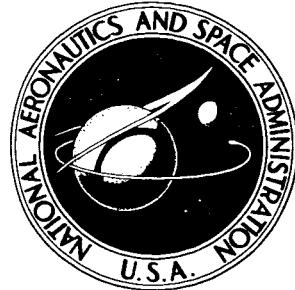


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ABSORPTION OF SOUND
IN AIR BELOW 1000 CPS

by Cyril M. Harris and W. Tempest

Prepared under Contract No. NAS 8-11002 by

COLUMBIA UNIVERSITY

New York, N. Y.

for

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION • WASHINGTON, D. C. • JUNE 1965

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ABSORPTION OF SOUND IN AIR BELOW 1000 CPS

SUMMARY

For many acoustic problems associated with the propagation of sound which is generated by launch vehicles, it is important to have accurate data of absorption of sound in air as a function of atmospheric conditions such as temperature, pressure, and humidity. Accurate data of this type have not been available below 2000 cps. Hence the purpose was to extend to lower frequencies the present range of reliable air absorption data. This report presents such information in the frequency range from about 125 cps to 1000 cps at 20° C, 0° C, -20° C, and -40° C.

The data described in this report can be applied to studies of acoustic propagation in the atmosphere in addition to the problem of establishing a theoretical model of sound absorption in air. In this connection measurements were made of the absorption in mixtures of oxygen and water vapor and also in mixtures of oxygen and deuterium oxide.

Author

SECTION I. INTRODUCTION

At present it is not possible to make accurate estimates of the attenuation of sound that has propagated through the atmosphere for a considerable distance. Such estimates are of considerable value in many acoustic problems associated with launch vehicles. The total attenuation between two points depends on a number of factors including the absorption of sound in air, refraction, and scattering. It is obvious that reliable data must be available which provide information regarding the absorption of sound in air as a function of atmospheric conditions. Unfortunately, accurate data of this type have not been available for frequencies below 2000 cps. In general, where such data have been required, they have been estimated by extrapolation from measurements at higher frequencies. The purpose of this study was to extend the range over which reliable air absorption data are available to lower frequencies.

During the past six years in this laboratory, an active program of research has been carried out for investigating the absorption of sound (from 125 cps to 12,500 cps) in air for different conditions of pressure, temperature, and humidity. The results of the measurements in the range from 2000 to 12,500 cps were published in a paper last year [1]. The present report on sound absorption in air provides data in the range from approximately 125 cps to 1000 cps.

In addition to the application of the data described in this report to studies of acoustic propagation in the atmosphere, these data can be applied to the problem of establishing a theoretical model of sound absorption in air. In this connection measurements were made of the absorption of sound in mixtures of oxygen and water vapor and also in mixtures of oxygen and deuterium oxide.

SECTION II. MEASUREMENT PROCEDURE

A detailed description of the experimental setup used for obtaining the data presented in this report has been given by Harris [1] in a paper which describes the technique of sound absorption measurement employed here. A complete description of the spherical chamber, the electro-acoustic measurement system, the humidity control, and evaluation of wall losses of the spherical chamber, given in that paper, is reproduced in Appendix A. A summary of this information is abstracted in this section.

The spherical chamber in which the measurements are made has an inner diameter of 1.68 meters. It is fabricated of heavy steel in order to minimize the effects of wall losses, which are quite low. For example, the reverberation time at 1000 cps when the chamber is filled with dry air is 43 seconds. Excellent temperature stability of the sphere is obtained and the temperature can be adjusted by pumping a coolant through coils affixed to the exterior surface of the chamber. The spherical chamber and associated equipment can be evacuated before filling the chamber with air to avoid contamination which can have considerable effect on the measurements.

Sound is introduced from a loudspeaker driving unit through a probe tube into the spherical chamber, thereby producing an acoustic point source within the chamber. This source was very poorly matched to the spherical enclosure so that its contribution to the absorption of the chamber would be negligible. The length of the probe was selected so that the point source is near a pressure maximum for the normal modes of vibration of the enclosure that are used in the low frequency measurements (described below), but of such a length as to discriminate against the excitation of nearby normal modes. After an acoustic steady-state has been established by the sound source, the source is turned off and the rate of decay of sound, in decibels per second, is measured.

The method of establishing a steady-state condition of humidity in the spherical enclosure is to pump the air from the sphere through an auxiliary "saturator" chamber which either adds or subtracts moisture--depending on the temperature of the saturator. Air is re-circulated through the saturator until the air contains approximately the amount of water vapor desired. Then the saturator is bypassed, but re-circulated until a steady-state humidity condition has been achieved--during this time, water vapor may be absorbed or given off by the steel walls of the spherical chamber. The humidity in the spherical enclosure is measured by an electric hygrometer which uses lithium chloride sensing elements manufactured by Hygrodynamics, Inc.

Nitrogen has a sound absorption value that is well established. Hence, if the sphere is filled with this gas it is possible to compute the contribution to the measured decay rate R_{N_2} that is due to nitrogen along. If decay rate measurements are made in the sphere when filled with nitrogen, the measured value of the decay rate will be greater than R_{N_2} ; the remaining contribution is due to losses at the wall. Now because air and nitrogen are similar in characteristic impedance and in molecular weight, the wall losses are approximately the same for the decay of sound when the sphere is filled with either gas. Thus, decay rate measurements in nitrogen (Tables 5 and 6) provide data for evaluating the wall losses when measurements are made in air. It follows that the decay rate of sound in the sphere, R_{air} , is given by eq. 3 of Appendix A:

$$R_{air} = R_{measured \text{ (air)}} - R_{measured \text{ (N}_2\text{)}} + R_{N_2}$$

In this manner the value of the rate of decay for sound in air was evaluated. The attenuation coefficient m per meter (as expressed in the equation $I = I_0 e^{-mx}$) is related to the decay rate by the equation:

$$m = R_{air} / (4.34c) \text{ meters}^{-1}$$

where c is the velocity in meters/seconds.

SECTION III. RESULTS OF MEASUREMENTS OF SOUND ABSORPTION IN AIR

In this report the results of measurement of the absorption of sound in air are given as a function of water vapor content at atmospheric pressure for four temperatures, 20°C , 0°C , -20°C , and -40°C . Additional data for air are given at 20°C for pressures of 400 mm and 200 mm. This information is presented in both tabular and graphic form.

The data presented in Reference 1 at higher frequencies were taken by measuring the rate of decay of a large number of modes of vibrations, within a third-octave band, which were excited by a random noise source. Here, in the lower frequency range, the decay rate of individual modes which are excited by a pure tone is measured. Thus, data are given for each of the conditions at the five normal frequencies (eigenfrequencies) of the following normal modes of vibration of the spherical chamber: $(1, 1)$, $(0, 1)$, $(0, 2)$, $(0, 3)$, and $(0, 4)$. For example, at normal pressure and a temperature of 20°C , the $(0, 1)$ normal mode of vibration, which is the first radial mode, has a normal frequency of 293 cps. Since the normal frequencies depend upon the velocity of sound, and since the velocity of sound is a function of temperature, the set of curves presented in Figures 1 through 4 are not at the same set of frequencies for the various temperatures.

The actual data points for the absorption measurements taken at atmospheric pressure are given in Tables 1 through 4 along with other system measurements. For application to practical problems, smoothed curves drawn through the actual data points are more useful. Such smoothed curves are shown in Figures 1 through 4. These data are in good agreement with earlier measurements at higher frequencies [1]. Good accuracy was obtained in all measurements except at -40°C where the attenuation is exceedingly low. For this reason the data at this temperature may be regarded as a best estimate. The data points corresponding to the smoothed curves are given in Tables 8 through 11. Data for reduced air pressure at 20°C are shown in Figures 10 and 11 and are listed in Table 6.

SECTION IV. COMPARISON WITH THEORY

It is of interest to compare the data presented here with the theoretical studies by Kneser [2] of the absorption of sound in air containing water vapor. The first comparison is shown in Figure 5. This curve of normalized attenuation versus normalized humidity was obtained as follows: The original data points for the attenuation coefficient due to molecular absorption are listed in Tables 1 through 4 under "AIR MOL." The data for each curve has a maximum attenuation value m_{\max} at a particular value of water vapor concentration, h_{\max} . The data points for each "attenuation versus water vapor" curve were normalized by dividing each value of AIR MOL by m_{\max} . According to the theory of Kneser, the normalized data for all frequencies should fall along the dashed curve shown. The solid curve which represents the present results is in close agreement with similar data presented by Harris [1] and with similar data obtained by Delsasso [3].

According to the theory, the maximum value of absorption increases linearly with frequency. This relationship is shown by the solid lines in Figure 6 for 20°C, 0°C, and -20°C. Also shown are the values of m_{\max} taken from the original data points.

In Figure 7 another comparison with theory is shown in a plot of relaxation frequency, f_{\max} , versus the molar concentration of water vapor in the air. The relaxation frequency for a given condition of humidity is the frequency of maximum absorption and is related to the angular relaxation frequency by the equation

$$k = 2\pi f_{\max} = \omega_{\max}$$

The data obtained in this study are plotted together with similar data from Reference 1 obtained at higher frequencies.

SECTION V. ABSORPTION OF SOUND IN OXYGEN-WATER AND OXYGEN-DEUTERIUM OXIDE MIXTURES

In the past, a number of experiments have been performed to determine the absorption of sound in dry oxygen and in oxygen containing water vapor [4, 11]. It has been shown that there is a peak in the curve of "sound absorption versus moisture content" due to the relaxation of the internal energy of the vibrational mode of the oxygen molecule. In the dry gas, recent work (Parker [7], Holmes, Smith and Tempest [8]) has shown the peak in absorption to occur at about 9 cps at a pressure of 1 atm and at a temperature of 20°C. Other work indicated a higher relaxation frequency (Knotzel and Knotzel [6], 50 cps; and Henderson [9], 60 cps). As is the case with air-water mixtures, measurements in oxygen-water mixtures have shown that small quantities of water significantly affect the relaxation frequency and that this frequency of maximum absorption rises rapidly with increasing moisture content.

Measurements are reported here of the absorption of sound in extremely-dry oxygen of high purity, as a function of water vapor content. Figure 8 shows the results plotted in the form of intensity attenuation coefficient m per meter as a function of moisture content in percent molar concentration of water for the following frequencies (the pairs of numbers in the brackets specify the normal mode of vibration): [(1, 1), 130 cps; (0, 1), 280 cps; (0, 2), 482 cps; (0, 3), 680 cps; (0, 4), 878 cps]. These data are tabulated in Table 12. The moisture content at which the peak in the absorption curve occurs, increases with increasing frequency. The expected values of maximum absorption at the various frequencies were calculated from the Kneser theory [2], and were found to be on average about 5 percent higher than the measured values.

Figure 9 shows a comparison between the experimental data presented here and data of other researchers. Four curves are plotted of relaxation frequency as a function of moisture content as calculated from the following equations which are given in their respective papers:

$$\text{Knudsen and Obert [5]} \quad f_{\max} = 4.96 \times 10^2 h + 6.05 \times 10^3 h^2$$

$$\text{Knotzel and Knotzel [6]} \quad f_{\max} = 40 + 1.95 \times 10^3 h + 1.32 \times 10^4 h^2$$

$$\text{Clark and Henderson [10]} \quad f_{\max} = 3 + 1.66 \times 10^3 h + 1.45 \times 10^4 h^2$$

$$\text{Harlow and Kitching [11]} \quad f_{\max} = 2.10 \times 10^2 h + 1.20 \times 10^4 h^2$$

where f_{\max} is the frequency of maximum absorption in cps and h is the percent molar concentration of water. The data of Knudsen and Obert, which differs considerably from the other results shown, is extrapolated from measurements at 3,000 cps and higher; it is probably subject to considerable error at low frequencies. In contrast, the data of

Harlow and Kitching is based on measurements at frequencies as low as 98 cps, which rules out error due to extrapolation. It is possible that the difference between their results and those of others may be due to the method by which they determined the moisture content in their gas. Before the air re-circulation system shown in Figure 14 (Appendix A) was developed for humidity control, some measurements were made in which moisture content was determined from weights of evaporated water in the system. Results so obtained were compared with results in which humidity is measured by the direct technique of circulating the gas over calibrated electrical conductivity elements. It was found that the two methods gave quite different results, in terms of the moisture content required to produce a particular frequency of maximum absorption, with the evaporation technique giving humidity levels as high as three times the direct measurements. It was concluded that a considerable amount of moisture may be taken out of the gas in the chamber by the walls. Such an effect would result in an apparently lower measured value of relaxation frequency for a given moisture content as reported by Harlow and Kitching. The results of the present study shown by the x's in Figure 9 are in good agreement with those of Knotzel and Knotzel; they are in very close agreement with the data of Clark and Henderson, thus supporting the view that the frequency dependence of the absorption peak on moisture content contains a quadratic term.

Data are shown in Figure 12 for the absorption of sound in a mixture of oxygen and deuterium oxide. (These data are tabulated in Table 13.) A comparison of Figures 8 and 12 indicates that for a given frequency, the maximum value of absorption in oxygen-water mixture is approximately the same as the maximum value for water vapor and deuterium oxide mixture. However, the curves for the oxygen-deuterium oxide mixture have their peaks at significantly lower vapor concentrations. At present there is no satisfactory theoretical model to explain these results but these data may prove useful in helping to provide the necessary information required in establishing such a model.

APPENDIX A

I. EXPERIMENTAL SETUP¹

Spherical Chamber

The spherical chamber used in this study has an inner diameter of 1.68 m (volume=2.48 m³). It was specially fabricated, in two hemispherical shells, from hot-rolled steel having a thickness of 16 mm. The two halves are fitted with flanges and bolted together with a Teflon gasket, as illustrated in Figure 13. That the acoustic boundary losses are low in this chamber is illustrated by the fact that at 1000 cps its reverberation time is 43 sec when the chamber is filled with dry air. Measurements of the decay of sound in the chamber, when it is filled with nitrogen, show that there are no isolated mechanical resonances of the spherical chamber housing which have significant effect on the rate of decay of sound in the enclosure over the frequency range employed. The entire chamber is packed in glass-fiber blankets to provide thermal insulation. Its temperature is controlled by pumping a methanol coolant through copper tubing fastened to the exterior surface of the sphere (Fig. 13). By this means the air temperature within the chamber can be set at any value between 20° and -60°C and can be held constant to within ± 0.1°C.

A high-capacity vacuum pump connected to the chamber, together with a diffusion pump, can reduce the pressure within the sphere and its associated air lines to 1 micron (mercury column height). This is essential in order to free the entire system from contamination and to rid all parts of the system of water vapor which may be absorbed by the interior walls of the sphere and walls of the air-circulation system. During the actual decay measurements, the air-circulation system is not in operation; then the lines are closed by gate valves to avoid the loss of acoustic energy from the spherical chamber to the lines.

Electro-Acoustic Measurement System

The sound source is a 60-watt loudspeaker unit that is coupled to the spherical chamber by a stainless steel probe tube, 1/4 inch in diameter, as illustrated in Figure 13. This arrangement provides an effective acoustic point source within the chamber at the end of the probe tube. The electrical and acoustical coupling of the acoustic source are purposely mismatched in impedance so that the amount of acoustic energy that

¹

The material contained in this Appendix is taken from the reprint "Absorption of Sound in Air in the Audio-Frequency Range," Cyril M. Harris, Journal of the Acoustical Society of America, Vol. 35, No. 1, pp. 11-17, January 1963, Reference 1.

is absorbed by this transducer, while it is inactive during decay measurement, will not be significant. The loudspeaker is driven from a random-noise source. A small dynamic microphone is located in the wall of the spherical chamber. The output of the microphone is amplified, fed through a Brüel and Kjaer third-octave filter (type 2109), and thence to a high-speed level recorder. When the random-noise source is turned off, a curve of the rate of decay of sound in the spherical chamber is obtained with the level recorder. The slope of this decay curve determines the decay rate in db/sec at the center frequency of the band at which the third-octave analyzer is set.

Humidity Control

The problem of accurately controlling and measuring the humidity in a chamber in which air absorption measurements are made has always presented difficulties. In past studies, the accuracy of humidity-measurement techniques at low values of humidity, a range which is often of considerable interest, has been poor. In addition to the question of accuracy, there is the problem of ensuring that the humidity measured actually is representative of conditions within the chamber. Difficulties arise because of the absorption of water by surfaces within the measurement system.

Humidity control and measurement probably account for a major source of discrepancy among published data on the absorption of sound in air. The method used here for establishing controlled conditions of humidity is illustrated in Figure 14. Air is circulated through a closed system by means of a circulation pump which consists of a small high-speed turbofan. Air leaves the spherical chamber through an outlet at the bottom of the sphere. Then it passes through a "saturator" which is a small stainless steel cylinder whose temperature can be controlled from approximately -60°C to +20°C by means of a coolant in which the saturator is immersed. Distilled water is contained in the bottom of the saturator. Moisture either is taken from the air that passes through the saturator and deposited in the saturator, or is taken from the saturator and added to the air that passes through the saturator -- depending upon the relative temperatures of the spherical chamber and the saturator. Air is recirculated through the system until the air in the spherical chamber contains approximately the amount of water vapor required to achieve the desired equilibrium condition. Then the saturator is bypassed (by a valve system that is not shown in Fig. 14); this causes the air to re-circulate from the sphere, through the pump, and then back to the sphere -- until a steady-state humidity condition is obtained. This usually requires about a half hour.

Two sets of electric hygrometers were employed to measure relative humidity. The operation of the hygrometers is based upon the change in the resistance, with humidity, of lithium chloride sensing elements (class A, type H) which are in a bridge circuit and are manufactured by Hygrodynamics, Inc. Under the conditions employed, these elements have a rapid response time and provide a continuous monitoring of the humidity within the spherical chamber during conditions of re-circulation of air. The individual sensing elements in the two sets covered the following ranges: 1.6 to 5%, 5 to 14%, 12

to 20%, 18 to 30%, 29 to 43%, 41 to 59%, 54 to 72%. The two sets were closely matched against each other. One set was placed at the air inlet near the top of the spherical chamber and the other at the air outlet at the bottom. Observations of the readings of these sets of elements were used to determine when equilibrium was achieved. These humidity-sensing elements were calibrated in the laboratory of the manufacturer immediately before the data contained in this paper were taken--then all units were calibrated once again in a similar manner directly after the experimental data were taken. Essentially, a substitution method of humidity calibration was employed so that the accuracy provided by the sensing elements was greater than that usually quoted for such units which are used under varying field conditions -- here the accuracy was better than $\pm 1\%$ RH (relative humidity) except in the lowest range where it was about $\pm 0.5\%$ RH.

Two calibration techniques are employed by the manufacturer of the humidity-sensing elements that were used. Above 5% RH, elements are calibrated in a controlled-humidity chamber using a high-precision psychrometer employing thermometers calibrated by the National Bureau of Standards. These psychrometric readings are referred to relative-humidity tables based on the barometric pressure corresponding to that in the calibration chamber. In the very low humidity range, elements are calibrated using a two-pressure technique embodying the principles outlined by Weaver and Riley in which a known humidity condition is generated by saturating a gas stream at elevated pressures, and then expanding to atmospheric pressure. Calibrations of the sensing elements used in this study are reproducible within $\pm 0.2\%$ RH. The two techniques are compared at the lower-humidity ranges and are in close agreement (within $\pm 0.5\%$ RH).

Evaluation of Wall Losses of Spherical Chamber

In order to determine the absorption of sound in air from measurements of the rate of decay of sound in the spherical chamber used in this study, it is necessary to know the extent of the contribution to the rate of decay that may be attributed to wall losses. This may be evaluated from measurements of the rate of decay of sound in the chamber when it is filled with nitrogen since nitrogen exhibits no anomalous absorption in the frequency range of measurement. By comparing the measured values of decay rate in nitrogen with the decay rate computed from absorption data for nitrogen, one obtains a small difference which represents the effects of wall losses. This is shown as follows: The decay rate of sound, $R_{\text{measured (air)}}$, that one measures in the spherical chamber when it is filled with air is given (in decibels per second) by

$$R_{\text{measured (air)}} = R_{\text{air}} + R_{\text{wall}}, \quad (1)$$

where R_{air} is the decay rate due to absorption in the air, and R_{wall} is the decay rate due to absorption at the walls.

When the chamber is filled with prepurified dry nitrogen,

$$R_{\text{measured (N}_2\text{)}} = R_{N_2} + R_{\text{wall}}, \quad (2)$$

where R_{N_2} is the decay rate due to absorption in nitrogen in db/sec.

If it is assumed that the wall losses for N_2 and air are approximately the same, because these gases are closely similar in molecular weight and characteristic impedance, then subtracting eq. 2 from eq. 1:

$$R_{\text{air}} = R_{\text{measured (air)}} - R_{\text{measured (N}_2\text{)}} + R_{N_2} \quad (3)$$

The first two terms on the right are obtained from measurements of the rate of decay of sound in the spherical chamber while the third term is calculated from the data for nitrogen by Parbrook and Tempest. Consideration has been given to possible variation in the boundary losses with changes in the humidity within the sphere. As pointed out by Evans and Bazley in discussing this possibility, the work of Knudsen, Wilson and Anderson indicates that such an effect is not significant; their data show that there is no appreciable change in wall absorption even when moisture condenses on the wall surfaces.

The value of R_{air} in db/sec given by eq. 3 is converted to the attenuation coefficient m per meter as expressed in the equation $I = I_0 e^{-mx}$ by the relation

$$m = R_{\text{air}} / (4.34c) \text{ meters}^{-1}$$

where c is the velocity of sound in m/sec.

APPENDIX B
TABULAR DATA *

TABLE NO.	DATA POINTS	GAS	PRESSURE MM	TEMPERATURE DEG. CENT
1	ORIGINAL	AIR + WATER VAPOR	760	20
2	ORIGINAL	AIR + WATER VAPOR	760	0
3	ORIGINAL	AIR + WATER VAPOR	760	-20
4	ORIGINAL	AIR + WATER VAPOR	760	-40
5	ORIGINAL ORIGINAL ORIGINAL ORIGINAL	DRY NITROGEN DRY NITROGEN DRY NITROGEN DRY NITROGEN	760 760 760 760	20 0 -20 -40
6A	ORIGINAL	AIR + WATER VAPOR	400	20
6B	ORIGINAL	AIR + WATER VAPOR	200	20
7	ORIGINAL	DRY NITROGEN VS. PRESSURE		20
8	SMOOTHED	AIR + WATER VAPOR	760	20
9	SMOOTHED	AIR + WATER VAPOR	760	0
10	SMOOTHED	AIR + WATER VAPOR	760	-20
11	SMOOTHED	AIR + WATER VAPOR	760	-40
12	ORIGINAL	OXYGEN + WATER VAPOR	760	20
13	ORIGINAL	OXYGEN + D20	760	20

* These tabular data, actually computer run sheets, are graphically illustrated in various figures from 1 through 12.

TABLE NO. 1
 TABULATION OF ORIGINAL DATA POINTS FOR
 ABSORPTION OF SOUND IN AIR VERSUS RELATIVE HUMIDITY
 AT 20 DEGREES CENTIGRADE

R.H.	TEMP	FREQ	LAMDA	AIR	AIR	AIR	AIR	MU	3000*
				+ WALL	ONLY	ONLY	CLAS	MOL	LOG
PRCT	DEG	CENT	CPS	METRS	DB/S	DB/S	DB/S	/M	RH
		1	2		3	4	5	/M	
									6
1234567890	1234567890	1234567890	1234567890	1234567890	1234567890	1234567890	1234567890	1234567890	1234567890
•1	20	136	2.520	2.54	1.99	.55	0037	0007	0037 0093-2999
1.2	20	136	2.520	3.18	1.99	1.19	0080	0007	0080 0202 238
1.4	20	136	2.520	3.08	1.99	1.09	0073	0007	0073 0184 438
1.8	20	136	2.520	2.76	1.99	.77	0052	0007	0052 0131 766
2.1	20	136	2.520	2.64	1.99	.65	0044	0007	0044 0111 967
2.7	20	136	2.520	2.50	1.99	.51	0034	0007	0034 0086 1294
3.8	20	136	2.520	2.36	1.99	.37	0025	0007	0025 0063 1739
5.1	20	136	2.520	2.30	1.99	.31	0021	0007	0021 0053 2123
6.1	20	136	2.520	2.26	1.99	.27	0018	0007	0018 0045 2356
6.2	20	136	2.520	2.36	1.99	.37	0025	0007	0025 0063 2377
7.2	20	136	2.520	2.32	1.99	.33	0022	0007	0022 0056 2572
7.4	20	136	2.520	2.26	1.99	.27	0018	0007	0018 0045 2608
8.2	20	136	2.520	2.35	1.99	.36	0024	0007	0024 0061 2741
9.0	20	136	2.520	2.22	1.99	.23	0015	0007	0015 0038 2863
10.1	20	136	2.520	2.26	1.99	.27	0018	0007	0018 0045 3013
13.3	20	136	2.520	2.38	1.99	.39	0026	0007	0026 0066 3372
16.3	20	136	2.520	2.35	1.99	.36	0024	0007	0024 0061 3637
20.0	20	136	2.520	2.36	1.99	.37	0025	0007	0025 0063 3903
25.4	20	136	2.520	2.23	1.99	.24	0016	0007	0016 0040 4215
31.0	20	136	2.520	2.22	1.99	.23	0015	0007	0015 0038 4474
39.0	20	136	2.520	2.22	1.99	.23	0015	0007	0015 0038 4773
•1	20	293	1.170	1.95	1.36	.59	0040	0032	0040 0047-2999
1.2	20	293	1.170	4.05	1.36	2.69	0181	0032	0181 0212 238
1.4	20	293	1.170	4.17	1.36	2.81	0189	0032	0189 0221 438
1.8	20	293	1.170	4.06	1.36	2.70	0181	0032	0181 0212 766
2.1	20	293	1.170	3.70	1.36	2.34	0157	0032	0157 0184 967
2.7	20	293	1.170	3.18	1.36	1.82	0122	0032	0122 0143 1294
3.8	20	293	1.170	2.86	1.36	1.50	0101	0032	0101 0118 1739
5.1	20	293	1.170	2.43	1.36	1.07	0072	0032	0072 0084 2123
6.1	20	293	1.170	2.22	1.36	.86	0058	0032	0058 0068 2356
6.2	20	293	1.170	2.22	1.36	.86	0058	0032	0058 0068 2377
7.2	20	293	1.170	2.12	1.36	.76	0051	0032	0051 0060 2572
7.4	20	293	1.170	2.09	1.36	.73	0049	0032	0049 0057 2608
8.2	20	293	1.170	2.07	1.36	.71	0048	0032	0048 0056 2741
9.0	20	293	1.170	2.01	1.36	.65	0044	0032	0044 0052 2863
10.1	20	293	1.170	2.03	1.36	.67	0045	0032	0045 0053 3013
13.3	20	293	1.170	1.99	1.36	.63	0042	0032	0042 0049 3372
16.3	20	293	1.170	1.98	1.36	.62	0042	0032	0042 0049 3637
20.0	20	293	1.170	1.98	1.36	.62	0042	0032	0042 0049 3903
25.4	20	293	1.170	1.97	1.36	.61	0041	0032	0041 0048 4215
31.0	20	293	1.170	1.98	1.36	.62	0042	0032	0042 0049 4474
39.0	20	293	1.170	1.96	1.36	.60	0040	0032	0040 0047 4773

* last column employed in computer plotting only.

TABLE NO. 1

TABULATION OF ORIGINAL DATA POINTS FOR
ABSORPTION OF SOUND IN AIR VERSUS RELATIVE HUMIDITY
AT 20 DEGREES CENTIGRADE

TABLE NO. 1
TABULATION OF ORIGINAL DATA POINTS FOR
ABSORPTION OF SOUND IN AIR VERSUS RELATIVE HUMIDITY
AT 20 DEGREES CENTIGRADE

* last column employed in computer plotting only.

TABLE NO. 2
TABULATION OF ORIGINAL DATA POINTS FOR
ABSORPTION OF SOUND IN AIR VERSUS RELATIVE HUMIDITY
AT 0 DEGREES CENTIGRADE

R.H.	TEMP	FREQ	LAMDA	AIR	AIR	AIR	AIR	MU	3000*
				+ PRCT	WALL	WALL	ONLY	ONLY	LOG
				DEG CENT	DB/S	DB/S	DB/S	/M	RH
1	2	3	4	5	6				
12345678901	12345678901	12345678901	12345678901	12345678901	12345678901	12345678901	12345678901	12345678901	12345678
.1	0	132	2.520	2.10	1.88	.22	0015	0007	0015 0038-2999
3.1	0	132	2.520	2.60	1.88	.72	0050	0007	0050 0126 1474
4.1	0	132	2.520	2.67	1.88	.79	0055	0007	0055 0138 1838
4.4	0	132	2.520	2.67	1.88	.79	0055	0007	0055 0138 1930
5.4	0	132	2.520	2.64	1.88	.76	0053	0007	0053 0133 2197
6.2	0	132	2.520	2.53	1.88	.65	0045	0007	0045 0113 2377
7.3	0	132	2.520	2.55	1.88	.67	0047	0007	0047 0118 2590
8.9	0	132	2.520	2.34	1.88	.46	0032	0007	0032 0080 2848
11.1	0	132	2.520	2.37	1.88	.49	0034	0007	0034 0085 3136
11.9	0	132	2.520	2.26	1.88	.38	0026	0007	0026 0065 3227
12.4	0	132	2.520	2.17	1.88	.29	0020	0007	0020 0050 3280
13.0	0	132	2.520	2.10	1.88	.22	0015	0007	0015 0038 3342
15.4	0	132	2.520	2.10	1.88	.22	0015	0007	0015 0038 3563
17.5	0	132	2.520	2.07	1.88	.19	0013	0007	0013 0033 3729
25.1	0	132	2.520	2.04	1.88	.16	0011	0007	0011 0028 4199
27.4	0	132	2.520	2.02	1.88	.14	0010	0007	0010 0025 4313
33.6	0	132	2.520	2.02	1.88	.14	0010	0007	0010 0025 4579
38.4	0	132	2.520	1.97	1.88	.09	0006	0007	0006 0015 4753
44.6	0	132	2.520	2.02	1.88	.14	0010	0007	0010 0025 4948
54.0	0	132	2.520	1.99	1.88	.11	0008	0007	0008 0020 5197
64.0	0	132	2.520	2.03	1.88	.15	0010	0007	0010 0025 5419
84.0	0	132	2.520	1.99	1.88	.11	0008	0007	0008 0020 5773
91.0	0	132	2.520	2.00	1.88	.12	0008	0007	0008 0020 5877
.1	0	282	1.170	1.63	1.34	.29	0020	0031	0020 0024-2999
3.1	0	282	1.170	2.49	1.34	1.15	0080	0031	0080 0094 1474
4.1	0	282	1.170	2.75	1.34	1.41	0098	0031	0098 0115 1838
4.4	0	282	1.170	2.92	1.34	1.58	0110	0031	0110 0129 1930
5.4	0	282	1.170	3.05	1.34	1.71	0119	0031	0119 0140 2197
6.2	0	282	1.170	3.08	1.34	1.74	0121	0031	0121 0142 2377
7.3	0	282	1.170	3.14	1.34	1.80	0125	0031	0125 0147 2590
8.9	0	282	1.170	3.07	1.34	1.73	0120	0031	0120 0141 2848
11.1	0	282	1.170	2.95	1.34	1.61	0112	0031	0112 0132 3136
11.9	0	282	1.170	2.75	1.34	1.41	0098	0031	0098 0115 3227
12.4	0	282	1.170	2.58	1.34	1.24	0086	0031	0086 0101 3280
13.0	0	282	1.170	2.39	1.34	1.05	0073	0031	0073 0086 3342
15.4	0	282	1.170	2.22	1.34	.88	0061	0031	0061 0072 3563
17.5	0	282	1.170	2.06	1.34	.72	0050	0031	0050 0059 3729
25.1	0	282	1.170	1.88	1.34	.54	0038	0031	0038 0045 4199
27.4	0	282	1.170	1.87	1.34	.53	0037	0031	0037 0043 4313
33.6	0	282	1.170	1.74	1.34	.40	0028	0031	0028 0033 4579
38.4	0	282	1.170	1.69	1.34	.35	0024	0031	0024 0028 4753
44.6	0	282	1.170	1.65	1.34	.31	0022	0031	0022 0026 4948
54.0	0	282	1.170	1.64	1.34	.30	0021	0031	0021 0025 5197
64.0	0	282	1.170	1.59	1.34	.25	0017	0031	0017 0020 5419
84.0	0	282	1.170	1.59	1.34	.25	0017	0031	0017 0020 5773
91.0	0	282	1.170	1.59	1.34	.25	0017	0031	0017 0020 5877

TABLE NO. 2
 TABULATION OF ORIGINAL DATA POINTS FOR
 ABSORPTION OF SOUND IN AIR VERSUS RELATIVE HUMIDITY
 AT 0 DEGREES CENTIGRADE

TABLE NO. 2
 TABULATION OF ORIGINAL DATA POINTS FOR
 ABSORPTION OF SOUND IN AIR VERSUS RELATIVE HUMIDITY
 AT 0 DEGREES CENTIGRADE

* last column employed in computer plotting only.

TABLE 3
TABULATION OF ORIGINAL DATA POINTS FOR
ABSORPTION OF SOUND IN AIR VERSUS RELATIVE HUMIDITY
AT -20 DEGREES CENTIGRADE

R.H.	TEMP	FREQ	LAMDA	AIR	AIR	AIR	AIR	MU	3000*
				+ DEG	ONLY	ONLY	CLAS	MOL	LOG
PRCT	CENT	CPS	METRS	WALL	WALL				RH
1	2	3	4						
1234567890	1234567890	1234567890	1234567890	1234567890	1234567890	1234567890	1234567890	1234567890	1234567890
1.0	-20	272	1.170	1.40	1.21	.19	0014	0029	0014
17.7	-20	272	1.170	1.65	1.21	.44	0032	0029	0032
22.2	-20	272	1.170	1.90	1.21	.69	0050	0029	0050
29.3	-20	272	1.170	2.10	1.21	.89	0064	0029	0064
31.1	-20	272	1.170	2.16	1.21	.95	0069	0029	0069
37.0	-20	272	1.170	2.16	1.21	.95	0069	0029	0069
42.8	-20	272	1.170	2.17	1.21	.91	0066	0029	0066
46.7	-20	272	1.170	2.05	1.21	.84	0061	0029	0061
58.0	-20	272	1.170	1.95	1.21	.74	0053	0029	0053
66.5	-20	272	1.170	1.86	1.21	.65	0047	0029	0047
72.0	-20	272	1.170	1.79	1.21	.58	0042	0029	0042
78.0	-20	272	1.170	1.73	1.21	.52	0038	0029	0038
80.0	-20	272	1.170	1.71	1.21	.50	0036	0029	0036
98.0	-20	272	1.170	1.68	1.21	.47	0034	0029	0034
1.0	-20	468	.680	1.19	.99	.20	0014	0086	0013
17.7	-20	468	.680	1.45	.99	.46	0033	0086	0032
22.2	-20	468	.680	1.78	.99	.79	0057	0086	0056
29.3	-20	468	.680	2.04	.99	1.05	0076	0086	0075
31.1	-20	468	.680	2.34	.99	1.35	0098	0086	0097
37.0	-20	468	.680	2.55	.99	1.56	0113	0086	0112
42.8	-20	468	.680	2.63	.99	1.64	0118	0086	0117
46.7	-20	468	.680	2.64	.99	1.65	0119	0086	0118
58.0	-20	468	.680	2.62	.99	1.63	0118	0086	0117
66.5	-20	468	.680	2.53	.99	1.54	0111	0086	0110
72.0	-20	468	.680	2.42	.99	1.43	0103	0086	0102
78.0	-20	468	.680	2.31	.99	1.32	0095	0086	0094
80.0	-20	468	.680	2.25	.99	1.26	0091	0086	0090
98.0	-20	468	.680	2.10	.99	1.11	0080	0086	0079

* last column employed in computer plotting only.

TABLE 3
 TABULATION OF ORIGINAL DATA POINTS FOR
 ABSORPTION OF SOUND IN AIR VERSUS RELATIVE HUMIDITY
 AT -20 DEGREES CENTIGRAD

R.H. PRCT	TEMP DEG CENT	FREQ METRS	LAMDA	AIR	AIR	AIR	AIR	MU	3000*
				+ WALL	ONLY WALL	ONLY CLAS	CLAS MOL		LOG
				DB/S	DB/S	DB/S	/M	/M	RH
12345678901234567890123456789012345678901234567890123456789012345678	12345678901234567890123456789012345678901234567890123456789012345678	12345678901234567890123456789012345678901234567890123456789012345678	12345678901234567890123456789012345678901234567890123456789012345678						
1.0	-20	660	.482	2.00	1.86	.14	0010	0170	0008 0004 0
17.7	-20	660	.482	2.32	1.86	.46	0033	0170	0031 0015 3744
22.2	-20	660	.482	2.66	1.86	.80	0058	0170	0056 0027 4039
29.3	-20	660	.482	2.98	1.86	1.12	0081	0170	0079 0038 4401
31.1	-20	660	.482	3.40	1.86	1.54	0111	0170	0109 0053 4478
37.0	-20	660	.482	3.73	1.86	1.87	0135	0170	0133 0064 4705
42.8	-20	660	.482	3.99	1.86	2.13	0154	0170	0152 0073 4894
46.7	-20	660	.482	4.14	1.86	2.28	0165	0170	0163 0079 5008
58.0	-20	660	.482	4.25	1.86	2.39	0173	0170	0171 0083 5290
66.5	-20	660	.482	4.23	1.86	2.37	0171	0170	0169 0082 5468
72.0	-20	660	.482	4.20	1.86	2.34	0169	0170	0167 0081 5572
78.0	-20	660	.482	4.08	1.86	2.22	0160	0170	0158 0076 5676
80.0	-20	660	.482	4.04	1.86	2.18	0157	0170	0155 0075 5709
98.0	-20	660	.482	3.96	1.86	2.10	0152	0170	0150 0072 5974
1.0	-20	853	.373	3.62	3.58	.04	0003	0288	0000 0000 0
17.7	-20	853	.373	3.82	3.58	.24	0017	0288	0014 0005 3744
22.2	-20	853	.373	4.05	3.58	.47	0034	0288	0031 0012 4039
29.3	-20	853	.373	4.38	3.58	.80	0058	0288	0055 0021 4401
31.1	-20	853	.373	4.83	3.58	1.25	0090	0288	0087 0033 4478
37.0	-20	853	.373	5.27	3.58	1.69	0122	0288	0119 0045 4705
42.8	-20	853	.373	5.67	3.58	2.09	0151	0288	0148 0055 4894
46.7	-20	853	.373	5.92	3.58	2.34	0169	0288	0166 0062 5008
58.0	-20	853	.373	6.20	3.58	2.62	0189	0288	0186 0070 5290
66.5	-20	853	.373	6.20	3.58	2.62	0189	0288	0186 0070 5468
72.0	-20	853	.373	6.35	3.58	2.77	0200	0288	0197 0074 5572
78.0	-20	853	.373	6.29	3.58	2.71	0196	0288	0193 0072 5676
80.0	-20	853	.373	6.21	3.58	2.63	0190	0288	0187 0070 5709
98.0	-20	853	.373	6.25	3.58	2.67	0193	0288	0190 0071 5974

* last column employed in computer plotting only.

TABLE 4

TABULATION OF ORIGINAL DATA POINTS FOR
 ABSORPTION OF SOUND IN AIR VERSUS RELATIVE HUMIDITY
 AT -40 DEGREES CENTIGRADE

R.H.	TEMP	FREQ	LAMDA	AIR	AIR	AIR	AIR	AIR	MU	3000*
				+	ONLY	ONLY	CLAS	MOL		LOG
PRCT	CENT	CPS	METRS	DEG	WALL	WALL				RH
1	2	3	4		5	6				
12345678901234567890123456789012345678901234567890123456789012345678										
9.0	40	260	1.170	1.34 1.31	.13 0010	0083 0009	0007 2680			
32.0	40	260	1.170	1.33 1.31	.12 0009	0083 0008	0006 4510			
43.0	40	260	1.170	1.37 1.31	.16 0012	0083 0011	0008 4910			
74.0	40	260	1.170	1.39 1.31	.18 0013	0083 0012	0009 5610			
88.0	40	260	1.170	1.38 1.31	.17 0013	0083 0012	0009 5830			
97.0	40	260	1.170	1.40 1.31	.19 0014	0083 0013	0010 5970			
9.0	40	447	.680	1.15 .95	.20 0015	0164 0013	0010 2860			
32.0	40	447	.680	1.12 .95	.17 0013	0164 0011	0009 4510			
43.0	40	447	.680	1.14 .95	.19 0014	0164 0013	0010 4910			
74.0	40	447	.680	1.17 .95	.22 0015	0164 0014	0011 5610			
88.0	40	447	.680	1.17 .95	.23 0016	0164 0014	0011 5830			
97.0	40	447	.680	1.18 .95	.24 0017	0164 0015	0012 5970			
9.0	40	631	.482	1.82 1.71	.11 0008	0277 0005	0004 2860			
32.0	40	631	.482	1.82 1.71	.11 0008	0277 0005	0004 4510			
43.0	40	631	.482	1.83 1.71	.12 0009	0277 0006	0004 4910			
74.0	40	631	.482	1.87 1.71	.16 0012	0277 0009	0006 5610			
88.0	40	631	.482	1.87 1.71	.16 0012	0277 0009	0006 5830			
97.0	40	631	.482	1.87 1.71	.16 0012	0277 0009	0006 5970			

* last column employed in computer plotting only.

TABLE NO. 5
 TABULATION OF DATA POINTS FOR
 ABSORPTION OF SOUND IN DRY NITROGEN
 AT 20 DEGREES CENTIGRADE
 FOR THE COMPUTATION OF WALL LOSSES

MICROPHN	1111111111111111	2222222222222222	2222222222222222	111111111111				
TEMP	+20C	0C	-20C	-40C				
MODE	F	R	F	R	F	R	F	R
11	139	2.14	134	1.88	129	1.92	---	---
01	298	1.39	288	1.34	277	1.28	265	1.21
02	512	1.20	495	1.10	475	1.02	456	0.95
03	724	2.06	698	2.62	673	1.93	644	1.71
04	933	4.31	900	4.00	867	3.49	830	3.13

TABLE 6A-----400 MM PRESSURE
 TABULATION OF ORIGINAL DATA POINTS FOR
 ABSORPTION OF SOUND IN AIR VERSUS RELATIVE HUMIDITY
 AT 20 DEGREES CENTIGRADE

* last column employed in computer plotting only.

TABLE 6A-----400 MM PRESSURE
 TABULATION OF ORIGINAL DATA POINTS FOR:
 ABSORPTION OF SOUND IN AIR VERSUS RELATIVE HUMIDITY
 AT 20 DEGREES CENTIGRADE

R.H. PRCT	TEMP CENT	FREQ CPS	LAMDA METRS	AIR	AIR	AIR	AIR	MU	3000*
				+	ONLY	ONLY	CLAS	MOL	LOG
				DEG	WALL	WALL	DB/S	DB/S	RH
1	2	3	4	5	6				
12345678901234567890123456789012345678901234567890123456789012345678									
1.5	20	504	.681 400	5.52	1.68	3.84	0258	0180	0256 0174 528
1.8	20	504	.681 400	6.33	1.68	4.65	0312	0180	0310 0211 766
1.9	20	504	.681 400	6.42	1.68	4.74	0318	0180	0316 0215 836
2.0	20	504	.681 400	6.23	1.68	4.55	0305	0180	0303 0206 903
2.2	20	504	.681 400	5.76	1.68	4.08	0274	0180	0272 0185 1027
2.8	20	504	.681 400	5.17	1.68	3.49	0234	0180	0232 0158 1341
4.8	20	504	.681 400	4.65	1.68	2.97	0199	0180	0197 0134 2044
5.2	20	504	.681 400	4.13	1.68	2.45	0164	0180	0162 0110 2148
5.8	20	504	.681 400	3.66	1.68	1.98	0133	0180	0131 0089 2290
6.7	20	504	.681 400	3.28	1.68	1.60	0107	0180	0105 0072 2478
8.0	20	504	.681 400	2.94	1.68	1.26	0085	0180	0083 0057 2709
10.0	20	504	.681 400	2.68	1.68	1.00	0067	0180	0065 0044 3000
12.2	20	504	.681 400	2.55	1.68	.87	0058	0180	0056 0038 3259
13.7	20	504	.681 400	2.51	1.68	.83	0056	0180	0054 0037 3410
18.5	20	504	.681 400	2.48	1.68	.80	0054	0180	0052 0035 3802
23.1	20	504	.681 400	2.45	1.68	.77	0052	0180	0050 0034 4091
26.8	20	504	.681 400	2.47	1.68	.79	0053	0180	0051 0035 4284
33.0	20	504	.681 400	2.50	1.68	.82	0055	0180	0053 0036 4556
37.0	20	504	.681 400	2.51	1.68	.83	0056	0180	0054 0037 4705
1.5	20	712	.482 400	7.30	2.92	4.38	0294	0368	0290 0140 528
1.8	20	712	.482 400	8.90	2.92	5.98	0401	0368	0397 0191 766
1.9	20	712	.482 400	9.38	2.92	6.46	0434	0368	0430 0207 836
2.0	20	712	.482 400	9.70	2.92	6.78	0455	0368	0451 0217 903
2.2	20	712	.482 400	9.48	2.92	6.56	0440	0368	0436 0210 1027
2.8	20	712	.482 400	9.00	2.92	6.08	0408	0368	0404 0195 1341
4.8	20	712	.482 400	8.32	2.92	5.40	0362	0368	0358 0173 2044
5.2	20	712	.482 400	7.51	2.92	4.59	0308	0368	0304 0147 2148
5.8	20	712	.482 400	6.75	2.92	3.83	0257	0368	0253 0122 2290
6.7	20	712	.482 400	6.00	2.92	3.08	0207	0368	0203 0098 2478
8.0	20	712	.482 400	5.33	2.92	2.41	0162	0368	0158 0076 2709
10.0	20	712	.482 400	4.80	2.92	1.88	0126	0368	0122 0059 3000
12.2	20	712	.482 400	4.52	2.92	1.60	0107	0368	0103 0050 3259
13.7	20	712	.482 400	4.38	2.92	1.46	0098	0368	0094 0045 3410
18.5	20	712	.482 400	4.21	2.92	1.29	0087	0368	0083 0040 3802
23.1	20	712	.482 400	4.08	2.92	1.16	0078	0368	0074 0036 4091
26.8	20	712	.482 400	4.07	2.92	1.15	0077	0368	0073 0035 4284
33.0	20	712	.482 400	4.04	2.92	1.12	0075	0368	0071 0034 4556
37.0	20	712	.482 400	4.07	2.92	1.15	0077	0368	0073 0035 4705

* last column employed in computer plotting only.

TABLE 6A-----400 MM PRESSURE
 TABULATION OF ORIGINAL DATA POINTS FOR
 ABSORPTION OF SOUND IN AIR VERSUS RELATIVE HUMIDITY
 AT 20 DEGREES CENTIGRADE

R.H.	TEMP	FREQ	LAMDA	AIR	AIR	AIR	AIR	MU	3000*			
				+ WALL	ONLY WALL	ONLY CLAS	MOL		LOG			
PRCT	CENT	CPS	METRS	DB/S	DB/S	DB/S	/M	/M	RH			
1	2	3	4	5	6							
1234567890	1234567890	1234567890	1234567890	1234567890	1234567890	1234567890	1234567890	1234567890	12345678			
1.5	20	918	.374	400	11.00	6.98	4.02	0270	0618	0264	0099	528
1.8	20	918	.374	400	13.00	6.98	6.02	0404	0618	0398	0149	766
1.9	20	918	.374	400	13.60	6.98	6.62	0444	0618	0438	0164	836
2.0	20	918	.374	400	14.70	6.98	7.72	0518	0618	0512	0191	903
2.2	20	918	.374	400	14.70	6.98	7.72	0518	0618	0512	0191	1027
2.8	20	918	.374	400	14.70	6.98	7.72	0518	0618	0512	0191	1341
4.8	20	918	.374	400	14.10	6.98	7.12	0478	0618	0472	0176	2044
5.2	20	918	.374	400	13.30	6.98	6.32	0424	0618	0418	0156	2148
5.8	20	918	.374	400	12.10	6.98	5.12	0344	0618	0338	0126	2290
6.7	20	918	.374	400	11.20	6.98	4.22	0283	0618	0277	0104	2478
8.0	20	918	.374	400	10.20	6.98	3.22	0216	0618	0210	0079	2709
10.0	20	918	.374	400	9.20	6.98	2.22	0149	0618	0143	0053	3000
12.2	20	918	.374	400	8.79	6.98	1.81	0122	0618	0116	0043	3259
13.7	20	918	.374	400	8.79	6.98	1.81	0122	0618	0116	0043	3410
18.5	20	918	.374	400	8.53	6.98	1.55	0104	0618	0098	0037	3802
23.1	20	918	.374	400	8.30	6.98	1.32	0089	0618	0083	0031	4091
26.8	20	918	.374	400	8.03	6.98	1.05	0070	0618	0064	0024	4284
33.0	20	918	.374	400	8.11	6.98	1.13	0076	0618	0070	0026	4556
37.0	20	918	.374	400	8.11	6.98	1.13	0076	0618	0070	0026	4705

* last column employed in computer plotting only.

TABLE 6B----200 MM PRESSURE
 TABULATION OF ORIGINAL DATA POINTS FOR
 ABSORPTION OF SOUND IN AIR VERSUS RELATIVE HUMIDITY
 AT 20 DEGREES CENTIGRADE

R.H. PRCT	TEMP CENT	FREQ CPS	LAMDA METRS	AIR	AIR	AIR	AIR	MU	3000*			
				+	ONLY	ONLY	CLAS	MOL	LOG			
				DEG	WALL	WALL	DB/S	DB/S	RH			
1	2	3	4	5	6							
12345678901234567890123456789012345678901234567890123456789012345678												
1.4	20	136	2.520	200	3.52	3.05	.47	0032	0027	0032	0081	438
1.5	20	136	2.520	200	3.59	3.05	.54	0036	0027	0036	0091	528
1.7	20	136	2.520	200	3.36	3.05	.31	0021	0027	0021	0053	691
1.8	20	136	2.520	200	3.30	3.05	.25	0017	0027	0017	0043	766
1.9	20	136	2.520	200	3.33	3.05	.28	0019	0027	0019	0048	836
2.1	20	136	2.520	200	3.30	3.05	.25	0017	0027	0017	0043	967
2.4	20	136	2.520	200	3.20	3.05	.15	0010	0027	0010	0025	1141
3.1	20	136	2.520	200	3.10	3.05	.05	0003	0027	0003	0008	1474
4.7	20	136	2.520	200	3.13	3.05	.08	0005	0027	0005	0013	2016
6.4	20	136	2.520	200	3.05	3.05	.00	0000	0027	0000	0000	2419
8.3	20	136	2.520	200	3.11	3.05	.06	0004	0027	0004	0010	2757
16.7	20	136	2.520	200	3.22	3.05	.17	0011	0027	0011	0028	3668
22.0	20	136	2.520	200	3.23	3.05	.18	0012	0027	0012	0030	4027
26.3	20	136	2.520	200	3.26	3.05	.21	0014	0027	0014	0035	4260
1.4	20	293	1.170	200	4.58	2.38	2.20	0148	0122	0147	0172	438
1.5	20	293	1.170	200	4.28	2.38	1.90	0128	0122	0127	0149	528
1.7	20	293	1.170	200	3.78	2.38	1.40	0094	0122	0093	0109	691
1.8	20	293	1.170	200	3.63	2.38	1.25	0084	0122	0083	0097	766
1.9	20	293	1.170	200	3.48	2.38	1.10	0074	0122	0073	0086	836
2.1	20	293	1.170	200	3.31	2.38	.93	0062	0122	0061	0071	967
2.4	20	293	1.170	200	3.23	2.38	.85	0057	0122	0056	0066	1141
3.1	20	293	1.170	200	3.10	2.38	.72	0048	0122	0047	0055	1474
4.7	20	293	1.170	200	2.95	2.38	.57	0038	0122	0037	0043	2016
6.4	20	293	1.170	200	2.81	2.38	.43	0029	0122	0028	0033	2419
8.3	20	293	1.170	200	2.72	2.38	.34	0023	0122	0022	0026	2757
16.7	20	293	1.170	200	2.74	2.38	.36	0024	0122	0023	0027	3668
22.0	20	293	1.170	200	2.77	2.38	.39	0026	0122	0025	0029	4027
26.3	20	293	1.170	200	2.83	2.38	.45	0030	0122	0029	0034	4260

* last column employed in computer plotting only.

TABLE 6B----200 MM PRESSURE
 TABULATION OF ORIGINAL DATA POINTS FOR
 ABSORPTION OF SOUND IN AIR VERSUS RELATIVE HUMIDITY
 AT 20 DEGREES CENTIGRADE

R.H.	TEMP	FREQ	LAMDA	AIR	AIR	AIR	AIR	MU	3000*
				+ WALL	ONLY WALL	ONLY	CLAS	MOL	LOG
PRCT	CENT	CPS	METRS	DB/S	DB/S	DB/S	/M	/M	RH
1	2	3	4	5	6				
123456789012345678901234567890123456789012345678901234567890123456789012345678									
1.4	20	504	.681	200	7.12	2.40	4.72	0317	0360 0313 0213 438
1.5	20	504	.681	200	6.84	2.40	4.44	0298	0360 0294 0200 528
1.7	20	504	.681	200	6.08	2.40	3.68	0247	0360 0243 0165 691
1.8	20	504	.681	200	5.80	2.40	3.40	0228	0360 0224 0153 766
1.9	20	504	.681	200	5.50	2.40	3.10	0208	0360 0204 0139 836
2.1	20	504	.681	200	5.10	2.40	2.70	0181	0360 0177 0121 967
2.4	20	504	.681	200	4.81	2.40	2.41	0162	0360 0158 0108 1141
3.1	20	504	.681	200	4.42	2.40	2.02	0136	0360 0132 0090 1474
4.7	20	504	.681	200	4.00	2.40	1.60	0107	0360 0103 0070 2016
6.4	20	504	.681	200	3.49	2.40	1.09	0073	0360 0069 0047 2419
8.3	20	504	.681	200	3.18	2.40	.78	0052	0360 0048 0033 2757
16.7	20	504	.681	200	3.02	2.40	.62	0042	0360 0038 0026 3668
22.0	20	504	.681	200	3.03	2.40	.63	0042	0360 0038 0026 4027
26.3	20	504	.681	200	3.11	2.40	.71	0048	0360 0044 0030 4260
-	1.4	20	712	.482	200	10.60	4.14	6.46	0434 0736 0427 0206 438
1.5	20	712	.482	200	10.70	4.14	6.56	0440	0736 0433 0209 528
1.7	20	712	.482	200	10.20	4.14	6.06	0407	0736 0400 0193 691
1.8	20	712	.482	200	10.00	4.14	5.86	0393	0736 0386 0186 766
1.9	20	712	.482	200	9.59	4.14	5.45	0366	0736 0359 0173 836
2.1	20	712	.482	200	9.04	4.14	4.90	0329	0736 0322 0155 967
2.4	20	712	.482	200	8.63	4.14	4.49	0301	0736 0294 0142 1141
3.1	20	712	.482	200	7.97	4.14	3.83	0257	0736 0250 0121 1474
4.7	20	712	.482	200	7.23	4.14	3.09	0207	0736 0200 0096 2016
6.4	20	712	.482	200	6.20	4.14	2.06	0138	0736 0131 0063 2419
8.3	20	712	.482	200	5.58	4.14	1.44	0097	0736 0090 0043 2757
16.7	20	712	.482	200	5.08	4.14	.94	0063	0736 0056 0027 3668
22.0	20	712	.482	200	5.02	4.14	.88	0059	0736 0052 0025 4027
26.3	20	712	.482	200	5.09	4.14	.95	0064	0736 0057 0027 4260

* last column employed in computer plotting only.

TABLE 6B----200 MM PRESSURE
 TABULATION OF ORIGINAL DATA POINTS FOR
 ABSORPTION OF SOUND IN AIR VERSUS RELATIVE HUMIDITY
 AT 20 DEGREES CENTIGRADE

R.H.	TEMP	FREQ	LAMDA	AIR	AIR	AIR	AIR	MU	3000*
				+ WALL	ONLY WALL	ONLY	CLAS	MOL	LOG
PRCT	DEG	CENT	CPS	DB/S	DB/S	DB/S	/M	/M	RH
	1	2		3	4		5		6
12345678901234567890123456789012345678901234567890123456789012345678									
1.4	20	918	•374	200	15.20	8.02	7.18	0482	1236 0470 0176 438
1.5	20	918	•374	200	15.80	8.02	7.78	0522	1236 0510 0191 528
1.7	20	918	•374	200	15.70	8.02	7.68	0516	1236 0504 0188 691
1.8	20	918	•374	200	16.00	8.02	7.98	0536	1236 0524 0196 766
1.9	20	918	•374	200	15.50	8.02	7.48	0502	1236 0490 0183 836
2.1	20	918	•374	200	14.70	8.02	6.68	0448	1236 0436 0163 967
2.4	20	918	•374	200	14.40	8.02	6.38	0428	1236 0416 0156 1141
3.1	20	918	•374	200	13.40	8.02	5.38	0361	1236 0349 0130 1474
4.7	20	918	•374	200	12.60	8.02	4.58	0307	1236 0295 0110 2016
6.4	20	918	•374	200	11.00	8.02	2.98	0200	1236 0188 0070 2419
8.3	20	918	•374	200	10.00	8.02	1.98	0133	1236 0121 0045 2757
16.7	20	918	•374	200	9.20	8.02	1.18	0079	1236 0067 0025 3668
22.0	20	918	•374	200	9.04	8.02	1.02	0068	1236 0056 0021 4027
26.3	20	918	•374	200	9.00	8.02	.98	0066	1236 0054 0020 4260

* last column employed in computer plotting only.

TABLE NO. 7
 TABULATION OF ORIGINAL DATA POINTS FOR
 ABSORPTION OF SOUND IN DRY NITROGEN
 AT 20 DEGREES CENTIGRADE

SPHERE CONTAINS TWO MICROPHONES+++NOMINAL VALUES OF FREQUENCY ARE LISTED

FREQUENCY	139 CPS	298 CPS	512 CPS	724 CPS	933 CPS
PRESSURE	R IN DB/S				
765 MM	2.14	1.39	1.20	2.06	4.31
493 MM	2.31	1.61	1.50	2.66	6.23
399 MM	2.42	1.75	1.68	2.92	6.98
298 MM	2.68	1.99	1.94	3.36	7.60
193 MM	3.08	2.41	2.44	4.20	8.05
148 MM	3.55	2.77	2.82	4.78	7.98

TABLE NO. 8
 TABULATION OF SMOOTHED DATA POINTS FOR
 ABSORPTION OF SOUND IN AIR VERSUS RELATIVE HUMIDITY
 AT 20 DEGREES CENTIGRADE

R.H.	TEMP	FREQ	LAMDA	AIR	AIR	AIR	AIR	MU	3000*		
				AIR	AIR	AIR	AIR	MU	LOG		
PRCT	CENT	CPS	METRS	WALL	WALL	ONLY	ONLY	CLAS	RH		
1	2	3	4	DB/S	DB/S	DB/S	/M	/M	6		
1234567890	1234567890	1234567890	1234567890	1234567890	1234567890	1234567890	1234567890	1234567890	1234567890		
1.0	20	136	2.520	2.54	1.99	.55	0009	0007	0009	0093	0000
1.2	20	136	2.520	3.18	1.99	1.19	0085	0007	0085	0202	238
1.4	20	136	2.520	3.08	1.99	1.09	0083	0007	0083	0184	438
1.8	20	136	2.520	2.76	1.99	.77	0074	0007	0074	0131	766
2.1	20	136	2.520	2.64	1.99	.65	0065	0007	0065	0111	967
2.7	20	136	2.520	2.50	1.99	.51	0048	0007	0048	0086	1294
3.8	20	136	2.520	2.36	1.99	.37	0032	0007	0032	0063	1739
5.1	20	136	2.520	2.30	1.99	.31	0023	0007	0023	0053	2123
6.1	20	136	2.520	2.26	1.99	.27	0020	0007	0020	0045	2356
6.2	20	136	2.520	2.36	1.99	.37	0019	0007	0019	0063	2377
7.2	20	136	2.520	2.32	1.99	.33	0017	0007	0017	0056	2572
7.4	20	136	2.520	2.26	1.99	.27	0017	0007	0017	0045	2608
8.2	20	136	2.520	2.35	1.99	.36	0017	0007	0017	0061	2741
9.0	20	136	2.520	2.22	1.99	.23	0017	0007	0017	0038	2863
10.1	20	136	2.520	2.26	1.99	.27	0017	0007	0017	0045	3013
13.3	20	136	2.520	2.38	1.99	.39	0017	0007	0017	0066	3372
16.3	20	136	2.520	2.35	1.99	.36	0017	0007	0017	0061	3637
20.0	20	136	2.520	2.36	1.99	.37	0017	0007	0017	0063	3903
25.4	20	136	2.520	2.23	1.99	.24	0017	0007	0017	0040	4215
31.0	20	136	2.520	2.22	1.99	.23	0017	0007	0017	0038	4474
39.0	20	136	2.520	2.22	1.99	.23	0017	0007	0017	0038	4773
1.2	20	293	1.170	4.05	1.36	2.69	0174	0032	0174	0212	238
1.4	20	293	1.170	4.17	1.36	2.81	0185	0032	0185	0221	438
1.8	20	293	1.170	4.06	1.36	2.70	0183	0032	0183	0212	766
2.1	20	293	1.170	3.70	1.36	2.34	0170	0032	0170	0184	967
2.7	20	293	1.170	3.18	1.36	1.82	0137	0032	0137	0143	1294
3.8	20	293	1.170	2.86	1.36	1.50	0092	0032	0092	0118	1739
5.1	20	293	1.170	2.43	1.36	1.07	0065	0032	0065	0084	2123
6.1	20	293	1.170	2.22	1.36	.86	0054	0032	0054	0068	2356
6.2	20	293	1.170	2.22	1.36	.86	0052	0032	0052	0068	2377
7.2	20	293	1.170	2.12	1.36	.76	0045	0032	0045	0060	2572
7.4	20	293	1.170	2.09	1.36	.73	0043	0032	0043	0057	2608
8.2	20	293	1.170	2.07	1.36	.71	0039	0032	0039	0056	2741
9.0	20	293	1.170	2.01	1.36	.65	0037	0032	0037	0052	2863
10.1	20	293	1.170	2.03	1.36	.67	0037	0032	0037	0053	3013
13.3	20	293	1.170	1.99	1.36	.63	0037	0032	0037	0049	3372
16.3	20	293	1.170	1.98	1.36	.62	0037	0032	0037	0049	3637
20.0	20	293	1.170	1.98	1.36	.62	0037	0032	0037	0049	3903
25.4	20	293	1.170	1.97	1.36	.61	0037	0032	0037	0048	4215
31.0	20	293	1.170	1.98	1.36	.62	0037	0032	0037	0049	4474
39.0	20	293	1.170	1.96	1.36	.60	0037	0032	0037	0047	4773

* last column employed in computer plotting only.

TABLE NO. 8
 TABULATION OF SMOOTHED DATA POINTS FOR
 ABSORPTION OF SOUND IN AIR VERSUS RELATIVE HUMIDITY
 AT 20 DEGREES CENTIGRADE

* last column employed in computer plotting only.

TABLE NO. 8
 TABULATION OF SMOOTHED DATA POINTS FOR
 ABSORPTION OF SOUND IN AIR VERSUS RELATIVE HUMIDITY
 AT 20 DEGREES CENTIGRADE

R.H.	TEMP	FREQ	LAMDA	AIR	AIR	AIR	AIR	MU	3000*		
				+ DEG	WALL	WALL	ONLY	ONLY	CLAS	MOL	LOG
				PRCT	CENT	CPS	METRS	DB/S	DB/S	DB/S	/M
1	2	3	4	5	6						
1234567890	1234567890	1234567890	1234567890	1234567890	1234567890	1234567890	1234567890	1234567890	1234567890		
.1	20	918	.374	5.22	4.50	.72	0027	0312	0024	0017	0000
1.2	20	918	.374	8.55	4.50	4.05	0291	0312	0288	0101	238
1.4	20	918	.374	9.26	4.50	4.76	0333	0312	0330	0119	438
1.8	20	918	.374	11.00	4.50	6.50	0417	0312	0414	0162	766
2.1	20	918	.374	12.40	4.50	7.90	0489	0312	0486	0197	967
2.7	20	918	.374	13.35	4.50	8.85	0585	0312	0582	0221	1294
3.8	20	918	.374	13.20	4.50	8.70	0591	0312	0588	0217	1739
5.1	20	918	.374	11.70	4.50	7.20	0483	0312	0480	0179	2123
6.1	20	918	.374	10.35	4.50	5.85	0405	0312	0402	0146	2356
6.2	20	918	.374	10.30	4.50	5.80	0389	0312	0386	0144	2377
7.2	20	918	.374	9.48	4.50	4.98	0327	0312	0324	0124	2572
7.4	20	918	.374	9.26	4.50	4.76	0315	0312	0312	0119	2608
8.2	20	918	.374	8.85	4.50	4.35	0285	0312	0282	0108	2741
9.0	20	918	.374	8.33	4.50	3.83	0255	0312	0252	0095	2863
10.1	20	918	.374	8.25	4.50	3.75	0225	0312	0222	0093	3013
13.3	20	918	.374	7.25	4.50	2.75	0165	0312	0162	0068	3372
16.3	20	918	.374	6.90	4.50	2.40	0135	0312	0132	0059	3637
20.0	20	918	.374	6.50	4.50	2.00	0123	0312	0120	0049	3903
25.4	20	918	.374	6.28	4.50	1.78	0123	0312	0120	0043	4215
31.0	20	918	.374	6.23	4.50	1.73	0123	0312	0120	0042	4474
39.0	20	918	.374	6.28	4.50	1.78	0123	0312	0120	0043	4773
39.5	20	918	.374	6.03	4.50	1.53	0123	0312	0120	0037	4790

* last column employed in computer plotting only.

TABLE NO. 9
 TABULATION OF SMOOTHED DATA POINTS FOR
 ABSORPTION OF SOUND IN AIR VERSUS RELATIVE HUMIDITY
 AT 0 DEGREES CENTIGRADE

R.H.	TEMP	FREQ	LAMDA	AIR	AIR	AIR	AIR	MU	3000*
				+ .	ONLY	ONLY	CLAS	MOL	LOG
PRCT	CENT	CPS	METRS	WALL	WALL				RH
1	2	3	4	DB/S	DB/S	DB/S	/M	/M	6
123456789012345678901234567890123456789012345678901234567890123456789012345678	123456789012345678901234567890123456789012345678901234567890123456789012345678	123456789012345678901234567890123456789012345678901234567890123456789012345678	123456789012345678901234567890123456789012345678901234567890123456789012345678	123456789012345678901234567890123456789012345678901234567890123456789012345678	123456789012345678901234567890123456789012345678901234567890123456789012345678	123456789012345678901234567890123456789012345678901234567890123456789012345678	123456789012345678901234567890123456789012345678901234567890123456789012345678	123456789012345678901234567890123456789012345678901234567890123456789012345678	123456789012345678901234567890123456789012345678901234567890123456789012345678
3.1	0	132	2.520	2.60	1.88	.72	0053	0007	0053 0126 1474
4.1	0	132	2.520	2.67	1.88	.79	0060	0007	0060 0138 1838
4.4	0	132	2.520	2.67	1.88	.79	0060	0007	0060 0138 1930
5.4	0	132	2.520	2.64	1.88	.76	0058	0007	0058 0133 2197
6.2	0	132	2.520	2.53	1.88	.65	0053	0007	0053 0113 2377
7.3	0	132	2.520	2.55	1.88	.67	0046	0007	0046 0118 2590
8.9	0	132	2.520	2.34	1.88	.46	0037	0007	0037 0080 2848
11.1	0	132	2.520	2.37	1.88	.49	0028	0007	0028 0085 3136
11.9	0	132	2.520	2.26	1.88	.38	0026	0007	0026 0065 3227
12.4	0	132	2.520	2.17	1.88	.29	0025	0007	0025 0050 3280
13.0	0	132	2.520	2.10	1.88	.22	0023	0007	0023 0038 3342
15.4	0	132	2.520	2.10	1.88	.22	0019	0007	0019 0038 3563
17.5	0	132	2.520	2.07	1.88	.19	0017	0007	0017 0033 3729
25.1	0	132	2.520	2.04	1.88	.16	0012	0007	0012 0028 4199
27.4	0	132	2.520	2.02	1.88	.14	0012	0007	0012 0025 4313
33.6	0	132	2.520	2.02	1.88	.14	0012	0007	0012 0025 4579
38.4	0	132	2.520	1.97	1.88	.09	0012	0007	0012 0015 4753
44.6	0	132	2.520	2.02	1.88	.14	0012	0007	0012 0025 4948
54.0	0	132	2.520	1.99	1.88	.11	0012	0007	0012 0020 5197
64.0	0	132	2.520	2.03	1.88	.15	0012	0007	0012 0025 5419
84.0	0	132	2.520	1.99	1.88	.11	0012	0007	0012 0020 5773
91.0	0	132	2.520	2.00	1.88	.12	0012	0007	0012 0020 5877
1.1	0	282	1.170	1.63	1.34	.29	0001	0031	0001 0024 0000
3.1	0	282	1.170	2.49	1.34	1.15	0070	0031	0070 0094 1474
4.1	0	282	1.170	2.75	1.34	1.41	0089	0031	0089 0115 1838
4.4	0	282	1.170	2.92	1.34	1.58	0096	0031	0096 0129 1930
5.4	0	282	1.170	3.05	1.34	1.71	0106	0031	0106 0140 2197
6.2	0	282	1.170	3.08	1.34	1.74	0123	0031	0123 0142 2377
7.3	0	282	1.170	3.14	1.34	1.80	0123	0031	0123 0147 2590
8.9	0	282	1.170	3.07	1.34	1.73	0119	0031	0119 0141 2848
11.1	0	282	1.170	2.95	1.34	1.61	0101	0031	0101 0132 3136
11.9	0	282	1.170	2.75	1.34	1.41	0095	0031	0095 0115 3227
12.4	0	282	1.170	2.58	1.34	1.24	0091	0031	0091 0101 3280
13.0	0	282	1.170	2.39	1.34	1.05	0087	0031	0087 0086 3342
15.4	0	282	1.170	2.22	1.34	.88	0070	0031	0070 0072 3563
17.5	0	282	1.170	2.06	1.34	.72	0060	0031	0060 0059 3729
25.1	0	282	1.170	1.88	1.34	.54	0040	0031	0040 0045 4199
27.4	0	282	1.170	1.87	1.34	.53	0036	0031	0036 0043 4313
33.6	0	282	1.170	1.74	1.34	.40	0029	0031	0029 0033 4579
38.4	0	282	1.170	1.69	1.34	.35	0026	0031	0026 0028 4753
44.6	0	282	1.170	1.65	1.34	.31	0025	0031	0025 0026 4948
54.0	0	282	1.170	1.64	1.34	.30	0025	0031	0025 0025 5197
64.0	0	282	1.170	1.59	1.34	.25	0025	0031	0025 0020 5419
84.0	0	282	1.170	1.59	1.34	.25	0025	0031	0025 0020 5773
91.0	0	282	1.170	1.59	1.34	.25	0025	0031	0025 0020 5877

* last column employed in computer plotting only.

TABLE NO. 9
 TABULATION OF SMOOTHED DATA POINTS FOR
 ABSORPTION OF SOUND IN AIR VERSUS RELATIVE HUMIDITY
 AT 0 DEGREES CENTIGRADE

* last column employed in computer plotting only.

TABLE NO. 9
 TABULATION OF SMOOTHED DATA POINTS FOR
 ABSORPTION OF SOUND IN AIR VERSUS RELATIVE HUMIDITY
 AT 0 DEGREES CENTIGRADE

R.H.	TEMP	FREQ	LAMDA	AIR	AIR	AIR	AIR	MU	3000*
				+	ONLY	ONLY	CLAS	MOL	LOG
PRCT	CENT	CPS	METRS	DEG	WALL	WALL			RH
1	2			3	4		5		6
123456789012345678901234567890123456789012345678901234567890123456789012345678	.1	0	886	•374	4.57	4.00	.57	0006	0299 0004 0014 0000
	3.1	0	886	•374	5.58	4.00	1.58	0115	0299 0113 0040 1474
	4.1	0	886	•374	6.08	4.00	2.08	0146	0299 0144 0053 1838
	4.4	0	886	•374	6.13	4.00	2.13	0158	0299 0156 0054 1930
	5.4	0	886	•374	6.65	4.00	2.65	0193	0299 0191 0068 2197
	6.2	0	886	•374	7.10	4.00	3.10	0221	0299 0219 0080 2377
	7.3	0	886	•374	7.43	4.00	3.43	0252	0299 0250 0088 2590
	8.9	0	886	•374	8.29	4.00	4.29	0306	0299 0304 0110 2848
	11.1	0	886	•374	8.68	4.00	4.68	0372	0299 0370 0120 3136
	11.9	0	886	•374	9.40	4.00	5.40	0378	0299 0378 0139 3227
	12.4	0.	886	•374	9.78	4.00	5.78	0388	0299 0386 0149 3280
	13.0	0	886	•374	10.00	4.00	6.00	0392	0299 0390 0155 3342
	15.4	0	886	•374	9.67	4.00	5.67	0388	0299 0386 0146 3563
	17.5	0	886	•374	9.45	4.00	5.45	0372	0299 0370 0141 3729
	27.4	0	886	•374	8.36	4.00	4.36	0256	0299 0254 0112 4313
	33.6	0	886	•374	7.40	4.00	3.40	0197	0299 0195 0087 4579
	38.4	0	886	•374	6.96	4.00	2.96	0170	0299 0168 0076 4753
	44.6	0	886	•374	6.52	4.00	2.52	0143	0299 0141 0064 4948
	54.0	0	886	•374	6.28	4.00	2.28	0115	0299 0113 0058 5197
	64.0	0	886	•374	5.77	4.00	1.77	0099	0299 0097 0045 5419
	84.0	0	886	•374	5.42	4.00	1.42	0080	0299 0078 0036 5780
	91.0	0	886	•374	5.36	4.00	1.36	0080	0299 0078 0034 5870

* last column employed in computer plotting only.

TABLE NO. 10

TABULATION OF SMOOTHED DATA POINTS FOR
 ABSORPTION OF SOUND IN AIR VERSUS RELATIVE HUMIDITY
 AT -20 DEGREES CENTIGRADE.

R.H.	TEMP	FREQ	LAMDA	AIR	AIR	AIR	AIR	MU	3000*
				+ DEG	ONLY	ONLY	CLAS	MOL	LOG
PRCT	CENT	CPS	METRS	WALL	WALL				RH
1	2	3	4	5	6				
1234567890	1234567890	1234567890	1234567890	1234567890	1234567890	1234567890	1234567890	1234567890	1234567890
17.7 -20	272	1.170	1.65	1.21	.44	0044	0029	0044	0038 3744
22.2 -20	272	1.170	1.90	1.21	.69	0058	0029	0058	0059 4039
29.3 -20	272	1.170	2.10	1.21	.89	0066	0029	0066	0075 4401
31.1 -20	272	1.170	2.16	1.21	.95	0067	0029	0067	0081 4478
37.0 -20	272	1.170	2.16	1.21	.95	0067	0029	0067	0081 4705
42.8 -20	272	1.170	2.12	1.21	.91	0062	0029	0062	0077 4894
46.7 -20	272	1.170	2.05	1.21	.84	0058	0029	0058	0072 5008
58.0 -20	272	1.170	1.95	1.21	.74	0049	0029	0049	0062 5290
66.5 -20	272	1.170	1.86	1.21	.65	0044	0029	0044	0055 5468
72.0 -20	272	1.170	1.79	1.21	.58	0042	0029	0042	0049 5572
78.0 -20	272	1.170	1.73	1.21	.52	0039	0029	0039	0045 5676
80.0 -20	272	1.170	1.71	1.21	.50	0038	0029	0038	0042 5709
98.0 -20	272	1.170	1.68	1.21	.47	0032	0029	0032	0040 5974
17.7 -20	468	.680	1.45	.99	.46	0037	0086	0036	0022 3744
22.2 -20	468	.680	1.78	.99	.79	0056	0086	0055	0038 4039
29.3 -20	468	.680	2.04	.99	1.05	0090	0086	0089	0051 4401
31.1 -20	468	.680	2.34	.99	1.35	0098	0086	0097	0066 4478
37.0 -20	468	.680	2.55	.99	1.56	0113	0086	0112	0076 4705
42.8 -20	468	.680	2.63	.99	1.64	0119	0086	0118	0080 4894
46.7 -20	468	.680	2.64	.99	1.65	0121	0086	0120	0080 5008
58.0 -20	468	.680	2.62	.99	1.63	0118	0086	0117	0080 5290
66.5 -20	468	.680	2.53	.99	1.54	0110	0086	0109	0075 5468
72.0 -20	468	.680	2.42	.99	1.43	0103	0086	0102	0070 5572
78.0 -20	468	.680	2.31	.99	1.32	0098	0086	0097	0064 5676
80.0 -20	468	.680	2.25	.99	1.26	0095	0086	0094	0061 5709
98.0 -20	468	.680	2.10	.99	1.11	0082	0086	0081	0054 5974

* last column employed in computer plotting only.

TABLE NO. 10

TABULATION OF SMOOTHED DATA POINTS FOR -
 ABSORPTION OF SOUND IN AIR VERSUS RELATIVE HUMIDITY
 AT -20 DEGREES CENTIGRADE

R.H.	TEMP	FREQ	LAMDA	AIR	AIR	AIR	AIR	MU	3000*
DEG				WALL	WALL	ONLY	ONLY	CLAS	LOG
PRCT	CENT	CPS	METRS	DB/S	DB/S	DB/S	/M	/M	RH
1	2	3	4	5	6				
1234567890123456789012345678901234567890123456789012345678									
17.7	-20	660	.482	2.32	1.86	.46	0033	0170	0031
22.2	-20	660	.482	2.66	1.86	.80	0052	0170	0050
29.3	-20	660	.482	2.98	1.86	1.12	0096	0170	0094
31.1	-20	660	.482	3.40	1.86	1.54	0110	0170	0108
37.0	-20	660	.482	3.73	1.86	1.87	0139	0170	0137
42.8	-20	660	.482	3.99	1.86	2.13	0159	0170	0157
46.7	-20	660	.482	4.14	1.86	2.28	0166	0170	0164
58.0	-20	660	.482	4.25	1.86	2.39	0174	0170	0172
66.5	-20	660	.482	4.23	1.86	2.37	0172	0170	0170
72.0	-20	660	.482	4.20	1.86	2.34	0167	0170	0165
78.0	-20	660	.482	4.08	1.86	2.22	0159	0170	0157
80.0	-20	660	.482	4.04	1.86	2.18	0157	0170	0155
98.0	-20	660	.482	3.96	1.86	2.10	0135	0170	0133
17.7	-20	853	.373	3.82	3.58	.24	0021	0288	0018
22.2	-20	853	.373	4.05	3.58	.47	0045	0288	0042
29.3	-20	853	.373	4.38	3.58	.80	0080	0288	0077
31.1	-20	853	.373	4.83	3.58	1.25	0089	0288	0086
37.0	-20	853	.373	5.27	3.58	1.69	0123	0288	0120
42.8	-20	853	.373	5.67	3.58	2.09	0152	0288	0149
46.7	-20	853	.373	5.92	3.58	2.34	0170	0288	0167
58.0	-20	853	.373	6.20	3.58	2.62	0194	0288	0191
66.5	-20	853	.373	6.20	3.58	2.62	0199	0288	0196
72.0	-20	853	.373	6.35	3.58	2.77	0201	0288	0198
78.0	-20	853	.373	6.29	3.58	2.71	0199	0288	0196
80.0	-20	853	.373	6.21	3.58	2.63	0197	0288	0194
98.0	-20	853	.373	6.25	3.58	2.67	0179	0288	0176

* last column employed in computer plotting only.

TABLE NO. 11

TABULATION OF SMOOTHED DATA POINTS FOR
 ABSORPTION OF SOUND IN AIR VERSUS RELATIVE HUMIDITY
 AT -40 DEGREES CENTIGRADE

* last column employed in computer plotting only.

TABLE NO. 12
 TABULATION OF ORIGINAL DATA POINTS FOR
 ABSORPTION OF SOUND IN OXYGEN VERSUS RELATIVE HUMIDITY
 AT 20 DEGREES CENTIGRADE

* last column employed in computer plotting only.

TABLE NO. 12
 TABULATION OF ORIGINAL DATA POINTS FOR
 ABSORPTION OF SOUND IN OXYGEN VERSUS RELATIVE HUMIDITY
 AT 20 DEGREES CENTIGRADE

* last column employed in computer plotting only.

TABLE NO. 12
 TABULATION OF ORIGINAL DATA POINTS FOR
 ABSORPTION OF SOUND IN OXYGEN VERSUS RELATIVE HUMIDITY
 AT 20 DEGREES CENTIGRADE

R.H.	TEMP	FREQ	LAMDA	02	02	02	02	MU	3000*
				+	ONLY	ONLY	CLAS	MOL	
				DEG	WALL	WALL			LOG
PRCT	CENT	CPS	METRS		DB/S	DB/S	DB/S	/M	RH
1	2			3	4	5		/M	6
12345678901	12345678901	12345678901	12345678901	12345678901	12345678901	12345678901	12345678901	12345678901	12345678
.0	20	874	.373	5.32	4.00	1.32	0093	0310	0090 0034 0
1.3	20	874	.373	6.86	4.00	2.86	0201	0310	0198 0074 342
1.4	20	874	.373	10.70	4.00	6.70	0471	0310	0468 0176 438
1.9	20	874	.373	13.00	4.00	9.00	0632	0310	0629 0236 836
2.3	20	874	.373	16.30	4.00	12.30	0864	0310	0861 0323 1085
2.8	20	874	.373	21.00	4.00	17.00	1194	0310	1191 0447 1341
4.2	20	874	.373	24.60	4.00	20.60	1447	0310	1444 0542 1870
5.1	20	874	.373	32.70	4.00	28.70	2016	0310	2013 0756 2123
5.9	20	874	.373	37.10	4.00	33.10	2325	0310	2322 0872 2313
6.4	20	874	.373	39.60	4.00	35.60	2501	0310	2498 0938 2419
8.3	20	874	.373	40.30	4.00	36.30	2550	0310	2547 0956 2757
8.9	20	874	.373	41.40	4.00	37.40	2627	0310	2624 0985 2848
9.9	20	874	.373	36.80	4.00	32.80	2304	0310	2301 0864 2987
10.8	20	874	.373	34.60	4.00	30.60	2149	0310	2146 0805 3100
12.8	20	874	.373	31.20	4.00	27.20	1911	0310	1908 0716 3322
14.9	20	874	.373	25.00	4.00	21.00	1475	0310	1472 0552 3520
17.3	20	874	.373	20.80	4.00	16.80	1180	0310	1177 0442 3714
20.3	20	874	.373	17.20	4.00	13.20	0927	0310	0924 0347 3922
24.0	20	874	.373	13.60	4.00	9.60	0674	0310	0671 0252 4141
29.0	20	874	.373	11.10	4.00	7.10	0499	0310	0496 0186 4387
32.5	20	874	.373	9.76	4.00	5.76	0405	0310	0402 0151 4536
44.0	20	874	.373	7.85	4.00	3.85	0270	0310	0267 0100 4930
50.0	20	874	.373	7.05	4.00	3.05	0214	0310	0211 0079 5097
54.0	20	874	.373	6.69	4.00	2.69	0189	0310	0186 0070 5197

* last column employed in computer plotting only.

* last column employed in computer plotting only.

TABLE NO. 13
 TABULATION OF ORIGINAL DATA POINTS FOR
 ABSORPTION OF SOUND IN OXYGEN VS CONCENTRATION OF DEUTERIUM OXIDE

R.H.	TEMP	FREQ	LAMDA	02	02	02	02	MU	3000*
PRCT	DEG	CENT	CPS	METRS	WALL	WALL			LOG
•1	20	479	•680	2•37	1•35	1•02	0072	0092	0071 0048-2999
1•2	20	479	•680	7•60	1•35	6•25	0440	0092	0439 0300 238
1•3	20	479	•680	9•23	1•35	7•88	0555	0092	0554 0378 342
1•4	20	479	•680	10•20	1•35	8•85	0624	0092	0623 0425 438
1•5	20	479	•680	11•20	1•35	9•85	0694	0092	0693 0473 528
1•6	20	479	•680	12•70	1•35	11•35	0800	0092	0799 0545 612
1•7	20	479	•680	14•00	1•35	12•65	0891	0092	0890 0608 691
1•8	20	479	•680	15•45	1•35	14•10	0994	0092	0993 0678 766
1•9	20	479	•680	17•30	1•35	15•95	1124	0092	1123 0767 836
2•2	20	479	•680	19•20	1•35	17•85	1258	0092	1257 0858 1027
2•5	20	479	•680	20•80	1•35	19•45	1371	0092	1370 0935 1194
4•1	20	479	•680	21•20	1•35	19•85	1399	0092	1398 0954 1838
4•3	20	479	•680	21•50	1•35	20•15	1420	0092	1419 0969 1900
4•8	20	479	•680	20•80	1•35	19•45	1371	0092	1370 0935 2044
5•8	20	479	•680	18•70	1•35	17•35	1223	0092	1222 0834 2290
7•1	20	479	•680	15•60	1•35	14•25	1004	0092	1003 0685 2554
8•2	20	479	•680	13•25	1•35	11•90	0839	0092	0838 0572 2741
10•9	20	479	•680	10•70	1•35	9•35	0659	0092	0658 0449 3112
14•0	20	479	•680	8•07	1•35	6•72	0474	0092	0473 0323 3438
18•0	20	479	•680	6•52	1•35	5•17	0364	0092	0363 0248 3766
22•4	20	479	•680	4•85	1•35	3•50	0247	0092	0246 0168 4051
28•8	20	479	•680	3•98	1•35	2•63	0185	0092	0184 0126 4378
32•0	20	479	•680	3•60	1•35	2•25	0159	0092	0158 0108 4515
37•0	20	479	•680	3•24	1•35	1•89	0133	0092	0132 0090 4705
43•0	20	479	•680	3•08	1•35	1•73	0122	0092	0121 0083 4900
47•0	20	479	•680	2•92	1•35	1•57	0111	0092	0110 0075 5016
•1	20	677	•482	3•69	1•93	1•76	0124	0183	0122 0059-2999
1•2	20	677	•482	9•08	1•93	7•15	0504	0183	0502 0242 238
1•3	20	677	•482	10•80	1•93	8•87	0625	0183	0623 0301 342
1•4	20	677	•482	11•85	1•93	9•92	0699	0183	0697 0337 438
1•5	20	677	•482	13•10	1•93	11•17	0787	0183	0785 0379 528
1•6	20	677	•482	14•70	1•93	12•77	0900	0183	0898 0434 612
1•7	20	677	•482	16•40	1•93	14•47	1020	0183	1018 0492 691
1•8	20	677	•482	18•20	1•93	16•27	1146	0183	1144 0553 766
1•9	20	677	•482	20•70	1•93	18•77	1323	0183	1321 0638 836
2•2	20	677	•482	23•70	1•93	21•77	1534	0183	1532 0740 1027
2•5	20	677	•482	27•10	1•93	25•17	1774	0183	1772 0856 1194
4•1	20	677	•482	28•90	1•93	26•97	1900	0183	1898 0917 1838
4•3	20	677	•482	29•80	1•93	27•87	1964	0183	1962 0948 1900
4•8	20	677	•482	31•70	1•93	29•77	2098	0183	2096 1012 2044
5•8	20	677	•482	31•30	1•93	29•37	2070	0183	2068 0999 2290
7•1	20	677	•482	27•90	1•93	25•97	1830	0183	1828 0883 2554
8•2	20	677	•482	24•40	1•93	22•47	1583	0183	1581 0764 2741
10•9	20	677	•482	20•40	1•93	18•47	1301	0183	1299 0627 3112
14•0	20	677	•482	16•10	1•93	14•17	0998	0183	0996 0481 3438
18•0	20	677	•482	12•90	1•93	10•97	0773	0183	0771 0372 3766
22•4	20	677	•482	9•85	1•93	7•92	0558	0183	0556 0269 4051
28•8	20	677	•482	8•15	1•93	6•22	0438	0183	0436 0211 4378
32•2	20	677	•482	7•43	1•93	5•50	0388	0183	0386 0186 4524
37•0	20	677	•482	6•64	1•93	4•71	0332	0183	0330 0159 4705
43•0	20	677	•482	6•38	1•93	4•45	0314	0183	0312 0151 4900
47•0	20	677	•482	6•05	1•93	4•12	0290	0183	0288 0139 5016

* last column employed in computer plotting only.

TABLE NO. 13

TABULATION OF ORIGINAL DATA POINTS FOR
ABSORPTION OF SOUND IN OXYGEN VS CONCENTRATION OF DEUTERIUM OXIDE
AT 20 DEGREES CENTIGRADE

R.H.	TEMP	FREQ	LAMDA	02 + DEG	02 ONLY	02 ONLY	02 CLAS	MU	3000*
PRCT	CENT	CPS	METRS	WALL	WALL	DB/S	DB/S	/M	LOG
1	2			3	4	5	6	/M	RH
1234567890	1234567890	1234567890	1234567890	1234567890	1234567890	1234567890	1234567890	1234567890	1234567890
•1	20	874	•373	5.63	4.00	1.63	0115	0310	0112 0042-2999
1.2	20	874	•373	10.90	4.00	6.90	0486	0310	0483 0181 238
1.3	20	874	•373	12.60	4.00	8.60	0606	0310	0603 0226 342
1.4	20	874	•373	13.50	4.00	9.50	0669	0310	0666 0249 438
1.5	20	874	•373	14.85	4.00	10.85	0765	0310	0762 0285 528
1.6	20	874	•373	16.60	4.00	12.60	0888	0310	0885 0331 612
1.7	20	874	•373	18.30	4.00	14.30	1008	0310	1005 0376 691
1.8	20	874	•373	19.90	4.00	15.90	1120	0310	1117 0418 766
1.9	20	874	•373	23.00	4.00	19.00	1339	0310	1336 0500 836
2.2	20	874	•373	26.00	4.00	22.00	1550	0310	1547 0579 1027
2.5	20	874	•373	30.00	4.00	26.00	1832	0310	1829 0684 1194
4.1	20	874	•373	32.20	4.00	28.20	1987	0310	1984 0742 1838
4.3	20	874	•373	36.40	4.00	32.40	2283	0310	2280 0853 1900
4.8	20	874	•373	38.90	4.00	34.90	2459	0310	2456 0919 2044
5.8	20	874	•373	40.70	4.00	36.70	2586	0310	2583 0966 2290
7.1	20	874	•373	37.40	4.00	33.40	2353	0310	2350 0879 2554
8.2	20	874	•373	34.70	4.00	30.70	2163	0310	2160 0808 2741
10.9	20	874	•373	30.50	4.00	26.50	1867	0310	1864 0697 3112
14.0	20	874	•373	25.50	4.00	21.50	1515	0310	1512 0566 3438
18.0	20	874	•373	20.70	4.00	16.70	1177	0310	1174 0439 3766
22.4	20	874	•373	16.00	4.00	12.00	0846	0310	0843 0315 4051
28.8	20	874	•373	13.50	4.00	9.50	0669	0310	0666 0249 4378
32.0	20	874	•373	12.40	4.00	8.40	0592	0310	0589 0220 4515
37.0	20	874	•373	11.20	4.00	7.20	0507	0310	0504 0189 4705
43.0	20	874	•373	10.80	4.00	6.80	0479	0310	0476 0178 4900
47.0	20	874	•373	10.40	4.00	6.40	0451	0310	0448 0168 5016

* last column employed in computer plotting only.

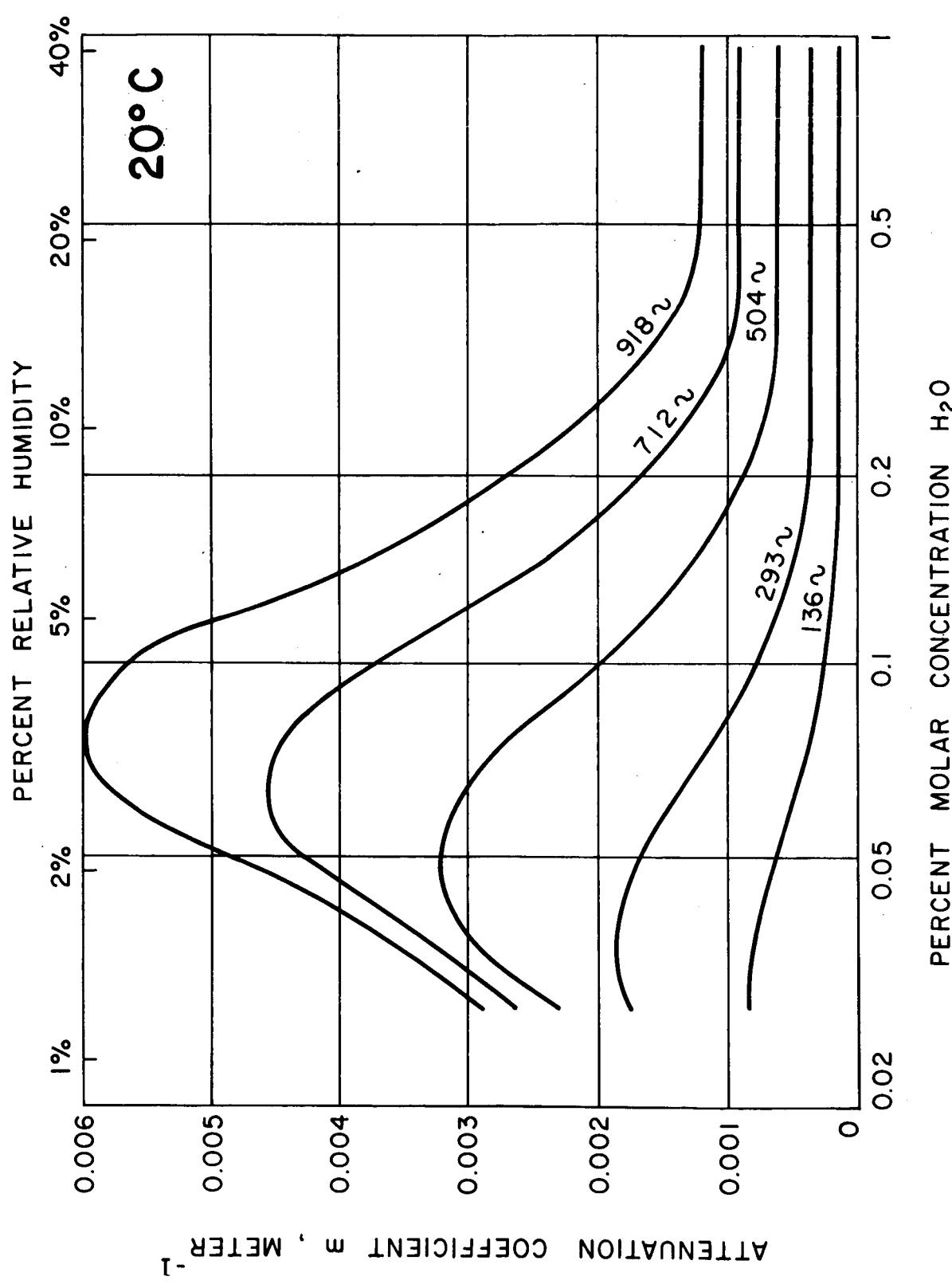


FIGURE 1. ATTENUATION COEFFICIENT m VERSUS PERCENT RELATIVE HUMIDITY FOR AIR AT 20°C AND NORMAL ATMOSPHERIC PRESSURE

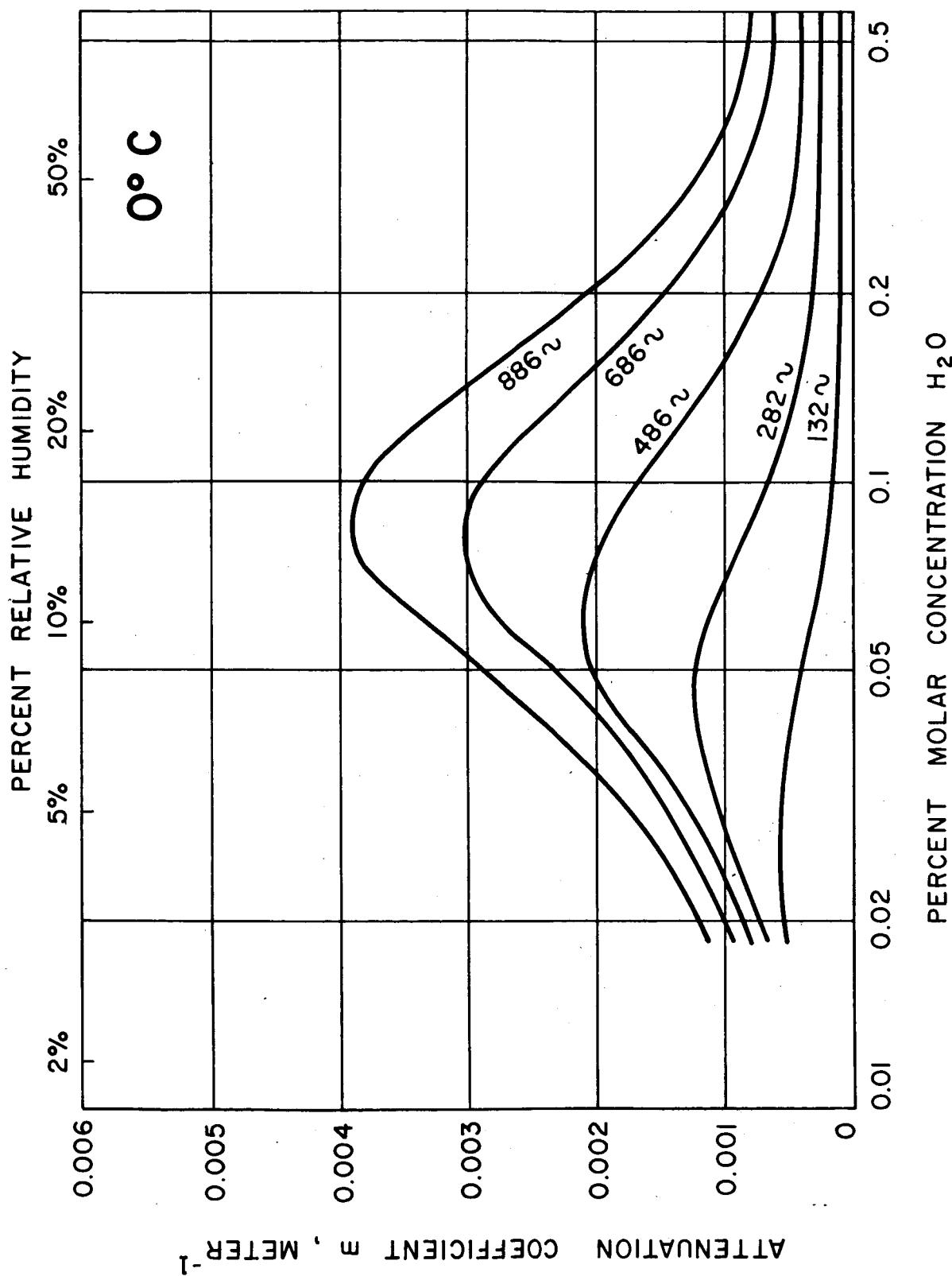


FIGURE 2. ATTENUATION COEFFICIENT E VERSUS PERCENT RELATIVE HUMIDITY FOR AIR AT $0^\circ C$ AND NORMAL ATMOSPHERIC PRESSURE

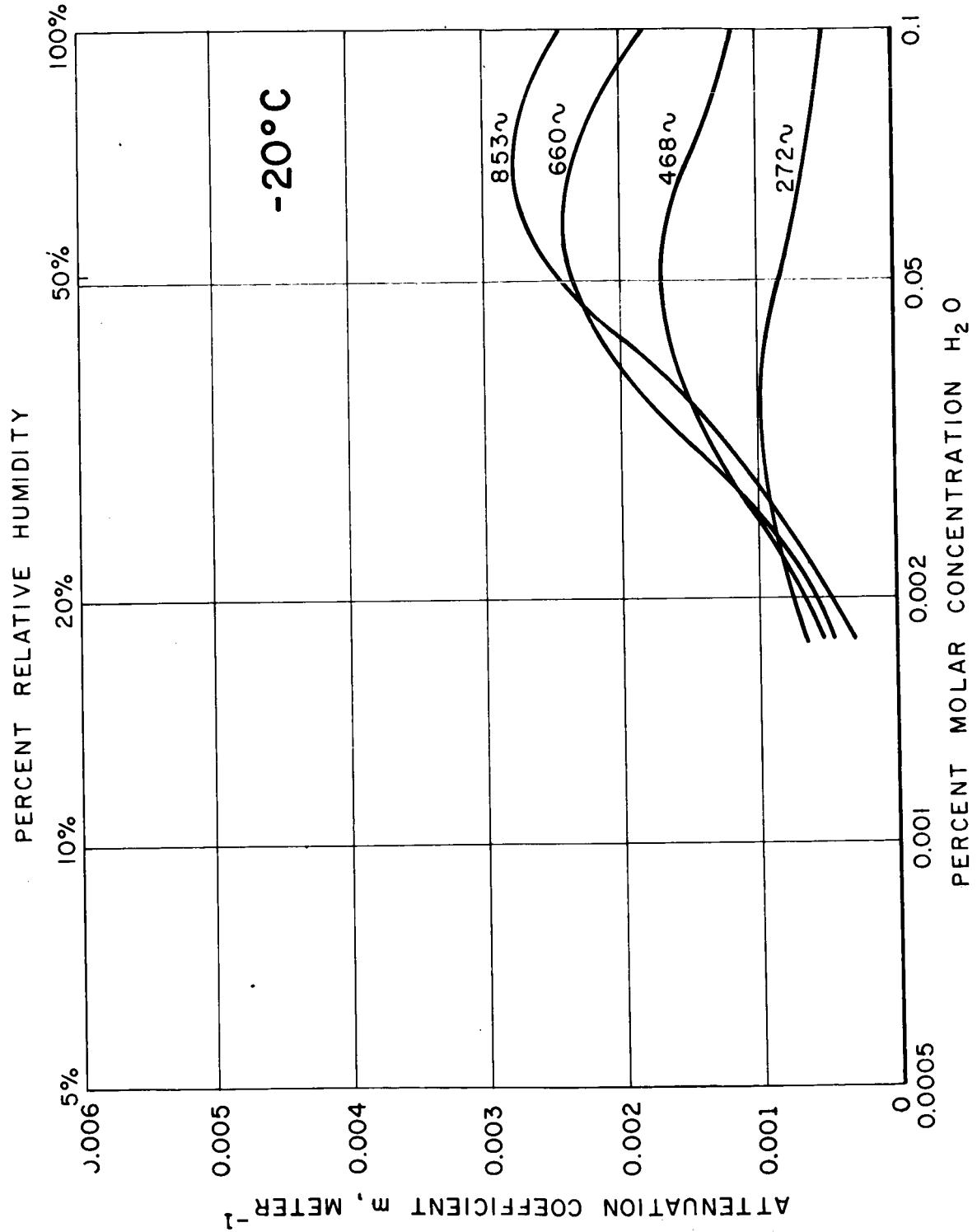


FIGURE 3. ATTENUATION COEFFICIENT m VERSUS PERCENT RELATIVE HUMIDITY FOR AIR AT -20°C AND NORMAL ATMOSPHERIC PRESSURE

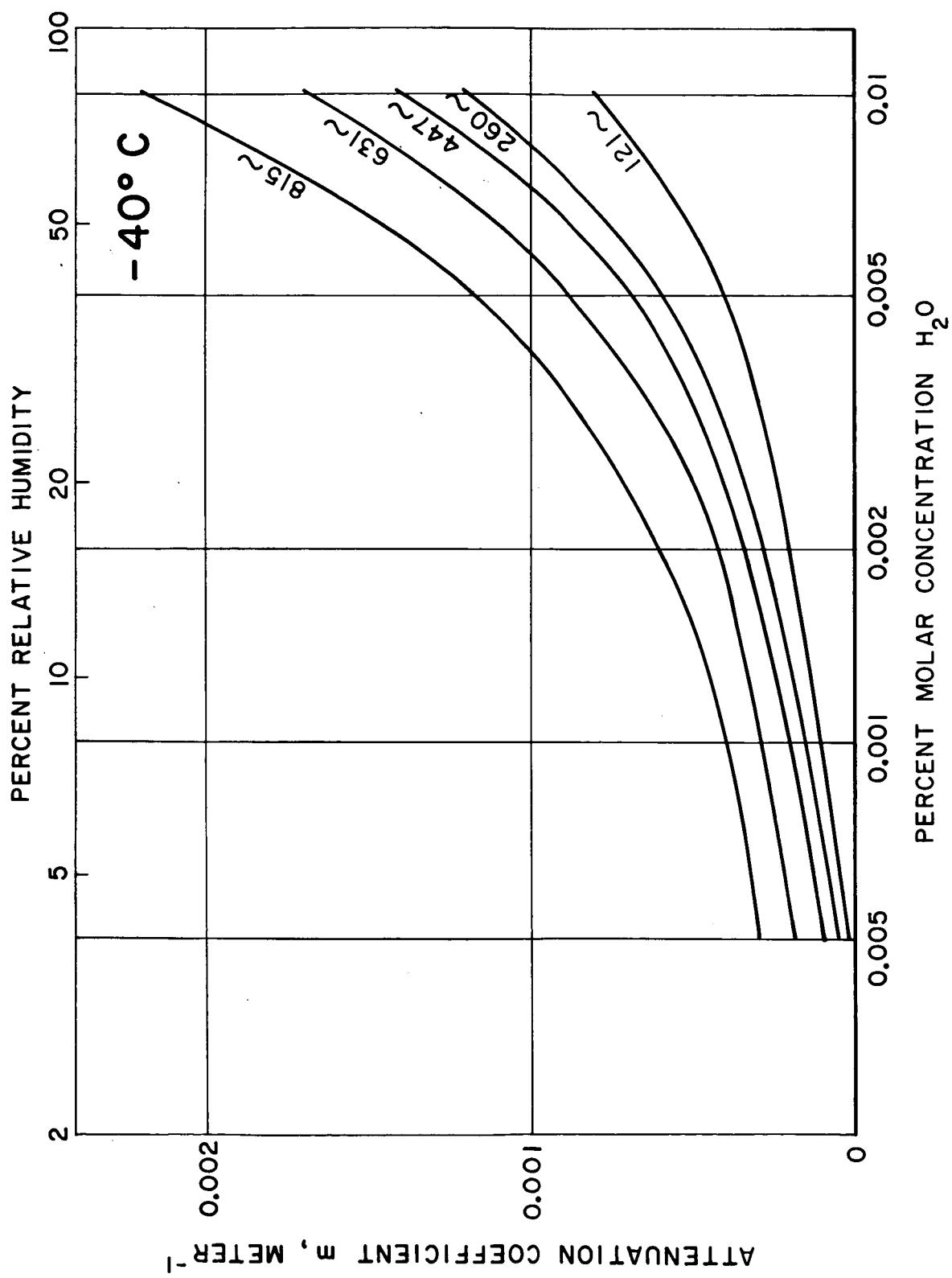


FIGURE 4. ATTENUATION COEFFICIENT m VERSUS PERCENT RELATIVE HUMIDITY FOR AIR AT -40°C AND NORMAL ATMOSPHERIC PRESSURE

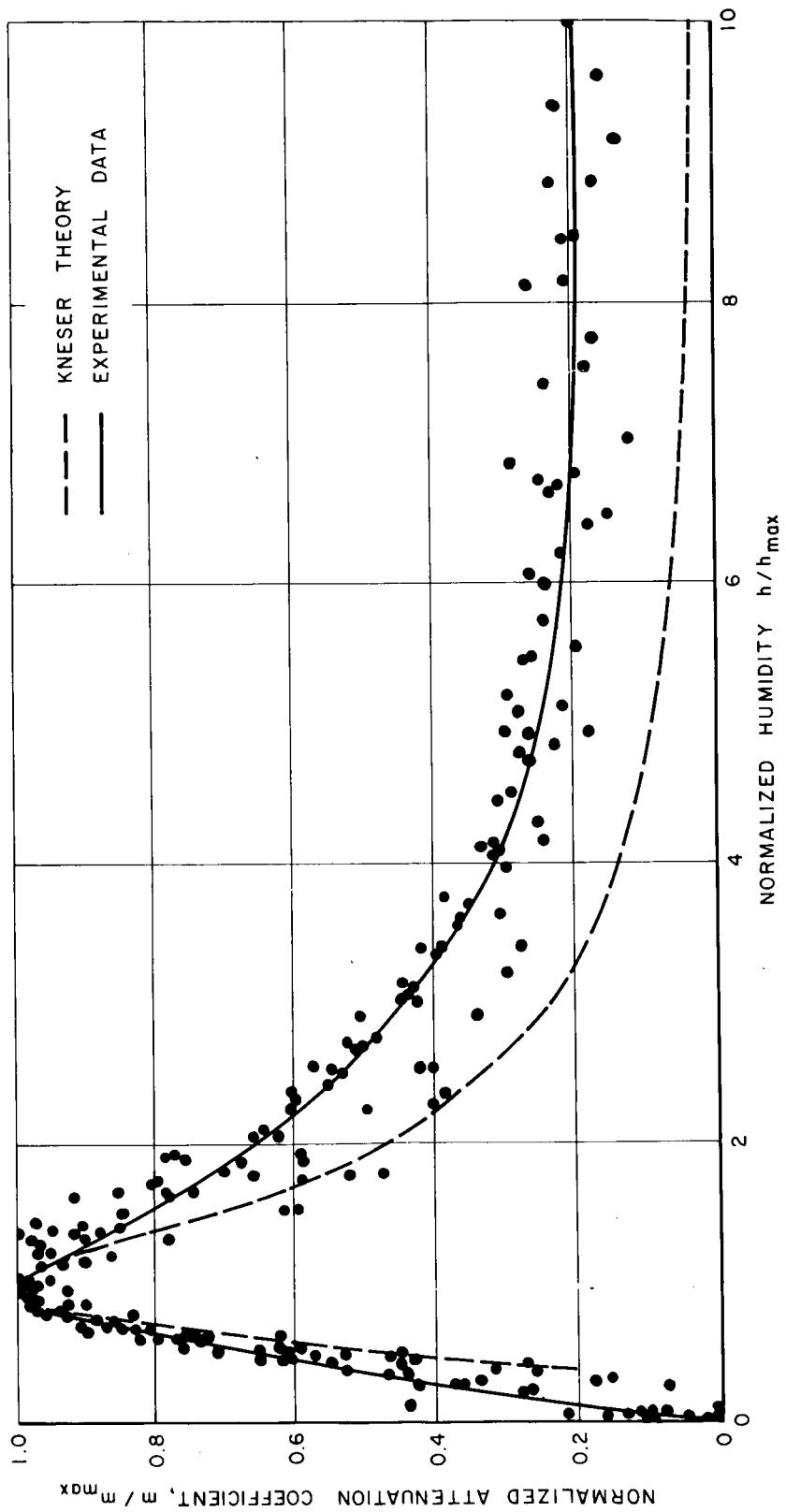


FIGURE 5. PLOT OF EXPERIMENTAL DATA AT 20°C, 0°C AND -20°C OF ATTENUATION IN AIR VERSUS HUMIDITY. THESE DATA ARE PRESENTED IN NORMALIZED FORM M/m_{\max} VERSUS h/h_{\max}

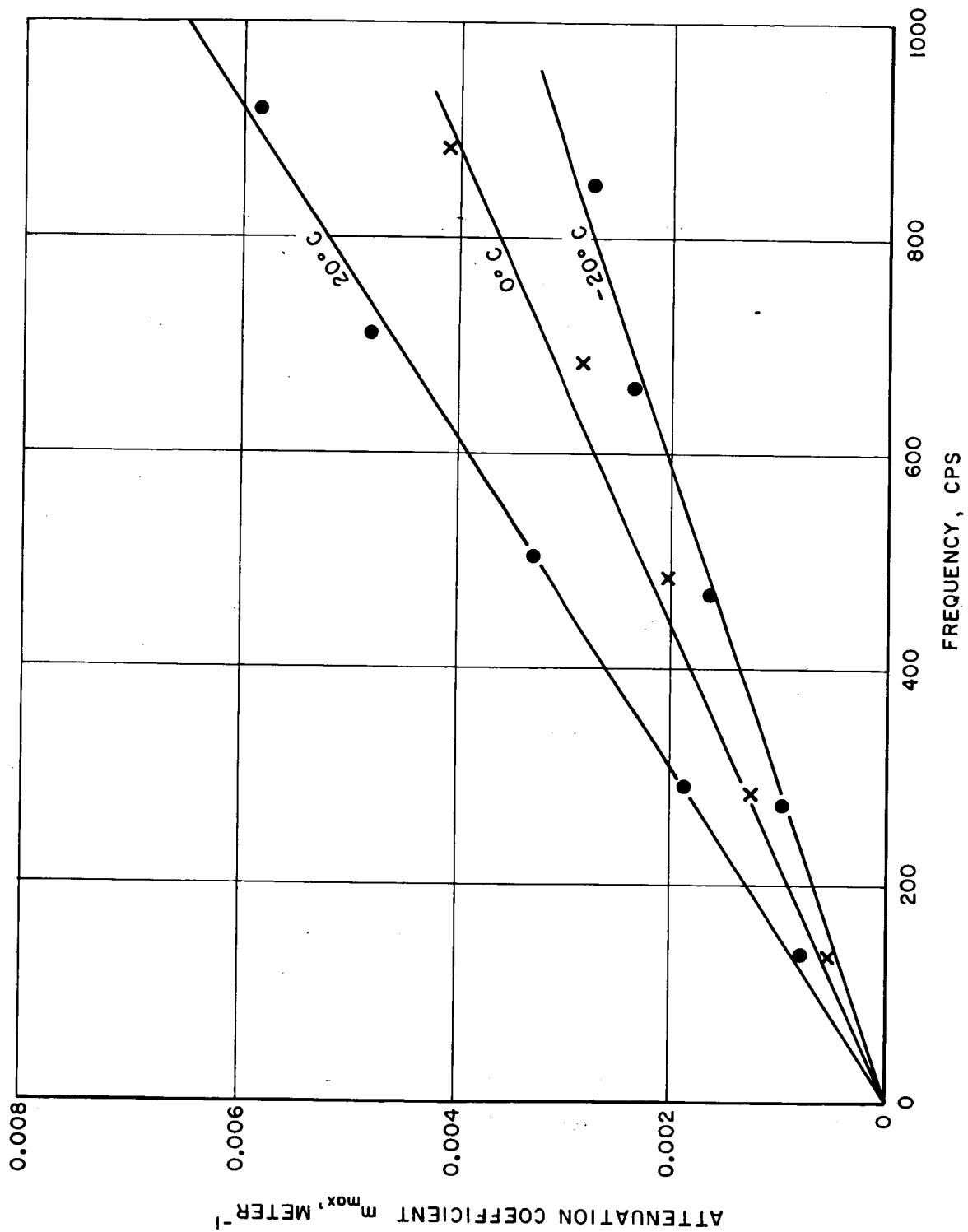


FIGURE 6. MAXIMUM ATTENUATION COEFFICIENT m_{\max} VERSUS FREQUENCY

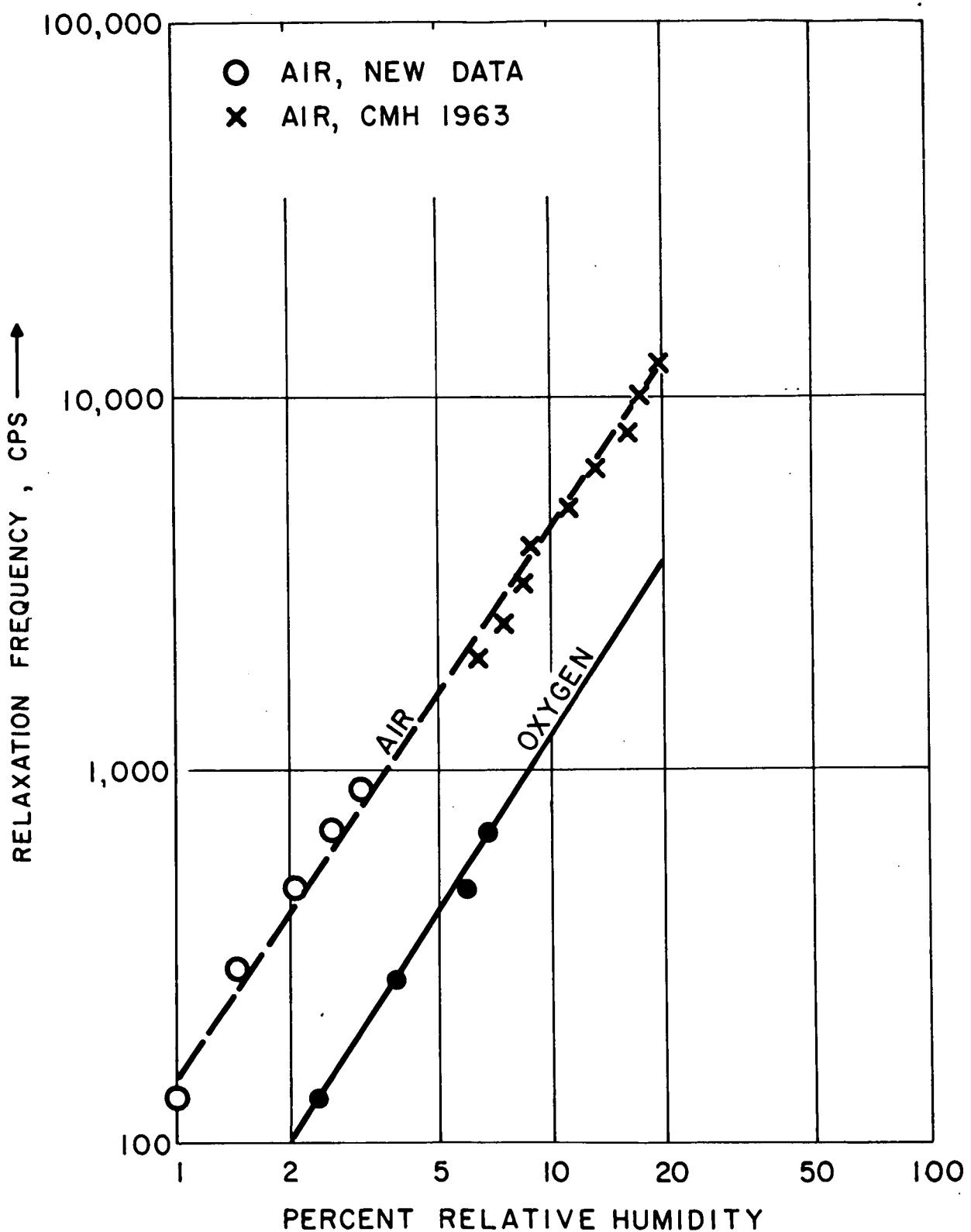


FIGURE 7. RELAXATION FREQUENCY PLOTTED AS A FUNCTION OF \underline{h} , THE PERCENT MOLAR CONCENTRATION OF WATER VAPOR IN AIR

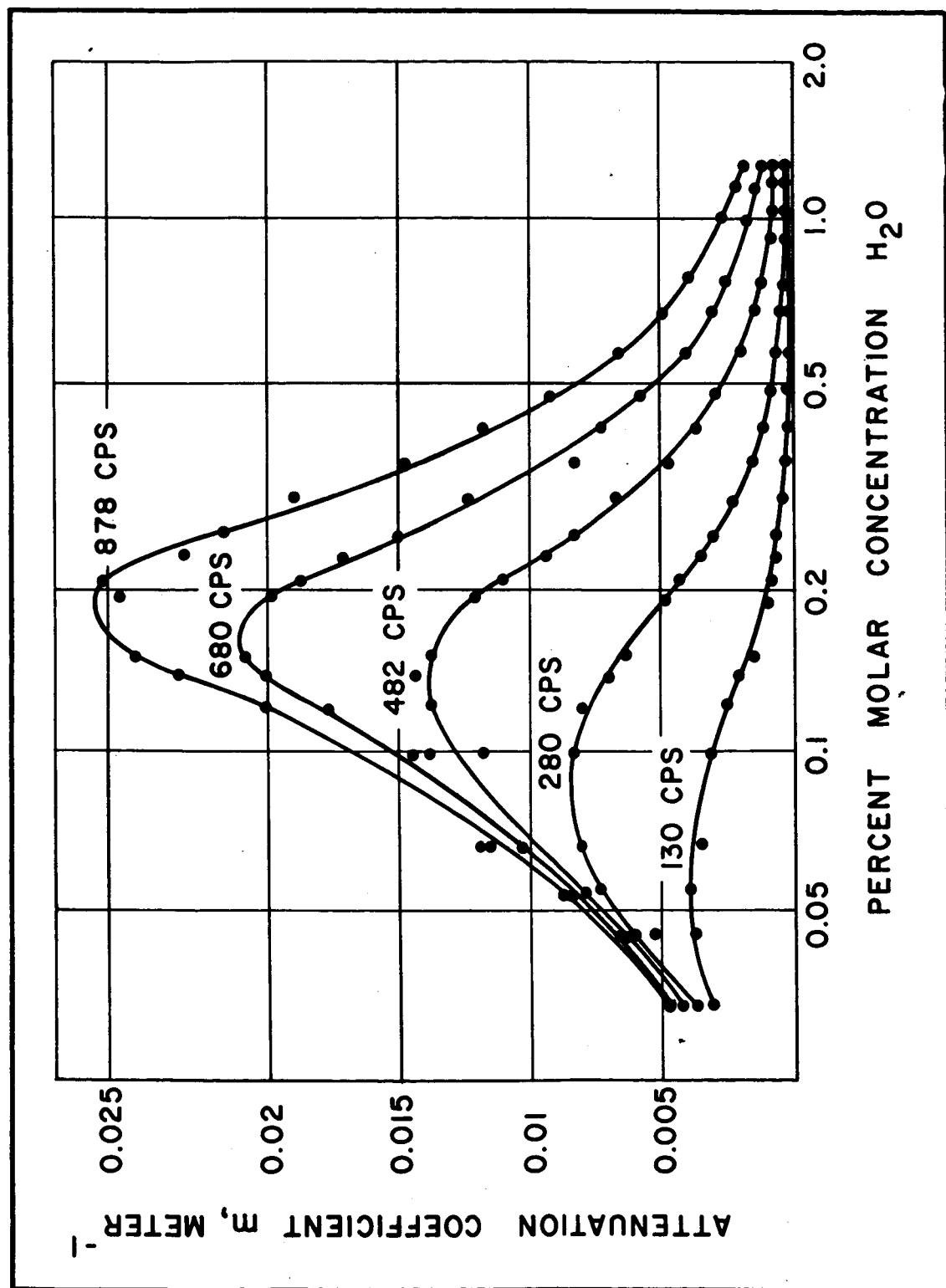


FIGURE 8. ATTENUATION COEFFICIENT m VERSUS PERCENT MOLAR CONCENTRATION OF WATER VAPOR FOR OXYGEN AT 20°C AND NORMAL PRESSURE

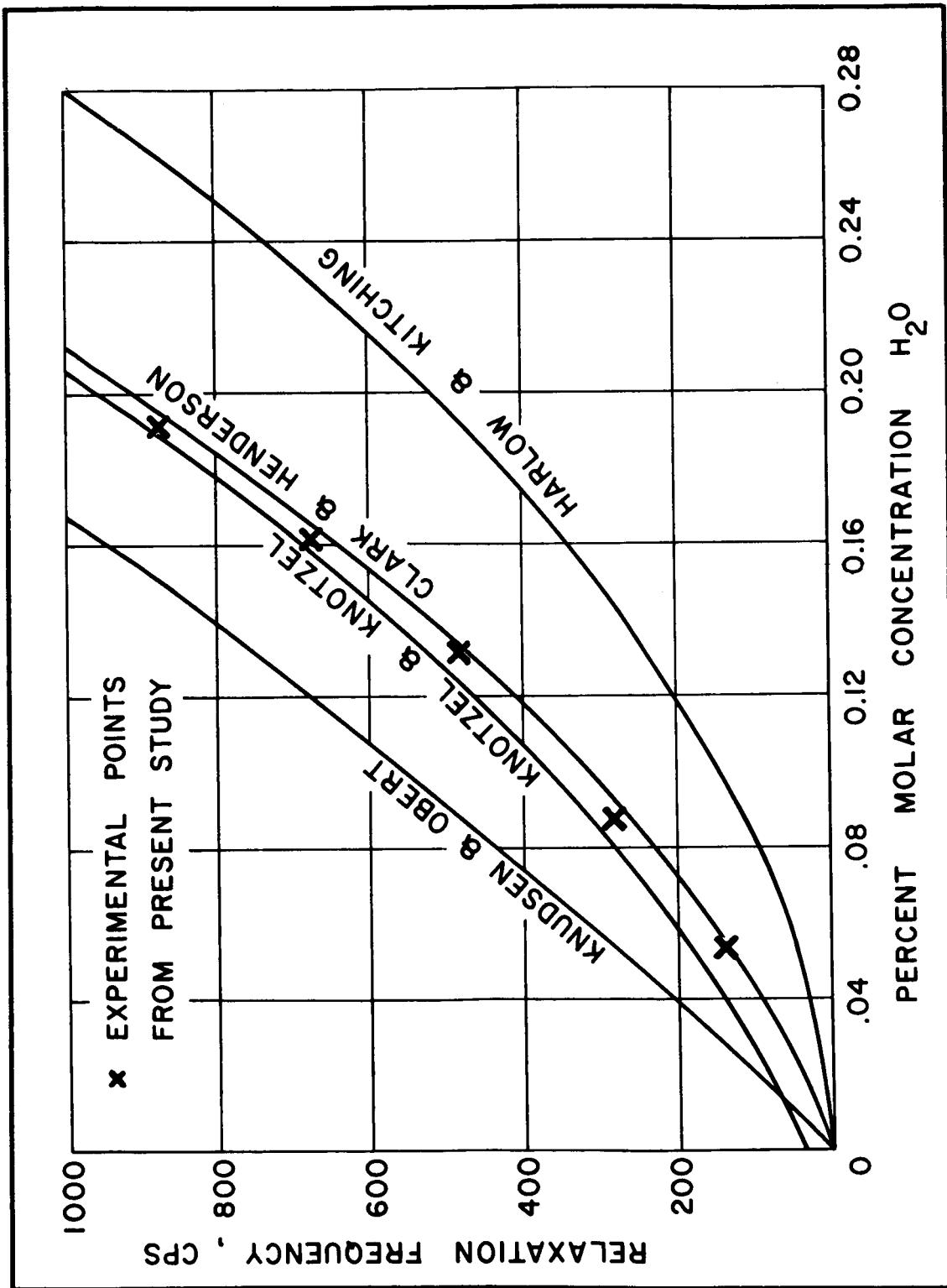


FIGURE 9. RELAXATION FREQUENCY, f_{\max} , PLOTTED AS A FUNCTION OF \underline{h} , THE PERCENT MOLAR CONCENTRATION OF WATER VAPOR IN OXYGEN

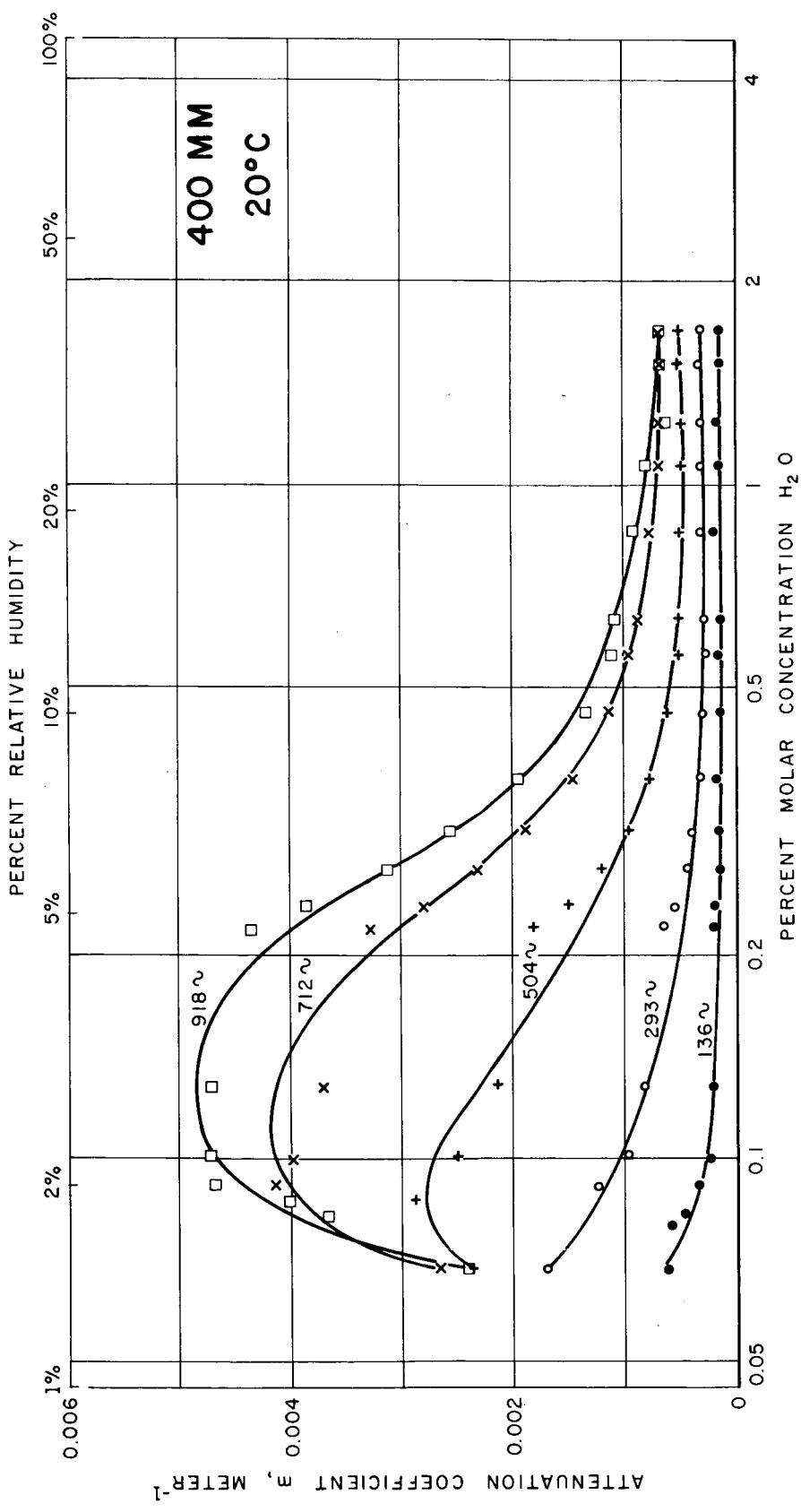


FIGURE 10. ATTENUATION COEFFICIENT m VERSUS PERCENT RELATIVE HUMIDITY FOR AIR AT 20°C AND PRESSURE OF 400 mm

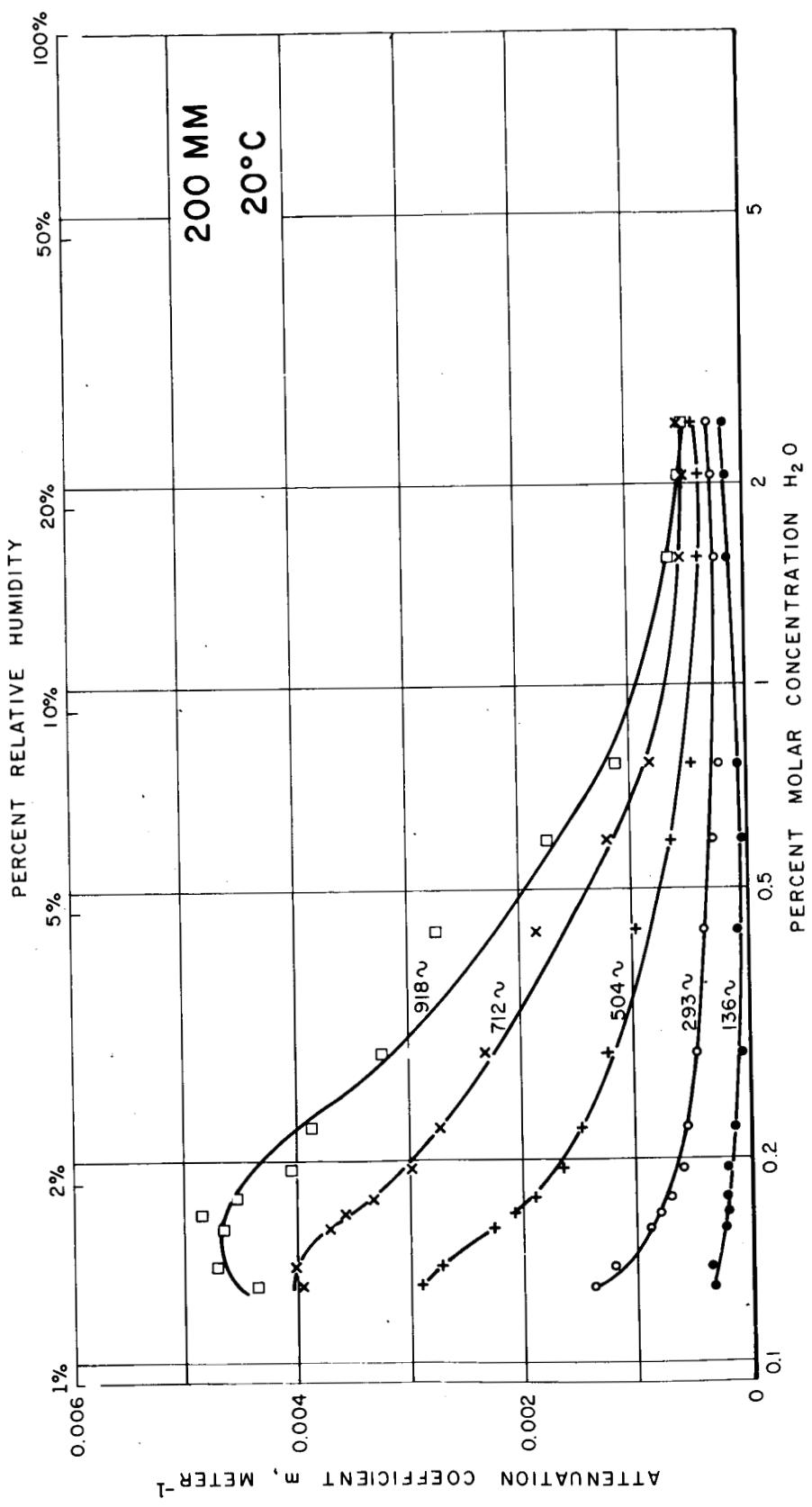


FIGURE 11. ATTENUATION COEFFICIENT m VERSUS PERCENT RELATIVE HUMIDITY FOR AIR AT 20°C AND PRESSURE OF 200 mm

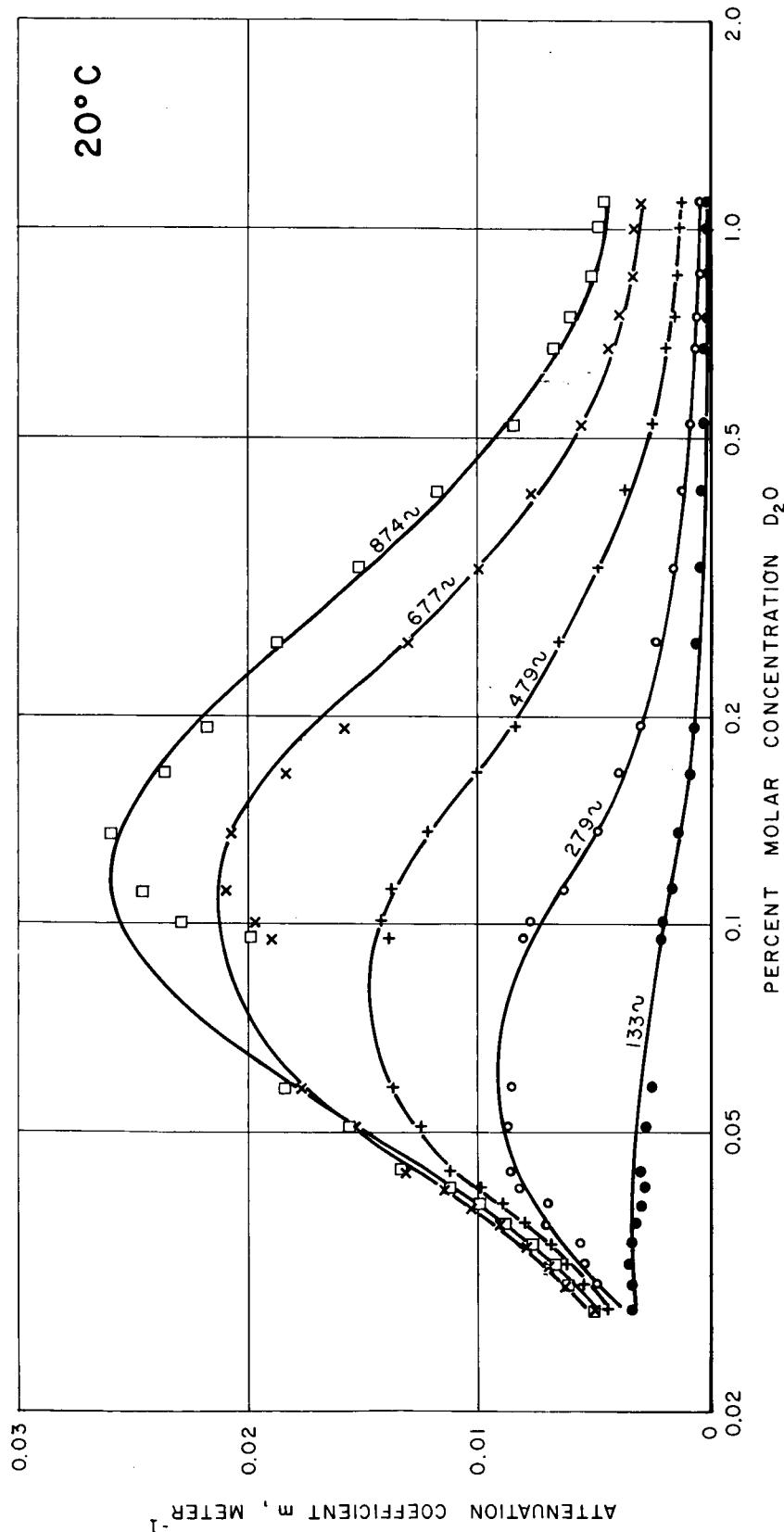


FIGURE 12. ATTENUATION COEFFICIENT m VERSUS PERCENT MOLAR CONCENTRATION OF DEUTERIUM OXIDE VAPOR FOR OXYGEN AT 20°C AND NORMAL PRESSURE

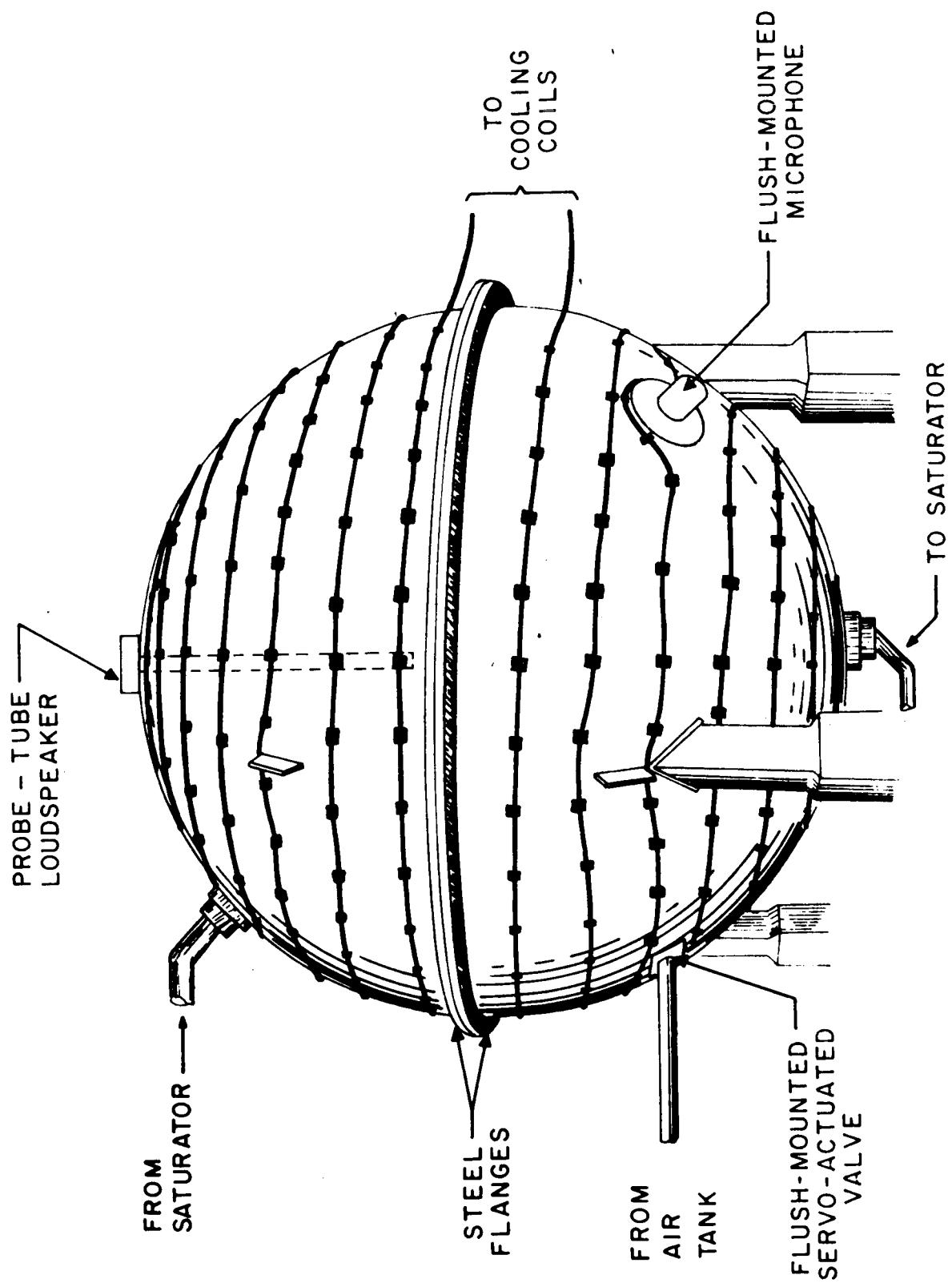


FIGURE 13. DRAWING SHOWING THE SPHERICAL CHAMBER USED IN MEASUREMENTS.
COPPER TUBING ATTACHED TO EXTERIOR SURFACE IS PART OF THE
TEMPERATURE-CONTROL SYSTEM

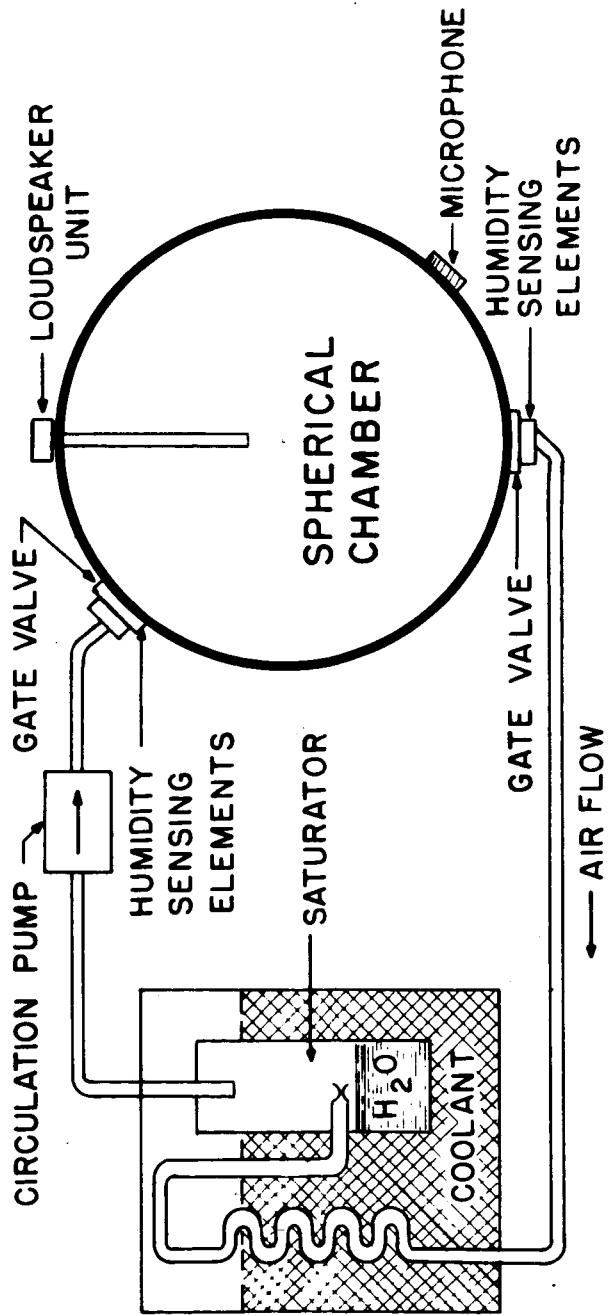


FIGURE 14. SIMPLIFIED SCHEMATIC DIAGRAM OF THE AIR-CIRCULATION SYSTEM. AIR IS RECIRCULATED CONTINUOUSLY THROUGH THE SPHERICAL CHAMBER. THE SATURATOR EITHER TAKES AWAY MOISTURE FROM THE AIR OR ADDS MOISTURE TO IT--DEPENDING ON THE RELATIVE TEMPERATURES OF THE SPHERICAL CHAMBER AND THE SATURATOR

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