ABSTRACT

This paper will introduce a new implementation for wireless electric power transfer systems: space applications. Due to the risks that constitute the use of electrical connector for some space missions/applications, a simple wireless power system design approach will be evaluated as an alternative for the use of electrical connectors. This approach takes into consideration the overall system performance by designing the magnetic resonance elements and by verifying the overall system electrical behavior. System characterization is accomplished by executing circuit and analytical simulations using Matlab® and LTSpiceIV® software packages. The design methodology was validated by two different experiments: frequency consideration (design of three magnetic elements) and a small scale proof-of-concept prototype. Experiment results shows successful wireless power transfer for all the cases studied. The proof-of-concept prototype provided ≈4 W of wireless power to the load (light bulb) at a separation of 3 cm from the source. In addition, a resonant circuit was designed and installed to the battery terminals of a handheld radio without batteries, making it turn on at a separation of ≈5 cm or less from the source. It was also demonstrated by prototype experimentation that multiple loads can be powered wirelessly at the same time with a single electric power source.

Keywords: Magnetic Resonance, Wireless Power Transfer, Magnetic Coupling, Space Systems, Power Amplifier.
**Overall System Operation**

An electric source circuit generates a sinusoidal signal (represented by a power amplifier, PA, in Fig. 1) inducing magnetic pulsation signals at the primary loop \((L_1)\) of the source resonating circuit \((C_1\text{ and } L_1)\). The secondary loop \((L_2)\) will receive the magnetic pulses due to the fact that is part of the load resonating circuit \((C_2\text{ and } L_2)\). The load resonating circuit is tuned to the same frequency as the primary circuit. This magnetic energy induces a sinusoidal electric signal in the secondary [2]. The alternate current (AC) signal is then rectified by a diode H-bridge and a capacitor to provide a direct current (DC) signal to the load. This will transfer energy wirelessly from the primary circuit (Vin, source) to the secondary circuit (Load) [2].

The overall system analysis and design was performed by a systematic series of simulations using the combination of Matlab® and LTSpiceIV® software packages. This integrated system circuit simulation combines different technical topics evaluated for the design. These topics were divided into two main design simulations: magnetic elements simulation and system circuit simulation. Each of these simulations provides an important contribution for the overall understanding of the system’s electrical behavior.

**Magnetic Elements Simulation**

The magnetic elements (Fig. 2) will be defined as the primary and secondary loops with their respective coupling capacitor for resonant circuit. To determine the magnetic element parameters, a Matlab® based code was generated using simple electromagnetic and circuit equations. This tool helped us to understand how to design the inductor loops and their corresponding coupling capacitor for the desired operating frequency.

![Fig. 2. WPT System Magnetic Element Definition](image)

The Eq. (1) defines the self inductance \((L)\) of an inductor loop with no magnetic core [3]:

\[
L = N^2 \ast R \ast \mu_0 \ast \left[ \ln \left( \frac{8R}{r} \right) - 1.75 \right]
\]  

Where:
- \(L\) = inductance of the loop
- \(N\) = number of turns in the loop
- \(R\) = radius of the loop
- \(r\) = loop conductor radius
- \(\mu_0\) = permeability of vacuum

In order to adequately transfer power wirelessly, the primary and the secondary magnetic loops need to be tuned to the same resonant frequency \((\omega_0, f_0)\). This tuning is accomplished by connecting a capacitor in series to the primary circuit and in parallel to the secondary circuit (also known as series-parallel coupling) [4]. The Eq. (2) is utilized to determine the capacitor value required to generate the resonant circuit with the inductor [5]:

\[
C = \frac{1}{\omega_0^2 \ast L}
\]  

Where:
- \(C\) = coupling capacitance required
- \(\omega_0\) = frequency of oscillation [rad/sec]
- \(L\) = inductance of the coil

An additional important calculation to be considered is the mutual inductance between the two loops. This value will be calculated for the required separation distance of the vacuum gap and then simulated in LTSpiceIV® to determine the overall circuit response. Before calculating the mutual inductance, it is required to determine the magnetic coupling coefficient using the Eq. (3) [6]. By using the magnetic coupling coefficient, a characterization of the mutual inductance can be obtained with Eq. (4) [7].

\[
k = \frac{1}{1 + 2/3 \left( \frac{D}{\sqrt{R_1 R_2}} \right)^{3/2}}
\]

\[
L_M = k \ast \sqrt{L_1 \ast L_2}
\]

Where:
- \(k\) = mutual coupling coefficient
- \(D\) = physical distance between \(L_1\) and \(L_2\)
- \(R_1\) = radius of the loop 1
- \(R_2\) = radius of the loop 1
- \(L_M\) = mutual inductance
- \(L_1\) = inductance of the loop 1
- \(L_2\) = inductance of the loop 2

A simple proof-of-concept prototype was assembled to demonstrate the proposed design methodology. The parameters used in the proof-of-concept prototype are listed in Table 1. These parameters will be later used to calculate the coupling capacitors, self inductance of the loops, and mutual inductance parameters. The calculated parameters using the developed Matlab® code are shown in Table 2.

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Symbol</th>
<th>Value</th>
<th>Units</th>
</tr>
</thead>
<tbody>
<tr>
<td>Number of turns</td>
<td>(N_1) &amp; (N_2)</td>
<td>8</td>
<td>turns</td>
</tr>
<tr>
<td>Radius of the Loops</td>
<td>(R_1) &amp; (R_2)</td>
<td>0.24</td>
<td>m</td>
</tr>
<tr>
<td>Loop conductor radius</td>
<td>(r_1) &amp; (r_2)</td>
<td>0.001</td>
<td>m</td>
</tr>
<tr>
<td>Loop conductor resistance (in DC)</td>
<td>(a)</td>
<td>0.064</td>
<td>Ohm</td>
</tr>
<tr>
<td>Frequency of operation</td>
<td>(f_0)</td>
<td>15</td>
<td>kHz</td>
</tr>
<tr>
<td>Vacuum Permeability</td>
<td>(\mu_0)</td>
<td>94.25</td>
<td>k Rad/s</td>
</tr>
<tr>
<td>Load (light bulb)</td>
<td>(R_0)</td>
<td>4</td>
<td>Ohms</td>
</tr>
<tr>
<td>Separation distance</td>
<td>(D)</td>
<td>0.03</td>
<td>m</td>
</tr>
</tbody>
</table>

The loop conductor resistance (litz wire cable) was calculated using reference [8]. Measured resistance for the filament. However, it was noted after system simulation and prototype experimentation that the light bulb filament was behaving as a 40 Ohms resistor.

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Symbol</th>
<th>Value</th>
<th>Units</th>
</tr>
</thead>
<tbody>
<tr>
<td>Self Inductance</td>
<td>(L_1) &amp; (L_2)</td>
<td>49.38</td>
<td>(\mu H)</td>
</tr>
<tr>
<td>Mutual Inductance</td>
<td>(L_M)</td>
<td>42.85</td>
<td>(\mu H)</td>
</tr>
<tr>
<td>Coupling Capacitor</td>
<td>(C_1) &amp; (C_2)</td>
<td>2.14</td>
<td>(\mu F)</td>
</tr>
<tr>
<td>Leakage Inductances</td>
<td>(L_{1kl}) &amp; (L_{1k2})</td>
<td>6.533</td>
<td>(\mu H)</td>
</tr>
</tbody>
</table>

The Mylar capacitors of 2.2uF (5% accuracy) were used. After circuit testing, the coupling frequency was found to be 15.5 kHz.
3. RESULTS

The analysis previously discussed was validated using two different experiments to better characterize the magnetic resonance concept: frequency considerations and a small scale proof-of-concept prototype.

Experiment #1: Frequency Considerations

To analyze the frequency of operation effects, three circuit configurations were designed with the same inductor loop characteristics (Table 3). The three frequencies of operation studied were: 84 kHz, 839 kHz and 1.757 MHz. The self inductances of the magnetic loops were determined with the Eq. (1) and coupling capacitors were selected to match the frequency of operation according to the Eq. (2). The testing configuration is illustrated in Fig. 2. The main objective of this test was to preliminary study the magnetic element behavior at different frequencies and validate that magnetic resonance can be achieved with the design approach described in the previous section (Analysis).

<table>
<thead>
<tr>
<th>Characteristic</th>
<th>Loop 1</th>
<th>Loop 2</th>
</tr>
</thead>
<tbody>
<tr>
<td>Radius [cm]</td>
<td>7.5</td>
<td>7.5</td>
</tr>
<tr>
<td>Number of Turns</td>
<td>7</td>
<td>7</td>
</tr>
</tbody>
</table>

The frequency consideration test results are listed in Table 4 and illustrated in Fig. 6. The testing circuit (Fig. 2) was powered by a function generator. The settings of the function generator remained unchanged throughout these tests for all three cases. The main objective of this experiment was met (to validate the magnetic coupling design approach described in the Analysis section). In addition, it was also noticed for the frequencies studied that magnetic coupling is greater at higher frequencies of operations. Further analysis/testing will be required to determine which frequency is the optimal.

<table>
<thead>
<tr>
<th>Frequency of Operation</th>
<th>Separation Distance (cm)</th>
<th>Vout (Vpeak)</th>
</tr>
</thead>
<tbody>
<tr>
<td>84 kHz</td>
<td>0</td>
<td>5</td>
</tr>
<tr>
<td></td>
<td>4</td>
<td>1.5</td>
</tr>
<tr>
<td></td>
<td>14</td>
<td>200mV</td>
</tr>
<tr>
<td>839 kHz</td>
<td>0</td>
<td>10</td>
</tr>
<tr>
<td></td>
<td>4</td>
<td>20</td>
</tr>
<tr>
<td></td>
<td>14</td>
<td>2.2</td>
</tr>
<tr>
<td>1.757 MHz</td>
<td>0</td>
<td>15</td>
</tr>
<tr>
<td></td>
<td>4</td>
<td>34</td>
</tr>
<tr>
<td></td>
<td>14</td>
<td>5</td>
</tr>
</tbody>
</table>

Note: The settings of the function generator (V,.) remained unchanged throughout these tests (all three cases).

4. CONCLUSION

The magnetic resonance concept was successfully demonstrated using two different experimental setups. The frequency consideration test results showed that magnetic coupling is greater at higher frequencies of operations. Further analysis/testing will be required to determine which frequency is the optimal.
Experiment #2: Small Scale Proof-of-Concept Prototype

A small scale proof-of-concept prototype was assembled with the values provided on Table 1 and Table 2 to validate the design approach discussed in the Analysis section. Using the block diagram in Fig. 1 as the design guideline, a series of commercial parts were evaluated, individually tested and selected to complete the prototype design (Fig. 7).

Due to the fact that the loops inductors were manually built, variability on the inductance value is expected. The Agilent LCR Meter 4980A was used to measure the inductances of the loops at the prototype operating frequency (15.5 kHz). Table 5 lists the measured loop inductances and the calculated mutual inductance for a separation distance of 3 cm. Fig. 8 illustrates the inductors built for the small scale prototype.

Two different alternatives were implemented/designed to provide the frequency of operation (sinusoidal at 15.5 kHz) required by the PA: XR2206 function generator integrated circuit [10] and by programming an audio signal. The audio signal was programmed in Matlab® as a sinewave with the required frequency, an audio file format (Windows Media Audio or WMA) was generated using Matlab®'s "wavwrite" command and then the audio file was downloaded and played using the iPhone music player. The iPhone's output is connected to the PA as the function generator (Fig. 11). The amplitude of this signal was controlled by the volume of the iPhone. Fig. 11 illustrates the output voltage supplied by the iPhone using the audio signal programmed in Matlab®.

The WPT LTSpiceIV® model was updated with the loop measurements acquired with the LCR meter (Fig. 9) and the simulation output is illustrated in Fig. 10. The green trace is the function generator/power amplifier voltage source (V_{in}), the blue trace is the secondary voltage before rectification (V_{c2}) and the red trace is the circuit output voltage (V_{out, out}).

![Fig. 7. Small Scale Proof-of-Concept Prototype](image1)

![Fig. 8. Loop Inductors Built for the Small Scale Prototype](image2)

![Fig. 9. Wireless Power Transfer Model with Measured Loop Inductances with a Separation Distance of D = 3cm](image3)

![Fig. 10. Simulation Output of the WPT Model with Measured Loop Inductances](image4)

The system operating frequency ($f_o$) was targeted to be 15 kHz; however, after further calibration and tuning, the system demonstrated to be magnetically coupled at ~15.5 kHz. This discrepancy is attributed to the coupling capacitor tolerance of 5%, the loop conductor radius measurement and the variability of the manually built inductor loops. An accurate representation of the loop conductor radius and coupling capacitor values are required for an accurate system coupling according to Eq. (1), Eq. (2) and Eq. (3).

Two different alternatives were implemented/designed to provide the frequency of operation (sinusoidal at 15.5 kHz) required by the PA: XR2206 function generator integrated circuit [10] and by programming an audio signal. The audio signal was programmed in Matlab® as a sinewave with the required frequency, an audio file format (Windows Media Audio or WMA) was generated using Matlab®'s "wavwrite" command and then the audio file was downloaded and played using the iPhone music player. The iPhone’s output is connected to the PA as the function generator (Fig. 11). The amplitude of this signal was controlled by the volume of the iPhone. Fig. 11 illustrates the output voltage supplied by the iPhone using the audio signal programmed in Matlab®.

![Table 5: Measured Loop Inductances and Mutual Inductance](image5)
The prototype performance was carefully characterized by measuring and plotting the output root mean square (RMS) voltage, current and power for different source/load separation distances (Fig. 14, Fig. 15 and Fig. 16). It is noticed that the optimum power transfer separation is about 3 cm (~4W). The peak power transfer distance result concurred with a similar study performed on magnetic resonance [12].
It is noticed that the theory presented in the Analysis section provides similar results than the small scale proof-of-concept prototype experimental results. However, it is also noticed that due to parasitic effects and unwanted capacitive coupling, internal to the inductor windings, provides an unpredicted response in the test data. Further analysis and experimentation will be required for an overall more accurate electrical characterization of the system.

An additional test performed to the prototype was to add a non-conductive material between the source element and the load element (i.e. wood, plastic, etc.). As expected, magnetic coupling was achieved even through a non-conductive material.

A second load was designed to operate using the prototype source (Fig. 17). A receiving magnetic element was designed and connected to the battery terminals of a handheld radio (Durabrand PR-355 AM/FM Sports Radio) to resonate at the same frequency as the wireless power source previously described \( f_0 \approx 15.5\text{kHz} \). The WPT receiver device designed to the handheld radio replaced the use of 3 AA batteries. The radio turns on within a proximity of \( ~5 \text{ cm} \) from the source. It was also noticed that the radio and the light bulb can receive power wirelessly at the same time using the same power source.

![Fig. 17. Loads: Light Bulb (left) and Handheld Radio (right)](image)

### 4. CONCLUSION

Theory analysis and experimental results suggest that magnetic resonance is a feasible and reliable technology that represents an alternative to conventional electric connectors. Preliminary testing also showed that magnetic resonance can be achieved through non-conductive materials (i.e. wood, plastic, etc.). Multiple mobile devices can be powered/recharged at the same time using a single source. This was accomplished by tuning the source and all the loads to the same operating frequency. In addition, it was demonstrated by prototype experimentation that magnetic resonance can be achieved within audible frequencies \((20\text{Hz} \leq f_0 \leq 20 \text{kHz})\). This can represent a major industrial advantage due to the fact that there are currently a wide range of options available for audio power amplifiers.

More testing and experimental data will be required for the implementation of a reliable and efficient wireless power system for space applications. In theory, the magnetic resonance principle is believed to operate in the space environment. However, using the principles discussed in this paper and additional analysis, a more advanced design will be evaluated for compliance to NASA and other military systems standards [13][14][15][16]. Design compliance to these standards will be highly dependent on the system application (i.e. launch vehicles, spacecraft, rover, wireless battery charger, docking systems, etc.)

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