizes, a90/95. The test methodology used in DOEPOD is based on the field of statistical sequential analysis founded by Abraham Wald, "Sequential analysis is a method of statistical inference whose characteristic feature is that the number of observations required by the procedure is not determined in advance of the experiment. The decision to terminate the experiment depends, at each stage, on the results of the observations previously made. A merit of the sequential method, as applied to testing statistical hypotheses, is that test procedures can be constructed which require, on average, a substantially smaller number of observations than equally reliable test procedures based on a predetermined number of observations." A. Wald, 1947.							
15. SUBJECT TERMS							
Defects; Flaws; Maximum destructive likelihood; Nondestructive evaluation; Probability of detection							
	16. SECURITY CLASSIFICATION OF:			18. NUMBER OF		19a. NAME OF RESPONSIBLE PERSON	
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