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TECHNICAL MEMORANDUM

X-690

PRESSURE DISTRIBUTIONS ON THE CYLINDRICAL PORTION OF A MISSILE WITH CRUCIFORM WINGS AT TRANSONIC SPEEDS

By Francis J. Capone

Langley Research Center
Langley Station, Hampton, Va.

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NATIONAL AERONAUTICS AND SPACE ADMINISTRATION

TECHNICAL MEMORANDUM X-690

PRESSURE DISTRIBUTIONS ON THE CYLINDRICAL PORTION OF A MISSILE WITH CRUCIFORM WINGS AT TRANSONIC SPEEDS*

By Francis J. Capone

SUMMARY

Pressure distributions have been measured at transonic speeds on the cylindrical portion of a missile with cruciform wings and with and without auxiliary-power exhaust bleed air. The tests were conducted in the Langley 16-foot transonic tunnel at Mach numbers from 0.70 to 1.03, at angles of attack from about -2.1° to 15.3°, and at roll angles of 0°, 45°, and 90°. The test Reynolds number per foot varied from 3.35×10^{6} to 4.05×10^{6}. The results of this investigation are presented as tables and figures of static-pressure error coefficient.

INTRODUCTION

A wind-tunnel investigation has been conducted at transonic speeds to determine the pressure distributions on the cylindrical portion near the midsection of a missile with cruciform wings and with two external longitudinal channels, which housed electrical cables. The body pressures are to be used as a measure of pressure altitude for purposes of missile arming by barometric fusing. The purpose of the investigation was to provide data showing which combination of orifices, when numerically averaged, would give the least error in measuring free-stream static pressure for various combinations of roll attitude and angle of attack.

Body pressures were measured at eight longitudinal stations, each with 14 orifices around the periphery in a plane perpendicular to the missile axis. Auxiliary-power-unit exhaust gases were simulated with a cold-air jet exhausting through a port forward of the orifices.

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Tests were conducted with and without exhaust-gas simulation at Mach numbers from 0.70 to 1.03, at angles of attack from -2.1° to 15.3°, and at roll angles of 0°, 45°, and 90°. The test Reynolds number per foot varied from 3.35×10^6 to 4.05×10^6. Results of tests conducted at supersonic speeds on the same missile with a different exhaust-port location are reported in references 1 and 2.

SYMBOLS

M	free-stream Mach number
p	measured surface static pressure, lb/sq ft
p_∞	free-stream static pressure, lb/sq ft
$\frac{p - p_\infty}{p_\infty}$	static-pressure error coefficient
w	weight flow of auxiliary-power-unit gases, lb/sec
α	angle of attack, referenced to body center line, deg
θ	orifice meridian row, 0° at top of missile, measured with wing 45° from top and exhaust port on bottom of missile, deg
ϕ	angle of roll, measured from top of missile with wing 45° from top and exhaust port on bottom of missile, deg

MODEL

A sketch and a photograph of the model are shown in figures 1 and 2, respectively. The model, a cruciform-winged missile, had a steel inner body covered with wood. The model, with an ogival nose, was 190.76 inches long and had a maximum body diameter of 14.00 inches. Each of the wings had a root chord of 86.40 inches, a tip chord of 12.70 inches, and a leading-edge sweep of 77.24°. There was no sweep to the trailing edge. Four thin metal struts were added to the wings to insure structural integrity of the model. (See fig. 2.) Two external body channels housing electrical cables were attached to the cylindrical portion of the model starting at a point 50.66 inches back from the nose and ending at the rear of the model. These channels were 2.13 inches wide and 0.86 inch thick. (See fig. 1.)

Surface pressures were measured at eight longitudinal station locations, each with 14 orifices around the periphery in a plane perpendicular to the model axis. The orifices of station 1 were located 73.03 inches back from the nose of the model. Distance between orifice stations was 2.63 inches. Each orifice, 0.04 inch in diameter, was countersunk 0.02 inch at an included angle of 82°, with a resulting 0.08-inch-diameter orifice at the surface of the model. A sketch showing orifice details is given in figure 1.

A sketch and photographs of the exhaust port are shown in figures 3 and 4, respectively. The exhaust port for the cold-air jet, which simulated the exhaust products of an auxiliary power unit, was located 70.22 inches back from the nose of the missile and 2.81 inches forward of the first orifice station (fig. 1); peripherally, the center line of the exhaust port was located at $\theta = 102^{\circ}$.

APPARATUS AND PROCEDURES

Wind Tunnel and Instrumentation

The present investigation was conducted in the Langley 16-foot transonic tunnel, which is a single-return atmospheric wind tunnel with a slotted octagonal test section. The speed range of this tunnel is from a Mach number of 0.20 to 1.10, with Mach number being varied over this range by a variation of tunnel drive power. The model support system pivoted in such a manner that the section of the model in which the orifices were located was kept on or near the tunnel center line throughout the angle-of-attack range.

Pressures were individually measured on 100-tube mercury-manometer boards. The boards were photographed and the film was read on a film-reading machine. The weight flow of the bleed air was determined from a calibrated venturi flowmeter. The angle of attack of the model was determined by means of an internally located pendulum-type strain-gage inclinometer.

Tests, Corrections, and Accuracies

The model was tested at Mach numbers from 0.70 to 1.03, at angles of attack from -2.1° to 15.3°, and at roll angles of 0°, 45°, and 90°. A cold-air jet at a weight flow of approximately 0.018 pound per second was used to simulate auxiliary-power exhaust gases.

Some of the data for particular orifices were found to be in error and have been omitted from both the tables and figures; therefore, the

data presented in the figures have not been faired between these data points. No other corrections were made to the data. The accuracies of the static-pressure error coefficient and test conditions have been estimated to be:

$\frac{p - p_\infty}{p_\infty}$	±0.005
M	±0.01
α, deg	±0.2
w, lb/sec	±0.005

L
1
8
8
2

PRESENTATION OF RESULTS

Tables I to VI present the static-pressure error coefficients at $\phi = 0^\circ$, 45°, and 90° for the tests conducted with and without exhaust-gas simulation at Mach numbers from 0.70 to 1.03. The variation of static-pressure error coefficient with longitudinal orifice station for M = 0.70 and M = 1.00 at the various roll angles of this investigation is presented in figures 5 to 10. An outline of the content of the data tables and figures is as follows:

	Table
Static-pressure error coefficient at:	
$\phi = 0^\circ$; without bleed air	I
$\phi = 0^\circ$; with bleed air	II
$\phi = 45^\circ$; without bleed air	III
$\phi = 45^\circ$; with bleed air	IV
$\phi = 90^\circ$; without bleed air	V
$\phi = 90^\circ$; with bleed air	VI

	Figure
Variation of static-pressure error coefficient with longitudinal orifice station for:	
M = 0.70; $\phi = 0^\circ$	5
M = 1.00; $\phi = 0^\circ$	6
M = 0.70; $\phi = 45^\circ$	7
M = 1.00; $\phi = 45^\circ$	8
M = 0.70; $\phi = 90^\circ$	9
M = 1.00; $\phi = 90^\circ$	10

CONCLUDING REMARK

Results have been presented of experimental pressure distributions obtained at transonic speeds over the cylindrical portion of a cruciform-wing missile configuration both with and without auxiliary exhaust bleed air. No analysis of the results is attempted.

Langley Research Center,
National Aeronautics and Space Administration,
Langley Station, Hampton, Va., March 19, 1962.

REFERENCES

1. Compitello, Frank E.: Hawk Missile Body-Port Pressure Distribution Survey at Various Angles of Attack and Roll for Mach Numbers of 1.36, 1.58, 1.88, 2.00, & 2.17. Tech. Memo. No. 21, Feltman Res. and Eng. Labs., Picatinny Arsenal (Dover, N. J.), Feb. 1959.

2. Compitello, Frank E.: Hawk Missile Manifolded Body-Port Pressure Distributions at Various Angles of Attack and Roll for Mach Numbers of 1.25, 1.36, 1.58, 1.88, 2.00, and 2.17. Tech. Memo. No. 37, Feltman Res. and Eng. Labs., Picatinny Arsenal (Dover, N. J.), Feb. 1960.

TABLE I.- BODY STATIC-PRESSURE ERROR COEFFICIENTS $(p - p_\infty)/p_\infty$ WITHOUT BLEED AIR.

(a) $\phi = 0^\circ$; M = 0.70.

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	$\alpha = -2.0^\circ$							
0.0	-0.0061	-0.0107	-0.0107	-0.0061	-0.0061	-0.0061	-0.0014	0.0032
22.5	-0.0107	-0.0107	-0.0014	-0.0107	-0.0061	-0.0061	-0.0014	0.0032
45.0	-0.0061	-0.0061	-0.0107	-0.0061	-0.0061		-0.0061	0.0214
67.5	-0.0107	-0.0107	-0.0061	-0.0061	-0.0061	-0.0014	-0.0014	0.0032
112.5	-0.0107	-0.0152	-0.0061	-0.0107	-0.0061	-0.0061	-0.0014	0.0077
135.0	-0.0198	-0.0107	-0.0061	-0.0107	-0.0061	-0.0107	0.0032	0.0169
157.5	-0.0152	-0.0061	-0.0107	-0.0014	-0.0061	-0.0061	-0.0014	-0.0014
180.0	-0.0107		-0.0061	-0.0061	-0.0061	-0.0061	0.0032	-0.0014
202.5	-0.0198	-0.0107	-0.0061	-0.0061	-0.0061	-0.0107	-0.0014	-0.0014
225.0	-0.0152	-0.0107	-0.0107	-0.0107	-0.0061	-0.0061	-0.0061	0.0123
247.5	-0.0107	-0.0061	-0.0014	-0.0014	-0.0061	-0.0014	-0.0014	0.0077
292.5	-0.0061	-0.0061	-0.0061	-0.0061	-0.0014	-0.0014	-0.0014	0.0077
315.0		-0.0061	-0.0014	-0.0014	0.0032	-0.0014	0.0032	0.0260
337.5	-0.0014	-0.0014	-0.0014	0.0032	0.0032	-0.0014	0.0077	
	$\alpha = 0^\circ$							
0.0	-0.0107	-0.0107	-0.0107	-0.0061	-0.0061	-0.0061	-0.0061	-0.0014
22.5	-0.0107	-0.0107	-0.0014	-0.0107	-0.0061	-0.0061	-0.0061	-0.0014
45.0	-0.0061	-0.0107	-0.0107	-0.0061	-0.0061		-0.0061	0.0169
67.5	-0.0107	-0.0107	-0.0061	-0.0061	-0.0061	-0.0014	-0.0014	0.0032
112.5	-0.0107	-0.0107	-0.0061	-0.0061	-0.0061	-0.0061	-0.0014	0.0077
135.0	-0.0152	-0.0107	-0.0061	-0.0107	-0.0061	-0.0107	0.0077	0.0169
157.5	-0.0152	-0.0014	-0.0107	0.0032	-0.0061	-0.0061	-0.0014	0.0032
180.0	-0.0107		-0.0061	-0.0061	-0.0061	-0.0061	0.0032	-0.0014
202.5	-0.0152	-0.0061	-0.0061	-0.0061	-0.0061	-0.0061	-0.0014	0.0032
225.0	-0.0107	-0.0061	-0.0107	-0.0014	-0.0061	-0.0014	-0.0014	0.0169
247.5	-0.0151	-0.0106	-0.0106	-0.0106	-0.0106	-0.0059	-0.0059	0.0032
292.5	-0.0106	-0.0151	-0.0106	-0.0106	-0.0106	-0.0106	-0.0059	0.0032
315.0		-0.0106	-0.0106	-0.0106	-0.0059	-0.0106	-0.0059	0.0168
337.5	-0.0106	-0.0106	-0.0106	-0.0059	-0.0059	-0.0106	-0.0014	
	$\alpha = 2.0^\circ$							
0.0	-0.0151	-0.0151	-0.0151	-0.0151	-0.0151	-0.0151	-0.0106	-0.0106
22.5	-0.0151	-0.0151	-0.0106	-0.0151	-0.0151	-0.0151	-0.0106	-0.0059
45.0	-0.0151	-0.0151	-0.0151	-0.0151	-0.0151		-0.0106	0.0077
67.5	-0.0151	-0.0151	-0.0106	-0.0106	-0.0151	-0.0106	-0.0106	-0.0014
112.5	-0.0197	-0.0197	-0.0151	-0.0151	-0.0151	-0.0151	-0.0106	-0.0014
135.0	-0.0242	-0.0151	-0.0106	-0.0151	-0.0106	-0.0151	-0.0014	0.0123
157.5	-0.0197	-0.0059	-0.0151	-0.0014	-0.0106	-0.0151	-0.0059	-0.0014
180.0	-0.0151		-0.0106	-0.0106	-0.0106	-0.0106	-0.0014	-0.0059
202.5	-0.0242	-0.0151	-0.0106	-0.0106	-0.0106	-0.0151	-0.0059	-0.0014
225.0	-0.0197	-0.0151	-0.0151	-0.0106	-0.0106	-0.0106	-0.0106	0.0077
247.5	-0.0107	-0.0107	-0.0061	-0.0061	-0.0107	-0.0014	-0.0061	0.0032
292.5	-0.0061	-0.0107	-0.0107	-0.0061	-0.0061	-0.0061	-0.0061	0.0032
315.0		-0.0107	-0.0107	-0.0107	-0.0061	-0.0107	-0.0014	0.0169
337.5	-0.0061	-0.0107	-0.0061	-0.0061	-0.0014	-0.0061	-0.0014	
	$\alpha = 4.0^\circ$							
0.0	-0.0107	-0.0107	-0.0107	-0.0061	-0.0061	-0.0061	-0.0061	-0.0014
22.5	-0.0107	-0.0107	-0.0014	-0.0107	-0.0107	-0.0061	-0.0061	-0.0061
45.0	-0.0107	-0.0107	-0.0107	-0.0107	-0.0107		-0.0061	0.0123
67.5	-0.0152	-0.0107	-0.0061	-0.0107	-0.0107	-0.0061	-0.0107	-0.0014
112.5	-0.0152	-0.0152	-0.0107	-0.0107	-0.0107	-0.0107	-0.0061	0.0032
135.0	-0.0198	-0.0107	-0.0107	-0.0152	-0.0061	-0.0107	0.0032	0.0169
157.5	-0.0107	-0.0014	-0.0061	0.0032	-0.0061	-0.0061	-0.0014	0.0032
180.0	-0.0107		-0.0061	-0.0014	-0.0014	-0.0061	0.0032	0.0032
202.5	-0.0198	-0.0107	-0.0061	-0.0061	-0.0061	-0.0107	-0.0014	0.0077
225.0	-0.0198	-0.0152	-0.0152	-0.0107	-0.0107	-0.0107	-0.0061	0.0123
247.5	-0.0107	-0.0107	-0.0061	-0.0061	-0.0107	-0.0061	-0.0061	0.0032
292.5	-0.0107	-0.0107	-0.0061	-0.0061	-0.0061	-0.0061	-0.0061	0.0032
315.0		-0.0107	-0.0061	-0.0061	-0.0061	-0.0107	-0.0014	0.0169
337.5	-0.0061	-0.0107	-0.0061	-0.0061	-0.0014	-0.0061	-0.0014	

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	$\alpha = 8.0^\circ$							
0.0	-0.0061	-0.0061	-0.0061	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015
22.5	-0.0153	-0.0107	-0.0061	-0.0107	-0.0107	-0.0107	-0.0107	-0.0061
45.0	-0.0107	-0.0107	-0.0107	-0.0107	-0.0107		-0.0107	0.0122
67.5	-0.0198	-0.0198	-0.0198	-0.0290	-0.0290	-0.0290	-0.0336	-0.0244
112.5	-0.0198	-0.0198	-0.0153	-0.0153	-0.0107	-0.0153	-0.0107	-0.0015
135.0	-0.0198	-0.0107	-0.0107	-0.0153	-0.0061	-0.0107	0.0031	0.0168
157.5	-0.0061	0.0122	0.0031	0.0076	-0.0015	-0.0015	0.0076	0.0122
180.0	-0.0015		0.0076	0.0076	0.0076	0.0031	0.0168	0.0122
202.5	-0.0107	-0.0015	-0.0015	0.0031	0.0031	-0.0015	0.0031	0.0168
225.0	-0.0153	-0.0107	-0.0153	-0.0107	-0.0107	-0.0107	-0.0015	0.0168
247.5	-0.0230	-0.0184	-0.0138	-0.0093	-0.0184	-0.0093	-0.0138	-0.0047
292.5	-0.0230	-0.0275	-0.0230	-0.0275	-0.0321	-0.0321	-0.0321	-0.0275
315.0		-0.0138	-0.0093	-0.0093	-0.0047	-0.0093	-0.0047	0.0181
337.5	-0.0093	-0.0093	-0.0093	-0.0047	-0.0047	-0.0047	-0.0001	
	$\alpha = 12.0^\circ$							
0.0	-0.0061	-0.0061	-0.0061	-0.0015	-0.0107	-0.0107	-0.0061	-0.0061
22.5	-0.0245	-0.0245	-0.0153	-0.0199	-0.0153	-0.0107	-0.0107	-0.0061
45.0	-0.0107	-0.0107	-0.0107	-0.0107	-0.0107		-0.0153	0.0032
67.5	-0.0705	-0.0705	-0.0567	-0.0521	-0.0475	-0.0429	-0.0429	-0.0382
112.5	-0.0290	-0.0290	-0.0245	-0.0245	-0.0245	-0.0245	-0.0199	-0.0153
135.0	-0.0245	-0.0153	-0.0153	-0.0199	-0.0107	-0.0153	-0.0015	0.0124
157.5	-0.0061	0.0170	0.0032	0.0078	0.0032	0.0078	0.0124	0.0215
180.0	0.0078		0.0170	0.0215	0.0215	0.0124	0.0261	0.0261
202.5	-0.0061	0.0032	0.0078	0.0124	0.0078	0.0032	0.0124	0.0261
225.0	-0.0199	-0.0199	-0.0199	-0.0153	-0.0107	-0.0107	-0.0061	0.0170
247.5	-0.0290	-0.0199	-0.0199	-0.0153	-0.0199	-0.0153	-0.0107	-0.0107
292.5	-0.0659	-0.0750	-0.0659	-0.0567	-0.0475	-0.0429	-0.0382	-0.0290
315.0		-0.0107	-0.0061	-0.0061	-0.0061	-0.0107	-0.0061	0.0124
337.5	-0.0199	-0.0199	-0.0153	-0.0107	-0.0061	-0.0107	-0.0015	
	$\alpha = 15.1^\circ$							
0.0	-0.0061	-0.0153	-0.0153	-0.0107	-0.0153	-0.0153	-0.0153	-0.0107
22.5	-0.0290	-0.0198	-0.0061	-0.0107	-0.0107	-0.0107	-0.0153	-0.0061
45.0	-0.0153	-0.0107	-0.0153	-0.0198	-0.0290		-0.0473	-0.0290
67.5	-0.0840	-0.0656	-0.0565	-0.0611	-0.0611	-0.0565	-0.0519	-0.0473
112.5	-0.0336	-0.0336	-0.0290	-0.0290	-0.0290	-0.0290	-0.0244	-0.0244
135.0	-0.0336	-0.0244	-0.0244	-0.0290	-0.0198	-0.0198	-0.0061	0.0031
157.5	-0.0107	0.0122	0.0031	0.0122	0.0031	0.0076	0.0168	0.0260
180.0	0.0168		0.0214	0.0260	0.0260	0.0214	0.0397	0.0351
202.5	-0.0015	0.0076	0.0122	0.0122	0.0122	0.0076	0.0214	0.0351
225.0	-0.0290	-0.0244	-0.0244	-0.0198	-0.0153	-0.0153	-0.0107	0.0122
247.5	-0.0336	-0.0290	-0.0244	-0.0198	-0.0244	-0.0198	-0.0153	-0.0153
292.5	-0.0977	-0.0931	-0.0794	-0.0702	-0.0611	-0.0611	-0.0565	-0.0565
315.0		-0.0153	-0.0107	-0.0153	-0.0153	-0.0290	-0.0336	-0.0198
337.5	-0.0244	-0.0153	-0.0061	-0.0015	0.0031	-0.0061	-0.0015	

TABLE I.- Continued.

(b) $\phi = 0^{\circ}$; M = 0.80.

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=-2.0°							
0.0	-0.0069	-0.0069	-0.0069	-0.0018	-0.0069	-0.0018	0.0032	0.0084
22.5	-0.0069	-0.0069	0.0032	-0.0069	-0.0018	-0.0018	-0.0018	0.0084
45.0	-0.0069	-0.0069	-0.0069	-0.0069	-0.0069		-0.0018	0.0335
67.5	-0.0119	-0.0069	-0.0018	-0.0069	-0.0069	0.0032	-0.0018	0.0084
112.5	-0.0119	-0.0119	-0.0069	-0.0069	-0.0018	-0.0069	-0.0018	0.0184
135.0	-0.0219	-0.0119	-0.0069	-0.0119	-0.0018	-0.0069	0.0084	0.0234
157.5	-0.0269	-0.0069	-0.0069	0.0032	-0.0018	-0.0069	0.0032	0.0084
180.0	-0.0219		-0.0018	-0.0018	-0.0018	-0.0069	0.0084	0.0032
202.5	-0.0219	-0.0119	-0.0069	-0.0018	-0.0018	-0.0069	0.0032	0.0084
225.0	-0.0169	-0.0069	-0.0119	-0.0069	-0.0069	-0.0069	-0.0018	0.0234
247.5	-0.0087	-0.0037	0.0014	0.0014	-0.0037	0.0064	0.0014	0.0166
292.5	-0.0037	-0.0087	-0.0037	-0.0037	-0.0037	0.0014	0.0014	0.0166
315.0		-0.0037	0.0014	0.0014	0.0014	-0.0037	0.0116	0.0419
337.5	0.0014	-0.0037	0.0014	0.0014	0.0064	0.0014	0.0116	
	α=0°							
0.0	-0.0069	-0.0069	-0.0069	-0.0069	-0.0069	-0.0069	-0.0018	0.0084
22.5	-0.0069	-0.0069	0.0032	-0.0069	-0.0069	-0.0018	-0.0018	0.0084
45.0	-0.0069	-0.0069	-0.0069	-0.0018	-0.0018		-0.0018	0.0335
67.5	-0.0119	-0.0069	-0.0018	-0.0069	-0.0018	0.0032	0.0032	0.0134
112.5	-0.0119	-0.0119	-0.0069	-0.0018	-0.0018	-0.0018	0.0032	0.0184
135.0	-0.0219	-0.0119	-0.0018	-0.0119	-0.0018	-0.0119	0.0084	0.0285
157.5	-0.0269	-0.0018	-0.0069	0.0032	-0.0069	-0.0119	0.0032	0.0084
180.0	-0.0269		-0.0018	-0.0018	-0.0018	-0.0119	0.0084	0.0032
202.5	-0.0269	-0.0119	-0.0069	-0.0069	-0.0018	-0.0119	-0.0018	0.0084
225.0	-0.0169	-0.0119	-0.0119	-0.0069	-0.0069	-0.0069	-0.0018	0.0234
247.5	-0.0119	-0.0069	-0.0069	-0.0018	-0.0069	-0.0018	-0.0018	0.0134
292.5	-0.0119	-0.0119	-0.0069	-0.0069	-0.0069	-0.0018	-0.0018	0.0134
315.0		-0.0119	-0.0069	-0.0069	-0.0018	-0.0069	0.0032	0.0285
337.5	-0.0069	-0.0069	-0.0069	-0.0018	-0.0018	-0.0069	0.0032	
	α=2.0°							
0.0	-0.0069	-0.0069	-0.0069	-0.0069	-0.0069	-0.0069	0.0032	0.0032
22.5	-0.0119	-0.0119	0.0032	-0.0119	-0.0069	-0.0069	-0.0018	0.0032
45.0	-0.0069	-0.0069	-0.0119	-0.0069	-0.0069		-0.0018	0.0234
67.5	-0.0119	-0.0069	-0.0018	-0.0069	-0.0069	0.0032	-0.0018	0.0134
112.5	-0.0119	-0.0119	-0.0069	-0.0069	-0.0018	-0.0069	-0.0018	0.0134
135.0	-0.0219	-0.0119	-0.0018	-0.0119	-0.0018	-0.0119	0.0084	0.0285
157.5	-0.0269		-0.0018	0.0084	-0.0018	-0.0069	0.0084	0.0134
180.0	-0.0269	0.0839	-0.0018	-0.0018	-0.0018	-0.0069	0.0084	0.0032
202.5	-0.0219	-0.0119	-0.0018	-0.0018	-0.0018	-0.0119	0.0032	0.0134
225.0	-0.0169	-0.0119	-0.0119	-0.0069	-0.0069	-0.0069	-0.0018	0.0285
247.5	-0.0169	-0.0119	-0.0069	-0.0018	-0.0119	-0.0069	-0.0018	0.0084
292.5	-0.0069	-0.0169	-0.0069	-0.0069	-0.0069	-0.0069	-0.0018	0.0084
315.0		-0.0119	-0.0069	-0.0069	-0.0018	-0.0069	-0.0018	0.0285
337.5	-0.0069	-0.0119	-0.0069	-0.0069	-0.0018	-0.0069	0.0032	
	α=4.0°							
0.0	-0.0118	-0.0168	-0.0168	-0.0118	-0.0118	-0.0118	-0.0068	-0.0018
22.5	-0.0168	-0.0118	-0.0018	-0.0168	-0.0118	-0.0118	-0.0068	-0.0018
45.0	-0.0168	-0.0168	-0.0168	-0.0118	-0.0118		-0.0068	0.0183
67.5	-0.0168	-0.0118	-0.0068	-0.0118	-0.0168	-0.0068	-0.0118	0.0033
112.5	-0.0218	-0.0218	-0.0118	-0.0168	-0.0118	-0.0118	-0.0068	0.0133
135.0	-0.0318	-0.0168	-0.0118	-0.0218	-0.0068	-0.0168	0.0033	0.0233
157.5	-0.0318	0.0033	-0.0068	0.0083	-0.0068	-0.0118	-0.0018	0.0083
180.0	-0.0268		-0.0018	-0.0018	-0.0018	-0.0118	0.0083	0.0033
202.5	-0.0268	-0.0118	-0.0068	-0.0068	-0.0068	-0.0118	-0.0018	0.0133
225.0	-0.0218	-0.0168	-0.0218	-0.0118	-0.0118	-0.0118	-0.0068	0.0233
247.5	-0.0168	-0.0118	-0.0118	-0.0068	-0.0168	-0.0068	-0.0068	0.0033
292.5	-0.0168	-0.0218	-0.0068	-0.0118	-0.0118	-0.0118	-0.0118	0.0033
315.0		-0.0168	-0.0118	-0.0118	-0.0068	-0.0168	-0.0018	0.0233
337.5	-0.0118	-0.0118	-0.0118	-0.0068	-0.0068	-0.0118	-0.0018	

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=8.0°							
0.0	-0.0069	-0.0069	-0.0069	-0.0018	-0.0069	-0.0069	0.0032	-0.0018
22.5	-0.0169	-0.0119	-0.0018	-0.0119	-0.0119	-0.0069	-0.0069	-0.0018
45.0	-0.0119	-0.0119	-0.0119	-0.0119	-0.0119		-0.0119	0.0234
67.5	-0.0269	-0.0269	-0.0219	-0.0320	-0.0370	-0.0320	-0.0370	-0.0219
112.5	-0.0219	-0.0219	-0.0169	-0.0169	-0.0119	-0.0169	-0.0119	0.0032
135.0	-0.0269	-0.0119	-0.0069	-0.0219	-0.0069	-0.0119	0.0084	0.0285
157.5	-0.0269	0.0184	0.0032	0.0134	0.0032	-0.0018	0.0084	0.0184
180.0	-0.0169		0.0134	0.0134	0.0134	0.0032	0.0234	0.0234
202.5	-0.0169	-0.0018	0.0032	0.0084	0.0084	-0.0018	0.0134	0.0285
225.0	-0.0219	-0.0169	-0.0169	-0.0069	-0.0069	-0.0069	-0.0018	0.0285
247.5	-0.0269	-0.0169	-0.0169	-0.0119	-0.0169	-0.0119	-0.0119	-0.0018
292.5	-0.0269	-0.0370	-0.0320	-0.0320	-0.0370	-0.0422	-0.0422	-0.0269
315.0		-0.0169	-0.0119	-0.0119	-0.0069	-0.0169	-0.0018	0.0234
337.5	-0.0119	-0.0119	-0.0119	-0.0119	-0.0069	-0.0119	-0.0018	
	α=12.0°							
0.0	-0.0018	-0.0018	-0.0069	-0.0018	-0.0069	-0.0119	-0.0018	-0.0018
22.5	-0.0520	-0.0269	-0.0119	-0.0219	-0.0169	-0.0119	-0.0119	-0.0018
45.0	-0.0069	-0.0069	-0.0119	-0.0119	-0.0169		-0.0219	0.0084
67.5	-0.0926	-0.0875	-0.0623	-0.0572	-0.0572	-0.0522	-0.0522	-0.0422
112.5	-0.0370	-0.0320	-0.0269	-0.0269	-0.0269	-0.0269	-0.0219	-0.0069
135.0	-0.0320	-0.0119	-0.0119	-0.0219	-0.0119	-0.0119	0.0084	0.0234
157.5	-0.0269	0.0234	0.0084	0.0184	0.0084	0.0084	0.0234	0.0335
180.0	-0.0069		0.0285	0.0285	0.0285	0.0234	0.0435	0.0385
202.5	-0.0069	0.0084	0.0134	0.0184	0.0184	0.0084	0.0234	0.0385
225.0	-0.0269	-0.0169	-0.0219	-0.0119	-0.0119	-0.0119	-0.0018	0.0285
247.5	-0.0370	-0.0269	-0.0269	-0.0169	-0.0269	-0.0169	-0.0219	-0.0069
292.5	-0.0875	-0.0976	-0.0875	-0.0773	-0.0623	-0.0572	-0.0522	-0.0422
315.0		-0.0119	-0.0069	-0.0119	-0.0069	-0.0169	-0.0119	0.0134
337.5	-0.0320	-0.0269	-0.0269	-0.0169	-0.0069	-0.0119	-0.0018	
	α=15.0°							
0.0	-0.0119	-0.0169	-0.0169	-0.0119	-0.0169	-0.0219	-0.0169	-0.0119
22.5	-0.0422	-0.0269	-0.0069	-0.0169	-0.0119	-0.0119	-0.0169	-0.0069
45.0	-0.0169	-0.0169	-0.0219	-0.0269	-0.0370		-0.0673	-0.0422
67.5	-0.0976	-0.0825	-0.0773	-0.0773	-0.0773	-0.0673	-0.0673	-0.0572
112.5	-0.0472	-0.0472	-0.0422	-0.0422	-0.0370	-0.0422	-0.0370	-0.0269
135.0	-0.0370	-0.0219	-0.0219	-0.0320	-0.0169	-0.0219	-0.0018	0.0134
157.5	-0.0320	0.0234	0.0084	0.0184	0.0134	0.0134	0.0285	0.0385
180.0	0.0084		0.0385	0.0435	0.0435	0.0335	0.0537	0.0537
202.5	-0.0018	0.0134	0.0184	0.0234	0.0234	0.0134	0.0335	0.0486
225.0	-0.0320	-0.0269	-0.0269	-0.0169	-0.0169	-0.0169	-0.0069	0.0234
247.5	-0.0422	-0.0370	-0.0320	-0.0269	-0.0320	-0.0169	-0.0169	-0.0169
292.5	-0.1329	-0.1379	-0.1279	-0.1227	-0.1177	-0.1177	-0.1177	-0.1177
315.0		-0.0219	-0.0169	-0.0219	-0.0219	-0.0370	-0.0422	-0.0169
337.5	-0.0370	-0.0320	-0.0219	-0.0119	-0.0069	-0.0169	-0.0069	

TABLE I.- Continued.

(c) $\phi = 0^{\circ}$; M = 0.90.

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=-2.1°							
0.0	-0.0084	-0.0084	-0.0084	0.0027	0.0027	-0.0029	0.0083	0.0194
22.5	-0.0084	-0.0084	0.0194	-0.0029	-0.0029	0.0027	0.0027	0.0250
45.0	-0.0029	-0.0029	-0.0029	-0.0029	-0.0029		0.0083	0.0528
67.5	-0.0084	-0.0084	0.0027	-0.0029	-0.0029	0.0027	0.0083	0.0194
112.5	-0.0140	-0.0140	-0.0029	-0.0029	0.0027	-0.0029	0.0027	0.0361
135.0	-0.0307	-0.0140	-0.0029	-0.0084	-0.0029	-0.0084	0.0138	0.0361
157.5	-0.0474	-0.0029	-0.0029	0.0083	-0.0029	-0.0084	0.0083	0.0194
180.0	-0.0363		0.0027	0.0027	0.0027	-0.0029	0.0194	0.0083
202.5	-0.0307	-0.0084	0.0027	0.0027	0.0027	-0.0029	0.0083	0.0194
225.0	-0.0196	-0.0084	-0.0084	-0.0029	-0.0029	0.0027	0.0027	0.0361
247.5	-0.0084	-0.0029	-0.0029	0.0083	-0.0084	0.0083	0.0027	0.0194
292.5	-0.0029	-0.0084	-0.0029	-0.0029	-0.0029	0.0027	0.0083	0.0250
315.0		-0.0084	-0.0029	-0.0029	0.0083	-0.0029	0.0138	0.0584
337.5	-0.0029	-0.0084	-0.0029	0.0027	0.0083	-0.0029	0.0138	
	α=-0.1°							
0.0	-0.0054	-0.0054	-0.0054	0.0002	0.0002	0.0002	0.0113	0.0168
22.5	-0.0109	-0.0054	0.0168	-0.0054	0.0002	0.0002	0.0057	0.0168
45.0	-0.0054	-0.0054	-0.0054	0.0002	0.0002		0.0057	0.0446
67.5	-0.0109	-0.0054	0.0002	0.0002	-0.0054	0.0057	0.0057	0.0224
112.5	-0.0165	-0.0109	0.0002	0.0002	0.0002	0.0002	0.0057	0.0335
135.0	-0.0276	-0.0054	0.0057	-0.0054	0.0057	-0.0054	0.0224	0.0446
157.5	-0.0443	0.0113	0.0002	0.0168	0.0002	0.0002	0.0113	0.0224
180.0	-0.0443		0.0057	0.0057	0.0057	-0.0054	0.0168	0.0113
202.5	-0.0332	-0.0054	0.0002	0.0002	0.0002	-0.0054	0.0113	0.0224
225.0	-0.0221	-0.0054	-0.0109	0.0002	0.0002	0.0002	0.0057	0.0391
247.5	-0.0109	-0.0054	-0.0054	0.0002	-0.0054	0.0057	0.0057	0.0224
292.5	-0.0054	-0.0109	-0.0054	-0.0054	0.0002	0.0002	0.0057	0.0224
315.0		-0.0109	0.0002	0.0002	0.0057	-0.0054	0.0113	0.0446
337.5	-0.0054	-0.0109	-0.0054	0.0002	0.0057	-0.0054	0.0113	
	α=2.0°							
0.0	-0.0051	-0.0051	-0.0051	0.0005	0.0005	0.0005	0.0061	0.0173
22.5	-0.0107	-0.0051	0.0173	-0.0051	0.0005	0.0005	0.0061	0.0173
45.0	-0.0051	-0.0051	-0.0051	-0.0051	-0.0051		0.0061	0.0396
67.5	-0.0107	-0.0051	0.0061	0.0005	-0.0051	0.0117	0.0061	0.0229
112.5	-0.0163	-0.0107	-0.0051	-0.0051	0.0005	-0.0051	0.0061	0.0285
135.0	-0.0330	-0.0107	0.0005	-0.0163	0.0005	-0.0107	0.0173	0.0452
157.5	-0.0610	0.0117	0.0005	0.0173	0.0005	-0.0051	0.0117	0.0229
180.0	-0.0554		0.0061	0.0061	0.0061	-0.0051	0.0173	0.0117
202.5	-0.0386	-0.0107	0.0005	0.0005	0.0005	-0.0107	0.0061	0.0229
225.0	-0.0274	-0.0107	-0.0163	-0.0051	-0.0051	-0.0051	0.0005	0.0396
247.5	-0.0107	-0.0051	-0.0051	0.0005	-0.0051	0.0061	0.0061	0.0173
292.5	-0.0051	-0.0107	0.0005	-0.0051	0.0005	0.0005	0.0061	0.0229
315.0		-0.0107	0.0005	0.0005	0.0061	0.0005	0.0117	0.0452
337.5	-0.0051	-0.0051	-0.0051	0.0005	0.0061	0.0005	0.0117	
	α=3.9°							
0.0	-0.0051	0.0005	0.0005	0.0061	0.0061	0.0061	0.0117	0.0173
22.5	-0.0051	-0.0051	0.0229	-0.0051	0.0005	0.0061	0.0061	0.0173
45.0	-0.0051	-0.0051	-0.0051	0.0005	0.0005		0.0061	0.0452
67.5	-0.0051	0.0005	0.0117	0.0005	-0.0051	0.0117	0.0061	0.0229
112.5	-0.0163	-0.0107	0.0005	-0.0051	0.0005	-0.0051	0.0061	0.0396
135.0	-0.0274	-0.0051	0.0061	-0.0051	0.0061	-0.0051	0.0229	0.0564
157.5	-0.0554	0.0229	0.0117	0.0229	0.0061	0.0005	0.0173	0.0285
180.0	-0.0442		0.0173	0.0173	0.0173	0.0005	0.0285	0.0229
202.5	-0.0274	0.0005	0.0117	0.0117	0.0061	0.0005	0.0173	0.0340
225.0	-0.0163	-0.0051	-0.0107	0.0005	0.0005	0.0005	0.0117	0.0452
247.5	-0.0107	-0.0051	0.0005	0.0061	-0.0051	0.0061	0.0061	0.0173
292.5	-0.0051	-0.0107	0.0005	0.0005	0.0005	0.0005	0.0061	0.0229
315.0		-0.0051	0.0005	0.0005	0.0061	0.0005	0.0117	0.0508
337.5	0.0005	0.0005	0.0005	0.0061	0.0117	0.0061	0.0173	

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=7.9°							
0.0	-0.0054	-0.0054	-0.0054	0.0002	0.0002	0.0002	0.0057	0.0113
22.5	-0.0165	-0.0109	0.0113	-0.0109	-0.0054	-0.0054	0.0002	0.0057
45.0	-0.0109	-0.0109	-0.0109	-0.0054	-0.0054		-0.0054	0.0335
67.5	-0.0276	-0.0332	-0.0276	-0.0387	-0.0498	-0.0387	-0.0443	-0.0221
112.5	-0.0276	-0.0276	-0.0165	-0.0221	-0.0109	-0.0165	-0.0054	0.0224
135.0	-0.0332	-0.0109	-0.0054	-0.0221	0.0002	-0.0109	0.0224	0.0446
157.5	-0.0721	0.0279	0.0113	0.0224	0.0057	0.0002	0.0168	0.0335
180.0	-0.0498		0.0224	0.0224	0.0168	0.0057	0.0335	0.0335
202.5	-0.0276	-0.0054	0.0057	0.0113	0.0057	-0.0054	0.0168	0.0391
225.0	-0.0332	-0.0165	-0.0221	-0.0109	-0.0109	-0.0109	-0.0054	0.0446
247.5	-0.0332	-0.0165	-0.0165	-0.0109	-0.0221	-0.0054	-0.0109	0.0002
292.5	-0.0332	-0.0387	-0.0332	-0.0443	-0.0443	-0.0443	-0.0443	-0.0276
315.0		-0.0221	-0.0109	-0.0109	0.0002	-0.0109	0.0002	0.0335
337.5	-0.0109	-0.0165	-0.0165	-0.0109	-0.0054	-0.0109	0.0002	
	α=11.9°							
0.0	0.0061	0.0005	-0.0051	0.0061	0.0005	-0.0051	0.0061	0.0117
22.5	-0.0330	-0.0274	0.0005	-0.0163	-0.0107	0.0005	0.0005	0.0117
45.0	-0.0051	0.0005	-0.0051	-0.0051	-0.0107		-0.0163	0.0173
67.5	-0.1113	-0.1001	-0.0666	-0.0554	-0.0554	-0.0442	-0.0442	-0.0386
112.5	-0.0386	-0.0330	-0.0274	-0.0274	-0.0218	-0.0274	-0.0163	0.0061
135.0	-0.0386	-0.0107	-0.0051	-0.0218	0.0005	-0.0051	0.0173	0.0396
157.5	-0.0721	0.0340	0.0229	0.0285	0.0229	0.0173	0.0340	0.0508
180.0	-0.0330		0.0452	0.0452	0.0452	0.0340	0.0620	0.0620
202.5	-0.0163	0.0173	0.0229	0.0285	0.0285	0.0173	0.0396	0.0620
225.0	-0.0330	-0.0163	-0.0163	-0.0107	-0.0051	-0.0051	0.0005	0.0508
247.5	-0.0330	-0.0218	-0.0163	-0.0107	-0.0218	-0.0051	-0.0051	0.0005
292.5	-0.0945	-0.1113	-0.1001	-0.0889	-0.0721	-0.0666	-0.0610	-0.0442
315.0		-0.0107	0.0005	-0.0051	0.0005	-0.0107	0.0005	0.0340
337.5	-0.0274	-0.0274	-0.0218	-0.0107	0.0005	-0.0051	0.0061	
	α=14.9°							
0.0	0.0005	-0.0051	-0.0051	0.0005	-0.0051	-0.0107	0.0005	0.0061
22.5	-0.0330	-0.0163	0.0117	-0.0051	-0.0051	-0.0051	-0.0051	0.0061
45.0	-0.0051	-0.0051	-0.0107	-0.0163	-0.0330		-0.0721	-0.0386
67.5	-0.1280	-0.0945	-0.0777	-0.0833	-0.0777	-0.0610	-0.0610	-0.0498
112.5	-0.0442	-0.0442	-0.0386	-0.0386	-0.0330	-0.0330	-0.0218	-0.0051
135.0	-0.0442	-0.0163	-0.0163	-0.0218	-0.0107	-0.0163	0.0117	0.0340
157.5	-0.0666	0.0396	0.0285	0.0396	0.0340	0.0285	0.0508	0.0676
180.0	-0.0107		0.0620	0.0676	0.0676	0.0508	0.0787	0.0843
202.5	0.0005	0.0285	0.0396	0.0452	0.0452	0.0340	0.0564	0.0787
225.0	-0.0330	-0.0163	-0.0163	-0.0107	-0.0051	0.0005	0.0061	0.0508
247.5	-0.0386	-0.0274	-0.0218	-0.0107	-0.0163	-0.0051	-0.0051	-0.0051
292.5	-0.1617	-0.1673	-0.1561	-0.1617	-0.1617	-0.1617	-0.1617	-0.1448
315.0		-0.0218	-0.0107	-0.0218	-0.0163	-0.0330	-0.0330	0.0005
337.5	-0.0386	-0.0274	-0.0163	-0.0051	0.0061	-0.0107	0.0061	

TABLE I.- Continued.

(d) $\phi = 0^{\circ}$; M = 0.95.

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=-2.1°							
0.0	-0.0029	-0.0088	-0.0029	0.0030	0.0030	-0.0029	0.0207	0.0266
22.5	-0.0088	-0.0088	0.0207	-0.0029	-0.0029	0.0030	0.0148	0.0325
45.0	-0.0088	-0.0029	-0.0029	-0.0029	-0.0029		0.0089	0.0620
67.5	-0.0088	-0.0088	0.0030	-0.0029	-0.0029	0.0089	0.0089	0.0325
112.5	-0.0206	-0.0206	0.0030	-0.0029	0.0089	-0.0029	0.0089	0.0443
135.0	-0.0383	-0.0088	0.0030	-0.0088	0.0089	-0.0029	0.0207	0.0502
157.5	-0.0560	0.0030	0.0030	0.0148	0.0030	-0.0029	0.0148	0.0266
180.0	-0.0560		0.0089	0.0089	0.0089	-0.0029	0.0266	0.0207
202.5	-0.0442	-0.0029	0.0030	0.0030	0.0030	-0.0029	0.0148	0.0266
225.0	-0.0324	-0.0088	-0.0088	0.0030	-0.0029	0.0030	0.0089	0.0443
247.5	-0.0147	0.0030	0.0030	0.0148	-0.0029	0.0148	0.0089	0.0266
292.5	-0.0029	-0.0088	-0.0029	-0.0029	0.0089	0.0089	0.0148	0.0325
315.0		-0.0088	0.0030	0.0030	0.0148	0.0030	0.0207	0.0679
337.5	0.0030	-0.0088	-0.0029	0.0089	0.0148	0.0030	0.0266	
	α=-0.1°							
0.0	-0.0029	-0.0029	-0.0029	0.0030	0.0030	0.0030	0.0207	0.0266
22.5	-0.0029	-0.0029	0.0207	0.0030	0.0030	0.0089	0.0148	0.0325
45.0	-0.0029	0.0030	0.0030	0.0030	0.0030		0.0148	0.0620
67.5	-0.0029	0.0030	0.0089	0.0089	0.0030	0.0207	0.0207	0.0384
112.5	-0.0206	-0.0088	0.0089	0.0030	0.0148	0.0030	0.0148	0.0502
135.0	-0.0265	0.0030	0.0148	0.0030	0.0207	0.0030	0.0325	0.0620
157.5	-0.0560	0.0148	0.0148	0.0266	0.0148	0.0030	0.0266	0.0384
180.0	-0.0560		0.0148	0.0148	0.0148	0.0030	0.0325	0.0266
202.5	-0.0324	0.0030	0.0089	0.0148	0.0089	-0.0029	0.0207	0.0384
225.0	-0.0206	0.0030	-0.0029	0.0089	0.0030	0.0089	0.0148	0.0561
247.5	-0.0147	0.0030	0.0030	0.0148	0.0030	0.0148	0.0089	0.0325
292.5	-0.0029	-0.0088	0.0030	0.0030	0.0030	0.0089	0.0384	
315.0		-0.0088	0.0030	0.0030	0.0148	0.0030	0.0207	0.0620
337.5	0.0030	-0.0029	-0.0029	0.0089	0.0148	0.0030	0.0266	
	α=1.9°							
0.0	0.0031	0.0031	0.0031	0.0090	0.0149	0.0149	0.0268	0.0268
22.5	-0.0029	0.0090	0.0327	0.0090	0.0090	0.0149	0.0209	0.0387
45.0	0.0031	0.0090	0.0090	0.0090	0.0090		0.0209	0.0624
67.5	0.0031	0.0090	0.0209	0.0090	0.0031	0.0268	0.0209	0.0446
112.5	-0.0147	-0.0029	0.0090	0.0090	0.0149	0.0090	0.0209	0.0565
135.0	-0.0266	0.0090	0.0268	0.0090	0.0209	0.0090	0.0446	0.0743
157.5	-0.0622	0.0268	0.0268	0.0327	0.0209	0.0090	0.0327	0.0446
180.0	-0.0563		0.0268	0.0268	0.0268	0.0090	0.0387	0.0387
202.5	-0.0325	0.0090	0.0209	0.0209	0.0149	0.0090	0.0327	0.0505
225.0	-0.0207	0.0090	0.0031	0.0149	0.0090	0.0090	0.0209	0.0624
247.5	-0.0029	0.0090	0.0090	0.0209	0.0090	0.0209	0.0209	0.0387
292.5	0.0031	-0.0029	0.0149	0.0090	0.0149	0.0149	0.0209	0.0446
315.0		0.0031	0.0090	0.0090	0.0209	0.0090	0.0268	0.0683
337.5	0.0090	0.0031	0.0031	0.0149	0.0209	0.0149	0.0327	
	α=3.8°							
0.0	0.0030	-0.0029	-0.0029	0.0030	0.0030	0.0030	0.0148	0.0207
22.5	-0.0088	-0.0029	0.0207	-0.0029	0.0030	0.0089	0.0148	0.0207
45.0	-0.0088	-0.0029	-0.0029	-0.0029	-0.0029		0.0089	0.0561
67.5	-0.0088	0.0030	0.0148	0.0030	-0.0088	0.0148	0.0089	0.0325
112.5	-0.0206	-0.0147	0.0030	-0.0088	0.0030	-0.0029	0.0148	0.0443
135.0	-0.0324	-0.0029	0.0148	-0.0088	0.0148	-0.0029	0.0325	0.0679
157.5	-0.0795	0.0266	0.0207	0.0325	0.0089	0.0030	0.0266	0.0384
180.0	-0.0737		0.0207	0.0207	0.0148	0.0030	0.0384	0.0325
202.5	-0.0383	0.0030	0.0089	0.0089	0.0089	-0.0029	0.0207	0.0443
225.0	-0.0324	-0.0029	-0.0088	0.0030	-0.0029	0.0030	0.0089	0.0561
247.5	-0.0206	-0.0029	-0.0029	0.0089	-0.0088	0.0089	0.0030	0.0266
292.5	-0.0088	-0.0147	0.0030	-0.0029	0.0030	0.0030	0.0030	0.0325
315.0		-0.0088	0.0030	0.0030	0.0089	-0.0029	0.0207	0.0620
337.5	0.0030	-0.0029	-0.0029	0.0089	0.0148	0.0030	0.0207	

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=7.9°							
0.0	0.0030	0.0030	0.0030	0.0148	0.0089	0.0089	0.0207	0.0266
22.5	-0.0088	-0.0029	0.0207	-0.0029	0.0030	0.0089	0.0148	0.0207
45.0	-0.0029	0.0030	0.0030	0.0030	-0.0029		0.0030	0.0561
67.5	-0.0265	-0.0206	-0.0206	-0.0324	-0.0442	-0.0324	-0.0324	-0.0088
112.5	-0.0206	-0.0147	-0.0088	-0.0147	-0.0029	-0.0147	0.0030	0.0384
135.0	-0.0265	-0.0029	0.0089	-0.0088	0.0148	-0.0029	0.0384	0.0679
157.5	-0.0854	0.0384	0.0325	0.0325	0.0207	0.0089	0.0325	0.0502
180.0	-0.0619		0.0384	0.0325	0.0325	0.0148	0.0502	0.0502
202.5	-0.0265	0.0148	0.0207	0.0207	0.0207	0.0030	0.0266	0.0561
225.0	-0.0324	-0.0029	-0.0147	0.0030	-0.0029	0.0030	0.0089	0.0620
247.5	-0.0265	-0.0088	-0.0088	-0.0029	-0.0147	0.0030	-0.0029	0.0148
292.5	-0.0265	-0.0383	-0.0265	-0.0383	-0.0383	-0.0383	-0.0383	-0.0147
315.0		-0.0147	-0.0029	-0.0029	0.0089	-0.0029	0.0148	0.0561
337.5	-0.0029	-0.0088	-0.0029	0.0030	0.0089	0.0030	0.0207	
	α=11.9°							
0.0	0.0089	0.0030	0.0030	0.0148	0.0089	-0.0029	0.0148	0.0207
22.5	-0.0265	-0.0265	0.0089	-0.0147	-0.0029	0.0030	0.0030	0.0207
45.0	-0.0029	0.0030	-0.0029	-0.0029	-0.0147		-0.0206	0.0207
67.5	-0.0678	-0.0560	-0.0501	-0.0619	-0.0678	-0.0501	-0.0442	-0.0265
112.5	-0.0324	-0.0265	-0.0206	-0.0265	-0.0147	-0.0206	-0.0088	0.0148
135.0	-0.0265	-0.0088	0.0030	-0.0206	0.0089	-0.0029	0.0266	0.0561
157.5	-0.0913	0.0443	0.0384	0.0384	0.0325	0.0266	0.0502	0.0679
180.0	-0.0501		0.0561	0.0561	0.0561	0.0384	0.0738	0.0738
202.5	-0.0147	0.0266	0.0325	0.0384	0.0325	0.0207	0.0502	0.0738
225.0	-0.0383	-0.0088	-0.0147	-0.0029	-0.0029	0.0030	0.0089	0.0620
247.5	-0.0383	-0.0147	-0.0147	-0.0029	-0.0206	0.0030	0.0030	0.0148
292.5	-0.0972	-0.0913	-0.0737	-0.0678	-0.0619	-0.0678	-0.0619	-0.0442
315.0		-0.0088	0.0030	-0.0029	0.0030	-0.0088	0.0030	0.0384
337.5	-0.0265	-0.0265	-0.0206	-0.0088	0.0089	-0.0029	0.0207	
	α=14.9°							
0.0	-0.0029	-0.0088	-0.0088	0.0030	-0.0088	-0.0206	0.0030	0.0030
22.5	-0.0442	-0.0324	-0.0029	-0.0206	-0.0265	-0.0265	-0.0324	-0.0206
45.0	-0.0206	-0.0265	-0.0383	-0.0560	-0.0737		-0.0795	-0.0324
67.5	-0.0854	-0.0737	-0.0678	-0.0795	-0.0854	-0.0678	-0.0619	-0.0383
112.5	-0.0383	-0.0383	-0.0324	-0.0383	-0.0265	-0.0265	-0.0147	0.0089
135.0	-0.0383	-0.0147	-0.0088	-0.0206	-0.0029	-0.0088	0.0207	0.0561
157.5	-0.0854	0.0443	0.0443	0.0502	0.0443	0.0325	0.0620	0.0797
180.0	-0.0383		0.0797	0.0797	0.0738	0.0561	0.0974	0.0974
202.5	-0.0029	0.0325	0.0443	0.0502	0.0502	0.0384	0.0620	0.0915
225.0	-0.0383	-0.0088	-0.0206	-0.0029	-0.0029	0.0030	0.0148	0.0679
247.5	-0.0383	-0.0147	-0.0147	-0.0029	-0.0147	0.0089	0.0030	0.0089
292.5	-0.1918	-0.1918	-0.1800	-0.1800	-0.1741	-0.1741	-0.1623	-0.1328
315.0		-0.0147	-0.0029	-0.0147	-0.0088	-0.0265	-0.0265	0.0089
337.5	-0.0324	-0.0324	-0.0206	-0.0029	0.0148	-0.0029	0.0148	

TABLE I.- Concluded.

(e) $\phi = 0^{\circ}$; M = 1.00.

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=-2.0°							
0.0	0.0606	0.0543	0.0416	0.0479	0.0416	0.0352	0.0543	0.0670
22.5	0.0543	0.0479	0.0733	0.0416	0.0416	0.0416	0.0479	0.0797
45.0	0.0543	0.0543	0.0416	0.0479	0.0352		0.0479	0.1114
67.5	0.0479	0.0479	0.0543	0.0479	0.0352	0.0479	0.0479	0.0733
112.5	0.0352	0.0352	0.0543	0.0416	0.0479	0.0352	0.0479	0.0860
135.0	0.0162	0.0479	0.0606	0.0416	0.0543	0.0289	0.0670	0.0987
157.5	0.0162	0.0606	0.0543	0.0670	0.0479	0.0352	0.0606	0.0733
180.0	0.0162		0.0606	0.0543	0.0543	0.0416	0.0670	0.0606
202.5	0.0162	0.0543	0.0606	0.0543	0.0479	0.0416	0.0606	0.0733
225.0	0.0289	0.0479	0.0479	0.0479	0.0416	0.0416	0.0479	0.0924
247.5	0.0416	0.0543	0.0543	0.0606	0.0352	0.0479	0.0416	0.0670
292.5	0.0606	0.0416	0.0479	0.0416	0.0479	0.0416	0.0479	0.0733
315.0		0.0479	0.0543	0.0416	0.0543	0.0416	0.0606	0.1114
337.5	0.0606	0.0479	0.0479	0.0479	0.0606	0.0416	0.0670	
	α=-0.1°							
0.0	0.0612	0.0548	0.0484	0.0548	0.0484	0.0420	0.0548	0.0676
22.5	0.0548	0.0548	0.0804	0.0484	0.0420	0.0484	0.0548	0.0740
45.0	0.0612	0.0612	0.0548	0.0548	0.0420		0.0548	0.1059
67.5	0.0548	0.0612	0.0676	0.0548	0.0420	0.0612	0.0548	0.0804
112.5	0.0356	0.0484	0.0612	0.0484	0.0548	0.0420	0.0548	0.0932
135.0	0.0229	0.0548	0.0676	0.0420	0.0548	0.0356	0.0676	0.0996
157.5	0.0037	0.0740	0.0612	0.0740	0.0484	0.0420	0.0676	0.0804
180.0	0.0037		0.0676	0.0612	0.0548	0.0420	0.0740	0.0676
202.5	0.0101	0.0612	0.0612	0.0612	0.0484	0.0356	0.0548	0.0804
225.0	0.0292	0.0548	0.0484	0.0548	0.0420	0.0420	0.0548	0.0996
247.5	0.0484	0.0612	0.0612	0.0676	0.0420	0.0548	0.0548	0.0740
292.5	0.0612	0.0548	0.0612	0.0484	0.0548	0.0484	0.0548	0.0868
315.0		0.0548	0.0612	0.0548	0.0612	0.0484	0.0676	0.1125
337.5	0.0676	0.0612	0.0548	0.0548	0.0612	0.0484	0.0676	
	α=2.0°							
0.0	0.0614	0.0550	0.0487	0.0487	0.0421	0.0421	0.0550	0.0614
22.5	0.0550	0.0550	0.0742	0.0421	0.0421	0.0421	0.0550	0.0679
45.0	0.0550	0.0550	0.0487	0.0487	0.0358		0.0487	0.0937
67.5	0.0550	0.0614	0.0679	0.0550	0.0421	0.0550	0.0487	0.0742
112.5	0.0292	0.0487	0.0550	0.0487	0.0487	0.0358	0.0487	0.0808
135.0	0.0100	0.0550	0.0614	0.0421	0.0550	0.0358	0.0679	0.1066
157.5	-0.0158	0.0742	0.0679	0.0742	0.0550	0.0358	0.0614	0.0742
180.0	-0.0158		0.0679	0.0614	0.0550	0.0358	0.0679	0.0679
202.5	-0.0092	0.0614	0.0614	0.0550	0.0487	0.0292	0.0550	0.0808
225.0	0.0163	0.0550	0.0487	0.0487	0.0421	0.0358	0.0487	0.1000
247.5	0.0425	0.0554	0.0554	0.0554	0.0425	0.0488	0.0488	0.0681
292.5	0.0554	0.0488	0.0554	0.0488	0.0488	0.0488	0.0488	0.0747
315.0		0.0554	0.0554	0.0488	0.0488	0.0425	0.0618	0.1004
337.5	0.0618	0.0554	0.0554	0.0554	0.0554	0.0425	0.0618	
	α=4.0°							
0.0	0.0548	0.0548	0.0485	0.0485	0.0419	0.0419	0.0548	0.0612
22.5	0.0485	0.0485	0.0740	0.0419	0.0419	0.0485	0.0548	0.0612
45.0	0.0485	0.0485	0.0485	0.0419	0.0356		0.0419	0.1063
67.5	0.0485	0.0612	0.0677	0.0485	0.0356	0.0485	0.0419	0.0677
112.5	0.0227	0.0485	0.0548	0.0419	0.0485	0.0356	0.0485	0.0806
135.0	-0.0031	0.0548	0.0612	0.0356	0.0548	0.0290	0.0740	0.1063
157.5	-0.0288	0.0806	0.0740	0.0740	0.0548	0.0356	0.0612	0.0806
180.0	-0.0160		0.0740	0.0677	0.0612	0.0356	0.0677	0.0740
202.5	-0.0223	0.0677	0.0612	0.0612	0.0485	0.0290	0.0548	0.0869
225.0	0.0033	0.0548	0.0419	0.0485	0.0419	0.0356	0.0419	0.0998
247.5	0.0357	0.0550	0.0484	0.0550	0.0357	0.0484	0.0421	0.0677
292.5	0.0484	0.0421	0.0550	0.0421	0.0421	0.0421	0.0421	0.0677
315.0		0.0484	0.0484	0.0421	0.0484	0.0357	0.0550	0.1063
337.5	0.0614	0.0484	0.0484	0.0484	0.0550	0.0421	0.0550	

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=8.0°							
0.0	0.0614	0.0550	0.0550	0.0614	0.0550	0.0484	0.0677	0.0677
22.5	0.0484	0.0421	0.0677	0.0421	0.0421	0.0421	0.0550	0.0614
45.0	0.0484	0.0484	0.0484	0.0421	0.0421		0.0484	0.1000
67.5	0.0291	0.0291	0.0228	0.0035	-0.0095	0.0035	0.0098	0.0421
112.5	0.0228	0.0484	0.0484	0.0357	0.0421	0.0228	0.0421	0.0807
135.0	-0.0095	0.0677	0.0614	0.0357	0.0550	0.0357	0.0807	0.1129
157.5	-0.0415	0.0936	0.0870	0.0807	0.0614	0.0484	0.0743	0.0936
180.0	-0.0158		0.0936	0.0870	0.0807	0.0484	0.0870	0.0936
202.5	-0.0222	0.0807	0.0743	0.0743	0.0677	0.0421	0.0677	0.1063
225.0	-0.0029	0.0550	0.0421	0.0484	0.0421	0.0357	0.0421	0.1063
247.5	0.0232	0.0488	0.0488	0.0488	0.0295	0.0425	0.0361	0.0618
292.5	0.0295	0.0168	0.0168	0.0039	-0.0025	-0.0025	-0.0025	0.0232
315.0		0.0425	0.0488	0.0488	0.0488	0.0425	0.0618	0.1068
337.5	0.0554	0.0488	0.0425	0.0488	0.0488	0.0425	0.0554	
	α=12.1°							
0.0	0.0677	0.0614	0.0550	0.0614	0.0484	0.0421	0.0550	0.0614
22.5	0.0098	0.0164	0.0421	0.0164	0.0228	0.0228	0.0291	0.0484
45.0	0.0484	0.0550	0.0421	0.0357	0.0228		0.0098	0.0550
67.5	-0.0673	-0.0222	-0.0029	-0.0095	-0.0095	0.0035	0.0035	0.0164
112.5	-0.0551	0.0421	0.0357	0.0228	0.0291	0.0164	0.0357	0.0614
135.0	-0.0930	0.0550	0.0677	0.0357	0.0550	0.0421	0.0743	0.1000
157.5	-0.0737	0.0807	0.1000	0.0936	0.0807	0.0677	0.0936	0.1129
180.0	-0.0415		0.1193	0.1193	0.1129	0.0807	0.1193	0.1256
202.5	-0.0866	0.0870	0.1000	0.1000	0.0870	0.0614	0.0870	0.1256
225.0	-0.0673	0.0614	0.0421	0.0484	0.0484	0.0421	0.0484	0.1129
247.5	-0.0029	0.0484	0.0421	0.0484	0.0291	0.0421	0.0421	0.0614
292.5	-0.0801	-0.0866	-0.0801	-0.0866	-0.0866	-0.0801	-0.0737	-0.0415
315.0		0.0484	0.0484	0.0421	0.0484	0.0291	0.0421	0.0870
337.5	0.0164	0.0098	0.0098	0.0228	0.0291	0.0228	0.0421	
	α=15.0°							
0.0	0.0614	0.0421	0.0358	0.0487	0.0358	0.0163	0.0421	0.0487
22.5	-0.0158	0.0035	0.0358	0.0163	0.0100	0.0100	0.0100	0.0358
45.0	0.0421	0.0421	0.0292	0.0229	-0.0029		-0.0350	0.0229
67.5	-0.1252	-0.0994	-0.0800	-0.0673	-0.0544	-0.0287	-0.0158	0.0035
112.5	0.0292	0.0292	0.0229	0.0100	0.0163	0.0100	0.0292	0.0421
135.0	-0.0350	0.0550	0.0614	0.0358	0.0487	0.0358	0.0679	0.1000
157.5	-0.0408	0.0937	0.1066	0.1066	0.0937	0.0871	0.1066	0.1321
180.0	-0.0221		0.1387	0.1387	0.1321	0.1066	0.1450	0.1516
202.5	-0.0287	0.1000	0.1066	0.1066	0.1000	0.0808	0.1066	0.1450
225.0	-0.0158	0.0487	0.0421	0.0487	0.0487	0.0421	0.0550	0.1258
247.5	0.0229	0.0422	0.0358	0.0422	0.0294	0.0552	0.0486	0.0616
292.5	-0.1766	-0.1830	-0.1766	-0.1636	-0.1443	-0.1315	-0.1121	-0.0800
315.0		0.0358	0.0422	0.0294	0.0294	0.0037	0.0037	0.0422
337.5	-0.0093	-0.0027	0.0037	0.0229	0.0358	0.0165	0.0358	

TABLE II.- BODY STATIC-PRESSURE ERROR COEFFICIENTS $(p - p_\infty)/p_\infty$ WITH BLEED AIR.

(a) $\phi = 0^\circ$; M = 0.70.

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=-2.1°; w=0.018							
0.0	-0.0015	-0.0015	-0.0061	0.0031	-0.0015	0.0031	0.0031	0.0124
22.5	-0.0015	-0.0015	0.0031	-0.0015	-0.0015	0.0031	0.0031	0.0124
45.0	-0.0015	-0.0015	-0.0015	-0.0015	0.0031	0.0078	0.0031	0.0262
67.5	-0.0015	-0.0061	-0.0015	-0.0015	-0.0015	0.0031	0.0031	0.0078
112.5	-0.0061	-0.0107	-0.0061	-0.0015	-0.0015	-0.0015	0.0031	0.0124
135.0	-0.0107	-0.0061	-0.0015	-0.0015	-0.0015	-0.0015	0.0078	0.0170
157.5	-0.0061	-0.0015	-0.0015	0.0031	-0.0015	-0.0015	0.0031	0.0031
180.0	-0.0107	0.0031	-0.0015	-0.0015	-0.0015	-0.0015	0.0031	0.0031
202.5	-0.0107	-0.0061	-0.0015	-0.0015	-0.0015	-0.0015	0.0031	0.0078
225.0	-0.0107	-0.0061	-0.0015	-0.0015	-0.0015	-0.0015	0.0031	0.0170
247.5	-0.0107	-0.0061	-0.0061	-0.0015	-0.0061	-0.0015	-0.0015	0.0032
292.5	-0.0061	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015	-0.0015	0.0078
315.0		-0.0061	-0.0061	-0.0061	-0.0015	-0.0061	0.0032	0.0262
337.5	-0.0061	-0.0061	-0.0061	-0.0015	0.0032	-0.0015	-0.0015	
	α=8.0°; w=0.018							
0.0	-0.0014	-0.0014	-0.0014	-0.0014	-0.0014	-0.0014	0.0032	0.0032
22.5	-0.0060	-0.0060	-0.0060	-0.0060	-0.0060	-0.0014	-0.0014	-0.0014
45.0	-0.0060	-0.0060	-0.0060	-0.0060	-0.0060	0.0032	-0.0014	0.0171
67.5	-0.0107	-0.0153	-0.0153	-0.0198	-0.0245	-0.0245	-0.0245	-0.0198
112.5	-0.0153	-0.0153	-0.0153	-0.0107	-0.0107	-0.0107	-0.0060	-0.0014
135.0	-0.0153	-0.0060	-0.0060	-0.0107	-0.0014	-0.0060	0.0079	0.0218
157.5	0.0032	0.0125	0.0032	0.0079	0.0032	0.0032	0.0079	0.0171
180.0	-0.0060	0.0125	0.0079	0.0079	0.0079	0.0079	0.0171	0.0125
202.5	-0.0107	-0.0014	-0.0014	0.0032	0.0079	0.0032	0.0079	0.0218
225.0	-0.0153	-0.0107	-0.0060	-0.0060	-0.0060	-0.0060	-0.0014	0.0171
247.5	-0.0152	-0.0152	-0.0152	-0.0107	-0.0107	-0.0107	-0.0107	-0.0061
292.5	-0.0199	-0.0199	-0.0199	-0.0245	-0.0291	-0.0291	-0.0337	-0.0245
315.0		-0.0107	-0.0061	-0.0061	-0.0061	-0.0107	-0.0015	0.0169
337.5	-0.0107	-0.0107	-0.0107	-0.0061	-0.0061	-0.0061	-0.0061	
	α=0°; w=0.018							
0.0	-0.0015	-0.0061	-0.0061	-0.0015	-0.0015	-0.0015	0.0031	0.0078
22.5	-0.0061	-0.0061	-0.0015	-0.0015	-0.0015	0.0031	0.0031	0.0078
45.0	-0.0015	-0.0015	-0.0015	-0.0015	0.0031	0.0078	0.0031	0.0262
67.5	-0.0015	-0.0015	-0.0015	-0.0015	-0.0015	0.0031	0.0031	0.0078
112.5	-0.0061	-0.0061	-0.0061	-0.0015	-0.0015	-0.0015	0.0031	0.0124
135.0	-0.0107	-0.0061	-0.0015	-0.0015	0.0031	-0.0015	0.0078	0.0216
157.5	-0.0061	0.0031	-0.0015	0.0031	-0.0015	-0.0015	0.0031	0.0078
180.0	-0.0107	0.0031	-0.0015	-0.0015	0.0031	-0.0015	0.0078	0.0031
202.5	-0.0154	-0.0061	-0.0015	-0.0015	0.0031	-0.0015	0.0031	0.0124
225.0	-0.0061	-0.0061	-0.0015	-0.0015	-0.0015	-0.0015	0.0031	0.0216
247.5	-0.0107	-0.0061	-0.0061	-0.0015	-0.0061	-0.0015	-0.0015	0.0032
292.5	-0.0061	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015	-0.0015	0.0078
315.0		-0.0061	-0.0061	-0.0061	-0.0015	-0.0061	0.0032	0.0215
337.5	-0.0061	-0.0061	-0.0061	-0.0015	-0.0015	-0.0015	-0.0015	
	α=12.0°; w=0.018							
0.0	-0.0015	-0.0015	-0.0061	-0.0015	-0.0061	-0.0061	-0.0061	-0.0015
22.5	-0.0200	-0.0200	-0.0154	-0.0154	-0.0107	-0.0107	-0.0061	-0.0015
45.0	-0.0061	-0.0061	-0.0061	-0.0061	-0.0107	-0.0061	-0.0107	0.0078
67.5	-0.0616	-0.0662	-0.0570	-0.0477	-0.0431	-0.0385	-0.0431	-0.0338
112.5	-0.0292	-0.0246	-0.0246	-0.0246	-0.0200	-0.0200	-0.0154	-0.0107
135.0	-0.0200	-0.0154	-0.0154	-0.0154	-0.0107	-0.0107	0.0031	0.0124
157.5	0.0078	0.0170	0.0078	0.0078	0.0078	0.0078	0.0170	0.0216
180.0	0.0031	0.0216	0.0170	0.0216	0.0216	0.0170	0.0262	0.0262
202.5	-0.0061	0.0031	0.0078	0.0078	0.0124	0.0078	0.0170	0.0309
225.0	-0.0200	-0.0154	-0.0107	-0.0154	-0.0107	-0.0107	-0.0015	0.0170
247.5	-0.0246	-0.0200	-0.0200	-0.0154	-0.0154	-0.0154	-0.0154	-0.0154
292.5	-0.0616	-0.0662	-0.0662	-0.0570	-0.0477	-0.0431	-0.0385	-0.0338
315.0		-0.0107	-0.0061	-0.0107	-0.0061	-0.0107	-0.0061	0.0124
337.5	-0.0200	-0.0200	-0.0200	-0.0154	-0.0107	-0.0107	-0.0061	
	α=2.0°; w=0.018							
0.0	-0.0061	-0.0061	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015	0.0032
22.5	-0.0061	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015	-0.0015	0.0032
45.0	-0.0061	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015	-0.0015	0.0169
67.5	-0.0061	-0.0061	-0.0015	-0.0061	-0.0015	-0.0015	-0.0015	0.0078
112.5	-0.0107	-0.0107	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015	0.0078
135.0	-0.0152	-0.0061	-0.0061	-0.0061	-0.0015	-0.0061	0.0032	0.0169
157.5	-0.0061	-0.0015	-0.0015	0.0032	-0.0015	-0.0061	0.0032	0.0078
180.0	-0.0152	-0.0015	-0.0061	-0.0015	-0.0015	-0.0015	0.0032	0.0032
202.5	-0.0199	-0.0107	-0.0061	-0.0061	-0.0015	-0.0061	0.0032	0.0078
225.0	-0.0152	-0.0107	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015	0.0169
247.5	-0.0107	-0.0061	-0.0061	-0.0015	-0.0061	-0.0015	-0.0015	0.0032
292.5	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015	-0.0015	-0.0015	0.0078
315.0		-0.0107	-0.0061	-0.0061	-0.0015	-0.0061	0.0032	0.0215
337.5	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015	-0.0061	-0.0015	
	α=15.3°; w=0.018							
0.0	-0.0061	-0.0107	-0.0152	-0.0107	-0.0152	-0.0152	-0.0107	-0.0061
22.5	-0.0245	-0.0199	-0.0107	-0.0107	-0.0107	-0.0107	-0.0107	-0.0061
45.0	-0.0152	-0.0152	-0.0152	-0.0199	-0.0245	-0.0291	-0.0429	-0.0291
67.5	-0.0843	-0.0705	-0.0614	-0.0614	-0.0614	-0.0566	-0.0566	-0.0475
112.5	-0.0382	-0.0382	-0.0382	-0.0337	-0.0337	-0.0291	-0.0291	-0.0291
135.0	-0.0291	-0.0199	-0.0199	-0.0199	-0.0152	-0.0199	-0.0107	0.0032
157.5	0.0032	0.0123	0.0078	0.0078	0.0078	0.0078	0.0169	0.0262
180.0	0.0078	0.0307	0.0262	0.0262	0.0307	0.0262	0.0353	0.0353
202.5	-0.0015	0.0078	0.0123	0.0123	0.0123	0.0123	0.0215	0.0353
225.0	-0.0291	-0.0245	-0.0199	-0.0199	-0.0152	-0.0152	-0.0107	0.0123
247.5	-0.0337	-0.0291	-0.0291	-0.0245	-0.0245	-0.0199	-0.0199	-0.0199
292.5	-0.1028	-0.0935	-0.0796	-0.0705	-0.0614	-0.0614	-0.0614	-0.0614
315.0		-0.0152	-0.0152	-0.0199	-0.0199	-0.0337	-0.0337	-0.0199
337.5	-0.0291	-0.0245	-0.0199	-0.0107	-0.0061	-0.0152	-0.0107	
	α=4.0°; w=0.018							
0.0	-0.0061	-0.0061	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015	0.0032
22.5	-0.0061	-0.0061	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015	0.0032
45.0	-0.0061	-0.0107	-0.0061	-0.0061	-0.0061	-0.0015	-0.0015	0.0169
67.5	-0.0061	-0.0061	-0.0015	-0.0061	-0.0061	-0.0015	-0.0015	0.0032
112.5	-0.0107	-0.0107	-0.0107	-0.0061	-0.0061	-0.0061	-0.0015	0.0078
135.0	-0.0152	-0.0061	-0.0061	-0.0061	-0.0015	-0.0061	0.0032	0.0215
157.5	-0.0015	0.0032	-0.0015	0.0032	-0.0015	-0.0061	0.0032	0.0078
180.0	-0.0152	0.0032	-0.0015	-0.0015	-0.0015	-0.0015	0.0078	0.0032
202.5	-0.0199	-0.0061	-0.0061	-0.0015	-0.0015	-0.0061	0.0032	0.0123
225.0	-0.0152	-0.0107	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015	0.0169
247.5	-0.0107	-0.0107	-0.0061	-0.0061	-0.0061	-0.0015	-0.0061	-0.0015
292.5	-0.0107	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015	-0.0061	0.0032
315.0		-0.0107	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015	0.0169
337.5	-0.0061	-0.0107	-0.0061	-0.0061	-0.0015	-0.0061	-0.0015	

TABLE II.- Continued.

(b) $\phi = 0^{\circ}$; M = 0.80.

θ, deg	$(p - p_{\infty})/p_{\infty}$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=-2.0°; w=0.018							
0.0	-0.0066	-0.0066	-0.0066	-0.0014	-0.0014	-0.0014	0.0087	0.0138
22.5	-0.0066	-0.0066	-0.0014	-0.0066	-0.0066	-0.0014	0.0037	0.0138
45.0	-0.0066	-0.0066	-0.0066	-0.0014	-0.0014	0.0087	-0.0014	0.0342
67.5	-0.0066	-0.0066	-0.0014	-0.0066	-0.0066	0.0037	-0.0014	0.0087
112.5	-0.0117	-0.0117	-0.0066	-0.0066	-0.0014	-0.0014	-0.0014	0.0138
135.0	-0.0218	-0.0117	-0.0066	-0.0066	-0.0014	-0.0117	0.0087	0.0241
157.5	-0.0167	-0.0066	-0.0066	-0.0014	-0.0014	-0.0066	0.0037	0.0087
180.0	-0.0268	-0.0014	-0.0066	-0.0014	-0.0014	-0.0066	0.0037	-0.0014
202.5	-0.0268	-0.0117	-0.0066	-0.0066	-0.0066	-0.0066	0.0037	0.0087
225.0	-0.0167	-0.0117	-0.0066	-0.0066	-0.0066	-0.0066	-0.0014	0.0241
247.5	-0.0116	-0.0064	-0.0064	-0.0014	-0.0064	-0.0014	-0.0064	0.0087
292.5	-0.0116	-0.0116	-0.0064	-0.0064	-0.0014	-0.0064	-0.0014	0.0087
315.0		-0.0116	-0.0064	-0.0064	-0.0014	-0.0064	0.0087	0.0340
337.5	-0.0064	-0.0064	-0.0064	-0.0014	0.0037	-0.0064	0.0037	
	α=0°; w=0.018							
0.0	-0.0066	-0.0066	-0.0066	-0.0014	-0.0014	-0.0014	0.0037	0.0087
22.5	-0.0066	-0.0066	-0.0014	-0.0066	-0.0014	-0.0014	0.0037	0.0138
45.0	-0.0066	-0.0066	-0.0066	-0.0014	-0.0014	0.0087	-0.0014	0.0342
67.5	-0.0066	-0.0066	-0.0066	-0.0066	-0.0066	0.0037	0.0037	0.0138
112.5	-0.0117	-0.0117	-0.0066	-0.0066	-0.0014	-0.0014	-0.0014	0.0190
135.0	-0.0167	-0.0066	-0.0066	-0.0066	-0.0014	-0.0066	0.0138	0.0291
157.5	-0.0167	-0.0014	-0.0014	0.0037	-0.0014	-0.0066	0.0037	0.0087
180.0	-0.0268	0.0037	-0.0014	-0.0014	-0.0014	-0.0014	0.0087	0.0037
202.5	-0.0268	-0.0117	-0.0066	-0.0066	-0.0014	-0.0066	0.0037	0.0138
225.0	-0.0167	-0.0066	-0.0066	-0.0066	-0.0014	-0.0014	0.0037	0.0241
247.5	-0.0116	-0.0064	-0.0064	-0.0014	-0.0064	-0.0014	-0.0014	0.0087
292.5	-0.0116	-0.0116	-0.0064	-0.0064	-0.0014	-0.0064	-0.0014	0.0139
315.0		-0.0116	-0.0064	-0.0064	-0.0014	-0.0064	0.0037	0.0340
337.5	-0.0064	-0.0116	-0.0064	-0.0064	-0.0014	-0.0064	0.0037	
	α=1.9°; w=0.018							
0.0	-0.0014	-0.0066	-0.0066	-0.0014	-0.0014	-0.0014	0.0037	0.0138
22.5	-0.0066	-0.0066	-0.0014	-0.0066	-0.0066	-0.0014	0.0037	0.0087
45.0	-0.0066	-0.0066	-0.0066	-0.0014	-0.0014	0.0087	0.0037	0.0291
67.5	-0.0066	-0.0066	0.0037	-0.0014	-0.0014	0.0087	-0.0014	0.0138
112.5	-0.0117	-0.0117	-0.0066	-0.0066	-0.0014	-0.0014	0.0037	0.0138
135.0	-0.0167	-0.0066	-0.0066	-0.0066	-0.0014	-0.0066	0.0087	0.0291
157.5	-0.0167	0.0037	-0.0014	0.0037	-0.0014	-0.0014	0.0087	0.0138
180.0	-0.0268	0.0037	-0.0014	-0.0014	0.0037	-0.0014	0.0087	0.0087
202.5	-0.0268	-0.0066	-0.0014	-0.0014	-0.0014	-0.0066	0.0037	0.0138
225.0	-0.0167	-0.0066	-0.0066	-0.0066	-0.0014	-0.0014	0.0037	0.0291
247.5	-0.0117	-0.0066	-0.0066	-0.0014	-0.0066	-0.0014	-0.0014	0.0087
292.5	-0.0066	-0.0066	-0.0014	-0.0066	-0.0014	-0.0014	0.0037	0.0138
315.0		-0.0066	-0.0014	-0.0014	-0.0014	-0.0014	0.0037	0.0342
337.5	-0.0066	-0.0066	-0.0066	-0.0014	0.0037	-0.0014	0.0037	
	α=3.9°; w=0.018							
0.0	-0.0066	-0.0066	-0.0066	-0.0014	-0.0014	-0.0014	0.0037	0.0087
22.5	-0.0066	-0.0066	-0.0014	-0.0066	-0.0066	-0.0014	0.0037	0.0087
45.0	-0.0066	-0.0066	-0.0066	-0.0066	-0.0066	0.0087	-0.0014	0.0291
67.5	-0.0066	-0.0066	0.0037	-0.0014	-0.0014	0.0037	-0.0014	0.0087
112.5	-0.0117	-0.0117	-0.0066	-0.0066	-0.0014	-0.0014	-0.0014	0.0138
135.0	-0.0218	-0.0066	-0.0014	-0.0066	-0.0014	-0.0066	0.0138	0.0291
157.5	-0.0167	0.0087	0.0037	0.0087	0.0037	-0.0014	0.0087	0.0138
180.0	-0.0268	0.0087	-0.0014	0.0037	0.0037	-0.0014	0.0138	0.0138
202.5	-0.0268	-0.0066	-0.0014	-0.0014	-0.0014	-0.0066	0.0087	0.0190
225.0	-0.0167	-0.0066	-0.0066	-0.0066	-0.0066	-0.0066	0.0037	0.0291
247.5	-0.0166	-0.0116	-0.0116	-0.0064	-0.0116	-0.0064	-0.0064	0.0037
292.5	-0.0116	-0.0116	-0.0064	-0.0064	-0.0064	-0.0064	-0.0064	0.0087
315.0		-0.0116	-0.0116	-0.0116	-0.0064	-0.0116	0.0037	0.0290
337.5	-0.0116	-0.0116	-0.0116	-0.0064	-0.0014	-0.0064	-0.0014	

θ, deg	$(p - p_{\infty})/p_{\infty}$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=6.0°; w=0.018							
0.0	-0.0014	-0.0014	-0.0014	-0.0014	-0.0014	-0.0014	0.0037	0.0087
22.5	-0.0117	-0.0117	-0.0066	-0.0066	-0.0066	-0.0014	-0.0014	0.0037
45.0	-0.0066	-0.0066	-0.0066	-0.0066	-0.0066	0.0037	-0.0014	0.0291
67.5	-0.0167	-0.0218	-0.0218	-0.0268	-0.0321	-0.0268	-0.0321	-0.0167
112.5	-0.0218	-0.0218	-0.0167	-0.0117	-0.0117	-0.0117	-0.0066	0.0087
135.0	-0.0218	-0.0066	-0.0066	-0.0117	-0.0014	-0.0066	0.0138	0.0291
157.5	-0.0117	0.0190	0.0138	0.0138	0.0037	0.0037	0.0190	0.0241
180.0	-0.0167	0.0190	0.0138	0.0138	0.0190	0.0138	0.0291	0.0241
202.5	-0.0167	-0.0014	0.0087	0.0087	0.0087	0.0037	0.0138	0.0291
225.0	-0.0167	-0.0117	-0.0066	-0.0066	-0.0066	-0.0066	-0.0014	0.0291
247.5	-0.0220	-0.0170	-0.0170	-0.0119	-0.0119	-0.0069	-0.0119	-0.0018
292.5	-0.0220	-0.0271	-0.0271	-0.0321	-0.0321	-0.0373	-0.0373	-0.0220
315.0		-0.0119	-0.0069	-0.0069	-0.0018	-0.0069	0.0032	0.0286
337.5	-0.0119	-0.0119	-0.0119	-0.0069	-0.0018	-0.0069	-0.0018	
	α=12.0°; w=0.018							
0.0	0.0034	-0.0017	-0.0017	0.0034	-0.0017	-0.0069	-0.0017	0.0084
22.5	-0.0271	-0.0221	-0.0170	-0.0170	-0.0120	-0.0069	-0.0069	0.0034
45.0	-0.0069	-0.0069	-0.0069	-0.0069	-0.0120	-0.0017	-0.0170	0.0135
67.5	-0.0782	-0.0832	-0.0629	-0.0578	-0.0527	-0.0475	-0.0475	-0.0425
112.5	-0.0323	-0.0323	-0.0323	-0.0271	-0.0221	-0.0221	-0.0170	-0.0120
135.0	-0.0271	-0.0170	-0.0120	-0.0170	-0.0069	-0.0120	0.0084	0.0187
157.5	-0.0120	0.0238	0.0135	0.0135	0.0084	0.0084	0.0238	0.0339
180.0	-0.0120	0.0339	0.0288	0.0288	0.0288	0.0238	0.0389	0.0389
202.5	-0.0120	0.0034	0.0135	0.0135	0.0187	0.0084	0.0238	0.0389
225.0	-0.0271	-0.0170	-0.0170	-0.0170	-0.0120	-0.0120	-0.0069	0.0238
247.5	-0.0320	-0.0270	-0.0270	-0.0220	-0.0220	-0.0169	-0.0169	-0.0169
292.5	-0.0828	-0.0879	-0.0828	-0.0776	-0.0625	-0.0575	-0.0523	-0.0423
315.0		-0.0169	-0.0119	-0.0119	-0.0067	-0.0169	-0.0119	0.0136
337.5	-0.0270	-0.0320	-0.0270	-0.0220	-0.0119	-0.0169	-0.0067	
	α=15.0°; w=0.018							
0.0	-0.0067	-0.0119	-0.0169	-0.0119	-0.0169	-0.0220	-0.0119	-0.0067
22.5	-0.0372	-0.0270	-0.0119	-0.0119	-0.0119	-0.0119	-0.0119	-0.0067
45.0	-0.0169	-0.0169	-0.0220	-0.0270	-0.0372	-0.0423	-0.0625	-0.0372
67.5	-0.0929	-0.0828	-0.0776	-0.0776	-0.0726	-0.0726	-0.0676	-0.0625
112.5	-0.0473	-0.0473	-0.0473	-0.0423	-0.0372	-0.0372	-0.0372	-0.0320
135.0	-0.0320	-0.0220	-0.0220	-0.0270	-0.0169	-0.0220	-0.0067	0.0084
157.5	-0.0169	0.0236	0.0136	0.0136	0.0136	0.0136	0.0287	0.0389
180.0	-0.0017	0.0439	0.0337	0.0389	0.0389	0.0337	0.0490	0.0490
202.5	-0.0067	0.0084	0.0186	0.0186	0.0186	0.0186	0.0287	0.0490
225.0	-0.0320	-0.0220	-0.0220	-0.0169	-0.0169	-0.0169	-0.0017	0.0236
247.5	-0.0372	-0.0320	-0.0270	-0.0220	-0.0220	-0.0169	-0.0169	-0.0169
292.5	-0.1284	-0.1284	-0.1232	-0.1132	-0.1132	-0.1132	-0.1182	-0.1132
315.0		-0.0220	-0.0169	-0.0220	-0.0220	-0.0320	-0.0320	-0.0067
337.5	-0.0372	-0.0270	-0.0220	-0.0119	-0.0067	-0.0169	-0.0067	

TABLE II.- Continued.

(c) $\phi = 0^{\circ}$; M = 0.90.

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=-2.0°; w=0.018							
0.0	0.0007	-0.0049	-0.0049	0.0007	0.0007	0.0007	0.0121	0.0291
22.5	-0.0049	-0.0049	0.0007	0.0007	0.0007	0.0065	0.0121	0.0291
45.0	0.0007	0.0007	0.0007	0.0007	0.0007	0.0177	0.0121	0.0574
67.5	-0.0049	-0.0049	0.0007	0.0007	0.0007	0.0065	0.0065	0.0233
112.5	-0.0106	-0.0106	0.0007	0.0007	0.0065	0.0007	0.0121	0.0291
135.0	-0.0218	-0.0049	0.0007	-0.0049	0.0065	-0.0049	0.0177	0.0403
157.5	-0.0276	0.0007	0.0065	0.0065	0.0007	0.0007	0.0121	0.0177
180.0	-0.0388	0.0065	0.0007	0.0065	0.0065	0.0007	0.0177	0.0121
202.5	-0.0332	-0.0049	0.0007	0.0007	0.0007	0.0007	0.0121	0.0233
225.0	-0.0218	-0.0049	-0.0049	0.0007	0.0007	0.0007	0.0065	0.0403
247.5	-0.0105	-0.0049	-0.0049	0.0008	-0.0049	0.0008	0.0008	0.0176
292.5	-0.0105	-0.0105	-0.0049	-0.0049	0.0008	0.0008	0.0064	0.0176
315.0		-0.0105	-0.0049	-0.0049	0.0008	-0.0049	0.0120	0.0514
337.5	-0.0049	-0.0105	-0.0105	-0.0049	0.0064	-0.0049	0.0120	
	α=-0.1°; w=0.018							
0.0	0.0007	-0.0049	-0.0049	0.0007	0.0007	0.0007	0.0121	0.0233
22.5	-0.0049	-0.0049	0.0007	0.0007	0.0007	0.0065	0.0121	0.0233
45.0	0.0007	0.0007	0.0007	0.0007	0.0007	0.0177	0.0121	0.0516
67.5	-0.0049	-0.0049	0.0007	0.0007	0.0007	0.0121	0.0065	0.0233
112.5	-0.0106	-0.0106	-0.0049	0.0007	0.0065	0.0007	0.0121	0.0291
135.0	-0.0218	-0.0049	0.0065	0.0007	0.0065	0.0007	0.0233	0.0459
157.5	-0.0276	0.0065	0.0065	0.0121	0.0065	0.0007	0.0121	0.0233
180.0	-0.0444	0.0065	0.0065	0.0065	0.0065	0.0007	0.0177	0.0177
202.5	-0.0332	-0.0049	0.0007	0.0007	0.0007	-0.0049	0.0121	0.0291
225.0	-0.0218	-0.0049	-0.0049	0.0007	0.0007	0.0007	0.0121	0.0403
247.5	-0.0164	-0.0052	-0.0052	0.0005	-0.0052	0.0005	0.0005	0.0173
292.5	-0.0108	-0.0052	-0.0052	-0.0052	0.0005	0.0005	0.0061	0.0230
315.0		-0.0108	-0.0052	-0.0052	0.0061	-0.0052	0.0117	0.0511
337.5	-0.0052	-0.0108	-0.0052	0.0005	0.0061	-0.0052	0.0117	
	α=1.9°; w=0.018							
0.0	-0.0108	-0.0108	-0.0108	-0.0052	-0.0052	-0.0052	0.0061	0.0116
22.5	-0.0108	-0.0108	-0.0052	-0.0052	-0.0052	0.0003	0.0061	0.0172
45.0	-0.0108	-0.0108	-0.0108	-0.0052	-0.0052	0.0061	0.0003	0.0341
67.5	-0.0108	-0.0052	0.0003	-0.0052	-0.0052	0.0061	0.0003	0.0229
112.5	-0.0221	-0.0165	-0.0108	-0.0108	-0.0052	-0.0052	0.0003	0.0229
135.0	-0.0334	-0.0108	-0.0052	-0.0108	0.0003	-0.0108	0.0116	0.0398
157.5	-0.0389	0.0061	0.0061	0.0061	0.0003	-0.0052	0.0116	0.0172
180.0	-0.0558	0.0061	0.0003	0.0003	0.0003	-0.0052	0.0116	0.0116
202.5	-0.0445	-0.0108	-0.0052	-0.0052	-0.0052	-0.0108	0.0061	0.0229
225.0	-0.0277	-0.0108	-0.0108	-0.0108	-0.0108	-0.0052	0.0003	0.0341
247.5	-0.0219	-0.0108	-0.0108	-0.0050	-0.0108	-0.0050	-0.0050	0.0061
292.5	-0.0163	-0.0163	-0.0108	-0.0108	-0.0050	-0.0050	0.0005	0.0173
315.0		-0.0163	-0.0050	-0.0108	-0.0050	-0.0108	0.0061	0.0395
337.5	-0.0108	-0.0108	-0.0108	-0.0050	0.0005	-0.0050	0.0061	
	α=4.0°; w=0.018							
0.0	-0.0049	-0.0049	-0.0049	0.0008	0.0008	0.0008	0.0120	0.0120
22.5	-0.0105	-0.0049	0.0008	-0.0049	-0.0049	0.0008	0.0064	0.0176
45.0	-0.0105	-0.0049	-0.0049	-0.0049	-0.0049	0.0120	0.0008	0.0457
67.5	-0.0049	-0.0049	0.0064	0.0008	-0.0049	0.0064	0.0008	0.0176
112.5	-0.0161	-0.0161	-0.0105	-0.0049	0.0008	-0.0049	0.0064	0.0234
135.0	-0.0272	-0.0049	0.0008	-0.0049	0.0064	-0.0049	0.0176	0.0457
157.5	-0.0442	0.0176	0.0120	0.0176	0.0064	0.0008	0.0176	0.0234
180.0	-0.0555	0.0120	0.0064	0.0064	0.0064	0.0008	0.0234	0.0176
202.5	-0.0386	-0.0049	0.0008	0.0008	0.0008	-0.0049	0.0120	0.0345
225.0	-0.0272	-0.0105	-0.0049	-0.0049	-0.0049	-0.0049	0.0064	0.0401
247.5	-0.0106	-0.0049	-0.0049	0.0007	0.0007	0.0065	0.0065	0.0177
292.5	-0.0106	-0.0049	0.0007	-0.0049	0.0007	0.0065	0.0065	0.0233
315.0		-0.0106	-0.0049	0.0007	0.0065	-0.0049	0.0121	0.0516
337.5	0.0007	-0.0049	-0.0049	0.0007	0.0065	0.0007	0.0121	

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=7.9°; w=0.018							
0.0	0.0005	-0.0052	-0.0052	0.0061	0.0005	0.0005	0.0117	0.0173
22.5	-0.0108	-0.0108	-0.0052	-0.0108	-0.0052	-0.0052	0.0005	0.0061
45.0	-0.0108	-0.0108	-0.0108	-0.0052	-0.0052	0.0061	-0.0052	0.0398
67.5	-0.0220	-0.0276	-0.0276	-0.0333	-0.0445	-0.0333	-0.0389	-0.0164
112.5	-0.0276	-0.0220	-0.0220	-0.0220	-0.0108	-0.0164	-0.0052	0.0117
135.0	-0.0333	-0.0164	-0.0108	-0.0164	-0.0052	-0.0108	0.0173	0.0398
157.5	-0.0558	0.0230	0.0117	0.0117	0.0061	0.0005	0.0173	0.0286
180.0	-0.0558	0.0230	0.0173	0.0173	0.0173	0.0061	0.0286	0.0286
202.5	-0.0389	-0.0052	0.0005	0.0061	0.0061	-0.0052	0.0173	0.0398
225.0	-0.0389	-0.0164	-0.0164	-0.0108	-0.0108	-0.0108	-0.0052	0.0398
247.5	-0.0276	-0.0164	-0.0164	-0.0108	-0.0164	-0.0052	-0.0108	0.0005
292.5	-0.0276	-0.0276	-0.0276	-0.0389	-0.0389	-0.0389	-0.0389	-0.0220
315.0		-0.0164	-0.0052	-0.0052	0.0005	-0.0052	0.0117	0.0453
337.5	-0.0052	-0.0108	-0.0108	-0.0052	0.0005	-0.0052	0.0061	
	α=12.0°; w=0.018							
0.0	0.0120	0.0007	0.0007	0.0063	0.0007	0.0007	0.0063	0.0176
22.5	-0.0276	-0.0219	-0.0163	-0.0107	-0.0107	-0.0049	0.0007	0.0176
45.0	-0.0049	-0.0049	-0.0049	-0.0049	-0.0049	0.0007	-0.0107	0.0232
67.5	-0.1067	-0.0955	-0.0616	-0.0558	-0.0558	-0.0502	-0.0502	-0.0388
112.5	-0.0332	-0.0332	-0.0276	-0.0276	-0.0219	-0.0219	-0.0107	0.0007
135.0	-0.0332	-0.0163	-0.0107	-0.0163	-0.0049	-0.0049	0.0176	0.0402
157.5	-0.0502	0.0346	0.0232	0.0232	0.0176	0.0176	0.0346	0.0516
180.0	-0.0332	0.0460	0.0402	0.0402	0.0402	0.0346	0.0572	0.0572
202.5	-0.0219	0.0120	0.0176	0.0232	0.0232	0.0176	0.0346	0.0629
225.0	-0.0332	-0.0163	-0.0107	-0.0107	-0.0049	-0.0049	0.0063	0.0460
247.5	-0.0389	-0.0276	-0.0276	-0.0164	-0.0220	-0.0108	-0.0108	-0.0052
292.5	-0.1007	-0.1064	-0.1064	-0.0951	-0.0782	-0.0670	-0.0670	-0.0501
315.0		-0.0164	-0.0052	-0.0108	-0.0052	-0.0164	-0.0052	0.0286
337.5	-0.0333	-0.0333	-0.0333	-0.0164	-0.0108	-0.0164	0.0005	
	α=15.0°; w=0.018							
0.0	0.0007	-0.0107	-0.0107	-0.0049	-0.0107	-0.0107	0.0007	0.0120
22.5	-0.0276	-0.0163	-0.0049	-0.0049	-0.0049	-0.0049	-0.0049	0.0063
45.0	-0.0107	-0.0107	-0.0163	-0.0219	-0.0332	-0.0388	-0.0672	-0.0388
67.5	-0.1124	-0.0955	-0.0841	-0.0841	-0.0785	-0.0672	-0.0672	-0.0502
112.5	-0.0502	-0.0446	-0.0446	-0.0446	-0.0388	-0.0332	-0.0219	-0.0163
135.0	-0.0388	-0.0163	-0.0163	-0.0219	-0.0107	-0.0163	0.0063	0.0346
157.5	-0.0502	0.0402	0.0290	0.0346	0.0290	0.0290	0.0516	0.0629
180.0	-0.0219	0.0685	0.0629	0.0572	0.0572	0.0516	0.0741	0.0741
202.5	-0.0107	0.0232	0.0290	0.0346	0.0346	0.0290	0.0460	0.0741
225.0	-0.0388	-0.0219	-0.0107	-0.0107	-0.0107	-0.0049	0.0063	0.0516
247.5	-0.0445	-0.0333	-0.0276	-0.0220	-0.0220	-0.0108	-0.0108	-0.0108
292.5	-0.1626	-0.1626	-0.1570	-0.1626	-0.1626	-0.1626	-0.1682	-0.1457
315.0		-0.0220	-0.0164	-0.0220	-0.0220	-0.0389	-0.0333	0.0061
337.5	-0.0389	-0.0389	-0.0276	-0.0108	-0.0052	-0.0164	-0.0052	

TABLE II.- Continued.

(d) $\phi = 0^{\circ}$; $M = 0.95$.

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=-2.0°; w=0.018							
0.0	-0.0029	-0.0088	-0.0088	0.0032	0.0032	0.0032	0.0209	0.0388
22.5	-0.0029	-0.0029	0.0032	-0.0029	-0.0029	0.0091	0.0150	0.0388
45.0	-0.0029	-0.0029	-0.0029	-0.0029	-0.0029	0.0209	0.0091	0.0625
67.5	-0.0088	-0.0029	-0.0029	0.0032	0.0032	0.0091	0.0091	0.0270
112.5	-0.0205	-0.0147	-0.0029	-0.0029	0.0091	0.0032	0.0150	0.0388
135.0	-0.0325	-0.0088	0.0032	-0.0029	0.0091	-0.0029	0.0209	0.0447
157.5	-0.0384	0.0032	0.0091	0.0091	0.0091	0.0032	0.0209	0.0270
180.0	-0.0502	0.0032	0.0032	0.0032	0.0032	0.0032	0.0209	0.0150
202.5	-0.0443	-0.0088	0.0032	0.0032	0.0032	-0.0029	0.0150	0.0270
225.0	-0.0264	-0.0088	-0.0029	0.0032	-0.0029	0.0032	0.0091	0.0447
247.5	-0.0088	-0.0029	0.0032	0.0091	-0.0029	0.0091	0.0032	0.0270
292.5	-0.0088	-0.0088	-0.0029	-0.0029	0.0032	0.0032	0.0150	0.0329
315.0		-0.0088	-0.0029	-0.0029	0.0091	0.0032	0.0209	0.0684
337.5	0.0032	-0.0088	-0.0029	0.0032	0.0150	-0.0029	0.0209	
	α=-0.1°; w=0.018							
0.0	0.0085	0.0025	0.0025	0.0085	0.0085	0.0085	0.0265	0.0385
22.5	0.0025	0.0025	0.0144	0.0085	0.0085	0.0144	0.0205	0.0445
45.0	0.0085	0.0085	0.0085	0.0085	0.0085	0.0265	0.0205	0.0684
67.5	0.0025	0.0025	0.0144	0.0085	0.0085	0.0265	0.0205	0.0445
112.5	-0.0095	-0.0036	0.0085	0.0085	0.0205	0.0144	0.0205	0.0504
135.0	-0.0216	0.0025	0.0144	0.0085	0.0205	0.0085	0.0324	0.0625
157.5	-0.0396	0.0144	0.0205	0.0205	0.0205	0.0085	0.0265	0.0385
180.0	-0.0515	0.0205	0.0205	0.0205	0.0205	0.0144	0.0324	0.0324
202.5	-0.0335	0.0025	0.0144	0.0144	0.0144	0.0085	0.0265	0.0385
225.0	-0.0216	0.0025	0.0025	0.0085	0.0144	0.0144	0.0205	0.0625
247.5	-0.0145	-0.0027	0.0034	0.0093	0.0034	0.0093	0.0093	0.0272
292.5	-0.0027	-0.0086	0.0034	-0.0027	0.0093	0.0093	0.0152	0.0331
315.0		-0.0086	0.0034	-0.0027	0.0093	0.0034	0.0211	0.0627
337.5	-0.0027	-0.0086	-0.0027	0.0034	0.0152	0.0034	0.0211	
	α=2.0°; w=0.018							
0.0	0.0031	-0.0029	-0.0029	0.0092	0.0092	0.0092	0.0210	0.0331
22.5	-0.0029	-0.0029	0.0092	0.0031	0.0031	0.0092	0.0210	0.0331
45.0	0.0031	0.0031	0.0031	0.0031	0.0031	0.0210	0.0151	0.0568
67.5	0.0031	0.0031	0.0151	0.0092	0.0031	0.0210	0.0151	0.0390
112.5	-0.0147	-0.0088	0.0031	0.0031	0.0151	0.0031	0.0151	0.0390
135.0	-0.0268	-0.0029	0.0092	0.0031	0.0151	0.0031	0.0331	0.0629
157.5	-0.0507	0.0151	0.0210	0.0210	0.0151	0.0031	0.0270	0.0331
180.0	-0.0625	0.0151	0.0151	0.0151	0.0151	0.0031	0.0270	0.0270
202.5	-0.0446	0.0031	0.0092	0.0092	0.0092	0.0031	0.0210	0.0449
225.0	-0.0327	-0.0029	0.0031	0.0031	0.0092	0.0092	0.0151	0.0568
247.5	-0.0205	-0.0029	-0.0029	0.0032	-0.0029	0.0032	0.0091	0.0209
292.5	-0.0088	-0.0088	-0.0029	-0.0029	0.0032	0.0032	0.0091	0.0329
315.0		-0.0088	-0.0029	-0.0029	0.0032	-0.0029	0.0150	0.0566
337.5	-0.0029	-0.0088	-0.0088	0.0032	0.0091	-0.0029	0.0150	
	α=3.9°; w=0.018							
0.0	0.0031	-0.0029	-0.0029	0.0031	0.0031	0.0092	0.0210	0.0270
22.5	-0.0029	-0.0029	0.0092	0.0031	0.0031	0.0092	0.0151	0.0270
45.0	-0.0029	-0.0029	-0.0029	0.0031	0.0031	0.0210	0.0151	0.0629
67.5	0.0031	0.0031	0.0092	0.0092	0.0031	0.0151	0.0092	0.0331
112.5	-0.0207	-0.0088	-0.0029	-0.0029	0.0031	0.0031	0.0151	0.0390
135.0	-0.0268	-0.0029	0.0031	-0.0029	0.0151	-0.0029	0.0270	0.0629
157.5	-0.0625	0.0210	0.0210	0.0210	0.0151	0.0031	0.0270	0.0390
180.0	-0.0685	0.0210	0.0151	0.0151	0.0151	0.0031	0.0331	0.0270
202.5	-0.0507	0.0031	0.0092	0.0092	0.0092	-0.0029	0.0210	0.0449
225.0	-0.0386	-0.0029	-0.0029	-0.0029	0.0031	0.0031	0.0092	0.0568
247.5	-0.0205	-0.0088	-0.0029	0.0032	-0.0029	0.0032	0.0032	0.0209
292.5	-0.0088	-0.0088	0.0032	-0.0029	0.0032	0.0032	0.0032	0.0270
315.0		-0.0147	-0.0029	-0.0029	0.0091	-0.0029	0.0150	0.0625
337.5	-0.0029	-0.0088	-0.0029	0.0032	0.0091	0.0032	0.0150	

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=7.9°; w=0.018							
0.0	0.0144	0.0085	0.0085	0.0144	0.0144	0.0144	0.0324	0.0385
22.5	-0.0036	0.0025	0.0085	0.0025	0.0085	0.0144	0.0205	0.0265
45.0	0.0025	0.0025	0.0025	0.0085	0.0085	0.0265	0.0144	0.0625
67.5	-0.0155	-0.0216	-0.0216	-0.0276	-0.0335	-0.0276	-0.0276	-0.0036
112.5	-0.0216	-0.0155	-0.0095	-0.0095	0.0025	-0.0036	0.0085	0.0324
135.0	-0.0216	0.0025	0.0025	-0.0036	0.0144	0.0025	0.0324	0.0684
157.5	-0.0695	0.0324	0.0324	0.0265	0.0205	0.0144	0.0324	0.0504
180.0	-0.0636	0.0385	0.0324	0.0324	0.0324	0.0205	0.0504	0.0504
202.5	-0.0396	0.0085	0.0144	0.0205	0.0205	0.0085	0.0265	0.0625
225.0	-0.0396	-0.0036	-0.0036	0.0025	0.0025	0.0025	0.0085	0.0625
247.5	-0.0266	-0.0086	-0.0086	-0.0027	-0.0086	0.0032	-0.0027	0.0153
292.5	-0.0205	-0.0266	-0.0266	-0.0385	-0.0325	-0.0385	-0.0385	-0.0146
315.0		-0.0146	0.0032	0.0032	0.0093	-0.0027	0.0212	0.0631
337.5	-0.0027	-0.0086	-0.0027	0.0032	0.0093	0.0032	0.0153	
	α=12.0°; w=0.018							
0.0	0.0150	0.0032	-0.0029	0.0150	0.0032	0.0032	0.0150	0.0270
22.5	-0.0264	-0.0264	-0.0088	-0.0088	-0.0029	0.0032	0.0091	0.0270
45.0	-0.0029	-0.0029	-0.0029	-0.0029	-0.0088	0.0032	-0.0147	0.0270
67.5	-0.0799	-0.0622	-0.0563	-0.0563	-0.0563	-0.0443	-0.0443	-0.0264
112.5	-0.0325	-0.0325	-0.0325	-0.0264	-0.0205	-0.0205	-0.0088	0.0091
135.0	-0.0264	-0.0088	-0.0029	-0.0147	0.0032	-0.0029	0.0209	0.0447
157.5	-0.0681	0.0388	0.0329	0.0270	0.0270	0.0270	0.0447	0.0625
180.0	-0.0502	0.0566	0.0566	0.0506	0.0506	0.0388	0.0625	0.0684
202.5	-0.0264	0.0150	0.0270	0.0329	0.0329	0.0209	0.0447	0.0743
225.0	-0.0384	-0.0147	-0.0088	-0.0088	-0.0029	0.0032	0.0150	0.0625
247.5	-0.0384	-0.0205	-0.0205	-0.0147	-0.0147	-0.0029	-0.0029	0.0091
292.5	-0.1097	-0.0918	-0.0799	-0.0740	-0.0681	-0.0681	-0.0681	-0.0502
315.0		-0.0088	0.0032	-0.0029	0.0032	-0.0147	-0.0029	0.0388
337.5	-0.0264	-0.0325	-0.0264	-0.0088	0.0032	-0.0088	0.0150	
	α=15.0°; w=0.018							
0.0	0.0032	-0.0088	-0.0147	0.0032	-0.0088	-0.0147	-0.0029	0.0209
22.5	-0.0384	-0.0264	-0.0147	-0.0205	-0.0264	-0.0264	-0.0325	-0.0147
45.0	-0.0147	-0.0264	-0.0384	-0.0563	-0.0681	-0.0563	-0.0740	-0.0264
67.5	-0.0740	-0.0740	-0.0740	-0.0799	-0.0859	-0.0681	-0.0681	-0.0384
112.5	-0.0443	-0.0443	-0.0443	-0.0384	-0.0264	-0.0264	-0.0147	-0.0029
135.0	-0.0325	-0.0147	-0.0088	-0.0147	-0.0029	-0.0088	0.0150	0.0447
157.5	-0.0681	0.0447	0.0388	0.0447	0.0388	0.0388	0.0625	0.0804
180.0	-0.0325	0.0743	0.0743	0.0684	0.0684	0.0566	0.0863	0.0922
202.5	-0.0147	0.0329	0.0388	0.0447	0.0447	0.0329	0.0566	0.0922
225.0	-0.0443	-0.0205	-0.0088	-0.0088	-0.0088	0.0032	0.0091	0.0625
247.5	-0.0384	-0.0205	-0.0205	-0.0088	-0.0088	0.0032	0.0032	0.0032
292.5	-0.1928	-0.1928	-0.1869	-0.1869	-0.1808	-0.1749	-0.1631	-0.1335
315.0		-0.0205	-0.0088	-0.0147	-0.0088	-0.0325	-0.0264	0.0209
337.5	-0.0325	-0.0325	-0.0264	-0.0088	0.0032	-0.0088	0.0032	

TABLE II.- Continued.

(e) $\phi = 0^{\circ}$; $M = 1.00$.

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=-2.0°; w=0.018							
0.0	0.0608	0.0481	0.0416	0.0481	0.0416	0.0353	0.0544	0.0736
22.5	0.0544	0.0481	0.0481	0.0416	0.0353	0.0416	0.0481	0.0799
45.0	0.0544	0.0544	0.0481	0.0416	0.0353	0.0544	0.0416	0.1056
67.5	0.0481	0.0481	0.0481	0.0416	0.0353	0.0416	0.0416	0.0673
112.5	0.0353	0.0353	0.0416	0.0416	0.0416	0.0353	0.0481	0.0736
135.0	0.0161	0.0416	0.0481	0.0353	0.0481	0.0289	0.0608	0.0865
157.5	0.0161	0.0544	0.0544	0.0544	0.0416	0.0353	0.0544	0.0608
180.0	0.0093	0.0544	0.0544	0.0481	0.0416	0.0353	0.0544	0.0544
202.5	0.0098	0.0416	0.0481	0.0416	0.0416	0.0289	0.0481	0.0673
225.0	0.0224	0.0416	0.0416	0.0353	0.0353	0.0353	0.0416	0.0865
247.5	0.0417	0.0546	0.0546	0.0483	0.0354	0.0483	0.0417	0.0610
292.5	0.0546	0.0483	0.0483	0.0417	0.0417	0.0417	0.0483	0.0673
315.0		0.0483	0.0546	0.0417	0.0483	0.0354	0.0546	0.1122
337.5	0.0610	0.0483	0.0483	0.0483	0.0483	0.0354	0.0546	
	α=0°; w=0.018							
0.0	0.0618	0.0554	0.0425	0.0488	0.0425	0.0425	0.0554	0.0747
22.5	0.0554	0.0554	0.0554	0.0425	0.0425	0.0425	0.0554	0.0811
45.0	0.0618	0.0554	0.0488	0.0488	0.0425	0.0554	0.0488	0.1068
67.5	0.0618	0.0554	0.0618	0.0488	0.0488	0.0554	0.0488	0.0811
112.5	0.0361	0.0425	0.0488	0.0425	0.0488	0.0425	0.0554	0.0811
135.0	0.0232	0.0554	0.0554	0.0425	0.0554	0.0425	0.0681	0.1004
157.5	0.0168	0.0681	0.0681	0.0618	0.0488	0.0425	0.0618	0.0747
180.0	0.0039	0.0681	0.0618	0.0554	0.0488	0.0425	0.0618	0.0618
202.5	0.0102	0.0554	0.0554	0.0488	0.0425	0.0361	0.0554	0.0747
225.0	0.0232	0.0488	0.0488	0.0488	0.0425	0.0425	0.0554	0.0940
247.5	0.0486	0.0616	0.0552	0.0552	0.0486	0.0486	0.0486	0.0744
292.5	0.0616	0.0552	0.0552	0.0486	0.0486	0.0486	0.0552	0.0808
315.0		0.0552	0.0552	0.0486	0.0552	0.0422	0.0616	0.1131
337.5	0.0680	0.0552	0.0486	0.0486	0.0552	0.0422	0.0616	
	α=2.0°; w=0.018							
0.0	0.0618	0.0554	0.0488	0.0488	0.0425	0.0425	0.0554	0.0681
22.5	0.0554	0.0554	0.0554	0.0488	0.0425	0.0488	0.0554	0.0747
45.0	0.0554	0.0554	0.0488	0.0488	0.0425	0.0554	0.0488	0.1004
67.5	0.0618	0.0618	0.0681	0.0554	0.0488	0.0618	0.0488	0.0811
112.5	0.0361	0.0488	0.0554	0.0425	0.0488	0.0425	0.0554	0.0811
135.0	0.0232	0.0554	0.0618	0.0488	0.0554	0.0361	0.0681	0.1004
157.5	0.0039	0.0747	0.0681	0.0681	0.0554	0.0425	0.0618	0.0747
180.0	-0.0091	0.0747	0.0618	0.0618	0.0554	0.0361	0.0681	0.0681
202.5	-0.0025	0.0554	0.0618	0.0488	0.0488	0.0361	0.0554	0.0811
225.0	0.0232	0.0554	0.0554	0.0488	0.0425	0.0425	0.0488	0.1004
247.5	0.0486	0.0552	0.0552	0.0552	0.0422	0.0486	0.0486	0.0680
292.5	0.0616	0.0552	0.0552	0.0486	0.0552	0.0486	0.0552	0.0808
315.0		0.0552	0.0552	0.0486	0.0552	0.0422	0.0616	0.1065
337.5	0.0680	0.0552	0.0486	0.0552	0.0552	0.0422	0.0616	

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=4.0°; w=0.018							
0.0	0.0618	0.0488	0.0488	0.0488	0.0488	0.0425	0.0554	0.0618
22.5	0.0554	0.0488	0.0554	0.0488	0.0425	0.0488	0.0554	0.0681
45.0	0.0554	0.0554	0.0488	0.0488	0.0425	0.0554	0.0488	0.1068
67.5	0.0618	0.0618	0.0681	0.0488	0.0425	0.0554	0.0425	0.0747
112.5	0.0295	0.0488	0.0488	0.0425	0.0488	0.0361	0.0488	0.0811
135.0	0.0168	0.0554	0.0618	0.0425	0.0554	0.0361	0.0681	0.1068
157.5	-0.0025	0.0811	0.0747	0.0747	0.0554	0.0425	0.0618	0.0747
180.0	-0.0154	0.0811	0.0747	0.0681	0.0618	0.0425	0.0747	0.0747
202.5	-0.0154	0.0618	0.0618	0.0554	0.0488	0.0361	0.0554	0.0875
225.0	0.0102	0.0554	0.0554	0.0488	0.0425	0.0425	0.0488	0.1068
247.5	0.0358	0.0552	0.0486	0.0486	0.0422	0.0486	0.0486	0.0680
292.5	0.0552	0.0552	0.0552	0.0422	0.0486	0.0486	0.0486	0.0744
315.0		0.0486	0.0552	0.0486	0.0552	0.0358	0.0616	
337.5	0.0616	0.0552	0.0486	0.0486	0.0552	0.0422	0.0616	0.0229
	α=7.9°; w=0.018							
0.0	0.0750	0.0622	0.0622	0.0686	0.0622	0.0556	0.0750	0.0816
22.5	0.0492	0.0492	0.0556	0.0427	0.0492	0.0492	0.0556	0.0686
45.0	0.0556	0.0556	0.0556	0.0556	0.0492	0.0622	0.0492	0.1074
67.5	0.0427	0.0361	0.0297	0.0103	0.0039	0.0103	0.0167	0.0427
112.5	0.0361	0.0492	0.0492	0.0427	0.0427	0.0361	0.0492	0.0816
135.0	0.0103	0.0686	0.0686	0.0492	0.0622	0.0427	0.0816	0.1139
157.5	-0.0286	0.0944	0.0944	0.0816	0.0686	0.0556	0.0750	0.0944
180.0	-0.0221	0.1010	0.1010	0.0944	0.0816	0.0622	0.0944	0.1010
202.5	-0.0416	0.0816	0.0816	0.0816	0.0686	0.0556	0.0750	0.1074
225.0	-0.0027	0.0622	0.0556	0.0556	0.0492	0.0427	0.0556	0.1139
247.5	0.0361	0.0553	0.0489	0.0489	0.0425	0.0489	0.0425	0.0684
292.5	0.0361	0.0294	0.0294	0.0101	0.0101	0.0037	0.0037	0.0294
315.0		0.0489	0.0553	0.0489	0.0553	0.0489	0.0620	0.1136
337.5	0.0553	0.0553	0.0489	0.0489	0.0553	0.0489	0.0620	
	α=12.0°; w=0.018							
0.0	0.0744	0.0616	0.0552	0.0616	0.0486	0.0422	0.0616	0.0744
22.5	0.0165	0.0165	0.0229	0.0229	0.0229	0.0294	0.0358	0.0616
45.0	0.0552	0.0552	0.0422	0.0422	0.0294	0.0422	0.0165	0.0616
67.5	-0.0478	-0.0157	-0.0027	-0.0027	-0.0027	0.0037	0.0037	0.0165
112.5	-0.0027	0.0358	0.0294	0.0229	0.0294	0.0229	0.0358	0.0616
135.0	-0.0285	0.0552	0.0616	0.0422	0.0552	0.0422	0.0680	0.1001
157.5	-0.0414	0.0873	0.0937	0.0873	0.0808	0.0744	0.0937	0.1131
180.0	-0.0351	0.1065	0.1195	0.1131	0.1065	0.0873	0.1195	0.1195
202.5	-0.0542	0.0873	0.1001	0.0937	0.0873	0.0680	0.0937	0.1259
225.0	-0.0285	0.0552	0.0486	0.0552	0.0486	0.0422	0.0552	0.1195
247.5	0.0099	0.0420	0.0420	0.0420	0.0356	0.0420	0.0420	0.0614
292.5	-0.0738	-0.0738	-0.0802	-0.0802	-0.0802	-0.0738	-0.0674	-0.0352
315.0		0.0484	0.0484	0.0420	0.0484	0.0356	0.0484	0.0999
337.5	0.0163	0.0163	0.0099	0.0227	0.0356	0.0227	0.0484	

TABLE II.- Concluded.

(f) $\phi = 0^{\circ}$; M = 1.03.

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	$\alpha=0^{\circ}$; w=0.018							
0.0	-0.0285	-0.0151	-0.0217	-0.0285	-0.0418	-0.0217	0.0720	0.1323
22.5	-0.0285	-0.0217	-0.0151	-0.0352	-0.0418	-0.0151	0.0720	0.1391
45.0	-0.0151	-0.0217	-0.0285	-0.0285	-0.0352	0.0050	0.0720	0.1658
67.5	-0.0151	-0.0217	-0.0217	-0.0285	-0.0352	-0.0016	0.0720	0.1391
112.5	-0.0553	-0.0619	-0.0352	-0.0352	-0.0285	-0.0151	0.0788	0.1457
135.0	-0.1021	-0.0486	-0.0217	-0.0352	-0.0217	-0.0084	0.0854	0.1592
157.5	-0.0820	-0.0352	-0.0151	-0.0151	-0.0217	-0.0084	0.0854	0.1323
180.0	-0.0955	-0.0352	-0.0217	-0.0217	-0.0217	-0.0151	0.0854	0.1256
202.5	-0.1089	-0.0486	-0.0217	-0.0217	-0.0285	-0.0217	0.0788	0.1391
225.0	-0.0619	-0.0553	-0.0285	-0.0285	-0.0352	-0.0151	0.0720	0.1524
247.5	-0.0286	-0.0353	-0.0286	-0.0220	-0.0353	-0.0085	0.0720	0.1389
292.5	-0.0220	-0.0220	-0.0151	-0.0353	-0.0286	-0.0151	0.0720	0.1456
315.0		-0.0220	-0.0151	-0.0353	-0.0286	-0.0220	0.0786	0.1658
337.5	-0.0220	-0.0220	-0.0151	-0.0220	-0.0286	-0.0220	0.0786	
	$\alpha=1.9^{\circ}$; w=0.018							
0.0	-0.0219	-0.0219	-0.0219	-0.0219	-0.0352	-0.0285	0.0524	0.1267
22.5	-0.0219	-0.0219	-0.0150	-0.0285	-0.0421	-0.0219	0.0457	0.1267
45.0	-0.0219	-0.0219	-0.0285	-0.0285	-0.0352	-0.0083	0.0389	0.1536
67.5	-0.0083	-0.0219	-0.0150	-0.0219	-0.0352	-0.0083	0.0255	0.1401
112.5	-0.0690	-0.0623	-0.0285	-0.0352	-0.0285	-0.0285	0.0255	0.1334
135.0	-0.1162	-0.0555	-0.0219	-0.0352	-0.0219	-0.0352	0.0322	0.1536
157.5	-0.0826	-0.0352	-0.0150	-0.0083	-0.0219	-0.0285	0.0255	0.1198
180.0	-0.1028	-0.0352	-0.0150	-0.0150	-0.0219	-0.0285	0.0255	0.1198
202.5	-0.1162	-0.0488	-0.0219	-0.0150	-0.0285	-0.0421	0.0119	0.1334
225.0	-0.0623	-0.0623	-0.0352	-0.0219	-0.0285	-0.0285	0.0053	0.1536
247.5	-0.0418	-0.0484	-0.0418	-0.0284	-0.0351	-0.0284	0.0119	0.1123
292.5	-0.0351	-0.0351	-0.0284	-0.0418	-0.0351	-0.0284	0.0119	0.1325
315.0		-0.0284	-0.0218	-0.0351	-0.0351	-0.0351	0.0387	0.1458
337.5	-0.0218	-0.0218	-0.0218	-0.0284	-0.0351	-0.0351	0.0454	

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	$\alpha=3.9^{\circ}$; w=0.018							
0.0	-0.0216	-0.0216	-0.0284	-0.0351	-0.0417	-0.0150	0.0715	0.1180
22.5	-0.0284	-0.0284	-0.0216	-0.0417	-0.0417	-0.0084	0.0649	0.1180
45.0	-0.0351	-0.0351	-0.0351	-0.0351	-0.0483	-0.0084	0.0649	0.1514
67.5	-0.0216	-0.0351	-0.0216	-0.0351	-0.0417	-0.0150	0.0449	0.1248
112.5	-0.0950	-0.0749	-0.0417	-0.0549	-0.0351	-0.0417	0.0182	0.1248
135.0	-0.1414	-0.0617	-0.0284	-0.0483	-0.0216	-0.0417	0.0248	0.1514
157.5	-0.0883	-0.0351	-0.0216	-0.0150	-0.0284	-0.0351	0.0182	0.1180
180.0	-0.1148	-0.0351	-0.0216	-0.0216	-0.0216	-0.0351	0.0182	0.1114
202.5	-0.1216	-0.0549	-0.0284	-0.0216	-0.0351	-0.0417	0.0050	0.1314
225.0	-0.0815	-0.0683	-0.0417	-0.0351	-0.0417	-0.0417	-0.0084	0.1514
247.5	-0.0484	-0.0553	-0.0418	-0.0284	-0.0351	-0.0284	0.0119	0.1190
292.5	-0.0351	-0.0284	-0.0284	-0.0418	-0.0351	-0.0218	0.0454	0.1325
315.0		-0.0351	-0.0218	-0.0351	-0.0351	-0.0284	0.0722	0.1593
337.5	-0.0149	-0.0218	-0.0218	-0.0284	-0.0284	-0.0149	0.0722	

TABLE III.- BODY STATIC-PRESSURE ERROR COEFFICIENTS $(p - p_\infty)/p_\infty$ WITHOUT BLEED AIR.

(a) $\phi = 45^\circ$; M = 0.70.

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station								$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8	1	2	3	4	5	6	7	8
	$\alpha=-2.1^\circ$								$\alpha=8.0^\circ$							
0.0	-0.0014	-0.0060	-0.0014	-0.0014	-0.0014	-0.0014	0.0032	0.0079	-0.0107	-0.0153	-0.0153	-0.0107	-0.0107	-0.0107	-0.0060	-0.0060
22.5	-0.0060	-0.0060	0.0079	-0.0060	-0.0014	-0.0014	0.0032	0.0079	-0.0198	-0.0198	-0.0060	-0.0198	-0.0198	-0.0153	-0.0153	-0.0153
45.0	-0.0014	-0.0060	-0.0060	-0.0014	-0.0014		0.0032	0.0218	-0.0245	-0.0245	-0.0245	-0.0198	-0.0198		-0.0198	0.0079
67.5	-0.0014	-0.0060	-0.0014	-0.0014	-0.0014	0.0032		0.0079	-0.0107	-0.0153	-0.0107	-0.0107	-0.0153	-0.0107		0.0032
112.5	-0.0107	-0.0107	-0.0060	-0.0014	-0.0014	-0.0014	0.0032	0.0125	-0.0014	-0.0060	-0.0014	-0.0014	0.0032	0.0032	0.0079	0.0218
135.0	-0.0153	-0.0060	-0.0060	-0.0060	-0.0014	-0.0060	0.0032	0.0171	-0.0107	-0.0014	0.0032	0.0032	0.0079	0.0032	0.0171	0.0356
157.5	-0.0107	0.0032	-0.0014	0.0032	-0.0014	-0.0060	0.0032	0.0079	-0.0198	0.0032	0.0032	0.0032	0.0032	-0.0014	0.0079	0.0125
180.0	-0.0153		-0.0060	-0.0014	-0.0014	-0.0060	0.0032	-0.0014	-0.0245		-0.0060	-0.0060	-0.0060	-0.0107	0.0032	-0.0014
202.5	-0.0153	-0.0060	-0.0014	-0.0014	-0.0014	-0.0060	0.0032	0.0079	-0.0291	-0.0198	-0.0198	-0.0198	-0.0153	-0.0198	-0.0107	-0.0014
225.0	-0.0107	-0.0060	-0.0060	-0.0060	-0.0060	-0.0014	-0.0014	0.0171	-0.0337	-0.0245	-0.0245	-0.0245	-0.0245	-0.0198	-0.0198	-0.0014
247.5	-0.0061	-0.0015	-0.0015	0.0032	-0.0061	0.0078	-0.0107	-0.0061	-0.0200	-0.0154	-0.0154	-0.0107	-0.0107	-0.0107	-0.0107	-0.0061
292.5	-0.0015	-0.0015	-0.0015	-0.0015	-0.0015	0.0078	-0.0061	-0.0061	-0.0107	-0.0107	-0.0107	-0.0107	-0.0107	-0.0107	-0.0061	-0.0061
315.0		-0.0015	-0.0015	-0.0015	0.0078	0.0307	-0.0061	-0.0015		-0.0015	-0.0015	-0.0015	-0.0061	-0.0015	0.0262	-0.0061
337.5	-0.0061	-0.0015	0.0032	-0.0015	0.0032	-0.0061	-0.0061		-0.0107	-0.0107	-0.0061	-0.0061	-0.0107	-0.0061	-0.0061	
	$\alpha=0^\circ$								$\alpha=12.0^\circ$							
0.0	-0.0060	-0.0060	-0.0060	-0.0014	-0.0060	-0.0060	-0.0014	0.0032	-0.0154	-0.0154	-0.0154	-0.0154	-0.0154	-0.0154	-0.0107	-0.0154
22.5	-0.0060	-0.0060	0.0079	-0.0060	-0.0014	-0.0014	0.0032	0.0079	-0.0338	-0.0292	-0.0154	-0.0292	-0.0246	-0.0246	-0.0246	-0.0200
45.0	-0.0060	-0.0060	-0.0060	-0.0060	-0.0014		-0.0014	0.0218	-0.0385	-0.0385	-0.0385	-0.0385	-0.0338		-0.0338	-0.0061
67.5	-0.0060	-0.0107	-0.0014	-0.0060	-0.0060	-0.0014		0.0032	-0.0200	-0.0292	-0.0246	-0.0246	-0.0246	-0.0154		-0.0061
112.5	-0.0107	-0.0107	-0.0060	-0.0060	-0.0014	-0.0060	-0.0014	0.0125	0.0078	0.0031	0.0124	0.0078	0.0124	0.0124	0.0170	0.0309
135.0	-0.0198	-0.0107	-0.0060	-0.0060	-0.0014	-0.0060	0.0079	0.0171	0.0078	0.0124	0.0170	0.0170	0.0216	0.0170	0.0355	0.0540
157.5	-0.0107	-0.0014	-0.0060	-0.0014	-0.0060	-0.0060	0.0032	0.0032	-0.0061	0.0078	0.0078	0.0124	0.0124	0.0078	0.0216	0.0216
180.0	-0.0107		-0.0014	-0.0014	-0.0014	-0.0060	0.0032	0.0032	-0.0246		-0.0061	-0.0061	-0.0061	-0.0154	0.0031	-0.0015
202.5	-0.0198	-0.0107	-0.0060	-0.0060	-0.0060	-0.0107	-0.0014	0.0079	-0.0431	-0.0338	-0.0292	-0.0338	-0.0292	-0.0338	-0.0292	-0.0154
225.0	-0.0153	-0.0107	-0.0060	-0.0060	-0.0060	-0.0060	-0.0014	0.0171	-0.0477	-0.0431	-0.0431	-0.0431	-0.0431	-0.0385	-0.0338	-0.0200
247.5	-0.0107	-0.0107	-0.0061	-0.0061	-0.0107	-0.0061	-0.0061	-0.0015	-0.0245	-0.0245	-0.0199	-0.0199	-0.0245	-0.0199	-0.0199	-0.0245
292.5	-0.0107	-0.0107	-0.0107	-0.0107	-0.0061	-0.0061	-0.0061	0.0032	-0.0291	-0.0337	-0.0291	-0.0337	-0.0291	-0.0291	-0.0337	-0.0245
315.0		-0.0107	-0.0061	-0.0107	-0.0061	-0.0061	-0.0015	0.0215		-0.0061	-0.0015	-0.0061	-0.0061	-0.0107	-0.0061	0.0215
337.5	-0.0107	-0.0107	-0.0107	-0.0061	-0.0061	-0.0107	-0.0061		-0.0245	-0.0291	-0.0291	-0.0245	-0.0245	-0.0291	-0.0291	
	$\alpha=2.0^\circ$								$\alpha=15.0^\circ$							
0.0	-0.0107	-0.0107	-0.0107	-0.0061	-0.0061	-0.0061	-0.0015	-0.0015	-0.0200	-0.0246	-0.0246	-0.0200	-0.0246	-0.0246	-0.0246	-0.0246
22.5	-0.0107	-0.0107	0.0032	-0.0107	-0.0061	-0.0061	-0.0015	0.0032	-0.0385	-0.0338	-0.0246	-0.0338	-0.0338	-0.0338	-0.0338	-0.0385
45.0	-0.0107	-0.0107	-0.0107	-0.0061	-0.0061		-0.0061	0.0169	-0.0570	-0.0570	-0.0570	-0.0523	-0.0523		-0.0523	-0.0292
67.5	-0.0061	-0.0107	-0.0015	-0.0061	-0.0061	-0.0015		0.0078	-0.0431	-0.0477	-0.0292	-0.0338	-0.0385	-0.0246		-0.0246
112.5	-0.0107	-0.0107	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015	0.0078	0.0170	0.0124	0.0170	0.0170	0.0216	0.0216	0.0262	0.0401
135.0	-0.0199	-0.0107	-0.0061	-0.0107	-0.0015	-0.0107	0.0032	0.0169	0.0124	0.0170	0.0262	0.0216	0.0309	0.0262	0.0401	0.0586
157.5	-0.0152	-0.0061	-0.0061	-0.0015	-0.0061	-0.0107	0.0032	0.0032	-0.0015	0.0078	0.0124	0.0170	0.0124	0.0078	0.0216	0.0262
180.0	-0.0107		-0.0015	-0.0015	-0.0061	-0.0107	-0.0015	-0.0015	-0.0385		-0.0200	-0.0154	-0.0200	-0.0246	-0.0061	-0.0107
202.5	-0.0199	-0.0107	-0.0061	-0.0061	-0.0061	-0.0107	-0.0015	0.0032	-0.0616	-0.0523	-0.0523	-0.0523	-0.0523	-0.0570	-0.0477	-0.0338
225.0	-0.0152	-0.0107	-0.0107	-0.0107	-0.0107	-0.0107	-0.0061	0.0123	-0.0708	-0.0662	-0.0662	-0.0662	-0.0616	-0.0616	-0.0570	-0.0431
247.5	-0.0107	-0.0107	-0.0107	-0.0061	-0.0107	-0.0061	-0.0061	-0.0015	-0.0292	-0.0246	-0.0246	-0.0246	-0.0246	-0.0246	-0.0292	-0.0338
292.5	-0.0107	-0.0107	-0.0061	-0.0061	-0.0061	-0.0061	-0.0061	0.0032	-0.0523	-0.0523	-0.0477	-0.0477		-0.0431	-0.0431	-0.0385
315.0		-0.0107	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015	0.0169		-0.0107	-0.0107	-0.0107	-0.0107	-0.0200	-0.0154	0.0124
337.5	-0.0107	-0.0107	-0.0107	-0.0061	-0.0015	-0.0061	-0.0015		-0.0523	-0.0523	-0.0431	-0.0385	-0.0338	-0.0385	-0.0338	
	$\alpha=3.9^\circ$															
0.0	-0.0107	-0.0152	-0.0107	-0.0107	-0.0107	-0.0107	-0.0061	-0.0061								
22.5	-0.0152	-0.0152	-0.0015	-0.0152	-0.0152	-0.0107	-0.0061	-0.0061								
45.0	-0.0152	-0.0107	-0.0107	-0.0107	-0.0107		-0.0107	0.0169								
67.5	-0.0107	-0.0107	-0.0061	-0.0107	-0.0107	-0.0015		0.0032								
112.5	-0.0152	-0.0152	-0.0061	-0.0107	-0.0061	-0.0061	-0.0015	0.0078								
135.0	-0.0199	-0.0107	-0.0061	-0.0107	-0.0015	-0.0107	0.0078	0.0215								
157.5	-0.0199	-0.0061	-0.0061	-0.0015	-0.0061	-0.0107	0.0032	0.0032								
180.0	-0.0152		-0.0061	-0.0015	-0.0061	-0.0107	-0.0015	-0.0015								
202.5	-0.0245	-0.0152	-0.0107	-0.0152	-0.0107	-0.0152	-0.0061	0.0032								
225.0	-0.0245	-0.0152	-0.0152	-0.0152	-0.0152	-0.0152	-0.0107	0.0078								
247.5	-0.0152	-0.0107	-0.0107	-0.0061	-0.0107	-0.0061	-0.0061	-0.0061								
292.5	-0.0061	-0.0107	-0.0061	-0.0061	-0.0061	-0.0061	-0.0061	0.0032								
315.0		-0.0107	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015	0.0169								
337.5	-0.0107	-0.0107	-0.0107	-0.0061	-0.0061	-0.0061	-0.0015									

TABLE III.- Continued.

(b) $\phi = 45^{\circ}$; $M = 0.80$.

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=-2.0°							
0.0	-0.0065	-0.0117	-0.0117	-0.0014	-0.0065	-0.0065	0.0037	0.0037
22.5	-0.0117	-0.0117	0.0140	-0.0065	-0.0065	-0.0014	-0.0014	0.0140
45.0	-0.0117	-0.0065	-0.0065	-0.0065	-0.0117		-0.0014	0.0293
67.5	-0.0117	-0.0065	-0.0065	-0.0065	-0.0065	-0.0014		0.0089
112.5	-0.0167	-0.0117	-0.0065	-0.0065	-0.0065	-0.0065	-0.0014	0.0191
135.0	-0.0218	-0.0117	-0.0065	-0.0117	-0.0014	-0.0065	0.0089	0.0243
157.5	-0.0270	-0.0014	-0.0065	0.0037	-0.0065	-0.0117	0.0037	0.0089
180.0	-0.0270		-0.0117	-0.0065	-0.0065	-0.0117	-0.0014	-0.0014
202.5	-0.0321	-0.0167	-0.0065	-0.0065	-0.0065	-0.0117	-0.0014	0.0037
225.0	-0.0218	-0.0117	-0.0167	-0.0117	-0.0117	-0.0065	-0.0014	0.0191
247.5	-0.0117	-0.0066	-0.0066	0.0037	-0.0066	-0.0015	-0.0015	0.0088
292.5	-0.0066	-0.0117	-0.0066	-0.0066	-0.0015	-0.0015	-0.0015	0.0139
315.0		-0.0117	-0.0066	-0.0066	-0.0015	-0.0066	0.0088	0.0344
337.5	-0.0066	-0.0117	-0.0066	-0.0015	0.0037	-0.0066	0.0088	
	α=-0.1°							
0.0	-0.0117	-0.0117	-0.0117	-0.0066	-0.0066	-0.0066	-0.0015	0.0037
22.5	-0.0117	-0.0117	0.0088	-0.0066	-0.0066	-0.0066	-0.0015	0.0088
45.0	-0.0117	-0.0117	-0.0117	-0.0066	-0.0117	0.0395	-0.0015	0.0293
67.5	-0.0117	-0.0066	-0.0066	-0.0066	-0.0117	-0.0015	0.0754	0.0088
112.5	-0.0168	-0.0168	-0.0117	-0.0117	-0.0066	-0.0117	-0.0066	0.0190
135.0	-0.0219	-0.0117	-0.0015	-0.0066	-0.0015	-0.0066	0.0139	0.0293
157.5	-0.0271	-0.0015	-0.0066	0.0088	-0.0015	-0.0066	0.0037	0.0088
180.0	-0.0219		-0.0015	-0.0015	-0.0015	-0.0066	0.0088	0.0037
202.5	-0.0271	-0.0117	-0.0066	-0.0066	-0.0066	-0.0117	-0.0015	0.0139
225.0	-0.0219	-0.0117	-0.0117	-0.0117	-0.0066	-0.0066	-0.0015	0.0242
247.5	-0.0117	-0.0066	-0.0066	-0.0015	-0.0066	-0.0015	-0.0066	0.0088
292.5	-0.0117	-0.0117	-0.0066	-0.0066	-0.0066	-0.0066	-0.0015	0.0088
315.0		-0.0117	-0.0066	-0.0066	-0.0015	-0.0066	0.0037	0.0293
337.5	-0.0066	-0.0117	-0.0066	-0.0066	-0.0015	-0.0066	0.0037	
	α=2.0°							
0.0	-0.0068	-0.0068	-0.0068	-0.0015	-0.0015	-0.0015	0.0036	0.0036
22.5	-0.0119	-0.0068	0.0139	-0.0068	-0.0068	-0.0015	0.0036	0.0086
45.0	-0.0068	-0.0068	-0.0068	-0.0068	-0.0068		-0.0015	0.0293
67.5	-0.0068	-0.0015	-0.0015	-0.0068	-0.0068	0.0036		0.0139
112.5	-0.0119	-0.0119	-0.0068	-0.0068	-0.0015	-0.0068	0.0036	0.0241
135.0	-0.0222	-0.0068	-0.0015	-0.0068	0.0036	-0.0068	0.0190	0.0344
157.5	-0.0324	0.0036	-0.0015	0.0086	-0.0015	-0.0068	0.0086	0.0139
180.0	-0.0222		0.0036	0.0036	-0.0015	-0.0068	0.0139	0.0086
202.5	-0.0273	-0.0068	-0.0015	-0.0015	-0.0015	-0.0068	0.0036	0.0139
225.0	-0.0170	-0.0119	-0.0119	-0.0068	-0.0068	-0.0068	-0.0015	0.0241
247.5	-0.0117	-0.0066	-0.0066	-0.0015	-0.0066	-0.0015	-0.0015	0.0037
292.5	-0.0066	-0.0117	-0.0066	-0.0066	-0.0015	-0.0015	-0.0015	0.0088
315.0		-0.0117	-0.0066	-0.0066	-0.0015	-0.0066	0.0037	0.0293
337.5	-0.0066	-0.0066	-0.0066	-0.0015	-0.0015	-0.0066	0.0037	
	α=4.0°							
0.0	-0.0066	-0.0117	-0.0117	-0.0066	-0.0066	-0.0066	-0.0014	0.0037
22.5	-0.0117	-0.0117	0.0088	-0.0117	-0.0117	-0.0066	-0.0014	0.0037
45.0	-0.0117	-0.0117	-0.0117	-0.0066	-0.0117		-0.0066	0.0346
67.5	-0.0117	-0.0066	0.0037	-0.0014	-0.0117	0.0037		0.0141
112.5	-0.0117	-0.0117	-0.0014	-0.0066	0.0037	-0.0014	0.0037	0.0242
135.0	-0.0221	-0.0066	0.0037	-0.0066	0.0088	-0.0066	0.0242	0.0397
157.5	-0.0375	0.0037	-0.0014	0.0141	0.0037	-0.0066	0.0141	0.0191
180.0	-0.0323		0.0037	-0.0014	-0.0014	-0.0066	0.0088	0.0088
202.5	-0.0272	-0.0066	-0.0066	-0.0066	-0.0066	-0.0117	-0.0014	0.0141
225.0	-0.0221	-0.0117	-0.0168	-0.0117	-0.0117	-0.0066	-0.0014	0.0191
247.5	-0.0168	-0.0117	-0.0117	-0.0066	-0.0117	-0.0066	-0.0066	-0.0015
292.5	-0.0066	-0.0117	-0.0066	-0.0066	-0.0066	-0.0066	-0.0066	0.0086
315.0		-0.0117	-0.0066	-0.0066	-0.0015	-0.0066	-0.0015	0.0240
337.5	-0.0117	-0.0117	-0.0117	-0.0066	-0.0015	-0.0066	-0.0015	

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=7.9°							
0.0	-0.0068	-0.0119	-0.0119	-0.0068	-0.0068	-0.0068	-0.0017	-0.0017
22.5	-0.0223	-0.0172	0.0036	-0.0172	-0.0223	-0.0119	-0.0119	-0.0119
45.0	-0.0223	-0.0223	-0.0275	-0.0223	-0.0223		-0.0172	0.0191
67.5	-0.0119	-0.0119	-0.0068	-0.0119	-0.0172	-0.0017		0.0087
112.5	-0.0017	-0.0017	0.0087	0.0036	0.0138	0.0087	0.0191	0.0397
135.0	-0.0068	0.0087	0.0138	0.0087	0.0242	0.0087	0.0346	0.0604
157.5	-0.0327	0.0036	0.0087	0.0242	0.0138	0.0036	0.0242	0.0293
180.0	-0.0585		0.0036	-0.0017	-0.0017	-0.0119	0.0138	0.0087
202.5	-0.0327	-0.0172	-0.0172	-0.0119	-0.0119	-0.0223	-0.0068	0.0087
225.0	-0.0379	-0.0223	-0.0275	-0.0223	-0.0223	-0.0223	-0.0172	0.0036
247.5	-0.0223	-0.0170	-0.0119	-0.0068	-0.0119	-0.0068	-0.0068	-0.0068
292.5	-0.0068	-0.0119	-0.0068	-0.0068	-0.0068	-0.0119	-0.0119	-0.0017
315.0		-0.0017	-0.0017	-0.0017	0.0034	-0.0017	0.0087	0.0344
337.5	-0.0068	-0.0068	-0.0068	-0.0068	-0.0017	-0.0068	-0.0017	
	α=12.0°							
0.0	-0.0222	-0.0222	-0.0222	-0.0170	-0.0170	-0.0170	-0.0170	-0.0222
22.5	-0.0428	-0.0377	-0.0170	-0.0377	-0.0324	-0.0324	-0.0273	-0.0324
45.0	-0.0531	-0.0531	-0.0531	-0.0479	-0.0531		-0.0479	-0.0015
67.5	-0.0377	-0.0377	-0.0324	-0.0273	-0.0324	-0.0222		-0.0068
112.5	0.0086	0.0036	0.0139	0.0086	0.0190	0.0139	0.0241	0.0448
135.0	-0.0015	0.0139	0.0241	0.0139	0.0293	0.0241	0.0499	0.0704
157.5	-0.0273	0.0036	0.0086	0.0241	0.0139	0.0086	0.0241	0.0293
180.0	-0.0686		-0.0068	-0.0119	-0.0170	-0.0222	-0.0015	-0.0015
202.5	-0.0582	-0.0428	-0.0377	-0.0428	-0.0428	-0.0479	-0.0377	-0.0222
225.0	-0.0633	-0.0531	-0.0582	-0.0531	-0.0531	-0.0531	-0.0479	-0.0222
247.5	-0.0322	-0.0271	-0.0271	-0.0219	-0.0271	-0.0219	-0.0271	-0.0322
292.5	-0.0373	-0.0424	-0.0373	-0.0424	-0.0373	-0.0373	-0.0424	-0.0322
315.0		-0.0117	-0.0066	-0.0066	-0.0015	-0.0117	-0.0066	0.0242
337.5	-0.0424	-0.0476	-0.0424	-0.0424	-0.0373	-0.0424	-0.0322	
	α=15.0°							
0.0	-0.0271	-0.0271	-0.0322	-0.0271	-0.0322	-0.0322	-0.0271	-0.0322
22.5	-0.0476	-0.0476	-0.0219	-0.0424	-0.0424	-0.0373	-0.0373	-0.0476
45.0	-0.0732	-0.0732	-0.0732	-0.0732	-0.0783		-0.0680	-0.0219
67.5	-0.0578	-0.0629	-0.0424	-0.0476	-0.0527	-0.0373		-0.0322
112.5	0.0139	0.0088	0.0190	0.0190	0.0293	0.0242	0.0344	0.0549
135.0	0.0139	0.0242	0.0395	0.0293	0.0445	0.0344	0.0650	0.0855
157.5	-0.0117	0.0088	0.0139	0.0293	0.0190	0.0139	0.0344	0.0344
180.0	-0.0732		-0.0168	-0.0219	-0.0219	-0.0322	-0.0066	-0.0117
202.5	-0.0783	-0.0578	-0.0629	-0.0629	-0.0680	-0.0732	-0.0578	-0.0373
225.0	-0.0885	-0.0834	-0.0885	-0.0834	-0.0783	-0.0783	-0.0680	-0.0424
247.5	-0.0373	-0.0322	-0.0322	-0.0322	-0.0322	-0.0322	-0.0322	-0.0424
292.5	-0.0680	-0.0732	-0.0629	-0.0578	-0.0578	-0.0527	-0.0527	-0.0424
315.0		-0.0168	-0.0117	-0.0168	-0.0117	-0.0271	-0.0219	0.0139
337.5	-0.0680	-0.0680	-0.0578	-0.0476	-0.0373	-0.0476	-0.0373	

TABLE III.- Continued.

(c) $\phi = 45^{\circ}$; M = 0.90.

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=-1.9°							
0.0	-0.0051	-0.0106	-0.0106	0.0005	-0.0051	-0.0051	0.0118	0.0174
22.5	-0.0106	-0.0106	0.0174	-0.0051	-0.0051	0.0005	0.0062	0.0231
45.0	-0.0051	-0.0051	-0.0051	-0.0051	-0.0051		0.0005	0.0455
67.5	-0.0106	-0.0106	-0.0051	-0.0051	-0.0051	0.0062		0.0174
112.5	-0.0164	-0.0164	-0.0051	-0.0051	0.0005	-0.0051	0.0062	0.0287
135.0	-0.0332	-0.0106	-0.0051	-0.0106	0.0005	-0.0106	0.0118	0.0342
157.5	-0.0444	0.0062	0.0062	0.0062	0.0005	-0.0051	0.0118	0.0174
180.0	-0.0444		-0.0051	0.0005	0.0005	-0.0051	0.0062	0.0062
202.5	-0.0388	-0.0106	-0.0051	-0.0051	-0.0051	-0.0106	0.0062	0.0174
225.0	-0.0275	-0.0106	-0.0106	-0.0051	-0.0106	-0.0051	0.0005	0.0342
247.5	-0.0109	0.0003	0.0003	0.0059	-0.0053	0.0059	0.0059	0.0227
292.5	0.0003	-0.0109	0.0003	0.0003	0.0003	0.0003	0.0059	0.0227
315.0		-0.0053	0.0003	0.0003	0.0059	0.0003	0.0171	0.0621
337.5	-0.0053	-0.0109	0.0003	0.0059	0.0115	0.0003	0.0171	
	α=0°							
0.0	-0.0052	-0.0108	-0.0108	0.0005	0.0005	0.0005	0.0117	0.0173
22.5	-0.0108	-0.0052	0.0173	-0.0052	-0.0052	0.0005	0.0061	0.0230
45.0	-0.0052	-0.0052	-0.0052	0.0005	0.0005		0.0061	0.0453
67.5	-0.0052	-0.0052	0.0005	0.0005	-0.0052	0.0061		0.0230
112.5	-0.0164	-0.0164	-0.0052	-0.0052	0.0005	-0.0052	0.0061	0.0286
135.0	-0.0333	-0.0108	0.0005	-0.0052	0.0061	-0.0052	0.0173	0.0398
157.5	-0.0445	0.0061	0.0061	0.0061	0.0005	-0.0052	0.0173	0.0230
180.0	-0.0445		0.0061	0.0061	0.0061	-0.0052	0.0173	0.0117
202.5	-0.0389	-0.0108	0.0005	-0.0052	0.0005	-0.0052	0.0061	0.0230
225.0	-0.0276	-0.0108	-0.0052	-0.0052	-0.0052	0.0005	0.0061	0.0342
247.5	-0.0108	-0.0052	-0.0052	0.0061	-0.0052	0.0005	0.0005	0.0173
292.5	-0.0052	-0.0108	-0.0052	-0.0052	0.0005	0.0005	0.0061	0.0230
315.0		-0.0108	0.0005	-0.0052	0.0061	-0.0052	0.0117	0.0511
337.5	-0.0052	-0.0108	-0.0052	0.0005	0.0061	-0.0052	0.0117	
	α=2.0°							
0.0	-0.0052	-0.0108	-0.0108	-0.0052	-0.0052	-0.0052	0.0061	0.0117
22.5	-0.0108	-0.0052	0.0173	-0.0052	-0.0052	0.0005	0.0061	0.0173
45.0	-0.0108	-0.0108	-0.0052	-0.0052	-0.0052		0.0005	0.0453
67.5	-0.0052	-0.0052	0.0061	0.0005	-0.0052	0.0117		0.0286
112.5	-0.0164	-0.0108	-0.0052	-0.0052	0.0005	-0.0052	0.0061	0.0342
135.0	-0.0333	-0.0108	0.0005	-0.0052	0.0061	-0.0052	0.0230	0.0511
157.5	-0.0558	0.0061	0.0061	0.0061	0.0005	-0.0052	0.0173	0.0230
180.0	-0.0558		0.0117	0.0061	0.0061	-0.0052	0.0173	0.0117
202.5	-0.0389	-0.0108	-0.0052	0.0005	0.0005	-0.0108	0.0061	0.0230
225.0	-0.0276	-0.0108	-0.0108	-0.0052	-0.0052	-0.0052	0.0005	0.0342
247.5	-0.0164	-0.0052	-0.0052	0.0005	-0.0052	0.0005	0.0005	0.0117
292.5	-0.0052	-0.0108	-0.0052	-0.0052	0.0005	0.0005	0.0061	0.0173
315.0		-0.0108	-0.0052	-0.0052	0.0061	0.0005	0.0117	0.0453
337.5	-0.0052	-0.0108	-0.0052	0.0005	0.0005	0.0005	0.0117	
	α=4.0°							
0.0	-0.0052	-0.0052	-0.0052	0.0005	0.0005	0.0005	0.0061	0.0117
22.5	-0.0108	-0.0108	0.0117	-0.0108	-0.0052	0.0005	0.0061	0.0117
45.0	-0.0108	-0.0052	-0.0052	-0.0052	-0.0052		0.0005	0.0511
67.5	0.0005	-0.0052	0.0061	0.0005	-0.0052	0.0117		0.0286
112.5	-0.0108	-0.0108	0.0005	0.0005	0.0061	0.0005	0.0117	0.0398
135.0	-0.0276	-0.0052	0.0117	0.0005	0.0117	0.0005	0.0286	0.0623
157.5	-0.0614	0.0117	0.0117	0.0117	0.0061	0.0005	0.0230	0.0286
180.0	-0.0726		0.0117	0.0061	0.0061	-0.0052	0.0173	0.0173
202.5	-0.0389	-0.0052	0.0005	0.0005	-0.0052	-0.0108	0.0061	0.0286
225.0	-0.0276	-0.0108	-0.0108	-0.0052	-0.0052	-0.0052	0.0005	0.0342
247.5	-0.0109	-0.0053	-0.0053	0.0003	0.0003	0.0003	0.0003	0.0115
292.5	0.0003	-0.0053	0.0003	0.0003	0.0059	0.0059	0.0059	0.0227
315.0		-0.0053	0.0003	0.0003	0.0059	0.0059	0.0115	0.0453
337.5	0.0003	-0.0053	0.0003	0.0003	0.0059	0.0059	0.0115	

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=8.0°							
0.0	-0.0110	-0.0166	-0.0110	-0.0110	-0.0054	-0.0054	0.0003	0.0003
22.5	-0.0277	-0.0277	0.0003	-0.0222	-0.0222	-0.0166	-0.0110	-0.0054
45.0	-0.0277	-0.0277	-0.0277	-0.0222	-0.0277		-0.0222	0.0340
67.5	-0.0110	-0.0166	-0.0054	-0.0166	-0.0222	-0.0054		0.0171
112.5	-0.0054	-0.0054	0.0059	0.0003	0.0115	0.0059	0.0228	0.0452
135.0	-0.0277	0.0003	0.0171	0.0059	0.0228	0.0059	0.0396	0.0734
157.5	-0.0727	0.0059	0.0171	0.0171	0.0115	0.0003	0.0284	0.0340
180.0	-0.1121		0.0059	0.0003	0.0003	-0.0166	0.0115	0.0115
202.5	-0.0560	-0.0222	-0.0166	-0.0166	-0.0166	-0.0277	-0.0110	0.0115
225.0	-0.0502	-0.0335	-0.0335	-0.0277	-0.0277	-0.0277	-0.0222	0.0171
247.5	-0.0220	-0.0164	-0.0164	-0.0052	-0.0108	-0.0052	-0.0052	0.0005
292.5	-0.0052	-0.0052	-0.0052	-0.0052	-0.0052	-0.0052	-0.0052	0.0061
315.0		0.0005	0.0061	0.0061	0.0117	0.0005	0.0117	0.0567
337.5	-0.0052	-0.0108	-0.0108	-0.0052	0.0005	-0.0052	0.0005	
	α=12.0°							
0.0	-0.0164	-0.0164	-0.0164	-0.0164	-0.0164	-0.0164	-0.0108	-0.0052
22.5	-0.0445	-0.0389	-0.0108	-0.0389	-0.0333	-0.0276	-0.0164	-0.0220
45.0	-0.0558	-0.0558	-0.0501	-0.0501	-0.0501		-0.0445	0.0173
67.5	-0.0389	-0.0389	-0.0276	-0.0276	-0.0333	-0.0164		0.0061
112.5	0.0117	0.0117	0.0230	0.0173	0.0286	0.0286	0.0398	0.0678
135.0	-0.0052	0.0230	0.0398	0.0286	0.0453	0.0342	0.0623	0.0959
157.5	-0.0501	0.0173	0.0286	0.0342	0.0286	0.0173	0.0453	0.0511
180.0	-0.1176		0.0005	0.0005	-0.0052	-0.0220	0.0117	0.0061
202.5	-0.0726	-0.0389	-0.0333	-0.0445	-0.0389	-0.0501	-0.0333	-0.0108
225.0	-0.0670	-0.0558	-0.0614	-0.0558	-0.0558	-0.0558	-0.0389	-0.0108
247.5	-0.0276	-0.0220	-0.0220	-0.0164	-0.0220	-0.0164	-0.0164	-0.0220
292.5	-0.0333	-0.0389	-0.0333	-0.0389	-0.0333	-0.0333	-0.0333	-0.0164
315.0		-0.0052	0.0061	0.0005	0.0117	-0.0052	0.0061	0.0511
337.5	-0.0389	-0.0501	-0.0445	-0.0389	-0.0333	-0.0389	-0.0276	
	α=15.1°							
0.0	-0.0276	-0.0331	-0.0331	-0.0276	-0.0276	-0.0276	-0.0220	-0.0220
22.5	-0.0555	-0.0500	-0.0276	-0.0500	-0.0444	-0.0389	-0.0276	-0.0389
45.0	-0.0834	-0.0892	-0.0834	-0.0779	-0.0834		-0.0723	-0.0052
67.5	-0.0612	-0.0723	-0.0500	-0.0500	-0.0612	-0.0331		-0.0276
112.5	0.0172	0.0227	0.0338	0.0283	0.0394	0.0394	0.0506	0.0786
135.0	0.0114	0.0338	0.0506	0.0394	0.0562	0.0451	0.0786	0.1120
157.5	-0.0331	0.0172	0.0283	0.0338	0.0283	0.0227	0.0506	0.0562
180.0	-0.1337		-0.0165	-0.0165	-0.0220	-0.0331	0.0003	-0.0052
202.5	-0.0947	-0.0555	-0.0668	-0.0723	-0.0723	-0.0834	-0.0612	-0.0331
225.0	-0.0947	-0.0892	-0.0947	-0.0892	-0.0834	-0.0834	-0.0723	-0.0276
247.5	-0.0390	-0.0334	-0.0334	-0.0334	-0.0334	-0.0277	-0.0277	-0.0334
292.5	-0.0724	-0.0724	-0.0613	-0.0613	-0.0501	-0.0501	-0.0501	-0.0334
315.0		-0.0165	-0.0054	-0.0165	-0.0054	-0.0221	-0.0165	0.0393
337.5	-0.0668	-0.0724	-0.0557	-0.0445	-0.0334	-0.0445	-0.0277	

TABLE III.- Continued.

(d) $\phi = 45^{\circ}$; M = 0.95.

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=-2.1°							
0.0	-0.0030	-0.0030	-0.0030	0.0030	0.0030	0.0030	0.0147	0.0265
22.5	-0.0088	-0.0030	0.0265	-0.0030	0.0030	0.0030	0.0088	0.0324
45.0	-0.0030	-0.0030	-0.0030	0.0030	-0.0030		0.0088	0.0561
67.5	-0.0088	-0.0030	0.0030	-0.0030	-0.0030	0.0088		0.0207
112.5	-0.0207	-0.0088	0.0030	0.0030	0.0088	0.0030	0.0088	0.0384
135.0	-0.0324	-0.0030	0.0088	0.0030	0.0147	0.0030	0.0265	0.0501
157.5	-0.0561	0.0147	0.0088	0.0207	0.0088	0.0030	0.0207	0.0265
180.0	-0.0501		0.0030	0.0030	0.0088	-0.0030	0.0207	0.0147
202.5	-0.0442	-0.0030	0.0030	0.0030	0.0030	-0.0030	0.0147	0.0265
225.0	-0.0265	-0.0088	-0.0088	0.0030	-0.0030	0.0030	0.0088	0.0501
247.5	-0.0089	0.0030	0.0030	0.0089	-0.0028	0.0089	0.0089	0.0266
292.5	-0.0028	-0.0089	-0.0028	-0.0028	0.0030	0.0030	0.0147	0.0325
315.0		-0.0089	-0.0028	-0.0028	0.0089	-0.0028	0.0208	0.0678
337.5	-0.0028	-0.0089	-0.0028	0.0030	0.0089	0.0030	0.0208	
	α=0°							
0.0	0.0028	-0.0030	-0.0030	0.0089	0.0028	0.0089	0.0207	0.0267
22.5	-0.0030	-0.0030	0.0326	0.0028	0.0028	0.0089	0.0148	0.0326
45.0	-0.0030	0.0028	0.0028	0.0089	0.0028		0.0148	0.0623
67.5	-0.0030	0.0028	0.0089	0.0028	0.0028	0.0207		0.0385
112.5	-0.0208	-0.0089	0.0028	0.0028	0.0089	0.0028	0.0148	0.0445
135.0	-0.0328	0.0028	0.0089	0.0028	0.0089	0.0028	0.0326	0.0563
157.5	-0.0623	0.0148	0.0089	0.0207	0.0089	-0.0030	0.0207	0.0267
180.0	-0.0564		0.0089	0.0089	0.0089	-0.0030	0.0207	0.0207
202.5	-0.0445	-0.0030	0.0028	0.0028	0.0028	-0.0030	0.0148	0.0326
225.0	-0.0328	-0.0089	-0.0089	-0.0030	-0.0030	-0.0030	0.0089	0.0445
247.5	-0.0089	0.0030	0.0030	0.0148	0.0030	0.0148	0.0148	0.0327
292.5	-0.0030	-0.0089	0.0030	0.0030	0.0089	0.0089	0.0148	0.0386
315.0		-0.0030	0.0030	0.0030	0.0089	0.0030	0.0207	0.0623
337.5	0.0030	-0.0030	0.0030	0.0030	0.0148	0.0030	0.0207	
	α=2.0°							
0.0	-0.0032	-0.0090	-0.0032	0.0028	0.0028	0.0028	0.0145	0.0205
22.5	-0.0090	-0.0090	0.0264	-0.0032	-0.0032	0.0028	0.0087	0.0264
45.0	-0.0090	-0.0032	-0.0032	-0.0032	-0.0032		0.0087	0.0559
67.5	-0.0090	0.0028	0.0087	0.0028	-0.0032	0.0145		0.0322
112.5	-0.0209	-0.0090	0.0028	-0.0032	0.0087	0.0028	0.0087	0.0441
135.0	-0.0386	-0.0090	0.0087	-0.0090	0.0087	-0.0032	0.0322	0.0618
157.5	-0.0740	0.0087	0.0087	0.0205	0.0087	-0.0032	0.0205	0.0322
180.0	-0.0740		0.0145	0.0087	0.0087	-0.0032	0.0205	0.0205
202.5	-0.0444	-0.0032	0.0028	0.0028	0.0028	-0.0090	0.0145	0.0322
225.0	-0.0326	-0.0090	-0.0090	-0.0032	-0.0032	-0.0032	0.0087	0.0441
247.5	-0.0147	-0.0030	-0.0030	0.0030	-0.0030	0.0088	0.0088	0.0207
292.5	-0.0030	-0.0088	0.0030	-0.0030	0.0030	0.0088	0.0088	0.0265
315.0		-0.0088	-0.0030	0.0030	0.0088	0.0030	0.0147	0.0501
337.5	-0.0030	-0.0088	-0.0030	0.0030	0.0088	0.0030	0.0147	
	α=3.9°							
0.0	-0.0032	-0.0090	-0.0090	-0.0032	-0.0032	0.0028	0.0087	0.0145
22.5	-0.0149	-0.0090	0.0205	-0.0090	-0.0032	0.0028	0.0087	0.0205
45.0	-0.0090	-0.0032	-0.0090	-0.0032	-0.0090		-0.0032	0.0618
67.5	-0.0090	0.0028	0.0087	0.0028	-0.0032	0.0145		0.0322
112.5	-0.0209	-0.0090	0.0028	0.0028	0.0087	0.0028	0.0145	0.0499
135.0	-0.0386	-0.0032	0.0087	-0.0032	0.0145	-0.0032	0.0382	0.0676
157.5	-0.0798	0.0087	0.0145	0.0205	0.0087	-0.0032	0.0264	0.0382
180.0	-0.0975		0.0145	0.0087	0.0028	-0.0032	0.0205	0.0205
202.5	-0.0444	-0.0032	0.0028	-0.0032	-0.0032	-0.0149	0.0087	0.0322
225.0	-0.0326	-0.0090	-0.0149	-0.0032	-0.0090	-0.0032	0.0028	0.0382
247.5	-0.0147	-0.0028	-0.0028	0.0030	-0.0028	0.0030	0.0030	0.0147
292.5	-0.0028	-0.0089	0.0030	0.0030	0.0030	0.0089	0.0089	0.0266
315.0		-0.0028	0.0030	0.0030	0.0089	0.0030	0.0147	0.0503
337.5	-0.0028	-0.0028	-0.0028	0.0030	0.0089	0.0030	0.0147	

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=7.9°							
0.0	-0.0149	-0.0149	-0.0149	-0.0090	-0.0032	-0.0032	0.0028	0.0028
22.5	-0.0326	-0.0267	0.0028	-0.0209	-0.0209	-0.0149	-0.0090	0.0028
45.0	-0.0326	-0.0326	-0.0267	-0.0267	-0.0326		-0.0209	0.0441
67.5	-0.0209	-0.0090	-0.0032	-0.0090	-0.0209	-0.0090		0.0205
112.5	-0.0149	-0.0032	0.0145	0.0087	0.0205	0.0145	0.0264	0.0618
135.0	-0.0444	0.0028	0.0264	0.0028	0.0264	0.0087	0.0499	0.0853
157.5	-0.0917	0.0028	0.0145	0.0264	0.0145	-0.0032	0.0322	0.0382
180.0	-0.1448		0.0087	0.0028	-0.0032	-0.0149	0.0205	0.0145
202.5	-0.0563	-0.0209	-0.0149	-0.0149	-0.0209	-0.0267	-0.0090	0.0145
225.0	-0.0503	-0.0326	-0.0326	-0.0326	-0.0326	-0.0267	-0.0209	0.0205
247.5	-0.0265	-0.0147	-0.0147	-0.0089	-0.0147	-0.0028	-0.0028	0.0030
292.5	-0.0028	-0.0089	-0.0028	-0.0028	-0.0028	-0.0028	-0.0028	0.0089
315.0		-0.0028	0.0030	0.0030	0.0147	0.0030	0.0208	0.0620
337.5	-0.0089	-0.0089	-0.0089	-0.0028	0.0030	-0.0028	0.0030	
	α=11.9°							
0.0	-0.0150	-0.0150	-0.0150	-0.0089	-0.0089	-0.0089	-0.0030	-0.0030
22.5	-0.0506	-0.0386	-0.0030	-0.0328	-0.0328	-0.0208	-0.0150	-0.0150
45.0	-0.0623	-0.0564	-0.0564	-0.0506	-0.0564		-0.0445	0.0267
67.5	-0.0506	-0.0445	-0.0386	-0.0328	-0.0328	-0.0208		0.0089
112.5	0.0028	0.0148	0.0326	0.0267	0.0326	0.0267	0.0445	0.0801
135.0	-0.0208	0.0267	0.0445	0.0267	0.0504	0.0326	0.0801	0.1097
157.5	-0.0684	0.0148	0.0267	0.0445	0.0267	0.0148	0.0504	0.0623
180.0	-0.1574		0.0089	0.0028	-0.0030	-0.0208	0.0148	0.0148
202.5	-0.0623	-0.0328	-0.0328	-0.0445	-0.0386	-0.0564	-0.0328	-0.0089
225.0	-0.0684	-0.0564	-0.0684	-0.0623	-0.0623	-0.0506	-0.0386	0.0028
247.5	-0.0265	-0.0206	-0.0206	-0.0147	-0.0206	-0.0089	-0.0147	-0.0147
292.5	-0.0384	-0.0442	-0.0323	-0.0384	-0.0323	-0.0265	-0.0265	-0.0089
315.0		-0.0028	0.0089	0.0089	0.0147	0.0030	0.0147	0.0620
337.5	-0.0442	-0.0501	-0.0442	-0.0384	-0.0265	-0.0323	-0.0206	
	α=15.0°							
0.0	-0.0265	-0.0265	-0.0324	-0.0207	-0.0265	-0.0207	-0.0147	-0.0207
22.5	-0.0561	-0.0501	-0.0147	-0.0442	-0.0384	-0.0265	-0.0147	-0.0207
45.0	-0.0915	-0.0915	-0.0855	-0.0796	-0.0855		-0.0678	0.0088
67.5	-0.0561	-0.0738	-0.0501	-0.0561	-0.0619	-0.0384		-0.0265
112.5	0.0147	0.0265	0.0384	0.0324	0.0501	0.0442	0.0561	0.0973
135.0	0.0030	0.0442	0.0619	0.0442	0.0678	0.0561	0.0973	0.1327
157.5	-0.0442	0.0207	0.0384	0.0561	0.0384	0.0265	0.0619	0.0678
180.0	-0.1740		-0.0088	-0.0088	-0.0147	-0.0324	0.0088	0.0030
202.5	-0.0855	-0.0442	-0.0619	-0.0678	-0.0738	-0.0855	-0.0619	-0.0324
225.0	-0.0796	-0.0855	-0.1032	-0.0915	-0.0855	-0.0796	-0.0738	-0.0147
247.5	-0.0384	-0.0323	-0.0323	-0.0265	-0.0265	-0.0206	-0.0206	-0.0206
292.5	-0.0737	-0.0796	-0.0620	-0.0559	-0.0442	-0.0442	-0.0384	-0.0147
315.0		-0.0206	-0.0028	-0.0147	-0.0028	-0.0206	-0.0089	0.0442
337.5	-0.0678	-0.0678	-0.0501	-0.0384	-0.0265	-0.0384	-0.0265	

TABLE III.- Continued.

(e) $\phi = 45^{\circ}$; M = 1.00.

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=-2.0°							
0.0	0.0677	0.0550	0.0484	0.0550	0.0421	0.0421	0.0614	0.0807
22.5	0.0614	0.0550	0.0743	0.0484	0.0421	0.0484	0.0550	0.0870
45.0	0.0614	0.0550	0.0484	0.0484	0.0484		0.0550	0.1129
67.5	0.0550	0.0550	0.0550	0.0484	0.0421	0.0550		0.0743
112.5	0.0421	0.0484	0.0550	0.0550	0.0484	0.0484	0.0550	0.0936
135.0	0.0228	0.0550	0.0614	0.0421	0.0550	0.0357	0.0677	0.0936
157.5	0.0164	0.0743	0.0677	0.0677	0.0550	0.0421	0.0677	0.0743
180.0	0.0164		0.0614	0.0550	0.0484	0.0421	0.0677	0.0614
202.5	0.0098	0.0550	0.0550	0.0484	0.0484	0.0357	0.0550	0.0807
225.0	0.0291	0.0550	0.0484	0.0484	0.0421	0.0421	0.0550	0.1000
247.5	0.0483	0.0610	0.0546	0.0546	0.0417	0.0483	0.0417	0.0737
292.5	0.0610	0.0483	0.0483	0.0417	0.0483	0.0417	0.0483	0.0737
315.0		0.0483	0.0546	0.0417	0.0483	0.0354	0.0546	0.1185
337.5	0.0610	0.0483	0.0483	0.0483	0.0483	0.0354	0.0610	
	α=0°							
0.0	0.0677	0.0550	0.0484	0.0550	0.0484	0.0421	0.0614	0.0743
22.5	0.0614	0.0550	0.0743	0.0484	0.0484	0.0484	0.0614	0.0807
45.0	0.0614	0.0550	0.0484	0.0484	0.0484		0.0550	0.1129
67.5	0.0614	0.0550	0.0614	0.0550	0.0421	0.0614		0.0807
112.5	0.0357	0.0484	0.0550	0.0484	0.0550	0.0421	0.0614	0.0870
135.0	0.0228	0.0550	0.0614	0.0484	0.0550	0.0421	0.0677	0.1063
157.5	0.0098	0.0743	0.0677	0.0677	0.0550	0.0421	0.0677	0.0807
180.0	0.0098		0.0677	0.0614	0.0550	0.0421	0.0677	0.0677
202.5	0.0098	0.0614	0.0614	0.0550	0.0484	0.0421	0.0614	0.0807
225.0	0.0291	0.0550	0.0550	0.0484	0.0484	0.0421	0.0550	0.1000
247.5	0.0417	0.0546	0.0483	0.0546	0.0417	0.0483	0.0483	0.0673
292.5	0.0546	0.0483	0.0483	0.0417	0.0483	0.0417	0.0483	0.0737
315.0		0.0417	0.0483	0.0417	0.0483	0.0354	0.0546	0.1058
337.5	0.0610	0.0483	0.0483	0.0417	0.0483	0.0354	0.0546	
	α=1.9°							
0.0	0.0614	0.0550	0.0484	0.0550	0.0484	0.0421	0.0614	0.0677
22.5	0.0550	0.0550	0.0807	0.0484	0.0484	0.0484	0.0550	0.0743
45.0	0.0614	0.0614	0.0550	0.0484	0.0484		0.0550	0.1129
67.5	0.0677	0.0614	0.0677	0.0550	0.0421	0.0614		0.0870
112.5	0.0357	0.0550	0.0614	0.0484	0.0550	0.0421	0.0550	0.0936
135.0	0.0098	0.0614	0.0677	0.0484	0.0614	0.0421	0.0743	0.1129
157.5	-0.0029	0.0743	0.0743	0.0677	0.0550	0.0421	0.0677	0.0807
180.0	-0.0029		0.0807	0.0677	0.0614	0.0421	0.0677	0.0677
202.5	0.0098	0.0614	0.0614	0.0550	0.0484	0.0357	0.0550	0.0807
225.0	0.0291	0.0614	0.0550	0.0550	0.0484	0.0421	0.0550	0.1000
247.5	0.0484	0.0550	0.0550	0.0550	0.0420	0.0550	0.0484	0.0678
292.5	0.0614	0.0550	0.0614	0.0484	0.0550	0.0484	0.0550	0.0805
315.0		0.0550	0.0550	0.0484	0.0550	0.0420	0.0614	0.0999
337.5	0.0678	0.0550	0.0550	0.0550	0.0550	0.0484	0.0614	

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=3.9°							
0.0	0.0614	0.0550	0.0484	0.0484	0.0420	0.0484	0.0550	0.0678
22.5	0.0484	0.0484	0.0742	0.0420	0.0420	0.0420	0.0484	0.0742
45.0	0.0614	0.0550	0.0550	0.0484	0.0420		0.0420	0.1257
67.5	0.0678	0.0614	0.0742	0.0550	0.0420	0.0614		0.0935
112.5	0.0356	0.0550	0.0678	0.0550	0.0550	0.0484	0.0614	0.0999
135.0	-0.0029	0.0678	0.0742	0.0550	0.0614	0.0420	0.0805	0.1257
157.5	-0.0159	0.0742	0.0742	0.0742	0.0614	0.0420	0.0742	0.0871
180.0	-0.0287		0.0805	0.0614	0.0550	0.0356	0.0678	0.0678
202.5	0.0099	0.0614	0.0614	0.0550	0.0484	0.0292	0.0550	0.0871
225.0	0.0227	0.0550	0.0484	0.0420	0.0356	0.0420	0.0484	0.0935
247.5	0.0422	0.0552	0.0486	0.0486	0.0422	0.0486	0.0486	0.0616
292.5	0.0616	0.0552	0.0616	0.0552	0.0552	0.0552	0.0552	0.0744
315.0		0.0552	0.0552	0.0486	0.0552	0.0486	0.0616	0.1001
337.5	0.0616	0.0552	0.0486	0.0486	0.0486	0.0422	0.0616	
	α=8.0°							
0.0	0.0486	0.0422	0.0422	0.0422	0.0422	0.0422	0.0552	0.0552
22.5	0.0358	0.0358	0.0616	0.0294	0.0229	0.0294	0.0422	0.0552
45.0	0.0358	0.0358	0.0358	0.0294	0.0229		0.0229	0.1065
67.5	0.0552	0.0486	0.0616	0.0422	0.0294	0.0358		0.0680
112.5	0.0101	0.0616	0.0808	0.0680	0.0744	0.0616	0.0744	0.1195
135.0	-0.0608	0.0808	0.1001	0.0744	0.0873	0.0616	0.1001	0.1516
157.5	-0.0672	0.0744	0.0937	0.0873	0.0680	0.0486	0.0873	0.1001
180.0	-0.0930		0.0744	0.0680	0.0616	0.0358	0.0744	0.0680
202.5	-0.0414	0.0552	0.0552	0.0422	0.0358	0.0229	0.0422	0.0680
225.0	0.0101	0.0422	0.0294	0.0294	0.0229	0.0229	0.0294	0.0808
247.5	0.0358	0.0486	0.0486	0.0486	0.0358	0.0422	0.0422	0.0552
292.5	0.0616	0.0616	0.0616	0.0486	0.0486	0.0486	0.0486	0.0616
315.0		0.0616	0.0680	0.0552	0.0680	0.0552	0.0680	0.1259
337.5	0.0552	0.0486	0.0486	0.0486	0.0486	0.0422	0.0486	
	α=14.9°							
0.0	0.0291	0.0291	0.0291	0.0357	0.0291	0.0291	0.0421	0.0421
22.5	0.0164	0.0228	0.0421	0.0098	0.0164	0.0228	0.0357	0.0357
45.0	-0.0095	-0.0158	-0.0158	-0.0158	-0.0222		-0.0158	0.0743
67.5	-0.0222	-0.0158	-0.0158	0.0035	0.0164	0.0357		0.0421
112.5	-0.0222	0.0743	0.1129	0.1063	0.1193	0.1063	0.1193	0.1579
135.0	-0.0866	0.0807	0.1386	0.1256	0.1386	0.1193	0.1579	0.2028
157.5	-0.0994	0.0614	0.1129	0.1256	0.1063	0.0870	0.1256	0.1322
180.0	-0.1573		0.0677	0.0614	0.0484	0.0164	0.0677	0.0550
202.5	-0.1573	0.0164	0.0164	-0.0029	-0.0158	-0.0415	-0.0158	0.0228
225.0	-0.0288	-0.0029	-0.0288	-0.0351	-0.0351	-0.0288	-0.0222	0.0484
247.5	0.0098	0.0227	0.0227	0.0290	0.0227	0.0290	0.0290	0.0290
292.5	-0.0221	-0.0221	-0.0029	-0.0092	0.0035	0.0035	0.0035	0.0354
315.0		0.0417	0.0610	0.0354	0.0483	0.0227	0.0417	0.1185
337.5	-0.0285	-0.0348	-0.0221	-0.0092	0.0035	-0.0092	0.0098	

TABLE III.- Concluded.

(f) $\phi = 45^{\circ}$; M = 1.03.

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	$\alpha=0°$							
0.0	-0.0218	-0.0218	-0.0218	-0.0218	-0.0418	-0.0418	0.0119	0.1123
22.5	-0.0284	-0.0218	0.0119	-0.0351	-0.0418	-0.0351	0.0119	0.1190
45.0	-0.0149	-0.0218	-0.0284	-0.0284	-0.0351		0.0050	0.1458
67.5	-0.0083	-0.0218	-0.0218	-0.0284	-0.0418	-0.0149		0.1257
112.5	-0.0619	-0.0619	-0.0284	-0.0351	-0.0284	-0.0351	0.0186	0.1325
135.0	-0.1222	-0.0484	-0.0218	-0.0418	-0.0218	-0.0351	0.0319	0.1392
157.5	-0.0821	-0.0284	-0.0149	-0.0083	-0.0218	-0.0351	0.0319	0.1190
180.0	-0.0821		-0.0149	-0.0149	-0.0218	-0.0418	0.0252	0.1123
202.5	-0.1156	-0.0418	-0.0149	-0.0149	-0.0351	-0.0418	0.0186	0.1190
225.0	-0.0619	-0.0553	-0.0351	-0.0218	-0.0351	-0.0351	0.0050	0.1325
247.5	-0.0351	-0.0484	-0.0351	-0.0149	-0.0418	-0.0284	-0.0016	0.1123
292.5	-0.0284	-0.0284	-0.0218	-0.0418	-0.0284	-0.0351	-0.0016	0.1123
315.0		-0.0284	-0.0149	-0.0418	-0.0284	-0.0484	0.0119	0.1458
337.5	-0.0284	-0.0284	-0.0218	-0.0284	-0.0351	-0.0484	0.0119	
	$\alpha=2.0°$							
0.0	-0.0216	-0.0216	-0.0284	-0.0351	-0.0417	-0.0150	0.0847	0.1248
22.5	-0.0284	-0.0216	0.0050	-0.0417	-0.0483	-0.0150	0.0781	0.1314
45.0	-0.0216	-0.0284	-0.0351	-0.0417	-0.0483		0.0715	0.1647
67.5	-0.0084	-0.0216	-0.0216	-0.0351	-0.0483	-0.0084		0.1446
112.5	-0.0617	-0.0683	-0.0351	-0.0417	-0.0284	-0.0284	0.0515	0.1446
135.0	-0.1348	-0.0549	-0.0216	-0.0483	-0.0216	-0.0284	0.0649	0.1647
157.5	-0.0950	-0.0417	-0.0150	-0.0150	-0.0216	-0.0284	0.0649	0.1380
180.0	-0.0815		-0.0150	-0.0150	-0.0216	-0.0351	0.0715	0.1248
202.5	-0.1282	-0.0417	-0.0216	-0.0216	-0.0351	-0.0351	0.0649	0.1380
225.0	-0.0815	-0.0549	-0.0351	-0.0284	-0.0417	-0.0284	0.0715	0.1514
247.5	-0.0483	-0.0483	-0.0351	-0.0284	-0.0417	-0.0084	0.0649	0.1180
292.5	-0.0216	-0.0351	-0.0284	-0.0483	-0.0351	-0.0150	0.0781	0.1314
315.0		-0.0284	-0.0216	-0.0417	-0.0351	-0.0150	0.0847	0.1514
337.5	-0.0284	-0.0284	-0.0351	-0.0417	-0.0417	-0.0150	0.0847	

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	$\alpha=4.0°$							
0.0	-0.0286	-0.0220	-0.0286	-0.0353	-0.0419	-0.0286	0.0585	0.1188
22.5	-0.0353	-0.0286	-0.0018	-0.0486	-0.0486	-0.0353	0.0317	0.1188
45.0	-0.0220	-0.0286	-0.0419	-0.0419	-0.0486		-0.0085	0.1724
67.5	-0.0085	-0.0286	-0.0220	-0.0353	-0.0419	-0.0151		0.1323
112.5	-0.0621	-0.0754	-0.0353	-0.0419	-0.0220	-0.0286	-0.0085	0.1323
135.0	-0.1426	-0.0621	-0.0151	-0.0486	-0.0151	-0.0286	0.0048	0.1522
157.5	-0.1022	-0.0486	-0.0151	-0.0151	-0.0220	-0.0286	0.0048	0.1188
180.0	-0.0889		-0.0151	-0.0220	-0.0286	-0.0419	0.0048	0.1055
202.5	-0.1357	-0.0486	-0.0286	-0.0286	-0.0353	-0.0555	0.0048	0.1254
225.0	-0.1022	-0.0555	-0.0353	-0.0286	-0.0419	-0.0419	0.0117	0.1389
247.5	-0.0619	-0.0553	-0.0352	-0.0285	-0.0418	-0.0285	0.0318	0.1055
292.5	-0.0217	-0.0352	-0.0217	-0.0352	-0.0352	-0.0217	0.0519	0.1256
315.0		-0.0285	-0.0217	-0.0352	-0.0285	-0.0217	0.0653	0.1391
337.5	-0.0217	-0.0217	-0.0285	-0.0352	-0.0352	-0.0217	0.0587	

TABLE IV.- BODY STATIC-PRESSURE ERROR COEFFICIENTS $(p - p_\infty)/p_\infty$ WITH BLEED AIR.

(a) $\phi = 45^\circ$; M = 0.70.

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=2.0°; w=0.018							
0.0	-0.0061	-0.0061	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015	0.0078
22.5	-0.0107	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015	-0.0015	0.0078
45.0	-0.0061	-0.0061	-0.0061	-0.0061	-0.0061	0.0032	-0.0015	0.0215
67.5	-0.0061	-0.0107	-0.0061	-0.0061	-0.0061	-0.0015	-0.0015	0.0032
112.5	-0.0152	-0.0152	-0.0107	-0.0061	-0.0061	-0.0061	-0.0015	0.0078
135.0	-0.0152	-0.0107	-0.0061	-0.0107	-0.0061	-0.0061	0.0032	0.0123
157.5	-0.0061	-0.0015	-0.0015	-0.0015	-0.0061	-0.0061	-0.0015	0.0032
180.0	-0.0199	-0.0061	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015	-0.0015
202.5	-0.0199	-0.0107	-0.0061	-0.0061	-0.0061	-0.0107	-0.0061	0.0032
225.0	-0.0152	-0.0107	-0.0107	-0.0061	-0.0107	-0.0061	-0.0061	0.0123
247.5	-0.0107	-0.0061	-0.0061	-0.0015	-0.0061	-0.0015	-0.0061	0.0032
292.5	-0.0107	-0.0107	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015	0.0032
315.0		-0.0107	-0.0061	-0.0061	-0.0015	-0.0061	0.0032	0.0261
337.5	-0.0061	-0.0107	-0.0107	-0.0061	-0.0015	-0.0061	-0.0015	
	α=0°; w=0.018							
0.0	-0.0061	-0.0061	-0.0061	-0.0015	-0.0015	-0.0015	0.0031	0.0078
22.5	-0.0061	-0.0061	-0.0015	-0.0015	-0.0015	-0.0015	0.0031	0.0078
45.0	-0.0015	-0.0015	-0.0015	-0.0015	-0.0015	0.0078	0.0031	0.0262
67.5	-0.0061	-0.0015	-0.0015	-0.0015	-0.0015	0.0031	0.0031	0.0078
112.5	-0.0061	-0.0107	-0.0061	-0.0015	-0.0015	-0.0015	0.0031	0.0124
135.0	-0.0154	-0.0061	-0.0015	-0.0015	-0.0015	-0.0061	0.0078	0.0170
157.5	-0.0061	-0.0015	-0.0015	0.0031	-0.0015	-0.0015	0.0031	0.0078
180.0	-0.0154	0.0031	-0.0015	0.0031	0.0031	-0.0015	0.0031	0.0031
202.5	-0.0154	-0.0061	-0.0015	-0.0015	-0.0015	-0.0015	0.0031	0.0124
225.0	-0.0107	-0.0061	-0.0061	-0.0061	-0.0015	-0.0015	0.0031	0.0216
247.5	-0.0061	-0.0061	-0.0015	-0.0015	-0.0015	-0.0015	-0.0015	0.0078
292.5	-0.0061	-0.0061	-0.0015	-0.0015	-0.0015	-0.0015	0.0031	0.0078
315.0		-0.0061	-0.0015	-0.0015	-0.0015	-0.0015	0.0031	0.0262
337.5	-0.0015	-0.0061	-0.0015	-0.0015	0.0031	-0.0015	0.0031	
	α=-2.0°; w=0.019							
0.0	-0.0061	-0.0107	-0.0107	-0.0061	-0.0061	-0.0061	-0.0015	0.0032
22.5	-0.0107	-0.0107	-0.0015	-0.0107	-0.0061	-0.0061	-0.0015	0.0032
45.0	-0.0061	-0.0061	-0.0061	-0.0061	-0.0061	0.0032	-0.0015	0.0215
67.5	-0.0061	-0.0061	-0.0015	-0.0061	-0.0061	-0.0015	-0.0015	0.0078
112.5	-0.0107	-0.0107	-0.0107	-0.0061	-0.0061	-0.0061	-0.0015	0.0078
135.0	-0.0152	-0.0107	-0.0061	-0.0107	-0.0061	-0.0061	0.0032	0.0215
157.5	-0.0107	-0.0015	-0.0061	-0.0015	-0.0061	-0.0061	0.0032	0.0032
180.0	-0.0152	0.0032	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015	-0.0015
202.5	-0.0199	-0.0107	-0.0061	-0.0061	-0.0061	-0.0107	-0.0015	0.0032
225.0	-0.0152	-0.0107	-0.0107	-0.0107	-0.0107	-0.0107	-0.0061	0.0123
247.5	-0.0152	-0.0107	-0.0107	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015
292.5	-0.0107	-0.0107	-0.0061	-0.0061	-0.0061	-0.0061	-0.0061	0.0032
315.0		-0.0107	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015	0.0169
337.5	-0.0061	-0.0107	-0.0107	-0.0061	-0.0061	-0.0061	-0.0015	
	α=4.0°; w=0.018							
0.0	-0.0014	-0.0060	-0.0060	-0.0014	-0.0014	-0.0014	0.0032	0.0032
22.5	-0.0108	-0.0108	-0.0014	-0.0060	-0.0060	-0.0014	-0.0014	0.0032
45.0	-0.0060	-0.0060	-0.0060	-0.0014	-0.0014	0.0032	-0.0014	0.0264
67.5	-0.0014	-0.0060	-0.0014	-0.0014	-0.0014	0.0032	0.0032	0.0078
112.5	-0.0060	-0.0060	-0.0014	-0.0014	0.0032	0.0032	0.0032	0.0172
135.0	-0.0108	-0.0014	0.0032	-0.0014	0.0032	0.0032	0.0126	0.0310
157.5	-0.0060	0.0032	0.0032	0.0032	0.0032	0.0032	0.0078	0.0126
180.0	-0.0060	0.0126	0.0032	0.0032	0.0032	-0.0014	0.0078	0.0032
202.5	-0.0154	-0.0060	-0.0060	-0.0060	-0.0014	-0.0060	-0.0014	0.0078
225.0	-0.0154	-0.0108	-0.0060	-0.0060	-0.0060	-0.0060	-0.0014	0.0172
247.5	-0.0153	-0.0107	-0.0107	-0.0061	-0.0107	-0.0061	-0.0061	-0.0061
292.5	-0.0107	-0.0061	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015	0.0032
315.0		-0.0107	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015	0.0170
337.5	-0.0107	-0.0107	-0.0107	-0.0061	-0.0061	-0.0061	-0.0015	

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=8.0°; w=0.018							
0.0	-0.0107	-0.0107	-0.0107	-0.0107	-0.0107	-0.0107	-0.0061	-0.0015
22.5	-0.0200	-0.0154	-0.0107	-0.0154	-0.0154	-0.0154	-0.0107	-0.0107
45.0	-0.0200	-0.0200	-0.0200	-0.0154	-0.0154	-0.0107	-0.0154	0.0124
67.5	-0.0061	-0.0107	-0.0061	-0.0107	-0.0107	-0.0061	-0.0061	0.0031
112.5	-0.0015	-0.0015	0.0031	0.0031	0.0078	0.0078	0.0124	0.0216
135.0	-0.0061	0.0031	0.0078	0.0031	0.0124	0.0078	0.0216	0.0355
157.5	-0.0107	-0.0015	0.0031	0.0078	0.0031	0.0031	0.0124	0.0124
180.0	-0.0246	0.0031	-0.0015	-0.0015	-0.0015	-0.0061	0.0031	0.0031
202.5	-0.0292	-0.0200	-0.0154	-0.0154	-0.0154	-0.0154	-0.0107	-0.0015
225.0	-0.0292	-0.0246	-0.0200	-0.0200	-0.0200	-0.0200	-0.0154	-0.0015
247.5	-0.0199	-0.0153	-0.0153	-0.0107	-0.0153	-0.0107	-0.0107	-0.0107
292.5	-0.0107	-0.0107	-0.0107	-0.0107	-0.0107	-0.0107	-0.0107	-0.0061
315.0		-0.0061	-0.0015	-0.0015	-0.0015	-0.0061	0.0032	0.0215
337.5	-0.0061	-0.0107	-0.0107	-0.0061	-0.0061	-0.0107	-0.0061	
	α=12.0°; w=0.018							
0.0	-0.0154	-0.0154	-0.0154	-0.0154	-0.0154	-0.0154	-0.0154	-0.0154
22.5	-0.0338	-0.0292	-0.0246	-0.0292	-0.0292	-0.0246	-0.0246	-0.0292
45.0	-0.0385	-0.0385	-0.0385	-0.0385	-0.0385	-0.0292	-0.0338	-0.0061
67.5	-0.0246	-0.0292	-0.0246	-0.0200	-0.0200	-0.0154	-0.0154	-0.0061
112.5	0.0078	0.0031	0.0078	0.0124	0.0170	0.0170	0.0216	0.0309
135.0	0.0078	0.0124	0.0170	0.0170	0.0262	0.0170	0.0355	0.0494
157.5	-0.0061	0.0078	0.0078	0.0124	0.0078	0.0078	0.0170	0.0216
180.0	-0.0338	0.0031	-0.0107	-0.0107	-0.0107	-0.0154	-0.0015	-0.0061
202.5	-0.0431	-0.0338	-0.0292	-0.0338	-0.0292	-0.0385	-0.0292	-0.0200
225.0	-0.0477	-0.0431	-0.0431	-0.0431	-0.0431	-0.0431	-0.0338	-0.0246
247.5	-0.0291	-0.0245	-0.0245	-0.0245	-0.0245	-0.0245	-0.0245	-0.0337
292.5	-0.0337	-0.0337	-0.0337	-0.0382	-0.0337	-0.0337	-0.0382	-0.0291
315.0		-0.0107	-0.0061	-0.0107	-0.0061	-0.0152	-0.0107	0.0123
337.5	-0.0291	-0.0382	-0.0337	-0.0337	-0.0337	-0.0382	-0.0291	
	α=15.0°; w=0.018							
0.0	-0.0245	-0.0245	-0.0291	-0.0245	-0.0291	-0.0291	-0.0245	-0.0245
22.5	-0.0382	-0.0382	-0.0337	-0.0382	-0.0382	-0.0337	-0.0337	-0.0429
45.0	-0.0566	-0.0566	-0.0566	-0.0566	-0.0566	-0.0521	-0.0566	-0.0291
67.5	-0.0382	-0.0475	-0.0337	-0.0337	-0.0382	-0.0291	-0.0291	-0.0245
112.5	0.0078	0.0078	0.0123	0.0169	0.0215	0.0215	0.0262	0.0353
135.0	0.0123	0.0215	0.0262	0.0215	0.0307	0.0262	0.0399	0.0583
157.5	-0.0061	0.0078	0.0123	0.0123	0.0123	0.0123	0.0215	0.0262
180.0	-0.0521	-0.0015	-0.0199	-0.0199	-0.0199	-0.0245	-0.0107	-0.0152
202.5	-0.0659	-0.0521	-0.0521	-0.0521	-0.0521	-0.0566	-0.0475	-0.0337
225.0	-0.0705	-0.0659	-0.0659	-0.0659	-0.0614	-0.0614	-0.0566	-0.0429
247.5	-0.0335	-0.0289	-0.0289	-0.0289	-0.0289	-0.0335	-0.0335	-0.0426
292.5	-0.0564	-0.0564	-0.0564	-0.0519	-0.0473	-0.0473	-0.0473	-0.0426
315.0		-0.0198	-0.0152	-0.0198	-0.0152	-0.0289	-0.0243	0.0032
337.5	-0.0564	-0.0564	-0.0519	-0.0426	-0.0380	-0.0426	-0.0380	

TABLE IV.- Continued.

(b) $\phi = 45^{\circ}$; $\overline{M} = 0.80$

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=-2.0°; w=0.019							
0.0	-0.0067	-0.0067	-0.0067	-0.0067	-0.0067	-0.0017	0.0034	0.0136
22.5	-0.0067	-0.0067	-0.0017	-0.0067	-0.0067	-0.0017	-0.0017	0.0136
45.0	-0.0067	-0.0067	-0.0067	-0.0067	-0.0067	0.0034	0.0034	0.0287
67.5	-0.0067	-0.0067	-0.0067	-0.0067	-0.0067	0.0034	0.0034	0.0084
112.5	-0.0119	-0.0119	-0.0067	-0.0067	-0.0017	-0.0017	0.0034	0.0136
135.0	-0.0169	-0.0119	-0.0067	-0.0067	-0.0017	-0.0067	0.0084	0.0236
157.5	-0.0169	-0.0017	-0.0017	0.0034	-0.0017	-0.0067	0.0034	0.0084
180.0	-0.0320	-0.0017	-0.0067	-0.0017	-0.0017	-0.0067	0.0034	-0.0017
202.5	-0.0270	-0.0119	-0.0067	-0.0067	-0.0067	-0.0067	-0.0017	0.0084
225.0	-0.0169	-0.0119	-0.0067	-0.0067	-0.0067	-0.0067	-0.0017	0.0236
247.5	-0.0119	-0.0018	-0.0018	0.0032	-0.0069	0.0032	-0.0018	0.0083
292.5	-0.0069	-0.0069	-0.0018	-0.0018	-0.0018	-0.0018	0.0032	0.0135
315.0		-0.0069	-0.0018	-0.0018	0.0032	-0.0018	0.0083	0.0367
337.5	-0.0018	-0.0069	-0.0069	-0.0018	0.0032	-0.0018	0.0083	
	α=0°; w=0.019							
0.0	-0.0014	-0.0066	-0.0066	-0.0014	-0.0014	-0.0014	0.0037	0.0138
22.5	-0.0066	-0.0066	0.0037	-0.0066	-0.0066	-0.0014	0.0037	0.0138
45.0	-0.0014	-0.0014	-0.0014	-0.0014	-0.0014	0.0087	0.0037	0.0342
67.5	-0.0066	-0.0066	-0.0014	-0.0014	-0.0014	0.0037	0.0037	0.0138
112.5	-0.0117	-0.0117	-0.0066	-0.0066	-0.0014	-0.0014	0.0037	0.0138
135.0	-0.0167	-0.0117	-0.0014	-0.0066	0.0037	-0.0066	0.0087	0.0291
157.5	-0.0167	-0.0014	-0.0014	0.0037	-0.0014	-0.0014	0.0087	0.0087
180.0	-0.0268	0.0037	-0.0014	-0.0014	0.0037	-0.0014	0.0087	0.0037
202.5	-0.0218	-0.0066	-0.0014	-0.0014	-0.0014	-0.0066	0.0037	0.0138
225.0	-0.0167	-0.0066	-0.0066	-0.0014	-0.0014	-0.0014	0.0037	0.0291
247.5	-0.0119	-0.0069	-0.0069	-0.0018	-0.0069	-0.0018	-0.0018	0.0083
292.5	-0.0069	-0.0069	-0.0069	-0.0069	-0.0018	-0.0018	0.0032	0.0135
315.0		-0.0069	-0.0018	-0.0018	0.0032	-0.0018	0.0083	0.0337
337.5	-0.0018	-0.0069	-0.0069	-0.0018	0.0032	-0.0018	0.0083	
	α=2.0°; w=0.019							
0.0	-0.0066	-0.0066	-0.0066	-0.0066	-0.0066	-0.0014	0.0037	0.0087
22.5	-0.0066	-0.0066	-0.0014	-0.0066	-0.0066	-0.0014	0.0037	0.0087
45.0	-0.0066	-0.0066	-0.0066	-0.0014	-0.0014	0.0087	0.0037	0.0342
67.5	-0.0066	-0.0014	-0.0014	-0.0014	-0.0014	0.0087	0.0037	0.0138
112.5	-0.0117	-0.0117	-0.0014	-0.0014	0.0037	-0.0014	0.0037	0.0190
135.0	-0.0218	-0.0066	-0.0014	-0.0066	0.0037	-0.0014	0.0138	0.0342
157.5	-0.0167	-0.0014	-0.0014	0.0037	-0.0014	-0.0066	0.0087	0.0138
180.0	-0.0218	0.0087	0.0037	0.0037	0.0037	-0.0014	0.0087	0.0037
202.5	-0.0268	-0.0066	-0.0014	-0.0014	-0.0014	-0.0066	0.0037	0.0138
225.0	-0.0167	-0.0066	-0.0066	-0.0066	-0.0066	-0.0014	-0.0014	0.0241
247.5	-0.0119	-0.0069	-0.0069	-0.0069	-0.0069	-0.0018	-0.0018	0.0032
292.5	-0.0069	-0.0069	-0.0069	-0.0069	-0.0018	-0.0018	-0.0018	0.0135
315.0		-0.0119	-0.0069	-0.0069	-0.0018	-0.0069	0.0032	0.0286
337.5	-0.0069	-0.0119	-0.0069	-0.0069	-0.0018	-0.0069	0.0032	
	α=4.0°; w=0.019							
0.0	-0.0119	-0.0119	-0.0119	-0.0067	-0.0067	-0.0067	-0.0017	0.0034
22.5	-0.0119	-0.0119	-0.0067	-0.0119	-0.0119	-0.0067	-0.0017	0.0034
45.0	-0.0119	-0.0119	-0.0119	-0.0067	-0.0119	0.0034	-0.0067	0.0337
67.5	-0.0067	-0.0067	-0.0017	-0.0067	-0.0067	0.0034	0.0034	0.0136
112.5	-0.0119	-0.0119	-0.0067	-0.0067	0.0034	-0.0017	0.0034	0.0186
135.0	-0.0169	-0.0067	-0.0017	-0.0067	0.0034	-0.0017	0.0136	0.0389
157.5	-0.0220	-0.0017	-0.0017	0.0034	-0.0017	-0.0017	0.0084	0.0136
180.0	-0.0320	0.0136	-0.0017	-0.0017	-0.0017	-0.0067	0.0034	0.0034
202.5	-0.0320	-0.0169	-0.0119	-0.0119	-0.0119	-0.0119	-0.0067	0.0084
225.0	-0.0270	-0.0169	-0.0169	-0.0119	-0.0119	-0.0119	-0.0067	0.0186
247.5	-0.0170	-0.0119	-0.0069	-0.0069	-0.0069	-0.0018	-0.0069	-0.0018
292.5	-0.0069	-0.0069	-0.0069	-0.0018	-0.0018	-0.0018	-0.0018	0.0083
315.0		-0.0069	-0.0018	-0.0018	-0.0018	-0.0018	0.0032	0.0286
337.5	-0.0069	-0.0069	-0.0069	-0.0069	-0.0018	-0.0018	0.0032	

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=8.0°; w=0.019							
0.0	-0.0120	-0.0120	-0.0120	-0.0120	-0.0069	-0.0069	-0.0069	-0.0017
22.5	-0.0221	-0.0221	-0.0170	-0.0221	-0.0221	-0.0170	-0.0120	-0.0120
45.0	-0.0221	-0.0221	-0.0221	-0.0221	-0.0221	-0.0120	-0.0170	0.0187
67.5	-0.0069	-0.0120	-0.0069	-0.0120	-0.0120	-0.0069	-0.0069	0.0084
112.5	-0.0017	-0.0017	0.0034	0.0034	0.0084	0.0084	0.0135	0.0339
135.0	-0.0069	0.0034	0.0135	0.0084	0.0187	0.0084	0.0288	0.0492
157.5	-0.0221	0.0034	0.0084	0.0135	0.0084	0.0034	0.0187	0.0187
180.0	-0.0475	0.0084	-0.0017	-0.0017	-0.0017	-0.0069	0.0084	0.0034
202.5	-0.0425	-0.0221	-0.0221	-0.0221	-0.0170	-0.0221	-0.0120	0.0034
225.0	-0.0374	-0.0271	-0.0271	-0.0271	-0.0271	-0.0271	-0.0170	0.0034
247.5	-0.0269	-0.0219	-0.0219	-0.0169	-0.0219	-0.0169	-0.0169	-0.0169
292.5	-0.0169	-0.0169	-0.0169	-0.0169	-0.0119	-0.0169	-0.0169	-0.0069
315.0		-0.0119	-0.0069	-0.0069	-0.0018	-0.0069	0.0032	0.0285
337.5	-0.0169	-0.0169	-0.0169	-0.0119	-0.0119	-0.0169	-0.0119	
	α=12.0°; w=0.018							
0.0	-0.0220	-0.0220	-0.0220	-0.0169	-0.0169	-0.0169	-0.0169	-0.0169
22.5	-0.0423	-0.0372	-0.0320	-0.0372	-0.0372	-0.0320	-0.0270	-0.0320
45.0	-0.0523	-0.0523	-0.0473	-0.0473	-0.0473	-0.0372	-0.0473	-0.0017
67.5	-0.0372	-0.0372	-0.0320	-0.0320	-0.0270	-0.0220	-0.0169	-0.0067
112.5	0.0034	0.0034	0.0084	0.0136	0.0186	0.0186	0.0236	0.0389
135.0	0.0034	0.0136	0.0186	0.0186	0.0287	0.0236	0.0389	0.0642
157.5	-0.0220	0.0034	0.0084	0.0136	0.0136	0.0084	0.0236	0.0287
180.0	-0.0625	0.0034	-0.0067	-0.0119	-0.0119	-0.0220	-0.0017	-0.0067
202.5	-0.0625	-0.0423	-0.0372	-0.0423	-0.0372	-0.0423	-0.0372	-0.0220
225.0	-0.0625	-0.0523	-0.0523	-0.0523	-0.0523	-0.0473	-0.0423	-0.0169
247.5	-0.0321	-0.0220	-0.0220	-0.0220	-0.0220	-0.0220	-0.0220	-0.0321
292.5	-0.0373	-0.0373	-0.0321	-0.0373	-0.0321	-0.0321	-0.0321	-0.0220
315.0		-0.0069	0.0032	-0.0069	-0.0018	-0.0119	-0.0018	0.0286
337.5	-0.0321	-0.0424	-0.0373	-0.0373	-0.0321	-0.0373	-0.0321	
	α=14.9°; w=0.018							
0.0	-0.0271	-0.0271	-0.0321	-0.0271	-0.0321	-0.0321	-0.0271	-0.0271
22.5	-0.0473	-0.0473	-0.0372	-0.0473	-0.0473	-0.0372	-0.0372	-0.0423
45.0	-0.0727	-0.0727	-0.0727	-0.0676	-0.0727	-0.0575	-0.0676	-0.0220
67.5	-0.0524	-0.0625	-0.0473	-0.0473	-0.0473	-0.0321	-0.0321	-0.0321
112.5	0.0084	0.0084	0.0135	0.0185	0.0236	0.0236	0.0337	0.0490
135.0	0.0135	0.0236	0.0287	0.0287	0.0388	0.0337	0.0540	0.0743
157.5	-0.0169	0.0033	0.0135	0.0185	0.0135	0.0135	0.0287	0.0287
180.0	-0.0929	-0.0017	-0.0220	-0.0220	-0.0271	-0.0321	-0.0119	-0.0169
202.5	-0.0829	-0.0625	-0.0676	-0.0625	-0.0676	-0.0727	-0.0625	-0.0423
225.0	-0.0929	-0.0829	-0.0829	-0.0829	-0.0777	-0.0777	-0.0727	-0.0423
247.5	-0.0373	-0.0321	-0.0321	-0.0271	-0.0271	-0.0321	-0.0321	-0.0373
292.5	-0.0676	-0.0626	-0.0575	-0.0575	-0.0474	-0.0474	-0.0474	-0.0373
315.0		-0.0119	-0.0069	-0.0119	-0.0119	-0.0220	-0.0170	0.0185
337.5	-0.0626	-0.0676	-0.0525	-0.0424	-0.0373	-0.0424	-0.0321	

TABLE IV.- Continued.

(c) $\phi = 45^{\circ}$; M = 0.90.

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=-2.0°; w=0.019							
0.0	-0.0049	-0.0049	-0.0105	0.0008	0.0008	0.0008	0.0120	0.0234
22.5	-0.0049	-0.0049	0.0008	-0.0049	-0.0049	0.0008	0.0064	0.0234
45.0	-0.0049	-0.0049	-0.0049	-0.0049	-0.0049	0.0176	0.0064	0.0514
67.5	-0.0049	-0.0049	0.0008	0.0008	0.0008	0.0064	0.0120	0.0176
112.5	-0.0161	-0.0105	-0.0049	0.0008	0.0064	0.0064	0.0064	0.0289
135.0	-0.0217	-0.0049	0.0008	0.0008	0.0064	0.0008	0.0176	0.0401
157.5	-0.0272	0.0064	0.0064	0.0064	0.0064	0.0008	0.0120	0.0176
180.0	-0.0442	0.0008	0.0008	0.0008	0.0008	0.0008	0.0120	0.0120
202.5	-0.0330	-0.0105	-0.0049	-0.0049	0.0008	-0.0049	0.0064	0.0234
225.0	-0.0217	-0.0105	-0.0049	-0.0049	-0.0049	0.0008	0.0064	0.0401
247.5	-0.0107	-0.0051	0.0005	0.0061	-0.0051	0.0061	0.0005	0.0173
292.5	-0.0051	-0.0051	-0.0051	-0.0051	0.0061	0.0005	0.0061	0.0287
315.0		-0.0107	0.0005	-0.0051	0.0061	0.0005	0.0173	0.0567
337.5	0.0005	-0.0107	-0.0051	0.0005	0.0061	0.0005	0.0117	
	α=0°; w=0.019							
0.0	-0.0051	-0.0051	-0.0051	0.0005	0.0005	0.0005	0.0117	0.0229
22.5	-0.0051	-0.0051	0.0061	0.0005	0.0005	0.0061	0.0117	0.0229
45.0	-0.0051	-0.0051	-0.0051	0.0005	0.0005	0.0173	0.0117	0.0511
67.5	-0.0051	-0.0051	0.0005	0.0005	0.0005	0.0117	0.0117	0.0229
112.5	-0.0163	-0.0107	-0.0051	-0.0051	0.0005	0.0005	0.0117	0.0287
135.0	-0.0219	-0.0051	0.0005	0.0005	0.0061	0.0005	0.0229	0.0455
157.5	-0.0277	0.0061	0.0061	0.0117	0.0061	0.0005	0.0173	0.0229
180.0	-0.0445	0.0117	0.0061	0.0061	0.0061	0.0005	0.0173	0.0173
202.5	-0.0333	-0.0051	0.0061	0.0061	0.0061	0.0005	0.0117	0.0287
225.0	-0.0219	0.0005	0.0005	0.0005	0.0005	0.0061	0.0117	0.0455
247.5	-0.0164	-0.0108	-0.0052	0.0003	-0.0052	0.0003	0.0003	0.0115
292.5	-0.0108	-0.0108	-0.0052	-0.0052	0.0003	0.0003	0.0059	0.0170
315.0		-0.0164	-0.0052	-0.0052	0.0003	-0.0052	0.0115	0.0451
337.5	-0.0052	-0.0108	-0.0108	-0.0052	0.0003	-0.0052	0.0059	
	α=2.0°; w=0.019							
0.0	-0.0052	-0.0052	-0.0108	-0.0052	0.0005	0.0005	0.0061	0.0173
22.5	-0.0108	-0.0108	0.0005	-0.0052	-0.0052	0.0005	0.0061	0.0230
45.0	-0.0052	-0.0052	-0.0052	-0.0052	-0.0052	0.0117	0.0061	0.0453
67.5	0.0005	-0.0052	0.0061	0.0005	0.0005	0.0117	0.0117	0.0286
112.5	-0.0164	-0.0108	-0.0052	-0.0052	0.0061	0.0005	0.0061	0.0286
135.0	-0.0276	-0.0052	0.0005	-0.0052	0.0061	0.0005	0.0230	0.0511
157.5	-0.0389	0.0061	0.0061	0.0061	0.0061	0.0005	0.0173	0.0230
180.0	-0.0501	0.0173	0.0117	0.0061	0.0061	0.0005	0.0173	0.0117
202.5	-0.0389	-0.0052	0.0005	0.0005	0.0005	-0.0052	0.0061	0.0230
225.0	-0.0220	-0.0052	-0.0052	-0.0052	-0.0052	0.0005	0.0061	0.0398
247.5	-0.0163	-0.0051	-0.0051	0.0005	-0.0051	0.0005	0.0005	0.0117
292.5	-0.0051	-0.0051	-0.0051	-0.0051	0.0005	0.0061	0.0061	0.0229
315.0		-0.0107	-0.0051	-0.0051	0.0061	-0.0051	0.0117	0.0399
337.5	-0.0051	-0.0107	-0.0051	0.0005	0.0061	0.0005	0.0117	
	α=4.0°; w=0.019							
0.0	-0.0107	-0.0107	-0.0107	-0.0051	-0.0051	-0.0051	0.0061	0.0117
22.5	-0.0107	-0.0107	0.0005	-0.0107	-0.0107	0.0005	0.0005	0.0117
45.0	-0.0107	-0.0107	-0.0107	-0.0051	-0.0051	0.0117	0.0005	0.0511
67.5	0.0005	0.0005	0.0061	0.0005	0.0005	0.0117	0.0117	0.0287
112.5	-0.0107	-0.0107	0.0005	0.0005	0.0061	0.0061	0.0117	0.0343
135.0	-0.0277	-0.0051	0.0061	0.0005	0.0117	0.0005	0.0287	0.0567
157.5	-0.0389	0.0061	0.0061	0.0117	0.0061	0.0005	0.0173	0.0287
180.0	-0.0613	0.0229	0.0117	0.0061	0.0061	0.0005	0.0173	0.0173
202.5	-0.0389	-0.0051	-0.0051	-0.0051	-0.0051	-0.0051	0.0061	0.0229
225.0	-0.0277	-0.0107	-0.0107	-0.0051	-0.0051	0.0005	0.0061	0.0399
247.5	-0.0165	-0.0109	-0.0109	-0.0053	-0.0053	0.0003	0.0003	0.0059
292.5	-0.0053	-0.0053	0.0003	0.0003	0.0059	0.0059	0.0059	0.0227
315.0		-0.0053	0.0003	0.0003	0.0059	0.0003	0.0115	0.0397
337.5	-0.0053	-0.0109	-0.0053	0.0003	0.0059	0.0003	0.0115	

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=8.0°; w=0.019							
0.0	-0.0108	-0.0164	-0.0164	-0.0108	-0.0108	-0.0052	0.0005	0.0061
22.5	-0.0276	-0.0276	-0.0164	-0.0220	-0.0220	-0.0164	-0.0108	-0.0052
45.0	-0.0276	-0.0276	-0.0276	-0.0276	-0.0276	-0.0108	-0.0220	0.0342
67.5	-0.0108	-0.0164	-0.0108	-0.0108	-0.0164	-0.0052	-0.0052	0.0173
112.5	-0.0052	-0.0052	0.0061	0.0061	0.0173	0.0117	0.0230	0.0453
135.0	-0.0164	0.0061	0.0173	0.0117	0.0230	0.0117	0.0398	0.0736
157.5	-0.0445	0.0005	0.0117	0.0173	0.0117	0.0061	0.0286	0.0286
180.0	-0.0951	0.0117	0.0061	0.0005	0.0005	-0.0052	0.0117	0.0061
202.5	-0.0558	-0.0220	-0.0220	-0.0220	-0.0220	-0.0220	-0.0108	0.0117
225.0	-0.0501	-0.0333	-0.0333	-0.0333	-0.0276	-0.0276	-0.0164	0.0173
247.5	-0.0221	-0.0165	-0.0109	-0.0109	-0.0109	-0.0053	-0.0053	-0.0053
292.5	-0.0053	-0.0053	-0.0053	-0.0053	-0.0053	-0.0053	-0.0053	0.0059
315.0		0.0003	0.0059	0.0003	0.0115	0.0003	0.0115	0.0509
337.5	-0.0053	-0.0109	-0.0109	-0.0053	0.0003	-0.0053	0.0003	
	α=12.0°; w=0.019							
0.0	-0.0164	-0.0164	-0.0164	-0.0164	-0.0164	-0.0164	-0.0108	-0.0052
22.5	-0.0445	-0.0389	-0.0333	-0.0389	-0.0389	-0.0276	-0.0220	-0.0220
45.0	-0.0614	-0.0614	-0.0558	-0.0501	-0.0558	-0.0389	-0.0445	0.0173
67.5	-0.0445	-0.0445	-0.0333	-0.0276	-0.0276	-0.0164	-0.0164	0.0005
112.5	0.0061	0.0061	0.0173	0.0173	0.0286	0.0286	0.0342	0.0623
135.0	-0.0052	0.0173	0.0342	0.0286	0.0398	0.0342	0.0623	0.0903
157.5	-0.0445	0.0061	0.0230	0.0286	0.0230	0.0173	0.0398	0.0453
180.0	-0.1120	0.0061	0.0005	-0.0052	-0.0108	-0.0164	0.0061	0.0005
202.5	-0.0782	-0.0445	-0.0389	-0.0445	-0.0445	-0.0501	-0.0389	-0.0164
225.0	-0.0726	-0.0614	-0.0614	-0.0614	-0.0614	-0.0558	-0.0445	-0.0108
247.5	-0.0334	-0.0221	-0.0221	-0.0221	-0.0221	-0.0165	-0.0165	-0.0221
292.5	-0.0390	-0.0390	-0.0334	-0.0334	-0.0334	-0.0278	-0.0278	-0.0165
315.0		-0.0053	0.0059	0.0003	0.0115	-0.0053	0.0059	0.0509
337.5	-0.0390	-0.0502	-0.0446	-0.0390	-0.0334	-0.0390	-0.0221	
	α=15.0°; w=0.019							
0.0	-0.0221	-0.0278	-0.0278	-0.0221	-0.0278	-0.0221	-0.0165	-0.0165
22.5	-0.0502	-0.0446	-0.0334	-0.0446	-0.0390	-0.0334	-0.0221	-0.0278
45.0	-0.0784	-0.0840	-0.0784	-0.0726	-0.0784	-0.0558	-0.0670	0.0003
67.5	-0.0502	-0.0670	-0.0446	-0.0446	-0.0502	-0.0278	-0.0278	-0.0221
112.5	0.0227	0.0227	0.0341	0.0397	0.0453	0.0453	0.0565	0.0791
135.0	0.0171	0.0397	0.0509	0.0453	0.0621	0.0565	0.0847	0.1127
157.5	-0.0334	0.0171	0.0341	0.0397	0.0341	0.0341	0.0509	0.0621
180.0	-0.1346	0.0059	-0.0109	-0.0109	-0.0165	-0.0221	0.0003	0.0003
202.5	-0.0952	-0.0502	-0.0670	-0.0614	-0.0670	-0.0726	-0.0558	-0.0334
225.0	-0.0952	-0.0840	-0.0896	-0.0840	-0.0784	-0.0726	-0.0670	-0.0221
247.5	-0.0389	-0.0333	-0.0276	-0.0276	-0.0276	-0.0276	-0.0220	-0.0276
292.5	-0.0726	-0.0670	-0.0614	-0.0558	-0.0445	-0.0445	-0.0445	-0.0220
315.0		-0.0164	-0.0052	-0.0108	0.0005	-0.0220	-0.0108	0.0342
337.5	-0.0670	-0.0726	-0.0558	-0.0445	-0.0333	-0.0445	-0.0276	

TABLE IV.- Continued.

(d) $\beta = 45^{\circ}$; M = 0.95.

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=-2.0°; w=0.019							
0.0	0.0032	-0.0029	-0.0029	0.0091	0.0032	0.0032	0.0209	0.0388
22.5	-0.0029	-0.0029	0.0091	0.0032	0.0032	0.0091	0.0150	0.0388
45.0	-0.0029	-0.0029	-0.0029	0.0032	0.0032	0.0209	0.0150	0.0625
67.5	-0.0029	-0.0029	0.0032	0.0032	0.0032	0.0150	0.0209	0.0329
112.5	-0.0147	-0.0088	0.0032	0.0032	0.0091	0.0091	0.0150	0.0388
135.0	-0.0264	-0.0029	0.0091	0.0032	0.0091	0.0032	0.0270	0.0506
157.5	-0.0384	0.0091	0.0150	0.0150	0.0091	0.0091	0.0209	0.0270
180.0	-0.0563	0.0032	0.0032	0.0032	0.0032	0.0032	0.0150	0.0150
202.5	-0.0443	-0.0088	0.0032	0.0032	0.0032	-0.0029	0.0150	0.0329
225.0	-0.0325	-0.0088	-0.0029	-0.0029	0.0032	0.0032	0.0150	0.0506
247.5	-0.0147	0.0032	0.0032	0.0091	-0.0029	0.0091	0.0032	0.0270
292.5	-0.0029	-0.0088	-0.0029	-0.0029	0.0091	0.0032	0.0150	0.0388
315.0		-0.0088	0.0032	0.0032	0.0150	0.0032	0.0209	0.0743
337.5	0.0032	-0.0088	-0.0029	0.0032	0.0150	0.0032	0.0209	
	α=0°; w=0.019							
0.0	-0.0029	-0.0088	-0.0029	0.0032	0.0032	0.0032	0.0150	0.0329
22.5	-0.0029	-0.0029	0.0091	0.0032	0.0032	0.0091	0.0150	0.0329
45.0	-0.0029	-0.0029	-0.0029	0.0032	0.0032	0.0209	0.0150	0.0625
67.5	-0.0029	-0.0029	0.0091	0.0032	0.0032	0.0150	0.0209	0.0329
112.5	-0.0205	-0.0088	-0.0029	0.0032	0.0091	0.0032	0.0150	0.0388
135.0	-0.0325	-0.0029	0.0032	0.0032	0.0091	0.0032	0.0270	0.0566
157.5	-0.0502	0.0091	0.0150	0.0150	0.0091	0.0032	0.0209	0.0270
180.0	-0.0622	0.0091	0.0091	0.0091	0.0091	0.0032	0.0209	0.0209
202.5	-0.0443	-0.0088	0.0032	0.0032	0.0032	0.0032	0.0150	0.0329
225.0	-0.0325	-0.0029	-0.0029	0.0032	0.0032	0.0032	0.0150	0.0506
247.5	-0.0147	-0.0029	-0.0029	0.0032	-0.0029	0.0091	0.0091	0.0270
292.5	-0.0088	-0.0088	-0.0029	-0.0029	0.0032	0.0032	0.0091	0.0329
315.0		-0.0088	-0.0029	-0.0029	0.0091	-0.0029	0.0209	0.0625
337.5	-0.0029	-0.0088	-0.0088	-0.0029	0.0091	-0.0029	0.0150	
	α=2.0°; w=0.019							
0.0	-0.0027	-0.0086	-0.0086	0.0034	0.0034	0.0034	0.0152	0.0272
22.5	-0.0086	-0.0027	0.0093	-0.0027	-0.0027	0.0093	0.0152	0.0331
45.0	-0.0027	-0.0027	-0.0027	-0.0027	-0.0027	0.0211	0.0152	0.0627
67.5	-0.0027	0.0034	0.0093	0.0034	0.0034	0.0211	0.0152	0.0390
112.5	-0.0204	-0.0086	-0.0027	0.0034	0.0093	0.0034	0.0152	0.0449
135.0	-0.0323	-0.0027	0.0093	0.0034	0.0152	0.0034	0.0331	0.0627
157.5	-0.0500	0.0093	0.0152	0.0152	0.0093	0.0034	0.0272	0.0331
180.0	-0.0679	0.0211	0.0152	0.0152	0.0152	0.0093	0.0211	0.0211
202.5	-0.0441	-0.0027	0.0034	0.0034	0.0034	-0.0027	0.0152	0.0331
225.0	-0.0323	-0.0027	-0.0027	-0.0027	0.0034	0.0034	0.0152	0.0508
247.5	-0.0145	-0.0027	-0.0027	0.0032	-0.0027	0.0091	0.0091	0.0210
292.5	-0.0086	-0.0027	0.0032	-0.0027	0.0091	0.0091	0.0151	0.0330
315.0		-0.0086	0.0032	0.0032	0.0091	-0.0027	0.0210	0.0567
337.5	-0.0027	-0.0086	-0.0027	0.0032	0.0091	0.0032	0.0151	

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=4.0°; w=0.019							
0.0	-0.0029	-0.0088	-0.0029	0.0032	0.0032	0.0032	0.0150	0.0270
22.5	-0.0088	-0.0088	0.0032	-0.0029	-0.0029	0.0032	0.0091	0.0270
45.0	-0.0088	-0.0088	-0.0029	-0.0029	-0.0029	0.0150	0.0032	0.0684
67.5	-0.0029	0.0032	0.0091	0.0032	0.0032	0.0209	0.0150	0.0388
112.5	-0.0205	-0.0088	0.0032	0.0032	0.0150	0.0091	0.0209	0.0447
135.0	-0.0325	-0.0029	0.0091	0.0032	0.0150	0.0032	0.0329	0.0684
157.5	-0.0563	0.0091	0.0150	0.0150	0.0150	0.0032	0.0270	0.0388
180.0	-0.0859	0.0270	0.0209	0.0091	0.0091	0.0032	0.0209	0.0209
202.5	-0.0443	-0.0029	0.0032	0.0032	-0.0029	-0.0088	0.0091	0.0329
225.0	-0.0325	-0.0088	-0.0088	-0.0029	-0.0029	-0.0029	0.0091	0.0447
247.5	-0.0263	-0.0087	-0.0087	-0.0027	-0.0027	-0.0027	0.0032	0.0091
292.5	-0.0087	-0.0087	-0.0027	-0.0027	0.0032	0.0032	0.0091	0.0268
315.0		-0.0146	-0.0027	-0.0027	0.0032	-0.0027	0.0149	0.0444
337.5	-0.0087	-0.0087	-0.0087	-0.0027	0.0032	-0.0027	0.0091	
	α=8.0°; w=0.019							
0.0	-0.0086	-0.0086	-0.0086	-0.0027	0.0032	0.0032	0.0093	0.0153
22.5	-0.0205	-0.0205	-0.0086	-0.0205	-0.0205	-0.0086	0.0032	0.0153
45.0	-0.0266	-0.0266	-0.0205	-0.0205	-0.0205	0.0032	-0.0146	0.0570
67.5	-0.0086	-0.0086	0.0032	-0.0086	-0.0086	0.0032	0.0032	0.0333
112.5	-0.0086	0.0032	0.0153	0.0153	0.0271	0.0212	0.0333	0.0631
135.0	-0.0266	0.0153	0.0271	0.0212	0.0333	0.0212	0.0570	0.0929
157.5	-0.0564	0.0093	0.0212	0.0271	0.0212	0.0153	0.0392	0.0511
180.0	-0.1221	0.0153	0.0153	0.0153	0.0093	0.0032	0.0212	0.0212
202.5	-0.0505	-0.0146	-0.0086	-0.0146	-0.0146	-0.0146	-0.0027	0.0212
225.0	-0.0444	-0.0266	-0.0266	-0.0266	-0.0205	-0.0205	-0.0086	0.0271
247.5	-0.0263	-0.0145	-0.0086	-0.0027	-0.0086	-0.0027	-0.0027	0.0034
292.5	-0.0027	-0.0027	-0.0027	-0.0027	0.0034	0.0034	0.0034	0.0152
315.0		-0.0027	0.0093	0.0093	0.0211	0.0034	0.0211	0.0686
337.5	-0.0086	-0.0086	-0.0086	-0.0027	0.0034	-0.0027	0.0034	
	α=12.0°; w=0.019							
0.0	-0.0147	-0.0147	-0.0147	-0.0147	-0.0147	-0.0088	-0.0029	0.0032
22.5	-0.0443	-0.0384	-0.0325	-0.0384	-0.0325	-0.0205	-0.0147	-0.0088
45.0	-0.0622	-0.0622	-0.0563	-0.0563	-0.0563	-0.0325	-0.0443	0.0329
67.5	-0.0502	-0.0502	-0.0384	-0.0325	-0.0325	-0.0205	-0.0147	0.0091
112.5	-0.0029	0.0091	0.0209	0.0270	0.0329	0.0329	0.0447	0.0743
135.0	-0.0205	0.0209	0.0388	0.0329	0.0506	0.0388	0.0684	0.1040
157.5	-0.0622	0.0091	0.0270	0.0329	0.0270	0.0209	0.0447	0.0566
180.0	-0.1453	0.0032	0.0032	-0.0029	-0.0088	-0.0205	0.0091	0.0091
202.5	-0.0681	-0.0384	-0.0384	-0.0443	-0.0443	-0.0502	-0.0325	-0.0088
225.0	-0.0681	-0.0622	-0.0622	-0.0622	-0.0622	-0.0563	-0.0384	-0.0029
247.5	-0.0267	-0.0206	-0.0206	-0.0147	-0.0206	-0.0088	-0.0088	-0.0147
292.5	-0.0385	-0.0385	-0.0326	-0.0326	-0.0267	-0.0267	-0.0206	-0.0029
315.0		-0.0029	0.0149	0.0090	0.0208	0.0030	0.0149	0.0683
337.5	-0.0385	-0.0504	-0.0445	-0.0326	-0.0267	-0.0326	-0.0147	

TABLE IV.- Continued.

(e) $\phi = 45^{\circ}$; M = 1.00.

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station								$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8	1	2	3	4	5	6	7	8
	α=-2.0°; w=0.019								α=4.0°; w=0.019							
0.0	0.0680	0.0552	0.0486	0.0552	0.0422	0.0422	0.0616	0.0808	0.0552	0.0486	0.0422	0.0486	0.0422	0.0422	0.0552	0.0680
22.5	0.0616	0.0552	0.0616	0.0486	0.0422	0.0486	0.0552	0.0808	0.0486	0.0422	0.0552	0.0422	0.0358	0.0422	0.0486	0.0680
45.0	0.0616	0.0552	0.0486	0.0486	0.0486	0.0616	0.0552	0.1131	0.0552	0.0486	0.0486	0.0422	0.0358	0.0552	0.0422	0.1195
67.5	0.0552	0.0552	0.0552	0.0552	0.0486	0.0552	0.0616	0.0744	0.0616	0.0616	0.0616	0.0552	0.0422	0.0552	0.0486	0.0873
112.5	0.0422	0.0486	0.0552	0.0486	0.0552	0.0486	0.0552	0.0808	0.0294	0.0486	0.0552	0.0552	0.0552	0.0486	0.0552	0.0937
135.0	0.0294	0.0552	0.0616	0.0486	0.0552	0.0422	0.0680	0.0937	0.0101	0.0616	0.0680	0.0552	0.0616	0.0422	0.0744	0.1195
157.5	0.0294	0.0744	0.0680	0.0680	0.0486	0.0486	0.0680	0.0744	-0.0027	0.0680	0.0744	0.0680	0.0552	0.0422	0.0680	0.0808
180.0	0.0101	0.0616	0.0616	0.0552	0.0486	0.0422	0.0616	0.0616	-0.0285	0.0873	0.0744	0.0616	0.0486	0.0422	0.0616	0.0616
202.5	0.0101	0.0486	0.0552	0.0486	0.0486	0.0358	0.0616	0.0744	-0.0027	0.0552	0.0552	0.0422	0.0422	0.0294	0.0486	0.0744
225.0	0.0294	0.0486	0.0486	0.0486	0.0422	0.0422	0.0486	0.1001	0.0165	0.0486	0.0422	0.0422	0.0358	0.0358	0.0422	0.0937
247.5	0.0486	0.0616	0.0552	0.0552	0.0422	0.0486	0.0486	0.0744	0.0422	0.0552	0.0486	0.0486	0.0422	0.0486	0.0486	0.0616
292.5	0.0616	0.0552	0.0552	0.0486	0.0486	0.0486	0.0552	0.0808	0.0616	0.0552	0.0552	0.0486	0.0552	0.0552	0.0552	0.0808
315.0		0.0552	0.0552	0.0486	0.0552	0.0422	0.0616	0.1259		0.0552	0.0552	0.0486	0.0552	0.0486	0.0616	0.1001
337.5	0.0680	0.0552	0.0486	0.0552	0.0552	0.0422	0.0616		0.0616	0.0552	0.0486	0.0486	0.0552	0.0486	0.0616	
	α=0°; w=0.019								α=8.0°; w=0.019							
0.0	0.0680	0.0552	0.0486	0.0486	0.0422	0.0422	0.0552	0.0808	0.0491	0.0491	0.0427	0.0427	0.0427	0.0427	0.0556	0.0556
22.5	0.0616	0.0552	0.0616	0.0486	0.0422	0.0486	0.0552	0.0744	0.0363	0.0363	0.0427	0.0296	0.0232	0.0363	0.0427	0.0622
45.0	0.0616	0.0552	0.0486	0.0486	0.0486	0.0616	0.0552	0.1131	0.0363	0.0363	0.0363	0.0363	0.0168	0.0427	0.0232	0.1138
67.5	0.0616	0.0616	0.0616	0.0552	0.0486	0.0616	0.0552	0.0873	0.0491	0.0556	0.0622	0.0491	0.0363	0.0363	0.0427	0.0750
112.5	0.0358	0.0422	0.0552	0.0486	0.0486	0.0422	0.0552	0.0873	0.0039	0.0686	0.0815	0.0750	0.0815	0.0686	0.0815	0.1138
135.0	0.0229	0.0486	0.0552	0.0486	0.0486	0.0358	0.0680	0.1001	-0.0480	0.0815	0.0945	0.0815	0.0945	0.0750	0.1074	0.1462
157.5	0.0165	0.0680	0.0616	0.0616	0.0486	0.0422	0.0616	0.0744	-0.0480	0.0686	0.0945	0.0945	0.0815	0.0622	0.0879	0.1010
180.0	0.0037	0.0680	0.0616	0.0552	0.0552	0.0422	0.0616	0.0616	-0.0803	0.0686	0.0815	0.0750	0.0622	0.0427	0.0686	0.0686
202.5	0.0101	0.0552	0.0552	0.0486	0.0486	0.0358	0.0552	0.0744	-0.0480	0.0491	0.0556	0.0491	0.0363	0.0296	0.0427	0.0686
225.0	0.0229	0.0552	0.0486	0.0422	0.0422	0.0422	0.0552	0.0937	-0.0027	0.0427	0.0363	0.0296	0.0296	0.0296	0.0363	0.0815
247.5	0.0486	0.0552	0.0552	0.0552	0.0422	0.0486	0.0486	0.0680	0.0296	0.0488	0.0424	0.0424	0.0360	0.0424	0.0424	0.0488
292.5	0.0552	0.0552	0.0552	0.0486	0.0486	0.0486	0.0552	0.0808	0.0554	0.0554	0.0554	0.0488	0.0488	0.0424	0.0488	0.0618
315.0		0.0486	0.0552	0.0486	0.0486	0.0358	0.0616	0.1131		0.0618	0.0682	0.0554	0.0682	0.0488	0.0682	0.1197
337.5	0.0616	0.0486	0.0486	0.0486	0.0552	0.0422	0.0616		0.0488	0.0424	0.0424	0.0424	0.0424	0.0360	0.0488	
	α=2.0°; w=0.019								α=12.0°; w=0.018							
0.0	0.0616	0.0486	0.0486	0.0486	0.0422	0.0422	0.0552	0.0744	0.0354	0.0354	0.0290	0.0354	0.0290	0.0290	0.0417	0.0483
22.5	0.0616	0.0552	0.0616	0.0486	0.0422	0.0486	0.0552	0.0744	0.0162	0.0162	0.0227	0.0098	0.0098	0.0162	0.0290	0.0354
45.0	0.0616	0.0552	0.0552	0.0486	0.0422	0.0616	0.0486	0.1131	-0.0029	-0.0092	-0.0029	-0.0029	-0.0158	0.0035	-0.0092	0.0737
67.5	0.0616	0.0616	0.0616	0.0552	0.0486	0.0616	0.0552	0.0873	-0.0092	-0.0092	0.0035	0.0098	0.0098	0.0227	0.0227	0.0546
112.5	0.0358	0.0486	0.0552	0.0486	0.0486	0.0422	0.0552	0.0873	0.0162	0.0673	0.0802	0.0802	0.0866	0.0802	0.0866	0.1249
135.0	0.0165	0.0552	0.0616	0.0486	0.0552	0.0422	0.0744	0.1131	-0.0285	0.0802	0.0993	0.0866	0.0993	0.0802	0.1122	0.1368
157.5	0.0101	0.0680	0.0680	0.0680	0.0552	0.0422	0.0680	0.0808	-0.0541	0.0610	0.0866	0.0929	0.0802	0.0610	0.0929	0.1058
180.0	-0.0027	0.0808	0.0744	0.0616	0.0552	0.0422	0.0680	0.0680	-0.1116	0.0483	0.0610	0.0483	0.0417	0.0162	0.0483	0.0417
202.5	0.0037	0.0552	0.0552	0.0486	0.0486	0.0358	0.0552	0.0808	-0.0733	0.0162	0.0162	0.0035	-0.0029	-0.0158	0.0035	0.0290
225.0	0.0294	0.0552	0.0552	0.0486	0.0422	0.0422	0.0552	0.1001	-0.0092	-0.0029	-0.0158	-0.0221	-0.0285	-0.0221	-0.0029	0.0417
247.5	0.0422	0.0552	0.0552	0.0552	0.0486	0.0486	0.0486	0.0680	0.0226	0.0290	0.0226	0.0290	0.0226	0.0290	0.0353	0.0290
292.5	0.0616	0.0552	0.0552	0.0486	0.0552	0.0486	0.0552	0.0808	0.0162	0.0162	0.0162	0.0098	0.0226	0.0226	0.0226	0.0481
315.0		0.0552	0.0552	0.0486	0.0552	0.0422	0.0616	0.1065		0.0546	0.0674	0.0546	0.0674	0.0417	0.0610	0.1185
337.5	0.0680	0.0552	0.0486	0.0486	0.0552	0.0422	0.0616		0.0098	-0.0029	-0.0029	-0.0029	0.0098	-0.0029	0.0162	

TABLE IV.- Concluded.

(f) $\phi = 45^{\circ}$; M = 1.03

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	$\alpha=0^{\circ}$; w=0.019							
0.0	-0.0288	-0.0220	-0.0288	-0.0288	-0.0421	-0.0154	0.0911	0.1376
22.5	-0.0288	-0.0220	-0.0154	-0.0354	-0.0487	-0.0088	0.0911	0.1376
45.0	-0.0220	-0.0220	-0.0354	-0.0354	-0.0421	0.0112	0.0911	0.1642
67.5	-0.0154	-0.0220	-0.0288	-0.0354	-0.0354	0.0046	0.0911	0.1376
112.5	-0.0621	-0.0621	-0.0421	-0.0421	-0.0354	-0.0088	0.0843	0.1376
135.0	-0.1085	-0.0553	-0.0288	-0.0421	-0.0288	-0.0088	0.0911	0.1510
157.5	-0.0887	-0.0421	-0.0220	-0.0220	-0.0288	-0.0088	0.0911	0.1310
180.0	-0.1085	-0.0354	-0.0220	-0.0220	-0.0288	-0.0088	0.0911	0.1175
202.5	-0.1219	-0.0553	-0.0288	-0.0288	-0.0354	-0.0154	0.0777	0.1310
225.0	-0.0687	-0.0621	-0.0288	-0.0288	-0.0421	-0.0088	0.0843	0.1510
247.5	-0.0351	-0.0483	-0.0351	-0.0284	-0.0417	-0.0084	0.0781	0.1314
292.5	-0.0284	-0.0216	-0.0284	-0.0417	-0.0351	-0.0084	0.0847	0.1380
315.0		-0.0216	-0.0216	-0.0417	-0.0284	-0.0216	0.0915	0.1647
337.5	-0.0284	-0.0216	-0.0216	-0.0284	-0.0351	-0.0216	0.0915	
	$\alpha=2.0^{\circ}$; w=0.019							
0.0	-0.0284	-0.0216	-0.0351	-0.0351	-0.0417	0.0050	0.0982	0.1314
22.5	-0.0351	-0.0284	-0.0216	-0.0417	-0.0483	-0.0018	0.0915	0.1314
45.0	-0.0216	-0.0284	-0.0417	-0.0417	-0.0483	0.0116	0.0915	0.1713
67.5	-0.0150	-0.0284	-0.0284	-0.0351	-0.0417	-0.0018	0.0915	0.1446
112.5	-0.0617	-0.0683	-0.0417	-0.0417	-0.0284	-0.0216	0.0781	0.1446
135.0	-0.1282	-0.0617	-0.0284	-0.0417	-0.0284	-0.0216	0.0982	0.1647
157.5	-0.0950	-0.0483	-0.0216	-0.0216	-0.0284	-0.0216	0.0915	0.1380
180.0	-0.1016	-0.0284	-0.0216	-0.0284	-0.0284	-0.0150	0.0847	0.1248
202.5	-0.1282	-0.0549	-0.0284	-0.0284	-0.0417	-0.0216	0.0847	0.1380
225.0	-0.0883	-0.0617	-0.0417	-0.0351	-0.0417	-0.0018	0.0847	0.1514
247.5	-0.0419	-0.0486	-0.0286	-0.0286	-0.0353	0.0117	0.0920	0.1323
292.5	-0.0220	-0.0220	-0.0220	-0.0353	-0.0286	0.0184	0.1055	0.1456
315.0		-0.0220	-0.0151	-0.0353	-0.0220	0.0117	0.1055	0.1591
337.5	-0.0220	-0.0220	-0.0220	-0.0353	-0.0286	0.0117	0.1055	

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	$\alpha=4.0^{\circ}$; w=0.019							
0.0	-0.0220	-0.0220	-0.0286	-0.0353	-0.0419	-0.0151	0.0786	0.1254
22.5	-0.0353	-0.0286	-0.0220	-0.0419	-0.0486	-0.0286	0.0720	0.1323
45.0	-0.0220	-0.0286	-0.0419	-0.0419	-0.0419	-0.0151	0.0452	0.1791
67.5	-0.0085	-0.0220	-0.0286	-0.0353	-0.0353	-0.0151	0.0317	0.1456
112.5	-0.0555	-0.0688	-0.0353	-0.0353	-0.0220	-0.0220	0.0250	0.1456
135.0	-0.1291	-0.0621	-0.0220	-0.0419	-0.0151	-0.0286	0.0385	0.1658
157.5	-0.0956	-0.0486	-0.0151	-0.0151	-0.0220	-0.0286	0.0317	0.1323
180.0	-0.1022	-0.0286	-0.0220	-0.0220	-0.0286	-0.0286	0.0385	0.1188
202.5	-0.1357	-0.0555	-0.0286	-0.0286	-0.0353	-0.0486	0.0385	0.1389
225.0	-0.0956	-0.0555	-0.0419	-0.0353	-0.0419	-0.0286	0.0518	0.1456
247.5	-0.0619	-0.0484	-0.0351	-0.0284	-0.0418	-0.0149	0.0587	0.1123
292.5	-0.0284	-0.0284	-0.0218	-0.0351	-0.0284	-0.0016	0.0855	0.1325
315.0		-0.0218	-0.0218	-0.0284	-0.0284	-0.0016	0.0855	0.1458
337.5	-0.0218	-0.0218	-0.0284	-0.0284	-0.0284	-0.0016	0.0855	

TABLE V.- BODY STATIC-PRESSURE ERROR COEFFICIENTS $(p - p_\infty)/p_\infty$ WITHOUT BLEED AIR.

(a) $\phi = 90^\circ$; M = 0.70.

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=-2.1°							
0.0	-0.0061	-0.0061	-0.0061	-0.0061	-0.0061	-0.0061	0.0032	0.0032
22.5	-0.0061	-0.0061	0.0032	-0.0061	-0.0061	-0.0014	-0.0014	0.0078
45.0	-0.0061	-0.0061	-0.0061	-0.0061	-0.0014		-0.0014	0.0217
67.5	-0.0061	-0.0061	-0.0014	-0.0061	-0.0061	-0.0014		0.0032
112.5	-0.0107	-0.0107	-0.0061	-0.0061	-0.0061	-0.0061	-0.0014	0.0078
135.0	-0.0153	-0.0061	-0.0061	-0.0061	-0.0014	-0.0014	0.0078	0.0171
157.5	-0.0061	0.0032	0.0032	0.0032	-0.0014	-0.0014	0.0032	0.0078
180.0	-0.0153		-0.0061	-0.0014	-0.0014	-0.0061	0.0032	0.0032
202.5	-0.0153	-0.0107	-0.0061	-0.0014	-0.0014	-0.0061	0.0032	0.0078
225.0	-0.0107	-0.0061	-0.0061	-0.0061	-0.0061	-0.0061	0.0032	0.0171
247.5	-0.0061	-0.0014	-0.0014	0.0032	-0.0014	0.0032	-0.0014	0.0078
292.5	-0.0014	-0.0061	-0.0014	-0.0014	-0.0014	-0.0014	0.0032	0.0125
315.0		-0.0061	-0.0014	-0.0014	0.0032	-0.0014	0.0032	0.0311
337.5	-0.0061	-0.0061	-0.0061	-0.0014	0.0032	-0.0014	0.0032	
	α=-0.1°							
0.0	-0.0107	-0.0107	-0.0107	-0.0060	-0.0060	-0.0060	-0.0014	0.0032
22.5	-0.0107	-0.0107	-0.0014	-0.0060	-0.0060	-0.0060	-0.0014	0.0032
45.0	-0.0060	-0.0060	-0.0060	-0.0060	-0.0060		-0.0014	0.0171
67.5	-0.0107	-0.0107	-0.0060	-0.0060	-0.0060	-0.0014		0.0032
112.5	-0.0107	-0.0107	-0.0060	-0.0107	-0.0060	-0.0060	-0.0014	0.0079
135.0	-0.0153	-0.0107	-0.0060	-0.0107	-0.0060	-0.0060	0.0032	0.0171
157.5	-0.0153	-0.0060	-0.0060	-0.0014	-0.0060	-0.0107	-0.0014	0.0032
180.0	-0.0107		-0.0060	-0.0060	-0.0060	-0.0060	0.0032	-0.0014
202.5	-0.0198	-0.0107	-0.0107	-0.0107	-0.0060	-0.0107	-0.0060	0.0032
225.0	-0.0153	-0.0107	-0.0107	-0.0107	-0.0107	-0.0107	-0.0060	0.0125
247.5	-0.0061	-0.0014	-0.0014	-0.0014	-0.0014	0.0032	-0.0014	0.0078
292.5	-0.0061	-0.0061	-0.0014	-0.0014	-0.0014	-0.0014	0.0032	0.0078
315.0		-0.0061	-0.0014	-0.0014	0.0032	-0.0014	0.0078	0.0265
337.5	-0.0014	-0.0061	-0.0014	-0.0014	0.0032	-0.0014	0.0032	
	α=1.9°							
0.0	-0.0061	-0.0061	-0.0061	-0.0014	-0.0014	-0.0014	-0.0014	0.0032
22.5	-0.0061	-0.0061	0.0032	-0.0014	-0.0014	-0.0014	0.0032	0.0078
45.0	-0.0014	-0.0014	-0.0014	-0.0014	-0.0014		0.0032	0.0265
67.5	-0.0014	-0.0014	0.0032	-0.0014	-0.0014	0.0032		0.0125
112.5	-0.0061	-0.0061	-0.0061	-0.0014	-0.0014	-0.0014	0.0032	0.0171
135.0	-0.0153	-0.0061	-0.0014	-0.0061	0.0032	-0.0061	0.0078	0.0217
157.5	-0.0153	-0.0014	-0.0014	-0.0014	-0.0014	-0.0061	0.0032	0.0032
180.0	-0.0061		0.0032	0.0032	-0.0014	-0.0061	0.0078	0.0032
202.5	-0.0153	-0.0061	-0.0014	-0.0014	-0.0014	-0.0061	-0.0014	0.0078
225.0	-0.0107	-0.0061	-0.0061	-0.0061	-0.0014	-0.0014	0.0032	0.0171
247.5	-0.0107	-0.0061	-0.0061	-0.0015	-0.0061	-0.0015	-0.0061	-0.0015
292.5	-0.0107	-0.0107	-0.0107	-0.0061	-0.0061	-0.0061	-0.0015	0.0031
315.0		-0.0107	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015	0.0216
337.5	-0.0107	-0.0107	-0.0061	-0.0061	-0.0015	-0.0061	-0.0015	
	α=3.9°							
0.0	-0.0061	-0.0107	-0.0107	-0.0061	-0.0061	-0.0061	-0.0014	0.0032
22.5	-0.0107	-0.0107	0.0032	-0.0061	-0.0061	-0.0014	-0.0014	0.0032
45.0	-0.0061	-0.0061	-0.0061	-0.0014	-0.0014		0.0032	0.0265
67.5	-0.0014	-0.0014	0.0032	0.0032	-0.0014	0.0078		0.0125
112.5	-0.0061	-0.0061	-0.0014	-0.0014	-0.0014	-0.0014	0.0078	0.0171
135.0	-0.0153	-0.0061	-0.0014	-0.0061	0.0032	-0.0061	0.0078	0.0265
157.5	-0.0247	-0.0061	-0.0061	-0.0014	-0.0061	-0.0061	0.0032	0.0032
180.0	-0.0153		-0.0014	-0.0014	-0.0061	-0.0061	0.0032	-0.0014
202.5	-0.0153	-0.0061	-0.0061	-0.0061	-0.0061	-0.0061	-0.0014	0.0032
225.0	-0.0107	-0.0107	-0.0061	-0.0061	-0.0061	-0.0061	-0.0014	0.0125
247.5	-0.0107	-0.0061	-0.0061	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015
292.5	-0.0061	-0.0107	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015	0.0031
315.0		-0.0107	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015	0.0170
337.5	-0.0107	-0.0107	-0.0107	-0.0107	-0.0061	-0.0107	-0.0061	

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=7.9°							
0.0	-0.0245	-0.0291	-0.0291	-0.0245	-0.0245	-0.0245	-0.0198	-0.0198
22.5	-0.0245	-0.0198	-0.0153	-0.0245	-0.0198	-0.0198	-0.0153	-0.0153
45.0	-0.0153	-0.0153	-0.0107	-0.0107	-0.0107		-0.0060	0.0218
67.5	-0.0014	-0.0014	0.0032	-0.0014	-0.0014	0.0079		0.0171
112.5	-0.0060	-0.0060	-0.0014	-0.0014	-0.0014	0.0032	0.0032	0.0171
135.0	-0.0245	-0.0198	-0.0107	-0.0153	-0.0107	-0.0153	0.0032	0.0171
157.5	-0.0523	-0.0291	-0.0245	-0.0198	-0.0245	-0.0245	-0.0153	-0.0153
180.0	-0.0430		-0.0245	-0.0245	-0.0245	-0.0291	-0.0198	-0.0245
202.5	-0.0291	-0.0245	-0.0198	-0.0198	-0.0198	-0.0245	-0.0198	-0.0153
225.0	-0.0198	-0.0198	-0.0153	-0.0153	-0.0153	-0.0153	-0.0107	-0.0014
247.5	-0.0154	-0.0107	-0.0107	-0.0061	-0.0107	-0.0107	-0.0107	-0.0061
292.5	-0.0107	-0.0107	-0.0107	-0.0107	-0.0107	-0.0107	-0.0107	-0.0061
315.0		-0.0154	-0.0107	-0.0107	-0.0107	-0.0107	-0.0061	0.0078
337.5	-0.0200	-0.0246	-0.0200	-0.0200	-0.0154	-0.0200	-0.0154	
	α=12.0°							
0.0	-0.0476	-0.0476	-0.0476	-0.0430	-0.0430	-0.0476	-0.0430	-0.0384
22.5	-0.0430	-0.0384	-0.0291	-0.0384	-0.0384	-0.0384	-0.0337	-0.0337
45.0	-0.0153	-0.0198	-0.0198	-0.0153	-0.0107		-0.0153	0.0171
67.5	0.0079	0.0032	0.0125	0.0079	0.0079	0.0171		0.0264
112.5	0.0032	-0.0014	0.0032	0.0079	0.0079	0.0079	0.0125	0.0309
135.0	-0.0291	-0.0245	-0.0153	-0.0198	-0.0107	-0.0198	-0.0014	0.0171
157.5	-0.0662	-0.0476	-0.0384	-0.0537	-0.0384	-0.0430	-0.0291	-0.0384
180.0	-0.0569		-0.0430	-0.0430	-0.0430	-0.0523	-0.0384	-0.0476
202.5	-0.0384	-0.0291	-0.0291	-0.0291	-0.0337	-0.0337	-0.0291	-0.0198
225.0	-0.0245	-0.0198	-0.0198	-0.0153	-0.0153	-0.0153	-0.0107	-0.0014
247.5	-0.0337	-0.0291	-0.0291	-0.0245	-0.0291	-0.0245	-0.0291	-0.0198
292.5	-0.0291	-0.0337	-0.0291	-0.0291	-0.0291	-0.0291	-0.0291	-0.0245
315.0		-0.0198	-0.0153	-0.0153	-0.0153	-0.0153	-0.0153	0.0032
337.5	-0.0337	-0.0337	-0.0291	-0.0291	-0.0245	-0.0291	-0.0245	
	α=14.9°							
0.0	-0.0619	-0.0665	-0.0665	-0.0619	-0.0619	-0.0665	-0.0619	-0.0571
22.5	-0.0619	-0.0571	-0.0432	-0.0571	-0.0571	-0.0525	-0.0525	-0.0571
45.0	-0.0201	-0.0201	-0.0201	-0.0201	-0.0153		-0.0201	0.0171
67.5	0.0171	0.0125	0.0171	0.0171	0.0171	0.0217		0.0357
112.5	0.0125	0.0078	0.0125	0.0125	0.0171	0.0171	0.0217	0.0404
135.0	-0.0293	-0.0247	-0.0153	-0.0201	-0.0153	-0.0201	-0.0061	0.0125
157.5	-0.0850	-0.0665	-0.0571	-0.0525	-0.0525	-0.0571	-0.0479	-0.0571
180.0	-0.0711		-0.0619	-0.0619	-0.0619	-0.0711	-0.0619	-0.0665
202.5	-0.0386	-0.0247	-0.0293	-0.0386	-0.0386	-0.0432	-0.0340	-0.0293
225.0	-0.0247	-0.0201	-0.0153	-0.0107	-0.0153	-0.0153	-0.0153	-0.0061
247.5	-0.0570	-0.0477	-0.0431	-0.0385	-0.0338	-0.0246	-0.0246	-0.0154
292.5	-0.0523	-0.0523	-0.0477	-0.0431	-0.0385	-0.0385	-0.0338	-0.0246
315.0		-0.0246	-0.0200	-0.0246	-0.0200	-0.0246	-0.0200	-0.0015
337.5	-0.0385	-0.0385	-0.0385	-0.0338	-0.0292	-0.0338	-0.0292	

TABLE V.- Continued.

(b) $\phi = 90^{\circ}$; M = 0.80.

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=-2.0°							
0.0	-0.0018	-0.0069	-0.0069	-0.0018	-0.0069	-0.0018	0.0034	0.0134
22.5	-0.0069	-0.0069	0.0084	-0.0069	-0.0018	-0.0018	0.0034	0.0134
45.0			-0.0018	-0.0018	-0.0018		0.0034	0.0287
67.5	-0.0069	-0.0069	-0.0018	-0.0018	-0.0018	0.0034		0.0084
112.5	-0.0119	-0.0119	-0.0069	-0.0018	-0.0018	-0.0018	0.0034	0.0186
135.0	-0.0171	-0.0069	-0.0018	-0.0069	-0.0018	-0.0018	0.0084	0.0287
157.5	-0.0222	0.0084	0.0034	0.0084	-0.0018	-0.0018	0.0084	0.0134
180.0	-0.0272		-0.0018	-0.0018	-0.0018	-0.0069	0.0084	0.0034
202.5	-0.0222	-0.0069	-0.0018	-0.0018	-0.0018	-0.0069	0.0034	0.0134
225.0	-0.0171	-0.0069	-0.0018	-0.0018	-0.0018	-0.0018	0.0034	0.0287
247.5	-0.0117	-0.0066	-0.0014	0.0037	-0.0014	0.0037	-0.0014	0.0138
292.5	-0.0066	-0.0066	-0.0014	-0.0014	-0.0014	-0.0014	0.0037	0.0138
315.0		-0.0117	-0.0066	-0.0066	-0.0014	-0.0066	0.0037	0.0393
337.5	-0.0066	-0.0117	-0.0066	-0.0066	-0.0014	-0.0014	0.0037	
	α=0°							
0.0	-0.0018	-0.0069	-0.0069	-0.0018	-0.0018	-0.0018	0.0034	0.0134
22.5	-0.0069	-0.0018	0.0084	-0.0018	-0.0018	0.0034	0.0034	0.0134
45.0	-0.0018	-0.0018	-0.0018	-0.0018	-0.0018		0.0034	0.0339
67.5	-0.0069	-0.0069	-0.0018	-0.0018	-0.0018	0.0034		0.0134
112.5	-0.0069	-0.0119	-0.0069	-0.0018	-0.0018	-0.0018	0.0034	0.0186
135.0	-0.0222	-0.0069	-0.0018	-0.0069	-0.0018	-0.0069	0.0084	0.0287
157.5	-0.0222	0.0034	-0.0018	0.0034	-0.0018	-0.0069	0.0034	0.0134
180.0	-0.0171		-0.0018	-0.0018	-0.0018	-0.0069	0.0084	0.0034
202.5	-0.0222	-0.0069	-0.0018	-0.0018	-0.0018	-0.0069	0.0034	0.0134
225.0	-0.0119	-0.0069	-0.0069	-0.0018	-0.0069	-0.0018	0.0034	0.0237
247.5	-0.0066	-0.0066	-0.0066	-0.0014	-0.0014	0.0037	0.0037	0.0087
292.5	-0.0066	-0.0066	-0.0066	-0.0066	-0.0014	-0.0014	0.0037	0.0138
315.0		-0.0066	-0.0014	-0.0014	0.0037	-0.0014	0.0087	0.0393
337.5	-0.0066	-0.0066	-0.0014	-0.0014	0.0037	-0.0014	0.0087	
	α=2.0°							
0.0	-0.0069	-0.0069	-0.0069	-0.0018	-0.0018	-0.0018	0.0034	0.0084
22.5	-0.0069	-0.0069	0.0084	-0.0069	-0.0018	-0.0018	0.0034	0.0134
45.0	-0.0069	-0.0069	-0.0069	-0.0018	-0.0018		0.0034	0.0339
67.5	-0.0018	-0.0069	0.0034	-0.0018	-0.0018	0.0084		0.0186
112.5	-0.0119	-0.0119	-0.0018	-0.0018	-0.0018	-0.0018	0.0034	0.0237
135.0	-0.0222	-0.0069	-0.0018	-0.0069	0.0034	-0.0018	0.0134	0.0339
157.5	-0.0324	-0.0018	-0.0018	0.0034	-0.0018	-0.0069	0.0084	0.0084
180.0	-0.0222		0.0034	0.0034	0.0034	-0.0018	0.0084	0.0034
202.5	-0.0222	-0.0069	-0.0018	-0.0018	-0.0018	-0.0069	0.0034	0.0134
225.0	-0.0119	-0.0069	-0.0069	-0.0018	-0.0069	-0.0018	0.0034	0.0237
247.5	-0.0069	-0.0069	-0.0018	-0.0018	-0.0018	-0.0018	-0.0018	0.0084
292.5	-0.0069	-0.0069	-0.0069	-0.0018	-0.0018	-0.0018	0.0034	0.0084
315.0		-0.0069	-0.0018	-0.0069	-0.0018	-0.0069	0.0034	0.0287
337.5	-0.0069	-0.0069	-0.0069	-0.0018	-0.0018	-0.0069	0.0034	
	α=4.0°							
0.0	-0.0119	-0.0119	-0.0119	-0.0069	-0.0069	-0.0069	-0.0018	0.0034
22.5	-0.0119	-0.0119	0.0034	-0.0069	-0.0069	-0.0018	-0.0018	0.0084
45.0	-0.0069	-0.0069	-0.0069	-0.0069	-0.0018		0.0034	0.0339
67.5	-0.0018	-0.0018	0.0034	0.0034	-0.0018	0.0084		0.0186
112.5	-0.0069	-0.0119	-0.0069	-0.0018	0.0034	-0.0018	0.0084	0.0237
135.0	-0.0222	-0.0119	-0.0018	-0.0069	-0.0018	-0.0069	0.0134	0.0339
157.5	-0.0425	-0.0069	-0.0069	-0.0018	-0.0069	-0.0069	0.0034	0.0084
180.0	-0.0425		-0.0018	-0.0018	-0.0018	-0.0119	0.0034	-0.0018
202.5	-0.0272	-0.0069	-0.0069	-0.0069	-0.0069	-0.0119	-0.0018	0.0084
225.0	-0.0171	-0.0069	-0.0069	-0.0069	-0.0069	-0.0069	-0.0018	0.0186
247.5	-0.0119	-0.0069	-0.0069	-0.0018	-0.0069	-0.0018	-0.0018	0.0034
292.5	-0.0069	-0.0069	-0.0069	-0.0069	-0.0018	-0.0018	-0.0018	0.0034
315.0		-0.0119	-0.0069	-0.0069	-0.0018	-0.0069	0.0034	0.0237
337.5	-0.0119	-0.0119	-0.0119	-0.0069	-0.0018	-0.0069	-0.0018	

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=8.0°							
0.0	-0.0321	-0.0321	-0.0321	-0.0321	-0.0321	-0.0321	-0.0220	-0.0169
22.5	-0.0321	-0.0271	-0.0169	-0.0271	-0.0271	-0.0220	-0.0169	-0.0169
45.0	-0.0119	-0.0119	-0.0119	-0.0119	-0.0119		-0.0068	0.0337
67.5	-0.0017	-0.0017	0.0084	0.0033	0.0033	0.0084		0.0236
112.5	-0.0068	-0.0119	-0.0017	0.0033	0.0033	0.0033	0.0084	0.0287
135.0	-0.0321	-0.0169	-0.0119	-0.0119	-0.0017	-0.0119	0.0084	0.0337
157.5	-0.0727	-0.0321	-0.0220	-0.0220	-0.0220	-0.0321	-0.0119	-0.0169
180.0	-0.0727		-0.0220	-0.0220	-0.0271	-0.0321	-0.0169	-0.0220
202.5	-0.0372	-0.0220	-0.0169	-0.0220	-0.0220	-0.0271	-0.0169	-0.0068
225.0	-0.0220	-0.0169	-0.0119	-0.0119	-0.0119	-0.0119	-0.0068	0.0033
247.5	-0.0119	-0.0069	-0.0069	-0.0069	-0.0119	-0.0069	-0.0119	-0.0069
292.5	-0.0119	-0.0119	-0.0119	-0.0119	-0.0069	-0.0069	-0.0069	-0.0018
315.0		-0.0119	-0.0119	-0.0119	-0.0069	-0.0119	-0.0069	0.0134
337.5	-0.0222	-0.0272	-0.0272	-0.0222	-0.0171	-0.0222	-0.0119	
	α=12.0°							
0.0	-0.0625	-0.0676	-0.0676	-0.0575	-0.0575	-0.0625	-0.0524	-0.0524
22.5	-0.0575	-0.0524	-0.0372	-0.0524	-0.0524	-0.0473	-0.0423	-0.0423
45.0	-0.0220	-0.0220	-0.0220	-0.0220	-0.0220		-0.0169	0.0287
67.5	0.0084	0.0033	0.0135	0.0084	0.0084	0.0185		0.0388
112.5	0.0033	-0.0017	0.0033	0.0084	0.0135	0.0084	0.0185	0.0388
135.0	-0.0423	-0.0321	-0.0220	-0.0271	-0.0169	-0.0271	-0.0017	0.0236
157.5	-0.1031	-0.0676	-0.0524	-0.0473	-0.0473	-0.0575	-0.0372	-0.0473
180.0	-0.1081		-0.0575	-0.0575	-0.0575	-0.0676	-0.0524	-0.0575
202.5	-0.0524	-0.0321	-0.0321	-0.0372	-0.0372	-0.0473	-0.0372	-0.0271
225.0	-0.0321	-0.0271	-0.0220	-0.0169	-0.0169	-0.0169	-0.0169	0.0033
247.5	-0.0473	-0.0423	-0.0423	-0.0372	-0.0423	-0.0372	-0.0372	-0.0220
292.5	-0.0423	-0.0473	-0.0423	-0.0423	-0.0423	-0.0423	-0.0372	-0.0271
315.0		-0.0271	-0.0220	-0.0220	-0.0169	-0.0220	-0.0169	0.0033
337.5	-0.0423	-0.0423	-0.0423	-0.0372	-0.0321	-0.0372	-0.0321	
	α=14.9°							
0.0	-0.0833	-0.0833	-0.0833	-0.0782	-0.0782	-0.0833	-0.0730	-0.0730
22.5	-0.0782	-0.0730	-0.0527	-0.0730	-0.0730	-0.0629	-0.0629	-0.0680
45.0	-0.0272	-0.0272	-0.0272	-0.0222	-0.0222		-0.0171	0.0287
67.5	0.0186	0.0186	0.0237	0.0237	0.0186	0.0287		0.0542
112.5	0.0134	0.0084	0.0186	0.0186	0.0237	0.0237	0.0287	0.0542
135.0	-0.0425	-0.0374	-0.0222	-0.0272	-0.0171	-0.0272	-0.0069	0.0237
157.5	-0.1241	-0.0883	-0.0730	-0.0629	-0.0680	-0.0730	-0.0578	-0.0730
180.0	-0.1241		-0.0782	-0.0782	-0.0782	-0.0883	-0.0730	-0.0833
202.5	-0.0527	-0.0272	-0.0374	-0.0477	-0.0477	-0.0527	-0.0425	-0.0324
225.0	-0.0374	-0.0272	-0.0171	-0.0171	-0.0171	-0.0222	-0.0171	-0.0069
247.5	-0.0679	-0.0578	-0.0527	-0.0425	-0.0425	-0.0271	-0.0221	-0.0120
292.5	-0.0629	-0.0629	-0.0527	-0.0527	-0.0425	-0.0425	-0.0374	-0.0271
315.0		-0.0271	-0.0221	-0.0271	-0.0221	-0.0271	-0.0170	0.0034
337.5	-0.0425	-0.0425	-0.0425	-0.0374	-0.0323	-0.0323	-0.0271	

TABLE V.- Continued.

(c) $\phi = 90^{\circ}$; $M = 0.90$.

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=-2.0°							
0.0	0.0007	-0.0049	-0.0049	0.0007	0.0007	0.0007	0.0120	0.0232
22.5	-0.0049	-0.0049	0.0007	0.0007	0.0007	0.0007	0.0063	0.0232
45.0	-0.0049	0.0007	0.0007	0.0007	0.0007		0.0063	0.0460
67.5	-0.0049	-0.0049	0.0007	0.0007	0.0007	0.0063		0.0232
112.5	-0.0107	-0.0107	-0.0049	-0.0049	0.0063	0.0007	0.0063	0.0232
135.0	-0.0219	-0.0049	0.0063	-0.0049	0.0063	0.0007	0.0176	0.0402
157.5	-0.0446	0.0176	0.0120	0.0120	0.0063	0.0007	0.0176	0.0232
180.0	-0.0446		0.0007	0.0007	0.0007	-0.0049	0.0176	0.0120
202.5	-0.0332	-0.0049	0.0007	0.0007	0.0007	-0.0049	0.0063	0.0290
225.0	-0.0219	-0.0049	0.0007	0.0007	0.0007	0.0007	0.0063	0.0402
247.5	-0.0053	0.0003	0.0059	0.0115	0.0003	0.0115	0.0059	0.0227
292.5	0.0003	-0.0053	0.0003	0.0003	0.0059	0.0059	0.0115	0.0285
315.0		-0.0053	0.0059	0.0003	0.0115	0.0003	0.0171	0.0565
337.5	0.0003	-0.0053	-0.0053	0.0059	0.0115	0.0003	0.0171	
	α=0°							
0.0	-0.0049	-0.0049	-0.0049	0.0007	0.0007	0.0007	0.0120	0.0232
22.5	-0.0049	-0.0049	0.0007	0.0007	0.0007	0.0007	0.0063	0.0232
45.0	-0.0049	-0.0049	-0.0049	0.0007	0.0007		0.0063	0.0516
67.5	-0.0049	-0.0049	0.0063	0.0007	0.0007	0.0120		0.0232
112.5	-0.0163	-0.0107	0.0007	0.0007	0.0007	0.0007	0.0063	0.0290
135.0	-0.0276	-0.0049	0.0007	-0.0049	0.0063	-0.0049	0.0232	0.0460
157.5	-0.0388	0.0120	0.0063	0.0063	0.0063	0.0007	0.0176	0.0232
180.0	-0.0388		0.0063	0.0063	0.0063	0.0007	0.0176	0.0120
202.5	-0.0332	-0.0049	0.0007	0.0007	0.0007	-0.0049	0.0063	0.0232
225.0	-0.0219	-0.0049	-0.0049	0.0007	0.0007	0.0007	0.0063	0.0402
247.5	-0.0108	-0.0052	-0.0052	0.0005	-0.0052	0.0061	0.0061	0.0173
292.5	-0.0052	-0.0108	-0.0052	-0.0052	0.0005	0.0005	0.0061	0.0230
315.0		-0.0108	-0.0052	-0.0052	0.0061	-0.0052	0.0117	0.0511
337.5	-0.0052	-0.0108	-0.0052	0.0005	0.0061	-0.0052	0.0117	
	α=2.0°							
0.0	-0.0049	-0.0049	-0.0049	0.0007	0.0007	0.0007	0.0120	0.0176
22.5	-0.0107	-0.0049	-0.0049	-0.0049	0.0007	0.0007	0.0063	0.0232
45.0	0.0007	-0.0049	-0.0049	0.0007	0.0007		0.0120	0.0516
67.5	0.0063	0.0007	0.0120	0.0063	0.0007	0.0120		0.0290
112.5	-0.0107	-0.0107	0.0007	0.0007	0.0063	0.0007	0.0120	0.0346
135.0	-0.0332	-0.0107	0.0007	-0.0049	0.0063	-0.0049	0.0232	0.0402
157.5	-0.0502	0.0007	0.0007	0.0063	0.0007	-0.0049	0.0120	0.0176
180.0	-0.0558		0.0120	0.0063	0.0063	-0.0049	0.0176	0.0120
202.5	-0.0332	-0.0049	0.0007	0.0007	0.0007	-0.0049	0.0063	0.0232
225.0	-0.0219	-0.0049	-0.0049	0.0007	0.0007	0.0007	0.0063	0.0346
247.5	-0.0108	-0.0052	-0.0052	0.0005	-0.0052	0.0005	0.0005	0.0117
292.5	-0.0052	-0.0108	-0.0052	-0.0052	0.0005	0.0005	0.0061	0.0173
315.0		-0.0108	-0.0052	-0.0052	0.0005	-0.0052	0.0061	0.0453
337.5	-0.0052	-0.0108	-0.0108	-0.0052	0.0005	-0.0052	0.0061	
	α=4.0°							
0.0	-0.0106	-0.0164	-0.0164	-0.0106	-0.0106	-0.0106	0.0005	0.0118
22.5	-0.0164	-0.0106	-0.0106	-0.0106	-0.0106	-0.0051	0.0005	0.0118
45.0	-0.0051	-0.0051	-0.0051	-0.0051	-0.0051		0.0062	0.0511
67.5	-0.0051	0.0005	0.0062	0.0005	0.0005	0.0118		0.0342
112.5	-0.0106	-0.0164	0.0005	-0.0051	0.0062	0.0005	0.0062	0.0287
135.0	-0.0388	-0.0164	-0.0051	-0.0106	0.0005	-0.0106	0.0174	0.0455
157.5	-0.0725	-0.0106	-0.0051	0.0005	-0.0051	-0.0106	0.0062	0.0118
180.0	-0.0894		0.0005	0.0005	-0.0051	-0.0106	0.0062	0.0005
202.5	-0.0388	-0.0106	-0.0051	-0.0051	-0.0051	-0.0164	0.0005	0.0174
225.0	-0.0275	-0.0106	-0.0051	-0.0051	-0.0051	-0.0051	0.0005	0.0231
247.5	-0.0108	0.0005	0.0005	0.0005	0.0005	0.0061	0.0061	0.0117
292.5	-0.0052	-0.0052	0.0005	0.0005	0.0005	0.0005	0.0061	0.0173
315.0		-0.0108	-0.0052	-0.0052	0.0005	-0.0052	0.0117	0.0398
337.5	-0.0108	-0.0164	-0.0108	-0.0052	0.0005	-0.0052	0.0061	

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=8.0°							
0.0	-0.0334	-0.0389	-0.0389	-0.0334	-0.0334	-0.0334	-0.0221	-0.0165
22.5	-0.0334	-0.0334	-0.0277	-0.0277	-0.0277	-0.0221	-0.0165	-0.0052
45.0	-0.0108	-0.0108	-0.0108	-0.0108	-0.0108		-0.0052	0.0567
67.5	0.0061	0.0061	0.0116	0.0061	0.0003	0.0172		0.0398
112.5	-0.0108	-0.0108	0.0061	0.0003	0.0116	0.0061	0.0172	0.0398
135.0	-0.0558	-0.0277	-0.0052	-0.0221	-0.0052	-0.0165	0.0116	0.0454
157.5	-0.1120	-0.0445	-0.0277	-0.0221	-0.0277	-0.0334	-0.0108	-0.0108
180.0	-0.1343		-0.0221	-0.0277	-0.0334	-0.0389	-0.0165	-0.0221
202.5	-0.0558	-0.0221	-0.0221	-0.0221	-0.0221	-0.0277	-0.0165	-0.0052
225.0	-0.0277	-0.0165	-0.0165	-0.0165	-0.0165	-0.0165	-0.0052	0.0116
247.5	-0.0164	-0.0108	-0.0052	-0.0052	-0.0108	-0.0052	-0.0108	0.0005
292.5	-0.0108	-0.0108	-0.0108	-0.0108	-0.0052	-0.0052	-0.0052	0.0061
315.0		-0.0164	-0.0108	-0.0108	-0.0052	-0.0052	0.0061	0.0230
337.5	-0.0220	-0.0276	-0.0276	-0.0220	-0.0108	-0.0164	-0.0052	
	α=12.0°							
0.0	-0.0669	-0.0725	-0.0725	-0.0669	-0.0612	-0.0669	-0.0501	-0.0501
22.5	-0.0669	-0.0612	-0.0556	-0.0612	-0.0612	-0.0444	-0.0444	-0.0388
45.0	-0.0219	-0.0219	-0.0219	-0.0164	-0.0164		-0.0106	0.0511
67.5	0.0174	0.0118	0.0231	0.0174	0.0174	0.0287		0.0568
112.5	0.0005	-0.0051	0.0118	0.0118	0.0231	0.0174	0.0287	0.0568
135.0	-0.0725	-0.0444	-0.0164	-0.0275	-0.0106	-0.0275	0.0062	0.0455
157.5	-0.1400	-0.0781	-0.0556	-0.0444	-0.0501	-0.0612	-0.0332	-0.0388
180.0	-0.1737		-0.0556	-0.0556	-0.0612	-0.0725	-0.0444	-0.0556
202.5	-0.0612	-0.0219	-0.0219	-0.0332	-0.0388	-0.0444	-0.0332	-0.0164
225.0	-0.0388	-0.0219	-0.0219	-0.0106	-0.0106	-0.0106	-0.0051	0.0118
247.5	-0.0558	-0.0445	-0.0389	-0.0333	-0.0445	-0.0276	-0.0333	-0.0164
292.5	-0.0445	-0.0501	-0.0445	-0.0445	-0.0389	-0.0389	-0.0333	-0.0220
315.0		-0.0220	-0.0164	-0.0164	-0.0108	-0.0164	-0.0052	0.0173
337.5	-0.0389	-0.0445	-0.0389	-0.0333	-0.0276	-0.0333	-0.0220	
	α=15.1°							
0.0	-0.1008	-0.1064	-0.1064	-0.0951	-0.0951	-0.0951	-0.0840	-0.0840
22.5	-0.0951	-0.0840	-0.0840	-0.0895	-0.0840	-0.0727	-0.0671	-0.0727
45.0	-0.0334	-0.0334	-0.0334	-0.0277	-0.0277		-0.0221	0.0509
67.5	0.0229	0.0229	0.0341	0.0285	0.0229	0.0454		0.0735
112.5	0.0172	0.0003	0.0229	0.0229	0.0341	0.0285	0.0398	0.0678
135.0	-0.0782	-0.0558	-0.0277	-0.0389	-0.0221	-0.0334	-0.0052	0.0398
157.5	-0.1794	-0.1177	-0.0840	-0.0782	-0.0840	-0.0895	-0.0671	-0.0782
180.0	-0.1963		-0.0895	-0.0895	-0.0951	-0.1064	-0.0840	-0.0951
202.5	-0.0782	-0.0277	-0.0334	-0.0502	-0.0558	-0.0558	-0.0445	-0.0334
225.0	-0.0445	-0.0277	-0.0165	-0.0165	-0.0221	-0.0221	-0.0221	-0.0052
247.5	-0.0782	-0.0614	-0.0558	-0.0445	-0.0445	-0.0220	-0.0220	-0.0052
292.5	-0.0782	-0.0726	-0.0614	-0.0614	-0.0501	-0.0445	-0.0389	-0.0220
315.0		-0.0333	-0.0276	-0.0276	-0.0220	-0.0276	-0.0164	0.0117
337.5	-0.0445	-0.0445	-0.0445	-0.0389	-0.0333	-0.0333	-0.0276	

TABLE V.- Continued.

(d) $\phi = 90^{\circ}$; M = 0.95.

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=-2.0°							
0.0	-0.0027	-0.0027	-0.0027	0.0032	0.0032	0.0032	0.0211	0.0331
22.5	-0.0027	-0.0027	0.0211	0.0032	0.0032	0.0091	0.0152	0.0391
45.0	0.0032	0.0032	0.0032	0.0032	0.0091		0.0211	0.0570
67.5	-0.0027	-0.0027	0.0032	0.0032	0.0091	0.0152		0.0331
112.5	-0.0147	-0.0027	0.0032	0.0032	0.0091	0.0091	0.0211	0.0391
135.0	-0.0267	0.0032	0.0091	0.0032	0.0091	0.0032	0.0271	0.0511
157.5	-0.0625	0.0211	0.0211	0.0211	0.0152	0.0032	0.0271	0.0331
180.0	-0.0564		0.0091	0.0091	0.0091	0.0032	0.0211	0.0211
202.5	-0.0446	-0.0027	0.0091	0.0091	0.0091	0.0032	0.0152	0.0331
225.0	-0.0267	-0.0027	-0.0027	0.0091	0.0032	0.0091	0.0152	0.0570
247.5	-0.0088	0.0031	0.0092	0.0151	0.0031	0.0151	0.0092	0.0331
292.5	0.0031	-0.0029	0.0031	0.0031	0.0092	0.0092	0.0151	0.0390
315.0		-0.0088	0.0031	0.0031	0.0092	0.0031	0.0210	0.0748
337.5	0.0031	-0.0029	-0.0029	0.0031	0.0151	0.0031	0.0210	
	α=0°							
0.0	0.0032	-0.0027	-0.0027	0.0032	0.0032	0.0032	0.0211	0.0331
22.5	-0.0027	-0.0027	0.0211	0.0032	0.0032	0.0091	0.0211	0.0391
45.0	0.0032	0.0032	0.0032	0.0032	0.0032		0.0152	0.0629
67.5	-0.0027	-0.0027	0.0091	0.0091	0.0032	0.0152		0.0391
112.5	-0.0206	-0.0088	0.0032	0.0032	0.0091	0.0091	0.0152	0.0450
135.0	-0.0326	-0.0027	0.0091	-0.0027	0.0091	0.0032	0.0271	0.0570
157.5	-0.0564	0.0152	0.0152	0.0152	0.0091	0.0032	0.0271	0.0331
180.0	-0.0564		0.0152	0.0152	0.0152	0.0032	0.0271	0.0271
202.5	-0.0385	0.0032	0.0091	0.0091	0.0091	0.0032	0.0152	0.0331
225.0	-0.0267	-0.0027	0.0032	0.0032	0.0032	0.0032	0.0152	0.0511
247.5	-0.0088	0.0031	0.0031	0.0092	0.0031	0.0151	0.0151	0.0331
292.5	-0.0029	-0.0029	0.0031	0.0031	0.0092	0.0092	0.0151	0.0390
315.0		-0.0029	0.0031	0.0031	0.0151	0.0031	0.0210	0.0688
337.5	0.0031	-0.0029	0.0031	0.0031	0.0151	0.0031	0.0210	
	α=2.0°							
0.0	-0.0087	-0.0087	-0.0087	-0.0028	-0.0028	-0.0028	0.0150	0.0269
22.5	-0.0087	-0.0087	0.0150	-0.0028	-0.0028	0.0030	0.0091	0.0269
45.0	-0.0028	-0.0028	-0.0028	-0.0028	-0.0028		0.0091	0.0625
67.5	-0.0028	0.0030	0.0091	0.0030	0.0030	0.0150		0.0386
112.5	-0.0207	-0.0148	0.0030	0.0030	0.0091	0.0030	0.0150	0.0447
135.0	-0.0443	-0.0087	0.0030	-0.0028	0.0091	-0.0028	0.0269	0.0564
157.5	-0.0682	0.0030	0.0091	0.0091	0.0030	-0.0028	0.0208	0.0269
180.0	-0.0800		0.0150	0.0091	0.0030	-0.0028	0.0208	0.0150
202.5	-0.0385	-0.0028	0.0030	0.0030	0.0030	-0.0028	0.0150	0.0269
225.0	-0.0265	-0.0087	-0.0028	0.0030	-0.0028	0.0030	0.0091	0.0386
247.5	-0.0147	-0.0027	0.0032	0.0091	0.0032	0.0091	0.0091	0.0271
292.5	-0.0027	-0.0088	-0.0027	-0.0027	0.0091	0.0032	0.0152	0.0271
315.0		-0.0088	0.0032	0.0032	0.0091	0.0032	0.0211	0.0629
337.5	-0.0027	-0.0088	-0.0027	0.0032	0.0091	0.0032	0.0211	
	α=4.0°							
0.0	-0.0088	-0.0088	-0.0147	-0.0027	-0.0027	-0.0027	0.0152	0.0211
22.5	-0.0147	-0.0088	0.0152	-0.0088	-0.0027	0.0032	0.0091	0.0331
45.0	-0.0027	-0.0027	-0.0027	0.0032	0.0032		0.0091	0.0749
67.5	0.0032	0.0032	0.0152	0.0091	0.0032	0.0211		0.0511
112.5	-0.0206	-0.0088	0.0091	0.0091	0.0152	0.0091	0.0211	0.0511
135.0	-0.0564	-0.0088	0.0091	-0.0027	0.0152	-0.0027	0.0271	0.0690
157.5	-0.0804	-0.0027	0.0091	0.0091	0.0032	-0.0088	0.0211	0.0271
180.0	-0.1102		0.0152	0.0091	0.0091	-0.0027	0.0211	0.0152
202.5	-0.0385	0.0032	0.0032	0.0032	0.0032	-0.0088	0.0152	0.0331
225.0	-0.0206	-0.0027	0.0032	0.0032	0.0032	0.0032	0.0152	0.0391
247.5	-0.0088	0.0032	0.0032	0.0091	0.0032	0.0091	0.0091	0.0211
292.5	-0.0027	-0.0027	0.0032	0.0032	0.0091	0.0091	0.0152	0.0271
315.0		-0.0088	0.0032	-0.0027	0.0091	0.0032	0.0211	0.0570
337.5	-0.0088	-0.0088	-0.0088	-0.0027	0.0032	-0.0027	0.0152	

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=8.0°							
0.0	-0.0326	-0.0326	-0.0385	-0.0267	-0.0267	-0.0267	-0.0088	-0.0027
22.5	-0.0326	-0.0267	-0.0027	-0.0267	-0.0267	-0.0147	-0.0088	0.0091
45.0	-0.0088	-0.0088	-0.0088	-0.0027	-0.0027		0.0032	0.0808
67.5	0.0152	0.0091	0.0271	0.0211	0.0152	0.0331		0.0629
112.5	-0.0206	-0.0088	0.0152	0.0152	0.0211	0.0152	0.0271	0.0629
135.0	-0.0984	-0.0206	0.0032	-0.0147	0.0091	-0.0147	0.0331	0.0629
157.5	-0.1521	-0.0326	-0.0147	-0.0088	-0.0147	-0.0267	0.0032	0.0091
180.0	-0.1639		-0.0088	-0.0147	-0.0206	-0.0326	-0.0027	-0.0088
202.5	-0.0564	-0.0147	-0.0088	-0.0147	-0.0147	-0.0206	-0.0088	0.0091
225.0	-0.0267	-0.0088	-0.0088	-0.0088	-0.0027	-0.0027	0.0091	0.0271
247.5	-0.0206	-0.0088	-0.0027	0.0032	-0.0088	0.0032	-0.0027	0.0091
292.5	-0.0088	-0.0088	-0.0088	0.0556	0.0622	0.0622	0.0686	0.0816
315.0		0.0556	0.0556	0.0556	0.0686	0.0622	0.0750	0.1010
337.5	0.0361	0.0297	0.0361	0.0427	0.0556	0.0492	0.0622	
	α=12.0°							
0.0	-0.0684	-0.0743	-0.0743	-0.0625	-0.0564	-0.0625	-0.0446	-0.0446
22.5	-0.0684	-0.0625	-0.0326	-0.0564	-0.0564	-0.0446	-0.0326	-0.0267
45.0	-0.0147	-0.0206	-0.0147	-0.0088	-0.0147		0.0032	0.0749
67.5	0.0211	0.0211	0.0331	0.0331	0.0271	0.0450		0.0808
112.5	0.0032	-0.0147	0.0271	0.0271	0.0331	0.0331	0.0391	0.0808
135.0	-0.0984	-0.0446	-0.0027	-0.0206	0.0032	-0.0147	0.0211	0.0690
157.5	-0.2118	-0.0684	-0.0446	-0.0385	-0.0446	-0.0625	-0.0206	-0.0267
180.0	-0.2058		-0.0446	-0.0505	-0.0564	-0.0684	-0.0385	-0.0505
202.5	-0.0684	-0.0147	-0.0088	-0.0206	-0.0326	-0.0385	-0.0206	-0.0027
225.0	-0.0326	-0.0147	-0.0088	-0.0027	-0.0027	-0.0027	0.0032	0.0211
247.5	-0.0505	-0.0385	-0.0326	-0.0267	-0.0326	-0.0206	-0.0206	-0.0027
292.5	-0.0446	-0.0446	-0.0385	-0.0385	-0.0326	-0.0326	-0.0267	-0.0088
315.0		-0.0206	-0.0147	-0.0147	-0.0027	-0.0088	0.0032	0.0331
337.5	-0.0385	-0.0385	-0.0385	-0.0267	-0.0206	-0.0267	-0.0088	
	α=15.0°							
0.0	-0.1044	-0.1103	-0.1103	-0.0924	-0.0865	-0.0924	-0.0686	-0.0745
22.5	-0.1103	-0.0924	-0.0686	-0.0924	-0.0865	-0.0745	-0.0566	-0.0566
45.0	-0.0269	-0.0328	-0.0269	-0.0208	-0.0208	0.0150	-0.0090	0.0747
67.5	0.0330	0.0269	0.0448	0.0389	0.0330	0.0568	0.1284	0.0926
112.5	0.0269	-0.0090	0.0330	0.0330	0.0448	0.0389	0.0509	0.0926
135.0	-0.0865	-0.1044	-0.0149	-0.0328	-0.0090	-0.0269	0.0150	0.0627
157.5	-0.2536	-0.0865	-0.0745	-0.0686	-0.0745	-0.0865	-0.0507	-0.0627
180.0	-0.2178	-0.0507	-0.0865	-0.0806	-0.0865	-0.0985	-0.0686	-0.0865
202.5	-0.0806	-0.0149	-0.0208	-0.0448	-0.0448	-0.0448	-0.0328	-0.0149
225.0	-0.0387	-0.0149	-0.0090	-0.0029	-0.0090	-0.0090	-0.0029	0.0150
247.5	-0.0682	-0.0563	-0.0504	-0.0385	-0.0385	-0.0207	-0.0207	0.0030
292.5	-0.0741	-0.0682	-0.0563	-0.0563	-0.0443	-0.0443	-0.0385	-0.0148
315.0		-0.0385	-0.0265	-0.0265	-0.0207	-0.0265	-0.0148	0.0208
337.5	-0.0504	-0.0504	-0.0443	-0.0385	-0.0265	-0.0326	-0.0207	

TABLE V.- Continued.

(e) $\phi = 90^{\circ}$; M = 1.00.

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	$\alpha = -2.0°$							
0.0	0.0550	0.0484	0.0421	0.0421	0.0421	0.0357	0.0550	0.0677
22.5	0.0550	0.0484	0.0484	0.0421	0.0421	0.0421	0.0484	0.0743
45.0	0.0550	0.0484	0.0421	0.0421	0.0421		0.0484	0.0936
67.5	0.0484	0.0484	0.0484	0.0484	0.0421	0.0484		0.0677
112.5	0.0357	0.0421	0.0484	0.0421	0.0421	0.0357	0.0550	0.0743
135.0	0.0164	0.0484	0.0550	0.0421	0.0484	0.0357	0.0614	0.0936
157.5	0.0035	0.0743	0.0677	0.0614	0.0484	0.0421	0.0614	0.0677
180.0	0.0035		0.0550	0.0484	0.0421	0.0357	0.0550	0.0614
202.5	-0.0029	0.0484	0.0484	0.0484	0.0421	0.0357	0.0550	0.0743
225.0	0.0228	0.0484	0.0484	0.0484	0.0421	0.0421	0.0484	0.1000
247.5	0.0486	0.0680	0.0616	0.0616	0.0486	0.0552	0.0486	0.0808
292.5	0.0616	0.0552	0.0616	0.0552	0.0552	0.0486	0.0552	0.0873
315.0		0.0552	0.0616	0.0552	0.0552	0.0422	0.0616	0.1259
337.5	0.0680	0.0552	0.0552	0.0552	0.0552	0.0486	0.0616	
	$\alpha = 0°$							
0.0	0.0614	0.0484	0.0421	0.0484	0.0421	0.0421	0.0550	0.0677
22.5	0.0550	0.0484	0.0484	0.0421	0.0421	0.0484	0.0550	0.0807
45.0	0.0614	0.0550	0.0484	0.0484	0.0421		0.0550	0.1063
67.5	0.0614	0.0550	0.0614	0.0550	0.0421	0.0550		0.0807
112.5	0.0357	0.0484	0.0550	0.0484	0.0484	0.0421	0.0550	0.0807
135.0	0.0164	0.0484	0.0550	0.0421	0.0484	0.0357	0.0614	0.1000
157.5	0.0035	0.0677	0.0614	0.0614	0.0484	0.0357	0.0614	0.0743
180.0	0.0098		0.0614	0.0550	0.0484	0.0357	0.0614	0.0614
202.5	0.0098	0.0550	0.0550	0.0484	0.0421	0.0357	0.0484	0.0743
225.0	0.0291	0.0484	0.0484	0.0484	0.0421	0.0421	0.0484	0.0936
247.5	0.0486	0.0616	0.0552	0.0552	0.0422	0.0552	0.0486	0.0744
292.5	0.0616	0.0486	0.0552	0.0486	0.0486	0.0486	0.0552	0.0808
315.0		0.0486	0.0552	0.0486	0.0552	0.0422	0.0616	0.1131
337.5	0.0616	0.0486	0.0486	0.0486	0.0552	0.0422	0.0616	
	$\alpha = 2.0°$							
0.0	0.0479	0.0351	0.0288	0.0351	0.0288	0.0288	0.0479	0.0606
22.5	0.0414	0.0351	0.0351	0.0351	0.0288	0.0351	0.0479	0.0734
45.0	0.0479	0.0414	0.0351	0.0351	0.0351		0.0414	0.1054
67.5	0.0542	0.0479	0.0542	0.0479	0.0351	0.0479		0.0797
112.5	0.0159	0.0351	0.0479	0.0414	0.0414	0.0351	0.0479	0.0863
135.0	-0.0161	0.0414	0.0479	0.0288	0.0414	0.0288	0.0606	0.0989
157.5	-0.0161	0.0479	0.0479	0.0479	0.0351	0.0288	0.0542	0.0671
180.0	-0.0161		0.0606	0.0479	0.0414	0.0288	0.0542	0.0542
202.5	-0.0033	0.0479	0.0414	0.0351	0.0351	0.0288	0.0414	0.0671
225.0	0.0159	0.0414	0.0414	0.0351	0.0351	0.0351	0.0414	0.0797
247.5	0.0354	0.0483	0.0417	0.0417	0.0354	0.0417	0.0483	0.0610
292.5	0.0483	0.0417	0.0417	0.0354	0.0417	0.0417	0.0483	0.0673
315.0		0.0417	0.0417	0.0417	0.0483	0.0354	0.0546	0.1058
337.5	0.0483	0.0417	0.0354	0.0417	0.0483	0.0354	0.0546	

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	$\alpha = 4.0°$							
0.0	0.0622	0.0492	0.0427	0.0492	0.0427	0.0361	0.0556	0.0686
22.5	0.0556	0.0556	0.0492	0.0492	0.0427	0.0427	0.0492	0.0750
45.0	0.0622	0.0622	0.0556	0.0556	0.0492		0.0556	0.1269
67.5	0.0750	0.0686	0.0816	0.0686	0.0556	0.0686		0.1010
112.5	0.0297	0.0556	0.0686	0.0622	0.0622	0.0556	0.0622	0.1010
135.0	-0.0155	0.0556	0.0686	0.0492	0.0622	0.0427	0.0750	0.1139
157.5	-0.0221	0.0622	0.0686	0.0622	0.0492	0.0361	0.0686	0.0750
180.0	-0.0416		0.0750	0.0622	0.0556	0.0361	0.0686	0.0622
202.5	0.0233	0.0686	0.0622	0.0556	0.0492	0.0427	0.0556	0.0750
225.0	0.0361	0.0622	0.0622	0.0556	0.0556	0.0492	0.0556	0.0880
247.5	0.0486	0.0552	0.0552	0.0552	0.0486	0.0486	0.0552	0.0616
292.5	0.0616	0.0552	0.0486	0.0486	0.0486	0.0486	0.0552	0.0680
315.0		0.0486	0.0552	0.0486	0.0486	0.0422	0.0552	0.1001
337.5	0.0552	0.0486	0.0422	0.0422	0.0486	0.0358	0.0552	
	$\alpha = 7.0°$							
0.0	0.0228	0.0098	0.0035	0.0164	0.0098	0.0035	0.0228	0.0357
22.5	0.0228	0.0228	0.0228	0.0164	0.0098	0.0164	0.0291	0.0550
45.0	0.0484	0.0484	0.0484	0.0421	0.0357		0.0357	0.1256
67.5	0.0743	0.0677	0.0807	0.0677	0.0550	0.0677		0.1063
112.5	0.0357	0.0421	0.0743	0.0550	0.0677	0.0550	0.0677	0.1063
135.0	-0.0544	0.0357	0.0614	0.0357	0.0550	0.0291	0.0677	0.1193
157.5	-0.1059	0.0291	0.0421	0.0357	0.0228	0.0035	0.0421	0.0484
180.0	-0.0994		0.0421	0.0291	0.0164	0.0035	0.0357	0.0291
202.5	0.0035	0.0484	0.0421	0.0357	0.0291	0.0164	0.0357	0.0550
225.0	0.0228	0.0421	0.0421	0.0421	0.0357	0.0421	0.0484	0.0677
247.5	0.0290	0.0417	0.0417	0.0417	0.0290	0.0354	0.0290	0.0417
292.5	0.0417	0.0354	0.0354	0.0290	0.0290	0.0290	0.0354	0.0483
315.0		0.0354	0.0354	0.0290	0.0354	0.0290	0.0417	0.0673
337.5	0.0290	0.0227	0.0162	0.0227	0.0290	0.0162	0.0354	
	$\alpha = 12.0°$							
0.0	-0.0095	-0.0222	-0.0288	-0.0158	-0.0158	-0.0351	-0.0029	-0.0029
22.5	-0.0095	-0.0029	-0.0029	-0.0095	-0.0222	-0.0095	0.0035	0.0228
45.0	0.0421	0.0421	0.0421	0.0421	0.0291		0.0291	0.1322
67.5	0.0807	0.0807	0.0936	0.0870	0.0743	0.0936		0.1256
112.5	0.0550	0.0228	0.0870	0.0807	0.0870	0.0743	0.0807	0.1193
135.0	-0.0481	-0.0351	0.0614	-0.0326	-0.0088	-0.0385	0.0032	0.0450
157.5	-0.2177	-0.0564	-0.0446	-0.0446	-0.0625	-0.0804	-0.0385	-0.0446
180.0	-0.1879		-0.0564	-0.0564	-0.0743	-0.0923	-0.0564	-0.0684
202.5	-0.0684	-0.0206	-0.0206	-0.0385	-0.0446	-0.0564	-0.0385	-0.0206
225.0	-0.0446	-0.0267	-0.0206	-0.0267	-0.0206	-0.0206	-0.0147	0.0032
247.5	-0.0027	0.0101	0.0165	0.0229	0.0037	0.0165	0.0165	0.0358
292.5	0.0037	0.0037	0.0037	0.0037	0.0037	0.0101	0.0101	0.0229
315.0		0.0294	0.0294	0.0294	0.0358	0.0294	0.0422	0.0744
337.5	0.0229	0.0229	0.0165	0.0229	0.0294	0.0165	0.0358	

TABLE V.- Concluded.

(f) $\phi = 90^{\circ}$; M = 1.03.

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=-0.1°							
0.0	-0.0217	-0.0217	-0.0217	-0.0285	-0.0418	-0.0352	0.0318	0.1190
22.5	-0.0285	-0.0217	0.0050	-0.0352	-0.0418	-0.0352	0.0318	0.1256
45.0	-0.0151	-0.0217	-0.0352	-0.0352	-0.0352		0.0318	0.1457
67.5	-0.0151	-0.0217	-0.0217	-0.0352	-0.0418	-0.0151		0.1323
112.5	-0.0619	-0.0619	-0.0352	-0.0352	-0.0285	-0.0285	0.0318	0.1323
135.0	-0.1156	-0.0553	-0.0285	-0.0418	-0.0217	-0.0352	0.0452	0.1457
157.5	-0.0820	-0.0352	-0.0151	-0.0151	-0.0285	-0.0352	0.0452	0.1190
180.0	-0.0820	0.0117	-0.0151	-0.0151	-0.0285	-0.0352	0.0452	0.1122
202.5	-0.1222	-0.0418	-0.0217	-0.0217	-0.0352	-0.0418	0.0318	0.1256
225.0	-0.0687	-0.0553	-0.0285	-0.0217	-0.0352	-0.0285	0.0318	0.1391
247.5	-0.0350	-0.0485	-0.0283	-0.0215	-0.0350	-0.0283	0.0187	0.1192
292.5	-0.0283	-0.0283	-0.0283	-0.0416	-0.0350	-0.0350	0.0253	0.1259
315.0		-0.0283	-0.0215	-0.0416	-0.0350	-0.0416	0.0320	0.1526
337.5	-0.0283	-0.0283	-0.0215	-0.0283	-0.0350	-0.0416	0.0320	
	α=1.9°							
0.0	-0.0285	-0.0285	-0.0353	-0.0353	-0.0485	-0.0285	0.0778	0.1311
22.5	-0.0353	-0.0285	-0.0020	-0.0485	-0.0485	-0.0285	0.0713	0.1311
45.0	-0.0220	-0.0285	-0.0419	-0.0485	-0.0485		0.0645	0.1643
67.5	-0.0154	-0.0220	-0.0353	-0.0419	-0.0419	-0.0154		0.1443
112.5	-0.0485	-0.0752	-0.0419	-0.0419	-0.0285	-0.0285	0.0645	0.1511
135.0	-0.1283	-0.0685	-0.0285	-0.0485	-0.0285	-0.0285	0.0778	0.1577
157.5	-0.1018	-0.0485	-0.0285	-0.0285	-0.0353	-0.0353	0.0778	0.1311
180.0	-0.0884		-0.0154	-0.0220	-0.0285	-0.0220	0.0844	0.1178
202.5	-0.1218	-0.0419	-0.0285	-0.0285	-0.0353	-0.0220	0.0778	0.1311
225.0	-0.0818	-0.0485	-0.0285	-0.0285	-0.0419	-0.0086	0.0844	0.1377
247.5	-0.0418	-0.0418	-0.0217	-0.0285	-0.0352	0.0117	0.0854	0.1256
292.5	-0.0217	-0.0285	-0.0285	-0.0418	-0.0285	-0.0016	0.0921	0.1323
315.0		-0.0285	-0.0217	-0.0352	-0.0285	-0.0084	0.0989	0.1592
337.5	-0.0217	-0.0217	-0.0285	-0.0352	-0.0352	-0.0151	0.0921	

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=3.9°							
0.0	-0.0418	-0.0352	-0.0418	-0.0418	-0.0553	-0.0553	0.0050	0.1122
22.5	-0.0418	-0.0352	-0.0084	-0.0486	-0.0553	-0.0418	-0.0217	0.1122
45.0	-0.0285	-0.0285	-0.0418	-0.0418	-0.0418		-0.0352	0.1592
67.5	-0.0084	-0.0084	-0.0217	-0.0352	-0.0352	-0.0151		0.1323
112.5	-0.0352	-0.0820	-0.0486	-0.0418	-0.0285	-0.0217	-0.0217	0.1323
135.0	-0.1222	-0.0820	-0.0352	-0.0553	-0.0217	-0.0352	-0.0016	0.1524
157.5	-0.1290	-0.0687	-0.0352	-0.0352	-0.0352	-0.0486	-0.0016	0.1122
180.0	-0.1089		-0.0285	-0.0285	-0.0285	-0.0486	0.0185	0.0989
202.5	-0.1290	-0.0486	-0.0352	-0.0352	-0.0418	-0.0418	0.0318	0.1190
225.0	-0.0955	-0.0486	-0.0352	-0.0352	-0.0418	-0.0285	0.0452	0.1256
247.5	-0.0484	-0.0418	-0.0284	-0.0284	-0.0351	-0.0149	0.0520	0.1123
292.5	-0.0284	-0.0351	-0.0351	-0.0351	-0.0351	-0.0218	0.0520	0.1057
315.0		-0.0351	-0.0284	-0.0418	-0.0351	-0.0351	0.0520	0.1392
337.5	-0.0351	-0.0351	-0.0351	-0.0418	-0.0418	-0.0484	0.0387	

TABLE VI.- BODY STATIC-PRESSURE ERROR COEFFICIENTS $(p - p_\infty)/p_\infty$ WITH BLEED AIR.

(a) $\phi = 90^\circ$; M = 0.70.

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station								$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8	1	2	3	4	5	6	7	8
	α=0°; w=0.018								α=8.0°; w=0.018							
0.0	-0.0061	-0.0061	-0.0061	-0.0015	-0.0015	-0.0015	0.0032	0.0078	-0.0245	-0.0245	-0.0245	-0.0245	-0.0199	-0.0245	-0.0199	-0.0153
22.5	-0.0061	-0.0061	0.0032	-0.0061	-0.0015	-0.0015	0.0032	0.0078	-0.0245	-0.0199	-0.0153	-0.0199	-0.0199	-0.0153	-0.0153	-0.0153
45.0	-0.0015	-0.0015	-0.0015	-0.0015	-0.0015		0.0032	0.0215	-0.0107	-0.0107	-0.0107	-0.0061	-0.0061		-0.0061	0.0261
67.5	-0.0061	-0.0061	-0.0015	-0.0015	-0.0015	0.0032		0.0078	0.0032	-0.0015	0.0032	0.0032	0.0032	0.0078		0.0215
112.5	-0.0061	-0.0107	-0.0061	-0.0015	-0.0015	-0.0015	0.0032	0.0124	-0.0015	-0.0061	-0.0015	-0.0015	0.0032	0.0032	0.0078	0.0215
135.0	-0.0107	-0.0061	-0.0015	-0.0061	-0.0015	-0.0061	0.0078	0.0215	-0.0199	-0.0153	-0.0061	-0.0107	-0.0015	-0.0107	0.0078	0.0215
157.5	-0.0061	-0.0015	-0.0015	-0.0015	-0.0015	-0.0061	0.0032	0.0032	-0.0475	-0.0245	-0.0199	-0.0153	-0.0199	-0.0245	-0.0107	-0.0153
180.0	-0.0153		-0.0061	-0.0015	-0.0015	-0.0061	0.0078	0.0032	-0.0429		-0.0199	-0.0199	-0.0199	-0.0290	-0.0153	-0.0199
202.5	-0.0153	-0.0061	-0.0061	-0.0015	-0.0015	-0.0061	0.0032	0.0078	-0.0290	-0.0199	-0.0153	-0.0153	-0.0153	-0.0199	-0.0153	-0.0107
225.0	-0.0153	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015	-0.0015	0.0170	-0.0199	-0.0153	-0.0107	-0.0107	-0.0153	-0.0107	-0.0061	0.0032
247.5	-0.0061	-0.0015	-0.0015	0.0031	-0.0015	0.0031	0.0031	0.0077	-0.0107	-0.0107	-0.0107	-0.0061	-0.0107	-0.0061	-0.0107	-0.0061
292.5	-0.0015	-0.0061	-0.0015	-0.0015	0.0031	0.0031	0.0031	0.0077	-0.0107	-0.0107	-0.0107	-0.0107	-0.0061	-0.0107	-0.0061	-0.0061
315.0		-0.0061	-0.0015	-0.0015	0.0031	-0.0015	0.0077	0.0261		-0.0107	-0.0107	-0.0107	-0.0061	-0.0107	-0.0061	0.0076
337.5	-0.0015	-0.0015	-0.0015	0.0031	0.0031	-0.0015	0.0077		-0.0198	-0.0198	-0.0198	-0.0153	-0.0153	-0.0198	-0.0107	
	α=2.0°; w=0.018								α=12.0°; w=0.018							
0.0	-0.0061	-0.0061	-0.0061	-0.0015	-0.0061	-0.0015	0.0031	0.0031	-0.0475	-0.0475	-0.0475	-0.0429	-0.0429	-0.0475	-0.0382	-0.0382
22.5	-0.0061	-0.0061	0.0031	-0.0061	-0.0015	-0.0015	0.0031	0.0076	-0.0382	-0.0382	-0.0290	-0.0382	-0.0382	-0.0336	-0.0290	-0.0336
45.0	-0.0061	-0.0015	-0.0061	-0.0015	-0.0015		0.0031	0.0260	-0.0107	-0.0153	-0.0153	-0.0107	-0.0107		-0.0107	0.0215
67.5	-0.0015	-0.0061	-0.0015	-0.0015	-0.0061	0.0031		0.0076	0.0124	0.0078	0.0124	0.0124	0.0078	0.0170		0.0307
112.5	-0.0107	-0.0107	-0.0061	-0.0061	-0.0015	-0.0015	-0.0015	0.0122	0.0078	0.0032	0.0078	0.0078	0.0124	0.0124	0.0170	0.0353
135.0	-0.0153	-0.0107	-0.0061	-0.0107	-0.0015	-0.0061	0.0076	0.0214	-0.0245	-0.0199	-0.0107	-0.0199	-0.0107	-0.0153	-0.0015	0.0170
157.5	-0.0153	-0.0061	-0.0061	-0.0015	-0.0061	-0.0107	0.0031	0.0031	-0.0659	-0.0475	-0.0382	-0.0336	-0.0336	-0.0429	-0.0290	-0.0336
180.0	-0.0153		-0.0061	-0.0015	-0.0015	-0.0061	0.0031	-0.0015	-0.0750		-0.0429	-0.0429	-0.0429	-0.0475	-0.0382	-0.0429
202.5	-0.0198	-0.0107	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015	0.0031	-0.0336	-0.0245	-0.0245	-0.0245	-0.0290	-0.0336	-0.0245	-0.0199
225.0	-0.0153	-0.0061	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015	0.0122	-0.0245	-0.0153	-0.0153	-0.0107	-0.0107	-0.0107	-0.0107	-0.0015
247.5	-0.0107	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015	-0.0015	0.0031	-0.0291	-0.0291	-0.0291	-0.0245	-0.0291	-0.0245	-0.0245	-0.0153
292.5	-0.0061	-0.0107	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015	0.0031	-0.0291	-0.0291	-0.0291	-0.0291	-0.0291	-0.0291	-0.0245	-0.0199
315.0		-0.0107	-0.0061	-0.0061	-0.0015	-0.0061	0.0031	0.0214		-0.0153	-0.0153	-0.0153	-0.0107	-0.0153	-0.0107	0.0031
337.5	-0.0061	-0.0107	-0.0061	-0.0061	-0.0015	-0.0061	0.0031		-0.0291	-0.0291	-0.0291	-0.0245	-0.0199	-0.0245	-0.0199	
	α=4.0°; w=0.018								α=15.0°; w=0.018							
0.0	-0.0061	-0.0107	-0.0107	-0.0061	-0.0061	-0.0061	-0.0015	0.0032	-0.0656	-0.0701	-0.0701	-0.0656	-0.0656	-0.0656	-0.0610	-0.0610
22.5	-0.0107	-0.0107	-0.0015	-0.0061	-0.0061	-0.0015	-0.0015	0.0032	-0.0610	-0.0610	-0.0519	-0.0610	-0.0564	-0.0519	-0.0519	-0.0610
45.0	-0.0061	-0.0061	-0.0061	-0.0015	-0.0015		0.0032	0.0261	-0.0243	-0.0243	-0.0243	-0.0243	-0.0243		-0.0198	0.0123
67.5	-0.0015	-0.0015	0.0032	-0.0015	-0.0015	0.0078		0.0170	0.0123	0.0077	0.0123	0.0123	0.0077	0.0169		0.0306
112.5	-0.0061	-0.0061	-0.0015	-0.0015	0.0032	-0.0015	0.0032	0.0170	0.0077	0.0032	0.0077	0.0077	0.0123	0.0123	0.0169	0.0351
135.0	-0.0153	-0.0107	-0.0061	-0.0107	-0.0015	-0.0061	0.0078	0.0215	-0.0335	-0.0289	-0.0243	-0.0289	-0.0198	-0.0243	-0.0107	0.0077
157.5	-0.0245	-0.0107	-0.0107	-0.0061	-0.0061	-0.0107	-0.0015	-0.0015	-0.0885	-0.0701	-0.0610	-0.0564	-0.0564	-0.0610	-0.0519	-0.0610
180.0	-0.0199		-0.0061	-0.0061	-0.0061	-0.0107	-0.0015	-0.0061	-0.0931		-0.0656	-0.0656	-0.0701	-0.0747	-0.0610	-0.0701
202.5	-0.0199	-0.0107	-0.0107	-0.0061	-0.0061	-0.0107	-0.0015	0.0032	-0.0473	-0.0289	-0.0335	-0.0426	-0.0426	-0.0473	-0.0380	-0.0335
225.0	-0.0153	-0.0107	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015	0.0124	-0.0289	-0.0243	-0.0198	-0.0198	-0.0198	-0.0198	-0.0243	-0.0107
247.5	-0.0061	-0.0061	-0.0061	-0.0015	-0.0061	-0.0015	-0.0015	0.0031	-0.0565	-0.0473	-0.0473	-0.0382	-0.0382	-0.0244	-0.0244	-0.0153
292.5	-0.0061	-0.0061	-0.0061	-0.0061	-0.0015	-0.0015	-0.0015	0.0031	-0.0519	-0.0519	-0.0473	-0.0427	-0.0382	-0.0382	-0.0336	-0.0290
315.0		-0.0061	-0.0061	-0.0061	-0.0015	-0.0061	0.0031	0.0168		-0.0244	-0.0198	-0.0244	-0.0198	-0.0244	-0.0153	-0.0061
337.5	-0.0107	-0.0107	-0.0107	-0.0061	-0.0015	-0.0061	-0.0015		-0.0382	-0.0336	-0.0336	-0.0336	-0.0290	-0.0336	-0.0290	

TABLE VI.- Continued.

(b) $\phi = 90^{\circ}$; M = 0.80.

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	$\alpha=0^{\circ}$; w=0.018							
0.0	-0.0068	-0.0068	-0.0068	-0.0018	-0.0068	-0.0018	0.0033	0.0083
22.5	-0.0068	-0.0068	0.0033	-0.0068	-0.0018	-0.0018	0.0033	0.0083
45.0	-0.0068	-0.0068	-0.0068	-0.0018	-0.0018		0.0033	0.0333
67.5	-0.0068	-0.0068	-0.0018	-0.0018	-0.0068	0.0033		0.0133
112.5	-0.0118	-0.0118	-0.0068	-0.0068	-0.0018	-0.0068	0.0033	0.0133
135.0	-0.0218	-0.0068	-0.0068	-0.0068	-0.0018	-0.0068	0.0083	0.0283
157.5	-0.0168	-0.0018	-0.0018	-0.0018	-0.0018	-0.0068	0.0033	0.0083
180.0	-0.0268		-0.0018	-0.0018	-0.0018	-0.0068	0.0083	0.0033
202.5	-0.0268	-0.0068	-0.0018	-0.0018	-0.0018	-0.0068	0.0033	0.0133
225.0	-0.0168	-0.0068	-0.0068	-0.0068	-0.0068	-0.0018	0.0033	0.0233
247.5	-0.0118	-0.0068	-0.0068	-0.0018	-0.0068	-0.0018	-0.0018	0.0083
292.5	-0.0118	-0.0118	-0.0068	-0.0068	-0.0068	-0.0018	-0.0018	0.0083
315.0		-0.0118	-0.0068	-0.0068	-0.0018	-0.0068	0.0033	0.0333
337.5	-0.0068	-0.0118	-0.0068	-0.0068	-0.0018	-0.0068	0.0033	

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	$\alpha=8.0^{\circ}$; w=0.018							
0.0	-0.0319	-0.0319	-0.0319	-0.0269	-0.0269	-0.0319	-0.0219	-0.0169
22.5	-0.0269	-0.0269	-0.0169	-0.0269	-0.0269	-0.0219	-0.0169	-0.0119
45.0	-0.0119	-0.0119	-0.0119	-0.0068	-0.0068		-0.0068	0.0383
67.5	0.0032	-0.0018	0.0082	0.0032	0.0032	0.0132		0.0283
112.5	-0.0018	-0.0068	-0.0018	0.0032	0.0082	0.0032	0.0082	0.0283
135.0	-0.0319	-0.0219	-0.0119	-0.0169	-0.0018	-0.0169	0.0082	0.0333
157.5	-0.0670	-0.0369	-0.0269	-0.0219	-0.0219	-0.0319	-0.0119	-0.0169
180.0	-0.0720		-0.0219	-0.0269	-0.0269	-0.0319	-0.0169	-0.0219
202.5	-0.0419	-0.0219	-0.0219	-0.0219	-0.0219	-0.0269	-0.0169	-0.0068
225.0	-0.0219	-0.0169	-0.0169	-0.0119	-0.0119	-0.0119	-0.0068	0.0032
247.5	-0.0168	-0.0168	-0.0118	-0.0118	-0.0168	-0.0118	-0.0168	-0.0118
292.5	-0.0168	-0.0168	-0.0118	-0.0118	-0.0118	-0.0118	-0.0118	-0.0068
315.0		-0.0168	-0.0168	-0.0168	-0.0118	-0.0168	-0.0068	0.0083
337.5	-0.0268	-0.0268	-0.0268	-0.0218	-0.0218	-0.0218	-0.0168	

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	$\alpha=2.0^{\circ}$; w=0.018							
0.0	-0.0018	-0.0069	-0.0069	-0.0018	-0.0018	-0.0018	0.0032	0.0084
22.5	-0.0069	-0.0069	0.0084	-0.0018	-0.0018	0.0032	0.0032	0.0134
45.0	-0.0018	-0.0018	-0.0018	-0.0018	0.0032		0.0032	0.0385
67.5	-0.0018	-0.0018	0.0032	0.0032	0.0032	0.0084		0.0184
112.5	-0.0069	-0.0069	-0.0018	-0.0018	0.0032	0.0032	0.0084	0.0234
135.0	-0.0169	-0.0069	-0.0018	-0.0069	0.0032	-0.0069	0.0134	0.0335
157.5	-0.0219	-0.0018	-0.0018	0.0032	-0.0018	-0.0069	0.0084	0.0084
180.0	-0.0269		0.0032	0.0032	0.0032	-0.0018	0.0084	0.0084
202.5	-0.0219	-0.0069	-0.0018	-0.0018	-0.0018	-0.0069	0.0032	0.0134
225.0	-0.0119	-0.0069	-0.0018	-0.0018	-0.0018	-0.0018	0.0032	0.0234
247.5	-0.0069	-0.0069	-0.0018	-0.0018	-0.0018	0.0032	-0.0018	0.0084
292.5	-0.0069	-0.0069	-0.0069	-0.0018	-0.0018	-0.0018	0.0032	0.0084
315.0		-0.0069	-0.0018	-0.0018	-0.0018	-0.0018	0.0032	0.0335
337.5	-0.0069	-0.0069	-0.0069	-0.0018	-0.0018	-0.0018	0.0032	

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	$\alpha=12.0^{\circ}$; w=0.018							
0.0	-0.0572	-0.0623	-0.0623	-0.0572	-0.0572	-0.0572	-0.0522	-0.0472
22.5	-0.0572	-0.0522	-0.0370	-0.0522	-0.0522	-0.0422	-0.0370	-0.0422
45.0	-0.0219	-0.0219	-0.0169	-0.0169	-0.0119	0.0032	-0.0119	0.0335
67.5	0.0134	0.0084	0.0184	0.0134	0.0084	0.0184	0.0638	0.0385
112.5	0.0032	-0.0018	0.0084	0.0084	0.0184	0.0134	0.0184	0.0435
135.0	-0.0370	-0.0320	-0.0169	-0.0219	-0.0119	-0.0219	0.0032	0.0234
157.5	-0.0976	-0.0673	-0.0472	-0.0422	-0.0472	-0.0522	-0.0370	-0.0422
180.0	-0.1227	-0.0269	-0.0522	-0.0522	-0.0522	-0.0623	-0.0472	-0.0522
202.5	-0.0472	-0.0269	-0.0269	-0.0320	-0.0370	-0.0422	-0.0320	-0.0219
225.0	-0.0320	-0.0219	-0.0169	-0.0169	-0.0119	-0.0119	-0.0119	0.0032
247.5	-0.0422	-0.0370	-0.0370	-0.0320	-0.0370	-0.0320	-0.0320	-0.0219
292.5	-0.0422	-0.0422	-0.0370	-0.0422	-0.0370	-0.0370	-0.0370	-0.0269
315.0		-0.0219	-0.0219	-0.0219	-0.0169	-0.0169	-0.0119	0.0032
337.5	-0.0370	-0.0370	-0.0370	-0.0320	-0.0269	-0.0320	-0.0269	

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	$\alpha=4.0^{\circ}$; w=0.018							
0.0	-0.0119	-0.0169	-0.0169	-0.0119	-0.0119	-0.0119	-0.0018	0.0032
22.5	-0.0119	-0.0119	-0.0018	-0.0119	-0.0119	-0.0069	-0.0018	0.0032
45.0	-0.0069	-0.0069	-0.0069	-0.0069	-0.0018		-0.0018	0.0335
67.5	-0.0018	-0.0069	0.0032	-0.0018	-0.0018	0.0084		0.0184
112.5	-0.0119	-0.0119	-0.0069	-0.0018	-0.0018	-0.0018	0.0032	0.0234
135.0	-0.0219	-0.0169	-0.0069	-0.0119	-0.0018	-0.0119	0.0084	0.0285
157.5	-0.0370	-0.0169	-0.0119	-0.0069	-0.0119	-0.0119	0.0032	0.0032
180.0	-0.0422		-0.0069	-0.0069	-0.0069	-0.0119	-0.0018	-0.0018
202.5	-0.0269	-0.0119	-0.0069	-0.0119	-0.0069	-0.0169	-0.0018	0.0084
225.0	-0.0169	-0.0119	-0.0069	-0.0069	-0.0069	-0.0069	-0.0018	0.0134
247.5	-0.0119	-0.0069	-0.0069	-0.0018	-0.0018	-0.0018	-0.0018	0.0032
292.5	-0.0069	-0.0069	-0.0069	-0.0069	-0.0018	-0.0018	0.0032	0.0082
315.0		-0.0069	-0.0069	-0.0069	-0.0018	-0.0069	0.0032	0.0284
337.5	-0.0119	-0.0119	-0.0119	-0.0069	-0.0018	-0.0069	0.0032	

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	$\alpha=15.0^{\circ}$; w=0.018							
0.0	-0.0825	-0.0825	-0.0825	-0.0773	-0.0773	-0.0825	-0.0723	-0.0723
22.5	-0.0723	-0.0723	-0.0572	-0.0723	-0.0723	-0.0623	-0.0572	-0.0673
45.0	-0.0269	-0.0269	-0.0269	-0.0219	-0.0219		-0.0169	0.0285
67.5	0.0184	0.0184	0.0234	0.0184	0.0184	0.0285		0.0537
112.5	0.0134	0.0084	0.0184	0.0184	0.0234	0.0234	0.0285	0.0537
135.0	-0.0422	-0.0370	-0.0219	-0.0269	-0.0169	-0.0269	-0.0069	0.0184
157.5	-0.1227	-0.0875	-0.0723	-0.0673	-0.0673	-0.0773	-0.0572	-0.0673
180.0	-0.1430		-0.0773	-0.0773	-0.0773	-0.0875	-0.0723	-0.0825
202.5	-0.0572	-0.0269	-0.0320	-0.0472	-0.0522	-0.0522	-0.0422	-0.0320
225.0	-0.0370	-0.0269	-0.0169	-0.0169	-0.0169	-0.0219	-0.0169	-0.0069
247.5	-0.0720	-0.0570	-0.0520	-0.0419	-0.0419	-0.0269	-0.0269	-0.0119
292.5	-0.0670	-0.0620	-0.0570	-0.0520	-0.0470	-0.0419	-0.0419	-0.0269
315.0		-0.0319	-0.0269	-0.0269	-0.0269	-0.0269	-0.0219	-0.0018
337.5	-0.0419	-0.0419	-0.0419	-0.0369	-0.0319	-0.0369	-0.0319	

TABLE VI.- Continued.

(c) $\phi = 90^{\circ}$; M = 0.90.

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	$\alpha=0^{\circ}$; w=0.018							
0.0	-0.0052	-0.0108	-0.0108	0.0003	0.0003	0.0003	0.0115	0.0170
22.5	-0.0052	-0.0052	0.0115	-0.0052	-0.0052	0.0003	0.0059	0.0228
45.0	-0.0052	-0.0052	-0.0052	0.0003	0.0003		0.0059	0.0451
67.5	-0.0052	-0.0052	0.0003	0.0003	-0.0052	0.0059		0.0228
112.5	-0.0164	-0.0164	-0.0052	-0.0052	0.0003	-0.0052	0.0059	0.0284
135.0	-0.0275	-0.0108	0.0003	-0.0052	0.0003	-0.0052	0.0170	0.0451
157.5	-0.0388	0.0003	0.0003	0.0059	0.0003	-0.0052	0.0115	0.0170
180.0	-0.0500		0.0003	0.0059	0.0003	-0.0052	0.0170	0.0115
202.5	-0.0388	-0.0108	0.0003	0.0003	0.0003	-0.0052	0.0059	0.0228
225.0	-0.0219	-0.0108	-0.0052	-0.0052	-0.0052	0.0003	0.0059	0.0339
247.5	-0.0107	-0.0051	0.0005	0.0061	0.0005	0.0061	0.0061	0.0229
292.5	-0.0051	-0.0051	0.0005	-0.0051	0.0061	0.0061	0.0117	0.0229
315.0		-0.0051	0.0005	0.0005	0.0061	0.0005	0.0173	0.0508
337.5	0.0005	-0.0051	-0.0051	0.0005	0.0061	0.0005	0.0173	
	$\alpha=1.9^{\circ}$; w=0.018							
0.0	-0.0052	-0.0108	-0.0108	-0.0052	-0.0052	-0.0052	0.0059	0.0170
22.5	-0.0108	-0.0108	0.0059	-0.0052	-0.0052	0.0003	0.0059	0.0170
45.0	-0.0052	-0.0052	-0.0052	-0.0052	-0.0052		0.0059	0.0506
67.5	-0.0052	-0.0052	0.0059	0.0003	-0.0052	0.0115		0.0284
112.5	-0.0164	-0.0164	-0.0052	-0.0052	0.0059	0.0003	0.0115	0.0339
135.0	-0.0332	-0.0164	0.0003	-0.0108	0.0059	-0.0052	0.0170	0.0451
157.5	-0.0444	-0.0052	0.0003	0.0003	0.0003	-0.0108	0.0115	0.0170
180.0	-0.0611		0.0003	0.0003	0.0003	-0.0052	0.0115	0.0059
202.5	-0.0388	-0.0108	-0.0052	-0.0052	-0.0052	-0.0108	0.0059	0.0170
225.0	-0.0219	-0.0108	-0.0052	-0.0052	-0.0052	-0.0052	0.0003	0.0284
247.5	-0.0165	-0.0054	-0.0054	0.0002	-0.0054	0.0002	0.0002	0.0113
292.5	-0.0054	-0.0109	-0.0054	-0.0054	0.0002	0.0002	0.0057	0.0168
315.0		-0.0109	-0.0054	-0.0054	0.0057	-0.0054	0.0113	0.0446
337.5	-0.0054	-0.0109	-0.0054	0.0002	0.0002	-0.0054	0.0113	
	$\alpha=4.0^{\circ}$; w=0.018							
0.0	-0.0051	-0.0107	-0.0107	-0.0051	-0.0051	-0.0051	0.0061	0.0117
22.5	-0.0107	-0.0107	0.0061	-0.0107	-0.0051	0.0005	0.0061	0.0173
45.0	-0.0051	-0.0051	-0.0051	0.0005	0.0005		0.0061	0.0567
67.5	0.0061	0.0005	0.0117	0.0061	0.0005	0.0173		0.0343
112.5	-0.0107	-0.0107	0.0005	0.0005	0.0061	0.0005	0.0117	0.0399
135.0	-0.0333	-0.0163	0.0005	-0.0107	0.0061	-0.0051	0.0229	0.0511
157.5	-0.0557	-0.0107	-0.0051	0.0005	0.0005	-0.0107	0.0117	0.0173
180.0	-0.0783		0.0005	0.0005	0.0005	-0.0107	0.0117	0.0061
202.5	-0.0389	-0.0107	0.0005	-0.0051	-0.0051	-0.0107	0.0061	0.0173
225.0	-0.0219	-0.0107	-0.0051	-0.0051	-0.0051	0.0005	0.0061	0.0287
247.5	-0.0051	0.0005	0.0005	0.0061	0.0005	0.0117	0.0061	0.0173
292.5	0.0005	-0.0051	0.0005	0.0005	0.0061	0.0061	0.0117	0.0229
315.0		-0.0051	0.0005	0.0005	0.0061	0.0005	0.0173	0.0455
337.5	-0.0051	-0.0107	-0.0051	0.0005	0.0005	-0.0051	0.0117	

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	$\alpha=8.0^{\circ}$; w=0.018							
0.0	-0.0332	-0.0388	-0.0388	-0.0275	-0.0275	-0.0332	-0.0164	-0.0108
22.5	-0.0332	-0.0275	-0.0108	-0.0275	-0.0275	-0.0164	-0.0108	-0.0052
45.0	-0.0108	-0.0108	-0.0052	-0.0052	-0.0108		0.0003	0.0562
67.5	0.0059	0.0059	0.0170	0.0115	0.0059	0.0228		0.0451
112.5	-0.0052	-0.0108	0.0059	0.0059	0.0170	0.0115	0.0170	0.0451
135.0	-0.0444	-0.0275	-0.0052	-0.0164	0.0003	-0.0164	0.0170	0.0506
157.5	-0.0947	-0.0388	-0.0219	-0.0164	-0.0219	-0.0332	-0.0052	-0.0052
180.0	-0.1170		-0.0164	-0.0219	-0.0219	-0.0332	-0.0108	-0.0164
202.5	-0.0500	-0.0219	-0.0164	-0.0164	-0.0164	-0.0219	-0.0108	0.0003
225.0	-0.0275	-0.0108	-0.0108	-0.0108	-0.0108	-0.0052	0.0003	0.0170
247.5	-0.0166	-0.0110	-0.0054	-0.0054	-0.0110	-0.0054	-0.0054	0.0002
292.5	-0.0110	-0.0110	-0.0054	-0.0110	-0.0054	-0.0054	-0.0054	0.0058
315.0		-0.0110	-0.0110	-0.0054	-0.0054	-0.0054	0.0002	0.0225
337.5	-0.0278	-0.0278	-0.0278	-0.0222	-0.0110	-0.0222	-0.0054	
	$\alpha=12.0^{\circ}$; w=0.018							
0.0	-0.0670	-0.0726	-0.0726	-0.0614	-0.0614	-0.0614	-0.0502	-0.0446
22.5	-0.0614	-0.0558	-0.0390	-0.0558	-0.0558	-0.0446	-0.0390	-0.0334
45.0	-0.0165	-0.0221	-0.0165	-0.0165	-0.0165	0.0115	-0.0109	0.0565
67.5	0.0171	0.0171	0.0285	0.0227	0.0171	0.0341	0.0903	0.0621
112.5	0.0059	0.0003	0.0171	0.0171	0.0285	0.0227	0.0341	0.0621
135.0	-0.0614	-0.0390	-0.0109	-0.0221	-0.0053	-0.0278	0.0115	0.0453
157.5	-0.1402	-0.0840	-0.0558	-0.0446	-0.0502	-0.0614	-0.0278	-0.0390
180.0	-0.1796	-0.0334	-0.0558	-0.0502	-0.0558	-0.0726	-0.0446	-0.0558
202.5	-0.0614	-0.0221	-0.0221	-0.0278	-0.0334	-0.0446	-0.0278	-0.0165
225.0	-0.0334	-0.0165	-0.0165	-0.0109	-0.0053	-0.0053	-0.0053	0.0115
247.5	-0.0554	-0.0442	-0.0442	-0.0330	-0.0442	-0.0330	-0.0330	-0.0163
292.5	-0.0442	-0.0498	-0.0442	-0.0442	-0.0386	-0.0386	-0.0330	-0.0218
315.0		-0.0218	-0.0163	-0.0163	-0.0107	-0.0163	-0.0051	0.0173
337.5	-0.0386	-0.0442	-0.0386	-0.0330	-0.0218	-0.0330	-0.0163	
	$\alpha=14.9^{\circ}$; w=0.017							
0.0	-0.0947	-0.1003	-0.1003	-0.0891	-0.0835	-0.0947	-0.0778	-0.0778
22.5	-0.0891	-0.0835	-0.0667	-0.0835	-0.0835	-0.0722	-0.0611	-0.0667
45.0	-0.0275	-0.0275	-0.0275	-0.0219	-0.0219		-0.0164	0.0506
67.5	0.0284	0.0284	0.0339	0.0339	0.0284	0.0451		0.0786
112.5	0.0170	0.0059	0.0284	0.0284	0.0339	0.0339	0.0395	0.0786
135.0	-0.0667	-0.0555	-0.0219	-0.0332	-0.0164	-0.0332	0.0059	0.0451
157.5	-0.1728	-0.1170	-0.0778	-0.0722	-0.0722	-0.0891	-0.0611	-0.0722
180.0	-0.2064		-0.0835	-0.0835	-0.0891	-0.1003	-0.0778	-0.0891
202.5	-0.0722	-0.0219	-0.0219	-0.0444	-0.0500	-0.0500	-0.0388	-0.0219
225.0	-0.0444	-0.0219	-0.0164	-0.0108	-0.0164	-0.0108	-0.0108	0.0059
247.5	-0.0780	-0.0613	-0.0557	-0.0389	-0.0389	-0.0222	-0.0222	-0.0054
292.5	-0.0725	-0.0669	-0.0557	-0.0557	-0.0445	-0.0389	-0.0334	-0.0166
315.0		-0.0278	-0.0222	-0.0222	-0.0166	-0.0222	-0.0110	0.0113
337.5	-0.0389	-0.0389	-0.0389	-0.0334	-0.0278	-0.0334	-0.0222	

TABLE VI.- Continued.

(d) $\phi = 90^0$; M = 0.95

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	$\alpha=0°$; w=0.018							
0.0	-0.0029	-0.0029	-0.0029	0.0030	0.0030	0.0030	0.0207	0.0326
22.5	-0.0029	-0.0029	0.0148	-0.0029	0.0030	0.0089	0.0148	0.0326
45.0	-0.0029	-0.0029	-0.0029	0.0030	0.0030		0.0148	0.0620
67.5	-0.0029	-0.0029	0.0089	0.0030	0.0030	0.0148		0.0385
112.5	-0.0205	-0.0087	0.0030	0.0030	0.0089	0.0030	0.0148	0.0444
135.0	-0.0324	-0.0087	0.0030	-0.0029	0.0089	-0.0029	0.0267	0.0561
157.5	-0.0501	0.0089	0.0089	0.0148	0.0089	-0.0029	0.0207	0.0326
180.0	-0.0677		0.0089	0.0089	0.0089	0.0030	0.0267	0.0207
202.5	-0.0442	-0.0087	0.0030	0.0030	0.0030	-0.0029	0.0148	0.0326
225.0	-0.0264	-0.0029	-0.0029	0.0030	0.0030	0.0030	0.0148	0.0502
247.5	-0.0144	-0.0027	0.0032	0.0091	0.0032	0.0091	0.0091	0.0328
292.5	-0.0027	-0.0086	-0.0027	-0.0027	0.0091	0.0091	0.0150	0.0328
315.0		-0.0086	0.0032	0.0032	0.0091	0.0032	0.0209	0.0622
337.5	-0.0027	-0.0086	-0.0027	0.0032	0.0091	0.0032	0.0209	
	$\alpha=2.0°$; w=0.018							
0.0	0.0030	-0.0029	-0.0029	0.0090	0.0090	0.0090	0.0208	0.0328
22.5	-0.0029	-0.0029	0.0149	0.0030	0.0030	0.0090	0.0208	0.0387
45.0	0.0030	0.0030	0.0030	0.0090	0.0090		0.0149	0.0683
67.5	0.0030	0.0030	0.0149	0.0090	0.0090	0.0208		0.0446
112.5	-0.0147	-0.0029	0.0090	0.0090	0.0149	0.0090	0.0208	0.0505
135.0	-0.0326	-0.0029	0.0090	0.0030	0.0149	0.0030	0.0328	0.0624
157.5	-0.0504	0.0030	0.0149	0.0149	0.0090	0.0030	0.0267	0.0328
180.0	-0.0740		0.0149	0.0149	0.0090	0.0030	0.0267	0.0267
202.5	-0.0385	0.0030	0.0090	0.0090	0.0090	0.0030	0.0149	0.0387
225.0	-0.0206	0.0030	0.0030	0.0090	0.0090	0.0090	0.0208	0.0505
247.5	-0.0088	0.0030	0.0030	0.0089	0.0030	0.0148	0.0148	0.0266
292.5	-0.0029	-0.0029	0.0030	0.0030	0.0089	0.0089	0.0148	0.0325
315.0		-0.0088	0.0030	0.0030	0.0148	0.0030	0.0207	0.0620
337.5	0.0030	-0.0029	-0.0029	0.0030	0.0089	0.0030	0.0207	
	$\alpha=4.0°$; w=0.018							
0.0	-0.0087	-0.0087	-0.0146	-0.0029	-0.0029	-0.0029	0.0089	0.0207
22.5	-0.0087	-0.0087	0.0089	-0.0087	-0.0029	0.0030	0.0089	0.0267
45.0	-0.0029	-0.0029	-0.0029	0.0030	0.0030		0.0089	0.0738
67.5	0.0030	0.0030	0.0148	0.0089	0.0030	0.0207		0.0502
112.5	-0.0205	-0.0087	0.0089	0.0030	0.0089	0.0030	0.0207	0.0502
135.0	-0.0501	-0.0146	0.0030	-0.0087	0.0089	-0.0029	0.0267	0.0620
157.5	-0.0677	-0.0146	0.0030	0.0030	0.0030	-0.0087	0.0148	0.0267
180.0	-0.1032		0.0089	0.0030	0.0030	-0.0087	0.0207	0.0148
202.5	-0.0442	-0.0029	0.0030	-0.0029	0.0030	-0.0029	0.0148	0.0326
225.0	-0.0264	-0.0029	-0.0029	0.0030	0.0030	0.0030	0.0089	0.0385
247.5	-0.0147	-0.0029	0.0030	0.0089	0.0030	0.0089	0.0148	0.0207
292.5	-0.0029	-0.0029	-0.0029	0.0030	0.0089	0.0089	0.0148	0.0266
315.0		-0.0088	-0.0029	0.0030	0.0089	0.0030	0.0148	0.0502
337.5	-0.0088	-0.0147	-0.0088	-0.0029	0.0030	-0.0029	0.0148	

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	$\alpha=8.0°$; w=0.018							
0.0	-0.0324	-0.0384	-0.0384	-0.0265	-0.0265	-0.0324	-0.0086	-0.0027
22.5	-0.0324	-0.0265	-0.0086	-0.0265	-0.0265	-0.0204	-0.0086	0.0091
45.0	-0.0086	-0.0086	-0.0027	-0.0027	-0.0027		0.0032	0.0803
67.5	0.0091	0.0091	0.0210	0.0151	0.0091	0.0269		0.0626
112.5	-0.0204	-0.0086	0.0151	0.0091	0.0210	0.0151	0.0269	0.0626
135.0	-0.0918	-0.0265	0.0032	-0.0145	0.0091	-0.0145	0.0330	0.0685
157.5	-0.1214	-0.0384	-0.0145	-0.0086	-0.0145	-0.0324	0.0091	0.0091
180.0	-0.1452		-0.0086	-0.0145	-0.0204	-0.0324	-0.0027	-0.0086
202.5	-0.0502	-0.0145	-0.0086	-0.0086	-0.0086	-0.0145	-0.0027	0.0151
225.0	-0.0265	-0.0086	-0.0027	-0.0027	-0.0027	0.0032	0.0091	0.0330
247.5	-0.0147	-0.0029	0.0031	0.0090	-0.0029	0.0031	0.0031	0.0149
292.5	-0.0029	-0.0029	-0.0029	-0.0029	0.0031	0.0031	0.0090	0.0149
315.0		-0.0088	-0.0029	-0.0029	0.0031	0.0031	0.0149	0.0387
337.5	-0.0207	-0.0266	-0.0207	-0.0147	-0.0029	-0.0147	0.0031	
	$\alpha=12.0°$; w=0.018							
0.0	-0.0679	-0.0739	-0.0739	-0.0620	-0.0561	-0.0620	-0.0443	-0.0443
22.5	-0.0679	-0.0620	-0.0384	-0.0561	-0.0561	-0.0443	-0.0324	-0.0265
45.0	-0.0145	-0.0204	-0.0145	-0.0086	-0.0145		-0.0027	0.0803
67.5	0.0269	0.0210	0.0330	0.0269	0.0210	0.0448		0.0803
112.5	0.0091	-0.0086	0.0269	0.0210	0.0389	0.0330	0.0448	0.0803
135.0	-0.0977	-0.0561	-0.0027	-0.0204	0.0032	-0.0204	0.0210	0.0685
157.5	-0.1807	-0.0800	-0.0502	-0.0384	-0.0443	-0.0620	-0.0204	-0.0265
180.0	-0.2105		-0.0502	-0.0443	-0.0502	-0.0679	-0.0384	-0.0443
202.5	-0.0620	-0.0204	-0.0145	-0.0204	-0.0265	-0.0384	-0.0204	-0.0027
225.0	-0.0324	-0.0145	-0.0086	-0.0027	0.0032	0.0032	0.0091	0.0269
247.5	-0.0504	-0.0385	-0.0325	-0.0207	-0.0325	-0.0147	-0.0207	0.0031
292.5	-0.0385	-0.0385	-0.0325	-0.0325	-0.0266	-0.0266	-0.0207	-0.0029
315.0		-0.0147	-0.0088	-0.0088	-0.0029	-0.0029	0.0090	0.0327
337.5	-0.0325	-0.0325	-0.0325	-0.0207	-0.0147	-0.0207	-0.0029	
	$\alpha=15.0°$; w=0.017							
0.0	-0.1036	-0.1095	-0.1036	-0.0918	-0.0859	-0.0918	-0.0679	-0.0739
22.5	-0.1036	-0.0859	-0.0620	-0.0859	-0.0800	-0.0679	-0.0561	-0.0561
45.0	-0.0265	-0.0265	-0.0204	-0.0145	-0.0204		-0.0086	0.0803
67.5	0.0389	0.0330	0.0448	0.0448	0.0389	0.0626		0.0982
112.5	0.0269	0.0032	0.0330	0.0330	0.0507	0.0448	0.0626	0.0982
135.0	-0.0800	-0.0800	-0.0145	-0.0324	-0.0027	-0.0265	0.0151	0.0626
157.5	-0.2046	-0.1273	-0.0739	-0.0620	-0.0739	-0.0859	-0.0443	-0.0561
180.0	-0.2461		-0.0800	-0.0739	-0.0859	-0.0977	-0.0620	-0.0800
202.5	-0.0859	-0.0145	-0.0145	-0.0324	-0.0384	-0.0384	-0.0265	-0.0086
225.0	-0.0384	-0.0145	-0.0027	0.0032	-0.0027	-0.0027	0.0032	0.0210
247.5	-0.0675	-0.0499	-0.0440	-0.0323	-0.0381	-0.0144	-0.0144	0.0032
292.5	-0.0675	-0.0675	-0.0499	-0.0499	-0.0381	-0.0381	-0.0323	-0.0144
315.0		-0.0323	-0.0262	-0.0203	-0.0144	-0.0203	-0.0086	0.0209
337.5	-0.0440	-0.0440	-0.0440	-0.0325	-0.0205	-0.0264	-0.0147	

TABLE VI.- Continued.

(e) $\phi = 90^0$; M = 1.00.

θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=0°; w=0.018							
0.0	0.0610	0.0546	0.0481	0.0546	0.0417	0.0417	0.0610	0.0801
22.5	0.0610	0.0546	0.0674	0.0481	0.0417	0.0481	0.0546	0.0801
45.0	0.0610	0.0546	0.0546	0.0481	0.0481		0.0546	0.1121
67.5	0.0610	0.0610	0.0610	0.0546	0.0417	0.0546		0.0801
112.5	0.0417	0.0481	0.0546	0.0481	0.0546	0.0417	0.0546	0.0865
135.0	0.0226	0.0546	0.0610	0.0481	0.0546	0.0353	0.0674	0.1056
157.5	0.0162	0.0674	0.0674	0.0610	0.0546	0.0417	0.0674	0.0801
180.0	0.0035		0.0610	0.0610	0.0546	0.0417	0.0674	0.0674
202.5	0.0162	0.0546	0.0610	0.0546	0.0481	0.0417	0.0546	0.0801
225.0	0.0353	0.0546	0.0546	0.0481	0.0481	0.0481	0.0546	0.0992
247.5	0.0421	0.0550	0.0550	0.0550	0.0421	0.0485	0.0485	0.0741
292.5	0.0614	0.0550	0.0550	0.0485	0.0485	0.0485	0.0550	0.0805
315.0		0.0485	0.0550	0.0485	0.0550	0.0421	0.0614	0.1126
337.5	0.0614	0.0485	0.0485	0.0485	0.0550	0.0421	0.0614	
	α=2.0°; w=0.018							
0.0	0.0610	0.0546	0.0481	0.0481	0.0417	0.0417	0.0610	0.0737
22.5	0.0610	0.0546	0.0674	0.0481	0.0417	0.0481	0.0546	0.0801
45.0	0.0610	0.0610	0.0546	0.0481	0.0481		0.0546	0.1121
67.5	0.0674	0.0674	0.0674	0.0546	0.0417	0.0610		0.0865
112.5	0.0417	0.0481	0.0610	0.0546	0.0546	0.0417	0.0610	0.0992
135.0	0.0162	0.0546	0.0610	0.0481	0.0546	0.0353	0.0737	0.1056
157.5	0.0098	0.0610	0.0610	0.0610	0.0481	0.0353	0.0610	0.0737
180.0	-0.0095		0.0674	0.0610	0.0481	0.0353	0.0674	0.0674
202.5	0.0162	0.0546	0.0610	0.0481	0.0481	0.0353	0.0546	0.0801
225.0	0.0353	0.0546	0.0546	0.0481	0.0417	0.0481	0.0546	0.0928
247.5	0.0417	0.0546	0.0546	0.0546	0.0417	0.0481	0.0481	0.0674
292.5	0.0546	0.0481	0.0481	0.0417	0.0481	0.0417	0.0481	0.0674
315.0		0.0481	0.0546	0.0417	0.0481	0.0353	0.0610	0.1056
337.5	0.0610	0.0481	0.0481	0.0481	0.0481	0.0353	0.0610	
	α=4.0°; w=0.018							
0.0	0.0481	0.0417	0.0353	0.0417	0.0353	0.0290	0.0481	0.0674
22.5	0.0481	0.0481	0.0546	0.0353	0.0353	0.0353	0.0481	0.0737
45.0	0.0546	0.0546	0.0481	0.0481	0.0417		0.0481	0.1249
67.5	0.0674	0.0610	0.0674	0.0546	0.0417	0.0610		0.0928
112.5	0.0290	0.0481	0.0610	0.0481	0.0546	0.0417	0.0610	0.0992
135.0	-0.0095	0.0481	0.0610	0.0417	0.0546	0.0290	0.0674	0.1121
157.5	-0.0158	0.0481	0.0546	0.0546	0.0417	0.0226	0.0610	0.0674
180.0	-0.0349		0.0610	0.0546	0.0417	0.0290	0.0610	0.0546
202.5	0.0098	0.0481	0.0546	0.0417	0.0417	0.0290	0.0481	0.0737
225.0	0.0290	0.0481	0.0481	0.0481	0.0417	0.0417	0.0546	0.0801
247.5	0.0420	0.0548	0.0548	0.0548	0.0420	0.0484	0.0548	0.0676
292.5	0.0548	0.0484	0.0484	0.0420	0.0484	0.0484	0.0548	0.0676
315.0		0.0484	0.0484	0.0420	0.0484	0.0420	0.0548	0.0932
337.5	0.0548	0.0420	0.0420	0.0420	0.0484	0.0356	0.0548	

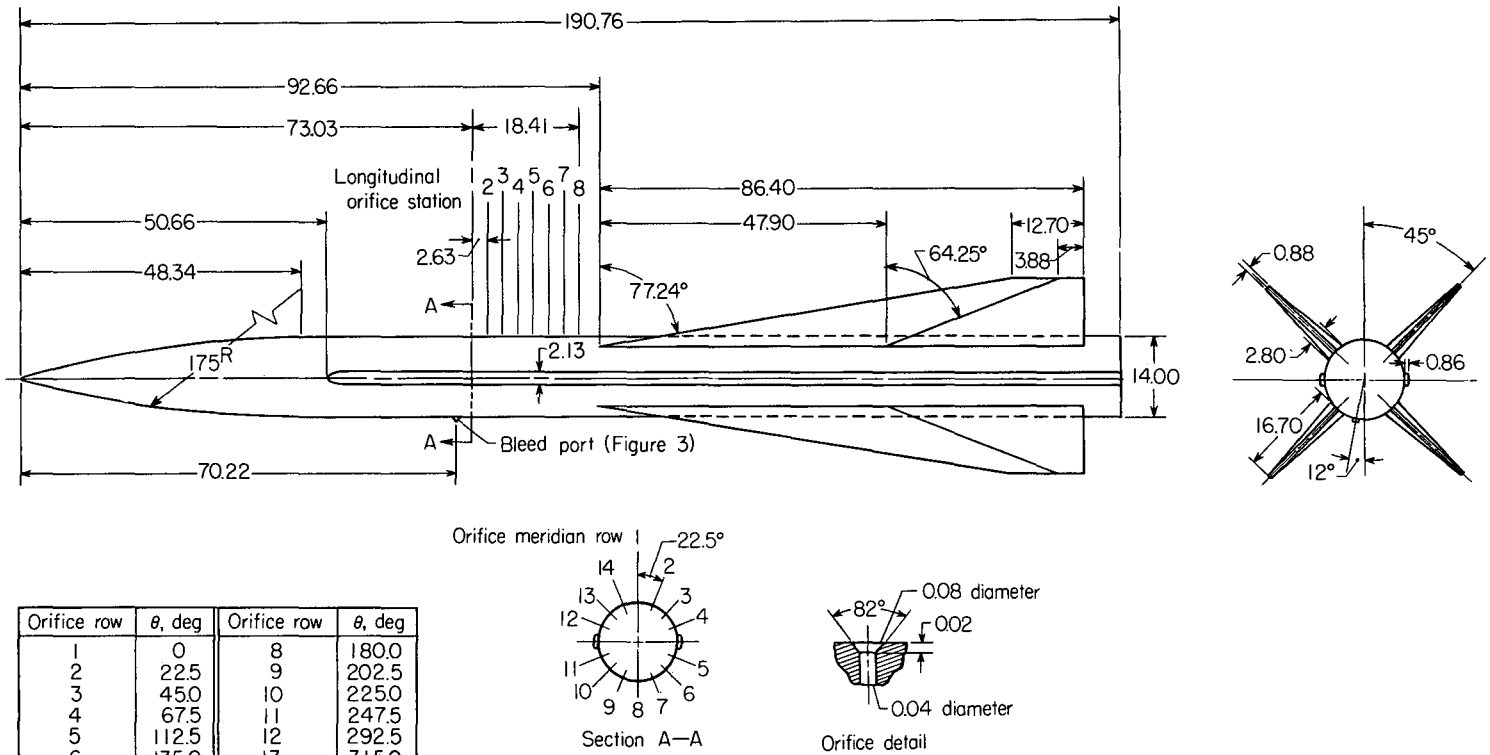
θ, deg	$(p - p_\infty)/p_\infty$ for longitudinal station							
	1	2	3	4	5	6	7	8
	α=8.0°; w=0.018							
0.0	0.0226	0.0162	0.0098	0.0162	0.0098	0.0035	0.0290	0.0353
22.5	0.0290	0.0290	0.0417	0.0162	0.0098	0.0162	0.0290	0.0546
45.0	0.0546	0.0481	0.0481	0.0481	0.0290		0.0353	0.1312
67.5	0.0737	0.0674	0.0801	0.0674	0.0546	0.0737		0.1056
112.5	0.0353	0.0417	0.0737	0.0546	0.0674	0.0546	0.0674	0.1056
135.0	-0.0540	0.0290	0.0610	0.0290	0.0546	0.0226	0.0674	0.1185
157.5	-0.0797	0.0162	0.0353	0.0353	0.0226	-0.0029	0.0481	0.0481
180.0	-0.0861		0.0417	0.0290	0.0162	-0.0029	0.0353	0.0290
202.5	0.0035	0.0417	0.0417	0.0353	0.0290	0.0162	0.0353	0.0546
225.0	0.0226	0.0417	0.0417	0.0417	0.0353	0.0417	0.0481	0.0674
247.5	0.0293	0.0421	0.0421	0.0421	0.0357	0.0421	0.0357	0.0485
292.5	0.0421	0.0421	0.0421	0.0357	0.0357	0.0357	0.0421	0.0485
315.0		0.0421	0.0421	0.0357	0.0421	0.0357	0.0485	0.0741
337.5	0.0357	0.0293	0.0230	0.0293	0.0357	0.0230	0.0421	
	α=12.0°; w=0.018							
0.0	-0.0095	-0.0158	-0.0286	-0.0158	-0.0158	-0.0349	-0.0029	-0.0095
22.5	-0.0095	-0.0029	0.0162	-0.0095	-0.0222	-0.0095	0.0035	0.0226
45.0	0.0417	0.0417	0.0417	0.0417	0.0290		0.0353	0.1312
67.5	0.0801	0.0801	0.0928	0.0865	0.0737	0.0928		0.1312
112.5	0.0610	0.0353	0.0865	0.0801	0.0865	0.0737	0.0865	0.1312
135.0	-0.0540	-0.0222	0.0546	0.0290	0.0481	0.0162	0.0674	0.1185
157.5	-0.1436	-0.0095	0.0098	0.0098	-0.0029	-0.0286	0.0226	0.0162
180.0	-0.1500		0.0035	-0.0029	-0.0158	-0.0413	0.0035	-0.0158
202.5	-0.0029	0.0353	0.0353	0.0226	0.0098	-0.0029	0.0226	0.0417
225.0	0.0162	0.0353	0.0417	0.0353	0.0353	0.0417	0.0481	0.0674
247.5	-0.0095	0.0035	0.0098	0.0162	0.0035	0.0162	0.0098	0.0290
292.5	0.0035	0.0035	0.0035	-0.0029	0.0035	0.0035	0.0035	0.0226
315.0		0.0226	0.0290	0.0226	0.0290	0.0290	0.0417	0.0737
337.5	0.0226	0.0162	0.0162	0.0226	0.0290	0.0162	0.0353	
	α=14.9°; w=0.018							
0.0	-0.0286	-0.0477	-0.0540	-0.0413	-0.0349	-0.0604	-0.0222	-0.0477
22.5	-0.0349	-0.0222	-0.0095	-0.0413	-0.0477	-0.0349	-0.0158	-0.0029
45.0	0.0290	0.0290	0.0353	0.0353	0.0226		0.0290	0.1312
67.5	0.0801	0.0865	0.1056	0.0992	0.0865	0.1056		0.1504
112.5	0.0737	0.0353	0.0865	0.0865	0.0992	0.0928	0.0992	0.1440
135.0	-0.0413	-0.0540	0.0481	0.0226	0.0481	0.0098	0.0546	0.1185
157.5	-0.1754	-0.1372	-0.0095	-0.0158	-0.0349	-0.0540	-0.0029	-0.0158
180.0	-0.1948		-0.0286	-0.0286	-0.0477	-0.0797	-0.0286	-0.0540
202.5	-0.0222	0.0353	0.0353	0.0098	-0.0029	-0.0029	0.0162	0.0290
225.0	-0.0222	0.0162	0.0353	0.0353	0.0290	0.0353	0.0417	0.0610
247.5	-0.0285	-0.0093	-0.0029	0.0035	-0.0093	0.0163	0.0099	0.0418
292.5	-0.0221	-0.0221	-0.0221	-0.0414	-0.0157	-0.0157	-0.0093	0.0227
315.0		-0.0093	0.0099	0.0163	0.0227	0.0227	0.0418	0.0674
337.5	0.0227	0.0163	0.0163	0.0163	0.0227	0.0163	0.0290	

TABLE VI.- Concluded.

(f) $\phi = 90^{\circ}$; M = 1.03.

θ, deg	$(p - p_{\infty})/p_{\infty}$ for longitudinal station							
	1	2	3	4	5	6	7	8
	$\alpha=0^{\circ}$; w=0.018							
0.0	-0.0280	-0.0214	-0.0280	-0.0280	-0.0479	-0.0214	0.0843	0.1306
22.5	-0.0280	-0.0280	-0.0082	-0.0347	-0.0479	-0.0148	0.0843	0.1372
45.0	-0.0214	-0.0214	-0.0347	-0.0347	-0.0413		0.0777	0.1571
67.5	-0.0148	-0.0280	-0.0280	-0.0347	-0.0413	-0.0016		0.1372
112.5	-0.0611	-0.0611	-0.0347	-0.0413	-0.0280	-0.0148	0.0777	0.1438
135.0	-0.1074	-0.0545	-0.0280	-0.0413	-0.0214	-0.0214	0.0911	0.1571
157.5	-0.0875	-0.0413	-0.0214	-0.0148	-0.0280	-0.0148	0.0843	0.1306
180.0	-0.1008		-0.0214	-0.0214	-0.0280	-0.0148	0.0843	0.1240
202.5	-0.1140	-0.0545	-0.0214	-0.0214	-0.0347	-0.0214	0.0777	0.1306
225.0	-0.0677	-0.0611	-0.0280	-0.0280	-0.0413	-0.0148	0.0777	0.1506
247.5	-0.0350	-0.0416	-0.0283	-0.0215	-0.0350	-0.0082	0.0782	0.1381
292.5	-0.0215	-0.0215	-0.0215	-0.0416	-0.0283	-0.0149	0.0782	0.1381
315.0		-0.0215	-0.0149	-0.0350	-0.0283	-0.0215	0.0848	0.1648
337.5	-0.0215	-0.0215	-0.0215	-0.0283	-0.0350	-0.0215	0.0915	
	$\alpha=2.0^{\circ}$; w=0.018							
0.0	-0.0283	-0.0215	-0.0283	-0.0283	-0.0416	-0.0350	0.0716	0.1381
22.5	-0.0283	-0.0215	-0.0016	-0.0350	-0.0482	-0.0283	0.0583	0.1381
45.0	-0.0149	-0.0149	-0.0283	-0.0350	-0.0416		0.0517	0.1715
67.5	-0.0082	-0.0215	-0.0283	-0.0350	-0.0082	0.1116		0.0249
112.5	-0.0681	-0.0350	-0.0350	-0.0215	-0.0215	0.0450	0.1582	0.0249
135.0	-0.1148	-0.0615	-0.0215	-0.0416	-0.0149	-0.0350	0.0649	0.1648
157.5	-0.1015	-0.0549	-0.0149	-0.0215	-0.0215	-0.0350	0.0649	0.1315
180.0	-0.1015		-0.0149	-0.0149	-0.0215	-0.0283	0.0716	0.1248
202.5	-0.1148	-0.0482	-0.0215	-0.0215	-0.0350	-0.0215	0.0716	0.1315
225.0	-0.0681	-0.0482	-0.0283	-0.0215	-0.0350	-0.0082	0.0782	0.1447
247.5	-0.0416	-0.0482	-0.0350	-0.0215	-0.0350	-0.0082	0.0716	0.1248
292.5	-0.0215	-0.0283	-0.0283	-0.0416	-0.0350	-0.0149	0.0716	0.1248
315.0		-0.0283	-0.0215	-0.0416	-0.0350	-0.0283	0.0782	0.1582
337.5	-0.0283	-0.0283	-0.0283	-0.0350	-0.0350	-0.0350	0.0716	

θ, deg	$(p - p_{\infty})/p_{\infty}$ for longitudinal station							
	1	2	3	4	5	6	7	8
	$\alpha=4.0^{\circ}$; w=0.018							
0.0	-0.0415	-0.0415	-0.0415	-0.0481	-0.0613	-0.0415	0.0775	0.1238
22.5	-0.0481	-0.0349	-0.0216	-0.0547	-0.0613	-0.0415	0.0643	0.1304
45.0	-0.0281	-0.0281	-0.0415	-0.0481	-0.0481		0.0445	0.1767
67.5	-0.0084	-0.0150	-0.0281	-0.0415	-0.0481	-0.0150		0.1503
112.5	-0.0349	-0.0811	-0.0547	-0.0481	-0.0281	-0.0281	0.0379	0.1503
135.0	-0.1208	-0.0876	-0.0415	-0.0613	-0.0281	-0.0415	0.0643	0.1701
157.5	-0.1208	-0.0745	-0.0415	-0.0349	-0.0415	-0.0415	0.0709	0.1238
180.0	-0.1274		-0.0349	-0.0281	-0.0349	-0.0281	0.0775	0.1106
202.5	-0.1274	-0.0481	-0.0349	-0.0349	-0.0415	-0.0150	0.0775	0.1238
225.0	-0.0876	-0.0481	-0.0349	-0.0349	-0.0349	0.0114	0.0840	0.1304
247.5	-0.0416	-0.0416	-0.0283	-0.0283	-0.0283	0.0316	0.0915	0.1248
292.5	-0.0215	-0.0283	-0.0283	-0.0350	-0.0215	0.0249	0.0983	0.1248
315.0		-0.0283	-0.0215	-0.0350	-0.0215	0.0050	0.0983	0.1514
337.5	-0.0283	-0.0350	-0.0350	-0.0350	-0.0350	-0.0149	0.0983	



Orifice row	θ, deg	Orifice row	θ, deg
1	0	8	180.0
2	22.5	9	202.5
3	45.0	10	225.0
4	67.5	11	247.5
5	112.5	12	292.5
6	135.0	13	315.0
7	157.5	14	337.5

Figure 1.- Sketch of model. All dimensions are in inches unless otherwise noted.

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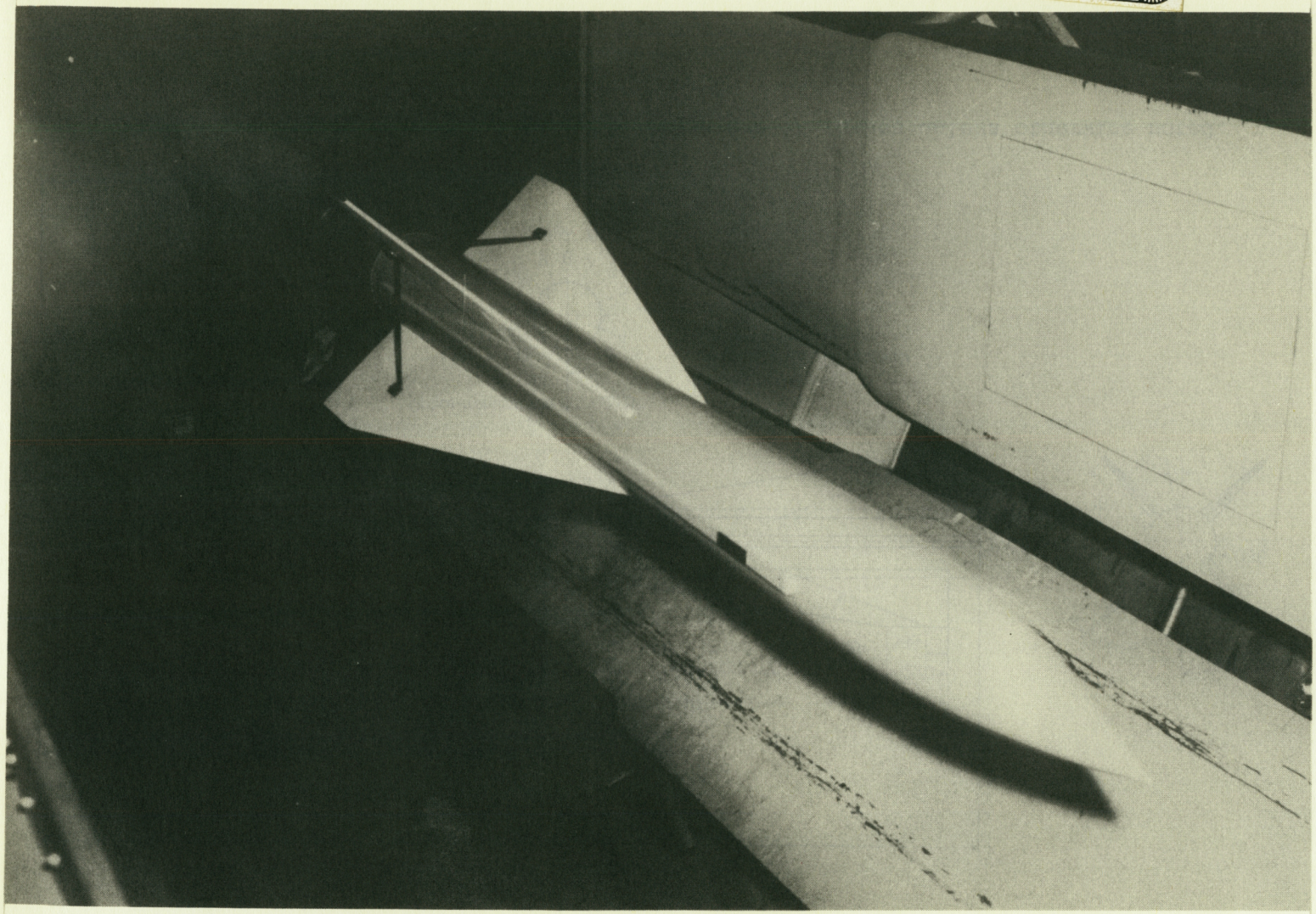

L-60-4840

Figure 2.- Photograph of model sting mounted in the Langley 16-foot transonic tunnel.

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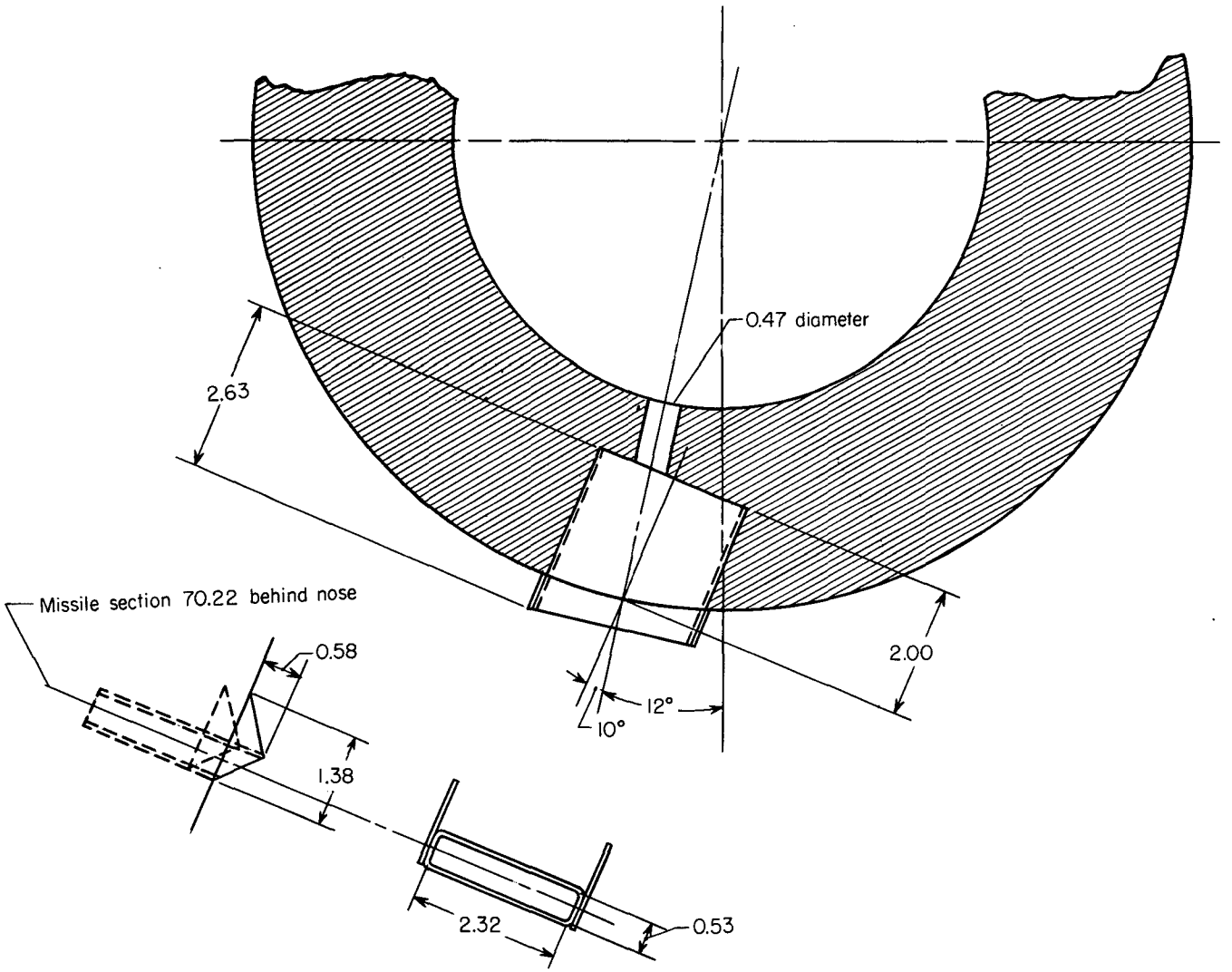

Figure 3.- Details of auxiliary exhaust bleed port. All dimensions are in inches unless otherwise noted.

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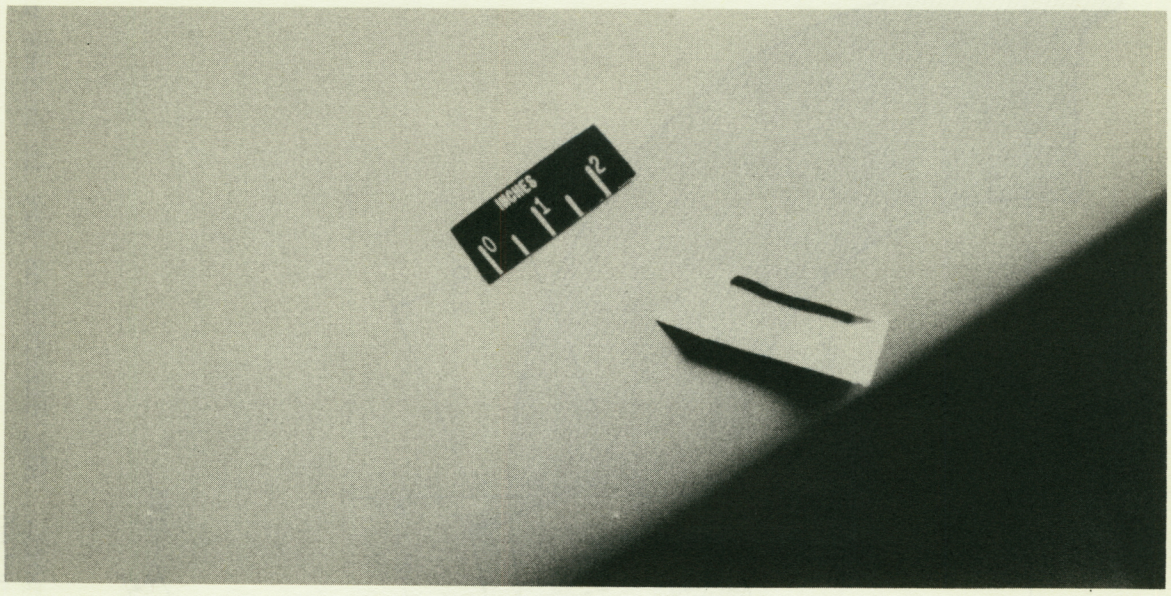
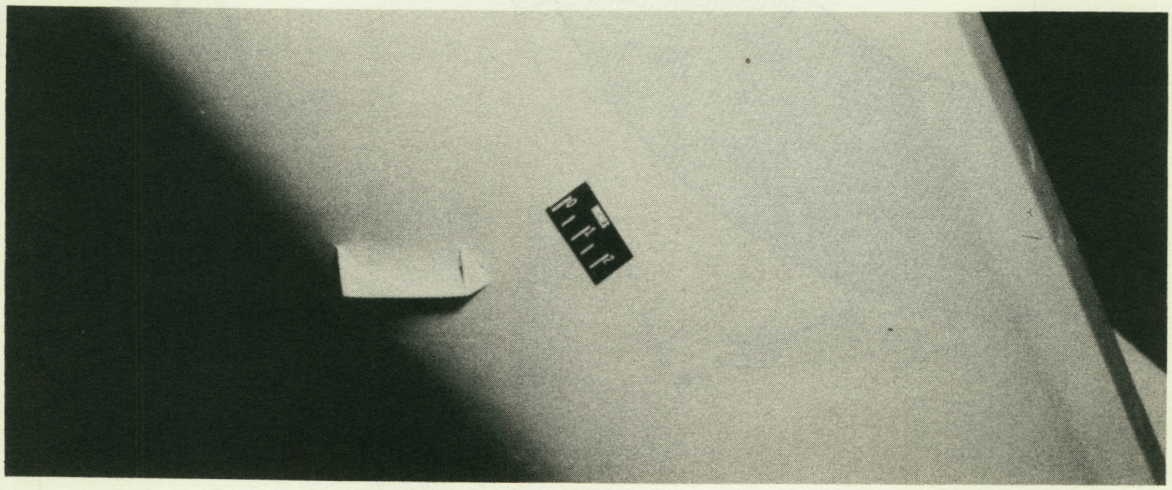


(a) As viewed from downstream. L-60-4843



(b) As viewed from upstream. L-60-4842

Figure 4.- Photographs of auxiliary exhaust bleed port.

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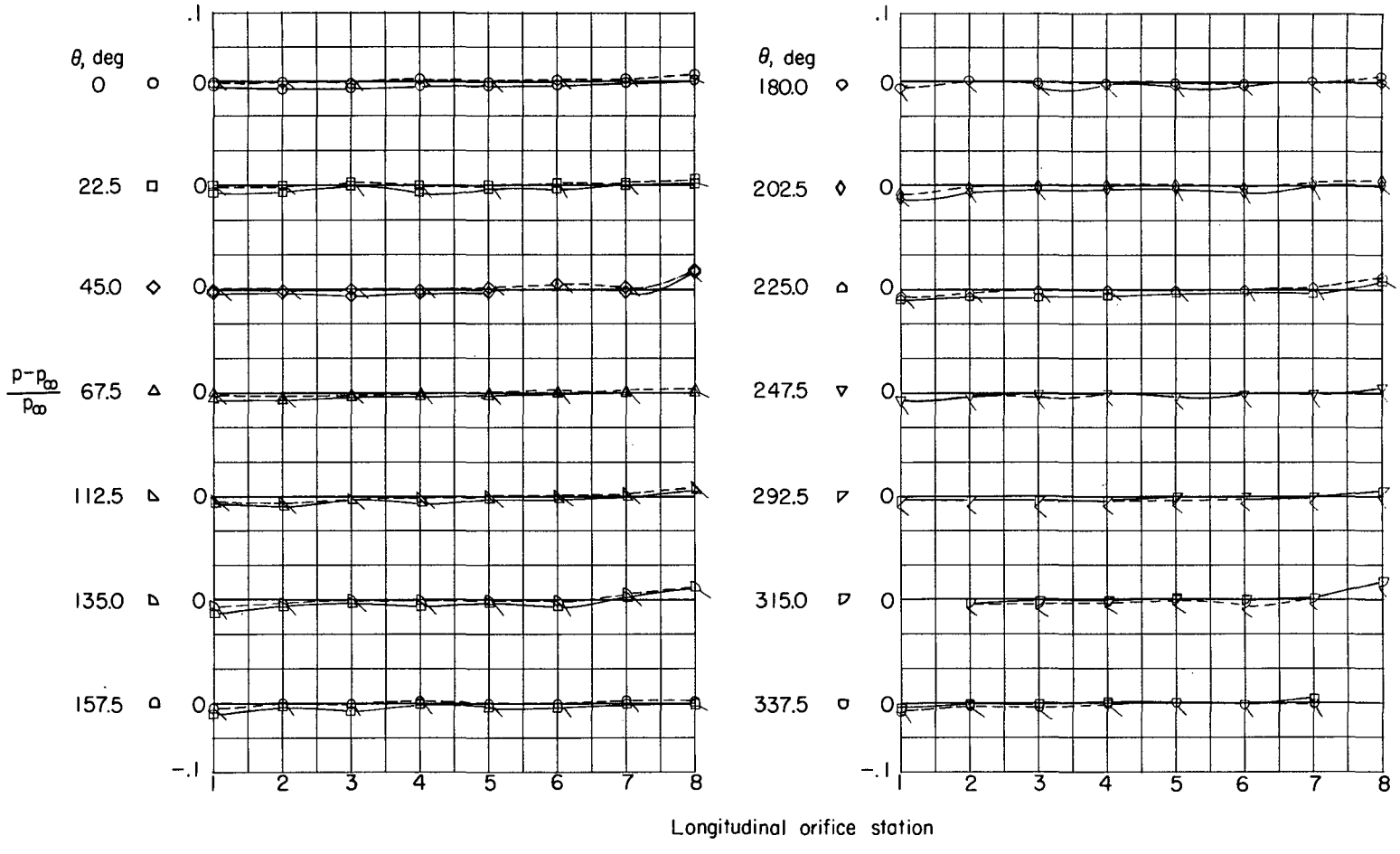
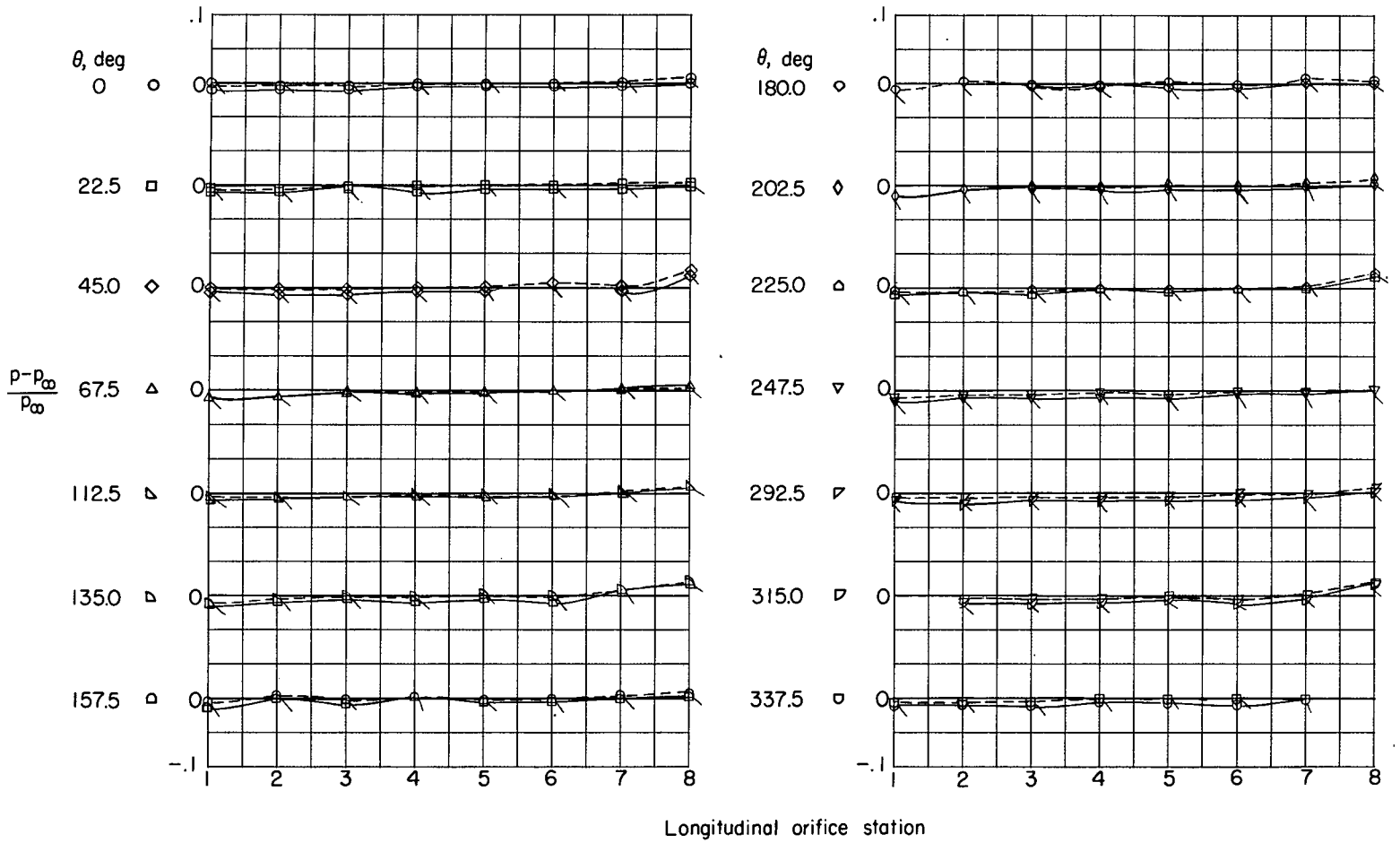


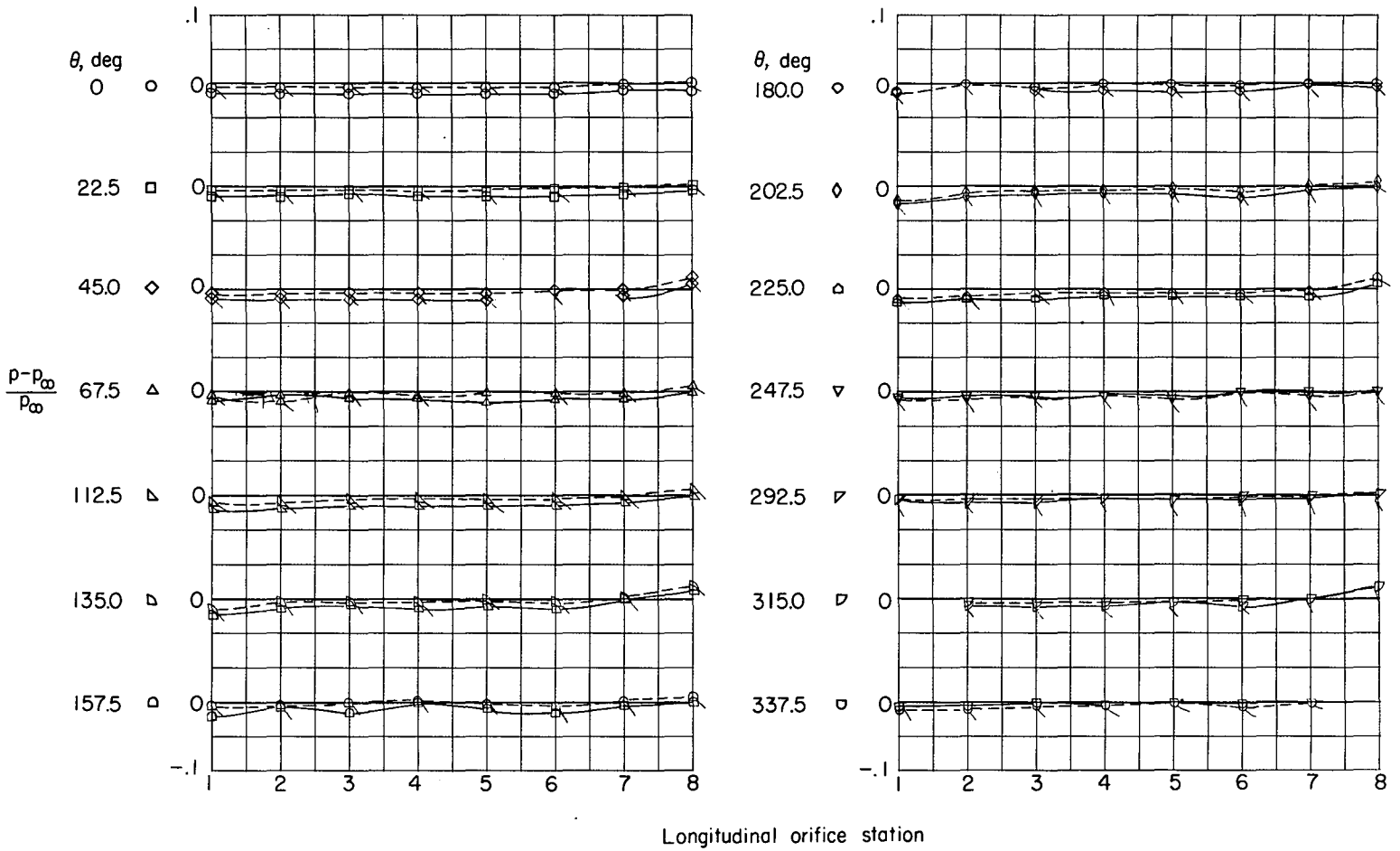
(a) $\alpha = -2.0^{\circ}$.

Figure 5.- Variation of static-pressure error coefficient with longitudinal orifice station for $\phi = 0^{\circ}$, $M = 0.70$, and $w = 0.018$ lb/sec. (Flagged symbols indicate exhaust bleed on.)



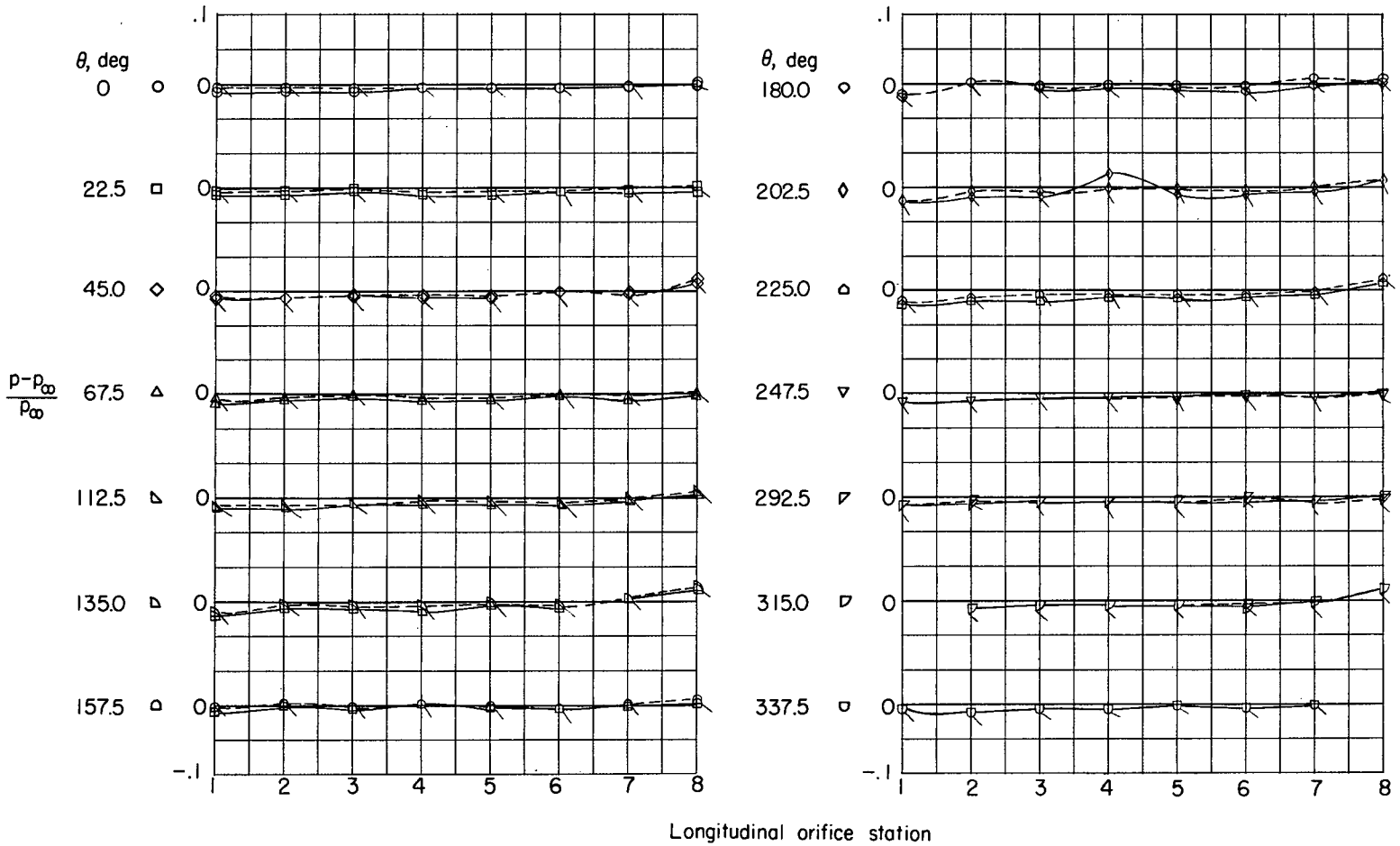
(b) $\alpha = 0^{\circ}$.

Figure 5.- Continued.



(c) $\alpha = 2.0^{\circ}$.

Figure 5.- Continued.



(d) $\alpha = 4.0^{\circ}$.

Figure 5.- Continued.

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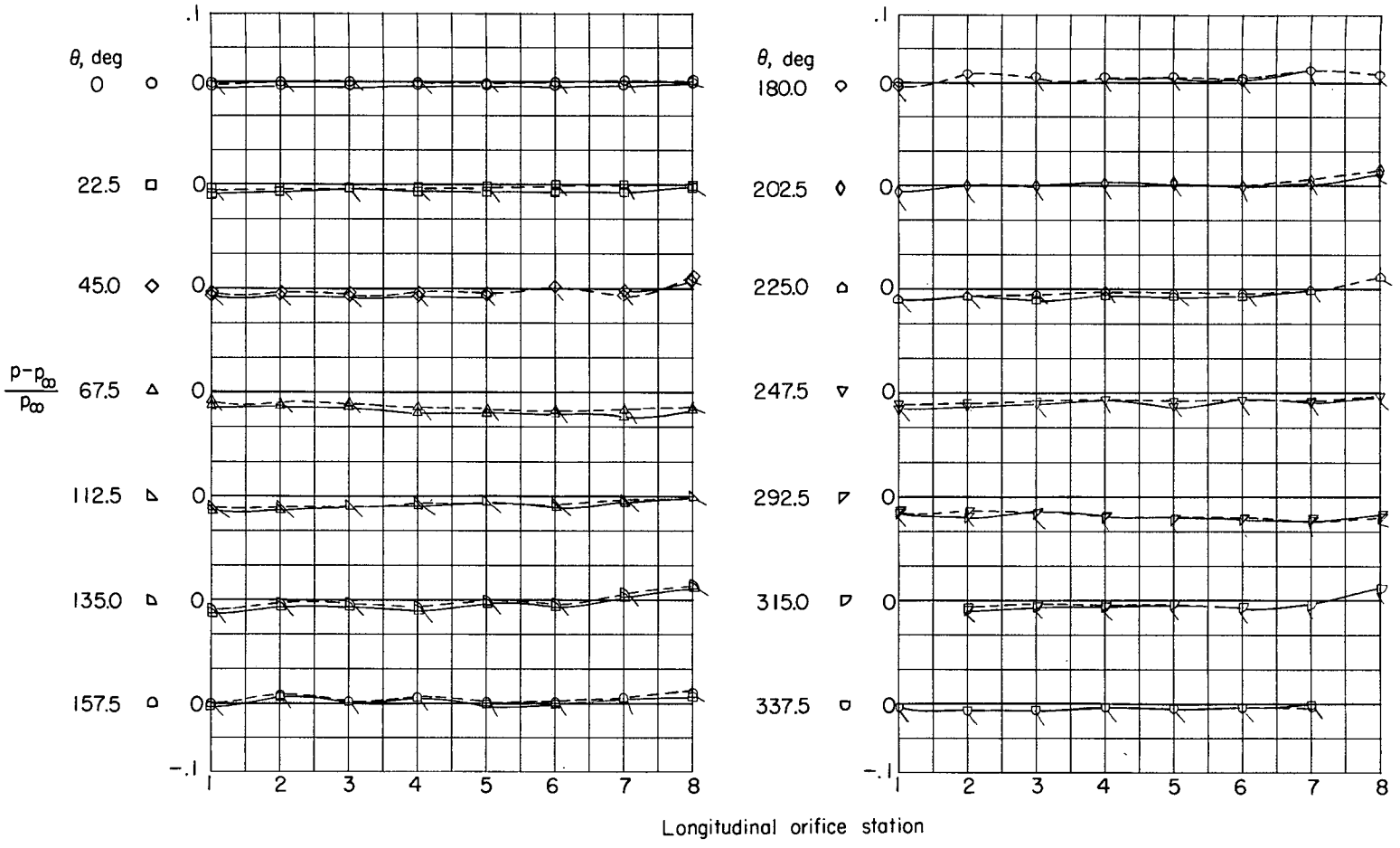
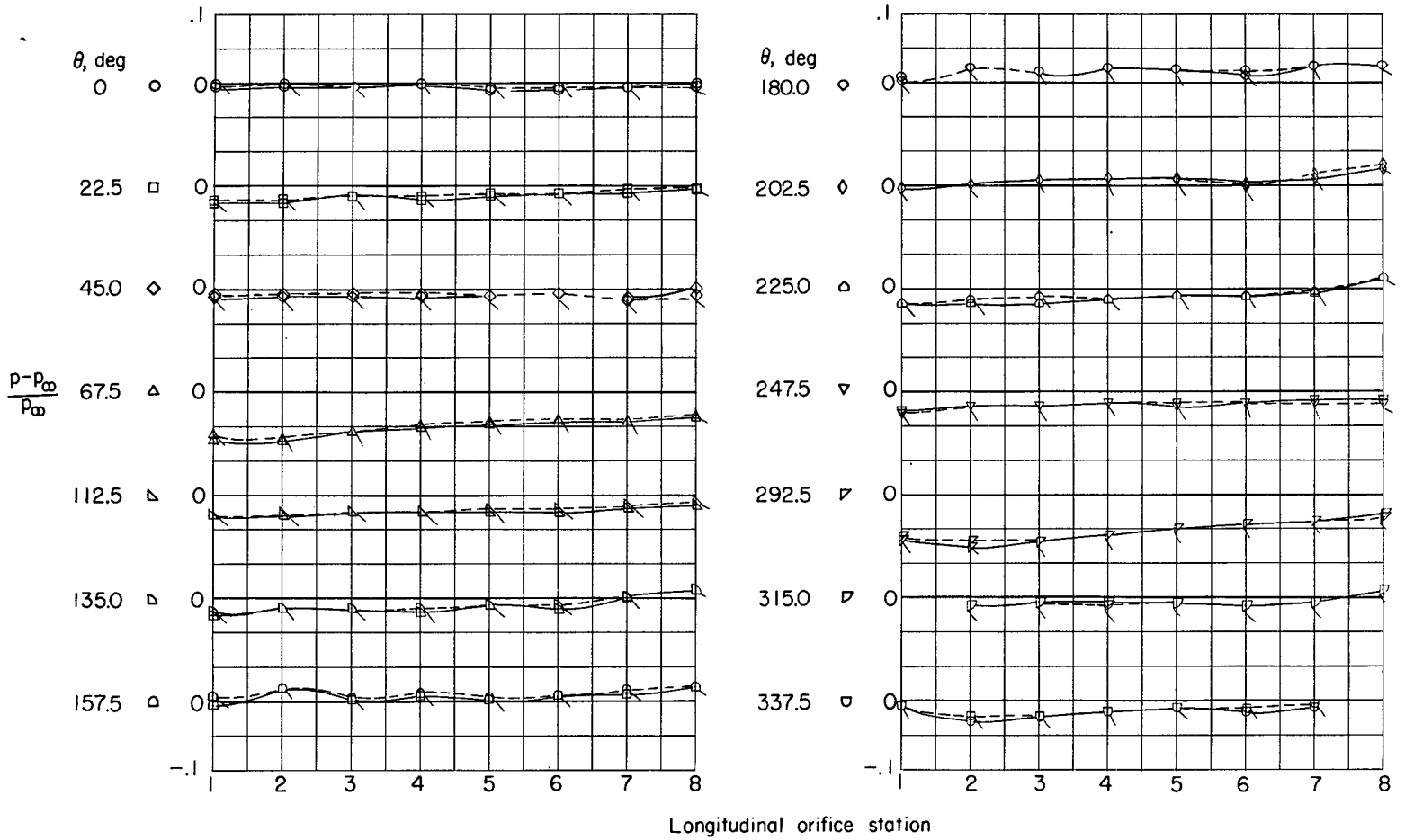


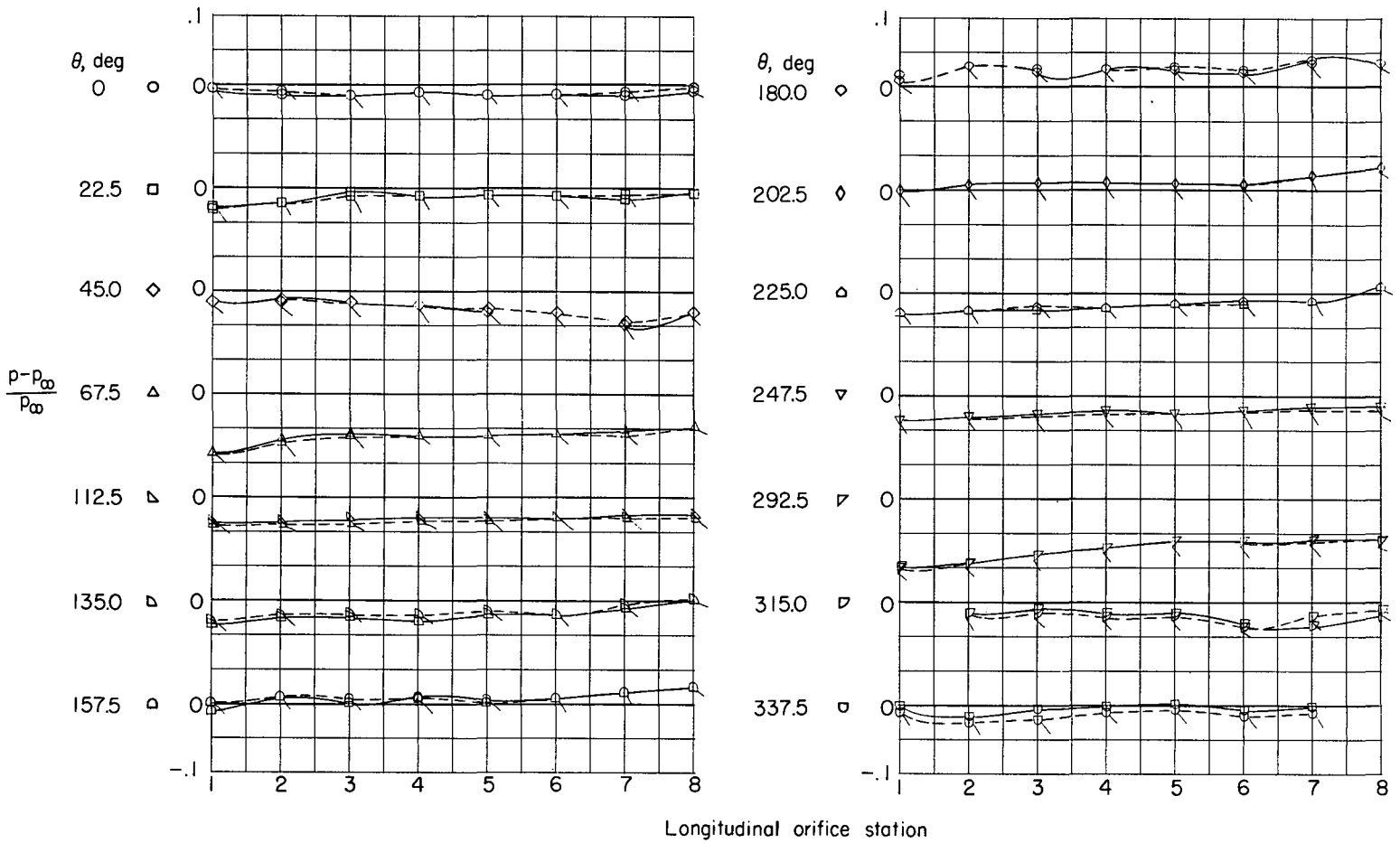
(e) $\alpha = 8.0^{\circ}$.

Figure 5.- Continued.



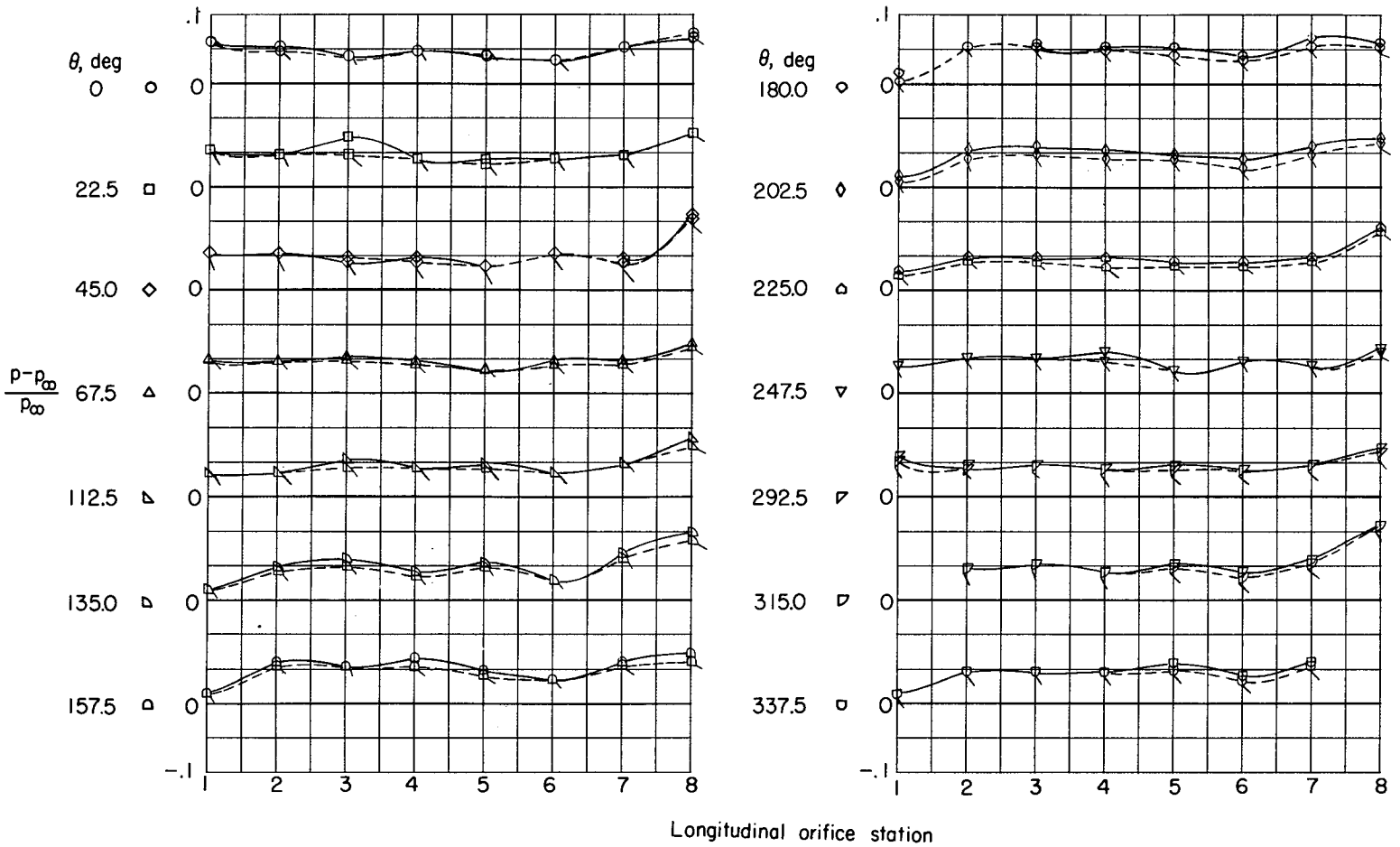
(f) $\alpha = 12.0^{\circ}$.

Figure 5.- Continued.



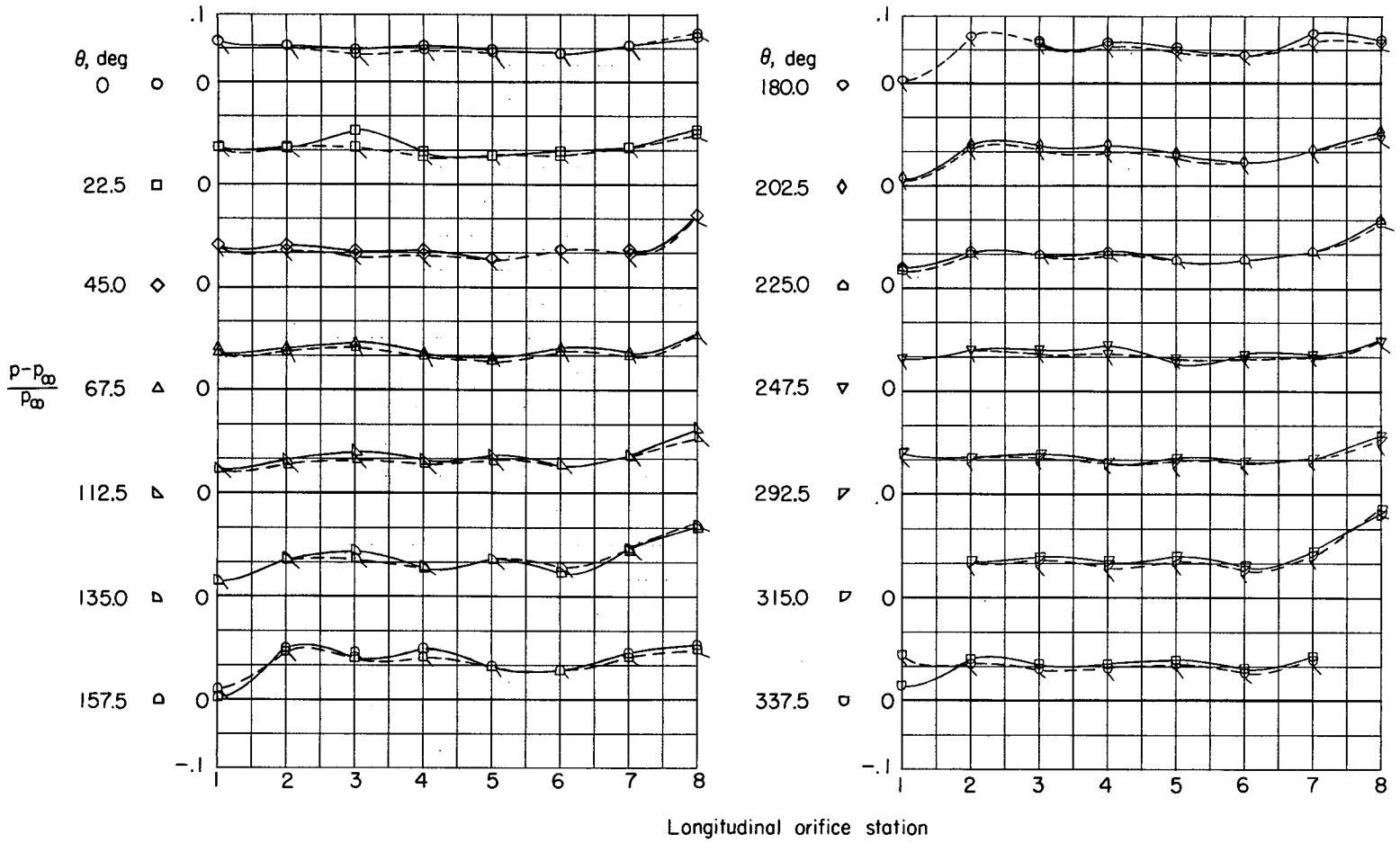
(g) $\alpha = 15.1^{\circ}$.

Figure 5.- Concluded.



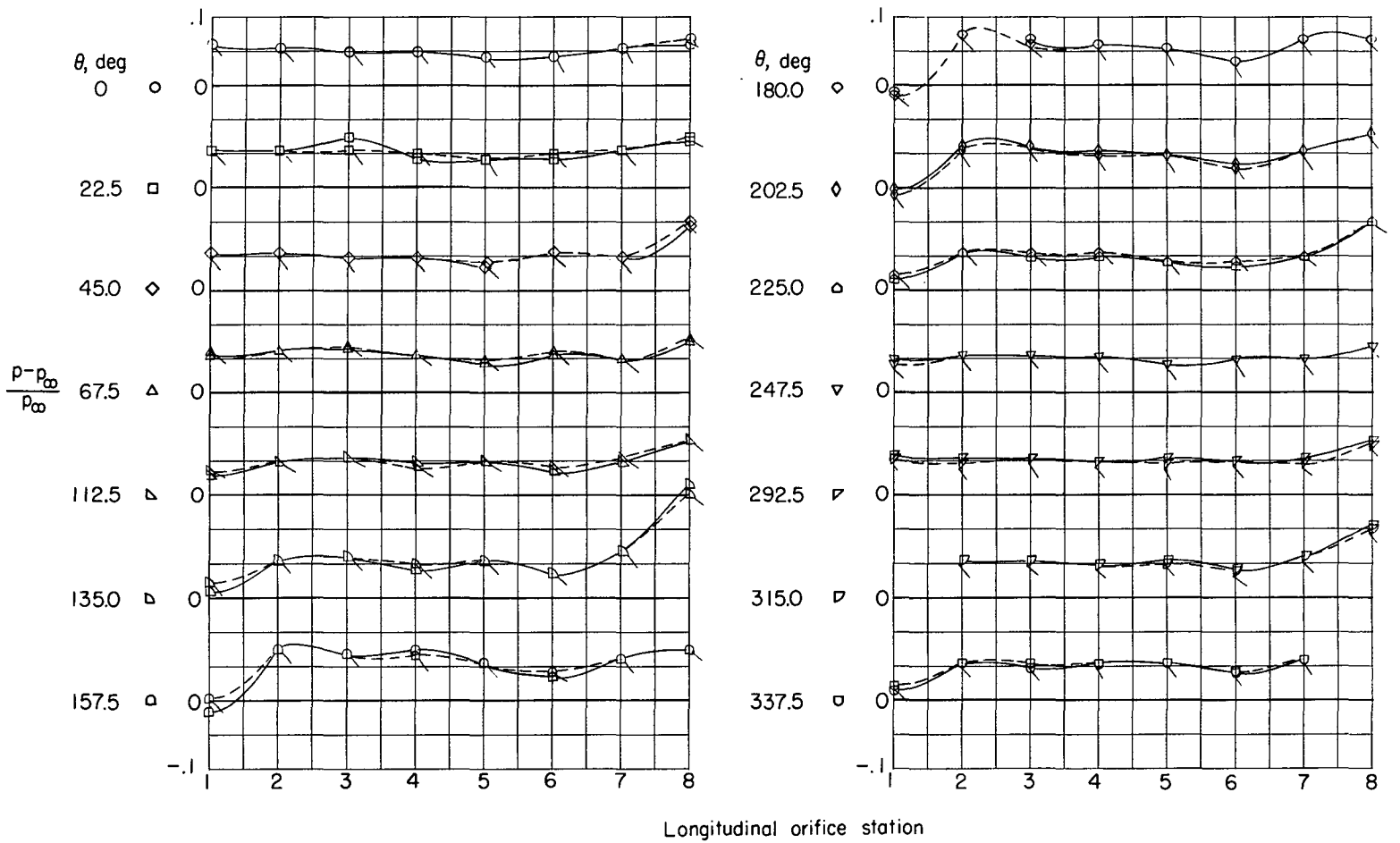
(a) $\alpha = -2.1^{\circ}$.

Figure 6.- Variation of static-pressure error coefficient with longitudinal orifice station for $\phi = 0^{\circ}$, $M = 1.00$, and $w = 0.018$ lb/sec. (Flagged symbols indicate exhaust bleed on.)



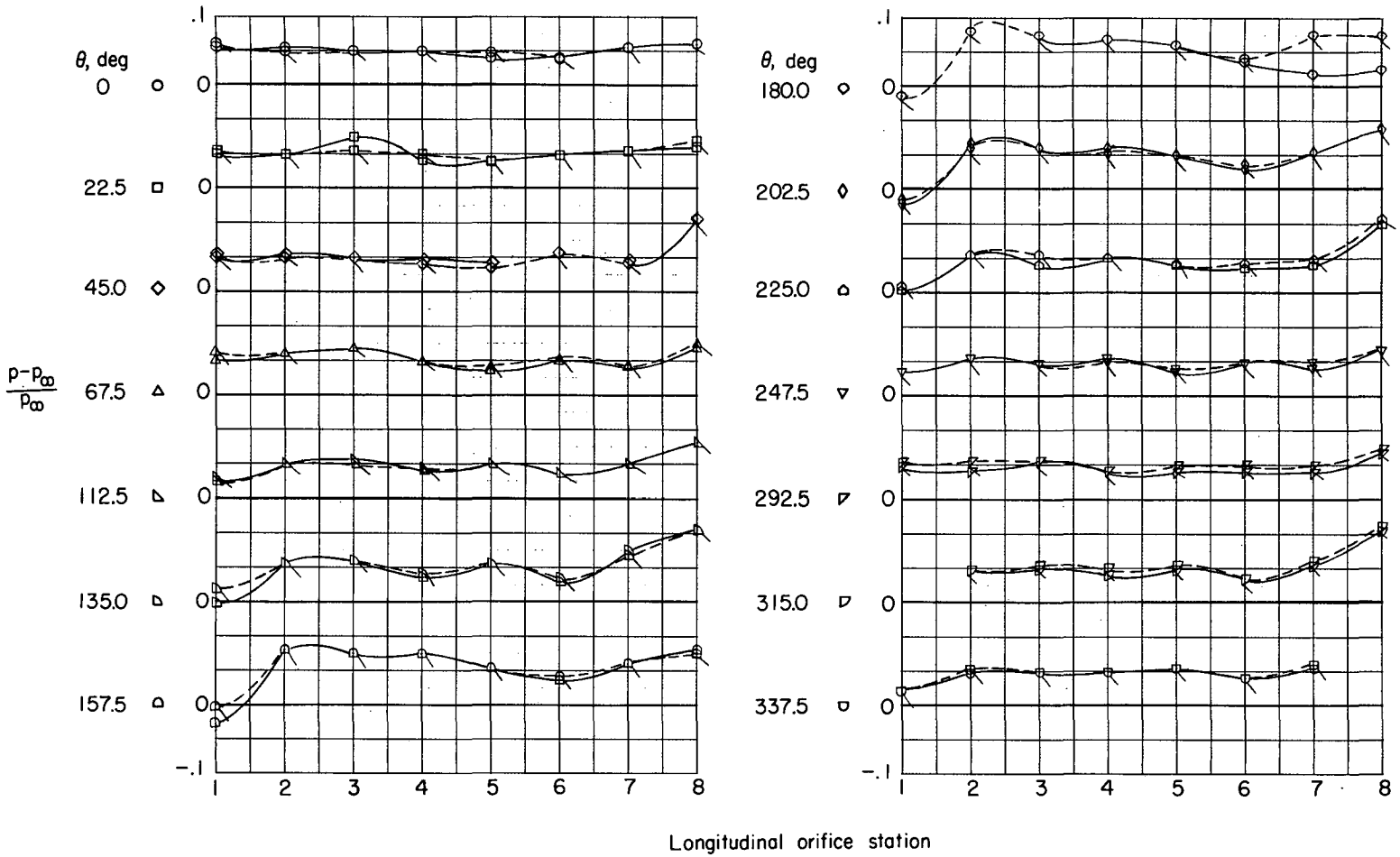
(b) $\alpha = -0.1^{\circ}$.

Figure 6.- Continued.



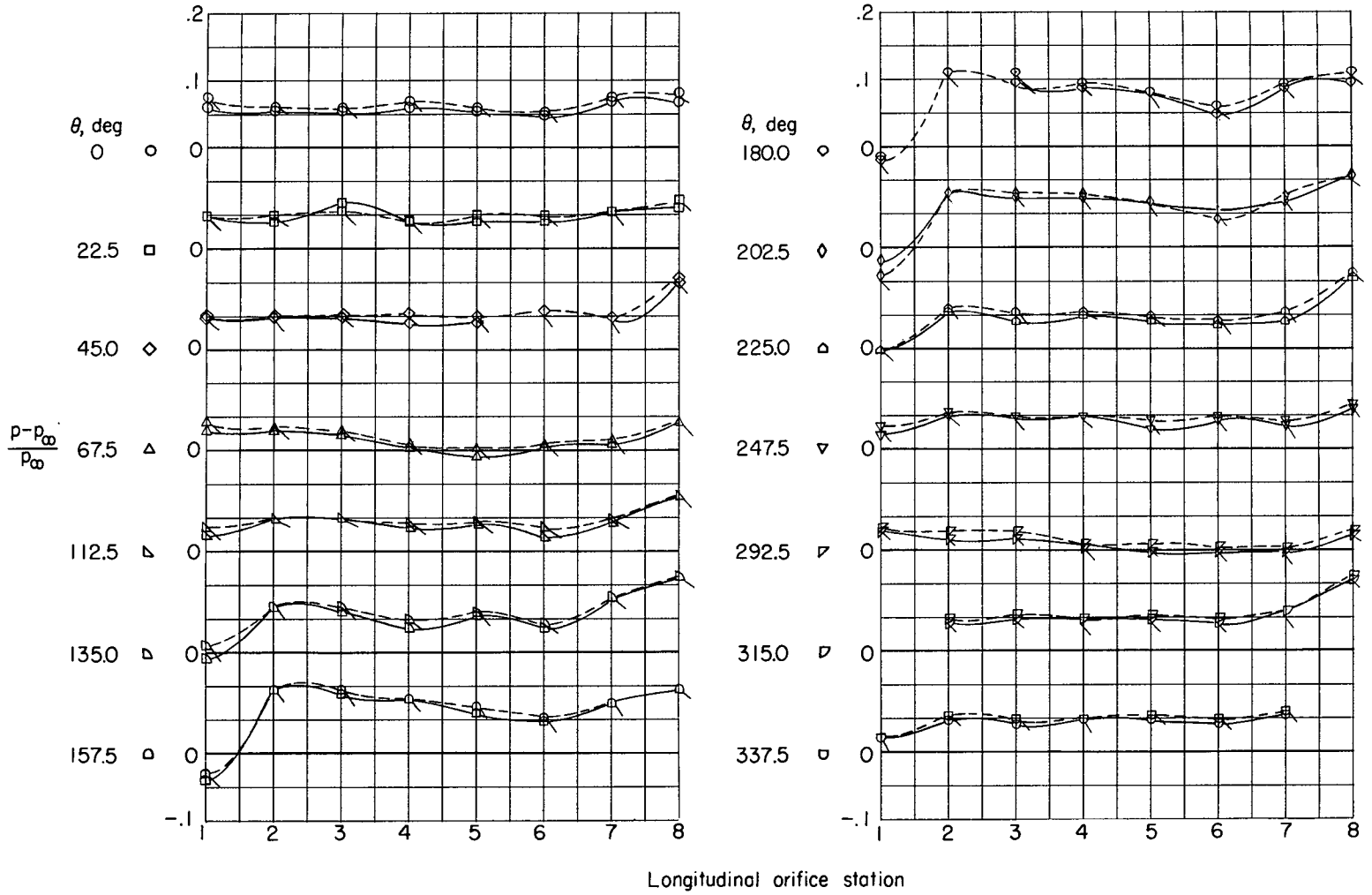
(c) $\alpha = 2.0^{\circ}$.

Figure 6.- Continued.



(d) $\alpha = 4.0^{\circ}$.

Figure 6.- Continued.



(e) $\alpha = 8.0^{\circ}$.

Figure 6.- Concluded.

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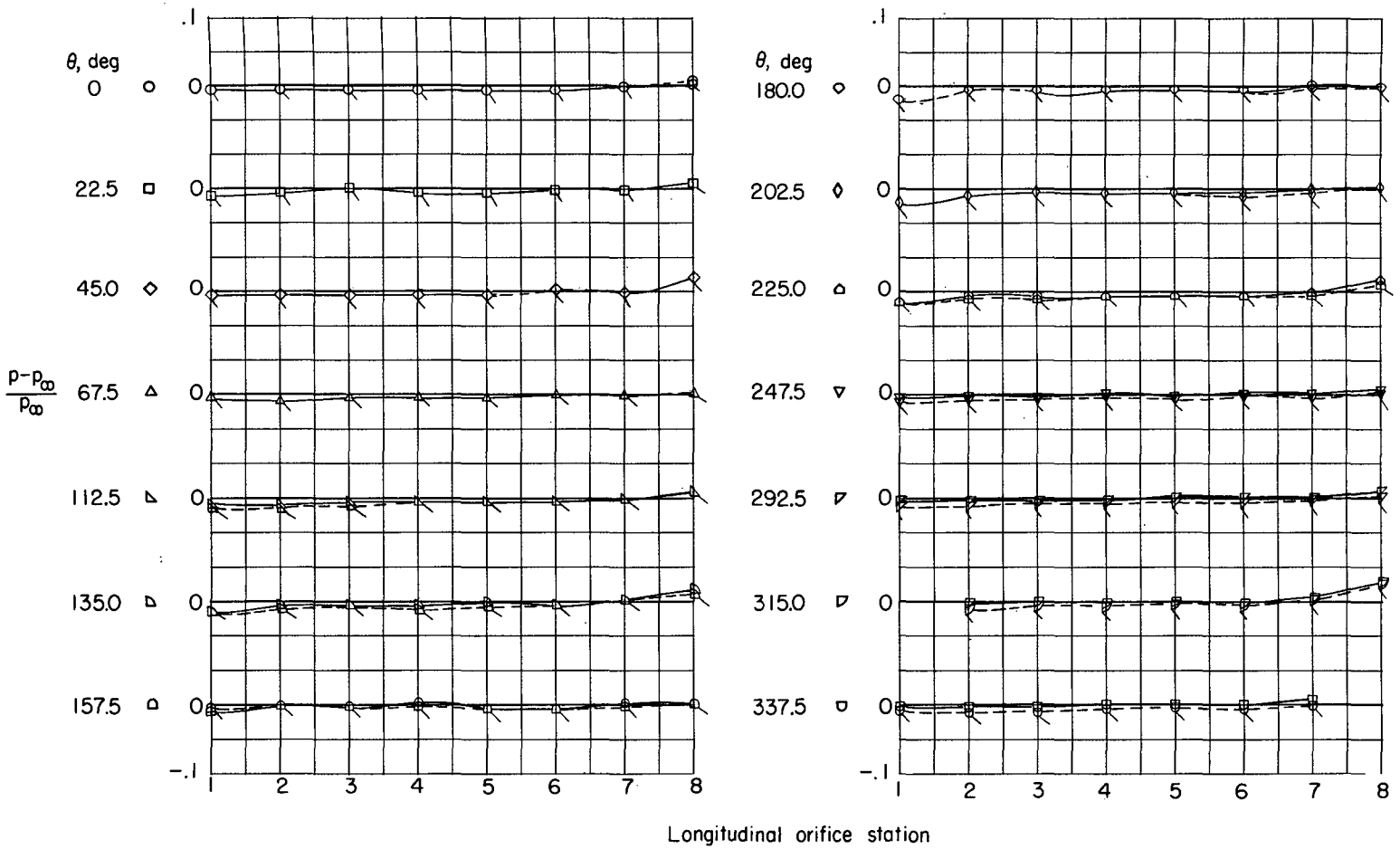
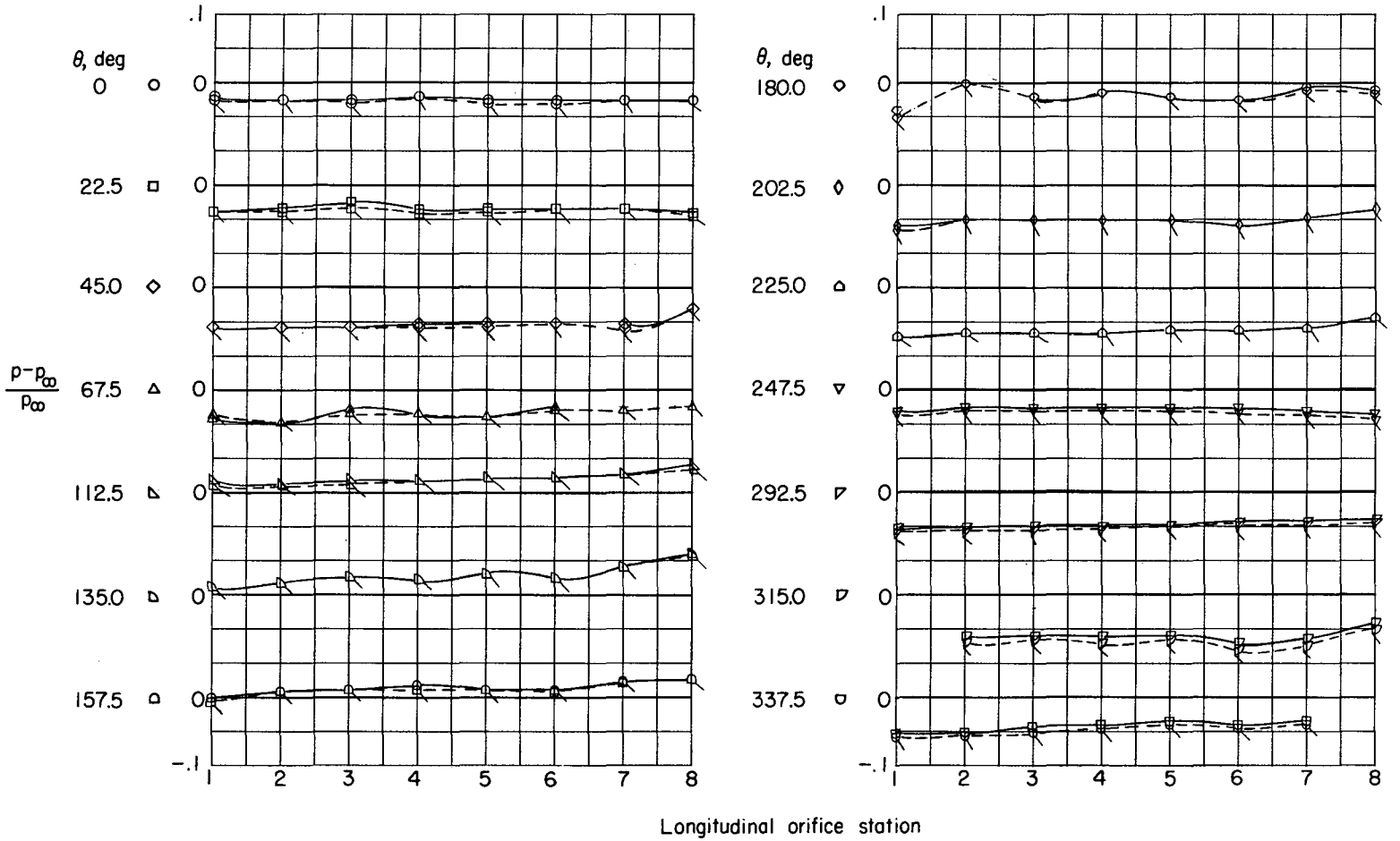


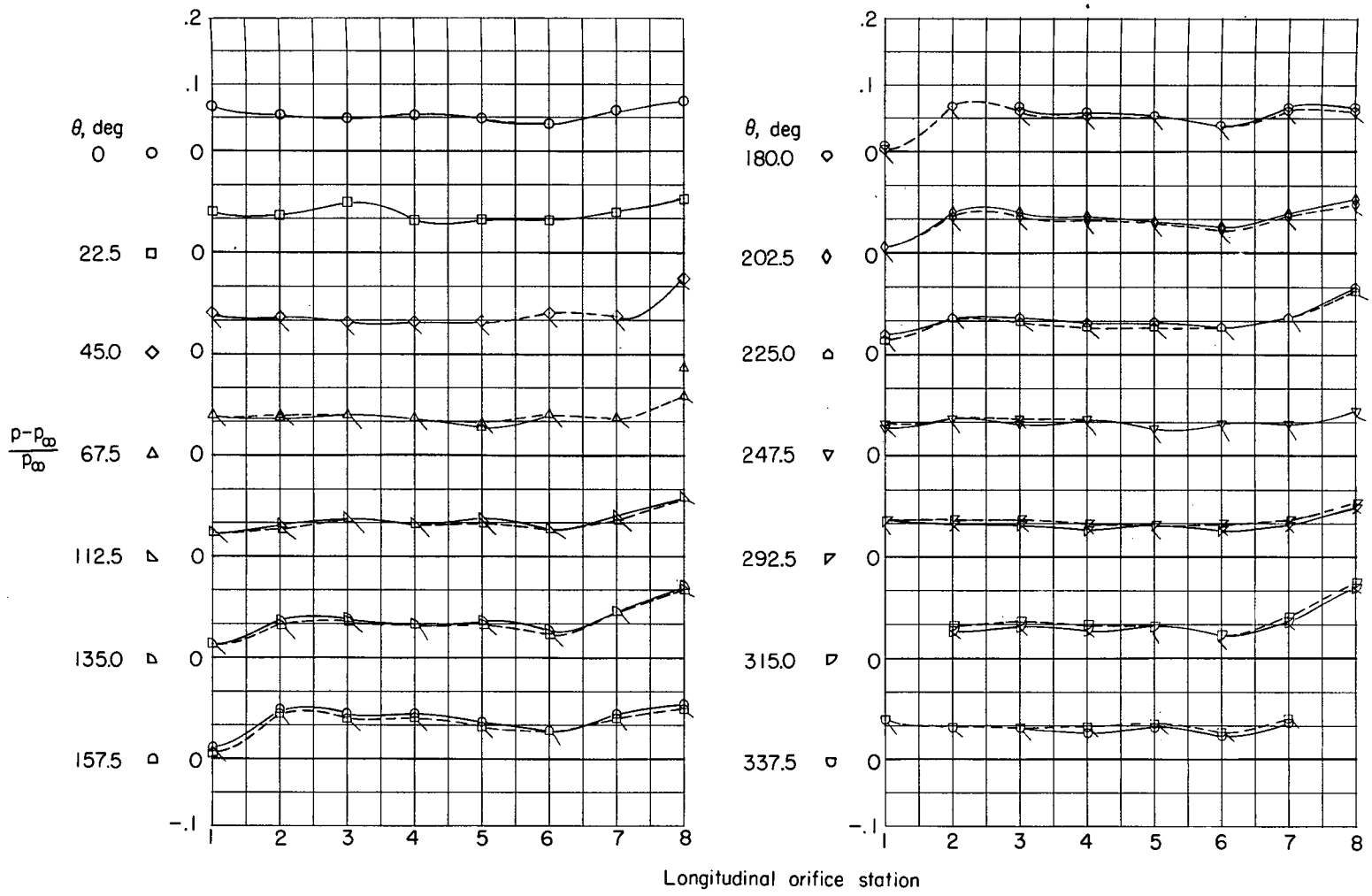
(a) $\alpha = 0^{\circ}$.

Figure 7.- Variation of static-pressure error coefficient with longitudinal orifice station for $\phi = 45^{\circ}$, $M = 0.70$, and $w = 0.018$ lb/sec. (Flagged symbols indicate exhaust bleed on.)



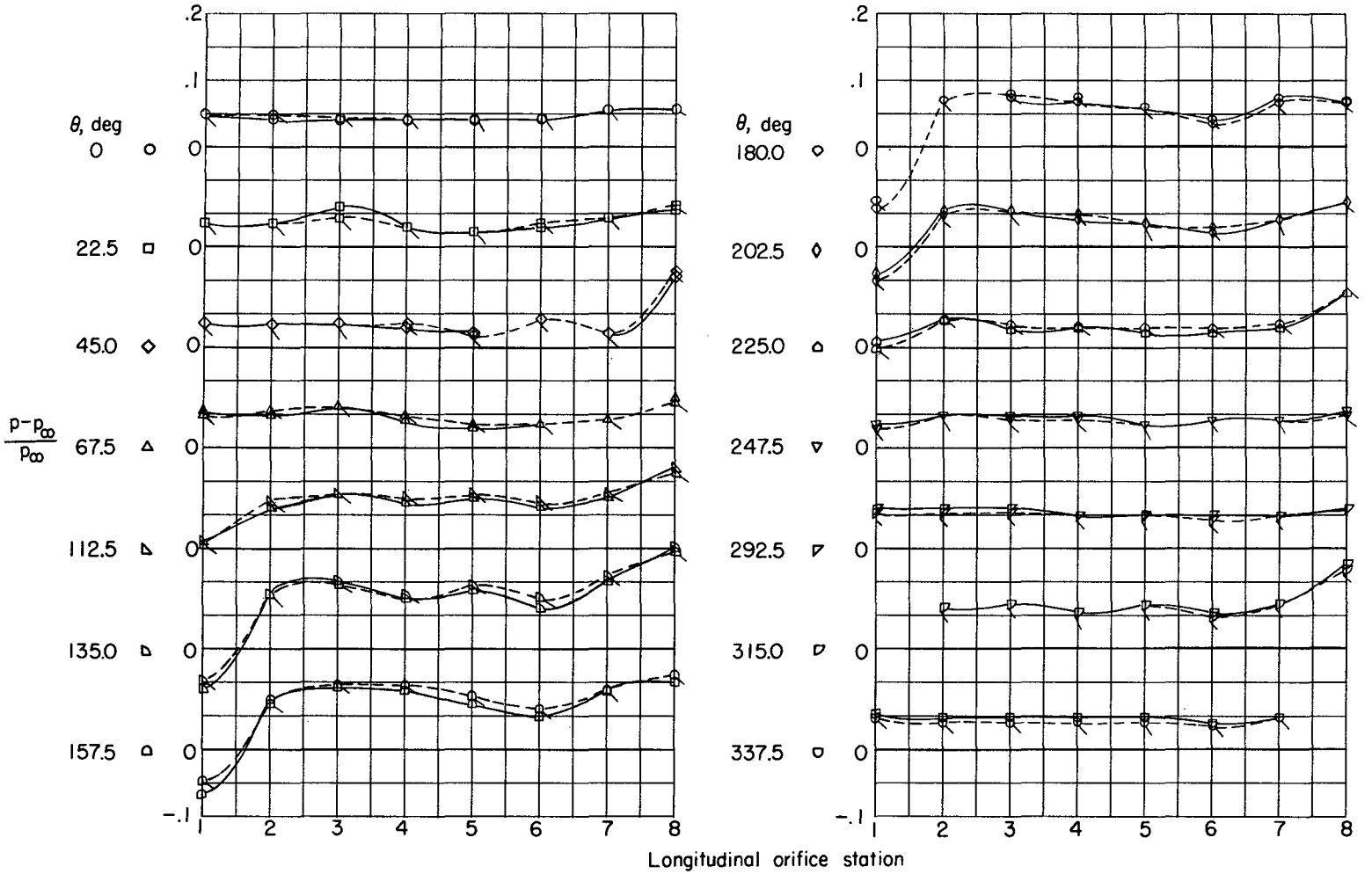
(b) $\alpha = 8.0^{\circ}$.

Figure 7.- Concluded.



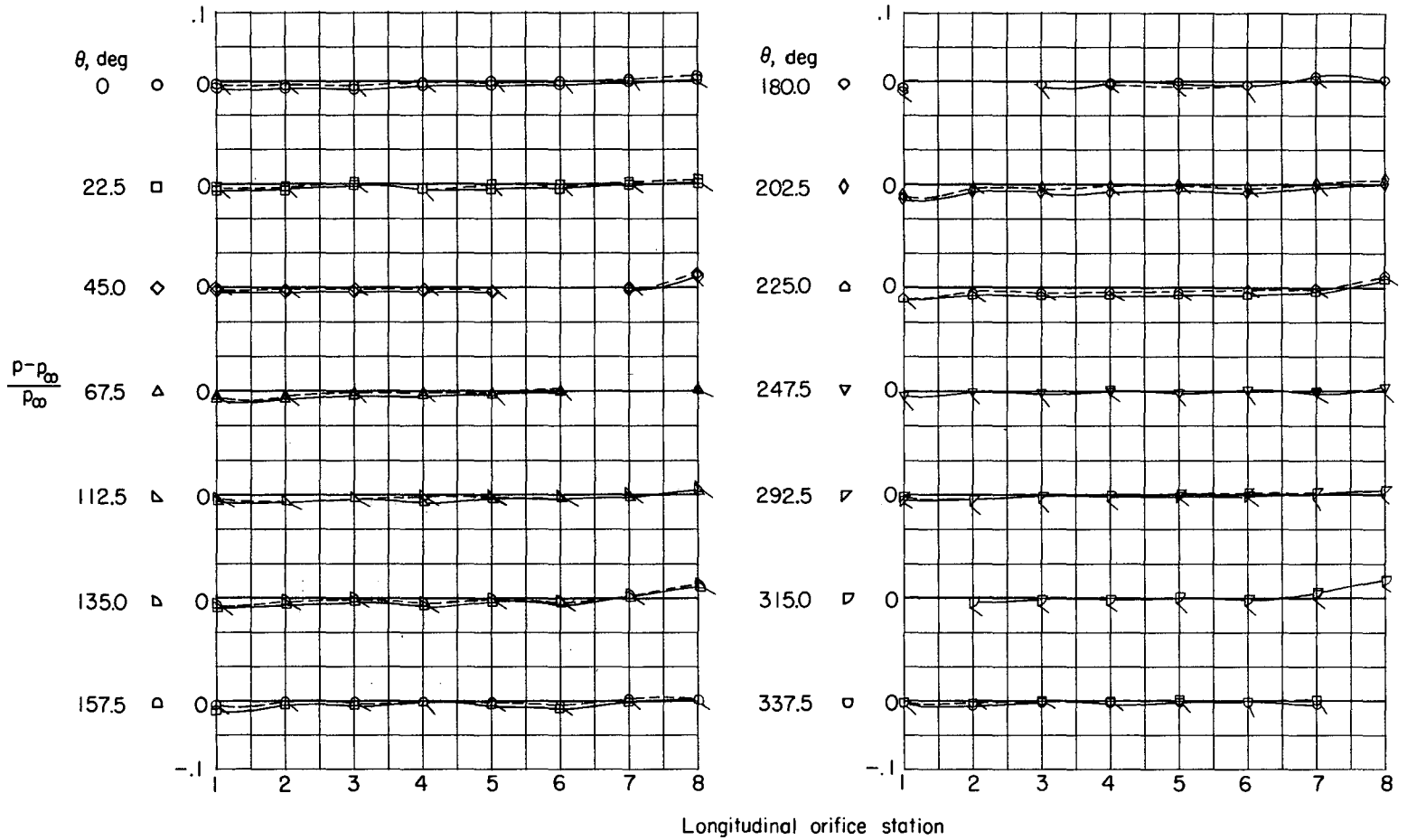
(a) $\alpha = 0^{\circ}$.

Figure 8.- Variation of static-pressure error coefficient with longitudinal orifice station for $\phi = 45^{\circ}$, M = 1.00, and w = 0.019 lb/sec. (Flagged symbols indicate exhaust bleed on.)



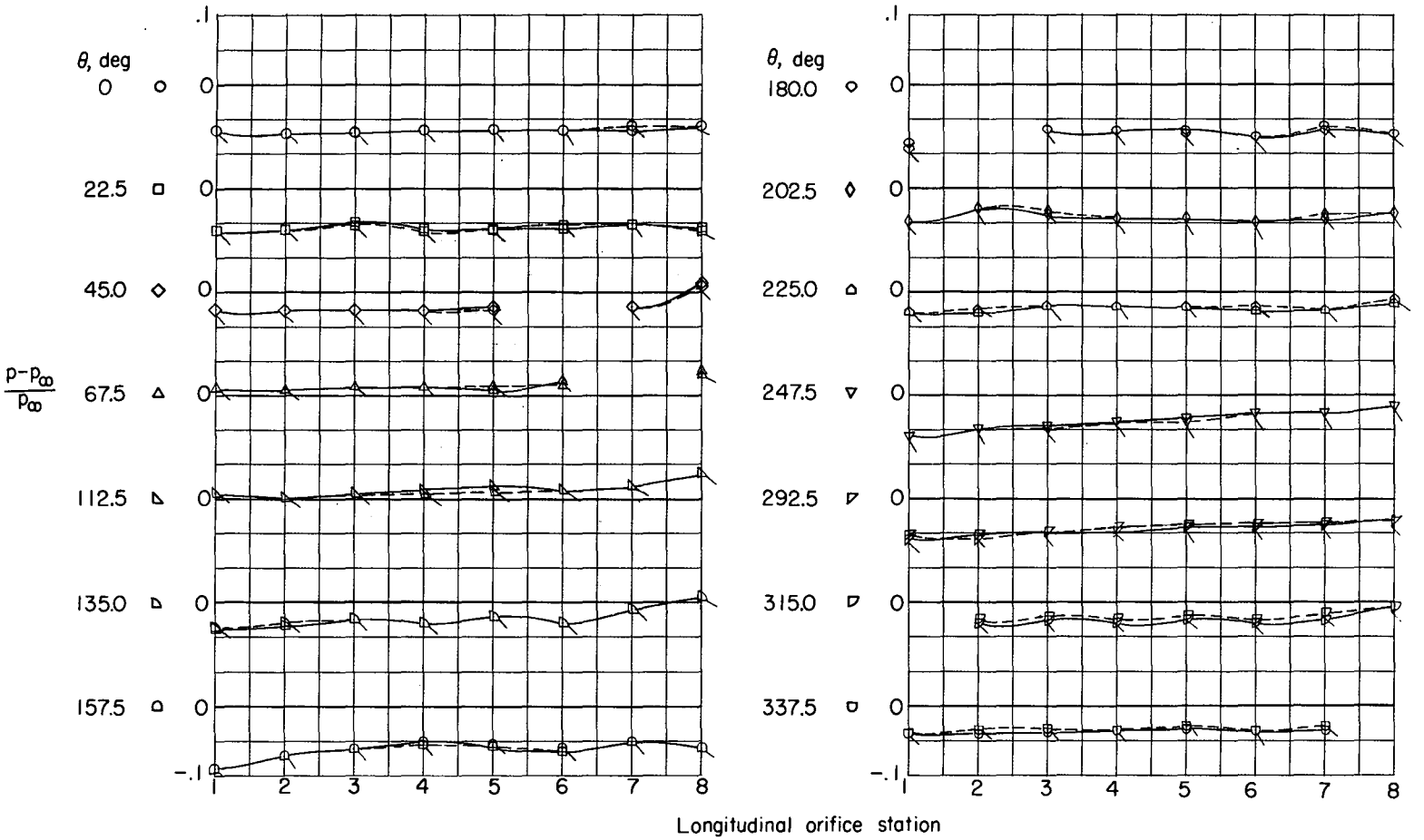
(b) $\alpha = 8.0^{\circ}$.

Figure 8.- Concluded.



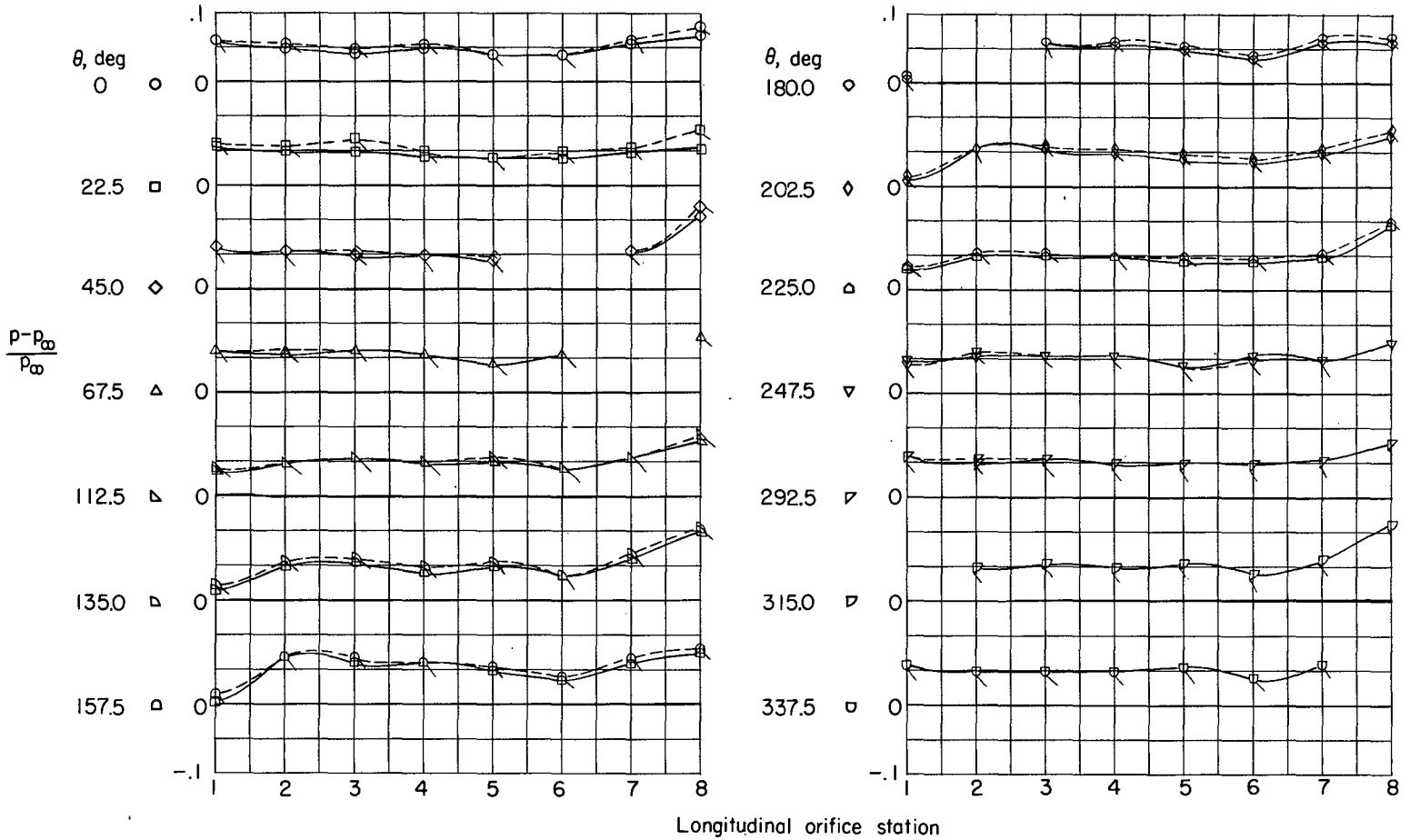
(a) $\alpha = -0.1^{\circ}$.

Figure 9.- Variation of static-pressure error coefficient with longitudinal orifice station for $\phi = 90^{\circ}$, $M = 0.70$, and $w = 0.018$ lb/sec. (Flagged symbols indicate exhaust bleed on.)



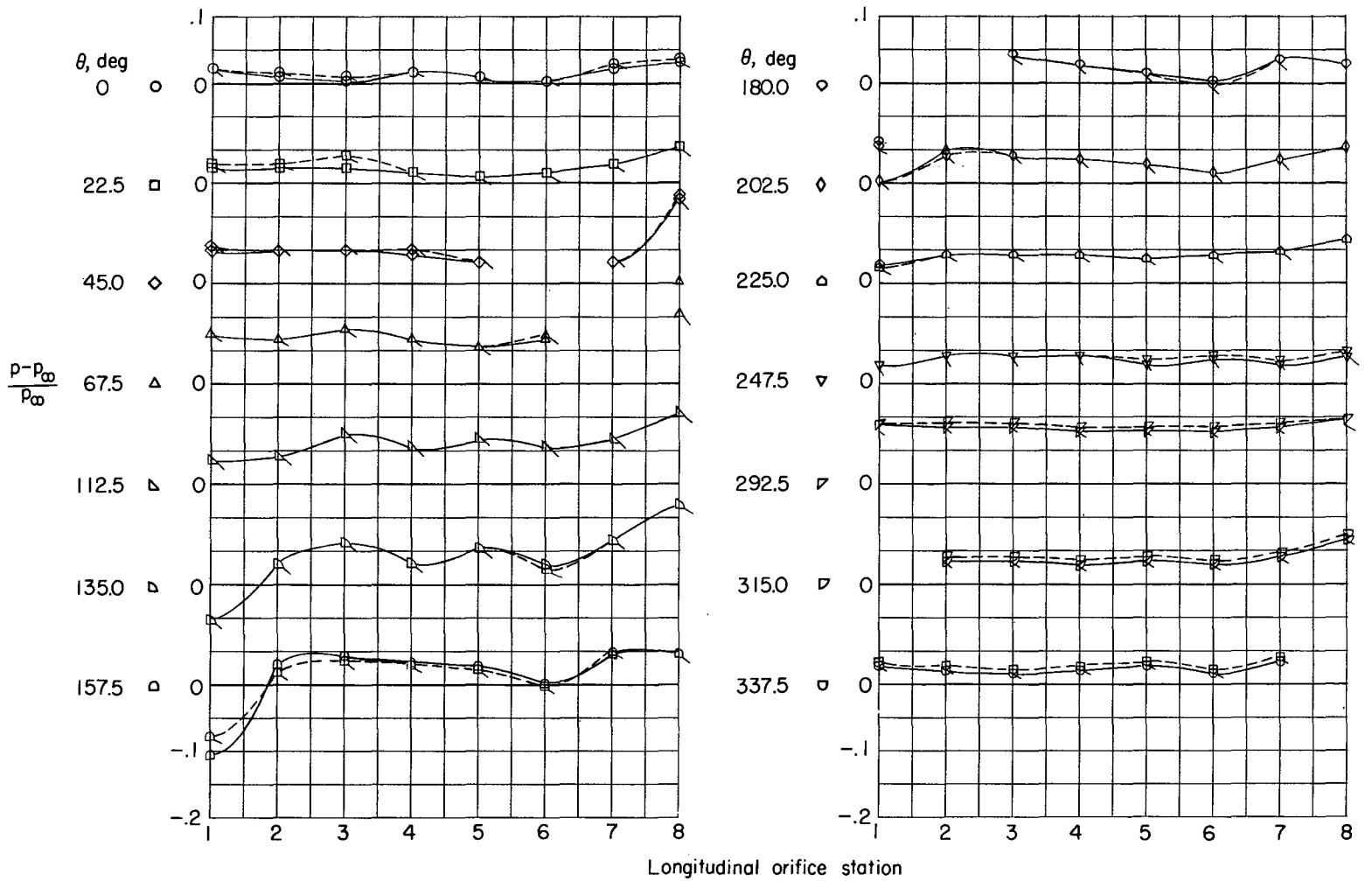
(b) $\alpha = 7.9^{\circ}$.

Figure 9.- Concluded.



(a) $\alpha = 0^{\circ}$.

Figure 10.- Variation of static-pressure error coefficient with longitudinal orifice station for $\phi = 90^{\circ}$, $M = 1.00$, and $w = 0.018$ lb/sec. (Flagged symbols indicate exhaust bleed on.)



(b) $\alpha = 7.9^{\circ}$.

Figure 10.- Concluded.

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