

NASA SP-3017

# CHARTS FOR APPROXIMATE

# THERMODYNAMIC PROPERTIES OF

# NITROGEN-OYXGEN MIXTURES

# FOWLER and BROWN

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# NATIONAL AERONAUTICS AND SPACE ADMINISTRATION

NASA SP-3017

# **CHARTS FOR APPROXIMATE**

# THERMODYNAMIC PROPERTIES

# OF NITROGEN-OYXGEN MIXTURES

BY BRUCE FOWLER and RONALD D. BROWN Langley Research Center



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### FOREWORD

The purpose of this paper is to present data, determined by one consistent approach, on the thermodynamic properties of nitrogen and three nitrogen-oxygen compositions and the dimensionless speed-of-sound parameter for each. These properties have been calculated over a temperature range from 200° to 15,000° K for a pressure range from  $10^{-4}$  to  $10^2$  atmospheres. The data are presented in a combination of Mollier charts and tables so that aerodynamic expansions can be performed. The results, which agree closely with more rigorous calculations, are considered suitable for engineering purposes.

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# SUMMARY

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Charts have been prepared which show the equilibrium thermodynamic properties of four nitrogen-oxygen mixtures, one of which approximates air (80 percent N<sub>2</sub> and 20 percent O<sub>2</sub>, by volume). The temperature range was from  $200^{\circ}$  to 15,000° K and the pressure range, from  $10^{-4}$  to  $10^2$  atmospheres. The thermodynamic properties have been computed in closed form, starting from the approximate partition functions.

### INTRODUCTION

One of the factors affecting the performance of the charring ablators which are used as thermal protective structures on high-speed reentry vehicles is oxidation. It has been shown in references 1 and 2 that oxidation varies directly as the oxygen concentration and inversely as the enthalpy of the environment.

In the actual reentry, the enthalpy is frequently higher than can be attained in the usual arc-heated wind-tunnel ground facility. In order to simulate the same oxidation and its effects in such a facility, the oxygen concentration must be reduced in direct proportion to enthalpy. These changes in the ratio of oxygen to nitrogen require thermodynamic charts to evaluate the desired aerodynamic characteristics.

In the present paper, Mollier charts of the equilibrium thermodynamic properties for four nitrogen-oxygen mixtures are presented. These charts have been prepared by using a generalized version of the procedure utilized by Hansen (ref. 3). Only the essential equations required for complete understanding and computation are presented in the text. The more detailed presentation and development of the equations and computation procedure can be found in reference 3.

Pressure and temperature are plotted as a function of enthalpy and dimensionless entropy. The temperature ranges from  $200^{\circ}$  K to  $6,000^{\circ}$  K at  $200^{\circ}$  increments and from  $6,000^{\circ}$  K to  $15,000^{\circ}$  K at  $500^{\circ}$  increments. Pressure ranges from  $10^{-4}$  to  $10^{2}$  atmospheres with five equal divisions between orders of magnitude.

#### SYMBOLS

An enthalpy scale is presented on all charts both in the U.S Customary Units and in the International System of Units, SI. Factors relating the two systems are given in reference 4.

a	speed	of	sound
а.	speed	OT.	sound

- a<sub>i</sub>, b<sub>i</sub> stoichiometric coefficients for species A<sub>i</sub> and B<sub>i</sub>, respectively
- A<sub>i</sub>,B<sub>i</sub> chemical species
- cp heat capacity per mol at constant pressure
- c<sub>v</sub> heat capacity per mol at constant density
- D dissociation energy per molecule

E energy per mol

- $E_{\rm O}$  energy per mol at zero absolute temperature
- g<sub>j</sub> degeneracy of the jth state

gn degeneracy of the nth electronic state

h Planck's constant

H enthalpy per mol

I molecular moment of inertia, also ionization energy per molecule

k Boltzmann constant

K<sub>p</sub> chemical equilibrium constant based on partial pressure

K<sub>p,1</sub> equilibrium constant for oxygen dissociation reaction

K<sub>p,2</sub> equilibrium constant for nitrogen dissociation reaction

K<sub>p,3</sub> equilibrium constant for atom ionization reactions

m mass of gas particle

M molecular weight

 $M_{O}$  molecular weight of undissociated mixture

n,	concentration in moles per unit volume									
р	pressure									
p <sub>o</sub>	reference pressure, 1 atmosphere									
ୟ	partition function									
Qp	pQ where p is unit pressure									
R	universal gas constant									
S	entropy per mol									
So	entropy per mol at 1 atmosphere pressure									
Т	absolute temperature									
x	mol fraction									
$Z = M_O/M$										
α	molecular symmetry number									
γ	ratio of specific heats, $c_p/c_v$									
€l	fraction of initial molecules of oxygen which are dissociated									
€2	fraction of initial molecules of nitrogen which are dissociated									
€3	fraction of atoms which are ionized									
€j	energy of the jth state									
€n	energy of the nth electronic state									
ν	vibrational frequency									
ρ	density									
$\Phi_{N_2}$	volume percent of $N_2$ molecules in initial undissociated composition									
<b>Φ</b> 02	volume percent of O2 molecules in initial undissociated composition									

### Subscripts:

# i index referring to molecule type

int internal

t,r,v,e indices referring to the contribution of translational, rotational, vibrational, and electronic energy modes, respectively

#### FUNDAMENTAL RELATIONS

The thermodynamic properties of four mixtures of nitrogen and oxygen were calculated on a high-speed digital computer by using the method and equations from Hansen (ref. 3). The program was generalized so that the initial concentration of nitrogen and oxygen and the weight of the undissociated molecules of each mixture were inputs. Therefore, the program allows complete flexibility for any mixture of nitrogen and oxygen.

The principal assumptions made for the thermodynamic calculations were the same as Hansen (ref. 3) and are as follows: each gas species obeys the ideal equation of state; individual diatomic molecules are rigid rotor-harmomic oscillators; the reactions are nitrogen and oxygen dissociation and atomic ionization; and formation of NO (nitric oxide) is neglected.

### Partition Function

All the thermodynamic properties of a gas may be calculated from its partition function. The partition function is defined as

$$Q = \sum_{j} g_{j} e^{-\frac{\epsilon_{j}}{kT}}$$
(1)

where  $\varepsilon_j$  is the energy of the jth state and  $g_j$  is the degeneracy of the jth state. The total partition function may be expressed as a product

$$Q = Q_{t}Q_{r}Q_{v}Q_{e}$$
(2)

The factors on the right-hand side of equation (2) are the partition functions associated with the translational, rotational, vibrational, and electronic energy modes of the gas particle. From the method of statistical mechanics the partition functions can be expressed as follows:

$$Q_{t} = \left(\frac{2\pi m kT}{h^{2}}\right)^{3/2} \frac{RT}{P}$$
(3)

$$Q_{r} = \frac{8\pi^{2}IkT}{ah^{2}}$$
(4)

$$Q_{\rm v} = \left(1 - e^{-\frac{h\nu}{kT}}\right)^{-1}$$
(5)

$$Q_{e} = \sum_{n=0}^{\infty} g_{n} e^{\frac{\epsilon_{n}}{kT}}$$
(6)

Values of all numerical constants and the complete partition-function expression for each species are given in table I and appendix A, respectively.

# Equilibrium Constant

The reactions considered can be generalized by the following expression:

$$\sum_{i} a_{i}A_{i} \rightleftharpoons \sum_{i} b_{i}B_{i}$$
(7)

where  $A_i$  and  $B_i$  are the reactants and products, respectively, and  $a_i$  and  $b_i$  are the corresponding stoichiometric coefficients.

The pressure equilibrium constant can be defined in terms of the partial pressures:

$$K_{p} = \frac{\Pi p^{b_{i}}(B_{i})}{\Pi p^{a_{i}}(A_{i})}$$
(8)

and is related to the partition functions by (see ch. VIII of ref. 5)

$$\ln K_{p} = -\frac{\Delta E_{o}}{RT} + \sum b_{i} \ln Q_{p}(B_{i}) - \sum a_{i} \ln Q_{p}(A_{i})$$
(9)

where  $Q_p = pQ$  for p = unit value and

$$\Delta E_{o} = \sum b_{i} E_{o}(B_{i}) - \sum a_{i} E_{o}(A_{i})$$
(10)

is the zero-point energy difference between the products and the reactants, both referring to the standard states.

The equation of state will be defined as

$$\frac{p}{\rho} = \frac{ZRT}{M_{O}}$$
(11)

where Z is the molecular weight ratio  $M_O/M$ . If  $\epsilon_1$  is the volume fraction of initial molecules that are dissociated into oxygen atoms,  $\epsilon_2$  is the volume fraction of initial molecules that are dissociated into nitrogen atoms, and  $\epsilon_3$ is the volume fraction of original atoms that are ionized after dissociation is completed, then the molecular-weight ratio is

$$Z = 1 + \epsilon_1 + \epsilon_2 + 2\epsilon_3 \tag{12}$$

The reactions are now assumed to be independent and to follow in sequence. The O<sub>2</sub> dissociation is assumed to be complete prior to N<sub>2</sub> dissociation and all dissociation to be complete prior to any ionization. The initial percentages of nitrogen and oxygen are taken as  $\varphi_{N_2}$  and  $\varphi_{O_2}$ , respectively. Only three major components exist at relatively low temperatures: molecular nitrogen, molecular oxygen, and atomic oxygen. The equilibrium constant for the oxygen dissociation reaction can be equated to the oxygen partial pressures expressed in terms of  $\varphi_{O_2}$  and  $\epsilon_1$ . The first dissociation fraction is then given by

$$\epsilon_{1} = \frac{-\varphi_{N_{2}} + \sqrt{(\varphi_{N_{2}})^{2} + 4\varphi_{O_{2}}\left(1 + \frac{4p}{K_{p,1}}\right)}}{2\left(1 + \frac{4p}{K_{p,1}}\right)}$$
(13)

The limit where  $\epsilon_1 = 0$  is the condition of no dissociation.

When the oxygen approaches complete dissociation  $\varepsilon_1\to\phi_{02}$  the nitrogen dissociation begins. The second dissociation fraction is similarly expressed by

$$\epsilon_{2} = \frac{-(1.0 + \varphi_{0_{2}} - \varphi_{N_{2}}) + \sqrt{(1 + \varphi_{0_{2}} - \varphi_{N_{2}})^{2} + 4\varphi_{N_{2}}(1 + \varphi_{0_{2}})(1 + \frac{4p}{K_{p,2}})}{2(1 + \frac{4p}{K_{p,2}})} \quad (14)$$

As  $\epsilon_2$  approaches the limit  $\phi_{N_2}$ , the dissociation of nitrogen is also complete and the ionization of the atoms begins. For the consideration of atomic

ionization, it is assumed that the atoms are of a single homogeneous species, because the ionization potential of the oxygen and nitrogen atoms is approximately equal. The ionization fraction is thus

$$\epsilon_{3} = \left(1 + \frac{p}{K_{p,3}}\right)^{-1/2}$$
(15)

where the equilibrium constant  $K_{p,3}$  is taken as a population-weighted average of the constants for the nitrogen and oxygen ionization reactions; that is,

$$K_{p,3} = \varphi_{N_2} K_p(N \rightarrow N^+ + e^-) + \varphi_{0_2} K_p(0 \rightarrow 0^+ + e^-)$$
 (16)

The component mol fractions of the gas mixture are

$$x_{0_2} = \frac{\varphi_{0_2} - \epsilon_1}{Z}$$
(17)

$$x_{N_2} = \frac{\phi_{N_2} - \epsilon_2}{Z}$$
(18)

$$x_0 = \frac{2\epsilon_1 - 2\phi_{02}\epsilon_3}{Z}$$
(19)

$$\mathbf{x}_{\mathrm{N}} = \frac{2\epsilon_2 - 2\phi_{\mathrm{N}_2}\epsilon_3}{\mathbf{Z}}$$
(20)

$$x_{N^{+}+0^{+}} = x_{e^{-}} = \frac{2\epsilon_{3}}{Z}$$
 (21)

### Partial Derivatives

The derivatives of  $Zx_i$  will be required and it can be seen from equations (17) to (21) that the derivatives of  $Zx_i$  are proportional to  $\partial \varepsilon_1 / \partial T$ ,  $\partial \varepsilon_2 / \partial T$ , and  $\partial \varepsilon_3 / \partial T$ . From equations (13), (14), and (16) the partial derivatives of  $\varepsilon_1$ ,  $\varepsilon_2$ , and  $\varepsilon_3$  at constant pressure are

$$\left(\frac{\partial \epsilon_{1}}{\partial T}\right)_{p} = \frac{\frac{d \ln K_{p,1}}{dT}}{\frac{2}{\epsilon_{1}} - \frac{1}{1 + \epsilon_{1}} + \frac{1}{\varphi_{0_{2}} - \epsilon_{1}}}$$
(22)

$$\left(\frac{\partial \epsilon_2}{\partial T}\right)_p = \frac{\frac{d \ln K_{p,2}}{dT}}{\frac{2}{\epsilon_2} - \frac{1}{\left(1 + \varphi_{0_2} + \epsilon_2\right)} + \frac{1}{\left(\varphi_{N_2} - \epsilon_2\right)}}$$
(23)

$$\begin{pmatrix} \frac{\partial \epsilon_3}{\partial T} \end{pmatrix}_{p} = \frac{\frac{d \ln K_{p,3}}{dT}}{\frac{2}{\epsilon_3} - \frac{1}{1 + \epsilon_3} + \frac{1}{1 - \epsilon_3}}$$
(24)

The derivatives of  $Zx_1$  are

$$\left(\frac{\partial Z \mathbf{x}_{O_2}}{\partial T}\right)_p = -\left(\frac{\partial \epsilon_1}{\partial T}\right)_p$$
(25)

$$\left(\frac{\partial Z x_{N_2}}{\partial T}\right)_p = -\left(\frac{\partial \epsilon_1}{\partial T}\right)_p$$
(26)

$$\left(\frac{\partial Z x_0}{\partial T}\right)_p = 2 \left[ \left(\frac{\partial \epsilon_1}{\partial T}\right)_p - \varphi_{02} \left(\frac{\partial \epsilon_3}{\partial T}\right)_p \right]$$
(27)

$$\left(\frac{\partial \mathbf{Z}\mathbf{x}_{\mathrm{N}}}{\partial \mathbf{T}}\right)_{\mathrm{p}} = 2\left[\left(\frac{\partial \mathbf{\varepsilon}_{2}}{\partial \mathbf{T}}\right)_{\mathrm{p}} - \varphi_{\mathrm{N}2}\left(\frac{\partial \mathbf{\varepsilon}_{3}}{\partial \mathbf{T}}\right)_{\mathrm{p}}\right]$$
(28)

$$\left(\frac{\partial Z \mathbf{x}_{e^{-}}}{\partial T}\right)_{p} = 2 \left(\frac{\partial \epsilon_{3}}{\partial T}\right)_{p}$$
(29)

Similarly, the expressions for the partial derivatives of  $\,\varepsilon_1,\,\,\varepsilon_2,\,\,{\rm and}\,\,\varepsilon_3\,$  at constant density are

$$\left(\frac{\partial \epsilon_{1}}{\partial T}\right)_{\rho} = \frac{\frac{d \ln \kappa_{p,1}}{dT} - \frac{1}{T}}{\frac{2}{\epsilon_{1}} + \frac{1}{\varphi_{02} - \epsilon_{1}}}$$
(30)

$$\left(\frac{\partial \epsilon_2}{\partial T}\right)_{\rho} = \frac{\frac{d \ln K_{p,2}}{dT} - \frac{1}{T}}{\frac{2}{\epsilon_2} + \frac{1}{\varphi_{N_2} - \epsilon_2}}$$
(31)

$$\left(\frac{\partial \epsilon_{3}}{\partial T}\right)_{\rho} = \frac{\frac{d \ln \kappa_{p,3}}{dT} - \frac{1}{T}}{\frac{2}{\epsilon_{3}} + \frac{1}{1 - \epsilon_{3}}}$$
(32)

It follows that the expressions for the derivatives of  $Zx_1$  at constant density can be expressed the same as equations (25) to (29) except that the constant-pressure subscript is replaced by the constant-density subscript.

## THERMODYNAMIC PROPERTIES

# Pure Gas

According to statistical mechanics (for example, ch. VIII of ref. 5), the energy and enthalpy per mol of pure gas are given by

$$\frac{\mathbf{E} - \mathbf{E}_{0}}{\mathbf{R}\mathbf{T}} = \mathbf{T} \left( \frac{\partial \ln \mathbf{Q}}{\partial \mathbf{T}} \right)_{\rho}$$
(33)

$$\frac{H - E_0}{RT} = T \left( \frac{\partial \ln Q}{\partial T} \right)_p$$
(34)

The energy and enthalpy per mol of gas due to translation and electronic excitation are given by

$$\left(\frac{\mathbf{E} - \mathbf{E}_{0}}{\mathbf{RT}}\right)_{t+e} = \frac{3}{2} + \frac{\sum \frac{\mathbf{\epsilon}_{n}}{\mathbf{kT}} \mathbf{g}_{n} e^{-\frac{\mathbf{\epsilon}_{n}}{\mathbf{kT}}}}{\sum \mathbf{g}_{n} e^{-\frac{\mathbf{\epsilon}_{n}}{\mathbf{kT}}}}$$
(35)

$$\left(\frac{H - E_{O}}{RT}\right)_{t+e} = \left(\frac{E - E_{O}}{RT}\right)_{t+e} + 1$$
(36)

For the molecular case the contributions of the rotational and vibrational energy must also be included. According to equations (4) and (5) the expression

$$\left(\frac{\mathbf{E}}{\mathbf{RT}}\right)_{\mathbf{r}+\mathbf{v}} = 1 + \frac{\mathbf{h}\mathbf{v}}{\mathbf{kT}} \left(\mathbf{e}^{\frac{\mathbf{h}\mathbf{v}}{\mathbf{kT}}} - 1\right)^{-1}$$
(37)

should be added to equations (35) and (36).

The specific heat per mol at constant density of pure gas is

$$\left(\frac{c_{v}}{R}\right)_{t+e} = \frac{3}{2} + \frac{\sum \left(\frac{\epsilon_{n}}{kT}\right)^{2} g_{n} e^{-\frac{\epsilon_{n}}{kT}}}{\sum g_{n} e^{-\frac{\epsilon_{n}}{kT}}} - \left(\frac{\sum \frac{\epsilon_{n}}{kT} g_{n} e^{-\frac{\epsilon_{n}}{kT}}}{\sum g_{n} e^{-\frac{\epsilon_{n}}{kT}}}\right)^{2}$$
(38)

For the diatomic molecules

$$\left(\frac{c_{v,int}}{R}\right)_{r+v} = 1 + \left(\frac{h\nu}{2kT}\right)^2 \left(\sinh\frac{h\nu}{2kT}\right)^{-2}$$
(39)

should be added to equation (38). The specific heat per mol at constant pressure of a pure gas is

$$\left(\frac{c_{\rm p}}{R}\right)_{\rm t+e} = \left(\frac{c_{\rm v}}{R}\right)_{\rm t+e} + 1 \tag{40}$$

The entropy is

$$\frac{S}{R} = \ln Q + T \left( \frac{\partial \ln Q}{\partial T} \right)_{p}$$
(41)

# Gas Mixture

Once the preceding relations have been determined the thermodynamic properties of the mixture follow readily. The energy per mol of mixture, in the nondimensional form, is simply

$$\frac{ZE}{RT} = Z \sum_{i} \frac{E_{i}}{RT}$$
(42)

and the dimensionless enthalpy per initial mol is

$$\frac{ZH}{RT} = \frac{ZE}{RT} + Z$$
(43)

The entropy per mol is obtained from the entropies of the components by use of

$$\frac{ZS}{R} = Z\left(\sum_{i} x_{i} \frac{S_{o,i}}{R} - \sum_{i} x_{i} \ln x_{i} - \ln \frac{p}{p_{o}}\right)$$
(44)

The specific heat at constant volume is given by

$$\frac{Zc_{v}}{R} = \frac{1}{R} \left( \frac{\partial ZE}{\partial T} \right)_{\rho} = Z \sum_{i} x_{i} \frac{c_{v,i}}{R} + T \sum_{i} \left( \frac{E_{i}}{RT} \right) \left( \frac{\partial Zx_{i}}{\partial T} \right)_{\rho}$$
(45)

The corresponding specific heat for constant pressure is

$$\frac{Zc_{p}}{R} = \frac{1}{R} \left( \frac{\partial ZH}{\partial T} \right)_{p} = Z \sum_{i} x_{i} \left( \frac{c_{v,i}}{R} + 1 \right) + T \sum_{i} \left( \frac{E_{i}}{RT} + 1 \right) \left( \frac{\partial Zx_{i}}{\partial T} \right)_{p}$$
(46)

The ratio of specific heats  $\gamma$  is used to obtain the dimensionless speed-of-sound parameter which is given by

$$\frac{a^{2}\rho}{p} = \gamma \frac{1 + \left(\frac{T}{Z}\right) \left(\frac{\partial Z}{\partial T}\right)_{\rho}}{1 + \left(\frac{T}{Z}\right) \left(\frac{\partial Z}{\partial T}\right)_{p}}$$
(47)

# DESCRIPTION OF CHARTS

The preceding equations have been used in a computer program to solve for the equilibrium thermodynamic properties of four nitrogen-oxygen mixtures. The temperature ranges from  $200^{\circ}$  to  $15,000^{\circ}$  K and the pressure ranges from  $10^{-4}$  to  $10^2$  atmospheres. The data are presented in charts and tables. The charts 'appear just as they came from the computer-plotting system, which accounts for the minor waviness in some of the curves.

Included on the plots of enthalpy against entropy are lines of constant temperature and pressure. Molecular-weight ratio Z is plotted as a function of temperature with lines of constant pressure shown. Constant-density lines are not included. The density can be computed from the equation of state.

Figure 1 is a key for all the thermodynamic charts. Figure 1(a) shows the range of enthalpies and entropies to be found in the first 17 charts of each mixture and figure 1(b) shows the range of temperature and molecular-weight ratio Z to be found in the succeeding 4 charts (charts 18 to 21) for each composition. The curves used for reference on figure 1 are for the mixture of 80 percent  $N_2$  and 20 percent  $O_2$ . The pressure divisions are noted only one time on each chart, but the divisions are consistent throughout all the data as five equal divisions between orders of magnitude.

Data for each composition are presented in thermodynamic charts and in reference tables of the ratio of specific heats  $\gamma$  and the dimensionless speed-of-sound parameter  $a^2\rho/p$ . The tables for each composition are placed immediately after the charts for the same composition. Data for 100 percent N<sub>2</sub> are given in figure 2 and table II; for 97 percent N<sub>2</sub> and 3 percent O<sub>2</sub>, in figure 3 and table III; for 90 percent N<sub>2</sub> and 10 percent O<sub>2</sub>, in figure 4 and table IV; and for 80 percent N<sub>2</sub> and 20 percent O<sub>2</sub>, in figure 5 and table V. Figure 6 is a comparison of the degree of difference between the enthalpies of the two end-point compositions as a function of temperature at 1 atmosphere of pressure.

### ACCURACY OF RESULTS

The data presented for  $N_2$  in figure 2 and table II show close agreement with the data in reference 6. A maximum deviation in any parameter is less than 1.0 percent up to the temperature range where the double-ionization reaction occurs in reference 6. Since only single ionization was considered in the present paper, these data for higher temperatures are not comparable. A deviation of several percent exists at these higher temperatures.

Since essentially the same program used in reference 3 was used to obtain the data presented in figure 5, the results agree within about 0.5 percent. The specific heat ratios in table V also agree within about 0.5 percent with those of reference 3. The values of dimensionless speed-of-sound parameter, however, deviate from those in reference 3 by as much as 4 percent in the temperature range of nitrogen ionization. This difference is attributed to an omission of a factor of 2 in the ionization fraction of equation (A86) of reference 7 which is the basic program used in reference 3.

There are no data with which to compare figures 3 and 4 and tables III and IV but since the same program was checked at the end-point compositions it is assumed that the results are as valid as those for 100 percent  $N_2$  and for 80 percent  $N_2$  and 20 percent  $O_2$ . It should be noted that because of the unchanging limits of corresponding charts for each mixture, chart 4 of figure 2 has been omitted since no data for that mixture fell within the limits.

Langley Research Center, National Aeronautics and Space Administration, Langley Station, Hampton, Va., December 21, 1964.

# APPENDIX A

### PRESSURE-INDEPENDENT PARTITION-FUNCTION EXPRESSIONS

The following equations for the pressure-independent partition functions, where temperature is in  ${}^{O}K$ , were used in the calculations of the thermodynamic properties for nitrogen-oxygen mixtures:

$$\ln Q_p(N_2) = \frac{7}{2} \ln T - 0.42 - \ln \left(1 - e^{-\frac{3390}{T}}\right)$$

$$\ln Q_{p}(O_{2}) = \frac{7}{2} \ln T + 0.11 - \ln \left(1 - e^{\frac{2270}{T}}\right) + \ln \left(3 + 2e^{\frac{11390}{T}} - \frac{18990}{T}\right)$$

$$\ln Q_{p}(0) = \frac{5}{2} \ln T + 0.50 + \ln \left( 5 + 3e^{\frac{-228}{T}} + e^{\frac{-326}{T}} + 5e^{\frac{-22800}{T}} + e^{\frac{-48600}{T}} \right)$$

$$\ln Q_{\rm p}(N) = \frac{5}{2} \ln T + 0.30 + \ln \left( \frac{27700}{4} + 10e^{\frac{27700}{T}} + 6e^{\frac{41500}{T}} \right)$$

$$\ln Q_{p}(0^{+}) = \frac{5}{2} \ln T + 0.50 + \ln \left( \frac{-\frac{38600}{T}}{4 + 10e} - \frac{58200}{T} \right)$$

$$\ln Q_{p}(N^{+}) = \frac{5}{2} \ln T + 0.30 + \ln \left( 1 + 3e^{\frac{70.6}{T}} - \frac{188.9}{T} - \frac{22000}{T} + 5e^{\frac{70.6}{T}} + 5e^{\frac{188.9}{T}} + 5e^{\frac{70.6}{T}} + 5e^{\frac{$$

$$-\frac{47000}{T} - \frac{67900}{T}$$

 $\ln Q_p(e^-) = \frac{5}{2} \ln T - 14.24$ 

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Ionization energy, I/k, oK			158,000	168,800			
Electronic energy, $\epsilon_n/k$ , $o_K$	0	0 11, 390 18, 990	0 228 326 148, 600	27,700 41,500	38, 600 58, 200	0 70.6 188.9 47,000 67,900	0
Electronic degeneracy, gn	1	гои	うろうろし	4 0 9 9	10 t	ユッララーち	Q
Dissociation energy, D/k, o <sub>K</sub>	113,200	59, 000					
Vibrational constant, hv/k, o <sub>K</sub>	3390	2270					
Rotational constant, $\frac{\alpha h^2}{\delta \pi^2 T k}$	5.78	4.16					
Molecular weight, M <sub>i</sub> , g/mol	28	32	16	14	16	74	1 1820
Particle	N2 N2	°0	0	N	+0	+ N	υ

TABLE I.- PARTITION-FUNCTION CONSTANTS







Dimensionless entropy



Figure 1.- Continued.

oiten theisw-heluceloM









Figure 2.- Thermodynamic charts for 100 percent  $\mathrm{N}_{2}.$ 



Chart 2

Figure 2.- Thermodynamic charts for 100 percent  $\mathrm{N}_2.$  Continued.





Figure 2.- Thermodynamic charts for 100 percent  $\ensuremath{\mathbb{N}_2}\xspace$  . Continued.

NOTE: No data appear on chart 4 for this composition.

Chart 4

Figure 2.- Thermodynamic charts for 100 percent  $\mathrm{N}_{2}.$  Continued.





Figure 2.- Thermodynamic charts for 100 percent  $\mathrm{N}_{2}.$  Continued.



Chart 6

Figure 2.- Thermodynamic charts for 100 percent  $\mathrm{N}_2.$  Continued.





Figure 2.- Thermodynamic charts for 100 percent  $\mathrm{N}_2.$  Continued.



Chart 8

Figure 2.- Thermodynamic charts for 100 percent  $N_2$ . Continued.





Figure 2.- Thermodynamic charts for 100 percent  $\mathrm{N}_2.$  Continued.





Figure 2.- Thermodynamic charts for 100 percent  $\ensuremath{\mathtt{N}}_2$  . Continued.





Figure 2.- Thermodynamic charts for 100 percent  $\mathrm{N}_2^{}\,.$  Continued.



Chart 12

Figure 2.- Thermodynamic charts for 100 percent  $\mathrm{N}_2.$  Continued.


Chart 13

Figure 2.- Thermodynamic charts for 100 percent  $\ensuremath{\mathtt{N}}_2.$  Continued.



Chart 14

Figure 2.- Thermodynamic charts for 100 percent  $\mathrm{N}_2.$  Continued.





Figure 2.- Thermodynamic charts for 100 percent  ${\rm N}_2.$  Continued.



Figure 2.- Thermodynamic charts for 100 percent  $\mathrm{N}_2.$  Continued.



Chart 17

Figure 2.- Thermodynamic charts for 100 percent  $\mathrm{N}_2.$  Continued.



Figure 2.- Thermodynamic charts for 100 percent  $N_2$ . Continued.





Figure 2.- Thermodynamic charts for 100 percent  $\mathrm{N}_{2}.$  Continued.



Chart 20

Figure 2.- Thermodynamic charts for 100 percent  $\mathrm{N}_2.$  Continued.





Figure 2.- Thermodynamic charts for 100 percent  $N_2$ . Concluded.

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## TABLE II. - THERMODYNAMIC PROPERTIES OF 100 PERCENT N2

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т,	Pressure, atmospheres, of -							
°ĸ	100	10	1.0	0.1	0.01	0.001	0.0001	
400 600 800 1,000 1,200 1,400 1,600 1,800 2,000 2,200 2,400 2,600 2,800 3,000 3,200 3,400 3,600 3,600 3,800 4,000 4,400 4,600 4,400 4,600 4,400 4,600 5,000 5,200 5,400 5,600 5,200 5,400 5,600 5,200 5,400 5,000 5,200 5,400 5,000 5,200 5,400 5,000 5,200 5,400 5,000 5,200 5,500 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000	1.00 1.3976 1.3827 1.3614 1.3431 1.3295 1.3198 1.3128 1.3077 1.3038 1.3009 1.2986 1.2953 1.2941 1.2930 1.2940 1.2930 1.2910 1.2930 1.2920 1.2910 1.2838 1.2833 1.2861 1.2832 1.2739 1.2595 1.2508 1.2595 1.2508 1.2415 1.2595 1.2508 1.2415 1.2595 1.2508 1.2415 1.2595 1.2508 1.2415 1.2595 1.2508 1.2415 1.2595 1.2508 1.2415 1.2595 1.2508 1.2415 1.2595 1.2508 1.2415 1.2595 1.2508 1.2415 1.2595 1.2508 1.2415 1.2595 1.2508 1.2415 1.2595 1.2508 1.2415 1.2595 1.2508 1.2415 1.2595 1.2508 1.2415 1.2595 1.2508 1.2415 1.2595 1.2508 1.2415 1.2595 1.2508 1.2131 1.2595 1.2508 1.2131 1.2595 1.2508 1.2131 1.2595 1.2508 1.2934 1.2034 1.2131 1.2595 1.2508 1.2151 1.2730 1.2739 1.2673 1.2595 1.2508 1.2151 1.2730 1.2739 1.2739 1.2739 1.2673 1.2595 1.2508 1.2131 1.2748 1.2748 1.2748 1.2748 1.2730	1.0 1.3976 1.3827 1.3614 1.3431 1.3295 1.3198 1.3128 1.3077 1.3038 1.3009 1.2986 1.2953 1.2940 1.2968 1.2953 1.2940 1.2928 1.2953 1.2940 1.2928 1.2953 1.2836 1.2781 1.2704 1.2603 1.2481 1.2209 1.2246 1.2209 1.2246 1.2209 1.2285 1.2298 1.2977 1.2580 1.2944 1.2580 1.2944 1.2772 1.2585 1.2502 1.2497 1.2427 1.2427 1.2427 1.2427 1.2427	1.0 1.3976 1.3827 1.3614 1.3295 1.3198 1.3128 1.3077 1.3038 1.3009 1.2986 1.2952 1.2952 1.2952 1.2938 1.2967 1.2952 1.2938 1.2952 1.2938 1.2952 1.2938 1.2952 1.2938 1.2952 1.2971 1.2564 1.2564 1.2564 1.2564 1.2797 1.264 1.2797 1.266 1.1755 1.1714 1.1756 1.1755 1.1714 1.2696 1.2734 1.2696 1.2349 1.2349 1.2340 1.2252 1.2178 1.2252 1.2361 1.2358 1.2252 1.2361 1.2340 1.2252 1.2178 1.2252 1.2361 1.2358 1.2252 1.2361 1.2358 1.2252 1.2361 1.2358 1.2252 1.2361 1.2358 1.2252 1.2361 1.2358 1.2252 1.2361 1.2358 1.2252 1.2361 1.2358 1.2252 1.2358 1.25588 1.25588 1.25588 1.25588 1.25588 1.25588 1.25588 1.2	0.1         1.3976         1.3827         1.3614         1.3431         1.3295         1.3198         1.3128         1.3077         1.3038         1.3009         1.2950         1.2950         1.2950         1.2950         1.2950         1.2930         1.2930         1.2930         1.2930         1.2972         1.2119         1.1584         1.1567         1.1636         1.1783         1.2930         1.2233         1.2592         1.2840         1.3008 <td>1. <math>3976</math> 1. <math>3827</math> 1. <math>3614</math> 1. <math>3431</math> 1. <math>3295</math> 1. <math>3128</math> 1. <math>3077</math> 1. <math>3038</math> 1. <math>3009</math> 1. <math>2985</math> 1. <math>2965</math> 1. <math>2943</math> 1. <math>2965</math> 1. <math>2943</math> 1. <math>2965</math> 1. <math>2943</math> 1. <math>2692</math> 1. <math>2458</math> 1. <math>2458</math> 1. <math>1457</math> 1. <math>1828</math> 1. <math>1457</math> 1. <math>1457</math> 1. <math>1280</math> 1. <math>2091</math> 1. <math>2251</math> 1. <math>2475</math> 1. <math>2475</math> 1. <math>2475</math> 1. <math>2475</math> 1. <math>2475</math> 1. <math>2475</math> 1. <math>2475</math> 1. <math>2219</math> 1. <math>2251</math> 1. <math>2252</math> 1. <math>1943</math> 1. <math>1785</math> 1. <math>1282</math> 1. <math>2252</math> 1. <math>1943</math> 1. <math>1282</math> 1. <math>2252</math> 1. <math>1943</math> 1. <math>1285</math> 1. <math>2630</math> 1. <math>2774</math> 1. <math>2637</math> 1. <math>2560</math> 1. <math>2560</math></td> <td>1. <math>3976</math> 1. <math>3827</math> 1. <math>3614</math> 1. <math>3431</math> 1. <math>3295</math> 1. <math>3128</math> 1. <math>3077</math> 1. <math>3038</math> 1. <math>3009</math> 1. <math>2984</math> 1. <math>2960</math> 1. <math>2920</math> 1. <math>2834</math> 1. <math>2960</math> 1. <math>2920</math> 1. <math>2834</math> 1. <math>2960</math> 1. <math>2920</math> 1. <math>2834</math> 1. <math>2648</math> 1. <math>1368</math> 1. <math>1368</math> 1. <math>1368</math> 1. <math>1346</math> 1. <math>1493</math> 1. <math>1779</math> 1. <math>2119</math> 1. <math>2292</math> 1. <math>2052</math> 1. <math>1870</math> 1. <math>1896</math> 1. <math>2115</math> 1. <math>2480</math> 1. <math>2035</math> 1. <math>1651</math> 1. <math>2480</math> 1. <math>2235</math> 1. <math>1651</math> 1. <math>2461</math> 1. <math>22558</math> 1. <math>2558</math> 1. <math>2558</math> 1. <math>2601</math> 1. <math>2467</math> 1. <math>2975</math> 1. <math>2467</math> 1. <math>2975</math> 1. <math>3687</math></td> <td>1. <math>3976</math> 1. <math>3827</math> 1. <math>3614</math> 1. <math>3431</math> 1. <math>3295</math> 1. <math>3198</math> 1. <math>3128</math> 1. <math>3077</math> 1. <math>3038</math> 1. <math>2981</math> 1. <math>2942</math> 1. <math>2852</math> 1. <math>2633</math> 1. <math>2981</math> 1. <math>2942</math> 1. <math>2633</math> 1. <math>2225</math> 1. <math>1733</math> 1. <math>1240</math> 1. <math>1240</math> 1. <math>1247</math> 1. <math>1655</math> 1. <math>2051</math> 1. <math>2073</math> 1. <math>1777</math> 1. <math>1736</math> 1. <math>2028</math> 1. <math>2455</math> 1. <math>2655</math> 1. <math>2544</math> 1. <math>1617</math> 1. <math>2008</math> 1. <math>2411</math> 1. <math>2123</math> 1. <math>2114</math> 1. <math>2623</math> 1. <math>3528</math> 1. <math>4464</math> 1. <math>5143</math> 1. <math>5538</math> 1. <math>5736</math></td>	1. $3976$ 1. $3827$ 1. $3614$ 1. $3431$ 1. $3295$ 1. $3128$ 1. $3077$ 1. $3038$ 1. $3009$ 1. $2985$ 1. $2965$ 1. $2943$ 1. $2965$ 1. $2943$ 1. $2965$ 1. $2943$ 1. $2692$ 1. $2458$ 1. $2458$ 1. $1457$ 1. $1828$ 1. $1457$ 1. $1457$ 1. $1280$ 1. $2091$ 1. $2251$ 1. $2475$ 1. $2475$ 1. $2475$ 1. $2475$ 1. $2475$ 1. $2475$ 1. $2475$ 1. $2219$ 1. $2251$ 1. $2252$ 1. $1943$ 1. $1785$ 1. $1282$ 1. $2252$ 1. $1943$ 1. $1282$ 1. $2252$ 1. $1943$ 1. $1285$ 1. $2630$ 1. $2774$ 1. $2637$ 1. $2560$ 1. $2560$	1. $3976$ 1. $3827$ 1. $3614$ 1. $3431$ 1. $3295$ 1. $3128$ 1. $3077$ 1. $3038$ 1. $3009$ 1. $2984$ 1. $2960$ 1. $2920$ 1. $2834$ 1. $2960$ 1. $2920$ 1. $2834$ 1. $2960$ 1. $2920$ 1. $2834$ 1. $2648$ 1. $1368$ 1. $1368$ 1. $1368$ 1. $1346$ 1. $1493$ 1. $1779$ 1. $2119$ 1. $2292$ 1. $2052$ 1. $1870$ 1. $1896$ 1. $2115$ 1. $2480$ 1. $2035$ 1. $1651$ 1. $2480$ 1. $2235$ 1. $1651$ 1. $2461$ 1. $22558$ 1. $2558$ 1. $2558$ 1. $2601$ 1. $2467$ 1. $2975$ 1. $2467$ 1. $2975$ 1. $3687$	1. $3976$ 1. $3827$ 1. $3614$ 1. $3431$ 1. $3295$ 1. $3198$ 1. $3128$ 1. $3077$ 1. $3038$ 1. $2981$ 1. $2942$ 1. $2852$ 1. $2633$ 1. $2981$ 1. $2942$ 1. $2633$ 1. $2225$ 1. $1733$ 1. $1240$ 1. $1240$ 1. $1247$ 1. $1655$ 1. $2051$ 1. $2073$ 1. $1777$ 1. $1736$ 1. $2028$ 1. $2455$ 1. $2655$ 1. $2544$ 1. $1617$ 1. $2008$ 1. $2411$ 1. $2123$ 1. $2114$ 1. $2623$ 1. $3528$ 1. $4464$ 1. $5143$ 1. $5538$ 1. $5736$	
13,500 14,000 14,500 15,000	$ \begin{array}{c} 1.2735\\ 1.2745\\ 1.2764\\ 1.2798 \end{array} $	1.2535 1.2642 1.2777 1.2934	1.2929 1.3125 1.3275 1.3361	1.3009 1.2930 1.2898 1.2963	1.2963 1.3427 1.3963 1.4478	1.4970 1.5356 1.5597 1.5740	1.5852 1.5905 1.5932 1.5945	

(a)	Ratio	of	specific	heats	γ

т,	Pressure, atmospheres, of -							
<sup>o</sup> ĸ	100	10	1.0	0.1	0.01	0.001	0.0001	
T, K 400 600 800 1,000 1,200 1,400 1,600 1,800 2,000 2,200 2,400 2,600 2,800 3,000 3,200 3,400 3,600 3,800 4,000 4,400 4,600 4,800 5,200 5,400 5,600 5,800 6,000 6,500 7,000 7,500 8,000 8,500	100 1. 3976 1. 3827 1. 3614 1. 3431 1. 3295 1. 3198 1. 3128 1. 3077 1. 3038 1. 3009 1. 2986 1. 2968 1. 2953 1. 2941 1. 2930 1. 2920 1. 2910 1. 2898 1. 2882 1. 2860 1. 2829 1. 2787 1. 2662 1. 2578 1. 2482 1. 2577 1. 2269 1. 2161 1. 1920 1. 1749 1. 1650 1. 1607 1. 1605	10 1.3976 1.3827 1.3614 1.3431 1.3295 1.3198 1.3128 1.3077 1.3038 1.3009 1.2986 1.2968 1.2953 1.2940 1.2928 1.2915 1.2898 1.2915 1.2898 1.2977 1.2697 1.2697 1.2591 1.2461 1.2313 1.2158 1.2006 1.1867 1.1746 1.1648 1.1490 1.1431 1.1436 1.1484 1.1569	Pressure, 1.0 1.3976 1.3827 1.3614 1.3431 1.3295 1.3198 1.3077 1.3038 1.3077 1.3038 1.3009 1.2986 1.2967 1.2952 1.2958 1.2971 1.2858 1.2795 1.2695 1.2695 1.2553 1.2553 1.2553 1.2165 1.1955 1.1604 1.1481 1.1392 1.1322 1.1296 1.1279 1.1332 1.1445 1.1635 1.1900	0.1 1.3976 1.3827 1.3614 1.3431 1.3295 1.3198 1.3077 1.3038 1.3009 1.2986 1.2950 1.2035 1.1161 1.1144 1.1147 1.1166 1.272 1.2055 1.2179 1.2105 1.2105 1.2105 1.2055 1.2105 1.2055 1.2179 1.2055 1.2105 1.2055 1.	0.01 1.3976 1.3976 1.3614 1.3614 1.3614 1.3295 1.3198 1.3128 1.3077 1.3038 1.3009 1.2985 1.2965 1.2942 1.2906 1.2832 1.2688 1.2447 1.2121 1.1774 1.1479 1.1269 1.1277 1.1055 1.1035 1.1035 1.1035 1.1053 1.1053 1.1051 1.1055	0.001 1.3976 1.3827 1.3614 1.3431 1.3295 1.3198 1.3077 1.3038 1.3009 1.2984 1.2960 1.2920 1.2833 1.2644 1.2313 1.1888 1.1493 1.1211 1.1046 1.0965 1.0937 1.0943 1.1032 1.1131 1.1300 1.1569 1.1928 1.2409 1.1944 1.1499 1.1267 1.1172	0.0001 1.3976 1.3827 1.3614 1.3431 1.3295 1.3198 1.3128 1.3077 1.3038 1.2981 1.2942 1.2851 1.2628 1.2211 1.1692 1.1269 1.1692 1.1269 1.0897 1.0861 1.0897 1.0861 1.0897 1.0861 1.0897 1.0861 1.2366 1.2609 1.2495 1.1747 1.1280 1.1040 1.1040 1.040	
8,500 9,000 9,500 10,000	1.1605 1.1633 1.1685 1.1758	1.1569 1.1693 1.1859 1.2041	1.1900 1.2122 1.2164 1.2067	1.2105 1.1880 1.1686 1.1561	1.1527 1.1375 1.1308 1.1295	1.1172 1.1155 1.1188 1.1268	1.1062 1.1146 1.1330 1.1718	
10,500 11,000 11,500 12,000 12,500 13,000 13,500 14,000	1.1853 1.1970 1.2100 1.2227 1.2331 1.2398 1.2427 1.2428	1.2181 1.2237 1.2217 1.2161 1.2099 1.2047 1.2010 1.1989	1.1937 1.1828 1.1753 1.1710 1.1694 1.1699 1.1722 1.1760	1.1494 1.1470 1.1478 1.1511 1.1566 1.1646 1.1757 1.1907	1.1321 1.1380 1.1476 1.1625 1.1854 1.2194 1.2661 1.3229	1.1414 1.1676 1.2121 1.2780 1.3575 1.4336 1.4930 1.5332	1.2434 1.3435 1.4417 1.5118 1.5525 1.5739 1.5848 1.5902	
14,500 15,000	1.2415 1.2397	1.1982	1.1814	1.2111 1.2378	1.3833 1.4390	1.5581 1.5730	1.5930 1.5944	

(ъ)	Dimensionless	speed-of-sound	parameter	a <sup>2</sup> o/p
(0)	DTHEIRTOUTESS	speed-or-sound	parameter	a p/p





Figure 3.- Thermodynamic charts for 97 percent  $\rm N_2$  and 3 percent  $\rm O_2.$ 



Figure 3.- Thermodynamic charts for 97 percent  $\mathrm{N_2}$  and 3 percent  $\mathrm{O_2}.$  Continued.





Figure 3.- Thermodynamic charts for 97 percent  $\mathrm{N}_2$  and 3 percent  $\mathrm{O}_2.$  Continued.



Figure 3.- Thermodynamic charts for 97 percent  $\rm N_2$  and 3 percent  $\rm O_2.$  Continued.



Chart 5

Figure 3.- Thermodynamic charts for 97 percent  $N_2$  and 3 percent  $O_2$ . Continued.





Figure 3.- Thermodynamic charts for 97 percent  $N_{\rm 2}$  and 3 percent  $0_{\rm 2}.$  Continued.





Figure 3.- Thermodynamic charts for 97 percent  $N_2$  and 3 percent  $O_2$ . Continued.



Figure 3.- Thermodynamic charts for 97 percent  $\rm N_2$  and 3 percent  $\rm O_2.$  Continued.



Chart 9

Figure 3.- Thermodynamic charts for 97 percent  $\rm N_2$  and 3 percent  $\rm O_2.$  Continued.



Figure 3.- Thermodynamic charts for 97 percent  $\rm N_2$  and 3 percent  $\rm O_2.$  Continued.





Figure 3.- Thermodynamic charts for 97 percent  $\mathrm{N}_2$  and 3 percent  $\mathrm{O}_2.$  Continued.



Chart 12

Figure 3.- Thermodynamic charts for 97 percent  $\rm N_2$  and 3 percent  $\rm O_2.$  Continued.





Figure 3.- Thermodynamic charts for 97 percent  $\mathrm{N}_2$  and 3 percent  $\mathrm{O}_2.$  Continued.



Chart 14

Figure 3.- Thermodynamic charts for 97 percent N2 and 3 percent O2. Continued.





Figure 3.- Thermodynamic charts for 97 percent  $N_{\rm 2}$  and 3 percent  $0_{\rm 2}.$  Continued.



Figure 3.- Thermodynamic charts for 97 percent  $\rm N_2$  and 3 percent  $\rm O_2.$  Continued.





Figure 3.- Thermodynamic charts for 97 percent  $\mathrm{N}_2$  and 3 percent  $\mathrm{O}_2.$  Continued.



Chart 18

Figure 3.- Thermodynamic charts for 97 percent  $\mathrm{N}_2$  and 3 percent  $\mathrm{O}_2.$  Continued.



Chart 19

Figure 3.- Thermodynamic charts for 97 percent  $\rm N_2$  and 3 percent  $\rm O_2.$  Continued.



Chart 20

Figure 3.- Thermodynamic charts for 97 percent  $\rm N_2$  and 3 percent  $\rm O_2.$  Continued.



Chart 21

Figure 3.- Thermodynamic charts for 97 percent  $\rm N_2$  and 3 percent  $\rm O_2.$  Concluded.

## TABLE III.- THERMODYNAMIC PROPERTIES OF 97 PERCENT N<sub>2</sub> AND 3 PERCENT $O_2$

т.	Pressure, atmospheres, of -							
<sup>ô</sup> K	100	10	1.0	0.1	0.01	0.001	0.0001	
400 600 800 1,000 1,200 1,400 1,600 2,200 2,400 2,600 2,200 2,400 2,600 2,800 3,200 3,200 3,600 3,600 3,600 3,600 3,600 4,000 4,600 4,600 4,600 4,600 5,200 5,600 1,000	100 1.3972 1.3817 1.3604 1.3422 1.3288 1.3192 1.3071 1.3031 1.2997 1.2965 1.2929 1.2886 1.2835 1.2778 1.2721 1.2670 1.2634 1.2618 1.2657 1.2657 1.2657 1.2657 1.2657 1.2657 1.2654 1.2654 1.2614 1.2614 1.2614 1.2614 1.2654 1.2756 1.2654 1.2752 1.2752 1.2754 1.2754	10 1. $3972$ 1. $3817$ 1. $3604$ 1. $3422$ 1. $3288$ 1. $3192$ 1. $3122$ 1. $3070$ 1. $2984$ 1. $2932$ 1. $2932$ 1. $2932$ 1. $2671$ 1. $2522$ 1. $2508$ 1. $2521$ 1. $2671$ 1. $2659$ 1. $22529$ 1. $263$ 1. $2131$ 1. $2019$ 1. $1938$ 1. $2190$ 1. $2553$ 1. $2846$ 1. $2738$ 1. $2572$ 1. $2509$ 1. $2509$ 1. $2509$ 1. $2509$ 1. $22509$ 1. $2437$ 1. $2470$	1.0 1.3972 1.3817 1.3604 1.3422 1.3288 1.3192 1.3122 1.3067 1.3014 1.2944 1.2839 1.2693 1.2693 1.2695 1.2696 1.2703 1.2611 1.2452 1.2696 1.2703 1.2611 1.2452 1.2258 1.2066 1.1902 1.1786 1.1727 1.1728 1.1786 1.1727 1.1788 1.2650 1.2727 1.2254 1.2254 1.22510 1.2714	0.1         1.3972         1.3817         1.3604         1.3422         1.3288         1.3192         1.3057         1.2973         1.2829         1.2610         1.2380         1.2256         1.2314         1.2532         1.2729         1.2610         1.2380         1.2256         1.2314         1.2532         1.2729         1.2610         1.2380         1.2517         1.922         1.1723         1.1606         1.1579         1.1639         1.1777         1.976         1.2204         1.2212         1.2212         1.22517         1.2212         1.2250         1.2250         1.2359         1.2663         1.963         1.963         1.963         1.963         1.963         1.2592         1.2839         1.3008         1.3060	$\begin{array}{c} 0.01 \\ \hline 1.3972 \\ 1.3817 \\ 1.3604 \\ 1.3422 \\ 1.3288 \\ 1.3191 \\ 1.3115 \\ 1.3025 \\ 1.2855 \\ 1.2555 \\ 1.2555 \\ 1.2555 \\ 1.2555 \\ 1.2555 \\ 1.2681 \\ 1.2831 \\ 1.2754 \\ 1.2528 \\ 1.2681 \\ 1.2754 \\ 1.2528 \\ 1.2206 \\ 1.1872 \\ 1.1612 \\ 1.1473 \\ 1.1464 \\ 1.1576 \\ 1.1790 \\ 1.2061 \\ 1.2307 \\ 1.2422 \\ 1.2355 \\ 1.2182 \\ 1.2061 \\ 1.2307 \\ 1.2422 \\ 1.2355 \\ 1.2651 \\ 1.2650 \\ 1.2656 \\ 1.265$	1. $3972$ 1. $3817$ 1. $3604$ 1. $3422$ 1. $3288$ 1. $3190$ 1. $2931$ 1. $2569$ 1. $2132$ 1. $2004$ 1. $2371$ 1. $2808$ 1. $2371$ 1. $2808$ 1. $2724$ 1. $2396$ 1. $1973$ 1. $1602$ 1. $1386$ 1. $1352$ 1. $1487$ 1. $1758$ 1. $2081$ 1. $2289$ 1. $2240$ 1. $2016$ 1. $1859$ 1. $2045$ 1. $1695$ 1. $1654$ 1. $2235$ 1. $2559$ 1. $2605$ 1. $2409$ 1. $2287$ 1. $2462$ 1. $2962$ 1. $3665$ 1. $4372$	1. 3972 1. 3972 1. 3817 1. 3604 1. 3422 1. 3288 1. 3185 1. 3047 1. 2687 1. 2102 1. 1878 1. 2378 1. 2291 1. 1777 1. 1393 1. 1250 1. 1745 1. 2011 1. 2201 1. 2202 1. 2207 1. 2501 1. 2207 1. 2501 1. 2207 1. 2500 1. 5500 1. 5706	
14,000 14,500 15,000	1.2757 1.2775 1.2806	1.2645 1.2778 1.2934	1.3124 1.3274 1.3360	1.2932 1.2897 1.2958	1.3407 1.3937 1.4445	1.5317 1.5555 1.5698	1.5862 1.5889 1.5902	

## (a) Ratio of specific heats $\gamma$

т,	Pressure, atmospheres, of -							
oĸ	100	10	1.0	0.1	0.01	0.001	0.0001	
400 600 800 1,000 1,200 1,400 1,600 2,000 2,200 2,400 2,600 2,800 3,200 3,200 3,200 3,400 3,600 3,200 3,600 3,200 3,600 3,600 4,000 4,600 4,600 4,600 5,600 5,600 5,600 5,600 5,600 5,600 5,600 5,600 5,600 5,600 5,600 5,600 5,600 5,600 5,900 1,000	1.3972 1.3817 1.3604 1.3422 1.3288 1.3192 1.3123 1.3071 1.3031 1.2997 1.2964 1.2927 1.2883 1.2828 1.2766 1.2700 1.2640 1.2592 1.2594 1.2594 1.2594 1.2594 1.2594 1.2594 1.2503 1.2415 1.2514 1.2503 1.2415 1.2514 1.2503 1.2415 1.2514 1.2503 1.2415 1.2514 1.2503 1.2415 1.2514 1.2503 1.2415 1.2514 1.2609 1.2604 1.2568 1.2503 1.2415 1.2514 1.2505 1.2415 1.2514 1.2505 1.2415 1.2514 1.2505 1.2415 1.2514 1.2505 1.2415 1.2514 1.2505 1.2415 1.2514 1.2505 1.2415 1.2514 1.2505 1.2415 1.2514 1.2505 1.2415 1.2514 1.2505 1.2415 1.2514 1.2505 1.2415 1.2514 1.2505 1.2415 1.2514 1.2505 1.2415 1.2514 1.2505 1.2415 1.2514 1.2505 1.2415 1.2505 1.2415 1.2505 1.2415 1.2505 1.2415 1.2505 1.2415 1.2505 1.2415 1.2505 1.2415 1.2505 1.2415 1.2505 1.2455 1.2505 1.2455 1.2505 1.2455 1.2555 1.2455 1.2555 1.2455 1.2555 1.2455 1.2555 1.2455 1.2555 1.2455 1.2555 1.2455 1.2555 1.2455 1.2555 1.2455 1.2555 1.2455 1.2555 1.2455 1.2555 1.2455 1.2555 1.2455 1.2555 1.2455 1.2555 1.2455 1.2555 1.2455 1.255	1. $3972$ 1. $3817$ 1. $3604$ 1. $3422$ 1. $3288$ 1. $3192$ 1. $3192$ 1. $3070$ 1. $3027$ 1. $2984$ 1. $2931$ 1. $2655$ 1. $2655$ 1. $2655$ 1. $2655$ 1. $2250$ 1. $2474$ 1. $2655$ 1. $2250$ 1. $2474$ 1. $2637$ 1. $2296$ 1. $2299$ 1. $2261$ 1. $2054$ 1. $1909$ 1. $12546$ 1. $2209$ 1. $2254$ 1. $2209$ 1. $2254$ 1. $2209$ 1. $2254$ 1. $1909$ 1. $1784$ 1. $1680$ 1. $1513$ 1. $1449$ 1. $1513$ 1. $1449$ 1. $1584$ 1. $1584$ 1. $1257$ 1. $2261$ 1. $2276$ 1. $2276$	1.3972 1.3817 1.3604 1.3422 1.3288 1.3192 1.3067 1.3013 1.2942 1.2834 1.2680 1.2507 1.2395 1.2544 1.2667 1.2684 1.2593 1.2427 1.2667 1.2684 1.2593 1.2427 1.2200 1.2004 1.1805 1.1638 1.1509 1.1414 1.1511 1.1512 1.1291 1.1343 1.1459 1.1657 1.2153 1.2188 1.2085 1.1950 1.2153 1.2188 1.2085 1.1950 1.2153 1.2168 1.2085 1.1950 1.2153 1.2188 1.2085 1.1950 1.1716 1.1706 1.1702	1. $3972$ 1. $3817$ 1. $3604$ 1. $3422$ 1. $3288$ 1. $3192$ 1. $3056$ 1. $2971$ 1. $2824$ 1. $2595$ 1. $2346$ 1. $2200$ 1. $2254$ 1. $2200$ 1. $2254$ 1. $2490$ 1. $2750$ 1. $2417$ 1. $2141$ 1. $1860$ 1. $1616$ 1. $1430$ 1. $1219$ 1. $1219$ 1. $1219$ 1. $1253$ 1. $1253$ 1. $1253$ 1. $1253$ 1. $1224$ 1. $1283$ 1. $1523$ 1. $1523$ 1. $1523$ 1. $1523$ 1. $1523$ 1. $1523$ 1. $1568$ 1. $1500$ 1. $1474$ 1. $1481$ 1. $1513$ 1. $1567$ 1. $1646$	1.3972 1.3817 1.3604 1.3422 1.3288 1.3191 1.3115 1.3024 1.2851 1.2541 1.2200 1.2062 1.2276 1.2659 1.2659 1.2822 1.2748 1.2516 1.2181 1.1292 1.1154 1.1078 1.1045	1. $3972$ 1. $3817$ 1. $3604$ 1. $3422$ 1. $3288$ 1. $3190$ 1. $3098$ 1. $2929$ 1. $2557$ 1. $2095$ 1. $1943$ 1. $2796$ 1. $2719$ 1. $2334$ 1. $2796$ 1. $2719$ 1. $2382$ 1. $1941$ 1. $1528$ 1. $1234$ 1. $1062$ 1. $0976$ 1. $0945$ 1. $0945$ 1. $0949$ 1. $1040$ 1. $1143$ 1. $1040$ 1. $1143$ 1. $1040$ 1. $1969$ 1. $2436$ 1. $1955$ 1. $1506$ 1. $1272$ 1. $1158$ 1. $1272$ 1. $158$ 1. $1295$ 1. $1269$ 1. $1272$ 1. $158$ 1. $1272$ 1. $156$ 1. $1272$ 1. $1269$ 1. $12764$ 1. $3551$ 1. $4305$ 1. $480h$	1. $3972$ 1. $3972$ 1. $3817$ 1. $3604$ 1. $3422$ 1. $3288$ 1. $3185$ 1. $3046$ 1. $2071$ 1. $1818$ 1. $2271$ 1. $1296$ 1. $2709$ 1. $2779$ 1. $1296$ 1. $1034$ 1. $0908$ 1. $0908$ 1. $0908$ 1. $1034$ 1. $0908$ 1. $1034$ 1. $0908$ 1. $1034$ 1. $0908$ 1. $1094$ 1. $1271$ 1. $1296$ 1. $1034$ 1. $0908$ 1. $1094$ 1. $1271$ 1. $1294$ 1. $2513$ 1. $1284$ 1. $1094$ 1. $1042$ 1. $1064$ 1. $1130$ 1. $1714$ 1. $2424$ 1. $2503$ 1. $1714$ 1. $2424$ 1. $2503$ 1. $1714$ 1. $2424$ 1. $25083$ 1. $5486$ 1. $5698$ 1. $5805$	
14,000 14,500 15,000	1.2447 1.2430 1.2409	1.1995 1.1987 1.1992	1.1761 1.1814 1.1881	1.1904 1.2104 1.2368	1.3208 1.3805 1.4357	1.5292 1.5540 1.5688	1.5860 1.5887 1.5901	

(b) Dimensionless speed-of-sound parameter  $\ a^2\rho/p$ 





Figure 4.- Thermodynamic charts for 90 percent  $N_{\rm 2}$  and 10 percent  $0_{\rm 2}.$ 



Chart 2

Figure 4.- Thermodynamic charts for 90 percent  $\mathrm{N}_2$  and 10 percent  $\mathrm{O}_2.$  Continued.




Figure 4.- Thermodynamic charts for 90 percent  $\rm N_2$  and 10 percent  $\rm O_2.$  Continued.



Figure 4.- Thermodynamic charts for 90 percent  $\mathrm{N}_2$  and 10 percent  $\mathrm{O}_2.$  Continued.



Chart 5

Figure 4.- Thermodynamic charts for 90 percent  $N_{\rm 2}$  and 10 percent  $O_{\rm 2}.$  Continued.



Figure 4.- Thermodynamic charts for 90 percent  $\mathrm{N}_2$  and 10 percent  $\mathrm{O}_2.$  Continued.





Figure 4.- Thermodynamic charts for 90 percent  ${\rm N_2}$  and 10 percent  ${\rm O_2}.$  Continued.



Figure 4.- Thermodynamic charts for 90 percent  $N_{\rm 2}$  and 10 percent  $O_{\rm 2}.$  Continued.



Figure 4.- Thermodynamic charts for 90 percent  $\mathrm{N}_2$  and 10 percent  $\mathrm{O}_2.$  Continued.



Figure 4.- Thermodynamic charts for 90 percent  ${\tt N}_2$  and 10 percent  ${\tt O}_2.$  Continued.





Figure 4.- Thermodynamic charts for 90 percent  $\mathrm{N}_2$  and 10 percent  $\mathrm{O}_2.$  Continued.



Chart 12

Figure 4.- Thermodynamic charts for 90 percent  ${\tt N}_2$  and 10 percent  ${\tt O}_2.$  Continued.



Chart 13

Figure 4.- Thermodynamic charts for 90 percent  $\mathrm{N}_2$  and 10 percent  $\mathrm{O}_2.$  Continued.





Figure 4.- Thermodynamic charts for 90 percent  $\mathrm{N}_2$  and 10 percent  $\mathrm{O}_2.$  Continued.





Figure 4.- Thermodynamic charts for 90 percent  $N_2$  and 10 percent  $O_2$ . Continued.



Chart 16

Figure 4.- Thermodynamic charts for 90 percent  ${\tt N}_2$  and 10 percent  ${\tt O}_2.$  Continued.





Figure 4.- Thermodynamic charts for 90 percent  $N_2$  and 10 percent  $O_2$ . Continued.



Chart 18

Figure 4.- Thermodynamic charts for 90 percent  $N_2$  and 10 percent  $O_2$ . Continued.



Chart 19

Figure 4.- Thermodynamic charts for 90 percent  $\rm N_2$  and 10 percent  $\rm O_2.$  Continued.



Chart 20

Figure 4.- Thermodynamic charts for 90 percent  $\mathrm{N}_2$  and 10 percent  $\mathrm{O}_2.$  Continued.



Chart 21

Figure 4.- Thermodynamic charts for 90 percent  $N_{\rm 2}$  and 10 percent  $O_{\rm 2}.$  Concluded.

	Pressure, atmospheres, of -							
°K	100	10	1.0	0.1	0.01	0.001	0.0001	
400 600 800 1,000 1,200 1,400 1,600 1,800 2,200 2,400 2,200 2,400 2,200 2,400 2,200 2,400 2,200 2,400 2,200 2,400 2,200 2,400 2,200 2,400 2,200 2,400 2,200 2,400 2,200 2,400 2,200 2,400 2,200 2,400 2,200 2,400 2,200 2,400 2,200 2,400 2,200 2,400 2,200 2,400 2,200 2,500 5,600 5,200 5,600 5,200 5,400 5,200 5,400 5,200 7,500 8,500 7,500 10,500 11,500 12,500 13,500	1. $3961$ 1. $3794$ 1. $3272$ 1. $3110$ 1. $3059$ 1. $2980$ 1. $2939$ 1. $2888$ 1. $2939$ 1. $2824$ 1. $2745$ 1. $2656$ 1. $2568$ 1. $2493$ 1. $2415$ 1. $2415$ 1. $2417$ 1. $2441$ 1. $2478$ 1. $2519$ 1. $2571$ 1. $2553$ 1. $2571$ 1. $2553$ 1. $22571$ 1. $2575$ 1. $2570$ 1. $2774$ 1. $2774$ 1. $2781$ 1. $2784$	1. $3961$ 1. $3794$ 1. $3794$ 1. $3580$ 1. $3402$ 1. $3272$ 1. $3178$ 1. $3110$ 1. $3057$ 1. $3010$ 1. $2956$ 1. $2882$ 1. $2775$ 1. $2636$ 1. $2485$ 1. $2251$ 1. $2262$ 1. $2247$ 1. $2304$ 1. $2252$ 1. $2247$ 1. $2304$ 1. $2252$ 1. $2247$ 1. $2304$ 1. $2252$ 1. $2247$ 1. $2304$ 1. $2252$ 1. $2247$ 1. $22530$ 1. $2235$ 1. $2114$ 1. $2018$ 1. $2176$ 1. $2176$ 1. $2176$ 1. $21956$ 1. $2752$ 1. $2752$ 1. $2794$ 1. $2668$ 1. $2553$ 1. $2532$ 1. $2532$ 1. $2532$ 1. $2532$ 1. $2532$ 1. $2563$ 1. $2552$ 1. $2552$ 1. $2552$	1. $3961$ 1. $3794$ 1. $3272$ 1. $3178$ 1. $2986$ 1. $2986$ 1. $2986$ 1. $2273$ 1. $2091$ 1. $2273$ 1. $2109$ 1. $2044$ 1. $2071$ 1. $2167$ 1. $2317$ 1. $2480$ 1. $2566$ 1. $2518$ 1. $2722$ 1. $2480$ 1. $2565$ 1. $2173$ 1. $1993$ 1. $1893$ 1. $2267$ 1. $2584$ 1. $2553$ 1. $2273$ 1. $2262$ 1. $2434$ 1. $2253$ 1. $22513$ 1. $22191$ 1. $2237$ 1. $2348$ 1. $2513$ 1. $2712$ 1. $2924$	1. 3961 1. 3794 1. 3794 1. 3794 1. 3794 1. 3580 1. 3402 1. 3271 1. 3178 1. 3106 1. 3033 1. 2914 1. 2692 1. 2368 1. 2060 1. 1890 1. 1882 1. 2988 1. 2236 1. 2236 1. 2296 1. 2296 1. 2296 1. 2025 1. 1801 1. 1660 1. 1611 1. 1649 1. 1765 1. 1939 1. 2140 1. 2322 1. 2409 1. 2140 1. 2291 1. 1939 1. 2140 1. 2291 1. 2091 1. 1982 1. 2991 1. 2991 1. 2091 1. 2091 1. 2091 1. 2091 1. 2091 1. 2091 1. 2091 1. 2091 1. 2091 1. 2095 1. 2091 1. 2095 1. 2091 1. 2091 1. 2095 1. 2091 1. 2095 1. 2091 1. 2095 1. 2091 1. 2091 1. 2095 1. 2095 1. 2005 1. 2005 1. 3019	1. $3961$ 1. $3794$ 1. $3794$ 1. $3580$ 1. $3402$ 1. $3271$ 1. $3097$ 1. $2977$ 1. $2977$ 1. $2977$ 1. $2977$ 1. $2977$ 1. $2281$ 1. $1879$ 1. $1714$ 1. $1771$ 1. $2030$ 1. $2479$ 1. $2743$ 1. $2648$ 1. $2338$ 1. $1978$ 1. $1685$ 1. $1518$ 1. $1571$ 1. $12648$ 1. $1571$ 1. $1685$ 1. $1518$ 1. $1571$ 1. $1756$ 1. $2977$ 1. $2246$ 1. $2211$ 1. $2307$ 1. $2246$ 1. $2105$ 1. $2086$ 1. $2459$ 1. $2027$ 1. $2325$ 1. $2027$ 1. $2325$ 1. $2646$ 1. $2925$ 1. $2646$ 1. $2925$	1. $3961$ 1. $3794$ 1. $3794$ 1. $3794$ 1. $3794$ 1. $3794$ 1. $3794$ 1. $3794$ 1. $3271$ 1. $3271$ 1. $3271$ 1. $2817$ 1. $2287$ 1. $2287$ 1. $1269$ 1. $1637$ 1. $2743$ 1. $2743$ 1. $2094$ 1. $1263$ 1. $2094$ 1. $1269$ 1. $1475$ 1. $1713$ 1. $1998$ 1. $2176$ 1. $2127$ 1. $1941$ 1. $1950$ 1. $2229$ 1. $2563$ 1. $2069$ 1. $1710$ 1. $1664$ 1. $22561$ 1. $22561$ 1. $22561$ 1. $2252$ 1. $2251$ 1. $2252$ 1. $2251$ 1. $2252$ 1. $2931$ 1. $3612$ 1. $4851$	1. $3961$ 1. $3794$ 1. $2977$ 1. $2977$ 1. $2436$ 1. $1715$ 1. $1446$ 1. $1597$ 1. $2306$ 1. $2922$ 1. $2874$ 1. $2444$ 1. $1236$ 1. $1591$ 1. $1923$ 1. $2082$ 1. $1924$ 1. $1716$ 1. $1777$ 1. $2154$ 1. $2603$ 1. $2769$ 1. $2602$ 1. $1864$ 1. $1532$ 1. $1626$ 1. $2011$ 1. $2415$ 1. $2602$ 1. $1626$ 1. $2011$ 1. $2415$ 1. $2415$ 1. $2601$ 1. $2415$ 1. $2415$ 1. $2424$ 1. $2595$ 1. $3466$ 1. $4372$ 1. $5029$ 1. $5412$ 1. $5613$ 1. $5714$	
14,500 15,000	1.2800	1.2781	1.3271	1.2896 1.2947	1.3876 1.4371	1.5461 1.5602	1.5790 1.5804	

(a) Ratio of specific heats  $\gamma$ 

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т, °к	Pressure, atmospheres, of -							
	100	10	1.0	0.1	0.01	0.001	0.0001	
400 600 800 1,000 1,200 1,400 1,600 1,800 2,000 2,200 2,400 2,600 2,800 3,000 3,200 3,400 3,600 3,800 4,000 4,200 4,400 4,600 4,200 4,400 4,600 4,200 4,400 4,600 5,000 5,200 5,400 5,600 5,200 5,400 5,600 5,200 5,400 5,000 5,200 5,0000 5,0000 5,0000 5,00000000	1.3961 1.3794 1.3580 1.3402 1.3272 1.3178 1.3110 1.3059 1.2938 1.2980 1.2938 1.2886 1.2818 1.2732 1.2634 1.2530 1.2435 1.2259 1.2259 1.2259 1.2259 1.2259 1.2259 1.2259 1.2259 1.2314 1.2356 1.2392 1.2314 1.2356 1.2392 1.2407 1.2390 1.2342 1.2568 1.2392 1.2407 1.2390 1.2342 1.2568 1.2044 1.1736 1.1679 1.1669 1.1693 1.1744 1.1822 1.1927 1.2055 1.2196 1.2329 1.2495	1.3961 1.3794 1.3580 1.3402 1.3272 1.3178 1.3110 1.3057 1.3010 1.2955 1.2879 1.2618 1.2449 1.2287 1.2160 1.2085 1.2066 1.2104 1.2189 1.2300 1.2395 1.2431 1.2388 1.2282 1.2144 1.2000 1.1254 1.257 1.1627 1.167 1.167 1.167 1.167 1.167 1.1623 1.268 1.2144 1.2000 1.267 1.268 1.2282 1.2282 1.2144 1.2000 1.1867 1.1754 1.1567 1.1623 1.1623 1.268 1.2145 1.2283 1.2284 1.2284 1.2284 1.2284 1.2284 1.2295	1.3961 1.3794 1.3794 1.3580 1.3402 1.3272 1.3178 1.3109 1.3051 1.2986 1.2882 1.2713 1.2477 1.2222 1.2014 1.1896 1.1882 1.1975 1.2162 1.2374 1.2467 1.2466 1.2314 1.2107 1.2466 1.2314 1.2107 1.1898 1.1717 1.1574 1.1574 1.1574 1.1351 1.1351 1.1372 1.2465 1.2374 1.2466 1.2314 1.2107 1.2574 1.2574 1.2574 1.2466 1.2314 1.2107 1.2574 1.1574 1.1574 1.1351 1.1372 1.2229 1.2246 1.2324 1.1372 1.1351 1.1372 1.1495 1.1712 1.2007 1.2229 1.2246 1.2126 1.1980 1.1779 1.1730 1.1730 1.1709 1.1730	1. $3961$ 1. $3794$ 1. $3794$ 1. $3580$ 1. $3402$ 1. $3271$ 1. $3178$ 1. $3178$ 1. $3033$ 1. $2912$ 1. $2683$ 1. $2912$ 1. $2683$ 1. $1993$ 1. $1763$ 1. $1993$ 1. $1763$ 1. $1699$ 1. $1813$ 1. $1699$ 1. $1259$ 1. $2258$ 1. $1964$ 1. $1700$ 1. $2258$ 1. $1964$ 1. $1700$ 1. $1259$ 1. $1259$ 1. $1259$ 1. $1207$ 1. $1184$ 1. $1192$ 1. $1271$ 1. $1285$ 1. $2171$ 1. $12585$ 1. $1512$ 1. $1484$ 1. $1518$ 1. $1570$ 1. $2700$ 1. $2285$ 1. $1570$	1. $3961$ 1. $3794$ 1. $3580$ 1. $3402$ 1. $3271$ 1. $3096$ 1. $2976$ 1. $1928$ 1. $1928$ 1. $1959$ 1. $1097$ 1. $1063$ 1. $1070$ 1. $1063$ 1. $1081$ 1. $1288$ 1. $1292$ 1. $2348$ 1. $1292$ 1. $1384$ 1. $1292$ 1. $1394$ 1. $1329$ 1. $1384$ 1. $1297$ 1. $1384$ 1. $1297$ 1. $1384$ 1. $1292$ 1. $1384$ 1. $1292$ 1. $1384$ 1. $1292$ 1. $1384$ 1. $1294$ 1. $1384$ 1. $1294$ 1. $1294$	1.3961 1.3794 1.3794 1.3580 1.3402 1.3271 1.3174 1.3066 1.2812 1.2265 1.1679 1.1407 1.1512 1.2081 1.2716 1.2825 1.2531 1.2063 1.1613 1.1289 1.1001 1.0965 1.0966 1.0998 1.1001 1.0965 1.0966 1.0998 1.1062 1.175 1.1771 1.1680 1.2073 1.2499 1.1980 1.1272 1.1844 1.1195 1.1272 1.1844 1.1195 1.2729 1.1413 1.1666 1.2094 1.2729 1.3496	1.3961 1.3794 1.3794 1.3580 1.3402 1.3271 1.3165 1.2423 1.1655 1.1286 1.1439 1.2254 1.2909 1.2867 1.2430 1.1844 1.1362 1.073 1.0933 1.0881 1.0918 1.1001 1.101 1.171 1.1499 1.2015 1.2527 1.2720 1.2556 1.1769 1.1294 1.101 1.169 1.1294 1.101 1.169 1.1294 1.100 1.1294 1.100 1.1294 1.101 1.1048 1.1069 1.1294 1.105 1.2566 1.1769 1.1294 1.101 1.1048 1.1069 1.1294 1.101 1.1330 1.1706 1.2400 1.3370 1.5033 1.5038	
13,500 14,000 14,500 15,000	1.2501 1.2490 1.2466 1.2438	1.2036 1.2010 1.1998 1.2000	1.1729 1.1764 1.1814 1.1879	1.1751 1.1895 1.2089 1.2345	1.2613 1.3159 1.3741 1.4281	1.4810 1.5201 1.5445 1.5592	1.5709 1.5762 1.5789 1.5803	

(b) Dimensionless speed-of-sound parameter  $~a^2\rho/p$ 





Figure 5.- Thermodynamic charts for 80 percent  $\rm N_2$  and 20 percent  $\rm O_2.$ 



Chart 2

Figure 5.- Thermodynamic charts for 80 percent  $\mathrm{N}_2$  and 20 percent  $\mathrm{O}_2.$  Continued.



Chart 3

Figure 5.- Thermodynamic charts for 80 percent  $\rm N_2$  and 20 percent  $\rm O_2$ . Continued.



Figure 5.- Thermodynamic charts for 80 percent  $\mathrm{N}_2$  and 20 percent  $\mathrm{O}_2.$  Continued.





Figure 5.- Thermodynamic charts for 80 percent  $\mathrm{N}_2$  and 20 percent  $\mathrm{O}_2.$  Continued.



Chart 6

Figure 5.- Thermodynamic charts for 80 percent  $\mathrm{N}_2$  and 20 percent  $\mathrm{O}_2.$  Continued.





Figure 5.- Thermodynamic charts for 80 percent  $\mathrm{N}_2$  and 20 percent  $\mathrm{O}_2.$  Continued.



Chart 8

Figure 5.- Thermodynamic charts for 80 percent  $\mathrm{N}_2$  and 20 percent  $\mathrm{O}_2.$  Continued.



Figure 5.- Thermodynamic charts for 80 percent  $N_{\rm 2}$  and 20 percent  $O_{\rm 2}.$  Continued.



Chart 10

Figure 5.- Thermodynamic charts for 80 percent  $\mathrm{N}_2$  and 20 percent  $\mathrm{O}_2.$  Continued.





Figure 5.- Thermodynamic charts for 80 percent  $\mathrm{N}_2$  and 20 percent  $\mathrm{O}_2.$  Continued.



Chart 12

Figure 5.- Thermodynamic charts for 80 percent  $\mathrm{N}_2$  and 20 percent  $\mathrm{O}_2.$  Continued.





Figure 5.- Thermodynamic charts for 80 percent  $N_2$  and 20 percent  $O_2$ . Continued.



Chart 14

Figure 5.- Thermodynamic charts for 80 percent  $N_2$  and 20 percent  $O_2$ . Continued.



Chart 15

Figure 5.- Thermodynamic charts for 80 percent  $N_2$  and 20 percent  $O_2$ . Continued.


Chart 16

Figure 5.- Thermodynamic charts for 80 percent  $\mathrm{N}_2$  and 20 percent  $\mathrm{O}_2.$  Continued.





Figure 5.- Thermodynamic charts for 80 percent  $\rm N_2$  and 20 percent  $\rm O_2.$  Continued.



Chart 18

Figure 5.- Thermodynamic charts for 80 percent  $N_{\rm 2}$  and 20 percent  $0_{\rm 2}.$  Continued.



Chart 19

Figure 5.- Thermodynamic charts for 80 percent  $\mathrm{N}_2$  and 20 percent  $\mathrm{O}_2.$  Continued.



Chart 20

Figure 5.- Thermodynamic charts for 80 percent  $N_{\rm 2}$  and 20 percent  $O_{\rm 2}.$  Continued.



Chart 21

Figure 5.- Thermodynamic charts for 80 percent  $\mathrm{N}_2$  and 20 percent  $\mathrm{O}_2.$  Concluded.

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Т,	Pressure, atmospheres, of -								
<u>о</u> К	100	10	1.0	0.1	0.01	0.001	0.0001		
400 600 800 1,000 1,200 1,400 1,600 1,200 1,400 1,600 2,200 2,400 2,400 2,400 2,400 2,600 2,400 2,600 3,200 3,400 3,600 3,600 4,600 4,600 4,600 5,600 5,600 5,600 5,600 5,600 5,600 6,500	100 1.3946 1.3761 1.3546 1.3773 1.3248 1.3159 1.3093 1.3043 1.3000 1.2958 1.2909 1.2846 1.2763 1.2663 1.2554 1.2450 1.2368 1.2554 1.2450 1.2368 1.2554 1.2450 1.2368 1.2571 1.2434 1.2499 1.2557 1.2598 1.2613 1.2583 1.2530 1.2549	10 1.3946 1.3761 1.3546 1.3773 1.3248 1.3159 1.3093 1.3040 1.2989 1.2926 1.2831 1.2695 1.2523 1.2346 1.2202 1.2120 1.2107 1.2151 1.2228 1.2314 1.2393 1.2462 1.2510 1.2516 1.2465 1.2247 1.2138 1.2056 1.206	1.0 1.3946 1.3761 1.3546 1.3546 1.3573 1.3248 1.3159 1.3091 1.3032 1.2956 1.2829 1.2622 1.2356 1.2107 1.1952 1.2177 1.2971 1.2771 1.2771 1.2771 1.2304 1.2124 1.2124 1.2124 1.1861 1.1817 1.1831 1.1896 1.2199	0.1 1. 3946 1. 3761 1. 3546 1. 3546 1. 3573 1. 3248 1. 3158 1. 3087 1. 3006 1. 2858 1. 2577 1. 2198 1. 1882 1. 1748 1. 1781 1. 1888 1. 2019 1. 2245 1. 2515 1. 2600 1. 22441 1. 2171 1. 1919 1. 1744 1. 1662 1. 1670 1. 1755 1. 1896 1. 2210 1. 2278	0.01 1.3946 1.3761 1.3546 1.3573 1.3248 1.3157 1.3074 1.2929 1.2599 1.2095 1.1702 1.1595 1.1682 1.1595 1.1682 1.1595 1.2633 1.2107 1.2563 1.2731 1.2508 1.2131 1.1569 1.1717 1.1569 1.1717 1.1915 1.2089 1.2170	0.001 1.3946 1.3761 1.3546 1.3573 1.3248 1.3153 1.3033 1.2716 1.2094 1.1576 1.1472 1.1584 1.1787 1.2394 1.2657 1.1803 1.1503 1.1503 1.1503 1.1503 1.1598 1.14657 1.1891 1.2030 1.1986 1.1858 1.1845 1.2040 1.2374 1.2650	0.0001 1.3946 1.3761 1.3546 1.3773 1.3248 1.3141 1.2911 1.2253 1.1527 1.1359 1.1479 1.1359 1.1479 1.1813 1.2712 1.3038 1.2659 1.2039 1.2659 1.2039 1.1544 1.1314 1.1332 1.1537 1.1809 1.1929 1.1801 1.1853 1.2315 1.2770 1.2878 1.2660 1.1886		
7,000 7,500 8,000 8,500 9,000 9,500	1.2225 1.2230 1.2354 1.2552 1.2753 1.2885	1.2166 1.2428 1.2637 1.2673 1.2595 1.2554	1.2457 1.2438 1.2349 1.2427 1.2523 1.2477	1.2162 1.2367 1.2517 1.2353 1.2131 1.2010	1.2577 1.2371 1.2012 1.1831 1.1849 1.2033	1.2105 1.1732 1.1677 1.1878 1.2237 1.2564	1.1547 1.1635 1.2015 1.2419 1.2438 1.2154		
10,000 10,500 11,000 11,500 12,000 12,500 13,000 13,500 14,000 14,500 15,000	1.2913 1.2869 1.2819 1.2802 1.2816 1.2835 1.2843 1.2840 1.2836 1.2840 1.2858	1.2588 1.2623 1.2608 1.2559 1.2513 1.2494 1.2513 1.2569 1.2662 1.2784 1.2930	1.2354 1.2254 1.2219 1.2256 1.2359 1.2516 1.2710 1.2918 1.3113 1.3266 1.3359	1.2015 1.2131 1.2335 1.2588 1.2834 1.3009 1.3072 1.3030 1.2947 1.2897 1.2897	1.2326 1.2629 1.2812 1.2801 1.2666 1.2570 1.2633 1.2889 1.3301 1.3791 1.268	1.2626 $1.2439$ $1.2299$ $1.2437$ $1.2888$ $1.3539$ $1.4203$ $1.4736$ $1.5101$ $1.5331$ $1.5470$	1.2114 1.2567 1.3404 1.4281 1.4919 1.5291 1.5485 1.5582 1.5530 1.5655 1.5655 1.5655		

(a) Ratio of specific heats  $\gamma$ 

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т,	Pressure, atmospheres, of -							
°Ŕ	100	10	1.0	0.1	0.01	0.001	0.0001	
400 600 800 1,000 1,200 1,400 1,600 1,800 2,000 2,400 2,600 2,400 2,600 3,000 3,200 3,400 3,600 3,800 4,200 4,400 4,600 4,600 4,600 5,000 5,0000 5,0000 5,0000 5,00000000	100 1. $3946$ 1. $3761$ 1. $3546$ 1. $3773$ 1. $3248$ 1. $3159$ 1. $3093$ 1. $3043$ 1. $3000$ 1. $2958$ 1. $2908$ 1. $2908$ 1. $2755$ 1. $2646$ 1. $2522$ 1. $2396$ 1. $2281$ 1. $2123$ 1. $2086$ 1. $2075$ 1. $2089$ 1. $2123$ 1. $2089$ 1. $2123$ 1. $2089$ 1. $2223$ 1. $2274$ 1. $2309$ 1. $2274$ 1. $2309$ 1. $2274$ 1. $2309$ 1. $2274$ 1. $2309$ 1. $2212$ 1. $2169$ 1. $2274$ 1. $2274$ 1. $2274$ 1. $2309$ 1. $2218$ 1. $2274$ 1. $2274$ 1. $2309$ 1. $2218$ 1. $2274$ 1. $2309$ 1. $2122$ 1. $2169$ 1. $2274$ 1. $2274$ 1. $2309$ 1. $2218$ 1. $2274$ 1. $2297$ 1. $2140$ 1. $1954$ 1. $1754$ 1. $1758$ 1. $1758$ 1. $1258$ 1. $2014$ 1. $22311$ 1. $2447$ 1. $2539$	10 1. $3946$ 1. $3761$ 1. $3546$ 1. $3773$ 1. $3248$ 1. $3159$ 1. $3093$ 1. $3040$ 1. $2989$ 1. $2924$ 1. $2827$ 1. $2683$ 1. $2497$ 1. $2295$ 1. $2110$ 1. $1970$ 1. $1854$ 1. $1872$ 1. $2035$ 1. $2158$ 1. $2232$ 1. $2110$ 1. $2332$ 1. $2158$ 1. $2232$ 1. $2158$ 1. $2232$ 1. $2110$ 1. $1979$ 1. $1859$ 1. $2158$ 1. $2232$ 1. $2110$ 1. $1979$ 1. $1859$ 1. $2158$ 1. $22516$ 1. $2232$ 1. $2110$ 1. $1979$ 1. $1648$ 1. $1554$ 1. $1554$ 1. $1554$ 1. $1554$ 1. $1554$ 1. $1554$ 1. $1554$ 1. $2257$ 1. $2267$ 1. $2254$ 1. $2254$ 1. $2254$ 1. $2254$ 1. $2254$ 1. $2254$ 1. $2267$ 1. $2$	1.0 1.3946 1.3761 1.3546 1.3773 1.3248 1.3159 1.3091 1.3032 1.2955 1.2825 1.2825 1.2825 1.2825 1.2825 1.2825 1.2825 1.2825 1.2825 1.2825 1.2609 1.2322 1.2032 1.1651 1.1651 1.1651 1.1651 1.1651 1.2039 1.2266 1.2403 1.2277 1.2025 1.1831 1.1671 1.1550 1.1466 1.1411 1.1558 1.1558 1.1699 1.2135 1.2349 1.2333 1.2135 1.2349 1.2255 1.1805 1.1751 1.1725	$\begin{array}{c} 0.1\\ 1.3946\\ 1.3761\\ 1.3761\\ 1.3546\\ 1.3773\\ 1.3248\\ 1.3158\\ 1.3087\\ 1.3006\\ 1.2854\\ 1.2159\\ 1.2564\\ 1.2159\\ 1.1786\\ 1.1554\\ 1.2574\\ 1.2578\\ 1.2578\\ 1.2578\\ 1.2578\\ 1.2578\\ 1.2578\\ 1.257\\ 1.1227\\ 1.1227\\ 1.1227\\ 1.1227\\ 1.1227\\ 1.1227\\ 1.1263\\ 1.2669\\ 1.2152\\ 1.2400\\ 1.2240\\ 1.257\\ 1.1268\\ 1.1750\\ 1.268\\ 1.1750\\ 1.1609\\ 1.1531\\ 1.1498\\ 1.1499\\ 1.1525\\ 1.1573\end{array}$	$\begin{array}{c} 0.01\\ \hline 1.3946\\ \hline 1.3761\\ \hline 1.3546\\ \hline 1.3573\\ \hline 1.3248\\ \hline 1.3157\\ \hline 1.3074\\ \hline 1.2927\\ \hline 1.2589\\ \hline 1.2056\\ \hline 1.4591\\ \hline 1.1357\\ \hline 1.1329\\ \hline 1.1357\\ \hline 1.1329\\ \hline 1.1501\\ \hline 1.1938\\ \hline 1.2488\\ \hline 1.2694\\ \hline 1.2475\\ \hline 1.2082\\ \hline 1.1709\\ \hline 1.1438\\ \hline 1.1096\\ \hline 1.1113\\ \hline 1.1257\\ \hline 1.1266\\ \hline 1.1108\\ \hline 1.1096\\ \hline 1.1113\\ \hline 1.155\\ \hline 1.1229\\ \hline 1.1434\\ \hline 1.1257\\ \hline 1.1288\\ \hline 1.1931\\ \hline 1.2482\\ \hline 1.2288\\ \hline 1.1931\\ \hline 1.2482\\ \hline 1.2288\\ \hline 1.1931\\ \hline 1.137\\ \hline 1.1337\\ \hline 1.1337\\ \hline 1.1377\\ \hline 1.1389\\ \hline 1.1477\\ \hline 1.1614\\ \hline 1.1825\end{array}$	$\begin{array}{c} 1.3946\\ 1.3761\\ 1.3546\\ 1.3773\\ 1.3248\\ 1.3153\\ 1.3032\\ 1.2710\\ 1.2064\\ 1.1468\\ 1.1210\\ 1.2064\\ 1.1468\\ 1.1210\\ 1.1230\\ 1.1270\\ 1.2315\\ 1.2841\\ 1.2715\\ 1.2841\\ 1.2715\\ 1.2841\\ 1.2715\\ 1.2239\\ 1.1740\\ 1.175\\ 1.1041\\ 1.0996\\ 1.0994\\ 1.1096\\ 1.0994\\ 1.1098\\ 1.1231\\ 1.1656\\ 1.2992\\ 1.2017\\ 1.1545\\ 1.1299\\ 1.1247\\ 1.2592\\ 1.2017\\ 1.1545\\ 1.1299\\ 1.1196\\ 1.1174\\ 1.1202\\ 1.1276\\ 1.1412\\ 1.1656\\ 1.2068\\ 1.2678\\ 1.3418\\ \end{array}$	$\begin{array}{c} 1.3946\\ 1.3761\\ 1.3546\\ 1.3773\\ 1.3248\\ 1.3140\\ 1.2909\\ 1.2235\\ 1.1440\\ 1.2909\\ 1.2235\\ 1.1440\\ 1.1101\\ 1.1139\\ 1.1666\\ 1.2673\\ 1.3025\\ 1.2645\\ 1.2005\\ 1.2645\\ 1.2005\\ 1.2645\\ 1.2005\\ 1.1461\\ 1.1132\\ 1.0971\\ 1.0908\\ 1.0904\\ 1.0904\\ 1.0904\\ 1.0904\\ 1.0904\\ 1.0904\\ 1.0904\\ 1.0904\\ 1.1039\\ 1.1241\\ 1.1628\\ 1.2202\\ 1.2707\\ 1.2834\\ 1.2617\\ 1.1791\\ 1.1628\\ 1.2202\\ 1.2707\\ 1.2834\\ 1.2617\\ 1.1791\\ 1.1309\\ 1.113\\ 1.1057\\ 1.1076\\ 1.1155\\ 1.1330\\ 1.1695\\ 1.2366\\ 1.3305\\ 1.4230\\ 1.4892\\ 1.5276\end{array}$	
13,500 14,000 14,500	1.2501 1.2580 1.2555 1.2518	1.2014 1.2063 1.2031 1.2015	1.1738 1.1769 1.1815	1.1745 1.1883 1.2068	1.2565 1.3090 1.3651 1.4175	1.4693 1.5075 1.5315 1.5460	1.5577 1.5628 1.5654 1.5668	

(b) Dimensionless speed-of-sound parameter  $a^2\rho/p$ 



Figure 6.- Comparison of enthalpy as a function of temperature for air and nitrogen at 1 atmosphere.

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Enthalpy, MJ/kg