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RESEARCH MEMORANDUM

TABULATED PRESSURE DATA FOR A SERIES OF CONTROLS ON A 60° DELTA WING AT MACH NUMBERS OF 1.61 AND 2.01

By Douglas R. Lord and K. R. Czarnecki

Langley Aeronautical Laboratory
Langley Field, Va.

NATIONAL ADVISORY COMMITTEE
FOR AERONAUTICS

WASHINGTON

March 30, 1956

NACA RM L55L05

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TABULATED PRESSURE DATA FOR A SERIES OF CONTROLS ON A 60° DELTA WING AT MACH NUMBERS OF 1.61 AND 2.01

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SUMMARY

An investigation has been made at Mach numbers of 1.61 and 2.01 and Reynolds numbers from 1.7×10^6 to 7.6×10^6 to determine the pressure distributions over a 60° delta wing having 20 different control configurations. Measurements were made at angles of attack from 0° to 15° for control deflections from -30° to 30°. This report presents the complete tabulated pressure data for the range of test conditions.

INTRODUCTION

As a part of a general program of research on controls, an investigation is underway in the Langley 4- by 4-foot supersonic pressure tunnel to determine the important parameters in the design of controls for use on a 60° delta wing at supersonic speeds. The results have been obtained from two series of tests by means of pressure distributions and direct measurements of hinge moments. The first series was conducted at a Mach number of 1.61 and consisted primarily of tip controls, some fence configurations, and a trailing-edge control with and without a spoiler mounted on the wing just ahead of the control. Much of the control hinge-moment and effectiveness results and some illustrative pressure distributions from this series have been presented in references 1 to 7. The second series of tests consisted of several trailing-edge controls and some fence configurations, all at a Mach number of 1.61 and four of the tip controls at a Mach number of 2.01.

Because of the time involved in the reduction and analysis of the data, and the immediate interest in the basic pressure data, the purpose of this report is to present tabulations of the pressures measured on the surfaces of the 20 configurations for both series of tests without any analysis. The tests were made for a wing angle-of-attack range from 0° to 15° and for a control deflection range from -30° to 30°. All

configurations were tested at a Reynolds number of 4.2×10^6 based on the wing mean aerodynamic chord, and one configuration was also tested at Reynolds numbers of 1.7×10^6 and 7.6×10^6 at a Mach number of 1.61.

SYMBOLS

$b/2$	wing semispan
c_R	wing root chord
C_p	pressure coefficient, $\frac{p - p_l}{q}$
M	stream Mach number
p	stream static pressure
p_l	local surface pressure
q	stream dynamic pressure
R	Reynolds number (based on wing mean aerodynamic chord)
x	distance from wing apex in chordwise direction
y	distance from wing apex in spanwise direction
α	wing angle of attack
δ	control deflection relative to wing (positive when control trailing edge is deflected down)

APPARATUS

Wind Tunnel

This investigation was conducted in the Langley 4- by 4-foot supersonic pressure tunnel, which is a rectangular, closed-throat, single-return type of wind tunnel with provisions for the control of the pressure, temperature, and humidity of the enclosed air. Flexible nozzle walls were adjusted to give the desired test section Mach numbers of 1.61 and 2.01. During the tests, the dewpoint was kept below -20° F so that the effects of water condensation in the supersonic nozzle were negligible.

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Model and Model Mounting

The model used in this investigation consisted of a half-delta wing having 11 interchangeable controls and various associated control adapters (or replacement sections) required to fit the controls to the basic wing component. The control configurations are presented in figure 1 grouped according to whether they were tip controls (fig. 1(a)), trailing-edge controls (fig. 1(b)), or tip controls with modifications such as fences or tabs (fig. 1(c)). The 11 basic configurations are identified as configurations A through G, I, J, J1, and J2. Modifications were made to these basic configurations to obtain the remaining 9 configurations. Configuration H was obtained by installing the control of configuration F in the hinge-line hole for configuration E. Configurations J3 and J4 were made from configuration J by adding paddle balances and a spoiler, respectively. Configuration E1 was obtained by adding a tab on a boom mounted on the inboard edge of the control of configuration E. Configurations E2, E3, and F1, F2, and F3 were made by mounting various fences on the wing at the wing-control juncture of configurations E and F, respectively. The location of the pressure orifices can be determined from tables 1 and 2 and the sketches in figure 2.

The basic wing had a 60° sweptback leading edge, a root chord of 18.14 inches, and a semispan of 10.48 inches. The wing had a rounded NACA 63-series section extending 30-percent root chord back from the leading edge, a constant-thickness center section with a thickness-chord ratio of 3 percent based on the root chord, and a sharp trailing edge. Near the wing tip, the nose section joined directly to the tapered trailing edge without any flat midsection. Configurations J1 and J2 had thickened trailing edges as shown in the sketches of figure 1.

The basic wing and controls were constructed of steel. (For details of construction, see ref. 1.) The paddle balances and tab were also constructed of steel. The spoiler and the fences were constructed of 1/16-inch stock brass.

The semispan wing was mounted horizontally in the tunnel from a turntable in a steel boundary-layer bypass plate which was located vertically in the test section about 10 inches from the sidewall, as shown in figures 3 and 4.

TESTS

The model angle of attack was changed by rotating the turntable in the bypass plate on which the wing was mounted. (See fig. 3.) The angle of attack was measured by a vernier on the outside of the tunnel, inasmuch as the angular deflection of the wing under load was negligible.

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Control deflection was changed by a gear mechanism mounted on the pressure box which rotated the strain-gage balance, the torque tube, and the control as a unit. The control deflections were set approximately with the aid of an electrical control-position indicator mounted on the torque tube close to the wing root and measured under load during testing with a cathetometer mounted outside the tunnel. The pressure distributions were determined from photographs of the multiple-tube manometer boards to which the pressure leads from the model orifices were connected.

Tests were made over an angle-of-attack range from 0° to 15° at increments of either 3° or 6°. The control deflection range was from -30° to 30° at increments of 5° or 10°. Most of the tests were made at a tunnel stagnation pressure of 15 lb/sq in. absolute at $M = 1.61$, and 17.5 lb/sq in. absolute at $M = 2.01$, corresponding to a Reynolds number, based on the mean aerodynamic chord of 12.10 inches, of 4.2×10^6. Configuration E was also tested at $R = 1.7 \times 10^6$ and 7.6×10^6 at $M = 1.61$.

PRECISION OF DATA

The mean Mach numbers in the region occupied by the model are estimated from calibrations to be 1.61 and 2.01 with local variations being smaller than ± 0.02. There is no evidence of any significant flow angularities. The estimated accuracies in setting the wing angle of attack and control deflection are $\pm 0.05^\circ$ and $\pm 0.1^\circ$, respectively. The measured pressure coefficients are believed accurate to ± 0.01. In order to facilitate the publication of the data, a complete final check has not been made and random errors may be present where damage to a model or malfunctioning of an orifice may have occurred during the tests. Such errors can usually be detected by a visual inspection of the plotted pressure distributions.

PRESENTATION OF DATA

The pressure measurements for the complete range of test conditions are presented in tables 3 to 28. The orifice locations are identical on the upper and lower surfaces; therefore, the location of an orifice on the upper surface corresponds to the identically numbered orifice on the lower surface. In many instances the orifice numbered 1 is on the leading edge of the wing and the pressure coefficient has been listed as if it were on the upper surface, there being no corresponding lower surface reading. The same is true for the orifices located at $x/c_R = 0.852$ on

the trailing-edge control configurations, for these orifices are located on the rounded leading-edge part of the control and are shielded from the stream by the wing. In other cases, where orifices were known to be bad, pressures may be listed on one surface only.

Langley Aeronautical Laboratory,
National Advisory Committee for Aeronautics,
Langley Field, Va., November 14, 1955.

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REFERENCES

1. Czarnecki, K. R., and Lord, Douglas R.: Hinge-Moment Characteristics for Several Tip Controls on a 60° Sweptback Delta Wing at Mach Number 1.61. NACA RM L52K28, 1953.

2. Czarnecki, K. R., and Lord, Douglas R.: Preliminary Investigation of the Effect of Fences and Balancing Tabs on the Hinge-Moment Characteristics of a Tip Control on a 60° Delta Wing at Mach Number 1.61. NACA RM L53D14, 1953.

3. Czarnecki, K. R., and Lord, Douglas R.: Load Distributions Associated With Controls at Supersonic Speeds. NACA RM L53D15a, 1953.

4. Lord, Douglas R., and Czarnecki, K. R.: Recent Information on Flap and Tip Controls. NACA RM L53I17a, 1953.

5. Lord, Douglas R., and Czarnecki, K. R.: Aerodynamic Characteristics of a Full-Span Trailing-Edge Control on a 60° Delta Wing With and Without a Spoiler at a Mach Number of 1.61. NACA RM L53L17, 1954.

6. Lord, Douglas R., and Czarnecki, K. R.: Aerodynamic Characteristics of Several Tip Controls on a 60° Delta Wing at a Mach Number of 1.61. NACA RM L54E25, 1954.

7. Czarnecki, K. R., and Lord, Douglas R.: Simplified Procedures for Estimating Flap-Control Loads at Supersonic Speeds. NACA RM L55E12, 1955.

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TABLE 1

SPANWISE LOCATION OF ORIFICE STATIONS

[Chordwise extent of stations shown in fig. 2 and table 2]

Configuration	Values of 2y/b at station -								
	1	2	3	4	5	6	7	8	9
A	0.048	0.210	0.372	0.537	0.592	0.745	0.860	See fig. 2	----------
B	.048	.210	.372	.537	See fig. 2	.602	See fig. 2	0.734	See fig. 2
C	.048	.210	.372	.537	.601	.640	.683	.758	See fig. 2
D	.055	.242	.430	.619	.688	.776	.876	.958	----------
E, E1, E2, E3, F F1, F2, F3, G, H	.048	.210	.372	.537	.597	.733	.869	.967	----------
I	.048	.210	.372	.537	.592	.745	See fig. 2	----------	----------
J, J1, J2, J3, J4	.048	.210	.372	.537	.592	.745	See fig. 2	----------	----------

TABLE 2

CHORDWISE LOCATION OF ORIFICES

[Spanwise location of orifice stations shown in fig. 2 and table 1]

(a) Configuration A

Orifice	Values of x/c_R at station -								
	1	2	3	4	5	6	7	8	9
1	0.048	0.210	0.372	0.535	0.592	0.745	0.872	0.852	
2	.075	.238	.400	.562	.619	.772	.919	.872	
3	.219	.381	.538	.700	.713	.816	.952	.919	
4	.334	.502	.659	.860	.779	.860	.982	.952	
5	.445	.612	.747	.897	.860	.852		.982	
6	.588	.756	.860	.936	.852	.872			
7	.742	.860	.897	.985	.872	.919			
8	.860	.897	.936		.919	.952			
9	.897	.936	.985		.952	.982			
10	.936	.985			.982				
11	.985								
12									
13									

[redacted]

TABLE 2.- Continued

CHORDWISE LOCATION OF ORIFICES

[Spanwise location of orifice stations shown in fig. 2 and table 1]

(b) Configuration B

Orifice	Values of x/c_R at station -								
	1	2	3	4	5	6	7	8	9
1	0.048	0.210	0.372	0.535	0.708	0.875	0.754	0.769	0.819
2	.075	.238	.400	.562	.761	.906	.799	.824	.871
3	.219	.381	.538	.700	.810	.945	.835	.879	.926
4	.334	.502	.659	.846		.986		.934	.988
5	.445	.612	.747	.901				.992	
6	.588	.756	.846	.950					
7	.742	.846	.901	.986					
8	.846	.901	.950						
9	.901	.950	.986						
10	.950	.986							
11	.986								
12									
13									

[redacted]

TABLE 2.- Continued

CHORDWISE LOCATION OF ORIFICES

[Spanwise location of orifice stations shown in fig. 2 and table 1]

(c) Configuration C

Orifice	Values of x/c_R at station -								
	1	2	3	4	5	6	7	8	9
1	0.048	0.210	0.372	0.535	0.876	0.674	0.683	0.758	0.871
2	.075	.238	.400	.562	.909	.769	.711	.785	.928
3	.219	.381	.538	.700	.947	.857	.780	.879	.986
4	.334	.502	.659	.846	.991		.876	.929	
5	.445	.612	.747	.901				.992	
6	.588	.756	.846	.950					
7	.742	.846	.901	.986					
8	.846	.901	.950						
9	.901	.950	.986						
10	.950	.986							
11	.986								
12									
13									

[redacted]

TABLE 2.- Continued

CHORDWISE LOCATION OF ORIFICES

[Spanwise location of orifice stations shown in fig. 2 and table 1]

(d) Configuration D

Orifice	Values of x/c_R at station -								
	1	2	3	4	5	6	7	8	9
1	0.048	0.210	0.372	0.535	0.595	0.672	0.758	0.862	
2	.075	.238	.400	.562	.623	.699	.785		
3	.219	.381	.538	.700	.675	.752	.813		
4	.334	.502	.659	.846	.744	.826	.851		
5	.445	.612	.747	.901	.821	.876	.901		
6	.588	.756	.846	.950	.899	.937			
7	.742	.846	.901	.984	.970				
8	.846	.901	.950						
9	.901	.950	.984						
10	.950	.984							
11	.984								
12									
13									

[redacted]

TABLE 2.- Continued

CHORDWISE LOCATION OF ORIFICES

[Spanwise location of orifice stations shown in fig. 2 and table 1]

(e) Configurations E, E1, E2, E3, F, F1, F2, F3, G, H

Orifice	Values of x/c_R at station -								
	1	2	3	4	5	6	7	8	9
1	0.048	0.210	0.372	0.535	0.597	0.730	0.864	0.987	
2	.075	.238	.400	.562	.625	.758	.892		
3	.219	.381	.538	.700	.674	.808	.941		
4	.334	.502	.659	.846	.746	.879	.986		
5	.445	.612	.747	.901	.840	.973			
6	.588	.756	.846	.950	.939				
7	.742	.846	.901	.984	.988				
8	.846	.901	.950						
9	.901	.950	.984						
10	.950	.984							
11	.984								
12									
13									

[redacted]

TABLE 2.- Continued

CHORDWISE LOCATION OF ORIFICES

[Spanwise location of orifice stations shown in fig. 2 and table 1]

(f) Configuration I

Orifice	Values of x/c_R at station -								
	1	2	3	4	5	6	7	8	9
1	0.048	0.210	0.372	0.535	0.597	0.753	0.890		
2	.075	.238	.400	.562	.624	.778	.985		
3	.219	.381	.538	.700	.719	.853			
4	.334	.502	.659	.860	.839	.945			
5	.445	.612	.747	.852	.919	.995			
6	.588	.756	.860	.896	.972				
7	.742	.860	.852	.935					
8	.860	.852	.896	.984					
9	.852	.896	.935						
10	.896	.935	.984						
11	.935	.984							
12	.984								
13									

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TABLE 2.- Concluded

CHORDWISE LOCATION OF ORIFICES

[Spanwise location of orifice stations shown in fig. 2 and table 1]

(g) Configurations J, J1, J2, J3, J4

Orifice	Values of x/c_R at station -								
	1	2	3	4	5	6	7	8	9
1	0.048	0.210	0.372	0.535	0.592	0.745	0.852		
2	.075	.238	.400	.562	.619	.772	.872		
3	.219	.381	.538	.700	.713	.816	.910		
4	.334	.502	.659	.860	.779	.860	.948		
5	.445	.612	.747	.852	.860	.872	.986		
6	.588	.756	.860	.872		.905			
7	.742	.860		.905		.949			
8	.860	.852		.949		.982			
9	.872	.872		.982					
10	.905	.905		1.000					
11	.949	.949							
12	.982	.982							
13		1.000							

[redacted]

Table 3

Pressure Coefficients on Delta Wing with Control

Configuration A M = 1.61 R = 4.2 x 10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 00°									δ = 00°									
1	.364	.357	.291	.263	.305	.337	.031	-.041								.041			1
2	.051	.033	.022	.022	.011	.008	.024	.051		.071		.041		.007	-.003	-.002	.032		2
3	.011	.012		-.002	-.011	-.010	-.223	.018		.030	.016	.000		.003	-.003	-.210	.027		3
4	.025	-.007	-.020	-.029	-.027	.055	-.220	-.139		.036		-.016	-.005	-.040	.016	-.209	-.174		4
5	.003	.001	-.005	-.146	.007	-.039		-.297		-.004	.002	.235	-.161	-.003			-.263		5
6	.006	-.011	.003	-.145	-.029	.005				.014	-.012	.010	-.153		-.018				6
7	.011	.013	-.162	-.170	-.137	-.226				.016	.003	-.161	-.166	.012	-.204				7
8	-.012	-.162	-.158		-.183	-.209				.045	-.149	-.158		-.176	-.201				8
9	-.153	-.151	-.148		-.160	-.193				-.157	-.149	-.156		-.174	-.190				9
10	-.099	-.158			-.156					-.082	-.142			-.161					10
11										-.155									11
	α = 00°									δ = 10°									
1	.368	.362	.292	.266	.317	.348	-.137	.048								.261			1
2	.052	.033	.027	.025	.020	.025	-.162	-.180		.084		.057		.018	.010	.252	.114		2
3	.020	.015		-.001	-.002	.008	-.342	-.188		.043	.033	.016		.013	.003	-.055	.282		3
4	.030	-.005	-.018	-.025	-.008	.070	-.337	-.382		.053		-.002	.014	-.031	.036	-.047	-.017		4
5	.007	.003	-.003	-.152	.022	.048		-.405		.012	.017	.318	-.114	.012			-.054		5
6	.008	-.007	.000	-.170	-.001	-.208				.032	.006	.031	-.099		.179				6
7	.013	.018	-.163	-.195	-.283	-.357				.039	.021	-.152	-.144	.082	.030				7
8	-.009	-.160	-.154		-.271	-.365				.059	-.143	-.146		-.028	.033				8
9	-.150	-.142	-.144		-.267	-.349				-.140	-.138	-.142		-.029	.027				9
10	-.100	-.154			-.266					-.059	-.127			-.027					10
11										-.136									11
	α = 00°									δ = 20°									
1	.370	.367	.290	.268	.308	.341	-.286	.152								.568			1
2	.052	.034	.026	.022	.019	.018	-.299	-.326		.080		.042		.010	.001	.487	.463		2
3	.018	.014		-.002	-.002	.002	-.407	-.412		.035	.019	.010		.005	-.001	.197	.538		3
4	.028	-.004	-.014	-.021	-.014	.065	-.409	-.458		.042		-.010	.007	-.037	.068	.279	.107		4
5	.011	.001	-.006	-.172	.014	.196		-.444		.000	.008	.303	-.080	.016			.270		5
6	.003	-.011	-.002	-.202	.016	-.331				.020	-.005	.024	-.077		.483				6
7	.017	.020	-.162	-.237	-.385	-.434				.027	.007	-.159	-.190	.065	.373				7
8	-.009	-.160	-.153		-.376	-.402				.046	-.155	-.151		.288	.331				8
9	-.150	-.145	-.146		-.343	-.339				-.151	-.146	-.134		.219	.282				9
10	-.095	-.157			-.388					-.073	-.138			.184					10
11										-.156									11
	α = 00°									δ = 30°									
1	.372	.366	.290	.268	.308	.337	-.429	.323								.954			1
2	.054	.038	.029	.030	.019	.023	-.428	-.405		.070		.041		.007	-.002	.794	.601		2
3	.023	.020		.004	-.001	.001	-.457	-.464		.035	.023	.006		.008	.016	.622	.829		3
4	.034	-.007	-.011	-.025	-.014	.002	-.461	-.487		.048		-.012	.177	-.035	.429	.590	.560		4
5	.016	.004	-.001	-.171	.020	.341		-.471		.005	.008	.310	.061	.302			.618		5
6	.004	-.006	.001	-.198	.018	-.417				.022	-.005	.022	-.081		.509				6
7	.019	.029	-.157	-.240	-.445	-.394				.029	.013	-.166	-.220	.005	.763				7
8	-.005	-.151	-.151		-.430	-.393				.050	-.149	-.137		.620	.646				8
9	-.146	-.137	-.139		-.409	-.384				-.151	-.145	-.003		.501	.590				9
10	-.101	-.149			-.425					-.071	-.138			.434					10
11										-.146									11
	α = 06°									δ = 00°									
1	.316	.110	.139	-.013	.086	.184	-.376	-.305								.300			1
2	-.089	-.268	-.344	-.376	-.366	-.393	-.344	-.370		.207		.244		.222	.229	.179	.258		2
3	-.072	-.082		-.172	-.293	-.354	-.440	-.302		.144	.163	.158		.167	.192	-.091	.223		3
4	-.054	-.100	-.127	-.154	-.159	-.297	-.423	-.454		.158		.122	.137	.103	.181	-.086	-.049		4
5	-.088	-.104	-.116	-.229	-.119	-.221		-.438		.114	.126	.078	-.067	.157			-.086		5
6	-.078	-.094	-.101	-.219	-.049	-.319				.131	.099	.133	-.071		.169				6
7	-.066	-.055	-.228	-.235	-.214	-.400				.119	.116	-.078	-.080	.213	-.088				7
8	-.082	-.219	-.231		-.240	-.371				.140	-.074	-.063		-.098	-.071				8
9	-.216	-.212	-.220		-.227	-.341				-.071	-.068	-.072		-.073	-.065				9
10	-.174	-.221			-.241					.005	-.065			-.077					10
11										-.095									11

[redacted]

Table 3 Continued

Pressure Coefficients on Delta Wing with Control

Configuration A M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 06°									δ = 10°									
1	.327	.111	.148	-.004	.095	.184	-.440	-.275		.222		.253		.223	.239	.598			1
2	-.091	-.271	-.338	-.372	-.372	-.393	-.421	-.412		.149	.162	.156		.161	.185	.405	.732		2
3	-.074	-.083		-.164	-.291	-.348	-.446	-.440		.161		.125	.146	.105	.186	.148	.457		3
4	-.056	-.098	-.124	-.149	-.153	-.299	-.446	-.457		.112	.133	.078	-.020	.158		.178	.065		4
5	-.088	-.096	-.112	-.239	-.105	-.081		-.456		.134	.105	.133	.001		.495		.191		5
6	-.082	-.093	-.097	-.243	-.038	-.395				.117	.119	-.080	-.055	.381	.218				6
7	-.067	-.054	-.235	-.261	-.338	-.454				.145	-.077	-.065		.095	.195				7
8	-.078	-.213	-.222		-.349	-.444				-.063	-.067	-.067		.120	.165				8
9	-.218	-.208	-.214		-.313	-.357				.012	-.061			.097					9
10	-.180	-.215			-.292					-.094									10
11																			11
	α = 06°									δ = 20°									
1	.326	.101	.138	-.006	.100	.179	-.422	.078		.212		.244		.217	.236	.911			1
2	-.088	-.277	-.343	-.382	-.368	-.395	-.420	-.432		.151	.165	.157		.163	.186	.637	1.543		2
3	-.073	-.085		-.165	-.292	-.349	-.429	-.438		.158		.125	.144	.107	.265	.474	.671		3
4	-.058	-.102	-.121	-.152	-.159	-.279	-.431	-.453		.106	.131	.073	.052	.165		.457	.436		4
5	-.092	-.098	-.116	-.242	-.113	-.372		-.421		.131	.100	.132	.065		.900		.504		5
6	-.081	-.094	-.094	-.264	-.014	-.457				.113	.116	-.081	-.108	.421	.564				6
7	-.067	-.057	-.233	-.296	-.417	-.462				.146	-.079	-.065		.427	.489				7
8	-.086	-.213	-.229		-.414	-.436				-.074	-.067	-.016		.355	.442				8
9	-.225	-.207	-.213		-.336	-.405				.012	-.065			.307					9
10	-.181	-.215			-.400					-.099									10
11																			11
	α = 06°									δ = 30°									
1	.325	.112	.140	-.005	.088	.180	-.433	-.010		.206		.244		.220	.234	1.007			1
2	-.090	-.277	-.342	-.374	-.366	-.398	-.436	-.442		.141	.157	.158		.150	.182	.968	1.261		2
3	-.069	-.090		-.167	-.293	-.349	-.439	-.446		.158		.120	.355	.105	.726	.826	.976		3
4	-.058	-.103	-.121	-.154	-.157	-.258	-.440	-.456		.101	.124	.074	.035	.472		.743	.809		4
5	-.087	-.098	-.115	-.244	-.116	-.472		-.442		.128	.101	.126	.048		.867		.746		5
6	-.080	-.089	-.100	-.274	-.071	-.478				.108	.108	-.070	-.123	.027	.944				6
7	-.064	-.059	-.232	-.287	-.471	-.456				.141	-.074	.005		.808	.829				7
8	-.080	-.216	-.224		-.446	-.461				-.073	-.075	.097		.667	.750				8
9	-.222	-.210	-.211		-.439	-.440				.005	-.058			.590					9
10	-.181	-.217			-.448					-.103									10
11																			11
	α = 12°									δ = 00°									
1	.196	-.103	-.032	-.194	-.174	-.193	-.446	-.313		.342		.395		.362	.375	.361			1
2	-.295	-.433	-.468	-.481	-.486	-.490	-.432	-.429		.264	.279	.285		.303	.330	.266	.369		2
3	-.141	-.194		-.441	-.453	-.478	-.434	-.445		.283		.248	.276	.238	.338	.012	.321		3
4	-.122	-.192	-.238	-.325	-.438	-.455	-.434	-.436		.235	.248	.192	.022	.304		.037	-.016		4
5	-.169	-.200	-.194	-.354	-.299	-.181		-.444		.235	.216	.247	.014		.281		.071		5
6	-.146	-.189	-.170	-.366	-.101	-.428				.195	.229	.003	-.001	.360	.009				6
7	-.138	-.127	-.286	-.332	-.352	-.465				.230	.009	.014		-.019	.024				7
8	-.135	-.281	-.284		-.373	-.429				.018	.007	.011		.014	.024				8
9	-.285	-.257	-.266		-.344	-.405				.029	.016			.013					9
10	-.229	-.271			-.314					.027									10
11																			11
	α = 12°									δ = 10°									
1	.196	-.104	-.025	-.191	-.172	-.198	-.417	-.150		.345		.396		.358	.368	.654			1
2	-.294	-.435	-.475	-.492	-.491	-.500	-.419	-.441		.269	.280	.286		.300	.331	.486	.910		2
3	-.140	-.185		-.441	-.453	-.486	-.428	-.435		.280		.248	.276	.240	.333	.334	.530		3
4	-.120	-.193	-.238	-.328	-.433	-.445	-.422	-.450		.239	.244	.184	.075	.303		.313	.263		4
5	-.170	-.194	-.190	-.350	-.296	.070		-.422		.237	.206	.252	.120		.684		.373		5
6	-.147	-.181	-.172	-.398	-.070	-.492				.195	.223	.007	.044	.637	.355				6
7	-.137	-.127	-.269	-.368	-.418	-.448				.231	.009	.017		.229	.314				7
8	-.137	-.273	-.280		-.394	-.443				.017	.012	.023		.236	.282				8
9	-.274	-.253	-.266		-.398	-.433				.030	.015			.213					9
10	-.229	-.271			-.367					.021									10
11																			11

[redacted]

Table 3 Continued

Pressure Coefficients on Delta Wing with Control

Configuration A M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
								α = 12°				δ = 20°								
1	.199	-.102	-.034	-.191	-.167	-.193	-.412	.261									.807			1
2	-.297	-.432	-.477	-.497	-.486	-.476	-.429	-.432			.349		.400		.364	.374	.778	1.350		2
3	-.140	-.194		-.445	-.444	-.474	-.438	-.441			.273	.289	.288		.306	.328	.658	.788		3
4	-.121	-.193	-.236	-.325	-.429	-.421	-.434	-.450			.291		.253	.288	.239	.652	.609	.626		4
5	-.168	-.199	-.191	-.351	-.288	.598		-.417			.242	.247	.198	.205	.336			.635		5
6	-.148	-.185	-.170	-.404	.014	-.474					.240	.217	.248	.208		.965				6
7	-.140	-.122	-.277	-.344	-.457	-.446					.199	.226	.005	-.014	.668	.716				7
8	-.135	-.277	-.280		-.456	-.446					.237	.017	.016		.557	.626				8
9	-.282	-.258	-.258		-.440	-.445					.016	.013	.132		.492	.591				9
10	-.235	-.271			-.446						.037	.020			.435					10
11											.021									11
								α = 12°				δ = 30°								
1	.194	-.100	-.029	-.187	-.171	-.188	-.439	.052									.854			1
2	-.293	-.431	-.474	-.493	-.482	-.471	-.438	-.442			.348		.394		.362	.368	1.080	1.196		2
3	-.135	-.185		-.436	-.450	-.473	-.446	-.453			.273	.277	.288		.304	.505	.959	1.056		3
4	-.120	-.189	-.225	-.319	-.435	-.409	-.446	-.466			.291		.254	.518	.240	.855	.834	.918		4
5	-.161	-.193	-.185	-.357	-.286	.585		-.440			.240	.250	.198	.247	.670			.807		5
6	-.145	-.181	-.165	-.399	-.068	-.483					.240	.216	.247	.185		.890				6
7	-.135	-.122	-.272	-.366	-.473	-.459					.191	.225	.022	-.061	.095	1.092				7
8	-.130	-.272	-.270		-.448	-.461					.239	.013	.168		.922	.949				8
9	-.277	-.255	-.234		-.468	-.453					.013	.006	.229		.794	.837				9
10	-.224	-.267			-.459						.043	.049			.698					10
11											.017									11
								α = -06°				δ = 00°								
1	.306	.397	.160	.141	.190	.125	.305	-.408									-.319			1
2	.188	.196	.218	.231	.220	.235	.182	.218			-.063		-.297		-.350	-.379	-.340	-.333		2
3	.120	.133		.132	.142	.180	-.112	.226			-.045	-.075	-.101		-.280	-.336	-.403	-.339		3
4	.128	.096	.110	.097	.117	.220	-.104	-.014			-.040		-.106	-.120	-.147	-.292	-.384	-.399		4
5	.115	.109	.101	-.052	.149	-.229		-.126			-.080	-.083	.222	-.227	-.120			-.390		5
6	.102	.092	.099	-.054	-.033	.147					-.058	-.083	-.068	-.225		-.288				6
7	.104	.110	-.080	-.094	-.038	-.102					-.049	-.069	-.224	-.228	-.098	-.351				7
8	.089	-.083	-.072		-.099	-.100					-.018	-.210	-.223		-.242	-.335				8
9	-.069	-.075	-.072		-.072	-.092					-.211	-.204	-.214		-.246	-.314				9
10	-.013	-.075			-.069						-.126	-.197			-.236					10
11											-.184									11
								α = -06°				δ = 10°								
1	.308	.397	.160	.151	.188	.119	.057	-.410									-.210			1
2	.190	.199	.228	.235	.224	.237	-.010	-.057			-.067		-.297		-.347	-.382	-.183	-.248		2
3	.121	.137		.140	.143	.180	-.251	.013			-.051	-.089	-.109		-.276	-.334	.333	-.174		3
4	.129	.100	.117	.101	.111	.222	-.248	-.146			-.045		-.110	-.119	-.144	-.288	-.324	-.290		4
5	.114	.110	.109	-.090	.152	-.231		-.295			-.084	-.082	.222	-.198	-.116			-.328		5
6	.105	.096	.101	-.114	-.003	-.113					-.066	-.092	-.073	-.199		-.224				6
7	.102	.114	-.077	-.162	-.228	-.287					-.052	-.075	-.223	-.208	-.016	-.226				7
8	.092	-.086	-.069		-.233	-.288					-.020	-.205	-.223		-.122	-.164				8
9	-.065	-.069	-.062		-.220	-.277					-.214	-.208	-.214		-.138	-.142				9
10	-.020	-.067			-.233						-.131	-.198			-.119					10
11											-.182									11
								α = -06°				δ = 20°								
1	.308	.395	.165	.148	.186	.124	-.142	-.314									-.010			1
2	.192	.196	.223	.237	.226	.244	-.183	-.255			-.061		-.296		-.348	-.390	.043	-.155		2
3	.126	.137		.137	.143	.183	-.365	-.187			-.041	-.080	-.103		-.277	-.339	-.184	.088		3
4	.127	.100	.115	.103	.117	.222	-.358	-.332			-.047		-.105	-.116	-.148	-.190	-.157	-.073		4
5	.117	.112	.107	-.090	.156	-.082		-.408			-.076	-.076	.230	-.163	-.113			-.099		5
6	.104	.096	.101	-.129	.055	-.293					-.059	-.086	-.071	-.206		.050				6
7	.106	.113	-.074	-.181	-.352	-.405					-.050	-.070	-.220	-.265	.027	.037				7
8	.089	-.084	-.070		-.356	-.411					-.018	-.198	-.220		.116	.112				8
9	-.057	-.069	-.065		-.338	-.348					-.214	-.205	-.205		.069	.112				9
10	-.016	-.068			-.365						-.129	-.197			.068					10
11											-.181									11

[redacted]

Table 3 Concluded

Pressure Coefficients on Delta Wing with Control

Configuration A M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	$\alpha = -06^\circ$									$\delta = 30^\circ$									
1	.314	.398	.164	.158	.191	.114	-.288	.612		-.068		-.298		-.346	-.137	.311			1
2	.193	.205	.224	.243	.227	.240	-.303	-.377		-.045	-.081	-.106		-.278	-.135	.416	.015		2
3	.129	.141		.136	.142	.184	-.423	-.402		-.040		-.101	.032	-.114	-.072	.104	.459		3
4	.128	.107	.113	.101	.119	.227	-.396	-.456		-.080	-.073	.249	-.163	.118		.211	.111		4
5	.121	.114	.111	-.082	.151	-.017		-.454		-.061	-.087	-.068	-.232		-.035		.216		5
6	.108	.097	.109	-.131	.092	-.403				-.049	-.072	-.216	-.299	.068	.211				6
7	.109	.117	-.074	-.179	-.429	-.394				-.017	-.204	-.177		.235	.288				7
8	.096	-.078	-.066		-.440	-.388				-.214	-.205	-.126		.248	.323				8
9	-.061	-.069	-.060		-.420	-.370				-.135	-.197			.266					9
10	-.011	-.062			-.410					-.182									10
11																			11
	$\alpha = -12^\circ$									$\delta = 00^\circ$									
1	.166	.275	.018	-.099	-.046	-.067	.407	-.438		-.269		-.435		-.469	-.495	-.416			1
2	.342	.347	.376	.382	.356	.359	.284	.354		-.116	-.151	-.348		-.429	-.462	-.432	-.431		2
3	.255	.260		.275	.282	.310	-.027	.324		-.107		-.189	-.288	-.422	-.444	-.420	-.413		3
4	.257	.237	.249	.223	.252	.353	.018	.058		-.146	-.163	-.118	-.348	-.273		-.413	-.399		4
5	.241	.237	.234	.034	.287	-.209		.014		-.131	-.172	-.147	-.356		-.411		-.409		5
6	.234	.218	.224	.032	-.099	.266				-.116	-.153	-.266	-.317	-.314	-.430				6
7	.206	.226	.016	-.020	.048	-.001				-.067	-.258	-.271		-.359	-.411				7
8	.213	.006	.022		-.008	-.011				-.259	-.243	-.263		-.359	-.385				8
9	.029	.027	.034		.010	.008				-.165	-.235			-.325					9
10	.077	.027			.014					-.197									10
11																			11
	$\alpha = -12^\circ$									$\delta = 10^\circ$									
1	.160	.266	.016	-.106	-.039	-.057	.128	-.473		-.268		-.436		-.474	-.492	-.404			1
2	.337	.344	.368	.380	.361	.364	.073	.020		-.111	-.170	-.345		-.421	-.475	-.390	-.426		2
3	.247	.245		.281	.289	.313	-.172	.099		-.106		-.192	-.282	-.425	-.451	-.435	-.369		3
4	.250	.231	.247	.224	.259	.355	-.173	-.073		-.145	-.153	-.153	-.323	-.259		-.417	-.406		4
5	.229	.227	.234	.018	.288	-.302		-.187		-.125	-.169	-.139	-.301		-.401		-.409		5
6	.226	.211	.221	-.032	-.073	-.029				-.112	-.155	-.262	-.330	-.254	-.428				6
7	.202	.219	.016	-.092	-.162	-.216				-.065	-.254	-.267		-.312	-.423				7
8	.208	.000	.024		-.180	-.228				-.258	-.240	-.252		-.313	-.395				8
9	.022	.017	.032		-.186	-.201				-.164	-.231			-.293					9
10	.075	.022			-.207					-.194									10
11																			11
	$\alpha = -12^\circ$									$\delta = 20^\circ$									
1	.161	.270	.010	-.101	-.052	-.067	-.082	-.393		-.276		-.451		-.487	-.489	-.326			1
2	.334	.349	.370	.380	.360	.355	-.120	-.193		-.126	-.178	-.349		-.432	-.474	-.233	-.401		2
3	.252	.249		.277	.279	.307	-.290	-.090		-.113		-.197	-.289	-.428	-.417	-.371	-.210		3
4	.253	.228	.247	.222	.254	.352	-.300	-.210		-.155	-.159	-.182	-.288	-.231		-.356	-.280		4
5	.231	.232	.233	.010	.284	-.401		-.339		-.130	-.176	-.148	-.318		-.382		-.310		5
6	.223	.216	.225	-.054	-.063	-.235				-.117	-.159	-.267	-.382	-.231	-.346				6
7	.204	.223	.015	-.108	-.312	-.356				-.069	-.263	-.273		-.249	-.329				7
8	.214	.005	.025		-.322	-.357				-.262	-.246	-.259		-.226	-.307				8
9	.028	.022	.035		-.315	-.348				-.176	-.235			-.166					9
10	.074	.026			-.329					-.205									10
11																			11
	$\alpha = -12^\circ$									$\delta = 30^\circ$									
1	.158	.263	.012	-.107	-.046	-.060	-.243	.590		-.262		-.445		-.456	-.377	-.177			1
2	.333	.340	.376	.376	.371	.370	-.255	-.336		-.114	-.164	-.348		-.434	-.366	.031	-.328		2
3	.246	.241		.278	.295	.314	-.388	-.244		-.099		-.190	-.270	-.368	-.348	-.182	.084		3
4	.249	.227	.245	.225	.263	.354	-.384	-.398		-.148	-.157	-.184	-.280	-.294		-.155	-.050		4
5	.226	.223	.231	.018	.288	-.356		-.418		-.121	-.165	-.138	-.312		-.331		-.057		5
6	.218	.212	.222	-.045	-.018	-.355				-.106	-.142	-.257	-.382	-.162	-.176				6
7	.201	.218	.012	-.100	-.411	-.442				-.065	-.251	-.247		-.208	-.113				7
8	.202	.000	.022		-.403	-.445				-.257	-.233	-.225		-.144	-.104				8
9	.017	.016	.027		-.388	-.438				-.165	-.230			-.084					9
10	.070	.022			-.420					-.191									10
11																			11

Table 4

Pressure Coefficients on Delta Wing with Control

Configuration B M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
								α = 00°		δ = 00°									
1	.396	.380	.300	.274	.012	-.166	.019	-.004	-.01					.026	-.170	.161	.002	.008	1
2	.069	.045	.032	.028	.006	-.179	-.009	.004	.014	.076		.044		-.008	-.177	.006	.019	.034	2
3	.032	.026		.013	-.012	-.162	-.018	-.023	.004	.042	.022	.011		-.012	-.147	-.011	-.017	.026	3
4	.039	.007	-.005	-.008		-.153		-.202	-.261	.048		-.008	-.010		-.149		-.204	-.278	4
5	.023	.010	.009	-.159				-.177		.004	.012	-.011	-.145				-.202		5
6	.015	.012	.017	-.147						.023	.025	.013	-.135						6
7	.048	.034	-.146	-.145						.039	.023	-.143	-.147						7
8	.005	-.135	-.143							.008	-.132	-.145							8
9	-.140	-.144	-.128							-.140	-.141	-.138							9
10	-.090	-.142								-.099	-.146								10
11	-.135									-.143									11
								α = 00°		δ = 10°									
1	.390	.372	.294	.267	.013	-.386	-.080	-.124	-.303					.023	.024	.161	.125	.240	1
2	.060	.039	.026	.024	.147	-.403	-.348	-.126	-.315	.075		.043		.032	.027	.175	.235	.296	2
3	.028	.019		.003	.180	-.394	-.327	-.157	-.333	.038	.032	.008		-.015	-.013	.188	.186	.308	3
4	.032	.002	-.012	.056		-.327		-.310	-.387	.041		-.015	.064		-.036		-.055	-.011	4
5	.016	.003	.000	-.238				-.291		-.002	.005	-.011	-.066				-.019		5
6	.010	.010	.011	-.313						.018	.023	.008	-.082						6
7	.039	.031	-.095	-.296						.035	.020	-.146	-.145						7
8	.005	-.140	-.119							.002	-.134	-.109							8
9	-.145	-.150	-.138							-.146	-.140	-.070							9
10	-.093	-.132								-.103	-.153								10
11	-.140									-.147									11
								α = 00°		δ = 20°									
1	.395	.380	.301	.273	.014	-.457	-.153	-.432	-.437					.020	.219	.160	.284	.517	1
2	.068	.047	.034	.030	.069	-.463	-.433	-.224	-.427	.075		.041		.016	.177	.183	.533	.582	2
3	.038	.026		.008	.447	-.445	-.424	-.231	-.427	.038	.037	.008		.072	.157	.313	.425	.511	3
4	.035	.007	-.007	.128		-.395		-.370	-.435	.041		-.016	.217		.089		.143	.252	4
5	.025	.011	.007	-.270				-.365		.001	.004	-.010	-.026				.203		5
6	.017	.015	.018	-.351						.019	.022	.006	-.154						6
7	.051	.042	-.051	-.357						.034	.018	-.137	-.220						7
8	.011	-.134	-.100							.003	-.136	-.003							8
9	-.139	-.136	-.129							-.144	-.145	-.019							9
10	-.088	-.093								-.101	-.147								10
11	-.130									-.144									11
								α = 00°		δ = 30°									
1	.397	.383	.304	.272	.016	-.481	-.323	-.482	-.483					.016	.479	.159	.835	.777	1
2	.069	.049	.035	.033	.073	-.481	-.457	-.430	-.455	.069		.039		.039	.448	.500	.720	.832	2
3	.038	.026		.011	.601	-.464	-.465	-.368	-.434	.031	.039	.005		.157	.437	.601	.620	.625	3
4	.041	.009	-.008	.232		-.416		-.439	-.396	.036		-.018	.273		.391		.511	.552	4
5	.020	.011	.009	-.298				-.372		-.004	.003	-.016	-.011				.484		5
6	.015	.016	.084	-.383						.014	.018	.003	-.216						6
7	.049	.042	-.021	-.387						.030	.013	.011	-.279						7
8	.015	-.133	-.091							-.003	-.141	.048							8
9	-.139	-.093	-.127							-.147	-.142	.007							9
10	-.087	-.046								-.104	-.022								10
11	-.127									-.133									11
								α = 06°		δ = 00°									
1	.346	.126	.163	.009	-.411	-.269	-.349	-.373	-.394					.284	-.052	.196	.202	.230	1
2	-.061	-.240	-.317	-.354	-.256	-.273	-.273	-.331	-.379	.204		.238		.141	-.082	.166	.196	.249	2
3	-.045	-.069		-.133	-.093	-.251	-.163	-.307	-.381	.139	.145	.149		.102	-.048	.154	.130	.241	3
4	-.032	-.087	-.114	-.117		-.245		-.326	-.395	.165		.113	.093		-.055		-.084	-.070	4
5	-.075	-.080	-.096	-.249				-.271		.109	.113	.093	-.052				-.085		5
6	-.056	-.069	-.084	-.234						.113	.130	.113	-.048						6
7	-.021	-.030	-.216	-.232						.125	.120	-.061	-.062						7
8	-.064	-.195	-.212							.101	-.062	-.071							8
9	-.202	-.206	-.187							-.069	-.067	-.075							9
10	-.125	-.204								-.042	-.068								10
11	-.174									-.091									11

[redacted]

Table 4 Continued

Pressure Coefficients on Delta Wing with Control

Configuration B M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 06°									δ = 10°									
1	.345	.131	.164	.012	-.344	-.408	-.360	-.429	-.438					.284	.175	.194	.370	.492	1
2	-.056	-.238	-.316	-.350	-.146	-.407	-.354	-.421	-.429	.210		.240		.141	.084	-.041	.527	.517	2
3	-.042	-.064		-.130	-.025	-.373	-.347	-.411	-.426	.145	.151	.151		.247	.079	.154	.390	.436	3
4	-.028	-.083	-.108	-.074		-.291		-.408	-.415	.170		.115	.280		.069		.133	.164	4
5	-.067	-.080	-.093	-.303				-.375		.118	.115	.091	.020				.125		5
6	-.056	-.064	-.078	-.339						.128	.134	.115	.014						6
7	-.020	-.026	-.190	-.313						.130	.124	-.058	-.069						7
8	-.060	-.188	-.182							.105	-.058	.005							8
9	-.203	-.198	-.192							-.059	-.062	.004							9
10	-.124	-.200								-.034	-.065								10
11	-.172									-.079									11
	α = 06°									δ = 20°									
1	.341	.127	.160	.008	-.343	-.454	-.428	-.441	-.456					.285	.437	.198	.527	.885	1
2	-.064	-.244	-.319	-.350	-.084	-.451	-.424	-.441	-.447	.207		.239		.141	.340	.373	.944	.772	2
3	-.052	-.073		-.127	.046	-.418	-.428	-.445	-.438	.137	.149	.151		.445	.301	.509	.677	.554	3
4	-.037	-.084	-.112	-.083		-.347		-.438	-.402	.168		.114	.382		.282		.474	.470	4
5	-.075	-.085	-.098	-.366				-.410		.110	.118	.090	.103				.419		5
6	-.061	-.073	-.047	-.408						.115	.131	.115	-.032						6
7	-.031	-.030	-.135	-.395						.125	.119	.047	-.138						7
8	-.068	-.194	-.187							.098	-.062	.086							8
9	-.208	-.189	-.209							-.067	-.064	.060							9
10	-.133	-.134								-.038	-.024								10
11	-.178									-.088									11
	α = 06°									δ = 30°									
1	.338	.118	.157	.008	-.178	-.475	-.456	-.464	-.475					.282	.592	.195	.926	1.175	1
2	-.067	-.248	-.323	-.357	-.014	-.468	-.466	-.462	-.459	.202		.237		.140	.605	.507	1.072	1.004	2
3	-.054	-.072		-.036	.041	-.397	-.462	-.464	-.450	.136	.147	.149		.455	.592	.690	.860	.831	3
4	-.040	-.084	-.120	-.123		-.361		-.456	-.426	.170		.111	.356		.460		.789	.672	4
5	-.077	-.082	-.099	-.364				-.409		.110	.115	.088	.134				.664		5
6	-.060	-.073	.056	-.403						.113	.130	.156	-.121						6
7	-.032	-.033	-.146	-.406						.124	.116	.146	-.174						7
8	-.075	-.160	-.216							.098	-.064	.130							8
9	-.211	-.123	-.243							-.070	.001	.087							9
10	-.127	-.117								-.037	.075								10
11	-.078									-.079									11
	α = 12°									δ = 00°									
1	.218	-.088	-.013	-.185	-.490	-.401	-.451	-.462	-.465					.395	.038	.182	.285	.361	1
2	-.270	-.417	-.455	-.470	-.451	-.368	-.434	-.453	-.446	.342		.392		.283	.017	.296	.335	.383	2
3	-.116	-.172		-.431	-.386	-.348	-.405	-.442	-.424	.272	.264	.285		.236	.056	.277	.255	.351	3
4	-.092	-.178	-.198	-.308		-.275		-.451	-.444	.290		.251	.223		.042		.028	.069	4
5	-.146	-.185	-.167	-.364				-.418		.241	.243	.219	.047				.023		5
6	-.127	-.169	-.151	-.387						.236	.262	.243	.051						6
7	-.111	-.110	-.259	-.345						.227	.237	.035	.031						7
8	-.137	-.259	-.264							.219	.032	.019							8
9	-.263	-.258	-.246							.036	.028	.023							9
10	-.178	-.256								.034	.024								10
11	-.228									.023									11
	α = 12°									δ = 10°									
1	.222	-.082	-.007	-.179	-.447	-.441	-.423	-.443	-.456					.394	.341	.182	.693	.660	1
2	-.268	-.413	-.461	-.482	-.378	-.387	-.429	-.442	-.439	.340		.390		.280	.269	.220	.713	.618	2
3	-.115	-.169		-.424	-.437	-.399	-.449	-.444	-.429	.265	.271	.282		.335	.265	.396	.510	.456	3
4	-.096	-.173	-.199	-.259		-.367		-.445	-.410	.285		.247	.311		.207		.298	.334	4
5	-.143	-.177	-.162	-.369				-.435		.236	.242	.216	.157				.259		5
6	-.123	-.164	-.125	-.394						.231	.258	.237	.128						6
7	-.110	-.112	-.244	-.303						.224	.230	.029	.010						7
8	-.134	-.254	-.254							.213	.025	.063							8
9	-.256	-.254	-.261							.033	.025	.096							9
10	-.175	-.238								.028	.016								10
11	-.225									.019									11

[redacted]

Table 4 Continued

Pressure Coefficients on Delta Wing with Control

Configuration B M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
								α = 12°		δ = 20°									
1	.223	-.085	-.007	-.179	-.381	-.436	-.421	-.437	-.445										1
2	-.268	-.415	-.460	-.456	-.292	-.420	-.438	-.430	-.431	.346		.396		.399	.616	.182	.962	1.001	2
3	-.109	-.173		-.339	-.409	-.379	-.459	-.439	-.422	.275	.280	.286		.290	.555	.409	1.042	.849	3
4	-.095	-.174	-.185	-.299		-.438		-.441	-.379	.295		.252	.476	.543	.505	.464	.779	.677	4
5	-.145	-.175	-.193	-.394				-.434		.243	.246	.222	.210		.422		.656	.568	5
6	-.123	-.144	-.124	-.339						.240	.262	.244	.098				.548		6
7	-.110	-.101	-.272	-.294						.228	.237	.096	-.046						7
8	-.129	-.248	-.313							.219	.029	.177							8
9	-.245	-.241	-.304							.036	.032	.171							9
10	-.155	-.234								.036	.058								10
11	-.211									.024									11
								α = 12°		δ = 30°									
1	.228	-.081	-.007	-.180	-.281	-.431	-.441	-.448	-.451										1
2	-.269	-.416	-.454	-.408	-.207	-.419	-.451	-.438	-.431	.340		.390		.393	.827	.181	.968	1.279	2
3	-.107	-.167		-.274	-.398	-.452	-.442	-.444	-.422	.265	.277	.283		.388	.866	.484	1.093	1.135	3
4	-.093	-.173	-.211	-.349		-.459		-.443	-.374	.290		.245	.544	.604	.806	.611	1.064	.953	4
5	-.146	-.172	-.133	-.399				-.425		.236	.240	.215	.286		.657		.947	.721	5
6	-.119	-.129	-.126	-.343						.231	.253	.278	.010				.740		6
7	-.092	-.061	-.254	-.287						.220	.226	.212	-.106						7
8	-.087	-.227	-.299							.210	.023	.247							8
9	-.197	-.254	-.193							.030	.081	.200							9
10	-.101	-.263								.030	.153								10
11	-.147									.015									11
								α = -06°		δ = 00°									
1	.307	.395	.177	.162	.268	-.006	.276	.248	.255										1
2	.195	.201	.224	.233	.150	-.049	.219	.203	.270	-.063		-.289		-.390	-.284	.220	-.262	-.409	2
3	.133	.139		.135	.108	-.043	.197	.162	.283	-.047	.055	-.110		-.302	-.297	-.274	-.346	-.412	3
4	.138	.102	.116	.102		-.052		-.070	-.055	-.040		-.106	-.115	-.108	-.257	-.192	-.289	-.413	4
5	.121	.112	.114	-.042				-.043		-.082	-.080	-.122	-.262		-.245		-.315	-.440	5
6	.110	.113	.112	-.041						-.063	-.066	-.088	-.237				-.308		6
7	.135	.134	-.074	-.049						-.044	-.067	-.216	-.234						7
8	.107	-.070	-.075							-.066	-.200	-.210							8
9	-.060	-.078	-.064							-.216	-.204	-.204							9
10	-.031	-.070								-.157	-.209								10
11	-.070									-.181									11
								α = -06°		δ = 10°									
1	.307	.394	.179	.161	.271	-.300	.114	.061	.035										1
2	.191	.196	.225	.237	.539	-.323	-.286	.005	.027	-.059		-.286		-.389	-.085	.223	-.211	-.134	2
3	.130	.144		.139	.279	-.315	-.288	-.041	.001	-.043	.063	-.107		-.312	-.140	-.425	-.169	-.072	3
4	.137	.107	.114	.179		-.312		-.216	-.303	-.035		-.105	-.090	-.071	-.148	.027	-.107	-.050	4
5	.124	.113	.116	-.153				-.199		-.079	-.076	-.119	-.184		-.148		-.186	-.312	5
6	.111	.116	.130	-.254						-.062	-.063	-.088	-.171				-.181		6
7	.135	.135	-.005	-.247						-.042	-.063	-.216	-.216						7
8	.109	-.073	-.040							-.064	-.193	-.193							8
9	-.071	-.068	-.060							-.212	-.200	-.165							9
10	-.034	-.024								-.151	-.205								10
11	-.069									-.178									11
								α = -06°		δ = 20°									
1	.308	.400	.177	.161	.274	-.440	-.033	-.118	-.339										1
2	.197	.203	.223	.237	.271	-.442	-.397	-.112	-.309	-.060		-.285		-.389	.150	.225	.143	.146	2
3	.131	.146		.136	.571	-.444	-.409	-.145	-.309	-.041	-.053	-.109		-.313	.115	-.161	-.041	.224	3
4	.139	.108	.115	.250		-.406		-.319	-.407	-.034		-.105	-.015	-.138	.082	-.137	.109	.284	4
5	.127	.113	.114	-.194				-.313		-.082	-.077	-.115	-.159		.101		-.006	.015	5
6	.110	.115	.157	-.290						-.061	-.064	-.087	-.246				.003		6
7	.136	.136	.025	-.296						-.043	-.064	-.214	-.268						7
8	.112	-.070	-.033							-.066	-.194	-.129							8
9	-.068	-.044	-.062							-.211	-.198	-.103							9
10	-.031	-.001								-.150	-.203								10
11	-.066									-.174									11

[redacted]

Table 4 Concluded

Pressure Coefficients on Delta Wing with Control

Configuration B M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	$\alpha = -06^\circ$									$\delta = 30^\circ$									
1	.305	.395	.177	.157	.273	-.482	-.160	-.463	-.442	-.063		-.291		-.370	.281	.225	.549	.445	1
2	.193	.201	.221	.241	.157	-.478	-.460	-.255	-.431	-.045	-.066	-.109		-.223	.308	.494	.205	.433	2
3	.131	.143		.138	.697	-.478	-.457	-.242	-.420	-.037		-.109	.022	-.066	.267	-.192	.339	.529	3
4	.139	.112	.113	.352		-.449		-.392	-.432	-.082	-.081	-.124	-.154		.168		.207	.294	4
5	.123	.113	.117	-.203				-.365		-.064	-.066	-.089	-.284				.211		5
6	.108	.118	.185	-.311						-.047	-.068	-.212	-.300						6
7	.133	.136	.051	-.318						-.070	-.198	-.058							7
8	.110	-.072	-.018							-.220	-.202	-.064							8
9	-.069	-.021	-.057							-.149	-.148								9
10	-.037	.024								-.172									10
11	-.068																		11
	$\alpha = -12^\circ$									$\delta = 00^\circ$									
1	.168	.265	.022	-.099	.387	.112	.473	.409	.402	-.270		-.452		-.493	-.429	.295	-.408	-.483	1
2	.342	.355	.379	.383	.300	.070	.387	.363	.424	-.119	-.184	-.351		-.449	-.406	-.459	-.471	-.462	2
3	.257	.255		.283	.238	.072	.364	.317	.413	-.107		-.189	-.292	-.411	-.363	-.431	-.454	-.428	3
4	.261	.239	.249	.230		.060		.057	.114	-.150	-.166	-.190	-.351		-.336		-.445	-.420	4
5	.240	.239	.248	.065				.079		-.132	-.170	-.157	-.378				-.437		5
6	.234	.243	.245	.064						-.124	-.149	-.258	-.321						6
7	.243	.253	.026	.064						-.123	-.255	-.261							7
8	.234	.020	.016							-.267	-.254	-.250							8
9	.032	.024	.026							-.194	-.254								9
10	.060	.035								-.215									10
11	.033																		11
	$\alpha = -12^\circ$									$\delta = 10^\circ$									
1	.164	.265	.028	-.097	.383	-.271	.249	.187	.168	-.273		-.453		-.497	-.403	.294	-.367	-.297	1
2	.338	.355	.381	.382	.735	-.257	-.200	.112	.185	-.118	-.184	-.353		-.435	-.421	-.490	-.399	-.340	2
3	.259	.254		.283	.426	-.202	-.236	.067	.191	-.110		-.193	-.277	-.399	-.335	-.451	-.418	-.347	3
4	.261	.240	.249	.304		-.210		-.140	-.134	-.152	-.168	-.189	-.347		-.323		-.462	-.424	4
5	.238	.237	.250	-.074				-.113		-.130	-.172	-.161	-.321				-.438		5
6	.232	.243	.308	-.189						-.129	-.150	-.261	-.322						6
7	.243	.252	.089	-.191						-.125	-.256	-.229							7
8	.234	.027	.045							-.270	-.256	-.237							8
9	.038	.071	.027							-.193	-.255								9
10	.060	.089								-.209									10
11	.034																		11
	$\alpha = -12^\circ$									$\delta = 20^\circ$									
1	.165	.263	.025	-.099	.392	-.389	.134	.058	-.142	-.269		-.451		-.495	-.430	.295	-.036	-.033	1
2	.346	.355	.380	.385	.713	-.411	-.336	.003	-.058	-.118	-.184	-.352		-.453	-.435	-.300	-.283	.013	2
3	.257	.253		.288	.681	-.420	-.371	-.079	-.098	-.107		-.192	-.208	-.357	-.369	-.488	-.331	.047	3
4	.262	.239	.253	.378		-.408		-.251	-.337	-.149	-.165	-.187	-.330		-.307		-.338	-.222	4
5	.240	.242	.253	-.107				-.245		-.129	-.168	-.155	-.340				-.347		5
6	.237	.245	.342	-.216						-.123	-.148	-.258	-.367						6
7	.247	.258	.122	-.225						-.126	-.257	-.130							7
8	.239	.028	.056							-.266	-.254	-.203							8
9	.037	.099	.026							-.187	-.252								9
10	.059	.106								-.201									10
11	.040																		11
	$\alpha = -12^\circ$									$\delta = 30^\circ$									
1	.160	.262	.021	-.103	.390	-.460	-.043	-.290	-.354	-.269		-.452		-.493	-.361	1.828	-.329	-.118	1
2	.335	.352	.379	.381	.313	-.468	-.426	-.140	-.417	-.121	-.185	-.354		-.457	-.318	.301	.463	.226	2
3	.257	.251		.284	.825	-.463	-.445		-.349	-.109		-.193	-.146	-.313	-.394	.437	.010	.262	3
4	.258	.235	.250	.484		-.453		-.197	-.339	-.150	-.167	-.191	-.329		-.373		-.195	.327	4
5	.236	.237	.252	-.118				-.348		-.129	-.174	-.157	-.347				-.261		5
6	.232	.242	.369	-.244						-.127	-.148	-.262	-.430						6
7	.242	.256	.141	-.252						-.126	-.258	-.133							7
8	.234	.026	.071							-.265	-.254	-.175							8
9	.033	.118	.027							-.184	-.254								9
10	.053	.120								-.195									10
11	.035																		11

Table 5

Pressure Coefficients on Delta Wing with Control

Configuration C M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 00°									δ = 00°									
1	.390	.359	.295	.274	-.138	.014	.335	.341	.032	.072		.039		-.108	.015			.012	1
2	.056	.043	.032	.032	-.185	.003	.030	.018	.000	.034	.003	.007		-.115	-.004	-.012	.012	.001	2
3	.029	.023		.009	-.149	.001	-.002	.010	-.284	.039		-.016		-.181	-.037	-.002	-.007	-.287	3
4	.035	.006	-.012	-.012	-.155		-.104	-.211		-.004	.005	-.033	-.013	-.169		-.055	-.204		4
5	.011	.011	.011	-.157				-.234		.014	.006	.001	-.163				-.203		5
6	.016	.012	.002	-.150						.029	.012	-.150	-.157						6
7	.038	.020	-.150	-.152						-.013	-.157	-.176	-.170						7
8	.004	-.146	-.150							-.155	-.172	-.155							8
9	-.148	-.141	-.135							-.107	-.157								9
10	-.112	-.148								-.151									10
11	-.161																		11
	α = 00°									δ = 10°									
1	.389	.356	.297	.274	-.328	.017	.369	.050	-.339	.071		.038		.232	.012			.271	1
2	.056	.043	.031	.033	-.335	-.041	-.031	-.287	-.369	.029	.014	.007		.073	.062	.139	.256	.272	2
3	.027	.021		.010	-.295	-.071	-.086	-.111	-.393	.036		-.015		-.040	.021	.184	.149	-.034	3
4	.032	.002	-.012	-.043	-.271		-.246	-.284		-.002	.005	-.033	.033	-.058		.088	-.092		4
5	.011	.008	.010	-.216				-.336		.012	.007	.003	-.075				-.029		5
6	.016	.012	.003	-.225						.024	.013	-.159	-.102						6
7	.038	.023	-.145	-.234						-.012	-.158	-.157	-.176						7
8	.003	-.146	-.159							-.157	-.174	-.110							8
9	-.149	-.140	-.153							-.110	-.159								9
10	-.115	-.144								-.155									10
11	-.164																		11
	α = 00°									δ = 20°									
1	.389	.357	.294	.276	-.443	.016	.162	-.263	-.383	.065		.035		.654	.010			.500	1
2	.057	.042	.032	.030	-.450	.283	-.080	-.370	-.415	.029	.014	.003		.305	.024	.513	.539	.469	2
3	.028	.023		.012	-.399	-.279	-.159	-.351	-.433	.033		-.021	.082	.187	.111	.446	.343	.210	3
4	.031	.004	-.012	-.025	-.413		-.342	-.347		-.008	.000	-.037	.010	.132		.207	.096		4
5	.007	.007	.012	-.250				-.397		.010	.001	-.001	-.141				.187		5
6	.015	.008	.003	-.295						.026	.008	-.165	-.238						6
7	.039	.021	-.114	-.284						-.014	-.160	-.071							7
8	.004	-.146	-.150							-.159	-.175	-.031							8
9	-.151	-.141	-.155							-.111	-.162								9
10	-.117	-.133								-.156									10
11	-.166																		11
	α = 00°									δ = 30°									
1	.390	.359	.299	.280	-.481	.022	-.152	-.388	-.424	.071		.039		1.248	.013			.730	1
2	.063	.051	.038	.042	-.484	.490	-.321	-.453	-.421	.035	.023	.011		.621	-.025	.844	.834	.589	2
3	.031	.030		.018	-.455	-.337	-.267	-.434	-.398	.041		-.014	.270	.483	.257	.747	.628	.561	3
4	.034	.009	-.006	.069	-.421		-.427	-.439		.000	.005	-.031	.058	.411		.504	.510		4
5	.012	.012	.016	-.273				-.424		.016	.007	.003	-.193				.466		5
6	.020	.017	.032	-.333						.029	.014	-.106	-.274						6
7	.043	.028	-.069	-.341						-.013	-.152	.020							7
8	.009	-.139	-.129							-.154	-.172	.006							8
9	-.140	-.116	-.145							-.103	-.077								9
10	-.110	-.083								-.144									10
11	-.155																		11
	α = 06°									δ = 00°									
1	.341	.097	.155	.005	-.228	-.373	.060	-.055	-.378	.205		.234		-.002	.227			.235	1
2	-.073	-.251	-.325	-.359	-.304	-.293	-.340	-.379	-.393	.138	.143	.154		-.030	.141	.217	.239	.234	2
3	-.055	-.070		-.127	-.248	-.078	-.312	-.331	-.402	.181		.114	.116	-.080	.098	.167	.154	-.080	3
4	-.031	-.088	-.116	-.130	-.251		-.259	-.390		.104	.114	.085	-.083	-.076		.107	-.085		4
5	-.081	-.083	-.096	-.235				-.351		.114	.116	.116	-.074				-.090		5
6	-.062	-.077	-.087	-.238						.118	.114	-.067	-.085						6
7	-.039	-.060	-.211	-.249						.092	-.077	-.098							7
8	-.075	-.203	-.214							-.074	-.100	-.075							8
9	-.204	-.202	-.201							-.049	-.078								9
10	-.170	-.206								-.083									10
11	-.198																		11

[redacted]

Table 5 Continued

Pressure Coefficients on Delta Wing with Control

Configuration C M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	$\alpha = 06^\circ$									$\delta = 10^\circ$									
1	.339	.088	.150	.002	-.388	-.347	.230	-.266	-.452	.207		.240		.408	.230		.523	.452	1
2	-.079	-.260	-.329	-.365	-.349	-.467	-.419	-.457	-.457	.141	.151	.154		.187	.202	.322	.375	.421	2
3	-.061	-.077		-.130	-.352	-.163	-.336	-.453	-.393	.185		.111	.164	.104	.221	.424	.096	.164	3
4	-.038	-.093	-.119	-.184	-.284		-.313	-.467		.109	.115	.087	.060	.082		.323	.126		4
5	-.083	-.087	-.097	-.290				-.443		.121	.120	.113	.020						5
6	-.070	-.078	-.068	-.303						.122	.113	-.073	-.087						6
7	-.049	-.067	-.200	-.301						.094	-.073	-.076							7
8	-.080	-.207	-.229							-.073	-.095	-.005							8
9	-.208	-.201	-.232							-.043	-.077								9
10	-.181	-.194								-.079									10
11	-.204																		11
	$\alpha = 06^\circ$									$\delta = 20^\circ$									
1	.338	.092	.153	.004	-.465	-.348	.038	-.367	-.464	.201		.237		.757	.227		.841	.700	1
2	-.076	-.258	-.327	-.363	-.451	.265	-.463	-.452	-.438	.139	.155	.151		.468	.034	.477	.659	.535	2
3	-.059	-.074		-.120	-.375	-.371	-.389	-.474	-.390	.185		.112	.323	.351	.434	.591	.439	.483	3
4	-.037	-.092	-.119	-.193	-.339		-.408	-.444		.105	.118	.087	.136	.288		.569	.383		4
5	-.081	-.089	-.098	-.328				-.441		.121	.115	.114	-.007						5
6	-.070	-.079	.008	-.356						.120	.116	-.072	-.121						6
7	-.047	-.068	-.179	-.369						.093	-.076	.053							7
8	-.082	-.203	-.233							-.074	-.095	.060							8
9	-.208	-.156	-.217							-.042	-.079								9
10	-.184	-.168								-.083									10
11	-.194																		11
	$\alpha = 12^\circ$									$\delta = 00^\circ$									
1	.198	-.117	-.035	-.196	-.447	-.484	-.322	-.334	-.464	.356		.409		.098	.369		.387	.377	1
2	.304	-.432	-.470	-.482	-.413	-.497	-.466	-.478	-.441	.283	.281	.297		.058	.287	.343	.333	.354	2
3	-.131	-.190		-.441	-.346	-.449	-.423	-.464	-.453	.309		.262	.262	.031	.244	.317	.035	.083	3
4	-.098	-.194	-.268	-.343	-.333		-.436	-.471		.244	.254	.223	.018	.031		.238	.028		4
5	-.159	-.196	-.217	-.370				-.432		.252	.252	.252	.031						5
6	-.139	-.171	-.168	-.354						.221	.243	.036	.018						6
7	-.123	-.144	-.262	-.308						.225	.024	-.002							7
8	-.146	-.271	-.267							.037	.000	.026							8
9	-.264	-.258	-.246							.016	.023								9
10	-.251	-.267								.035									10
11	-.225																		11
	$\alpha = 12^\circ$									$\delta = 10^\circ$									
1	.196	-.119	-.034	-.195	-.414	-.478	.025	-.406	-.413	.352		.409		.557	.369		.687	.595	1
2	-.301	-.431	-.471	-.481	-.421	-.492	-.421	-.419	-.398	.277	.284	.292		.290	.283	.555	.582	.461	2
3	-.131	-.191		-.405	-.438	-.449	-.418	-.427	-.346	.305		.261	.316	.246	.470	.409	.315	.375	3
4	-.097	-.191	-.267	-.272	-.398		-.428	-.418		.237	.250	.219	.185	.204		.347	.269		4
5	-.163	-.199	-.217	-.333				-.425		.248	.250	.246	.143						5
6	-.144	-.172	-.141	-.334						.217	.240	.021	.012						6
7	-.125	-.142	-.243	-.323						.223	.020	.041							7
8	-.148	-.270	-.282							.034	-.005	.113							8
9	-.268	-.236	-.285							.016	.014								9
10	-.252	-.245								.030									10
11	-.222																		11
	$\alpha = 12^\circ$									$\delta = 20^\circ$									
1	.196	-.119	-.036	-.192	-.437	-.430	-.173	-.425	-.437	.349		.405		.832	.364		1.024	.803	1
2	.304	-.432	-.473	-.461	-.444	.068	-.418	-.433	-.425	.275	.282	.291		.596	.150	.741	.838	.659	2
3	-.129	-.192		-.340	-.444	.472	-.431	-.448	-.372	.304		.255	.504	.507	.703	.524	.642	.591	3
4	-.097	-.192	-.181	-.385	-.435		-.446	-.442		.238	.251	.216	.235	.438		.669	.544		4
5	-.159	-.197	-.165	-.420				-.448		.245	.247	.246	.102						5
6	-.142	-.159	-.136	-.399						.214	.235	.032	-.034						6
7	-.125	-.121	-.267	-.281						.216	.017	.166							7
8	-.141	-.244	-.278							.032	-.006	.174							8
9	-.255	-.227	-.283							.013	.019								9
10	-.222	-.236								.028									10
11	-.179																		11

[redacted]

Table 5 Continued

Pressure Coefficients on Delta Wing with Control

Configuration C $M = 1.61$ $R = 4.2 \times 10^6$

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	$\alpha = 12^\circ$									$\delta = 30^\circ$									
1	.199	-.107	-.025	-.182	-.430	-.345	-.291	-.441	-.418					1.016	.369			1.018	1
2	-.298	-.423	-.441	-.282	-.438	.411	-.453	-.427	-.414	.349		.409		.954	.170	1.078	1.254	.885	2
3	-.124	-.185		-.281	-.469	-.471	-.425	-.432	-.395	.279	.284	.292		.785	.966	.767	1.162	.721	3
4	-.092	-.187	-.249	-.355	-.446		-.432	-.425		.306		.261	.597	.651		.962	.975		4
5	-.151	-.163	-.080	-.389				-.432		.239	.252	.217	.343				.759		5
6	-.134	-.144	-.092	-.369						.246	.249	.265	.050						6
7	-.093	-.074	-.210	-.363						.215	.238	.227	-.067						7
8	-.104	-.217	-.276							.219	.020	.245							8
9	-.216	-.231	-.165							.035	.040	.208							9
10	-.168	-.226								.015	.164								10
11	-.128									.031									11
	$\alpha = 15^\circ$									$\delta = 00^\circ$									
1	.142	-.174	-.151	-.235	-.453	-.498	-.387	-.394	-.406					.171	.445			.458	1
2	-.356	-.445	-.471	-.473	-.437	-.494	-.421	-.448	-.389	.419		.457		.112	.385	.407	.463	.377	2
3	-.147	-.238		-.448	-.428	-.451	-.435	-.417	-.344	.343	.349	.364		.107	.345	.410	.432	.179	3
4	-.107	-.218	-.382	-.327	-.380		-.404	-.407		.362		.359	.365	.107		.316	.104		4
5	-.180	-.214	-.310	-.387				-.406		.309	.338	.336	.084				.104		5
6	-.160	-.201	-.207	-.344						.326	.358	.356	.100						6
7	-.139	-.165	-.277	-.264						.321	.356	.119	.094						7
8	-.160	-.284	-.281							.332	.100	.073							8
9	-.274	-.279	-.269							.121	.074	.089							9
10	-.256	-.273								.074	.094								10
11	-.223									.124									11
	$\alpha = 15^\circ$									$\delta = 10^\circ$									
1	.141	-.177	-.159	-.246	-.407	-.445	-.058	-.429	-.401					.637	.445			.662	1
2	-.355	-.449	-.483	-.472	-.436	-.450	-.392	-.408	-.379	.415		.455		.363	.395	.626	.800	.480	2
3	-.149	-.237		-.373	-.428	-.427	-.406	-.412	-.328	.341	.350	.363		.338	.620	.390	.673	.451	3
4	-.109	-.219	-.391	-.342	-.398		-.413	-.408		.362		.355	.448	.298		.394	.414		4
5	-.180	-.217	-.312	-.370				-.415		.305	.335	.330	.269				.371		5
6	-.163	-.200	-.151	-.375						.324	.354	.347	.237						6
7	-.138	-.165	-.291	-.313						.319	.351	.104	.088						7
8	-.164	-.273	-.325							.326	.094	.140							8
9	-.273	-.240	-.330							.117	.063	.185							9
10	-.256	-.238								.070	.083								10
11	-.210									.120									11
	$\alpha = 15^\circ$									$\delta = 20^\circ$									
1	.138	-.183	-.162	-.247	-.437	-.432	-.229	-.437	-.430					.905	.440			.865	1
2	-.358	-.451	-.458	-.382	-.443	.006	-.428	-.432	-.415	.413		.452		.673	.241	.834	1.133	.734	2
3	-.151	-.247		-.356	-.440	-.484	-.425	-.443	-.370	.337	.345	.359		.607	.819	.432	.984	.636	3
4	-.114	-.214	-.405	-.397	-.436		-.445	-.435		.355		.353	.626	.526		.764	.772		4
5	-.184	-.197	-.337	-.442				-.445		.301	.333	.324	.330				.632		5
6	-.168	-.190	-.199	-.413						.318	.349	.343	.178						6
7	-.140	-.162	-.269	-.347						.316	.349	.155	.037						7
8	-.153	-.247	-.289							.320	.093	.259							8
9	-.266	-.242	-.284							.110	.063	.255							9
10	-.251	-.264								.066	.123								10
11	-.159									.110									11
	$\alpha = 15^\circ$									$\delta = 30^\circ$									
1	.140	-.177	-.156	-.233	-.436	-.389	-.309	-.433	-.423					1.071	.440			1.088	1
2	-.356	-.423	-.360	-.282	-.445	.336	-.440	-.429	-.411	.418		.451		1.024	.347	1.134	1.360	.929	2
3	-.144	-.332		-.310	-.442	-.485	-.425	-.435	-.370	.341	.348	.361		.875	1.037	.777	1.270	.758	3
4	-.111	-.297	-.260	-.377	-.437		-.438	-.430		.359		.353	.728	.731		1.030	1.062		4
5	-.180	-.156	-.147	-.406				-.445		.303	.336	.327	.403				.807		5
6	-.148	-.129	-.169	-.367						.324	.351	.397	.121						6
7	-.111	-.090	-.230	-.353						.317	.347	.321	-.004						7
8	-.114	-.257	-.251							.324	.095	.331							8
9	-.212	-.264	-.195							.112	.174	.288							9
10	-.184	-.046								.070	.258								10
11	-.154									.121									11

[redacted]

Table 5 Continued

Pressure Coefficients on Delta Wing with Control

Configuration C · M = 1.61 · R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	$\alpha = -06^\circ$									$\delta = 00^\circ$									
1	.297	.359	.169	.157	-.035	.234	.123	.172	.264	-.081		-.312		-.211	-.368		-.355	-.363	-.404	1
2	.200	.213	.238	.256	-.073	.140	.263	.241	.243	-.057	-.089	-.116		-.182	-.288		-.289	-.330	-.410	2
3	.138	.148		.148	-.052	.146	.157	.180	-.071	-.049		-.118	-.133	-.268	-.118		-.207	-.383	-.410	3
4	.145	.106	.128	.127	-.062		.047	-.084		-.092	-.093	-.126	-.241	-.266				-.358		4
5	.117	.122	.129	-.079				-.126		-.076	-.085	-.100	-.249							5
6	.122	.124	.115	-.064						-.059	-.081	-.226	-.264							6
7	.140	.128	-.063	-.059						-.098	-.219	-.245								7
8	.108	-.066	-.061							-.224	-.233	-.228								8
9	-.069	-.064	-.047							-.171	-.222									9
10	-.039	-.065								-.196										10
11	-.090																			11
	$\alpha = -06^\circ$									$\delta = 10^\circ$									
1	.303	.368	.174	.160	-.283	.238	.442	.266	.042	-.076		-.307		.030	-.365		.127	-.056	-.038	1
2	.209	.219	.244	.256	-.296	.166	.152	.037	-.013	-.051	-.089	-.115		-.039	-.377		-.447	-.213	-.028	2
3	.141	.156		.151	-.243	.039	-.004	.034	-.309	-.044		-.112	-.101	-.168	-.267		-.175	-.343	-.293	3
4	.155	.115	.133	.123	-.237		-.194	-.198		-.089	-.088	-.135	-.211	-.161				-.190		4
5	.125	.129	.136	-.129				-.260		-.070	-.083	-.094	-.224							5
6	.127	.132	.129	-.172						-.053	-.076	-.204	-.264							6
7	.144	.137	-.047	-.178						-.093	-.209	-.222								7
8	.113	-.059	-.059							-.220	-.228	-.209								8
9	-.067	-.053	-.054							-.169	-.215									9
10	-.033	-.047								-.192										10
11	-.083																			11
	$\alpha = -06^\circ$									$\delta = 20^\circ$									
1	.302	.370	.178	.162	-.414	.237	.211	-.202	-.311	-.081		-.310		.257	-.369				.203	1
2	.205	.222	.246	.264	-.429	.256	.053	-.310	-.320	-.050	-.088	-.115		.177	-.326		.516	.226	.233	2
3	.143	.156		.155	-.392	.007	-.110	-.067	-.414	-.042		-.117	-.048	.066	-.356		.201	-.083	-.044	3
4	.160	.117	.132	.109	-.396		-.288	-.273		-.090	-.092	-.135	-.161	.021			-.133	-.221		4
5	.124	.127	.137	-.137				-.361		-.071	-.082	-.099	-.253					-.003		5
6	.129	.130	.125	-.202						-.052	-.075	-.208	-.318							6
7	.145	.140	-.038	-.214						-.095	-.212	-.191								7
8	.115	-.056	-.065							-.222	-.231	-.146								8
9	-.065	-.052	-.060							-.164	-.216									9
10	-.032	-.043								-.193										10
11	-.083																			11
	$\alpha = -06^\circ$									$\delta = 30^\circ$									
1	.304	.365	.174	.159	-.463	.238	-.103	-.390	-.378	-.077		-.313		.806	-.372				.428	1
2	.205	.220	.244	.260	-.472	.497	-.063	-.429	-.393	-.057	-.089	-.119		.323	-.320		.829	.483	.458	2
3	.140	.151		.156	-.453	-.114	-.224	-.228	-.432	-.044		-.119	.005	.291	-.228		.546	.100	.210	3
4	.162	.112	.129	.169	-.454		-.383	-.337		-.088	-.091	-.137	-.149	.241			.017	-.040		4
5	.122	.121	.135	-.167				-.398		-.072	-.084	-.100	-.292					.229		5
6	.122	.125	.123	-.228						-.055	-.079	-.215	-.348							6
7	.140	.132	.000	-.246						-.101	-.215	-.088								7
8	.111	-.059	-.051							-.226	-.232	-.093								8
9	-.067	-.054	-.064							-.169	-.185									9
10	-.036	-.025								-.194										10
11	-.090																			11
	$\alpha = -12^\circ$									$\delta = 00^\circ$									
1	.176	.257	.027	-.088	.060	.369	-.055	-.079	.405	-.275		-.435		-.405	-.470				-.447	1
2	.349	.352	.382	.391	.031	.275	.402	.373	.354	-.115	-.195	-.350		-.240	-.487		-.439	-.403	-.437	2
3	.253	.252		.287	.053	.279	.302	.326	.070	-.095		-.195	-.324	-.371	-.453		-.397	-.434	-.442	3
4	.288	.239	.255	.253	.041		.167	.023		-.154	-.164	-.173	-.338	-.300			-.402	-.437		4
5	.233	.240	.251	.008				-.030		-.128	-.168	-.156	-.332					-.419		5
6	.228	.242	.231	.036						-.121	-.156	-.254	-.300							6
7	.233	.239	.025	.041						-.153	-.267	-.281								7
8	.223	.023	.030							-.264	-.275	-.267								8
9	.016	.030	.050							-.195	-.262									9
10	.038	.025								-.222										10
11	-.006																			11

[redacted]

Table 5 Concluded

Pressure Coefficients on Delta Wing with Control

Configuration C M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = -12°									δ = 10°									
1	.174	.251	.021	-.098	-.233	.363	.492	.266	.204	-.275		-.452		-.429	-.479			-.256	1
2	.343	.349	.375	.378	-.250	.397	.279	.199	.175	-.120	-.186	-.358		-.255	-.514	.214	-.163	-.292	2
3	.254	.245		.278	-.210	.143	-.053	.137	-.143	-.098		-.196	-.297	-.382	-.487	-.469	-.343	-.408	3
4	.282	.233	.246	.235	-.189		-.127	-.163		-.154	-.170	-.182	-.279	-.382		-.412	-.441		4
5	.230	.230	.239	-.054				-.203		-.132	-.171	-.158	-.343				-.422		5
6	.224	.237	.246	-.110						-.120	-.158	-.232	-.307						6
7	.228	.233	.031	-.118						-.155	-.269	-.265							7
8	.217	.018	.019							-.267	-.279	-.267							8
9	.007	.036	.020							-.199	-.265								9
10	.031	.033								-.223									10
11	-.007																		11
	α = -12°									δ = 20°									
1	.193	.271	.038	-.080	-.370	.370	.269	-.173	-.085	-.273		-.454		-.399	-.479			.059	1
2	.361	.364	.394	.395	-.384	.354	.168	-.198	-.112	-.118	-.182	-.358		-.264	-.515	.553	.129	.076	2
3	.270	.263		.296	-.360	.161	-.082	.023	-.363	-.099		-.197	-.226	-.432	-.490	.237	-.248	-.188	3
4	.306	.251	.264	.253	-.347		-.266	-.248		-.153	-.169	-.177	-.360	-.359		-.448	-.388		4
5	.248	.251	.261	-.045				-.338		-.133	-.169	-.157	-.355				-.389		5
6	.241	.254	.263	-.129						-.119	-.156	-.229	-.363						6
7	.247	.251	.055	-.145						-.154	-.275	-.229							7
8	.237	.035	.032							-.268	-.279	-.220							8
9	.026	.054	.038							-.196	-.265								9
10	.049	.058								-.223									10
11	.007																		11
	α = -12°									δ = 30°									
1	.180	.252	.021	-.095	-.430	.368	-.069	-.368	-.284	-.271		-.455		-.342	-.477			.258	1
2	.344	.349	.381	.383	-.439	.555	.012	-.373	-.302	-.121	-.187	-.356		-.281	-.502	.857	.425	.295	2
3	.256	.251		.284	-.422	.272	-.167	-.060	-.408	-.095		-.198	-.187	-.427	-.471	.618	-.135	.042	3
4	.288	.237	.253	.281	-.424		-.351	-.310		-.155	-.170	-.180	-.345	-.396		-.454	-.305		4
5	.235	.242	.250	-.057				-.396		-.133	-.171	-.159	-.364				-.285		5
6	.230	.244	.246	-.147						-.119	-.160	-.241	-.381						6
7	.232	.238	.068	-.169						-.156	-.273	-.196							7
8	.225	.022	.030							-.268	-.278	-.192							8
9	.014	.049	.021							-.193	-.266								9
10	.035	.065								-.222									10
11	.001																		11

[redacted]

Table 6

Pressure Coefficients on Delta Wing with Control

Configuration D M = 1.61 R = 4.2 x 10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 00°									δ = 00°									
1	.383	.349	.289	.276	.318	.318		.029		.047		.033		-.029	.023	.035			1
2	.059	.043	.032	.030	.031	.029	.033			.010	.013	.000		.029	-.001	.013			2
3	.024	.023		.018	.018	1.734	.015			.018		-.022	-.012	.001	-.018	-.007			3
4	.034	.011	-.014	.002	-.001	-.001	.018			-.006	-.002	-.017	-.154	-.013	-.038	-.172			4
5	.011	.006	.005	-.147	-.010	-.016	-.105			.003	.016	.018	-.146	-.165	-.172				5
6	.020	.052	.016	-.157	-.139	-.170				.003	.014	-.151	-.140	-.149					6
7	.032	.028	-.146	-.159	-.155					.003	-.142	-.146							7
8	.009	-.138	-.133							-.142	-.144	-.139							8
9	.224	-.137	-.151							-.085	-.144								9
10	-.062	-.137								-.143									10
11	-.137																		11
	α = 00°									δ = 05°									
1	.389	.352	.293	.281	.290	.279		-.230		.067		.048		.124	.144	.169			1
2	.065	.054	.041	.034	-.056	-.180	-.203			.031	.029	.008		.137	.069	.134			2
3	.033	.031		-.012	-.022	1.736	-.088			.037		-.013	.022	.058	.069	.086			3
4	.039	.018	-.003	-.038	-.040	-.058	-.073			.001	.003	.006	-.145	.024	.037	-.090			4
5	.016	.016	-.007	-.172	-.040	-.069	-.159			.029	.028	.041	-.142	-.129	-.127				5
6	.018	.061	-.002	-.174	-.174	-.196				.016	.029	-.118	-.150	-.114					6
7	.039	.025	-.155	-.174	-.178					.016	-.128	-.118							7
8	.021	-.141	-.156							-.136	-.115	-.118							8
9	.230	-.141	-.156							-.077	-.115								9
10	-.062	-.155								-.123									10
11	-.133																		11
	α = 00°									δ = 10°									
1	.383	.354	.281	.279	.299	.209		-.345		.067		.035		.234	.294	.284			1
2	.065	.047	.033	.032	-.038	-.298	-.316			.033	.031	.012		.354	.170	.235			2
3	.029	.022		-.110	-.050	1.739	-.244			.033		-.023	.017	.120	.145	.184			3
4	.038	.014	-.006	-.056	-.075	-.095	-.166			-.006	.007	-.007	-.161	.057	.101	-.047			4
5	.017	.013	-.003	-.174	-.078	-.105	-.167			.020	.019	.067	-.202	-.092	-.077				5
6	.020	.056	-.029	-.191	-.204	-.227				.018	.020	-.101	-.168	-.071					6
7	.039	.027	-.177	-.190	-.229					.010	-.115	-.101							7
8	.014	-.154	-.178							-.136	-.101	-.107							8
9	.213	-.161	-.174							-.074	-.102								9
10	-.060	-.161								-.129									10
11	-.131																		11
	α = 00°									δ = 15°									
1	.388	.352	.289	.284	.303	.115		-.362		.072		.043		.335	.414	.407			1
2	.070	.054	.042	.043	-.265	-.323	-.351			.036	.035	.001		.322	.303	.355			2
3	.032	.032		-.119	-.085	1.738	-.303			.039		-.018	-.014	.223	.226	.295			3
4	.043	.014	-.002	-.114	-.133	-.111	-.299			.001	.007	.001	-.205	.120	.179	.022			4
5	.025	.014	.017	-.185	-.136	-.133	-.331			.022	.029	.108	-.244	-.048	-.005				5
6	.017	.059	-.058	-.194	-.215	-.232				.021	.024	-.078	-.196	.002					6
7	.044	.044	-.199	-.190	-.266					.007	-.092	-.077							7
8	.020	-.145	-.199							-.131	-.077	-.094							8
9	.209	-.162	-.197							-.078	-.082								9
10	-.047	-.180								-.108									10
11	-.120																		11
	α = 00°									δ = 20°									
1	.388	.352	.288	.280	.305	.039		-.390		.064		.033		.482	.502	.530			1
2	.066	.048	.038	.035	-.355	-.367	-.379			.035	.029	.003		.481	.434	.473			2
3	.032	.029		.123	-.126	1.739	-.370			.037		-.011	-.094	.372	.337	.419			3
4	.042	.012	-.006	-.218	-.180	-.264	-.385			-.004	.001	.000	-.211	.189	.284	.120			4
5	.022	.012	.055	-.221	-.184	-.200	-.392			.021	.018	.134	-.245	.029	.079				5
6	.014	.055	-.074	-.195	-.244	-.256				.014	.022	-.058	-.221	.074					6
7	.038	.054	-.235	-.194	-.317					.003	-.071	-.069							7
8	.015	-.143	-.227							-.137	-.056	-.087							8
9	.214	-.173	-.227							-.072	-.062								9
10	-.043	-.186								-.076									10
11	-.111																		11

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Table 6 Continued

Pressure Coefficients on Delta Wing with Control

Configuration D M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station								Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 00°									δ = 25°									
1	.395	.356	.298	.287	.290	-.032		-.407		.051		.035		.639	.664	.630			1
2	.073	.058	.043	.035	-.392	-.400	-.393			.024	.033	-.007		.647	.600	.600			2
3	.043	.034		.403	-.178	1.743	-.388			.032		-.018	-.164	.524	.445	.532			3
4	.044	.020	-.002	-.304	-.199	-.337	-.412			-.015	-.003	.003	-.231	.268	.406	.168			4
5	.030	.021	.110	-.279	-.223	-.286	-.412			.010	.016	.173	-.271	.120	.185				5
6	.025	.069	-.092	-.217	-.227	-.295				.008	.026	-.039	-.256	.160					6
7	.051	.078	-.257	-.198	-.341					-.002	-.049	-.064							7
8	.028	-.136	-.257							-.140	-.039	-.109							8
9	.223	-.166	-.253							-.058	-.040								9
10	-.020	-.181								-.034									10
11	-.089																		11
	α = 00°									δ = 30°									
1	.387	.345	.290	.277	.264	-.115		-.416		.061		.038		.811	.801	.740			1
2	.060	.044	.042	.029	-.415	-.413	-.412			.033	.036	.005		.792	.710	.725			2
3	.030	.023		.618	-.252	1.747	-.405			.033		-.017	-.192	.688	.555	.677			3
4	.034	.007	-.003	-.369	-.240	-.377	-.431			-.001	-.003	.013	-.275	.371	.536	.219			4
5	.023	.005	.169	-.295	-.269	-.335	-.424			.015	.026	.219	-.312	.220	.301				5
6	.009	.062	-.105	-.232	-.223	-.333				.014	.059	-.018	-.272	.250					6
7	.038	.083	-.280	-.211	-.354					-.003	-.020	-.069							7
8	.025	-.137	-.298							-.129	-.003	-.109							8
9	.209	-.181	-.293							-.021	-.014								9
10	.002	-.196								.100									10
11	-.074																		11
	α = 03°									δ = 00°									
1	.380	.221	.228	.145	.231	.258		-.255		.129		.149		.157	.152	.178			1
2	-.005	-.071	-.139	-.202	-.199	-.230	-.262			.066	.077	.072		.124	.110	.140			2
3	-.020	-.026		-.072	-.083	1.749	-.214			.071		.048	.055	.076	.066	.131			3
4	-.006	-.041	-.070	-.068	-.075	-.088	-.094			.041	.052	.040	-.108	.053	.052	-.087			4
5	-.034	-.041	-.047	-.190	.085	-.095	-.182			.054	.067	.072	-.099	-.106	-.104				5
6	-.021	.002	-.040	-.202	-.188	-.234				.053	.064	-.106	-.099	-.106					6
7	-.009	-.024	-.178	-.202	-.198					.047	-.110	-.109							7
8	-.025	-.175	-.180							-.116	-.102	-.100							8
9	.226	-.169	-.180							-.053	-.105								9
10	-.097	-.169								-.122									10
11	-.151																		11
	α = 06°									δ = -02°									
1	.340	.105	.153	.020	.196	.181		-.362		.184		.230		.245	.232	.248			1
2	-.069	-.244	-.312	-.355	-.362	-.385	-.390			.115	.137	.139		.197	.170	.219			2
3	-.049	-.065		-.208	-.310	1.742	-.337			.128		.107	.082	.160	.147	.179			3
4	-.032	-.080	-.110	-.137	-.250	-.277	-.319			.110	.103	.088	-.079	.122	.105	-.037			4
5	-.077	-.079	-.090	-.228	-.140	-.186	-.355			.105	.121	.114	-.079	-.021	-.031				5
6	-.054	-.034	-.067	-.247	-.288	-.308				.105	.107	-.083	-.079	-.047					6
7	-.043	-.052	-.204	-.246	-.303					.095	-.080	-.083							7
8	-.065	-.193	-.206							-.064	-.080	-.084							8
9	.212	-.191	-.206							-.016	-.076								9
10	-.110	-.191								-.092									10
11	-.163																		11
	α = 06°									δ = 00°									
1	.334	.101	.144	.015	.176	.164		-.344		.191		.234		.239	.249	.262			1
2	-.067	-.246	-.314	-.355	-.323	-.351	-.355			.127	.146	.152		.210	.182	.210			2
3	-.052	-.067		-.147	-.281	1.744	-.341			.140		.103	.121	.148	.133	.184			3
4	-.035	-.080	-.122	-.123	-.166	-.217	-.316			.110	.112	.101	-.057	.120	.111	-.030			4
5	-.084	-.081	-.098	-.235	-.119	-.146	-.355			.110	.132	.136	-.051	-.059	-.049				5
6	-.055	-.039	-.083	-.231	-.223	-.276				.110	.120	-.064	-.051	-.058					6
7	-.045	-.057	-.222	-.230	-.246					.106	-.064	-.061							7
8	-.059	-.196	-.211							-.057	-.054	-.055							8
9	.210	-.198	-.213							-.013	-.053								9
10	-.111	-.201								-.083									10
11	-.172																		11

[redacted]

Table 6 Continued

Pressure Coefficients on Delta Wing with Control

Configuration D M = 1.61 R = 4.2 x 10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
								α = 06°		δ = 05°									
1	.339	.096	.149	.014	.266	.074		-.397											1
2	-.073	-.245	-.313	-.343	-.372	-.408	-.418			.195		.230		.416	.361	.363			2
3	-.055	-.073		-.096	-.349	1.748	-.403			.121	.143	.138		.392	.287	.319			3
4	-.042	-.083	-.109	-.137	-.198	-.323	-.388			.132		.104	.163	.222	.222	.267			4
5	-.078	-.083	-.130	-.251	-.148	-.170	-.390			.098	.108	.087	-.041	.191	.190	-.002			5
6	-.063	-.035	-.098	-.240	-.220	-.273				.106	.128	.162	-.036	.024	.005				6
7	-.041	-.060	-.226	-.238	-.244					.110	.109	-.030	-.101	.011					7
8	-.064	-.214	-.226							.098	-.053	-.030							8
9	.206	-.205	-.226							-.064	-.037	-.030							9
10	-.109	-.212								-.016	-.038								10
11	-.176									-.068									11
								α = 06°		δ = 10°									
1	.336	.096	.150	.017	.288	.043		-.420											1
2	-.080	-.249	-.318	-.343	-.385	-.420	-.441			.202		.228		.556	.491	.466			2
3	-.060	-.076		-.213	-.338	1.746	-.434			.136	.147	.149		.586	.400	.432			3
4	-.052	-.084	-.102	-.133	-.210	-.369	-.417			.143		.112	.189	.342	.318	.371			4
5	-.087	-.087	-.096	-.244	-.163	-.292	-.417			.113	.111	.067	-.029	.268	.274	.079			5
6	-.064	-.031	-.135	-.231	-.221	-.307				.118	.131	.204	-.114	.057	.076				6
7	-.045	-.048	-.244	-.222	-.275					.118	.111	.004	-.154	.065					7
8	-.065	-.209	-.232							.104	-.036	.004							8
9	.194	-.240	-.227							-.058	-.007	-.013							9
10	-.110	-.233								-.004	-.007								10
11	-.158									-.067									11
								α = 06°		δ = 15°									
1	.338	.101	.157	.027	.324	-.006		-.450											1
2	-.069	-.245	-.307	-.312	-.403	-.443	-.451			.200		.226		.622	.662	.592			2
3	-.053	-.066		-.440	-.398	1.743	-.451			.130	.141	.144		.590	.553	.563			3
4	-.037	-.079	-.083	-.229	-.227	-.412	-.448			.136		.107	.174	.462	.439	.441			4
5	-.078	-.081	-.070	-.255	-.178	-.375	-.436			.109	.103	.060	-.048	.366	.392	.149			5
6	-.056	.001	-.176	-.215	-.229	-.362				.111	.126	.231	-.180	.144	.173				6
7	-.041	-.024	-.268	-.205	-.344					.111	.109	.036	-.162	.174					7
8	-.052	-.201	-.244							.095	-.012	.014							8
9	.193	-.234	-.224							-.061	.007	-.014							9
10	-.087	-.243								-.010	.012								10
11	-.139									-.051									11
								α = 06°		δ = 20°									
1	.343	.102	.152	.019	.313	-.071		-.451											1
2	-.069	-.244	-.313	-.342	-.418	-.449	-.470			.201		.231		.786	.768	.701			2
3	-.058	-.067		-.043	-.421	1.747	-.466			.124	.134	.144		.606	.696	.684			3
4	-.040	-.079	-.053	-.393	-.272	-.436	-.460			.147		.110	.142	.668	.558	.536			4
5	-.083	-.078	-.069	-.290	-.233	-.409	-.446			.109	.109	.065	-.107	.479	.502	.187			5
6	-.062	.034	-.177	-.231	-.253	-.400				.111	.129	.267	-.205	.228	.279				6
7	-.047	-.024	-.316	-.180	-.390					.111	.120	.066	-.146	.252					7
8	-.037	-.212	-.281							.096	.020	.022							8
9	.192	-.226	-.262							-.053	.039	-.006							9
10	-.076	-.244								-.001	.040								10
11	-.129									-.016									11
								α = 06°		δ = 25°									
1	.344	.108	.154	.025	.304	-.129		-.442											1
2	-.061	-.232	-.306	-.210	-.430	-.453	-.467			.195		.237		.904	.908	.815			2
3	-.050	-.060		.369	-.418	1.748	-.462			.126	.141	.148		.715	.856	.820			3
4	-.032	-.076	-.030	-.347	-.319	-.441	-.456			.131		.104	.115	.875	.730	.633			4
5	-.071	-.069	-.029	-.376	-.276	-.415	-.442			.108	.103	.066	-.178	.640	.569	.240			5
6	-.051	.087	-.194	-.232	-.251	-.410				.107	.121	.315	-.223	.331	.398				6
7	-.036	-.012	-.302	-.098	-.409					.106	.163	.074	-.112	.338					7
8	.017	-.212	-.316							.093	.052	.012							8
9	.195	-.240	-.289							-.055	.070	-.014							9
10	-.047	-.239								.032	.054								10
11	-.106									.032									11

[redacted]

Table 6 Continued

Pressure Coefficients on Delta Wing with Control

Configuration D M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 06°									δ = 30°									
1	.341	-.110	-.157	-.025	-.262	-.191		-.438		.190		.237		1.053	1.030	.923			1
2	-.066	-.239	-.302	-.144	-.449	-.460	-.472			.129	.147	.156		.874	1.018	.943			2
3	-.051	-.066		.718	-.424	1.755	-.464			.139		.105	.084	1.058	.874	.728			3
4	-.038	-.076	.054	-.291	-.384	-.450	-.449			.111	.102	.101	-.236	.791	.641	.298			4
5	-.078	-.079	.006	-.420	-.307	-.426	-.438			.109	.118	.353	-.180	.474	.523				5
6	-.053	.129	-.213	-.216	-.292	-.418				.098	.231	.079	-.107	.396					6
7	-.044	-.002	.324	-.216	-.443					.088	.089	.007							7
8	.095	-.213	-.329							-.039	.079	-.026							8
9	.195	-.232	-.270							.107	.056								9
10	-.038	-.231								.108									10
11	-.086																		11
	α = 12°									δ = 00°									
1	.214	-.092	-.011	-.178	.063	-.037		-.358		.324		.394		.393	.373	.401			1
2	-.284	-.419	-.452	-.483	-.337	-.349	-.363			.267	1.014	.278		.343	.336	.367			2
3	-.124	-.176		-.442	-.350	1.755	-.379			.272		.244	.260	.299	.283	.311			3
4	-.097	-.169	-.217	-.353	-.323	-.351	-.360			.236	.243	.244	.053	.286	.247	.057			4
5	-.155	-.179	-.168	-.390	-.276	-.322	-.358			.237	.263	.257	.052	.047	.056				5
6	-.132	-.154	-.160	-.363	-.284	-.340				.226	.241	.033	.059	.057					6
7	-.132	-.130	-.259	-.346	-.273					.237	.028	.035							7
8	-.130	-.254	-.266							.041	.040	.040							8
9	.218	-.245	-.266							.071	.040								9
10	-.183	-.255								.022									10
11	-.212																		11
	α = 12°									δ = 05°									
1	.214	-.089	-.016	-.178	.212	-.086		-.394		.333		.395		.605	.490	.492			1
2	-.286	-.422	-.460	-.473	-.392	-.390	-.399			.270	.971	.286		.518	.449	.479			2
3	-.129	-.178		-.428	-.409	1.753	-.416			.271		.246	.340	.435	.379	.384			3
4	-.099	-.175	-.182	-.282	-.378	-.394	-.402			.240	.242	.235	.099	.388	.333	.096			4
5	-.155	-.181	-.204	-.325	-.314	-.364	-.396			.241	.259	.303	.082	.158	.154				5
6	-.133	-.155	-.178	-.329	-.323	-.374				.220	.242	.071	.001	.140					6
7	-.125	-.132	-.269	-.305	-.320					.233	.052	.071							7
8	-.125	-.278	-.201							.042	.066	.071							8
9	.203	-.263	-.268							.073	.060								9
10	-.173	-.263								.032									10
11	-.214																		11
	α = 12°									δ = 10°									
1	.224	-.091	-.006	-.177	.282	-.134		-.394		.331		.396		.732	.661	.605			1
2	-.272	-.419	-.453	-.452	-.407	-.418	-.423			.268	.957	.289		.714	.580	.583			2
3	-.118	-.177		-.470	-.423	1.755	-.437			.276		.254	.379	.501	.502	.497			3
4	-.101	-.171	-.187	-.281	-.405	-.413	-.423			.236	.237	.200	.124	.418	.432	.172			4
5	-.151	-.175	-.187	-.310	-.341	-.396	-.409			.236	.258	.348	-.032	.348	.273				5
6	-.130	-.117	-.245	-.288	-.364	-.383				.224	.241	.120	-.055	.243					6
7	-.127	-.106	-.306	-.197	-.359					.227	.083	.103							7
8	-.110	-.272	-.286							.034	.096	.103							8
9	.190	-.286	-.260							.066	.101								9
10	-.137	-.302								.052									10
11	-.184																		11
	α = 12°									δ = 20°									
1	.209	-.099	-.018	-.171	.271	-.182		-.395		.334		.390		.894	.958	.836			1
2	-.285	-.424	-.454	-.295	-.437	-.439	-.046			.269	.937	.280		.883	.909	.845			2
3	-.125	-.184		-.151	-.430	1.759	-.443			.269		.250	.368	.844	.795	.692			3
4	-.107	-.178	-.070	-.240	-.431	-.436	-.431			.228	.244	.207	-.017	.695	.599	.254			4
5	-.158	-.161	-.144	-.262	-.356	-.412	-.426			.228	.263	.441	-.134	.530	.495				5
6	-.131	-.081	-.280	-.162	-.377	-.403				.215	.280	.174	-.147	.398					6
7	-.107	-.128	-.343	-.165	-.390					.229	.137	.120							7
8	-.065	-.284	-.282							.037	.155	.098							8
9	.156	-.292	-.134							.130	.138								9
10	-.126	-.309								.149									10
11	-.177																		11

[redacted]

Table 6 Continued

Pressure Coefficients on Delta Wing with Control

Configuration D M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
								α = 12°		δ = 30°									
1	.225	-.090	-.011	-.171	.052	-.258		-.395											1
2	-.276	-.417	-.380	-.224	-.437	-.438	-.451			.320		.391		1.158	1.219	1.042			2
3	-.117	-.151		.430	-.444	1.754	-.436			.275	.924	.281		1.087	1.196	1.078			3
4	-.099	-.127	-.141	-.388	-.431	-.444	-.434			.272		.250	.265	1.190	1.049	.855			4
5	-.146	-.116	-.175	-.313	-.346	-.423	-.417			.228	.236	.342	-.103	.982	.785	.558			5
6	-.117	.014	-.279	-.154	-.400	-.422				.233	.258	.478	-.177	.745	.652				6
7	-.021	-.089	-.308	-.153	-.416					.216	.393	.174	-.210	.534					7
8	.019	-.263	-.258							.227	.183	.106							8
9	.187	-.263	-.170							.118	.178	.067							9
10	-.106	-.137								.241	.149								10
11	-.189									.264									11
								α = 15°		δ = 00°									
1	.136	-.189	-.195	-.268	-.111	-.163		-.438											1
2	-.363	-.447	-.481	-.487	-.466	-.466	-.465			.426		.470		.477	.488	.513			2
3	-.162	-.245		-.414	-.460	1.756	-.462			.357	.870	.374		.479	.462	.502			3
4	-.142	-.214	-.376	-.348	-.441	-.464	-.457			.361		.377	.391	.435	.432	.438			4
5	-.179	-.218	-.358	-.381	-.352	-.439	-.451			.307	.366	.401	.148	.421	.350	.118			5
6	-.169	-.196	-.320	-.338	-.401	-.439				.352	.399	.384	.148	.160	.181				6
7	-.153	-.161	-.332	-.305	-.347					.349	.368	.129	.148	.162					7
8	-.153	-.292	-.313							.353	.124	.129							8
9	.241	-.286	-.313							.135	.130	.129							9
10	-.197	-.280								.144	.124								10
11	-.215									.122									11
								α = 15°		δ = 20°									
1	.128	-.192	-.187	-.254	.220	-.251		-.398											1
2	-.375	-.443	-.421	-.339	-.442	-.448	-.448			.428		.469		1.015	1.093	.920			2
3	-.164	-.318		-.223	-.442	1.754	-.439			.355	.364	.378		.971	1.080	.956			3
4	-.146	-.319	-.252	-.407	-.435	-.446	-.437			.364		.378	.536	.904	.957	.781			4
5	-.183	-.176	-.213	-.410	-.345	-.434	-.436			.308	.363	.442	.072	.817	.687	.354			5
6	-.171	-.101	-.329	-.395	-.408	-.434				.356	.396	.573	-.061	.642	.611				6
7	-.114	-.146	-.340	-.347	-.400					.349	.500	.260	-.094	.479					7
8	-.096	-.297	-.285							.357	.244	.214							8
9	.188	-.324	-.169							.206	.243	.200							9
10	-.153	-.305								.271	.259								10
11	-.215									.321									11
								α = -06°		δ = 10°									
1	.315	.368	.169	.164	.345	.281		.004											1
2	.185	.200	.218	.236	.098	.029	.002			-.066		-.280		.103	.000	.028			2
3	.128	.140		.110	.078	1.757	.019			-.055	-.078	-.109		-.141	-.103	-.022			3
4	.126	.102	.112	.002	.023	.032	.019			-.049		-.099	-.138	-.171	-.101	-.002			4
5	.119	.108	.112	-.076	-.023	-.003	-.091			-.086	-.074	-.059	-.260	-.105	-.059	-.151			5
6	.105	.159	.070	-.128	-.260	-.166				-.056	-.068	-.057	-.220	-.198	-.190				6
7	.132	.120	-.106	-.152	-.196					-.066	-.040	-.193	-.210	-.194					7
8	.111	-.075	-.110							-.066	-.174	-.179							8
9	.234	-.090	-.119							-.192	-.175	-.181							9
10	.002	-.090								-.113	-.183								10
11	-.072									-.143									11
								α = -06°		δ = 20°									
1	.316	.376	.179	.162	.295	.074		-.246											1
2	.195	.200	.226	.236	-.031	-.194	-.204			-.076		-.295		.402	.232	.247			2
3	.136	.142		.142	-.032	1.756	-.163			-.059	-.091	-.108		.243	.053	.176			3
4	.136	.108	.118	-.114	-.104	-.061	-.198			-.061		-.108	-.171	-.186	-.036	.123			4
5	.125	.111	.137	-.152	-.146	-.089	-.263			-.093	-.081	-.055	-.298	-.078	.056	-.046			5
6	.110	.166	.052	-.166	-.265	-.191				-.070	-.064	-.034	-.258	-.163	-.114				6
7	.133	.136	-.138	-.162	-.283					-.072	-.035	-.167	-.281	-.105					7
8	.115	-.079	-.146							-.072	-.154	-.175							8
9	.221	-.092	-.165							-.198	-.161	-.182							9
10	.004	-.101								-.102	-.161								10
11	-.057									-.117									11

[redacted]

Table 6 Continued

Pressure Coefficients on Delta Wing with Control

Configuration D M = 1.61 R = 4.2 x 10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = -06°									δ = 30°									
1	.313	.371	.177	.164	.262	-.098		-.337		-.071		-.292		.774	.488	.489			1
2	.190	.198	.223	.237	-.288	-.321	-.320			-.063	-.086	-.105		.507	.310	.423			2
3	.130	.145		.469	-.116	1.760	-.314			-.055		-.105	-.240	.049	.248	.371			3
4	.130	.113	.119	-.280	-.201	-.212	-.349			-.084	-.083	-.074	-.329	.060	.293	.123			4
5	.121	.115	.245	-.280	-.252	-.187	-.363			-.058	-.068	.027	-.356	.001	.093				5
6	.100	.167	.013	-.198	-.252	-.237				-.071	-.017	-.111	-.379	.069					6
7	.128	.167	-.163	-.180	-.364					-.075	-.109	-.149							7
8	.112	-.074	-.185							-.195	-.122	-.187							8
9	.205	-.106	-.196							-.075	-.108								9
10	.020	-.115								-.056									10
11	-.037																		11
	α = -12°									δ = 00°									
1	.169	.257	.010	-.102	.013	-.137		.377		-.250		-.447		-.216	-.265	-.261			1
2	.348	.351	.376	.385	.372	.368	.369			-.123	-.129	-.358		-.286	-.303	-.239			2
3	.258	.253		.277	.329	1.762	.352			-.118		-.189	-.307	-.270	-.279	-.159			3
4	.257	.241	.244	.245	.286	.288	.310			-.144	-.167	-.186	-.357	-.259	-.279	-.333			4
5	.236	.229	.262	.055	.233	.259	.087			-.130	-.167	-.147	-.346	-.262	-.300				5
6	.228	.297	.241	.048	-.027	.006				-.130	-.148	-.271	-.290	-.268					6
7	.250	.243	.028	.036	-.005					-.130	-.251	-.264							7
8	.231	.024	.028							-.240	-.247	-.258							8
9	.263	.033	.035							-.162	-.254								9
10	.087	.037								-.199									10
11	.029																		11
	α = -12°									δ = 10°									
1	.167	.250	.011	-.101	.409	.209		.178		-.273		-.460		.076	-.161	-.210			1
2	.346	.351	.374	.380	.236	.205	.198			-.130	-.165	-.375		-.278	-.257	-.209			2
3	.257	.250		.266	.207	1.752	.170			-.126		-.201	-.290	-.355	-.316	-.138			3
4	.257	.239	.256	.093	.131	.133	.156			-.152	-.172	-.147	-.322	-.323	-.314	-.350			4
5	.232	.230	.277	-.018	.034	.111	-.001			-.131	-.174	-.163	-.273	-.310	-.361				5
6	.224	.295	.185	-.063	-.037	-.109				-.146	-.114	-.295	-.269	-.307					6
7	.249	.247	-.025	-.073	-.155					-.140	-.242	-.281							7
8	.238	.016	-.038							-.250	-.248	-.265							8
9	.252	.007	-.038							-.146	-.267								9
10	.088	.002								-.162									10
11	.030																		11
	α = -12°									δ = 20°									
1	.178	.257	.016	-.101	.322	.086		-.096		-.271		-.447		.418	.107	.073			1
2	.352	.353	.382	.389	.136	-.112	-.003			-.117	-.166	-.358		.189	-.101	-.012			2
3	.259	.253		.325	.180	1.755	-.027			-.113		-.193	-.341	-.384	-.265	-.033			3
4	.259	.241	.250	-.024	-.071	.024	-.053			-.157	-.166	-.109	-.324	-.356	-.261	-.272			4
5	.233	.234	.278	-.110	-.153	-.015	-.096			-.127	-.166	-.129	-.308	-.326	-.335				5
6	.239	.304	.183	-.101	-.154	-.153				-.139	-.092	-.284	-.302	-.319					6
7	.254	.246	-.044	-.102	-.278					-.138	-.204	-.297							7
8	.248	.012	-.065							-.240	-.218	-.254							8
9	.241	.007	-.073							-.107	-.244								9
10	.080	-.002								-.113									10
11	.032																		11
	α = -12°									δ = 30°									
1	.174	.259	.023	-.090	.271	-.111		-.259		-.263		-.449		.760	.388	.290			1
2	.347	.356	.380	.389	-.204	-.262	-.229			-.128	-.171	-.358		.509	.106	.190			2
3	.258	.254		.506	-.045	1.757	-.240			-.122		-.191	-.352	-.152	-.145	.122			3
4	.258	.245	.259	-.165	-.177	-.054	-.271			-.152	-.165	-.137	-.399	-.333	-.129	-.123			4
5	.237	.238	.353	-.223	-.225	-.129	-.282			-.127	-.165	-.098	-.387	-.302	-.227				5
6	.236	.305	.171	-.148	-.225	-.246				-.143	-.089	-.267	-.378	-.250					6
7	.256	.272	-.066	-.131	-.355					-.134	-.167	-.282							7
8	.256	.014	-.092							-.242	-.200	-.263							8
9	.223	-.007	-.102							-.096	-.240								9
10	.097	-.012								-.096									10
11	.043																		11

[redacted]

Table 6 Concluded

Pressure Coefficients on Delta Wing with Control

Configuration D M = 1.61 R = 4.2 x 10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	$\alpha = -15^\circ$									$\delta = 00^\circ$									
1	.058	.161	-.126	-.190	-.103	-.167	.	.466											1
2	.435	.448	.460	.478	.462	.457	.471			-.371		-.471		-.148	-.225	-.247			2
3	.347	.349		.407	.445	1.755	.476			-.166	-.205	-.424		-.254	-.290	-.227			3
4	.347	.355	.403	.379	.401	.401	.430			-.167		-.391	-.341	-.320	-.317	-.165			4
5	.334	.381	.437	.152	.355	.373	.154			-.187	-.220	-.379	-.373	-.373	-.320	-.351			5
6	.374	.450	.379	.145	.046	.080				-.184	-.220	-.310	-.373	-.349	-.345				6
7	.394	.383	.132	.130	.054					-.178	-.167	-.335	-.265	-.325					7
8	.368	.130	.124							-.174	-.281	-.317							8
9	.320	.130	.135							-.273	-.281	-.308							9
10	.176	.130								-.189	-.273								10
11	.130									-.188									11

[redacted]

Table 7

Pressure Coefficients on Delta Wing with Control

Configuration E M = 1.61 R = 1.7 x 10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 00°									δ = -30°									
1	.401	.391	.330	.314		-.298	-.321			.122		.069		-.387	-.362	-.397	-.311		1
2	.094	.061	.053	.026	.835	.759	.728			.079	.023	.003		-.201	-.397	-.349			2
3	.071	.045		.316	.743		.354			.056		.064	-.323	-.242	-.397				3
4	.057	.033	.018	-.151	.703	.665	.405			.018	.059	.127	-.278	-.234	-.397				4
5	.035	.041	.088	-.247	.461	.369				.061	.074	-.043	-.183	-.351					5
6	.045	.084	.255	-.278	.252					.028	.094	-.237	-.181	-.316					6
7	.069	.161	.010	-.257						.048	-.099	-.275							7
8	.037	.000	-.035							-.053	-.125	-.237							8
9	-.100	.018	-.100							-.008	-.168								9
10	.022	.018								-.028									10
11	.022																		11
	α = 00°									δ = -25°									
1	.381	.387	.350	.297		-.262	-.318			.087		.066		-.407	-.377	-.423	-.351		1
2	.079	.043	.043	.041	.652	.642	.652			.038	.023	.008		-.183	-.423	-.387			2
3	.035	.035		.234	.563		.199			.038		.033	-.239	-.234	-.423				3
4	.047	.014	.006	-.086	.530	.514	.278			.003	.059	.036	-.239	-.211	-.423				4
5	.018	.014	.041	-.250	.339	.237				.038	.059	-.046	-.176	-.362					5
6	.029	.063	.165	-.267	.160					.008	.059	-.232	-.165	-.334					6
7	.053	.124	-.039	-.242						.031	-.109	-.244							7
8	.016	-.067	-.051							-.087	-.148	-.219							8
9	-.110	-.012	-.102							-.048	-.165								9
10	-.051	-.031								-.061									10
11	-.047																		11
	α = 00°									δ = -20°									
1	.391	.393	.326	.334		-.168	-.288			.081		.061		-.390	-.369	-.428	-.339		1
2	.081	.061	.045	.065	.494	.514	.558			.048	.025	.020		-.137	-.420	-.384			2
3	.047	.053		.193	.430		.122			.051		.020	-.186	-.222	-.420				3
4	.063	.026	.026	-.004	.387	.418	.168			-.005	.051	.023	-.186	-.158	-.379				4
5	.041	.031	.061	-.232	.242	.137				.061	.051	-.023	-.186	-.341					5
6	.041	.077	.143	-.216	.087					.025	.051	-.209	-.155	-.313					6
7	.057	.122	-.028	-.178						.031	-.122	-.209							7
8	.037	-.063	-.049							-.102	-.145	-.193							8
9	-.096	-.026	-.073							-.053	-.153								9
10	-.029	-.037								-.089									10
11	-.069																		11
	α = 00°									δ = -15°									
1	.385	.358	.310	.295		-.064	-.199			.089		.061		-.362	-.372	-.418	-.331		1
2	.069	.029	.041	.045	.359	.420	.438			.038	.025	.023		-.109	-.384	-.392			2
3	.035	.031		.143	.298		.020			.038		.008	-.109	-.191	-.387				3
4	.035	.014	-.004	.033	.222	.293	.074			-.003	.064	.008	-.150	-.109	-.313				4
5	.035	.026	.029	-.191	.181	.013				.043	.036	-.048	-.188	-.321					5
6	.012	.055	.100	-.201	.003					.028	.036	-.168	-.165	-.272					6
7	.041	.104	-.084	-.176						.031	-.135	-.191							7
8	.018	-.108	-.065							-.130	-.132	-.178							8
9	-.134	-.069	-.083							-.061	-.140								9
10	-.053	-.077								-.115									10
11	-.106																		11
	α = 00°									δ = -10°									
1	.393	.367	.307	.287		.048	-.066			.092		.048		-.216	-.341	-.405	-.334		1
2	.073	.053	.033	.033	.278	.313	.336			.046	.023	.013		-.074	-.344	-.387			2
3	.035	.033		.094	.262		-.038			.043		.013	-.046	-.171	-.288				3
4	.037	.020	-.006	.018	.140	.232	-.008			-.010	.059	.013	-.127	-.069	-.288				4
5	.026	.020	.031	-.165	.130	-.020				.038	.038	-.033	-.163	-.270					5
6	.041	.053	.067	-.158	-.041					.031	.038	-.181	-.163	-.219					6
7	.045	.092	-.086	-.158						.031	-.135	-.176							7
8	.018	-.104	-.084							-.115	-.135	-.120							8
9	-.130	-.102	-.096							-.059	-.135								9
10	-.049	-.086								-.104									10
11	-.112																		11

[redacted]

Table 7 Continued

Pressure Coefficients on Delta Wing with Control

Configuration E M = 1.61 R = 1.7 x 10^6

Orif	Upper Surface at Station									Lower Surface at Station								
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9
	α = 00°									δ = 00°								
1	.389	.365	.307	.303		.242	.181			.089		.109		-.033	-.165	-.206	-.283	
2	.077	.041	.035	.039	.148	.155	.148			.048	.023	.003		-.008	-.165	-.293		
3	.037	.033		.026	.104		-.099			.051		.008	.013	-.069	-.109			
4	.037	.016	.000	.008	.076	.120	-.076			.005	.064	.008	-.120	-.013	-.224			
5	.018	.016	.026	-.160	.059	-.074				.046	.043	.033	-.120	-.186				
6	.037	.077	.018	-.125	-.079					.028	.043	-.140	-.120	-.171				
7	.037	.102	-.138	-.145						.028	-.125	-.140						
8	.037	-.136	-.138							-.135	-.125	-.097						
9	-.114	-.124	-.128							-.056	-.125							
10	-.065	-.124								-.120								
11	-.116																	
	α = 00°									δ = 03°								
1	.389	.373	.324	.291		.303	.247			.074		.069		.028	-.031	-.048	-.237	
2	.079	.051	.039	.047	.092	.053	.048			.048	.028	.023		.028	-.031	-.232		
3	.031	.028		-.008	.048		-.171			.051		.023	.038	-.053	-.031			
4	.031	.029	-.006	-.004	.038	.059	-.115			-.008	.071	.023	-.135	.013	-.204			
5	.020	.029	.020	-.163	.038	-.130				.048	.048	.023	-.135	-.148				
6	.035	.055	.004	-.140	-.107					.028	.048	-.132	-.135	-.143				
7	.047	.096	-.143	-.140						.028	-.104	-.130						
8	.016	-.143	-.143							-.109	-.104	-.089						
9	-.126	-.141	-.143							-.048	-.104							
10	-.063	-.141								-.109								
11	-.102																	
	α = 00°									δ = 10°								
1	.377	.371	.310	.294		.215	.166			.087		.056		.240	.230	.230	-.023	
2	.069	.039	.045	.043	-.097	-.133	-.146			.056	.028	.018		.248	.166	-.056		
3	.028	.034		-.087	-.026		-.271			.051		.000	.046	.077	.128			
4	.036	.016	.008	-.038	-.041	-.051	-.220			.005	.054	.026	-.151	.089	-.074			
5	.022	.018	.024	-.166	-.020	-.179				.041	.041	.051	-.169	-.049				
6	.024	.061	-.018	-.166	-.184					.028	.046	-.082	-.159	-.038				
7	.049	.091	-.160	-.166						.026	-.107	-.092						
8	.028	-.144	-.170							-.118	-.089	-.082						
9	-.116	-.144	-.158							-.061	-.082							
10	-.067	-.152								-.107								
11	-.122																	
	α = 00°									δ = 20°								
1	.379	.373	.310	.296		.066	.003			.092		.049		.460	.460	.440	.187	
2	.073	.043	.047	.039	-.194	-.225	-.240			.056	.041	.015		.389	.389	.092		
3	.026	.034		.085	-.082		-.325			.051		.000	-.054	.271	.317			
4	.034	.018	.022	-.188	-.115	-.184	-.276			.005	.054	.033	-.197	.205	.077			
5	.024	.018	.053	-.205	-.061	-.253				.038	.043	.151	-.238	.061				
6	.026	.063	-.053	-.166	-.245					.020	.051	-.051	-.194	.097				
7	.045	.109	-.211	-.164						.026	-.084	-.072						
8	.030	-.140	-.205							-.113	-.041	-.072						
9	-.111	-.152	-.213							-.056	-.051							
10	-.057	-.172								-.077								
11	-.103																	
	α = 00°									δ = 29°								
1	.367	.355	.300	.290		-.079	-.120			.082		.054		.706	.655	.606	.437	
2	.059	.032	.038	.030	-.274	-.289	-.296			.046	.023	.010		.644	.588	.297		
3	.014	.022		.501	-.161		-.353			.043		-.005	-.156	.547	.529			
4	.024	.006	.038	-.316	-.176	-.251	-.320			-.003	.054	.033	-.251	.373	.268			
5	.008	.010	.138	-.304	-.161	-.322				.033	.038	.220	-.276	.202				
6	.016	.069	-.081	-.184	-.304					.010	.069	-.018	-.261	.240				
7	.038	.124	-.263	-.164						.023	-.031	-.064						
8	.028	-.150	-.276							-.120	-.015	-.105						
9	-.091	-.172	-.237							-.028	-.023							
10	-.036	-.190								-.008								
11	-.073																	

[redacted]

Table 7 Continued

Pressure Coefficients on Delta Wing with Control

Configuration E M = 1.61 R = 1.7 x 10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 06°									δ = -30°									
1	.328	.114	.151	.024		-.079	-.094			.222		.275		-.262	-.216	-.255	-.293		1
2	-.079	-.220	-.289	-.318	.779	.440	.560			.160	.155	.155		-.089	-.272	-.326			2
3	-.039	-.067		-.269	.481		.079			.160		.109	-.211	-.191	-.295				3
4	-.039	-.083	-.102	-.220	.053	.374	.140			.079	.178	.222	-.242	-.153	-.293				4
5	-.077	-.083	-.049	-.326	.171	.130				.150	.158	.074	-.171	-.283					5
6	-.067	-.035	.012	-.336	.043					.127	.171	-.150	-.158	-.262					6
7	-.037	.063	-.116	-.328						.137	-.053	-.160							7
8	-.071	-.126	-.136							-.008	-.059	-.160							8
9	-.191	-.126	-.181							.020	-.087								9
10	-.057	-.122								-.013									10
11	-.057																		11
	α = 06°									δ = -20°									
1	.344	.108	.179	.012		.015	-.028			.224		.255		-.186	-.247	-.295	-.298		1
2	-.073	-.206	-.301	-.348	.458	.247	.308			.135	.165	.145		-.046	-.293	-.346			2
3	-.043	-.055		-.334	.227		-.053			.153		.145	-.089	-.173	-.201				3
4	-.031	-.088	-.106	-.151	-.165	.145	-.018			.094	.188	.145	-.155	-.173	-.247				4
5	-.073	-.084	-.029	-.278	.031	-.048				.181	.145	.094	-.140	-.316					5
6	-.059	-.043	-.029	-.250	-.094					.120	.145	-.140	-.140	-.237					6
7	-.045	.053	-.187	-.250						.135	-.053	-.140							7
8	-.069	-.167	-.179							-.041	-.048	-.115							8
9	-.179	-.163	-.179							-.003	-.053								9
10	-.092	-.163								-.046									10
11	-.112																		11
	α = 06°									δ = -10°									
1	.360	.130	.171	.008		.257	.216			.227		.270		.081	-.069	-.130	-.283		1
2	-.086	-.208	-.273	-.342	.183	.074	.099			.145	.155	.173		.056	-.059	-.244			2
3	-.035	-.029		-.295	-.092		-.178			.160		.148	.018	-.046	-.046				3
4	-.020	-.083	-.108	-.126	-.181	-.008	-.115			.107	.191	.104	-.066	-.041	-.191				4
5	-.063	-.079	-.028	-.267	-.031	-.150				.160	.143	.109	-.094	-.234					5
6	-.055	-.031	-.065	-.191	-.160					.120	.143	-.094	-.099	-.196					6
7	-.020	.059	-.181	-.191						.145	-.053	-.094							7
8	-.059	-.167	-.181							-.018	-.048	-.094							8
9	-.191	-.165	-.181							.003	-.053								9
10	-.102	-.165								-.028									10
11	-.118																		11
	α = 06°									δ = 00°									
1	.330	.098	.175	.018		.201	.165			.216		.250		.227	.158	.135	-.132		1
2	-.069	-.214	-.287	-.332	-.099	-.145	-.140			.140	.145	.155		.183	.135	-.115			2
3	-.041	-.065		-.179	-.229		-.252			.140		.125	.125	.064	.089				3
4	-.033	-.077	-.108	-.124	-.171	-.135	-.222			.089	.155	.125	-.043	.104	-.104				4
5	-.084	-.077	-.096	-.234	-.089	-.214				.137	.155	.140	-.043	-.087					5
6	-.053	-.045	-.088	-.216	-.211					.120	.150	-.046	-.043	-.079					6
7	-.049	.022	-.208	-.199						.120	-.048	-.046							7
8	-.057	-.206	-.208							-.046	-.043	-.046							8
9	-.183	-.202	-.208							-.013	-.043								9
10	-.108	-.202								-.043									10
11	-.167																		11
	α = 06°									δ = 10°									
1	.336	.124	.166	.026		-.089	-.164			.210		.256		.550	.511	.465	.261		1
2	-.069	-.201	-.280	-.282	-.343	-.373	-.355			.156	.159	.156		.552	.422	.169			2
3	-.057	-.061		-.255	-.325		-.376			.161		.130	.199	.381	.348				3
4	-.036	-.075	-.091	-.120	-.210	-.340	-.345			.107	.171	.110	-.010	.338	.153				4
5	-.075	-.077	-.081	-.248	-.128	-.373				.143	.143	.225	-.095	.143					5
6	-.061	-.026	-.116	-.205	-.325					.123	.136	.003	-.120	.148					6
7	-.038	.022	-.229	-.192						.123	-.018	.005							7
8	-.051	-.207	-.223							-.046	.018	.000							8
9	-.172	-.227	-.215							-.010	.005								9
10	-.105	-.223								-.041									10
11	-.140																		11

[redacted]

Table 7 Continued

Pressure Coefficients on Delta Wing with Control

Configuration E $M = 1.61$ $R = 1.7 \times 10^6$

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	$\alpha = 06^\circ$									$\delta = 20^\circ$									
1	.338	.122	.178	.030		-.189	-.235										.455		1
2	-.069	-.205	-.278	-.290	-.348	-.373	-.353			.225		.243		.711	.708	.606			2
3	-.047	-.057		-.120	-.340		-.381			.159	.153	.159		.586	.634	.322			3
4	-.030	-.077	-.065	-.338	-.258	-.340	-.345			.148		.123	.169	.637	.550				4
5	-.083	-.079	-.063	-.297	-.136	-.366				.102	.164	.105	-.084	.519	.312				5
6	-.061	.012	-.168	-.222	-.366					.141	.143	.297	-.174	.284					6
7	-.034	.038	-.310	-.164						.123	.138	.072	-.123	.289					7
8	-.032	-.203	-.274							.110	.031	.023							8
9	-.136	-.219	-.249							-.049	.061	.010							9
10	-.079	-.239								-.005	.051								10
11	-.113									.000									11
	$\alpha = 06^\circ$									$\delta = 29^\circ$									
1	.345	.134	.184	.039		-.151	-.192										.652		1
2	-.055	-.190	-.265	-.152	-.322	-.335	-.340			.217		.253		.977	.869	.683			2
3	-.051	-.051		.569	-.256		-.363			.164	.159	.166		.759	.849	.606			3
4	-.026	-.065	.010	-.278	-.238	-.304	-.332			.161		.125	.136	.936	.693				4
5	-.067	-.063	.016	-.396	-.187	-.345				.110	.171	.141	-.182	.734	.552				5
6	-.049	.103	-.170	-.228	-.338					.146	.146	.371	-.161	.453					6
7	-.026	.059	-.304	-.128						.130	.220	.095	-.105	.473					7
8	.055	-.209	-.304							.125	.107	.013							8
9	-.061	-.229	-.257							-.031	.105	-.003							9
10	-.036	-.219								.092	.077								10
11	-.063									.107									11
	$\alpha = 12^\circ$									$\delta = -25^\circ$									
1	.246	-.059	.006	-.175		.003	.051										-.229		1
2	-.273	-.407	-.454	-.426	.586	.120	.173			.349		.379		.074	-.089	-.120			2
3	-.140	-.136		-.458	.344		-.222			.275	.290	.288		.015	-.150	-.222			3
4	-.088	-.153	-.197	-.334	-.336	-.130	-.206			.272		.252	-.069	-.094	-.023				4
5	-.155	-.153	-.092	-.344	-.242	-.252				.201	.303	.272	-.160	-.148	-.193				5
6	-.136	-.124	-.126	-.356	-.306					.242	.278	.209	-.115	-.270					6
7	-.104	.022	-.259	-.311						.242	.247	-.053	-.107	-.257					7
8	-.132	-.183	-.277							.242	.018	-.071							8
9	-.216	-.214	-.259							.053	.018	-.048							9
10	-.132	-.224								.059	.003								10
11	-.124									.059									11
	$\alpha = 12^\circ$									$\delta = -20^\circ$									
1	.216	-.083	-.006	-.198		.148	.145										-.155		1
2	-.289	-.421	-.462	-.430	.311	-.089	-.094			.341		.379		.178	.081	.036			2
3	-.128	-.140		-.466	.036		-.326			.242	.270	.288		.112	.031	-.125			3
4	-.114	-.171	-.226	-.352	-.364	-.237	-.298			.252		.270	-.013	-.008	.031				4
5	-.161	-.171	-.116	-.341	-.278	-.336				.219	.300	.262	-.115	-.051	-.130				5
6	-.138	-.120	-.157	-.316	-.334					.247	.270	.165	-.087	-.211					6
7	-.130	.014	-.295	-.316						.211	.242	-.033	-.087	-.191					7
8	-.147	-.214	-.295							.247	.028	-.051							8
9	-.240	-.226	-.295							.033	.028	-.053							9
10	-.136	-.253								.033	-.008								10
11	-.134									.033									11
	$\alpha = 12^\circ$									$\delta = -10^\circ$									
1	.236	-.069	-.002	-.175		.153	.107										-.023		1
2	-.283	-.415	-.440	-.411	.023	-.260	-.283			.339		.400		.255	.222	.199			2
3	-.114	-.138		-.434	-.372		-.356			.262	.272	.283		.216	.155	-.053			3
4	-.100	-.159	-.200	-.271	-.364	-.278	-.334			.262		.234	.089	.127	.120				4
5	-.175	-.159	-.132	-.318	-.283	-.377				.196	.300	.244	-.018	.059	-.066				5
6	-.128	-.120	-.149	-.272	-.321					.234	.267	.211	-.048	-.120					6
7	-.122	.006	-.269	-.265						.209	.247	-.025	-.048	-.122					7
8	-.114	-.240	-.269							.229	.023	-.028							8
9	-.236	-.236	-.248							.028	.023	-.028							9
10	-.141	-.253								.059	-.003								10
11	-.147									.033									11

[redacted]

Table 7 Concluded

Pressure Coefficients on Delta Wing with Control

Configuration E M = 1.61 R = 1.7×10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
								α = 12°					δ = 00°							
1	.232	-.083	-.008	-.177		-.043	-.079				.328		.392		.377	.384	.349	.097		1
2	-.271	-.393	-.415	-.417	-.293	-.321	-.316				.247	.257	.278		.341	.326	.046			2
3	-.122	-.130		-.407	-.346		-.356				.247		.257	.270	.278	.257				3
4	-.106	-.165	-.189	-.261	-.331	-.288	-.341				.206	.288	.239	.048	.288	.048				4
5	-.145	-.165	-.169	-.346	-.242	-.341					.252	.260	.252	.048	.069					5
6	-.130	-.126	-.161	-.321	-.321						.232	.244	.028	.048	.117					6
7	-.110	-.055	-.263	-.321							.237	.028	.028							7
8	-.126	-.232	-.259								.025	.048	.046							8
9	-.232	-.218	-.248								.053	.048								9
10	-.149	-.248									.048									10
11	-.181																			11
								α = 12°					δ = 03°							
1	.255	-.053	.033	-.147		.010	-.010				.359		.412		.517	.392	.349	.117		1
2	-.252	-.362	.391	-.371	-.163	-.204	-.199				.298	.290	.300		.418	.362	.046			2
3	-.081	-.112		-.387	-.244		-.298				.283		.270	.323	.306	.303				3
4	-.065	-.140	-.179	-.277	-.244	-.204	-.252				.232	.323	.255	.097	.316	.076				4
5	-.143	-.140	-.147	-.331	-.199	-.260					.280	.285	.295	.099	.071					5
6	-.096	-.034	-.147	-.318	-.255						.239	.255	.053	.066	.102					6
7	-.083	-.028	-.246	-.318							.239	.051	.053							7
8	-.096	-.218	-.246								.048	.074	.097							8
9	-.210	-.236	-.250								.069	.076								9
10	-.130	-.238									.066									10
11	-.153																			11
								α = 12°					δ = 10°							
1	.231	-.079	.002	-.160		-.228	-.258				.371		.404		.736	.624	.542	.396		1
2	-.270	-.391	-.422	-.387	-.368	-.394	-.353				.284	.289	.294		.688	.563	.271			2
3	-.120	-.138		-.432	-.373		-.373				.284		.268	.401	.478	.486				3
4	-.099	-.150	-.186	-.308	-.350	-.353	-.343				.222	.315	.228	.120	.494	.294				4
5	-.144	-.152	-.191	-.307	-.332	-.371					.253	.274	.368	.008	.284					5
6	-.130	-.081	-.237	-.210	-.363						.233	.258	.120	-.049	.276					6
7	-.105	-.038	-.282	-.217							.243	.095	.113							7
8	-.105	-.263	-.302								.051	.130	.120							8
9	-.209	-.282	-.266								.069	.120								9
10	-.136	-.290									.089									10
11	-.164																			11
								α = 12°					δ = 20°							
1	.229	-.073	-.004	-.162		-.210	-.235				.358		.389		.913	.874	.688	.678		1
2	-.278	-.397	-.381	-.294	-.350	-.386	-.358				.286	.297	.302		.867	.841	.596			2
3	-.116	-.142		-.219	-.350		-.373				.279		.263	.384	.841	.685				3
4	-.097	-.158	-.219	-.268	-.307	-.340	-.348				.220	.302	.217	.013	.759	.565				4
5	-.148	-.156	-.124	-.251	-.276	-.368					.256	.268	.460	-.107	.517					5
6	-.130	-.032	-.265	-.164	-.343						.225	.291	.174	-.118	.501					6
7	-.113	-.032	-.369	-.138							.235	.166	.133							7
8	-.051	-.253	-.298								.051	.192	.118							8
9	-.158	-.284	-.164								.120	.166								9
10	-.116	-.294									.194									10
11	-.128																			11
								α = 12°					δ = 29°							
1	.219	-.089	-.002	-.166		-.166	-.199				.355		.391		1.071	.974	.780	.683		1
2	-.278	-.385	-.369	-.282	-.366	-.381	-.368				.286	.276	.286		.979	1.000	.762			2
3	-.134	-.154		.320	-.361		-.386				.281		.266	.297	1.036	.816				3
4	-.103	-.154	-.105	-.361	-.286	-.350	-.361				.228	.302	.251	-.072	.908	.696				4
5	-.156	-.124	-.188	-.164	-.240	-.378					.251	.268	.506	-.138	.678					5
6	-.138	-.026	-.298	-.133	-.340						.230	.404	.182	-.153	.601					6
7	-.034	-.024	-.345	-.107							.245	.210	.128							7
8	.000	-.259	-.265								.102	.187	.110							8
9	-.144	-.282	-.164								.256	.169								9
10	-.122	-.184									.289									10
11	-.160																			11

[redacted]

Table 8

Pressure Coefficients on Delta Wing with Control

Configuration E M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station								Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	$\alpha = 00^\circ$									$\delta = -03^\circ$									
1	.385	.291	.291	.261	.073	.251	.219			.065	.024	.038		.000	-.034	-.063	-.261		1
2	.069	.038	.034	.033	.054	.095	.114			.035		.024		-.001	-.040	-.229			2
3	.027	.017		.030	.025		-.208			.035		-.011	-.028	-.020	-.045				3
4	.029	.005	-.016	.029	.003	.041	-.204			.002	.045	-.016	-.165	-.018	-.184				4
5	.014	.027	.009	-.143	-.149	-.165				.063	.558	.002	-.162	-.163					5
6	.016	.051	.029	-.138						.025	.016	-.148	-.157	-.118					6
7	.037	.029	-.128	-.145						.021	-.142	-.154							7
8	.021	-.130	-.128							-.129	-.140	-.146							8
9	-.126	-.125	-.134							-.096	-.145								9
10	-.077	-.125								-.131									10
11	-.126																		11
	$\alpha = 00^\circ$									$\delta = 00^\circ$									
1	.379	.285	.286	.250	.033	.296	.280			.060	.004	.029		.038	.029	.013	-.234		1
2	.057	.034	.033	.025	.015	.028	.030			.031		.019		.020	.002	-.202			2
3	.021	.013		.013	-.005		-.231			.033	.024	-.022	-.008	-.005	-.015				3
4	.023	.002	-.016	-.002	-.010	-.010	-.213			.002	1.042	-.017	-.158	-.004	-.171				4
5	.008	.015	-.001	-.152	-.160	-.198				.057	.016	.007	-.153	-.154					5
6	.006	.044	.011	-.154						.021	-.141	-.147	-.149	-.130					6
7	.031	.025	-.148	-.156						.020	-.138	-.145							7
8	.016	-.137	-.147							-.135	-.139	-.143							8
9	-.134	-.133	-.155							-.100									9
10	-.079	-.137								-.136									10
11	-.137																		11
	$\alpha = 00^\circ$									$\delta = 05^\circ$									
1	.373	.285	.285	.250	-.019	.255	.227			.057	.011	.031		.129	.151	.147	-.128		1
2	.057	.034	.029	.027	-.023	-.072	-.186			.030		.019		.095	.087	-.131			2
3	.025	.010		-.015	-.040		-.292			.029	.023	-.017	.036	.030	.064				3
4	.023	.002	-.013	-.030	-.038	-.057	-.272			-.002	.930	-.008	-.156	.028	-.130				4
5	.009	.014	-.013	-.163	-.192	-.215				.051	.012	.029	-.148	-.112					5
6	.003	.044	-.009	-.175						.018	-.136	-.129	-.152	-.098					6
7	.030	.019	-.158	-.175						.013	-.124	-.124							7
8	.016	-.150	-.162							-.138	-.126	-.129							8
9	-.128	-.154	-.162							-.106									9
10	-.087	-.154								-.135									10
11	-.141																		11
	$\alpha = 00^\circ$									$\delta = 10^\circ$									
1	.377	.288	.286	.260	-.124	.163	.107			.061	.019	.035		.234	.233	.257	-.027		1
2	.063	.035	.034	.030	-.050	-.237	-.330			.032		.021		.351	.174	-.069			2
3	.026	.014		-.079	-.092		-.358			.034	.023	-.015	.012	.080	.138				3
4	.021	.005	-.006	-.054	-.053	-.118	-.331			-.003	.871	-.006	-.176	.063	-.078				4
5	.009	.020	-.002	-.165	-.235	-.229				.054	.014	.060	-.189	-.064					5
6	.010	.050	-.025	-.196						.019	-.124	-.108	-.173	-.057					6
7	.033	.025	-.171	-.193						.015	-.109	-.104							7
8	.016	-.149	-.177							-.137	-.105	-.110							8
9	-.124	-.157	-.176							-.107									9
10	-.082	-.160								-.128									10
11	-.136																		11
	$\alpha = 00^\circ$									$\delta = 15^\circ$									
1	.372	.280	.277	.251	-.301	.054	-.021			.052	.014	.022		.318	.352	.359	.082		1
2	.057	.033	.028	.022	-.082	-.318	-.358			.022		.013		.307	.281	.004			2
3	.019	.010		-.149	-.161		-.408			.024	.017	-.025	.011	.156	.220				3
4	.020	.002	-.015	-.101	-.054	-.299	-.399			-.005	.802	-.025	-.210	.113	-.010				4
5	.007	.016	.002	-.190	-.302	-.246				.052	.007	.084	-.222	-.018					5
6	-.002	.044	-.065	-.204						.018	-.118	-.100	-.188	.020					6
7	.025	.024	-.200	-.191						.007	-.103	-.101							7
8	.006	-.158	-.205							-.143	-.101	-.109							8
9	-.128	-.173	-.200							-.111									9
10	-.085	-.184								-.120									10
11	-.134																		11

[redacted]

Table 8 Continued

Pressure Coefficients on Delta Wing with Control

Configuration E M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
								α = 00°		δ = 20°									
1	.374	.285	.278	.252		-.036	-.126										.213		1
2	.056	.029	.025	.021	-.364	-.352	-.386			.058		.030		.440	.473	.464			2
3	.020	.012		.015	-.135		-.429			.028	.020	.016		.382	.392	.095			3
4	.022	.002	-.013	-.170	-.183	-.378	-.414			.034		-.022	-.047	.292	.320				4
5	.009	.014	.031	-.200	-.057	-.322				-.002	.027	-.019	-.220	.186	.089				5
6	.000	.045	-.083	-.191	-.345					.057	.762	.119	-.276	.053					6
7	.028	.043	-.230	-.184						.019	.014	-.078	-.216	.084					7
8	.009	-.155	-.227							.010	-.091	-.086							8
9	-.155	-.174	-.227							-.134	-.073	-.101							9
10	-.074	-.187								-.100	-.073								10
11	-.120									-.092									11
								α = 00°		δ = 25°									
1	.375	.286	.279	.254		-.138	-.215										.363		1
2	.053	.031	.026	.025	-.400	-.384	-.413			.070		.037		.577	.588	.568			2
3	.020	.012		.270	-.173		-.446			.039	.035	.018		.557	.507	.197			3
4	.018	-.003	-.014	-.268	-.229	-.414	-.427			.048		-.019	-.129	.460	.435				4
5	.007	.013	.075	-.247	-.170	-.400				.010	.046	-.014	-.240	.276	.193				5
6	.000	.047	-.095	-.182	-.365					.071	.720	.153	-.282	.133					6
7	.025	.052	-.255	-.171						.032	.035	-.057	-.248	.175					7
8	.007	-.150	-.245							.019	-.059	-.067							8
9	-.110	-.176	-.252							-.120	-.050	-.105							9
10	-.065	-.193								-.076	-.048								10
11	-.110									-.045									11
								α = 00°		δ = 30°									
1	.378	.286	.281	.255		-.223	-.294										.516		1
2	.062	.036	.029	.032	-.421	-.414	-.435			.059		.035		.756	.708	.659			2
3	.022	.016		.533	-.243		-.458			.030	.020	.021		.697	.638	.324			3
4	.027	.005	-.010	-.344	-.259	-.438	-.406			.034		-.014	-.154	.629	.587				4
5	.007	.017	.142	-.308	-.281	-.431				-.003	.038	-.006	-.282	.398	.330				5
6	.005	.053	-.101	-.206	-.404					.060	.664	.167	-.298	.241					6
7	.032	.077	-.276	-.196						.017	.046	-.027	-.272	.290					7
8	.015	-.142	-.284							.000	-.047	-.060							8
9	-.074	-.181	-.274							-.130	-.027	-.109							9
10	-.038	-.197								-.055	-.023								10
11	-.080									-.006									11
								α = 03°		δ = -03°									
1	.383	.211	.237	.169		.280	.258										-.137		1
2	-.003	-.061	-.120	-.172	-.189	-.091	-.052			.121		.142		.115	.112	.086			2
3	-.018	-.029		-.048	-.050		-.318			.083	.073	.092		.072	.065	-.140			3
4	-.009	-.043	-.071	-.050	-.064	-.123	-.260			.083		.053	.021	.093	.032				4
5	-.034	-.038	-.038	-.191	-.062	-.244				.059	.104	.038	-.125	.041	-.108				5
6	-.022	.007	-.024	-.176	-.217					.102	.547	.050	-.127	-.117					6
7	-.005	-.011	-.166	-.171						.074	.065	-.115	-.120	-.100					7
8	-.016	-.163	-.164							.065	-.106	-.117							8
9	-.163	-.163	-.175							-.084	-.100	-.113							9
10	-.102	-.163								-.071	-.100								10
11	-.153									-.100									11
								α = 03°		δ = 00°									
1	.383	.203	.238	.168		.260	.237										-.155		1
2	-.004	-.063	-.121	-.170	-.144	-.154	-.167			.116		.141		.147	.137	.129			2
3	-.019	-.029		-.051	-.068		-.284			.083	.057	.087		.097	.092	-.141			3
4	-.012	-.047	-.066	-.059	-.069	-.061	-.262			.080		.053	.041	.055	.064				4
5	-.038	-.042	-.042	-.189	-.074	-.237				.062	.097	.041	-.110	.053	-.127				5
6	-.018	.007	-.036	-.181	-.195					.100	.833	.063	-.112	-.109					6
7	-.006	-.016	-.178	-.181						.071	.062	-.104	-.106	-.080					7
8	-.017	-.169	-.175							.064	-.103	-.108							8
9	-.166	-.168	-.179							-.089	-.096	-.104							9
10	-.102	-.167								-.073	-.093								10
11	-.156									-.105									11

[redacted]

Table 8 Continued

Pressure Coefficients on Delta Wing with Control

Configuration E M = 1.61 R = 4.2 x 10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
								α = 03°			δ = 05°								
1	.382	.206	.241	.173		.170	.126										-.051		1
2	-.002	-.062	-.117	-.167	-.211	-.324	-.336			.107		.134		.305	.228	.233			2
3	-.020	-.028		-.091	-.113		-.386			.072	.056	.080		.205	.181	-.079			3
4	-.013	-.042	-.066	-.091	-.110	-.119	-.377			.072		.045	.073	.117	.132				4
5	-.040	-.035	-.057	-.205	-.112	-.270				.049	.087	.038	-.104	.098	-.072				5
6	-.023	.011	-.052	-.202	-.229					.091	.760	.081	-.098	-.071					6
7	-.007	-.020	-.191	-.199						.062	.050	-.091	-.124	-.045					7
8	-.020	-.173	-.189							.055	-.102	-.090							8
9	-.161	-.176	-.185							-.100	-.087	-.089							9
10	-.102	-.178								-.086	-.085								10
11	-.158									-.113									11
								α = 03°			δ = 10°								
1	.382	.210	.235	.164		.074	.020										.051		1
2	-.006	-.064	-.123	-.172	-.281	-.349	-.367			.117		.142		.386	.345	.341			2
3	-.015	-.030		-.175	-.092		-.414			.081	.071	.087		.467	.278	-.008			3
4	-.011	-.044	-.070	-.111	-.134	-.268	-.391			.082		.052	.088	.189	.217				4
5	-.039	-.042	-.055	-.188	-.101	-.274				.059	.096	.024	-.090	.166	-.010				5
6	-.024	.009	-.081	-.205	-.249					.101	.726	.123	-.147	.012					6
7	-.005	-.014	-.209	-.194						.070	.057	-.058	-.151	.016					7
8	-.019	-.183	-.207							.058	-.079	-.059							8
9	-.162	-.197	-.201							-.088	-.063	-.066							9
10	-.102	-.197								-.078	-.058								10
11	-.158									-.100									11
								α = 03°			δ = 15°								
1	.386	.212	.243	.172		-.005	-.079										.167		1
2	-.005	-.063	-.119	-.171	-.333	-.369	-.382			.115		.141		.444	.453	.434			2
3	-.014	-.030		-.371	-.099		-.428			.081	.075	.086		.440	.379	.072			3
4	-.010	-.040	-.067	-.157	-.182	-.337	-.401			.081		.050	.065	.297	.314				4
5	-.036	-.036	-.035	-.206	-.109	-.328				.059	.098	.014	-.120	.236	.065				5
6	-.020	.011	-.105	-.208	-.289					.103	.698	.156	-.195	.075					6
7	-.002	-.001	-.234	-.198						.071	.054	-.035	-.161	.091					7
8	-.014	-.181	-.230							.058	-.063	-.042							8
9	-.148	-.200	-.216							-.086	-.040	-.055							9
10	-.085	-.206								-.078	-.039								10
11	-.140									-.091									11
								α = 03°			δ = 20°								
1	.379	.211	.238	.169		-.110	-.179										.318		1
2	-.007	-.068	-.121	-.176	-.379	-.391	-.409			.102		.131		.532	.578	.538			2
3	-.011	-.029		-.071	-.171		-.442			.069	.066	.076		.499	.491	.170			3
4	-.014	-.046	-.071	-.252	-.211	-.390	-.413			.069		.040	.028	.436	.442				4
5	-.039	-.041	-.007	-.222	-.108	-.392				.046	.090	.001	-.158	.323	.164				5
6	-.028	.013	-.137	-.220	-.322					.090	.658	.181	-.245	.147					6
7	-.007	.009	-.250	-.204						.058	.045	-.015	-.184	.182					7
8	-.018	-.178	-.270							.045	-.054	-.040							8
9	-.140	-.205	-.259							-.099	-.032	-.056							9
10	-.080	-.216								-.085	-.032								10
11	-.134									-.079									11
								α = 03°			δ = 25°								
1	.381	.209	.238	.169		-.202	-.272										.446		1
2	-.006	-.064	-.123	-.167	-.413	-.419	-.436			.114		.138		.613	.680	.628			2
3	-.015	-.027		.253	-.259		-.455			.076	.079	.085		.678	.615	.276			3
4	-.014	-.039	-.068	-.352	-.238	-.429	-.398			.078		.050	-.011	.600	.554				4
5	-.040	-.038	.039	-.229	-.179	-.440				.056	.100	.007	-.190	.434	.284				5
6	-.025	.022	-.143	-.223	-.360					.099	.628	.213	-.259	.227					6
7	-.007	.025	-.287	-.192						.067	.067	.012	-.206	.272					7
8	-.013	-.177	-.277							.051	-.024	-.024							8
9	-.117	-.207	-.285							-.088	-.003	-.052							9
10	-.063	-.220								-.063	-.001								10
11	-.110									-.028									11

[redacted]

Table 8 Continued

Pressure Coefficients on Delta Wing with Control

Configuration E M = 1.61 R = 4.2 x 10^6

Orif	Upper Surface at Station									Lower Surface at Station								Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 03°									δ = 30°									
1	.385	.209	.236	.168		-.261	-.319										.612		1
2	-.005	-.061	-.120	-.167	-.425	-.435	-.436			.118		.140		.772	.781	.688			2
3	-.016	-.026		.523	-.316		-.436			.082	.088	.089		.816	.738	.431			3
4	-.014	-.042	-.068	-.440	-.270	-.438	-.400			.081		.051	-.024	.780	.655				4
5	-.040	-.038	.088	-.306	-.253	-.435				.059	.099	.018	-.246	.570	.431				5
6	-.026	.048	-.152	-.227	-.387					.105	.593	.252	-.274	.337					6
7	-.005	.041	-.307	-.184						.072	.108	.034	-.237	.389					7
8	.001	-.175	-.288							.053	.007	-.020							8
9	.084	-.210	-.297							-.083	.028	-.063							9
10	.044	-.224								-.016	.020								10
11	-.078									.014									11
	α = 06°									δ = -03°									
1	.348	.134	.173	.039		.232	.208										-.093		1
2	-.063	-.219	-.372	-.340	-.246	-.275	-.271			.188		.239		.203	.176	.156			2
3	-.052	-.074		-.206	-.259		-.372			.142	.144	.174		.140	.123	-.100			3
4	-.040	-.077	-.107	-.124	-.166	-.194	-.336			.157		.121	.078	.108	.092				4
5	-.075	-.074	-.079	-.232	-.091	-.264				.122	.191	.106	-.055	.091	-.075				5
6	-.060	-.032	-.070	-.207	-.243					.154	.178	.107	-.081	-.086					6
7	-.041	-.041	-.195	-.201						.130	.124	-.062	-.082	-.087					7
8	-.052	-.181	-.194							.123	-.063	-.073							8
9	-.187	-.189	-.197							-.020	-.052	-.073							9
10	-.111	-.188								-.028	-.056								10
11	-.169									-.051									11
	α = 06°									δ = 00°									
1	.344	.118	.159	.025		.189	.175										-.102		1
2	-.075	-.236	-.325	-.356	-.200	-.223	-.224			.189		.241		.229	.204	.201			2
3	-.060	-.085		-.190	-.221		-.327			.144	.143	.172		.178	.158	-.104			3
4	-.051	-.088	-.115	-.149	-.122	-.144	-.299			.157		.125	.117	.117	.120				4
5	-.085	-.087	-.103	-.236	-.090	-.246				.122	.171	.114	-.047	.117	-.078				5
6	-.066	-.045	-.084	-.278	-.211					.157	.898	.130	-.053	-.057					6
7	-.048	-.057	-.216	-.220						.130	.126	-.047	-.048	-.024					7
8	-.063	-.198	-.220							.124	-.051	-.055							8
9	-.195	-.202	-.219							-.030	-.042	-.053							9
10	-.131	-.206								-.025	-.041								10
11	-.184									-.055									11
	α = 06°									δ = 05°									
1	.354	.128	.170	.037		.088	.053										.013		1
2	-.066	-.225	-.314	-.327	-.314	-.338	-.344			.183		.235		.374	.319	.310			2
3	-.050	-.076		-.126	-.276		-.384			.138	.136	.160		.330	.260	-.024			3
4	-.041	-.084	-.105	-.143	-.168	-.250	-.371			.150		.115	.162	.194	.209				4
5	-.076	-.078	-.113	-.238	-.135	-.285				.117	.167	.102	-.034	.184	-.020				5
6	-.058	-.030	-.093	-.227	-.252					.148	.845	.151	-.027	-.010					6
7	-.043	-.057	-.218	-.217						.122	.114	-.032	-.074	.020					7
8	-.056	-.197	-.218							.116	-.047	-.037							8
9	-.185	-.203	-.213							-.040	-.034	-.039							9
10	-.127	-.206								-.041	-.033								10
11	-.183									-.062									11
	α = 06°									δ = 10°									
1	.344	.123	.166	.034		-.015	-.068										.134		1
2	-.079	-.234	-.321	-.346	-.356	-.384	-.379			.181		.229		.504	.426	.405			2
3	-.061	-.081		-.200	-.330		-.409			.137	.132	.161		.487	.370	.053			3
4	-.048	-.089	-.107	-.144	-.188	-.313	-.386			.149		.108	.183	.286	.299				4
5	-.082	-.087	-.106	-.238	-.139	-.365				.113	.166	.074	-.020	.254	.063				5
6	-.066	-.029	-.122	-.229	-.279					.145	.819	.183	-.089	.070					6
7	-.045	-.051	-.241	-.216						.118	.102	-.007	-.134	.079					7
8	-.056	-.212	-.234							.109	-.042	-.015							8
9	-.184	-.233	-.221							-.039	-.020	-.025							9
10	-.121	-.225								-.048	-.017								10
11	-.181									-.066									11

[redacted]

Table 8 Continued

Pressure Coefficients on Delta Wing with Control

Configuration E $M = 1.61$ $R = 4.2 \times 10^6$

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
	$\alpha = 06^\circ$										$\delta = 15^\circ$									
1	.346	.125	.166	.033		-.106	-.157											.276		1
2	-.073	-.228	-.318	-.329	-.378	-.408	-.393				.183		.229		.605	.541	.501			2
3	-.058	-.083		-.445	-.383		-.415				.139	.133	.162		.624	.472	.138			3
4	-.050	-.087	-.100	-.193	-.220	-.355	-.386				.151		.113	.181	.402	.407				4
5	-.078	-.082	-.079	-.264	-.141	-.405					.118	.171	.071	-.050	.338	.149				5
6	-.066	-.015	-.162	-.203	-.322						.148	.794	.221	-.145	.160					6
7	-.044	-.039	-.262	-.205							.122	.106	.024	-.162	.161					7
8	-.066	-.202	-.249								.112	-.018	.008							8
9	-.166	-.236	-.229								-.034	.003	-.075							9
10	-.107	-.243									-.046	.011								10
11	-.158										-.049									11
	$\alpha = 06^\circ$										$\delta = 20^\circ$									
1	.344	.125	.166	.033		-.181	-.232											.397		1
2	-.070	-.232	-.315	-.323	-.394	-.471	-.404				.187		.234		.697	.654	.595			2
3	-.057	-.078		-.238	-.407		-.423				.140	.136	.164		.545	.600	.238			3
4	-.051	-.085	-.072	-.324	-.239	-.377	-.386				.154		.116	.158	.564	.531				4
5	-.079	-.083	-.070	-.291	-.159	-.424					.119	.175	.073	-.078	.455	.260				5
6	-.064	.011	-.175	-.221	-.354						.150	.778	.262	-.188	.250					6
7	-.048	-.034	-.305	-.196							.129	.112	.056	-.140	.264					7
8	-.043	-.206	-.282								.110	.010	.019							8
9	-.144	-.226	-.248								-.032	.032	-.005							9
10	-.091	-.245									-.038	.036								10
11	-.143										-.022									11
	$\alpha = 06^\circ$										$\delta = 25^\circ$									
1	.345	.123	.168	.031		-.243	-.290											.546		1
2	-.071	-.225	-.316	-.333	-.411	-.434	-.424				.176		.225		.836	.773	.656			2
3	-.058	-.082		.176	-.413		-.433				.135	.130	.156		.607	.723	.378			3
4	-.048	-.086	-.054	-.410	-.260	-.407	-.382				.148		.109	.132	.759	.635				4
5	-.080	-.083	-.048	-.362	-.211	-.440					.110	.170	.068	-.150	.586	.388				5
6	-.064	.043	-.170	-.263	-.389						.145	.751	.294	-.219	.330					6
7	-.042	-.020	-.320	-.203							.120	.124	.076	-.119	.358					7
8	-.009	-.213	-.327								.102	.029	.019							8
9	-.104	-.241	-.282								-.038	.059	-.014							9
10	-.075	-.237									-.021	.051								10
11	-.125										.006									11
	$\alpha = 06^\circ$										$\delta = 30^\circ$									
1	.339	.118	.163	.028		-.295	-.335											.683		1
2	-.076	-.237	-.321	-.217	-.429	-.442	-.433				.174		.225		.975	.887	.717			2
3	-.061	-.088		.524	-.425		-.424				.131	.127	.157		.739	.860	.584			3
4	-.048	-.095	-.038	-.379	-.336	-.423	-.386				.145		.105	.103	.947	.709				4
5	-.082	-.086	-.016	-.441	-.247	-.434					.109	.168	.071	-.209	.719	.572				5
6	-.070	.075	-.202	-.276	-.147						.141	.723	.329	-.235	.438					6
7	-.046	-.014	-.324	-.159							.115	.175	.082	-.120	.482					7
8	.026	-.221	-.335								.096	.064	.010							8
9	-.076	-.253	-.302								-.038	.078	-.029							9
10	-.061	-.254									.031	.058								10
11	-.107										.058									11
	$\alpha = 09^\circ$										$\delta = -30^\circ$									
1	.269	.001	.082	-.120		-.186	-.174											-.369		1
2	-.166	-.363	-.406	-.438	.755	.344	.404				.269		.307		-.338	-.295	-.312			2
3	-.102	-.119		-.477	.449		-.028				.193	.201	.224		-.104	-.338	-.379			3
4	-.088	-.134	-.151	-.253	-.118	.113	-.007				.201		.176	-.196	-.204	-.340				4
5	-.120	-.122	-.090	-.371	-.081	-.058					.172	.204	.263	-.230	-.290	-.286				5
6	-.098	-.085	-.067	-.385	-.079						.166	.191	.101	-.181	-.365					6
7	-.093	-.031	-.225	-.378							.160	.200	-.122	-.159	-.362					7
8	-.107	-.148	-.210								.170	-.037	-.150							8
9	-.216	-.175	-.225								.022	-.052	-.147							9
10	-.091	-.191									.027	-.072								10
11	-.091										.001									11

[redacted]

Table 8 Continued

Pressure Coefficients on Delta Wing with Control

Configuration E M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 09°									δ = -25°									
1	.264	-.007	.079	-.128		-.101	-.093			.264		.304		-.192	-.294	-.309	-.394		1
2	-.168	-.371	-.414	-.448	.595	.237	.287			.187	.195	.218		-.060	-.327	-.386			2
3	-.109	-.212		-.494	.335		-.099			.196		.168	-.128	-.195	-.206				3
4	-.091	-.135	-.153	-.251	-.265	.021	-.096			.171	.200	.211	-.182	-.283	-.251				4
5	-.126	-.137	-.074	-.340	-.145	-.146				.163	.188	.107	-.164	-.388					5
6	-.117	-.087	-.091	-.327	-.233					.158	.181	-.113	-.157	-.362					6
7	-.093	-.049	-.236	-.309						.164	-.041	-.130							7
8	-.110	-.176	-.218							.006	-.052	-.130							8
9	-.223	-.202	-.232							.013	-.069								9
10	-.118	-.215								-.021									10
11	-.124																		11
	α = 09°									δ = -20°									
1	.261	-.011	.076	-.136		.032	.044			.258		.302		.092	-.190	-.250	-.403		1
2	-.172	-.375	-.414	-.439	.435	.133	.175			.186	.194	.218		-.001	-.245	-.354			2
3	-.111	-.123		-.507	.183		-.171			.191		.168	-.065	-.148	-.033				3
4	.096	-.139	-.154	-.229	-.354	-.065	-.180			.164	.197	.175	-.147	-.249	-.210				4
5	.131	-.137	-.087	-.302	-.212	-.226				.158	.186	.114	-.148	-.374					5
6	-.115	-.096	-.119	-.271	-.251					.157	.170	-.101	-.143	-.256					6
7	.094	-.057	-.238	-.276						.160	-.042	-.117							7
8	.111	-.194	-.220							.003	-.049	-.115							8
9	.234	-.206	-.235							.007	-.062								9
10	-.124	-.230								-.026									10
11	-.140																		11
	α = 09°									δ = -15°									
1	.276	.000	.085	-.117		.202	.194			.274		.316		.138	.018	.003	-.225		1
2	-.159	.351	.401	-.432	.234	-.025	.007			.205	.207	.234		.085	.037	-.188			2
3	.093	-.108		-.474	-.047		-.305			.206		.180	-.001	-.015	.004				3
4	.080	-.123	-.152	-.215	-.335	-.190	-.297			.177	.213	.172	-.091	-.085	-.141				4
5	-.120	-.119	-.085	-.290	-.206	-.327				.176	.200	.131	-.105	-.233					5
6	-.101	-.081	-.127	-.218	-.240					.170	.176	-.079	-.104	-.212					6
7	-.085	-.046	-.224	-.249						.176	-.028	-.084							7
8	-.096	-.190	-.215							.015	-.033	-.087							8
9	-.214	-.206	-.223							.024	-.047								9
10	-.114	-.225								-.017									10
11	-.137																		11
	α = 09°									δ = -10°									
1	.290	.013	.103	-.099		.257	.236			.258		.301		.160	.106	.073	-.224		1
2	-.148	-.343	-.392	-.416	.115	-.093	-.081			.182	.190	.216		.127	.069	-.177			2
3	.075	-.099		-.465	-.255		-.304			.190		.165	.039	.037	.037				3
4	.067	-.116	-.124	-.197	-.369	-.202	-.279			.163	.197	.159	-.064	-.045	-.131				4
5	-.108	-.116	-.083	-.314	-.192	-.345				.156	.184	.119	-.102	-.183					5
6	-.083	-.067	-.116	-.236	-.255					.156	.163	-.077	-.102	-.200					6
7	-.067	-.043	-.213	-.255						.158	-.037	-.083							7
8	-.091	-.189	-.205							-.008	-.047	-.081							8
9	-.205	-.197	-.213							.005	-.059								9
10	-.108	-.213								-.031									10
11	-.140																		11
	α = 09°									δ = -05°									
1	.284	.010	.098	-.102	-.160	.186	.148			.270		.312		.235	.212	.200	-.087		1
2	-.153	-.349	-.388	-.417	-.366	-.339	-.339			.198	.202	.226		.174	.153	-.096			2
3	-.090	-.095		-.431	-.297	-.294	-.413			.205		.180	.103	.125	.117				3
4	-.076	-.119	-.139	-.220	-.204	-.383	-.388			.176	.207	.175	-.026	.097	-.067				4
5	-.106	-.115	-.115	-.301	-.276					.174	.198	.147	-.056	-.108					5
6	-.090	-.066	-.102	-.263						.168	.177	-.045	-.064	-.107					6
7	-.074	-.065	-.229	-.213						.173	-.028	-.054							7
8	-.085	-.202	-.218							.006	-.028	-.047							8
9	-.210	-.214	-.217							.022	-.033								9
10	-.129	-.214								-.017									10
11	-.156																		11

[redacted]

Table 8 Continued

Pressure Coefficients on Delta Wing with Control

Configuration E M = 1.61 R = 4.2 x 10^6

Orif	Upper Surface at Station									Lower Surface at Station								
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9
	α = 09°									δ = -03°								
1	.289	.037	.096	-.065		.131	.112			.241		.309		.258	.248		-.060	
2	-.145	-.346	-.391	-.425	-.257	-.341	-.352			.196	.189	.222		.184	.192	.234		
3	-.087	-.107		-.404	-.326		-.402			.202		.174	.122	.151	.141	-.080		
4	-.074	-.118	-.118	-.297	-.305	-.273	-.393			.168	.245	.163	-.022	.124	-.041			
5	-.109	-.117	-.122	-.312	-.228	-.385				.186	1.231	.145	-.054	-.071				
6	-.096	-.079	-.117	-.292	-.273					.165	.163	-.032	-.050	-.078				
7	-.074	-.077	-.234	-.221						.174	-.031	-.044						
8	-.084	-.213	-.231							.015	-.025	-.042						
9	-.214	-.216	-.228							-.003	-.023							
10	-.136	-.223								-.029								
11	-.186																	
	α = 09°									δ = 00°								
1	.279	.007	.086	-.119		.090	.036			.270		.312		.291	.296		-.005	
2	-.151	-.349	-.394	-.431	-.377	-.401	-.404			.201	.206	.226		.236	.237	.292		
3	-.090	-.107		-.416	-.318		-.421			.205		.179	.167	.193	.193	-.037		
4	-.075	-.123	-.148	-.292	-.306	-.347	-.411			.176	.212	.170	-.001	.182	-.009			
5	-.109	-.121	-.145	-.314	-.238	-.380				.173	.197	.178	-.013	-.008				
6	-.094	-.077	-.120	-.285	-.280					.173	.170	-.016	-.009	.012				
7	-.081	-.079	-.241	-.263						.167	-.020	-.024						
8	-.092	-.218	-.241							.000	-.009	-.019						
9	-.215	-.219	-.236							.020	-.012							
10	-.137	-.224								-.024								
11	-.183																	
	α = 09°									δ = 03°								
1	.277	.007	.093	-.113		.025	-.038			.275		.315		.384	.367		-.063	
2	-.145	-.344	-.396	-.423	-.355	-.375	-.372			.206	.206	.232		.305	.295	.344		
3	-.079	-.104		-.362	-.370		-.393			.213		.177	.215	.244	.247	.007		
4	-.076	-.119	-.137	-.241	-.296	-.334	-.380			.181	.215	3.167	.021	.232	.036			
5	-.102	-.119	-.137	-.274	-.225	-.388				.175	.198	.203	.019	.026				
6	-.096	-.074	-.128	-.272	-.279					.177	.174	.004	.015	.046				
7	-.074	-.004	-.243	-.258						.171	-.007	.000						
8	-.095	-.223	-.248							-.002	.002	.006						
9	-.204	-.222	-.239							.021	.002							
10	-.140	-.225								-.020								
11	-.183																	
	α = 09°									δ = 05°								
1	.276	.033	.086	-.075		-.030	-.082			.243		.311		.482	.395		.111	
2	-.152	-.346	-.391	-.408	-.414	-.435	-.434			.194	.187	.233		.395	.340	.381		
3	-.093	-.114		-.371	-.392		-.443			.207		.178	.231	.300	.284	.038		
4	-.082	-.125	-.141	-.223	-.325	-.399	-.437			.173	.258	.162	.023	.274	.066			
5	-.114	-.116	-.154	-.275	-.237	-.419				.190	.970	.208	.019	.057				
6	-.101	-.078	-.145	-.263	-.292					.162	.166	.006	-.044	.082				
7	-.083	-.092	-.249	-.261						.162	-.008	.005						
8	-.092	-.221	-.255							-.001	.008	.004						
9	-.216	-.230	-.255							-.013	.011							
10	-.155	-.234								-.022								
11	-.207																	
	α = 09°									δ = 10°								
1	.276	.033	.083	-.074		-.125	-.172			.245		.311		.644	.495		.236	
2	-.153	-.350	-.402	-.413	-.424	-.440	-.439			.198	.194	.231		.544	.445	.469		
3	-.096	-.111		-.426	-.420		-.436			.210		.177	.268	.377	.384	.116		
4	-.083	-.127	-.094	-.169	-.380	-.417	-.418			.174	.258	.139	.049	.349	.151			
5	-.116	-.118	-.149	-.262	-.253	-.435				.192	.918	.252	-.031	.149				
6	-.099	-.064	-.185	-.251	-.324					.166	.160	.039	-.088	.159				
7	-.080	-.082	-.261	-.244						.165	.007	.034						
8	-.087	-.239	-.262							.007	.030	.022						
9	-.202	-.262	-.252							-.008	.034							
10	-.136	-.271								-.012								
11	-.190																	

[redacted]

Table 8 Continued

Pressure Coefficients on Delta Wing with Control

Configuration E M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 09°									δ = 15°									
1	.282	.034	.091	-.069		-.220	-.271			.246		.313		.654	.615	.568	.358		1
2	-.148	-.344	-.389	-.399	-.430	-.455	-.432			.199	.202	.232		.728	.568	.212			2
3	-.085	-.108		-.428	-.447		-.416			.213		.183	.283	.487	.505				3
4	-.073	-.122	-.072	-.135	-.426	-.423	-.391			.176	.261	.130	.004	.450	.261				4
5	-.112	-.115	-.096	-.244	-.257	-.452				.194	.858	.292	-.100	.255					5
6	.097	-.025	-.216	-.264	-.401					.170	.162	.077	-.133	.245					6
7	.080	-.056	-.274	-.220						.164	.033	.059							7
8	-.078	-.229	-.248							.013	.058	.041							8
9	-.180	-.260	-.238							-.007	.065								9
10	-.114	-.270								.012									10
11	-.159																		11
	α = 09°									δ = 20°									
1	.276	.035	.091	-.071		-.261	-.307			.250		.318		.762	.734	.629	.492		1
2	-.147	-.345	-.395	-.393	-.432	-.455	-.395			.204	.212	.239		.734	.683	.336			2
3	-.084	-.110		-.308	-.456		-.407			.218		.183	.261	.675	.607				3
4	-.071	-.127	-.048	-.022	-.441	-.416	-.380			.178	.266	.136	-.028	.572	.372				4
5	-.106	-.117	-.127	-.250	-.251	-.425				.198	.826	.340	-.156	.344					5
6	-.097	.008	-.213	-.198	-.428					.176	.174	.115	-.164	.346					6
7	-.076	-.065	-.311	-.182						.164	.060	.067							7
8	-.053	-.220	-.248							.010	.088	.042							8
9	-.145	-.259	-.227							.005	.091								9
10	-.105	-.277								.036									10
11	-.149																		11
	α = 09°									δ = 25°									
1	.282	.037	.097	-.059		-.303	-.343			.247		.311		.893	.842	.683	.648		1
2	-.149	-.339	-.388	-.236	-.442	-.465	-.379			.197	.207	.230		.788	.807	.511			2
3	-.089	-.105		.107	-.467		-.398			.212		.177	.231	.865	.681				3
4	-.074	-.117	-.022	-.003	-.450	-.432	-.366			.172	.263	.133	-.100	.711	.513				4
5	-.113	-.111	-.078	-.223	-.277	-.389				.192	.788	.375	-.175	.435					5
6	-.095	.041	-.221	-.162	-.449					.170	.202	.128	-.187	.461					6
7	-.072	-.068	-.319	-.134						.158	.088	.068							7
8	.001	-.227	-.262							.001	.113	.031							8
9	-.109	-.246	-.170							.039	.101								9
10	-.088	-.261								.075									10
11	-.141																		11
	α = 09°									δ = 30°									
1	.288	.039	.099	-.057		-.328	-.360			.247		.312		1.012	.951	.761	.712		1
2	-.143	-.341	-.383	-.203	-.442	-.455	-.374			.198	.215	.232		.886	.945	.705			2
3	-.085	-.101		.464	-.448		-.379			.219		.181	.195	1.033	.753				3
4	-.068	-.117	.059	-.153	-.445	-.425	-.353			.173	.266	.146	-.143	.815	.680				4
5	-.109	-.096	-.142	-.192	-.324	-.389				.195	.758	.407	-.180	.561					5
6	-.093	.068	-.207	-.104	-.453					.175	.265	.132	-.192	.564					6
7	-.043	-.065	-.306	-.124						.161	.125	.059							7
8	.033	-.234	-.226							.016	.128	.023							8
9	-.087	-.261	-.224							.103	.106								9
10	-.083	-.245								.154									10
11	-.141																		11
	α = 12°									δ = -30°									
1	.194	-.118	-.035	-.223		-.172	-.106			.364		.416		-.183	-.241	-.267	-.364		1
2	-.306	-.425	-.467	-.485	.772	.263	.307			.293	.296	.308		-.055	-.287	-.353			2
3	-.132	-.189		-.490	.497		-.098			.292		.274	-.128	-.191	-.155				3
4	-.118	-.185	-.269	-.379	-.177	-.021	-.100			.246	.309	.348	-.183	-.294	-.256				4
5	-.152	-.193	-.160	-.423	-.244	-.202				.267	.291	.198	-.136	-.377					5
6	-.140	-.187	-.124	-.368	-.305					.256	.280	-.049	-.108	-.404					6
7	-.133	-.095	-.282	-.353						.274	.033	-.079							7
8	-.144	-.198	-.308							.089	.023	-.080							8
9	-.247	-.225	-.277							.074	.000								9
10	-.108	-.234								.057									10
11	-.108																		11

[redacted]

Table 8 Continued

Pressure Coefficients on Delta Wing with Control

Configuration E M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
								α = 12°		δ = -25°									
1	.196	-.118	-.037	-.221		-.043	.023										-.331		1
2	-.305	-.425	-.471	-.488	.621	.165	.191			.363		.416		.121	-.143	-.162			2
3	-.138	-.194		-.494	.407		-.184			.290	.298	.308		.000	-.203	-.286			3
4	-.109	-.184	-.268	-.378	-.368	-.110	-.191			.298		.273	-.057	-.148	-.016				4
5	-.155	-.195	-.126	-.397	-.253	-.279				.253	.310	.301	-.136	-.258	-.206				5
6	-.143	-.164	-.146	-.323	-.331					.268	.293	.204	-.110	-.378					6
7	-.131	-.087	-.282	-.319						.254	.270	-.043	-.101	-.376					7
8	-.135	-.208	-.319							.269	.034	-.064							8
9	-.243	-.227	-.285							.076	.024	-.062							9
10	-.125	-.238								.064	.005								10
11	-.127									.054									11
								α = 12°		δ = -20°									
1	.186	-.122	-.046	-.226		.099	.142										-.283		1
2	-.310	-.439	-.479	-.496	.473	.064	.075			.361		.414		.169	-.024	-.039			2
3	-.143	-.200		-.509	.212		-.257			.286	.293	.300		.087	-.075	-.224			3
4	-.115	-.191	-.283	-.366	-.434	-.181	-.261			.291		.267	-.007	-.104	-.002				4
5	-.160	-.203	-.140	-.365	-.275	-.333				.249	.303	.276	-.109	-.223	-.175				5
6	-.148	-.174	-.160	-.308	-.333					.264	.290	.206	-.098	-.361					6
7	-.137	-.073	-.292	-.303						.245	.257	-.037	-.094	-.331					7
8	-.142	-.222	-.305							.263	.030	-.053							8
9	-.256	-.238	-.300							.069	.025	-.052							9
10	-.149	-.260								.059	.007								10
11	-.149									.046									11
								α = 12°		δ = -15°									
1	.191	-.125	-.042	-.220		.249	.243										-.174		1
2	-.306	-.428	-.475	-.485	.304	-.065	-.103			.361		.414		.204	.127	.097			2
3	-.137	-.192		-.500	-.039		-.343			.288	.295	.305		.154	.098	-.154			3
4	-.120	-.186	-.277	-.347	-.422	-.257	-.318			.292		.271	.052	-.003	.050				4
5	-.156	-.195	-.160	-.331	-.289	-.378				.249	.308	.266	-.064	-.116	-.129				5
6	-.139	-.170	-.171	-.300	-.327					.269	.293	.208	-.066	-.272					6
7	-.133	-.072	-.306	-.290						.251	.255	-.026	-.071	-.238					7
8	-.139	-.229	-.293							.264	.036	-.034							8
9	-.247	-.243	-.291							.070	.027	-.035							9
10	-.152	-.262								.060	.009								10
11	-.160									.041									11
								α = 12°		δ = -10°									
1	.190	-.127	-.041	-.225		.203	.150										-.095		1
2	-.303	-.429	-.476	-.496	.145	-.212	-.331			.361		.411		.243	.212	.193			2
3	-.140	-.198		-.501	-.308		-.394			.287	.294	.300		.211	.154	-.100			3
4	-.123	-.187	-.273	-.317	-.409	-.310	-.388			.292		.276	.104	.111	.113				4
5	-.157	-.208	-.174	-.331	-.285	-.402				.248	.305	.279	-.024	-.024	-.082				5
6	-.140	-.171	-.174	-.279	-.327					.267	.292	.209	-.046	-.088					6
7	-.133	-.088	-.289	-.267						.251	.266	-.011	-.049	-.189					7
8	-.133	-.242	-.295							.265	.035	-.018							8
9	-.253	-.253	-.292							.066	.026	-.018							9
10	-.161	-.267								.070	.015								10
11	-.173									.046									11
								α = 12°		δ = -05°									
1	.199	-.107	-.037	-.228		.068	.011										.003		1
2	-.297	-.425	-.471	-.486	-.166	-.425	-.422			.360		.410		.307	.294	.277			2
3	-.129	-.190		-.483	-.423		-.431			.289	.295	.309		.246	.233	-.034			3
4	-.105	-.185	-.264	-.297	-.373	-.360	-.419			.292		.283	.167	.204	.198				4
5	-.155	-.195	-.186	-.343	-.296	-.400				.249	.301	.273	.019	.116	-.017				5
6	-.140	-.167	-.187	-.280	-.337					.267	.296	.226	-.007	-.080					6
7	-.127	-.110	-.276	-.242						.250	.258	.012	-.015	-.110					7
8	-.131	-.253	-.269							.267	.034	.004							8
9	-.245	-.242	-.273							.074	.034	.006							9
10	-.169	-.267								.068	.025								10
11	-.187									.043									11

[redacted]

Table 8 Continued

Pressure Coefficients on Delta Wing with Control

Configuration E M = 1.61 R = 4.2 x 10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
								α = 12°		δ = 00°									
1	.199	-.111	-.036	-.221		-.035	-.097										.098		1
2	-.298	-.431	-.474	-.490	-.348	-.425	-.421			.359		.411		.361	.371	.364			2
3	-.133	-.194		-.479	-.420		-.424			.286	.293	.302		.317	.324	.030			3
4	-.108	-.188	-.273	-.339	-.371	-.389	-.407			.293		.274	.243	.272	.280				4
5	-.160	-.199	-.216	-.340	-.310	-.382				.246	.302	.257	.063	.265	.058				5
6	-.138	-.171	-.167	-.321	-.348					.264	.289	.256	.044	.056					6
7	-.135	-.116	-.278	-.245						.247	.253	.039	.044	.071					7
8	-.135	-.269	-.269							.254	.041	.032							8
9	-.252	-.254	-.269							.059	.047	.042							9
10	-.177	-.263								.064	.043								10
11	-.201									.038									11
								α = 12°		δ = 03°									
1	.189	-.127	-.048	-.227		-.112	-.164										.152		1
2	-.316	-.435	-.475	-.500	-.303	-.395	-.390			.349		.406		.446	.427	.413			2
3	-.137	-.200		-.444	-.425		-.389			.279	.286	.294		.388	.385	.068			3
4	-.119	-.193	-.281	-.357	-.400	-.362	-.377			.287		.263	.292	.334	.337				4
5	-.160	-.199	-.222	-.383	-.340	-.368				.242	.301	.252	.081	.314	.099				5
6	-.146	-.172	-.179	-.377	-.366					.260	.277	.280	.076	.091					6
7	-.141	-.138	-.288	-.387						.242	.250	.053	.080	.110					7
8	-.141	-.273	-.282							.244	.044	.053							8
9	-.257	-.255	-.276							.042	.055	.061							9
10	-.178	-.265								.055	.051								10
11	-.212									.036									11
								α = 15°		δ = -30°									
1	.152	-.162	-.151	-.256		-.163	-.058										-.347		1
2	-.356	-.450	-.486	-.502	.755	-.204	.230			.412		.450		.048	-.165	-.190			2
3	-.153	-.245		-.505	.568		-.154			.347	.342	.359		-.012	-.182	-.297			3
4	-.138	-.221	-.357	-.411	-.223	-.095	-.161			.349		.336	-.050	-.177	-.055				4
5	-.182	-.235	-.261	-.424	-.336	-.264				.307	.366	.423	-.142	-.254	-.230				5
6	-.164	-.197	-.210	-.405	-.338					.314	.393	.271	-.079	-.367					6
7	-.148	-.121	-.318	-.338						.336	.349	.006	-.057	-.398					7
8	-.159	-.206	-.326							.385	.092	-.023							8
9	-.266	-.227	-.335							.135	.085	-.022							9
10	-.133	-.249								.114	.060								10
11	-.105									.107									11
								α = 15°		δ = -25°									
1	.148	-.167	-.157	-.257		.013	.123										-.292		1
2	-.360	-.453	-.491	-.502	.614	.114	.118			.413		.451		.211	-.049	-.038			2
3	-.153	-.241		-.509	.404		-.234			.342	.346	.360		.068	-.106	-.202			3
4	-.135	-.221	-.364	-.409	-.422	-.174	-.242			.346		.339	.013	-.124	.021				4
5	-.183	-.238	-.242	-.374	-.358	-.330				.305	.359	.387	-.093	-.174	-.182				5
6	-.167	-.204	-.220	-.390	-.339					.310	.394	.282	-.066	-.360					6
7	-.152	-.116	-.316	-.323						.335	.347	.016	-.052	-.346					7
8	-.161	-.217	-.329							.376	.091	-.004							8
9	-.272	-.243	-.345							.129	.090	-.008							9
10	-.145	-.257								.109	.061								10
11	-.124									.103									11
								α = 15°		δ = -20°									
1	.146	-.166	-.157	-.259		.203	.253										-.193		1
2	-.361	-.451	-.493	-.506	.460	.006	-.016			.414		.456		.223	.108	.090			2
3	-.152	-.239		-.510	.200		-.312			.344	.350	.365		.155	.099	-.161			3
4	-.134	-.217	-.364	-.400	-.457	-.238	-.293			.349		.340	.074	-.085	.064				4
5	-.182	-.237	-.241	-.368	-.351	-.373				.310	.365	.372	-.061	-.143	-.145				5
6	-.166	-.201	-.217	-.333	-.342					.313	.398	.291	-.042	-.348					6
7	-.148	-.098	-.321	-.299						.338	.350	.030	-.034	-.259					7
8	-.159	-.236	-.329							.370	.103	.015							8
9	-.267	-.250	-.331							.129	.094	.011							9
10	-.153	-.264								.115	.066								10
11	-.143									.110									11

[redacted]

Table 8 Continued

Pressure Coefficients on Delta Wing with Control

Configuration E $M = 1.61$ $R = 4.2 \times 10^6$

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	$\alpha = 15^\circ$									$\delta = -15^\circ$									
1	.151	-.161	-.151	-.252		.256	.189			.416		.457		.263	.223	.188	-.101		1
2	-.358	-.449	-.484	-.496	.327	-.106	-.163			.348	.346	.363		.225	.174	-.093			2
3	-.145	-.235		-.499	-.041		-.369			.351		.351	.125	.014	.132				3
4	-.132	-.215	-.358	-.385	-.442	-.282	-.361			.305	.365	.378	-.015	-.067	-.097				4
5	-.180	-.239	-.247	-.369	-.342	-.393				.313	.398	.291	-.015	-.286					5
6	-.161	-.197	-.224	-.327	-.338					.335	.354	.045	-.013	-.210					6
7	-.144	-.085	-.317	-.284						.366	.104	.033							7
8	-.155	-.241	-.312							.134	.092	.030							8
9	-.265	-.262	-.321							.123	.071								9
10	-.157	-.268								.117									10
11	.156																		11
	$\alpha = 15^\circ$									$\delta = -10^\circ$									
1	.144	-.170	-.160	-.263		.117	.035			.410		.448		.303	.283	.266	-.022		1
2	-.366	-.456	-.496	-.506	.144	-.284	-.404			.338	.347	.357		.294	.239	-.043			2
3	-.153	-.239		-.502	-.378		-.420			.345		.355	.181	.157	.199				3
4	-.144	-.223	-.371	-.345	-.433	-.331	-.406			.301	.360	.391	.031	.039	-.043				4
5	-.188	-.241	-.270	-.373	-.342	-.414				.307	.391	.290	.005	-.153					5
6	-.171	-.203	-.232	-.307	-.350					.332	.353	.054	.010	-.162					6
7	-.153	-.104	-.311	-.279						.366	.094	.042							7
8	-.161	-.259	-.324							.136	.088	.043							8
9	-.276	-.278	-.328							.122	.074								9
10	-.176	-.281								.105									10
11	-.184																		11
	$\alpha = 15^\circ$									$\delta = -05^\circ$									
1	.145	-.172	-.156	-.264		-.018	-.094			.408		.448		.352	.346	.342	.073		1
2	-.365	-.458	-.496	-.505	-.134	-.405	-.405			.335	.340	.365		.296	.308	.018			2
3	-.154	-.243		-.481	-.433		-.414			.340		.361	.231	.257	.266				3
4	-.141	-.219	-.369	-.355	-.408	-.355	-.400			.302	.358	.367	.063	.155	.026				4
5	-.184	-.238	-.284	-.369	-.342	-.402				.308	.392	.301	.041	-.026					5
6	-.169	-.203	-.228	-.321	-.357					.327	.338	.069	.033	-.107					6
7	-.154	-.120	-.321	-.266						.363	.091	.062							7
8	-.162	-.264	-.317							.130	.094	.062							8
9	-.275	-.274	-.313							.111	.084								9
10	-.187	-.276								.096									10
11	-.196																		11
	$\alpha = 15^\circ$									$\delta = 00^\circ$									
1	.145	-.174	-.164	-.275		-.161	-.206			.409		.448		.416	.450	.443	.216		1
2	-.377	-.456	-.499	-.503	-.334	-.375	-.358			.336	.342	.355		.390	.422	.113			2
3	-.159	-.247		-.485	-.410		-.374			.347		.337	.350	.368	.377				3
4	-.146	-.227	-.378	-.378	-.393	-.347	-.357			.304	.359	.361	.126	.368	.136				4
5	-.188	-.245	-.318	-.400	-.333	-.374				.309	.374	.351	.115	.133					5
6	-.172	-.209	-.232	-.381	-.360					.330	.346	.106	.123	.151					6
7	-.161	-.146	-.321	-.293						.342	.107	.107							7
8	-.161	-.292	-.311							.124	.113	.108							8
9	-.279	-.291	-.306							.117	.105								9
10	-.200	-.291								.113									10
11	-.220																		11
	$\alpha = 15^\circ$									$\delta = 03^\circ$									
1	.149	-.165	-.159	-.255		-.170	-.200			.405		.447		.535	.499	.481	.270		1
2	-.365	-.456	-.498	-.494	-.271	-.328	-.317			.335	.339	.358		.490	.478	.148			2
3	-.156	-.240		-.467	-.382		-.354			.346		.333	.405	.434	.431				3
4	-.140	-.227	-.369	-.387	-.365	-.310	-.333			.304	.356	.357	.156	.424	.178				4
5	-.186	-.245	-.299	-.414	-.316	-.360				.304	.364	.375	.155	.173					5
6	-.167	-.201	-.232	-.405	-.340					.326	.346	.127	.149	.190					6
7	-.153	-.153	-.312	-.322						.328	.117	.130							7
8	-.160	-.283	-.306							.116	.125	.127							8
9	-.270	-.291	-.306							.120	.115								9
10	-.195	-.291								.122									10
11	-.226																		11

[redacted]

Table 8 Continued

Pressure Coefficients on Delta Wing with Control

Configuration E M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
								$\alpha = -03^\circ$		$\delta = -03^\circ$									
1	.362	.327	.238	.246		.136	.099										-.337		1
2	.131	.127	.147	.158	.209	.215	.228			-.020		-.119		-.212	-.250	-.282			2
3	.073	.084		.093	.198		-.131			-.010	-.046	-.046		-.072	-.206	-.341			3
4	.084	.053	.059	.084	.107	.122	-.119			-.008		-.063	-.081	-.095	-.122				4
5	.061	.070	.071	-.098	.083	-.102				-.038	.030	-.066	-.209	-.082	-.242				5
6	.065	.110	.081	-.088	-.088					.034	.831	-.045	-.193	-.206					6
7	.081	.077	-.087	-.097						-.017	-.030	-.191	-.190	-.170					7
8	.065	-.094	-.093							-.023	-.175	-.186							8
9	-.097	-.084	-.092							-.163	-.170	-.177							9
10	-.052	-.081								-.115	-.178								10
11	-.102									-.157									11
								$\alpha = -03^\circ$		$\delta = 00^\circ$									
1	.350	.327	.233	.246		.193	.162										-.351		1
2	.123	.129	.144	.163	.150	.162	.164			-.019		-.124		-.164	-.216	-.244			2
3	.066	.073		.070	.111		-.156			-.013	-.048	-.051		-.074	-.108	-.296			3
4	.075	.047	.059	.052	.069	.089	-.150			-.008		-.069	-.066	-.091	-.098				4
5	.062	.064	.061	-.101	.054	-.132				-.040	.028	-.063	-.202	-.074	-.231				5
6	.064	.109	.069	-.098	-.114					.031	.792	-.037	-.194	-.198					6
7	.076	.073	-.099	-.103						-.014	-.024	-.187	-.191						7
8	.064	-.103	-.105							-.025	-.175	-.181							8
9	-.096	-.102	-.103							-.169	-.170	-.180							9
10	-.050	-.098								-.116	-.176								10
11	-.102									-.153									11
								$\alpha = -03^\circ$		$\delta = 05^\circ$									
1	.359	.326	.227	.238		.293	.265										-.274		1
2	.124	.127	.133	.149	.090	.066	.054			-.018		-.119		-.073	-.047	-.023			2
3	.070	.075		.027	.059		-.215			-.011	-.037	-.044		-.055	-.032	-.228			3
4	.079	.055	.055	.005	.022	.022	-.176			-.007		-.065	-.074	-.076	-.040				4
5	.062	.059	.048	-.121	.012	-.156				-.039	.030	-.049	-.195	-.048	-.196				5
6	.056	.106	.032	-.138	-.157					.033	.754	-.019	-.185	-.181					6
7	.082	.070	-.122	-.140						-.017	-.016	-.173	-.178	-.144					7
8	.060	-.117	-.132							-.027	-.164	-.164							8
9	-.090	-.114	-.127							-.168	-.155	-.172							9
10	-.047	-.115								-.109	-.158								10
11	-.104									-.143									11
								$\alpha = -03^\circ$		$\delta = 10^\circ$									
1	.360	.323	.223	.239		.258	.229										-.161		1
2	.128	.124	.137	.152	.040	-.028	-.114			-.020		-.126		.086	.115	.118			2
3	.069	.075		.019	.017		-.260			-.011	-.036	-.047		.033	.036	-.157			3
4	.079	.043	.047	-.034	-.023	-.022	-.242			-.006		-.067	-.088	-.055	.029				4
5	.066	.061	.040	-.119	-.033	-.192				-.046	.027	-.032	-.215	-.021	-.154				5
6	.061	.109	.012	-.156	-.208					.035	.726	-.005	-.218	-.151					6
7	.081	.070	-.140	-.160						-.020	-.010	-.159	-.207	-.110					7
8	.065	-.120	-.148							-.024	-.154	-.157							8
9	-.088	-.125	-.151							-.167	-.149	-.167							9
10	-.047	-.134								-.105	-.146								10
11	-.102									-.132									11
								$\alpha = -03^\circ$		$\delta = 15^\circ$									
1	.355	.328	.235	.247		.175	.129										-.033		1
2	.125	.129	.136	.156	-.040	-.188	-.239			-.017		-.124		.228	.222	.244			2
3	.073	.075		.031	-.020		-.329			-.011	-.032	-.048		.104	.141	-.076			3
4	.079	.054	.059	-.078	-.092	-.084	-.319			-.008		-.069	-.102	-.037	.112				4
5	.063	.061	.052	-.137	-.047	-.214				-.040	.028	-.024	-.283	.016	-.088				5
6	.061	.114	.005	-.153	-.262					.033	.696	.016	-.259	-.101					6
7	.075	.070	-.158	-.174						-.018	-.008	-.143	-.222	-.055					7
8	.061	-.119	-.165							-.018	-.142	-.137							8
9	-.077	-.127	-.160							-.168	-.133	-.155							9
10	-.047	-.139								-.103	-.134								10
11	-.102									-.116									11

[redacted]

Table 8 Continued

Pressure Coefficients on Delta Wing with Control

Configuration E M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	$\alpha = -03^\circ$									$\delta = 20^\circ$									
1	.353	.323	.229	.240		.072	.017			-.018		-.123		.393	.336	.373	.097		1
2	.122	.131	.137	.154	-.239	-.269	-.299			-.008	-.027	-.048		.240	.264	.019			2
3	.071	.079		.063	-.084		-.371			-.007		-.067	-.166	.036	.222				3
4	.080	.056	.053	-.145	-.155	-.231	-.369			-.041	.028	-.028	-.325	.071	-.003				4
5	.066	.065	.069	-.163	-.067	-.231				.033	.666	.040	-.253	-.034					5
6	.060	.117	-.004	-.168	-.314					-.021	-.004	-.124	-.228	.017					6
7	.079	.081	-.180	-.168						-.020	-.131	-.122							7
8	.064	-.120	-.174							-.167	-.115	-.144							8
9	-.075	-.134	-.187							-.103	-.117								9
10	-.039	-.147								-.100									10
11	-.100																		11
	$\alpha = -03^\circ$									$\delta = 25^\circ$									
1	.365	.328	.223	.234		-.037	-.089			-.020		-.122		.552	.459	.483	.238		1
2	.127	.128	.139	.157	-.335	-.330	-.349			-.013	-.024	-.047		.398	.368	.117			2
3	.077	.078		.219	-.117		-.412			-.007		-.068	-.248	.129	.336				3
4	.087	.052	.052	-.204	-.201	-.333	-.398			-.041	.031	-.030	-.309	.136	.095				4
5	.068	.060	.109	-.204	-.154	-.306				.033	.639	.070	-.325	.041					5
6	.061	.106	-.019	-.197	-.362					-.021	-.003	-.108	-.296	.103					6
7	.079	.093	-.191	-.175						-.027	-.109	-.121							7
8	.060	-.123	-.199							-.169	-.099	-.139							8
9	-.065	-.136	-.202							-.092	-.101								9
10	-.031	-.156								-.074									10
11	-.081																		11
	$\alpha = -03^\circ$									$\delta = 30^\circ$									
1	.359	.323	.224	.245		-.131	-.175			-.017		-.128		.715	.551	.587	.392		1
2	.132	.129	.145	.157	-.376	-.368	-.384			-.003	-.048	-.046		.489	.489	.213			2
3	.070	.075		.418	-.158		-.432			-.001		-.066	-.292	.250	.445				3
4	.077	.057	.056	-.279	-.238	-.382	-.415			-.039	.033	-.028	-.289	.218	.197				4
5	.069	.061	.167	-.241	-.220	-.362				.038	.613	.101	-.321	.126					5
6	.058	.110	-.040	-.198	-.389					-.017	.012	-.089	-.338	.196					6
7	.078	.111	-.211	-.168						-.027	-.089	-.115							7
8	.067	-.111	-.231							-.157	-.076	-.155							8
9	-.061	-.142	-.233							-.069	-.074								9
10	-.017	-.161								-.038									10
11	-.065																		11
	$\alpha = -06^\circ$									$\delta = -03^\circ$									
1	.293	.349	.183	.164		.008	-.051			-.074		-.299		-.286	-.244	-.269	-.278		1
2	.195	.204	.219	.237	.298	.285	.307			-.054	-.091	-.120		-.260	-.289	-.310			2
3	.126	.150		.156	.274		-.105			-.051		-.107	-.153	-.164	-.266				3
4	.129	.110	.118	.146	.180	.175	-.084			-.084	-.084	-.122	-.249	-.120	-.259				4
5	.120	.111	.118	-.040	.151	-.051				-.062	.867	-.090	-.233	-.201					5
6	.107	.158	.131	-.042	-.057					-.055	-.072	-.223	-.230	1.701					6
7	.134	.125	-.045	-.058						-.062	-.203	-.218							7
8	.114	-.056	-.049							-.199	-.204	-.211							8
9	-.048	-.050	-.050							-.142	-.208								9
10	-.012	-.049								-.190									10
11	-.064																		11
	$\alpha = -06^\circ$									$\delta = 00^\circ$									
1	.306	.363	.196	.171		.102	.071			-.066		-.284		-.280	-.263	-.282	-.325		1
2	.196	.206	.224	.231	.225	.229	.245			-.045	-.083	-.110		-.251	-.268	-.338			2
3	.122	.151		.127	.182		-.124			-.040		-.101	-.140	-.137	-.237				3
4	.124	.111	.120	.108	.133	.134	-.108			-.075	-.072	-.100	-.226	-.112	-.257				4
5	.115	.115	.120	-.044	.110	-.084				-.056	1.095	-.074	-.229	-.218					5
6	.099	.164	.115	-.063	-.073					-.050	-.053	-.211	-.226	1.719					6
7	.125	.128	-.056	-.071						-.054	-.191	-.204							7
8	.114	-.066	-.069							-.192	-.190	-.203							8
9	-.046	-.061	-.073							-.131	-.195								9
10	-.007	-.056								-.173									10
11	-.072																		11

[redacted]

Table 8 Continued

Pressure Coefficients on Delta Wing with Control

Configuration E M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	$\alpha = -06^\circ$									$\delta = 05^\circ$									
1	.300	.340	.177	.164		.185	.164										-.338		1
2	.191	.188	.213	.217	.163	.151	.149			-.069		-.290		-.166	-.206	-.208			2
3	.124	.141		.060	.118		-.159			-.052	-.092	-.119		-.262	-.227	-.351			3
4	.115	.093	.108	.038	.076	.083	-.152			-.048		-.110	-.128	-.154	-.194				4
5	.112	.103	.106	-.091	.060	-.128				-.080	-.081	-.090	-.238	-.092	-.245				5
6	.099	.151	.068	-.106	-.135					-.063	1.056	-.066	-.224	-.216					6
7	.120	.114	-.100	-.114						-.052	-.047	-.211	-.211	1.714					7
8	.106	-.087	-.106							-.058	-.196	-.192							8
9	-.045	-.089	-.102							-.197	-.186	-.207							9
10	-.018	-.092								-.126	-.195								10
11	-.074									-.169									11
	$\alpha = -06^\circ$									$\delta = 10^\circ$									
1	.294	.345	.183	.169		.268	.254										-.274		1
2	.187	.191	.214	.217	.108	.064	.040			-.063		-.283		.059	-.067	-.051			2
3	.115	.147		.094	.076		-.202			-.042	-.082	-.110		-.210	-.122	-.276			3
4	.120	.101	.110	-.007	.028	.032	-.180			-.040		-.106	-.160	-.197	-.104				4
5	.110	.106	.099	-.072	-.018	-.162				-.076	-.076	-.060	-.258	-.080	-.210				5
6	.094	.154	.061	-.121	-.184					-.054	1.031	-.060	-.237	-.205					6
7	.116	.114	-.113	-.132						-.049	-.033	-.193	-.226	1.716					7
8	.106	-.077	-.120							-.056	-.179	-.178							8
9	-.043	-.088	-.126							-.192	-.180	-.196							9
10	-.028	-.095								-.121	-.176								10
11	-.076									-.144									11
	$\alpha = -06^\circ$									$\delta = 15^\circ$									
1	.296	.324	.183	.150		.202	.195										-.139		1
2	.191	.196	.221	.224	.076	-.068	-.185			-.082		-.293		.232	.098	.123			2
3	.111	.146		.111	.029		-.274			-.048	-.068	-.087		-.014	-.004	-.169			3
4	.120	.106	.110	-.058	-.063	-.032	-.264			-.040		-.103	-.132	-.234	.033				4
5	.106	.113	.102	-.097	-.110	-.206				-.074	.004	-.056	-.315	-.081	-.150				5
6	.099	.159	.055	-.124	-.257					-.002	.489	-.048	-.236	-.157					6
7	.117	.120	-.119	-.140						-.052	-.028	-.180	-.243	-.142					7
8	.107	-.081	-.133							-.052	-.167	-.170							8
9	-.037	-.095	-.142							-.191	-.170	-.185							9
10	-.022	-.097								-.112	-.167								10
11	-.075									-.133									11
	$\alpha = -06^\circ$									$\delta = 20^\circ$									
1	.296	.353	.183	.157		.118	.120										-.046		1
2	.192	.200	.215	.228	-.062	-.164	-.177			-.068		-.291		.383	.175	.215			2
3	.122	.150		.118	-.036		-.298			-.049	-.089	-.155		.161	.066	-.098			3
4	.122	.106	.107	-.114	-.108	-.079	-.290			-.042		-.108	-.129	-.203	.118				4
5	.114	.111	.121	-.141	-.137	-.199				-.076	-.077	-.045	-.318	-.070	-.110				5
6	.102	.159	.041	-.153	-.278					-.057	.991	-.036	-.237	-.129					6
7	.122	.125	-.136	-.147						-.053	-.025	-.170	-.279	1.710					7
8	.109	-.088	-.149							-.054	-.156	-.164							8
9	-.032	-.093	-.163							-.195	-.159	-.178							9
10	-.022	-.109								-.114	-.159								10
11	-.059									-.111									11
	$\alpha = -06^\circ$									$\delta = 25^\circ$									
1	.300	.356	.188	.173		-.001	.004										.127		1
2	.205	.206	.235	.243	-.253	-.272	-.274			-.070		-.296		.555	.308	.363			2
3	.133	.156		.233	-.087		-.360			-.051	-.088	-.116		.279	.186	.025			3
4	.136	.116	.124	-.160	-.177	-.242	-.350			-.047		-.108	-.174	-.185	.249				4
5	.129	.122	.165	-.177	-.162	-.247				-.082	-.079	-.054	-.311	-.008	-.007				5
6	.115	.170	.041	-.175	-.333					-.059	.953	-.015	-.352	-.057					6
7	.133	.142	-.147	-.168						-.055	-.028	-.160	-.290	1.708					7
8	.123	-.081	-.157							-.057	-.143	-.158							8
9	-.012	-.090	-.156							-.193	-.149	-.170							9
10	-.006	-.101								-.104	-.145								10
11	-.042									-.090									11

[redacted]

Table 8 Continued

Pressure Coefficients on Delta Wing with Control

Configuration E M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station								
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9
	α = -06°									δ = 30°								
1	.286	.352	.178	.159		-.090	-.079			-.071		-.296		.716	.408	.499	.260	
2	.197	.206	.219	.233	-.320	-.326	-.325			-.048	-.089	-.117		.415	.291	.118		
3	.129	.149		.359	-.119		-.395			-.044		-.108	-.220	-.087	.358			
4	.135	.109	.115	-.246	-.211	-.311	-.379			-.079	-.080	-.068	-.316	.073	.095			
5	.125	.108	.210	-.231	-.193	-.307				-.059	.925	.013	-.366	.023				
6	.111	.160	.019	-.191	-.360					-.054	-.023	-.140	-.353	1.701				
7	.125	.155	-.165	-.169						-.059	-.126	-.149						
8	.117	-.084	-.188							-.192	-.133	-.186						
9	-.014	-.115	-.183							-.092	-.131							
10	.003	-.125								-.067								
11	-.038																	
	α = -09°									δ = -30°								
1	.229	.333	.095	.002		-.394	-.377			-.175		-.395		-.455	-.444	-.395	-.329	
2	.279	.296	.306	.319	1.082	1.016	.815			-.089	-.127	-.197		-.448	-.446	-.366		
3	.196	.212		.429	.948		.725			-.090		.036	-.214	-.448	-.424			
4	.206	.172	.190	.207	1.124	.783	.616			-.111	-.059	-.142	-.159	-.363	-.388			
5	.186	.185	.205	-.165	.874	.648				-.092	.035	-.217	-.131	-.449				
6	.188	.235	.400	-.182	.585					-.048	-.077	-.301	-.123	-.436				
7	.200	.311	.138	-.197						.044	-.237	-.213						
8	.177	.133	.048							-.088	-.254	-.199						
9	.002	.127	.004							-.091	-.140							
10	.148	.101								-.119								
11	.173																	
	α = -09°									δ = -25°								
1	.211	.319	.084	-.014		-.366	-.361			-.176		-.403		-.454	-.457	-.405	-.344	
2	.260	.278	.306	.300	.929	.890	.716			-.082	-.131	-.155		-.455	-.460	-.375		
3	.190	.208		.426	.831		.491			-.094		.003	-.046	-.448	-.434			
4	.199	.159	.178	.245	.950	.700	.523			-.121	-.090	-.205	-.208	-.326	-.387			
5	.168	.169	.150	-.130	.751	.507				-.094	.001	-.203	-.167	-.438				
6	.174	.212	.373	-.172	.434					-.070	-.086	-.331	-.116	-.432				
7	.181	.222	.127	-.180						-.007	-.232	-.280						
8	.157	.087	.053							-.118	-.253	-.239						
9	-.024	.103	.018							-.098	-.265							
10	.087	.089								-.125								
11	.081																	
	α = -09°									δ = -20°								
1	.219	.323	.087	-.007		-.341	-.362			-.182		-.401		-.451	-.457	-.432	-.358	
2	.274	.280	.305	.306	.816	.772	.659			-.096	-.136	-.172		-.462	-.472	-.402		
3	.193	.204		.399	.759		.327			-.096		-.035	.007	-.450	-.451			
4	.194	.166	.189	.275	.746	.636	.410			-.122	-.101	-.123	-.220	-.292	-.409			
5	.175	.173	.146	-.062	.617	.362				-.097	-.005	-.208	-.192	-.428				
6	.181	.217	.337	-.149	.335					-.096	-.080	-.304	-.156	-.428				
7	.192	.190	.127	-.180						-.036	-.225	-.261						
8	.164	.056	.072							-.129	-.268	-.149						
9	-.013	.078	.042							-.101	-.275							
10	.038	.083								-.127								
11	.034																	
	α = -09°									δ = -15°								
1	.214	.315	.069	-.012		-.290	-.344			-.180		-.407		-.447	-.453	-.446	-.371	
2	.263	.276	.292	.300	.684	.653	.603			-.090	-.131	-.174		-.448	-.465	-.420		
3	.190	.203		.369	.723		.193			-.096		-.057	-.111	-.434	-.456			
4	.194	.163	.172	.282	.553	.540	.258			-.118	-.103	-.103	-.241	-.270	-.424			
5	.167	.168	.144	-.016	.467	.252				-.098	-.039	-.229	-.285	-.402				
6	.175	.210	.288	-.112	.252					-.104	-.069	-.308	-.213	-.407				
7	.181	.166	.079	-.134						-.084	-.229	-.253						
8	.156	.024	.053							-.180	-.276	-.229						
9	-.018	.037	.028							-.115	-.286							
10	.016	.053								-.132								
11	-.003																	

[redacted]

Table 8 Continued

Pressure Coefficients on Delta Wing with Control

Configuration E M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = -09°									δ = -10°									
1	.230	.332	.091	.007		-.220	-.285										-.378		1
2	.282	.293	.311	.330	.695	.542	.528			-.176		-.400		-.428	-.434	-.437			2
3	.191	.213		.341	.607		.102			-.085	-.126	-.165		-.424	-.443	-.419			3
4	.205	.179	.194	.304	.394	.433	.154			-.088		-.079	-.156	-.399	-.441				4
5	.187	.184	.166	.032	.360	.157				-.111	-.098	-.143	-.251	-.255	-.389				5
6	.184	.229	.259	-.035	.170					-.090	-.066	-.176	-.263	-.331					6
7	.192	.176	.057	-.090						-.090	-.083	-.254	-.232	-.343					7
8	.170	.018	.057							-.088	-.232	-.253							8
9	-.009	.025	.039							-.186	-.264	-.229							9
10	.024	.033								-.127	-.251								10
11	-.010									-.159									11
	α = -09°									δ = -05°									
1	.221	.328	.084	.011		-.127	-.189										-.417		1
2	.269	.291	.312	.328	.515	.423	.429			-.178		-.401		-.410	-.417	-.436			2
3	.198	.215		.275	.428		.005			-.087	-.131	-.175		-.393	-.424	-.431			3
4	.203	.178	.190	.257	.335	.319	.042			-.092		-.130	-.213	-.362	-.421				4
5	.181	.182	.194	.046	.294	.056				-.113	-.104	-.169	-.282	-.265	-.413				5
6	.185	.231	.224	.037	.054					-.095	-.105	-.137	-.270	-.307					6
7	.191	.185	.013	-.037						-.101	-.109	-.248	-.247	-.246					7
8	.171	-.007	.019							-.096	-.233	-.248							8
9	-.012	.004	.010							-.212	-.237	-.230							9
10	.025	.006								-.154	-.239								10
11	-.020									-.187									11
	α = -09°									δ = 00°									
1	.217	.319	.075	-.012		-.047	-.093										-.424		1
2	.256	.279	.298	.309	.327	.323	.333			-.184		-.413		-.397	-.414	-.425			2
3	.186	.203		.205	.265		-.066			-.100	-.143	-.179		-.367	-.410	-.426			3
4	.192	.166	.178	.177	.218	.226	-.036			-.102		-.151	-.299	-.347	-.393				4
5	.166	.175	.183	.002	.193	-.023				-.128	-.114	-.168	-.325	-.266	-.401				5
6	.174	.221	.173	-.017	-.019					-.108	-.116	-.130	-.302	-.291					6
7	.182	.178	-.025	-.016						-.106	-.110	-.263	-.274	-.266					7
8	.158	-.023	-.025							-.106	-.232	-.250							8
9	-.017	-.024	-.031							-.229	-.235	-.243							9
10	.024	-.020								-.162	-.245								10
11	-.029									-.190									11
	α = -09°									δ = 03°									
1	.235	.339	.100	.013		.044	.023										-.361		1
2	.279	.296	.316	.330	.283	.259	.281			-.181		-.400		-.283	-.338	-.355			2
3	.207	.219		.171	.208		-.088			-.089	-.137	-.163		-.323	-.330	-.360			3
4	.207	.187	.203	.152	.154	.184	-.066			-.093		-.143	-.294	-.310	-.321				4
5	.190	.191	.198	-.012	.146	-.065				-.122	-.112	-.139	-.329	-.215	-.359				5
6	.189	.246	.168	-.037	-.064					-.097	-.104	-.122	-.286	-.282					6
7	.202	.196	-.019	-.049						-.097	-.094	-.244	-.211	-.268					7
8	.187	-.019	-.026							-.100	-.221	-.234							8
9	.013	-.020	-.029							-.214	-.221	-.226							9
10	.046	-.017								-.149	-.226								10
11	-.008									-.177									11
	α = -12°									δ = -30°									
1	.156	.247	.002	-.112		-.424	-.393										-.380		1
2	.343	.350	.377	.380	1.117	1.077	.867			-.281		-.444		-.474	-.468	-.416			2
3	.248	.261		.495	1.018		.784			-.121	-.191	-.273		-.444	-.461	-.401			3
4	.247	.230	.247	.288	1.157	.849	.654			-.119		-.088	-.387	-.463	-.451				4
5	.232	.232	.310	-.108	.951	.712				-.151	-.130	-.183	-.244	-.429	-.427				5
6	.230	.284	.455	-.146	.671					-.125	-.021	-.273	-.113	-.412					6
7	.242	.384	.168	-.165						-.068	-.105	-.340	-.116	-.410					7
8	.223	.172	.100							.021	-.266	-.273							8
9	.061	.165	.075							-.126	-.275	-.144							9
10	.225	.144								-.115	-.145								10
11	.263									-.157									11

[redacted]

Table 8 Continued

Pressure Coefficients on Delta Wing with Control

Configuration E M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	$\alpha = -12°$									$\delta = -25°$									
1	.151	.242	-.005	-.124		-.411	-.392			-.282		-.445		-.468	-.472	-.411	-.377		1
2	.336	.347	.375	.373	.979	.941	.733			-.126	-.198	-.305		-.445	-.461	-.396			2
3	.248	.256		.489	.896		.645			-.122		-.046	.388	-.468	-.442				3
4	.243	.232	.248	.336	.991	.733	.573			-.153	-.122	-.195	.259	-.434	-.423				4
5	.235	.234	.232	-.088	.801	.588				-.130	-.077	-.240	.168	-.411					5
6	.226	.284	.441	-.122	.539					-.103	-.145	-.381	.153	-.407					6
7	.236	.313	.195	-.145						-.024	-.278	-.316							7
8	.218	.148	.114							-.145	-.290	-.130							8
9	.020	.159	.066							-.134	-.290								9
10	.158	.145								-.149									10
11	.198																		11
	$\alpha = -12°$									$\delta = -20°$									
1	.160	.257	.002	-.120		-.385	-.373			-.289		-.447		-.457	-.470	-.402	-.372		1
2	.340	.352	.381	.381	.864	.831	.677			-.123	-.201	-.305		-.441	-.460	-.385			2
3	.250	.261		.493	.827		.419			-.127		-.088	-.341	-.466	-.430				3
4	.252	.240	.249	.374	.785	.670	.485			-.161	-.150	-.092	-.269	-.423	-.412				4
5	.241	.244	.214	-.019	.699	.453				-.131	-.092	-.263	-.201	-.411					5
6	.234	.284	.415	-.119	.419					-.132	-.127	-.356	-.205	-.400					6
7	.247	.269	.170	-.142						-.077	-.277	-.292							7
8	.229	.241	.122							-.172	-.297	-.131							8
9	.016	.129	.091							-.127	-.305								9
10	.106	.147								-.140									10
11	.133																		11
	$\alpha = -12°$									$\delta = -15°$									
1	.157	.243	.003	-.109		-.344	-.357			-.281		-.448		-.450	-.466	-.399	-.356		1
2	.338	.350	.388	.379	.809	.721	.632			-.116	-.182	-.372		-.442	-.456	-.366			2
3	.246	.266		.447	.766		.277			-.113		-.140	-.353	-.455	-.427				3
4	.254	.243	.256	.390	.604	.608	.373			-.156	-.142	-.147	-.322	-.403	-.401				4
5	.244	.239	.228	.037	.555	.330				-.115	-.091	-.261	-.240	-.400					5
6	.242	.286	.371	-.070	.328					-.133	-.113	-.328	-.222	-.391					6
7	.247	.244	.153	-.102						-.091	-.267	-.270							7
8	.233	.091	.114							-.184	-.288	-.213							8
9	.028	.111	.107							-.127	-.312								9
10	.077	.122								-.143									10
11	.077																		11
	$\alpha = -12°$									$\delta = -10°$									
1	.157	.243	.002	-.118		-.302	-.335			-.277		-.454		-.450	-.469	-.403	-.352		1
2	.328	.343	.378	.368	.739	.594	.562			-.123	-.196	-.382		-.445	-.468	-.374			2
3	.239	.260		.411	.669		.155			-.119		-.179	-.325	-.448	-.433				3
4	.250	.229	.243	.371	.454	.505	.216			-.148	-.141	-.198	-.319	-.382	-.391				4
5	.236	.232	.225	.100	.463	.216				-.126	-.114	-.227	-.270	-.414					5
6	.231	.284	.314	.000	.222					-.142	-.116	-.303	-.198	-.380					6
7	.253	.237	.100	-.052						-.116	-.276	-.308							7
8	.227	.062	.096							-.216	-.293	-.253							8
9	.034	.073	.088							-.143	-.308								9
10	.068	.080								-.170									10
11	.054																		11
	$\alpha = -12°$									$\delta = -05°$									
1	.156	.245	-.002	-.118		-.222	-.288			-.274		-.453		-.436	-.464	-.434	-.379		1
2	.332	.358	.380	.384	.604	.478	.484			-.121	-.191	-.379		-.434	-.462	-.403			2
3	.245	.262		.339	.498		.060			-.122		-.191	-.319	-.427	-.450				3
4	.252	.238	.244	.318	.428	.394	.107			-.159	-.140	-.203	-.335	-.351	-.402				4
5	.243	.238	.247	.094	.377	.113				-.122	-.165	-.174	-.323	-.383					5
6	.234	.286	.275	.095	.114					-.137	-.144	-.284	-.303	-.337					6
7	.245	.235	.065	-.013						-.127	-.267	-.290							7
8	.225	.037	.062							-.236	-.254	-.273							8
9	.031	.053	.065							-.167	-.257								9
10	.073	.056								-.197									10
11	.033																		11

Table 8 Continued

Pressure Coefficients on Delta Wing with Control

Configuration E M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = -12°									δ = 00°									
1	.163	.252	.004	-.113		-.145	-.203										-.415		1
2	.337	.351	.378	.384	.396	.389	.402			-.274		-.449		-.420	-.450	-.449			2
3	.248	.259		.274	.341		-.011			-.119	-.191	-.371		-.415	-.451	-.427			3
4	.256	.243	.247	.254	.295	.297	.033			-.113		-.214	-.324	-.401	-.432				4
5	.235	.237	.262	.057	.269	.036				-.147	-.143	-.183	-.354	-.321	-.417				5
6	.234	.288	.239	.055	.037					-.119	-.163	-.145	-.361	-.341					6
7	.245	.242	.033	.049						-.131	-.129	-.271	-.311	-.300					7
8	.224	.025	.037							-.127	-.263	-.270							8
9	.038	.032	.038							-.246	-.245	-.258							9
10	.074	.037								-.156	-.244								10
11	.022									-.184									11
	α = -12°									δ = 03°									
1	.158	.256	.011	-.111		-.104	-.176										-.396		1
2	.338	.359	.381	.388	.348	.347	.346			-.277		-.444		-.397	-.457	-.434			2
3	.253	.267		.238	.285		-.031			-.123	-.193	-.378		-.407	-.447	-.414			3
4	.248	.243	.265	.201	.245	.254	.003			-.118		-.212	-.313	-.407	-.421				4
5	.236	.243	.254	.036	.213	-.002				-.154	-.140	-.152	-.348	-.302	-.424				5
6	.236	.302	.224	.018	.005					-.122	-.158	-.156	-.320	-.354					6
7	.246	.243	.019	.018						-.133	-.111	-.272	-.253	-.329					7
8	.246	.018	.010							-.119	-.251	-.264							8
9	.054	.023	.019							-.237	-.245	-.254							9
10	.078	.025								-.150	-.252								10
11	.033									-.177									11
	α = -15°									δ = -30°									
1	.082	.184	-.097	-.177		-.445	-.376										-.369		1
2	.408	.414	.436	.436	1.171	1.138	.936			-.366		-.321		-.444	-.456	-.420			2
3	.327	.336		.646	1.078		.872			-.160	-.373	-.273		-.448	-.447	-.401			3
4	.323	.309	.352	.467	1.206	.972	.710			-.159		-.237	-.420	-.460	-.436				4
5	.308	.340	.551	-.050	1.048	.806				-.180	-.072	-.252	-.392	-.447	-.426				5
6	.327	.399	.566	-.094	.798					-.127	-.073	-.349	-.337	-.444					6
7	.350	.520	.248	-.113						-.053	-.129	-.325	-.261	-.424					7
8	.359	.239	.186							-.058	-.279	-.269							8
9	.293	.261	.171							-.195	-.290	-.214							9
10	.346	.319								-.163	-.094								10
11	.352									-.216									11
	α = -15°									δ = -25°									
1	.062	.166	-.114	-.196			-.375										-.371		1
2	.398	.411	.422	.410	1.063	1.039	.831			-.369		-.379		-.442	-.457	-.421			2
3	.314	.318		.623	.991		.755			-.155	-.343	-.301		-.447	-.448	-.401			3
4	.309	.295	.338	.489	1.031	.823	.633			-.157		-.303	-.421	-.457	-.437				4
5	.282	.323	.435	-.019	.872	.698				-.177	-.104	-.280	-.414	-.447	-.421				5
6	.310	.382	.540	-.073	.684					-.154	-.123	-.320	-.387	-.441					6
7	.344	.480	.237	-.103						-.127	-.140	-.352	-.301	-.419					7
8	.323	.216	.172							-.057	-.299	-.261							8
9	.163	.215	.137							-.186	-.311	-.174							9
10	.297	.216								-.146	-.130								10
11	.304									-.194									11
	α = -15°									δ = -20°									
1	.073	.184	-.096	-.183		-.428	-.385										-.363		1
2	.404	.427	.439	.448	.972	.931	.704			-.376		-.432		-.438	-.457	-.407			2
3	.328	.336		.635	.904		.622			-.167	-.341	-.400		-.445	-.446	-.391			3
4	.319	.313	.357	.531	.841	.718	.555			-.169		-.165	-.428	-.455	-.433				4
5	.303	.339	.395	.053	.761	.576				-.190	-.097	-.189	-.392	-.433	-.413				5
6	.319	.404	.542	-.074	.527					-.161	-.090	-.325	-.366	-.410					6
7	.358	.460	.240	-.095						-.151	-.136	-.391	-.320	-.405					7
8	.326	.204	.196							-.084	-.301	-.316							8
9	.126	.216	.172							-.186	-.326	-.155							9
10	.248	.207								-.141	-.254								10
11	.285									-.179									11

[redacted]

Table 8 Concluded

Pressure Coefficients on Delta Wing with Control

Configuration E M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	$\alpha = -15^\circ$									$\delta = -15^\circ$									
1	.074	.190	-.095	-.184		-.392	-.375										-.345		1
2	.407	.425	.434	.440	.889	.810	.660			-.361		-.420		-.428	-.450	-.400			2
3	.325	.333		.573	.842		.433			-.147	-.339	-.406		-.438	-.437	-.378			3
4	.319	.311	.356	.533	.651	.666	.479			-.155		-.222	-.411	-.438	-.419				4
5	.307	.337	.374	.185	.675	.441				-.174	-.096	-.211	-.371	-.414	-.394				5
6	.323	.408	.500	-.018	.411					-.154	-.067	-.366	-.343	-.390					6
7	.359	.407	.218	-.054						-.161	-.142	-.408	-.338	-.381					7
8	.325	.178	.176							-.106	-.285	-.333							8
9	.101	.180	.178							-.196	-.310	-.263							9
10	.194	.180								-.152	-.252								10
11	.223									-.167									11
	$\alpha = -15^\circ$									$\delta = -10^\circ$									
1	.074	.184	-.096	-.185		-.362	-.373										-.349		1
2	.399	.419	.434	.434	.800	.688	.605			-.362		-.438		-.436	-.460	-.407			2
3	.317	.323		.532	.750		.258			-.152	-.335	-.419		-.445	-.441	-.379			3
4	.313	.316	.353	.522	.549	.594	.358			-.156		-.378	-.363	-.431	-.421				4
5	.303	.336	.377	.215	.587	.306				-.176	-.098	-.400	-.390	-.400	-.394				5
6	.318	.399	.444	.066	.315					-.152	-.121	-.390	-.309	-.381					6
7	.358	.378	.182	-.007						-.159	-.143	-.366	-.321	-.365					7
8	.322	.144	.165							-.144	-.292	-.327							8
9	.108	.151	.172							-.238	-.313	-.316							9
10	.169	.156								-.172	-.205								10
11	.158									-.189									11
	$\alpha = -15^\circ$									$\delta = -05^\circ$									
1	.075	.176	-.099	-.183		-.324	-.364										-.358		1
2	.408	.420	.432	.435	.715	.582	.542			-.366		-.438		-.442	-.467	-.426			2
3	.323	.332		.448	.634		.154			-.150	-.335	-.407		-.447	-.453	-.385			3
4	.316	.308	.353	.439	.566	.493	.218			-.156		-.390	-.354	-.417	-.428				4
5	.301	.338	.390	.178	.500	.202				-.176	-.100	-.399	-.394	-.379	-.405				5
6	.327	.402	.397	.190	.196					-.152	-.155	-.362	-.385	-.375					6
7	.364	.357	.145	.086						-.160	-.147	-.352	-.294	-.328					7
8	.325	.123	.150							-.149	-.271	-.302							8
9	.109	.129	.144							-.265	-.276	-.295							9
10	.149	.133								-.185	-.250								10
11	.121									-.193									11
	$\alpha = -15^\circ$									$\delta = 00^\circ$									
1	.064	.172	-.108	-.194		-.249	-.313										-.408		1
2	.391	.410	.424	.424	.459	.473	.473			-.365		-.439		-.433	-.467	-.450			2
3	.310	.319		.364	.432		.065			-.154	-.334	-.406		-.425	-.468	-.431			3
4	.311	.306	.352	.348	.389	.393	.110			-.154		-.389	-.339	-.394	-.459				4
5	.294	.326	.382	.137	.377	.106				-.179	-.102	-.376	-.361	-.324	-.433				5
6	.318	.396	.345	.122	.110					-.156	-.154	-.358	-.353	-.370					6
7	.349	.339	.097	.119						-.169	-.132	-.367	-.269	-.301					7
8	.328	.089	.097							-.156	-.251	-.305							8
9	.099	.095	.096							-.271	-.259	-.294							9
10	.139	.096								-.182	-.258								10
11	.089									-.186									11
	$\alpha = -15^\circ$									$\delta = 03^\circ$									
1	.075	.178	-.097	-.185		-.360	-.302										-.409		1
2	.399	.422	.428	.435	.371	.424	.427			-.366		-.441		-.417	-.472	-.443			2
3	.331	.330		.316	.336		.028			-.151	-.337	-.408		-.401	-.470	-.421			3
4	.322	.306	.392	.296	.297	.347	.068			-.155		-.392	-.330	-.405	-.450				4
5	.310	.337	.381	.112	.053	.060				-.176	-.105	-.382	-.339	-.340	-.425				5
6	.328	.422	.319	.084	1.765					-.157	-.157	-.347	-.272	-.373					6
7	.359	.342	.083	.074						-.167	-.138	-.367	1.777	-.311					7
8	.345	.090	.079							-.158	-.253	-.307							8
9	.109	.093	.074							-.272	-.248	-.290							9
10	.140	.092								-.185	-.258								10
11	.085									-.182									11

[redacted]

Table 9

Pressure Coefficients on Delta Wing with Control

Configuration E M = 1.61 R = 7.6×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 00°									δ = -20°									
1	.382	.355	.273	.271		-.118	-.233			.070		.051		-.375	-.354	-.393	-.408		1
2	.048	.030	.017	.011	.413	.470	.476			.031	.010	.001		-.127	-.385	-.428			2
3	.011	.021		.147	.370		.042			.029		-.013	-.175	-.181	-.418				3
4	.020	-.003	-.019	-.017	.280	.317	.070			.002	.047	.018	-.200	-.041	-.299				4
5	.006	.000	-.013	-.235	.185	.045				.013	.020	-.071	-.197	-.340					5
6	.005	.040	.101	-.248	.024					.028	.035	-.227	-.186	-.315					6
7	.024	.006	-.077	-.211						.010	-.152	-.214							7
8	-.001	-.096	-.087							-.127	-.168	-.213							8
9	-.141	-.087	-.112							-.070	-.183								9
10	-.067	-.087								-.126									10
11	-.127																		11
	α = 00°									δ = -10°									
1	.390	.363	.277	.270		.105	.019			.071		.048		-.073	-.291	-.336	-.389		1
2	.057	.040	.023	.016	.204	.247	.273			.032	.010	.001		-.059	-.135	-.378			2
3	.018	.022		.072	.248		-.109			.029		-.014	-.070	-.089	-.124				3
4	.024	.002	-.015	.035	.080	.135	-.101			.001	.049	-.018	-.163	-.054	-.224				4
5	.014	.002	.007	-.160	.058	-.105				.015	.020	-.030	-.200	-.241					5
6	.003	.047	.048	-.183	-.089					.030	.020	-.176	-.183	-.213					6
7	.026	.011	-.117	-.171						.011	-.155	-.175							7
8	.004	-.124	-.112							-.134	-.160	-.171							8
9	-.134	-.122	-.121							-.080	-.163								9
10	-.071	-.118								-.142									10
11	-.138																		11
	α = 00°									δ = -04°									
1	.392	.361	.282	.284		.234	.163			.076		.048		-.018	-.086	-.100	-.387		1
2	.058	.038	.026	.024	.109	.141	.162			.033	.013	.001		-.017	-.072	-.279			2
3	.018	.027		.031	.092		-.172			.034		-.013	-.042	-.050	-.065				3
4	.026	.004	-.010	.021	.036	.059	-.166			.007	.059	-.022	-.173	-.045	-.207				4
5	.016	.004	.013	-.145	.020	-.157				.021	.022	-.009	-.167	-.186					5
6	.002	.049	.027	-.132	-.137					.029	.018	-.158	-.160	-.160					6
7	.025	.022	-.128	-.150						.013	-.147	-.158							7
8	.010	-.132	-.127							-.131	-.147	-.153							8
9	-.134	-.131	-.134							-.074	-.151								9
10	-.072	-.128								-.143									10
11	-.145																		11
	α = 00°									δ = 00°									
1	.395	.362	.282	.285		.303	.262			.079		.050		.030	.008	-.008	-.285		1
2	.058	.037	.027	.026	.044	.045	.059			.037	.013	.004		.018	-.012	-.225			2
3	.020	.026		.018	.026		-.217			.037		-.011	-.016	-.015	-.017				3
4	.027	.003	-.007	-.005	.003	.011	-.210			.007	.060	-.013	-.151	-.013	-.189				4
5	.018	.004	.001	-.150	-.008	-.188				.022	.022	.007	-.147	-.155					5
6	-.001	.048	.011	-.141	-.156					.029	.021	-.144	-.144	-.137					6
7	.025	.020	-.142	-.143						.013	-.137	-.143							7
8	.011	-.134	-.143							-.134	-.136	-.143							8
9	-.130	-.140	-.147							-.072	-.138								9
10	-.069	-.141								-.139									10
11	-.144																		11
	α = 00°									δ = 10°									
1	.398	.367	.282	.288		.212	.130			.080		.051		.231	.227	.244	-.057		1
2	.065	.044	.029	.033	-.065	-.213	-.316			.041	.015	.008		.305	.163	-.077			2
3	.023	.031		-.058	-.038		-.371			.041		-.011	.026	.076	.125				3
4	.029	.010	-.005	-.047	-.069	-.099	-.282			.009	.061	.001	-.148	.060	-.085				4
5	.021	.010	-.007	-.155	-.041	-.238				.025	.024	.056	-.177	-.070					5
6	.008	.057	-.022	-.187	-.229					.030	.024	-.105	-.162	-.069					6
7	.028	.023	-.170	-.177						.016	-.117	-.104							7
8	.015	-.147	-.174							-.132	-.108	-.110							8
9	-.121	-.157	-.168							-.074	-.107								9
10	-.068	-.158								-.129									10
11	-.137																		11

[redacted]

Table 9 Continued

Pressure Coefficients on Delta Wing with Control

Configuration E M = 1.61 R = 7.6×10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
	α = 00°										δ = 20°									
1	.393	.360	.278	.282		.011	-.090											.172		1
2	.059	.037	.027	.026	-.269	-.321	-.364				.079		.049		.414	.454	.438			2
3	.021	.026		-.041	-.119		-.415				.036	.012	.005		.353	.357	.067			3
4	.024	.004	-.007	-.157	-.171	-.327	-.374				.038		-.014	-.030	.259	.299				4
5	.015	.002	.018	-.185	-.031	-.295					.008	.058	-.021	-.225	.167	.059				5
6	.001	.051	-.073	-.188	-.327						.025	.019	.110	-.271	.036					6
7	.022	.031	-.221	-.184							.028	.020	-.071	-.206	.059					7
8	.008	-.149	-.215								.008	-.093	-.075							8
9	-.121	-.173	-.216								-.134	-.077	-.098							9
10	-.063	-.186									-.077	-.075								10
11	-.127										-.105									11
	α = 00°										δ = 29°									
1	.395	.365	.280	.285		-.159	-.238											.435		1
2	.065	.040	.026	.027	-.341	-.381	-.410				.075		.044		.647	.644	.609			2
3	.024	.028		.399	-.193		-.450				.037	.011	.002		.646	.554	.245			3
4	.022	.005	-.010	-.324	-.243	-.398	-.400				.039		-.018	-.165	.539	.500				4
5	.015	.004	.102	-.290	-.208	-.397					.006	.056	-.029	-.258	.315	.240				5
6	.004	.054	-.099	-.199	-.377						.021	.020	.157	-.274	.173					6
7	.022	.063	-.265	-.188							.025	.030	-.036	-.264	.199					7
8	.012	-.149	-.267								.002	-.056	-.064							8
9	-.099	-.185	-.263								-.135	-.043	-.103							9
10	-.038	-.199									-.062	-.041								10
11	-.107										-.034									11
	α = 06°										δ = -04°									
1	.346	.115	.153	.018		.250	.228											-.164		1
2	-.069	-.268	-.328	-.360	-.135	-.140	-.176				.209		.233		.170	.143	.125			2
3	-.059	-.067		-.171	-.303		-.341				.147	.150	.151		.117	.091	-.148			3
4	-.049	-.086	-.111	-.148	-.162	-.183	-.330				.149		.116	.066	.068	.066				4
5	-.080	-.085	-.089	-.236	-.102	-.247					.123	.168	.103	-.080	.062	-.106				5
6	-.062	-.038	-.073	-.218	-.228						.117	.135	.095	-.099	-.121					6
7	-.044	-.049	-.201	-.197							.131	.125	-.078	-.098	-.131					7
8	-.063	-.189	-.203								.118	-.069	-.085							8
9	-.196	-.194	-.207								-.041	-.070	-.082							9
10	-.117	-.191									-.008	-.072								10
11	-.172										-.067									11
	α = 06°										δ = 00°									
1	.345	.110	.147	.025		.200	.155											-.106		1
2	-.068	-.267	-.331	-.360	-.248	-.279	-.288				.204		.235		.215	.209	.202			2
3	-.061	-.071		-.199	-.269		-.384				.144	.149	.151		.167	.150	-.103			3
4	-.051	-.087	-.111	-.139	-.166	-.197	-.367				.144		.114	.102	.114	.118				4
5	-.083	-.088	-.100	-.231	-.121	-.271					.122	.168	.102	-.067	.105	-.076				5
6	-.065	-.040	-.081	-.221	-.238						.117	.134	.114	-.064	-.068					6
7	-.049	-.060	-.210	-.222							.131	.119	-.062	-.060	-.054					7
8	-.066	-.194	-.209								.114	-.063	-.066							8
9	-.194	-.197	-.213								-.045	-.059	-.066							9
10	-.127	-.199									-.013	-.059								10
11	-.184										-.072									11
	α = 06°										δ = 10°									
1	.346	.110	.148	.025		.005	-.090											.111		1
2	-.069	-.268	-.333	-.361	-.372	-.424	-.422				.202		.231		.446	.402	.387			2
3	-.062	-.069		-.087	-.347		-.433				.141	.147	.148		.446	.329	.034			3
4	-.054	-.089	-.111	-.142	-.208	-.308	-.418				.141		.112	.175	.269	.278				4
5	-.084	-.088	-.112	-.238	-.134	-.403					.121	.164	.073	-.036	.233	.044				5
6	-.067	-.036	-.110	-.234	-.293						.114	.128	.172	-.083	.049					6
7	-.051	-.068	-.239	-.212							.124	.106	-.015	-.129	.053					7
8	-.063	-.217	-.234								.102	-.044	-.014							8
9	-.184	-.225	-.230								-.056	-.030	-.028							9
10	-.129	-.221									-.021	-.025								10
11	-.184										-.074									11

[redacted]

Table 9 Concluded

Pressure Coefficients on Delta Wing with Control

Configuration E M = 1.61 R = 7.6×10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
								α = 06°					δ = 20°							
1	.341	.110	.145	.021		-.145	-.209											.346		1
2	-.075	-.269	-.335	-.358	-.396	-.441	-.431				.203		.229		.665	.603	.554			2
3	-.069	-.073		-.354	-.403		-.437				.137	.146	.144		.523	.546	.199			3
4	-.059	-.092	-.089	-.294	-.236	-.359	-.419				.137		.108	.157	.512	.481				4
5	-.088	-.092	-.084	-.289	-.132	-.429					.115	.162	.062	-.084	.402	.201				5
6	-.072	-.005	-.200	-.218	-.351						.111	.124	.241	-.211	.201					6
7	-.055	-.041	-.289	-.204							.123	.101	.046	-.163	.202					7
8	-.059	-.209	-.269								.096	-.012	.018							8
9	-.158	-.241	-.246								-.051	.015	-.011							9
10	-.100	-.257									-.022	.024								10
11	-.157										-.052									11

[redacted]

Table 10

Pressure Coefficients on Delta Wing with Control

Configuration E1 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
								α = 00°					δ = 00°							
1	.349	.315	.314	.361	.303	.298	.282				.076	.058	.040	.074	.029	.034	.025			1
2	.066	.044	.037	.081	.069	.029	.053				.036		.008	.010	.012	.008				2
3	.034	.018	.018	.017	.081	.034	-.184				.030	.014	-.001	.020	.005	-.130				3
4	.037	.016	-.001	.014	.025	.001	-.200				.010	.002	-.021	-.140	.001	-.148				4
5	.031	-.002	-.018	-.140	.006	-.170					.027	.036	.018	-.138	-.140	-.160				5
6	.025	.065	.018	-.140	-.141	-.180					.013	.031	-.131	-.132	-.119					6
7	.009	.029	-.135	-.138	-.140						.020	-.133	-.118							7
8		-.135	-.130								-.118	-.131	-.127							8
9	-.121	-.137	-.139								-.081	-.134								9
10	-.071	.220									-.124									10
11	-.122																			11
								α = 00°					δ = 10°							
1	.347	.315			.291	.179	.202	-.274			.074	.059			.093	.183	.201	-.133		1
2	.066	.045			.013	-.094	-.114				.035				.117	.131	-.072			2
3	.034	.018			.015	-.084	-.249				.036	.014			.073	-.057	-.067			3
4	.041	.016			-.013	-.061	-.245				.010	.031			.057	-.081				4
5	.032	-.009			-.038	-.195					.025	.026			-.071	-.092				5
6	.025	.076			-.176	-.203					.045	.030			-.080					6
7	-.019	.031			-.168						.023	-.109								7
8		-.151									-.124	-.099								8
9	-.126	-.165									-.084									9
10	-.074	.213									-.123									10
11	-.126																			11
								α = 00°					δ = 20°							
1	.345	.314	.312	.334	.176	-.003	.005	-.326			.073	.058	.037	.011	.251	.401	.409	.110		1
2	.066	.045	.039	.052	-.140	-.219	-.249				.035		.032	.123	.308	.344	.130			2
3	.034	.019	.203	.001	-.018	-.232	-.320				.039	.014	-.001	-.041	.255	.078	.132			3
4	.043	.015	-.097	-.153	-.077	-.199	-.306				.009	.012	-.040	-.200	.178	.067				4
5	.031	.090	-.009	-.199	-.110	-.255					.027	.049	.122	-.247	.051	.059				5
6	.023	.051	-.039	-.189	-.241	-.253					.027	.023	-.065	-.190	.027					6
7	.036	.064	-.186	-.151	-.224						.049	-.084	-.065							7
8		-.145	-.186								-.102	-.058	-.095							8
9	-.168	-.176	-.190								-.070	-.058								9
10	-.084	.205									-.096									10
11	-.123																			11
								α = 00°					δ = 30°							
1	.342	.311	.308	.341	-.029	-.183	-.195	-.358			.069	.052	.032	.064	.545	.640	.570	.432		1
2	.062	.042	.035	.333	-.289	-.304	-.334				.031		.007	.203	.638	.622	.435			2
3	.030	.013	.095	.401	-.102	-.331	-.377				.035	.009	.000	-.189	.544	.264	.421			3
4	.039	.011	-.010	-.322	-.161	-.329	-.348				.003	-.001	-.016	-.284	.389	.334				4
5	.027	.211	-.005	-.270	-.239	-.348					.021	.040	.200	-.313	.258	.315				5
6	.017	.041	-.098	-.216	-.320	-.331					.007	.076	-.016	-.301	.205					6
7	.169	.048	-.234	-.153	-.294						.012	-.024	-.061							7
8		-.115	-.237								-.112	-.020	-.118							8
9	-.189	-.172	-.241								-.015	-.016								9
10	-.124	.193									-.012									10
11	-.086																			11
								α = 03°					δ = 00°							
1	.339	.201	.232	.307	.299	.159	.180	-.396			.146	.164	.153	.222	.249	.202	.212	-.070		1
2	-.018	-.118	-.145	-.194	-.107	-.335	-.347				.091		.084	.059	.140	.158	-.037			2
3	-.023	-.052	-.048	-.085	-.042	-.202	-.382				.086	.080	.061	.058	.134	-.022	-.047			3
4	-.012	-.042	-.089	-.053	-.153	-.186	-.374				.065	.057	.024	-.085	.101	-.037				4
5	-.032	-.070	-.119	-.189	-.104	-.292					.073	.100	.068	-.093	-.059	-.065				5
6	-.026	.009	-.034	-.187	-.248	-.303					.065	.064	-.086	-.086	-.045					6
7	-.039	-.017	-.182	-.184	-.233						.065	-.103	-.089							7
8		-.170	-.172								-.088	-.096	-.090							8
9	-.163	-.176	-.182								-.063	-.095								9
10	-.109	.226									-.109									10
11	-.150																			11

Table 10 Continued

Pressure Coefficients on Delta Wing with Control

Configuration E1 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
	α = 06°										δ = −30°									
1	.315	.132	.158	.135	−.046	−.106	−.139	.103			.207	.233	.239	.344	.036	−.240	−.253	−.327		1
2	−.072	−.236	−.323	−.399	.727	.335	.447				.141		.447	.328	−.128	−.277	−.319			2
3	−.055	−.091	−.091	−.305	.319	.258	.072				.142	.119	.051	−.222	−.090	−.265	−.336			3
4	−.037	−.087	−.101	−.221	−.092	.276	.057				.116	.284	.180	−.202	−.212	−.224				4
5	−.072	−.085	−.078	−.317	.122	.084					.123	.119	.084	−.149	−.320	−.261				5
6	−.061	−.023	.016	−.339	−.003	.039					.171	.174	−.123	−.125	−.251					6
7	−.054	−.031	−.151	−.330	−.002						.016	−.074	−.154							7
8		−.128	−.155								−.097	−.117	−.183							8
9	−.164	−.135	−.195								−.018	−.139								9
10	−.080	.218									−.059									10
11	−.077																			11
	α = 06°										δ = −20°									
1	.317	.134	.161	.072	.206	.144	.103	−.178			.209	.234	.240	.192	.224	−.093	−.107	−.252		1
2	−.070	−.233	−.320	−.376	.307	.078	.160				.144		.220	.131	.018	−.112	−.215			2
3	−.052	−.088	−.059	−.298	.090	.012	−.179				.145	.119	.107	−.087	−.002	−.126	−.232			3
4	−.036	−.084	−.124	−.142	−.177	−.036	−.185				.116	.138	.111	−.135	−.086	−.116				4
5	−.069	−.074	−.078	−.279	−.026	−.122					.130	.189	.091	−.128	−.239	−.162				5
6	−.060	−.040	−.043	−.244	−.161	−.158					.073	.131	−.111	−.121	−.174					6
7	−.035	−.037	−.180	−.255	−.158						.088	−.089	−.130							7
8		−.155	−.166								−.042	−.096	−.145							8
9	−.181	−.162	−.183								−.018	−.099								9
10	−.105	.228									−.057									10
11	−.127																			11
	α = 06°										δ = −10°									
1	.319	.136	.162	.123	.336	.220	.212	−.309			.210	.235	.241	.315	.437	.128	.114	−.105		1
2	−.068	−.231	−.316	−.349	−.072	−.213	−.160				.145		.085	.055	.135	.103	−.071			2
3	−.050	−.086	−.097	−.226	−.085	−.214	−.335				.148	.118	.140	.015	.091	−.039	−.084			3
4	−.035	−.081	−.116	−.131	−.170	−.220	−.324				.117	.087	.104	−.082	.046	−.035				4
5	−.066	−.070	−.093	−.244	−.081	−.244					.133	.186	.099	−.105	−.107	−.084				5
6	−.059	−.038	−.061	−.212	−.249	−.263					.087	.126	−.082	−.114	−.094					6
7	−.037	−.038	−.198	−.216	−.252						.126	−.073	−.096							7
8		−.176	−.178								−.029	−.071	−.107							8
9	−.187	−.182	−.199								−.012	−.073								9
10	−.115	.236									−.056									10
11	−.151																			11
	α = 06°										δ = 00°									
1	.319	.144	.166	.257	.219	−.034	−.018	−.374			.208	.231	.241	.299	.482	.352	.348	.099		1
2	−.062	−.202	−.282	−.293	−.246	−.373	−.381				.144		.169	.144	.333	.309	.113			2
3	−.045	−.081	−.094	−.212	−.094	−.366	−.414				.149	.113	.130	.136	.269	.087	.099			3
4	−.032	−.078	−.104	−.134	−.194	−.331	−.379				.117	.122	.069	−.024	.224	.095				4
5	−.063	−.101	−.064	−.212	−.141	−.329					.134	.172	.141	−.034	.057	.058				5
6	−.055	−.020	−.076	−.217	−.295	−.328					.127	.118	−.032	−.026	.037					6
7	−.069	−.052	−.207	−.214	−.298						.127	−.055	−.037							7
8		−.195	−.194								−.041	−.046	−.040							8
9	−.191	−.204	−.206								−.027	−.042								9
10	−.131	.245									−.072									10
11	−.169																			11
	α = 06°										δ = 10°									
1	.317	.135	.163	.114	.178	−.073	−.059	−.386			.207	.233	.241	.222	.462	.403	.393	.129		1
2	−.069	−.226	−.304	−.302	−.262	−.394	−.400				.142		.216	.226	.427	.360	.138			2
3	−.051	−.087	−.157	−.182	−.094	−.373	−.426				.148	.115	.109	.202	.307	.100	.136			3
4	−.037	−.081	−.114	−.094	−.181	−.324	−.393				.115	.148	.053	.009	.278	.104				4
5	−.068	−.095	−.083	−.240	−.137	−.354					.130	.153	.201	−.094	.098	.089				5
6	−.049	−.023	−.109	−.222	−.280	−.348					.148	.122	.011	−.120	.048					6
7	−.077	−.032	−.214	−.214	−.278						.127	−.025	.020							7
8		−.212	−.205								−.045	−.005	.004							8
9	−.197	−.236	−.205								−.032	−.006								9
10	−.134	.227									−.066									10
11	−.172																			11

[redacted]

Table 10 Continued

Pressure Coefficients on Delta Wing with Control

Configuration E1 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
								α = 06°				δ = 20°								
1	.315	.135	.162	.333	-.031	-.245	-.254	-.362			.206	.232	.237	.276	.642	.658	.543	.427		1
2	-.068	-.231	-.315	-.176	-.367	-.415	-.414				.142		.169	.308	.661	.642	.431			2
3	-.052	-.088	.192	-.168	-.132	-.415	-.426				.149	.112	.147	.161	.627	.283	.410			3
4	-.037	-.084	-.183	-.282	-.235	-.393	-.390				.114	.112	.068	-.045	.516	.351				4
5	-.066	.053	-.102	-.262	-.198	-.404					.129	.176	.284	-.210	.307	.319				5
6	-.062	-.090	-.164	-.220	-.336	-.385					.115	.143	.074	-.204	.232					6
7	.029	.006	-.272	-.162	-.346						.139	.021	.036							7
8		-.188	-.272								-.021	.056	.002							8
9	-.248	-.232	-.252								.006	.060								9
10	-.136	.219									.010									10
11	-.150																			11
								α = 06°				δ = 30°								
1	.314	.132	.158	.130	-.119	-.336	-.337	-.339			.203	.230	.235	.254	.881	.881	.729	.612		1
2	-.070	-.234	-.320	-.134	-.411	-.432	-.407				.139		.161	.426	.898	.887	.699			2
3	-.055	-.090	-.074	.555	-.158	-.439	-.412				.147	.109	.116	.099	.945	.481	.622			3
4	-.039	-.086	.010	-.354	-.293	-.423	-.379				.110	.107	.231	-.220	.748	.583				4
5	-.069	-.014	-.098	-.341	-.266	-.399					.126	.151	.365	-.251	.548	.519				5
6	-.066	.043	-.270	-.301	-.385	-.359					.110	.268	.093	-.243	.404					6
7	.151	-.021	-.358	-.260	-.389						.110	.094	.015							7
8		-.224	-.240								-.010	.091	-.010							8
9	-.156	-.240	-.245								.127	.065								9
10	-.138	.217									.162									10
11	-.176																			11
								α = 09°				δ = 00°								
1	.279	.078	.073	.207	.228	-.066	-.024	-.418			.276	.310	.310	.435	.370	.335	.344	.051		1
2	-.162	-.387	-.408	-.384	-.215	-.419	-.428				.202		.226	.192	.280	.298	.079			2
3	-.088	-.139	-.165	-.420	-.161	-.408	-.429				.205	.194	.191	.205	.250	.065	.080			3
4	-.073	-.125	-.131	-.246	-.328	-.376	-.416				.182	.181	.118	.030	.220	.072				4
5	-.109	-.168	-.185	-.307	-.256	-.401					.187	.245	.205	.027	.037	.040				5
6	-.094	-.059	-.122	-.267	-.319	-.372					.158	.162	.006	.024	.039					6
7	-.130	-.089	-.233	-.253	-.287						.178	-.016	.002							7
8		-.223	-.220								.000	-.005	.001							8
9	-.214	-.241	-.236								-.001	-.003								9
10	-.151	.257									-.037									10
11	-.190																			11
								α = 12°				δ = -30°								
1	.243	.034	-.034	-.103	.074	-.060	-.011	-.127			.354	.387	.401	.378	.041	-.135	-.147	-.293		1
2	-.273	-.428	-.456	-.475	.679	.168	.224				.269		.523	.425	-.017	-.152	-.237			2
3	-.118	-.207	-.331	-.473	.355	.048	-.139				.258	.262	.226	-.106	-.003	-.172	-.247			3
4	-.109	-.195	-.241	-.357	-.274	-.067	-.187				.249	.337	.324	-.147	-.195	-.152				4
5	-.140	-.179	-.166	-.372	-.268	-.231					.258	.331	.212	-.120	-.314	-.193				5
6	-.128	-.142	-.136	-.339	-.301	-.259					.167	.247	-.059	-.116	-.259					6
7	-.129	-.111	-.277	-.320	-.280						.223	-.005	-.093							7
8		-.185	-.290								.084	.004	-.116							8
9	-.219	-.206	-.289								.065	-.015								9
10	-.123	.228									.053									10
11	-.101																			11
								α = 12°				δ = -20°								
1	.241	.032	-.035	-.089	.440	.191	.205	-.313			.353	.385	.399	.427	.205	.063	.069	-.179		1
2	-.275	-.429	-.454	-.472	.285	-.114	-.095				.268		.280	.376	.115	.089	-.102			2
3	-.119	-.208	-.333	-.464	.024	-.160	-.316				.258	.261	.282	.020	.064	-.065	-.113			3
4	-.110	-.197	-.247	-.318	-.372	-.236	-.329				.248	.222	.261	-.067	-.068	-.059				4
5	-.141	-.168	-.177	-.316	-.281	-.354					.274	.332	.195	-.105	-.243	-.110				5
6	-.128	-.155	-.160	-.278	-.333	-.357					.173	.231	-.045	-.109	-.175					6
7	-.116	-.092	-.273	-.278	-.312						.265	.028	-.055							7
8		-.206	-.294								.076	.022	-.055							8
9	-.244	-.222	-.306								.061	.006								9
10	-.148	.247									.044									10
11	-.141																			11

[redacted]

Table 10 Continued

Pressure Coefficients on Delta Wing with Control

Configuration E1 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 12°									δ = -10°									
1	.243	.035	-.033	-.078	.410	.033	.059	-.386		.354	.387	.399	.549	.341	.270	.280	-.014		1
2	-.272	-.426	-.439	-.446	-.170	-.399	-.396			.270		.339	.229	.185	.237	.023			2
3	-.116	-.205	-.336	-.436	-.154	-.362	-.407			.259	.273	.307	.133	.112	.032	.027			3
4	-.107	-.193	-.225	-.272	-.356	-.361	-.390			.251	.222	.248	.003	.093	.040				4
5	-.138	-.189	-.184	-.312	-.287	-.397				.280	.338	.199	-.043	-.070	-.010				5
6	-.126	-.137	-.203	-.267	-.353	-.374				.211	.250	-.009	-.055	-.077					6
7	-.127	-.094	-.277	-.226	-.330					.284	.030	-.007							7
8		-.205	-.230							.085	.031	-.011							8
9	-.244	-.250	-.257							.066	.023								9
10	-.157	.266								.038									10
11	-.157																		11
	α = 12°									δ = 00°									
1	.239	.035	-.034	.101	.284	.034	.047	-.226		.348	.380	.395	.494	.191	.283	.243	-.046		1
2	-.259	-.376	-.417	-.431	.037	-.112	-.112			.265		.289	.284	.276	.265	.009			2
3	-.120	-.201	-.355	-.427	-.053	-.181	-.257			.254	.262	.264	.295	.228	.012	.026			3
4	-.111	-.189	-.205	-.316	-.291	-.208	-.231			.246	.245	.200	.086	.157	.024				4
5	-.143	-.208	-.131	-.325	-.255	-.305				.277	.318	.274	.078	-.069	.005				5
6	-.129	-.127	-.163	-.327	-.263	-.270				.211	.224	.052	.078	-.077					6
7	-.149	-.103	-.280	-.303	-.240					.246	.033	.052							7
8		-.246	-.270							.047	.050	.054							8
9	-.236	-.268	-.264							.040	.048								9
10	-.162	.269								.018									10
11	-.198																		11
	α = 12°									δ = 10°									
1	.239	.031	-.036	.027	.008	-.203	-.203	-.298		.349	.382	.394	.379	.490	.549	.457	.305		1
2	-.273	-.406	-.425	-.415	-.252	-.293	-.290			.265		.369	.391	.606	.536	.310			2
3	-.122	-.208	-.299	-.432	-.145	-.331	-.336			.255	.258	.254	.389	.514	.212	.315			3
4	-.112	-.176	-.219	-.312	-.346	-.337	-.308			.246	.279	.191	.149	.477	.257				4
5	-.143	-.175	-.158	-.322	-.315	-.356				.246	.299	.358	.005	.244	.230				5
6	-.111	-.099	-.246	-.305	-.336	-.320				.250	.256	.134	-.057	.161					6
7	-.137	-.048	-.220	-.307	-.306					.253	.083	.120							7
8		-.259	-.285							.057	.107	.110							8
9	-.273	-.283	-.297							.058	.105								9
10	-.152	.243								.066									10
11	-.186																		11
	α = 12°									δ = 20°									
1	.239	.031	-.037	.124	-.093	-.311	-.298	-.319		.348	.381	.394	.459	.771	.779	.618	.521		1
2	-.276	-.422	-.428	-.312	-.362	-.385	-.353			.265		.307	.529	.904	.790	.589			2
3	-.121	-.208	-.198	-.352	-.176	-.407	-.358			.255	.257	.280	.395	.832	.384	.535			3
4	-.112	-.187	-.232	-.345	-.390	-.404	-.340			.246	.240	.243	.055	.714	.494				4
5	-.143	-.014	-.190	-.299	-.344	-.362				.244	.305	.453	-.122	.483	.440				5
6	-.129	-.095	-.233	-.220	-.391	-.331				.212	.333	.182	-.140	.343					6
7	-.035	-.111	-.367	-.169	-.365					.260	.152	.136							7
8		-.214	-.299							.082	.177	.099							8
9	-.272	-.243	-.198							.153	.159								9
10	-.159	.227								.211									10
11	-.172																		11
	α = 12°									δ = 30°									
1	.237	.029	-.037	-.052	-.122	-.383	-.351	-.335		.348	.381	.393	.398	1.113	1.046	.870	.681		1
2	-.277	-.427	-.368	-.172	-.408	-.413	-.365			.264		.303	.560	1.192	1.072	.857			2
3	-.123	-.195	-.212	.469	-.183	-.423	-.368			.254	.255	.253	.316	1.206	.820	.733			3
4	-.113	-.136	-.125	-.419	-.419	-.416	-.353			.245	.237	.462	-.066	.969	.739				4
5	-.144	-.037	-.186	-.360	-.387	-.380				.243	.286	.498	-.141	.752	.642				5
6	-.108	.024	-.311	-.226	-.407	-.357				.211	.428	.198	-.160	.549					6
7	.134	-.093	-.394	-.226	-.389					.268	.203	.147							7
8		-.266	-.261							.217	.211	.105							8
9	-.198	-.300	-.191							.313	.255								9
10	-.183	.236								.315									10
11	-.260																		11

[redacted]

Table 10 Concluded

Pressure Coefficients on Delta Wing with Control

Configuration E1 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
								α = 15°			δ = 00°									
1	.198	-.044	-.164	.066	.247	-.046	-.055	-.290			.423	.452	.450	.593	.289	.426	.361	.129		1
2	-.357	-.441	-.433	-.451	-.067	-.185	-.224				.335		.375	.374	.394	.416	.170			2
3	-.150	-.327	-.398	-.435	-.100	-.241	-.305				.320	.373	.370	.419	.345	.128	.183			3
4	-.142	-.299	-.366	-.323	-.342	-.277	-.294				.318	.354	.356	.163	.335	.114				4
5	-.173	-.198	-.264	-.370	-.316	-.356					.403	.418	.384	.161	.042	.105				5
6	-.155	-.113	-.354	-.348	-.329	-.333					.332	.340	.135	.161	.035					6
7	-.181	-.116	-.385	-.256	-.276						.348	.119	.137							7
8		-.245	-.358								.119	.134	.133							8
9	-.257	-.270	-.352								.115	.122								9
10	-.168	.278									.109									10
11	-.193																			11

[redacted]

Table 11

Pressure Coefficients on Delta Wing with Control

Configuration E2 M = 1.61 R = 4.2 x 10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 00°									δ = -30°									
1	.387	.342	.281	.259		.261	-.351										-.360		1
2	.059	.037	.024	.521	.805	.790	.661			.076		.053		-.413	-.384	-.406			2
3	.026	.016		-.012	.771		.202			.043	.027	.015		-.359	-.395	1.753			3
4	.030	.002	.085	-.017	.777	.605	.333			.037		.084	-.065	-.271	-.422				4
5	.007	-.001	-.006	-.089	.651	1.754				.005	.029	-.004	-.180	-.281	-.394				5
6	.012	.109	-.034	-.056	.252					.033	.089	-.012	-.161	-.375					6
7	.029	.021	-.122	-.067						.020	.035	-.172	-.163	-.382					7
8	.057	-.163	-.079							.066	-.137	-.171							8
9	-.091	-.163	-.058							-.072	-.140	-.171							9
10	-.048	-.128								-.046	-.139								10
11	-.146									-.133									11
	α = 00°									δ = -20°									
1	.392	.349	.286	.262		.432	-.209										-.377		1
2	.064	.038	.029	.523	.465	.504	.528			.074		.047		-.332	-.340	-.382			2
3	.030	.024		-.003	.429		.076			.033	.016	.007		-.188	-.351	1.746			3
4	.032	.011	.092	-.057	.430	.411	.108			.031		.082	-.064	-.182	-.353				4
5	.012	.007	-.001	-.127	.405	1.752				-.003	.028	-.013	-.181	-.165	-.353				5
6	.017	.116	-.025	-.078	.072					.028	.080	-.015	-.171	-.277					6
7	.035	.027	-.176	-.085						.016	.018	-.177	-.166	-.275					7
8	.061	-.155	-.133							.056	-.154	-.179							8
9	-.086	-.158	-.097							-.080	-.154	-.176							9
10	-.042	-.151								-.053	-.148								10
11	-.140									-.141									11
	α = 00°									δ = -10°									
1	.395	.353	.288	.268		.582	.051										-.323		1
2	.067	.043	.031	.527	.212	.269	.340			.082		.049		-.093	-.230	-.282			2
3	.030	.026		-.005	.193		.100			.046	.017	.014		-.098	-.208	1.755			3
4	.034	.010	.092	-.062	.212	.218	-.054			.039		.087	-.049	-.095	-.117				4
5	.016	.007	-.002	-.154	.197	1.752				.013	.021	-.005	-.166	-.087	-.231				5
6	.021	.119	-.026	-.100	-.041					.030	.084	-.008	-.154	-.200					6
7	.041	.029	-.180	-.108						.017	.031	-.163	-.156	-.197					7
8	.065	-.152	-.172							.064	-.137	-.171							8
9	-.081	-.157	-.143							-.078	-.145	-.166							9
10	-.039	-.152								-.048	-.139								10
11	-.137									-.135									11
	α = 00°									δ = 00°									
1	.383	.336	.275	.253		1.728	.295										-.231		1
2	.051	.030	.021	.525	.034	.029	.063			.072		.042		.019	.001	.011			2
3	.019	.011		-.013	.021		.116			.035	.004	-.003		-.002	-.005	1.740			3
4	.019	-.003	.085	-.068	.018	.031	-.178			.027		.075	-.064	-.019	-.007				4
5	-.002	-.007	-.013	-.167	.030	1.746				-.005	.017	-.015	-.176	.014	-.158				5
6	.003	.105	-.037	-.132	-.143					.014	.086	-.022	-.150	-.137					6
7	.023	.012	-.187	-.138						.010	.022	-.173	-.152	-.138					7
8	.047	-.168	-.185							.054	-.150	-.172							8
9	-.101	-.170	-.179							-.089	-.156	-.164							9
10	-.058	-.165								-.062	-.152								10
11	-.153									-.148									11
	α = 00°									δ = 10°									
1	.390	.346	.282	.264		1.710	.110										-.023		1
2	.062	.042	.030	.531	-.068	-.269	-.293			.074		.040		.211	.245	.299			2
3	.027	.024		-.002	-.097		-.072			.041	.018	.004		.178	.225	1.743			3
4	.031	.011	.098	-.056	-.072	-.093	-.328			.038		.072	-.065	.167	.192				4
5	.014	.005	-.002	-.176	-.070	1.746				-.003	.018	-.010	-.158	.193	-.060				5
6	.009	.117	-.027	-.149	-.216					.019	.082	-.017	-.126	-.032					6
7	.034	.025	-.178	-.155						.013	.019	-.174	-.125	-.025					7
8	.063	-.152	-.183							.057	-.155	-.172							8
9	-.083	-.156	-.179							-.082	-.151	-.148							9
10	-.047	-.148								-.052	-.149								10
11	-.139									-.144									11

[redacted]

Table 11 Continued

Pressure Coefficients on Delta Wing with Control

Configuration E2 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
	α = 00°										δ = 20°									
1	.388	.342	.280	.262		1.705	-.106				.072		.050		.455	.480	.504	.235		1
2	.055	.036	.027	.528	-.167	-.347	-.358				.042	.027	.014		.436	.511	1.752			2
3	.025	.019		-.002	-.167		-.157				.042		.078	-.056	.390	.403				3
4	.029	.002	.095	-.063	-.149	-.278	-.382				-.001	.036	-.006	-.131	.419	.076				4
5	.011	.000	-.006	-.185	-.149	1.751					.034	.086	-.012	-.086	.096					5
6	.000	.112	-.029	-.155	-.270						.017	.029	-.172	-.089	.068					6
7	.030	.020	-.185	-.155							.058	-.145	-.134							7
8	.059	-.158	-.188								-.078	-.143	-.099							8
9	-.089	-.157	-.192								-.040	-.145								9
10	-.055	-.152									-.136									10
11	-.146																			11
	α = 00°										δ = 30°									
1	.392	.348	.284	.266		1.691	-.278				.065		.034		.784	.759	.634	.513		1
2	.061	.040	.033	.536	-.369	-.406	-.392				.035	.017	.003		.754	.715	1.742			2
3	.032	.024		-.002	-.337		-.233				.044		.065	-.036	.733	.591				3
4	.033	.007	.100	-.068	-.245	-.365	-.400				-.003	.023	-.011	-.093	.642	.269				4
5	.014	.003	-.001	-.191	-.242	1.750					.022	.078	-.015	-.069	.231					5
6	.009	.119	-.024	-.157	-.354						.010	.025	-.140	-.078	.168					6
7	.035	.027	-.183	-.164							.055	-.143	-.093							7
8	.065	-.149	-.187								-.093	-.153	-.044							8
9	-.084	-.154	-.183								-.049	-.124								9
10	-.051	-.152									-.143									10
11	-.139																			11
	α = 06°										δ = -30°									
1	.336	.083	.137	-.022		.194	-.215				.205		.246		-.359	-.318	-.350	-.371		1
2	-.089	-.268	-.335	-.160	.526	.595	.553				.145	.162	.162		-.179	-.333	1.745			2
3	-.063	-.079		-.272	.466		.042				.145		.290	.055	-.173	-.358				3
4	-.047	-.090	-.067	-.097	.537	.405	.124				.105	.138	.164	-.094	-.186	-.333				4
5	-.083	-.089	-.210	-.178	.388	1.747					.129	.252	.089	-.089	-.271					5
6	-.074	-.002	-.240	-.165	.055						.126	.159	-.090	-.101	-.281					6
7	-.047	-.107	-.180	-.167							.252	-.034	-.098							7
8	-.044	-.270	-.149								.027	-.024	-.095							8
9	-.169	-.292	-.154								.036	-.049								9
10	-.136	-.204									-.039									10
11	-.222																			11
	α = 06°										δ = -20°									
1	.337	.088	.142	-.013		.230	-.021				.217		.262		-.257	-.236	-.263	-.338		1
2	-.084	-.261	-.323	-.151	.232	.356	.373				.152	.169	.173		-.118	-.227	1.753			2
3	-.061	-.074		-.263	.213		.030				.156		.301	.065	-.081	-.229				3
4	-.046	-.085	-.056	-.105	.303	.215	-.037				.120	.148	.181	-.088	-.099	-.229				4
5	-.079	-.083	-.200	-.174	.174	1.757					.141	.260	.113	-.080	-.201					5
6	-.066	.003	-.227	-.154	-.067						.137	.176	-.077	-.089	-.205					6
7	-.046	-.105	-.192	-.172							.261	-.020	-.083							7
8	-.043	-.271	-.170								.048	-.016	-.080							8
9	-.167	-.285	-.165								.047	-.034								9
10	-.133	-.290									-.022									10
11	-.224																			11
	α = 06°										δ = -10°									
1	.349	.089	.145	-.008		.247	.250				.224		.266		-.066	-.101	-.053	-.269		1
2	-.071	-.253	-.313	-.150	.034	.114	.131				.164	.176	.175		-.068	.007	1.754			2
3	-.052	-.071		-.259	.052		.078				.169		.306	.068	.018	-.007				3
4	-.039	-.077	-.052	-.106	.116	.073	-.122				.127	.148	.187	.084	.012	-.194				4
5	-.069	-.079	-.197	-.187	.033	1.764					.152	.268	.113	.074	-.138					5
6	-.059	.009	-.228	-.157	-.136						.146	.183	-.073	-.080	-.134					6
7	-.038	-.096	-.191	-.169							.276	-.020	-.077							7
8	-.034	-.261	-.186								.049	-.011	-.071							8
9	-.159	-.279	-.185								.052	-.024								9
10	-.127	-.289									-.017									10
11	-.206																			11

[redacted]

Table 11 Continued

Pressure Coefficients on Delta Wing with Control

Configuration E2 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 06°									δ = 00°									
1	.340	.080	.144	-.019		1.565	.177			.207		.252		.103	.212	.261	-.054		1
2	-.082	-.261	-.327	-.154	-.132	-.250	-.312			.152	.173	.168		.072	.213	1.748			2
3	-.064	-.078		-.266	-.074		-.286			.158		.295	.056	.171	.154				3
4	-.049	-.088	-.064	-.110	-.053	-.106	-.288			.114	.129	.177	-.089	.169	-.042				4
5	-.079	-.089	-.208	-.195	-.103	1.752				.135	.254	.108	-.070	-.025					5
6	-.073	.000	-.238	-.180	-.252					.132	.171	-.086	-.072	-.005					6
7	-.050	-.108	-.201	-.191						.256	-.027	-.091							7
8	.043	-.269	-.201							.040	-.023	-.078							8
9	-.169	-.291	-.209							.046	-.036								9
10	-.140	-.298								-.026									10
11	-.218																		11
	α = 06°									δ = 10°									
1	.338	.080	.143	-.017		1.473	-.080			.220		.247		.343	.487	.456	.182		1
2	-.083	-.263	-.328	-.151	-.288	-.343	-.375			.159	.168	.173		.303	.454	1.750			2
3	-.064	-.079		-.262	-.155		-.316			.167		.307	.062	.411	.373				3
4	-.050	-.088	-.063	-.112	-.153	-.281	-.361			.122	.144	.183	-.068	.381	.082				4
5	-.082	-.090	-.207	-.204	-.197	1.751				.139	.263	.109	-.034	.118					5
6	-.075	-.001	-.233	-.194	-.298					.135	.169	-.079	-.033	.120					6
7	-.054	-.108	-.201	-.185						.259	-.024	-.070							7
8	-.045	-.269	-.205							.044	-.020	-.053							8
9	-.169	-.290	-.209							.046	-.034								9
10	-.147	-.299								-.027									10
11	-.217																		11
	α = 06°									δ = 20°									
1	.342	.081	.146	-.015		1.097	-.252			.215		.251		.619	.714	.596	.478		1
2	-.082	-.257	-.325	-.147	-.357	-.398	-.399			.153	.161	.165		.586	.661	1.748			2
3	-.064	-.077		-.260	-.304		-.333			.163		.301	.064	.682	.560				3
4	-.046	-.086	-.062	-.113	-.238	-.361	-.393			.113	.140	.177	-.018	.602	.282				4
5	-.078	-.089	-.205	-.202	-.247	1.759				.140	.259	.108	.011	.274					5
6	-.072	.003	-.230	-.190	-.339					.135	.168	-.083	.012	.263					6
7	-.048	-.105	-.201	-.184						.257	-.026	-.037							7
8	-.044	-.268	-.204							.038	-.022	.006							8
9	-.166	-.289	-.210							.043	-.037								9
10	-.144	-.294								-.034									10
11	-.215																		11
	α = 06°									δ = 30°									
1	.335	.074	.139	-.025		.644	-.328			.218		.250		.983	.873	.711	.673		1
2	-.086	-.266	-.333	-.154	-.400	-.426	-.363			.154	.165	.171		.951	.856	1.754			2
3	-.069	-.083		-.266	-.373		-.335			.165		.305	.175	.938	.671				3
4	-.051	-.092	-.072	-.121	-.362	-.371	-.356			.122	.142	.177	.016	.831	.567				4
5	-.086	-.095	-.213	-.204	-.356	1.752				.146	.259	.108	.035	.521					5
6	-.081	-.002	-.242	-.184	-.365					.137	.173	.018	.033	.482					6
7	-.055	-.113	-.213	-.181						.259	-.024	.015							7
8	-.048	-.274	-.214							.045	.049	.037							8
9	-.174	-.297	-.215							.051	.061								9
10	-.151	-.266								-.032									10
11	-.220																		11
	α = 12°									δ = -30°									
1	.214	-.110	-.017	-.171		.191	-.117			.351		.400		-.308	-.253	-.320	-.355		1
2	-.288	-.421	-.464	-.435	.393	.400	.422			.272	.286	.302		-.109	-.279	1.748			2
3	-.130	-.181		-.446	.174		-.059			.270		.463	.198	-.138	-.298				3
4	-.106	-.169	-.201	-.304	.290	.260	.004			.244	.267	.314	.006	-.152	-.264				4
5	-.154	-.182	-.271	-.243	.239	1.750				.246	.388	.239	.019	-.247					5
6	-.133	-.109	-.335	-.202	-.057					.418	.350	.038	.042	-.254					6
7	-.124	-.177	-.404	-.135						.366	.078	.038							7
8	-.096	-.307	-.371							.109	.065	.038							8
9	-.210	-.328	-.246							.089	.039								9
10	-.168	-.335								.055									10
11	-.243																		11

[redacted]

Table 11 Continued

Pressure Coefficients on Delta Wing with Control

Configuration E2 M = 1.61 R = 4.2 x 10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
								α = 12°		δ = -20°									
1	.210	-.116	-.030	-.183		.198	.174			.342		.409		-.138	-.096	-.172	-.287		1
2	-.288	-.428	-.469	-.436	.086	.135	.214			.278	.287	.301		-.032	-.052	1.753			2
3	-.128	-.185		-.459	-.039		-.075			.275		.471	.215	-.020	-.059				3
4	-.108	-.174	-.205	-.317	.105	.086	-.153			.247	.266	.321	.013	-.040	-.197				4
5	-.157	-.188	-.277	-.244	.063	1.757				.243	.395	.246	.022	-.174					5
6	-.138	-.114	-.341	-.209	-.156					.414	.353	.050	.046	-.174					6
7	-.127	-.183	-.410	-.134						.377	.082	.045							7
8	-.101	-.316	-.380							.121	.067	.041							8
9	-.209	-.334	-.319							.094	.043								9
10	-.180	-.341								.056									10
11	-.251																		11
								α = 12°		δ = -10°									
1	.208	-.115	-.029	-.186		.194	.198			.342		.399		-.047	.103	.142	-.153		1
2	-.287	-.430	-.468	-.436	-.101	-.082	-.126			.273	.282	.294		-.008	.118	1.748			2
3	-.128	-.185		-.456	-.111		-.045			.278		.473	.196	.100	.084				3
4	-.112	-.176	-.207	-.316	-.016	-.005	-.198			.248	.266	.323	.003	.082	-.134				4
5	-.160	-.192	-.275	-.253	-.045	1.747				.244	.395	.241	.016	-.095					5
6	-.139	-.112	-.349	-.217	-.204					.417	.352	.045	.046	-.086					6
7	-.131	-.190	-.414	-.144						.378	.083	.039							7
8	-.099	-.324	-.387							.120	.066	.035							8
9	-.214	-.337	-.350							.091	.043								9
10	-.184	-.347								.053									10
11	-.255																		11
								α = 12°		δ = 00°									
1	.222	-.104	-.013	-.171		.449	-.033			.348		.399		.139	.401	.391	.096		1
2	-.274	-.420	-.460	-.415	-.327	-.396	-.409			.274	.278	.295		.132	.357	1.750			2
3	-.121	-.173		-.448	-.168		-.363			.272		.468	.183	.339	.293				3
4	-.103	-.171	-.185	-.309	-.134	-.208	-.407			.237	.251	.319	.003	.278	.038				4
5	-.150	-.178	-.263	-.251	-.155	1.754				.235	.383	.239	.024	.056					5
6	-.134	-.105	-.333	-.216	-.296					.399	.348	.039	.058	.075					6
7	-.123	-.186	-.408	-.137						.371	.079	.037							7
8	-.095	-.311	-.374							.117	.062	.043							8
9	-.207	-.328	-.321							.088	.045								9
10	-.179	-.336								.055									10
11	-.249																		11
								α = 12°		δ = 10°									
1	.220	-.106	-.017	-.174		.350	-.233			.337		.392		.371	.617	.538	.372		1
2	-.276	-.426	-.464	-.423	-.373	-.428	-.428			.276	.277	.290		.381	.574	1.746			2
3	-.126	-.178		-.453	-.266		-.378			.276		.470	.174	.566	.476				3
4	-.108	-.174	-.190	-.314	-.214	-.350	-.422			.235	.251	.316	.027	.485	.215				4
5	-.157	-.180	-.267	-.249	-.235	1.752				.235	.384	.235	.068	.201					5
6	-.138	-.107	-.337	-.216	-.339					.401	.344	.035	.100	.234					6
7	-.128	-.188	-.408	-.124						.372	.076	.056							7
8	-.095	-.315	-.377							.114	.059	.082							8
9	-.208	-.335	-.269							.095	.040								9
10	-.185	-.339								.046									10
11	-.252																		11
								α = 12°		δ = 20°									
1	.223	-.103	-.011	-.170		.253	-.317			.347		.400		.685	.787	.634	.598		1
2	-.271	-.422	-.458	-.414	-.394	-.430	-.428			.269	.283	.289		.768	.766	1.743			2
3	-.119	-.174		-.446	-.374		-.377			.278		.465	.239	.800	.605				3
4	-.104	-.169	-.183	-.306	-.282	-.381	-.411			.241	.254	.320	.089	.725	.490				4
5	-.152	-.174	-.262	-.246	-.312	1.746				.237	.384	.234	.105	.419					5
6	-.130	-.099	-.331	-.211	-.394					.402	.345	.101	.150	.533					6
7	-.126	-.182	-.402	-.087						.370	.082	.120							7
8	-.092	-.309	-.373							.114	.074	.129							8
9	-.203	-.326	-.202							.096	.103								9
10	-.184	-.335								.045									10
11	-.245																		11

[redacted]

Table 11 Continued

Pressure Coefficients on Delta Wing with Control

Configuration E2 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
	$\alpha = -06^\circ$										$\delta = -30^\circ$									
1	.292	.347	.165	.144		.081	-.354				-.063		-.286		-.437	-.404	-.418	-.384		1
2	.193	.201	.228	.879	1.029	.898	.714				-.046	-.082	-.104		-.366	-.407	1.754			2
3	.126	.142		.163	.988		.251				-.051		-.047	-.114	-.357	-.429				3
4	.128	.101	.289	.169	.970	.678	.499				-.081	-.057	-.206	-.198	-.336	-.406				4
5	.112	.110	.160	.006	.835	1.754					-.051	-.018	-.179	-.197	-.383					5
6	.106	.267	.077	.028	.470						-.065	-.095	-.200	-.189	-.371					6
7	.152	.160	.001	.013							-.036	-.254	-.202							7
8	.234	-.055	.003								-.161	-.270	-.194							8
9	.018	.014	.014								-.126	-.133								9
10	.040	.049									-.216									10
11	-.049																			11
	$\alpha = -06^\circ$										$\delta = -20^\circ$									
1	.294	.357	.169	.146		.142	-.301				-.058		-.277		-.396	-.365	-.411	-.384		1
2	.192	.207	.228	.884	.635	.735	.622				-.034	-.070	-.098		-.287	-.381	1.757			2
3	.133	.143		.169	.625		.072				-.035		-.037	-.099	-.246	-.405				3
4	.135	.110	.292	.052	.716	.567	.275				-.067	-.046	-.200	-.195	-.230	-.406				4
5	.119	.117	.167	-.029	.608	1.754					-.043	-.010	-.179	-.188	-.329					5
6	.112	.274	.079	.014	.236						-.056	-.085	-.189	-.182	-.330					6
7	.155	.160	-.097	.018							-.028	-.237	-.193							7
8	.235	-.049	-.039								-.151	-.259	-.183							8
9	.022	-.051	.000								-.113	-.204								9
10	.044	-.051									-.201									10
11	-.045																			11
	$\alpha = -06^\circ$										$\delta = -10^\circ$									
1	.296	.352	.169	.142		.187	-.162				-.052		-.279		-.321	-.302	-.354	-.370		1
2	.196	.202	.230	.888	.336	.495	.489				-.025	-.061	-.088		-.149	-.313	1.748			2
3	.135	.149		.161	.318		-.019				-.036		-.036	-.102	-.162	-.334				3
4	.133	.112	.292	.037	.414	.383	.081				-.059	-.051	-.195	-.191	-.175	-.348				4
5	.120	.115	.163	-.087	.374	1.762					-.036	-.003	-.184	-.188	-.272					5
6	.114	.271	.075	-.028	.094						-.048	-.085	-.190	-.183	-.265					6
7	.155	.166	-.101	-.019							-.027	-.246	-.191							7
8	.243	-.049	-.092								-.147	-.261	-.184							8
9	.024	-.052	-.064								-.109	-.241								9
10	.044	-.056									-.206									10
11	-.044																			11
	$\alpha = -06^\circ$										$\delta = 00^\circ$									
1	.294	.353	.170	.143		.076	.089				-.061		-.283		-.145	-.304	-.358	-.373		1
2	.189	.204	.232	.888	.163	.257	.301				-.036	-.071	-.094		-.095	-.149	1.754			2
3	.126	.146		.166	.100		.173				-.040		-.045	-.103	-.127	-.171				3
4	.128	.112	.287	.043	.237	.223	-.011				-.067	-.049	-.207	-.192	-.155	-.325				4
5	.120	.113	.161	-.096	.180	1.756					-.045	-.013	-.189	-.181	-.262					5
6	.106	.276	.077	-.072	-.013						-.057	-.095	-.190	-.188	-.248					6
7	.152	.163	-.103	-.073							-.036	-.250	-.188							7
8	.241	-.050	-.098								-.160	-.267	-.189							8
9	.021	-.051	-.092								-.119	-.243								9
10	.040	-.056									-.211									10
11	-.038																			11
	$\alpha = -06^\circ$										$\delta = 10^\circ$									
1	.311	.354	.173	.155		.202	.250				-.051		-.277		.035	.117	.094	-.162		1
2	.189	.196	.223	.895	-.071	-.118	-.039				-.035	-.058	-.098		.083	.073	1.743			2
3	.127	.139		.156	-.053		-.321				-.037		-.036	-.112	.071	.005				3
4	.130	.106	.280	.038	.040	.004	-.230				-.073	-.049	-.203	-.188	.016	-.158				4
5	.116	.104	.153	-.110	.001	1.749					-.044	-.008	-.152	-.175	-.142					5
6	.100	.265	.070	-.082	-.152						-.057	-.090	-.189	-.182	-.148					6
7	.148	.156	-.109	-.089							-.031	-.250	-.183							7
8	.236	-.051	-.106								-.156	-.262	-.175							8
9	.018	-.056	-.110								-.115	-.215								9
10	.033	-.057									-.213									10
11	-.044																			11

[redacted]

Table 11 Continued

Pressure Coefficients on Delta Wing with Control

Configuration E2 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = -06°									δ = 20°									
1	.308	.352	.169	.152		.214	.033			-.050		-.271		.241	.350	.347	.050		1
2	.189	.195	.223	.906	-.242	-.270	-.257			-.033	-.038	-.090		.240	.285	1.754			2
3	.125	.139		.161	-.100		-.321			-.027		-.032	-.097	.290	.195				3
4	.125	.105	.281	.039	-.070	-.197	-.333			-.063	-.048	-.195	-.160	.188	-.051				4
5	.117	.106	.156	-.105	-.080	1.757				-.035	-.006	-.154	-.157	-.060					5
6	.100	.267	.073	-.082	-.221					-.050	-.082	-.189	-.167	-.060					6
7	.152	.158	-.108	-.089						-.025	-.240	-.158							7
8	.236	-.047	-.105							-.154	-.258	-.143							8
9	.019	-.052	-.104							-.106	-.210								9
10	.033	-.057								-.206									10
11	-.040																		11
	α = -06°									δ = 30°									
1	.306	.352	.196	.150		.201	-.159			-.058		-.286		.535	.600	.533	.297		1
2	.191	.198	.227	.906	-.337	-.353	-.354			-.041	-.044	-.097		.491	.525	1.746			2
3	.128	.140		.158	-.183		-.348			-.035		-.044	-.091	.528	.426				3
4	.129	.109	.282	.037	-.166	-.326	-.391			-.069		-.208	-.164	.407	.101				4
5	.117	.106	.157	-.112	-.162	1.747				-.046	-.012	-.168	-.154	.091					5
6	.104	.271	.072	-.093	-.290					-.060	-.096	-.191	-.166	.015					6
7	.156	.163	-.110	-.103						-.035	-.257	-.138							7
8	.240	-.044	-.108							-.159	-.266	-.136							8
9	.022	-.051	-.112							-.110	-.121								9
10	.034	-.058								-.213									10
11	-.037																		11
	α = -12°									δ = -30°									
1	.174	.235	.012	-.093		.000	-.356			-.252		-.430		-.407	-.387	-.407	-.348		1
2	.331	.345	.371	1.190	1.188	1.126	.900			-.099	-.156	-.337		-.383	-.382	1.753			2
3	.245	.240		.341	.528		.496			-.094		-.155	-.265	-.354	-.407				3
4	.254	.230	.462	.324	.728	.884	.671			-.131	-.128	-.239	-.211	-.353	-.392				4
5	.230	.224	.306	.160	.718	1.763				-.103	-.082	-.304	-.194	-.385					5
6	.226	.404	.270	.189	.668					-.120	-.163	-.367	-.067	-.360					6
7	.421	.331	.184	.242						-.068	-.282	-.333							7
8	.356	.080	.205							-.173	-.295	-.142							8
9	.104	.157	.205							-.149	-.295								9
10	.112	.181								-.205									10
11	.061																		11
	α = -12°									δ = -20°									
1	.170	.234	.017	-.100		.037	-.341			-.250		-.427		-.409	-.384	-.418	-.366		1
2	.335	.343	.374	1.190	.711	.818	.669			-.103	-.155	-.339		-.367	-.388	1.760			2
3	.243	.235		.340	.807		.293			-.103		-.152	-.269	-.300	-.409				3
4	.249	.228	.461	.234	.862	.632	.428			-.138	-.140	-.240	-.223	-.305	-.398				4
5	.228	.225	.306	.088	.752	1.755				-.099	-.090	-.300	-.202	-.375					5
6	.223	.402	.204	.125	.405					-.127	-.162	-.386	-.091	-.335					6
7	.421	.326	.100	.174						-.071	-.282	-.350							7
8	.355	.060	.125							-.178	-.297	-.174							8
9	.105	.053	.124							-.154	-.320								9
10	.108	.094								-.231									10
11	.038																		11
	α = -12°									δ = -10°									
1	.167	.233	.017	1.186		.066	-.243			-.258		-.446		-.355	-.361	-.412	-.401		1
2	.331	.344	.374	.335	.376	.626	.559			-.120	-.167	-.346		-.272	-.356	1.752			2
3	.246	.239		.169	.388		.141			-.118		-.162	-.281	-.218	-.367				3
4	.250	.232	.459	1.725	.587	.485	.201			-.148	-.154	-.252	-.239	-.231	-.395				4
5	.227	.226	.311	.017	.467	1.749				-.119	-.103	-.318	-.214	-.324					5
6	.221	.405	.205	.058	.192					-.137	-.180	-.398	-.122	-.320					6
7	.418	.326	.053	.107						-.086	-.297	-.360							7
8	.358	.064	.077							-.199	-.313	-.212							8
9	.102	.038	-.094							-.163	-.328								9
10	.105	.026								-.246									10
11	.042																		11

Table 11 Concluded

Pressure Coefficients on Delta Wing with Control

Configuration E2 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = -12°									δ = 00°									
1	.167	.225	.009	-.114		.211	-.115										-.392		1
2	.334	.346	.374	1.188	.124	.389	.404			-.271		-.460		-.339	-.305	-.362			2
3	.249	.247		.338	.131		-.172			-.123	-.161	-.369		-.180	-.293	1.750			3
4	.253	.232	.458	.174	.359	.298	.017			-.115		-.206	-.297	-.157	-.221				4
5	.229	.226	.311	-.024	.256	1.750				-.157	-.165	-.267	-.248	-.180	-.324				5
6	.224	.408	.213	.010	.021					-.127	-.111	-.324	-.233	-.293					6
7	.425	.328	.031	.052						-.127	-.195	-.407	-.157	-.301					7
8	.358	.064	.020							-.096	-.316	-.377							8
9	.107	.042	.029							-.206	-.328	-.233							9
10	.106	.031								-.165	-.343								10
11	.049									-.263									11
	α = -12°									δ = 10°									
1	.170	.234	.019	-.104		.211	.222										-.312		1
2	.337	.356	.385	1.200	-.043	.150	.196			-.267		-.453		-.168	-.093	-.111			2
3	.251	.256		.350	.002		-.252			-.119	-.161	-.369		-.108	-.062	1.754			3
4	.258	.241	.467	.187	.135	.105	-.142			-.115		-.199	-.290	-.055	-.051				4
5	.236	.236	.324	-.013	.082	1.754				-.153	-.161	-.263	-.244	-.089	-.237				5
6	.230	.420	.224	.002	-.104					-.123	-.111	-.320	-.225	-.225					6
7	.434	.338	.044	.033						-.123	-.191	-.407	-.161	-.237					7
8	.365	.074	.033							-.085	-.312	-.365							8
9	.113	.051	.034							-.202	-.320	-.233							9
10	.108	.041								-.161	-.335								10
11	.053									-.259									11
	α = -12°									δ = 20°									
1	.166	.228	.015	-.112		.204	.186										-.099		1
2	.333	.348	.377	1.195	-.211	-.108	-.223			-.253		-.439		.108	.165	.203			2
3	.246	.245		.340	-.022		-.306			-.112	-.158	-.352		-.022	.149	1.751			3
4	.256	.235	.461	.180	-.010	-.049	-.259			-.106		-.165	-.277	.134	.077				4
5	.230	.230	.317	-.014	-.050	1.753				-.140	-.151	-.250	-.223	.074	-.158				5
6	.227	.412	.216	.012	-.187					-.113	-.099	-.313	-.202	-.139					6
7	.431	.331	.035	.040						-.130	-.182	-.395	-.146	-.158					7
8	.363	.068	.027							-.083	-.293	-.357							8
9	.108	.044	.022							-.191	-.308	-.205							9
10	.103	.035								-.148	-.322								10
11	.050									-.242									11
	α = -12°									δ = 30°									
1	.173	.239	.020	-.103		.213	-.067										.119		1
2	.339	.358	.385	1.203	-.326	-.303	-.335			-.261		-.439		.407	.409	.395			2
3	.252	.259		.346	-.099		-.329			-.112	-.154	-.350		.184	.390	1.745			3
4	.263	.246	.469	.193	-.124	-.281	-.371			-.102		-.169	-.276	.364	.240				4
5	.239	.239	.323	-.015	-.145	1.749				-.143	-.151	-.250	-.212	.263	-.032				5
6	.234	.423	.226	.011	-.260					-.114	-.095	-.308	-.187	-.032					6
7	.439	.341	.044	.037						-.130	-.175	-.390	-.134	-.094					7
8	.368	.075	.037							-.080	-.295	-.350							8
9	.113	.056	.033							-.201	-.307	-.175							9
10	.109	.041								-.144	-.320								10
11	.059									-.242									11

[redacted]

Table 12

Pressure Coefficients on Delta Wing with Control

Configuration E3 M = 1.61 R = 4.2 x 10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 00°									δ = -30°									
1	.384	.340	.286	.266		-.011	-.339			.084		.052		-.422	-.404	-.413	-.361		1
2	.064	.039	.029	.420	.797	.725	.674			.050	.028	.016		-.297	-.419	1.730			2
3	.032	.022		-.002	.765		.125			.045		.097	-.273	-.235	-.432				3
4	.042	.007	.072	.068	.682	.557	.314			.016	.016	-.001	-.335	-.244	-.404				4
5	.012	.009	.006	-.229	.312	1.732				.035	.098	-.067	-.208	-.316					5
6	.017	.110	.171	-.259	.175					.034	.035	-.229	-.150	-.360					6
7	.033	.024	-.022	-.270						.072	-.153	-.241							7
8	.056	-.161	-.033							-.065	-.163	-.237							8
9	-.087	-.017	-.091							-.042	-.175								9
10	-.041	-.004								-.126									10
11	-.135																		11
	α = 00°									δ = -20°									
1	.381	.333	.279	.262		.126	-.207			.077		.044		-.346	-.361	-.393	-.395		1
2	.056	.033	.023	.417	.471	.507	.487			.045	.024	.008		-.204	-.378	1.722			2
3	.025	.012		-.007	.441		-.021			.040		.087	-.156	-.166	-.376				3
4	.036	.000	.064	.064	.423	.285	.072			.010	.011	-.011	-.208	-.141	-.348				4
5	.007	.005	-.002	-.162	.138	1.727				.030	.089	-.051	-.186	-.259					5
6	.015	.106	.067	-.186	.014					.028	.029	-.215	-.180	-.279					6
7	.029	.016	-.054	-.175						.065	-.162	-.219							7
8	.051	-.182	-.068							-.075	-.162	-.205							8
9	-.094	-.095	-.087							-.053	-.165								9
10	-.051	-.056								-.141									10
11	-.152																		11
	α = 00°									δ = -10°									
1	.384	.335	.281	.262		.249	.043			.076		.053		-.103	-.260	-.316	-.359		1
2	.058	.032	.024	.420	.216	.276	.298			.040	.023	.013		-.106	-.253	1.727			2
3	.026	.016		-.007	.196		-.055			.039		.094	-.068	-.131	-.129				3
4	.032	.001	.065	.044	.204	.131	-.087			.011	.015	-.003	-.157	-.062	-.237				4
5	.007	.002	-.001	-.134	.057	1.727				.026	.093	-.028	-.165	-.191					5
6	.014	.105	-.004	-.141	-.091					.024	.032	-.181	-.160	-.185					6
7	.031	.020	-.103	-.143						.065	-.156	-.172							7
8	.057	-.180	-.105							-.076	-.147	-.167							8
9	-.092	-.158	-.112							-.050	-.147								9
10	-.048	-.112								-.144									10
11	-.149																		11
	α = 00°									δ = 00°									
1	.381	.337	.281	.264		.332	.288			.080		.049		.033	.014	.004	-.255		1
2	.056	.035	.026	.424	.036	.033	.053			.044	.028	.014		.013	-.016	1.722			2
3	.023	.015		-.005	.023		-.020			.043		.091	.003	-.033	-.025				3
4	.029	.002	.069	.003	.002	-.004	-.187			.010	.015	-.004	-.136	.006	-.176				4
5	.004	.004	-.001	-.147	.003	1.727				.034	.093	-.011	-.134	-.142					5
6	.009	.109	-.024	-.126	-.153					.031	.032	-.145	-.134	-.128					6
7	.030	.020	-.153	-.132						.063	-.159	-.136							7
8	.057	-.175	-.143							-.072	-.145	-.131							8
9	-.094	-.162	-.144							-.044	-.132								9
10	-.052	-.145								-.141									10
11	-.151																		11
	α = 00°									δ = 20°									
1	.385	.340	.282	.270		.418	-.067			.075		.040		.453	.461	.437	.164		1
2	.060	.042	.029	.440	-.240	-.277	-.272			.038	.023	.006		.439	.411	1.725			2
3	.029	.021		-.001	-.174		.091			.045		.075	.061	.379	.267				3
4	.038	.006	.073	-.155	-.130	-.248	-.329			.004	.011	-.012	-.152	.123	.027				4
5	.015	.009	.003	-.227	-.108	1.727				.027	.085	.080	-.191	.021					5
6	.008	.112	-.055	-.184	-.243					.022	.024	-.052	-.189	.050					6
7	.035	.024	-.219	-.177						.057	-.166	-.062							7
8	.067	-.177	-.219							-.079	-.082	-.080							8
9	.243	-.170	-.216							-.049	-.047								9
10	-.046	-.170								-.146									10
11	-.142																		11

[redacted]

Table 12 Continued

Pressure Coefficients on Delta Wing with Control

Configuration E3 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 00°									δ = 30°									
1	.384	.338	.281	.270		.292	-.217			.071		.035		.773	.696	.635	.467		1
2	.059	.038	.029	.445	-.330	-.354	-.345			.035	.017	.003		.741	.604	1.725			2
3	.027	.020		-.004	-.274		-.017			.040		.072	.061	.643	.486				3
4	.032	.006	.073	-.279	-.201	-.332	-.364			-.001	.006	-.016	-.222	.219	.257				4
5	.011	.007	.006	-.341	-.208	1.724				.024	.082	.175	-.290	.182					5
6	.006	.114	-.073	-.193	-.298					.017	.022	-.022	-.289	.258					6
7	.033	.020	-.240	-.164						.054	-.163	-.039							7
8	.066	-.177	-.253							-.084	-.018	-.084							8
9	.240	-.182	-.251							-.049	-.003								9
10	-.049	-.187								-.135									10
11	-.144																		11
	α = 06°									δ = -30°									
1	.332	.086	.143	.007		.025	-.266			.211		.241		-.398	-.358	-.389	-.400		1
2	-.082	-.258	-.327	-.147	.559	.623	.514			.142	.161	.160		-.135	-.388	1.733			2
3	-.062	-.082		-.229	.503		-.044			.151		.290	-.180	-.168	-.413				3
4	-.046	-.092	-.069	-.077	.562	.248	.092			.115	.125	.129	-.280	-.178	-.351				4
5	-.086	-.091	-.213	-.241	-.149	1.733				.139	.257	.013	-.253	-.275					5
6	-.068	-.006	-.012	-.227	-.105					.139	.145	-.183	-.222	-.303					6
7	-.053	-.112	-.091	-.250						.252	-.056	-.198							7
8	-.049	-.276	-.144							.023	-.065	-.186							8
9	.204	-.161	-.175							.007	-.094								9
10	-.125	-.099								-.059									10
11	-.220																		11
	α = 06°									δ = -20°									
1	.331	.085	.144	.012		.144	-.062			.206		.241		-.302	-.273	-.304	-.367		1
2	-.082	-.254	-.324	-.140	.239	.369	.317			.138	.158	.157		-.105	-.281	1.732			2
3	-.063	-.081		-.229	.225		-.127			.147		.285	-.077	-.080	-.220				3
4	-.046	-.086	-.069	-.076	.307	.062	-.090			.113	.116	.130	-.152	-.087	-.239				4
5	-.086	-.091	-.212	-.205	-.145	1.734				.114	.250	.022	-.142	-.220					5
6	-.068	.000	-.088	-.207	-.163					.132	.135	-.165	-.142	-.229					6
7	-.056	-.108	-.125	-.212						.249	-.062	-.163							7
8	-.049	-.273	-.156							.018	-.062	-.148							8
9	.204	-.292	-.177							.006	-.090								9
10	-.133	-.133								-.062									10
11	-.222																		11
	α = 06°									δ = -10°									
1	.332	.085	.144	.010		.204	.254			.203		.239		-.074	-.048	-.019	-.242		1
2	-.084	-.251	-.326	-.137	-.013	.080	.092			.142	.156	.157		-.077	.038	1.731			2
3	-.064	-.082		-.231	.038		-.149			.146		.289	.029	.033	-.008				3
4	-.051	-.090	-.069	-.092	.095	-.078	-.241			.113	.116	.134	-.084	.023	-.172				4
5	-.090	-.091	-.212	-.211	-.113	1.734				.114	.251	.041	-.097	-.156					5
6	-.073	.000	-.170	-.191	-.194					.130	.140	-.127	-.097	-.158					6
7	-.054	-.109	-.167	-.194						.245	-.059	-.108							7
8	-.048	-.274	-.177							.023	-.055	-.098							8
9	.202	-.296	-.190							.011	-.081								9
10	-.135	-.212								-.058									10
11	-.223																		11
	α = 06°									δ = 00°									
1	.341	.095	.146	.015		.146	.174			.213		.242		.094	.211	.227	-.084		1
2	-.067	-.243	-.318	-.131	-.092	-.219	-.281			.144	.159	.161		.068	.200	1.733			2
3	-.050	-.073		-.227	-.068		-.101			.156		.287	.120	.172	.115				3
4	-.035	-.085	-.064	-.122	-.045	-.148	-.289			.120	.122	.139	-.048	.122	-.084				4
5	-.079	-.084	-.210	-.232	-.133	1.730				.123	.253	.056	-.053	-.057					5
6	-.059	.004	-.202	-.213	-.224					.135	.143	-.065	-.047	-.039					6
7	-.043	-.101	-.189	-.218						.245	-.060	-.059							7
8	-.037	-.265	-.199							.026	-.048	-.052							8
9	.202	-.290	-.207							.016	-.052								9
10	-.127	-.257								-.059									10
11	-.213																		11

[redacted]

Table 12 Continued

Pressure Coefficients on Delta Wing with Control

Configuration E3 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 06°									δ = 20°									
1	.334	.083	.144	.007		.154	-.223										.407		1
2	-.081	-.264	-.328	-.146	-.346	-.391	-.388			.212		.247		.607	.673	.589			2
3	-.061	-.077		-.245	-.303		-.161			.151	.161	.162		.585	.567	1.728			3
4	-.046	-.089	-.061	-.207	-.267	-.356	-.388			.161		.297	.217	.628	.515				4
5	-.084	-.088	-.209	-.283	-.221	1.732				.114	.125	.141	-.061	.335	.261				5
6	-.076	.002	-.245	-.221	-.308					.137	.257	.220	-.192	.190					6
7	-.051	-.105	-.219	-.198						.140	.142	.053	-.208	.214					7
8	-.045	-.268	-.237							.255	-.056	.039							8
9	.222	-.289	-.250							.027	.070	.015							9
10	-.147	-.270								.025	.073								10
11	-.220									-.059									11
	α = 12°									δ = -30°									
1	.224	-.095	-.012	-.170		.094	-.174										-.389		1
2	-.269	-.416	-.455	-.424	.425	.442	.398			.344		.388		-.317	-.284	-.341			2
3	-.118	-.171		-.457	.194		-.126			.273	.279	.290		-.080	-.326	1.733			3
4	-.099	-.169	-.175	-.348	.322	.135	-.058			.275		.462	-.127	-.144	-.248				4
5	-.150	-.172	-.267	-.321	-.174	1.737				.239	.240	.251	-.240	-.177	-.277				5
6	-.130	-.103	-.343	-.288	-.389					.238	.371	.113	-.199	-.296					6
7	-.118	-.184	-.151	-.295						.414	.295	-.081	-.151	-.321					7
8	-.091	-.313	-.192							.348	.026	-.092							8
9	.196	-.326	-.233							.087	-.003	-.095							9
10	-.163	-.220								.050	-.035								10
11	-.245									.007									11
	α = 12°									δ = -20°									
1	.222	-.097	-.012	-.172		.188	.158										-.321		1
2	-.269	-.426	-.465	-.416	.099	.165	.231			.339		.390		-.168	-.092	-.124			2
3	-.123	-.178		-.461	-.033		-.200			.271	.274	.291		.004	-.036	1.736			3
4	-.104	-.167	-.175	-.326	.127	.025	-.189			.273		.462	.000	-.017	-.049				4
5	-.156	-.175	-.266	-.309	-.255	1.736				.234	.244	.254	-.114	-.051	-.209				5
6	-.135	-.101	-.340	-.260	-.369					.234	.371	.122	-.087	-.205					6
7	-.122	-.191	-.265	-.247						.407	.296	-.066	-.075	-.225					7
8	-.094	-.316	-.190							.348	.030	-.055							8
9	.191	-.333	-.215							.086	.000	-.051							9
10	-.173	-.343								.053	-.030								10
11	-.254									.005									11
	α = 12°									δ = -10°									
1	.223	-.090	-.011	-.168		.174	.207										-.105		1
2	-.270	-.415	-.461	-.416	-.186	-.141	-.180			.343		.395		-.039	.214	.187			2
3	-.121	-.172		-.461	-.113		-.213			.273	.278	.293		-.002	.161	1.738			3
4	-.103	-.169	-.174	-.316	-.028	-.080	-.290			.278		.469	.116	.138	.093				4
5	-.150	-.173	-.269	-.294	-.293	1.738				.242	.247	.261	-.015	.079	-.093				5
6	-.129	-.103	-.344	-.227	-.323					.237	.373	.132	-.028	-.122					6
7	-.118	-.186	-.312	-.214						.407	.297	-.017	-.017	-.112					7
8	-.090	-.313	-.217							.352	.035	.001							8
9	.197	-.329	-.223							.085	.011	.002							9
10	-.171	-.337								.056	-.015								10
11	-.249									.008									11
	α = 12°									δ = 00°									
1	.220	-.098	-.011	-.169		.088	-.039										.069		1
2	-.266	-.424	-.459	-.407	-.275	-.321	-.338			.341		.385		.122	.425	.352			2
3	-.120	-.175		-.460	-.172		-.189			.270	.278	.290		.117	.331	1.736			3
4	-.102	-.172	-.175	-.318	-.129	-.194	-.359			.277		.466	.213	.340	.242				4
5	-.154	-.178	-.269	-.359	-.280	1.737				.238	.240	.259	.030	.205	.028				5
6	-.132	-.105	-.339	-.295	-.277					.234	.368	.148	.050	.034					6
7	-.122	-.190	-.378	-.261						.401	.291	.048	.063	.045					7
8	-.095	-.321	-.246							.347	.030	.057							8
9	.189	-.330	-.235							.087	.013	.059							9
10	-.182	-.338								.057	.030								10
11	-.253									.008									11

[redacted]

Table 12 Continued

Pressure Coefficients on Delta Wing with Control

Configuration E3 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
								α = 12°					δ = 20°							
1	.218	-.100	-.015	-.172		.044	-.295				.341		.387		.667	.759		.586		1
2	-.272	-.418	-.458	-.418	-.390	-.422	-.413				.273	.275	.289		.753	.723	.636			2
3	-.121	-.177		-.466	-.372		-.244				.278		.464	.388	.761	.617	1.726			3
4	-.105	-.174	-.181	-.278	-.318	-.393	-.407				.244	.242	.258	.006	.486	.505				4
5	-.154	-.170	-.281	-.311	-.346	1.730					.235	.370	.359	-.138	.259					5
6	-.134	-.107	-.337	-.235	-.392						.402	.295	.201	-.125	.292					6
7	-.126	-.192	-.409	-.244							.348	.069	.152							7
8	-.098	-.325	-.271								.089	.171	.112							8
9	.210	-.337	-.226								.058	.156								9
10	-.189	-.340									.023									10
11	-.250																			11
								α = -06°					δ = -30°							
1	.310	.349	.168	.158		-.095	-.376				-.055		-.278		-.448	-.419	-.426	-.361		1
2	.194	.193	.220	.865	1.009	.856	.734				-.037	-.076	-.097		-.379	-.435	1.738			2
3	.127	.140		.152	.946		.295				-.042		-.049	-.381	-.385	-.452				3
4	.130	.107	.279	.261	.895	.685	.503				-.073	-.069	-.206	-.268	-.361	-.414				4
5	.118	.112	.136	-.183	.522	1.739					-.050	-.012	-.191	-.217	-.403					5
6	.108	.264	.310	-.271	.340						-.055	-.094	-.253	-.198	-.407					6
7	.145	.133	.116	-.280							-.032	-.251	-.262							7
8	.230	.028	.028								-.158	-.270	-.257							8
9	.241	.134	-.017								-.126	-.180								9
10	.030	.121									-.175									10
11	.007																			11
								α = -06°					δ = -20°							
1	.305	.346	.166	.159		.000	-.314				-.055		-.281		-.416	-.394	-.419	-.395		1
2	.192	.195	.219	.865	.628	.681	.616				-.039	-.073	-.101		-.314	-.413	1.739			2
3	.127	.140		.156	.615		.039				-.041		-.053	-.216	-.294	-.430				3
4	.128	.110	.280	.211	.636	.521	.253				-.072	-.067	-.209	-.276	-.216	-.423				4
5	.120	.111	.133	-.080	.303	1.738					-.050	-.014	-.184	-.225	-.311					5
6	.107	.263	.203	-.182	.166						-.054	-.098	-.229	-.197	-.349					6
7	.146	.133	.039	-.208							-.034	-.252	-.247							7
8	.230	-.075	.036								-.161	-.272	-.238							8
9	.244	.044	-.002								-.128	-.138								9
10	.023	.064									-.216									10
11	-.064																			11
								α = -06°					δ = -10°							
1	.309	.350	.171	.160		.122	-.140				-.054		-.276		-.313	-.312	-.382	-.379		1
2	.196	.196	.226	.865	.321	.499	.442				-.038	-.071	-.093		-.156	-.313	1.737			2
3	.132	.139		.155	.311		-.085				-.039		-.045	-.149	-.172	-.341				3
4	.133	.108	.285	.171	.406	.306	.034				-.073	-.065	-.202	-.232	-.158	-.358				4
5	.124	.114	.138	-.054	.197	1.739					-.048	-.012	-.165	-.223	-.247					5
6	.107	.269	.088	-.075	.011						-.052	-.092	-.205	-.205	-.238					6
7	.153	.139	-.008	-.120							-.033	-.249	-.213							7
8	.238	-.069	-.014								-.160	-.268	-.212							8
9	.241	-.044	-.015								-.120	-.145								9
10	.023	.012									-.217									10
11	-.062																			11
								α = -06°					δ = 00°							
1	.307	.348	.167	.156		.171	.130				-.055		-.285		-.102	-.187	-.279	-.342		1
2	.190	.193	.222	.866	.099	.237	.254				-.037	-.071	-.106		-.072	-.103	1.736			2
3	.129	.135		.152	.081		-.141				-.038		-.053	-.114	-.070	-.188				3
4	.131	.109	.283	.109	.208	.135	-.108				-.071	-.072	-.214	-.224	-.126	-.267				4
5	.118	.109	.135	-.063	.114	1.738					-.049	-.016	-.156	-.219	-.215					5
6	.104	.264	.037	-.051	-.081						-.053	-.099	-.193	-.217	-.208					6
7	.147	.135	-.065	-.059							-.033	-.253	-.200							7
8	.231	-.072	-.065								-.161	-.272	-.199							8
9	.235	-.073	-.059								-.123	-.156								9
10	.013	-.060									-.219									10
11	-.066																			11

[redacted]

Table 12 Continued

Pressure Coefficients on Delta Wing with Control

Configuration E3 M = 1.61 R = 4.2 x 10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = -06°									δ = 20°									
1	.308	.352	.171	.154		.059	.015										.030		1
2	.197	.199	.225	.885	-.310	-.324	-.291			-.062		-.289		.239	.363	.295			2
3	.129	.146		.158	-.101		-.284			-.040	-.063	-.104		.235	.283	1.729			3
4	.132	.111	.285	-.086	-.072	-.161	-.381			-.038		-.053	-.067	.300	.057				4
5	.119	.115	.139	-.159	-.080	1.731				-.075	-.075	-.214	-.196	-.126	-.099				5
6	.103	.279	.015	-.135	-.244					-.050	-.019	-.069	-.210	-.138					6
7	.157	.145	-.165	-.144						-.057	-.101	-.122	-.210	-.130					7
8	.240	-.063	-.158							-.037	-.259	-.146							8
9	.254	-.077	-.149							-.166	-.272	-.165							9
10	.019	-.088								-.120	-.092								10
11	-.060									-.222									11
	α = -06°									δ = 30°									
1	.306	.352	.167	.153		.022	-.144										.242		1
2	.199	.200	.225	.893	-.361	-.369	-.356			-.067		-.294		.533	.596	.468			2
3	.130	.145		.157	-.143		-.320			-.044	-.084	-.107		.493	.457	1.726			3
4	.129	.109	.287	-.195	-.146	-.307	-.414			-.042		-.058	-.078	.526	.221				4
5	.117	.113	.138	-.271	-.156	1.726				-.078	-.079	-.219	-.227	-.162	.029				5
6	.103	.273	.000	-.243	-.277					-.056	-.029	-.007	-.228	-.073					6
7	.160	.145	-.188	-.231						-.059	-.108	-.090	-.243	.010					7
8	.243	-.064	-.200							-.044	-.261	-.135							8
9	.254	-.086	-.188							-.169	-.148	-.162							9
10	.020	-.099								-.125	-.075								10
11	-.058									-.229									11
	α = -12°									δ = -10°									
1	.171	.242	.015	-.079		-.056	-.272										-.407		1
2	.349	.346	.375	1.189	.367	.639	.553			-.261		-.440		-.394	-.414	-.443			2
3	.250	.242		.285	.391		.152			-.112	-.167	-.358		-.279	-.386	1.738			3
4	.252	.234	.457	.296	.547	.472	.183			-.110		-.171	-.265	-.223	-.384				4
5	.228	.229	.251	.041	.327	1.738				-.145	-.156	-.260	-.324	-.302	-.414				5
6	.226	.392	.216	.004	.104					-.116	-.099	-.320	-.285	-.314					6
7	.421	.291	.125	-.011						-.129	-.184	-.395	-.280	-.331					7
8	.337	.022	.120							-.085	-.303	-.243							8
9	.261	.073	.100							-.198	-.312	-.191							9
10	.077	.092								-.166	-.323								10
11	.003									-.253									11
	α = -12°									δ = 00°									
1	.170	.241	.013	-.076		-.033	-.127										-.403		1
2	.352	.345	.375	1.193	.138	.436	.391			-.263		-.437		-.342	-.391	-.434			2
3	.249	.241		.290	.131		.168			-.108	-.156	-.358		-.174	-.293	1.739			3
4	.255	.233	.459	.216	.370	.276	.015			-.109		-.176	-.304	-.170	-.251				4
5	.233	.230	.255	.022	.217	1.739				-.141	-.156	-.265	-.346	-.292	-.387				5
6	.226	.401	.132	.045	.014					-.116	-.103	-.324	-.305	-.288					6
7	.424	.290	.066	.067						-.128	-.184	-.370	-.223	-.317					7
8	.335	.018	.052							-.085	-.305	-.237							8
9	.263	-.001	.060							-.198	-.313	-.216							9
10	.075	.023								-.166	-.329								10
11	.002									-.255									11
	α = -12°									δ = 20°									
1	.165	.237	.015	-.081		.089	.187										-.113		1
2	.334	.352	.380	1.204	-.217	-.042	-.110			-.272		-.446		.090	.160	.186			2
3	.249	.248		.290	.014		-.290			-.114	-.167	-.369		-.025	.138	1.727			3
4	.257	.241	.466	.007	.019	-.033	-.260			-.111		-.184	-.309	.134	.005				4
5	.235	.237	.263	-.115	-.040	1.727				-.149	-.162	-.266	-.294	-.241	-.249				5
6	.227	.405	.119	-.078	-.209					-.124	-.110	-.333	-.266	-.315					6
7	.433	.297	-.054	-.064						-.133	-.187	-.264	-.252	-.314					7
8	.343	.027	-.054							-.088	-.309	-.184							8
9	.275	-.007	-.051							-.205	-.321	-.207							9
10	.081	-.024								-.164	-.318								10
11	.009									-.264									11

[redacted]

Table 12 Concluded

Pressure Coefficients on Delta Wing with Control

Configuration E3 M = 1.61 R = 4.2 x 10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
	$\alpha = -12°$										$\delta = 30°$									
1	.163	.230	.007	-.089		.086	-.006				-.276		-.451		.386	.371	.339	.033		1
2	.330	.342	.374	1.201	-.283	-.203	-.244				-.115	-.183	-.373		.163	.385	1.729			2
3	.248	.241		.285	-.052		-.308				-.110		-.187	-.317	.329	.101				3
4	.251	.233	.461	-.135	-.084	-.136	-.335				-.150	-.165	-.270	-.313	-.206	-.235				4
5	.225	.228	.259	-.255	-.126	1.730					-.124	-.109	-.335	-.299	-.358					5
6	.222	.401	.105	-.189	-.270						-.134	-.190	-.153	-.301	-.332					6
7	.430	.285	-.082								-.095	-.310	-.191							7
8	.337	.017	-.100								-.206	-.324	-.229							8
9	.265	-.015	-.102								-.163	-.148								9
10	.066	-.037									-.265									10
11	.002																			11

[redacted]

Table [13]

Pressure Coefficients on Delta Wing with Control

Configuration [F] $M = 1.61$ $R = 4.2 \times 10^6$

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	$\alpha = 00°$									$\delta = -20°$									
1	.387	.359	.289	.265	.280	.226	-.220	.246									-.383		1
2	.051	.033	.020	.027	.568	.573	1.592			.076		.058		-.331	-.357	-.325			2
3	.024	.015		.129	.444	.524	.140			.040	.023	.017		-.147	.971	-.372			3
4	.027	.002	-.020	-.063	.471	.402	.175			.043		-.007	-.252	-.134	-.387	-.383			4
5	.001	.004	-.019	-.231	.171	.139				.012	.015	.093	-.294	-.255	-.374				5
6	.015	.058	.151	-.220	.219					.023	.039	-.046	-.278	-.271					6
7	.037	.025	-.039	-.218	.094					.022	.075	-.230	-.237	-.289					7
8	-.002	-.101	-.063							.004	-.130	-.256							8
9	-.154	-.056	-.090							-.124	-.151	-.236							9
10	-.069	-.056								-.025	-.175								10
11	-.125									-.103									11
	$\alpha = 00°$									$\delta = 00°$									
1	.378	.353	.277	.231	.331	.237	.311	-.254									-.254		1
2	.046	.028	.016	.014	.055	.055	1.743			.085		.059		.039	.013	.029			2
3	.011	.009		.006	.041	.021	-.194			.036	.028	.015		.008	-.002	-.203			3
4	.021	-.009	-.026	-.026	.001	.011	-.187			.038		.002	-.006	.008	-.010	-.186			4
5	.000	-.007	-.008	-.128	9.745	-.161				-.002	.021	-.013	-.140	-.004	-.177				5
6	.001	.048	.005	-.135	.208					.027	.037	.013	-.139	-.140					6
7	.023	.012	-.155	-.136	-.147					.023	.028	-.135	-.139	-.144					7
8	-.006	-.156	-.158							.008	-.128	-.141							8
9	-.144	-.146	-.162							-.117	-.128	-.141							9
10	-.087	-.156								-.051	-.128								10
11	-.150									-.140									11
	$\alpha = 00°$									$\delta = 10°$									
1	.052	.036	.025	.256	.225	.207	.040	-.351									-.036		1
2	.016	.008	.741	.015	-.037	-.197	9.699			.074		.039		.242	.223	.285			2
3	.026	-.002		-.095	-.031	-.153	-.328			.034	.018	.004		.232	.202	-.067			3
4	.007	-.003	.002	-.106	-.069	-.173	-.300			.045		-.006	.016	.140	.136	-.053			4
5	.007	.059	-.050	-.173	1.743	-.273				-.005	.011	-.036	-.129	.069	-.081				5
6	.033	.033		-.190	.191					.014	.025	.075	-.171	-.055					6
7	-.003	-.151	-.183	-.196	-.214					.014	.013	-.088	-.169	-.079					7
8	-.138	-.169	-.194							.000	-.121	-.099							8
9	-.075	-.180	-.199							-.134	-.102	-.102							9
10	-.142	.285								-.053	-.102								10
11	.355									-.143									11
	$\alpha = 00°$									$\delta = 20°$									
1	.381	.357	.278	.259	.176	.202	-.193	-.366									.232		1
2	.052	.032	.027	.020	-.300	-.305	1.667			.076		.041		.575	.499	.525			2
3	.022	.017		.334	-.098	-.305	-.366			.038	.019	.003		.420	.483	.126			3
4	.026	-.002	-.014	-.256	-.158	-.329	-.360			.049		-.007	-.099	.449	.361	.163			4
5	.013	-.002	.102	-.309	1.738	-.335				.004	.017	-.032	-.237	.194	.093				5
6	.004	.057	-.061	-.275	.206					.017	.030	.149	-.234	.088					6
7	.029	.074	-.249	-.234	-.285					.017	.016	-.034	-.234	.094					7
8	.003	-.142	-.262							.000	-.093	-.053							8
9	-.138	-.170	-.251							-.135	-.045	-.068							9
10	-.049	-.193								-.049	-.057								10
11	-.112									-.131									11
	$\alpha = 00°$									$\delta = 30°$									
1	.380	.354	.282	.258	-.028	.202	-.305	-.360									.512		1
2	.052	.031	.018	.021	-.387	-.368	1.628			.072		.038		.915	.785	.695			2
3	.012	.008		.752	-.220	-.381	-.367			.038	.017	.015		.740	.741	.449			3
4	.025	-.005	-.016	-.365	-.249	-.381	-.396			.053		-.004	-.245	.798	.607	.499			4
5	.011	-.003	.274	-.429	1.743	-.377				-.002	.016	-.034	-.293	.385	.408				5
6	.002	.055	-.046	-.402	.191					.021	.038	.220	-.259	.316					6
7	.034	.135	-.281	-.319	-.332					.021	.023	.017	-.246	.345					7
8	.011	-.113	-.322							-.002	-.014	-.028							8
9	-.072	-.165	-.336							-.142	.002	-.055							9
10	.011	-.201								-.031	-.005								10
11	-.052									.011									11

[redacted]

Table 13 Continued

Pressure Coefficients on Delta Wing with Control

Configuration F M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 06°									δ = -20°									
1	.332	.101	.148	-.015	.281	.230	-.053	.056									-.402		1
2	-.083	-.259	-.324	-.365	.574	.313	1.567			.207		.233		-.349	-.323	-.319			2
3	-.062	-.076		-.273	.296	.188	-.031			.138	.143	.152		-.084	.841	-.387			3
4	-.053	-.094	-.120	-.217	.045	.086	.013			.145		.112	-.141	-.117	-.310	-.385			4
5	-.087	-.094	-.054	-.277	-.048	-.030				.108	.110	.162	-.228	-.210	-.277				5
6	-.074	-.041	.003	-.242	.202					.110	.143	.057	-.222	-.257					6
7	-.050	-.030	-.181	-.290	-.082					.095	.142	-.132	-.208	-.296					7
8	-.077	-.160	-.165							.116	-.078	-.157							8
9	-.200	-.149	-.180							-.055	-.091	-.156							9
10	-.097	-.163								.017	-.101								10
11	-.118									-.059									11
	α = 06°									δ = 00°									
1	.330	.083	.142	-.017	.138	.237	.072	-.369									-.068		1
2	-.094	-.270	-.335	-.375	-.292	-.312	1.579			.211		.254		.256	.212	.237			2
3	-.072	-.084		-.214	-.239	-.290	-.353			.144	.158	.163		.187	.170	-.059			3
4	-.053	-.099	-.116	-.148	-.160	-.271	-.368			.161		.116	.108	.149	.134	-.047			4
5	-.086	-.097	-.097	-.222	1.743	-.277				.110	.122	.106	-.047	.132	-.042				5
6	-.079	-.049	-.093	-.223	.214					.123	.153	.129	-.040	-.034					6
7	-.052	-.058	-.218	-.225	-.242					.108	.124	-.065	-.049	-.036					7
8	-.083	-.206	-.225							.116	-.049	-.063							8
9	-.204	-.210	-.219							-.049	-.049	-.059							9
10	-.146	-.212								.019	-.055								10
11	-.181									-.066									11
	α = 06°									δ = 10°									
1	.332	.093	.142	-.019	.201	.220	-.160	-.387									.150		1
2	-.089	-.271	-.335	-.358	-.343	-.366	1.536			.221		.247		.495	.445	.443			2
3	-.071	-.082		-.437	-.310	-.366	-.382			.161	.166	.159		.470	.402	.074			3
4	-.053	-.096	-.111	-.159	-.179	-.344	-.387			.161		.124	.202	.383	.321	.104			4
5	-.082	-.100	-.073	-.216	1.747	-.367				.112	.134	.063	-.003	.288	.066				5
6	-.076	-.032	-.169	-.215	.214					.134	.159	.208	-.045	.089					6
7	-.047	-.042	-.252	-.207	-.263					.117	.117	.015	-.137	.064					7
8	-.076	-.209	-.264							.109	-.036	.006							8
9	-.178	-.238	-.250							-.055	-.007	-.008							9
10	-.119	-.257								.016	-.007								10
11	-.166									-.074									11
	α = 06°									δ = 20°									
1	.330	.091	.146	-.016	.159	.220	-.300	-.386									.408		1
2	-.086	-.269	-.334	-.302	-.397	-.411	1.455			.216		.245		.682	.738	.629			2
3	-.070	-.083		.398	-.358	-.401	-.376			.149	.155	.161		.521	.683	.334			3
4	-.056	-.095	-.065	-.310	-.277	-.394	-.393			.153		.121	.208	.847	.544	.385			4
5	-.086	-.097	.019	-.383	.210	-.394				.107	.126	.059	-.033	.518	.315				5
6	-.079	.025	-.160	-.360	.210					.127	.144	.296	-.175	.315					6
7	-.047	-.003	-.318	-.261	-.319					.115	.108	.093	-.141	.277					7
8	-.038	-.214	-.343							.102	-.004	.039							8
9	-.115	-.244	-.321							-.052	.053	.045							9
10	-.077	-.248								.010	.053								10
11	-.141									-.053									11
	α = 06°									δ = 30°									
1	.324	.084	.132	-.027	-.041	.224	-.344	-.388									.615		1
2	-.089	-.275	-.344	-.194	-.425	-.424	1.344			.218		.249		1.088	.987	.790			2
3	-.071	-.088		.262	-.378	-.422	-.376			.147	.161	.159		.909	.976	.718			3
4	-.061	-.097	.012	-.301	-.335	-.406	-.405			.159		.118	.181	.978	.693	.659			4
5	-.092	-.104	.092	-.347	-.206	-.405				.112	.122	.079	-.103	.771	.663				5
6	-.085	.134	-.202	-.323	.211					.128	.158	.355	-.214	.631					6
7	-.056	.029	-.331	-.325	-.378					.123	.158	.122	-.117	.559					7
8	.109	-.209	-.366							.092	.089	.092							8
9	-.019	-.240	-.348							-.053	.101	.077							9
10	-.041	-.242								.075	.086								10
11	-.098									.075									11

[redacted]

Table 13 Continued

Pressure Coefficients on Delta Wing with Control

Configuration F M = 1.61 R = 4.2 x 10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 12°									δ = -20°									
1	.207	-.100	-.021	-.197	.301	.215	.076	-.153		.345		.402		.006	-.160	-.108	-.317		1
2	-.284	-.422	-.474	-.493	.599	.169	1.469			.277	.278	.290		.028	.668	-.218			2
3	-.136	-.185		-.498	.319	.012	-.177			.271		.257	-.051	-.044	.004	-.196			3
4	-.116	-.179	-.215	-.403	-.038	-.110	-.214			.234	.248	.281	-.174	-.184	-.183				4
5	-.153	-.194	-.116	-.367	-.301	-.290				.236	.277	.202	-.145	-.243					5
6	-.138	-.163	-.125	-.319	.186					.217	.248	-.027	-.142	-.216					6
7	-.133	-.089	-.270	-.305	-.312					.249	.021	-.072							7
8	-.138	-.215	-.297							.057	.014	-.076							8
9	-.246	-.220	-.310							.072	.001								9
10	-.141	-.233								.031									10
11	-.138																		11
	α = 12°									δ = 00°									
1	.197	-.111	-.030	-.209	-.011	.219	-.209	-.414		.345		.402		.388	.335	.366	.065		1
2	-.297	-.431	-.471	-.482	-.430	-.440	1.187			.277	.281	.288		.319	.307	.042			2
3	-.138	-.191		-.457	-.390	-.428	-.400			.277		.258	.237	.290	.257	.063			3
4	-.115	-.187	-.227	-.373	-.355	-.406	-.413			.245	.251	.243	.049	.260	.055				4
5	-.163	-.200	-.183	-.375	-.276	-.394				.247	.281	.253	.049	.070					5
6	-.143	-.169	-.165	-.354	.202					.208	.239	.036	.038	.055					6
7	-.138	-.129	-.274	-.365	-.332					.231	.025	.028							7
8	-.145	-.271	-.275							.048	.045	.035							8
9	-.260	-.257	-.276							.081	.044								9
10	-.205	-.269								.030									10
11	-.223																		11
	α = 12°									δ = 10°									
1	.197	-.111	-.030	-.210	.152	.212	-.307	-.377		.343		.397		.728	.596	.553	.292		1
2	-.305	-.434	-.475	-.472	-.445	-.428	1.072			.275	.281	.292		.654	.566	.236			2
3	-.142	-.192		-.479	-.408	-.421	-.366			.279		.257	.392	.522	.451	.290			3
4	-.120	-.191	-.198	-.372	-.392	-.397	-.397			.225	.244	.187	.149	.446	.241				4
5	-.165	-.197	-.163	-.362	-.329	-.384				.232	.275	.343	.068	.232					5
6	-.145	-.102	-.275	-.269	.195					.206	.219	.110	-.034	.220					6
7	-.136	-.086	-.326	-.286	-.379					.219	.055	.097							7
8	-.125	-.285	-.305							.028	.082	.100							8
9	-.220	-.308	-.278							.065	.098								9
10	-.148	-.319								.020									10
11	-.189																		11
	α = 12°									δ = 20°									
1	.196	-.108	-.029	-.203	.014	.222	-.364	-.380		.345		.393		.916	.890	.669	.547		1
2	-.302	-.436	-.458	-.293	-.429	-.429	.967			.274	.276	.285		.765	.852	.599			2
3	-.136	-.197		.370	-.429	-.424	-.371			.276		.244	.454	.971	.623	.572			3
4	-.113	-.189	-.068	-.401	-.419	-.407	-.398			.237	.246	.177	.150	.712	.542				4
5	-.167	-.162	-.169	-.318	-.371	-.401				.241	.275	.429	-.105	.518					5
6	-.145	-.025	-.287	-.206	.201					.196	.231	.188	-.127	.483					6
7	-.107	-.095	-.376	-.127	-.393					.206	.105	.153							7
8	-.038	-.257	-.347							.022	.147	.163							8
9	-.145	-.300	-.187							.073	.147								9
10	-.124	-.312								.073									10
11	-.172																		11
	α = 12°									δ = 30°									
1	.204	-.107	-.028	-.191	-.136	.231	-.390	-.367		.338		.398		1.197	1.130	.922	.682		1
2	-.297	-.433	-.346	-.201	-.431	-.420	.897			.277	.286	.289		1.024	.025	.870			2
3	-.133	-.173		.409	-.412	-.412	-.370			.285		.250	.414	9.147	.903	.723			3
4	-.115	-.143	-.117	-.320	-.411	-.405	-.388			.242	.246	.194	.062	.971	.778				4
5	-.162	-.127	-.090	-.343	-.390	-.404				.242	.272	.481	-.124	.822					5
6	-.117	.105	-.250	-.310	.206					.220	.303	.253	-.151	.669					6
7	.011	-.023	-.343	-.280	-.407					.219	.179	.209							7
8	.075	-.205	-.320							.024	.228	.167							8
9	-.080	-.246	-.318							.177	.197								9
10	-.095	-.233								.210									10
11	-.170																		11

[redacted]

Table 13 Continued

Pressure Coefficients on Delta Wing with Control

Configuration F M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
	α = −06°										δ = −20°									
1	.307	.391	.171	.155	.273	.269	−.257	.386										−.376		1
2	.176	.190	.211	.229	.546	.768	1.414				−.055		−.291		−.300	−.374	−.319			2
3	.120	.136		.130	.546	.698	.317				−.042	−.084	−.117		−.271	.574	−.338			3
4	.120	.094	.104	.175	.851	.585	.338				−.043		−.058	−.319	−.269	−.317	−.346			4
5	.115	.100	.081	−.080	−.025	.317					−.083	−.076	.015	−.402	−.300	−.345				5
6	.102	.161	.281	−.196	.254						−.060	−.015	−.174	−.393	−.271					6
7	.132	.107	.083	−.130	.221						−.060	.002	−.300	−.292	−.311					7
8	.096	−.021	.036								−.042	−.192	−.339							8
9	−.084	.035	.014								−.105	−.233	−.315							9
10	−.004	.037									−.044	−.239								10
11	−.066										−.134									11
	α = −06°										δ = 00°									
1	.293	.385	.158	.132	.229	.302	.021	−.142										−.229		1
2	.179	.200	.219	.238	.240	.236	.807				−.067		−.293		−.142	−.214	−.155			2
3	.123	.138		.133	.152	.151	−.099				−.044	−.077	−.108		−.142	−.199	−.179			3
4	.124	.093	.111	.111	.126	.133	−.170				−.050		−.105	−.129	−.108	−.172	−.203			4
5	.102	.106	.130	−.029	.005	−.082					−.076	−.077	−.104	−.227	−.073	−.152				5
6	.113	.172	.115	−.037	.277						−.059	−.057	−.071	−.227	−.174					6
7	.130	.129	−.069	−.044	−.116						−.059	−.058	−.212	−.219	−.131					7
8	.099	−.064	−.072								−.077	−.191	−.212							8
9	−.070	−.071	−.069								−.189	−.191	−.201							9
10	−.002	−.069									−.109	−.191								10
11	−.069										−.171									11
	α = −06°										δ = 10°									
1	.292	.384	.156	.134	.284	.292	.253	−.236										−.238		1
2	.185	.201	.225	.240	.128	.056	.744				−.074		−.297		.141	−.037	.008			2
3	.124	.137		.128	.103	.054	−.173				−.047	−.084	−.117		−.098	−.088	−.225			3
4	.126	.102	.114	−.018	.052	.039	−.173				−.051		−.111	−.178	−.208	−.142	−.225			4
5	.109	.111	.117	−.116	−.016	−.140					−.070	−.080	−.069	−.250	−.120	−.206				5
6	.111	.176	.089	−.131	.273						−.066	−.063	−.067	−.223	−.193					6
7	.127	.127	−.113	−.127	−.185						−.055	−.029	−.199	−.228	−.189					7
8	.108	−.076	−.122								−.074	−.173	−.199							8
9	−.063	−.080	−.125								−.188	−.181	−.188							9
10	−.002	−.090									−.108	−.194								10
11	−.065										−.146									11
	α = −06°										δ = 20°									
1	.292	.389	.154	.136	.186	.286	−.002	−.330										−.019		1
2	.187	.195	.228	.245	.034	−.186	.671				−.071		−.303		.538	.232	.264			2
3	.126	.142		.243	−.004	−.178	−.286				−.052	−.084	−.111		.211	.118	−.101			3
4	.125	.107	.114	−.133	−.099	−.178	−.269				−.052		−.107	−.186	−.019	.023	−.056			4
5	.113	.115	.187	−.224	−.147	−.203					−.092	−.085	−.085	−.269	−.067	−.101				5
6	.111	.182	.062	−.201	.271						−.066	−.068	.000	−.262	−.136					6
7	.126	.148	−.131	−.197	−.263						−.066	−.045	−.181	−.281	−.135					7
8	.116	−.074	−.156								−.087	−.154	−.174							8
9	−.056	−.094	−.169								−.190	−.140	−.174							9
10	.007	−.104									−.100	−.157								10
11	−.047										−.116									11
	α = −06°										δ = 30°									
1	.292	.383	.155	.133	.005	.283	−.223	−.364										.307		1
2	.179	.199	.226	.242	−.286	−.309	.607				−.076		−.307		.907	.506	.573			2
3	.123	.138		.588	−.118	−.320	−.366				−.044	−.087	−.116		.601	.367	.188			3
4	.125	.109	.115	−.253	−.224	−.334	−.345				−.044		−.108	−.247	.485	.353	.248			4
5	.113	.111	.332	−.375	−.264	−.325					−.083	−.084	−.093	−.319	.040	.124				5
6	.105	.178	.066	−.326	.273						−.060	−.070	.066	−.331	.041					6
7	.122	.208	−.188	−.285	−.341						−.062	−.045	−.142	−.358	.100					7
8	.111	−.055	−.206								−.081	−.098	−.141							8
9	−.023	−.093	−.210								−.196	−.098	−.158							9
10	.055	−.121									−.075	−.119								10
11	−.005										−.040									11

[redacted]

Table 13 Concluded

Pressure Coefficients on Delta Wing with Control

Configuration F M = 1.61 R = 4.2 x 10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = -12°									δ = -20°									
1	.149	.239	-.005	-.129	.160	.330	-.285	.522									-.386		1
2	.333	.345	.377	.372	.875	.920	1.292			-.273		-.424		-.404	-.430	-.403			2
3	.246	.249		.115	.759	.879	.629			-.113	-.191	-.273		-.395	.399	-.402			3
4	.246	.234	.248	.459	.973	.704	.543			-.117		-.063	-.357	-.396	-.408	-.402			4
5	.232	.234	.215	.116	.391	.572				-.149	-.130	-.150	-.262	-.357	-.403				5
6	.229	.309	.425	-.095	.334					-.125	-.040	-.275	-.197	-.392					6
7	.245	.237	.194	-.115	.448					-.099	-.087	-.374	-.130	-.330					7
8	.207	.104	.150							-.045	-.233	-.302							8
9	.007	.146	.161							-.125	-.276	-.147							9
10	.089	.146								-.095	-.304								10
11	.089									-.140									11
	α = -12°									δ = 00°									
1	.166	.261	.023	-.113	.070	.300	-.137	.017									-.305		1
2	.326	.337	.370	.373	.369	.369	.569			-.260		-.442		-.219	-.300	-.239			2
3	.245	.236		.273	.338	.324	.011			-.112	-.171	-.351		-.243	-.315	-.283			3
4	.245	.225	.238	.242	.290	.282	-.015			-.112		-.185	-.328	-.260	-.299	-.288			4
5	.225	.222	.270	.062	.171	.038				-.146	-.156	-.174	-.364	-.260	-.297				5
6	.219	.296	.240	.049	.291					-.119	-.163	-.154	-.346	-.283					6
7	.240	.248	.029	.039	-.002					-.119	-.142	-.256	-.340	-.211					7
8	.222	.029	.026							-.143	-.249	-.256							8
9	.029	.028	.031							-.234	-.249	-.251							9
10	.079	.028								-.145	-.248								10
11	.029									-.188									11
	α = -12°									δ = 10°									
1	.158	.258	.015	-.120	.369	.305	.161	-.122									-.333		1
2	.317	.337	.367	.371	.248	.196	.545			-.266		-.440		.167	-.164	-.202			2
3	.241	.237		.357	.218	.174	-.100			-.114	-.178	-.344		-.156	-.228	-.310			3
4	.240	.222	.242	.075	.152	.135	-.082			-.114		-.187	-.316	-.367	-.278	-.306			4
5	.216	.220	.259	-.054	.035	-.085				-.151	-.159	-.131	-.316	-.307	-.348				5
6	.219	.306	.194	-.054	.288					-.121	-.159	-.160	-.257	-.307					6
7	.237	.242	-.031	-.059	-.171					-.122	-.103	-.283	-.250	-.278					7
8	.228	.015	-.049							-.138	-.232	-.283							8
9	.020	.002	-.043							-.239	-.228	-.271							9
10	.070	-.007								-.122	-.244								10
11	.029									-.142									11
	α = -12°									δ = 20°									
1	.156	.258	.016	-.120	.219	.312	.117	-.254									-.185		1
2	.323	.341	.364	.373	.155	-.053	.519			-.260		-.440		.542	.111	.095			2
3	.240	.236		.302	-.094	-.064	-.182			-.105	-.172	-.343		.254	-.030	-.213			3
4	.242	.222	.242	-.044	-.055	.071	-.173			-.105		-.179	-.379	-.123	-.162	-.222			4
5	.220	.224	.295	-.152	-.094	-.152				-.147	-.152	-.126	-.360	-.332	-.323				5
6	.221	.302	.191	-.128	.290					-.115	-.164	-.093	-.305	-.293					6
7	.237	.246	-.037	-.126	-.230					-.122	-.095	-.261	-.317	-.314					7
8	.237	.015	-.075							-.133	-.187	-.290							8
9	.037	-.002	-.086							-.229	-.197	-.290							9
10	.078	-.011								-.114	-.226								10
11	.029									-.103									11
	α = -12°									δ = 30°									
1	.156	.251	.014	-.126	.039	.313	-.141	-.325									.084		1
2	.318	.336	.366	.374	-.098	-.239	.482			-.267		-.447		.875	.361	.344			2
3	.237	.233		.556	-.027	-.246	-.311			-.105	-.184	-.351		.619	.182	-.029			3
4	.243	.225	.241	-.172	-.172	-.196	-.282			-.112		-.185	-.373	.414	.013	-.029			4
5	.220	.222	.427	-.312	-.199	-.249				-.143	-.159	-.146	-.400	-.346	-.214				5
6	.211	.298	.167	-.244	.291					-.120	-.159	-.050	-.368	-.261					6
7	.233	.288	-.065	-.216	-.318					-.120	-.111	-.240	-.367	-.263					7
8	.239	.017	-.110							-.135	-.154	-.291							8
9	.067	-.011	-.126							-.227	-.166	-.290							9
10	.110	-.022								-.098	-.215								10
11	.056									-.064									11

[redacted]

Table 14

Pressure Coefficients on Delta Wing with Control

Configuration F1 M = 1.61 R = 4.2 x 10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
								α = 00°			δ = -30°									
1	.343	.292	.303	.300	.098			.404			.073	.060	.043	.494	-.312	-.356	-.352	-.342		1
2	.064	.038	.030	.429	.845	.776					.036		.009	-.018	-.257	-.350	-.373			2
3	.026	.015	.007	-.007	.771	.747	.365				.028	.010	.096	-.066	-.246	-.340	-.368			3
4	.036	.005	.086	-.069	.774	.630	.389				.007	.003	-.025	-.192	-.247	-.358				4
5	.015	.007	-.028	-.116	.694	.315					.023	.111	-.024	-.181	-.324					5
6	.024	.120	-.027	-.076							.013	.038	-.178	-.172						6
7	.013	.021	-.184	-.084	.220						.077	-.137	-.170							7
8		-.148	-.088								-.076	-.142	-.180							8
9	-.080	-.162	-.097								-.047	-.147								9
10	-.034	.237									-.119									10
11	-.122																			11
								α = 00°			δ = -20°									
1	.346	.298	.307	.303	.291			.164			.078	.064	.048	.491	-.234	-.300	-.300	-.311		1
2	.066	.042	.032	.433	.468	.507					.038		.014	-.015	-.126	-.282	-.341			2
3	.028	.019	.010	-.008	.427	.458	.094				.032	.014	.101	-.056	-.140	-.263	-.334			3
4	.038	.012	.092	-.064	.468	.452	.140				.010	.006	-.024	-.177	-.155	-.306				4
5	.021	.011	-.027	-.167	.448	.110					.027	.114	-.020	-.169	-.255					5
6	.027	.123	-.023	-.102							.018	.044	-.170	-.162						6
7	.014	.026	-.178	-.091	.039						.079	-.137	-.158							7
8		-.143	-.175								-.069	-.140	-.168							8
9	-.076	-.155	-.143								-.040	-.143								9
10	-.031	.241									-.115									10
11	-.119																			11
								α = 00°			δ = -10°									
1	.347	.301	.306	.306	.330			-.034			.079	.064	.046	.494	-.104	-.198	-.208	-.247		1
2	.064	.041	.034	.441	.230	.287					.038		.012	-.017	-.040	-.150	-.267			2
3	.028	.021	.010	-.009	.196	.243	-.049				.034	.018	.099	-.058	-.058	-.097	-.280			3
4	.038	.014	.095	-.061	.240	.245	-.020				.009	.007	-.020	-.171	-.080	-.196				4
5	.023	.012	-.026	-.166	.212	-.020					.028	.112	-.023	-.156	-.191					5
6	.027	.128	-.022	-.132							.016	.044	-.164	-.151						6
7	.014	.029	-.179	-.119	-.068						.078	-.138	-.153							7
8		-.140	-.171								-.072	-.139	-.159							8
9	-.073	-.154	-.174								-.039	-.144								9
10	-.027	.241									-.115									10
11	-.116																			11
								α = 00°			δ = 00°									
1	.349	.300	.307	.307	.286			-.266			.077	.061	.046	.499	.020	.005	-.010	-.261		1
2	.063	.040	.031	.443	.013	-.001					.039		.011	-.017	-.004	-.003	-.213			2
3	.028	.018	.011	-.009	-.009	-.018	-.215				.029	.013	.097	-.059	-.002	-.005	-.197			3
4	.035	.017	.099	-.060	-.016	.001	-.202				.011	.007	-.025	-.164	-.002	-.172				4
5	.031	.011	-.043	-.166	-.011	-.185					.029	.111	-.020	-.139	-.143					5
6	.022	.124	-.024	-.147							.011	.043	-.170	-.134						6
7	.010	.030	-.177	-.142	-.171						.078	-.138	-.158							7
8		-.139	-.167								-.069	-.142	-.151							8
9	-.068	-.155	-.173								-.038	-.146								9
10	-.031	.239									-.116									10
11	-.116																			11
								α = 00°			δ = 10°									
1	.348	.300	.307	.305	.274			-.280			.078	.065	.043	.509	.078	.092	.088	-.217		1
2	.066	.043	.034	.447	.001	-.049					.039		.013	-.019	.063	.073	-.173			2
3	.028	.019	.013	-.006	-.016	-.041	-.238				.034	.015	.094	-.060	.067	.072	-.149			3
4	.039	.017	.096	-.057	-.027	-.023	-.220				.012	.006	-.026	-.167	.073	-.132				4
5	.032	.013	-.032	-.169	-.024	-.193					.027	.112	-.020	-.129	-.094					5
6	.022	.126	-.024	-.159							.011	.043	-.171	-.122						6
7	.010	.032	-.176	-.158	-.161						.077	-.138	-.158							7
8		-.137	-.165								-.073	-.142	-.146							8
9	-.069	-.151	-.179								-.036	-.147								9
10	-.032	.239									-.115									10
11	-.117																			11

[redacted]

Table 14 Continued

Pressure Coefficients on Delta Wing with Control

Configuration F1 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
								α = 00°				δ = 20°							
1	.345	.297	.304	.301	.225			-.301		.073	.060	.039	.511	.296	.342	.332	-.028		1
2	.067	.044	.032	.447	-.105	-.152				.034		.007	-.020	.246	.295	-.035			2
3	.030	.017	.013	-.006	-.070	-.129	-.282			.038	.011	.092	-.066	.288	.282	.012			3
4	.040	.014	.096	-.056	-.090	-.134	-.262			.009	.002	-.030	-.164	.282	-.005				4
5	.030	.009	-.028	-.175	-.100	-.257				.026	.105	-.024	-.106	.046					5
6	.020	.129	-.023	-.177						.007	.036	-.172	-.094						6
7	.010	.030	-.171	-.174	-.209					.072	-.142	-.166							7
8		-.139	-.171							-.075	-.150	-.116							8
9	-.068	-.152	-.189							-.038	-.151								9
10	-.036	.235								-.117									10
11	-.114																		11
								α = 00°				δ = 30°							
1	.352	.299	.304	.303	.145			-.313		.075	.060	.039	.514	.547	.565	.485	.166		1
2	.067	.044	.035	.455	-.181	-.212				.032		.008	-.017	.490	.532	.144			2
3	.031	.019	.013	-.003	-.131	-.195	-.310			.040	.011	.093	-.072	.520	.439	.191			3
4	.041	.014	.096	-.060	-.144	-.210	-.291			.011	.003	-.031	-.129	.483	.135				4
5	.029	.010	-.027	-.185	-.154	-.301				.026	.105	-.024	-.078	.190					5
6	.021	.130	-.026	-.190						.004	.039	-.179	-.084						6
7	.011	.031	-.175	-.183	-.242					.071	-.140	-.109							7
8		-.140	-.181							-.073	-.146	-.072							8
9	-.063	-.148	-.199							-.032	-.150								9
10	-.036	.236								-.115									10
11	-.111																		11
								α = 03°				δ = 00°							
1	.344	.224	.234	.209	.265			-.224		.143	.152	.155	.741	.113	.109	.176	-.139		1
2	.003	-.055	-.110	.003	.000	-.051				.089		.093	.111	.069	.085	-.113			2
3	-.010	-.035	-.031	-.102	.009	-.019	-.214			.084	.064	.188	-.005	.081	.140	-.098			3
4	.003	-.030	.002	-.108	-.009	-.053	-.197			.061	.060	.106	-.140	.130	-.079				4
5	-.023	-.032	-.134	-.183	-.049	-.202				.080	.189	.053	-.114	-.040					5
6	-.020	.063	-.068	-.166						.058	.121	-.127	-.108						6
7	-.016	-.055	-.205	-.155	-.175					.182	-.082	-.125							7
8		-.206	-.185							.001	-.073	-.127							8
9	-.121	-.202	-.187							.006	-.086								9
10	-.089	.249								-.058									10
11	-.180																		11
								α = 06°				δ = -30°							
1	.321	.153	.156	.115	.225			.290		.211	.237	.242	.888	-.361	-.374	-.380	-.373		1
2	-.065	-.216	-.316	-.118	.639	.627				.148		.168	.199	-.235	-.375	-.406			2
3	-.048	-.084	-.087	-.237	.471	.613	.173			.145	.130	.299	.038	-.180	-.391	-.392			3
4	-.031	-.078	-.054	-.152	.581	.490	.229			.122	.115	.188	-.111	-.195	-.372				4
5	-.068	-.075	-.217	-.195	.498	.153				.127	.280	.104	-.114	-.288					5
6	-.051	.014	-.204	-.152						.131	.181	-.089	-.119						6
7	-.056	-.105	-.251	-.137	.067					.285	-.005	-.093							7
8		-.255	-.201							.051	-.020	-.095							8
9	-.152	-.279	-.140							.031	-.047								9
10	-.110	.265								-.014									10
11	-.207																		11
								α = 06°				δ = -20°							
1	.319	.148	.153	.113	.306			.040		.207	.234	.240	.883	-.267	-.305	-.308	-.335		1
2	-.069	-.218	-.317	-.118	.299	.371				.143		.163	.200	-.137	-.260	-.341			2
3	-.048	-.085	-.088	-.235	.217	.343	-.012			.141	.125	.295	.047	-.094	-.266	-.338			3
4	-.032	-.079	-.057	-.153	.291	.266	.011			.121	.113	.189	-.105	-.111	-.218				4
5	-.070	-.078	-.218	-.208	.274	-.006				.122	.276	.105	-.109	-.212					5
6	-.052	.010	-.206	-.175						.122	.177	-.083	-.117						6
7	-.057	-.106	-.254	-.160	-.069					.278	-.011	-.089							7
8		-.260	-.204							.049	-.019	-.095							8
9	-.155	-.279	-.199							.031	-.040								9
10	-.115	.262								-.013									10
11	-.209																		11

[redacted]

Table 14 Continued

Pressure Coefficients on Delta Wing with Control

Configuration F1 M = 1.61 R = 4.2 x 10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
								α = 06°		δ = −10°									
1	.321	.152	.154	.117	.292			−.221		.209	.238	.241	.879	.000	−.060	−.057	−.209		1
2	−.065	−.214	−.314	−.113	−.043	.078				.143		.166	.210	−.002	.010	−.145			2
3	−.045	−.083	−.086	−.239	.014	.060	−.192			.146	.127	.296	.048	.030	.020	−.151			3
4	−.031	−.078	−.053	−.149	.100	.066	−.193			.122	.116	.197	−.102	.025	−.114				4
5	−.067	−.075	−.216	−.205	.057	−.180				.126	.279	.108	−.101	−.107					5
6	−.050	.014	−.206	−.184						.121	.183	−.082	−.105						6
7	−.055	−.103	−.254	−.171	−.189					.281	−.007	−.086							7
8		−.257	−.201							.057	−.017	−.089							8
9	−.152	−.278	−.200							.036	−.036								9
10	−.115	.264								−.009									10
11	−.206																		11
								α = 06°		δ = 00°									
1	.324	.153	.158	.119	.206			−.299		.213	.239	.243	.878	.168	.185	.296	−.049		1
2	−.062	−.209	−.311	−.109	−.054	−.210				.147		.167	.213	.110	.253	−.043			2
3	−.042	−.081	−.084	−.234	−.061	−.093	−.303			.151	.129	.300	.043	.136	.224	−.024			3
4	−.028	−.075	−.050	−.147	−.067	−.086	−.280			.127	.117	.199	−.108	.218	−.010				4
5	−.066	−.072	−.205	−.205	−.096	−.255				.129	.283	.111	−.098	.024					5
6	−.046	.018	−.201	−.190						.124	.187	−.084	−.089						6
7	−.053	−.100	−.248	−.180	−.229					.284	−.007	−.093							7
8		−.254	−.195							.060	−.015	−.090							8
9	−.148	−.274	−.201							.041	−.039								9
10	−.115	.268								−.007									10
11	−.201																		11
								α = 06°		δ = 10°									
1	.319	.148	.154	.114	.168			−.341		.206	.233	.239	.875	.381	.396	.486	.148		1
2	−.067	−.216	−.317	−.111	−.249	−.311				.144		.166	.208	.304	.474	.089			2
3	−.048	−.087	−.088	−.238	−.127	−.253	−.373			.146	.122	.297	.036	.302	.397	.134			3
4	−.036	−.080	−.057	−.151	−.150	−.276	−.349			.121	.109	.193	−.112	.415	.122				4
5	−.071	−.078	−.218	−.210	−.185	−.355				.122	.276	.106	−.082	.143					5
6	−.055	.013	−.206	−.199						.119	.180	−.088	−.062						6
7	−.059	−.105	−.255	−.189	−.282					.278	−.011	−.098							7
8		−.259	−.203							.053	−.023	−.093							8
9	−.154	−.279	−.209							.038	−.044								9
10	−.123	.263								−.013									10
11	−.206																		11
								α = 06°		δ = 20°									
1	.315	.146	.149	.109	.048			−.362		.202	.233	.236	.877	.683	.718	.606	.393		1
2	−.066	−.217	−.317	−.112	−.348	−.373				.139		.160	.205	.601	.697	.321			2
3	−.051	−.089	−.090	−.235	−.251	−.344	−.398			.144	.118	.296	.034	.671	.524	.388			3
4	−.037	−.084	−.056	−.151	−.221	−.362	−.378			.118	.108	.193	−.084	.631	.328				4
5	−.073	−.079	−.220	−.213	−.260	−.402				.121	.273	.101	−.043	.320					5
6	−.057	.011	−.208	−.204						.121	.175	−.092	−.004						6
7	−.061	−.108	−.256	−.193	−.332					.275	−.014	−.067							7
8		−.263	−.206							.052	−.024	−.038							8
9	−.152	−.282	−.216							.036	−.044								9
10	−.128	.258								−.019									10
11	−.206																		11
								α = 06°		δ = 30°									
1	.316	.145	.151	.110	−.139			−.374		.203	.231	.235	.877	1.105	.892	.730	.567		1
2	−.069	−.218	−.319	−.112	−.399	−.408				.139		.158	.201	.994	.874	.633			2
3	−.050	−.089	−.093	−.239	−.326	−.380	−.398			.146	.114	.294	.059	.966	.598	.578			3
4	−.038	−.084	−.061	−.152	−.332	−.391	−.385			.117	.106	.191	−.035	.832	.561				4
5	−.072	−.082	−.226	−.217	−.344	−.403				.123	.274	.101	−.014	.602					5
6	−.061	.011	−.212	−.205						.122	.176	−.040	.036						6
7	−.058	−.108	−.257	−.189	−.324					.276	−.015	−.022							7
8		−.263	−.208							.050	−.025	−.005							8
9	−.155	−.283	−.218							.038	.014								9
10	−.129	.259								−.019									10
11	−.208																		11

[redacted]

Table 14 Continued

Pressure Coefficients on Delta Wing with Control

Configuration F1 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
								α = 09°				δ = 00°								
1	.284	.072	.065	.022	.142			-.255			.288	.316	.318	1.059	.201	.250	.408	.047		1
2	-.143	-.352	-.408	-.264	-.167	-.240					.207		.243	.305	.143	.366	.015			2
3	-.078	-.135	-.160	-.425	-.101	-.183	-.307				.212	.190	.422	.105	.257	.318	.048			3
4	-.066	-.123	-.093	-.210	-.110	-.131	-.291				.181	.177	.268	-.066	.307	.065				4
5	-.102	-.121	-.235	-.230	-.129	-.276					.189	.365	.172	-.059	.086					5
6	-.090	-.027	-.291	-.202							.300	.309	-.032	-.042						6
7	-.093	-.152	-.376	-.195	-.246						.354	.052	-.009							7
8		-.286	-.369								.097	.023	-.027							8
9	-.176	-.299	-.201								.076	-.001								9
10	-.144	.290									.026									10
11	-.222																			11
								α = 12°				δ = -30°								
1	.246	.009	-.031	-.040	.279			.082			.350	.382	.394	1.206	-.286	-.254	-.282	-.328		1
2	-.263	-.424	-.454	-.425	.449	.377					.267		.311	.362	-.071	-.273	-.324			2
3	-.114	-.214	-.380	-.441	.220	.383	.026				.256	.258	.516	.181	-.097	-.279	-.338			3
4	-.105	-.192	-.153	-.305	.268	.358	.042				.248	.242	.334	-.008	-.129	-.258				4
5	-.138	-.169	-.272	-.257	.342	.011					.243	.437	.251	.013	-.232					5
6	-.125	-.092	-.334	-.210							.466	.370	.063	.054						6
7	-.125	-.163	-.408	-.093	-.051						.412	.088	.035							7
8		-.303	-.352								.122	.061	.023							8
9	-.195	-.323	-.232								.094	.042								9
10	-.160	.285									.067									10
11	-.241																			11
								α = 12°				δ = -20°								
1	.245	.010	-.030	-.044	.296			-.165			.349	.381	.391	1.198	-.152	-.094	-.133	-.231		1
2	-.266	-.425	-.454	-.422	.118	.090					.266		.307	.362	-.019	-.045	-.181			2
3	-.117	-.214	-.378	-.446	-.056	.117	-.134				.256	.257	.512	.193	.011	-.034	-.183			3
4	-.108	-.192	-.156	-.302	.099	.144	-.133				.244	.239	.336	-.002	-.025	-.156				4
5	-.142	-.168	-.273	-.264	.115	-.129					.242	.431	.253	.013	-.150					5
6	-.125	-.093	-.338	-.224							.458	.370	.067	.054						6
7	-.130	-.164	-.408	-.113	-.173						.398	.089	.041							7
8		-.303	-.400								.122	.065	.026							8
9	-.195	-.323	-.246								.096	.047								9
10	-.166	.283									.068									10
11	-.241																			11
								α = 12°				δ = -10°								
1	.249	.017	-.027	-.047	.156			-.351			.350	.382	.390	1.192	.155	.226	.271	.027		1
2	-.261	-.423	-.454	-.419	-.261	-.260					.267		.306	.369	.133	.230	.036			2
3	-.113	-.210	-.378	-.445	-.230	-.208	-.317				.258	.257	.516	.193	.220	.181	.013			3
4	-.105	-.191	-.156	-.306	-.096	-.102	-.296				.248	.239	.345	-.010	.176	.036				4
5	-.134	-.167	-.274	-.268	-.105	-.268					.243	.437	.257	.014	.001					5
6	-.121	-.091	-.340	-.230							.462	.373	.066	.059						6
7	-.126	-.163	-.410	-.124	-.277						.402	.093	.040							7
8		-.301	-.400								.131	.067	.026							8
9	-.192	-.320	-.249								.105	.049								9
10	-.165	.284									.073									10
11	-.239																			11
								α = 12°				δ = 00°								
1	.234	.019	-.028	-.044	.097			-.320			.352	.383	.388	1.192	.229	.466	.460	.143		1
2	-.253	-.414	-.449	-.419	-.296	-.332					.270		.302	.371	.184	.443	.086			2
3	-.109	-.207	-.379	-.445	-.165	-.255	-.371				.260	.260	.519	.175	.395	.364	.121			3
4	-.098	-.190	-.157	-.309	-.170	-.230	-.354				.250	.244	.348	-.019	.369	.110				4
5	-.134	-.163	-.270	-.271	-.177	-.345					.247	.440	.257	.018	.128					5
6	-.122	-.086	-.339	-.233							.468	.377	.059	.100						6
7	-.119	-.161	-.407	-.110	-.287						.408	.092	.031							7
8		-.303	-.394								.136	.068	.019							8
9	-.186	-.320	-.242								.110	.048								9
10	-.162	.282									.076									10
11	-.235																			11

[redacted]

Table 14 Concluded

Pressure Coefficients on Delta Wing with Control

Configuration F1 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
								$\alpha = 12^\circ$			$\delta = 10^\circ$									
1	.251	.015	-.032	-.049	-.082			-.358			.349	.379	.385	1.190	.454	.663	.569	.358		1
2	-.261	-.424	-.457	-.421	-.378	-.394					.268		.301	.369	.407	.636	.279			2
3	-.113	-.211	-.382	-.453	-.302	-.360	-.405				.259	.256	.516	.170	.636	.486	.342			3
4	-.105	-.192	-.160	-.311	-.223	-.366	-.392				.247	.239	.345	-.014	.561	.294				4
5	-.138	-.170	-.274	-.276	-.248	-.408					.245	.437	.253	.065	.280					5
6	-.122	-.090	-.342	-.230							.466	.373	.058	.140						6
7	-.127	-.165	-.411	-.100	-.334						.405	.088	.039							7
8		-.303	-.350								.131	.063	.059							8
9	-.192	-.324	-.234								.104	.045								9
10	-.168	.280									.069									10
11	-.242																			11
								$\alpha = 12^\circ$			$\delta = 20^\circ$									
1	.249	.013	-.032	-.049	-.078			-.362			.350	.379	.387	1.192	.772	.837	.675	.529		1
2	-.263	-.427	-.458	-.424	-.417	-.422					.267		.300	.368	.782	.805	.586			2
3	-.112	-.212	-.382	-.451	-.369	-.399	-.398				.257	.254	.516	.184	.850	.552	.541			3
4	-.105	-.192	-.162	-.312	-.281	-.386	-.383				.245	.237	.343	.051	.760	.551				4
5	-.137	-.168	-.275	-.272	-.344	-.397					.247	.435	.249	.121	.547					5
6	-.122	-.091	-.344	-.194							.465	.373	.085	.212						6
7	-.128	-.164	-.413	-.086	-.328						.404	.088	.099							7
8		-.304	-.249								.130	.067	.085							8
9	-.190	-.324	-.224								.104	.088								9
10	-.170	.281									.071									10
11	-.241																			11
								$\alpha = 12^\circ$			$\delta = 30^\circ$									
1	.246	.012	-.033	-.049	-.212			-.358			.347	.379	.386	1.194	1.236	.969	.870	.684		1
2	-.258	-.426	-.457	-.423	-.420	-.410					.268		.300	.367	1.123	1.068	.885			2
3	-.121	-.215	-.385	-.438	-.385	-.394	-.387				.255	.253	.515	.303	1.091	.870	.760			3
4	-.108	-.195	-.159	-.324	-.341	-.385	-.377				.247	.234	.340	.117	.922	.755				4
5	-.139	-.170	-.282	-.243	-.368	-.387					.240	.436	.354	.239	.796					5
6	-.124	-.090	-.344	-.172							.464	.379	.167	.261						6
7	-.128	-.158	-.411	-.076	-.345						.403	.140	.162							7
8		-.305	-.225								.129	.159	.173							8
9	-.191	-.326	-.206								.138	.147								9
10	-.168	.281									.146									10
11	-.233																			11
								$\alpha = 15^\circ$			$\delta = 00^\circ$									
1	.202	-.067	-.172	-.068	.073			-.241			.424	.453	.460	1.332	.179	.576	.535	.253		1
2	-.376	-.448	-.436	-.425	-.237	-.241					.334		.382	.498	.195	.558	.216			2
3	-.150	-.352	-.406	-.416	-.218	-.217	-.295				.322	.326	.645	.397	.553	.454	.267			3
4	-.141	-.308	-.335	-.431	-.164	-.245	-.274				.314	.440	.557	.134	.472	.220				4
5	-.172	-.150	-.409	-.445	-.175	-.330					.343	.596	.414	.134	.225					5
6	-.159	-.076	-.427	-.297							.588	.456	.146	.135						6
7	-.163	-.198	-.419	-.259	-.254						.476	.151	.131							7
8		-.334	-.410								.181	.139	.120							8
9	-.210	-.357	-.243								.151	.125								9
10	-.197	.298									.132									10
11	-.256																			11

Table 15

Pressure Coefficients on Delta Wing with Control

Configuration F2 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station								Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 00°									δ = 00°									
1	.343	.304	.300	.300	.309			-.283		.069	.051	.030	.029	.166	.121	.133	-.109		1
2	.062	.040	.035	.027	.010	-.035				.030		.002	-.005	.109	.092	-.111			2
3	.031	.016	.012	.005	.008	-.036	-.239			.032	.007	-.018	-.005	.089	.060	-.100			3
4	.040	.007	-.007	.009	-.006	-.032	-.229			.004	-.003	-.027	-.156	.032	-.064				4
5	.027	.007	-.011	-.148	-.016	-.172				.020	.032	.014	-.147	-.063					5
6	.019	.058	.014	-.147						.004	.022	-.142	-.182						6
7	.009	.016	-.144	-.154	-.166					.014	-.138	-.136							7
8		-.139	-.140							-.133	-.132	-.138							8
9	-.125	-.137	-.142							-.071	-.142								9
10	-.067	.238								-.135									10
11	-.130																		11
	α = 00°									δ = 10°									
1	.344	.306	.300	.301	.278			-.297		.068	.051	.030	.029	.160	.141	.154	-.121		1
2	.063	.041	.036	.030	.005	-.068				.029		.002	.056	.098	.104	-.120			2
3	.031	.017	.013	-.060	-.002	-.051	-.255			.033	.008	-.019	.029	.081	.070	-.108			3
4	.040	.007	-.005	-.044	-.024	-.051	-.240			.003	-.002	-.027	-.170	.034	-.072				4
5	.028	.007	-.025	-.132	-.032	-.194				.019	.031	.062	-.162	-.042					5
6	.018	.060	-.031	-.131						.001	.016	-.101	-.182						6
7	.010	.023	-.178	-.139	-.177					.012	-.123	-.101							7
8		-.145	-.174							-.134	-.104	-.120							8
9	-.121	-.156	-.170							-.072	-.112								9
10	-.063	.238								-.134									10
11	-.126																		11
	α = 00°									δ = 20°									
1	.342	.305	.299	.302	.231			-.317		.067	.050	.030	.028	.329	.276	.325	.000		1
2	.062	.041	.037	.032	-.075	-.154				.028		.002	.099	.231	.279	-.030			2
3	.030	.017	.014	.237	-.042	-.140	-.295			.034	.007	-.019	.034	.239	.198	.003			3
4	.040	.008	-.005	-.199	-.078	-.165	-.283			.002	-.003	-.032	-.218	.102	.032				4
5	.028	.007	.023	-.177	-.105	-.238				.019	.027	.134	-.162	.116					5
6	.017	.062	-.044	-.129						-.002	.012	-.049	-.181						6
7	.008	.056	-.228	-.131	-.218					.009	-.114	-.054							7
8		-.134	-.240							-.136	-.060	-.100							8
9	-.115	-.157	-.238							-.071	-.065								9
10	-.043	.238								-.125									10
11	-.103																		11
	α = 00°									δ = 30°									
1	.342	.305	.299	.301	.160			-.328		.067	.048	.030	.027	.605	.555	.504	.003		1
2	.062	.040	.036	.032	-.168	-.214				.027		.002	.096	.419	.502	.141			2
3	.031	.015	.013	.635	-.092	-.206	-.321			.034	.005	-.020	-.098	.470	.388	.206			3
4	.040	.007	-.006	-.350	-.132	-.240	-.310			.002	-.005	-.033	-.238	.208	.200				4
5	.027	.007	.127	-.372	-.180	-.290				.019	.024	.213	-.153	.283					5
6	.017	.062	-.031	-.164						-.002	.010	.011	-.178						6
7	.009	.117	-.259	-.125	-.254					.008	-.054	-.021							7
8		-.106	-.293							-.136	-.002	-.075							8
9	-.071	-.152	-.309							-.055	-.011								9
10	.017	.238								-.013									10
11	-.047																		11
	α = 03°									δ = 00°									
1	.343		.224	.199	.131			-.354		.140	.149	.153	.156	.256	.217	.227	-.041		1
2	-.002	-.070	-.116	-.175	-.213	-.270				.085		.086	.062	.191	.172	-.063			2
3	-.015	-.044	-.042	-.067	-.171	-.226	-.349			.083	.060	.054	.092	.150	.125	-.054			3
4	-.002	-.038	-.070	-.081	-.175	-.205	-.337			.059	.056	.032	-.089	.133	-.042				4
5	-.024	-.041	-.101	-.214	-.162	-.308				.075	.091	.069	-.083	-.061					5
6	-.024	.011	-.038	-.210						.051	.072	-.097	-.085						6
7	-.023	-.028	-.184	-.210	-.242					.066	-.098	-.088							7
8		-.171	-.179							-.094	-.092	-.084							8
9	-.160	-.170	-.191							-.040	-.100								9
10	-.099	.248								-.099									10
11	-.152																		11

[redacted]

Table 15 Continued

Pressure Coefficients on Delta Wing with Control

Configuration F2 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station								Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 06°									δ = -30°									
1	.315	.135	.142	.105	.240			-.023		.206	.238	.238	.238	-.099	-.145	-.135	-.235		1
2	-.076	-.232	-.325	-.339	.667	.282				.142		.162	.557	-.002	-.172	-.243			2
3	-.054	-.093	-.099	-.092	.323	.150	-.078			.139	.115	.117	-.206	-.064	-.161	-.260			3
4	-.040	-.087	-.112	-.234	.185	.142	-.050			.112	.108	.288	-.210	-.159	-.215				4
5	-.071	-.085	-.088	-.283	-.044	.009				.125	.156	.075	-.007	-.262					5
6	-.064	-.041	.052	-.267						.108	.195	-.160	.008						6
7	-.062	-.057	-.146	-.208	.077					.125	-.042	-.171							7
8		-.123	-.124							-.023	-.079	-.185							8
9	-.190	-.117	-.161							.039	-.110								9
10	-.084	.264								-.003									10
11	-.071																		11
	α = 06°									δ = -20°									
1	.315	.136	.144	.107	.313			-.263		.206	.238	.237	.237	.080	.005	.001	-.156		1
2	-.075	-.230	-.325	-.337	.230	-.015				.142		.161	.198	.104	-.020	-.150			2
3	-.053	-.092	-.098	-.177	-.034	-.105	-.273			.139	.114	.117	-.055	.048	.002	-.163			3
4	-.039	-.085	-.110	-.168	-.189	-.121	-.266			.112	.109	.151	-.043	-.031	-.124				4
5	-.069	-.085	-.077	-.284	-.121	-.174				.127	.154	.074	.009	-.183					5
6	-.063	-.039	-.010	-.239						.105	.146	-.116	-.001						6
7	-.060	-.051	-.183	-.246	-.091					.123	-.063	-.134							7
8		-.156	-.153							-.042	-.078	-.138							8
9	-.188	-.153	-.182							.006	-.094								9
10	-.104	.265								-.043									10
11	-.128																		11
	α = 06°									δ = -10°									
1	.315	.136	.145	.107	.284			-.361		.206	.239	.236	.237	.267	.182	.181	-.035		1
2	-.075	-.229	-.323	-.336	-.124	-.234				.142		.160	.127	.218	.154	-.041			2
3	-.053	-.092	-.098	-.193	-.254	-.268	-.365			.141	.113	.116	.102	.164	.112	-.049			3
4	-.040	-.085	-.110	-.134	-.241	-.263	-.359			.111	.110	.092	-.007	.104	-.032				4
5	-.068	-.084	-.082	-.278	-.149	-.265				.127	.156	.099	.003	-.088					5
6	-.064	-.036	-.070	-.250						.103	.126	-.092	-.011						6
7	-.061	-.046	-.200	-.261	-.207					.121	-.062	-.094							7
8		-.177	-.181							-.044	-.064	-.058							8
9	-.186	-.186	-.200							-.003	-.081								9
10	-.110	.264								-.056									10
11	-.145																		11
	α = 06°									δ = 00°									
1	.316	.137	.146	.108	.165			-.354		.205	.238	.237	.235	.287	.250	.259	-.026		1
2	-.073	-.221	-.317	-.333	-.191	-.255				.142		.161	.129	.213	.198	-.048			2
3	-.052	-.090	-.096	-.156	-.162	-.246	-.351			.141	.111	.117	.181	.170	.154	-.036			3
4	-.040	-.083	-.108	-.108	-.141	-.247	-.344			.112	.110	.100	-.019	.132	-.020				4
5	-.060	-.083	-.096	-.256	-.124	-.258				.128	.152	.131	-.015	-.036					5
6	-.061	-.035	-.083	-.251						.103	.127	-.050	-.023						6
7	-.060	-.068	-.215	-.250	-.226					.118	-.052	-.036							7
8		-.202	-.209							-.052	-.050	-.032							8
9	-.188	-.201	-.218							-.002	-.059								9
10	-.129	.267								-.057									10
11	-.174																		11
	α = 06°									δ = 10°									
1	.317	.137	.146	.108	.168			-.362		.206	.239	.237	.235	.361	.362	.342	.030		1
2	-.073	-.225	-.323	-.335	-.241	-.293				.142		.160	.220	.322	.293	-.006			2
3	-.052	-.090	-.096	-.317	-.209	-.284	-.366			.144	.111	.116	.230	.241	.237	.027			3
4	-.039	-.083	-.108	-.172	-.166	-.288	-.358			.113	.110	.059	-.064	.208	.047				4
5	-.066	-.083	-.102	-.225	-.138	-.292				.129	.151	.201	-.028	.072					5
6	-.064	-.032	-.161	-.218						.103	.108	.017	-.032						6
7	-.060	-.040	-.244	-.218	-.239					.117	-.043	.009							7
8		-.199	-.245							-.055	-.011	-.027							8
9	-.169	-.227	-.246							-.010	-.011								9
10	-.103	.263								-.067									10
11	-.151																		11

[redacted]

Table 15 Continued

Pressure Coefficients on Delta Wing with Control

Configuration F2 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station								Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 06°									δ = 20°									
1	.315	.136	.145	.108	.160			-.356									.259		1
2	-.071	-.217	-.310	-.315	-.286	-.319				.205	.235	.235	.235	.533	.620	.528			2
3	-.051	-.088	-.095	.234	-.258	-.313	-.367			.141		.158	.099	.472	.558	.188			3
4	-.039	-.081	-.054	-.319	-.204	-.323	-.357			.143	.109	.115	.297	.665	.448	.296			4
5	-.066	-.081	-.042	-.333	-.188	-.332				.112	.109	.057	-.078	.403	.287				5
6	-.063	.010	-.169	-.211						.127	.148	.280	-.042	.369					6
7	-.058	-.009	-.282	-.170	-.271					.101	.106	.099	-.017						7
8		-.191	.315							.114	-.022	.048							8
9	-.112	-.218	-.302							-.053	.053	-.005							9
10	-.058	.263								-.008	.053								10
11	-.119									-.050									11
	α = 06°									δ = 30°									
1	.315	.136	.145	.107	.073			-.371									.515		1
2	-.073	-.227	-.323	-.321	-.343	-.362				.203	.238	.235	.234	.874	.888	.688			2
3	-.054	-.092	-.097	.255	-.308	-.358	-.391			.140		.158	.116	.742	.853	.559			3
4	-.041	-.086	.001	-.369	-.279	-.371	-.381			.144	.109	.115	.279	.914	.617	.570			4
5	-.068	-.085	.087	-.331	-.257	-.368				.111	.109	.059	-.068	.643	.573				5
6	-.066	.128	-.207	.291						.126	.149	.353	-.018	.640					6
7	-.062	.028	-.323	-.268	-.317					.100	.129	.135	-.019						7
8		-.194	.288							.113	.076	.086							8
9	-.012	-.233	-.278							-.053	.109	.044							9
10	-.019	.263								.034	.086								10
11	-.068									.067									11
	α = 09°									δ = 00°									
1	.277		.056	.018	-.029			-.334									.106		1
2	-.186	-.401	-.423	-.417	-.248	-.290				.277	.313	.304	.312	.417	.396	.394			2
3	-.098	-.158	-.164	-.388	-.233	-.311	-.365			.192		.232	.198	.353	.348	.060			3
4	-.084	-.138	-.158	-.178	-.294	-.352	-.359			.197	.191	.174	.268	.318	.288	.091			4
5	-.117	-.128	-.260	-.286	-.308	-.395				.176	.164	.159	.042	.296	.062				5
6	-.101	-.088	-.127	.275						.165	.209	.182	.049	.032					6
7	-.112	-.107	-.245	-.269	-.307					.134	.173	-.013	.036						7
8		-.229	.238							.166	-.016	.011							8
9	-.220	-.234	-.244							-.012	-.010	.022							9
10	-.148	.270								.021	-.019								10
11	-.194									-.018									11
	α = 12°									δ = -30°									
1	.236		-.054	-.091	.267			-.226									-.136		1
2	-.279	-.443	-.471	-.479	.570	.045				.357	.385	.398	.384	.114	.001	.035			2
3	-.130	-.215	-.354	-.490	.253	-.094	-.263			.270		.308	.505	.144	-.013	-.124			3
4	-.121	-.188	-.233	-.414	-.029	-.178	-.271			.260	.259	.258	-.091	.046	.028	-.146			4
5	-.148	-.194	-.176	-.400	-.371	-.328				.244	.240	.384	.002	-.081	-.128				5
6	-.135	-.154	-.084	.308						.250	.298	.206	.146	-.227					6
7	-.142	-.116	-.260	-.241	-.280					.211	.293	-.031	.140						7
8		-.183	-.292							.271	.039	-.064							8
9	-.252	-.181	-.303							.091	.017	-.084							9
10	-.127	.299								.101	.002								10
11	-.108									.067									11
	α = 12°									δ = -20°									
1	.239		-.051	-.086	.288			-.330									.022		1
2	-.279	-.441	-.468	-.475	.131	-.199				.358	.386	.398	.386	.360	.228	.244			2
3	-.129	-.211	-.350	-.475	-.118	-.266	-.349			.269		.309	.311	.300	.209	.014			3
4	-.119	-.186	-.231	-.380	-.363	-.307	-.344			.260	.260	.259	.123	.218	.165	.000			4
5	-.147	-.190	-.172	-.360	-.352	-.380				.245	.242	.276	.115	.105	-.005				5
6	-.133	-.149	-.127	-.312						.251	.300	.225	.158	-.100					6
7	-.141	-.111	-.272	-.202	-.312					.211	.263	-.007	.134						7
8		-.208	.300							.267	.036	-.035							8
9	-.246	-.211	-.308							.070	.029	.034							9
10	-.149	.301								.082	.021								10
11	-.146									.049									11

[redacted]

Table 15 Continued

Pressure Coefficients on Delta Wing with Control

Configuration F2 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
								α = 12°			δ = −10°									
1	.238		−.052	−.091	.120			−.332			.358	.385	.395	.383	.548	.467	.447	.221		1
2	−.275	−.441	−.460	−.470	−.259	−.336					.271		.307	.377	.474	.418	.190			2
3	−.126	−.212	−.345	−.443	−.333	−.346	−.368				.261	.259	.260	.283	.415	.337	.177			3
4	−.120	−.186	−.238	−.323	−.382	−.365	−.357				.244	.239	.264	.135	.336	.176				4
5	−.148	−.189	−.190	−.328	−.357	−.388					.250	.305	.223	.153	.088					5
6	−.132	−.149	−.176	−.301							.210	.261	−.005	.128						6
7	−.141	−.103	−.280	−.201	−.335						.268	.045	.017							7
8		−.233	−.292								.063	.032	.083							8
9	−.244	−.240	−.285								.087	.021								9
10	−.154	.300									.055									10
11	−.170																			11
								α = 12°			δ = 00°									
1	.240	−.004	−.051	−.087	.063			−.210			.357	.385	.399	.385	.330	.325	.307	−.019		1
2	−.273	−.407	−.450	−.464	−.124	−.160					.269		.306	.291	.267	.284	−.034			2
3	−.125	−.213	−.310	−.428	−.129	−.181	−.262				.259	.259	.259	.379	.241	.231	.008			3
4	−.119	−.190	−.271	−.331	−.199	−.231	−.246				.247	.241	.254	.132	.226	−.007				4
5	−.146	−.188	−.223	−.315	−.214	−.277					.249	.293	.267	.142	−.013					5
6	−.134	−.154	−.168	−.297							.211	.258	.051	.123						6
7	−.140	−.132	−.271	−.203	−.170						.252	.047	.086							7
8		−.265	−.264								.047	.052	.097							8
9	−.244	−.260	−.269								.081	.046								9
10	−.169	.300									.052									10
11	−.206																			11
								α = 12°			δ = 10°									
1	.239	−.005	−.050	−.088	.071			−.258			.357	.386	.399	.385	.575	.497	.460	.158		1
2	−.276	−.430	−.464	−.471	−.230	−.244					.270		.307	.373	.504	.467	.108			2
3	−.125	−.213	−.325	−.455	−.220	−.256	−.304				.259	.258	.257	.424	.423	.391	.186			3
4	−.119	−.191	−.186	−.310	−.277	−.297	−.290				.248	.242	.203	.101	.401	.159				4
5	−.144	−.189	−.233	−.292	−.281	−.326					.250	.292	.345	.129	.168					5
6	−.133	−.113	−.268	−.287							.212	.237	.124	.111						6
7	−.140	−.102	−.325	−.268	−.233						.249	.071	.118							7
8		−.263	−.295								.040	.103	.105							8
9	−.212	−.293	−.264								.068	.105								9
10	−.125	.299									.056									10
11	−.169																			11
								α = 12°			δ = 20°									
1	.239	−.003	−.051	−.088	.053			−.282			.357	.385	.399	.385	.785	.761	.594	.406		1
2	−.277	−.435	−.454	−.429	−.284	−.286					.270		.307	.143	.671	.739	.431			2
3	−.125	−.210	−.323	.199	−.269	−.295	−.325				.260	.258	.258	.509	.800	.549	.464			3
4	−.119	−.186	−.170	−.401	−.317	−.329	−.313				.247	.241	.202	.078	.601	.446				4
5	−.144	−.172	−.115	−.333	−.319	−.348					.250	.290	.442	.114	.507					5
6	−.133	−.063	−.254	−.219							.216	.238	.198	.117						6
7	−.127	−.092	−.361	−.141	−.278						.247	.126	.158							7
8		−.240	−.301								.040	.170	.110							8
9	−.128	−.279	−.153								.080	.158								9
10	−.081	.299									.108									10
11	−.129																			11
								α = 12°			δ = 30°									
1	.239	−.003	−.051	−.087	−.033			−.298			.356	.385	.397	.384	1.047	1.025	.800	.579		1
2	−.276	−.437	−.374	−.321	−.317	−.313					.270		.304	.140	.882	1.013	.732			2
3	−.125	−.193	−.259	.464	−.302	−.320	−.341				.259	.256	.256	.554	1.055	.790	.654			3
4	−.118	−.145	−.020	−.372	−.342	−.351	−.330				.246	.242	.201	.106	.849	.700				4
5	−.143	−.129	−.121	−.264	−.345	−.364					.251	.290	.500	.193	.827					5
6	−.113	.073	−.284	−.227							.221	.312	.266	.157						6
7	−.053	−.025	−.299	−.190	−.312						.246	.201	.211							7
8		−.205	−.271								.046	.235	.176							8
9	−.057	−.201	−.252								.198	.212								9
10	−.047	.301									.240									10
11	−.120																			11

[redacted]

Table 15 Concluded

Pressure Coefficients on Delta Wing with Control

Configuration F2 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
								$\alpha = 15^\circ$			$\delta = 00^\circ$									
1	.207		-.161	-.168	-.028			-.299										.115		1
2	-.361	-.450	-.451	-.406	-.128	-.217					.419	.446	.448	.433	.448	.429	.416			2
3	-.148	-.311	-.403	-.364	-.140	-.259	-.337				.329		.365	.385	.396	.407	.076			3
4	-.138	-.291	-.389	-.328	-.254	-.321	-.333				.316	.323	.349	.514	.374	.337	.126			4
5	-.174	-.153	-.310	-.371	-.337	-.390					.309	.329	.377	.232	.354	.077				5
6	-.159	-.145	-.365	-.334							.322	.398	.365	.250	.066					6
7	-.165	-.146	-.333	-.275	-.316						.307	.365	.131	.217						7
8		-.262	-.291								.357	.121	.170							8
9	-.262	-.275	-.295								.127	.124	.181							9
10	-.183	.319									.149	.123								10
11	-.210										.131									11

[redacted]

Table 16

Pressure Coefficients on Delta Wing with Control

Configuration F3 $M = 1.61$ $R = 4.2 \times 10^6$

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
	$\alpha = 00°$										$\delta = -15°$									
1	.347	.312	.304	.304	.373			.031			.077	.063	.046	.510	-.189	-.263	-.251	-.260		1
2	.062	.037	.031	.423	.332	.404					.036		.011	-.014	-.086	-.238	-.298			2
3	.029	.013	.009	-.006	.302	.278	-.029				.032	.015	.092	-.109	-.077	-.233	-.310			3
4	.041	.009	.093	.064	.331	.211	-.057				.009	.006	-.026	-.185	-.092	-.265				4
5	.022	.005	-.032	-.121	.051	-.028					.026	.109	-.045	-.192	-.210					5
6	.022	.125	-.038	-.153							.017	.035	-.195	-.180						6
7	.009	.018	-.066	-.157	-.095						.079	-.162	-.185							7
8		-.167	-.077								-.076	-.155	-.185							8
9	-.077	-.153	-.093								-.047	-.160								9
10	-.040	.251									-.138									10
11	-.137																			11
	$\alpha = 00°$										$\delta = 00°$									
1	.344	.308	.302	.299	.380			-.293			.071	.057	.042	.504	.118	.067	.077	-.196		1
2	.058	.035	.027	.424	.023	-.048					.034		.007	-.020	.031	.009	-.173			2
3	.023	.009	.006	-.009	-.009	-.071	-.240				.026	.010	.083	-.001	.039	-.003	-.164			3
4	.034	.007	.086	.002	-.022	-.039	-.235				.006	.002	-.034	-.141	.016	-.151				4
5	.026	.003	-.035	-.139	-.016	-.193					.022	.102	-.029	-.143	-.128					5
6	.014	.117	-.047	-.150							.007	.030	-.144	-.136						6
7	.006	.017	-.156	-.154	-.161						.072	-.167	-.129							7
8		-.172	-.142								-.079	-.156	-.135							8
9	-.079	-.164	-.153								-.047	-.138								9
10	-.047	.244									-.143									10
11	-.139																			11
	$\alpha = 00°$										$\delta = 10°$									
1	.344	.310	.302	.303	.306			-.341			.072	.058	.043	.506	.277		.261	-.072		1
2	.061	.038	.030	.432	-.036						.034		.008	-.016	.164		-.085			2
3	.027	.011	.009	.000	-.073		-.324				.038	.009	.085	.046	.192		-.073			3
4	.039	.009	.083	-.070	-.126		-.315				.007	.003	-.029	-.129	.097					4
5	.028	.005	-.032	-.163	-.066						.023	.104	-.018	-.133	-.077					5
6	.015	.122	-.041	-.180							.007	.031	-.088	-.143						6
7	.006	.021	-.186	-.172	-.188						.071	-.166	-.085							7
8		-.166	-.178								-.077	-.151	-.096							8
9	-.075	-.160	-.187								-.048	-.101								9
10	-.049	.245									-.143									10
11	-.136																			11
	$\alpha = 00°$										$\delta = 20°$									
1	.346	.311	.302	.302	.244			-.364			.074	.059	.041	.505	.519	.507	.447	.135		1
2	.064	.039	.032	.439	-.232	-.323					.033		.007	-.015	.397	.426	.070			2
3	.031	.013	.011	.002	-.166	-.290	-.377				.040	.013	.083	.071	.440	.245	.108			3
4	.043	.010	.084	-.154	-.135	-.294	-.369				.009	.003	-.034	-.125	.044	.047				4
5	.030	.005	-.032	-.227	-.141	-.335					.025	.102	.055	-.182	.007					5
6	.017	.123	-.049	-.225							.008	.033	-.040	-.168						6
7	.010	.023	-.217	-.215	-.244						.069	-.164	-.054							7
8		-.162	-.224								-.076	-.097	-.072							8
9	-.072	-.164	-.227								-.044	-.043								9
10	-.048	.248									-.145									10
11	-.131																			11
	$\alpha = 00°$										$\delta = 30°$									
1	.343	.307	.300	.298	.038			-.365			.069	.055	.036	.498	.851	.731	.641	.425		1
2	.060	.035	.027	.442	-.337	-.370					.028		.003	-.018	.785	.644	.350			2
3	.026	.011	.009	-.002	-.213	-.364	-.406				.036	.005	.079	.089	.708	.480	.392			3
4	.038	.007	.081	-.385	-.275	-.385	-.393				.003	-.001	-.037	-.147	.207	.295				4
5	.024	.003	-.034	-.404	-.324	-.400					.020	.098	.172	-.273	.176					5
6	.013	.123	-.065	-.304							.002	.027	-.007	-.304						6
7	.006	.021	-.254	-.220	-.336						.063	-.168	-.025							7
8		-.166	-.271								-.082	-.002	-.077							8
9	-.076	-.179	-.282								-.050	.006								9
10	-.057	.244									-.138									10
11	-.134																			11

[redacted]

Table 16 Continued

Pressure Coefficients on Delta Wing with Control

Configuration F3 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station								Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 03°									δ = 00°									
1	.338	.233	.226	.196	.316			-.378		.139	.147	.152	.708	.142	.152	.212	-.086		1
2	-.009	-.070	-.123	-.014	-.083	-.200				.086		.085	.094	.089	.172	-.096			2
3	-.020	-.046	-.046	-.117	-.072	-.129	-.349			.081	.060	.184	.067	.094	.093	-.088			3
4	-.007	-.039	-.009	-.073	-.057	-.156	-.343			.063	.051	.071	-.091	.108	-.079				4
5	-.030	-.044	-.159	-.180	-.107	-.283				.075	.188	.008	-.088	-.077					5
6	-.027	.056	-.122	-.188						.053	.085	-.094	-.084						6
7	-.023	-.064	-.185	-.192	-.246					.172	-.046	-.086							7
8		-.216	-.176							-.022	-.099	-.091							8
9	-.125	-.227	-.185							-.016	-.089								9
10	-.104	.251								-.098									10
11	-.191																		11
	α = 06°									δ = -30°									
1	.318	.167	.150	.109	.292			.146		.208	.233	.238	.894	-.287	-.292	-.285	-.343		1
2	-.068	-.216	-.318	-.127	.592	.576				.143		.162	.160	-.090	-.311	-.352			2
3	-.050	-.089	-.090	-.233	.411	.501	.039			.140	.124	.296	-.213	-.123	-.303	-.368			3
4	-.033	-.083	-.054	-.061	.544	.240	.018			.123	.109	.154	-.286	-.170	-.284				4
5	-.070	-.082	-.224	-.242	.038	-.012				.119	.273	.001	-.281	-.268					5
6	-.053	.009	-.050	-.247						.126	.156	-.181	-.265						6
7	-.059	-.109	-.069	-.269	-.105					.262	-.044	-.207							7
8		-.265	-.111							.033	-.072	-.193							8
9	-.156	-.170	-.151							.006	-.099								9
10	-.116	.264								-.049									10
11	-.211																		11
	α = 06°									δ = -20°									
1	.318	.168	.152	.111	.359			-.080		.205	.230	.235	.892	-.200	-.198	-.179	-.290		1
2	-.069	-.216	-.316	-.121	.244	.324				.139		.160	.150	-.031	-.189	-.283			2
3	-.050	-.090	-.094	-.232	.180	.289	-.122			.137	.121	.290	-.094	-.028	-.157	-.298			3
4	-.034	-.084	-.056	-.066	.264	.103	-.151			.121	.110	.123	-.170	-.069	-.198				4
5	-.073	-.083	-.224	-.212	-.098	-.172				.118	.265	.022	-.164	-.204					5
6	-.057	.010	-.164	-.206						.114	.143	-.162	-.164						6
7	-.060	-.110	-.117	-.207	-.187					.252	-.043	-.157							7
8		-.262	-.128							.020	-.065	-.137							8
9	-.156	-.287	-.154							.002	-.092								9
10	-.119	.265								-.051									10
11	-.211																		11
	α = 06°									δ = -10°									
1	.318	.167	.150	.113	.349			-.280		.203	.228	.234	.887	.012	-.004	.055	-.163		1
2	-.076	-.216	-.316	-.118	-.083	.024				.138		.159	.152	.005	.077	-.141			2
3	-.052	-.092	-.093	-.226	-.027	.008	-.267			.136	.121	.290	.022	.083	.033	-.145			3
4	-.037	-.085	-.057	-.084	.056	-.067	-.289			.122	.106	.127	-.101	.043	-.115				4
5	-.072	-.084	-.226	-.201	-.157	-.275				.118	.266	.039	-.106	-.126					5
6	-.057	.011	-.203	-.193						.111	.141	-.124	-.108						6
7	-.063	-.110	-.160	-.192	-.233					.251	-.045	-.104							7
8		-.265	-.166							.022	-.060	-.093							8
9	-.159	-.289	-.175							.003	-.080								9
10	-.123	.263								-.052									10
11	-.213																		11
	α = 06°									δ = 00°									
1	.315	.164	.150	.113	.275			-.252		.200	.229	.233	.888	.125	.199	.243	-.093		1
2	-.073	-.217	-.314	-.114	-.034	-.151				.135		.158	.153	.078	.216	-.093			2
3	-.052	-.091	-.092	-.230	-.042	-.064	-.270			.136	.119	.288	.116	.205	.136	-.060			3
4	-.038	-.086	-.056	-.125	-.047	-.118	-.254			.119	.103	.126	-.055	.134	-.056				4
5	-.079	-.084	-.217	-.222	-.142	-.258				.116	.265	.052	-.046	-.053					5
6	-.059	.009	-.204	-.229						.110	.137	-.056	-.044						6
7	-.063	-.109	-.188	-.225	-.207					.250	-.044	-.052							7
8		-.266	-.197							.020	-.059	-.042							8
9	-.158	-.287	-.205							.002	-.048								9
10	-.127	.263								-.056									10
11	-.211																		11

[redacted]

Table 16 Continued

Pressure Coefficients on Delta Wing with Control

Configuration F3 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
								α = 06°		δ = 10°									
1	.314	.165	.150	.111	.226			-.328		.201	.228	.233	.885	.374	.500	.436	.112		1
2	-.074	.218	-.314	-.115	-.234	-.294				.135		.157	.149	.289	.409	.063			2
3	-.051	-.090	-.093	-.227	-.121	-.244	-.357			.137	.116	.287	.166	.406	.315	.097			3
4	-.039	-.086	-.056	-.167	-.156	-.286	-.340			.121	.106	.127	-.049	.239	.071				4
5	-.075	-.085	-.225	-.241	-.177	-.361				.115	.263	.094	-.057	.032					5
6	-.057	.011	-.203	-.241						.109	.138	.001	-.120						6
7	-.062	-.110	-.212	-.226	-.241					.245	-.046	-.005							7
8		-.265	-.222							.019	-.033	-.012							8
9	-.159	-.287	-.231							.005	.017								9
10	-.129	.263								-.058									10
11	-.211																		11
								α = 06°		δ = 20°									
1	.315	.166	.149	.112	.093			-.352		.202	.227	.232	.885	.696	.700	.604	.373		1
2	-.073	-.216	-.315	-.113	-.341	-.368				.132		.154	.149	.616	.600	.278			2
3	-.053	-.090	-.093	-.225	-.266	-.346	-.381			.140	.117	.287	.208	.674	.497	.352			3
4	-.039	-.086	-.057	-.233	-.262	-.365	-.368			.122	.104	.125	-.042	.377	.296				4
5	-.077	-.084	-.225	-.309	-.233	-.396				.117	.262	.209	-.157	.173					5
6	-.059	.013	-.203	-.277						.108	.136	.055	-.203						6
7	-.063	-.108	-.235	-.243	-.312					.246	-.042	.047							7
8		-.262	-.250							.018	.069	.015							8
9	-.158	-.284	-.261							.006	.071								9
10	-.131	.261								-.056									10
11	-.212																		11
								α = 06°		δ = 30°									
1	.319	.169	.151	.112	-.102			-.355		.203	.228	.234	.885	1.082	.872	.716	.573		1
2	-.072	-.215	-.313	-.111	-.386	-.405				.137		.158	.152	.962	.830	.619			2
3	-.052	-.090	-.092	-.224	-.332	-.386	-.393			.143	.117	.287	.282	.904	.621	.591			3
4	-.037	-.085	-.056	-.311	-.303	-.402	-.376			.122	.106	.126	-.093	.581	.595				4
5	-.075	-.081	-.221	-.438	-.337	-.399				.118	.262	.335	-.232	.418					5
6	-.060	.016	-.202	-.376						.112	.138	.118	-.251						6
7	-.063	-.105	-.261	-.311	-.358					.244	.044	.047							7
8		-.262	-.279							.021	.147	.030							8
9	-.156	-.286	-.300							.013	.113								9
10	-.130	.262								.018									10
11	-.195																		11
								α = 09°		δ = 00°									
1	.277	.092	.056	.013	.182			-.352		.286	.316	.318	1.071	.208	.441	.376	.073		1
2	-.163	-.369	-.419	-.275	-.258	-.335				.206		.242	.226	.152	.362	.024			2
3	-.093	-.141	-.189	-.418	-.181	-.266	-.385			.207	.185	.411	.182	.362	.276	.061			3
4	-.079	-.130	-.103	-.206	-.152	-.222	-.375			.179	.175	.193	-.006	.225	.040				4
5	-.108	-.129	-.259	-.288	-.254	-.384				.193	.342	.110	.007	.010					5
6	-.101	-.035	-.292	-.258						.283	.241	.007	.018						6
7	-.101	-.156	-.352	-.260	-.324					.321	.010	.053							7
8		-.288	-.230							.057	-.014	.047							8
9	-.185	-.307	-.214							.043	.012								9
10	-.163	.294								-.021									10
11	-.232																		11
								α = 12°		δ = -30°									
1	.239	.017	-.048	-.056	.286			.042		.356	.384	.392	1.209	-.232	-.229	-.251	-.351		1
2	-.275	-.439	-.467	-.437	.430	.405				.267		.308	.344	-.075	-.266	-.331			2
3	-.125	-.219	-.400	-.451	.278	.394	-.032			.259	.259	.492	-.175	-.099	-.101	-.343			3
4	-.115	-.190	-.177	-.298	.317	.239	-.085			.245	.241	.307	-.250	-.162	-.253				4
5	-.149	-.184	-.299	-.331	.053	-.196				.250	.425	.134	-.196	-.265					5
6	-.132	-.102	-.343	-.312						.448	.332	-.064	-.160						6
7	-.138	-.171	-.178	-.306	-.353					.386	.046	-.090							7
8		-.312	-.180							.101	.005	-.097							8
9	-.199	-.335	-.223							.067	-.027								9
10	-.167	.304								.024									10
11	-.246																		11

[redacted]

Table 16 Continued

Pressure Coefficients on Delta Wing with Control

Configuration F3 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 12°									δ = −20°									
1	.242	.022	−.044	−.055	.358	.080		−.218		.358	.387	.394	1.208	−.177	−.003	−.025	−.251		1
2	−.273	−.434	−.464	−.439	.100	.106	−.181			.270		.308	.285	.051	.015	−.193			2
3	−.119	−.213	−.393	−.456	−.060	.094	−.220			.265	.263	.489	−.006	.027	−.009	−.178			3
4	−.110	−.187	−.176	−.276	.078	−.291				.249	.244	.261	−.109	−.019	−.169				4
5	−.141	−.180	−.288	−.281	−.138					.254	.408	.142	−.094	−.182					5
6	−.126	−.097	−.341	−.273						.436	.323	−.034	−.067						6
7	−.132	−.170	−.294	−.233	−.345					.368	.043	−.028							7
8		−.308	−.192							.092	.013	−.038							8
9	−.196	−.328	−.201							.067	−.016								9
10	−.168	.306								.022									10
11	−.244																		11
	α = 12°									δ = −10°									
1	.243	.020	−.045	−.053	.264			−.386		.359	.387	.395	1.203	.051	.254	.238	−.042		1
2	−.271	−.435	−.468	−.438	−.247	−.264				.271		.308	.287	.077	.203	−.047			2
3	−.123	−.215	−.393	−.460	−.196	−.202	−.340			.264	.262	.492	.127	.193	.131	−.041			3
4	−.110	−.188	−.178	−.305	−.086	−.103	−.323			.248	.245	.262	−.019	.141	−.037				4
5	−.141	−.179	−.287	−.294	−.297	−.358				.253	.409	.149	−.013	−.064					5
6	−.125	−.097	−.340	−.238						.434	.321	.023	.012						6
7	−.133	−.172	−.373	−.193	−.349					.368	.046	.024							7
8		−.308	−.234							.092	.017	.015							8
9	−.197	−.329	−.208							.067	.000								9
10	−.174	.308								.020									10
11	−.246																		11
	α = 12°									δ = 00°									
1	.237	.017	−.048	−.056	.165			−.240		.353	.381	.388	1.200	.150	.438	.369	.040		1
2	−.273	−.421	−.457	−.439	−.168	−.197				.263		.304	.285	.128	.344	.008			2
3	−.125	−.218	−.395	−.451	−.100	−.147	−.290			.258	.256	.489	.232	.379	.286	.055			3
4	−.116	−.193	−.178	−.335	−.119	−.188	−.281			.242	.237	.258	.044	.233	.050				4
5	−.148	−.186	−.278	−.350	−.262	−.320				.247	.403	.177	.069	.053					5
6	−.133	−.101	−.341	−.326						.428	.316	.087	.117						6
7	−.140	−.179	−.408	−.282	−.262					.362	.036	.080							7
8		−.312	−.266							.086	.028	.072							8
9	−.202	−.332	−.200							.063	.048								9
10	−.180	.303								.015									10
11	−.251																		11
	α = 12°									δ = 10°									
1	.237	.016	−.047	−.056	.147			−.287		.355	.382	.393	1.204	.377	.628	.525	.261		1
2	−.267	−.434	−.464	−.439	−.264	−.283				.269		.305	.286	.333	.517	.224			2
3	−.126	−.217	−.393	−.463	−.205	−.254	−.325			.259	.258	.491	.306	.580	.449	.266			3
4	−.115	−.193	−.178	−.292	−.190	−.286	−.318			.245	.238	.263	.067	.362	.222				4
5	−.146	−.183	−.285	−.348	−.299	−.358				.249	.404	.247	.077	.140					5
6	−.132	−.102	−.340	−.300						.432	.318	.156	.021						6
7	−.127	−.179	−.410	−.303	−.288					.364	.040	.146							7
8		−.315	−.288							.089	.093	.116							8
9	−.199	−.330	−.188							.067	.106								9
10	−.182	.306								.015									10
11	−.246																		11
	α = 12°									δ = 20°									
1	.236	.015	−.047	−.057	−.039			−.316		.353	.380	.390	1.199	.797	.815	.677	.527		1
2	−.274	−.442	−.470	−.441	−.356	−.358				.266		.303	.283	.813	.777	.582			2
3	−.128	−.220	−.390	−.480	−.318	−.346	−.370			.258	.257	.489	.406	.838	.556	.551			3
4	−.118	−.192	−.183	−.297	−.325	−.369	−.360			.244	.238	.259	.040	.559	.568				4
5	−.140	−.185	−.303	−.316	−.373	−.385				.248	.404	.409	−.046	.303					5
6	−.132	−.101	−.336	−.320						.428	.318	.236	−.027						6
7	−.139	−.183	−.409	−.311	−.354					.360	.089	.157							7
8		−.320	−.300							.085	.184	.130							8
9	−.202	−.339	−.191							.069	.158								9
10	−.186	.303								.060									10
11	−.246																		11

[redacted]

Table 16 Concluded

Pressure Coefficients on Delta Wing with Control

Configuration F3 M = 1.61 R = 4.2 x 10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
								α = 12°					δ = 30°							
1	.234	.014	-.051	-.057	-.201	-.400		-.346			.348	.378	.390	1.197	1.194	.956	.859	.683		1
2	-.277	-.440	-.473	-.443	-.402	-.392	-.394				.262		.301	.282	1.124	1.071	.869			2
3	-.127	-.221	-.393	-.486	-.375	-.406	-.381				.258	.253	.487	.428	1.068	.821	.748			3
4	-.119	-.196	-.183	-.348	-.389	-.408					.243	.234	.264	.076	.717	.725				4
5	-.149	-.187	-.307	-.399	-.418						.244	.401	.511	-.076	.469					5
6	-.134	-.103	-.335	-.381							.427	.380	.249	-.155						6
7	-.142	-.183	-.411	-.322	-.387						.361	.216	.254							7
8		-.321	-.379								.104	.222	.210							8
9	-.205	-.339	-.220								.171	.208								9
10	-.183	.303									.226									10
11	-.234																			11
								α = 15°					δ = 00°							
1	.201	-.052	-.163	-.059	.117	-.249		-.265			.417	.447	.451	1.314	.163	.563	.475	.208		1
2	-.365	-.452	-.446	-.432	-.225	-.233	-.309				.325		.373	.370	.178	.451	.169			2
3	-.148	-.323	-.401	-.412	-.190	-.269	-.310				.316	.320	.582	.363	.463	.399	.219			3
4	-.138	-.293	-.325	-.348	-.174	-.374					.307	.366	.382	.131	.327	.169				4
5	-.174	-.150	-.403	-.393	-.258						.323	.540	.338	.167	.164					5
6	-.158	-.080	-.422	-.366							.534	.372	.145	.153						6
7	-.166	-.197	-.258	-.314	-.354						.415	.081	.131							7
8		-.335	-.231								.127	.100	.118							8
9	-.215	-.354	-.300								.102	.106								9
10	-.195	.296									.059									10
11	-.262																			11
								α = -06°					δ = 00°							
1	.281	.267	.103	.141	.353	.147		-.119			-.064	-.259	-.312	-.138	-.143	-.210	-.242	-.327		1
2	.193	.206	.230	.907	.123	.224	-.108				-.047		-.104	-.218	-.067	-.094	-.327			2
3	.132	.140	.174	.188	.091	.152	-.133				-.054	-.077	-.044	-.130	-.056	-.171	-.293			3
4	.129	.109	.289	.122	.192	-.075					-.071	-.086	-.220	-.231	-.145	-.259				4
5	.135	.114	.118	-.047	.134						-.057	-.005	-.203	-.225	-.223					5
6	.117	.282	.040	-.056							-.069	-.106	-.180	-.217						6
7	.134	.139	-.070	-.054	-.080						-.035	-.261	-.187							7
8		-.046	-.060								-.163	-.281	-.196							8
9	.021	-.068	-.049								-.126	-.199								9
10	.038	.329									-.230									10
11	-.050																			11
								α = -06°					δ = 20°							
1	.280	.265	.097	.133	.261	-.204		-.300			-.068	-.263	-.319	-.149	.273	.339	.276	-.050		1
2	.195	.204	.226	.906	-.208	-.190	-.303				-.051		-.110	-.228	.189	.300	-.098			2
3	.134	.139	.170	.185	-.058	-.182	-.312				-.057	-.080	-.051	-.069	.281	.056	-.085			3
4	.127	.109	.287	-.076	-.035	-.226					-.076	-.091	-.229	-.216	-.087	-.146				4
5	.134	.111	.116	-.161	-.089						-.060	-.018	-.117	-.212	-.163					5
6	.114	.282	.025	-.155							-.072	-.110	-.119	-.209						6
7	.135	.138	-.170	-.158	-.208						-.042	-.267	-.130							7
8		-.045	-.167								-.167	-.284	-.150							8
9	.020	-.075	-.150								-.128	-.099								9
10	.032	.324									-.238									10
11	-.048																			11

[redacted]

Table 17

Pressure Coefficients on Delta Wing with Control

Configuration G M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
	α = 00°										δ = 00°									
1	.385	.350	.277	.272	.210		.284	-.239										-.276		1
2	.055	.027	.020	.018	.052	.064					.083		.048		.033	.006	.013			2
3	.017	.011		.015	.036	.033	-.169				.042	.028	.013		.014	.001	-.212			3
4	.027	-.009	-.018	-.023	.027	.018	-.188				.042		.000	-.015	.006	-.011	-.219			4
5	.008	-.002	-.003	-.130		-.157					.006	.017	-.015	-.135	-.003	-.189				5
6	.005	.047	.007	-.130							.025	.038	.020	-.140	-.143					6
7	.031	.025	-.149	-.131	-.117						.025	.021	-.137	-.139	-.148					7
8	.006	-.146	-.155								.019	-.130	-.138							8
9	-.145	-.146	-.157								-.136	-.127	-.135							9
10	-.079	-.146									-.066	-.129								10
11	-.142										-.129									11
	α = 00°										δ = 10°									
1	.383	.354	.282	.275	-.217		.186	-.343										-.007		1
2	.055	.033	.025	.025	-.070	-.254					.084		.048		.237	.286	.325			2
3	.020	.016		.048	-.051	-.229	-.325				.039	.031	.015		.161	.222	-.070			3
4	.026	-.002	-.011	-.128	-.047	-.189	-.335				.046		-.005	.046	.197	.188	-.058			4
5	.010	-.001	.020	-.199		-.224					.000	.012	-.027	-.129	.091	-.071				5
6	.004	.052	-.037	-.205							.022	.036	.082	-.161	-.080					6
7	.036	.045	-.203	-.199	-.195						.022	.019	-.080	-.161	-.081					7
8	.007	-.143	-.200								.016	-.127	-.086							8
9	-.136	-.159	-.204								-.149	-.092	-.088							9
10	-.072	-.174									-.070	-.091								10
11	-.136										-.140									11
	α = 00°										δ = 20°									
1	.385	.353	.286	.273	-.325		.045	-.377										.217		1
2	.053	.036	.026	.025	-.310	-.343					.073		.038		.584	.563	.538			2
3	.018	.015		.400	-.125	-.350	-.383				.022	.021	.004		.375	.482	.084			3
4	.029	-.002	-.008	-.292	-.126	-.339	-.388				.043		-.021	-.019	.455	.385	.133			4
5	.012	.002	.169	-.304		-.338					-.001	.001	-.042	-.268	.261	.054				5
6	.003	.054	-.016	-.338							.019	.027	.125	-.270	.022					6
7	.035	.094	-.233	-.340	-.272						.017	.006	-.030	-.229	.058					7
8	.007	-.123	-.271								.006	-.143	-.032							8
9	-.133	-.154	-.275								-.167	-.057	-.061							9
10	-.038	-.177									-.070	-.045								10
11	-.098										-.145									11
	α = 00°										δ = 30°									
1	.384	.354	.286	.275	-.389		.102	-.369										.523		1
2	.055	.029	.024	.021	-.396	-.394					.070		.045		.918	.847	.729			2
3	.022	.014		.314	-.240	-.403	-.372				.034	.021	.007		.730	.788	.367			3
4	.030	-.002	-.012	-.477	-.255	-.382	-.388				.049		-.016	-.171	.805	.634	.449			4
5	.010	.002	.284	-.406		-.372					-.003	.006	-.042	-.330	.646	.351				5
6	.001	.056	.088	-.460							.017	.033	.224	-.276	.204					6
7	.039	.175	-.223	-.442	-.316						.019	.003	.057	-.331	.299					7
8	.016	-.069	-.303								.002	-.089	.005							8
9	-.053	-.130	-.340								-.154	-.027	-.034							9
10	.038	-.170									-.051	.023								10
11	-.013										-.019									11
	α = 06°										δ = 00°									
1	.327	.087	.124	-.010	-.353		.085	-.393										-.059		1
2	-.094	-.290	-.344	-.382	-.353	-.387					.206		.247		.271	.257	.271			2
3	-.077	-.093		-.218	-.332	-.364	-.398				.142	.152	.154		.247	.201	-.006			3
4	-.059	-.106	-.132	-.165	-.239	-.348	-.398				.163		.120	.123	.193	.180	-.040			4
5	-.097	-.103	-.108	-.209		-.281					.107	.121	.098	-.040	.153	-.015				5
6	-.085	-.052	-.102	-.228							.128	.140	.134	-.041	-.019					6
7	-.052	-.052	-.227	-.236	-.270						.110	.126	-.049	-.040	-.001					7
8	-.076	-.216	-.233								.110	-.064	-.056							8
9	-.218	-.214	-.237								-.064	-.051	-.056							9
10	-.155	-.221									.001	-.051								10
11	-.195										-.085									11

Table 17 Continued

Pressure Coefficients on Delta Wing with Control

Configuration G M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
								α = 06°				δ = 10°							
1	.332	.098	.138	-.002	-.366		.014	-.402		.208		.247		.336	.565	.504	.161		1
2	-.089	-.285	-.335	-.349	-.389	-.414				.138	.153	.153		.322	.455	.066			2
3	-.070	-.081		-.067	-.349	-.403	-.405			.151		.112	.270	.600	.359	.106			3
4	-.054	-.097	-.121	-.193	-.192	-.387	-.406			.108	.125	.064	.008	.325	.066				4
5	-.086	-.095	-.047	-.233		-.370				.121	.136	.189	-.021	.080					5
6	-.074	-.037	-.150	-.236						.106	.108	.025	-.110	.068					6
7	-.042	-.002	-.286	-.224	-.262					.107	-.072	.014							7
8	-.073	-.192	-.304							-.083	-.017	.014							8
9	-.178	-.220	-.267							-.003	.002								9
10	-.113	-.245								-.105									10
11	-.151																		11
								α = 06°				δ = 20°							
1	.328	.096	.143	-.005	-.389		-.080	-.381		.206		.249		.580	.793	.675	.453		1
2	-.088	-.274	-.339	-.305	-.412	-.428				.138	.155	.153		.661	.765	.281			2
3	-.071	-.080		.205	-.368	-.412	-.402			.151		.112	.305	.634	.584	.373			3
4	-.053	-.096	-.067	-.389	-.253	-.406	-.402			.109	.116	.049	-.002	.683	.294				4
5	-.083	-.094	.121	-.372		-.392				.114	.142	.258	-.124	.281					5
6	-.078	.019	-.146	-.281						.114	.109	.105	-.181	.251					6
7	-.047	.044	-.268	-.347	-.301					.101	-.081	.064							7
8	-.032	-.178	-.327							-.083	.045	.084							8
9	-.091	-.218	-.340							.014	.055								9
10	-.044	-.244								-.100									10
11	-.115																		11
								α = 06°				δ = 30°							
1	.326	.093	.132	-.006	-.410		-.162	-.388		.199		.241		1.022	1.019	.860	.658		1
2	-.093	-.287	-.340	-.219	-.436	-.427				.142	.161	.155		.935	1.019	.693			2
3	-.075	-.090		.100	-.387	-.427	-.407			.159		.117	.282	.814	.777	.615			3
4	-.059	-.098	-.041	-.426	-.317	-.408	-.407			.112	.128	.064	.027	.983	.618				4
5	-.092	-.100	.221	-.258		-.392				.127	.140	.328	-.192	.630					5
6	-.087	.138	-.086	-.352						.114	.104	.142	-.214	.540					6
7	-.050	.112	-.317	-.298	-.348					.108	.017	.178							7
8	.137	-.166	-.322							-.074	.106	.142							8
9	.033	-.186	-.331							.034	.121								9
10	.019	-.206								.006									10
11	-.065																		11
								α = 12°				δ = 00°							
1	.207	-.098	-.022	-.180	-.290		-.005	-.356		.348		.394		.422	.400	.399	.063		1
2	-.290	-.425	-.448	-.470	-.300	-.312				.279	.282	.293		.363	.348	-.003			2
3	-.136	-.187		-.444	-.246	-.311	-.368			.286		.254	.276	.326	.286	.037			3
4	-.114	-.179	-.229	-.355	-.282	-.284	-.356			.242	.244	.213	.058	.283	.012				4
5	-.164	-.183	-.191	-.348		-.322				.242	.277	.250	.058	.063					5
6	-.142	-.163	-.177	-.363						.202	.229	.037	.059	.014					6
7	-.131	-.112	-.273	-.333	-.247					.235	.018	.037							7
8	-.137	-.271	-.275							.031	.043	.050							8
9	-.264	-.266	-.277							.056	.043								9
10	-.196	-.267								.032									10
11	-.218																		11
								α = 12°				δ = 10°							
1	.202	-.103	-.025	-.184	-.340		-.093	-.361		.349		.400		.604	.691	.603	.366		1
2	-.287	-.436	-.469	-.462	-.349	-.363				.277	.286	.281		.557	.624	.187			2
3	-.137	-.185		-.083	-.321	-.351	-.361			.292		.253	.461	.684	.523	.269			3
4	-.116	-.179	-.167	-.371	-.348	-.340	-.361			.247	.254	.186	.160	.535	.214				4
5	-.162	-.188	-.083	-.318		-.353				.246	.281	.333	.119	.244					5
6	-.146	-.078	-.244	-.281						.199	.227	.140	-.021	.195					6
7	-.128	-.067	-.361	-.245	-.312					.229	.020	.121							7
8	-.110	-.247	-.308							.023	.078	.137							8
9	-.208	-.289	-.250							.057	.117								9
10	-.121	-.312								-.006									10
11	-.163																		11

[redacted]

Table 17 Continued

Pressure Coefficients on Delta Wing with Control

Configuration G M = 1.61 R = 4.2 x 10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
								α = 12°					δ = 20°							
1	.205	-.102	-.024	-.181	-.389		-.175	-.372												1
2	-.294	-.435	-.453	-.266	-.389	-.385					.342		.404		.856	.953	.706	.554		2
3	-.134	-.185		.132	-.364	-.385	-.387				.267	.278	.279		.721	.920	.554			3
4	-.114	-.182	-.133	-.407	-.378	-.371	-.387				.284		.244	.554	.799	.681	.514			4
5	-.160	-.149	-.080	-.281		-.387					.236	.244	.180	.201	.862	.482				5
6	-.141	.016	-.098	-.164							.236	.266	.379	-.001	.487					6
7	-.086	-.034	-.350	-.169	-.357						.204	.214	.204	-.101	.443					7
8	-.013	-.204	-.310								.222	.015	.202							8
9	-.107	-.258	-.234								.007	.135	.204							9
10	-.083	-.274									.083	.142								10
11	-.164										-.022									11
								α = 12°					δ = 30°							
1	.204	-.101	-.023	-.157	-.417		-.249	-.355												1
2	-.290	-.430	-.302	-.173	-.395	-.385					.342		.394		1.206	1.182	.962	.719		2
3	-.136	-.170		-.193	-.385	-.385	-.381				.268	.272	.283		1.044	1.193	.876			3
4	-.117	-.145	-.044	-.421	-.385	-.385	-.381				.277		.236	.641	.939	1.000	.701			4
5	-.159	-.123	-.072	-.271		-.372					-.234	.236	.192	.156	1.215	.778				5
6	-.110	.158	-.072	-.328							.234	.262	.437	-.081	.832					6
7	.067	.053	-.308	-.317	-.391						.200	.210	.285	-.122	.664					7
8	.142	-.097	-.338								.214	.067	.285							8
9	-.036	-.192	-.308								.004	.231	.246							9
10	-.068	-.159									.086	.231								10
11	-.113										.038									11
								α = -.06°					δ = 00°							
1	.292	.363	.151	.146	.325		-.129	-.085												1
2	.181	.198	.221	.235	.263	.271					-.069		-.302		-.209	-.260	-.260	-.336		2
3	.127	.133		.129	.202	.213	-.100				-.050	-.082	-.119		-.190	-.267	-.263			3
4	.128	.100	.108	.120	.169	.171	-.069				-.047		-.105	-.143	-.102	-.202	-.301			4
5	.110	.105	.124	-.043		-.047					-.087	-.082	-.114	-.208	-.118	-.212				5
6	.106	.162	.116	-.045							-.066	-.058	-.085	-.228	-.232					6
7	.129	.122	-.065	-.043	-.052						-.060	-.063	-.218	-.235	-.195					7
8	.108	-.070	-.065								-.061	-.204	-.216							8
9	-.070	-.068	-.068								-.212	-.198	-.216							9
10	-.016	-.066									-.126	-.200								10
11	-.075										-.174									11
								α = -.06°					δ = 10°							
1	.299	.365	.156	.143	-.050		.205	-.252												1
2	.183	.199	.224	.237	.106	-.018					-.069		-.302		.167	.008	.031	-.248		2
3	.126	.135		.097	.078	.039	-.187				-.043	-.086	-.116		-.045	-.070	-.235			3
4	.125	.103	.110	-.011	.048	.031	-.187				-.043		-.108	-.240	-.152	-.041	-.235			4
5	.112	.106	.124	-.138		-.148					-.083	-.092	-.075	-.250	-.162	-.247				5
6	.101	.169	.085	-.147							-.064	-.065	-.050	-.222	-.231					6
7	.119	.131	-.101	-.151	-.166						-.064	-.037	-.180	-.222	-.228					7
8	.106	-.091	-.118								-.064	-.172	-.204							8
9	-.055	-.083	-.127								-.201	-.174	-.204							9
10	-.006	-.081									-.109	-.166								10
11	-.066										-.136									11
								α = -.06°					δ = 20°							
1	.291	.366	.150	.144	-.248		.142	-.331												1
2	.194	.197	.222	.238	-.116	-.219					-.075		-.302		.559	.284	.294	.010		2
3	.127	.134		.296	-.025	-.219	.298				-.040	-.087	-.118		.223	.140	-.082			3
4	.128	.107	.111	-.095	-.082	-.208	.311				-.049		-.108	-.261	.136	.139	-.080			4
5	.114	.108	.211	-.239		-.208					-.085	-.087	-.095	-.277	-.210	-.186				5
6	.101	.169	.065	-.220							-.068	-.070	.025	-.226	-.190					6
7	.125	.158	-.134	-.228	-.230						-.069	-.054	-.166	-.278	-.194					7
8	.106	-.073	-.153								-.061	-.148	-.189							8
9	-.050	-.096	-.169								-.211	-.130	-.171							9
10	.002	-.104									-.106	-.152								10
11	-.044										-.121									11

Table 17 Concluded

Pressure Coefficients on Delta Wing with Control

Configuration G M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	$\alpha = -06^\circ$									$\delta = 30^\circ$									
1	.295	.369	.151	.146	-.337		.019	-.365		-.069		-.301		.902	.578	.579	.266		1
2	.182	.202	.223	.241	-.316	-.319				-.043	-.084	-.109		.637	.432	.105			2
3	.133	.140		.007	-.117	-.339	-.371			-.043		-.109	-.212	.579	.358	.157			3
4	.129	.107	.113	-.320	-.218	-.314	-.369			-.086	-.080	-.094	-.306	-.049	.049				4
5	.119	.110	.269	-.356		-.314				-.060	-.064	.074	-.295	-.094					5
6	.103	.174	.146	-.363						-.063	-.043	-.104	-.333	-.022					6
7	.126	.236	-.149	-.365	-.301					-.063	-.124	-.139							7
8	.112	-.026	-.209							-.210	-.098	-.160							8
9	-.034	-.076	-.235							-.086	-.090								9
10	.054	-.097								-.061									10
11	.016																		11
	$\alpha = -12^\circ$									$\delta = 00^\circ$									
1	.165	.257	.009	-.089	.290		-.252	.002		-.255		-.442		-.314	-.366	-.349	-.389		1
2	.332	.341	.362	.367	.412	.408				-.114	-.164	-.343		-.314	-.376	-.332			2
3	.239	.236		.272	.361	.359	.018			-.114		-.183	-.321	-.303	-.325	-.364			3
4	.244	.223	.232	.258	.316	.306	.072			-.148	-.166	-.180	-.319	-.303	-.342				4
5	.221	.222	.252	.066		.071				-.121	-.166	-.145	-.331	-.317					5
6	.218	.291	.236	.057						-.121	-.121	-.261	-.317	-.283					6
7	.236	.239	.028	.058	.064					-.121	-.249	-.263							7
8	.216	.027	.025							-.251	-.249	-.262							8
9	.020	.025	.036							-.164	-.249								9
10	.068	.028								-.188									10
11	.016																		11
	$\alpha = -12^\circ$									$\delta = 10^\circ$									
1	.169	.262	.011	-.096	.206		-.070	-.075		-.258		-.448		.141	-.165	-.209	-.361		1
2	.323	.337	.367	.376	.243	.191				-.108	-.162	-.351		-.133	-.230	-.324			2
3	.237	.232		.244	.202	.186	-.083			-.108		-.183	-.396	-.338	-.283	-.324			3
4	.241	.218	.232	.087	.193	.153	-.075			-.146	-.164	-.130	-.342	-.325	-.349				4
5	.223	.223	.259	-.078		-.070				-.121	-.164	-.130	-.258	-.301					5
6	.218	.295	.219	-.078						-.121	-.093	-.263	-.232	-.294					6
7	.232	.237	-.016	-.091	-.121					-.121	-.211	-.283							7
8	.223	.012	-.041							-.247	-.217	-.276							8
9	.035	.009	-.052							-.137	-.250								9
10	.061	.002								-.137									10
11	.020																		11
	$\alpha = -12^\circ$									$\delta = 20^\circ$									
1	.160	.259	.007	-.103	-.166		.158	-.329		-.267		-.453		.560	.179	.135	-.165		1
2	.322	.334	.359	.367	.149	-.155				-.124	-.167	-.352		.279	-.005	-.228			2
3	.236	.235		.310	.064	-.140	-.241			-.118		-.193	-.441	.116	-.063	-.228			3
4	.237	.221	.231	.042	-.059	.058	-.249			-.146	-.166	-.151	-.365	-.367	-.329				4
5	.217	.221	.306	-.176		-.182				-.125	-.166	-.136	-.310	-.320					5
6	.215	.290	.186	-.159						-.126	-.111	-.254	-.286	-.345					6
7	.231	.250	-.032	-.166	-.218					-.131	-.190	-.282							7
8	.220	.005	-.064							-.259	-.216	-.273							8
9	.046	-.008	-.083							-.131	-.206								9
10	.076	-.016								-.120									10
11	.024																		11
	$\alpha = -12^\circ$									$\delta = 30^\circ$									
1	.161	.261	.009	-.104	-.262		.048	-.343		-.268		-.444		.868	.424	.346	.054		1
2	.331	.335	.365	.369	-.161	-.248				-.114	-.160	-.356		.593	.240	-.099			2
3	.241	.240		.415	-.024	-.255	-.313			-.114		-.189	-.384	.532	.071	-.075			3
4	.245	.224	.242	.079	-.155	-.157	-.317			-.148	-.170	-.140	-.388	-.310	-.276				4
5	.220	.221	.422	-.320		-.246				-.127	-.170	-.054	-.373	-.302					5
6	.216	.298	.229	-.298						-.127	-.107	-.218	-.365	-.331					6
7	.239	.315	-.063	-.261	-.278					-.127	-.204	-.254							7
8	.229	.038	-.088							-.233	-.147	-.267							8
9	.086	.002	-.116							-.077	-.175								9
10	.130	-.019								-.090									10
11	.077																		11

[redacted]

Table 18

Pressure Coefficients on Delta Wing with Control

Configuration H M = 1.61 R = 4.2 x 10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 00°									δ = 00°									
1	.347	.315	.305	.345	.437	.035		-.229		.077	.060	.041	.102	.123	.019	.015	-.252		1
2	.068	.045	.038	.097	.097	.010	-.198			.035		.010	-.001	.007	.002	-.213			2
3	.032	.022	.013	.005	.019	-.005	-.203			.031	.014	.002	-.040	-.003	-.020	-.199			3
4	.039	.019	.010	-.030	.009	-.173				.009	.006	-.030	-.164	-.017	.160				4
5	.032	.014	-.030	-.167	-.011					.027	.037	.020	-.138	-.153					5
6	.024	.071	.018	-.152						.009	.030	-.138	-.099						6
7	.016	.022	-.144	-.115	-.146					.026	-.130	-.132							7
8		-.133	-.143							-.116	-.125	-.143							8
9	-.111	-.137	-.155							-.060	-.132								9
10	-.054	.249								-.125									10
11	-.127																		11
	α = 00°									δ = 10°									
1	.354	.317	.309	.345	.328	-.126				.079	.062	.043	.039	.347	.218		-.093		1
2	.070	.049	.041	.039	.024	-.095				.036		.013	.073	.118	.153				2
3	.036	.024	.016	-.089	-.013	-.106				.040	.015	-.010	-.006	.057	.128				3
4	.045	.021	.029	-.066	-.059	-.204				.014	.007	.005	-.144	.070	.159				4
5	.037	.017	-.045	-.165	-.083					.034	.031	.073	-.193	-.049					5
6	.028	.085	-.018	-.202						.012	.048	-.097	-.091						6
7	.021	.018	-.173	-.188	-.202					.026	-.101	-.103							7
8		-.150	-.173							-.116	-.093	-.115							8
9	-.101	-.159	-.177							-.049	-.100								9
10	-.053	.219								-.097									10
11	-.125																		11
	α = 00°									δ = 20°									
1	.354	.319	.309	.347	.247	-.237		-.332		.079	.061	.040	.037	.576	.477	.463	.136		1
2	.072	.050	.044	.039	-.169	-.224	-.335			.039		.011	.181	.325	.401	.074			2
3	.037	.026	.019	-.007	-.062	-.259	-.324			.045	.015	-.011	-.115	.265	.324	.115			3
4	.048	.020	.033	-.219	-.121	-.283				.014	.007	.022	-.237	.184	.181				4
5	.037	.016	-.018	-.250	-.212					.032	.027	.144	-.232	.066					5
6	.024	.095	-.085	-.211						.012	.055	-.052	-.238						6
7	.023	.038	-.236	-.194	-.256					.028	-.055	-.079							7
8		-.148	-.223							-.119	-.047	-.089							8
9	-.078	-.174	-.228							-.034	-.057								9
10	-.035	.214								-.039									10
11	-.104																		11
	α = 00°									δ = 30°									
1	.349	.316	.308	.345	.094	-.324		-.338		.076	.058	.037	.034	.861	.736	.659	.421		1
2	.070	.048	.041	.037	-.297	-.319	-.376			.035		.009	.217	.653	.678	.336			2
3	.035	.022	.016	.566	-.152	-.349	-.360			.044	.012	-.014	-.237	.695	.548	.411			3
4	.047	.017	.041	-.384	-.207	-.361				.011	.003	.077	-.294	.354	.248				4
5	.033	.014	.079	-.378	-.312					.028	.024	.225	-.302	.260					5
6	.020	.151	-.126	-.257						.009	.134	-.040	-.313						6
7	.023	.072	-.295	-.228	-.314					.019	-.012	-.069							7
8		-.146	-.313							-.118	-.003	-.101							8
9	-.013	-.187	-.307							.044	-.031								9
10	.001	.203								.034									10
11	-.066																		11
	α = 03°									δ = 00°									
1	.343	.229	.235	.215	.345	-.250		-.368		.140	.148	.155	.252	.302	.209	.219	-.056		1
2	.004	-.059	-.110	-.128	-.053	-.206	-.348			.087		.090	.081	.182	.156	-.070			2
3	-.012	-.038	-.032	-.058	-.118	-.137	-.322			.084	.060	.076	.037	.146	.107	-.067			3
4	-.002	-.036	-.045	-.092	-.085	-.258				.058	.055	.041	-.112	.095	.169				4
5	-.019	-.034	-.066	-.206	-.094					.077	.104	.082	-.089	-.060					5
6	-.025	.023	-.036	-.191						.057	.081	-.089	-.074						6
7	-.011	-.030	-.182	-.136	-.248					.070	-.091	-.089							7
8		-.174	-.182							-.075	-.085	-.098							8
9	-.150	-.171	-.192							-.023	-.087								9
10	-.097	.249								-.092									10
11	-.158																		11

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Table 18 Continued

Pressure Coefficients on Delta Wing with Control

Configuration H M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
								α = 06°			δ = -30°									
1	.317	.162	.152	.120	.208			.190			.207	.232	.238	.241	-.263	-.282	-.280	-.347		1
2	-.073	-.222	-.319	-.359	.828	.469					.141		.165	.413	-.064	-.324	-.347			2
3	-.051	-.090	-.094	-.271	.614	.337	.078				.141	.124	.119	-.277	-.149	-.270	-.359			3
4	-.036	-.083	-.116	-.230	.392	.260	.080				.120	.110	.195	-.291	-.250	.088				4
5	-.072	-.081	.013	-.299	-.050	.117					.121	.200	-.002	-.246	-.222					5
6	-.058	-.036	.030	-.364							.103	.154	-.179	-.192						6
7	-.057	.028	-.136	-.375	-.002						.176	-.079	-.191							7
8		-.106	-.170								.040	-.103	-.195							8
9	-.179	-.127	-.194								.022	-.108								9
10	-.026	.225									-.043									10
11	-.044																			11
								α = 06°			δ = -20°									
1	.318	.167	.156	.124	.347			-.075			.206	.232	.238	.241	-.119	-.181	-.178	-.303		1
2	-.070	-.221	-.314	-.355	.568	.251					.141		.166	.052	.026	-.224	-.276			2
3	-.049	-.086	-.090	-.310	.282	.108	-.121				.141	.125	.132	-.115	-.054	-.082	-.292			3
4	-.033	-.081	-.111	-.193	-.042	.037	-.148				.123	.111	.092	-.169	-.136	.117				4
5	-.069	-.080	-.024	-.262	-.079	-.060					.120	.185	.048	-.184	-.237					5
6	-.054	-.031	-.028	-.315							.102	.125	-.130	-.166						6
7	-.055	-.006	-.165	-.271	-.143						.148	-.078	-.140							7
8		-.142	-.174								-.006	-.089	-.145							8
9	-.178	-.159	-.184								.000	-.092								9
10	-.068	.237									-.062									10
11	-.103																			11
								α = 06°			δ = -10°									
1	.320	.167	.158	.125	.444			-.291			.205	.230	.237	.302	.202	.078	.069	-.143		1
2	-.069	-.219	-.312	-.348	.343	-.030					.140		.163	.079	.169	.079	-.124			2
3	-.049	-.085	-.090	-.294	-.078	-.137	-.295				.142	.124	.167	.001	.109	.041	-.129			3
4	-.033	-.079	-.110	-.157	-.240	-.159	-.305				.121	.111	.076	-.096	.025	.151				4
5	-.069	-.079	-.069	-.227	-.123	-.220					.120	.179	.085	-.129	-.184					5
6	-.054	-.027	-.061	-.226							.098	.119	-.094	-.131						6
7	-.056	-.030	-.194	-.214	-.261						.137	-.065	-.098							7
8		-.176	-.192								-.021	-.069	-.101							8
9	-.177	-.183	-.206								-.006	-.073								9
10	-.090	.238									-.065									10
11	-.139																			11
								α = 06°			δ = 00°									
1	.318	.166	.155	.124	.325			-.318			.204	.229	.236	.400	.320	.240	.218	-.114		1
2	-.072	-.225	-.312	-.318	-.048	-.204					.135		.161	.137	.189	.178	-.101			2
3	-.049	-.088	-.090	-.131	-.175	-.156	-.314				.142	.120	.152	.093	.146	.136	-.078			3
4	-.035	-.081	-.095	-.148	-.165	-.190	-.306				.123	.107	.100	-.085	.128	.184				4
5	-.073	-.081	-.119	-.209	-.110	-.259					.116	.167	.132	-.055	-.061					5
6	-.057	-.020	-.079	-.229							.096	.129	-.052	-.057						6
7	-.057	-.073	-.213	-.165	-.207						.131	-.053	-.054							7
8		-.201	-.213								-.031	-.047	-.066							8
9	-.182	-.201	-.221								.007	-.047								9
10	-.118	.263									-.061									10
11	-.177																			11
								α = 06°			δ = 10°									
1	.317	.169	.158	.126	.247			-.346			.206	.230	.237	.236	.513	.442	.428	.102		1
2	-.068	-.219	-.309	-.309	-.232	-.316					.140		.162	.282	.476	.376	.051			2
3	-.049	-.085	-.009	-.249	-.204	-.286	-.364				.145	.121	.117	.140	.383	.311	.095			3
4	-.034	-.079	-.044	-.137	-.195	-.307	-.350				.124	.108	.139	-.040	.266	.193				4
5	-.073	-.079	-.111	-.204	-.162	-.347					.120	.147	.204	-.133	.120					5
6	-.057	.006	-.146	-.226							.097	.150	.005	.001						6
7	-.058	-.060	-.244	-.205	-.259						.116	-.014	-.014							7
8		-.211	-.225								-.040	-.005	-.024							8
9	-.164	-.243	-.226								.015	-.003								9
10	-.106	.233									-.026									10
11	-.161																			11

[redacted]

Table 18 Continued

Pressure Coefficients on Delta Wing with Control

Configuration H M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
								α = 06°					δ = 20°							
1	.321	.167	.154	.121	.165	-.372		-.355			.205	.228	.233	.230	.742	.734	.613	.367		1
2	-.065	-.219	-.313	-.297	-.337	-.355	-.381				.139		.158	.406	.620	.660	.287			2
3	-.049	-.088	-.093	-.116	-.289	-.373	-.370				.146	.119	.111	.100	.824	.529	.360			3
4	-.036	-.080	.076	-.325	-.252	-.396					.125	.106	.116	-.150	.449	.265				4
5	-.071	-.079	-.112	-.304	-.280						.120	.145	.289	-.212	.279					5
6	-.056	.068	-.185	-.263							.099	.184	.047	-.102						6
7	-.054	-.049	-.321	-.211	-.324						.115	.033	.022							7
8		-.219	-.314								-.042	.048	-.008							8
9	-.106	-.243	-.273								.061	.035								9
10	-.078	.236									.030									10
11	-.135																			11
								α = 06°					δ = 30°							
1	.317	.165	.153	.121	.003	-.398		-.356			.201	.229	.234	.233	1.002	.962	.733	.600		1
2	-.070	-.220	-.313	-.122	-.384	-.388	-.393				.138		.159	.484	.932	.923	.665			2
3	-.051	-.088	-.092	.560	-.337	-.400	-.381				.144	.117	.114	.042	.958	.657	.632			3
4	-.037	-.082	.158	-.371	-.325	-.406					.123	.106	.282	-.211	.714	.381				4
5	-.071	-.082	-.057	-.304	-.338						.118	.145	.339	-.194	.544					5
6	-.058	.148	-.219	-.272							.098	.272	.068	-.078						6
7	-.049	-.033	-.342	-.232	-.368						.114	.083	.033							7
8		-.221	-.296								.010	.072	.002							8
9	-.054	-.237	-.246								.141	.056								9
10	-.045	.229									.151									10
11	-.122																			11
								α = 09°					δ = 00°							
1	.278	.096	.062	.023	.259	-.174		-.207			.281	.313	.314	.566	.372	.287	.269	-.066		1
2	-.157	-.357	-.409	-.412	-.022	-.160	-.265				.198		.241	.212	.263	.233	-.072			2
3	-.088	-.138	-.198	-.366	-.110	-.200	-.254				.207	.187	.232	.159	.207	.193	-.033			3
4	-.076	-.128	-.132	-.233	-.200	-.279					.178	.173	.174	-.036	.184	.216				4
5	-.109	-.125	-.165	.215	-.216						.182	.244	.197	-.007	-.025					5
6	-.096	-.075	-.131	-.272							.152	.196	-.006	-.031						6
7	-.099	-.117	-.240	-.187	-.183						.203	-.001	-.011							7
8		-.241	-.244								.024	.007	-.019							8
9	-.209	-.231	-.249								.047	.003								9
10	-.148	.278									-.009									10
11	-.197																			11
								α = 12°					δ = -30°							
1	.242	.016	-.043	-.078	.280	.269		-.111			.372	.386	.398	.390	-.066	-.141	-.112	-.267		1
2	-.274	-.434	-.464	-.480	.790	.084	-.159				.270		.309	.423	.060	-.153	-.232			2
3	-.121	-.214	-.346	-.493	.568	-.046	-.192				.259	.261	.266	-.152	-.049	-.057	-.250			3
4	-.112	-.191	-.218	-.381	.263	-.253					.247	.244	.309	-.207	-.160	.131				4
5	-.141	-.183	-.085	.250	-.387						.253	.371	.162	-.163	-.233					5
6	-.129	-.151	-.131	-.375							.216	.263	-.072	-.135						6
7	-.132	-.018	-.280	-.363	-.315						.329	.019	-.093							7
8		-.183	-.295								.107	.019	-.098							8
9	-.237	-.209	-.297								.075	.006								9
10	-.057	.254									.035									10
11	-.088																			11
								α = 12°					δ = -20°							
1	.241	.016	-.041	-.073	.408	.059		-.281			.375	.388	.401	.393	.179	.013	.032	-.192		1
2	-.274	-.434	-.461	-.476	.568	-.095	-.281				.271		.314	.288	.179	.003	-.146			2
3	-.120	-.215	-.343	-.484	.287	-.181	-.300				.261	.261	.340	-.010	.057	.073	-.136			3
4	-.111	-.191	-.215	-.349	-.186	-.343					.246	.244	.246	-.107	-.063	.153				4
5	-.139	-.182	-.119	.262	-.374						.251	.341	.196	-.112	-.180					5
6	-.129	-.149	-.150	-.333							.215	.249	-.037	-.104						6
7	-.133	-.061	-.288	-.300	-.337						.296	.027	-.049							7
8		-.204	-.300								.086	.031	-.051							8
9	-.237	-.225	-.288								.072	.017								9
10	-.106	.265									.029									10
11	-.125																			11

[redacted]

Table 18 Continued

Pressure Coefficients on Delta Wing with Control

Configuration H M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
								α = 12°			δ = −10°									
1	.241	.019	−.040	−.073	.454			−.383			.375	.387	.399	.532	.396	.286	.268	.019		1
2	−.272	−.433	−.459	−.471	.315	−.237					.271		.311	.236	.333	.233	.009			2
3	−.119	−.212	−.345	−.461	−.206	−.288	−.376				.261	.261	.320	.115	.255	.183	.001			3
4	−.111	−.189	−.212	−.300	−.413	−.315	−.375				.247	.245	.275	−.020	.144	.202				4
5	−.138	−.179	−.169	.268	−.377	−.389					.252	.326	.213	−.054	−.121					5
6	−.128	−.146	−.166	−.279							.217	.265	−.003	−.061						6
7	−.133	−.093	−.296	−.258	−.360						.285	.037	−.006							7
8		−.232	−.286								.083	.037	−.006							8
9	−.236	−.245	−.279								.087	.030								9
10	−.138	.272									.044									10
11	−.170																			11
								α = 12°			δ = 00°									
1	.238	.011	−.049	−.083	.138			−.339			.373	.386	.397	.664	.501	.410	.406	.102		1
2	−.283	−.438	−.468	−.458	−.152	−.345					.270		.311	.306	.391	.360	.056			2
3	−.125	−.219	−.372	−.464	−.279	−.330	−.373				.261	.262	.304	.237	.331	.303	.096			3
4	−.118	−.193	−.177	−.345	−.330	−.345	−.360				.250	.244	.271	.032	.300	.255				4
5	−.145	−.185	−.255	.292	−.319	−.372					.250	.316	.278	.064	.070					5
6	−.135	−.138	−.195	−.333							.213	.271	.057	.019						6
7	−.139	−.137	−.269	−.249	−.268						.275	.055	.051							7
8		−.279	−.286								.078	.068	.041							8
9	−.234	−.252	−.282								.100	.069								9
10	−.178	.298									.056									10
11	−.216																			11
								α = 12°			δ = 10°									
1	.237	.015	−.044	−.077	.083			−.350			.370	.382	.394	.385	.661	.583	.531	.266		1
2	−.275	−.436	−.449	−.443	−.283	−.386					.265		.307	.456	.632	.549	.190			2
3	−.123	−.216	−.376	−.479	−.339	−.377	−.384				.258	.255	.255	.316	.570	.453	.258			3
4	−.116	−.195	−.283	−.215	−.367	−.384	−.372				.245	.238	.320	.103	.472	.274				4
5	−.144	−.186	−.240	.252	−.367	−.387					.248	.287	.360	−.030	.266					5
6	−.131	−.110	−.305	−.326							.211	.305	.108	−.035						6
7	−.136	−.119	−.285	−.205	−.314						.244	.095	.096							7
8		−.282	−.282								.068	.107	.091							8
9	−.200	−.307	−.255								.118	.099								9
10	−.143	.258									.112									10
11	−.186																			11
								α = 12°			δ = 20°									
1	.238	.014	−.044	−.077	−.014			−.355			.369	.381	.392	.384	.937	.883	.660	.539		1
2	−.276	−.437	−.434	−.356	−.365	−.400					.266		.305	.555	.811	.853	.628			2
3	−.124	−.214	−.295	−.213	−.375	−.393	−.383				.257	.255	.255	.396	.977	.615	.578			3
4	−.116	−.195	−.079	−.293	−.397	−.400	−.373				.244	.239	.349	−.053	.717	.366				4
5	−.143	−.167	−.225	.246	−.395	−.391					.248	.285	.440	−.111	.535					5
6	−.131	−.077	−.258	−.209							.217	.364	.168	−.102						6
7	−.106	−.154	−.333	−.165	−.363						.244	.150	.133							7
8		−.277	−.266								.096	.152	.103							8
9	−.160	−.289	−.182								.183	.145								9
10	−.134	.251									.221									10
11	−.187																			11
								α = 12°			δ = 30°									
1	.237	.013	−.045	−.071	−.132			−.366			.369	.381	.392	.383	1.205	1.106	.888	.671		1
2	−.276	−.433	−.327	−.220	−.398	−.408					.266		.303	.577	1.048	1.102	.841			2
3	−.123	−.188	−.226	.461	−.394	−.402	−.391				.258	.253	.254	.342	1.152	.862	.726			3
4	−.115	−.123	−.203	−.217	−.408	−.409	−.382				.243	.238	.484	−.093	.961	.470				4
5	−.142	−.089	−.225	.257	−.405	−.399					.250	.286	.490	−.143	.780					5
6	−.103	.053	−.307	−.284							.227	.427	.207	−.170						6
7	.026	−.082	−.313	−.247	−.394						.274	.200	.149							7
8		−.230	−.283								.212	.212	.113							8
9	−.120	−.255	−.274								.303	.249								9
10	−.098	.262									.312									10
11	−.196																			11

[redacted]

Table 18 Concluded

Pressure Coefficients on Delta Wing with Control

Configuration H M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
	α = 15°										δ = 00°									
1	.200	-.064	-.180	-.179	.032			-.285			.430	.461	.460	.724	.544	.479	.455	.173		1
2	-.375	-.449	-.436	-.412	-.100	-.228					.338		.389	.419	.469	.459	.126			2
3	-.153	-.363	-.412	-.342	-.135	-.255	-.322				.325	.333	.415	.343	.434	.376	.216			3
4	-.145	-.321	-.402	-.341	-.216	-.316	-.325				.318	.350	.420	.115	.390	.295				4
5	-.175	-.156	-.361	.318	-.324	-.366					.345	.435	.394	.148	.155					5
6	-.163	-.124	-.384	-.356							.338	.395	.141	.098						6
7	-.166	-.167	-.350	-.259	-.342						.393	.145	.131							7
8		-.276	-.300								.170	.153	.121							8
9	-.258	-.283	-.300								.171	.148								9
10	-.196	.321									.143									10
11	-.230																			11

[redacted]

Table 19

Pressure Coefficients on Delta Wing with Control

Configuration 1 M = 1.61 R = 4.2 x 10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 00°									δ = 00°									
1	.400		.315	.302	.367	.393	.022					.035	.039	.021	.032				1
2	.063		.031	.030	.024	.024	-.256					.006	.000	.001	.019	-.264			2
3			.011	.009	.010	.011						-.013	.081	-.007	.008				3
4			-.005	.017	-.019	-.188						-.009		-.156	-.186				4
5			-.006	-.116	-.153	.177						.060	-.153	-.141	-.165				5
6			.024	-.138	-.143								-.139						6
7			-.096	-.134								-.135	-.138						7
8			-.131	-.142								-.136							8
9			-.143									-.132							9
10			-.145																10
	α = 00°									δ = 10°									
1	.408			.311	.374	.395	.019					.046	.049	.029	.035				1
2	.075			.042	.034	.029	-.255					.019	.010	.009	.020	-.261			2
3			.026	.022	.020	.016						-.001	.088	.000	.010				3
4			.011	.030	-.009	-.182						.004		-.098	-.186				4
5			.007	-.107	-.182	-.171						.072	.047	-.132	-.164				5
6			.038	-.262	-.196								.030						6
7			-.050	-.244								.110	.011						7
8			-.251	-.233								.140							8
9			-.294									.133							9
10			-.214																10
	α = 00°									δ = 20°									
1	.404	.306	.328	.313	.376	.395	.018			.078	.059	.046	.048	.028	.038				1
2	.070	.050	.046	.044	.035	.031	-.254			.040		.019	.010	.008	.019	-.262			2
3	.036	.024	.024	.023	.022	.019				.043	.019	-.002	.091	.000	.010				3
4	.041	.020	.010	.030	-.007	-.181				.015	.013	.002		-.064	-.186				4
5	.033	.021	.005	-.059	-.191	-.170				.031	-.004	.096	.340	-.178	-.153				5
6	.021	.038	.039	-.349	-.215					.046	.216		.324						6
7	.040	.026	.069	-.326						.241		.548	.262						7
8	.018	.129	-.342	-.314							.530	.561							8
9	.164	-.355	-.376							.411	.565	.477							9
10	-.339	-.357	-.245							.443	.491								10
11	-.353	-.245								.387									11
12	-.234																		12
	α = 00°									δ = 30°									
1	.398	.295	.315	.301	.366	.389	.009			.066	.045	.031	.032	.016	.032				1
2	.061	.038	.032	.030	.023	.024	-.265			.027		.002	-.005	-.003	.009	-.272			2
3	.026	.011	.009	.008	.009	.009				.032	.003	-.018	.361	.170	.000				3
4	.031	.007	-.005	.017	-.019	-.191				.003	-.002	-.013		.014	-.109				4
5	.023	.007	-.010	-.041	-.210	-.182				.018	.003	.424	.674	-.169	.034				5
6	.010	.024	.024	-.426	-.225					.220	.425		.684						6
7	.031	.020	.130	-.365						.390		.614	.513						7
8	.008	.205	-.414	-.389							.563	.840							8
9	.226	-.415	-.373							.497	.805	.697							9
10	-.410	-.371	-.372							.615	.706								10
11	-.371	-.344								.544									11
12	-.295																		12
	α = 03°									δ = 00°									
1	.402	.190	.245	.203	.307	.321	.161			.135	.142	.147	.160	.147	-.232				1
2	-.007	-.066	-.121	-.185	-.198	-.245	-.375			.080		.084	.070	.095	.154	-.153			2
3	-.019	-.043	-.044	-.069	-.082	-.085				.079	.057	.054	.177	.066	.080				3
4	-.010	-.043	-.066	-.056	-.088	-.248				.056	.052	.044		-.107	-.130				4
5	-.031	-.044	-.060	-.120	-.209	-.243				.072	.033	.127	-.102	-.098	-.107				5
6	-.031	-.022	-.035	-.201	-.194					.082	.198		-.093						6
7	-.007	-.040	-.085	-.184						.123		-.098	-.091						7
8	-.030	-.080	-.166	-.194							-.095	-.087							8
9	-.015	-.161	-.197							-.102	-.105	-.089							9
10	-.166	-.187	-.193							-.101	-.100								10
11	-.184	-.190								-.103									11
12	-.187																		12

[redacted]

Table 19 Continued

Pressure Coefficients on Delta Wing with Control

Configuration I M = 1.61 R = 4.2 x 10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 06°									δ = 00°									
1	.377	.124	.168	.119	.210	.286	.258								-.380				1
2	-.070	-.229	-.310	-.351	-.357	-.378	-.399			.205	.225	.235	.241	.240	.245	-.066			2
3	-.055	-.088	-.092	-.124	-.282	-.312				.135		.162	.141	.160	.168				3
4	-.041	-.085	-.107	-.116	-.123	-.362				.139	.119	.119	.260	.134	-.074				4
5	-.075	-.082	-.105	-.131	-.248	-.249				.120	.109	.106		-.059	-.052				5
6	-.061	-.063	-.073	-.226	-.226					.119	.086	.192	-.066	-.050					6
7	-.044	-.074	-.091	-.208						.125	.258		-.050						7
8	-.066	-.081	-.175	-.219						.177		-.070	-.051						8
9	-.005	-.169	-.218								-.069	-.056							9
10	-.181	-.198	-.209							-.068	-.076	-.058							10
11	-.194	-.199								-.067	-.070								11
12	-.191									-.075									12
	α = 06°									δ = 10°									
1	.376	.122	.166	.116	.209	.285	.259								-.382				1
2	-.074	-.238	-.319	-.357	-.363	-.382	-.399			.203	.224	.233	.241	.238	.245	-.064			2
3	-.057	-.091	-.095	-.127	-.286	-.314				.133		.159	.139	.158	.170				3
4	-.044	-.089	-.110	-.119	-.127	-.365				.138	.118	.115	.256	.132	-.073				4
5	-.077	-.088	-.109	-.143	-.283	-.252				.118	.107	.104		-.002	-.025				5
6	-.064	-.065	-.076	-.310	-.285					.116	.084	.188	.127	-.066					6
7	-.047	-.075	-.065	-.290						.122	.255		-.127						7
8	-.069	-.053	-.278	-.261						.184		.206	-.086						8
9	.028	-.277	-.325								.189	.223							9
10	-.282	-.301	-.212							.181	.198	.209							10
11	-.299	-.197								.201	.201								11
12	-.184									.165									12
	α = 06°									δ = 20°									
1	.373	.120	.164	.115	.209	.285	.257								-.382				1
2	-.076	-.239	-.320	-.358	-.363	-.381	-.399			.201	.223	.232	.240	.236	.243	-.065			2
3	-.058	-.093	-.097	-.128	-.285	-.313				.131		.158	.136	.157	.170				3
4	-.045	-.090	-.112	-.119	-.127	-.364				.137	.116	.114	.260	.130	-.074				4
5	-.078	-.089	-.109	-.116	-.288	-.251				.117	.106	.102		.074	.109				5
6	-.065	-.065	-.072	-.385	-.300					.116	.082	.391	.537	-.099					6
7	-.047	-.060	.158	-.337						.123	.449		.475						7
8	-.072	.196	-.364	-.320						.394		.690	.371						8
9	.214	-.369	-.340								.652	.694							9
10	-.363	-.345	-.294							.569	.691	.562							10
11	-.369	-.273								.602	.564								11
12	-.259									.468									12
	α = 06°									δ = 30°									
1	.373	.120	.165	.115	.210	.285	.326								-.381				1
2	-.074	-.238	-.318	-.357	-.361	-.380	-.393			.201	.223	.232	.239	.236	.243	-.023			2
3	-.057	-.093	-.095	-.127	-.284	-.311				.131		.159	.136	.157	.341				3
4	-.044	-.089	-.110	-.118	-.126	-.363				.138	.116	.116	.456	.435	.102				4
5	-.077	-.089	-.107	-.153	-.286	-.244				.117	.106	.295		.102	.140				5
6	-.064	-.065	-.072	-.413	-.296					.116	.423	.521	.602	-.077					6
7	-.048	-.061	.177	-.365						.372	.551		.733						7
8	-.068	.223	-.416	-.366						.556		.653	.573						8
9	.332	-.418	-.365								.672	.881							9
10	-.396	-.367	-.360							.689	.902	.775							10
11	-.369	-.335								.785	.788								11
12	-.298									.616									12
	α = 09°									δ = 00°									
1	.308	.051	.070	.023	.052	.157	.353								-.457				1
2	-.162	-.343	-.400	-.430	-.439	-.453	-.463			.282	.307	.314	.324	.326	.324	.020			2
3	-.094	-.141	-.223	-.348	-.391	-.405				.197		.239	.217	.239	.256				3
4	-.081	-.134	-.147	-.153	-.312	-.450				.203	.188	.188	.351	.211	-.004				4
5	-.114	-.132	-.148	-.148	-.326	-.323				.180	.175	.175		-.002	.014				5
6	-.102	-.119	-.114	-.280	-.261					.182	.151	.264	-.001	.014					6
7	-.090	-.122	-.086	-.262						.177	.324		.014						7
8	-.110	-.090	-.222	-.265						.248		-.013	.007						8
9	.009	-.222	-.261								-.007	.002							9
10	-.235	-.251	-.248							-.009	-.011	.001							10
11	-.235	-.248								-.010	-.006								11
12	-.220									-.017									12

[redacted]

Table 19 Continued

Pressure Coefficients on Delta Wing with Control

Configuration I M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
								α = 12°		δ = 00°									
1	.266	-.025	-.050	-.089	-.129	-.036	.423								-.445				1
2	-.301	-.443	-.465	-.481	-.488	-.474	-.383			.359	.388	.397	.405	.404	.405	.111			2
3	-.131	-.216	-.356	-.440	-.455	-.470				.269		.312	.299	.326	.335				3
4	-.123	-.197	-.245	-.302	-.334	-.438				.259	.264	.263	.436	.293	.063				4
5	-.150	-.191	-.223	-.261	-.385	-.413				.251	.247	.249		.056	.078				5
6	-.139	-.169	-.159	-.374	-.357					.255	.220	.339	.047	.080					6
7	-.130	-.147	-.087	-.401						.231	.394		.074						7
8	-.146	-.086	-.241	-.358						.318		.030	.059						8
9	.026	-.234	-.273								.039	.050							9
10	-.250	-.269	-.253							.041	.039	.052							10
11	-.255	-.263								.041	.043								11
12	-.218									.035									12
								α = 12°		δ = 10°									
1	.265	-.025	-.051	-.088	-.128	-.035	.422								-.461				1
2	-.300	-.441	-.469	-.485	-.493	-.479	-.438			.360	.388	.397	.404	.404	.403	.109			2
3	-.131	-.215	-.355	-.439	-.456	-.476				.270		.311	.299	.325	.334				3
4	-.123	-.197	-.245	-.302	-.334	-.455				.259	.264	.263	.436	.292	.066				4
5	-.149	-.191	-.222	-.278	-.406	-.418				.250	.247	.249		.134	.149				5
6	-.138	-.169	-.158	-.396	-.394					.255	.220	.338	.294	.039					6
7	-.129	-.147	-.067	-.388						.231	.394		.288						7
8	-.147	-.050	-.327	-.274						.325		.400	.224						8
9	.074	-.328	-.358								.391	.413							9
10	-.324	-.345	-.248							.387	.395	.381							10
11	-.340	-.232								.399	.388								11
12	-.232									.333									12
								α = 12°		δ = 20°									
1	.265	-.025	-.051	-.089	-.128	-.034	.421								-.445				1
2	-.300	-.443	-.472	-.490	-.495	-.478	-.419			.359	.388	.395	.403	.401	.402	.222			2
3	-.132	-.214	-.355	-.441	-.457	-.476				.269		.310	.297	.322	.335				3
4	-.124	-.197	-.245	-.295	-.334	-.440				.258	.261	.262	.598	.306	.300				4
5	-.150	-.191	-.220	-.098	-.400	-.418				.249	.246	.247		.260	.280				5
6	-.139	-.170	-.156	-.400	-.382					.255	.217	.674	.759	.017					6
7	-.131	-.147	.323	-.345						.234	.690		.647						7
8	-.147	.334	-.387	-.341						.642		.876	.488						8
9	.351	-.378	-.369								.851	.868							9
10	-.386	-.370	-.303							.782	.869	.676							10
11	-.385	-.307								.804	.681								11
12	-.277									.598									12
								α = 12°		δ = 30°									
1	.266	-.024	-.049	-.088	-.127	-.033	.517								-.449				1
2	-.297	-.440	-.474	-.491	-.495	-.480	-.435			.358	.387	.394	.402	.401	.419	.352			2
3	-.131	-.215	-.353	-.440	-.456	-.472				.269		.307	.297	.322	.508				3
4	-.123	-.197	-.243	-.297	-.333	-.448				.260	.261	.262	.656	.641	.315				4
5	-.149	-.192	-.218	-.103	-.402	-.428				.248	.247	.652		.286	.240				5
6	-.140	-.168	-.156	-.407	-.379					.258	.674	.740	.806	-.017					6
7	-.129	-.145	.319	-.371						.618	.769		.910						7
8	-.149	.352	-.385	-.384						.774		.915	.662						8
9	.451	-.377	-.376								.917	1.122							9
10	-.420	-.377	-.357							.861	1.117	.865							10
11	-.393	-.359								.939	.865								11
12	-.304									.739									12
								α = 15°		δ = 00°									
1	.231	-.094	-.184	-.194	-.269	-.146	.504								-.403				1
2	-.372	-.445	-.445	-.445	-.452	-.452	-.317			.436	.459	.455	.460	.488	.499	.236			2
3	-.163	-.356	-.415	-.439	-.450	-.430				.340		.390	.412	.439	.455				3
4	-.155	-.336	-.402	-.394	-.436	-.431				.324	.337	.373	.576	.415	.140				4
5	-.181	-.162	-.395	-.311	-.456	-.373				.323	.356	.380		.133	.166				5
6	-.171	-.175	-.385	-.427	-.443					.355	.339	.455	.134	.160					6
7	-.162	-.177	-.093	-.413						.334	.513		.164						7
8	-.176	-.066	-.304	-.348						.434		.117	.139						8
9	.054	-.261	-.293								.127	.136							9
10	-.276	-.293	-.268							.128	.123	.144							10
11	-.284	-.192								.136	.126								11
12	-.153									.118									12

[redacted]

Table 19 Continued

Pressure Coefficients on Delta Wing with Control

Configuration I M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station 1	2	3	4	5	6	7	8	9	Lower Surface at Station 1	2	3	4	5	6	7	8	9	Orif
								$\alpha = -03^\circ$		$\delta = 00^\circ$									
1	.372	.314	.244	.261	.316	.341	-.205			.013	-.036	-.093	-.098	-.149	.148				1
2	.114	.106	.123	.133	.124	.143	-.165			-.010		-.045	-.069	-.074	-.200	-.356			2
3	.065	.069	.086	.068	.082	.077				-.009	-.018	-.059	.023	-.069	-.080				3
4	.066	.045	.049	.069	.040	-.143				-.030	-.040	-.059		-.202	-.239				4
5	.070	.052	.038	-.127	-.118	-.138				-.018	-.053	.016	-.166	-.182	-.226				5
6	.051	.069	.064	-.131	-.114					-.001	.093		-.158						6
7	.063	.046	-.100	-.139						.044		-.146	-.161						7
8	.047	-.091	-.136	-.144							-.135	-.156							8
9	.000	-.116	-.131							-.151	-.151	-.146							9
10	-.124	-.139	-.135							-.155	-.149								10
11	-.134	-.140								-.155									11
12	-.132																		12
								$\alpha = -06^\circ$		$\delta = 00^\circ$									
1	.316	.284	.141	.150	.181	.186	-.379			-.068	-.247	-.301	-.319	-.352	.245				1
2	.182	.189	.215	.223	.210	.231	-.066			-.056		-.106	-.140	-.277	-.357	-.388			2
3	.120	.136	.159	.138	.143	.159				-.060	-.076	-.105	-.074	-.120	-.302				3
4	.118	.099	.110	.137	.110	-.085				-.076	-.087	-.111		-.248	-.353				4
5	.121	.106	.099	-.134	-.063	-.077				-.061	-.097	-.031	-.234	-.224	-.254				5
6	.103	.127	.119	-.055	-.064					-.044	.039		-.212						6
7	.113	.094	-.115	-.065						.003		-.191	-.222						7
8	.101	-.100	-.078	-.071							-.181	-.215							8
9	.020	-.068	-.066							-.200	-.205	-.177							9
10	-.074	-.076	-.080							-.203	-.194								10
11	-.078	-.078								-.189									11
12	-.077																		12
								$\alpha = -06^\circ$		$\delta = 10^\circ$									
1	.319	.287	.144	.151	.182	.187	-.385			-.066	-.253	-.306	-.335	-.356	.247				1
2	.187	.194	.219	.226	.212	.234	-.064			-.053		-.103	-.139	-.278	-.338	-.393			2
3	.125	.140	.164	.140	.147	.162				-.057	-.074	-.103	-.072	-.119	-.306				3
4	.122	.103	.114	.141	.114	-.083				-.073	-.084	-.109		-.206	-.358				4
5	.125	.110	.103	-.128	-.112	-.075				-.059	-.094	-.024	-.118	-.182	-.256				5
6	.107	.132	.123	-.191	-.132					-.041	.044		-.101						6
7	.118	.099	-.082	-.167						.015		-.024	-.109						7
8	.105	-.065	-.194	-.182							-.009	-.005							8
9	.025	-.211	-.238							-.041	-.012	-.005							9
10	-.197	-.224	-.236							-.019	-.011								10
11	-.220	-.224								-.030									11
12	-.218																		12
								$\alpha = -06^\circ$		$\delta = 20^\circ$									
1	.316	.284	.141	.148	.178	.184	-.388			-.068	-.257	-.307	-.339	-.359	.252				1
2	.186	.195	.219	.228	.215	.238	-.063			-.055		-.105	-.141	-.283	-.336	-.395			2
3	.125	.139	.164	.143	.149	.163				-.059	-.077	-.105	-.065	-.122	-.310				3
4	.122	.103	.114	.143	.115	-.080				-.076	-.086	-.111		-.170	-.360				4
5	.124	.109	.103	-.045	-.126	-.074				-.061	-.097	.059	.113	-.226	-.249				5
6	.107	.131	.125	-.311	-.159					-.043	.132		.148						6
7	.119	.102	.077	-.278						.147		.302	.118						7
8	.108	.113	-.310	-.285							.316	.338							8
9	.131	-.329	-.353							.265	.350	.305							9
10	-.312	-.336	-.242							.286	.310								10
11	-.328	-.227								.247									11
12	-.231																		12
								$\alpha = -06^\circ$		$\delta = 30^\circ$									
1	.318	.285	.141	.149	.178	.182	-.389			-.066	-.258	-.308	-.339	-.357	.255				1
2	.189	.198	.222	.230	.220	.241	-.060			-.053		-.103	-.140	-.283	-.332	-.388			2
3	.127	.141	.167	.146	.153	.167				-.056	-.075	-.103	.212	.091	-.310				3
4	.124	.106	.118	.147	.119	-.077				-.073	-.084	-.109		-.135	-.366				4
5	.126	.112	.108	.066	-.125	-.069				-.059	-.095	.274	.392	-.245	-.148				5
6	.109	.135	.130	-.388	-.158					-.014	.309		.430						6
7	.122	.114	.158	-.346						.303		.445	.306						7
8	.111	.193	-.356	-.334							.441	.588							8
9	.230	-.367	-.350							.463	.603	.523							9
10	-.382	-.348	-.318							.589	.560								10
11	-.382	-.308								.501									11
12	-.288																		12

Table 19 Continued

Pressure Coefficients on Delta Wing with Control

Configuration I M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	$\alpha = -09^\circ$									$\delta = 00^\circ$									
1	.273	.220	.041	.016	.022	-.005	-.448			-.142	-.328	-.388	-.391	-.423	.329				1
2	.271	.273	.300	.296	.299	.317	.011			-.090		-.215	-.310	-.382	-.444	-.427			2
3	.189	.196	.240	.218	.227	.238				-.092	-.120	-.136	-.140	-.239	-.394				3
4	.188	.167	.180	.213	.188	-.022				-.107	-.132	-.144		-.305	-.435				4
5	.190	.172	.170	-.145	-.007	-.015				-.096	-.132	-.072	-.249	-.277	-.307				5
6	.166	.195	.185	-.017	-.014					-.077	-.035		-.235						6
7	.179	.155	-.116	-.034						-.034		-.194	-.234						7
8	.169	-.097	-.056	-.036							-.188	-.221							8
9	.041	-.040	-.031							-.202	-.202	-.190							9
10	-.050	-.047	-.050							-.210	-.202								10
11	-.046	-.051								-.191									11
12	-.048																		12
	$\alpha = -12^\circ$									$\delta = 00^\circ$									
1	.209	.103	-.067	-.157	-.150	-.207	-.424			-.286	-.393	-.447	-.466	-.483	.407				1
2	.347	.360	.390	.370	.373	.391	.109			-.132		-.305	-.334	-.409	-.463	-.331			2
3	.265	.272	.312	.305	.313	.329				-.129	-.160	-.291	-.244	-.330	-.442				3
4	.268	.245	.260	.298	.275	.052				-.145	-.148	-.272		-.365	-.414				4
5	.248	.248	.251	-.216	.064	.071				-.132	-.157	-.161	-.356	-.316	-.348				5
6	.248	.280	.263	.068	.064					-.117	-.049		-.359						6
7	.253	.229	-.143	.061						-.087		-.264	-.260						7
8	.243	-.093	.031	.052							-.227	-.245							8
9	.066	.040	.055							-.253	-.253	-.264							9
10	.032	.045	.031							-.255	-.189								10
11	.038	.037								-.178									11
12	.036																		12
	$\alpha = -12^\circ$									$\delta = 10^\circ$									
1	.210	.105	-.066	-.156	-.151	-.208	-.423			-.285	-.393	-.444	-.465	-.483	.406				1
2	.347	.369	.390	.371	.373	.393	.109			-.131		-.304	-.334	-.407	-.461	-.318			2
3	.265	.273	.313	.305	.313	.330				-.127	-.160	-.291	-.238	-.330	-.441				3
4	.269	.246	.261	.298	.276	.050				-.145	-.147	-.271		-.338	-.410				4
5	.248	.248	.252	-.277	-.006	.049				-.132	-.157	-.158	-.310	-.330	-.338				5
6	.248	.281	.264	-.109	-.022					-.116	-.047		-.305						6
7	.254	.231	-.126	-.091						-.080		-.126	-.270						7
8	.244	-.070	-.164	-.136							-.076	-.085							8
9	.072	-.151	-.165							-.118	-.072	-.069							9
10	-.139	-.162	-.171							-.098	-.076								10
11	-.160	-.165								-.131									11
12	-.164																		12
	$\alpha = -12^\circ$									$\delta = 20^\circ$									
1	.210	.105	-.065	-.157	-.151	-.210	-.432			-.284	-.392	-.444	-.466	-.482	.408				1
2	.348	.363	.392	.373	.374	.394	.110			-.130		-.305	-.334	-.408	-.464	-.317			2
3	.267	.274	.314	.307	.315	.330				-.127	-.159	-.292	-.201	-.322	-.443				3
4	.270	.247	.263	.299	.278	.053				-.144	-.147	-.272		-.286	-.411				4
5	.249	.249	.254	-.168	-.030	.044				-.131	-.157	-.136	-.207	-.373	-.316				5
6	.249	.282	.266	-.249	-.062					-.115	.012		-.166						6
7	.256	.233	-.036	-.231						.067		.122	-.157						7
8	.248	.057	-.279	-.273							.214	.230							8
9	.127	-.284	-.301							.136	.230	.243							9
10	-.263	-.289	-.269							.157	.219								10
11	-.280	-.231								.124									11
12	-.226																		12
	$\alpha = -12^\circ$									$\delta = 30^\circ$									
1	.210	.105	-.067	-.158	-.152	-.210	-.348			-.285	-.394	-.445	-.467	-.482	.409				1
2	.346	.361	.391	.372	.378	.397	.111			-.131		-.306	-.335	-.411	-.457	-.257			2
3	.265	.273	.315	.306	.316	.333				-.128	-.160	-.294	-.153	-.211	-.400				3
4	.269	.246	.262	.299	.278	.057				-.145	-.148	-.273		-.353	-.415				4
5	.249	.248	.255	-.061	-.035	.044				-.132	-.157	.056	-.053	-.356	-.380				5
6	.248	.282	.268	-.350	-.066					-.113	.206		.044						6
7	.256	.236	.147	-.340						.188		.601	-.007						7
8	.252	.211	-.363	-.293							.356	.676							8
9	.207	-.373	-.375							.400	.561	.593							9
10	-.351	-.362	-.297							.431	.525								10
11	-.363	-.277								.343									11
12	-.255																		12

[redacted]

Table 19 Concluded

Pressure Coefficients on Delta Wing with Control

Configuration I M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
	$\alpha = -15^\circ$										$\delta = 30^\circ$									
1	.166	.016	-.134	-.279	-.293	-.361	-.398				-.345	-.413	-.436	-.441	-.447	.480	-.310			1
2	.403	.415	.430	.423	.449	.475	.193				-.153		-.385	-.412	-.429	-.437				2
3	.319	.332	.394	.400	.409	.434					-.152	-.264	-.391	-.352	-.414	-.424				3
4	.331	.305	.357	.393	.381	.108					-.169	-.157	-.388		-.434	-.410				4
5	.306	.340	.363	-.198	.128	.130					-.156	-.176	-.309	-.357	-.425	-.359				5
6	.330	.385	.357	.115	.122						-.135	-.081		-.372						6
7	.341	.315	-.133	.095							-.114		-.236	-.328						7
8	.336	-.078	.055	.089								-.210	-.236							8
9	.091	.073	.097								-.241	-.231	-.218							9
10	.061	.078	.067								-.249	-.147								10
11	.079	.065									-.143									11
12	.073																			12

[redacted]

Table 20

Pressure Coefficients on Delta Wing with Control

Configuration J M = 1.61 R = 4.2 x 10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 00°									δ = 00°									
1	.386	.368	.289	.275	.310	.358	1.711												1
2	.053	.033	.030	.031	.017	.013	.031			.079		.044		.014	.012	.021			2
3	.021	.016		.007	-.003	.002	.016			.041	.020	.007		.010	.002	.029			3
4	.025	.011	-.009	-.020	-.021	.070	-.165			.032		-.005	-.005	-.031	.033	-.129			4
5	.007	.011	.002	-.043	.010	.007	-.271			.001	.014	-.022		.016	.059	-.271			5
6	.014	.000	.008	-.139						.020	.000	.033	-.145		-.196				6
7	.016	.008		-.157		-.185				.022	.007		-.139		-.201				7
8	.009	.084		-.148		-.166				.026			-.139		-.203				8
9		-.124		-.138									-.148						9
10	-.084	-.142									-.150								10
11	-.075	-.142								-.115	-.147								11
12	-.123	-.140								-.144	-.130								12
	α = 00°									δ = 10°									
1	.394	.375	.293	.279	.306	.360	1.710												1
2	.064	.037	.038	.030	.011	.014	-.192			.076		.040		.004	.005	.387			2
3	.026	.018		.005	-.002	-.001	-.189			.033	.019	.007		.008	.001	.291			3
4	.028	.006	-.011	-.015	-.016	.070	-.376			.037		-.004	-.008	-.038	.028	.032			4
5	.015	.009	.002	-.025	.016	-.198	-.389			.006	.012	-.025		.014	.264	-.061			5
6	.015	-.001	.009	-.290						.021	-.002	.032	.100		.051				6
7	.020	.009		-.321		-.346				.018	.007		.122		.036				7
8	.002	.089		-.315		-.321				.050			.129		.028				8
9		-.287		-.302									.142						9
10	-.200	-.297									.123								10
11	-.070	-.321								.095	.127								11
12	-.185	-.139								.125	.131								12
	α = 00°									δ = 20°									
1	.397	.370	.289	.276	.309	.364	1.709												1
2	.062	.044	.039	.039	.020	.020	-.336			.069		.035		-.004	-.004	.966			2
3	.026	.024		.008	-.004	.006	-.413			.031	.016	.004		.000	-.007	.508			3
4	.026	.008	-.007	-.007	-.015	.080	-.426			.036		-.013	.272	-.041	.061	.124			4
5	.011	.011	.007	.138	.021	-.324	-.412			-.001	.000	-.031		.208	.582	.232			5
6	.015	-.001	.017	-.394						.013	-.007	.309	.319		.385				6
7	.023	.024		-.326		-.339				.017	.307		.555		.403				7
8	.039	.164		-.300		-.294				.252			.603		.381				8
9		-.381		-.290									.528						9
10	-.313	-.400									.509								10
11	-.148	-.324								.489	.563								11
12	-.180	-.271								.483	.521								12
	α = 00°									δ = 30°									
1	.388	.374	.288	.271	.307	.358	1.705												1
2	.056	.039	.032	.026	.016	.011	-.415			.072		.029		-.007	.031	.976			2
3	.025	.018		.007	-.001	.000	-.455			.025	.010	.001		-.003	.349	.795			3
4	.029	.002	-.007	-.012	-.020	.100	-.461			.036		-.018	.421	.357	.620	.616			4
5	.017	.007	.003	.211	.024	-.407	-.441			-.005	.006	.316		.441	.573	.632			5
6	.006	-.005	.010	-.344						.014	.362	.400	.423		.848				6
7	.015	.025		-.337		-.349				.325	.419		.600		.768				7
8	.040	.190		-.347		-.357				.411			.740		.649				8
9		-.388		-.340									.669						9
10	-.374	-.376									.462								10
11	-.191	-.377								.664	.598								11
12	-.290	-.354								.641	.588								12
	α = 06°									δ = 00°									
1	.338	.114	.160	.010	.120	.219	1.710												1
2	-.074	-.234	-.307	±.351	-.361	-.382	-.361			.210		.233		.214	.227	.208			2
3	-.054	-.076		-.130	-.276	-.336	-.380			.136	.146	.149		.154	.185	.231			3
4	-.050	-.079	-.109	-.135	-.127	-.286	-.431			.136		.110	.113	.097	.198	-.014			4
5	-.078	-.083	-.100	-.067	-.101	-.287	-.411			.109	.114	.084		.169	.160	-.100			5
6	-.058	-.084	-.086	-.230						.108	.094	.129	-.049		-.078				6
7	-.051	-.074		-.236		-.338				.109	.102		-.049		-.086				7
8	-.030	.078		-.228		-.304				.068			-.051		-.087				8
9		-.183		-.204									-.059						9
10	-.132	-.192									-.089								10
11	-.128	-.204								-.025	-.074								11
12	-.166	-.198								-.082	-.054								12

[redacted]

Table 20 Continued

Pressure Coefficients on Delta Wing with Control

Configuration J M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station								Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 06°									δ = 10°								
1	.339	.114	.159	.002	.116	.219	1.708												1
2	-.081	-.242	-.317	-.359	-.362	-.388	-.406			.201		.236		.208	.231	.675			2
3	-.065	-.080		-.133	-.279	-.341	-.426			.132	.145	.148		.144	.182	.441			3
4	-.051	-.088	-.115	-.137	-.129	-.292	-.425			.138		.111	.112	.094	.195	.075			4
5	-.089	-.087	-.107	-.039	-.106	-.348	-.424			.111	.114	.083		.172	.461	.157			5
6	-.066	-.089	-.083	-.345						.112	.093	.131	.257		.227				6
7	-.063	-.072		-.363		-.420				.101	.095		.270		.219				7
8	-.038	.082		-.367		-.376				.083			.282		.201				8
9		-.321		-.228									.289						9
10	-.262	-.327									.240								10
11	-.107	-.353								.220	.249								11
12	-.217	-.179								.248	.255								12
	α = 06°									δ = 20°								
1	.341	.113	.158	.003	.123	.230	1.710												1
2	-.069	-.238	-.310	-.347	-.360	-.386	-.383			.204		.234		.208	.225	1.190			2
3	-.058	-.078		-.132	-.272	-.339	-.401			.138	.143	.149		.150	.183	.600			3
4	-.044	-.086	-.109	-.129	-.118	-.274	-.406			.140		.108	.521	.092	.632	.497			4
5	-.078	-.086	-.100	.287	-.100	-.394	-.374			.116	.118	.082		.513	.796	.558			5
6	-.065	-.082	-.075	-.413						.113	.096	.504	.523		.726				6
7	-.059	-.056		-.362		-.349				.105	.486		.719		.663				7
8	-.013	.185		-.330		-.361				.431			.762		.585				8
9		-.399		-.318									.651						9
10	-.337	-.407									.645								10
11	-.208	-.335								.646	.704								11
12	-.220	-.251								.577	.631								12
	α = 06°									δ = 30°								
1	.342	.120	.158	.007	.123	.234	1.707												1
2	-.074	-.234	-.314	-.355	-.362	-.382	-.398			.200		.238		.208	.312	1.306			2
3	-.056	-.078		-.130	-.272	-.321	-.402			.134	.143	.146		.150	.632	.966			3
4	-.047	-.081	-.112	-.127	-.117	-.261	-.393			.145		.112	.629	.577	.704	.847			4
5	-.078	-.083	-.099	.294	-.100	-.424	-.387			.118	.116	.508		.645	.617	.743			5
6	-.063	-.079	-.075	-.356						.113	.520	.579	.641		1.074				6
7	-.057	-.047		-.358		-.391				.489	.580		.876		.997				7
8	-.011	.197		-.374		-.393				.575			.999		.800				8
9		-.438		-.363									.852						9
10	-.395	-.408									.609								10
11	-.218	-.396								.740	.715								11
12	-.294	-.336								.671	.682								12
	α = 12°									δ = 00°								
1	.209	-.096	-.015	-.199	-.168	-.190	1.710												1
2	-.289	-.420	-.452	-.467	-.489	-.503	-.416			.335		.394		.361	.373	.363			2
3	-.124	-.183		-.424	-.448	-.475	-.416			.270	.279	.288		.297	.327	.304			3
4	-.109	-.173	-.218	-.315	-.434	-.448	-.406			.274		.249	.247	.233	.339	.021			4
5	-.154	-.185	-.176	-.086	-.309	-.423	-.410			.238	.245	.216		.333	.251	.057			5
6	-.137	-.171	-.146	-.361						.238	.218	.257	.061		.042				6
7	-.129	-.146		-.371		-.411				.199	.208		.055		.039				7
8	-.096	.077		-.361		-.397				.133			.054		.036				8
9		-.237		-.334									.042						9
10	-.211	-.250									.002								10
11	-.158	-.258								.048	.019								11
12	-.196	-.253								.044	.033								12
	α = 12°									δ = 10°								
1	.210	-.094	-.017	-.199	-.170	-.190	1.705												1
2	-.294	-.424	-.459	-.484	-.490	-.499	-.420			.339		.398		.359	.372	.875			2
3	-.126	-.183		-.430	-.449	-.479	-.413			.273	.280	.290		.295	.325	.489			3
4	-.117	-.185	-.214	-.310	-.433	-.442	-.409			.274		.253	.248	.229	.339	.226			4
5	-.162	-.185	-.176	-.013	-.303	-.434	-.402			.240	.248	.213		.334	.614	.387			5
6	-.138	-.177	-.149	-.423						.238	.219	.254	.432		.412				6
7	-.135	-.149		-.426		-.414				.200	.207		.439		.415				7
8	-.106	.082		-.438		-.409				.145			.457		.377				8
9		-.360		-.326									.438						9
10	-.301	-.371									.405								10
11	-.159	-.380								.373	.401								11
12	-.232	-.220								.393	.405								12

[redacted]

Table 20 Continued

Pressure Coefficients on Delta Wing with Control

Configuration J M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 12°									δ = 20°									
1	.221	-.078	-.002	-.181	-.157	-.171	1.700												1
2	-.280	-.412	-.452	-.471	-.477	-.473	-.396			.345		.398		.366	.377	1.266			2
3	-.113	-.167		-.413	-.436	-.457	-.406			.281	.281	.292		.292	.377	.800			3
4	-.093	-.167	-.202	-.294	-.415	-.404	-.406			.292		.260	.737	.239	.874	.737			4
5	-.145	-.169	-.161	.514	-.277	-.417	-.396			.260	.260	.218		.747	.821	.684			5
6	-.122	-.160	-.129	-.449						.260	.239	.715	.747		.980				6
7	-.122	-.132		-.427		-.396				.218	.694		.906		.853				7
8	-.079	.218		-.374		-.396				.641			.906		.715				8
9		-.417		-.396									.758						9
10	-.353	-.427									.843								10
11	-.237	-.343								.811	.874								11
12	-.247	-.269								.694	.768								12
	α = 12°									δ = 30°									
1	.208	-.096	-.013	-.199	-.167	-.242	1.711												1
2	-.285	-.423	-.461	-.482	-.489	-.485	-.394			.335		.390		.352	.656	1.103			2
3	-.128	-.182		-.430	-.456	-.475	-.406			.263	.279	.288		.469	.879	1.053			3
4	-.118	-.179	-.210	-.299	-.439	-.396	-.402			.273		.253	.800	.738	.897	.933			4
5	-.161	-.185	-.174	.500	-.263	-.412	-.393			.239	.237	.719		.831	.758	.777			5
6	-.136	-.173	-.147	-.397						.237	.714	.775	.796		1.261				6
7	-.134	-.140		-.392		-.407				.658	.776		.937		1.095				7
8	-.091	.216		-.410		-.398				.775			1.019		.874				8
9		-.421		-.400									.876						9
10	-.412	-.417									.902								10
11	-.227	-.411								.916	1.036								11
12	-.312	-.391								.807	.911								12
	α = -06°									δ = 00°									
1	.319	.389	.176	.167	.190	.185	1.705												1
2	.185	.189	.217	.227	.212	.221	.225			-.065		-.288		-.340	-.366	-.356			2
3	.121	.136		.125	.132	.175	.220			-.044	-.082	-.107		-.264	-.326	-.364			3
4	.121	.100	.106	.092	.109	.215	-.030			-.049		-.100	-.118	-.150	-.280	-.420			4
5	.112	.110	.098	-.046	.138	.164	-.098			-.082	-.080	-.121		-.109	-.073	-.407			5
6	.105	.090	.105	-.069						-.061	-.082	-.060	-.222		-.341				6
7	.099	.086		-.086		-.084				-.054	-.071		-.216		-.322				7
8	.034	.107		-.082		-.069				-.010			-.211		-.307				8
9		-.077		-.074									-.204						9
10	-.037	-.107									-.186								10
11	-.010	-.088								-.169	-.202								11
12	-.071	-.076								-.181	-.184								12
	α = -06°									δ = 10°									
1	.302	.376	.165	.145	.172	.163	1.705												1
2	.172	.181	.203	.214	.201	.209	-.052			-.057		-.283		-.340	-.363	-.263			2
3	.103	.124		.121	.118	.161	-.006			-.041	-.078	-.107		-.269	-.320	-.185			3
4	.103	.087	.093	.084	.096	.202	-.176			-.043		-.097	-.111	-.150	-.270	-.240			4
5	.093	.098	.087	-.038	.121	-.105	-.283			-.073	-.073	-.118		-.110	-.024	-.344			5
6	.084	.080	.092	-.244						-.058	-.084	-.056	-.033		-.176				6
7	.084	.072		-.275		-.286				-.049	-.059		.010		-.126				7
8	.019	.112		-.271		-.267				.030			.021		-.124				8
9		-.254		-.263									.026						9
10	-.140	-.258									.043								10
11	-.039	-.284								.010	.046								11
12	-.175	-.156								.037	.046								12
	α = -06°									δ = 20°									
1	.319	.395	.179	.163	.185	.173	1.708												1
2	.190	.195	.222	.232	.223	.231	-.238			-.064		-.290		-.348	-.372	-.163			2
3	.128	.145		.145	.143	.190	-.177			-.044	-.083	-.110		-.282	-.325	.067			3
4	.128	.111	.118	.107	.119	.226	-.323			-.042		-.097	.092	-.145	-.162	-.025			4
5	.122	.116	.115	.115	.153	-.247	-.374			-.083	-.073	-.122		-.092	.044	-.121			5
6	.105	.100	.114	-.355						-.059	-.083	.166	.151		.076				6
7	.099	.107		-.377		-.385				-.053	.180		.361		.155				7
8	.084	.181		-.382		-.292				.162			.391		.159				8
9		-.354		-.255									.365						9
10	-.295	-.374									.371								10
11	-.110	-.379								.331	.410								11
12	-.175	-.217								.362	.388								12

[redacted]

Table 20 Concluded

Pressure Coefficients on Delta Wing with Control

Configuration J M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = -06°									δ = 30°									
1	.310	.394	.168	.149	.182	.185	1.711												1
2	.190	.196	.228	.240	.230	.234	-.369			-.072		-.301		-.345	-.012	.291			2
3	.123	.143		.140	.144	.190	-.359			-.048	-.086	-.111		-.098	.067	.460			3
4	.123	.102	.118	.109	.118	.219	-.413			-.048		-.105	.165	-.047	.101	.148			4
5	.116	.109	.116	.140	.151	-.347	-.419			-.086	-.077	.018		.094	.151	.267			5
6	.100	.093	.116	-.335						-.060	.146	.333	.175		.198				6
7	.105	.123		-.328		-.351				.101	.343		.443		.258				7
8	.108	.228		-.333		-.333				.300			.539		.217				8
9		-.383		-.324									.532						9
10	-.362	-.360									.485								10
11	-.193	-.359								.649	.620								11
12	-.239	-.337								.620	.590								12
	α = -12°									δ = 00°									
1	.147	.230	-.012	-.135	-.084	-.131	1.709												1
2	.351	.357	.390	.390	.376	.364	.385			-.303		-.443		-.490	-.492	-.432			2
3	.263	.260		.297	.302	.320	.379			-.125	-.203	-.381		-.449	-.483	-.407			3
4	.266	.247	.262	.247	.266	.353	.022			-.131		-.234	-.290	-.443	-.469	-.405			4
5	.239	.252	.252	-.046	.296	.354	.080			-.161	-.181	-.201		-.302	-.086	-.424			5
6	.245	.234	.247	.049						-.136	-.191	-.151	-.359		-.424				6
7	.222	.218		.033		.039				-.130	-.164		-.343		-.407				7
8	.136	.160		.043		.074				-.057			-.342		-.419				8
9		.034		.059									-.339						9
10	-.005	.000									-.244								10
11	.136	.029								-.223	-.265								11
12	.057	.037								-.229	-.243								12
	α = -12°									δ = 10°									
1	.141	.225	-.011	-.132	-.086	-.136	1.708												1
2	.345	.362	.393	.391	.377	.366	.055			-.308		-.461		-.487	-.492	-.442			2
3	.270	.261		.295	.306	.326	.110			-.133	-.207	-.384		-.452	-.482	-.428			3
4	.260	.247	.263	.252	.272	.350	-.076			-.132		-.241	-.300	-.449	-.468	-.439			4
5	.241	.254	.252	-.053	.292	.033	-.132			-.165	-.183	-.208		-.290	-.096	-.433			5
6	.251	.234	.248	-.170						-.143	-.193	-.159	-.263		-.433				6
7	.226	.226		-.203		-.199				-.134	-.170		-.229		-.437				7
8	.123	.136		-.200		-.179				-.043			-.219		-.322				8
9		-.191		-.189									-.228						9
10	-.127	-.195									-.064								10
11	.017	-.213								-.064	-.056								11
12	-.145	-.207								-.068	-.034								12
	α = -12°									δ = 20°									
1	.146	.228	-.017	-.133	-.092	-.140	1.707												1
2	.345	.361	.394	.388	.379	.369	-.184			-.308		-.466		-.466	-.392	-.373			2
3	.266	.260		.301	.298	.325	-.071			-.127	-.210	-.393		-.460	-.384	-.252			3
4	.263	.249	.264	.247	.268	.351	-.220			-.133		-.239	-.198	-.402	-.377	-.272			4
5	.241	.249	.251	.007	.291	-.177	-.305			-.162	-.185	-.202		-.294	-.077	-.352			5
6	.248	.231	.247	-.317						-.142	-.193	.003	-.191		-.286				6
7	.225	.225		-.346		-.348				-.133	-.138		-.189		-.243				7
8	.140	.189		-.349		-.339				.098			-.144		-.236				8
9		-.324		-.341									-.107						9
10	-.274	-.343									.245								10
11	-.090	-.348								.196	.253								11
12	-.272	-.195								.252	.291								12
	α = -12°									δ = 30°									
1	.149	.228	-.013	-.138	-.088	-.137	1.706												1
2	.348	.369	.395	.394	.381	.371	-.325			-.310		-.457		-.337	-.210	-.118			2
3	.267	.260		.305	.306	.331	-.219			-.131	-.211	-.366		-.316	-.172	.104			3
4	.261	.249	.265	.249	.272	.361	-.360			-.129		-.320	-.140	-.277	-.142	-.006			4
5	.239	.249	.256	.013	.297	-.292	-.392			-.165	-.179	-.233		-.178	.016	-.091			5
6	.244	.236	.249	-.409						-.142	-.184	.115	-.138		-.095				6
7	.230	.234		-.398		-.331				-.085	.196		-.097		-.067				7
8	.187	.250		-.347		-.324				.191			-.054		-.111				8
9		-.406		-.328									-.065						9
10	-.349	-.414									.557								10
11	-.200	-.369								.515	.585								11
12	-.238	-.333								.483	.551								12

[redacted]

Table 21

Pressure Coefficients on Delta Wing with Control

Configuration J1 M = 1.61 R = 4.2 x 10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 00°									δ = 00°									
1	.347	.302	.312	.306	.321	.326	-.054			.073	.056	.039	.039	.006	.003	-.002			1
2	.067	.048	.043	.035	.024	.008	.117			.042		.009	.003	.001	-.007	.002			2
3	.038	.023	.018	.009	-.002	.003	.050			.034	.017	-.007	-.013	-.035	.019	-.019			3
4	.040	.018	.002	-.012	-.016	.061	.043			.014	.007	-.007		.023	-.031	-.005			4
5	.032	.020	-.006	-.035	.019	.026	.059			.028	-.018	.044	-.097		-.092				5
6	.024	-.001	.008	-.017		-.052				.024	.018		-.100		-.143				6
7	.022	.018		-.056		-.095				.050			-.087		-.133				7
8	.015	-.014		-.058		-.087				-.029	-.063		-.084						8
9	-.002	.006		-.042						-.083	-.058								9
10	-.059	-.036		-.290						-.091	-.079								10
11	-.056	-.052								-.088	-.078								11
12	-.038	-.037																	12
13		-.268																	13
	α = 00°									δ = 10°									
1	.346	.303	.310		.322	.330	-.006			.073	.056		.039	.002	.002	.121			1
2	.070	.050	.045		.039	.022	-.062			.038			.005	.003	-.006	.178			2
3	.039	.025			.007	.014	-.078			.040	.006		-.006	-.039	.024	.180			3
4	.045	.020			-.007	.074	-.126			.013	-.017			.022	.137	.180			4
5	.036	.021			.028	-.118	-.156			.028	.014		.086		.101				5
6	.020	.001				-.169				.023	.123		.104		.043				6
7	.025	.022				-.226				.069			.121		.046				7
8	.015	-.008				-.208				.113	.127		.132						8
9	-.137	-.128								.068	.141								9
10	-.134	-.149		-.289						.102	.140								10
11	-.171	-.186								.104	.116								11
12	-.170	-.172																	12
13		-.269																	13
	α = 00°									δ = 20°									
1	.347	.306	.314		.327	.333	-.082			.073	.055		.040	-.006	.001	.335			1
2	.070	.052	.046		.035	.030	-.228			.039			.003	-.001	-.009	.451			2
3	.038	.028			.007	.017	-.234			.045	.016		.186	-.042	.058	.397			3
4	.048	.018			-.011	.083	-.342			.013	.003			.060	.479	.356			4
5	.038	.020		.106	.035	-.272	-.364			.029	-.020		.337		.409				5
6	.022	.004		-.282		-.293				.021	.251		.534		.379				6
7	.028	.038		-.318		-.341				.234			.568		.369				7
8	.066	.125		-.311		-.325				.330	.400		.498						8
9	-.277	-.253		-.302						.437	.559								9
10	-.227	-.277		-.293						.466	.572								10
11	-.289	-.313								.413	.490								11
12	-.300	-.304																	12
13		-.259																	13
	α = 00°									δ = 30°									
1	.350	.308	.316	.313	.329	.334	-.294			.076	.060	.041	.040	-.002	.026	.841			1
2	.076	.055	.052	.050	.042	.035	-.338			.038		.018	.009	.003	.326	.835			2
3	.042	.031	.027	.027	.014	.025	-.397			.049	.018	-.007	.453	.356	.562	.683			3
4	.053	.024	.014	.005	-.002	.124	-.420			.017	.009	.077		.460	.604	.627			4
5	.040	.023	.003	.329	.046	-.373	-.424			.030	.144	.529	.475		.809				5
6	.024	.006	.033	-.366		-.376				.284	.496		.668		.751				6
7	.032	.051		-.393		-.405				.387			.785		.645				7
8	.072	.207		-.378		-.375				.420	.508		.688						8
9	-.362	-.319		-.358						.510	.808								9
10	-.315	-.362		-.298						.603	.939								10
11	-.371	-.373								.550	.758								11
12	-.286	-.350																	12
13		-.273																	13
	α = 03°									δ = 00°									
1	.348	.207	.249	.224	.240	.338	-.169			.146	.151	.151	.159	.133	.143	.112			1
2	.005	-.047	.094	-.155	-.182	-.234	-.189			.090		.089	.075	.095	.103	.106			2
3	.007	-.028	-.026	-.058	-.079	-.102	-.180			.095	.075	.062	.054	.034	.102	.101			3
4	.008	-.023	-.052	-.070	-.073	-.024	-.184			.076	.060	.050		.102	.027	.114			4
5	-.020	-.027	-.050	-.030	-.048	-.014	-.182			.075	.027	.084	-.053		-.026				5
6	-.011	-.037	-.036	-.059		-.100				.065	.063		-.061		-.079				6
7	-.007	-.019		-.091		-.163				.075			-.052		-.072				7
8	.014	-.010		-.081		-.149				-.006	-.034		-.039						8
9	-.036	-.007		-.077						-.048	-.032								9
10	-.075	-.055		-.290						-.065	-.046								10
11	-.072	-.072								-.052	-.044								11
12	-.058	-.059																	12
13		-.265																	13

[redacted]

Table 21 Continued

Pressure Coefficients on Delta Wing with Control

Configuration J1 M = 1.61 R = 4.2 x 10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
								α = 06°		δ = 00°									
1	.320	.128	.158	.124	.105	.186	-.310			.213	.241	.244	.252	.224	.233	.178			1
2	-.070	-.227	-.303	-.343	-.351	-.373	-.330			.145		.173	.150	.162	.191	.204			2
3	-.048	-.080	-.083	-.116	-.274	-.326	-.332			.150	.130	.126	.123	.112	.197	.170			3
4	-.033	-.072	-.095	-.125	-.093	-.268	-.337			.125	.118	.112		.191	.107	.193			4
5	-.062	-.073	-.102	-.034	-.084	-.248	-.330			.131	.081	.147	.010		.055				5
6	-.055	-.081	-.077	-.112		-.256				.113	.116		-.001		-.004				6
7	-.051	-.059		-.136		-.248				.107			.005		.012				7
8	-.001	-.013		-.123		-.218				.034	.004		.018						8
9	-.079	-.046		-.116						-.018	-.001								9
10	-.100	-.086		-.293						-.022	.007								10
11	-.105	-.112								-.005	.001								11
12	-.093	-.097																	12
13		-.280																	13
								α = 06°		δ = 10°									
1	.327	.135	.169	.124	.105	.189	-.316			.218	.246	.247	.255	.224	.232	.480			1
2	-.059	-.223	-.299	-.339	-.347	-.373	-.366			.154		.172	.147	.162	.187	.416			2
3	-.040	-.075	-.078	-.112	-.271	-.327	-.390			.161	.132	.129	.124	.106	.193	.351			3
4	-.026	-.067	-.091	-.117	-.092	-.266	-.397			.130	.124	.111		.190	.388	.306			4
5	-.055	-.067	-.098	-.017	-.083	-.297	-.388			.143	.086	.146	.251		.277				5
6	-.048	-.076	-.072	-.216		-.330				.118	.121		.262		.237				6
7	-.044	-.052		-.240		-.327				.118			.282		.232				7
8	.006	-.003		-.232		-.303				.221	.240		.278						8
9	-.184	-.144		-.217						.229	.249								9
10	-.168	-.185		-.285						.247	.259								10
11	-.209	-.219								.231	.243								11
12	-.212	-.208																	12
13		-.269																	13
								α = 06°		δ = 30°									
1	.321	.136	.166	.128	.109	.193	-.087			.208	.240	.245	.253	.221	.303	1.191			1
2	-.048	-.224	-.301	-.337	-.344	-.367	-.430			.145		.173	.147	.159	.630	1.044			2
3	-.044	-.080	-.079	-.119	-.267	-.315	-.439			.157	.125	.129	.627	.586	.664	.871			3
4	-.030	-.073	-.090	-.111	-.088	-.197	-.444			.122	.121	.516		.635	.715	.737			4
5	-.060	-.071	-.097	.434	-.079	-.413	-.432			.138	.533	.583	.655		1.052				5
6	-.056	-.078	-.056	-.378		-.432				.499	.573		.870		.995				6
7	-.048	-.024		-.392		-.428				.560			.987		.807				7
8	.017	.168		-.377		-.381				.583	.566		.834						8
9	-.377	-.290		-.331						.691	.660								9
10	-.325	-.364		-.309						.805	.800								10
11	-.388	-.353								.700	.735								11
12	-.314	-.310																	12
13		-.288																	13
								α = 09°		δ = 00°									
1	.290	.079	.085	.042	-.051	-.023	-.367			.292	.318	.319	.329	.302	.310	.235			1
2	-.140	-.328	-.386	-.413	-.421	-.446	-.398			.211		.249	.219	.233	.261	.259			2
3	-.071	-.120	-.143	-.334	-.379	-.414	-.421			.220	.204	.192	.188	.178	.257	.220			3
4	-.060	-.112	-.126	-.188	-.352	-.365	-.429			.196	.184	.176		.269	.158	.228			4
5	-.093	-.106	-.134	-.043	-.210	-.350	-.416			.190	.142	.204	.058		.097				5
6	-.083	-.118	-.102	-.174		-.363				.163	.174		.047		.049				6
7	-.076	-.097		-.194		-.376				.146			.056		.066				7
8	-.011	-.009		-.177		-.330				.052	-.044		.069						8
9	-.100	-.052		-.167						.024	.037								9
10	-.110	-.115		-.307						.022	.056								10
11	-.123	-.147								.042	.049								11
12	-.116	-.128																	12
13		-.282																	13
								α = 12°		δ = 00°									
1	.254	.011	-.010	-.044	-.164	-.182	-.397			.355	.384	.389	.396	.371	.376	.267			1
2	-.255	-.403	-.435	-.457	-.468	-.474	-.424			.272		.310	.287	.296	.341	.289			2
3	-.109	-.193	-.303	-.403	-.430	-.456	-.441			.265	.265	.260	.249	.252	.327	.269			3
4	-.101	-.179	-.218	-.276	-.413	-.425	-.436			.255	.245	.240		.344	.191	.257			4
5	-.133	-.158	-.173	-.038	-.276	-.391	-.419			.249	.198	.262	.076		.126				5
6	-.119	-.147	-.130	-.252		-.396				.208	.224		.067		.080				6
7	-.112	-.118		-.268		-.413				.169			.073		.097				7
8	-.046	.003		-.261		-.364				.052	.068		.086						8
9	-.101	-.052		-.252						.042	.048								9
10	-.117	-.109		-.329						.040	.065								10
11	-.133	-.141								.061	.060								11
12	-.126	-.122																	12
13		-.285																	13

[redacted]

Table 21 Continued

Pressure Coefficients on Delta Wing with Control

Configuration J1 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
								α = 12°			δ = 10°									
1	.248	.002	-.013	-.045	-.155	-.178	-.356				.348	.380	.393	.402	.374	.378	.747			1
2	-.261	-.411	-.438	-.457	-.458	-.468	-.415				.264		.310	.290	.311	.338	.578			2
3	-.114	-.198	-.297	-.398	-.420	-.449	-.422				.256	.261	.262	.249	.256	.323	.486			3
4	-.106	-.186	-.214	-.269	-.403	-.414	-.419				.248	.240	.240		.345	.654	.462			4
5	-.136	-.162	-.171	.016	-.261	-.424	-.415				.241	.192	.263	.466		.452				5
6	-.125	-.148	-.122	-.321		-.416					.200	.218		.461		.469				6
7	-.118	-.120		-.340		-.409					.165			.498		.442				7
8	-.051	.005		-.338		-.393					.368	.405		.465						8
9	-.237	-.185		-.320							.411	.440								9
10	-.225	-.244		-.330							.426	.448								10
11	-.273	-.277									.387	.421								11
12	-.280	-.262																		12
13		-.258																		13
								α = 12°			δ = 20°									
1	.251	.002	-.015	-.047	-.159	-.175	-.076				.351	.379	.387	.400	.371	.379	1.242			1
2	-.260	-.413	-.443	-.461	-.465	-.456	-.438				.266		.306	.285	.304	.347	.865			2
3	-.113	-.200	-.301	-.403	-.425	-.449	-.425				.260	.261	.260	.729	.247	.841	.731			3
4	-.106	-.187	-.217	-.268	-.408	-.389	-.424				.251	.239	.234		.728	1.061	.651			4
5	-.136	-.166	-.173	.590	-.241	-.449	-.420				.242	.189	.688	.749		.937				5
6	-.125	-.151	-.117	-.379		-.438					.210	.681		.884		.821				6
7	-.118	-.123		-.393		-.422					.642			.884		.712				7
8	-.031	.283		-.394		-.411					.684	.700		.725						8
9	-.320	-.245		-.387							.780	.842								9
10	-.298	-.333		-.339							.787	.858								10
11	-.354	-.360									.634	.705								11
12	-.340	-.339																		12
13		-.259																		13
								α = 12°			δ = 30°									
1	.244	-.006	-.021	-.051	-.163	-.206	.058				.343	.370	.384	.392	.362	.633	1.051			1
2	-.268	-.420	-.448	-.463	-.468	-.456	-.440				.257		.301	.385	.333	.863	1.093			2
3	-.124	-.207	-.308	-.409	-.429	-.450	-.433				.251	.251	.251	.813	.739	.894	.903			3
4	-.113	-.195	-.222	-.266	-.412	-.372	-.432				.241	.231	.708		.834	.964	.743			4
5	-.146	-.172	-.177	.653	-.224	-.448	-.423				.233	.701	.775	.817		1.250				5
6	-.132	-.159	-.124	-.426		-.438					.652	.760		.978		1.070				6
7	-.123	-.130		-.434		-.433					.749			1.060		.865				7
8	-.049	.200		-.416		-.427					.769	.757		.879						8
9	-.394	-.289		-.380							.862	.887								9
10	-.375	-.406		-.353							.872	1.006								10
11	-.417	-.395									.709	.848								11
12	-.347	-.341																		12
13		-.315																		13
								α = 15°			δ = 00°									
1	.212	-.056	-.146	-.147	-.268	-.292	-.338				.441	.468	.466	.471	.463	.487	.369			1
2	-.352	-.417	-.412	-.408	-.421	-.424	-.400				.347		.402	.413	.434	.462	.413			2
3	-.139	-.317	-.372	-.386	-.402	-.410	-.410				.336	.346	.384	.370	.386	.432	.352			3
4	-.131	-.289	-.360	-.353	-.400	-.375	-.388				.333	.362	.379		.483	.313	.314			4
5	-.158	-.136	-.355	.030	-.375	-.406	-.346				.354	.322	.376	.205		.218				5
6	-.147	-.162	-.330	-.338		-.419					.319	.345		.192		.226				6
7	-.141	-.141		-.359		-.396					.255			.196		.222				7
8	-.067	.029		-.348		-.356					.149	.183		.218						8
9	-.136	-.079		-.338							.154	.167								9
10	-.153	-.159		-.345							.159	.187								10
11	-.172	-.195									.176	.178								11
12	-.180	-.177																		12
13		-.287																		13
								α = -03°			δ = 00°									
1	.318	.314	.235	.268	.290	.293	-.161				.007	-.042	-.093	-.123	-.165	-.219	-.139			1
2	.120	.122	.139	.153	.148	.153	.244				-.007		-.035	-.055	-.063	-.108	-.163			2
3	.074	.078	.105	.077	.091	.110	.134				-.010	-.018	-.048	-.051	-.089	-.054	-.183			3
4	.075	.055	.067	.045	.053	.141	.135				-.030	-.035	-.054		-.031	-.057	-.154			4
5	.080	.064	.042	-.030	.096	.097	.141				-.015	-.061	-.007	-.094		-.121				5
6	.060	.040	.053	.015		-.020					-.018	-.024		-.110		-.139				6
7	.052	.059		-.047		-.071					.042			-.096		-.128				7
8	.011	-.011		-.048		-.042					-.059	-.069		-.072						8
9	.022	.051		-.042							-.097	-.064								9
10	-.049	-.028		-.305							-.105	-.076								10
11	-.038	-.049									-.096	-.075								11
12	-.015	-.030																		12
13		-.283																		13

[redacted]

Table 21 Continued

Pressure Coefficients on Delta Wing with Control

Configuration J1 M = 1.61 R = 4.2 x 10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = -06 °									δ = 00 °									
1	.283	.284	.140	.155	.199	.146	-.245			-.063	-.237	-.288	-.314	-.327	-.363	-.318			1
2	.197	.206	.232	.242	.243	.233	.327			-.043		-.091	-.126	-.265	-.327	-.350			2
3	.137	.150	.178	.151	.153	.189	.270			-.050	-.065	-.091	-.094	-.122	-.276	-.364			3
4	.137	.114	.130	.110	.126	.221	.265			-.065	-.077	-.101		-.093	-.260	-.344			4
5	.137	.120	.099	-.027	.155	.217	.262			-.055	-.095	-.046	-.176		-.297				5
6	.120	.097	.107	.121		.120				-.050	-.060		-.183		-.282				6
7	.105	.108		.065		.045				.035			-.166		-.255				7
8	.044	-.005		.059		.059				-.128	-.233		-.156						8
9	.107	.116		.079						-.137	-.125								9
10	.025	.051		-.289						-.158	-.146								10
11	.029	.046								-.162	-.146								11
12	.065	.063																	12
13		-.287																	13
	α = -06 °									δ = 10 °									
1	.291	.296	.151	.158	.202	.151	-.248			-.050	-.232	-.284	-.319	-.327	-.368	-.302			1
2	.212	.222	.247	.249	.245	.244	.118			-.032		-.085	-.125	-.267	-.327	-.287			2
3	.146	.166	.189	.158	.159	.198	.120			-.036	-.055	-.084	-.087	-.122	-.263	-.279			3
4	.150	.129	.141	.118	.134	.231	.114			-.059	-.068	-.095		-.092	-.230	-.267			4
5	.150	.134	.111	-.024	.163	.027	.124			-.042	-.085	-.041	-.052		-.212				5
6	.134	.112	.117	-.043		-.054				-.038	-.045		-.029		-.178				6
7	.121	.126		-.090		-.104				.065			-.003		-.151				7
8	.073	.007		-.097		-.099				.027	.020		-.017						8
9	-.048	-.011		-.081						-.013	.037								9
10	-.072	-.081		-.277						-.003	.030								10
11	-.101	-.108								.000	.017								11
12	-.083	-.084																	12
13		-.261																	13
	α = -06 °									δ = 20 °									
1	.281	.282	.134	.146	.186	.137	-.310			-.064	-.248	-.301	-.333	-.342	-.376	-.232			1
2	.203	.211	.232	.239	.238	.238	-.099			-.044		-.099	-.138	-.284	-.331	-.097			2
3	.145	.152	.177	.149	.151	.195	-.053			-.051	-.069	-.099	.077	-.137	-.180	-.043			3
4	.134	.116	.128	.108	.126	.226	-.071			-.070	-.081	-.110		-.057	-.129	.015			4
5	.141	.121	.100	.072	.158	-.175	-.087			-.056	-.103	.091	.105		-.008				5
6	.121	.101	.110	-.212		-.216				-.052	.169		.247		.064				6
7	.113	.121		-.252		-.265				.174			.293		.082				7
8	.105	.116		-.253		-.259				.196	.224		.269						8
9	-.213	-.154		-.241						.248	.318								9
10	-.180	-.229		-.290						.272	.344								10
11	-.244	-.262								.253	.298								11
12	-.251	-.252																	12
13		-.277																	13
	α = -06 °									δ = 30 °									
1	.281	.284	.134	.143	.188	.142	.057			-.063	-.252	-.300	-.334	-.342	-.043	.077			1
2	.208	.215	.239	.245	.244	.243	-.259			-.043		-.097	-.106	-.140	.030	.326			2
3	.147	.155	.182	.157	.157	.204	-.200			-.048	-.069	-.100	.158	-.059	.071	.338			3
4	.140	.119	.132	.118	.132	.239	-.302			-.069	-.081	-.071	.309	.085	.048	.355			4
5	.144	.125	.107	.177	.164	-.317	-.319			-.054	.139	.309	.230		.132				5
6	.126	.106	.122	-.327		-.335				.064	.306		.452		.215				6
7	.120	.137		-.356		-.367				.290			.527		.183				7
8	.149	.207		-.354		-.363				.327	.315		.510						8
9	-.338	-.237		-.347						.506	.461								9
10	-.296	-.341		-.298						.619	.572								10
11	-.348	-.361								.542	.526								11
12	-.351	-.344																	12
13		-.263																	13
	α = -09 °									δ = 00 °									
1	.254	.226	.035	.010	.064	.009	-.228			-.142	-.325	-.383	-.387	-.412	-.436	-.295			1
2	.283	.285	.315	.310	.314	.306	.356			-.079		-.215	-.313	-.367	-.409	-.309			2
3	.211	.213	.251	.223	.229	.254	.298			-.084	-.116	-.132	-.191	-.333	-.379	-.312			3
4	.206	.178	.194	.172	.198	.276	.293			-.102	-.128	-.146		-.178	-.294	-.259			4
5	.194	.187	.161	-.068	.220	.242	.278			-.088	-.122	-.081	-.189		-.303				5
6	.186	.162	.162	.131		.126				-.080	-.105		-.191		-.273				6
7	.169	.170		.060		.049				.029			-.163		-.256				7
8	.098	.001		.055		.087				-.118	-.116		-.126						8
9	.121	.146		.069						-.122	-.109								9
10	.040	.048		-.307						-.143	-.119								10
11	.054	.035								-.133	-.110								11
12	.081	.054																	12
13		-.281																	13

[redacted]

Table 21 Concluded

Pressure Coefficients on Delta Wing with Control

Configuration J1 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	$\alpha = -12°$									$\delta = 00°$									
1	.183	.107	-.067	-.157	-.084	-.129	-.202			-.278	-.376	-.422	-.429	-.460	-.471	-.412			1
2	.363	.374	.402	.383	.381	.372	.468			-.118		-.291	-.300	-.417	-.469	-.409			2
3	.278	.288	.320	.306	.316	.339	.419			-.125	-.157	-.270	-.211	-.341	-.447	-.408			3
4	.285	.252	.274	.252	.285	.354	.393			-.132	-.137	-.257		-.276	-.407	-.388			4
5	.261	.261	.236	-.095	.306	.359	.359			-.125	-.150	-.199	-.297		-.408				5
6	.270	.238	.238	.253		.250				-.117	-.124		-.297		-.391				6
7	.246	.243		.192		.195				.023			-.281		-.378				7
8	.163	.017		.195		.220				-.192	-.184		-.266						8
9	.221	.243		.216						-.165	-.175								9
10	.166	.180		-.297						-.212	-.201								10
11	.160	.173								-.220	-.195								11
12	.188	.194																	12
13		-.289																	13
	$\alpha = -12°$									$\delta = 10°$									
1	.187	.111	-.066	-.154	-.084	-.126	-.219			-.278	-.378	-.425	-.433	-.461	-.477	-.436			1
2	.362	.375	.404	.388	.383	.375	.188			-.118		-.292	-.301	-.413	-.470	-.429			2
3	.280	.291	.323	.309	.316	.342	.208			-.120	-.158	-.270	-.203	-.337	-.443	-.421			3
4	.286	.257	.277	.259	.286	.357	.222			-.130	-.137	-.257		-.261	-.399	-.400			4
5	.262	.264	.241	-.088	.305	.106	.230			-.120	-.151	-.201	-.224		-.398				5
6	.272	.242	.241	.026		.032				-.112	-.122		-.216		-.381				6
7	.248	.244		-.027		-.027				.037			-.177		-.354				7
8	.164	.015		-.032		-.010				-.028	-.032		-.192						8
9	.010	.050		-.014						-.054	-.017								9
10	-.030	-.032		-.301						-.068	-.032								10
11	-.047	-.046								-.068	-.039								11
12	-.022	-.020																	12
13		-.281																	13
	$\alpha = -12°$									$\delta = 20°$									
1	.186	.106	-.073	-.169	-.095	-.141	-.272			-.284	-.389	-.440	-.448	-.456	-.384	-.385			1
2	.363	.375	.404	.388	.383	.374	-.043			-.121		-.306	-.339	-.421	-.359	-.328			2
3	.281	.290	.323	.309	.314	.338	.018			-.126	-.165	-.281	-.190	-.365	-.306	-.286			3
4	.287	.257	.274	.253	.284	.356	.034			-.140	-.145	-.270		-.235	-.334	-.259			4
5	.261	.262	.239	-.070	.305	-.113	.050			-.127	-.157	-.197	-.155		-.297				5
6	.270	.245	.241	-.167		-.158				-.117	.055		-.150		-.264				6
7	.250	.248		-.210		-.211				.121			-.120		-.260				7
8	.179	.100		-.211		-.205				.158	.161		-.104						8
9	-.172	-.110		-.198						.164	.266								9
10	-.149	-.188		-.332						.175	.286								10
11	-.194	-.220								.178	.268								11
12	-.203	-.212																	12
13		-.294																	13
	$\alpha = -12°$									$\delta = 30°$									
1	.186	.105	-.073	-.165	-.092	-.136	-.312			-.280	-.384	-.432	-.418	-.340	-.222	-.154			1
2	.362	.374	.402	.386	.381	.375	-.203			-.124		-.311	-.324	-.311	-.186	-.061			2
3	.282	.288	.324	.309	.314	.342	-.116			-.122	-.163	-.270	-.114	-.270	-.149	.017			3
4	.286	.255	.276	.256	.284	.358	-.125			-.142	-.144	-.264		-.149	-.179	.072			4
5	.263	.260	.243	-.009	.305	-.260	-.153			-.125	-.146	.069	-.133		-.138				5
6	.266	.244	.242	-.282		-.276				-.084	.205		-.114		-.107				6
7	.247	.255		-.314		-.318				.220			-.089		-.149				7
8	.207	.214		-.314		-.323				.273	.219		-.101						8
9	-.286	-.191		-.305						.388	.400								9
10	-.241	-.298		-.333						.428	.580								10
11	-.296	-.320								.373	.521								11
12	-.309	-.319																	12
13		-.290																	13
	$\alpha = -15°$									$\delta = 00°$									
1		.042	-.118	-.252	-.157	-.216	-.187												1
2		.429	.441	.421	.430	.421	.473			-.339	-.393	-.417	-.410	-.430	-.426	-.327			2
3	.333	.345	.383	.390	.393	.420	.440			-.131		-.367	-.377	-.407	-.412	-.331			3
4	.342	.312	.363	.337	.371	.421	.395			-.132	-.239	-.375	-.341	-.401	-.389	-.315			4
5	.320	.342	.326	-.065	.382	.391	.358			-.151	-.137	-.368		-.355	-.347	-.252			5
6	.335	.336	.319	.282		.253				-.136	-.161	-.288	-.307		-.362				6
7	.321	.323		.200		.200				-.117	-.136		-.325		-.319				7
8	.176	.045		.194		.237				.020			-.309		-.309				8
9	.261	.282		.221						-.140	-.148		-.288						9
10	.193	.189		-.344						-.142	-.133								10
11	.191	.174								-.179	-.146								11
12	.224	.193								-.167	-.138								12
13		-.281																	13

[redacted]

Table 22

Pressure Coefficients on Delta Wing with Control

Configuration J2 M = 1.61 R = 4.2 x 10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 00°									δ = 00°									
1	.343			.297	.300	.329	-.050			.068		.030	.032	-.001	.002	-.006			1
2	.062			.023	.014	.005	.065			.032		.002	-.007	-.006	-.010	.003			2
3	.027			.000	-.015	-.001	.101			.025		-.017	-.019	-.046	.019	-.014			3
4	.033			-.024	-.026	.061						-.026		.020	-.027	-.017			4
5	.023			-.040	.009	.047	.067					.034	-.023		-.035				5
6	.016			.022		.015							-.030		-.048				6
7	.011			.030		.003							-.036		-.034				7
8	.018			.035		.022							-.024						8
9	.025			.030															9
10	.013			-.313															10
11	.023																		11
12	.032																		12
	α = 00°									δ = 10°									
1	.338	.294	.309	.301	.308	.325	-.016			.062	.042	.030	.036	-.001	-.005	.290			1
2	.057	.036	.034	.028	.024	.010	-.142			.025		.001	-.002	-.006	-.015	.238			2
3	.024	.011	.008	.007	-.005	.005	-.021			.027	.002	-.021	-.008	-.044	.017	.243			3
4	.033	.007	-.004	-.019	-.019	.065				.000	-.004	-.022		.025	.216	.241			4
5	.024	.005	-.016	.010	.019	-.157	-.226			.014	-.030	.039	.232		.272				5
6	.013	-.015	-.003	-.170		-.171				.005	.003		.277		.229				6
7	.008	.005		-.166		-.200				.106			.286		.220				7
8	.028	.030		-.154		-.168				.225	.297		.296						8
9	-.176	-.149		-.163						.226	.313								9
10	-.125	-.146		-.313							.300								10
11	-.164	-.166									.280								11
12	-.164	-.171																	12
13		-.301																	13
	α = 00°									δ = 20°									
1	.338	.296		.302	.304	.322	-.105			.063	.046	.026	.030	-.010	-.007	.508			1
2	.065	.038		.031	.026	.014	-.281			.024		.000	-.006	-.009	-.013	.586			2
3	.025	.011	.015	.008	-.005	.006	-.079			.034	.003	-.023	.347	-.049	.252	.591			3
4	.038	.009	-.002	-.015	-.020	.085				-.002	.000	-.021		.354	.525	.550			4
5	.027	.007	-.017	.230	.023	-.291	-.359			.017	-.026	.440	.381		.763				5
6	.010	-.013	.009	-.289		-.289				.018	.406		.616		.650				6
7	.013	.028		-.299		-.317				.327			.744		.583				7
8	.071	.186		-.284		-.292				.371	.418		.637						8
9	-.293	-.269		-.290						.531	.634								9
10	-.216	-.273		-.337							.763								10
11	-.292	-.287									.614								11
12	-.287	-.295																	12
13		-.326																	13
	α = 00°									δ = 30°									
1	.339	.299	.310	.302	.305	.321	.404			.064	.044	.028	.030	-.011	.053	.969			1
2	.062	.042	.035	.034	.028	.022	-.368			.026		.002	.021	.003	.395	.914			2
3	.027	.015	.010	.013	.000	.010	-.114			.035	.004	-.011	.539	.408	.677	.829			3
4	.040	.011	-.001	-.013	-.019	.109				.003	-.006	.326		.532	.963	.695			4
5	.028	.009	-.013	.361	.024	-.388	-.422			.018	.363	.571	.555		.956				5
6	.011	-.009	.010	-.378		-.378				.364	.529		.700		.872				6
7	.019	.031		-.393		-.396				.409			.794		.760				7
8	.065	.160		-.378		-.380				.466	.575		.703						8
9	-.376	-.359		-.380						.531	.892								9
10	-.316	-.370		-.346							1.023								10
11	-.382	-.379									.854								11
12	-.372	-.386																	12
13		-.342																	13
	α = 03°									δ = 00°									
1	.337	.186	.236	.206	.274	-.322	-.186			.132	.142	.148	.159	.132	.150	.126			1
2	-.007	-.068	-.118	-.190	-.208	-.255	-.226			.077		.084	.070	.092	.106	.139			2
3	-.022	-.046	-.044	-.075	-.092	-.133	-.114			.082	.057	.051	.049	.027	.099	.133			3
4	-.005	-.042	-.067	-.086	-.092	-.034				.055	.051	.030		.111	.046	.129			4
5	-.030	-.044	-.072	-.040	-.059	-.026	-.208			.067	.015	.077	.055		.066				5
6	-.032	-.060	-.055	-.046		-.076				.054	.051		.039		.044				6
7	-.030	-.038		-.035		-.091				.078			.029		.051				7
8	.014	-.004		-.026		-.074				.058	.034		.047						8
9	-.022	.000		-.030						.026	.048								9
10	-.019	-.005		-.308							.036								10
11	-.026	-.010									.035								11
12	-.021	-.014																	12
13		-.300																	13

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Table 22 Continued

Pressure Coefficients on Delta Wing with Control

Configuration J2 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 06°									δ = 00°									
1	.312	.112	.154	.112	.112	.169	-.333			.200	.225	.232	.240	.212	.221	.194			1
2	-.080	-.250	-.329	-.364	-.373	-.398	-.354			.132		.156	.139	.152	.182	.216			2
3	-.062	-.095	-.100	-.131	-.295	-.349	-.196			.138	.118	.114	.113	.096	.171	.216			3
4	-.044	-.091	-.114	-.145	-.121	-.288				.116	.105	.083		.186	.124	.211			4
5	-.078	-.088	-.118	-.049	-.101	-.268	-.340			.115	.067	.131	.110		.138				5
6	-.067	-.100	-.096	-.103		-.233				.096	.100		.091		.101				6
7	-.066	-.075		-.082		-.200				.104			.076		.112				7
8	.003	-.007		-.063		-.150				.077	.095		.095						8
9	-.048	-.034		-.070						.072	.084								9
10	-.043	-.032		-.322							.076								10
11	-.052	-.043									.075								11
12	-.049	-.043																	12
13		-.309																	13
	α = 06°									δ = 10°									
1	.312	.114	.157	.117	.116	.173	-.305			.199	.225	.235	.244	.213	.222	.579			1
2	-.080	-.247	-.325	-.362	-.363	-.392	-.405			.130		.155	.139	.150	.179	.485			2
3	-.061	-.093	-.097	-.133	-.288	-.346	-.180			.139	.119	.114	.124	.097	.170	.491			3
4	-.043	-.088	-.111	-.140	-.116	-.287				.112	.105	.085		.191	.476	.450			4
5	-.077	-.087	-.118	.057	-.099	-.326	-.400			.119	.069	.142	.447		.525				5
6	-.066	-.096	-.085	-.239		-.341				.097	.100		.477		.456				6
7	-.063	.060		-.238		-.322				.173			.485		.433				7
8	.019	.075		-.224		-.281				.363	.439		.467						8
9	-.209	-.197		-.222						.417	.464								9
10	-.169	-.197		-.330							.454								10
11	-.218	-.211									.424								11
12	-.208	-.217																	12
13		-.313																	13
	α = 06°									δ = 20°									
1	.316	.119	.160	.120	.122	.175	.249			.203	.230	.233	.245	.213	.220	1.247			1
2	-.069	-.231	-.308	-.337	-.345	-.370	-.426			.137		.161	.139	.153	.178	.857			2
3	-.052	-.084	-.082	-.121	-.272	-.325	-.099			.148	.117	.119	.548	.107	.615	.776			3
4	-.035	-.077	-.095	-.118	-.104	-.251				.113	.111	.092		.557	.768	.662			4
5	-.068	-.077	-.102	.401	-.088	-.417	-.426			.126	.095	.542	.562		1.016				5
6	-.060	-.087	-.063	-.337		-.421				.183	.531		.711		.856				6
7	-.055	-.030		-.368		-.394				.502			.829		.737				7
8	.023	.169		-.364		-.375				.539	.538		.724						8
9	-.322	-.312		-.360						.667	.697								9
10	-.274	-.322		-.343							.827								10
11	-.342	-.353									.724								11
12	-.331	-.353																	12
13		-.322																	13
	α = 06°									δ = 30°									
1	.315	.113	.155	.113	.117	.181	.028			.199	.222	.229	.238	.210	.543	.943			1
2	-.079	-.249	-.325	-.361	-.367	-.383	-.473			.129		.153	.353	.191	.714	1.118			2
3	-.059	-.093	-.096	-.136	-.286	-.334	-.109			.142	.109	.228	.667	.617	.736	.958			3
4	-.042	-.088	-.110	-.133	-.117	-.210				.112	.106	.521		.678	.772	.763			4
5	-.073	-.084	-.116	.454	-.098	-.467	-.464			.125	.551	.599	.699		1.044				5
6	-.068	-.095	-.077	-.418		-.461				.548	.589		.923		1.104				6
7	-.063	-.040		-.440		-.445				.575			1.074		.909				7
8	-.005	.141		-.436		-.445				.588	.578		.929						8
9	-.402	-.396		-.423						.666	.644								9
10	-.371	-.408		-.367							.767								10
11	-.413	-.407									.723								11
12	-.374	-.359																	12
13		-.334																	13
	α = 09°									δ = 00°									
1	.274	.046	.067	.018	-.064	-.052	-.306			.276	.304	.309	.321	.298	.310	.279			1
2	-.166	-.355	-.411	-.436	-.443	-.463	-.427			.193		.237	.211	.227	.259	.301			2
3	-.096	-.145	-.198	-.354	-.402	-.432	-.220			.204	.186	.183	.180	.171	.249	.303			3
4	-.080	-.134	-.151	-.210	-.380	-.383				.176	.170	.149		.272	.212	.292			4
5	-.113	-.131	-.156	-.062	-.239	-.365	-.425			.177	.129	.194	.192		.232				5
6	-.104	-.144	-.131	-.175		-.357				.146	.155		.169		.194				6
7	-.101	-.119		-.159		-.342				.141			.150		.204				7
8	-.023	-.001		-.137		-.300				.124	.162		.178						8
9	-.095	-.082		-.140						.140	.158								9
10	-.080	-.089		-.341							.141								10
11	-.091	-.101									.148								11
12	-.095	-.096																	12
13		-.319																	13

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Table 22 Continued

Pressure Coefficients on Delta Wing with Control

Configuration J2 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
							α = 12°			δ = 00°									
1	.247	-.017	-.031	-.075	-.184	-.206	-.291			.344	.372	.379	.390	.355	.367	.334			1
2	-.264	-.413	-.454	-.476	-.483	-.492	-.455			.260		.295	.279	.296	.326	.349			2
3	-.121	-.206	-.346	-.420	-.450	-.473	-.227			.253	.249	.246	.241	.243	.316	.373			3
4	-.112	-.196	-.220	-.310	-.436	-.449				.244	.233	.213		.342	.273	.344			4
5	-.146	-.180	-.201	-.053	-.300	-.411	-.435			.236	.185	.253	.250		.288				5
6	-.131	-.166	-.168	-.267		-.400				.194	.208		.223		.257				6
7	-.125	-.136		-.265		-.399				.169			.204		.264				7
8	-.043	.005		-.239		-.363				.167	.211		.231						8
9	-.110	-.099		-.244						.200	.215								9
10	-.096	-.107		-.367							.193								10
11	-.121	-.121									.199								11
12	-.115	-.113																	12
13		-.320																	13
							α = 12°			δ = 10°									
1	.244	-.019	-.031	-.075	-.185	-.210	-.137			.343	.372	.382	.390	.356	.366	.837			1
2	-.268	-.433	-.465	-.486	-.488	-.505	-.458			.260		.294	.276	.292	.320	.661			2
3	-.126	-.210	-.352	-.431	-.453	-.482	-.174			.252	.251	.245	.365	.236	.310	.643			3
4	-.117	-.198	-.220	-.302	-.435	-.448				.243	.231	.214		.387	.821	.569			4
5	-.144	-.183	-.202	.310	-.292	-.444	-.433			.234	.182	.359	.666		.753				5
6	-.134	-.167	-.162	-.331		-.422				.194	.355		.720		.652				6
7	-.130	-.134		-.335		-.419				.390			.681		.595				7
8	-.031	.199		-.315		-.400				.575	.638		.600						8
9	-.215	-.219		-.308						.638	.682								9
10	-.190	-.210		-.378							.648								10
11	-.243	-.227									.564								11
12	-.230	-.227																	12
13		-.330																	13
							α = 12°			δ = 20°									
1	.241	-.021	-.032	-.077	-.185	-.207	.290			.338	.368	.377	.387	.353	.366	1.111			1
2	-.272	-.439	-.470	-.489	-.493	-.490	-.465			.257		.292	.274	.290	.736	.928			2
3	-.123	-.214	-.354	-.424	-.456	-.478	-.146			.249	.248	.243	.757	.585	.850	.831			3
4	-.119	-.200	-.221	-.302	-.439	-.400				.242	.228	.502		.776	.973	.673			4
5	-.149	-.185	-.202	.614	-.286	-.467	-.441			.232	.559	.734	.763		1.115				5
6	-.137	-.171	-.162	-.394		-.443				.506	.719		.935		.950				6
7	-.131	-.134		-.399		-.440				.705			.973		.791				7
8	-.047	.251		-.386		-.432				.720	.726		.800						8
9	-.315	-.323		-.384						.834	.871								9
10	-.285	-.317		-.392							.931								10
11	-.345	-.337									.777								11
12	-.333	-.338																	12
13		-.351																	13
							α = 12°			δ = 30°									
1	.244	-.015	-.028	-.065	-.170	-.280	.162			.341	.370	.376	.385	.351	.724	.972			1
2	-.261	-.417	-.445	-.466	-.470	-.465	-.445			.260		.291	.683	.644	.879	1.115			2
3	-.116	-.199	-.333	-.410	-.434	-.461	-.139			.252	.248	.577	.847	.789	.928	.960			3
4	-.111	-.188	-.204	-.270	-.413	-.384				.241	.233	.738		.868	.999	.745			4
5	-.141	-.173	-.188	.684	-.240	-.451	-.426			.262	.736	.809	.847		1.296				5
6	-.130	-.158	-.148	-.408		-.430				.703	.794		1.003		1.165				6
7	-.122	-.127		-.411		-.429				.781			1.100		.946				7
8	-.059	.185		-.396		-.426				.796	.788		.939						8
9	-.359	-.366		-.387						.865	.903								9
10	-.342	-.362		-.371							1.037								10
11	-.384	-.367									.904								11
12	-.368	-.352																	12
13		-.337																	13
							α = 15°			δ = 00°									
1	.204	-.083	-.155	-.171	-.284	-.306	-.228			.420	.448	.446	.444	.425	.460	.409			1
2	-.365	-.451	-.457	-.441	-.452	-.449	-.416			.323		.368	.386	.404	.433	.434			2
3	-.149	-.305	-.403	-.410	-.437	-.435	-.232			.307	.317	.350	.343	.356	.419	.454			3
4	-.141	-.292	-.384	-.394	-.432	-.400				.314	.323	.326		.458	.373	.436			4
5	-.172	-.158	-.379	.032	-.409	-.430	-.384			.317	.288	.348	.353		.382				5
6	-.162	-.186	-.345	-.377		-.440				.283	.308		.328		.379				6
7	-.152	-.163		-.384		-.425				.239			.301		.371				7
8	-.056	.048		-.377		-.390				.252	.309		.332						8
9	-.134	-.124		-.370						.295	.315								9
10	-.132	-.137		-.398							.290								10
11	-.154	-.163									.298								11
12	-.150	-.154																	12
13		-.335																	13

[redacted]

Table 22 Continued

Pressure Coefficients on Delta Wing with Control

Configuration J2 M = 1.61 R = 4.2 x 10⁶

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = −03°									δ = 00°									
1	.324	.312	.244	.260	.300	.278	−.164			.007	−.044	−.097	−.117	−.171	−.223	−.142			1
2	.118	.117	.132	.135	.131	.129	.136			−.008		−.044	−.069	−.075	−.110	−.149			2
3	.069	.075	.092	.063	.073	.092	.120			−.007	−.020	−.062	−.060	−.106	−.068	−.183			3
4	.075	.050	.055	.031	.033	.126				−.032	−.040	−.074		−.042	−.050	−.141			4
5	.078	.058	.028	−.026	.076	.083	.106			−.015	−.065	−.019	−.016		−.063				5
6	.060	.031	.036	.048		.018				−.023	−.027		−.047		−.065				6
7	.052	.050		.038		.015				.048			−.044		−.043				7
8	.032	.022		.015		.046				−.006	.013		−.020						8
9	.042	.067		.034						−.021	.009								9
10	.031	.053		−.329							−.015								10
11	.048	.050									−.007								11
12	.057	.044																	12
13		−.302																	13
	α = −06°									δ = 00°									
1	.280	.280	.135	.147	.204	.137	−.281			−.068	−.245	−.293	−.329	−.337	−.364	−.370			1
2	.183	.194	.216	.223	.216	.218	.252			−.051		−.103	−.137	−.273	−.327	−.392			2
3	.121	.138	.163	.131	.129	.177	.249			−.057	−.075	−.103	−.104	−.145	−.281	−.400			3
4	.126	.100	.112	.089	.101	.203				−.076	−.087	−.120		−.108	−.272	−.377			4
5	.125	.108	.083	−.034	.136	.215	.280			−.063	−.106	−.060	−.133		−.279				5
6	.109	.084	.085	.153		.186				−.060	−.069		−.134		−.237				6
7	.096	.092		.151		.158				.027			−.125		−.178				7
8	.065	.019		.146		.166				−.088	−.065		−.120						8
9	.126	.140		.147						−.073	−.075								9
10	.114	.135		−.313							−.103								10
11	.121	.146									−.101								11
12	.134	.137																	12
13		−.304																	13
	α = −06°									δ = 10°									
1	.278	.280	.138	.149	.207	.142	−.312			−.065	−.240	−.287	−.322	−.329	−.357	−.295			1
2	.183	.193	.218	.226	.222	.224	.007			−.050		−.097	−.130	−.264	−.317	−.257			2
3	.123	.137	.165	.138	.137	.185	.175			−.057	−.071	−.096	−.064	−.132	−.262	−.211			3
4	.124	.103	.117	.096	.110	.211				−.076	−.081	−.112		−.099	−.201	−.204			4
5	.126	.109	.089	.016	.145	−.030	.073			−.062	−.104	−.031	.050		−.067				5
6	.106	.089	.092	−.077		−.051				−.060	−.037		.112		−.010				6
7	.096	.099		−.076		−.080				.076			.123		.023				7
8	.068	.072		−.072		−.060				.114	.181		.130						8
9	−.105	−.081		−.077						.117	.182								9
10	−.060	−.075		−.304							.166								10
11	−.099	−.089									.153								11
12	−.091	−.093																	12
13		−.302																	13
	α = −06°									δ = 20°									
1	.274	.278	.134	.141	.200	.133	−.213			−.069	−.249	−.299	−.329	−.339	−.353	−.162			1
2	.187	.196	.221	.228	.227	.231	−.180			−.051		−.101	−.135	−.272	−.291	.007			2
3	.125	.142	.167	.143	.144	.194	.056			−.058	−.072	−.099	−.162	−.134	−.110	.083			3
4	.127	.106	.119	.101	.116	.219				−.076	−.085	−.117		.183	−.056	.122			4
5	.129	.113	.091	.173	.154	−.206	−.150			−.063	−.106	.244	.224		.149				5
6	.108	.090	.104	−.226		−.212				−.060	.244		.428		.263				6
7	.099	.114		−.236		−.237				.240			.495		.272				7
8	.133	.176		−.226		−.228				.302	.282		.441						8
9	−.253	−.228		−.234						.441	.453								9
10	−.175	−.222		−.319							.531								10
11	−.244	−.240									.471								11
12	−.244	−.249																	12
13		−.316																	13
	α = −06°									δ = 30°									
1	.270	.273	.129	.142	.196	.181	.186			−.069	−.249	−.298	−.331	−.230	.055	.231			1
2	.191	.202	.226	.235	.233	.240	−.278			−.051		−.095	−.046	−.056	.141	.413			2
3	.125	.146	.175	.151	.154	.210	−.010			−.054	−.072	−.104	.134	−.009	.178	.460			3
4	.132	.110	.126	.110	.125	.240				−.073	−.083	.191		.105	.141	.433			4
5	.133	.118	.100	.159	.161	−.296	−.288			−.060	.206	.314	.192		.193				5
6	.113	.097	.113	−.301		−.288				.207	.341		.326		.259				6
7	.105	.126		−.313		−.312				.319			.413		.237				7
8	.142	.196		−.300		−.307				.342	.344		.430						8
9	−.321	−.299		−.310						.514	.462								9
10	−.251	−.298		−.321							.599								10
11	−.326	−.310									.567								11
12	−.313	−.321																	12
13		−.322																	13

[redacted]

Table 22 Continued

Pressure Coefficients on Delta Wing with Control

Configuration J2 $M = 1.61$ $R = 4.2 \times 10^6$

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	$\alpha = -09^\circ$									$\delta = 00^\circ$									
1	.239	.208	.028	.005	.064	-.005	-.235			-.165	-.347	-.402	-.409	-.427	-.453	-.331			1
2	.264	.277	.305	.302	.302	.298	.327			-.092		-.230	-.326	-.382	-.428	-.327			2
3	.187	.200	.241	.215	.218	.247	.294			-.100	-.130	-.137	-.191	-.345	-.395	-.364			3
4	.191	.167	.185	.163	.188	.261				-.114	-.137	-.158		-.191	-.325	-.302			4
5	.182	.176	.153	-.050	.216	.273	.342			-.105	-.132	-.087	-.156		-.323				5
6	.171	.151	.150	.214		.233				-.096	-.113		-.170		-.286				6
7	.154	.144		.202		.211				.015			-.144		-.243				7
8	.109	.029		.187		.227				-.088	-.072		-.118						8
9	.154	.190		.197						-.093	-.079								9
10	.159	.181		-.341							-.103								10
11	.172	.187									-.093								11
12	.183	.179																	12
13		-.323																	13
	$\alpha = -12^\circ$									$\delta = 00^\circ$									
1	.182	.102	-.071	-.159	-.089	-.137	-.195			-.280	-.390	-.440	-.454	-.486	-.485	-.410			1
2	.347	.359	.389	.375	.363	.360	.425			-.131		-.304	-.333	-.444	-.476	-.406			2
3	.259	.275	.312	.292	.297	.319	.357			-.134	-.165	-.272	-.237	-.354	-.461	-.405			3
4	.268	.241	.258	.232	.263	.334				-.148	-.151	-.257		-.272	-.421	-.371			4
5	.251	.244	.220	-.065	.284	.376	.451			-.134	-.163	-.198	-.282		-.403				5
6	.244	.222	.214	.314		.357				-.126	-.133		-.299		-.382				6
7	.222	.215		.304		.351				.001			-.276		-.370				7
8	.164	.055		.319		.341				-.135	-.129		-.263						8
9	.252	.282		.308						-.124	-.134								9
10	.268	.292		-.355							-.168								10
11	.278	.305									-.161								11
12	.282	.290																	12
13		-.327																	13
	$\alpha = -12^\circ$									$\delta = 10^\circ$									
1	.182	.101	-.073	-.162	-.095	-.141	-.305			-.280	-.394	-.450	-.465	-.491	-.491	-.437			1
2	.347	.359	.387	.376	.364	.360	.098			-.131		-.305	-.337	-.446	-.481	-.428			2
3	.259	.275	.311	.292	.298	.323	.276			-.135	-.166	-.273	-.195	-.358	-.457	-.419			3
4	.268	.242	.258	.234	.262	.336				-.147	-.153	-.256		-.226	-.403	-.382			4
5	.254	.245	.222	-.063	.286	.089	.232			-.121	-.162	-.199	-.203		-.365				5
6	.247	.226	.215	.020		.068				-.125	-.112		-.171		-.325				6
7	.224	.218		.021		.039				.051			-.157		-.308				7
8	.164	.056		.028		.061				.056	.104		-.163						8
9	-.026	.009		.015						.027	.079								9
10	.024	.015		-.358							.061								10
11	-.003	.010									.053								11
12	.010	.011																	12
13		-.325																	13
	$\alpha = -12^\circ$									$\delta = 20^\circ$									
1	.180	.100	-.066	-.152	-.092	-.135	-.331			-.269	-.376	-.426	-.438	-.428	-.309	-.276			1
2	.348	.359	.387	.378	.367	.365	-.108			-.127		-.289	-.332	-.382	-.289	-.242			2
3	.261	.275	.315	.290	.301	.327	.150			-.128	-.157	-.257	-.200	-.347	-.255	-.176			3
4	.269	.245	.260	.237	.267	.341				-.140	-.141	-.243		-.236	-.270	-.183			4
5	.256	.247	.224	-.024	.290	-.103	.036			-.126	-.152	.010	-.157		-.221				5
6	.248	.231	.220	-.155		-.123				-.117	.171		-.128		-.174				6
7	.226	.227		-.163		-.153				.152			-.101		-.202				7
8	.181	.182		-.151		-.142				.241	.204		-.088						8
9	-.190	-.158		-.163						.295	.387								9
10	-.110	-.151		-.342							.448								10
11	-.163	-.167									.400								11
12	-.164	-.175																	12
13		-.321																	13
	$\alpha = -12^\circ$									$\delta = 30^\circ$									
1	.183	.104	-.070	-.159	-.096	-.131	-.236			-.276	-.393	-.416	-.383	-.275	-.151	-.055			1
2	.352	.364	.394	.383	.375	.364	-.264			-.129		-.341	-.281	-.264	-.108	.063			2
3	.264	.278	.319	.301	.308	.327	-.009			-.133	-.166	-.292	-.082	-.230	-.074	.142			3
4	.272	.247	.263	.242	.272	.341				-.148	-.144	-.214		-.126	-.090	.171			4
5	.260	.248	.230	.015	.295	-.261	-.210			-.130	-.015	.047	-.079		-.060				5
6	.251	.230	.224	-.294		-.275				.098	.244		-.043		-.027				6
7	.233	.239		-.308		-.302				.251			.010		-.073				7
8	.219	.244		-.293		-.300				.292	.256		-.006						8
9	-.311	-.289		-.303						.436	.473								9
10	-.235	-.295		-.345							.686								10
11	-.303	-.306									.624								11
12	-.294	-.317																	12
13		-.359																	13

[redacted]

Table 22 Concluded

Pressure Coefficients on Delta Wing with Control

Configuration J2 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
	$\alpha = -15^\circ$										$\delta = 00^\circ$									
1	.117	-.007	-.154	-.292	-.194	-.253	-.177				-.373	-.419	-.435	-.431	-.457	-.446	-.343			1
2	.416	.425	.440	.434	.448	.430	.459				-.161		-.394	-.409	-.434	-.433	-.341			2
3	.323	.344	.398	.401	.406	.433	.404				-.164	-.284	-.404	-.374	-.424	-.411	-.359			3
4	.333	.317	.372	.341	.383	.423					-.178	-.158	-.394		-.382	-.370	-.285			4
5	.321	.352	.332	-.005	.398	.444	.490				-.163	-.183	-.329	-.316		-.379				5
6	.346	.341	.316	.383		.406					-.146	-.154		-.347		-.341				6
7	.322	.313		.358		.399					-.015			-.325		-.323				7
8	.196	.090		.358		.401					-.113	-.116		-.305						8
9	.306	.342		.353							-.128	-.113								9
10	.327	.353		-.380								-.142								10
11	.347	.349										-.133								11
12	.344	.340																		12
13		-.329																		13

[redacted]

Table 23

Pressure Coefficients on Delta Wing with Control

Configuration J3 M = 1.61 R = 4.2 x 10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
								α = 00°		δ = 00°									
1	.341	.296	.310	.299	.338	.370	.106			.065	.044	.032	.034	-.001	.000	.206			1
2	.060	.037	.031	.027	.017	.003	.165			.030		.002	-.003	-.005	-.009	.186			2
3	.027	.010	.007	.001	-.009	.001	.234			.027	.002	-.019	.001	-.042	-.051	-.122			3
4	.035	.007	-.007	-.022	-.021	.063	-.121			.002	-.006	-.018		.063	.175	-.272			4
5	.024	.003	-.019	-.112	.008	.169	-.213			.017	-.029	.040	.103		-.132				5
6	.017	-.017	-.005	.072						.013	.060		-.072		-.404				6
7	.013	.004		-.112		-.325				.045			-.350		-.219				7
8	-.003	-.038		-.228		-.138							-.157						8
9		-.091		-.084							-.167								9
10	-.110	-.110								-.191	-.171								10
11	-.120	-.099								-.153	-.155								11
12	-.095	-.091																	12
								α = 00°		δ = 10°									
1	.337	.292	.306	.297	.339	.363	.114			.059	.040	.025	.028	-.010	-.006	.416			1
2	.056	.035	.030	.026	.017	.009	.099			.023		-.002	-.007	-.010	-.017	.278			2
3	.024	.007	.006	-.001	-.007	.002	.118			.027	-.003	-.024	.197	-.049	.385	.001			3
4	.034	.003	-.008	-.024	-.021	.084	-.198			-.003	-.010	-.020		.310	.345	-.139			4
5	.020	.002	-.021	-.114	.007	.096	-.311			.011	-.034	.036	.065		-.263				5
6	.010	-.017	-.006	.065						.007	.052		-.241		-.198				6
7	.009	.004		.033		-.370				.056			-.015		-.050				7
8	-.007	-.044		-.337		-.280							.047						8
9		-.232		-.234							.006								9
10	-.204	-.236								-.009	.062								10
11	-.253	-.247								.044	.097								11
12	-.239	-.181																	12
								α = 00°		δ = 30°									
1	.338	.294	.304	.296	.338	.359	.101			.056	.036	.022	.023	-.018	.099	1.207			1
2	.060	.036	.031	.030	.024	.023	-.072			.022		-.005	-.010	-.014	.485	.507			2
3	.024	.008	.007	.003	-.004	.014	-.223			.026	-.006	-.027	.374	.344	.483	.423			3
4	.035	.003	-.006	-.014	-.017	.113	-.367			-.005	-.011	.075		.250	.813	.583			4
5	.021	.000	-.019	-.108	.021	.159	-.411			.013	.231	.542	.587		.078				5
6	.009	-.013	.003	.009						.284	.499		.425		.508				6
7	.013	.014		.093		-.380				.386			.573		.449				7
8	.035	.084		-.411		-.406					.750		.486						8
9		-.360		-.387															9
10	-.333	-.338								.575	.924								10
11	-.364	-.311								.571	.806								11
12	-.280	-.282																	12
								α = 00°		δ = 20°									
1	.340	.297	.308	.299	.342	.362	.089			.058	.040	.024	.028	-.013	-.011	.628			1
2	.061	.039	.035	.032	.026	.021	-.043			.025		-.001	-.007	-.010	.074	.494			2
3	.027	.011	.009	.006	-.001	.011	-.092			.028	-.002	-.024	-.106	-.049	.032	.175			3
4	.035	.006	-.003	-.015	-.012	.064	-.381			-.003	-.009	-.018		-.067	.297	.273			4
5	.023	.005	-.016	-.105	.017	.218	-.423			.015	-.028	.365	.126		.016				5
6	.014	-.011	.004	.098						.010	.348		.201		.316				6
7	.014	.013		.100		-.376				.256			.422		.313				7
8	.038	.081		-.417		-.416					.621		.415						8
9		-.375		-.404															9
10	-.345	-.322								.512	.666								10
11	-.363	-.298								.517	.595								11
12	-.242	-.276																	12
								α = 03°		δ = 00°									
1	.340	.190	.237	.195	.268	.345	-.012			.132	.139	.145	.157	.129	.140	.268			1
2	-.008	-.068	-.122	-.185	-.211	-.258	-.022			.077		.081	.067	.088	.100	.207			2
3	-.022	-.047	-.045	-.076	-.097	-.118	-.012			.080	.052	.049	.068	.023	.117	-.072			3
4	-.011	-.046	-.069	-.088	-.089	-.032	-.211			.052	.048	.039		.149	.287	-.174			4
5	-.031	-.047	-.072	-.103	-.067	.037	-.363			.067	.016	.077	.158		-.056				5
6	-.031	-.060	-.056	-.017						.056	.113		-.162		-.318				6
7	-.030	-.041		-.080		-.370				.075			-.281		-.169				7
8	-.017	-.056		-.339		-.204					-.118		-.090						8
9		-.148		-.138															9
10	-.153	-.161								-.160	-.112								10
11	-.158	-.160								-.120	-.091								11
12	-.144	-.159																	12

[redacted]

Table 23 Continued

Pressure Coefficients on Delta Wing with Control

Configuration J3 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
								α = 06°			δ = 00°									
1	.314	.118	.159	.103	.113	.210	-.269													1
2	-.076	-.235	-.323	-.362	-.372	-.387	-.169				.199	.226	.233	.240	.216	.224	.304			2
3	-.059	-.095	-.106	-.133	-.296	-.345	-.180				.133		.161	.138	.152	.182	.190			3
4	-.039	-.091	-.116	-.145	-.103	-.221	-.348				.148	.115	.113	.243	.097	.355	-.049			4
5	-.077	-.088	-.118	-.099	-.106	-.181	-.396				.115	.104	.100		.342	.331	-.129			5
6	-.065	-.098	-.093	-.099							.117	.068	.136	.187		.018				6
7	-.062	-.077		-.124		-.367					.100	.169		-.209		-.305				7
8	-.017	-.063		-.310		-.243					.110			-.207		-.139				8
9		-.156		-.142								-.117		-.067						9
10	-.157	-.162										-.099								10
11	-.170	-.170									-.139	-.064								11
12	-.158	-.162									-.093									12
								α = 06°			δ = 10°									
1	.313	.117	.157	.103	.115	.210	-.313													1
2	-.079	-.242	-.327	-.366	-.371	-.394	-.243				.201	.223	.233	.240	.211	.224	.338			2
3	-.058	-.095	-.108	-.140	-.293	-.343	-.269				.134		.161	.133	.147	.183	.332			3
4	-.041	-.092	-.117	-.146	-.104	-.261	-.395				.147	.113	.112	.223	.094	.358	.076			4
5	-.077	-.089	-.120	-.100	-.105	-.212	-.417				.112	.103	.098		.354	.277	.077			5
6	-.067	-.099	-.093	-.120							.119	.065	.137	.067		-.026				6
7	-.063	-.078		-.011		-.381					.098	.167		-.144		.018				7
8	-.024	-.059		-.358		-.325					.124			.149		.131				8
9		-.273		-.280										.194						9
10	-.252	-.274										.144								10
11	-.295	-.294									.150	.228								11
12	-.207	-.186									.195	.247								12
								α = 06°			δ = 20°									
1	.312	.118	.157	.102	.116	.215	-.285													1
2	-.078	-.240	-.327	-.362	-.370	-.392	-.292				.200	.223	.233	.239	.208	.225	.666			2
3	-.059	-.095	-.108	-.141	-.293	-.339	-.336				.133		.159	.132	.146	.777	.511			3
4	-.041	-.091	-.114	.018	-.103	-.234	-.433				.149	.109	.112	.075	.090	.027	.302			4
5	-.078	-.089	-.117	-.095	-.105	-.100	-.429				.109	.104	.096		-.015	.268	.519			5
6	-.068	-.097	-.089	.163							.121	.066	.500	.242		.335				6
7	-.064	-.071		.087		-.391					.100	.502		.317		.420				7
8	-.011	.019		-.400		-.411					.420			.556		.401				8
9		-.367		-.387										.468						9
10	-.314	-.350										.629								10
11	-.343	-.290									.625	.692								11
12	-.249	-.256									.584	.624								12
								α = 06°			δ = 30°									
1	.312	.116	.156	.101	.117	.215	.060													1
2	-.079	-.243	-.329	-.366	-.371	-.391	-.392				.199	.222	.232	.236	.208	.511	1.080			2
3	-.059	-.099	-.108	-.141	-.294	-.312	-.382				.132		.157	.134	.146	.950	.460			3
4	-.041	-.093	-.116	-.106	-.100	-.259	-.460				.149	.106	.109	.467	.594	.595	.567			4
5	-.077	-.090	-.118	-.096	-.105	-.187	-.446				.106	.101	.506		.455	1.193	.596			5
6	-.070	-.100	-.087	.049							.118	.521	.571	.793		.389				6
7	-.064	-.069		.085		-.417					.482	.569		.532		.660				7
8	-.015	.023		-.422		-.441					.556			.671		.566				8
9		-.353		-.413										.566						9
10	-.359	-.345										.681								10
11	-.349	-.326									.782	.855								11
12	-.308	-.306									.744	.805								12
								α = 09°			δ = 00°									
1	.273	.047	.064	.014	-.064	-.020	-.345													1
2	-.166	-.344	-.400	-.425	-.434	-.429	-.296				.273	.301	.309	.320	.296	.306	.216			2
3	-.095	-.144	-.233	-.344	-.394	-.425	-.290				.191		.233	.208	.224	.255	.169			3
4	-.079	-.136	-.147	-.215	-.366	-.343	-.430				.203	.178	.180	.425	.171	.614	-.004			4
5	-.117	-.133	-.155	-.092	-.237	-.302	-.436				.170	.165	.164		.519	.225	-.047			5
6	-.105	-.144	-.132	-.149							.175	.125	.195	.218		.037				6
7	-.103	-.123		-.187		-.383					.143	.228		-.304		-.173				7
8	-.043	-.079		-.362		-.341					.132			-.035		-.054				8
9		-.216		-.201										.014						9
10	-.198	-.214										-.054								10
11	-.220	-.234									-.081	-.020								11
12	-.211	-.227									-.026	.029								12

[redacted]

Table 23 Continued

Pressure Coefficients on Delta Wing with Control

Configuration J3 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
								α = 12°			δ = 00°									
1	.239	-.025	-.049	-.093	-.199	-.205	-.378				.351	.382	.391	.394	.368	.372	.280			1
2	-.292	-.436	-.470	-.488	-.495	-.472	-.372				.264		.304	.285	.306	.334	.113			2
3	-.131	-.220	-.341	-.437	-.463	-.465	-.366				.256	.253	.254	.465	.253	.603	-.010			3
4	-.125	-.199	-.252	-.316	-.445	-.423	-.445				.241	.237	.237		.593	.489	-.018			4
5	-.152	-.193	-.227	-.092	-.302	-.387	-.447				.243	.191	.264	.305		.060				5
6	-.142	-.181	-.167	-.234							.198	.294		-.215		-.215				6
7	-.137	-.147		-.359		-.401					.175			-.018		-.052				7
8	-.078	-.082		-.306		-.383								.031						8
9		-.214		-.267								-.044								9
10	-.199	-.212									-.059	-.008								10
11	-.223	-.229									.001	.068								11
12	-.214	-.218																		12
								α = 12°			δ = 10°									
1	.239	-.029	-.050	-.093	-.202	-.204	-.410				.349	.381	.390	.391	.364	.368	.255			1
2	-.294	-.444	-.477	-.496	-.500	-.485	-.392				.264		.301	.281	.300	.736	.450			2
3	-.132	-.223	-.341	-.445	-.465	-.480	-.399				.255	.251	.252	.232	.246	.306	.178			3
4	-.124	-.200	-.253	-.318	-.446	-.411	-.456				.242	.235	.233		.367	.223	.290			4
5	-.155	-.196	-.227	-.089	-.321	-.389	-.441				.243	.189	.319	.226		.146				5
6	-.144	-.182	-.168	-.277							.196	.292		-.031		.192				6
7	-.138	-.148		-.313		-.420					.200			.290		.272				7
8	-.090	-.077		-.351		-.391								.335						8
9		-.316		-.346								.326								9
10	-.286	-.315									.337	.401								10
11	-.327	-.334									.388	.404								11
12	-.218	-.239																		12
								α = 12°			δ = 20°									
1	.239	-.027	-.048	-.092	-.197	-.202	.095				.351	.380	.391	.391	.363	.367	.990			1
2	-.292	-.444	-.474	-.490	-.472	-.363	-.424				.263		.302	.279	.298	.911	.496			2
3	-.130	-.220	-.339	-.425	-.452	-.351	-.432				.255	.252	.253	.622	.532	.248	.517			3
4	-.123	-.200	-.247	-.198	-.382	-.341	-.464				.242	.236	.233		.298	1.007	.570			4
5	-.153	-.192	-.228	-.087	-.263	-.350	-.439				.244	.203	.740	.759		.547				5
6	-.142	-.181	-.152	-.231							.226	.705		.591		.641				6
7	-.136	-.146		-.318		-.441					.676			.770		.582				7
8	-.083	.014		-.392		-.389								.652						8
9		-.405		-.367								.850								9
10	-.346	-.391									.798	.879								10
11	-.383	-.340									.700	.760								11
12	-.316	-.314																		12
								α = 12°			δ = 30°									
1	.239	-.026	-.049	-.093	-.196	-.278	.046				.350	.380	.390	.390	.362	.876	.967			1
2	-.292	-.445	-.476	-.493	-.485	-.450	-.451				.263		.301	.400	.359	1.001	.666			2
3	-.131	-.219	-.339	-.434	-.461	-.446	-.449				.255	.251	.252	.746	.875	.739	.797			3
4	-.123	-.198	-.248	-.165	-.433	-.427	-.473				.241	.236	.716		.726	1.149	.707			4
5	-.153	-.193	-.222	-.084	-.173	-.383	-.450				.244	.719	.801	1.022		.853				5
6	-.143	-.180	-.161	-.125							.677	.786		.788		.836				6
7	-.135	-.145		-.261		-.453					.772			.847		.669				7
8	-.083	.011		-.406		-.409								.712						8
9		-.373		-.402								.910								9
10	-.384	-.370									.880	1.023								10
11	-.379	-.350									.785	.901								11
12	-.341	-.339																		12
								α = 15°			δ = 00°									
1	.197	-.097	-.187	-.191	-.314	-.319	-.408				.429	.458	.452	.466	.453	.472	.242			1
2	-.400	-.460	-.445	-.439	-.457	-.366	-.353				.334		.394	.403	.423	.705	.141			2
3	-.163	-.374	-.420	-.428	-.444	-.352	-.408				.321	.336	.372	.498	.368	.560	.083			3
4	-.157	-.334	-.420	-.345	-.444	-.313	-.437				.318	.355	.368		.636	.195	.168			4
5	-.183	-.165	-.424	-.083	-.300	-.294	-.399				.351	.309	.386	.352		.086				5
6	-.174	-.195	-.379	-.229							.305	.416		-.281		.046				6
7	-.169	-.175		-.405		-.443					.269			.108		.119				7
8	-.106	-.073		-.441		-.355								.178						8
9		-.264		-.367								.097								9
10	-.245	-.267									.062	.204								10
11	-.277	-.290									.141	.199								11
12	-.191	-.175																		12

[redacted]

Table 23 Continued

Pressure Coefficients on Delta Wing with Control

Configuration J3 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
								$\alpha = -03^\circ$			$\delta = 00^\circ$									
1	.313	.305	.228	.252	.292	.316	-.026				-.003	-.058	-.113	-.136	-.194	-.238	.047			1
2	.115	.112	.130	.138	.136	.137	.316				-.019		-.059	-.079	-.088	-.134	-.009			2
3	.064	.066	.091	.059	.070	.096	.247				-.019	-.031	-.071	-.040	-.117	-.066	-.163			3
4	.068	.044	.051	.028	.040	.111	-.154				-.042	-.052	-.075		-.018	.073	-.280			4
5	.071	.049	.024	-.080	.072	.261	-.222				-.028	-.076	-.024	.034		-.285				5
6	.056	.029	.036	.096							-.032	.013		-.124		-.323				6
7	.043	.046		-.117		-.387					.017			-.282		-.183				7
8	.009	-.035		-.314		-.198								-.124						8
9		-.129		-.137								-.134								9
10	-.134	-.149									-.181	-.126								10
11	-.146	-.149									-.135	-.114								11
12	-.125	-.140																		12
								$\alpha = -06^\circ$			$\delta = 00^\circ$									
1	.277	.278	.131	.140	.204	.165	-.154				-.076	-.258	-.315	-.345	-.358	-.385	-.159			1
2	.184	.193	.217	.224	.222	.221	.329				-.058		-.113	-.149	-.294	-.338	-.269			2
3	.124	.135	.159	.132	.129	.165	.281				-.063	-.080	-.113	-.079	-.151	-.251	-.390			3
4	.124	.099	.113	.349	.112	.542	-.034				-.081	-.093	-.123		-.095	-.129	-.405			4
5	.123	.104	.083	-.082	.387	.375	-.068				-.067	-.114	-.061	-.141		-.377				5
6	.108	.082	.089	.047							-.066	-.029		-.102		-.361				6
7	.093	.093		-.281		-.146					.008			-.396		-.276				7
8	.046	-.018		-.070		-.051								-.222						8
9		-.022		-.007								-.218								9
10	-.040	-.042									-.250	-.231								10
11	-.056	-.021									-.219	-.196								11
12	-.015	.002																		12
								$\alpha = -06^\circ$			$\delta = 10^\circ$									
1	.276	.278	.131	.138	.203	.161	-.120				-.076	-.261	-.315	-.350	-.358	-.387	-.099			1
2	.183	.195	.220	.228	.223	.223	.330				-.058		-.113	-.149	-.294	-.346	-.109			2
3	.126	.137	.162	.137	.134	.168	.187				-.064	-.081	-.113	.081	-.152	-.105	-.255			3
4	.124	.100	.116	.095	.117	.213	-.171				-.081	-.093	-.124		.125	-.026	-.371			4
5	.124	.104	.087	-.079	.138	.428	-.223				-.068	-.113	-.065	-.005		-.400				5
6	.109	.085	.093	.283							-.068	-.030		-.247		-.319				6
7	.095	.096		-.017		-.324					.021			-.079		-.166				7
8	.046	-.020		-.331		-.272								-.038						8
9		-.213		-.222								-.036								9
10	-.179	-.215									-.091	-.010								10
11	-.222	-.234									-.032	.017								11
12	-.211	-.225																		12
								$\alpha = -06^\circ$			$\delta = 20^\circ$									
1	.277	.278	.127	.136	.199	.157	-.056				-.078	-.264	-.317	-.351	-.363	-.384	-.042			1
2	.185	.196	.220	.226	.226	.225	.187				-.058		-.117	-.152	-.297	-.345	.063			2
3	.126	.138	.162	.138	.136	.170	.162				-.064	-.083	-.116	-.127	-.155	-.112	-.077			3
4	.123	.101	.114	.197	.120	.263	-.219				-.081	-.094	-.126		-.087	-.038	-.196			4
5	.124	.103	.089	.149	.338	.308	-.314				-.069	-.115	.126	-.046		-.249				5
6	.108	.085	.098	.094							-.067	.172		-.059		-.092				6
7	.095	.100		.043		-.346					.163			.198		-.002				7
8	.079	.087		-.383		-.356								.155						8
9		-.315		-.327								.283								9
10	-.273	-.318									.241	.354								10
11	-.323	-.281									.294	.346								11
12	-.220	-.196																		12
								$\alpha = -06^\circ$			$\delta = 30^\circ$									
1	.274	.276	.126	.131	.195	.187	.210				-.081	-.265	-.321	-.353	-.309	-.050	.245			1
2	.187	.198	.221	.228	.229	.231	.024				-.059		-.116	-.076	-.103	-.030	.408			2
3	.128	.139	.165	.140	.138	.175	.131				-.065	-.083	-.117	.063	-.047	.133	.134			3
4	.124	.103	.116	.099	.124	.228	-.296				-.083	-.096	.015		.022	.178	.134			4
5	.123	.105	.091	.230	.147	.112	-.381				-.069	.145	.314	.116		.026				5
6	.108	.089	.100	-.059							.064	.303		.112		.155				6
7	.100	.108		.051		-.349					.286			.306		.144				7
8	.110	.132		-.404		-.404								.316						8
9		-.391		-.391								.443								9
10	-.334	-.346									.603	.561								10
11	-.367	-.301									.588	.537								11
12	-.276	-.265																		12

[redacted]

Table 23 Continued

Pressure Coefficients on Delta Wing with Control

Configuration J3 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	$\alpha = -09^\circ$									$\delta = 00^\circ$									
1	.243	.215	.032	.011	.080	.027	-.226			-.139	-.350	-.404	-.413	-.431	-.451	-.252			1
2	.256	.263	.293	.291	.296	.289	.263			-.095		-.200	-.321	-.385	-.427	-.295			2
3	.182	.187	.233	.204	.204	.216	.255			-.099	-.128	-.144	-.172	-.338	-.318	-.401			3
4	.183	.158	.176	.395	.185	.513	-.001			-.114	-.139	-.159		-.173	-.253	-.386			4
5	.173	.161	.141	.227	.438	.317	-.043			-.103	-.139	-.089	-.192		-.429				5
6	.162	.138	.144	.058						-.098	-.093		-.174		-.351				6
7	.145	.145		-.290		-.165				-.007			-.372		-.305				7
8	.060	-.012		-.051		-.016							-.205						8
9		-.005		.016															9
10	-.026	-.031									-.211								10
11	-.030	-.009								-.255	-.224								11
12	.007	.029								-.232	-.215								12
	$\alpha = -12^\circ$									$\delta = 00^\circ$									
1	.178	.104	-.075	-.161	-.081	-.148	-.243			-.287	-.387	-.444	-.447	-.452	-.357	-.269			1
2	.335	.356	.382	.368	.362	.351	.219			-.135		-.307	-.355	-.413	-.324	-.353			2
3	.258	.267	.303	.291	.293	.309	.252			-.138	-.162	-.298	-.152	-.363	-.290	-.443			3
4	.263	.237	.256	.411	.269	.476	.044			-.151	-.153	-.281		-.208	-.269	-.413			4
5	.241	.235	.217	.229	.458	.279	.092			-.141	-.167	-.198	-.148		-.378				5
6	.241	.215	.220	.251						-.130	-.113		-.349		-.389				6
7	.212	.211		-.283		-.055				-.030			-.402		-.337				7
8	.105	.009		.045		.073							-.293						8
9		.080		.114															9
10	.067	.060									-.261								10
11	.056	.110								-.292	-.277								11
12	.102	.143								-.241	-.170								12
	$\alpha = -12^\circ$									$\delta = 10^\circ$									
1	.178	.102	-.077	-.165	-.086	-.149	-.187			-.290	-.392	-.451	-.457	-.472	-.445	-.288			1
2	.335	.356	.383	.370	.363	.357	.317			-.136		-.312	-.330	-.430	-.408	-.358			2
3	.257	.268	.305	.292	.293	.312	.118			-.138	-.163	-.300	-.174	-.383	-.362	-.438			3
4	.263	.240	.257	.530	.268	.653	-.075			-.153	-.154	-.282		-.250	-.313	-.420			4
5	.244	.236	.218	.228	.593	.555	-.078			-.139	-.167	-.208	-.138		-.417				5
6	.242	.218	.220	.260						-.131	-.115		-.353		-.386				6
7	.212	.215		-.128		-.237				-.019			-.285		-.314				7
8	.101	.013		-.175		-.144							-.251						8
9		-.108		-.098															9
10	-.095	-.115									-.157								10
11	-.132	-.113								-.186	-.148								11
12	-.103	-.092								-.146	-.096								12
	$\alpha = -12^\circ$									$\delta = 20^\circ$									
1	.177	.102	-.079	-.166	-.088	-.154	-.153			-.292	-.397	-.452	-.462	-.465	-.397	-.258			1
2	.336	.350	.383	.372	.367	.356	.132			-.136		-.312	-.347	-.425	-.370	-.289			2
3	.260	.269	.308	.294	.296	.313	.050			-.139	-.167	-.300	-.188	-.383	-.311	-.362			3
4	.264	.241	.259	.583	.273	.693	-.202			-.153	-.155	-.286		-.288	-.309	-.401			4
5	.245	.237	.221	.229	.656	.312	-.231			-.140	-.169	-.192	-.159		-.354				5
6	.240	.222	.224	.097						-.129	.021		-.308		-.304				6
7	.215	.220		-.024		-.310				.091			-.133		-.252				7
8	.115	.093		-.328		-.293							-.136						8
9		-.256		-.274															9
10	-.220	-.259									.122								10
11	-.266	-.270								.047	.212								11
12	-.254	-.187								.149	.237								12
	$\alpha = -12^\circ$									$\delta = 30^\circ$									
1	.177	.101	-.077	-.165	-.085	-.147	-.224			-.294	-.395	-.437	-.419	-.327	-.245	-.170			1
2	.339	.360	.386	.375	.372	.360	-.055			-.136		-.336	-.313	-.305	-.261	-.048			2
3	.262	.269	.312	.298	.300	.315	.058			-.137	-.166	-.313	-.145	-.270	-.142	-.116			3
4	.265	.244	.261	.411	.278	.666	-.241			-.151	-.151	-.275		-.179	-.170	-.212			4
5	.246	.240	.227	.294	.576	.060	-.319			-.138	-.148	.099	-.121		-.130				5
6	.241	.226	.230	-.044						-.117	.213		-.180		-.148				6
7	.219	.230		-.002		-.329				.220			-.078		-.136				7
8	.182	.194		-.373		-.376							-.066						8
9		-.349		-.363															9
10	-.318	-.322									.391								10
11	-.345	-.294								.419	.563								11
12	-.234	-.246								.418	.539								12

[redacted]

Table 23 Concluded

Pressure Coefficients on Delta Wing with Control

Configuration J3 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
	$\alpha = -15^\circ$										$\delta = 00^\circ$									
1	.127	.003	-.153	-.289	-.179	-.251	-.265				-.386	-.425	-.439	-.432	-.433	-.353	-.307			1
2	.413	.415	.429	.415	.428	.416	.170				-.164		-.407	-.420	-.437	-.343	-.378			2
3	.317	.332	.374	.384	.384	.707	.221				-.166	-.286	-.415	-.293	-.428	-.317	-.418			3
4	.331	.300	.355	.421	.376	.451	.043				-.182	-.165	-.415		-.301	-.297	-.381			4
5	.306	.327	.317	.293	.468	.264	.162				-.168	-.188	-.338	-.204		-.386				5
6	.322	.323	.351	.408							-.151	-.144		-.426		-.398				6
7	.304	.308		-.320		-.032					-.052			-.416		-.338				7
8	.166	.058		.075		.121								-.342						8
9		.122		.165								-.251								9
10	.099	.097									-.295	-.265								10
11	.099	.180									-.251	-.153								11
12	.146	.169																		12

[redacted]

Table 24

Pressure Coefficients on Delta Wing with Control

Configuration J4 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	$\alpha = 0^\circ$									$\delta = -30^\circ$									
1	.379	.365	.279	.258	.300	.349	.150			.078		.047		.023	.028	-.429			1
2	.050	.033	.018	.013	.000	.142	1.016			.039	.028	.013		.016	.013	-.457			2
3	.015	.007		.065	.000	.330	.895			.044		.002	.017	-.023	.057	-.461			3
4	.023	-.007	.325	.043	.419	.630	.579			.004	.015	-.018		.041	-.147	-.450			4
5	-.002	.007	.338	.080	.182	.986	.627			.023	.005	.048	-.378		-.416				5
6	.143	.410	.154	.055						.008	.022		-.333		-.363				6
7	.396	.148		.197		.671				.060			-.342		-.378				7
8	.136	.127		.510		.625							-.351						8
9		.149		.634							-.372								9
10	.166	.159									-.378								10
11	.248	.306								-.246	-.345								11
12	.247	.331								-.285									12
	$\alpha = 0^\circ$									$\delta = -20^\circ$									
1	.383	.361	.280	.262	.302	.352	.186			.074		.042		.023	.021	-.346			1
2	.050	.029	.018	.018	.000	.105	1.005			.041	.015	.008		.011	.011	-.451			2
3	.013	.008		.063	.001	.201	.669			.037		.000	-.002	.032	.057	-.460			3
4	.023	-.005	.310	-.168	.404	.397	.147			.002	.010	-.025		.031	-.119	-.464			4
5	-.001	.004	.342	-.011	-.049	.895	.348			.025	.002	.037	-.400		-.424				5
6	.118	.408	-.123	-.158						.006	.008		-.408		-.417				6
7	.391	-.110		-.008		.321				.002			-.294		-.327				7
8	-.128	.051		.221		.294							-.283						8
9		-.109		.342							-.425								9
10	-.057	-.043									-.354								10
11	.085	.089								-.176	-.253								11
12	.108	.113								-.220									12
	$\alpha = 0^\circ$									$\delta = -10^\circ$									
1	.379	.369	.289	.265	.302	.350	.145			.071		.048		.018	.022	-.218			1
2	.052	.033	.025	.022	.002	.141	.759			.035	-.010	.010		.010	.011	-.190			2
3	.017	.011		.053	.006	.206	.427			.035		.000	-.007	-.032	.050	-.397			3
4	.025	-.001	.198	-.329	.395	.158	.048			.001	.014	-.023		.020	-.058	-.407			4
5	-.002	.012	.341	-.124	-.153	.548	.039			.018	-.002	.032	-.302		-.325				5
6	.154	.400	-.314	-.287						.004	.003		-.302		-.341				6
7	.388	-.300		-.133		.037				-.003			-.301		-.339				7
8	-.311	.010		.022		.003							-.303						8
9		-.271		.094							-.313								9
10	-.189	-.163									-.316								10
11	-.062	-.071								-.072	-.167								11
12	-.046	-.037								-.195									12
	$\alpha = 0^\circ$									$\delta = 0^\circ$									
1	.383	.371	.282	.268	.304	.352	.098			.087		.046		.024	.022	-.013			1
2	.054	.036	.023	.019	.005	.107	.256			.042	-.074	.012		.018	.010	.022			2
3	.018	.011		.073	.020	.199	.187			.044		.001	-.003	.026	.037	-.138			3
4	.029	-.003	.143	-.409	.384	.157	-.064			.010	.018	-.022		.022	.064	-.289			4
5	.005	.005	.338	-.205	-.209	.164	-.169			.024	.003	.033	-.142		-.196				5
6	.152	.402	-.396	-.343						.014	.007		-.141		-.201				6
7	.396	-.382		-.222		-.182				.011			-.138		-.198				7
8	-.392	.000		-.160		-.212							-.144						8
9		-.324		-.131							-.164								9
10	-.257	-.249									-.146								10
11	-.130	-.203								-.111	-.129								11
12	-.124	-.154								-.142									12
	$\alpha = 0^\circ$									$\delta = 10^\circ$									
1	.385	.362	.279	.264	.307	.347	.102			.068		.039		.008	.016	.340			1
2	.050	.035	.029	.018	.001	.070	-.038			.028	.011	.003		.004	.000	.284			2
3	.014	.011		.070	.008	.211	-.048			.028		-.014	-.020	-.038	.032	.022			3
4	.013	-.002	.191	-.443	.370	.161	-.222			-.001	.012	-.033		.015	.251	-.074			4
5	.004	-.003	.346	-.220	-.218	-.082	-.360			.013	-.002	.019	.098		.051				5
6	.043	.402	-.435	-.387						.022	-.002		.109		.030				6
7	.417	-.412		-.335		-.328				-.002			.122		.014				7
8	-.411	-.027		-.326		-.338							.123						8
9		-.350		-.307							.120								9
10	-.301	-.326									.115								10
11	-.137	-.262								.085	.118								11
12	-.237	-.176								.115									12

[redacted]

Table 24 Continued

Pressure Coefficients on Delta Wing with Control

Configuration J4 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 00°									δ = 20°									
1	.387	.361	.283	.263	.306	.352	.232			.067		.036		.002	.008	.627			1
2	.057	.034	.025	.023	.002	.076	-.243			.028	.011	.004		-.002	-.008	.503			2
3	.020	.013		.061	.003	.216	-.183			.032		-.015	.252	-.042	.082	.119			3
4	.022	.000	.188	-.447	.385	.185	-.407			-.004	.006	-.032		.138	.532	.213			4
5	.005	.003	.345	.015	-.216	-.255	-.412			.011	-.010	.292	.324		.377				5
6	.041	.407	-.438	-.400						.019	.304		.554		.398				6
7	.424	-.411		-.383		-.412				.225			.595		.374				7
8	-.406	.055		-.388		-.272							.521						8
9		-.395		-.349							.506								9
10	-.320	-.344								.450	.555								10
11	-.196	-.264								.458	.511								11
12	-.258	-.226																	12
	α = 00°									δ = 30°									
1	.383	.365	.282	.265	.309	.351	.423			.073		.032		.004	.001	.886			1
2	.050	.039	.026	.025	.015	.076	-.340			.035	.014	.007		.001	.359	.797			2
3	.016	.013		.057	.002	.224	-.418			.044		-.016	.423	.374	.635	.614			3
4	.027	.002	.185	-.440	.385	.201	-.439			-.005	.007	.327		.436	.599	.630			4
5	.010	.001	.346	.131	-.218	-.349	-.429			.012	.361	.382	.426		.825				5
6	.039	.402	-.437	-.370						.302	.425		.618		.755				6
7	.423	-.414		-.373		-.352				.408			.755		.646				7
8	-.396	.109		-.382		-.319							.682						8
9		-.409		-.356							.465								9
10	-.327	-.338								.679	.617								10
11	-.229	-.297								.649	.606								11
12	-.286	-.266																	12
	α = 06°									δ = -30°									
1	.320	.083	.131	-.028	.081	.208	.213			.211		.253		.226	.253	-.381			1
2	-.097	-.280	-.341	-.388	-.385	.052	.291			.152	.160	.169		.176	.202	-.339			2
3	-.079	-.092		-.075	-.151	.053	.498			.151		.128	.138	.113	.222	-.429			3
4	-.065	-.108	.003	-.050	-.027	.084	.134			.115	.130	.106		.204	-.137	-.327			4
5	-.099	-.105	.284	.137	.121	.101	.237			.129	.111	.154	-.380		-.415				5
6	-.058	.305	.052	-.025						.103	.120		-.337		-.361				6
7	.244	.028		.096		.214				.094			-.333		-.372				7
8	.037	.126		.347		.175							-.338						8
9		.054		.453							-.363								9
10	.084	.087								-.280	-.362								10
11	.196	.257								-.254	-.327								11
12	.215	.308																	12
	α = 06°									δ = -20°									
1	.329	.091	.139	-.016	.087	.186	.106			.207		.249		.226	.251	-.265			1
2	-.093	-.275	-.336	-.382	-.387	-.043	.140			.151	.176	.161		.176	.197	-.166			2
3	-.075	-.087		-.096	-.210	-.080	.194			.154		.125	.127	.112	.216	-.336			3
4	-.054	-.094	-.008	-.229	.086	-.048	-.031			.111	.125	.105		.189	-.100	-.300			4
5	-.092	-.098	.296	.019	-.126	-.018	-.077			.128	.110	.149	-.361		-.380				5
6	-.062	.307	-.193	-.217						.107	.120		-.366		-.389				6
7	.253	-.195		-.096		.012				.070			-.370		-.397				7
8	-.215	.061		.074		-.011							-.325						8
9		-.178		.168							-.393								9
10	-.112	-.100								-.221	-.393								10
11	.042	.041								-.216	-.213								11
12	.068	.078																	12
	α = 06°									δ = -10°									
1	.327	.096	.138	-.011	.094	.189	.003			.207		.246		.217	.239	-.085			1
2	-.085	-.266	-.333	-.376	-.377	-.060	-.039			.146	.158	.157		.162	.190	.025			2
3	-.068	-.083		-.093	-.222	-.119	-.029			.149		.122	.120	.097	.201	-.138			3
4	-.056	-.095	-.010	-.356	.137	-.139	-.220			.101	.120	.092		.177	-.015	-.212			4
5	-.089	-.091	.302	-.077	-.209	-.129	-.310			.120	.101	.139	-.249		-.267				5
6	-.063	.308	-.338	-.333						.093	.103		-.252		-.273				6
7	.271	-.343		-.210		-.185				.056			-.252		-.277				7
8	-.345	.034		-.096		-.201							-.261						8
9		-.315		-.034							-.281								9
10	-.233	-.212								-.058	-.277								10
11	-.086	-.127								-.183	-.252								11
12	-.068	-.083																	12

[redacted]

Table 24 Continued

Pressure Coefficients on Delta Wing with Control

Configuration J4 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 06°									δ = 00°									
1	.329	.092	.138	-.010	.094	.191	-.047												1
2	-.092	-.274	-.339	-.370	-.382	-.078	-.197			.219		.247		.234	.248	.235			2
3	-.075	-.083		-.090	-.240	-.127	-.339			.159	.160	.161		.168	.194	.239			3
4	-.056	-.094	-.013	-.428	.157	-.194	-.393			.160		.126	.129	.113	.212	.000			4
5	-.088	-.095	.293	-.174	-.262	-.186	-.394			.112	.131	.100		.187	.183	-.038			5
6	-.076	.310	-.419	-.366						.132	.115	.148	-.023		-.042				6
7	.272	-.417		-.280		-.309				.106	.113		-.024		-.056				7
8	-.406	.022		-.226		-.320				.060			-.028		-.062				8
9		-.360		-.157									-.037						9
10	-.263	-.301									-.061								10
11	-.142	-.243								-.014	-.051								11
12	-.156	-.158								-.060	-.036								12
	α = 06°									δ = 10°									
1	.326	.094	.143	-.007	.104	.193	-.037												1
2	-.090	-.265	-.330	-.373	-.382	-.122	-.308			.205		.238		.222	.240	.686			2
3	-.069	-.094		-.094	-.277	-.118	-.438			.143	.152	.154		.158	.186	.457			3
4	-.058	-.095	.063	-.461	.264	-.208	-.448			.144		.123	.121	.105	.207	.082			4
5	-.088	-.098	.299	-.147	-.270	-.276	-.442			.107	.130	.095		.177	.461	.173			5
6	-.077	.328	-.443	-.412						.129	.107	.138	.268		.238				6
7	.284	-.438		-.364		-.384				.119	.104		.277		.233				7
8	-.409	.012		-.293		-.314				.079			.291		.213				8
9		-.374		-.199									.292						9
10	-.299	-.325									.257								10
11	-.164	-.253								.218	.251								11
12	-.240	-.210								.252	.252								12
	α = 06°									δ = 20°									
1	.327	.098	.141	-.011	.102	.200	.162												1
2	-.085	-.267	-.328	-.368	-.379	-.129	-.344			.212		.241		.217	.241	1.195			2
3	-.068	-.084		-.091	-.266	-.115	-.442			.142	.162	.151		.161	.187	.599			3
4	-.059	-.093	.061	-.451	.257	-.196	-.456			.150		.117	.526	.098	.646	.511			4
5	-.079	-.096	.311	.282	-.266	-.362	-.422			.105	.119	.091		.526	.786	.559			5
6	-.079	.317	-.430	-.411						.121	.100	.515	.538		.738				6
7	.280	-.420		-.375		-.335				.123	.496		.724		.670				7
8	-.400	.127		-.326		-.315				.424			.768		.593				8
9		-.388		-.270									.660						9
10	-.322	-.337									.658								10
11	-.235	-.286								.666	.714								11
12	-.284	-.260								.619	.635								12
	α = 06°									δ = 30°									
1	.334	.101	.149	-.002	.111	.212	.171												1
2	-.082	-.256	-.324	-.366	-.371	-.125	-.425			.215		.241		.222	.348	1.265			2
3	-.065	-.079		-.078	-.269	-.098	-.456			.149	.155	.151		.165	.639	.978			3
4	-.051	-.087	.069	-.455	.267	-.154	-.466			.150		.117	.627	.592	.706	.862			4
5	-.082	-.093	.314	.287	-.256	-.400	-.411			.107	.117	.507		.651	.618	.744			5
6	-.075	.329	-.434	-.406						.124	.526	.590	.635		1.078				6
7	.294	-.427		-.395		-.357				.498	.581		.873		1.012				7
8	-.411	.164		-.379		-.356				.564			1.005		.805				8
9		-.404		-.352									.856						9
10	-.345	-.356									.620								10
11	-.249	-.328								.805	.737								11
12	-.301	-.305								.750	.701								12
	α = 12°									δ = -30°									
1	.192	-.123	-.036	-.199	-.176	.025	.061												1
2	-.311	-.441	-.459	-.369	-.290	.035	.072			.346		.401		.372	.397	-.346			2
3	-.142	-.199		-.256	-.210	-.060	.177			.285	.288	.303		.323	.353	-.222			3
4	-.125	-.194	-.270	-.172	-.224	-.127	.002			.291		.268	.269	.255	.355	-.369			4
5	-.165	-.167	-.046	.129	-.176	-.100	-.031			.243	.255	.239		.357	-.130	-.414			5
6	-.150	.200	-.211	-.155						.251	.238	.273	-.414		-.399				6
7	.183	-.176		-.143		-.077				.191	.232		-.398		-.370				7
8	-.158	.093		-.083		-.072				.133			-.334		-.341				8
9		-.159		-.093									-.326						9
10	-.078	-.095									-.424								10
11	.154	.210								-.319	-.372								11
12	.230	.338								-.298	-.317								12

[redacted]

Table 24 Continued

Pressure Coefficients on Delta Wing with Control

Configuration J4 M = 1.61 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 12°									δ = -20°									
1	.197	-.109	-.028	-.196	-.168	-.031	-.007			.341		.398		.370	.390	-.205			1
2	-.306	-.426	-.450	-.417	-.337	-.059	.035			.277	.290	.298		.318	.345	-.059			2
3	-.132	-.192		-.299	-.267	-.098	-.057			.290		.265	.266	.249	.353	-.189			3
4	-.111	-.188	-.336	-.300	-.274	-.182	.192			.248	.252	.235		.355	-.056	-.324			4
5	-.159	-.194	.056	.073	-.297	-.152	-.256			.254	.236	.267	-.334		-.335				5
6	-.141	.205	-.316	-.277						.185	.229		-.339		-.352				6
7	.200	-.303		-.245		-.197				.124			-.344		-.361				7
8	-.325	.079		-.197		-.170							-.347						8
9		-.301		-.169							-.362								9
10	-.193	-.228									-.364								10
11	-.017	-.050								-.201	-.246								11
12	.016	.026								-.285									12
	α = 12°									δ = -10°									
1	.192	-.123	-.034	-.199	-.176	-.051	-.098			.348		.397		.367	.389	.024			1
2	-.307	-.431	-.465	-.422	-.351	-.096	-.175			.282	.283	.298		.312	.345	.113			2
3	-.136	-.197		-.310	-.283	-.158	-.219			.287		.264	.259	.247	.356	-.071			3
4	-.117	-.192	-.329	-.399	-.304	-.231	-.374			.233	.257	.241		.344	.068	-.147			4
5	-.162	-.199	.048	.008	-.392	-.207	-.397			.245	.233	.266	-.168		-.175				5
6	-.149	.200	-.402	-.372						.183	.220		-.170		-.195				6
7	.192	-.393		-.322		-.263				.127			-.177		-.196				7
8	-.383	.068		-.266		-.227							-.187						8
9		-.382		-.208							-.217								9
10	-.263	-.316									-.214								10
11	-.143	-.212								-.039	-.202								11
12	-.119	-.130								-.147									12
	α = 12°									δ = 00°									
1	.189	-.121	-.039	-.196	-.175	-.051	-.108			.349		.396		.371	.384	.371			1
2	-.308	-.417	-.447	-.408	-.359	-.103	-.291			.282	.220	.295		.313	.341	.317			2
3	-.134	-.196		-.308	-.288	-.182	-.391			.291		.259	.258	.246	.349	.026			3
4	-.114	-.191	-.323	-.455	-.310	-.252	-.405			.241	.248	.235		.343	.266	.071			4
5	-.168	-.194	.053	-.107	-.443	-.248	-.399			.244	.228	.266	.086		.059				5
6	-.149	.206	-.465	-.405						.194	.226		.071		.050				6
7	.197	-.454		-.364		-.299				.134			.065		.050				7
8	-.409	.046		-.316		-.272							.060						8
9		-.407		-.233							.023								9
10	-.308	-.375									.034								10
11	-.191	-.290								.064	.046								11
12	-.209	-.195								.062									12
	α = 12°									δ = 10°									
1	.197	-.107	-.026	-.188	-.163	-.036	.039			.352		.405		.375	.389	.877			1
2	-.299	-.422	-.451	-.412	-.352	-.085	-.350			.282	.297	.302		.314	.342	.482			2
3	-.134	-.189		-.304	-.274	-.168	-.432			.288		.269	.258	.249	.350	.227			3
4	-.118	-.184	-.303	-.443	-.298	-.251	-.433			.244	.249	.226		.348	.623	.395			4
5	-.157	-.190	.091	-.018	-.435	-.355	-.327			.249	.239	.274	.439		.421				5
6	-.144	.217	-.448	-.397						.209	.225		.442		.427				6
7	.205	-.442		-.356		-.298				.147			.461		.386				7
8	-.407	.052		-.326		-.291							.442						8
9		-.404		-.291							.415								9
10	-.304	-.367									.404								10
11	-.201	-.316								.373	.400								11
12	-.263	-.261								.396									12
	α = 12°									δ = 20°									
1	.190	-.115	-.032	-.195	-.170	-.046	.348			.342		.398		.366	.370	1.234			1
2	-.300	-.434	-.465	-.420	-.362	-.093	-.419			.278	.280	.295		.304	.340	.737			2
3	-.144	-.197		-.306	-.288	-.175	-.463			.277		.255	.740	.234	.880	.714			3
4	-.125	-.193	-.310	-.453	-.307	-.249	-.448			.236	.244	.216		.749	.838	.657			4
5	-.166	-.198	.083	.501	-.434	-.401	-.358			.237	.222	.710	.737		.945				5
6	-.145	.206	-.465	-.387						.201	.698		.904		.827				6
7	.209	-.463		-.372		-.333				.631			.897		.699				7
8	-.424	.207		-.370		-.332							.744						8
9		-.427		-.340							.844								9
10	-.348	-.395									.853								10
11	-.261	-.361								.792	.742								11
12	-.302	-.314								.693									12

[redacted]

Table 24 Continued

Pressure Coefficients on Delta Wing with Control

Configuration J4 M = 1.61 R = 4.2 x 10⁶

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 12°									δ = 30°									
1	.202	-.106	-.026	-.189	-.162	-.077	.255			.345		.398		.361	.662	1.162			1
2	-.299	-.433	-.458	-.422	-.356	-.107	-.416			.274	.282	.289		.470	.880	1.024			2
3	-.138	-.191		-.310	-.274	-.170	-.433			.280		.256	.815	.753	.912	.964			3
4	-.110	-.190	-.298	-.448	-.304	-.214	-.407			.243	.251	.755		.838	.781	.810			4
5	-.162	-.195	.088	.500	-.432	-.417	-.371			.242	.723	.785	.806		1.273				5
6	-.142	.216	-.466	-.401						.668	.784		.958		1.121				6
7	.214	-.462		-.384		-.369				.784			1.038		.908				7
8	-.433	.219		-.391		-.365							.885						8
9		-.438		-.374															9
10	-.378	-.410									.910								10
11	-.262	-.389								.927	1.039								11
12	-.323	-.347								.819	.912								12
	α = -06°									δ = -30°									
1	.303	.378	.168	.154	.184	.144	.120			-.058		-.303		-.337	-.369	-.413			1
2	.182	.190	.215	.230	.206	.445	1.209			-.043	-.067	-.110		-.267	-.318	-.402			2
3	.117	.132		.526	.505	.567	1.030			-.047		-.098	-.089	-.148	-.276	-.400			3
4	.116	.097	.486	.155	.522	.625	.810			-.078	-.073	-.119		-.096	-.108	-.269			4
5	.107	.110	.557	.020	.409	.660	.756			-.055	-.080	-.054	-.413		-.396				5
6	.143	.548	.311	.168						-.067	-.058		-.353		-.402				6
7	.524	.275		.424		.880				.003			-.366		-.417				7
8	.274	.158		.644		.794							-.370						8
9		.279		.688															9
10	.316	.311									-.413								10
11	.383	.470								-.286	-.392								11
12	.390	.502								-.316	-.338								12
	α = -06°									δ = -20°									
1	.298	.379	.165	.151	.180	.146	.336			-.064		-.303		-.347	-.366	-.428			1
2	.181	.189	.211	.230	.210	.422	1.222			-.046	-.069	-.108		-.273	-.329	-.434			2
3	.115	.128		.522	.492	.375	.758			-.048		-.100	-.112	-.150	-.291	-.432			3
4	.114	.092	.477	-.081	.497	.517	.424			-.078	-.074	-.120		-.102	-.127	-.309			4
5	.102	.103	.554	-.037	.066	.658	.515			-.056	-.084	-.057	-.432		-.418				5
6	.130	.544	-.009	-.073						-.073	-.070		-.343		-.371				6
7	.515	-.042		.113		.474				-.036			-.320		-.413				7
8	-.043	.094		.357		.468							-.333						8
9		-.033		.421															9
10	.047	.048									-.434								10
11	.203	.200								-.191	-.355								11
12	.221	.241								-.284	-.268								12
	α = -06°									δ = -10°									
1	.302	.386	.169	.147	.183	.150	-.007			-.072		-.310		-.348	-.377	-.459			1
2	.185	.194	.219	.234	.217	.427	.820			-.055	-.087	-.112		-.275	-.329	-.460			2
3	.120	.132		.523	.499	.357	.552			-.057		-.104	-.121	-.158	-.284	-.467			3
4	.123	.103	.481	-.280	.496	.214	.073			-.091	-.082	-.123		-.109	-.115	-.465			4
5	.112	.108	.564	-.162	-.081	.543	.213			-.066	-.089	-.067	-.359		-.427				5
6	.131	.553	-.248	-.245						-.076	-.082		-.357		-.413				6
7	.524	-.257		-.054		.118				-.057			-.359		-.400				7
8	-.271	.032		.108		.128							-.333						8
9		-.240		.178															9
10	-.093	-.120									-.359								10
11	.046	-.006								-.134	-.359								11
12	.064	.029								-.271	-.175								12
	α = -06°									δ = 00°									
1	.311	.387	.174	.159	.195	.155	-.092			-.056		-.288		-.342	-.358	-.396			1
2	.192	.204	.222	.244	.228	.435	.341			-.039	-.068	-.090		-.263	-.317	-.421			2
3	.127	.137		.534	.505	.366	.322			-.039		-.082	-.115	-.136	-.275	-.454			3
4	.123	.105	.486	-.376	.510	.215	-.001			-.069	-.062	-.111		-.095	-.056	-.457			4
5	.115	.114	.564	-.235	-.150	.235	-.020			-.048	-.070	-.046	-.216		-.341				5
6	.124	.553	-.365	-.300						-.062	-.065		-.204		-.321				6
7	.533	-.364		-.140		-.137				-.036			-.199		-.316				7
8	-.342	.026		-.064		-.148							-.199						8
9		-.322		-.037															9
10	-.143	-.225									-.209								10
11	-.079	-.158								-.157	-.193								11
12	-.120	-.125								-.176	-.177								12

[redacted]

Table 24 Continued

Pressure Coefficients on Delta Wing with Control

Configuration J4 M = 1.61 R = 4.2 x 10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = -06°									δ = 10°									
1	.296	.385	.157	.138	.173	.120	-.142			-.078		-.310		-.359	-.391	-.299			1
2	.191	.204	.225	.245	.232	.429	.033			-.054	-.086	-.116		-.292	-.348	-.263			2
3	.127	.139		.538	.509	.360	.096			-.056		-.112	-.135	-.151	-.304	-.308			3
4	.123	.104	.493	-.424	.521	.210	-.105			-.090	-.087	-.130		-.116	.001	-.348			4
5	.111	.111	.575	-.268	-.188	-.035	-.194			-.071	-.090	-.071	-.025		-.259				5
6	.155	.560	-.424	-.365						-.063	-.086		-.014		-.156				6
7	.533	-.419		-.253		-.315				-.054			.005		-.131				7
8	-.381	.003		-.246		-.321							.003						8
9		-.372		-.242							.029								9
10	-.216	-.330								-.018	.042								10
11	-.089	-.277								.012	.037								11
12	-.225	-.178																	12
	α = -06°									δ = 20°									
1	.294	.385	.163	.143	.168	.113	-.121			-.083		-.320		-.372	-.381	-.252			1
2	.191	.204	.228	.245	.235	.436	-.188			-.059	-.092	-.121		-.303	-.371	-.054			2
3	.132	.138		.536	.512	.361	-.071			-.058		-.114	-.042	-.154	-.195	-.101			3
4	.122	.109	.501	-.433	.525	.217	-.228			-.093	-.093	-.136		-.114	.034	-.195			4
5	.112	.109	.580	-.139	-.188	-.191	-.331			-.073	-.098	.059	.144		-.038				5
6	.152	.564	-.435	-.396						-.061	.121		.324		.064				6
7	.538	-.436		-.360		-.396				.108			.354		.083				7
8	-.378	.057		-.360		-.356					.344		.335						8
9		-.405		-.342						.280	.371								9
10	-.292	-.382								.320	.354								10
11	-.152	-.298																	11
12	-.235	-.228																	12
	α = -06°									δ = 30°									
1	.288	.393	.157	.129	.161	.114	.108			-.085		-.318		-.366	-.028	.093			1
2	.187	.196	.224	.235	.230	.430	-.340			-.063	-.092	-.122		-.147	.017	.387			2
3	.129	.134		.546	.510	.363	-.238			-.059		-.115	.183	-.072	.045	.114			3
4	.125	.107	.498	-.438	.526	.216	-.422			-.095	-.093	-.106		.068	.112	.152			4
5	.112	.107	.577	-.102	-.197	-.316	-.418			-.079	.032	.322	.194		.117				5
6	.134	.557	-.431	-.415						.018	.329		.422		.174				6
7	.537	-.431		-.373		-.361				.287			.521		.149				7
8	-.355	.105		-.379		-.340					.487		.514						8
9		-.439		-.355						.629	.613								9
10	-.328	-.378								.599	.575								10
11	-.209	-.328																	11
12	-.287	-.290																	12
	α = -12°									δ = -30°									
1	.164	.247	.020	-.110	-.047	-.252	.140			-.270		-.450		-.467	-.481	-.416			1
2	.342	.342	.370	.373	.352	.573	.944			-.112	-.177	-.351		-.418	-.481	-.413			2
3	.242	.242		.721	.716	.716	1.107			-.108		-.215	-.251	-.416	-.434	-.408			3
4	.251	.225	.683	.267	.683	.787	.921			-.148	-.161	-.178		-.257	-.097	-.397			4
5	.227	.291	.756	-.023	.411	.826	.805			-.120	-.163	-.123	-.439		-.403				5
6	.388	.754	.414	.270						-.133	-.145		-.412		-.412				6
7	.716	.373		.539		-.985				-.044			-.424		-.428				7
8	.375	.177		.793		.865					-.424		-.411						8
9		.372		.828						-.308	-.403								9
10	.416	.392								-.319	-.355								10
11	.484	.548																	11
12	.478	.578																	12
	α = -12°									δ = -20°									
1	.158	.250	.021	-.108	-.047	-.243	.312			-.273		-.447		-.473	-.473	-.433			1
2	.336	.346	.373	.379	.356	.528	1.073			-.120	-.180	-.354		-.426	-.487	-.426			2
3	.247	.242		.727	.712	.497	.808			-.115		-.216	-.259	-.429	-.453	-.428			3
4	.246	.231	.678	-.016	.659	.605	.609			-.155	-.163	-.179		-.269	-.123	-.377			4
5	.228	.259	.747	-.115	.066	.806	.640			-.122	-.168	-.123	-.462		-.417				5
6	.360	.753	.042	-.012						-.136	-.161		-.407		-.432				6
7	.707	.023		.190		.616				-.071			-.411		-.441				7
8	.020	.103		.464		.584							-.377						8
9		.028		.517							-.437								9
10	.111	.082								-.252	-.365								10
11	.275	.256								-.297	-.281								11
12	.303	.302																	12

[redacted]

Table 24 Concluded

Pressure Coefficients on Delta Wing with Control

Configuration J4 M = 1.61 R = 4.2 x 10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = -12°									δ = -10°									
1	.166	.251	.021	-.108	-.047	-.247	.082												1
2	.342	.348	.374	.379	.359	.528	.838			-.270		-.449		-.479	-.481	-.442			2
3	.250	.244		.720	.712	.467	.589			-.114	-.180	-.354		-.433	-.490	-.431			3
4	.248	.233	.680	-.239	.660	.278	.147			-.114		-.218	-.270	-.420	-.462	-.429			4
5	.230	.262	.754	-.205	-.082	.623	.338			-.155	-.162	-.191		-.273	-.115	-.380			5
6	.358	.755	-.217	-.204						-.126	-.165	-.128	-.421		-.417				6
7	.713	-.219		.033		.235				-.142	-.155		-.417		-.430				7
8	-.232	.041		.209		.263				-.098			-.421		-.446				8
9		-.214		.252									-.347						9
10	-.028	-.094									-.380								10
11	.128	.048								-.164	-.381								11
12	.130	.088								-.283	-.211								12
	α = -12°									δ = 00°									
1	.159	.247	.010	-.116	-.059	-.257	-.090												1
2	.333	.339	.369	.368	.356	.514	.390			-.272		-.444		-.478	-.482	-.435			2
3	.243	.234		.714	.707	.457	.362			-.116	-.174	-.354		-.434	-.486	-.409			3
4	.243	.225	.671	-.364	.653	.251	.005			-.116		-.226	-.284	-.424	-.457	-.415			4
5	.225	.257	.749	-.286	-.178	.270	.069			-.155	-.159	-.187		-.291	-.107	-.359			5
6	.360	.743	-.359	-.272						-.125	-.168	-.125	-.344		-.413				6
7	.710	-.367		-.093		-.091				-.140	-.159		-.352		-.420				7
8	-.357	.026		-.012		-.052				-.103			-.336		-.434				8
9		-.323		.026									-.315						9
10	-.088	-.212									-.269								10
11	-.037	-.136								-.216	-.258								11
12	-.085	-.088								-.221	-.234								12
	α = -12°									δ = 10°									
1	.170	.244	.013	-.114	-.045	-.254	-.147												1
2	.329	.343	.367	.374	.353	.524	.055			-.285		-.448		-.483	-.497	-.461			2
3	.240	.234		.721	.708	.454	.116			-.130	-.184	-.360		-.441	-.497	-.421			3
4	.236	.225	.679	-.411	.649	.263	-.095			-.130		-.201	-.291	-.435	-.486	-.431			4
5	.224	.270	.744	-.316	-.205	-.023	-.132			-.164	-.175	-.195		-.287	-.125	-.434			5
6	.368	.743	-.416	-.328						-.138	-.183	-.140	-.226		-.423				6
7	.707	-.415		-.220		-.292				-.125	-.167		-.206		-.407				7
8	-.380	.000		-.204		-.287				-.104			-.187		-.371				8
9		-.367		-.195									-.187						9
10	-.187	-.321									-.082								10
11	-.062	-.273								-.073	-.065								11
12	-.209	-.193								-.061	-.048								12
	α = -12°									δ = 20°									
1	.166	.248	.010	-.119	-.052	-.256	-.135												1
2	.331	.338	.370	.379	.354	.519	-.183			-.289		-.453		-.461	-.407	-.342			2
3	.243	.240		.728	.719	.466	-.076			-.123	-.190	-.360		-.447	-.388	-.294			3
4	.237	.232	.680	-.415	.660	.256	-.205			-.123		-.203	-.220	-.405	-.383	-.307			4
5	.224	.271	.751	-.284	-.215	-.210	-.286			-.158	-.171	-.190		-.318	-.102	-.343			5
6	.370	.750	-.427	-.382						-.139	-.178	-.083	-.113		-.345				6
7	.711	-.432		-.335		-.397				-.123	-.162		-.101		-.321				7
8	-.378	.031		-.346		-.398				.027			-.045		-.307				8
9		-.417		-.343									.033						9
10	-.286	-.405									.250								10
11	-.148	-.326								.206	.271								11
12	-.222	-.233								.250	.298								12
	α = -12°									δ = 30°									
1	.166	.253	.018	-.118	-.046	-.243	-.067												1
2	.336	.338	.368	.370	.357	.524	-.316			-.284		-.453		-.306	-.202	-.071			2
3	.240	.235		.719	.719	.468	-.202			-.118	-.186	-.333		-.291	-.164	.046			3
4	.236	.227	.687	-.414	.658	.264	-.318			-.120		-.244	-.159	-.250	-.140	-.025			4
5	.222	.281	.755	-.253	-.213	-.302	-.376			-.156	-.166	-.211		-.189	.004	-.085			5
6	.374	.751	-.427	-.422						-.131	-.179	.114	-.145		-.110				6
7	.718	-.429		-.382		-.364				-.091	.207		-.079		-.141				7
8	-.370	.078		-.379		-.360				.191			-.010		-.208				8
9		-.444		-.358									.014						9
10	-.329	-.408									.573								10
11	-.200	-.341								.554	.580								11
12	-.278	-.289								.506	.550								12

[redacted]

Table 25

Pressure Coefficients on Delta Wing with Control

Configuration A M = 2.01 R = 4.2×10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
								α = 00°			δ = 00°									
1	.364	.323	.328	.323	.333	.329	.071				.060	.053	.046	.046	.021	.026	.083			1
2	.059	.045	.052	.049	.041	.032	.042				.023		-.001	-.006	.001	.005	.010			2
3	.025	.010	.003	.000	-.001	.013	-.146				.009	.001	-.009	-.015	-.031	.008				3
4	.018	.008	-.009	-.024	-.011	.039	-.142				.000	-.008	-.038	-.131	-.015					4
5	.008	.002	-.030	-.119	.008	-.004					.008	-.027	.025	-.127		-.015				5
6	.010	-.027	-.008	-.114	-.025	.026					-.005	.014	-.121	-.125	.042	-.141				6
7	.001	.003	-.118	-.124	-.077	-.146					-.004	-.113	-.119		-.133	-.149				7
8	-.023	-.111	-.113		-.122	-.136					-.114	-.114	-.121		-.120	-.134				8
9	-.104	-.107	-.113		-.129	-.135					-.059	-.110			-.129					9
10	-.075	-.109			-.122						-.121									10
11																				11
								α = 00°			δ = 10°									
1	.366	.325	.331		.337	.331	-.057	.052			.062	.056			.026	.027	.244			1
2	.060	.046	.056		.048	.037	-.093	-.100			.025				.005	.006	.218	.115		2
3	.027	.012			.004	.017	-.202	-.098			.012	.003			-.027	.028	-.015	.237		3
4	.020	.010			-.006	.046	-.191	-.174			.002	-.006			-.009		-.042	.051		4
5	.010	.004			.013	.034		-.207			.009	-.024				.070		-.020		5
6	.013	-.027			-.012	-.113					-.003	.017			.120	.016				6
7	.003	.005			-.159	-.205					-.003	-.110			-.013	.019				7
8	-.020	-.109			-.182	-.208					-.112	-.109			-.018	.017				8
9	-.100	-.104			-.179	-.208					-.056	-.107			-.028					9
10	-.074	-.107			-.177						-.119									10
11																				11
								α = 00°			δ = 20°									
1	.367	.326	.331	.327	.337	.331	-.149	.093			.063	.055	.049	.049	.024	.026	.455			1
2	.062	.048	.056	.056	.049	.039	-.176	-.191			.026		.003	-.002	.006	.006	.480	.234		2
3	.028	.013	.009	.006	.005	.020	-.242	-.210			.013	.005	-.005	-.010	-.028	.059	.161	.504		3
4	.022	.012	-.004	-.017	-.005	.055	-.233	-.234			.003	-.005	-.035	-.100	-.005		.146	.200		4
5	.012	.006	-.022	-.128	.014	.067		-.240			.011	-.024	.028	-.102		.149		.183		5
6	.013	-.026	-.002	-.142	.006	-.192					-.001	.016	-.117	-.140	.110	.273				6
7	.004	.006	-.111	-.158	-.214	-.244					-.001	-.110	-.114		.192	.261				7
8	-.019	-.107	-.107		-.229	-.244					-.111	-.111	-.116		.171	.240				8
9	-.099	-.103	-.107		-.226	-.241					-.054	-.107			.149					9
10	-.075	-.105			-.229						-.117									10
11																				11
								α = 00°			δ = 30°									
1	.364	.325	.330	.326	.336	.331	-.230	.299			.060	.053	.048	.046	.021	.024	.823			1
2	.062	.046	.055	.055	.048	.041	-.254	-.246			.023		.001	-.005	.002	.006	.784	.469		2
3	.027	.012	.008	.006	.003	.021	-.268	-.262			.013	.003	-.006	-.008	-.031	.215	.500	.793		3
4	.023	.011	-.003	-.018	-.006	.095	-.266	-.267			.000	-.007	-.038	-.087	.019		.524	.355		4
5	.012	.005	-.022	-.131	.012	.174		-.266			.009	-.026	.026	-.094		.321		.547		5
6	.012	-.027	-.002	-.146	.060	-.241					-.002	.015	-.119	-.149	.089	.685				6
7	.001	.006	-.113	-.161	-.258	-.259					-.002	-.112	-.116		.539	.627				7
8	-.019	-.110	-.108		-.267	-.259					-.114	-.113	-.116		.478	.539				8
9	-.099	-.105	-.108		-.264	-.255					-.055	-.109			.424					9
10	-.081	-.107			-.260						-.120									10
11																				11
								α = 03°			δ = 00°									
1	.366	.257	.306	.287	.319	.345	-.070	-.034			.123	.144	.141	.145	.121	.135	.233			1
2	.012	-.028	-.053	-.064	-.070	-.100	-.092	-.084			.067		.070	.056	.075	.093	.119	.187		2
3	-.005	-.030	-.043	-.050	-.062	-.079	-.223	-.088			.059	.053	.046	.038	.033	.082	-.071	.149		3
4	-.004	-.029	-.047	-.066	-.063	-.023	-.202	-.162			.047	.041	.014	-.085	.045		-.071	-.016		4
5	-.021	-.033	-.048	-.143	-.042	-.034		-.225			.053	.013	.075	-.085		.117		-.080		5
6	-.019	-.056	-.038	-.138	-.019	-.053					.039	.063	-.085	-.089	.128	-.079				6
7	-.026	-.026	-.138	-.147	-.136	-.201					.029	-.080	-.082		-.094	-.066				7
8	-.042	-.130	-.133		-.156	-.194					-.074	-.080	-.083		-.081	-.059				8
9	-.125	-.127	-.132		-.163	-.194					-.038	-.077			-.071					9
10	-.098	-.128			-.163						-.087									10
11																				11

[redacted]

Table 25 Continued

Pressure Coefficients on Delta Wing with Control

Configuration A $M = 2.01$ $R = 4.2 \times 10^6$

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	$\alpha = 06^\circ$									$\delta = -30^\circ$									
1	.353	.215	.258	.224	.255	.285	.414	.001		.185	.216	.226	.230	.210	.228	-.115	-.211		1
2	-.049	-.128	-.150	-.178	-.171	-.194	.499	.122		.121		.128	.120	.146	.172	-.189	-.217		2
3	-.037	-.063	-.121	-.143	-.156	-.172	.144	.540		.107	.106	.104	.097	.094	.173	-.257	-.260		3
4	-.040	-.061	-.082	-.071	-.133	.001	.174	.329		.102	.092	.066	-.059	.104		-.240	-.264		4
5	-.057	-.072	-.089	-.157	-.042	.053		.229		.101	.057	.131	-.076		-.214				5
6	-.052	-.083	-.075	-.186	.008	.089				.084	.114	-.048	-.101	-.193	-.267				6
7	-.056	-.056	-.165	-.216	-.016	.280				.068	-.046	-.045		-.265	-.258				7
8	-.063	-.150	-.160		.356	.277				-.038	-.047	-.049		-.261	-.226				8
9	-.149	-.149	-.149		.328	.265				-.018	-.044			-.262					9
10	-.124	-.152			.295					-.042									10
11																			11
	$\alpha = 06^\circ$									$\delta = -20^\circ$									
1	.353	.215	.259	.226	.258	.285	.122	-.102		.186	.216	.226	.232	.210	.226	-.008	-.129		1
2	-.047	-.127	-.148	-.175	-.170	-.194	.196	-.010		.122		.128	.121	.146	.171	-.116	-.103		2
3	-.036	-.062	-.121	-.140	-.156	-.158	-.057	.225		.107	.107	.104	.099	.093	.170	-.215	-.218		3
4	-.038	-.060	-.082	-.102	-.154	-.106	-.045	.126		.102	.093	.066	-.057	.103		-.200	-.227		4
5	-.056	-.071	-.089	-.157	-.121	-.072		-.008		.102	.058	.130	-.074		-.139				5
6	-.050	-.082	-.075	-.165	-.020	.067				.085	.114	-.047	-.099	-.111	-.239				6
7	-.056	-.055	-.165	-.200	-.078	.012				.069	-.045	-.044		-.231	-.228				7
8	-.063	-.149	-.161		.104	.021				-.038	-.045	-.048		-.220	-.208				8
9	-.148	-.148	-.157		.084	.013				-.017	-.042			-.225					9
10	-.124	-.150			.066					-.042									10
11																			11
	$\alpha = 06^\circ$									$\delta = -10^\circ$									
1	.351	.214	.258	.226	.257	.285	-.059	-.116		.183	.215	.227	.230	.209	.226	.164	.024		1
2	-.049	-.128	-.150	-.176	-.171	-.193	-.038	-.080		.120		.128	.118	.145	.171	.016	.045		2
3	-.037	-.063	-.121	-.141	-.156	-.172	-.204	-.019		.106	.106	.104	.097	.092	.169	-.129	-.092		3
4	-.040	-.061	-.082	-.105	-.158	-.140	-.198	-.086		.099	.092	.066	-.058	.103		-.114	-.154		4
5	-.057	-.071	-.088	-.159	-.126	-.111		-.195		.101	.056	.130	-.071		.005				5
6	-.052	-.032	-.074	-.160	-.023	-.139				.083	.113	-.048	-.094	.024	-.154				6
7	-.056	-.056	-.163	-.170	-.120	-.165				.068	-.046	-.045		-.151	-.137				7
8	-.063	-.150	-.160		-.093	-.160				-.039	-.048	-.048		-.143	-.127				8
9	-.148	-.148	-.157		-.102	-.162				-.017	-.044			-.137					9
10	-.125	-.151			-.113					-.044									10
11																			11
	$\alpha = 06^\circ$									$\delta = 00^\circ$									
1	.351	.216	.259	.225	.255	.284	-.142	-.092		.179	.209	.222	.222	.205	.223	.270	.250		1
2	-.043	-.107	-.135	-.164	-.167	-.187	-.150	-.153		.116		.122	.114	.140	.167	.185	.215		2
3	-.034	-.059	-.118	-.130	-.153	-.172	-.240	-.149		.103	.099	.100	.093	.088	.167	-.032	.029		3
4	-.037	-.059	-.081	-.107	-.158	-.137	-.220	-.200		.096	.089	.062	-.055	.098		-.053	-.039		4
5	-.055	-.070	-.068	-.174	-.128	-.093		-.234		.100	.056	.125	-.050		.194				5
6	-.049	-.078	-.075	-.168	-.030	-.127				.082	.113	-.050	-.055	.194	-.043				6
7	-.055	-.056	-.165	-.180	-.167	-.219				.067	-.048	-.048		-.066	-.040				7
8	-.063	-.150	-.163		-.189	-.219				-.040	-.048	-.051		-.047	-.033				8
9	-.148	-.149	-.158		-.180	-.220				-.017	-.045			-.046					9
10	-.125	-.150			-.175					-.044									10
11																			11
	$\alpha = 06^\circ$									$\delta = 10^\circ$									
1	.351	.215	.258	.225	.256	.286	-.216	-.102		.182	.214	.224	.228	.206	.225	.489	.634		1
2	-.049	-.125	-.148	-.175	-.169	-.191	-.228	-.222		.119		.125	.117	.143	.169	.428	.452		2
3	-.037	-.062	-.120	-.140	-.156	-.177	-.262	-.233		.104	.104	.102	.096	.091	.169	.136	.159		3
4	-.040	-.061	-.082	-.107	-.158	-.136	-.252	-.246		.098	.091	.065	-.035	.100		.121	.162		4
5	-.056	-.071	-.081	-.181	-.126	-.068		-.255		.102	.056	.129	-.010		.472				5
6	-.052	-.082	-.074	-.182	-.027	-.201				.082	.113	-.049	-.032	.334	.191				6
7	-.057	-.056	-.164	-.193	-.216	-.252				.067	-.048	-.046		.092	.182				7
8	-.062	-.149	-.161		-.237	-.254				-.040	-.048	-.050		.098	.165				8
9	-.147	-.148	-.158		-.215	-.236				-.016	-.045			.092					9
10	-.125	-.151			-.200					-.045									10
11																			11

[redacted]

Table 25 Continued

Pressure Coefficients on Delta Wing with Control

Configuration A M = 2.01 R = 4.2 x 10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
								α = 06°					δ = 20°						
1	.351	.215	.258	.225	.257	.287	-.258	-.069		.183	.214	.223	.228	.206	.224	.821			1
2	-.050	-.127	-.149	-.176	-.169	-.192	-.263	-.257		.120		.125	.117	.142	.168	.692	1.287		2
3	-.038	-.063	-.122	-.142	-.155	-.176	-.276	-.264		.104	.104	.101	.096	.090	.170	.428	.712		3
4	-.041	-.062	-.083	-.107	-.157	-.131	-.271	-.269		.098	.090	.064	-.010	.100		.438	.319		4
5	-.057	-.072	-.086	-.182	-.125	.063		-.267		.101	.056	.127	.005		.694		.460		5
6	-.052	-.082	-.075	-.190	-.010	-.243				.082	.112	-.050	-.061	.302	.547				6
7	-.058	-.056	-.165	-.196	-.250	-.270				.067	-.048	-.047		.353	.506				7
8	-.063	-.150	-.163		-.255	-.265				-.042	-.048	-.050		.360	.435				8
9	-.149	-.149	-.160		-.239	-.251				-.016	-.045			.337					9
10	-.127	-.151			-.233					-.046									10
11																			11
								α = 06°					δ = 30°						
1	.352	.215	.259	.226	.258	.287	-.274	-.061		.184	.215	.224	.229	.206	.222	1.170			1
2	-.048	-.127	-.148	-.174	-.169	-.190	-.276	-.273		.120		.126	.118	.141	.167	.992	.982		2
3	-.036	-.062	-.121	-.139	-.154	-.174	-.281	-.275		.106	.105	.102	.101	.089	.477	.804	.971		3
4	-.039	-.060	-.082	-.104	-.156	-.118	-.278	-.276		.098	.092	.064	.020	.182		.741	.748		4
5	-.055	-.070	-.087	-.181	-.127	.364		-.273		.102	.057	.127	.028		.726		.767		5
6	-.051	-.082	-.074	-.189	.115	-.264				.082	.112	-.049	-.065	.268	.946				6
7	-.057	-.054	-.164	-.191	-.265	-.281				.067	-.048	-.046		.731	.820				7
8	-.062	-.149	-.161		-.266	-.272				-.041	-.048	-.044		.666	.723				8
9	-.147	-.147	-.158		-.257	-.264				-.014	-.045			.591					9
10	-.127	-.149			-.255					-.047									10
11																			11
								α = 09°					δ = 00°						
1	.334	.177	.204	.160	.150	.196	-.167	-.142		.255	.291	.305	.306	.286	.304	.325			1
2	-.107	-.184	-.212	-.232	-.230	-.247	-.165	-.194		.174		.199	.181	.212	.248	.258	.316		2
3	-.064	-.127	-.187	-.201	-.216	-.229	-.189	-.166		.160	.164	.164	.162	.157	.232	.021	.286		3
4	-.066	-.095	-.163	-.192	-.216	-.199	-.179	-.175		.159	.146	.120	-.007	.163		-.012	.073		4
5	-.085	-.103	-.117	-.210	-.205	-.088		-.167		.154	.104	.189	-.008		.258		.018		5
6	-.078	-.107	-.113	-.214	-.012	-.164				.131	.170	-.010	-.016	.284	.026				6
7	-.083	-.084	-.187	-.221	-.185	-.179				.114	-.010	-.007		-.016	.002				7
8	-.082	-.165	-.183		-.186	-.187				.000	-.008	-.012		.003	.009				8
9	-.166	-.169	-.185		-.179	-.195				.015	-.006			-.002					9
10	-.147	-.170			-.171					.003									10
11																			11
								α = 12°					δ = -30°						
1	.299	.133	.131	.092	.021	.060	.024	-.247		.333	.367	.374	.374	.353	.374	-.037			1
2	-.176	-.254	-.279	-.290	-.280	-.275	.179	-.186		.237		.267	.256	.288	.319	-.143	-.169		2
3	-.098	-.193	-.246	-.263	-.266	-.278	-.070	.218		.218	.229	.229	.222	.225	.296	-.233	-.122		3
4	-.089	-.125	-.219	-.232	-.264	-.233	-.056	.139		.221	.204	.181	.029	.233		-.214	-.227		4
5	-.115	-.133	-.181	-.269	-.210	-.217		.017		.212	.156	.252	.005		-.170		-.238		5
6	-.112	-.136	-.178	-.269	.035	-.218				.183	.230	.033	-.031	-.156	-.258				6
7	-.114	-.119	-.224	-.287	-.136	.046				.165	.032	.041		-.258	-.250				7
8	-.107	-.190	-.215		-.003	-.027				.038	.028	.031		-.261	-.218				8
9	-.190	-.189	-.226		-.016	-.031				.052	.034			-.257					9
10	-.172	-.196			-.022					.042									10
11																			11
								α = 12°					δ = -20°						
1	.299	.134	.133	.093	.024	.062	-.126	-.220		.335	.367	.374	.375	.353	.373	.081			1
2	-.175	-.252	-.277	-.288	-.278	-.275	-.064	-.220		.237		.268	.257	.287	.320	-.041	-.058		2
3	-.097	-.191	-.245	-.261	-.265	-.270	-.215	-.034		.218	.229	.230	.225	.226	.294	-.168	-.008		3
4	-.098	-.126	-.217	-.251	-.262	-.255	-.211	-.078		.222	.205	.182	.033	.235		-.157	-.128		4
5	-.116	-.133	-.179	-.261	-.236	-.189		-.176		.214	.157	.254	.008		-.059		-.185		5
6	-.111	-.134	-.176	-.260	.036	-.242				.184	.232	.033	-.027	-.040	-.200				6
7	-.113	-.118	-.222	-.287	-.186	-.196				.165	.033	.041		-.202	-.193				7
8	-.107	-.190	-.213		-.160	-.191				.038	.031	.032		-.205	-.175				8
9	-.189	-.189	-.227		-.171	-.192				.052	.034			-.207					9
10	-.171	-.194			-.172					.045									10
11																			11

[redacted]

Table 25 Continued

Pressure Coefficients on Delta Wing with Control

Configuration A M = 2.01 R = 4.2×10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
								α = 12°			δ = -10°									
1	.299	.133	.131	.092	.023	.062	-.223	-.174			.335	.367	.373	.374	.352	.371	.236			1
2	-.175	-.252	-.279	-.288	-.280	-.283	-.212	-.254			.239		.267	.257	.284	.319	.101	.113		2
3	-.097	-.191	-.246	-.261	-.266	-.275	-.276	-.196			.218	.230	.229	.225	.224	.290	-.066	.139		3
4	-.099	-.125	-.219	-.257	-.264	-.264	-.266	-.228			.223	.206	.181	.033	.232		-.065	-.012		4
5	-.116	-.133	-.180	-.262	-.248	-.114		-.256			.214	.157	.252	.011		.104		-.071		5
6	-.111	-.135	-.178	-.255	.031	-.264					.183	.230	.033	-.023	.121	-.098				6
7	-.113	-.118	-.223	-.276	-.244	-.268					.166	.031	.040		-.108	-.097				7
8	-.106	-.190	-.215		-.252	-.269					.038	.029	.031		-.104	-.086				8
9	-.189	-.188	-.229		-.258	-.269					.052	.033			-.109					9
10	-.172	-.194			-.254						.044									10
11																				11
								α = 12°			δ = 00°									
1	.303	.142	.139	.099	.028	.067	-.220	-.158			.333	.362	.373	.371	.353	.373	.377			1
2	-.153	-.217	-.245	-.258	-.260	-.276	-.222	-.234			.236		.268	.257	.290	.320	.320	.380		2
3	-.089	-.168	-.225	-.231	-.247	-.259	-.229	-.222			.217	.223	.231	.225	.226	.294	.070	.348		3
4	-.083	-.117	-.200	-.241	-.250	-.251	-.223	-.226			.218	.203	.180	.042	.234		.059	.102		4
5	-.109	-.126	-.138	-.248	-.237	-.069		-.214			.214	.156	.251	.039		.333		.095		5
6	-.104	-.124	-.170	-.250	.018	-.211					.182	.232	.034	.039	.357	.075				6
7	-.106	-.114	-.216	-.245	-.219	-.227					.163	.031	.041		.031	.055				7
8	-.102	-.184	-.207		-.229	-.234					.040	.031	.031		.055	.064				8
9	-.185	-.183	-.221		-.223	-.233					.054	.034			.048					9
10	-.167	-.188			-.203						.044									10
11																				11
								α = 12°			δ = 10°									
1	.302	.136	.135	.097	.027	.067	-.255	-.138			.336	.370	.376	.376	.353	.375	.593			1
2	-.167	-.234	-.259	-.273	-.269	-.287	-.255	-.258			.240		.269	.259	.291	.322	.562	.768		2
3	-.093	-.182	-.237	-.247	-.257	-.266	-.254	-.254			.219	.232	.233	.227	.226	.294	.306	.585		3
4	-.084	-.120	-.210	-.252	-.256	-.261	-.250	-.252			.221	.206	.184	.068	.235		.292	.240		4
5	-.110	-.128	-.154	-.264	-.242	.024		-.241			.216	.158	.255	.104		.619		.334		5
6	-.108	-.129	-.172	-.259	.037	-.243					.185	.233	.037	.073	.553	.348				6
7	-.109	-.114	-.218	-.261	-.247	-.254					.165	.034	.045		.216	.327				7
8	-.102	-.185	-.208		-.255	-.260					.041	.031	.034		.230	.296				8
9	-.185	-.183	-.223		-.243	-.252					.056	.036			.217					9
10	-.168	-.189			-.230						.045									10
11																				11
								α = 12°			δ = 20°									
1	.302	.135	.134	.095	.026	.067	-.275	.012			.337	.369	.375	.375	.353	.373	1.013			1
2	-.172	-.246	-.270	-.281	-.276	-.293	-.276	-.283			.240		.268	.257	.288	.319	.822	1.524		2
3	-.095	-.188	-.241	-.255	-.262	-.271	-.272	-.274			.220	.232	.230	.226	.223	.316	.674	.816		3
4	-.087	-.123	-.215	-.254	-.260	-.257	-.270	-.272			.221	.207	.182	.105	.234		.618	.612		4
5	-.113	-.131	-.168	-.275	-.243	.297		-.262			.216	.158	.253	.136		.818		.654		5
6	-.110	-.132	-.174	-.259	.071	-.273					.184	.231	.034	.048	.532	.752				6
7	-.112	-.116	-.220	-.240	-.272	-.276					.164	.033	.042		.515	.672				7
8	-.104	-.187	-.210		-.273	-.278					.038	.030	.034		.513	.597				8
9	-.187	-.185	-.225		-.272	-.271					.056	.035			.484					9
10	-.172	-.192			-.263						.042									10
11																				11
								α = 12°			δ = 30°									
1	.302	.136	.135	.096	.027	.069	-.281	-.007			.337	.369	.375	.375	.352	.371	1.114			1
2	-.171	-.247	-.272	-.281	-.275	-.281	-.283	-.292			.241		.269	.256	.287	.319	1.189	1.280		2
3	-.094	-.187	-.241	-.256	-.262	-.272	-.279	-.281			.221	.233	.230	.243	.223	.759	1.041	1.154		3
4	-.087	-.122	-.215	-.250	-.260	-.236	-.277	-.279			.222	.207	.182	.168	.502		.961	.999		4
5	-.111	-.129	-.171	-.277	-.243	.540		-.273			.217	.158	.252	.168		.833		.947		5
6	-.109	-.132	-.175	-.255	.290	-.282					.185	.230	.034	.023	.535	1.218				6
7	-.111	-.114	-.219	-.248	-.281	-.281					.165	.033	.042		.930	1.052				7
8	-.103	-.186	-.211		-.281	-.283					.039	.030	.063		.868	.961				8
9	-.185	-.195	-.223		-.281	-.279					.056	.035			.785					9
10	-.171	-.190			-.270						.042									10
11																				11

[redacted]

Table 25 Concluded

Pressure Coefficients on Delta Wing with Control

Configuration A M = 2.01 R = 4.2×10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
	$\alpha = 15^\circ$										$\delta = 00^\circ$									
1	.276	.096	.049	.023	-.059	-.065	-.235	-.158			.381	.436	.437	.431	.412	.434	.394	.448		1
2	-.209	-.270	-.292	-.299	-.296	-.304	-.224	-.261			.297		.334	.320	.353	.377	.385	.414		2
3	-.117	-.246	-.271	-.278	-.286	-.297	-.230	-.219			.283	.294	.293	.294	.287	.352	.128	.133		3
4	-.115	-.151	-.237	-.286	-.280	-.291	-.229	-.212			.284	.268	.241	.091	.297		.119			4
5	-.139	-.156	-.198	-.284	-.271	-.022		-.210			.270	.209	.318	.089		.418				5
6	-.133	-.151	-.204	-.278	.063	-.265					.229	.296	.076	.078	.445	.132				6
7	-.134	-.142	-.247	-.263	-.235	-.234					.218	.076	.085		.089	.115				7
8	-.123	-.209	-.247		-.237	-.240					.081	.073	.072		.111	.122				8
9	-.204	-.205	-.245		-.232	-.232					.095	.077			.103					9
10	-.188	-.211			-.215						.089									10
11																				11

[redacted]

Table 26

Pressure Coefficients on Delta Wing with Control

Configuration E M = 2.01 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station								Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 00°									δ = 00°									
1	.368	.338	.332	.330	.327	.316	.286	-.140		.060	.053	.049	.047	.052	.042	.054	-.122		1
2	.067	.051	.061	.060	.066	.038	.047			.027		.003	.002	.022	.019	-.106			2
3	.033	.016	.012	.008	.017	.023	-.129			.015	.005	-.002	-.001	.005	-.086	-.116			3
4	.026	.014	-.002	-.008	.015	-.002	-.147			.005	-.005	-.033	-.117	.002	-.113				4
5	.013	.007	-.026	.118	.003	-.125				.009	.002	.006	-.109	-.109	-.121				5
6	.016	.030	.008	-.108	-.113	-.131				-.005	.004	-.106	-.103	-.120					6
7	.010	.010	-.103	-.105	-.106					.004	-.104	-.106							7
8		-.099	-.104							-.089	-.098	-.102							8
9	-.089	-.100	-.107							-.070	-.102								9
10	-.060	.127								-.096									10
11	-.087																		11
	α = 00°									δ = 10°									
1	.369			.331	.342	.204	.212	-.219		.064			.051	.206	.276	.259	.019		1
2	.072			.065	-.024	-.153	-.187			.032			.070	.352	.162	.021			2
3	.038			-.040	-.028	-.118	-.221			.020			.019	.078	.016	.012			3
4	.033			-.051	-.044	-.084	-.214			.012			-.113	.056	-.031				4
5	.019			.113	-.045	-.169				.016			-.129	-.035	-.040				5
6	.022			-.126	-.158	-.167				.002		-.074	-.116	-.064					6
7	.016			-.129	-.148					.007		-.074							7
8										-.080		-.068							8
9	-.079									-.060									9
10	-.053																		10
11	-.078																		11
	α = 00°									δ = 20°									
1	.367	.336	.330	.328	.304	.091	.098	-.236		.059	.053	.049	.048	.431	.439	.429	.146		1
2	.067	.053	.064	.062	-.147	-.190	-.222			.026		.004	.106	.367	.351	.161			2
3	.032	.017	.015	.077	-.073	-.182	-.244			.015	.008	-.001	-.051	.283	.125	.147			3
4	.026	.015	.002	-.118	-.088	-.171	-.232			.003	-.003	-.036	-.172	.138	.072				4
5	.015	.008	.012	.102	-.090	-.212				.009	.004	.063	-.171	.048	.066				5
6	.016	.031	-.015	-.142	-.188	-.198				-.003	.006	-.049	-.137	.018					6
7	.010	.015	-.136	-.136	-.179					.000	-.099	-.056							7
8		-.077	-.145							-.085	-.086	-.055							8
9	-.085	-.089	-.151							-.067	-.070								9
10	-.060	.108								-.094									10
11	-.085																		11
	α = 00°									δ = 30°									
1	.366	.336	.329	.328	.176	-.077	-.113	-.253		.059	.052	.046	.043	.935	.789	.704	.521		1
2	.068	.053	.063	.061	-.226	-.232	-.255			.025		.002	.021	.646	.704	.491			2
3	.033	.017	.015	.816	-.172	-.243	-.267			.019	.009	-.003	-.154	.809	.384	.475			3
4	.030	.016	.001	-.223	-.145	-.243	-.254			.003	-.003	-.040	-.188	.395	.392				4
5	.015	.009	.110	.098	-.172	-.261				.009	.003	.122	-.201	.307	.363				5
6	.016	.032	.015	-.192	-.230	-.247				-.003	.005	-.017	-.210	.263					6
7	.010	.046	-.152	-.173	-.222					-.003	-.099	-.039							7
8		-.044	-.181							-.086	-.046	-.051							8
9	-.085	-.071	-.193							-.066	-.031								9
10	-.056	.103								-.093									10
11	-.069																		11
	α = 03°									δ = 00°									
1	.363	.274	.297	.277	.307	.261	.262	-.221		.121	.149	.146	.151	.160	.161	.161	-.046		1
2	-.001	-.052	-.071	-.077	-.100	-.111	-.121			.071		.070	.062	.104	.106	-.037			2
3	-.016	-.039	-.052	-.064	-.096	-.101	-.215			.058	.057	.046	.031	.082	-.017	-.050			3
4	-.013	-.034	-.054	-.071	-.087	-.103	-.206			.047	.039	.011	-.079	.057	-.050				4
5	-.028	-.044	-.091	.135	-.080	-.189				.051	.050	.050	-.073	-.069	-.066				5
6	-.029	-.018	-.039	-.147	-.183	-.197				.028	.043	-.073	-.073	-.076					6
7	-.033	-.034	-.138	-.143	-.171					.040	-.076	-.075							7
8		-.131	-.138							-.062	-.074	-.071							8
9	-.124	-.133	-.140							-.042	-.076								9
10	-.097	.135								-.072									10
11	-.119																		11

[redacted]

Table 26 Continued

Pressure Coefficients on Delta Wing with Control

Configuration E M = 2.01 R = 4.2×10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
								α = 06°					δ = -30°							
1	.349	.217	.251	.218	.141	.008	-.049	.170			.183	.212	.224	.229	-.146	-.210	-.207	-.248		1
2	-.056	-.136	-.155	-.179	.915	.475	.518				.118		.126	.680	-.076	-.214	-.239			2
3	-.043	-.074	-.126	-.116	.511	.376	.150				.102	.100	.100	-.188	-.092	-.216	-.246			3
4	-.048	-.068	-.088	-.216	.050	.292	.095				.096	.088	.127	-.210	-.173	-.191				4
5	-.062	-.078	-.091	.113	-.006	.068					.099	.099	.102	-.175	-.223	-.198				5
6	-.059	-.049	.017	-.244	.003	.025					.064	.107	-.086	-.139	-.237					6
7	-.059	-.065	-.117	-.240	.022						.090	.002	-.110							7
8		-.147	-.125								-.026	-.015	-.119							8
9	-.141	-.108	-.136								-.006	-.041								9
10	-.105	.116									-.025									10
11	-.136																			11
								α = 06°					δ = -20°							
1	.351	.221	.254	.223	.243	.191	.106	.015			.188	.217	.228	.232	-.029	-.171	-.167	-.236		1
2	-.048	-.125	-.145	-.172	.538	.260	.291				.122		.127	.185	-.012	-.175	-.211			2
3	-.035	-.064	-.117	-.165	.207	.160	-.008				.107	.106	.104	-.089	-.058	-.161	-.217			3
4	-.041	-.059	-.080	-.193	-.123	.087	-.045				.100	.094	.103	-.125	-.140	-.146				4
5	-.054	-.068	-.082	.124	-.076	-.087					.103	.104	.085	-.125	-.213	-.149				5
6	-.051	-.039	-.012	-.201	-.107	-.101					.070	.102	-.066	-.117	-.221					6
7	-.051	-.056	-.125	-.193	-.085						.094	-.014	-.084							7
8		-.137	-.134								-.016	-.021	-.092							8
9	-.132	-.117	-.134								.000	-.038								9
10	-.098	.127									-.027									10
11	-.125																			11
								α = 06°					δ = -10°							
1	.354	.222	.257	.225	.301	.272	.208	-.178			.189	.218	.229	.233	.203	.041	.087	-.012		1
2	-.051	-.129	-.149	-.171	.034	-.038	-.011				.124		.131	.102	.146	.121	.001			2
3	-.038	-.067	-.120	-.145	-.153	-.086	-.197				.107	.106	.104	-.006	.109	.019	-.027			3
4	-.043	-.061	-.082	-.165	-.156	-.122	-.213				.102	.095	.091	-.066	.042	.009				4
5	-.056	-.071	-.041	.135	-.124	-.209					.106	.104	.090	-.081	-.062	-.030				5
6	-.054	-.039	-.046	-.176	-.200	-.221					.072	.102	-.056	-.083	-.056					6
7	-.054	-.057	-.145	-.174	-.190						.094	-.028	-.066							7
8		-.140	-.147								-.017	-.029	-.067							8
9	-.139	-.132	-.146								.002	-.039								9
10	-.104	.140									-.032									10
11	-.131																			11
								α = 06°					δ = 00°							
1	.363	.227	.258	.223	.277	.205	.218	-.230			.185	.209	.226	.225	.252	.238	.239	.017		1
2	-.044	-.102	-.128	-.142	-.142	-.156	-.162				.120		.127	.124	.178	.181	.027			2
3	-.033	-.059	-.116	-.130	-.132	-.153	-.240				.106	.096	.102	.088	.154	.035	.009			3
4	-.038	-.059	-.078	-.115	-.121	-.161	-.230				.098	.092	.063	-.025	.118	.002				4
5	-.054	-.068	-.019	.142	-.122	-.215					.103	.103	.103	-.030	-.020	-.020				5
6	-.051	-.035	-.068	-.172	-.193	-.215					.073	.098	-.034	-.028	-.034					6
7	-.052	-.057	-.159	-.170	-.186						.092	-.037	-.037							7
8		-.142	-.157								-.019	-.031	-.034							8
9	-.137	-.145	-.161								.002	-.035								9
10	-.104	.149									-.035									10
11	-.129																			11
								α = 06°					δ = 10°							
1	.351	.219	.254	2.741	.303	.091	.109	-.237			.185	.214	2.745	.229	.376	.406	.391	.110		1
2	-.052	-.127	-.149	2.351	-.183	-.192	-.208				.119		2.646	.197	.437	.333	.137			2
3	-.039	-.070	2.397	2.324	-.153	-.199	-.247				.103	.102	2.620	.159	.272	.122	.124			3
4	-.045	-.064	2.437	2.408	-.147	-.201	-.236				.096	.091	2.580	-.001	.209	.079				4
5	-.059	-.074	2.460	2.645	-.124	-.234					.102	.101	2.648	-.045	.083	.067				5
6	-.056	-.043	2.428	-.170	-.196	-.229					.073	.095	2.522	-.088	.037					6
7	-.057	-.051	2.341	-.166	-.186						.088	-.041	2.525							7
8		-.139	2.343								-.020	-.036	2.529							8
9	-.141	-.152	2.350								-.003	-.030								9
10	-.107	.126									-.038									10
11	-.130																			11

[redacted]

Table 26 Continued

Pressure Coefficients on Delta Wing with Control

Configuration E M = 2.01 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 06°									δ = 20°									
1	.354	.223	.258	.223	.269	-.006	-.037	-.252		.190	.218	.227	.231	.505	.676	.592	.350		1
2	-.039	-.117	-.137	-.165	-.214	-.218	-.240			.127		.129	.185	.604	.587	.348			2
3	-.027	-.058	-.112	-.010	-.192	-.232	-.265			.110	.109	.103	.138	.618	.293	.339			3
4	-.033	-.053	-.074	-.168	-.176	-.235	-.255			.104	.098	.064	-.077	.399	.262				4
5	-.045	-.063	-.034	.124	-.139	-.258				.109	.107	.181	-.118	.251	.251				5
6	-.043	-.033	-.103	-.183	-.214	-.250				.082	.102	.059	-.107	.190					6
7	-.044	-.004	-.173	-.155	-.209					.095	-.030	.062							7
8		-.109	-.188							-.011	-.016	.046							8
9	-.124	-.132	-.193							.006	.017								9
10	-.084	.128								-.027									10
11	-.094																		11
	α = 06°									δ = 30°									
1	.351	.219	.255	.221	.172	-.125	-.157	-.244		.184	.214	.223	.228	.879	.947	.768	.669		1
2	-.052	-.129	-.149	-.174	-.243	-.237	-.259			.120		.126	.207	.960	.902	.688			2
3	-.039	-.070	-.121		-.233	-.256	-.272			.104	.102	.099	.108	1.026	.533	.659			3
4	-.045	-.064	-.080	-.195	-.219	-.258	-.261			.098	.091	.059	-.125	.722	.578				4
5	-.058	-.074	.009	.116	-.174	-.271				.102	.101	.254	-.163	.529	.543				5
6	-.056	-.042	-.096	-.213	-.245	-.282				.074	.095	.118	-.128	.428					6
7	-.056	.027	-.212	-.201	-.241					.087	-.037	.077							7
8		-.107	-.228							-.026	.055	.039							8
9	-.124	-.141	-.230							-.003	.071								9
10	-.046	.118								-.033									10
11	-.060																		11
	α = 09°									δ = 00°									
1		.181	.200	.157	.209	.133	.167	-.149		.254	.287	.304	.301	.301	.290	.289	.013		1
2	-.108	-.181	-.203	-.197	-.114	-.109	-.129			.173		.196	.185	.231	.229	.050			2
3	-.068	-.133	-.182	-.201	-.126	-.132	-.170			.159	.157	.163	.147	.207	.057	.045			3
4	-.073	-.099	-.158	-.192	-.137	-.140	-.142			.157	.145	.117	.017	.170	.015				4
5	-.089	-.106	-.109	.152	-.168	-.192				.154	.155	.156	.015	.011	.013				5
6	-.082	-.077	-.109	-.218	-.167	-.171				.117	.148	.006	.012	-.018					6
7	-.085	-.088	-.183	-.210	-.143					.143	.001	.002							7
8		-.164	-.183							.021	.006	.002							8
9	-.162	-.170	-.185							.038	.001								9
10	-.125	.160								.001									10
11	-.150																		11
	α = 12°									δ = -30°									
1	.304	.136	.138	.100	.138	-.071	-.054	.085		.331	.367	.374	.376	-.159	-.188	-.172	-.218		1
2	-.172	-.243	-.264	-.273	.947	.372	.381			.239		.268	.662	-.030	-.196	-.214			2
3	-.092	-.183	-.230	-.283	.607	.221	.052			.223	.228	.232	-.153	-.063	-.199	-.228			3
4	-.098	-.121	-.207	-.295	-.001	.104	.009			.226	.208	.252	-.169	-.190	-.145				4
5	-.112	-.128	-.153	.151	-.181	-.064				.215	.223	.225	-.112	-.201	-.165				5
6	-.108	-.099	-.085	-.284	-.189	-.082				.174	.228	.015	-.080	-.238					6
7	-.107	-.117	-.184	-.268	-.156					.202	.030	-.023							7
8		-.172	-.219							.059	.070	-.037							8
9	-.174	-.129	-.229							.060	.045								9
10	-.134	.156								.078									10
11	-.157																		11
	α = 12°									δ = -20°									
1	.301	.131	.135	.098	.290	.223	.199	-.176		.327	.364	.373	.374	.221	.046	.103	-.049		1
2	-.175	-.248	-.266	-.264	.401	.003	-.001			.235		.266	.353	.144	.077	-.023			2
3	-.096	-.187	-.231	-.253	.034	-.080	-.183			.219	.223	.229	.010	.068	.016	-.042			3
4	-.103	-.125	-.206	-.268	-.241	-.140	-.204			.225	.205	.238	-.062	-.033	-.005				4
5	-.117	-.132	-.145	.163	-.231	-.228				.211	.220	.208	-.055	-.116	-.036				5
6	-.112	-.101	-.121	-.247	-.253	-.229				.171	.215	.023	-.051	-.121					6
7	-.111	-.120	-.201	-.228	-.233					.199	.027	-.005							7
8		-.174	-.211							.064	.055	-.013							8
9	-.181	-.157	-.223							.056	.039								9
10	-.143	.167								.059									10
11	-.163																		11

[redacted]

Table 26 Continued

Pressure Coefficients on Delta Wing with Control

Configuration E M = 2.01 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 12°									δ = -10°									
1	.303	.132	.138	.099	.287	.157	.167	-.253		.329	.366	.373	.374	.320	.278	.276	.055		1
2	-.164	-.237	-.259	-.261	-.081	-.189	-.222			.237		.267	.244	.247	.236	.076			2
3	-.088	-.176	-.228	-.228	-.247	-.220	-.257			.221	.226	.230	.098	.199	.088	.055			3
4	-.094	-.116	-.198	-.258	-.243	-.229	-.251			.226	.207	.214	.003	.114	.067				4
5	-.107	-.124	-.139	.178	-.235	-.262				.214	.221	.207	-.012	-.005	.030				5
6	-.103	-.091	-.139	-.243	-.259	-.255				.174	.218	.027	-.013	-.022					6
7	-.103	-.111	-.204	-.221	-.239					.200	.031	.013							7
8		-.163	-.208							.073	.059	.009							8
9	-.170	-.166	-.216							.064	.052								9
10	-.135	.184								.059									10
11	-.152																		11
	α = 12°									δ = 00°									
1	.301	.142	.142	.101	.149	.067	.106	-.207		.323	.355	.367	.366	.370	.361	.360	.076		1
2	-.143	-.204	-.228	-.231	-.182	-.171	-.202			.230		.261	.249	.300	.308	.117			2
3	-.081	-.158	-.212	-.226	-.184	-.194	-.221			.217	.215	.226	.211	.273	.115	.106			3
4	-.086	-.111	-.189	-.236	-.181	-.197	-.199			.221	.203	.174	.066	.234	.078				4
5	-.102	-.120	-.124	.183	-.200	-.233				.211	.217	.213	.064	.065	.067				5
6	-.098	-.087	-.158	-.246	-.205	-.214				.173	.205	.053	.062	.035					6
7	-.098	-.107	-.210	-.223	-.182					.199	.035	.046							7
8		-.168	-.206							.073	.053	.048							8
9	-.168	-.176	-.213							.064	.048								9
10	-.131	.192								.052									10
11	-.149																		11
	α = 12°									δ = 10°									
1	.298	.131	.131	.095	.232	-.024	-.032	-.221		.324	.361	.369	.370	.618	.558	.516	.261		1
2	-.169	-.228	-.250	-.248	-.214	-.198	-.225			.232		.261	.347	.572	.510	.277			2
3	-.095	-.177	-.229	-.255	-.217	-.223	-.234			.217	.220	.225	.328	.390	.248	.269			3
4	-.101	-.122	-.196	-.240	-.215	-.225	-.216			.222	.203	.172	.094	.387	.215				4
5	-.116	-.131	-.145	.159	-.220	-.246				.210	.218	.245	.026	.237	.215				5
6	-.111	-.098	-.186	-.255	-.228	-.229				.172	.203	.098	-.020	.174					6
7	-.112	-.089	-.224	-.236	-.203					.195	.034	.107							7
8		-.178	-.213							.063	.047	.102							8
9	-.179	-.185	-.201							.053	.057								9
10	-.141	.166								.048									10
11	-.147																		11
	α = 12°									δ = 20°									
1	.301	.133	.135	.098	.208	-.122	-.139	-.227		.327	.364	.371	.373	.789	.818	.682	.538		1
2	-.171	-.238	-.259	-.251	-.237	-.217	-.230			.235		.264	.254	.729	.785	.545			2
3	-.093	-.183	-.230	-.127	-.237	-.243	-.240			.219	.224	.228	.345	.711	.447	.525			3
4	-.099	-.123	-.124	-.207	-.239	-.241	-.228			.225	.205	.175	-.013	.604	.470				4
5	-.113	-.131	-.138	.146	-.238	-.250				.212	.220	.313	-.044	.488	.450				5
6	-.109	-.076	-.151	-.255	-.239	-.239				.176	.204	.176	-.052	.375					6
7	-.110	-.066	-.232	-.243	-.223					.196	.037	.168							7
8		-.171	-.208							.052	.070	.136							8
9	-.163	-.193	-.192							.053	.113								9
10	-.106	.152								.052									10
11	-.114																		11
	α = 12°									δ = 25°									
1	.298	.131	.133	.095	.159	-.170	-.183	-.234		.324	.361	.370	.370	.918	.952	.766	.694		1
2	-.175	-.245	-.265	-.253	-.247	-.226	-.236			.232		.262	.217	.870	.953	.720			2
3	-.096	-.188	-.233	-.276	-.248	-.254	-.244			.216	.221	.226	.333	.868	.569	.688			3
4	-.103	-.127	-.092	-.230	-.250	-.250	-.234			.221	.202	.172	-.034	.755	.639				4
5	-.116	-.135	-.123	.142	-.250	-.254				.210	.217	.360	-.066	.640	.589				5
6	-.112	-.021	-.172	-.246	-.250	-.246				.174	.201	.210	-.057	.509					6
7	-.113	-.072	-.246	-.248	-.236					.193	.036	.167							7
8		-.174	-.196							.050	.111	.134							8
9	-.142	-.201	-.192							.051	.147								9
10	-.082	.148								.048									10
11	-.102																		11

[redacted]

Table 26 Concluded

Pressure Coefficients on Delta Wing with Control

Configuration E $M = 2.01$ $R = 4.2 \times 10^6$

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
	$\alpha = 15^\circ$										$\delta = 00^\circ$									
1	.277	.080	.039	.017	.058	-.038	-.041	-.201										.203		1
2	-.208	-.264	-.282	-.283	-.165	-.157	-.189				.395	.446	.445	.438	.496	.462	.447			2
3	-.117	-.239	-.263	-.282	-.178	-.200	-.219				.310		.344	.337	.428	.420	.214			3
4	-.125	-.153	-.231	-.286	-.215	-.213	-.201				.295	.304	.301	.313	.387	.199	.203			4
5	-.139	-.154	-.186	.264	-.241	-.243					.294	.277	.246	.136	.342	.175				5
6	-.134	-.121	-.201	-.283	-.247	-.228					.286	.298	.290	.140	.150	.154				6
7	-.132	-.144	-.241	-.238	-.212						.230	.276	.115	.129	.118					7
8		-.201	-.240								.272	.033	.106							8
9	-.196	-.200	-.237								.125	.102	.108							9
10	-.163	.272									.115	.101								10
11	-.171										.100									11

[redacted]

Table 27

Pressure Coefficients on Delta Wing with Control

Configuration F M = 2.01 R = 4.2×10^6

Orif	Upper Surface at Station 1	2	3	4	5	6	7	8	9	Lower Surface at Station 1	2	3	4	5	6	7	8	9	Orif
								α = 00°			δ = 00°								
1	.385	.347	.341	.342	.415	.090				.081	.069	.063	.082	.055	.037				1
2	.082	.062	.070	.070	.083	.046				.043		.022	.015	.023					2
3	.049	.028	.023	.027	.043	.032				.030	-.020	.010	-.010	.006					3
4	.045	.027	.010	-.002	.023	-.102				.019	.010	-.019	-.101	-.010					4
5	.034	.020	-.015	.148	.013					.028	.017	.020	-.101	-.103					5
6	.033	.045	.023	-.095						.012	.019	-.094	-.095						6
7	.027	.023	-.092	-.094	-.097					.025	-.089	-.096							7
8		-.088	-.090							-.083	-.084	-.092							8
9	-.077	-.088	-.096							-.044	-.088								9
10	-.045	.153								-.084									10
11	-.073																		11
								α = 00°			δ = 10°								
1				.346	.389			-.159									-.042		1
2				.073	.056	-.062						.066	.064	.227	.272	.243			2
3			.026	-.024	.009	-.045	-.166					.023	.080	.150	.159	-.037			3
4			.013	-.078	-.020	-.045	-.163					.012	.021	.105	.120	-.034			4
5			.013	.152	-.040	-.148						-.023	-.083	.066	-.055				5
6			.010	-.130								.050	-.112	-.048					6
7			-.115	-.133	-.119							-.066	-.110						7
8			-.118									-.062							8
9			-.122									-.060							9
								α = 00°			δ = 20°								
1	.386	.353	.346	.343	.335	-.128		-.185									.144		1
2	.087	.068	.073	.072	-.074	-.113	-.196			.080	.067	.059	.058	.569	.485	.467			2
3	.053	.034	.023	.349	-.027	-.131	-.193			.044		.019	.050	.310	.386	.121			3
4	.049	.031	.011	-.179	-.066	-.193				.035	.021	.008	-.060	.345	.314	.119			4
5	.038	.024	.018	.149	-.112					.020	.008	-.028	-.154	.148	.055				5
6	.035	.048	.021	-.187						.031	.017	.062	-.163	.039					6
7	.031	.028	-.133	-.187	-.146					.017	.019	-.030	-.148						7
8		-.059	-.155							.021	-.095	-.034							8
9	-.077	-.069	-.163							-.087	-.090	-.038							9
10	-.045	.155								-.041	-.070								10
11	-.066									-.086									11
								α = 00°			δ = 30°								
1	.388	.356	.347	.344	.206			-.192									.424		1
2	.089	.072	.076	.077	-.146					.083	.070	.063	.062	.912	.773	.732			2
3	.056	.036	.028	.248	-.096		-.207			.047		.022	-.001	.641	.737	.367			3
4	.051	.035	.016	-.223	-.119		-.203			.039	.024	.013	-.162	.658	.584	.374			4
5	.042	.028	.106	.154	-.157					.023	.010	-.024	-.191	.302	.290				5
6	.038	.049	.092	-.259						.034	.017	.121	-.176	.241					6
7	.033	.071	-.116	-.254	-.170					.022	.019	.017	-.178						7
8		-.015	-.161							.025	-.089	-.002							8
9	-.074	-.039	-.183							-.085	-.065	-.016							9
10	-.038	.159								-.037	-.022								10
11	-.040									-.081									11
								α = 03°			δ = 00°								
1	.387	.307	.324	.306	.357			-.200									.063		1
2	.037	-.009	-.040	-.051	-.080	-.115				.150	.168	.162	.164	.297	.242	.251			2
3	.022	-.005	-.029	-.037	-.063	-.114	-.203			.096		.089	.083	.217	.189	.038			3
4	.019	-.005	-.032	-.062	-.067	-.107	-.200			.087	.074	.064	.049	.184	.148	.024			4
5	.005	-.013	-.021	.151	-.084	-.185				.073	.062	.027	-.062	.113	.024				5
6	.007	.013	-.019	-.133						.081	.071	.069	-.059	-.014					6
7	.002	-.005	-.120	-.131	-.157					.060	.067	-.056	-.056						7
8		-.106	-.117							.077	-.058	-.056							8
9	-.092	-.108	-.124							-.044	-.052	-.052							9
10	-.058	.157								-.012	-.055								10
11	-.086									-.044									11

[redacted]

Table 27 Continued

Pressure Coefficients on Delta Wing with Control

Configuration F M = 2.01 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
								α = 06°		δ = -30°									
1	.375	.266	.275	.245	.336			.219		.208	.232	.241	.244	-.115	-.157	-.156	-.182		1
2	-.023	-.111	-.138	-.167	.905	.525				.144		.142	.386	-.029	-.163	-.191			2
3	-.012	-.049	-.109	-.137	.629	.444	.150			.128	.121	.116	-.109	-.077	-.174	-.201			3
4	-.016	-.045	-.071	-.225	.450	.318	.109			.126	.107	.078	-.248	-.127	-.168				4
5	-.034	-.056	-.076	.160	.070	.076				.123	.116	.166	-.246	-.193					5
6	-.029	-.025	.031	-.235						.093	.119	-.051	-.228						6
7	-.031	-.042	-.078	-.235	-.028					.117	.033	-.098							7
8		-.132	-.095							-.014	.020	-.106							8
9	-.124	-.106	-.110							.013	-.007								9
10	-.073	.167								-.002									10
11	-.111																		11
								α = 06°		δ = -20°									
1	.374	.266	.275	.245	.419			-.003		.208	.233	.239	.241	-.021	-.090	-.094	-.144		1
2	-.025	-.110	-.138	-.167	.629	.292				.143		.142	.357	.035	-.091	-.145			2
3	-.012	-.048	-.113	-.110	.265	.189	-.028			.128	.123	.114	-.109	-.019	-.103	-.157			3
4	-.017	-.044	-.074	-.203	.064	.110	-.062			.125	.109	.081	-.176	-.073	-.111				4
5	-.033	-.055	-.079	.160	-.080	-.080				.123	.117	.112	-.154	-.157					5
6	-.029	-.023	.002	-.206						.094	.113	-.060	-.144						6
7	-.032	-.041	-.113	-.189	-.139					.120	-.002	-.078							7
8		-.131	-.116							-.013	-.002	-.088							8
9	-.122	-.116	-.131							.013	-.023								9
10	-.076	.168								-.007									10
11	-.111																		11
								α = 06°		δ = -10°									
1	.371	.261	.271	.240	.467			-.152		.203	.227	.232	.237	.171	.039	.019	-.068		1
2	-.027	-.112	-.139	-.166	.204	.078				.139		.136	.126	.122	.064	-.062			2
3	-.016	-.051	-.112	-.164	-.007	-.025	-.155			.123	.116	.112	-.007	.077	.045	-.071			3
4	-.019	-.047	-.075	-.178	-.147	-.053	-.166			.122	.102	.099	-.101	.027	-.045				4
5	-.038	-.057	-.075	.156	-.128	-.185				.117	.111	.097	-.096	-.089					5
6	-.032	-.027	-.031	-.180						.091	.107	-.051	-.098						6
7	-.035	-.043	-.137	-.178	-.180					.114	-.017	-.062							7
8		-.131	-.138							-.016	-.020	-.066							8
9	-.123	-.121	-.148							.009	-.031								9
10	-.083	.162								-.013									10
11	-.114																		11
								α = 06°		δ = 00°									
1	.378	.268	.278	.249	.328			-.211		.208	.233	.241	.246	.282	.244	.247	.020		1
2	-.020	-.102	-.129	-.156	-.098	-.131				.144		.144	.142	.205	.188	.006			2
3	-.010	-.044	-.103	-.138	-.085	-.128	-.217			.128	.123	.119	.104	.167	.145	-.001			3
4	-.013	-.041	-.066	-.110	-.091	-.125	-.212			.126	.109	.076	-.020	.135	-.002				4
5	-.032	-.051	-.060	.164	-.097	-.193				.123	.116	.116	-.019	-.011					5
6	-.026	-.019	-.053	-.164						.101	.113	-.021	-.016						6
7	-.030	-.038	-.145	-.164	-.158					.119	-.023	-.023							7
8		-.128	-.144							-.012	-.015	-.020							8
9	-.118	-.131	-.150							.014	-.020								9
10	-.078	.167								-.010									10
11	-.109																		11
								α = 06°		δ = 10°									
1	.375	.266	.276	.247	.341			-.213		.207	.230	.239	.242	.381	.470	.425	.127		1
2	-.021	-.106	-.130	-.155	-.143	-.166				.142		.143	.189	.351	.371	.109			2
3	-.012	-.046	-.101	-.231	-.120	-.162	-.220			.125	.121	.119	.158	.364	.298	.109			3
4	-.016	-.041	-.063	-.113	-.116	-.163	-.216			.124	.108	.076	.009	.254	.083				4
5	-.033	-.053	-.042	.164	-.124	-.208				.120	.114	.127	-.008	.085					5
6	-.027	-.021	-.071	-.148						.104	.111	.019	-.069						6
7	-.031	-.028	-.171	-.152	-.164					.112	-.024	.027							7
8		-.113	-.179							-.017	-.023	.027							8
9	-.119	-.127	-.178							.015	-.020								9
10	-.078	.167								-.013									10
11	-.105																		11

[redacted]

Table 27 Continued

Pressure Coefficients on Delta Wing with Control

Configuration F M = 2.01 R = 4.2 x 10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
								α = 06°			δ = 20°									
1	.375	.265	.272	.245	.275	-.205		-.225			.206	.227	.235	.239	.682	.691	.660	.354		1
2	-.023	-.109	-.134	-.160	-.191	-.199	-.236				.141		.137	.051	.593	.664	.303			2
3	-.013	-.048	-.106	.562	-.172	-.209	-.232				.125	.120	.113	.168	.792	.548	.313			3
4	-.017	-.045	-.070	-.249	-.157	-.235					.124	.105	.071	-.013	.434	.261				4
5	-.034	-.055	.066	.159	-.170						.121	.112	.124	-.075	.243					5
6	-.028	-.024	-.070	-.248							.103	.107	.069	-.105						6
7	-.032	.016	-.195	-.231	-.193						.110	-.028	.071							7
8		-.088	-.187								-.019	-.027	.060							8
9	-.121	-.114	-.204								.014	-.005								9
10	-.073	.166									-.016									10
11	-.081																			11
								α = 06°			δ = 30°									
1	.371	.263	.271	.242	.148			-.243			.203	.227	.233	.236	.960	.955	.838	.616		1
2	-.026	-.111	-.141	-.167	-.226	-.234					.139		.135	.050	.857	.936	.577			2
3	-.016	-.051	-.112	.159	-.208	-.231	-.256				.123	.118	.111	.162	.694	.771	.605			3
4	-.019	-.047	-.072	-.243	-.201	-.241	-.253				.124	.102	.067	-.058	.686	.537				4
5	-.037	-.059	.117	.158	-.207	-.258					.117	.109	.202	-.130	.494					5
6	-.032	-.023	-.040	-.228							.101	.104	.119	-.149						6
7	-.035	.069	-.193	-.198	-.224						.106	-.031	.101							7
8		-.079	-.221								-.026	.003	.091							8
9	-.102	-.111	-.232								.014	.064								9
10	-.010	.164									-.015									10
11	-.023																			11
								α = 09°			δ = 00°									
1	.353	.223	.226	.187	.288			-.188			.271	.303	.316	.320	.301	.274	.263	-.023		1
2	-.080	-.160	-.198	-.217	-.079	-.097					.193		.211	.205	.219	.214	-.015			2
3	-.040	-.099	-.170	-.222	-.084	-.108	-.195				.178	.182	.177	.166	.181	.173	-.011			3
4	-.039	-.073	-.143	-.207	-.103	-.121	-.190				.177	.163	.132	.020	.166	-.024				4
5	-.061	-.078	-.096	.177	-.116	-.194					.171	.171	.170	.026	.006					5
6	-.053	-.046	-.091	-.219							.148	.165	.019	.025						6
7	-.057	-.063	-.167	-.217	-.152						.167	.018	.020							7
8		-.139	-.173								.028	.023	.020							8
9	-.132	-.148	-.177								.062	.019								9
10	-.092	.184									.030									10
11	-.123																			11
								α = 12°			δ = -30°									
1	.324	.171	.160	.124	.351			.114			.350	.381	.389	.393	-.096	-.132	-.117	-.167		1
2	-.145	-.225	-.257	-.270	.958	.434					.255		.283	.556	.026	-.157	-.169			2
3	-.070	-.163	-.222	-.283	.771	.311	.054				.236	.249	.248	-.005	-.052	-.119	-.184			3
4	-.066	-.100	-.201	-.298	.594	.142	.003				.239	.224	.196	-.218	-.119	-.138				4
5	-.088	-.107	-.143	.219	-.210	-.085					.229	.237	.287	-.203	-.205					5
6	-.084	-.076	-.064	-.290							.196	.234	.049	-.157						6
7	-.084	-.095	-.147	-.274	-.216						.224	.125	.006							7
8		-.155	-.198								.073	.105	-.019							8
9	-.159	-.123	-.214								.087	.076								9
10	-.109	.229									.096									10
11	-.134																			11
								α = 12°			δ = -20°									
1	.324	.170	.162	.123	.458			-.113			.349	.380	.388	.394	.134	.015	.027	-.087		1
2	-.144	-.224	-.257	-.269	.658	.185					.254		.284	.437	.145	-.022	-.073			2
3	-.069	-.160	-.222	-.289	.309	.052	-.121				.235	.250	.247	.004	.066	.099	-.091			3
4	-.065	-.099	-.203	-.294	-.034	-.045	-.148				.240	.225	.222	-.105	-.028	-.051				4
5	-.088	-.106	-.139	.219	-.239	-.196					.230	.237	.238	-.082	-.137					5
6	-.082	-.075	-.087	-.267							.196	.232	.046	-.070						6
7	-.084	-.094	-.165	-.230	-.240						.224	.093	.020							7
8		-.152	-.202								.073	.084	.004							8
9	-.153	-.131	-.218								.088	.064								9
10	-.110	.228									.085									10
11	-.135																			11

[redacted]

Table 27 Continued

Pressure Coefficients on Delta Wing with Control

Configuration F M = 2.01 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 12°									δ = -10°									
1	.324	.181	.162	.124	.525			-.214		.351	.380	.388	.393	.316	.224	.228	.042		1
2	-.142	-.221	-.257	-.267	.270	-.018				.257		.282	.357	.266	.208	.040			2
3	-.068	-.160	-.221	-.282	-.055	-.107	-.207			.238	.251	.248	.106	.205	.163	.028			3
4	-.062	-.095	-.202	-.273	-.248	-.151	-.212			.241	.226	.240	-.031	.105	.045				4
5	-.085	-.102	-.132	.220	-.234	-.236				.232	.239	.237	-.016	-.040					5
6	-.080	-.071	-.121	-.238						.197	.234	.049	-.021						6
7	-.081	-.089	-.198	-.210	-.240					.224	.078	.028							7
8		-.145	-.189							.073	.080	.022							8
9	-.151	-.143	-.210							.088	.067								9
10	-.112	.228								.084									10
11	-.133																		11
	α = 12°									δ = 00°									
1	.320	.174	.157	.121	.195			-.217		.346	.376	.385	.388	.423	.391	.388	.107		1
2	-.144	-.226	-.259	-.270	-.182	-.185				.253		.280	.278	.342	.334	.095			2
3	-.071	-.164	-.225	-.272	-.167	-.183	-.225			.234	.247	.242	.237	.304	.286	.103			3
4	-.067	-.103	-.205	-.259	-.175	-.193	-.220			.238	.222	.190	.071	.279	.086				4
5	-.089	-.110	-.145	.216	-.184	-.234				.227	.233	.232	.080	.091					5
6	-.084	-.078	-.152	-.264						.195	.222	.070	.078						6
7	-.087	-.096	-.204	-.216	-.185					.217	.059	.069							7
8		-.159	-.211							.070	.067	.069							8
9	-.157	-.168	-.209							.087	.062								9
10	-.116	.223								.074									10
11	-.138																		11
	α = 12°									δ = 10°									
1	.321	.169	.160	.124	.262			-.234		.347	.378	.386	.390	.631	.611	.571	.279		1
2	-.144	-.223	-.257	-.248	-.206	-.215				.254		.280	.306	.566	.553	.249			2
3	-.070	-.162	-.221	-.284	-.193	-.212	-.240			.234	.249	.244	.346	.494	.479	.257			3
4	-.065	-.099	-.189	-.274	-.206	-.224	-.236			.239	.224	.191	.150	.439	.218				4
5	-.089	-.106	-.139	.218	-.212	-.251				.229	.236	.241	.106	.245					5
6	-.083	-.073	-.129	-.248						.203	.225	.113	.035						6
7	-.084	-.053	-.224	-.234	-.207					.216	.063	.131							7
8		-.149	-.205							.069	.063	.128							8
9	-.153	-.163	-.197							.087	.067								9
10	-.109	.225								.075									10
11	-.114																		11
	α = 12°									δ = 20°									
1	.321	.167	.159	.123	.202			-.239		.346	.377	.382	.390	.736	.872	.761	.501		1
2	-.143	-.226	-.259	-.251	-.228	-.231				.254		.280	.149	.725	.827	.462			2
3	-.070	-.162	-.225	.423	-.213	-.230	-.247			.234	.248	.244	.403	.764	.705	.494			3
4	-.067	-.101	-.102	-.280	-.227	-.240	-.242			.240	.222	.189	.128	.615	.428				4
5	-.089	-.107	-.099	.217	-.235	-.257				.229	.233	.246	.019	.522					5
6	-.084	-.049	-.135	-.256						.198	.223	.177	-.051						6
7	-.084	-.028	-.243	-.241	-.224					.215	.062	.182							7
8		-.131	-.227							.065	.060	.164							8
9	-.135	-.166	-.174							.087	.094								9
10	-.054	.226								.074									10
11	-.074																		11
	α = 12°									δ = 30°									
1	.317	.164	.152	.114	.067			-.241		.340	.371	.377	.383	1.061	1.146	.921	.787		1
2	-.150	-.232	-.266	-.242	-.248	-.239				.249		.273	.141	1.003	1.141	.851			2
3	-.077	-.170	-.228	.208	-.231	-.239	-.251			.228	.240	.236	.437	.979	.873	.838			3
4	-.075	-.107	-.061	-.299	-.246	-.250	-.243			.232	.214	.181	.109	.889	.819				4
5	-.095	-.114	-.012	.209	-.253	-.261				.223	.225	.356	-.051	.835					5
6	-.090	.056	-.144	-.191						.195	.215	.237	-.077						6
7	-.090	-.016	-.245	-.200	-.243					.207	.056	.217							7
8		-.135	-.228							.056	.114	.207							8
9	-.028	-.162	-.210							.083	.171								9
10	.008	.219								.064									10
11	-.051																		11

[redacted]

Table 27 Concluded

Pressure Coefficients on Delta Wing with Control

Configuration F $M = 2.01$ $R = 4.2 \times 10^6$

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
	$\alpha = 15^\circ$										$\delta = 00^\circ$									
1	.294	.117	.066	.043	.188			-.053			.393	.451	.451	.444	.383	.358	.346	.052		1
2	-.190	-.257	-.284	-.288	.141	.036					.315		.348	.343	.343	.320	.054			2
3	-.094	-.235	-.263	-.294	.146	.005	-.102				.300	.312	.307	.307	.301	.287	.068			3
4	-.091	-.131	-.228	-.285	.023	-.081	-.114				.304	.285	.254	.123	.259	.066				4
5	-.118	-.137	-.180	.257	-.228	-.178					.288	.300	.297	.130	.085					5
6	-.110	-.102	-.181	-.265							.240	.282	.117	.127						6
7	-.112	-.124	-.227	-.253	-.230						.280	.106	.111							7
8		-.179	-.228								.118	.113	.113							8
9	-.176	-.183	-.234								.127	.107								9
10	-.138	.274									.121									10
11	-.152																			11

[redacted]

Table 28

Pressure Coefficients on Delta Wing with Control

Configuration G M = 2.01 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 00°									δ = 00°									
1	.369	.333	.330	.329	.233	.319	.217			.064	.058	.050	.050	.039	.029	.024			1
2	.063	.047	.055	.052	.090	.058	.052			.029		.003	.003	.020	.006	-.121			2
3	.029	.015	.013	.003	.031	.023	-.118			.017	.008	-.003	-.019	.005	-.013	-.136			3
4	.024	.014	-.006	-.025	.021	.097	-.120			.004	-.003	-.037	-.116	-.016	-.133				4
5	.013	.006	-.025	.107	-.011	-.127				.013	.004	.007	-.115	-.121					5
6	.013	.030	.006	-.114	-.106					-.003	.006	-.106	-.111	-.122					6
7	.010	.008	-.106	-.117	-.097					.004	-.101	-.109							7
8		-.101	-.110							-.096	-.097	-.107							8
9	-.093	-.102	-.116							-.063	-.101								9
10	-.063	.114								-.101									10
11	-.088																		11
	α = 00°									δ = 10°									
1	.370	.334		.330	-.007	.261	.216			.064			.052	.191	.249	.262	-.027		1
2	.064	.050		.057	-.013	-.108	-.135			.029			.051	.178	.173	-.030			2
3	.031	.016		.034	-.016	-.098	-.178			.019			.017	.127	.120	-.047			3
4	.025	.014		-.082	-.025	.089	-.180			.005			-.110	.034	-.073				4
5	.015	.009		.118	-.065	-.162				.013			-.134	-.075					5
6	.014	.031		-.149	-.137					.000			-.125	-.082					6
7	.012	.011		-.154	-.125					.015									7
8		-.092								-.097									8
9	-.092	-.096								-.060									9
10	-.065	.123								-.102									10
11	-.086																		11
	α = 00°									δ = 20°									
1	.370	.335	.331	.330	-.093	.093	.170			.063	.057	.050	.049	.505	.469	.483	.152		1
2	.063	.050	.059	.059	-.110	-.169	-.192			.027		.004	-.012	.316	.417	.090			2
3	.030	.016	.016	.439	-.052	-.160	-.209			.020	.009	-.002	-.010	.388	.304	.092			3
4	.027	.015	-.002	-.209	-.080	.120	-.209			.003	-.004	-.040	-.185	.178	.034				4
5	.016	.008	-.017	.162	-.115	-.205				.012	.002	.006	-.177	-.008					5
6	.013	.032	.048	-.207	-.166					.003	.006	-.042	-.200	.001					6
7	.012	.012	-.123	-.211	-.151					.005	-.103	-.028							7
8		-.069	-.158							-.102	-.103	-.034							8
9	-.095	-.068	-.178							-.054	-.099								9
10	-.067	.171								-.105									10
11	-.082																		11
	α = 00°									δ = 30°									
1	.369	.335	.331	.331	-.164	-.041	.118			.063	.057	.050	.048	.840	.771	.749	.428		1
2	.064	.051	.059	.058	-.184	-.215	-.230			.027		.003	-.017	.649	.789	.297			2
3	.031	.016	.016	-.006	-.126	-.207	-.230			.021	.008	-.002	-.086	.581	.613	.350			3
4	.027	.014	-.002	-.263	-.143	.147	-.230			.003	-.005	-.040	-.239	.552	.242				4
5	.015	.008	-.020	.188	-.154	-.238				.012	.001	-.001	-.213	.129					5
6	.014	.031	.130	-.266	-.198					.003	.004	.008	-.211	.192					6
7	.013	.045	-.078	-.275	-.181					.000	-.104	.006							7
8		-.013	-.152							-.103	-.104	-.011							8
9	-.096	-.031	-.185							-.049	-.060								9
10	-.063	.198								-.106									10
11	-.054																		11
	α = 03°									δ = 00°									
1	.382	.271	.316	.299	.039	.295	.252			.137	.158	.155	.165	.193	.199	.183	-.033		1
2	.021	-.023	-.045	-.053	-.040	-.084	-.100			.085		.084	.080	.190	.143	-.015			2
3	.008	-.022	-.033	-.034	-.062	-.088	-.185			.074	.066	.062	.048	.146	.135	-.045			3
4	.008	-.021	-.035	-.060	-.053	.138	-.171			.067	.056	.028	-.060	.091	-.025				4
5	-.009	-.023	-.046	.163	-.095	-.168				.066	.062	.063	-.057	-.036					5
6	-.005	-.002	-.017	-.128	-.193					.051	.060	-.057	-.055	-.027					6
7	-.010	-.014	-.119	-.128	-.076					.058	-.058	-.058							7
8		-.113	-.115							-.052	-.055	-.053							8
9	-.106	-.113	-.122							-.021	-.058								9
10	-.070	.160								-.062									10
11	-.098																		11

[redacted]

Table 28 Continued

Pressure Coefficients on Delta Wing with Control

Configuration G M = 2.01 R = 4.2×10^6

Orif	Upper Surface at Station										Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9		1	2	3	4	5	6	7	8	9	
	α = 06°										δ = -30°									
1	.373	.229	.271	.240	.624	-.031	.013				.199	.225	.235	.242	-.012	-.099	-.123	-.163		1
2	-.032	-.114	-.132	-.157	.883	.567	.570				.136		.140	.045	.023	-.117	-.133			2
3	-.020	-.052	-.104	-.134	.668	.417	.126				.120	.117	.116	-.143	-.026	-.088	-.171			3
4	-.024	-.051	-.068	-.202	.407	.186	.138				.118	.102	.075	-.199	-.081	-.133				4
5	-.041	-.060	-.072	.157	-.034	.027					.113	.110	.229	-.214	-.165					5
6	-.038	-.030	.006	-.213	-.155						.084	.108	-.002	-.221	-.151					6
7	-.040	-.047	-.070	-.209	-.020						.107	.027	-.066							7
8		-.134	-.077								-.015	.040	-.097							8
9	-.130	-.124	-.091								.010	.012								9
10	-.083	.155									-.019									10
11	-.118																			11
	α = 06°										δ = -20°									
1	.372	.229	.273	.242	.525	.108	.095				.198	.225	.235	.240	.100	.003	-.029	-.112		1
2	-.031	-.110	-.130	-.156	.503	.249	.282				.137		.139	.424	.106	-.013	-.079			2
3	-.020	-.048	-.103	-.127	.195	.132	-.084				.119	.118	.116	-.028	.062	.018	-.113			3
4	-.024	-.048	-.067	-.173	.082	.146	-.089				.119	.103	.075	-.160	-.019	-.068				4
5	-.041	-.057	-.068	.149	-.131	-.122					.113	.109	.134	-.146	-.113					5
6	-.038	-.027	.009	-.168	-.175						.084	.107	-.045	-.140	-.098					6
7	-.040	-.044	-.100	-.178	-.083						.105	-.007	-.066							7
8		-.130	-.112								-.013	.003	-.071							8
9	-.125	-.120	-.116								.009	-.016								9
10	-.082	.148									-.022									10
11	-.117																			11
	α = 06°										δ = -10°									
1	.375	.232	.275	.243	.411	.191	.169				.203	.227	.234	.242	.178	.126	.082	-.042		1
2	-.025	-.110	-.130	-.154	.191	.069	.090				.139		.140	.131	.179	.108	-.013			2
3	-.014	-.048	-.102	-.142	.002	-.033	-.163				.122	.119	.116	.008	.160	.129	-.044			3
4	-.019	-.047	-.066	-.143	-.110	.134	-.167				.121	.104	.096	-.088	.061	-.012				4
5	-.037	-.057	-.058	.153	-.152	-.176					.116	.109	.102	-.084	-.060					5
6	-.033	-.026	-.020	-.163	-.181						.086	.108	-.038	-.090	-.044					6
7	-.035	-.043	-.108	-.158	-.092						.107	-.017	-.047							7
8		-.130	-.130								-.013	-.017	-.052							8
9	-.123	-.119	-.142								.012	-.029								9
10	-.082	.152									-.024									10
11	-.114																			11
	α = 06°										δ = 00°									
1	.375	-.111			-.083	.256	.239				.203			.239	.277	.296	.274	.048		1
2	-.023	-.048			-.129	-.169	-.179				.139			.137	.279	.228	.065			2
3	-.014	-.048			-.120	-.154	-.197				.123			.099	.212	.214	.023			3
4	-.017	-.058			-.109	.141	-.198				.121			-.024	.159	.041				4
5	-.036	-.026		.172	-.117	-.198					.116			-.021	.008					5
6	-.032	-.042		-.162	-.167						.094			-.018	.026					6
7	-.034	-.132		-.166	-.087						.105									7
8		-.132									-.017									8
9	-.123	.174									.021									9
10	-.086										-.033									10
11	-.113																			11
	α = 06°										δ = 10°									
1	.369	.243	.293	.264	-.088	.172	.202				.205	.242	.255	.257	.290	.458	.421	.114		1
2	-.019	-.086	-.104	-.133	-.131	-.179	-.196				.145		.158	.123	.353	.371	.089			2
3	-.010	-.027	-.080	-.035	-.113	-.167	-.204				.130	.137	.136	.192	.400	.283	.074			3
4	-.012	-.025	-.045	-.105	-.095	.161	-.206				.129	.124	.093	.027	.277	.069				4
5	-.029	-.034	-.020	.207	-.112	-.203					.125	.128	.114	.033	.062					5
6	-.024	-.002	-.043	-.131	-.153						.110	.125	.028	-.011	.059					6
7	-.027	-.011	-.131	-.141	-.070						.119	-.005	.046							7
8		-.087	-.154								-.003	-.007	.052							8
9	-.109	-.096	-.165								.040	-.010								9
10	-.074	.206									-.016									10
11	-.092																			11

[redacted]

Table 28 Continued

Pressure Coefficients on Delta Wing with Control

Configuration G M = 2.01 R = 4.2×10^6

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	α = 06°									δ = 20°									
1	.368	.241	.288	.257	-.131	.044	.159										.335		1
2	-.021	-.090	-.109	-.139	-.165	-.204	-.220			.203	.238	.248	.250	.548	.717	.683			2
3	-.011	-.030	-.084	.120	-.148	-.196	-.220			.144		.151	.059	.455	.656	.239			3
4	-.013	-.028	-.049	-.242	-.117	.229	-.221			.128	.133	.129	.311	.472	.555	.275			4
5	-.032	-.037	.110	.282	-.135	-.222				.128	.119	.087	-.039	.590	.216				5
6	-.026	-.005	.013	-.203	-.172					.123	.122	.096	-.013	.203					6
7	-.029	.046	-.156	-.138	-.083					.110	.122	.055	-.094	.217					7
8		-.046	-.189							.113	-.009	.101							8
9	-.113	-.073	-.185							-.012	-.011	.089							9
10	-.065	.283								.046	-.016								10
11	-.052									-.021									11
	α = 06°									δ = 30°									
1	.373	.231	.273	.242	-.167	-.037	.124										.619		1
2	-.027	-.112	-.128	-.152	-.195	-.217	-.229			.198	.223	.231	.238	.849	.934	.871			2
3	-.018	-.050	-.100	.008	-.177	-.210	-.224			.135		.135	.058	.630	.979	.522			3
4	-.021	-.049	-.066	-.276	-.148	.240	-.225			.118	.114	.112	.273	.639	.809	.555			4
5	-.040	-.059	.190	.284	-.166	-.231				.117	.100	.070	-.049	.983	.462				5
6	-.035	-.025	.031	-.173	-.192					.111	.103	.084	-.060	.428					6
7	-.038	.082	-.136	-.173	-.104					.098	.103	.116	-.132	.486					7
8		-.059	-.197							.097	-.030	.112							8
9	-.087	-.078	-.218							-.032	-.029	.105							9
10	.015	.288								.034	.027								10
11	.010									-.031									11
	α = 09°									δ = 00°									
1	.358	.196	.224	.184	-.017	.182	.202										.055		1
2	-.083	-.173	-.196	-.209	-.043	-.110	-.134			.272	.302	.314	.314	.300	.342	.322			2
3	-.043	-.110	-.164	-.213	-.058	-.110	-.158			.193		.208	.203	.272	.274	.043			3
4	-.042	-.081	-.132	-.199	-.087	.148	-.161			.178	.178	.174	.166	.268	.225	.029			4
5	-.064	-.087	-.084	.185	-.141	-.191				.178	.158	.130	.023	.206	.030				5
6	-.059	-.058	-.089	-.207	-.179					.170	.161	.168	.026	.034					6
7	-.062	-.070	-.158	-.209	-.095					.143	.159	.020	.028	.029					7
8		-.144	-.164							.157	.013	.021							8
9	-.141	-.149	-.164							.027	.016	.021							9
10	-.100	.188								.058	.012								10
11	-.130									.012									11
	α = 12°									δ = -30°									
1	.325	.164	.168	.131	.641	-.054	.034										-.149		1
2	-.137	-.213	-.238	-.249	.925	.476	.421			.354	.389	.396	.397	.050	-.079	-.096			2
3	-.064	-.156	-.207	-.255	.769	.298	.021			.261		.291	.163	.096	-.105	-.106			3
4	-.062	-.090	-.175	-.270	.461	.189	.003			.242	.257	.254	.207	.005	-.028	-.155			4
5	-.081	-.096	-.129	.193	-.171	-.107				.249	.234	.202	-.131	-.041	-.095				5
6	-.077	-.067	-.057	-.259	-.223					.239	.246	.349	-.195	-.160					6
7	-.076	-.083	-.134	-.246	-.113					.201	.238	.087	-.181	-.146					7
8		-.142	-.174							.228	.138	.034							8
9	-.143	-.117	-.192							.089	.134	.015							9
10	-.102	.202								.088	.102								10
11	-.125									.096									11
	α = 12°									δ = -20°									
1	.324	.148	.152	.119	.541	.073	.125										-.076		1
2	-.156	-.235	-.254	-.259	.620	.192	.177			.348	.376	.381	.386	.208	.056	.039			2
3	-.080	-.176	-.220	-.269	.314	.062	-.136			.252		.277	.477	.210	.040	-.019			3
4	-.078	-.112	-.188	-.284	.135	.163	-.148			.232	.241	.240	.110	.103	.149	-.070			4
5	-.099	-.117	-.140	.179	-.231	-.195				.238	.216	.191	-.111	-.015	-.017				5
6	-.095	-.088	-.077	-.250	-.233					.227	.228	.251	-.094	-.098					6
7	-.095	-.103	-.164	-.226	-.120					.188	.221	.052	-.087	-.076					7
8		-.164	-.195							.214	.093	.034							8
9	-.165	-.137	-.204							.072	.082	.015							9
10	-.124	.184								.069	.063								10
11	-.149									.072									11

[redacted]

Table 28 Continued

Pressure Coefficients on Delta Wing with Control

Configuration G $M = 2.01$ $R = 4.2 \times 10^6$

Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	$\alpha = 12^\circ$									$\delta = -10^\circ$									
1	.328	.164	.166	.130	.362	.110	.194			.356	.387	.393	.395	.329	.267	.221	.072		1
2	-.135	-.215	-.240	-.246	.324	.005	-.008			.264		.290	.310	.377	.250	.126			2
3	-.063	-.157	-.206	-.243	.050	-.091	-.195			.245	.256	.253	.095	.263	.286	.067			3
4	-.061	-.092	-.174	-.271	-.102	.167	-.199			.250	.231	.230	-.048	.109	.113				4
5	-.080	-.098	-.116	.192	-.222	-.222				.242	.242	.238	-.040	.013					5
6	-.076	-.067	-.085	-.228	-.224					.202	.238	.067	-.042	.060					6
7	-.076	-.084	-.160	-.204	-.109					.227	.095	.050							7
8		-.143	-.178							.089	.085	.034							8
9	-.141	-.128	-.195							.088	.071								9
10	-.104	.201								.089									10
11	-.127																		11
	$\alpha = 12^\circ$									$\delta = 00^\circ$									
1	.325	.149	.152	.118	-.116	.100	.191			.346	.375	.380	.383	.359	.386	.379	.084		1
2	-.150	-.223	-.244	-.252	-.143	-.183	-.208			.251		.275	.273	.321	.321	.063			2
3	-.077	-.170	-.218	-.257	-.138	-.175	-.200			.231	.239	.238	.235	.287	.270	.058			3
4	-.077	-.110	-.186	-.254	-.142	.188	-.204			.235	.214	.186	.074	.250	.056				4
5	-.096	-.116	-.132		-.174	.222				.226	.225	.226	.077	.071					5
6	-.092	-.086	-.155	-.243	-.202					.192	.216	.067	.082	.060					6
7	-.094	-.100	-.201	-.208	-.115					.210	.056	.064							7
8		-.164	-.206							.068	.058	.066							8
9	-.166	-.168	-.201							.078	.055								9
10	-.130	.230								.059									10
11	-.146																		11
	$\alpha = 12^\circ$									$\delta = 10^\circ$									
1	.324	.150	.150	.115	-.148	.000	.153			.348	.375	.382	.382	.482	.601	.561	.232		1
2	-.154	-.235	-.255	-.246	-.178	.204	-.224			.253		.275	.149	.473	.537	.172			2
3	-.077	-.178	-.223	-.113	-.170	-.198	-.212			.232	.239	.238	.372	.536	.450	.194			3
4	-.078	-.113	-.186	-.272	-.165	.216	-.214			.239	.214	.184	.166	.435	.172				4
5	-.098	-.119	-.131	.257	-.195	-.232				.228	.225	.198	.141	.212					5
6	-.094	-.088	-.101	-.239	-.213					.200	.216	.091	.076	.170					6
7	-.095	-.054	-.213	-.225	-.123					.215	.053	.120							7
8		-.156	-.222							.059	.050	.131							8
9	-.167	-.166	-.203							.087	.043								9
10	-.121	.265								.051									10
11	-.112																		11
	$\alpha = 12^\circ$									$\delta = 20^\circ$									
1	.324	.152	.150	.116	-.179	-.069	.144			.348	.376	.382	.383	.674	.909	.812	.537		1
2	-.155	-.237	-.259	-.246	-.204	-.225	-.243			.252		.275	.145	.708	.903	.415			2
3	-.078	-.178	-.224	.155	-.194	-.220	-.230			.232	.240	.238	.478	.695	.750	.475			3
4	-.077	-.113	-.113	-.284	-.176	.322	-.232			.238	.215	.183	.176	.782	.406				4
5	-.098	-.120	-.098	.375	-.217	-.246				.228	.224	.190	.105	.450					5
6	-.094	-.072	-.118	-.253	-.224					.203	.216	.121	-.019	.440					6
7	-.095	.006	-.203	-.224	-.121					.212	.054	.187							7
8		-.128	-.227							.050	.049	.185							8
9	-.133	-.155	-.211							.107	.041								9
10	-.033	.381								.043									10
11	-.048																		11
	$\alpha = 12^\circ$									$\delta = 30^\circ$									
1	.327	.170	.168	.131	-.186	-.103	.149			.356	.389	.395	.396	1.003	1.182	1.000	.832		1
2	-.135	-.214	-.238	-.113	-.207	-.227	-.242			.263		.290	.159	1.005	1.214	.841			2
3	-.062	-.154	-.181	-.176	-.192	-.224	-.229			.245	.257	.253	.591	.862	.968	.803			3
4	-.062	-.091	-.047	-.254	-.165	.345	-.229			.252	.232	.198	.237	1.137	.803				4
5	-.079	-.095	-.062	.400	-.215	-.242				.242	.242	.207	.038	.834					5
6	-.075	.103	-.071	-.234	-.216					.220	.234	.228	-.051	.815					6
7	-.074	.058	-.156	-.178	-.098					.222	.075	.259							7
8		-.083	-.209							.069	.071	.272							8
9	.026	-.106	-.167							.129	.127								9
10	.062	.405								.062									10
11	.005																		11

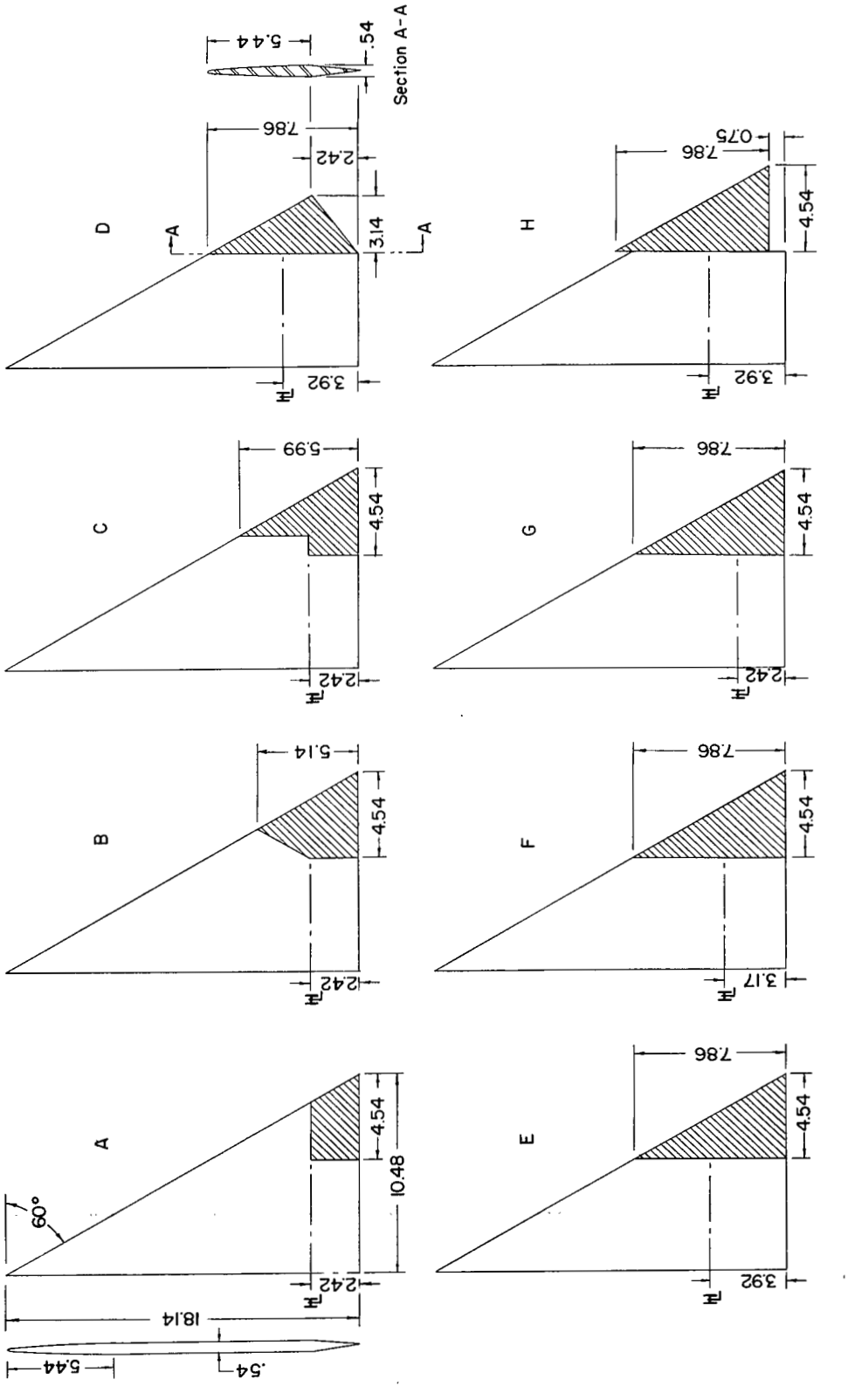
Table 28 Concluded

Pressure Coefficients on Delta Wing with Control.

Configuration G $M = 2.01$ $R = 4.2 \times 10^6$

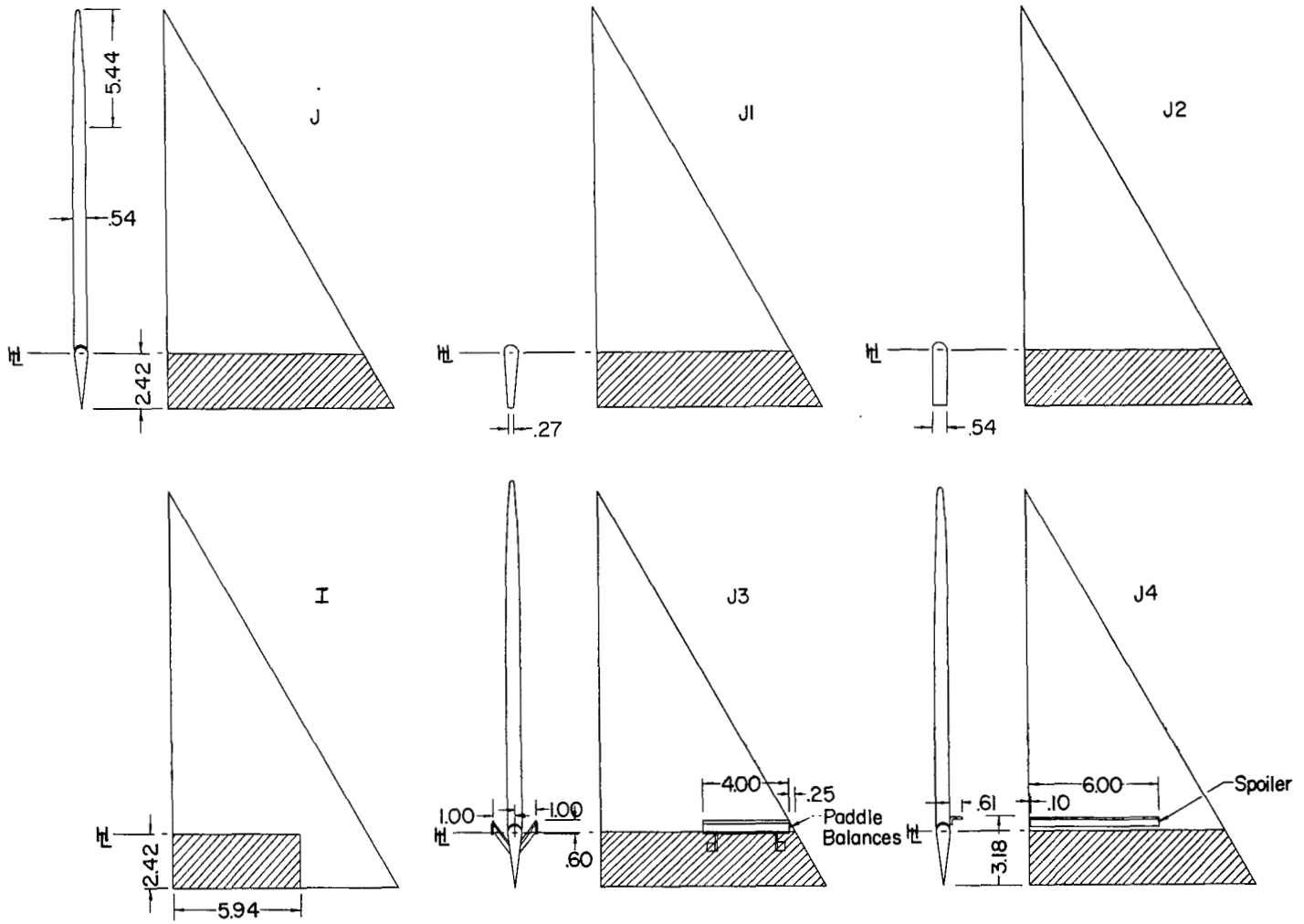
Orif	Upper Surface at Station									Lower Surface at Station									Orif
	1	2	3	4	5	6	7	8	9	1	2	3	4	5	6	7	8	9	
	$\alpha = 15^\circ$									$\delta = 00^\circ$									
1	.297	.112	.064	.049	-.075	-.004	.177			.397	.450	.451	.446	.451	.461	.453	.149		1
2	-.195	-.259	-.273	-.271	-.105	-.151	-.179			.317		.346	.336	.410	.404	.114			2
3	-.098	-.239	-.251	-.276	-.100	-.154	-.175			.304	.308	.307	.317	.375	.349	.121			3
4	-.095	-.138	-.217	-.272	-.131	.246	-.182			.306	.282	.250	.134	.332	.119				4
5	-.121	-.142	-.177	.286	-.207	-.218				.292	.296	.293	.139	.140					5
6	-.116	-.112	-.181	-.238	-.235					.241	.280	.121	.141	.123					6
7	-.116	-.128	-.221	-.210	-.091					.277	.103	.116							7
8		-.181	-.220							.123	.105	.121							8
9	-.182	-.185	-.222							.124	.104								9
10	-.149	.293								.112									10
11	-.156																		11

[redacted]



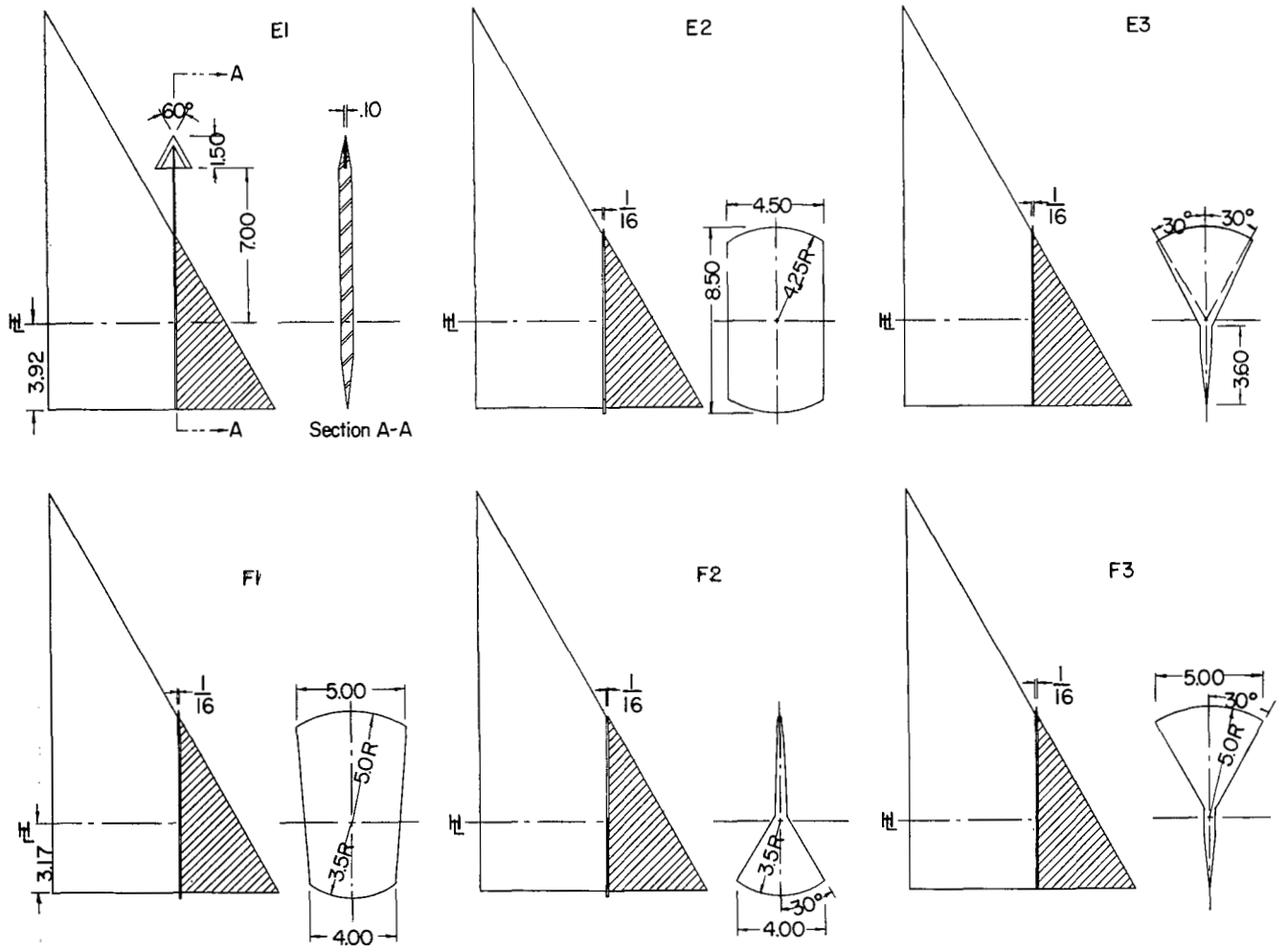
(a) Tip-control configurations.

Figure 1.- Dimensional sketches of test configurations. (All dimensions are in inches.)



(b) Trailing-edge-control configurations.

Figure 1.- Continued.



(c) Tab and fence configurations.

Figure 1.- Concluded.

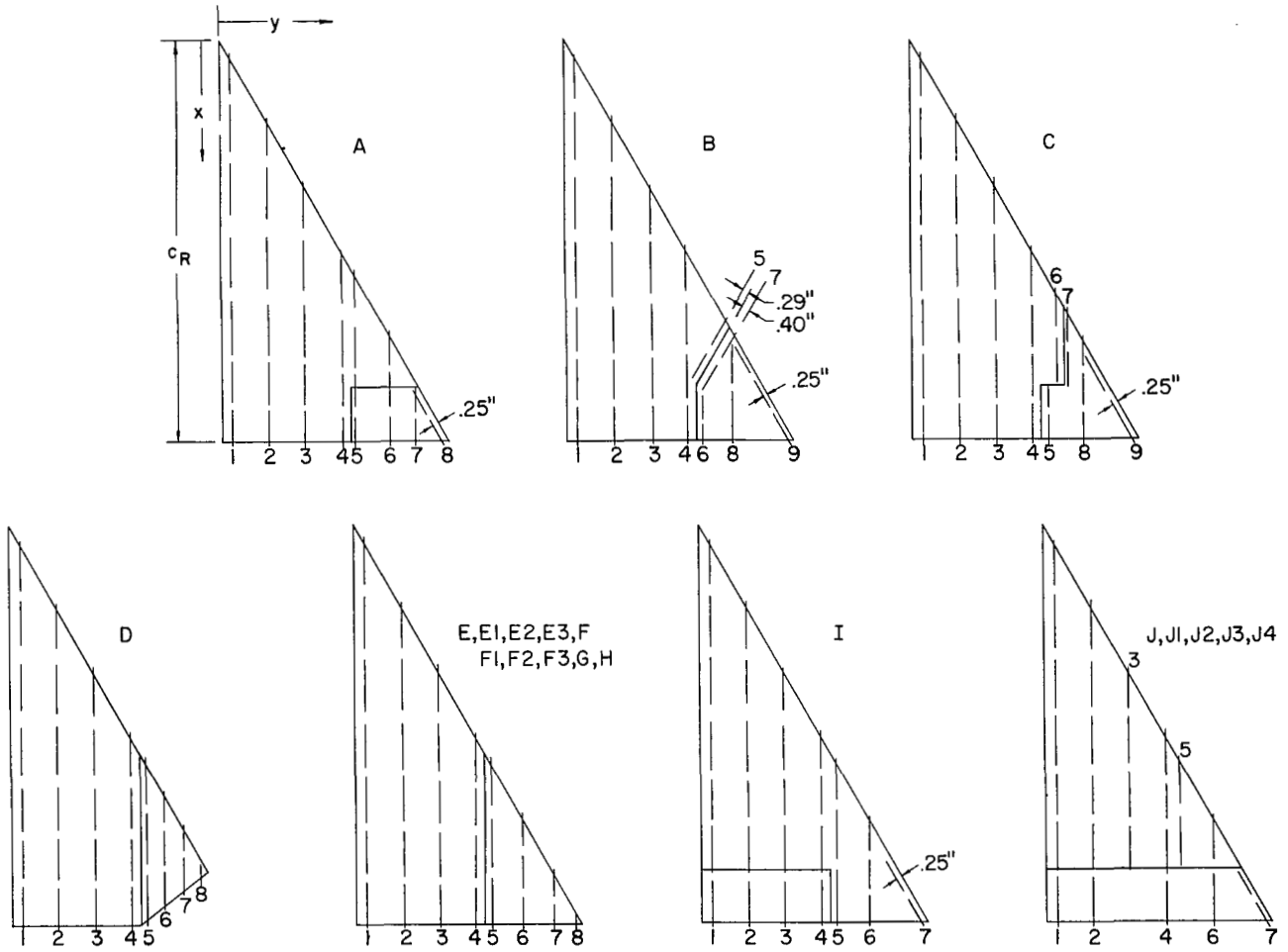
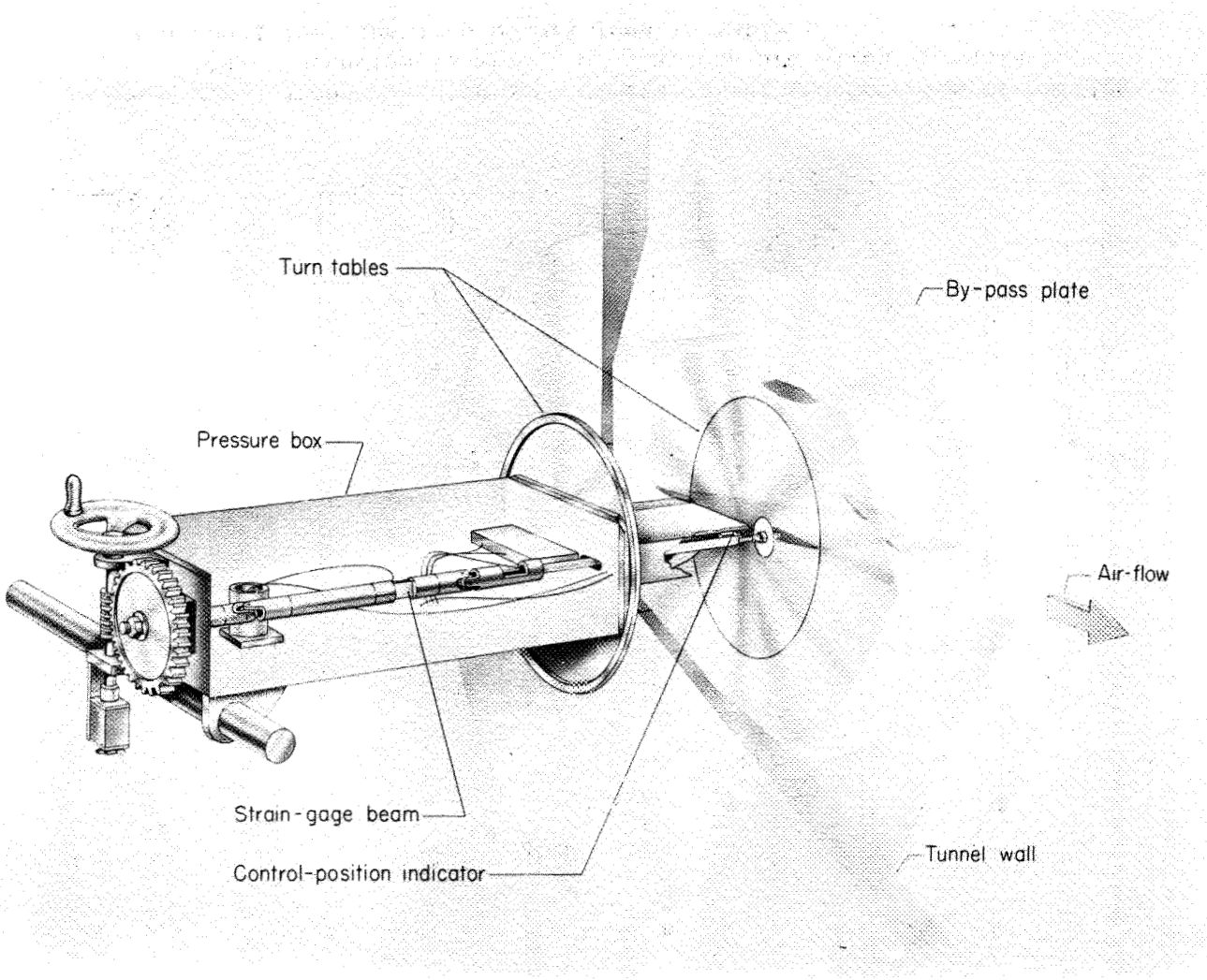
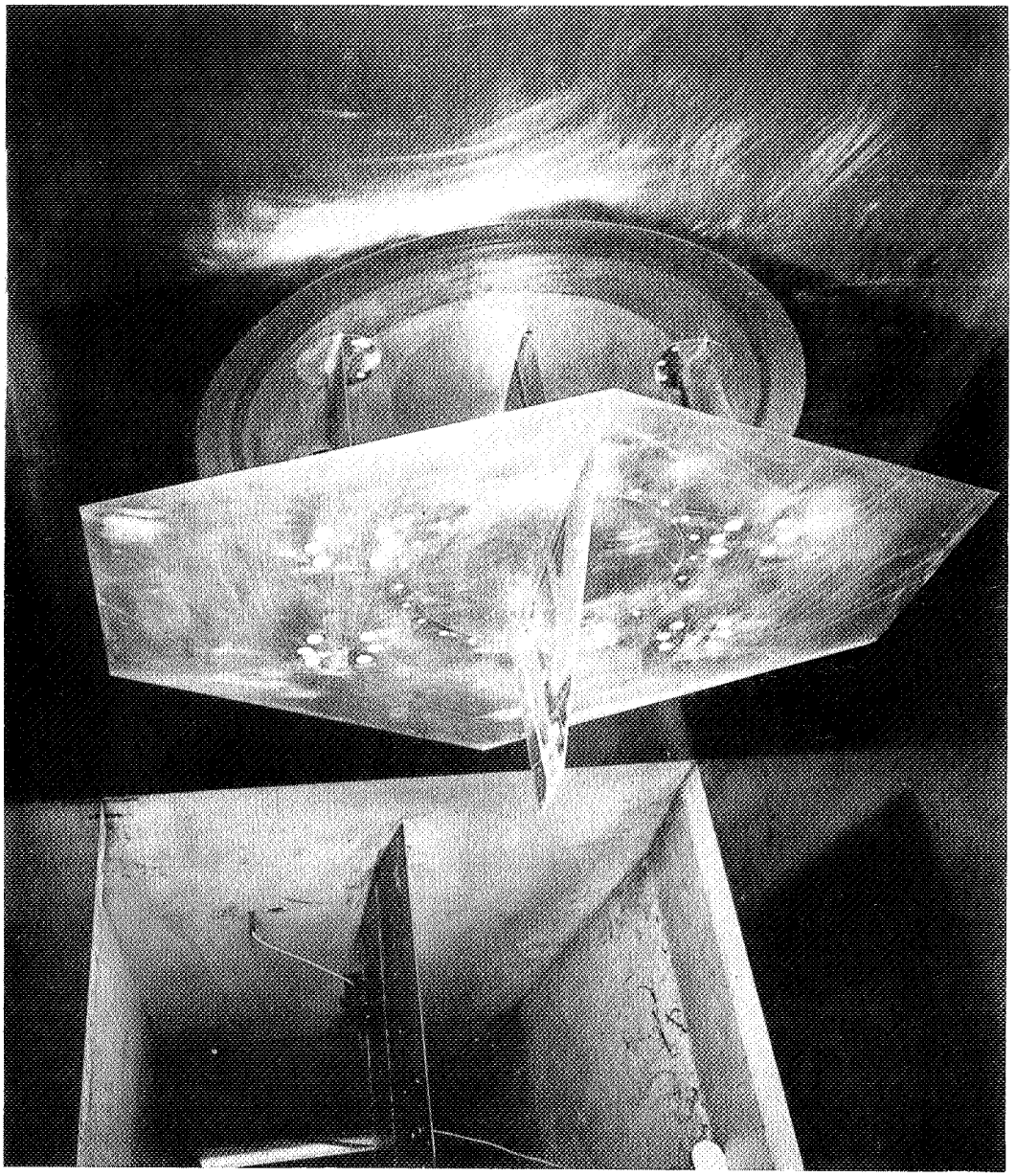


Figure 2.- Sketches showing approximate extent and location of orifice stations. Spanwise locations of stations are given in table 1 and chordwise locations of orifices in table 2.



L-77038

Figure 3.- Sketch of test setup showing one of the tip-control installations.



L-75294

Figure 4.- Photograph of configuration J mounted on boundary-layer bypass plate.

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