

Computer Program for Design of Multistage Axial-Flow Compressors

Prepared for

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION

Contract NAS3-7277

N 67-31412
(ACCESSION NUMBER)
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(THRU)
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15
(PAGES)

(NASA OR TMX OR AD NUMBER)

Allison Division • General Motors

Indianapolis, Indiana

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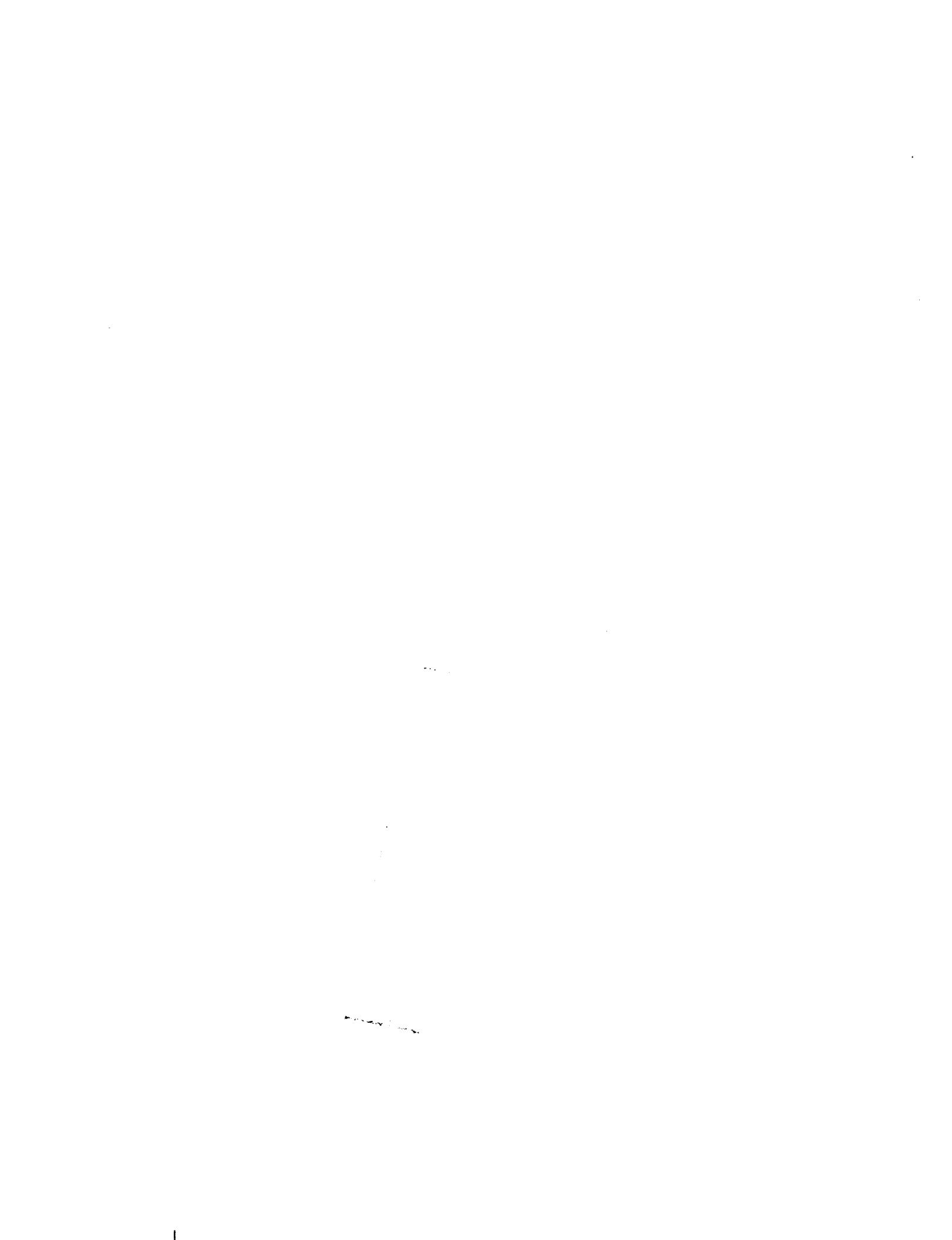
Contract NAS3-7277

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ABSTRACT

A compressor design program was developed based on simple-radial-equilibrium design philosophy with constant efficiency radially. The program was developed specifically for the determination of the flow path for a given overall pressure ratio or number of stages by specifying the tip axial velocity ratio across each blade row and initial blade row aspect ratio. Energy addition at the rotor tip is specified through rotor tip diffusion factor. The variation of energy addition radially is arbitrary. The rotor tip diffusion factor is reduced if limit values are exceeded on stator hub Mach number, stator hub diffusion factor, and rotor relative exit hub flow angle. Blade row aspect ratio is reduced if limit values are exceeded on hub and tip ramp angles.

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SUMMARY

This technical report contains the development of the compressor design program based on simple-radial-equilibrium design philosophy with constant efficiency radially. A detailed description is given of this compressor design program and its capabilities.

The program logic is developed in detail in the System of Equations (Appendix A) and in the Flow Charts (Appendix C). Sections indicated in Appendices A and C are cross referenced through Roman numerals. The FORTRAN listing of the computer program is given in Appendix B which is also cross referenced with the Flow Charts through statement numbers.

The input format is described in Appendix D. There are two types of input format available for the user. One option is a "Standard" format and the other option is a "Namelist" format which permits minimum amount of data for either one or more compressor problems. It should be noted that the reading of input data is generally the major portion of the machine time for a single compressor problem.

Two sample problems, which show the output format, are given in Appendix E. The first sample problem is a free vortex case and the second problem is a nonfree vortex case in the first stage. Two input data listings are also shown in Appendix E. The listing on page E-1 is for the two sample problems and is in the Namelist format. The listing on page E-2 is the Standard format for the free vortex sample problem.

INTRODUCTION

The work reported herein was performed under contract NAS3-7277 for the NASA-Lewis Research Center to devise a compressor design computer program for making a parametric compressor study on advanced multistage axial-flow compressors. The purpose of this study is to examine a wide range of design parameters to determine their effects and indicate significant areas for study and research to increase average stage pressure ratio and reduce compressor length.

To obtain the effects of the design parameters on average stage pressure ratio and compressor length, it was necessary to devise a compressor design program to compute the flow path for arbitrary specified conditions. Since the effects of streamlining curvature or radial velocity are not well defined for state-of-the-art compressor design technology, the simple-radial-equilibrium design philosophy was selected. Constant efficiency radially was also selected as the type of blading required for the high loadings to be investigated and their element losses are not known.

Additional requirements of this design program to accomplish the objective are:

1. Energy addition is to be determined through rotor tip diffusion factor and is to be reduced from an initial value if stator hub diffusion factor, stator hub Mach number, or rotor relative hub exit flow angle exceed specified limits.
2. Blade row axial length is to be determined through blade aspect ratio which will be increased by reducing aspect ratio when hub and tip ramp angle have attained their specified limit values before continuity has been satisfied.
3. The flow path will be computed until either a specified overall pressure ratio or maximum number of stages has been exceeded.

This compressor design program can be used for obtaining compressor results over a range of design parameters within the scope of design philosophy selected.

SYMBOLS

Note: The primary symbols are illustrated schematically in Figure 1.

a	sonic velocity, ft/sec
A	annulus area, in. ²
AR	aspect ratio
b	blade row axial length, in.
B, C, D, E	constants in tangential velocity equation
c _p	constant pressure specific heat, BTU/lb _m -°R
D	diffusion factor
F	blade force, lb _f /lb _m
g _c	gravitational constant, ft-lb _m /lb _f -sec ²
H	enthalpy, BTU/lb _m
J	mechanical equivalent of heat, ft-lb _f /BTU
L	compressor length, in.
M	Mach number
M	molecular weight, lb _m /mole
n	stage number
N	number of stages
P	pressure, lb _f /in. ²
Q	heat transfer rate, BTU/lb _m -sec
R	radius, in.
R _C	total pressure ratio

R, θ, z	cylindrical coordinates
R	universal gas constant, 1545.4 ft-lbf/mole-°R
R_m	gas constant, ft-lbf/lbm-°R
S	entropy, BTU/lbm-°R
T	temperature, °R
T_R	total temperature ratio
t	time, sec
U	wheel speed, ft/sec
V	gas velocity, ft/sec
\dot{w}	flow rate, lb _m /sec
Z	loss parameter

Greek

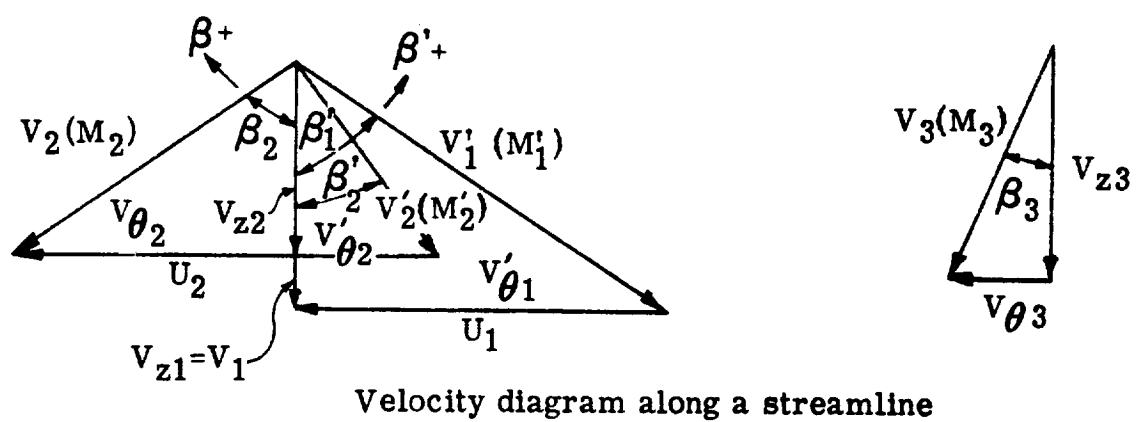
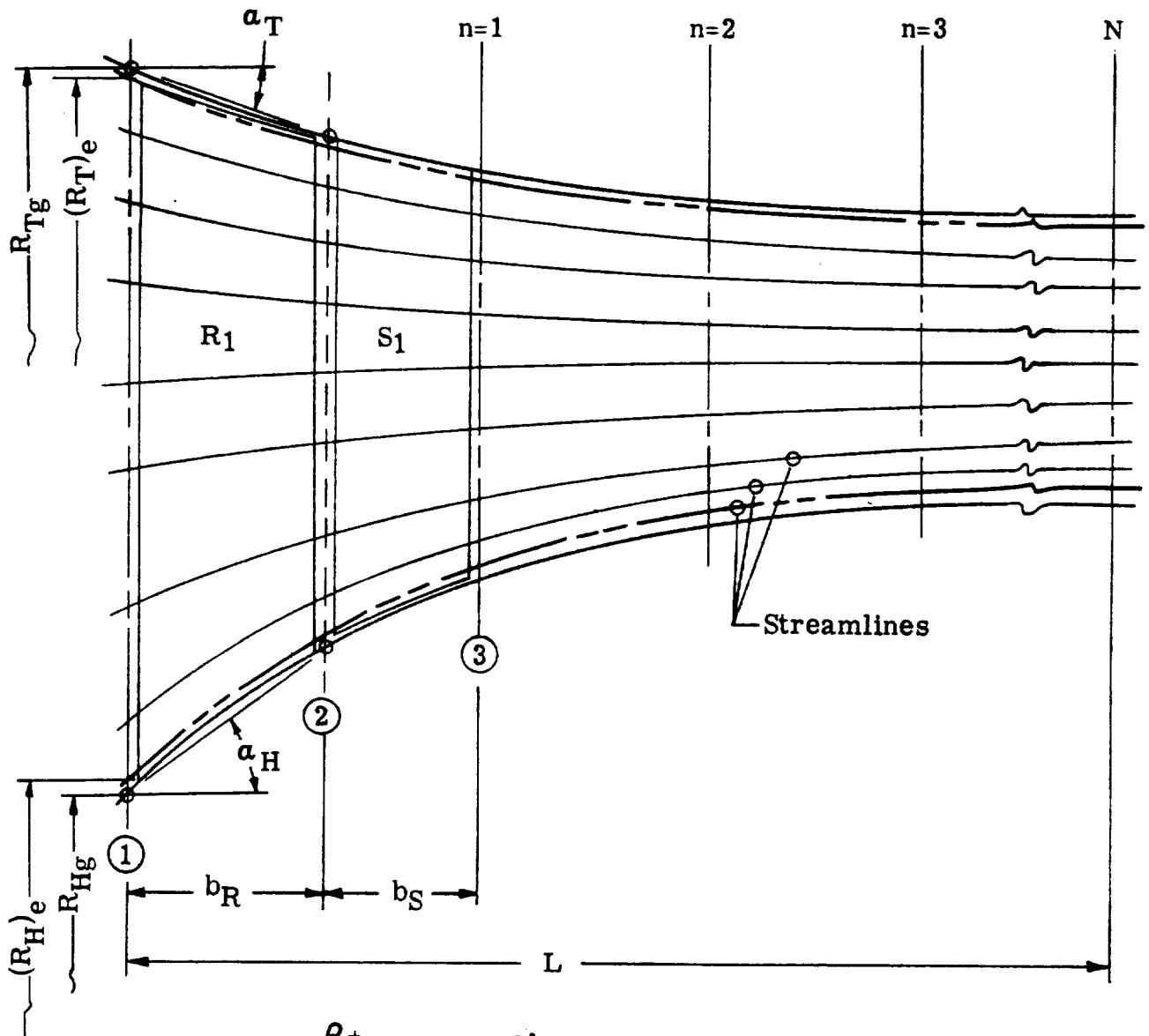
α	ramp angle, degrees
β	flow angle, degrees
γ	ratio of specific heats
ϵ	weight flow convergence tolerance
δ^*	blockage factor
η_{ad}	adiabatic efficiency
η_P	polytropic efficiency
ω	angular velocity, rad/sec
$\bar{\omega}$	loss coefficient
ρ	gas density, lb _m /ft ³
σ	solidity (chord/spacing)

Subscripts

e	effective
f	fractional
g	geometric
H	hub
i	initial
id	ideal
L	limit
m	streamline number
n	stage number
N	number of streamlines and number of stages
ov	overall and cumulative
R	rotor, radial direction, or ratio
S	stator and stage
t	total
T	tip
z	axial direction
1	rotor inlet
2	stator inlet
3	stator outlet
θ	tangential direction

Superscript

' relative value



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Figure 1. Schematic presentation of symbols.

AXIAL-FLOW COMPRESSOR DESIGN PROGRAM

PROGRAM DESCRIPTION

The basic equations of motion which govern the three-dimensional flow of an inviscid compressible gas through a turbomachine have been derived in many reports such as Reference 1.

The pertinent equations for steady axisymmetric flow in cylindrical coordinates are:

Continuity Equation

$$\frac{1}{R} \frac{\partial(PRV_R)}{\partial R} + \frac{1}{R} \frac{\partial(PV_\theta)}{\partial \theta} + \frac{\partial(PV_z)}{\partial z} = 0 \quad (1)$$

Radial Equation of Motion

$$g_c J \frac{\partial H_t}{\partial R} = g_c F_R + g_c J T \frac{\partial S}{\partial R} + \frac{V_\theta}{R} \frac{\partial(RV_\theta)}{\partial R} \\ + V_z \left(\frac{\partial V_z}{\partial R} - \frac{\partial V_R}{\partial z} \right) \quad (2)$$

Circumferential Equation of Motion

$$0 = g_c F_\theta - \frac{1}{R} \left[V_R \frac{\partial(RV_\theta)}{\partial R} + V_z \frac{\partial(RV_\theta)}{\partial z} \right] \quad (3)$$

Axial Equation of Motion

$$g_c J \frac{\partial H_t}{\partial z} = g_c F_z + g_c J T \frac{\partial S}{\partial z} + \frac{V_\theta}{R} \frac{\partial(RV_\theta)}{\partial z} \\ - V_R \left[\frac{\partial V_z}{\partial R} - \frac{\partial V_R}{\partial z} \right] \quad (4)$$

Energy Equation

$$\frac{DH_t}{Dt} = Q + \frac{\omega}{g_c J} \frac{D(RV_\theta)}{Dt} \quad (5)$$

Gradient of Entropy

$$\frac{DS}{Dt} = \frac{Q}{T} \quad (6)$$

Condition of Integrability

$$\frac{\partial}{\partial R} \left(\frac{F_z}{RF_\theta} \right) = \frac{\partial}{\partial z} \left(\frac{F_R}{RF_\theta} \right) \quad (7)$$

Equations (1) through (7) relate eight unknowns in F_R , F_θ , F_z , V_R , V_θ , V_z , S , and H_t .

The compressor design analysis considered for this study is referred to as the simple-radial-equilibrium solution without entropy gradient. The simplifying assumptions to be made are.

1. Only stations between blade rows are considered; therefore, F_R , F_θ and F_z are zero.
2. Heat transfer is zero; therefore, Q is zero.
3. Consideration need be given only to the radial equation of motion.
4. $\partial S / \partial R = 0$
5. $\partial V_R / \partial z = 0$; therefore, streamline curvature is ignored.

With these assumptions, Equations (3), (4), (6), and (7) are eliminated. Equation (1) is then rewritten for convenience as

$$\dot{w} = 2\pi \int_{R_H}^{R_T} \rho V_z R dR \quad (8)$$

and Equations (2) and (5) become

$$g_c J \frac{\partial H_t}{\partial R} = \frac{V_\theta}{R} \frac{\partial (RV_\theta)}{\partial R} + V_z \frac{\partial V_z}{\partial R} \quad (9)$$

$$g_c J \Delta H_t = \omega \Delta (RV_\theta) \quad (10)$$

The usual method in the solution of this set of equations is to specify an efficiency or total pressure loss, flow path geometry, and energy addition through total enthalpy change or exit tangential velocity. With the blade row inlet conditions known, the exit velocity conditions are then determined iteratively through Equations (8) and (9).

The primary objective of this compressor design program, however, is to determine the flow path of the compressor for a given overall pressure ratio. The secondary objective is that resultant aerodynamic parameters (defined as stator hub Mach number, rotor relative hub exit flow angle, and stator hub diffusion factor) must be less than or equal to a specified value and that blade aspect ratio is equal to or less than an initial value as required by specified limit values of hub and tip ramp angle.

To accomplish this objective, it is required that energy addition be determined through rotor tip diffusion factor, axial velocity ratio at the tip, and a specified form for tangential velocity distribution. Once the energy addition has been determined, the blade row exit annulus area is determined. With appropriate hierarchy established on the limit ramp angle, the exit annulus area can be located radially and the aerodynamic parameter values calculated. If the aerodynamic parameter limits are exceeded, the rotor tip diffusion factor must be reduced to lower the aerodynamic parameter values.

The detailed procedure to accomplish the aforementioned objectives and the development of the program logic to computerize this compressor design analysis are discussed in the following subsection. A detailed summary of the step-by-step calculation is given in Appendix A.

DEVELOPMENT OF PROGRAM LOGIC

Rotor tip diffusion factor and tip axial velocity ratio are two parameters exerting a controlling influence on stage configuration. For the case of a rotor of defined tip solidity having inlet and outlet radii, these two parameters define stage energy addition. Under these restricted conditions, the equation for diffusion factor at the rotor tip may be resolved to give outlet absolute tangential velocity and from this energy addition is obtained.

The method of rewriting the equation for diffusion factor in the form of a quadratic in V_{θ} is developed in Appendix A.

$$V_{\theta T2} = \frac{1}{2 \left(1 - \frac{1}{4 \sigma^2 RT} \right)} \left\{ 2 \left(U_{T2} + \frac{q}{2 \sigma RT} \right) - \left[4 \left(U_{T2} + \frac{q}{2 \sigma RT} \right)^2 \left(\frac{1}{1 - \frac{1}{4 \sigma^2 RT}} \right) - 4 \left(V_{z2}^2 + U_{T2}^2 - q^2 \right) \right]^{1/2} \right\} \quad (11)$$

where

$$q = (1 - D_{RT}) V'_{T1} + \frac{1}{2 \sigma RT} (U_{T1} - V_{\theta T1} - U_{T2}) \quad (12)$$

As always, in the case of a quadratic, certain restrictions in the selection of roots must be recognized. These restrictions are emphasized at appropriate places in this report.

The absolute tangential velocity at the rotor exit is defined by the non-linear functional relationship:

$$V_{\theta 2} = \frac{B}{R_2} + C + DR_2 + ER_2^2 \quad (13)$$

where B, C, D, and E are constant coefficients. To use this expression for the radial evaluation of tangential velocity, some arbitrary method of determining the coefficients must be adopted since only one boundary condition (i.e., at the tip) is known. It was decided to set values for the usually less prominent coefficients C, D, and E and compute a value for B. This decision was influenced by the fact that assigning a value of zero to C, D, and E results in a "free-vortex" type velocity distribution.

The radial profile of axial velocity may be obtained by substituting Equation (13) into Equation (9) and integrating the resulting function with respect to R.

Rewriting Equation (9) as

$$V_z \frac{\partial V_z}{\partial R} = g_c J \frac{\partial H_t}{\partial R} - \frac{V_\theta}{R} \frac{\partial (RV_\theta)}{\partial R}$$

or

$$\frac{\partial V_z^2}{\partial R} = 2 g_c J c_p \frac{\partial T_t}{\partial R} - \frac{\partial V_\theta^2}{\partial R} - \frac{2 V_\theta^2}{R} \quad (14)$$

Squaring Equation (13) and differentiating gives

$$\begin{aligned} \frac{\partial V_\theta^2}{\partial R} = & - \frac{2B^2}{R^3} - \frac{2BC}{R^2} + 2(BE + CD) + 2(2CE + D^2)R \\ & + 6DER^2 + 4E^2R^3 \end{aligned} \quad (15)$$

Squaring Equation (13) and multiplying by 2/R gives

$$\begin{aligned} \frac{2V_\theta^2}{R} = & \frac{2B^2}{R^3} + \frac{4BC}{R^2} + \frac{2(2BD + C^2)}{R} + 4(BE + CD) \\ & + 2(2CE + D^2)R + 4DER^2 + 2E^2R^3 \end{aligned} \quad (16)$$

Substituting Equations (15) and (16) into Equation (14) and integrating gives

$$\begin{aligned} V_z^2 = & 2 g_c J c_p T_t + \frac{2BC}{R} - (4BD + 2C^2) \log R - 6(BE + CD)R \\ & - (4CE + 2D^2)R^2 - \frac{10}{3} DER^3 - \frac{3}{2} E^2R^4 + K \end{aligned} \quad (17)$$

where K is a constant of integration, the value of which may be established by the boundary conditions.

The program commences by defining conditions at the rotor inlet: hub/tip radius ratio, tip speed, tip axial velocity, blockage factors, and the absolute tangential velocity distribution. Assuming stagnation pressure and temperature uniform radially, the axial velocity distribution is determined by integrating the radial equilibrium equation. The mass flow is determined by integrating the flow derivative in the radial direction. Having determined the axial velocity distribution at the rotor inlet, all other aerodynamic quantities may be readily calculated.

To determine rotor outlet conditions, values must be assigned to the rotor tip diffusion factor and tip axial velocity ratio. Further, to define the axial location of the rotor exit station, an "aspect ratio" is required. This "aspect ratio" is interpreted as the result of dividing the difference of the

geometric tip and hub radii at the rotor inlet station by the axial projected distance between inlet and exit stations. To account for nonisentropic compression, a rotor polytropic efficiency is required. This is assumed constant radially.

The rotor outlet conditions are arrived at by an iterative procedure which commences by setting the geometric exit hub and tip radii equal to the inlet. From the rotor tip diffusion factor, tip solidity, blockage factors and axial velocity ratio, the tip absolute tangential velocity is established and from this boundary condition, the tangential velocity distribution across the annulus may be established. The energy transfer and stagnation pressure rise may now be calculated.

Since all the radial variables in the equilibrium equation are now known, this equation may be numerically integrated and, from the boundary condition of a defined tip axial velocity, a constant of integration evaluated. This results in an axial velocity distribution across the annulus at the rotor exit station. From the radial distribution of axial velocity, the rate of change of flow with respect to radius may be established and integrated numerically to give the flow through the rotor exit station. If this flow does not equal the rotor inlet flow, the hub radius is increased (or reduced) and the calculation repeated until convergence occurs.

Once the calculation converges on mass flow, the rotor hub ramp angle is calculated and checked against an assigned limit. If the hub ramp angle violates the assigned limit, then the rotor geometric exit hub radius is set at a value for which the limit is attained, and the rotor geometric exit tip radius reduced to the point which satisfies the flow requirements. Should the reduction of the rotor exit tip radius cause a violation of the assigned tip ramp angle limit, then the "aspect ratio" is reduced and the calculation repeated until continuity of flow is obtained.

Having satisfied ramp angle tests and continuity of flow, the program now tests the absolute Mach number and relative flow angle at the exit of the rotor hub. If either of these parameters (in this stated order) violates its assigned limit, the program reduces the rotor tip diffusion factor and repeats the calculation until these limit tests are satisfied.

The calculation now proceeds to establish stator exit conditions. To determine the stator exit annulus, the coefficients in the polynomial, as defined by Equation (13), defining absolute tangential velocity at the stator exit are required. A polytropic stage efficiency, stator hub solidity, blockage factors, tip axial velocity ratio, and aspect ratio are also required.

The stator exit calculations for satisfying continuity commence similar to those for the rotor by setting the exit geometric hub and tip radius equal to the inlet values. The hub and tip ramp angles are then tested in the same

order as for the rotor and the aspect ratio relaxed if necessary to satisfy the geometric limits. When the assigned geometric limits have been satisfied, the stator hub diffusion factor is checked against its assigned limit. If this limit is violated, the rotor tip diffusion factor is reduced and the calculation repeated for the current stage.

When a stage configuration, satisfying all limits, is achieved, the pressure ratio and energy addition are mass averaged to give stage performance. Successive stages are added until some predetermined limit in overall pressure ratio is achieved. If the limit in overall pressure cannot be exceeded in a predetermined maximum number of stages, the calculation is terminated and the values calculated up to this point printed out.

The logic of the program is restricted to consider only tip radii at any station which is equal to, or less than, the inlet blade tip radii. Positive tip ramp angles cannot occur.

This design program has been extensively used in a parametric compressor study of advanced multistage axial-flow compressors reported in Reference 2.

PROGRAM RESTRICTIONS

It has been pointed out already that the expression for the absolute tangential velocity is in the form of a quadratic and subject to restrictions on the choice of roots. It is incumbent on the user, when defining the absolute tangential velocity through the use of the polynomial coefficients, that rational input values for the coefficients be used since only restricted levels satisfy the equation of continuity.

A further restriction applies to defining the input level of rotor tip diffusion factor. If a maximum level is exceeded, both roots are complex and the physical meaning is lost. The program has error messages imbedded in the logic so that this condition may be readily identified.

The maximum level of rotor tip diffusion factor for the inlet flow conditions, tip speed, axial velocity ratio, and solidity can be easily established. The diffusion factor is

$$D_R = 1 - \frac{V'_2}{V'_1} + \frac{V'_{\theta 1} - V'_{\theta 2}}{2 \sigma V'_1} \quad (18)$$

or

$$D_R = 1 - \frac{V_{z2}}{\left| \cos \beta_2' \right| V_1'} + \frac{(U_1 - V_{\theta 1}) - V_{z2} \tan \beta_2'}{2 \sigma V_1'} \quad (19)$$

Since with established inlet conditions and V_{z2} the rotor diffusion factor is dependent only on $V_{\theta 2}'$ or β_2' , Equation (19) can be solved for its maximum value. Upon differentiating

$$\frac{d(D_R)}{d \beta_2'} = - \frac{V_{z2}}{\cos^2 \beta_2' V_1'} \sin \beta_2' - \frac{V_{z2}}{2 \sigma V_1'} \frac{1}{\cos^2 \beta_2'}$$

Setting the right hand side to zero and solving for β_2' , it is found that

$$\beta_{2 \max}' = \arcsin \left(-\frac{1}{2 \sigma} \right) \quad (20)$$

and that D_R is at its maximum value. Substitution of Equation (20) into Equation (19) yields

$$D_{R \max} = 1 - \frac{V_{z2}}{\left(\frac{\sqrt{4 \sigma^2 - 1}}{2 \sigma} \right) V_1'} + \frac{(U_1 - V_{\theta 1}) + \frac{V_{z2}}{\sqrt{4 \sigma^2 - 1}}}{2 \sigma V_1'} \quad (21)$$

REFERENCES

1. Aerodynamic Design of Axial-Flow Compressor, NASA-SP-36, 1965, (Revised).
2. Miller, M. L. and Bryans, A. C., Parametric Compressor Study of Advanced Multistage Axial-Flow Compressors, Allison Division, GMC, EDR 4576, NASA CR-797, 1967.

APPENDIX A
SYSTEM OF EQUATIONS

A-1-

The system of equations given herein defines a method for the aerodynamic design of multistage, axial-flow compressors. The resulting designs satisfy prescribed limits on such parameters as:

- Rotor hub relative outlet flow angle.
- Stator hub inlet Mach number.
- Stator hub diffusion factor.
- Hub and tip ramp angles.

As a basis for calculation, the following simplifying assumptions are made:

- The working fluid is a perfect gas with constant specific heat.
- The flow is axisymmetric, steady, and radially isentropic.
- The effect of streamline curvature is neglected.

Roman numerals are used to define each section of the calculation. These in turn appear on the FORTRAN source deck listing (Appendix B) and on the logical flow chart (Appendix C).

SECTION I

At the inlet of the compressor the following quantities are known:

Specific heat at constant pressure	c_p
Equivalent molecular weight	M
Ratio of specific heats	γ
Inlet total pressure	P_{ti}
Inlet total temperature	T_{ti}
Inlet tip radius	R_{T1i}
Inlet tip speed	U_{T1i}
Inlet hub/tip radius ratio	$(R_H/R_T)_{1i}$
Inlet axial velocity at tip	V_{zT1i}
Blockage factor at tip	δ_{T1}^*
Blockage factor at hub	δ_{H1}^*
Number of radial stations used	N
Coefficients in absolute tangential velocity equation	B_1, C_1, D_1, E_1

At each successive stage in the compressor the following quantities are known.

Axial velocity ratio at rotor tip	(V_{zT2}/V_{zT1})
Rotor polytropic efficiency	η_{PR}
Rotor tip solidity	σ_{RT}
Rotor aspect ratio	AR_R
Blockage factor at tip—rotor outlet	δ_{T2}^*
Blockage factor at hub—rotor outlet	δ_{H2}^*
Ramp angle limit, rotor hub	a_{RHL}
Ramp angle limit, rotor tip	a_{RTL}
Stage energy addition, either	
Rotor tip diffusion factor and	D_{RT}
coefficients in absolute tangential velocity at rotor outlet	C_2, D_2, E_2
or	
Coefficients in absolute tangential velocity at rotor outlet	B_2, C_2, D_2, E_2
Axial velocity ratio at stator tip	(V_{zT3}/V_{zT2})
Stage polytropic efficiency	η_{PS}
Stator hub solidity	σ_{SH}
Stator aspect ratio	AR_S
Blockage factor at tip—stator outlet	δ_{T3}^*
Blockage factor at hub—stator outlet	δ_{H3}^*
Ramp angle limit, stator hub	a_{SHL}
Ramp angle limit, stator tip	a_{STL}
Limiting stator hub diffusion factor	D_{SHL}
Limiting stator hub Mach number	M_{SHL}
Limiting relative air angle at rotor hub (outlet)	β'_{2HL}
Coefficients in absolute tangential velocity equation, stator outlet	B_3, C_3, D_3, E_3

SECTION II

Set the rotor inlet tip radius equal to the initial value.

$$R_{T1} = R_{T1i}$$

Calculate the gas constant.

$$R_M = 1545.4/M$$

The stagnation density is

$$\rho_{t1} = \frac{144.0 P_{t1}}{R_M T_{t1}}$$

The rotor hub geometric radius is

$$R_{H1} = R_{T1} \left(\frac{R_H}{R_T} \right)_1$$

The rotor tip effective radius is

$$R_{1,1} = \left\{ \delta_{T1}^* R_{T1}^2 + (1 - \delta_{T1}^*) R_{H1}^2 \right\}^{1/2}$$

The rotor hub effective radius is

$$R_{1,N} = \left\{ \delta_{H1}^* R_{H1}^2 + (1 - \delta_{H1}^*) R_{T1}^2 \right\}^{1/2}$$

where blockage is defined as

$$(1 - \delta_{Tg}^*) (R_{Tg}^2 - R_{Hg}^2) \equiv (R_{Tg}^2 - R_{Te}^2)$$

and

$$(1 - \delta_{Hg}^*) (R_{Tg}^2 - R_{Hg}^2) \equiv (R_{He}^2 - R_{Hg}^2)$$

such that

$$\dot{w} = 2\pi (\delta_T^* + \delta_H^* - 1) \int_{R_{Hg}}^{R_{Tg}} \rho V_z R dR$$

The axial velocity at the rotor tip may be used to evaluate the constant of integration in Equation (17).

$$\begin{aligned}
 K_1 = & V_{zT1}^2 - 2 B_1 C_1 / R_{1,1} + 2 (2 B_1 D_1 + C_1^2) \log R_{1,1} \\
 & + 6 (B_1 E_1 + C_1 D_1) R_{1,1} + 2 (2 C_1 E_1 + D_1^2) R_{1,1}^2 \\
 & + [(10/3) D_1 E_1] R_{1,1}^3 + [(3/2) E_1^2] R_{1,1}^4 - 2 g_c J c_p T_{t1,1}
 \end{aligned}$$

Since the compressor inlet total temperature is assumed radially constant the $2 g_c J c_p T_t$ term in the foregoing equation may be ignored.

The inlet axial velocity and blade speed at the rotor tip are set to their initial value

$$V_{z1,1} = V_{zT1i}$$

and

$$U_{T1} = U_{T1i}$$

SECTION III

The annulus at the rotor inlet is subdivided into N concentric rings of equal height, giving N+1 reference radii. At each of these radii compute the axial velocity using Equation (17) and the constant of integration from Section II. The following equations are evaluated from m = 2 to m = N.

Reference radii

$$R_{1,m} = R_{1,m-1} - \frac{R_{1,1} - R_{1,N}}{(N-1)}$$

Axial velocity

$$\begin{aligned}
 V_{z1,m} = & \left(2 B_1 C_1 / R_{1,m} - 2 (2 B_1 D_1 + C_1^2) \log R_{1,m} \right. \\
 & - 6 (B_1 E_1 + C_1 D_1) R_{1,m} - 2 (2 C_1 E_1 + D_1^2) R_{1,m}^2 \\
 & \left. - [(10/3) D_1 E_1] R_{1,m}^3 - [(3/2) E_1^2] R_{1,m}^4 + K_1 \right)^{1/2}
 \end{aligned}$$

SECTION IV

Calculate the conditions at the rotor inlet by executing the following steps from $m = 1$ to $m = N$.

Rotor blade speed

$$U_{1,m} = R_{1,m} \left(\frac{U_{T1i}}{R_{T1i}} \right)$$

Absolute tangential velocity

$$V_{\theta 1,m} = \frac{B_1}{R_{1,m}} + C_1 + D_1 R_{1,m} + E_1 R_{1,m}^2$$

Absolute velocity

$$V_{1,m} = \left(V_{z1,m}^2 + V_{\theta 1,m}^2 \right)^{1/2}$$

Static density

$$\rho_{1,m} = \rho_{t1,m} \left(1.0 - \frac{V_{1,m}^2}{2 g_c J c_p T_{ti}} \right)^{1/(\gamma-1)}$$

Absolute air angle

$$\beta_{1,m} = \tan^{-1} \left(\frac{V_{\theta 1,m}}{V_{z1,m}} \right)$$

Relative air angle

$$\beta'_{1,m} = \tan^{-1} \left(\frac{U_{1,m} - V_{\theta 1,m}}{V_{z1,m}} \right)$$

Relative velocity

$$V'_{1,m} = \frac{V_{z1,m}}{\cos \beta'_{1,m}}$$

Relative Mach number

$$M'_{1,m} = \frac{V'_{1,m}}{\left[g_c \gamma R_m \left(T_{ti} - \frac{V_{1,m}^2}{2 g_c J c_p} \right) \right]^{1/2}}$$

Absolute Mach number

$$M_{1,m} = \frac{V_{1,m}}{\left[g_c \gamma R_m \left(T_{ti} - \frac{V_{1,m}^2}{2 g_c J c_p} \right) \right]^{1/2}}$$

Axial Mach number

$$M_{z1,m} = \frac{V_{z1,m}}{\left[g_c \gamma R_m \left(T_{ti} - \frac{V_{z1,m}^2}{2 g_c J c_p} \right) \right]^{1/2}}$$

Set the total temperature and pressure at each radial station equal to the value at the inlet.

$$T_{t1,m} = T_{ti}$$

$$P_{t1,m} = P_{ti}$$

SECTION V

Summate the weight flow across the annulus at the inlet of the first rotor.

$$\dot{w}_1 = \sum_{m=1}^{N-1} \frac{\pi (R_{1,m}^2 - R_{1,m+1}^2)}{144.0} \frac{(\rho_{1,m} V_{z1,m} + \rho_{1,m+1} V_{z1,m+1})}{2.0}$$

This completes the calculations for the inlet of the first rotor. Before proceeding to the rotor outlet calculation, set each of the ramp angles to zero,

$$\alpha_{RT} = 0.0$$

$$\alpha_{RH} = 0.0$$

$$\alpha_{ST} = 0.0$$

$$\alpha_{SH} = 0.0$$

and save initial values of aspect ratio and the B coefficient in the polynomial for tangential velocity.

$$AR_{Ri} = AR_R$$

$$AR_{Si} = AR_S$$

$$B_{2S} = B_2$$

SECTION VI

The absolute tangential velocity at the rotor outlet tip may be explicitly defined as a polynomial function of R_2 , or implicitly defined through the rotor tip diffusion factor, D_{RT} . If D_{RT} is not given, go to Section VII.

If D_{RT} is given the B coefficient in the function for absolute tangential velocity is evaluated as follows. Determine the axial distance between rotor inlet and rotor outlet.

$$b_R = \frac{R_{T1} - R_{H1}}{AR_R}$$

Calculate rotor outlet tip radius,

$$R_{T2} = R_{T1} + b_R \tan \alpha_{RT}$$

axial velocity,

$$V_{zT2} = V_{zT1} \left(\frac{V_{zT2}}{V_{zT1}} \right)$$

and blade speed.

$$U_{T2} = R_{T2} \left(\frac{U_{T1i}}{R_{T1i}} \right)$$

The diffusion factor at the rotor tip is given by

$$D_{RT} = 1.0 - \frac{V'_{T2}}{V'_{T1}} + \frac{V'_{\theta T1} - V'_{\theta T2}}{2 \sigma_{RT} V'_{T1}}$$

or

$$D_{RT} = 1.0 - \frac{V'_{T2}}{V'_{T1}} + \frac{U_{T1} - V_{\theta T1} - U_{T2} + V_{\theta T2}}{2 \sigma_{RT} V'_{T1}}$$

This may be rearranged as

$$V'_{T2} = \frac{V_{\theta T2}}{2 \sigma_{RT}} + \left[(1.0 - D_{RT}) V'_{T1} + \frac{U_{T1} - V_{\theta T1} - U_{T2}}{2 \sigma_{RT}} \right]$$

or as

$$V'_{T2} = R V_{\theta T2} + Q \quad (A-1)$$

where

$$R = \frac{1}{2 \sigma_{RT}}$$

and

$$Q = \left[(1.0 - D_{RT}) V'_{T1} + \frac{U_{T1} - V_{\theta T1} - U_{T2}}{2 \sigma_{RT}} \right]$$

now

$$V'_{T2} = \left[(U_{T2} - V_{\theta T2})^2 + V_{zT2}^2 \right]^{1/2} \quad (A-2)$$

Squaring and equating (A-1) and (A-2) results in

$$U_{T2}^2 - 2 U_{T2} V_{\theta T2} + V_{\theta T2}^2 + V_{zT2}^2 = R^2 V_{\theta T2}^2 + 2 QR V_{\theta T2} + Q^2$$

which reduces to

$$V_{\theta T2}^2 + \left[\frac{-2 (U_{T2} + RQ)}{1.0 - R^2} \right] V_{\theta T2} + \left[\frac{V_{zT2}^2 + U_{T2}^2 - Q^2}{1.0 - R^2} \right] = 0$$

or

$$V_{\theta T2,1}^2 + S V_{\theta T2,1} + T = 0 \quad (A-3)$$

where

$$S = \left[\frac{-2(U_{T2} + RQ)}{1.0 - R^2} \right]$$

and

$$T = \left[\frac{V_{zT2}^2 + U_{T2}^2 - Q^2}{1.0 - R^2} \right]$$

The absolute tangential velocity at the rotor tip may be obtained by solving Equation (A-3).

$$V_{\theta T2} = \frac{-S - \sqrt{S^2 - 4T}}{2}$$

The calculation is restricted to positive real roots. The coefficient B_2 is given by

$$B_2 = R_{T2} V_{\theta T2} - C_2 R_{T2} - D_2 R_{T2}^2 - E_2 R_{T2}^3$$

Go to Section VIII.

SECTION VII

Determine the axial distance between rotor inlet and rotor outlet.

$$b_R = \frac{R_{T1} - R_{H1}}{AR_R}$$

Calculate rotor outlet tip radius,

$$R_{T2} = R_{T1} + b_R \tan \alpha_{RT}$$

axial velocity,

$$V_{zT2} = V_{zT1} \left(\frac{V_{zT2}}{V_{zT1}} \right)$$

and blade speed at geometric tip radii

$$U_{T2} = R_{T2} \left(\frac{U_{T1i}}{R_{T1i}} \right)$$

SECTION VIII

Set axial velocity at effective tip radii

$$V_{z2,1} = V_{zT2}$$

At the rotor exit station calculate the following.

Geometric hub radius

$$R_{H2} = R_{H1} + b_R \tan \alpha_{RH}$$

Effective tip radius

$$R_{2,1} = \left\{ \delta_{T2}^* R_{T2}^2 + (1 - \delta_{T2}^*) R_{H2}^2 \right\}^{1/2}$$

Effective hub radius

$$R_{2,N} = \left\{ \delta_{H2}^* R_{H2}^2 + (1 - \delta_{H2}^*) R_{T2}^2 \right\}^{1/2}$$

Geometric annulus area

$$A_{2g} = \pi (R_{T2}^2 - R_{H2}^2)$$

Effective annulus area

$$A_{2e} = \pi (R_{2,1}^2 - R_{2,N}^2)$$

Blade speed at effective tip radii

$$U_{2,1} = R_{2,1} \left(\frac{U_{T1i}}{R_{T1i}} \right)$$

Absolute tangential velocity at effective tip radii

$$V_{\theta 2,1} = \frac{B_2}{R_{2,1}} + C_2 + D_2 R_{2,1} + E_2 R_{2,1}^2$$

Total temperature at effective tip radii

$$T_{t2,1} = T_{t1,1} + \frac{(U_{2,1} V_{\theta 2,1} - U_{1,1} V_{\theta 1,1})}{g_c J c_p}$$

and the constant of integration, K_2 , for the axial velocity equation is

$$\begin{aligned}
 K_2 = & v_{zT2}^2 - 2 B_2 C_2 / R_{2,1} + 2 (2 B_2 D_2 + C_2^2) \log R_{2,1} \\
 & + 6 (B_2 E_2 + C_2 D_2) R_{2,1} + 2 (2 C_2 E_2 + D_2^2) R_{2,1}^2 \\
 & + [(10/3) D_2 E_2] R_{2,1}^3 + [(3/2) E_2^2] R_{2,1}^4 - 2 g_c J c_p T_{t2,1}
 \end{aligned}$$

SECTION IX

The annulus at the rotor exit is subdivided into N concentric rings of equal height, giving $N+1$ reference radii. At each of these radii, compute the blade speed, absolute tangential velocity, total temperature, and axial velocity. The following steps are executed for $m = 2, N$.

$$R_{2,m} = R_{2,m-1} - \frac{R_{2,1} - R_{2,N}}{(N-1)}$$

$$U_{2,m} = R_{2,m} \left(\frac{U_{T1i}}{R_{T1i}} \right)$$

$$v_{\theta 2,m} = \frac{B_2}{R_{2,m}} + C_2 + D_2 R_{2,m} + E_2 R_{2,m}^2$$

$$T_{t2,m} = T_{t1,m} + \frac{U_{2,m} v_{\theta 2,m} - U_{1,m} v_{\theta 1,m}}{g_c J c_p}$$

$$\begin{aligned}
 v_{z2,m} = & \left\{ 2 B_2 C_2 / R_{2,m} - 2 (2 B_2 D_2 + C_2^2) \log R_{2,m} \right. \\
 & - 6 (B_2 E_2 + C_2 D_2) R_{2,m} - 2 (2 C_2 E_2 + D_2^2) R_{2,m}^2 \\
 & \left. - [(10/3) D_2 E_2] R_{2,m}^3 - [(3/2) E_2^2] R_{2,m}^4 + 2 g_c J c_p T_{t2,m} + K_2 \right\}^{1/2}
 \end{aligned}$$

SECTION X

At the rotor exit station, the following functions are evaluated for $m = 1, N$.

Total pressure

$$P_{t2,m} = P_{t1,m} \left(\frac{T_{t2,m}}{T_{t1,m}} \right)^{\gamma_{PR} (\gamma / (\gamma - 1))}$$

Total density

$$\rho_{t2,m} = \frac{144.0 P_{t2,m}}{\gamma_m T_{t2,m}}$$

Absolute velocity

$$V_{2,m} = (V_{z2,m}^2 + V_{\theta 2,m}^2)^{1/2}$$

Static density

$$\rho_{2,m} = \rho_{t2,m} \left(1.0 - \frac{V_{2,m}^2}{2 g_c J c_p T_{t2,m}} \right)^{1/(\gamma-1)}$$

Absolute air angle

$$\beta_{2,m} = \tan^{-1} \left(\frac{V_{\theta 2,m}}{V_{z2,m}} \right)$$

Relative air angle

$$\beta'_{2,m} = \tan^{-1} \left(\frac{U_{2,m} - V_{\theta 2,m}}{V_{z2,m}} \right)$$

Relative velocity

$$V'_{2,m} = \frac{V_{z2,m}}{\cos \beta'_{2,m}}$$

Diffusion factor

$$D_{R,m} = 1.0 - \frac{V'_{2,m}}{V'_{1,m}} + \frac{[(U_{1,m} - V_{\theta 1,m}) - (U_{2,m} - V_{\theta 2,m})]}{2 \sigma_{RT} V'_{1,m}} \left[\frac{(R_{T1} + R_{T2})}{(R_{1,m} + R_{2,m})} \right]^{-1}$$

Static temperature

$$T_{2,m} = T_{t2,m} - \frac{V_{2,m}^2}{2 g_c J c_p}$$

Sonic velocity

$$a_{2,m} = (g_c \gamma \rho_m T_{2,m})^{1/2}$$

Absolute Mach number

$$M_{2,m} = \frac{V_{2,m}}{a_{2,m}}$$

Ideal relative total pressure ratio

$$(P'_{Rt,m})_{id} = \left\{ 1.0 + \frac{\frac{\gamma-1}{2} \left[1.0 - \left(\frac{R_{1,m}}{R_{2,m}} \right)^2 \right] U_{2,m}^2}{g_c \gamma R_m \left[T_{t1,m} + \frac{V_{1,m}'^2 - V_{1,m}^2}{2 g_c J c_p} \right]} \right\}^{\gamma/(\gamma-1)}$$

Loss coefficient

$$\bar{\omega}_{R,m} = (P'_{Rt,m})_{id} \left[\frac{1.0 - \frac{\left(\frac{P_{t2,m}}{P_{t1,m}} \right) \gamma/(\gamma-1)}{\left(\frac{T_{t2,m}}{T_{t1,m}} \right)}}{1.0 - \left(\frac{1.0}{1.0 + \frac{\gamma-1}{2} M_{1,m}'^2} \right)^{\gamma/(\gamma-1)}} \right]$$

Relative Mach number

$$M'_{2,m} = \frac{V'_{2,m}}{a_{2,m}}$$

Axial Mach number

$$M_{z2,m} = \frac{V_{z2,m}}{a_{2,m}}$$

Loss parameter

$$Z_{R,m} = \frac{\bar{\omega}_{R,m} \cos \beta'_{2,m}}{2 \sigma_{RT}} \left[\frac{(R_{T1} + R_{T2})}{(R_{1,m} + R_{2,m})} \right]^{-1}$$

SECTION XI

Summate the weight flow across the annulus at the exit of the rotor.

$$\dot{w}_2 = \sum_{m=1}^{N-1} \frac{\pi(R_{2,m}^2 - R_{2,m+1}^2)}{144.0} \frac{(\rho_{2,m} V_{z2,m} + \rho_{2,m+1} V_{z2,m+1})}{2.0}$$

SECTION XII

Calculate the absolute value of the error by which the weight flow at the rotor exit differs from the weight flow at the rotor inlet.

$$\epsilon_{\dot{w}} = \frac{|\dot{w}_2 - \dot{w}_1|}{\dot{w}_2}$$

If $\epsilon_{\dot{w}} \leq 0.001$ continuity of flow is assumed to be satisfied and the calculation proceeds to Section XXIV. If $\epsilon_{\dot{w}} > 0.001$ the rotor exit annulus area must be altered to satisfy continuity. Since this may be accomplished in one of three ways, a logical test must be made to determine the method to be followed.

If the rotor hub ramp angle is less than its specified limit, proceed to Section XXIII. If the rotor hub ramp angle is at its specified limit but the rotor tip ramp angle is equal to or less than zero and greater than its limit, proceed to Section XXV. If both the rotor hub and tip ramp angles are at their limit, calculate a new geometric area for the rotor exit.

$$A_{\text{new}} = A_{2g} + \frac{A_{2g} (\dot{w}_1 - \dot{w}_2)}{\dot{w}_2}$$

If the absolute value of the rotor tip ramp angle is equal to the absolute value of the rotor hub ramp angle proceed to Section XXVII; if the angles are unequal proceed to Section XXVI.

SECTION XIII

Having satisfied the limitations on rotor hub and tip ramp angles the absolute Mach number at the rotor hub is tested. If the Mach number does not exceed its desired limit go to Section XIV. If the desired limit is exceeded, modify the B coefficient in Equation (13) and calculate a new value for the absolute tangential velocity at the rotor tip.

The revised value of B_2 is calculated as follows. The total temperature at the rotor tip is

$$T_{t2,N} = T_{t1,N} + \frac{U_{2,N} V_{\theta 2,N} - U_{1,N} V_{\theta 1,N}}{g_c J c_p}$$

and the static temperature is

$$T_{2,N} = T_{t2,N} - \frac{v_{z2,N}^2 + v_{\theta 2,N}^2}{2 g_c J c_p}$$

Combine these two equations and obtain the square of the Mach number.

$$M_{2,N}^2 = \frac{v_{z2,N}^2 + v_{\theta 2,N}^2}{g_c \gamma \mathcal{R}_m \left(T_{t1,N} + \frac{U_{2,N} v_{\theta 2,N} - U_{1,N} v_{\theta 1,N}}{g_c J c_p} - \frac{v_{z2,N}^2 + v_{\theta 2,N}^2}{2 g_c J c_p} \right)}$$

This may be rearranged to give

$$v_{z2,N}^2 + v_{\theta 2,N}^2 = AA \left(T_{t1,N} + \frac{U_{2,N} v_{\theta 2,N} - U_{1,N} v_{\theta 1,N}}{g_c J c_p} - \frac{v_{z2,N}^2 + v_{\theta 2,N}^2}{2 g_c J c_p} \right)$$

where

$$AA = M_{2,N}^2 g_c \gamma \mathcal{R}_m$$

Separating the terms gives a quadratic in $v_{\theta 2,N}$:

$$\begin{aligned} v_{\theta 2,N}^2 \left(1 + \frac{AA}{2 g_c J c_p} \right) - v_{\theta 2,N} \left(\frac{AA U_{2,N}}{g_c J c_p} \right) \\ + \left(v_{z2,N}^2 - AA T_{t1,N} + \frac{AA U_{1,N} v_{\theta 1,N}}{g_c J c_p} - \frac{AA v_{z2,N}^2}{2 g_c J c_p} \right) = 0 \end{aligned}$$

or

$$\begin{aligned} v_{\theta 2,N}^2 + v_{\theta 2,N} \left(-\frac{2BB U_{2,N}}{1+BB} \right) + \left(\frac{v_{z2,N}^2 - AA T_{t1,N} + BB v_{z2,N}^2}{1+BB} \right) \\ + \left(2BB U_{1,N} v_{\theta 1,N} \right) = 0 \end{aligned}$$

where

$$BB = \frac{AA}{2 g_c J c_p}$$

This quadratic may be solved for $V_{\theta 2, N}$.

$$V_{\theta 2, N} = - CC + \sqrt{CC^2 - DD}$$

where

$$CC = - \frac{BB U_{2, N}}{1 + BB}$$

and

$$DD = \left(\frac{V_{z2, N}^2 - AA T_{t1, N} + BB V_{z2, N}^2}{1 + BB} + 2 BB U_{1, N} V_{\theta 1, N} \right)$$

The B_2 coefficient is given by

$$B_2 = V_{\theta 2, N} R_{2, N} - C_2 R_{2, N} - D_2 R_{2, N}^2 - E_2 R_{2, N}^3$$

Reinitialize the values of rotor hub ramp angle, rotor tip ramp angle, and aspect ratio,

$$\alpha_{RH} = 0.0$$

$$\alpha_{RT} = 0.0$$

$$AR_R = AR_{Ri}$$

and return to Section VII.

SECTION XIV

Test to see if the outlet relative flow angle at the rotor hub exceeds the desired limit. If the limit is not exceeded, go to Section XV. If the limit is exceeded modify the B_2 coefficient as follows.

$$B_2 = (U_{2, N} - V_{z2, N} \tan \beta'_{SH}) R_{2, N} - C_2 R_{2, N} - D_2 R_{2, N}^2 - E_2 R_{2, N}^3$$

Reinitialize rotor hub ramp angle, tip ramp angle, and aspect ratio

$$\alpha_{RH} = 0.0$$

$$\alpha_{RT} = 0.0$$

$$AR_R = AR_{Ri}$$

and return to Section VII.

SECTION XV

Having satisfied the specified limits on rotor hub and tip ramp angles, hub outlet absolute Mach number, and outlet relative air angle, the calculation proceeds to establish stator outlet conditions. Determine the axial distance between stator inlet and stator outlet.

$$b_S = \frac{R_{T2} - R_{H2}}{AR_S}$$

Calculate stator outlet tip radius

$$R_{T3} = R_{T2} + b_S \tan \alpha_{ST}$$

Set the outlet total temperature at the stator tip

$$T_{t3,1} = T_{t2,1}$$

Geometric hub radius

$$R_{H3} = R_{H2} + b_S \tan \alpha_{SH}$$

Effective tip radius

$$R_{3,1} = \left\{ \delta_{T3}^* R_{T3}^2 + (1 - \delta_{T3}^*) R_{H3}^2 \right\}^{1/2}$$

Effective hub radius

$$R_{3,N} = \left\{ \delta_{H3}^* R_{H3}^2 + (1 - \delta_{H3}^*) R_{T3}^2 \right\}^{1/2}$$

Geometric annulus area

$$A_{3g} = \pi(R_{T3}^2 - R_{H3}^2)$$

Effective annulus area

$$A_{3e} = \pi(R_{3,1}^2 - R_{3,N}^2)$$

Tip axial velocity

$$V_{zT3} = V_{zT2} \left(\frac{V_{zT3}}{V_{zT2}} \right)$$

Evaluate the constant of integration K_3 , for the axial velocity equation.

$$\begin{aligned} K_3 = & V_{zT3}^2 - 2 B_3 C_3 / R_{3,1} + 2 (2 B_3 D_3 + C_3^2) \log R_{3,1} + 6 (B_3 E_3 + C_3 D_3) R_{3,1} \\ & + 2 (2 C_3 E_3 + D_3^2) R_{3,1}^2 + [(10/3) D_3 E_3] R_{3,1}^3 + [(3/2) E_3^2] R_{3,1}^4 \\ & - 2 g_c J c_p T_{t3,1} \end{aligned}$$

Set the axial velocity at the effective tip radii.

$$V_{z3,1} = V_{zT3}$$

SECTION XVI

The annulus at the stator exit is subdivided into N concentric rings of equal height, giving $N+1$ reference radii. At each of these radii calculate the total temperature and axial velocity.

$$R_{3,m} = R_{3,m-1} - \frac{R_{3,1} - R_{3,N}}{N - 1}$$

$$T_{t3,m} = T_{t2,m}$$

$$\begin{aligned} V_{z3,m} = & \left\{ 2 B_3 C_3 / R_{3,m} - 2 (2 B_3 D_3 + C_3^2) \log R_{3,m} - 6 (B_3 E_3 + C_3 D_3) R_{3,m} \right. \\ & - 2 (2 C_3 E_3 + D_3^2) R_{3,m}^2 - [(10/3) D_3 E_3] R_{3,m}^3 - [(3/2) E_3^2] R_{3,m}^4 \\ & \left. + 2 g_c J c_p T_{t3,m} + K_3 \right\}^{1/2} \end{aligned}$$

SECTION XVII

At the stator exit station the following functions are evaluated for $m=1, N$.

Absolute tangential velocity

$$V_{\theta 3,m} = \frac{B_3}{R_{3,m}} + C_3 + D_3 R_{3,m} + E_3 R_{3,m}^2$$

Total pressure

$$P_{t3,m} = P_{t1,m} \left(\frac{T_{t3,m}}{T_{t1,m}} \right)^{\eta_{PS} (\gamma/(\gamma-1))}$$

Total density

$$\rho_{t3, m} = \frac{144.0 P_{t3, m}}{\gamma_m T_{t3, m}}$$

Absolute velocity

$$v_{3, m} = (v_{z3, m}^2 + v_{\theta3, m}^2)^{1/2}$$

Static density

$$\rho_{3, m} = \rho_{t3, m} \left(1.0 - \frac{v_{3, m}^2}{2 g_c J c_p T_{t3, m}} \right)^{1/(\gamma-1)}$$

Absolute air angle

$$\theta_{3, m} = \tan^{-1} \left(\frac{v_{\theta3, m}}{v_{z3, m}} \right)$$

Diffusion factor

$$D_{S, m} = 1.0 - \frac{v_{3, m}}{v_{2, m}} + \frac{(v_{\theta2, m} - v_{\theta3, m})}{2 \sigma_{SH} v_{2, m}} \left[\frac{(R_{H2} + R_{H3})}{(R_{2, m} + R_{3, m})} \right]^{-1}$$

Loss coefficient

$$\bar{\omega}_{S, m} = \frac{\left(1.0 - \frac{P_{t3, m}}{P_{t2, m}} \right)}{\left[1.0 - \frac{1.0}{\left(1.0 + \frac{\gamma-1}{2} M_{2, m}^2 \right)^{\gamma/(\gamma-1)}} \right]}$$

Sonic velocity

$$a_{3, m} = \left[g_c \gamma \rho_m \left(T_{t3, m} - \frac{v_{3, m}^2}{2 g_c J c_p} \right) \right]^{1/2}$$

Absolute Mach number

$$M_{3, m} = \frac{v_{3, m}}{a_{3, m}}$$

Loss parameter

$$Z_{S,m} = \frac{\bar{s}_{S,m} \cos \beta_{3,m}}{2 \sigma_{SH}} \left[\frac{R_{H2} + R_{H3}}{R_{2,m} + R_{3,m}} \right]^{-1}$$

SECTION XVIII

Summate the weight flow across the annulus at the exit of the stator.

$$\dot{w}_3 = \sum_{m=1}^{N-1} \frac{\pi (R_{3,m}^2 - R_{3,m+1}^2)}{144.0} \frac{(\rho_{3,m} V_{z3,m} + \rho_{3,m+1} V_{z3,m+1})}{2.0}$$

SECTION XIX

Calculate the following mass averaged parameters:

Stage pressure ratio

$$R_c = \left\{ \sum_{m=1}^{N-1} S \left[\left(\frac{P_{t3,m} + P_{t3,m+1}}{P_{t1,m} + P_{t1,m+1}} \right)^{(\gamma-1)/\gamma} - 1.0 \right] \right\}^{\gamma/(\gamma-1)}$$

Cumulative pressure ratio

$$(R_c)_{ov} = \left\{ \frac{\sum_{m=1}^{N-1} S \left[\left(\frac{P_{t3,m} + P_{t3,m+1}}{2.0 P_{ti}} \right)^{(\gamma-1)/\gamma} - 1.0 \right]}{\dot{w}_3} \right\}^{\gamma/(\gamma-1)}$$

Stage temperature ratio

$$T_R = \left\{ \frac{\sum_{m=1}^{N-1} S \left[\left(\frac{T_{t3,m} + T_{t3,m+1}}{T_{t1,m} + T_{t1,m+1}} \right) - 1.0 \right]}{\dot{w}_3} \right\}$$

Cumulative temperature ratio

$$(T_R)_{ov} = \left\{ \frac{\sum_{m=1}^{N-1} S \left[\left(\frac{T_{t3,m} + T_{t3,m+1}}{2.0 T_{ti}} \right) - 1.0 \right]}{\dot{w}_3} \right\}$$

where:

$$S = \frac{\pi (R_{3,m}^2 - R_{3,m+1}^2)}{144.0} \frac{(\rho_{3,m} V_{z3,m} + \rho_{3,m+1} V_{z3,m+1})}{2.0}$$

The stage adiabatic efficiency is given by

$$\eta_{ad} = \left[\frac{R_c^{(\gamma-1)/\gamma} - 1.0}{T_R - 1.0} \right]$$

and cumulative adiabatic efficiency by

$$(\eta_{ad})_{ov} = \left[\frac{(R_c)_{ov}^{(\gamma-1)/\gamma} - 1.0}{(T_R)_{ov} - 1.0} \right]$$

Calculate the absolute value of the error by which the weight flow at the stator exit differs from the weight flow at the rotor inlet.

$$\epsilon_{\dot{w}} = \frac{|\dot{w}_3 - \dot{w}_1|}{\dot{w}_3}$$

If $\epsilon_{\dot{w}} \leq 0.001$, continuity of flow is assumed to be satisfied and the calculation proceeds to Section XXIX. If $\epsilon_{\dot{w}} > 0.001$, the stator exit annulus area must be altered to satisfy continuity. This is accomplished in a manner similar to that outlined for the rotor in Section XII.

If the stator hub ramp angle is less than its specified limit proceed to Section XXVIII. If the stator hub ramp angle is at its specified limit, but the stator tip ramp angle is equal to or less than zero, and greater than its limit proceed to Section XXX. If both the stator hub and tip ramp angles are at their limit calculate a new effective area for the stator exit.

$$A_{new} = A_{3e} + \frac{A_{3e} (\dot{w}_1 - \dot{w}_3)}{\dot{w}_3}$$

If the absolute value of the stator tip ramp angle is equal to the absolute value of the stator hub ramp angle proceed to Section XXXII; if the angles are unequal proceed to Section XXXI.

SECTION XX

Having satisfied the limitations on stator hub and tip ramp angles, the diffusion factor at the stator hub is tested to determine if it exceeds a desired limit. If the limit has not been exceeded, go to Section XXI. If the limit has been exceeded, modify the B_2 coefficient in the polynomial function for absolute tangential velocity at the rotor exit and calculate new rotor exit conditions.

The revised value of B_2 is calculated as follows.

The stator hub D-factor is given by

$$D_{SH} = 1.0 - \frac{V_{3,N}}{(V_{\theta 2,N}^2 + V_{z2,N}^2)^{1/2}} + \frac{(V_{\theta 2,N} - V_{\theta 3,N})}{2 \sigma_{SH} (V_{\theta 2,N}^2 + V_{z2,N}^2)^{1/2}}$$

This may be rearranged to give

$$\frac{V_{3,N} + (V_{\theta 3,N} - V_{\theta 2,N})/2 \sigma_{SH}}{(1.0 - D_{SH})} = (V_{\theta 2,N}^2 + V_{z2,N}^2)^{1/2}$$

or

$$AF + BF V_{\theta 2,N} = (V_{\theta 2,N}^2 + V_{z2,N}^2)^{1/2} \quad (A-4)$$

where

$$AF = \frac{-V_{3,N} - V_{\theta 3,N}/2 \sigma_{SH}}{D_{SH} - 1.0}$$

$$BF = 1/2 \sigma_{SH} (D_{SH} - 1.0)$$

Squaring Equation (A-4) and rearrangement into a quadratic in $V_{\theta 2}$ yields

$$V_{\theta 2,N}^2 + 2 CF V_{\theta 2,N} + DF = 0$$

where

$$CF = \frac{-(AF)(BF)}{1 - (BF)^2}$$

$$DF = \frac{V_{Z2,N}^2 - (AF)^2}{1 - (BF)^2}$$

Thus, the absolute tangential velocity at the rotor hub is given by

$$V_{\theta 2,N} = -CF \pm \sqrt{CF^2 - DF}$$

The required root must be positive. If two positive roots occur, the original expression for D_{SH} should be tested to determine which is the correct root. The new value for the B_2 coefficient is given by

$$B_2 = R_{2,N} V_{\theta 2,N} - C_2 R_{2,N} - D_2 R_{2,N}^2 - E_2 R_{2,N}^3$$

Reinitialize hub and tip ramp angles, and aspect ratios for both rotor and stator.

$$\alpha_{RH} = 0.0$$

$$\alpha_{RT} = 0.0$$

$$\alpha_{SH} = 0.0$$

$$\alpha_{ST} = 0.0$$

$$AR_R = AR_{Ri}$$

$$AR_S = AR_{Si}$$

and return to Section VII.

SECTION XXI

This completes the performance calculations for a stage. Print the stage output and test if the required overall pressure ratio has been achieved.

If the required pressure ratio has been reached, print a statement to this effect and proceed to Section I and commence another data set. If the required pressure ratio has not been reached, test to determine if the maximum number of stages has been exceeded. If the maximum number of stages has not been exceeded, go to Section XXII and calculate the inlet conditions to the next rotor. If the maximum number of stages has been exceeded, print a statement to this effect and proceed to Section I and commence another data set.

SECTION XXII

Calculate the conditions at the rotor inlet by executing the following steps from m=1 to m=N.

Rotor blade speed

$$U_{1,m} = R_{3,m} \left(\frac{U_{T1i}}{R_{T1i}} \right)$$

Absolute tangential velocity

$$V_{\theta 1,m} = V_{\theta 3,m}$$

Absolute velocity

$$V_{1,m} = V_{3,m}$$

Absolute air angle

$$\beta_{1,m} = \beta_{3,m}$$

Relative air angle

$$\beta'_{1,m} = \tan^{-1} \left(\frac{U_{1,m} - V_{\theta 1,m}}{V_{z3,m}} \right)$$

Relative velocity

$$V'_{1,m} = \frac{V_{z3,m}}{\cos \beta'_{1,m}}$$

Axial velocity

$$V_{z1,m} = V_{z3,m}$$

Reference radius

$$R_{1,m} = R_{3,m}$$

Sonic speed

$$a_{1,m} = \left[g_c \gamma R_m \left(T_{t3,m} - \frac{V_{1,m}^2}{2 g_c J c_p} \right) \right]^{1/2}$$

Absolute Mach number

$$M_{1,m} = \frac{V_{1,m}}{a_{1,m}}$$

Relative Mach number

$$M'_{1,m} = \frac{V'_{1,m}}{a_{1,m}}$$

Total temperature

$$T_{t1,m} = T_{t3,m}$$

Total pressure

$$P_{t1,m} = P_{t3,m}$$

Tip radius

$$R_{T1} = R_{T3}$$

Hub radius

$$R_{H1} = R_{H3}$$

Proceed to Section I and commence the calculation of another stage.

SECTION XXIII

Calculate new rotor exit annulus area, hub radius, and ramp angle.

$$A_{new} = A_{2e} + \frac{A_{2e} (\dot{w}_1 - \dot{w}_2)}{\dot{w}_2}$$

$$R_{Hnew} = \left[R_{T,2}^2 - \frac{A_{new}}{\pi(\delta_{T2}^* + \delta_{H2}^* - 1)} \right]^{1/2}$$

$$\alpha_{RH} = \tan^{-1} \left[\frac{(R_{Hnew} - R_{H1})}{b_R} \right]$$

Go to Section VIII.

SECTION XXIV

At this point in the calculation, continuity of flow has been satisfied; however, the hub or tip ramp angle limits may have been violated in the last iterative loop.

A three-branch logical test is made to determine the history of ramp angle changes. This test is as follows: If the hub ramp angle has not been previously set to its limit, check to see if it now exceeds its limit. If the limit is not exceeded go to Section XIII. If the limit is exceeded set $\alpha_{RH} = \alpha_{RHL}$ and go to Section VIII.

If the hub ramp angle has been previously set at its limit, but the tip ramp angle has not, check to see if the tip ramp angle is now below its limit. If the limit is not violated, test to see if α_{RT} is positive. If yes, this is considered unacceptable and the calculation is terminated. If no, go to Section XIII. If the limit is violated, set $\alpha_{RT} = \alpha_{RTL}$ and go to Section VI. If both the hub and tip ramp angles have been previously set at their limit go to Section XIII.

SECTION XXV

Calculate new rotor exit annulus area, tip radius, and tip ramp angle.

$$A_{new} = A_{2e} + \frac{A_{2e} (\dot{w}_1 - \dot{w}_2)}{\dot{w}_2}$$

$$R_{Tnew} = \left[R_{H2}^2 + A_{new}/\pi (\delta_{T2}^* + \delta_{H2}^* - 1) \right]^{1/2}$$

$$\alpha_{RT} = \tan^{-1} \left[\frac{(R_{Tnew} - R_{T1})}{b_R} \right]$$

Go to Section VI.

SECTION XXVI

Calculate a new value for the axial distance between rotor inlet and exit reference stations. The new annulus area calculated in Section XII may also be expressed as

$$A_{\text{new}} = \pi (R_{T2}^2 - R_{H2}^2)$$

where

$$R_{T2} = R_{T1} + b_R \tan \alpha_{RTL}$$

and

$$R_{H2} = R_{H1} + b_R \tan \alpha_{RHL}$$

or

$$\begin{aligned} A_{\text{new}}/\pi &= (R_{T1}^2 + 2 b_R R_{T1} \tan \alpha_{RTL} + b_R^2 \tan^2 \alpha_{RTL}) \\ &\quad - (R_{H1}^2 + 2 b_R R_{H1} \tan \alpha_{RHL} + b_R^2 \tan^2 \alpha_{RHL}) \end{aligned}$$

This may be rearranged as:

$$\begin{aligned} 0 &= b_R^2 (\tan^2 \alpha_{RTL} - \tan^2 \alpha_{RHL}) + 2 b_R (R_{T1} \tan \alpha_{RTL} - R_{H1} \tan \alpha_{RHL}) \\ &\quad + (R_{T1}^2 - R_{H1}^2 - A_{\text{new}}/\pi) \end{aligned}$$

or

$$0 = b_R^2 + 2 BE b_R + CE$$

where

$$BE = \frac{R_{T1} \tan \alpha_{RTL} - R_{H1} \tan \alpha_{RHL}}{AE}$$

$$CE = \frac{R_{T1}^2 - R_{H1}^2 - A_{\text{new}}/\pi}{AE}$$

and

$$AE = (\tan^2 \alpha_{RTL} - \tan^2 \alpha_{RHL})$$

The axial distance between rotor inlet and exit reference stations is given by:

$$b_R = -BE + \sqrt{BE^2 - CE}$$

Calculate new aspect ratio.

$$AR_R = \frac{(R_{T1} - R_{H1})}{b_R}$$

Go to Section VI.

SECTION XXVII

This section is similar to Section XXVI with the restriction that $|a_{RHL}| = |a_{RTL}|$. This gives

$$A_{new}/\pi = (R_{T1}^2 - 2 b_R R_{T1} \tan a_{RHL} - R_{H1}^2 - 2 b_R R_{H1} \tan a_{RHL})$$

or

$$b_R = \frac{R_{T1}^2 - R_{H1}^2 - A_{new}/\pi}{2 \tan a_{RHL} (R_{T1} + R_{H1})}$$

Calculate new aspect ratio.

$$AR_R = \frac{(R_{T1} - R_{H1})}{b_R}$$

Go to Section VI.

SECTION XXVIII

Calculate new effective annulus area at stator exit.

$$A_{new} = A_{3e} + \frac{A_{3e} (\dot{w}_1 - \dot{w}_3)}{\dot{w}_3}$$

Calculate new hub radius.

$$R_{H_{new}} = \left[R_{T3}^2 - \frac{A_{new}}{\pi (\delta_{T3}^* + \delta_{H3}^* - 1)} \right]^{1/2}$$

Calculate hub ramp angle.

$$a_{SH} = \tan^{-1} \left(\frac{R_{H_{new}} - R_{H2}}{b_S} \right)$$

Go to Section XV.

SECTION XXIX

The situation in the stator at this point is similar to that which prevailed in the rotor at Section XXIV and an analogous test is made to determine ramp angle changes. If the hub ramp angle has not been previously set to its limit, check to see if it now exceeds its limit. If the limit is not exceeded go to Section XX. If the limit is exceeded, set $\alpha_{SH} = \alpha_{SHL}$ and go to Section XV.

If the hub ramp angle has been previously set at its limit, but the tip ramp angle has not, check to see if the tip ramp angle is now below its limit. If the limit is not violated, test if α_{ST} is positive. If yes, this is considered unacceptable and the calculation is terminated. If no, go to Section XX. If the limit is violated, set $\alpha_{ST} = \alpha_{STL}$ and go to Section XV. If both the hub and tip ramp angles have been previously set at their limit go to Section XX.

SECTION XXX

Calculate a new effective annulus area at stator exit.

$$A_{new} = A_{3e} + \frac{A_{3e} (\dot{w}_1 - \dot{w}_3)}{\dot{w}_3}$$

Calculate new tip radius.

$$R_{T_{new}} = \left[R_{H3}^2 + \frac{A_{new}}{\pi(\delta_{T3}^* + \delta_{H3}^* - 1)} \right]^{1/2}$$

Calculate new tip ramp angle.

$$\alpha_{ST} = \tan^{-1} \left[\frac{R_{T_{new}} - R_{T2}}{b_S} \right]$$

Go to Section XV.

SECTION XXXI

Using a method similar to that derived in Section XXVI for the rotor, a new value for the axial distance between stator inlet and exit reference stations may be calculated.

$$b_S = -BE + \sqrt{BE^2 - CE}$$

where

$$BE = \frac{R_{T2} \tan \alpha_{STL} - R_{H2} \tan \alpha_{SHL}}{AE}$$

$$CE = \frac{R_{T2}^2 - R_{H2}^2 - A_{new}/\pi}{AE}$$

and

$$AE = \tan^2 \alpha_{STL} - \tan^2 \alpha_{SHL}$$

Calculate new aspect ratio.

$$AR_S = \frac{R_{T2} - R_{H2}}{b_S}$$

Go to Section XV.

SECTION XXXII

This section is similar to Section XXVII for the rotor. The axial distance between the inlet and exit reference stations

$$b_S = \frac{R_{T2}^2 - R_{H2}^2 - A_{new}/\pi}{2 \tan \alpha_{RHL} (R_{T2} + R_{H2})}$$

Calculate new aspect ratio.

$$AR_S = \frac{R_{T2} - R_{H2}}{b_S}$$

Go to Section XV.

APPENDIX B

FORTRAN IV SOURCE DECK LISTING

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$EXECUTE      IBJOB
$IBJOB N34
$IBFTC MAIN    DD,NOLIST

C      *** ADVANCED MULTISTAGE AXIAL-FLCW COMPRESSOR DESIGN CALCULATION
C      *** CALCULATIONS ARE MADE AT UP TO 11 RADIAL POSITIONS USING THE
C      *** ENERGY, MOMENTUM AND CONTINUITY EQUATIONS.

C      *** AXISYMMETRIC FLOW IS ASSUMED AND NO RADIAL GRADIENTS OF
C      *** ENTROPY NOR EFFECT OF CURVATURES OF STREAMLINES ARE INCLUDED

C      *** BOUNDARY LAYER BLOCKAGE FACTORS ARE INCLUDED WITH MASS FLOW
C      *** BEING INTEGRATED RADIALLY.

C      *** THE WORKING FLUID IS A PERFECT GAS WITH CONSTANT SPECIFIC
C      *** HEAT.

C      *** STAGES WILL BE ADDED UNTIL A SPECIFIED PRESSURE RATIO IS
C      *** INCLUDED.

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REAL MW,NPR,NPS,MSH,K1,M1P,K2,M2,K3
REAL M1,MZ1,M2P,MZ2,M3,MZ3
DIMENSION M1(11),MZ1(11),M2P(11),MZ2(11),M3(11),MZ3(11),A3(11)
DIMENSION VT2OT1(50),NPR(50),SRTIP(50),ARR(50),DTIP2(50),DH2(50),
1ARHL(50),ARTL(50),DRT(50),B2(50),C2(50),D2(50),E2(50),VT3OT2(50),
2NPS(50),SSH(50),ARS(50),DTIP3(50),DH3(50),ASHL(50),ASTL(50),
3DSH(50),MSH(50),BPSH(50),B3(50),C3(50),D3(50),E3(50)
DIMENSION VZ1(11),U1(11),VO1(11),RHOS1(11),BETA1(11),BETA1P(11),
1VIP(11),M1P(11),TT1(11),PT1(11),RS1VZ1(11),ACNE(11),R2(11),U2(11),
2VO2(11),TT2(11),VZ2(11),PT2(11),RHOT2(11),V2(11),RHOS2(11),
3BETA2(11),BETA2P(11),V2P(11),DR(11),TS2(11),ATWO(11),M2(11),
4PRI(11),WRB(11),ZR(11),RS2VZ2(11),ATO(11),TT3(11),R3(11),VO3(11),
5PT3(11),RHOT3(11),V3(11),RHOS3(11),BETA3(11),DS(11),WSB(11),
6ZS(11),RS3VZ3(11),ATHRE(11),WW3(11)
DIMENSION R1(11),V1(11),VZ3(11)
DIMENSION ARHD(50),ARTD(50),ASHD(50),ASTD(50),BET1D(11),BET1PD(11),
1,BET2D(11),BET2PD(11),BET3D(11),BPSD(50),TITL(12)
DIMENSION BO(50),ARO(50),ASC(50)
COMMON /SINITL/CON5,CP,DH1,DTIP1,ER1,ER2,ER3,ER4,ER5,ER6,ER7,GAM,
1MW,RCLIM,RHORT1,RTIP1I,TEMP,UTIP1I,VZTIP1
COMMON /CHEC/IFLAG,NSLM
COMMON /COM2/PTI,TTI,CON1,CON2,CCN3,CON4,DOGM1,B1,C1,D1,E1
COMMON /COM3/IGO,ITS,ITR,IOP,T,IIB,IID,IIM,FACTOR,ANM1,CON6,CON7,
1CON8,ITAL7
COMMON I,INC,IPR2,N,VT2OT1,NPR,SRTIP,ARRI,DTIP2,DH2,ARHD,ARTD,DRT,
182SAVE,C2,D2,E2,VT3OT2,NPS,SSH,ARS1,DTIP3,DH3,ASHD,ASTD,DSH,MSH,
2BPSD,B3,C3,D3,E3,W1,RCO,TRO,ETA0,RC,TR,ETA,RTIP1,ARR,ARS,RH1,RTIP2
3,RH2,RTIP3,RH3,BS,M,BET1D,BETA1,BET1PD,BETA1P,R1,U1,VZ1,VO1,V1,
4VIP,M1P,M1,MZ1,BET2D,BETA2,BET2PD,BETA2P,R2,U2,VZ2,VO2,V2,V2P,DR,
5M2P,M2,MZ2,BET3D,BETA3,R3,VZ3,VO3,V3,DS,M3,WRB,ZR,WSB,ZS,MZ3,ALPST
6,ALPSH,IERROR
COMMON IPR1,K1,UTIP1,RM,RHOT1,AONE,RS1VZ1,NM1,RHOS1,TT1,PT1,W2,
1EWA,VZTIP2,A2G,A2E,K2,ITAL1,ALPRH,RHNEW,ANEW,TAARTL,TAAARHL,AE,BE,
2CE,ALPRT,RTNEW,R2,TT2,PT2,RHOT2,RHOS2,TS2,ATWO,PRI,ATO,RS2VZ2
3,UTIP2,VOTIP2,Q,R,S,T,ITAL2,AA,BB,CC,DD,ITAL3,BPSH,W3,A3G,A3E,PT3,
4VZTIP3,K3,PRW3,PROW3,TRW3,TRW3,TT3,RHOS3,TAASHL,TAASTL,ASHL,ASTL,
5A3,ATHRE,RS3VZ3,WW3,ITAL8,AF,BF,CF,DF

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6,VZTIPO,ARHL,ARTL,RHOT3,TITL,BO,ARC,ASO
NAMELIST /NAME/CP,MW,GAM,TTI,PTI,RCLIM,RTIP1I,UTIP1I,RHORT1,VZTIPO
1,DTIP1,DH1,B1,C1,D1,E1,N,NSLIM,IPR1,IPR2,VT20T1,NPR,SRTIP,ARO,
2DTIP2,DH2,ARHD,ARTD,DRT,BO,C2,D2,E2,VT30T2,NPS,SSH,ASO,DTIP3,DH3,
3ASHD,ASTD,DSH,MSH,BPSD,B3,C3,D3,E3

C     *** IPR1 IS A DUMP TRIGGER WHICH IS USED AS FOLLOWS ...
C     *** WHEN =0, DUMPS WILL NOT OCCUR.
C     *** WHEN =1, A MINIMUM OF DYNAMIC DUMPS WILL OCCUR.
C     *** WHEN =2, ALL DYNAMIC DUMPS WILL OCCUR.

C     *** IPR2 IS A TRIGGER WHICH WHEN =1, WILL CAUSE ONLY INFORMATION
C     *** AT THE HUB AND TIP TO BE PRINTED. IF IPR2 =0, INFORMATION
C     *** AT ALL STATIONS WILL BE PRINTED.

C     *** START SECTION I

10 READ (5,11) IREAD,(TITL(I),I=1,12)
11 FORMAT (I1,A5,11A6)
1900 WRITE (6,26) (TITL(I),I=1,12)
26 FORMAT (1H123X,A5,11A6///)
IERROR=0

C     *** READ INITIAL DATA

C     *** READ DATA FOR EACH STAGE

IF (IREAD.GT.0) GO TO 19
READ (5,NAME)
GO TO 21
19 READ(5,15) CP,MW,GAM,TTI,PTI,RCLIM,RTIP1I,UTIP1I,RHORT1,VZTIPO,
1 DTIP1,DH1,B1,C1,D1,E1,N,NSLIM,IPR1,IPR2
15 FORMAT (9F8.0/7F8.0,2I3,2I1)
20 DO 22 I=1,NSLIM
    READ (5,25) VT20T1(I),NPR(I),SRTIP(I),ARO(I),DTIP2(I),DH2(I),
1ARHD(I),ARTD(I),DRT(I),BO(I),C2(I),D2(I),E2(I)
    READ (5,25) VT30T2(I),NPS(I),SSH(I),ASO(I),DTIP3(I),DH3(I),ASHD(I)
1,ASTD(I),DSH(I),MSH(I),BPSD(I),B3(I),C3(I),D3(I),E3(I)
22 CONTINUE
25 FORMAT(8F9.0)

C     *** END SECTION I

21 DO 24 I=1,NSLIM
    B2(I)=BO(I)
    ARR(I)=ARO(I)
24 ARS(I)=ASO(I)
    ITR=0
    ITS=0
    IIM=0
    IIR=0
    IID=0
    VZTIPI=VZTIPO
    CALL CHECK
    IF (IFLAG.GT.0) GO TO 350C
    CALL INITL
    IF (TFLAG.GT.0) GO TO 10

```

```

C     *** CALCULATE AT FIRST ROTOR INLET... WHEEL SPEED, THETA VELOCITY
C     *** ABSOLUTE VELOCITY, STATIC DENSITY, ABSOLUTE FLOW ANGLE,
C     *** RELATIVE FLOW ANGLE, RELATIVE VELOCITY, RELATIVE MACH NUMBER
C     *** SET TOTAL TEMPERATURE, CALCULATE ABSOLUTE MACH NUMBER,
C     *** AXIAL MACH NUMBER, AND SET TOTAL PRESSURE

CALL INLET
IF (IFLAG.GT.0) GO TO 10

C     *** TEST THE DUMP TRIGGER

101 IF (IPRI-1) 120,6000,6000
6000 CALL OUT1

C     *** THIS ENDS INLET COMPUTATIONS
C     *** NOW LET US START THE ROTOR EXIT COMPUTATIONS
C     *** START MAJOR DO LOOP CN NUMBER OF STAGES

120 DO 1000 I=1,NSLIM
    IOPT=1
    FACTOR=1.0

C     *** INITIALIZE LOOP COUNTERS

122 ITAL1=0
    ITAL2=0
    ITAL3=C
    ITAL7=0
    ITAL8=0

C     *** SET RAMP ANGLES TO ZERO

ALPRT= 0.
ALPRH= 0.
ALPST= 0.
ALPSH= 0.

C     *** SAVE INPUT ASPECT RATIOS AND B2

ARRI=ARR(I)
ARSI=ARS(I)
B2SAVE=B2(I)

C     *** START SECTION VI

C     *** IF DRT(I) (D-FACTOR) AT THE TIP IS NON-ZERO WE MUST
C     *** CALCULATE B2 IN THE POLYNOMIAL EXPRESSION OF WHIRL VELOCITY
C     *** B2/R+C2*D2*R+E2*R*R

130 IF ((ITAL2+ITAL3+ITAL8).GT.0) GO TO 140
    IF (DRT(I).EQ.0.) GO TO 140

C     *** COMPUTE AXIAL BLADE LENGTH (ROTOR)

BR= (RTIP1-RH1)/ARR(I)

C     *** CALCULATE TIP RADIUS AT ROTOR EXIT

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RTIP2= RTIP1+BR*SIN(ALPRT)/COS(ALPRT)
C      *** SET AXIAL VELOCITY AT TIP
VZTIP2= VZTIP1*VT2DT1(I)
C      *** CALCULATE TIP WHEEL SPEED F.P.S.
UTIP2= CON4*RTIP2
C      *** PREPARE TO CALCULATE COEFFICIENT OF 1/R IN WHIRL VELOCITY
C      *** POLYNOMIAL FROM D-FACTOR INITIAL

Q= V1P(I)*(1.-DRT(I))+(UTIP1-V01(I)-UTIP2)/(2.*SRTIP(I))
R= 1./(2.*SRTIP(I))
ER1= 1.-R*R
S= -2.*(UTIP2+Q*R)/ER1
T= (VZTIP2**2 + UTIP2**2 - Q*Q)/ER1
TEMP=S*S-4.*T
IF (TEMP.GE.0.) GO TO 8011
WRITE (6,8010)
8010 FORMAT(//104H WITH INPUT ROTOR INLET AND EXIT CONDITIONS, THE GIVE
IN DRT WOULD REQUIRE NEGATIVE TANGENTIAL VEL. AT TIP )
GO TO 3500
8011 VOTIP2= (-S - SQRT(TEMP))/2.

C      *** B2 IS THE COEFFICIENT OF 1/R
B2(I)=RTIP2*VOTIP2-C2(I)*RTIP2-D2(I)*RTIP2**2-E2(I)*RTIP2**3

C      *** END SECTION VI
C      *** TEST THE DUMP TRIGGER

132 IF (IPR1-1) 160,6030,6030
6030 CALL OUT3
GO TO 160

C      *** START SECTION VII
C      *** COMPUTE AXIAL BLADE LENGTH (ROTOR)

140 BR= (RTIP1-RH1)/ARR(I)

C      *** CALCULATE ROTOR EXIT TIP RADIUS
RTIP2= RTIP1+BR*SIN(ALPRT)/COS(ALPRT)

C      *** CALCULATE ROTOR EXIT TIP AXIAL VELOCITY
VZTIP2= VZTIP1*VT2DT1(I)

C      *** CALCULATE ROTOR EXIT TIP WHEEL SPEED
UTIP2= CON4*RTIP2

C      *** END SECTION VII

```

```

C     *** START SECTION VIII

160 VZ2(1)= VZTIP2

C     *** CALCULATE HUB RADIUS AT RCTCR EXIT

RH2= RH1 & ER*SIN(ALPRH)/CCS(ALPRH)

C     *** CALCULATE EFFECTIVE TIP AND HUB RADII

R2(1)=SQRT(ETIP2(1)*RTIP2**2&(1.-CTIP2(1))*RF2**2)
R2(N)=SQRT(CH2(1)*RF2**2&(1.-CH2(1))*RTIP2**2)

C     *** CALCULATE GEOMETRIC AREA AND EFFECTIVE AREA

A2G=3.1415926*(RTIP2**2-RF2*RF2)
A2E=3.1415926*(R2(1)**2-R2(N)**2)

C     *** CALCULATE TIP WHEEL SPEED

U2(1)= CCN4*R2(1)

C     *** CALCULATE TIP TANGENTIAL VELOCITY

VC2(1)= E2(1)/R2(1) & C2(1) & C2(1)*R2(1)&E2(1)*R2(1)**2

C     *** CALCULATE TIP RCTOR EXIT TOTAL TEMPERATURE

TT2(1)= TT1(1)&(U2(1)*VO2(1)-U1(1)*VO1(1))/CCN5

C     *** PREPARE TO CALCULATE CONSTANT IN THE AXIAL VELOCITY EQ. (K1)

ER1= 2.*E2(1)*C2(1)
ER2= 4.*E2(1)*C2(1)&2.*C2(1)**2
ER3= 6.*E2(1)*E2(1)&6.*C2(1)*C2(1)
ER4= 4.*C2(1)*E2(1)&2.*C2(1)**2
ER5= 10.*C2(1)*E2(1)/3.
ER6= 1.5*E2(1)**2
170 K2= VZTIP2**2-ER1/R2(1)&ER2*ALCG(R2(1)) & ER3*R2(1) & ER4*R2(1)**2
1 & ER5*R2(1)**3 & ER6*R2(1)**4 - CON1*TT2(1)

C     *** END SECTION VIII

C     *** START SECTION IX

180 ER7=(R2(1)-R2(N))/ANM1

C     *** DIVIDE FLOW PATH INTO EQUAL PARTS
C     *** CALCULATE INTERMEDIATE RADII, WHEEL SPEED, TANGENTIAL
C     *** VELOCITY, TOTAL TEMPERATURE, AND AXIAL VELOCITY AT EACH
C     *** STREAMLINE

CC 190 M=2,N
R2(M)= R2(M-1) - ER7
U2(M)= CCN4*R2(M)
VC2(M)= E2(1)/R2(M) & C2(1) & C2(1)*R2(M)&E2(1)*R2(M)**2
TT2(M)= TT1(M)&(U2(M)*VO2(M)-U1(M)*VO1(M))/CCN5
TEMP=ER1/R2(M)-ER2*ALCG(R2(M))-ER3*R2(M)-ER4*R2(M)**2-ER5*K2(M)**3

```

```

1-ER6*R2(M)**4+CON1*TT2(M)+K2
IF (TEMP.GE.0.) GO TO 190
WRITE (6,8015)
8016 FORMAT (//66H AXIAL VELOCITY IS NEGATIVE FOR SOME RADIAL LOCATION
1AT ROTOR EXIT )
GO TO 3500
190 VZ2(M)=SQRT(TEMP)

C      *** END SECTION IX

C      *** START SECTION X

C      *** CALCULATE AT ROTOR EXIT FOR ALL STREAMLINES ...
C      *** TOTAL PRESSURE, TOTAL DENSITY, ABSOLUTE VELOCITY, STATIC
C      *** DENSITY, ABSOLUTE FLOW ANGLE, RELATIVE FLOW ANGLE, RELATIVE
C      *** VELOCITY, ROTOR D-FACTOR, STATIC TEMPERATURE, STATIC
C      *** PRESSURE, SONIC VELOCITY, ABSOLUTE MACH NUMBER, OMEGA BAR,
C      *** LOSS FUNCTION, RELATIVE MACH NUMBER, AND AXIAL MACH NUMBER

DO 210 M=1,N
TEMP=TT2(M)/TT1(M)
IF (TEMP.GE.0.) GO TO 8019
WRITE (6,8018)
8018 FORMAT (//57H THE ABSOLUTE TOTAL TEMPERATURE AT ROTOR EXIT IS NEGA
TIVE )
GO TO 3500
8019 PT2(M)=PT1(M)*TEMP**NPR(I)*CON6
RHOT2(M)= PT2(M)*144./(RM*TT2(M))
V2(M)= SQRT(VZ2(M)**2 + VO2(M)**2)
TEMP=1.-V2(M)**2/(CON1*TT2(M))
IF (TEMP.GE.0.) GO TO 8021
WRITE (6,2020)
2020 FORMAT (//58H THE ABSOLUTE STATIC TEMPERATURE AT ROTOR EXIT IS NEG
ATIVE )
GO TO 3500
8021 RHOS2(M)=RHOT2(M)*TEMP**COGM1
BETA2(M)= ATAN(VO2(M)/VZ2(M))
BETA2P(M)=ATAN((U2(M)-VO2(M))/VZ2(M))
V2P(M)= VZ2(M)/COS(BETA2P(M))
DR(M)= 1.-V2P(M)/V1P(M) + (U1(M)-VO1(M)-U2(M)+VO2(M))/(2.*SRTIP(I)
1 *V1P(M)*(RTIP1+RTIP2)/(R1(M)+R2(M)))
TS2(M)= TT2(M) - V2(M)**2/CCN1
ATWD(M)= SQRT(CON3*TS2(M))
M2(M)= V2(M)/ATWD(M)
TEMP=1.+CON7*(1.-(R1(M)/R2(M))**2)*U2(M)**2/(CCN3*(TT1(M)+(V1P(M)*
1*2-V1(M)**2)/CON1))
IF (TEMP.GE.0.) GO TO 8023
WRITE (6,8022)
8022 FORMAT (//86H THE IDEAL RELATIVE TOTAL PRESSURE IN ROTOR OMEGA BAR
1 EQUATION IS NEGATIVE. BAD DATA. )
GO TO 3500
8023 PRI(M)=TEMP**CON6
WRB(M)= PRI(M)*(1.-PT2(M)/PT1(M)/(TT2(M)/TT1(M))**CON6)/(1. -
1 (1./((1.+CON7*M1P(M)**2)**2)**CON6)
M2P(M)= V2P(M)/ATWD(M)
M2Z(M)= VZ2(M)/ATWD(M)
210 ZR(M)=WRB(M)*COS(BETA2P(M))/(2.*SRTIP(I)*(RTIP1+RTIP2)/(R1(M) +
1 R2(M)))

```

```

C     *** END SECTION X

C     *** START SECTION XI

C     *** CALCULATE MASS FLOW

220 W2= C.
    GO 230 M=1,NM1
    RS2VZ2(M)= (RFCS2(M)*VZ2(M)*RHCS2(M&1)*VZ2(M&1))/2.
    ATC(M)= 3.1415926*(R2(M)**2-R2(M&1)**2)/144.
230 W2= W2 & RS2VZ2(M)*ATC(M)

C     *** END SECTION XI

C     *** RCTCR EXIT COMPUTATIONS ARE COMPLETED
C     *** PREPARE TO MAKE LIMIT CHECKS - PRIOR TO STATIC CALCULATIONS

C     *** START SECTION XII

EWAA= ABS(W2-W1)/W2

C     *** TEST FOR MASS FLOW BALANCE
C     *** IF MASS FLOW MATCHES GO TO 250

232 IF (EWAA.LE..CC1) GO TO 235

C     *** CHECK LOOP COUNT AND IF GREATER THAN OR EQUAL TO 50 PROCEED
C     *** TO NEXT DATA SET

IF (ITAL1.GE.50) GO TO 3000
ITAL1= ITAL1 + 1

C     *** TEST THE DUMP TRIGGER

IF (IPR1-1) 231,6050,EC50
6050 CALL CUT2
231 IF (ITR-1) 233,254,234

C     *** END SECTION XII

C     *** START SECTION XXIII

C     *** CALCULATE NEW EFFECTIVE AREA TO MATCH MASS FLOW

233 ANEW= A2E & (W1-W2)*A2E/W2

C     *** NEW TIP RADIUS

TEMP=RTIP2**2-ANEW/(3.1415927*(CH2(I)*CTIP2(I)-1.))
IF (TEMP.EE.C.) GO TO 8025
WRITE (6,EC24)
8024 FORMAT (//98H AREA REQUIRED TO MATCH MASS FLOW WITH GIVEN TIP RADI
IUS REQUIRES NEGATIVE HUB RADIUS AT RCTCR EXIT )
GO TO 3500
8025 RHNEW=SQRT(TEMP)

C     *** CALCULATE RCTCR HUB RAMP ANGLE

```

ALPRH= ATAN((RHNEW-RH1)/BR)
GO TO 160

C *** END SECTION XXIII

C *** START SECTION XXV

C *** CALCULATE NEW EFFECTIVE AREA

254 ANEH=A2E&(W1-W2)*A2E/W2

C *** CALCULATE NEW TIP RADIALS

RTNEW=SQRT(RH2**2&ANEH/(3.1415927*(DH2(I)&DTIP2(I)-1.)))

C *** CALCULATE NEW TIP RAMP ANGLE

ALPRT=ATAN((RTNEW-RTIP1)/ER)
GO TO 130

C *** END SECTION XXV

C *** CALCULATE NEW GEOMETRIC AREA

234 ANEH=A2G&(W1-W2)*A2G/W2

C *** CALCULATE NEW AXIAL LENGTH

TAARHL= SIN(ARTL(I))/CCS(ARTL(I))
IF (ABS(ARTL(I)) .NE. ABS(TAARHL)) GO TO 253

C *** START SECTION XXVII

BR=(RTIP1**2-RF1**2-ANEH/3.1415926)/(2.*TAARHL*(RTIP1*RH1))
GO TO 272

C *** END SECTION XXVII

C *** START SECTION XXVI

253 TAARTL= SIN(ARTL(I))/CCS(ARTL(I))
AE= TAARTL**2 - TAARHL**2
BE= (RTIP1*TAARTL - RF1*TAARHL)/AE
CE=(RTIP1**2-RF1**2-ANEH/3.1415926)/AE
BR= -EE & SQRT(BE**2 - CE)

C *** CALCULATE NEW ASPECT RATIO

272 ARR(I)=(RTIP1 - RF1)/ER
GO TO 130

C *** END SECTION XXVI

C *** START SECTION XXIV

235 IF (ITR-1) 236,237,250

C *** IF NEW RAMP ANGLE EXCEEDS ITS LIMIT SET IT TO THE LIMIT

236 IF (ALPRH.GT.ARHL(I)) GO TO 2332
GO TO 250

2332 ALPRH= ARHL(I)

ITR=1

WRITE (6,2333)

2333 FORMAT (1H030X43H*** ROTOR HUB RAMP ANGLE LIMIT VIOLATED *** /)
GO TO 160

C *** IF NEW RAMP ANGLE EXCEEDS ITS LIMIT SET IT TO THE LIMIT

237 IF (ALPRT.GE.ARTL(I)) GO TO 255

ALPRT=ARTL(I)

ITR=2

WRITE (6,2335)

2335 FORMAT (1H030X43H*** ROTOR TIP RAMP ANGLE LIMIT VIOLATED *** /)
GO TO 130

C *** ENSURE THAT THE TIP RAMP ANGLE IS NOT POSITIVE

255 IF (ALPRT.LE.0.) GO TO 250

WRITE (6,256)

256 FORMAT (// 45H ROTOR TIP RAMP ANGLE IS POSITIVE. BAD DATA)
GO TO 3500

C *** END SECTION XXIV

250 CALL MIDDLE

IGC=IGO

GO TO (360,140,300C,301C,3020,3500),IGO

360 ITAL7=0

ITS=0

C *** CHECK HUB D-FACTOR AGAINST ITS LIMIT

C *** RECALCULATE 1/R COEFFICIENT TO MEET D-FACTOR TEST

IF (IOPT.EQ.0) GO TO 420

DF3=DS(N)-DSH(I)

IF (DF3) 285,500,391

C *** START SECTION XX (CONTINUED AT ST. 421)

420 IF (DS(N).LE.DSH(I)) GO TO 500

GO TO 421

285 IF (ITAL8.EQ.0) GO TO 500

IF (ABS(DF3/DSH(I)).LE..001) GO TO 392

DFL3=DF3

BL3=B2(I)

```
IID=1  
387 B2(I)=BH3-DFH3*(BH3-BL3)/(DFH3-DFL3)  
389 ITAL8=ITAL8+1
```

C *** CHECK LOOP COUNT

```
IF (ITAL8.GE.50) GO TO 3030  
ALPRH=0.0  
ALPRT=0.0  
ARR(I)=ARRI  
ALPSH=0.  
ALPST=C.  
ARS(I)=ARSI  
GO TO 368  
391 IF (ITAL8.EQ.0) GO TO 390  
IF (ABS(DF3/DSH(I)).LE..001) GO TO 392  
DFH3=DF3  
BH3=B2(I)  
IF (IID.GT.0) GO TO 387  
B2(I)=CH3*B2(I)  
GO TO 389  
390 DFH3=DF3  
BH3=B2(I)
```

C *** SECTION XX (CONTINUED)

```
421 WRITE (6,2355)  
2355 FORMAT (1H03UX42H*** STATOR HUB D FACTOR LIMIT VIOLATED *** / )
```

C *** CHECK LOOP COUNT

```
IF (ITAL8.GE.50) GO TO 3030  
ITAL8= ITAL8 + 1
```

C *** IF THE STATOR HUB D FACTOR LIMIT IS 1., THE ABSOLUTE
C *** VELOCITY AT THE STATOR EXIT MAY BE CALCULATED DIRECTLY.
C *** THE EQUATIONS USED OTHERWISE MAY INTRODUCE EXTRANEOUS ROOTS
C *** WHICH WILL BE DEALT WITH BY THE PROGRAM.

```
IF (DSH(I).NE.1.) GO TO 425  
V02(N)=2.*SSH(I)*V3(N)+V03(N)  
GO TO 440  
425 AF= (-V3(N)-V03(N)/(2.*SSH(I)))/(DSH(I)-1.)  
BF= 1./((DSH(I)-1.)*2.*SSH(I))  
CF= -AF*BF/(1.-BF*BF)  
DF= (V02(N)**2-AF*AF)/(1.-BF*BF)  
TEMP=CF*CF-DF  
IF (TEMP.GE.0.) GO TO 8039  
WRITE (6,8038)  
8038 FORMAT (// 96H IN CORRECTING FOR EXCESSIVE STATOR HUB D-FACTOR, SO  
1UARE ROOT OF NEGATIVE NUMBER WAS ENCOUNTERED )  
GO TO 3500
```

C *** CALCULATE BOTH ROOTS

```
8039 V02(N)=-CF+SQRT(TEMP)  
V02SV=-CF-SQRT(TEMP)  
IF (V02(N).GE.0.) GO TO 433
```

C *** THE FIRST ROOT IS NEGATIVE. USE THE SECOND ROOT IF POSITIVE
 IF (V02SV.GE.0.) GO TO 437
 C *** BOTH ROOTS WERE NEGATIVE
 WRITE (6,8040)
 8040 FORMAT (// 62H NO POSITIVE ROOTS FOUND FOR STATOR ABSOLUTE VELOCITY
 EQUATION)
 GO TO 3500

C *** THE FIRST ROOT IS POSITIVE. IF THE SECOND ROOT IS NEGATIVE
 C *** USE THE FIRST

433 IF (V02SV.LT.0.) GO TO 440

C *** BOTH ROOTS WERE POSITIVE. DETERMINE WHICH SATISFIES THE
 C *** D FACTOR EQUATION

```

SR00T=SQRT(V02(N)**2+VZ2(N)**2)
TRY1=1.-V3(N)/SR00T-(V03(N)-V02(N))/(2.*SSH(I)*SR00T)
SR00T=SQRT(V02SV**2+VZ2(N)**2)
TRY2=1.-V3(N)/SR00T-(V03(N)-V02SV)/(2.*SSH(I)*SR00T)
IF (ABS(TRY1-DSH(I))/DSH(I).GT..01)    GO TO 434
  
```

C *** THE FIRST ROOT SATISFIED THE D FACTOR EQUATION. IF THE
 C *** SECOND DOES NOT, USE THE FIRST

IF (ABS(TRY2-DSH(I))/DSH(I).GT..01) GO TO 440

C *** BOTH ROOTS SATISFIED THE D FACTOR EQUATION. USE THE SMALLER

IF (V02(N)-V02SV) 440,440,437

C *** THE FIRST ROOT DID NOT SATISFY THE D FACTOR EQUATION.
 C *** IF THE SECOND DOES, USE IT

434 IF (ABS(TRY2-DSH(I))/DSH(I).LE..01) GO TO 437

C *** NEITHER ROOT SATISFIED THE D FACTOR EQUATION

WRITE (6,435)

```

435 FORMAT (// 69H NEITHER POSITIVE ROOT WOULD SATISFY THE STATOR HUB  

D FACTOR EQUATION )  

GO TO 3500
  
```

C *** USE THE SECOND ROOT

437 V02(N)=V02SV
 440 B2(I)=R2(N)*V02(N)-C2(I)*R2(N)-D2(I)*R2(N)**2-E2(I)*R2(N)**3

C *** END SECTION XX

```

ALPRH=0.  

ALPRT=0.  

ALPSH=0.  

ALPST=0.
  
```

```

ARS(I)=ARSI
ARR(I)=ARRI
IF (INOPT.EQ.0) GO TO 368
CH3= .95
IF (RH3.GT.B2(I)) GO TO 368
CH3= 1.05

C      *** TEST THE DUMP TRIGGER

368 IF ((IPR1-1) 140,6150,6150
6150 CALL OUT7
GO TO 140
392 DS(N)=DSH(I)

C      *** START SECTION XXI (CONTINUED IN OUTPUT S.R.)

500 CALL OUTPUT
IID=0
IF((RC0-RCLIM).LT.0.) GO TO 501
WRITE (6,502)
502 FORMAT (1H024X71H*** OVERALL PRESSURE RATIO LIMIT HAS BEEN REACHED
1 -- GO TO NEW DATA *** // )
GO TO 10
501 IF ((I-NSLIM).LT.0) GO TO 540
WRITE (6,504)
504 FORMAT (1H020X81H*** NUMBER OF STAGES FOR THIS DATA SET HAS BEEN R
EACHED -- GO TO NEW DATA SET *** // )
GO TO 10

C      *** END SECTION XXI

C      *** START SECTION XXII

C      *** PUT STATOR EXIT PARAMETERS INTO ROTOR INLET FOR NEXT STAGE

540 DO 550 M=1,N
U1(M)=UTIP1*I*R3(M)/RTIP1I
VO1(M)= VO3(M)
V1(M)= V3(M)
BETA1(M)= BETA3(M)
BETA1P(M)= ATAN((U1(M)-VO1(M))/VZ3(M))
V1P(M)= VZ3(M)/COS(BETA1P(M))
VZ1(M)= VZ3(M)
R1(M)= R3(M)
AONE(M)= SQRT(CON3*TT3(M)-V1(M)**2/CON1)
M1P(M)=V1P(M)/AONE(M)
TT1(M)= TT3(M)
M1(M)= V1(M)/AONE(M)
MZ1(M)= VZ1(M)/AONE(M)
550 PT1(M)= PT3(M)
RTIP1= RTIP3
RH1= RH3
VZTIP1= VZTIP3
UTIP1= U1(1)
WRITE (6,2360)
2360 FORMAT (1H1)
1000 CONTINUE

```

C *** PROGRAM COMPLETED CURRENT STAGE - OFF TO ANOTHER STAGE

GO TO 10

C *** END SECTION XXII

3000 WRITE (6,3001)

3001 FORMAT (1H05X105H*** ERROR MESSAGE *** ITERATION COUNT EXCEEDED 50
10 ON FLOW LOSS GREATER THAN .001 TEST, GO TO NEXT DATA SET //)
GO TO 3500

3010 IF (IOPT.EQ.1) GO TO 3600
WRITE (6,3011)

3011 FORMAT (1H0 5X 92H*** ERROR MESSAGE *** ITERATION COUNT EXCEEDED 5
10 ON MACH NO. LIMIT TEST, GO TO NEW DATA SET //)
GO TO 3500

3020 IF (IOPT.EQ.1) GO TO 3600
WRITE (6,3021)

3021 FORMAT (1H0 5X 93H*** ERROR MESSAGE *** ITERATION COUNT EXCEEDED 5
10 ON AIR ANGLE LIMIT TEST, GO TO NEW DATA SET //)
GO TO 3500

3030 IF (IOPT.EQ.1) GO TO 3600
WRITE (6,3031)

3031 FORMAT (1H0 5X100H*** ERROR MESSAGE *** ITERATION COUNT EXCEEDED 5
10 ON DIFFUSION FACTOR LIMIT TEST, GO TO NEW DATA SET //)

3500 IERROR=1
CALL OUTPUT
GO TO 10

3600 FACTOR=.998
ARR(I)=ARRI
ARS(I)=ARSI
B2(I)=B2SAVE
WRITE (6,3601) I

3601 FORMAT (//1X36(1H*),3X5HSTAGE13,33H IS NOT THE OPTIMUM CONFIGURAT
1ION 3X36(1H*) //)
IOPT=0
GO TO 122
END

```

$IRFTC INITL DD,NOLIST
C      *** INITL SUBROUTINE
      SUBROUTINE INITL
      REAL MW,NPR,NPS,MSH,K1,M1P,K2,M2,K3
      REAL M1,MZ1,M2P,MZ2,M3,MZ3
      DIMENSION M1(11),MZ1(11),M2P(11),MZ2(11),M3(11),MZ3(11),A3(11)
      DIMENSION VT2OT1(50),NPR(50),SRTIP(50),ARR(50),DTIP2(50),DH2(50),
1ARHL(50),ARTL(50),DRT(50),B2(50),C2(50),D2(50),E2(50),VT3OT2(50),
2NPS(50),SSH(50),ARS(50),DTIP3(50),DH3(50),ASHL(50),ASTL(50),
3DSH(50),MSH(50),BPSH(50),B3(50),C3(50),D3(50),E3(50)
      DIMENSION VZ1(11),U1(11),VO1(11),RHOS1(11),BETA1P(11),BETA1P(11),
1V1P(11),M1P(11),TT1(11),PT1(11),RS1VZ1(11),AONE(11),R2(11),U2(11),
2VO2(11),TT2(11),VZ2(11),PT2(11),RHOT2(11),V2(11),RHOS2(11),
3BETA2(11),BETA2P(11),V2P(11),DR(11),TS2(11),ATWO(11),M2(11),
4PRI(11),WRB(11),ZR(11),RS2VZ2(11),ATO(11),TT3(11),R3(11),VO3(11),
5PT3(11),RHOT3(11),V3(11),RHOS3(11),BETA3(11),DS(11),WSB(11),
6ZS(11),RS3VZ3(11),ATHRE(11),WW3(11)
      DIMENSION R1(11),V1(11),VZ3(11)
      DIMENSION ARHD(50),ARTD(50),ASHD(50),ASTD(50),BET1D(11),BET1PD(11),
1,BET2D(11),BET2PD(11),BET3D(11),BPSD(50),TITL(12)
      DIMENSION BO(50),AP0(50),ASC(50)
      COMMON /SINITL/CONS,CP,DH1,DTIP1,ER1,ER2,ER3,ER4,ER5,ER6,ER7,GAM,
1MW,RCLIM,RHORT1,RTIP1I,TEMP,UTIP1I,VZTIP1
      COMMON /CHEC/IFLAG,NSLIM
      COMMON /COM2/PTI,TTI,CON1,CON2,CON3,CON4,ODGM1,B1,C1,D1,E1
      COMMON /COM3/IGO,ITS,ITR,IOPT,IIB,IID,IIM,FACTOR,ANM1,CON6,CON7,
1CON8,ITAL7
      COMMON I,INC,IPR2,N,VT2OT1,NPR,SRTIP,ARRI,DTIP2,DH2,ARHD,ARTD,DRT,
1B2SAVE,C2,D2,E2,VT3OT2,NPS,SSH,ARSI,DTIP3,DH3,ASHD,ASTD,DSH,MSH,
2BPSD,B3,C3,D3,E3,W1,RCC,TRO,FTA0,RC,TR,ETA,RTIP1,ARR,ARS,RH1,RTIP2
3,RH2,RTIP3,RH3,BR,BS,M,BET1D,BETA1,BET1PD,BETA1P,R1,U1,VZ1,VO1,V1,
4V1P,M1P,M1,MZ1,BET2D,BETA2,BET2PD,BETA2P,R2,U2,VZ2,VO2,V2,V2P,DR,
5M2P,M2,MZ2,BET3D,BETA3,R3,VZ3,VO3,V3,DS,M3,WRB,ZR,WSB,ZS,MZ3,ALPST
6,ALPSH,IERROR
      COMMON IPR1,K1,UTIP1,RM,RHOT1,AGNE,RS1VZ1,NM1,RHOS1,TT1,PT1,W2,
1EWA,VZTIP2,A2G,A2E,K2,ITAL1,ALPRH,RHNEW,ANEW,TAARTL,TAARHL,AE,BE,
2CE,ALPRT,RTNEW,B2,TT2,PT2,RHOT2,RHCS2,TS2,ATWC,PRI,ATO,RS2VZ2
3,UTIP2,VOTIP2,Q,R,S,T,ITAL2,AA,BB,CC,DD,ITAL3,BPSH,W3,A3G,A3E,PT3,
4VZTIP3,K3,PRW3,PROW3,TRW3,TROW3,TT3,RHOS3,TAASHL,TAASTL,ASHL,ASTL,
5A3,ATHRE,RS3VZ3,WW3,ITAL8,AF,BF,CF,DF
6,VZTIPO,ARHL,ARTL,RHOT3,TITL,BO,ARC,ASO

```

C *** WRITE OUT INPUT DATA

```

      WRITE (6,2000)
2000 FORMAT(1H020X80H***** PARAMETRIC STUDY OF ADVANCED MULTISTAGE A
1XIAL-FLOW COMPRESSORS ***** // /35X50H*** R O T O R I N L E
2T I N P U T D A T A *** // )
      WRITE (6,2010) N,NSLIM,CP,MW,GAM,TTI,PTI,RCLIM,RTIP1I,UTIP1I,
1 RHORT1,VZTIP1,DTIP1,DH1,B1,C1,D1,E1
2010 FORMAT (/3X8HNO. RAD.8X6HNUMBER8X8HSP. HEAT8X8HMOL. WT.6X8HRATIO 0
1F4X45HIN. TOT. TEMP. IN. TCT. PR. MASS AVG. TOT./3X8HSTATIONS8X
26HSTAGES6X12H(BTU/(LB-R))6X7H(MOLES)7X8HSP. HEAT7X8H(DEG. R)9X5H(P
3SI)8X9HPR. RATIO //18,I15,F17.4,F16.4,F14.4,F16.4,F15.4,F14.4// 1
47X40HTIP RADIUS TIP WHEEL SPEED HUB TO TIP5X10HAXIAL VEL.4X27HT
5IP BLOCKAGE HUB BLOCKAGE/18X8H(INCHES)7X8H(FT/SEC)5X12HRADIUS RA
6T105X8H(FT/SEC)8X6HFACTOR9X6HFACTOR // F26.4,F16.4,F13.4,F16.4,F14
7.4,F15.4 // 38X44HCOEFFICIENTS IN TANGENTIAL VELOCITY EQUATION //

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```

837X1HE14X1HC14X1HC14X1HE // 27X4F15.4 /// 1X118(1H*) // )
IF (N.LE.11) GO TC 28
WRITE (6,27)
27 FORMAT (//56F HAVE CONSIDERED MORE THAN 10 FLOW CHANNELS. CHECK DATA )
1ATA )
GO TC 1C
28 IF (NSLIM.LE.5C) GO TC 30
WRITE (6,29)
29 FORMAT (// 49F HAVE CONSIDERED MORE THAN 50 STAGES. CHECK DATA )
GO TC 1C

C      *** START SECTION II

C      *** SET TIP EQUAL TO INITIAL TIP RADIALS

30 RTIP1= RTIP1I

C      *** CALCULATE GAS CONSTANT

RM= 1545.4/MW
AN= N
NM1= N-1
ANM1=NM1
33 I=1,NSLIM

C      *** CHANGE DEGREES TO RADIANS

ARHL(I)=ARFC(I)*.C174533
BPSH(I)=BPSC(I)*.C174533
ARTL(I)=ARTC(I)*.C174533
ASHL(I)=ASFC(I)*.C174533
33 ASTL(I)=ASTC(I)*.C174533

C      *** CALCULATE TOTAL DENSITY

RHCT1=PTI*144./(RM*TTI)

C      *** CALCULATE RADIUS OF HUB STREAMLINE

RH1= RTIP1*RHCT1

C      *** CALCULATE RADIUS OF HUB AND TIP STREAMLINES

WRITE (6,233C)
2330 FORMAT (1F1)
IF (CTIP1.GT.C.) GO TC 80C1
WRITE (6,80C1)
8000 FORMAT (//52H TIP BLOCKAGE FACTOR NOT POSITIVE AT INLET. BAD DATA)
GO TO 1C
8001 R1(1)=SQRT(CTIP1*RTIP1**2*(1.-CTIP1)*RH1**2)
IF (DH1.GT.C.) GO TO 80C3
WRITE (6,80C2)
8002 FORMAT (//52H HUB BLOCKAGE FACTOR NOT POSITIVE AT INLET BAD DATA)
GO TC 1C
8003 R1(N)=SQRT(DH1*RH1**2*(1.-DH1)*RTIP1**2)

C      *** CALCULATE COEFFICIENTS IN THE AXIAL VELOCITY EQUATION

```

```

ER1= 2.*B1*C1
ER2= 4.*B1*D1+2.*C1*C1
ER3= 6.*B1*E1+6.*C1*D1
ER4= 4.*C1*E1+2.*D1*D1
ER5=10.*D1*E1/3.
ER6=1.5*E1*E1

C      *** SET WHEEL TIP SPEED

UTIP1=UTIP1I

C      *** CALCULATE CONSTANT OF INTEGRATION

K1= VZTIP1**2-ER1/ R1(1)+ER2*ALOG(R1(1))+ER3*R1(1)+ER4*R1(1)**2 +
1 ER5*R1(1)**3 + ER6*R1(1)**4

C      *** SET AXIAL VELOCITY AT THE TIP = TO INITIAL AXIAL VELOCITY

40 VZ1(1)= VZTIP1

C      *** END SECTION II

C      *** START SECTION III

50 ER7= (R1(1)-R1(N))/ANM1
DO 60 M=2,N

C      *** CALCULATE STREAMLINE RADII

R1(M)= R1(M-1) - ER7

C      *** CALCULATE AXIAL VELOCITY AT EACH RADIUS

TEMP = (ER1/R1(M)-ER2*ALOG(R1(M))-ER3*R1(M) - ER4*R1(M)**2 -
1 ER5*R1(M)**3 - ER6*R1(M)**4 + K1)
IF (TEMP.GE.0.) GO TO 8005
WRITE (6,8004)

8004 FORMAT (//61H AXIAL VELOCITY IS NEGATIVE FOR SOME RADIAL LOCATION
1AT INLET )
GO TO 10
8005 VZ1(M)=TEMP**.5
60 CONTINUE

C      *** END SECTION III

C      *** CALCULATE CONSTANTS

OOGM1= 1./(GAM-1.)
CON1= 50056.*CP
CON2= CON1*TTI
CON3= 32.174*GAM*RM
CON4= UTIP1I/RTIP1I
CON5= .5*CON1
CON6= GAM/(GAM-1.)
CON7= (GAM-1.)/2.
CON8= (GAM-1.)/GAM
RETURN
10 IFLAG=1

```

**RETURN
END**

```

$IBFTC MIDDLE DD,NOLIST
C      *** MIDDLE SUBROUTINE
      SUBROUTINE MIDDLE
      REAL MW,NPR,NPS,MSH,K1,M1P,K2,M2,K3
      REAL M1,MZ1,M2P,M72,M3,M73
      DIMENSION M1(11),MZ1(11),M2P(11),MZ2(11),M3(11),MZ3(11),A3(11)
      DIMENSION VT20T1(50),NPR(50),SRTIP(50),ARR(50),DTIP2(50),DH2(50),
1ARHL(50),ARTL(50),DRT(50),B2(50),C2(50),D2(50),E2(50),VT30T2(50),
2NPS(50),SSH(50),ARS(50),DTIP3(50),DH3(50),ASHL(50),ASTL(50),
3DSH(50),MSH(50),BPSH(50),B3(50),C3(50),D3(50),E3(50)
      DIMENSION VZ1(11),U1(11),VC1(11),RHCS1(11),BETA1(11),BETA1P(11),
1V1P(11),M1P(11),TT1(11),PT1(11),RS1VZ1(11),ACNE(11),R2(11),U2(11),
2V02(11),TT2(11),VZ2(11),PT2(11),RHOT2(11),V2(11),RHOS2(11),
3BETA2(11),BETA2P(11),V2P(11),DR(11),TS2(11),ATWD(11),M2(11),
4PRI(11),WRB(11),ZR(11),RS2VZ2(11),ATO(11),TT3(11),R3(11),V03(11),
5PT3(11),RHOT3(11),V3(11),RHCS3(11),BETA3(11),DS(11),WSB(11),
6ZS(11),RS3VZ3(11),ATHRE(11),WW3(11)
      DIMENSION R1(11),V1(11),VZ3(11)
      DIMENSION ARHD(50),ARTD(50),ASHD(50),ASTD(50),BET1D(11),BET1PD(11)
1,BET2D(11),BET2PD(11),BET3D(11),BPSD(50),TITL(12)
      DIMENSION BO(50),RD(50),ASC(50)
      COMMON /CHEC/IFLAG,NSLIM
      COMMON /COM2/PTI,TT1,CON1,CON2,CON3,CON4,COGM1,B1,C1,D1,E1
      COMMON /COM3/IGO,ITS,ITR,ICPT,IIB,IID,IIM,FACTOR,ANM1,CON6,CON7,
1CCN8,ITAL7
      COMMON I,INC,IPR2,N,VT20T1,NPR,SRTIP,ARRI,DTIP2,DH2,ARHD,ARTD,DRT,
1P2SAVE,C2,D2,E2,VT30T2,NPS,SSH,ARSI,DTIP3,DH3,ASHD,ASTD,DSH,MSH,
2BPSD,B3,C3,D3,E3,W1,RCD,TR0,ETA0,RC,TR,ETA,RTIP1,ARR,ARS,RH1,RTIP2
3,RH2,RTIP3,RH3,BR,RS,M,BET1D,BETA1,BET1PD,BETA1P,R1,U1,VZ1,V01,V1,
4V1P,M1P,M1,MZ1,BET2D,BETA2,BET2PD,BETA2P,R2,U2,VZ2,V02,V2,V2P,DR,
5M2P,M2,MZ2,BET3D,BETA3,R3,VZ3,V03,V3,DS,W3,WRB,ZR,WSB,ZS,MZ3,ALPST
6,ALPSH,IERROR
      COMMON IPR1,K1,UTIP1,RM,RHOT1,AONE,RS1VZ1,NM1,RHOS1,TT1,PT1,W2,
1EWA,VZTIP2,A2G,A2F,K2,ITAL1,ALPRH,RHNEW,ANEW,TAARTL,TAARHL,AE,BE,
2CE,ALPRT,RTNEW,B2,TT2,PT2,RHOT2,RHOS2,TS2,ATWD,PRI,ATC,RS2VZ2
3,UTIP2,VOTIP2,Q,R,S,T,ITAL2,AA,BB,CC,DD,ITAL3,BPSH,W3,A3G,A3E,PT3,
4VZTIP3,K3,PRW3,PRW3,TRW3,TROW3,TT3,RHOS3,TAASHL,TAASTL,ASHL,ASTL,
5A3,ATHRE,RS3VZ3,WW3,ITAL8,AF,BF,CF,DF
6,VZTIP0,ARHL,ARTL,RHOT3,TITL,BO,ARC,ASO
250 ITAL1 = 0
      I=I
      N=N
      NM1=NM1
      IGO=1
      ITR=0

C      *** ALTER THE COEFFICIENT OF I/R IN THE TANGENTIAL VELOCITY
C      *** POLYNOMIAL TO SATISFY MACH NUMBER LIMIT

      IF (IOPT.EQ.0) GO TO 400
      DF1=M2(N)-MSH(I)
      IF (DF1) 283,260,251

C      *** START SECTION XIII (CONTINUED AT ST. 401)

400 IF (M2(N).LE.MSH(I)) GO TO 260
      GO TO 401
283 IF (ITAL2.EQ.0) GO TO 260

```

```
IF (ABS(DF1/MSH(I)).LE..001) GO TO 252
DFL1=DF1
BL1=B2(I)
IIM=1
257 B2(I)=BH1-DFH1*(BH1-BL1)/(DFH1-DFL1)
259 ITAL2=ITAL2+1
```

C *** CHECK LOOP COUNT

```
IF (ITAL2.GE.50) GO TO 3010
ALPRH=0.0
ALPRT=0.0
ARR(I)=ARRI
GO TO 258
251 IF (ITAL2.EQ.0) GO TO 280
IF (ABS(DF1/MSH(I)).LF..001) GO TO 252
DFH1=DF1
BH1=B2(I)
IF(IIM.GT.0) GO TO 257
B2(I)=CH1*B2(I)
GO TO 259
280 DFL1=DF1
BH1=B2(I)
```

C *** SECTION XIII (CONTINUED)

```
401 WRITE (6,2337)
2337 FORMAT (1H030X42H*** STATOR HUB MACH NO. LIMIT VIOLATED *** / )
```

C *** CHECK LOOP COUNT

```
IF (ITAL2.GE.50) GO TO 3010
ITAL2= ITAL2 + 1
AA=MSH(I)**2*CON3*FACTOR
BB= AA/CON1
CC= -BB*U2(N)/(1.+BB)
DD= (VZ2(N)**2*(1.+BB)-AA*TT1(N)+2.*BB*U1(N)*VC1(N))/(1.+BB)
TEMP=CC**2-DD
IF (TEMP.GE.0.) GO TO 8027
WRITE (6,8026)
8026 FORMAT(//106H IN CORRECTING FOR EXCESSIVE HUB MACH NUMBER AT ROTOR
1 EXIT, SQUARE ROOT OF NEGATIVE NUMBER WAS ENCOUNTERED )
GO TO 3500
8027 VO2(N)=-CC+SQRT(TEMP)
B2(I)=R2(N)*VO2(N)-C2(I)*R2(N)-D2(I)*R2(N)**2-E2(I)*R2(N)**3
ALPRH=0.
ALPRT=0.
ARR(I)=ARRI
IF (INPT.EQ.0) GO TO 258
CH1 = 0.95
IF (BF1.GT.B2(I)) GO TO 258
CH1 = 1.05
```

C *** TEST THE DUMP TRIGGER

```
258 IF (IPR1-1) 140,6070,6070
6070 CALL OUT4
GO TO 140
```

```

C      *** END SECTION XIII

252 M2(N)=MSH(I)
260 ITAL2= 0
   IIM=0

C      *** CHECK RELATIVE FLOW ANGLE.  IF LESS THAN THE LIMIT, ALTER
C      *** THE COEFFICIENT OF 1/R IN THE TANGENTIAL VELOCITY POLYNOMIAL

IF (IOPT.EQ.0) GO TO 410
DF2=BETA2P(N)-BPSH(I)
IF (DF2) 281,299,284

C      *** START SECTION XIV (CONTINUED AT ST. 411)

410 IF (BETA2P(N).GE.BPSH(I)) GO TO 299
   GO TO 411
284 IF (ITAL3.EQ.0) GO TO 299
   IF (ABS(DF2/BPSH(I)).LE..001) GO TO 282
   DFL2=DF2
   BL2=B2(I)
   IIB=1
287 B2(I)=BH2-DFH2*(BH2-BL2)/(DFH2-DFL2)
289 ITAL3=ITAL3+1

C      *** CHECK LOOP COUNT

IF (ITAL3.GE.50) GO TO 3020
ALPRH=0.0
ALPRT=0.0
ARR(I)=ARRI
GO TO 268
281 IF (ITAL3.EQ.0) GO TO 290
   IF (ABS(DF2/BPSH(I)).LE..001) GO TO 282
   DFH2=DF2
   BH2=R2(I)
   IF (IIB.GT.0) GOTO 287
   B2(I)=CH2*R2(I)
   GO TO 289
290 DFL2=DF2
   BH2=B2(I)

C      *** SECTION XIV (CONTINUED)

411 WRITE (6,234)
2340 FORMAT (1H030X47H*** ROTOR HUB RELATIVE ANGLE LIMIT VIOLATED ***/)

C      *** CHECK LOOP COUNT

IF (ITAL3.GE.50) GO TO 3020
ITAL3= ITAL3 + 1
B2(I)=(U2(N)-VZ2(N)*SIN(BPSH(I))/COS(BPSH(I)))*R2(N)-C2(I)*R2(N)-
1D2(I)**2-E2(I)*R2(N)**3
ALPRH=0.
ALPRT=0.
ARR(I)=ARRI
IF (IOPT.EQ.0) GO TO 268

```

```

CH2=0.95
IF (BF2.GT.B2(I)) GO TO 268
CH2=1.05

C      *** TEST THE DUMP TRIGGER

268 IF (IPRI-1) 140,6C8C,6C8C
6080 CALL CUT5
GO TO 140

C      *** END SECTION XIV

282 BETA2P(N)=BPSH(I)

C      *** START SECTION XV

C      *** WE HAVE SATISFIED ALL TESTS - OFF TO STATOR CALCULATIONS
C      *** BEGIN STATOR EXIT COMPUTATIONS
C      *** RESET LCCP COUNTERS

299 ITAL3=0
IIE=0

C      *** CALCULATE BLADE AXIAL LENGTH

300 ES=(RTIP2 - RF2)/ARS(I)

C      *** CALCULATE STATOR EXIT TIP RADIUS
RTIP3= RTIP2 & ES*SIN(ALPST)/COS(ALPST)

C      *** SET TOTAL TEMPERATURE AT THE TIP
TT3(I)= TT2(I)

C      *** CALCULATE STATION EXIT FLOW RADIUS
RF3= RF2 & ES*SIN(ALPSH)/COS(ALPSH)

C      *** CALCULATE TIP AND FLOW STREAMLINE RADII
R3(I)=SQRT(CTIP3(I)*RTIP3**2*(1.-CTIP3(I))*RF3**2)
R3(N)=SQRT(CH3(I)*RF3**2*(1.-CH3(I))*RTIP3**2)

C      *** CALCULATE GEOMETRIC AREA OF STATOR EXIT
A3G= 3.1415926*(RTIP3**2 - RF3**2)

C      *** CALCULATE EFFECTIVE AREA OF STATOR EXIT
A3E= 3.1415926*(R3(I)**2 - R3(N)**2)

C      *** CALCULATE DESIRED AXIAL VELOCITY AT THE TIP
VZTIP3= VZTIP2*VT2CT2(I)
ER1= 2.*B3(I)*C3(I)
ER2= 4.*E3(I)*C3(I)&2.*C3(I)**2
ER3= 6.*B3(I)*E3(I)&6.*C3(I)*C3(I)

```

```

ER4= 4.*C3(I)*E3(I)+2.*D3(I)**2
ER5= 10.*D3(I)*E3(I)/3.
ER6= 1.5*E3(I)**2

C      *** CALCULATE CONSTANT OF INTEGRATION

      K3= VZTIP3**2 - ER1/R3(1) + ER2*ALOG(R3(1)) + ER3*R3(1) + ER4*
      1 R3(1)**2 + ER5*R3(1)**3 + ER6*R3(1)**4 - CON1*TT3(1)

C      *** SET AXIAL VELOCITY AT THE TIP

302 VZ3(1)= VZTIP3

C      *** END SECTION XV

C      *** START SECTION XVI

      ER7= (R3(1)-R3(N))/ANM1
      DO 310 M=2,N

C      *** GET STREAMLINE RADII

      R3(M)= R3(M-1)-ER7

C      *** SET TOTAL TEMPERATURE AT EACH STREAMLINE

      TT3(M)= TT2(M)

C      *** CALCULATE AXIAL VELOCITY AT EACH STREAMLINE

      TEMP=ER1/R3(M)-ER2*ALOG(R3(M))-ER3*R3(M)-ER4*R3(M)**2-ER5*R3(M)**3
      1-ER6*R3(M)**4+CON1*TT3(M)+K3
      IF (TEMP.GE.0.) GO TO 310
      WRITE (6,8032)
8032 FORMAT (/6TH AXIAL VELOCITY IS NEGATIVE FOR SOME RADIAL LOCATION
      1AT STATOR EXIT )
      GO TO 3500
      310 VZ3(M)=SQRT(TEMP)

C      *** END SECTION XVI

C      *** START SECTION XVII

C      *** CALCULATE WHIRL VELOCITY, ABSOLUTE VELOCITY, STATIC
C      *** TEMPERATURE, STATIC PRESSURE, TOTAL PRESSURE, STATIC
C      *** DENSITY, ABSOLUTE FLOW ANGLE, D-FACTOR, OMEGA BAR, SONIC
C      *** VELOCITY, ABSOLUTE MACH NUMBER, AXIAL MACH NUMBER, AND
C      *** LOSS FACTOR

      DO 320 M=1,N
      VD3(M)= B3(I)/R3(M) + C3(I) + D3(I)*R3(M)+E3(I)*R3(M)**2
      TEMP=TT3(M)/TT1(M)
      IF (TEMP.GE.0.) GO TO 8051
      WRITE (6,8050)
8050 FORMAT (/58H THE ABSOLUTE TOTAL TEMPERATURE AT STATOR EXIT IS NEG
      1ATIVE )
      GO TO 3500
      8051 PT3(M)=PT1(M)*TEMP***(NPS(I)*CON6)

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RHOT3(M)=PT3(M)*144./IRM*TT3(M))
V3(M)= SQRT(VZ3(M)**2 + VO3(M)**2)
TEMP=1.-V3(M)**2/(CON1*TT3(M))
IF (TEMP.GE.0.) GO TO 8053
WRITE (6,8052)
8052 FORMAT (//59H THE ABSOLUTE STATIC TEMPERATURE AT STATOR EXIT IS NE
1GATIVE )
GO TO 3500
8053 RHOS3(M)=RHOT3(M)*TEMP**00GM1
BETA3(M)= ATAN(VO3(M)/VZ3(M))
DS(M)= 1.-V3(M)/V2(M) + (VO2(M)-VO3(M))/(2.*SSH(I)*V2(M)*(R2(N)+
1R3(N))/(R2(M)+R3(M)))
WSB(M)= (1.-PT3(M)/PT2(M))/(1.-(1./(1.+CON7*M2(M)**2))**CON6)
A3(M)= SQRT(CON3*(TT3(M)-V3(M)**2/CON1))
M3(M)= V3(M)/A3(M)
MZ3(M)= VZ3(M)/A3(M)
320 ZS(M)=WSB(M)*CCS(BETA3(M))/(2.*SSH(I)*(RH2+RH3)/(R2(M)+R3(M)))
C      *** INITIALIZE CALCULATION OF MASS FLOW AND MASS AVERAGED
C      *** CONDITIONS
322 W3=0.
PRW3= 0.
PROW3=0.
TRW3= 0.
TROW3=0.
C      *** END SECTION XVII
C      *** START SECTION XVIII
C      *** CALCULATE MASS AVERAGED QUANTITIES
DO 330 M=1,NM1
RS3VZ3(M)= (RHOS3(M)*VZ3(M)+RHOS3(M+1)*VZ3(M+1))/2.
ATHRE(M)= 3.1415926*(R3(M)**2 - R3(M+1)**2)/144.
WW3(M)= RS3VZ3(M)*ATHRE(M)
TEMP=(PT3(M)+PT3(M+1))/(PT1(M)+PT1(M+1))
IF (TEMP.GE.0.) GO TO 8035
WRITE (6,8034)
8034 FORMAT (//63H THE INITIAL TOTAL PRESSURE AT THE INLET IS NEGATIVE.
1  BAD DATA )
GO TO 3500
8035 PRW3=PRW3+( TEMP **CON8-1.)*WW3(M)
PROW3=PROW3+((PT3(M)+PT3(M+1))/(2.*PT1))**CON8-1.)*WW3(M)
TRW3=TRW3+((TT3(M)+TT3(M+1))/(TT1(M)+TT1(M+1))-1.)*WW3(M)
TROW3=TROW3+((TT3(M)+TT3(M+1))/(2.*TT1)-1.)*WW3(M)
C      *** CALCULATE FLOW RATE (W3)
330 W3= W3 + WW3(M)
C      *** END SECTION XVIII
C      *** START SECTION XIX
C      *** CALCULATE MASS AVERAGE QUANTITIES
C      *** COMPUTE MASS AVERAGED TOTAL PRESSURE RATIO

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340 RC= (PRW3/W3E1.)**CCNE
C      *** OVERALL MASS AVERAGED TOTAL PRESSURE RATIO
RCC=(PRCW3/W3E1.)**CCNE
C      *** TOTAL TEMPERATURE RATIO
TR= TRW3/W3 & 1.
C      *** OVERALL TOTAL TEMPERATURE RATIO
TRC=TRCW3/W3 & 1.
C      *** EFFICIENCY
ETA= (RC**CCNE-1.)/(TR-1.)
C      *** OVERALL EFFICIENCY
350 ETAC=(RCC**CCNE-1.)/(TRC-1.)
C      *** COMPLETE MASS FLOW RATE PERCENT ERROR
EWA= ABS(W3-W1)/W3
C      *** PREPARE TO MAKE LIMIT CHECKS
C      *** FIRST TEST FOR MASS FLOW BALANCE
351 IF (EWA.LE..CC1) GO TO 372
IF (ITAL7.GE.50) GO TO 300C
ITAL7= ITAL7 & 1
C      *** TEST THE CUMP TRIGGER
IF (IPR1-1) 352,613C,613C
6130 CALL CUT6
C      *** END SECTION XIX
353 IF (ITS-1) 37C,354,371
C      *** START SECTION XXVIII
C      *** CALCULATE NEW EQUIVALENT AREA
370 ANEW= A3E & (W1-W3)*A3E/W3
C      *** CALCULATE NEW HUB RADIALS
TEMP=RTIP3**2-ANEW/(3.1415927*(CH3(I)&CTIP3(I)-1.))
IF (TEMP.GE.0.) GO TO 8037
WRITE (6,EC36)
8036 FORMAT(//100F AREA REQUIRED TO MATCH MASS FLOW WITH GIVEN TIP RADI
1US REQUIRES NEGATIVE HUB RADIUS AT STATOR EXIT. / 32H (CHECK STATE
2R EFFICIENCY INPUT) )
GO TO 350C

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8037 RHNEW=SCR1(TEMP)

C      *** CALCULATE NEW HLB RAMP ANGLE

ALPSH= ATAN((RHNEW-RH2)/BS)
GO TO 300

C      *** END SECTION XXVIII

C      *** START SECTION XXX

C      *** CALCULATE NEW EFFECTIVE AREA

354 ANEW=A3E&(W1-W3)*A3E/W3

C      *** CALCULATE NEW TIP RADIALS

RTNEW=SQRT(RH3**2&ANEW/(3.1415927*(CH3(I)&DTIP3(I)-1.)))

C      *** CALCULATE NEW TIP RAMP ANGLE

ALPST=ATAN((RTNEW-RTIP2)/BS)
GO TO 300

C      *** END SECTION XXX

C      *** CALCULATE NEW GEOMETRIC AREA

371 ANEW=A3G&(W1-W3)*A3G/W3

C      *** CALCULATE NEW AXIAL LENGTH

TAASHL=SIN(ASHL(I))/CCS(ASHL(I))
IF ( ABS(ASTL(I)) .NE. ABS(ASHL(I)) ) GO TO 356

C      *** START SECTION XXXII

BS=(RTIP2**2-RH2**2-ANEW/3.1415926)/(2.*TAASHL*(RTIP2&RH2))
GO TO 357

C      *** END SECTION XXXII

C      *** START SECTION XXXI

356 TAASTL=SIN(ASTL(I))/CCS(ASTL(I))
AE=TAASTL**2-TAASHL**2
BE=(RTIP2*TAASTL-RH2*TAASHL)/AE
CE=(RTIP2**2-RH2**2-ANEW/3.1415926)/AE
ES=-BE&SQRT(BE**2-CE)

C      *** CALCULATE NEW ASPECT RATIO

357 ARS(I)=(RTIP2-RH2)/BS
GO TO 300

C      *** END SECTION XXXI

C      *** START SECTION XXXIX

```

372 IF (ITS-1) 373,374,360

C *** IF HUB RAMP ANGLE EXCEEDS THE LIMIT, SET THE RAMP ANGLE TO
C *** THE LIMIT

373 IF (ALPSH.GT.ASHL(I)) GO TO 2344
GO TO 360

2344 ALPSH=ASHL(I)
ITS=1
WRITE (6,2345)

2345 FORMAT (1H030X44H*** STATOR HUB RAMP ANGLE LIMIT VIOLATED *** /)
GO TO 300

C *** CHECK TIP RAMP ANGLE AGAINST ITS LIMIT

374 IF (ALPST.GE.ASTL(I)) GO TO 355
ALPST=ASTL(I)
ITS=2
WRITE (6,2350)

2350 FORMAT (1H030X44H*** STATOR TIP RAMP ANGLE LIMIT VIOLATED *** /)
GO TO 300

C *** END SECTION XXIX

C *** ENSURE THAT THE TIP RAMP ANGLE IS NOT POSITIVE

355 IF (ALPST.LE.0.) GO TO 360
WRITE (6,358)

358 FORMAT (// 46H STATOR TIP RAMP ANGLE IS POSITIVE. BAD DATA.)
GO TO 3500

140 IGO=2
RETURN

3000 IGO=3
RETURN

3010 IGO=4
RETURN

3020 IGO=5
RETURN

3500 IGO=6

360 RETURN
END

```

$IBFTC CHECK
  SUBROUTINE CHECK
    REAL MW,NPR,NPS,MSH,K1,M1P,K2,M2,K3
    REAL M1,MZ1,M2P,MZ2,M3,MZ3
    DIMENSION M1(11),MZ1(11),M2P(11),MZ2(11),M3(11),MZ3(11),A3(11)
    DIMENSION VT2OT1(50),NPR(50),SRTIP(50),ARR(50),DTIP2(50),DH2(50),
    1ARHL(50),ARTL(50),DRT(50),B2(50),C2(50),D2(50),E2(50),VT3OT2(50),
    2NPS(50),SSH(50),ARS(50),DTIP3(50),DH3(50),ASHL(50),ASTL(50),
    3DSH(50),MSH(50),BPSH(50),B3(50),C3(50),D3(50),E3(50)
    DIMENSION VZ1(11),U1(11),V01(11),RHOS1(11),BETA1(11),BETA1P(11),
    1V1P(11),M1P(11),TT1(11),PT1(11),RS1VZ1(11),ACNE(11),R2(11),U2(11),
    2V02(11),TT2(11),VZ2(11),PT2(11),RHCT2(11),V2(11),RHOS2(11),
    3BETA2(11),BETA2P(11),V2P(11),DR(11),TS2(11),ATWO(11),M2(11),
    4PRI(11),WRB(11),ZR(11),RS2VZ2(11),ATO(11),TT3(11),R3(11),V03(11),
    5PT3(11),RHOT3(11),V3(11),RHCS3(11),BETA3(11),DS(11),WSB(11),
    6ZS(11),RS3VZ3(11),ATHRE(11),WW3(11)
    DIMENSION R1(11),V1(11),VZ3(11)
    DIMENSION ARHD(50),ARTD(50),ASHD(50),ASTD(50),BET1D(11),BET1PD(11)
    1,BET2D(11),BET2PD(11),BET3D(11),BPSD(50),TITL(12)
    DIMENSION BO(50),ARO(50),ASO(50)
    COMMON /CHEC/IFLAG,NSLIM
    COMMON I,INC,IPR2,N,VT2OT1,NPR,SRTIP,ARRI,DTIP2,DH2,ARHD,ARTD,DRT,
    1B2SAVE,C2,D2,E2,VT3OT2,NPS,SSH,ARS,I,DTIP3,DH3,ASHD,ASTD,DSH,MSH,
    2BPSD,B3,C3,D3,E3,W1,RCO,TRO,ETAQ,RC,TR,ETA,RTIP1,ARR,ARS,RH1,RTIP2
    3,RH2,RTIP3,RH3,BS,M,BET1D,BETA1,BET1PD,BETA1P,R1,U1,VZ1,V01,V1,
    4V1P,M1P,M1,MZ1,BET2D,BETA2,BET2PD,BETA2P,R2,U2,VZ2,V02,V2,V2P,DR,
    5M2P,M2,MZ2,BET3D,BETA3,R3,VZ3,V03,V3,DS,M3,WRB,ZR,WSB,ZS,MZ3,ALPST
    6,ALPSH,IERROR
    COMMON IPR1,K1,UTIP1,RM,RHOT1,ACNE,RS1VZ1,NM1,RHOS1,TT1,PT1,W2,
    1EWA,VZTIP2,A2G,A2E,K2,ITAL1,ALPRH,RHNEW,ANEW,TAARTL,TAARHL,AE,BE,
    2CE,ALPRT,RTNEW,B2,TT2,PT2,RHOT2,RHCS2,TS2,ATWO,PRI,ATO,RS2VZ2
    3,UTIP2,VOTIP2,Q,R,S,T,ITAL2,AA,BB,CC,DD,ITAL3,BPSH,W3,A3G,A3E,PT3,
    4VZTIP3,K3,PRW3,PROW3,TRW3,TROW3,TT3,RHOS3,TAASHL,TAASTL,ASHL,ASTL,
    5A3,ATHRE,RS3VZ3,WW3,ITAL8,AF,BF,CF,DF
    6,VZTIPO,ARHL,ARTL,RHOT3,TITL,BO,ARC,ASO
    IFLAG=0
    DO 23 I=1,NSLIM
    IF (DTIP2(I).GT.0.) GO TO 8013
    WRITE (6,8012)

 9012 FORMAT (//57H TIP BLOCKAGE FACTCR NCT POSITIVE AT ROTOR EXIT. BAD
 1CATA )
    IFLAG=1
    GO TO 3500

 8013 IF (DH2(I).GT.0.) GO TO 8015
    WRITE (6,8014)

 8014 FORMAT (//57H HUB BLOCKAGE FACTCR NOT POSITIVE AT ROTOR EXIT. BAD
 1CATA )
    IFLAG=1
    GO TO 3500

 8015 IF (DTIP3(I).GT.0.) GO TO 8029
    WRITE (6,8028)

 8028 FORMAT (//58H TIP BLOCKAGE FACTCR NCT POSITIVE AT STATOR EXIT. BAD
 1 CATA)
    IFLAG=1
    GO TO 3500

 8029 IF (DH3(I).GT.0.) GO TO 8031
    WRITE (6,8030)

 8030 FORMAT (//58H HUB BLOCKAGE FACTCR NCT POSITIVE AT STATOR EXIT. BAD

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```
1 DATA
IFLAG=1
GO TO 3500
8031 IF (ARTD(I).LE.0.) GO TO 2300
ARTD(I)=-ARTD(I)
WRITE (6,2301) I
2301 FORMAT (1H010X52H***ERROR ON ROTOR TIP RAMP ANGLE INPUT FOR STAGE
XNO. I3,3X48HTHIS ANGLE CHANGED FROM POSITIVE TO NEGATIVE *** //)
2300 IF (ASTD(I).LE.0.) GO TO 2310
ASTD(I)=-ASTD(I)
WRITE (6,2308) I
2308 FORMAT (1H010X53H***ERRCR ON STATOR TIP RAMP ANGLE INPUT FOR STAGE
X NO. I3,3X48HTHIS ANGLE CHANGED FROM POSITIVE TO NEGATIVE *** //)
2310 IF (ARHD(I).GE.0.) GO TO 2320
ARHD(I)=-ARHD(I)
WRITE (6,2312) I
2312 FORMAT (1H010X52H***ERROR ON ROTOR HUB RAMP ANGLE INPUT FOR STAGE
XNO. I3,3X48HTHIS ANGLE CHANGED FRCM NEGATIVE TO POSITIVE *** //)
2320 IF (ASHD(I).GE.0.) GO TO 23
ASHD(I)=-ASHD(I)
WRITE (6,2322) I
2322 FORMAT (1H010X53H***ERROR ON STATOR HUB RAMP ANGLE INPUT FOR STAGE
X NO. I3,3X48HTHIS ANGLE CHANGED FRCM NEGATIVE TO POSITIVE *** //)
23 CONTINUE
3500 RETURN
END
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$IBFTC INLET
SUBROUTINE INLET
COMMON /CHEC/IFLAG,NSLIM
COMMON /COM2/PTI,TTI,CON1,CON2,CON3,CON4,OOGM1,B1,C1,D1,E1
REAL MW,NPR,NPS,MSH,K1,M1P,K2,M2,K3
REAL M1,MZ1,M2P,MZ2,M3,MZ3
DIMENSION M1(11),MZ1(11),M2P(11),MZ2(11),M3(11),MZ3(11),A3(11)
DIMENSION VT2OT1(50),NPR(50),SRTIP(50),ARR(50),DTIP2(50),DH2(50),
1ARHL(50),ARTL(50),DRT(50),B2(50),C2(50),D2(50),E2(50),VT3OT2(50),
2NPS(50),SSH(50),ARS(50),DTIP3(50),DH3(50),ASHL(50),ASTL(50),
3DSH(50),MSH(50),BPSH(50),B3(50),C3(50),D3(50),E3(50)
DIMENSION VZ1(11),U1(11),V01(11),RHOS1(11),BETA1(11),BETA1P(11),
1V1P(11),M1P(11),TT1(11),PT1(11),RS1VZ1(11),AONE(11),R2(11),U2(11),
2V02(11),TT2(11),VZ2(11),PT2(11),RHOT2(11),V2(11),RHOS2(11),
3BETA2(11),BETA2P(11),V2P(11),DR(11),TS2(11),ATWO(11),M2(11),
4PRI(11),WRB(11),ZR(11),RS2VZ2(11),ATO(11),TT3(11),R3(11),V03(11),
5PT3(11),RHOT3(11),V3(11),RHCS3(11),BETA3(11),DS(11),WSB(11),
6ZS(11),RS3VZ3(11),ATHRE(11),WW3(11)
DIMENSION R1(11),V1(11),VZ3(11)
DIMENSION ARHD(50),ARTD(50),ASHD(50),ASTD(50),BET1D(11),BET1PD(11)
1,BET2D(11),BET2PD(11),BET3D(11),BPSD(50),TITL(12)
DIMENSION BO(50),ARO(50),ASO(50)
COMMON I,INC,IPR2,N,VT2OT1,NPR,SRTIP,ARRI,DTIP2,DH2,ARHD,ARTD,DRT,
1B2SAVE,C2,D2,E2,VT3OT2,NPS,SSH,ARSI,DTIP3,DH3,ASHD,ASTD,DSH,MSH,
2BPSD,B3,C3,D3,E3,W1,RC0,TR0,ETAC,RC,TR,ETA,RTIP1,ARR,ARS,RH1,RTIP2
3,RH2,RTIP3,RH3,BR,BS,M,BET1D,BETA1,BET1PD,BETA1P,R1,U1,VZ1,V01,V1,
4V1P,M1P,M1,MZ1,BET2D,BETA2,BET2PD,BETA2P,R2,U2,VZ2,V02,V2,V2P,DR,
5M2P,M2,MZ2,BET3D,BETA3,R3,VZ3,V03,V3,DS,M3,WRB,ZR,WSB,ZS,MZ3,ALPST
6,ALPSH,IERROR
COMMON IPR1,K1,UTIP1,RM,RHOT1,AONE,RS1VZ1,NM1,RHOS1,TT1,PT1,W2,
1EWA,VZTIP2,A2G,A2E,K2,ITAL1,ALPRH,RHNEW,ANEW,TAARTL,TAARHL,AE,BE,
2CE,ALPRT,RTNEW,B2,TT2,PT2,RHOT2,RHCS2,TS2,ATWO,PRI,ATO,RS2VZ2
3,UTIP2,VOTIP2,Q,R,S,T,ITAL2,AA,BB,CC,DD,ITAL3,BPSH,W3,A3G,A3E,PT3,
4VZTIP3,K3,PRW3,PROW3,TRW3,TRCH3,TT3,RHOS3,TAASHL,TAASTL,ASHL,ASTL,
5A3,ATHRE,RS3VZ3,WW3,ITAL8,AF,BF,CF,DF
6,VZTIPO,ARHL,ARTL,RHOT3,TITL,BO,ARC,ASO
C      *** CHECK ON THE INPUT PARAMETERS OF THE ROTOR HUB AND TIP
C      BLOCKAGE FACTORS, THE STATOR HUB AND TIP BLOCKAGE FACTORS
C      AND THE RAMP ANGLES FOR ALL STAGES
IFLAG=0

C      *** START SECTION IV

C0 80 M=1,N
U1(M)=CON4*R1(M)
V01(M)=B1/R1(M) + C1 + D1*R1(M) + E1*R1(M)**2
V1(M)= SQRT(VZ1(M)**2+V01(M)**2)
TEMP=1.-V1(M)**2/CON2
IF (TEMP.GE.0.) GO TO 8007
WRITE (6,8006)

8006 FORMAT (//5H ABSOLUTE STATIC TEMPERATURE AT ROTOR INLET IS NEGATI
1VE )
IFLAG=1
GO TO 10

8007 RHOS1(M)=RHOT1*TEMP**OOGM1
BETA1(M)= ATAN(V01(M)/VZ1(M))
BETA1P(M)=ATAN((U1(M)-V01(M))/VZ1(M))
V1P(M)=VZ1(M)/COS(BETA1P(M))


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TEMP=CON3*(TTI-V1(M)**2/CON1)
IF (TEMP.GE.0.) GO TO 8C09
WRITE (6,8006)
IFLAG=1
GO TO 10
8009 M1P(M)= V1P(M)/SQRT(TEMP)
TT1(M)= TTI
M1(M)=V1(M)/SQRT(TEMP)
MZ1(M)=VZ1(M)/SQRT(TEMP)
80 PT1(M)= PTI

C      *** END SECTION IV

C      *** START SECTION V

C      *** CALCULATE MASS FLOW

90 W1= 0.
DO 100 M=1,NM1
RS1VZ1(M)= (RHOS1(M)*VZ1(M)+RHOS1(M+1)*VZ1(M+1))/2.
ADNE(M)= 3.1415926*(R1(M)*R1(M)-R1(M+1)*R1(M+1))/144.
100 W1= W1 + RS1VZ1(M)*ACNE(M)

C      *** END SECTION V

10 RETURN
END

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** $IBFTC OUT1      LIST
      SUBROUTINE OUT1
      REAL MW,NPR,NPS,MSH,K1,M1P,K2,M2,K3
      REAL M1,MZ1,M2P,MZ2,M3,MZ3
      DIMENSION M1(11),MZ1(11),M2P(11),MZ2(11),M3(11),MZ3(11),A3(11)
      DIMENSION VT2OT1(50),NPR(50),SRТИP(50),ARR(50),DTIP2(50),DH2(50),
1ARHL(50),ARTL(50),DRT(50),B2(50),C2(50),D2(50),E2(50),VT3OT2(50),
2NPS(50),SSH(50),ARS(50),DTIP3(50),DH3(50),ASHL(50),ASTL(50),
3DSH(50),MSH(50),BPSH(50),B3(50),C3(50),D3(50),E3(50)
      DIMENSION VZ1(11),U1(11),V01(11),RHOS1(11),BETA1(11),BETA1P(11),
1V1P(11),M1P(11),TT1(11),PT1(11),RS1VZ1(11),ACNE(11),R2(11),U2(11),
2V02(11),TT2(11),VZ2(11),PT2(11),RHOT2(11),V2(11),RHOS2(11),
3BETA2(11),BETA2P(11),V2P(11),DR(11),TS2(11),ATWO(11),M2(11),
4PRI(11),WRB(11),ZR(11),RS2VZ2(11),ATO(11),TT3(11),R3(11),V03(11),
5PT3(11),RHOT3(11),V3(11),RHCS3(11),BETA3(11),DS(11),WSB(11),
6ZS(11),RS3VZ3(11),ATHRE(11),WW3(11)
      DIMENSION R1(11),V1(11),VZ3(11)
      DIMENSION ARHD(50),ARTD(50),ASHD(50),ASTD(50),BET1D(11),BET1PD(11),
1,BET2D(11),BET2PD(11),BET3D(11),BPSD(50),TITL(12)
      DIMENSION BO(50),ARO(50),ASC(50)
      COMMON I,INC,IPR2,N,VT2OT1,NPR,SRТИP,ARRI,DTIP2,DH2,ARHD,ARTD,DRT,
1B2SAVE,C2,D2,E2,VT3OT2,NPS,SSH,ARSI,DTIP3,DH3,ASHD,ASTD,DSH,MSH,
2BPSD,B3,C3,D3,E3,W1,RC0,TRO,ETA0,RC,TR,ETA,RTIPI,ARR,ARS,RH1,RTIP2
3,RH2,RTIP3,RH3,BR,BS,M,BET1D,BETA1,BET1PD,BETA1P,R1,U1,VZ1,V01,V1,
4V1P,M1P,M1,MZ1,BET2D,BETA2,BET2PD,BETA2P,R2,U2,VZ2,V02,V2,V2P,DR,
5M2P,M2,MZ2,BET3D,BETA3,R3,VZ3,V03,V3,DS,M3,WRB,ZR,WSB,ZS,MZ3,ALPST
6,ALPSH,IERROR
      COMMON IPR1,K1,UTIP1,RM,RHOT1,AONE,RS1VZ1,NM1,RHOS1,TT1,PT1,W2,
1EWA,VZTIP2,A2G,A2E,K2,ITAL1,ALPRH,RHNEW,ANEW,TAARTL,TAARHL,AE,BE,
2CE,ALPRT,RTNEW,B2,TT2,PT2,RHOT2,RHOS2,TS2,ATWO,PRI,ATO,RS2VZ2
3,UTIP2,VOTIP2,Q,R,S,T,ITAL2,AA,BB,CC,DD,ITAL3,BPSH,W3,A3G,A3E,PT3,
4VZTIP3,K3,PRW3,PROW3,TRW3,TROW3,TT3,RHOS3,TAASHL,TAASTL,ASHL,ASTL,
5A3,ATHRE,RS3VZ3,WW3,ITAL8,AF,BF,CF,DF
6,VZTIPO,ARHL,ARTL,RHOT3,TITL,BO,ARC,AS0
      GO TO (600C,6020),IPR1
6000 WRITE (6,6001) W1,K1,UTIP1,RTIP1,RM,RHOT1
6001 FORMAT (1H013X2HW118X2HK117X5HUTIP115X5HRTIP115X2HRM17X5HRHCT1//
1 6E20.8 //)
      WRITE (6,6003)
6003 FORMAT (13X2HR118X3HVZ117X3HV01 //)
      DO 6002 M=1,N
6002 WRITE (6,6005) R1(M),VZ1(M),V01(M)
6005 FORMAT (3E20.8)
      RETURN
6020 WRITF (6,6001) W1,K1,UTIP1,RTIP1,RM,RHOT1
      WRITE (6,6024)
6024 FORMAT (1H011X2HR114X3HVZ114X3HV0115X2HM1 14X3HMZ1 14X3HM1P 14X
13HV1P //)
      DO 6026 M=1,N
6026 WRITF (5,6025) R1(M),VZ1(M),V01(M), M1(M), MZ1(M), M1P(M), V1P(M)
6025 FORMAT (7E17.8)
      WRITE (6,6015) (AONF(M),RS1VZ1(M),M=1,NM1)
6015 FORMAT (1H09X4HAONE12X6HRS1VZ1//(2E17.8))
      WRITE (6,6027)
6027 FORMAT (1H0 /11X2HU115X2HV113X5HRHCS112X5HBETA112X6HBETA1P12X3HTT1
1 14X3HPT1 //)
      DO 6028 M=1,N

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602R WRITE (6,6025) U1(M),V1(M),RHOS1(M),BETA1(M),BETA1P(M),TT1(M),
1 PT1(M)
RFTURN
END
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$*
$IRFTC OUT2 LIST
SUBROUTINE OUT2
REAL MW,NPR,NPS,MSH,K1,M1P,K2,M2,K3
REAL M1,MZ1,M2P,MZ2,M3,MZ3
DIMENSION M1(11),MZ1(11),M2P(11),MZ2(11),M3(11),MZ3(11),A3(11)
DIMENSION VT20T1(50),NPR(50),SRTIP(50),ARR(50),DTIP2(50),DH2(50),
1ARHL(50),ARTL(50),DRT(50),B2(50),C2(50),D2(50),E2(50),VT30T2(50),
2NPS(50),SSH(50),ARS(50),DTIP3(50),DH3(50),ASHL(50),ASTL(50),
3DSH(50),MSH(50),BPSH(50),B3(50),C3(50),D3(50),E3(50)
DIMENSION VZ1(11),U1(11),V01(11),RHCS1(11),BETA1P(11),BETA1P(11),
1V1P(11),M1P(11),TT1(11),PT1(11),RS1VZ1(11),ACNE(11),R2(11),U2(11),
2V02(11),TT2(11),VZ2(11),PT2(11),RHOT2(11),V2(11),RHOS2(11),
3BETA2(11),BETA2P(11),V2P(11),DR(11),TS2(11),ATWO(11),M2(11),
4PRI(11),WRB(11),ZR(11),RS2VZ2(11),ATO(11),TT3(11),R3(11),V03(11),
5PT3(11),RHOT3(11),V3(11),RHOS3(11),BETA3(11),DS(11),WSB(11),
6ZS(11),RS3VZ3(11),ATHRE(11),WW3(11)
DIMENSION R1(11),V1(11),VZ3(11)
DIMENSION ARHD(50),ARTD(50),ASHD(50),ASTD(50),BET1D(11),BET1PD(11)
1,BET2D(11),BET2PD(11),BFT3D(11),BPSD(50),TITL(12)
DIMENSION BO(50),ARO(50),ASC(50)
COMMON I,INC,IPR2,N,VT20T1,NPR,SRTIP,ARRI,DTIP2,DH2,ARHD,ARTD,DRT,
1B2SAVE,C2,D2,E2,VT30T2,NPS,SSH,ARSI,DTIP3,DH3,ASHD,ASTD,DSH,MSH,
2BPSD,B3,C3,D3,E3,W1,RC0,TRO,ETA0,RC,TR,ETA,RTIP1,ARR,ARS,RH1,RTIP2
3,RH2,RTIP3,RH3,BR,BS,M,BET1D,BETA1,BET1PD,BETA1P,R1,U1,VZ1,V01,V1,
4V1P,M1P,M1,MZ1,BET2D,BETA2,BET2PD,BETA2P,R2,U2,VZ2,V02,V2,V2P,DR,
5M2P,M2,MZ2,BET3D,BETA3,R3,VZ3,V03,V3,DS,M3,WRB,ZR,WSB,ZS,MZ3,ALPST
6,ALPSH,IERROR
COMMON IPR1,K1,UTIP1,RM,RHOT1,ACNE,RS1VZ1,NM1,RHOS1,TT1,PT1,W2,
1EWA,VZTIP2,A2G,A2E,K2,ITAL1,ALPRH,RHNEW,ANEW,TAARTL,TAARHL,AE,BE,
2CE,ALPRT,RTNEW,B2,TT2,PT2,RHOT2,PHOS2,TS2,ATWO,PRI,ATO,RS2VZ2
3,UTIP2,VOTIP2,Q,R,S,T,ITAL2,AA,BB,CC,DD,ITAL3,BPSH,W3,A3G,A3E,PT3,
4VZTIP3,K3,PRW3,PROW3,TRW3,TROW3,TT3,RHOS3,TAASHL,TAASL,ASHL,ASTL,
5A3,ATHRE,R3VZ3,WW3,ITAL8,AF,BF,CF,DF
6,VZTIPO,ARHL,ARLT,RHOT3,TITL,BO,ARC,ASD
GO TO (6050,6055),IPR1
6050 WRITE (6,6051) BR,RTIP2,VZTIP2,W1,W2,EWA,BETA2P(N),M2(N),B2(I)
6051 FORMAT (1H08X2HBR9X5HRTIP27X6HVZTIP210X2HW11X2HW211X3HEWA5X9HRTA
12P(N)7X5HM2(N)8X5HR2(I) //9F13.5 //)
RETURN
6055 WRITE (6,6051) BR,RTIP2,VZTIP2,W1,W2,EWA,BETA2P(N),M2(N),B2(I)
WRITE (6,6056) RH2,A2G,A2E,K2
6056 FORMAT(1H013X3HRH217X3HA2G17X3HA2E17X2HK2 // 4E20.8 //11X3HVZ2
114X2HR215X2HU215X3HV0214X3HTT214X3HPT212X5HRHOT2 // )
6025 FORMAT(7E17.8)
DO 6057 M=1,N
6057 WRITE (6,6025) VZ2(M),R2(M),U2(M),V02(M),TT2(M),PT2(M),RHOT2(M)
WRITE (6,6058)
6058 FORMAT (1H0/9X2HV214X5HRHOS212X5HRTA212X3HV2P15X2HDR15X3HTS2 // )
DO 6059 M=1,N
6059 WRITE (6,6025) V2(M),RHOS2(M),BETA2(M),V2P(M),DR(M),TS2(M)
WRITE (6,6060) (ATWO(M),M2(M),MZ2(M),M2P(M),PRI(M),WRB(M),ZR(M),
1M=1,N)
6060 FORMAT (1H07X4HATWO13X2HM212X3HMZ212X3HM2P12X3HPRI12X3HWRB13X2HZR
1//(7E15.7))
WRITE (6,6061) (ATO(M),RS2VZ2(M),M=1,NM1)
6061 FORMAT (1H011X3HAT011X6HRS2VZ2//(2E17.8))
WRITE (6,6062) ITAL1,ALPRH,RHNEW,ANEW,TAARTL,TAARHL,AE,BE,CE,ARR(I

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1),ALPRT,RTNEW  
6062 FORMAT (1H0/7X5HITAL1I2X5HALPRH12X5HRHNEW13X4HANEW12X6HTAARTL1I1X6H  
1TAARHL //I11,6X5E17.8 //9X2HAE15X2HBE15X2HCE13X6HARR(1)11X5HALPRT  
2I2X5HRTNEW //6E17.8 )  
  RETURN  
  END
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**  

$IBFTC OUTPUT  

C      *** OUTPUT SUBROUTINE  

SUBROUTINE OUTPUT  

REAL MW,NPR,NPS,MSH,K1,M1P,K2,M2,K3  

REAL M1,MZ1,M2P,MZ2,M3,MZ3  

DIMENSION M1(11),MZ1(11),M2P(11),MZ2(11),M3(11),MZ3(11),A3(11)  

DIMENSION VT2OT1(50),NPR(50),SRTIP(50),ARR(50),DTIP2(50),DH2(50),  

1ARHL(50),ARTL(50),DRT(50),B2(50),C2(50),D2(50),E2(50),VT3OT2(50),  

2NPS(50),SSH(50),ARS(50),DTIP3(50),DH3(50),ASHL(50),ASTL(50),  

3DSH(50),MSH(50),BPSH(50),B3(50),C3(50),D3(50),E3(50)  

DIMENSION VZ1(11),U1(11),VO1(11),RHOS1(11),BETA1(11),BETA1P(11),  

1V1P(11),M1P(11),TT1(11),PT1(11),RS1VZ1(11),ACNE(11),R2(11),U2(11),  

2VO2(11),TT2(11),VZ2(11),PT2(11),RHOT2(11),V2(11),RHOS2(11),  

3BETA2(11),BETA2P(11),V2P(11),DR(11),TS2(11),ATWO(11),M2(11),  

4PRI(11),WRB(11),ZR(11),RS2VZ2(11),ATO(11),TT3(11),R3(11),VO3(11),  

5PT3(11),RHOT3(11),V3(11),RHOS3(11),BETA3(11),DS(11),WSB(11),  

6ZS(11),RS3VZ3(11),ATHRE(11),WW3(11)  

DIMENSION R1(11),V1(11),VZ3(11)  

DIMENSION ARHD(50),ARTD(50),ASHD(50),ASTD(50),BET1D(11),BET1PD(11)  

1,BET2D(11),BET2PD(11),BET3D(11),BPSD(50),TITL(12)  

DIMENSION RD(50),ARO(50),ASC(50)  

COMMON I,INC,IPR2,N,VT2OT1,NPR,SRTIP,ARRI,DTIP2,DH2,ARHD,ARTD,DRT,  

1B2SAVE,C2,D2,E2,VT3OT2,NPS,SSH,ARSI,DTIP3,DH3,ASHD,ASTD,DSH,MSH,  

2BPSD,B3,C3,D3,E3,W1,RCQ,TRO,ETAQ,RC,TR,ETA,RTIP1,ARR,ARS,RH1,RTIP2  

3,RH2,RTIP3,RH3,BR,BS,M,BET1D,BETA1,BET1PD,BETA1P,R1,U1,VZ1,VO1,V1,  

4V1P,M1P,M1,MZ1,BET2D,BETA2,RET2PD,BETA2P,R2,U2,VZ2,VO2,V2,V2P,DR,  

5M2P,M2,MZ2,BET3D,BETA3,R3,VZ3,VO3,V3,DS,M3,WRB,ZR,WSB,ZS,MZ3,ALPST  

6,ALPSH,IERROR  

COMMON IPR1,K1,UTIP1,RM,RHOT1,AONE,RS1VZ1,NM1,RHOS1,TT1,PT1,W2,  

1EWA,VZTIP2,A2G,A2E,K2,ITAL1,ALPRH,RHNEW,ANEW,TAARTL,TAARHL,AE,BE,  

2CE,ALPRT,RTNEW,B2,TT2,PT2,RHOT2,RHOS2,TS2,ATWO,PRI,ATC,RS2VZ2  

3,UTIP2,VOTIP2,Q,R,S,T,ITAL2,AA,BB,CC,DD,ITAL3,BPSH,W3,A3G,A3E,PT3,  

4VZTIP3,K3,PRW3,PROW3,TRW3,TROW3,TT3,RHOS3,TAASHL,TAASTL,ASHL,ASTL,  

5A3,ATHRE,RS3VZ3,WW3,ITAL8,AF,BF,CF,DF  

6,VZTIPO,ARHL,ARTL,RHOT3,TITL,BO,ARC,ASO

C      *** SECTION XXI (CONTINUED FROM MAIN)

C      *** WRITE TITLE

500 WRITE (6,2020) [  

2020 FORMAT (1H141X37H***** S T A G E   D A T A ***** //54X9H$TAG  

1E NO. [3 //]  

INC=1  

IF (IPR2.GT.0) INC=N-1

C      *** WRITE ROTOR TITLE

WRITE (6,2030)  

2030 FORMAT( 49X24H*** ROTOR INPUT DATA *** / )

C      *** WRITE ROTOR INPUT QUANTITIES AND TITLE FOR STATOR

WRITE (6,2040) VT2OT1(I),NPR(I),SRTIP(I),ARRI ,DTIP2(I),DH2(I),  

1ARHD(I),ARTD(I),DRT(I),BPSD(I),B2SAVE,C2(I),D2(I),E2(I)  

2040 FORMAT (/65X3HTIP12X3HHUB10X9HMAX ANGLE5X9HMAX ANGLE/12H AXIAL VE  

1L.5X10HPOLYTOPIC6X8HSOLIDITY8X6HASPECT8X9HBLOCKAGE7X8HBLOCKAGE7X
```

29HHUB TAPERSX9HTIP TAPER /4X5HRATIO8X10HEFFICIENCY7X6HAT TIP9X5HRA
3TID10X6HFACTOR SX6HFACTOR8X9H(DEGREES)5X9H(DEGREES) //F10.4,5F15.4,
42F15.3 //16X13HMIN REL. FLOW39X44HCOEFFICIENTS IN TANGENTIAL VELOC
5ITY EQUATION /30H MAX ROTOR ANGLE ROTOR HUB /27H DIF. FACTOR
6 (DEGREES)40X1HB14X1HC14X1HD14X1HE //F10.4,F16.4,31X,
74F15.4 //47X25H*** STATOR INPUT DATA ***)

C *** WRITE STATOR INPUT QUANTITIES

WRITE (6,2050) VT30T2(I),NPS(I),SSH(I),ARSI ,DTIP3(I),DH3(I),
1 ASHD(I),ASTD(I),DSH(I),MSH(I), B3(I),C3(I),D3(I),E3(I)
2050 FORMAT (/ 4X5HAXIAL10X5HTOTAL41X3HTIP12X3HHUB10X9HMAX ANGLE6X9HMA
1X ANGLE/11H VELOCITY6X10HPOLYTROPIC 6X8HSOLIDITY8X6HASPECT8X8HBL
2OCKAGE7X8HBLOCKAGE7X9HHUB TAPER6X9HTIP TAPER/4X5HRATIO8X10HEFFICIE
3NCY7X6HAT HUB9X5HRATIO10X6HFACTOR9X6HFACTOR8X9H(DEGREES)6X9H(DEGRE
4ES) // F10.4,5F15.4,F16.4,F15.4 // 68X44HCOEFFIC
5IENTS IN TANGENTIAL VELOCITY EQUATION /29H MAX. STATOR MAX HUB
6INLET / 28H DIF. FACTOR MACH NUMBER
7 39X1HB14X1HC14X1HD14X1HE //F10.4,F15.4, 32X4F15.4)
IF (IERROR.GT.0) RETURN

C *** WRITE STAGE OUTPUT QUANTITIES

ALPRTD=ALPRT/.0174533
ALPRHD=ALPRH/.0174533
ALPSTD=ALPST/.0174533
ALPSHD=ALPSH/.0174533
WRITE (6,2060) W1,RCC,TRO,ETA0,RC,TR,ETA,ARR(I),ARS(I),RTIP1,RH1,
1RTIP2,RH2,RTIP3,RH3,BR,BS,ALPRTD,ALPRHD,ALPSTD,ALPSHD
2060 FORMAT (//30X59H****--**--**--** STAGE OUTPUT DATA ***
1---**--**--** //46X20HMASS FLOW (LB/SEC) = F8.3 //4X7HOVERALL8X7HOVERA
2LL8X7HOVERALL7X9HMASS AVE.6X9HMASS AVE.22X5HROTOR10X6HSTATOR/12H
3 MASS AVE.6X9HMASS AVE.6X9HMASS AVE.6X8HPRESSURE6X11HTEMPERATURE5X
49HMASS AVE.7X6HASPECT9X6HASPECT /12H PR. RATIO5X11HTEMP. RATIO4X
510EFFICIENCY8X5HRATIO10X5HRATIO7X10HEFFICIENCY7X5HRATIO10X5HRATIO
6//F10.4,7F15.4 //12H ROTOR TIP 6X9HROTOR HUB 6X9HROTOR TIP6X9HR
*OTOR HUB 5X 10HSTATOR TIP 5X 10HSTATOR HUB
7 5X11HROTOR PROJ.3X12HSTATOR PROJ. /3X8HRAD. 1-G7X8HRAD. 1
8-G7X8HRAD. 2-G7X8HRAD. 2-G7X8HRAD. 3-G7X8HRAD. 3-G8X6HLENGTH9X6HLE
9NGTH /3X8H(INCHES)7(7X8H(INCHES)) //F11.4,F14.4,6F15.4 // 32X
1 9HROTOR TIP6X9HROTOR HUB5X10HSTATOR TIP5X10HSTATOR HUB / 26X
2 4(5X10HRAMP ANGLE) / 25X4(6X9H(DEGREES)) // 25X4F15.4)

C *** WRITE ROTOR TITLE PART 1

WRITE (6,2064)
2064 FORMAT(1H124X70H****--**--**--** ROTOR INLET OUTPUT D
IATA ****--**--** //)

C *** WRITE ROTOR TITLE PART 2

WRITE (6,2065)
2065 FORMAT (5X6HRADIUS4X5HWHEEL4X5HAXIAL2X8HTANGENT.3X4HABS.5X4HREL.
15X4HABS.5X4HREL.4X5HTOTAL4X5HTOTAL11X4HREL.3X4HABS./4H STA3X2H-E6X
25HSPEED4X4HVEL.5X4HVEL.5X4HVEL.5X4HVEL.3X24HAIR ANG. AIR ANG. TEM
3P.4X6HPRESS.10X17HMACH MACH LOSS /91H NO. (IN) (FT/SEC) (FT/
4SEC) (FT/SEC) (FT/SEC) (DEG) (DEG) (DEG R) (PSI)
511X18HNO. NO. COEFF //)

C *** CONVERT ANGLES FROM RADIANS TO DEGREES

```
DO 2070 M=1,N,INC  
BET1D(M)=BETA1(M)/ .0174533  
BET1PD(M)=BETA1P(M)/.0174533
```

C *** WRITE ROTOR INLET COMPUTED QUANTITIES

```
2070 WRITE (6,2075) M,R1(M),U1(M),VZ1(M),VO1(M),V1(M),V1P(M),BET1D(M),  
1BET1PD(M),TT1(M),PT1(M),M1P(M),M1(M),WRB(M)  
2075 FORMAT (I3,F8.3,F10.3,4F9.3,2F8.3,F10.3,F9.3,7X,3F7.3 )
```

C *** WRITE ROTOR EXIT TITLE

```
WRITE (6,2080)  
2080 FORMAT (//26X68H***** R C T O R E X I T C U T P U T D A  
1 T A ***** // 5X6HRADIUS4X5HWHEEL4X5HAXIAL2X8HTANGENT.3X  
24HABS.5X4HREL.5X4HARS.5X4HREL.4X5HTOTAL4X5HTOTAL3X5HROTOR3X4HREL.  
33X4HABS. / 4H STA3X2H-E6X5HSPEED4X4HVEL.5X4HVEL.5X4HVEL.  
43X24HAIR ANG. AIR ANG. TEMP.4X6PRESS.3X4HDIF.3X4HMACH3X4HMACH 2X  
5 4HLOSS /119H NO. (IN) (FT/SEC) (FT/SEC) (FT/SEC) (FT/SEC) (FT/  
6SEC) (DEG) (DEG) (DEG R) (PSI) FACTOR NO. NO. FUNC  
7 // )
```

C *** CONVERT ANGLES FROM RADIANS TO DEGREES

```
DO 2090 M=1,N,INC  
BET2D(M)=BETA2(M)/.0174533  
BET2PD(M)=BETA2P(M)/.0174533
```

C *** WRITE ROTOR EXIT COMPUTED QUANTITIES

```
2090 WRITE (6,2095) M,R2(M),U2(M),VZ2(M),VO2(M),V2(M),V2P(M),BET2D(M),  
1BET2PD(M),TT2(M),PT2(M),DR(M),M2P(M),M2(M),ZR(M)  
2095 FORMAT (I3,F8.3,F10.3,4F9.3,2F8.3,F10.3,F9.3,4F7.3 )
```

C *** WRITE STATOR EXIT TITLE

```
WRITE (6,2100)  
2100 FORMAT ( //25X70H***** S T A T O R E X I T O U T P U T  
1D A T A ***** // 5X6HRADIUS13X22HAXIAL TANGENT. ABS.14X  
2 4HABS.30X19HSTATOR AXIAL ABS. / 9H STA -E15X4HVEL.5X4HVEL. 5X  
34HVEL. 12X8HAIR ANG.21X4HLOSS4X4HDIF.2X4HMACH4X4HMACH2X4HLOSS /  
44H NO.2X4H(IN)12X26H(FT/SEC) (FT/SEC) (FT/SEC)11X5H(DEG)123X 32HCOE  
5FF FACTOR NO. NO. FUNC // )
```

C *** CONVERT ANGLES FROM RADIANS TO DEGREES

```
DO 2110 M=1,N,INC  
BET3D(M)=BETA3(M)/.0174533
```

C *** WRITE STATOR EXIT COMPUTED QUANTITIES

```
2110 WRITE (6,2120) M,R3(M),VZ3(M),VO3(M),V3(M),BET3D(M),WSB(M),DS(M),  
1MZ3(M),M3(M),ZS(M)  
2120 FORMAT (I3,F8.3,10X,4F9.3,F17.3,20X,5F7.3 )  
RETURN
```

C *** SECTION XXI (CONTINUED IN MAIN AFTER ST. 500)

END

```

** $IBFTC OUT3 LIST
      SUBROUTINE OUT3
      REAL MW,NPR,NPS,MSH,K1,M1P,K2,M2,K3
      REAL M1,MZ1,M2P,MZ2,M3,MZ3
      DIMENSION M1(11),MZ1(11),M2P(11),MZ2(11),M3(11),MZ3(11),A3(11)
      DIMENSION VT2OT1(50),NPR(50),SRTIP(50),ARR(50),DTIP2(50),DH2(50),
     1ARHL(50),ARTL(50),DRT(50),B2(50),C2(50),D2(50),E2(50),VT3OT2(50),
     2NPS(50),SSH(50),ARS(50),DTIP3(50),DH3(50),ASHL(50),ASTL(50),
     3DSH(50),MSH(50),BPSH(50),B3(50),C3(50),D3(50),E3(50)
      DIMENSION VZ1(11),U1(11),VC1(11),RHOS1(11),BETA1(11),BETA1P(11),
     1V1P(11),M1P(11),TT1(11),PT1(11),RS1VZ1(11),AONE(11),R2(11),U2(11),
     2V02(11),TT2(11),VZ2(11),PT2(11),RHOT2(11),V2(11),RHOS2(11),
     3BETA2(11),BETA2P(11),V2P(11),DR(11),TS2(11),ATWO(11),M2(11),
     4PRI(11),WRB(11),ZR(11),RS2VZ2(11),ATO(11),TT3(11),R3(11),V03(11),
     5PT3(11),RHOT3(11),V3(11),RHOS3(11),BETA3(11),DS(11),WSB(11),
     6ZS(11),RS3VZ3(11),ATHRE(11),WW3(11)
      DIMENSION R1(11),V1(11),VZ3(11)
      DIMENSION ARHD(50),ARTD(50),ASHD(50),ASTD(50),BET1D(11),BET1PD(11)
     1,BET2D(11),BET2PD(11),BET3D(11),BPSD(50),TITL(12)
      DIMENSION BO(50),ARO(50),ASO(50)
      COMMON I,INC,IPR2,N,VT2OT1,NPR,SRTIP,ARR,DTIP2,DH2,ARHD,ARTD,DRT,
     1B2SAVE,C2,D2,E2,VT3OT2,NPS,SSH,ARS,DTIP3,DH3,ASHD,ASTD,DSH,MSH,
     2BPSD,B3,C3,D3,E3,W1,RC0,TRO,ETA0,RC,TR,ETA,RTIP1,ARR,ARS,RH1,RTIP2
     3,RH2,RTIP3,RH3,BR,BS,M,BET1D,BETA1,BET1PD,BETA1P,R1,U1,VZ1,V01,V1,
     4V1P,M1P,M1,MZ1,BET2D,BETA2,BET2PD,BETA2P,R2,U2,VZ2,V02,V2,V2P,DR,
     5M2P,M2,MZ2,BET3D,BETA3,R3,VZ3,V03,V3,DS,M3,WRB,ZR,WSB,ZS,MZ3,ALPST
     6,ALPSH,IERROR
      COMMON IPR1,K1,UTIP1,RM,RHOT1,AONE,RS1VZ1,NM1,RHOS1,TT1,PT1,W2,
     1EWA,VZTIP2,A2G,A2E,K2,ITAL1,ALPRH,RHNEW,ANEW,TAARTL,TAARHL,AE,BE,
     2CE,ALPRT,RTNEW,B2,TT2,PT2,RHOT2,RHOS2,TS2,ATWO,PRI,ATO,RS2VZ2
     3,UTIP2,VOTIP2,Q,R,S,T,ITAL2,AA,BB,CC,DD,ITAL3,BPSH,W3,A3G,A3E,PT3,
     4VZTIP3,K3,PRW3,PROW3,TRW3,TROW3,TT3,RHOS3,TAASHL,TAASTL,ASHL,ASTL,
     5A3,ATHRE,RS3VZ3,WW3,ITAL8,AF,BF,CF,DF
     6,VZTIPO,ARHL,ARTL,RHOT3,TITL,BO,ARC,ASO
      GO TO (6030,6035),IPR1
6030 WRITE (6,6031) BR,RTIP2,VZTIP2,UTIP2,VOTIP2,B2(I)
6031 FORMAT (1H013X2HBR17X5HRTIP214X6HVZTIP215X5HUTIP214X6HVOTIP2 15X
     1 5HB2(I) // 6E20.8 //)
      RETURN
6035 WRITE (6,6031) BR,RTIP2,VZTIP2,UTIP2,VOTIP2,B2(I)
      WRITE (6,6036) Q,R,S,T
6036 FORMAT (1H014X1HQ19X1HR19X1HS19X1HT //4E20.8 // 45X28H*** ROTOR MA
     1SS FLOW TEST *** // )
      RETURN
      END

```

```

** $IBFTC OUT4 LIST
SUBROUTINE OUT4
REAL MW,NPR,NPS,MSH,K1,M1P,K2,M2,K3
REAL M1,MZ1,M2P,MZ2,M3,MZ3
DIMENSION M1(11),MZ1(11),M2P(11),MZ2(11),M3(11),MZ3(11),A3(11)
DIMENSION VT20T1(50),NPR(50),SRTIP(50),ARR(50),DTIP2(50),DH2(50),
1ARHL(50),ARTL(50),DRT(50),B2(50),C2(50),D2(50),E2(50),VT30T2(50),
2NPS(50),SSH(50),ARS(50),DTIP3(50),DH3(50),ASHL(50),ASTL(50),
3DSH(50),MSH(50),BPSH(50),B3(50),C3(50),D3(50),E3(50)
DIMENSION VZ1(11),U1(11),V01(11),RHCS1(11),BETA1(11),BFTA1P(11),
1V1P(11),M1P(11),TT1(11),PT1(11),RS1VZ1(11),ACNE(11),R2(11),U2(11),
2V02(11),TT2(11),VZ2(11),PT2(11),RHOT2(11),V2(11),RHOS2(11),
3BETA2(11),BETA2P(11),V2P(11),DR(11),TS2(11),ATWO(11),M2(11),
4PRI(11),WRB(11),ZP(11),RS2VZ2(11),ATO(11),TT3(11),R3(11),V03(11),
5PT3(11),RHOT3(11),V3(11),RHOS3(11),BETA3(11),DS(11),WSB(11),
6ZS(11),RS3VZ3(11),ATHRE(11),WW3(11)
DIMENSION R1(11),V1(11),VZ3(11)
DIMENSION ARHD(50),ARTD(50),ASHD(50),ASTD(50),BFT1D(11),BET1PD(11),
1,BET2D(11),BET2PD(11),BET3D(11),BPSD(50),TITL(12)
DIMENSION BO(50),AP0(50),ASC(50)
COMMON I,INC,IPR2,N,VT20T1,NPR,SRTIP,ARRI,DTIP2,DH2,ARHD,ARTD,DRT,
1B2SAVE,C2,D2,E2,VT30T2,NPS,SSH,ARSI,DTIP3,DH3,ASHD,ASTD,DSH,MSH,
2PPSD,B3,C3,D3,E3,W1,RC0,TRO,ETA0,RC,TR,ETA,RTIP1,ARR,ARS,RH1,RTIP2
3,RH2,RTIP3,RH3,BR,BS,M,BET1D,BETA1,BET1PD,BETA1P,R1,U1,VZ1,V01,V1,
4V1P,M1P,M1,MZ1,BET2D,BETA2,BET2PD,BETA2P,R2,U2,VZ2,V02,V2,V2P,DR,
5M2P,M2,MZ2,BET3D,BETA3,R3,VZ3,V03,V3,DS,M3,WRB,ZR,WSB,ZS,MZ3,ALPST
6,ALPSH,IERROR
COMMON IPR1,K1,UTIP1,RM,RHOT1,AONE,RS1VZ1,NM1,RHOS1,TT1,PT1,W2,
1EWA,VZTIP2,A2G,A2E,K2,ITAL1,ALPRH,RHNEW,ANEW,TAARTL,TAARHL,AE,BE,
2CE,ALPRT,RTNEW,B2,TT2,PT2,RHOT2,RHOS2,TS2,ATWO,PRI,ATO,RS2VZ2
3,UTIP2,VOTIP2,Q,R,S,T,ITAL2,AA,BB,CC,DD,ITAL3,BPSH,W3,A3G,A3E,PT3,
4VZTIP3,K3,PRW3,PROW3,TRW3,TRW3,TT3,RHOS3,TAASHL,TAASTL,ASHL,ASTL,
5A3,ATHRE,RS3VZ3,WW3,ITAL8,AF,BF,CF,DF
6,VZTIPO,ARHL,ARTL,RHOT3,TITL,BO,ARO,AS0
6070 WRITE (6,6071) ITAL2,B2(I),V02(N),AA,BB,CC,DD,M2(N),MSH(I)
6071 FORMAT (1H06H ITAL25X5HR2(I)9X6HV02(N)9X2HAA11X2HBB11X2HCC11X2HDD
1 9X5HM2(N)8X6HMSH(I) // I4,2X8F13.5 // )
RETURN
END

```

```

$*
$IBFTC OUT5      LIST
SURROUTINE OUT5
REAL MW,NPR,NPS,MSH,K1,M1P,K2,M2,K3
REAL M1,MZ1,M2P,MZ2,M3,MZ3
DIMENSION M1(11),MZ1(11),M2P(11),MZ2(11),M3(11),MZ3(11),A3(11)
DIMENSION VT20T1(50),NPR(50),SRTIP(50),ARR(50),DTIP2(50),DH2(50),
1ARHL(50),ARTL(50),DRT(50),B2(50),C2(50),D2(50),E2(50),VT30T2(50),
2NPS(50),SSH(50),ARS(50),DTIP3(50),DH3(50),ASHL(50),ASTL(50),
3DSH(50),MSH(50),BPSH(50),B3(50),C3(50),D3(50),E3(50)
DIMENSION VZ1(11),U1(11),V01(11),RHOS1(11),BETA1(11),BETA1P(11),
1V1P(11),M1P(11),TT1(11),PT1(11),RS1VZ1(11),ACNE(11),R2(11),U2(11),
2V02(11),TT2(11),VZ2(11),PT2(11),RHOT2(11),V2(11),RHOS2(11),
3BETA2(11),BETA2P(11),V2P(11),DR(11),TS2(11),ATW0(11),M2(11),
4PRI(11),WRB(11),ZR(11),RS2VZ2(11),ATO(11),TT3(11),R3(11),V03(11),
5PT3(11),RHOT3(11),V3(11),RHOS3(11),BETA3(11),DS(11),WSB(11),
6ZS(11),RS3VZ3(11),ATHRE(11),WW3(11)
DIMENSION R1(11),V1(11),VZ3(11)
DIMENSION ARHD(50),ARTD(50),ASHD(50),ASTD(50),BET1D(11),BET1PD(11)
1,BET2D(11),BET2PD(11),BET3D(11),BPSD(50),TITL(12)
DIMENSION BO(50),ARC(50),ASC(50)
COMMON I,INC,IPR2,N,VT20T1,NPR,SRTIP,ARRI,DTIP2,DH2,ARHD,ARTD,DRT,
1B2SAVE,C2,D2,E2,VT30T2,NPS,SSH,ARSI,DTIP3,DH3,ASHD,ASTD,DSH,MSH,
2BPSD,B3,C3,D3,E3,W1,RCO,TRO,ETA0,RC,TR,ETA,RTIP1,ARR,ARS,RH1,RTIP2
3,RH2,RTIP3,RH3,BS,M,BET1D,BETA1,BET1PD,BETA1P,R1,U1,VZ1,V01,V1,
4V1P,M1P,M1,MZ1,BET2D,BETA2,BET2PD,BETA2P,R2,U2,VZ2,V02,V2,V2P,DR,
5M2P,M2,MZ2,BET3D,BETA3,R3,VZ3,V03,V3,DS,M3,WRB,ZR,WSB,ZS,MZ3,ALPST
6,ALPSH,IERROR
COMMON IPR1,K1,UTIP1,RM,RHOT1,ACNE,RS1VZ1,NM1,RHOS1,TT1,PT1,W2,
1EWA,VZTIP2,A2G,A2E,K2,ITAL1,ALPRH,RHNEW,ANEW,TAARTL,TAARHL,AE,BE,
2CE,ALPRT,RTNEW,R2,TT2,PT2,RHOT2,RHOS2,TS2,ATW0,PRI,ATO,RS2VZ2
3,UTIP2,VNTTP2,Q,R,S,T,ITAL2,AA,BB,CC,DD,ITAL3,BPSH,W3,A3G,A3E,PT3,
4VZTIP3,K3,PRW3,PROW3,TRW3,TRW3,TT3,RHOS3,TAASHL,TAASTL,ASHL,ASTL,
5A3,ATHRE,RS3VZ3,WW3,ITAL8,AF,BF,CF,OF
6,VZTIP0,ARHL,ARTL,RHOT3,TITL,BO,ARC,AS0
6080 WRITE (6,6081) ITAL3,B2(I),BETA2P(N),BPSH(I)
6081 FORMAT (1H08H ITAL35X5HB2(I)6X9HBETA2P(N)5X7HBPSH(I) // 14,2X
1 3F13.5 // )
RETURN
END

```

```

$*
$IBFTC DUT6      LIST
      SUBROUTINE DUT6
      REAL MW,NPR,NPS,MSH,K1,M1P,K2,M2,K3
      REAL M1,MZ1,M2P,MZ2,M3,MZ3
      DIMENSION M1(11),MZ1(11),M2P(11),MZ2(11),M3(11),MZ3(11),A3(11)
      DIMENSION VT20T1(50),NPR(50),SRTIP(50),ARR(50),DTIP2(50),DH2(50),
     1ARHL(50),ARTL(50),DRT(50),B2(50),C2(50),D2(50),E2(50),VT30T2(50),
     2NPS(50),SSH(50),ARS(50),DTIP3(50),DH3(50),ASHL(50),ASTL(50),
     3DSH(50),MSH(50),BPSH(50),B3(50),C3(50),D3(50),E3(50)
      DIMENSION VZ1(11),U1(11),V01(11),RHOS1(11),BETA1P(11),BETA1P(11),
     1V1P(11),M1P(11),TT1(11),PT1(11),RS1VZ1(11),ACNE(11),R2(11),U2(11),
     2V02(11),TT2(11),VZ2(11),PT2(11),RHOT2(11),V2(11),RHOS2(11),
     3BETA2(11),BETA2P(11),V2P(11),DR(11),TS2(11),ATWO(11),M2(11),
     4PRI(11),WRB(11),ZR(11),RS2VZ2(11),ATO(11),TT3(11),R3(11),V03(11),
     5PT3(11),RHOT3(11),V3(11),RHOS3(11),BETA3(11),DS(11),WSB(11),
     6ZS(11),RS3VZ3(11),ATHRE(11),WW3(11)
      DIMENSION R1(11),V1(11),VZ3(11)
      DIMENSION ARHD(50),ARTD(50),ASHD(50),ASTD(50),BET1D(11),BET1PD(11)
     1,BET2D(11),BET2PD(11),BET3D(11),BPSD(50),TITL(12)
      DIMENSION BO(50),ARO(50),ASC(50)
      COMMON I,INC,IPR2,N,VT20T1,NPR,SRTIP,ARR,DTIP2,DH2,ARHD,ARTD,DRT,
     1B2SAVE,C2,D2,E2,VT30T2,NPS,SSH,ARS,DTIP3,DH3,ASHD,ASTD,DSH,MSH,
     2BPSD,B3,C3,D3,E3,W1,RCC,TRD,ETA0,RC,TR,ETA,RTIP1,ARR,ARS,RH1,RTIP2
     3,RH2,RTIP3,RH3,BR,BS,M,BET1D,BETA1,BET1PD,BETA1P,R1,U1,VZ1,V01,V1,
     4V1P,M1P,M1,MZ1,BET2D,BETA2,BET2PD,BETA2P,R2,U2,VZ2,V02,V2,V2P,DR,
     5M2P,M2,MZ2,BET3D,BETA3,R3,VZ3,V03,V3,DS,M3,WRB,ZR,WSB,ZS,MZ3,ALPST
     6,ALPSH,IERROR
      COMMON IPR1,K1,UTIP1,RM,RHOT1,ACNE,RS1VZ1,NM1,RHOS1,TT1,PT1,W2,
     1EWA,VZTIP2,A2G,A2E,K2,ITAL1,ALPRH,RHNEW,ANEW,TAARTL,TAARHL,AE,BE,
     2CE,ALPRT,RTNEW,B2,TT2,PT2,RHOT2,RHOS2,TS2,ATWO,PRI,ATO,RS2VZ2
     3,UTIP2,VOTIP2,Q,R,S,T,ITAL2,AA,BB,CC,DD,ITAL3,BPSH,W3,A3G,A3E,PT3,
     4VZTIP3,K3,PRW3,PROW3,TRW3,TRGW3,TT3,RHOS3,TAASHL,TAASTL,ASHL,ASTL,
     5A3,ATHRE,RS3VZ3,WW3,ITAL8,AF,BF,CF,DF
     6,VZTIP0,ARHL,ARTL,RHOT3,TITL,BO,ARC,ASO
      GO TO (6130,6135),IPR1
6130 WRITE (6,6131) W1,W3,EWA,RC,RC0,TR,TR0,FTA,ETAC
6131 FORMAT (1H07X2HW11X2HW311X3HEWA1UX2HRC11X3HRC010X2HTR11X3HTR01UX
     13HETA9X4HETA0 // 9F13.5 // )
      RETURN
6135 WRITE (6,6131) W1,W3,EWA,RC,RC0,TR,TR0,ETA,ETA0
      WRITE (6,6136) BS,RTIP3,RH3,A3G,A3E,VZTIP3,K3,PRW3,PROW3,TRW3,
     1 TROW3
6136 FORMAT (1H013X2HRS17X5HRTIP316X3HRH317X3HA3G17X3HA3E15X6HVZTIP3 //
     1 6E20.8 // 13X2HK317X4HPRW316X5HPROW315X4HTRW316X5HTROW3 // 5E20.8 // //
     211X3HTT314X2HR315X3HVZ314X3HV0314X3HPT313X5HRHOS313X2HV3 // )
      DO 6137 M=1,N
6137 WRITE (6,6025) TT3(M),R3(M),VZ3(M),V03(M),PT3(M),RHOS3(M),V3(M)
6025 FORMAT (7E17.8)
      WRITE (6,6132) ALPSH,RHNEW,ANEW,TAASTL,TAASHL,ASHL(I),AE,BE,CE,ARS
     1(I),ALPST,RTNEW,ASTL(I)
6132 FORMAT (1H0/24X5HALPSH12X5HRHNEW13X4HANEW12X6HTAASTL11X6HTAAASHL10X
     17HASHL(I) // 17X6E17.8 // 9X2HAE15X2HBE15X2HCE13X6HARS(I)11X5HALPST
     212X5HRTNEW11X7HASTL(I) // 7E17.8 )
      WRITE (6,6138)
6138 FORMAT (1H08X5HBETA315X2HDS14X3HWSB15X2HZS // )
      DO 6139 M=1,N
6139 WRITE (6,6140) BETA3(M),DS(M),WSB(M),ZS(M)

```

```
6140 FORMAT (4E17.8)
      WRITE (6,6141) (A3(M),M3(M),M23(M),M=1,N)
6141 FORMAT (1H011X2HA315X2HM314X3HM23//(3E17.8))
      WRITE (6,6142) (ATHRE(M),RS3VZ3(M),WW3(M),M=1,NM1)
6142 FORMAT (1H08X5HATHRE12X6HRS3VZ313X3HWW3 // (3E17.8))
      RETURN
      END
```

```

** $IBFTC OUT7      LIST
      SUBROUTINE OUT7
      REAL MW,NPR,NPS,MSH,K1,M1P,K2,M2,K3
      REAL M1,MZ1,M2P,MZ2,M3,MZ3
      DIMENSION M1(11),MZ1(11),M2P(11),MZ2(11),M3(11),MZ3(11),A3(11)
      DIMENSION VT20T1(50),NPR(50),SRTIP(50),ARR(50),DTIP2(50),DH2(50),
1ARHL(50),ARTL(50),DRT(50),B2(50),C2(50),D2(50),E2(50),VT30T2(50),
2NPS(50),SSH(50),ARS(50),DTIP3(50),DH3(50),ASHL(50),ASTL(50),
3DSH(50),MSH(50),BPSH(50),B3(50),C3(50),D3(50),E3(50)
      DIMENSION VZ1(11),U1(11),V01(11),RHOS1(11),BETA1(11),BETA1P(11),
1V1P(11),M1P(11),TT1(11),PT1(11),RS1VZ1(11),ACNE(11),R2(11),U2(11),
2V02(11),TT2(11),VZ2(11),PT2(11),RHOT2(11),V2(11),RHOS2(11),
3BETA2(11),BETA2P(11),V2P(11),DR(11),TS2(11),ATWO(11),M2(11),
4PRI(11),WRB(11),ZP(11),RS2VZ2(11),ATO(11),TT3(11),R3(11),V03(11),
5PT3(11),RHOT3(11),V3(11),RHOS3(11),BETA3(11),DS(11),WSB(11),
6ZS(11),RS3VZ3(11),ATHRE(11),WW3(11)
      DIMENSION R1(11),V1(11),VZ3(11)
      DIMENSION ARHD(50),ARTD(50),ASHD(50),ASTD(50),BET1D(11),BET1PD(11)
1,BET2D(11),BET2PD(11),BET3D(11),BPSD(50),TITL(12)
      DIMENSION BO(50),ARO(50),ASC(50)
      COMMON I,INC,IPR2,N,VT20T1,NPR,SRTIP,ARRI,DTIP2,DH2,ARHD,ARTD,DRT,
1B2SAVE,C2,D2,E2,VT30T2,NPS,SSH,ARSI,DTIP3,DH3,ASHD,ASTD,DSH,MSH,
2BPSD,B3,C3,D3,E3,W1,RCO,TRO,ETA0,RC,TR,ETA,RTIPI,ARR,ARS,RH1,RTIP2
3,RH2,RTIP3,RH3,BR,BS,M,BET1D,BFTA1,BET1PD,BETA1P,R1,U1,VZ1,V01,V1,
4V1P,M1P,M1,MZ1,BET2D,BETA2,BET2PD,BETA2P,R2,U2,VZ2,V02,V2,V2P,DR,
5M2P,M2,MZ2,BET3D,BETA3,R3,VZ3,V03,V3,DS,M3,WRB,ZR,WSB,ZS,MZ3,ALPST
6,ALPSH,IERROR
      COMMON IPR1,K1,UTIPI,RM,RHOT1,ACNE,RSIVZ1,NM1,RHOS1,TT1,PT1,W2,
1EWA,VZTIPO,A2G,A2E,K2,ITAL1,ALPRH,RHNEW,ANEW,TAARTL,TAARHL,AE,BE,
2CE,ALPRT,RTNEW,B2,TT2,PT2,RHOT2,RHOS2,TS2,ATWO,PRI,ATO,RS2VZ2
3,UTIPI,RVOTIPO,Q,R,S,T,ITAL2,AA,RR,CC,DD,ITAL3,BPSH,W3,A3G,A3E,PT3,
4VZTIPO,K3,PRW3,PROW3,TRW3,TROW3,TT3,RHOS3,TAASHL,TAASTL,ASHL,ASTL,
5A3,ATHRE,RS3VZ2,WW3,ITAL8,AF,BF,CF,DF
6,VZTIPO,ARHL,ARTL,RHOT3,TITL,BO,ARC,ASO
6150 WRITE (6,6151) ITAL8,B2(11),V02(N),AF,BF,CF,DF,DS(N),DSH(I)
6151 FORMAT (1H0SH ITALR10X5HB2(I)12X6HV02(N)14X2HAF16X2HBF16X2HCF 16X
1 2HDF // I4.2X6F18.8 // 16X5HDS(N) 12X 6HDSH(I) // 6X 2E18.8
2 //25X69H*** THIS BRANCH RETURNS TO ROTOR CAL
3CULATION AT STATEMENT NO. 160 *** // )
      RETURN
      END
$DATA

```

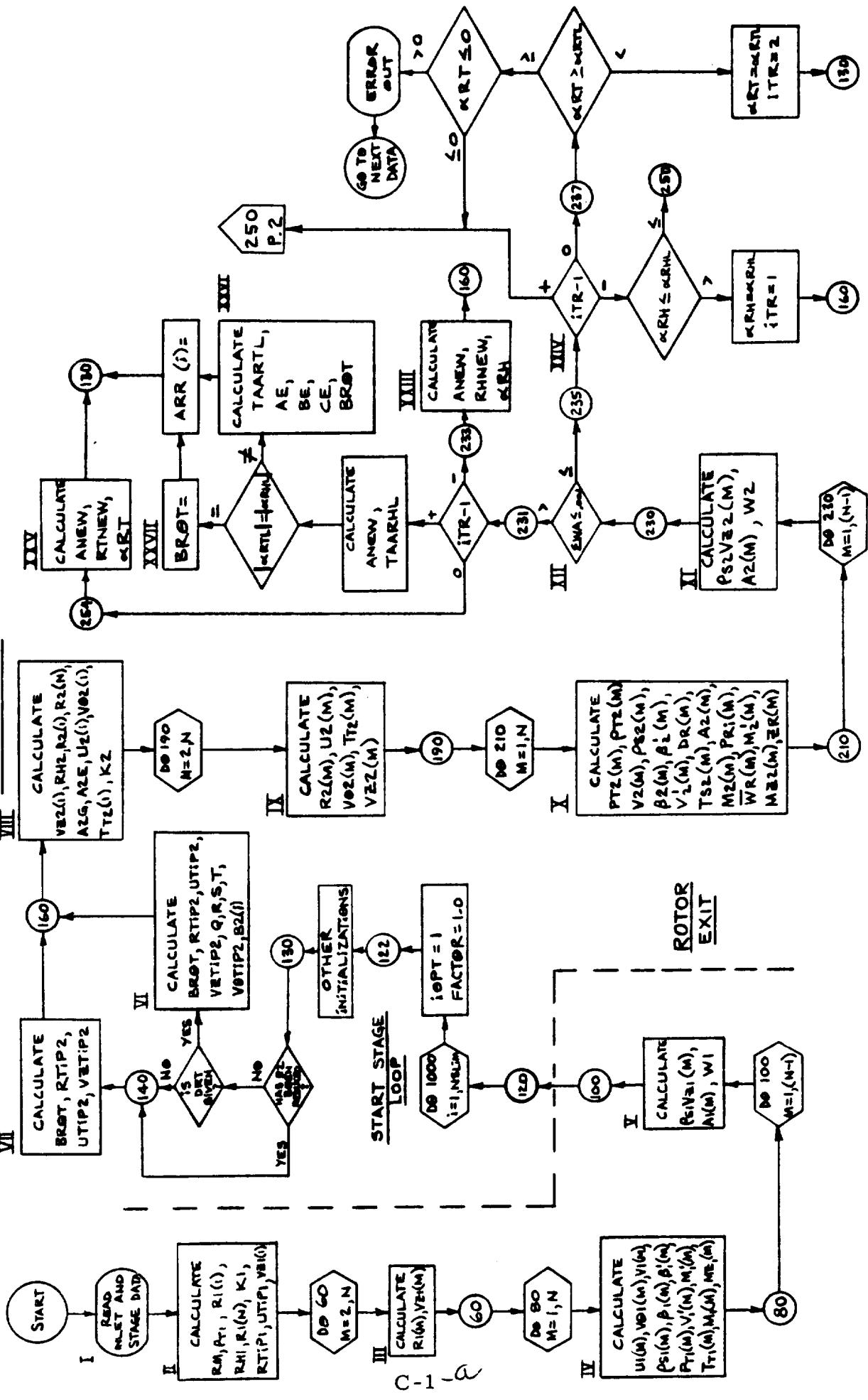
APPENDIX C

PROGRAM FLOW CHARTS

(l-1)

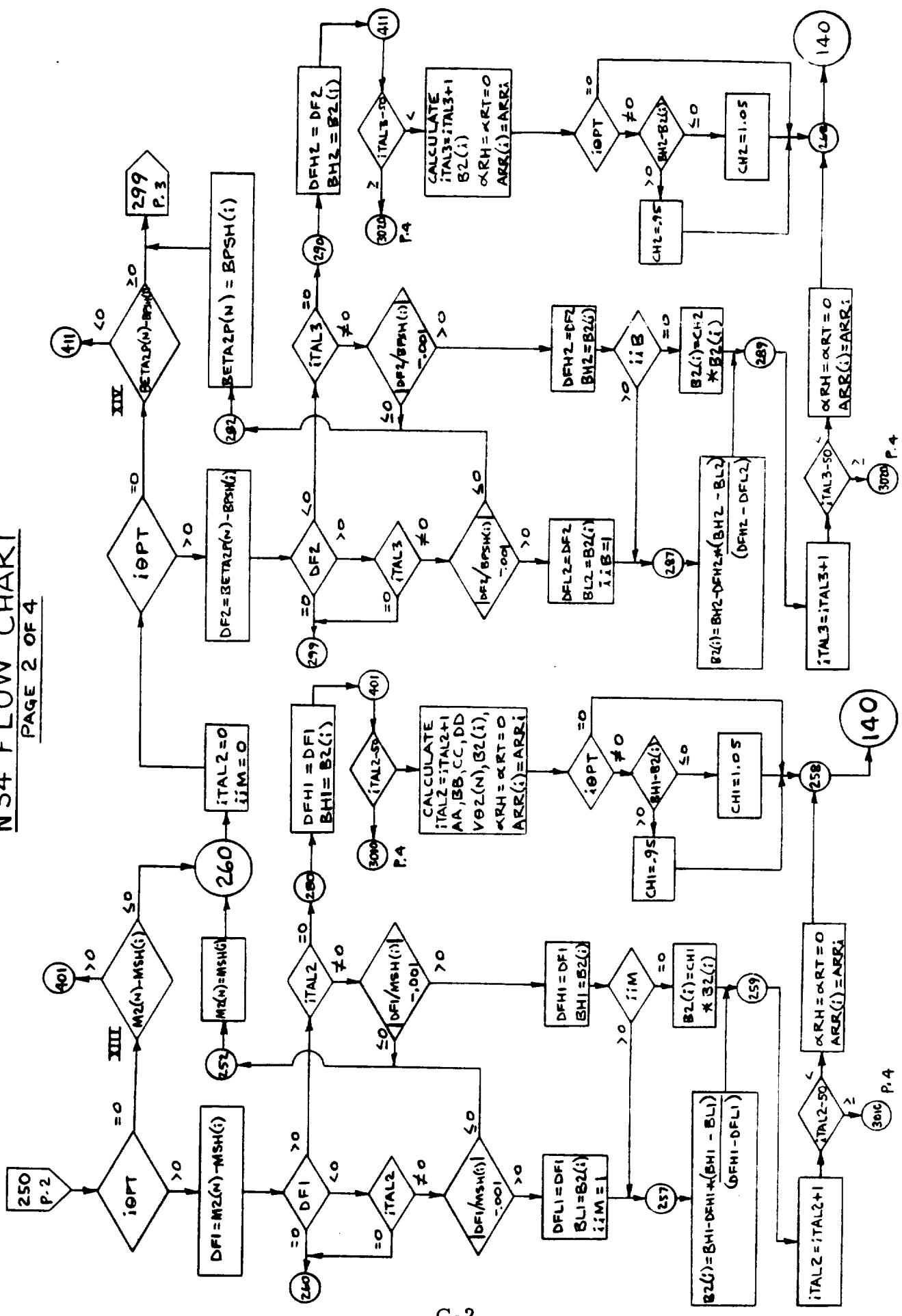
N 34 FLOW CHART

PAGE 1 OF 4



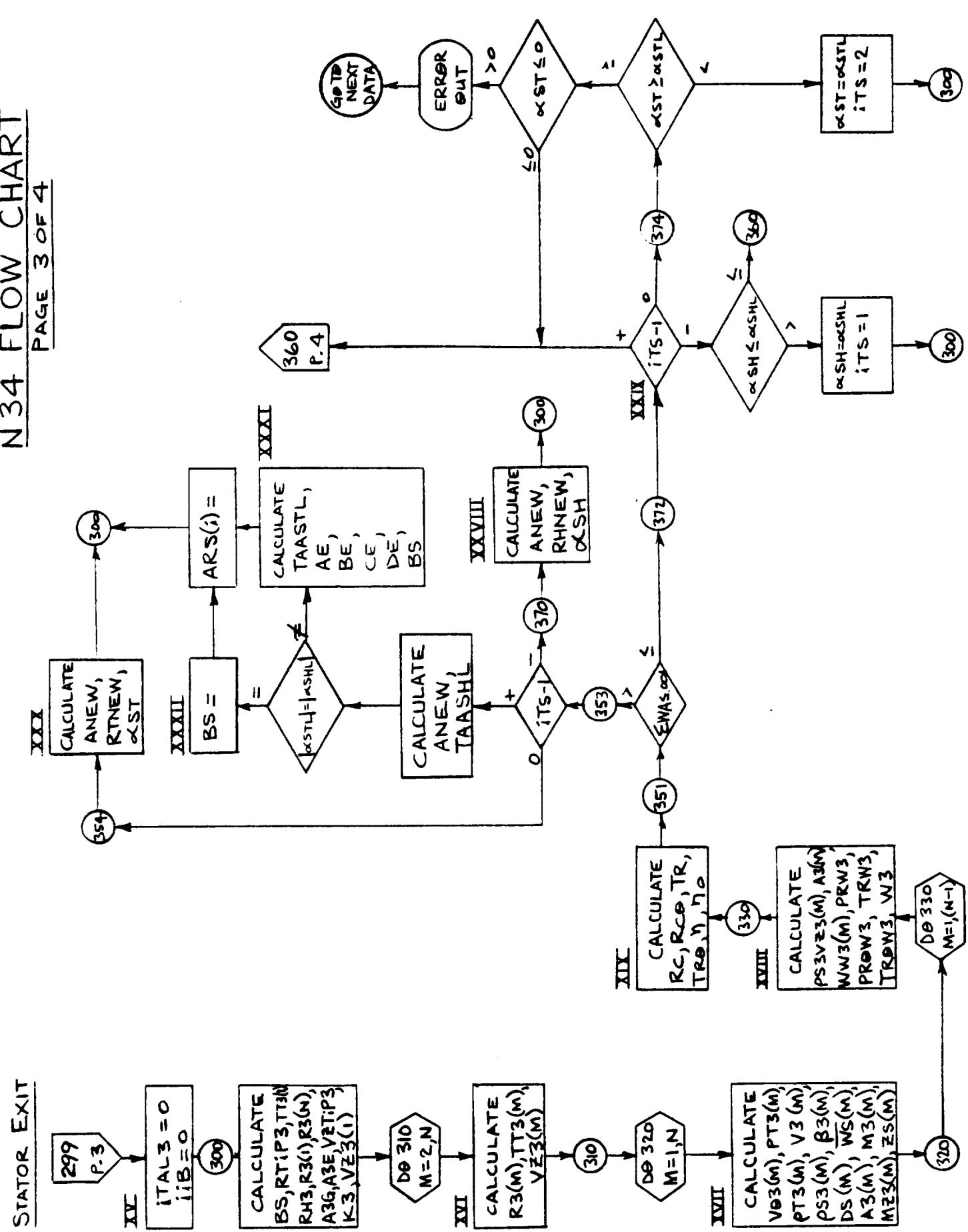
N34 FLOW CHART

PAGE 2 OF 4



N 34 FLOW CHART

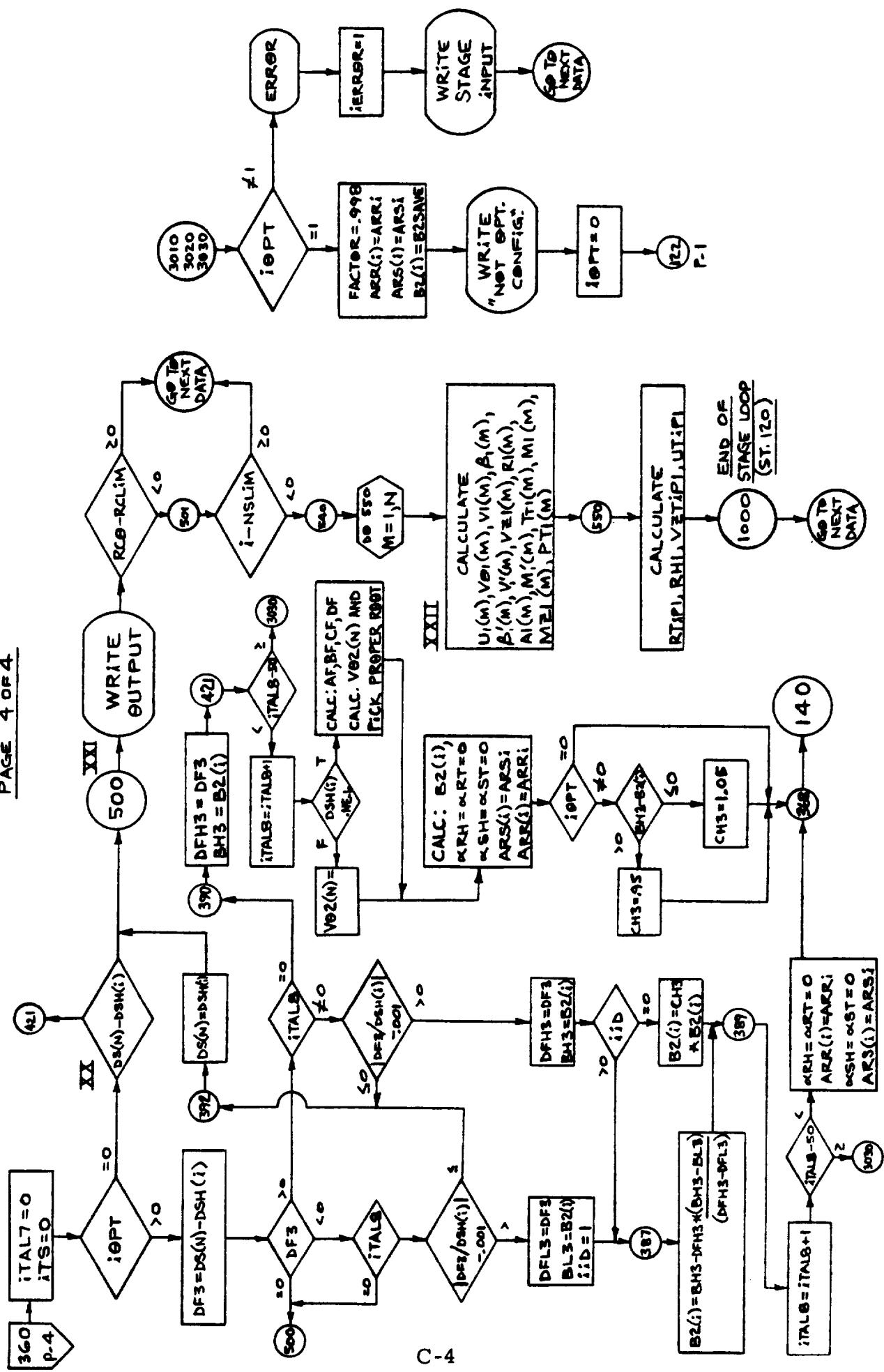
PAGE 3 OF 4



STATOR EXIT

N 34 FLOW CHART
PAGE 4 OF 4

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APPENDIX D

INPUT FORMAT - DATA PREPARATION

D-1

N34 DATA PREPARATION

The N34 program utilizes the option of using the FORTRAN IV NAMELIST method of data input. The standard input method may still be used and the two may be intermixed from one data set to the next within a run. In either case, each input should be entered as a decimal number except IREAD, N, NSLIM, IPR1, and IPR2 which are integers. A sample data sheet for each method is included.

STANDARD OPTION

Card 1

Column 1 must contain a 1 which signifies that the standard input option is to be used. Columns 2 through 72 contain alphanumeric information to be printed at the beginning of the run.

Remaining Cards

These cards are used as shown on the data sheet.

NAMELIST OPTION

Card 1

Column 1 must contain a 0 (zero) which signifies that the NAMELIST option is to be used. Columns 2 through 72 contain alphanumeric information to be printed at the beginning of the run.

Card 2

Card 2 is the first card used by NAMELIST. Column 1 must be blank. Columns 2 through 6 must contain "\$NAME". Column 7 must be blank. The remainder of Card 2 is similar to Card 3 through the last card.

Card 3 Through the Last Card

These cards are punched as in the NAMELIST sample. Any number of sets of "variable = constant," may be put on a card, but the following conditions must be met.

1. Column 1 must always be blank.
2. No blanks are permitted except at end of card and in Column 1.
3. Each data card must end with a comma following a "variable = constant" set with the exception of the last card of a data set.

4. The last card of a data set must end with a \$ symbol.
5. Arrays are read as on the 5th card of the NAMELIST sample data sheet.

Example: SRTIP will contain 1.3 in 10 locations beginning with SRTIP(1). ARO will contain 4. in (1), 3.5 in (2), and 2.5 in 8 locations beginning with ARO(3).

Additional Comments on NAMELIST

The input parameters may be in any order on the cards. More or less items may be put on a card than are shown in the sample and may appear in any column (other than Column 1). Columns 73 through 80 are for data (NAMELIST ONLY) and may not be used for identification. More numbers may be read into an array than can be put on one card. The first card must end with a constant followed by a comma, and the next card must start with the next constant beginning in Column 2 and continuing on as before.

STACKING DATA

Data sets may be stacked. The option of using NAMELIST or the standard method of input may be changed from set to set within a run. Once the initial data have been read by either method, new sets may be read by using a complete standard data set or with NAMELIST as follows: A title card with a zero in Column 1 is followed by the card(s) needed to change any value(s) used in the initial data set. These cards must follow the same rules as a complete NAMELIST data set. The flexibility of the NAMELIST option will allow the input data to be simplified to whatever degree the user wishes.

N 34 SAMPLE DATA SHEET (STANDARD)

READ

IDENTIFICATION
NUMBER

ONE TITLE CARD OF ALPHANUMERIC INFORMATION									
1	C _P (BTU/LB°R)	GAM (OR)	P _{T1} (PSI)	RCLIM (INCHES)	D _{T1P1} (FT/SEC)	UT _{T1P1} (FT/SEC)	RH/R _{T1P1}		
					B1	E1	N	N3	I _{P1} R ₁
*	V _{T1P1} (FT/SEC)	D _{H1}							I _{P1} R ₂
*	V _{T2BT1} (1)	NPR(1)	SRTIP(1)	ARR(1)	DTIP2(1)	DH2(1)	ARHL(1) (DEGREES)	ARTL(1) (DEGREES)	ROTSE 1
*	DRT(1)	B2(1)	C2(1)	D2(1)	E2(1)				ROTSE 1
*	VT3BT2(1)	NPS(1)	SSH(1)	ARS(1)	DTIP3(1)	DH3(1)	A _{SHL} (1) (DEGREES)	A _{STL} (1) (DEGREES)	ROTTER 1
*	DSH(1)	M _{SH} (1)	BPSH(1)	B3(1)	C3(1)	D3(1)	E3(1)		ROTTER 1
*	DRT(NS)	NPR(NS)	SRTIP(NS)	ARR(NS)	DTIP2(NS)	DH2(NS)	ARHL(NS) (DEGREES)	ARTL(NS) (DEGREES)	ROTOR(NS)
*	VT2BT(NS)	NPS(NS)	SSH(NS)	ARS(NS)	DTIP3(NS)	DH3(NS)			ROTTER(NS)
*	DSH(NS)	M _{SH} (NS)	BPSH(NS)	B3(NS)	C3(NS)	D3(NS)	E3(NS)		ROTTER(NS)

* D-3

* NOTE: CONTINUE THESE 4 CARDS IN ORDER
UNTIL NO. STAGES IS COMPLETED.

N 34 SAMPLE DATA SHEET

READ

TITLE CARD
 STD. DATA
 NASA DATA
 \$NAME CP=.24, MW=29., GAM=1.4, TTI=519., PTi=14:7, RCCLiM=9., RTiPi(i=12.)
 UTiPi(i=100., RHRTi=1.4, VTiP0=600., DTiPi(i=1., DH1=1., BI=0., CI=0., DI=0.),
 EI=0., N=11, NSLIM=10, iPRI=0, iPR2=0, VT20Ti(i)=10*1., NPR(i)=10*.85,
 SRTiP(i)=10*1.3, AR0(i)=4., 3.5, 8*2.5, DTiP2(i)=10*1., DH2(i)=10*1.,
 ARHD(i)=10*40., ARTD(i)=10*-20., DRT(i)=.35, .4, 8*.45, B0(i)=10*0.,
 C2(i)=10*0., D2(i)=10*0., E2(i)=10*0., VT30Ti(i)=10*1., NPS(i)=10*.85,
 SSH(i)=10*2., ASE(i)=4., 3.5, 8*2.5, DTiP3(i)=10*1., DH3(i)=10*1.,
 ASHD(i)=10*40., ASTD(i)=10*-20., DSH(i)=10*.5, MSH(i)=10*.8,
 BPSD(i)=10*-10., B3(i)=10*0., C3(i)=10*0., D3(i)=10*0., E3(i)=10*0., \$
 BPSD(i)=0.04

APPENDIX E

OUTPUT FORMAT—SAMPLE PROBLEMS

E-1

FREE VERTEX CASE

ADVANCED MULTISTAGE AXIAL-FLOW COMPRESSORS * * * * *

*** A I D E U T Z

NO. RAD. STATIONS	NORM SEP STAGES	SP. HEAT (BTU/(LB-°F))	WCL. WT. (MOLDS)	RATIO OF SP. HEAT	IN. TOT. TEMP. (DEG. R)	IN. TOT. PR. (PSI)	MASS AVG. TOR. PR. RATIO
11	1.0	0.2430	2.0 • 1.00	1.04000	519.0000	14.700	9.0000

HUB RADIUS (INCHES)	TIP WHEEL SPEED (FT/SEC.)	HUB TO TIP RADIAL DISTANCE (INCHES)	AXIAL VEL. (FT/SEC.)	TIP BLOCKAGE FACTOR	HUB BLOCKAGE FACTOR
4.000	4.000	4.000	4.000	1.000	1.000
4.000	4.000	4.000	4.000	1.000	1.000

CATHOLIC CHURCH IN LANCASHIRE VOLUME EIGHT

*** 21100 AIR RAM ANGLE LIMIT VIOLATED ***

*** 21100 MACH NO. LIMIT VIOLATED ***

*** 21100 ALFA CRITATIVE ANGLE LIMIT VIOLATED ***

* * * * * ROTOR INLET OUTPUT DATA * * * * *

STAN NO.	RADIUS IN.	WHEEL SPEED (FT/SEC)	Axial Vel. (FT/SEC)	Tangent. (FT/SEC)	Abs. Vel. (FT/SEC)	REL. (FT/SEC)	AIR ANG. (DEG)	TEMP. (DEG R)	TOTAL PRESS. (PSI)	REL. MACH NO.	ABS. MACH NO.	LOSS COEFF
1	12.000	10.000	50.000	50.000	50.000	50.000	50.000	50.000	519.000	1.076	0.554	0.082
2	11.290	54.000	50.000	50.000	50.000	50.000	50.000	50.000	519.000	1.029	0.554	0.089
3	10.560	38.450	50.000	50.000	50.000	50.000	50.000	50.000	519.000	0.953	0.554	0.095
4	9.940	32.000	50.000	50.000	50.000	50.000	50.000	50.000	519.000	0.939	0.554	0.103
5	9.120	27.600	50.000	50.000	50.000	50.000	50.000	50.000	519.000	0.894	0.554	0.111
6	8.430	23.000	50.000	50.000	50.000	50.000	50.000	50.000	519.000	0.851	0.554	0.120
7	7.580	18.450	50.000	50.000	50.000	50.000	50.000	50.000	519.000	0.810	0.554	0.130
8	6.950	15.000	50.000	50.000	50.000	50.000	50.000	50.000	519.000	0.770	0.554	0.141
9	6.240	12.500	50.000	50.000	50.000	50.000	50.000	50.000	519.000	0.733	0.554	0.152
10	5.520	10.000	50.000	50.000	50.000	50.000	50.000	50.000	519.000	0.698	0.554	0.165
11	4.900	8.000	50.000	50.000	50.000	50.000	50.000	50.000	519.000	0.666	0.554	0.178

* * * * * ROTOR EXIT OUTPUT DATA * * * * *

STAN NO.	RADIUS IN.	WHEEL SPEED (FT/SEC)	Axial Vel. (FT/SEC)	Tangent. (FT/SEC)	Abs. Vel. (FT/SEC)	REL. (FT/SEC)	AIR ANG. (DEG)	TEMP. (DEG R)	TOTAL PRESS. (PSI)	REL. MACH NO.	ABS. MACH NO.	LOSS FUNC
1	12.000	10.000	50.000	50.000	50.000	50.000	50.000	50.000	573.955	20.007	0.328	0.021
2	11.290	55.2497	50.000	50.000	50.000	50.000	50.000	50.000	573.955	20.007	0.344	0.023
3	10.560	49.458	50.000	50.000	50.000	50.000	50.000	50.000	573.955	20.007	0.352	0.024
4	9.940	45.7222	50.000	50.000	50.000	50.000	50.000	50.000	573.955	20.007	0.359	0.026
5	9.120	40.525	50.000	50.000	50.000	50.000	50.000	50.000	573.955	20.007	0.366	0.028
6	8.430	37.225	50.000	50.000	50.000	50.000	50.000	50.000	573.955	20.007	0.373	0.030
7	7.580	34.2175	50.000	50.000	50.000	50.000	50.000	50.000	573.955	20.007	0.373	0.031
8	6.950	31.443	50.000	50.000	50.000	50.000	50.000	50.000	573.955	20.007	0.369	0.032
9	6.240	29.031	50.000	50.000	50.000	50.000	50.000	50.000	573.955	20.007	0.356	0.033
10	5.520	27.155	50.000	50.000	50.000	50.000	50.000	50.000	573.955	20.007	0.329	0.033
11	4.900	25.473	50.000	50.000	50.000	50.000	50.000	50.000	573.955	20.007	0.329	0.033

* * * * * STATOR EXIT OUTPUT DATA * * * * *

STAN NO.	RADIUS IN.	WHEEL SPEED (FT/SEC)	Axial Vel. (FT/SEC)	Tangent. (FT/SEC)	Abs. Vel. (FT/SEC)	REL. (FT/SEC)	AIR ANG. (DEG)	TEMP. (DEG R)	TOTAL PRESS. (PSI)	REL. MACH NO.	ABS. MACH NO.	LOSS FUNC
1	12.000	10.000	50.000	50.000	50.000	50.000	50.000	50.000	50.000	0.640	0.345	0.525
2	11.290	55.2497	50.000	50.000	50.000	50.000	50.000	50.000	50.000	0.639	0.353	0.525
3	10.560	49.458	50.000	50.000	50.000	50.000	50.000	50.000	50.000	0.638	0.362	0.525
4	9.940	45.7222	50.000	50.000	50.000	50.000	50.000	50.000	50.000	0.637	0.372	0.525
5	9.120	40.525	50.000	50.000	50.000	50.000	50.000	50.000	50.000	0.636	0.384	0.525
6	8.430	37.225	50.000	50.000	50.000	50.000	50.000	50.000	50.000	0.635	0.397	0.525
7	7.580	34.2175	50.000	50.000	50.000	50.000	50.000	50.000	50.000	0.641	0.411	0.525
8	6.950	31.443	50.000	50.000	50.000	50.000	50.000	50.000	50.000	0.633	0.427	0.525
9	6.240	29.031	50.000	50.000	50.000	50.000	50.000	50.000	50.000	0.630	0.446	0.525
10	5.520	27.155	50.000	50.000	50.000	50.000	50.000	50.000	50.000	0.628	0.467	0.525
11	4.900	25.473	50.000	50.000	50.000	50.000	50.000	50.000	50.000	0.626	0.491	0.525

No data output appears on this
page since there were no aerodynamic
parameter or geometric violations.

***** STAGE DATA *****

STAGE NO. 2

*** ROTOR INPUT DATA ***

AXIAL VEL. RATIO	ROT. TIP VEL. (IN/SEC)	SOLIDITY AT TIP	ASPECT RATIO	TIP BLOCKAGE FACTOR	HUB BLOCKAGE FACTOR	MAX ANGLE HUB TAPER (DEGREES)
1.0000	2.0175	0.3000	2.0000	1.0000	1.0000	-20.0000

MAX. STATOR VFL. RATIO	ROT. TIP VEL. (IN/SEC)	SOLIDITY AT TIP	ASPECT RATIO	TIP BLOCKAGE FACTOR	HUB BLOCKAGE FACTOR	MAX ANGLE HUB TAPER (DEGREES)
1.0000	2.0175	0.3000	2.0000	1.0000	1.0000	-20.0000

MAX. STATOR
VFL. RATIO = 1.0000
ROT. TIP VEL. (IN/SEC) = 2.0175
SOLIDITY AT TIP = 0.3000
ASPECT RATIO = 2.0000

*** STATOR INPUT DATA ***

AXIAL VFL. RATIO	ROT. TIP VEL. (IN/SEC)	SOLIDITY AT TIP	ASPECT RATIO	TIP BLOCKAGE FACTOR	HUB BLOCKAGE FACTOR	MAX ANGLE HUB TAPER (DEGREES)
1.0000	2.0175	0.3000	2.0000	1.0000	1.0000	-20.0000

MAX. STATOR VFL. RATIO	ROT. TIP VEL. (IN/SEC)	SOLIDITY AT TIP	ASPECT RATIO	TIP BLOCKAGE FACTOR	HUB BLOCKAGE FACTOR	MAX ANGLE HUB TAPER (DEGREES)
1.0000	2.0175	0.3000	2.0000	1.0000	1.0000	-20.0000

E-8

***** STAGE OUTPUT DATA *****

MASS FLOW (LB/SEC) = 104.443

OVERALL MASS AVE. EFF. RATIO	ROT. TIP VEL. (IN/SEC)	ROT. TIP MASS AVE. EFFICIENCY	ROT. TIP MASS AVE. PRESSURE RATIO	MASS AVE. TEMPERATURE RATIO	MASS AVE. EFFICIENCY	POT. ASPECT RATIO	STATOR PROJ. LENGTH (INCHES)	STATOR PROJ. LENGTH (INCHES)
1.0000	2.0175	1.0000	1.0000	1.0000	1.0000	3.0000	3.0000	3.0000

ROT. TIP RAD. 3-G (INCHES)	ROT. TIP RAD. 2-G (INCHES)	ROT. TIP RAD. 3-G (INCHES)	ROT. TIP RAD. 2-G (INCHES)	STATOR RAD. 3-G (INCHES)	STATOR RAD. 3-G (INCHES)	STATOR RAD. 3-G (INCHES)	STATOR PROJ. LENGTH (INCHES)	STATOR PROJ. LENGTH (INCHES)
12.0000	2.0175	12.0000	7.0764	12.0000	7.0764	12.0000	1.0000	1.0000

ROT. TIP RAD. ANGLE (DEGREES)	STATOR HUB RAMP ANGLE (DEGREES)	STATOR HUB RAMP ANGLE (DEGREES)						
1.0000	2.0175	1.0000	2.0175	1.0000	2.0175	1.0000	1.0000	1.0000

16.8212

***** ROTOR INLET OUTPUT DATA *****

STA NO.	RADIUS (IN)	WHEEL SPFED (FT/SEC)	AXIAL VEL. (FT/SEC)	TANGENT. VEL. (FT/SEC)	AHS. (FT/SEC)	RFL. VFL. (FT/SEC)	ABS. AIR ANG. (DEG)	REL. AIR ANG. (DEG)	TOTAL TEMP. (DEG R)	TOTAL PRESS. (PSI)	REL. MACH NO.	LOSS COEF.
1	12.000	1.0000	0.0000	0.0000	116.190	J.0000	59.330	573.955	19.832	J.994	0.511	0.99
2	11.481	0.5834	0.0000	0.0000	112.9276	J.0000	57.906	573.955	19.832	J.962	0.511	0.104
3	10.561	0.3344	0.0000	0.0000	109.2930	J.0000	56.639	573.955	19.832	J.931	0.511	0.110
4	10.441	0.2782	0.0000	0.0000	105.6703	J.0000	55.410	573.955	19.832	J.900	0.511	0.116
5	9.321	0.2575	0.0000	0.0000	102.1547	J.0000	54.031	573.955	19.832	J.870	0.511	0.122
6	8.447	0.2470	0.0000	0.0000	98.5426	J.0000	52.654	573.955	19.832	J.841	0.511	0.129
7	8.882	0.2154	0.0000	0.0000	95.2508	J.0000	50.971	573.955	19.832	J.812	0.511	0.137
8	9.362	0.2059	0.0000	0.0000	92.0572	J.0000	49.271	573.955	19.832	J.783	0.511	0.145
9	7.443	0.1553	0.0000	0.0000	80.0244	J.0000	47.46	573.955	19.832	J.756	0.511	0.154
10	7.322	0.1324	0.0000	0.0000	75.6304	J.0000	45.485	573.955	19.832	J.729	0.511	0.163
11	6.303	0.0924	0.0000	0.0000	425.433	J.0000	43.377	573.955	19.832	J.703	0.511	0.173

***** ROTOR EXIT OUTPUT DATA *****

STA NO.	RADIUS (IN)	WHEEL SPFED (FT/SEC)	AXIAL VEL. (FT/SEC)	TANGENT. VEL. (FT/SEC)	AHS. (FT/SEC)	RFL. VFL. (FT/SEC)	ABS. AIR ANG. (DEG)	REL. AIR ANG. (DEG)	TOTAL TEMP. (DEG R)	TOTAL PRESS. (PSI)	REL. MACH NO.	LOSS FUNC.
1	12.000	1.0000	0.0000	0.0000	351.700	33.285	45.219	639.780	27.654	L.440	0.712	0.327
2	11.577	0.6477	0.0000	0.0000	255.427	81.730	34.335	42.767	539.780	C.408	J.683	0.608
3	11.155	0.52374	0.0000	0.0000	425.342	73.547	78.394	35.334	539.780	C.415	J.656	0.630
4	10.732	0.49432	0.0000	0.0000	44.204	74.520	751.359	45.384	37.002	L.423	J.629	0.624
5	10.310	0.45314	0.0000	0.0000	46.021	75.517	721.517	37.482	33.619	L.430	J.604	0.634
6	9.987	0.2335	0.0000	0.0000	47.690	76.515	541.642	38.653	29.830	L.437	J.561	0.645
7	9.465	0.21722	0.0000	0.0000	54.421	78.136	56.523	39.979	25.595	L.441	J.560	0.658
8	9.442	0.2155	0.0000	0.0000	78.274	78.730	542.033	41.172	20.471	L.454	J.672	0.638
9	8.520	0.2026	0.0000	0.0000	55.046	52.303	523.031	42.635	15.627	L.442	J.526	0.639
10	8.157	0.1933	0.0000	0.0000	57.821	43.370	43.988	43.972	9.885	L.454	J.515	0.705
11	7.774	0.1770	0.0000	0.0000	555.442	51.1075	45.489	3.593	639.780	L.454	J.510	0.726

***** STATOR EXIT OUTPUT DATA *****

STA NO.	RADIUS (IN)	WHEEL SPFED (FT/SEC)	AXIAL VEL. (FT/SEC)	TANGENT. VEL. (FT/SEC)	AHS. (FT/SEC)	RFL. VFL. (FT/SEC)	ABS. AIR ANG. (DEG)	REL. AIR ANG. (DEG)	TOTAL TEMP. (DEG R)	TOTAL PRESS. (PSI)	REL. MACH NO.	LOSS FUNC.
1	12.000	1.0000	0.0000	0.0000	220.0	J.0000	0.044	0.372	0.496	0.016		
2	11.614	0.643	0.0000	0.0000	60.000	J.0000	0.043	1.496	0.496	0.016		
3	11.229	0.5200	0.0000	0.0000	52.000	J.0000	0.042	0.398	1.496	0.496	0.015	
4	10.842	0.4900	0.0000	0.0000	50.000	J.0000	0.041	0.395	1.496	0.496	0.014	
5	10.456	0.4500	0.0000	0.0000	48.000	J.0000	0.040	0.405	1.496	0.496	0.013	
6	10.070	0.4100	0.0000	0.0000	46.000	J.0000	0.039	0.415	1.496	0.496	0.012	
7	9.494	0.3800	0.0000	0.0000	44.000	J.0000	0.038	0.425	0.496	0.496	0.011	
8	9.298	0.3500	0.0000	0.0000	42.000	J.0000	0.036	0.437	1.496	0.496	0.010	
9	8.912	0.3200	0.0000	0.0000	40.000	J.0000	0.035	0.449	0.496	0.496	0.009	
10	8.525	0.3000	0.0000	0.0000	38.000	J.0000	0.033	0.463	0.496	0.496	0.008	
11	8.130	0.2800	0.0000	0.0000	36.000	J.0000	0.032	0.477	0.496	0.496	0.007	

No data output appears on this
page since there were no aerodynamic
parameter or geometric violations.

***** STAGE DATA *****

STAGE NO. 2

*** RECTOR INPUT DATA ***

COEFFICIENTS IN TANGENTIAL VELOCITY EQUATION					
AXIAL VFL. RATION	POLYTRAPIC EFFICIENCY	SOLIDITY AT TIP	ASPFCT RATIO	TIP BLOCKAGE FACTOR	HUB BLOCKAGE FACTOR
1.0000	1.0751	1.0000	1.0000	1.0000	1.0000
MAX. RATOR DIF. FACTOR	AVNL. FLWN ANGLE ROTAT HUB	(DEGREES)	H	C	D
0.4532	-1.2000	-0.0000	0.0000	0.0000	0.0000
MAX ANGLE HUB TAPER (DEGREES)	MAX ANGLE TIP TAPER (DEGREES)			E	G.0000
0.0000	-20.00				

STATJR INPUT DATA *#*

COEFFICIENTS IN TANGENTIAL VELOCITY EQUATION					
Axial Velocity Ratio	Total Polytropic Efficiency	Solidity at hub	Aspect Ratio	Hub Blockage Factor	Max Angle Hub Taper (Degrees)
1.0000	0.9504	2.0000	2.5000	1.0000	40.0000
1.0000	0.9504	2.0000	2.5000	1.0000	40.0000
1.0000	0.9504	2.0000	2.5000	1.0000	40.0000

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***** P C T J P I N L F O U T P U T D A T A *****

STATION NO.	RADIUS -F (IN)	WHEEL SPEED (FT/SEC)	Axial Tangent. ABS. VFL. (FT/SEC)	REL. VFL. (FT/SEC)	Abs. AIR ANG. (DEG)	REL. AIR ANG. (DEG)	RFL. (PSI)	TOTAL PRESS. (PSI)	RFL. NO.	Abs. MACH NO.	Loss Coeff
1	12.0	10.000	1.000	0.000	0.000	0.000	59.36	639.780	27.393	0.941	0.100
2	11.014	9.672	0.999	0.000	0.000	0.000	59.203	639.780	27.393	0.919	0.113
3	11.526	9.357	0.998	0.000	0.000	0.000	57.330	539.780	27.393	0.887	0.117
4	11.242	9.034	0.997	0.000	0.000	0.000	56.412	529.780	27.293	0.875	0.122
5	11.854	8.714	0.996	0.000	0.000	0.000	55.448	519.780	27.393	0.854	0.127
6	11.324	8.395	0.995	0.000	0.000	0.000	54.435	529.780	27.393	0.832	0.132
7	10.884	8.072	0.994	0.000	0.000	0.000	53.360	539.780	27.393	0.811	0.138
8	10.376	7.750	0.993	0.000	0.000	0.000	52.246	539.780	27.393	0.791	0.143
9	9.842	7.428	0.992	0.000	0.000	0.000	51.166	539.780	27.393	0.770	0.149
10	9.225	7.105	0.991	0.000	0.000	0.000	50.118	539.780	27.393	0.750	0.155
11	8.134	6.782	0.990	0.000	0.000	0.000	49.055	539.780	27.393	0.731	0.163

***** P C T J P I N L F O U T P U T D A T A *****

STATION NO.	RADIUS -F (IN)	WHEEL SPEED (FT/SEC)	Axial Tangent. ABS. VFL. (FT/SEC)	REL. VFL. (FT/SEC)	Abs. AIR ANG. (DEG)	REL. AIR ANG. (DEG)	RFL. (PSI)	TOTAL PRESS. (PSI)	RFL. NO.	Abs. MACH NO.	Loss Coeff
1	12.0	10.000	1.000	0.000	0.000	0.000	36.930	42.537	714.612	0.450	0.031
2	11.091	9.675	0.999	0.000	0.000	0.000	37.583	40.452	714.612	0.457	0.032
3	11.361	9.358	0.998	0.000	0.000	0.000	38.353	38.121	714.512	0.464	0.033
4	11.042	9.041	0.997	0.000	0.000	0.000	39.151	35.733	714.512	0.471	0.035
5	11.723	8.714	0.996	0.000	0.000	0.000	39.957	33.557	714.412	0.478	0.036
6	11.203	8.395	0.995	0.000	0.000	0.000	40.763	31.382	714.312	0.485	0.037
7	10.876	8.072	0.994	0.000	0.000	0.000	41.569	29.212	714.212	0.492	0.039
8	10.358	7.750	0.993	0.000	0.000	0.000	42.375	27.042	714.112	0.500	0.040
9	9.825	7.428	0.992	0.000	0.000	0.000	43.182	24.872	714.012	0.508	0.041
10	9.206	7.105	0.991	0.000	0.000	0.000	43.989	22.702	713.912	0.516	0.043
11	8.116	6.782	0.990	0.000	0.000	0.000	44.796	20.532	713.812	0.523	0.044

***** P C T J P I N L F O U T P U T D A T A *****

STATION NO.	RADIUS -F (IN)	WHEEL SPEED (FT/SEC)	Axial Tangent. ABS. VFL. (FT/SEC)	REL. VFL. (FT/SEC)	Abs. AIR ANG. (DEG)	REL. AIR ANG. (DEG)	RFL. (PSI)	TOTAL PRESS. (PSI)	RFL. NO.	Abs. MACH NO.	Loss Coeff
1	12.000	10.000	1.000	0.000	0.000	0.000	0.046	0.450	0.450	0.468	0.015
2	11.767	9.675	0.999	0.000	0.000	0.000	0.049	0.458	0.458	0.468	0.015
3	11.414	9.358	0.998	0.000	0.000	0.000	0.044	0.463	0.463	0.468	0.014
4	11.122	9.041	0.997	0.000	0.000	0.000	0.043	0.468	0.468	0.468	0.013
5	10.839	8.714	0.996	0.000	0.000	0.000	0.042	0.473	0.473	0.468	0.012
6	10.537	8.395	0.995	0.000	0.000	0.000	0.041	0.478	0.478	0.468	0.012
7	10.243	8.072	0.994	0.000	0.000	0.000	0.040	0.483	0.483	0.468	0.011
8	9.745	7.750	0.993	0.000	0.000	0.000	0.039	0.489	0.489	0.468	0.011
9	9.245	7.428	0.992	0.000	0.000	0.000	0.038	0.495	0.495	0.468	0.010
10	8.626	7.105	0.991	0.000	0.000	0.000	0.037	0.500	0.500	0.468	0.010
11	8.365	6.782	0.990	0.000	0.000	0.000	0.036	0.479	0.479	0.468	0.009

***** P C T J P I N L F O U T P U T D A T A *****

STATION NO.	RADIUS -F (IN)	WHEEL SPEED (FT/SEC)	Axial Tangent. ABS. VFL. (FT/SEC)	REL. VFL. (FT/SEC)	Abs. AIR ANG. (DEG)	REL. AIR ANG. (DEG)	RFL. (PSI)	TOTAL PRESS. (PSI)	RFL. NO.	Abs. MACH NO.	Loss Coeff
1	12.000	10.000	1.000	0.000	0.000	0.000	0.046	0.450	0.450	0.468	0.015
2	11.767	9.675	0.999	0.000	0.000	0.000	0.049	0.458	0.458	0.468	0.015
3	11.414	9.358	0.998	0.000	0.000	0.000	0.044	0.463	0.463	0.468	0.014
4	11.122	9.041	0.997	0.000	0.000	0.000	0.043	0.468	0.468	0.468	0.013
5	10.839	8.714	0.996	0.000	0.000	0.000	0.042	0.473	0.473	0.468	0.012
6	10.537	8.395	0.995	0.000	0.000	0.000	0.041	0.478	0.478	0.468	0.012
7	10.243	8.072	0.994	0.000	0.000	0.000	0.040	0.483	0.483	0.468	0.011
8	9.745	7.750	0.993	0.000	0.000	0.000	0.039	0.489	0.489	0.468	0.011
9	9.245	7.428	0.992	0.000	0.000	0.000	0.038	0.495	0.495	0.468	0.010
10	8.626	7.105	0.991	0.000	0.000	0.000	0.037	0.459	0.459	0.468	0.010
11	8.365	6.782	0.990	0.000	0.000	0.000	0.036	0.479	0.479	0.468	0.009

No data output appears on this page since there were no aerodynamic parameter or geometric violations.

***** STAGE DATA *****

STAGE NO. 4

*** ROTOR INPUT DATA ***

AXIAL VEL. RATIO	OVERALL EFFICIENCY	SOLIDITY AT TIP	TIP BLOCKAGE FACTOR	HUB BLOCKAGE FACTOR	MAX ANGLE HUB TAPER (DEGREES)	MAX ANGLE TIP TAPER (DEGREES)
1.000	1.000	1.000	1.000	1.000	40.000	-20.000
MAX. ROTOR DIFF. FACTOR	AVERAGE FLOW ACROSS ONE ROW OF BLADES					
0.650	-1.000					

Coefficients in Tangential Velocity Equation

R	C	E
0.0000	0.0000	0.0000
U.0000	U.0000	U.0000

*** STATOR INPUT DATA ***

AXIAL VELOCITY RATIO	TOTAL SOLIDITY AT HUB	SOLIDITY AT TIP	TIP BLOCKAGE FACTOR	HUB BLOCKAGE FACTOR	MAX ANGLE HUB TAPER (DEGREES)	MAX ANGLE TIP TAPER (DEGREES)
1.000	0.250	2.00	1.000	1.000	40.000	-20.000
MAX. STATOR DIFF. FACTOR	MAX. HUB INLET SOLIDITY					
0.650	0.3	U.0000	U.0000	U.0000	U.0000	0.0000

Coefficients in Tangential Velocity Equation

R	C	E
0.0000	0.0000	0.0000
U.0000	U.0000	U.0000

***** STAGE OUTPUT DATA *****

MASS FLOW (LB/SEC) = 164.463

OVERALL MASS AVE. RATIOS	FRICTIONAL MASS AVE. EFFICIENCY	MASS AVE. PRESSURE RATIO	MASS AVE. TEMPERATURE RATIO	POTTER STATOR TIP RAD. 2-G (INCHES)	POTTER HUB RAD. 3-G (INCHES)	POTTER PROJ. LENGTH (INCHES)	STATOR ASPECT RATIO
3.4826	1.0211	U.9220	U.3449	1.1.147	U.2426	2.5000	2.500
ROTOR TIP RAD. 1-G (INCHES)	ROTOR HUB RAD. 1-G (INCHES)						
12.000	3.0724	U.2000	2.05207	1.2.000	2.00000	1.1711	0.9913
POTTER TIP RAD. AVE. (INCHES)	POTTER HUB RAD. AVE. (INCHES)						
U.000	20.0000	3.0000	3.0000				
STATOR HUB RAMP ANGLE (DEGREES)							
C.4806							

***** Q U O T E R I N L I F T C U T P U T D A T A *****

TEST NO.	RADIUS -E (IN.)	WHEEL SPEED (FT/SEC.)	AXIAL VEL. (FT/SEC.)	TANGENT. VEL. (FT/SEC.)	ABS. VFL. (FT/SEC.)	REL. VFL. (FT/SEC.)	ABS. AIR ANG. (DEG.)	REL. AIR ANG. (DEG.)	TOTAL PRESS. (PSI)	TOTAL TEMP. (DEG R.)	REL. MACH NU.	ABS. MACH NU.	LOSS COEFF
1	12.0	10.0	600.0	600.0	1165.190	1165.190	10.000	5.000	59.336	714.512	38.667	0.459	0.105
2	11.767	975.0	522.0	522.0	1145.339	1145.339	6.000	3.000	58.436	714.612	38.067	0.458	0.109
3	11.414	951.2	514.0	514.0	1124.029	1124.029	6.000	3.000	57.757	714.612	38.067	0.458	0.112
4	11.222	926.8	505.0	505.0	1104.863	1104.863	6.000	3.000	57.092	714.612	38.067	0.458	0.115
5	11.329	902.4	497.0	497.0	1083.839	1083.839	6.000	3.000	57.391	714.612	38.067	0.458	0.119
6	10.536	974.0	500.0	500.0	1063.438	1063.438	6.000	3.000	55.253	714.612	38.067	0.458	0.123
7	10.243	857.0	481.0	481.0	1043.345	1043.345	6.000	3.000	54.697	714.612	38.067	0.458	0.127
8	9.451	421.0	215.0	215.0	1021.520	1021.520	6.000	3.000	54.111	714.512	38.067	0.458	0.131
9	8.659	41.4	20.5	20.5	1001.350	1001.350	6.000	3.000	53.295	714.612	38.067	0.458	0.135
10	9.355	76.0	37.0	37.0	984.493	984.493	6.000	3.000	52.446	714.612	38.067	0.458	0.139
11	9.072	75.0	31.7	31.7	965.176	965.176	6.000	3.000	51.563	714.612	38.067	0.458	0.144

STA. NO.	RADIUS -F (IN)	WHEELED SPEED (FT/SEC.)	AXIAL VFL. (FT/SEC.)	TANGENT. VEL. (FT/SEC.)	AHS. VFL. (FT/SEC.)	PFL. VFL. (FT/SEC.)	ABS. AIR ANG. (DEG.)	REL. AIR ANG. (DEG.)	TOTAL PRESS. (PSI)	ROTDR. TEMP. (DEG. R.)	RFL. MACH NO.	LOSS FUNC.	
1	12.000	6.000	4.45	4.50	749.554	314.236	38.339	42.537	786.443	51.643	6.610	0.562	
2	11.752	973.346	2.45	3.00	554.369	794.225	37.414	40.935	789.443	51.643	6.595	0.531	
3	11.504	553.555	2.45	3.00	554.415	761.403	774.559	38.355	39.229	789.443	51.643	6.562	0.532
4	11.257	531.443	2.45	3.00	550.600	479.474	755.352	38.612	37.408	786.443	51.643	6.537	0.533
5	11.009	517.339	2.45	3.00	550.426	439.456	736.376	39.035	35.445	789.443	51.643	6.553	0.534
6	10.761	495.738	2.45	3.00	511.251	721.326	714.817	39.375	33.391	789.443	51.643	6.540	0.535
7	10.513	875.245	2.45	3.00	512.057	736.454	711.272	40.534	34.275	789.443	51.643	6.527	0.535
8	10.265	855.433	2.45	3.00	525.454	757.550	549.753	41.211	28.490	789.443	51.643	6.515	0.537
9	10.017	845.789	2.45	3.00	538.452	638.434	659.186	41.905	26.644	789.443	51.643	6.504	0.538
10	9.770	814.123	2.45	3.00	552.453	654.377	654.745	42.520	21.591	789.443	51.643	6.496	0.539
11	9.522	793.475	6.00	1.50	556.443	795.454	641.553	43.354	20.723	789.443	51.643	6.499	0.540

No data output appears on this
page since there were no aerodynamic
parameter or geometric violations.

DATA STAGETRANSFORMATIONS

STAGE NO. 5

***** INPUT DATA *****

AXIAL VEL. RATING	AIR REL. FLOW ANGLE ROTOR W/R DIF. FACTOR	SURFACE AT TIP	ASPFCT RATIO	TIP BLOCKAGE FACTOR	HUB BLOCKAGE FACTOR	MAX ANGLE HUB TAPER (DEGREES)	MAX ANGLE TIP TAPER (DEGREES)	Coefficients in Tangential Velocity Equation
1.0000	0.8750	1.0000	2.5000	1.0000	1.0000	40.000	-20.000	B C D E
0.4500	0.8750	0.8750	2.5000	0.8750	0.8750	0.0000	0.0000	0.0000

SEARCHING FOR STATION INPUT DATA

COEFFICIENTS IN TANGENTIAL VELOCITY EQUATION					
AXIAL VELOCITY RATIO	TOTAL POLYTRIPIC EFFICIENCY	SOLUBILITY AT 40°H	ASPECT RATIO	TIP BLOCKAGE FACTOR	HUB BLOCKAGE FACTOR
1.0000	3.0500	2.0000	1.0000	1.0000	1.0000

S T A C E D U T R O I D A *

***** STARTER EXHAUST OUTPUT DATA *****

RADIUS STA. NO.	WHEEL SPEED (FT/SEC)	AXIAL TANGENT. VEL. (FT/SEC)	AIR. VEL. (FT/SEC)	RFL. (FT/SEC)	ABS. VEL. (FT/SEC)	REL. AIR ANG. (DEG)	TOTAL TEMP. (DEG F)	TOTAL PRESS. (PSI)	REL. MACH NO.	ABS. MACH NO.	LOSS COEFF
1 12.0	310.0	116.6	140	0.000	59.036	793.443	51.195	0.847	0.436	0.104	
2 11.740	310.0	114.9	70.7	0.000	58.542	786.443	51.195	0.835	0.436	0.105	
3 11.537	310.0	113.5	31.1	0.000	58.034	789.443	51.195	0.823	0.436	0.107	
4 11.354	310.0	111.7	66.7	0.000	57.510	789.443	51.195	0.811	0.436	0.111	
5 11.176	310.0	110.8	90.0	0.000	56.971	789.443	51.195	0.600	0.436	0.114	
6 10.995	310.0	109.0	124.4	0.000	56.416	790.443	51.195	0.788	0.436	0.117	
7 10.825	310.0	108.3	53.9	0.000	55.345	790.443	51.195	0.776	0.436	0.119	
8 10.661	310.0	106.2	179.0	0.000	55.256	787.443	51.195	0.765	0.436	0.122	
9 10.500	310.0	105.7	217.9	0.000	54.649	789.443	51.195	0.753	0.436	0.125	
10 10.340	310.0	102.1	353	0.000	54.324	783.443	51.195	0.742	0.435	0.129	
11 10.187	310.0	27.1	305.9	0.000	53.379	789.443	51.195	0.731	0.436	0.132	

***** TURBINE EXIT OUTPUT DATA *****

RADIUS STA. NO.	WHEEL SPEED (FT/SEC)	AXIAL TANGENT. VEL. (FT/SEC)	AIR. VEL. (FT/SEC)	RFL. (FT/SEC)	ABS. VEL. (FT/SEC)	REL. AIR ANG. (DEG)	TOTAL TEMP. (DEG F)	TOTAL PRESS. (PSI)	REL. MACH NO.	ABS. MACH NO.	LOSS FUNC	
1 12.0	116.6	140	914.286	36.839	42.537	864.274	67.558	0.450	0.581	0.535	0.029	
2 11.91	116.6	117.9	759.120	37.300	41.257	864.274	67.558	0.570	0.529	0.530		
3 11.692	116.6	116.5	760.551	37.771	39.911	864.274	67.558	0.559	0.542	0.031		
4 11.462	116.6	114.5	764.514	38.253	38.493	864.274	67.558	0.455	0.548	0.032		
5 11.233	116.6	112.5	769.651	38.745	36.305	864.274	67.558	0.470	0.537	0.032		
6 11.004	116.6	110.5	774.788	39.235	35.426	864.274	67.558	0.475	0.527	0.033		
7 10.775	116.6	108.5	780.517	39.755	33.767	864.274	67.558	0.516	0.559	0.034		
8 10.546	116.6	106.5	786.554	7.71.344	41.297	32.018	864.274	57.558	0.494	0.507	0.035	
9 10.317	116.6	104.5	812.302	59.6.034	40.924	30.174	864.274	67.558	0.499	0.497	0.036	
10 10.087	116.6	102.5	818.153	540.070	41.372	28.232	864.274	67.558	0.493	0.573	0.037	
11 10.858	116.6	97.5	824.323	448.537	41.933	26.191	864.274	67.558	0.496	0.578	0.037	

***** STATOR EXIT OUTPUT DATA *****

RADIUS STA. NO.	WHEEL SPEED (FT/SEC)	AXIAL TANGENT. VEL. (FT/SEC)	AIR. VEL. (FT/SEC)	RFL. (FT/SEC)	ABS. VEL. (FT/SEC)	REL. AIR ANG. (DEG)	TOTAL TEMP. (DEG F)	TOTAL PRESS. (PSI)	REL. MACH NO.	ABS. MACH NO.	LOSS FUNC	
1 12.0	116.6	140	914.286	36.839	42.537	864.274	67.558	0.450	0.581	0.535	0.029	
2 11.91	116.6	117.9	759.120	37.300	41.257	864.274	67.558	0.570	0.529	0.530		
3 11.692	116.6	116.5	760.551	37.771	39.911	864.274	67.558	0.559	0.542	0.031		
4 11.462	116.6	114.5	764.514	38.253	38.493	864.274	67.558	0.455	0.548	0.032		
5 11.233	116.6	112.5	769.651	38.745	36.305	864.274	67.558	0.470	0.537	0.032		
6 11.004	116.6	110.5	774.788	39.235	35.426	864.274	67.558	0.475	0.527	0.033		
7 10.775	116.6	108.5	780.517	39.755	33.767	864.274	67.558	0.516	0.559	0.034		
8 10.546	116.6	106.5	786.554	7.71.344	41.297	32.018	864.274	57.558	0.494	0.507	0.035	
9 10.317	116.6	104.5	812.302	59.6.034	40.924	30.174	864.274	67.558	0.499	0.497	0.036	
10 10.087	116.6	102.5	818.153	540.070	41.372	28.232	864.274	67.558	0.493	0.573	0.037	
11 10.858	116.6	97.5	824.323	448.537	41.933	26.191	864.274	67.558	0.496	0.578	0.037	

***** STATOR EXIT OUTPUT DATA *****

RADIUS STA. NO.	WHEEL SPEED (FT/SEC)	AXIAL TANGENT. VEL. (FT/SEC)	AIR. VEL. (FT/SEC)	RFL. (FT/SEC)	ABS. VEL. (FT/SEC)	REL. AIR ANG. (DEG)	TOTAL TEMP. (DEG F)	TOTAL PRESS. (PSI)	REL. MACH NO.	ABS. MACH NO.	LOSS FUNC	
1 12.0	116.6	140	914.286	36.839	42.537	864.274	67.558	0.450	0.581	0.535	0.029	
2 11.91	116.6	117.9	759.120	37.300	41.257	864.274	67.558	0.570	0.529	0.530		
3 11.692	116.6	116.5	760.551	37.771	39.911	864.274	67.558	0.559	0.542	0.031		
4 11.462	116.6	114.5	764.514	38.253	38.493	864.274	67.558	0.455	0.548	0.032		
5 11.233	116.6	112.5	769.651	38.745	36.305	864.274	67.558	0.470	0.537	0.032		
6 11.004	116.6	110.5	774.788	39.235	35.426	864.274	67.558	0.475	0.527	0.033		
7 10.775	116.6	108.5	780.517	39.755	33.767	864.274	67.558	0.516	0.559	0.034		
8 10.546	116.6	106.5	786.554	7.71.344	41.297	32.018	864.274	57.558	0.494	0.507	0.035	
9 10.317	116.6	104.5	812.302	59.6.034	40.924	30.174	864.274	67.558	0.499	0.497	0.036	
10 10.087	116.6	102.5	818.153	540.070	41.372	28.232	864.274	67.558	0.493	0.573	0.037	
11 10.858	116.6	97.5	824.323	448.537	41.933	26.191	864.274	67.558	0.496	0.578	0.037	

No data output appears on this page since there were no aerodynamic parameter or geometric violations.

S T A N D A R D A G E S

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STATION NO.	ABS. VEL. (FT/SEC.)	AXIAL VEL. (FT/SEC.)	TANGENT. VEL. (FT/SEC.)	ABS. VEL. (FT/SEC.)	REL. VEL. (FT/SEC.)	AIR ANG. (DEG)	REL. VEL. (FT/SEC.)	AIR ANG. (DEG)	TEMP. (DEG R)	TOTAL PRESS. (PSI)	TOTAL PRESS. (PSI)	REFL. MACH NO.	AHS. MACH NO.	LOSS COEF.
1	12.1	1.0	1.0	12.0	0.0	0.0	12.0	0.0	0.0	864.274	864.274	0.417	0.417	0.103
2	11.312	1.94	3.43	12.0	0.0	0.0	12.0	0.0	0.0	864.274	864.274	0.417	0.417	0.104
3	11.324	1.64	5.57	12.0	0.0	0.0	12.0	0.0	0.0	864.274	864.274	0.417	0.417	0.105
4	11.326	1.60	6.07	12.0	0.0	0.0	12.0	0.0	0.0	864.274	864.274	0.417	0.417	0.109
5	11.244	1.37	3.37	12.0	0.0	0.0	12.0	0.0	0.0	864.274	864.274	0.417	0.417	0.113
6	11.261	1.17	6.65	12.0	0.0	0.0	12.0	0.0	0.0	864.274	864.274	0.417	0.417	0.117
7	11.272	1.15	5.68	12.0	0.0	0.0	12.0	0.0	0.0	864.274	864.274	0.417	0.417	0.117
8	11.294	0.91	6.21	12.0	0.0	0.0	12.0	0.0	0.0	864.274	864.274	0.417	0.417	0.119
9	11.316	0.77	3.55	12.0	0.0	0.0	12.0	0.0	0.0	864.274	864.274	0.417	0.417	0.121
10	11.318	0.65	3.97	12.0	0.0	0.0	12.0	0.0	0.0	864.274	864.274	0.417	0.417	0.124
11	11.321	0.43	3.31	12.0	0.0	0.0	12.0	0.0	0.0	864.274	864.274	0.417	0.417	0.124

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STATION NO.	ABS. VEL. (FT/SEC.)	AXIAL VEL. (FT/SEC.)	TANGENT. VEL. (FT/SEC.)	ABS. VEL. (FT/SEC.)	REL. VEL. (FT/SEC.)	AIR ANG. (DEG)	ABS. VEL. (FT/SEC.)	REL. VEL. (FT/SEC.)	AIR ANG. (DEG)	TOTAL PRESS. (PSI)	TOTAL PRESS. (PSI)	REFL. MACH NO.	AHS. MACH NO.	LOSS FUNC.
1	12.010	1.0	1.0	12.0	0.0	0.0	12.0	0.0	0.0	864.274	864.274	0.417	0.417	0.103
2	11.436	0.93	3.13	12.0	0.0	0.0	12.0	0.0	0.0	864.274	864.274	0.417	0.417	0.104
3	11.472	0.72	6.23	12.0	0.0	0.0	12.0	0.0	0.0	864.274	864.274	0.417	0.417	0.109
4	11.507	0.53	9.39	12.0	0.0	0.0	12.0	0.0	0.0	864.274	864.274	0.417	0.417	0.113
5	11.343	0.45	2.52	12.0	0.0	0.0	12.0	0.0	0.0	864.274	864.274	0.417	0.417	0.117
6	11.176	0.31	5.55	12.0	0.0	0.0	12.0	0.0	0.0	864.274	864.274	0.417	0.417	0.121
7	11.315	0.17	3.79	12.0	0.0	0.0	12.0	0.0	0.0	864.274	864.274	0.417	0.417	0.124
8	11.351	0.44	1.19	12.0	0.0	0.0	12.0	0.0	0.0	864.274	864.274	0.417	0.417	0.124
9	11.366	0.60	5.52	12.0	0.0	0.0	12.0	0.0	0.0	864.274	864.274	0.417	0.417	0.125
10	11.322	0.75	9.14	12.0	0.0	0.0	12.0	0.0	0.0	864.274	864.274	0.417	0.417	0.125
11	11.359	0.63	1.13	12.0	0.0	0.0	12.0	0.0	0.0	864.274	864.274	0.417	0.417	0.125

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STATION NO.	ABS. VEL. (FT/SEC.)	AXIAL VEL. (FT/SEC.)	TANGENT. VEL. (FT/SEC.)	ABS. VEL. (FT/SEC.)	REL. VEL. (FT/SEC.)	AIR ANG. (DEG)	ABS. VEL. (FT/SEC.)	REL. VEL. (FT/SEC.)	AIR ANG. (DEG)	TOTAL PRESS. (PSI)	TOTAL PRESS. (PSI)	REFL. MACH NO.	AHS. MACH NO.	LOSS FUNC.
1	12.010	1.0	1.0	12.0	0.0	0.0	12.0	0.0	0.0	864.274	864.274	0.417	0.417	0.103
2	11.944	0.94	3.43	12.0	0.0	0.0	12.0	0.0	0.0	864.274	864.274	0.417	0.417	0.104
3	11.653	1.11	5.21	12.0	0.0	0.0	12.0	0.0	0.0	864.274	864.274	0.417	0.417	0.109
4	11.521	1.01	3.21	12.0	0.0	0.0	12.0	0.0	0.0	864.274	864.274	0.417	0.417	0.113
5	11.476	1.11	3.76	12.0	0.0	0.0	12.0	0.0	0.0	864.274	864.274	0.417	0.417	0.117
6	11.219	1.21	5.63	12.0	0.0	0.0	12.0	0.0	0.0	864.274	864.274	0.417	0.417	0.121
7	11.264	1.16	6.64	12.0	0.0	0.0	12.0	0.0	0.0	864.274	864.274	0.417	0.417	0.121
8	11.327	0.91	3.55	12.0	0.0	0.0	12.0	0.0	0.0	864.274	864.274	0.417	0.417	0.124
9	11.375	0.55	6.94	12.0	0.0	0.0	12.0	0.0	0.0	864.274	864.274	0.417	0.417	0.124
10	11.359	0.35	1.34	12.0	0.0	0.0	12.0	0.0	0.0	864.274	864.274	0.417	0.417	0.124

No data output appears on this
page since there were no aerodynamic
parameter or geometric violations.

***** STAGE DATA *****

STAGE NO. 7

*** ROTCF INPUT DATA ***

	POLYTRAPIC EFFICIENCY	SOLIDITY AT TIP	TIP BLOCKAGE FACTOR	HUB BLOCKAGE FACTOR	MAX ANGLE HUB TAPER (DEGREES)	MAX ANGLE TIP TAPER (DEGREES)
AXIAL VEL. RATIO	1.075	1.030	1.000	1.000	40.000	-20.000
MAX ROTCF DIFF. FACTOR	1.450	-1.000	-	-	-	-

	POLYTRAPIC EFFICIENCY	SOLIDITY AT HIGH MACH NUMBER	TIP BLOCKAGE FACTOR	HUB BLOCKAGE FACTOR	MAX ANGLE HUB TAPER (DEGREES)	MAX ANGLE TIP TAPER (DEGREES)
AXIAL VFLNCY RATIO	1.035	2.000	1.000	1.000	40.000	-20.000
MAX. STATOR DIFF. FACTOR	1.000	-	-	-	-	-

*** STATOR INPUT DATA ***

	TOTAL POLYTRAPIC EFFICIENCY	SOLIDITY AT HIGH MACH NUMBER	TIP BLOCKAGE FACTOR	HUB BLOCKAGE FACTOR	MAX ANGLE HUB TAPER (DEGREES)	MAX ANGLE TIP TAPER (DEGREES)
AXIAL VFLNCY RATIO	1.035	2.000	1.000	1.000	40.000	-20.000
MAX. STATOR DIFF. FACTOR	1.000	-	-	-	-	-

***** STAGE OUTPUT DATA *****

MASS FLOW (LB/SEC) = 104.442

	OVERALL MASS AVE. TEMP. RATIO	OVERALL MASS AVE. PRESSURE RATIO	MASS AVE. TEMPERATURE RATIO	MASS AVE. EFFICIENCY	ROTATING STATOR RAD. 3-6 (INCHES)	STATOR TIP RAD. 3-6 (INCHES)	ROTATING STATOR RAD. 3-6 (INCHES)	STATOR LENGTH (INCHES)	STATOR PROJ. LENGTH (INCHES)	STATOR LENGTH (INCHES)
OVERALL MASS AVE. TEMP. RATIO	1.03326	1.0342	1.0252	1.0747	0.8451	0.8451	0.8451	0.8451	0.8451	0.8451
ROTATING STATOR RAD. 3-6 (INCHES)	1.20000	1.20000	1.06136	1.06136	1.06136	1.06136	1.06136	1.06136	1.06136	1.06136
ROTATING STATOR RAD. 3-6 (INCHES)	1.00000	1.00000	0.91991	0.91991	0.91991	0.91991	0.91991	0.91991	0.91991	0.91991

CONTINUATION OF PROJECT 304 INPUT OUTPUT DATA *****

STA NO.	RADIUS IN.	AXIAL VEL. (FT/SEC)	TANGENT. VEL. (FT/SEC)	AIR. VEL. (FT/SEC)	RFL. (FT/SEC)	ABS. VEL. (FT/SEC)	RFL. (FT/SEC)	AIR ANG. (DEG)	AIR ANG. (DEG)	RFL. (DEG)	TOTAL PRESS. (PSI)	REFL. MACH NO.	ABS. MACH NO.	LOSS COEFF
1	12.0	16.000	0.000	16.000	1.166.190	16.000	1.166.190	0.000	0.000	0.000	95.906	0.777	0.450	0.100
2	11.0	16.044	0.044	16.044	1.165.040	16.044	1.165.040	0.044	0.044	0.044	95.866	0.749	0.400	0.102
3	11.037	17.0	0.55	17.0	1.147.948	17.0	1.147.948	0.55	0.55	0.55	95.806	0.772	0.400	0.104
4	11.074	17.0	0.54	17.0	1.132.987	17.0	1.132.987	0.54	0.54	0.54	95.806	0.765	0.400	0.105
5	11.127	17.0	0.52	17.0	1.121.958	17.0	1.121.958	0.52	0.52	0.52	95.806	0.747	0.400	0.107
6	11.181	17.0	0.50	17.0	1.110.930	17.0	1.110.930	0.50	0.50	0.50	95.806	0.744	0.400	0.107
7	11.234	17.0	0.48	17.0	1.100.892	17.0	1.100.892	0.48	0.48	0.48	95.806	0.733	0.400	0.112
8	11.287	17.0	0.46	17.0	1.089.854	17.0	1.089.854	0.46	0.46	0.46	95.806	0.725	0.400	0.112
9	11.340	17.0	0.44	17.0	1.078.817	17.0	1.078.817	0.44	0.44	0.44	95.806	0.718	0.400	0.114
10	11.393	17.0	0.42	17.0	1.067.780	17.0	1.067.780	0.42	0.42	0.42	95.806	0.711	0.400	0.115
11	11.446	17.0	0.40	17.0	1.056.744	17.0	1.056.744	0.40	0.40	0.40	95.806	0.704	0.400	0.116
12	11.499	17.0	0.38	17.0	1.045.707	17.0	1.045.707	0.38	0.38	0.38	95.806	0.696	0.400	0.116

***** C R T C P E X I T C U T P U T D A T A *****

STA NO.	RADIUS IN.	AXIAL VEL. (FT/SEC)	TANGENT. VEL. (FT/SEC)	AIR. VEL. (FT/SEC)	RFL. (FT/SEC)	ABS. VEL. (FT/SEC)	RFL. (FT/SEC)	AIR ANG. (DEG)	AIR ANG. (DEG)	RFL. (DEG)	TOTAL PRESS. (PSI)	REFL. MACH NO.	ABS. MACH NO.	LOSS COEFF
1	12.0	1.000	0.000	1.000	7.45.6.04	1.000	7.45.6.04	0.000	0.000	0.000	10.13.357	1.08.515	0.450	0.024
2	11.0	1.042	0.042	1.042	7.45.4.725	1.042	7.45.4.725	0.042	0.042	0.042	10.13.337	1.08.515	0.454	0.024
3	11.074	1.075	0.075	1.075	7.45.3.533	1.075	7.45.3.533	0.075	0.075	0.075	10.13.337	1.08.515	0.454	0.029
4	11.127	1.105	0.105	1.105	7.45.2.509	1.105	7.45.2.509	0.105	0.105	0.105	10.13.337	1.08.515	0.454	0.031
5	11.181	1.147	0.147	1.147	7.45.1.487	1.147	7.45.1.487	0.147	0.147	0.147	10.13.337	1.08.515	0.465	0.031
6	11.234	1.189	0.189	1.189	7.45.0.464	1.189	7.45.0.464	0.189	0.189	0.189	10.13.337	1.08.515	0.465	0.031
7	11.287	1.230	0.230	1.230	7.44.9.452	1.230	7.44.9.452	0.230	0.230	0.230	10.13.337	1.08.515	0.459	0.031
8	11.340	1.272	0.272	1.272	7.44.8.452	1.272	7.44.8.452	0.272	0.272	0.272	10.13.337	1.08.515	0.459	0.032
9	11.393	1.317	0.317	1.317	7.44.7.452	1.317	7.44.7.452	0.317	0.317	0.317	10.13.337	1.08.515	0.476	0.032
10	11.446	1.361	0.361	1.361	7.44.6.452	1.361	7.44.6.452	0.361	0.361	0.361	10.13.337	1.08.515	0.430	0.033
11	11.499	1.405	0.405	1.405	7.44.5.452	1.405	7.44.5.452	0.405	0.405	0.405	10.13.337	1.08.515	0.472	0.033
12	11.553	1.449	0.449	1.449	7.44.4.452	1.449	7.44.4.452	0.449	0.449	0.449	10.13.337	1.08.515	0.472	0.034

STA NO.	RADIUS IN.	AXIAL VEL. (FT/SEC)	TANGENT. VEL. (FT/SEC)	AIR. VEL. (FT/SEC)	RFL. (FT/SEC)	ABS. VEL. (FT/SEC)	RFL. (FT/SEC)	AIR ANG. (DEG)	AIR ANG. (DEG)	RFL. (DEG)	TOTAL PRESS. (PSI)	REFL. MACH NO.	ABS. MACH NO.	LOSS COEFF
1	12.0	1.000	0.000	1.000	7.45.6.04	1.000	7.45.6.04	0.000	0.000	0.000	10.13.357	1.08.515	0.454	0.024
2	11.0	1.042	0.042	1.042	7.45.4.725	1.042	7.45.4.725	0.042	0.042	0.042	10.13.337	1.08.515	0.454	0.029
3	11.074	1.075	0.075	1.075	7.45.3.533	1.075	7.45.3.533	0.075	0.075	0.075	10.13.337	1.08.515	0.454	0.031
4	11.127	1.105	0.105	1.105	7.45.2.509	1.105	7.45.2.509	0.105	0.105	0.105	10.13.337	1.08.515	0.454	0.031
5	11.181	1.147	0.147	1.147	7.45.1.487	1.147	7.45.1.487	0.147	0.147	0.147	10.13.337	1.08.515	0.465	0.031
6	11.234	1.189	0.189	1.189	7.45.0.464	1.189	7.45.0.464	0.189	0.189	0.189	10.13.337	1.08.515	0.465	0.031
7	11.287	1.230	0.230	1.230	7.44.9.452	1.230	7.44.9.452	0.230	0.230	0.230	10.13.337	1.08.515	0.459	0.031
8	11.340	1.272	0.272	1.272	7.44.8.452	1.272	7.44.8.452	0.272	0.272	0.272	10.13.337	1.08.515	0.459	0.032
9	11.393	1.317	0.317	1.317	7.44.7.452	1.317	7.44.7.452	0.317	0.317	0.317	10.13.337	1.08.515	0.476	0.032
10	11.446	1.361	0.361	1.361	7.44.6.452	1.361	7.44.6.452	0.361	0.361	0.361	10.13.337	1.08.515	0.430	0.033
11	11.499	1.405	0.405	1.405	7.44.5.452	1.405	7.44.5.452	0.405	0.405	0.405	10.13.337	1.08.515	0.472	0.033

E-24

STA NO.	RADIUS IN.	AXIAL VEL. (FT/SEC)	TANGENT. VEL. (FT/SEC)	AIR. VEL. (FT/SEC)	RFL. (FT/SEC)	ABS. VEL. (FT/SEC)	RFL. (FT/SEC)	AIR ANG. (DEG)	AIR ANG. (DEG)	RFL. (DEG)	TOTAL PRESS. (PSI)	REFL. MACH NO.	ABS. MACH NO.	LOSS COEFF
1	12.0	1.000	0.000	1.000	7.45.6.04	1.000	7.45.6.04	0.000	0.000	0.000	10.13.357	1.08.515	0.454	0.024
2	11.0	1.042	0.042	1.042	7.45.4.725	1.042	7.45.4.725	0.042	0.042	0.042	10.13.337	1.08.515	0.454	0.029
3	11.074	1.075	0.075	1.075	7.45.3.533	1.075	7.45.3.533	0.075	0.075	0.075	10.13.337	1.08.515	0.454	0.031
4	11.127	1.105	0.105	1.105	7.45.2.509	1.105	7.45.2.509	0.105	0.105	0.105	10.13.337	1.08.515	0.454	0.031
5	11.181	1.147	0.147	1.147	7.45.1.487	1.147	7.45.1.487	0.147	0.147	0.147	10.13.337	1.08.515	0.465	0.031
6	11.234	1.189	0.189	1.189	7.45.0.464	1.189	7.45.0.464	0.189	0.189	0.189	10.13.337	1.08.515	0.465	0.031
7	11.287	1.230	0.230	1.230	7.44.9.452	1.230	7.44.9.452	0.230	0.230	0.230	10.13.337	1.08.515	0.459	0.031
8	11.340	1.272	0.272	1.272	7.44.8.452	1.272	7.44.8.452	0.272	0.272	0.272	10.13.337	1.08.515	0.459	0.032
9	11.393	1.317	0.317	1.317	7.44.7.452	1.317	7.44.7.452	0.317	0.317	0.317	10.13.337	1.08.515	0.476	0.032
10	11.446	1.361	0.361	1.361	7.44.6.452	1.361	7.44.6.452	0.361	0.361	0.361	10.13.337	1.08.515	0.430	0.033
11	11.499	1.405	0.405	1.405	7.44.5.452	1.405	7.44.5.452	0.405	0.405	0.405	10.13.337	1.08.515	0.472	0.033

STA NO.	RADIUS IN.	AXIAL VEL. (FT/SEC)	TANGENT. VEL. (FT/SEC)	AIR. VEL. (FT/SEC)	RFL. (FT/SEC)	ABS. VEL. (FT/SEC)	RFL. (FT/SEC)	AIR ANG. (DEG)	AIR ANG. (DEG)	RFL. (DEG)	TOTAL PRESS. (PSI)	REFL. MACH NO.	ABS. MACH NO.	LOSS COEFF
1	12.0	1.000	0.000	1.000	7.45.6.04	1.000	7.45.6.04	0.000	0.000	0.000	10.13.357	1.08.515	0.454	0.024
2	11.0	1.042	0.042	1.042	7.45.4.725	1.042	7.45.4.725	0.042	0.042	0.042	10.13.337	1.08.515	0.454	0.029
3	11.074	1.075	0.075	1.075	7.45.3.533	1.075	7.4							

No data output appears on this page since there were no aerodynamic parameter or geometric violations.

***** STAGE DATA *****

STAGE NO. 9

*** INPUT DATA ***

Axial Vel. Data	Solidity at Tip	Aspect Ratio	Tip Blockage Factor	Max Angle Hub Taper (Degrees)
1.0000	0.375	1.0000	1.0000	-20.000
Max Rotating Diff. Factor	Avg. Rel. Fr. L. No. 4 Visible Stage (Degrees)			
0.45	-1.0000			

COEFFICIENTS IN TANGENTIAL VELOCITY EQUATION

R	C	D	E	
0.0000	0.0000	0.0000	0.0000	
*** STAGE INPUT DATA ***				
Axial Velocity Ratio	Solidity at Hub	Aspect Ratio	Tip Blockage Factor	Max Angle Hub Taper (Degrees)
1.0000	0.375	1.0000	1.0000	-20.000
Max Stage Factor	Max Hub Inlet Mach Number			
0.45	0.300			

COEFFICIENTS IN TANGENTIAL VELOCITY EQUATION

R	C	D	E
0.0000	0.0000	0.0000	0.0000
***** STAGE OUTPUT DATA *****			
VASS Flow (LB/SEC) = 104.443	MASS Ave. Pressure Ratio	MASS Ave. Temperature Ratio	Rotor Aspect Ratio
Overall Mass Ave. Temp. Ratio	Mass Ave. Efficiency	MASS AVE. EFFICIENCY	
9.0427	2.0578	1.0751	1.0733
Rotor Tip Rad. 1-5 (INCHES)	Rotor Tip Rad. 2-5 (INCHES)	Stator Tip Rad. 3-5 (INCHES)	Stator Proj. Length (INCHES)
12.000	12.000	12.000	12.000
Tip Tip Gap Angle (Degrees)	Rotor Hub Ramp Angle (Degrees)	Stator Tip Ramp Angle (Degrees)	Stator Hub Ramp Angle (Degrees)
0.0000	0.0000	0.0000	0.0000

* * * * * C O N T R O L I N E T O U T P U T D A T A * * * * *

STA N. (IN)	RADIUS -E (IN)	W.A.FL (SF)	AXIAL VEL. (FT/SEC)	TANGENT. VEL. (FT/SEC)	ABS. (FT/SEC)	REL. (DEG)	AIR ANG. (DEG)	REL. PRESS. (PSI)	TOTAL PRESS. (PSI)	REL. MACH NO.	ABS. MACH NO.	LOSS COEFF
1	12.000	0.000	0.000	0.000	0.000	0.000	0.000	59.036	1013.937	107.750	0.743	0.385
2	12.500	0.470	0.470	0.470	0.557	7.72	0.079	58.750	1013.937	107.750	0.741	0.385
3	11.774	0.717	0.717	0.717	0.800	3.91	0.000	58.471	1013.937	107.750	0.735	0.385
4	11.304	0.625	0.625	0.625	0.700	1.18	0.10	58.181	1013.937	107.750	0.729	0.385
5	11.472	0.632	0.632	0.632	0.700	1.29	0.07	57.937	1013.937	107.750	0.723	0.385
6	11.343	0.615	0.615	0.615	0.690	1.16	0.04	57.598	1013.937	107.750	0.718	0.385
7	11.224	0.594	0.594	0.594	0.680	1.00	0.01	57.285	1013.937	107.750	0.712	0.385
8	11.076	0.594	0.594	0.594	0.670	0.85	0.00	56.974	1013.937	107.750	0.706	0.385
9	11.044	0.588	0.588	0.588	0.660	0.76	0.00	56.659	1013.937	107.750	0.700	0.385
10	10.942	0.586	0.586	0.586	0.650	0.62	0.00	56.339	1013.937	107.750	0.694	0.385
11	10.530	0.496	0.496	0.496	0.500	0.00	0.00	56.014	1013.937	107.750	0.598	0.385

* * * * * C O N T R O L E X I T O U T P U T D A T A * * * * *

STA N. (IN)	RADIUS -E (IN)	W.A.FL (SF)	AXIAL VEL. (FT/SEC)	TANGENT. VEL. (FT/SEC)	ABS. (FT/SEC)	REL. (DEG)	AIR ANG. (DEG)	REL. PRESS. (PSI)	TOTAL PRESS. (PSI)	REL. MACH NO.	ABS. MACH NO.	LOSS FUNC
1	12.000	0.000	0.000	0.000	0.000	0.000	0.000	42.537	1088.758	134.555	0.515	0.474
2	11.592	0.600	0.600	0.600	0.74	7.11	0.00	41.788	1088.768	134.555	0.509	0.476
3	11.424	0.599	0.599	0.599	0.736	7.55	0.19	37.386	41.916	1088.768	0.503	0.478
4	11.646	0.712	0.712	0.712	0.735	7.57	0.35	37.586	40.221	1088.768	0.497	0.480
5	11.529	0.631	0.631	0.631	0.725	7.46	0.55	37.947	39.474	1088.768	0.491	0.493
6	11.411	0.595	0.595	0.595	0.72	7.62	0.97	37.237	38.552	1088.768	0.486	0.483
7	11.203	0.417	0.417	0.417	0.675	7.65	1.75	37.692	38.622	1088.768	0.480	0.485
8	11.175	0.312	0.312	0.312	0.673	7.73	2.47	38.315	36.783	1088.768	0.473	0.474
9	11.157	0.214	0.214	0.214	0.671	7.73	2.82	39.112	35.955	1088.768	0.469	0.475
10	10.939	0.101	0.101	0.101	0.671	7.75	3.13	31.556	39.411	1088.768	0.463	0.492
11	10.521	0.017	0.017	0.017	0.663	7.81	3.42	32.972	39.748	33.911	0.455	0.494

* * * * * S T A T O R E X I T O U T P U T D A T A * * * * *

STA N. (IN)	RADIUS -E (IN)	W.A.FL (SF)	AXIAL VEL. (FT/SEC)	TANGENT. VEL. (FT/SEC)	ABS. (FT/SEC)	REL. (DEG)	AIR ANG. (DEG)	REL. PRESS. (PSI)	TOTAL PRESS. (PSI)	STATOR AXIAL DIF. FACTOR	STATOR MACH NO.	LOSS FUNC
1	12.000	0.000	0.000	0.000	0.000	0.000	0.000	0.044	0.366	0.376	0.912	
2	11.487	0.599	0.599	0.599	0.72	7.55	1.29	0.043	0.358	0.376	0.912	
3	11.774	0.312	0.312	0.312	0.673	7.73	1.97	0.043	0.370	0.376	0.912	
4	11.551	0.214	0.214	0.214	0.671	7.73	2.37	0.043	0.373	0.376	0.911	
5	11.547	0.101	0.101	0.101	0.671	7.75	2.61	0.042	0.375	0.376	0.911	
6	11.434	0.017	0.017	0.017	0.663	7.81	2.89	0.042	0.377	0.376	0.911	
7	11.321	0.000	0.000	0.000	0.000	0.000	0.000	0.042	0.380	0.376	0.911	
8	11.208	0.000	0.000	0.000	0.000	0.000	0.000	0.041	0.393	0.376	0.911	
9	11.185	0.000	0.000	0.000	0.000	0.000	0.000	0.041	0.395	0.376	0.910	
10	11.092	0.000	0.000	0.000	0.000	0.000	0.000	0.041	0.398	0.376	0.910	
11	10.850	0.000	0.000	0.000	0.000	0.000	0.000	0.040	0.400	0.376	0.910	

*** OVERALL PRESSURE RATIO LIMIT HAS BEEN REACHED -- GO TO NEW DATA ***

NIN-FREE VORTEX CASE

***** PARAMETRIC STUDY OF ADVANCED MULTISTAGE AXIAL-FLOW COMPRESSORS *****

*** CFD INPUT INPUT DATA ***

NO. STAGES	NO. RAD. STAGES	SF. HEAT FACTR(LD-2)	W/H. WT. (WCLSS)	RATIO OF SP. HEAT	IN. TOT. TEMP. (DEG. R)	IN. TOT. PR. (PSI)	MASS AVG. TOT. PR. RATIO
11	11	1.200	2.9.000	1.400	519.000	14.700	9.0000

TIP RAD. (IN.4S)	TIP HEAT SPEED (FT/SEC)	AIR TO TIP RADIAL RATIO	AXIAL VEL. (FT/SEC)	TIP BLOCKAGE FACTOR	HUB BLOCKAGE FACTOR
1.2000	1.0000	2.400	500.000	1.0000	1.0000

COEFFICIENTS IN TANGENTIAL VFLCITY EQUATION

A	C	D	E
0.0000	0.0000	0.0000	0.0000

*** KITCP HUH RAMP ANGLE LIMIT VIOLATED ***
*** STATION HUH VACH NC. LIMIT VIOLATED ***
*** RJTCR HUH RAMP ANGLE LIMIT VIOLATED ***
*** RCTIP HUH RAMP ANGLE LIMIT VIOLATED ***

***** STAGE DATA *****

STAGE NO. 1

*** ROTOR INPUT DATA ***

AXIAL VEL. RATIO	Axial Velocity Efficiency	SOLIDITY AT TIP	ASPECT RATIO	TIP BLOCKAGE FACTOR	HUB BLOCKAGE FACTOR	MAX ANGLE HUB TAPER (DEGREES)	MAX ANGLE TIP TAPER (DEGREES)
1.2000	~ 0.750	1.000	4.0000	1.0000	1.0000	40.000	-20.000
MAX ROTOR DIF. FACTOR	ATN QFL. FLOW ANGLE AT STAGE OUT (DEGREES)						
1.0500	0.0000						

COEFFICIENTS IN TANGENTIAL VELOCITY EQUATION

B	C	D	E
0.0000	0.0000	30.000	0.0000

*** STATOR INPUT DATA ***

AXIAL VELOCITY RATIO	TOTAL POLYTRIPIC EFFICIENCY	SOLIDITY AT HUB	ASPECT RATIO	TIP BLOCKAGE FACTOR	HUB BLOCKAGE FACTOR	MAX ANGLE HUB TAPER (DEGREES)	MAX ANGLE TIP TAPER (DEGREES)
1.1200	0.6500	2.0000	4.0000	1.0000	1.0000	40.000	-20.0000
MAX. STATOR DIF. FACTOR	MAX HUB INLET MACH NUMBER						
1.0600	0.0000						

COEFFICIENTS IN TANGENTIAL VELOCITY EQUATION

B	C	D	E
0.0000	0.0000	0.0000	0.0000

***** STAGE CUTOUT DATA *****

MASS FLOW (LB/SEC) = 104.443

OVERALL MASS AVE. PR. RATIO	OVERALL MASS AVE. TEMP. RATIN	MASS AVE. PRESSURE RATIO	MASS AVE. TEMPERATURE RATIO	MASS AVE. EFFICIENCY	ROT TOP ASPECT RATIO	STATOR PROJ. LENGTH (INCHES)	STATOR ASPECT RATIO
1.3647	1.162	0.9421	1.1602	1.0247	1.1602	0.9431	4.0000
ROTOR TIP RAD. 1-6 (INCHES)	ROTOR HUB RAD. 1-6 (INCHES)	ROTOR HUB RAD. 2-6 (INCHES)	ROTOR HUB RAD. 3-6 (INCHES)	STATOR TIP RAD. 2-6 (INCHES)	STATOR HUB RAD. 3-6 (INCHES)	ROTOR PROJ. LENGTH (INCHES)	STATOR PROJ. LENGTH (INCHES)
12.0000	10.9000	11.4659	11.8469	11.114	6.6334	1.8000	1.3841
ROTOR TIP RAMP ANGLE (DEGREES)	ROTOR HUB RAMP ANGLE (DEGREES)	STATOR TIP RAMP ANGLE (DEGREES)	STATOR HUB RAMP ANGLE (DEGREES)				
-4.0615	4.0000	0.0000	0.0000				

13.1379

***** P O W E R I N L E T O U T P U T D A T A *****

RADIUS	W-H.FL. SPEED (FT/SEC)	AXIAL VEL. (FT/SEC)	TANGENT. VEL. (FT/SEC)	AIR VEL. (FT/SEC)	REL. VEL. (FT/SEC)	ABS. VEL. (FT/SEC)	AIR ANG. (DEG)	REL. AIR ANG. (DEG)	TOTAL TEMP. (DEG R)	TOTAL PRESS. (PSI)	REL. MACH NO.	ABS. MACH NO.	LOSS COEFF
1 1.2004	54.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	59.036	519.000	1.076	0.554	0.111
2 1.1299	54.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	57.450	519.000	1.029	0.554	0.111
3 1.0560	49.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	55.713	519.000	1.070	0.554	0.112
4 0.9840	42.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	53.87	519.000	1.070	0.554	0.112
5 0.9120	37.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	51.710	519.000	1.070	0.554	0.113
6 0.8400	32.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	49.395	519.000	1.070	0.554	0.113
7 7.780	54.0000	6.940	0.0000	6.940	37.726	0.0000	46.848	0.0000	46.848	519.000	0.810	0.554	0.114
8 6.960	59.0000	6.940	0.0000	6.940	93.420	0.0000	44.029	0.0000	44.029	519.000	0.770	0.554	0.114
9 6.240	52.0000	6.940	0.0000	6.940	79.307	0.0000	40.314	0.0000	40.314	519.000	0.733	0.554	0.115
10 5.520	45.0000	6.940	0.0000	6.940	75.604	0.0000	37.476	0.0000	37.476	519.000	0.698	0.554	0.115
11 4.800	41.0000	6.940	0.0000	6.940	721.110	0.0000	33.691	0.0000	33.691	519.000	0.666	0.554	0.114

***** R U T C P F X I T O U T P U T D A T A *****

RADIUS	W-H.FL. SPEED (FT/SEC)	AXIAL VEL. (FT/SEC)	TANGENT. VEL. (FT/SEC)	AIR VEL. (FT/SEC)	REL. VEL. (FT/SEC)	ABS. VEL. (FT/SEC)	AIR ANG. (DEG)	REL. AIR ANG. (DEG)	TOTAL TEMP. (DEG R)	TOTAL PRESS. (PSI)	ROT.R DIF. FACTOR	REL. MACH NO.	ABS. MACH NO.	LOSS FUNC
1 11.847	597.242	720.000	462.373	555.396	400.671	32.740	36.052	595.077	22.350	0.393	0.787	0.756	0.034	
2 11.293	541.404	656.218	451.631	620.957	851.776	32.960	35.411	589.755	21.742	0.394	0.753	0.734	0.033	
3 10.744	654.557	673.326	445.415	494.795	312.175	33.212	34.000	584.678	21.174	0.375	0.720	0.713	0.032	
4 10.195	64.832	436.544	436.443	780.323	774.422	33.467	32.598	579.956	20.644	0.356	0.687	0.693	0.030	
5 9.652	81.2.631	531.729	421.273	759.450	737.112	33.736	34.166	575.289	20.150	0.357	0.655	0.674	0.029	
6 9.179	755.554	511.324	412.679	737.578	70.454	34.022	29.358	570.977	19.591	0.348	0.624	0.657	0.028	
7 8.525	711.416	593.421	405.192	713.555	557.320	34.325	27.220	506.921	19.265	0.339	0.595	0.641	0.026	
8 7.971	664.273	577.223	316.755	731.375	635.283	34.051	24.696	563.120	18.873	0.330	0.567	0.627	0.025	
9 7.419	613.140	562.542	394.277	537.296	805.842	21.630	559.574	18.511	0.319	0.542	0.615	0.023		
10 6.864	572.500	550.652	391.513	575.844	579.700	35.401	18.180	556.283	18.307	0.320	0.606	0.606	0.022	
11 575.865	54.0000	292.791.437	667.351	557.795	35.355	13.372	553.247	17.877	0.292	0.500	0.600	0.600	0.020	

***** S T A T C R F X I T O U T P U T D A T A *****

RADIUS	STA -E (IN)	AXIAL VEL. (FT/SEC)	TANGENT. VEL. (FT/SEC)	AIR VEL. (FT/SEC)	AIR ANG. (DEG)	STA TUR DIF. FACTOR								
1 11.847	306.400	765.562	1.000	724.728	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
2 11.326	306.400	563.595	0.000	693.396	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
3 11.904	306.400	559.461	0.000	553.591	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
4 11.283	306.400	516.361	0.000	515.361	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
5 9.762	306.400	542.414	0.000	542.414	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
6 6.240	306.400	559.461	0.000	553.591	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
7 8.719	306.400	516.361	0.000	515.361	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
8 6.137	306.400	516.361	0.000	515.361	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
9 7.476	306.400	472.312	0.000	472.312	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
10 7.155	306.400	426.040	0.000	426.040	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
11 6.433	306.400	384.235	0.000	384.235	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000

*** ROTOR HUB RELATIVE ANGLE LIMIT VIOLATED ***

*** STATOR HUB D FACTOR LIMIT VIOLATED ***

***** STAGE DATA *****

STAGE NO. 2

*** ROTOR INPUT DATA ***

AXIAL VEL. RATIO	POLYTOPIC EFFICIENCY	SLIPPERY AT TIP	TIP BLOCKAGE FACTOR	HUB BLOCKAGE FACTOR	MAX ANGLE HUB TAPER (DEGREES)	MAX ANGLE TIP TAPER (DEGREES)
1.0000	0.5750	1.0000	3.0000	1.0000	40.0000	-20.0000

MAX ROTOP
ANGLE 3-D TIP HUB
(DEGREES)

1.0000

-1.0000

AXIAL VELCITY RATIO	TOTAL POLYTOPIC EFFICIENCY	SLIPPERY AT HUB	TIP BLOCKAGE FACTOR	HUB BLOCKAGE FACTOR	MAX ANGLE HUB TAPER (DEGREES)	MAX ANGLE TIP TAPER (DEGREES)
1.0000	0.3500	2.0000	3.5000	1.0000	40.0000	-20.0000

MAX COEFFICIENTS IN TANGENTIAL VELOCITY EQUATION

B C D E

0.0000 0.0000 0.0000 0.0000

*** STATOR INPUT DATA ***

AXIAL VELCITY RATIO	TOTAL POLYTOPIC EFFICIENCY	SLIPPERY AT HUB	TIP BLOCKAGE FACTOR	HUB BLOCKAGE FACTOR	MAX ANGLE HUB TAPER (DEGREES)	MAX ANGLE TIP TAPER (DEGREES)
1.0000	0.3500	2.0000	3.5000	1.0000	40.0000	-20.0000

MAX COEFFICIENTS IN TANGENTIAL VELOCITY EQUATION

B C D E

0.0000 0.0000 0.0000 0.0000

***** STAG F OUTPUT DATA *****

MASS FLOW (LB/SEC) = 104.443

OVERALL MASS AVE. PR. RATIO	OVERALL MASS AVE. PRESSURE EFFICIENCY	MASS AVE. PRESSURE RATIO	MASS AVE. TEMPERATURE RATIO	MASS AVE. EFFICIENCY
1.6815	1.1927	1.0000	1.02342	1.0733

ROTOR TIP RAD. 1-G (INCHES)	ROTOR TIP RAD. 2-G (INCHES)	ROTOR HUB RAD. 2-G (INCHES)	STATOR TIP RAD. 3-G (INCHES)	STATOR HUB RAD. 3-G (INCHES)	ROTOR PROJ. LENGTH (INCHES)	STATOR PROJ. LENGTH (INCHES)
1.1045	6.0534	1.1045	1.1045	1.1045	7.5460	1.4396

STATOR TIP RAD. ANGLE (DEGREES)	STATOR HUB RAD. ANGLE (DEGREES)	STATOR TIP RAMP ANGLE (DEGREES)	STATOR HUB RAMP ANGLE (DEGREES)
1.0000	20.0000	0.0000	6.9607

***** R T O P I N L E T O U T P U T D A T A *****

STA NO.	RADIUS -F (IN)	WHEEL			AXIAL			TANGENT.			ABS. VEL. (FT/SEC)			REL. VEL. (FT/SEC)			AIR ANG. (DEG)			TOTAL PRESS. (PSI)			REL. MACH NO.			ABS. MACH NO.			LOSS CREEF		
		SIDE	VELOCITY	ANGLE	VELOCITY	ANGLE	ANGLE	VELOCITY	ANGLE	ANGLE	VELOCITY	ANGLE	ANGLE	VELOCITY	ANGLE	ANGLE	VELOCITY	ANGLE	ANGLE	VELOCITY	ANGLE	ANGLE	VELOCITY	ANGLE	ANGLE	VELOCITY	ANGLE	ANGLE			
1	11.347	6.67	242	3.51	4.0	1.0	0.0	3.51	4.0	1.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	50.757	595.087	22.084	1.067	0.675	0.059	1.021	0.644	0.062				
2	11.324	5.43	737	7.65	6.82	1.0	0.0	5.52	12.15	3.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	50.9	58.9	21.505	1.076	0.612	0.066	1.024	0.647	0.068				
3	11.304	5.10	451	7.24	7.74	1.0	0.0	5.28	11.55	7.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	51.168	58.4	67.8	1.054	0.579	0.072	1.024	0.613	0.069				
4	11.282	5.84	523	5.93	5.62	0.0	0.0	5.43	5.64	10.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	51.419	57.9	85.6	1.044	0.547	0.074	1.024	0.578	0.078				
5	9.762	11.30	452	4.42	2.14	0.0	0.0	5.42	4.24	16.36	4.16	0.0	0.0	0.0	0.0	0.0	0.0	0.0	51.759	57.5	28.9	1.069	0.542	0.074	1.024	0.577	0.079				
6	5.240	7.71	314	3.01	5.83	0.0	0.0	5.10	5.36	9.76	5.07	0.0	0.0	0.0	0.0	0.0	0.0	0.0	52.049	57.0	97.7	1.052	0.534	0.096	1.024	0.513	0.096				
7	7.10	7.25	559	2.59	4.81	0.0	0.0	5.58	4.31	9.16	4.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0	52.452	56.6	92.1	1.017	0.479	0.095	1.024	0.796	0.095				
8	11.167	6.61	123	516	6.61	0.0	0.0	5.15	9.21	8.56	0.38	0.0	0.0	0.0	0.0	0.0	0.0	0.0	52.935	56.3	12.0	1.073	0.444	0.105	1.024	0.776	0.105				
9	7.176	6.22	672	4.76	6.12	0.0	0.0	4.72	9.12	7.95	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	53.074	55.9	3.89	0.686	0.408	0.123	1.024	0.408	0.123				
10	7.155	5.85	234	4.26	5.32	0.0	0.0	4.26	7.49	7.34	5.77	0.0	0.0	0.0	0.0	0.0	0.0	0.0	54.259	55.6	2.83	1.070	0.636	0.137	1.024	0.371	0.137				
11	6.637	5.91	727	5.24	2.25	0.0	0.0	3.24	4.39	6.73	2.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0	55.197	55.3	24.7	1.077	0.584	0.333	1.024	0.333	0.159				

***** R T C R E X I T C U T P U T D A T A *****

STA NO.	RADIUS -F (IN)	WHEEL			AXIAL			TANGENT.			ABS. VEL. (FT/SEC)			REL. VEL. (FT/SEC)			AIR ANG. (DEG)			TOTAL PRESS. (PSI)			REL. MACH NO.			ABS. MACH NO.			LOSS FUNC		
		SIDE	VELOCITY	ANGLE	VELOCITY	ANGLE	ANGLE	VELOCITY	ANGLE	ANGLE	VELOCITY	ANGLE	ANGLE	VELOCITY	ANGLE	ANGLE	VELOCITY	ANGLE	ANGLE	VELOCITY	ANGLE	ANGLE	VELOCITY	ANGLE	ANGLE	VELOCITY	ANGLE	ANGLE			
1	11.347	6.67	242	3.51	4.0	1.0	0.0	3.51	4.0	1.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	42.177	63.7	26.5	27.236	0.224	0.719	0.016	1.024	0.647	0.017			
2	11.324	5.43	737	7.65	6.82	1.0	0.0	5.52	12.15	3.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	41.753	53.1	93.4	23.5	0.872	0.689	0.017	1.024	0.613	0.019			
3	11.304	5.10	451	7.24	7.74	1.0	0.0	5.28	11.55	7.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	41.245	51.5	93.7	24.5	0.825	0.660	0.019	1.024	0.591	0.019			
4	11.282	5.84	523	5.93	5.62	0.0	0.0	5.43	5.64	10.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	40.935	52.0	95.6	25.349	0.252	0.766	0.019	1.024	0.631	0.019			
5	9.762	3.73	639	5.42	2.16	0.0	0.0	5.42	2.16	3.02	0.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0	39.891	49.7	1.91	24.801	0.274	0.712	0.019	1.024	0.604	0.019			
6	5.219	9.61	563	5.01	5.34	0.0	0.0	5.16	5.17	3.78	5.39	0.0	0.0	0.0	0.0	0.0	0.0	0.0	27.759	38.953	1.56	24.290	0.238	0.657	0.020	1.024	0.578	0.020			
7	9.173	7.64	427	5.64	4.34	0.0	0.0	5.31	4.34	6.49	4.31	0.0	0.0	0.0	0.0	0.0	0.0	0.0	30.679	37.786	1.816	23.816	0.322	0.553	0.022	1.024	0.602	0.022			
8	8.727	7.27	291	5.15	3.51	0.0	0.0	3.45	3.57	6.22	5.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0	34.195	34.2	2.9	35.350	0.546	0.531	0.023	1.024	0.551	0.023			
9	8.262	5.61	155	4.72	6.12	0.0	0.0	3.57	4.11	5.69	5.73	0.0	0.0	0.0	0.0	0.0	0.0	0.0	37.721	37.7	2.21	34.338	0.293	0.489	0.026	1.024	0.494	0.026			
10	7.936	6.53	619	4.20	5.89	0.0	0.0	3.27	5.67	5.74	5.79	0.0	0.0	0.0	0.0	0.0	0.0	0.0	42.129	31.703	7.03	22.602	0.423	0.431	0.026	1.024	0.494	0.026			
11	7.391	5.15	393	3.84	2.35	0.0	0.0	4.11	3.72	5.62	5.99	0.0	0.0	0.0	0.0	0.0	0.0	0.0	43.575	46.953	2.24	22.264	0.471	0.372	0.032	1.024	0.482	0.032			

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***** S T A T C & E X I T C U T P U T D A T A *****

STA NO.	RADIUS -E (IN)	AXIAL			TANGENT.			ABS. VEL. (FT/SEC)			REL. VEL. (FT/SEC)			AIR ANG. (DEG)			TOTAL PRESS. (PSI)			REL. MACH NO.			ABS. MACH NO.			LOSS FUNC		
		SIDE	VELOCITY	ANGLE	VELOCITY	ANGLE	ANGLE	VELOCITY	ANGLE	ANGLE	VELOCITY	ANGLE	ANGLE	VELOCITY	ANGLE	ANGLE	VELOCITY	ANGLE	ANGLE	VELOCITY	ANGLE	ANGLE	VELOCITY	ANGLE	ANGLE	VELOCITY	ANGLE	ANGLE
1	11.347	6.67	242	3.51	4.0	1.0	0.0	3.51	4.0	1.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	42.177	63.7	26.5	27.236	0.224	0.719	0.016	1.024	0.647	0.017
2	11.417	5.43	737	7.65	6.82	1.0	0.0	5.52	12.15	3.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	41.753	53.1	93.4	23.5	0.872	0.689	0.017	1.024	0.613	0.019	
3	11.597	6.61	451	7.24	7.74	1.0	0.0	5.28	11.55	7.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0	41.245	51.5	95.6	25.349	0.252	0.766	0.019	1.024	0.631	0.019	
4	11.557	5.84	523	5.93	5.62	0.0	0.0	5.43	5.64	10.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0	40.935	49.7	1.91	24.801	0.274	0.712	0.019	1.024	0.578	0.019	
5	11.127	4.20	214	5.42	2.16	0.0	0.0	5.42	2.16	3.02	0.93	0.0	0.0	0.0	0.0	0.0	0.0	39.891	49.7	1.91	24.801	0.274	0.712	0.019	1.024	0.578	0.019	
6	9.556	3.84	236	5.62	5.34	0.0	0.0	5.52	5.34	6.25	5.36	0.0	0.0	0.0	0.0	0.0	0.0	40.536	49.7	2.21	24.801	0.274	0.712	0.019	1.024	0.578	0.019	
7	9.244	3.59	451	5.15	4.34	0.0	0.0	3.45	3.57	6.22	5.74	0.0	0.0	0.0	0.0	0.0	0.0	34.195	34.2	2.9	35.350	0.546	0.531	0.023	1.024	0.551	0.023	
8	8.835	3.15	451	5.15	4.34	0.0	0.0	3.45	3.57	6.22	5.74	0.0	0.0	0.0	0.0	0.0	0.0	34.195	34.2	2.9	35.350	0.5						

*** RELATIVE HUB ANGLE RELATIVE ANGLE LIMIT VIOLATED ***
*** STATION HUB D FACTOR LIMIT VIOLATED ***

***** STAGE DATA *****

STAGE NO. 2

*** ROTOR INPUT DATA ***

AXIAL VELOCITY RATIO	POLYTRONIC EFFICIENCY	SOLIDITY AT TIP	ASPECT RATIO	TIP BLOCKAGE FACTOR	HUB BLOCKAGE FACTOR	MAX ANGLE HUB TAPER (DEGREES)	MAX ANGLE TIP TAPER (DEGREES)
1.000	2.275	1.000	2.500	1.000	1.000	40.000	-20.000
MAX ROTOR ANGLE TIP TAPER (DEGREES)							
41.46° ± 2.00° ± 0.00°							
MAX ROTOR ANGLE 20.00°							
MAX ROTOR ANGLE 20.00°							
MAX ROTOR ANGLE 20.00°							

COEFFICIENTS IN TANGENTIAL VELOCITY EQUATION

R	C	C	D	E
0.000	0.000	0.000	0.000	0.000

*** STATOR INPUT DATA ***

AXIAL VELOCITY RATIO	TOTAL POLYTRONIC EFFICIENCY	SOLIDITY AT HUB	ASPECT RATIO	TIP BLOCKAGE FACTOR	HUB BLOCKAGE FACTOR	MAX ANGLE HUB TAPER (DEGREES)	MAX ANGLE TIP TAPER (DEGREES)
1.000	0.350	2.000	2.500	1.000	1.000	40.000	-20.000
MAX STATOR MACH HUB INLET MACH NUMBER							
0.500							
MAX STATOR MACH NUMBER							

COEFFICIENTS IN TANGENTIAL VELOCITY EQUATION

R	C	C	D	E
0.000	0.000	0.000	0.000	0.000

***** STAGE OUTPUT DATA *****

OVERALL MASS AVE. PR. RATING	OVERALL MASS AVE. TEMP. RATING	MASS AVE. PRESSURE RATIO	MASS AVE. TEMPERATURE RATIO	ROTOR ASPECT RATIO	STATOR ASPECT RATIO
2.0931	1.2759	1.3139	1.2410	1.0753	0.8453
ROTOR TIP RAD. 1-6 (INCHES)	ROTOR TIP RAD. 2-6 (INCHES)	ROTOR HUB RAD. 2-6 (INCHES)	ROTOR HUB RAD. 3-6 (INCHES)	ROTOR PROJ. LENGTH (INCHES)	STATOR PROJ. LENGTH (INCHES)
11.8469	7.5450	11.9469	0.1451	11.8469	8.2791
STATOR HUB RAMP ANGLE (DEGREES)					
13.02286					
0.00000					
5.1331					

***** R C T J P I N L E T O U T P U T D A T A *****

STA NO.	RADIUS -F (IN)	WHEEL		AXIAL		TANGENT.		ABS.		REL.		TOTAL		RET. MACH NO.	ABS. MACH NO.	LOSS COEFF
		SPEED (FT/SEC)	VEL. (FT/SEC)	VFL. (FT/SEC)	VEL. (FT/SEC)	VEL. (FT/SEC)	VEL. (FT/SEC)	AIR ANG. (DEG)	AIR ANG. (DEG)	TEMP. (DEG R)	TEMP. (DEG R)	TOTAL PRESS. (PSI)				
1	11.947	6.61.242	306.***	0.0.0.0	0.0.0.0	1274.727	0.0.0.0	50.757	637.266	27.074	1.0.31	0.652	0.062			
2	11.417	6.61.412	765.552	0.0.0.0	0.0.0.0	1221.224	0.0.0.0	51.174	631.934	26.405	0.592	0.622	0.065			
3	10.697	6.61.551	724.723	0.0.0.0	0.0.0.0	167.632	0.0.0.0	51.636	626.856	25.779	0.552	0.591	0.070			
4	10.557	6.61.554	683.654	0.0.0.0	0.0.0.0	114.097	0.0.0.0	52.151	622.035	25.194	0.912	0.559	0.075			
5	10.127	643.313	642.216	0.0.0.0	0.0.0.0	136.459	0.0.0.0	52.728	617.468	24.647	0.871	0.528	0.081			
6	9.656	AC3.0.43	504.536	0.0.0.0	0.0.0.0	1036.763	0.0.0.0	53.380	613.156	24.139	0.830	0.495	0.088			
7	6.265	772.139	558.491	0.0.0.0	0.0.0.0	952.997	0.0.0.0	54.124	609.100	23.667	0.798	0.462	0.096			
8	8.836	735.359	515.951	0.0.0.0	0.0.0.0	899.150	0.0.0.0	54.980	605.299	23.230	0.746	0.428	0.105			
9	8.456	750.518	97.012	0.0.0.0	0.0.0.0	72.912	0.0.0.0	55.977	601.753	22.828	0.703	0.393	0.117			
10	7.976	654.572	529.056	0.0.0.0	0.0.0.0	429.036	0.0.0.0	57.156	598.462	22.458	0.666	0.358	0.131			
11	7.546	673.837	584.230	0.0.0.0	0.0.0.0	284.230	0.0.0.0	58.574	595.426	22.121	0.616	0.321	0.147			

***** R C T C R E X I T O U T P U T D A T A *****

STA NO.	RADIUS -F (IN)	WHEEL		AXIAL		TANGENT.		ABS.		REL.		TOTAL		RET. MACH NO.	ABS. MACH NO.	LOSS COEFF
		SPEED (FT/SEC)	VEL. (FT/SEC)	VEL. (FT/SEC)	VEL. (FT/SEC)	VEL. (FT/SEC)	VEL. (FT/SEC)	AIR ANG. (DEG)	AIR ANG. (DEG)	TEMP. (DEG R)	TEMP. (DEG R)	TOTAL PRESS. (PSI)				
1	11.847	547.242	546.416	454.574	470.713	19.330	41.136	633.757	33.590	0.245	0.876	0.699	0.018			
2	11.477	653.492	765.552	291.372	319.449	1013.737	29.475	49.352	678.425	32.818	0.257	0.829	0.670	0.019		
3	11.107	525.592	724.724	785.625	955.246	22.603	40.722	673.348	32.094	0.271	0.783	0.642	0.019			
4	10.737	394.722	635.564	312.121	751.439	998.179	24.541	46.446	568.526	31.417	0.286	0.735	0.615	0.020		
5	10.267	663.892	348.214	323.214	719.948	330.469	26.719	40.894	653.959	30.784	0.304	0.688	0.589	0.021		
6	9.997	833.842	600.634	345.244	637.757	744.038	29.171	39.557	659.648	30.194	0.324	0.639	0.564	0.022		
7	9.526	812.212	558.431	549.119	658.133	713.794	31.936	39.113	655.591	29.647	0.347	0.590	0.540	0.023		
8	9.256	771.322	515.951	342.227	633.331	553.629	35.055	38.424	551.790	26.139	0.374	0.540	0.517	0.024		
9	8.836	740.524	472.912	377.415	644.865	595.414	38.570	37.540	648.244	26.671	0.406	0.490	0.497	0.026		
10	8.516	702.681	549.53	392.109	532.993	42.652	36.996	644.953	28.241	0.444	0.438	0.479	0.028			
11	8.146	573.814	394.230	311.340	562.915	469.162	46.554	34.841	641.917	27.848	0.430	0.463	0.463	0.031		

***** S T A T O R E X I T O U T P U T D A T A *****

STA NO.	RADIUS -F (IN)	AXIAL		TANGENT.		ABS.		AIR ANG. (DEG)		STATOR AXIAL DIF. FACTOR		STATOR DIF. FACTOR		STATOR AXIAL MACH NO.	STATOR DIF. MACH NO.	LOSS FUNC.
		VFL. (FT/SEC)	VEL. (FT/SEC)	VFL. (FT/SEC)	VEL. (FT/SEC)	AIR ANG. (DEG)	AIR ANG. (DEG)	TEMP. (DEG R)	TEMP. (DEG R)	REL. (DEG)	REL. (DEG)	LOSS COEFF	COEFF			
1	11.947	765.552	755.052	724.723	724.723	0.0.0.0	0.0.0.0	0.0.0.0	0.0.0.0	0.0.0.0	0.0.0.0	0.022	0.176	0.656	0.008	
2	11.490	558.431	558.431	515.951	515.951	0.0.0.0	0.0.0.0	0.0.0.0	0.0.0.0	0.0.0.0	0.0.0.0	0.024	0.193	0.623	0.008	
3	11.133	515.951	515.951	472.912	472.912	0.0.0.0	0.0.0.0	0.0.0.0	0.0.0.0	0.0.0.0	0.0.0.0	0.026	0.207	0.590	0.009	
4	10.777	472.912	472.912	429.595	429.595	0.0.0.0	0.0.0.0	0.0.0.0	0.0.0.0	0.0.0.0	0.0.0.0	0.028	0.226	0.556	0.009	
5	10.420	429.595	429.595	386.215	386.215	0.0.0.0	0.0.0.0	0.0.0.0	0.0.0.0	0.0.0.0	0.0.0.0	0.030	0.249	0.522	0.010	
6	10.053	386.215	386.215	348.215	348.215	0.0.0.0	0.0.0.0	0.0.0.0	0.0.0.0	0.0.0.0	0.0.0.0	0.033	0.276	0.488	0.010	
7	9.706	348.215	348.215	305.613	305.613	0.0.0.0	0.0.0.0	0.0.0.0	0.0.0.0	0.0.0.0	0.0.0.0	0.036	0.307	0.454	0.011	
8	9.340	305.613	305.613	262.912	262.912	0.0.0.0	0.0.0.0	0.0.0.0	0.0.0.0	0.0.0.0	0.0.0.0	0.039	0.344	0.420	0.011	
9	8.753	262.912	262.912	220.912	220.912	0.0.0.0	0.0.0.0	0.0.0.0	0.0.0.0	0.0.0.0	0.0.0.0	0.042	0.385	0.385	0.011	
10	8.035	220.912	220.912	178.912	178.912	0.0.0.0	0.0.0.0	0.0.0.0	0.0.0.0	0.0.0.0	0.0.0.0	0.045	0.439	0.349	0.012	
11	8.270	178.912	178.912	146.428	146.428	0.0.0.0	0.0.0.0	0.0.0.0	0.0.0.0	0.0.0.0	0.0.0.0	0.048	0.313	0.313	0.012	

*** STATE HUGH D FACTOR LIMIT VIOLATED ***

***** STAGE DATA *****

STAGE NO. 4

*** WRITER INPUT DATA ***

	Axial Velocity Ratio	Solidity at Tip	Aspect Ratio	HUB BLOCKAGE Factor	MAX ANGLE HUB TAPER (DEGREES)
1.0450	1.0750	1.0000	1.0000	1.0000	-20.000
MAX ROTATIONAL DIFF. FACTOR	MAX REL. FLOW ANGLE ROTOR HUB (DEGREES)				
1.0500	-1.0000				

*** STAGE INPUT DATA ***

	Axial Velocity Ratio	Solidity at Hub	Aspect Ratio	HUB BLOCKAGE Factor	MAX ANGLE HUB TAPER (DEGREES)
1.0000	1.0000	1.0000	1.0000	1.0000	-20.0000
MAX STATOR DIFF. FACTOR	MAX HUB INLET MACH NUMBER				
0.9500	1.0000				

*** COEFFICIENTS IN TANGENTIAL VELOCITY EQUATION

B	C	D	E
0.0000	0.0000	0.0000	0.0000

*** COEFFICIENTS IN TANGENTIAL VELOCITY EQUATION

B	C	D	E
0.0000	0.0000	0.0000	0.0000

MASS FLOW (LB/SEC) = 104.443

OVERALL MASS AVE. PR. RATIO	OVERALL MASS AVE. TEMP. RATIO	MASS AVE. PRESSURE RATIO	MASS AVE. TEMPERATURE RATIO	RQTR ASPECT RATIO	STATOR PROJ. LENGTH (INCHES)
2.0823	1.3750	0.8295	1.2409	1.0752	0.8453
ROTOR TIP RAD. 1-6 (INCHES)	ROT. TIP RAD. 2-6 (INCHES)	ROTOR HUB RAD. 2-6 (INCHES)	STATOR TIP RAD. 3-6 (INCHES)	ROTOR HUB RAD. 3-6 (INCHES)	ROTOR PROJ. LENGTH (INCHES)
11.8469	9.3794	11.8469	9.7507	11.8469	8.8550
ROTOR TIP RAMP ANGLES (DEGREES)	ROTOR HUB RAMP ANGLE (DEGREES)	STATOR TIP RAMP ANGLE (DEGREES)	STATOR HUB RAMP ANGLE (DEGREES)	STATOR PROJ. LENGTH (INCHES)	STATOR HUB RAMP ANGLE (DEGREES)
0.0000	0.0000	0.0000	0.0000	1.2385	4.9979

***** STATION INLET OUTPUT DATA *****

RADIUS	STA -E	WHEEL SPEED (FT/SEC)	TANGENT.	ABS. VEL.	REL. VEL.	AIR ANG. (DEG)	REL. AIR ANG. (DEG)	TOTAL TEMP. (DEG R)	TOTAL PRESS. (PSI)	REL. MACH NO.	ABS. MACH NO.	LOSS COEFF
NO.	(IN)	(FT/SEC)	(FT/SEC)	(FT/SEC)	(FT/SEC)	(DEG)	(DEG)	(DEG R)	(PSI)			
1	11.947	587.242	3.6.4.0	Co.0.5	1274.727	0.0.0.0	50.757	583.757	33.383	0.995	0.629	0.065
2	11.491	587.511	7.0.0.452	Co.2.0	1225.980	0.0.0.0	51.352	678.455	32.515	0.961	0.500	0.069
3	11.122	927.779	7.24.0.729	Co.0.0	1177.286	0.0.0.0	52.065	673.368	31.894	0.925	0.570	0.073
4	10.777	587.645	5.83.0.326	Co.0.0	1429.623	0.0.0.0	52.724	658.526	31.219	J.8C1	0.540	0.079
5	10.42	941.319	5.42.0.214	Co.0.0	1390.955	0.0.0.0	53.512	663.955	30.585	0.856	0.509	0.081
6	10.073	587.592	6.0.0.246	Co.0.0	1031.439	0.0.0.0	54.372	659.648	30.062	0.822	0.477	0.089
7	9.726	587.352	5.57.0.457	Co.0.0	382.934	0.0.0.0	55.375	29.456	0.784	0.445	0.096	
8	9.345	777.419	4.15.0.651	Co.0.0	936.490	0.0.0.0	56.494	651.790	0.747	0.413	0.105	
9	8.943	747.337	4.72.0.517	Co.0.0	386.131	0.0.0.0	57.745	448.244	0.711	0.379	0.115	
10	8.546	717.455	4.27.0.401	Co.0.0	827.962	0.0.0.0	59.195	644.953	28.057	0.673	0.345	0.125
11	8.275	587.923	5.94.0.232	Co.0.0	780.755	0.0.0.0	59.385	641.917	27.666	0.636	0.310	0.139

***** STATION EXIT OUTPUT DATA *****

RADIUS	STA -E	WHEEL SPEED (FT/SEC)	TANGENT.	ABS. VEL.	REL. VEL.	AIR ANG. (DEG)	REL. AIR ANG. (DEG)	TOTAL TEMP. (DEG R)	TOTAL PRESS. (PSI)	REL. MACH NO.	ABS. MACH NO.	LOSS FUNC
NO.	(IN)	(FT/SEC)	(FT/SEC)	(FT/SEC)	(FT/SEC)	(DEG)	(DEG)	(DEG R)	(PSI)			
1	11.947	597.242	4.0.0.400	Co.2.0	1057.473	20.0.647	40.280	733.678	41.427	0.262	0.832	0.019
2	11.537	587.443	745.452	Co.2.0	326.745	1.0.0.3.92	22.371	40.305	728.356	0.275	0.791	0.651
3	11.228	587.434	724.724	Co.0.0	752.479	2.51.0.510	23.364	40.319	723.289	0.299	0.749	0.524
4	10.918	907.436	693.596	Co.0.0	329.707	7.54.0.953	25.740	40.319	719.467	0.305	0.707	0.598
5	10.609	994.034	642.215	Co.0.0	336.333	726.351	842.106	40.305	713.900	38.106	0.323	0.573
6	10.259	354.232	601.525	Co.0.0	349.531	564.386	787.032	30.201	40.267	739.598	0.343	0.621
7	9.990	932.433	526.465	Co.0.0	564.662	731.271	32.832	40.206	705.532	0.366	0.577	0.525
8	9.690	816.629	515.951	Co.0.0	371.295	626.043	676.715	35.782	40.115	701.731	0.392	0.533
9	9.370	780.925	472.513	Co.0.0	306.102	509.205	617.229	39.909	39.997	498.195	0.422	0.488
10	9.060	785.023	462.040	Co.0.0	307.311	534.773	558.531	42.793	39.817	694.364	0.456	0.442
11	8.751	723.221	410.379	Co.0.0	302.007	499.658	460.953	39.308	39.358	591.858	0.499	0.445

***** STATION EXIT OUTPUT DATA *****

RADIUS	STA -E	WHEEL SPEED (FT/SEC)	TANGENT.	ABS. VEL.	REL. VEL.	AIR ANG. (DEG)	REL. AIR ANG. (DEG)	TOTAL TEMP. (DEG R)	TOTAL PRESS. (PSI)	REL. MACH NO.	ABS. MACH NO.	LOSS FUNC
NO.	(IN)	(FT/SEC)	(FT/SEC)	(FT/SEC)	(FT/SEC)	(DEG)	(DEG)	(DEG R)	(PSI)			
1	11.947	597.242	4.0.0.400	Co.0.0	302.000	4.0.0.4.00	20.0.647	40.280	733.678	0.262	0.832	0.019
2	11.549	587.452	745.452	Co.0.0	726.728	2.51.0.510	22.371	40.305	728.356	0.275	0.791	0.651
3	11.243	587.434	724.724	Co.0.0	303.000	7.54.0.953	23.364	40.319	723.289	0.299	0.749	0.524
4	10.951	907.436	693.596	Co.0.0	304.000	642.215	842.106	40.305	713.900	38.106	0.323	0.573
5	10.652	994.034	642.215	Co.0.0	305.000	542.215	594.215	40.305	703.500	30.106	0.323	0.573
6	10.353	354.232	601.525	Co.0.0	306.000	534.773	558.531	42.793	39.817	694.364	0.456	0.442
7	10.054	587.452	558.461	Co.0.0	307.000	515.000	534.773	42.793	39.817	694.364	0.456	0.442
8	9.755	515.000	515.000	Co.0.0	308.000	472.000	472.000	40.305	39.817	694.364	0.456	0.442
9	9.457	472.000	472.000	Co.0.0	309.000	427.000	427.000	40.305	39.817	694.364	0.456	0.442
10	9.158	427.000	427.000	Co.0.0	310.000	384.220	384.220	40.305	39.817	694.364	0.456	0.442
11	8.859	384.220	384.220	Co.0.0	311.000	344.220	344.220	40.305	39.817	694.364	0.456	0.442

***** STATION EXIT OUTPUT DATA *****

RADIUS	STA -E	WHEEL SPEED (FT/SEC)	TANGENT.	ABS. VEL.	REL. VEL.	AIR ANG. (DEG)	REL. AIR ANG. (DEG)	TOTAL TEMP. (DEG R)	TOTAL PRESS. (PSI)	REL. MACH NO.	ABS. MACH NO.	LOSS FUNC
NO.	(IN)	(FT/SEC)	(FT/SEC)	(FT/SEC)	(FT/SEC)	(DEG)	(DEG)	(DEG R)	(PSI)			
1	11.947	597.242	4.0.0.400	Co.0.0	302.000	4.0.0.4.00	20.0.647	40.280	733.678	0.262	0.832	0.019
2	11.549	587.452	745.452	Co.0.0	726.728	2.51.0.510	22.371	40.305	728.356	0.275	0.791	0.651
3	11.243	587.434	724.724	Co.0.0	303.000	7.54.0.953	23.364	40.319	723.289	0.299	0.749	0.524
4	10.951	907.436	693.596	Co.0.0	304.000	642.215	842.106	40.305	713.900	38.106	0.323	0.573
5	10.652	994.034	642.215	Co.0.0	305.000	542.215	594.215	40.305	703.500	30.106	0.323	0.573
6	10.353	354.232	601.525	Co.0.0	306.000	534.773	558.531	42.793	39.817	694.364	0.456	0.442
7	10.054	587.452	558.461	Co.0.0	307.000	515.000	534.773	42.793	39.817	694.364	0.456	0.442
8	9.755	515.000	515.000	Co.0.0	308.000	472.000	472.000	40.305	39.817	694.364	0.456	0.442
9	9.457	472.000	472.000	Co.0.0	309.000	427.000	427.000	40.305	39.817	694.364	0.456	0.442
10	9.158	427.000	427.000	Co.0.0	310.000	384.220	384.220	40.305	39.817	694.364	0.456	0.442
11	8.859	384.220	384.220	Co.0.0	311.000	344.220	344.220	40.305	39.817	694.364	0.456	0.442

***** STATION EXIT OUTPUT DATA *****

RADIUS	STA -E	WHEEL SPEED (FT/SEC)	TANGENT.	ABS. VEL.	REL. VEL.	AIR ANG. (DEG)	REL. AIR ANG. (DEG)	TOTAL TEMP. (DEG R)	TOTAL PRESS. (PSI)	REL. MACH NO.	ABS. MACH NO.	LOSS FUNC
NO.	(IN)	(FT/SEC)	(FT/SEC)	(FT/SEC)	(FT/SEC)	(DEG)	(DEG)	(DEG R)	(PSI)			
1	11.947	597.242	4.0.0.400	Co.0.0	302.000	4.0.0.4.00	20.0.647	40.280	733.678	0.262	0.832	0.019
2	11.549	587.452	745.452	Co.0.0	726.728	2.51.0.510	22.371	40.305	728.356	0.275	0.791	0.651
3	11.243	587.434	724.724	Co.0.0	303.000	7.54.0.953	23.364	40.319	723.289	0.299	0.749	0.524
4	10.951	907.436	693.596	Co.0.0	304.000	642.215	842.106	40.305	713.900	38.106	0.323	0.573
5	10.652	994.034	642.215	Co.0.0	305.000	542.215	594.215	40.305	703.500	30.106	0.323	0.573
6	10.353	354.232	601.525	Co.0.0	306.000	534.773	558.531	42.793	39.817	694.364	0.456	0.442
7	10.054	587.452	558.461	Co.0.0	307.000	515.000	534.773	42.793	39.817	694.364	0.456	0.442
8	9.755	515.000	515.000	Co.0.0	308.000	472.000	472.000	40.305	39.817	694.364	0.456	0.442
9	9.457	472.000	472.000	Co.0.0	309.000	427.000	427.000	40.305	39.817	694.364	0.456	0.442
10	9.158	427.000	427.000	Co.0.0	310.000	384.						

*** STARTING WITH A FACTORY LIMIT VIOLATED ***

***** STAGE DATA *****

STAGE NO. 5

* * * * * DATA PAGE

COEFFICIENTS IN TANGENTIAL VELOCITY EQUATION					
Axial Velocity Pattern	Total Ductoric Efficiency	Solidity at hub	Aspect Ratio	Tip Blockage Factor	Hub Blockage Factor
1.000	0.950	2.000	2.000	1.000	40.000
0.500	0.200	0.500	0.500	0.500	-20.000

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***** F F T O R I N L E T O U T P U T D A T A *****

RADIUS STA NO. (IN)	WHEEL SPEED (FT/SEC.)	TANGENT. VEL. (FT/SEC.)	ABS. VEL. (FT/SEC.)	REL. VEL. (FT/SEC.)	AIR ANG. (DEG.)	REL. AIR ANG. (DEG.)	TOTAL PRESS. (PSI)		REFL. MACH NO.	ABS. MACH NO.	LOSS COEFF		
							AIR ANG. (DEG.)	TEMP. (DEG R)					
1 11.947	9.07	24.2	30.6	4.1	30.6	4.1	274	727	0.000	50.757	733	628	
2 11.546	6.62	34.3	76.5	6.52	76.5	6.52	1223	757	0.000	51.494	729	366	
3 11.248	5.27	44.3	72.4	7.28	72.4	7.28	1134	919	0.000	52.293	723	289	
4 10.954	4.12	54.4	58.3	5.36	58.3	5.36	935	595	0.000	53.163	718	467	
5 10.652	3.87	57.4	54.2	2.35	54.2	2.35	640	2.56	10.95	54.114	713	900	
6 10.353	3.62	74.5	60.1	6.25	60.1	6.25	1051	175	0.000	55.155	709	588	
7 10.054	3.37	94.5	55.8	4.91	55.8	4.91	1065	924	0.000	56.312	705	532	
8 9.756	3.11	94.6	51.6	4.61	51.6	4.61	745	94	4.62	57.596	701	731	
9 9.457	2.83	74.5	47.2	5.12	47.2	5.12	472	422	916	59.032	699	185	
10 9.158	2.58	14.7	42.6	3.81	42.6	3.81	426	394	975	50.1	60.553	35.523	
11 8.859	7.63	24.7	36.2	2.39	36.2	2.39	324	239	132	2.255	62.54	691	858

***** R C T C R E X I T O U T P U T D A T A *****

RADIUS STA NO. (IN)	WHEEL SPEED (FT/SEC.)	TANGENT. VEL. (FT/SEC.)	ABS. VEL. (FT/SEC.)	REL. VEL. (FT/SEC.)	AIR ANG. (DEG.)	REL. AIR ANG. (DEG.)	TOTAL PRESS. (PSI)		REFL. MACH NO.	ABS. MACH NO.	LOSS FUNC		
							AIR ANG. (DEG.)	TEMP. (DEG R)					
1 11.947	9.07	24.2	106	4.7	106	4.7	967	634	1046	1.198	21.089	39.675	
2 11.546	6.62	34.3	75.5	6.52	75.5	6.52	932	996	329	23.187	39.782	781	378
3 11.248	5.27	44.3	72.4	7.28	72.4	7.28	435	51.9	94.6	10.197	24.842	49.945	0.303
4 10.954	4.12	54.4	58.3	5.36	58.3	5.36	247	44.1	76.5	52.4	26.675	77.1	179
5 10.652	3.87	57.4	54.2	2.35	54.2	2.35	351	74.7	73.2	23.4	94.612	76.6	613
6 10.353	3.62	74.5	60.1	6.25	60.1	6.25	350	40.5	76.0	4.710	40.495	47.208	0.337
7 10.054	3.37	94.5	55.8	4.91	55.8	4.91	755	625	96.9	9.930	30.974	76.2	301
8 9.756	3.11	94.6	51.6	4.61	51.6	4.61	372	2.54	64.3	3.317	41.850	75.0	443
9 9.457	2.83	74.5	47.2	5.12	47.2	5.12	386	41.8	64.2	6.611	39.932	75.0	897
10 9.158	2.58	14.7	42.6	3.81	42.6	3.81	400	1.51	59.5	6.611	43.533	43.819	0.466
11 8.859	7.63	24.7	36.2	2.39	36.2	2.39	411	451	525	2.355	42.959	744	571

***** S T A T O R F X I T C U T P U T D A T A *****

RADIUS STA NO. (IN)	WHEEL SPEED (FT/SEC.)	TANGENT. VEL. (FT/SEC.)	ABS. VEL. (FT/SEC.)	REL. VEL. (FT/SEC.)	AIR ANG. (DEG.)	REL. AIR ANG. (DEG.)	TOTAL PRESS. (PSI)		REFL. MACH NO.	ABS. MACH NO.	LOSS FUNC		
							AIR ANG. (DEG.)	TEMP. (DEG R)					
1 11.947	9.07	24.2	106	4.7	106	4.7	967	634	1046	1.198	21.089	39.675	
2 11.546	6.62	34.3	75.5	6.52	75.5	6.52	932	996	329	23.187	39.782	781	378
3 11.248	5.27	44.3	72.4	7.28	72.4	7.28	435	51.9	94.6	10.197	24.842	49.945	0.303
4 10.954	4.12	54.4	58.3	5.36	58.3	5.36	247	44.1	76.5	52.4	26.675	77.1	179
5 10.652	3.87	57.4	54.2	2.35	54.2	2.35	351	74.7	73.2	23.4	94.612	76.6	613
6 10.353	3.62	74.5	60.1	6.25	60.1	6.25	350	40.5	76.0	4.710	40.495	47.208	0.337
7 10.054	3.37	94.5	55.8	4.91	55.8	4.91	755	625	96.9	9.930	30.974	75.0	443
8 9.756	3.11	94.6	51.6	4.61	51.6	4.61	372	2.54	64.3	3.317	41.850	75.0	897
9 9.457	2.83	74.5	47.2	5.12	47.2	5.12	386	41.8	64.2	6.611	39.932	44.393	0.466
10 9.158	2.58	14.7	42.6	3.81	42.6	3.81	400	1.51	59.5	6.611	43.533	43.819	0.466
11 8.859	7.63	24.7	36.2	2.39	36.2	2.39	411	451	525	2.355	42.959	744	571

*** STATE OR HURD FACTORY LIMIT VIOLATED ***

***** STAGE DATA *****

STAGE NO., 6

*** ROTOR INPUT DATA ***

AXIAL VFL. RATIO	POLYTOPIC EFFICIENCY	SOLIDITY AT TIP	ASPECT RATIO	TIP BLOCKAGE FACTOR	HUB BLOCKAGE FACTOR	MAX ANGLE HUB TAPER (DEGREES)	MAX ANGLE TIP TAPER (DEGREES)
1.0100	0.3750	1.0000	2.5000	1.0000	1.0000	40.000	-20.000
MAX. ROTOR ANGLE. FACTOR	AIR REL. FLW ANGLE. 3-G RAD. (DEGREES)						
0.4500	-1.0000						

Coefficients in Tangential Velocity Equation

B	C	D	E
0.0000	0.0000	0.0000	0.0000

*** STATOR INPUT DATA ***

AXIAL VELOCITY RATIO	TOTAL POLYTOPIC EFFICIENCY	SOLIDITY AT TIP	ASPECT RATIO	TIP BLOCKAGE FACTOR	HUB BLOCKAGE FACTOR	MAX ANGLE HUB TAPER (DEGREES)	MAX ANGLE TIP TAPER (DEGREES)
1.0000	0.3750	1.0000	2.5000	1.0000	1.0000	40.000	-20.0000
MAX. STATOR DIF. FACTOR	MAX. RAD. TIP/T RAD. NUMBER						
0.5000	0.0000						

Coefficients in Tangential Velocity Equation

P	C	D	E
0.0000	0.0000	0.0000	0.0000

***** STAG FLOW INPUT DATA *****

OVERALL MASS AVG. PR. RATIO	OVERALL MASS AVE. TEP. RATIO	OVERALL MASS AVE. EFFICIENCY	MASS AVE. PRESSURE RATIO	MASS AVE. TEMPERATURE RATIO	MASS AVE. EFFICIENCY	POT. PR. ASPECT RATIO	STATOR ASPECT RATIO
3.017t	1.05825	0.91927	1.02247	1.05717	0.9455	2.5000	2.5000
ROTOR TIP RAD. 1-G (INCHES)	ROTOR HUB RAD. 1-G (INCHES)	ROTOR HUB RAD. 2-G (INCHES)	ROTOR TIP RAD. 3-G (INCHES)	STATOR HUB RAD. 3-G (INCHES)	ROTOR PROJ. LENGTH (INCHES)	STATOR PROJ. LENGTH (INCHES)	STATOR PROJ. LENGTH (INCHES)
11.2469	3.0226	1.08464	3.05254	11.8469	5.6951	1.6097	0.8886
ROTOR TIP RAD. 2-G (INCHES)	ROTOR HUB RAD. 2-G (INCHES)	ROTOR HUB RAD. 3-G (INCHES)	STATOR TIP RAD. 3-G (INCHES)	STATOR HUB RAD. 3-G (INCHES)	STATOR TIP RAD. 3-G (INCHES)	STATOR HUB RAD. 3-G (INCHES)	STATOR HUB RAD. 3-G (INCHES)
10.0000	10.0000	10.0000	10.0000	10.0000	10.0000	10.0000	10.0000

***** RADIATOR INLET OUTPUT DATA *****

RA DIUS STA NO.	RH FEL. SPEED (FT/SEC)	AXIAL VEL. (FT/SEC)	TANGENT. VEL. (FT/SEC)	AHS. (FT/SEC)	REFL. VEL. (FT/SEC)	AIR ANG. (DEG)	REL. TEMP. (DEG R)	TOTAL PRESS. (PSI)	TOTAL MACH NO.	LOSS COEFF
1 11.647	667.242	54.440	1.050	3.024	1.274.727	3.000	50.757	786.410	50.412	0.587
2 11.554	616.235	751.052	1.232.722	0.000	51.606	781.078	49.598	7.900	0.559	0.072
3 11.442	645.175	722.728	1.191.940	0.000	52.520	774.001	48.645	0.873	0.531	0.076
4 11.345	624.134	587.652	1.030	5.05	1.149.490	0.000	53.500	771.179	0.845	0.502
5 11.247	613.098	642.215	1.010	2.015	1.119.215	1.000	54.592	756.613	46.915	0.473
6 11.156	602.055	641.625	1.000	3.015	1.057.088	0.000	55.752	752.304	46.136	0.446
7 11.052	591.025	584.450	0.950	4.015	1.024.294	0.000	57.931	753.245	45.407	0.414
8 10.950	586.569	515.329	0.900	5.015	0.945.814	0.000	58.438	754.443	44.734	0.383
9 10.847	575.514	475.214	0.850	6.010	476.912	0.000	59.925	750.897	44.111	0.352
10 10.746	567.313	465.189	0.800	5.015	426.332	0.500	61.731	747.606	43.538	0.320
11 10.643	557.232	432.250	0.750	6.010	384.230	0.000	62.693	744.571	43.014	0.117
										0.648
										0.297
										0.126

***** ROTON EXIT OUTPUT DATA *****

RA DIUS STA NO.	RH FEL. SPEED (FT/SEC)	AXIAL VEL. (FT/SEC)	TANGENT. VEL. (FT/SEC)	AHS. (FT/SEC)	REFL. VEL. (FT/SEC)	AIR ANG. (DEG)	REL. TEMP. (DEG R)	TOTAL PRESS. (PSI)	TOTAL MACH NO.	LOSS FUNC
1 11.847	687.242	416.401	3.340.242	276.912	1.037.666	2.000	841.339	62.237	0.237	0.639
2 11.625	659.739	765.652	24.0	54.9	437.088	39.0	315	835.006	61.073	0.303
3 11.403	650.215	126.728	1.47.224	0.3.513	942.770	25.500	761	836.929	50.979	0.215
4 11.180	621.706	0.83	354.423	760.874	894.933	27.385	40.195	826.107	56.051	0.330
5 10.959	613.193	642.215	561.3.1	746.871	845.773	29.361	40.574	921.541	57.989	0.348
6 10.736	594.681	501.536	345.2.7	709.261	21.553	41.209	817.229	57.367	0.595	0.023
7 10.514	587.153	568.491	376.5.9	572.585	760.341	23.933	41.814	812.173	56.253	0.393
8 10.292	357.557	515.592	542.6.67	443.513	500.955	36.705	42.559	809.372	55.476	0.413
9 10.070	502.314	472.512	592.1.16	515.011	650.026	39.740	41.320	805.925	54.758	0.440
10 9.849	522.532	423.018	412.3.3	598.011	590.432	43.137	44.290	802.534	54.056	0.431
11 9.628	802.123	352.230	411.3.2	548.048	460.950	45.484	46.429	790.499	53.491	0.402
										0.413
										0.027

***** STATOR EXIT OUTPUT DATA *****

RA DIUS STA NO.	RH FEL. SPEED (FT/SEC)	AXIAL VEL. (FT/SEC)	TANGENT. VEL. (FT/SEC)	AHS. (FT/SEC)	REFL. VEL. (FT/SEC)	AIR ANG. (DEG)	APS. (DEG)	AIR ANG. (DEG)	LOSS COEFF	STATOR AXIAL DIF. FACTOR	LOSS MACH NO.	LOSS FUNC
1 11.847	687.242	416.401	3.340.242	276.912	1.037.666	2.000	30.000	30.000	0.025	0.134	0.587	0.009
2 11.625	659.739	765.652	24.0	54.9	437.088	39.0	315	30.000	0.025	0.226	0.557	0.009
3 11.403	650.215	126.728	1.47.224	0.3.513	942.770	25.500	39.000	39.000	0.029	0.245	0.497	0.008
4 11.180	621.706	0.83	354.423	760.874	894.933	27.385	40.195	40.195	0.031	0.034	0.268	0.009
5 10.959	613.193	642.215	561.3.1	746.871	845.773	29.361	40.574	40.574	0.034	0.467	0.467	0.010
6 10.736	594.681	501.536	345.2.7	709.261	21.553	41.209	817.229	817.229	0.037	0.293	0.437	0.010
7 10.514	587.153	568.491	376.5.9	572.585	760.341	23.933	41.814	41.814	0.040	0.323	0.406	0.011
8 10.292	357.557	515.592	542.6.67	443.513	500.955	36.705	42.559	42.559	0.043	0.433	0.375	0.012
9 10.070	502.314	472.512	592.1.16	515.011	650.026	39.740	41.320	41.320	0.047	0.398	0.344	0.012
10 9.849	522.532	423.018	412.3.3	598.011	590.432	43.137	44.290	44.290	0.051	0.445	0.312	0.013
11 9.628	802.123	352.230	411.3.2	548.048	460.950	45.484	46.429	46.429	0.056	0.500	0.280	0.014

*** STARTED HIGH Q FACTOR LIMIT VIOLATED ***

***** 5 T A C E D A T A *****

STAGE No. 7

* * * DATOR INPUT DATA * * *

COEFFICIENTS IN TANGENTIAL VELOCITY EQUATION					
Axial Vel. Ratio	Polynomial Efficiency at Tip	Solidity at Tip	Aspect Ratio	Tip Blockage Factor	HUB BLOCKAGE FACTOR
1.000	0.975	1.035	2.050	1.000	1.000
MAX ROTOR DIFF. FACTOR	MAX REL. FING. ANGLE (DEGREES)	MAX REL. FING. ANGLE (DEGREES)	ASPECT RATIO	TIP BLOCKAGE FACTOR	HUB BLOCKAGE FACTOR
1.045	-1.000	-1.000	0.000	0.000	0.000
MAX ANGLE TIP TAPER (DEGREES)	MAX ANGLE HUB TAPER (DEGREES)	MAX ANGLE HUB TAPER (DEGREES)	MAX ANGLE TIP TAPER (DEGREES)	MAX ANGLE HUB TAPER (DEGREES)	MAX ANGLE TIP TAPER (DEGREES)
-26.000	-26.000	-26.000	-26.000	-26.000	-26.000

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AXIAL FLUX DENSITY PATTERN	TOTAL SCALINITY AT HIGH	ASPECT RATIO	TIP BLOCKAGE FACTOR	HUB BLOCKAGE FACTOR	MAX ANGLE HUB TAPER (DEGREES)	MAX ANGLE TIP TAPER (DEGREES)
UNI-L -FF-F-F-F-C	0.547 ± 0.010	1.0	0.547 ± 0.010	0.547 ± 0.010	± 1.0	± 1.0

COEFFICIENTS IN TANGENTIAL VELOCITY EQUATION

MAX. STATOR DIFF. FACTUR	MAX. HUB DIFF.
$A_{ACF} - \frac{1}{4} A_{HCF}$	$\frac{1}{4} A_{HCF}$

RADIUS -E (IN.)	STA. (FT)	VFL. (FT/SEC.)	AXIAL VEL. (FT/SEC.)	TANGENT. VEL. (FT/SEC.)	A.S. (FT/SEC.)	REL. VEL. (FT/SEC.)	ABS. AIR ANG. (DEG.)	REL. AIR ANG. (DEG.)	TOTAL		LOSS COEFF.	
									TEMP. (DEG R)	PRESS. (PSI)		
1	11.647	2.67	2.242	0.64	3.64	1.274	727	0.00	757	841.339	0.369	
2	11.632	5.94	3.14	1.65	7.55	7.55	227	0.00	51.695	836.056	0.373	
3	11.417	5.61	3.779	7.22	7.22	7.24	728	119.5	973	52.701	0.376	
4	11.241	9.43	4.67	5.82	5.66	5.82	5.96	115.6	931	53.783	0.380	
5	11.086	9.15	5.16	5.42	2.15	5.42	2.15	111.8	357	821.541	0.385	
6	11.771	9.67	5.44	5.46	5.35	107.3	954	0.00	56.215	817.229	0.090	
7	11.566	12.7	6.55	4.49	10.0	10.0	491	104.1	970	57.589	813.173	0.095
8	11.442	8.41	7.24	5.16	5.16	5.16	3.91	101.4	3.95	59.387	809.372	0.101
9	11.126	8.23	7.75	5.12	5.12	5.12	2.78	97.6	731	805.825	0.420	
10	9.919	8.25	8.35	4.29	4.29	4.29	3.12	92.0	673	802.534	0.762	
11	9.555	8.77	8.27	3.84	3.84	3.84	2.39	92.0	673	64.565	799.499	0.114

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STA. NO.	RADIUS -F (FT.)	WHEEL SPEED (FT./SEC.)	AXIAL VEL. (FT./SEC.)	TANGENT. VEL. (FT./SEC.)	APC. (FT./SEC.)	PEL. VEL. (FT./SEC.)	ABS. AIR ANG. (DEG.)	REL. AIR ANG. (DEG.)	TOTAL		ROT.R. PRESS. (PSI)	REL. MACH NO.	LOSS FUNC.
									TEMP. (DEG R.)	PRESS. (PSI)			
1	11.847	557.242	356.411	245.154	877.135	1,031.942	23.169	38.531	898.057	76.553	0.295	0.729	0.620
2	11.455	571.345	765.552	320.742	842.165	925.582	26.212	39.027	892.725	74.229	0.309	0.697	0.595
3	11.465	555.451	724.728	355.575	897.679	940.149	24.193	39.568	887.648	72.983	0.323	0.665	0.571
4	11.275	537.555	683.595	352.365	773.824	994.522	27.943	40.164	882.826	71.912	0.339	0.633	0.547
5	11.084	523.355	642.216	359.343	746.632	949.679	29.370	40.824	878.259	70.715	0.357	0.606	0.524
6	10.933	607.755	656.636	375.304	750.167	802.591	32.004	41.561	873.948	69.689	0.376	0.568	0.501
7	10.712	691.356	559.451	391.067	774.345	755.228	42.271	42.394	870.891	68.733	0.397	0.535	0.479
8	10.512	675.373	516.924	338.902	764.152	790.544	37.000	43.367	866.650	67.845	0.420	0.502	0.457
9	10.321	663.077	472.612	286.117	717.462	826.499	39.955	44.453	862.544	67.024	0.445	0.469	0.437
10	10.140	644.234	425.024	405.575	585.553	615.515	43.246	45.755	859.252	66.267	0.474	0.436	0.417
11	9.935	629.436	396.235	412.341	570.372	567.050	46.956	47.339	856.217	65.575	0.506	0.402	0.399

* * * STATEMENT OF FACTS WHICH WERE VIOLATED * * *

***** STAGE DATA *****

STAGE NO. 8

*** ROTOR INPUT DATA ***

AXIAL VEL. RATIO	TOTAL POLYTROPIC EFFICIENCY	SOLIDITY AT TIP	TIP BLOCKAGE FACTOR	HUB BLOCKAGE FACTOR	MAX ANGLE HUB TAPER (DEGREES)
1.0	0.3750	1.0000	2.0000	1.0000	-20.000
MAX ROTOR AXIAL DIF. FACTOR	AUXILIARY ROT. DIF. FACTOR (DEGREES)				
1.0450	-1.0000				

MAX. STATOR DIF. FACTOR	MAX. HUB INLET MACH NUMBER	TOTAL POLYTROPIC EFFICIENCY	SOLIDITY AT HUB	TIP BLOCKAGE FACTOR	HUB BLOCKAGE FACTOR	MAX ANGLE HUB TAPER (DEGREES)
1.0000	0.3500	1.0000	2.0000	1.0000	1.0000	-20.0000
MAX. STATOR DIF. FACTOR	MAX. HUB INLET MACH NUMBER					
0.5000	0.3000					

*** STATOR INPUT DATA ***

AXIAL VELOCITY RATIO	TOTAL POLYTROPIC EFFICIENCY	SOLIDITY AT HUB	TIP BLOCKAGE FACTOR	HUB BLOCKAGE FACTOR	MAX ANGLE HUB TAPER (DEGREES)
1.0000	0.3500	1.0000	2.0000	1.0000	-20.0000
MAX. STATOR DIF. FACTOR	MAX. HUB INLET MACH NUMBER				
0.5000	0.3000				

*** COEFFICIENTS IN TANGENTIAL VELOCITY EQUATION ***

MAX. STATOR DIF. FACTOR	COEFFICIENTS IN TANGENTIAL VELOCITY EQUATION
E-51	B C D E F G
0.5000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000

***** STAGE OUTPUT DATA *****

OVERALL MASS AVF. PR. RATIO	OVERALL MASS AVF. TE42. RATIO	OVERALL MASS AVF. EFFICIENCY	MASS AVE. PRESSURE RATIO	MASS AVE. TEMPERATURE RATIO	MASS AVE. TEMPERATURE RATIO	ROTOR PROJ. LENGTH (INCHES)	STATOR PROJ. LENGTH (INCHES)	STATOR PROJ. LENGTH (INCHES)
5.7805	1.0000	0.3100	1.0200	1.0663	0.8450	2.5000	2.5000	2.5000
ROTOR TIP RAD. 1-6 (INCHES)	ROT. RAD. 1-6 (INCHES)	ROT. RAD. 2-6 (INCHES)	ROT. RAD. 2-6 (INCHES)	ROT. RAD. 3-6 (INCHES)	STATOR TIP RAD. 3-6 (INCHES)	ROT. RAD. 3-G (INCHES)	STATOR HUB RAD. 3-G (INCHES)	STATOR HUB RAD. 3-G (INCHES)
11.2469	2.0369	2.0369	1.01955	1.01955	11.8469	10.2429	0.7401	0.6605
ROT. TIP DAMP ANGLE (DEGREES)	ROT. HUB RAMP ANGLE (DEGREES)	STATOR TIP RAMP ANGLE (DEGREES)	STATOR HUB RAMP ANGLE (DEGREES)					
E-51	15.0365	15.0365	4.1014	4.1014	0.0000	0.0000	0.0000	0.0000

***** TURBINE INLET OUTPUT DATA *****

RADIUS STA NO.	WHEEL SPEED (IN)	AXIAL TANGENT. VEL. (FT/SEC)			A.P.S. VEL. (FT/SEC)			REL. VEL. (DEG)			TOTAL PRESS. (PSI)			ABS. MACH NO.	LOSS COEF.
		(FT/SEC)	(FT/SEC)	(FT/SEC)	(FT/SEC)	(FT/SEC)	(FT/SEC)	(DEG)	(DEG)	(DEG)	(DEG)	(DEG)	(DEG)		
1 11.347	587.024	464.424	30.374	1274.727	0.00J	50.757	898.657	75.123	0.868	0.549	0.079	0.079	0.079	0.079	
2 11.562	775.824	751.067	745.532	1237.290	0.00J	51.767	892.725	73.964	0.845	0.523	0.075	0.075	0.075	0.075	
3 11.477	667.464	724.723	724.733	1196.374	0.00J	52.447	987.648	72.562	0.822	0.497	0.077	0.077	0.077	0.077	
4 11.262	312.534	533.676	184.565	1164.192	0.00J	54.053	982.826	71.396	0.799	0.470	0.081	0.081	0.081	0.081	
5 11.157	612.532	642.216	442.216	1126.552	0.00J	55.245	978.259	70.303	0.776	0.442	0.081	0.081	0.081	0.081	
6 11.352	611.151	600.536	500.536	1136.422	0.00J	56.582	973.948	69.291	0.753	0.415	0.081	0.081	0.081	0.081	
7 10.737	611.743	550.641	550.641	1054.732	0.00J	58.028	869.891	68.329	0.386	0.096	0.096	0.096	0.096	0.096	
8 10.652	277.346	516.357	215.061	1110.533	0.00J	59.595	866.096	67.444	0.707	0.358	0.110	0.110	0.110	0.110	
9 10.357	611.837	472.012	472.012	984.367	0.00J	61.303	952.544	66.526	0.684	0.329	0.103	0.103	0.103	0.103	
10 10.142	542.476	426.081	426.081	925.046	0.00J	63.174	955.253	65.973	0.662	0.299	0.112	0.112	0.112	0.112	
11 9.957	321.155	584.246	164.024	717.403	0.00J	65.239	856.217	65.183	0.640	0.268	0.113	0.113	0.113	0.113	

***** EXIT OUTPUT DATA *****

RADIUS STA NO.	WHEEL SPEED (IN)	AXIAL TANGENT. VEL. (FT/SEC)			A.P.S. VEL. (FT/SEC)			REL. VEL. (DEG)			TOTAL PRESS. (PSI)			ABS. MACH NO.	LOSS COEF.
		(FT/SEC)	(FT/SEC)	(FT/SEC)	(FT/SEC)	(FT/SEC)	(FT/SEC)	(DEG)	(DEG)	(DEG)	(DEG)	(DEG)	(DEG)		
1 11.347	587.024	806.423	253.978	1025.334	23.71	23.70	39.142	956.235	91.346	0.302	0.701	0.602	0.602	0.602	0.602
2 11.692	971.431	765.452	252.982	345.424	491.740	25.424	38.750	950.703	80.547	0.316	0.671	0.578	0.578	0.578	0.578
3 11.517	553.713	724.723	354.122	411.051	229.056	25.677	39.414	945.826	80.124	0.330	0.641	0.555	0.555	0.555	0.555
4 11.351	615.354	592.564	352.126	352.235	494.235	29.281	40.144	941.004	86.807	0.346	0.612	0.531	0.531	0.531	0.531
5 11.184	932.195	542.195	374.982	742.574	45.710	30.272	40.952	936.438	85.562	0.353	0.582	0.509	0.509	0.509	0.509
6 11.321	613.435	613.435	231.042	717.935	80.623	32.358	41.853	932.126	84.398	0.382	0.552	0.486	0.486	0.486	0.486
7 10.856	512.273	651.534	347.295	579.574	761.397	36.670	42.867	924.076	83.412	0.433	0.521	0.465	0.465	0.465	0.465
8 10.591	486.614	515.531	352.252	442.157	717.571	37.242	44.521	924.258	92.303	0.425	0.491	0.444	0.444	0.444	0.444
9 10.526	577.453	472.012	350.446	459.343	672.935	40.0113	45.351	920.722	81.360	0.449	0.461	0.423	0.423	0.423	0.423
10 10.361	613.339	426.081	426.081	523.454	63.325	46.907	91.7.431	80.509	0.476	0.430	0.404	0.404	0.404	0.404	0.404
11 10.156	843.627	394.736	411.312	352.085	592.091	45.949	46.751	914.395	70.722	0.506	0.399	0.386	0.386	0.386	0.386

***** STATION 0 EXIT OUTPUT DATA *****

RADIUS STA NO.	WHEEL SPEED (IN)	AXIAL TANGENT. VEL. (FT/SEC)			A.P.S. VEL. (FT/SEC)			REL. VEL. (DEG)			TOTAL PRESS. (PSI)			ABS. MACH NO.	LOSS COEF.
		(FT/SEC)	(FT/SEC)	(FT/SEC)	(FT/SEC)	(FT/SEC)	(FT/SEC)	(DEG)	(DEG)	(DEG)	(DEG)	(DEG)	(DEG)		
1 11.947	936.413	501.17	3.574	501.17	0.00J	0.00J	0.00J	0.00J	0.00J	0.00J	0.00J	0.00J	0.201	0.548	0.017
2 11.647	745.652	501.17	745.652	501.17	0.00J	0.00J	0.00J	0.00J	0.00J	0.00J	0.00J	0.00J	0.216	0.520	0.018
3 11.526	724.722	501.17	724.722	501.17	0.00J	0.00J	0.00J	0.00J	0.00J	0.00J	0.00J	0.00J	0.233	0.493	0.011
4 11.356	633.565	501.17	432.532	501.17	0.00J	0.00J	0.00J	0.00J	0.00J	0.00J	0.00J	0.00J	0.252	0.465	0.009
5 11.205	542.215	501.17	442.215	501.17	0.00J	0.00J	0.00J	0.00J	0.00J	0.00J	0.00J	0.00J	0.274	0.436	0.009
6 11.145	616.574	501.17	501.17	501.17	0.00J	0.00J	0.00J	0.00J	0.00J	0.00J	0.00J	0.00J	0.309	0.408	0.010
7 10.884	508.461	501.17	508.461	501.17	0.00J	0.00J	0.00J	0.00J	0.00J	0.00J	0.00J	0.00J	0.329	0.380	0.011
8 10.724	515.961	501.17	515.961	501.17	0.00J	0.00J	0.00J	0.00J	0.00J	0.00J	0.00J	0.00J	0.362	0.354	0.012
9 10.564	472.012	501.17	472.012	501.17	0.00J	0.00J	0.00J	0.00J	0.00J	0.00J	0.00J	0.00J	0.321	0.321	0.013
10 10.412	420.081	501.17	420.081	501.17	0.00J	0.00J	0.00J	0.00J	0.00J	0.00J	0.00J	0.00J	0.292	0.292	0.014
11 10.243	394.245	501.17	394.245	501.17	0.00J	0.00J	0.00J	0.00J	0.00J	0.00J	0.00J	0.00J	0.261	0.261	0.015

*** STABIL. MTF D FACTOR LIMIT VIOLATED ***

***** STAGE DATA *****

STAGE NO. 0

*** ROTOR INPUT DATA ***

AXIAL VEL. RATIO	ROTOR TIPIC TIP TAPER	SURFACE AT TIP	TIP BLOCKAGE FACTOR	HUB BLOCKAGE FACTOR	MAX ANGLE HUB TAPER (DEGREES)
1.000	0.375	1.000	1.000	1.000	-20.000
MAX. ROTOR TIP. FACTOR	MAX. SURFACE HUB (DEGREES)				
0.450	-0.100				

*** STATOR INPUT DATA ***

AXIAL VFLRACTY RATIO	ROTOR TIPIC EFFICIENCY	SURFACE AT HUB	AFFECT RATIO	TIP BLOCKAGE FACTOR	HUB BLOCKAGE FACTOR	MAX ANGLE HUB TAPER (DEGREES)
1.000	0.350	2.000	2.000	1.000	1.000	-20.0000
MAX. STATOR DIF. FACTOR	MAX. HUB INLET MACH NUMBER					
0.500	0.800					

***** STAGE OUTPUT DATA *****

OVERALL MASS AVE. PR. RATIO	CURRENT MASS AVE. PR. RATIO	MASS AVE. PRESSURE RATIO	MASS AVE. TEMPERATURE RATIO	ROTOR ASPECT RATIO	STATOR ASPECT RATIO
6.209	1.0178	0.955	1.200	4.0635	6.9460
ROTOR TIP RAD. 1-G (INCHES)	ROTOR HUB RAD. 1-G (INCHES)	ROTOR TIP RAD. 2-G (INCHES)	ROTOR HUB RAD. 2-G (INCHES)	ROTOR PROJ. LENGTH (INCHES)	STATOR PROJ. LENGTH (INCHES)
11.8469	10.7479	11.9469	10.4061	11.8469	10.4456
ROTOR TIP RAMP ANGLE (DEGREES)	ROTOR HUB RAMP ANGLE (DEGREES)	STATOR TIP RAMP ANGLE (DEGREES)	STATOR HUB RAMP ANGLE (DEGREES)	ROTOR PROJ. LENGTH (INCHES)	STATOR PROJ. LENGTH (INCHES)
6.209	14.2758	0.0000	0.0000	0.6416	0.5763
				3.0120	

--*** C F R I N L E T O U T P U T D A T A ***-***-***

STATION NO.	RADIUS -E (IN)	W-HFL (Ft/sec)	W-HFL (Ft/sec)	AXIAL TANGENT. VEL. (FT/SEC)	A.S. VEL. (FT/SEC)	REL. VEL. (FT/SEC)	REL. VEL. (FT/SEC)	AIR ANG. (DEG)	AIR ANG. (DEG)	REL. TEMP. (DEG R)	REL. TEMP. (DEG R)	TOTAL PRESS. (PSI)	TOTAL PRESS. (PSI)	REFL. MACH NO.	REFL. MACH NO.	LOSS COEFF
1	11.447	CF7.242	84.4.4.0	1.000	1.000	1.274.727	0.000	30.757	95.235	90.547	0.841	0.532	6.370			
2	11.447	573.372	765.352	1.000	1.000	1.234.812	0.000	51.820	35.903	89.053	0.820	0.507	0.273			
3	11.525	66.523	724.723	1.000	1.000	1.263.243	0.000	52.925	94.5.826	87.645	0.799	0.481	0.477			
4	11.446	367.142	682.555	1.000	1.000	1.159.687	0.000	54.180	94.1.004	95.324	0.755	0.455	0.381			
5	11.445	433.773	642.015	1.000	1.000	1.143.303	0.000	55.461	93.6.438	95.6.83	0.756	0.429	0.384			
6	11.444	12.444	761.534	1.000	1.000	1.236.997	0.000	56.877	93.2.126	93.923	0.735	0.401	0.389			
7	11.444	367.342	554.447	1.000	1.000	1.055.193	0.000	58.378	92.8.070	82.941	0.714	0.374	0.393			
8	11.444	953.273	515.531	1.000	1.000	1.031.349	0.000	59.949	92.4.268	81.836	0.693	0.346	0.398			
9	11.444	433.303	72.912	1.000	1.000	990.294	0.000	61.755	92.0.722	80.905	0.572	0.318	0.104			
10	11.443	46.064	726.034	1.000	1.000	967.314	0.000	63.000	91.7.431	80.048	0.652	0.289	0.110			
11	11.442	654.574	334.030	1.000	1.000	935.071	0.000	65.765	914.305	79.263	0.632	0.259	0.116			

--*** C F R E X I T O U T P U T D A T A ***-***-***

STATION NO.	RADIUS -E (IN)	W-HFL (Ft/sec)	W-HFL (Ft/sec)	AXIAL TANGENT. VEL. (FT/SEC)	A.S. VEL. (FT/SEC)	REL. VEL. (FT/SEC)	REL. VEL. (FT/SEC)	AIR ANG. (DEG)	AIR ANG. (DEG)	REL. TEMP. (DEG R)	REL. TEMP. (DEG R)	TOTAL PRESS. (PSI)	TOTAL PRESS. (PSI)	ROTATOR DIF. FACTOR	ROTATOR DIF. FACTOR	LOSS FUNC
1	11.447	587.242	80.6.4.0	1.000	1.000	1.020.935	1.000	24.133	37.320	1.015.645	1.08.894	0.308	0.676	0.585	0.021	
2	11.447	575.236	72.5.352	1.000	1.000	84.8.513	0.978.531	25.533	38.522	1.016.283	1.17.205	0.322	0.648	0.562	0.222	
3	11.446	662.721	724.724	1.000	1.000	91.3.345	0.96.390	27.064	35.248	1.05.5.205	1.05.513	0.336	0.620	0.539	0.222	
4	11.445	561.023	585.555	1.000	1.000	77.5.590	0.95.590	28.740	40.130	1.00.0.384	1.04.115	0.352	0.592	0.516	0.223	
5	11.443	433.211	642.215	1.000	1.000	7.5.763	0.95.597	30.5.97	41.6.600	99.6.817	1.02.710	0.359	0.564	0.494	0.223	
6	11.442	527.211	60.7.78	1.000	1.000	71.4.314	0.94.314	32.6.42	42.0.95	99.1.505	1.01.396	0.397	0.536	0.472	0.224	
7	11.442	616.002	656.465	1.000	1.000	53.9.742	0.91.525	34.9.68	43.250	97.7.449	1.00.169	0.417	0.508	0.451	0.224	
8	11.442	513.153	515.191	1.000	1.000	74.6.765	72.4.320	37.4.29	44.5.70	99.2.648	98.5.28	0.429	0.489	0.431	0.225	
9	11.442	891.032	476.5.7	1.000	1.000	61.9.535	60.1.600	40.6.241	46.5.72	98.6.102	97.9.72	0.452	0.452	0.411	0.225	
10	11.441	179.455	+29.0.81	1.000	1.000	53.6.532	53.6.991	43.3.95	47.917	97.6.811	96.599	0.478	0.424	0.391	0.225	
11	11.440	667.173	384.230	1.000	1.000	54.7.455	54.7.205	42.9.49	49.374	97.3.775	96.106	0.535	0.395	0.373	0.225	

--*** S T A T O R F X I T O U T P U T D A T A ***-***-***

STATION NO.	RADIUS -E (IN)	W-HFL (Ft/sec)	W-HFL (Ft/sec)	AXIAL TANGENT. VEL. (FT/SEC)	A.S. VEL. (FT/SEC)	REL. VEL. (FT/SEC)	REL. VEL. (FT/SEC)	AIR ANG. (DEG)	AIR ANG. (DEG)	LOSS COEFF	LOSS COEFF	STATOR AXIAL DIF. FACTOR	STATOR AXIAL DIF. FACTOR	LOSS FUNC
1	11.447	11.847	765.452	1.000	1.000	7.5.5.252	7.4.7.24	1.000	1.000	0.035	0.035	0.204	0.531	0.007
2	11.447	714.717	315.321	1.000	1.000	7.4.7.724	7.4.7.724	1.000	1.000	0.027	0.027	0.219	0.504	0.008
3	11.447	311.567	414.555	1.000	1.000	5.5.5.595	5.5.5.595	1.000	1.000	0.030	0.030	0.236	0.477	0.008
4	11.447	411.427	411.427	1.000	1.000	5.4.2.215	5.4.2.215	1.000	1.000	0.032	0.032	0.255	0.450	0.009
5	11.446	211.286	211.286	1.000	1.000	5.4.2.215	5.4.2.215	1.000	1.000	0.035	0.035	0.277	0.423	0.009
6	11.445	11.145	558.461	1.000	1.000	5.5.5.595	5.5.5.595	1.000	1.000	0.038	0.038	0.302	0.395	0.010
7	11.445	515.454	515.454	1.000	1.000	5.5.5.595	5.5.5.595	1.000	1.000	0.042	0.042	0.331	0.368	0.011
8	11.445	10.956	315.321	1.000	1.000	5.15.5.991	5.15.5.991	1.000	1.000	0.045	0.045	0.340	0.340	0.012
9	11.445	10.736	472.611	1.000	1.000	5.72.5.12	5.72.5.12	1.000	1.000	0.050	0.050	0.403	0.311	0.013
10	11.445	10.596	764.071	1.000	1.000	4.76.5.87	4.76.5.87	1.000	1.000	0.055	0.047	0.282	0.282	0.014
11	11.445	1.445	384.230	1.000	1.000	4.94.6.15	4.94.6.15	1.000	1.000	0.060	0.060	0.500	0.253	0.015

*** STATEMENT HERE IF FACTORY LIMIT VIOLATED ***

* * * * * STAGE DATA *

STAGE NO. 10

*** ROTOR INPUT DATA ***

AXIAL VEL. RATIO	POLYTRONIC EFFICIENCY AT TIP	SLIDILITY AT TIP	HUB BLOCKAGE FACTOR	MAX ANGLE HUB TAPER (DEGREES)	MAX ANGLE TIP TAPER (DEGREES)
1.000	0.3769	1.5000	1.0000	40.000	-20.000
MAX ROTOR DIF. FACTOR	AIR REL. FLOW ANGLE ROTOR (DEGREES)				
1.000	0.4500	1.0000			

COEFFICIENTS IN TANGENTIAL VELOCITY EQUATION

R	C	D	E
0.0000	0.0000	0.0000	0.0000

*** STATOR INPUT DATA ***

AXIAL POLYTRONIC EFFICIENCY	SLIDILITY AT HUB	HUB BLOCKAGE FACTOR	MAX ANGLE HUB TAPER (DEGREES)	MAX ANGLE TIP TAPER (DEGREES)
1.000	0.9500	2.0000	1.0000	40.000
MAX. STATOR DIF. FACTOR	MAX HUB INLET MACH NUMBER			
0.5000	0.9300			

***** STAGE OUTPUT DATA *****

MASS FLOW (LB/SEC) = 134.443

OVERALL MASS AVE. PR. RATIO	OVERALL MASS AVE. TEMP. RATIO	MASS AVE. PRESSURE RATIO	MASS AVF.	EFFICIENCY	ROTOR ASPECT RATIO	STATOR ASPECT RATIO
8.2676	2.0341	0.4013	1.1915	1.0607	0.8462	2.5000
ROTOR TIP RAD. 1-G (INCHES)	ROTOR HUB RAD. 2-G (INCHES)	ROTOR TIP RAD. 2-G (INCHES)	ROTOR HUB RAD. 3-G (INCHES)	STATOR TIP RAD. 3-G (INCHES)	ROTOR HUB RAD. 2-G (INCHES)	ROTOR PROJ. LENGTH (INCHES)
11.3449	11.4456	11.3466	11.5809	11.8469	10.6138	0.5064
ROTOR TIP RAMP ANGLE (DEGREES)	ROTOR HUB RAMP ANGLE (DEGREES)	STATOR TIP RAMP ANGLE (DEGREES)	STATOR HUB RAMP ANGLE (DEGREES)	STATOR PROJ. LENGTH (INCHES)	STATOR HUB RAMP ANGLE (DEGREES)	STATOR PROJ. LENGTH (INCHES)
0.1000	13.5651	0.0000	3.07305	3.07305	0.0000	0.0000

***** ROTATING INLET OUTPUT DATA *****

STATION NO.	RADIUS -E (IN)	VELOC. (FT/SEC)	TANGENT. VEL. (FT/SEC)	AHS. (FT/SEC)	REL. VFL. (FT/SEC)	AHS. AIR ANG. (DEG)	REL. AIR ANG. (DEG)	TOTAL TEMP. (DEG R)	TOTAL PRESS. (PSI)	REL. MACH NO.	AHS. MACH NO.	LOSS COEFF
1	11.847	667.647	667.647	667.647	667.647	0.000	0.000	1274.727	50.757	1015.615	108.321	0.516
2	11.707	575.024	575.024	575.024	575.024	1.45	0.610	51.974	1010.283	106.638	0.796	0.492
3	11.567	664.945	664.945	664.945	664.945	0.000	0.000	1205.947	52.051	1005.205	105.052	0.776
4	11.427	562.242	562.242	562.242	562.242	5.96	0.610	1172.179	54.325	1090.384	103.559	0.755
5	11.287	647.215	647.215	647.215	647.215	1.139	0.000	1139.875	55.674	995.617	102.159	0.441
6	11.146	522.552	522.552	522.552	522.552	0.000	0.000	1106.879	57.416	931.505	110.849	0.415
7	11.006	617.475	617.475	617.475	617.475	0.000	0.000	1073.835	58.662	97.449	10.627	0.598
8	10.864	615.437	615.437	615.437	615.437	0.000	0.000	1042.135	50.324	93.648	9.450	0.363
9	10.724	553.413	553.413	553.413	553.413	4.72	0.000	1011.216	52.117	98.012	10.437	0.336
10	10.586	692.441	692.441	692.441	692.441	2.56	0.000	1080.956	64.051	975.911	96.467	0.102
11	10.446	971.432	971.432	971.432	971.432	0.000	0.000	1046.239	551.437	56.192	56.192	0.280
									973.175	95.578	95.578	0.114

***** RETRO EXIT OUTPUT DATA *****

STATION NO.	RADIUS -E (IN)	VELOC. (FT/SEC)	TANGENT. VEL. (FT/SEC)	AHS. (FT/SEC)	REL. VFL. (FT/SEC)	AHS. AIR ANG. (DEG)	REL. AIR ANG. (DEG)	TOTAL TEMP. (DEG R)	TOTAL PRESS. (PSI)	RET. MACH NO.	AHS. MACH NO.	LOSS FUNC
1	11.847	697.242	697.242	697.242	697.242	0.000	0.000	1117.131	24.491	37.556	129.276	0.653
2	11.706	575.591	575.591	575.591	575.591	0.000	0.000	975.367	25.972	39.332	107.558	0.326
3	11.566	664.141	664.141	664.141	664.141	0.000	0.000	935.040	27.381	39.186	105.581	0.341
4	11.426	562.530	562.530	562.530	562.530	0.000	0.000	893.953	29.038	40.121	106.759	123.917
5	11.346	545.039	545.039	545.039	545.039	0.000	0.000	852.929	30.865	41.153	106.492	122.339
6	11.212	534.424	534.424	534.424	534.424	0.000	0.000	813.915	32.971	42.298	1051.880	120.862
7	11.087	521.534	521.534	521.534	521.534	0.000	0.000	776.925	35.100	43.577	1047.824	119.483
8	10.951	512.367	512.367	512.367	512.367	0.000	0.000	737.958	37.578	45.019	1044.323	118.201
9	10.812	472.823	472.823	472.823	472.823	0.000	0.000	680.055	40.344	46.561	1040.477	117.012
10	10.777	482.235	482.235	482.235	482.235	0.000	0.000	648.197	43.448	48.551	1037.196	115.517
11	10.541	691.735	691.735	691.735	691.735	0.000	0.000	542.955	46.348	50.759	1034.150	114.912

***** START EXIT OUTPUT DATA *****

STATION NO.	RADIUS -E (IN)	VELOC. (FT/SEC)	TANGENT. VEL. (FT/SEC)	AHS. (FT/SEC)	REL. VFL. (FT/SEC)	AHS. AIR ANG. (DEG)	REL. AIR ANG. (DEG)	TOTAL TEMP. (DEG R)	TOTAL PRESS. (PSI)	RET. MACH NO.	AHS. MACH NO.	LOSS FUNC
1	11.847	697.242	697.242	697.242	697.242	0.000	0.000	1117.131	24.491	37.556	129.276	0.559
2	11.706	575.591	575.591	575.591	575.591	0.000	0.000	975.367	25.972	39.332	107.558	0.326
3	11.566	664.141	664.141	664.141	664.141	0.000	0.000	935.040	27.381	39.186	105.581	0.341
4	11.426	562.530	562.530	562.530	562.530	0.000	0.000	893.953	29.038	40.121	106.759	123.917
5	11.346	545.039	545.039	545.039	545.039	0.000	0.000	852.929	30.865	41.153	106.492	122.339
6	11.212	534.424	534.424	534.424	534.424	0.000	0.000	813.915	32.971	42.298	1051.880	120.862
7	11.087	521.534	521.534	521.534	521.534	0.000	0.000	776.925	35.100	43.577	1047.824	119.483
8	10.951	512.367	512.367	512.367	512.367	0.000	0.000	737.958	37.578	45.019	1044.323	118.201
9	10.812	472.823	472.823	472.823	472.823	0.000	0.000	680.055	40.344	46.561	1040.477	117.012
10	10.777	482.235	482.235	482.235	482.235	0.000	0.000	648.197	43.448	48.551	1037.196	115.517
11	10.541	691.735	691.735	691.735	691.735	0.000	0.000	542.955	46.348	50.759	1034.150	114.912