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BASIC PRESSURE MEASUREMENTS ON A 0.0667-SCALE MODEL OF THE NORTH AMERICAN X-15 RESEARCH AIRPLANE AT TRANSONIC SPEEDS

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Langley Research Center
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SUMMARY

In order to determine local loadings and interference effects at transonic speeds, basic pressure measurements have been made on a 0.0667-scale model of an interim configuration of the North American X-15 research airplane in the Langley 8-foot transonic pressure tunnel at Mach numbers from 0.60 to 1.18, angles of attack from -20° to 20°, and angles of sideslip from -5° to 5°. The results are presented in tabular form without analysis.

INTRODUCTION

As part of the wind-tunnel program required for the development of the North American X-15 research airplane, a 0.0667-scale pressure model of an interim configuration of the X-15 has been tested in the Langley 8-foot transonic pressure tunnel in order to determine local pressures on the fuselage-fairing-canopy area and local pressures and interference effects on the horizontal and vertical tail surfaces at transonic speeds. Tests of this model at Mach numbers from 2.30 to 4.65 are reported in reference 1. Tests of force models of the configuration are reported in references 2 to 5.

The X-15 is a rocket-powered research airplane designed for hypersonic speeds at very high altitudes. It employs a 5-percent-thick low-aspect-ratio trapezoidal wing mounted in the midposition on a fuselage consisting of a body of revolution with large side fairings. The 45° sweptback horizontal tail is all-movable for pitch control and may be deflected differentially for roll control. The outboard panels of the

upper and lower vertical-tail surfaces may be deflected for directional control; the inboard panels are fixed and support the speed brakes.

The model was tested at Mach numbers from 0.60 to 1.18, angles of attack from -20° to 20°, and angles of sideslip from -5° to 5°. Local pressure coefficients were obtained for the model with the speed brakes open and closed and with vertical-tail deflections from -7.5° to 7.5°. The results are presented in tabular form without analysis.

SYMBOLS

b	exposed span
C_p	pressure coefficient, $\frac{p_l - p}{q}$
c	local chord measured parallel to fuselage center line
$\bar{c}$	mean aerodynamic chord
l	fuselage length
M	free-stream Mach number
p	free-stream static pressure
p_l	local static pressure
q	free-stream dynamic pressure
R	Reynolds number
x	distance from nose of fuselage or from leading edge of airfoil surface measured parallel to fuselage center line
y	spanwise distance measured from juncture of airfoil surface and fuselage or fuselage side fairings
α	angle of attack of fuselage center line
β	angle of sideslip
δ_e	deflection of horizontal tail, positive when trailing edge is down

δ_V deflection of upper and lower vertical tail surfaces, positive when trailing edge is to the left

ϕ angular location of fuselage orifices, measured counterclockwise from bottom of fuselage when facing forward

Orifice locations:

C canopy

F fuselage side fairings

J fuselage-canopy juncture

APPARATUS AND TESTS

Model

The 0.0667-scale pressure model of the North American X-15 research airplane used in this investigation was supplied by the contractor. It was constructed of stainless steel. Photographs of the model are presented in figure 1, and dimensional details are shown in figure 2 and table I.

The model closely approximated configuration 3 of the X-15. Distinguishing features of this configuration as compared to earlier configurations include an increased fuselage diameter, shortened fuselage side fairings, increased leading-edge radii on wing and horizontal tail, a larger vertical tail having 10° full-wedge airfoil sections and with the total exposed area distributed 55 percent above the fuselage and 45 percent below, and reduced speed-brake area. Unlike configuration 3, however, the wing of the configuration tested had not been moved forward 3.6 inches (full scale), the horizontal tail had not been moved rearward 5.4 inches (full scale), and there were no landing skids. The contractor's code designation of the model tested was $B_2W_2X_4H_3V_{U_5}J_{U_2}V_{L_7}J_{L_2}$.

The horizontal tail was fixed at a deflection angle of 0° for these tests, whereas the speed brakes and the outer panels of the upper and lower vertical tail surfaces could be deflected about hinge lines having 0° sweepback.

Tunnel and Model Support

The tests were conducted in the Langley 8-foot transonic pressure tunnel which is a single-return, rectangular, slotted-throat wind tunnel

having controls that allow for the independent variation of Mach number, stagnation pressure, temperature, and humidity.

The model was attached to a sting support which had a diameter approximately equal to that of the base of the fuselage. The sting support was cylindrical for 4.5 base diameters downstream of the model base and at its downstream end was attached to the larger tunnel support sting which could be rotated by means of an arc-shaped support strut to obtain changes in angle of attack. Variations in angle of sideslip were obtained by insertion of properly angled couplings in the model support system.

Measurements and Accuracy

Local static pressures were measured by using a total of 205 flush-mounted orifices distributed over the right half of the model. Measurements on the right wing were limited to one row of orifices on the upper and lower surfaces and on the right horizontal tail to two rows of orifices on the upper and lower surfaces. One orifice was located in the base of the upper vertical tail. Orifice locations are diagrammed and tabulated in figure 3. Pressure coefficients were determined from these measurements and are believed to be accurate within ±0.005.

The angle of attack was set to within ±0.1° and the angle of sideslip to within ±0.2° by means of a pendulum-type attitude indicator and calibrations of sting deflection with respect to model load. Model loads were determined from wind-tunnel tests of a nearly identical force model of the X-15 airplane. Control deflection inaccuracies are unknown but are believed to be small.

The average test Mach number was determined to within ±0.003 from a calibration with respect to the pressure in the chamber surrounding the slotted test section.

Tests

The complete model was tested with the horizontal tail undeflected and the speed brakes closed for vertical-tail deflections of -7.5°, 0°, and 7.5°. The model was also tested with the horizontal and vertical tails undeflected and the speed brakes opened 35°.

The model was tested at Mach numbers from 0.60 to 1.18, angles of attack from -20° to 20°, and angles of sideslip of -5°, 0°, and 5°. The tests were conducted at a tunnel stagnation pressure of approximately 1 atmosphere, the average test Reynolds number based on the wing mean

aerodynamic chord varying from approximately 2.2×10^6 to 2.8×10^6 over the Mach number range. (See fig. 4.) For all tests, boundary-layer transition strips consisting of No. 120 carborundum grains were installed along the 10-percent-chord lines of the wing and tail surfaces and at 10 percent of the body length.

Corrections

Tunnel boundary interference at subsonic speeds is minimized by the slotted test section, and no corrections for this interference have been applied. With respect to supersonic boundary-reflected disturbances, the effects of reflected compression waves on the pressure distribution over the model are negligible at a Mach number of 1.03, and the effects of reflected expansion waves were minimized by testing the model a few inches off the tunnel center line. (See ref. 6.) At a Mach number of 1.18 the reflected disturbances passed well downstream of the base of the model.

SUMMARY OF RESULTS

The pressure coefficients for each surface of a 0.0667-scale model of the X-15 airplane are tabulated as a function of configuration, Mach number, angle of attack, and angle of sideslip and are presented in tables II to VI as follows:

Surface	Table
Fuselage	II
Right wing	III
Right horizontal tail	IV
Vertical tails and speed brakes	V
Base of upper vertical tail	VI

Langley Research Center,
National Aeronautics and Space Administration,
Langley Field, Va., July 13, 1960.

REFERENCES

1. Hodge, B. Leon, and Burbank, Paige B.: Pressure Distribution of a 0.0667-Scale Model of the X-15 Airplane for an Angle-of-Attack Range of 0° to 28° at Mach Numbers of 2.30, 2.88, and 4.65. NASA TM X-275, 1960.

2. Lopez, Armando E., and Tinling, Bruce E.: The Static and Dynamic-Rotary Stability Derivatives at Subsonic Speeds of a Model of the X-15 Research Airplane. NACA RM A58F09, 1958.

3. Tunnell, Phillips J., and Latham, Eldon A.: The Static and Dynamic-Rotary Stability Derivatives of a Model of the X-15 Research Airplane at Mach Numbers From 1.55 to 3.50. NASA MEMO 12-23-58A, 1959.

4. Franklin, Arthur E., and Lust, Robert M.: Investigation of the Aerodynamic Characteristics of a 0.067-Scale Model of the X-15 Airplane (Configuration 3) at Mach Numbers of 2.29, 2.98, and 4.65. NASA TM X-38, 1959.

5. Dunning, Robert W.: The Control Characteristics of Two Preliminary Models of the X-15 Research Airplane at Mach Numbers of 2.98 and 4.01. NASA TM X-212, 1960.

6. Wright, Ray H., Ritchie, Virgil S., and Pearson, Albin O.: Characteristics of the Langley 8-Foot Transonic Tunnel With Slotted Test Section. NACA Rep. 1389, 1958. (Supersedes NACA RM L51H10 by Wright and Ritchie and RM L51K14 by Ritchie and Pearson.)

TABLE I.- DIMENSIONS OF THE 0.0667-SCALE PRESSURE MODEL OF THE NORTH AMERICAN X-15 RESEARCH AIRPLANE

Wing:	
Airfoil section	Modified NACA 66-005
Total area, sq in.	128.150
Exposed area, sq in.	67.260
Total span, in.	17.898
Exposed span, in.	12.028
Total aspect ratio	2.50
Leading-edge sweepback, deg	36.75
Quarter-chord-line sweepback, deg	25.64
Trailing-edge sweepforward, deg	17.75
Root chord at center line, in.	11.932
Exposed root chord, in.	8.801
Tip chord, in.	2.386
Total taper ratio	0.20
Mean aerodynamic chord based on total area, in.	8.220
Longitudinal distance from fuselage nose to $\bar{c}/4$, in.	23.411
Dihedral, deg	0
Incidence, deg	0
Horizontal tail (in plane of surface):	
Airfoil section	Modified NACA 66-005
Total area, sq in.	73.850
Exposed area, sq in.	32.710
Total span, in.	14.980
Exposed span, in.	9.068
Exposed aspect ratio	2.51
Leading-edge sweepback, deg	50.58
Quarter-chord-line sweepback, deg	45.00
Trailing-edge sweepback, deg	19.28
Root chord at center line, in.	8.175
Exposed root chord, in.	5.616
Tip chord, in.	1.686
Exposed taper ratio	0.30
Mean aerodynamic chord based on exposed area, in.	4.002
Hinge line, percent exposed $\bar{c}$	37
Longitudinal distance from total wing $\bar{c}/4$ to exposed tail $\bar{c}/4$, in.	11.450
Dihedral, deg	-15.00
Upper vertical tail (exposed panel):	
Airfoil section	10° wedge
Area, sq in.	26.075
Span, in.	3.668
Aspect ratio	0.52
Leading-edge sweepback, deg	30
Trailing-edge sweepback, deg	0

TABLE I.- DIMENSIONS OF THE 0.0667-SCALE PRESSURE MODEL OF

THE NORTH AMERICAN X-15 RESEARCH AIRPLANE - Concluded

Root chord, in.	8.171
Tip chord, in.	6.053
Taper ratio	0.74
Mean aerodynamic chord, in.	7.153
Longitudinal distance from total wing $\bar{c}/4$ to exposed panel $\bar{c}/4$, in.	9.630
Movable portion -	
Area, sq in.	16.945
Span, in.	2.501
Root chord, in.	7.495
Tip chord, in.	6.053
Hinge line, percent exposed panel $\bar{c}$	29
Speed brake (one side) -	
Area, sq in.	3.533
Chord, in.	2.560
Average span, in.	1.380
Lower vertical tail (exposed panel):	
Airfoil section	10° wedge
Area, sq in.	22.385
Span, in.	3.068
Aspect ratio	0.42
Leading-edge sweepback, deg	30
Trailing-edge sweepback, deg	0
Root chord, in.	8.171
Tip chord, in.	6.420
Taper ratio	0.79
Mean aerodynamic chord, in.	7.322
Longitudinal distance from total wing $\bar{c}/4$ to exposed panel $\bar{c}/4$, in.	9.516
Movable portion -	
Area, sq in.	13.220
Span, in.	1.901
Root chord, in.	7.495
Tip chord, in.	6.420
Hinge line, percent exposed panel $\bar{c}$	30
Speed brake (one side) -	
Area, sq in.	3.533
Chord, in.	2.560
Average span, in.	1.380
Fuselage:	
Length, in.	39.353
Maximum depth, in.	3.733
Maximum width with side fairings, in.	5.867
Fineness ratio without side fairings	10.54
Base diameter, in.	3.193

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE

(a) M = 0.60

Pressure coefficients C_p on -

Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage								Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage - Concluded							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx -5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed											$\beta \approx -5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed							
1	.026	0				.152	.234	.327	.431	.544	55	.503	F				.004	-.058	-.307	-.678	-.687
2	.026	90				.116	.082	.006			56	.503	135				-.008	-.052	-.124	-.200	-.351
3	.026	180				.151	.077	.010			57	.588	0				-.038	.041	.123	.208	.306
4	.084	0				.028	.100	.188	.286	.396	58	.588	180				-.030	-.104	-.212	-.267	-.357
5	.084	45				-.001	.026	-.005			59	.604	15				-.036	.033	.105	.182	.269
6	.084	90				.014	-.026	-.077			60	.604	30				-.030	.047	.121	.193	.272
7	.084	135				-.003	-.031	-.071			61	.604	50				-.035	.055	.145	.228	.319
8	.084	180				.041	-.022	-.074			62	.604	F				-.042	.068	.174	.271	.366
9	.134	J				.084	.036	.003			63	.604	F				-.038	-.140	-.214	-.623	-1.251
10	.156	J				.003	-.030	-.043	-.036		64	.604	135				-.030	-.113	-.229	-.366	-.679
12	.173	30				-.077	-.061	-.050	-.027		65	.690	0				-.010	.038	.088	.140	.214
13	.173	60				-.083	-.097	-.143	-.212		66	.690	180				-.017	-.050	-.117	-.238	-.302
14	.173	90				-.084	-.099	-.157	-.247		67	.706	15				-.005	.031	.072	.113	.172
15	.173	135				-.084	-.086	-.098	-.125		68	.706	30				.001	.036	.071	.108	.158
16	.173	J				-.057	-.073	-.071	-.058		69	.706	50				.006	.046	.084	.122	.171
17	.173	C				-.026	-.063	-.083	-.084		70	.706	F				.014	.053	.092	.128	.172
18	.190	J				-.109	-.106	-.096	-.078		71	.706	F				-.023	-.051	-.099	-.167	-.310
19	.190	C				-.123	-.148	-.162	-.164		72	.706	135				-.012	-.046	-.097	-.203	-.251
20	.197	C				-.317	-.369	-.403	-.409		73	.753	0				.080	.110	.146	.183	.236
21	.207	C				-.234	-.251	-.267	-.271	-.221	74	.753	180				.067	.039	.010	-.097	-.172
23	.216	C				-.254	-.278	-.271	-.245	-.219	75	.770	15				-.086	-.062	-.029	.017	.060
24	.226	23				-.088	-.076	-.058	-.022	.023	76	.770	30				-.031	-.011	.015	.048	.073
25	.226	45				-.084	-.089	-.115	-.147	-.191	77	.770	50				-.008	.019	.046	.078	.106
26	.226	68				-.091	-.114	-.175	-.267	-.396	78	.770	F				.017	.039	.063	.081	.087
27	.226	90				-.092	-.112	-.175	-.279	-.426	79	.770	F				.046	.048	.038	.018	-.024
28	.226	135				-.167	-.183	-.205	-.243	-.322	80	.770	F				-.006	-.020	-.042	-.086	-.146
29	.226	C				-.251	-.254	-.258	-.263	-.273	81	.770	135				-.040	-.048	-.060	-.094	-.136
30	.263	C				-.108	-.124	-.118	-.094	-.102	82	.820	15				-.063	-.033	.003	.053	.105
31	.283	0				-.094	-.062	-.009	.063	.153	83	.820	38				-.049	-.014	.022	.067	.110
32	.299	30				-.075	-.075	-.074	-.063	-.043	84	.820	F				-.040	-.004	.040	.092	.153
33	.299	60				-.060	-.033	-.026	-.030	-.047	85	.820	F				-.027	.012	.052	.102	.154
34	.299	F				-.066	-.036	-.048	-.104	-.204	86	.820	F								
35	.299	F				-.044	-.083	-.203	-.398	-.691	87	.820	F				.021	.060	.109	.162	.188
36	.299	F				-.069	-.143	-.262	-.422	-.625	88	.820	F				-.045	-.077	-.127	-.201	-.221
37	.299	135				-.106	-.077	-.095	-.150	-.216	89	.820	F				-.042	-.068	-.113	-.164	-.189
38	.319	C				-.026	-.055	-.092	-.118	-.181	90	.820	F				-.050	-.073	-.104	-.140	-.189
39	.350	20				-.042	-.030	-.013	.021	.073	91	.820	F				-.059	-.080	-.106	-.140	-.187
40	.350	40				-.031	-.024	-.024	-.020	-.016	92	.820	142				-.013	-.100			
41	.350	60				-.031	-.005	.023	.058	.096	94	.897	30				-.120	-.092	-.057	-.005	.055
42	.350	F				-.035	-.014	-.023	-.056	-.106	95	.897	50				-.124	-.097	-.057	.002	.071
43	.350	F				-.036	-.088	-.245	-.502	-.889	96	.897	F				-.124	-.091	-.048	.016	.086
44	.350	F				-.031	-.075	-.150	-.287	-.486	97	.897	F				-.133	-.159	-.190	-.236	-.296
45	.350	135				-.009	-.026	-.063	-.104	-.126	98	.897	130				-.126	-.141	-.167	-.209	-.281
46	.367	0				-.045	-.014	.033	.103	.192	99	.897	150				-.132	-.146	-.157	-.198	-.274
47	.367	180				-.018	-.044	-.060	-.085	-.135	102	.984	0				-.259	-.241	-.241	-.223	-.193
48	.486	0				-.028	.020	.085	.165	.259	104	.984	60				-.190	-.179	-.186	-.184	-.189
49	.486	180				-.027	-.069	-.142	-.178	-.175	105	.984	90				-.184	-.176	-.183	-.188	-.213
50	.503	15				-.022	.022	.073	.138	.219	106	.984	135				-.164	-.161	-.150	-.153	-.166
51	.503	30				-.015	.020	.058	.101	.159	107	.984	180				-.309	-.317	-.297	-.344	-.394
52	.503	50				-.010	.032	.078	.130	.188											
53	.503	F				.008	.033	.053	.074	.098											
54	.503	F				.009	-.085	-.316	-.578	-.953											

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(a) M = 0.60 - Continued

Pressure coefficients C_p on -

Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage								Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage - Concluded							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx -5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open											$\beta \approx -5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open							
1	.026	0	-.069	.010	.110	.163	.243	.335	.441	.553	55	.503	F	.091	.048	.030	.012	-.059	-.317	-.684	-.686
2	.026	90	-.309	.002	.106	.125	.086	.007	-.119	-.309	56	.503	135	.148	.064	.023	.000	-.047	-.118	-.198	-.361
3	.026	180	.554	.345	.208	.158	.078	.012	-.018	-.064	57	.588	0	-.357	-.216	-.064	-.019	.059	.138	.221	.320
4	.084	0	-.131	-.077	-.005	.037	.109	.195	.295	.406	58	.588	180	.291	.123	.024	-.019	-.096	-.203	-.256	-.352
5	.045	84	-.195	-.054	.005	.008	.030	-.002	-.017	-.059	59	.604	15	-.365	-.194	-.060	-.018	.053	.124	.198	.283
6	.084	90	-.398	-.085	-.010	.024	-.025	-.083	-.203	-.391	60	.604	30	-.456	-.175	-.058	-.011	.064	.136	.206	.285
7	.084	135	-.079	-.010	.007	.004	-.027	-.070	-.122	-.199	61	.604	50	-.769	-.212	-.065	-.015	.076	.162	.245	.330
8	.084	180	.410	.211	.091	.046	-.021	-.074	-.081	-.122	62	.604	F	-1.156	-.236	-.093	-.020	.088	.192	.286	.379
9	.134	J	.393	.221	.120	.090	.036	.009	-.016	-.050	63	.604	F	.354	.176	.042	-.026	-.139	-.202	-.676	-1.265
10	.156	J	.219	.086	.027	.011	-.022	-.037	-.032	.004	64	.604	135	.285	.136	.029	-.017	-.108	-.218	-.363	-.705
12	.173	30	-.170	-.102	-.079	-.065	-.054	-.042	-.019	.004	65	.690	0	-.307	-.109	-.007	.018	.065	.112	.162	.235
13	.173	60	-.280	-.137	-.082	-.073	-.093	-.143	-.213	-.321	66	.690	180	.180	.071	.030	.006	-.033	-.098	-.224	-.296
14	.173	90	-.449	-.179	-.088	-.073	-.096	-.156	-.255	-.407	67	.706	15	-.250	-.096	.005	.024	.060	.096	.136	.193
15	.173	135	-.220	-.130	-.084	-.073	-.082	-.094	-.122	-.166	68	.706	30	-.195	-.059	.008	.030	.062	.097	.131	.180
16	.173	J			-.043	-.050	-.068	-.060	-.053	-.040	69	.706	50	-.163	-.060	.016	.035	.069	.108	.145	.193
17	.173	C	.174	.046	-.008	-.018	-.061	-.082	-.082	-.096	70	.706	F	-.208	-.059	.022	.042	.076	.117	.150	.192
18	.190	J	-.040	-.102	-.105	-.104	-.101	-.089	-.074	-.126	71	.706	F	.122	.049	.028	.002	-.031	-.079	-.157	-.311
19	.190	C	.054	-.047	-.097	-.112	-.147	-.157	-.163	-.145	72	.706	135	.120	.047	.025	.013	-.025	-.077	-.191	-.243
20	.197	C	.069	-.154	-.267	-.307	-.367	-.396	-.408	-.402	73	.753	0	-.172	.018	.097	.114	.143	.179	.212	.264
21	.207	C	-.072	-.161	-.208	-.224	-.249	-.265	-.265	-.221	74	.753	180	.183	.117	.113	.097	.067	.044	-.080	-.162
23	.216	C	.029	-.140	-.225	-.247	-.273	-.263	-.241	-.216	75	.770	15	-.006	-.062	-.038	-.034	-.018	.014	.063	.095
24	.226	23	-.137	-.094	-.089	-.080	-.070	-.050	-.012	.029	76	.770	30	-.054	-.046	.003	.017	.030	.056	.086	.109
25	.226	45	-.192	-.097	-.074	-.072	-.087	-.113	-.148	-.190	77	.770	50	-.058	-.027	.023	.037	.060	.089	.116	.139
26	.226	68	-.289	-.138	-.085	-.083	-.110	-.173	-.267	-.402	78	.770	F	-.014	-.001	.057	.060	.077	.101	.115	.116
27	.226	90	-.428	-.172	-.092	-.086	-.108	-.175	-.283	-.436	79	.770	F	-.127	.046	.083	.083	.080	.073	.047	-.005
28	.226	135	-.141	-.140	-.156	-.157	-.179	-.202	-.245	-.326	80	.770	F	.006	.011	.042	.032	.017	-.005	-.057	-.137
29	.226	C	-.175	-.215	-.236	-.241	-.249	-.253	-.259	-.270	81	.770	135	.009	-.020	.012	.001	-.010	-.022	-.063	-.118
30	.263	C	.075	-.049	-.090	-.100	-.119	-.109	-.088	-.098	82	.820	15	-.086	-.089	.015	.025	.046	.081	.127	.171
31	.283	C	-.212	-.111	-.099	-.084	-.051	-.001	.072	.161	83	.820	38	-.081	-.071	.017	.038	.065	.100	.138	.174
32	.299	30	-.272	-.084	-.074	-.069	-.071	-.067	-.057	-.042	84	.820	F	-.060	-.048	.029	.045	.076	.117	.164	.215
33	.299	60	-.232	-.138	-.074	-.052	-.029	-.022	-.027	-.048	85	.820	F	-.050	-.047	.040	.054	.083	.123	.168	.210
34	.299	F	-.482	-.235	-.094	-.058	-.027	-.044	-.108	-.211	86	.820	F	-.019	-.015						
35	.299	F	-.657	-.197	-.052	-.037	-.084	-.207	-.415	-.711	87	.820	F	-.002	-.004	.067	.092	.128	.174	.222	.233
36	.299	F	-.241	-.050	-.035	-.062	-.148	-.272	-.441	-.634	88	.820	F	-.009	-.020	.024	.010	-.036	-.072	-.151	-.185
37	.299	135			-.028	-.041	-.065	-.105	-.165	-.233	89	.820	F	-.039	-.019	.028	.016	-.021	-.050	-.108	-.152
38	.319	C	.140	.021	-.011	-.020	-.051	-.087	-.117	-.183	90	.820	F	-.029	-.030	.027	.014	-.019	-.036	-.076	-.149
39	.350	20	-.064	-.039	-.036	-.032	-.023	-.005	.029	.080	91	.820	F	-.018	-.043	.016	.011	-.021	-.029	-.071	-.141
40	.350	40	-.162	-.063	-.031	-.021	-.016	-.016	-.015	-.011	92	.820	142	-.035	-.064	.004	-.006	-.027	-.030	-.054	-.121
41	.350	60	-.124	-.094	-.038	-.022	.004	.032	.065	.105	93	.820	165	-.011	-.074						
42	.350	F	-.431	-.141	-.053	-.025	-.006	-.018	-.053	-.105	94	.897	30	-.174	-.121	.188	.231	.271	.301	.331	.359
43	.350	F	-.823	-.244	-.046	-.028	-.090	-.256	-.533	-.916	95	.897	50	-.184	-.139	.149	.153	.180	.209	.246	.285
44	.350	F	-.099	-.015	-.007	-.025	-.073	-.147	-.295	-.495	96	.897	F	-.180	-.147	.078	.094	.113	.147	.186	.233
45	.350	135	.004	.009	.010	-.002	-.022	-.060	-.098	-.126	97	.897	F	-.065	-.113	.038	.024	-.025	-.007	-.046	-.122
46	.367	0	-.172	-.075	-.048	-.037	-.005	.042	.113	.201	98	.897	130	-.070	-.113	.112	.129	.075	.131	.100	.004
47	.367	180	.215	.068	.007	-.012	-.042	-.053	-.079	-.137	99	.897	150	-.072	-.118	.225	.206	.187	.272	.244	.164
48	.486	0	-.172	-.129	-.038	-.014	.034	.098	.179	.275	102	.984	0	-.350	-.242	-.422	-.421	-.410	-.390	-.339	-.311
49	.486	180	.255	.088	.008	-.018	-.060	-.136	-.172	-.168	103	.984	30	-.255	-.193						
50	.503	15	-.211	-.101	-.033	-.008	.034	.086	.152	.231	104	.984	60	-.190	-.158	-.343	-.348	-.357	-.321	-.326	-.344
51	.503	30	-.378	-.087	-.026	-.003	.032	.069	.113	.170	105	.984	90	-.195	-.168	-.405	-.297	-.323	-.302	-.324	-.310
52	.503	50	-.473	-.109	-.023	.003	.044	.090	.141	.200	106	.984	135	-.154	-.150	-.456	-.449	-.439	-.421	-.488	-.535
53	.503	F	-.545	-.325	-.012	.020	.044	.064	.081	.106	107	.984	180	-.254	-.305	-.453	-.451	-.450	-.465	-.525	-.551
54	.503	F	-.743	-.291	-.010	.020	-.095	-.333	-.607	-.995											

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(a) M = 0.60 - Continued

Pressure coefficients C_p on -

Model orifice number	x/l	ϕ, deg	Fuselage								Model orifice number	x/l	ϕ, deg	Fuselage - Concluded							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			β ≈ 0°; δ_e = 0°; δ_v = 0°; brakes closed											β ≈ 0°; δ_e = 0°; δ_v = 0°; brakes closed							
1	.026	0	-.049	.043		.175	.262	.354	.461	.569	54	.503	F	-.810	-.307		.016	-.093	-.348	-.610	-.876
2	.026	90	-.213	.084		.191	.158	.085	-.045	-.232	55	.503	F	.164	.091		.003	-.073	-.248	-.850	-.752
3	.026	180	.569	.358		.178	.113	.045	-.006	-.051	56	.503	135	.231	.110		-.004	-.060	-.117	-.171	-.259
4	.084	0	-.089	-.041		.049	.125	.227	.326	.431	57	.588	0	-.377	-.175		-.014	.065	.147	.232	.332
5	.084	45	-.307	-.080		.054	.095	.114	.135	.126	58	.588	180	.324	.148		-.014	-.088	-.173	-.259	-.390
6	.084	90	-.331	-.045		.063	.033	-.034	-.149	-.312	59	.604	15	-.412	-.194		-.018	.062	.141	.221	.317
7	.084	135	.099	.103		.053	-.006	-.069	-.163	-.272	60	.604	30	-.427	-.196		-.012	.070	.157	.227	.325
8	.084	180	.436	.238		.065	.012	-.033	-.067	-.088	61	.604	50	-.494	-.223		-.024	.071	.162	.247	.345
9	.134	J	.413	.235		.105	.052	.027	.001	-.014	62	.604	F	-1.133	-.271		-.038	.078	.181	.278	.382
10	.156	J	.351	.212		.132	.086	.063	.038	.011	63	.604	F	.373	.174		-.040	-.161	-.254	-.301	-1.201
12	.173	30	-.189	-.116		-.049	-.007	.034	.083	.125	64	.604	135	.322	.153		-.024	-.114	-.218	-.276	-.513
13	.173	60	-.362	-.151		-.039	-.030	-.050	-.097	-.173	65	.690	0	-.189	-.073		.013	.060	.107	.156	.232
14	.173	90	-.417	-.141		-.035	-.055	-.109	-.214	-.359	66	.690	180	.203	.095		.003	-.033	-.089	-.191	-.198
15	.173	135	-.055	-.013		-.013	-.038	-.068	-.107	-.147	67	.706	15	-.301	-.062		.024	.065	.103	.144	.211
16	.173	J	.213	.106		.051	.023	.012	-.006	-.035	68	.706	30	-.206	-.049		.031	.071	.109	.143	.204
17	.173	C	.311	.169		.075	.042	.021	.006	.003	69	.706	50	-.294	-.050		.036	.073	.106	.136	.192
18	.190	J	.073	.002		-.024	-.040	-.045	-.071	-.114	70	.706	F	-.373	-.047		.045	.081	.109	.127	.183
19	.190	C	.161	.027		-.050	-.085	-.107	-.115	-.122	71	.706	F	.126	.066		.007	-.025	-.094	-.259	-.415
20	.197	C	.102	-.134		-.304	-.360	-.392	-.416	-.409	72	.706	135	.149	.076		.011	-.022	-.084	-.230	-.323
21	.207	C	.015	-.111		-.187	-.222	-.246	-.252	-.250	73	.753	0	-.007	.055		.094	.125	.158	.189	.245
23	.216	C	.061	-.126		-.236	-.259	-.261	-.247	-.234	74	.753	180	.197	.137		.087	.071	.033	-.044	-.041
24	.226	23	-.184	-.109		-.060	-.025	.019	.073	.135	75	.770	15	-.145	.067		.119	.150	.172	.193	.237
25	.226	45	-.215	-.121		-.051	-.031	-.030	-.033	-.049	76	.770	30	-.197	.030		.087	.113	.134	.152	.189
26	.226	68	-.386	-.163		-.065	-.069	-.108	-.177	-.279	77	.770	50	-.153	.025		.071	.091	.111	.122	.157
27	.226	90	-.425	-.160		-.069	-.088	-.152	-.254	-.398	78	.770	F	-.149	.035		.072	.089	.103	.094	.109
28	.226	135	-.056	-.098		-.154	-.194	-.230	-.271	-.324	79	.770	F	-.825	-.823		.100	.095	.079	-.028	-.086
29	.226	C	-.060	-.137		-.241	-.278	-.305	-.324	-.325	80	.770	F	.005	.060		.058	.042	.002	-.118	-.238
30	.263	C	.122	-.006		-.070	-.078	-.078	-.068	-.062	81	.770	135	.075	.072		.060	.039	.004	-.115	-.223
31	.283	0	-.072	-.090		-.070	-.037	.014	.086	.176	82	.820	15	-.091	.011		.040	.063	.087	.125	.174
32	.299	30	-.219	-.111		-.063	-.033	-.006	.032	.077	83	.820	38	-.186	.003		.038	.063	.093	.129	.175
33	.299	60	-.285	-.188		-.064	-.019	.009	.027	.033	84	.820	F	-.109	.009		.034	.063	.097	.149	.206
34	.299	F	-.669	-.297		-.071	-.017	-.013	-.051	-.122	85	.820	F	-.121	.000		.027	.059	.097	.146	.197
35	.299	F	-.659	-.187		-.026	-.066	-.185	-.382	-.659	86	.820	F	-.114	.017		.042	.080	.119	.168	.209
36	.299	F	-.163	-.021		-.074	-.178	-.335	-.540	-.772	87	.820	F	-.111	.031		.054	.103	.153	.242	.288
37	.299	135	.037	.013		-.058	-.105	-.158	-.202	-.252	88	.820	F	.043	.024		.021	-.027	-.091	-.247	-.297
38	.319	C	.183	.055		-.010	-.028	-.042	-.052	-.056	89	.820	F	-.001	.026		.020	-.011	-.060	-.151	-.216
39	.350	20	-.273	-.060		-.022	.008	.046	.100	.167	90	.820	F	.011	.022		.023	-.006	-.045	-.125	-.214
40	.350	40	-.123	-.083		-.024	.008	.032	.063	.093	91	.820	F	.035	.022		.026	.003	-.033	-.117	-.210
41	.350	60	-.110	-.118		-.036	.008	.049	.098	.152	92	.820	142				.029	.009	-.027	-.115	-.302
42	.350	F	-.484	-.201		-.041	.003	.013	.005	-.022	93	.820	165	.085	.040						
43	.350	F	-.857	-.229		-.021	-.081	-.239	-.501	-.862	94	.897	30	-.229	-.107		-.083	-.062	-.029	.025	.080
44	.350	F	-.019	.019		-.038	-.108	-.203	-.324	-.523	95	.897	50	-.217	-.108		-.089	-.066	-.027	.034	.094
45	.350	135	.098	.050		-.012	-.044	-.078	-.093	-.103	96	.897	F	-.243	-.116		-.102	-.072	-.030	.039	.105
46	.367	0	-.045	-.042		-.024	.007	.057	.127	.215	97	.897	F	-.847	-.849		-.085	-.110	-.143	-.217	-.316
47	.367	180	.245	.092		.013	.006	.003	.015	.019	98	.897	130	-.017	-.078		-.076	-.098	-.127	-.202	-.340
48	.486	0	-.175	-.077		-.006	.044	.110	.194	.291	99	.897	150	-.023	-.082		-.076	-.095	-.143	-.237	-.256
49	.486	180	.287	.113		-.005	-.045	-.079	-.107	-.179	102	.984	0	-.337	-.256		-.216	-.210	-.220	-.209	-.176
50	.503	15	-.207	-.113		-.003	.053	.121	.200	.292	103	.984	30	-.287	-.208		-.169	-.167	-.177	-.166	-.144
51	.503	30	-.198	-.112		-.001	.057	.116	.183	.258	104	.984	60	-.190	-.171		-.161	-.165	-.176	-.186	-.195
52	.503	50	-.278	-.114		-.002	.056	.116	.181	.255	105	.984	90	-.196	-.169		-.161	-.163	-.176	-.201	-.234
53	.503	F	-.708	-.257		.011	.060	.098	.135	.175	106	.984	135	-.112	-.117		-.131	-.135	-.140	-.154	-.206
											107	.984	180	-.232	-.275		-.263	-.281	-.304	-.301	-.372

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(a) M = 0.60 - Continued

Pressure coefficients C_p on -

Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage								Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage - Concluded							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open											$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open							
1	.026	0			.128	.170	.256	.353	.456	.565	55	.503	F			.039	.009	-.064	-.236	-.842	-.755
2	.026	90			.179	.191	.168	.087	-.043	-.229	56	.503	135			.034	.000	-.052	-.111	-.161	-.253
3	.026	180			.229	.181	.115	.052	-.006	-.047	57	.588	0			-.066	-.020	.059	.144	.231	.328
4	.084	0			.025	.046	.120	.226	.324	.429	58	.588	180			.037	-.010	-.082	-.171	-.254	-.387
5	.084	45			.015	.052	.096	.113	.140	.128	59	.604	15			-.068	-.022	.058	.141	.222	.315
6	.084	90			.045	.062	.041	-.031	-.148	-.310	60	.604	30			-.071	-.019	.067	.154	.232	.324
7	.084	135			.076	.055	.004	-.073	-.162	-.270	61	.604	50			-.085	-.027	.069	.162	.248	.343
8	.084	180			.110	.066	.017	-.033	-.067	-.088	62	.604	F			-.117	-.043	.074	.183	.278	.380
9	.134	J			.138	.105	.060	.025	.000	-.015	63	.604	F			.037	-.035	-.148	-.250	-.272	-1.168
10	.156	J			.153	.130	.093	.062	.039	.012	64	.604	135			.034	-.020	-.106	-.215	-.270	-.504
12	.173	30			-.074	-.043	.003	.047	.090	.136	65	.690	0			-.014	.011	.058	.107	.156	.231
13	.173	60			-.070	-.041	-.025	-.049	-.091	-.164	66	.690	180			.031	.009	-.024	-.087	-.191	-.198
14	.173	90			-.056	-.037	-.047	-.107	-.208	-.352	67	.706	15			.003	.024	.066	.107	.146	.213
15	.173	135			-.006	-.010	-.031	-.069	-.106	-.148	68	.706	30			.010	.034	.075	.113	.146	.205
16	.173	J			.067	.053	.030	.014	-.003	-.035	69	.706	50			.020	.041	.079	.113	.138	.195
17	.173	C			.103	.079	.053	.020	.008	.013	70	.706	F			.028	.049	.087	.116	.131	.184
18	.190	J			-.019	-.023	-.034	-.043	-.068	-.113	71	.706	F			.041	.020	-.011	-.083	-.257	-.424
19	.190	C			-.035	-.045	-.080	-.109	-.112	-.118	72	.706	135			.043	.022	-.007	-.073	-.223	-.327
20	.197	C			-.260	-.301	-.351	-.397	-.409	-.408	73	.753	0			.077	.092	.125	.158	.192	.244
21	.207	C			-.161	-.188	-.219	-.244	-.250	-.247	74	.753	180			.104	.093	.078	.041	-.036	-.044
23	.216	C			-.211	-.237	-.254	-.258	-.247	-.233	75	.770	15			.130	.151	.184	.207	.226	.268
24	.226	23			-.082	-.061	-.020	.019	.074	.134	76	.770	30			.098	.116	.142	.164	.176	.213
25	.226	45			-.075	-.051	-.028	-.023	-.028	-.041	77	.770	50			.081	.094	.115	.134	.142	.174
26	.226	68			-.084	-.067	-.062	-.106	-.171	-.276	78	.770	F			.082	.092	.109	.123	.108	.123
27	.226	90			-.080	-.069	-.084	-.148	-.248	-.394	79	.770	F			.118	.118	.117	.094	-.018	-.081
28	.226	135			-.134	-.154	-.187	-.234	-.270	-.324	80	.770	F			.089	.082	.072	.029	-.098	-.229
29	.226	C			-.227	-.244	-.276	-.305	-.320	-.324	81	.770	135			.102	.095	.080	.037	-.088	-.205
30	.263	C			-.059	-.072	-.079	-.080	-.066	-.067	82	.820	15			.087	.100	.124	.147	.177	.218
31	.283	0			-.085	-.072	-.038	.015	.088	.175	83	.820	38			.069	.081	.104	.130	.158	.198
32	.299	30			-.084	-.064	-.034	-.003	.034	.076	84	.820	F			.057	.069	.098	.130	.174	.227
33	.299	60			-.103	-.067	-.018	.012	.027	.032	85	.820	F			.042	.057	.087	.126	.167	.214
34	.299	F			-.134	-.077	-.015	-.012	-.042	-.118	86	.820	F			.050	.067	.104	.140	.186	.220
35	.299	F			-.048	-.025	-.063	-.183	-.375	-.652	87	.820	F			.058	.077	.123	.172	.261	.299
36	.299	F			-.032	-.071	-.172	-.331	-.535	-.770	88	.820	F			.064	.049	.008	-.056	-.225	-.281
37	.299	135			-.034	-.056	-.104	-.157	-.201	-.252	89	.820	F			.065	.054	.025	-.021	-.123	-.194
38	.319	C			.001	-.007	-.022	-.038	-.047	-.059	90	.820	F			.062	.057	.036	-.008	-.095	-.193
39	.350	20			-.038	-.025	.007	.047	.101	.167	91	.820	F			.070	.065	.052	.014	-.080	-.181
40	.350	40			-.045	-.026	.007	.034	.064	.094	92	.820	142			.090	.085	.073	.033	-.061	-.249
41	.350	60			-.061	-.037	.007	.049	.099	.152	94	.897	30			-.074	-.066	-.050	-.023	.026	.070
42	.350	F			-.086	-.044	.002	.015	.008	-.018	95	.897	50			-.077	-.070	-.051	-.018	.041	.092
43	.350	F			-.050	-.022	-.070	-.231	-.492	-.854	96	.897	F			-.091	-.080	-.055	-.016	.050	.106
44	.350	F			-.008	-.036	-.103	-.200	-.319	-.523	97	.897	F			-.056	-.059	-.076	-.118	-.193	-.300
45	.350	135			.008	-.010	-.042	-.080	-.095	-.104	98	.897	130			-.051	-.054	-.061	-.100	-.180	-.341
46	.367	0			-.037	-.027	.005	.055	.126	.213	99	.897	150			-.056	-.051	-.062	-.113	-.225	-.253
47	.367	180			.030	.017	.012	.006	.014	.014	102	.984	0			-.292	-.289	-.292	-.278	-.255	-.229
48	.486	0			-.034	-.009	.041	.109	.192	.288	103	.984	30			-.224	-.221	-.220	-.220	-.201	-.181
49	.486	180			.022	-.002	-.040	-.078	-.101	-.181	104	.984	60			-.168	-.164	-.164	-.178	-.182	-.201
50	.503	15			-.041	-.007	.051	.122	.201	.291	105	.984	90			-.136	-.160	-.160	-.175	-.195	-.233
51	.503	30			-.039	-.004	.054	.117	.184	.257	106	.984	135			-.329	-.138	-.138	-.142	-.167	-.221
52	.503	50			-.042	-.006	.053	.116	.183	.254	107	.984	180			-.010	-.326	-.322	-.341	-.393	-.488
53	.503	F			-.032	.009	.058	.099	.137	.178											
54	.503	F			-.027	.019	-.080	-.340	-.603	-.867											

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(a) M = 0.60 - Continued

Pressure coefficients C_p on -

Model orifice number	x/l	ϕ, deg	Fuselage								Model orifice number	x/l	ϕ, deg	Fuselage - Concluded							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			β ≈ 0°; δ_e = 0°; δ_v = -7.5°; brakes closed											β ≈ 0°; δ_e = 0°; δ_v = -7.5°; brakes closed							
1	.026	0			.132	.171	.258	.355	.456	.565	55	.503	F			.040	.007	-.066	-.245	-.832	-.758
2	.026	90			.175	.184	.159	.083	-.045	-.229	56	.503	135			.033	-.001	-.057	-.108	-.165	-.259
3	.026	180			.233	.179	.114	.050	-.003	-.047	57	.588	0			-.064	-.019	.061	.147	.230	.330
4	.084	0			.026	.047	.120	.228	.324	.429	58	.588	180			.039	-.009	-.084	-.168	-.250	-.378
5	.084	45			.017	.050	.094	.115	.136	.121	59	.604	15			-.066	-.023	.058	.141	.220	.315
6	.084	90			.045	.058	.034	-.033	-.147	-.309	60	.604	30			-.070	-.020	.066	.152	.229	.321
7	.084	135			.076	.053	-.001	-.066	-.157	-.262	61	.604	50			-.086	-.030	.067	.161	.245	.342
8	.084	180			.110	.066	.014	-.029	-.061	-.087	62	.604	F			-.120	-.047	.071	.182	.275	.379
9	.134	J			.143	.107	.058	.026	.002	-.015	63	.604	F			.036	-.036	-.156	-.250	-.279	-1.194
10	.156	J			.148	.124	.085	.061	.038	.009	64	.604	135			.033	-.022	-.111	-.214	-.272	-.489
12	.173	30			-.075	-.053	-.010	.034	.079	.125	65	.690	0			-.010	.012	.059	.109	.157	.231
13	.173	60			-.064	-.043	-.029	-.050	-.094	-.171	66	.690	180			.034	.008	-.028	-.084	-.184	-.197
14	.173	90			-.053	-.038	-.052	-.106	-.207	-.355	67	.706	15			.000	.020	.061	.104	.140	.208
15	.173	135			-.005	-.016	-.033	-.065	-.106	-.144	68	.706	30			.003	.025	.066	.105	.136	.197
16	.173	J			.063	.048	.024	.011	-.005	-.033	69	.706	50			.009	.027	.066	.101	.128	.184
17	.173	C			.102	.071	.040	.020	.006	.001	70	.706	F			.013	.034	.071	.103	.120	.173
18	.190	J			-.021	-.029	-.040	-.045	-.065	-.116	71	.706	F			.023	.000	-.032	-.098	-.248	-.397
19	.190	C			-.036	-.053	-.083	-.107	-.111	-.121	72	.706	135			.031	.006	-.025	-.084	-.220	-.319
20	.197	C			-.254	-.301	-.354	-.389	-.409	-.406	73	.753	0			.081	.095	.128	.163	.192	.246
21	.207	C			-.161	-.188	-.221	-.245	-.248	-.244	74	.753	180			.109	.093	.076	.041	-.035	-.040
23	.216	C			-.208	-.233	-.255	-.255	-.242	-.229	75	.770	15			.061	.080	.113	.140	.158	.202
24	.226	23			-.078	-.062	-.024	.021	.072	.133	76	.770	30			.038	.055	.082	.106	.119	.157
25	.226	45			-.070	-.052	-.028	-.026	-.031	-.046	77	.770	50			.031	.042	.064	.088	.097	.132
26	.226	68			-.081	-.065	-.063	-.106	-.171	-.276	78	.770	F			.040	.049	.066	.083	.076	.091
27	.226	90			-.078	-.067	-.087	-.144	-.246	-.393	79	.770	F			.082	.079	.075	.060	-.028	-.087
28	.226	135			-.130	-.155	-.187	-.223	-.264	-.318	80	.770	F			.038	.034	.018	-.019	-.125	-.241
29	.226	C			-.222	-.242	-.272	-.299	-.314	-.316	81	.770	135			.041	.030	.010	-.025	-.135	-.245
30	.263	C			-.053	-.068	-.079	-.078	-.067	-.061	82	.820	15			-.047	-.033	-.004	.028	.064	.118
31	.283	0			-.083	-.071	-.037	.017	.087	.175	83	.820	38			-.031	-.016	.015	.050	.088	.137
32	.299	30			-.077	-.064	-.034	-.007	.035	.076	84	.820	F			-.027	-.012	.022	.062	.112	.172
33	.299	60			-.098	-.066	-.019	.013	.029	.030	85	.820	F			-.032	-.015	.024	.068	.114	.170
34	.299	F			-.130	-.074	-.017	-.008	-.042	-.121	86	.820	F			-.011	.007	.050	.093	.141	.185
35	.299	F			-.046	-.031	-.065	-.180	-.372	-.645	87	.820	F			.006	.024	.072	.128	.213	.261
36	.299	F			-.031	-.070	-.174	-.324	-.524	-.760	88	.820	F			.012	-.007	-.053	-.115	-.268	-.303
37	.299	135			-.030	-.054	-.099	-.150	-.195	-.252	89	.820	F			.007	-.009	-.041	-.084	-.171	-.232
38	.319	C			.008	-.005	-.025	-.035	-.045	-.054	90	.820	F			-.003	-.017	-.039	-.079	-.151	-.237
39	.350	20			-.035	-.024	.006	.048	.100	.165	91	.820	F			-.012	-.021	-.040	-.078	-.156	-.244
40	.350	40			-.043	-.025	.006	.034	.061	.092	92	.820	142			-.016	-.029	-.047	-.087	-.170	-.348
41	.350	60			-.059	-.036	.006	.050	.097	.151	94	.897	30			-.121	-.111	-.083	-.043	.011	.069
42	.350	F			-.082	-.043	.001	.016	.006	-.020	95	.897	50			-.132	-.120	-.090	-.045	.018	.080
43	.350	F			-.046	-.023	-.071	-.229	-.488	-.852	96	.897	F			-.142	-.127	-.093	-.041	.027	.094
44	.350	F			-.004	-.035	-.102	-.194	-.314	-.514	97	.897	F			-.097	-.108	-.132	-.175	-.237	-.329
45	.350	135			.012	-.009	-.044	-.076	-.089	-.101	98	.897	130			-.092	-.100	-.119	-.160	-.227	-.348
46	.367	0			-.035	-.025	.006	.058	.127	.213	99	.897	150			-.098	-.105	-.123	-.171	-.253	-.281
47	.367	180			.032	.016	.008	.009	.017	.021	102	.984	0			-.252	-.249	-.218	-.192	-.211	-.193
48	.486	0			-.031	-.008	.043	.112	.191	.290	103	.984	30			-.187	-.185	-.171	-.157	-.150	-.118
49	.486	180			.026	-.002	-.041	-.073	-.099	-.178	104	.984	60			-.168	-.166	-.167	-.173	-.182	-.192
50	.503	15			-.036	-.005	.051	.121	.198	.289	105	.984	90			-.164	-.164	-.167	-.177	-.197	-.234
51	.503	30			-.036	-.003	.054	.117	.179	.255	106	.984	135			-.128	-.133	-.130	-.141	-.150	-.215
52	.503	50			-.038	-.005	.053	.116	.178	.252	107	.984	180			-.271	-.276	-.282	-.304	-.345	-.427
53	.503	F			-.032	.009	.058	.098	.131	.172											
54	.503	F			-.024	.016	-.087	-.339	-.606	-.875											

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(a) M = 0.60 - Continued

Pressure coefficients C_p on -

Model orifice number	x/l	ϕ, deg	Fuselage								Model orifice number	x/l	ϕ, deg	Fuselage - Concluded						
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			β ≈ 0°; δ_e = 0°; δ_v = 7.5°; brakes closed											β ≈ 0°; δ_e = 0°; δ_v = 7.5°; brakes closed							
1	.026	0			.134	.172	.259	.353	.457	.568	55	.503	F			.048	.017	-.059	-.228	-.819	-.742
2	.026	90			.178	.194	.161	.088	-.038	-.223	56	.503	135			.044	.007	-.050	-.104	-.158	-.250
3	.026	180			.236	.185	.113	.054	-.003	-.045	57	.588	0			-.052	-.008	.071	.154	.237	.336
4	.084	0			.030	.049	.122	.225	.322	.431	58	.588	180			.050	.002	-.073	-.154	-.239	-.377
5	.084	45			.022	.055	.092	.120	.138	.128	59	.604	15			-.053	-.010	.068	.150	.228	.324
6	.084	90			.050	.062	.038	-.027	-.140	-.304	60	.604	30			-.055	-.007	.077	.162	.238	.330
7	.084	135			.080	.059	-.001	-.065	-.153	-.261	61	.604	50			-.070	-.015	.077	.171	.253	.351
8	.084	180			.115	.070	.015	-.030	-.064	-.088	62	.604	F			-.103	-.032	.083	.191	.283	.387
9	.134	J			.145	.106	.055	.028	.004	-.012	63	.604	F			.048	-.019	-.136	-.239	-.248	-1.143
10	.156	J			.153	.132	.091	.066	.040	.013	64	.604	135			.047	-.009	-.097	-.200	-.258	-.502
12	.173	30			-.062	-.040	-.004	.041	.087	.135	65	.690	0			.011	.033	.077	.127	.170	.247
13	.173	60			-.063	-.041	-.030	-.047	-.091	-.165	66	.690	180			.052	.027	-.011	-.068	-.177	-.188
14	.173	90			-.048	-.034	-.050	-.104	-.202	-.346	67	.706	15			.027	.048	.085	.128	.160	.228
15	.173	135			.000	-.006	-.035	-.064	-.103	-.139	68	.706	30			.031	.053	.091	.132	.159	.219
16	.173	J			.069	.056	.026	.017	.000	-.028	69	.706	50			.039	.057	.094	.132	.151	.207
17	.173	C			.112	.087	.044	.023	.010	.015	70	.706	F			.045	.064	.100	.134	.142	.196
18	.190	J			-.015	-.022	-.041	-.041	-.064	-.108	71	.706	F			.055	.034	-.003	-.067	-.244	-.410
19	.190	C			-.023	-.043	-.086	-.105	-.110	-.116	72	.706	135			.060	.039	.002	-.058	-.209	-.316
20	.197	C			-.255	-.295	-.351	-.388	-.406	-.403	73	.753	0			.112	.124	.156	.190	.217	.269
21	.207	C			-.157	-.183	-.220	-.241	-.247	-.245	74	.753	180			.136	.120	.101	.065	-.019	-.023
23	.216	C			-.204	-.233	-.252	-.252	-.244	-.230	75	.770	15			.138	.156	.186	.212	.224	.265
24	.226	23			-.075	-.058	-.022	.019	.073	.137	76	.770	30			.112	.127	.152	.176	.182	.218
25	.226	45			-.066	-.049	-.030	-.020	-.026	-.037	77	.770	50			.100	.111	.130	.153	.154	.188
26	.226	68			-.078	-.063	-.064	-.103	-.169	-.274	78	.770	F			.102	.111	.125	.142	.125	.138
27	.226	90			-.076	-.064	-.085	-.142	-.242	-.391	79	.770	F			.136	.135	.128	.112	-.005	-.070
28	.226	135			-.126	-.148	-.186	-.224	-.266	-.314	80	.770	F			.102	.095	.079	.044	-.088	-.222
29	.226	C			-.214	-.238	-.275	-.301	-.316	-.317	81	.770	135			.110	.102	.078	.042	-.085	-.207
30	.263	C			-.051	-.066	-.076	-.073	-.064	-.059	82	.820	15			.115	.126	.148	.175	.200	.245
31	.283	0			-.078	-.067	-.035	.018	.088	.179	83	.820	38			.109	.121	.144	.172	.195	.235
32	.299	30			-.076	-.061	-.034	-.003	.035	.079	84	.820	F			.104	.115	.141	.173	.213	.264
33	.299	60			-.094	-.064	-.015	.015	.032	.037	85	.820	F			.090	.104	.134	.171	.207	.253
34	.299	F			-.124	-.074	-.020	-.007	-.037	-.116	86	.820	F			.097	.113	.147	.185	.224	.257
35	.299	F			-.039	-.026	-.060	-.171	-.360	-.643	87	.820	F			.105	.122	.165	.217	.296	.325
36	.299	F			-.027	-.065	-.165	-.311	-.510	-.755	88	.820	F			.094	.078	.026	-.039	-.224	-.291
37	.299	135			-.024	-.051	-.100	-.149	-.195	-.247	89	.820	F			.097	.079	.048	.004	-.108	-.179
38	.319	C			.012	-.001	-.024	-.035	-.044	-.054	90	.820	F			.097	.087	.061	.022	-.073	-.170
39	.350	20			-.031	-.019	.008	.048	.101	.169	91	.820	F			.101	.095	.072	.039	-.059	-.163
40	.350	40			-.038	-.022	.009	.037	.065	.098	92	.820	142			.112	.106	.085	.048	-.053	-.255
41	.350	60			-.054	-.032	.009	.053	.098	.155	94	.897	30			.280	.293	.317	.340	.368	.396
42	.350	F			-.077	-.038	.005	.019	.010	-.015	95	.897	50			.207	.212	.223	.247	.284	.320
43	.350	F			-.041	-.018	-.066	-.210	-.470	-.837	96	.897	F			.123	.130	.147	.177	.216	.260
44	.350	F			.000	-.031	-.101	-.192	-.310	-.510	97	.897	F			.085	.083	.063	.034	-.064	-.181
45	.350	135			.017	-.003	-.044	-.071	-.087	-.096	98	.897	130			.174	.172	.159	.136	.040	-.128
46	.367	0			-.030	-.021	.009	.059	.127	.218	99	.897	150			.291	.281	.272	.241	.132	.106
47	.367	180			.037	.024	.009	.009	.018	.024	102	.984	0			-.412	-.413	-.413	-.399	-.341	-.294
48	.486	0			-.025	-.001	.046	.114	.194	.295	103	.984	30			-.427	-.426	-.422	-.405	-.362	-.329
49	.486	180			.033	.005	-.035	-.068	-.093	-.172	104	.984	60			-.319	-.317	-.320	-.318	-.308	-.361
50	.503	15			-.029	.002	.057	.127	.202	.298	105	.984	90			-.215	-.272	-.262	-.289	-.289	-.181
51	.503	30			-.029	.004	.060	.122	.185	.263	106	.984	135			-.444	-.450	-.444	-.452	-.516	-.560
52	.503	50			-.030	.002	.058	.121	.185	.261	107	.984	180			-.459	-.459	-.476	-.485	-.528	-.612
53	.503	F			-.023	.016	.063	.104	.139	.182											
54	.503	F			-.017	.022	-.070	-.309	-.573	-.849											

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(a) M = 0.60 - Continued

Pressure coefficients C_p on -

Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage								Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage - Concluded							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed											$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed							
1	.026	0	-.069	.007		.154	.249	.355	.454	.571	55	.503	F	.240	.141		-.003	-.110	-.236	-.949	-.858
2	.026	90	-.114	.169		.268	.229	.136	-.008	-.205	56	.503	135	.300	.151		-.018	-.103	-.145	-.175	-.248
3	.026	180	.547	.338		.129	.064	.005	-.028	-.061	57	.588	0	-.354	-.222		-.037	.048	.134	.220	.326
4	.084	0	-.132	-.067		.028	.112	.210	.307	.425	58	.588	180	.301	.131		-.047	-.129	-.225	-.266	-.365
5	.084	45	-.360	-.110		.100	.173	.217	.249	.260	59	.604	15	-.369	-.211		-.037	.054	.146	.229	.339
6	.084	90	-.259	.026		.128	.100	.034	-.113	-.291	60	.604	30	-.369	-.215		-.562	-.281	-.034	.109	.259
7	.084	135	.254	.205		.064	-.017	-.124	-.245	-.374	61	.604	50	-.446	-.252		-.017	.088	.184	.270	.379
8	.084	180	.410	.209		.031	-.030	-.061	-.095	-.125	62	.604	F	-.784	-.342		-.027	.097	.203	.297	.413
9	.134	J	.396	.220		.065	.028	-.003	-.024	-.046	63	.604	F	.388	.190		-.064	-.185	-.327	-.359	-1.068
10	.156	J	.468	.336		.218	.175	.137	.088	.011	64	.604	135	.347	.164		-.048	-.148	-.250	-.286	-.457
12	.173	30	-.257	-.168		-.044	.043	.111	.180	.240	65	.690	0	-.329	-.117		-.015	.038	.091	.143	.227
13	.173	60	-.447	-.176							66	.690	180	.184	.074		-.029	-.068	-.134	-.251	-.306
14	.173	90	-.372	-.096		.002	-.004	-.069	-.182	-.337	67	.706	15	-.344	-.084		.004	.057	.103	.148	.230
15	.173	135	.104	.099		.036	-.008	-.068	-.134	-.181	68	.706	30	-.381	-.073		.030	.079	.121	.159	.237
16	.173	J	.340	.223		.133	.101	.069	.023	-.034	69	.706	50	-.471	-.056		.054	.098	.127	.150	.224
17	.173	C	.434	.292		.156	.115	.083	.067	.072	70	.706	F	-.591	-.066		.071	.109	.127	.137	.204
18	.190	J	.200	.108		.045	.024	-.012	-.066	-.135	71	.706	F	.133	.084		.033	-.012	-.114	-.405	-.578
19	.190	C	.269	.129		-.008	-.047	-.076	-.083	-.066	72	.706	135	.168	.097		.023	-.019	-.094	-.301	-.406
20	.197	C	.062	-.155		-.355	-.396	-.426	-.426	-.404	73	.753	0	-.176	.008		.062	.097	.137	.174	.236
21	.207	C	.114	-.034		-.165	-.213	-.228	-.226	-.216	74	.753	180	.184	.118		.052	.022	-.003	-.114	-.182
23	.216	C	.033	-.136		-.263	-.290	-.276	-.238	-.218	75	.770	15	-.252	.111		.249	.274	.293	.306	.363
24	.226	23	-.215	-.157		-.063	-.005	.068	.145	.227	76	.770	30	-.283	.088		.169	.197	.217	.228	.281
25	.226	45	-.330	-.180		-.060	.012	.052	.071	.081	77	.770	50	-.324	.059		.125	.151	.165	.164	.210
26	.226	68	-.465	-.191		-.030	-.023	-.041	-.094	-.186	78	.770	F	-.353	.056		.113	.133	.138	.100	.133
27	.226	90	-.405	-.140		-.030	-.060	-.124	-.232	-.387	79	.770	F	-.390	.100		.155	.136	.084	-.146	-.199
28	.226	135	.030	-.046		-.150	-.212	-.261	-.307	-.355	80	.770	F	.003	.104		.114	.080	.021	-.216	-.365
29	.226	C	.042	-.132		-.295	-.356	-.392	-.410	-.398	81	.770	135	.138	.146		.133	.095	.035	-.177	-.328
30	.263	C	.092	-.041		-.115	-.128	-.120	-.109	-.119	82	.820	15	-.184	.098						
31	.283	0	-.203	-.114		-.095	-.052	.011	.080	.181	83	.820	38	-.223	.080		.121	.142	.170	.200	.252
32	.299	30	-.227	-.168		-.076	-.023	.041	.104	.174	84	.820	F	-.204	.055		.093	.122	.160	.208	.270
33	.299	60	-.414	-.245		-.061	.000	.054	.090	.111	85	.820	F	-.236	.040		.072	.106	.153	.208	.260
34	.299	F	-.814	-.376		-.072	.005	.034	.015	-.048	86	.820	F	-.251	.051		.076	.118	.170	.230	.272
35	.299	F	-.645	-.176		-.003	-.055	-.176	-.378	-.662	87	.820	F	-.283	.064		.088	.131	.202	.315	.375
36	.299	F	-.078	.021		-.113	-.237	-.416	-.650	-.926	88	.820	F	.100	.072		.088	.025	-.075	-.316	-.522
37	.299	135	.117	.041		-.093	-.172	-.238	-.293	-.302	89	.820	F	.056	.072		.080	.030	-.028	-.179	-.308
38	.319	C	.148	.023		-.040	-.071	-.100	-.137	-.202	90	.820	F	.076	.076		.090	.048	-.002	-.146	-.284
39	.350	20	-.202	-.093		-.049	.011	.076	.144	.235	91	.820	F	.105	.091		.108	.069	.016	-.130	-.272
40	.350	40	-.131	-.137		-.035	.024	.079	.128	.186	92	.820	142				.143	.115	.054	-.105	-.254
41	.350	60	-.249	-.156		-.037	.022	.085	.140	.211	93	.820	165	.190	.155		.170	.136	.084	-.065	-.219
42	.350	F	-.537	-.264		-.039	.026	.060	.063	.053	94	.897	30	-.271	-.073		-.056	-.028	.016	.067	.121
43	.350	F	-.862	-.235		-.011	-.073	-.240	-.508	-.882	95	.897	50	-.271	-.080		-.058	-.032	.014	.075	.134
44	.350	F	.058	.057		-.056	-.162	-.272	-.393	-.593	96	.897	F	-.305	-.097		-.073	-.040	.014	.082	.146
45	.350	135	.180	.086		-.039	-.102	-.140	-.145	-.117	97	.897	F	.057	-.036		-.035	-.070	-.117	-.212	-.340
46	.367	0	-.142	-.078		-.053	-.015	.045	.113	.211	98	.897	130	.042	-.029		-.017	-.044	-.090	-.185	-.314
47	.367	180	.227	.075		-.025	-.057	-.063	-.100	-.165	99	.897	150	.035	-.028		-.023	-.050	-.082	-.164	-.296
48	.486	0	-.170	-.135		-.035	.022	.098	.179	.288	102	.984	0	-.364	-.248		-.271	-.258	-.244	-.226	-.193
49	.486	180	.265	.094		-.036	-.082	-.152	-.176	-.177	103	.984	30	-.300	-.205						
50	.503	15	-.160	-.129		-.387	-.081	.104	.200	.318	104	.984	60	-.218	-.180		-.164	-.172	-.176	-.189	-.209
51	.503	30	-.177	-.148		-.013	.068	.157	.239	.332	105	.984	90	-.239	-.180		-.164	-.176	-.185	-.225	-.264
52	.503	50	-.221	-.150		.000	.079	.161	.236	.322	106	.984	135	-.111	-.114		-.134	-.149	-.159	-.191	-.230
53	.503	F	-.943	-.217		.021	.090	.150	.201	.252	107	.984	180	-.252	-.306		-.319	-.328	-.316	-.372	-.427
54	.503	F	-.826	-.339		.013	-.109	-.372	-.627	-.893											

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(a) M = 0.60 - Concluded

Pressure coefficients C_p on -

Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage								Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage - Concluded							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open											$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open							
1	.026	0			.101	.150	.245	.342	.452	.564	55	.503	F			.058	.010	-.089	-.214	-.908	-.850
2	.026	90			.270	.275	.237	.151	.010	-.189	56	.503	135			.045	-.005	-.085	-.136	-.160	-.228
3	.026	180			.197	.144	.071	.010	-.021	-.059	57	.588	0			-.067	-.029	.054	.134	.226	.327
4	.084	0			-.013	.027	.109	.200	.307	.419	58	.588	180			.017	-.030	-.104	-.204	-.248	-.348
5	.084	45			.069	.096	.169	.217	.253	.259	59	.604	15			-.073	-.029	.061	.146	.236	.339
6	.084	90			.128	.138	.107	.037	-.095	-.276	60	.604	30			-.605	-.540	-.459	-.299	-.164	-.103
7	.084	135			.134	.086	-.007	-.111	-.227	-.365	61	.604	50			-.070	-.012	.093	.183	.277	.379
8	.084	180			.091	.045	-.026	-.058	-.086	-.125	62	.604	F			-.095	-.022	.101	.200	.305	.413
9	.134	J			.111	.077	.033	.004	-.016	-.044	63	.604	F			.045	-.030	-.157	-.304	-.309	-.978
10	.156	J			.259	.231	.182	.141	.100	.013	64	.604	135			.040	-.023	-.121	-.225	-.267	-.421
12	.173	30			-.073	-.032	.042	.108	.174	.241	65	.690	0			-.011	.006	.056	.103	.161	.237
14	.173	90			.011	.011	.003	-.059	-.165	-.324	66	.690	180			.019	-.008	-.041	-.105	-.230	-.294
15	.173	135			.074	.051	-.001	-.060	-.122	-.179	67	.706	15			.009	.030	.077	.122	.167	.242
16	.173	J			.168	.144	.106	.074	.035	-.029	68	.706	30			.030	.052	.099	.138	.177	.248
17	.173	C			.205	.170	.121	.087	.075	.071	69	.706	50			.057	.077	.118	.145	.167	.233
18	.190	J			.069	.056	.028	-.005	-.053	-.131	70	.706	F			.074	.094	.129	.145	.155	.215
19	.190	C			.042	.008	-.041	-.070	-.077	-.071	71	.706	F			.082	.057	.018	-.075	-.380	-.560
20	.197	C			-.293	-.338	-.390	-.419	-.418	-.404	72	.706	135			.075	.048	.010	-.058	-.277	-.393
21	.207	C			-.117	-.154	-.201	-.223	-.220	-.214	73	.753	0			.082	.095	.125	.162	.204	.255
23	.216	C			-.232	-.258	-.281	-.274	-.236	-.216	74	.753	180			.099	.083	.053	.032	-.084	-.163
24	.226	23			-.097	-.066	-.002	.064	.136	.223	75	.770	15			.276	.286	.309	.323	.338	.385
25	.226	45			-.072	-.034	.019	.051	.076	.083	76	.770	30			.197	.210	.233	.251	.260	.304
26	.226	68			-.063	-.031	-.012	-.033	-.082	-.175	77	.770	50			.155	.168	.189	.203	.197	.235
27	.226	90			-.038	-.027	-.050	-.114	-.217	-.373	78	.770	F			.145	.153	.171	.174	.134	.158
28	.226	135			-.106	-.140	-.197	-.252	-.297	-.349	79	.770	F			.186	.184	.176	.124	-.126	-.194
29	.226	C			-.241	-.286	-.343	-.384	-.404	-.395	80	.770	F			.160	.150	.124	.064	-.187	-.345
30	.263	C			-.099	-.109	-.119	-.118	-.106	-.114	81	.770	135			.186	.171	.142	.080	-.141	-.307
31	.283	0			-.100	-.089	-.050	.005	.082	.177	83	.820	38			.198	.205	.220	.240	.267	.306
32	.299	30			-.106	-.076	-.018	.040	.106	.172	84	.820	F			.164	.175	.197	.227	.273	.322
33	.299	60			-.112	-.066	.002	.054	.094	.114	85	.820	F			.140	.152	.179	.215	.269	.309
34	.299	F			-.135	-.067	.013	.036	.024	-.039	86	.820	F			.137	.151	.185	.226	.284	.317
35	.299	F			-.012	.004	-.039	-.159	-.355	-.634	87	.820	F			.146	.156	.195	.254	.366	.408
36	.299	F			-.021	-.079	-.217	-.394	-.627	-.896	88	.820	F			.154	.141	.088	-.018	-.269	-.497
37	.299	135			-.037	-.082	-.156	-.226	-.283	-.296	89	.820	F			.152	.137	.097	.033	-.138	-.280
38	.319	C			-.019	-.029	-.059	-.094	-.126	-.191	90	.820	F			.163	.152	.122	.061	-.099	-.248
39	.350	20			-.059	-.040	.013	.072	.150	.232	91	.820	F			.179	.173	.146	.086	-.081	-.235
40	.350	40			-.065	-.034	.025	.076	.134	.186	92	.820	142			.217	.210	.192	.130	-.053	-.213
41	.350	60			-.068	-.034	.023	.081	.146	.211	93	.820	165			.246	.240	.216	.158	-.012	-.172
42	.350	F			-.091	-.039	.027	.060	.073	.062	94	.897	30			.351	.353	.364	.382	.411	.434
43	.350	F			-.012	.007	-.053	-.216	-.482	-.843	95	.897	50			.259	.261	.269	.285	.324	.356
44	.350	F			.003	-.044	-.144	-.256	-.376	-.571	96	.897	F			.170	.173	.185	.211	.258	.294
45	.350	135			.009	-.029	-.087	-.131	-.139	-.113	97	.897	F			.136	.134	.114	.054	-.093	-.247
46	.367	0			-.054	-.046	-.014	.042	.117	.210	98	.897	130			.234	.237	.224	.177	.019	-.138
47	.367	180			.002	-.018	-.044	-.059	-.090	-.155	99	.897	150			.350	.349	.331	.280	.171	.032
48	.486	0			-.046	-.028	.025	.095	.185	.284	102	.984	0			-.431	-.439	-.430	-.411	-.362	-.328
49	.486	180			.003	-.024	-.067	-.139	-.164	-.167	104	.984	60			-.343	-.346	-.327	-.323	-.325	-.347
50	.503	15			-.614	-.550	-.474	-.319	-.177	-.109	105	.984	90			-.332	-.371	-.367	-.361	-.345	-.352
51	.503	30			-.054	-.011	.072	.154	.242	.335	106	.984	135			-.464	-.468	-.465	-.466	-.527	-.616
52	.503	50			-.038	.006	.082	.158	.242	.325	107	.984	180			-.471	-.479	-.462	-.454	-.523	-.575
53	.503	F			-.027	.024	.094	.151	.210	.257											
54	.503	F			.008	.038	-.080	-.345	-.598	-.861											

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(b) M = 0.90

Pressure coefficients C_p on -

Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage								Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage - Concluded							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx -5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed											$\beta \approx -5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed							
1	.026	0				.203	.295	.398	.510	.625	55	.503	F				.014	-.028	-.164	-.317	-.452
2	.026	90				.178	.130	.054	-.064	-.237	56	.503	135				.001	-.022	-.023	-.074	-.385
3	.026	180				.200	.117	.073	.037	.004	57	.588	0				-.043	.081	.183	.288	.390
4	.084	0				.054	.138	.235	.343	.463	58	.588	180				-.043	-.238	-.363	-.438	-.559
5	.084	45				.029	.052	.029	.027	.016	59	.604	15				-.053	.067	.161	.259	.354
6	.084	90				.033	-.008	-.065	-.175	-.366	60	.604	30				-.044	.084	.178	.273	.359
7	.084	135				.014	-.020	-.058	-.120	-.178	61	.604	50				-.050	.092	.203	.308	.404
8	.084	180				.061	.001	-.042	-.066	-.102	62	.604	F				-.054	.107	.233	.350	.452
9	.134	J				.101	.047	.018	.001	-.045	63	.604	F				-.062	-.336	-.543	-.842	-1.191
10	.156	J				.044	.004	.001	.016	.070	64	.604	135				-.050	-.295	-.485	-.705	-.909
12	.173	30				-.096	-.072	-.041	-.005	.041	65	.690	0				-.008	.046	.086	.164	.263
13	.173	60				-.103	-.113	-.152	-.211	-.290	66	.690	180				-.023	-.048	-.194	-.418	-.680
14	.173	90				-.099	-.111	-.161	-.260	-.378	67	.706	15				.011	.047	.065	.127	.216
15	.173	135				-.081	-.078	-.077	-.104	-.135	68	.706	30				.015	.053	.067	.128	.211
16	.173	J				-.033	-.050	-.039	-.012	.016	69	.706	50				.020	.062	.078	.141	.227
17	.173	C				.005	-.034	-.037	-.032	-.025	70	.706	F				.031	.070	.087	.152	.236
18	.190	J				-.111	-.106	-.081	-.047	-.063	71	.706	F				-.011	-.022	-.200	-.642	-.834
19	.190	C				-.117	-.139	-.135	-.132	-.094	72	.706	135				-.003	-.014	-.158	-.428	-.618
20	.197	C				-.316	-.367	-.386	-.394	-.383	73	.753	0				.142	.171	.161	.180	.253
21	.207	C				-.207	-.215	-.217	-.206	-.135	74	.753	180				.126	.115	.010	-.134	-.292
23	.216	C				-.479	-.525	-.538	-.536	-.532	75	.770	15				-.030	-.016	-.017	.002	.054
24	.226	23				-.135	-.118	-.082		.046	76	.770	30				.001	.010	-.019	-.023	.038
25	.226	45				-.141	-.152	-.159	-.170	-.177	77	.770	50				.021	.041	.003	-.018	.046
26	.226	68				-.174	-.198	-.241	-.307	-.404	78	.770	F				.047	.065	.012	-.042	.006
27	.226	90				-.212	-.227	-.262	-.330	-.415	79	.770	F				.082	.092	.012	-.088	-.118
28	.226	135				-.502	-.486	-.455	-.455	-.511	80	.770	F				.033	.031	-.047	-.192	-.407
29	.226	C				-.571	-.606	-.695	-.704	-.738	81	.770	135				-.001	.013	-.037	-.135	-.209
30	.263	C				-.085	-.075	-.048	-.029	-.040	82	.820	15				-.050	-.019	-.004	.007	.055
31	.283	0				-.121	-.085	-.027	.057	.163	83	.820	38				-.037	-.001	.014	.016	.055
32	.299	30				-.102	-.099	-.090	-.064	-.024	84	.820	F				-.027	.011	.033	.044	.093
33	.299	60				-.080	-.050	-.032	-.015	.011	85	.820	F				-.012	.024	.044	.048	.088
34	.299	F				-.081	-.048	-.060	-.097	-.119	87	.820	F				.045	.069	.084	.090	.135
35	.299	F				-.061	-.113	-.240	-.460	-.693	88	.820	F				-.024	-.041	-.062	-.153	-.353
36	.299	F				-.084	-.176	-.303	-.454	-.601	89	.820	F				-.029	-.041	-.063	-.163	-.309
37	.299	135				-.056	-.082	-.119	-.161	-.183	90	.820	F				-.037	-.057	-.088	-.217	-.376
38	.319	C				-.025	-.052	-.071	-.074	-.128	91	.820	F				-.053	-.069	-.101	-.233	-.387
39	.350	20				-.048	-.038	-.010	.038	.104	92	.820	142				-.222	-.223	-.225	-.229	-.235
40	.350	40				-.036	-.029	-.019	.000	.030	94	.897	30				-.148	-.106	-.045	.011	.067
41	.350	60				-.038	-.008	.031	.080	.142	95	.897	50				-.155	-.110	-.043	.022	.081
42	.350	F				-.040	-.016	-.016	-.027	-.032	96	.897	F				-.155	-.106	-.036	.034	.098
43	.350	F				-.043	-.111	-.282	-.564	-.888	97	.897	F				-.172	-.207	-.222	-.261	-.336
44	.350	F				-.034	-.078	-.147	-.278	-.606	98	.897	130				-.159	-.181	-.189	-.235	-.308
45	.350	135				-.008	-.020	-.049	-.056	-.077	99	.897	150				-.158	-.173	-.179	-.227	-.297
46	.367	0				-.052	-.018	.040	.122	.222	102	.984	0				-.279	-.274	-.268	-.259	-.256
47	.367	180				-.015	-.040	-.039	-.032	-.036	104	.984	60				-.249	-.239	-.240	-.247	-.287
48	.486	0				-.021	.036	.115	.211	.317	105	.984	90				-.246	-.242	-.247	-.263	-.321
49	.486	180				-.020	-.043	-.050	-.040	-.060	106	.984	135				-.229	-.234	-.217	-.245	-.302
50	.503	15				-.010	.041	.110	.192	.284	107	.984	180				-.354	-.363	-.333	-.384	-.485
51	.503	30				-.003	.038	.091	.155	.229											
52	.503	50				.002	.053	.116	.185	.265											
53	.503	F				.019	.054	.098	.146	.212											
54	.503	F				.015	-.061	-.174	-.370	-.404											

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(b) M = 0.90 - Continued

Pressure coefficients C_p on -

Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage								Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage - Concluded							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx -5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open											$\beta \approx -5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open							
1	.026	0	-.002	.065	.161	.211	.302	.402	.513	.633	55	.503	F	.199	.091	.037	.021	-.025	-.169	-.313	-.448
2	.026	90	-.250	.045	.153	.180	.127	.048	-.070	-.248	56	.503	135	.222	.095	.031	.010	-.018	-.019	-.075	-.423
3	.026	180	.643	.411	.251	.198	.114	.070	.034	.001	57	.588	0	-.498	-.358	-.106	-.019	.101	.195	.296	.401
4	.084	0	-.115	-.046	.017	.062	.145	.239	.347	.468	58	.588	180	.385	.182	.039	-.033	-.238	-.339	-.402	-.550
5	.084	45	-.180	-.041	.022	.025	.052	.031	.026	.013	59	.604	15	-.581	-.400	-.110	-.024	.089	.176	.268	.365
6	.084	90	-.384	-.078	.018	.034	-.006	-.069	-.177	-.378	60	.604	30	-.680	-.414	-.108	-.016	.104	.192	.281	.371
7	.084	135	-.003	.014	.025	.016	-.020	-.060	-.117	-.180	61	.604	50	-.856	-.442	-.119	-.021	.114	.216	.318	.416
8	.084	180	.486	.254	.106	.058	.002	-.044	-.068	-.103	62	.604	F	-1.084	-.551	-.150	-.025	.130	.249	.361	.464
9	.134	J	.465	.263	.140	.099	.046	.018	-.001	-.046	63	.604	F	.451	.236	.051	-.050	-.327	-.505	-.788	-1.185
10	.156	J	.303	.139	.067	.044	.005	.001	.019	.073	64	.604	135	.383	.194	.040	-.039	-.289	-.440	-.659	-.901
12	.173	30	-.226	-.146	-.106	-.091	-.069	-.039	-.002	.045	65	.690	0	-.691	-.200	.006	.029	.079	.110	.184	.283
13	.173	60	-.307	-.187	-.112	-.100	-.112	-.152	-.212	-.298	66	.690	180	.235	.061	.033	.008	-.022	-.180	-.381	-.631
14	.173	90	-.540	-.240	-.111	-.095	-.109	-.162	-.258	-.383	67	.706	15	-.607	-.153	.035	.049	.082	.093	.150	.239
15	.173	135	-.194	-.147	-.090	-.078	-.075	-.077	-.104	-.137	68	.706	30	-.579	-.131	.036	.053	.085	.095	.149	.231
16	.173	J			-.022	-.033	-.049	-.037	-.010	.015	69	.706	50	-.633	-.148	.045	.058	.094	.105	.162	.247
17	.173	C	.246	.081	.021	.006	-.032	-.037	-.031	-.023	70	.706	F	-.743	-.168	.052	.067	.101	.113	.172	.255
18	.190	J	-.010	-.109	-.110	-.107	-.101	-.079	-.045	-.064	71	.706	F	.185	.035	.042	.021	-.009	-.200	-.553	-.566
19	.190	C	.089	-.050	-.100	-.115	-.138	-.137	-.131	-.090	72	.706	135	.178	.036	.043	.029	.002	-.171	-.390	-.443
20	.197	C	.091	-.149	-.272	-.314	-.365	-.386	-.391	-.383	73	.753	0	-.295	.015	.166	.184	.210	.198	.216	.288
21	.207	C	-.051	-.173	-.197	-.204	-.214	-.214	-.202	-.132	74	.753	180	.199	.130	.180	.163	.148	.030	-.155	-.463
23	.216	C	-.017	-.292	-.438	-.479	-.525	-.538	-.534	-.533	75	.770	15	.042	-.014	.016	.017	.023	.020	.030	.086
24	.226	23	-.102	-.111	-.133	-.131	-.112	-.076	-.021	.048	76	.770	30	-.028	-.028	.052	.059	.059	.032	.024	.079
25	.226	45	-.195	-.123	-.128	-.134	-.146	-.154	-.169	-.178	77	.770	50	-.126	-.034	.070	.079	.092	.059	.037	.091
26	.226	68	-.218	-.159	-.155	-.168	-.197	-.239	-.307	-.412	78	.770	F	-.303	-.008	.106	.102	.112	.065	.014	.050
27	.226	90	-.376	-.195	-.198	-.206	-.224	-.261	-.329	-.422	79	.770	F	-.356	-.081	.133	.130	.131	.055	-.068	-.125
28	.226	135	-.205	-.432	-.492	-.496	-.481	-.452	-.455	-.516	80	.770	F	-.120	-.055	.084	.081	.069	-.012	-.190	-.446
29	.226	C	-.351	-.518	-.588	-.560	-.608	-.676	-.680	-.731	81	.770	135	-.054	-.071	.050	.049	.049	-.011	-.141	-.208
30	.263	C	.085	-.058	-.084	-.082	-.069	-.044	-.028	-.047	82	.820	15	-.321	-.095	.060	.067	.082	.094	.103	.148
31	.283	0	-.198	-.133	-.127	-.113	-.078	-.020	.062	.171	83	.820	38	-.278	-.064	.062	.083	.105	.117	.118	.153
32	.299	30	-.257	-.096	-.096	-.097	-.095	-.085	-.061	-.021	84	.820	F	-.182	-.028	.074	.091	.118	.135	.148	.194
33	.299	60	-.204	-.155	-.093	-.074	-.045	-.024	.012	.015	85	.820	F	-.226	-.012	.089	.101	.128	.143	.150	.186
34	.299	F	-.427	-.265	-.110	-.073	-.042	-.052	-.094	-.118	86	.820	F	-.235	.042						
35	.299	F	-.670	-.220	-.063	-.055	-.112	-.238	-.459	-.702	87	.820	F	-.184	.074	.126	.143	.165	.181	.195	.238
36	.299	F	-.165	-.055	-.046	-.080	-.171	-.297	-.443	-.607	88	.820	F	-.134	-.067	.067	.059	.031	.003	-.144	-.423
37	.299	135			-.034	-.049	-.073	-.104	-.148	-.179	89	.820	F	-.180	-.071	.073	.060	.035	.005	-.134	-.317
38	.319	C	.180	.026	-.012	-.021	-.049	-.068	-.076	-.133	90	.820	F	-.177	-.069	.066	.057	.024	-.012	-.168	-.353
39	.350	20	-.037	-.022	-.043	-.042	-.033	-.006	.043	.111	91	.820	F	-.162	-.078	.051	.046	.020	-.020	-.172	-.369
40	.350	40	-.104	-.058	-.035	-.029	-.023	-.015	.003	.034	92	.820	142	-.156	-.087	.038	.026	.004	-.029	-.187	-.437
41	.350	60	-.113	-.087	-.043	-.029	.000	.037	.085	.149	93	.820	165	-.114	-.091						
42	.350	F	-.436	-.143	-.056	-.031	-.010	-.012	-.025	-.029	94	.897	30	-.208	-.129	.239	.309	.375	.407	.430	.456
43	.350	F	-.970	-.273	-.049	-.035	-.105	-.273	-.541	-.902	95	.897	50	-.199	-.145	.231	.240	.285	.314	.343	.378
44	.350	F	-.031	-.015	-.011	-.030	-.075	-.144	-.279	-.671	96	.897	F	-.199	-.153	.168	.193	.226	.257	.289	.326
45	.350	135	.056	.015	.008	-.003	-.016	-.045	-.053	-.080	97	.897	F	-.110	-.148	.129	.110	.060	.085	-.006	-.167
46	.367	0	-.096	-.068	-.053	-.044	-.011	.047	.128	.230	98	.897	130	-.111	-.139	.205	.220	.171	.232	.135	-.006
47	.367	180	.257	.077	.008	-.011	-.035	-.033	-.031	-.039	99	.897	150	-.116	-.143	.312	.271	.275	.351	.273	.191
48	.486	0	-.023	-.068	-.025	-.007	.049	.126	.221	.329	102	.984	0	-.413	-.285	-.495	-.499	-.492	-.462	-.444	-.437
49	.486	180	.317	.115	.011	-.013	-.038	-.047	-.035	-.057	103	.984	30	-.347	-.252						
50	.503	15	-.049	-.007	-.019	.003	.054	.119	.199	.292	104	.984	60	-.239	-.219	-.589	-.594	-.604	-.544	-.554	-.587
51	.503	30	-.219	.004	-.012	.010	.049	.100	.162	.237	105	.984	90	-.254	-.234	-.617	-.599	-.621	-.603	-.628	-.654
52	.503	50	-.328	-.012	-.004	.016	.066	.123	.192	.273	106	.984	135	-.248	-.232	-.634	-.604	-.594	-.558	-.626	-.665
53	.503	F	-.359	-.163	.013	.031	.065	.106	.152	.220	107	.984	180	-.333	-.352	-.505	-.519	-.522	-.540	-.585	-.582
54	.503	F	-.295	-.135	.008	.027	-.057	-.166	-.383	-.402											

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(b) M = 0.90 - Continued

Pressure coefficients C_p on -

Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage								Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage - Concluded							
			$\alpha = -20^\circ$	$\alpha = -10^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 15^\circ$	$\alpha = 20^\circ$				$\alpha = -20^\circ$	$\alpha = -10^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 15^\circ$	$\alpha = 20^\circ$
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed											$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed							
1	.026	0	.021	.087		.217	.315	.412	.522		55	.503	F	.257	.138		.010	-.021	-.201	-.393	
2	.026	90	-.131	.129		.232	.201	.131	.018		56	.503	135	.299	.150		.003	-.023	.000	-.007	
3	.026	180	.648	.426		.216	.150	.090	.050		57	.588	0	-.487	-.355		-.029	.103	.203	.307	
4	.084	0	-.072	-.026		.080	.175	.266	.371		58	.588	180	.415	.214		-.031	-.222	-.356	-.433	
5	.084	45	-.203	-.041		.073	.121	.167	.190		59	.604	15	-.654	-.378		-.046	.089	.188	.292	
6	.084	90	-.277	-.029		.078	.052	-.015	-.117		60	.604	30	-.773	-.371		-.043	.100	.203	.306	
7	.084	135	.175	.137		.066	.006	-.065	-.140		61	.604	50	-.907	-.389		-.053	.098	.208	.319	
8	.084	180	.501	.284		.077	.024	-.020	-.047		62	.604	F	-1.052	-.458		-.068	.104	.229	.349	
9	.134	J	.474	.278		.115	.066	.033	.017		63	.604	F	.467	.243		-.076	-.348	-.493	-.788	
10	.156	J	.423	.271		.166	.124	.103	.089		64	.604	135	.418	.214		-.059	-.296	-.397	-.519	
12	.173	30	-.232	-.161		-.058	-.001	.045	.103		65	.690	0	-.499	-.162		.001	.061	.097	.175	
13	.173	60	-.414	-.199		-.058	-.038	-.050	-.079		66	.690	180	.255	.081		-.018	-.028	-.153	-.422	
14	.173	90	-.468	-.189		-.044	-.052	-.104	-.196		67	.706	15	-.429	-.119		.027	.072	.087	.149	
15	.173	135	-.014	-.001		.005	-.009	-.031	-.050		68	.706	30	-.588	-.339		.035	.079	.091	.151	
16	.173	J	.275	.151		.085	.064	.053	.049		69	.706	50	-.598	-.131		.042	.082	.089	.148	
17	.173	C	.373	.221		.126	.093	.077	.082		70	.706	F	-.699	-.131		.052	.091	.091	.149	
18	.190	J	.109	.021		-.010	-.014	-.016	-.029		71	.706	F	.191	.041		.010	.008	-.156	-.504	
19	.190	C	.196	.052		-.027	-.050	-.058	-.045		72	.706	135	.202	.053		.009	.003	-.141	-.413	
20	.197	C	.115	-.122		-.299	-.345	-.367	-.379		73	.753	0	-.253	.044		.132	.161	.148	.160	
21	.207	C	.029	-.094		-.140	-.151	-.153	-.131		74	.753	180	.191	.116		.122	.124	.037	-.102	
23	.216	C	.001	-.269		-.454	-.496	-.526	-.537		75	.770	15	-.054	.091		.174	.207	.189	.179	
24	.226	23	-.199	-.127		-.105	-.058	-.005	.067		76	.770	30	-.315	.032		.139	.165	.137	.113	
25	.226	45	-.193	-.154		-.107	-.075	-.056	-.036		77	.770	50	-.415	.016		.119	.137	.101	.055	
26	.226	68	-.337	-.198		-.144	-.134	-.149	-.188		78	.770	F	-.450	.014		.119	.133	.081	-.009	
27	.226	90	-.410	-.209		-.183	-.176	-.201	-.264		79	.770	F	-.011	-.011		.150	.151	.069	-.190	
28	.226	135	-.068	-.315		-.448	-.427	-.409	-.401		80	.770	F	-.071	.026		.106	.106	.009	-.271	
29	.226	C	-.180	-.437		-.660	-.793	-.792	-.778		81	.770	135	.045	.056		.108	.104	.016	-.182	
30	.263	C	.136	-.003		-.052	-.041	-.027	-.008		82	.820	15	-.252	.035		.076	.098	.096	.091	
31	.283	0	-.075	-.104		-.102	-.061	-.004	.078		83	.820	38	-.355	.032		.078	.103	.102	.098	
32	.299	30	-.231	-.128		-.098	-.060	-.021	.027		84	.820	F	-.226	.043		.076	.104	.110	.121	
33	.299	60	-.238	-.213		-.096	-.039	-.002	.034		85	.820	F	-.336	.037		.070	.101	.113	.120	
34	.299	F	-.697	-.369		-.100	-.038	-.023	-.037		86	.820	F	-.330	.067		.089	.123	.133	.152	
35	.299	F	-.611	-.222		-.056	-.100	-.209	-.389		87	.820	F	-.306	.084		.105	.141	.158	.229	
36	.299	F	-.088	-.028		-.106	-.220	-.372	-.564		88	.820	F	-.061	.007		.061	.030	-.022	-.262	
37	.299	135	.086	.015		-.080	-.122	-.153	-.177		89	.820	F	-.128	.008		.060	.041	-.001	-.194	
38	.319	C	.218	.066		-.013	-.025	-.028	-.022		90	.820	F	-.129	.006		.058	.041	-.006	-.196	
39	.350	20	-.204	-.054		-.036	.000	.045	.110		91	.820	F	-.107	.009		.061	.050	-.004	-.180	
40	.350	40	-.099	-.072		-.038	.000	.034	.077		92	.820	142				.066	.057	.001	-.173	
41	.350	60	-.036	-.107		-.049	.001	.052	.114		93	.820	165	-.011	.031						
42	.350	F	-.646	-.200		-.054	-.004	.017	.030		94	.897	30	-.245	-.121		-.120	-.079	-.019	.046	
43	.350	F	-.910	-.293		-.036	-.095	-.242	-.462		95	.897	50	-.208	-.113		-.128	-.082	-.016	.060	
44	.350	F	.043	.023		-.048	-.115	-.188	-.314		96	.897	F	-.245	-.119		-.140	-.088	-.015	.065	
45	.350	135	.147	.062		-.016	-.041	-.049	-.048		97	.897	F	-.011	-.012		-.115	-.147	-.182	-.238	
46	.367	0	.001	-.017		-.038	.000	.057	.137		98	.897	130	-.040	-.099		-.101	-.125	-.157	-.225	
47	.367	180	.280	.102		.004	.007	.025	.047		99	.897	150	-.052	-.102		-.099	-.125	-.170	-.255	
48	.486	0	-.026	.016		-.005	.056	.135	.230		102	.984	0	-.380	-.279		-.237	-.234	-.230	-.226	
49	.486	180	.343	.146		-.006	-.017	.007	.017		103	.984	30	-.341	-.256		-.219	-.213	-.210	-.209	
50	.503	15	-.077	-.016		.002	.075	.155	.247		104	.984	60	-.254	-.223		-.213	-.214	-.224	-.239	
51	.503	30	-.063	-.006		.006	.077	.150	.230		105	.984	90	-.264	-.229		-.221	-.226	-.238	-.265	
52	.503	50	-.158	.014		.005	.077	.151	.232		106	.984	135	-.201	-.177		-.208	-.212	-.221	-.273	
53	.503	F	-.344	-.208		.017	.080	.139	.199		107	.984	180	-.299	-.285		-.278	-.283	-.319	-.360	
54	.503	F	-.436	-.186		.016	-.051	-.175	-.300												

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(b) M = 0.90 - Continued

Pressure coefficients C_p on -

Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage								Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage - Concluded						
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open											$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open							
1	.026	0			.180	.219	.314	.414	.522	.637	55	.503	F			.047	.013	-.018	-.198	-.392	-.291
2	.026	90			.227	.236	.206	.134	.019	-.143	56	.503	135			.042	.007	-.021	.004	-.002	-.194
3	.026	180			.274	.219	.152	.092	.051	.021	57	.588	0			-.125	-.028	.100	.203	.306	.411
4	.084	0			.047	.083	.174	.268	.371	.487	58	.588	180			.050	-.025	-.220	-.353	-.432	-.448
5	.084	45			.054	.078	.124	.164	.194	.205	59	.604	15			-.144	-.043	.088	.190	.293	.397
6	.084	90			.072	.081	.056	-.011	-.120	-.248	60	.604	30			-.148	-.040	.099	.204	.307	.409
7	.084	135			.099	.071	.007	-.063	-.147	-.225	61	.604	50			-.169	-.050	.098	.211	.320	.428
8	.084	180			.127	.081	.024	-.019	-.048	-.068	62	.604	F			-.205	-.066	.106	.231	.350	.464
9	.134	J			.157	.118	.063	.035	.017	.009	63	.604	F			.034	-.071	-.344	-.487	-.802	-.932
10	.156	J			.198	.173	.130	.106	.089	.073	64	.604	135			.036	-.053	-.291	-.387	-.520	-1.014
12	.173	30			-.087	-.056	.000	.053	.109	.175	65	.690	0			-.012	.006	.062	.100	.176	.277
13	.173	60			-.085	-.055	-.032	-.044	-.076	-.127	66	.690	180			.018	-.008	-.023	-.156	-.421	-.583
14	.173	90			-.061	-.041	-.050	-.102	-.194	-.335	67	.706	15			.022	.035	.076	.092	.151	.248
15	.173	135			.016	.011	-.006	-.027	-.051	-.081	68	.706	30			.030	.044	.084	.096	.153	.248
16	.173	J			.104	.094	.068	.057	.050	.029	69	.706	50			.043	.053	.089	.094	.150	.243
17	.173	C			.157	.132	.099	.083	.083	.107	70	.706	F			.053	.063	.098	.097	.152	.244
18	.190	J			.000	-.001	-.010	-.013	-.028	-.080	71	.706	F			.041	.025	.020	-.148	-.489	-.833
19	.190	C			.002	-.020	-.046	-.053	-.044	-.017	72	.706	135			.041	.023	.014	-.131	-.403	-.921
20	.197	C			-.256	-.297	-.347	-.374	-.382	-.372	73	.753	0			.130	.140	.168	.156	.168	.248
21	.207	C			-.121	-.131	-.146	-.147	-.128	-.096	74	.753	180			.146	.135	.135	.054	-.082	-.044
23	.216	C			-.416	-.456	-.505	-.526	-.540	-.534	75	.770	15			.193	.211	.241	.222	.212	.275
24	.226	23			-.121	-.104	-.059	-.003	.069	.153	76	.770	30			.161	.175	.195	.169	.144	.205
25	.226	45			-.120	-.104	-.071	-.051	-.034	-.018	77	.770	50			.144	.150	.164	.129	.082	.143
26	.226	68			-.154	-.143	-.133	-.148	-.187	-.253	78	.770	F			.144	.147	.157	.105	.013	.059
27	.226	90			-.192	-.179	-.174	-.200	-.263	-.352	79	.770	F			.169	.177	.174	.084	-.194	-.173
28	.226	135			-.456	-.445	-.423	-.407	-.397	-.427	80	.770	F			.142	.140	.134	.034	-.268	-.511
29	.226	C			-.559	-.666	-.802	-.808	-.788	-.789	81	.770	135			.154	.148	.141	.049	-.159	-.386
30	.263	C			-.045	-.045	-.037	-.024	-.007	.004	82	.820	15			.146	.155	.172	.165	.153	.198
31	.283	0			-.110	-.098	-.061	-.003	.076	.182	83	.820	38			.128	.136	.154	.149	.135	.173
32	.299	30			-.109	-.094	-.058	-.020	.028	.098	84	.820	F			.119	.128	.149	.153	.156	.201
33	.299	60			-.131	-.094	-.039	-.002	.034	.079	85	.820	F			.107	.116	.141	.148	.149	.183
34	.299	F			-.152	-.099	-.037	-.023	-.038	-.043	86	.820	F			.118	.129	.156	.165	.176	.197
35	.299	F			-.067	-.053	-.099	-.210	-.388	-.597	87	.820	F			.128	.139	.172	.191	.262	.256
36	.299	F			-.058	-.102	-.220	-.379	-.564	-.908	88	.820	F			.112	.102	.068	.007	-.283	-.327
37	.299	135			-.049	-.077	-.123	-.154	-.180	-.246	89	.820	F			.109	.104	.082	.033	-.182	-.268
38	.319	C			.003	-.010	-.022	-.024	-.022	-.011	90	.820	F			.113	.108	.090	.037	-.175	-.356
39	.350	20			-.044	-.033	.000	.047	.111	.195	91	.820	F			.120	.118	.108	.048	-.147	-.345
40	.350	40			-.052	-.035	.000	.036	.078	.133	92	.820	142			.140	.136	.127	.071	-.120	-.351
41	.350	60			-.068	-.046	.001	.052	.114	.189	94	.897	30			-.095	-.086	-.060	-.012	.041	.087
42	.350	F			-.092	-.052	-.003	.019	.030	.043	95	.897	50			-.100	-.091	-.060	-.002	.061	.113
43	.350	F			-.053	-.031	-.092	-.243	-.457	-.769	96	.897	F			-.113	-.100	-.065	.002	.072	.127
44	.350	F			-.016	-.043	-.114	-.189	-.316	-.497	97	.897	F			-.071	-.076	-.101	-.142	-.217	-.357
45	.350	135			.008	-.012	-.041	-.047	-.048	-.057	98	.897	130			-.057	-.061	-.079	-.117	-.209	-.325
46	.367	0			-.043	-.034	.000	.057	.136	.238	99	.897	150			-.061	-.062	-.081	-.133	-.242	-.308
47	.367	180			.020	.009	.008	.025	.047	.044	102	.984	0			-.304	-.315	-.320	-.294	-.278	-.273
48	.486	0			-.019	-.003	.056	.136	.230	.338	103	.984	30			-.263	-.272	-.278	-.257	-.244	-.248
49	.486	180			.025	.000	-.017	.008	.015	-.014	104	.984	60			-.230	-.226	-.235	-.241	-.251	-.302
50	.503	15			-.021	.006	.075	.157	.247	.349	105	.984	90			-.227	-.228	-.239	-.249	-.276	-.336
51	.503	30			-.019	.008	.077	.151	.231	.321	106	.984	135			-.225	-.227	-.232	-.235	-.286	-.318
52	.503	50			-.015	.007	.077	.153	.232	.321	107	.984	180			-.363	-.364	-.356	-.380	-.423	-.519
53	.503	F			-.003	.020	.080	.142	.201	.272											
54	.503	F			-.001	.021	-.051	-.175	-.299	-.497											

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(b) M = 0.90 - Continued

Pressure coefficients C_p on -

Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage								Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage - Concluded							
			$\alpha = -20^\circ$	$\alpha = -10^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 15^\circ$	$\alpha = 20^\circ$				$\alpha = -20^\circ$	$\alpha = -10^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 15^\circ$	$\alpha = 20^\circ$
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = -7.5^\circ$; brakes closed											$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = -7.5^\circ$; brakes closed							
1	.026	0			.180	.219	.315	.416	.521	.635	55	.503	F			.043	.014	-.021	-.193	-.392	-.291
2	.026	90			.222	.232	.203	.135	.016	-.148	56	.503	135			.040	.005	-.021	.006	-.006	-.208
3	.026	180			.274	.222	.151	.098	.052	.022	57	.588	0			-.125	-.030	.101	.207	.307	.410
4	.084	0			.047	.084	.175	.270	.370	.484	58	.588	180			.050	-.024	-.218	-.342	-.426	-.451
5	.084	45			.055	.072	.119	.165	.183	.194	59	.604	15			-.145	-.045	.087	.193	.291	.396
6	.084	90			.065	.078	.051	-.012	-.119	-.255	60	.604	30			-.149	-.042	.098	.206	.305	.407
7	.084	135			.094	.069	.007	-.058	-.140	-.221	61	.604	50			-.170	-.054	.096	.214	.318	.426
8	.084	180			.127	.082	.025	-.016	-.047	-.068	62	.604	F			-.207	-.070	.103	.234	.348	.462
9	.134	J			.157	.119	.066	.038	.017	.009	63	.604	F			.033	-.069	-.342	-.517	-.749	-1.015
10	.156	J			.189	.166	.123	.103	.087	.071	64	.604	135			.035	-.052	-.290	-.405	-.521	-1.041
12	.173	30			-.098	-.067	-.010	.044	.093	.159	65	.690	0			-.012	.005	.061	.103	.175	.277
13	.173	60			-.087	-.059	-.038	-.048	-.085	-.140	66	.690	180			.015	-.011	-.027	-.151	-.421	-.580
14	.173	90			-.067	-.043	-.053	-.102	-.198	-.342	67	.706	15			.019	.030	.071	.092	.149	.245
15	.173	135			.007	.007	-.010	-.027	-.051	-.084	68	.706	30			.022	.035	.075	.094	.150	.242
16	.173	J			.098	.084	.060	.055	.047	.027	69	.706	50			.032	.041	.077	.091	.145	.237
17	.173	C			.138	.114	.090	.079	.076	.094	70	.706	F			.038	.049	.084	.092	.148	.238
18	.190	J			-.005	-.008	-.015	-.014	-.032	-.081	71	.706	F			.023	.008	.001	-.145	-.515	-.915
19	.190	C			-.014	-.026	-.052	-.057	-.049	-.024	72	.706	135			.029	.009	-.001	-.132	-.429	-.897
20	.197	C			-.255	-.296	-.347	-.371	-.381	-.372	73	.753	0			.132	.141	.168	.160	.169	.248
21	.207	C			-.121	-.132	-.151	-.147	-.133	-.096	74	.753	180			.143	.134	.132	.054	-.089	-.036
23	.216	C			-.413	-.453	-.505	-.522	-.539	-.533	75	.770	15			.132	.148	.179	.169	.158	.215
24	.226	23			-.120	-.106	-.063	-.001	.063	.145	76	.770	30			.104	.117	.138	.116	.090	.145
25	.226	45			-.120	-.107	-.079	-.055	-.042	-.027	77	.770	50			.090	.095	.109	.078	.030	.086
26	.226	68			-.157	-.147	-.138	-.153	-.193	-.261	78	.770	F			.096	.099	.107	.061	-.030	.003
27	.226	90			-.193	-.185	-.180	-.200	-.268	-.359	79	.770	F			.125	.130	.129	.058	-.172	-.189
28	.226	135			-.459	-.449	-.426	-.405	-.402	-.433	80	.770	F			.085	.085	.082	-.006	-.254	-.651
29	.226	C			-.556	-.656	-.800	-.803	-.789	-.792	81	.770	135			.090	.082	.077	.000	-.180	-.309
30	.263	C			-.041	-.043	-.035	-.020	-.007	.004	82	.820	15			-.034	-.021	.000	.003	-.008	.049
31	.283	0			-.111	-.100	-.061	.000	.075	.182	83	.820	38			-.010	.004	.029	.036	.027	.077
32	.299	30			-.108	-.094	-.061	-.019	.025	.093	84	.820	F			.002	.015	.041	.054	.059	.114
33	.299	60			-.128	-.095	-.041	.002	.030	.074	85	.820	F			.003	.016	.046	.063	.066	.109
34	.299	F			-.153	-.099	-.040	-.022	-.043	-.050	86	.820	F			.030	.043	.075	.091	.103	.133
35	.299	F			-.069	-.054	-.103	-.206	-.391	-.603	87	.820	F			.052	.062	.094	.112	.157	.169
36	.299	F			-.056	-.099	-.219	-.365	-.561	-.877	88	.820	F			.032	.021	-.013	-.044	-.246	-.256
37	.299	135			-.049	-.076	-.120	-.146	-.177	-.244	89	.820	F			.022	.014	-.003	-.033	-.208	-.230
38	.319	C			.002	-.009	-.023	-.020	-.022	-.012	90	.820	F			.013	.005	-.013	-.054	-.228	-.368
39	.350	20			-.043	-.034	-.001	.049	.107	.190	91	.820	F			.002	-.005	-.019	-.065	-.241	-.369
40	.350	40			-.051	-.035	-.001	.037	.073	.127	92	.820	142			-.014	-.018	-.033	-.088	-.279	-.464
41	.350	60			-.066	-.046	.001	.055	.112	.186	94	.897	30			-.173	-.156	-.111	-.041	.022	.076
42	.350	F			-.090	-.052	-.004	.021	.027	.038	95	.897	50			-.183	-.166	-.118	-.042	.030	.090
43	.350	F			-.056	-.034	-.093	-.239	-.463	-.776	96	.897	F			-.196	-.176	-.122	-.038	.040	.103
44	.350	F			-.014	-.043	-.113	-.180	-.311	-.491	97	.897	F			-.142	-.158	-.194	-.218	-.268	-.398
45	.350	135			.007	-.011	-.040	-.044	-.048	-.057	98	.897	130			-.128	-.143	-.175	-.199	-.259	-.352
46	.367	0			-.042	-.035	.000	.062	.136	.237	99	.897	150			-.129	-.141	-.175	-.207	-.278	-.326
47	.367	180			.021	.009	.008	.030	.048	.045	102	.984	0			-.300	-.306	-.294	-.256	-.283	-.282
48	.486	0			-.019	-.003	.056	.140	.229	.337	103	.984	30			-.251	-.251	-.244	-.221	-.222	-.230
49	.486	180			.025	-.001	-.016	.012	.016	-.013	104	.984	60			-.219	-.218	-.224	-.228	-.247	-.287
50	.503	15			-.020	.005	.074	.159	.244	.346	105	.984	90			-.220	-.222	-.228	-.233	-.262	-.324
51	.503	30			-.018	.008	.076	.153	.227	.315	106	.984	135			-.203	-.207	-.205	-.207	-.230	-.322
52	.503	50			-.014	.007	.076	.155	.228	.318	107	.984	180			-.336	-.344	-.345	-.359	-.388	-.477
53	.503	F			-.003	.019	.079	.143	.196	.267											
54	.503	F			-.004	.020	-.051	-.170	-.302	-.491											

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(b) M = 0.90 - Continued

Pressure coefficients C_p on -

Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage								Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage - Concluded							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 7.5°$; brakes closed											$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 7.5°$; brakes closed							
1	.026	0			.185	.226	.319	.417	.525	.639	55	.503	F			.056	.024	-.022	-.197	-.376	-.288
2	.026	90			.227	.240	.200	.133	.020	-.146	56	.503	135			.051	.017	-.015	.007	.004	-.192
3	.026	180			.276	.224	.147	.092	.055	.023	57	.588	0			-.104	-.007	.116	.214	.316	.416
4	.084	0			.051	.089	.180	.270	.376	.487	58	.588	180			.063	-.011	-.229	-.334	-.401	-.436
5	.084	45			.061	.082	.123	.165	.192	.201	59	.604	15			-.116	-.017	.108	.202	.303	.404
6	.084	90			.071	.085	.046	-.014	-.117	-.251	60	.604	30			-.121	-.015	.117	.215	.316	.415
7	.084	135			.099	.072	-.003	-.063	-.141	-.225	61	.604	50			-.144	-.026	.116	.222	.330	.434
8	.084	180			.132	.085	.019	-.020	-.044	-.067	62	.604	F			-.182	-.041	.125	.243	.360	.469
9	.134	J			.161	.122	.064	.038	.022	.010	63	.604	F			.048	-.067	-.365	-.466	-.755	-.949
10	.156	J			.197	.175	.124	.106	.092	.072	64	.604	135			.051	-.039	-.303	-.362	-.509	-1.015
12	.173	30			-.083	-.045	.008	.053	.116	.170	65	.690	0			.021	.041	.091	.123	.194	.291
13	.173	60			-.081	-.050	-.036	-.044	-.075	-.132	66	.690	180			.047	.023	-.008	-.135	-.362	-.497
14	.173	90			-.059	-.037	-.059	-.102	-.194	-.338	67	.706	15			.054	.069	.104	.117	.171	.263
15	.173	135			.015	.016	-.011	-.026	-.046	-.081	68	.706	30			.059	.075	.111	.120	.172	.262
16	.173	J			.105	.093	.062	.057	.053	.027	69	.706	50			.070	.082	.114	.118	.168	.256
17	.173	C			.162	.139	.095	.083	.087	.104	70	.706	F			.076	.091	.121	.119	.169	.256
18	.190	J			.001	.001	-.013	-.013	-.025	-.079	71	.706	F			.063	.050	.027	-.140	-.451	-.775
19	.190	C			.004	-.016	-.050	-.056	-.041	-.015	72	.706	135			.066	.050	.026	-.128	-.379	-.835
20	.197	C			-.252	-.294	-.348	-.373	-.376	-.372	73	.753	0			.169	.181	.202	.191	.199	.275
21	.207	C			-.118	-.128	-.149	-.146	-.124	-.094	74	.753	180			.177	.167	.153	.066	-.109	-.175
23	.216	C			-.408	-.450	-.505	-.523	-.534	-.529	75	.770	15			.206	.224	.249	.233	.221	.281
24	.226	23			-.114	-.097	-.056	.001	.074	.154	76	.770	30			.180	.194	.208	.184	.160	.217
25	.226	45			-.111	-.090	-.068	-.049	-.027	-.021	77	.770	50			.167	.173	.183	.150	.105	.164
26	.226	68			-.147	-.136	-.133	-.144	-.184	-.253	78	.770	F			.169	.174	.179	.129	.040	.092
27	.226	90			-.183	-.170	-.178	-.200	-.259	-.353	79	.770	F			.192	.201	.188	.103	-.182	-.118
28	.226	135			-.452	-.439	-.421	-.404	-.393	-.427	80	.770	F			.160	.159	.142	.041	-.262	-.468
29	.226	C			-.545	-.654	-.798	-.790	-.774	-.778	81	.770	135			.166	.161	.141	.048	-.179	-.387
30	.263	C			-.039	-.039	-.037	-.022	-.003	.006	82	.820	15			.180	.190	.203	.203	.201	.244
31	.283	0			-.103	-.089	-.056	.003	.084	.185	83	.820	38			.176	.187	.201	.202	.198	.236
32	.299	30			-.101	-.084	-.053	-.016	.036	.100	84	.820	F			.174	.184	.201	.210	.221	.265
33	.299	60			-.122	-.084	-.034	.004	.040	.083	85	.820	F			.164	.175	.197	.209	.219	.252
34	.299	F			-.144	-.083	-.033	-.020	-.030	-.043	86	.820	F			.174	.187	.213	.226	.246	.265
35	.299	F			-.060	-.046	-.110	-.208	-.395	-.596	87	.820	F			.185	.196	.228	.253	.334	.336
36	.299	F			-.052	-.103	-.250	-.376	-.572	-.908	88	.820	F			.158	.148	.097	.025	-.325	-.370
37	.299	135			-.043	-.069	-.122	-.148	-.169	-.241	89	.820	F			.154	.149	.115	.054	-.165	-.269
38	.319	C			.010	-.004	-.023	-.022	-.014	-.011	90	.820	F			.157	.154	.120	.060	-.158	-.340
39	.350	20			-.037	-.023	.007	.051	.117	.196	91	.820	F			.158	.159	.134	.066	-.137	-.333
40	.350	40			-.044	-.026	.004	.040	.083	.134	92	.820	142			.167	.165	.142	.073	-.133	-.341
41	.350	60			-.060	-.037	.006	.057	.120	.190	94	.897	30			.377	.394	.426	.456	.479	.500
42	.350	F			-.083	-.043	.001	.024	.035	.044	95	.897	50			.310	.320	.335	.361	.396	.424
43	.350	F			-.045	-.025	-.118	-.246	-.478	-.772	96	.897	F			.232	.243	.261	.295	.329	.360
44	.350	F			-.007	-.036	-.116	-.181	-.307	-.491	97	.897	F			.182	.180	.147	.093	-.021	-.232
45	.350	135			.013	-.005	-.038	-.042	-.038	-.052	98	.897	130			.275	.270	.251	.203	.094	-.086
46	.367	0			-.035	-.025	.005	.064	.144	.242	99	.897	150			.387	.380	.365	.311	.196	.113
47	.367	180			.029	.018	.012	.030	.055	.049	102	.984	0			-.502	-.492	-.489	-.462	-.446	-.445
48	.486	0			-.009	.011	.066	.144	.239	.343	103	.984	30			-.545	-.541	-.543	-.509	-.448	-.433
49	.486	180			.035	.009	-.011	.014	.026	-.009	104	.984	60			-.582	-.572	-.586	-.570	-.510	-.565
50	.503	15			-.011	.018	.085	.165	.255	.353	105	.984	90			-.596	-.602	-.626	-.625	-.616	-.664
51	.503	30			-.008	.021	.086	.159	.238	.323	106	.984	135			-.624	-.631	-.626	-.601	-.601	-.662
52	.503	50			-.006	.022	.089	.160	.240	.325	107	.984	180			-.484	-.487	-.521	-.528	-.542	-.612
53	.503	F			.006	.032	.088	.149	.207	.274											
54	.503	F			.008	.026	-.071	-.173	-.305	-.493											

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(b) M = 0.90 - Continued

Pressure coefficients C_p on -

Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage								Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage - Concluded							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed											$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed							
1	.026	0	-.005	.067		.210	.315	.421	.537	.658	55	.503	F	.325	.190		-.003	-.027	-.287	-.355	-.320
2	.026	90	-.017	.223		.319	.274	.191	.058	-.118	56	.503	135	.369	.194		-.062	-.035	-.001	.017	-.443
3	.026	180	.630	.409		.181	.104	.068	.033	-.006	57	.588	0	-.494	-.368		-.032	.093	.198	.306	.412
4	.084	0	-.117	-.048		.057	.155	.258	.371	.496	58	.588	180	.391	.194		-.104	-.278	-.382	-.444	-.630
5	.084	45	-.354	-.080		.134	.209	.264	.304	.332	59	.604	15	-.620	-.393		-.048	.088	.201	.315	.427
6	.084	90	-.205	.052		.182	.119	.070	-.077	-.241	60	.604	30	-.740	-.385		.062	.176	.284	.369	.452
7	.084	135	.324	.245		.092	-.012	-.115	-.240	-.369	61	.604	50	-1.004	-.407		-.034	.122	.242	.358	.470
8	.084	180	.475	.258		.058	-.008	-.048	-.076	-.114	62	.604	F	-.942	-.428		-.042	.132	.263	.389	.505
9	.134	J	.461	.267		.089	.039	.016	-.002	-.033	63	.604	F	.484	.251		-.087	-.412	-.541	-.849	-.959
10	.156	J	.540	.392		.266	.210	.165	.109	.053	64	.604	135	.440	.223		-.033	-.354	-.406	-.583	-1.147
12	.173	30	-.273	-.208		-.034	.053	.133	.213	.285	65	.690	0	-.629	-.233		-.007	.049	.094	.182	.284
13	.173	60	-.519	-.217							66	.690	180	.239	.066		.045	-.059	-.255	-.430	-.780
14	.173	90	-.394	-.118		.031	.008	-.055	-.165	-.330	67	.706	15	-.574	-.163		.028	.074	.096	.174	.276
15	.173	135	.155	.131		.084	.035	-.008	-.048	-.079	68	.706	30	-.600	-.163		.049	.095	.111	.189	.285
16	.173	J	.405	.276		.186	.150	.119	.071	.022	69	.706	50	-.673	-.180		.074	.113	.116	.187	.281
17	.173	C	.499	.352		.225	.185	.171	.178	.186	70	.706	F	-.774	-.200		.091	.125	.117	.187	.278
18	.190	J	.241	.139		.087	.065	.029	-.025	-.089	71	.706	F	.208	.055		.033	.036	-.204	-.547	-.841
19	.190	C	.319	.168		.056	.023	.019	.037	.071	72	.706	135	.225	.070		.125	.024	-.180	-.383	-1.009
20	.197	C	.074	-.155		-.355	-.396	-.400	-.392	-.379	73	.753	0	-.277	.004		.140	.164	.153	.186	.263
21	.207	C	.136	.000		-.066	-.084	-.076	-.046	-.040	74	.753	180	.203	.123		.217	.105	-.014	-.132	-.132
23	.216	C	-.008	-.273		-.501	-.541	-.539	-.529	-.533	75	.770	15	-.325	.103		.332	.348	.320	.325	.387
24	.226	23	-.207	-.172		-.100	-.023	.062	.155	.251	76	.770	30	-.463	.078		.245	.263	.226	.223	.288
25	.226	45	-.275	-.210		-.071	-.008	.044	.084	.115	77	.770	50	-.536	.033		.195	.210	.153	.131	.191
26	.226	68	-.431	-.234		-.091	-.061	-.057	-.086	-.147	78	.770	F	-.531	.007		.177	.189	.097	.031	.081
27	.226	90	-.439	-.198		-.111	-.110	-.139	-.212	-.326	79	.770	F	-.507	-.033		.179	.196	-.017	-.292	-.342
28	.226	135	.018	-.149		-.350	-.348	-.340	-.343	-.366	80	.770	F	-.043	.051		.202	.151	-.029	-.385	-.503
29	.226	C	-.008	-.289		-.759	-.810	-.810	-.874	-.815	81	.770	135	.123	.129		.147	.166	.012	-.252	-.679
30	.263	C	.101	-.042		-.104	-.071	-.056	-.039	-.072	82	.820	15	-.281	.126						
31	.283	0	-.197	-.128		-.119	-.073	-.005	.085	.202	83	.820	38	-.389	.096		.188	.197	.194	.196	.244
32	.299	30	-.216	-.179		-.090	-.038	.034	.113	.203	84	.820	F	-.354	.083		.161	.179	.194	.208	.263
33	.299	60	-.389	-.282		-.083	-.015	.045	.100	.167	85	.820	F	-.407	.066		.142	.165	.188	.206	.256
34	.299	F	-1.068	-.442		-.026	-.009	.022	.024	.044	86	.820	F	-.415	.072		.151	.177	.213	.238	.282
35	.299	F	-.535	-.197		-.129	-.088	-.200	-.400	-.528	87	.820	F	-.449	.075		.163	.190	.266	.341	.395
36	.299	F	.006	.016		-.118	-.294	-.508	-.978	-1.223	88	.820	F	.011	.075		.143	.092	-.105	-.507	-.611
37	.299	135	.165	.041		-.034	-.194	-.235	-.223	-.342	89	.820	F	-.031	.058		.151	.099	-.014	-.272	-.360
38	.319	C	.184	.032		-.008	-.063	-.086	-.105	-.151	90	.820	F	-.023	.069		.169	.111	.007	-.254	-.357
39	.350	20	-.186	-.078		-.047	.012	.084	.171	.274	91	.820	F	.011	.087		.204	.136	.030	-.218	-.412
40	.350	40	-.070	-.113		-.041	.023	.086	.154	.232	92	.820	142				.236	.183	.064	-.161	-.538
41	.350	60	-.094	-.151		-.042	.021	.092	.170	.257	93	.820	165	.135	.158		-.045	.200	.108	-.098	-.229
42	.350	F	-.758	-.267		-.046	.025	.066	.097	.125	94	.897	30	-.306	-.094		-.079	-.038	.042	.100	.155
43	.350	F	-.801	-.257		-.064	-.091	-.257	-.442	-.730	95	.897	50	-.297	-.095		-.083	-.043	.045	.112	.172
44	.350	F	.124	.066		-.038	-.170	-.255	-.414	-.839	96	.897	F	-.355	-.106		-.096	-.052	.048	.120	.180
45	.350	135	.229	.101		-.025	-.087	-.088	-.054	-.090	97	.897	F	.058	-.017		-.024	-.088	-.144	-.262	-.467
46	.367	0	-.089	-.063		-.057	-.016	.051	.141	.251	98	.897	130	.045	-.014		-.029	-.057	-.116	-.227	-.440
47	.367	180	.264	.088		-.025	-.046	-.046	-.051	-.074	99	.897	150	.032	-.020		-.299	-.067	-.104	-.205	-.373
48	.486	0	-.023	-.065		-.022	.043	.132	.235	.348	102	.984	0	-.413	-.283		-.042	-.296	-.276	-.272	-.264
49	.486	180	.322	.126		.038	-.045	-.053	-.037	-.120	103	.984	30	-.367	-.258						
50	.503	15	-.002	-.028		.010	.093	.192	.294	.405	104	.984	60	-.318	-.245		-.223	-.228	-.238	-.280	-.328
51	.503	30	-.021	-.032		.004	.105	.202	.301	.404	105	.984	90	-.319	-.245		-.232	-.238	-.259	-.318	-.390
52	.503	50	-.390	-.008		.021	.114	.209	.302	.398	106	.984	135	-.244	-.201		-.371	-.242	-.250	-.303	-.417
53	.503	F	-.352	-.147		.038	.125	.204	.277	.353	107	.984	180	-.335	-.349		-.010	-.373	-.348	-.403	-.538
54	.503	F	-.612	-.178		.012	-.053	-.186	-.301	-.514											

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(b) M = 0.90 - Concluded

Pressure coefficients C_p on -

Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage								Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage - Concluded							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open											$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open							
1	.026	0			.153	.207	.311	.418	.530	.651	55	.503	F			.068	.024	-.018	-.222	-.383	-.307
2	.026	90			.322	.322	.281	.200	.070	-.103	56	.503	135			.055	.009	-.028	.003	.023	-.369
3	.026	180			.245	.188	.112	.072	.036	.000	57	.588	0			-.107	-.021	.101	.204	.307	.414
4	.084	0			.014	.057	.153	.255	.366	.488	58	.588	180			.031	-.039	-.252	-.353	-.412	-.603
5	.084	45			.096	.133	.208	.263	.304	.334	59	.604	15			-.127	-.033	.098	.207	.316	.427
6	.084	90			.158	.185	.126	.077	-.067	-.225	60	.604	30			.147	.208	.275	.326	.364	.368
7	.084	135			.155	.101	-.002	-.104	-.230	-.355	61	.604	50			-.143	-.022	.129	.247	.360	.470
8	.084	180			.115	.065	-.002	-.042	-.073	-.109	62	.604	F			-.177	-.032	.138	.267	.388	.505
9	.134	J			.135	.095	.046	.021	.001	-.030	63	.604	F			.039	-.072	-.382	-.414	-.850	-.881
10	.156	J			.305	.271	.216	.173	.114	.060	64	.604	135			.037	-.057	-.329	-.374	-.520	-1.087
12	.173	30			-.088	-.035	.053	.131	.207	.291	65	.690	0			.006	.025	.077	.115	.193	.293
14	.173	90			.018	.034	.015	-.044	-.155	-.309	66	.690	180			.026	.003	-.027	-.179	-.397	-.712
15	.173	135			.111	.088	.042	-.002	-.045	-.074	67	.706	15			.042	.060	.104	.122	.190	.288
16	.173	J			.215	.191	.156	.125	.077	.029	68	.706	30			.063	.081	.126	.137	.202	.299
17	.173	C			.263	.229	.189	.174	.178	.192	69	.706	50			.093	.108	.144	.141	.201	.291
18	.190	J			.104	.091	.071	.037	-.020	-.080	70	.706	F			.110	.122	.156	.141	.198	.288
19	.190	C			.088	.060	.028	.022	.036	.073	71	.706	F			.095	.079	.066	-.180	-.466	-.727
20	.197	C			-.307	-.348	-.390	-.396	-.392	-.377	72	.706	135			.088	.069	.054	-.158	-.360	-.822
21	.207	C			-.049	-.065	-.080	-.074	-.047	-.031	73	.753	0			.161	.178	.202	.194	.217	.291
23	.216	C			-.451	-.494	-.536	-.537	-.527	-.525	74	.753	180			.180	.164	.144	.023	-.159	-.360
24	.226	23			-.131	-.096	-.022	.062	.153	.252	75	.770	15			.365	.373	.388	.364	.367	.422
25	.226	45			-.110	-.069	-.005	.045	.087	.119	76	.770	30			.281	.291	.308	.277	.269	.327
26	.226	68			-.121	-.087	-.055	-.052	-.079	-.135	77	.770	50			.235	.243	.257	.207	.182	.238
27	.226	90			-.126	-.105	-.103	-.131	-.204	-.310	78	.770	F			.221	.226	.237	.153	.086	.132
28	.226	135			-.350	-.347	-.344	-.337	-.340	-.358	79	.770	F			.259	.259	.243	.034	-.265	-.268
29	.226	C			-.674	-.735	-.789	-.788	-.864	-.808	80	.770	F			.230	.225	.199	.019	-.339	-.504
30	.263	C			-.090	-.085	-.067	-.052	-.039	-.057	81	.770	135			.257	.248	.215	.057	-.237	-.646
31	.283	0			-.125	-.113	-.070	-.005	.083	.197	83	.820	38			.279	.281	.291	.290	.290	.331
32	.299	30			-.135	-.100	-.035	.034	.110	.203	84	.820	F			.249	.255	.273	.288	.302	.347
33	.299	60			-.142	-.087	-.013	.047	.100	.169	85	.820	F			.227	.235	.257	.282	.297	.339
34	.299	F			-.159	-.084	-.005	.028	.027	.047	86	.820	F			.227	.237	.264	.302	.322	.358
35	.299	F			-.032	-.020	-.075	-.189	-.387	-.513	87	.820	F			.237	.243	.273	.352	.414	.451
36	.299	F			-.051	-.116	-.274	-.473	-.944	-1.205	88	.820	F			.233	.225	.172	-.054	-.456	-.689
37	.299	135			-.064	-.108	-.182	-.227	-.221	-.313	89	.820	F			.229	.222	.183	.052	-.228	-.389
38	.319	C			-.020	-.029	-.053	-.081	-.099	-.147	90	.820	F			.240	.236	.200	.076	-.203	-.328
39	.350	20			-.063	-.041	.015	.086	.170	.269	91	.820	F			.257	.255	.226	.105	-.171	-.367
40	.350	40			-.071	-.037	.026	.089	.155	.230	92	.820	142			.289	.292	.275	.137	-.123	-.463
41	.350	60			-.075	-.037	.024	.093	.170	.255	93	.820	165			.321	.321	.290	.183	-.057	-.225
42	.350	F			-.100	-.042	.028	.070	.103	.128	94	.897	30			.464	.469	.482	.513	.530	.553
43	.350	F			-.018	-.001	-.075	-.236	-.447	-.711	95	.897	50			.373	.377	.386	.414	.441	.470
44	.350	F			-.006	-.053	-.154	-.244	-.402	-.759	96	.897	F			.288	.292	.305	.345	.375	.404
45	.350	135			.005	-.029	-.076	-.083	-.051	-.077	97	.897	F			.249	.250	.212	.109	-.105	-.357
46	.367	0			-.056	-.050	-.012	.054	.139	.247	98	.897	130			.349	.354	.327	.219	.032	-.307
47	.367	180			-.001	-.017	-.037	-.037	-.048	-.070	99	.897	150			.468	.465	.424	.345	.213	-.113
48	.486	0			-.030	-.015	.049	.136	.234	.346	102	.984	0			-.498	-.499	-.496	-.477	-.459	-.432
49	.486	180			.007	-.014	-.035	-.045	-.031	-.099	104	.984	60			-.591	-.587	-.574	-.533	-.502	-.525
50	.503	15			.144	.183	.233	.278	.314	.320	105	.984	90			-.613	-.615	-.623	-.630	-.644	-.652
51	.503	30			-.031	.011	.107	.205	.303	.402	106	.984	135			-.608	-.602	-.601	-.613	-.642	-.639
52	.503	50			-.009	.029	.119	.212	.303	.396	107	.984	180			-.524	-.521	-.518	-.546	-.586	-.611
53	.503	F			.007	.043	.129	.208	.279	.353											
54	.503	F			.033	.048	-.035	-.171	-.295	-.524											

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(c) M = 0.95

Pressure coefficients C_p on -

Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage								Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage - Concluded							
			$\alpha = -20^\circ$	$\alpha = -10^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 15^\circ$	$\alpha = 20^\circ$				$\alpha = -20^\circ$	$\alpha = -10^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 15^\circ$	$\alpha = 20^\circ$
			$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed											$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed							
1	.026	0				.225	.306	.410	.527	.655	55	.503	F				.027	.009	-.104	-.249	-.309
2	.026	90				.201	.169	.087	-.027	-.199	56	.503	135				.015	.013	.028	-.053	-.410
3	.026	180				.223	.147	.103	.065	.043	57	.588	0				-.036	.084	.201	.317	.428
4	.084	0				.068	.144	.241	.358	.487	58	.588	180				-.031	-.179	-.297	-.378	-.494
5	.045	84				.047	.065	.051	.047	.049	59	.604	15				-.056	.066	.179	.288	.393
6	.090	84				.047	.013	-.039	-.145	-.338	60	.604	30				-.047	.081	.196	.304	.399
7	.084	135				.031	-.001	-.038	-.096	-.158	61	.604	50				-.053	.088	.218	.338	.443
8	.084	180				.077	.013	-.020	-.052	-.085	62	.604	F				-.054	.102	.249	.380	.491
9	.134	J				.119	.065	.037	.020	-.025	63	.604	F				-.053	-.256	-.457	-.858	-1.018
10	.156	J				.071	.034	.024	.046	.106	64	.604	135				-.046	-.226	-.399	-.602	-.795
12	.173	30				-.089	-.066	-.037	.005	.068	65	.690	0				-.011	.025	.093	.191	.299
13	.173	60				-.093	-.098	-.132	-.193	-.277	66	.690	180				-.034	-.305	-.509	-.618	-.795
14	.173	90				-.084	-.091	-.137	-.230	-.348	67	.706	15				.023	.037	.074	.154	.252
15	.173	135				-.058	-.054	-.052	-.073	-.098	68	.706	30				.027	.043	.079	.156	.250
16	.173	J				-.004	-.022	-.014	.017	.053	69	.706	50				.031	.051	.090	.172	.266
17	.173	C				.034	.000	-.008	.004	.018	70	.706	F				.044	.057	.100	.186	.279
18	.190	J				-.086	-.083	-.061	-.018	-.027	71	.706	F				-.001	-.113	-.487	-.567	-1.046
19	.190	C				-.091	-.114	-.110	-.098	-.051	72	.706	135				.006	-.106	-.536	-.674	-.858
20	.197	C				-.272	-.318	-.340	-.343	-.325	73	.753	0				.173	.190	.186	.196	.275
21	.207	C				-.167	-.172	-.167	-.151	-.072	74	.753	180				.158	.145	-.038	-.290	-.610
23	.216	C				-.426	-.464	-.476	-.473	-.464	75	.770	15				.012	.024	.023	.053	.101
24	.226	23				-.156	-.124	-.086	-.021	.065	76	.770	30				.034	.037	-.001	.017	.068
25	.226	45				-.157	-.149	-.151	-.155	-.148	77	.770	50				.050	.060	-.002	-.003	.057
26	.226	68				-.191	-.188	-.219	-.288	-.379	78	.770	F				.076	.086	.000	-.058	.001
27	.226	90				-.223	-.203	-.226	-.288	-.363	79	.770	F				.112	.130	.020	-.230	-.387
28	.226	135				-.475	-.439	-.400	-.399	-.457	80	.770	F				.063	.080	.010	-.502	-.472
29	.226	C				-.616	-.663	-.736	-.804	-.853	81	.770	135				.034	.064	.037	-.434	-.566
30	.263	C				-.325	-.318	-.175	-.085	-.083	82	.820	15				-.017	.010	-.008	-.130	.045
31	.283	0				-.207	-.186	-.089	.038	.173	83	.820	38				-.008	.024	.008	-.073	.048
32	.299	30				-.083	-.105	-.131	-.079	-.005	84	.820	F				-.001	.031	.019	-.042	.089
33	.299	60				-.060	-.046	-.070	-.034	.042	85	.820	F				.015	.044	.028	-.031	.088
34	.299	F				-.054	-.033	-.097	-.113	-.074	86	.820	F								
35	.299	F				-.029	-.077	-.144	-.534	-.634	87	.820	F				.072	.085	.069	.032	.125
36	.299	F				-.046	-.123	-.222	-.425	-.822	88	.820	F				.003	.015	-.022	-.159	-.129
37	.299	135				-.015	-.033	-.063	-.115	-.135	89	.820	F				-.003	.009	-.030	-.203	-.167
38	.319	C				.004	-.016	-.030	-.042	-.097	90	.820	F				-.013	-.013	-.046	-.173	-.223
39	.350	20				-.042	-.034	-.009	.037	.124	91	.820	F				-.028	-.024	-.050	-.134	-.115
40	.350	40				-.029	-.021	-.011	.006	.046	92	.820	142				-.012	-.010	-.011	-.013	-.143
41	.350	60				-.029	-.003	.037	.096	.157	94	.897	30				-.129	-.096	-.045	-.001	.065
42	.350	F				-.030	-.004	.000	.003	-.013	95	.897	50				-.135	-.100	-.041	.013	.081
43	.350	F				-.028	-.074	-.222	-.533	-.649	96	.897	F				-.134	-.097	-.035	.027	.098
44	.350	F				-.019	-.051	-.111	-.229	-.840	97	.897	F				-.147	-.162	-.170	-.224	-.355
45	.350	135				.007	.004	-.021	-.036	-.055	98	.897	130				-.131	-.138	-.141	-.190	-.328
46	.367	0				-.048	-.018	.041	.125	.237	99	.897	150				-.132	-.136	-.134	-.186	-.299
47	.367	180				-.014	-.028	-.010	.018	.010	102	.984	0				-.326	-.327	-.305	-.282	-.272
48	.486	0				-.012	.037	.125	.232	.348	104	.984	60				-.331	-.324	-.301	-.280	-.359
49	.486	180				-.013	-.020	-.023	.014	-.011	105	.984	90				-.340	-.336	-.316	-.308	-.408
50	.503	15				.003	.048	.124	.215	.316	106	.984	135				-.313	-.324	-.273	-.268	-.353
51	.503	30				.009	.045	.108	.179	.264	107	.984	180				-.393	-.397	-.361	-.368	-.483
52	.503	50				.014	.061	.132	.211	.299											
53	.503	F				.030	.064	.119	.178	.251											
54	.503	F				.028	-.012	-.082	-.259	-.287											

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(c) M = 0.95 - Continued

Pressure coefficients C_p on -

Model orifice number	x/l	ϕ, deg	Fuselage								Model orifice number	x/l	ϕ, deg	Fuselage - Concluded							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			β ≈ -5°; δ_e = 0°; δ_v = 0°; brakes open											β ≈ -5°; δ_e = 0°; δ_v = 0°; brakes open							
1	.026	0	.035	.093	.181	.228	.317	.418	.530	.658	55	.503	F	.237	.115	.050	.035	.012	-.111	-.243	-.311
2	.026	90	-.224	.077	.176	.203	.159	.083	-.032	-.217	56	.503	135	.257	.115	.045	.021	.022	.027	-.057	-.443
3	.026	180	.668	.424	.274	.223	.146	.101	.064	.038	57	.588	0	-.477	-.320	-.107	-.019	.112	.217	.325	.436
4	.084	0	-.098	-.028	.036	.072	.155	.251	.361	.493	58	.588	180	.425	.202	.053	-.021	-.187	-.302	-.370	-.505
5	.084	45	-.169	-.020	.040	.046	.070	.054	.047	.042	59	.604	15	-.533	-.359	-.130	-.032	.095	.195	.298	.400
6	.084	90	-.353	-.052	.036	.050	.021	-.043	-.148	-.357	60	.604	30	-.614	-.364	-.126	-.024	.112	.212	.311	.407
7	.084	135	.027	.033	.041	.032	.000	-.039	-.100	-.169	61	.604	50	-.768	-.401	-.132	-.030	.120	.236	.347	.451
8	.084	180	.510	.263	.124	.076	.020	-.022	-.051	-.089	62	.604	F	-.966	-.461	-.159	-.032	.134	.266	.390	.498
9	.134	J	.490	.276	.158	.119	.066	.038	.019	-.032	63	.604	F	.492	.253	.062	-.039	-.270	-.458	-.866	-1.017
10	.156	J	.334	.161	.093	.072	.037	.030	.047	.104	64	.604	135	.424	.216	.053	-.032	-.237	-.410	-.609	-.801
12	.173	30	-.266	-.150	-.102	-.085	-.058	-.029	.011	.064	65	.690	0	-.828	-.532	.029	.037	.080	.116	.206	.314
13	.173	60	-.343	-.186	-.102	-.090	-.094	-.131	-.191	-.288	66	.690	180	.278	.073	.039	.017	-.083	-.394	-.501	-.759
14	.173	90	-.539	-.227	-.100	-.083	-.086	-.137	-.234	-.360	67	.706	15	-.771	-.539	.064	.066	.090	.099	.172	.269
15	.173	135	-.165	-.124	-.068	-.057	-.048	-.048	-.074	-.107	68	.706	30	-.811	-.521	.066	.070	.095	.103	.173	.265
16	.173	J			.007	-.004	-.018	-.009	.018	.047	69	.706	50	-.865	-.528	.075	.074	.104	.115	.188	.282
17	.173	C	.275	.103	.050	.035	.003	-.004	.003	.017	70	.706	F	-.971	-.506	.083	.084	.111	.124	.200	.293
18	.190	J	.016	-.089	-.085	-.083	-.076	-.053	-.017	-.032	71	.706	F	.235	.053	.055	.041	.020	-.394	-.742	-1.071
19	.190	C	.114	-.033	-.074	-.089	-.109	-.106	-.096	-.054	72	.706	135	.225	.053	.056	.050	.037	-.402	-.533	-.850
20	.197	C	.112	-.122	-.234	-.270	-.315	-.338	-.342	-.330	73	.753	0	-.727	-.013	.200	.214	.236	.210	.230	.307
21	.207	C	-.029	-.149	-.160	-.165	-.167	-.163	-.150	-.075	74	.753	180	.237	.165	.211	.194	.192	.099	-.171	-.627
23	.216	C	-.024	-.285	-.394	-.428	-.463	-.476	-.472	-.469	75	.770	15	-.666	-.012	.058	.053	.064	.046	.063	.120
24	.226	23	-.059	-.216	-.170	-.153	-.119	-.078	-.016	.068	76	.770	30	-.654	.017	.091	.088	.091	.034	.029	.095
25	.226	45	-.156	-.243	-.172	-.155	-.143	-.146	-.151	-.157	77	.770	50	-.469	.020	.106	.107	.122	.049	.015	.094
26	.226	68	-.183	-.325	-.213	-.190	-.184	-.218	-.288	-.391	78	.770	F	-.447	.031	.141	.130	.144	.052	-.036	.034
27	.226	90	-.469	-.401	-.253	-.222	-.203	-.227	-.289	-.372	79	.770	F	-.491	-.057	.170	.158	.175	.049	-.133	-.172
28	.226	135	-.409	-.550	-.496	-.476	-.433	-.396	-.402	-.467	80	.770	F	-.096	-.043	.118	.112	.120	.027	-.107	-.241
29	.226	C	-.325	-.490	-.578	-.618	-.664	-.738	-.808	-.854	81	.770	135	.007	-.037	.081	.080	.104	.049	-.028	-.146
30	.263	C	.084	-.036	-.154	-.206	-.238	-.110	-.065	-.090	82	.820	15	-.099	-.059	.097	.097	.112	.107	.100	.152
31	.283	0	-.209	-.127	-.113	-.111	-.166	-.068	.046	.180	83	.820	38	-.066	-.019	.099	.112	.135	.129	.109	.160
32	.299	30	-.246	-.088	-.085	-.090	-.098	-.112	-.074	-.006	84	.820	F	-.019	.007	.112	.119	.144	.145	.134	.200
33	.299	60	-.193	-.138	-.077	-.060	-.036	-.044	-.027	.043	85	.820	F	-.100	.018	.126	.129	.154	.154	.133	.196
34	.299	F	-.438	-.239	-.089	-.054	-.026	-.057	-.108	-.076	86	.820	F	-.213	.063						
35	.299	F	-.624	-.183							87	.820	F	-.175	.098	.168	.171	.186	.189	.167	.232
36	.299	F	-.117	-.020	-.011	-.044	-.125	-.241	-.399	-.870	88	.820	F	-.183	-.145	.095	.092	.089	.041	-.095	-.111
37	.299	135			.002	-.011	-.028	-.069	-.114	-.152	89	.820	F	-.189	-.152	.103	.092	.086	.038	-.136	-.145
38	.319	C	.203	.035	.014	.002	-.014	-.025	-.044	-.105	90	.820	F	-.216	-.169	.099	.088	.072	.014	-.169	-.258
39	.350	20	-.006	-.012	-.035	-.038	-.025	.001	.044	.125	91	.820	F	-.238	-.198	.082	.076	.064	.007	-.164	-.216
40	.350	40	-.106	-.044	-.027	-.024	-.013	-.003	.013	.050	92	.820	142	-.294	-.235	.071	.056	.050	-.004	-.165	-.186
41	.350	60	-.069	-.066	-.035	-.025	.007	.047	.101	.163	93	.820	165	-.222	-.256						
42	.350	F	-.553	-.127	-.047	-.025	.004	.006	.003	-.010	94	.897	30	-.184	-.103	.263	.325	.404	.434	.448	.479
43	.350	F	-.820	-.245	-.040	-.025	-.077	-.233	-.553	-.636	95	.897	50	-.187	-.123	.258	.268	.345	.344	.363	.401
44	.350	F	-.003	-.003	.002	-.017	-.048	-.114	-.232	-.871	96	.897	F	-.204	-.133	.202	.225	.262	.290	.314	.349
45	.350	135	.080	.026	.021	.008	.008	-.022	-.031	-.061	97	.897	F	-.215	-.120	.169	.148	.109	.133	.036	-.122
46	.367	0	-.051	-.055	-.046	-.041	-.006	.051	.132	.244	98	.897	130	-.205	-.110	.241	.256	.213	.273	.173	.041
47	.367	180	.278	.079	.011	-.010	-.022	-.005	.019	.008	99	.897	150	-.199	-.114	.345	.307	.309	.383	.318	.202
48	.486	0	-.001	-.021	-.006	-.001	.057	.139	.241	.356	102	.984	0	-.400	-.298	-.552	-.562	-.546	-.505	-.499	-.478
49	.486	180	.346	.126	.023	-.003	-.014	-.019	.013	-.016	103	.984	30	-.357	-.279						
50	.503	15	.002	.042	.003	.013	.066	.136	.222	.322	104	.984	60	-.289	-.278	-.699	-.710	-.710	-.652	-.655	-.715
51	.503	30	-.154	.053	.010	.019	.063	.120	.187	.267	105	.984	90	-.293	-.291	-.720	-.713	-.721	-.677	-.695	-.741
52	.503	50	-.283	.040	.017	.024	.079	.144	.218	.304	106	.984	135	-.305	-.308	-.649	-.620	-.712	-.598	-.647	-.714
53	.503	F	-.266	-.054	.034	.040	.080	.130	.184	.255	107	.984	180	-.367	-.383	-.589	-.595	-.598	-.570	-.595	-.657
54	.503	F	-.219	-.074	.025	.036	-.008	-.088	-.279	-.286											

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(c) M = 0.95 - Continued

Pressure coefficients C_p on -

Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage								Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage - Concluded							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed											$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed							
1	.026	0	.054	.114		.243	.329	.431	.543	.661	55	.503	F	.295	.159		.025	.016	-.173	-.244	-.227
2	.026	90	-.100	.160		.255	.229	.159	.048	-.124	56	.503	135	.331	.167		.020	.014	.053	.044	-.422
3	.026	180	.671	.441		.242	.179	.117	.078	.051	57	.588	0	-.391	-.293		-.017	.113	.228	.340	.447
4	.084	0	-.057	-.006		.104	.187	.280	.388	.509	58	.588	180	.452	.235		-.017	-.171	-.282	-.359	-.391
5	.084	45	-.185	-.017		.090	.135	.181	.205	.222	59	.604	15	-.596	-.363		-.042	.094	.212	.325	.433
6	.084	90	-.258	.000		.094	.072	.006	-.094	-.241	60	.604	30	-.812	-.370		-.039	.103	.226	.338	.443
7	.084	135	.202	.152		.085	.025	-.045	-.125	-.217	61	.604	50	-.875	-.387		-.048	.102	.232	.351	.463
8	.084	180	.523	.297		.096	.045	-.005	-.032	-.056	62	.604	F	-1.037	-.438		-.059	.110	.251	.382	.496
9	.134	J	.497	.291		.133	.081	.051	.031	.018	63	.604	F	.504	.251		-.068	-.279	-.491	-.805	-.980
10	.156	J	.451	.291		.193	.153	.127	.116	.099	64	.604	135	.456	.231		-.051	-.237	-.389	-.587	-1.014
12	.173	30	-.260	-.150		-.078	-.048	.013	.081	.171	65	.690	0	-.671	-.490		-.006	.035	.103	.202	.310
13	.173	60	-.435	-.189		-.046	-.023	-.035	-.065	-.125	66	.690	180	.295	.087		-.039	-.335	-.488	-.573	-.739
14	.173	90	-.455	-.159		-.025	-.031	-.083	-.179	-.325	67	.706	15	-.731	-.499		.039	.055	.090	.174	.276
15	.173	135	.016	.023		.034	.021	.002	-.019	-.058	68	.706	30	-.567	-.246		.046	.063	.095	.178	.277
16	.173	J	.302	.175		.117	.092	.082	.080	.056	69	.706	50	-.897	-.491		.056	.066	.093	.176	.273
17	.173	C	.400	.243		.160	.127	.110	.114	.135	70	.706	F	-.998	-.492		.068	.073	.097	.182	.278
18	.190	J	.135	.045		.024	.016	.013	.004	-.051	71	.706	F	.237	.047		.021	-.138	-.464	-.739	-1.054
19	.190	C	.219	.074		.008	-.018	-.024	-.010	.021	72	.706	135	.245	.058		.016	-.162	-.501	-.471	-.964
20	.197	C	.135	-.096		-.249	-.290	-.312	-.322	-.315	73	.753	0	-.655	.060		.161	.174	.154	.167	.256
21	.207	C	.054	-.056		-.082	-.094	-.093	-.071	-.034	74	.753	180	.222	.128		.154	.169	.063	-.508	-.753
23	.216	C	-.005	-.250		-.395	-.431	-.459	-.469	-.461	75	.770	15	-.440	.134		.206	.228	.191	.181	.252
24	.226	23	-.149	-.226		-.124	-.069	-.006	.071	.163	76	.770	30	-.623	.062		.173	.186	.135	.109	.180
25	.226	45	-.152	-.249		-.123	-.082	-.052	-.028	-.008	77	.770	50	-.551	.056		.152	.157	.095	.042	.113
26	.226	68	-.213	-.337		-.156	-.132	-.138	-.172	-.237	78	.770	F	-.485	.064		.155	.155	.074	-.045	.021
27	.226	90	-.582	-.362		-.178	-.157	-.176	-.234	-.328	79	.770	F	-.013	-.013		.185	.174	.077	-.262	-.455
28	.226	135	-.258	-.449		-.399	-.370	-.352	-.341	-.388	80	.770	F	-.082	.040		.143	.143	.058	-.288	-.478
29	.226	C	-.279	-.457		-.683	-.806	-.873	-.878	-.845	81	.770	135	.071	.068		.145	.148	.060	-.331	-.779
30	.263	C	.143	.054		-.259	-.272	-.157	-.055	-.022	82	.820	15	.037	.124		.111	.123	.093	.025	.109
31	.283	0	-.080	-.098		-.117	-.104	-.038	.067	.191	83	.820	38	-.052	.112		.114	.129	.102	.033	.110
32	.299	30	-.275	-.122		-.086	-.091	-.065	.016	.109	84	.820	F	.006	.115		.113	.131	.112	.059	.146
33	.299	60	-.255	-.205		-.082	-.057	-.061	.017	.099	85	.820	F	-.239	.111		.107	.129	.112	.059	.141
34	.299	F	-.839	-.321		-.081	-.042	-.105	-.054	-.013	86	.820	F	-.333	.141		.126	.151	.135	.096	.185
35	.299	F	-.552	-.184		-.033	-.075	-.369	-.442	-.542	87	.820	F	-.210	.164		.142	.170	.155	.157	.337
36	.299	F	-.046	-.005		-.078	-.173	-.354	-.876	-1.094	88	.820	F	-.130	.005		.099	.083	.021	-.188	-.342
37	.299	135	.114	.033		-.041	-.078	-.092	-.167	-.319	89	.820	F	-.150	.015		.094	.093	.039	-.169	-.221
38	.319	C	.238	.076		.018	.015	.022	.042	.026	90	.820	F	-.161	.020		.094	.091	.047	-.173	-.292
39	.350	20	-.189	-.038		-.030	.003	.049	.109	.204	91	.820	F	-.133	.018		.097	.100	.059	-.099	-.262
40	.350	40	-.093	-.056		-.029	.005	.042	.077	.142	92	.820	142				.101	.105	.076	-.083	-.085
41	.350	60	-.039	-.092		-.039	.008	.062	.120	.197	93	.820	165	-.044	.037						
42	.350	F	-.811	-.187		-.044	.004	.032	.044	.050	94	.897	30	-.272	-.082		-.095	-.065	-.019	.035	.099
43	.350	F	-.845	-.223		-.022	-.071	-.220	-.388	-.760	95	.897	50	-.250	-.079		-.102	-.069	-.013	.051	.119
44	.350	F	.066	.031		-.032	-.091	-.153	-.288	-.867	96	.897	F	-.277	-.086		-.112	-.076	-.013	.056	.129
45	.350	135	.168	.072		.005	-.016	-.023	-.023	-.152	97	.897	F	-.013	-.012		-.092	-.106	-.142	-.255	-.448
46	.367	0	.021	-.004		-.031	.003	.063	.144	.252	98	.897	130	-.163	-.093		-.078	-.089	-.114	-.222	-.355
47	.367	180	.300	.105		.019	.035	.063	.084	.070	99	.897	150	-.172	-.097		-.077	-.090	-.125	-.186	-.330
48	.486	0	.022	.060		.006	.062	.150	.254	.366	102	.984	0	-.364	-.293		-.275	-.267	-.255	-.248	-.242
49	.486	180	.371	.155		.007	.014	.055	.082	.096	103	.984	30	-.361	-.282		-.271	-.266	-.253	-.241	-.251
50	.503	15	-.071	.036		.018	.085	.174	.272	.378	104	.984	60	-.299	-.274		-.281	-.284	-.275	-.278	-.386
51	.503	30	-.098	.044		.021	.088	.169	.256	.348	105	.984	90	-.300	-.278		-.296	-.301	-.295	-.307	-.416
52	.503	50	-.177	.063		.020	.088	.171	.259	.352	106	.984	135	-.309	-.228		-.271	-.278	-.262	-.287	-.362
53	.503	F	-.264	-.136		.031	.093	.163	.231	.306	107	.984	180	-.321	-.313		-.319	-.323	-.333	-.362	-.441
54	.503	F	-.300	-.105		.030	-.014	-.111	-.188	-.345											

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(c) M = 0.95 - Continued

Pressure coefficients C_p on -

Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage								Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage - Concluded							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open											$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open							
1	.026	0			.202	.243	.327	.427	.542	.661	55	.503	F			.061	.031	.019	-.165	-.243	-.214
2	.026	90			.251	.259	.235	.163	.052	-.114	56	.503	135			.056	.024	.017	.052	.050	-.405
3	.026	180			.297	.248	.182	.118	.079	.055	57	.588	0			-.109	-.023	.107	.223	.339	.445
4	.084	0			.064	.103	.183	.277	.388	.508	58	.588	180			.067	-.004	-.162	-.281	-.359	-.385
5	.084	45			.071	.093	.138	.177	.215	.231	59	.604	15			-.138	-.048	.089	.208	.326	.433
6	.084	90			.089	.100	.077	.008	-.095	-.230	60	.604	30			-.140	-.044	.100	.222	.340	.445
7	.084	135			.116	.091	.029	-.046	-.129	-.211	61	.604	50			-.156	-.052	.098	.228	.353	.462
8	.084	180			.147	.102	.045	-.004	-.033	-.055	62	.604	F			-.185	-.066	.104	.248	.382	.498
9	.134	J			.175	.138	.086	.049	.031	.022	63	.604	F			.049	-.051	-.268	-.491	-.804	-.962
10	.156	J			.225	.201	.159	.129	.117	.102	64	.604	135			.049	-.037	-.226	-.382	-.582	-1.003
12	.173	30			-.081	-.050	.005	.058	.122	.192	65	.690	0			-.050	.002	.039	.102	.204	.311
13	.173	60			-.071	-.043	-.019	-.031	-.059	-.113	66	.690	180			.001	-.022	-.323	-.483	-.559	-.730
14	.173	90			-.045	-.022	-.027	-.080	-.175	-.307	67	.706	15			.038	.048	.062	.092	.179	.280
15	.173	135			.042	.041	.025	.001	-.017	-.053	68	.706	30			.045	.058	.072	.096	.182	.281
16	.173	J			.136	.125	.100	.084	.082	.060	69	.706	50			.057	.069	.077	.095	.180	.278
17	.173	C			.189	.167	.135	.113	.119	.142	70	.706	F			.063	.081	.086	.099	.185	.282
18	.190	J			.033	.029	.020	.015	.003	-.043	71	.706	F			.045	.041	-.065	-.404	-.735	-1.012
19	.190	C			.035	.016	-.011	-.024	-.008	.026	72	.706	135			.044	.035	-.081	-.464	-.553	-.951
20	.197	C			-.211	-.247	-.290	-.321	-.325	-.312	73	.753	0			.168	.170	.184	.162	.181	.267
21	.207	C			-.066	-.077	-.089	-.092	-.068	-.032	74	.753	180			.173	.168	.182	.083	-.495	-.690
23	.216	C			-.364	-.393	-.437	-.461	-.468	-.458	75	.770	15			.227	.241	.262	.225	.212	.284
24	.226	23			-.159	-.122	-.069	-.008	.075	.166	76	.770	30			.198	.206	.217	.169	.140	.211
25	.226	45			-.165	-.124	-.079	-.051	-.021	.003	77	.770	50			.183	.184	.188	.126	.070	.140
26	.226	68			-.200	-.155	-.126	-.135	-.166	-.226	78	.770	F			.184	.181	.182	.100	-.017	.044
27	.226	90			-.219	-.173	-.152	-.173	-.224	-.322	79	.770	F			.199	.211	.199	.096	-.239	-.415
28	.226	135			-.416	-.396	-.369	-.354	-.340	-.380	80	.770	F			.173	.173	.173	.083	-.235	-.476
29	.226	C			-.608	-.676	-.808	-.877	-.877	-.839	81	.770	135			.185	.184	.184	.093	-.242	-.646
30	.263	C			-.100	-.232	-.270	-.151	-.054	-.018	82	.820	15			.186	.188	.199	.167	.102	.175
31	.283	0			-.090	-.093	-.101	-.037	.069	.193	83	.820	38			.168	.172	.182	.152	.083	.149
32	.299	30			-.103	-.085	-.083	-.063	.020	.114	84	.820	F			.161	.163	.177	.157	.106	.181
33	.299	60			-.117	-.082	-.053	-.064	.020	.102	85	.820	F			.150	.153	.170	.152	.099	.166
34	.299	F			-.138	-.083	-.038	-.104	-.050	-.007	86	.820	F			.162	.166	.186	.171	.127	.202
35	.299	F			-.044	-.029	-.068	-.363	-.435	-.530	87	.820	F			.176	.176	.202	.194	.188	.345
36	.299	F			-.030	-.066	-.167	-.345	-.876	-1.058	88	.820	F			.145	.140	.122	.048	-.154	-.317
37	.299	135			-.016	-.034	-.075	-.094	-.169	-.314	89	.820	F			.140	.140	.133	.070	-.144	-.199
38	.319	C			.027	.020	.015	.018	.041	.033	90	.820	F			.144	.143	.140	.089	-.143	-.280
39	.350	20			-.037	-.027	.003	.049	.112	.208	91	.820	F			.152	.154	.155	.109	-.062	-.272
40	.350	40			-.044	-.029	.005	.042	.080	.144	92	.820	142			.171	.171	.173	.142	-.032	-.063
41	.350	60			-.059	-.039	.006	.061	.120	.198	94	.897	30			-.063	-.059	-.041	-.009	.030	.086
42	.350	F			-.083	-.045	.005	.032	.046	.054	95	.897	50			-.066	-.062	-.042	.002	.054	.115
43	.350	F			-.044	-.018	-.063	-.214	-.380	-.735	96	.897	F			-.079	-.074	-.048	.006	.063	.129
44	.350	F			.000	-.025	-.085	-.153	-.293	-.845	97	.897	F			-.048	-.049	-.063	-.100	-.224	-.401
45	.350	135			.021	.007	-.016	-.023	-.021	-.147	98	.897	130			-.034	-.036	-.041	-.073	-.205	-.331
46	.367	0			-.034	-.030	.002	.061	.144	.252	99	.897	150			-.039	-.035	-.045	-.083	-.171	-.323
47	.367	180			.032	.026	.034	.060	.085	.076	102	.984	0			-.352	-.365	-.377	-.334	-.300	-.327
48	.486	0			.004	.008	.060	.148	.254	.365	103	.984	30			-.326	-.337	-.353	-.321	-.288	-.337
49	.486	180			.036	.014	.017	.054	.082	.098	104	.984	60			-.302	-.301	-.308	-.295	-.290	-.381
50	.503	15			.006	.018	.082	.172	.274	.378	105	.984	90			-.307	-.309	-.319	-.309	-.320	-.422
51	.503	30			.008	.021	.085	.169	.259	.350	106	.984	135			-.346	-.349	-.369	-.320	-.324	-.344
52	.503	50			.011	.020	.086	.170	.261	.353	107	.984	180			-.423	-.422	-.416	-.409	-.432	-.525
53	.503	F			.023	.032	.090	.162	.233	.308											
54	.503	F			.016	.035	-.007	-.108	-.189	-.347											

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(c) M = 0.95 - Continued

Pressure coefficients C_p on -

Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage								Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage - Concluded							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = -7.5°$; brakes closed											$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = -7.5°$; brakes closed							
1	.026	0			.203	.242	.326	.431	.546	.659	55	.503	F			.058	.026	.011	-.172	-.234	-.224
2	.026	90			.244	.253	.222	.156	.047	-.123	56	.503	135			.053	.020	.011	.051	.044	-.404
3	.026	180			.295	.244	.176	.116	.082	.053	57	.588	0			-.106	-.023	.109	.228	.343	.445
4	.084	0			.064	.101	.183	.280	.390	.506	58	.588	180			.067	-.009	-.173	-.280	-.353	-.384
5	.084	45			.073	.089	.129	.180	.206	.218	59	.604	15			-.136	-.048	.090	.212	.329	.430
6	.084	90			.083	.093	.065	.002	-.095	-.241	60	.604	30			-.137	-.044	.100	.226	.342	.440
7	.084	135			.114	.084	.016	-.047	-.124	-.213	61	.604	50			-.153	-.055	.098	.232	.355	.460
8	.084	180			.148	.099	.038	-.005	-.030	-.057	62	.604	F			-.183	-.067	.105	.252	.385	.495
9	.134	J			.176	.135	.079	.049	.032	.019	63	.604	F			.048	-.058	-.284	-.492	-.795	-.962
10	.156	J			.216	.191	.142	.125	.116	.097	64	.604	135			.047	-.045	-.239	-.384	-.591	-.998
12	.173	30			-.088	-.062	-.011	.046	.109	.175	65	.690	0			-.070	-.002	.039	.108	.208	.309
13	.173	60			-.073	-.046	-.028	-.036	-.067	-.127	66	.690	180			-.007	-.029	-.335	-.485	-.561	-.715
14	.173	90			-.049	-.029	-.038	-.086	-.180	-.318	67	.706	15			.029	.041	.057	.096	.181	.276
15	.173	135			.035	.031	.014	-.002	-.018	-.059	68	.706	30			.031	.047	.063	.100	.183	.276
16	.173	J			.127	.114	.084	.079	.081	.058	69	.706	50			.039	.053	.064	.097	.181	.272
17	.173	C			.171	.145	.118	.107	.113	.130	70	.706	F			.038	.064	.071	.101	.187	.276
18	.190	J			.026	.021	.009	.011	.003	-.049	71	.706	F			.023	.018	-.119	-.548	-.455	-1.073
19	.190	C			.018	.006	-.021	-.029	-.011	.018	72	.706	135			.023	.014	-.131	-.546	-.600	-.959
20	.197	C			-.211	-.248	-.297	-.319	-.322	-.314	73	.753	0			.169	.167	.179	.174	.184	.266
21	.207	C			-.068	-.081	-.100	-.096	-.069	-.036	74	.753	180			.168	.162	.172	.058	-.431	-.713
23	.216	C			-.363	-.396	-.444	-.461	-.465	-.462	75	.770	15			.172	.181	.203	.189	.188	.242
24	.226	23			-.161	-.125	-.074	-.010	.070	.159	76	.770	30			.145	.150	.160	.134	.116	.168
25	.226	45			-.164	-.123	-.087	-.058	-.030	-.010	77	.770	50			.133	.129	.132	.091	.045	.099
26	.226	68			-.200	-.158	-.138	-.142	-.174	-.239	78	.770	F			.139	.133	.131	.077	-.041	.012
27	.226	90			-.221	-.180	-.165	-.177	-.232	-.330	79	.770	F			.157	.164	.158	.092	-.271	-.491
28	.226	135			-.419	-.403	-.378	-.356	-.342	-.388	80	.770	F			.121	.120	.122	.053	-.357	-.541
29	.226	C			-.600	-.674	-.799	-.864	-.867	-.837	81	.770	135			.126	.120	.120	.045	-.528	-.667
30	.263	C			-.211	-.256	-.235	-.157	-.066	-.016	82	.820	15			.005	.005	.015	-.007	-.301	-.003
31	.283	0			-.087	-.110	-.102	-.035	.068	.190	83	.820	38			.029	.032	.046	.033	-.197	.037
32	.299	30			-.098	-.084	-.082	-.065	.015	.105	84	.820	F			.043	.044	.061	.053	-.093	.083
33	.299	60			-.113	-.082	-.053	-.062	.016	.096	85	.820	F			.045	.046	.066	.063	-.063	.090
34	.299	F			-.131	-.080	-.039	-.107	-.055	-.016	86	.820	F			.075	.073	.096	.095	.012	.149
35	.299	F			-.043	-.033	-.080	-.371	-.443	-.544	87	.820	F			.100	.094	.116	.111	.097	.314
36	.299	F			-.026	-.070	-.181	-.325	-.894	-1.086	88	.820	F			.061	.051	.038	.011	-.239	-.336
37	.299	135			-.013	-.036	-.078	-.092	-.172	-.309	89	.820	F			.047	.042	.044	.024	-.206	-.244
38	.319	C			.030	.018	.007	.019	.044	.026	90	.820	F			.041	.035	.032	.018	-.215	-.306
39	.350	20			-.036	-.030	-.001	.049	.107	.201	91	.820	F			.028	.023	.026	.016	-.157	-.271
40	.350	40			-.042	-.031	.001	.041	.076	.137	92	.820	142			.012	.009	.008	.011	-.143	-.128
41	.350	60			-.058	-.041	.004	.062	.118	.194	94	.897	30			-.136	-.126	-.094	-.046	.012	.077
42	.350	F			-.081	-.046	.001	.031	.040	.047	95	.897	50			-.144	-.136	-.102	-.047	.023	.093
43	.350	F			-.044	-.022	-.076	-.224	-.373	-.758	96	.897	F			-.154	-.143	-.105	-.044	.031	.106
44	.350	F			-.001	-.029	-.091	-.152	-.295	-.864	97	.897	F			-.114	-.126	-.149	-.170	-.293	-.479
45	.350	135			.023	.006	-.019	-.022	-.020	-.153	98	.897	130			-.100	-.114	-.132	-.149	-.233	-.354
46	.367	0			-.035	-.032	.000	.064	.145	.250	99	.897	150			-.101	-.111	-.131	-.156	-.193	-.308
47	.367	180			.032	.022	.027	.062	.086	.073	102	.984	0			-.348	-.357	-.343	-.337	-.318	-.334
48	.486	0			.003	.005	.059	.152	.257	.364	103	.984	30			-.313	-.319	-.310	-.306	-.303	-.330
49	.486	180			.036	.009	.011	.057	.085	.096	104	.984	60			-.302	-.305	-.305	-.294	-.290	-.364
50	.503	15			.006	.015	.081	.174	.275	.375	105	.984	90			-.307	-.312	-.313	-.310	-.313	-.404
51	.503	30			.009	.019	.083	.169	.257	.344	106	.984	135			-.280	-.281	-.277	-.268	-.271	-.354
52	.503	50			.012	.018	.082	.171	.260	.348	107	.984	180			-.391	-.391	-.380	-.384	-.414	-.498
53	.503	F			.022	.029	.088	.162	.231	.302											
54	.503	F			.017	.031	-.017	-.112	-.185	-.341											

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(c) M = 0.95 - Continued

Pressure coefficients C_p on -

Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage								Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage - Concluded							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 7.5°$; brakes closed											$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 7.5°$; brakes closed							
1	.026	0			.204	.243	.329	.429	.540	.660	55	.503	F			.068	.037	.022	-.151	-.263	-.215
2	.026	90			.249	.258	.229	.164	.057	-.116	56	.503	135			.063	.030	.021	.054	.052	-.395
3	.026	180			.297	.248	.180	.120	.082	.054	57	.588	0			-.100	-.011	.122	.232	.341	.448
4	.084	0			.065	.104	.186	.278	.385	.507	58	.588	180			.081	.007	-.162	-.275	-.353	-.388
5	.084	45			.075	.090	.134	.179	.210	.225	59	.604	15			-.130	-.033	.107	.216	.327	.436
6	.084	90			.087	.097	.073	.010	-.088	-.231	60	.604	30			-.131	-.029	.117	.230	.339	.446
7	.084	135			.114	.089	.028	-.040	-.117	-.206	61	.604	50			-.149	-.039	.116	.236	.353	.465
8	.084	180			.147	.102	.046	.000	-.030	-.053	62	.604	F			-.179	-.055	.122	.256	.382	.501
9	.134	J			.177	.140	.086	.053	.033	.022	63	.604	F			.061	-.039	-.266	-.460	-.654	-.961
10	.156	J			.220	.199	.153	.129	.117	.099	64	.604	135			.062	-.024	-.225	-.367	-.514	-1.004
12	.173	30			-.081	-.052	.003	.053	.114	.189	65	.690	0			.034	.046	.087	.121	.210	.318
13	.173	60			-.071	-.042	-.022	-.031	-.060	-.116	66	.690	180			.046	.027	-.077	-.385	-.481	-.718
14	.173	90			-.046	-.025	-.030	-.076	-.165	-.305	67	.706	15			.081	.084	.109	.113	.185	.289
15	.173	135			.039	.037	.022	.002	-.017	-.052	68	.706	30			.087	.091	.114	.117	.190	.288
16	.173	J			.132	.121	.093	.083	.083	.059	69	.706	50			.098	.100	.119	.115	.187	.285
17	.173	C			.186	.166	.130	.113	.118	.140	70	.706	F			.105	.109	.127	.119	.192	.288
18	.190	J			.028	.027	.016	.014	.005	-.046	71	.706	F			.076	.069	.038	-.304	-.582	-.732
19	.190	C			.031	.013	-.014	-.025	-.009	.024	72	.706	135			.077	.066	.041	-.319	-.490	-.809
20	.197	C			-.210	-.247	-.292	-.317	-.324	-.312	73	.753	0			.203	.206	.224	.189	.199	.284
21	.207	C			-.069	-.078	-.093	-.092	-.071	-.035	74	.753	180			.204	.197	.207	.130	-.326	-.453
23	.216	C			-.361	-.392	-.437	-.459	-.469	-.461	75	.770	15			.239	.251	.275	.237	.224	.286
24	.226	23			-.157	-.122	-.069	-.010	.072	.165	76	.770	30			.215	.222	.237	.186	.158	.218
25	.226	45			-.163	-.127	-.084	-.053	-.031	.000	77	.770	50			.203	.204	.212	.148	.098	.153
26	.226	68			-.198	-.157	-.128	-.134	-.166	-.230	78	.770	F			.206	.204	.209	.123	.023	.057
27	.226	90			-.215	-.177	-.156	-.173	-.224	-.325	79	.770	F			.225	.231	.227	.107	-.114	-.394
28	.226	135			-.418	-.400	-.373	-.352	-.340	-.383	80	.770	F			.193	.193	.191	.087	-.144	-.464
29	.226	C			-.601	-.674	-.800	-.869	-.880	-.839	81	.770	135			.198	.193	.193	.104	-.104	-.407
30	.263	C			-.078	-.158	-.181	-.113	-.037	-.006	82	.820	15			.216	.221	.231	.212	.189	.234
31	.283	0			-.087	-.092	-.092	-.032	.068	.195	83	.820	38			.212	.218	.231	.215	.190	.229
32	.299	30			-.099	-.084	-.072	-.058	.017	.113	84	.820	F			.211	.216	.231	.222	.210	.261
33	.299	60			-.114	-.081	-.043	-.052	.018	.103	85	.820	F			.203	.207	.226	.221	.207	.253
34	.299	F			-.141	-.084	-.035	-.089	-.054	-.011	86	.820	F			.214	.219	.241	.237	.226	.285
35	.299	F			-.045	-.029	-.074	-.335	-.428	-.532	87	.820	F			.228	.229	.254	.260	.261	.412
36	.299	F			-.036	-.065	-.170	-.224	-.742	-1.051	88	.820	F			.191	.184	.158	.077	-.090	-.305
37	.299	135			-.013	-.034	-.070	-.088	-.152	-.297	89	.820	F			.185	.184	.171	.097	-.086	-.188
38	.319	C			.029	.023	.013	.020	.039	.030	90	.820	F			.191	.188	.173	.099	-.100	-.292
39	.350	20			-.034	-.024	.007	.052	.111	.209	91	.820	F			.193	.194	.183	.106	-.077	-.249
40	.350	40			-.039	-.024	.009	.045	.082	.146	92	.820	142			.198	.200	.188	.116	-.078	-.174
41	.350	60			-.054	-.034	.011	.064	.124	.200	94	.897	30			.408	.422	.455	.483	.498	.523
42	.350	F			-.077	-.040	.009	.035	.056	.055	95	.897	50			.343	.352	.366	.392	.417	.449
43	.350	F			-.044	-.018	-.064	-.195	-.381	-.740	96	.897	F			.270	.279	.297	.329	.350	.387
44	.350	F			.003	-.023	-.084	-.147	-.263	-.827	97	.897	F			.224	.224	.200	.143	.008	-.205
45	.350	135			.025	.009	-.013	-.019	-.019	-.131	98	.897	130			.314	.305	.300	.245	.116	-.024
46	.367	0			-.030	-.024	.008	.067	.146	.254	99	.897	150			.424	.416	.413	.356	.284	.187
47	.367	180			.037	.028	.034	.064	.086	.075	102	.984	0			-.564	-.562	-.555	-.526	-.495	-.496
48	.486	0			.009	.016	.070	.154	.254	.368	103	.984	30			-.666	-.655	-.579	-.514	-.464	-.436
49	.486	180			.043	.020	.021	.058	.080	.097	104	.984	60			-.690	-.683	-.697	-.678	-.641	-.702
50	.503	15			.012	.027	.092	.178	.274	.380	105	.984	90			-.700	-.707	-.719	-.716	-.704	-.742
51	.503	30			.014	.029	.094	.174	.259	.351	106	.984	135			-.720	-.715	-.713	-.603	-.615	-.689
52	.503	50			.017	.028	.094	.174	.259	.353	107	.984	180			-.592	-.599	-.610	-.592	-.585	-.629
53	.503	F			.028	.040	.100	.167	.233	.309											
54	.503	F			.020	.038	-.004	-.095	-.180	-.350											

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(c) M = 0.95 - Continued

Pressure coefficients C_p on -

Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage								Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage - Concluded							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed											$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed							
1	.026	0	.031	.093		.231	.326	.432	.550	.685	55	.503	F	.359	.206		.023	.016	-.226	-.203	-.242
2	.026	90	.011	.253		.342	.301	.219	.090	-.091	56	.503	135	.400	.207		.009	.010	-.046	.027	-.499
3	.026	180	.655	.419		.203	.132	.091	.057	.029	57	.588	0	-.491	-.326		-.028	.098	.216	.332	.448
4	.084	0	-.101	-.029		.073	.162	.263	.382	.521	58	.588	180	.429	.212		-.059	-.212	-.321	-.401	-.560
5	.084	45	-.344	-.052		.148	.217	.272	.319	.356	59	.604	15	-.677	-.375		-.051	.088	.216	.340	.461
6	.084	90	-.177	.078		.197	.140	.087	-.054	-.220	60	.604	30	-.798	-.376		-.044	.052	.175	.328	.464
7	.084	135	.349	.256		.107	.012	-.096	-.222	-.369	61	.604	50	-.940	-.401		-.034	.121	.255	.383	.506
8	.084	180	.500	.264		.072	.009	-.035	-.068	-.105	62	.604	F	-1.008	-.478		-.038	.130	.275	.412	.541
9	.134	J	.486	.277		.105	.057	.028	.008	-.022	63	.604	F	.521	.263		-.104	-.326	-.629	-.841	-.978
10	.156	J	.562	.406		.289	.237	.188	.127	.075	64	.604	135	.479	.238		-.091	-.278	-.410	-.671	-1.007
12	.173	30	-.313	-.199		-.026	.054	.132	.216	.308	65	.690	0	-.829	-.532		-.012	.031	.099	.203	.319
13	.173	60	-.535	-.204							66	.690	180	.279	.077		-.043	-.382	-.539	-.666	-.786
14	.173	90	-.370	-.091		.049	.029	-.034	-.153	-.339	67	.706	15	-.881	-.498		.035	.059	.099	.193	.307
15	.173	135	.181	.152		.111	.068	.023	-.014	-.044	68	.706	30	-.800	-.464		.059	.080	.113	.207	.319
16	.173	J	.428	.295		.214	.182	.147	.099	.054	69	.706	50	-.736	-.497		.088	.097	.119	.210	.316
17	.173	C	.522	.370		.255	.219	.202	.212	.221	70	.706	F	-.801	-.538		.107	.107	.122	.212	.316
18	.190	J	.264	.161		.117	.096	.057	.002	-.062	71	.706	F	.252	.073		.063	-.128	-.519	-.797	-.729
19	.190	C	.342	.188		.090	.061	.053	.073	.115	72	.706	135	.267	.084		.049	-.176	-.569	-.369	-.988
20	.197	C	.094	-.133		-.313	-.348	-.354	-.344	-.321	73	.753	0	-.653	-.018		.171	.182	.165	.194	.287
21	.207	C	.160	.039		-.013	-.027	-.022	.012	.031	74	.753	180	.235	.154		.156	.130	-.085	-.380	-.645
23	.216	C	-.016	-.272		-.448	-.480	-.482	-.472	-.465	75	.770	15	-.599	.112		.362	.365	.331	.321	.398
24	.226	23	-.171	-.272		-.127	-.040	.050	.153	.267	76	.770	30	-.628	.121		.279	.281	.238	.214	.297
25	.226	45	-.195	-.315		-.095	-.021	.036	.088	.132	77	.770	50	-.491	.133		.227	.227	.169	.115	.197
26	.226	68	-.584	-.339		-.109	-.061	-.050	-.072	-.131	78	.770	F	-.439	.143		.210	.209	.122	.006	.079
27	.226	90	-.474	-.309		-.112	-.094	-.116	-.180	-.268	79	.770	F	-.489	.143		.247	.227	.065	-.280	-.376
28	.226	135	.007	-.348		-.307	-.299	-.293	-.299	-.326	80	.770	F	-.055	.138		.211	.189	.090	-.332	-.560
29	.226	C	-.060	-.487		-.870	-.896	-.886	-.853	-.791	81	.770	135	.141	.187		.235	.210	.091	-.202	-.735
30	.263	C	.105	-.014		-.362	-.298	-.193	-.110	-.131	82	.820	15	-.081	.233						
31	.283	0	-.201	-.127		-.231	-.164	-.055	.069	.211	83	.820	38	-.283	.206		.220	.220	.196	.153	.226
32	.299	30	-.217	-.184		-.136	-.126	-.016	.100	.220	84	.820	F	-.232	.176		.196	.202	.194	.166	.241
33	.299	60	-.477	-.304		-.132	-.127	-.015	.092	.191	85	.820	F	-.383	.163		.177	.188	.189	.161	.233
34	.299	F	-1.023	-.436		-.123	-.134	-.044	.028	.078	86	.820	F	-.391	.181		.187	.202	.212	.194	.263
35	.299	F	-.473	-.177		-.057	-.248	-.288	-.360	-.461	87	.820	F	-.359	.192		.197	.214	.252	.289	.387
36	.299	F	.043	.022		-.126	-.507	-.707	-.881	-1.090	88	.820	F	-.061	.106		.181	.152	.012	-.376	-.868
37	.299	135	.190	.042		-.092	-.144	-.256	-.338	-.450	89	.820	F	-.140	.109		.178	.158	.057	-.213	-.667
38	.319	C	.205	.038		-.006	-.029	-.049	-.071	-.131	90	.820	F	-.156	.116		.186	.169	.095	-.246	-.361
39	.350	20	-.157	-.065		-.042	.011	.073	.162	.287	91	.820	F	-.091	.131		.201	.192	.130	-.076	-.342
40	.350	40	-.056	-.100		-.036	.025	.078	.142	.245	92	.820	142				.237	.240	.173	.010	-.696
41	.350	60	-.046	-.142		-.036	.026	.086	.151	.269	93	.820	165	.090	.192		.267	.265	.212	.042	-.088
42	.350	F	-.893	-.262		-.038	.032	.075	.073	.141	94	.897	30	-.364	-.058		-.057	-.028	.026	.084	.162
43	.350	F	-.742	-.212		.001	-.060	-.184	-.540	-.665	95	.897	50	-.342	-.062		-.062	-.032	.028	.098	.182
44	.350	F	.148	.071		-.053	-.136	-.209	-.599	-.946	96	.897	F	-.443	-.079		-.075	-.041	.029	.108	.191
45	.350	135	.251	.103		-.022	-.054	-.039	-.055	-.108	97	.897	F	.026	-.046		-.025	-.043	-.107	-.290	-.496
46	.367	0	-.048	-.049		-.057	-.016	.048	.136	.266	98	.897	130	.014	-.032		-.004	-.017	-.073	-.224	-.604
47	.367	180	.285	.089		-.023	-.031	-.019	.004	-.027	99	.897	150	-.007	-.034		-.012	-.032	-.064	-.199	-.459
48	.486	0	-.021	-.019		-.016	.047	.141	.252	.375	102	.984	0	-.413	-.287		-.343	-.344	-.330	-.315	-.315
49	.486	180	.351	.135		-.018	-.020	-.029	.006	-.069	103	.984	30	-.402	-.282						
50	.503	15	.000	.019		.002	.087	.192	.311	.434	104	.984	60	-.360	-.297		-.301	-.296	-.300	-.329	-.436
51	.503	30	-.016	.018		.015	.109	.213	.323	.432	105	.984	90	-.363	-.304		-.313	-.312	-.320	-.367	-.475
52	.503	50	-.410	.041		.032	.120	.220	.323	.427	106	.984	135	-.434	-.310		-.354	-.338	-.293	-.321	-.447
53	.503	F	-.258	-.086		.047	.133	.220	.302	.385	107	.984	180	-.372	-.387		-.421	-.406	-.362	-.403	-.523
54	.503	F	-.483	-.111		.046	-.006	-.113	-.203	-.382											

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(c) M = 0.95 - Concluded

Pressure coefficients C_p on -

Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage								Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage - Concluded						
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open											$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open							
1	.026	0			.173	.224	.323	.425	.543	.673	55	.503	F			.078	.039	.024	-.196	-.206	-.231
2	.026	90			.339	.344	.309	.230	.104	-.076	56	.503	135			.066	.026	.015	.047	.057	-.463
3	.026	180			.264	.214	.141	.097	.062	.030	57	.588	0			-.111	-.024	.107	.216	.330	.444
4	.084	0			.029	.067	.158	.257	.374	.509	58	.588	180			.042	-.029	-.194	-.310	-.382	-.551
5	.084	45			.109	.142	.218	.269	.319	.356	59	.604	15			-.151	-.048	.099	.215	.338	.458
6	.084	90			.171	.199	.148	.089	-.039	-.206	60	.604	30			-.047	-.043	.011	.093	.177	.357
7	.084	135			.169	.121	.024	-.082	-.209	-.360	61	.604	50			-.151	-.035	.128	.255	.380	.501
8	.084	180			.128	.083	.015	-.028	-.061	-.101	62	.604	F			-.176	-.044	.136	.274	.410	.536
9	.134	J			.151	.115	.066	.034	.014	-.022	63	.604	F			.046	-.063	-.304	-.573	-.739	-.952
10	.156	J			.327	.298	.245	.196	.134	.082	64	.604	135			.042	-.054	-.259	-.368	-.569	-.991
12	.173	30			-.085	-.034	.053	.130	.213	.304	65	.690	0			.027	.034	.077	.111	.210	.321
14	.173	90			.031	.050	.038	-.023	-.135	-.325	66	.690	180			.028	.014	-.122	-.353	-.569	-.735
15	.173	135			.134	.117	.077	.030	-.009	-.041	67	.706	15			.072	.077	.110	.115	.204	.313
16	.173	J			.241	.220	.187	.152	.108	.058	68	.706	30			.096	.099	.130	.129	.218	.325
17	.173	C			.290	.262	.225	.205	.212	.227	69	.706	50			.128	.127	.148	.135	.219	.320
18	.190	J			.131	.122	.103	.065	.011	-.055	70	.706	F			.145	.143	.159	.138	.220	.320
19	.190	C			.118	.095	.067	.055	.073	.118	71	.706	F			.107	.103	.067	-.290	-.661	-.855
20	.197	C			-.272	-.305	-.340	-.350	-.342	-.322	72	.706	135			.099	.090	.065	-.316	-.450	-.893
21	.207	C			.002	-.008	-.023	-.021	.010	.035	73	.753	0			.194	.211	.229	.193	.225	.307
23	.216	C			-.407	-.439	-.473	-.478	-.471	-.465	74	.753	180			.210	.201	.183	.069	-.180	-.593
24	.226	23			-.176	-.131	-.040	.047	.150	.262	75	.770	15			.398	.404	.415	.365	.370	.431
25	.226	45			-.156	-.102	-.020	.037	.089	.131	76	.770	30			.318	.324	.335	.274	.270	.332
26	.226	68			-.163	-.112	-.059	-.047	-.064	-.122	77	.770	50			.270	.275	.285	.202	.182	.235
27	.226	90			-.149	-.112	-.089	-.109	-.170	-.259	78	.770	F			.256	.260	.266	.148	.087	.117
28	.226	135			-.318	-.306	-.295	-.290	-.293	-.321	79	.770	F			.292	.293	.284	.052	-.123	-.325
29	.226	C			-.763	-.854	-.888	-.884	-.854	-.787	80	.770	F			.262	.262	.247	.068	-.243	-.495
30	.263	C			-.276	-.303	-.254	-.153	-.096	-.111	81	.770	135			.288	.284	.266	.114	-.086	-.723
31	.283	0			-.114	-.166	-.160	-.052	.064	.204	83	.820	38			.315	.316	.320	.296	.286	.327
32	.299	30			-.140	-.104	-.091	-.014	.096	.215	84	.820	F			.286	.291	.301	.295	.297	.344
33	.299	60			-.147	-.101	-.100	-.014	.089	.187	85	.820	F			.266	.271	.286	.287	.290	.335
34	.299	F			-.164	-.096	-.117	-.041	.027	.077	86	.820	F			.267	.273	.292	.307	.311	.358
35	.299	F			-.031	-.022	-.232	-.278	-.349	-.450	87	.820	F			.277	.280	.299	.350	.391	.461
36	.299	F			-.047	-.103	-.383	-.702	-.862	-1.090	88	.820	F			.268	.265	.234	-.018	-.365	-.830
37	.299	135			-.046	-.080	-.105	-.194	-.313	-.428	89	.820	F			.263	.262	.242	.075	-.169	-.560
38	.319	C			.005	.000	-.021	-.043	-.064	-.130	90	.820	F			.273	.275	.258	.108	-.167	-.301
39	.350	20			-.061	-.041	.015	.077	.158	.284	91	.820	F			.290	.293	.280	.146	-.097	-.311
40	.350	40			-.070	-.036	.027	.084	.142	.241	92	.820	142			.322	.328	.325	.188	-.005	-.565
41	.350	60			-.072	-.036	.027	.092	.152	.264	93	.820	165			.353	.357	.344	.233	.048	-.066
42	.350	F			-.098	-.042	.034	.081	.078	.141	94	.897	30			.499	.507	.517	.537	.551	.577
43	.350	F			-.014	.008	-.047	-.186	-.519	-.657	95	.897	50			.410	.416	.421	.440	.461	.495
44	.350	F			.001	-.038	-.123	-.190	-.491	-.932	96	.897	F			.328	.334	.342	.372	.397	.431
45	.350	135			.016	-.011	-.046	-.042	-.045	-.100	97	.897	F			.289	.294	.265	.163	-.055	-.317
46	.367	0			-.055	-.049	-.011	.050	.136	.258	98	.897	130			.385	.394	.374	.271	.099	-.360
47	.367	180			.002	-.013	-.023	-.016	.005	-.026	99	.897	150			.501	.504	.471	.390	.229	-.059
48	.486	0			-.014	-.008	.054	.141	.249	.369	102	.984	0			-.575	-.578	-.566	-.533	-.517	-.512
49	.486	180			.013	-.004	-.009	-.024	.008	-.072	104	.984	60			-.698	-.697	-.676	-.649	-.659	-.614
50	.503	15			-.033	-.024	.007	.063	.131	.309	105	.984	90			-.726	-.729	-.713	-.710	-.731	-.704
51	.503	30			-.009	.020	.113	.213	.320	.428	106	.984	135			-.858	-.855	-.775	-.624	-.663	-.701
52	.503	50			.013	.036	.125	.219	.320	.424	107	.984	180			-.615	-.616	-.611	-.588	-.608	-.640
53	.503	F			.027	.051	.137	.220	.302	.382											
54	.503	F			.046	.059	.011	-.100	-.195	-.386											

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(d) M = 1.03

Pressure coefficients C_p on -

Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage								Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage - Concluded							
			$\alpha = -20^\circ$	$\alpha = -10^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 15^\circ$	$\alpha = 20^\circ$				$\alpha = -20^\circ$	$\alpha = -10^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 15^\circ$	$\alpha = 20^\circ$
			$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed											$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed							
1	.026	0				.311	.393	.492	.593	.702	55	.503	F				-.049	-.005	.020	-.078	-.174
2	.026	90				.289	.248	.160	.054	-.114	56	.503	135				-.056	.003	.122	.009	-.300
3	.026	180				.308	.231	.179	.145	.126	57	.588	0				.018	.157	.301	.408	.504
4	.084	0				.158	.234	.324	.424	.536	58	.588	180				.020	-.104	-.188	-.264	-.367
5	.084	45				.139	.153	.126	.123	.114	59	.604	15				.007	.140	.280	.382	.471
6	.084	90				.135	.107	.028	-.077	-.274	60	.604	30				.014	.156	.298	.396	.479
7	.084	135				.115	.081	.028	-.037	-.102	61	.604	50				.010	.162	.320	.430	.521
8	.084	180				.162	.103	.049	.014	-.034	62	.604	F				.013	.179	.352	.472	.568
9	.134	J				.207	.148	.104	.049	-.051	63	.604	F				.001	-.177	-.341	-.662	-.780
10	.156	J				.167	.128	.111	.124	.152	64	.604	135				.011	-.147	-.295	-.451	-.603
12	.173	30				.009	.029	.044	.067	.113	65	.690	0				-.122	.007	.184	.289	.385
13	.173	60				.005	-.005	-.058	-.148	-.227	66	.690	180				-.119	-.262	-.385	-.526	-.667
14	.173	90				.011	.001	-.060	-.170	-.387	67	.706	15				-.143	-.017	.163	.254	.342
15	.173	135				.042	.046	.036	.012	-.041	68	.706	30				-.140	-.007	.169	.256	.339
16	.173	J				.097	.077	.078	.105	.122	69	.706	50				-.138	.007	.182	.272	.358
17	.173	C				.136	.102	.085	.093	.089	70	.706	F				-.137	.018	.195	.285	.370
18	.190	J				.010	.016	.031	.070	.057	71	.706	F				-.165	-.309	-.442	-.678	-.869
19	.190	C				.005	-.017	-.020	-.007	.027	72	.706	135				-.146	-.292	-.417	-.548	-.723
20	.197	C				-.158	-.207	-.236	-.237	-.223	73	.753	0				.131	.196	.251	.292	.364
21	.207	C				-.052	-.059	-.060	-.043	.029	74	.753	180				.085	.021	-.148	-.568	-.657
23	.216	C				-.294	-.332	-.355	-.349	-.339	75	.770	15				.032	.086	.137	.172	.212
24	.226	23				-.060	-.031	-.002	.052	.094	76	.770	30				.029	.066	.102	.135	.178
25	.226	45				-.059	-.055	-.070	-.081	-.132	77	.770	50				.028	.059	.080	.116	.167
26	.226	68				-.086	-.088	-.139	-.210	-.386	78	.770	F				.062	.069	.037	.066	.117
27	.226	90				-.113	-.096	-.133	-.204	-.218	79	.770	F				.087	.114	.003	-.246	-.477
28	.226	135				-.340	-.305	-.275	-.291	-.344	80	.770	F				.054	.055	-.030	-.610	-.749
29	.226	C				-.465	-.520	-.615	-.682	-.708	81	.770	135				.027	.041	-.123	-.561	-.734
30	.263	C				-.294	-.291	-.255	-.190	-.150	82	.820	15				.036	.030	-.070	-.113	.028
31	.283	0				-.151	-.088	-.014	.071	.208	83	.820	38				.046	.058	-.022	-.070	.030
32	.299	30				-.148	-.123	-.089	-.113	.031	84	.820	F				.055	.068	.016	.029	.073
33	.299	60				-.133	-.103	-.049	.023	.113	85	.820	F				.074	.086	.034	.065	.095
34	.299	F				-.132	-.110	-.088	-.040	.019	86	.820	F								
35	.299	F				-.114	-.195	-.358	-.423	-.497	87	.820	F				.134	.143	.113	.137	.303
36	.299	F				-.136	-.263	-.476	-.791	-.916	88	.820	F				.065	.077	-.021	-.065	-.211
37	.299	135				-.083	-.131	-.201	-.265	-.286	89	.820	F				.057	.078	-.013	-.048	-.094
38	.319	C				-.071	-.124	-.198	-.246	-.294	90	.820	F				.050	.066	-.004	-.021	-.077
39	.350	20				-.114	-.119	-.081	.003	.156	91	.820	F				.027	.055	.001	.037	-.047
40	.350	40				-.095	-.104	-.106	-.039	.087	92	.820	142				-.003	-.003	-.004	-.004	-.004
41	.350	60				-.090	-.072	-.056	.037	.190	94	.897	30				-.014	.000	.008	.046	.152
42	.350	F				-.093	-.080	-.123	-.073	.039	95	.897	50				-.017	-.005	.007	.058	.169
43	.350	F				-.084	-.182	-.388	-.689	-.755	96	.897	F				-.014	-.002	.013	.069	.184
44	.350	F				-.052	-.116	-.251	-.714	-.985	97	.897	F				-.026	-.055	-.149	-.197	-.291
45	.350	135				-.016	-.040	-.102	-.141	.004	98	.897	130				-.011	-.032	-.114	-.138	-.227
46	.367	C				-.110	-.092	-.032	.081	.266	99	.897	150				-.013	-.028	-.097	-.121	-.179
47	.367	180				-.032	-.063	-.074	.016		102	.984	0				-.359	-.387	-.408	-.390	-.368
48	.486	0				-.070	-.051	.181	.311	.412	104	.984	60				-.307	-.331	-.381	-.461	-.565
49	.486	180				-.077	-.083	.077	.126	.110	105	.984	90				-.329	-.352	-.407	-.478	-.552
50	.503	15				-.064	-.039	.198	.299	.385	106	.984	135				-.345	-.414	-.463	-.536	-.633
51	.503	30				-.057	-.030	.183	.266	.335	107	.984	180				-.417	-.447	-.507	-.553	-.617
52	.503	50				-.050	.009	.213	.300	.373											
53	.503	F				-.044	.014	.204	.272	.332											
54	.503	F				-.054	-.030	.000	-.108	-.116											

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(d) M = 1.03 - Continued

Pressure coefficients C_p on -

Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage								Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage - Concluded							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx -5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open											$\beta \approx -5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open							
1	.026	0	.128	.176	.264	.315	.397	.496	.596	.708	55	.503	F	.324	.208	-.045	-.048	.009	.012	-.078	-.179
2	.026	90	-.134	.156	.260	.289	.234	.159	.048	-.124	56	.503	135	.341	.203	-.054	-.055	.020	.124	.004	-.316
3	.026	180	.726	.510	.354	.303	.221	.176	.141	.122	57	.588	0	-.375	-.199	-.051	.028	.170	.308	.414	.511
4	.084	0	-.026	.059	.123	.161	.236	.328	.428	.542	58	.588	180	.510	.309	.096	.014	-.109	-.189	-.263	-.377
5	.084	45	-.092	.058	.122	.131	.150	.129	.121	.113	59	.604	15	-.393	-.230	-.070	.016	.153	.287	.388	.479
6	.084	90	-.291	.025	.119	.135	.103	.028	-.082	-.284	60	.604	30	-.460	-.237	-.066	.022	.170	.305	.401	.484
7	.084	135	.110	.119	.123	.115	.076	.027	-.038	-.105	61	.604	50	-.574	-.281	-.071	.019	.177	.328	.436	.528
8	.084	180	.565	.352	.204	.158	.099	.050	.012	-.035	62	.604	F	-.775	-.363	-.095	.021	.195	.360	.478	.575
9	.134	J	.551	.365	.240	.203	.141	.106	.045	-.056	63	.604	F	.576	.363	.103	-.006	-.186	-.331	-.673	-.784
10	.156	J	.407	.260	.185	.166	.123	.115	.125	.156	64	.604	135	.511	.324	.093	.004	-.156	-.302	-.457	-.610
12	.173	30	-.198	-.069	-.014	.011	.027	.047	.068	.117	65	.690	0	-.668	-.403	-.172	-.098	.076	.198	.298	.397
13	.173	60	-.271	-.109	-.017	.007	-.011	-.058	-.154	-.230	66	.690	180	.374	.171	-.045	-.123	-.273	-.388	-.512	-.666
14	.173	90	-.455	-.148	-.011	.013	-.004	-.061	-.180	-.396	67	.706	15	-.590	-.411	-.013	.013	.105	.180	.264	.355
15	.173	135	-.075	-.026	.026	.043	.042	.037	.009	-.040	68	.706	30	-.653	-.396	-.009	.030	.111	.185	.267	.352
16	.173	J			.101	.095	.075	.083	.106	.121	69	.706	50	-.722	-.409	-.011	.042	.118	.198	.283	.369
17	.173	C	.347	.205	.144	.135	.096	.087	.091	.093	70	.706	F	-.782	-.451	-.015	.038	.122	.208	.296	.381
18	.190	J	.099	.012	.006	.012	.015	.036	.071	.054	71	.706	F	.335	.154	.012	-.045	-.315	-.445	-.686	-.891
19	.190	C	.191	.071	.017	.004	-.020	-.017	-.008	.032	72	.706	135	.327	.151	.025	-.052	-.300	-.422	-.552	-.733
20	.197	C	.187	-.005	-.126	-.160	-.213	-.236	-.237	-.222	73	.753	0	-.656	-.137	.250	.290	.286	.281	.312	.387
21	.207	C	.049	-.036	-.054	-.052	-.062	-.059	-.041	.030	74	.753	180	.340	.238	.279	.264	.156	-.083	-.490	-.600
23	.216	C	.039	-.158	-.270	-.298	-.337	-.353	-.347	-.343	75	.770	15	-.555	-.133	.142	.148	.139	.146	.179	.218
24	.226	23	-.225	-.125	-.082	-.058	-.034	.000	.055	.099	76	.770	30	-.673	-.059	.177	.181	.150	.116	.143	.187
25	.226	45	-.323	-.158	-.078	-.057	-.058	-.067	-.078	-.132	77	.770	50	-.646	-.031	.189	.196	.173	.104	.125	.179
26	.226	68	-.414	-.232	-.111	-.085	-.092	-.139	-.215	-.392	78	.770	F	-.608	.040	.230	.220	.194	.084	.074	.127
27	.226	90	-.645	-.310	-.144	-.110	-.099	-.134	-.207	-.214	79	.770	F	-.679	-.052	.248	.239	.237	.072	-.187	-.382
28	.226	135	-.387	-.424	-.362	-.334	-.305	-.273	-.292	-.350	80	.770	F	.033	-.010	.202	.207	.184	.067	-.271	-.362
29	.226	C	-.233	-.349	-.437	-.469	-.526	-.618	-.684	-.706	81	.770	135	.128	.057	.162	.180	.172	.062	-.536	-.744
30	.263	C	-.046	-.270	-.298	-.295	-.292	-.251	-.184	-.152	82	.820	15	-.446	-.021	.203	.208	.199	.177	.190	.228
31	.283	0	-.221	-.190	-.181	-.148	-.087	-.010	.074	.217	83	.820	38	-.113	-.002	.203	.219	.220	.194	.209	.235
32	.299	30	-.264	-.152	-.156	-.148	-.124	-.085	-.111	.032	84	.820	F	-.041	.030	.215	.224	.227	.204	.232	.278
33	.299	60	-.176	-.211	-.153	-.132	-.105	-.047	.031	.117	85	.820	F	.005	.039	.231	.235	.238	.212	.240	.289
34	.299	F	-.452	-.316	-.165	-.132	-.115	-.088	-.037	.021	86	.820	F	-.036	.082						
35	.299	F	-.511	-.236							87	.820	F	-.041	.107	.270	.282	.272	.250	.282	.506
36	.299	F	-.010	-.050	-.087	-.136	-.267	-.469	-.799	-.917	88	.820	F	-.030	-.031	.203	.202	.188	.090	.032	-.237
37	.299	135			-.058	-.082	-.135	-.200	-.264	-.287	89	.820	F	-.038	-.040	.204	.200	.184	.087	.028	-.019
38	.319	C	.244	.018	-.053	-.076	-.131	-.198	-.249	-.248	90	.820	F	-.283	-.062	.201	.196	.174	.089	.035	.002
39	.350	20	.103	-.088	-.111	-.114	-.123	-.078	.013	.164	91	.820	F	-.240	-.087	.185	.188	.169	.094	.091	.068
40	.350	40	-.031	-.122	-.098	-.095	-.108	-.103	-.028	.094	92	.820	142	-.164	-.120	.173	.167	.157	.094	.090	.073
41	.350	60	.035	-.151	-.102	-.090	-.074	-.054	.048	.200	93	.820	165	-.090	-.142						
42	.350	F	-.759	-.211	-.112	-.092	-.083	-.127	-.065	.045	94	.897	30	-.135	-.092	.332	.385	.474	.499	.520	.559
43	.350	F	-.541	-.354	-.090	-.084	-.186	-.387	-.691	-.761	95	.897	50	-.154	-.117	.325	.339	.387	.411	.438	.484
44	.350	F	.073	-.033	-.033	-.056	-.124	-.254	-.727	-.984	96	.897	F	-.196	-.138	.287	.312	.346	.360	.388	.436
45	.350	135	.145	.014	-.003	-.017	-.046	-.104	-.122	.021	97	.897	F	-.063	-.069	.263	.244	.201	.187	.099	-.036
46	.367	0	.059	-.130	-.115	-.110	-.093	-.028	.097	.276	98	.897	130	-.052	-.069	.325	.343	.296	.313	.250	.129
47	.367	180	.336	.064	-.014	-.034	-.065	-.075	.046	.099	99	.897	150	-.053	-.083	.420	.382	.369	.411	.404	.284
48	.486	0	.088	.072	-.070	-.068	-.051	.189	.319	.420	102	.984	0	-.590	-.455	-.491	-.510	-.496	-.506	-.498	-.468
49	.486	180	.424	.195	-.075	-.077	-.084	.080	.124	.102	103	.984	30	-.591	-.449						
50	.503	15	.122	.160	-.052	-.063	-.014	.206	.304	.392	104	.984	60	-.460	-.376	-.653	-.627	-.653	-.635	-.702	-.738
51	.503	30	.016	.167	-.045	-.057	-.002	.190	.270	.340	105	.984	90	-.475	-.401	-.688	-.612	-.629	-.659	-.685	-.725
52	.503	50	-.249	.135	-.038	-.050	.034	.218	.304	.379	106	.984	135	-.513	-.478	-.732	-.605	-.698	-.852	-.804	-.705
53	.503	F	-.088	.037	-.032	-.043	.042	.209	.276	.337	107	.984	180	-.451	-.478	-.553	-.547	-.556	-.602	-.669	-.723
54	.503	F	-.094	.036	-.066	-.055	-.007	.002	-.118	-.119											

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(d) M = 1.03 - Continued

Pressure coefficients C_p on -

Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage								Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage - Concluded							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed											$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed							
1	.026	0	.140	.187		.325	.406	.503	.606	.719	55	.503	F	.382	.233		-.063	-.012	-.085	-.004	-.093
2	.026	90	-.014	.225		.335	.303	.233	.128	-.035	56	.503	135	.414	.238		-.059	.002	.149	.061	-.305
3	.026	180	.729	.508		.322	.254	.195	.160	.139	57	.588	0	-.227	-.164		.038	.182	.321	.430	.529
4	.084	0	.008	.062		.187	.265	.352	.451	.566	58	.588	180	.536	.327		.040	-.088	-.146	-.177	-.257
5	.084	45	-.119	.050		.178	.213	.254	.275	.289	59	.604	15	-.375	-.243		.020	.164	.306	.417	.517
6	.084	90	-.169	.064		.178	.145	.077	-.023	-.172	60	.604	30	-.625	-.253		.024	.174	.318	.430	.526
7	.084	135	.276	.218		.166	.097	.021	-.065	-.143	61	.604	50	-.708	-.274		.016	.173	.325	.443	.545
8	.084	180	.582	.365		.177	.117	.066	.033	.006	62	.604	F	-.778	-.383		.008	.182	.346	.472	.579
9	.134	J	.556	.362		.215	.159	.115	.063	-.010	63	.604	F	.589	.351		-.007	-.195	-.412	-.556	-.769
10	.156	J	.517	.367		.280	.231	.204	.188	.142	64	.604	135	.543	.326		.008	-.150	-.264	-.571	-.822
12	.173	30	-.195	-.088		.044	.088	.135	.172	.212	65	.690	0	-.593	-.375		-.106	.029	.189	.300	.402
13	.173	60	-.359	-.118		.044	.059	.039	-.020	-.071	66	.690	180	.390	.172		-.108	-.245	-.353	-.471	-.595
14	.173	90	-.367	-.089		.065	.050	-.010	-.107	-.333	67	.706	15	-.638	-.397		-.128	.006	.170	.274	.371
15	.173	135	.101	.103		.128	.107	.086	.063	.002	68	.706	30	-.655	-.485		-.125	.011	.176	.278	.372
16	.173	J	.376	.257		.208	.178	.167	.160	.130	69	.706	50	-.759	-.410		-.132	.010	.175	.278	.370
17	.173	C	.471	.323		.250	.214	.195	.199	.216	70	.706	F	-.835	-.457		-.134	.015	.182	.283	.374
18	.190	J	.214	.130		.120	.104	.097	.081	.045	71	.706	F	.338	.130		-.163	-.311	-.404	-.688	-.852
19	.190	C	.294	.160		.104	.075	.064	.074	.115	72	.706	135	.345	.139		-.145	-.291	-.410	-.608	-.851
20	.197	C	.209	.006		-.134	-.181	-.206	-.221	-.198	73	.753	0	-.637	-.438		.056	.138	.204	.270	.351
21	.207	C	.139	.043		.029	.012	.013	.034	.084	74	.753	180	.326	.170		-.030	-.231	-.410	-.539	-.620
23	.216	C	.066	-.144		-.268	-.307	-.333	-.345	-.323	75	.770	15	-.657	-.003		.189	.234	.253	.286	.346
24	.226	23	-.296	-.144		-.032	.021	.072	.130	.200	76	.770	30	-.704	-.061		.162	.186	.191	.218	.278
25	.226	45	-.324	-.189		-.027	.013	.030	.036	.025	77	.770	50	-.688	-.049		.143	.153	.142	.153	.217
26	.226	68	-.533	-.251		-.056	-.030	-.048	-.097	-.213	78	.770	F	-.718	.030		.148	.142	.106	.071	.133
27	.226	90	-.583	-.277		-.071	-.051	-.077	-.144	-.164	79	.770	F	-.003	-.003		.182	.122	.079	-.212	-.419
28	.226	135	-.282	-.333		-.269	-.247	-.230	-.234	-.293	80	.770	F	.046	.070		.136	.110	.043	-.241	-.437
29	.226	C	-.177	-.327		-.540	-.670	-.734	-.745	-.691	81	.770	135	.189	.115		.128	.084	-.111	-.617	-.833
30	.263	C	.091	-.174		-.241	-.245	-.231	-.212	-.088	82	.820	15	.159	.157		.178	.176	.135	.130	.195
31	.283	0	-.042	-.158		-.136	-.082	-.017	.090	.233	83	.820	38	.056	.137		.181	.184	.146	.142	.204
32	.299	30	-.233	-.203		-.136	-.081	-.007	.057	.162	84	.820	F	.108	.136		.182	.190	.159	.167	.246
33	.299	60	-.264	-.289		-.143	-.095	-.010	.066	.166	85	.820	F	-.058	.130		.179	.196	.162	.176	.253
34	.299	F	-.792	-.408		-.145	-.109	-.042	.010	.072	86	.820	F	-.109	.151		.199	.225	.194	.223	.315
35	.299	F	-.466	-.223		-.114	-.189	-.275	-.339	-.410	87	.820	F	-.116	.158		.216	.258	.233	.333	.486
36	.299	F	.020	-.039		-.171	-.329	-.618	-.753	-.920	88	.820	F	.057	.058		.166	.125	.041	-.294	-.477
37	.299	135	.154	.005		-.121	-.201	-.280	-.352	-.402	89	.820	F	.051	.057		.162	.144	.067	-.134	-.281
38	.319	C	.289	.051		-.067	-.102	-.139	-.182	-.199	90	.820	F	.026	.054		.163	.156	.099	-.075	-.062
39	.350	20	-.130	-.127		-.103	-.081	-.020	.077	.244	91	.820	F	-.013	.056		.165	.170	.120	-.042	-.069
40	.350	40	.001	-.147		-.101	-.082	-.041	.042	.184	92	.820	142				.168	.181	.144	.086	.025
41	.350	60	.037	-.185		-.113	-.076	-.031	.071	.236	93	.820	165	.058	.081						
42	.350	F	-.835	-.289		-.118	-.082	-.085	-.016	.103	94	.897	30	-.203	-.040		.010	.022	.028	.069	.174
43	.350	F	-.740	-.348		-.096	-.177	-.453	-.568	-.633	95	.897	50	-.201	-.048		.003	.015	.025	.084	.194
44	.350	F	.132	-.003		-.078	-.180	-.301	-.822	-.880	96	.897	F	-.330	-.057		-.006	.009	.024	.088	.201
45	.350	135	.232	.055		-.024	-.072	-.102	-.140	-.055	97	.897	F	-.003	-.003		.011	-.010	-.073	-.226	-.355
46	.367	0	.134	-.082		-.090	-.071	-.014	.089	.286	98	.897	130	-.014	-.035		.024	.010	-.048	-.140	-.308
47	.367	180	.358	.079		-.001	-.004	.002	.072	.164	99	.897	150	-.016	-.037		.025	.009	-.055	-.103	-.235
48	.486	0	.135	.158		-.057	-.037	.201	.332	.438	102	.984	0	-.548	-.441		-.328	-.356	-.380	-.367	-.343
49	.486	180	.446	.198		-.062	-.050	.152	.195	.206	103	.984	30	-.549	-.438		-.313	-.354	-.392	-.401	-.383
50	.503	15	.040	.142		-.054	-.003	.243	.354	.452	104	.984	60	-.469	-.374		-.261	-.296	-.382	-.471	-.544
51	.503	30	-.165	.147		-.054	.006	.238	.339	.424	105	.984	90	-.486	-.395		-.278	-.319	-.382	-.462	-.532
52	.503	50	-.214	.158		-.059	.019	.244	.343	.428	106	.984	135	-.479	-.442		-.347	-.411	-.461	-.536	-.615
53	.503	F	-.148	-.030		-.056	.022	.238	.318	.389	107	.984	180	-.410	-.430		-.369	-.417	-.476	-.528	-.560
54	.503	F	-.119	-.038		-.060	-.079	-.018	-.049	-.179											

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(d) M = 1.03 - Continued

Pressure coefficients C_p on -

Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage								Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage - Concluded						
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open											$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open							
1	.026	0			.290	.327	.411	.497	.597	.719	55	.503	F			-.044	-.062	-.016	-.093	-.010	-.083
2	.026	90			.334	.341	.311	.234	.131	-.026	56	.503	135			-.042	-.058	-.002	.140	.067	-.295
3	.026	180			.375	.325	.259	.193	.157	.143	57	.588	0			-.039	.038	.183	.313	.422	.529
4	.084	0			.152	.190	.270	.348	.443	.565	58	.588	180			.131	.041	-.082	-.152	-.182	-.250
5	.084	45			.160	.180	.222	.250	.277	.298	59	.604	15			-.064	.022	.166	.299	.411	.518
6	.084	90			.174	.183	.157	.079	-.025	-.161	60	.604	30			-.064	.026	.175	.312	.424	.528
7	.084	135			.202	.170	.106	.020	-.068	-.141	61	.604	50			-.079	.019	.175	.318	.437	.546
8	.084	180			.231	.183	.125	.065	.030	.011	62	.604	F			-.104	.010	.183	.339	.465	.580
9	.134	J			.260	.220	.163	.112	.060	-.004	63	.604	F			.112	-.010	-.191	-.412	-.556	-.761
10	.156	J			.314	.287	.242	.204	.186	.148	64	.604	135			.113	.010	-.144	-.265	-.566	-.821
12	.173	30			.014	.048	.097	.128	.172	.240	65	.690	0			-.182	-.104	.031	.184	.295	.403
13	.173	60			.022	.051	.071	.040	-.017	-.059	66	.690	180			-.025	-.106	-.240	-.356	-.469	-.586
14	.173	90			.050	.073	.060	-.008	-.097	-.321	67	.706	15			-.206	-.126	.007	.168	.272	.374
15	.173	135			.137	.136	.118	.085	.060	.009	68	.706	30			-.209	-.124	.013	.174	.275	.375
16	.173	J			.231	.216	.191	.165	.156	.137	69	.706	50			-.220	-.128	.012	.173	.273	.373
17	.173	C			.281	.258	.225	.198	.198	.225	70	.706	F			-.223	-.130	.017	.179	.279	.377
18	.190	J			.131	.128	.114	.097	.079	.053	71	.706	F			-.081	-.161	-.304	-.402	-.682	-.837
19	.190	C			.135	.113	.085	.064	.073	.122	72	.706	135			-.067	-.143	-.288	-.412	-.613	-.825
20	.197	C			-.096	-.133	-.176	-.218	-.228	-.196	73	.753	0			.064	.083	.147	.216	.277	.363
21	.207	C			.047	.036	.021	.013	.032	.087	74	.753	180			.059	.023	-.213	-.415	-.538	-.610
23	.216	C			-.233	-.268	-.308	-.337	-.351	-.319	75	.770	15			.206	.231	.263	.283	.311	.376
24	.226	23			-.058	-.027	.029	.070	.127	.203	76	.770	30			.187	.203	.215	.223	.243	.306
25	.226	45			-.057	-.018	.021	.029	.040	.033	77	.770	50			.177	.182	.179	.175	.178	.239
26	.226	68			-.088	-.051	-.021	-.049	-.098	-.184	78	.770	F			.176	.183	.163	.141	.094	.151
27	.226	90			-.103	-.064	-.041	-.077	-.146	-.162	79	.770	F			.169	.212	.126	.113	-.184	-.402
28	.226	135			-.278	-.261	-.238	-.233	-.237	-.287	80	.770	F			.174	.175	.125	.071	-.211	-.438
29	.226	C			-.458	-.541	-.668	-.738	-.749	-.690	81	.770	135			.182	.175	.104	-.078	-.377	-.774
30	.263	C			-.255	-.235	-.235	-.234	-.219	-.095	82	.820	15			.263	.253	.244	.209	.198	.260
31	.283	0			-.150	-.131	-.075	-.017	.085	.233	83	.820	38			.237	.234	.231	.197	.185	.245
32	.299	30			-.155	-.133	-.072	-.011	.052	.164	84	.820	F			.232	.229	.234	.204	.206	.286
33	.299	60			-.179	-.141	-.087	-.015	.060	.168	85	.820	F			.222	.223	.234	.202	.208	.281
34	.299	F			-.192	-.140	-.101	-.046	.005	.074	86	.820	F			.232	.236	.260	.226	.248	.334
35	.299	F			-.103	-.109	-.181	-.275	-.338	-.401	87	.820	F			.240	.250	.293	.262	.358	.492
36	.299	F			-.096	-.179	-.322	-.617	-.753	-.903	88	.820	F			.241	.203	.155	.079	-.186	-.284
37	.299	135			-.071	-.121	-.194	-.285	-.360	-.399	89	.820	F			.220	.205	.179	.103	-.062	-.142
38	.319	C			-.039	-.066	-.097	-.142	-.185	-.195	90	.820	F			.218	.208	.196	.142	-.033	-.049
39	.350	20			-.103	-.098	-.075	-.024	.072	.244	91	.820	F			.221	.218	.219	.170	.004	-.062
40	.350	40			-.111	-.099	-.076	-.044	.038	.188	92	.820	142			.234	.230	.241	.207	.135	.016
41	.350	60			-.127	-.108	-.071	-.036	.064	.236	94	.897	30			.053	.043	.047	.039	.068	.165
42	.350	F			-.150	-.114	-.076	-.087	-.019	.107	95	.897	50			.047	.038	.044	.042	.084	.192
43	.350	F			-.094	-.095	-.169	-.441	-.564	-.623	96	.897	F			.035	.028	.040	.043	.092	.203
44	.350	F			-.033	-.077	-.174	-.303	-.824	-.881	97	.897	F			.052	.047	.036	-.037	-.207	-.331
45	.350	135			.007	-.021	-.066	-.107	-.150	-.054	98	.897	130			.063	.062	.061	-.007	-.119	-.264
46	.367	0			-.086	-.085	-.066	-.018	.081	.285	99	.897	150			.058	.062	.058	-.011	-.087	-.198
47	.367	180			.019	.005	.003	-.005	.039	.165	102	.984	0			-.423	-.408	-.426	-.442	-.440	-.416
48	.486	0			-.052	-.053	-.032	.185	.325	.438	103	.984	30			-.420	-.405	-.432	-.468	-.485	-.467
49	.486	180			-.052	-.057	-.048	.142	.192	.208	104	.984	60			-.300	-.292	-.324	-.399	-.507	-.587
50	.503	15			-.042	-.052	-.009	.231	.348	.454	105	.984	90			-.318	-.312	-.351	-.419	-.506	-.576
51	.503	30			-.043	-.051	-.003	.228	.334	.428	106	.984	135			-.411	-.411	-.455	-.527	-.590	-.678
52	.503	50			-.046	-.056	.010	.232	.337	.431	107	.984	180			-.498	-.489	-.525	-.592	-.656	-.685
53	.503	F			-.051	-.053	.010	.228	.313	.390											
54	.503	F			-.083	-.061	-.096	-.026	-.054	-.183											

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(d) M = 1.03 - Continued

Pressure coefficients C_p on -

Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage								Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage - Concluded							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = -7.5°$; brakes closed											$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = -7.5°$; brakes closed							
1	.026	0			.288	.329	.411	.506	.604	.715	55	.503	F			-.046	-.062	-.016	-.078	-.005	-.086
2	.026	90			.327	.335	.306	.236	.132	-.032	56	.503	135			-.045	-.059	-.002	.148	.063	-.290
3	.026	180			.377	.325	.260	.200	.162	.139	57	.588	0			-.041	.038	.181	.321	.429	.526
4	.084	0			.151	.189	.270	.356	.451	.560	58	.588	180			.127	.041	-.080	-.143	-.171	-.250
5	.084	45			.161	.183	.218	.257	.274	.284	59	.604	15			-.067	.021	.166	.307	.416	.513
6	.084	90			.169	.178	.153	.080	-.018	-.168	60	.604	30			-.067	.024	.175	.320	.429	.523
7	.084	135			.197	.169	.105	.028	-.057	-.138	61	.604	50			-.081	.017	.175	.326	.442	.541
8	.084	180			.229	.182	.125	.074	.035	.006	62	.604	F			-.108	.009	.183	.347	.472	.576
9	.134	J			.261	.218	.163	.122	.067	-.010	63	.604	F			.110	-.004	-.187	-.397	-.544	-.757
10	.156	J			.305	.280	.232	.207	.190	.142	64	.604	135			.112	.012	-.142	-.256	-.551	-.807
12	.173	30			.004	.033	.086	.126	.164	.221	65	.690	0			-.186	-.105	.031	.193	.302	.400
13	.173	60			.019	.047	.066	.043	-.019	-.073	66	.690	180			-.026	-.105	-.236	-.343	-.458	-.578
14	.173	90			.047	.066	.057	-.005	-.094	-.329	67	.706	15			-.208	-.127	.007	.176	.277	.370
15	.173	135			.129	.129	.113	.090	.066	.004	68	.706	30			-.211	-.126	.011	.180	.281	.371
16	.173	J			.223	.209	.185	.169	.163	.131	69	.706	50			-.222	-.131	.010	.179	.280	.370
17	.173	C			.263	.239	.217	.197	.197	.211	70	.706	F			-.227	-.132	.015	.185	.285	.373
18	.190	J			.123	.119	.109	.101	.085	.046	71	.706	F			-.082	-.160	-.301	-.392	-.672	-.837
19	.190	C			.116	.107	.081	.066	.074	.110	72	.706	135			-.068	-.142	-.282	-.402	-.594	-.815
20	.197	C			-.094	-.131	-.177	-.209	-.221	-.200	73	.753	0			.048	.078	.140	.224	.281	.362
21	.207	C			.042	.031	.018	.014	.034	.080	74	.753	180			.017	-.001	-.260	-.401	-.521	-.602
23	.216	C			-.235	-.267	-.307	-.328	-.344	-.320	75	.770	15			.141	.170	.214	.257	.292	.348
24	.226	23			-.061	-.032	.028	.076	.128	.194	76	.770	30			.121	.142	.163	.194	.223	.277
25	.226	45			-.060	-.026	.020	.032	.038	.020	77	.770	50			.110	.120	.123	.138	.155	.212
26	.226	68			-.092	-.055	-.023	-.047	-.097	-.211	78	.770	F			.114	.126	.112	.093	.072	.131
27	.226	90			-.108	-.069	-.044	-.073	-.142	-.165	79	.770	F			.101	.161	.110	.074	-.214	-.450
28	.226	135			-.286	-.268	-.243	-.227	-.234	-.291	80	.770	F			.099	.114	.083	.027	-.258	-.448
29	.226	C			-.453	-.534	-.649	-.717	-.733	-.690	81	.770	135			.105	.102	.047	-.124	-.594	-.826
30	.263	C			-.269	-.242	-.236	-.229	-.215	-.106	82	.820	15			.074	.056	.015	-.130	-.162	.002
31	.283	0			-.152	-.133	-.075	-.008	.089	.227	83	.820	38			.097	.086	.066	-.030	-.077	.089
32	.299	30			-.154	-.134	-.073	-.005	.055	.155	84	.820	F			.110	.103	.094	.027	.010	.154
33	.299	60			-.179	-.143	-.088	-.009	.064	.162	85	.820	F			.113	.109	.109	.050	.046	.187
34	.299	F			-.194	-.145	-.105	-.041	.009	.068	86	.820	F			.139	.137	.150	.102	.126	.267
35	.299	F			-.105	-.112	-.172	-.273	-.336	-.409	87	.820	F			.157	.161	.185	.150	.246	.469
36	.299	F			-.095	-.167	-.318	-.610	-.742	-.909	88	.820	F			.139	.110	.084	.002	-.301	-.574
37	.299	135			-.071	-.118	-.188	-.270	-.343	-.397	89	.820	F			.108	.102	.102	.025	-.167	-.353
38	.319	C			-.043	-.068	-.096	-.138	-.178	-.197	90	.820	F			.091	.095	.104	.049	-.122	-.126
39	.350	20			-.102	-.099	-.077	-.019	.074	.236	91	.820	F			.070	.083	.105	.055	-.078	-.122
40	.350	40			-.110	-.099	-.077	-.041	.038	.178	92	.820	142			.045	.065	.093	.060	.026	-.035
41	.350	60			-.126	-.109	-.072	-.030	.068	.229	94	.897	30			-.019	-.017	.005	.022	.047	.150
42	.350	F			-.148	-.115	-.076	-.083	-.017	.097	95	.897	50			-.028	-.026	-.005	.017	.050	.165
43	.350	F			-.096	-.093	-.168	-.415	-.565	-.635	96	.897	F			-.036	-.032	-.008	.019	.057	.174
44	.350	F			-.035	-.075	-.169	-.292	-.789	-.878	97	.897	F			-.009	-.019	-.034	-.103	-.271	-.380
45	.350	135			.004	-.021	-.062	-.097	-.142	-.069	98	.897	130			.001	-.008	-.019	-.085	-.177	-.347
46	.367	0			-.087	-.086	-.066	-.011	.088	.281	99	.897	150			.005	-.001	-.017	-.087	-.147	-.258
47	.367	180			.017	.003	.001	.003	.052	.165	102	.984	0			-.409	-.401	-.433	-.422	-.412	-.419
48	.486	0			-.054	-.054	-.032	.193	.330	.434	103	.984	30			-.370	-.362	-.417	-.435	-.447	-.443
49	.486	180			-.053	-.060	-.048	.150	.199	.206	104	.984	60			-.304	-.291	-.316	-.380	-.453	-.540
50	.503	15			-.045	-.052	-.010	.238	.353	.447	105	.984	90			-.314	-.304	-.335	-.399	-.471	-.537
51	.503	30			-.044	-.052	-.004	.233	.337	.419	106	.984	135			-.353	-.329	-.400	-.439	-.541	-.622
52	.503	50			-.048	-.056	.010	.239	.341	.423	107	.984	180			-.490	-.476	-.512	-.571	-.634	-.688
53	.503	F			-.053	-.053	.012	.233	.317	.383											
54	.503	F			-.087	-.060	-.093	-.019	-.044	-.181											

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(d) M = 1.03 - Continued

Pressure coefficients C_p on -

Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage							Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage - Concluded						
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15° α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15° α = 20°
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 7.5°$; brakes closed										$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 7.5°$; brakes closed						
1	.026	0			.289	.329	.412	.505	.604 .716	55	.503	F			-.048	-.062	-.012	-.080	-.005 -.088
2	.026	90			.329	.338	.304	.241	.133 -.032	56	.503	135			-.045	-.058	.003	.149	.075 -.295
3	.026	180			.374	.325	.255	.202	.161 .138	57	.588	0			-.039	.039	.187	.323	.429 .528
4	.084	0			.151	.189	.270	.356	.451 .562	58	.588	180			.125	.043	-.085	-.143	-.174 -.254
5	.084	45			.161	.181	.218	.258	.279 .289	59	.604	15			-.061	.022	.170	.309	.417 .516
6	.084	90			.171	.181	.148	.085	-.020 -.167	60	.604	30			-.063	.025	.180	.322	.430 .527
7	.084	135			.195	.168	.099	.028	-.060 -.142	61	.604	50			-.078	.018	.179	.328	.443 .545
8	.084	180			.227	.183	.120	.071	.035 .006	62	.604	F			-.106	.008	.188	.349	.472 .578
9	.134	J			.258	.217	.161	.121	.067 -.007	63	.604	F			.102	-.010	-.199	-.396	-.560 -.769
10	.156	J			.306	.283	.237	.210	.193 .146	64	.604	135			.106	.011	-.149	-.257	-.560 -.821
12	.173	30			.015	.045	.096	.135	.176 .231	65	.690	0			-.179	-.093	.048	.199	.301 .405
13	.173	60			.021	.049	.067	.046	-.014 -.068	66	.690	180			-.027	-.104	-.245	-.347	-.459 -.589
14	.173	90			.048	.069	.057	-.002	-.086 -.327	67	.706	15			-.127	-.028	.069	.186	.276 .375
15	.173	135			.132	.131	.114	.092	.064 .008	68	.706	30			-.116	-.022	.072	.190	.279 .375
16	.173	J			.223	.212	.185	.171	.164 .134	69	.706	50			-.097	-.011	.072	.189	.278 .373
17	.173	C			.277	.255	.220	.202	.202 .221	70	.706	F			-.078	-.009	.075	.195	.284 .378
18	.190	J			.124	.123	.111	.104	.085 .050	71	.706	F			-.051	-.097	-.262	-.396	-.646 -.848
19	.190	C			.128	.111	.081	.069	.076 .117	72	.706	135			-.036	-.084	-.286	-.403	-.601 -.835
20	.197	C			-.098	-.132	-.178	-.209	-.221 -.198	73	.753	0			.255	.273	.255	.248	.274 .366
21	.207	C			.041	.033	.018	.018	.035 .083	74	.753	180			.262	.267	.207	-.339	-.463 -.615
23	.216	C			-.236	-.268	-.309	-.330	-.344 -.323	75	.770	15			.302	.323	.322	.299	.292 .366
24	.226	23			-.060	-.029	.030	.076	.129 .200	76	.770	30			.285	.301	.281	.246	.225 .299
25	.226	45			-.052	-.019	.021	.034	.041 .022	77	.770	50			.279	.286	.256	.204	.161 .236
26	.226	68			-.089	-.051	-.024	-.045	-.094 -.138	78	.770	F			.284	.289	.249	.175	.079 .150
27	.226	90			-.105	-.068	-.045	-.072	-.140 -.180	79	.770	F			.290	.309	.234	.157	-.159 -.329
28	.226	135			-.285	-.268	-.241	-.227	-.230 -.295	80	.770	F			.266	.276	.218	.115	-.405 -.403
29	.226	C			-.462	-.537	-.663	-.728	-.742 -.699	81	.770	135			.270	.275	.220	-.005	-.320 -.659
30	.263	C			-.257	-.236	-.234	-.229	-.211 -.092	82	.820	15			.319	.318	.309	.270	.224 .299
31	.283	0			-.153	-.132	-.073	-.010	.093 .231	83	.820	38			.312	.315	.310	.275	.227 .295
32	.299	30			-.154	-.132	-.071	-.004	.055 .159	84	.820	F			.313	.315	.314	.284	.251 .329
33	.299	60			-.178	-.141	-.086	-.008	.065 .164	85	.820	F			.308	.310	.317	.286	.253 .324
34	.299	F			-.187	-.140	-.100	-.040	.012 .068	86	.820	F			.319	.323	.339	.307	.285 .364
35	.299	F			-.105	-.111	-.182	-.270	-.335 -.411	87	.820	F			.330	.335	.364	.337	.369 .503
36	.299	F			-.108	-.173	-.335	-.608	-.765 -.921	88	.820	F			.298	.284	.237	.140	-.242 -.479
37	.299	135			-.075	-.119	-.192	-.274	-.348 -.400	89	.820	F			.287	.284	.256	.161	-.065 -.292
38	.319	C			-.045	-.066	-.095	-.137	-.178 -.191	90	.820	F			.290	.288	.265	.193	-.081 -.090
39	.350	20			-.104	-.098	-.073	-.018	.077 .241	91	.820	F			.289	.294	.279	.214	-.046 -.144
40	.350	40			-.111	-.099	-.076	-.039	.041 .183	92	.820	142			.293	.296	.286	.233	.078 -.029
41	.350	60			-.129	-.109	-.070	-.029	.070 .234	94	.897	30			.480	.496	.535	.548	.562 .594
42	.350	F			-.150	-.114	-.075	-.081	-.016 .102	95	.897	50			.418	.431	.449	.459	.482 .524
43	.350	F			-.095	-.093	-.175	-.418	-.565 -.634	96	.897	F			.360	.370	.391	.401	.418 .463
44	.350	F			-.036	-.075	-.173	-.295	-.812 -.883	97	.897	F			.319	.315	.288	.229	.046 -.134
45	.350	135			.003	-.021	-.063	-.099	-.138 -.050	98	.897	130			.401	.387	.384	.326	.243 .067
46	.367	0			-.089	-.086	-.064	-.011	.088 .285	99	.897	150			.507	.495	.493	.430	.415 .288
47	.367	180			.017	.005	.002	.003	.050 .165	102	.984	0			-.514	-.507	-.504	-.510	-.503 -.479
48	.486	0			-.054	-.054	-.032	.200	.331 .436	103	.984	30			-.457	-.450	-.463	-.491	-.496 -.513
49	.486	180			-.053	-.058	-.047	.152	.200 .203	104	.984	60			-.575	-.566	-.605	-.639	-.699 -.780
50	.503	15			-.045	-.052	-.002	.242	.354 .451	105	.984	90			-.529	-.540	-.577	-.678	-.679 -.749
51	.503	30			-.046	-.053	.004	.238	.339 .424	106	.984	135			-.780	-.817	-.731	-.698	-.789 -.722
52	.503	50			-.049	-.057	.015	.243	.343 .428	107	.984	180			-.565	-.568	-.584	-.634	-.691 -.701
53	.503	F			-.053	-.055	.020	.239	.319 .388										
54	.503	F			-.082	-.059	-.095	-.016	-.051 -.186										

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(d) M = 1.03 - Continued

Pressure coefficients c_p on -

Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage								Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage - Concluded							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed											$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed							
1	.026	0	.124	.170		.313	.413	.514	.618	.736	55	.503	F	.442	.292		-.065	.026	-.036	-.042	-.127
2	.026	90	.095	.317		.416	.374	.288	.165	-.003	56	.503	135	.479	.292		-.068	.042	.157	-.018	-.446
3	.026	180	.713	.501		.285	.213	.172	.140	.122	57	.588	0	-.382	-.206		.027	.174	.320	.424	.527
4	.084	0	-.041	.042		.160	.251	.347	.449	.571	58	.588	180	.515	.315		-.004	-.126	-.205	-.269	-.404
5	.084	45	-.281	.014		.232	.301	.348	.384	.416	59	.604	15	-.624	-.246		.006	.166	.322	.433	.542
6	.084	90	-.091	.142		.276	.215	.157	.017	-.137	60	.604	30	-.749	-.251		.083	.224	.380	.481	.571
7	.084	135	.415	.330		.189	.086	-.031	-.156	-.296	61	.604	50	-.776	-.274		.028	.201	.362	.476	.583
8	.084	180	.560	.347		.157	.091	.037	-.004	-.046	62	.604	F	-.792	-.479		.025	.212	.382	.505	.616
9	.134	J	.547	.361		.191	.137	.100	.025	-.054	63	.604	F	.604	.369		-.042	-.242	-.428	-.564	-.789
10	.156	J	.626	.486		.372	.316	.257	.186	.112	64	.604	135	.564	.342		-.030	-.191	-.293	-.691	-.821
12	.173	30	-.246	-.136		.067	.147	.211	.272	.353	65	.690	0	-.642	-.419		-.111	.032	.204	.303	.407
13	.173	60	-.448	-.135							66	.690	180	.376	.172		-.149	-.297	-.416	-.553	-.621
14	.173	90	-.279	-.019		.141	.114	.033	-.141	-.288	67	.706	15	-.799	-.421		-.129	.031	.198	.293	.397
15	.173	135	.255	.235		.204	.158	.110	.082	-.002	68	.706	30	-.935	-.416		-.117	.045	.212	.308	.407
16	.173	J	.495	.379		.303	.267	.225	.175	.127	69	.706	50	-.820	-.427		-.109	.054	.218	.310	.405
17	.173	C	.587	.453		.344	.306	.289	.297	.300	70	.706	F	-.780	-.427		-.113	.058	.223	.312	.407
18	.190	J	.337	.250		.211	.187	.138	.077	.034	71	.706	F	.354	.162		-.181	-.333	-.525	-.634	-.761
19	.190	C	.410	.279		.188	.158	.147	.166	.217	72	.706	135	.365	.171		-.164	-.313	-.424	-.739	-.891
20	.197	C	.168	-.023		-.198	-.233	-.244	-.238	-.211	73	.753	0	-.624	-.160		.147	.211	.246	.293	.376
21	.207	C	.239	.145		.102	.086	.090	.124	.177	74	.753	180	.338	.222		.092	.000	-.170	-.594	-.638
23	.216	C	.046	-.153		-.312	-.345	-.351	-.347	-.333	75	.770	15	-.493	.006		.366	.394	.394	.410	.479
24	.226	23	-.314	-.197		-.021	.060	.135	.206	.302	76	.770	30	-.695	.021		.295	.311	.299	.308	.383
25	.226	45	-.427	-.251		.010	.079	.122	.147	.163	77	.770	50	-.537	.067		.242	.253	.224	.213	.288
26	.226	68	-.616	-.269		-.001	.039	.034	-.007	-.110	78	.770	F	-.463	.128		.224	.225	.168	.107	.178
27	.226	90	-.494	-.231		.000	.012	-.025	-.103	-.086	79	.770	F	-.317	.139		.247	.207	.057	-.141	-.255
28	.226	135	-.151	-.235		-.180	-.171	-.174	-.196	-.274	80	.770	F	.069	.167		.222	.171	.022	-.278	-.514
29	.226	C	-.151	-.351		-.729	-.747	-.739	-.717	-.665	81	.770	135	.251	.230		.248	.167	.035	-.414	-.593
30	.263	C	-.031	-.264		-.312	-.276	-.245	-.181	-.113	82	.820	15	.033	.247						
31	.283	0	-.200	-.190		-.143	-.069	.011	.100	.253	83	.820	38	-.443	.227						
32	.299	30	-.225	-.284		-.144	-.051	.034	.130	.271	84	.820	F	-.114	.195		.274	.267	.236	.217	.299
33	.299	60	-.497	-.367		-.128	-.041	.045	.136	.253	85	.820	F	-.248	.163		.255	.256	.237	.229	.313
34	.299	F	-.904	-.478		-.112	-.042	.027	.086	.155	86	.820	F	-.249	.173		.240	.248	.229	.222	.306
35	.299	F	-.423	-.204		-.061	-.149	-.199	-.268	-.338	87	.820	F	-.343	.174		.254	.268	.253	.254	.336
36	.299	F	.082	-.007		-.192	-.468	-.598	-.764	-.919	88	.820	F	.103	.122		.269	.291	.297	.349	.455
37	.299	135	.224	.015		-.200	-.322	-.476	-.699	-.594	89	.820	F	-.010	.125		.240	.198	.061	-.241	-.577
38	.319	C	.251	.011		-.088	-.146	-.221	-.280	-.336	90	.820	F	-.047	.138		.240	.181	-.010	-.466	-.706
39	.350	20	-.130	-.164		-.122	-.065	.034	.163	.331	91	.820	F	.027	.158		.249	.216	.070	-.094	-.260
40	.350	40	.042	-.215		-.118	-.058	.033	.146	.293	92	.820	142				.264	.242	.161	-.120	-.223
41	.350	60	-.121	-.271		-.120	-.061	.029	.152	.314	93	.820	165	.198	.228		.295	.290	.219	-.040	-.520
42	.350	F	-.776	-.418		-.123	-.052	-.002	.086	.201	94	.897	30	-.326	-.022		.341	.337	.250	.191	-.064
43	.350	F	-.636	-.324		-.092	-.196	-.372	-.465	-.534	95	.897	50	-.283	-.029		.036	.053	.085	.151	.241
44	.350	F	.211	.040		-.140	-.293	-.705	-.946	-.894	96	.897	F	-.470	-.056		.023	.044	.086	.166	.260
45	.350	135	.309	.090		-.065	-.135	-.171	-.179	-.075	97	.897	F	.044	.009		.012	.039	.089	.176	.268
46	.367	0	.068	-.132		-.115	-.089	-.008	.127	.307	98	.897	130	.020	.019		.062	.042	-.068	-.289	-.387
47	.367	180	.346	.067		-.041	-.067	-.089	.048	.068	99	.897	150	.003	.017		.079	.068	-.004	-.256	-.494
48	.486	0	.077	.079		-.081	-.054	.217	.330	.444	102	.984	0	-.606	-.473		.078	.060	.006	-.163	-.441
49	.486	180	.430	.209		-.080	-.069	.087	.112	.053	103	.984	30	-.602	-.459		-.385	-.412	-.423	-.402	-.375
50	.503	15	.007	.132		-.070	.050	.282	.393	.503	104	.984	60	-.457	-.371		-.264	-.289	-.404	-.493	-.580
51	.503	30	-.019	.137		-.066	.070	.299	.401	.503	105	.984	90	-.492	-.394		-.279	-.313	-.406	-.487	-.574
52	.503	50	-.272	.149		-.055	.085	.306	.403	.499	106	.984	135	-.482	-.450		-.377	-.427	-.491	-.614	-.587
53	.503	F	-.136	-.131		-.045	.095	.306	.383	.461	107	.984	180	-.449	-.470		-.437	-.474	-.541	-.593	-.659
54	.503	F	-.276	-.028		-.044	-.046	-.021	-.076	-.231											

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(d) M = 1.03 - Concluded

Pressure coefficients C_p on -

Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage								Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage - Concluded							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open											$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open							
1	.026	0			.256	.307	.407	.505	.611	.727	55	.503	F			-.045	-.066	.018	-.057	-.037	-.118
2	.026	90			.413	.415	.378	.300	.180	.007	56	.503	135			-.052	-.071	.031	.158	.020	-.422
3	.026	180			.342	.289	.219	.179	.143	.123	57	.588	0			-.059	.019	.171	.313	.420	.524
4	.084	0			.118	.153	.247	.339	.443	.564	58	.588	180			.082	.002	-.115	-.197	-.265	-.408
5	.084	45			.190	.226	.298	.346	.385	.417	59	.604	15			-.089	-.001	.161	.313	.428	.538
6	.084	90			.249	.276	.221	.167	.031	-.127	60	.604	30			.135	.202	.272	.388	.473	.481
7	.084	135			.247	.193	.099	-.015	-.147	-.289	61	.604	50			-.090	.018	.194	.352	.471	.581
8	.084	180			.208	.159	.097	.045	.001	-.045	62	.604	F			-.115	.013	.205	.372	.499	.614
9	.134	J			.233	.193	.143	.106	.034	-.050	63	.604	F			.088	-.035	-.223	-.447	-.547	-.786
10	.156	J			.405	.373	.321	.266	.196	.123	64	.604	135			.083	-.025	-.178	-.262	-.652	-.816
12	.173	30			.008	.061	.147	.208	.269	.350	65	.690	0			-.183	-.105	.070	.201	.303	.408
14	.173	90			.121	.138	.123	.047	-.127	-.278	66	.690	180			-.067	-.141	-.283	-.399	-.541	-.618
15	.173	135			.223	.203	.164	.117	.084	.010	67	.706	15			-.107	-.031	.109	.200	.295	.401
16	.173	J			.325	.303	.272	.232	.184	.135	68	.706	30			-.115	-.026	.124	.213	.309	.412
17	.173	C			.373	.344	.311	.293	.299	.308	69	.706	50			-.066	-.004	.133	.220	.312	.410
18	.190	J			.222	.211	.192	.147	.084	.037	70	.706	F			-.023	-.001	.134	.223	.314	.410
19	.190	C			.211	.186	.161	.151	.166	.219	71	.706	F			-.074	-.127	-.309	-.487	-.383	-.713
20	.197	C			-.163	-.198	-.228	-.241	-.236	-.213	72	.706	135			-.055	-.123	-.300	-.412	-.534	-.890
21	.207	C			.111	.100	.089	.090	.124	.180	73	.753	0			.240	.279	.274	.268	.308	.391
23	.216	C			-.279	-.313	-.342	-.349	-.345	-.334	74	.753	180			.277	.261	.127	-.096	-.413	-.601
24	.226	23			-.080	-.029	.056	.129	.205	.300	75	.770	15			.453	.466	.459	.428	.437	.508
25	.226	45			-.057	.004	.085	.119	.149	.167	76	.770	30			.392	.399	.384	.340	.337	.414
26	.226	68			-.062	-.008	.039	.036	.000	-.091	77	.770	50			.349	.355	.334	.269	.245	.321
27	.226	90			-.045	-.006	.014	-.018	-.092	-.129	78	.770	F			.337	.341	.311	.217	.143	.209
28	.226	135			-.195	-.185	-.170	-.171	-.188	-.269	79	.770	F			.348	.357	.306	.111	-.108	-.181
29	.226	C			-.633	-.729	-.745	-.740	-.717	-.667	80	.770	F			.337	.340	.277	.108	-.229	-.387
30	.263	C			-.335	-.316	-.275	-.246	-.184	-.114	81	.770	135			.363	.363	.291	.117	-.552	-.511
31	.283	0			-.177	-.149	-.072	.004	.092	.247	83	.820	38			.409	.403	.388	.350	.332	.395
32	.299	30			-.193	-.151	-.055	.028	.125	.268	84	.820	F			.384	.382	.375	.350	.344	.409
33	.299	60			-.189	-.135	-.045	.040	.132	.250	85	.820	F			.367	.367	.365	.343	.338	.400
34	.299	F			-.191	-.119	-.041	.023	.085	.155	86	.820	F			.369	.372	.377	.363	.363	.420
35	.299	F			-.068	-.065	-.143	-.191	-.258	-.331	87	.820	F			.380	.380	.392	.404	.444	.519
36	.299	F			-.107	-.191	-.444	-.579	-.741	-.912	88	.820	F			.371	.354	.303	.069	-.419	-.681
37	.299	135			-.139	-.197	-.309	-.454	-.693	-.610	89	.820	F			.361	.356	.319	.154	-.227	-.513
38	.319	C			-.067	-.089	-.136	-.212	-.269	-.270	90	.820	F			.368	.368	.335	.177	-.067	-.264
39	.350	20			-.149	-.126	-.069	.026	.155	.326	91	.820	F			.380	.384	.359	.256	-.088	-.209
40	.350	40			-.162	-.124	-.059	.025	.140	.289	92	.820	142			.404	.414	.400	.315	-.015	-.461
41	.350	60			-.168	-.125	-.056	.021	.145	.309	93	.820	165			.437	.448	.444	.340	.216	-.060
42	.350	F			-.194	-.129	-.052	-.009	.081	.198	94	.897	30			.576	.583	.592	.598	.618	.648
43	.350	F			-.102	-.094	-.178	-.360	-.454	-.528	95	.897	50			.489	.494	.499	.505	.531	.569
44	.350	F			-.061	-.136	-.278	-.638	-.935	-.891	96	.897	F			.417	.423	.429	.439	.470	.507
45	.350	135			-.016	-.064	-.129	-.166	-.173	-.068	97	.897	F			.381	.381	.343	.234	-.023	-.158
46	.367	0			-.119	-.117	-.088	-.016	.117	.300	98	.897	130			.467	.471	.441	.355	.080	-.294
47	.367	180			-.020	-.042	-.064	-.083	.049	.075	99	.897	150			.581	.580	.548	.425	.322	.012
48	.486	0			-.080	-.083	-.054	.203	.326	.439	102	.984	0			-.515	-.524	-.506	-.512	-.495	-.460
49	.486	180			-.083	-.084	-.071	.085	.117	.064	104	.984	60			-.581	-.581	-.548	-.620	-.655	-.646
50	.503	15			.097	.135	.186	.296	.313	.224	105	.984	90			-.589	-.615	-.522	-.657	-.674	-.739
51	.503	30			-.081	-.069	.049	.288	.399	.500	106	.984	135			-.872	-.881	-.836	-.849	-.724	-.746
52	.503	50			-.068	-.059	.067	.295	.401	.497	107	.984	180			-.559	-.567	-.550	-.609	-.683	-.712
53	.503	F			-.071	-.050	.074	.297	.383	.459											
54	.503	F			-.068	-.046	-.076	-.010	-.067	-.240											

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(e) M = 1.18

Pressure coefficients C_p on -

Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage								Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage - Concluded							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx -5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed											$\beta \approx -5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed							
1	.026	0				.256	.332	.435	.551	.689	55	.503	F				-.041	-.064	-.199	-.457	-.319
2	.026	90				.241	.220	.135	-.008	-.201	56	.503	135				-.046	-.048	-.072	-.192	-.499
3	.026	180				.256	.200	.155	.122	.089	57	.588	0				.036	.152	.321	.430	.540
4	.084	0				.158	.212	.311	.423	.548	58	.588	180				.017	-.042	-.083	-.095	-.198
5	.084	45				.126	.137	.150	.138	.154	59	.604	15				.037	.191	.324	.425	.523
6	.084	90				.117	.097	.029	-.069	-.220	60	.604	30				.043	.203	.344	.446	.537
7	.084	135				.093	.065	.022	-.023	-.084	61	.604	50				.040	.201	.349	.463	.584
8	.084	180				.137	.085	.030	.000	-.030	62	.604	F				.043	.219	.390	.524	.640
9	.134	J				.098	.045	.016	-.007	-.085	63	.604	F				.047	-.080	-.220	-.454	-.567
10	.156	J				.181	.121	.093	.095	.117	64	.604	135				.051	-.060	-.158	-.245	-.397
12	.173	30				.004	.022	.050	.099	.155	65	.690	0				-.045	.094	.223	.364	.475
13	.173	60				.003	-.019	-.061	-.108	-.171	66	.690	180				-.033	-.151	-.263	-.369	-.415
14	.173	90				.030	-.006	-.078	-.189	-.364	67	.706	15				-.063	.069	.203	.340	.442
15	.173	135				.089	.070	.054	.001	-.069	68	.706	30				-.062	.073	.214	.347	.444
16	.173	J				.153	.115	.105	.119	.100	69	.706	50				-.063	.077	.224	.362	.465
17	.173	C				.194	.149	.125	.111	.083	70	.706	F				-.063	.086	.243	.380	.481
18	.190	J				.061	.060	.082	.102	.042	71	.706	F				-.066	-.187	-.303	-.474	-.614
19	.190	C				.060	.032	.039	.034	.040	72	.706	135				-.050	-.175	-.280	-.361	-.486
20	.197	C				-.078	-.127	-.153	-.171	-.192	73	.753	0				-.063	.083	.289	.401	.483
21	.207	C				.025	.027	.023	.023	.058	74	.753	180				-.080	-.193	-.305	-.406	-.411
23	.216	C				-.191	-.223	-.239	-.243	-.276	75	.770	15				.018	.164	.269	.322	.363
24	.226	23				-.019	-.010	.011	.061	.126	76	.770	30				-.020	.128	.233	.287	.330
25	.226	45				-.005	-.018	-.059	-.081	-.094	77	.770	50				-.046	.085	.196	.261	.317
26	.226	68				-.020	-.032	-.098	-.232	-.337	78	.770	F				-.060	.046	.153	.216	.272
27	.226	90				-.024	-.024	-.064	-.155	-.322	79	.770	F				.003	.000	-.069	-.160	-.277
28	.226	135				-.196	-.172	-.154	-.187	-.268	80	.770	F				-.077	-.178	-.315	-.379	-.510
29	.226	C				-.308	-.360	-.479	-.552	-.568	81	.770	135				-.072	-.205	-.318	-.396	-.513
30	.263	C				-.264	-.248	-.220	-.195	-.238	82	.820	15				-.053	-.041	-.004	.044	.100
31	.283	0				-.069	-.032	.009	.068	.159	83	.820	38				-.023	-.017	-.016	.005	.060
32	.299	30				-.078	-.066	-.090	-.120	-.084	84	.820	F				.000	.009	.015	.013	.066
33	.299	60				-.078	-.036	.019	.048	-.004	85	.820	F				.034	.040	.046	-.004	-.011
34	.299	F				-.083	-.052	-.002	.031	.054	86	.820	F								
35	.299	F				-.078	-.139	-.213	-.275	-.349	87	.820	F				.109	.142	.174	.156	.078
36	.299	F				-.110	-.204	-.422	-.549	-.634	88	.820	F				.065	.001	-.067	.010	-.223
37	.299	135				-.064	-.101	-.163	-.235	-.331	89	.820	F				.050	.008	-.011	.063	-.059
38	.319	C				-.079	-.126	-.182	-.233	-.259	90	.820	F				.034	.012	.028	.099	-.024
39	.350	20				-.091	-.066	-.012	.069	.017	91	.820	F				.005	-.002	.033	.074	-.077
40	.350	40				-.079	-.065	-.026	.038	.113	92	.820	142				.007	.188	.007	.181	.008
41	.350	60				-.075	-.043	.009	.095	.169	94	.897	30				.030	.044	.076	.146	.231
42	.350	F				-.078	-.060	-.045	.028	.113	95	.897	50				.024	.031	.068	.143	.247
43	.350	F				-.081	-.144	-.380	-.468	-.535	96	.897	F				.022	.030	.066	.148	.264
44	.350	F				-.059	-.118	-.222	-.620	-.726	97	.897	F				-.036	-.052	-.119	-.142	-.212
45	.350	135				-.007	-.038	-.091	-.145	-.239	98	.897	130				.007	.010	-.041	-.063	-.096
46	.367	0				-.089	-.048	.029	.132	.196	99	.897	150				.013	.023	-.002	-.006	-.025
47	.367	180				-.006	-.048	-.064	-.085	-.209	102	.984	0				-.320	-.322	-.297	-.261	-.226
48	.486	0				-.044	-.050	-.015	.082	.193	104	.984	60				-.227	-.223	-.236	-.310	-.389
49	.486	180				-.058	-.074	-.078	-.088	-.173	105	.984	90				-.248	-.242	-.259	-.324	-.381
50	.503	15				-.042	-.065	-.045	.028	.126	106	.984	135				-.296	-.278	-.294	-.373	-.456
51	.503	30				-.040	-.070	-.065	-.024	.068	107	.984	180				-.365	-.348	-.387	-.428	-.455
52	.503	50				-.038	-.059	-.049	-.015	.083											
53	.503	F				-.031	-.056	-.073	-.071	.017											
54	.503	F				-.041	-.112	-.264	-.308	-.227											

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(e) M = 1.18 - Continued

Pressure coefficients C_p on -

Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage								Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage - Concluded							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx -5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open											$\beta \approx -5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open							
1	.026	0	.083	.147	.214	.259	.343	.441	.560	.697	55	.503	F	.011	-.073	-.053	-.040	-.068	-.219	-.474	-.321
2	.026	90	-.217	.125	.242	.242	.217	.132	-.023	-.213	56	.503	135	.051	-.059	-.056	-.045	-.045	-.074	-.202	-.527
3	.026	180	.710	.441	.301	.254	.192	.151	.114	.086	57	.588	0	-.179	-.087	-.019	.038	.172	.327	.433	.545
4	.084	0	-.020	.035	.112	.157	.222	.316	.428	.554	58	.588	180	.549	.307	.080	.015	-.046	-.087	-.094	-.204
5	.084	45	-.076	.037	.102	.126	.142	.150	.136	.155	59	.604	15	-.180	-.108	-.030	.042	.208	.330	.427	.528
6	.084	90	-.246	.029	.109	.116	.095	.022	-.079	-.240	60	.604	30	-.249	-.112	-.024	.049	.220	.351	.449	.541
7	.084	135	.142	.109	.102	.093	.062	.020	-.029	-.093	61	.604	50	-.394	-.152	-.026	.045	.219	.356	.469	.590
8	.084	180	.572	.319	.185	.135	.080	.030	-.003	-.030	62	.604	F	-.577	-.244	-.049	.048	.236	.396	.529	.646
9	.134	J	.586	.330	.140	.096	.045	.015	-.008	-.095	63	.604	F	.649	.379	.137	.042	-.090	-.246	-.513	-.578
10	.156	J	.472	.298	.214	.182	.118	.093	.095	.115	64	.604	135	.580	.345	.127	.047	-.065	-.164	-.257	-.410
12	.173	30	-.145	-.019	-.009	.006	.027	.055	.103	.156	65	.690	0	-.478	-.271	-.123	-.040	.109	.229	.368	.480
13	.173	60	-.202	-.043	.004	.003	-.018	-.064	-.113	-.178	66	.690	180	.467	.217	.047	-.036	-.159	-.268	-.374	-.426
14	.173	90	-.396	-.062	.024	.030	-.011	-.088	-.204	-.386	67	.706	15	-.382	-.279	-.136	-.059	.084	.211	.344	.447
15	.173	135	.015	.051	.084	.088	.069	.049	-.005	-.078	68	.706	30	-.418	-.265	-.136	-.056	.089	.222	.352	.448
16	.173	J			.166	.151	.116	.102	.122	.092	69	.706	50	-.472	-.277	-.137	-.058	.094	.232	.367	.470
17	.173	C	.422	.271	.211	.195	.148	.124	.106	.082	70	.706	F	-.518	-.300	-.147	-.061	.104	.251	.385	.485
18	.190	J	.181	.073	.058	.062	.064	.083	.098	.033	71	.706	F	.451	.206	.018	-.068	-.196	-.311	-.489	-.638
19	.190	C	.272	.132	.077	.058	.034	.040	.027	.036	72	.706	135	.439	.200	.023	-.052	-.181	-.286	-.365	-.500
20	.197	C	.274	.067	-.038	-.079	-.128	-.154	-.176	-.199	73	.753	0	-.510	-.297	-.136	-.057	.105	.299	.407	.491
21	.207	C	.151	.061	.033	.025	.033	.022	.022	.057	74	.753	180	.465	.221	-.004	-.083	-.193	-.150	-.405	-.421
23	.216	C	.125	-.065	-.162	-.190	-.218	-.240	-.244	-.281	75	.770	15	-.394	-.208	-.071	.024	.182	.275	.324	.367
24	.226	23	-.114	-.044	-.021	-.018	-.008	.015	.062	.128	76	.770	30	-.435	-.286	-.091	-.015	.144	.237	.288	.332
25	.226	45	-.218	-.065	-.011	-.004	-.019	-.062	-.087	-.099	77	.770	50	-.418	-.257	-.111	-.039	.099	.200	.263	.320
26	.226	68	-.300	-.124	-.032	-.018	-.033	-.104	-.242	-.347	78	.770	F	-.379	-.247	-.115	-.055	.057	.157	.218	.274
27	.226	90	-.562	-.191	-.047	-.023	-.022	-.071	-.164	-.335	79	.770	F	-.408	-.039	.010	.003	-.002	-.075	-.164	-.295
28	.226	135	-.286	-.280	-.221	-.194	-.167	-.154	-.191	-.279	80	.770	F	.200	.086	-.024	-.078	-.184	-.321	-.384	-.525
29	.226	C	-.093	-.218	-.285	-.311	-.363	-.489	-.562	-.568	81	.770	135	.288	.172	.004	-.075	-.210	-.321	-.410	-.526
30	.263	C	.003	-.185	-.259	-.261	-.244	-.218	-.196	-.249	82	.820	15	-.418	-.184	.116	.090	-.034	-.001	.044	.100
31	.283	0	-.243	-.139	-.100	-.069	-.028	.009	.068	.164	83	.820	38	-.345	-.057	.116	.117	-.001	-.016	.006	.067
32	.299	30	-.289	-.108	-.094	-.074	-.065	-.095	-.126	-.084	84	.820	F	-.062	.013	.129	.119	.033	.020	.016	.093
33	.299	60	-.321	-.161	-.100	-.076	-.028	.021	.046	-.015	85	.820	F	.125	.040	.139	.123	.058	.051	.007	.025
34	.299	F	-.352	-.232	-.117	-.081	-.044	.000	.033	.052	86	.820	F	.111	.066						
35	.299	F	-.470	-.155							87	.820	F	.070	.065	.159	.158	.159	.184	.175	.280
36	.299	F	-.091	-.008	-.059	-.112	-.220	-.451	-.583	-.647	88	.820	F	.022	.115	.097	.079	.004	-.048	.023	-.209
37	.299	135			-.036	-.063	-.106	-.173	-.247	-.353	89	.820	F	-.011	.073	.074	.064	.012	.004	.068	-.061
38	.319	C	.073	-.076	-.071	-.080	-.129	-.185	-.246	-.264	90	.820	F	-.159	.023	.048	.050	.020	.038	.103	-.032
39	.350	20	-.101	-.074	-.098	-.090	-.061	-.007	.069	.016	91	.820	F	-.062	-.032	.001	.026	.010	.038	.075	-.075
40	.350	40	-.412	-.095	-.088	-.079	-.063	-.023	.040	.113	92	.820	142	.007	-.059	-.038	-.019	-.013	-.022	-.083	-.463
41	.350	60	-.320	-.127	-.092	-.073	-.040	.012	.098	.170	93	.820	165	.072	-.047						
42	.350	F	-.493	-.168	-.104	-.077	-.059	-.043	.031	.115	94	.897	30	.026	.057	.195	.287	.442	.522	.587	.658
43	.350	F	-.654	-.270	-.092	-.080	-.154	-.406	-.487	-.554	95	.897	50	-.015	.024	.213	.293	.374	.450	.513	.589
44	.350	F	.087	.021	-.029	-.060	-.125	-.243	-.657	-.738	96	.897	F	-.080	-.018	.197	.310	.378	.425	.476	.553
45	.350	135	.127	.072	.016	-.009	-.041	-.098	-.153	-.253	97	.897	F	.048	-.086	.288	.256	.215	.248	.197	.012
46	.367	0	-.197	-.114	-.107	-.088	-.040	.033	.133	.192	98	.897	130	.049	-.043	.309	.322	.301	.363	.316	.167
47	.367	180	.257	.108	.019	-.007	-.047	-.064	-.088	-.209	99	.897	150	-.008	-.030	.364	.293	.329	.420	.445	.316
48	.486	0	-.180	-.104	-.044	-.042	-.047	-.012	.084	.198	102	.984	0	-.417	-.345	-.353	-.384	-.369	-.358	-.337	-.299
49	.486	180	.185	.000	-.050	-.056	-.077	-.080	-.099	-.182	103	.984	30	-.415	-.331						
50	.503	15	-.141	-.032	-.036	-.044	-.063	-.043	.031	.138	104	.984	60	-.335	-.241	-.396	-.409	-.400	-.425	-.469	-.480
51	.503	30	-.185	-.026	-.031	-.041	-.069	-.063	-.021	.075	105	.984	90	-.349	-.257	-.425	-.201	-.283	-.466	-.509	-.515
52	.503	50	-.414	-.059	-.029	-.039	-.058	-.048	-.013	.087	106	.984	135	-.354	-.318	-.520	-.501	-.603	-.710	-.645	-.505
53	.503	F	-.340	-.215	-.031	-.031	-.057	-.073	-.071	.021	107	.984	180	-.348	-.378	-.431	-.403	-.406	-.452	-.515	-.540
54	.503	F	-.284	-.221	-.063	-.041	-.126	-.297	-.291	-.228											

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(e) M = 1.18 - Continued

Pressure coefficients C_p on -

Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage								Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage - Concluded							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed											$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed							
1	.026	0	.113	.166		.272	.356	.462	.577	.710	55	.503	F	.079	-.033		-.036	-.069	-.283	-.376	-.311
2	.026	90	-.049	.191		.280	.262	.210	.069	-.079	56	.503	135	.130	-.015		-.029	-.031	-.032	-.146	-.401
3	.026	180	.712	.463		.267	.213	.182	.153	.117	57	.588	0	.018	-.037		.030	.169	.358	.471	.585
4	.084	0	.006	.060		.167	.252	.353	.462	.583	58	.588	180	.592	.367		.041	-.023	-.021	.026	.027
5	.084	45	-.109	.052		.160	.202	.259	.297	.329	59	.604	15	-.142	-.120		.037	.203	.360	.475	.587
6	.084	90	-.123	.094		.158	.157	.108	.001	-.130	60	.604	30	-.442	-.135		.039	.209	.370	.489	.600
7	.084	135	.300	.217		.144	.093	.039	-.052	-.133	61	.604	50	-.491	-.167		.031	.206	.373	.496	.617
8	.084	180	.587	.357		.163	.109	.073	.031	.004	62	.604	F	-.519	-.231		.027	.211	.389	.527	.656
9	.134	J	.589	.344		.114	.073	.050	.011	-.014	63	.604	F	.663	.394		.011	-.127	-.275	-.506	-.546
10	.156	J	.577	.417		.287	.228	.189	.151	.098	64	.604	135	.615	.375		.024	-.080	-.146	-.341	-.684
12	.173	30	-.117	-.038		.027	.053	.113	.178	.269	65	.690	0	-.372	-.247		-.020	.133	.261	.394	.507
13	.173	60	-.272	-.059		.038	.053	.054	.022	-.008	66	.690	180	.491	.256		-.020	-.134	-.220	-.289	-.380
14	.173	90	-.276	-.018		.080	.034	-.026	-.131	-.279	67	.706	15	-.420	-.272		-.039	.109	.243	.376	.484
15	.173	135	.185	.177		.177	.142	.104	.057	-.022	68	.706	30	-.340	-.194		-.039	.110	.248	.380	.486
16	.173	J	.450	.330		.264	.223	.193	.167	.110	69	.706	50	-.532	-.283		-.048	.109	.249	.377	.485
17	.173	C	.541	.396		.313	.271	.240	.229	.230	70	.706	F	-.589	-.307		-.057	.109	.255	.385	.492
18	.190	J	.297	.201		.171	.160	.149	.118	.050	71	.706	F	.452	.221		-.060	-.176	-.283	-.566	-.612
19	.190	C	.372	.231		.157	.132	.125	.132	.151	72	.706	135	.457	.226		-.043	-.166	-.265	-.398	-.673
20	.197	C	.294	.089		-.063	-.104	-.126	-.152	-.147	73	.753	0	-.434	-.287		-.042	.115	.260	.389	.479
21	.207	C	.233	.143		.107	.105	.112	.134	.144	74	.753	180	.451	.196		-.066	-.171	-.261	-.345	-.422
23	.216	C	.149	-.038		-.159	-.185	-.208	-.225	-.217	75	.770	15	-.456	-.282		.059	.217	.347	.423	.490
24	.226	23	-.187	-.063		.006	.040	.084	.151	.233	76	.770	30	-.512	-.290		.001	.145	.277	.356	.424
25	.226	45	-.201	-.089		.016	.042	.038	.046	.065	77	.770	50	-.512	-.271		-.040	.084	.212	.291	.363
26	.226	68	-.415	-.150		.007	.023	-.009	-.111	-.175	78	.770	F	-.474	-.258		-.065	.030	.139	.215	.288
27	.226	90	-.449	-.170		.015	.028	-.003	-.094	-.353	79	.770	F	.008	.007		.039	.001	-.015	-.175	-.320
28	.226	135	-.181	-.190		-.137	-.113	-.102	-.130	-.231	80	.770	F	.210	.073		-.076	-.161	-.304	-.471	-.549
29	.226	C	-.042	-.203		-.415	-.520	-.569	-.581		81	.770	135	.339	.182		-.069	-.199	-.306	-.402	-.619
30	.263	C	-.030	-.179		-.202	-.187	-.170	-.141		82	.820	15	-.064	.162		.160	.151	.160	.171	.232
31	.283	0	-.105	-.110		-.063	-.018	.035	.096	.188	83	.820	38	-.046	.107		.170	.173	.183	.151	.188
32	.299	30	-.271	-.136		-.063	-.005	.043	.043		84	.820	F	-.023	.116		.175	.188	.213	.192	.190
33	.299	60	-.264	-.211		-.087	-.002	.080	.141	.162	85	.820	F	.024	.109		.175	.195	.226	.217	.153
34	.299	F	-.594	-.310		-.091	-.010	.061	.109	.137	86	.820	F	-.038	.130		.192	.224	.266	.269	.315
35	.299	F	-.415	-.156		-.047	-.094	-.121	-.180	-.259	87	.820	F	-.056	.133		.202	.252	.320	.326	.515
36	.299	F	.015	.005		-.115	-.268	-.407	-.519	-.671	88	.820	F	.173	.138		.157	.071	-.021	-.101	-.250
37	.299	135	-.004	.024		-.098	-.162	-.225	-.316	-.366	89	.820	F	.158	.123		.146	.094	.043	.005	-.137
38	.319	C	.071	-.012		-.063	-.088	-.111	-.155	-.183	90	.820	F	.008	.128		.148	.122	.080	.060	-.102
39	.350	20	-.311	-.106		-.050	-.001	.072	.152	.234	91	.820	F	.039	.129		.152	.136	.098	.183	-.062
40	.350	40	-.204	-.130		-.053	-.013	.052	.121	.190	92	.820	142				.153	.147	.096	.194	-.015
41	.350	60	-.226	-.168		-.065	-.018	.056	.140	.230	93	.820	165	.219	.139						
42	.350	F	-.659	-.262		-.078	-.030	.013	.071	.139	94	.897	30	-.103	.042		.069	.071	.099	.164	.253
43	.350	F	-.536	-.262		-.067	-.135	-.286	-.375	-.454	95	.897	50	-.120	.028		.057	.062	.093	.165	.264
44	.350	F	.131	.039		-.087	-.180	-.343	-.691	-.768	96	.897	F	-.250	.013		.044	.056	.088	.164	.269
45	.350	135	.210	.107		-.012	-.054	-.087	-.155	-.203	97	.897	F	.008	.007		.054	.044	-.014	-.140	-.262
46	.367	0	-.051	-.072		-.049	-.004	.078	.170	.273	98	.897	130	.105	.019		.069	.068	.019	-.100	-.235
47	.367	180	.299	.138		.042	.031	.018	-.008	-.028	99	.897	150	.103	.013		.074	.077	.022	-.051	-.143
48	.486	0	-.117	-.023		-.025	-.019	.011	.112	.225	102	.984	0	-.380	-.337		-.308	-.303	-.280	-.246	-.213
49	.486	180	.220	.034		-.030	-.021	-.017	-.015	-.067	103	.984	30	-.376	-.338		-.298	-.296	-.288	-.270	-.244
50	.503	15	-.190	-.047		-.019	-.004	.019	.090	.198	104	.984	60	-.322	-.260		-.221	-.228	-.266	-.325	-.387
51	.503	30	-.282	-.053		-.016	-.007	.012	.061	.160	105	.984	90	-.327	-.278		-.241	-.247	-.264	-.317	-.378
52	.503	50	-.355	-.058		-.021	-.017	.005	.042	.141	106	.984	135	-.303	-.293		-.286	-.299	-.325	-.389	-.467
53	.503	F	-.289	-.281		-.022	-.021	-.012	-.007	.081	107	.984	180	-.272	-.333		-.335	-.331	-.356	-.410	-.415
54	.503	F	-.216	-.315		-.027	-.114	-.253	-.263	-.229											

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(e) M = 1.18 - Continued

Pressure coefficients C_p on -

Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage								Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage - Concluded							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open											$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open							
1	.026	0			.242	.274	.351	.452	.566	.697	55	.503	F			-.017	-.031	-.072	-.295	-.380	-.321
2	.026	90			.279	.286	.260	.202	.065	-.084	56	.503	135			-.013	-.028	-.037	-.043	-.154	-.401
3	.026	180			.315	.269	.210	.170	.142	.109	57	.588	0			-.009	.028	.158	.344	.458	.570
4	.084	0			.131	.170	.248	.343	.450	.569	58	.588	180			.096	.041	-.027	-.033	.018	.019
5	.084	45			.149	.165	.201	.251	.292	.324	59	.604	15			-.020	.036	.190	.347	.462	.573
6	.084	90			.157	.162	.156	.099	-.006	-.132	60	.604	30			-.022	.037	.197	.358	.477	.587
7	.084	135			.176	.146	.092	.028	-.061	-.144	61	.604	50			-.036	.028	.194	.361	.484	.603
8	.084	180			.203	.165	.108	.063	.022	-.007	62	.604	F			-.058	.024	.198	.376	.514	.643
9	.134	J			.156	.116	.070	.038	.001	-.025	63	.604	F			.108	.013	-.125	-.279	-.499	-.553
10	.156	J			.321	.293	.228	.179	.142	.086	64	.604	135			.115	.027	-.085	-.156	-.350	-.691
12	.173	30			.007	.032	.079	.135	.194	.263	65	.690	0			-.094	-.021	.127	.249	.381	.494
13	.173	60			.033	.043	.053	.047	.019	-.012	66	.690	180			.064	-.020	-.138	-.233	-.296	-.383
14	.173	90			.075	.084	.033	-.036	-.135	-.282	67	.706	15			-.110	-.040	.103	.232	.365	.472
15	.173	135			.181	.182	.143	.094	.050	-.030	68	.706	30			-.112	-.040	.106	.236	.369	.474
16	.173	J			.283	.268	.223	.182	.157	.100	69	.706	50			-.124	-.048	.105	.238	.368	.473
17	.173	C			.338	.318	.272	.232	.225	.220	70	.706	F			-.138	-.056	.106	.243	.375	.480
18	.190	J			.181	.176	.160	.140	.110	.048	71	.706	F			.021	-.060	-.179	-.295	-.571	-.609
19	.190	C			.182	.163	.135	.120	.126	.141	72	.706	135			.035	-.045	-.168	-.275	-.408	-.676
20	.197	C			-.028	-.064	-.110	-.145	-.166	-.158	73	.753	0			-.129	-.042	.112	.257	.388	.475
21	.207	C			.125	.111	.104	.106	.127	.134	74	.753	180			.006	-.063	-.175	-.269	-.353	-.426
23	.216	C			-.129	-.162	-.195	-.220	-.237	-.228	75	.770	15			-.023	.068	.221	.349	.430	.496
24	.226	23			-.012	.010	.039	.077	.143	.224	76	.770	30			-.072	.011	.148	.279	.360	.429
25	.226	45			-.003	.021	.044	.035	.041	.061	77	.770	50			-.103	-.032	.086	.212	.294	.364
26	.226	68			-.013	.011	.022	-.016	-.115	-.184	78	.770	F			-.102	-.063	.028	.134	.214	.285
27	.226	90			-.008	.016	.026	-.011	-.101	-.359	79	.770	F			.036	.047	.003	-.011	-.170	-.296
28	.226	135			-.144	-.135	-.114	-.112	-.140	-.242	80	.770	F			-.044	-.065	-.151	-.310	-.483	-.357
29	.226	C			-.326	-.421	-.525	-.575	.007	-.570	81	.770	135			.001	-.054	-.191	-.258	-.408	-.618
30	.263	C			-.214	-.201	-.193	-.183	-.151	-.150	82	.820	15			.254	.261	.261	.261	.252	.298
31	.283	0			-.077	-.060	-.021	.028	.084	.175	83	.820	38			.236	.253	.255	.257	.238	.244
32	.299	30			-.087	-.061	-.008	.033	.044	.034	84	.820	F			.235	.253	.262	.274	.271	.273
33	.299	60			-.115	-.087	-.009	.069	.132	.158	85	.820	F			.228	.249	.260	.276	.285	.280
34	.299	F			-.128	-.092	-.022	.051	.101	.131	86	.820	F			.232	.261	.282	.305	.326	.378
35	.299	F			-.052	-.046	-.103	-.128	-.185	-.266	87	.820	F			.236	.270	.306	.343	.406	.568
36	.299	F			-.068	-.112	-.266	-.408	-.520	-.672	88	.820	F			.248	.231	.141	.035	-.056	-.263
37	.299	135			-.060	-.098	-.168	-.237	-.330	-.383	89	.820	F			.243	.226	.171	.097	.065	-.055
38	.319	C			-.046	-.064	-.094	-.119	-.164	-.192	90	.820	F			.237	.231	.199	.141	.099	-.080
39	.350	20			-.069	-.047	-.006	.064	.143	.223	91	.820	F			.241	.240	.214	.153	.214	-.039
40	.350	40			-.077	-.052	-.016	.045	.113	.180	92	.820	142			.256	.250	.228	.146	.277	.090
41	.350	60			-.093	-.065	-.022	.046	.130	.219	94	.897	30			.111	.106	.100	.104	.157	.236
42	.350	F			-.115	-.072	-.030	.008	.067	.132	95	.897	50			.099	.095	.095	.105	.165	.249
43	.350	F			-.079	-.065	-.130	-.288	-.377	-.456	96	.897	F			.086	.084	.089	.102	.165	.255
44	.350	F			-.041	-.086	-.183	-.360	.008	-.778	97	.897	F			.105	.104	.097	.060	-.079	-.212
45	.350	135			.018	-.011	-.060	-.099	-.165	-.211	98	.897	130			.112	.115	.117	.089	-.024	-.181
46	.367	0			-.068	-.048	-.007	.069	.162	.264	99	.897	150			.110	.119	.121	.092	.000	-.120
47	.367	180			.064	.045	.025	.007	-.016	-.045	102	.984	0			-.361	-.365	-.365	-.339	-.308	-.272
48	.486	0			-.035	-.028	-.025	-.002	.100	.209	103	.984	30			-.362	-.369	-.372	-.359	-.334	-.321
49	.486	180			-.030	-.033	-.031	-.028	-.028	-.079	104	.984	60			-.233	-.237	-.247	-.281	-.354	-.423
50	.503	15			-.027	-.020	-.014	.011	.081	.186	105	.984	90			-.249	-.258	-.267	-.290	-.352	-.412
51	.503	30			-.020	-.016	-.008	.004	.053	.149	106	.984	135			-.299	-.304	-.321	-.355	-.413	-.508
52	.503	50			-.030	-.019	-.019	-.004	.034	.129	107	.984	180			-.457	-.448	-.428	-.470	-.513	-.550
53	.503	F			-.033	-.020	-.022	-.021	-.015	.069											
54	.503	F			-.054	-.025	-.111	-.259	-.276	-.243											

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(e) M = 1.18 - Continued

Pressure coefficients C_p on -

Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage								Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage - Concluded							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = -7.5°$; brakes closed											$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = -7.5°$; brakes closed							
1	.026	0			.239	.276	.351	.451	.563	.693	55	.503	F			-.021	-.039	-.078	-.298	-.385	-.339
2	.026	90			.273	.281	.253	.195	.056	-.094	56	.503	135			-.019	-.031	-.038	-.045	-.164	-.403
3	.026	180			.317	.270	.207	.169	.140	.107	57	.588	0			-.005	.028	.162	.348	.458	.570
4	.084	0			.128	.167	.248	.343	.449	.568	58	.588	180			.100	.043	-.029	-.031	.020	.019
5	.084	45			.141	.167	.195	.254	.282	.310	59	.604	15			-.023	.036	.198	.349	.461	.571
6	.084	90			.152	.157	.157	.094	-.012	-.141	60	.604	30			-.025	.040	.206	.360	.476	.585
7	.084	135			.173	.144	.087	.023	-.061	-.137	61	.604	50			-.040	.032	.202	.363	.484	.602
8	.084	180			.206	.165	.106	.058	.019	-.007	62	.604	F			-.060	.031	.207	.380	.515	.642
9	.134	J			.160	.118	.067	.037	-.001	-.026	63	.604	F			.116	.017	-.129	-.279	-.508	-.546
10	.156	J			.314	.286	.220	.174	.137	.088	64	.604	135			.124	.028	-.086	-.155	-.343	-.661
12	.173	30			.008	.028	.079	.130	.184	.255	65	.690	0			-.099	-.024	.126	.249	.380	.494
13	.173	60			.031	.041	.047	.038	.006	-.022	66	.690	180			.069	-.017	-.140	-.228	-.292	-.379
14	.173	90			.073	.079	.028	-.040	-.143	-.283	67	.706	15			-.115	-.043	.104	.232	.364	.472
15	.173	135			.176	.177	.135	.092	.045	-.031	68	.706	30			-.117	-.043	.105	.237	.368	.473
16	.173	J			.274	.263	.213	.179	.152	.101	69	.706	50			-.128	-.052	.103	.238	.367	.473
17	.173	C			.318	.303	.261	.225	.209	.214	70	.706	F			-.143	-.060	.103	.244	.375	.479
18	.190	J			.174	.169	.152	.135	.107	.038	71	.706	F			.024	-.058	-.182	-.294	-.566	-.611
19	.190	C			.167	.157	.127	.111	.115	.131	72	.706	135			.039	-.040	-.172	-.276	-.398	-.660
20	.197	C			-.025	-.064	-.111	-.143	-.164	-.169	73	.753	0			-.135	-.047	.110	.259	.390	.476
21	.207	C			.122	.108	.098	.098	.120	.128	74	.753	180			.009	-.064	-.178	-.271	-.351	-.420
23	.216	C			-.127	-.160	-.197	-.220	-.235	-.227	75	.770	15			-.043	.053	.216	.347	.425	.485
24	.226	23			-.015	.008	.034	.074	.136	.215	76	.770	30			-.092	-.001	.145	.279	.357	.419
25	.226	45			-.006	.017	.040	.029	.031	.049	77	.770	50			-.119	-.044	.084	.212	.291	.356
26	.226	68			-.019	.008	.016	-.024	-.125	-.193	78	.770	F			-.115	-.068	.027	.136	.213	.281
27	.226	90			-.015	.015	.020	-.017	-.104	-.362	79	.770	F			.024	.036	-.009	-.028	-.194	-.330
28	.226	135			-.151	-.139	-.119	-.116	-.139	-.242	80	.770	F			-.044	-.075	-.175	-.314	-.474	-.569
29	.226	C			-.312	-.408	-.515	-.572	-.586	-.568	81	.770	135			.002	-.067	-.208	-.316	-.406	-.605
30	.263	C			-.217	-.210	-.193	-.184	-.161	-.151	82	.820	15			.025	.014	-.004	-.006	.000	.025
31	.283	0			-.081	-.062	-.021	.025	.084	.174	83	.820	38			.080	.081	.071	.059	.025	.052
32	.299	30			-.088	-.063	-.012	.040	.025	.023	84	.820	F			.103	.113	.115	.115	.073	.078
33	.299	60			-.115	-.085	-.003	.066	.125	.145	85	.820	F			.111	.128	.137	.146	.111	.013
34	.299	F			-.129	-.088	-.009	.047	.093	.122	86	.820	F			.135	.160	.183	.204	.183	.141
35	.299	F			-.055	-.045	-.099	-.137	-.195	-.274	87	.820	F			.150	.180	.221	.271	.244	.360
36	.299	F			-.064	-.110	-.257	-.417	-.526	-.661	88	.820	F			.160	.138	.040	-.054	-.136	-.271
37	.299	135			-.056	-.097	-.159	-.233	-.323	-.370	89	.820	F			.144	.124	.067	.013	-.036	-.184
38	.319	C			-.042	-.060	-.092	-.122	-.167	-.193	90	.820	F			.115	.112	.083	.047	.037	-.133
39	.350	20			-.073	-.051	-.009	.059	.137	.218	91	.820	F			.090	.093	.079	.052	.131	-.070
40	.350	40			-.081	-.054	-.019	.040	.106	.173	92	.820	142			.052	.062	.059	.022	.088	-.094
41	.350	60			-.097	-.068	-.023	.044	.125	.214	94	.897	30			.034	.042	.051	.082	.158	.240
42	.350	F			-.120	-.076	-.032	.005	.060	.126	95	.897	50			.022	.027	.035	.069	.155	.246
43	.350	F			-.085	-.068	-.144	-.301	-.389	-.465	96	.897	F			.006	.014	.024	.058	.155	.251
44	.350	F			-.043	-.085	-.183	-.348	-.682	-.762	97	.897	F			-.009	-.009	-.021	-.094	-.215	-.330
45	.350	135			.017	-.011	-.062	-.098	-.166	-.217	98	.897	130			.028	.025	.015	-.045	-.134	-.286
46	.367	0			-.071	-.048	-.009	.070	.158	.254	99	.897	150			.053	.048	.032	-.034	-.080	-.163
47	.367	180			.065	.042	.021	.008	-.015	-.041	102	.984	0			-.342	-.350	-.365	-.333	-.305	-.261
48	.486	0			-.026	-.022	-.021	.009	.100	.209	103	.984	30			-.333	-.345	-.367	-.343	-.328	-.303
49	.486	180			-.025	-.025	-.026	-.026	-.032	-.080	104	.984	60			-.251	-.249	-.257	-.274	-.340	-.408
50	.503	15			-.025	-.017	-.010	.007	.077	.182	105	.984	90			-.265	-.265	-.272	-.294	-.352	-.415
51	.503	30			-.026	-.016	-.015	-.002	.047	.143	106	.984	135			-.298	-.300	-.309	-.329	-.411	-.487
52	.503	50			-.032	-.021	-.025	-.008	.028	.123	107	.984	180			-.427	-.447	-.441	-.463	-.501	-.532
53	.503	F			-.037	-.023	-.030	-.026	-.021	.063											
54	.503	F			-.060	-.028	-.121	-.265	-.274	-.238											

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(e) M = 1.18 - Continued

Pressure coefficients C_p on -

Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage								Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage - Concluded						
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 7.5°$; brakes closed											$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 7.5°$; brakes closed							
1	.026	0			.242	.280	.357	.455	.571	.697	55	.503	F			-.015	-.030	-.070	-.287	-.376	-.303
2	.026	90			.279	.289	.263	.206	.067	-.084	56	.503	135			-.013	-.032	-.031	-.040	-.150	-.391
3	.026	180			.324	.278	.215	.178	.148	.112	57	.588	0			-.001	.033	.173	.351	.465	.573
4	.084	0			.131	.171	.254	.346	.454	.570	58	.588	180			.114	.051	-.020	-.030	.021	.018
5	.084	45			.147	.177	.203	.255	.293	.321	59	.604	15			-.019	.046	.210	.353	.469	.576
6	.084	90			.155	.165	.161	.096	-.004	-.129	60	.604	30			-.022	.049	.216	.364	.483	.589
7	.084	135			.181	.151	.100	.029	-.057	-.137	61	.604	50			-.037	.040	.211	.368	.491	.606
8	.084	180			.214	.169	.114	.064	.025	-.001	62	.604	F			-.061	.035	.216	.384	.522	.646
9	.134	J			.165	.125	.076	.043	.006	-.021	63	.604	F			.128	.025	-.126	-.266	-.489	-.546
10	.156	J			.326	.300	.230	.179	.145	.093	64	.604	135			.137	.036	-.075	-.151	-.339	-.667
12	.173	30			.016	.042	.095	.145	.200	.270	65	.690	0			-.096	-.021	.129	.253	.385	.494
13	.173	60			.036	.049	.056	.046	.019	-.010	66	.690	180			.080	-.009	-.132	-.228	-.292	-.380
14	.173	90			.080	.090	.040	-.032	-.133	-.273	67	.706	15			-.114	-.038	.107	.235	.368	.471
15	.173	135			.184	.182	.143	.097	.051	-.022	68	.706	30			-.117	-.039	.108	.240	.371	.474
16	.173	J			.283	.271	.222	.184	.160	.111	69	.706	50			-.130	-.051	.107	.241	.371	.473
17	.173	C			.341	.321	.269	.234	.223	.229	70	.706	F			-.143	-.059	.109	.247	.378	.480
18	.190	J			.183	.175	.160	.142	.113	.049	71	.706	F			.034	-.051	-.177	-.289	-.558	-.634
19	.190	C			.184	.164	.136	.121	.126	.140	72	.706	135			.049	-.034	-.166	-.269	-.401	-.657
20	.197	C			-.020	-.059	-.106	-.137	-.160	-.158	73	.753	0			-.132	-.045	.116	.253	.381	.466
21	.207	C			.127	.110	.105	.107	.128	.133	74	.753	180			.018	-.058	-.175	-.266	-.348	-.423
23	.216	C			-.122	-.157	-.191	-.214	-.230	-.226	75	.770	15			-.036	.057	.216	.338	.415	.478
24	.226	23			-.010	.012	.041	.082	.143	.220	76	.770	30			-.086	.000	.144	.268	.347	.413
25	.226	45			-.006	.022	.047	.039	.040	.059	77	.770	50			-.113	-.041	.083	.204	.283	.350
26	.226	68			-.016	.010	.024	-.014	-.114	-.179	78	.770	F			-.108	-.066	.029	.130	.208	.276
27	.226	90			-.012	.019	.027	-.008	-.093	-.353	79	.770	F			.040	.046	.002	-.020	-.176	-.322
28	.226	135			-.148	-.136	-.114	-.108	-.133	-.236	80	.770	F			-.038	-.067	-.156	-.308	-.476	-.566
29	.226	C			-.309	-.406	-.519	-.576	-.585	-.569	81	.770	135			.010	-.058	-.201	-.310	-.402	-.592
30	.263	C			-.210	-.197	-.188	-.176	-.151	-.143	82	.820	15			.232	.220	.177	.169	.178	.289
31	.283	0			-.073	-.057	-.012	.037	.091	.178	83	.820	38			.230	.226	.195	.190	.174	.292
32	.299	30			-.083	-.058	-.004	.051	.042	.033	84	.820	F			.230	.230	.211	.221	.235	.335
33	.299	60			-.112	-.081	.003	.072	.133	.159	85	.820	F			.221	.225	.215	.232	.261	.353
34	.299	F			-.129	-.086	-.005	.053	.099	.132	86	.820	F			.221	.235	.241	.269	.310	.434
35	.299	F			-.050	-.039	-.092	-.131	-.186	-.263	87	.820	F			.220	.240	.264	.316	.365	.599
36	.299	F			-.055	-.101	-.260	-.409	-.514	-.657	88	.820	F			.206	.195	.102	-.012	-.106	-.303
37	.299	135			-.049	-.091	-.155	-.228	-.319	-.374	89	.820	F			.196	.188	.129	.048	.012	-.073
38	.319	C			-.037	-.057	-.083	-.118	-.160	-.188	90	.820	F			.184	.193	.159	.089	.053	-.102
39	.350	20			-.069	-.046	-.001	.066	.144	.223	91	.820	F			.179	.198	.175	.112	.177	-.041
40	.350	40			-.077	-.052	-.014	.047	.114	.180	92	.820	142			.173	.197	.182	.108	.202	.032
41	.350	60			-.094	-.064	-.020	.050	.132	.220	94	.897	30			.470	.506	.564	.604	.648	.699
42	.350	F			-.117	-.073	-.029	.011	.068	.133	95	.897	50			.429	.455	.488	.520	.569	.631
43	.350	F			-.081	-.064	-.137	-.288	-.375	-.453	96	.897	F			.389	.416	.446	.478	.518	.572
44	.350	F			-.035	-.076	-.174	-.344	-.677	-.767	97	.897	F			.370	.362	.348	.317	.155	-.023
45	.350	135			.025	-.005	-.057	-.095	-.157	-.206	98	.897	130			.444	.420	.423	.401	.341	.151
46	.367	0			-.067	-.050	-.003	.073	.163	.266	99	.897	150			.541	.524	.543	.522	.483	.345
47	.367	180			.069	.047	.027	.010	-.010	-.037	102	.984	0			-.360	-.358	-.364	-.359	-.337	-.303
48	.486	0			-.021	-.022	-.021	.010	.102	.210	103	.984	30			-.317	-.314	-.352	-.372	-.382	-.366
49	.486	180			-.023	-.025	-.017	-.024	-.026	-.070	104	.984	60			-.397	-.404	-.399	-.437	-.470	-.488
50	.503	15			-.019	-.013	-.006	.012	.083	.188	105	.984	90			-.229	-.218	-.336	-.453	-.492	-.488
51	.503	30			-.020	-.012	-.011	.004	.054	.149	106	.984	135			-.599	-.645	-.628	-.582	-.601	-.529
52	.503	50			-.026	-.017	-.021	-.003	.034	.129	107	.984	180			-.420	-.423	-.438	-.481	-.510	-.527
53	.503	F			-.031	-.016	-.024	-.020	-.013	.070											
54	.503	F			-.058	-.023	-.117	-.254	-.260	-.227											

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Continued

(e) M = 1.18 - Continued

Pressure coefficients C_p on -

Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage								Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage - Concluded							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed											$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed							
1	.026	0	.093	.158		.255	.344	.448	.577	.725	55	.503	F	.158	.004		-.047	-.088	-.396	-.262	-.323
2	.026	90	.092	.276		.365	.333	.244	.126	.006	56	.503	135	.202	.024		-.049	-.056	-.069	-.139	-.467
3	.026	180	.703	.441		.242	.191	.152	.112	.088	57	.588	0	-.190	-.081		.009	.114	.309	.431	.560
4	.084	0	-.028	.035		.154	.225	.326	.445	.581	58	.588	180	.556	.334		.002	-.053	-.092	-.119	-.193
5	.084	45	-.241	.028		.212	.282	.337	.392	.441	59	.604	15	-.414	-.133		.010	.150	.327	.460	.591
6	.084	90	-.037	.153		.239	.216	.152	.052	-.084	60	.604	30	-.536	-.146		.059	.123	.288	.445	.607
7	.084	135	.430	.312		.177	.093	-.016	-.132	-.269	61	.604	50	-.595	-.195		.024	.174	.362	.507	.638
8	.084	180	.567	.324		.139	.078	.030	-.008	-.036	62	.604	F	-.576	-.343		.025	.191	.380	.535	.674
9	.134	J	.584	.337		.083	.040	.003	-.023	-.080	63	.604	F	.665	.382		-.005	-.153	-.372	-.466	-.571
10	.156	J	.683	.526		.376	.298	.214	.131	.062	64	.604	135	.622	.363		-.005	-.107	-.175	-.429	-.704
12	.173	30	-.180	-.076		.056	.136	.210	.293	.380	65	.690	0	-.435	-.271		-.028	.113	.242	.378	.494
13	.173	60	-.398	-.057							66	.690	180	.468	.223		-.063	-.172	-.277	-.384	-.412
14	.173	90	-.189	.057		.144	.078	.008	-.093	-.227	67	.706	15	-.620	-.269		-.043	.108	.239	.377	.491
15	.173	135	.333	.299		.249	.193	.109	.049	-.071	68	.706	30	-.750	-.266		-.033	.120	.254	.391	.504
16	.173	J	.565	.441		.352	.304	.237	.164	.090	69	.706	50	-.645	-.269		-.028	.128	.262	.397	.506
17	.173	C	.656	.516		.408	.367	.326	.317	.280	70	.706	F	-.568	-.304		-.030	.132	.271	.403	.509
18	.190	J	.418	.323		.268	.241	.182	.110	.027	71	.706	F	.458	.216		-.087	-.195	-.394	-.501	-.543
19	.190	C	.488	.349		.256	.234	.214	.224	.241	72	.706	135	.467	.220		-.077	-.173	-.277	-.487	-.706
20	.197	C	.248	.052		-.101	-.136	-.167	-.183	-.192	73	.753	0	-.426	-.318		-.040	.117	.306	.406	.489
21	.207	C	.344	.256		.214	.207	.203	.232	.249	74	.753	180	.461	.202		-.090	-.191	-.300	-.416	-.426
23	.216	C	.128	-.053		-.198	-.217	-.227	-.231	-.257	75	.770	15	-.508	-.064		.230	.370	.463	.529	.595
24	.226	23	-.237	-.103		.011	.078	.136	.221	.315	76	.770	30	-.505	-.064		.091	.250	.357	.425	.496
25	.226	45	-.324	-.147		.047	.112	.117	.152	.188	77	.770	50	-.466	-.140		-.019	.123	.255	.329	.405
26	.226	68	-.523	-.159		.059	.099	.054	-.018	-.067	78	.770	F	-.434	-.131		-.063	.027	.147	.227	.303
27	.226	90	-.378	-.107		.080	.098	.054	-.152	-.309	79	.770	F	-.259	-.045		.112	.100	-.024	-.141	-.194
28	.226	135	-.085	-.093		-.055	-.042	-.051	-.129	-.266	80	.770	F	.225	.080		.005	.001	-.253	-.174	-.454
29	.226	C	-.025	-.229		-.573	-.578	-.579	-.564	-.549	81	.770	135	.390	.233		-.028	-.087	-.286	-.499	-.430
30	.263	C	.010	-.168		-.273	-.245	-.214	-.192	-.244	82	.820	15	.191	.230						
31	.283	0	-.249	-.137		-.076	-.030	.019	.089	.202	83	.820	38	-.328	.204		.330	.319	.306	.318	.375
32	.299	30	-.296	-.192		-.065	.017	.093	.167	.149	84	.820	F	.047	.195		.317	.314	.312	.332	.395
33	.299	60	-.433	-.271		-.072	.026	.115	.199	.250	85	.820	F	-.100	.171		.304	.305	.307	.331	.392
34	.299	F	-.746	-.358		-.070	.029	.108	.168	.208	86	.820	F	-.153	.155		.311	.319	.339	.372	.436
35	.299	F	-.351	-.120		-.033	-.029	-.063	-.122	-.201	87	.820	F	-.374	.121		.325	.332	.397	.482	.575
36	.299	F	.077	.045		-.117	-.277	-.378	-.499	-.655	88	.820	F	.338	.264		.287	.204	-.098	-.290	-.509
37	.299	135	.158	.031		-.125	-.245	-.461	-.532	-.520	89	.820	F	.223	.231		.281	.215	.063	-.111	-.583
38	.319	C	.047	-.081		-.096	-.129	-.185	-.237	-.276	90	.820	F	.178	.230		.294	.232	.079	.051	-.179
39	.350	20	-.328	-.152		-.077	-.002	.079	.161	.259	91	.820	F	.219	.242		.313	.256	.180	.021	-.190
40	.350	40	-.200	-.203		-.077	-.003	.072	.163	.249	92	.820	142				.337	.294	.162	.111	-.412
41	.350	60	-.640	-.228		-.080	-.014	.069	.173	.280	93	.820	165	.348	.317		.386	.313	.142	.178	.113
42	.350	F	-.712	-.340		-.084	-.020	.051	.132	.203	94	.897	30	-.268	.093		.113	.111	.121	.194	.303
43	.350	F	-.486	-.227		-.047	-.138	-.214	-.286	-.380	95	.897	50	-.184	.085		.098	.099	.117	.195	.320
44	.350	F	.178	.033		-.147	-.262	-.591	-.724	-.794	96	.897	F	-.302	.067		.086	.093	.117	.197	.330
45	.350	135	.257	.070		-.093	-.158	-.197	-.232	-.221	97	.897	F	.120	.081		.143	.125	.045	-.146	-.214
46	.367	0	-.180	-.127		-.072	-.013	.063	.168	.248	98	.897	130	.138	.085		.154	.154	.113	-.129	-.277
47	.367	180	.274	.106		-.005	-.037	-.066	-.096	-.218	99	.897	150	.138	.080		.161	.156	.132	-.030	-.258
48	.486	0	-.176	-.101		-.055	-.048	-.011	.091	.211	102	.984	0	-.440	-.345		-.331	-.326	-.309	-.276	-.231
49	.486	180	.202	.017		-.057	-.069	-.085	-.125	-.215	103	.984	30	-.426	-.334						
50	.503	15	-.181	-.049		-.045	-.026	.007	.108	.266	104	.984	60	-.335	-.257		-.219	-.210	-.273	-.355	-.431
51	.503	30	-.205	-.053		-.040	-.015	.014	.111	.269	105	.984	90	-.358	-.273		-.239	-.228	-.271	-.338	-.407
52	.503	50	-.514	-.068		-.029	-.015	-.001	.089	.274	106	.984	135	-.302	-.285		-.275	-.291	-.334	-.450	-.349
53	.503	F	-.335	-.286		-.029	-.006	-.010	.052	.231	107	.984	180	-.340	-.370		-.378	-.348	-.397	-.444	-.478
54	.503	F	-.336	-.306		-.034	-.118	-.300	-.427	-.328											

TABLE II.- PRESSURE COEFFICIENTS MEASURED ON FUSELAGE - Concluded

(e) M = 1.18 - Concluded

Pressure coefficients C_p on -

Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage							Model orifice number	$\frac{x}{l}$	ϕ, deg	Fuselage - Concluded						
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15° α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15° α = 20°
			$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open										$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open						
1	.026	0			.211	.253	.341	.447	.575 .714	55	.503	F			-.018	-.050	-.091	-.389	-.250 -.316
2	.026	90			.361	.362	.334	.247	.132 .013	56	.503	135			-.027	-.054	-.060	-.070	-.126 -.431
3	.026	180			.295	.241	.185	.151	.115 .087	57	.588	0			-.030	.007	.108	.307	.429 .551
4	.084	0			.111	.154	.222	.325	.441 .572	58	.588	180			.070	-.002	-.055	-.091	-.123 -.199
5	.084	45			.178	.203	.280	.336	.393 .439	59	.604	15			-.050	.007	.142	.323	.456 .582
6	.084	90			.235	.233	.217	.156	.057 -.074	60	.604	30			.197	.298	.170	.233	.344 .471
7	.084	135			.232	.170	.095	-.012	-.129 -.264	61	.604	50			-.058	.021	.168	.359	.504 .631
8	.084	180			.197	.138	.079	.032	-.006 -.036	62	.604	F			-.082	.020	.186	.377	.532 .667
9	.134	J			.139	.083	.039	.005	-.018 -.082	63	.604	F			.098	-.012	-.156	-.367	-.475 -.567
10	.156	J			.423	.377	.300	.217	.135 .068	64	.604	135			.093	-.007	-.109	-.177	-.421 -.694
12	.173	30			.016	.040	.133	.209	.290 .374	65	.690	0			-.112	-.034	.108	.239	.375 .489
14	.173	90			.146	.136	.080	.011	-.089 -.218	66	.690	180			.030	-.063	-.173	-.280	-.394 -.406
15	.173	135			.270	.244	.195	.111	.053 -.060	67	.706	15			-.124	-.047	.102	.236	.374 .485
16	.173	J			.378	.351	.305	.238	.170 .094	68	.706	30			-.117	-.037	.115	.251	.389 .499
17	.173	C			.438	.406	.367	.326	.319 .286	69	.706	50			-.122	-.035	.122	.259	.395 .502
18	.190	J			.283	.265	.241	.184	.116 .033	70	.706	F			-.129	-.039	.125	.267	.401 .504
19	.190	C			.281	.252	.234	.215	.226 .245	71	.706	F			.015	-.088	-.196	-.392	-.508 -.536
20	.197	C			-.062	-.108	-.137	-.165	-.182 -.192	72	.706	135			.028	-.077	-.175	-.279	-.469 -.676
21	.207	C			.226	.210	.204	.201	.231 .257	73	.753	0			-.130	-.043	.114	.307	.405 .490
23	.216	C			-.160	-.200	-.222	-.229	-.232 -.257	74	.753	180			-.014	-.093	-.143	-.104	-.420 -.412
24	.226	23			-.027	.004	.075	.133	.219 .308	75	.770	15			.159	.239	.374	.467	.532 .602
25	.226	45			.001	.026	.107	.115	.152 .184	76	.770	30			.050	.109	.257	.361	.429 .503
26	.226	68			.014	.056	.097	.057	-.016 -.065	77	.770	50			-.040	-.004	.130	.260	.331 .411
27	.226	90			.045	.076	.095	.055	-.139 -.300	78	.770	F			-.030	-.055	.027	.150	.229 .306
28	.226	135			-.062	-.058	-.045	-.052	-.124 -.257	79	.770	F			.112	.117	.116	.004	-.121 -.178
29	.226	C			-.530	-.584	-.585	-.583	-.569 -.552	80	.770	F			-.014	.022	.046	.001	-.152 -.429
30	.263	C			-.258	-.282	-.248	-.211	-.187 -.236	81	.770	135			.044	.001	.031	-.099	-.340 -.411
31	.283	0			-.094	-.077	-.033	.020	.088 .196	83	.820	38			.357	.360	.342	.333	.371 .457
32	.299	30			-.115	-.072	.012	.091	.166 .149	84	.820	F			.338	.347	.337	.338	.387 .476
33	.299	60			-.131	-.080	.021	.113	.196 .259	85	.820	F			.324	.334	.327	.333	.387 .472
34	.299	F			-.131	-.089	.023	.105	.166 .210	86	.820	F			.320	.337	.338	.358	.423 .506
35	.299	F			-.008	-.041	-.032	-.062	-.120 -.192	87	.820	F			.333	.348	.348	.408	.523 .621
36	.299	F			-.038	-.127	-.275	-.377	-.499 -.638	88	.820	F			.326	.318	.253	-.004	-.202 -.508
37	.299	135			-.063	-.125	-.243	-.462	-.535 -.530	89	.820	F			.328	.316	.265	.123	-.021 -.544
38	.319	C			-.079	-.104	-.131	-.186	-.237 -.280	90	.820	F			.330	.328	.279	.130	.081 -.119
39	.350	20			-.111	-.078	-.006	.078	.160 .254	91	.820	F			.341	.347	.296	.205	.069 -.129
40	.350	40			-.125	-.078	-.006	.072	.162 .245	92	.820	142			.359	.370	.330	.205	.158 -.417
41	.350	60			-.126	-.082	-.017	.068	.172 .273	93	.820	165			.401	.416	.342	.194	.218 .092
42	.350	F			-.149	-.086	-.022	.051	.133 .200	94	.897	30			.632	.641	.652	.670	.708 .753
43	.350	F			-.063	-.062	-.139	-.212	-.286 -.369	95	.897	50			.524	.535	.550	.577	.621 .674
44	.350	F			-.066	-.148	-.262	-.599	-.731 -.787	96	.897	F			.461	.478	.494	.520	.560 .614
45	.350	135			-.043	-.097	-.161	-.200	-.232 -.219	97	.897	F			.441	.435	.382	.268	.097 -.027
46	.367	0			-.085	-.074	-.018	.063	.164 .243	98	.897	130			.516	.514	.481	.373	.172 -.077
47	.367	180			.033	-.007	-.041	-.066	-.095 -.224	99	.897	150			.645	.643	.582	.442	.394 .138
48	.486	0			-.057	-.054	-.051	-.012	.088 .204	102	.984	0			-.329	-.387	-.376	-.364	-.321 -.284
49	.486	180			-.054	-.066	-.072	-.085	-.124 -.212	104	.984	60			-.376	-.397	-.402	-.428	-.473 -.464
50	.503	15			.116	.176	.079	.063	.073 .095	105	.984	90			-.244	-.225	-.330	-.503	-.473 -.597
51	.503	30			-.069	-.042	-.019	.012	.109 .242	106	.984	135			-.681	-.744	-.693	-.657	-.584 -.568
52	.503	50			-.056	-.029	-.017	-.001	.088 .245	107	.984	180			-.423	-.404	-.409	-.452	-.529 -.494
53	.503	F			-.052	-.026	-.009	-.003	.050 .204										
54	.503	F			-.053	-.052	-.118	-.296	-.437 -.348										

TABLE III.- PRESSURE COEFFICIENTS MEASURED ON RIGHT WING

(a) M = 0.60

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Lower surface							Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper surface						
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx -5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed											$\beta \approx -5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed							
200	.180	.000				.630	.131	-1.013	-2.040	-1.853											
201	.180	.100				-.029	.223	.418	.549	.634	202	.180	.100				-.043	-.526	-1.975	-1.762	-1.788
203	.180	.200				-.060	.135	.286	.414	.519	204	.180	.200				-.060	-.268	-.351	-1.405	-1.653
205	.180	.300				-.078	.072	.204	.317	.422	206	.180	.300				-.079	-.208	-.270	-1.064	-1.421
207	.180	.400				-.094	.026	.135	.233	.333	208	.180	.400				-.084	-.176	-.270	-.804	-1.111
209	.180	.500				-.094	.000	.086	.168	.257	210	.180	.500				-.095	-.164	-.251	-.668	-.955
211	.180	.600				-.087	-.016	.051	.113	.189	212	.180	.600				-.099	-.149	-.226	-.588	-.823
213	.180	.700				-.046	.009	.053	.093	.147	214	.180	.700				-.060	-.095	-.181	-.568	-.686
215	.180	.800				-.014	.022	.048	.062	.088	216	.180	.800				-.036	-.058	-.179	-.329	-.581
217	.180	.900				-.003	.017	.026	.008	-.015	218	.180	.900				-.022	-.037	-.163	-.158	-.491
			$\beta \approx -5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open											$\beta \approx -5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open							
200	.180	.000	-1.646	-1.240	.387	.632	.080	-1.073	-2.022	-1.826											
201	.180	.100	-.599	-2.143	-.226	-.007	.245	.435	.562	.645	202	.180	.100	.625	.417	.136	-.040	-.577	-2.038	-1.708	-1.773
203	.180	.200	-1.494	-.316	-.173	-.037	.156	.303	.430	.534	204	.180	.200	.508	.290	.068	-.054	-.279	-.437	-1.439	-1.645
205	.180	.300	-1.307	-.294	-.152	-.055	.096	.221	.332	.437	206	.180	.300	.413	.207	.028	-.068	-.201	-.265	-1.107	-1.416
207	.180	.400	-1.110	-.258	-.140	-.071	.047	.153	.249	.350	208	.180	.400	.317	.138	.003	-.068	-.166	-.258	-.844	-1.107
209	.180	.500	-.946	-.227	-.122	-.070	.023	.106	.185	.275	210	.180	.500	.249	.088	-.018	-.077	-.151	-.239	-.697	-.947
211	.180	.600	-.800	-.218	-.097	-.062	.008	.070	.131	.207	212	.180	.600	.169	.039	-.035	-.079	-.131	-.219	-.618	-.815
213	.180	.700	-.679	-.188	-.043	-.019	.031	.071	.110	.165	214	.180	.700	.126	.030	-.012	-.037	-.078	-.187	-.562	-.675
215	.180	.800	-.560	-.223	-.004	.013	.046	.067	.079	.108	216	.180	.800	.069	.020	.006	-.014	-.036	-.203	-.311	-.578
217	.180	.900	-.449	-.183	.017	.027	.042	.044	.026	.004	218	.180	.900	-.019	-.001	.018	.008	-.012	-.167	-.169	-.496
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed											$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed							
200	.180	.000	-1.532	-1.042		.714	.232	-.768	-1.707	-1.636											
201	.180	.100	-1.492	-1.715		-.029	.243	.442	.578	.676	202	.180	.100	.670	.432		-.049	-.638	-1.768	-1.548	-1.590
203	.180	.200	-1.453	-.995		-.059	.143	.303	.429	.542	204	.180	.200	.534	.283		-.068	-.275	-.928	-1.272	-1.542
205	.180	.300	-1.308	-.337		-.074	.080	.209	.323		206	.180	.300	.428	.191		-.079	-.227	-.307	-1.010	-1.380
207	.180	.400	-1.052	-.271		-.087	.033	.138	.231	.342	208	.180	.400	.329	.129		-.080	-.191	-.256	-.806	-1.086
209	.180	.500	-.817	-.239		-.083	.010	.089	.163	.263	210	.180	.500	.253	.082		-.088	-.170	-.252	-.693	-.863
211	.180	.600	-.691	-.205		-.073	-.004	.052	.105	.192	212	.180	.600	.172	.035		-.087	-.142	-.232	-.612	-.753
213	.180	.700	-.631	-.155		-.023	.023	.057	.080	.147	214	.180	.700	.121	.037		-.042	-.084	-.177	-.535	-.693
215	.180	.800	-.594	-.106		.013	.043	.053	.041	.085	216	.180	.800	.053	.028		-.010	-.038	-.127	-.473	-.646
217	.180	.900	-.538	-.065		.030	.044	.033	-.035	-.027	218	.180	.900	-.055	.009		.009	-.007	-.084	-.408	-.587
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open											$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open							
200	.180	.000			.429	.703	.289	-.736	-1.670	-1.593											
201	.180	.100			-.272	-.044	.235	.439	.574	.670	202	.180	.100			.143	-.039	-.558	-1.722	-1.505	-1.547
203	.180	.200			-.206	-.067	.135	.303	.421	.539	204	.180	.200			.069	-.055	-.261	-.921	-1.231	-1.506
205	.180	.300			-.182	-.081	.075	.210	.321	.433	206	.180	.300			.025	-.071	-.219	-.289	-.971	-1.349
207	.180	.400			-.163	-.090	.032	.138	.231	.340	208	.180	.400			-.004	-.071	-.180	-.253	-.770	-1.057
209	.180	.500			-.138	-.085	.009	.091	.165	.262	210	.180	.500			-.024	-.077	-.159	-.243	-.671	-.841
211	.180	.600			-.106	-.071	-.002	.057	.108	.192	212	.180	.600			-.037	-.074	-.131	-.220	-.593	-.735
213	.180	.700			-.046	-.020	.028	.062	.082	.149	214	.180	.700			-.004	-.034	-.071	-.164	-.526	-.679
215	.180	.800			.001	.019	.050	.061	.046	.089	216	.180	.800			.018	.000	-.025	-.116	-.471	-.636
217	.180	.900			.030	.039	.055	.043	-.030	-.023	218	.180	.900			.031	.021	.009	-.067	-.408	-.578

TABLE III.- PRESSURE COEFFICIENTS MEASURED ON RIGHT WING - Continued

(a) M = 0.60 - Concluded

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Lower surface							Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper surface						
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx 0°$; $\delta_e = 0°$; δ_v = -7.5°; brakes closed										$\beta \approx 0°$; $\delta_e = 0°$; δ_v = -7.5°; brakes closed							
200	.180	.000			.437	.700	.255	-.769	-1.709	-1.704										
201	.180	.100			-.270	-.045	.235	.438	.571	.670	202	.180	.100		.141	-.040	-.557	-1.764	-1.578	-1.644
203	.180	.200			-.208	-.071	.133	.300	.418	.536	204	.180	.200		.066	-.062	-.278	-.855	-1.298	-1.574
205	.180	.300			-.183	-.084	.074	.208	.317	.433	206	.180	.300		.022	-.076	-.229	-.270	-1.030	-1.376
207	.180	.400			-.168	-.096	.026	.136	.229	.338	208	.180	.400		-.005	-.080	-.186	-.247	-.813	-1.082
209	.180	.500			-.144	-.092	.002	.086	.160	.259	210	.180	.500		-.028	-.089	-.169	-.245	-.691	-.874
211	.180	.600			-.116	-.081	-.011	.050	.101	.186	212	.180	.600		-.045	-.090	-.149	-.230	-.603	-.762
213	.180	.700			-.058	-.034	.016	.053	.077	.142	214	.180	.700		-.018	-.048	-.088	-.176	-.522	-.701
215	.180	.800			-.016	.001	.033	.048	.038	.079	216	.180	.800		.001	-.019	-.044	-.130	-.454	-.652
217	.180	.900			.008	.017	.032	.026	-.037	-.034	218	.180	.900		.009	-.004	-.015	-.088	-.387	-.590
			$\beta \approx 0°$; $\delta_e = 0°$; δ_v = 7.5°; brakes closed										$\beta \approx 0°$; $\delta_e = 0°$; δ_v = 7.5°; brakes closed							
200	.180	.000			.437	.705	.280	-.737	-1.646	-1.581										
201	.180	.100			-.253	-.035	.243	.442	.573	.674	202	.180	.100		.151	-.025	-.478	-1.593	-1.508	-1.540
203	.180	.200			-.191	-.057	.143	.308	.421	.544	204	.180	.200		.078	-.043	-.271	-.880	-1.214	-1.498
205	.180	.300			-.167	-.070	.085	.219	.322	.440	206	.180	.300		.034	-.056	-.219	-.326	-.943	-1.337
207	.180	.400			-.150	-.079	.042	.151	.238	.349	208	.180	.400		.008	-.059	-.174	-.254	-.738	-1.045
209	.180	.500			-.122	-.072	.020	.105	.170	.272	210	.180	.500		-.010	-.066	-.152	-.235	-.640	-.831
211	.180	.600			-.090	-.056	.011	.073	.115	.201	212	.180	.600		-.022	-.063	-.125	-.204	-.565	-.725
213	.180	.700			-.029	-.006	.040	.081	.093	.158	214	.180	.700		.009	-.022	-.066	-.153	-.502	-.669
215	.180	.800			.018	.033	.062	.083	.057	.100	216	.180	.800		.031	.012	-.018	-.103	-.445	-.627
217	.180	.900			.047	.055	.068	.064	-.017	-.010	218	.180	.900		.043	.037	.018	-.045	-.366	-.566
			$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed										$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed							
200	.180	.000	-1.898	-.715		.762	.207	-.560	-1.587	-1.675										
201	.180	.100	-1.495	-1.139		-.010	.281	.476	.613	.723	202	.180	.100	.706	.455		-.097	-.997	-1.177	-1.467	-1.606
203	.180	.200	-1.321	-.995		-.040	.170	.321	.450	.577	204	.180	.200	.555	.302		-.110	-.316	-1.019	-1.080	-1.535
205	.180	.300	-.923	-.845		-.056	.103	.229	.343	.463	206	.180	.300	.445	.214		-.113	-.221	-.866	-.809	-1.278
207	.180	.400	-.778	-.670		-.068	.054	.154	.249	.371	208	.180	.400	.342	.147		-.108	-.185	-.660	-.709	-.932
209	.180	.500	-.755	-.523		-.066	.030	.104	.177	.288	210	.180	.500	.263	.093		-.103	-.160	-.514	-.674	-.825
211	.180	.600	-.739	-.384		-.056	.017	.063	.114	.211	212	.180	.600	.176	.050		-.094	-.133	-.410	-.647	-.794
213	.180	.700	-.708	-.271		-.005	.046	.064	.082	.164	214	.180	.700	.121	.044		-.036	-.068	-.318	-.621	-.758
215	.180	.800	-.668	-.181		.035	.065	.053	.037	.095	216	.180	.800	.046	.034		.004	-.020	-.231	-.578	-.717
217	.180	.900	-.622	-.105		.059	.071	.018	-.063	-.032	218	.180	.900	-.084	-.001		.022	.017	-.156	-.525	-.660
			$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open										$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open							
200	.180	.000			.543	.770	.291	-.501	-1.460	-1.754										
201	.180	.100			-.236	-.030	.269	.466	.611	.719	202	.180	.100		.141	-.056	-.830	-1.159	-1.398	-1.550
203	.180	.200			-.183	-.045	.164	.315	.451	.572	204	.180	.200		.069	-.061	-.265	-1.016	-1.006	-1.466
205	.180	.300			-.159	-.058	.101	.228	.344	.462	206	.180	.300		.032	-.068	-.207	-.827	-.753	-1.191
207	.180	.400			-.140	-.068	.059	.157	.255	.370	208	.180	.400		.006	-.065	-.172	-.600	-.656	-.865
209	.180	.500			-.110	-.058	.039	.110	.185	.289	210	.180	.500		-.006	-.064	-.144	-.447	-.624	-.779
211	.180	.600			-.076	-.042	.031	.075	.124	.215	212	.180	.600		-.012	-.053	-.116	-.344	-.597	-.755
213	.180	.700			-.010	.012	.062	.079	.098	.171	214	.180	.700		.026	-.003	-.046	-.251	-.571	-.725
215	.180	.800			.043	.058	.087	.076	.057	.106	216	.180	.800		.055	.036	.005	-.172	-.536	-.685
217	.180	.900			.077	.085	.094	.048	-.038	-.016	218	.180	.900		.076	.064	.043	-.103	-.484	-.628

TABLE III.- PRESSURE COEFFICIENTS MEASURED ON RIGHT WING - Continued

(b) M = 0.90

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Lower surface							Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper surface						
			$\alpha \approx -20^\circ$	$\alpha \approx -10^\circ$	$\alpha \approx -3^\circ$	$\alpha \approx 0^\circ$	$\alpha \approx 5^\circ$	$\alpha \approx 10^\circ$	$\alpha \approx 15^\circ$	$\alpha \approx 20^\circ$			$\alpha \approx -20^\circ$	$\alpha \approx -10^\circ$	$\alpha \approx -3^\circ$	$\alpha \approx 0^\circ$	$\alpha \approx 5^\circ$	$\alpha \approx 10^\circ$	$\alpha \approx 15^\circ$	$\alpha \approx 20^\circ$
			$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed										$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed							
200	.180	.000				.687	.460	-.034	-.742	-1.165										
201	.180	.100				-.013	.278	.472	.614	.703	202	.180	.100				-.036	-.652	-1.287	-1.223	-1.380
203	.180	.200				-.059	.184	.348	.484	.591	204	.180	.200				-.076	-.501	-1.221	-1.149	-1.270
205	.180	.300				-.100	.106	.253	.384	.496	206	.180	.300				-.105	-.405	-.514	-1.014	-1.098
207	.180	.400				-.138	.040	.171	.296	.409	208	.180	.400				-.123	-.388	-.481	-.849	-.986
209	.180	.500				-.140	-.001	.108	.224	.335	210	.180	.500				-.145	-.348	-.515	-.795	-.975
211	.180	.600				-.127	-.032	.050	.158	.265	212	.180	.600				-.155	-.181	-.492	-.759	-.987
213	.180	.700				-.049	.003	.045	.133	.229	214	.180	.700				-.071	-.083	-.387	-.687	-.939
215	.180	.800				.005	.034	.033	.098	.180	216	.180	.800				-.022	-.028	-.311	-.653	-.792
217	.180	.900				.028	.040	-.019	.022	.085	218	.180	.900				.006	-.002	-.282	-.619	-.745
			$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open										$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open							
200	.180	.000	-1.265	-.190	.586	.697	.425	-.067	-.782	-1.187										
201	.180	.100	-1.303	-.013	-.248	.022	.302	.485	.622	.709	202	.180	.100	.701	.470	.157	-.042	-.685	-1.251	-1.091	-1.306
203	.180	.200	-.013	-1.208	-.207	-.026	.207	.363	.495	.601	204	.180	.200	.590	.346	.080	-.073	-.497	-1.145	-1.057	-1.196
205	.180	.300	-1.044	-.381	-.219	-.066	.129	.268	.395	.508	206	.180	.300	.499	.257	.030	-.095	-.395	-.659	-.934	-1.025
207	.180	.400	-.924	-.490	-.218	-.101	.067	.187	.308	.423	208	.180	.400	.410	.176	-.007	-.105	-.316	-.521	-.799	-.952
209	.180	.500	-.903	-.508	-.166	-.100	.029	.126	.238	.350	210	.180	.500	.336	.108	-.041	-.120	-.200	-.473	-.748	-.941
211	.180	.600	-.869	-.467	-.112	-.087	.001	.072	.173	.281	212	.180	.600	.252	.034	-.070	-.118	-.173	-.430	-.708	-.948
213	.180	.700	-.845	-.381	-.025	-.014	.033	.068	.149	.246	214	.180	.700	.207	.020	-.016	-.039	-.083	-.344	-.656	-.873
215	.180	.800	-.794	-.310	.032	.040	.061	.056	.114	.197	216	.180	.800	.148	-.002	.024	.014	-.021	-.290	-.613	-.748
217	.180	.900	-.664	-.277	.060	.065	.067	.005	.037	.102	218	.180	.900	.047	-.061	.047	.042	.023	-.238	-.578	-.759
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed										$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed							
200	.180	.000	-1.150	-.018		.772	.600	.169	-.413											
201	.180	.100	-1.185	-1.015		-.021	.294	.479	.629		202	.180	.100	.744	.492		-.039	-.566	-1.131	-1.133	
203	.180	.200	-1.138	-1.007		-.073	.177	.346	.486		204	.180	.200	.616	.352		-.085	-.446	-1.135	-1.020	
205	.180	.300	-1.044	-.872		-.113	.099	.246	.383		206	.180	.300	.514	.264		-.119	-.441	-.896	-.915	
207	.180	.400	-.959	-.726		-.155	.032	.160	.290		208	.180	.400	.418	.178		-.135	-.435	-.633	-.814	
209	.180	.500	-.910	-.637		-.151	-.010	.097	.214		210	.180	.500	.343	.111		-.158	-.410	-.529	-.761	
211	.180	.600	-.876	-.559		-.130	-.037	.038	.146		212	.180	.600	.257	.034		-.155	-.158	-.479	-.715	
213	.180	.700	-.861	-.459		-.039	.010	.039	.123		214	.180	.700	.209	.020		-.058	-.044	-.400	-.683	
215	.180	.800	-.777	-.373		.025	.052	.031	.089		216	.180	.800	.150	.000		-.001	.011	-.341	-.654	
217	.180	.900	-.713	-.288		.058	.070	-.017	.013		218	.180	.900	.045	-.057		.035	.043	-.281	-.612	
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open										$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open							
200	.180	.000			.670	.773	.611	.183	-.392	-1.002										
201	.180	.100			-.287	-.020	.291	.481	.630	.740	202	.180	.100			.157	-.033	-.514	-1.095	-1.106	-1.213
203	.180	.200			-.256	-.069	.178	.349	.491	.612	204	.180	.200			.076	-.079	-.426	-1.100	-1.012	-1.171
205	.180	.300			-.286	-.110	.098	.248	.383	.508	206	.180	.300			.015	-.113	-.428	-.874	-.901	-1.069
207	.180	.400			-.303	-.150	.031	.163	.291	.414	208	.180	.400			-.027	-.130	-.426	-.646	-.799	-.939
209	.180	.500			-.214	-.145	-.007	.100	.216	.336	210	.180	.500			-.068	-.150	-.400	-.532	-.746	-.895
211	.180	.600			-.127	-.118	-.031	.043	.148	.264	212	.180	.600			-.094	-.141	-.142	-.482	-.698	-.899
213	.180	.700			-.034	-.028	.017	.044	.125	.228	214	.180	.700			-.026	-.045	-.035	-.402	-.667	-.851
215	.180	.800			.033	.038	.062	.037	.093	.181	216	.180	.800			.023	.014	.022	-.337	-.641	-.792
217	.180	.900			.073	.074	.084	-.008	.018	.089	218	.180	.900			.055	.053	.058	-.276	-.603	-.713

TABLE III.- PRESSURE COEFFICIENTS MEASURED ON RIGHT WING - Continued

(b) M = 0.90 - Concluded

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Lower surface								Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper surface							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = -7.5°$; brakes closed											$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = -7.5°$; brakes closed							
200	.180	.000			.666	.769	.602	.176	-.409	-1.010												
201	.180	.100			-.295	-.026	.290	.483	.627	.738	202	.180	.100			.158	-.032	-.523	-1.163	-1.156	-1.342
203	.180	.200			-.258	-.074	.176	.350	.488	.607	204	.180	.200			.075	-.075	-.422	-1.135	-1.052	-1.273
205	.180	.300			-.287	-.116	.097	.250	.382	.505	206	.180	.300			.013	-.112	-.426	-.895	-.948	-1.102
207	.180	.400			-.309	-.158	.028	.164	.290	.414	208	.180	.400			-.029	-.129	-.423	-.558	-.838	-.978
209	.180	.500			-.232	-.154	-.013	.101	.214	.334	210	.180	.500			-.072	-.156	-.418	-.511	-.779	-.928
211	.180	.600			-.136	-.131	-.041	.043	.145	.261	212	.180	.600			-.105	-.157	-.178	-.477	-.730	-.938
213	.180	.700			-.045	-.041	.004	.042	.121	.226	214	.180	.700			-.041	-.061	-.047	-.391	-.695	-.881
215	.180	.800			.018	.021	.045	.033	.087	.175	216	.180	.800			.004	-.003	.006	-.328	-.663	-.827
217	.180	.900			.051	.051	.062	-.016	.012	.082	218	.180	.900			.029	.028	.034	-.282	-.621	-.708
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 7.5°$; brakes closed											$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 7.5°$; brakes closed							
200	.180	.000			.668	.777	.582	.167	-.413	-1.009												
201	.180	.100			-.282	.002	.310	.491	.637	.744	202	.180	.100			.168	-.041	-.655	-1.042	-1.060	-1.200
203	.180	.200			-.242	-.046	.196	.361	.500	.616	204	.180	.200			.086	-.085	-.553	-1.034	-.993	-1.158
205	.180	.300			-.267	-.086	.119	.261	.394	.513	206	.180	.300			.028	-.117	-.513	-.852	-.883	-1.052
207	.180	.400			-.258	-.121	.054	.177	.301	.421	208	.180	.400			-.012	-.128	-.463	-.650	-.786	-.922
209	.180	.500			-.167	-.109	.018	.117	.230	.344	210	.180	.500			-.046	-.136	-.356	-.552	-.733	-.877
211	.180	.600			-.102	-.084	-.004	.063	.163	.274	212	.180	.600			-.068	-.112	-.171	-.489	-.690	-.882
213	.180	.700			-.011	.001	.041	.064	.141	.239	214	.180	.700			-.002	-.022	-.051	-.405	-.650	-.838
215	.180	.800			.056	.064	.084	.058	.108	.191	216	.180	.800			.044	.036	.007	-.330	-.624	-.761
217	.180	.900			.095	.099	.101	.013	.032	.099	218	.180	.900			.078	.076	.020	-.259	-.589	-.698
			$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed											$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed							
200	.180	.000	-1.018	.115		.848	.658	.222	-.359	-.972												
201	.180	.100	-.986	-.949		.014	.332	.539	.687	.797	202	.180	.100	.784	.518		-.095	-1.113	-1.018	-1.167	-1.269
203	.180	.200	-1.004	-.845		-.034	.216	.391	.541	.659	204	.180	.200	.639	.377		-.128	-.504	-.916	-1.091	-1.142
205	.180	.300	-1.000	-.731		-.081	.130	.285	.429	.553	206	.180	.300	.534	.272		-.156	-.486	-.838	-.985	-1.089
207	.180	.400	-.980	-.661		-.126	.056	.194	.331	.456	208	.180	.400	.432	.187		-.163	-.478	-.731	-.869	-.995
209	.180	.500	-.959	-.602		-.124	.014	.127	.255	.375	210	.180	.500	.353	.117		-.171	-.496	-.666	-.813	-.979
211	.180	.600	-.930	-.532		-.101	-.013	.065	.182	.300	212	.180	.600	.265	.038		-.135	-.147	-.579	-.762	-.956
213	.180	.700	-.894	-.459		-.009	.036	.062	.155	.260	214	.180	.700	.219	.031		-.033	-.016	-.491	-.721	-.914
215	.180	.800	-.850	-.388		.058	.080	.049	.120	.209	216	.180	.800	.159	.007		.031	.039	-.415	-.684	-.860
217	.180	.900	-.797	-.318		.099	.105	-.008	.037	.111	218	.180	.900	.051	-.057		.076	.073	-.346	-.641	-.817
			$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open											$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open							
200	.180	.000			.777	.846	.673	.249	-.316	-.950												
201	.180	.100			-.224	.015	.328	.539	.683	.795	202	.180	.100			.154	-.061	-1.085	-.949	-1.033	-1.145
203	.180	.200			-.213	-.032	.217	.390	.537	.656	204	.180	.200			.079	-.097	-.457	-.825	-1.010	-1.068
205	.180	.300			-.249	-.072	.135	.287	.427	.551	206	.180	.300			.021	-.121	-.457	-.746	-.944	-1.022
207	.180	.400			-.238	-.105	.068	.200	.333	.456	208	.180	.400			-.017	-.124	-.448	-.650	-.824	-.929
209	.180	.500			-.142	-.093	.034	.137	.258	.378	210	.180	.500			-.046	-.124	-.286	-.584	-.762	-.919
211	.180	.600			-.084	-.065	.015	.080	.189	.304	212	.180	.600			-.053	-.094	-.076	-.501	-.706	-.902
213	.180	.700			.011	.024	.068	.081	.166	.266	214	.180	.700			.020	.001	.009	-.421	-.649	-.865
215	.180	.800			.083	.091	.115	.073	.131	.218	216	.180	.800			.075	.065	.066	-.350	-.598	-.830
217	.180	.900			.131	.135	.141	.020	.050	.119	218	.180	.900			.114	.112	.106	-.283	-.559	-.780

TABLE III.- PRESSURE COEFFICIENTS MEASURED ON RIGHT WING - Continued

(c) M = 0.95

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Lower surface							Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper surface						
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx -5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed											$\beta \approx -5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed							
200	.180	.000				.706	.574	.132	-.551	-1.001											
201	.180	.100				.000	.274	.478	.637	.734	202	.180	.100				-.012	-.442	-1.063	-1.279	-1.345
203	.180	.200				-.049	.174	.357	.510	.625	204	.180	.200				-.056	-.353	-1.011	-1.312	-1.211
205	.180	.300				-.101	.093	.264	.412	.533	206	.180	.300				-.097	-.342	-.436	-.993	-1.048
207	.180	.400				-.165	.022	.181	.325	.448	208	.180	.400				-.129	-.334	-.481	-.730	-.971
209	.180	.500				-.200	-.026	.116	.253	.375	210	.180	.500				-.170	-.361	-.524	-.720	-.979
211	.180	.600				-.200	-.074	.056	.188	.307	212	.180	.600				-.237	-.426	-.552	-.583	-.978
213	.180	.700				-.052	-.037	.054	.167	.272	214	.180	.700				-.110	-.419	-.452	-.492	-.985
215	.180	.800				.030	.015	.050	.138	.228	216	.180	.800				.002	-.075	-.398	-.560	-.967
217	.180	.900				.060	.048	.009	.072	.143	218	.180	.900				.038	.027	-.335	-.633	-.833
			$\beta \approx -5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open											$\beta \approx -5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open							
200	.180	.000	-1.111	-.030	.619	.712	.544	.095	-.592	-1.023											
201	.180	.100	-1.412	-1.102	-.210	.020	.304	.497	.645	.738	202	.180	.100	.734	.481	.178	-.006	-.485	-1.116	-1.272	-1.248
203	.180	.200	-.013	-1.140	-.194	-.030	.209	.379	.520	.632	204	.180	.200	.627	.360	.099	-.049	-.394	-1.065	-1.271	-1.201
205	.180	.300	-1.075	-.457	-.218	-.077	.129	.283	.422	.541	206	.180	.300	.537	.272	.043	-.081	-.356	-.403	-.852	-1.057
207	.180	.400	-1.014	-.519	-.278	-.130	.063	.202	.336	.458	208	.180	.400	.452	.190	.002	-.102	-.346	-.376	-.634	-.987
209	.180	.500	-.993	-.568	-.301	-.127	.022	.138	.265	.386	210	.180	.500	.382	.127	-.042	-.128	-.371	-.400	-.672	-1.013
211	.180	.600	-.988	-.553	-.142	-.108	-.014	.082	.201	.319	212	.180	.600	.299	.046	-.094	-.158	-.430	-.486	-.685	-1.011
213	.180	.700	-1.001	-.449	.015	-.002	.028	.080	.180	.285	214	.180	.700	.256	.037	-.018	-.025	-.145	-.438	-.631	-1.029
215	.180	.800	-.979	-.434	.071	.063	.073	.074	.150	.239	216	.180	.800	.202	.018	.042	.040	.025	-.344	-.626	-1.020
217	.180	.900	-.832	-.336	.098	.092	.096	.031	.082	.154	218	.180	.900	.109	-.027	.074	.073	.082	-.225	-.611	-.739
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed											$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed							
200	.180	.000	-.993	.121		.806	.697	.300	-.242	-.860											
201	.180	.100	-.013	-.924		.004	.294	.497	.655	.768	202	.180	.100	.774	.502		-.015	-.497	-1.067	-1.267	-1.397
203	.180	.200	-1.357	-.883		-.052	.181	.365	.518	.641	204	.180	.200	.650	.358		-.065	-.334	-.991	-1.215	-1.334
205	.180	.300	-1.159	-.844		-.102	.099	.265	.413	.541	206	.180	.300	.553	.272		-.109	-.349	-.889	-1.235	-1.136
207	.180	.400	-1.002	-.640		-.169	.021	.178	.322	.449	208	.180	.400	.455	.183		-.144	-.355	-.450	-.860	-.956
209	.180	.500	-.961	-.566		-.215	-.031	.111	.249	.374	210	.180	.500	.382	.113		-.180	-.383	-.477	-.337	-.933
211	.180	.600	-.938	-.548		-.239	-.092	.045	.178	.301	212	.180	.600	.297	.026		-.268	-.440	-.520	-.578	-.946
213	.180	.700	-.779	-.553		-.041	-.043	.044	.157	.268	214	.180	.700	.254	.025		-.144	-.447	-.476	-.660	-.900
215	.180	.800	-.804	-.514		.054	.031	.043	.129	.223	216	.180	.800	.201	.008		.032	-.077	-.383	-.655	-.723
217	.180	.900	-.813	-.324		.093	.075	.004	.064	.137	218	.180	.900	.102	-.030		.072	.051	-.316	-.615	-.780
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open											$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open							
200	.180	.000			.715	.796	.709	.315	-.228	-.845											
201	.180	.100			-.230	-.013	.283	.492	.655	.768	202	.180	.100			.178	.004	-.405	-1.066	-1.269	-1.362
203	.180	.200			-.219	-.061	.176	.364	.519	.642	204	.180	.200			.094	-.044	-.315	-1.002	-1.218	-1.307
205	.180	.300			-.248	-.111	.094	.262	.414	.541	206	.180	.300			.029	-.091	-.335	-.887	-1.227	-1.139
207	.180	.400			-.301	-.177	.016	.174	.323	.450	208	.180	.400			-.023	-.124	-.342	-.435	-.761	-.924
209	.180	.500			-.342	-.224	-.033	.108	.248	.374	210	.180	.500			-.077	-.164	-.369	-.449	-.523	-.888
211	.180	.600			-.371	-.238	-.089	.045	.180	.302	212	.180	.600			-.172	-.251	-.428	-.485	-.645	-.888
213	.180	.700			-.082	-.016	-.027	.045	.159	.269	214	.180	.700			-.058	-.068	-.410	-.420	-.646	-.720
215	.180	.800			.069	.067	.049	.045	.131	.225	216	.180	.800			.034	.045	-.021	-.365	-.620	-.764
217	.180	.900			.113	.107	.094	.009	.066	.141	218	.180	.900			.079	.087	.080	-.288	-.612	-.792

TABLE III.- PRESSURE COEFFICIENTS MEASURED ON RIGHT WING - Continued

(c) M = 0.95 - Concluded

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Lower surface								Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper surface							
			$\alpha = -20^\circ$	$\alpha = -10^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 15^\circ$	$\alpha = 20^\circ$				$\alpha = -20^\circ$	$\alpha = -10^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 15^\circ$	$\alpha = 20^\circ$
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = -7.5^\circ$; brakes closed											$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = -7.5^\circ$; brakes closed							
200	.180	.000			.725	.795	.687	.292	-.238	-.856											
201	.180	.100			-.249	-.011	.290	.498	.657	.764	202	.180	.100			.175	-.005	-.486	-1.065	-1.261	-1.397
203	.180	.200			-.224	-.062	.177	.368	.521	.639	204	.180	.200			.093	-.054	-.342	-.995	-1.215	-1.330
205	.180	.300			-.247	-.112	.096	.266	.418	.538	206	.180	.300			.027	-.100	-.356	-.866	-1.250	-1.107
207	.180	.400			-.299	-.178	.019	.178	.325	.448	208	.180	.400			-.022	-.135	-.363	-.457	-.870	-.930
209	.180	.500			-.339	-.223	-.032	.112	.252	.371	210	.180	.500			-.078	-.173	-.389	-.514	-.622	-.923
211	.180	.600			-.369	-.246	-.090	.047	.182	.298	212	.180	.600			-.177	-.260	-.447	-.583	-.436	-.938
213	.180	.700			-.172	-.045	-.041	.045	.162	.266	214	.180	.700			-.103	-.145	-.452	-.604	-.492	-.959
215	.180	.800			.048	.050	.028	.044	.134	.221	216	.180	.800			.013	.025	-.079	-.527	-.621	-.927
217	.180	.900			.094	.085	.068	.007	.068	.136	218	.180	.900			.058	.063	.045	-.258	-.674	-.644
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 7.5^\circ$; brakes closed											$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 7.5^\circ$; brakes closed							
200	.180	.000			.712	.793	.690	.309	-.228	-.855											
201	.180	.100			-.222	-.004	.297	.497	.653	.767	202	.180	.100			.188	.014	-.412	-.963	-1.029	-1.308
203	.180	.200			-.207	-.053	.190	.370	.519	.643	204	.180	.200			.105	-.033	-.315	-.862	-1.000	-1.250
205	.180	.300			-.244	-.100	.111	.271	.414	.542	206	.180	.300			.042	-.077	-.336	-.752	-.935	-1.087
207	.180	.400			-.294	-.160	.040	.185	.324	.453	208	.180	.400			-.006	-.109	-.341	-.379	-.771	-.877
209	.180	.500			-.333	-.178	-.002	.121	.250	.377	210	.180	.500			-.055	-.141	-.367	-.375	-.704	-.730
211	.180	.600			-.273	-.109	-.036	.060	.184	.307	212	.180	.600			-.118	-.191	-.422	-.421	-.647	-.777
213	.180	.700			.025	.014	.027	.064	.164	.274	214	.180	.700			-.007	-.006	-.128	-.370	-.599	-.843
215	.180	.800			.098	.087	.091	.064	.137	.230	216	.180	.800			.063	.062	.065	-.299	-.560	-.826
217	.180	.900			.135	.127	.127	.026	.071	.144	218	.180	.900			.103	.104	.120	-.176	-.489	-.748
			$\beta \approx 5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed											$\beta \approx 5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed							
200	.180	.000	-.902	.265		.876	.762	.366	-.178	-.819											
201	.180	.100	-.013	-1.084		.036	.326	.547	.704	.825	202	.180	.100	.816	.524		-.070	-.889	-1.068	-1.287	-1.379
203	.180	.200	-.013	-.819		-.019	.214	.400	.561	.692	204	.180	.200	.674	.385		-.107	-.404	-.972	-1.228	-1.364
205	.180	.300	-.013	-.700		-.071	.125	.294	.451	.589	206	.180	.300	.572	.284		-.151	-.395	-.952	-1.165	-1.270
207	.180	.400	-.013	-.688		-.147	.043	.202	.354	.494	208	.180	.400	.473	.196		-.181	-.392	-.828	-1.133	-1.092
209	.180	.500	-.851	-.667		-.196	-.012	.132	.277	.413	210	.180	.500	.396	.125		-.205	-.423	-.617	-.876	-.881
211	.180	.600	-.964	-.667		-.227	-.074	.064	.206	.339	212	.180	.600	.309	.039		-.301	-.468	-.577	-.648	-.780
213	.180	.700	-.915	-.667		-.001	-.010	.065	.184	.301	214	.180	.700	.268	.037		-.098	-.497	-.449	-.680	-.890
215	.180	.800	-.858	-.364		.085	.058	.062	.153	.252	216	.180	.800	.209	.028		.066	-.061	-.266	-.701	-.877
217	.180	.900	-.820	-.147		.129	.103	.020	.083	.164	218	.180	.900	.108	-.007		.110	.075	-.230	-.645	-.832
			$\beta \approx 5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open											$\beta \approx 5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open							
200	.180	.000			.819	.871	.781	.395	-.138	-.793											
201	.180	.100			-.192	.020	.318	.539	.697	.819	202	.180	.100			.172	-.015	-.870	-1.049	-1.034	-1.368
203	.180	.200			-.198	-.036	.213	.395	.554	.683	204	.180	.200			.096	-.064	-.372	-.953	-1.024	-1.359
205	.180	.300			-.234	-.086	.129	.291	.445	.581	206	.180	.300			.028	-.105	-.371	-.858	-.999	-1.152
207	.180	.400			-.286	-.153	.053	.202	.351	.486	208	.180	.400			-.023	-.137	-.374	-.634	-.909	-.975
209	.180	.500			-.330	-.185	.011	.137	.277	.411	210	.180	.500			-.068	-.162	-.407	-.495	-.888	-.936
211	.180	.600			-.249	-.082	-.022	.075	.207	.337	212	.180	.600			-.119	-.197	-.452	-.441	-.788	-.924
213	.180	.700			.059	.040	.050	.078	.188	.302	214	.180	.700			.026	.029	-.125	-.401	-.712	-.875
215	.180	.800			.130	.116	.117	.076	.158	.255	216	.180	.800			.092	.095	.086	-.362	-.633	-.842
217	.180	.900			.170	.162	.159	.032	.088	.167	218	.180	.900			.141	.144	.150	-.298	-.559	-.823

TABLE III.- PRESSURE COEFFICIENTS MEASURED ON RIGHT WING - Continued

(d) M = 1.03

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Lower surface								Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper surface							
			$\alpha = -20^\circ$	$\alpha = -10^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 15^\circ$	$\alpha = 20^\circ$				$\alpha = -20^\circ$	$\alpha = -10^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 15^\circ$	$\alpha = 20^\circ$
			$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed											$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed							
200	.180	.000				.742	.640	.187	-.426	-.797												
201	.180	.100				.057	.348	.578	.715	.797	202	.180	.100				.031	-.374	-.997	-1.151	-1.208
203	.180	.200				.014	.254	.462	.595	.696	204	.180	.200				.001	-.306	-.984	-1.061	-.963
205	.180	.300				-.032	.173	.369	.502	.609	206	.180	.300				-.038	-.264	-.381	-.740	-.847
207	.180	.400				-.095	.098	.288	.420	.529	208	.180	.400				-.076	-.262	-.385	-.617	-.800
209	.180	.500				-.138	.048	.225	.351	.459	210	.180	.500				-.110	-.287	-.423	-.634	-.817
211	.180	.600				-.178	-.020	.162	.290	.395	212	.180	.600				-.187	-.346	-.480	-.662	-.820
213	.180	.700				-.198	-.038	.156	.269	.365	214	.180	.700				-.208	-.361	-.485	-.672	-.834
215	.180	.800				-.186	-.027	.150	.243	.326	216	.180	.800				-.204	-.356	-.494	-.682	-.831
217	.180	.900				-.166	-.025	.115	.184	.249	218	.180	.900				-.220	-.361	-.488	-.689	-.837
			$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open											$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open							
200	.180	.000	-.909	.037	.690	.748	.611	.169	-.448	-.814												
201	.180	.100	-1.199	-.954	-.134	.077	.367	.586	.721	.801	202	.180	.100	.804	.587	.215	.017	-.400	-.988	-1.162	-1.213
203	.180	.200	-.968	-.961	-.127	.031	.274	.472	.602	.701	204	.180	.200	.704	.471	.140	-.011	-.324	-.980	-1.052	-.964
205	.180	.300	-.861	-.360	-.153	-.021	.193	.378	.510	.615	206	.180	.300	.621	.385	.086	-.046	-.278	-.403	-.754	-.851
207	.180	.400	-.834	-.406	-.200	-.083	.119	.298	.427	.536	208	.180	.400	.535	.305	.036	-.081	-.270	-.383	-.633	-.807
209	.180	.500	-.841	-.449	-.234	-.126	.070	.234	.360	.469	210	.180	.500	.471	.240	-.007	-.112	-.294	-.419	-.648	-.831
211	.180	.600	-.846	-.474	-.264	-.164	.009	.174	.298	.405	212	.180	.600	.394	.158	-.093	-.188	-.351	-.473	-.676	-.828
213	.180	.700	-.858	-.495	-.256	-.182	.029	.169	.278	.375	214	.180	.700	.354	.143	-.117	-.208	-.366	-.482	-.685	-.838
215	.180	.800	-.861	-.500	-.016	.002	.073	.163	.251	.334	216	.180	.800	.307	.124	-.046	-.093	-.305	-.489	-.692	-.836
217	.180	.900	-.855	-.362	.121	.157	.095	.127	.192	.257	218	.180	.900	.220	.076	.122	.133	-.029	-.303	-.696	-.844
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed											$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed							
200	.180	.000	-.798	.205		.841	.773	.373	-.130	-.668												
201	.180	.100	-1.198	-.842		.055	.362	.584	.732	.835	202	.180	.100	.842	.590		.033	-.638	-.919	-1.094	-1.192
203	.180	.200	-1.148	-.848		.002	.254	.459	.603	.714	204	.180	.200	.724	.458		-.004	-.264	-.862	-1.049	-1.121
205	.180	.300	-.972	-.746		-.032	.173	.362	.504	.620	206	.180	.300	.633	.376		-.044	-.266	-.783	-1.044	-.922
207	.180	.400	-.851	-.471		-.097	.095	.276	.417	.534	208	.180	.400	.543	.287		-.082	-.272	-.340	-.627	-.786
209	.180	.500	-.794	-.425		-.144	.045	.210	.346	.463	210	.180	.500	.473	.218		-.104	-.297	-.377	-.530	-.789
211	.180	.600	-.787	-.460		-.182	-.027	.141	.279	.393	212	.180	.600	.393	.130		-.184	-.350	-.446	-.590	-.802
213	.180	.700	-.795	-.488		-.198	-.052	.136	.259	.363	214	.180	.700	.354	.117		-.217	-.373	-.464	-.608	-.809
215	.180	.800	-.808	-.500		-.195	-.046	.132	.233	.323	216	.180	.800	.303	.096		-.213	-.366	-.481	-.616	-.823
217	.180	.900	-.799	-.414		-.181	-.041	.100	.176	.247	218	.180	.900	.214	.042		-.225	-.308	-.470	-.622	-.830
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open											$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open							
200	.180	.000			.793	.833	.767	.388	-.117	-.650												
201	.180	.100			-.133	.051	.362	.575	.724	.836	202	.180	.100			.233	.029	-.642	-.908	-1.093	-1.154
203	.180	.200			-.144	.002	.255	.452	.597	.717	204	.180	.200			.155	-.008	-.259	-.860	-1.045	-1.097
205	.180	.300			-.155	-.031	.176	.354	.496	.621	206	.180	.300			.096	-.048	-.259	-.784	-1.043	-.921
207	.180	.400			-.204	-.095	.097	.268	.409	.535	208	.180	.400			.046	-.088	-.267	-.337	-.641	-.774
209	.180	.500			-.244	-.143	.047	.202	.338	.462	210	.180	.500			.002	-.110	-.293	-.376	-.530	-.772
211	.180	.600			-.277	-.179	-.025	.135	.272	.395	212	.180	.600			-.092	-.188	-.345	-.446	-.588	-.781
213	.180	.700			-.291	-.195	-.049	.131	.254	.364	214	.180	.700			-.131	-.218	-.369	-.464	-.608	-.793
215	.180	.800			-.281	-.192	-.044	.129	.229	.326	216	.180	.800			-.134	-.214	-.359	-.480	-.616	-.803
217	.180	.900			-.149	-.171	-.038	.098	.173	.250	218	.180	.900			-.154	-.222	-.242	-.353	-.607	-.808

TABLE III.- PRESSURE COEFFICIENTS MEASURED ON RIGHT WING - Continued

(d) M = 1.03 - Concluded

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Lower surface							Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper surface						
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15° α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15° α = 20°
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = -7.5°$; brakes closed										$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = -7.5°$; brakes closed						
200	.180	.000			.793	.834	.769	.387	-.114 -.660										
201	.180	.100			-.136	.051	.363	.584	.731 .831	202	.180	.100			.232	.040	-.602	-.893	-1.061 -1.166
203	.180	.200			-.147	.001	.253	.459	.602 .711	204	.180	.200			.156	.003	-.258	-.841	-1.028 -1.112
205	.180	.300			-.159	-.032	.175	.363	.503 .618	206	.180	.300			.095	-.041	-.256	-.741	-1.022 -.906
207	.180	.400			-.208	-.096	.096	.277	.415 .531	208	.180	.400			.047	-.077	-.263	-.327	-.592 -.761
209	.180	.500			-.246	-.145	.047	.213	.345 .459	210	.180	.500			.002	-.099	-.287	-.375	-.519 -.759
211	.180	.600			-.280	-.180	-.024	.144	.279 .391	212	.180	.600			-.091	-.179	-.340	-.439	-.572 -.777
213	.180	.700			-.293	-.198	-.050	.139	.260 .361	214	.180	.700			-.130	-.213	-.363	-.459	-.594 -.793
215	.180	.800			-.286	-.194	-.045	.136	.237 .321	216	.180	.800			-.131	-.207	-.357	-.472	-.601 -.805
217	.180	.900			-.227	-.181	-.043	.105	.179 .246	218	.180	.900			-.155	-.223	-.352	-.476	-.611 -.812
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 7.5°$; brakes closed										$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 7.5°$; brakes closed						
200	.180	.000			.784	.827	.753	.390	-.101 -.663										
201	.180	.100			-.136	.054	.369	.584	.729 .834	202	.180	.100			.221	.032	-.654	-.897	-1.107 -1.184
203	.180	.200			-.137	.010	.261	.461	.602 .716	204	.180	.200			.142	-.004	-.279	-.846	-1.058 -1.130
205	.180	.300			-.156	-.032	.181	.363	.502 .619	206	.180	.300			.083	-.048	-.282	-.759	-1.021 -.928
207	.180	.400			-.207	-.094	.103	.279	.415 .535	208	.180	.400			.031	-.087	-.278	-.325	-.635 -.784
209	.180	.500			-.243	-.141	.053	.214	.345 .463	210	.180	.500			-.011	-.109	-.303	-.370	-.529 -.786
211	.180	.600			-.274	-.177	-.017	.147	.279 .396	212	.180	.600			-.104	-.188	-.355	-.438	-.573 -.796
213	.180	.700			-.286	-.193	-.043	.144	.261 .365	214	.180	.700			-.136	-.218	-.373	-.456	-.390 -.798
215	.180	.800			-.086	-.088	.005	.144	.236 .326	216	.180	.800			-.127	-.179	-.257	-.470	-.328 -.801
217	.180	.900			.143	.169	.077	.113	.178 .250	218	.180	.900			.120	.140	-.053	-.201	-.446 -.605
			$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed										$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed						
200	.180	.000	-.708	.309		.910	.818	.422	-.077 -.628										
201	.180	.100	.000	-.849		.085	.407	.646	.782 .889	202	.180	.100	.883	.626		-.021	-.774	-.937	-1.120 -1.179
203	.180	.200	.000	-.659		.036	.296	.505	.646 .761	204	.180	.200	.751	.490		-.065	-.380	-.892	-1.091 -1.220
205	.180	.300	.000	-.550		-.005	.211	.404	.541 .664	206	.180	.300	.654	.393		-.082	-.331	-.874	-1.040 -1.125
207	.180	.400	.000	-.554		-.072	.127	.315	.450 .573	208	.180	.400	.558	.304		-.119	-.318	-.761	-.981 -.935
209	.180	.500	-.931	-.559		-.124	.071	.245	.376 .498	210	.180	.500	.488	.233		-.146	-.337	-.496	-.797 -.865
211	.180	.600	-.832	-.563		-.161	-.006	.177	.307 .428	212	.180	.600	.405	.147		-.209	-.379	-.460	-.628 -.833
213	.180	.700	-.605	-.576		-.190	-.034	.174	.286 .394	214	.180	.700	.365	.139		-.246	-.400	-.482	-.491 -.772
215	.180	.800	-.626	-.538		-.194	-.013	.169	.258 .351	216	.180	.800	.315	.121		-.245	-.390	-.495	-.280 -.521
217	.180	.900	-.685	-.249		-.137	.028	.129	.194 .270	218	.180	.900	.222	.071		-.191	-.226	-.206	-.447 -.592
			$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open										$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open						
200	.180	.000			.881	.901	.834	.458	-.033 -.614										
201	.180	.100			-.130	.073	.392	.632	.776 .884	202	.180	.100			.202	.001	-.738	-.893	-1.110 -1.174
203	.180	.200			-.155	.019	.286	.491	.640 .755	204	.180	.200			.135	-.042	-.335	-.840	-1.077 -1.213
205	.180	.300			-.164	-.018	.200	.391	.536 .657	206	.180	.300			.069	-.077	-.306	-.827	-1.024 -1.131
207	.180	.400			-.214	-.081	.118	.303	.443 .569	208	.180	.400			.019	-.111	-.299	-.707	-.977 -.945
209	.180	.500			-.247	-.133	.067	.236	.373 .496	210	.180	.500			-.019	-.135	-.321	-.469	-.745 -.871
211	.180	.600			-.285	-.169	-.009	.169	.305 .426	212	.180	.600			-.118	-.203	-.362	-.434	-.310 -.705
213	.180	.700			-.291	-.192	-.037	.168	.286 .395	214	.180	.700			-.166	-.239	-.386	-.459	-.443 -.545
215	.180	.800			-.002	-.076	.065	.168	.260 .352	216	.180	.800			-.146	-.156	-.332	-.198	-.523 -.662
217	.180	.900			.177	.198	.143	.132	.197 .271	218	.180	.900			.157	.172	.070	-.149	-.514 -.679

TABLE III.- PRESSURE COEFFICIENTS MEASURED ON RIGHT WING - Continued

(e) M = 1.18

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Lower surface α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°	Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper surface α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx -5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed											$\beta \approx -5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed							
200	.180	.000				.775	.773	.461	-.089	-.540											
201	.180	.100				.066	.341	.585	.757	.869	202	.180	.100				.050	-.187	-.616	-.779	-.863
203	.180	.200				.025	.275	.496	.651	.774	204	.180	.200				.011	-.159	-.601	-.680	-.744
205	.180	.300				.016	.214	.415	.568	.693	206	.180	.300				.015	-.162	-.282	-.449	-.565
207	.180	.400				-.034	.150	.342	.493	.618	208	.180	.400				-.008	-.161	-.255	-.410	-.534
209	.180	.500				-.067	.104	.286	.431	.556	210	.180	.500				-.023	-.166	-.285	-.440	-.554
211	.180	.600				-.096	.057	.218	.372	.498	212	.180	.600				-.083	-.210	-.324	-.472	-.565
213	.180	.700				-.122	.039	.210	.363	.478	214	.180	.700				-.116	-.226	-.337	-.505	-.584
215	.180	.800				-.109	.053	.217	.351	.451	216	.180	.800				-.103	-.221	-.340	-.511	-.594
217	.180	.900				-.092	.067	.204	.314	.393	218	.180	.900				-.105	-.224	-.338	-.504	-.596
			$\beta \approx -5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open											$\beta \approx -5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open							
200	.180	.000	-.629	.380	.762	.778	.761	.441	-.122	-.556											
201	.180	.100	-.909	-.552	-.082	.075	.368	.596	.763	.873	202	.180	.100	.873	.563	.205	.044	-.252	-.656	-.838	-.913
203	.180	.200	-.894	.008	-.093	.035	.298	.503	.657	.778	204	.180	.200	.781	.480	.148	.006	-.178	-.656	-.688	-.749
205	.180	.300	-.620	-.351	-.100	.020	.234	.423	.573	.698	206	.180	.300	.705	.413	.123	.010	-.183	-.307	-.471	-.598
207	.180	.400	-.576	-.330	-.124	-.029	.169	.350	.498	.623	208	.180	.400	.628	.353	.100	-.013	-.174	-.273	-.440	-.571
209	.180	.500	-.567	-.338	-.157	-.064	.122	.293	.437	.561	210	.180	.500	.572	.302	.084	-.028	-.178	-.300	-.470	-.577
211	.180	.600	-.575	-.350	-.184	-.090	.075	.225	.378	.504	212	.180	.600	.501	.215	.016	-.089	-.221	-.338	-.506	-.583
213	.180	.700	-.597	-.358	-.197	-.112	.059	.216	.368	.483	214	.180	.700	.471	.204	-.025	-.119	-.233	-.347	-.533	-.595
215	.180	.800	-.610	-.372	-.192	-.112	.070	.224	.355	.455	216	.180	.800	.435	.193	-.019	-.106	-.230	-.349	-.545	-.606
217	.180	.900	-.622	-.377	-.177	-.089	.083	.210	.318	.396	218	.180	.900	.366	.150	-.022	-.108	-.238	-.355	-.550	-.614
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed											$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed							
200	.180	.000	-.522	.455		.885	.907	.628	.175	-.401											
201	.180	.100	-.862	-.548		.072	.338	.591	.776	.913	202	.180	.100	.916	.596		.062	-.434	-.543	-.795	-.878
203	.180	.200	-.861	-.465		.017	.257	.488	.660	.797	204	.180	.200	.804	.491		-.004	-.198	-.542	-.815	-.892
205	.180	.300	-.686	-.398		.012	.209	.407	.572	.708	206	.180	.300	.719	.425		-.006	-.185	-.541	-.491	-.703
207	.180	.400	-.543	-.434		-.040	.159	.340	.492	.628	208	.180	.400	.633	.356		-.036	-.183	-.372	-.378	-.540
209	.180	.500	-.515	-.420		-.077	.110	.289	.430	.563	210	.180	.500	.570	.303		-.057	-.195	-.268	-.400	-.529
211	.180	.600	-.530	-.402		-.107	.068	.220	.366	.500	212	.180	.600	.496	.211		-.087	-.222	-.303	-.422	-.543
213	.180	.700	-.543	-.383		-.122	.037	.205	.358	.479	214	.180	.700	.466	.203		-.119	-.235	-.326	-.435	-.548
215	.180	.800	-.569	-.368		-.110	.059	.210	.349	.453	216	.180	.800	.430	.193		-.112	-.224	-.327	-.447	-.567
217	.180	.900	-.569	-.354		-.092	.055	.203	.314	.396	218	.180	.900	.355	.146		-.111	-.222	-.332	-.464	-.588
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open											$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open							
200	.180	.000			.871	.855	.867	.615	.183	-.399											
201	.180	.100			-.082	.049	.322	.577	.761	.900	202	.180	.100			.196	.062	-.403	-.491	-.758	-.869
203	.180	.200			-.102	.012	.246	.477	.646	.784	204	.180	.200			.130	-.004	-.190	-.428	-.757	-.887
205	.180	.300			-.103	.015	.205	.401	.557	.694	206	.180	.300			.097	-.004	-.181	-.410	-.515	-.704
207	.180	.400			-.137	-.040	.155	.328	.478	.614	208	.180	.400			.057	-.037	-.175	-.396	-.386	-.542
209	.180	.500			-.160	-.078	.104	.277	.416	.549	210	.180	.500			.054	-.060	-.191	-.360	-.401	-.532
211	.180	.600			-.192	-.107	.064	.208	.353	.488	212	.180	.600			.000	-.088	-.216	-.360	-.424	-.546
213	.180	.700			-.202	-.123	.033	.194	.345	.467	214	.180	.700			-.035	-.117	-.233	-.361	-.438	-.550
215	.180	.800			-.195	-.109	.053	.198	.336	.440	216	.180	.800			-.020	-.111	-.222	-.350	-.449	-.569
217	.180	.900			-.168	-.091	.050	.191	.302	.384	218	.180	.900			-.044	-.109	-.212	-.341	-.456	-.586

TABLE III.- PRESSURE COEFFICIENTS MEASURED ON RIGHT WING - Concluded

(e) M = 1.18 - Concluded

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Lower surface							Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper surface						
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = -7.5°$; brakes closed											$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = -7.5°$; brakes closed							
200	.180	.000			.856	.852	.862	.601	.163	-.405	202	.180	.100			.217	.070	-.434	-.558	-.782	-.856
201	.180	.100			-.083	.048	.329	.581	.760	.896	204	.180	.200			.142	.006	-.200	-.555	-.794	-.867
203	.180	.200			-.099	.021	.254	.481	.645	.782	206	.180	.300			.102	-.002	-.186	-.533	-.487	-.673
205	.180	.300			-.106	.012	.211	.403	.557	.693	208	.180	.400			.065	-.034	-.186	-.356	-.383	-.521
207	.180	.400			-.141	-.045	.155	.329	.478	.614	210	.180	.500			.067	-.048	-.197	-.270	-.401	-.515
209	.180	.500			-.164	-.081	.105	.278	.416	.549	212	.180	.600			.011	-.082	-.226	-.315	-.425	-.530
211	.180	.600			-.196	-.111	.063	.208	.352	.488	214	.180	.700			-.026	-.115	-.240	-.334	-.439	-.545
213	.180	.700			-.204	-.126	.031	.195	.345	.467	216	.180	.800			-.014	-.108	-.230	-.338	-.452	-.564
215	.180	.800			-.200	-.114	.054	.200	.336	.440	218	.180	.900			-.038	-.107	-.224	-.338	-.466	-.576
217	.180	.900			-.175	-.095	.049	.192	.303	.384											
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 7.5°$; brakes closed											$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 7.5°$; brakes closed							
200	.180	.000			.856	.855	.865	.607	.166	-.398	202	.180	.100			.222	.074	-.439	-.521	-.756	-.854
201	.180	.100			-.086	.046	.335	.587	.769	.901	204	.180	.200			.155	.017	-.194	-.482	-.758	-.866
203	.180	.200			-.099	.029	.265	.487	.654	.787	206	.180	.300			.114	.006	-.185	-.516	-.518	-.683
205	.180	.300			-.105	.007	.219	.407	.564	.696	208	.180	.400			.079	-.024	-.183	-.391	-.383	-.530
207	.180	.400			-.142	-.046	.158	.333	.485	.616	210	.180	.500			.080	-.040	-.197	-.303	-.393	-.521
209	.180	.500			-.168	-.079	.109	.281	.421	.550	212	.180	.600			.020	-.077	-.222	-.317	-.418	-.535
211	.180	.600			-.195	-.105	.070	.212	.359	.488	214	.180	.700			-.018	-.107	-.234	-.330	-.435	-.548
213	.180	.700			-.200	-.119	.043	.197	.350	.468	216	.180	.800			-.010	-.103	-.223	-.332	-.444	-.569
215	.180	.800			-.194	-.112	.055	.203	.340	.441	218	.180	.900			-.028	-.098	-.221	-.328	-.451	-.579
217	.180	.900			-.171	-.090	.058	.196	.304	.384											
			$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed											$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed							
200	.180	.000	-.423	.584		.951	.957	.667	.196	-.347	202	.180	.100	.947	.606		.042	-.445	-.594	-.752	-.857
201	.180	.100	.007	.006		.067	.357	.617	.812	.949	204	.180	.200	.818	.492		-.024	-.224	-.469	-.708	-.859
203	.180	.200	.007	-.522		.015	.265	.495	.683	.825	206	.180	.300	.724	.411		-.027	-.220	-.437	-.692	-.827
205	.180	.300	.007	-.406		-.001	.204	.410	.586	.729	208	.180	.400	.634	.343		-.059	-.210	-.420	-.656	-.703
207	.180	.400	.007	-.377		-.047	.133	.334	.500	.645	210	.180	.500	.570	.288		-.094	-.228	-.434	-.577	-.630
209	.180	.500	-.667	-.382		-.087	.086	.282	.434	.577	212	.180	.600	.494	.191		-.135	-.255	-.436	-.490	-.594
211	.180	.600	-.594	-.387		-.116	.068	.213	.371	.512	214	.180	.700	.466	.170		-.154	-.268	-.426	-.466	-.588
213	.180	.700	-.579	-.383		-.120	.043	.200	.363	.491	216	.180	.800	.429	.173		-.130	-.243	-.407	-.457	-.585
215	.180	.800	-.584	-.379		-.095	.061	.214	.356	.462	218	.180	.900	.356	.140		-.130	-.236	-.384	-.456	-.581
217	.180	.900	-.563	-.365		-.084	.057	.214	.317	.400											
			$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open											$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open							
200	.180	.000			.943	.945	.954	.674	.212	-.323	202	.180	.100			.210	.051	-.448	-.609	-.771	-.853
201	.180	.100			-.229	.055	.347	.612	.807	.940	204	.180	.200			.142	-.011	-.246	-.466	-.729	-.848
203	.180	.200			-.132	.008	.258	.490	.678	.816	206	.180	.300			.100	-.020	-.215	-.420	-.707	-.821
205	.180	.300			-.124	-.006	.198	.406	.581	.720	208	.180	.400			.050	-.051	-.208	-.387	-.677	-.709
207	.180	.400			-.158	-.055	.127	.330	.496	.636	210	.180	.500			.025	-.084	-.227	-.407	-.603	-.636
209	.180	.500			-.170	-.091	.081	.280	.432	.570	212	.180	.600			-.019	-.128	-.254	-.427	-.515	-.592
211	.180	.600			-.204	-.120	.061	.211	.367	.506	214	.180	.700			-.055	-.146	-.268	-.428	-.480	-.583
213	.180	.700			-.198	-.119	.039	.195	.360	.485	216	.180	.800			-.040	-.126	-.243	-.416	-.471	-.576
215	.180	.800			-.186	-.106	.054	.209	.354	.457	218	.180	.900			-.058	-.126	-.233	-.392	-.474	-.567
217	.180	.900			-.166	-.091	.051	.210	.316	.397											

TABLE IV.- PRESSURE COEFFICIENTS MEASURED ON RIGHT HORIZONTAL TAIL

(a) M = 0.60

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Lower surface								Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper surface							
			$\alpha = -20^\circ$	$\alpha = -10^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 15^\circ$	$\alpha = 20^\circ$				$\alpha = -20^\circ$	$\alpha = -10^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 15^\circ$	$\alpha = 20^\circ$
			$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed											$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed							
304	.260	.200				-.146	-.212	-.258	-.255	-.421	300	.260	.000				.258	-.115	-.492	-.943	-1.366
306	.260	.300				-.151	-.206	-.259	-.299	-.375	301	.260	.100				-.042	.043	.121	.201	.301
308	.260	.400				-.163	-.211	-.262	-.311	-.388	303	.260	.200				-.064	.012	.085	.165	.274
310	.260	.500				-.175	-.216	-.260	-.315	-.393	307	.260	.400				-.117	-.056	.014	.099	.200
314	.260	.700				-.149	-.177	-.217	-.261	-.333	309	.260	.500				-.138	-.085	-.020	.064	.157
316	.260	.800				-.135	-.159	-.191	-.231	-.290	313	.260	.700				-.150	-.109	-.059	.011	.085
											315	.260	.800				-.143	-.112	-.074	-.017	.039
322	.620	.200				-.181	-.301	-.748	-1.373	-1.400	317	.260	.900				-.131	-.108	-.082	-.042	-.009
324	.620	.400				-.184	-.246	-.320	-.399	-1.094											
326	.620	.600				-.151	-.190	-.217	-.218	-.426	323	.620	.400				-.124	-.048	.033	.134	.224
328	.620	.800				-.095	-.117	-.139	-.158	-.292	327	.620	.800				-.105	-.081	-.043	.016	.045
			$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open											$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open							
304	.260	.200	-.117	-.126	-.054	-.085	-.165	-.178	-.177	-.401	300	.260	.000	-.301	.031	.356	.221	-.182	-.507	-.962	-1.335
306	.260	.300	-.063	-.118	-.058	-.089	-.161	-.176	-.218	-.324	301	.260	.100	-.077	-.020	.010	.057	.130	.196	.266	.350
308	.260	.400	-.046	-.121	-.072	-.107	-.158	-.182	-.230	-.335	303	.260	.200	-.093	-.067	-.002	.041	.098	.164	.238	.331
310	.260	.500	-.050	-.130	-.094	-.118	-.175	-.189	-.240	-.343	307	.260	.400	-.150	-.147	-.027	.004	.053	.112	.182	.265
314	.260	.700	-.041	-.115	-.102	-.119	-.169	-.175	-.221	-.302	309	.260	.500	-.174	-.170	-.044	-.018	.026	.081	.148	.223
316	.260	.800	-.039	-.108	-.112	-.124	-.169	-.171	-.211	-.278	313	.260	.700	-.187	-.173	-.075	-.057	-.027	.019	.074	.132
											315	.260	.800	-.178	-.160	-.102	-.089	-.066	-.029	.017	.060
322	.620	.200	-.068	-.067	-.123	-.173	-.351	-.721	-1.444	-1.247	317	.260	.900	-.153	-.137	-.129	-.122	-.110	-.079	-.044	-.017
324	.620	.400	-.030	-.104	-.145	-.174	-.247	-.302	-.401	-1.048											
326	.620	.600	-.018	-.110	-.145	-.161	-.207	-.244	-.228	-.461	323	.620	.400	-.281	-.164	-.108	-.074	-.012	.061	.145	.222
328	.620	.800	-1.881	-1.880	-.113	-.124	-.151	-.183	-.187	-.333	327	.620	.800	-.208	-.122	-.133	-.119	-.098	-.060	-.006	.020
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed											$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed							
304	.260	.200	.079	-.066		-.082	-.157	-.226	-.254	-.693	300	.260	.000	-.319	.204		.365	.153	-.365	-1.121	-1.588
306	.260	.300	.074	-.083		-.095	-.157	-.226	-.281	-.388	301	.260	.100	-.248	-.072		-.048	.044	.139	.269	.358
308	.260	.400	.060	-.104		-.112	-.169	-.231	-.300	-.404	303	.260	.200	-.242	-.093		-.073	.008	.100	.228	.323
310	.260	.500	.033	-.125		-.135	-.181	-.240	-.308	-.406	307	.260	.400	-.267	-.131		-.111	-.055	.026	.140	.230
314	.260	.700	.012	-.116		-.114	-.150	-.197	-.262	-.354	309	.260	.500	-.275	-.149		-.131	-.081	-.008	.096	.179
316	.260	.800	-.004	-.109		-.103	-.138	-.179	-.235	-.311	313	.260	.700	-.265	-.157		-.138	-.104	-.051	.030	.092
											315	.260	.800	-.245	-.148		-.132	-.106	-.067	-.007	.038
322	.620	.200	.136	-.159		-.114	-.248	-.639	-1.358	-1.306	317	.260	.900	-.211	-.130		-.114	-.099	-.076	-.040	-.017
324	.620	.400	.107	-.147		-.140	-.225	-.315	-.968	-1.645											
326	.620	.600	.053	-.123		-.126	-.174	-.215	-.225	-.620	323	.620	.400	-.465	-.151		-.140	-.056	.048	.172	.250
328	.620	.800	-.007	-.091		-.076	-.108	-.133	-.132	-.349	327	.620	.800	-.337	-.140		-.107	-.079	-.039	.020	.037
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open											$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open							
304	.260	.200			-.034	-.056	-.120	-.197	-.238	-.690	300	.260	.000			.430	.384	.182	-.306	-1.083	-1.559
306	.260	.300			-.052	-.072	-.123	-.192	-.247	-.368	301	.260	.100			-.069	-.031	.057	.152	.281	.365
308	.260	.400			-.074	-.091	-.135	-.199	-.268	-.381	303	.260	.200			-.090	-.052	.024	.109	.238	.329
310	.260	.500			-.100	-.115	-.153	-.213	-.282	-.385	307	.260	.400			-.118	-.095	-.039	.036	.150	.234
314	.260	.700			-.088	-.097	-.129	-.178	-.240	-.336	309	.260	.500			-.134	-.114	-.068	.002	.106	.183
316	.260	.800			-.081	-.089	-.116	-.159	-.216	-.296	313	.260	.700			-.138	-.126	-.093	-.043	.038	.095
											315	.260	.800			-.129	-.122	-.097	-.061	.001	.040
322	.620	.200			-.062	-.095	-.219	-.619	-1.279	-1.245	317	.260	.900			-.111	-.105	-.092	-.071	-.033	-.015
324	.620	.400			-.102	-.122	-.198	-.280	-.941	-1.574											
326	.620	.600			-.102	-.113	-.155	-.197	-.215	-.614	323	.620	.400			-.168	-.131	-.052	.051	.175	.250
328	.620	.800			-.063	-.067	-.095	-.123	-.119	-.342	327	.620	.800			-.112	-.098	-.074	-.034	.025	.042

TABLE IV.- PRESSURE COEFFICIENTS MEASURED ON RIGHT HORIZONTAL TAIL - Continued

(a) M = 0.60 - Concluded

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Lower surface α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°	Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper surface α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = -7.5°$; brakes closed											$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = -7.5°$; brakes closed							
304	.260	.200			-.072	-.103	-.178	-.254	-.260	-.647	300	.260	.000			.408	.360	.152	-.351	-1.113	-1.567
306	.260	.300			-.090	-.116	-.179	-.249	-.302	-.403	301	.260	.100			-.122	-.079	.016	.121	.247	.342
308	.260	.400			-.108	-.133	-.188	-.252	-.319	-.418	303	.260	.200			-.144	-.103	-.016	.084	.207	.308
310	.260	.500			-.130	-.154	-.199	-.258	-.326	-.423	307	.260	.400			-.164	-.137	-.073	.011	.124	.218
314	.260	.700			-.111	-.129	-.164	-.213	-.273	-.368	309	.260	.500			-.179	-.156	-.098	-.021	.082	.170
316	.260	.800			-.103	-.116	-.145	-.187	-.242	-.322	313	.260	.700			-.173	-.158	-.119	-.059	.020	.086
											315	.260	.800			-.157	-.146	-.118	-.074	-.012	.035
322	.620	.200			-.081	-.126	-.258	-.626	-1.429	-1.366	317	.260	.900			-.132	-.125	-.108	-.080	-.043	-.020
324	.620	.400			-.125	-.152	-.236	-.332	-.925	-1.656											
326	.620	.600			-.118	-.136	-.183	-.223	-.212	-.598	323	.620	.400			-.199	-.158	-.070	.039	.163	.246
328	.620	.800			-.073	-.084	-.112	-.140	-.132	-.335	327	.620	.800			-.129	-.115	-.087	-.042	.016	.040
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 7.5°$; brakes closed											$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 7.5°$; brakes closed							
304	.260	.200			.007	-.017	-.087	-.143	-.213	-.675	300	.260	.000			.491	.445	.141	-.342	-1.072	-1.538
306	.260	.300			-.006	-.027	-.084	-.142	-.211	-.340	301	.260	.100			.014	.048	.129	.213	.324	.403
308	.260	.400			-.025	-.043	-.091	-.149	-.228	-.348	303	.260	.200			.008	.038	.104	.176	.288	.375
310	.260	.500			-.053	-.071	-.114	-.162	-.248	-.356	307	.260	.400			-.003	.016	.062	.124	.219	.296
314	.260	.700			-.065	-.078	-.109	-.152	-.235	-.326	309	.260	.500			-.017	-.001	.035	.091	.178	.249
316	.260	.800			-.077	-.088	-.116	-.151	-.226	-.300	313	.260	.700			-.045	-.037	-.012	.029	.092	.145
											315	.260	.800			-.074	-.070	-.053	-.021	.029	.069
322	.620	.200			-.057	-.093	-.220	-.647	-1.246	-1.186	317	.260	.900			-.106	-.103	-.095	-.072	-.041	-.017
324	.620	.400			-.101	-.127	-.201	-.284	-.885	-1.478											
326	.620	.600			-.117	-.131	-.175	-.212	-.239	-.625	323	.620	.400			-.111	-.084	-.017	.071	.180	.254
328	.620	.800			-.089	-.097	-.128	-.159	-.165	-.387	327	.620	.800			-.120	-.112	-.093	-.059	.000	.018
			$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed											$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed							
304	.260	.200	.223	-.033		-.028	-.113	-.202	-.647	-1.272	300	.260	.000	-.839	.041		.522	.327	-.360	-1.341	-1.702
306	.260	.300	.205	-.028		-.055	-.121	-.206	-.294	-.545	301	.260	.100	-.608	-.021		-.051	.054	.195	.362	.435
308	.260	.400	.175	-.036		-.080	-.135	-.217	-.283	-.477	303	.260	.200	-.448	-.061		-.081	.026	.154	.306	.394
310	.260	.500	.130	-.050		-.109	-.153	-.226	-.295	-.447	307	.260	.400	-.459	-.134		-.102	-.035	.073	.196	.278
314	.260	.700	.069	-.046		-.100	-.128	-.191	-.259	-.383	309	.260	.500	-.459	-.158		-.119	-.059	.032	.139	.219
316	.260	.800	.032	-.051		-.090	-.115	-.172	-.232	-.342	313	.260	.700	-.430	-.168		-.127	-.087	-.018	.055	.113
											315	.260	.800	-.398	-.158		-.118	-.091	-.042	.009	.048
322	.620	.200	.283	.061		-.090	-.224	-.982	-1.153	-1.260	317	.260	.900	-.347	-.138		-.102	-.088	-.061	-.037	-.025
324	.620	.400	.211	.019		-.124	-.210	-.336	-1.434	-1.329											
326	.620	.600	.103	-.016		-.115	-.167	-.184	-.662	-1.159	323	.620	.400	-.774	-.288		-.154	-.049	.090	.206	.286
328	.620	.800	-.010	-.032		-.069	-.101	-.106	-.219	-.612	327	.620	.800	-.542	-.198		-.107	-.073	-.023	.010	.025
			$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open											$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open							
304	.260	.200			.063	.041	-.042	-.130	-.626	-1.256	300	.260	.000			.565	.538	.312	-.314	-1.284	-1.612
306	.260	.300			.043	.026	-.046	-.132	-.221	-.514	301	.260	.100			.013	.052	.140	.255	.417	.476
308	.260	.400			.020	.003	-.061	-.141	-.209	-.431	303	.260	.200			.011	.036	.123	.215	.367	.441
310	.260	.500			-.012	-.027	-.083	-.156	-.231	-.399	307	.260	.400			.017	.034	.085	.164	.277	.344
314	.260	.700			-.030	-.039	-.082	-.149	-.225	-.358	309	.260	.500			.006	.020	.060	.129	.227	.286
316	.260	.800			-.045	-.053	-.090	-.146	-.216	-.329	313	.260	.700			-.017	-.013	.011	.058	.127	.171
											315	.260	.800			-.045	-.043	-.028	.005	.056	.084
322	.620	.200			-.011	-.051	-.187	-.887	-1.074	-1.142	317	.260	.900			-.077	-.078	-.073	-.055	-.023	-.014
324	.620	.400			-.060	-.086	-.187	-.289	-1.378	-1.271											
326	.620	.600			-.087	-.100	-.159	-.192	-.655	-1.104	323	.620	.400			-.118	-.085	.001	.112	.226	.294
328	.620	.800			-.068	-.076	-.114	-.136	-.258	-.654	327	.620	.800			-.107	-.100	-.077	-.035	.011	.014

TABLE IV.- PRESSURE COEFFICIENTS MEASURED ON RIGHT HORIZONTAL TAIL - Continued

(b) M = 0.90

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Lower surface								Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper surface							
			$\alpha = -20^\circ$	$\alpha = -10^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 15^\circ$	$\alpha = 20^\circ$				$\alpha = -20^\circ$	$\alpha = -10^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 15^\circ$	$\alpha = 20^\circ$
			$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed											$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed							
304	.260	.200				-.156	-.217	-.242	-.311	-.774	300	.260	.000				.295	.022	-.329	-.934	-1.182
306	.260	.300				-.172	-.229	-.252	-.323	-.452	301	.260	.100				-.032	.043	.131	.211	.282
308	.260	.400				-.197	-.249	-.276	-.344	-.462	303	.260	.200				-.062	.011	.108	.195	.265
310	.260	.500				-.246	-.302	-.325	-.379	-.482	307	.260	.400				-.136	-.069	.031	.129	.205
314	.260	.700				-.270	-.328	-.348	-.369	-.441	309	.260	.500				-.173	-.107	-.007	.092	.165
316	.260	.800				-.270	-.322	-.346	-.344	-.405	313	.260	.700				-.248	-.182	-.071	.024	.090
											315	.260	.800				-.275	-.204	-.105	-.020	.035
322	.620	.200				-.263	-.428	-.836	-1.001	-1.059	317	.260	.900				-.269	-.224	-.146	-.077	-.037
324	.620	.400				-.307	-.383	-.511	-1.080	-1.209											
326	.620	.600				-.327	-.415	-.422	-.520	-.785	323	.620	.400				-.206	-.112	.027	.145	.212
328	.620	.800				-.199	-.224	-.228	-.370	-.547	327	.620	.800				-.278	-.219	-.115	-.043	-.005
			$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open											$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open							
304	.260	.200	-.072	-.134	.005	-.026	-.102	-.120	-.248	-1.000	300	.260	.000	-.342	-.460	.395	.282	-.013	-.402	-.909	-1.177
306	.260	.300	-.066	-.147	.003	-.026	-.091	-.113	-.221	-.498	301	.260	.100	-.301	.057	.079	.124	.190	.262	.327	.387
308	.260	.400	-.074	-.171	-.007	-.035	-.095	-.113	-.222	-.438	303	.260	.200	-.275	-.030	.070	.113	.179	.254	.318	.378
310	.260	.500	-.093	-.204	-.030	-.056	-.110	-.125	-.234	-.399	307	.260	.400	-.248	-.127	.058	.095	.149	.217	.278	.335
314	.260	.700	-.082	-.218	-.050	-.069	-.120	-.138	-.245	-.381	309	.260	.500	-.238	-.159	.046	.080	.131	.192	.249	.300
316	.260	.800	-.087	-.217	-.075	-.090	-.138	-.158	-.254	-.380	313	.260	.700	-.216	-.220	.018	.043	.080	.130	.174	.214
											315	.260	.800	-.206	-.233	-.021	-.003	.025	.065	.100	.131
322	.620	.200	-.034	-.215	-.096	-.142	-.411	-.817	-.860	-.919	317	.260	.900	-.190	-.236	-.092	-.082	-.061	-.029	-.003	.018
324	.620	.400	-.010	-.221	-.136	-.167	-.227	-.395	-.960	-1.108											
326	.620	.600	-.035	-.206	-.186	-.206	-.270	-.285	-.508	-.829	323	.620	.400	-.332	-.143	-.050	-.014	.048	.132	.200	.249
328	.620	.800	-.552	-.551	-.216	-.236	-.288	-.306	-.434	-.647	327	.620	.800	-.276	-.185	-.220	-.203	-.169	-.111	-.061	-.027
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed											$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed							
304	.260	.200	.046	-.112		-.075	-.140	-.188	-.538		300	.260	.000	-.573	-.201		.386	.228	-.180	-1.021	
306	.260	.300	.043	-.113		-.102	-.158	-.206	-.283		301	.260	.100	-.389	.076		-.030	.060	.159	.288	
308	.260	.400	.031	-.125		-.132	-.186	-.232	-.301		303	.260	.200	-.389	.030		-.060	.016	.123	.251	
310	.260	.500	.003	-.151		-.186	-.242	-.291	-.341		307	.260	.400	-.331	-.075		-.133	-.064	.048	.168	
314	.260	.700	-.004	-.150		-.211	-.264	-.306	-.349		309	.260	.500	-.329	-.122		-.171	-.102	.008	.122	
316	.260	.800	-.022	-.152		-.211	-.262	-.293	-.332		313	.260	.700	-.310	-.188		-.246	-.174	-.059	.044	
											315	.260	.800	-.299	-.200		-.269	-.197	-.094	-.004	
322	.620	.200	.113	-.118		-.166	-.318	-.833	-.955		317	.260	.900	-.276	-.198		-.259	-.215	-.134	-.065	
324	.620	.400	.084	-.117		-.232	-.332	-.466	-1.098												
326	.620	.600	.031	-.123		-.263	-.365	-.417	-.784		323	.620	.400	-.512	-.208		-.226	-.116	.049	.178	
328	.620	.800	-.035	-.114		-.173	-.194	-.203	-.439		327	.620	.800	-.453	-.197		-.276	-.226	-.109	-.036	
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open											$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open							
304	.260	.200			-.021	-.037	-.100	-.154	-.610	-.991	300	.260	.000			.460	.415	.246	-.197	-1.015	-1.163
306	.260	.300			-.049	-.065	-.118	-.170	-.274	-.501	301	.260	.100			-.022	.006	.086	.185	.303	.355
308	.260	.400			-.081	-.096	-.146	-.196	-.278	-.472	303	.260	.200			-.054	-.022	.044	.152	.268	.325
310	.260	.500			-.135	-.150	-.201	-.251	-.315	-.477	307	.260	.400			-.123	-.100	-.041	.067	.179	.244
314	.260	.700			-.158	-.172	-.226	-.265	-.325	-.450	309	.260	.500			-.160	-.138	-.083	.025	.131	.197
316	.260	.800			-.165	-.178	-.228	-.266	-.313	-.424	313	.260	.700			-.233	-.211	-.153	-.047	.048	.109
											315	.260	.800			-.258	-.235	-.180	-.085	-.003	.048
322	.620	.200			-.104	-.137	-.278	-.782		-1.057	317	.260	.900			-.257	-.242	-.205	-.130	-.065	-.030
324	.620	.400			-.177	-.200	-.291	-.457	-1.023	-1.090											
326	.620	.600			-.218	-.234	-.319	-.380	-.794	-.983	323	.620	.400			-.244	-.204	-.102	.058	.182	.249
328	.620	.800			-.157	-.161	-.189	-.212	-.438	-.658	327	.620	.800			-.283	-.268	-.217	-.105	-.035	.000

TABLE IV.- PRESSURE COEFFICIENTS MEASURED ON RIGHT HORIZONTAL TAIL - Continued

(b) M = 0.90 - Concluded

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Lower surface								Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper surface							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = -7.5°$; brakes closed											$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = -7.5°$; brakes closed							
304	.260	.200			-.089	-.111	-.179	-.219	-.387	-.752	300	.260	.000			.413	.371	.208	-.143	-.957	-1.156
306	.260	.300			-.116	-.135	-.198	-.235	-.303	-.491	301	.260	.100			-.098	-.066	.020	.125	.250	.315
308	.260	.400			-.145	-.165	-.226	-.264	-.333	-.497	303	.260	.200			-.133	-.094	-.015	.099	.219	.291
310	.260	.500			-.199	-.222	-.279	-.318	-.376	-.515	307	.260	.400			-.193	-.165	-.093	.025	.141	.217
314	.260	.700			-.226	-.255	-.311	-.349	-.379	-.484	309	.260	.500			-.231	-.202	-.131	-.013	.098	.174
316	.260	.800			-.229	-.256	-.317	-.337	-.358	-.451	313	.260	.700			-.304	-.280	-.212	-.081	.023	.090
											315	.260	.800			-.338	-.317	-.235	-.112	-.022	.036
322	.620	.200			-.154	-.192	-.346	-.803	-.995	-1.149	317	.260	.900			-.330	-.309	-.240	-.148	-.079	-.039
324	.620	.400			-.232	-.266	-.369	-.505	-1.239	-1.194											
326	.620	.600			-.274	-.314	-.419	-.463	-.730	-.964	323	.620	.400			-.293	-.254	-.144	.034	.164	.239
328	.620	.800			-.191	-.198	-.226	-.202	-.425	-.661	327	.620	.800			-.373	-.331	-.256	-.125	-.046	-.006
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 7.5°$; brakes closed											$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 7.5°$; brakes closed							
304	.260	.200			.073	.057	-.021	-.081	-.724	-1.053	300	.260	.000			.557	.514	.232	-.253	-1.005	-1.176
306	.260	.300			.065	.047	-.024	-.084	-.252	-.499	301	.260	.100			.094	.126	.203	.294	.401	.437
308	.260	.400			.050	.032	-.036	-.096	-.230	-.439	303	.260	.200			.092	.123	.188	.277	.381	.419
310	.260	.500			.021	.005	-.060	-.120	-.241	-.420	307	.260	.400			.094	.118	.162	.239	.324	.367
314	.260	.700			-.001	-.011	-.072	-.136	-.266	-.414	309	.260	.500			.087	.106	.144	.215	.289	.330
316	.260	.800			-.027	-.034	-.094	-.156	-.275	-.410	313	.260	.700			.057	.071	.098	.152	.207	.239
											315	.260	.800			.011	.025	.044	.085	.130	.156
322	.620	.200			-.014	-.058	-.313	-.789	-.879	-.996	317	.260	.900			-.065	-.053	-.041	-.012	.021	.038
324	.620	.400			-.078	-.104	-.229	-.444	-.954	-1.042											
326	.620	.600			-.138	-.150	-.239	-.323	-.797	-.965	323	.620	.400			-.044	-.009	.060	.164	.250	.293
328	.620	.800			-.154	-.165	-.246	-.312	-.548	-.727	327	.620	.800			-.189	-.177	-.150	-.085	-.031	.000
			$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed											$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed							
304	.260	.200	.189	.059		.004	-.079	-.196	-1.246	-1.418	300	.260	.000	-.791	.001		.575	.409	-.393	-1.170	-.010
306	.260	.300	.176	.052		-.027	-.104	-.166	-.540	-.880	301	.260	.100	-.659	-.039		-.005	.078	.268	.378	.430
308	.260	.400	.156	.032		-.064	-.138	-.211	-.423	-.660	303	.260	.200	-.524	-.058		-.045	.047	.229	.334	.400
310	.260	.500	.118	-.005		-.122	-.194	-.267	-.409	-.604	307	.260	.400	-.523	-.131		-.106	-.036	.126	.233	.302
314	.260	.700	.079	-.031		-.140	-.220	-.280	-.400	-.550	309	.260	.500	-.529	-.165		-.148	-.075	.076	.181	.251
316	.260	.800	.048	-.050		-.143	-.223	-.271	-.380	-.513	313	.260	.700	-.513	-.205		-.213	-.140	-.001	.088	.153
											315	.260	.800	-.492	-.212		-.232	-.163	-.043	.031	.086
322	.620	.200	.248	.107		-.094	-.263	-.715	-.955	-1.108	317	.260	.900	-.447	-.200		-.234	-.190	-.095	-.043	-.002
324	.620	.400	.200	.051		-.165	-.311	-.865	-1.044	-1.106											
326	.620	.600	.111	-.009		-.210	-.343	-.591	-1.191	-1.040	323	.620	.400	-.744	-.323		-.224	-.092	.115	.236	.307
328	.620	.800	.008	-.048		-.138	-.183	-.269	-.845	-.963	327	.620	.800	-.655	-.261		-.251	-.205	-.082	-.019	.029
			$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open											$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open							
304	.260	.200			.147	.129	.048	-.069	-1.201	-1.447	300	.260	.000			.646	.614	.427	-.442	-1.064	-.009
306	.260	.300			.132	.114	.044	-.040	-.515	-.868	301	.260	.100			.102	.137	.219	.388	.478	.512
308	.260	.400			.112	.097	.030	-.064	-.363	-.618	303	.260	.200			.096	.126	.206	.352	.449	.492
310	.260	.500			.078	.065	.003	-.094	-.316	-.545	307	.260	.400			.118	.139	.188	.299	.375	.422
314	.260	.700			.054	.046	-.013	-.113	-.321	-.510	309	.260	.500			.115	.131	.173	.268	.335	.379
316	.260	.800			.031	.026	-.035	-.136	-.321	-.491	313	.260	.700			.094	.102	.130	.197	.245	.280
											315	.260	.800			.054	.059	.078	.128	.165	.194
322	.620	.200			.054	.024	-.140	-.636	-.844	-1.077	317	.260	.900			-.018	-.016	-.008	.028	.051	.069
324	.620	.400			-.013	-.034	-.158	-.839	-.901	-1.069											
326	.620	.600			-.079	-.088	-.184	-.452	-1.107	-1.140	323	.620	.400			-.041	-.003	.082	.223	.305	.353
328	.620	.800			-.093	-.097	-.162	-.253	-.819	-.962	327	.620	.800			-.136	-.130	-.109	-.036	.008	.039

TABLE IV.- PRESSURE COEFFICIENTS MEASURED ON RIGHT HORIZONTAL TAIL - Continued

(c) M = 0.95

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Lower surface							Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper surface						
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx -5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed										$\beta \approx -5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed							
304	.260	.200				-.123	-.156	-.207	-.380	-.809	300	.260	.000				.324	.160	-.177	-.883	-.986
306	.260	.300				-.143	-.166	-.198	-.333	-.536	301	.260	.100				-.006	.046	.112	.163	.256
308	.260	.400				-.163	-.194	-.228	-.329	-.501	303	.260	.200				-.035	.017	.092	.160	.238
310	.260	.500				-.215	-.242	-.275	-.393	-.519	307	.260	.400				-.110	-.064	.023	.116	.191
314	.260	.700				-.261	-.292	-.316	-.433	-.536	309	.260	.500				-.153	-.100	-.011	.085	.163
316	.260	.800				-.268	-.299	-.332	-.440	-.537	313	.260	.700				-.222	-.170	-.071	.030	.104
											315	.260	.800				-.263	-.217	-.097	-.008	.058
322	.620	.200				-.243	-.318	-.658	-.931	-.979	317	.260	.900				-.283	-.232	-.130	-.058	-.007
324	.620	.400				-.282	-.332	-.359	+1.074	-1.129											
326	.620	.600				-.347	-.393	-.422	-.584	-.897	323	.620	.400				-.185	-.115	.020	.144	.224
328	.620	.800				-.310	-.369	-.413	-.511	-.761	327	.620	.800				-.304	-.230	-.125	-.043	.012
			$\beta \approx -5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open										$\beta \approx -5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open							
304	.260	.200	-.215	-.217	.043	.013	-.037	-.074	-.290	-.651	300	.260	.000	-.360	-.401	.418	.328	.108	-.330	-.899	-1.008
306	.260	.300	-.203	-.157	.046	.020	-.029	-.063	-.220	-.420	301	.260	.100	-.442	.029	.120	.153	.210	.283	.338	.375
308	.260	.400	-.195	-.152	.037	.013	-.034	-.060	-.212	-.375	303	.260	.200	-.419	-.031	.111	.143	.203	.278	.333	.374
310	.260	.500	-.220	-.175	.018	-.007	-.050	-.074	-.214	-.368	307	.260	.400	-.391	-.115	.099	.131	.183	.250	.306	.350
314	.260	.700	-.164	-.211	.002	-.014	-.056	-.082	-.214	-.365	309	.260	.500	-.380	-.147	.090	.119	.168	.230	.281	.324
316	.260	.800	-.162	-.227	-.019	-.033	-.072	-.101	-.221	-.357	313	.260	.700	-.332	-.205	.067	.090	.128	.177	.215	.249
											315	.260	.800	-.312	-.235	.034	.049	.079	.120	.148	.176
322	.620	.200	-.123	-.211	-.047	-.086	-.258	-.665	-.747	-.837	317	.260	.900	-.292	-.256	-.031	-.022	.001	.034	.051	.070
324	.620	.400	-.122	-.245	-.081	-.108	-.165	-.340	-.860	-1.002											
326	.620	.600	-.128	-.279	-.126	-.147	-.202	-.219	-.514	-.774	323	.620	.400	-.480	-.146	.003	.034	.092	.175	.237	.277
328	.620	.800	-.437	-.442	-.155	-.171	-.219	-.244	-.464	-.697	327	.620	.800	-.385	-.279	-.148	-.135	-.103	-.053	-.016	.013
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed										$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed							
304	.260	.200	-.117	-.097		-.043	-.077	-.155	-.537	-1.184	300	.260	.000	-.409	-.076		.471	.339	-.074	-.859	-1.112
306	.260	.300	-.106	-.107		-.070	-.099	-.168	-.296	-.795	301	.260	.100	-.504	.094		.007	.072	.147	.241	.323
308	.260	.400	-.073	-.129		-.101	-.129	-.197	-.312	-.637	303	.260	.200	-.592	.035		-.024	.031	.116	.213	.298
310	.260	.500	-.083	-.169		-.159	-.188	-.251	-.368	-.574	307	.260	.400	-.534	-.068		-.103	-.053	.042	.151	.238
314	.260	.700	-.039	-.197		-.196	-.236	-.292	-.409	-.595	309	.260	.500	-.531	-.112		-.143	-.091	.006	.114	.198
316	.260	.800	-.044	-.212		-.211	-.250	-.320	-.420	-.608	313	.260	.700	-.476	-.188		-.217	-.158	-.055	.050	.125
											315	.260	.800	-.433	-.238		-.252	-.204	-.081	.011	.074
322	.620	.200	.045	-.188		-.141	-.239	-.583	-.911	-1.019	317	.260	.900	-.368	-.258		-.271	-.218	-.119	-.042	.007
324	.620	.400	.033	-.205		-.206	-.275	-.397	+1.098	-1.105											
326	.620	.600	-.003	-.224		-.291	-.348	-.433	-.822	-1.207	323	.620	.400	-.649	-.175		-.196	-.110	.048	.181	.260
328	.620	.800	-.049	-.197		-.256	-.331	-.419	-.536	-1.011	327	.620	.800	-.538	-.294		-.312	-.227	-.117	-.029	.029
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open										$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open							
304	.260	.200			.007	-.003	-.038	-.122	-.485	-1.072	300	.260	.000			.481	.447	.320	-.087	-.893	-1.065
306	.260	.300			-.022	-.032	-.061	-.133	-.278	-.688	301	.260	.100			.025	.040	.100	.175	.262	.332
308	.260	.400			-.057	-.065	-.092	-.160	-.291	-.554	303	.260	.200			-.010	.012	.060	.144	.235	.308
310	.260	.500			-.116	-.126	-.151	-.219	-.343	-.513	307	.260	.400			-.083	-.069	-.025	.064	.163	.243
314	.260	.700			-.147	-.158	-.186	-.258	-.375	-.547	309	.260	.500			-.122	-.109	-.068	.024	.124	.202
316	.260	.800			-.163	-.171	-.210	-.274	-.386	-.551	313	.260	.700			-.192	-.177	-.139	-.041	.056	.125
											315	.260	.800			-.230	-.221	-.178	-.072	.014	.073
322	.620	.200			-.093	-.111	-.207	-.611	-.879	-.969	317	.260	.900			-.253	-.242	-.197	-.112	-.042	.005
324	.620	.400			-.170	-.182	-.239	-.359	+1.015	-1.020											
326	.620	.600			-.236	-.253	-.311	-.396	-.797	-1.096	323	.620	.400			-.200	-.173	-.098	.057	.186	.261
328	.620	.800			-.216	-.220	-.293	-.387	-.514	-.894	327	.620	.800			-.305	-.285	-.212	-.114	-.028	.027

TABLE IV.- PRESSURE COEFFICIENTS MEASURED ON RIGHT HORIZONTAL TAIL - Continued

(c) M = 0.95 - Concluded

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Lower surface α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°	Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper surface α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = -7.5°$; brakes closed											$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = -7.5°$; brakes closed							
304	.260	.200			-.064	-.082	-.120	-.177	-.615	-1.196	300	.260	.000			.433	.396	.282	.003	-.723	-1.107
306	.260	.300			-.091	-.106	-.143	-.191	-.304	-.796	301	.260	.100			-.049	-.035	.029	.109	.204	.298
308	.260	.400			-.118	-.132	-.169	-.219	-.331	-.630	303	.260	.200			-.089	-.066	-.006	.080	.182	.276
310	.260	.500			-.171	-.184	-.225	-.270	-.380	-.567	307	.260	.400			-.146	-.132	-.081	.007	.123	.215
314	.260	.700			-.216	-.229	-.285	-.329	-.438	-.607	309	.260	.500			-.190	-.176	-.116	-.030	.088	.176
316	.260	.800			-.234	-.255	-.286	-.352	-.454	-.626	313	.260	.700			-.260	-.244	-.195	-.099	.026	.105
											315	.260	.800			-.311	-.301	-.243	-.124	-.010	.058
322	.620	.200			-.144	-.162	-.274	-.510	-.959	-1.027	317	.260	.900			-.326	-.310	-.258	-.145	-.057	-.005
324	.620	.400			-.214	-.243	-.322	-.419	-1.122	-1.154											
326	.620	.600			-.310	-.324	-.391	-.467	-.820	-1.229	323	.620	.400			-.247	-.221	-.137	.006	.162	.248
328	.620	.800			-.263	-.289	-.368	-.446	-.566	-1.037	327	.620	.800			-.374	-.355	-.262	-.138	-.037	.021
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 7.5°$; brakes closed											$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 7.5°$; brakes closed							
304	.260	.200			.113	.099	.053	-.037	-.258	-1.012	300	.260	.000			.540	.506	.329	-.189	-.866	-1.050
306	.260	.300			.107	.094	.054	-.027	-.181	-.570	301	.260	.100			.138	.157	.222	.315	.389	.449
308	.260	.400			.095	.083	.044	-.034	-.171	-.435	303	.260	.200			.135	.155	.207	.302	.377	.437
310	.260	.500			.067	.057	.017	-.054	-.188	-.401	307	.260	.400			.139	.155	.193	.272	.338	.393
314	.260	.700			.052	.045	.005	-.067	-.202	-.414	309	.260	.500			.133	.146	.180	.251	.309	.359
316	.260	.800			.027	.022	-.017	-.093	-.222	-.404	313	.260	.700			.108	.118	.144	.196	.240	.278
											315	.260	.800			.067	.077	.096	.138	.170	.200
322	.620	.200			.030	.007	-.093	-.587	-.786	-.870	317	.260	.900			-.004	.005	.017	.048	.069	.091
324	.620	.400			-.028	-.042	-.111	-.316	-.851	-.890											
326	.620	.600			-.083	-.095	-.152	-.243	-.549	-.957	323	.620	.400			.013	.038	.096	.203	.276	.323
328	.620	.800			-.119	-.122	-.178	-.247	-.449	-.809	327	.620	.800			-.136	-.123	-.093	-.033	.010	.043
			$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed											$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed							
304	.260	.200	.108	.024		.039	-.010	-.178	-1.124	-1.377	300	.260	.000	-.706	.185		.604	.500	-.045	-.971	-.017
306	.260	.300	.113	-.010		.002	-.041	-.165	-.391	-1.176	301	.260	.100	-.634	.002		.029	.086	.214	.330	.415
308	.260	.400	.107	-.049		-.034	-.078	-.199	-.389	-.811	303	.260	.200	-.496	-.038		-.012	.057	.176	.299	.393
310	.260	.500	.086	-.103		-.100	-.143	-.256	-.433	-.596	307	.260	.400	-.531	-.121		-.077	-.026	.088	.211	.312
314	.260	.700	.076	-.146		-.130	-.183	-.301	-.474	-.591	309	.260	.500	-.547	-.154		-.120	-.065	.045	.166	.266
316	.260	.800	.054	-.163		-.147	-.207	-.324	-.490	-.566	313	.260	.700	-.558	-.218		-.189	-.129	-.022	.091	.181
											315	.260	.800	-.529	-.253		-.225	-.162	-.054	.043	.123
322	.620	.200	.210	-.148		-.079	-.199	-.552	-.980	-1.058	317	.260	.900	-.484	-.287		-.239	-.173	-.095	-.018	.046
324	.620	.400	.182	-.186		-.148	-.244	-.568	-1.073	-1.074											
326	.620	.600	.116	-.207		-.230	-.327	-.493	-1.178	-1.068	323	.620	.400	-.871	-.247		-.197	-.083	.080	.235	.330
328	.620	.800	.027	-.192		-.201	-.308	-.456	-.945	-.965	327	.620	.800	-.645	-.383		-.301	-.204	-.107	-.004	.070
			$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open											$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open							
304	.260	.200			.183	.175	.120	.010	-.978	-1.407	300	.260	.000			.669	.649	.531	-.313	-1.047	-.015
306	.260	.300			.169	.162	.112	-.007	-.293	-1.046	301	.260	.100			.148	.172	.233	.393	.461	.522
308	.260	.400			.148	.146	.099	-.025	-.252	-.653	303	.260	.200			.139	.160	.228	.369	.441	.506
310	.260	.500			.120	.115	.067	-.053	-.249	-.515	307	.260	.400			.165	.181	.220	.323	.383	.446
314	.260	.700			.105	.104	.051	-.061	-.255	-.493	309	.260	.500			.163	.176	.209	.296	.351	.408
316	.260	.800			.082	.081	.030	-.083	-.269	-.487	313	.260	.700			.145	.155	.176	.236	.274	.319
											315	.260	.800			.109	.116	.132	.174	.203	.238
322	.620	.200			.092	.024	-.046	-.570	-.839	-1.033	317	.260	.900			.039	.046	.052	.080	.097	.124
324	.620	.400			.031	-.032	-.075	-.723	-.880	-1.039											
326	.620	.600			-.034	-.049	-.119	-.361	-.973	-1.134	323	.620	.400			.015	.045	.121	.256	.325	.382
328	.620	.800			-.054	-.774	-.131	-.265	-.712	-1.025	327	.620	.800			-.090	-.085	-.062	.004	.046	.087

TABLE IV.- PRESSURE COEFFICIENTS MEASURED ON RIGHT HORIZONTAL TAIL - Continued

(d) M = 1.03

Pressure coefficients c_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Lower surface								Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper surface							
			$\alpha = -20^\circ$	$\alpha = -10^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 15^\circ$	$\alpha = 20^\circ$				$\alpha = -20^\circ$	$\alpha = -10^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 15^\circ$	$\alpha = 20^\circ$
			$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed											$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed							
304	.260	.200				-.005	-.056	-.199	-.701	-.956	300	.260	.000				.390	.235	-.153	-.605	-.815
306	.260	.300				-.026	-.064	-.207	-.340	-.855	301	.260	.100				.106	.141	.160	.221	.377
308	.260	.400				-.046	-.096	-.225	-.341	-.537	303	.260	.200				.083	.116	.140	.183	.342
310	.260	.500				-.094	-.134	-.257	-.346	-.445	307	.260	.400				.014	.040	.070	.134	.270
314	.260	.700				-.127	-.175	-.273	-.353	-.480	309	.260	.500				-.031	-.004	.032	.113	.236
316	.260	.800				-.126	-.184	-.279	-.322	-.502	313	.260	.700				-.092	-.073	-.026	.081	.181
											315	.260	.800				-.133	-.092	-.037	.058	.144
322	.620	.200				-.127	-.228	-.601	-.859	-.938	317	.260	.900				-.138	-.112	-.059	.023	.092
324	.620	.400				-.162	-.230	-.460	-1.029	-1.091											
326	.620	.600				-.215	-.284	-.374	-.673	-1.097	323	.620	.400				-.057	-.018	.069	.183	.281
328	.620	.800				-.183	-.261	-.365	-.459	-.851	327	.620	.800				-.156	-.110	-.034	.042	.108
			$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open											$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open							
304	.260	.200	-.022	-.090	.152	.128	.071	-.003	-.435	-.939	300	.260	.000	-.240	-.294	.473	.412	.199	-.211	-.735	-.785
306	.260	.300	-.047	-.075	.152	.132	.079	-.002	-.154	-.631	301	.260	.100	-.380	-.088	.228	.262	.302	.338	.388	.489
308	.260	.400	-.065	-.059	.143	.125	.074	.000	-.118	-.431	303	.260	.200	-.345	-.082	.210	.250	.296	.333	.383	.475
310	.260	.500	-.116	-.104	.126	.104	.057	-.003	-.147	-.323	307	.260	.400	-.356	-.131	.196	.232	.278	.315	.363	.433
314	.260	.700	-.145	-.134	.110	.099	.056	.000	-.120	-.290	309	.260	.500	-.360	-.147	.187	.221	.265	.299	.344	.407
316	.260	.800	-.136	-.146	.088	.080	.040	-.015	-.113	-.288	313	.260	.700	-.372	-.179	.166	.195	.229	.257	.292	.339
											315	.260	.800	-.336	-.225	.136	.158	.185	.208	.234	.272
322	.620	.200	-.133	-.106	.061	.028	-.143	-.524	-.733	-.788	317	.260	.900	-.336	-.241	.078	.097	.114	.131	.149	.178
324	.620	.400	-.143	-.162	.033	.010	-.054	-.324	-.973	-.946											
326	.620	.600	-.113	-.210	-.006	-.026	-.085	-.139	-.379	-.815	323	.620	.400	-.494	-.195	.109	.147	.197	.247	.298	.355
328	.620	.800	-.292	-.290	-.029	-.044	-.094	-.154	-.287	-.608	327	.620	.800	-.485	-.288	-.023	-.004	.021	.050	.080	.119
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed											$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed							
304	.260	.200	.048	-.012		.052	.004	-.138	-.855	-1.097	300	.260	.000	-.256	-.055		.526	.369	-.015	-.536	-.004
306	.260	.300	.013	-.040		.030	-.014	-.128	-.228	-.957	301	.260	.100	-.520	.016		.106	.168	.189	.250	.383
308	.260	.400	-.017	-.075		.003	-.038	-.139	-.177	-.544	303	.260	.200	-.454	-.196		.079	.125	.153	.216	.351
310	.260	.500	-.076	-.128		-.050	-.091	-.177	-.242	-.451	307	.260	.400	-.411	-.072		.008	.042	.077	.163	.288
314	.260	.700	-.103	-.164		-.077	-.137	-.232	-.331	-.501	309	.260	.500	-.437	-.099		-.036	.000	.041	.135	.256
316	.260	.800	-.063	-.175		-.083	-.136	-.250	-.360	-.515	313	.260	.700	-.478	-.156		-.097	-.070	-.002	.092	.202
											315	.260	.800	-.487	-.197		-.133	-.099	-.031	.070	.165
322	.620	.200	.026	-.179		-.035	-.149	-.485	-.790	-.967	317	.260	.900	-.494	-.222		-.132	-.101	-.045	.036	.109
324	.620	.400	.012	-.190		-.106	-.197	-.343	-.941	-1.069											
326	.620	.600	-.014	-.209		-.169	-.251	-.366	-.914	-1.148	323	.620	.400	-.568	-.156		-.073	-.014	.090	.209	.326
328	.620	.800	-.031	-.203		-.123	-.227	-.357	-.539	-1.005	327	.620	.800	-.576	-.298		-.166	-.105	-.026	.054	.128
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open											$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open							
304	.260	.200			.109	.088	.037	-.091	-.796	-.996	300	.260	.000			.556	.506	.321	-.017	-.546	-.896
306	.260	.300			.081	.063	.025	-.082	-.076	-.714	301	.260	.100			.124	.135	.200	.215	.271	.397
308	.260	.400			.049	.035	-.001	-.099	-.147	-.487	303	.260	.200			.097	.110	.155	.180	.240	.366
310	.260	.500			-.007	-.021	-.055	-.154	-.244	-.456	307	.260	.400			.036	.038	.071	.097	.170	.297
314	.260	.700			-.032	-.042	-.089	-.195	-.327	-.485	309	.260	.500			-.004	-.002	.030	.059	.138	.263
316	.260	.800			-.046	-.051	-.092	-.214	-.348	-.481	313	.260	.700			-.070	-.069	-.033	.003	.088	.203
											315	.260	.800			-.092	-.085	-.060	-.022	.062	.162
322	.620	.200			.004	-.011	-.112	-.461	-.768	-.865	317	.260	.900			-.117	-.111	-.082	-.042	.028	.108
324	.620	.400			-.058	-.070	-.145	-.311	-.907	-.917											
326	.620	.600			-.131	-.134	-.198	-.340	-.818	-1.061	323	.620	.400			-.072	-.056	.012	.095	.205	.328
328	.620	.800			-.099	-.103	-.188	-.319	-.559	-.912	327	.620	.800			-.166	-.149	-.090	-.025	.046	.128

TABLE IV.- PRESSURE COEFFICIENTS MEASURED ON RIGHT HORIZONTAL TAIL - Continued

(a) M = 1.03 - Concluded

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Lower surface							Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper surface						
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = -7.5°$; brakes closed										$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = -7.5°$; brakes closed							
304	.260	.200			.031	.013	-.024	-.167	-.830	-1.080	300	.260	.000			.493	.451	.325	.018	-.442	-.856
306	.260	.300			.012	-.001	-.037	-.158	-.391	-1.028	301	.260	.100			.058	.065	.124	.157	.204	.358
308	.260	.400			-.014	-.025	-.061	-.180	-.278	-.685	303	.260	.200			.024	.041	.088	.130	.177	.326
310	.260	.500			-.062	-.070	-.103	-.203	-.263	-.481	307	.260	.400			-.025	-.017	.023	.068	.133	.262
314	.260	.700			-.090	-.103	-.157	-.251	-.350	-.515	309	.260	.500			-.069	-.060	-.017	.035	.102	.229
316	.260	.800			-.104	-.114	-.163	-.271	-.369	-.530	313	.260	.700			-.125	-.113	-.078	-.036	.047	.176
											315	.260	.800			-.159	-.151	-.129	-.056	.037	.142
322	.620	.200			-.051	-.058	-.165	-.444	-.798	-1.039	317	.260	.900			-.184	-.175	-.132	-.081	.015	.094
324	.620	.400			-.121	-.133	-.205	-.367	-.948	-1.107											
326	.620	.600			-.193	-.193	-.270	-.392	-.893	-1.102	323	.620	.400			-.110	-.087	-.018	.065	.182	.309
328	.620	.800			-.148	-.152	-.244	-.377	-.559	-1.053	327	.620	.800			-.224	-.204	-.138	-.053	.041	.119
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 7.5°$; brakes closed										$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 7.5°$; brakes closed							
304	.260	.200			.227	.210	.145	.025	-.823	-1.136	300	.260	.000			.619	.576	.332	-.018	-.752	-.003
306	.260	.300			.219	.203	.148	.048	-.081	-.747	301	.260	.100			.248	.268	.337	.365	.432	.503
308	.260	.400			.206	.191	.140	.042	-.078	-.416	303	.260	.200			.245	.263	.321	.355	.424	.496
310	.260	.500			.181	.165	.120	.028	-.078	-.291	307	.260	.400			.247	.261	.302	.334	.399	.463
314	.260	.700			.163	.154	.107	.023	-.075	-.275	309	.260	.500			.239	.251	.289	.320	.377	.436
316	.260	.800			.140	.133	.087	.000	-.087	-.255	313	.260	.700			.213	.225	.254	.279	.322	.367
											315	.260	.800			.174	.186	.210	.229	.261	.298
322	.620	.200			.140	.111	-.035	-.602	-.731	-.864	317	.260	.900			.110	.120	.138	.150	.172	.200
324	.620	.400			.088	.069	-.011	-.119	-.919	-.832											
326	.620	.600			.037	.025	-.045	-.155	-.509	-.938	323	.620	.400			.128	.153	.217	.278	.352	.407
328	.620	.800			.004	-.002	-.067	-.174	-.344	-.754	327	.620	.800			-.008	.005	.040	.074	.117	.154
			$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed										$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed							
304	.260	.200	.051	.102		.110	.047	-.149	-.980	-1.198	300	.260	.000	-.348	.153		.651	.466	-.018	-.692	-.005
306	.260	.300	.098	.062		.081	.025	-.136	-.257	-1.137	301	.260	.100	-.547	-.037		.111	.175	.254	.366	.468
308	.260	.400	.116	.021		.050	-.005	-.147	-.318	-.709	303	.260	.200	-.419	-.062		.074	.142	.226	.343	.448
310	.260	.500	.108	-.043		-.008	-.064	-.198	-.359	-.500	307	.260	.400	-.430	-.127		.012	.063	.150	.269	.379
314	.260	.700	.135	-.088		-.034	-.107	-.242	-.432	-.548	309	.260	.500	-.455	-.158		-.033	.026	.114	.231	.339
316	.260	.800	.125	-.097		-.040	-.103	-.273	-.436	-.567	313	.260	.700	-.524	-.210		-.094	-.037	.062	.170	.267
											315	.260	.800	-.557	-.237		-.124	-.043	.040	.132	.217
322	.620	.200	.238	-.052		.015	-.137	-.576	-.911	-1.012	317	.260	.900	-.567	-.261		-.115	-.062	.011	.083	.150
324	.620	.400	.232	-.106		-.049	-.186	-.624	-1.088	-1.111											
326	.620	.600	.186	-.128		-.127	-.236	-.431	-1.098	-1.048	323	.620	.400	-.690	-.243		-.087	.024	.172	.305	.406
328	.620	.800	.115	-.137		-.085	-.216	-.401	-.836	-1.029	327	.620	.800	-.724	-.340		-.192	-.079	.011	.099	.173
			$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open										$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open							
304	.260	.200			.289	.274	.204	-.016	-1.102	-1.204	300	.260	.000			.752	.718	.542	-.047	-.855	-.005
306	.260	.300			.274	.263	.201	.040	-.231	-1.130	301	.260	.100			.253	.280	.340	.424	.509	.575
308	.260	.400			.258	.247	.189	.026	-.172	-.680	303	.260	.200			.246	.268	.331	.409	.498	.564
310	.260	.500			.228	.218	.162	.003	-.164	-.362	307	.260	.400			.267	.283	.322	.380	.456	.517
314	.260	.700			.209	.204	.146	.013	-.160	-.363	309	.260	.500			.265	.278	.311	.360	.428	.485
316	.260	.800			.187	.186	.124	.002	-.157	-.354	313	.260	.700			.249	.258	.281	.314	.364	.408
											315	.260	.800			.214	.220	.239	.262	.299	.335
322	.620	.200			.197	.177	.029	-.489	-.886	-.986	317	.260	.900			.149	.154	.165	.179	.203	.231
324	.620	.400			.138	.126	.021	-.549	-.942	-1.063											
326	.620	.600			.076	.076	-.021	-.196	-.892	-1.092	323	.620	.400			.129	.159	.238	.327	.412	.466
328	.620	.800			.057	.061	-.042	-.180	-.588	-.920	327	.620	.800			.029	.034	.063	.106	.156	.195

TABLE IV.- PRESSURE COEFFICIENTS MEASURED ON RIGHT HORIZONTAL TAIL - Continued

(e) M = 1.18

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Lower surface								Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper surface							
			$\alpha \approx -20^\circ$	$\alpha = -10^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 15^\circ$	$\alpha = 20^\circ$				$\alpha \approx -20^\circ$	$\alpha = -10^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 15^\circ$	$\alpha = 20^\circ$
			$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed											$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed							
304	.260	.200				-.060	-.148	-.381	-.561	-.711	300	.260	.000				.422	.142	-.128	-.408	-.655
306	.260	.300				-.066	-.130	-.213	-.242	-.637	301	.260	.100				.064	.118	.170	.242	.437
308	.260	.400				-.082	-.138	-.232	-.272	-.459	303	.260	.200				.034	.075	.127	.271	.411
310	.260	.500				-.112	-.151	-.250	-.296	-.394	307	.260	.400				-.042	-.020	.143	.208	.348
314	.260	.700				-.122	-.162	-.230	-.313	-.421	309	.260	.500				-.064	.052	.096	.181	.319
316	.260	.800				-.112	-.138	-.198	-.318	-.402	313	.260	.700				-.018	.007	.047	.129	.282
											315	.260	.800				-.042	-.017	.021	.099	.260
322	.620	.200				-.131	-.286	-.464	-.644	-.748	317	.260	.900				-.064	-.033	.007	.107	.227
324	.620	.400				-.159	-.225	-.517	-.704	-.797											
326	.620	.600				-.191	-.249	-.373	-.693	-.801	323	.620	.400				.057	.072	.142	.215	.369
328	.620	.800				-.130	-.148	-.282	-.396	-.692	327	.620	.800				-.063	-.007	.032	.162	.250
			$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open											$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open							
304	.260	.200	.011	-.057	.025	-.009	-.133	-.376	-.616	-.737	300	.260	.000	-.157	-.340	.454	.362	.117	-.150	-.487	-.658
306	.260	.300	-.020	-.044	.059	.038	-.054	-.187	-.205	-.726	301	.260	.100	-.295	.007	.130	.167	.179	.277	.441	.592
308	.260	.400	.024	-.051	.109	.092	.030	-.071	-.220	-.497	303	.260	.200	-.293	-.052	.101	.152	.244	.325	.450	.579
310	.260	.500	.006	-.096	.166	.151	.094	.107	-.106	-.311	307	.260	.400	-.280	-.133	.118	.239	.319	.375	.456	.551
314	.260	.700	-.026	-.100	.212	.202	.178	.146	-.030	-.181	309	.260	.500	-.270	-.139	.126	.254	.330	.383	.447	.531
316	.260	.800	-.033	-.083	.203	.192	.178	.142	.025	-.154	313	.260	.700	-.251	-.037	.235	.275	.333	.371	.415	.478
											315	.260	.800	-.262	-.038	.231	.259	.306	.336	.370	.420
322	.620	.200	-.004	-.073	.171	.139	-.347	-.506	-.695	-.738	317	.260	.900	-.265	-.047	.205	.220	.254	.277	.302	.340
324	.620	.400	-.026	-.128	.149	.112	.122	-.558	-.812	-.846											
326	.620	.600	-.053	-.135	.128	.104	.090	.095	-.341	-.709	323	.620	.400	-.455	-.094	.225	.264	.326	.368	.417	.477
328	.620	.800	-.066	-.073	.121	.107	.049	.064	-.088	-.475	327	.620	.800	-.445	-.103	.147	.162	.190	.210	.243	.277
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed											$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed							
304	.260	.200	.156	.077		.094	.013	-.355	-.665	-.815	300	.260	.000	-.170	.126		.558	.333	.014	-.315	-.609
306	.260	.300	.114	.040		.074	.012	-.127	-.368	-.800	301	.260	.100	-.555	-.097		.154	.213	.248	.351	.461
308	.260	.400	.086	.011		.046	-.011	-.102	-.187	-.569	303	.260	.200	-.337	-.082		.120	.165	.218	.307	.424
310	.260	.500	.046	-.021		-.004	-.049	-.078	-.209	-.383	307	.260	.400	-.315	-.070		.038	.089	.135	.230	.354
314	.260	.700	.018	-.032		-.027	-.061	-.096	-.233	-.386	309	.260	.500	-.302	-.077		.012	.042	.099	.190	.323
316	.260	.800	.015	-.042		-.043	-.073	-.132	-.241	-.392	313	.260	.700	-.322	-.091		-.037	-.001	.069	.138	.289
											315	.260	.800	-.336	-.103		-.055	-.026	.033	.096	.273
322	.620	.200	.056	.019		.009	-.139	-.422	-.624	-.795	317	.260	.900	-.345	-.118		-.067	-.041	.022	.131	.244
324	.620	.400	.038	-.039		-.053	-.127	-.563	-.728	-.831											
326	.620	.600	.053	-.087		-.144	-.197	-.253	-.735	-.793	323	.620	.400	-.580	-.148		-.012	.069	.167	.267	.405
328	.620	.800	.108	-.098		-.085	-.154	-.249	-.493	-.825	327	.620	.800	-.441	-.168		-.101	-.034	.060	.198	.277
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open											$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open							
304	.260	.200			.169	.137	.072	-.297	-.664	-.807	300	.260	.000			.603	.541	.300	-.044	-.376	-.637
306	.260	.300			.140	.126	.056	.020	-.179	-.739	301	.260	.100			.168	.205	.258	.293	.370	.464
308	.260	.400			.106	.098	.054	-.008	-.117	-.399	303	.260	.200			.144	.176	.221	.250	.325	.426
310	.260	.500			.063	.058	.020	.001	-.152	-.313	307	.260	.400			.086	.097	.122	.155	.236	.346
314	.260	.700			.009	.008	-.021	-.079	-.189	-.343	309	.260	.500			.039	.050	.075	.125	.196	.310
316	.260	.800			.012	-.004	-.045	-.097	-.209	-.355	313	.260	.700			-.015	-.005	.024	.080	.139	.271
											315	.260	.800			-.036	-.025	-.006	.045	.095	.253
322	.620	.200			.077	.045	-.073	-.303	-.549	-.736	317	.260	.900			-.050	-.041	-.024	.016	.113	.230
324	.620	.400			.005	-.009	-.084	-.400	-.644	-.803											
326	.620	.600			-.075	-.074	-.135	-.300	-.658	-.806	323	.620	.400			-.012	.022	.090	.175	.271	.394
328	.620	.800			-.045	-.046	-.118	-.225	-.417	-.750	327	.620	.800			-.100	-.081	-.018	.056	.177	.264

TABLE IV.- PRESSURE COEFFICIENTS MEASURED ON RIGHT HORIZONTAL TAIL - Concluded

(e) M = 1.18 - Concluded

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Lower surface							Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper surface						
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15° α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15° α = 20°
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = -7.5°$; brakes closed										$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = -7.5°$; brakes closed						
304	.260	.200			.048	.030	-.055	-.375	-.666 -.769	300	.260	.000			.544	.486	.276	.009	-.273 -.506
306	.260	.300			.014	-.004	-.078	-.242	-.527 -.736	301	.260	.100			.026	.078	.148	.170	.243 .404
308	.260	.400			-.015	-.032	-.093	-.203	-.266 -.667	303	.260	.200			.002	.045	.080	.118	.191 .383
310	.260	.500			-.063	-.067	-.124	-.205	-.304 -.456	307	.260	.400			-.043	-.037	-.013	.010	.203 .329
314	.260	.700			-.086	-.091	-.144	-.191	-.304 -.433	309	.260	.500			-.085	-.084	-.064	.100	.171 .295
316	.260	.800			-.097	-.097	-.125	-.188	-.298 -.436	313	.260	.700			-.059	-.036	-.006	.069	.130 .242
										315	.260	.800			-.083	-.065	-.025	.032	.090 .218
322	.620	.200			-.030	-.053	-.205	-.452	-.644 -.779	317	.260	.900				-.081	-.045	.016	.101 .203
324	.620	.400			-.094	-.098	-.205	-.443	-.715 -.820										
326	.620	.600			-.176	-.176	-.252	-.360	-.711 -.818	323	.620	.400			-.123	-.096	.066	.155	.249 .366
328	.620	.800			-.143	-.145	-.208	-.317	-.624 -.775	327	.620	.800			-.145	-.106	-.038	.049	.159 .250
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 7.5°$; brakes closed										$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 7.5°$; brakes closed						
304	.260	.200			.198	.183	.107	-.241	-.647 -.820	300	.260	.000			.600	.553	.308	-.004	-.381 .014
306	.260	.300			.221	.214	.152	.099	-.315 -.761	301	.260	.100			.203	.229	.279	.336	.471 .592
308	.260	.400			.238	.232	.186	.184	-.036 -.476	303	.260	.200			.148	.152	.161	.167	.175 .580
310	.260	.500			.243	.235	.191	.131	.034 -.236	307	.260	.400			.300	.316	.355	.408	.471 .558
314	.260	.700			.262	.255	.212	.155	.116 -.140	309	.260	.500			.311	.325	.363	.412	.466 .540
316	.260	.800			.249	.244	.202	.144	.109 -.120	313	.260	.700			.310	.325	.357	.396	.439 .491
										315	.260	.800			.286	.302	.329	.359	.394 .436
322	.620	.200			.208	.171	.003	-.310	-.539 -.722	317	.260	.900			.238	.254	.275	.297	.321 .355
324	.620	.400			.181	.167	.098	-.431	-.709 -.839										
326	.620	.600			.153	.151	.074	-.001	-.400 -.748	323	.620	.400			.239	.266	.330	.398	.460 .516
328	.620	.800			.156	.150	.075	-.006	-.144 -.514	327	.620	.800			.166	.174	.202	.232	.268 .309
			$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed										$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed						
304	.260	.200	.159	.163		.189	.112	-.311	-.607 -.804	300	.260	.000	-.082	.294		.705	.465	.031	-.275 .007
306	.260	.300	.128	.133		.170	.104	-.047	-.270 -.721	301	.260	.100	-.451	.034		.208	.267	.305	.376 .509
308	.260	.400	.111	.103		.142	.086	.013	-.111 -.685	303	.260	.200	-.382	.043		.161	.224	.267	.338 .475
310	.260	.500	.078	.053		.095	.025	-.020	-.191 -.430	307	.260	.400	-.272	.019		.101	.135	.185	.272 .418
314	.260	.700	.067	.012		.048	-.005	-.113	-.228 -.401	309	.260	.500	-.291	-.020		.050	.081	.149	.250 .389
316	.260	.800	.090	.000		.045	-.022	-.119	-.214 -.425	313	.260	.700	-.347	-.086		-.010	.025	.112	.202 .349
										315	.260	.800	-.385	-.119		-.031	.007	.076	.200 .321
322	.620	.200	.203	.014		.110	-.052	-.347	-.573 -.762	317	.260	.900	-.405	-.140		-.052	-.011	.056	.196 .279
324	.620	.400	.220	-.031		.047	-.073	-.449	-.690 -.789										
326	.620	.600	.241	-.071		-.034	-.142	-.382	-.711 -.797	323	.620	.400	-.493	-.143		.012	.109	.226	.352 .486
328	.620	.800	.221	-.047		-.006	-.111	-.263	-.501 -.731	327	.620	.800	-.524	-.209		-.105	-.004	.101	.224 .309
			$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open										$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open						
304	.260	.200			.301	.292	.216	-.068	-.610 -.814	300	.260	.000			.780	.738	.525	.065	-.324 .007
306	.260	.300			.306	.301	.232	.131	-.029 -.699	301	.260	.100			.246	.269	.331	.411	.517 .633
308	.260	.400			.307	.303	.236	.118	.026 -.577	303	.260	.200			.261	.271	.335	.414	.507 .625
310	.260	.500			.298	.295	.225	.086	.055 -.294	307	.260	.400			.327	.341	.380	.448	.522 .600
314	.260	.700			.311	.307	.238	.104	.024 -.284	309	.260	.500			.344	.356	.388	.447	.512 .580
316	.260	.800			.298	.295	.224	.108	.007 -.282	313	.260	.700			.354	.364	.388	.427	.476 .528
										315	.260	.800			.334	.341	.360	.389	.427 .470
322	.620	.200			.270	.261	.089	-.323	-.563 -.690	317	.260	.900			.284	.290	.302	.321	.348 .382
324	.620	.400			.234	.229	.103	-.424	-.716 -.805										
326	.620	.600			.191	.198	.088	-.104	-.522 -.773	323	.620	.400			.231	.264	.349	.433	.511 .576
328	.620	.800			.182	.189	.084	-.026	-.251 -.666	327	.620	.800			.170	.183	.219	.259	.304 .348

TABLE V.- PRESSURE COEFFICIENTS MEASURED ON VERTICAL TAIL AND SPEED BRAKES

(a) M = 0.60

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper tail								Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Lower tail							
			$\alpha = -20^\circ$	$\alpha = -10^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 15^\circ$	$\alpha = 20^\circ$				$\alpha = -20^\circ$	$\alpha = -10^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 15^\circ$	$\alpha = 20^\circ$
			$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_r = 0^\circ$; brakes closed											$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_r = 0^\circ$; brakes closed							
401	.110	.647				-.204	-.207	-.221			441	.130	.647				-.209	-.181	-.153	-.113	-.062
402	.110	.681				-.122	-.140	-.141			442	.130	.682				-.098	-.078	-.045	.001	.056
403	.110	.698				-.115	-.135	-.134			443	.130	.700				-.096	-.075	-.044	.001	.054
404	.110	.748				-.138	-.152	-.151			444	.130	.748				-.112	-.096	-.069	-.028	.021
405	.110	.832				-.159	-.173	-.158			445	.130	.832				-.130	-.117	-.099	-.065	-.027
406	.110	.949				-.214	-.228	-.196			446	.130	.949				-.177	-.168	-.159	-.138	-.111
410	.250	.000				.658	.626	.601			450	.300	.000				.444	.503	.559	.641	.678
411	.250	.200				-.077	-.093	-.168			451	.300	.200				-.044	-.021	.011	.053	.093
412	.250	.400				-.069	-.091	-.151			452	.300	.400				-.051	-.027	.004	.049	.103
413	.250	.600				-.115	-.136	-.182			453	.300	.600				-.102	-.080	-.051	-.007	.043
414	.250	.630				-.214	-.231	-.252			454	.300	.633				-.194	-.166	-.140	-.103	-.061
415	.250	.668				-.101	-.118	-.184			455	.300	.668				-.090	-.072	-.039	.008	.057
416	.250	.685				-.101	-.120	-.176			456	.300	.686				-.085	-.069	-.039	.004	.053
417	.250	.738				-.121	-.140	-.188			457	.300	.738				-.099	-.084	-.057	-.018	.026
418	.250	.825				-.142	-.158	-.204			458	.300	.825				-.106	-.094	-.076	-.042	-.004
419	.250	.947				-.208	-.223	-.245			459	.300	.947				-.165	-.158	-.149	-.125	-.092
420	.500	.000				.615	.547	.489			460	.600	.000				.364	.461	.546	.643	.683
421	.500	.100				-.172	-.250	-.280			461	.600	.100				-.097	-.116	-.129	-.074	-.082
422	.500	.200				-.068	-.095	-.119			462	.600	.200				-.045	-.011	.026	.063	.107
423	.500	.300				-.065	-.085	-.114			463	.600	.300				-.042	-.015	.020	.055	.101
424	.500	.400				-.066	-.092	-.115			464	.600	.400				-.054	-.027	.005	.042	.090
425	.500	.500				-.077	-.099	-.118			465	.600	.500				-.064	-.038	-.007	.031	.076
426	.500	.600				-.089	-.106	-.121			466	.600	.600				-.082	-.061	-.032	.005	.052
427	.500	.700									467	.600	.700				-.084	-.066	-.042	-.008	.032
428	.500	.800				-.132	-.143	-.152			468	.600	.800				-.102	-.089	-.072	-.037	.003
429	.500	.900				-.164	-.175	-.180			469	.600	.900				-.130	-.123	-.114	-.086	-.045
430	.830	.000				.654	.583	.527			470	.800	.000				.539	.619	.691	.768	.813
431	.830	.200				-.111	-.129	-.142			471	.800	.200				-.072	-.036	.005	.044	.091
432	.830	.400				-.084	-.088	-.102			472	.800	.400				-.062	-.036	-.007	.035	.082
433	.830	.600				-.089	-.096	-.104			473	.800	.600				-.074	-.056	-.028	.012	.057
434	.830	.800				-.120	-.125	-.127			474	.800	.800				-.098	-.089	-.067	-.027	.010
			$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_r = 0^\circ$; brakes open											$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_r = 0^\circ$; brakes open							
401	.110	.647	-.125	-.186	.516	.493	.306	.506	.566	.478	441	.130	.647			.408	.487	.507	.516	.524	.524
402	.110	.681	-.059	-.106	.764	.740	.410	.742	.850	.779	442	.130	.682	-.128	-.106	.745	.818	.823	.816	.781	.771
403	.110	.698	-.059	-.103	.714	.709	.383	.718	.770	.721	443	.130	.700	-.126	-.108	.658	.735	.741	.733	.708	.692
404	.110	.748	-.084	-.126	.501	.499	.338	.601	.547	.457	444	.130	.748	-.148	-.123	.495	.532	.539	.542	.539	.537
405	.110	.832	-.118	-.153	.355	.357	.238	.444	.396	.293	445	.130	.832	-.165	-.130	.390	.393	.385	.387	.391	.397
406	.110	.949	-.184	-.215	.130	.135	.048	.196	.164	.068	446	.130	.949	-.219	-.166	.174	.156	.143	.141	.145	.151
410	.250	.000	.849	.704	.678	.657	.616	.638	.679	.662	450	.300	.000	.522	.236	.408	.460	.515	.573	.659	.687
411	.250	.200	-.009	-.069	.000	-.005	-.027	-.087	-.075	-.071	451	.300	.200	-.151	-.115	.024	.037	.054	.081	.121	.154
412	.250	.400	-.005	-.055	.081	.074	.048	.019	.025	-.025	452	.300	.400	-.146	-.106	.086	.102	.123	.150	.186	.226
413	.250	.600	-.056	-.105	.351	.355	.261	.323	.384	.352	453	.300	.600	-.168	-.138	.327	.356	.367	.375	.404	.430
414	.250	.630	-.152	-.193	.435	.438	.345	.412	.465	.429	454	.300	.633	-.272	-.187	.416	.434	.431	.427	.446	.467
415	.250	.668	-.038	-.088	.659	.689	.611	.642	.777	.772	455	.300	.668	-.156	-.141	.757	.734	.701	.670	.651	.669
416	.250	.685	-.044	-.093	.594	.622	.527	.534	.665	.677	456	.300	.686	-.144	-.133	.660	.648	.621	.600	.592	.611
417	.250	.738	-.067	-.110	.444	.447	.330	.363	.470	.430	457	.300	.738	-.157	-.139	.457	.471	.474	.476	.479	.484
418	.250	.825	-.096	-.138	.311	.301	.190	.303	.348	.284	458	.300	.825	-.157	-.148	.323	.325	.335	.354	.372	.376
419	.250	.947	-.170	-.211	.105	.101	.024	.138	.147	.094	459	.300	.947	-.218	-.192	.118	.113	.118	.131	.156	.173
420	.500	.000	.877	.717	.654	.611	.535	.496	.469	.032	460	.600	.000	.364	.142	.288	.367	.464	.553	.655	.690
421	.500	.100	-.074	-.251	-.108	-.084	-.203	-.166	-.200	-.400	461	.600	.100	-.223	-.021	.020	-.011	-.050	-.070	-.016	-.035
422	.500	.200	-.009	-.030	.019	.005	-.024	-.033	-.127	-.252	462	.600	.200	-.197	-.087	.012	.035	.068	.103	.137	.172
423	.500	.300	.001	-.028	.049	.039	.006	.004	-.089	-.165	463	.600	.300	-.192	-.093	.041	.062	.088	.121	.153	.187
424	.500	.400	-.004	-.041	.080	.069	.027	.048	-.055	-.092	464	.600	.400	-.204	-.094	.059	.084	.110	.141	.171	.202
425	.500	.500	-.017	-.055	.115	.104	.056	.099	-.011	-.013	465	.600	.500	-.212	-.094	.089	.118	.144	.170	.197	.228
426	.500	.600	-.035	-.069	.110	.098	.040	.093	-.016	.020	466	.600	.600	1.060	1.071	.083	.105	.132	.159	.184	.211
427	.500	.700	-.056	-.091							467	.600	.700	-.233	-.103	-.067	-.051	-.030	-.003	.030	.054
428	.500	.800	-.083	-.119	-.223	-.227	-.247	-.205	-.232	-.252	468	.600	.800	-.232	-.113	-.218	-.211	-.194	-.172	-.145	-.127
429	.500	.900	-.119	-.160	-.306	-.312	-.318	-.276	-.285	-.333	469	.600	.900			-.297	-.291	-.283	-.265	-.244	-.231
430	.830	.000	.895	.775	.701	.659	.576	.531	.527	.491	470	.800	.000	.433	.371	.486	.544	.623	.700	.777	.817
431	.830	.200	.001	-.063	-.024	-.054	-.069	-.070	-.074	-.109	471	.800	.200	-.131	-.122	-.022	.005	.041	.081	.117	.155
432	.830	.400	-.020	-.057	.018	.008	-.017	-.004	-.023	-.103	472	.800	.400	-.146	-.069	.039	.051	.078	.106	.145	.179
433	.830	.600	-.023	-.073	-.012	-.022	-.044	-.032	-.055	-.141	473	.800	.600	-.164	-.083	.019	.034	.054	.084	.118	.151
434	.830	.800	-.046	-.110	-.122	-.123	-.145	-.153	-.194	-.308	474	.800	.800			-.151	-.135	-.117	-.097	-.068	-.042

TABLE V.- PRESSURE COEFFICIENTS MEASURED ON VERTICAL TAIL AND SPEED BRAKES - Continued

(a) M = 0.60 - Continued

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper tail							Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Lower tail						
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15° α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15° α = 20°
			β ≈ 0°; δ_e = 0°; δ_v = 0°; brakes closed										β ≈ 0°; δ_e = 0°; δ_v = 0°; brakes closed						
401	.110	.647	-.088	-.155		-.151	-.167	-.192	-.230 -.298	441	.130	.647	-.292	-.191		-.168	-.154	-.136	-.097 -.044
402	.110	.681	-.011	-.073		-.069	-.081	-.114	-.179 -.239	442	.130	.682	-.198	-.077		-.063	-.047	-.017	.034 .082
403	.110	.698	-.013	-.073		-.068	-.080	-.110	-.172 -.237	443	.130	.700	-.189	-.074		-.062	-.047	-.020	.029 .074
404	.110	.748	-.045	-.103		-.093	-.105	-.135	-.189 -.258	444	.130	.748	-.212	-.096		-.084	-.069	-.048	-.004 .039
405	.110	.832	-.086	-.134		-.121	-.128	-.157	-.203 -.283	445	.130	.832	-.231	-.115		-.105	-.098	-.084	-.051 -.018
406	.110	.949	-.162	-.197		-.180	-.186	-.209	-.236 -.327	446	.130	.949	-.271	-.165		-.146	-.143	-.145	-.129 -.104
410	.250	.000	.940	.899		.876	.879	.904	.935 .924	450	.300	.000				.804	.831	.854	.888 .915
411	.250	.200	.105	.058		.059	.045	.011	-.061 -.126	451	.300	.200	-.104	.021		.057	.080	.106	.140 .186
412	.250	.400	.063	.007		.008	-.007	-.035	-.097 -.164	452	.300	.400	-.144	-.024		-.001	.023	.053	.102 .153
413	.250	.600	-.009	-.068		-.063	-.076	-.102	-.146 -.222	453	.300	.600	-.200	-.081		-.066	-.049	-.022	.023 .073
414	.250	.630	-.119	-.175		-.163	-.181	-.205	-.240 -.312	454	.300	.633	-.291	-.178		-.155	-.143	-.130	-.096 -.050
415	.250	.668	.013	-.048		-.048	-.056	-.081	-.125 -.206	455	.300	.668	-.185	-.066		-.056	-.040	-.008	.042 .090
416	.250	.685	.003	-.052		-.052	-.061	-.084	-.131 -.211	456	.300	.686	-.180	-.061		-.052	-.036	-.011	.037 .082
417	.250	.738	-.026	-.080		-.077	-.085	-.109	-.151 -.234	457	.300	.738	-.193	-.076		-.069	-.055	-.031	.010 .056
418	.250	.825	-.063	-.110		-.102	-.107	-.128	-.169 -.256	458	.300	.825	-.203	-.089		-.082	-.075	-.059	-.023 -.012
419	.250	.947	-.144	-.185		-.177	-.186	-.197	-.220 -.309	459	.300	.947	-.236	-.210		-.140	-.136	-.133	-.112 -.081
420	.500	.000	.937	.862		.781	.750	.742	.757 .770	460	.600	.000	.734	.739		.793	.834	.870	.912 .945
421	.500	.100	.131	.078		.072	.052	.017	-.033 -.099	461	.600	.100	-.104	.018		.070	.097	.122	.153 .196
422	.500	.200	.096	.048		.041	.023	-.005	-.053 -.125	462	.600	.200	-.118	-.002		.035	.061	.089	.127 .173
423	.500	.300	.076	.027		.019	.001	-.023	-.071 -.139	463	.600	.300	-.126	-.013		.012	.038	.068	.110 .159
424	.500	.400	.060	.006		-.001	-.016	-.040	-.087 -.156	464	.600	.400	-.142	-.031		-.011	.016	.048	.093 .142
425	.500	.500	.039	-.013		-.020	-.036	-.057	-.100 -.172	465	.600	.500	-.152	-.043		-.026	-.002	.028	.076 .123
426	.500	.600	.018	-.033		-.036	-.050	-.069	-.106 -.180	466	.600	.600				-.045	-.024	.004	.048 .093
427	.500	.700	-.005	-.056		-.057	-.070	-.088	-.123 -.198	467	.600	.700	-.171	-.066		-.053	-.035	-.012	.032 .071
428	.500	.800	-.041	-.089		-.087	-.100	-.111	-.143 -.219	468	.600	.800	-.189	-.088		-.073	-.058	-.039	-.006 .032
429	.500	.900	-.091	-.134		-.128	-.140	-.154	-.176 -.255	469	.600	.900	-.217	-.124		-.109	-.099	-.088	-.060 -.027
430	.830	.000	.949	.847		.749	.705	.678	.667 .674	470	.800	.000	.725	.723		.781	.825	.870	.924 .961
431	.830	.200	.100	.039						471	.800	.200				.023	.051	.085	.126 .172
432	.830	.400	.063	.007		-.013	-.035	-.061	-.082 -.139	472	.800	.400	-.135	-.039		-.012	.015	.049	.094 .142
433	.830	.600	.039	-.015		-.037	-.052	-.069	-.093 -.143	473	.800	.600	-.151	-.060		-.038	-.015	.013	.061 .103
434	.830	.800	-.014	-.066		-.081	-.094	-.107	-.125 -.177	474	.800	.800	-.173	-.089		-.071	-.053	-.031	.008 .043
			β ≈ 0°; δ_e = 0°; δ_v = 0°; brakes open										β ≈ 0°; δ_e = 0°; δ_v = 0°; brakes open						
401	.110	.647			-.149	-.148	-.146	-.175	-.238 -.323	441	.130	.647			-.186	-.184	-.175	-.152	-.114 -.087
402	.110	.681			-.063	-.057	-.055	-.095	-.167 -.253	442	.130	.682			-.056	-.054	-.045	-.028	.012 .051
403	.110	.698			-.064	-.057	-.055	-.093	-.160 -.252	443	.130	.700			-.059	-.057	-.047	-.031	.007 .044
404	.110	.748			-.100	-.092	-.091	-.125	-.187 -.287	444	.130	.748			-.085	-.083	-.078	-.064	-.030 .000
405	.110	.832			-.136	-.127	-.125	-.158	-.209 -.315	445	.130	.832			-.112	-.113	-.110	-.103	-.077 -.054
406	.110	.949			-.196	-.189	-.186	-.208	-.243 -.343	446	.130	.949			-.171	-.171	-.170	-.163	-.143 -.130
410	.250	.000			.872	.863	.871	.888	.875 .919	450	.300	.000			.801	.815	.843	.873	.900 .930
411	.250	.200			.164	.161	.154	.113	.021 -.052	451	.300	.200			.129	.140	.157	.173	.189 .222
412	.250	.400			.049	.051	.050	.015	-.064 -.148	452	.300	.400			.031	.036	.050	.070	.107 .146
413	.250	.600			-.068	-.062	-.062	-.090	-.164 -.269	453	.300	.600			-.071	-.068	-.060	-.041	-.007 .025
414	.250	.630			-.194	-.184	-.181	-.217	-.285 -.383	454	.300	.633			-.192	-.189	-.184	-.168	-.137 -.118
415	.250	.668			-.071	-.060	-.055	-.094	-.173 -.288	455	.300	.668			-.068	-.067	-.062	-.052	-.022 .006
416	.250	.685			-.071	-.057	-.055	-.090	-.171 -.287	456	.300	.686			-.061	-.062	-.056	-.043	-.016 .007
417	.250	.738			-.102	-.091	-.087	-.119	-.200 -.317	457	.300	.738			-.080	-.080	-.077	-.068	-.042 -.022
418	.250	.825			-.137	-.124	-.116	-.149	-.230 -.353	458	.300	.825			-.099	-.100	-.099	-.094	-.077 -.064
419	.250	.947			-.191	-.187	-.183	-.198	-.252 -.357	459	.300	.947			-.163	-.160	-.155	-.148	-.133 -.126
420	.500	.000			.691	.675	.648	.646	.672 .703	460	.600	.000			.762	.784	.823	.873	.917 .957
421	.500	.100			.279	.270	.258	.230	.180 .118	461	.600	.100			.217	.232	.257	.277	.299 .334
422	.500	.200			.177	.178	.172	.142	.092 .014	462	.600	.200			.118	.130	.149	.175	.205 .241
423	.500	.300			.117	.117	.111	.090	.041 -.035	463	.600	.300			.077	.085	.106	.130	.158 .196
424	.500	.400			.078	.080	.076	.052	.007 -.075	464	.600	.400			.046	.053	.073	.094	.128 .168
425	.500	.500			.047	.050	.045	.031	-.013 -.099	465	.600	.500			.026	.032	.050	.074	.110 .146
426	.500	.600			.026	.032	.028	.014	-.030 -.116	466	.600	.600			.001	.007	.023	.046	.080 .115
427	.500	.700			-.002	.002	.002	-.012	-.053 -.143	467	.600	.700			-.009	-.005	.008	.027	.060 .092
428	.500	.800			-.034	-.032	-.028	-.042	-.079 -.171	468	.600	.800			-.032	-.030	-.020	-.002	.026 .053
429	.500	.900			-.077	-.075	-.066	-.079	-.115 -.208	469	.600	.900			-.068	-.065	-.059	-.047	-.023 .001
430	.830	.000			.595	.555	.501	.465	.456 .469	470	.800	.000			.687	.713	.761	.824	.885 .935
431	.830	.200								471	.800	.200			.087	.100	.127	.162	.198 .243
432	.830	.400			.053	.046	.032	.011	-.018 -.064	472	.800	.400			.026	.038	.065	.100	.144 .188
433	.830	.600			.025	.016	.008	-.010	-.029 -.076	473	.800	.600			-.008	.002	.025	.060	.103 .145
434	.830	.800			-.019	-.025	-.037	-.050	-.061 -.113	474	.800	.800			-.039	-.032	-.014	.013	.053 .089

TABLE V.- PRESSURE COEFFICIENTS MEASURED ON VERTICAL TAIL AND SPEED BRAKES - Continued

(a) M = 0.60 - Continued

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper tail								Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Lower tail							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			β ≈ 0°; δ_e = 0°; δ_v = -7.5°; brakes closed											β ≈ 0°; δ_e = 0°; δ_v = -7.5°; brakes closed							
401	.110	.647			-.172	-.180	-.189	-.217	-.262	-.316	441	.130	.647			-.198	-.194	-.168	-.136	-.101	-.047
402	.110	.681			-.090	-.097	-.105	-.145	-.212	-.257	442	.130	.682			-.099	-.091	-.071	-.035	.014	.060
403	.110	.698			-.087	-.093	-.098	-.136	-.203	-.253	443	.130	.700			-.094	-.088	-.068	-.034	.011	.053
404	.110	.748			-.108	-.111	-.118	-.151	-.211	-.270	444	.130	.748			-.108	-.103	-.086	-.056	-.017	.020
405	.110	.832			-.122	-.124	-.128	-.156	-.213	-.277	445	.130	.832			-.115	-.113	-.100	-.079	-.055	-.013
406	.110	.949			-.172	-.175	-.179	-.196	-.237	-.318	446	.130	.949			-.151	-.152	-.141	-.128	-.122	-.088
410	.250	.000			.912	.900	.900	.920	.947	.933	450	.300	.000			.762	.778	.808	.834	.860	.891
411	.250	.200			-.062	-.077	-.096	-.128	-.202	-.282	451	.300	.200			-.080	-.063	-.029	.004	.035	.077
412	.250	.400			-.052	-.065	-.083	-.112	-.117	-.176	452	.300	.400			-.083	-.066	-.032	.004	.082	.163
413	.250	.600			-.098	-.107	-.115	-.145	-.168	-.232	453	.300	.600			-.112	-.105	-.080	-.032	.030	.080
414	.250	.630			-.184	-.197	-.212	-.226	-.272	-.344	454	.300	.633			-.187	-.183	-.153	-.118	-.099	-.063
415	.250	.668			-.096	-.102	-.106	-.135	-.160	-.227	455	.300	.668			-.113	-.106	-.085	-.035	.020	.073
416	.250	.685			-.100	-.102	-.106	-.135	-.158	-.228	456	.300	.686			-.105	-.098	-.079	-.032	.023	.070
417	.250	.738			-.110	-.110	-.115	-.142	-.170	-.245	457	.300	.738			-.110	-.103	-.087	-.046	.002	.048
418	.250	.825			-.115	-.119	-.126	-.140	-.171	-.254	458	.300	.825			-.104	-.099	-.084	-.053	-.015	.028
419	.250	.947			-.163	-.168	-.172	-.179	-.211	-.297	459	.300	.947			-.142	-.141	-.122	-.098	-.071	-.036
420	.500	.000			.744	.711	.681	.662	.699	.720	460	.600	.000			.416	.456	.512	.548	.586	.633
421	.500	.100			-.145	-.154	-.162	-.197	-.268	-.328	461	.600	.100			-.058	-.051	-.031	.018	-.029	-.079
422	.500	.200			-.047	-.058	-.081	-.108	-.169	-.246	462	.600	.200			-.061	-.041	-.004	.039	.094	.144
423	.500	.300			-.033	-.049	-.072	-.100	-.150	-.216	463	.600	.300			-.059	-.044	-.006	.039	.092	.144
424	.500	.400			-.041	-.057	-.081	-.106	-.148	-.210	464	.600	.400			-.074	-.058	-.024	.020	.072	.124
425	.500	.500			-.058	-.074	-.091	-.118	-.156	-.218	465	.600	.500			-.086	-.073	-.039	.004	.052	.100
426	.500	.600			-.082	-.096	-.110	-.131	-.167	-.232	466	.600	.600			-.106	-.096	-.067	-.030	.011	.057
427	.500	.700			-.109	-.114	-.128	-.148	-.187	-.254	467	.600	.700			-.115	-.108	-.082	-.049	-.019	.020
428	.500	.800			-.124	-.131	-.141	-.159	-.195	-.268	468	.600	.800			-.121	-.116	-.096	-.071	-.041	-.005
429	.500	.900			-.147	-.152	-.165	-.176	-.211	-.286	469	.600	.900			-.144	-.139	-.121	-.098	-.071	-.035
430	.830	.000			.701	.660	.604	.565	.561	.582	470	.800	.000			.482	.524	.593	.659	.711	.759
431	.830	.200									471	.800	.200			-.060	-.049	-.022	.010	.046	.097
432	.830	.400			-.053	-.064	-.074	-.097	-.134	-.195	472	.800	.400			-.066	-.055	-.031	.001	.042	.093
433	.830	.600			-.070	-.079	-.082	-.101	-.136	-.195	473	.800	.600			-.087	-.077	-.058	-.032	.005	.049
434	.830	.800			-.107	-.109	-.113	-.127	-.155	-.220	474	.800	.800			-.107	-.102	-.090	-.074	-.050	-.028
			β ≈ 0°; δ_e = 0°; δ_v = 7.5°; brakes closed											β ≈ 0°; δ_e = 0°; δ_v = 7.5°; brakes closed							
401	.110	.647			.544	.544	.546	.525	.474	.425	441	.130	.647			.524	.529	.548	.558	.567	.579
402	.110	.681			.782	.794	.785	.758	.695	.669	442	.130	.682			.865	.866	.865	.852	.831	.828
403	.110	.698			.762	.756	.733	.706	.609	.646	443	.130	.700			.749	.759	.777	.782	.780	.778
404	.110	.748			.539	.541	.510	.464	.375	.407	444	.130	.748			.570	.572	.569	.568	.572	.577
405	.110	.832			.404	.424	.398	.351	.282	.251	445	.130	.832			.464	.455	.428	.420	.418	.423
406	.110	.949			.180	.204	.205	.190	.167	.032	446	.130	.949			.232	.212	.190	.180	.177	.182
410	.250	.000			.890	.883	.885	.906	.938	.926	450	.300	.000			.803	.815	.840	.867	.892	.921
411	.250	.200			.137	.128	.109	.080	-.003	-.073	451	.300	.200			.122	.131	.153	.180	.205	.245
412	.250	.400			.153	.151	.132	.113	.038	-.030	452	.300	.400			.145	.152	.172	.200	.232	.274
413	.250	.600			.429	.423	.412	.399	.347	.317	453	.300	.600			.402	.406	.422	.439	.456	.482
414	.250	.630			.482	.487	.487	.490	.472	.405	454	.300	.633			.483	.484	.491	.503	.512	.533
415	.250	.668			.768	.772	.782	.796	.796	.730	455	.300	.668			.825	.818	.812	.815	.818	.834
416	.250	.685			.711	.705	.700	.698	.674	.662	456	.300	.686			.708	.711	.721	.733	.748	.763
417	.250	.738			.673	.673	.669	.671	.674	.421	457	.300	.738			.487	.485	.490	.504	.525	.547
418	.250	.825			.331	.334	.339	.342	.362	.276	458	.300	.825			.357	.349	.347	.359	.382	.406
419	.250	.947			.138	.140	.150	.159	.176	.081	459	.300	.947			.150	.144	.142	.152	.174	.198
420	.500	.000			.810	.790	.759	.748	.758	.776	460	.600	.000			.786	.807	.844	.882	.918	.950
421	.500	.100			.141	.128	.105	.078	.012	-.056	461	.600	.100			.114	.129	.155	.182	.201	.242
422	.500	.200			.126	.116	.093	.071	.005	-.068	462	.600	.200			.098	.113	.136	.166	.193	.234
423	.500	.300			.124	.117	.097	.077	.020	-.057	463	.600	.300			.105	.114	.136	.166	.197	.239
424	.500	.400			.137	.130	.110	.093	.035	-.032	464	.600	.400			.119	.127	.147	.179	.211	.250
425	.500	.500			.164	.158	.139	.123	.075	.012	465	.600	.500			.146	.156	.176	.204	.234	.272
426	.500	.600			.150	.144	.122	.116	.085	.035	466	.600	.600			.132	.139	.157	.186	.217	.253
427	.500	.700			-.024	-.036	-.058	-.053	-.070	-.132	467	.600	.700			-.041	-.034	-.015	.015	.049	.087
428	.500	.800			-.190	-.198	-.214	-.205	-.222	-.301	468	.600	.800			-.202	-.199	-.186	-.161	-.130	-.094
429	.500	.900			-.283	-.286	-.300	-.293	-.310	-.388	469	.600	.900			-.284	-.284	-.277	-.258	-.235	-.204
430	.830	.000			.784	.755	.710	.683	.667	.672	470	.800	.000			.767	.789	.830	.877	.924	.967
431	.830	.200									471	.800	.200			.084	.094	.119	.154	.188	.229
432	.830	.400			.075	.067	.040	.026	-.013	-.066	472	.800	.400			.085	.095	.119	.154	.190	.232
433	.830	.600			.026	.017	-.007	-.019	-.048	-.091	473	.800	.600			.044	.055	.079	.112	.150	.191
434	.830	.800			-.098	-.107	-.131	-.144	-.158	-.201	474	.800	.800			-.141	-.133	-.112	-.080	-.043	-.001

TABLE V.- PRESSURE COEFFICIENTS MEASURED ON VERTICAL TAIL AND SPEED BRAKES - Continued

(a) M = 0.60 - Concluded

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	x/c	Upper tail							Model orifice number	$\frac{y}{b/2}$	x/c	Lower tail						
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			β ≈ 5°; δ_e = 0°; δ_v = 0°; brakes closed										β ≈ 5°; δ_e = 0°; δ_v = 0°; brakes closed							
401	.110	.647	-.054	-.126		-.123	-.130	-.152	-.233	-.339	441	.130	.647	-.326	-.169		-.174	-.151	-.119	-.076	-.025
402	.110	.681	.041	-.023		-.009	-.014	-.058	-.142	-.274	442	.130	.682	-.242	-.042		-.019	-.004	.028	.070	.121
403	.110	.698	.038	-.023		-.008	-.012	-.056	-.141	-.269	443	.130	.700	-.235	-.039		-.034	-.005	.026	.066	.111
404	.110	.748	-.003	-.058							444	.130	.748	-.254	-.061		-.047	-.037	-.008	.026	.071
405	.110	.832	-.057	-.099		-.079	-.079	-.113	-.193	-.312	445	.130	.832	-.279	-.087		-.076	-.069	-.052	-.028	.006
406	.110	.949	-.152	-.187		-.172	-.167	-.188	-.263	-.360	446	.130	.949	-.306	-.145		-.147	-.142	-.136	-.125	-.098
410	.250	.000	.833	.740		.539	.552	.606	.744	.688	450	.300	.000	.353	.688		.747	.797	.855	.899	.933
411	.250	.200	.229	.195		.209	.196	.136	-.010	-.150	451	.300	.200	-.139	.141		.172	.190	.208	.230	.283
412	.250	.400	.143	.086		.092	.083	.044	-.060	-.189	452	.300	.400	-.182	.045		.063	.086	.118	.162	.216
413	.250	.600	.047	-.016		-.011	-.018	-.048	-.129	-.248	453	.300	.600	-.233	-.042		-.034	-.013	.021	.065	.115
414	.250	.630	-.090	-.151							454	.300	.633	-.317	-.166		-.165	-.143	-.113	-.078	-.030
415	.250	.668	.068	.004		.004	.000	-.030	-.106	-.236	455	.300	.668	-.220	-.030		-.016	.003	.035	.078	.129
416	.250	.685	.058	-.006		-.001	-.005	-.036	-.110	-.242	456	.300	.686	-.217	-.024		-.012	.003	.035	.074	.122
417	.250	.738	.021	-.037		-.033	-.036	-.061	-.132	-.258	457	.300	.738	-.225	-.044		-.042	-.020	.009	.047	.087
418	.250	.825	-.028	-.076		-.066	-.067	-.089	-.160	-.281	458	.300	.825	-.230	-.062		-.054	-.044	-.023	.003	.042
419	.250	.947	-.132	-.175		-.163	-.161	-.174	-.243	-.344	459	.300	.947	-.287	-.140		-.154	-.129	-.117	-.101	-.071
420	.500	.000				.530	.481	.471	.414	.075	460	.600	.000	.610	.651		.700	.771	.852	.907	.953
421	.500	.100	.303	.267		.271	.250	.205	.084	-.069	461	.600	.100	-.043	.189		.238	.257	.272	.289	.336
422	.500	.200	.208	.164		.177	.160	.123	.022	-.105	462	.600	.200	-.108	.092		.127	.152	.179	.210	.268
423	.500	.300	.161	.108		.099	.100	.069	-.017	-.133	463	.600	.300	-.128	.043		.075	.108	.139	.180	.234
424	.500	.400	.139	.067		.071	.059	.029	-.043	-.153	464	.600	.400	-.145	.022		.043	.067	.107	.148	.203
425	.500	.500	.108	.039		.037	.026	-.001	-.060	-.167	465	.600	.500	-.155	-.004		.012	.041	.080	.124	.177
426	.500	.600	.080	.023		.005	.003	-.017	-.073	-.176	466	.600	.600	-.168	-.028		-.028	.012	.049	.089	.141
427	.500	.700				-.016	-.023	-.040	-.090	-.192	467	.600	.700	-.171	-.036		-.023	-.004	.028	.067	.114
428	.500	.800	.001	-.051		-.054	-.056	-.069	-.120	-.221	468	.600	.800	-.190	-.063		-.049	-.034	-.008	.025	.066
429	.500	.900	-.063	-.109		-.109	-.106	-.113	-.167	-.261	469	.600	.900	-.219	-.099		-.091	-.080	-.063	-.042	-.004
430	.830	.000	.863	.745		.543	.487	.444	.402	.392	470	.800	.000	.624	.610		.696	.765	.843	.904	.949
431	.830	.200	.194	.132		.081	.066	.039	-.014	-.081	471	.800	.200	-.100	.039		.063	.110	.160	.198	.258
432	.830	.400	.147	.068		-.152	-.016	-.018	-.050	-.106	472	.800	.400	-.123	-.009		.015	.050	.098	.143	.203
433	.830	.600	.111	.033		-.015	-.028	-.043	-.065	-.120	473	.800	.600	-.136	-.041		-.019	.011	.054	.098	.155
434	.830	.800	.044	-.026		-.060	-.071	-.080	-.101	-.152	474	.800	.800	-.155	-.071		-.056	-.032	-.001	.038	.087
			β ≈ 5°; δ_e = 0°; δ_v = 0°; brakes open										β ≈ 5°; δ_e = 0°; δ_v = 0°; brakes open							
401	.110	.647				.620	.633	.644	.535	.459	.365	441	.130	.647				.599	.599	.596	.600	.610	.623
402	.110	.681				.856	.868	.889	.736	.676	.587	442	.130	.682				.926	.925	.914	.903	.896	.895
403	.110	.698				.786	.793	.790	.680	.646	.548	443	.130	.700				.793	.795	.792	.791	.795	.796
405	.110	.832				.458	.477	.494	.468	.310	.122	444	.130	.748				.624	.618	.604	.594	.595	.598
406	.110	.949				.227	.244	.260	.247	.071	-.107	445	.130	.832				.511	.500	.478	.461	.459	.459
												446	.130	.949				.269	.257	.238	.223	.220	.217
410	.250	.000				.558	.542	.539	.580	.758	.712												
411	.250	.200				.281	.277	.263	.206	.045	-.109	450	.300	.000				.727	.751	.797	.849	.905	.933
412	.250	.400				.235	.234	.223	.185	.065	-.077	451	.300	.200				.254	.255	.262	.273	.294	.334
413	.250	.600				.466	.468	.462	.419	.352	.230	452	.300	.400				.217	.221	.233	.252	.290	.329
415	.250	.668				.802	.804	.808	.764	.714	.540	453	.300	.600				.449	.450	.457	.469	.492	.513
416	.250	.685				.708	.706	.699	.683	.653	.494	454	.300	.633				.519	.519	.526	.535	.554	.566
417	.250	.738				.485	.486	.486	.506	.444	.337	455	.300	.668				.840	.847	.850	.854	.871	.893
418	.250	.825				.352	.355	.358	.384	.312	.192	456	.300	.686				.700	.707	.716	.727	.744	.758
419	.250	.947				.157	.159	.167	.186	.126	-.005	457	.300	.738				.498	.500	.504	.515	.538	.556
												458	.300	.825				.375	.375	.376	.386	.409	.430
420	.500	.000				.566	.530	.472	.468	.442	.112	459	.300	.947				.178	.175	.178	.186	.208	.227
421	.500	.100				.330	.325	.306	.257	.129	-.029												
422	.500	.200				.254	.250	.234	.192	.081	-.057	460	.600	.000				.661	.695	.765	.844	.916	.953
423	.500	.300				.214	.210	.193	.158	.062	-.065	461	.600	.100				.289	.298	.312	.321	.336	.374
424	.500	.400				.203	.199	.185	.154	.071	-.050	462	.600	.200				.201	.207	.225	.246	.275	.317
425	.500	.500				.208	.204	.193	.165	.096	-.008	463	.600	.300				.175	.185	.204	.224	.265	.305
426	.500	.600				.174	.167	.155	.139	.090	.004	464	.600	.400				.173	.181	.199	.226	.265	.303
427	.500	.700				-.022	-.031	-.043	-.042	-.080	-.143	465	.600	.500				.184	.193	.210	.236	.276	.312
428	.500	.800				-.195	-.204	-.211	-.204	-.244	-.302	466	.600	.600				.150	.158	.178	.205	.247	.279
429	.500	.900				-.287	-.293	-.298	-.301	-.341	-.399	467	.600	.700				-.039	-.031	-.008	.022	.065	.104
												468	.600	.800				-.200	-.197	-.181	-.158	-.119	-.085
430	.830	.000				.592	.556	.490	.458	.428	.391	469	.600	.900				-.282	-.282	-.269	-.255	-.226	-.198
431	.830	.200				.164	.147	.120	.095	.036	-.041												
432	.830	.400				-.673	-.594	-.528	-.441	-.392	-.382	470	.800	.000				.646	.691	.759	.832	.905	.948
433	.830	.600				.037	.021	.001	-.010	-.033	-.084	471	.800	.200				.137	.149	.176	.214	.258	.305
434	.830	.800				-.094	-.109	-.126	-.139	-.152	-.192	472	.800	.400				.112	.123	.151	.187	.234	.280
												473	.800	.600				.045	.057	.085	.122	.175	.220
												474	.800	.800				-.146	-.138	-.112	-.077	-.028	.018

TABLE V.- PRESSURE COEFFICIENTS MEASURED ON VERTICAL TAIL AND SPEED BRAKES - Continued

(b) M = 0.90

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper tail								Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Lower tail							
			$\alpha = -20^\circ$	$\alpha = -10^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 15^\circ$	$\alpha = 20^\circ$				$\alpha = -20^\circ$	$\alpha = -10^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 15^\circ$	$\alpha = 20^\circ$
			$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed											$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed							
401	.110	.647				-.274	-.256	-.286	-.339	-.402	441	.130	.647				-.273	-.238	-.183	-.130	-.081
402	.110	.681				-.149	-.187	-.165	-.197	-.270	442	.130	.682				-.130	-.089	-.027	.028	.080
403	.110	.698				-.153	-.189	-.167	-.205	-.262	443	.130	.700				-.128	-.083	-.022	.029	.078
404	.110	.748				-.193	-.223	-.210	-.252	-.307	444	.130	.748				-.172	-.128	-.066	-.010	.037
405	.110	.832				-.221	-.254	-.251	-.293	-.353	445	.130	.832				-.209	-.174	-.113	-.062	-.021
406	.110	.949				-.246	-.278	-.224	-.274	-.373	446	.130	.949				-.224	-.217	-.193	-.168	-.150
410	.250	.000				.899	.878	.735	.835	.645	450	.300	.000				.679	.722	.778	.826	.854
411	.250	.200				-.081	-.119	-.208	-.266	-.390	451	.300	.200				-.039	-.018	-.015	-.004	.035
412	.250	.400				-.063	-.093	-.140	-.143	-.215	452	.300	.400				-.029	.002	.029	.050	.096
413	.250	.600				-.143	-.168	-.190	-.187	-.274	453	.300	.600				-.125	-.089	-.043	-.001	.048
414	.250	.630				-.263	-.282	-.317	-.342	-.416	454	.300	.633				-.250	-.207	-.156	-.115	-.078
415	.250	.668				-.125	-.167	-.211	-.168	-.267	455	.300	.668				-.125	-.085	-.026	.028	.078
416	.250	.685				-.136	-.173	-.189	-.174	-.255	456	.300	.686				-.120	-.083	-.026	.024	.072
417	.250	.738				-.172	-.209	-.227	-.219	-.286	457	.300	.738				-.149	-.110	-.051	-.002	.042
418	.250	.825				-.198	-.232	-.260	-.244	-.320	458	.300	.825				-.172	-.139	-.085	-.038	.003
419	.250	.947				-.239	-.267	-.255	-.263	-.373	459	.300	.947				-.210	-.203	-.174	-.147	-.120
420	.500	.000				.808	.754	.702	.468	.688	460	.600	.000				.653	.719	.793	.855	.888
421	.500	.100				-.423	-.495	-.436	-.459	-.432	461	.600	.100				-.390	-.366	-.309	-.122	-.221
422	.500	.200				-.059	-.064	-.137	-.403	-.479	462	.600	.200				-.017	.020	.019	.030	.069
423	.500	.300				-.034	-.074	-.121	-.272	-.356	463	.600	.300				-.005	.026	.039	.049	.088
424	.500	.400				-.049	-.084	-.110	-.243	-.221	464	.600	.400				-.037	-.006	.022	.046	.085
425	.500	.500				-.081	-.111	-.134	-.250	-.243	465	.600	.500				-.072	-.034	.004	.039	.080
426	.500	.600				-.109	-.141	-.160	-.252	-.271	466	.600	.600				-.112	-.070	-.025	.014	.057
427	.500	.700									467	.600	.700				-.127	-.087	-.038	.004	.044
428	.500	.800				-.171	-.201	-.226	-.277	-.295	468	.600	.800				-.158	-.123	-.074	-.029	.005
429	.500	.900				-.195	-.219	-.237	-.286	-.318	469	.600	.900				-.181	-.160	-.122	-.085	-.053
430	.830	.000				.772	.711	.669	.651	.719	470	.800	.000				.720	.793	.867	.926	.971
431	.830	.200				-.137	-.262	-.283	-.197	-.280	471	.800	.200				-.111	-.018	.006	.038	.069
432	.830	.400				-.074	-.075	-.096	-.145	-.177	472	.800	.400				-.041	-.029	.006	.030	.074
433	.830	.600				-.110	-.118	-.123	-.151	-.205	473	.800	.600				-.101	-.074	-.025	.015	.061
434	.830	.800				-.152	-.163	-.165	-.185	-.222	474	.800	.800				-.145	-.120	-.071	-.026	.007
			$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open											$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open							
401	.110	.647	-.181	-.227	.588	.560	.375	.629	.504	.472	441	.130	.647			.486	.579	.620	.625	.619	.625
402	.110	.681	-.084	-.124	.829	.840	.483	.907	.815	.804	442	.130	.682	-.168	-.108	.819	.929	.924	.898	.865	.859
403	.110	.698	-.087	-.130	.827	.820	.480	.847	.882	.783	443	.130	.700	-.178	-.121	.720	.859	.871	.842	.803	.789
404	.110	.748	-.124	-.174	.613	.587	.461	.702	.619	.462	444	.130	.748	-.209	-.151	.558	.641	.660	.656	.643	.638
405	.110	.832	-.159	-.206	.458	.441	.379	.553	.433	.248	445	.130	.832	-.227	-.180	.483	.508	.508	.507	.503	.501
406	.110	.949	-.244	-.273	.282	.270	.217	.334	.242	.065	446	.130	.949	-.255	-.205	.337	.317	.307	.301	.296	.295
410	.250	.000	1.031	.967	.908	.893	.846	.749	.834	.601	450	.300	.000	.409	.576	.647	.684	.724	.783	.821	.852
411	.250	.200	-.073	-.060	.017	.013	-.024	-.108	-.208	-.410	451	.300	.200	-.462	-.133	.049	.057	.058	.066	.068	.109
412	.250	.400	-.071	-.052	.143	.131	.099	.057	.002	-.123	452	.300	.400	-.265	-.087	.156	.173	.198	.212	.226	.264
413	.250	.600	-.106	-.127	.451	.443	.327	.441	.458	.327	453	.300	.600	-.286	-.157	.412	.460	.467	.469	.483	.509
414	.250	.630	-.217	-.245	.533	.518	.374	.544	.472	.415	454	.300	.633	-.384	-.230	.522	.543	.541	.527	.532	.555
415	.250	.668	-.059	-.097	.757	.782	.527	.813	.829	.720	455	.300	.668	-.326	-.171	.872	.854	.805	.738	.701	.728
416	.250	.685	-.073	-.109	.706	.732	.487	.704	.839	.635	456	.300	.686	-.257	-.159	.780	.780	.727	.681	.659	.684
417	.250	.738	-.102	-.145	.556	.547	.361	.517	.571	.406	457	.300	.738	-.267	-.183	.560	.588	.582	.571	.560	.570
418	.250	.825	-.132	-.179	.418	.397	.254	.432	.421	.277	458	.300	.825	-.274	-.202	.433	.440	.457	.465	.466	.467
419	.250	.947	-.218	-.257	.236	.226	.128	.269	.248	.135	459	.300	.947	-.315	-.247	.261	.248	.256	.267	.278	.286
420	.500	.000	1.012	.922	.840	.803	.739	.691	.443	.756	460	.600	.000	.732	.524	.595	.648	.714	.790	.843	.880
421	.500	.100	-.088	-.298	-.348	-.363	-.399	-.183	-.449	-.442	461	.600	.100	-.404	-.559	-.210	-.236	-.268	-.262	-.238	-.184
422	.500	.200	-.032	-.006	.060	.054	.025	-.041	-.291	-.474	462	.600	.200	-.317	-.052	.068	.090	.111	.111	.113	.153
423	.500	.300	-.057	-.030	.113	.096	.055	.022	-.172	-.244	463	.600	.300	-.158	-.059	.113	.138	.171	.180	.181	.216
424	.500	.400	-.065	-.050	.153	.137	.097	.094	-.078	-.098	464	.600	.400	-.188	-.067	.134	.165	.199	.208	.216	.249
425	.500	.500	-.070	-.073	.210	.187	.152	.166	.024	-.005	465	.600	.500	-.200	-.088	.173	.212	.246	.256	.265	.296
426	.500	.600	-.078	-.096	.218	.198	.143	.166	.064	.038	466	.600	.600	1.178	1.184	.184	.216	.247	.261	.270	.298
427	.500	.700	-.092	-.118							467	.600	.700	-.204	-.129	.008	.031	.051	.081	.105	.130
428	.500	.800	-.120	-.154	-.187	-.203	-.227	-.186	-.212	-.326	468	.600	.800	-.204	-.157	-.190	-.174	-.154	-.123	-.103	-.087
429	.500	.900	-.155	-.191	-.315	-.332	-.347	-.279	-.297	-.436	469	.600	.900			-.318	-.309	-.284	-.257	-.251	-.244
430	.830	.000	1.024	.913	.821	.782	.712	.669	.640	.733	470	.800	.000	.756	.594	.674	.729	.805	.873	.925	.969
431	.830	.200	-.025	.005	-.033	-.113	-.198	-.172	-.111	-.232	471	.800	.200	-.152	-.196	-.018	-.008	.010	.109	.118	.160
432	.830	.400	-.073	-.069	.101	.087	.072	.069	.013	-.076	472	.800	.400	-.163	-.033	.143	.152	.163	.178	.192	.225
433	.830	.600	-.057	-.091	.074	.058	.047	.061	-.002	-.055	473	.800	.600	-.171	-.099	.118	.139	.155	.179	.200	.229
434	.830	.800	-.099	-.133	-.081	-.095	-.124	-.136	-.184	-.200	474	.800	.800			-.136	-.106	-.071	-.047	-.025	.001

TABLE V.- PRESSURE COEFFICIENTS MEASURED ON VERTICAL TAIL AND SPEED BRAKES - Continued

(b) M = 0.90 - Continued

Pressure coefficients C_p on -

Model orifice number	y/(b/2)	x/c	Upper tail								Model orifice number	y/(b/2)	x/c	Lower tail							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			β ≈ 0°; δ_e = 0°; δ_v = 0°; brakes closed											β ≈ 0°; δ_e = 0°; δ_v = 0°; brakes closed							
401	.110	.647	-.139	-.199		-.207	-.228	-.255	-.283		441	.130	.647	-.351	-.249		-.242	-.213	-.165	-.108	
402	.110	.681	-.014	-.080		-.090	-.113	-.149	-.187		442	.130	.682	-.215	-.095		-.106	-.061	.002	.070	
403	.110	.698	-.019	-.087		-.093	-.116	-.147	-.180		443	.130	.700	-.181	-.091		-.106	-.061	.001	.065	
404	.110	.748	-.060	-.131		-.138	-.159	-.193	-.221		444	.130	.748	-.223	-.128		-.149	-.106	-.042	.022	
405	.110	.832	-.101	-.160		-.163	-.180	-.210	-.234		445	.130	.832	-.244	-.160		-.190	-.152	-.093	-.036	
406	.110	.949	-.197	-.216		-.197	-.202	-.224	-.252		446	.130	.949	-.282	-.187		-.190	-.184	-.165	-.140	
410	.250	.000	1.026	.992		.970	.978	1.024	1.021		450	.300	.000				.898	.929	.946	.965	
411	.250	.200	.019	.051		.095	.087	.038	-.098		451	.300	.200	-.255	.041		.090	.115	.112	.108	
412	.250	.400	-.001	-.005		.017	.003	-.030	-.124		452	.300	.400	-.216	-.006		.006	.040	.068	.103	
413	.250	.600	-.043	-.085		-.085	-.101	-.122	-.167		453	.300	.600	-.223	-.095		-.103	-.067	-.018	.036	
414	.250	.630	-.185	-.224		-.222	-.243	-.275	-.316		454	.300	.633	-.343	-.236		-.230	-.199	-.156	-.112	
415	.250	.668	.013	-.049		-.063	-.081	-.099	-.125		455	.300	.668	-.195	-.077		-.098	-.053	.010	.077	
416	.250	.685	-.004	-.064		-.078	-.095	-.117	-.145		456	.300	.686	-.188	-.074		-.095	-.052	.007	.069	
417	.250	.738	-.037	-.102		-.116	-.136	-.155	-.178		457	.300	.738	-.199	-.105		-.130	-.085	-.023	.038	
418	.250	.825	-.072	-.132		-.143	-.156	-.174	-.196		458	.300	.825	-.211	-.123		-.159	-.120	-.061	-.006	
419	.250	.947	-.170	-.196		-.185	-.187	-.200	-.239		459	.300	.947	-.247	-.198		-.178	-.167	-.139	-.108	
420	.500	.000	1.020	.955		.866	.840	.836	.849		460	.600	.000	.864	.840		.882	.926	.960	.992	
421	.500	.100	.077	.079		.108	.098	.054	-.045		461	.600	.100	-.198	.037		.102	.131	.125	.119	
422	.500	.200	.019	.033		.065	.053	.013	-.086		462	.600	.200	-.252	.017		.056	.086	.095	.104	
423	.500	.300	.006	.012		.031	.019	-.013	-.097		463	.600	.300	-.163	-.001		.024	.057	.079	.103	
424	.500	.400	.006	-.004		-.001	-.014	-.040	-.103		464	.600	.400	-.182	-.020		-.014	.023	.058	.096	
425	.500	.500	.002	-.028		-.033	-.049	-.071	-.114		465	.600	.500	-.173	-.047		-.047	-.007	.039	.087	
426	.500	.600	-.008	-.050		-.059	-.078	-.100	-.125		466	.600	.600				-.086	-.043	.008	.062	
427	.500	.700	-.020	-.069		-.089	-.107	-.126	-.135		467	.600	.700	-.171	-.087		-.103	-.059	-.003	.052	
428	.500	.800	-.051	-.104		-.117	-.132	-.145	-.156		468	.600	.800	-.188	-.111		-.134	-.094	-.038	.015	
429	.500	.900	-.098	-.137		-.143	-.151	-.159	-.171		469	.600	.900	-.203	-.132		-.152	-.128	-.083	-.041	
430	.830	.000	1.035	.946		.832	.784	.756	.745		470	.800	.000	.839	.815		.865	.917	.961	1.004	
431	.830	.200	.042	.029							471	.800	.200				.037	.071	.090	.108	
432	.830	.400	.019	-.006		-.024	-.048	-.069	-.104		472	.800	.400	-.155	-.037		-.023	.017	.057	.098	
433	.830	.600	.018	-.026		-.056	-.079	-.095	-.102		473	.800	.600	-.159	-.077		-.080	-.033	.019	.074	
434	.830	.800	-.022	-.069		-.099	-.119	-.125	-.120		474	.800	.800	-.163	-.110		-.126	-.084	-.028	.024	
			β ≈ 0°; δ_e = 0°; δ_v = 0°; brakes open											β ≈ 0°; δ_e = 0°; δ_v = 0°; brakes open							
401	.110	.647			-.209	-.203	-.214	-.252	-.311	-.414	441	.130	.647			-.251	-.255	-.245	-.203	-.154	-.112
402	.110	.681			-.060	-.057	-.070	-.114	-.180	-.306	442	.130	.682			-.086	-.076	-.050	-.001	.047	.091
403	.110	.698			-.068	-.064	-.077	-.115	-.167	-.297	443	.130	.700			-.087	-.078	-.052	-.005	.041	.083
404	.110	.748			-.122	-.119	-.133	-.170	-.217	-.342	444	.130	.748			-.138	-.132	-.107	-.056	-.008	.030
405	.110	.832			-.170	-.161	-.171	-.207	-.252	-.401	445	.130	.832			-.190	-.184	-.164	-.115	-.070	-.039
406	.110	.949			-.206	-.200	-.202	-.216	-.239	-.454	446	.130	.949			-.196	-.197	-.195	-.178	-.162	-.149
410	.250	.000			.986	.975	.970	1.024	1.013	.983	450	.300	.000			.907	.918	.943	.964	.984	1.018
411	.250	.200			.212	.213	.209	.144	-.019	-.142	451	.300	.200			.185	.191	.200	.184	.161	.202
412	.250	.400			.073	.075	.069	.028	-.121	-.280	452	.300	.400			.056	.059	.073	.087	.106	.147
413	.250	.600			-.070	-.066	-.071	-.103	-.194	-.323	453	.300	.600			-.088	-.085	-.068	-.031	.006	.042
414	.250	.630			-.258	-.253	-.257	-.278	-.348	-.437	454	.300	.633			-.243	-.246	-.236	-.202	-.159	-.128
415	.250	.668			-.061	-.053	-.062	-.111	-.206	-.406	455	.300	.668			-.098	-.092	-.071	-.032	.005	.038
416	.250	.685			-.066	-.061	-.070	-.113	-.203	-.336	456	.300	.686			-.093	-.086	-.062	-.020	.018	.050
417	.250	.738			-.120	-.113	-.123	-.165	-.249	-.388	457	.300	.738			-.128	-.122	-.100	-.058	-.019	.013
418	.250	.825			-.164	-.153	-.161	-.202	-.292	-.451	458	.300	.825			-.166	-.161	-.141	-.099	-.063	-.039
419	.250	.947			-.201	-.190	-.191	-.210	-.316	-.520	459	.300	.947			-.182	-.183	-.179	-.159	-.146	-.140
420	.500	.000			.886	.862	.828	.843	.879	.869	460	.600	.000			.890	.909	.947	.987	1.021	1.060
421	.500	.100			.332	.325	.316	.277	.191	.102	461	.600	.100			.277	.288	.305	.295	.283	.327
422	.500	.200			.212	.214	.211	.175	.061	-.078	462	.600	.200			.153	.159	.175	.179	.176	.221
423	.500	.300			.139	.137	.136	.103	-.003	-.168	463	.600	.300			.101	.106	.124	.132	.139	.181
424	.500	.400			.089	.090	.086	.062	-.025	-.164	464	.600	.400			.056	.063	.084	.104	.124	.165
425	.500	.500			.053	.050	.046	.027	-.036	-.149	465	.600	.500			.020	.028	.052	.084	.116	.155
426	.500	.600			.019	.020	.012	-.003	-.048	-.157	466	.600	.600			-.025	-.016	.011	.051	.089	.129
427	.500	.700			-.016	-.016	-.026	-.036	-.064	-.173	467	.600	.700			-.052	-.043	-.013	.032	.075	.111
428	.500	.800			-.056	-.054	-.059	-.070	-.095	-.192	468	.600	.800			-.089	-.080	-.051	-.003	.041	.073
429	.500	.900			-.089	-.084	-.086	-.090	-.112	-.213	469	.600	.900			-.114	-.108	-.088	-.047	-.012	.013
430	.830	.000			.761	.719	.661	.642	.649	.686	470	.800	.000			.827	.851	.899	.954	.998	1.046
431	.830	.200									471	.800	.200			.111	.118	.145	.159	.171	.224
432	.830	.400			.052	.038	.021	.002	-.034	-.082	472	.800	.400			.026	.038	.070	.106	.139	.186
433	.830	.600			.014	.002	-.020	-.029	-.039	-.077	473	.800	.600			-.042	-.027	.009	.062	.110	.155
434	.830	.800			-.039	-.050	-.067	-.069	-.059	-.091	474	.800	.800			-.099	-.084	-.046	.011	.063	.102

TABLE V.- PRESSURE COEFFICIENTS MEASURED ON VERTICAL TAIL AND SPEED BRAKES - Continued

(b) M = 0.90 - Continued

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper tail								Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Lower tail							
			$\alpha = -20^\circ$	$\alpha = -10^\circ$	$\alpha = -5^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 15^\circ$	$\alpha = 20^\circ$				$\alpha = -20^\circ$	$\alpha = -10^\circ$	$\alpha = -5^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 15^\circ$	$\alpha = 20^\circ$
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = -7.5^\circ$; brakes closed											$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = -7.5^\circ$; brakes closed							
401	.110	.647			-.260	-.271	-.294	-.301	-.316	-.402	441	.130	.647			-.275	-.272	-.246	-.181	-.121	-.066
402	.110	.681			-.132	-.143	-.173	-.204	-.254	-.312	442	.130	.682			-.164	-.149	-.106	-.033	.025	.072
403	.110	.698			-.139	-.150	-.177	-.207	-.242	-.317	443	.130	.700			-.166	-.152	-.109	-.036	.019	.068
404	.110	.748			-.182	-.190	-.222	-.253	-.279	-.373	444	.130	.748			-.205	-.195	-.155	-.077	-.018	.033
405	.110	.832			-.191	-.198	-.224	-.252	-.277	-.387	445	.130	.832			-.233	-.226	-.188	-.114	-.060	-.011
406	.110	.949			-.186	-.188	-.194	-.222	-.231	-.327	446	.130	.949			-.188	-.187	-.179	-.157	-.134	-.111
410	.250	.000			1.002	.993	.995	1.042	1.043	1.001	450	.300	.000			.887	.899	.925	.950	.969	1.003
411	.250	.200			-.072	-.079	-.091	-.142	-.351	-.436	451	.300	.200			-.082	-.064	-.038	-.041	-.085	-.022
412	.250	.400			-.049	-.062	-.084	-.103	-.107	-.150	452	.300	.400			-.078	-.060	-.021	.022	.100	.165
413	.250	.600			-.130	-.137	-.157	-.158	-.173	-.249	453	.300	.600			-.153	-.141	-.107	-.026	.036	.085
414	.250	.630			-.258	-.289	-.309	-.293	-.330	-.398	454	.300	.633			-.268	-.264	-.218	-.144	-.126	-.091
415	.250	.668			-.139	-.149	-.168	-.167	-.186	-.270	455	.300	.668			-.190	-.173	-.128	-.036	.028	.082
416	.250	.685			-.152	-.157	-.176	-.185	-.208	-.287	456	.300	.686			-.171	-.160	-.126	-.039	.025	.074
417	.250	.738			-.178	-.183	-.206	-.219	-.235	-.325	457	.300	.738			-.198	-.188	-.153	-.065	-.005	.046
418	.250	.825			-.180	-.189	-.212	-.218	-.233	-.328	458	.300	.825			-.205	-.199	-.160	-.083	-.023	.023
419	.250	.947			-.162	-.169	-.177	-.184	-.179	-.275	459	.300	.947			-.174	-.168	-.148	-.103	-.067	-.042
420	.500	.000			.890	.868	.838	.844	.876	.868	460	.600	.000			.701	.727	.769	.808	.840	.865
421	.500	.100			-.178	-.171	-.180	-.258	-.438	-.463	461	.600	.100			-.108	-.100	-.087	-.095	-.230	-.287
422	.500	.200			-.048	-.061	-.085	-.126	-.278	-.476	462	.600	.200			-.046	-.026	.012	.039	.057	.082
423	.500	.300			-.021	-.035	-.063	-.082	-.121	-.205	463	.600	.300			-.044	-.027	.014	.063	.102	.149
424	.500	.400			-.035	-.055	-.083	-.101	-.138	-.153	464	.600	.400			-.076	-.060	-.017	.042	.091	.132
425	.500	.500			-.070	-.089	-.119	-.130	-.158	-.221	465	.600	.500			-.110	-.092	-.050	.016	.069	.110
426	.500	.600			-.115	-.135	-.163	-.171	-.195	-.252	466	.600	.600			-.160	-.143	-.099	-.033	.017	.059
427	.500	.700			-.163	-.178	-.202	-.217	-.234	-.305	467	.600	.700			-.185	-.175	-.137	-.073	-.025	.013
428	.500	.800			-.180	-.191	-.215	-.223	-.240	-.312	468	.600	.800			-.195	-.187	-.155	-.094	-.048	-.016
429	.500	.900			-.156	-.162	-.179	-.183	-.196	-.280	469	.600	.900			-.179	-.171	-.145	-.098	-.063	-.042
430	.830	.000			.827	.791	.736	.716	.713	.734	470	.800	.000			.711	.745	.802	.860	.903	.941
431	.830	.200									471	.800	.200			.023	.037	.036	-.025	-.048	.048
432	.830	.400			-.063	-.074	-.092	-.107	-.143	-.175	472	.800	.400			-.075	-.056	-.013	.026	.053	.092
433	.830	.600			-.105	-.117	-.135	-.146	-.165	-.215	473	.800	.600			-.143	-.127	-.084	-.035	.001	.041
434	.830	.800			-.147	-.153	-.164	-.173	-.184	-.245	474	.800	.800			-.178	-.170	-.135	-.094	-.065	-.054
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 7.5^\circ$; brakes closed											$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 7.5^\circ$; brakes closed							
401	.110	.647			.608	.613	.612	.568	.493	.302	441	.130	.647			.638	.643	.650	.654	.647	.655
402	.110	.681			.857	.864	.859	.803	.737	.582	442	.130	.682			.976	.976	.954	.926	.889	.891
403	.110	.698			.881	.873	.843	.776	.697	.722	443	.130	.700			.876	.895	.918	.919	.909	.908
404	.110	.748			.653	.646	.594	.507	.435	.454	444	.130	.748			.679	.689	.690	.695	.703	.705
405	.110	.832			.514	.522	.465	.385	.325	.182	445	.130	.832			.576	.572	.542	.534	.534	.535
406	.110	.949			.336	.358	.317	.269	.231	.006	446	.130	.949			.391	.375	.346	.341	.338	.338
410	.250	.000			.996	.987	.994	1.033	1.045	.982	450	.300	.000			.909	.922	.944	.964	.984	1.015
411	.250	.200			.188	.187	.167	.106	-.065	-.220	451	.300	.200			.184	.194	.206	.205	.204	.247
412	.250	.400			.212	.212	.188	.141	.010	-.159	452	.300	.400			.212	.222	.239	.259	.281	.316
413	.250	.600			.538	.533	.515	.473	.407	.316	453	.300	.600			.516	.525	.540	.560	.569	.585
414	.250	.630			.552	.566	.579	.577	.534	.353	454	.300	.633			.603	.599	.590	.593	.587	.631
415	.250	.668			.847	.863	.888	.903	.888	.749	455	.300	.668			.941	.930	.908	.887	.880	.889
416	.250	.685			.854	.850	.831	.806	.786	.801	456	.300	.686			.855	.862	.871	.877	.884	.884
417	.250	.738			.593	.593	.578	.540	.552	.491	457	.300	.738			.608	.611	.615	.632	.654	.662
418	.250	.825			.436	.444	.439	.404	.427	.287	458	.300	.825			.471	.467	.460	.473	.490	.506
419	.250	.947			.267	.275	.268	.256	.280	.146	459	.300	.947			.282	.277	.274	.287	.303	.319
420	.500	.000			.910	.890	.855	.851	.856	.837	460	.600	.000			.885	.909	.945	.979	1.012	1.048
421	.500	.100			.194	.188	.165	.113	-.016	-.160	461	.600	.100			.174	.189	.207	.204	.199	.243
422	.500	.200			.172	.169	.145	.095	-.041	-.229	462	.600	.200			.160	.172	.190	.198	.206	.247
423	.500	.300			.179	.174	.145	.102	-.021	-.179	463	.600	.300			.170	.181	.199	.216	.233	.269
424	.500	.400			.204	.200	.178	.137	.034	-.117	464	.600	.400			.195	.206	.226	.247	.270	.302
425	.500	.500			.256	.250	.229	.194	.115	-.001	465	.600	.500			.247	.259	.276	.301	.323	.350
426	.500	.600			.262	.257	.235	.214	.176	.091	466	.600	.600			.256	.266	.285	.306	.330	.354
427	.500	.700			.042	.036	.011	.002	-.005	-.067	467	.600	.700			.040	.051	.073	.107	.139	.168
428	.500	.800			-.176	-.179	-.204	-.210	-.219	-.289	468	.600	.800			-.176	-.170	-.150	-.113	-.083	-.057
429	.500	.900			-.307	-.309	-.325	-.326	-.338	-.415	469	.600	.900			-.311	-.308	-.293	-.261	-.236	-.217
430	.830	.000			.880	.852	.800	.773	.746	.756	470	.800	.000			.866	.892	.935	.978	1.021	1.061
431	.830	.200									471	.800	.200			.146	.160	.181	.196	.209	.250
432	.830	.400			.151	.140	.109	.078	.009	-.084	472	.800	.400			.169	.183	.206	.229	.254	.286
433	.830	.600			.116	.105	.074	.052	.027	-.027	473	.800	.600			.150	.164	.189	.219	.252	.281
434	.830	.800			-.061	-.077	-.113	-.125	-.126	-.162	474	.800	.800			-.119	-.103	-.074	-.027	.014	.049

TABLE V.- PRESSURE COEFFICIENTS MEASURED ON VERTICAL TAIL AND SPEED BRAKES - Continued

(b) M = 0.90 - Concluded

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper tail								Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Lower tail							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			β ≈ 5°; δ_e = 0°; δ_v = 0°; brakes closed											β ≈ 5°; δ_e = 0°; δ_v = 0°; brakes closed							
401	.110	.647	-.089	-.155		-.171	-.186	-.207	-.304	-.411	441	.130	.647	-.372	-.223		-.237	-.211	-.141	-.089	-.035
402	.110	.681	.062	.004		-.004	-.033	-.081	-.172	-.281	442	.130	.682	-.272	-.062		-.047	-.011	.068	.124	.174
403	.110	.698	.056	-.003		-.011	-.034	-.083	-.175	-.277	443	.130	.700	-.250	-.056		-.047	-.011	.064	.117	.167
404	.110	.748	.013	-.049							444	.130	.748	-.277	-.094		-.098	-.062	.014	.066	.115
405	.110	.832	-.040	-.089		-.093	-.112	-.149	-.235	-.351	445	.130	.832	-.298	-.123		-.139	-.107	-.040	.004	.047
406	.110	.949	-.156	-.171		-.148	-.155	-.191	-.270	-.401	446	.130	.949	-.334	-.161		-.156	-.158	-.134	-.120	-.100
410	.250	.000	.989	.947		.840	.821	.764	.874	.989	450	.300	.000	.235	.811		.902	.937	.974	1.004	1.038
411	.250	.200	.179	.194		.271	.262	.162	-.021	-.295	451	.300	.200	-.244	.172		.233	.239	.222	.225	.277
412	.250	.400	.103	.086		.120	.108	.043	-.105	-.286	452	.300	.400	-.244	.050		.082	.104	.143	.177	.231
413	.250	.600	.036	-.013		-.017	-.035	-.075	-.166	-.290	453	.300	.600	-.252	-.062		-.060	-.027	.040	.090	.142
414	.250	.630	-.145	-.193							454	.300	.633	-.366	-.219		-.227	-.198	-.135	-.089	-.039
415	.250	.668	.090	.032		.009	-.014	-.050	-.128	-.245	455	.300	.668	-.220	-.052		-.050	-.008	.071	.127	.179
416	.250	.685	.072	.014		-.003	-.027	-.062	-.142	-.252	456	.300	.686	-.234	-.048		-.046	-.008	.067	.121	.171
417	.250	.738	.034	-.025		-.046	-.069	-.098	-.173	-.291	457	.300	.738	-.248	-.076		-.083	-.043	.031	.084	.134
418	.250	.825	-.010	-.061		-.074	-.095	-.118	-.192	-.310	458	.300	.825	-.256	-.093		-.108	-.073	-.005	.038	.082
419	.250	.947	-.122	-.146		-.135	-.143	-.164	-.236	-.348	459	.300	.947	-.295	-.143		-.139	-.135	-.101	-.081	-.054
420	.500	.000				.782	.731	.676	.389	.902	460	.600	.000	.738	.797		.854	.907	.966	1.011	1.055
421	.500	.100	.275	.274		.327	.310	.250	.105	-.099	461	.600	.100	-.087	.227		.296	.304	.285	.285	.337
422	.500	.200	.155	.153		.223	.210	.146	-.001	-.245	462	.600	.200	-.235	.107		.160	.180	.187	.206	.267
423	.500	.300	.111	.102		.140	.125	.070	-.070	-.256	463	.600	.300	-.168	.054		.098	.126	.158	.185	.238
424	.500	.400	.107	.078		.084	.065	.020	-.088	-.221	464	.600	.400	-.169	.019		.046	.079	.127	.167	.218
425	.500	.500	.091	.052		.038	.015	-.019	-.100	-.210	465	.600	.500	-.167	-.018		.002	.039	.099	.148	.200
426	.500	.600	.074	.025		.004	-.021	-.045	-.111	-.209	466	.600	.600	-.186	-.054		-.045	-.004	.066	.117	.168
427	.500	.700				-.026	-.051	-.066	-.118	-.223	467	.600	.700	-.180	-.062		-.063	-.020	.051	.101	.148
428	.500	.800	.017	-.034		-.061	-.081	-.091	-.138	-.243	468	.600	.800	-.200	-.085		-.094	-.055	.012	.059	.102
429	.500	.900	-.039	-.077		-.091	-.105	-.111	-.155	-.238	469	.600	.900	-.214	-.106		-.114	-.091	-.040	-.004	.031
430	.830	.000	1.009	.911		.688	.628	.590	.584	.741	470	.800	.000	.795	.750		.823	.885	.957	1.010	1.055
431	.830	.200	.148	.119		.090	.072	.030	-.083	-.220	471	.800	.200	-.204	.042		.089	.123	.167	.197	.258
432	.830	.400	.121	.066		.010	-.020	-.045	-.093	-.116	472	.800	.400	-.132	-.015		.011	.056	.114	.161	.219
433	.830	.600	.107	.040		-.024	-.055	-.064	-.085	-.117	473	.800	.600	-.141	-.063		-.053	-.004	.070	.126	.180
434	.830	.800	.060	-.009		-.073	-.099	-.095	-.102	-.137	474	.800	.800	-.155	-.096		-.101	-.056	.017	.068	.117
			β ≈ 5°; δ_e = 0°; δ_v = 0°; brakes open											β ≈ 5°; δ_e = 0°; δ_v = 0°; brakes open							
401	.110	.647			.714	.728	.747	.594	.457	.245	441	.130	.647			.733	.727	.724	.715	.722	.742
402	.110	.681			.963	.980	.997	.823	.701	.439	442	.130	.682			1.055	1.046	1.031	1.009	.993	1.000
403	.110	.698			.932	.933	.899	.814	.739	.450	443	.130	.700			.929	.928	.934	.945	.940	.942
404	.110	.748									444	.130	.748			.746	.738	.728	.726	.722	.724
405	.110	.832			.577	.595	.625	.553	.333	-.178	445	.130	.832			.635	.619	.600	.589	.579	.582
406	.110	.949			.394	.408	.426	.366	.148	-.296	446	.130	.949			.426	.412	.398	.392	.383	.384
410	.250	.000			.848	.828	.836	.764	.871	.703	450	.300	.000			.887	.903	.941	.982	1.010	1.044
411	.250	.200			.351	.353	.346	.234	.014	-.281	451	.300	.200			.330	.325	.326	.313	.313	.357
412	.250	.400			.305	.307	.295	.210	.014	-.230	452	.300	.400			.287	.288	.302	.325	.344	.382
413	.250	.600			.599	.598	.583	.512	.407	.163	453	.300	.600			.575	.576	.582	.600	.612	.630
414	.250	.630									454	.300	.633			.657	.653	.655	.663	.675	.693
415	.250	.668			.908	.915	.952	.830	.751	.723	455	.300	.668			.978	.976	.976	.977	.980	1.011
416	.250	.685			.865	.859	.846	.794	.756	.630	456	.300	.686			.848	.853	.865	.882	.889	.898
417	.250	.738			.615	.614	.620	.612	.522	.272	457	.300	.738			.627	.626	.631	.649	.659	.673
418	.250	.825			.470	.472	.487	.480	.366	.060	458	.300	.825			.496	.493	.495	.510	.522	.539
419	.250	.947			.296	.296	.309	.316	.229	-.096	459	.300	.947			.309	.305	.310	.330	.341	.360
420	.500	.000			.813	.775	.727	.682	.423	.892	460	.600	.000			.832	.860	.914	.975	1.016	1.059
421	.500	.100			.398	.395	.382	.305	.133	-.130	461	.600	.100			.366	.369	.377	.361	.358	.401
422	.500	.200			.319	.318	.307	.228	.045	-.228	462	.600	.200			.270	.269	.283	.288	.298	.349
423	.500	.300			.279	.275	.262	.189	.008	-.219	463	.600	.300			.242	.247	.266	.287	.306	.348
424	.500	.400			.281	.278	.262	.198	.048	-.166	464	.600	.400			.252	.259	.277	.305	.328	.365
425	.500	.500			.314	.310	.294	.241	.122	-.113	465	.600	.500			.292	.298	.316	.345	.366	.398
426	.500	.600			.298	.292	.279	.240	.158	-.013	466	.600	.600			.277	.284	.304	.338	.361	.392
427	.500	.700			.063	.052	.040	.020	-.035	-.110	467	.600	.700			.039	.051	.078	.120	.155	.192
428	.500	.800			-.164	-.173	-.179	-.183	-.241	-.319	468	.600	.800			-.178	-.167	-.144	-.104	-.071	-.035
429	.500	.900			-.298	-.305	-.304	-.302	-.353	-.425	469	.600	.900			-.309	-.302	-.287	-.251	-.222	-.193
430	.830	.000			.755	.708	.637	.601	.577	.754	470	.800	.000			.789	.824	.891	.964	1.013	1.061
431	.830	.200			.215	.200	.183	.126	-.007	-.204	471	.800	.200			.203	.204	.230	.265	.289	.339
432	.830	.400			.073	.050	.031	.014	-.010	-.014	472	.800	.400			.199	.210	.237	.275	.304	.345
433	.830	.600			.125	.107	.082	.065	.022	-.048	473	.800	.600			.148	.163	.194	.239	.276	.318
434	.830	.800			-.069	-.090	-.115	-.114	-.132	-.155	474	.800	.800			-.132	-.115	-.080	-.024	.024	.073

TABLE V.- PRESSURE COEFFICIENTS MEASURED ON VERTICAL TAIL AND SPEED BRAKES - Continued

(c) M = 0.95

Pressure coefficients C_p on -

Model orifice number	y/b/2	x/c	Upper tail							Model orifice number	y/b/2	x/c	Lower tail						
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			β ≈ -5°; δ_e = 0°; δ_v = 0°; brakes closed										β ≈ -5°; δ_e = 0°; δ_v = 0°; brakes closed							
401	.110	.647				-.270	-.236	-.246	-.287	-.388	441	.130	.647				-.264	-.248	-.199	-.144	-.087
402	.110	.681				-.113	-.148	-.113	-.155	-.317	442	.130	.682				-.109	-.068	-.014	.033	.092
403	.110	.698				-.122	-.153	-.119	-.155	-.313	443	.130	.700				-.100	-.062	-.012	.032	.095
404	.110	.748				-.179	-.195	-.173	-.219	-.363	444	.130	.748				-.155	-.117	-.055	-.004	.053
405	.110	.832				-.228	-.246	-.238	-.288	-.408	445	.130	.832				-.206	-.167	-.103	-.048	.001
406	.110	.949				-.272	-.309	-.279	-.356	-.462	446	.130	.949				-.272	-.240	-.184	-.144	-.119
410	.250	.000				.935	.945	.754	.685	.569	450	.300	.000				.733	.769	.809	.875	.901
411	.250	.200				-.052	-.087	-.133	-.136	-.062	451	.300	.200				-.012	.004	.004	-.154	.048
412	.250	.400				-.031	-.049	-.086	-.127	-.150	452	.300	.400				-.002	.019	.038	.034	.092
413	.250	.600				-.121	-.134	-.140	-.149	-.268	453	.300	.600				-.104	-.080	-.047	-.016	.044
414	.250	.630				-.275	-.277	-.286	-.301	-.405	454	.300	.633				-.251	-.226	-.179	-.146	-.089
415	.250	.668				-.097	-.129	-.167	-.145	-.290	455	.300	.668				-.114	-.072	-.011	.039	.093
416	.250	.685				-.110	-.136	-.140	-.137	-.290	456	.300	.686				-.099	-.064	-.012	.037	.090
417	.250	.738				-.157	-.178	-.185	-.190	-.326	457	.300	.738				-.133	-.096	-.041	.009	.064
418	.250	.825				-.200	-.219	-.236	-.240	-.360	458	.300	.825				-.168	-.131	-.072	-.018	.027
419	.250	.947				-.267	-.287	-.294	-.314	-.417	459	.300	.947				-.241	-.212	-.151	-.108	-.077
420	.500	.000				.851	.801	.719	.461	.769	460	.600	.000				.709	.767	.825	.908	.944
421	.500	.100				-.219	-.337	-.348	-.282	-.309	461	.600	.100				-.151	-.060	-.637	-.474	.053
422	.500	.200				-.017	-.055	-.062	-.212	-.045	462	.600	.200				-.003	.032	.100	.048	.092
423	.500	.300				-.011	-.019	-.050	-.174	-.091	463	.600	.300				.008	.029	.059	.029	.082
424	.500	.400				-.034	-.037	-.056	-.179	-.115	464	.600	.400				-.025	.000	.025	.020	.078
425	.500	.500				-.066	-.076	-.086	-.183	-.175	465	.600	.500				-.059	-.029	.005	.018	.077
426	.500	.600				-.101	-.112	-.121	-.192	-.230	466	.600	.600				-.106	-.072	-.027	.002	.062
427	.500	.700									467	.600	.700				-.119	-.080	-.030	.009	.057
428	.500	.800				-.171	-.189	-.212	-.243	-.298	468	.600	.800				-.156	-.119	-.061	-.016	.026
429	.500	.900				-.203	-.227	-.249	-.275	-.323	469	.600	.900				-.201	-.163	-.099	-.056	-.021
430	.830	.000				.804	.750	.684	.603	.644	470	.800	.000				.761	.823	.885	.961	1.007
431	.830	.200				.015	-.141	-.216	-.199	-.163	471	.800	.200				.042	.064	.100	.059	.092
432	.830	.400				-.045	-.052	-.049	-.077	-.091	472	.800	.400				-.028	-.006	.013	.010	.068
433	.830	.600				-.090	-.101	-.092	-.120	-.179	473	.800	.600				-.095	-.062	-.022	.009	.065
434	.830	.800				-.144	-.161	-.161	-.174	-.235	474	.800	.800				-.146	-.110	-.056	-.013	.024
			β ≈ -5°; δ_e = 0°; δ_v = 0°; brakes open										β ≈ -5°; δ_e = 0°; δ_v = 0°; brakes open							
401	.110	.647	-.286	-.219	.632	.604	.404	.664	.550	.461	441	.130	.647			.513	.600	.651	.652	.572	.647
402	.110	.681	-.165	-.077	.860	.863	.510	.940	.863	.687	442	.130	.682	-.188	-.077	.838	.947	.962	.928	.787	.870
403	.110	.698	-.163	-.088	.831	.828	.516	.875	.904	.637	443	.130	.700	-.199	-.093	.727	.877	.907	.878	.772	.813
404	.110	.748	-.210	-.141	.651	.620	.492	.725	.638	.413	444	.130	.748	-.226	-.129	.564	.666	.695	.696	.661	.669
405	.110	.832	-.261	-.190	.502	.481	.408	.583	.457	.238	445	.130	.832	-.264	-.177	.503	.542	.548	.547	.512	.533
406	.110	.949	-.329	-.271	.333	.328	.262	.380	.278	.096	446	.130	.949	-.329	-.230	.390	.371	.362	.357	.321	.341
410	.250	.000	1.068	.998	.953	.936	.936	.788	.782	.681	450	.300	.000	.207	.561	.697	.724	.767	.818	.858	.893
411	.250	.200	-.185	-.251	.058	.039	.015	-.083	-.167	-.157	451	.300	.200	-.248	-.080	.085	.083	.088	.077	.114	.119
412	.250	.400	-.087	-.016	.172	.158	.146	.095	.034	-.118	452	.300	.400	-.169	-.054	.190	.204	.231	.236	.241	.276
413	.250	.600	-.166	-.102	.483	.458	.365	.473	.481	.317	453	.300	.600	-.248	-.137	.439	.488	.504	.497	.518	.534
414	.250	.630	-.320	-.241	.556	.542	.408	.576	.510	.366	454	.300	.633	-.346	-.219	.555	.572	.580	.554	.526	.580
415	.250	.668	-.139	-.054	.708	.738	.550	.837	.837	.580	455	.300	.668	-.297	-.150	.906	.890	.844	.757	.748	.747
416	.250	.685	-.151	-.069	.673	.693	.504	.726	.818	.574	456	.300	.686	-.254	-.139	.808	.815	.770	.707	.730	.708
417	.250	.738	-.180	-.113	.574	.578	.373	.545	.584	.417	457	.300	.738	-.274	-.164	.586	.615	.621	.609	.628	.597
418	.250	.825	-.225	-.162	.452	.440	.274	.464	.442	.277	458	.300	.825	-.287	-.198	.469	.474	.493	.508	.508	.496
419	.250	.947	-.284	-.238	.286	.279	.171	.304	.278	.161	459	.300	.947	-.353	-.267	.317	.297	.304	.317	.319	.327
420	.500	.000	1.041	.946	.876	.843	.790	.722	.409	.789	460	.600	.000	.353	.552	.656	.694	.762	.829	.884	.924
421	.500	.100	-.250	-.708	-.296	-.330	-.388	-.284	-.329	-.335	461	.600	.100	-.650	-.464	-.235	-.246	-.243	-.162	.039	-.129
422	.500	.200	-.123	-.291	.070	.077	.079	.004	-.264	-.127	462	.600	.200	-.226	-.002	.107	.116	.134	.121	.134	.166
423	.500	.300	-.107	-.003	.147	.135	.108	.065	-.108	-.108	463	.600	.300	-.069	-.012	.153	.170	.203	.195	.184	.221
424	.500	.400	-.091	.000	.190	.177	.146	.137	-.014	-.046	464	.600	.400	-.066	-.028	.173	.199	.233	.234	.231	.262
425	.500	.500	-.114	-.035	.248	.230	.197	.206	.087	.063	465	.600	.500	-.117	-.061	.209	.243	.281	.287	.292	.315
426	.500	.600	-.142	-.073	.258	.236	.184	.207	.122	.109	466	.600	.600	.057	1.204	.217	.247	.281	.293	.305	.321
427	.500	.700	-.169	-.087							467	.600	.700	-.203	-.119	.031	.052	.079	.109	.134	.152
428	.500	.800	-.195	-.135	-.177	-.201	-.213	-.169	-.199	-.296	468	.600	.800	-.230	-.158	-.179	-.168	-.146	-.107	-.081	-.071
429	.500	.900	-.226	-.166	-.310	-.330	-.345	-.293	-.305	-.412	469	.600	.900			-.321	-.313	-.289	-.250	-.233	-.232
430	.830	.000	1.048	.931	.852	.811	.755	.695	.648	.663	470	.800	.000	.447	.602	.719	.762	.837	.897	.950	1.001
431	.830	.200	-.012	-.057	.008	-.034	-.157	-.163	-.157	-.176	471	.800	.200	-.320	-.124	.009	.015	.046	.119	.156	.171
432	.830	.400	-.107	-.032	.140	.124	.121	.108	.072	-.026	472	.800	.400	-.071	.003	.182	.188	.199	.204	.204	.241
433	.830	.600	-.106	-.067	.114	.097	.092	.107	.049	-.017	473	.800	.600	-.152	-.082	.157	.176	.193	.211	.226	.255
434	.830	.800	-.157	-.115	-.042	-.059	-.084	-.100	-.139	-.157	474	.800	.800			-.106	-.080	-.043	-.017	.009	.027

TABLE V.- PRESSURE COEFFICIENTS MEASURED ON VERTICAL TAIL AND SPEED BRAKES - Continued

(c) M = 0.95 - Continued

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper tail								Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Lower tail							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			β ≈ 0°; δ_e = 0°; δ_v = 0°; brakes closed											β ≈ 0°; δ_e = 0°; δ_v = 0°; brakes closed							
401	.110	.647	-.274	-.230		-.220	-.224	-.243	-.283	-.390	441	.130	.647	-.345	-.231		-.230	-.221	-.193	-.134	-.068
402	.110	.681	-.129	-.061		-.052	-.065	-.099	-.148	-.342	442	.130	.682	-.334	-.065		-.075	-.038	.019	.077	.134
403	.110	.698	-.122	-.068		-.064	-.072	-.103	-.139	-.326	443	.130	.700	-.297	-.056		-.070	-.035	.018	.075	.127
404	.110	.748	-.160	-.129		-.126	-.138	-.172	-.210	-.375	444	.130	.748	-.295	-.111		-.124	-.091	-.030	.030	.085
405	.110	.832	-.113	-.180		-.165	-.183	-.222	-.272	-.427	445	.130	.832	-.325	-.169		-.184	-.147	-.081	-.021	.029
406	.110	.949	-.182	-.245		-.227	-.271	-.343	-.368	-.508	446	.130	.949	-.386	-.237		-.245	-.212	-.152	-.112	-.082
410	.250	.000	1.052	1.014		1.013	1.020	1.014	.958	.875	450	.300	.000				.931	.954	.963	.983	1.020
411	.250	.200	-.011	.055		.129	.138	.126	.061	.102	451	.300	.200	.063	.133		.125	.137	.107	.044	.127
412	.250	.400	-.102	.004		.047	.050	.036	-.036	-.075	452	.300	.400	-.093	.059		.040	.061	.071	.070	.138
413	.250	.600	-.143	-.076		-.061	-.065	-.076	-.121	-.261	453	.300	.600	-.228	-.053		-.074	-.050	-.015	.024	.084
414	.250	.630	-.289	-.246		-.237	-.239	-.247	-.287	-.387	454	.300	.633	-.329	-.213		-.229	-.212	-.181	-.136	-.079
415	.250	.668	-.105	-.030		-.032	-.038	-.052	-.110	-.288	455	.300	.668	-.284	-.044		-.077	-.032	.025	.083	.140
416	.250	.685	-.113	-.048		-.049	-.057	-.078	-.121	-.299	456	.300	.686	-.276	-.042		-.062	-.030	.021	.075	.131
417	.250	.738	-.135	-.099		-.103	-.113	-.133	-.172	-.329	457	.300	.738	-.274	-.085		-.105	-.071	-.011	.047	.100
418	.250	.825	-.093	-.146		-.143	-.160	-.181	-.226	-.369	458	.300	.825	-.291	-.128		-.150	-.113	-.049	.009	.059
419	.250	.947	-.155	-.215		-.246	-.265	-.279	-.297	-.408	459	.300	.947	-.320	-.225		-.222	-.184	-.122	-.079	-.048
420	.500	.000	1.040	.973		.897	.881	.860	.837	.850	460	.600	.000	.837	.860		.912	.950	.974	1.005	1.051
421	.500	.100	.070	.080		.142	.149	.157	.106	.161	461	.600	.100	.112	.139		.137	.153	.114	.057	.144
422	.500	.200	-.023	.036		.094	.101	.103	.052	.087	462	.600	.200	.050	.103		.088	.107	.092	.044	.127
423	.500	.300	-.068	.026		.060	.060	.061	.006	.006	463	.600	.300	-.016	.072		.055	.078	.081	.059	.129
424	.500	.400	-.096	.004		.028	.026	.022	-.033	-.071	464	.600	.400	-.080	.038		.017	.043	.062	.065	.130
425	.500	.500	-.116	-.019		-.010	-.014	-.017	-.068	-.150	465	.600	.500	-.140	.000		-.020	.009	.042	.068	.127
426	.500	.600	-.122	-.048		-.047	-.055	-.060	-.104	-.221	466	.600	.600				-.074	-.039	.008	.053	.107
427	.500	.700	-.127	-.063		-.074	-.085	-.096	-.128	-.275	467	.600	.700	-.229	-.067		-.080	-.046	.006	.056	.104
428	.500	.800	-.108	-.108		-.120	-.134	-.151	-.180	-.296	468	.600	.800	-.251	-.114		-.129	-.089	-.027	.027	.073
429	.500	.900	-.092	-.135		-.146	-.160	-.179	-.215	-.314	469	.600	.900	-.291	-.165		-.179	-.137	-.067	-.019	.019
430	.830	.000	1.052	.959		.851	.820	.794	.771	.763	470	.800	.000	.818	.839		.899	.942	.978	1.017	1.065
431	.830	.200	-.007	.034							471	.800	.200				.069	.092	.089	.055	.133
432	.830	.400	-.081	.002		-.005	-.011	-.011	-.041	-.073	472	.800	.400	-.074	.018		.004	.034	.060	.070	.132
433	.830	.600	-.093	-.024		-.044	-.057	-.063	-.086	-.176	473	.800	.600	-.173	-.051		-.068	-.027	.023	.065	.119
434	.830	.800	-.088	-.071		-.105	-.124	-.138	-.143	-.214	474	.800	.800	-.225	-.118		-.124	-.082	-.018	.036	.080
			β ≈ 0°; δ_e = 0°; δ_v = 0°; brakes open											β ≈ 0°; δ_e = 0°; δ_v = 0°; brakes open							
401	.110	.647			-.216	-.212	-.208	-.225	-.279	-.401	441	.130	.647			-.228	-.233	-.231	-.215	-.178	-.130
402	.110	.681			-.025	-.023	-.027	-.065	-.150	-.344	442	.130	.682			-.047	-.043	-.024	.012	.054	.106
403	.110	.698			-.037	-.037	-.038	-.070	-.128	-.338	443	.130	.700			-.045	-.042	-.024	.010	.050	.101
404	.110	.748			-.105	-.106	-.106	-.143	-.209	-.376	444	.130	.748			-.107	-.105	-.088	-.045	.001	.047
405	.110	.832			-.163	-.160	-.167	-.209	-.291	-.436	445	.130	.832			-.166	-.165	-.146	-.100	-.051	-.012
406	.110	.949			-.232	-.224	-.244	-.311	-.378	-.556	446	.130	.949			-.244	-.243	-.221	-.168	-.134	-.108
410	.250	.000			1.013	1.012	1.020	1.026	.976	.900	450	.300	.000			.939	.947	.968	.979	.997	1.035
411	.250	.200			.242	.243	.252	.229	.144	.182	451	.300	.200			.222	.223	.227	.183	.110	.181
412	.250	.400			.100	.103	.111	.093	.000	-.060	452	.300	.400			.093	.092	.098	.091	.073	.132
413	.250	.600			-.041	-.037	-.033	-.052	-.129	-.297	453	.300	.600			-.050	-.052	-.042	-.022	.001	.044
414	.250	.630			-.233	-.230	-.225	-.227	-.278	-.408	454	.300	.633			-.220	-.223	-.215	-.190	-.156	-.120
415	.250	.668			-.030	-.023	-.024	-.069	-.220	-.406	455	.300	.668			-.066	-.066	-.054	-.024	.006	.045
416	.250	.685			-.038	-.034	-.033	-.068	-.144	-.331	456	.300	.686			-.054	-.052	-.036	-.006	.026	.064
417	.250	.738			-.101	-.098	-.098	-.136	-.214	-.385	457	.300	.738			-.097	-.096	-.081	-.046	-.008	.031
418	.250	.825			-.154	-.146	-.151	-.197	-.286	-.443	458	.300	.825			-.141	-.140	-.124	-.083	-.044	-.012
419	.250	.947			-.259	-.260	-.272	-.303	-.368	-.544	459	.300	.947			-.213	-.211	-.191	-.149	-.121	-.105
420	.500	.000			.911	.900	.879	.851	.842	.802	460	.600	.000			.924	.941	.975	1.006	1.041	1.081
421	.500	.100			.359	.353	.358	.365	.312	.348	461	.600	.100			.312	.317	.328	.290	.242	.314
422	.500	.200			.239	.242	.252	.257	.199	.217	462	.600	.200			.187	.187	.197	.178	.117	.197
423	.500	.300			.162	.163	.174	.179	.114	.093	463	.600	.300			.137	.138	.149	.133	.092	.162
424	.500	.400			.114	.115	.123	.125	.057	.007	464	.600	.400			.091	.093	.106	.107	.093	.150
425	.500	.500			.076	.075	.079	.081	.016	-.026	465	.600	.500			.053	.055	.072	.088	.097	.147
426	.500	.600			.036	.037	.040	.039	-.017	-.143	466	.600	.600			.002	.004	.025	.052	.081	.130
427	.500	.700			.002	.001	-.001	-.006	-.055	-.195	467	.600	.700			-.025	-.020	.000	.038	.077	.118
428	.500	.800			-.046	-.048	-.052	-.061	-.105	-.218	468	.600	.800			-.072	-.066	-.042	.008	.051	.090
429	.500	.900			-.075	-.076	-.080	-.097	-.138	-.254	469	.600	.900			-.120	-.114	-.084	-.031	.012	.042
430	.830	.000			.798	.757	.715	.660	.646	.592	470	.800	.000			.861	.884	.927	.973	1.019	1.063
431	.830	.200									471	.800	.200			.145	.149	.168	.160	.116	.207
432	.830	.400			.072	.063	.058	.058	.030	-.004	472	.800	.400			.060	.066	.089	.108	.110	.172
433	.830	.600			.028	.016	.005	.004	-.016	-.086	473	.800	.600			-.016	-.007	.021	.063	.101	.154
434	.830	.800			-.032	-.045	-.064	-.069	-.074	-.138	474	.800	.800			-.088	-.077	-.042	.018	.072	.116

TABLE V.- PRESSURE COEFFICIENTS MEASURED ON VERTICAL TAIL AND SPEED BRAKES - Continued

(c) M = 0.95 - Continued

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper tail							Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Lower tail						
			$\alpha = -20^\circ$	$\alpha = -10^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 15^\circ$	$\alpha = 20^\circ$			$\alpha = -20^\circ$	$\alpha = -10^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 15^\circ$	$\alpha = 20^\circ$
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = -7.5^\circ$; brakes closed										$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = -7.5^\circ$; brakes closed							
401	.110	.647			-.245	-.249	-.259	-.278	-.302	-.395	441	.130	.647			-.251	-.252	-.237	-.223	-.146	-.072
402	.110	.681			-.097	-.107	-.121	-.153	-.188	-.315	442	.130	.682			-.131	-.125	-.091	-.030	.026	.085
403	.110	.698			-.112	-.120	-.136	-.159	-.191	-.323	443	.130	.700			-.139	-.132	-.089	-.035	.020	.081
404	.110	.748			-.179	-.192	-.207	-.231	-.265	-.395	444	.130	.748			-.189	-.182	-.146	-.090	-.018	.047
405	.110	.832			-.215	-.227	-.251	-.284	-.325	-.461	445	.130	.832			-.236	-.230	-.194	-.125	-.051	.009
406	.110	.949			-.231	-.240	-.294	-.352	-.388	-.512	446	.130	.949			-.269	-.269	-.231	-.146	-.112	-.080
410	.250	.000			1.026	1.024	1.029	1.022	.975	.856	450	.300	.000			.924	.931	.947	.970	.994	1.023
411	.250	.200			-.050	-.054	-.051	-.027	-.126	-.066	451	.300	.200			-.050	-.042	-.028	-.086	-.201	-.159
412	.250	.400			-.017	-.028	-.043	-.040	-.090	-.086	452	.300	.400			-.038	-.028	-.001	.030	.074	.160
413	.250	.600			-.099	-.101	-.113	-.119	-.137	-.229	453	.300	.600			-.113	-.106	-.088	-.032	.029	.087
414	.250	.630			-.271	-.273	-.277	-.274	-.294	-.364	454	.300	.633			-.248	-.249	-.237	-.182	-.138	-.097
415	.250	.668			-.126	-.136	-.147	-.134	-.172	-.300	455	.300	.668			-.194	-.186	-.130	-.046	.025	.087
416	.250	.685			-.136	-.140	-.149	-.154	-.188	-.301	456	.300	.686			-.157	-.151	-.117	-.048	.020	.078
417	.250	.738			-.175	-.188	-.206	-.206	-.233	-.352	457	.300	.738			-.193	-.187	-.152	-.085	-.005	.055
418	.250	.825			-.196	-.216	-.235	-.242	-.276	-.394	458	.300	.825			-.209	-.203	-.167	-.093	-.014	.041
419	.250	.947			-.222	-.253	-.291	-.294	-.310	-.397	459	.300	.947			-.246	-.237	-.179	-.085	-.045	-.018
420	.500	.000			.918	.904	.875	.852	.848	.814	460	.600	.000			.753	.775	.807	.842	.895	.914
421	.500	.100			-.189	-.180	-.155	-.100	-.212	-.138	461	.600	.100			-.097	-.090	-.058	-.152	-.325	-.237
422	.500	.200			-.025	-.036	-.046	-.026	-.102	-.024	462	.600	.200			-.008	.002	.028	.048	-.003	.071
423	.500	.300			.015	.000	-.016	-.013	-.064	-.054	463	.600	.300			-.005	.003	.032	.069	.057	.131
424	.500	.400			-.008	-.021	-.040	-.037	-.077	-.106	464	.600	.400			-.038	-.031	.000	.045	.054	.124
425	.500	.500			-.043	-.059	-.081	-.080	-.107	-.173	465	.600	.500			-.076	-.066	-.034	.016	.045	.109
426	.500	.600			-.104	-.120	-.139	-.138	-.154	-.236	466	.600	.600			-.137	-.128	-.098	-.043	.001	.060
427	.500	.700			-.165	-.183	-.202	-.203	-.233	-.340	467	.600	.700			-.193	-.183	-.145	-.093	-.041	.017
428	.500	.800			-.195	-.211	-.226	-.237	-.263	-.360	468	.600	.800			-.206	-.200	-.171	-.107	-.052	-.003
429	.500	.900			-.173	-.193	-.226	-.241	-.271	-.348	469	.600	.900			-.227	-.219	-.172	-.084	-.050	-.026
430	.830	.000			.858	.818	.775	.741	.722	.694	470	.800	.000			.761	.789	.833	.880	.940	.973
431	.830	.200									471	.800	.200			.067	.071	.048	-.012	.053	.029
432	.830	.400			-.037	-.047	-.059	-.051	-.075	-.114	472	.800	.400			-.039	-.028	.005	.025	.033	.082
433	.830	.600			-.095	-.107	-.120	-.119	-.135	-.214	473	.800	.600			-.126	-.116	-.079	-.042	-.002	.043
434	.830	.800			-.157	-.168	-.185	-.197	-.205	-.283	474	.800	.800			-.193	-.182	-.146	-.102	-.056	-.035
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 7.5^\circ$; brakes closed										$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 7.5^\circ$; brakes closed							
401	.110	.647			.640	.646	.644	.592	.506	.355	441	.130	.647			.666	.669	.677	.673	.651	.669
402	.110	.681			.884	.900	.887	.821	.788	.634	442	.130	.682			.999	.997	.983	.941	.902	.900
403	.110	.698			.920	.921	.899	.826	.832	.776	443	.130	.700			.900	.913	.948	.950	.936	.933
404	.110	.748			.692	.689	.654	.555	.562	.485	444	.130	.748			.706	.716	.724	.731	.735	.735
405	.110	.832			.548	.569	.519	.415	.410	.232	445	.130	.832			.610	.610	.582	.572	.565	.565
406	.110	.949			.388	.413	.381	.306	.300	.062	446	.130	.949			.445	.431	.402	.393	.385	.383
410	.250	.000			1.023	1.019	1.023	1.044	1.040	1.003	450	.300	.000			.939	.946	.967	.981	.998	1.033
411	.250	.200			.220	.219	.213	.154	.045	.024	451	.300	.200			.218	.222	.234	.215	.194	.240
412	.250	.400			.245	.244	.235	.183	.070	-.140	452	.300	.400			.247	.252	.267	.280	.288	.326
413	.250	.600			.573	.572	.561	.516	.471	.368	453	.300	.600			.547	.554	.572	.588	.590	.606
414	.250	.630			.579	.591	.595	.598	.550	.403	454	.300	.633			.632	.628	.618	.621	.597	.646
415	.250	.668			.864	.881	.898	.910	.906	.794	455	.300	.668			.970	.959	.936	.897	.897	.891
416	.250	.685			.887	.887	.879	.847	.855	.821	456	.300	.686			.885	.891	.904	.903	.919	.906
417	.250	.738			.627	.629	.621	.587	.603	.507	457	.300	.738			.641	.642	.647	.666	.683	.691
418	.250	.825			.471	.477	.480	.444	.468	.311	458	.300	.825			.509	.505	.496	.508	.517	.533
419	.250	.947			.313	.321	.326	.302	.328	.172	459	.300	.947			.332	.327	.321	.332	.343	.361
420	.500	.000			.927	.911	.890	.879	.863	.885	460	.600	.000			.914	.933	.967	.997	1.024	1.065
421	.500	.100			.222	.221	.212	.165	.093	.102	461	.600	.100			.209	.217	.234	.209	.185	.234
422	.500	.200			.202	.201	.191	.144	.047	.001	462	.600	.200			.195	.201	.216	.211	.199	.244
423	.500	.300			.208	.207	.197	.156	.058	-.084	463	.600	.300			.204	.210	.227	.235	.238	.275
424	.500	.400			.242	.235	.222	.182	.091	-.084	464	.600	.400			.231	.238	.255	.272	.281	.314
425	.500	.500			.295	.290	.276	.238	.173	.055	465	.600	.500			.284	.292	.311	.331	.343	.369
426	.500	.600			.301	.296	.282	.260	.228	.142	466	.600	.600			.291	.298	.317	.337	.354	.381
427	.500	.700			.076	.067	.046	.035	.031	-.033	467	.600	.700			.065	.075	.098	.132	.159	.190
428	.500	.800			-.159	-.166	-.186	-.197	-.196	-.263	468	.600	.800			-.167	-.159	-.136	-.099	-.071	-.046
429	.500	.900			-.306	-.312	-.332	-.337	-.337	-.403	469	.600	.900			-.320	-.313	-.293	-.256	-.228	-.209
430	.830	.000			.905	.873	.838	.806	.783	.777	470	.800	.000			.894	.915	.956	.998	1.033	1.079
431	.830	.200									471	.800	.200			.180	.187	.206	.210	.206	.253
432	.830	.400			.190	.184	.167	.137	.086	-.023	472	.800	.400			.207	.216	.238	.256	.267	.300
433	.830	.600				.149	.126	.100	.078	.015	473	.800	.600			.189	.200	.224	.254	.276	.307
434	.830	.800			-.023	-.039	-.069	-.086	-.089	-.138	474	.800	.800			-.088	-.076	-.045	.000	.037	.075

TABLE V.- PRESSURE COEFFICIENTS MEASURED ON VERTICAL TAIL AND SPEED BRAKES - Continued

(c) M = 0.95 - Concluded

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper tail								Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Lower tail							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			β ≈ 5°; δ_e = 0°; δ_v = 0°; brakes closed											β ≈ 5°; δ_e = 0°; δ_v = 0°; brakes closed							
401	.110	.647	-.137	-.198		-.171	-.163	-.176	-.281	-.406	441	.130	.647	-.377	-.183		-.209	-.202	-.171	-.121	-.042
402	.110	.681	.049	-.001		.020	.008	-.058	-.199	-.329	442	.130	.682	-.392	-.042		-.025	.008	.066	.125	.195
403	.110	.698	.043	-.013		.008	.000	-.066	-.203	-.309	443	.130	.700	-.368	-.042		-.017	.009	.062	.120	.188
404	.110	.748	.003	-.072							444	.130	.748	-.357	-.089		-.080	-.052	.010	.069	.138
405	.110	.832	-.032	-.111		-.095	-.117	-.185	-.309	-.463	445	.130	.832	-.380	-.146		-.136	-.106	-.042	.019	.080
406	.110	.949	-.114	-.181		-.149	-.167	-.245	-.367	-.578	446	.130	.949	-.399	-.213		-.207	-.165	-.120	-.081	-.045
410	.250	.000	1.025	.973		.892	.904	.794	.674	.969	450	.300	.000	.494	.771		.938	.966	.992	1.020	1.060
411	.250	.200	.141	.226		.303	.319	.264	.112	-.053	451	.300	.200	.048	.273		.263	.258	.231		.261
412	.250	.400	.015	.092		.145	.157	.123	-.007	-.196	452	.300	.400	-.160	.130		.109	.120	.129		.222
413	.250	.600	-.004	-.018		.003	.002	-.035	-.162	-.292	453	.300	.600	-.269	-.021		-.033	-.012	.028		.147
414	.250	.630	-.201	-.219							454	.300	.633	-.357	-.183		-.209	-.195	-.159		-.045
415	.250	.668	.079	.026		.031	.021	-.026	-.157	-.288	455	.300	.668	-.324	-.028		-.036	.004	.067		.202
416	.250	.685	.057	.005		.014	.004	-.043	-.172	-.302	456	.300	.686	-.323	-.024		-.019	.010	.065		.191
417	.250	.738	.024	-.045		-.040	-.052	-.096	-.214	-.346	457	.300	.738	-.345	-.067		-.067	-.034	.026		.154
418	.250	.825	-.003	-.083		-.077	-.097	-.149	-.262	-.425	458	.300	.825	-.336	-.110		-.104	-.069	-.008		.112
419	.250	.947	-.086	-.167		-.144	-.171	-.228	-.321	-.525	459	.300	.947	-.358	-.195		-.179	-.137	-.090		-.003
420	.500	.000				.828	.774	.623	.458	.818	460	.600	.000	.752	.825		.900	.944	.986		1.078
421	.500	.100	.254	.304		.357	.366	.351	.257	.261	461	.600	.100	.241	.316		.324	.320	.279		.324
422	.500	.200	.098	.170		.249	.263	.239	.150	.097	462	.600	.200	.070	.198		.184	.191	.178		.251
423	.500	.300	.027	.114		.162	.174	.153	.062	-.014	463	.600	.300	-.042	.133		.121	.141	.140		.226
424	.500	.400	.029	.080		.105	.109	.087	-.006	-.106	464	.600	.400	-.114	.079		.071	.092	.114		.214
425	.500	.500	.034	.047		.057	.052	.029	-.065	-.167	465	.600	.500	-.163	.029		.022	.050	.087		.201
426	.500	.600	.035	.014		.016	.007	-.020	-.113	-.208	466	.600	.600	-.225	-.031		-.038	.000	.049		.174
427	.500	.700				-.020	-.034	-.065	-.144	-.279	467	.600	.700	-.270	-.052		-.048	-.013	.046		.164
428	.500	.800	.015	-.051		-.063	-.083	-.122	-.190	-.345	468	.600	.800	-.269	-.102		-.098	-.054	.010		.128
429	.500	.900	-.021	-.079		-.100	-.123	-.165	-.222	-.400	469	.600	.900	-.281	-.150		-.146	-.095	-.033		.068
430	.830	.000	1.037	.923		.733	.668	.573	.518	.564	470	.800	.000	.671	.761		.859	.915	.973		1.077
431	.830	.200	.080	.090		.098	.115	.110	.057	.060	471	.800	.200	.017	.125		.104	.131	.137		.246
432	.830	.400	.058	.063		.036	.023	.008	-.045	-.071	472	.800	.400	-.100	.034		.037	.068	.102		.213
433	.830	.600	.070	.030		-.014	-.034	-.054	-.098	-.140	473	.800	.600	-.198	-.044		-.041	.000	.059		.188
434	.830	.800	.050	-.019		-.079	-.105	-.132	-.152	-.262	474	.800	.800	-.219	-.119		-.108	-.058	.012		.138
			β ≈ 5°; δ_e = 0°; δ_v = 0°; brakes open											β ≈ 5°; δ_e = 0°; δ_v = 0°; brakes open							
401	.110	.647			.741	.760	.779	.625	.435	.345	441	.130	.647			.766	.764	.757	.729	.734	.758
402	.110	.681			.989	1.013	1.033	.830	.604	.584	442	.130	.682			1.084	1.081	1.062	1.032	1.013	1.012
403	.110	.698			.962	.970	.949	.812	.605	.537	443	.130	.700			.961	.965	.967	.978	.977	.978
404	.110	.748									444	.130	.748			.779	.774	.764	.757	.753	.753
405	.110	.832			.613	.637	.656	.580	.416	-.155	445	.130	.832			.673	.663	.640	.621	.611	.612
406	.110	.949			.445	.463	.475	.423	.257	-.285	446	.130	.949			.477	.471	.453	.439	.428	.429
410	.250	.000			.897	.882	.902	.795	.812	.998	450	.300	.000			.924	.940	.972	1.000	1.026	1.064
411	.250	.200			.383	.388	.393	.286	.122	-.069	451	.300	.200			.363	.359	.354	.319	.312	.356
412	.250	.400			.336	.341	.339	.252	.087	-.156	452	.300	.400			.321	.322	.331	.337	.348	.391
413	.250	.600			.633	.637	.628	.543	.370	.236	453	.300	.600			.609	.613	.617	.628	.634	.654
414	.250	.630									454	.300	.633			.691	.690	.688	.679	.682	.714
415	.250	.668			.935	.946	.974	.869	.648	.840	455	.300	.668			1.009	1.011	1.006	.993	.997	1.025
416	.250	.685			.899	.898	.887	.823	.646	.674	456	.300	.686			.882	.890	.900	.917	.927	.930
417	.250	.738			.648	.653	.654	.638	.538	.331	457	.300	.738			.661	.664	.666	.678	.687	.704
418	.250	.825			.506	.514	.522	.514	.431	.061	458	.300	.825			.534	.534	.532	.541	.548	.567
419	.250	.947			.345	.350	.355	.361	.301	-.142	459	.300	.947			.357	.357	.359	.371	.381	.405
420	.500	.000			.855	.829	.776	.708	.405	.864	460	.600	.000			.867	.894	.942	.991	1.032	1.077
421	.500	.100			.427	.428	.429	.361	.251	.288	461	.600	.100			.400	.402	.403	.361	.350	.399
422	.500	.200			.348	.351	.353	.275	.149	.096	462	.600	.200			.301	.304	.308	.291	.295	.348
423	.500	.300			.308	.310	.308	.234	.098	-.019	463	.600	.300			.276	.281	.293	.299	.307	.356
424	.500	.400			.313	.315	.306	.239	.105	-.082	464	.600	.400			.288	.295	.308	.323	.337	.378
425	.500	.500			.350	.351	.340	.282	.161	-.072	465	.600	.500			.331	.338	.351	.368	.385	.419
426	.500	.600			.334	.332	.322	.283	.182	.039	466	.600	.600			.315	.324	.341	.365	.385	.424
427	.500	.700			.088	.079	.068	.056	-.007	-.082	467	.600	.700			.065	.079	.104	.142	.172	.213
428	.500	.800			-.152	-.161	-.170	-.163	-.215	-.321	468	.600	.800			-.171	-.158	-.132	-.089	-.060	-.025
429	.500	.900			-.301	-.310	-.316	-.294	-.337	-.450	469	.600	.900			-.325	-.312	-.289	-.245	-.216	-.188
430	.830	.000			.775	.738	.675	.626	.569	.616	470	.800	.000			.826	.857	.917	.979	1.028	1.078
431	.830	.200			.241	.236	.229	.168	.075	.055	471	.800	.200			.236	.237	.254	.269	.285	.346
432	.830	.400			.208	.213	.207	.185	.158	.091	472	.800	.400			.236	.247	.269	.294	.315	.360
433	.830	.600			.164	.152	.129	.107	.056	-.031	473	.800	.600			.188	.203	.230	.268	.298	.343
434	.830	.800			-.034	-.053	-.078	-.081	-.104	-.151	474	.800	.800			-.108	-.087	-.052	.001	.044	.095

TABLE V.- PRESSURE COEFFICIENTS MEASURED ON VERTICAL TAIL AND SPEED BRAKES - Continued

(d) M = 1.03

Pressure coefficients C_p on -

Model orifice number	y/b/2	x/c	Upper tail								Model orifice number	y/b/2	x/c	Lower tail							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			β ≈ -5°; δ_e = 0°; δ_v = 0°; brakes closed											β ≈ -5°; δ_e = 0°; δ_v = 0°; brakes closed							
401	.110	.647				-.143	-.133	-.195	-.199	-.284	441	.130	.647				-.155	-.163	-.167	-.151	-.023
402	.110	.681				.017	-.032	-.074	-.102	-.175	442	.130	.682				.022	.004	.021	.106	.192
403	.110	.698				.005	-.040	-.084	-.105	-.176	443	.130	.700				.027	.037	.050	.106	.185
404	.110	.748				-.050	-.080	-.116	-.163	-.237	444	.130	.748				-.034	-.017	.005	.063	.144
405	.110	.832				-.097	-.129	-.171	-.237	-.301	445	.130	.832				-.082	-.063	-.036	.026	.097
406	.110	.949				-.145	-.196	-.234	-.348	-.396	446	.130	.949				-.156	-.137	-.095	-.046	-.005
410	.250	.000				1.007	.937	.585	.445	.848	450	.300	.000				.813	.867	.907	.948	.969
411	.250	.200				-.020	.001	-.101	-.080	-.574	451	.300	.200				.032	.004	-.110	-.102	.059
412	.250	.400				.092	.054	-.022	-.060	.010	452	.300	.400				.100	.120	.101	.131	.182
413	.250	.600				-.003	-.037	-.079	-.110	-.122	453	.300	.600				.000	.013	.011	.037	.130
414	.250	.630				-.186	-.171	-.227	-.263	-.294	454	.300	.633				-.170	-.158	-.169	-.141	-.043
415	.250	.668				.029	-.025	-.144	-.155	-.129	455	.300	.668				.005	.007	.023	.108	.196
416	.250	.685				.018	-.035	-.071	-.108	-.143	456	.300	.686				.019	.028	.038	.107	.189
417	.250	.738				-.031	-.071	-.114	-.161	-.195	457	.300	.738				-.017	.003	.020	.081	.158
418	.250	.825				-.072	-.111	-.145	-.215	-.249	458	.300	.825				-.051	-.034	-.006	.057	.124
419	.250	.947				-.134	-.179	-.218	-.311	-.338	459	.300	.947				-.119	-.104	-.059	-.008	.034
420	.500	.000				.905	.843	.706	.716	.830	460	.600	.000				.783	.867	.924	.981	1.011
421	.500	.100				-.478	-.165	-.565	-.603	-.797	461	.600	.100				-.518	-.495	-.454	-.323	-.149
422	.500	.200				.026	.049	-.037	-.016	-.138	462	.600	.200				.162	.160	.098	.062	.175
423	.500	.300				.133	.081	.007	-.015	-.026	463	.600	.300				.145	.150	.126	.123	.157
424	.500	.400				.105	.067	-.010	-.025	.015	464	.600	.400				.096	.106	.088	.110	.164
425	.500	.500				.061	.024	-.042	-.051	.000	465	.600	.500				.061	.072	.062	.091	.165
426	.500	.600				.016	-.013	-.085	-.091	-.066	466	.600	.600				.007	.017	.019	.053	.143
427	.500	.700									467	.600	.700				.002	.009	.020	.076	.148
428	.500	.800				-.046	-.082	-.146	-.183	-.195	468	.600	.800				-.035	-.020	.003	.059	.122
429	.500	.900				-.078	-.118	-.186	-.240	-.249	469	.600	.900				-.076	-.059	-.021	.031	.084
430	.830	.000				.860	.790	.690	.635	.672	470	.800	.000				.825	.909	.969	1.027	1.066
431	.830	.200				.176	.039	-.252	-.248	-.522	471	.800	.200				.195	.198	.143	.111	.172
432	.830	.400				.076	.057	.028	.053	.089	472	.800	.400				.088	.093	.071	.096	.152
433	.830	.600				.026	.001	-.027	-.051	.010	473	.800	.600				.016	.024	.025	.065	.152
434	.830	.800				-.026	-.057	-.089	-.148	-.135	474	.800	.800				-.029	-.014	.011	.066	.115
			β ≈ -5°; δ_e = 0°; δ_v = 0°; brakes open											β ≈ -5°; δ_e = 0°; δ_v = 0°; brakes open							
401	.110	.647	-.188	-.228	.698	.682	.457	.587	.668	.503	441	.130	.647			.580	.667	.712	.677	.629	.694
402	.110	.681	-.009	-.048	.912	.932	.551	.754	.889	.664	442	.130	.682	-.144	-.063	.874	1.005	.989	.896	.838	.897
403	.110	.698	-.011	-.033	.890	.882	.568	.776	.810	.651	443	.130	.700	-.136	-.072	.749	.927	.954	.903	.860	.851
404	.110	.748	-.060	-.079	.719	.675	.579	.747	.666	.490	444	.130	.748	-.184	-.109	.580	.727	.760	.757	.760	.724
405	.110	.832	-.112	-.126	.583	.551	.531	.663	.526	.323	445	.130	.832	-.228	-.133	.537	.622	.621	.602	.598	.596
406	.110	.949	-.202	-.203	.434	.425	.406	.460	.361	.189	446	.130	.949	-.310	-.196	.463	.475	.454	.435	.425	.429
410	.250	.000	1.126	1.078	1.027	1.015	.931	.653	.489	.926	450	.300	.000	.788	.400	.786	.817	.852	.896	.943	.958
411	.250	.200	-.059	-.159	.171	.146	.127	.012	-.011	-.041	451	.300	.200	-.641	-.083	.182	.189	.176	.191	.196	.229
412	.250	.400	-.110	-.042	.265	.256	.237	.181	.096	.087	452	.300	.400	.046	-.021	.277	.298	.311	.306	.326	.365
413	.250	.600	-.036	-.079	.563	.534	.406	.500	.461	.411	453	.300	.600	-.114	-.135	.502	.561	.574	.589	.601	.611
414	.250	.630	-.225	-.251	.630	.622	.420	.550	.574	.451	454	.300	.633	-.273	-.276	.623	.649	.647	.607	.582	.640
415	.250	.668	-.009	-.040	.774	.810	.501	.784	.778	.631	455	.300	.668	-.130	-.173	.983	.957	.898	.811	.759	.787
416	.250	.685	-.001	-.033	.742	.763	.487	.778	.666	.641	456	.300	.686	-.127	-.133	.858	.879	.832	.809	.784	.785
417	.250	.738	-.030	-.051	.645	.647	.417	.678	.532	.519	457	.300	.738	-.162	-.151	.644	.690	.698	.704	.712	.687
418	.250	.825	-.071	-.089	.533	.527	.362	.582	.471	.377	458	.300	.825	-.199	-.159	.547		.572	.546	.566	.579
419	.250	.947	-.148	-.157	.384	.387	.284	.412	.344	.266	459	.300	.947	-.284	-.215	.423	.404	.397	.392	.398	.423
420	.500	.000	1.099	1.019	.946	.917	.852	.691	.692	.833	460	.600	.000	.593	.556	.736	.788	.847	.907	.972	.995
421	.500	.100	-.151	-.477	.049	-.184	-.267	-.190	-.495	-.578	461	.600	.100	-.871	-.541	-.110	-.137	-.073	-.278	-.167	.210
422	.500	.200	-.068	-.192	.178	.182	.184	.098	.114	-.251	462	.600	.200	-.439	.039	.209	.224	.216	.257	.265	.261
423	.500	.300	-.003	.000	.227	.240	.204	.148	.099	.042	463	.600	.300	.038	.040	.248	.271	.279	.265	.271	.305
424	.500	.400	-.080	-.004	.270	.276	.240	.201	.148	.150	464	.600	.400	.068	.021	.262	.294	.310	.299	.313	.350
425	.500	.500	-.136	-.036	.326	.324	.283	.254	.219	.204	465	.600	.500	-.003	-.032	.290	.334	.361	.359	.376	.405
426	.500	.600	-.028	-.061	.336	.327	.259	.228	.216	.218	466	.600	.600	.140	1.246	.298	.338	.364	.374	.388	.413
427	.500	.700	-.036	-.060							467	.600	.700	-.117	-.117	.109	.142	.166	.187	.211	.245
428	.500	.800	-.047	-.065	-.088	-.122	-.136	-.131	-.193	-.199	468	.600	.800	-.171	-.132	-.109	-.083	-.061	-.035	-.012	.022
429	.500	.900	-.082	-.091	-.231	-.255	-.271	-.261	-.334	-.345	469	.600	.900			-.256	-.236	-.214	-.196	-.179	-.146
430	.830	.000	1.104	1.005	.914	.884	.807	.704	.628	.664	470	.800	.000	.602	.609	.792	.845	.904	.961	1.023	1.060
431	.830	.200	.102	-.104	.170	.092	-.051	-.127	-.253	-.264	471	.800	.200	-.369	-.154	.121	.126	.191	.258	.258	.282
432	.830	.400	-.056	-.023	.230	.225	.224	.233	.142	.079	472	.800	.400	.087	.061	.272	.284	.280	.280	.290	.321
433	.830	.600	-.113	-.058	.216	.198	.190	.176	.154	.097	473	.800	.600	-.052	-.077	.245	.271	.282	.299	.316	.343
434	.830	.800	.007	-.048	.064	.044	.015	-.039	-.047	-.068	474	.800	.800			-.015	.023	.050	.073	.098	.128

TABLE V.- PRESSURE COEFFICIENTS MEASURED ON VERTICAL TAIL AND SPEED BRAKES - Continued

(d) M = 1.03 - Continued

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper tail								Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Lower tail							
			$\alpha = -20^\circ$	$\alpha = -10^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 15^\circ$	$\alpha = 20^\circ$				$\alpha = -20^\circ$	$\alpha = -10^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 15^\circ$	$\alpha = 20^\circ$
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed											$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed							
401	.110	.647	-.162	-.177		-.117	-.127	-.173	-.206	-.284	441	.130	.647	-.288	-.179		-.132	-.136	-.141	-.123	-.037
402	.110	.681	.019	-.029		.062	.048	-.023	-.102	-.228	442	.130	.682	-.266	-.075		.022	.011	.024	.134	.229
403	.110	.698	.028	-.010		.055	.040	-.013	-.075	-.204	443	.130	.700	-.228	.003		.048	.060	.074	.134	.221
404	.110	.748	-.032	-.070		-.011	-.033	-.102	-.141	-.245	444	.130	.748	-.230	-.062		-.009	.005	.026	.085	.173
405	.110	.832	-.092	-.130		-.045	-.077	-.162	-.242	-.323	445	.130	.832	-.296	-.104		-.061	-.047	-.016	.046	.125
406	.110	.949	-.176	-.208		-.113	-.181	-.273	-.386	-.450	446	.130	.949	-.378	-.191		-.131	-.117	-.083	-.022	.029
410	.250	.000	1.117	1.056		1.041	1.027	.972	.829	.832	450	.300	.000				.964	.990	1.012	1.040	1.077
411	.250	.200	.097	.100		.202	.222	.188	.180	.232	451	.300	.200	.192	.171		.194	.187	.147	.146	.211
412	.250	.400	.069	.020		.139	.142	.100	.049	.041	452	.300	.400	.041	.098		.131	.135	.117	.129	.225
413	.250	.600	.010	-.016		.044	.036	-.006	-.053	-.135	453	.300	.600	-.128	-.004		.036	.042	.041	.070	.159
414	.250	.630	-.176	-.193		-.141	-.148	-.176	-.217	-.277	454	.300	.633	-.257	-.160		-.129	-.128	-.132	-.109	-.039
415	.250	.668	.043	-.006		.081	.066	-.007	-.064	-.165	455	.300	.668	-.206	-.080		-.007	.004	.029	.137	.234
416	.250	.685	.033	-.006		.069	.054	.005	-.069	-.172	456	.300	.686	-.177	-.005		.049	.054	.066	.134	.222
417	.250	.738	.000	-.040		-.010	-.011	-.062	-.109	-.199	457	.300	.738	-.213	-.035		.010	.024	.045	.103	.190
418	.250	.825	-.048	-.085		-.024	-.050	-.108	-.186	-.262	458	.300	.825	-.256	-.076		-.031	-.018	.013	.076	.153
419	.250	.947	-.116	-.154		-.121	-.150	-.180	-.280	-.352	459	.300	.947	-.355	-.169		-.094	-.083	-.048	.013	.064
420	.500	.000	1.096	1.014		.941	.913	.864	.721	.695	460	.600	.000	.690	.847		.955	.992	1.024	1.062	1.106
421	.500	.100	.183	.138		.214	.235	.215	.220	.251	461	.600	.100	-.057	.184		.201	.198	.156	.163	.228
422	.500	.200	.077	.063		.174	.193	.168	.154	.198	462	.600	.200	.201	.150		.165	.163	.129	.135	.213
423	.500	.300	.019	.029		.150	.157	.126	.100	.120	463	.600	.300	.123	.118		.144	.144	.122	.130	.217
424	.500	.400	.068	.025		.122	.123	.086	.050	.044	464	.600	.400	.041	.079		.113	.119	.104	.119	.213
425	.500	.500	.054	.019		.091	.085	.044	.005	-.027	465	.600	.500	-.029	.038		.083	.090	.086	.111	.208
426	.500	.600	.031	-.002		.052	.039	.001	-.029	-.087	466	.600	.600				.034	.040	.046	.087	.185
427	.500	.700	.010	-.019		.038	.018	-.024	-.068	-.151	467	.600	.700	-.155	-.022		.029	.039	.054	.111	.191
428	.500	.800	-.017	-.053		-.004	-.031	-.084	-.142	-.198	468	.600	.800	-.210	-.067		-.014	.000	.030	.090	.165
429	.500	.900	-.048	-.088		-.026	-.056	-.124	-.200	-.255	469	.600	.900	-.264	-.108		-.055	-.037	-.003	.060	.122
430	.830	.000	1.107	1.004		.911	.871	.804	.748	.646	470	.800	.000	.671	.836		.946	.988	1.028	1.072	1.119
431	.830	.200	.092	.052							471	.800	.200				.153	.151	.126	.136	.218
432	.830	.400	.074	.012		.096	.088	.049	.033	.037	472	.800	.400	.034	.060		.104	.112	.100	.119	.213
433	.830	.600	.054	.016		.058	.036	-.009	-.026	-.049	473	.800	.600	-.073	-.019		.036	.047	.055	.105	.199
434	.830	.800	.019	-.018		.008	-.025	-.074	-.121	-.150	474	.800	.800	-.184	-.074		-.011	.006	.036	.100	.171
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open											$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open							
401	.110	.647			-.106	-.099	-.096	-.145	-.207	-.256	441	.130	.647			-.109	-.120	-.126	-.142	-.130	-.061
402	.110	.681			.087	.091	.086	.021	-.117	-.213	442	.130	.682			.081	.063	.044	.022	.097	.195
403	.110	.698			.074	.080	.076	.017	-.107	-.198	443	.130	.700			.086	.076	.080	.071	.102	.187
404	.110	.748			-.001	.008	.003	-.072	-.159	-.250	444	.130	.748			.018	.009	.013	.012	.048	.137
405	.110	.832			-.058	-.044	-.057	-.142	-.264	-.343	445	.130	.832			-.036	-.045	-.037	-.037	.010	.086
406	.110	.949			-.119	-.110	-.142	-.232	-.383	-.481	446	.130	.949			-.119	-.124	-.114	-.101	-.056	.001
410	.250	.000			1.061	1.047	1.037	.987	.824	.843	450	.300	.000			.977	.985	1.009	1.025	1.051	1.093
411	.250	.200			.302	.310	.332	.289	.272	.251	451	.300	.200			.300	.285	.265	.222	.206	.267
412	.250	.400			.178	.187	.205	.160	.104	.057	452	.300	.400			.194	.176	.165	.130	.134	.222
413	.250	.600			.062	.068	.073	.023	-.054	-.153	453	.300	.600			.068	.056	.052	.037	.053	.130
414	.250	.630			-.119	-.113	-.109	-.143	-.201	-.269	454	.300	.633			-.100	-.111	-.109	-.114	-.092	-.024
415	.250	.668			.065	.078	.078	-.022	-.193	-.270	455	.300	.668			.030	-.002	-.035	-.075	.023	.127
416	.250	.685			.074	.080	.078	.022	-.090	-.224	456	.300	.686			.079	.068	.066	.053	.079	.156
417	.250	.738			.002	.014	.011	-.065	-.146	-.277	457	.300	.738			.027	.018	.018	.010	.041	.122
418	.250	.825			-.040	-.028	-.038	-.111	-.230	-.359	458	.300	.825			-.016	-.026	-.022	-.025	.019	.088
419	.250	.947			-.136	-.132	-.143	-.184	-.327	-.473	459	.300	.947			-.094	-.097	-.092	-.083	-.044	.002
420	.500	.000			.981	.955	.911	.860	.785	.783	460	.600	.000			.974	.992	1.028	1.056	1.092	1.138
421	.500	.100			.417	.420	.437	.410	.388	.357	461	.600	.100			.390	.377	.364	.333	.335	.393
422	.500	.200			.300	.312	.339	.314	.291	.275	462	.600	.200			.272	.250	.239	.201	.201	.281
423	.500	.300			.226	.238	.265	.237	.206	.190	463	.600	.300			.233	.214	.200	.160	.162	.246
424	.500	.400			.191	.200	.217	.186	.144	.118	464	.600	.400			.196	.182	.177	.145	.148	.236
425	.500	.500			.162	.169	.179	.140	.088	.054	465	.600	.500			.163	.151	.151	.129	.141	.231
426	.500	.600			.132	.136	.138	.099	.036	.001	466	.600	.600			.114	.105	.107	.093	.117	.207
427	.500	.700			.101	.106	.103	.061	-.027	-.066	467	.600	.700			.094	.087	.091	.084	.117	.203
428	.500	.800			.056	.063	.053	.000	-.072	-.131	468	.600	.800			.048	.044	.054	.056	.102	.180
429	.500	.900			.026	.033	.022	-.036	-.112	-.190	469	.600	.900			.008	.006	.019	.028	.076	.142
430	.830	.000			.870	.824	.763	.690	.604	.574	470	.800	.000			.916	.940	.988	1.026	1.070	1.122
431	.830	.200									471	.800	.200			.237	.210	.196	.166	.185	.284
432	.830	.400			.159	.158	.154	.114	.087	.093	472	.800	.400			.168	.159	.165	.145	.159	.254
433	.830	.600			.124	.118	.106	.062	.016	.025	473	.800	.600			.098	.092	.104	.102	.135	.233
434	.830	.800			.066	.060	.040	-.012	-.055	-.083	474	.800	.800			.034	.035	.053	.065	.120	.205

TABLE V.- PRESSURE COEFFICIENTS MEASURED ON VERTICAL TAIL AND SPEED BRAKES - Continued

(d) M = 1.03 - Continued

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper tail								Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Lower tail						
			$\alpha = -20^\circ$	$\alpha = -10^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 15^\circ$	$\alpha = 20^\circ$				$\alpha = -20^\circ$	$\alpha = -10^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 15^\circ$	$\alpha = 20^\circ$
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = -7.5^\circ$; brakes closed											$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = -7.5^\circ$; brakes closed							
401	.110	.647			-.129	-.130	-.137	-.194	-.244	-.328	441	.130	.647			-.141	-.145	-.138	-.144	-.144	-.018
402	.110	.681			.021	.019	.013	-.091	-.155	-.245	442	.130	.682			-.005	-.007	-.021	.003	.055	.159
403	.110	.698			.004	-.003	-.008	-.061	-.131	-.241	443	.130	.700			-.009	-.011	.014	.032	.058	.153
404	.110	.748			-.088	-.089	-.108	-.183	-.191	-.315	444	.130	.748			-.078	-.078	-.062	-.042	.003	.122
405	.110	.832			-.127	-.129	-.159	-.231	-.273	-.377	445	.130	.832			-.122	-.118	-.097	-.071	.001	.095
406	.110	.949			-.136	-.126	-.202	-.303	-.385	-.474	446	.130	.949			-.175	-.164	-.138	-.105	-.039	.028
410	.250	.000			1.065	1.053	1.040	.995	.846	.843	450	.300	.000			.956	.971	.999	1.027	1.053	1.085
411	.250	.200			-.018	.009	.047	.026	-.019	-.258	451	.300	.200			.020	.009	-.020	-.097	-.100	.021
412	.250	.400			.088	.074	.068	.014	-.083	.022	452	.300	.400			.071	.071	.093	.093	.126	.248
413	.250	.600			.015	.012	.005	-.053	-.117	-.147	453	.300	.600			.006	.004	.013	.033	.071	.162
414	.250	.630			-.168	-.159	-.163	-.220	-.265	-.280	454	.300	.633			-.140	-.143	-.161	-.132	-.090	-.022
415	.250	.668			-.029	-.042	-.056	-.101	-.139	-.206	455	.300	.668			-.088	-.086	-.052	-.013	.024	.157
416	.250	.685			-.039	-.033	-.039	-.109	-.158	-.223	456	.300	.686			-.048	-.049	-.049	-.014	.037	.143
417	.250	.738			-.099	-.106	-.126	-.166	-.195	-.285	457	.300	.738			-.101	-.096	-.083	-.051	.013	.128
418	.250	.825			-.107	-.120	-.145	-.192	-.236	-.317	458	.300	.825			-.111	-.102	-.079	-.048	.037	.124
419	.250	.947			-.138	-.139	-.169	-.214	-.294	-.360	459	.300	.947			-.126	-.109	-.086	-.067	.018	.084
420	.500	.000			.980	.954	.915	.869	.800	.719	460	.600	.000			.811	.844	.894	.931	.964	.989
421	.500	.100			-.185	-.146	-.058	-.048	-.053	-.484	461	.600	.100			-.056	-.125	-.198	-.195	-.175	-.144
422	.500	.200			-.040	-.005	.055	-.002	.004	.073	462	.600	.200			.092	.097	.122	.037	.045	.176
423	.500	.300			.124	.107	.096	.045	-.024	.051	463	.600	.300			.105	.103	.126	.123	.126	.207
424	.500	.400			.103	.089	.074	.019	-.044	-.007	464	.600	.400			.075	.073	.091	.098	.108	.201
425	.500	.500			.064	.052	.035	-.021	-.087	-.081	465	.600	.500			.042	.043	.061	.073	.090	.186
426	.500	.600			.005	-.005	-.023	-.069	-.112	-.141	466	.600	.600			-.019	-.014	.001	.015	.035	.130
427	.500	.700			-.103	-.112	-.138	-.210	-.246	-.309	467	.600	.700			-.119	-.113	-.100	-.082	-.030	.081
428	.500	.800			-.106	-.115	-.143	-.208	-.227	-.319	468	.600	.800			-.117	-.110	-.096	-.072	-.009	.075
429	.500	.900			-.087	-.077	-.124	-.207	-.276	-.342	469	.600	.900			-.144	-.127	-.075	-.058	.006	.068
430	.830	.000			.919	.881	.825	.767	.696	.661	470	.800	.000			.816	.854	.913	.961	1.005	1.039
431	.830	.200									471	.800	.200			.170	.140	.147	.120	.111	.198
432	.830	.400			.073	.060	.060	.010	-.031	-.002	472	.800	.400			.077	.077	.087	.088	.087	.169
433	.830	.600			.014	.005	-.008	-.054	-.091	-.106	473	.800	.600			-.009	-.002	.012	.023	.033	.125
434	.830	.800			-.061	-.065	-.085	-.134	-.184	-.237	474	.800	.800			-.092	-.082	-.070	-.054	-.005	.053
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 7.5^\circ$; brakes closed											$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 7.5^\circ$; brakes closed							
401	.110	.647			.715	.723	.719	.660	.580	.520	441	.130	.647			.740	.741	.741	.716	.715	.724
402	.110	.681			.946	.962	.947	.882	.824	.717	442	.130	.682			1.062	1.053	1.035	.994	.943	.947
403	.110	.698			.986	.983	.961	.891	.930	.761	443	.130	.700			.964	.975	1.014	1.017	.994	.991
404	.110	.748			.767	.761	.723	.628	.713	.556	444	.130	.748			.773	.784	.797	.797	.801	.806
405	.110	.832			.634	.650	.593	.478	.540	.368	445	.130	.832			.688	.689	.661	.641	.633	.640
406	.110	.949			.489	.513	.477	.372	.419	.219	446	.130	.949			.545	.529	.498	.477	.469	.474
410	.250	.000			1.085	1.080	1.073	1.026	.948	.849	450	.300	.000			1.003	1.009	1.022	1.031	1.047	1.085
411	.250	.200			.311	.317	.315	.269	.183	.220	451	.300	.200			.322	.320	.307	.272	.227	.303
412	.250	.400			.339	.340	.333	.280	.171	.078	452	.300	.400			.345	.348	.354	.345	.342	.396
413	.250	.600			.655	.652	.642	.587	.570	.476	453	.300	.600			.626	.631	.651	.656	.650	.675
414	.250	.630			.659	.671	.673	.659	.574	.521	454	.300	.633			.710	.704	.686	.659	.647	.705
415	.250	.668			.930	.953	.958	.957	.886	.810	455	.300	.668			1.031	1.018	.987	.924	.941	.920
416	.250	.685			.957	.956	.944	.902	.938	.814	456	.300	.686			.949	.956	.972	.961	.976	.957
417	.250	.738			.709	.708	.702	.660	.684	.597	457	.300	.738			.718	.719	.727	.737	.750	.763
418	.250	.825			.562	.569	.571	.513	.534	.457	458	.300	.825			.596	.591	.581	.578	.585	.609
419	.250	.947			.416	.425	.432	.370	.420	.347	459	.300	.947			.436	.428	.420	.417	.425	.446
420	.500	.000			.998	.979	.945	.897	.870	.762	460	.600	.000			.977	.996	1.025	1.045	1.070	1.115
421	.500	.100			.314	.320	.316	.284	.221	.274	461	.600	.100			.313	.314	.306	.264	.219	.300
422	.500	.200			.295	.299	.297	.259	.179	.209	462	.600	.200			.300	.300	.297	.270	.238	.310
423	.500	.300			.304	.307	.298	.257	.162	.141	463	.600	.300			.307	.309	.311	.298	.284	.343
424	.500	.400			.334	.333	.324	.278	.202	.114	464	.600	.400			.329	.334	.346	.340	.339	.387
425	.500	.500			.388	.384	.374	.326	.286	.187	465	.600	.500			.377	.386	.401	.403	.408	.445
426	.500	.600			.396	.390	.375	.338	.321	.246	466	.600	.600			.385	.392	.407	.411	.424	.455
427	.500	.700			.173	.164	.142	.107	.104	.062	467	.600	.700			.158	.168	.192	.206	.229	.270
428	.500	.800			-.067	-.075	-.099	-.130	-.134	-.175	468	.600	.800			-.079	-.069	-.046	-.032	-.008	.031
429	.500	.900			-.217	-.226	-.249	-.281	-.294	-.339	469	.600	.900			-.237	-.230	-.206	-.196	-.174	-.138
430	.830	.000			.970	.945	.898	.840	.818	.748	470	.800	.000			.958	.980	1.018	1.046	1.079	1.129
431	.830	.200									471	.800	.200			.285	.288	.287	.270	.250	.317
432	.830	.400			.289	.285	.269	.229	.180	.122	472	.800	.400			.307	.313	.329	.326	.329	.374
433	.830	.600			.261	.252	.229	.190	.173	.114	473	.800	.600			.289	.300	.321	.332	.349	.388
434	.830	.800			.084	.069	.039	.001	-.006	-.058	474	.800	.800			.014	.027	.057	.080	.113	.160

TABLE V.- PRESSURE COEFFICIENTS MEASURED ON VERTICAL TAIL AND SPEED BRAKES - Continued

(d) M = 1.03 - Concluded

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper tail								Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Lower tail							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed											$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed							
401	.110	.647	-.141	-.129		-.071	-.055	-.094	-.226	-.374	441	.130	.647	-.344	-.169		-.102	-.102	-.094	-.056	.021
402	.110	.681	.088	.043		.118	.109	.012	-.167	-.326	442	.130	.682	-.320	-.011		.009	.067	.134	.208	.287
403	.110	.698	.094	.052		.107	.101	.001	-.131	-.318	443	.130	.700	-.320	-.011		.082	.102	.137	.203	.280
404	.110	.748	.052	-.019							444	.130	.748	-.289	-.057		.021	.042	.080	.151	.228
405	.110	.832	.044	-.082		.002	-.018	-.116	-.269	-.420	445	.130	.832	-.368	-.108		-.023	-.001	.039	.106	.177
406	.110	.949	-.024	-.143		-.038	-.063	-.189	-.376	-.516	446	.130	.949	-.457	-.176		-.091	-.063	-.022	.024	.072
410	.250	.000	1.085	1.031		.954	.814	.584	.426	.930	450	.300	.000	.913	.655		.989	1.024	1.050	1.076	1.113
411	.250	.200	.245	.261		.364	.389	.273	.240	-.001	451	.300	.200	.094	.288		.315	.298	.268	.253	.333
412	.250	.400	.075	.119		.213	.240	.180	.081	-.133	452	.300	.400	-.072	.162		.166	.171	.171	.205	.295
413	.250	.600	.029	.039		.090	.100	.021	-.065	-.271	453	.300	.600	-.226	.014		.066	.073	.089	.145	.225
414	.250	.630	-.153	-.146							454	.300	.633	-.322	-.149		-.101	-.097	-.088	-.044	.028
415	.250	.668	.105	.053		.125	.121	.023	-.119	-.295	455	.300	.668	-.285	-.018		-.013	.053	.130	.208	.291
416	.250	.685	.101	.060		.111	.106	.011	-.103	-.302	456	.300	.686	-.250	.015		.074	.100	.134	.201	.278
417	.250	.738	.073	.007		.058	.048	-.034	-.136	-.332	457	.300	.738	-.277	-.030		.037	.059	.095	.167	.244
418	.250	.825	.068	-.041		.024	.005	-.088	-.203	-.375	458	.300	.825	-.308	-.072		.003	.031	.070	.137	.206
419	.250	.947	-.003	-.107		-.041	-.071	-.166	-.296	-.456	459	.300	.947	-.410	-.148		-.067	-.032	.009	.058	.110
420	.500	.000				.877	.826	.648	.742	.897	460	.600	.000	.854	.813		.951	1.004	1.046	1.088	1.127
421	.500	.100	.354	.342		.416	.429	.387	.368	.326	461	.600	.100	.297	.356		.376	.357	.328	.310	.394
422	.500	.200	.198	.202		.313	.335	.290	.259	.162	462	.600	.200	.139	.232		.234	.224	.213	.219	.322
423	.500	.300	.112	.127		.226	.248	.210	.154	.057	463	.600	.300	.030	.168		.163	.174	.173	.203	.298
424	.500	.400	.080	.094		.169	.191	.145	.072	-.032	464	.600	.400	-.056	.115		.139	.151	.159	.198	.286
425	.500	.500	.070	.081		.134	.143	.086	.006	-.111	465	.600	.500	-.124	.064		.111	.123	.138	.193	.276
426	.500	.600	.051	.053		.101	.097	.035	-.041	-.172	466	.600	.600	-.158	.001		.054	.071	.103	.170	.256
427	.500	.700				.078	.064	-.005	-.098	-.233	467	.600	.700	-.200	-.010		.053	.078	.111	.175	.251
428	.500	.800	.076	-.007		.038	.015	-.059	-.152	-.278	468	.600	.800	-.236	-.061		.008	.042	.085	.149	.220
429	.500	.900	.066	-.041		.012	-.017	-.105	-.202	-.323	469	.600	.900	-.299	-.108		-.034	.003	.052	.110	.171
430	.830	.000	1.098	.997		.789	.710	.591	.551	.635	470	.800	.000	.768	.752		.916	.984	1.036	1.082	1.128
431	.830	.200	.170	.121		.157	.176	.155	.116	.106	471	.800	.200	.059	.159		.140	.148	.167	.205	.313
432	.830	.400	.111	.087		.112	.111	.053	-.018	-.068	472	.800	.400	-.087	.071		.124	.136	.149	.197	.286
433	.830	.600	.090	.063		.085	.064	.003	-.058	-.120	473	.800	.600	-.115	-.021		.043	.073	.112	.181	.267
434	.830	.800	.106	.018		.027	-.007	-.071	-.137	-.199	474	.800	.800	-.203	-.082		-.002	.038	.084	.154	.229
			$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open											$\beta \approx 5°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open							
401	.110	.647			.807	.822	.844	.570	.625	.351	441	.130	.647			.832	.828	.818	.782	.783	.817
402	.110	.681			1.045	1.063	1.081	.673	.837	.630	442	.130	.682			1.133	1.125	1.111	1.081	1.055	1.061
403	.110	.698			1.024	1.026	1.011	.684	.798	.598	443	.130	.700			1.018	1.021	1.028	1.037	1.037	1.035
405	.110	.832			.693	.714	.734	.708	.464	-.059	444	.130	.748			.842	.837	.829	.819	.816	.821
406	.110	.949			.538	.555	.579	.551	.336	-.205	445	.130	.832			.752	.737	.714	.689	.679	.684
											446	.130	.949			.576	.560	.542	.523	.514	.518
410	.250	.000			.973	.958	.939	.672	.474	.977											
411	.250	.200			.463	.475	.486	.374	.266	-.007	450	.300	.000			.992	1.004	1.032	1.056	1.082	1.116
412	.250	.400			.421	.429	.430	.363	.178	-.121	451	.300	.200			.458	.442	.419	.378	.358	.423
413	.250	.600			.707	.710	.704	.507	.538	.309	452	.300	.400			.414	.410	.405	.394	.410	.462
415	.250	.668			.992	1.004	1.036	.635	.957	.894	453	.300	.600			.685	.686	.689	.691	.701	.725
416	.250	.685			.962	.958	.952	.635	.857	.745	454	.300	.633			.764	.759	.754	.728	.736	.776
417	.250	.738			.723	.726	.734	.632	.667	.503	455	.300	.668			1.070	1.068	1.061	1.034	1.043	1.073
418	.250	.825			.590	.596	.611	.609	.562	.265	456	.300	.686			.946	.951	.965	.982	.991	.993
419	.250	.947			.440	.445	.457	.466	.438	.051	457	.300	.738			.738	.737	.740	.742	.754	.770
											458	.300	.825			.621	.615	.612	.609	.618	.640
420	.500	.000			.928	.894	.835	.670	.729	.893	459	.300	.947			.456	.451	.452	.454	.465	.487
421	.500	.100			.504	.512	.516	.454	.396	.344											
422	.500	.200			.430	.440	.446	.378	.295	.181	460	.600	.000			.932	.959	1.007	1.046	1.090	1.129
423	.500	.300			.393	.401	.407	.341	.216	.080	461	.600	.100			.489	.482	.459	.407	.394	.468
424	.500	.400			.400	.403	.399	.336	.200	-.005	462	.600	.200			.396	.387	.373	.343	.346	.416
425	.500	.500			.437	.439	.430	.353	.257	-.029	463	.600	.300			.372	.370	.368	.350	.364	.425
426	.500	.600			.423	.419	.414	.317	.310	.170	464	.600	.400			.383	.384	.389	.382	.402	.451
427	.500	.700			.178	.167	.159	.103	.109	.069	465	.600	.500			.423	.426	.434	.435	.456	.495
428	.500	.800			-.061	-.072	-.075	-.108	-.127	-.186	466	.600	.600			.406	.413	.427	.435	.460	.498
429	.500	.900			-.212	-.225	-.223	-.243	-.280	-.367	467	.600	.700			.157	.170	.194	.213	.249	.294
											468	.600	.800			-.078	-.066	-.040	-.023	.009	.054
430	.830	.000			.846	.805	.727	.614	.543	.601	469	.600	.900			-.237	-.223	-.197	-.183	-.154	-.111
431	.830	.200			.327	.330	.334	.270	.193	.144											
432	.830	.400			.306	.300	.297	.168	.047	-.034	470	.800	.000			.893	.925	.983	1.036	1.085	1.130
433	.830	.600			.262	.249	.231	.174	.143	.073	471	.800	.200			.337	.328	.327	.310	.341	.413
434	.830	.800			.070	.050	.031	-.001	-.022	-.073	472	.800	.400			.335	.342	.354	.357	.383	.436
											473	.800	.600			.286	.299	.324	.343	.378	.425
											474	.800	.800			-.003	.015	.050	.080	.127	.182

TABLE V.- PRESSURE COEFFICIENTS MEASURED ON VERTICAL TAIL AND SPEED BRAKES - Continued

(e) M = 1.18

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper tail								Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Lower tail							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			β ≈ -5°; δ_e = 0°; δ_v = 0°; brakes closed											β ≈ -5°; δ_e = 0°; δ_v = 0°; brakes closed							
401	.110	.647				-.068	-.077	-.033	-.044	-.112	441	.130	.647				-.066	-.054	-.043	-.010	.036
402	.110	.681				.031	.032	.023	-.027	-.009	442	.130	.682				.016	.005	.034	.125	.282
403	.110	.698				.035	.024	.050	-.007	-.019	443	.130	.700				.047	.045	.062	.156	.280
404	.110	.748				-.001	-.008	.013	-.066	-.091	444	.130	.748				.010	.035	.059	.139	.249
405	.110	.832				-.047	-.053	-.053	-.139	-.177	445	.130	.832				-.029	-.007	.027	.104	.215
406	.110	.949				-.091	-.102	-.107	-.183	-.261	446	.130	.949				-.074	-.052	-.025	.048	.152
410	.250	.000				1.080	.941	.454	.398	.943	450	.300	.000				.942	1.002	1.041	1.065	1.086
411	.250	.200				-.107	-.208	-.335	-.384	-.399	451	.300	.200				-.092	-.039	.012	.058	.107
412	.250	.400				-.004	.010	-.005	.077	-.066	452	.300	.400				.103	.012	.000	.041	.125
413	.250	.600				.061	.024	.033	.021	.056	453	.300	.600				.068	.075	.096	.147	.218
414	.250	.630				-.081	-.116	-.075	-.104	-.101	454	.300	.633				-.051	-.054	-.042	-.001	.048
415	.250	.668				.034	.038	-.004	-.076	.031	455	.300	.668				.000	.040	.058	.143	.279
416	.250	.685				.044	.035	-.021	-.059	.012	456	.300	.686				.037	.051	.077	.159	.285
417	.250	.738				.025	.004	-.004	-.074	-.050	457	.300	.738				.035	.042	.065	.150	.260
418	.250	.825				-.012	-.030	-.029	-.114	-.117	458	.300	.825				.000	.014	.047	.126	.240
419	.250	.947				-.066	-.088	-.073	-.138	-.195	459	.300	.947				-.041	-.027	.007	.078	.183
420	.500	.000				.997	.915	.818	.818	.833	460	.600	.000				.934	1.005	1.054	1.092	1.125
421	.500	.100				-.301	-.391	-.318	-.428	-.443	461	.600	.100				-.327	-.254	-.219	-.208	-.191
422	.500	.200				-.140	-.229	-.299	-.362	-.407	462	.600	.200				-.135	-.071	-.020	.054	.249
423	.500	.300				-.098	-.081	-.072	-.035	-.384	463	.600	.300				.016	.009	.058	.112	.179
424	.500	.400				.088	.129	.093	.148	.016	464	.600	.400				.156	.004	-.004	.040	.126
425	.500	.500				.095	.115	.104	.131	.164	465	.600	.500				.131	.103	.103	.071	.215
426	.500	.600				.076	.059	.045	.046	.087	466	.600	.600				.076	.088	.107	.153	.215
427	.500	.700									467	.600	.700				.029	.041	.056	.129	.241
428	.500	.800				.010	.001	-.028	-.067	-.063	468	.600	.800				.015	.026	.044	.126	
429	.500	.900				-.016	-.025	-.051	-.091	-.096	469	.600	.900				-.012	.003	.032	.103	.217
430	.830	.000				.969	.888	.810	.783	.774	470	.800	.000				.957	1.028	1.083	1.128	1.170
431	.830	.200				-.169	-.267	-.325	-.409	-.390	471	.800	.200				-.052	.045	.117	.186	.264
432	.830	.400				.092	.155	.178	.160	.078	472	.800	.400				.145	-.013	-.001	.050	.130
433	.830	.600				.065	.068	.059	.052	.071	473	.800	.600				.079	.087	.112	.156	.228
434	.830	.800				.017	.023	.010	-.026	-.019	474	.800	.800				.015	.026	.050	.128	.230
			β ≈ -5°; δ_e = 0°; δ_v = 0°; brakes open											β ≈ -5°; δ_e = 0°; δ_v = 0°; brakes open							
401	.110	.647	-.142	-.114	.527	.511	.386	.676	.721	.447	441	.130	.647								
402	.110	.681	.018	-.031	.697	.811	.513	.838	.941	.566	442	.130	.682	-.017	.093	.231	.487	.659	.659	.700	.769
403	.110	.698	.052	-.019	.865	.847	.603	.859	.870	.639	443	.130	.700	-.015	.077	.314	.898	.999	.957	.920	.910
404	.110	.748	.048	-.054	.861	.729	.740	.898	.776	.672	444	.130	.748	-.070	.023	.369	.770	.878	.904	.899	.884
405	.110	.832	.005	-.105	.675	.659	.655	.795	.653	.513	445	.130	.832	-.138	.001	.491	.694	.715	.712	.718	.733
406	.110	.949	-.079	-.167	.559	.578	.560	.618	.507	.359	446	.130	.949	-.220	.011	.602	.608	.582	.563	.561	.574
410	.250	.000	1.231	1.184	1.126	1.082	.855	.463	.386	.943	450	.300	.000	.734	.601	.891	.940	1.008	1.043	1.064	1.083
411	.250	.200	.098	-.016	-.073	-.104	-.180	-.343	-.394	-.396	451	.300	.200	-.416	-.310	.068	-.031	-.031	.015	.056	.111
412	.250	.400	.045	-.108	.068	.185	.198	.116	.132	.024	452	.300	.400	.101	.099	.200	.263	.278	.273	.369	.456
413	.250	.600	-.041	-.011	.532	.541	.380	.583	.517	.402	453	.300	.600	.046	.022	.303	.545	.623	.625	.678	.727
414	.250	.630	-.157	-.133	.487	.537	.377	.711	.640	.431	454	.300	.633	-.100	-.119	.422	.571	.595	.590	.682	.740
415	.250	.668	-.057	-.011	.761	.783	.408	.954	.807	.563	455	.300	.668	-.010	-.032	.871	.944	.825	.789	.802	.891
416	.250	.685	-.040	-.003	.967	.899	.447	.881	.701	.631	456	.300	.686	-.008	.011	.811	.979	.950	.887	.827	.901
417	.250	.738	.052	-.029	.845	.761	.512	.793	.621	.697	457	.300	.738	-.052	-.026	.663	.787	.858	.876	.822	.829
418	.250	.825	.048	-.059	.637	.631	.521	.738	.600	.565	458	.300	.825	-.111	-.034	.654	.657	.661	.672	.695	.701
419	.250	.947	-.016	-.110	.514	.537	.452	.580	.507	.454	459	.300	.947	-.188	-.044	.610	.545	.527	.519	.534	.563
420	.500	.000	1.198	1.114	1.034	.994	.904	.787	.828	.836	460	.600	.000	.761	.741	.878	.936	1.012	1.057	1.090	1.120
421	.500	.100	-.173	-.254	-.260	-.299	-.399	-.347	-.421	-.442	461	.600	.100	-.568	-.495	-.361	-.318	-.240	-.210	-.218	-.203
422	.500	.200	.081	-.034	-.091	-.141	-.225	-.294	-.368	-.406	462	.600	.200	-.422	-.317	.018	-.105	-.063	-.015	.057	.303
423	.500	.300	.154	-.075	-.093	-.047	.091	.001	.028	-.133	463	.600	.300	-.074	.133	.248	.262	.019	.062	.125	.365
424	.500	.400	.091	-.021	.187	.275	.287	.218	.228	.094	464	.600	.400	.169	.199	.218	.278	.301	.298	.371	.438
425	.500	.500	.027	-.044	.371	.340	.330	.344	.323	.276	465	.600	.500	.148	.144	.225	.338	.413	.437	.468	.516
426	.500	.600	-.015	-.005	.400	.381	.312	.352	.333	.301	466	.600	.600	.343	1.390	.292	.397	.445	.463	.496	.540
427	.500	.700	-.061	-.026							467	.600	.700	-.012	.039	.167	.249	.286	.307	.343	.388
428	.500	.800	-.015	-.035	.058	.034	.005	.036	-.038	.001	468	.600	.800	-.074	.017	-.002	.041	.078	.101	.136	.183
429	.500	.900	.041	-.055	-.088	-.095	-.111	-.099	-.164	-.127	469	.600	.900			-.103	-.100	-.073	-.052	-.023	.026
430	.830	.000	1.201	1.100	1.011	.964	.880	.795	.776	.766	470	.800	.000	.736	.779	.900	.957	1.034	1.085	1.127	1.168
431	.830	.200	.194	-.084	-.114	-.170	.274	-.323	-.400	-.384	471	.800	.200	-.475	-.268	.205	-.029	.055	.124	.190	.335
432	.830	.400	.110	-.005	.155	.263	.264	.266	.201	.082	472	.800	.400	.124	.177	.220	.281	.294	.282	.352	.416
433	.830	.600	.037	-.057	.311	.296	.265	.282	.265	.234	473	.800	.600	.057	.084	.255	.338	.380	.396	.430	.472
434	.830	.800	-.048	-.010	.191	.177	.152	.127	.094	.132	474	.800	.800			.103	.140	.178	.200	.240	.284

TABLE V.- PRESSURE COEFFICIENTS MEASURED ON VERTICAL TAIL AND SPEED BRAKES - Continued

(e) M = 1.18 - Continued

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper tail α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°	Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Lower tail α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed											$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes closed							
401	.110	.647	-.011	-.074		-.013	-.003	-.031	-.098	-.151	441	.130	.647	-.144	-.035		-.017	-.022	-.008	.027	.080
402	.110	.681	.119	-.002		.053	.060	.034	-.085	-.147	442	.130	.682	-.155	-.012		.010	.015	.037	.105	.279
403	.110	.698	.138	.015		.087	.086	.066	-.069	-.142	443	.130	.700	-.141	.021		.072	.047	.061	.141	.307
404	.110	.748	.097	-.011		.038	.043	.038	-.097	-.177	444	.130	.748	-.156	.087		.048	.054	.068	.144	.266
405	.110	.832	.042	-.063		-.014	-.012	-.019	-.133	-.242	445	.130	.832	-.228	-.002		.006	.014	.034	.112	.234
406	.110	.949	-.044	-.132		-.095	-.085	-.109	-.210	-.304	446	.130	.949	-.280	-.076		-.048	-.036	.015	.065	.179
410	.250	.000	.008	1.144		1.067	1.011	.988	.920	.928	450	.300	.000				.986	1.054	1.109	1.148	1.189
411	.250	.200	.257	.164		.166	.250	.199	.051	-.350	451	.300	.200	-.318	.209		.163	.150	.179	.207	.272
412	.250	.400	.082	.080		.142	.171	.183	.216	.220	452	.300	.400	.207	.175		.162	.149	.183	.222	.288
413	.250	.600	.121	.028		.101	.112	.078	.016	-.029	453	.300	.600	-.012	.084		.098	.092	.115	.172	.253
414	.250	.630	-.023	-.089		-.032	-.019	-.036	-.099	-.140	454	.300	.633	-.115	-.020		-.014	-.021	-.005	.034	.091
415	.250	.668	.145	.005		.065	.072	.059	-.049	-.094	455	.300	.668	-.117	.013		.031	.032	.055	.126	.277
416	.250	.685	.146	.027		.086	.091	.090	-.031	-.090	456	.300	.686	-.088	.061		.065	.073	.092	.155	.298
417	.250	.738	.126	.014		.071	.082	.060	-.058	-.137	457	.300	.738	-.129	.069		.067	.062	.073	.155	.280
418	.250	.825	.087	-.016		.027	.027	.038	-.078	-.181	458	.300	.825	-.173	.020		.022	.035	.054	.133	.259
419	.250	.947	.024	-.067		-.021	-.009	-.020	-.116	-.240	459	.300	.947	-.157	-.030		-.024	-.011	.039	.095	.213
420	.500	.000	1.197	1.102		.906	.898	.839	.815	.819	460	.600	.000	.806	.823		.971	1.049	1.113	1.164	1.213
421	.500	.100	.335	.231		.090	-.015	-.121	-.244	-.323	461	.600	.100	-.364	-.161		.133	.192	.244	.278	.333
422	.500	.200	.229	.128		.226	.263	.295	.250	-.048	462	.600	.200	-.247	.247		.158	.088	.129	.191	.259
423	.500	.300	.172	.099		.150	.186	.233	.283	.303	463	.600	.300	.275	.214		.152	.136	.136	.128	.201
424	.500	.400	.109	.084		.123	.150	.156	.181	.200	464	.600	.400	.195	.168		.144	.130	.170	.216	.275
425	.500	.500	.058	.068		.116	.142	.129	.107	.104	465	.600	.500	.116	.134		.132	.121	.153	.203	.280
426	.500	.600	.102	.041		.110	.118	.104	.039	.019	466	.600	.600				.102	.100	.120	.173	.257
427	.500	.700	.119	.008		.078	.084	.092	-.006	-.063	467	.600	.700	-.063	.082		.064	.071	.085	.152	.273
428	.500	.800	.114	.010		.053	.054	.065	-.029	-.106	468	.600	.800	-.110	.052		.044	.053	.069	.149	.263
429	.500	.900	.085	-.010		.020	.025	.024	-.056	-.131	469	.600	.900	-.148	.005		.010	.025	.054	.127	.245
430	.830	.000	1.205	1.101		.950	.872	.805	.756	.740	470	.800	.000	.792	.831		.983	1.057	1.128	1.175	1.224
431	.830	.200	.242	.108							471	.800	.200				.150	.088	.136	.192	.264
432	.830	.400	.144	.090		.107	.144	.163	.147	.156	472	.800	.400	.187	.165		.141	.119	.160	.210	.268
433	.830	.600	.078	.060		.112	.112	.103	.062	.047	473	.800	.600	.043	.085		.101	.105	.127	.182	.266
434	.830	.800	.134	.023		.060	.063	.064	.012	-.030	474	.800	.800	-.069	.037		.041	.054	.077	.153	.267
			$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open											$\beta \approx 0°$; $\delta_e = 0°$; $\delta_v = 0°$; brakes open							
401	.110	.647			-.003	.007	.015	.002	-.069	-.145	441	.130	.647			.009	.001	-.011	-.015	.016	.062
402	.110	.681			.068	.080	.087	.086	-.034	-.147	442	.130	.682			.041	.035	.031	.029	.083	.176
403	.110	.698			.086	.099	.109	.103	-.025	-.141	443	.130	.700			.091	.075	.054	.044	.097	.222
404	.110	.748			.048	.059	.080	.078	-.056	-.179	444	.130	.748			.085	.071	.059	.046	.100	.219
405	.110	.832			-.021	-.002	.009	-.014	-.122	-.252	445	.130	.832			.035	.025	.016	.013	.067	.178
406	.110	.949			-.094	-.069	-.069	-.109	-.221	-.336	446	.130	.949			-.033	-.039	-.042	-.005	.020	.137
410	.250	.000			1.106	1.069	1.005	.978	.907	.919	450	.300	.000			.947	.993	1.061	1.112	1.150	1.188
411	.250	.200			.323	.335	.347	.340	.400	.322	451	.300	.200			.309	.303	.290	.283	.284	.324
412	.250	.400			.210	.227	.245	.230	.233	.148	452	.300	.400			.216	.206	.182	.185	.219	.279
413	.250	.600			.110	.125	.138	.132	.033	-.092	453	.300	.600			.134	.122	.106	.102	.145	.213
414	.250	.630			-.007	.003	.006	.008	-.070	-.187	454	.300	.633			.016	.011	.005	.008	.047	.096
415	.250	.668			-.002	.013	.028	.019	-.064	-.162	455	.300	.668			.014	.010	-.003	-.017	.012	.070
416	.250	.685			.076	.094	.110	.111	-.036	-.212	456	.300	.686			.091	.082	.066	.048	.105	.184
417	.250	.738			.058	.079	.116	.101	-.049	-.212	457	.300	.738			.109	.077	.045	.028	.086	.204
418	.250	.825			.005	.027	.046	.009	-.096	-.277	458	.300	.825			.045	.038	.024	.015	.063	.175
419	.250	.947			-.051	-.030	-.028	-.058	-.173	-.352	459	.300	.947			-.019	-.025	-.027	.007	.028	.138
420	.500	.000			1.064	1.022	.937	.841	.820	.818	460	.600	.000			1.001	1.050	1.108	1.153	1.193	1.232
421	.500	.100			.429	.431	.426	.404	.219	-.061	461	.600	.100			.392	.398	.406	.420	.447	.489
422	.500	.200			.332	.349	.360	.359	.398	.383	462	.600	.200			.288	.275	.261	.262	.271	.324
423	.500	.300			.254	.272	.291	.292	.321	.294	463	.600	.300			.235	.222	.195	.193	.195	.258
424	.500	.400			.206	.224	.245	.239	.240	.208	464	.600	.400			.206	.195	.176	.188	.227	.285
425	.500	.500			.182	.195	.209	.202	.171	.128	465	.600	.500			.199	.188	.170	.180	.223	.285
426	.500	.600			.156	.167	.180	.201	.124	.057	466	.600	.600			.171	.165	.147	.143	.188	.264
427	.500	.700			.115	.127	.144	.160	.081	-.002	467	.600	.700			.132	.122	.115	.111	.158	.242
428	.500	.800			.096	.120	.136	.134	.051	-.037	468	.600	.800			.117	.104	.092	.083	.144	.258
429	.500	.900			.071	.085	.093	.089	.024	-.072	469	.600	.900			.075	.068	.066	.092	.132	.243
430	.830	.000			.991	.952	.877	.819	.783	.743	470	.800	.000			.981	1.024	1.079	1.128	1.172	1.215
431	.830	.200									471	.800	.200			.222	.212	.206	.220	.247	.312
432	.830	.400			.140	.142	.147	.144	.135	.129	472	.800	.400			.184	.170	.162	.187	.233	.299
433	.830	.600			.131	.139	.144	.167	.114	.058	473	.800	.600			.152	.151	.138	.146	.196	.284
434	.830	.800			.103	.110	.122	.115	.070	.027	474	.800	.800			.096	.086	.091	.099	.164	.277

TABLE V.- PRESSURE COEFFICIENTS MEASURED ON VERTICAL TAIL AND SPEED BRAKES - Continued

(e) M = 1.18 - Continued

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper tail								Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Lower tail							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			β ≈ 0°; δ_e = 0°; δ_v = -7.5°; brakes closed											β ≈ 0°; δ_e = 0°; δ_v = -7.5°; brakes closed							
401	.110	.647			-.021	-.018	-.028	-.072	-.120	-.179	441	.130	.647			-.040	-.034	-.035	-.021	.012	.056
402	.110	.681			.052	.043	.027	-.021	-.108	-.166	442	.130	.682			-.008	.000	-.004	.029	.128	.238
403	.110	.698			.083	.084	.059	.002	-.089	-.166	443	.130	.700			.054	.065	.039	.054	.156	.240
404	.110	.748			-.001	-.007	-.015	-.040	-.146	-.235	444	.130	.748			-.009	.001	.012	.028	.100	.183
405	.110	.832			-.074	-.076	-.091	-.125	-.217	-.303	445	.130	.832			-.061	-.055	-.041	-.026	.061	.158
406	.110	.949			-.126	-.129	-.147	-.168	-.272	-.359	446	.130	.949			-.102	-.096	-.077	-.016	.029	.145
410	.250	.000			1.108	1.072	1.010	.970	.892	.905	450	.300	.000			.942	.989	1.062	1.114	1.151	1.188
411	.250	.200			-.046	-.056	-.074	-.301	-.385	-.463	451	.300	.200			-.065	-.067	-.035	.008	.046	.087
412	.250	.400			.002	.030	.047	.069	.128	.122	452	.300	.400			.101	.069	.052	.071	.061	.267
413	.250	.600			.086	.087	.075	.031	-.019	-.032	453	.300	.600			.062	.073	.077	.099	.190	.265
414	.250	.630			-.039	-.041	-.046	-.074	-.124	-.155	454	.300	.633			-.036	-.028	-.032	-.030	.067	.108
415	.250	.668			.033	.028	.015	-.018	-.094	-.118	455	.300	.668			-.009	.008	.005	.051	.105	.219
416	.250	.685			.045	.040	.026	-.003	-.080	-.125	456	.300	.686			-.007	.011	.024	.040	.135	.215
417	.250	.738			-.013	-.022	-.028	-.058	-.153	-.201	457	.300	.738			-.031	-.020	-.007	.002	.094	.186
418	.250	.825			-.055	-.061	-.081	-.088	-.182	-.241	458	.300	.825			-.066	-.060	-.031	-.015	.085	.188
419	.250	.947			-.063	-.058	-.063	-.079	-.180	-.278	459	.300	.947			-.086	-.078	-.038	.002	.066	.184
420	.500	.000			1.052	1.007	.914	.832	.825	.819	460	.600	.000			.914	.958	1.016	1.052	1.081	1.112
421	.500	.100			-.066	-.070	-.182	-.298	-.416	-.525	461	.600	.100			-.096	-.071	-.037	.002	.022	.049
422	.500	.200			-.091	-.087	.011	-.137	-.349	-.478	462	.600	.200			-.021	-.112	-.100	-.065	.010	.153
423	.500	.300			-.043	.007	.053	.118	.179	.132	463	.600	.300			.154	.118	.045	.025	.071	.159
424	.500	.400			.070	.102	.116	.116	.138	.125	464	.600	.400			.128	.115	.085	.097	.086	.245
425	.500	.500			.081	.089	.091	.072	.050	.053	465	.600	.500			.095	.108	.097	.134	.193	.274
426	.500	.600			.073	.079	.063	.018	-.026	-.031	466	.600	.600			.046	.066	.075	.097	.159	.227
427	.500	.700			-.060	-.066	-.082	-.110	-.164	-.185	467	.600	.700			-.060	-.051	-.052	-.034	.040	.133
428	.500	.800			-.039	-.044	-.057	-.083	-.154	-.214	468	.600	.800			-.053	-.053	-.047	-.036	.049	.143
429	.500	.900			-.055	-.062	-.083	-.088	-.161	-.226	469	.600	.900			-.070	-.066	-.055	-.015	.054	.156
430	.830	.000			1.017	.979	.905	.832	.749	.728	470	.800	.000			.920	.967	1.029	1.073	1.112	1.152
431	.830	.200									471	.800	.200			.155	.008	.028	.085	.142	.209
432	.830	.400			.067	.086	.116	.130	.128	.151	472	.800	.400			.121	.113	.086	.079	.043	.210
433	.830	.600			.071	.079	.070	.033	.003	-.006	473	.800	.600			.055	.072	.083	.099	.156	.225
434	.830	.800			-.013	-.017	-.026	-.040	-.091	-.129	474	.800	.800			-.041	-.038	-.027	-.019	.058	.131
			β ≈ 0°; δ_e = 0°; δ_v = 7.5°; brakes closed											β ≈ 0°; δ_e = 0°; δ_v = 7.5°; brakes closed							
401	.110	.647			.703	.720	.740	.729	.678	.589	441	.130	.647			.749	.758	.748	.742	.760	.804
402	.110	.681			.948	.968	.982	.950	.885	.761	442	.130	.682			1.098	1.097	1.063	1.025	.974	1.022
403	.110	.698			1.073	1.071	1.048	.998	.946	.793	443	.130	.700			1.034	1.067	1.128	1.120	1.082	1.101
404	.110	.748			.883	.869	.835	.781	.784	.617	444	.130	.748			.859	.877	.904	.914	.926	.937
405	.110	.832			.733	.756	.712	.634	.640	.425	445	.130	.832			.808	.801	.767	.751	.750	.765
406	.110	.949			.612	.640	.624	.556	.523	.261	446	.130	.949			.692	.665	.628	.608	.604	.613
410	.250	.000			1.117	1.076	1.014	.983	.932	.925	450	.300	.000			.948	.994	1.059	1.104	1.142	1.180
411	.250	.200			.153	.252	.277	.279	.115	-.180	451	.300	.200			.266	.240	.162	.174	.200	.293
412	.250	.400			.260	.290	.317	.308	.215	.210	452	.300	.400			.333	.333	.318	.341	.409	.481
413	.250	.600			.692	.699	.706	.689	.643	.533	453	.300	.600			.678	.691	.705	.712	.734	.777
414	.250	.630			.646	.689	.721	.731	.665	.596	454	.300	.633			.749	.735	.688	.680	.702	.772
415	.250	.668			.927	.966	.997	1.015	.914	.839	455	.300	.668			1.092	1.066	1.015	.920	1.001	.992
416	.250	.685			1.068	1.057	1.046	1.016	.949	.841	456	.300	.686			1.065	1.076	1.101	1.059	1.093	1.060
417	.250	.738			.830	.825	.816	.806	.762	.680	457	.300	.738			.831	.831	.845	.862	.873	.894
418	.250	.825			.668	.682	.691	.684	.647	.562	458	.300	.825			.722	.709	.692	.691	.702	.733
419	.250	.947			.541	.557	.576	.554	.561	.445	459	.300	.947			.585	.567	.551	.547	.559	.584
420	.500	.000			1.013	.968	.898	.835	.809	.812	460	.600	.000			.937	.988	1.061	1.114	1.160	1.204
421	.500	.100			.137	.111	-.007	-.122	-.240	-.322	461	.600	.100			.200	.149	.196	.237	.269	.324
422	.500	.200			.179	.240	.273	.312	.281	.113	462	.600	.200			.218	.184	.101	.124	.183	.333
423	.500	.300			.145	.185	.235	.256	.275	.298	463	.600	.300			.274	.253	.177	.185	.304	.409
424	.500	.400			.308	.326	.348	.345	.203	.189	464	.600	.400			.340	.345	.335	.353	.411	.479
425	.500	.500			.438	.439	.444	.434	.372	.217	465	.600	.500			.432	.440	.455	.469	.504	.553
426	.500	.600			.467	.472	.472	.463	.431	.354	466	.600	.600			.471	.478	.487	.497	.530	.572
427	.500	.700			.278	.274	.263	.255	.241	.207	467	.600	.700			.276	.281	.297	.317	.355	.405
428	.500	.800			.061	.056	.041	.032	.030	.000	468	.600	.800			.059	.060	.074	.097	.132	.186
429	.500	.900			-.079	-.083	-.093	-.106	-.100	-.142	469	.600	.900			-.085	-.087	-.076	-.055	-.022	.030
430	.830	.000			1.005	.960	.872	.800	.755	.737	470	.800	.000			.942	.995	1.067	1.121	1.169	1.214
431	.830	.200									471	.800	.200			.222	.183	.107	.131	.185	.354
432	.830	.400			.301	.327	.337	.336	.271	.171	472	.800	.400			.340	.344	.339	.350	.407	.470
433	.830	.600			.353	.349	.343	.329	.312	.259	473	.800	.600			.387	.394	.409	.426	.461	.509
434	.830	.800			.201	.192	.179	.165	.163	.128	474	.800	.800			.148	.153	.177	.202	.245	.302

TABLE V.- PRESSURE COEFFICIENTS MEASURED ON VERTICAL TAIL AND SPEED BRAKES - Concluded

(e) M = 1.18 - Concluded

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper tail								Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Lower tail							
			α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°				α = -20°	α = -10°	α = -3°	α = 0°	α = 5°	α = 10°	α = 15°	α = 20°
			β ≈ 5°; δ_e = 0°; δ_v = 0°; brakes closed											β ≈ 5°; δ_e = 0°; δ_v = 0°; brakes closed							
401	.110	.647	.033	-.014		.057	.075	.048	-.066	-.244	441	.130	.647	-.264	-.023		.023	.014	.015	.061	.123
402	.110	.681	.131	.047		.119	.151	.129	-.037	-.210	442	.130	.682	-.260	.101		.031	.029	.047	.123	.358
403	.110	.698	.162	.072		.155	.160	.118	-.021	-.216	443	.130	.700	-.280	.101		.068	.064	.082	.175	.357
404	.110	.748	.118	.042							444	.130	.748	-.276	.062		.077	.075	.104	.186	.314
405	.110	.832	.061	.005		.036	.037	.008	-.129	-.307	445	.130	.832	-.328	.012		.029	.040	.090	.180	.282
406	.110	.949	-.026	-.059		-.003	-.020	-.066	-.208	-.401	446	.130	.949	-.378	-.063		-.023	-.002	.066	.163	.219
410	.250	.000	1.192	1.138		1.034	.875	.447	.381	.931	450	.300	.000	.843	.692		1.046	1.105	1.142	1.177	1.210
411	.250	.200	.390	.349		.414	.387	.212	.267	.149	451	.300	.200	.231	.297		.385	.363	.347	.362	.410
412	.250	.400	.216	.183		.282	.303	.255	.224	-.048	452	.300	.400	.014	.226		.239	.223	.217	.260	.360
413	.250	.600	.171	.092		.169	.182	.138	.057	-.182	453	.300	.600	-.168	.128		.123	.117	.128	.198	.300
414	.250	.630	.026	-.032							454	.300	.633	-.247	.005		.013	.008	.016	.066	.136
415	.250	.668	.160	.050		.102	.113	.136	-.010	-.211	455	.300	.668	-.240	.054		.042	.043	.062	.140	.358
416	.250	.685	.169	.081		.135	.153	.124	.011	-.216	456	.300	.686	-.222	.114		.077	.084	.106	.181	.354
417	.250	.738	.150	.069		.117	.112	.083	-.022	-.244	457	.300	.738	-.252	.092		.074	.077	.107	.195	.328
418	.250	.825	.108	.043		.069	.067	.030	-.070	-.279	458	.300	.825	-.290	.045		.042	.058	.106	.199	.311
419	.250	.947	.048	.006		.024	.011	-.043	-.144	-.341	459	.300	.947	-.325	-.019		.002	.025	.092	.189	.252
420	.500	.000				.992	.909	.773	.839	.838	460	.600	.000	.840	.852		1.033	1.093	1.141	1.187	1.227
421	.500	.100	.495	.439		.455	.427	.357	.398	.392	461	.600	.100	.386	.365		.432	.427	.419	.434	.486
422	.500	.200	.343	.305		.380	.376	.311	.346	.244	462	.600	.200	.246	.278		.304	.294	.285	.308	.387
423	.500	.300	.249	.210		.296	.304	.264	.271	.137	463	.600	.300	.139	.210		.238	.225	.224	.262	.363
424	.500	.400	.204	.159		.233	.249	.233	.191	.055	464	.600	.400	.052	.168		.180	.177	.187	.248	.350
425	.500	.500	.203	.127		.187	.200	.191	.118	-.014	465	.600	.500	-.019	.143		.145	.147	.167	.231	.337
426	.500	.600	.193	.103		.149	.153	.134	.061		466	.600	.600	-.091	.116		.107	.110	.131	.199	.310
427	.500	.700				.113	.117	.100	.002	-.143	467	.600	.700	-.148	.103		.078	.087	.105	.184	.333
428	.500	.800	.141	.061		.077	.076	.052	-.032	-.179	468	.600	.800	-.182	.066		.058	.073	.117	.201	.320
429	.500	.900	.111	.059		.053	.048	.017	-.058	-.207	469	.600	.900	-.211	.013		.024	.048	.119	.203	.296
430	.830	.000	1.198	1.100		.930	.844	.756	.737	.743	470	.800	.000	.832	.851		1.010	1.078	1.130	1.178	1.222
431	.830	.200	.297	.211		.236	.230	.199	.219	.202	471	.800	.200	.189	.179		.217	.212	.231	.275	.372
432	.830	.400	.237	.129		.134	.132	.131	.081	.057	472	.800	.400	.037	.114		.132	.145	.174	.244	.347
433	.830	.600	.224	.109		.092	.081	.073	.008	-.051	473	.800	.600	-.068	.101		.081	.096	.126	.203	.323
434	.830	.800	.182	.075		.068	.059	.037	-.016	-.090	474	.800	.800	-.120	.043		.042	.063	.115	.204	.328
			β ≈ 5°; δ_e = 0°; δ_v = 0°; brakes open											β ≈ 5°; δ_e = 0°; δ_v = 0°; brakes open							
401	.110	.647			.835	.857	.878	.528	.709	.334	441	.130	.647			.899	.878	.859	.825	.869	.909
402	.110	.681			1.093	1.122	1.095	.593	.901	.571	442	.130	.682			1.225	1.209	1.178	1.138	1.132	1.144
403	.110	.698			1.138	1.141	1.015	.626	.834	.670	443	.130	.700			1.133	1.145	1.150	1.157	1.150	1.148
404	.110	.748									444	.130	.748			.945	.941	.932	.929	.931	.941
405	.110	.832			.784	.808	.832	.817	.543	-.081	445	.130	.832			.862	.841	.815	.796	.795	.806
406	.110	.949			.654	.672	.710	.696	.418	-.351	446	.130	.949			.710	.690	.668	.650	.649	.657
410	.250	.000			1.080	1.037	.888	.461	.435	.946	450	.300	.000			.997	1.046	1.104	1.143	1.177	1.210
411	.250	.200			.423	.441	.418	.233	.298	.157	451	.300	.200			.415	.409	.380	.365	.390	.478
412	.250	.400			.399	.415	.430	.380	.286	-.009	452	.300	.400			.396	.383	.367	.386	.454	.540
413	.250	.600			.776	.783	.754	.502	.605	.340	453	.300	.600			.767	.768	.765	.774	.801	.836
414	.250	.630									454	.300	.633			.831	.810	.787	.761	.805	.867
415	.250	.668			1.027	1.049	1.136	.596	1.033	.843	455	.300	.668			1.161	1.146	1.127	1.077	1.120	1.146
416	.250	.685			1.083	1.079	1.048	.622	.905	.737	456	.300	.686			1.073	1.084	1.100	1.114	1.115	1.113
417	.250	.738			.829	.826	.840	.684	.726	.505	457	.300	.738			.848	.845	.845	.856	.867	.889
418	.250	.825			.686	.693	.736	.745	.646	.168	458	.300	.825			.741	.725	.717	.718	.733	.760
419	.250	.947			.561	.564	.595	.616	.538	-.163	459	.300	.947			.588	.582	.578	.580	.595	.620
420	.500	.000			1.046	.997	.916	.753	.849	.881	460	.600	.000			.980	1.024	1.090	1.140	1.184	1.226
421	.500	.100			.462	.474	.452	.367	.423	.405	461	.600	.100			.446	.448	.434	.427	.449	.526
422	.500	.200			.391	.408	.413	.344	.369	.265	462	.600	.200			.345	.332	.311	.303	.352	.465
423	.500	.300			.347	.353	.376	.341	.304	.170	463	.600	.300			.320	.303	.279	.295	.382	.491
424	.500	.400			.387	.396	.393	.358	.271	.088	464	.600	.400			.373	.366	.360	.389	.453	.536
425	.500	.500			.475	.477	.462	.388	.334	.036	465	.600	.500			.475	.472	.473	.493	.539	.598
426	.500	.600			.495	.485	.484	.362	.398	.205	466	.600	.600			.493	.494	.503	.524	.563	.612
427	.500	.700			.269	.258	.248	.188	.217	.168	467	.600	.700			.258	.266	.288	.320	.366	.423
428	.500	.800			.041	.028	.033	.029	.007	-.053	468	.600	.800			.035	.040	.061	.094	.139	.197
429	.500	.900			-.090	-.103	-.094	-.083	-.129	-.219	469	.600	.900			-.103	-.100	-.084	-.054	-.008	.048
430	.830	.000			.993	.932	.842	.741	.710	.718	470	.800	.000			.965	1.008	1.077	1.131	1.177	1.220
431	.830	.200			.265	.268	.276	.249	.237	.230	471	.800	.200			.259	.247	.231	.253	.328	.460
432	.830	.400			.288	.264	.286	.255	.212	.146	472	.800	.400			.338	.322	.329	.370	.438	.524
433	.830	.600			.313	.302	.287	.233	.219	.115	473	.800	.600			.368	.377	.397	.431	.481	.539
434	.830	.800			.169	.144	.135	.131	.101	.058	474	.800	.800			.103	.117	.146	.192	.248	.316

TABLE VI.- PRESSURE COEFFICIENT MEASURED AT THE BASE OF THE UPPER VERTICAL TAIL

(a) M = 0.60

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper tail							
			$\alpha = -20^\circ$	$\alpha = -10^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 15^\circ$	$\alpha = 20^\circ$
			$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed							
600	.150	1.000				-.323	-.333	-.317	-.360	-.414
			$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open							
600	.150	1.000	-.257	-.309	-.604	-.608	-.600	-.537	-.576	-.600
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed							
600	.150	1.000	-.239	-.284		-.271	-.291	-.313	-.320	-.390
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open							
600	.150	1.000			-.298	-.300	-.302	-.318	-.365	-.448
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = -7.5^\circ$; brakes closed							
600	.150	1.000			-.288	-.287	-.287	-.308	-.359	-.436
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 7.5^\circ$; brakes closed							
600	.150	1.000			-.560	-.564	-.568	-.523	-.567	-.681
			$\beta \approx 5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed							
600	.150	1.000	-.262	-.318		-.345	-.335	-.335	-.392	-.445
			$\beta \approx 5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open							
600	.150	1.000			-.625	-.621	-.612	-.536	-.584	-.610

TABLE VI.- PRESSURE COEFFICIENT MEASURED AT THE BASE OF THE UPPER VERTICAL TAIL - Continued

(b) M = 0.90

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper tail							
			$\alpha = -20^\circ$	$\alpha = -10^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 15^\circ$	$\alpha = 20^\circ$
			$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed							
600	.150	1.000				-.365	-.374	-.355	-.409	-.500
			$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open							
600	.150	1.000	-.331	-.357	-.666	-.659	-.659	-.641	-.690	-.795
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed							
600	.150	1.000	-.305	-.297		-.293	-.304	-.337	-.372	
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open							
600	.150	1.000			-.385	-.383	-.388	-.409	-.454	-.568
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = -7.5^\circ$; brakes closed							
600	.150	1.000			-.355	-.359	-.362	-.375	-.406	-.502
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 7.5^\circ$; brakes closed							
600	.150	1.000			-.669	-.654	-.670	-.676	-.715	-.791
			$\beta \approx 5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed							
600	.150	1.000	-.345	-.356		-.375	-.383	-.371	-.417	-.543
			$\beta \approx 5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open							
600	.150	1.000			-.665	-.655	-.651	-.635	-.689	-.815

TABLE VI.- PRESSURE COEFFICIENT MEASURED AT THE BASE OF THE UPPER VERTICAL TAIL - Continued

(c) M = 0.95

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper tail							
			$\alpha = -20^\circ$	$\alpha = -10^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 15^\circ$	$\alpha = 20^\circ$
			$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed							
600	.150	1.000				-.401	-.404	-.378	-.386	-.487
			$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open							
600	.150	1.000	-.369	-.388	-.744	-.745	-.758	-.704	-.726	-.814
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed							
600	.150	1.000	-.330	-.324		-.330	-.336	-.349	-.377	-.459
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open							
600	.150	1.000			-.450	-.449	-.442	-.445	-.471	-.558
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = -7.5^\circ$; brakes closed							
600	.150	1.000			-.420	-.414	-.399	-.400	-.427	-.509
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 7.5^\circ$; brakes closed							
600	.150	1.000			-.756	-.746	-.757	-.769	-.746	-.767
			$\beta \approx 5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed							
600	.150	1.000	-.378	-.393		-.426	-.422	-.389	-.413	-.531
			$\beta \approx 5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open							
600	.150	1.000			-.772	-.774	-.780	-.711	-.743	-.828

TABLE VI.- PRESSURE COEFFICIENT MEASURED AT THE BASE OF THE UPPER VERTICAL TAIL - Continued

(d) M = 1.03

Pressure coefficients C_p on -

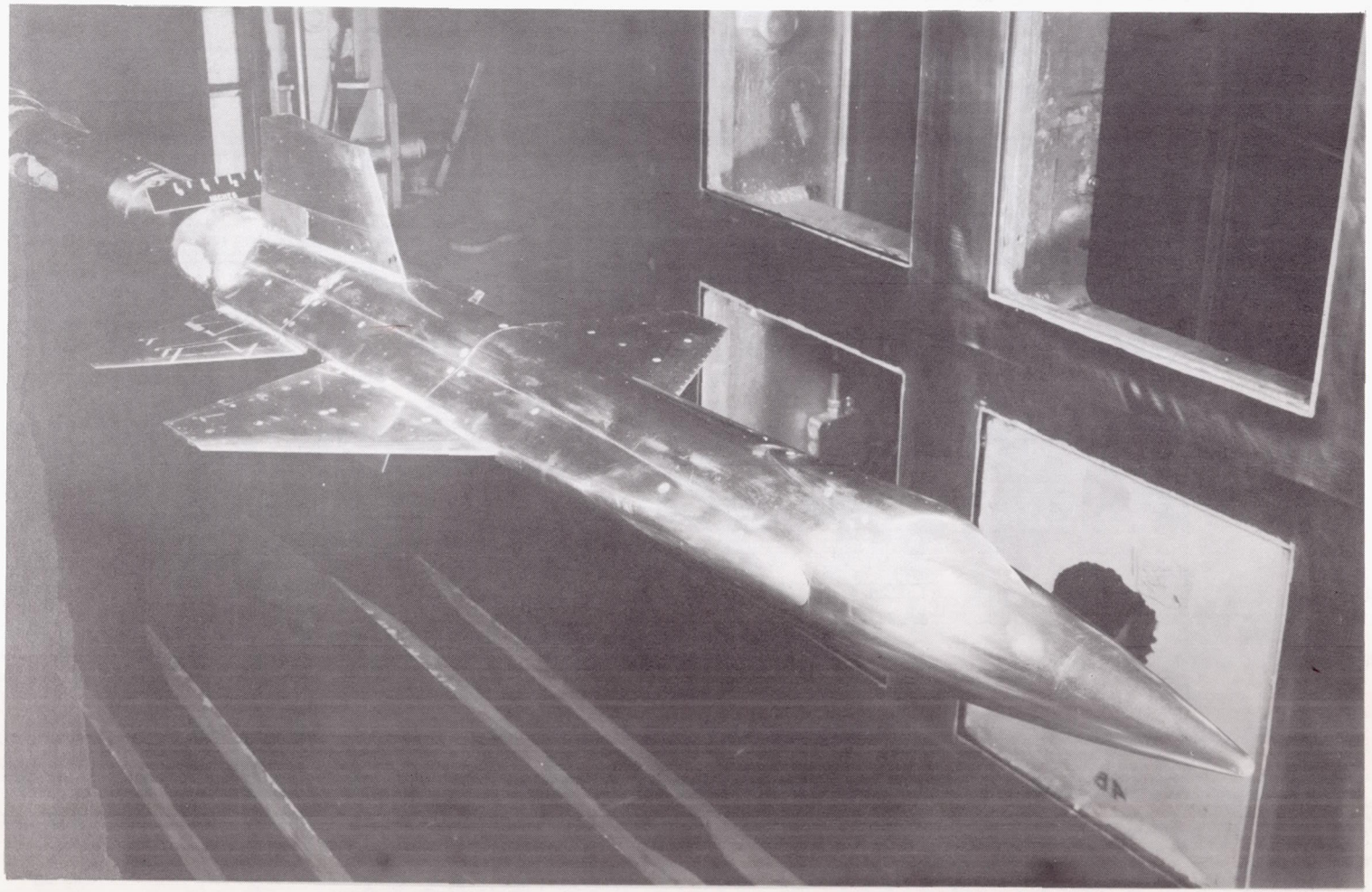
Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper tail							
			$\alpha = -20^\circ$	$\alpha = -10^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 15^\circ$	$\alpha = 20^\circ$
			$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed							
600	.150	1.000				-.429	-.458	-.515	-.565	-.623
			$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open							
600	.150	1.000	-.450	-.480	-.726	-.729	-.746	-.788	-.827	-.854
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed							
600	.150	1.000	-.419	-.439		-.376	-.425	-.489	-.544	-.574
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open							
600	.150	1.000			-.505	-.498	-.531	-.598	-.658	-.690
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = -7.5^\circ$; brakes closed							
600	.150	1.000			-.508	-.494	-.525	-.584	-.644	-.681
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 7.5^\circ$; brakes closed							
600	.150	1.000			-.715	-.719	-.744	-.791	-.812	-.838
			$\beta \approx 5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed							
600	.150	1.000	-.465	-.480		-.444	-.484	-.550	-.605	-.672
			$\beta \approx 5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open							
600	.150	1.000			-.714	-.734	-.757	-.781	-.828	-.861

TABLE VI.- PRESSURE COEFFICIENT MEASURED AT THE BASE OF THE UPPER VERTICAL TAIL - Concluded

(e) M = 1.18

Pressure coefficients C_p on -

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Upper tail							
			$\alpha = -20^\circ$	$\alpha = -10^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 15^\circ$	$\alpha = 20^\circ$
			$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed							
600	.150	1.000				-.372	-.342	-.381	-.422	-.457
			$\beta \approx -5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open							
600	.150	1.000	-.347	-.380	-.573	-.572	-.586	-.591	-.632	-.628
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed							
600	.150	1.000	-.276	-.341		-.337	-.333	-.365	-.417	-.420
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open							
600	.150	1.000			-.449	-.442	-.432	-.462	-.504	-.549
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = -7.5^\circ$; brakes closed							
600	.150	1.000			-.441	-.438	-.430	-.446	-.492	-.531
			$\beta \approx 0^\circ$; $\delta_e = 0^\circ$; $\delta_v = 7.5^\circ$; brakes closed							
600	.150	1.000			-.586	-.574	-.582	-.600	-.613	-.641
			$\beta \approx 5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes closed							
600	.150	1.000	-.348	-.376		-.377	-.356	-.404	-.449	-.481
			$\beta \approx 5^\circ$; $\delta_e = 0^\circ$; $\delta_v = 0^\circ$; brakes open							
600	.150	1.000			-.586	-.586	-.592	-.601	-.611	-.618



L-58-2647

Figure 1.- Photographs of the 0.0667-scale pressure model of the X-15 airplane as tested in the Langley 8-foot transonic pressure tunnel.

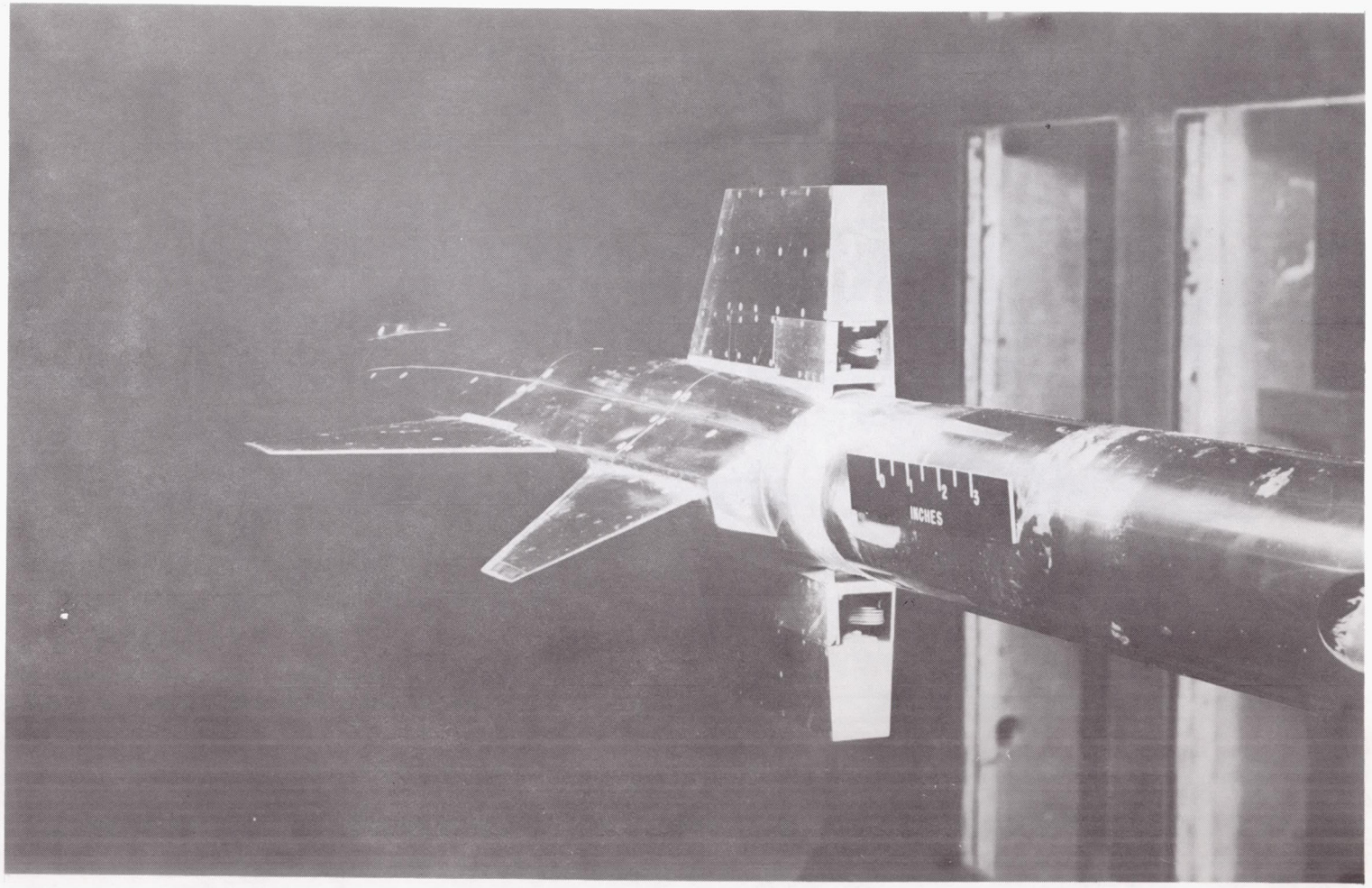


Figure 1.- Concluded.

L-58-2649

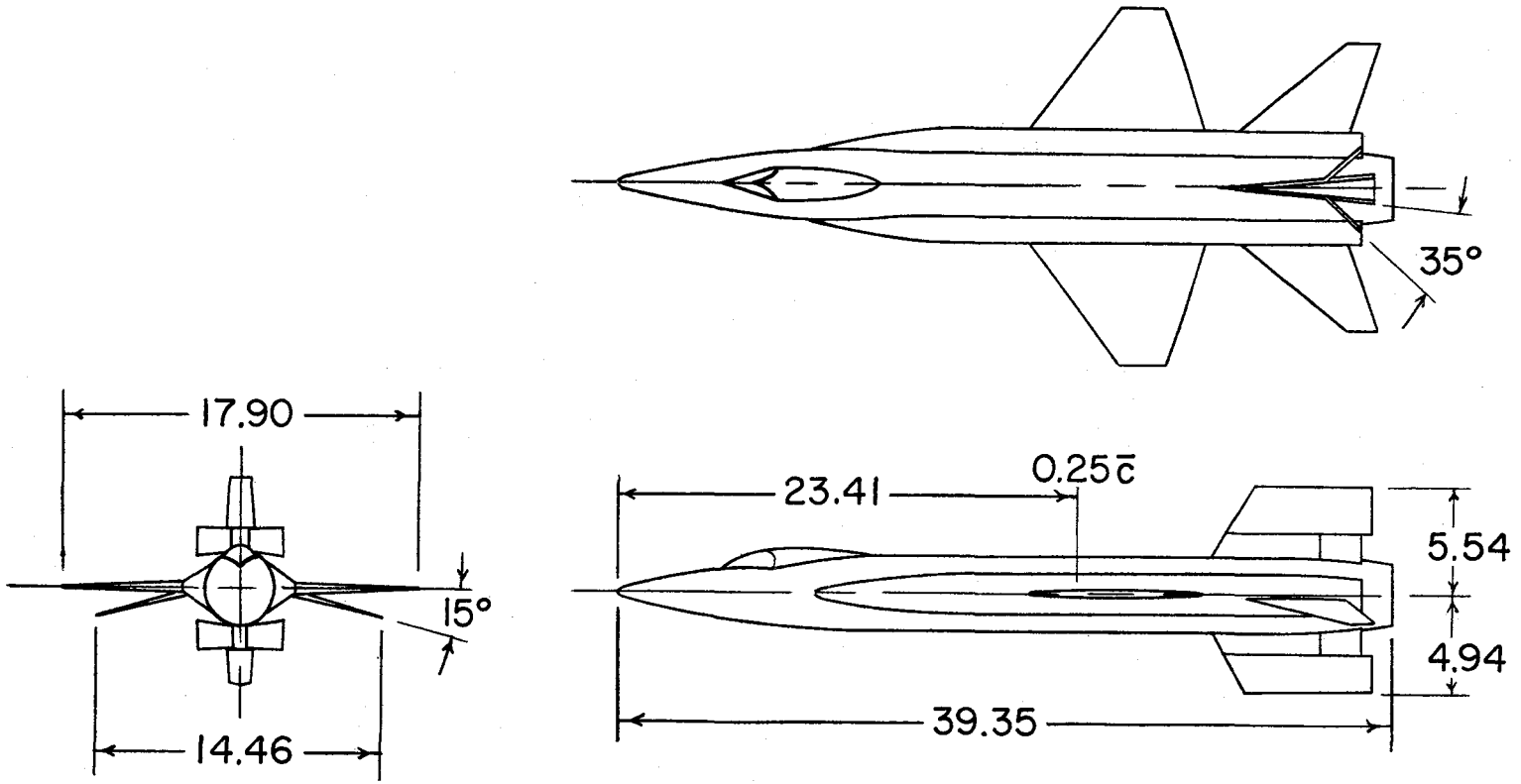
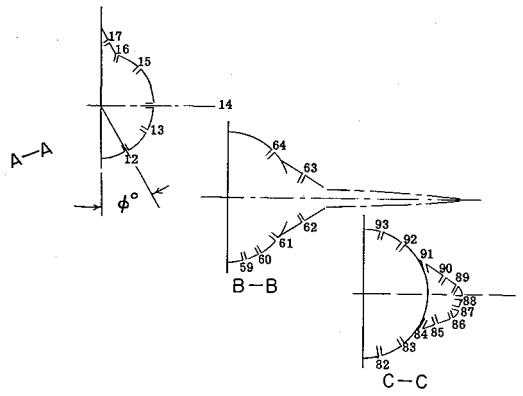
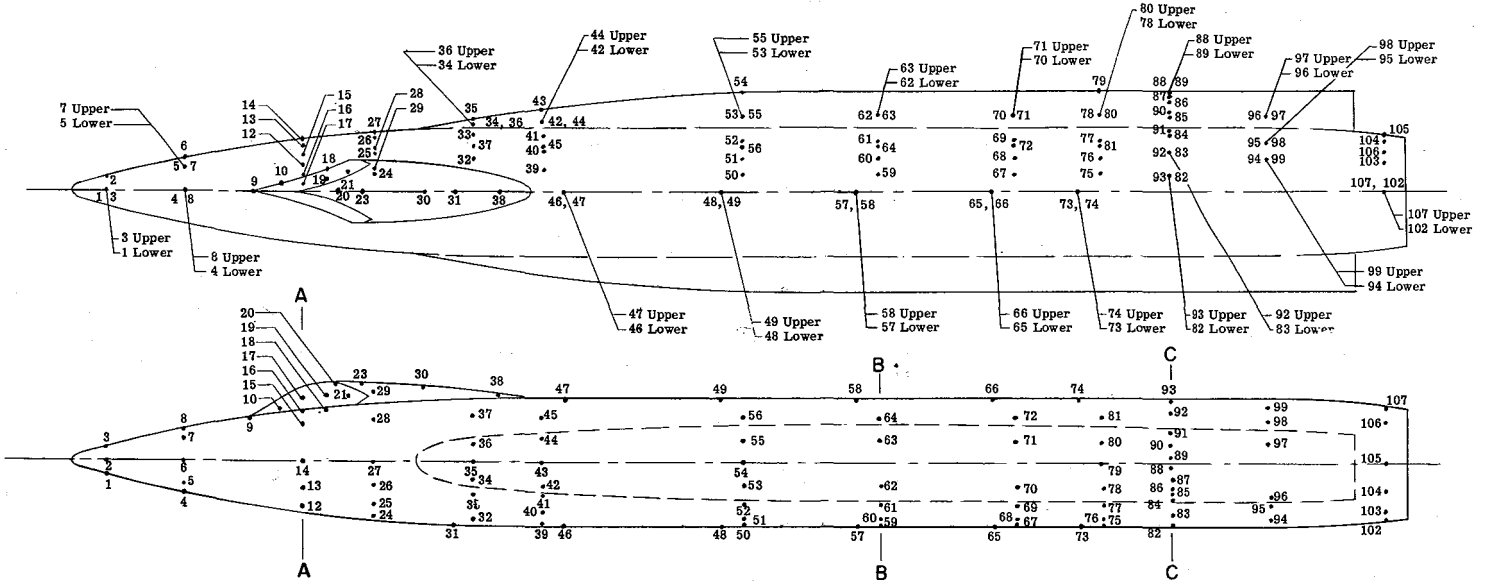


Figure 2.- Drawing of the 0.0667-scale pressure model of the X-15 with speed brakes open. All dimensions are in inches unless otherwise noted.



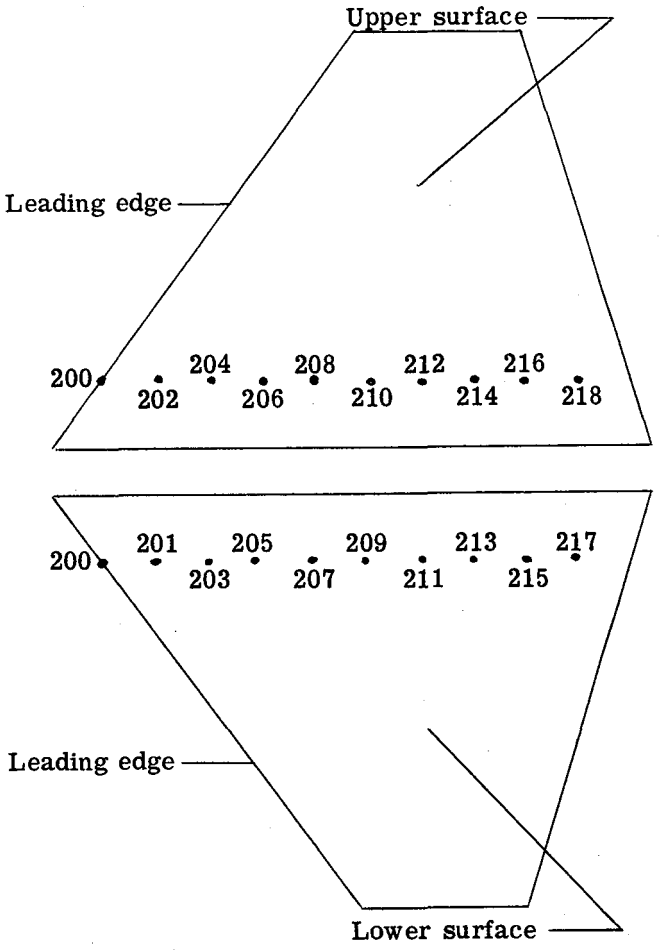
Model orifice number	x/l	ϕ, deg	Model orifice number	x/l	ϕ, deg	Model orifice number	x/l	ϕ, deg	Model orifice number	x/l	ϕ, deg
1	0.026	0	29	0.226	Canopy	55	0.503	Fairing	81	0.770	135
2	.026	90	30	.263	Canopy	56	.503	135	82	.820	15
3	.026	180	31	.283	0	57	.588	0	83	.820	38
4	.084	0	32	.299	30	58	.588	180	84	.820	Fairing
5	.084	45	33	.299	60	59	.604	15	85	.820	Fairing
6	.084	90	34	.299	Fairing	60	.604	30	86	.820	Fairing
7	.084	135	35	.299	Fairing	61	.604	50	87	.820	Fairing
8	.084	180	36	.299	Fairing	62	.604	Fairing	88	.820	Fairing
9	.134	Juncture	37	.299	135	63	.604	Fairing	89	.820	Fairing
10	.156	Juncture	38	.319	Canopy	64	.604	135	90	.820	Fairing
12	.173	30	39	.350	20	65	.690	0	91	.820	Fairing.
13	.173	60	40	.350	40	66	.690	180	92	.820	142
14	.173	90	41	.350	60	67	.706	15	93	.820	165
15	.173	135	42	.350	Fairing	68	.706	30	94	.897	30
16	.173	Juncture	43	.350	Fairing	69	.706	50	95	.897	50
17	.173	Canopy	44	.350	Fairing	70	.706	Fairing	96	.897	Fairing
18	.190	Juncture	45	.350	135	71	.706	Fairing	97	.897	Fairing
19	.190	Canopy	46	.367	0	72	.706	135	98	.897	130
20	.197	Canopy	47	.367	180	73	.753	0	99	.897	150
21	.207	Canopy	48	.486	0	74	.753	180			
23	.216	Canopy	49	.486	180	75	.770	15	102	.984	0
24	.226	22.5	50	.503	15	76	.770	30	103	.984	30
25	.226	45	51	.503	30	77	.770	50	104	.984	60
26	.226	67.5	52	.503	50	78	.770	Fairing	105	.984	90
27	.226	90	53	.503	Fairing	79	.770	Fairing	106	.984	135
28	.226	135	54	.503	Fairing	80	.770	Fairing	107	.984	180



(a) Orifices on fuselage.

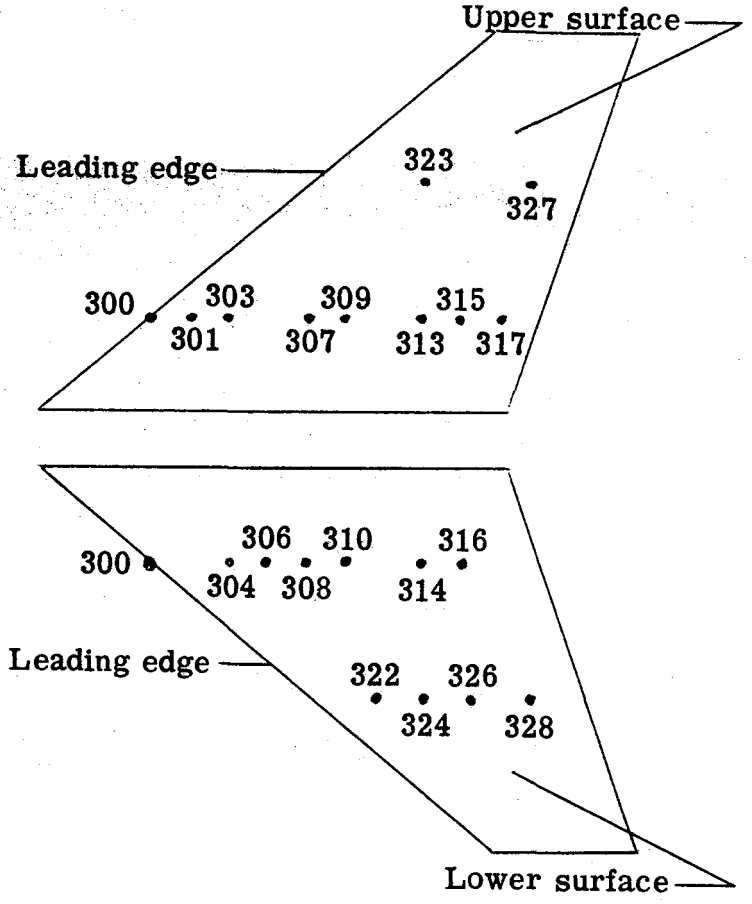
Figure 3.- Location of orifices on model.

Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$
200	0.18	0
201		.10
202		.10
203		.20
204		.20
205		.30
206		.30
207		.40
208		.40
209		.50
210		.50
211		.60
212		.60
213		.70
214		.70
215		.80
216		.80
217		.90
218		.90



(b) Orifices on right wing.

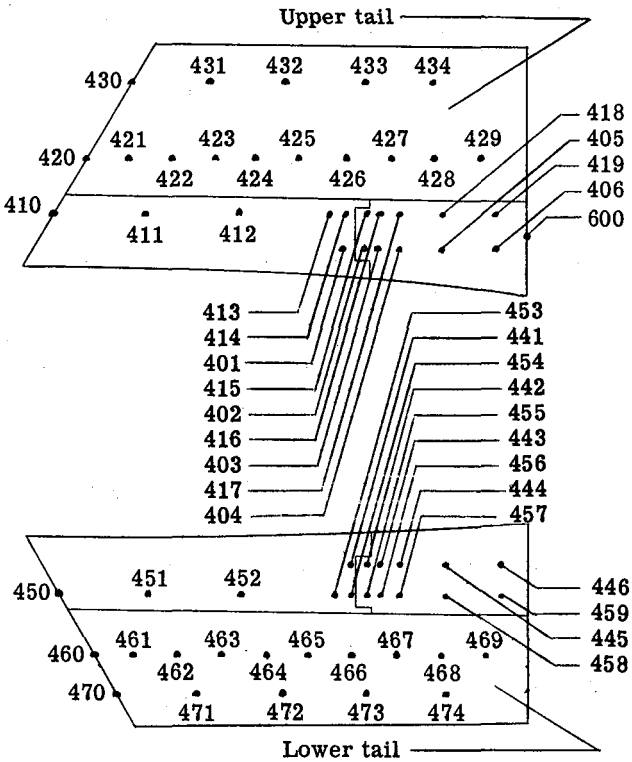
Figure 3.- Continued.



Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$
300	0.26	0
301	↓	.10
303		.20
304		.20
306		.30
307		.40
308		.40
309		.50
310		.50
313		.70
314		.70
315		.80
316		.80
317		.90
322	.62	.20
323	↓	.40
324		.40
326		.60
327		.80
328		.80

(c) Orifices on right horizontal tail.

Figure 3.- Continued.



Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$	Model orifice number	$\frac{y}{b/2}$	$\frac{x}{c}$
401	0.11	0.647	425	0.50	0.500	455	0.30	0.668
402	.11	.681	426	.50	.600	456	.30	.686
403	.11	.698	427	.50	.700	457	.30	.738
404	.11	.748	428	.50	.800	458	.30	.825
405	.11	.832	429	.50	.900	459	.30	.947
406	.11	.949	430	.83	0	460	.60	0
410	.25	0	431	.83	.200	461	.60	.100
411	.25	.200	432	.83	.400	462	.60	.200
412	.25	.400	433	.83	.600	463	.60	.300
413	.25	.600	434	.83	.800	464	.60	.400
414	.25	.630	441	.13	.647	465	.60	.500
415	.25	.668	442	.13	.682	466	.60	.600
416	.25	.685	443	.13	.700	467	.60	.700
417	.25	.738	444	.13	.748	468	.60	.800
418	.25	.825	445	.13	.832	469	.60	.900
419	.25	.947	446	.13	.949	470	.80	0
420	.50	0	450	.30	0	471	.80	.200
421	.50	.100	451	.30	.200	472	.80	.400
422	.50	.200	452	.30	.400	473	.80	.600
423	.50	.300	453	.30	.600	474	.80	.800
424	.50	.400	454	.30	.633	600	.15	1.000

(d) Orifices on right vertical tail including speed brakes.

Figure 3.- Concluded.

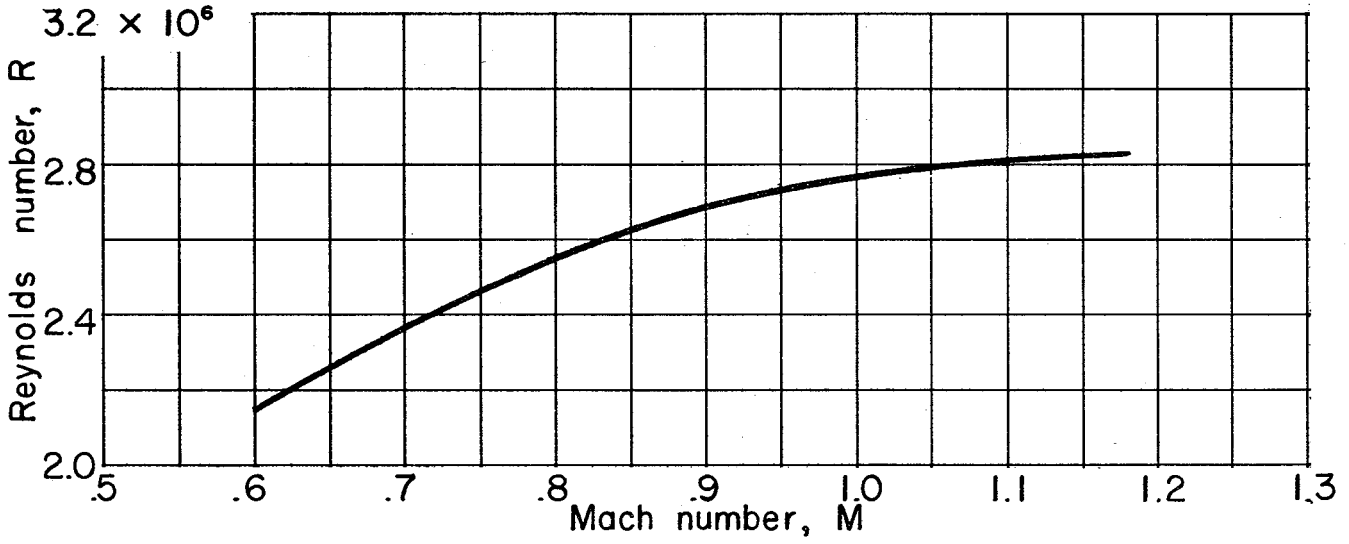


Figure 4.- Variation with Mach number of test Reynolds number based on wing $\bar{c}$ = 8.22 inches.