

15 NOVEMBER 1963

Temp
197740

GPO PRICE \$ _____
 CFSTI PRICE(S) \$ _____
 Hard copy (HC) \$ 7.21
 Microfiche (MF) \$ 2.25
 ff 653 July 65

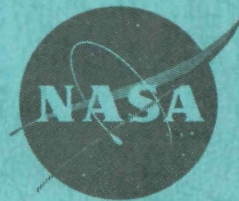
PROGRAMMER'S MANUAL for Interplanetary Error Propagation Program

FACILITY FORM 802

N66-15732

_____ (ACCESSION NUMBER)	_____ (THRU)
<u>421</u> (PAGES)	<u>1</u> (CODE)
<u>OR69535</u> (NASA CR OR TMX OR AD NUMBER)	<u>30</u> (CATEGORY)

CONTRACT NAS 5-3342



prepared for

National Aeronautics and Space Administration
Goddard Space Flight Center
Greenbelt, Maryland

PHILCO

A SUBSIDIARY OF

Ford Motor Company

WDL DIVISION

PALO ALTO, CALIFORNIA

7
R&T - 18040

WDL-TR2184
15 November 1963

**PROGRAMMER'S MANUAL FOR INTERPLANETARY
ERROR PROPAGATION PROGRAM**

Prepared by

PHILCO CORPORATION
A Subsidiary of Ford Motor Company
WDL Division
Palo Alto, California

CONTRACT NAS 5-3342

Prepared for

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION
GODDARD SPACE FLIGHT CENTER
Greenbelt, Maryland

ABSTRACT

WDL-TR2184
PROGRAMMER'S MANUAL FOR
INTERPLANETARY ERROR PROPAGATION PROGRAM
15 November 1963

UNCLASSIFIED

420 pages
NAS 5-3342

15732

This report discusses the subroutines that are used in the Interplanetary Error Propagation Program. A narrative description and card listing are provided for each subroutine; flow diagrams are included, if applicable. A listing of assigned locations in common is also presented.

Author

THIS UNCLASSIFIED ABSTRACT IS DESIGNED FOR RETENTION IN A STANDARD 3-BY-5 CARD-SIZE FILE, IF DESIRED. WHERE THE ABSTRACT COVERS MORE THAN ONE SIDE OF THE CARD, THE ENTIRE RECTANGLE MAY BE CUT OUT AND FOLDED AT THE DOTTED CENTER LINE. (IF THE ABSTRACT IS CLASSIFIED, HOWEVER, IT MUST NOT BE REMOVED FROM THE DOCUMENT IN WHICH IT IS INCLUDED.)

FOREWORD

This report is submitted to the National Aeronautics and Space Administration, Goddard Space Flight Center, in fulfilling the requirements of Contract NAS 5-3342.

The documentation provided by Philco WDL in support of the Interplanetary Error Propagation Program consists of the following three volumes:

- WDL-TR2184, "Programmer's Manual for Interplanetary Error Propagation Program"
- WDL-TR2185, "User's Manual for Interplanetary Error Propagation Program"
- Guidance and Control System Engineering Department Technical Report No. 4, "The application of State Space Methods to Navigation Problems," by Stanley F. Schmidt

These volumes discuss the theory of the Schmidt-Kalman filter used in the program for data smoothing, the manner in which the program is used, and subroutine description and listing.

Page intentionally left blank

TABLE OF CONTENTS

<u>Section</u>		<u>Page</u>
1	INTRODUCTION	1-1
	1.1 General.	1-1
	1.2 General Program Description.	1-1
 <u>Main Chains</u>		
	MAIN(Chain 1)	M-3
	MAIN(Chain 2)	M-13
	MAIN(Chain 3)	M-19
 <u>Subroutine Listing</u>		
	ARKTAN	S-3
	ARKTNS	S-5
	ASINH	S-7
	BODY	S-9
	BVEC	S-15
	CHNGP	S-23
	COMPHQ	S-27
	CONST1	S-41
	CONVPI	S-51
	CORRTP	S-63
	CROSS	S-67
	(CSH)S	S-69
	DE6FN	S-71
	DOT	S-117
	EARTR	S-119
	ECLIP	S-145
	ENCKE	S-147
	ERP	S-151
	ERPT	S-153
	FINP	S-155
	FNORM	S-173

TABLE OF CONTENTS (Cont'd)

<u>Section</u>	<u>Page</u>
<u>Subroutine Listing (Cont'd)</u>	
GHA	S-175
GOTOB	S-179
GOTOR	S-197
GUID	S-203
HOUR	S-217
HPHT	S-221
INPUT	S-223
INTR, INTRI	S-231
INV3	S-245
INVAO	S-249
LOADO	S-251
LOADT	S-253
MASS	S-255
MATRX	S-259
MATSUB	S-261
MNA	S-267
MNAND	S-273
MONBTR	S-277
MULT	S-285
NUTA IT	S-287
OBLN	S-295
ONBTR	S-303
ORTC	S-307
OUTC	S-311
OUTDAT	S-321
OUTP	S-325
PTRAN	S-338
RETRO	S-341
ROTATE	S-347
ROTEQ	S-349
RVIN	S-355

TABLE OF CONTENTS (Cont'd)

<u>Section</u>		<u>Page</u>
<u>Subroutine Listing (Cont'd)</u>		
	RVOUT	S-361
	SDEC	S-365
	SETN	S-369
	SHIFTP	S-371
	STEPFC	S-375
	TIMEC	S-391
	TIMED	S-395
	TRAC	S-397
	TRANSH	S-403

LIST OF TABLES

<u>Number</u>		<u>Page</u>
1-1	List of Assigned Quantities in Common "C" Array.	1-3
1-2	List of Assigned Quantities in Common "S" Array.	1-6
1-3	List of Assigned Quantities in Common "IC" Array.	1-12
1-4	List of Assigned Quantities in Common "T" Array.	1-15

Page Intentionally Left Blank

PROGRAM SUBROUTINE LISTING

ARKTNS	Single Precision Arctangent
ARKTAN	Double Precision Arctangent
ASINH(X)	Function Evaluation
BODY	Calculates Accelerations Due to Perturbing Bodies
BVEC	Calculates B Vector
CHNGP	Determines when to Shift Body Center
COMPHQ	Computations for ONBTR and MONBTR Subroutines
CONST1	Array of Input Constants
CONVPI	Converts Input Covariance Matrix to 1950
CORRTP	Updates P Matrix
CROSS	Cross Product
(CSH)S	Fortran II Card Image Input Subroutine
DE6FN	FAP Integration Subroutine
DOT	Function Forming Dot Product
EARTR	Updates Covariance Matrix for Earth Based Tracking
ECLIP	Transforms Coordinates through Transformations
ENCKE	Calculates Perturbation due to Deviation from CONIC
ERP	Prints Out Ephemeris Error
ERPT	Prints Out Time of Ephemeris Error
FINP	Data Input Subroutine
FNORM	Norm of A Vector
GHA	Greenwich Hour Angle
GOTOB	Main Subroutine for Integration of Trajectories
GOTOR	Iterates to Solve Kepler's Equation
GUID	Performs Guidance Calculations
HOUR	Reads Printer Clock
HPHT	Performs Matrix Multiplication $H*P*HT$
INPUT	Converts Inputs to Equinox of 1950 Reference
INTR	FAP Ephemeris Subroutine
INV3	Inverts Up to a 6 By 6 Matrix
INVAO	Forms Inverse of Transition Matrix
LOADO	Obtains Transition Matrix From T Array

LOADT	Puts Unit ICS On Perturbation Equations
MASS	Arranges Gravitational Constants of Bodies Considered
MATRX	Multiplies $A*B=C$ or $A*B*AT=C$ Max Dimension (10.10)
MATSUB	Error Propagation Logic Subroutine
MNA	Transformation to Selenocentric Coordinates
MNAND	Transformation for Selenocentric Velocities
MONBTR	Updates Covariance Matrix for Moon Beacons
MULT	Multiplies Two 3 by 3 Matrices
NUTAIT	Calculates Nutation Matrix
OBLN	Calculates Acceleration Due to Oblateness
ONBTR	Updates Covariance Matrix for Onboard Tracking
ORTC	Outputs Orbital Parameters
OUTC	Outputs Trajectory
OUTDAT	Outputs Calendar Date
OUTP	Outputs RMS Values of Orbital Parameters
PTRAN	Transforms P Matrix
RETRO	Performs Retro Fire
ROTATE	Calculates Transformation for Rotation About an Axis
ROTEQ	Calculates Matrix from Equinox 1950 to Mean Equinox of Date
RVIN	Transforms Coordinates From Spherical to Cartesian
RVOUT	Transforms Coordinates from Cartesian to Spherical
SDEC	Second Derivative Subroutine
SETN	Set Read and Write Tape Numbers
SHIFTP	Shifts Body Center
STEPC	Move Along Conic in Time
TIMEC	Converts Calendar Date to Days from 1950
TIMED	Converts Days Hours Min Sec to Seconds
TRAC	Tracking Station Coordinates
TRANSH	Transforms H Matrix From Date to 1950

WDL-TR2184

PROGRAMMER'S MANUAL FOR INTERPLANETARY ERROR
PROPAGATION PROGRAM

SECTION 1

INTRODUCTION

1.1 GENERAL

This manual contains subroutine descriptions, logic, and FORTRAN listings for the Interplanetary Error Propagation Program. Listings of the quantities which are in the four common storage arrays (T,S,C, and IC) are also included.

1.2 GENERAL DESCRIPTION OF METHOD OF ORBIT DETERMINATION USED IN PROGRAM

The classical approach to the determination of an orbit from tracking data is the maximum likelihood, least-squares technique. This program uses a different approach to this problem. The relationships between the observed tracking data and the initial conditions (or an equivalent set of parameters) which determine the orbit are highly nonlinear. Therefore, it is assumed that a preliminary estimate of the initial conditions and, therefore, the orbit, is known. The equations are then linearized about this "nominal" orbit and an adjustment to the nominal orbit found from the differences between the observed tracking data and the predicted tracking data based on the nominal orbit. In the least-squares technique, the data is processed in parallel in the sense that the normal equations are summed over all the available tracking data before a modification to the nominal orbit is determined.

The Schmidt-Kalman technique differs from the classical least-squares approach in two ways: first, the estimate used is based upon the minimization of a risk function different from that used in the least-squares approach and, second, the data is processed serially instead of in parallel. The Schmidt-Kalman technique depends upon a linearization of the relations between the orbit parameters and the observed tracking data. Therefore, it assumes some nominal trajectory and an associated error estimate (covariance matrix) for the nominal trajectory.

GENERAL FLOW DIAGRAM
OF OVERALL ERROR PROPAGATION PROGRAM

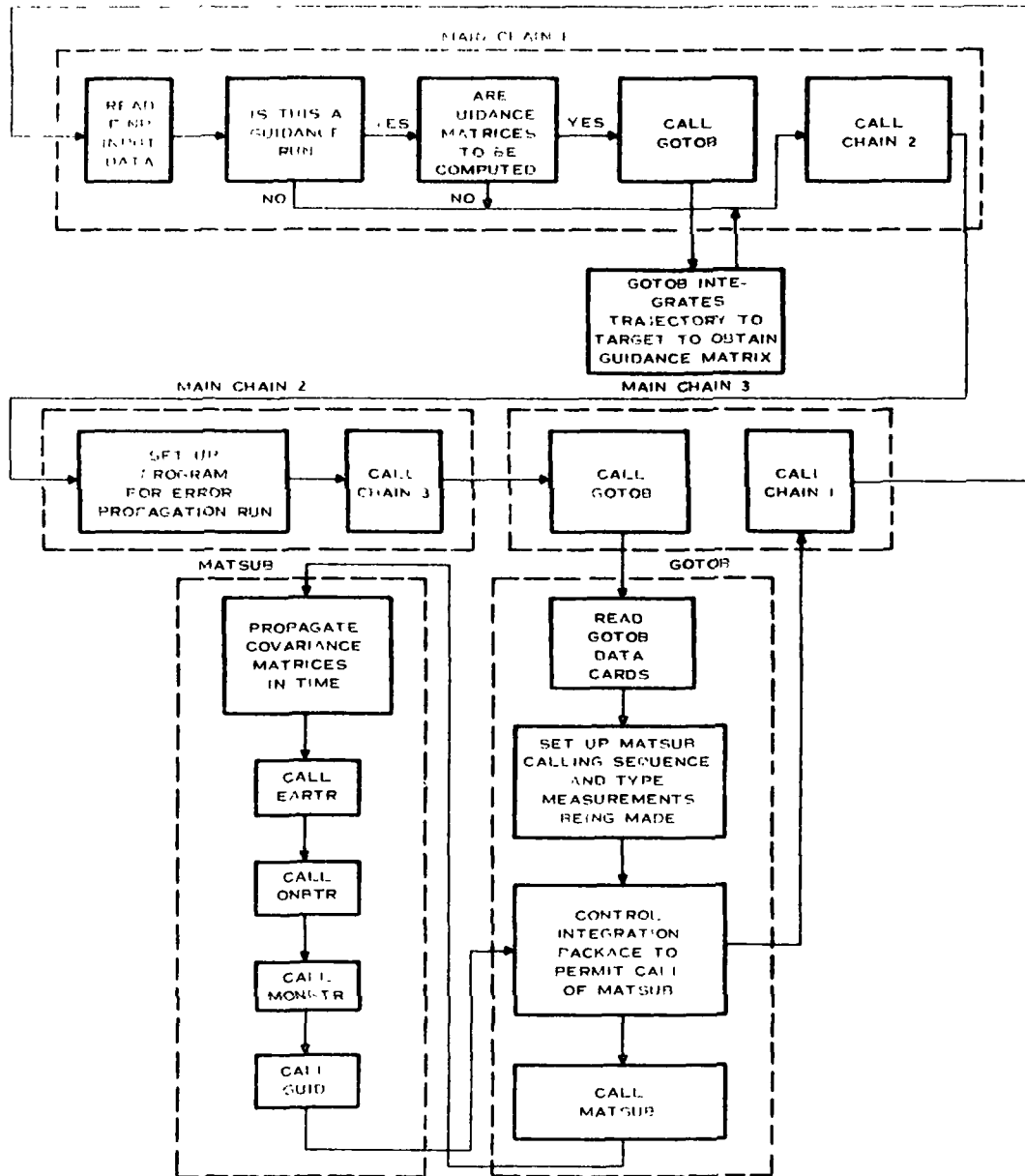


Figure 1-1

The serial processing of the tracking data and associated updating of the nominal orbit occurs as follows: At the start of the time period for which tracking data are to be processed and an improved estimate of the orbit is to be obtained, it is assumed that an estimate of the orbit (a set of state variables) and an error estimate exist. Both of these estimates are updated to an instant of time when tracking data are available. Based upon the available tracking data at this time, a revised estimate of the nominal trajectory is obtained together with a revised estimate of the associated covariance matrix. These two estimates are then propagated along the orbit until additional tracking data become available. In this way, the orbit is updated and tracking data are processed serially.

1.3 GENERAL PROGRAM DESCRIPTION

This program is capable of error studies and their propagation along lunar and planetary trajectories. The design of the program is such as to facilitate the accurate and rapid evaluation of tracking systems for a given lunar or interplanetary trajectory. The program is also able to analyze the errors based on ground tracking as well as on-board tracking independently and in combination. The program has the option to calculate the errors and their projection to the target planets for a probe or a spacecraft based on the following type of measurements.

- a. Earth-based tracking
 1. Range
 2. Range rate
 3. Azimuth
 4. Elevation
 5. Minitrack data

- b. On-board tracking
 1. Right ascension
 2. Declination
 3. Range
 4. Range rate
 5. Range and range rate from beacons on the target planets.

The program is also capable of propagating guidance covariance matrices along the nominal trajectory. The program has the facility of using two types of guidance laws: (1) Fixed time of arrival, and (2) Variable time of arrival with the constraint that the energy with respect to the target be held constant.

The program is composed of three chains. Each link is complete in itself; that is, each contains a main program and all necessary sub-routines. Control is passed from one link to the next by the CALL CHAIN statement. The program requires an ephemeris tape for operation. Figure 1-1 shows a general block diagram of the flow through the program.

The following tables show the assigned locations in "common storage":

Table 1-1:	"C" Array	-----	Floating Point Variables
Table 1-2:	"S" Array	-----	Floating Point Constants
Table 1-3:	"IC" Array	-----	Fixed Point Variables
Table 1-4:	"T" Array	-----	Storage for Integration Routine

TABLE 1-1

LIST OF ASSIGNED QUANTITIES IN COMMON "C" ARRAY

DIMENSION 1000			
CELL	FORTRAN NAME	DIMENSION	DESCRIPTION
C(10)	TW		Whole days from 1950 at last rectification
C(11)	TF		Fractional days from 1950 at last rectification
C(12)	TSECO		Time in seconds at last rectification
C(13)	TP1		Time in whole days
C(14)	TP2		Time in fractional days
C(15)	XP	(3)	X, Y, Z, equinox of 1950
C(18)	VXP	(3)	\dot{X} , \dot{Y} , \dot{Z} equinox of 1950
C(21)	AE	(3)	Acceleration due to deviation from conic
C(24)	AO	(3)	Acceleration due to oblateness
C(27)	CA	(3)	Acceleration due to perturbing bodies
C(30)	TSEC		Seconds from start - zero reference time
C(33)	X	(3)	Reference conic X, Y, Z
C(36)	VX	(3)	Reference conic \dot{X} , \dot{Y} , \dot{Z}
C(46)	XSO	(3)	Initial position for STEPC conic
C(49)	VXSO	(3)	Initial velocity for STEPC conic
C(55)	μ		Gravity constant of central body
C(56)	VKB	(6)	Gravitational constants of bodies used
C(62)	PO	(22)	Ephemeris positions of bodies
C(84)	VE	(22)	Ephemeris velocities of bodies
C(106)	RBO	(6)	Distances to bodies

DIMENSION 1000			
CELL	FORTTRAN NAME	DIMENSION	DESCRIPTION
C(112)	RBOP	(6)	Distances to bodies
C(120)	EN	(3,3)	Nutation matrix
C(129)	EA	(3,3)	Transformation from 1950 to mean equinox of date
C(138)	AN	(3,3)	Transformation from 1950 to true equator of date
C(147)	ECL	(3,3)	Transformation from 1950 to ecliptic of date
C(156)	ECX	(3)	Position: ecliptic coordinates
C(159)	ECV	(3)	Velocity: ecliptic coordinates
C(162)	BET		Angle from line of nodes to radius vector
C(163)	THT		True anomaly
C(171)	BP	(3,3)	Acceleration partials for use in variational equations
C(180)	SMA		Semi-Major Axis
C(181)	ECC		Eccentricity
C(182)	RCA		Radius of closest approach
C(183)	OINC		Orbital inclination
C(184)	OMG		Longitude of ascending node
C(185)	BEP		Argument of periapsis
C(186)	XED	(3)	Position: equator date
C(189)	VED	(3)	Velocity: equator date
C(192)	RCV	(3)	$\vec{R} \times \vec{v}$
C(195)	RCV2		$ \vec{R} \times \vec{v} ^2$
C(196)	R2		R^2

DIMENSION 1000			
CELL	FORTRAN NAME	DIMENSION	DESCRIPTION
C(197)	v^2		v^2
C(198)	RDV		$\frac{\dot{r}}{R} \cdot \dot{v}$
C(199)	C3		$C_3 = v^2 - \frac{2L}{R}$
C(460)	PFTA	(6,6)	Deviation From Nominal Covariance Matrix
C(568)	TRANS	(3,6)	Guidance partial matrix being used on runs
C(622)	TLAST	(4,6)	Delta time since last observation in ONBTR
C(647)	TOUT		Time to output for MATSUB
C(648)	TGUIDE		Time to make guidance correction
C(649)	TSECP		LAST TIME through MATSUB
C(650)	TPRINT		Output print interval
C(651)	TSTART		Start time
C(652)	P	(6,6)	Knowledge of state covariance matrix
C(752)	AOS	(6,6)	Transition matrix from start to present time
C(788)	STPARS	(3,3)	Station partials MONBTR
C(797)	CIOMP		Compute guidance matrices
C(800)	STPARD	(3,3)	Station partials MONBTR
C(888)	}		Constants used in COMPHQ
C(900)			
C(973)	OUTPUT	(6)	Data for output purposes

TABLE 1-2
LIST OF ASSIGNED QUANTITIES IN COMMON "S" ARRAY

DIMENSION 1000			
CELL	FORTRAN NAME	DIMENSION	DESCRIPTION
S(1)			Earth Planetary Mass
S(2)			Moon Planetary Mass
S(3)			Sun Planetary Mass
S(4)			Venus Planetary Mass
S(5)			Mars Planetary Mass
S(6)			Jupiter Planetary Mass
S(7)			SPARE
S(8)			SPARE
S(9)			SPARE
S(10) } S(19) }			Earth Constants
S(20) } S(29) }			Moon Constants
S(30) } S(39) }			Sun Constants
S(40) } S(49) }			Venus Constants
S(50) } S(59) }			Mars Constants
S(60) } S(69) }			Jupiter Constants
S(70)			86400. Conversion factor days to seconds
S(71)			1/86400. Conversion factor seconds to days

DIMENSION 1000			
CELL	FORTRAN NAME	DIMENSION	DESCRIPTION
S(72)			.017453296 Conversion factor for degrees to radians
S(73)			57.29578 Conversion factor for radians to degrees
S(80)	AT		Launch latitude - degrees
S(81)	ON		Launch longitude - degrees
S(82)	AL		Launch altitude - km.
S(83)	TLTI		Time from launch to injection, days hours. min sec
S(84)	FAZ		Firing azimuth
S(110)	TSTOP		Time to stop calling MATSUB
S(111)	TIM		Type of input
S(112)	DATE		Start date
S(113)	FDATE		Fractional start date
S(114)	CIBDY		Central body
S(115)	X	(3)	Initial position
S(118)	VX	(3)	Initial velocity
S(121)	TIBDY		Target Body
S(122)	OUTTP		Type of output
S(124)	SKTB		Type of stop

EARTH BASED TRACKING DATA

N = 0 - 19

CELL	DESCRIPTION	UNITS
S(125)+N*15	Variance of range	KM ²
S(126)+N*15	Variance of azimuth	RAD ²
S(127)+N*15	Variance of elevation	RAD ²
S(128)+N*15	Variance of range rate	KM ² /SEC ²
S(129)+N*15	Variance of latitude	RAD ²
S(130)+N*15	Variance of longitude	RAD ²
S(131)+N*15	Variance of altitude	KM ²
S(132)+N*15	Variance of azimuth biases	RAD ²
S(133)+N*15	Variance of elevation biases	RAD ²
S(134)+N*15	Latitude of station	DEG
S(135)+N*15	Longitude of station	DEC
S(136)+N*15	Altitude of station	KM
S(137)+N*15	Station name	
S(138)+N*15	Period of observation	SEC
S(139)+N*15	Variance of time bias	SEC ²
S(425)	Velocity of light error	KM ² /SEC ²

ON-BOARD TRACKING DATA

S(426)	Variance of range	KM ²
S(427)	Variance of right ascension	RAD ²
S(428)	Variance of declination	RAD ²
S(429)	Variance of range rate	KM ² /SEC ²
S(430)	Variance of range bias	KM ²
S(431)	Variance of right ascension bias	RAD ²

CELL	DESCRIPTION	UNITS
S(432)	Variance of declination bias	RAD ²
S(433)	Variance of range rate bias	KM ² /SEC ²
S(434)	Variance of clock time bias	SEC ²
S(435)	Spare	
S(436)	Spare	

N = 0 - 5 EARTH, MOON, SUN, VENUS, MARS, JUPITER

CELL	FORTRAN NAME	DIMENSION	DESCRIPTION	UNITS
S(437)+4*N			Period of range observation	SEC
S(438)+4*N			Period of right ascension Observation	SEC
S(439)+4*N			Period of declination Observation	SEC
S(440)+4*N			Period of range rate Observation	SEC
S(471)			Shutoff Error (Rocket)	(%) ²
S(473)			Pointing Error (Motor)	(RAD) ²
S(475)			Type of guidance decision 0-Time + Ratio	
S(476)	TGUID	(6)	Times for guidance correction	
S(483)	GDCOR		Ratio for making guidance correction	
S(484)	DMON		Error in monitoring guidance correction	(%) ²
S(485)	ENKE		Correction criteria for deviation from reference conic	

CELL	FORTRAN NAME	DIMENSION	DESCRIPTION	UNITS
MOON BEACON TRACKING DATA N = 0 - 9				
S(500)+N*15			Variance of range	KM ²
S(501)+N*15			Variance of right ascension	RAD ²
S(502)+N*15			Variance of declination	RAD ²
S(503)+N*15			Variance of range rate	KM ² /SEC ²
S(504)+N*15			Variance of range bias	KM ²
S(505)+N*15			Variance of right ascension bias	RAD ²
S(506)+N*15			Variance of declination bias	RAD ²
S(507)+N*15			Variance range rate bias	KM ² /SEC ²
S(508)+N*15			Variance clock bias	SEC ²
S(509)+N*15			Latitude of station	DEG
S(510)+N*15			Longitude of station	DEG
S(511)+N*15			Altitude of station	KM
S(512)+N*15			Station name	
S(513)+N*15			Period of observation	SEC
S(514)+N*15			SPARE	
S(650)	PARI	(21)	Initial deviation from nominal covariance matrix	
S(671)	PI	(21)	Initial knowledge of state covariance matrix	
S(720)	PUPIN		Type of coordinates for PI	
S(721)	PARIN		Type of coordinates for PARI	
S(722)	FTA	(3,6)	Guidance transition matrix fixed time arrival	

CELL	FORTRAN NAME	DIMENSION	DESCRIPTION	UNITS
S(740)	CTE	(3,6)	Guidance transition matrix constant energy WRT* target	

MOON BEACON DATA

N = 0 - 9

S(758)+N*3			Variance of station latitude	RAD ²
S(759)+N*3			Variance of station longitude	RAD ²
S(760)+N*3			Variance of station altitude	KM ²

EARTH BASED TRACKING DATA

N = 0 - 19

S(788)+N*5			Tracking Station horizon	RAD
S(789)+N*5			Variance of M dircos	
S(790)+N*5			Variance of M dircos bias	
S(791)+N*5			Variance of L dircos	
S(792)+N*5			Variance of L dircos bias	
S(888)	RETR		Key to call subroutine RETRO	
S(900)	RAD	(6)	Radius to bodies	
				* with respect to

TABLE 1-3

LIST OF ASSIGNED QUANTITIES IN COMMON "IC" ARRAY

DIMENSION 300			
CELL	FORTRAN NAME	DIMENSION	DESCRIPTION
IC(1)	N		# of sets of equations
IC(2)	IOR		body center
IC(3)	NOR		new body center
IC(4)	KSTP		type stop
IC(5)	KTYPE		switch indicating type stop
IC(6)	ITARG		target body
IC(7)	KOUT		type of output
IC(8)	IMMSUB		key to test if MATSUB is to be called
IC(10)			+ if tracking station 1 considered
IC(11)			+ if tracking station 2 considered
IC(12)			+ if tracking station 3 considered
.			
.			
.			
.			
IC(29)			+ if station 20 considered
IC(30)			+ range, 0 no range
IC(31)			+ AZ-EL, 0 no AZ-EL
IC(32)			+ dircos, 0 no dircos
IC(33)			+ range rate, 0 no range rate
.			
.			
.			
.			

} Station
1

CELL	FORTRAN NAME	DIMENSION	DESCRIPTION
IC(106)			+ range, 0 no range
IC(107)			+ AZ-EL, 0 no AZ-EL
IC(108)			+ dircos 0 no dircos
IC(109)			+ range rate, 0 no range rate
IC(110)			Earth observed + yes, 0 no
IC(111)			Moon observed, + yes, 0 no
IC(112)			Sun observed, + yes, 0 no
IC(113)			Venus observed, + yes, 0 no
IC(114)			Mars observed, + yes, 0 no
IC(115)			Jupiter observed, + yes, 0 no
IC(116)			range, + yes, 0 no
IC(117)			rt. ascension, + yes, 0 no
IC(118)			declination, + yes, 0 no
IC(119)			range rate, + yes, 0 no
.			
.			
.			
.			
.			
IC(136)			range, + yes, 0 no
IC(137)			rt. ascension, + yes, 0 no
IC(138)			declination, + yes, 0 no
IC(139)			range rate, + yes, 0 no
IC(140)			+ Moon beacon station 1
.			o
.			
IC(149)			+ Moon beacon station 10
.			o

Station # 20

Earth on-board measurements

Jupiter on-board measurements

10 Moon beacon stations

CELL	FORTRAN NAME	DIMENSION	DESCRIPTION
IC(150)			+ range o
IC(151)			+ right ascension o
IC(152)			+ declination o
IC(153)			+ range rate o
.			
.			
.			
.			
.			
IC(186)			+ range o
IC(187)			+ right ascension o
IC(188)			+ declination o
IC(189)			+ range rate o
IC(190)	LSTAT		Key for earth based tracking
IC(191)	LONB		Key for on-board tracking
IC(192)	LMB		Key for moon beacon tracking
IC(193)	IGUID		Positive if guidance run
IC(194)	ISTAT	(20)	Keep account which of 20 trackers saw vehicle last time in MATSUB
IC(214)	NOUT		Output indicator
IC(215)	PUPIN		type of P matrix input
IC(216)	PARIN		type of PAR matrix input
IC(217)	IGDTP		type of guidance
IC(218)	IGDKEY		guidance key set in main
IC(219)	IGD		number of guidance corrections
IC(220)	IMOONB	(20)	Keep account which of 10 moon beacons saw vehicle last time in MATSUB
IC(231)	NSTEP		Key for STEPC

TABLE 1-4
LIST OF ASSIGNED QUANTITIES IN COMMON "T" ARRAY

This is the common storage block for the integration package. See the sub-routine writeup for DE6FN for definitions of the quantities in storage.

DIMENSION 1360	
CELL	DESCRIPTION
T(1)	N No. of Equations
T(2)	X
T(3)	H Step Size
T(4)	y_i $i = 1, N$
T(N+4)	y_i' $i = 1, N$
T(2N+4)	y_i'' $i = 1, N$ second derivatives stored by V subroutine
T(3N+4)	y_i' $i = 1, N$ most significant
T(4N+4)	y_i' $i = 1, N$ least significant
T(5N+4)	$\Delta y_i'$ $i = 1, N$
T(6N+4)	$\Delta y_i'$ $i = 1, N$
T(7N+4)	y_i $i = 1, N$ most significant
T(8N+4)	y_i $i = 1, N$ least significant
T(9N+4)	y_{i3} $i = 1, N$
T(10N+4)	y_{i3}' $i = 1, N$
	} saved for central difference equations

DIMENSION 1360	
CELL	DESCRIPTION
T(11N+4)	y''_{i0} $i = 1, N$
T(12N+4)	y''_{i1} $i = 1, N$
T(13N+4)	y''_{i2} $i = 1, N$
T(14N+4)	y''_{i3} $i = 1, N$
T(15N+4)	y''_{i4} $i = 1, N$
T(16N+4)	y''_{i5} $i = 1, N$
T(17N+4)	y''_{i6} $i = 1, N$
T(18N+4)	used only if coordinates changed.
T(19N+4)	11 N storages. N sets of differences saved for next cowell step.
.	
.	
.	
.	
T(30N-8)	

MAIN CHAINS

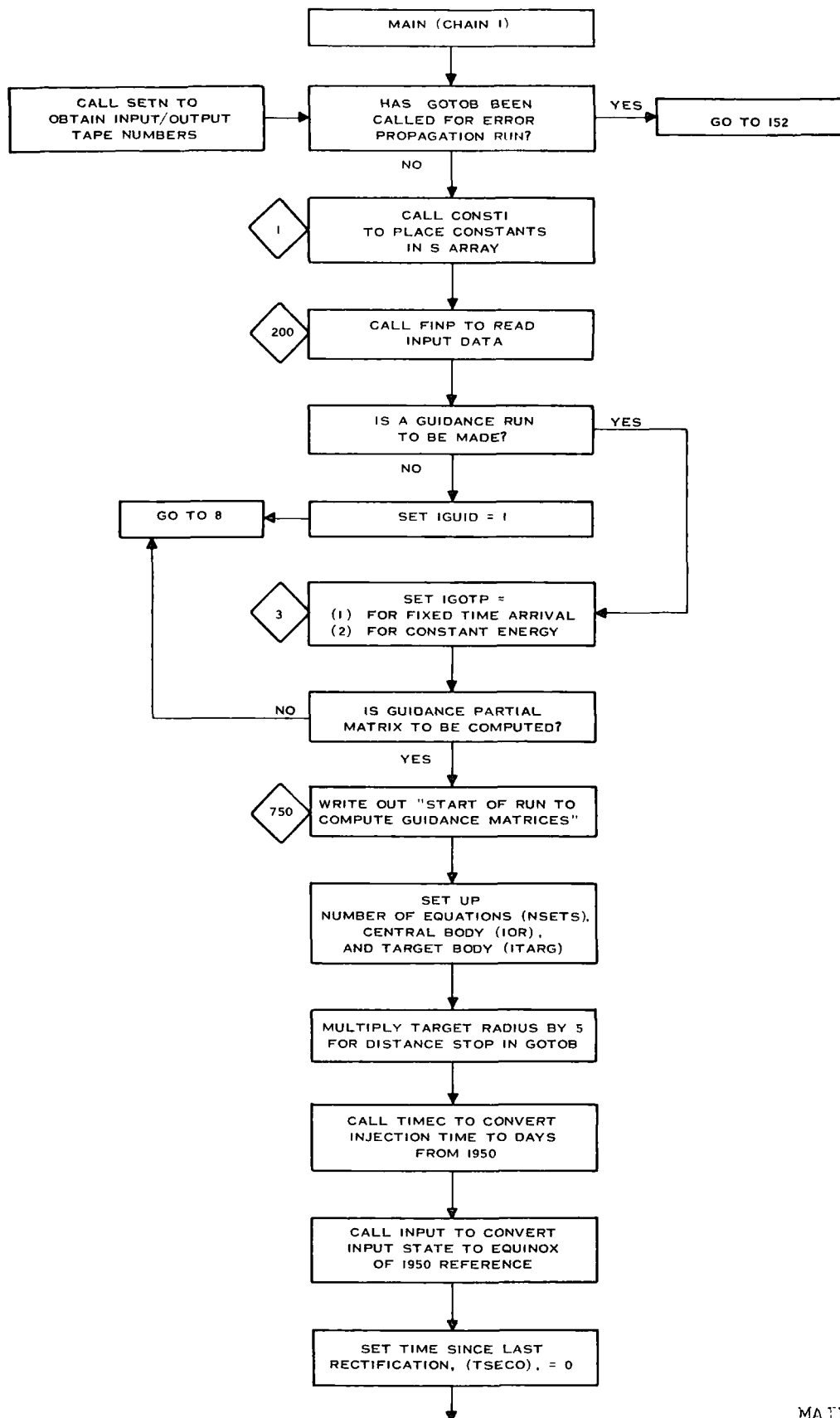
M-1

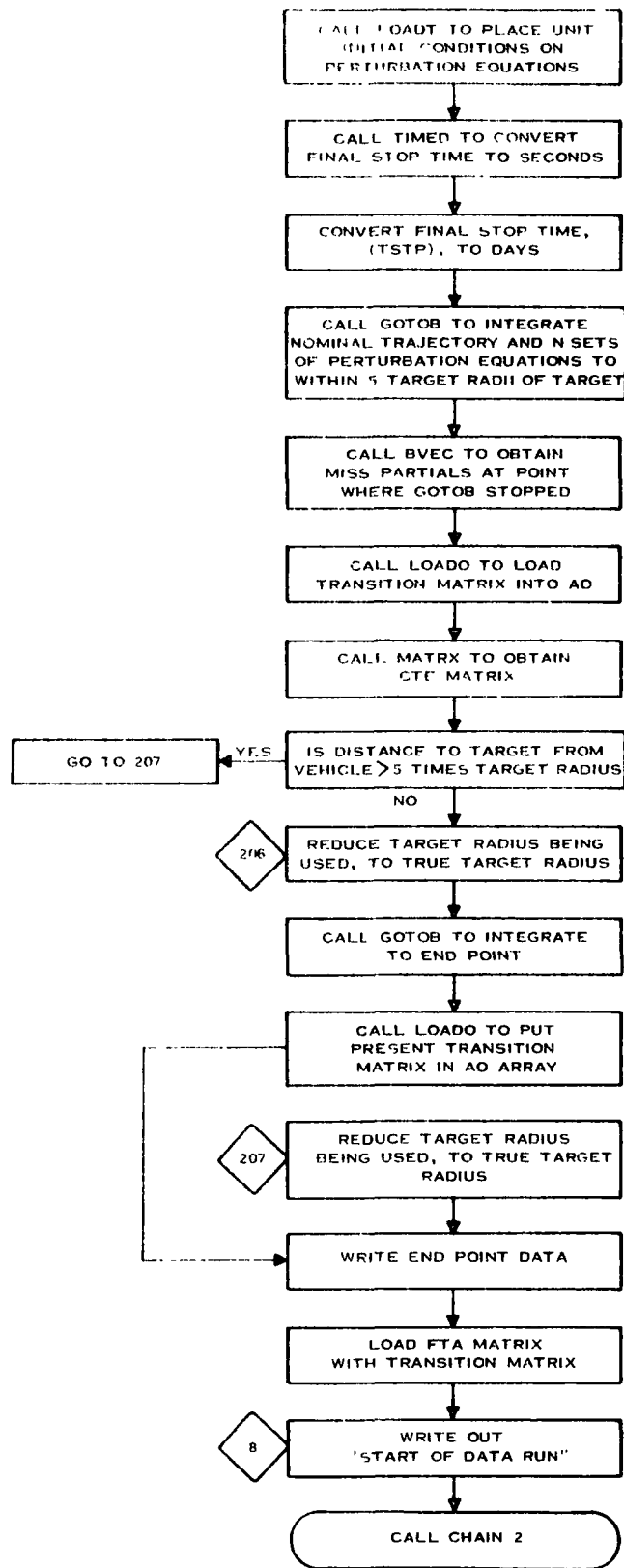
Page Intentionally Left Blank

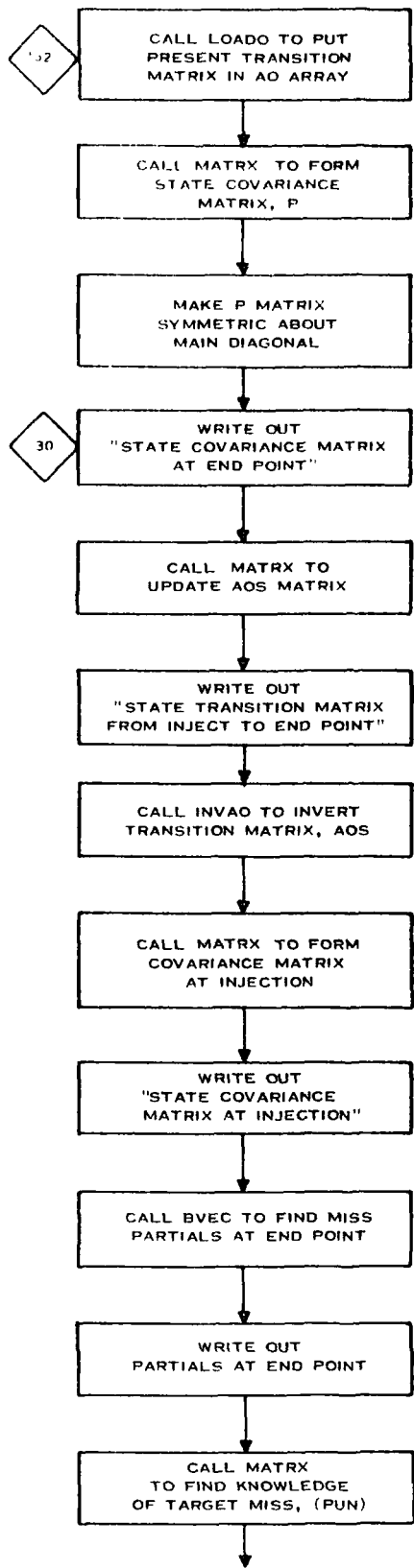
Subroutine: MAIN (Chain 1)

Purpose: Set up program to perform guidance runs to obtain transition and partial matrices. Call Chain 2 for error propagation runs and write out end point data after program returns from Chain 3.

Common storages used or required:	<u>T, S, C, IC</u>
Subroutines required:	<u>BVEC, CHAIN, CONST1, FINP, GOTOB, INPUT, INVAO, LOADO, LOADT, MATRX, RETRO, TIMEC, TIMED</u>
Functions required:	<u>None</u>
Approximate number of storages required:	<u>793 DEC</u>

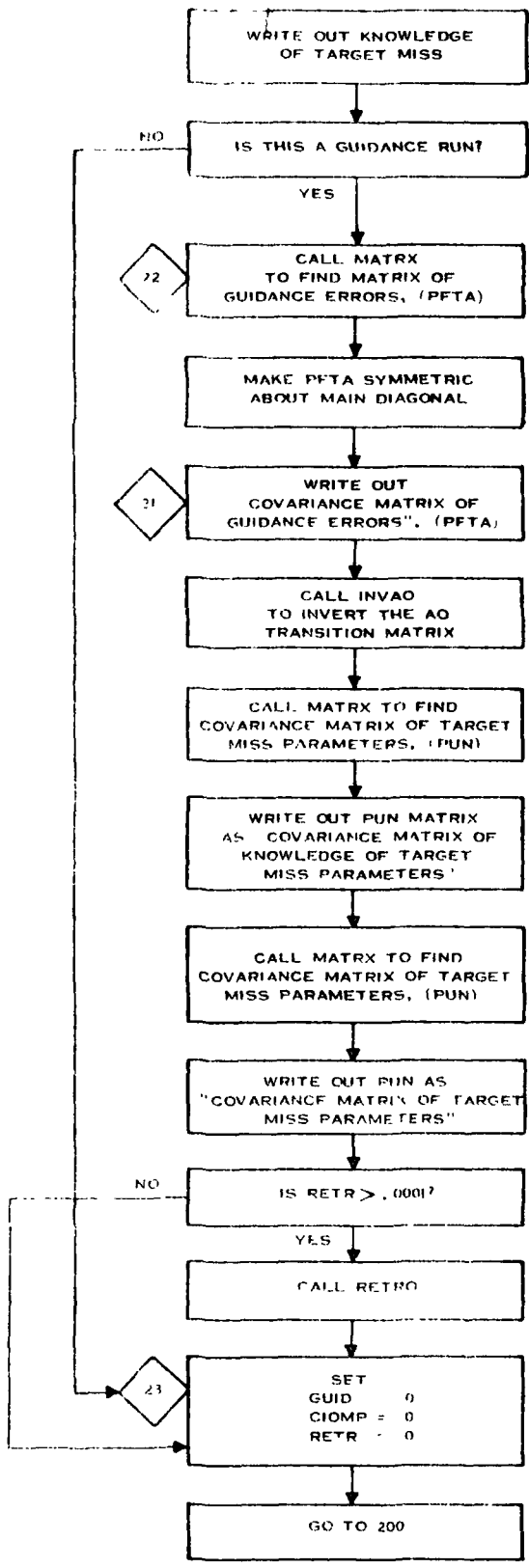






M-6

MAIN (CHAIN-1)-4



MAIN (CHAIN 1)

*	LABEL		MAI1
CEC20D2	MAIN PROGRAM		MAI10000
C	ERROR PROPAGATION		MAI10010
C	ALONG INTERPLANETARY TRAJECTORIES		MAI10015
C	REQUIRES FOLLOWING SUBROUTINES AND FUNCTIONS		MAI10020
C	ARKTNS SINGLE PRECISION ARCTANGENT		MAI10030
C	ARKTAN DOUBLE PRECISION ARCTANGENT		MAI10040
C	ASINH(X) FUNCTION EVALUATION		MAI10050
C	BODY CALCULATES ACCELERATIONS DUE TO PERTURBING BODIES		MAI10060
C	BVEC CALCULATES B VECTOR		MAI10070
C	CHNGP DETERMINES WHEN TO SHIFT BODY CENTER		MAI10090
C	COMPHQ COMPUTATIONS FOR ONBTR AND MONBTR SUBROUTINES		MAI10095
C	CONST1 ARRAY OF INPUT CONSTANTS		MAI10100
C	CONVPI CONVERTS INPUT COVARIANCE MATRIX TO 1950		MAI10110
C	CORRTP UPDATES P MATRIX		MAI10020
C	CROSS CROSS PRODUCT		MAI10130
C	DOT FUNCTION FORMING DOT PRODUCT		MAI10140
C	DE6FN FAP INTEGRATION SUBROUTINE		MAI10160
C	EARTR UPDATES COVARIANCE MATRIX FOR EARTH BASED TRACKING		MAI10170
C	ECLIP TRANSFORMS COORDINATES THROUGH TRANSFORMATIONS		MAI10180
C	ENCKE CALCULATES PERTURBATION DUE TO DEVIATION FROM CONIC		MAI10190
C	ERP PRINTS OUT EPHEMERIS ERROR		MAI10195
C	ERPT PRINTS OUT TIME OF EPHEMERIS ERROR		MAI10197
C	FINP DATA INPUT SUBROUTINE		MAI10200
C	FNORM NORM OF A VECTOR		MAI10210
C	GHA GREENWICH HOUR ANGLE		MAI10220
C	GOTOB MAIN SUBROUTINE FOR INTEGRATION OF TRAJECTORIES		MAI10230
C	GOTOR ITERATES TO SOLVE KEPLER'S EQUATION		MAI10235
C	GUID PERFORMS GUIDANCE CALCULATIONS		MAI10240
C	HPHT PERFORMS MATRIX MULTIPLICATION $H * P * H^T$		MAI10245
C	INPUT CONVERTS INPUTS TO EQUINOX OF 1950 REFERENCE		MAI10250
C	INTR FAP EPHEMERIS SUBROUTINE		MAI10260
C	INVAO FORMS INVERSE OF TRANSITION MATRIX		MAI10270
C	INV3 INVERTS UP TO A 6 BY 6 MATRIX		MAI10280
C	LOADO OBTAINS TRANSITION MATRIX FROM T ARRAY		MAI10290
C	LOADT PUTS UNIT ICS ON PERTURBATION EQUATIONS		MAI10300
C	MASS ARRANGES GRAVITATIONAL CONSTANTS OF BODIES CONSIDERED		MAI10310
C	MATRIX MULTIPLIES $A * B = C$ OR $A * B * A^T = C$ MAX DIMENSION(10,10)		MAI10320
C	MATSUB ERROR PROPAGATION LOGIC SUBROUTINE		MAI10330
C	MNA TRANSFORMATION TO SELENOCENTRIC COORDINATES		MAI10340
C	MNAND TRANSFORMATION FOR SELENOCENTRIC VELOCITIES		MAI10345
C	MONBTR UPDATES COVARIANCE MATRIX FOR MOON BEACONS		MAI10350
C	MULT MULTIPLIES TWO 3 BY 3 MATRICES		MAI10370
C	NUTAIT CALCULATES NUTATION MATRIX		MAI10380
C	OBLIN CALCULATES ACCELERATION DUE TO OBLATENESS		MAI10390
C	ONBTR UPDATES COVARIANCE MATRIX FOR ONBOARD TRACKING		MAI10400
C	ORTC OUTPUTS ORBITAL PARAMETERS		MAI10420
C	OUTC OUTPUTS TRAJECTORY		MAI10440
C	OUTDAT OUTPUTS CALENDAR DATE		MAI10430
C	OUTP OUTPUTS RMS VALUES OF ORBITAL PARAMETERS		MAI10450
C	PTRAN TRANSFORMS P MATRIX		MAI10452

MAIN (CHAIN 1) (Cont'd)

RETRO	PERFORMS RETRO FIRE	MAI10455
ROTATE	CALCULATES TRANSFORMATION FOR ROTATION ABOUT AN AXIS	MAI10460
ROTEQ	CALCULATES MATRIX FROM EQUINOX 1950 TO MEAN EQUINOX OF DATE	MAI10465
		MAI10468
RVIN	TRANSFORMS COORDINATES FROM SPHERICAL TO CARTESIAN	MAI10470
RVOUT	TRANSFORMS COORDINATES FROM CARTESIAN TO SPHERICAL	MAI10480
SDEC	SECOND DERIVATIVE SUBROUTINE	MAI10530
SETN	SET READ AND WRITE TAPE NUMBERS	MAI10535
SHIFTP	SHIFTS BODY CENTER	MAI10540
STEPIC	MOVE ALONG CONIC IN TIME	MAI10545
TIMEC	CONVERTS CALENDAR DATE TO DAYS FROM 1950	MAI10550
TIMED	CONVERTS DAYS HOURS.MIN SEC TO SECONDS	MAI10560
TRAC	TRACKING STATION COORDIATES	MAI10570
TRANSH	TRANSFORMS H MATRIX FROM DATE TO 1950	MAI10580
	COMMON T,S,C,IC	MAI10600
	DIMENSION T(1360),S(1000),C(1000),IC(300),X(3)	MAI10610
	1,VX(3),XP(3),VXP(3),AN(3,3),UM(6),BV(4),PBV(3,6)	MAI10620
	2,AO(6,6),PARI(21),PI(21),ISTAT(20),FTA(3,6)	MAI10630
	3,TRANS(3,6)	MAI10640
	4,PFTA(6,6),P(6,6),TGUID(6)	MAI10650
	DIMENSION AOS(6,6),RAD(6), RBOP(6),CTE(3,6),AOI(6,6),PUN(3,3)	MAI10660
	EQUIVALENCE(T,TDUM),(S,SDUM),(C,CDUM),(IC,IDUM),	MAI10670
	1(IC(8),IMMSUB),(S(112),DATE),(S(113),FDATE),(S(115),X),(S(118),VX)	MAI10680
	2,(IC(193),IGUID),(S(110),TSTOP),(IC(2),IOR),(S(111),TIM)	MAI10690
	3,(IC(6),ITARG),(IC(4),KSTP),(IC(1),NSETS),(C(10),TW),(C(11),TF)	MAI10700
	4,(C(138),AN),(C(12),TSECO),(S(71),STD),(S(1),UM),(C(15),XP)	MAI10710
	5,(C(18),VXP),(C(13),TP1),(C(14),TP2),(S(671),PI),(S(650),PARI)	MAI10720
	6,(IC(194),ISTAT),(IC(7),KOUT),(C(649),TSECP),(S(122),OUTTP)	MAI10730
	7,(C(460),PFTA),(C(652),P)	MAI10740
	8,(S(114),CIBDY),(S(121),TIBDY),(S(722),FTA),(S(124),SKTB)	MAI10750
	9,(S(720),PUPIN),(S(721),PARIN)	MAI10760
	EQUIVALENCE (C(752),AOS),(S(900),RAD),(C(112),RBOP),(C(30),TSEC)	MAI10770
	1,(S(740),CTE),(C(648),TGUIDE),(C(850),AOI),(C(850),PUN)	MAI10780
	EQUIVALENCE (S(476),TGUID),(IC(219),IGD)	MAI10790
	1,(IC(218),IGDKY),(IC(217),IGDTP),(C(568),TRANS)	MAI10800
	EQUIVALENCE (T(1358),TSTP),(C(797),COMP),(S(888),RETR)	MAI10810
	CALL SETN(NIN,NUTS)	MAI10811
	IF(T(1359)-1359.)1,152,1	MAI10820
1	CALL CONST1	MAI10830
	THE CONSTS OF S ARRAY ARE READ IN	MAI10840
200	CONTINUE	MAI10850
	WRITE OUTPUT TAPE NUTS,700	MAI10851
700	FORMAT(26H1 START OF FINP INPUT DATA)	MAI10855
	CALL FINP(22,S,TIM,CIBDY,TIBDY,GUID,SKTB,CIOMP	MAI10860
	1,TSTOP,X,VX,DATE,FDATE,FTA,PI,PARI,TGUID,GID,PUPIN,PARIN,CTE,	MAI10865
	2RETR,OUTTP,	MAI10870
	2S TIM CIBDY TIBDY GUID SKTB CIOMP TSTOP X VX DATE	MAI10880
	3FDATE FTA PI PARI TGUID GID PUPIN PARIN CTE RETR OUTTP	MAI10885
	4)	MAI10890
	GUID IS SET POSITIVE IF GUIDANCE IS CONSIDERED	MAI10900
	IF(GUID) 2,2,3	MAI10910

MAIN (CHAIN 1) (Cont'd)

2	CONTINUE	MAI1092
	IGUID=1	MAI1093
	GO TO 8	MAI1094
3	CONTINUE	MAI1095
	IGD=GID	MAI1096
	IGDTP = GUID	MAI1097
	IF(IGDTP-3) 204,204,205	MAI1098
205	CONTINUE	MAI1099
	IGDTP=2	MAI1100
204	CONTINUE	MAI1101
	IGUID=2	MAI1102
C	CIOMP IS SET POSITIVE IF MATRICES ARE TO BE COMPUTED	MAI1103
	IF(CIOMP) 8,8,4	MAI1104
4	CONTINUE	MAI1105
	COMP=CIOMP	MAI1106
	WRITE OUTPUT TAPE NUTS,750	MAI1107
750	FORMAT(43H1START OF RUN TO COMPUTE GUIDANCE MATRICES)	MAI1108
	NSETS=7	MAI1109
	IOR=S(114)	MAI1110
	ITARG=S(121)	MAI1111
	RAD(ITARG)=5.*RAD(ITARG)	MAI1112
	KIN=S(111)	MAI1113
	CALL TIMEC(DATE, FDATE, TW, TF)	MAI1114
	CALL INPUT(KIN, XP, VXP, TW, TF, AN, X, VX)	MAI1115
	TSECO =0.	MAI1116
	KSTP=1	MAI1117
	CALL LOADT	MAI1118
	CALL TIMED(TSTOP, TSTPS)	MAI1119
	TSTP=TSTPS*STD	MAI1120
	IMMSUB=1	MAI1121
	CALL GOTOB(TSTP)	MAI1122
	CALL BVEC(IOR, ITARG, XP, VXP, BV, PBV, TP1, TP2, UM)	MAI1123
	CALL LOADO(A0)	MAI1124
	CALL MATRX(PBV, A0, CTE, 3, 6, 6, 0)	MAI1125
	IF(RBOP(ITARG) - RAD(ITARG)) 206, 206, 207	MAI1126
206	CONTINUE	MAI1127
	RAD(ITARG) = RAD(ITARG) / 5.	MAI1128
	TSECO = TSEC	MAI1129
	CALL GOTOB(TSTP)	MAI1130
	CALL LOADO(A0)	MAI1131
	GO TO 208	MAI1132
207	CONTINUE	MAI1133
	RAD(ITARG) = RAD(ITARG) / 5.	MAI1134
208	CONTINUE	MAI1135
	WRITE OUTPUT TAPE NUTS, 706, ((A0(I,J), J=1,6), I=1,6)	MAI1136
706	FORMAT(31H0TRANSITION MATRIX TO END POINT//(6E17,8))	MAI1137
	WRITE OUTPUT TAPE NUTS, 707, ((CIE(I,J), J=1,6), I=1,3)	MAI1138
707	FORMAT(49H0B VECTOR TRANSITION MATRIX. BY ROWS B,T,B,R,VINF//	MAI1139
	1(6E17,8))	MAI1140
	DO 6 I=1,3	MAI1141
	DO 6 J=1,6	MAI1142

MAIN (CHAIN 1) - (Cont'd)

```

      FTA(I,J)=AO(I,J)
4 CONTINUE
8 CONTINUE
      WRITE OUTPUT TAPE NUTS,751
751 FORMAT(18H1START OF DATA RUN)
      CALL CHAIN(2,B3)
152 CALL LOADO(AO)
      AO IS TRANSITION MATRIX FROM LAST TIME IN MATSUB
      CALL MATRX(AO,P,P,6,6,6,1)
      DO 30 I=1,6
      DO 30 J=I,6
      P(I,J)=(P(I,J)+P(J,I))/2.
      P(J,I)=P(I,J)
30 CONTINUE
      P IS STATE COVARIANCE MATRIX AT END POINT
      WRITE OUTPUT TAPE NUTS,800,((P(I,J),J=1,6),I=1,6)
800 FORMAT(38H0 STATE COVARIANCE MATRIX AT END POINT
1/(6E17.8))
      CALL MATRX(AO,AOS,AOS,6,6,6,0)
      AOS IS TRANSITION MATRIX FROM INJECTION TO END POINT
      WRITE OUTPUT TAPE NUTS,801,((ACS(I,J),J=1,6)I=1,6)
801 FORMAT(50H0 STATE TRANSITION MATRIX FROM INJECT TO END POINT
1/(6E17.8))
      CALL INVAO(AOS,AOI)
      FORMS INVERSE OF AOS
      CALL MATRX(AOI,P,ACS,6,6,6,1)
      WRITE OUTPUT TAPE NUTS,802,AOS
802 FORMAT(38H0 STATE COVARIANCE MATRIX AT INJECTION
1/(6E17.8))
      CALL BVEC(IOR,ITARG,XP,VXP,BV,PBV,TP1,TP2,UM)
      WRITE OUTPUT TAPE NUTS,810,((PBV(J,I),I=1,6),J=1,3)
810 FORMAT(40H0 B*T,B*R,VINF PARTIALS AT END POINT PBV
1/(6E17.8))
      CALL MATRX(PBV,P,PUN,3,6,6,1)
      WRITE OUTPUT TAPE NUTS,811,PUN
811 FORMAT(47H0 COVARIANCE MATRIX OF KNOWLEGE OF B*T,d*R,VINF
1/(3E20.8))
      IGUID = IGUID
      GO TO (23,22),IGUID
22 CONTINUE
      CALL MATRX(AO,PFTA,PFTA,6,6,6,1)
      DO 31 I=1,6
      DO 31 J=I,6
      PFTA(I,J)=(PFTA(I,J)+PFTA(J,I))/2.
      PFTA(J,I)=PFTA(I,J)
31 CONTINUE
      WRITE OUTPUT TAPE NUTS,804,((PTFA(I,J),J=1,6),I=1,6)
804 FORMAT(38H0 COVARIANCE MATRIX OF GUIDANCE ERRORS
1/(6E17.8))
      CALL INVAO(AO,AOI)
      CALL MATRX(TRANS,AOI,TRANS,3,6,6,0)

```

MAI11430
 MAI11440
 MAI11450
 MAI11460
 MAI11470
 MAI11480
 MAI11490
 MAI11500
 MAI11510
 MAI11511
 MAI11512
 MAI11514
 MAI11516
 MAI11518
 MAI11520
 MAI11530
 MAI11540
 MAI11550
 MAI11560
 MAI11570
 MAI11580
 MAI11590
 MAI11600
 MAI11610
 MAI11620
 MAI11630
 MAI11640
 MAI11650
 MAI11660
 MAI11670
 MAI11680
 MAI11690
 MAI11700
 MAI11710
 MAI11720
 MAI11730
 MAI11740
 MAI11750
 MAI11760
 MAI11770
 MAI11780
 MAI11781
 MAI11782
 MAI11784
 MAI11786
 MAI11788
 MAI11790
 MAI11800
 MAI11810
 MAI11820
 MAI11830

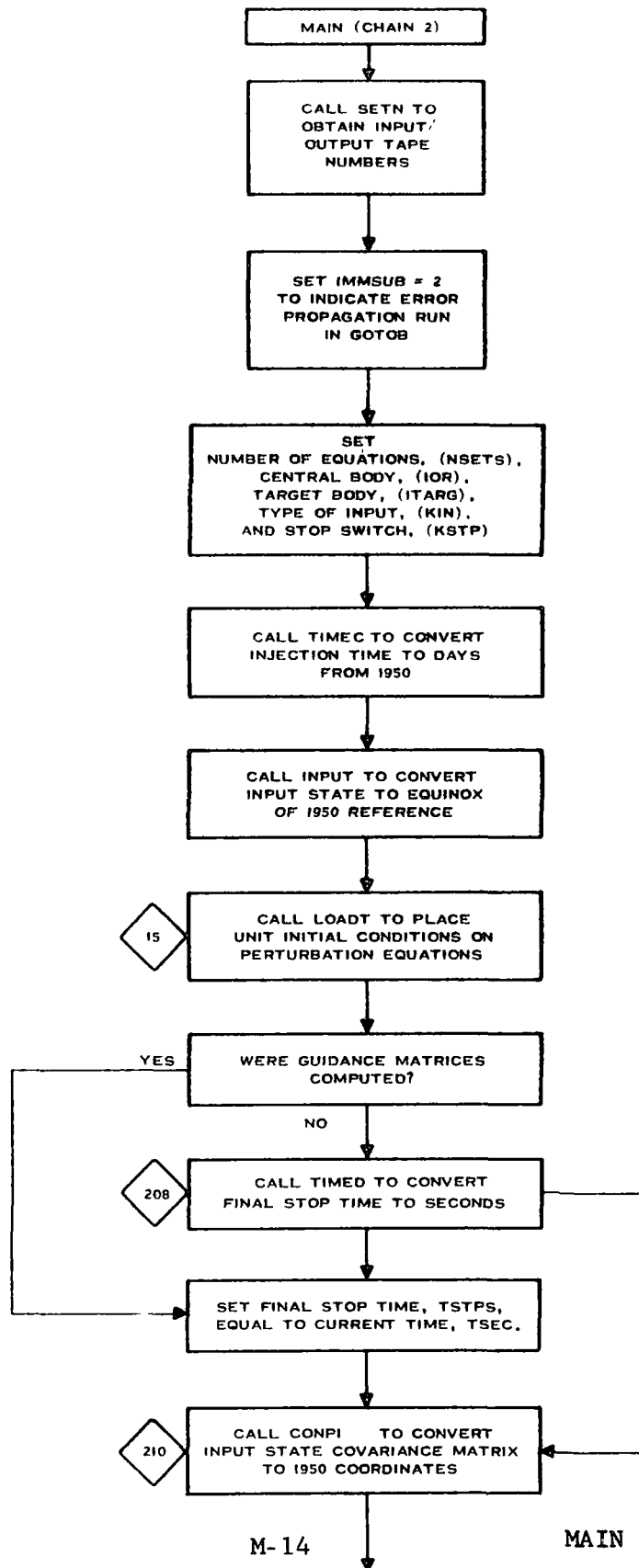
MAIN (CHAIN 1) (Cont'd)

	CALL MATRX(TRANS,P,PUN,3,6,6,1)	MAI1184
	WRITE OUTPUT TAPE NUTS,803,PUN	MAI1185
803	FORMAT(58H0 COVARIANCE MATRIX OF KNOWLEDGE OF TARGET MISS PARAMETE	MAI1186
	1RS	MAI1187
	2/(3E20.8))	MAI1188
	CALL MATRX(TRANS,PFTA,PUN,3,6,6,1)	MAI1189
	WRITE OUTPUT TAPE NUTS,807,PUN	MAI1190
807	FORMAT(45H0 COVARIANCE MATRIX OF TARGET MISS PARAMETERS	MAI1191
	1/(3E20.8))	MAI1192
	IF(RETR=.0001)23,23,10	MAI1192
10	CONTINUE	MAI1192
	CALL RETRO	MAI1192
23	CONTINUE	MAI1193
	RETR=0.	MAI1193
	GUID=0	MAI1194
	CIOMP=0	MAI1195
	GO TO 200	MAI1196
	END	MAI1

Subroutine: MAIN (Chain 2)

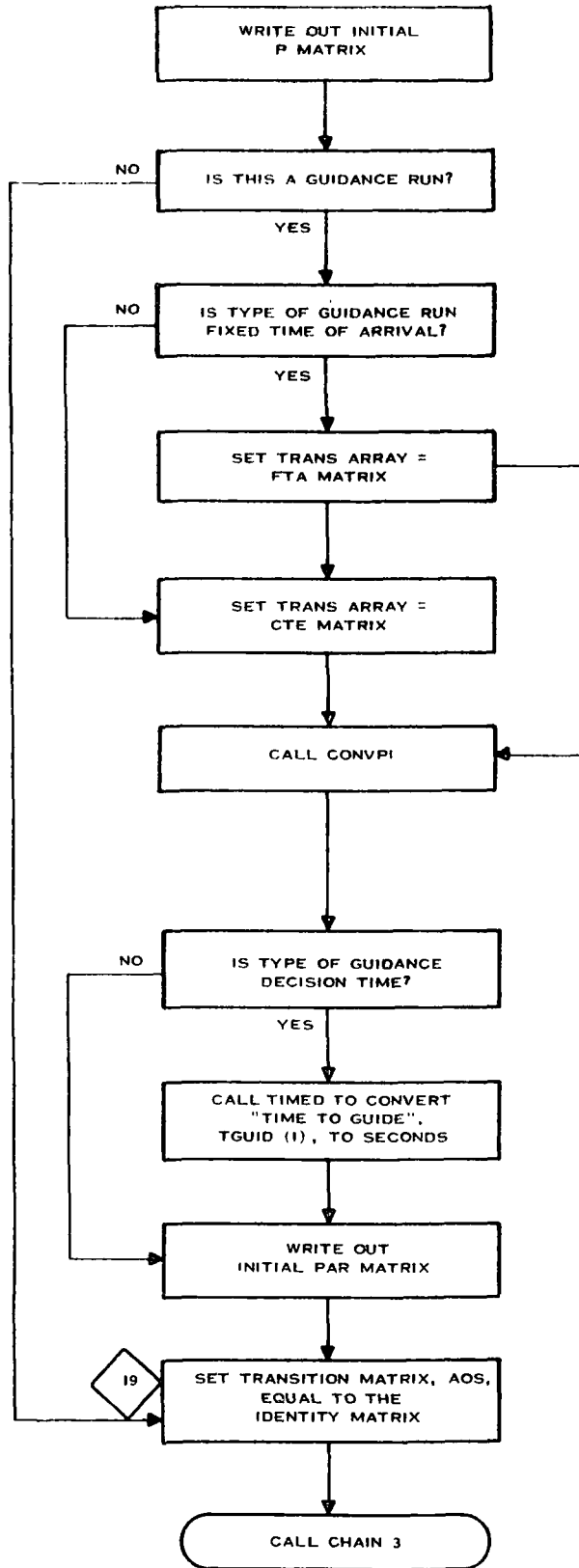
Purpose: Set up program to perform error propagation run. Call Chain 3 to make data run.

Common storages used or required:	<u>T, S, C, IC</u>
Subroutines required:	<u>CHAIN, CONVPI, INPUT, TIMEC, TIMED</u>
Functions required:	<u>None</u>
Approximate number of storages required:	<u>317 DEC</u>



M-14

MAIN (CHAIN 2) -2



M-15

MAIN (CHAIN 2) -3

MAIN (CHAIN 2)

* LABEL	MAI2
* SYMBOL TABLE	MAI2
CEC20E2 PART 2 MAIN CONTINUED	MAI20000
COMMON T,S,C,IC	MAI20010
·DIMENSION T(1360),S(1000),C(1000),IC(300),X(3)	MAI20020
1,VX(3),XP(3),VXP(3),AN(3,3),UM(6),BV(4),PBV(3,6)	MAI20030
·2,AO(6,6),PARI(21),PI(21),ISTAT(20),FTA(3,6)	MAI20040
·3,TRANS(3,6)	MAI20050
·4,PFTA(6,6),P(6,6),TGUID(6)	MAI20060
·DIMENSION AOS(6,6),RAD(6),RBOP(6),CTE(3,6),AOI(6,6),PUN(3,3)	MAI20070
·EQUIVALENCE(T,TDUM),(S,SDUM),(C,CDUM),(IC,IDUM),	MAI20080
1(IC(8),IMMSUB),(S(112),DATE),(S(113),FDATE),(S(115),X),(S(118),VX)	MAI20090
2,(IC(193),IGUID),(S(110),TSTOP),(IC(2),IOR),(S(111),TIM)	MAI20100
·3,(IC(6),ITARG),(IC(4),KSTP),(IC(1),NSETS),(C(10),TW),(C(11),TF)	MAI20110
·4,(C(138),AN),(C(12),TSECO),(S(71),STD),(S(1),UM),(C(15),XP)	MAI20120
·5,(C(18),VXP),(C(13),TP1),(C(14),TP2),(S(671),PI),(S(650),PARI)	MAI20130
·6,(IC(194),ISTAT),(IC(7),KOUT),(C(649),TSECP)	MAI20140
·7,(C(460),PFTA),(C(652),P)	MAI20150
·8,(S(114),CIBDY),(S(121),TIBDY),(S(722),FTA),(S(124),SKTB)	MAI20160
·9,(S(720),PUPIN),(S(721),PARIN)	MAI20170
·EQUIVALENCE(C(752),AOS),(S(900),RAD),(C(112),RBOP),(C(30),TSEC)	MAI20180
1,(S(740),CTE),(C(648),TGUIDE),(C(850),AOI),(C(850),PUN)	MAI20190
·EQUIVALENCE(S(476),TGUID),(IC(219),IGD)	MAI20200
·1,(IC(218),IGDKY),(IC(217),IGDTP),(C(568),TRANS)	MAI20210
·EQUIVALENCE(T(1358),TSTP),(C(797),COMP)	MAI20220
CALL SETN(NIN,NOUT)	MAI20225
IMMSUB=2	MAI20230
·NSETS=7	MAI20240
IOR =S(114)	MAI20250
ITARG=S(121)	MAI20260
KIN =S(111)	MAI20270
KSTP=S(124)	MAI20280
·CALL TIMEC(DATE,FDATE,TW,TF)	MAI20290
·CALL INPUT(KIN,XP,VXP,TW,TF,AN,X,VX)	MAI20300
TSECO =0.	MAI20310
·DO 15 I=1,20	MAI20320
ISTAT(I)=0	MAI20330
15 CONTINUE	MAI20340
KOUT=S(122)	MAI20350
·CALL LOADT	MAI20360
TSECP=0.	MAI20370
IF(COMP)208,208,209	MAI20380
208 CONTINUE	MAI20390
CALL TIMED(TSTOP,TSTPS)	MAI20400
GO TO 210	MAI20410
·209 TSTRS=TSEC	MAI20420
·210 CONTINUE	MAI20430
TSTP=TSTPS*STD	MAI20440
INPUP=PUPIN	MAI20450
CALL CONVPI(INPUP,PI,P)	MAI20460
WRITE OUTPUT TAPE NOUT,708	MAI20470

MAIN (CHAIN 2) (Cont'd)

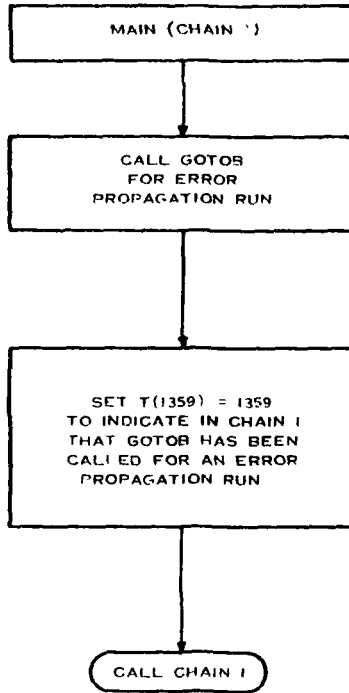
708	FORMAT(18H0INITIAL P MATRIX)	MAI20480
	WRITE OUTPUT TAPE (NOUT,709,P	MAI20490
709	FORMAT(6E17,8)	MAI20500
	IGUID=IGUID	MAI20510
	GO TO (19,18), IGUID	MAI20520
18	CONTINUE	MAI20530
	IGDTP=IGDTP	MAI20540
	GO TO(211,212,212),IGDTP	MAI20550
211	CONTINUE	MAI20560
	DO 202 I=1,3	MAI20570
	DO 202 J=1,6	MAI20580
	TRANS(I,J)=FTA(I,J)	MAI20590
202	CONTINUE	MAI20600
	GO TO 214	MAI20610
212	DO 213 I=1,3	MAI20620
	DO 213 J=1,6	MAI20630
213	TRANS(I,J)=CTE(I,J)	MAI20640
214	CONTINUE	MAI20650
	IGDKY=1	MAI20660
	INPAR=PARIN	MAI20670
	CALL CONVPI(INPAR,PARI,PFTA)	MAI20680
	S(475) CONTAINS TYPE OF GUIDANCE DECISION 0 TIME + RATIO	MAI20690
	IF(S(475))17,17,20	MAI20700
17	CONTINUE	MAI20710
	CALL TIMED(TGUID(1),TGUIDE)	MAI20720
20	CONTINUE	MAI20730
	WRITE OUTPUT TAPE (NOUT,710	MAI20740
710	FORMAT(20H0 INITIAL PAR MATRIX)	MAI20750
	WRITE OUTPUT TAPE (NOUT,709,PFTA	MAI20760
19	CONTINUE	MAI20770
	DO 150 I=1,6	MAI20780
	DO 151 J=1,6	MAI20790
151	AOS (I,J) =0,	MAI20800
150	AOS (I,I)=1,	MAI20810
	CALL CHAIN(3,B3)	MAI20820
	END	MAI2

Page Intentionally Left Blank

Subroutine: MAIN (Chain 3)

Purpose: Call subroutine GOTOB to perform integration of trajectory for an error propagation run. Set cell T(1359) = 1359 to indicate GOTOB has been called and call Chain 1.

Common storages used or required:	T
Subroutines required:	GOTOB
Functions required:	None
Approximate number of storages required:	



IN (CHAIN 3)

LABEL
SYMBOL TABLE
C20C2 CHAIN 3 GOTOB ONLY
COMMON T
DIMENSION T(1360)
EQUIVALENCE(T(1358),TSTP)
CALL GOTOB(TSTP)
T(1359)=1359,
CALL CHAIN(1,B3)
END

MAI3
MAI3
MAI30000
MAI30010
MAI30020
MAI30030
MAI30040
MAI30050
MAI30060
MAI3

MAIN (CHAIN 3) -3

M-21

Page Intentionally Left Blank

SUBROUTINES

(Subroutine discussion is presented in the following manner: (1) subroutine description, (2) subroutine flow diagrams, if applicable, (3) subroutine listings.)

Page Intentionally Left Blank


```

* LABEL
* SYMBOL TABLE
CEC2021 FUNCTION ARKTAN
CALL SETN(NIN,NOUT)
FUNCTION ARKTAN(N,X,Y)
D P=3.14159265
K=N/180
D ARKTAN = ATANF(ABSF(Y/X))
IF(Y)1,2,3
1 GO TO (4,5),K
4 IF (X)10,11,12
D 10 ARKTAN = ARKTAN=P
GO TO 9
D 11 ARKTAN = -P+.5
GO TO 9
D 12 ARKTAN = -ARKTAN
GO TO 9
5 IF (X)13,14,15
D 13 ARKTAN = P+ARKTAN
GO TO 9
D 14 ARKTAN = 3.*.5*P
GO TO 9
D 15 ARKTAN = 2.*P-ARKTAN
GO TO 9
2 IF (X)16,17,9
D 16 ARKTAN = P
GO TO 9
17 WRITE OUTPUT:TAPE NOUT,18
18 FORMAT (90H0
1 FAILED - ARKTAN(0/0) IS UNDEFINED/1H0)
GO TO 9
3 IF(X)8,19,9
D 8 ARKTAN = P-ARKTAN
GO TO 9
D 19 ARKTAN = .5*P
9 RETURN
END
    
```

```

ARKT
ARKT
ARKT0000
ARKT0015
ARKT0010
ARKT0020
ARKT0030
ARKT0040
ARKT0050
ARKT0060
ARKT0070
ARKT0080
ARKT0090
ARKT0100
ARKT0110
ARKT0120
ARKT0130
ARKT0140
ARKT0150
ARKT0160
ARKT0170
ARKT0180
ARKT0190
ARKT0200
ARKT0210
ARKT0220
ARKT0230
ARKT0240
ARKT0250
ARKT0260
ARKT0270
ARKT0280
ARKT0290
ARKT0300
ARKT0310
ARKT0320
ARKT
    
```

THE ARKTAN FUNCTION HAS

* LABEL	ARKS
* SYMBOL TABLE	ARKS
CEC2022 FUNCTION ARKTNS	ARKS0000
FUNCTION ARKTNS(N,X,Y)	ARKS0010
CALL SETN(NIN,NOUT)	ARKS0015
P=3.14159265	ARKS0020
K=N/180	ARKS0030
ARKTNS = ATANF(ABS(Y/X))	ARKS0040
IF(Y)1,2,3	ARKS0050
1 GO TO (4,5),K	ARKS0060
4 IF (X)10,11,12	ARKS0070
10 ARKTNS = ARKTNS-P	ARKS0080
GO TO 9	ARKS0090
11 ARKTNS = -P+.5	ARKS0100
GO TO 9	ARKS0110
12 ARKTNS = -ARKTNS	ARKS0120
GO TO 9	ARKS0130
5 IF (X)13,14,15	ARKS0140
13 ARKTNS = P+ARKTNS	ARKS0150
GO TO 9	ARKS0160
14 ARKTNS = 3.*.5*P	ARKS0170
GO TO 9	ARKS0180
15 ARKTNS = 2.*P-ARKTNS	ARKS0190
GO TO 9	ARKS0200
2 IF (X)16,17,9	ARKS0210
16 ARKTNS = P	ARKS0220
GO TO 9	ARKS0230
17 WRITE OUTPUT TAPE NOUT,18	ARKS0240
18 FORMAT (90H0	THE ARKTAN FUNCTION HAS
1 FAILED - ARKTAN(0/0) IS UNDEFINED/1H0)	ARKS0250
GO TO 9	ARKS0260
3 IF(X)8,19,9	ARKS0270
8 ARKTNS = P-ARKTNS	ARKS0280
GO TO 9	ARKS0290
19 ARKTNS = .5*P	ARKS0300
9 RETURN	ARKS0310
END	ARKS0320
	ARKS

Function: ASINH

Purpose: To compute $\theta = \operatorname{arcsinh}(X) = \log_e (X + \sqrt{X^2 + 1})$

Calling Sequence:
 $Y = \operatorname{ASINH}(X)$

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	X				
O	ASINH			radians	$\sinh^{-1}(X) = \log_e (X + \sqrt{X^2 + 1})$

Common storages used or required: None

Subroutines required: None

Functions required: LOGF

Approximate number of storages required: _____

ASINH

WDL-TR2184

```
* LABEL  
* SYMBOL TABLE  
FUNCTION ASINH(X)  
.ASINH=LOGF(X+SQRTF(X*X+1.0))  
RETURN  
END
```

```
ASIN  
ASIN  
ASIN000  
ASIN001U  
ASIN0020  
ASIN
```


Subroutine: BODY

Purpose: To compute the perturbing acceleration due to the perturbing bodies included in the ephemeris. It also computes the first variation of the perturbing acceleration for use in the integration of the variational equations.

Calling Sequence:

CALL BODY (XP, PO, VKB, RBO, RBOP, CA, NOR, BP, T, NEQ, U)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	XP	3	\vec{R}	Km	Position vector
I	PO	22	\vec{R}_i	Km	Positions of bodies in ephemeris
I	VKB	6	μ_i	Km^3/sec^2	Gravitational constants of bodies being considered
O	RBOP	6	$ \vec{R}_{iV} $	Km	Magnitude of position of vehicle relative to i th body
O	RBO	6	\vec{R}_i	Km	Position of i th body relative to central body

(Cont'd.)

Common storages used or required: None

Subroutines required: None

Functions required: FNORM

Approximate number of storages required: 445 DEC

(Cont'd.)

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
O	CA	3			Perturbation accelerations
I	NOR	1			Number of central body
O	BP	3,3	$\frac{\partial x_i}{\partial x_j}$		First variation of perturbation accelerations
I/O	T	1360			Common T Block
I	NEQ	1			Number of equations being integrated
I	U	1	μ	Km ³ /sec ²	Central body gravitational constant

Equation Being Solved

The perturbation term due to the n bodies being considered is:

$$\vec{P} = - \sum_{j=1}^n \mu_j \frac{\vec{R}_{jp}}{R_{jp}^3} + \frac{\vec{R}_j}{R_j^3}$$

where $\vec{R}_{jp} = \vec{R} - \vec{R}_j$.

The vector \vec{P} is placed in the cells called CA.

If the number of equations being solved is greater than three, the first variation of \vec{P} with respect to position is determined and placed in the T block for the integration package

$$AP = \frac{\partial \ddot{x}_i}{\partial x_j} \quad \begin{matrix} i = 1,3 \\ j = 1,3 \end{matrix}$$

The form of AP is obtained by differentiating

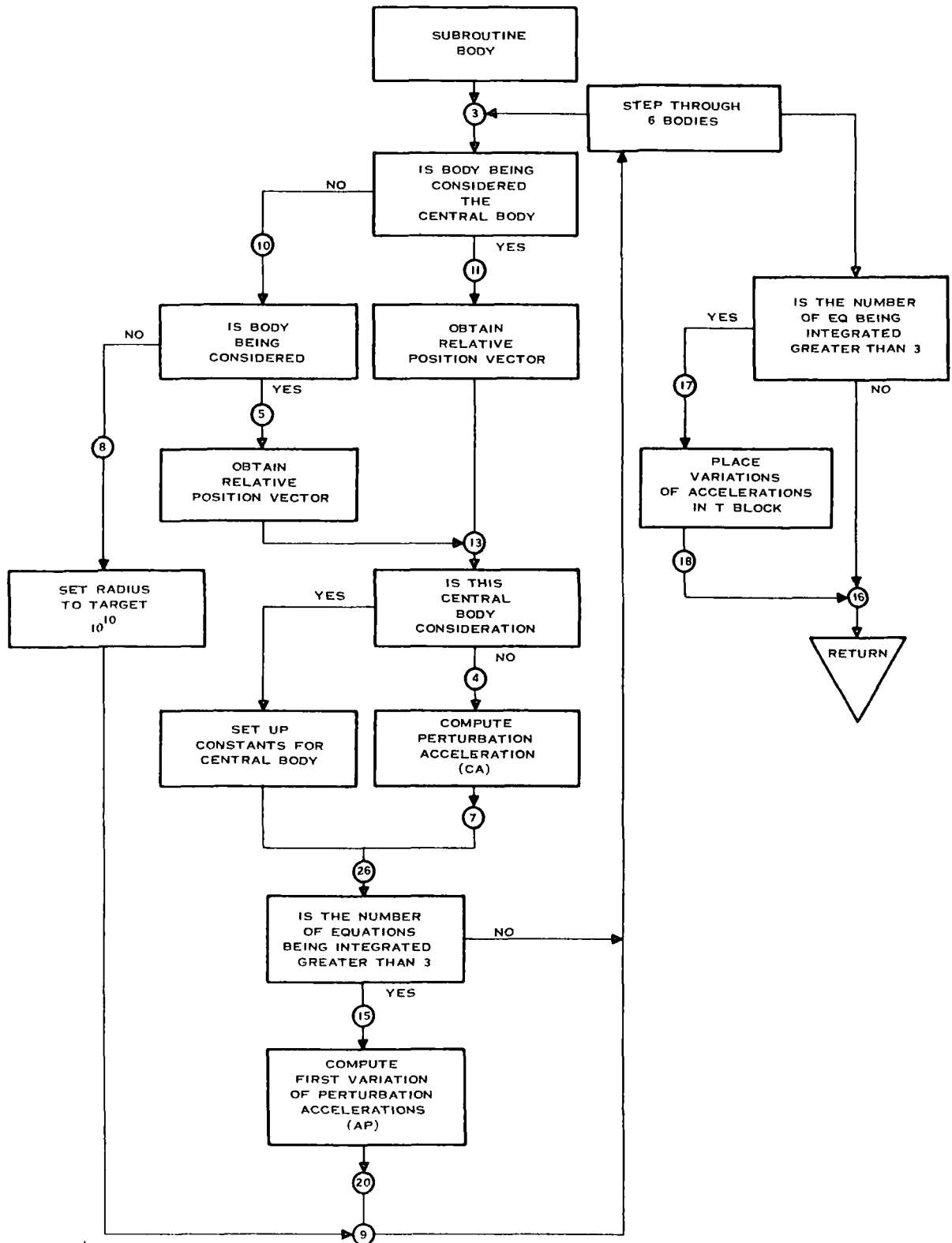
$$-\mu \frac{\vec{R}}{R^3} + \vec{P}$$

with respect to X_j . This yields:

$$AP_{ij} = - \sum_{k=0}^n \mu_k \left\{ \frac{1}{R_{kp}^3} \frac{\partial \vec{R}}{\partial X_j} - \frac{3}{R_{kp}^5} \left(\vec{R}_{kp} \cdot \frac{\partial \vec{R}}{\partial X_j} \right) \vec{R}_{kp} \right\}$$

with $\mu_0 = \mu$ and $\vec{R}_{0p} = \vec{R}$

$$\text{or } AP_{ij} = \sum_{k=0}^n \frac{\mu_k}{R_{kp}^3} \left\{ 3 \frac{\vec{R}_{kp} \vec{R}_{kp}^T}{R_{kp}^5} - I \right\}$$



* LABEL	BODY
* SYMBOL TABLE	BODY
SUBROUTINE BODY(X,PO,VKB,RBO,RBOP,CA,NOR,AP,T,NEQ,U)	BODY000
DIMENSION X(3),PO(22),VKB(6),RBO(6),RBOP(6),CA(3),XN(18),RJP(3),	BODY001
1AP(3,3),T(1360)	BODY002
N = NOR	BODY003
DO 1 I=1,15	BODY004
J = 23-I	BODY005
1 XN(I) = PO(J)	BODY006
DO 2 I=16,18	BODY007
J = 20-I	BODY008
2 XN(I) = PO(J)	BODY009
DO 3 I=1,3	BODY010
CA(I)=0.	BODY011
3 CONTINUE	BODY012
DO 9 I=1,6	BODY013
K1 = 3*I-3	BODY014
IF(I-N)10,11,10	BODY015
11 CONTINUE	BODY016
DO 12 J=1,3	BODY017
RJP(J)=X(J)	BODY018
12 CONTINUE	BODY019
GO TO 13	BODY020
10 CONTINUE	BODY021
IF (VKB(I)) 5,8,5	BODY022
5 DO 6 J=1,3	BODY023
K = K1+J	BODY024
RJP(J) = X(J) - XN(K)	BODY025
6 CONTINUE	BODY026
13 CONTINUE	BODY027
RBOP(I) = FNORM(RJP)	BODY028
RBO(I) = FNORM(XN(K1+1))	BODY029
R3 = RBOP(I)**3	BODY030
X3 = RBO(I)**3	BODY031
FAC=VKB(I)/R3	BODY032
FAX=VKB(I)/X3	BODY033
IF(I-N)4,23,4	BODY034
4 CONTINUE	BODY035
C ACCELERATIONS (NEGATIVE) DUE TO PERTURRING BODIES	BODY036
DO 7 J=1,3	BODY037
K1J = K1 + J	BODY038
CA(J)=CA(J)+FAC*RJP(J)+FAX*XN(K1J)	BODY039
7 CONTINUE	BODY040
GO TO 26	BODY041
23 CONTINUE	BODY042
FAC=U/R3	BODY043
FAX=U/X3	BODY044
26 CONTINUE	BODY045
DO 24 J=1,3	BODY046
RJP(J)=RJP(J)/RBOP(I)	BODY047
24 CONTINUE	BODY048

BODY - 5

C	RJP IS NOW A UNIT VECTOR	BODY0490
	IF(NEQ-3)14,14,15	BODY0500
15	CONTINUE	BODY0510
C	PARTIALS FOR PERTURBATION EQUATIONS	BODY0520
	DO 20 J=1,3	BODY0530
	J=J	BODY0540
	DO 20 K=J,3	BODY0550
	AP(J,K)=AP(J,K)+FAC*(3.*RJP(J)*RJP(K))	BODY0560
	IF(J-K)21,22,21	BODY0570
21	CONTINUE	BODY0580
	AP(K,J)=AP(J,K)	BODY0590
	GO TO 20	BODY0600
22	CONTINUE	BODY0610
	AP(J,J)=AP(J,J)-FAC	BODY0620
20	CONTINUE	BODY0630
25	FORMAT(3E16,8)	BODY0640
14	CONTINUE	BODY0650
	GO TO 9	BODY0660
8	RBOP(I) = 1,E10	BODY0670
9	CONTINUE	BODY0680
	NS=NEQ/3-1	BODY0690
	IF(NS)16,16,17	BODY0700
16	CONTINUE	BODY0710
	RETURN	BODY0720
17	CONTINUE	BODY0730
	DO 18 I=1,NS	BODY0740
	NST=2*NEQ+3*3*I	BODY0750
	NSTP=3+3*I	BODY0760
	DO 19 J=1,3	BODY0770
	KK=NST+J	BODY0780
	T(KK)=0.	BODY0790
	DO 19 K=1,3	BODY0800
	JJ=NSTP+K	BODY0810
	T(KK)=T(KK)+AP(J,K)*T(JJ)	BODY0820
19	CONTINUE	BODY0830
18	CONTINUE	BODY0840
	GO TO 16	BODY0850
	END	BODY

Subroutine: BVEC

Purpose: To obtain the matrix of target miss partials; B·T, B·R, and V infinity with respect to the state.

Calling Sequence:

CALL BVEC (IOR, ITARG, X, V, BV, PBV, TW, TF, UM)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	IOR	1			Central body
I	ITARG	1			Target body
I	X	3	\vec{R}		Position vector
I	V	3	\vec{U}		Velocity vector
O	BV	4			Nominal Miss Parameters
O	PBV	(3,6)			Matrix of Miss Partial
I	TW	1	t	days	Whole days from 1950
I	TF	1	t	days	Fractional days from 1950
I	UM	1	μ	Km ³ /sec ²	Gravitational constant

Common storages used or required:

None

Subroutines required:

DOT, INTRI, CROSS

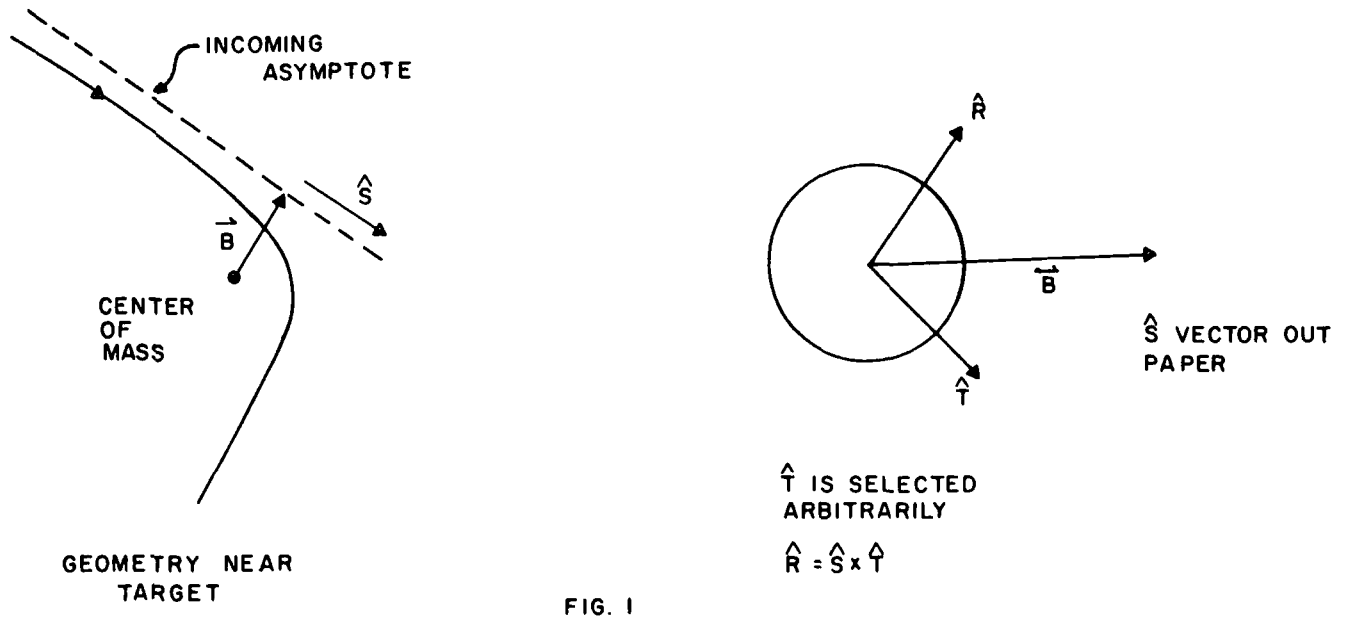
Functions required:

FNORM

Approximate number of storages required:

Derivation of the \vec{B} , \hat{S} , \hat{T} , and \hat{R} vectors

The B , R , S , and T vectors are used to define a target miss (see Fig. 1 below)



\vec{B} , the position vector in the plane of the trajectory originating at the center of gravity of the target and directed perpendicularly to the incoming asymptote of the hyperbola, is approximately the vector miss which would occur if the target had no mass.

To determine the target miss direction relative to the target, a set of orthogonal vectors is computed. Let \hat{S} be a unit vector in the direction of the incoming asymptote, \hat{T} be a unit vector perpendicular to \hat{S} that lies in a fixed plane of interest such as the equatorial plane, and \hat{R} be a unit vector to form a right-handed system.

$$\hat{R} = \hat{S} \times \hat{T}$$

Since \vec{B} is perpendicular to \hat{S} , it lies in the plane determined by \hat{R} and \hat{T} . The variables which are used to describe the miss relative to a plane of interest are the projections of \vec{B} on \hat{T} and \hat{R} , i.e., $\vec{B} \cdot \hat{T}$ and $\vec{B} \cdot \hat{R}$.

The quantities used in the derivation of the vectors are the following:

$$h = |\vec{R} \times \vec{v}| \quad C_3 = v^2 - \frac{2\mu}{R}$$

$$e = \sqrt{1 + \frac{h^2 C_3}{\mu^2}} \quad p = \frac{h^2}{\mu}$$

True anomaly

$$\theta = \cos^{-1} \left[\frac{1}{e} \left(\frac{p}{R} - 1 \right) \right]$$

Unit vectors to specify orientation of conic

$$\vec{\zeta} = \frac{\vec{R} \times \vec{v}}{|\vec{R} \times \vec{v}|} \quad \vec{M} = \vec{\zeta} \times \frac{\vec{R}}{|\vec{R}|}$$

$$\vec{\xi} = \frac{\vec{R}}{|\vec{R}|} \cos \theta - \vec{M} \sin \theta$$

$$\vec{h} = \vec{\zeta} \times \vec{\xi}$$

The unit vector in the direction of the asymptote is given by

$$\hat{S} = \frac{1}{e} \vec{\xi} + \sqrt{1 - \left(\frac{1}{e}\right)^2} \vec{n}$$

The impact parameter

$$\vec{B} = |\vec{B}| \left[\sqrt{1 - \left(\frac{1}{e}\right)^2} \vec{s} - \frac{1}{e} \vec{n} \right]$$

where $|\vec{B}| = \frac{\mu}{c^3} \sqrt{e^2 - 1}$

Also
$$T_X = \frac{S_Y}{\sqrt{S_X^2 + S_Y^2}}$$

$$T_Y = - \frac{S_X}{\sqrt{S_X^2 + S_Y^2}}$$

$$T_Z = 0$$

and
$$\hat{R} = \hat{S} \times \hat{T}$$

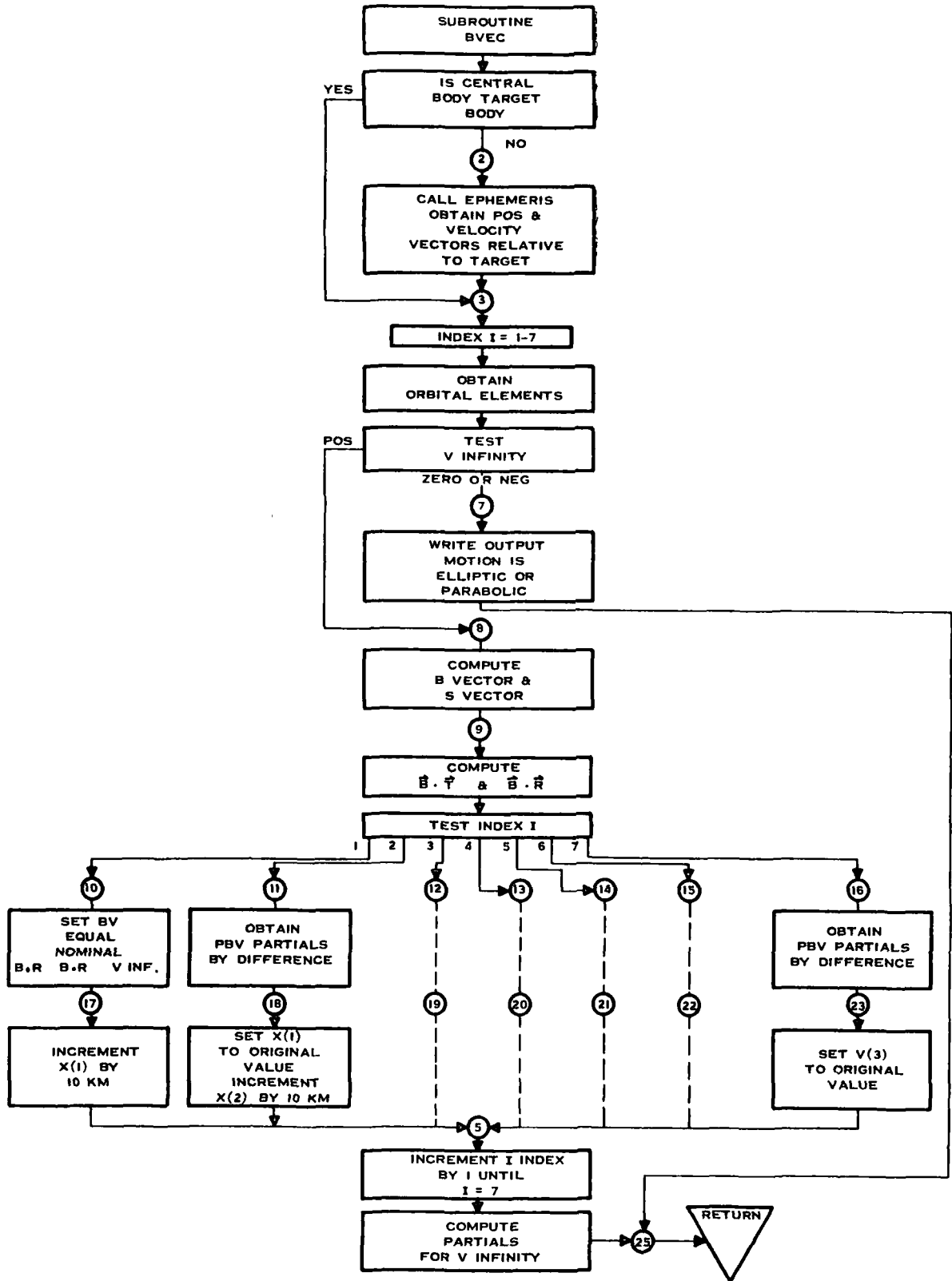
Derivation of partials of V infinity with respect to the state

$$V_{INF} = \sqrt{v^2 - \frac{2\mu}{R}}$$

$$\frac{\partial V_{INF}}{\partial X_i} = \frac{\mu X_i}{(V_{INF}) R^3} \quad i = 1, 2, 3$$

$$\frac{\partial V_{INF}}{\partial X_i} = \frac{X_i}{(V_{INF})} \quad i = 1, 2, 3$$

Reference: JPL EXTERNAL PUBLICATION NO. 674



* LABEL	BVEC
* SYMBOL TABLE	BVEC
CEC2001 SUBROUTINE BVEC	BVEC0000
SUBROUTINE BVEC (IOR,ITARG,X,V,BV,PBV,TW,TF,UM)	BVEC0010
DIMENSION X(3),V(3),XP(3),VP(3),BV(4),PBV(3,6),PO(22),VE(22)	BVEC0020
1,BD(3),CP(3),RB(3),RM(3),UM(6),PP(3),QQ(3),S(3),B(3),RR(3),TT(3)	BVEC0030
CALL SETN(NIN,NOUT)	BVEC0035
D=2,E6	BVEC0040
DO 1 I=1,3	BVEC0050
XP(I)=X(I)	BVEC0060
VP(I)=V(I)	BVEC0070
1 CONTINUE	BVEC0080
IF (IOR=ITARG) 2,3,2	BVEC0090
2 CONTINUE	BVEC0100
N=IOR=1	BVEC0110
CALL INTR1(TW,TF,N,PO,1,VE,D)	BVEC0120
IC=26=3*ITARG	BVEC0130
DO 4 I=1,3	BVEC0140
IB=IC-I	BVEC0150
XP(I)=XP(I)=PO(IB)	BVEC0160
VP(I)=VP(I)=VE(IB)	BVEC0170
4 CONTINUE	BVEC0180
3 CONTINUE	BVEC0190
DO 5 I=1,7	BVEC0200
CALL CROSS(XP,VP,CP)	BVEC0210
D=FNORM(CP)	BVEC0220
R=FNORM(XP)	BVEC0230
DO 6 J=1,3	BVEC0240
CP(J)=CP(J)/D	BVEC0250
RB(J)=XP(J)/R	BVEC0260
6 CONTINUE	BVEC0270
CALL CROSS(CP,RB,RM)	BVEC0280
U=UM(ITARG)	BVEC0290
C3=DOT(VP,VP)=2.*U/R	BVEC0300
IF (C3) 7,7,8	BVEC0310
7 CONTINUE	BVEC0320
WRITE OUTPUT TAPE NOUT,100	BVEC0330
100 FORMAT(32H MOTION IS ELLIPTIC OR PARABOLIC)	BVEC0340
GO TO 25	BVEC0350
8 CONTINUE	BVEC0360
P=D**2/U	BVEC0370
E2=1.+P*C3/U	BVEC0380
E = SQRTF(E2)	BVEC0390
A=U/C3	BVEC0400
SEM2=E2-1.	BVEC0410
SEM1=SQRTF(SEM2)	BVEC0420
ASE=A+SEM2/E	BVEC0430
SE = SEM1/E	BVEC0440
RDOT=DOT(XP,VP)/R	BVEC0450
CTHET=(P-R)/(E+R)	BVEC0460
STHET=(RDOT*SQRTF(P/U))/E	BVEC0470

BVEC - 6

```

DO 9 J=1,3
PP(J)=CTHET*RB(J)-STHET*RM(J)
QQ(J)=STHET*RB(J)+CTHET*RM(J)
S(J)=PP(J)/E+SE*QQ(J)
B(J)=ASE*PP(J)-A*SE*QQ(J)
9 CONTINUE
S2=SQRTF(S(1)**2+S(2)**2)
TT(1)=S(2)/S2
TT(2)=-S(1)/S2
TT(3)=0,
CALL CROSS(S,TT,RR)
BD(1)=DOT(B,TT)
BD(2)=DOT(B,RR)
I=I
GO TO (10,11,12,13,14,15,16),I
10 CONTINUE
DO 17 J=1,2
BV(J)=BD(J)
17 CONTINUE
BV(3)=SQRTF(C3)
XP(1)=XP(1)+10.
GO TO 5
11 CONTINUE
DO 18 J=1,2
PBV(J,1)=(BD(J)-BV(J))/10.
18 CONTINUE
XP(1)=XP(1)-10.
XP(2)=XP(2)+10.
GO TO 5
12 CONTINUE
DO 19 J=1,2
PBV(J,2)=(BD(J)-BV(J))/10.
19 CONTINUE
XP(2)=XP(2)-10.
XP(3)=XP(3)+10.
GO TO 5
13 CONTINUE
DO 20 J=1,2
PBV(J,3)=(BD(J)-BV(J))/10.
20 CONTINUE
XP(3)=XP(3)-10.
VP(1)=VP(1)+.01
GO TO 5
14 CONTINUE
DO 21 J=1,2
PBV(J,4)=(BD(J)-BV(J))*100.
21 CONTINUE
VP(1)=VP(1)+.01
VP(2)=VP(2)+.01
GO TO 5
15 CONTINUE

```

BVEC0480
BVEC0490
BVEC0500
BVEC0510
BVEC0520
BVEC0530
BVEC0540
BVEC0550
BVEC0560
BVEC0570
BVEC0580
BVEC0590
BVEC0600
BVEC0610
BVEC0620
BVEC0630
BVEC0640
BVEC0650
BVEC0660
BVEC0670
BVEC0680
BVEC0690
BVEC0700
BVEC0710
BVEC0720
BVEC0730
BVEC0740
BVEC0750
BVEC0760
BVEC0770
BVEC0780
BVEC0790
BVEC0800
BVEC0810
BVEC0820
BVEC0830
BVEC0840
BVEC0850
BVEC0860
BVEC0870
BVEC0880
BVEC0890
BVEC0900
BVEC0910
BVEC0920
BVEC0930
BVEC0940
BVEC0950
BVEC0960
BVEC0970
BVEC0980

DO 22 J=1,2	BVEC0990
PBV(J,5)=(BD(J)-BV(J))*100.	BVEC1000
22 CONTINUE	BVEC1010
VP(2)=VP(2)-.01	BVEC1020
VP(3)=VP(3)+.01	BVEC1030
GO TO 5	BVEC1040
16 CONTINUE	BVEC1050
DO 23 J=1,2	BVEC1060
PBV(J,6)=(BD(J)-BV(J))*100.	BVEC1070
23 CONTINUE	BVEC1080
VP(3)=VP(3)-.01	BVEC1090
5 CONTINUE	BVEC1100
VIN=SQRTF(C3)	BVEC1110
UR2=1.*U/R**3	BVEC1120
UR3=UR2/VIN	BVEC1130
DO 24 I=1,3	BVEC1140
J=I+3	BVEC1150
PBV(3,J)=VP(I)/VIN	BVEC1160
PBV(3,I)=UR3*XP(I)	BVEC1170
24 CONTINUE	BVEC1180
25 CONTINUE	BVEC1190
RETURN	BVEC1200
END	BVEC

Subroutine: CHNGP

Purpose: To choose the appropriate body center as a function of distance from the present central body.

Calling Sequence:

CALL CHNGP (NOR, IOR, RAD)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
O	NOR	1			New body center
I	IOR	1			Present body center
I	RAD	6		Kn.	RAD(I) = distance from body I to vehicle

Common storages used or required: None

Subroutines required: None

Functions required: None

Approximate number of storages required:

Method of Selecting Body Center

<u>Present Central Body</u>	<u>New Central Body</u>	
1) Earth	Sun	$R_1 \geq 25 \times 10^5$
	Earth	$R_2 \geq 3 \times 10^4$
	Moon	$R_2 \leq 3 \times 10^4$
2) Moon	Moon	$R_2 < 3 \times 10^4$
	Earth	$R_2 \geq 3 \times 10^4$
3) Sun	Earth	$R_1 \leq 25 \times 10^5$
	Venus	$R_4 < 25 \times 10^5$
	Mars	$R_5 < 25 \times 10^5$
	Jupiter	$R_6 < 25 \times 10^5$
	Sun	(if none of above)
4) Venus	Venus	$R_4 < 25 \times 10^5$
	Sun	$R_4 \geq 25 \times 10^5$
5) Mars	Mars	$R_5 < 25 \times 10^5$
	Sun	$R_5 \geq 25 \times 10^5$
6) Jupiter	Jupiter	$R_6 \geq 25 \times 10^5$
	Sun	$R_6 < 25 \times 10^5$

where $R_i = \text{RAD}(I) = \text{distance from body (i) to the vehicle.}$

LABEL	CHNG
SYMBOL TABLE:	CHNG
C2002	CHNG
SUBROUTINE CHNGP(NOR, IOR, RAD)	CHNG0000
DIMENSION RAD(6)	CHNG0010
IO = IOR	CHNG0020
NOR = IOR	CHNG0025
GO TO (1,2,3,4,4,4), IO	CHNG0030
1 IF (RAD(1)-2500000.) 11,12,12	CHNG0040
11 IF (RAD(2)-30000.) 13,14,14	CHNG0050
12 NOR = 3	CHNG0060
GO TO 14	CHNG0070
13 NOR = 2	CHNG0080
14 RETURN	CHNG0090
2 IF (RAD(2)-30000.) 14,21,21	CHNG0100
21 NOR = 1	CHNG0110
GO TO 14	CHNG0120
3 IF (RAD(1)-2500000.) 31,31,32	CHNG0130
31 NOR = 1	CHNG0140
GO TO 14	CHNG0150
32 DO 34 I=4,6	CHNG0160
IF (RAD(I)-2500000.) 33,34,34	CHNG0170
33 NOR = I	CHNG0180
GO TO 14	CHNG0190
34 CONTINUE	CHNG0200
GO TO 14	CHNG0210
4 IF (RAD(IO)-2500000.) 14,41,41	CHNG0220
41 NOR = 3	CHNG0230
GO TO 14	CHNG0240
END	CHNG

Page Intentionally Left Blank

Subroutine: COMPHQ

Purpose: To compute the H matrix of measurement partials with respect to the vehicle state and the variance of the measurements. The subroutine is called by ONBTR, on-board tracking subroutine, and MONBTR, the moon beacon tracking subroutine. The types of measurements which are evaluated are range, right ascension, declination, and range rate. After computation of the H matrix and the measurement error, subroutine CORRTP is called to perform the filtering of the measurement and updating of the state covariance matrix, P.

Calling Sequence:

CALL COMPHQ (JJJ, KK, NN)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	JJJ	1			Type of measurement
I	KK	1			On-board or moon beacon
I	NN	1			Key for locating constants in storage

Common storages used or required: T, S, C, IC

Subroutines required: CORRTP, DOT

Functions required: SQRT

Approximate number of storages required: 388 DEC

Calling Sequence Elaboration

The calling sequence of COMPHQ consists of CALL COMPHQ (JJJ, KK, NN) where:

JJJ is a key which indicates the type of measurement being performed.

1. Range
2. Right ascension
3. Declination
4. Range rate

KK is a key which indicates if the measurements being made are:
(1) on-board measurements or (2) moon beacons.

NN is a key which is used to obtain constants out of the common S array.

COMPHQ Partial Derivatives

To perform the covariance matrix updating for on-board observations and moon based beacons, a number of partial derivatives are required. The partials are derived in the following paragraphs.

The following quantities and relationships are used in the derivations. The vehicle's position, \vec{X} , and velocity, $\dot{\vec{X}}$, relative to the celestial body or moon beacon are obtained from common. These vectors may be written as:

$$\vec{X} = \begin{pmatrix} X_1 \\ X_2 \\ X_3 \end{pmatrix} = -\vec{X}_V + \vec{X}_B = \begin{pmatrix} -X_V + X_B \\ -Y_V + Y_B \\ -Z_V + Z_B \end{pmatrix}$$

$$\dot{\vec{X}} = \begin{pmatrix} \dot{X}_1 \\ \dot{X}_2 \\ \dot{X}_3 \end{pmatrix} = -\dot{\vec{X}}_V + \dot{\vec{X}}_B$$

Two relationships which will be used in the derivation are:

$$\frac{\partial \text{PAR}}{\partial \vec{X}} = - \frac{\partial \text{PAR}}{\partial \vec{X}_V}$$

$$\frac{\partial \text{PAR}}{\partial \dot{\vec{X}}} = - \frac{\partial \text{PAR}}{\partial \dot{\vec{X}}_V}$$

The FORTRAN program names for the above vector are as follows:

<u>FORTTRAN</u> <u>NAME</u>	<u>DIMENSION</u>	<u>DERIVATION</u> <u>NAME</u>	<u>DIMENSION</u>
XREL	(3)	\vec{X}	(3)
VREL	(3)	$\dot{\vec{X}}$	(3)

The quantities being measured are the following:

$$R = \text{RANGE} = |\vec{X}| = (\vec{X} \cdot \vec{X})^{1/2}$$

$$R = \text{Range Rate} = \frac{d}{dt} |\vec{X}| = \frac{\vec{X} \cdot \dot{\vec{X}}}{R}$$

$$\text{RA} = \tan^{-1} \left\{ \frac{X_2}{X_1} \right\}$$

$$\text{DEC} = \sin^{-1} \left\{ \frac{X_3}{R} \right\}$$

- A. The following is a derivation of the partials relating the types of measurements and the vehicle state. In the program, these partials are used as a row vector. The FORTRAN name of the vector is H. H may be written as follows:

$$H = \left(\frac{\partial \text{MEAS}}{\partial X_V}; \frac{\partial \text{MEAS}}{\partial Y_V}; \frac{\partial \text{MEAS}}{\partial Z_V}; \frac{\partial \text{MEAS}}{\partial \dot{X}_V}; \frac{\partial \text{MEAS}}{\partial \dot{Y}_V}; \frac{\partial \text{MEAS}}{\partial \dot{Z}_V} \right)$$

(1) Derivation of partials for range measurement.

$$R = (\vec{X} \cdot \vec{X})^{1/2}$$

$$H_R = \left(\frac{\partial R}{\partial \vec{X}_V}; \frac{\partial R}{\partial \vec{X}_V} \right) = \left(-\frac{X_1}{R}; -\frac{X_2}{R}; -\frac{X_3}{R}; 0; 0; 0 \right)$$

(2) Derivation of partials for range rate measurement.

$$\dot{R} = \frac{\vec{X} \cdot \dot{\vec{X}}}{R}$$

$$H_{RR} = \left(\frac{\partial \dot{R}}{\partial \vec{X}_V}; \frac{\partial \dot{R}}{\partial \dot{\vec{X}}_V} \right) = \left(-\frac{\dot{X}_1}{R} + \frac{\dot{R}}{R^2} X_1; -\frac{\dot{X}_2}{R} + \frac{\dot{R}}{R^2} X_2; -\frac{\dot{X}_3}{R} + \frac{\dot{R}}{R^2} X_3; \right.$$

$$\left. \frac{X_1}{R}; \frac{X_2}{R}; \frac{X_3}{R} \right)$$

(3) Derivation of partials for right ascension measurement.

$$RA = \tan^{-1} \left(\frac{X_2}{X_1} \right) \equiv \tan^{-1} \gamma$$

$$\frac{\partial RA}{\partial PAR} = (1 + \gamma^2)^{-1} \frac{\partial \gamma}{\partial PAR}$$

$$(1 + \gamma^2)^{-1} = \frac{X_1^2}{X_1^2 + X_2^2}$$

$$H_{RA} = \left(\frac{\partial RA}{\partial \vec{X}_V}; \frac{\partial RA}{\partial \dot{\vec{X}}_V} \right) = \left(\frac{X_2}{X_1^2 + X_2^2}; \frac{X_1}{X_1^2 + X_2^2}; 0; 0; 0; 0 \right)$$

(4) Derivation of partials for declination measurement.

$$\text{DEC} = \text{Sin}^{-1} \left(\frac{X_3}{R} \right) \equiv \text{Sin}^{-1} \gamma$$

$$\frac{\partial \text{DEC}}{\partial \text{PAR}} = [1 - \gamma^2]^{-1/2} \frac{\partial \gamma}{\partial \text{PAR}}$$

$$[1 - \gamma^2]^{-1/2} = \frac{R}{\sqrt{X_1^2 + X_2^2}}$$

$$H_{\text{DEC}} = \left(\frac{\partial \text{DEC}}{\partial \vec{X}_V}; \frac{\partial \text{DEC}}{\partial \vec{X}_V} \right) = \left(\frac{X_1 X_3}{\sqrt{X_1^2 + X_2^2} R^2}; \frac{X_2 X_3}{R^2 \sqrt{X_1^2 + X_2^2}}; \frac{\sqrt{X_1^2 + X_2^2}}{R^2}; \right. \\ \left. 0; 0; 0 \right)$$

B. In order to include errors in the measurements being made due to station location errors and time bias, the partials of the measurements with respect to latitude, longitude, altitude, and time are required. In the program, the station location errors are used as a row vector with FORTRAN name DUM. DUM may be written as follows:

$$\text{DUM} = \left(\frac{\partial \text{MEAS}}{\partial \text{LAT}}; \frac{\partial \text{MEAS}}{\partial \text{LON}}; \frac{\partial \text{MEAS}}{\partial \text{ALT}} \right)$$

The following matrices are obtained from MONBTR and used in the computation of DUM.

$$\text{STPARS} = \begin{pmatrix} \frac{\partial X_1}{\partial \text{LAT}} & \frac{\partial X_1}{\partial \text{LON}} & \frac{\partial X_1}{\partial \text{ALT}} \\ \frac{\partial X_2}{\partial \text{LAT}} & \frac{\partial X_2}{\partial \text{LON}} & \frac{\partial X_2}{\partial \text{ALT}} \\ \frac{\partial X_3}{\partial \text{LAT}} & \frac{\partial X_3}{\partial \text{LON}} & \frac{\partial X_3}{\partial \text{ALT}} \end{pmatrix}$$

$$\text{STPARD} = \begin{pmatrix} \frac{\partial \dot{X}_1}{\partial \text{LAT}} & \frac{\partial \dot{X}_1}{\partial \text{LON}} & \frac{\partial \dot{X}_1}{\partial \text{ALT}} \\ \frac{\partial \dot{X}_2}{\partial \text{LAT}} & \frac{\partial \dot{X}_2}{\partial \text{LON}} & \frac{\partial \dot{X}_2}{\partial \text{ALT}} \\ \frac{\partial \dot{X}_3}{\partial \text{LAT}} & \frac{\partial \dot{X}_3}{\partial \text{LON}} & \frac{\partial \dot{X}_3}{\partial \text{ALT}} \end{pmatrix}$$

(1) Derivation of range measurement error partials.

$$\frac{\partial R}{\partial LAT} = \sum_{i=1}^3 \frac{\partial R}{\partial X_i} \frac{\partial X_i}{\partial LAT}$$

$$\frac{\partial R}{\partial LAT} = \sum_{i=1}^3 -H_R(1, i) \text{ STPARS}(i, 1)$$

Similarly

$$\frac{\partial R}{\partial LON} = \sum_{i=1}^3 -H_R(1, i) \text{ STPARS}(i, 2)$$

$$\frac{\partial R}{\partial ALT} = \sum_{i=1}^3 -H_R(1, i) \text{ STPARS}(i, 3)$$

(2) Derivation of range rate measurement error partials.

$$\frac{\partial \dot{R}}{\partial LAT} = \sum_{i=1}^3 \frac{\partial \dot{R}}{\partial X_i} \frac{\partial X_i}{\partial LAT} + \frac{\partial \dot{R}}{\partial \dot{X}_i} \frac{\partial \dot{X}_i}{\partial LAT}$$

$$\frac{\partial \dot{R}}{\partial LAT} = \sum_{i=1}^3 -H_{RR}(1, i) \text{ STPARS}(i, 1) - H_{RR}(1, i+3) \text{ STPARD}(i, 1)$$

Similarly

$$\frac{\partial \dot{R}}{\partial LON} = \sum_{i=1}^3 -H_{RR}(1, i) \text{ STPARS}(i, 2) - H_{RR}(1, i+3) \text{ STPARD}(i, 2)$$

$$\frac{\partial \dot{R}}{\partial \text{ALT}} = \sum_{i=1}^3 -H_{RR}(1,i) \text{STPARS}(i,3) - H_{RR}(1,i+3) \text{STPARD}(i,3)$$

(3) Derivation of right ascension measurement error partials.

$$\frac{\partial \text{RA}}{\partial \text{LAT}} = \sum_{i=1}^3 \frac{\partial \text{RA}}{\partial X_i} \frac{\partial X_i}{\partial \text{LAT}}$$

$$\frac{\partial \text{RA}}{\partial \text{LAT}} = \sum_{i=1}^3 -H_{RA}(1,i) \text{STPARS}(i,1)$$

Similarly

$$\frac{\partial \text{RA}}{\partial \text{LON}} = \sum_{i=1}^3 -H_{RA}(1,i) \text{STPARS}(i,2)$$

$$\frac{\partial \text{RA}}{\partial \text{ALT}} = \sum_{i=1}^3 -H_{RA}(1,i) \text{STPARS}(i,3)$$

(4) Derivation of declination measurement error partials.

$$\frac{\partial \text{DEC}}{\partial \text{LAT}} = \sum_{i=1}^3 \frac{\partial \text{DEC}}{\partial X_i} \frac{\partial X_i}{\partial \text{LAT}}$$

$$\frac{\partial \text{DEC}}{\partial \text{LAT}} = \sum_{i=1}^3 -H_{DEC}(1,i) \text{STPARS}(i,1)$$

Similarly

$$\frac{\partial \text{DEC}}{\partial \text{LON}} = \sum_{i=1}^3 -H_{DEC}(1,i) \text{STPARS}(i,2)$$

$$\frac{\partial \text{DEC}}{\partial \text{ALT}} = \sum_{i=1}^3 -H_{\text{DEC}}(1,i) \text{STPARS}(i,3)$$

- (5) Derivation of time derivatives of measurement quantities to permit inclusion of time bias errors.

$$\frac{\partial R}{\partial t} = \dot{R} = \frac{\vec{X} \cdot \dot{\vec{X}}}{R}$$

$$\frac{\partial \text{RA}}{\partial t} = \sum_{i=1}^3 \frac{\partial \text{RA}}{\partial X_i} \frac{\partial X_i}{\partial t}$$

$$\frac{\partial \text{RA}}{\partial t} = \sum_{i=1}^3 -H_{\text{RA}}(1,i) \dot{X}_i$$

Similarly

$$\frac{\partial \text{DEC}}{\partial t} = \sum_{i=1}^3 -H_{\text{DEC}}(1,i) \dot{X}_i$$

The errors in the measurements are computed in the following manner for station location errors and time bias.

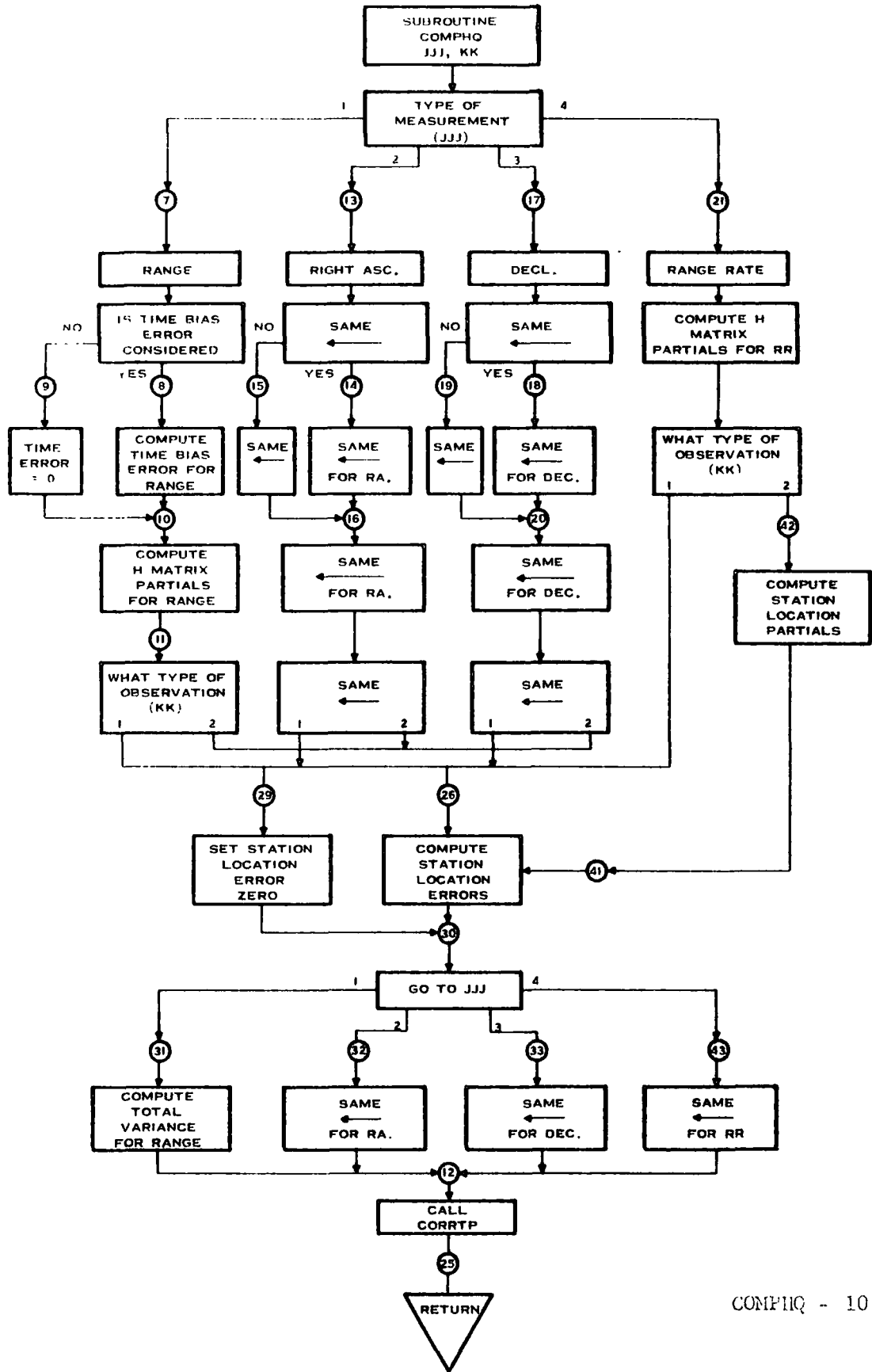
$$\text{QQSTAT} = \left(\text{DUM}_{\text{MEAS}} \right)^2 \begin{pmatrix} \sigma^2_{\text{LAT}} \\ \sigma^2_{\text{LON}} \\ \sigma^2_{\text{ALT}} \end{pmatrix}$$

Station
Location
Error

1×1 1×3 3×1

$$QQDOT = \left(\frac{\partial MEAS}{\partial t} \cdot \sigma_{TIME} \right)^2 \quad \text{Time Bias Error}$$

The computation of the H matrices and the measurement errors are the primary computations in COMPHQ. COMPHQ calls CORRTP which uses quantities to update the state covariance matrix.



COMPHQ - 10

* LABEL	COMP
* SYMBOL TABLE	COMP
CEC2008 SUBROUTINE COMPHQ	COMP
SUBROUTINE COMPHQ(JJJ, KK, NN)	COMP0000
COMMON T, S, C, IC	COMP0010
DIMENSION T(1360), S(1000), C(1000), IC(1)	COMP0020
1, XREL(3), VREL(3), H(6), P(6,6), STPARS(3,3), DUM(3), OUTPUT(6)	COMP0025
DIMENSION STPARD(3,3)	COMP0030
EQUIVALENCE (T, TDUM), (S, SDUM), (C, CDUM), (IC, ICDUM)	COMP0040
1, (C(895), XREL), (C(898), VREL), (C(894), OBNO), (C(893), XMAG),	COMP0050
2(C(892), DEX), (C(891), DEN1), (C(890), DEN2), (C(788), STPARS)	COMP0060
3, (C(889), DEX2), (C(888), DEX3), (C(652), P), (C(973), OUTPUT)	COMP0065
4, (S(73), RTD)	COMP0070
EQUIVALENCE (C(800), STPARD)	COMP0075
KK 1=ONBOARD MEASUREMENTS 2=MOON BEACONS	COMP0080
JJJ 1=RANGE 2=RIGHT ASC. 3=DECL. 4=RANGE RATE	COMP0090
NN=NN	COMP0100
JJJ=JJJ	COMP0110
KK=KK	COMP0120
NNN=NN/5+657	COMP0130
GO TO (7, 13, 17, 21), JJJ	COMP0140
7 CONTINUE	COMP0150
IF(S(NN+8))9,9,8	COMP0160
8 CONTINUE	COMP0170
GET HERE TO COMPUTE ERROR IN RANGE OBS. DUE TO TIME BIAS.	COMP0180
RDOT=DOT(XREL, VREL)*DEX3	COMP0190
RDOT=RANGE RATE	COMP0200
OUTPUT(2)=RDOT	COMP0205
RDOT2=RDOT*RDOT	COMP0210
QQRDOT=RDOT2*S(NN+8)	COMP0220
QQRDOT=RANGE VARIANCE DUE TO TIME BIAS	COMP0230
GO TO 10	COMP0240
9 CONTINUE	COMP0250
QQRDOT=0.	COMP0260
10 CONTINUE	COMP0270
THE FOLLOWING ARE H MATRIX CALCULATIONS FOR RANGE	COMP0280
DO 11 I=1,3	COMP0290
K=I+3	COMP0300
H(I)=-XREL(I)*DEX3	COMP0310
H(K)=0.	COMP0320
11 CONTINUE	COMP0330
GO TO (29, 26), KK	COMP0340
31 CONTINUE	COMP0350
QQ=S(NN)/OBNO+S(NN+4)+QQRDOT+S(425)*XMAG**2+QQSTAT	COMP0360
QQ=TOTAL RANGE VARIANCE=INSTR.*BIAS+TIME BIAS ERROR+SPEED LIGHT	COMP0370
+STATION LOCATION ERRORS	COMP0380
12 CONTINUE	COMP0390
CALL CORRTP (QQ, H, P)	COMP0400
CORRTP UPDATES COVARIANCE MATRIX FOR MEASUREMENT	COMP0410
GO TO 25	COMP0420
13 CONTINUE	COMP0430

	IF(S(NN+8))15,15,14	COMP0440
14	CONTINUE	COMP0450
C	GET HERE TO COMPUTE ERROR IN RA MEASUREMENT DUE TO CLOCK BIAS	COMP0460
	RADOT=(VREL(2)*XREL(1)-VREL(1)*XREL(2))*DEN2	COMP0470
	CUTPUT(4)=RADOT*RTD	COMP0475
C	RADOT=RIGHT ASCENSION RATE	COMP0480
	RADOT2=RADOT*RADOT	COMP0490
	QQRADT=RADOT2*S(NN+8)	COMP0500
C	QQRADT=RIGHT ASCENSION VARIANCE DUE TO TIME BIAS	COMP0510
	GO TO 16	COMP0520
15	CONTINUE	COMP0530
	QGRADT=0.	COMP0540
16	CONTINUE	COMP0550
C	THE FOLLOWING ARE H MATRIX CALCULATIONS FOR RA	COMP0560
	H(6)=0.	COMP0570
	H(5)=0.	COMP0580
	H(4)=0.	COMP0590
	H(3)=0.	COMP0600
	H(1)= XREL(2)*DEN2	COMP0610
	H(2)=-XREL(1)*DEN2	COMP0620
	GO TO (29,26),KK	COMP0630
32	CONTINUE	COMP0640
	QQ=S(NN+1)/OBNO+S(NN+5)+QQRADT+QQSTAT	COMP0650
C	QQ=TOTAL RIGHT ASCENSION VARIANCE	COMP0660
	GO TO 12	COMP0670
17	CONTINUE	COMP0680
	IF(S(NN+8))19,19,18	COMP0690
18	CONTINUE	COMP0700
C	GET HERE TO COMPUTE ERROR IN DEC.MEAS.DUE TO CLOCK BIAS	COMP0710
	CRUD=XREL(1)*VREL(1)+XREL(2)*VREL(2)	COMP0720
	CRUD2=VREL(3)*DEX-XREL(3)*CRUD	COMP0730
	DEDOT=CRUD2/(SQRTF(DEX)*DEX2)	COMP0740
	OUTPUT(6)=DEDOT*RTD	COMP0745
	DEDOT2=DEDOT*DEDOT	COMP0750
	QQDEDT=DEDOT2*S(NN+8)	COMP0760
C	QQDEDT=DECLINATION VARIANCE DUE TO TIME BIAS	COMP0770
	GO TO 20	COMP0780
19	CONTINUE	COMP0790
	QQDEDT=0.	COMP0800
20	CONTINUE	COMP0810
C	THE FOLLOWING ARE H MATRIX COMP. FOR DECLINATION	COMP0820
	H(4)=0.	COMP0830
	H(5)=0.	COMP0840
	H(6)=0.	COMP0850
	H(1)= XREL(1)*XREL(3)*DEN1	COMP0860
	H(2)= XREL(2)*XREL(3)*DEN1	COMP0870
	H(3)=-DEX+DEN1	COMP0880
	GO TO (29,26),KK	COMP0890
33	CONTINUE	COMP0900
	QQ=S(NN+2)/OBNO+S(NN+6)+QQDEDT+QQSTAT	COMP0910
C	QQ=TOTAL DECLINATION VARIANCE	COMP0920

```

GO TO 12
21 CONTINUE
THE FOLLOWING ARE H MATRIX COMP. FOR RANGE RATE
RDOT=DOT(XREL,VREL)*DEX3
OUTPUT(2)=RDOT
DO 22 J=1,3
K=J+3
H(K)=XREL(J)*DEX3
H(J)=DEX3*(VREL(J)+H(K)*RDOT)
22 CONTINUE
GO TO (29,42),KK
42 CONTINUE
DO 40 I=1,3
DUM(I)=0.
DO 40 J=1,3
JJ=J+3
40 DUM(I)=DUM(I)+H(J)*STPARS(J,I)+H(JJ)*STPARD(J,I)
GO TO 41
43 CONTINUE
QQ=S(NN+3)/OBNO+S(NN+7)*QQSTAT
QQ=RANGE RATE VARIANCE
GO TO 12
26 CONTINUE
THE FOLLOWING COMPUTATIONS ARE FOR STATION LOCATION ERRORS
DO 27 I=1,3
DUM(I)=0.
DO 27 J=1,3
DUM(I)=DUM(I)+H(J)*STPARS(J,I)
27 CONTINUE
41 CONTINUE
QQSTAT=0.
DO 28 I=1,3
L=NNN+I
QQSTAT=QQSTAT+(DUM(I)**2)*S(L)
28 CONTINUE
GO TO 30
29 CONTINUE
QQSTAT=0.
30 CONTINUE
GO TO(31,32,33,43),JJJ
25 CONTINUE
RETURN
END

```

COMP093
 COMP094
 COMP095
 COMP096
 COMP096
 COMP097
 COMP098
 COMP099
 COMP100
 COMP100
 COMP100
 COMP100
 COMP100
 COMP101
 COMP101
 COMP101
 COMP101
 COMP101
 COMP101
 COMP102
 COMP102
 COMP102
 COMP102
 COMP102
 COMP103
 COMP104
 COMP105
 COMP106
 COMP107
 COMP108
 COMP109
 COMP110
 COMP111
 COMP111
 COMP111
 COMP112
 COMP113
 COMP114
 COMP115
 COMP116
 COMP117
 COMP118
 COMP119
 COMP120
 COMP121
 COMP122
 COMP123
 COMP

Page Intentionally Left Blank

Subroutine: CONST1

Purpose: To read permanent or semipermanent constants into the common S array.

Calling Sequence:

CALL CONST1

Input and Output

Common storages used or required:	<u>T, S</u>
Subroutines required:	<u>None</u>
Functions required:	<u>None</u>
Approximate number of storages required:	<u>669 DEC</u>

* LABEL	CONS
* SYMBOL TABLE	CONS
CEC2026 SUBROUTINE CONST1	CONS
SUBROUTINE CONST1	CONS0000
COMMON T,S	CONS0010
DIMENSION T(1360),S(1000)	CONS0020
EQUIVALENCE (T,TDUM),(S,SDUM)	CONS0030
C PLANETARY MASSES 1-6,	CONS0040
C PLANETARY MASSES 1-6 ,ORDER EARTH,MOON,SUN,VENUS,MARS,JUPITER	CONS0050
C -KM**3/SEC2	CONS0060
S(1)=398603,2	CONS0070
S(2)=4900.7588	CONS0080
S(3)=.13271545E12	CONS0090
S(4)=324769,50	CONS0100
S(5)=42915.515	CONS0110
S(6)=.12671059E9	CONS0120
C 6-9 ARE SPARES	CONS0130
C 10-19 ARE EARTH CONSTANTS,RATE,J,H,D,EQUAT RAD,POLAR RAD	CONS0140
C RAD/SEC	CONS0150
S(10)=7.2921152E-5	CONS0160
S(11)=.162345E-2	CONS0170
S(12)=-.575E-5	CONS0180
S(13)=.7875E-5	CONS0190
S(14)=6378.2064	CONS0200
S(15)=6356.5838	CONS0210
C 20-29 ARE MOON CONSTANTS ,G,A,B,C,RAD	CONS0220
S(20)=.6671E-19	CONS0230
S(21)=.88746E29	CONS0240
S(22)=.88764E29	CONS0250
S(23)=.88801E29	CONS0260
S(24)=1738.	CONS0270
C 30-59 SUN CONSTANTS	CONS0280
C 40-49 VENUS CONSTANTS	CONS0290
C 50-59 MARS CONSTANTS	CONS0300
C 60-69 JUPITER CONSTANTS	CONS0310
C CONVERSION FACTOR DAYS TO SECONDS	CONS0320
S(70)=86400.	CONS0330
C CONVERSION FACTOR SECONDS TO DAYS	CONS0340
S(71)=1./S(70)	CONS0350
C CONVERSION FACTOR FOR DEGREES TO RADIANS	CONS0360
S(72)=.017453296	CONS0370
C CONVERSION FACTOR FOR RADIANS TO DEGREES	CONS0380
S(73)=57.29578	CONS0390
S(80)=28.48713	CONS0400
S(81)=279.42315	CONS0410
S(82)=.00257	CONS0420
S(84)=90.	CONS0430
C 111 IS TYPE OF INPUT(1)EQUATOR 1950 (2)EQUATOR OF DATE(3)	CONS0440
C EARTH-FIXED	CONS0450
C (4),(5),(6) ARE SPHERICAL INPUT IN, RESPECTIVELY, (1),(2),(3)	CONS0460
C 112 AND 113 ARE(YEAR MONTH.DAY)(HOUR MIN.SEC) OF INJECTION DATE	CONS0470

C	114 IS CENTRAL BODY NUMBER, (1)EARTH, (2)MOON (3)SUN (4)VENUS (5)		CONS04
C	MARS (6)JUPITER		CONS04
C	115-120 ARE INPUT STATE CORRESPONDING TO S(111) THRU 114,		CONS05
C	121 TARGET BODY		CONS05
C	122 TYPE OF OUTPUT; KOUT		CONS05
	S(121)=2.		CONS05
C	123 TSECO		CONS05
C	N GOES FROM 0 TO 19		CONS05
C	(125)+N*15 VARIANCE OF RANGE	KM**2	CONS05
C	(126)+N*15 VARIANCE OF AZIMUTH	RAD**2	CONS05
C	(127)+N*15 VARIANCE OF ELEVATION	RAD**2	CONS05
C	(128)+N*15 VARIANCE OF RANGE RATE	KM**2/SEC**2	CONS05
C	(129)+N*15 VARIANCE OF LATITUDE	RAD**2	CONS06
C	(130)+N*15 VARIANCE OF LONGITUDE	RAD**2	CONS06
C	(131)+N*15 VARIANCE OF ALTITUDE	KM**2	CONS06
C	(132)+N*15 VARIANCE OF AZIMUTH BIASES	RAD**2	CONS06
C	(133)+N*15 VARIANCE OF ELEVATION BIASES	RAD**2	CONS06
C	(134)+N*15 LATITUDE OF STATION	DEG	CONS06
C	(135)+N*15 LONGITUDE OF STATION	DEG	CONS06
C	(136)+N*15 ALTITUDE OF STATION	KM	CONS06
C	(137)+N*15 STATION NAME		CONS06
C	(138)+N*15 PERIOD OF OBSERVATION	SEC	CONS06
C	(139)+N*15 VARIANCE OF TIME BIAS	SEC**2	CONS07
C	STATION 1 ANTIGUA RADAR 91.1		CONS07
	S(125)=.000225		CONS07
	S(126)=.000004		CONS07
	S(127)=.000004		CONS07
	S(128)=.00000001		CONS07
	S(129)=.0000000001		CONS07
	S(130)=.0000000001		CONS07
	S(131)=.0001		CONS07
	S(134)=17.0267		CONS07
	S(135)=298.2247		CONS08
	S(136)=0.		CONS08
	S(137)=6HANTIG		CONS08
	S(138)=1.		CONS08
C	STATION 2 ASCENSION RADAR 12.16		CONS08
	S(140)=.000225		CONS08
	S(141)=.000004		CONS08
	S(142)=.000004		CONS08
	S(143)=.00000001		CONS08
	S(144)=.0000000001		CONS08
	S(145)=.0000000001		CONS09
	S(146)=.0001		CONS09
	S(149)=7.898		CONS09
	S(150)=345.587393		CONS09
	S(151)=0.		CONS09
	S(152)=6HASCENS		CONS09
	S(153)=1.		CONS09
C	STATION 3 MILLSTONE HILL RADAR		CONS09
	S(155)=.000225		CONS09

S(156)=,000004
 S(157)=,000004
 S(158)=,00000001
 S(159)=,0000000001
 S(160)=,0000000001
 S(161)=,0001
 S(164)=42.4232
 S(165)=288.5080
 S(166)=0.
 S(167)=6HMILHIL
 S(168)=1.

CONS0990
 CONS1000
 CONS1010
 CONS1020
 CONS1030
 CONS1040
 CONS1050
 CONS1060
 CONS1070
 CONS1080
 CONS1090

C

STATION 4 MOBILE STATION MTS

S(170)= 2500.E-6
 S(171)= .04 E-6
 S(172)= .04 E-6
 S(173)= .04 E-6
 S(174)= 1. E-10
 S(175)= 1. E-10
 S(176)= 9. E-6
 S(177)= .0016E-6
 S(178)= .0016E-6
 S(179)=-25.88472
 S(180)= 27.70528
 S(181)= 1.54302
 S(182)=6HMOBMTS
 S(183)= 30.
 S(184)= 9.E-6

CONS1100
 CONS1110
 CONS1120
 CONS1130
 CONS1140
 CONS1150
 CONS1160
 CONS1170
 CONS1180
 CONS1190
 CONS1200
 CONS1210
 CONS1220
 CONS1230
 CONS1240

C

STATION 5 AMR TRACKER GE

S(185)=,000225
 S(186)=,000004
 S(187)=,000004
 S(188)=,00000001
 S(189)=,0000000001
 S(190)=,0000000001
 S(191)=,0001
 S(194)=28.278103
 S(195)=279.418297
 S(196)=0.
 S(197)=6HGEMR
 S(198)=1.

CONS1250
 CONS1260
 CONS1270
 CONS1280
 CONS1290
 CONS1300
 CONS1310
 CONS1320
 CONS1330
 CONS1340
 CONS1350
 CONS1360
 CONS1370
 CONS1380

C

STATION 6 BERMUDA

S(200)=,000225
 S(201)=,000004
 S(202)=,000004
 S(203)=,00000001
 S(204)=,0000000001
 S(205)=,0000000001
 S(206)=,0001
 S(209)=32.160973
 S(210)=295.299179
 S(211)=0.

CONS1390
 CONS1400
 CONS1410
 CONS1420
 CONS1430
 CONS1440
 CONS1450
 CONS1460
 CONS1470
 CONS1480
 CONS1490

	S(212)=6HBERMUD	CONS15
	S(213)=1.	CONS15
C	STATION 7 GOLDSTONE RECEIVER	CONS15
C	50M SIG	CONS15
	S(215) =2500.E-6	CONS15
C	.2MIL	CONS15
	S(216) =.04 E-6	CONS15
C	.2MIL	CONS15
	S(217) =.04 E-6	CONS15
C	.2M/SEC	CONS15
	S(218) =.04 E-6	CONS16
C	63.78M	CONS16
	S(219) =1.E=10	CONS16
C	63.78M	CONS16
	S(220) =1.E=10	CONS16
C	3M	CONS16
	S(221) =9.E=6	CONS16
C	.04MR	CONS16
	S(222) =.0016E-6	CONS16
C	.04MR	CONS16
	S(223) =.0016E-6	CONS16
	S(224) =35.3895	CONS17
	S(225) =243.15175	CONS17
	S(226) =1.03754	CONS17
	S(227)=6HGOSTRC	CONS17
	S(228) =30.	CONS17
	S(229) =9.E=6	CONS17
C	STATION 8 GOLDSTONE TRANSMITTER	CONS17
	S(230)=.000225	CONS17
	S(231)=.000004	CONS17
	S(232)=.000004	CONS18
	S(233)=.00000001	CONS18
	S(234)=.0000000001	CONS18
	S(235)=.0000000001	CONS18
	S(236)=.0001	CONS18
	S(239) =35.29985	CONS18
	S(240) =243.19539	CONS18
	S(241) =.98949	CONS18
	S(242)=6HGOSTTR	CONS18
	S(243)=1.0	CONS18
C	STATION 9 GBI RADAR XN=2	CONS19
	S(245)=.000225	CONS19
	S(246)=.000004	CONS19
	S(247)=.000004	CONS19
	S(248)=.00000001	CONS19
	S(249)=.0000000001	CONS19
	S(250)=.0000000001	CONS19
	S(251)=.0001	CONS19
	S(254)=26.459736	CONS19
	S(255)=281.651892	CONS19
	S(256)=0.	CONS20

S(257)=6HGBIRAD
 S(258)=1.0
 C STATION 10 JOHANNESBURG
 C 50M SIG
 S(260) =2500.E-6
 C .2MIL
 S(261) =.04 E-6
 C .2MIL
 S(262) =.04 E-6
 C .2M/SEC
 S(263) =.04 E-6
 C 63.78M
 S(264) =1.E-10
 C 63.78M
 S(265) =1.E-10
 C 3M SIG
 S(266) = 9.E-6
 C .04MR
 S(267) = .0016E-6
 C .04MR
 S(268) = .0016E-6
 C DEG
 S(269) =-25,88735
 C DEG
 S(270) = 27,68478
 C KM
 S(271) = 1,38192
 S(272)=6HJOHABG
 C SEC
 S(273) = 30,
 C 3MS SIG
 S(274) = 9.E-6
 C STATION IN HAWAII
 S(275)=,000225
 S(276)=,000004
 S(277)=,000004
 S(278)=,00000001
 S(279)=,0000000001
 S(280)=,0000000001
 S(281)=,0001
 S(284)=18,823066
 S(285)=204,314722
 S(286)=0,
 S(287)=6HHAWAII
 S(288)=1,0
 C STATION 12 JODRELL BANK
 S(290)=,000225
 S(291)=,000004
 S(292)=,000004
 S(293)=,00000001
 S(294)=,0000000001

CONS2010
 CONS2020
 CONS2030
 CONS2040
 CONS2050
 CONS2060
 CONS2070
 CONS2080
 CONS2090
 CONS2100
 CONS2110
 CONS2120
 CONS2130
 CONS2140
 CONS2150
 CONS2160
 CONS2170
 CONS2180
 CONS2190
 CONS2200
 CONS2210
 CONS2220
 CONS2230
 CONS2240
 CONS2250
 CONS2260
 CONS2270
 CONS2280
 CONS2290
 CONS2300
 CONS2310
 CONS2320
 CONS2330
 CONS2340
 CONS2350
 CONS2360
 CONS2370
 CONS2380
 CONS2390
 CONS2400
 CONS2410
 CONS2420
 CONS2430
 CONS2440
 CONS2450
 CONS2460
 CONS2470
 CONS2480
 CONS2490
 CONS2500
 CONS2510

S(295)=.0000000001

CONS25

S(296)=.0001

CONS25

S(299)=53.049636

CONS25

S(300)=357.693889

CONS25

S(301)=0.

CONS25

S(302)=6HJODBNK

CONS25

S(303)=1.0

CONS25

C STATION 13 PUERTO RICO RADAR 9.1

CONS25

S(305)=.000225

CONS26

S(306)=.000004

CONS26

S(307)=.000004

CONS26

S(308)=.00000001

CONS26

S(309)=.0000000001

CONS26

S(310)=.0000000001

CONS26

S(311)=.0001

CONS26

S(314)=18.060396

CONS26

S(315)=292.911805

CONS26

S(316)=0.

CONS26

S(317)=6HPURICO

CONS27

S(318)=1.0

CONS27

C STATION 14 SAN SALVADORE

CONS27

S(320)=.000225

CONS27

S(321)=.000004

CONS27

S(322)=.000004

CONS27

S(323)=.00000001

CONS27

S(324)=.0000000001

CONS27

S(325)=.0000000001

CONS27

S(326)=.0001

CONS27

S(329)=23.173566

CONS28

S(330)=285.4956

CONS28

S(331)=0.

CONS28

S(332)=6HSANSAL

CONS28

S(333)=1.0

CONS28

C STATION 15 WOOMERA

CONS28

C 50W SIG

CONS28

S(335) = 2500.E-6

CONS28

.2MIL

CONS28

S(336) = .04E-6

CONS28

.2MIL

CONS29

S(337) = .04E-6

CONS29

.2M/SEC

CONS29

S(338) = .04E-6

CONS29

63.78M

CONS29

S(339) = 1.E-10

CONS29

63.78M

CONS29

S(340) = 1.E-10

CONS29

3M

CONS29

S(341) = .9.E-6

CONS29

.04MR

CONS30

S(342) = .0016E-6

CONS30

.04MR

CONS30

S(343) = .0016E-6
 S(344) = -31,38287
 S(345) = 136,88502
 S(346) = .15079
 S(347) = 6HWOMERA
 C SEC
 S(348) = 30.
 C 3MS
 S(349) = 9.E-6
 C STATION 16 JPL CAPE CANAUERAL
 S(350) = .000225
 S(351) = .000004
 S(352) = .000004
 S(353) = .00000001
 S(354) = .0000000001
 S(355) = .0000000001
 S(356) = .0001
 C DEG
 S(359) = 28,48713
 C DEG
 S(360) = 279.42315
 C KM
 S(361) = .00257
 S(362) = 6HCAPJET
 S(363) = 1.0
 C 425 = SPEED OF LIGHT ACCURACY
 C STATION 17 MAJUNGA
 S(369) = .0000000001
 S(370) = .0000000001
 S(371) = .0001
 S(374) = -15,216666
 S(375) = 46.38333
 S(377) = 6HMAJUNG
 S(378) = 30.
 C STATION 18 CARNARVCN
 S(384) = .0000000001
 S(385) = .0000000001
 S(386) = .0001
 S(389) = -24,8666
 S(390) = 113.63333
 S(392) = 6HCARNVN
 S(393) = 30.
 C STATION 19 ROSMAN
 S(399) = .0000000001
 S(400) = .0000000001
 S(401) = .0001
 S(404) = 35.20000
 S(405) = 277.1333
 S(407) = 6HROSMAN
 S(408) = 30.
 S(425) = 1.E-12

CONS3030
 CONS3040
 CONS3050
 CONS3060
 CONS3070
 CONS3080
 CONS3090
 CONS3100
 CONS3110
 CONS3120
 CONS3130
 CONS3140
 CONS3150
 CONS3160
 CONS3170
 CONS3180
 CONS3190
 CONS3200
 CONS3210
 CONS3220
 CONS3230
 CONS3240
 CONS3250
 CONS3260
 CONS3265
 CONS3270
 CONS3271
 CONS3272
 CONS3273
 CONS3274
 CONS3275
 CONS3276
 CONS3277
 CONS3278
 CONS3279
 CONS3280
 CONS3281
 CONS3282
 CONS3283
 CONS3284
 CONS3285
 CONS3286
 CONS3287
 CONS3288
 CONS3289
 CONS3290
 CONS3291
 CONS3292
 CONS3293
 CONS3294
 CONS3295

C FROM S(426) TO S(470) IS ONBOARD ERROR DATA

- S(475)=1.0
- S(476)=100.
- S(477)=200.
- S(478)=300.
- S(479)=400.
- S(480)=500.
- S(481)=600.
- S(485)=.03

CONS330
 CONS331
 CONS332
 CONS333
 CONS334
 CONS335
 CONS336
 CONS337
 CONS338

C N GOES FROM 0 TO 9 LUNAR BASED BEACONS

- C (500)+N*15 VARIANCE OF RANGE KM2
- C (501)+N*15 VARIANCE OF AZIMUTH RAD2
- C (502)+N*15 VARIANCE OF ELEVATION RAD2
- C (503)+N*15 VARIANCE OF RANGE RATE KM2/SEC2
- C (504)+N*15 VARIANCE OF LATITUDE RAD2
- C (505)+N*15 VARIANCE OF LONGITUDE RAD2
- C (506)+N*15 VARIANCE OF ALTITUDE KM2
- C (507)+N*15 VARIANCE OF AZIMUTH BIAS RAD2
- C (508)+N*15 VARIANCE OF ELEVATION BIAS RAD2
- C (509)+N*15 LATITUDE OF STATION DEG
- C (510)+N*15 LONGITUDE OF STATION DEG
- C (511)+N*15 ALTITUDE OF STATION KM
- C (512)+N*15 STATION NAME
- C (513)+N*15 PERIOD OF OBSERVATION SEC
- C (514)+N*15 SPARE
- C (650) TO (685) IS INITIAL P MATRIX
- C (686) TO (721) INITIAL RAR MATRIX
- C (722) TO (739) TRANSITION MATRIX FTA GUIDANCE

CONS339
 CONS340
 CONS341
 CONS342
 CONS343
 CONS344
 CONS345
 CONS346
 CONS347
 CONS348
 CONS349
 CONS350
 CONS351
 CONS352
 CONS353
 CONS354
 CONS355
 CONS356

- S(900)=6378,165
- S(901)=1738,
- RETURN
- END

CONS357
 CONS358
 CONS360
 CONS

Page Intentionally Left Blank

Subroutine: CONVPI

Purpose: Subroutine CONVPI transforms the input covariance matrices to the mean equinox of 1950 coordinate system. The input covariance matrices may be input in four coordinate systems:

1. Instantaneous launch pad tangent plane
2. Instantaneous injection tangent plane
3. True equinox of date
4. Mean equinox of 1950.

Calling Sequence:

CALL CONVPI (ITYPE, PIN, POUT)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	ITYPE	1			Logic key which indicates the type of input coordinate frame
I	PIN	21		Km ² , (Km/Sec) ²	Upper half of input covariance matrix in vector form
O	POUT	6, 6	$E(\vec{X}_{50} \vec{X}_{50}^T)$	Km ² , (Km/sec) ²	Output covariance matrix (1950)

Common storages used or required:

T, S, C, IC

Subroutines required:

CROSS, GHA, MULT, NUTAIT, PTRAN,
ROTEQ, TIMED, TRAC

Functions required:

COS SIN
FNORM

Approximate number of storages required:

476 DEC

Calling Sequence Elaboration

The calling sequence consists of CALL CONVPI (INTYPE, PIN, POUT)
where:

INTYPE is a logic key which indicates the type of coordinate system in which the input covariance matrix is expressed. The range of the key is one to five. One through four indicate the four coordinate systems described above. A five in the call sequence indicates that the input matrix is in the same coordinate frame as the input matrix of the preceding call of the subroutine.

PIN is in the input covariance matrix. The matrix must be in the form of a column matrix with dimension (21). The (21) elements represent the upper half of the input covariance matrix.

$$\text{PIN} = \begin{bmatrix} 1 & 2 & 3 & 4 & 5 & 6 \\ & 7 & 8 & 9 & 10 & 11 \\ & & 12 & 13 & 14 & 15 \\ & & & 16 & 17 & 18 \\ & & & & 19 & 20 \\ & & & & & 21 \end{bmatrix}$$

Input Elements

The required order of the input covariance matrix is the following:
For INTYPE = 1 or 2

$$\text{PIN} = \text{E} \begin{bmatrix} \text{AV} \\ \text{NOR} \\ \text{ALT} \\ \dot{\text{AV}} \\ \dot{\text{NOR}} \\ \dot{\text{ALT}} \end{bmatrix} \begin{bmatrix} \text{AV} \\ \text{NOR} \\ \text{ALT} \\ \dot{\text{AV}} \\ \dot{\text{NOR}} \\ \dot{\text{ALT}} \end{bmatrix}^T$$

6×1 1×6

where

$$\hat{\text{AV}} \equiv \frac{\vec{\text{R}} \times \vec{\text{v}}}{|\vec{\text{R}} \times \vec{\text{v}}|} \times \frac{\vec{\text{R}}}{|\vec{\text{R}}|} = \text{coordinate along velocity}$$

$$\hat{\text{NOR}} \equiv \frac{\vec{\text{R}} \times \vec{\text{v}}}{|\vec{\text{R}} \times \vec{\text{v}}|} = \text{coordinate normal to orbit plane}$$

$$\hat{\text{ALT}} = \frac{\vec{\text{R}}}{|\vec{\text{R}}|} = \text{coordinate in direction of altitude}$$

Dots represent corresponding rates.

For INTYPE = 3 or 4

$$\text{PIN} = \text{E} \begin{bmatrix} \text{X} \\ \text{Y} \\ \text{Z} \\ \dot{\text{X}} \\ \dot{\text{Y}} \\ \dot{\text{Z}} \end{bmatrix} \begin{bmatrix} \text{X} \\ \text{Y} \\ \text{Z} \\ \dot{\text{X}} \\ \dot{\text{Y}} \\ \dot{\text{Z}} \end{bmatrix}^T$$

6×1 1×6

POUT is the output covariance matrix in cartesian coordinates mean equator 1950.

CONVPI Transformations

INTYPE = 1 Transformation from launch pad tangent plane to 1950.

Required input constants for operation:

LAUNCH PAD COORDINATES

S(80) Altitude (KM)
 S(81) Longitude (DEG)
 S(82) Latitude (DEG)

LAUNCH AZIMUTH

S(84) Azimuth (DEG)

TIME FROM LAUNCH TO INJECTION

S(83) Time DAYS HOURS. MIN SEC

The transformation from launch pad azimuth coordinates, (AV, NOR, ALT) to mean equinox of 1950 (X_{50} , Y_{50} , Z_{50}) is obtained as follows. Subroutine TRAC is called with launch time and launch pad coordinates to obtain a set of orthogonal unit vectors. The unit vectors, in equator of date, are: \hat{U}_D , unit up vector through the launch pad, \hat{E}_D , unit east vector, and \hat{N}_D , unit north vector. These unit vectors written in matrix form represent the transformation from equator of date coordinates to launch pad coordinates of date

$$\begin{matrix} \vec{X}_{LP} \\ 3 \times 1 \end{matrix} = \begin{bmatrix} \hat{N}_D^T \\ \hat{E}_D^T \\ \hat{U}_D^T \end{bmatrix} \begin{matrix} \vec{X}_{DATE} \\ 3 \times 1 \end{matrix} \quad (1)$$

3x3

The transformation from launch pad coordinates, (N, E, U), to the desired launch azimuth coordinates, (AV, NOR, ALT), is a rotation about the \hat{U} vector by an angle equal to the launch azimuth.

$$\begin{matrix} \vec{X}_{LAZ} \\ 3 \times 1 \end{matrix} = \begin{matrix} \begin{bmatrix} \cos LAZ & \sin LAZ & 0 \\ -\sin LAZ & \cos LAZ & 0 \\ 0 & 0 & 1 \end{bmatrix} \\ 3 \times 3 \end{matrix} \begin{matrix} \vec{X}_{LP} \\ 3 \times 1 \end{matrix} = (ROT) \begin{matrix} \vec{X}_{LP} \\ 3 \times 1 \end{matrix} \quad (2)$$

substituting for \vec{X}_{LP} from equation (1) yields

$$\begin{matrix} \vec{X}_{LAZ} \\ 3 \times 1 \end{matrix} = (ROT) \begin{matrix} \begin{bmatrix} \hat{N}_D^T \\ \hat{E}_D^T \\ \hat{U}_D^T \end{bmatrix} \\ 3 \times 3 \end{matrix} \begin{matrix} \vec{X}_{DATE} \\ 3 \times 1 \end{matrix} \quad (3)$$

Subroutines ROTEQ and NUTAIT are called to obtain transformation matrix (AN) which is the transformation from mean equinox of 1950 to true equator of date.

$$\begin{matrix} \vec{X}_{DATE} \\ 3 \times 1 \end{matrix} = (AN) \begin{matrix} \vec{X}_{1950} \\ 3 \times 1 \end{matrix} \quad (4)$$

Substituting equation (4) into (3) yields

$$\begin{matrix} \vec{X}_{LAZ} \\ 3 \times 1 \end{matrix} = (ROT) \begin{matrix} \begin{bmatrix} \hat{N}_D^T \\ \hat{E}_D^T \\ \hat{U}_D^T \end{bmatrix} \\ 3 \times 3 \end{matrix} (AN) \begin{matrix} \vec{X}_{1950} \\ 3 \times 1 \end{matrix} \quad (5)$$

or

$$\vec{x}_{1950} = \left\{ \begin{array}{c} (\dot{A}N)^T \\ \hat{N}_D^T \\ \hat{E}_D^T \\ \hat{U}_D^T \end{array} \right\}^T (\text{ROT})^T \vec{x}_{\text{LAZ}} = (\text{TRANS}) \vec{x}_{\text{LAZ}} \quad (6)$$

3×1 3×3 3×3 3×3 3×1 3×3 3×1

The corresponding velocity transformation is the following:

$$\dot{\vec{x}}_{1950} = (\text{TRANS}) \dot{\vec{x}}_{\text{LAZ}} \quad (7)$$

under the assumption that $(\dot{A}N) = 0$ which implies $(\text{TRANS}) = 0$.

The 3×3 matrix, (TRANS), is the desired transformation from launch azimuth coordinates to mean equator of 1950. Subroutine PTRAN is called with a 2 in the call list to perform the desired covariance matrix transformation.

$$E \left\{ \begin{array}{c} \vec{x}_{1950} \\ \vec{x}_{1950}^T \end{array} \right\} = \left\{ \begin{array}{cc} (\text{TRANS}) & 0 \\ 3 \times 3 & 3 \times 3 \end{array} \right\} E \left\{ \begin{array}{c} \vec{x}_{\text{LAZ}} \\ \vec{x}_{\text{LAZ}}^T \end{array} \right\} \left\{ \begin{array}{cc} (\text{TRANS}) & 0 \\ 0 & (\text{TRANS}) \end{array} \right\}^T \quad (8)$$

6×6 6×6 6×6 6×6

where \vec{x}_{1950} and \vec{x}_{LAZ} now represent the total state vector (position and velocity).

INTYPE = 2 Transformation from injection tangent plane to 1950.

The transformation from injection tangent plane coordinates, (AV, NOR, ALT), to mean equinox 1950 is obtained as follows. The unit vectors for the injection tangent plane coordinates are obtained in equator of 1950.

$$AV_{50} = \frac{\vec{R} \times \vec{v}}{|\vec{R} \times \vec{v}|} \times \frac{\vec{R}}{|\vec{R}|}$$

$$\text{NOR}_{50} = \frac{\vec{R} \times \vec{v}}{|\vec{R} \times \vec{v}|} \quad (9)$$

$$\text{ALT}_{50} = \frac{\vec{R}}{|\vec{R}|}$$

These vectors written in matrix form represent the transformation from mean equinox of 1950 to injection tangent plane

$$\begin{array}{ccc} \vec{X}_{ITP} & = & \begin{bmatrix} \hat{A}V_{50}^T \\ \hat{N}OR_{50}^T \\ \hat{A}LT_{50}^T \end{bmatrix} \vec{X}_{1950} \\ 3 \times 1 & & 3 \times 3 \quad 3 \times 1 \end{array} \quad (10)$$

or

$$\begin{array}{ccc} \vec{X}_{1950} & = & \begin{bmatrix} \hat{A}V_{50}^T \\ \hat{N}OR_{50}^T \\ \hat{A}LT_{50}^T \end{bmatrix}^T \vec{X}_{ITP} \\ 3 \times 1 & & 3 \times 3 \quad 3 \times 1 \end{array} \quad (11)$$

$$\vec{X}_{ITP} = (\text{TRANS}) \vec{X}_{ITP}$$

3x1 3x3 3x1

The corresponding velocity transformation is

$$\begin{array}{ccc} \dot{\vec{X}}_{1950} & = & (\text{TRANS}) \dot{\vec{X}}_{ITP} \\ 3 \times 1 & & 3 \times 3 \quad 3 \times 1 \end{array} \quad (12)$$

Subroutine PTRAN is called with a 2 in the call list and the operation presented in equation (8) is performed with the 3x3 matrix, (TRANS), defined in equation (11).

INTYPE = 3 Transformation from equator of date to equator of 1950.

The transformation from equator of date to equator of 1950 is obtained as follows. Subroutines ROTEQ and NUTAIT are called to obtain (AN), the required transformation matrix.

$$\begin{array}{c} \vec{X}_{\text{DATE}} \\ 3 \times 1 \end{array} = \begin{array}{c} (\text{AN}) \\ 3 \times 3 \end{array} \begin{array}{c} \vec{X}_{1950} \\ 3 \times 1 \end{array} \quad (13)$$

or

$$\begin{array}{c} \vec{X}_{1950} \\ 3 \times 1 \end{array} = \begin{array}{c} (\text{AN})^T \\ 3 \times 3 \end{array} \begin{array}{c} \vec{X}_{\text{DATE}} \\ 3 \times 1 \end{array} = \begin{array}{c} (\text{TRANS}) \\ 3 \times 3 \end{array} \begin{array}{c} \vec{X}_{\text{DATE}} \\ 3 \times 1 \end{array} \quad (14)$$

The corresponding velocity transformation is

$$\begin{array}{c} \dot{\vec{X}}_{1950} \\ 3 \times 1 \end{array} = \begin{array}{c} (\text{TRANS}) \\ 3 \times 3 \end{array} \begin{array}{c} \dot{\vec{X}}_{\text{DATE}} \\ 3 \times 1 \end{array} \quad (15)$$

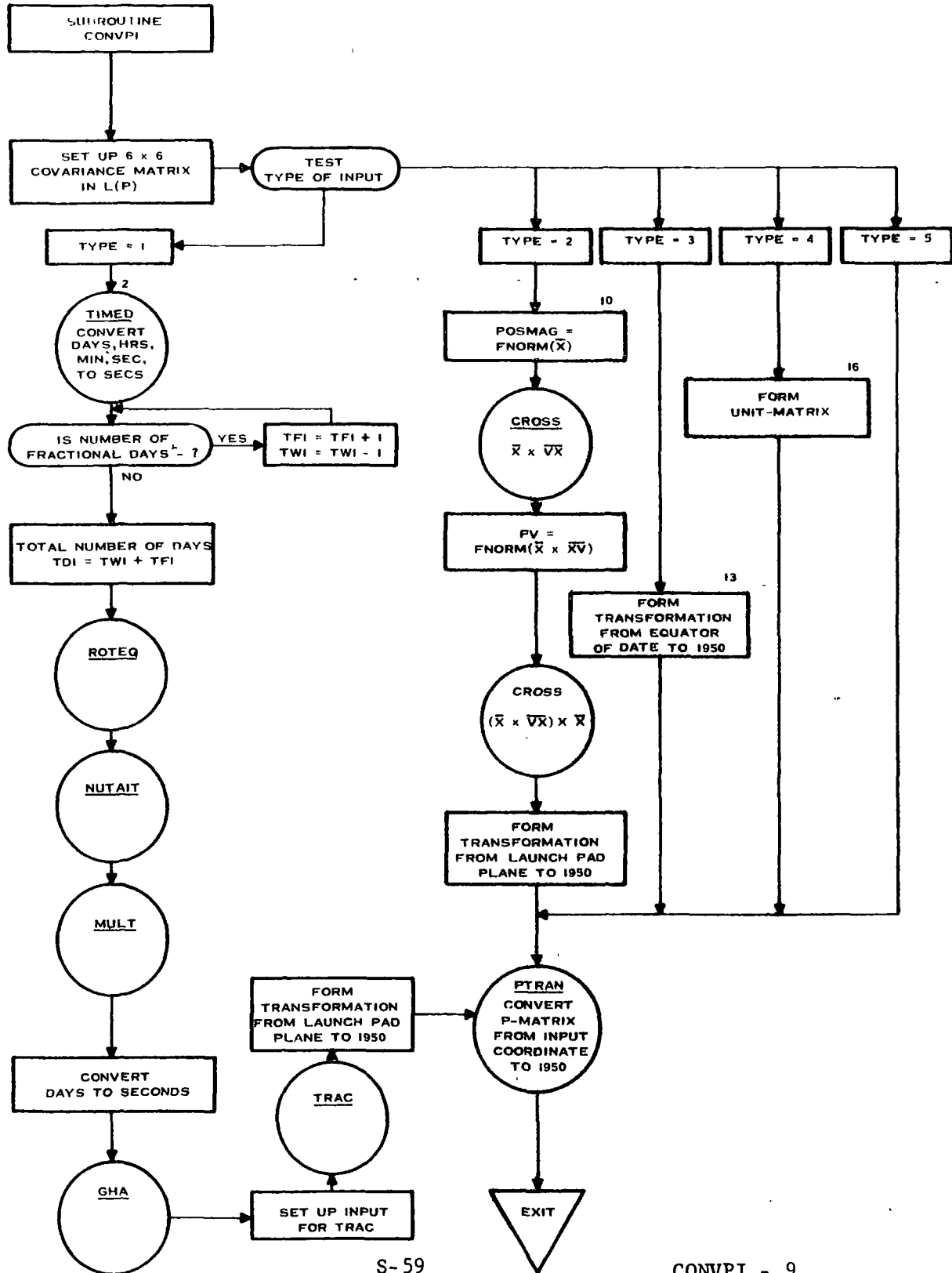
Subroutine PTRAN is called with a 2 in the call list and the operation presented in equation (8) is performed with the 3x3 matrix, (TRANS), defined in equation (14).

INTYPE = 4 Transformation from equator of 1950 to equator of 1950.

The transformation is the unit matrix.

$$\begin{array}{c} \vec{X}_{1950} \\ 3 \times 1 \end{array} = \begin{array}{c} (\text{I}) \\ 3 \times 3 \end{array} \begin{array}{c} \vec{X}_{1950} \\ 3 \times 1 \end{array} = \begin{array}{c} (\text{TRANS}) \\ 3 \times 3 \end{array} \begin{array}{c} \vec{X}_{1950} \\ 3 \times 1 \end{array} \quad (16)$$

INTYPE = 5 The subroutine calls PTRAN to perform the operation presented in equation (8) with the transformation matrix, (TRANS), which is in storage from the previous call of CONVPI.



S-59

CONVPI - 9

CONV
 CONV
 CONV
 CONV0030
 CONV0040
 CONV0050
 CONV0060
 CONV0070
 CONV0080
 CONV0090
 CONV0100
 CONV0110
 CONV0120
 CONV0130
 CONV0140
 CONV0150
 CONV0160
 CONV0170
 CONV0180
 CONV0190
 CONV0200
 CONV0210
 CONV0220
 CONV0230
 CONV0240
 CONV0250
 CONV0260
 CONV0270
 CONV0280
 CONV0290
 CONV0300
 CONV0310
 CONV0320
 CONV0330
 CONV0340
 CONV0350
 CONV0360
 CONV0370
 CONV0380
 CONV0390
 CONV0400
 CONV0410
 CONV0420
 CONV0430
 CONV0440
 CONV0450
 CONV0460
 CONV0470
 CONV0480
 CONV0490
 CONV0500

```

* LABEL
* SYMBOL TABLE
SEC2010 SUBROUTINE CONVPI
SUBROUTINE CONVPI(INPUTP,PI,PS)
COMMON T,S,C,IC
DIMENSION T(1360),S(1000),C(1000),IC(1)
1,PI(21),P(6,6),A(3,3),EM(3,3),AN(3,3),U(3)
2,E(3),EN(3),PDUMP(3,3),DUM(3,3),PS(6,6)
3,X(3),VX(3),ORORB(3),ALV(3),RT(3)
EQUIVALENCE (T,TDUM),(S,SDUM),(C,CDUM),(IC,ICDUM)
1,(S(70),DTS),(S(72),DR),(S(83),TLTI)
2,(C(138),AN),(S(115),X),(S(118),VX),(C(10),TW)
3,(C(11),TF),(C(129),A),(C(120),EM)
1 INPUT DETERMINES TYPE OF INPUT 1.LAUNCH PAD TANGENT PLANE
2.INJECTION TANGENT PLANE 3.EQUATOR DATE 4.EQ1950 5.USE MATRIX
THE REQUIRED ORDER OF INPUT VECTOR OF WHICH PI IS THE COVARIANCE
MATRIX FOR TANGENT PLANE CASES IS FOLLOWING:
1.ALONG VELOCITY,2.NORMAL TO ORBIT,3.ALTITUDE,4,5,6 CORRES.RATES
K=0
DO 1 I=1,6
I=I
DO 1 J=I,6
K=K+1
P(I,J)=PI(K)
P(J,I)=P(I,J)
1 CONTINUE
INPUTP=INPUTP
GO TO (2,10,13,16,8),INPUTP
2 CONTINUE
CALL TIMED(TLTI,TT)
TFI=TF-(TT/86400.)
TWI=TW
3 CONTINUE
IF(TFI)4,5,5
4 CONTINUE
TFI=TFI+1.
TWI=TWI-1.
GO TO 3
5 CONTINUE
TDI=TWI+TFI
CALL ROTEQ(TDI,A)
CALL NUTAIT(TDI,OM,CR,DDC,EM,EPSIL)
CALL MULT(EM,A,AN,N)
FSEC=DTS*TFI
CALL GHA(FSEC,TWI,GH,EM(2,1),OMEGA)
GH=GH*DR
AT=S(80)*DR
ON=S(81)*DR
AL=S(82)
CALL TRAC(ON,AT,AL,GH,U,E,EN,RT,AC,SL,CL,ST,CT)
FAZ=S(84)*DR

```

	SAZ=SINF(FAZ)	CONV05
	CAZ=COSF(FAZ)	CONV05
	DO 6 I=1,3	CONV05
	PDUMP(I,1)=CAZ*EN(I)+SAZ*E(I)	CONV05
	PDUMP(I,2)=SAZ*EN(I)+CAZ*E(I)	CONV05
	PDUMP(I,3)=U(I)	CONV05
6	CONTINUE	CONV05
	DO 7 I=1,3	CONV05
	DO 7 J=1,3	CONV05
	DUM(I,J)=0.	CONV06
	DO 7 K=1,3	CONV06
	DUM(I,J)=DUM(I,J)+AN(K,I)*PDUMP(K,J)	CONV06
7	CONTINUE	CONV06
C	DUM IS TRANSFORMATION FROM LAUNCH PAD PLANE TO 1950	CONV06
8	CONTINUE	CONV06
C	CALL PTRAN(P,DUM,PS,2)	CONV06
C	PTRAN CONVERTS P MATRIX FROM INPUT COORDINATES TO EQ. 1950	CONV06
	GO TO 15	CONV06
10	CONTINUE	CONV06
	POSMAG=FNORM(X)	CONV07
	CALL CROSS(X,VX,ORORB)	CONV07
	PV=FNORM(ORORB)	CONV07
	CALL CROSS(ORORB,X,ALV)	CONV07
	AL=POSMAG*PV	CONV07
	DO 11 I=1,3	CONV07
	PDUMP(I,1)=ALV(I)/AL	CONV07
	PDUMP(I,2)=ORORB(I)/PV	CONV07
	PDUMP(I,3)=X(I)/POSMAG	CONV07
11	CONTINUE	CONV07
	DO 12 I=1,3	CONV08
	DO 12 J=1,3	CONV08
	DUM(I,J)=0.	CONV08
	DO 12 K=1,3	CONV08
	DUM(I,J)=DUM(I,J)+AN(K,I)*PDUMP(K,J)	CONV08
12	CONTINUE	CONV08
C	DUM IS TRANSFORMATION FROM INJECTION TAN. PLANE TO 1950	CONV08
	GO TO 8	CONV08
13	CONTINUE	CONV08
	DO 14 I=1,3	CONV08
	DO 14 J=1,3	CONV09
	DUM(I,J)=AN(J,I)	CONV09
C	DUM IS TRANSFORMATION FROM EQUATOR OF DATE TO 1950	CONV09
14	CONTINUE	CONV09
	GO TO 8	CONV09
16	CONTINUE	CONV09
	DO 17 I=1,3	CONV09
	DO 18 J=1,3	CONV09
	DUM(I,J)=0.	CONV09
	DUM(J,I)=DUM(I,J)	CONV09
18	CONTINUE	CONV10
	DUM(I,I)=1.	CONV10

CONVPI

WDL-TR2184

17 CONTINUE
GO TO 8
15 CONTINUE
RETURN
END

CONV1020
CONV1030
CONV1040
CONV1050
CONV

S-62

CONVPI - 12

Subroutine: CORRTP

Purpose: To perform the filtering or weighting of the observation being made and updating of the state covariance matrix for the inclusion of the observation.

Calling Sequence:

CALL CORRTP (QQ, H, P)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	QQ	1	σ_{MEAS}^2		Measurement variance
I	H	(1,6)	$\frac{\partial MEAS}{\partial STATE}$		Measurement partials
I,O	P	(6,6)	$E(\hat{x} \hat{x}^T)$		State covariance matrix

Common storages used or required: None

Subroutines required: None

Functions required: None

Approximate number of storages required: 124 DEC

Equation Being Solved

The updating of the state covariance matrix for an observation assuming the Schmidt-Kahlman optimum filter is used on the data is the following:

$$P_{NEW} = P_{OLD} - P_o H^T (H P_o H^T + QQ)^{-1} H P_o$$

Page Intentionally Left Blank

Subroutine: CROSS

Purpose: To find the cross product of two 3-dimensional vectors.

Calling Sequence:

CALL CROSS (A, B, C)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	A	3			First input vector
I	B	3			Second input vector
O	C	3			Result = AXB

Common storages used or required: None

Subroutines required: None

Functions required: None

Approximate number of storages required: _____

CROSS

WDL-TR2184

LABEL
SYMBOL TABLE
SUBROUTINE CROSS(A,B,C)
DIMENSION A(3),B(3),C(3)
C(1)=A(2)*B(3)-A(3)*B(2)
C(2)=A(3)*B(1)-A(1)*B(3)
C(3)=A(1)*B(2)-A(2)*B(1)
RETURN
END

CROS
CROS
CROS0000
CROS0010
CROS0020
CROS0030
CROS0040
CROS0050
CROS

Subroutine: (CSH)S

Purpose: This is the standard Fortran II card image input subroutine modified to output the card image, accept logical input and output tape numbers from SETN, and call subroutine HOUR to read the clock if desired.

Calling Sequence:

CALL (CSH)S (BUFF)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
0	BUFF	12			Buffer for contents of card read.

Common storages used or required: None.

Subroutines required: SETN, HOUR, System read routines.

Functions required: None.

Approximate number of storages required: _____

Page Intentionally Left Blank

Subroutine: DE6FN

Identification

RW DE6FN
704 - FORTRAN SAP Language Subroutine
STL

Purpose

This FORTRAN subprogram integrates a set of N simultaneous second-order ordinary differential equations in which first derivatives may or may not appear. It is the FORTRAN version of the standard subroutine RW DE6F.

Restrictions

Same as explained in the write-up for RW DE6F.

Method

A fourth-order Runge-Kutta method (RW DE5F) is used to start the integration and to change the step-size during integration. A Cowell "second-sum" method based on sixth differences is used to continue the integration. While input to this routine is single precision, double precision is used internally to control round-off errors. Truncation error can be controlled by choosing an appropriate step-size, or by using the variable step-size mode of operation. The set-up entry uses the auxiliary subroutine to evaluate the second-order derivatives. The values of the variables and derivatives are consistent at all times. A detailed description of the method used is available in Appendix A.

Usage

- a. Calling LIST for set-up entry (performed prior to initiating the integration).

CALL DE6FN(10,11,T(1),N,V,J,K,A3,A4,A5,A6)

IO is the same as PO of RW DE6F write-up.

- +1 1st derivatives are present in the evaluation of the second derivatives.
- 1 1st derivatives are missing in the evaluation of the second derivatives.

I1 is the same as P1 of RW DE6F write-up.

- +1 Variable step-size mode of operation is used.
- 1 Fixed step-size mode of operation is used.

T is the name of the floating point array which is of dimension $30N+3$ and is reserved by the user. This region should be located in COMMON, since it must be referred to by the main program and by the subroutine V. T(1) need not be set equal to N; however, all other requirements that concern the usage of area T apply. The value of N is not available to the programmer in T(1) and if it is required by the auxiliary subroutine, it should appear in COMMON also.

N is the number of equations (an integer).

V is the name of a FORTRAN subroutine for evaluating the derivatives y_i . This subroutine must be named in the main program by the use of an "F" card.

J equates to B in RW DE6F write-up (an integer).

K equates to R in RW DE6F write-up (an integer).

A3 equates to $\alpha+3$ in RW DE6F write-up (floating point).

A4 equates to $\alpha+4$ in RW DE6F write-up (floating point).

A5 equates to $\alpha+5$ in RW DE6F write-up (floating point).

A6 equates to $\alpha+6$ in RW DE6F write-up (floating point).

For meaning of N, V, J, K, A3, A4, A5, A6 refer to RW DE6F write-up.

Region T contains the following information prior to Set-up Entry.

T(2)	x	value of independent variable
T(3)	h	value of step-size
T(4) thru	y_i thru	values of the independent variables y_i
T(N+3)	y_{11}	
T(N+4) thru	y_i' thru	values of the first derivatives y_i'
T(2N+3)	y_N'	
T(2N+4) thru	y_i'' thru	values of the second derivatives y_i''
T(3N+3)	y_N''	
T(3N+4) - T(30N+4)		temporary storage

More detailed description of this storage may be found in the RW DE6F write-up.

b. RW DE6FN entry to integrate one step.

CALL DE6FPI (ACCUM)

Upon return ACCUM will have the results which formerly appeared in the accumulator.

- c. RW DE6FN entry for a running start.
CALL DE6FP2
- d. RW DE6FN entry for a change of step-size in Cowell/Runge-Kutta System.
CALL DE6FP3(H)
H is the new value of h which was formerly placed in the accumulator prior to entry.
- e. RW DE6FN entry for a change of step-size for a final integration.
CALL DE6FP4
T(3) must be set to the correct value before the CALL.
- f. RW DE6FN entry to initiate a running change in coordinates and to set a list call to a non-zero value.
CALL DE6FNZ (VALUE)
- g. RW DE6FN entry to change from variable mode to fixed mode.
CALL DE6FNG
- h. RW DE6FN entry to change from fixed mode to variable mode.
CALL DE6FPS
- i. RW DE6FN entry to change the value of h_{\min} .
CALL DE6FMN (VALUE)
VALUE is the new h_{\min} in floating point.
- j. RW DE6FN entry to change the value of h_{\max} .
CALL DE6FMA (VALUE)
VALUE is the new h_{\max} value in floating point.
- k. RW DE6FN entry to change the value of y_{\min} .
CALL DE6FCM (VALUE)
VALUE is the new y_{\min} value in floating point.
- l. RW DE6FN entry to change the value of R after a Cowell integration step.
CALL DE6FCH(NR,R)
NR is the integer value of R.
R is the value in floating point.

Identification

RWDE6F Floating Point Cowell (Second Sum), Runge-Kutta
Integration of Second-Order Equations

704 - SAP

STL

Purpose

To solve a set of N simultaneous second-order ordinary differential equations in which first derivatives may or may not appear.

Restrictions

No internal checks are made for overflow or underflow. The user must provide an auxiliary subroutine which evaluates the second-order derivatives. The initial conditions must be set up prior to the first set up entry.

Method

A fourth-order Runge-Kutta method* (RWDE5F) is used to start the integration and to change the step-size during integration. A Cowell "second-sum" method based on sixth differences is used to continue the integration. While input to this routine is single precision, double precision is used internally to control round-off errors. Truncation error can be controlled by choosing an appropriate step-size, or by using the variable step-size mode of operation. The set-up entry uses the auxiliary subroutine to evaluate the second-order derivatives. The values of the variables and derivatives are consistent at all times. A detailed description of the method used is available in Appendix A of this Subroutine.

Usage

Calling sequence to set up a problem:

<u>Loc.</u>	<u>Instruction</u>	<u>Comments</u>
Y	TSX DE6F,4	Set up entry.
$\alpha+1$	PO T,O,V	Option, addresses of storage and auxiliary subroutines.
$\alpha+2$	PI B,O,R	Option and Parameters
$\alpha+3$	DEC 1E-S	S is the number of significant figures desired.
$\alpha+4$	DEC h _{min}	Minimum step-size. Floating point.

* Scarborough, T.B., Numerical Mathematical Analysis, Third Edition, John Hopkins Press, Baltimore, 1955 (pp. 301-302)

<u>Loc.</u>	<u>Instruction</u>	<u>Comments</u>
$\alpha+5$	DEC h_{\max}	Maximum step-size. Floating point.
$\alpha+6$	DEC y_{\min}	Minimum y_i value allowed for testing. Floating point. (See Appendix A for details of y_{\min} .)

Calling sequence to integrate all variables one step:

α	TSX DE6F+1,4	Integration entry.
$\alpha+1$	Return	Sign of AC will be plus if the integration was Runge-Kutta and minus if Cowell.

The address T is the first of $30N+3$ calls arranged as follows:

T	PZE N,0,0	N is the number of equations. Fixed point.
T+1	x	Value of independent variable. Floating point.
T+2	h	Value of step-size. Floating point.
T+23 thru	y_i thru	Values of the dependent variables y_i . Floating point
T+N+2	y_N	
T+N+3 thru	y'_i thru	Values of the first derivatives y'_i . Floating point
T+2N+2	y'_N	
T+3N+3 thru	y''_i thru	Locations where the user's auxiliary subroutine must store the second derivatives y''_i .
T+3N+3	y''_N	
T+3N+3 thru T+30N+2		27N cells of temporary storage.

T+3N+3 thru T+9N+2 (6N) are used by the Runge-Kutta subroutine (RWDE5F). T+4N+3 thru T+5N+2 and T+8N+3 thru T+9N+2 contain the least significant parts (except when a change of coordinates is in progress) of y'_i and y_i respectively, and must be preserved through the entire integration procedure. The final 21N cells of the T storage are used by the Cowell subroutine and must also be preserved. (See Appendix E of this subroutine for a detailed description of these 27N cells.)

The address V is the entry point of the auxiliary subroutine which evaluates the derivatives y''_i and is entered by the calling sequence:

α	TSX V,4	Index registers need not be saved in V.
$\alpha+1$	Return	Return must be made via a TRA 1,4.

The first B ($\leq N$) equations are tested to determine whether it is necessary to halve or possibly to double the step-size or to proceed with a Cowell integration step.

For a given step-size h , the Cowell integration step is h and the Runge-Kutta integration step is h/R .

Options

- PO - PZE 1st derivatives are present in the evaluation of the second derivatives
 - MZE 1st derivatives are missing in the evaluation of the second derivatives.
 Pl = PZE Variable step-size mode of operation is used.
 = MZE Fixed step-size mode of operation is used.

If $1E-S$, h_{\min} , h_{\max} , and y_{\min} are not specified (0 in first calling sequence), the subroutine will set them to $1E-9$, 0, $1E18$, and 1., respectively.

Special Usage (See Appendices A and B for complete details.)

The following special usages are possible:

1. Running change of coordinates.
2. Running start.
3. Change of step-size by user in the Cowell/Runge-Kutta system.
4. Change of step-size for a final integration or at some prescribed value of x .

Space Required (In addition to T and V).

955 calls of program and constants. (Includes DE5F.)

44 calls of COMMON thru COMMON + 43.

Timing

Set-up time. (V=time for 1 entry to the auxiliary subroutine.)

.012 [$12N + 512$] ms. + 1V.

To integrate one step:

1. Runge-Kutta (AC=+ after an integration return.)

A. With 1st derivatives.

.012 [$476N + (8N+18)/R + 240$] ms. + 4V.

B. Without 1st derivatives.

.012 [$383N + (8N + 18)/R + 240$] ms. + 3V.

Timing (Continued)

2. Cowell (AC= - after an integration return.)

A. With 1st derivatives.

.012 [2901N + 92B + 194] ms. + 2V.

+ .012 [2124N + 34] ms. if previous integration
was Runge-Kutta.

B. Without 1st derivatives.

.012 2334N + 92B + 194 ms. + 2V.

+ .012 2124N + 38B + 34 ms. if previous integration was
Runge-Kutta.

3. Change of Coordinates. (In addition to first part of 2A or 2B.)

.012 [2286N] ms. + 8V.

METHOD

This routine is prepared to solve the following system:

$$\left. \begin{aligned} 1) \quad y_i'' &= f_i(x, y_i, \dots, y_N, y_i', \dots, y_N') \\ y_i(x_0) &= y_{i0}, \quad y_i'(x_0) = y'_{i0} \end{aligned} \right\} \quad i = 1, 2, \dots, N$$

In case none of the f_i involve the first derivatives y_i' , time is saved by indicating this in the set-up. The Runge-Kutta routine RWDE5F is used to start the integration and also to change the step-size h . The user must ask for each integration step, and the routine will follow this sequence:

1. R Runge-Kutta steps of size $\frac{h \text{ start}}{R}$ are taken to obtain y_{i1} , y'_{i1} , y''_{i1} . This is continued until we reach y_{i6} , y'_{i6} , y''_{i6} , after a total of $6R$ Runge-Kutta steps. The integer R ($=4$ if unspecified) simply allows Runge-Kutta to operate at a smaller step than the main program.
2. For each of the N equations, that part of the difference table above the diagonal line is constructed in three steps:

		y''_{10}							
			Δ^I_{10}		Δ^{II}_{10}				
		y''_{11}							
			Δ^I_{11}		Δ^{III}_{10}				
		y''_{12}			Δ^{II}_{11}		Δ^{IV}_{10}		
			Δ^I_{12}		Δ^{III}_{11}		Δ^V_{10}		
<u>"F₁₄</u>	<u>y''₁₃</u>			<u>Δ^{II}_{12}</u>		<u>Δ^{IV}_{11}</u>		<u>Δ^{VI}_{10}</u>	
	<u>'F₁₄</u>		<u>Δ^I_{13}</u>		<u>Δ^{III}_{12}</u>		<u>Δ^V_{11}</u>		
"F ₁₅	y''_{14}			Δ^{II}_{13}		Δ^{IV}_{12}		Δ^{VI}_{11}	
	'F ₁₅		Δ^I_{14}		Δ^{III}_{13}		Δ^V_{12}		
"F ₁₆	y''_{15}			Δ^{II}_{14}		Δ^{IV}_{13}			
	'F ₁₆		Δ^I_{15}		Δ^{III}_{14}				
"F ₁₇	y''_{16}			Δ^{II}_{15}					
	'F ₁₇		Δ^I_{16}						
"F ₁₈	y''_{17}								
	'F ₁₈								
"F ₁₉									

First the known y''_{10} through y''_{16} are differenced to give the right half of the table. Next are calculated in extra precision:

$$2) \quad 'F_{14} = \frac{y_{13}}{h^2} - C_0 y''_{13} - C_2 \Delta^{II}_{12} - C_4 \Delta^{IV}_{11} - C_6 \Delta^{VI}_{10}$$

$$3) \quad 'F_{i4} = \frac{y'_{i3}}{h} - D_0 y''_{i3} - D_1 \Delta_{i3}^I - D_2 \Delta_{i2}^{II} - D_3 \Delta_{i2}^{III} \\ - D_4 \Delta_{i1}^{IV} - D_5 \Delta_{i1}^V - D_6 \Delta_{i0}^{VI}$$

The table is then completed down to the diagonal line, by requiring the difference between any entry and the entry above to equal the entry to the right. The constants used in equations (2) - (7) are given in the description of the Livermore Cowell routine.

3. Before going to a Cowell step, the step-size h is tested. The tests are omitted, however, if the user so indicates in the initial calling sequence, in which case h is fixed. Only the first B equations are used to test, where $1 \leq B \leq N$ and $B = N$ if unspecified. We determine--

$$v = \frac{\max_{1 \leq i \leq B}}{\max(y_{i6}, y_{\min})} \left| \frac{\Delta_{i1}^V}{\max(y_{i6}, y_{\min})} \right|. \quad \text{If } v \geq \frac{10^{3-S}}{h^2}, \text{ then the}$$

ratio of 5th difference to function is too large -- if S decimal places are to be retained at that step. Therefore, h is reduced to $h/2$ and Runge-Kutta re-entered for another sequence of $6R$ steps. These begin with the latest calculated values (y_{i6}, y'_{i6}) and no ground is retraced. The constant y_{\min} ($=1$ if unspecified) prevents division by y near a zero; for example, in sine calculation $y_{\min} = .1$ avoids difficulty near 180° . The integer S , taken as 9 if unspecified, allows a large h if chosen smaller, say $S = 7$.

$$\text{If } \frac{10^{-1-S}}{h^2} < v < \frac{10^{3-S}}{h^2}, \text{ we proceed to a Cowell step.}$$

If $v \leq \frac{10^{-1-S}}{h^2}$, we may be able to double h . We test further

to see that

$$W = \frac{\max_{1 \leq i \leq B}}{\left| \frac{\Delta_{i0}^{VI}}{\max(y_{i6}, y_{\min})} \right|} \leq \frac{10^{-1-S}}{h^2},$$

and if so, we re-enter Runge-Kutta after replacing h by $2h$, since the step-size h has led to needlessly small difference to function ratios. Of course, h is not halved or doubled if this would violate h_{\min} or h_{\max} , which are 0 and 10^{18} if unspecified.

4. The Cowell integration begins with predictions:

$$4) \quad y_{i7} = h^{2s} ({}^I F_{i8} + N_0 y''_{i6} + N_1 \Delta_{i5}^I + \dots + N_6 \Delta_{i0}^{VI})$$

$$5) \quad y'_{i7} = h ({}^I F_{i7} + \dot{N}_0 y''_{i6} + \dot{N}_1 \Delta_{i5}^I + \dots + \dot{N}_6 \Delta_{i0}^{VI})$$

These use the row of the difference table above the diagonal line; only this row is needed for a Cowell step and is kept up to date as the integration proceeds. (We mention that the above prediction for y'_{i7} is omitted in the missing first derivative option.) Now from y_{i7} and y'_{i7} , we obtain y''_{i7} and then complete the row of differences out to Δ_{i1}^{VI} under the diagonal line in the table. With this row, we calculate final corrected values --

$$6) \quad y_{i7} = h^{2s} ({}^I F_{i8} + B_0 y''_{i7} + \dots + B_6 \Delta_{i1}^{VI})$$

$$7) \quad y'_{i7} = h ({}^I F_{i7} + \dot{B}_0 y''_{i7} + \dots + \dot{B}_6 \Delta_{i1}^{VI})$$

From these we get corrected values for y''_{i7} , and recalculate the entire row under the diagonal line. This completes the integration step. Using the new row of differences, the next step begins by testing the step-size (i.e., at 3.).

Further Properties of the Program

In some problems, information about the first derivative (velocity) may be less reliable than information about the function (position). The user may then choose a "running change of coordinates" or a "running start;" these depend on the fact that with 8 consecutive values of the y_i (and the y_i' in case first derivatives are present in the f_i) the Cowell part of the program can be self-starting. The mathematics is simple: step No. 1 is omitted, and No. 2 modified to calculate $'F_{i4}$ and $'F_{i5}$ from Eq. (2) (instead of $'F_{i4}$ and $'F_{i4}$). The difference table may again be completed, and Cowell integration begins. The user, having tested the AC to establish that the previous step was a Cowell step, begins a running change of coordinates by setting cell DE6F + 500 to non-zero. He then sets up a counter and begins immediately to store 8 consecutive values of the y_i starting at T+3+11N (and y_i' starting at T+3+3N, if they appear in the f_i). After changing the coordinates the 8th time, the user may change the second derivative evaluation routines; if x and h are to be in new units this should also be done. When another step is asked for, the routine will form a difference table in the new coordinates and proceed to a Cowell step.

The mechanics of a running start are similar; after going through the set-up routine, the user loads his values of y_{i0} through y_{i7} (and the y_i' if needed in the f_i) into the same locations as above and makes the required transfer.

There may also be occasions on which the user will wish to modify h himself; e.g., if he wishes to produce the numerical solution at some prescribed value of x, or if he wishes to approach a running change of coordinates at a step-size smaller than that being used by the routine. The technique of modifying h is described in Appendix B.

APPENDIX B

USAGE AND CODING INFORMATION

There are essentially two entries to the subroutine. The first entry must be made once at the beginning to set up the addresses, options, parameters, etc., of the routine for integration of N simultaneous second-order, ordinary differential equations, in which first derivatives may or may not appear. The first entry utilizes the auxiliary subroutine to evaluate the second-order derivatives at the initial conditions. Thus, the initial conditions must be set up prior to the first entry. The second entry may be used any number of times after the first to integrate all y_i from x to $x+h$ by a Cowell step; or x to $x+h/R$ by a Runge-Kutta step.

The first entry has the following calling sequence:

<u>Loc.</u>	<u>Instruction</u>	<u>Comments</u>
α	TSX DE6F,4	Set-up entry.
$\alpha+1$	PO T,O,V	Option, addresses of storage and auxiliary subroutine.
$\alpha+2$	Pl B,O,R	Option and parameters.
$\alpha+3$	DEC lE-S	S is the number of significant figures desired.
$\alpha+4$	DEC h_{\min}	Minimum step-size. Floating point.
$\alpha+5$	DEC h_{\max}	Maximum step-size. Floating point.
$\alpha+6$	DEC y_{\min}	Minimum y_i value allowed for testing. Floating point.
$\alpha+7$	Return	

($\alpha+1$): T is the address of the first word of a block of $30N+3$ cells of temporary storage arranged as follows:

<u>Loc.</u>	<u>Contents</u>	<u>Comments</u>
T	PZE N,0,0	N is the number of equations. Fixed point.
T+1	x	Value of independent variable. Floating point.
T+2	h	Value of step-size. Floating point.
T+3 thru T+N+2	y_i thru y_N }	Values of the dependent variables y_i . Floating point.
T+N+3 thru T+2N+2	y'_i thru y'_N }	Values of the first derivatives y'_i . Floating point.
T+2N+3 thru T+3N+2	y''_i thru y''_N }	Locations where the user's auxiliary subroutine must store the second derivatives y''_i . Floating point.
T+3N+3 thru T+30N+2		27N cells of temporary storage.

The next 27N storages of T are temporary storages. The Runge-Kutta subroutine uses the first 6N cells (T+3N+2 thru T+9N+3) and the Cowell routine uses the final 21N cells (T+9N+3 thru T+30N+2). However, if a change of coordinates (see Special Usage) is made, the Cowell routine will also use the first 6N cells. The attached T Storage Chart shows the set-up of the entire T region. The N cells starting at T+5N+3 and the N cells starting at T+6N+3 are used by the Runge-Kutta subroutine to compute $\Delta'y_{iN}$ and Δy_{iN} . However, $\Delta'y_{iN}$ and Δy_{iN} are destroyed before final exit, and these cells contain intermediate values of no significance to the user. The left side of the chart shows the storage for the normal case where 6R Runge-Kutta steps are taken (using the first 9N cells of T for each integration) before an attempt is made to proceed to a Cowell step. At the beginning of each set of R steps, the Cowell subroutine saves the values of the second derivatives (7 sets starting at T+11N+3). In addition, the values of y_{i3} and y'_{i3} are saved, starting at T+9N+3 and T+10N+3 respectively, for use in the central difference equations where $'F_{i4}$ and $'F_{i4}$ are calculated. Care must be exercised in using certain values in the temporary region.

For instance, after a Runge-Kutta integration step, the most significant values of y_i and y_i' , starting at $T+7N+3$ and $T+3N+3$ respectively, will be the values of the previous integration; while the least significant values of y_i and y_i' , starting at $T+8N+3$ and $T+4N+3$, respectively, will be the values of the present integration. The Cowell routine also saves the least significant values of y_i and y_i' (unless a change of coordinates is in progress) in these same storages at the end of each integration. The $11N$ storages starting at $T+19N+3$ contain the right half of the N difference tables, an example of which is shown in Appendix A. The right side of the chart shows other values which are stored in the T region during a change of coordinates and will be explained later under Special Usage. Even though only one symbol is given (y_{10}' , etc.), it should be understood that N values are stored as in the left side of the chart. Thus, y_{10}' signifies $y_{10}', y_{20}', y_{30}', \dots, y_{NO}'$.

The address V is the entry point of an auxiliary subroutine which the user must provide to evaluate the second derivatives y_i'' . This subroutine must store y_i'' in $T+2N+3$ through $T+3N+2$ as shown above. The subroutine is entered by the calling sequence:

<u>Loc.</u>	<u>Instruction</u>	<u>Comments</u>
α	TSX V,4	Index registers need not be saved.
$\alpha+1$	Return	Return via a TRA 1,4.

The derivatives y_i'' are evaluated during the set-up and at the end of each integration step. Thus, the values of the variables and the derivatives are consistent at all times. Extra precision is recommended for the evaluation of the second derivatives y_i'' .

PO should be set to PZE if the first derivatives are present in the evaluation of the second derivatives. If first derivatives are not present, PO should be set to MZE.

($\alpha+2$): P1 should be set to PZE if a variable step-size is wanted. For a fixed step-size; P1 should be set to MZE. The former allows doubling and halving while the latter restricts the routine to a fixed r . The user may change the mode of operation externally at any time by setting cell DE6F+501 to plus for a variable step-size and minus for a fixed step-size.

Only the first B ($1 \leq B \leq N$) equations are tested to determine doubling or halving of h . Thus, the user should arrange the N equations in descending order of importance, and specify B accordingly. If $B = 0$ in the calling sequence, it will be set to N .

R is the ratio of the Cowell step-size to the Runge-Kutta step-size. Thus, smaller integration steps can be taken in the Runge-Kutta subroutine by setting R greater than 1. If $R = 0$ in the calling sequence, it will be set to 4. R is saved in the decrement of cell DE6F+516 and in floating point in cell DE6F+517. After any Cowell integration step (AC= -), the user should change R by changing both of these cells.

($\alpha+3$): $1E-S$ is a floating point number where S is the number of significant figures of accuracy desired at each step. The user should experiment with S to fit his own particular problem. The 1 of $1E-S$ may also be varied from 1 to 9 ($1E-S$ thru $9E-S$) for a final degree of control over the accuracy testing. If $1E-S=0$ in the calling sequence, it will be set to $1E-9$.

($\alpha+4$): h_{\min} is a floating point number giving a lower bound for h . h_{\min} is saved in cell DE6F+509 and can be changed at any time.

($\alpha+5$): h_{\max} is a floating point number giving an upper bound for h . If $h_{\max}=0$ in the calling sequence, the upper bound will be set to $1E18$. h_{\max} is saved in cell DE6F+510 and can be changed at any time.

($\alpha+6$): y_{\min} is a positive floating point number which is used in testing the step-size. If $y_{\min}=0$ in the calling sequence, it will be set to 1. y_{\min} is saved in cell DE6F+511 and can be changed at any time.

If the fixed step-size mode of operation is selected ($P1=MZE$), then B, $1E-S$, h_{\min} , h_{\max} , and y_{\min} are all ignored by the subroutine. (If $P1=MZE$, set $B = 1$ for maximum efficiency.)

The integration entry has the following calling sequence:

<u>Loc.</u>	<u>Instruction</u>	<u>Comments</u>
α	TSX DE6F+1,4	Integrates all variables one step.
$\alpha+1$	Return	

Upon return from the integration entry, the accumulator will be plus if the integration was a Runge-Kutta step and minus if the integration was a Cowell step. Ordinarily, x will have been advanced to $x+h/R$ for a Runge-Kutta step and $x+h$ for a Cowell step. However, in the variable h mode, it is possible that the value of h in $T+2$ prior to the integration entry has been changed to $h/2$ or $2h$. In this case, the integration step will be a Runge-Kutta step, and the value of x will be either $x+h/2R$ or $x+2h/R$. All values of y_i , y_i' , and y_i'' will be consistent with the new value of x . The user must never change the value of the step-size h except as described under Special Usage.

Special Usage (See Appendix A. Further Properties of the Program.)

1. Running Change of Coordinates. (Normal Entries.)

After any Cowell integration step (AC= -), the user may initialize the beginning of a change of coordinates by setting cell DE6F+500 to non-zero. Starting with the present values, he begins to save eight consecutive sets of y_i starting at $T+11N+3$ (and y_i' starting at $T+3N+3$ if they appear in the y_i''). He continues to use the integration entry above. The routine will

detect the non-zero value stored in cell DE6F+500 and will begin a count-down in cell DE6F+502 from 8 (-1) 0. The next seven integrations will be Cowell steps and all testing will be discontinued during this period. After the eighth set of y_i (y_{i7}), and y_i' (y_{i7}') if necessary, have been stored (DE6F+502 will have a fixed point 1 in the address), the user may change the second derivative evaluation routine V and the units of x and h. The units of the eight sets of y_i and y_i' may be changed while storing each set, or after all eight sets have been stored. When another integration step is asked for, the routine will perform the change of coordinates and proceed to a Cowell integration step. Cell DE6F+500 will be restored to zero, and an 8 will be restored to the address of cell DE6F+502. Thus, the routine will be ready for another change of coordinates and will operate under standard conditions.

2. Running Start. (Special Entry.)

A running start is similar to a running change of coordinates except that the user must supply all eight sets of y_i (and y_i' if necessary) at one time. The following sequence of operations must be followed:

- A. Set up the initial conditions in the T storage. Only N, x, and h are needed, although the eight sets of y_i (but not y_i') can also be stored at this time. x must correspond to y_{i7} and h must be the interval at which the y_i have been obtained. Thus, $x = x_0 + 7h$ where x_0 corresponds to y_0 (and y_0').
- B. Use the first entry calling sequence to set up all parameters and options. The V subroutine will be used but will have no effect on the problem. Also, cells T+4N+3 thru T+5N+2 and T+8N+3 thru T+9N+2 will be set to zero. Thus, the eight sets of y_i' must be stored after the setup entry.
- c. Store eight consecutive sets (equal intervals) of y_i starting at cell T+11N+3 (and eight consecutive sets of y_i' starting at cell T+3N+3, if needed).

D. Execute the following calling sequence one time:

<u>Loc.</u>	<u>Instruction</u>	<u>Comments</u>
α	TSX DE6F+16,4	Enter only once.
$\alpha+1$	Return	Integrates 1 step.

E. Continue with the regular integration entry (TSX DE6F+1,4) to integrate further. Step D integrates all variables one Cowell step, and $x(x_0 + 7h)$ is advanced to $x + h(x_0 + 8h)$. From this point, the routine will operate under normal conditions.

3. Change of Step-Size in the Cowell/Runge-Kutta System. (Special Entry.)

During the integration procedure, the user may wish to output for a specific value of x without interrupting the Cowell/Runge-Kutta integration procedure. Or, he may wish to change the value of the step size h prior to a running change of coordinates. He can do this after any integration entry with the following procedure:

<u>Loc.</u>	<u>Instruction</u>	<u>Comments</u>
α	TSX DE6F+22,4	Changes h and starts new series of 6R Runge-Kutta steps.
$\alpha+1$	Return	

Thus, the integration step will be h/R . Continue with the regular integration entry (TSX DE6F+1,4) to integrate further.

If the above procedure is being used to reduce the step-size prior to a change of coordinates, the user must prevent the routine from doubling again until after the change of coordinates. Doubling can be prevented either by storing zero in cell DE6F+510 (h_{\max}), or by setting cell DE6F+501 (fixed step size) negative prior to the above entry. After the change of coordinates, the user may restore the above cells.

4. Change of Step Size for a Final Integration. (Special Entry.)

This is simply a direct transfer to the Runge-Kutta integration subroutine and should be used to end exactly at a specific value of x .

After changing the value of h in T+2,

<u>Loc.</u>	<u>Instruction</u>	<u>Comment</u>
α	TSX DE6F+588,4	Integrates one step with the Runge-Kutta subroutine.
$\alpha+1$	Return	

The integration step will be the value of h in T+2. This procedure could be used in the middle of the integration procedure if 3. above (TSX DE6F+22,4) is used immediately afterwards to restart in the Cowell/Runge-Kutta system.

In addition to the user's auxiliary subroutine and the 30N+3 cells for the T storage, the storage requirements are 955 words for RWDE6F plus 44 words of COMMON.

The value of the independent variable x is accumulated in double precision when incremented by h . The least significant part of x is saved in cell DE6F+718.

APPENDIX B - T STORAGE CHART

	N	x	h										
T+3	y_1	y_2	.	.	y_N	Initial conditions which user must supply.							
T+N+3	y_1'	y_2'	.	.	y_N'								
T+2N+3	y_1''	y_2''	.	.	y_N''	2nd derivatives stored by V subroutine.							
T+3N+3	y_1'	y_2'	.	.	y_N'	Most significant	y_{10}'	y_{10}''	Coordinate Change				
T+4N+3	y_1'	y_2'	.	.	y_N'	Least significant	y_{11}'	y_{11}''	8 sets of consecutive				
T+5N+3	$\Delta y_1'$	$\Delta y_2'$.	.	$\Delta y_N'$	Destroyed by R.K.	y_{12}'	y_{12}''	y_1' saved by user if				
T+6N+3	$\Delta y_1'$	$\Delta y_2'$.	.	$\Delta y_N'$	Destroyed by R.K.	y_{k3}'	y_{k3}''	$y'' = f(x, y, y')$. Cowell				
T+7N+3	y_1	y_2	.	.	y_N	Most significant	y_{14}'	y_{14}''	stores y_1'' over y_1' .				
T+8N+3	y_1	y_2	.	.	y_N	Least significant	y_{15}'	y_{15}''					
T+9N+3	y_{13}	y_{23}	.	.	y_{N3}	Saved for central	y_{16}'	y_{16}''					
T+10N+3	y_{13}'	y_{23}'	.	.	y_{N3}'	difference equations	y_{17}'	y_{17}''					
T+11N+3	y_{10}''	y_{20}''	.	.	y_{N0}''	Normal Case.	y_{10}		Coordinate Change				
T+12N+3	y_{11}''	y_{21}''	.	.	y_{N1}''	Saved from 6R R-K	y_{11}		8 sets of consecutive				
T+13N+3	y_{12}''	y_{22}''	.	.	y_{N2}''	steps. Used to form	y_{12}		y_1 saved by user.				
T+14N+3	y_{13}''	y_{23}''	.	.	y_{N3}''	difference tables in	y_{13}		Cowell uses (with V sub)				
T+15N+3	y_{14}''	y_{24}''	.	.	y_{N4}''	an attempt to proceed	y_{14}		to form y_1'' above.				
T+16N+3	y_{15}''	y_{25}''	.	.	y_{N5}''	to a Cowell step.	y_{15}						
T+17N+3	y_{16}''	y_{26}''	.	.	y_{N6}''		y_{16}						
T+18N+3	Used only if coordinates changed.							y_{17}					
T+19N+3	Δ_{10}^{VI}	Δ_{11}^V	Δ_{12}^{IV}	Δ_{13}^{III}	Δ_{14}^{II}	Δ_{15}^I	y_{16}''	"F ₁₈	"F ₁₈	'F ₁₇	'F ₁₇	11N storages.	
T+19N+14	Δ_{20}^{VI}	Δ_{21}^V	Δ_{22}^{IV}	Δ_{23}^{III}	Δ_{24}^{II}	Δ_{25}^I	y_{26}''	"F ₂₈	"F ₂₈	'F ₂₇	'F ₂₇	N sets of	
T+19N+25	Δ_{30}^{VI}	Δ_{32}^V	Δ_{32}^{IV}	Δ_{33}^{III}	Δ_{34}^{II}	Δ_{35}^I	y_{36}''	"F ₃₈	"F ₃₈	'F ₃₇	'F ₃₇	differences	
.	↑	↑	↑	↑	saved for	
.	Most	Lat.	Most	Lat.	next Cowell	
.	Sig.	Sig.	Sig.	Sig.	step.	
T+30N-8	Δ_{N0}^{VI}	Δ_{N1}^V	Δ_{N2}^{IV}	Δ_{N3}^{III}	Δ_{N4}^{II}	Δ_{N5}^I	y_{N6}''	"F _{N8}	"F _{N8}	'F _{N7}	'F _{N7}	(See Appendix A)	

```

* FAP
  TTL DE6FN COWELL INTEGRATION ROUTINE CORRECTED 6/63
  LBL DE6FN
  COUNT 1100
  ENTRY DE6FN
  ENTRY DE6FP1
  ENTRY DE6FP2
  ENTRY DE6FP3
  ENTRY DE6FNZ
  ENTRY DE6FPS
  ENTRY DE6FNG
  ENTRY DE6FCH
  ENTRY DE6FCM
  ENTRY DE6FP4
  ENTRY DE6FMN
  ENTRY DE6FMA
  PZE 0
  PZE 0
  PZE 0
DE6FN  SXD DE6FN-1,1      SAVE 1R
        SXD DE6FN-2,2
        SXD DE6FN-3,4
        CLA 5,4
        STA DUX1
        CLA 6,4
        STA BCOM          LOC B
        CLA 7,4
        STA RCOM          LOC R
BCOM   CLA *
        STA CALL+1
        ARS 18
        STO CELM1
RCOM   CLA *
        ADD CELM1
        STO CALL+2      2ND WORD
        CLA 8,4
        STA **1
        CLA *
        STO CALL+3      3RD WORD
        CLA 9,4
        STA **1
        CLA *
        STO CALL+4      4TH WORD
        CLA 10,4
        STA **1
        CLA *
        STO CALL+5      5TH WORD
        CLA 11,4
        STA **1
        CLA *
        STO CALL+6      6TH WORD
  
```

```

DE6FN
DE6FN0000
DE6FN0010
DE6FN0020
DE6FN0030
DE6FN0040
DE6FN0050
DE6FN0060
DE6FN0070
DE6FN0080
DE6FN0090
DE6FN0100
DE6FN0110
DE6FN0120
DE6FN0130
DE6FN0140
DE6FN0150
DE6FN0160
DE6FN0170
DE6FN0180
DE6FN0190
DE6FN0200
DE6FN0210
DE6FN0220
DE6FN0230
DE6FN0240
DE6FN0250
DE6FN0260
DE6FN0270
DE6FN0280
DE6FN0290
DE6FN0300
DE6FN0310
DE6FN0320
DE6FN0330
DE6FN0340
DE6FN0350
DE6FN0360
DE6FN0370
DE6FN0380
DE6FN0390
DE6FN0400
DE6FN0410
DE6FN0420
DE6FN0430
DE6FN0440
DE6FN0450
DE6FN0460
DE6FN0470
DE6FN0480
DE6FN0490
  
```

CLA 2,4
 STA ++1
 CLA *
 TPL ++3
 CLS CALL+2
 STO CALL+2
 CLA 4,4
 STA NTOTA
 CLA 3,4
 STA REVER+3
 STA REVER+5
 STA NTOT
 STA COMN
 STA COMCEL
 STA SVTD
 NTOTA CLA *
 ARS 18
 NTOT STO *
 COMCEL LDQ *
 MPY TRTY
 STQ CELM1
 CLA SVTD
 SUB CELM1
 SUB TWO
 ADM CALL+1
 STA START
 STO CALL+1
 CLA 1,4
 STA ++1
 CLA *
 TPL ++3
 CLS CALL+1
 STO CALL+1
 COMN LDQ *
 MPY FIFTN
 STQ CELM1
 CLA CELM1
 ADD ONE
 STO HN
 CLA START
 ADD HN
 STA REVER+2
 STA REVER+4
 TSX REVER,4
 CALL TSX DE6F,4
 PZE ,,DUX
 PZE *
 PZE *
 PZE *
 PZE *
 PZE *

SET SIGN
 2ND WORD
 LOC ENDT
 FIND TOP T
 SAP T
 SET SIGN PO
 COMPUTE
 MID POINT
 ENTER

DE6FN050
 DE6FN051
 DE6FN052
 DE6FN053
 DE6FN054
 DE6FN055
 DE6FN056
 DE6FN057
 DE6FN058
 DE6FN059
 DE6FN060
 DE6FN061
 DE6FN062
 DE6FN063
 DE6FN064
 DE6FN065
 DE6FN066
 DE6FN067
 DE6FN068
 DE6FN069
 DE6FN070
 DE6FN071
 DE6FN072
 DE6FN073
 DE6FN074
 DE6FN075
 DE6FN076
 DE6FN077
 DE6FN078
 DE6FN079
 DE6FN080
 DE6FN081
 DE6FN082
 DE6FN083
 DE6FN084
 DE6FN085
 DE6FN086
 DE6FN087
 DE6FN088
 DE6FN089
 DE6FN090
 DE6FN091
 DE6FN092
 DE6FN093
 DE6FN094
 DE6FN095
 DE6FN096
 DE6FN097
 DE6FN098
 DE6FN099
 DE6FN100

```

REVER IN
    TSX REVER,4
    LXD DE6FN-1,1
    LXD DE6FN-2,2
    LXD DE6FN-3,4
    TRA 12,4
    LXA HN,1
    LXD ZERO,2
    LDQ *,1
    CLA *,2
    STO *,1
    STQ *,2
    TXI **1,2,1
    TIX IN,1,1
    TRA 1,4
DE6FP1
    SXD DE6FN-1,1
    SXD DE6FN-2,2
    SXD DE6FN-3,4
    TSX REVER,4
    TSX DE6F+1,4
    STO CELM1
    TSX REVER,4
    LXD DE6FN-1,1
    LXD DE6FN-2,2
    LXD DE6FN-3,4
    CLA 1,4
    STA **2
    CLA CELM1
    STO *
    TRA 2,4
DE6FP2
    SXD DE6FN-1,1
    SXD DE6FN-2,2
    SXD DE6FN-3,4
    TSX REVER,4
    TSX DE6F+16,4
    TSX REVER,4
    LXD DE6FN-1,1
    LXD DE6FN-2,2
    LXD DE6FN-3,4
    TRA 1,4
DE6FP3
    SXD DE6FN-1,1
    SXD DE6FN-2,2
    SXD DE6FN-3,4
    TSX REVER,4
    LXD DE6FN-3,4
    CLA 1,4
    STA **1
    CLA *
    TSX DE6F+22,4
    TSX REVER,4
    LXD DE6FN-1,1
    LXD DE6FN-2,2

```

REVERSE T BLOCK

```

DE6FN1010
DE6FN1020
DE6FN1030
DE6FN1040
DE6FN1050
DE6FN1060
DE6FN1070
DE6FN1080
DE6FN1090
DE6FN1100
DE6FN1110
DE6FN1120
DE6FN1130
DE6FN1140
DE6FN1150
DE6FN1160
DE6FN1170
DE6FN1180
DE6FN1190
DE6FN1200
DE6FN1210
DE6FN1220
DE6FN1230
DE6FN1240
DE6FN1250
DE6FN1260
DE6FN1270
DE6FN1280
DE6FN1290
DE6FN1300
DE6FN1310
DE6FN1320
DE6FN1330
DE6FN1340
DE6FN1350
DE6FN1360
DE6FN1370
DE6FN1380
DE6FN1390
DE6FN1400
DE6FN1410
DE6FN1420
DE6FN1430
DE6FN1440
DE6FN1450
DE6FN1460
DE6FN1470
DE6FN1480
DE6FN1490
DE6FN1500
DE6FN1510

```



```

LINKA  CLA *
        STO DE6F+516
LINKB  CLA *
        STO DE6F+517
        TRA 3,4
ZERO   PZE 0
ONE    DEC 1
TWO    DEC 2
FIFTN  DEC 15
HN     PZE 0
SVTD   PZE 0
COMMON BSS 44
DE6F   TRA DE6F+0799      COWELL METHOD INTEGRATION SUB (TR SETUP)
        SXD DE6F+0504,1    2ND ENTRY, BEGIN
        SXD DE6F+0505,2    INTEGRATION
        SXD DE6F+0506,4
        CLA DE6F+0500      TEST SWITCH FOR COORD. CHANGE
        TZE DE6F+0011     0=NORMAL CASE
        CLA DE6F+0502      8(-1)0
        SUB DE6F+0531      1
        STO DE6F+0502
        TNZ DE6F+0011     CONTINUE IF NOT ZERO
        TRA DE6F+0091     TR FOR COORD. CHANGE
        CLA DE6F+0503      TEST R.K. OR COWELL
        TMI DE6F+0185     -=COWELL
        CLA DE6F+0709      TEST 1ST TIME FOR R.K. +=
        TMI DE6F+0043      =2N=3RD, ..., RTH R.K. INTEGR.
        TRA DE6F+0030     TR TO BEGIN RUNGE KUTTA SERIES (R)
        SXD DE6F+0504,1    PROGRAMMER MAY ENTER HERE FOR
        SXD DE6F+0505,2    SPECIAL COORD. CHANGE, 8 SETS
        SXD DE6F+0506,4    OF Y,S MUST BE IN T+11N+3
        STZ DE6F+0502      AND T MUST BE AT 8TH Y.
        SXD DE6F+0500,4    8 SETS OF Y PRIME MUST BE
        TRA DE6F+0091     AT T+3N+3 IF F(X,Y,Y PRIME) USED.
        SXD DE6F+0504,1    PROGRAMMER MAY ENTER HERE WITH H IN AC
        SXD DE6F+0505,2    AND START NEW RUNGE KUTTA SERIES
        SXD DE6F+0506,4    H/R WILL BE INTEGRATION STEP.
        STO COMMON+000
        CLA DE6F+0500      NEW H
        TNZ DE6F+0006     CANNOT CHANGE H IF COORD.
        LDQ COMMON+000    CHANGE IS IN PROGRESS
        TSX DE6F+0077,2   NEW H
        CLA DE6F+0519     CHANGE VMIN, VMAX, WMAX FOR H2
        FDP DE6F+0517     H/R=R.K. H FOR EACH STEP
        STQ 0              R=TOTAL R.K. STEPS
        LDQ DE6F+0519     (T+2)
        FMP DE6F+0519     DELTA (T) = H
        STO DE6F+0520     DELTA (T) SQUARED
        STZ DE6F+0518     SET K=0, (K=0(1)6)
        SSM
        STO DE6F+0709     FIX SWITCH FOR 2ND, ETC ENTRIES
    
```

DE6FN2030
 DE6FN2040
 DE6FN2050
 DE6FN2060
 DE6FN2070
 DE6FN2080
 DE6FN2090
 DE6FN2100
 DE6FN2110
 DE6FN2140
 DE6FN2160
 DE6FN2170
 DE6FN2180
 DE6FN2190
 DE6FN2200
 DE6FN2210
 DE6FN2220
 DE6FN2230
 DE6FN2240
 DE6FN2250
 DE6FN2260
 DE6FN2270
 DE6FN2280
 DE6FN2290
 DE6FN2300
 DE6FN2310
 DE6FN2320
 DE6FN2330
 DE6FN2340
 DE6FN2350
 DE6FN2360
 DE6FN2370
 DE6FN2380
 DE6FN2390
 DE6FN2400
 DE6FN2410
 DE6FN2420
 DE6FN2430
 DE6FN2440
 DE6FN2450
 DE6FN2460
 DE6FN2470
 DE6FN2480
 DE6FN2490
 DE6FN2500
 DE6FN2510
 DE6FN2520
 DE6FN2530
 DE6FN2540
 DE6FN2550
 DE6FN2560

LXA DE6F+0527,1	7N(FIX TO SAVE 2ND DERIV.)	DE6FN251
SXD DE6F+0527,1	7N(=N)N	DE6FN251
CLA DE6F+0516	R=R,K. STEPS PER DELTA(T)	DE6FN251
STO DE6F+0515	R IN DECR.	DE6FN26
LXD DE6F+0515,1	R(=1)1	DE6FN26
CLA DE6F+0516	R=TOTAL R,K. STEPS PER D(T)	DE6FN26
SUB DE6F+0515	R(I)=CURRENT RI=R(=1)1 IN DECR.	DE6FN26
TNZ DE6F+0054	TR IF NOT 1ST R	DE6FN26
LXA DE6F+0710,4	N	DE6FN26
LXD DE6F+0527,2	7N(=N)N	DE6FN26
CLA 0,4	T+3N+3(2ND DERIV.)	DE6FN26
STO 0,2	T+11N+3+(7N),(7N 2ND DERIVS)	DE6FN26
TXI DE6F+0052,2,-1		DE6FN26
TIX DE6F+0049,4,1		DE6FN27
SXD DE6F+0527,2	7N(=N)N	DE6FN27
LXA DE6F+0518,2		DE6FN27
TXH DE6F+0122,2,5	IF K=6, TR TO COWELL	DE6FN27
TSX DE6F+0588,4	TR TO RUNGE KUTTA INTEGRATION	DE6FN27
TIX DE6F+0070,1,1	REDUCE R TIL R=RN	DE6FN27
LXD DE6F+0516,1	R=RN (RESTORE R FOR NEXT CYCLE)	DE6FN27
CLA DE6F+0518	K=0(1)6	DE6FN27
ADD DE6F+0531	1-	DE6FN27
STO DE6F+0518		DE6FN27
SUB DE6F+0533	3	DE6FN28
TNZ DE6F+0070	SAVE Y(3) AND Y(3) PRIME IF 0	DE6FN28
LXA DE6F+0710,2	N	DE6FN28
CLA 0,2	T+N+3=Y(I)=DEPENDENT VAR. (YI)	DE6FN28
STO 0,2	T+10N+3=Y(3)	DE6FN28
CLA 0,2	T+2N+3=Y(I) PRIME=1ST DERIV.	DE6FN28
STO 0,2	T+11N+3=Y(3)PRIME	DE6FN28
TIX DE6F+0065,2,1		DE6FN28
SXD DE6F+0515,1	SAVE R	DE6FN28
SSP	=RUNGE KUTTA	DE6FN28
STO DE6F+0503	=COWELL METHOD	DE6FN29
LXD DE6F+0506,4		DE6FN29
LXD DE6F+0504,1	1 R,K. STEP COMPLETED	DE6FN29
LXD DE6F+0505,2		DE6FN29
TRA 1,4	RETURN TO PROGRAMMER	DE6FN29
CLA DE6F+0519	OLD H (SUB. FOR NEW VMIN, VMAX, WMAX)	DE6FN29
STO COMMON+001	H1=OLD H (SAVE FOR CHANGE OF HMAX)	DE6FN29
CLA DE6F+0520	OLD H SQ.=H1 SQ.	DE6FN29
STO COMMON+000	H1 SQ.	DE6FN29
STQ DE6F+0519	NEW H=H2	DE6FN29
FMP DE6F+0519		DE6FN30
STO DE6F+0520	NEW H SQ.=H2 SQ.	DE6FN30
LXA DE6F+0533,5	3 IN IR1, IR4	DE6FN30
CLA COMMON+000	H1 SQ.	DE6FN30
FDP DE6F+0520	H2 SQ.	DE6FN30
FMP DE6F+0515,4	CHANGE VMIN, VMAX, VMAX	DE6FN30
STO DE6F+0515,4	(V/H1 SQ.)X(H1 SQ)/(H2 SQ.)	DE6FN30
TIX DE6F+0085,4,1		DE6FN30

TRA 1,2			DE6FN3080
LDQ 0	T+2=H (COORD. CHANGE BEGINS)		DE6FN3090
FMP DE6F+0544	-8.		DE6FN3100
FAD 0	T+1=T		DE6FN3110
STO 0	T+1		DE6FN3120
LXA DE6F+0528,1	8N		DE6FN3130
SXD DE6F+0528,1	8N(-N)0		DE6FN3140
CLA 0	T+1=(T)		DE6FN3150
FAD 0	T+2=H		DE6FN3160
STO 0	T+1=(T+H)		DE6FN3170
LXA DE6F+0710,2	N		DE6FN3180
CLA 0,1	T+11N+3+(8N)=(Y0,Y1,...,Y7)		DE6FN3190
STO 0,2	T+N+3		DE6FN3200
CLA 0,1	T+3N+3*(8N)=1ST DERIV.		DE6FN3210
STO 0,2	T+2N+3(IF SAVED)		DE6FN3220
TXI DE6F+0106,1,-1	MOVE DEPENDENT VAR. TO T+3 THRU T+N+2		DE6FN3230
TIX DE6F+0101,2,1			DE6FN3240
TSX 0,4	V (FORM2ND DERIV.)		DE6FN3250
LXD DE6F+0528,1	8N		DE6FN3260
LXA DE6F+0710,2	N		DE6FN3270
CLA 0,2	T+3N+3 (2ND DERIV.)		DE6FN3280
STO 0,1	T+3N+3+(8N)		DE6FN3290
TXI DE6F+0113,1,-1	STORE 2ND DERIV. (8 SETS)		DE6FN3300
TIX DE6F+0110,2,1			DE6FN3310
TXH DE6F+0096,1,0	LOOP FOR 8 SETS OF Y		DE6FN3320
LDQ 0	(T+2)=H=DELTA(T)		DE6FN3330
TSX DE6F+0077,2	CHANGE VMIN, VMAX, WMAX		DE6FN3340
CLA DE6F+0519	H2=NEW H		DE6FN3350
FDP COMMON+001	H1=OLD H		DE6FN3360
FMP DE6F+0512,1	CHANGE UNITS OF HMIN,HMAX,		DE6FN3370
STO DE6F+0512,1	AND XMIN		DE6FN3380
TIX DE6F+0117,1,1			DE6FN3390
STZ DE6F+0521	CLEAR W, W=MAX (DELTA VII)/Y		DE6FN3400
STZ DE6F+0522	CLEAR V, V=MAX (DELTA VI)/Y		DE6FN3410
LXA DE6F+0529,4	.11N		DE6FN3420
SXD DE6F+0529,4			DE6FN3430
LXA DE6F+0710,4	N		DE6FN3440
LXA DE6F+0527,2	7N		DE6FN3450
SXD DE6F+0527,2	7N(-1)6N		DE6FN3460
CLA 0,4	T+N+3=Y		DE6FN3470
STO DE6F+0711	SEE V AND W CALC.		DE6FN3480
CLA DE6F+0502	NORMALLY=8 (NO CHANGE IN COORD.)		DE6FN3490
TNZ DE6F+0316	0=COORD. CHANGE		DE6FN3500
TSX DE6F+0380,2	FORM DIFF.		DE6FN3510
PZE 0	T+3N+3+(7N)		DE6FN3520
CLA DE6F+0520	H.SQ.		DE6FN3530
TSX DE6F+0344,2	FORM SUM OF PRODUCTS		DE6FN3540
PZE DE6F+0552,0,COMMON+21	C(I)XDELTAS		DE6FN3550
CLA 0,4	T+15N+3(Y3,COORD. CHANGE)		DE6FN3560
TSX DE6F+0482,2	ADD Y3 TO C+3,0+4		DE6FN3570
TSX DE6F+0373,2	F4(II) IN A1 AND A2		DE6FN3580

```

CLS DE6F+0507
STO DE6F+0714      -F4(II)
CLS DE6F+0508
STO DE6F+0715
TSX DE6F+0380,2    FORM DIFF.
PZE 0              T+4N+3+(7N)
TSX DE6F+0345,2    H. SQ. STILL IN COM+2
PZE DE6F+0552,0,COMMON+21
CLA 0,4            T+16N+3,(Y4, COORD. CHANGE)
TSX DE6F+0482,2    ADD Y4 TO C+3,C+4
TSX DE6F+0373,2    F5(II) IN A1 AND A2
CLA DE6F+0714
STO COMMON+003     -F4(II)
CLA DE6F+0715
STO COMMON+004
TSX DE6F+0491,2    F4(I)=F5(II)-F4(II)
STO COMMON+003     -F4(I)
STQ COMMON+004
CLA COMMON+008     Y4 (2ND DERIV.)
TSX DE6F+0482,2    F5(I) IN COMMON+3,4
LXA DE6F+0533,1    3
TSX DE6F+0491,2    F5(II) OR F6(II) IF COORD. CHG.
STO DE6F+0507
STQ DE6F+0508
CLA COMMON+012,1   Y(4),Y(5),Y(6) 2ND DERIV.
TSX DE6F+0482,2    OR Y(5),Y(6),Y(7) IF COORD. CHANGE
TSX DE6F+0491,2    FORM F5(II),F6(II),F7(II),F8(II)
TIX DE6F+0163,1,1 OR F6(II),F7(II),F8(II),F9(II)

STO COMMON+027     F8(II) OR F9(II)
STQ COMMON+028
CLA COMMON+003     F7(I) OR F8(I)
STO COMMON+029
CLA COMMON+004
STO COMMON+030
LXD DE6F+0529,1    11N(=11)11
LXA DE6F+0541,2    11
CLA COMMON+031,2   SAVE DIFF. AND F8(II),F7(I)
STO 0,1            T+19N+3+(11N)
TXI DE6F+0180,1,-1
TIX DE6F+0177,2,1
SXD DE6F+0529,1    SAVE FOR NEXT SET
LXD DE6F+0527,2
TXI DE6F+0184,2,-1
TIX DE6F+0128,4,1 COMPLETE N EQNS.
TSX DE6F+0414,4    TEST H (MAY TR R.K. AGAIN)
CLA DE6F+0502      8(=1)0 IF COORD. CHG. (NORMALLY=8)
TNZ DE6F+0191      IF NOT=0, STILL IN COORD. CHG. OR NORMAL
CLA DE6F+0538      8 RESTORE COUNTER FOR
STO DE6F+0502      NEXT CHANGE IN COORD.
STZ DE6F+0500      RESTORE SWCH TO NORMAL

```

```

DE6FN359
DE6FN360
DE6FN361
DE6FN362
DE6FN363
DE6FN364
DE6FN365
DE6FN366
DE6FN367
DE6FN368
DE6FN369
DE6FN370
DE6FN371
DE6FN372
DE6FN373
DE6FN374
DE6FN375
DE6FN376
DE6FN377
DE6FN378
DE6FN379
DE6FN380
DE6FN381
DE6FN382
DE6FN383
DE6FN384
DE6FN385
DE6FN386
DE6FN387
DE6FN388
DE6FN389
DE6FN390
DE6FN391
DE6FN392
DE6FN393
DE6FN394
DE6FN395
DE6FN396
DE6FN397
DE6FN398
DE6FN399
DE6FN400
DE6FN401
DE6FN402
DE6FN403
DE6FN404
DE6FN405
DE6FN406
DE6FN407
DE6FN408
DE6FN409

```

DE6FN (Cont'd)

CLA DE6F+0519	H		DE6FN4100
STO		T+2=(H) RESTORE AFTER R,K.	DE6FN4110
FAD		T+1=T=INDEPENDENT VAR.	DE6FN4120
STO COMMON+000		T+H/2 (MOST SIG.)	DE6FN4130
STQ COMMON+001		LST, SIG.	DE6FN4140
CLA COMMON+001			DE6FN4150
FAD DE6F+0718		CUM, LST, SIG.	DE6FN4160
FAD COMMON+000			DE6FN4170
STQ DE6F+0718		SAVE LST, SIG. FOR NEXT INTEGRATION	DE6FN4180
STO		T+1=(T+H)	DE6FN4190
LXA DE6F+0710,4		N	DE6FN4200
LXA DE6F+0529,1		11N	DE6FN4210
CLA DE6F+0530		T+19N+3+(7)	DE6FN4220
STA DE6F+0208			DE6FN4230
STA DE6F+0218		T+19N+3+(7)	DE6FN4240
CLA DE6F+0520			DE6FN4250
TSX DE6F+0344,2			DE6FN4260
PZE 0,0,DE6F+0566		N+3+(7) STORED ABOVE (+11N)	DE6FN4270
LDQ DE6F+0520	H SQ		DE6FN4280
FMP 0,1		T+19N+3+(11N+7)=F8(II)	DE6FN4290
TSX DE6F+0473,2			DE6FN4300
FAD COMMON+003			DE6FN4310
STO 0,4		T+N+3=NEW Y	DE6FN4320
CLA DE6F+0717		TEST MISSING 1ST DERIV. IN F	DE6FN4330
TMI DE6F+0224		=F(X,Y), +=F(X,Y,Y PRIME)	DE6FN4340
CLA DE6F+0519	H		DE6FN4350
TSX DE6F+0344,2			DE6FN4360
PZE 0,0,DE6F+0587		N+3+(7) (+11N) INCR. BY 11.	DE6FN4370
LDQ DE6F+0519	H		DE6FN4380
FMP 0,1		T+19N+3+(11N+9)=F7(I)	DE6FN4390
TSX DE6F+0473,2			DE6FN4400
FAD COMMON+003			DE6FN4410
STO 0,4		T+2N+3=NEW Y PRIME	DE6FN4420
CAL DE6F+0208		T+19N+3+(7)	DE6FN4430
ADM DE6F+0541	11		DE6FN4440
STA DE6F+0208			DE6FN4450
STA DE6F+0218			DE6FN4460
TXI DE6F+0229,1,-11		SET UP NEXT F8(II),F7(I)	DE6FN4470
TIX DE6F+0206,4,1		LOOP FOR N EQNS.	DE6FN4480
TSX 0,4		V (TR TO FORM 2ND DERIV.)	DE6FN4490
LXA DE6F+0529,1		11N	DE6FN4500
LXA DE6F+0710,4		N	DE6FN4510
LXA DE6F+0541,2		11	DE6FN4520
CLA 0,1		T+19N+3+(11N)	DE6FN4530
STO COMMON+031,2		READ DIFF. TO COM+20	DE6FN4540
TXI DE6F+0237,1,-1			DE6FN4550
TIX DE6F+0234,2,1			DE6FN4560
SXD DE6F+0529,1			DE6FN4570
CLA 0,4		T+3N+3=Y(7) 2ND DERIV.	DE6FN4580
STO COMMON+039		Y(7) 2ND DERIV.	DE6FN4590
LXA DE6F+0536,1		6	DE6FN4600

DE6FN (Cont'd)

LXA DE6F+0571,2	ZERO TO IR2	DE6FN461
FSB COMMON+026,2	Y(6) 2ND DERIV. D5(I)...D0(VI)	DE6FN462
STO COMMON+038,2	D6(I),D5(II),D4(III),...,D1(VI)	DE6FN463
TXI DE6F+0246,2,1	WE ARE GOING BACKWARDS HERE	DE6FN464
TIX DE6F+0243,1,1		DE6FN465
CLA DE6F+0520	H SQ.	DE6FN466
TSX DE6F+0344,2	B(I) X DELTAS	DE6FN467
PZE DE6F+0573,0,COMMON+40		DE6FN468
LDQ DE6F+0520	H SQ.	DE6FN469
FMP COMMON+027	F8(II)	DE6FN470
TSX DE6F+0473,2		DE6FN471
FAD COMMON+003		DE6FN472
STO 0,4	T+N+3=NEW Y	DE6FN473
CLA DE6F+0500	TEST COORD. CHANGE	DE6FN474
TNZ DE6F+0258	CANNOT SAVE IF COORD. CHANGE	DE6FN475
STQ 0,4	T+9N+3=LST. SIG. (FOR R.K.)	DE6FN476
CLA DE6F+0519	H	DE6FN477
TSX DE6F+0344,2	B(I) DOT Y DELTAS	DE6FN478
PZE DE6F+0580,0,COMMON+40		DE6FN479
LDQ DE6F+0519	H	DE6FN480
FMP COMMON+029	F7(I)	DE6FN481
TSX DE6F+0473,2		DE6FN482
FAD COMMON+003		DE6FN483
STO 0,4	T+2N+3=NEW Y PRIME	DE6FN484
CLA DE6F+0500		DE6FN485
TNZ DE6F+0269		DE6FN486
STQ 0,4	T+5N+3=LST. SIG. (FOR R.K.)	DE6FN487
LXD DE6F+0529,1		DE6FN488
TIX DE6F+0233,4,1	COMPLETE N SETS	DE6FN489
TSX 0,4	V (FORM Y(7) 2ND DERIV.	DE6FN490
STZ DE6F+0522	CLEAR V	DE6FN491
STZ DE6F+0521	CLEAR W	DE6FN492
LXA DE6F+0529,4	11N	DE6FN493
LXA DE6F+0710,1	N	DE6FN494
SXD DE6F+0529,4	11N(-11)11	DE6FN495
LXA DE6F+0541,2	11	DE6FN496
CLA 0,4	T+19N+3+(11N)	DE6FN497
STO COMMON+031,2	READ DIFF. TO COM+20	DE6FN498
TXI DE6F+0281,4,-1		DE6FN499
TIX DE6F+0278,2,1		DE6FN500
CLA 0,1	T+3N+3=Y(7) 2ND DERIV.	DE6FN501
STO COMMON+039	Y(7) 2ND DERIV.	DE6FN502
CLA COMMON+029	F7(I) MOST SIG.	DE6FN503
STO COMMON+003		DE6FN504
CLA COMMON+030	F7(I) LST. SIG.	DE6FN505
STO COMMON+004		DE6FN506
CLA COMMON+039	Y(7) 2ND DERIV.	DE6FN507
TSX DE6F+0482,2		DE6FN508
STO COMMON+042	F8(I) MOST SIG.	DE6FN509
STQ COMMON+043	F8(I) LST. SIG.	DE6FN510
CLA COMMON+027	F8(II) MOST. SIG.	DE6FN511

DE6FN (Cont'd)

STO DE6F+0507		DE6FN5120
CLA COMMON+028	F8(II) LST. SIG.	DE6FN5130
STO DE6F+0508		DE6FN5140
TSX DE6F+0491,2	DOUBLE PREC. FAD	DE6FN5150
STO COMMON+040	F9(II) MOST. SIG.	DE6FN5160
STQ COMMON+041	F9(II) LST. SIG.	DE6FN5170
LXA DE6F+0536,4	6	DE6FN5180
LXA DE6F+0571,2		DE6FN5190
CLA COMMON+039,2	Y(7) 2ND DERIV., D6(I), ..., D1(VI)	DE6FN5200
FSB COMMON+026,2	Y(6) 2ND DERIV., D5(I), ..., D0(VI)	DE6FN5210
STO COMMON+038,2	D6(I), D5(II), ..., D1(VI)	DE6FN5220
TXI DE6F+0305,2,1	WE ARE GOING BACKWARDS HERE	DE6FN5230
TIX DE6F+0301,4,1		DE6FN5240
LXD DE6F+0529,4	11N(-11)11	DE6FN5250
LXA DE6F+0541,2	11	DE6FN5260
CLA COMMON+044,2	SAVE FOR NEXT INTEGRATION	DE6FN5270
STO 0,4	T+19N+3+(11N)	DE6FN5280
TXI DE6F+0311,4,-1		DE6FN5290
TIX DE6F+0308,2,1		DE6FN5300
TXH DE6F+0340,1,*	N=B IN DECR.	DE6FN5310
TIX DE6F+0276,1,1	COMPLETE N SETS	DE6FN5320
SSM	=COWELL STEP	DE6FN5330
TRA DE6F+0072	RETURN TO PROGRAMMER	DE6FN5340
TSX DE6F+0380,2	NORMAL CASE (NO COORD. CHANGE)	DE6FN5350
PZE 0	T+11N+3+(7N) (FORM DIFF.)	DE6FN5360
CLA DE6F+0519	H	DE6FN5370
TSX DE6F+0344,2	FORM SUM OF PRODUCTS	DE6FN5380
PZE DE6F+0559,0,COMMON+21	D(I)XDELTA	DE6FN5390
CLA 0,4	T+11N+3 (Y3 DOT)	DE6FN5400
TSX DE6F+0482,2	ADD Y3 DOT TO C+3,C+4	DE6FN5410
TSX DE6F+0373,2	F4(I) IN A1 AND A2	DE6FN5420
CLA DE6F+0507		DE6FN5430
STO DE6F+0714	F4(I)	DE6FN5440
CLA DE6F+0508		DE6FN5450
STO DE6F+0715		DE6FN5460
CLA DE6F+0520	H SQ.	DE6FN5470
TSX DE6F+0344,2	FORM SUM OF PRODUCTS	DE6FN5480
PZE DE6F+0552,0,COMMON+21	D(I) X DELTAS	DE6FN5490
CLA 0,4	T+10N+3 (Y3)	DE6FN5500
TSX DE6F+0482,2	ADD Y3 TO C+3,C+4	DE6FN5510
TSX DE6F+0373,2	F4(II) IN A1 AND A2	DE6FN5520
CLA DE6F+0714	F4(I)	DE6FN5530
STO COMMON+003		DE6FN5540
CLA DE6F+0715		DE6FN5550
STO COMMON+004		DE6FN5560
TXH DE6F+0453,4,*	N=B IN DECR. (TEST 1ST B EQNS)	DE6FN5570
TRA DE6F+0161		DE6FN5580
CLA 0,1	T+N+3=Y	DE6FN5590
STO DE6F+0711	Y	DE6FN5600
TSX DE6F+0455,2	FORM MAX V. W.	DE6FN5610
TRA DE6F+0313	FOR THIS Y	DE6FN5620

DE6FN (Cont'd)

STO COMMON+002	H SQ, OR H IN AC	DE6FN562
SXD DE6F+0707,1	SUB, TO FORM (CONSTANTS X DIFF.)	DE6FN564
SXD DE6F+0708,2		DE6FN565
CAL 1,2	A,0,B (A=CONSTANTS, B=DIFF.)	DE6FN566
STA DE6F+0356	CONSTANT ADDR. +7	DE6FN567
ARS 18		DE6FN568
STA DE6F+0357	DIFF. ADDR. +7	DE6FN569
CLA COMMON+008	Y3. 2ND DERIV.	DE6FN570
STO COMMON+014	(OR Y4 IF COORD, CHANGE)	DE6FN571
STZ COMMON+003		DE6FN572
STZ COMMON+004		DE6FN573
LXA DE6F+0537,1		DE6FN574
LDQ 0,1		DE6FN575
FMP 0,1	CO+7, OR DO+7, OR N6+7, ETC.	DE6FN576
TSX DE6F+0473,2	COMMON+21, OR COM+27, ETC.	DE6FN577
TIX DE6F+0356,1,1	ACCUM. PRODUCT IN C+3,C+4.	DE6FN578
LDQ COMMON+002		DE6FN579
FMP COMMON+003	H SQ, OR H	DE6FN580
STO COMMON+003	MOST SIG.	DE6FN581
STQ COMMON+000		DE6FN582
LDQ COMMON+002	H SQ, OR H	DE6FN583
FMP COMMON+004		DE6FN584
FAD COMMON+000		DE6FN585
FAD COMMON+003		DE6FN586
STO COMMON+003	MOST SIG. IN COMMON+3	DE6FN587
STQ COMMON+004	LST. SIG. IN COMMON+4	DE6FN588
LXD DE6F+0707,1		DE6FN589
LXD DE6F+0708,2		DE6FN590
TRA 2,2		DE6FN591
CLA COMMON+003	DIVIDES C+3,C+4 BY C+2	DE6FN592
FDP COMMON+002	H SQ OR H	DE6FN593
STQ DE6F+0507	MOST SIG. IN A1	DE6FN594
FAD COMMON+004	REMAINDER + LST. SIG.	DE6FN595
FDP COMMON+002	H SQ, OR H	DE6FN596
STQ DE6F+0508	LST. SIG. IN A2	DE6FN597
TRA 1,2		DE6FN598
SXD DE6F+0716,2	MOVE 2ND DERIV. AND FORM DIFF.	DE6FN599
CAL 1,2	STARTING ADDR. OF 2ND DERIV.	DE6FN600
STA DE6F+0385		DE6FN601
LXD DE6F+0527,2	7N(-1)6N	DE6FN602
LXA DE6F+0571,1		DE6FN603
CLA 0,2	START ADDR. (T+11N+3+(7N), ETC.)	DE6FN604
STO COMMON+005,1	MOVE 2ND DERIV. TO COM+5	DE6FN605
STO COMMON+020,1	AND COM+20	DE6FN606
TXI DE6F+0389,1,-1		DE6FN607
TIX DE6F+0385,2,+	N IN DECR.	DE6FN608
LXA DE6F+0536,2	6 (FORM DIFFERENCES)	DE6FN609
SXD COMMON+000,2		DE6FN610
LXA DE6F+0571,1	ZERO (2ND DERIV. STORED AT	DE6FN611
CLA COMMON+021,1	AT COMMON+5, AGAIN AT COM +20	DE6FN612
FSB COMMON+020,1	FORM DIFFERENCES IN	DE6FN613

DE6FN (Cont'd)

STO COMMON+020,1	COM+20 THRU COM+25	DE6FN6140
TXI DE6F+0397,1,-1		DE6FN6150
TIX DE6F+0393,2,1	LOOP 6,5,.,.,.,1 TIMES	DE6FN6160
LXD COMMON+000,2		DE6FN6170
TXH DE6F+0405,2,5	TR IF 1ST DIFF.	DE6FN6180
TXH DE6F+0408,2,3	TR IF 2ND OR 3RD DIFF.	DE6FN6190
TXH DE6F+0411,2,1	TR IF 4TH OR 5TH DIFF.	DE6FN6200
TIX DE6F+0391,2,1		DE6FN6210
LXD DE6F+0716,2		DE6FN6220
TRA 2,2		DE6FN6230
CLA COMMON+023	DELTA (I)3	DE6FN6240
STO COMMON+015	IN COM+15	DE6FN6250
TRA DE6F+0402		DE6FN6260
CLA COMMON+022	DELTA (II)2 OR DELTA (III)2	DE6FN6270
STO COMMON+021,2	IN COM+16 OR COM+17	DE6FN6280
TRA DE6F+0402		DE6FN6290
CLA COMMON+021	DELTA(IV)1 OR DELTA(V)1	DE6FN6300
STO COMMON+021,2	IN COM+18 OR COM+19	DE6FN6310
TRA DE6F+0402		DE6FN6320
CLA DE6F+0500	SWITCH (0=NORMAL CASE)	DE6FN6330
TNZ 1,4	- STOP TEST IF NON/ZERO	DE6FN6340
CLA DE6F+0501	TEST FIXED H	DE6FN6350
TMI 1,4	-=FIXED H INTERGRATION	DE6FN6360
CLA DE6F+0519	H=DELTA(T) COWELL TEST	DE6FN6370
FDP DE6F+0719	2.	DE6FN6380
STQ COMMON+000	H/2	DE6FN6390
CLA DE6F+0523	002.0 (WILL MULT BY 2 SQUARED	DE6FN6400
STO COMMON+001	WILL MULT VMAX, VMIN, AND WMAX	DE6FN6410
CLA DE6F+0509	MINIMUM H ALLOWED (CAN=0)	DE6FN6420
LRS 0	SET SIGNS PLUS	DE6FN6430
TLQ DE6F+0438	H/2 LESS THAN H MIN.	DE6FN6440
CLA DE6F+0513	10 TO (3=S)/(H SQUARED) =MAX V	DE6FN6450
LDQ DE6F+0522	V=MAX (DELTA VI)/Y	DE6FN6460
TLQ DE6F+0438	V LESS THAN MAX. V	DE6FN6470
CLA COMMON+000	H/2 OR 2H	DE6FN6480
STO DE6F+0519	SET H=H/2 (OR 2H) AND	DE6FN6490
LXA DE6F+0533,4	3 (SCALE VMIN, VMAX, AND WMAX)	DE6FN6500
CLA DE6F+0515,4	VMIN, VMAX, AND WMAX	DE6FN6510
TZE DE6F+0436	SKIP IF ZERO	DE6FN6520
ADD COMMON+001	* OR = 002.0	DE6FN6530
STO DE6F+0515,4	NEW VALUES DUE TO CHANGE IN H	DE6FN6540
TIX DE6F+0432,4,1		DE6FN6550
TRA DE6F+0030	RETURN TO RUNGE KUTTA	DE6FN6560
CLA DE6F+0519	H=DELTA(T)	DE6FN6570
FAD DE6F+0519		DE6FN6580
STO COMMON+000	2H	DE6FN6590
SSP		DE6FN6600
LDQ DE6F+0510	MAXIMUM H ALLOWED	DE6FN6610
TLQ DE6F+0452	2H GREATER THAN H MAX.	DE6FN6620
LDQ DE6F+0512	10 TO (-1=S)/(H SQUARED)= VMIN	DE6FN6630
CLA DE6F+0522	V=MAX(DELTA VII)/Y	DE6FN6640

DE6FN- (Cont'd)

TLQ DE6F+0452	V GR. THAN V MIN	DE6FN666
CLS DE6F+0523	002.0 DIVIDES BY 2 SQUARED	DE6FN666
STO COMMON+001	DECREASES VMIN, WMAX, VMAX	DE6FN666
CLA DE6F+0514	10 TO $(-1+S)/(H \text{ SQUARED}) = HMAX$	DE6FN666
LDO DE6F+0521	$W = MAX (\Delta VII) / Y$	DE6FN666
TLO DE6F+0429	W LESS THAN W MAX. (SET H=2H)	DE6FN670
TRA 1,4	RETURN TO PROGRAM	DE6FN670
TSX DE6F+0455,2	FORM LARGEST V AND W	DE6FN670
TRA DE6F+0339		DE6FN670
CLA DE6F+0501	SUB TO FORM MAX V AND W FOR 1ST N-B EQNS.	DE6FN670
TMI 1,2	--FIXED H INTEGRATION	DE6FN670
CLA DE6F+0711	Y	DE6FN670
SSP	SET Y PLUS	DE6FN670
LDO DE6F+0511	A=MIN. Y ALLOWED	DE6FN670
TLQ DE6F+0462	TR. IF Y GREATER THAN Y MIN.	DE6FN670
STQ DE6F+0711	OTHERWISE, SET Y=Y MIN.=A	DE6FN680
SXD COMMON+002,1		DE6FN680
LXA DE6F+0532,1	2	DE6FN680
CLA COMMON+022,1	DELTA VI (OR DELTA V)	DE6FN680
FDP DE6F+0711	Y (OR Y MIN)	DE6FN680
CLA DE6F+0523,1	MAX, W (OR V) THIS FAR.	DE6FN680
LRS 0	SET SIGNS PLUS	DE6FN680
TLQ DE6F+0470	NEW W (OR V) IS SMALLER	DE6FN680
STQ DE6F+0523,1	NEW MAX, W (OR V)	DE6FN680
TIX DE6F+0464,1,1	LOOP FOR V	DE6FN680
LXD COMMON+002,1		DE6FN690
TRA 1,2		DE6FN690
STQ COMMON+000	LST SIG. (PREC. AND 1/2)	DE6FN690
FAD COMMON+003	MOST SIG.	DE6FN690
STO COMMON+003		DE6FN690
STQ COMMON+001		DE6FN690
CLA COMMON+000		DE6FN690
FAD COMMON+001		DE6FN690
FAD COMMON+004		DE6FN690
STO COMMON+004	LST. SIG.	DE6FN690
TRA 1,2		DE6FN700
UFA COMMON+003	ADDS AC TO COM+3, COM+4	DE6FN700
STO COMMON+003	AND STORES ANSWER IN C+3,C+4.	DE6FN700
STQ COMMON+000		DE6FN700
CLA COMMON+000		DE6FN700
UFA COMMON+004		DE6FN700
FAD COMMON+003		DE6FN700
STO COMMON+003	MOST SIG. IN COMMON+3	DE6FN700
STQ COMMON+004	LST. SIG. IN COMMON+4	DE6FN700
TRA 1,2		DE6FN700
CLA DE6F+0507	DOUBLE PRECISION FAD	DE6FN710
UFA COMMON+003		DE6FN710
STO COMMON+001		DE6FN710
STQ COMMON+000		DE6FN710
CLA COMMON+000		DE6FN710
UFA DE6F+0508		DE6FN710

DE6FN (Cont'd)

UFA COMMON*004		DE6FN7160
FAD COMMON*001		DE6FN7170
TRA 1,2		DE6FN7180
BSS 1	SWITCH (PROGRAMMER CHANGES) (0=NORMAL)	DE6FN7190
BSS 1	FIXED H STORAGE (=FIXED STEP SIZE)	DE6FN7200
BSS 1	COUNTER FOR CHANGE OF COORD.	DE6FN7210
BSS 1	*=R,K, STEP, =COWELL STEP	DE6FN7220
BSS 1	SAVE INDEX REG. FOR (IR1)	DE6FN7230
BSS 1	COWELL METHOD (IR2)	DE6FN7240
BSS 1	(IR4)	DE6FN7250
BSS 1	1ST NO. (MOST SIG.)	DE6FN7260
BSS 1	1ST NO. (LST. SIG.)	DE6FN7270
BSS 1	MIN. H (ABS. VALUE) PROG. SPEC.	DE6FN7280
BSS 1	HMAX (IF H=0, SET HMAX= 1E18	DE6FN7290
BSS 1	A=MIN. Y ALLOWED FOR TEST	DE6FN7300
BSS 1	10 TO (-1-S)/(H SQUARED)=VMIN	DE6FN7310
BSS 1	10 TO (3-S)/(H SQUARED)=VMAX	DE6FN7320
BSS 1	10 TO (-1-S)/(H SQUARED)=WMAX	DE6FN7330
BSS 1	R(I)=CURRENT RI=R(-1)1 IN DECR.	DE6FN7340
BSS 1	R=TOTAL ITERATIONS PER D(T)	DE6FN7350
BSS 1	R (FLOATING PT.) (ABOVE=FIXED PT.)	DE6FN7360
BSS 1	0(1)8 (COUNTER FOR R.K. LOOPS)	DE6FN7370
BSS 1	H=DELTA(T)=CURRENT D(T)	DE6FN7380
BSS 1	DELTA (T) SQUARED	DE6FN7390
BSS 1	W=MAX (DELTA VII)/Y	DE6FN7400
BSS 1	V=MAX(DELTA VI)/Y	DE6FN7410
OCT 002000000000	MULT. BY 2 SQUARED (OR DIVIDE)	DE6FN7420
OCT 233000000000	NO TO FLOAT FIXED PT NO.	DE6FN7430
DEC 1E18	IF H=0, SET HMAX = 1E18	DE6FN7440
DEC 0	2N	DE6FN7450
DEC 0	7N	DE6FN7460
DEC 0	.8N	DE6FN7470
DEC 0	11N	DE6FN7480
DEC 0	DUMMY=T+19N+3+(7)	DE6FN7490
DEC 1	1	DE6FN7500
DEC 2	2	DE6FN7510
DEC 3	3	DE6FN7520
DEC 4	4	DE6FN7530
DEC 5	5	DE6FN7540
DEC 6	6	DE6FN7550
DEC 7	7	DE6FN7560
DEC 8	8	DE6FN7570
DEC 9	9	DE6FN7580
DEC 10	10	DE6FN7590
DEC 11	11	DE6FN7600
DEC 13	13	DE6FN7610
DEC 1.		DE6FN7620
DEC =8.	=8.	DE6FN7630
DEC =8.333333333E-2	(SIGNS HAVE BEEN REVERSED) (C0)	DE6FN7640
DEC 0	C1=0	DE6FN7650
DEC +4.166666667E-3	C2	DE6FN7660

DE6FN (Cont'd)

DEC 0	C3=0	DE6FN76
DEC -5,125661376E-4	C4	DE6FN76
DEC 0	C5=0	DE6FN76
DEC +7,964065256E-5	C6	DE6FN77
DEC +0,5	(SIGNS HAVE BEEN REVERSED) (D0)	DE6FN77
DEC +8,333333333E-2	D1	DE6FN77
DEC -4,166666667E-2	D2	DE6FN77
DEC -1,527777778E-2	D3	DE6FN77
DEC +7,638888889E-3	D4	DE6FN77
DEC +3,1580688E-3	D5	DE6FN77
DEC -1,5790344E-3	D6	DE6FN77
DEC +6,549575617E-2	(NO CHANGE IN SIGNS) (N6)	DE6FN77
DEC +6,820436508E-2	N5	DE6FN77
DEC +7,134589948E-2	N4	DE6FN78
DEC +0,075	N3	DE6FN78
DEC +7,916666667E-2	N2	DE6FN78
DEC +8,333333333E-2	N1	DE6FN78
DEC +8,333333333E-2	N0	DE6FN78
DEC -2,708608907E-3	B6	DE6FN78
DEC -3,141534392E-3	B5	DE6FN78
DEC -3,654100529E-3	B4	DE6FN78
DEC -4,166666667E-3	B3	DE6FN78
DEC -4,166666667E-3	B2	DE6FN78
DEC 0	B1=0	DE6FN79
DEC +8,333333333E-2	B0	DE6FN79
DEC -1,136739418E-2	B6 DOT	DE6FN79
DEC -1,426917989E-2	B5 DOT	DE6FN79
DEC -1,875E-2	B4 DOT	DE6FN79
DEC -2,638888889E-2	B3 DOT	DE6FN79
DEC -4,166666667E-2	B2 DOT	DE6FN79
DEC -8,333333333E-2	B1 DOT	DE6FN79
DEC +0,5	B0 DOT	DE6FN79
DEC .304224537	(NO CHANGE IN SIGNS) (N6 DOT)	DE6FN79
DEC .315591931	N5 DOT	DE6FN80
DEC .329861111	N4 DOT	DE6FN80
DEC .348611111	N3 DOT	DE6FN80
DEC .375000000	N2 DOT	DE6FN80
DEC .416666666	N1 DOT	DE6FN80
DEC .500000000	N0 DOT	DE6FN80
TRA DE6F+0725	TO SET UP ROUTINE (RUNGE KUTTA SUB)	DE6FN80
SXD DE6F+0707,1	SAVE INDEX REG.	DE6FN80
SXD DE6F+0708,2	FROM	DE6FN80
SXD DE6F+0709,4	MAIN PROGRAM (NEW R.K. STARTS)	DE6FN80
CLA 0	(T+2)=H	DE6FN81
STO DE6F+0713	H	DE6FN81
FDP DE6F+0719	2,	DE6FN81
STQ DE6F+0714	H/2	DE6FN81
STQ DE6F+0715	H/2,	DE6FN81
FMP DE6F+0713	H	DE6FN81
STO DE6F+0711	(H SQ)/2	DE6FN81
FDP DE6F+0720	4,	DE6FN81

DE6FN (Cont'd)

STQ DE6F+0712.	(H SQ)/8	DE6FN8180
CLA DE6F+0713	H	DE6FN8190
FDP DE6F+0722	6,	DE6FN8200
STQ DE6F+0716	H/6	DE6FN8210
LXA DE6F+0710,1	N	DE6FN8220
CLA 0,1	SAVE YI (T+N+3)=YI (M.S.)	DE6FN8230
STO 0,1	(T+8N+3)=YI MOST SIG.	DE6FN8240
CLA 0,1	SAVE YI PRIME (T+2N+3)	DE6FN8250
STO 0,1	(T+4N+3)=YI PRIME MOST SIG.	DE6FN8260
TIX DE6F+0604,1,1		DE6FN8270
LXA DE6F+0723,1	1	DE6FN8280
SXD DE6F+0724,1	K=1(+1)4	DE6FN8290
LXA DE6F+0710,6	N TO IR2 AND IR4	DE6FN8300
TXL DE6F+0629,1,1	TR IF K=1	DE6FN8310
TXL DE6F+0649,1,2	TR IF K=2	DE6FN8320
TXL DE6F+0629,1,3	TR IF K=3	DE6FN8330
LXA DE6F+0710,2	K=4 (N TO IR4)	DE6FN8340
CLA 0,2	T+3N+3=F(X,Y,Y PRIME)	DE6FN8350
FAD 0,2	T+6N+3=CUM. D(YN) PRIME.	DE6FN8360
STO 0,2	T+6N+3=NEW D(YN) PRIME	DE6FN8370
TIX DE6F+0616,2,1		DE6FN8380
TXH DE6F+0669,1,3	OUT IF K=4	DE6FN8390
TIX DE6F+0615,1,1	ADD 2F(X,Y,PRIME) IF K=2,3	DE6FN8400
LXD DE6F+0724,1	K	DE6FN8410
TXH DE6F+0626,1,2	TR IF K=3	DE6FN8420
CLA DE6F+0717	TEST MISSING 1ST DERIV. IN F	DE6FN8430
TMI DE6F+0628	=F(X,Y,Y PRIME)	DE6FN8440
TSX 0,4	V (TR OUT FOR F(X,Y,Y PRIME)	DE6FN8450
LXD DE6F+0724,1		DE6FN8460
TXI DE6F+0610,1,1	INCREASE K BY 1	DE6FN8470
CLA 0	T+1=(T)	DE6FN8480
FAD DE6F+0714	H/2	DE6FN8490
STO COMMON+000	T+H/2 (MOST SIG.)	DE6FN8500
STQ COMMON+001	LST. SIG.	DE6FN8510
CLA COMMON+001		DE6FN8520
FAD DE6F+0718	CUM. LST. SIG.	DE6FN8530
FAD COMMON+000		DE6FN8540
STQ DE6F+0718.	SAVE LST. SIG. FOR NEXT INTEGRATION	DE6FN8550
STO 0	T+1=(T+H/2)	DE6FN8560
TIX DE6F+0639,1,1	IR1=1 IF K=1, IR1=2 IF K=3	DE6FN8570
LDQ DE6F+0713,1	(H SQ)/8 OR (H SQ)/2 (K=1,3)	DE6FN8580
FMP 0,2	T+3N+3=F(X,Y,Y PRIME)	DE6FN8590
STO COMMON+000		DE6FN8600
LDQ DE6F+0715,1	(H/2) OR (H) K=1 OR 3	DE6FN8610
FMP 0,2	T+4N+3=YN PRIME (M.S.)	DE6FN8620
FAD COMMON+000	(H SQ)/8 X F(X,Y,YP)	DE6FN8630
FAD 0,2	T+8N+3=YN (M.S.)	DE6FN8640
STO 0,2	T+N+3=YN AT (T+H/2) OR (T+H)	DE6FN8650
TIX DE6F+0639,2,1	N WAS IN IR2	DE6FN8660
LXD DE6F+0724,1	RESTORE K TO 1 OR 3	DE6FN8670
CLA DE6F+0717	TEST MISSING 1ST DERIV. IN F	DE6FN8680

DE6FN (Cont'd)

TMI DE6F+0656	=F(X,Y), +=F(X,Y,Y PRIME)	DE6FN86
LDQ DE6F+0716,1	H/2 OR H	DE6FN87
FMP 0,4	T+3N+3=F(X,Y,Y PRIME)	DE6FN87
FAD 0,4	T+4N+3=YN PRIME (M.S.)	DE6FN87
STO 0,4	T+2N+3=NEW Y PRIME	DE6FN87
TIX DE6F+0651,4,1		DE6FN87
LXA DE6F+0710,2	N	DE6FN87
TXL DE6F+0664,1,1	TR TO STORE IF K=1	DE6FN87
CLA 0,2	T+3N+3=F(X,Y,Y PRIME)	DE6FN87
FAD 0,2	T+7N+3=CUM.DELTA(YN)	DE6FN87
STO 0,2	T+7N+3	DE6FN87
TIX DE6F+0658,2,1		DE6FN88
TXL DE6F+0615,1,2	TR IF K=2 (CONNOT=1)	DE6FN88
TXI DE6F+0615,1,-1	REDUCE K FROM 3 TO 2.	DE6FN88
CLA 0,2	T+3N+3=F(X,Y,Y PRIME)	DE6FN88
STO 0,2	T+6N+3=STORE FOR D(YN)PRIME	DE6FN88
STO 0,2	T+7N+3=STORE FOR D(YN)	DE6FN88
TIX DE6F+0664,2,1	N WAS IN IR2	DE6FN88
TRA DE6F+0626	TR FOR K=2	DE6FN88
LXA DE6F+0717,4	2N	DE6FN88
LXA DE6F+0710,2	N	DE6FN88
LDQ DE6F+0716	H/6	DE6FN89
FMP 0,4	T+7N+3=D(YN)P AND D(YN)	DE6FN89
STQ COMMON+002		DE6FN89
UFA 0,2	T+4N+3=YN PRIME (M.S.)	DE6FN89
STO COMMON+000		DE6FN89
STQ COMMON+001		DE6FN89
CLA COMMON+001		DE6FN89
UFA 0,2	T+5N+3=YN PRIME (LST. SIG.)	DE6FN89
UFA COMMON+002		DE6FN89
FAD COMMON+000		DE6FN89
STO 0,4	T+3N+3=(YN)P AND (YN) (M.S.)	DE6FN90
STQ 0,4	T+7N+3=(YN)P AND (YN) (L.S.)	DE6FN90
TXN DE6F+0686,4,1	(YN) DESTROYS F(X,Y,Y PRIME)	DE6FN90
TIX DE6F+0671,2,1	(YN)P AT T+N+3 (COMPLETED)	DE6FN90
TRA DE6F+0670	(YN) AT T+2N+3 (NOT COMPLETED)	DE6FN90
LXA DE6F+0710,2	N	DE6FN90
LDQ DE6F+0713	H	DE6FN90
FMP 0,2	T+3N+3=(YN PRIME + H/6(DY)	DE6FN90
STQ COMMON+002		DE6FN90
UFA 0,2	T+8N+3=YN (M.S.)	DE6FN90
STO COMMON+000		DE6FN91
STQ COMMON+001		DE6FN91
CLA COMMON+001		DE6FN91
UFA 0,2	T+9N+3=YN (L.S.)	DE6FN91
UFA COMMON+002		DE6FN91
FAD COMMON+000		DE6FN91
STO 0,2	T+N+3=Y(N+1) (M.S.)	DE6FN91
STQ 0,2	T+9N+3=Y(N+1) (L.S.)	DE6FN91
CLA 0,2	T+6N+3=Y(N+1)P (L.S.)	DE6FN91
STO 0,2	T+5N+3 (SAVE LST. SIG.)	DE6FN91

DE6FN (Cont'd)

TIX DE6F+0687,2,1			DE6FN9200
TSX 0,4	V (FORM 2ND DERIV.)		DE6FN9210
LXD DE6F+0709,4			DE6FN9220
LXD DE6F+0707,1			DE6FN9230
LXD DE6F+0708,2			DE6FN9240
TRA 1,4	LEAVE SUB, FROM 2ND ENTRY		DE6FN9250
PZE 2,0,0	IR1 SAVED IN DECR.		DE6FN9260
BSS 11			DE6FN9270
DEC 2.	2.		DE6FN9280
DEC 4.	4.		DE6FN9290
DEC 8.	8.		DE6FN9300
DEC 6.	6.		DE6FN9310
DEC 1	1		DE6FN9320
BSS 1	K=1(+1)4		DE6FN9330
SXD DE6F+0707,1	R.K. SET UP ENTRY		DE6FN9340
SXD DE6F+0708,2			DE6FN9350
SXD DE6F+0709,4			DE6FN9360
STZ DE6F+0718	CLEAR LST. SIG. OF T		DE6FN9370
CLA 1,4	T,0,V		DE6FN9380
STA DE6F+0708	T=ADDRESS		DE6FN9390
STO DE6F+0717	=F(X,Y), +=F(X,Y,Y PRIME)		DE6FN9400
STA DE6F+0737			DE6FN9410
ARS 18	V TO ADDR.		DE6FN9420
STA DE6F+0796	V		DE6FN9430
STA DE6F+0702	V		DE6FN9440
STA DE6F+0626			DE6FN9450
CLA	(T)=N		DE6FN9460
STO DE6F+0710	N		DE6FN9470
CAL DE6F+0708	T		DE6FN9480
ADD DE6F+0723	1		DE6FN9490
			DE6FN9500
STA DE6F+0629	T+1		DE6FN9510
STA DE6F+0637			DE6FN9520
ADD DE6F+0723	1		DE6FN9530
STA DE6F+0591	T+2		DE6FN9540
ADD DE6F+0723	1		DE6FN9550
ADM DE6F+0710	N		DE6FN9560
STA DE6F+0604	T+N+3=YI (STARTS AT T+3)		DE6FN9570
STA DE6F+0697	T+N+3=YI		DE6FN9580
STA DE6F+0646	T+N+3		DE6FN9590
ADM DE6F+0710	N		DE6FN9600
STA DE6F+0606	T+2N+3=YI PRIME (STARTS T+N+3)		DE6FN9610
STA DE6F+0654			DE6FN9620
ADM DE6F+0710	N		DE6FN9630
STA DE6F+0616	T+3N+3=2ND DERIV.		DE6FN9640
STA DE6F+0681			DE6FN9650
STA DE6F+0640	T+3N+3		DE6FN9660
STA DE6F+0652	T+3N+3		DE6FN9670
STA DE6F+0658	T+3N+3		DE6FN9680
STA DE6F+0664			DE6FN9690
STA DE6F+0688	T+3N+3		DE6FN9700

DE6FN (Cont'd)

ADM DE6F+0710	N	DE6FN9710
STA DE6F+0653	T+4N+3	DE6FN9720
STA DE6F+0607		DE6FN9730
STA DE6F+0643	T+4N+3	DE6FN9740
STA DE6F+0674	T+4N+3	DE6FN9750
ADM DE6F+0710	N	DE6FN9760
STA DE6F+0793	T+5N+3	DE6FN9770
STA DE6F+0700		DE6FN9780
STA DE6F+0678		DE6FN9790
ADM DE6F+0710	N	DE6FN9800
STA DE6F+0617	T+6N+3	DE6FN9810
STA DE6F+0618		DE6FN9820
STA DE6F+0665		DE6FN9830
STA DE6F+0699	T+6N+3	DE6FN9840
ADM DE6F+0710	N	DE6FN9850
STA DE6F+0660	T+7N+3	DE6FN9860
STA DE6F+0672		DE6FN9870
STA DE6F+0659		DE6FN9880
STA DE6F+0666		DE6FN9890
STA DE6F+0682	T+7N+3	DE6FN9900
ADM DE6F+0710	N	DE6FN9910
STA DE6F+0605	T+8N+3	DE6FN9920
STA DE6F+0645		DE6FN9930
STA DE6F+0690		DE6FN9940
ADM DE6F+0710	N	DE6FN9950
STA DE6F+0694	T+9N+3	DE6FN9960
STA DE6F+0698	T+9N+3	DE6FN9970
STA DE6F+0794		DE6FN9980
		DE6FN9990

DE6FN (Cont'd)

CAL DE6F+0710	N	DE6FN10000
PAX 0,1	N TO IR1	DE6FN10010
ADM DE6F+0710	N	DE6FN10020
STA DE6F+0717	2N TO ADDR. OF SAVE+10	DE6FN10030
STZ 0,1	T+5N+3 (CLEAR Y PRIME L.S.)	DE6FN10040
STZ 0,1	T+9N+3 (CLEAR Y LST. SIG.)	DE6FN10050
TIX DE6F+0793,1,1		DE6FN10060
TSX 0,4	V (FORM 2ND DERIV.)	DE6FN10070
LXD DE6F+0709,4	RESTORE IRC	DE6FN10080
TXI DE6F+0704,4,-1	TRA 2,4 FROM HERE	DE6FN10090
SXD DE6F+0504,1	COWELL SETUP	DE6FN10100
SXD DE6F+0505,2		DE6FN10110
SXD DE6F+0506,4		DE6FN10120
CLA 1,4	T,0,V	DE6FN10130
STO DE6F+0805	FIX RUNGE KUTTA (1ST ENTRY)	DE6FN10140
TSX DE6F+0587,4	TR TO SET UP RUNGE KUTTA	DE6FN10150
PZE	T,0,V	DE6FN10160
LXD DE6F+0506,4	RESTORE IR4 AFTER R.K.	DE6FN10170
CAL DE6F+0702	V	DE6FN10180
STA DE6F+0107	V	DE6FN10190
STA DE6F+0230	V	DE6FN10200
STA DE6F+0271	V	DE6FN10210
CAL DE6F+0717	2N	DE6FN10220
STA DE6F+0526		DE6FN10230
ADM DE6F+0645	T+8N+3	DE6FN10240
STA DE6F+0134	T+10N+3=T+3N+3+(7N)	DE6FN10250
STA DE6F+0066		DE6FN10260
STA DE6F+0331		DE6FN10270
ADM DE6F+0710	N	DE6FN10280
STA DE6F+0103	T+11N+3=T+3N+3+(8N)	DE6FN10290
STA DE6F+0111	T+3N+3+(8N)	DE6FN10300
STA DE6F+0146	T+4N+3+(7N)	DE6FN10310
STA DE6F+0068	T+11N+3	DE6FN10320
STA DE6F+0321		DE6FN10330
CAL DE6F+0794	T+9N+3	DE6FN10340
STA DE6F+0257		DE6FN10350
CAL DE6F+0700	T+5N+3	DE6FN10360
STA DE6F+0268		DE6FN10370
CAL DE6F+0681	T+3N+3	DE6FN10380
STA DE6F+0049		DE6FN10390
STA DE6F+0110		DE6FN10400
STA DE6F+0239		DE6FN10410
STA DE6F+0282	T+3N+3	DE6FN10420
CAL DE6F+0606	T+2N+3	DE6FN10430
STA DE6F+0067		DE6FN10440
STA DE6F+0104		DE6FN10450
STA DE6F+0223		DE6FN10460
STA DE6F+0265	T+2N+3	DE6FN10470
CAL DE6F+0697	T+N+3	DE6FN10480
STA DE6F+0065		DE6FN10490
STA DE6F+0102		DE6FN10500

DE6FN (Cont'd)

STA DE6F+0129		DE6FN105
STA DE6F+0213		DE6FN105
STA DE6F+0254		DE6FN105
STA DE6F+0340	T+N+3	DE6FN105
CAL DE6F+0629	T+1	DE6FN105
STA DE6F+0093		DE6FN105
STA DE6F+0094		DE6FN105
STA DE6F+0097		DE6FN105
STA DE6F+0099		DE6FN105
STA DE6F+0193		DE6FN106
STA DE6F+0200	T+1	DE6FN106
CAL DE6F+0591	T+2	DE6FN106
STA DE6F+0032		DE6FN106
STA DE6F+0091		DE6FN106
STA DE6F+0923	T+2	DE6FN106
STA DE6F+0098		DE6FN106
STA DE6F+0115		DE6FN106
STA DE6F+0192	T+2	DE6FN106
LDQ DE6F+0538	8	DE6FN106
MPY DE6F+0710	N	DE6FN107
STQ DE6F+0528	8N	DE6FN107
CAL DE6F+0528	8N	DE6FN107
SBM DE6F+0710	N	DE6FN107
STA DE6F+0527	7N	DE6FN107
ADM DE6F+0526	2N	DE6FN107
ADM DE6F+0526	2N	DE6FN107
STA DE6F+0529	11N	DE6FN107
ADM DE6F+0672	T+7N+3	DE6FN107
STA DE6F+0050	T+18N+3=T+11N+3+(7N)	DE6FN107
STA DE6F+0317	T+18N+3=T+11N+3+(7N)	DE6FN108
ADM DE6F+0710	N	DE6FN108
STA DE6F+0101	T+19N+3=T+11N+3+(8N)	DE6FN108
ADM DE6F+0537	7	DE6FN108
STA DE6F+0530	T+19N+10=T+19N+3+(7)	DE6FN108
CAL DE6F+0101	T+19N+3	DE6FN108
ADM DE6F+0529	11N	DE6FN108
STA DE6F+0178	T+30N+3=T+19N+3+(11N)	DE6FN108
STA DE6F+0234		DE6FN108
STA DE6F+0278		DE6FN108
STA DE6F+0309	T+30N+3	DE6FN109
ADM DE6F+0537	7	DE6FN109
STA DE6F+0210	T+30N+10=T+19N+3+(11N+7)	DE6FN109
ADM DE6F+0532	2	DE6FN109
STA DE6F+0220	T+30N+12=T+19N+3+(11N+9)	DE6FN109
CAL DE6F+0317	7+18N+3	DE6FN109
SBM DE6F+0526	2N	DE6FN109
STA DE6F+0149	T+16N+3	DE6FN109
SBM DE6F+0710	N	DE6FN109
STA DE6F+0138	T+15N+3	DE6FN109
LXA DE6F+0710,1	N	DE6FN110
SXD DE6F+0389,1	N TO DECR.	DE6FN110

DE6FN (Cont'd)

CLA 2,4	PZE=VAR, STEP SIZE (B,0,R)	DE6FN11020
STO DE6F+0501	MZE=FIXED STEP SIZE	DE6FN11030
STZ COMMON+000		DE6FN11040
STA COMMON+000	B (B LESS THAN OR =N)	DE6FN11050
STZ DE6F+0516		DE6FN11060
STD DE6F+0516	R=TOTAL R.K. LOOPS PER D(T)	DE6FN11070
CLA DE6F+0516		DE6FN11080
ARS 18		DE6FN11090
TNZ DE6F+0903		DE6FN11100
LXA DE6F+0534,1	4	DE6FN11110
SXD DE6F+0516,1	IF R=0, SET R=4	DE6FN11120
CLA DE6F+0534	4	DE6FN11130
ADD DE6F+0524	2330000000000	DE6FN11140
FAD DE6F+0571	FLOAT FIXED PT. NO.	DE6FN11150
STO DE6F+0517	R IN FLOATING PT.	DE6FN11160
CLA COMMON+000	TEST B=0	DE6FN11170
TNZ DE6F+0910		DE6FN11180
CLA DE6F+0710	IF B=0, SET B=N	DE6FN11190
STA COMMON+000	N	DE6FN11200
CAL DE6F+0710	N	DE6FN11210
SBM COMMON+000	B (OR N, IF B=0)	DE6FN11220
TPL DE6F+0914	PROGRAMMER GOOFED, IF MINUS	DE6FN11230
CLM	SET B=N IF B TOO LARGE (N-B=0)	DE6FN11240
ALS 18	N=B TO DECR.	DE6FN11250
STD DE6F+0338	1ST B EQNS. TESTED	DE6FN11260
STD DE6F+0312	N=B	DE6FN11270
CLA 3,4	S	DE6FN11280
TNZ DE6F+0920	IF S=0, SET S=9	DE6FN11290
CLA DE6F+0954	1E-9	DE6FN11300
STO COMMON+000	S (SEE VMIN, VMAX, WMAX.	DE6FN11310
STZ DE6F+0503	*=R.K., -=COWELL	DE6FN11320
STZ DE6F+0709	*=1ST R.K. INTEGRATION, -=2ND, ETC.	DE6FN11330
CLA	T+2=DELTA(T)=H	DE6FN11340
STO DE6F+0519		DE6FN11350
CLA 6,4	A=MIN. Y ALLOWED	DE6FN11360
TNZ DE6F+0928		DE6FN11370
CLA DE6F+0543	1. (IF A=0, SET A=1.)	DE6FN11380
STO DE6F+0511		DE6FN11390
CLA 4,4	MINIMUM H ALLOWED (FLOATING PT.)	DE6FN11400
SSP		DE6FN11410
STO DE6F+0509		DE6FN11420
CLA 5,4	MAXIMUM H ALLOWED (FLOATING PT.)	DE6FN11430
SSP		DE6FN11440
TNZ DE6F+0936	IF H=0, SET HMAX= 1E18	DE6FN11450
CLA DE6F+0525	1E18	DE6FN11460
STO DE6F+0510		DE6FN11470
LDQ DE6F+0519	DELTA(T)=H	DE6FN11480
FMP DE6F+0519		DE6FN11490
STO DE6F+0520	H SQ.	DE6FN11500
CLA COMMON+000	1E-S	DE6FN11510
FDP DE6F+0520	H SQ.	DE6FN11520

DE6FN (Cont'd)

FMP DE6F+0952	.1	DE6FN115
STO DE6F+0512	$V_{MIN} = (10)^{**}(-1-S)/H \text{ SQ.}$	DE6FN115
STO DE6F+0514	WMAX	DE6FN115
FDP DE6F+0953	1E-4	DE6FN115
STQ DE6F+0513	$V_{MAX} = (10)^{**}(3-S)/H \text{ SQ.}$	DE6FN115
STZ DE6F+0500	SWITCH (PROGRAMMER SETS NON/ZERO)	DE6FN115
CLA DE6F+0538	8 (SET UP COUNTER IN CASE	DE6FN115
STO DE6F+0502	OF CHANGE IN COORD.)	DE6FN115
LXD DE6F+0506,4	RETURN TO PROGRAMMER. (1ST ENTRY)	DE6FN115
TXI DE6F+0074,4,-6	TRA 7,4	DE6FN115
DEC .1	.1	DE6FN115
DEC 1E-4	.0001=1E-4	DE6FN115
DEC 1E-9	1E-9 (IF S=0)	DE6FN115
BREAK EQU *		DE6FN115
END EQU *		DE6FN115

Page Intentionally Left Blank

Function: DOT

Purpose: To find the dot product of two three-dimensional vectors.

Calling Sequence:

$$Z = \text{DOT}(X, Y)$$

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	X	3			First input vector
I	Y	3			Second input vector
O	Z				$Z = X(1)Y(1)+X(2)Y(2)+X(3)Y(3)$

Common storages used or required: None

Subroutines required: None

Functions required: None

Approximate number of storages required: _____

DOT

```
* LABEL  
* SYMBOL TABLE  
FUNCTION DOT(X,Y)  
DIMENSION X(3),Y(3)  
DOT = X(1)*Y(1) + X(2)*Y(2) + X(3)*Y(3)  
RETURN  
END
```

```
DOTO  
DOTO  
DOT0000  
DOT0010  
DOT0020  
DOT0030  
DOTO
```

Subroutine: EARTR

Purpose: Subroutine EARTR determines which tracking stations can observe the vehicle at the time EARTR is called. The subroutine then updates the state covariance matrix for the types of observations being performed by the tracking station. The possible types of observations are: range, range rate, azimuth-elevation, and direction cosines. The measurements may be corrupted by the following types of errors: random, bias, time bias, and station location errors. The subroutine input and output quantities are in common storage.

Calling Sequence:

CALL EARTR

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I					Quantities obtained from common
O					Quantities placed in common

Common storages used or required:

T, S, C, IC

Subroutines required:

CORRTP, DOT, GHA, INTRI, MATRX,
NUTAIT, SETN, TRAC, TRANSH

Functions required:

ARKTNS, ATAN, COS,
FNORM, SQRT, SIN

Approximate number of storages required:

1530

EARTR Partial Derivatives

To perform the covariance matrix updating for earth based tracking observations, a number of partial derivatives are required. The updating of the covariance matrix for observations requires the partial derivatives relating the types of measurements and the vehicle state. The evaluation of the errors in the measurements due to station location errors and time bias requires the partials which relate the measurements and the station latitude, longitude, altitude, and time.

The following quantities and relationships are used in the derivations of the various partials. Four important vectors are obtained by calling subroutine TRAC. Three unit vectors, \hat{U} , \hat{E} , \hat{N} , which form a topocentric orthogonal coordinate system and the vector X_T are obtained from the center of the earth to tracker.

The unit vectors are the up, east, and north vectors. These vectors may be written as follows:

$$U_1 = \cos(\text{LAT}) \cos(\text{LON})$$

$$U_2 = \cos(\text{LAT}) \sin(\text{LON})$$

$$U_3 = \sin(\text{LAT})$$

$$E_1 = -\sin(\text{LON})$$

$$E_2 = \cos(\text{LON})$$

$$E_3 = 0$$

$$N_1 = -\sin(\text{LAT}) \cos(\text{LON})$$

$$N_2 = -\sin(\text{LAT}) \sin(\text{LON})$$

$$N_3 = \cos(\text{LAT})$$

$$\text{LON} = \omega(t + t_0) + \text{LON}'$$

$$\text{LON}' = \text{STATION LONGITUDE}$$

$$\omega = \text{EARTH'S ROTATION RATE}$$

$$\omega t_0 = \text{GREENWICH'S LONGITUDE AT EPOCH}$$

$$x_T = \left(\frac{R_E}{C} + H \right) U_1$$

H = ALTITUDE

$$y_T = \left(\frac{R_E}{C} + H \right) U_2$$

$$C = \left[\cos^2(\text{LAT}) + \frac{R_P^2}{R_E^2} \sin^2(\text{LAT}) \right]^{1/2}$$

$$z_T = \left(\frac{R_P^2}{R_E C} + H \right) U_3$$

 R_E = EQUATORIAL RADIUS R_P = POLAR RADIUS

The vehicle's position, \vec{X}_v , and velocity, $\dot{\vec{X}}_v$, are obtained from common storage.

$$\vec{X}_v = \begin{pmatrix} X_v \\ Y_v \\ Z_v \end{pmatrix}$$

$$\dot{\vec{X}}_v = \begin{pmatrix} \dot{X}_v \\ \dot{Y}_v \\ \dot{Z}_v \end{pmatrix}$$

The tracking station velocity is obtained by differentiating \vec{X}_T .

$$\frac{d}{dt} (\vec{X}_T) = \dot{\vec{X}}_T = \begin{pmatrix} \dot{X}_T \\ \dot{Y}_T \\ \dot{Z}_T \end{pmatrix}$$

$$\dot{X}_T = -\omega \left(\frac{R_E}{C} + H \right) \cos(\text{LAT}) \sin(\text{LON})$$

$$\dot{Y}_T = \omega \left(\frac{R_E}{C} + H \right) \cos(\text{LAT}) \cos(\text{LON})$$

$$\dot{Z}_T = 0$$

The vector from the tracking station to vehicle may then be written as

$$\begin{array}{ccccccc} \vec{X} & = & \begin{pmatrix} X_1 \\ X_2 \\ X_3 \end{pmatrix} & = & \vec{X}_V - \vec{X}_T & = & \begin{pmatrix} X_V - X_T \\ Y_V - Y_T \\ Z_V - Z_T \end{pmatrix} \\ 3 \times 1 & & 3 \times 1 & & 3 \times 1 & & 3 \times 1 \end{array}$$

A relationship which will be used in the derivations is

$$\frac{\partial \text{PAR}}{\partial \vec{X}_V} = \frac{\partial \text{PAR}}{\partial \vec{X}}$$

The FORTRAN program names for the above vectors are as follows:

<u>FORTTRAN NAME</u>	<u>DIMENSION</u>	<u>DERIVATION NAME</u>	<u>DIMENSION</u>
U	(3)	U	(3)
E	(3)	E	(3)
EN	(3)	N	(3)
X	(3)	X_V	(3)
RT	(3)	X_T	(3)
Y	(3)	$X = X_V - X_T$	(3)
A	(1)	R_E	(1)
B	(1)	R_P	(1)
RAT	(1)	$ X $	(1)
XD	(3)	$\dot{X} = \dot{X}_V - \dot{X}_T$	(3)

The quantities being measured are the following:

$$R = \text{RANGE} = |\vec{X}| = (\vec{X} \cdot \vec{X})^{1/2}$$

$$\dot{R} = \text{RANGE RATE} = \frac{d}{dt} |\vec{X}| = \frac{\vec{X} \cdot \dot{\vec{X}}}{R}$$

$$AZ = \tan^{-1} \left\{ \frac{\frac{\vec{X} \cdot \hat{E}}{\vec{X} \cdot \hat{N}}}{\frac{\vec{X} \cdot \hat{N}}{\vec{X} \cdot \hat{N}}} \right\}$$

$$EL = \sin^{-1} \frac{(\hat{U} \cdot \vec{X})}{R}$$

Below is a list of partial derivatives which will be used in the application of the chain rule for partial derivatives.

$$\frac{\partial U_1}{\partial LAT} = N_1$$

$$\frac{\partial E_1}{\partial LAT} = 0$$

$$\frac{\partial U_2}{\partial LAT} = N_2$$

$$\frac{\partial E_2}{\partial LAT} = 0$$

$$\frac{\partial U_3}{\partial LAT} = N_3$$

$$\frac{\partial E_e}{\partial LAT} = 0$$

$$\frac{\partial U_1}{\partial LON} = \cos(LAT) \sin(LON)$$

$$\frac{\partial E_1}{\partial LON} = -\cos(LON)$$

$$\frac{\partial U_2}{\partial LON} = \cos(LAT) \cos(LON)$$

$$\frac{\partial E_2}{\partial LON} = -\sin(LON)$$

$$\frac{\partial U_3}{\partial LON} = 0$$

$$\frac{\partial E_3}{\partial LON} = 0$$

$$\frac{\partial U_1}{\partial ALT} = 0$$

$$\frac{\partial E_1}{\partial ALT} = 0$$

$$\frac{\partial U_2}{\partial ALT} = 0$$

$$\frac{\partial E_2}{\partial ALT} = 0$$

$$\frac{\partial U_3}{\partial ALT} = 0$$

$$\frac{\partial E_3}{\partial ALT} = 0$$

$$\frac{\partial N_1}{\partial LAT} = -U_1$$

$$\frac{\partial N_2}{\partial LAT} = -U_2$$

$$\frac{\partial N_3}{\partial LAT} = -U_3$$

$$\frac{\partial N_1}{\partial LON} = \sin(LAT) \sin(LON)$$

$$\frac{\partial N_2}{\partial LON} = -\sin(LAT) \cos(LON)$$

$$\frac{\partial N_3}{\partial LON} = 0$$

$$\frac{\partial N_1}{\partial ALT} = 0$$

$$\frac{\partial N_2}{\partial ALT} = 0$$

$$\frac{\partial N_3}{\partial ALT} = 0$$

$$\frac{\partial U_1}{\partial t} = -\omega \sin(LON) \cos(LAT)$$

$$\frac{\partial U_2}{\partial t} = \omega \cos(LON) \cos(LAT)$$

$$\frac{\partial U_3}{\partial t} = 0$$

$$\frac{\partial E_1}{\partial t} = -\omega \cos(LON)$$

$$\frac{\partial E_2}{\partial t} = -\omega \sin(LON)$$

$$\frac{\partial E_3}{\partial t} = 0$$

$$\frac{\partial N_1}{\partial t} = \omega \sin(LAT) \sin(LON)$$

$$\frac{\partial N_2}{\partial t} = -\omega \sin(LAT) \cos(LON)$$

$$\frac{\partial N_3}{\partial t} = 0$$

FORTTRAN 3x3 matrix called DRT

$$DRT = \begin{pmatrix} \frac{\partial X_1}{\partial LAT} & \frac{\partial X_1}{\partial LON} & \frac{\partial X_1}{\partial ALT} \\ \frac{\partial X_2}{\partial LAT} & \frac{\partial X_2}{\partial LON} & \frac{\partial X_2}{\partial ALT} \\ \frac{\partial X_3}{\partial LAT} & \frac{\partial X_3}{\partial LON} & \frac{\partial X_3}{\partial ALT} \end{pmatrix}$$

3x3 3x3

$$DRT(1,1) = - \frac{\partial x_T}{\partial LAT} = \left(\frac{R_E}{C} + H \right) \sin(LAT) \cos(LON) + U_1 \frac{R_E}{C^2} \frac{\partial C}{\partial LAT}$$

$$\frac{\partial C}{\partial LAT} = \frac{\sin(LAT) \cos(LAT)}{C} \left(1 - \frac{R_P^2}{R_E^2} \right)$$

$$DRT(2,1) = - \frac{\partial y_T}{\partial LAT} = U_2 \frac{R_E}{C^2} \frac{\partial C}{\partial LAT} + \left(\frac{R_E}{C} + H \right) \sin(LAT) \sin(LON)$$

$$DRT(3,1) = - \frac{\partial z_T}{\partial LAT} = - \left(\frac{R_P^2}{R_E C} + H \right) \cos(LAT) + U_3 \frac{R_P^2}{R_E C^2} \frac{\partial C}{\partial LAT}$$

$$DRT(1,2) = - \frac{\partial x_T}{\partial LON} = -E_1 \left(\frac{R_E}{C} + H \right) \cos(LAT)$$

$$DRT(2,2) = - \frac{\partial y_T}{\partial LON} = -E_2 \left(\frac{R_E}{C} + H \right) \cos(LAT)$$

$$DRT(3,2) = 0$$

$$DRT(1,3) = -U_1$$

$$DRT(2,3) = -U_2$$

$$DRT(3,3) = -U_3$$

$$\frac{\partial \dot{x}_1}{\partial LAT} = - \frac{\partial \dot{x}_T}{\partial LAT} = -\omega \left(\frac{R_E}{C} + H \right) \sin(LAT) \sin(LON)$$

$$\frac{\partial \dot{x}_2}{\partial LAT} = - \frac{\partial \dot{y}_T}{\partial LAT} = \omega \left(\frac{R_E}{C} + H \right) \sin(LAT) \cos(LON)$$

$$\frac{\partial \dot{x}_3}{\partial LAT} = - \frac{\partial \dot{z}_T}{\partial LAT} = 0$$

$$\frac{\partial \dot{x}_1}{\partial \text{LON}} = - \frac{\partial \dot{x}_T}{\partial \text{LON}} = \omega \left(\frac{R_E}{C} + H \right) \cos(\text{LAT}) \cos(\text{LON})$$

$$\frac{\partial \dot{x}_2}{\partial \text{LON}} = - \frac{\partial \dot{y}_T}{\partial \text{LON}} = \omega \left(\frac{R_E}{C} + H \right) \cos(\text{LAT}) \sin(\text{LON})$$

$$\frac{\partial \dot{x}_3}{\partial \text{LON}} = - \frac{\partial \dot{z}_T}{\partial \text{LON}} = 0$$

$$\frac{\partial \dot{x}_1}{\partial \text{ALT}} = - \frac{\partial \dot{x}_T}{\partial \text{ALT}} = \omega \cos(\text{LAT}) \sin(\text{LON})$$

$$\frac{\partial \dot{x}_2}{\partial \text{ALT}} = - \frac{\partial \dot{y}_T}{\partial \text{ALT}} = -\omega \cos(\text{LAT}) \cos(\text{LON})$$

$$\frac{\partial \dot{x}_3}{\partial \text{ALT}} = - \frac{\partial \dot{z}_T}{\partial \text{ALT}} = 0$$

- A. The following is a derivation of the partials relating the types of measurements and the vehicle state. In the program, these partials are used as a row vector. The FORTRAN name of the vector is H. H may be written as follows:

$$H = \left(\frac{\partial \text{MEAS}}{\partial X_V}; \frac{\partial \text{MEAS}}{\partial Y_V}; \frac{\partial \text{MEAS}}{\partial Z_V}; \frac{\partial \text{MEAS}}{\partial \dot{X}_V}; \frac{\partial \text{MEAS}}{\partial \dot{Y}_V}; \frac{\partial \text{MEAS}}{\partial \dot{Z}_V} \right)$$

1x6

1x6

- (1) Derivation of partials for range measurement

$$R = (\vec{X} \cdot \vec{X})^{1/2}$$

$$H_R = \left(\frac{\partial R}{\partial X_V}; \frac{\partial R}{\partial Y_V} \right) = \left(\frac{X_1}{R}; \frac{X_2}{R}; \frac{X_3}{R}; 0; 0; 0 \right)$$

1x6

1x6

1x6

(2) Derivation of partials for range rate measurement.

$$\dot{R} = \frac{\vec{X} \cdot \dot{\vec{X}}}{R}$$

$$H_{RR} = \left(\frac{\partial \dot{R}}{\partial \dot{X}_V}; \frac{\partial \dot{R}}{\partial \dot{X}_V} \right) = \left(\frac{\dot{X}_1}{R} - \frac{\dot{R}}{R^2} (X_1); \frac{\dot{X}_2}{R} - \frac{\dot{R}}{R^2} (X_2); \frac{\dot{X}_3}{R} - \frac{\dot{R}}{R^2} (X_3); \frac{X_1}{R}; \frac{X_2}{R}; \frac{X_3}{R} \right)$$

(3) Derivation of partials for azimuth measurement.

$$AZ = \tan^{-1} \left(\frac{\vec{X} \cdot \hat{E}}{\vec{X} \cdot \hat{N}} \right) \equiv \tan^{-1} \gamma$$

$$\frac{\partial AZ}{\partial PAR} = [1 + \gamma^2]^{-1} \frac{\partial \gamma}{\partial PAR}$$

$$[1 + \gamma^2]^{-1} = \frac{(\vec{X} \cdot \hat{N})^2}{S^2} \quad S^2 = (\vec{X} \cdot \hat{E})^2 + (\vec{X} \cdot \hat{N})^2$$

$$H_{AZ} = \left(\frac{\partial AZ}{\partial \dot{X}_V}; \frac{\partial AZ}{\partial \dot{X}_V} \right) = \left(\frac{E_1 (\hat{N} \cdot \vec{X})}{S^2} - \frac{\hat{E} \cdot \vec{X} (N_1)}{S^2}; \frac{E_2 (\hat{N} \cdot \vec{X})}{S^2} - \frac{\hat{E} \cdot \vec{X} (N_2)}{S^2}; \frac{E_3 (\hat{N} \cdot \vec{X})}{S^2} - \frac{\hat{E} \cdot \vec{X} (N_3)}{S^2}; 0; 0; 0 \right)$$

(4) Derivation of partials for elevation measurement.

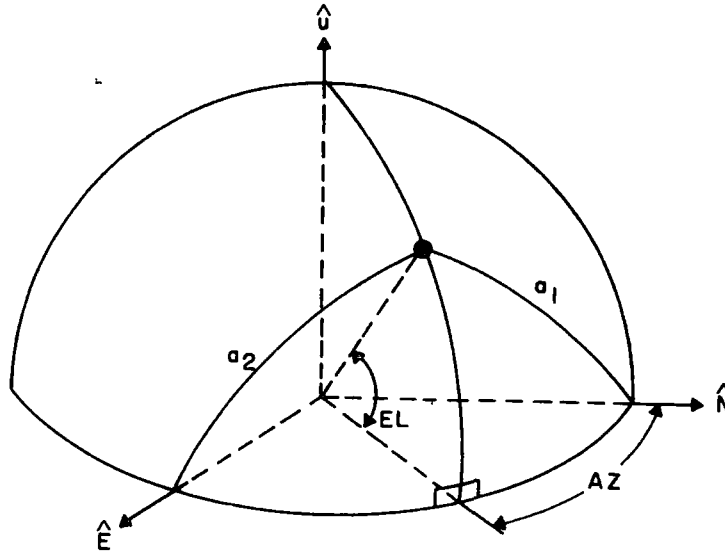
$$EL = \sin^{-1} \left(\frac{\hat{U} \cdot \vec{X}}{R} \right) \equiv \sin^{-1} \gamma$$

$$\frac{\partial EL}{\partial PAR} = [1 - \gamma^2]^{-1/2} \frac{\partial \gamma}{\partial PAR}$$

$$(1 - \gamma^2)^{-1/2} = \frac{R}{S}$$

$$H_{EL} = \left(\frac{\partial EL}{\partial \hat{X}} ; \frac{\partial EL}{\partial \hat{X}} \right) = \left(\frac{U_1}{S} - \frac{(\hat{U} \cdot \hat{X})}{R^2 S} x_1 ; \frac{U_2}{S} - \frac{(\hat{U} \cdot \hat{X})}{R^2 S} x_2 ; \right. \\ \left. \frac{U_3}{S} - \frac{(\hat{U} \cdot \hat{X})}{R^2 S} ; 0 ; 0 ; 0 \right)$$

- (5) Derivation of partials for direction cosines. The partials for the l and m direction cosines are obtained by combining the azimuth and elevation partials as follows:



$$m = \cos(a_1) = \cos AZ \cos EL$$

$$l = \cos(a_2) = \sin AZ \cos EL$$

$$\frac{\partial m}{\partial PAR} = - \cos AZ \sin EL \frac{\partial EL}{\partial PAR} - \sin AZ \cos EL \frac{\partial AZ}{\partial PAR}$$

$$\frac{\partial l}{\partial PAR} = - \sin AZ \sin EL \frac{\partial EL}{\partial PAR} + \cos AZ \cos EL \frac{\partial AZ}{\partial PAR}$$

$$H_m = \begin{pmatrix} \frac{\partial m}{\partial X} & \frac{\partial m}{\partial Y} \end{pmatrix} = \begin{pmatrix} -\cos AZ & \sin EL & -\sin AZ & \cos EL \end{pmatrix} \begin{pmatrix} H_{AZ} \\ H_{EL} \end{pmatrix}$$

1x6 1x6 1x2 2x6

$$H_\ell = \begin{pmatrix} \frac{\partial \ell}{\partial X} & \frac{\partial \ell}{\partial Y} \end{pmatrix} = \begin{pmatrix} -\sin AZ & \sin EL & \cos AZ & \cos EL \end{pmatrix} \begin{pmatrix} H_{AZ} \\ H_{EL} \end{pmatrix}$$

1x6 1x6 1x2 2x6

- B. In order to include errors in the measurements being made due to station location errors and time bias, the partials of the measurements with respect to latitude, longitude, altitude, and time are required. In the program, the station location partials are used as a row vector with FORTRAN name SPART. SPART may be written as follows:

$$SPART = \left(\frac{\partial MEAS}{\partial LAT} ; \frac{\partial MEAS}{\partial LON} ; \frac{\partial MEAS}{\partial ALT} \right)$$

- (1) Derivations of range measurement error partials.

$$\frac{\partial R}{\partial LAT} = \sum_{i=1}^3 \frac{\partial R}{\partial X_i} \frac{\partial X_i}{\partial LAT}$$

$$\frac{\partial R}{\partial LAT} = \sum_{i=1}^3 H_R(1,i) DRT(i,1)$$

Similarly

$$\frac{\partial R}{\partial LON} = \sum_{i=1}^3 H_R(1,i) DRT(i,2)$$

$$\frac{\partial R}{\partial ALT} = \sum_{i=1}^3 H_R(1, i) DRT(1, 3)$$

$$SPART_R = \left(\frac{\partial R}{\partial LAT}; \frac{\partial R}{\partial LON}; \frac{\partial R}{\partial ALT} \right)$$

(2) Derivation of range rate measurement error partials.

$$\frac{\partial \dot{R}}{\partial LAT} = \sum_{i=1}^3 \frac{\partial \dot{R}}{\partial X_i} \frac{\partial X_i}{\partial LAT} + \frac{\partial \dot{R}}{\partial \dot{X}_i} \frac{\partial \dot{X}_i}{\partial LAT}$$

$$\frac{\partial \dot{R}}{\partial LAT} = \sum_{i=1}^3 H_{RR}(1, i) DRT(1, 1) + H_{RR}(1, i+3) \frac{\partial \dot{X}_i}{\partial LAT}$$

Similarly

$$\frac{\partial \dot{R}}{\partial LON} = \sum_{i=1}^3 H_{RR}(1, i) DRT(1, 2) + H_{RR}(1, i+3) \frac{\partial \dot{X}_i}{\partial LON}$$

$$\frac{\partial \dot{R}}{\partial ALT} = \sum_{i=1}^3 H_{RR}(1, i) DRT(1, 3) + H_{RR}(1, i+3) \frac{\partial \dot{X}_i}{\partial ALT}$$

$$SPART_{RR} = \left(\frac{\partial \dot{R}}{\partial LAT}; \frac{\partial \dot{R}}{\partial LON}; \frac{\partial \dot{R}}{\partial ALT} \right)$$

(3) Derivation of azimuth measurement error partials.

$$\frac{\partial AZ}{\partial LAT} = \sum_{i=1}^3 \frac{\partial AZ}{\partial X_i} \frac{\partial X_i}{\partial LAT} + \frac{\partial AZ}{\partial E_i} \frac{\partial E_i}{\partial LAT} + \frac{\partial AZ}{\partial N_i} \frac{\partial N_i}{\partial LAT}$$

(=0)

$$\frac{\partial AZ}{\partial N_i} = - \frac{X_i (\vec{X} \cdot \hat{E})}{S^2} \quad i = 1, 2, 3$$

$$\frac{\partial AZ}{\partial LAT} = \sum_{i=1}^3 H_{AZ}(1,i) DRT(i,1) - \frac{X_i(\vec{X} \cdot \hat{E})}{S^2} \frac{\partial N_i}{\partial LAT}$$

$$\frac{\partial AZ}{\partial LON} = \sum_{i=1}^3 \frac{\partial AZ}{\partial X_i} \frac{\partial X_i}{\partial LON} + \frac{\partial AZ}{\partial E_i} \frac{\partial E_i}{\partial LON} + \frac{\partial AZ}{\partial N_i} \frac{\partial N_i}{\partial LON}$$

$$\frac{\partial AZ}{\partial E_i} = \frac{X_i(\vec{X} \cdot \hat{N})}{S^2} \quad i = 1, 2, 3$$

$$\frac{\partial AZ}{\partial LON} = \sum_{i=1}^3 H_{AZ}(1,i) DRT(i,2) + \frac{X_i}{S^2} (\vec{X} \cdot \hat{N}) \frac{\partial E_i}{\partial LON} - \frac{X_i}{S^2} (\vec{X} \cdot \hat{E}) \frac{\partial N_i}{\partial LON}$$

$$\frac{\partial AZ}{\partial ALT} = \sum_{i=1}^3 \frac{\partial AZ}{\partial X_i} \frac{\partial X_i}{\partial ALT} + \frac{\partial AZ}{\partial E_i} \frac{\partial E_i}{\partial ALT} + \frac{\partial AZ}{\partial N_i} \frac{\partial N_i}{\partial ALT}$$

(=0) (=0)

$$\frac{\partial AZ}{\partial ALT} = \sum_{i=1}^3 H_{AZ}(1,i) DRT(i,3)$$

$$SPART_{AZ} = \left(\frac{\partial AZ}{\partial LAT} ; \frac{\partial AZ}{\partial LON} ; \frac{\partial AZ}{\partial ALT} \right)$$

(4) Derivation of elevation measurement error partials.

$$\frac{\partial EL}{\partial LAT} = \sum_{i=1}^3 \frac{\partial EL}{\partial X_i} \frac{\partial X_i}{\partial LAT} + \frac{\partial EL}{\partial U_i} \frac{\partial U_i}{\partial LAT}$$

$$\frac{\partial EL}{\partial U_i} = \frac{X_i}{S} \quad i = 1, 2, 3$$

$$\frac{\partial EL}{\partial LAT} = \sum_{i=1}^3 H_{EL}(1,i) DRT(i,1) + \frac{x_i}{s} \frac{\partial U_i}{\partial LAT}$$

$$\frac{\partial EL}{\partial LON} = \sum_{i=1}^3 \frac{\partial EL}{\partial X_i} \frac{\partial X_i}{\partial LON} + \frac{\partial EL}{\partial U_i} \frac{\partial U_i}{\partial LON}$$

$$\frac{\partial EL}{\partial LON} = \sum_{i=1}^3 H_{EL}(1,i) DRT(i,2) + \frac{x_i}{s} \frac{\partial U_i}{\partial LON}$$

$$\frac{\partial EL}{\partial ALT} = \sum_{i=1}^3 \frac{\partial EL}{\partial X_i} \frac{\partial X_i}{\partial ALT} + \frac{\partial EL}{\partial U_i} \frac{\partial U_i}{\partial ALT} \quad (=0)$$

$$\frac{\partial EL}{\partial ALT} = \sum_{i=1}^3 H_{ALT}(1,i) DRT(i,3)$$

$$SPART_{EL} = \left(\frac{\partial EL}{\partial LAT} ; \frac{\partial EL}{\partial LON} ; \frac{\partial EL}{\partial ALT} \right)$$

(5) Derivation of direction cosine measurement error partials.

$$SPART_m = \begin{pmatrix} -\cos AZ \sin EL & -\sin AZ \cos EL \end{pmatrix} \begin{pmatrix} SPART_{AZ} \\ SPART_{EL} \end{pmatrix}$$

1x3

1x2

2x3

$$SPART_\rho = \begin{pmatrix} -\sin AZ \sin EL & \cos AZ \cos EL \end{pmatrix} \begin{pmatrix} SPART_{AZ} \\ SPART_{EL} \end{pmatrix}$$

1x3

1x2

2x3

- (6) Derivations of time derivatives of measurement quantities to permit inclusion of time bias errors.

$$\frac{\partial R}{\partial t} = \dot{R} = \frac{\vec{X} \cdot \dot{\vec{X}}}{R}$$

$$\frac{\partial AZ}{\partial t} = \sum_{i=1}^3 \frac{\partial AZ}{\partial X_i} \frac{\partial X_i}{\partial t} + \frac{\partial AZ}{\partial E_i} \frac{\partial E_i}{\partial t} + \frac{\partial AZ}{\partial N_i} \frac{\partial N_i}{\partial t}$$

$$\frac{\partial AZ}{\partial t} = \sum_{i=1}^3 H_{AZ}(1,i) \dot{X}_i + \frac{\partial AZ}{\partial E_i} \dot{E}_i + \frac{\partial AZ}{\partial N_i} \dot{N}_i$$

$$\frac{\partial EL}{\partial t} = \sum_{i=1}^3 H_{EL}(1,i) \dot{X}_i + \frac{\partial EL}{\partial E_i} \dot{E}_i + \frac{\partial EL}{\partial N_i} \dot{N}_i$$

- (7) The time partials for the ℓ and m direction cosines are obtained by the following combination of azimuth and elevation partials.

$$\frac{\partial m}{\partial t} = \begin{pmatrix} -\cos AZ & \sin EL & -\sin AZ & \cos EL \end{pmatrix} \begin{pmatrix} \frac{\partial AZ}{\partial t} \\ \frac{\partial EL}{\partial t} \end{pmatrix}$$

1x1 1x2 2x1

$$\frac{\partial \ell}{\partial t} = \begin{pmatrix} -\sin AZ & \sin EL & \cos AZ & \cos EL \end{pmatrix} \begin{pmatrix} \frac{\partial AZ}{\partial t} \\ \frac{\partial EL}{\partial t} \end{pmatrix}$$

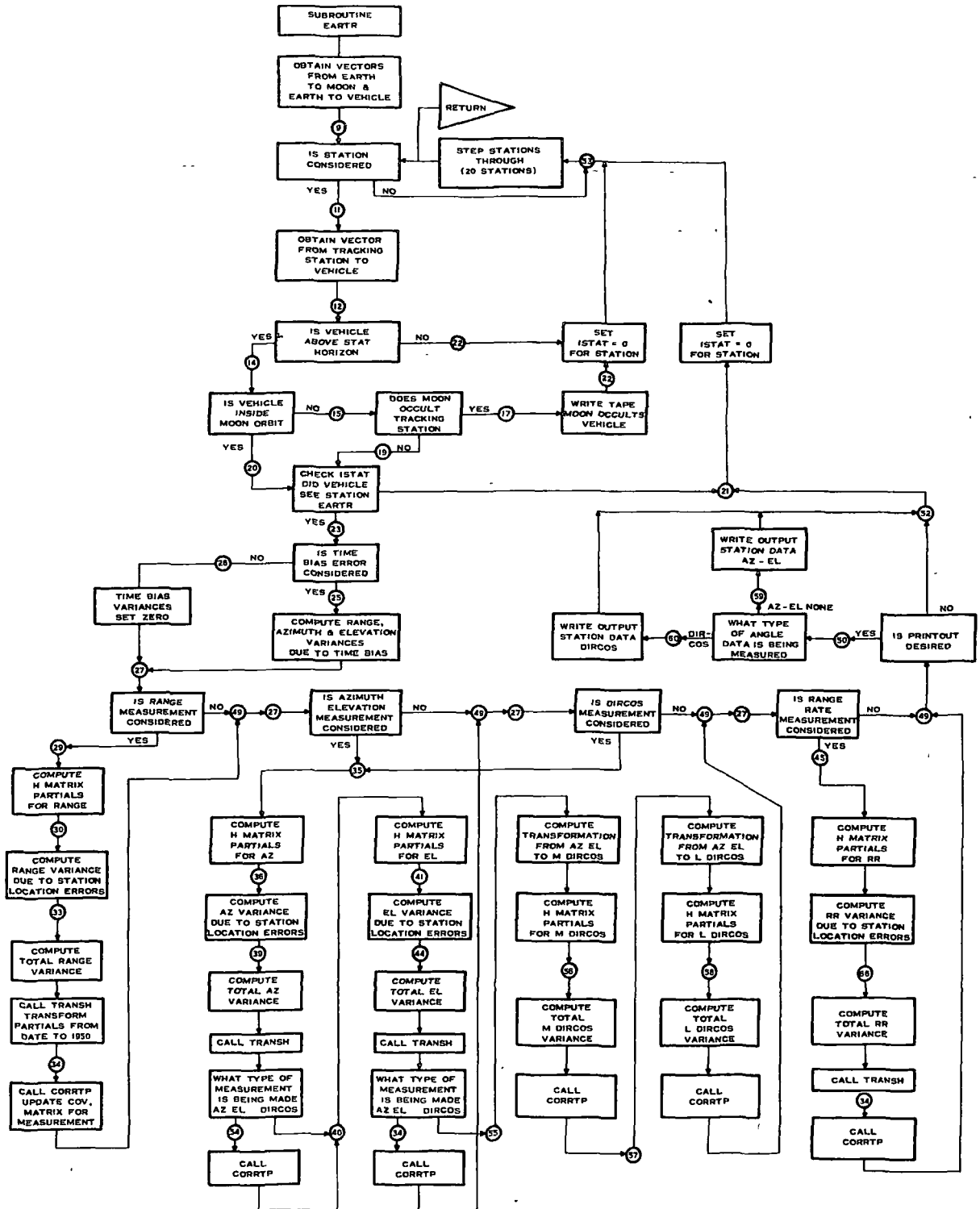
1x1 1x2 2x1

The errors in the measurements are computed in the following manner for station location errors and time bias.

$$\begin{array}{rcl}
 \text{QQS} & = & \left(\begin{array}{c} \text{SPART} \\ \text{MEAS} \end{array} \right)^2 \begin{pmatrix} \sigma^2_{\text{LAT}} \\ \sigma^2_{\text{LON}} \\ \sigma^2_{\text{ALT}} \end{pmatrix} & \text{Station Location Error} \\
 1 \times 1 & & 1 \times 3 & 3 \times 1
 \end{array}$$

$$\text{QQDOT} = \left\{ \frac{\partial \text{MEAS}}{\partial t} \cdot \sigma_{\text{TIME}} \right\}^2 \quad \text{Time Bias Error}$$

The computation of the H matrices and the measurement errors are the primary computations in EARTR. These quantities are input to subroutine CORRTP which does the weighting of the measurement and updating of the state covariance matrix.



EARTR

*	LABEL	EART
*	SYMBOL TABLE	EART
	SUBROUTINE: EARTR	EART0000
C	SUBROUTINE: EARTR UPDATES THE COVARIANCE MATRIX USED	EART0005
C	IN EARTH TRACKING	EART0007
	COMMON T,S,C,IC	EART0010
	DIMENSION PO(22),VE(22),XED(3),VED(3),AN(3,3),RBOP(6),POSM(3),	EART0020
	1VOSM(3),POVRM(3),EM(3,3),EN(3),U(3),E(3),RT(3),Y(3),TD(3),	EART0030
	2ISTAT(20),H(6),X(3),VX(3),T(1360),S(1000),C(1000),IC(1),ISA(20),	EART0040
	3IMSTA(4,20),P(6,6),SPART(3),DRT(3,3),XD(3),SPART2(3),HA(6),HCOS(6)	EART0050
	EQUIVALENCE (T,TDUM),(S,SDUM),(C,CDUM)	EART0060
	1,(IC(3),NOR),(C(13),TW),(C(14),TF),(C(62),PO),(C(84),VE)	EART0070
	2,(C(112),RBOP),(C(138),AN),(C(120),EM),(C(15),X),(C(18),VX),	EART0080
	3(S(70),DTS),(S(71),STD),(S(72),DR),(S(73),RD),(IC(194),ISTAT)	EART0090
	4,(IC(10),ISA),(IC(30),IMSTA),(IC(214),NOUT),(C(652),P)	EART0100
	5,(C(649),TSECP),(C(30),TSEC),(S(10),W),(S(14),A),(S(15),B)	EART0110
	CALL SETN(NIN,NUTS)	EART0115
	NB=NOR-1	EART0120
	DIS=1.E10	EART0130
	CALL INTR1 (TW,TF,NB,PO,1,VE,DIS)	EART0140
	CALL MATRX(AN,X,XED,3,3,1,0)	EART0150
	CALL MATRX(AN,VX,VED,3,3,1,0)	EART0160
C	XED=VECTOR FROM NB BODY TO VEHICLE, VED=VELOCITY EQUATOR OF DATE	EART0170
	MS=1	EART0180
	IF(RBOP(1)-330000.)10,2,2	EART0190
C	RBOP= MAGNITUDE OF VECTOR FROM VEHICLE TO BODY	EART0200
	2 CONTINUE	EART0210
	IF (NOR=1)3,5,3	EART0220
	3 CONTINUE	EART0230
C	HERE IF OUTSIDE MOON AND NOT EARTH REFERENCED	EART0240
	DO 4 I=1,3	EART0250
	POSM(I)=0.	EART0260
	VOSM(I)=0.	EART0270
	DO 4 J=1,3	EART0280
	K=23-J	EART0290
	XED(I)=XED(I)-AN(I,J)*PO(K)	EART0300
	VED(I)=VED(I)-AN(I,J)*VE(K)	EART0310
	L=20-J	EART0320
	POSM(I)=POSM(I)+AN(I,J)*(PO(L)-PO(K))	EART0330
	VOSM(I)=VOSM(I)+AN(I,J)*(VE(L)-VE(K))	EART0340
C	POSM IS A VECTOR FROM EARTH TO MOON	EART0350
	4 CONTINUE	EART0360
	GO TO 7	EART0370
	5 CONTINUE	EART0380
C	HERE IF OUTSIDE MOON AND EARTH REFERENCED	EART0390
	DO 6 I=1,3	EART0400
	POSM(I)=0	EART0410
	VOSM(I)=0	EART0420
	DO 6 J=1,3	EART0430
	K=20-J	EART0440
	POSM(I)=POSM(I)+AN(I,J)*PO(K)	EART0450

EARTR (Cont'd)

C	TO DETERMINE IF MOON OCCULTS VEHICLE	EART093
	DOTTD=DOT(POVRM,TD)	EART094
	IF(DOTTD)19,19,16	EART095
16	CONTINUE	EART096
	IF(DOTTD=(SQRTF(RADM**2-1739,**2))/RADM)19,19,17	EART097
17	WRITE OUTPUT TAPE (NUTS,18,SNAME	EART098
18	FORMAT (27HMOON OCCULTS VEHICLE FROM,A6,8H TRACKER)	EART099
	GO TO 22	EART100
19	CONTINUE	EART101
20	CONTINUE	EART102
	SEC=DOT(TD,EN)	EART103
	CE=DOT(TD,E)	EART104
	AZMTH =ARKTNS(360,SEC,CE)	EART105
	IF(ISTAT(III))21,21,23	EART106
C	ISTAT IS SET ONE IF THE STATION SAW VEHICLE ON PREVIOUS TIME.	EART106
C	THROUGH MATSUB	EART1066
C	ZERO IF IT COULD NOT SEE IT	EART1070
21	CONTINUE	EART108
C	HERE IF STATION SEES THE VEHICLE.	EART1090
	ISTAT(III)=1	EART1100
	GO TO 53	EART111
22	CONTINUE	EART112
	ISTAT(III)=0	EART1130
C	VEHICLE WAS NOT OBSERVED BY STATION	EART1140
	GO TO 53	EART115
23	CONTINUE	EART1160
	OBNO=INTF((TSEC-TSECP)/S(NN+13))	EART1170
C	OBNO IS THE NUMBER OF OBSERVATIONS SINCE LAST TIME IN MATSUB.	EART118
	XTU=DOT(Y,U)	EART1190
	XTE=DOT(Y,E)	EART1200
	XTN=DOT(Y,EN)	EART121
	TPD2=XTE**2+XTN**2	EART122
	TPD=SQRTF(TPD2)	EART1230
	ALLY=XTN/TPD2	EART1240
	GAM=XTU*XTE	EART1250
	BET=XTE/TPD2	EART1260
	DEL=XTU*XTN	EART1270
	D=1./RAT**2/TPD	EART128
	CA=AC/A	EART129
	BA=B*B/(A*A)	EART1300
	GG=CA*(1.-BA)*SL*CL*CA*CA	EART131
	DRT(1,1)=A*GG*U(1)+(AC+AL)*EN(1)	EART132
	DRT(2,1)=A*GG*U(2)+(AC+AL)*EN(2)	EART1330
	DRT(3,1)=(B*B/A)*GG*U(3)+BA*(AC+AL)*EN(3)	EART1340
	DRT(1,2)=(AC+AL)*CL*E(1)	EART135
	DRT(2,2)=(AC+AL)*CL*E(2)	EART1360
	DRT(3,2)=0.0	EART1370
	DO 24 I=1,3	EART138
	DRT(I,3)=U(I)	EART139
C	THE ABOVE QUANTITIES ARE USED ONLY FOR H MATRIX CALCULATIONS	EART1400
24	CONTINUE	EART141

EARTR (Cont'd)

```

AA=S(10)*CL*(AC+AL)
XD(1)=VED(1)-AA*E(1)
XD(2)=VED(2)-AA*E(2)
XD(3)=VED(3)
XDTU=DOT(XD,U)
XDTE=DOT(XD,E)
XDTE=DOT(XD,E)
XDTE=DOT(XD,EN)
RDOT=DOT(XD,Y)/RAT
RDOT=RANGE RATE
ADOT=W*SL-W*CL*ALLY*XTU+ALLY*XDTE-BET*XDTN
ADOT=AZIMUTH RATE
EDOT=(1./TPD)*(W*CL*XTE+XDTU-RDOT*XTU/RAT)
EDOT=ELEVATION RATE
IF(S(NN+14))26,26,25
25 CONTINUE
RDOT2=RDOT*RDOT
QQRDOT=RDOT2*S(NN+14)
QQRDOT=RANGE VARIANCE DUE TO TIME BIAS
ADOT2=ADOT*ADOT
QQADOT=ADOT2*S(NN+14)
QQADOT=AZIMUTH VARIANCE DUE TO TIME BIAS
EDOT2=EDOT*EDOT
QQEDOT=EDOT2*S(NN+14)
QQEDOT=ELEVATION VARIANCE DUE TO TIME BIAS
GO TO 27
26 CONTINUE
QQRDOT=0.
QQADOT=0.
QQEDOT=0.
27 CONTINUE
DO 49 II=1,4
IF (IMSTA(II,III)) 49,49,28
28 CONTINUE
II=II
GO TO (29,35,35,45),II
II DESIGNATES TYPE OF MEASUREMENT 1=RANGE 2=AZ+EL 3=DIRCOS
4=RANGE RATE
29 CONTINUE
CALCULATES H MATRIX FOR RANGE
DO 30 J=1,3
H(J)=TD(J)
30 CONTINUE
DO 32 I=1,3
SPART(I)=0.
SPART=PARTIALS OF RANGE WRT STATION LOCATION
DO 31 K=1,3
SPART(I)=SPART(I)+H(K)*DRT(K,I)
31 CONTINUE
SPART2(I)=SPART(I)*SPART(I)
32 CONTINUE
QQS=0.

```

EART142
EART143
EART144
EART145
EART146
EART147
EART148
EART149
EART150
EART151
EART152
EART153
EART154
EART155
EART156
EART157
EART158
EART159
EART160
EART161
EART162
EART163
EART164
EART165
EART166
EART167
EART168
EART169
EART170
EART171
EART172
EART173
EART174
EART175
EART176
EART176
EART176
EART177
EART178
EART179
EART180
EART181
EART182
EART183
EART184
EART185
EART186
EART187
EART188
EART189
EART190

EARTR (Cont'd)

	DO 33 I=1,3	EART1910
C	QQS=RANGE VARIANCE DUE TO STATION LOCATION ERRORS	EART1920
	KL=NN+3+I	EART1930
	QQS=QQS+SPART2(I)*S(KL)	EART1940
33	CONTINUE	EART1950
	QQ=S(NN)/OBNO+RAT*S(425)*RAT+QQS+QQRDOT	EART1960
C	QQ=TOTAL RANGE VARIANCE	EART1970
	CALL TRANSH(H,1)	EART1980
C	TRANSH TRANSFORMS H MATRIX FROM EQUINOX OF DATE TO 1950	EART1990
34	CONTINUE	EART2000
	CALL CORRTP (QQ,H,P)	EART2010
C	CORRTP UPDATES COVARIANCE MATRIX FOR PARTICULAR TYPE	EART2015
C	OF MEASUREMENT	EART2016
	GO TO 49	EART2020
35	CONTINUE	EART2030
C	THE FOLLOWING CALCULATIONS GIVE H MATRIX FOR AZIMUTH	EART2040
	DO 36 J=1,3	EART2050
	HA(J)=ALLY*E(J)-BET*EN(J)	EART2060
36	CONTINUE	EART2070
	DO 37 I=1,3	EART2080
	SPART(I)=0.	EART2090
C	SPART=PARTIALS OF AZIMUTH WRT STATION LOCATION	EART2100
	DO 37 K=1,3	EART2110
	SPART(I)=SPART(I)-HA(K)*DRT(K,I)	EART2120
37	CONTINUE	EART2130
	SPART(1)=SPART(1)+BET*XTU	EART2140
	PLUS=BET*SL*XTE-ALLY*(Y(1)+CT+Y(2)*ST)	EART2150
	SPART(2)=SPART(2)+PLUS	EART2160
	DO 38 I=1,3	EART2170
	SPART2(I)=SPART(I)+SPART(I)	EART2180
38	CONTINUE	EART2190
	QQSA=0.	EART2200
	DO 39 I=1,3	EART2210
C	QQSA=AZIMUTH VARIANCE DUE TO STATION LOCATION ERRORS	EART2220
	KL=NN+3+I	EART2230
	QQSA=QQSA+SPART2(I)*S(KL)	EART2240
39	CONTINUE	EART2250
	QQ=S(NN+1)/OBNO+S(NN+7)+QQSA+QQADOT	EART2260
C	QQ=TOTAL AZIMUTH VARIANCE	EART2270
	CALL TRANSH(HA,1)	EART2280
	IF(II=2)54,54,40	EART2290
54	CONTINUE	EART2300
	CALL CORRTP(QQ,HA,P)	EART2310
40	CONTINUE	EART2320
C	THE FOLLOWING CALCULATIONS GIVE H MATRIX FOR ELEVATION	EART2330
	DO 41 J=1,3	EART2340
	H(J)= U(J)/TPD=Y(J)*XTU+D	EART2350
41	CONTINUE	EART2360
	DO 42 I=1,3	EART2370
	SPART(I)=0.	EART2380
C	SPART=PARTIALS OF ELEVATION WRT STATION LOCATION	EART2390

EARTR (Cont'd)

	DO 42 K=1,3	EART240
	SPART(I)=SPART(I)-H(K)*DRT(K,I)	EART241
	42 CONTINUE	EART242
	SPART(1)=SPART(1)+XTN/TPD	EART243
	SPART(2)=SPART(2)+XTE*CL/TPD	EART244
	DO 43 I=1,3	EART245
	SPART2(I)=SPART(I)*SPART(I)	EART246
	43 CONTINUE	EART247
	QQS=0.	EART248
	DO 44 I=1,3	EART249
	QQS=ELEVATION VARIANCE DUE TO STATION LOCATION ERRORS	EART250
	KL=NN+3+I	EART251
	QQS=QQS+SPART2(I)*S(KL)	EART252
	44 CONTINUE	EART253
	QQ=S(NN+2)/OBNO+S(NN+8)*QQS+QQEDOT	EART254
	QQ=TOTAL ELEVATION VARIANCE	EART255
	CALL TRANSH(H,1)	EART256
	IF(II=2)34,34,55	EART257
	55 CONTINUE	EART258
	DIRCOS=DOT(EN,TD)	EART259
	SINANG=SQRTF(1.-DIRCOS**2)	EART260
	TANANG=SINANG/DIRCOS	EART261
	ANGM=ATANF(TANANG)	EART262
	ANGM=ANGM*RD	EART263
	CA=COSF(AZMTH)	EART264
	SA=SINF(AZMTH)	EART265
	SE=SINF(ELEV)	EART266
	CE=COSF(ELEV)	EART267
	C1=-SA*CE	EART268
	C2=-CA*SE	EART269
	ANGMDT=C1*EDOT+C2*ADOT	EART270
	ANGMDT=ANGMDT*RD	EART271
	DO 56 I=1,3	EART272
	HCOS(I)=C1*H(I)+C2*HA(I)	EART273
	56 CONTINUE	EART274
	QQSCOS=C1*QQS+C2*QQSA	EART275
	QQSCOS IS THE VARIANCE IN THE M DIRECTION COSINE DUE TO STATION	EART276
	LOCATION ERRORS	EART277
	QQCDOT=C1*QQEDOT+C2*QQADOT	EART278
	QQ=S(NDUM+1)/OBNO+S(NDUM+2)+QQSCOS+QQCDOT	EART279
	QQ=TOTAL VARIANCE OF M DIRECTION COSINE	EART280
	CALL CORRTP(QQ,HCOS,P)	EART281
	57 CONTINUE	EART282
	DIRCOS=DOT(E,TD)	EART283
	SINANG=SQRTF(1.-DIRCOS**2)	EART284
	TANANG=SINANG/DIRCOS	EART285
	ANGL=ATANF(TANANG)	EART286
	ANGL=ANGL*RD	EART287
	C1=CA*CE	EART288
	C2=-SA*SE	EART289
	ANGLDT=C1*EDOT+C2*ADOT	EART290

EARTR (Cont'd)

	ANGLDT=ANGLDT*RD	EART2910
	DO 58 I=1,3	EART2920
	HCOS(I)=C1*H(I)+C2*HA(I)	EART2930
58	CONTINUE	EART2940
	QQSCOS=C1*QQS+C2*QQSA	EART2950
C	QQSCOS IS THE L DIRECTION COSINE ERROR DUE TO STATION LOCATION	EART2960
C	ERROR	EART2970
	QQCDOT=C1*QQEDOT+C2*QQADOT	EART2980
	QQ=S(NDUM+3)/OBNO+S(NDUM+4)+QQSCOS+QQODOT	EART2990
C	QQ=TOTAL L DIRECTION COSINE VARIANCE	EART3000
	CALL CORRTP(QQ,HCOS,P)	EART3010
	GO TO 49	EART3020
45	CONTINUE	EART3030
C	THE FOLLOWING CALCULATIONS GIVE H MATRIX FOR RANGE RATE	EART3040
47	DO 48 J=1,3	EART3050
	K=J+3	EART3060
	H(K)=TD(J)	EART3070
	H(J)=(1./RAT)*(XD(J)-RDOT*TD(J))	EART3080
48	CONTINUE	EART3090
	CNST=B*B/A+((1./CA)**3)	EART3091
	DO 65 J=1,3	EART3092
	JJ=3*J-2	EART3093
	SPART(J)=-DOT(H,DRT(JJ))	EART3094
65	CONTINUE	EART3095
	SPART(1)=SPART(1)*S(10)*U(3)*(CNST+AL)*XTE/RAT	EART3096
	SPART(2)=SPART(2)-AA*(TD(2)*E(1)-TD(1)*E(2))	EART3097
	SPART(3)=SPART(3)-S(10)*EN(3)*XTE/RAT	EART3098
	QQS=0.	EART3099
	DO 66 I=1,3	EART3100
	KL=NN+3*I	EART3101
	QQS=QQS+(SPART(I)**2)*S(KL)	EART3102
66	CONTINUE	EART3103
	QQ=S(NN+3)/OBNO+QQS	EART3104
	CALL TRANSH(H,2)	EART3110
	GO TO 34	EART3120
49	CONTINUE	EART3130
	NOUT=NOUT	EART3140
	GO TO (52,50),NOUT	EART3150
50	CONTINUE	EART3160
	IF(IMSTA(3,III))59,59,60	EART3170
59	CONTINUE	EART3180
	EDOT=EDOT*RD	EART3190
	ADOT=ADOT*RD	EART3200
	AZMTH =AZMTH*RD	EART3210
	ELEV=ELEV*RD	EART3220
	WRITE OUTPUT TAPE NUTS,51,SNAME,RAT,RDOT,AZMTH,ADOT,ELEV,EDOT	EART3230
51	FORMAT (17H TRACKER STATION ,A6,/4H RNGE15.8,5H RGRE15.8,	EART3240
	15H AZME15.8,5H AZRE15.8,5H ELEE15.8,5H ELRE15.8)	EART3250
	GO TO 52	EART3260
60	CONTINUE	EART3270
	WRITE OUTPUT TAPE NUTS,61,SNAME,RAT,RDOT,ANGL,ANGLDT,ANGM,ANGMDT	EART3280

EARTR (Cont'd)

61 FORMAT (17H TRACKER STATION ,A6,/4H RNGE15.8,5H RGRE15.8,
 15H LCSE15.8,5H LCRE15.8,5H MCSE15.8,5H MCRE15.8)
 52 CONTINUE
 GO TO 21
 53 CONTINUE
 RETURN
 END

EART32
 EART33
 EART33
 EART33
 EART33
 EART33
 EART33
 EART

Page Intentionally Left Blank

Subroutine: ECLIP

Purpose: To replace each of two 3-dimensional vectors by its product with a given 3 x 3 matrix. This subroutine is used for transforming position and velocity vectors.

Calling Sequence:

CALL ECLIP (X, VX, ECL)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I-O	X	3			Xout = (ECL) Xin
I-O	VX	3			VXout = (ECL) VXin
I	ECL	3,3			TRANSFORMATION MATRIX

Common storages used or required:

None

Subroutines required:

None

Functions required:

None

Approximate number of storages required:

ECLIP

WDL-TR2184

```
* LABEL
* SYMBOL TABLE
SUBROUTINE ECLIP(X,VX,ECL)
DIMENSION X(3),VX(3),XP(3),VXP(3),ECL(3,3)
DO 1 I=1,3
XP(I) = 0.
VXP(I) = 0.
DO 1 J=1,3
XP(I) = XP(I) + ECL(I,J)*X(J)
1 VXP(I) = VXP(I) + ECL(I,J)*VX(J)
DO 2 I=1,3
X(I) = XP(I)
2 VX(I) = VXP(I)
RETURN
END
```

ECLP
ECLP
ECLP0000
ECLP0010
ECLP0020
ECLP0030
ECLP0040
ECLP0050
ECLP0060
ECLP0070
ECLP0080
ECLP0090
ECLP0100
ECLP0110
ECLP

ECLIP - 2

Subroutine: ENCKE

Purpose: To perform the calculation of the ENCKE contribution to the acceleration. These are perturbations in acceleration due to deviation from the osculating conic.

Calling Sequence:

CALL ENCKE (U, X, D, AE)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	U	1	μ	Km^3/sec^2	Gravitational constant
I	X	3	X, Y, Z	Km	Position on the conic
I	D	3	X', Y', Z'	Km	Position deviation from the conic
O	AE	3		Km/sec^2	ENCKE acceleration terms

Common storages used or required:

None

Subroutines required:

None

Functions required:

SORT, DOT

Approximate number of storages required:

158 DEC

Equation Being Solved

The perturbation acceleration due to deviation from the reference conic is the following

$$\vec{A}E = \frac{\mu}{R_o^3} (\vec{R} F(Q) - \vec{D})$$

where $\vec{R} = \vec{R}_o + \vec{D}$. The solution, R_o , for the position in the two body orbit is provided by STEPC, and is saved from step to step so that a new R_o is calculated only when the time has changed.

$F(Q) = 1 - (1 + 2Q)^{-3/2}$ is calculated from the series expansion

$$F(Q) = Q \sum_{j=0}^6 a_j Q^j$$

where

$$a_0 = 3$$

$$a_1 = -7.5$$

$$a_2 = 17.5$$

$$a_3 = 39.375$$

$$a_4 = 86.625$$

$$a_5 = 187.6875$$

$$a_6 = 402.1875$$

and

$$Q = \frac{\vec{D} \cdot \left(\vec{R}_o + \frac{\vec{D}}{2} \right)}{R_o^2}$$

Page Intentionally Left Blank

Subroutine: ERP

Purpose: To write on the output tape: EPHEMERIS FAILED DUE TO TAPE REDUNDANCIES, and then to CALL EXIT. Should this message occur, and the tape was actually mounted on the correct unit, try again or try a different copy of the ephemeris tape.

Calling Sequence:

CALL ERP

Input and Output

Common storages used or required:	None
Subroutines required:	SETN, EXIT
Functions required:	
Approximate number of storages required:	

ERP

WDL-TR2184

```
* LABEL  
CEC20GD  
SUBROUTINE ERP  
CALL SETN(NIN,NOUT)  
1 FORMAT(42H EPHEMERIS FAILED DUE TO TAPE REDUNDANCIES)  
WRITE OUTPUT TAPE NOUT,1  
CALL EXIT  
RETURN  
END
```

```
ERPO  
ERPO  
ERP0000  
ERP0010  
ERP0020  
ERP0030  
ERP0040  
ERP0050  
ERPO
```

S-152

ERP-2

Subroutine: ERPT

Purpose: To write on the output tape: EPHEMERIS FAILED LOOKING FOR T = () DAYS SINCE 1950.0, and to call EXIT.

The cause of this condition is either incorrect input or not having the ephemeris tape mounted correctly.

Calling Sequence:

CALL ERPT(T)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	T			days	Time (in days since 1950.0) for which INTR was searching the tape

Common storages used or required: None

Subroutines required: SETN, EXIT

Functions required: None

Approximate number of storages required:

ERPT

WDL-TR2184

```
* LABEL  
CEC20GE  
SUBROUTINE ERPT(T)  
CALL SETN(NIN,NOUT)  
WRITE OUTPUT TAPE NOUT,2,T  
2 FORMAT(33H EPHEMERIS FAILED LOOKING FOR T =,F20.0,  
118H DAYS SINCE 1950,0)  
CALL EXIT  
RETURN  
END
```

ERPT
ERPT
ERPT0000
ERPT0010
ERPT0020
ERPT0030
ERPT0040
ERPT0050
ERPT0060
ERPT

ERPT-2

Subroutine: FINP

Identification

RW FINP - Decimal, Octal, BCD, Variable Data Input
7090 FAP Subroutine
W.J. Stoner, August 24, 1961
Aerospace Corporation

Purpose

To read a set of Hollerith punched data and/or header cards into core with one FORTRAN CALL statement.

To convert the data fields to binary and store in core according to their associated conversion codes.

Restrictions

This routine uses (CSH)S to accomplish the BCD card image read. Tape troubles or other errors from this routine are indicated by the printout of HPR 1,4.

This routine uses (EXE) to print HPR 2,4 in case of errors such as non-Hollerith characters, data out of range, illegal format, subscripts too large for the array previously defined, etc. Upon detection of any error, control is immediately sent to (EXE) and no more cards are processed.

Method

Decimal numbers are converted to binary integers and then scaled to the indicated power of ten.

Octal numbers are converted to binary integers.

Hollerith words are stored directly.

Range: Decimal to floating binary conversion 10^{-38}
 Decimal to fixed binary; 1 to 9 digits*
 Decimal integer to binary integer; 1 to 5 digits
 Octal integer to binary integer; 0 to 235 - 1

*the magnitude of the number depends upon the location of the decimal point.

Usage

Format:

1. The data card format, available on keypunch form M-1, consists of four subfields containing the conversion code, location, number, and exponent, respectively.

FINP-1

S-155

	Data Field	Data Field	Data Field	Data Field
Subfield	1	2	3	4
Conversion Code	1	19	37	55
Location	2-6	20-24	38-42	56-60
Value	7-16	25-34	43-52	61-70
Exponent	17-18	35-36	53-54	71-72

where conversion code is one of the alphabetic characters defined below which specifies the type of conversion to be used on the value field, the location specifies the cell into which the converted value field is to be stored, the value subfield contains the data to be converted, and the exponent contains the power of ten by which floating data is to be scaled, or the location of the binary point of fixed point data.

- The header card format consists of a conversion code in column 1, a sequence number in columns 2-6, and any Hollerith information in columns 7-72.

Decimal Points:

Decimal points may be placed anywhere in the value field except that they may not occur in the same column as a minus sign (11 punch) since this results in a non-Hollerith character. If the decimal point would normally appear at the right of the number punched in the value field, then it is optional.

Minus Signs:

Minus signs are 11 punches over any digit of the field. If all of the available columns of the field are not used, minus signs may be punched as the left character of the field.

Values:

Values must always be written to the extreme left of a field. It is not necessary that the entire field be filled as the first blank denotes the end of value. Superfluous low order zeros should be omitted as they increase conversion error.

The only exception to partial fields is BCK data where the entire field, including blanks, is stored.

Location:

The location may be specified by either absolute octal, a variable or array name, or the element subscripts in a one or two dimensional array. If the locations contain five digits, it is interpreted as octal. All five columns must be punched for octal locations.

If the location contains at least one non-numeric character, it is interpreted as a variable or array name which must appear exactly as given in the CALL statement (see Calling Sequence below). The contents of the number and exponent fields, if they are numeric data, are stored in the cell for the variable or the first cell for the array. This location then becomes the origin for all subscript locations following until another variable or array name is encountered. Caution must be taken to load an array name prior to subscript locations.

If the location contains four or fewer digits, it is interpreted as a subscript except for conversion code H explained below. Single dimension array subscripts must be left-justified with leading zeros optional. Two dimension array subscripts must be denoted by two subfields of two columns each containing i and j, respectively. The i and j subfields must be separated by a comma and must contain two-digit integers.

If the location is left blank, then the location counter within the routine is decreased by 1 and the associated number is stored in the cell immediately preceding the cell where the last number was stored. Thus, an entire array may be read in by specifying the initial location only.

Conversion Codes:

Blank: Floating decimal

The number in the value field times the power of ten in the exponent field is converted to floating binary. Checks are made for overflow and format errors.

F: Fixed decimal

The number in the value field is converted to fixed point binary and stored with the binary point located at the position specified by the number in the exponent field. An overflow error check is made.

I: Decimal integer

The number in the value field is converted to a fixed point binary integer with the binary point following position 17. The exponent field is ignored. A decimal point is considered an error.

B: Octal

The value plus exponent fields are converted as a logical octal word. It is not necessary to include leading zeros but the first octal digit must always occupy the leftmost position of the field.

D: BCI Data

The contents of the value plus exponent fields are interpreted as two BCI words and stored in two consecutive cells in descending order beginning at the location specified by the location field.

H: Heading Card

A card with an H in column 1 is considered a BCI heading card. If the location field is blank, the card is ignored. If the location field contains a left-justified one to four digit positive decimal integer V (octal, negative, or variable locations are not permitted), columns 7-72 of the card are stored directly in 11 consecutive words in descending order. The location of the first of these words is calculated by the routine as $HEAD(1+11*(V-1))$ where HEAD is defined as the last variable or array named in the CALL statement. Each card may be used as one record of output using FORMAT option A with column 7 of the card providing the code for printer spacing on output.

A: Variable names as data

The value plus exponent fields are interpreted in a pseudo FAP instruction format AAAAA T DDDDD P where the fields to replace are address, tag, decrement, and prefix, respectively. The address and decrement fields are defined normally to be 5 characters and the tag and prefix as one octal numeric character each. Any field containing less than the normal number of characters must end with a comma while fields of normal length must not. Any address or decrement field containing less than 5 numeric characters are converted as octal. Any address or decrement field containing at least one non-numeric character is interpreted as a variable or array name. Variable addresses cause the entire word from the compiler generated calling sequence to be loaded into the location word (i.e., the TSX X is stored in the location specified if X is the variable appearing in the address field). Variable decrements cause the right-most 18 bits from the compiler generated calling sequence to be loaded into the location word's prefix and decrement. Numeric tags and prefixes are loaded directly into the corresponding parts of the location words. Null fields are not loaded. Since the first blank indicates the end of the loading of a word, address only, address-tag, address-tag-decrement, or entire word may be loaded as desired.

G: Temporary Origin

The value in the first location field on the card is used as a temporary origin for tables. The location is saved and if data cards follow with blank location fields the corresponding data is stored consecutively in descending order beginning with the cell specified in the location in the G card. Columns 7-72 are ignored and may be used to identify the table.

The first nonblank location starts a new origin. If this nonblank location is a subscript, it references the last variable or array named, which may or may not have been on the G card.

J: Transfer

The location specified with this prefix must be an octal address and is the only part of the data field that is interpreted. The subroutine causes a transfer to the octal location specified and does not interpret the remaining fields on the card.

L: Two dimension array i_{\max} , j_{\max} definition

The location field contains the name of the array to be loaded. The value field is defined to consist of 2 subfields, separated by a comma, of 2 columns each containing the two-digit decimal integers for i_{\max} and j_{\max} respectively where i_{\max} and j_{\max} generally appear in a DIMENSION statement. The i_{\max} and j_{\max} values are retained to compute the successive subscripted locations until redefined. Blank address fields may follow this array definition if successive elements of the array are to be loaded.

M: Two dimension array i_{\max} , j_{\max} definition

Conversion is identical to L except the entire array is preset to zero.

E: End Case

This defines an end-of-case and control is returned to the FORTRAN object program. The rest of this field and the remaining fields on the card are ignored.

Calling Sequence:

The following two types of CALL statements may be used:

I. CALL FINP (n,X,Y,ZETA,...,mHX⁽⁵⁾Y⁽⁵⁾ZETA⁽²⁾...) where

- A. n is the number of variables and/or arrays in the list, excluding n itself.
- B. X, Y, ZETA,... are the names of variables and/or arrays restricted to at most 5 characters each, one character of which is non-numeric.
- C. m is 6 times n. Hence, mH allows for 6n Hollerith characters to follow.

D. X(5)Y(5)ZETA(2)... is a list of the items previously named in exactly the same order with (i) indicating the number, i, of blanks necessary to provide six Hollerith characters for each item. Since each item name is restricted to 5 characters, the minimum value of (i) is (1).

II. CALL FINP (0) where the number of items is given as zero. This CALL statement must be used only after a CALL statement of type I has been executed. When the subroutine encounters a zero for the number of items, it immediately refers to the last executed CALL FINP with a nonzero number of items for the names of the items to be loaded.

Space Requirements

613 cells.

Number of Pages

Writeup	6
Listing	<u>12</u>
Total	18

FINP

* FAP				FINP
	LBL	FINP		FINP
	TTL	FINP INPUT ROUTINE		FINP
	ENTRY	FINP		FINP01
	REM	CALL FINP (N,A,B,DATA,...,6NHA	B DATA ...)	FINP000
	REM	WHERE N IS NUM OF VARIABLES AND		FINP000
	REM	6N IS 6 TIMES NUM OF VARIABLES		FINP000
FINP	TXH	0,0,0		FINP000
	SXD	GIN00,4		FINP000
	SXD	GIN02,1		FINP000
	SXD	GIN05,2		FINP000
	SXD	STOP1,4		FINP000
	SXD	STOP2,4		FINP001
	CLA*	1,4		FINP001
	TNZ	INPT1		FINP001
	STO	COMMON+28	FLAG TO USE PREVIOUS CALL	FINP001
INPT1	TXL	INPT2		FINP001
	STO	COMMON+28	FLAG TO USE PRESENT CALL	FINP001
	SXD	FINPT,4		FINP001
	NOP			FINP001
	COM			FINP001
	STD	++1		FINP001
	TXI	++1,4,0		FINP002
INPT2	SXD	GIN00,4		FINP002
	LXD	FINPT,4		FINP002
	CLA*	1,4		FINP002
	ARS	18		FINP002
	STO	COMMON+29	N	FINP002
	ALS	18		FINP002
	COM			FINP002
	STD	TBL03		FINP002
	STD	++1		FINP002
	TXI	++1,4,0		FINP003
	CLA	0,4		FINP003
	STA	GIN01	ADDRESS OF HEADER	FINP003
	CLA	1,4		FINP003
	STA	TBL01	ADDRESS OF BCD TABLE	FINP003
	STO	ERROR		FINP003
GINA	LXD	GIN00,4		FINP003
	CALL	(CSH)S		FINP003
	PZE	COMMON,0,-1		FINP003
STOP1	PZE	1,4		FINP003
	AXC	COMMON,1		FINP004
	TXI	++1,1,-12		FINP004
	SXD	GINC,1		FINP004
	SXD	GIN11+1;1		FINP004
	AXC	COMMON,1		FINP004
	CLA	BLANK		FINP004
GINB	CAS	0,1		FINP004
	TXL	GINC+2		FINP004
	TXI	++2,1,-1		FINP004

GINC	TXL	GINC+2		FINP0049
	TXH	GINB,1,**		FINP0050
	TXL	GINA		FINP0051
	AXC	COMMON,1		FINP0052
	LDQ	0,1		FINP0053
GIN01	PXD	**	SAVE PREFIX CODE	FINP0054
	LGL	6		FINP0055
	STO	PREFIX		FINP0056
	STQ	0,1		FINP0057
	SUB	ME	E	FINP0058
	TZE	GIN13	END	FINP0059
	LGL	30	SAVE LAST DIGIT OF ADDRESS	FINP0060
	ANA	MASK1		FINP0061
	STO	ADDIND		FINP0062
	STZ	SUM	TEST FOR BLANK ADDRESS	FINP0063
	STZ	SIGN		FINP0064
	CLA	0,1		FINP0065
	CAS	MASK2		FINP0066
	TXL	**+2		FINP0067
	TXL	GIN06	BLANK	FINP0068
	LRS	18	TEST FOR MATRIX	FINP0069
	ANA	MASK1		FINP0070
	SUB	MASK4		FINP0071
	TNZ	GIN17-2		FINP0072
	TSX	MTX00,4	MATRIX	FINP0073
	TRA	GINER	OUTSIDE MATRIX	FINP0074
	TRA	GIN20		FINP0075
MASK4	OCT	73		FINP0076
	AXT	5,4		FINP0077
	LDQ	0,1		FINP0078
GIN17	PXD			FINP0079
	LGL	6		FINP0080
	PAX	0,2		FINP0081
	TXL	GIN18,2,9		FINP0082
	TXH	GIN19,2,48		FINP0083
	TXL	GIN19,2,47		FINP0084
GIN18	TIX	GIN17,4,1		FINP0085
	TXL	GIN16		FINP0086
GIN19	CLA	0,1	SYMBOLIC	FINP0087
	ORA	MASK3		FINP0088
	TSX	TBL00,4		FINP0089
	LLS	35		FINP0090
	STA	GIN00		FINP0091
GIN20	CLA	MASK3		FINP0092
	STO	ADDIND		FINP0093
	TXL	GIN07		FINP0094
GIN16	CLA	ADDIND	TEST FOR OCTAL	FINP0095
	SUB	MASK3		FINP0096
	TZE	GIN04		FINP0097
	LXA	5B35,2	SET-UP OCTAL ADDRESS	FINP0098
	TSX	OCTAL,4		FINP0099


```

BLANK BCI 1,
      REM
HGIN00 CLA CRDADD
      CAS MASK2
      TXL **2
      TXL GIN12
      LDQ CRDADD
      MPY 11B35
      STQ COMMON
      CAL GIN01
      SBM COMMON
      STA HGIN01
      LXD 1B35,4
      LXA 11B35,1
      CLA COMMON+12,1
HGIN01 STO **,4
      TXI **1,4,1
      TIX HGIN01=1,1,1
      TXL GIN12
GGIN00 CLA ADDIND
      SUB MASK3
      TZE GGIN01
      PXD
      TXL GGIN02
GGIN01 CAL GIN00
GGIN02 ADD 1B35
      ADD CRDADD
      STA SGIN03
      TXL GIN12
BGIN00 STZ SUM
      STZ SIGN
      LXA M6B35,2
      TSX OCTAL,4
      TXI BGIN04,1,-1
      TXI BGIN01,1,-1
BGIN01 LXA M6B35,2
      TSX OCTAL,4
      TXH 4
BGIN02 TSX SGIN00,4
BGIN03 TXL GIN11,,**
BGIN04 TXH BGIN03,2,5
      TXL BGIN02
IGIN00 TSX DECNO,4
      TXH GINER,2,0
      LLS 18
      TXL BGIN02
DGIN00 LDQ 0,1
      TSX SGIN00,4
      CLA MASK2
      STO CRDADD
      LDQ 1,1

```

BLANK

EXIT FOR NEW PREFIX
BLANK

INTERGER FORMAT
ERROR FOR NON-INTEGER

```

FINP0151
FINP0152
FINP0153
FINP0154
FINP0155
FINP0156
FINP0157
FINP0158
FINP0159
FINP0160
FINP0161
FINP0162
FINP0163
FINP0164
FINP0165
FINP0166
FINP0167
FINP0168
FINP0169
FINP0170
FINP0171
FINP0172
FINP0173
FINP0174
FINP0175
FINP0176
FINP0177
FINP0178
FINP0179
FINP0180
FINP0181
FINP0182
FINP0183
FINP0184
FINP0185
FINP0186
FINP0187
FINP0188
FINP0189
FINP0190
FINP0191
FINP0192
FINP0193
FINP0194
FINP0195
FINP0196
FINP0197
FINP0198
FINP0199
FINP0200
FINP0201

```

DECNO TXI BGINO2,1,-1
 SXD BGINO3,4
 CLA 1,1
 ALS 24
 SLW COMMON*20
 STZ SUM
 STZ SIGN
 LXA 100B35,2
 CLS M6B35
 TSX DECIM,4
 TXI DEC2+1,1,-1
 TXI DEC1,1,-1

6
 END ON BLANK
 4

DECN1 CLA 4B35
 TSX DECIM,4
 DEC2 TXH 2,**,
 TXL DEC4,2,99
 TXL GIN11,2,100
 DEC3 LXD 1B35,2
 DEC4 LXD BGINO3,4
 LXD BGINO3,4

DECEN SXD GINO3,4
 TSX DECNO,4
 STQ COMMON*13
 SXD DEC2,2
 CLA DEC2
 STZ SUM
 STZ SIGN
 LDQ COMMON*20
 STQ 0,1
 TSX DECIM,4
 TXH
 LXD GINO3,4
 TRA 1,4

FGIN00 TSX DECEN,4
 STQ COMMON
 CAL DEC2
 COM
 ADD 1B17
 PDX 0,2
 CLA COMMON
 SUB BREF,2
 TMI GINER
 STA FGINO1
 LDQ COMMON*13
 MPY FREF,2

FGIN01 LRS **
 TNZ GINER
 TXL BGINO2,**,
 LGIN00 TSX DECEN,4
 STQ COMMON

FIXED PT. CONVERSION

FLTG. PT. CONVERSION

FINP0202
 FINP0203
 FINP0204
 FINP0205
 FINP0206
 FINP0207
 FINP0208
 FINP0209
 FINP0210
 FINP0211
 FINP0212
 FINP0213
 FINP0214
 FINP0215
 FINP0216
 FINP0217
 FINP0218
 FINP0219
 FINP0220
 FINP0221
 FINP0222
 FINP0223
 FINP0224
 FINP0225
 FINP0226
 FINP0227
 FINP0228
 FINP0229
 FINP0230
 FINP0231
 FINP0232
 FINP0233
 FINP0234
 FINP0235
 FINP0236
 FINP0237
 FINP0238
 FINP0239
 FINP0240
 FINP0241
 FINP0242
 FINP0243
 FINP0244
 FINP0245
 FINP0246
 FINP0247
 FINP0248
 FINP0249
 FINP0250
 FINP0251
 FINP0252



```

LXD DECN2,2
PXD ,2
ARS 18
SSM
ADD COMMON
LRS 35
DVP 10B35
SUB M9B35
PAX ,2
CLM
LLS 35
ADD 5B35
TMI GINER
PAX ,4
SXD FGINO1*2,1
CLA XREF1,2
ADD XREF2,4
ADD 126B35
TRL LGINOA
STZ COMMON+13
LGINOA PAX 0,1
LDQ FREF1,2
MPR FREF2,4
LRS 35
MPY COMMON+13
LLS 2
TZE LGINO3
LGINO1 TZE LGINO2
LRS 1
TXI LGINO1,1,1
LGINO2 PXD ,1
ARS 18
LLS 0
LRS 8
LGINO3 LXD FGINO1*2,1
TNZ GINER
TXL BGINO2
SGINOO CLA CRDADD
SUB MASK2
TZE SGINO1
CLA ADDIND
SUB MASK3
TZE SGINOA
CLA CRDADD
TXL SGINO2
SGINOA CAL GINOO
SUB CRDADD
TXL SGINO2
SGINO1 CAL SGINO3
SUB 1B35
SGINO2 STA SGINO3

```

HIGH DIGIT

SAVE ADD REFERENCE

EXIT TO STORE
STORE ROUTINE

ADD 1 TO OLD ADDRESS

```

FINP0253
FINP0254
FINP0255
FINP0256
FINP0257
FINP0258
FINP0259
FINP0260
FINP0261
FINP0262
FINP0263
FINP0264
FINP0265
FINP0266
FINP0267
FINP0268
FINP0269
FINP0270
FINP0271
FINP0272
FINP0273
FINP0274
FINP0275
FINP0276
FINP0277
FINP0278
FINP0279
FINP0280
FINP0281
FINP0282
FINP0283
FINP0284
FINP0285
FINP0286
FINP0287
FINP0288
FINP0289
FINP0290
FINP0291
FINP0292
FINP0293
FINP0294
FINP0295
FINP0296
FINP0297
FINP0298
FINP0299
FINP0300
FINP0301
FINP0302
FINP0303

```


END ON DIGIT COUNT

DECIM7	TIX	DECIM1,4,1	FINP0355
	LXD	DECIM2,4	FINP0356
	TXI	DECIM8*1,4,-1	FINP0357
	DEC	133	FINP0358
100B35	DEC	100	FINP0359
	DEC	67	FINP0360
	DEC	34	FINP0361
1B35	DEC	1	FINP0362
	DEC	-33	FINP0363
	DEC	-66	FINP0364
	DEC	-99	FINP0365
	DEC	-132	FINP0366
XREF2	DEC	.918354961680	FINP0367
	DEC	.788860905380	FINP0368
	DEC	.677626357980	FINP0369
	DEC	.582076609280	FINP0370
	DEC	.580	FINP0371
	DEC	.858993459280	FINP0372
	DEC	.737869763080	FINP0373
	DEC	.633825300280	FINP0374
	DEC	.544451787180	FINP0375
FREF2	DEC	30	FINP0376
	DEC	27	FINP0377
	DEC	24	FINP0378
	DEC	20	FINP0379
17B35	DEC	17	FINP0380
	DEC	14	FINP0381
10B35	DEC	10	FINP0382
	DEC	7	FINP0383
4B35	DEC	4	FINP0384
BREF	DEC	1	FINP0385
	DEC	-3	FINP0386
M6B35	DEC	-6	FINP0387
M9B35	DEC	-9	FINP0388
	DEC	-13	FINP0389
	DEC	-16	FINP0390
	DEC	-19	FINP0391
	DEC	-23	FINP0392
	DEC	-26	FINP0393
XREF1	DEC	-29	FINP0394
	DEC	.931322574780	FINP0395
	DEC	.745058059780	FINP0396
	DEC	.596046447880	FINP0397
	DEC	.953674316580	FINP0398
	DEC	.762939453180	FINP0399
	DEC	.610351562580	FINP0400
	DEC	.976562580	FINP0401
	DEC	.7812580	FINP0402
	DEC	.62580	FINP0403
FREF	DEC	.580	FINP0404
	DEC	.880	FINP0405

	STA	SGIN03		FINP0457
	TSX	MTX00,4		FINP0458
MCD02	INOP	**		FINP0459
	LDQ	I		FINP0460
	STQ	IMAX		FINP0461
	MPY	J		FINP0462
	STQ	IJ		FINP0463
	LXA	MCD02,4		FINP0464
	TXL	MCD04,4,12		FINP0465
	LXA	IJ,4		FINP0466
	TXI	**1,4,-1		FINP0467
	SXD	**6,4		FINP0468
	CLA	GIN00		FINP0469
	STA	**2		FINP0470
	LXD	1B35,4		FINP0471
	STZ	**4		FINP0472
	TXI	**1,4,1		FINP0473
	TXL	*-2,4,**		FINP0474
MCD04	TXI	GIN11,1,-1		FINP0475
*				FINP0476
ACD0	STZ	CTR		FINP0477
	STZ	PASS		FINP0478
ACD1	STZ	PF		FINP0479
	AXT	5,2		FINP0480
	TSX	SYM00,4		FINP0481
	AXT	0,4	BLANK	FINP0482
	TXH	ACD6,2,1		FINP0483
	TXL	ACD12,4,0	NULL AND BLANK	FINP0484
	TXL	ACD6+1	NULL	FINP0485
ACD6	STQ	PF		FINP0486
	TXL	ACD10,4,0	BLANK	FINP0487
	AXT	1,2		FINP0488
	TSX	SYM00,4		FINP0489
	AXT	0,4	BLANK	FINP0490
	TXL	ACD10,2,1	NULL	FINP0491
	XCL			FINP0492
	ALS	15		FINP0493
	STT	PF		FINP0494
ACD10	LDQ	PF		FINP0495
	CLS	PASS		FINP0496
	STO	PASS		FINP0497
	TPL	ACD15		FINP0498
	STQ	WORD		FINP0499
	TXH	ACD1,4,0	NOT BLANK	FINP0500
ACD12	LXA	CTR,4		FINP0501
	TXH	ACD14,4,6		FINP0502
	TXI	**1,1,-1		FINP0503
	TXL	**3,4,1	BLANK	FINP0504
ACD14	LDQ	WORD		FINP0505
	TSX	SGIN00,4		FINP0506
	TXL	GIN11		FINP0507

ACD15	RQL	18		FINP05
	SLQ	WORD		FINP05
	TXL	ACD12		FINP05
* SYM00	SXD	SYM02,2	LXA L(NO CHARACTERS),2	FINP05
	SXA	SYM14,4	TSX SYM00,4	FINP05
	STZ	PSYM	BALNK	FINP05
	AXT	1,2	NORMAL IR2=1 IF NULL	FINP05
SYM01	CLA	CTR		FINP05
	ADD	1B35		FINP05
	STO	CTR		FINP05
	SUB	10B35+1	7	FINP05
	TNZ	**2		FINP05
	TXI	**1,1,-1		FINP05
	LDQ	0,1		FINP05
	CAL	PSYM		FINP05
	LGL	6		FINP05
	SLW	PSYM		FINP05
	STQ	0,1		FINP05
	ANA	MASK1		FINP05
	SUB	MASK3		FINP05
	TZE	SYM20	BLANK	FINP05
	SUB	11B35		FINP05
	TZE	SYM21	COMMA	FINP05
	TXI	**1,2,1		FINP05
SYM02	TXL	SYM01,2,**		FINP05
	CAL	PSYM		FINP05
SYM03	TXI	**1,2,-1		FINP05
	SXA	SYM06,2	NO CHARACTERS:	FINP05
	LDQ	MASK2		FINP05
SYM04	LGL	6	LEFT JUSTIFY	FINP05
	TXI	**1,2,1		FINP05
	TXL	SYM04,2,5		FINP05
	SLW	SYMBL		FINP05
	CAL	PSYM		FINP05
	ANA	BLANK		FINP05
	TNZ	SYM10	SYMBOLIC	FINP05
SYM06	AXT	**2	NO CHARACTERS:	FINP05
	LDQ	SYMBL		FINP05
	STZ	SUM		FINP05
	STZ	SIGN		FINP05
	TXL	SYM08,2,4	DECIMAL	FINP05
	TSX	OCTAL1,4	OCTAL	FINP05
	TXL	GINER		FINP05
	TSX	SYM14,2		FINP05
SYM08	CLA	0,1		FINP05
	STQ	0,1		FINP05
	STO	SYMBL		FINP05
	PXA	,2		FINP05
	TSX	DECIM,4		FINP05
	TXL	GINER		FINP05

	CLA	SYMBL		FINP0559
	STO	0,1		FINP0560
	TSX	SYM14,2		FINP0561
SYM10	CLA	SYMBL:		FINP0562
	TSX	TBL00,4		FINP0563
SYM14	AXT	** ,4		FINP0564
	TRA	2,4	EXIT	FINP0565
SYM20	TXI	**1,4,1	BLANK	FINP0566
	SXA	SYM14,4		FINP0567
SYM21	TXL	SYM14+1,2,1	NULL FIELD	FINP0568
SYM25	CAL	PSYM		FINP0569
	ARS	6		FINP0570
	SLW	PSYM		FINP0571
	TXL	SYM03		FINP0572
TBL00	LXD	TBL01+1,2		FINP0573
TBL01	CAS	** ,2		FINP0574
	TXL	**2		FINP0575
	TXI	TBL02,2,-2		FINP0576
	TXI	**1,2,-1		FINP0577
TBL03	TXH	TBL01,2,**		FINP0578
	TXL	GINER,0,-1		FINP0579
TBL02	SXA	**1,2		FINP0580
	AXC	0,2		FINP0581
	SXA	**2,2		FINP0582
	LXD	FINPT,2		FINP0583
	LDQ	** ,2		FINP0584
	LXD	TBL03+1,2		FINP0585
	TRA	1,4		FINP0586
IMAX	PZE			FINP0587
IJ	PZE			FINP0588
COMMON	BSS	31		FINP0589
GIN00	SYN	COMMON+30		FINP0590
PF	SYN	COMMON+15		FINP0591
PASS	SYN	COMMON+16		FINP0592
CTR	EQU	COMMON+17		FINP0593
SYMBL	EQU	COMMON+18		FINP0594
PSYM	EQU	COMMON+19		FINP0595
CRDADD	EQU	COMMON+21		FINP0596
SIGN	EQU	COMMON+22		FINP0597
SUM	EQU	COMMON+23		FINP0598
ADDIND	EQU	COMMON+24		FINP0599
PREFIX	EQU	COMMON+25		FINP0600
WORD	SYN	COMMON+26		FINP0601
ERROR	SYN	COMMON+27		FINP0602
I	SYN	PASS		FINP0603
J	SYN	CTR		FINP0604
FINPT	SYN	FINP		FINP0605
	END			FINP

Function: FNORM

Purpose: To find the magnitude of a 3-dimensional vector.

Calling Sequence:

Y = FNORM(X)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	X	3	X_1, X_2, X_3		
O	FNORM	1			$FNORM = (X_1^2 + X_2^2 + X_3^2)^{\frac{1}{2}}$

Common storages used or required: None

Subroutines required: None

Functions required: SQRTF

Approximate number of storages required: _____

FNORM

```
*      SYMBOL TABLE
CEC2018  FUNCTION FNORM
          FUNCTION FNORM(X)
          DIMENSION X(3)
1  FNORM = SQRTF(X(1)**2+X(2)**2+X(3)**2)
3  RETURN
END
```

FNOR
FNOR
FNOR0000
FNOR0010
FNOR0020
FNOR0030
FNOR

Subroutine: GHA

Purpose: To determine the Greenwich Hour Angle of the first point of Aries for a given date and time.

Calling Sequence:

CALL GHA (TSEC, D, GHAN, DA, OMEGA)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	TSEC	1		seconds	Fractional part of day from D
I	D	1		days	Whole days from Jan. 1, 1950
O	GHAN	1		degrees	Greenwich Hour Angle, $0 \leq \text{GHA} < 360$
I	DA	1			Adjustment due to nutation*
O	OMEGA	1	ω_e	degrees/sec	Rate of rotation of the earth
					*DA = EN(2,1) of EN nutation matrix from NUTATE

Common storages used or required:

None

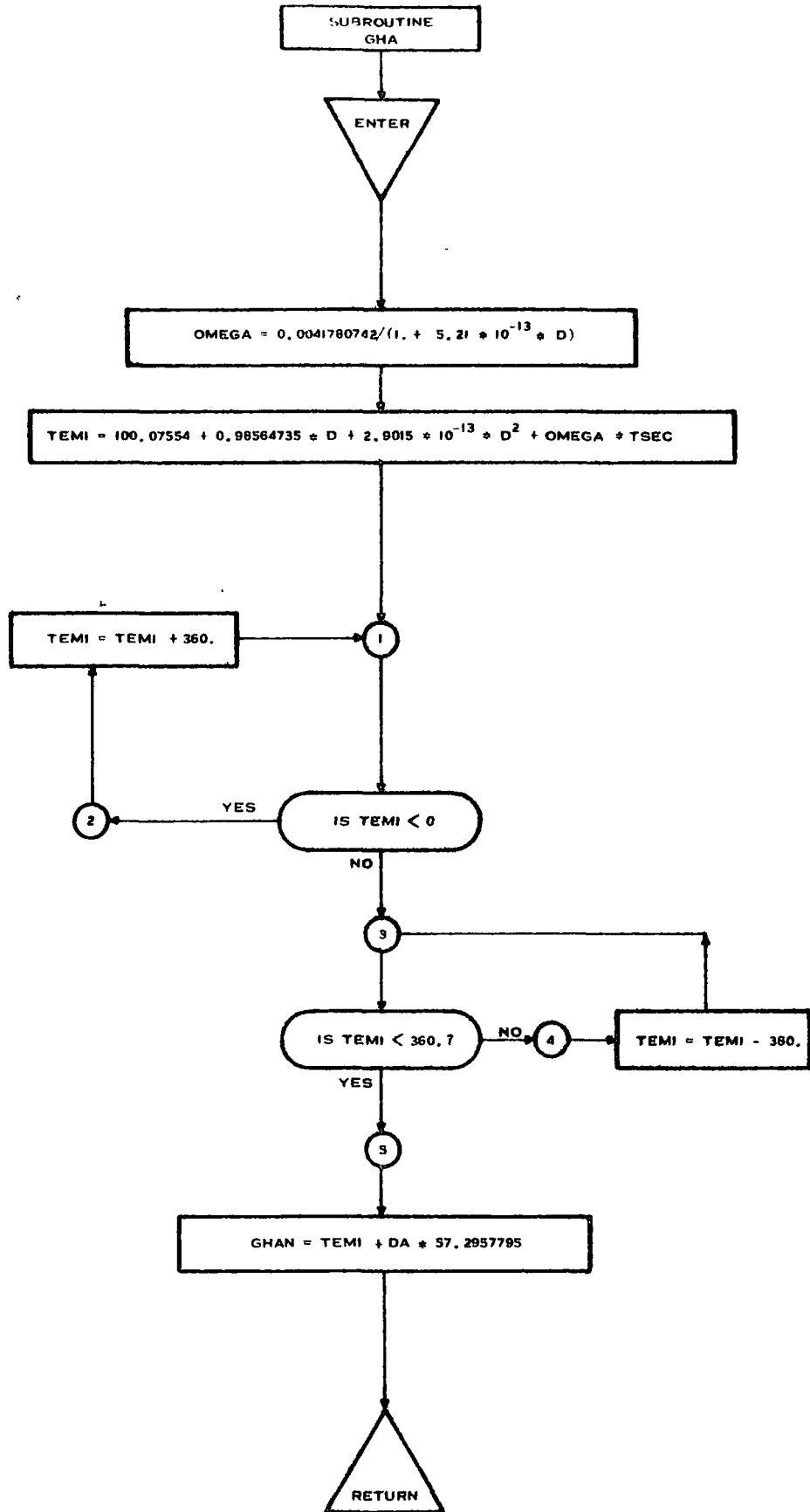
Subroutines required:

None

Functions required:

None

Approximate number of storages required:



GHA

```

* LABEL
CEC20AG
SUBROUTINE GHA(TSEC,D,GHAN,DA,OMEGA)
OMEGA = .0041780742/(1.+5.21E-13*D)
DD=D
D DD=DD*(.98564735/360.)
D DD=DD-INTF(DD)
DF=DD
TEM1 = 100.07554+360.*DF +2.9015E-13*D*D+OMEGA*TSEC
1 IF (TEM1) 2,3,3
2 TEM1 = TEM1+360.
GO TO 1
3 IF (TEM1-360.) 5,4,4
4 TEM1 = TEM1-360.
GO TO 3
5 GHAN = TEM1*DA*57.2957795
RETURN
END

```

GHA0
GHA0
GHA000
GHA001
GHA002
GHA003
GHA004
GHA005
GHA006
GHA007
GHA008
GHA009
GHA010
GHA011
GHA012
GHA013
GHA014
GHA0

Page Intentionally Left Blank

Subroutine: GOTOB

Purpose: It is a logic type of subroutine to read input data cards, set up a sequence for calling subroutine MATSUB, interpret types of measurements being made, and control integration package to perform specific operations (read new data, call MATSUB, stop, etc.) at specified times.

Calling Sequence:

CALL GOTOB (TSTPD)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	TSTPD	1	time	days	Desired stop time in days from start

Common storages used or required:

T, S, C, IC

Subroutines required:

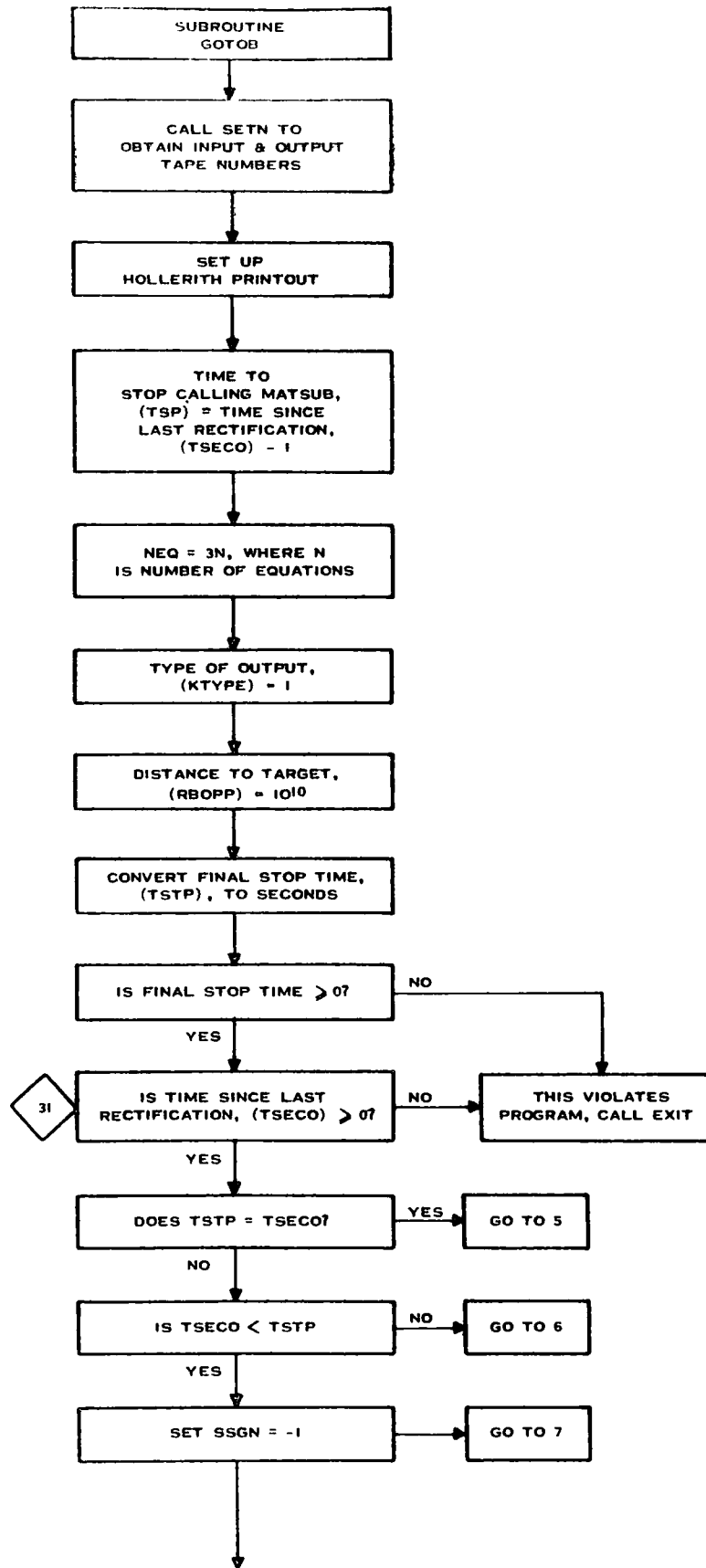
CHNGP, DE6FN, DE6FP, DE6FP3, DE6FP4, EXIT, MASS, MATSUB, MULT, NUTAIT, OUTC, ROTEQ,

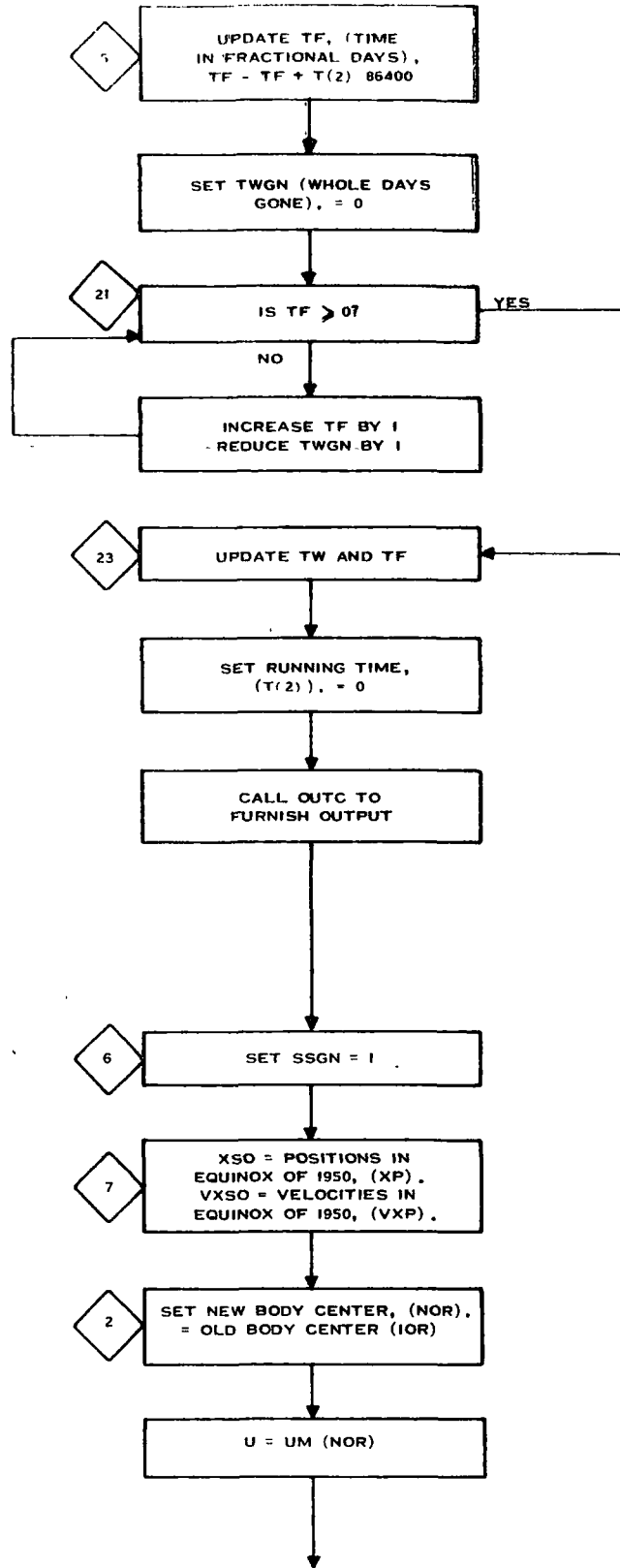
Functions required:

SDEC, SETN, SHIFTP, TIMED, FNORM (FIL) (RTN) (SLI)

Approximate number of storages required:

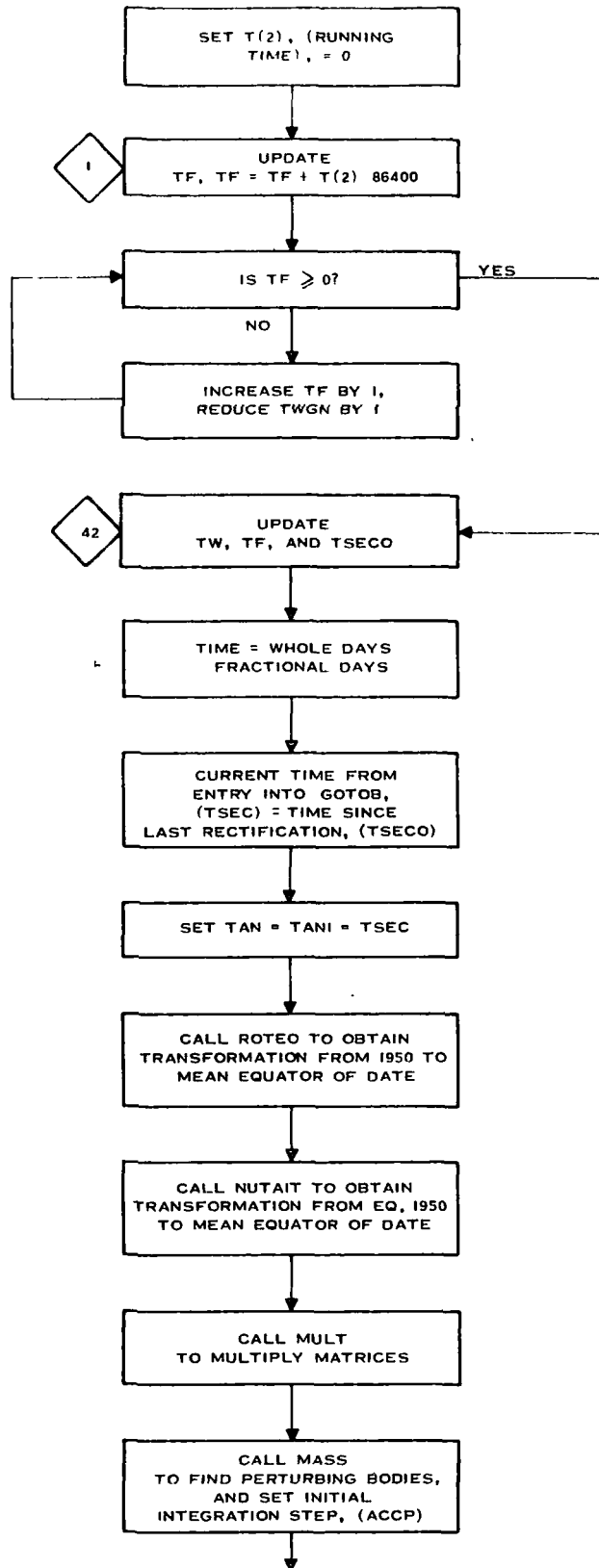
1242 DEC

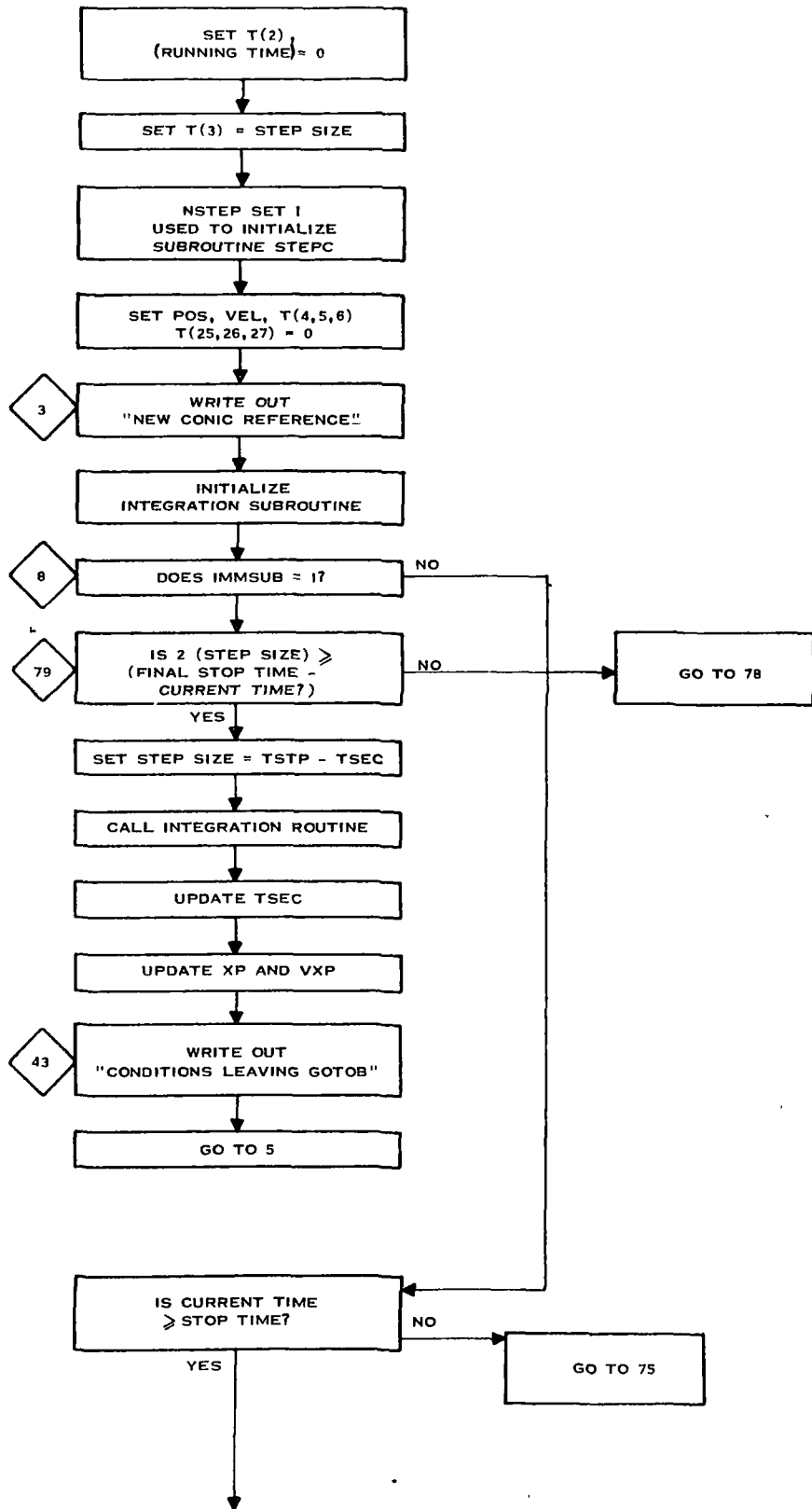




S-181

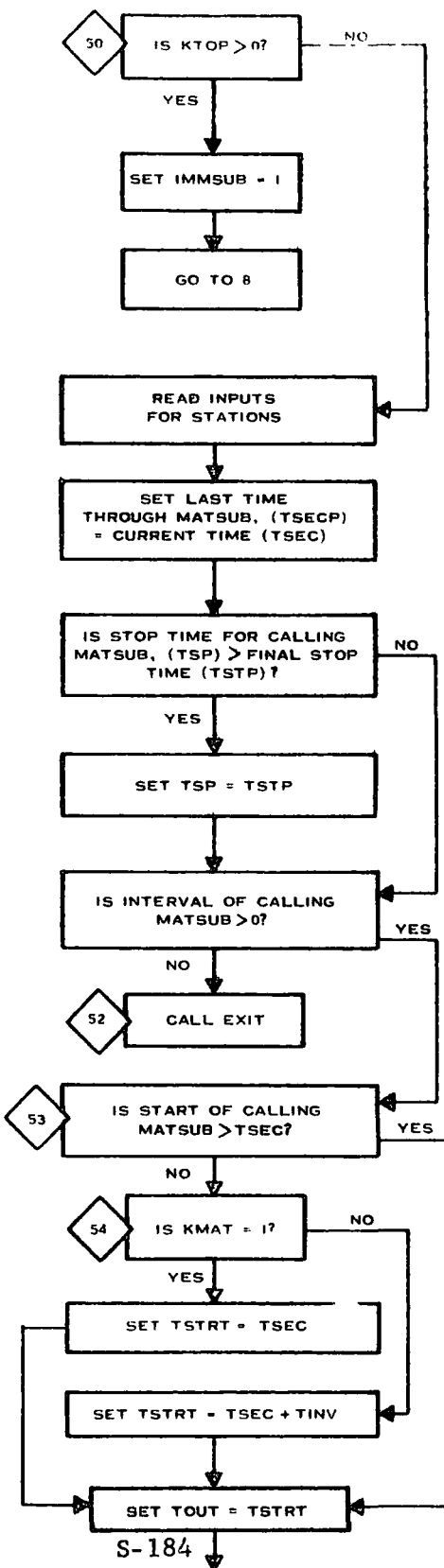
GOTOB-3





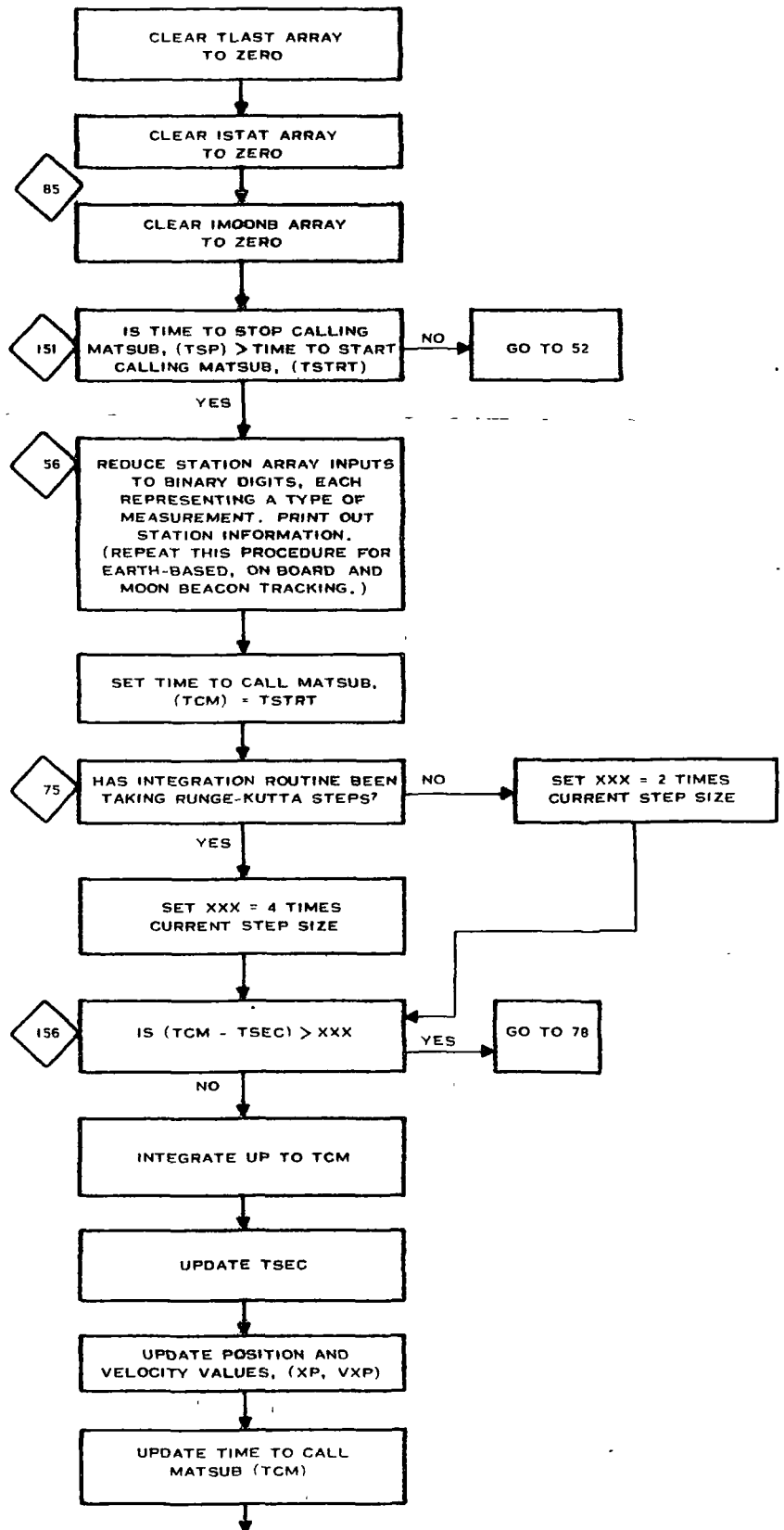
S-183

GOTOB-5



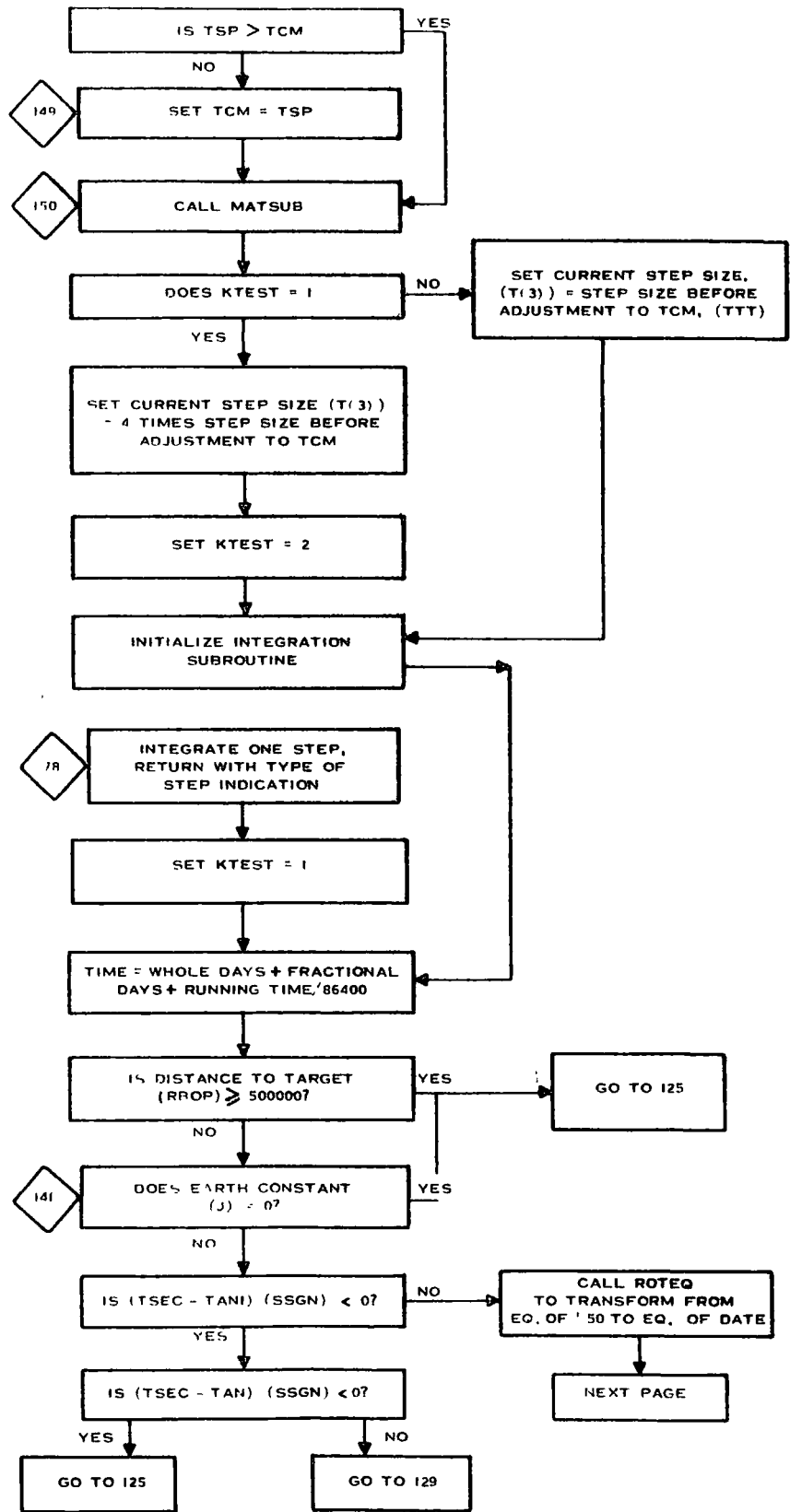
S-184

GOTOB-6



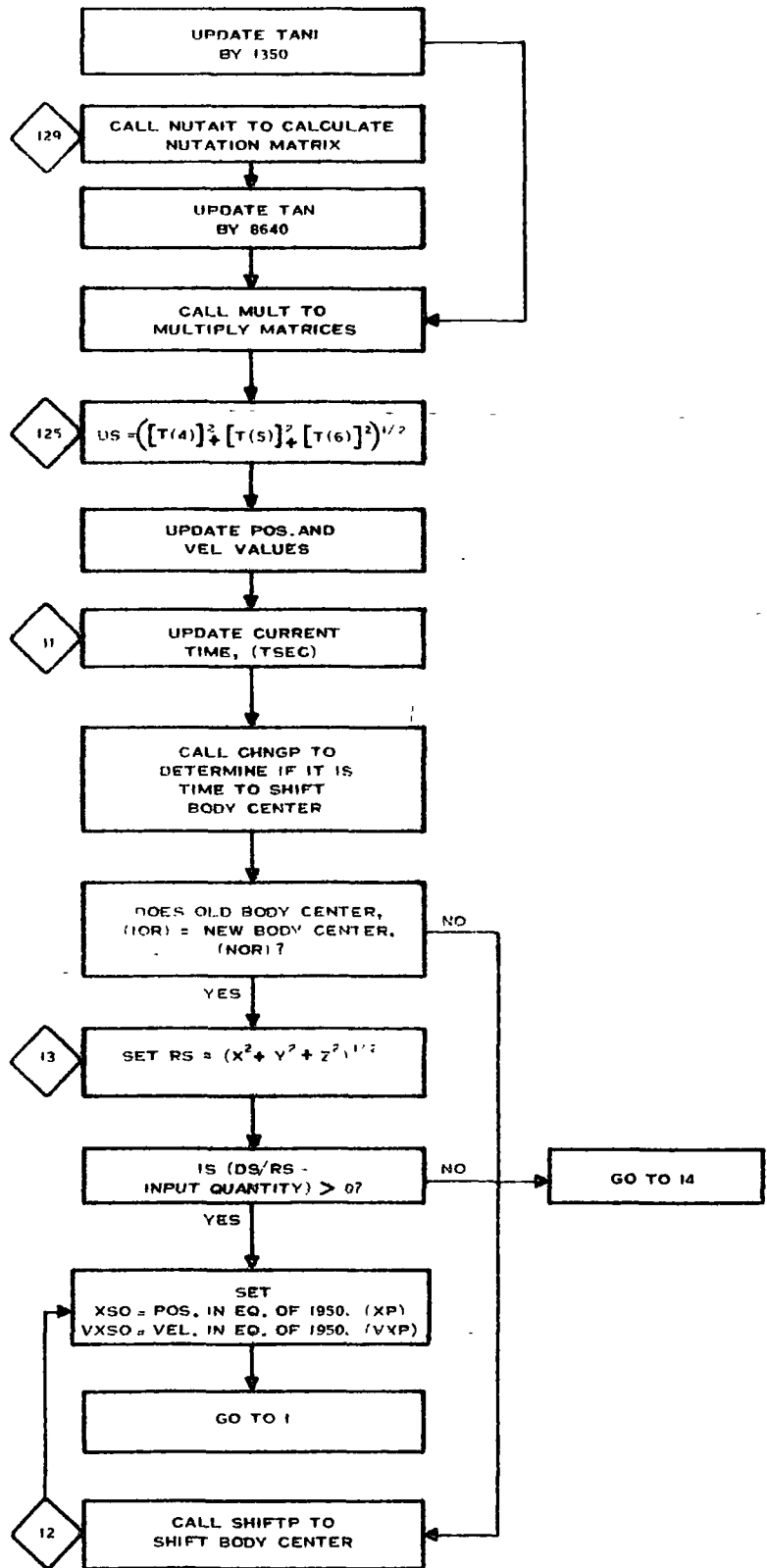
S-185

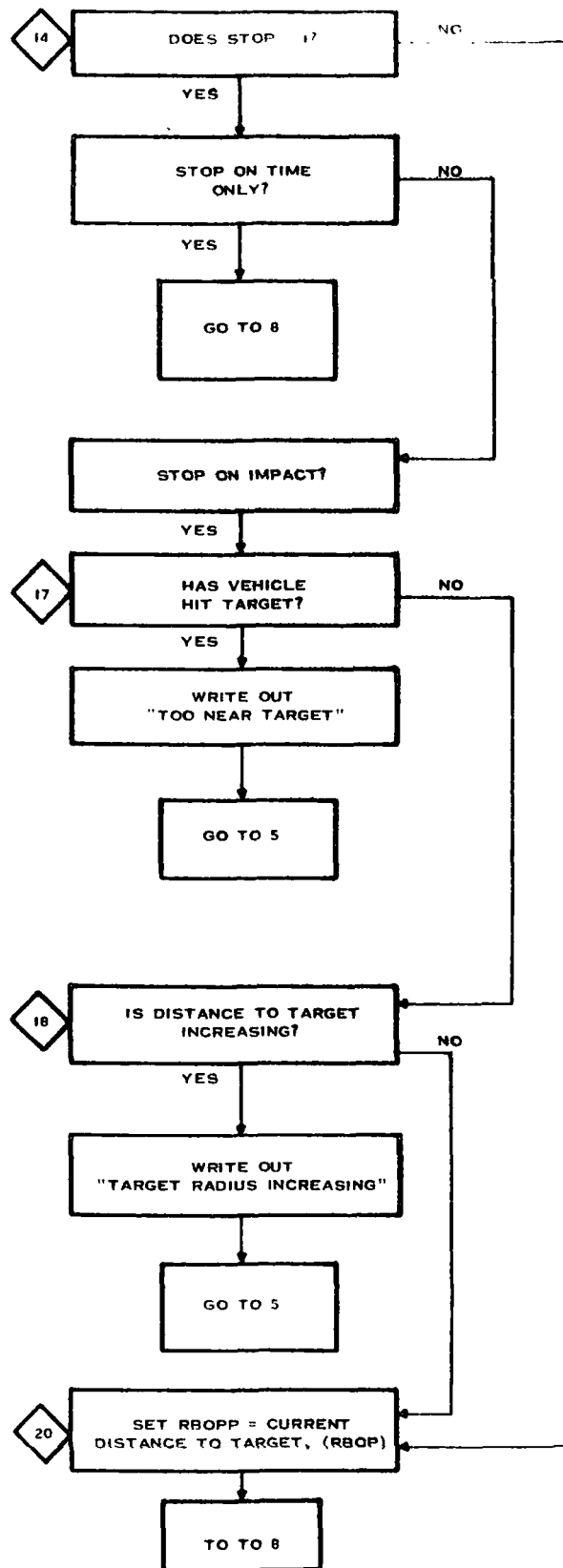
GOTOB-7



S-186

GOTOB-8





1000 (Cont'd)

	K=I+NEQV	GOTB1320
	XP(I)=X(I)+T(I+3)	GOTB1330
	VXP(I)=VX(I)+T(K)	GOTB1340
43	CONTINUE	GOTB1350
	WRITE OUTPUT TAPE NOUT,39	GOTB1360
39	FORMAT(25H0CONDITIONS LEAVING GOTOB)	GOTB1370
	WRITE OUTPUT TAPE NOUT,750	GOTB1380
750	FORMAT(21H STOPPED ON TIME STOP)	GOTB1390
	GO TO 5	GOTB1400
10	CONTINUE	GOTB1410
	IF(TSEC=TSP)75,50,50	GOTB1420
50	CONTINUE	GOTB1430
C	KTOP IS SET +1 ON LAST CARD OF SEQUENCE FOR NORMAL TIME STOP	GOTB1435
C	OF GOTOB	GOTB1436
	IF(KTOP)51,51,80	GOTB1440
80	CONTINUE	GOTB1450
	IMMSUB=1	GOTB1460
	GO TO 8	GOTB1470
51	READ INPUT TAPE NIN,700,ISA,IONB,IMB	GOTB1480
700	FORMAT(20I2,4X,6I2,4X,10I2)	GOTB1490
	READ INPUT TAPE NIN,701,KTOP,TSTR,TSP1,TINT,TPRIN	GOTB1500
701	FORMAT(1X,I1,4E17.8)	GOTB1510
	WRITE OUTPUT TAPE NOUT,708,KTOP,TSTR,TSP1,TINT,TPRIN	GOTB1520
708	FORMAT(/7H0 KTOP=,I1,7H TSTR=,1E17.8,7H TSP1=,1E17.8,7H TINT=	GOTB1530
	1,1E17.8,8H TPRIN=,1E17.8)	GOTB1540
	TSECP=TSEC	GOTB1550
C	SUBROUTINE TIMED CONVERTS INPUT TIMES FROM FORMAT	GOTB1555
C	(DAYS HOURS).(MIN SEC)	GOTB1556
	CALL TIMED(TSTR,TSTRT)	GOTB1560
C	TSTRT =START TIME FOR CALLING MATSUB	GOTB1570
	CALL TIMED(TSP1,TSP)	GOTB1580
C	TSP =STOP TIME AND INDICATOR FOR NEW DATA	GOTB1590
	STOP=KTOP	GOTB1600
	IF(TSP-TSTP)101,101,100	GOTB1610
100	TSP=TSTP	GOTB1620
101	CONTINUE	GOTB1630
	CALL TIMED(TINT,TINV)	GOTB1640
C	TINV =INTERVAL OF CALLING MATSUB	GOTB1650
	CALL TIMED(TPRIN,TPRINT)	GOTB1660
C	TPRINT=PRINT INTERVAL FOR MATSUB	GOTB1670
	IF(TINV) 52,52,53	GOTB1680
52	WRITE OUTPUT TAPE NOUT,702	GOTB1690
702	FORMAT(26H0YOU BOTCHED UP INPUT DATA)	GOTB1700
	CALL EXIT	GOTB1710
53	CONTINUE	GOTB1720
	IF(TSTRT-TSEC) 54,54,158	GOTB1730
54	CONTINUE	GOTB1740
	GO TO (152,153),KMAT	GOTB1750
152	TSTRT=TSEC	GOTB1760
	TOUT=TSEC	GOTB1770
	GO TO 158	GOTB1780

GOTOB-(Con't)

153	TSTRT=TSEC+TINV	GOTB179
	TOUT=TSEC+TPRINT	GOTB180
	GO TO 151	GOTB181
158	CONTINUE	GOTB182
	TOUT=TSTRT	GOTB183
	DO 84 I=1,4	GOTB184
	DO 84 J=1,6	GOTB185
	TLAST(I,J) =0.	GOTB186
84	CONTINUE	GOTB187
	DO 85 I=1,20	GOTB188
	ISTAT(I) =0	GOTB189
85	CONTINUE	GOTB190
	DO 86 I=1,10	GOTB191
	IMOONB(I)=0.	GOTB192
86	CONTINUE	GOTB193
151	CONTINUE	GOTB194
	IF(TSP-TSTRT) 52,52,55	GOTB195
55	CONTINUE	GOTB196
	LSTAT=1	GOTB197
	LONB=1	GOTB198
	LMB=1	GOTB199
	L=122	GOTB200
	DO 61 I=1,20	GOTB201
	L=L+15	GOTB202
	IF (ISA(I)) 61,61,56	GOTB203
56	CONTINUE	GOTB204
	WRITE OUTPUT TAPE NOUT,709,I,S(L)	GOTB205
709	FORMAT (17H STATION NUMBER ,I2,2H ,,A6,2H ,,10H MEASURES)	GOTB206
	BBB = ISA(I)	GOTB207
	LSTAT=2	GOTB208
	DO 60 J=1,4	GOTB209
	CCC=BBB/2.	GOTB210
	DDD=INTF(CCC)	GOTB211
	IF(CCC-DDD) 57,57,58	GOTB212
57	CONTINUE	GOTB213
C.	THE KS, KONB, AND KMB ARRAYS ARE COLUMN WISE ARRANGED IN BINARY	GOTB214
C.	FOR INDICATING TYPE MEASUREMENTS MADE ,KS FOR EARTH BASED TRACKING	GOTB215
C.	KONB FOR ONBOARD TRACKING, KMB FOR LUNAR BEACONS.	GOTB216
	KS(J,I)=0	GOTB217
	GO TO 59	GOTB218
58	CONTINUE	GOTB219
	KS(J,I)=1	GOTB220
	WRITE OUTPUT TAPE NOUT,703,SMEAS(J)	GOTB221
703	FORMAT (1H A6)	GOTB222
59	CONTINUE	GOTB223
	BBB=DDD	GOTB224
60	CONTINUE	GOTB225
61	CONTINUE	GOTB226
	DO 62 I=1,6	GOTB227
	IF (IONB(I)) 62,62,63	GOTB228
63	CONTINUE	GOTB229

GOTOB (Cont'd)

WRITE OUTPUT TAPE NOUT,704,BNAME(I)	GOTB2300
704 FORMAT (28H VEHICLE TO CELESTIAL BODY ,A6,10H MEASURES)	GOTB2310
LONB=2	GOTB2320
BBB=IONB(I)	GOTB2330
DO 68 J=1,4	GOTB2340
CCC=BBB/2.	GOTB2350
DDD=INTF(CCC)	GOTB2360
IF(CCC-DDD) 64,64,65	GOTB2370
64 CONTINUE	GOTB2380
KONB(J,I)=0	GOTB2390
GO TO 67	GOTB2400
65 CONTINUE	GOTB2410
KONB(J,I)=1	GOTB2420
WRITE OUTPUT TAPE NOUT,703,TOBM(J)	GOTB2430
67 CONTINUE	GOTB2440
BBB=DDD	GOTB2450
68 CONTINUE	GOTB2460
62 CONTINUE	GOTB2470
DO 74 I=1,10	GOTB2480
IF (IMB(I)) 74,74,69	GOTB2490
69 CONTINUE	GOTB2500
WRITE OUTPUT TAPE NOUT,706,I	GOTB2510
706 FORMAT (33H VEHICLE TO LUNAR BEACON NUMBER ,I2,10H MEASURES)	GOTB2520
LMB=2	GOTB2530
BBB=IMB(I)	GOTB2540
DO 73 J=1,4	GOTB2550
CCC=BBB/2.	GOTB2560
DDD=INTF(CCC)	GOTB2570
IF(CCC-DDD) 70,70,71	GOTB2580
70 CONTINUE	GOTB2590
KMB(J,I)=0	GOTB2600
GO TO 72	GOTB2610
71 CONTINUE	GOTB2620
KMB(J,I)=1	GOTB2630
WRITE OUTPUT TAPE NOUT,703,TOBM(J)	GOTB2640
72 CONTINUE	GOTB2650
BBB=DDD	GOTB2660
73 CONTINUE	GOTB2670
74 CONTINUE	GOTB2680
TCM=TSTRT	GOTB2690
75 CONTINUE	GOTB2700
IF(ACCUM) 154,154,155	GOTB2710
155 XXX=4.*T(3)	GOTB2720
GO TO 156	GOTB2730
154 XXX=2.*T(3)	GOTB2740
156 CONTINUE	GOTB2750
IF(TCM-TSEC=XXX) 76,76,78	GOTB2760
76 CONTINUE	GOTB2770
TT=TCM-TSEC	GOTB2780
TTT=T(3)	GOTB2790
T(3)=TT	GOTB2800

GOTOB (Cont'd)

DO 77 I=1,4	GOTB281
CALL DE6FP3(TT)	GOTB282
77 CONTINUE	GOTB283
TSEC = TSECO + T(2)	GOTB284
DO 157 I=1,3	GOTB285
K=I+NEQV	GOTB286
XP(I) = X(I)+T(I+3)	GOTB287
157 VXP(I) = VX(I)+T(K)	GOTB288
TCM=TCM+TINV	GOTB289
IF(TCM-TSP) 150,150,149	GOTB290
149 TCM=TSP	GOTB291
150 CONTINUE	GOTB292
CALL MATSUB	GOTB293
KMAT=2	GOTB294
IF(KTEST-1)81,81,82	GOTB295
81 T(3)=4.*TTT	GOTB296
KTEST=2	GOTB297
GO TO 87	GOTB298
82 T(3)=TTT	GOTB298
87 CONTINUE	GOTB299
CALL DE6FN(-1,1,T,NEQ,SDEC,3,4,1,E-9,3,456,172800.,86400.)	GOTB300
GO TO 113	GOTB301
78 CONTINUE	GOTB302
CALL DE6FP1(ACCUM)	GOTB303
KTEST=1	GOTB303
113 TIME = TW+TF + T(2)/86400.	GOTB304
IF(RBOP-500000.) 141,125,125	GOTB305
141 IF(VJ) 127,125,127	GOTB306
127 IF((TSEC-TAN1)*SSGN)142,126,126	GOTB307
142 IF((TSEC-TAN)*SSGN)125,129,129	GOTB308
126 CALL ROTEQ(TIME,EA)	GOTB309
TAN1=TAN1+1350.*SSGN	GOTB310
GO TO 140	GOTB311
129 CALL NUTAIT (TIME,CM,CRUD,DDC,EN,EPSIL)	GOTB312
TAN=TAN+8640.*SSGN	GOTB313
140 CALL MULT(EN,EA,AN,0)	GOTB314
125 CONTINUE	GOTB315
DS=FNORM(T(4))	GOTB316
DO 11 I=1,3	GOTB317
K=I+NEQV	GOTB318
XP(I)=X(I)+T(I+3)	GOTB319
VXP(I)=VX(I)+T(K)	GOTB320
11 CONTINUE	GOTB321
TSEC = TSECO + T(2)	GOTB322
CALL CHNGP(NOR,IOR,RBOP)	GOTB323
IF(IOR-NOR)12,13,12	GOTB324
13 CONTINUE	GOTB325
RS=FNORM(X)	GOTB326
IF(DS/RS-ENKE)14,15,15	GOTB327
15 CONTINUE	GOTB328
DO 16 I=1,3	GOTB329

GOTOB (Cont'd)

	XSO(I)=XP(I)	GOTB3300
	VXSO(I)=VXP(I)	GOTB3310
16	CONTINUE	GOTB3320
	GO TO 1	GOTB3330
12	CONTINUE	GOTB3340
	CALL SHIFTP(IOR,NOR,U,UM,XP,VXP,PO,VE,TF,TW,T(2))	GOTB3350
	GO TO 15	GOTB3360
14	CONTINUE	GOTB3370
	ITARG = ITARG	GOTB3380
	IF(STOP=1.)20,83,83	GOTB3390
83	CONTINUE	GOTB3400
	KSTP=KSTP	GOTB3410
	GO TO (17,18,8),KSTP	GOTB3420
17	CONTINUE	GOTB3430
	IF(RBOP(ITARG)-RAD(ITARG))19,19,18	GOTB3440
19	CONTINUE	GOTB3450
	WRITE OUTPUT TAPE NOUT,39	GOTB3460
	WRITE OUTPUT TAPE NOUT,34,RBOP(ITARG),RAD(ITARG),ITARG	GOTB3470
34	FORMAT(21H TOO NEAR TARG RBOP=,1E17.8,5H RAD=,1E17.8,6H TARG=,I1)	GOTB3480
	KTYPE=2	GOTB3490
	GO TO 5	GOTB3500
18	CONTINUE	GOTB3510
	IF(RBOP(ITARG)-RBOPP)20,35,35	GOTB3520
35	CONTINUE	GOTB3530
	WRITE OUTPUT TAPE NOUT,39	GOTB3540
	WRITE OUTPUT TAPE NOUT,36,RBOP(ITARG),RBOPP,ITARG	GOTB3550
36	FORMAT(29H TARG RADIUS INCREASING RBOP=,1E17.8,7H RBOPP=,1E17.8,6H	GOTB3560
	1 TARG=,I1)	GOTB3570
	KTYPE=2	GOTB3580
	GO TO 5	GOTB3590
20	CONTINUE	GOTB3600
	RBOPP=RBOP(ITARG)	GOTB3610
	GO TO 8	GOTB3620
	END	GOTB

Subroutine: GOTOR

Purpose: To solve Kepler's equation for incremental excentric anomaly on a conic section given the incremental mean anomaly (time).

Calling Sequence:

CALL GOTOR (K, VM, C, F, E1)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	K	1	K		Orbit type (1) Elliptic (2) Hyperbolic
I	VM	1	ΔM	RAD	Incremental mean anomaly
I	C	2	$C_1 C_2$		Kepler's equation coefficients
O	F	4	F		Trigonometric functions of incremental eccentric anomaly
I/O		1	ΔE	RAD	Incremental eccentric anomaly

Common storages used or required: None

Subroutines required: None

Functions required: SIN, COS, EXP

Approximate number of storages required: 476 DEC

Discussion (See subroutine STEPC)

The incremental eccentric anomaly, φ , is implicitly expressed as a function of incremental mean anomaly, ΔM , and conic coefficients, C_1 and C_2 , by transcendental equations

$$\Delta M = (\varphi - \sin \varphi) + C_1 \sin \varphi - C_2(\cos \varphi - 1) \quad \underline{\text{elliptical}}$$

$$\Delta M = (\sinh \varphi - \varphi) + C_1 \sinh \varphi + C_2(\cosh \varphi - 1) \quad \underline{\text{hyperbolic}}$$

The two equations above may be written as a single equation

$$\Delta M = f_1(\varphi) + C_1 f_3(\varphi) + C_2 f_4(\varphi)$$

if the convention below is adopted.

For the elliptical case, let

$$f_1(\varphi) = \varphi - \sin \varphi$$

$$f_2(\varphi) = 1 - \cos \varphi$$

$$f_3(\varphi) = \sin \varphi$$

$$f_4(\varphi) = \cos \varphi$$

and for the hyperbolic case, let

$$f_1(\varphi) = \sinh \varphi - \varphi$$

$$f_2(\varphi) = \cosh \varphi - 1$$

$$f_3(\varphi) = \sinh \varphi$$

$$f_4(\varphi) = \cosh \varphi$$

When $|\varphi| \leq 1$, numerical accuracy requires that $f_1(\varphi)$ and $f_2(\varphi)$ be computed by truncated series expansions. Otherwise, the computer library functions SINF, COSF and EXPF are used in the computation.

The slope of the function

$$F(\varphi) = f_1(\varphi) + C_1 f_3(\varphi) + C_2 f_4(\varphi)$$

at φ is seen to be

$$F'(\varphi) = f_2(\varphi) + C_1 f_4(\varphi) + C_2 f_3(\varphi).$$

$F(\varphi)$ is a monotonically increasing function of φ so that any solution of the equation $F(\varphi) = \Delta M$ is obviously unique. Newton's method of iteration is used. That is, letting φ_n be the n^{th} estimate of φ , the $(n+1)^{\text{st}}$ estimate is calculated from

$$\varphi_{n+1} = \varphi_n + \frac{\Delta M - F(\varphi_n)}{F'(\varphi_n)}$$

The iteration is halted and φ is said to be φ_n when

$$\left| \frac{\varphi_{n+1} - \varphi_n}{\varphi_{n+1} + \varphi_n} \right| \leq 3. \times 10^{-8}$$

or when $n = 20$, whichever occurs first. The $f_1(\varphi)$ as well as φ are output from GOTOR to avoid their re-computation outside the subroutine.

GOTOR

* LABEL	GOTR
CEC2091 NEW GOTOR	GOTR
SUBROUTINE GOTOR(K,VM,C,F,E1)	GOTR0010
DIMENSION C(2),F(4)	GOTR0020
NMAX=20	GOTR0030
N=0	GOTR0040
GO TO (1,2),K	GOTR0050
1 CONTINUE	GOTR0060
C FIRST GUESS IS OBTAINED FOR ELLIPTICAL CASE	GOTR0070
8 CONTINUE	GOTR0080
IF(E1=1.)30,31,31	GOTR0090
30 CONTINUE	GOTR0100
D2=E1*E1	GOTR0110
F(1)=E1*D2*(0.16666667E+00-D2*(0.83333333E-02-D2*(0.198412698E-03	GOTR0120
1-D2*(0.275573192E-05-D2*0.250521083E-07)))	GOTR0130
F(2)= D2*(0.5-D2*(0.41666667E-1-D2*(0.13888889E-2-D2*(0.24801587E-	GOTR0140
14-D2*0.27557319E-6)))	GOTR0150
F(3)=E1-F(1)	GOTR0160
F(4)=1.-F(2)	GOTR0170
GO TO 3	GOTR0180
31 CONTINUE	GOTR0190
F(3)=SINF(E1)	GOTR0200
F(4)=COSF(E1)	GOTR0210
F(1)=E1-F(3)	GOTR0220
F(2)=1.-F(4)	GOTR0230
GO TO 3	GOTR0240
2 CONTINUE	GOTR0250
C FIRST GUESS IS OBTAINED FOR HYPERBOLIC CASE	GOTR0260
9 CONTINUE	GOTR0270
IF(E1=1.)32,33,33	GOTR0280
32 CONTINUE	GOTR0290
D2=E1*E1	GOTR0300
F(1) =E1*D2*(0.16666667E+00+D2*(0.83333333E-02+D2*(0.198412698E-03	GOTR0310
1+D2*(0.275573192E-05+D2*0.250521083E-07)))	GOTR0320
F(2) =D2*(0.5+D2*(0.41666667E-1+D2*(0.13888889E-2+D2*(0.24801587E	GOTR0330
1-4+D2*0.27557319E-6)))	GOTR0340
F(3)=E1+F(1)	GOTR0350
F(4)=1.+F(2)	GOTR0360
GO TO 3	GOTR0370
33 CONTINUE	GOTR0380
EX=.5*EXPF(E1)	GOTR0390
OX=.25/EX	GOTR0400
F(3)=EX-OX	GOTR0410
F(4)=EX+OX	GOTR0420
F(1)=F(3)-E1	GOTR0430
F(2)=F(4)-1.	GOTR0440
3 CONTINUE	GOTR0450
CM=F(1)+C(1)*F(3)+C(2)*F(2)	GOTR0460
DM=F(2)+C(1)*F(4)+C(2)*F(3)	GOTR0470
DE=(VM-CM)/DM	GOTR0480
ERROR=DE	GOTR0490

GOTOR(Cont'd)

AB=ABSF(DE)	GOTR050
IF(AB=1,)10,10,11	GOTR051
11 DE=DE/AB	GOTR052
10 E2=E1+DE	GOTR053
IF(ABSF((E2-E1)/(E2+E1))-3.E-8)4,4,5	GOTR054
5 CONTINUE	GOTR055
IF(N=NMAX)6,7,7	GOTR056
7 CONTINUE	GOTR057
GO TO 4	GOTR058
6 CONTINUE	GOTR059
N=N+1	GOTR060
E1=E2	GOTR061
GO TO (8,9),K	GOTR062
4 CONTINUE	GOTR063
RETURN	GOTR064
END	GOTR

Page Intentionally Left Blank

Subroutine: GUID

Purpose: To determine the times when guidance corrections are to be made. Compute the correction to be made and determine the error in the correction being performed. Then the subroutine updates both the state and guidance covariance matrices for the correction.

Calling Sequence:

CALL GUID

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I					Quantities obtained from common
O					Quantities returned to common

Common storages used or required:

T, S, C, IC

Subroutines required:

INV3, MARX, SETN, SQRTF, TIMED

Functions required:

(FIL) (STH)

Approximate number of storages required:

1022 DEC

Theory for updating covariance matrices for a guidance correction.

The following quantities will be used in the derivation to follow.

$PAR(t_0)$ = covariance matrix of errors at injection

$\hat{x}(t)$ = estimate of state at time t

$\tilde{x}(t)$ = error in estimate of state at time t

$x(t)$ = true state at time t

$E(\tilde{x} \tilde{x}^T) = P(t)$ = covariance matrix of error in estimate at time t

The quantities \hat{x} , \tilde{x} , and x are all considered as deviation quantities from the nominal trajectory which arrives at the target in the desired manner.

Using linear theory for the deviations

$$x(t) = \Phi X(t_0)$$

where Φ is the transition matrix relating unit deviations in injection errors to deviations at time t . Then

$$PAR(t) = E(x(t) x(t)^T) = \Phi PAR(t_0) \Phi^T \quad (1)$$

where $PAR(t)$ is the covariance matrix of deviations from the nominal trajectory prior to any midcourse corrections.

Assuming we have a transition matrix which relates the vehicle state at time (t) to some desired conditions at the target, a guidance law may be derived to meet the desired end conditions. The two laws which the program can solve are: (1) Fixed Time of Arrival, and (2) Constant Energy with Respect to the Target.

$$\underline{C}(T) = (A_1 \ A_2) \begin{pmatrix} \underline{x}(t) \\ \underline{\dot{x}}(t) \end{pmatrix} \quad (2)$$

3 x 1 3 x 6 6 x 1

where $\underline{C}(T)$ = target conditions at time T

$(A_1 \ A_2)$ = transition matrix

For Fixed Time of Arrival:

$$\underline{C}(T) = \begin{pmatrix} x(T) \\ y(T) \\ z(T) \end{pmatrix}$$

3 x 1 3 x 1

For Constant Energy with Respect to the Target:

$$\underline{C}(T) = \begin{pmatrix} \delta B \cdot T(T) \\ \delta B \cdot R(T) \\ \delta V_{INF} \end{pmatrix}$$

The guidance law is derived such that the estimate of $\underline{C}(T)$, which represents deviations from the nominal trajectory at the target, is zero when the vehicle arrives at the target.

$$\underline{C}(T) = A_1 \hat{\underline{x}}(t) + A_2 \hat{\underline{\dot{x}}}(t)$$

3x1 3x3 3x1 3x3 3x1

(3)

The velocity correction is selected such that:

$$\underline{C}(T) + A_2 \dot{\underline{x}}_g = 0 = A_1 \hat{\underline{x}}(t) + A_2 \hat{\underline{x}}(t) + A_2 \dot{\underline{x}}_g \quad (4)$$

$\dot{\underline{x}}_g$ is multiplied by A_2 because as can be seen in equation (3), A_2 is a matrix of sensitivity partials relating $\underline{C}(T)$ to velocity deviations at time (t).

Solving equation 4 for $\dot{\underline{x}}_g$ yields

$$\dot{\underline{x}}_g = A_2^{-1} \underline{C}(T) = -A_2^{-1} A_1 \hat{\underline{x}}(t) - I \hat{\underline{x}}(t) \quad (5)$$

$$\dot{\underline{x}}_g = - \begin{bmatrix} A_2^{-1} A_1 & I \end{bmatrix} \begin{pmatrix} \hat{\underline{x}}(t) \\ \hat{\underline{x}}(t) \end{pmatrix} \quad (6)$$

We are interested in the covariance matrix PAR at (T), that is, at the time of arrival, since this is the covariance matrix of errors in guidance.

If we find $E(\underline{x}(t) \underline{x}(t)^T)$ after a correction, the use of equation (1) will propagate it to the target.

Let subscript (a) define the state after a correction, and subscript (b) define the state before the correction.

Then

$$\begin{pmatrix} \underline{x}_a \\ \dot{\underline{x}}_a \end{pmatrix} = \begin{pmatrix} \underline{x}_b \\ \dot{\underline{x}}_b \end{pmatrix} + \begin{pmatrix} 0 \\ \dot{\underline{x}}_g \end{pmatrix} + \begin{pmatrix} 0 \\ q \end{pmatrix}$$

where \dot{x}_g is the computed velocity correction and q is the error in making the correction. This is under the assumption of an impulsive correction. Utilizing equation (5), and since $x_a = \hat{x}_a + \tilde{x}_a$

$$\begin{pmatrix} \dot{x}_a \\ \dot{x}_a \end{pmatrix} = \begin{pmatrix} I & 0 \\ -A_2 A_1 & 0 \end{pmatrix} \begin{pmatrix} \hat{x}_b \\ \hat{x}_b \end{pmatrix} + \begin{pmatrix} \tilde{x}_b \\ \tilde{x}_b \end{pmatrix} + \begin{pmatrix} 0 \\ q \end{pmatrix} \quad (7)$$

and

$$E(x_a x_a^T) = \begin{bmatrix} I & 0 \\ -A_2 A_1 & 0 \end{bmatrix} E(\hat{x}_b \hat{x}_b^T) \begin{bmatrix} I & 0 \\ -A_2 A_1 & 0 \end{bmatrix}^T + E(\tilde{x}_b \tilde{x}_b^T) \\ 6 \times 6 \quad 6 \times 6 \quad 6 \times 6 \quad 6 \times 6 \quad 6 \times 6 \\ + E \begin{bmatrix} 0 & (0 \quad q^T) \\ q & \end{bmatrix} + \text{CROSS TERMS} \\ 6 \times 6$$

The cross terms are zero because:

1. $E(\hat{x} \tilde{x}^T) = 0$ because of using an optimum estimation procedure
2. $E(\hat{x} q_s^T) = E(\hat{x} \hat{x}^T) E(S) = 0$
 $E(\hat{x} q_p^T) = E(\hat{x} \hat{x}^T) E(U) = 0$

for the two types of correction errors described below.

The two types of errors considered in making a guidance correction are shutoff error and pointing.

A. Shutoff Error

Let the correction by $\dot{x}_g = \begin{pmatrix} v_x \\ v_y \\ v_z \end{pmatrix}$

The shutoff error is

$$\vec{\epsilon}_s = S \dot{\underline{x}}_g$$

where S is a scalar random variable which is gaussian $(0, \sigma_s)$.

B. Pointing Error

The pointing error is $\vec{\epsilon}_p = \vec{U} \times \dot{\underline{x}}_g$

where $U = (U_x, U_y, U_z)$ is a three dimensional spherical gaussian random variable with sigmas equal to σ_p and mean 0.

The two types of expected values of interest in equation (8) for the error in correction are $E(qq^T)$ and $E(\hat{x}q^T)$

$$\vec{q} = \vec{\epsilon}_p + \vec{\epsilon}_s$$

$$E(qq^T) = (\sigma_s^2 - \sigma_p^2) E(\dot{\underline{x}}_g \dot{\underline{x}}_g^T) + \sigma_p^2 E(\dot{\underline{x}}_g^T \dot{\underline{x}}_g) I$$

$$E(\hat{x}q^T) = 0$$

The two remaining expected values in equation (8) may be written as follows:

$$E(\hat{x} \hat{x}^T) = E(x - \tilde{x}) (x - \tilde{x})^T = E(x x^T) - E(x \tilde{x}^T) + E(\tilde{x} \tilde{x}^T) - E(\tilde{x} x^T)$$

$$\text{but } E(x \tilde{x}^T) = E([\hat{x} + \tilde{x}] \tilde{x}^T) = E(\tilde{x} \tilde{x}^T)$$

$$\text{since } E(\hat{x} \tilde{x}) = 0$$

$$\therefore E(\hat{x} \hat{x}^T) = E(x x^T) - E(\tilde{x} \tilde{x}^T)$$

$$E(\hat{x} \hat{x}^T) = PAR_b - P_b$$

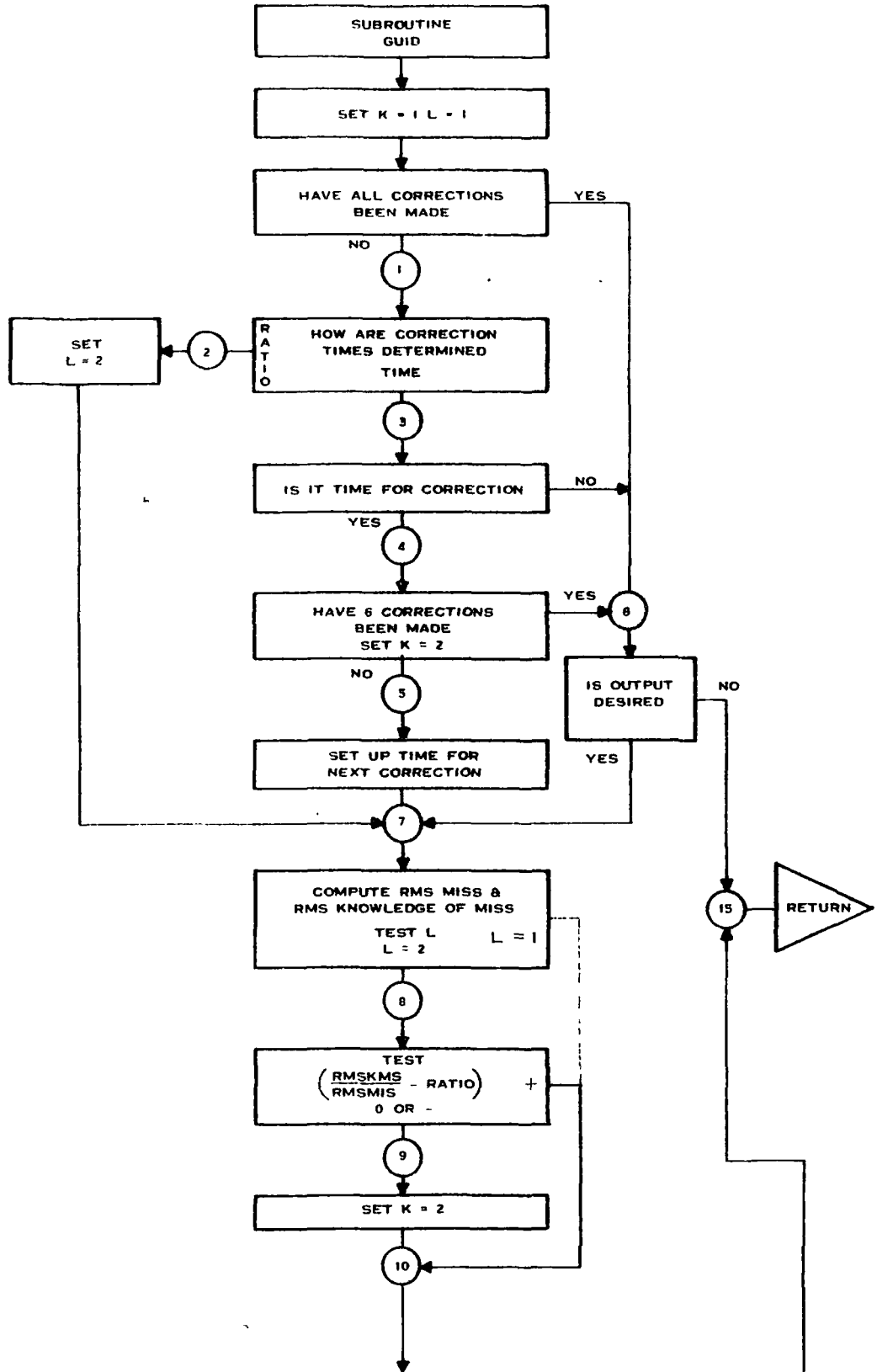
Finally

$$\begin{aligned}
 \text{PAR}_a &= \begin{bmatrix} I & 0 \\ -A_2^1 A_1 & 0 \end{bmatrix} \begin{bmatrix} \text{PAR}_b - P_b \end{bmatrix} \begin{bmatrix} I & 0 \\ -A_2^1 A_1 & 0 \end{bmatrix}^T \\
 6 \times 6 & \quad \quad 6 \times 6 \quad \quad 6 \times 6 \quad \quad \quad 6 \times 6 \\
 & + P_b + \begin{bmatrix} 0 & 0 \\ 0 & E(qq^T) \end{bmatrix} \\
 6 \times 6 & \quad \quad 6 \times 6
 \end{aligned}$$

The covariance matrix of the knowledge of the state is updated to account for the lack of exact knowledge of the correction.

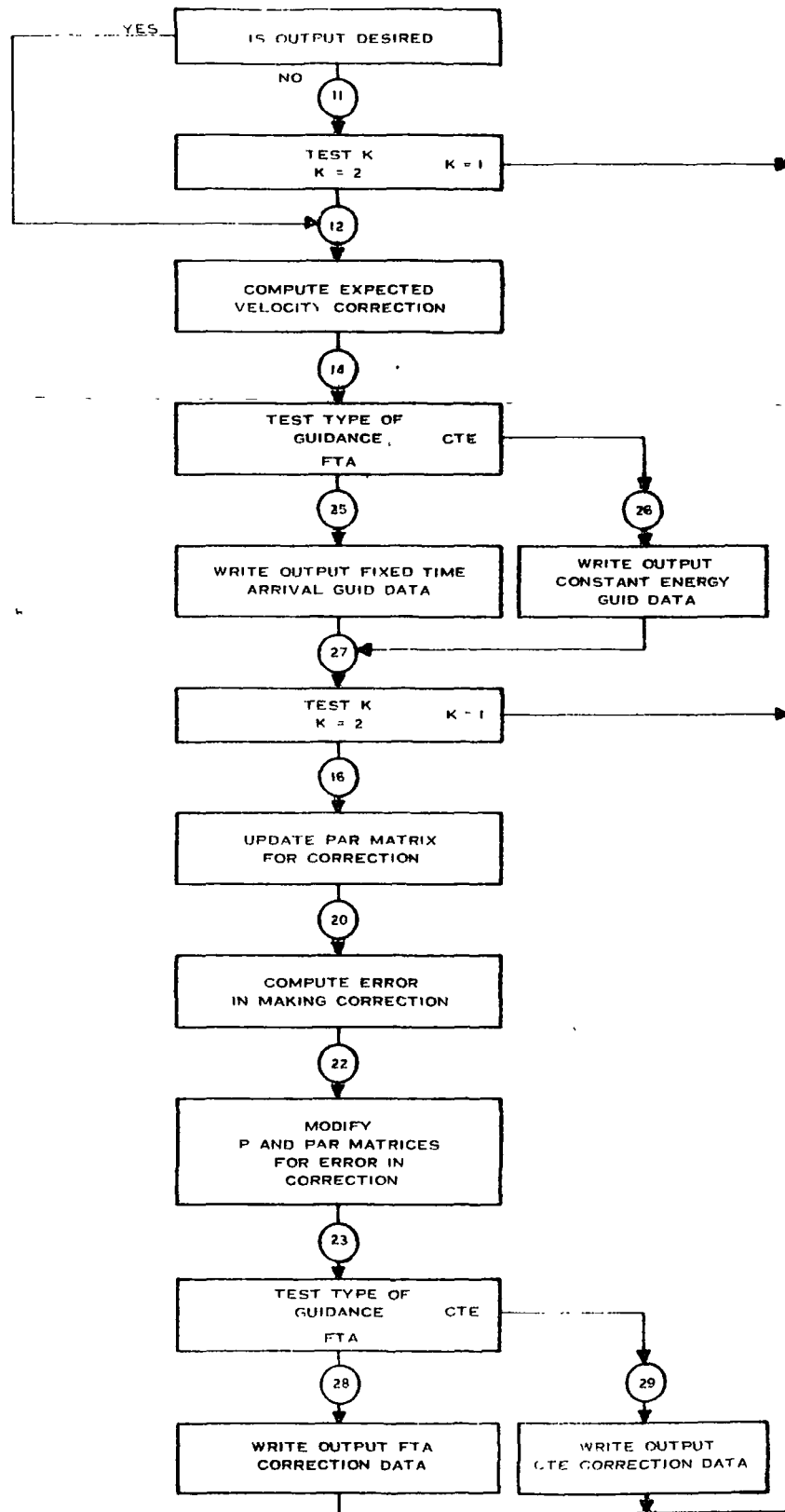
$$\begin{aligned}
 P_a &= P_b + \delta \begin{bmatrix} 0 & 0 \\ 0 & E(qq^T) \end{bmatrix} \\
 6 \times 6 \quad 6 \times 6 & \quad \quad 6 \times 6
 \end{aligned}$$

where δ indicates the ability to monitor (ON BOARD) the error in correction.



S-210

GUID-8



S-211

GUID-9

GUID

*	LABEL	GUID
*	SYMBOL TABLE	GUID
SEC2005	SUBROUTINE GUID	GUID
	SUBROUTINE GUID	GUID0000
	COMMON T,S,C,IC	GUID0010
	DIMENSION T(1360),S(1000),C(1000),IC(1)	GUID0020
	1,TPAR(3,6),PAR(6,6),P(6,6),DUP(3,3)	GUID0030
	2,TGUID(6),DUM(3,3),DUN(3,3),DUMM(6,6)	GUID0040
	EQUIVALENCE (T,TDUM),(S,SDUM),(C,CDUM)	GUID0050
	1,(IC,ICDUM),(C(568),TPAR),(C(460),PAR)	GUID0060
	2,(C(652),P),(IC(218),N),(C(648),TGUIDE)	GUID0070
	3,(IC(219),IGD),(IC(217),IGDTP),(IC(214),NOUT)	GUID0080
	4,(C(30),TSEC),(S(476),TGUID),(S(483),RATIO)	GUID0090
	5,(S(473),QQPT),(S(471),QQSO),(S(484),DMONIT)	GUID0100
	CALL SETN(NIN,NUTS)	GUID0105
:	IGD=NUMBER OF GUIDANCE CORRECTIONS TO BE MADE	GUID0110
:	N KEY USED TO TEST NUMBER OF GUIDANCE CORRECTIONS WHICH HAVE	GUID0120
:	BEEN MADE	GUID0130
:	S(475) 0=GUIDE ON INPUT TIMES + GUIDE ON A RATIO TEST	GUID0140
:	IGDTP 1,FTA 2,CTE 3.MINIMUM FUEL	GUID0150
:	DMONIT=ACCURACY OF MONITORING THE GUIDANCE CORRECTION	GUID0160
	NOUT=NOUT	GUID0170
	K=1	GUID0180
	L=1	GUID0190
	IF(IGD-N)6,1,1	GUID0200
1	IF(S(475))3,3,2	GUID0210
2	L=2	GUID0220
	GO TO 7	GUID0230
3	IF(TGUIDE-TSEC)4,4,6	GUID0240
4	CONTINUE	GUID0250
	K=2	GUID0260
	N=N+1	GUID0270
	IF(N-7)5,6,6	GUID0280
5	CALL TIMED(TGUID(N),TGUIDE)	GUID0290
	GO TO 7	GUID0300
6	CONTINUE	GUID0310
	GO TO (15,7),NOUT	GUID0320
7	CALL MATRX(TPAR,P,DUM,3,6,6,1)	GUID0330
	RMSKMS=SQRTF(DUM(1,1)+DUM(2,2)+DUM(3,3))	GUID0340
	CALL MATRX(TPAR,PAR,DUN,3,6,6,1)	GUID0350
	RMSMIS=SQRTF(DUN(1,1)+DUN(2,2)+DUN(3,3))	GUID0360
	GO TO (10,8),L	GUID0370
8	IF((RMSKMS/RMSMIS)-RATIO)9,9,10	GUID0380
9	K=2	GUID0390
	N=N+1	GUID0400
10	GO TO (11,12),NOUT	GUID0410
11	GO TO (15,12),K	GUID0420
12	CONTINUE	GUID0430
	DO 13 I=1,3	GUID0440
	DO 13 J=1,3	GUID0450
	JJ=J+3	GUID0460

GUID (Cont'd)

	DUP(I,J)=-TPAR(I, JJ)	GUID047
13	CONTINUE	GUID048
	CALL INV3(DUP,3,DET)	GUID049
	DO 14 I=1,3	GUID050
	DO 14 J=1,3	GUID051
	DUM(I,J)=DUN(I,J)-DUM(I,J)	GUID052
14	CONTINUE	GUID053
	RMSPAP=SQRTF(PAR(1,1)+PAR(2,2)+PAR(3,3))	GUID054
	RMSPAV=SQRTF(PAR(4,4)+PAR(5,5)+PAR(6,6))	GUID055
	CALL MATRX(DUP,DUM,DUM,3,3,3,1)	GUID056
C	DUM IS THE COVARIANCE MATRIX OF INDICATED VELOCITY CORRECTION	GUID057
	RMSV2=DUM(1,1)+DUM(2,2)+DUM(3,3)	GUID058
	RMSV=SQRTF(RMSV2)	GUID059
	IGDTP=IGDTP	GUID059
	GO TO (25,26),IGDTP	GUID059
25	CONTINUE	GUID059
	WRITE OUTPUT TAPE NUTS,800,RMSMIS,RMSPAP,RMSKMS,RMSPAV,RMSV	GUID060
800	FORMAT(18HOGUID DATA FOLLOWS, /	GUID061
	124H RMS FTA TARGET MISS=,E15.8,	GUID062
	225H RMS POS DEV FROM NOM=,E15.8, /	GUID063
	324H RMS KNOW. OF MISS=,E15.8,	GUID064
	425H RMS VEL DEV FROM NOM=,E15.8, /	GUID065
	524H RMS VEL REQ=,E15.8)	GUID065
	GO TO 27	GUID065
26	CONTINUE	GUID065
	RMSMIS=SQRTF(DUN(1,1)+DUN(2,2))	GUID065
	RMSVIN=SQRTF(DUN(3,3))	GUID065
	WRITE OUTPUT TAPE NUTS,802,RMSMIS,RMSPAP,RMSVIN,RMSPAV,RMSKMS,RMSV	GUID066
802	FORMAT(18HOGUID DATA FOLLOWS, /	GUID066
	124H RMS TARGET POS MISS=,E15.8,	GUID066
	225H RMS POS. DEV FROM NOM=,E15.8, /	GUID066
	324H RMS VINFINITY MISS=,E15.8,	GUID066
	425H RMS VEL DEV FROM NOM=,E15.8, /	GUID066
	324H RMS KNOW. OF MISS=,E15.8,	GUID066
	525H RMS VEL REQ=,E15.8)	GUID066
27	CONTINUE	GUID066
	GO TO (15,16),K	GUID067
15	RETURN	GUID068
16	CONTINUE	GUID069
C	FOLLOWING IS UPDATING OF PAR MATRIX FOR GUIDANCE CORRECTION	GUID070
	DO 17 I=1,6	GUID071
	DO 17 J=I,6	GUID072
	PAR(I,J)=PAR(I,J)-P(I,J)	GUID073
	PAR(J,I)=PAR(I,J)	GUID074
17	CONTINUE	GUID075
	CALL MATRX(DUP,TPAR,DUP,3,3,3,0)	GUID076
	DO 19 I=1,3	GUID077
	II=I+3	GUID078
	DO 18 J=1,3	GUID079
	IJJ=J+3	GUID080
	DUMM(II,J)=DUP(I,J)	GUID081

GUID (Cont'd)

	DUMM(I, JJ)=0.	GUID0820
	DUMM(II, JJ)=0.	GUID0830
18	DUMM(I, J)=0.	GUID0840
19	DUMM(I, I)=1.	GUID0850
	CALL MATRX(DUMM, PAR, PAR, 6, 6, 6, 1)	GUID0860
	DO 20 I=1, 6	GUID0870
	DO 20 J=I, 6	GUID0880
	PAR(I, J)=PAR(I, J)+P(I, J)	GUID0890
	PAR(J, I)=PAR(I, J)	GUID0900
20	CONTINUE	GUID0910
	CRUD=QQPT+RMSV2	GUID0920
	QQ=QQSO-QQPT	GUID0930
	DO 22 I=1, 3	GUID0940
	DO 21 J=I, 3	GUID0950
	DUN(I, J)=QQ*DUM(I, J)	GUID0960
	DUN(J, I)=DUN(I, J)	GUID0965
21	CONTINUE	GUID0970
	DUN(I, I)=DUN(I, I)+CRUD	GUID0980
22	CONTINUE	GUID0990
	RMSERR=SQRTF(DUN(1, 1)+DUN(2, 2)+DUN(3, 3))	GUID1000
	DO 23 I=1, 3	GUID1010
	II=I+3	GUID1020
	DO 23 J=I, 3	GUID1030
	JJ=J+3	GUID1040
	PAR(II, JJ)=PAR(II, JJ)+DUN(I, J)	GUID1050
	PAR(JJ, II)=PAR(II, JJ)	GUID1060
	P(II, JJ)=P(II, JJ)+DMONIT*DUN(I, J)	GUID1070
	P(JJ, II)=P(II, JJ)	GUID1080
23	CONTINUE	GUID1090
	CALL MATRX(TPAR, PAR, DUN, 3, 6, 6, 1)	GUID1100
	RMSPAP=SQRTF(PAR(1, 1)+PAR(2, 2)+PAR(3, 3))	GUID1105
	RMSPAP=SQRTF(PAR(1, 1)+PAR(2, 2)+PAR(3, 3))	GUID1110
	RMSPAV=SQRTF(PAR(4, 4)+PAR(5, 5)+PAR(6, 6))	GUID1115
	GO TO (28, 29), IGDTP	GUID1120
28	CONTINUE	GUID1125
	RMSMIS=SQRTF(DUN(1, 1)+DUN(2, 2)+DUN(3, 3))	GUID1130
	WRITE OUTPUT TAPE NUTS, 801, RMSERR, RMSPAP, RMSMIS, RMSPAV	GUID1140
801	FORMAT(32H ***GUIDANCE CORRECTION MADE***,	GUID1150
	1/24H RMS ERROR IN CORR.=, E15, 8,	GUID1160
	225H RMS POS DEV FROM NOM.=, E15, 8,	GUID1170
	3/24H RMS MIS AFT CORR.=, E15, 8,	GUID1180
	425H RMS VEL DEV FROM NOM.=, E15, 8)	GUID1190
	GO TO 15	GUID1200
29	CONTINUE	GUID1210
	RMSMIS=SQRTF(DUN(1, 1)+DUN(2, 2))	GUID1220
	RMSVIN=SQRTF(DUN(3, 3))	GUID1230
	WRITE OUTPUT TAPE NUTS, 803, RMSERR, RMSPAP, RMSMIS, RMSPAV, RMSVIN	GUID1240
803	FORMAT(32H ***GUIDANCE CORRECTION MADE***,	GUID1250
	1/24H RMS ERROR IN CORR.=, E15, 8,	GUID1260
	225H RMS POS DEV FROM NOM.=, E15, 8, /	GUID1270
	3/24H RMS POS MIS AFT CORR.=, E15, 8,	GUID1280

GUID (Cont'd)

425H RMS VEL DEV FROM NOM=,E15.8,
5/24H RMS VINF AFT CORR.=,E15.8)
30 CONTINUE
GO TO 15
END

GUID129
GUID130
GUID131
GUID132
GUID

S-215

GUID-13

Page Intentionally Left Blank

Subroutine: HOUR

Purpose: To provide a reading of the printer clock in hours since midnight. This is the STL subroutine RW HOUR.

Calling Sequence:

CALL HOUR(A)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
O	A			hours	Time

Common storages used or required: None

Subroutines required: None

Functions required: None

Approximate number of storages required: 86 cells

Restrictions

Clock advance is suppressed during readout so that elapsed time will be off $.4N$ seconds where N is the number of times the clock is selected.

HOUR will always provide a floating point number if the printer is available. Therefore, a faulty clock or the wrong board will be indicated.

Use

The main application of HOUR is to time cases through use of the FINP "CLOCK" option.

HOUR

FAP

HOUR SUBROUTINE 10-27-31

HOUR

HOUR

ENTRY
CLA
STA
SXA
SXA
TCOA

HOUR
1,4
SSAM
SAMX,4
SAMX+1,2
*

DELAY

RPR
SPRA
SPRA
SPRA

6
9
10

ECHO CHECK
READ CLOCK
SUPPRESS SPACING
AND PRINTING

AXT
STZ
TIX
RCHA
TCOA

24,4
SAMZ+24,4
*-1,4,1
SAMIO
*

TRANSMIT CLOCK READING

STZ
STZ
AXT

SAMZ+18
SAMZ+20
18,4

SAM1

CAL
ORS
LDQ

SAMZ+18,4
SAMZ+18
SAMZ+18

8-4 LEFT ADD ECHOS
AND CONVERT TO
BCD

PXD
AXT

5,2

SAM3

LGL
ALS
TIX
LGL
ACL

1
5
SAM3,2,1
1
SAMZ+20

SLW
TIX
STZ

SAMZ+20
SAM1,4,2
SAMZ+22

AXT
LDQ

6,4
SAMZ+20

SAM4

PXD
LGL
SLW
CLA
ALS

6
SAMZ+23
SAMZ+22
2

ADD
ALS
ADD

SAMZ+22
1
SAMZ+23

STO
TIX
LDQ

SAMZ+22
SAM4,4,1
SAMZZ

DVP
XCL
ORA
FAD

SIX
SA
SA

HOUR000
HOUR001
HOUR002
HOUR003
HOUR004
HOUR005
HOUR006
HOUR007
HOUR008
HOUR009
HOUR010
HOUR011
HOUR012
HOUR013
HOUR014
HOUR015
HOUR016
HOUR017
HOUR018
HOUR019
HOUR020
HOUR021
HOUR022
HOUR023
HOUR024
HOUR025
HOUR026
HOUR027
HOUR028
HOUR029
HOUR030
HOUR031
HOUR032
HOUR033
HOUR034
HOUR035
HOUR036
HOUR037
HOUR038
HOUR039
HOUR040
HOUR041
HOUR042
HOUR043
HOUR044
HOUR045
HOUR046
HOUR047
HOUR048
HOUR049

HOURL (Cont'd)

HOUR0500
HOUR0510
HOUR0520
HOUR0530
HOUR0540
HOUR0550
HOUR0560
HOUR0570
HOUR0580
HOUR0590
HOUR0600
HOUR0610
HOUR0620
HOUR0630
HOUR0640
HOUR0650
HOUR0660

CAS M24

FSB M24

NOP

MOD 24 HOURS
MIDNIGHT ONLY

SSAM STO **0

SAMX AXT **0,4

AXT **0,2

TRA 2,4

EXIT

SAMIO IOCP SAMZ,2+0,26

NON TRANSMIT 26 COPIES

IOCP SAMZ,0,1

27TH COPY 9L ECHO

IOCP SAMZ+1,2,3

NON TRANSMIT 9R,12L,12R

IOCD SAMZ+2,0,16

8L TO 1R ECHOS

SA OCT 214000000000

M24 DEC 24,

SIX DEC 6000B15

SAMZZ PZE

SAMZ BSS 24

END

Subroutine: HPHT

Purpose: To perform the matrix multiplication $(RMS)^2 = H \cdot P \cdot H^T$.
 The square root of $(RMS)^2$ is taken and RMS, which is the standard deviation of the parameter being considered, is output from the subroutine.

Calling Sequence:

CALL HPHT (H, P, RMS)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	H	(1,6)	$\frac{\partial \text{PAR}}{\partial \text{STATE}}$		Parameter Partial Matrix
I	P	(6,6)	$E(\vec{X} \vec{X}^T)$		State Covariance Matrix
O	RMS	1			Standard deviation of parameter due to state variance.

Common storages used or required: None

Subroutines required: None

Functions required: SQRT

Approximate number of storages required:

HPHT

```
* LABEL
* SYMBOL TABLE
SUBROUTINE HPHT(H,P,RMS)
DIMENSION H(6),P(6,6),DUM(6)
DO 1 I=1,6
DUM(I)=0.
DO 1 J=1,6
DUM(I)=DUM(I)+H(J)+P(J,I)
1 CONTINUE
VAR2=0.
DO 2 I=1,6
VAR2=VAR2+DUM(I)+H(I)
2 CONTINUE
RMS=SQRTF(VAR2)
RETURN
END
```

```
HPHT
HPHT
HPHT0000
HPHT0010
HPHT0020
HPHT0030
HPHT0040
HPHT0050
HPHT0060
HPHT0070
HPHT0080
HPHT0090
HPHT0100
HPHT0110
HPHT0120
HPHT
```

Subroutine: INPUT

Purpose: To transform input initial conditions of position and velocity in various coordinate systems to Cartesian coordinates with respect to earth's equator and equinox of 1950. Input may be Cartesian referred to (1) mean equator and equinox, 1950; (2) true equator and equinox of date; (3) earth-fixed or spherical; (4) mean equator and equinox of 1950; (5) true equator and equinox of date; (6) earth-fixed.

Calling Sequence:

CALL INPUT (K, XOUT, VOUT, TW, TF, AN, XIN, VIN)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	K	1			Type of input: K=1 for (1) above, etc.
O	XOUT	3		see following pgs	Position, equinox 1950.0
O	VOUT	3			Velocity, equinox 1950.0
I	TW	1		days	Whole number of days past 1950.
I	TF	1		days	Fractional number of days past TW
O	AN	3,3			Transformation matrix from system (1) to (2)
I	XIN	3		see following pgs	Input position vector
I	VIN	3		see following pgs	Input velocity vector

Common storages used or required:

None

Subroutines required:

ROTEQ, NUTAIT, MULT, RVIN, INV3, GHA, SETN

Functions required:

SIN, COS

Approximate number of storages required:

Input format:For Cartesian coordinates: $[K = 1, 2, 3]$

$$XIN(1) = X$$

$$XIN(2) = Y$$

$$XIN(3) = Z$$

$$VIN(1) = \dot{X}$$

$$VIN(2) = \dot{Y}$$

$$VIN(3) = \dot{Z}$$

For sperical coordinates: $[K = 4, 5, 6]$

$$XIN(1) = R = \text{magnitude of radius vector}$$

$$XIN(2) = \delta = \text{declination (degrees)}$$

$$XIN(3) = \theta = \text{right ascension (degrees)}$$

$$VIN(1) = V = \text{magnitude of velocity}$$

$$VIN(2) = \gamma = \text{flight path angle (degrees)}$$

$$VIN(3) = \sigma = \text{azimuth angle (degrees)}$$

Input Transformations:

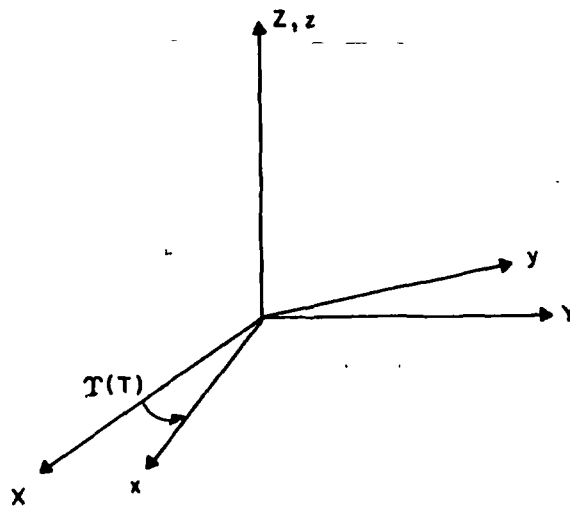
K = 1 The input is in mean equinox of 1950 and no transformation is required

$$\begin{array}{ccc} \vec{X}_{OUT}_{50} & = & \vec{X}_{IN}_{50} \\ 3 \times 1 & & 3 \times 1 \end{array} \quad \begin{array}{ccc} \vec{V}_{OUT}_{50} & = & \vec{V}_{IN}_{50} \\ 3 \times 1 & & 3 \times 1 \end{array}$$

K = 2 Subroutines ROTEQ and NUTAIT are called to obtain the transformation matrix, AN, from mean equator 1950 to true equator of date

$$\begin{array}{ccccc} \vec{X}_{OUT}_{50} & = & (AN)^T & X_{IN}_{DATE} & \\ 3 \times 1 & & 3 \times 3 & 3 \times 1 & \end{array} \quad \begin{array}{ccccc} \vec{V}_{OUT}_{50} & = & (AN)^T & \vec{V}_{IN}_{DATE} & \\ 3 \times 1 & & 3 \times 3 & 3 \times 1 & \end{array}$$

K = 3 The earth fixed Cartesian coordinate system is assumed to rotate with the earth. The X-Y plane is coincident with the earth's true equator of date, the X axis lying in the Greenwich meridian and the Z axis along the earth's spin axis. Subroutine GHA is called with time, T, to obtain the Greenwich hour angle, $\gamma^{(T)}$, of the true vernal equinox of date. The transformations from earth fixed coordinates to true equator of date are the following:



X, Y, Z: TRUE EQUATOR DATE

x, y, z: EARTH FIXED

$$\begin{matrix}
 X \\
 Y \\
 Z
 \end{matrix}
 \begin{matrix}
 \text{DATE} \\
 \text{DATE} \\
 \text{DATE}
 \end{matrix}
 =
 \begin{pmatrix}
 \cos \gamma & -\sin \gamma & 0 \\
 \sin \gamma & \cos \gamma & 0 \\
 0 & 0 & 1
 \end{pmatrix}
 \begin{matrix}
 z \\
 y \\
 z
 \end{matrix}
 \begin{matrix}
 \text{EF} \\
 \text{EF} \\
 \text{EF}
 \end{matrix}$$

3x1

and

$$V_{\text{DATE}} = \begin{pmatrix} \dot{X} \\ \dot{Y} \\ \dot{Z} \end{pmatrix}_{\text{DATE}} = \begin{pmatrix} \cos \gamma & -\sin \gamma & 0 \\ \sin \gamma & \cos \gamma & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \end{pmatrix}_{\text{EF}} +$$

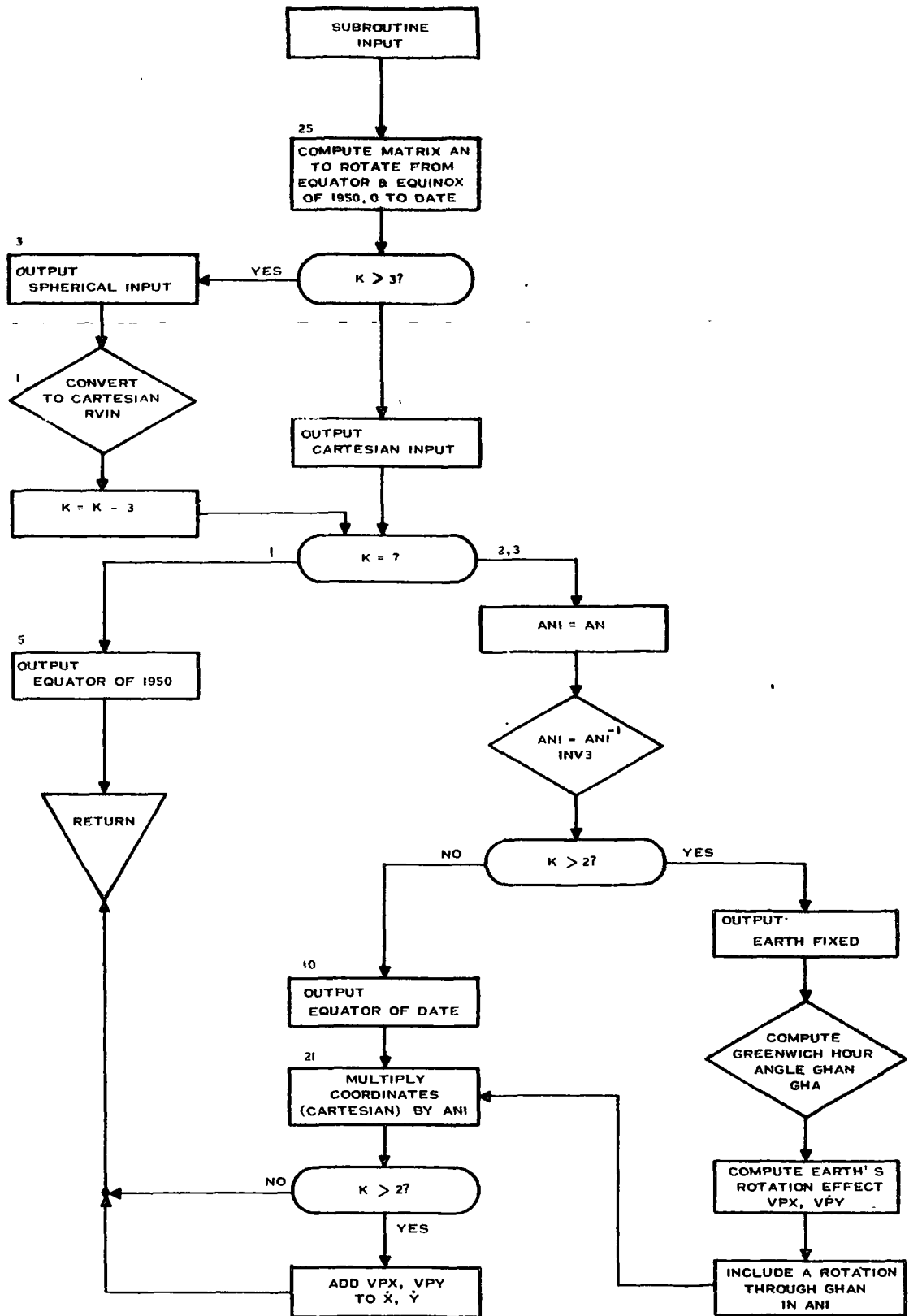
$$\omega \begin{pmatrix} -\sin \gamma & -\cos \gamma & 0 \\ \cos \gamma & -\sin \gamma & 0 \\ 0 & 0 & 0 \end{pmatrix} \begin{pmatrix} x \\ y \\ z \end{pmatrix}_{\text{EF}}$$

where $\omega = \frac{d}{dt}\{\gamma(t)\}$ = earth's rotation rate

Subroutines ROTEQ and NUTAIT are called to obtain the AN transformation which completes the transformation to equator 1950.

$$\begin{matrix} \vec{X}_{\text{OUT}} = (\text{AN})^T \vec{X}_{\text{DATE}} & \vec{V}_{\text{OUT}} = (\text{AN})^T \vec{V}_{\text{DATE}} \\ 3 \times 1 & 3 \times 3 & 3 \times 1 & 3 \times 1 & 3 \times 3 & 3 \times 1 \end{matrix}$$

K = 4, 5, or 6 In each of these cases, subroutine RVIN is called to transform the spherical sets of coordinates to Cartesian coordinates of the same reference frame. Following this spherical to Cartesian conversion, the transformation procedures which are followed for the transformation to 1950 are identical to those described for the corresponding reference frames for K = 1, 2, or 3.



S-227

INPUT-5

INPUT

* LABEL	INPT
* SYMBOL TABLE	INPT
CEC2013. SUBROUTINE INPUT	INPT
SUBROUTINE INPUT(K,X,V,TW,TF,AN,XIN,VIN)	INPT0000
C XIN AND VIN ARE INPUTS, X AND V ARE OUTPUTS IN EQUINOX 1950	INPT0010
C K IS TYPE INPUT (1) EQUATOR 1950; (2) EQUATOR OF DATE (3)	INPT0015
C EARTH-FIXED	INPT0016
C (4),(5),(6), ARE SPHERICAL INPUT RESP,,(1),(2),(3)	INPT0020
DIMENSION X(3),V(3),SP(6),EN(3,3),A(3,3),AN(3,3),ANI(3,3),B(3,3)	INPT0030
DIMENSION XIN(3),VIN(3)	INPT0040
CALL SETN(NIN,NOUT)	INPT0045
TD = TW+TF	INPT0050
DO 25 I=1,3	INPT0060
X(I)=XIN(I)	INPT0070
V(I)=VIN(I)	INPT0080
25 CONTINUE	INPT0090
CALL ROTEG(TD,A)	INPT0100
CALL NUTAIT (TD,OM,CRUD,DDC,EN,EPSIL)	INPT0110
CALL MULT(EN,A,AN,0)	INPT0120
IF (K-3) 4,4,3	INPT0130
4 WRITE OUTPUT TAPE NOUT,15,X,V	INPT0140
15 FORMAT(17H CARTESIAN INPUT 6E17.8)	INPT0150
GO TO 16	INPT0160
3 WRITE OUTPUT TAPE NOUT,17,X,V	INPT0170
17 FORMAT(17H SPHERICAL INPUT 6E17.8)	INPT0180
DO 2 I=1,3	INPT0190
J = I+3	INPT0200
SP(I) = X(I)	INPT0210
2 SP(J) = V(I)	INPT0220
1 CALL RVIN(SP,X,V)	INPT0230
K = K-3	INPT0240
16 DO 12 I=1,3	INPT0250
J = I+3	INPT0260
SP(I) = X(I)	INPT0270
12 SP(J) = V(I)	INPT0280
GO TO (5,7,7), K	INPT0290
5 WRITE OUTPUT TAPE NOUT,18	INPT0300
18 FORMAT(16H EQUATOR OF 1950)	INPT0310
GO TO 13	INPT0320
7 CONTINUE	INPT0330
DO 6 I=1,3	INPT0340
DO 6 J=1,3	INPT0350
6 ANI(I,J) = AN(I,J)	INPT0360
CALL INV3(ANI,3,D)	INPT0370
IF (K-2) 10,10,8	INPT0380
8 DD = EN(2,1)	INPT0390
WRITE OUTPUT TAPE NOUT,20	INPT0400
20 FORMAT(12H EARTH FIXED)	INPT0410
TS = TF*86400.	INPT0420
CALL GHA(TS,TW,GHAN,DD,OMEGA)	INPT0430
OMEGA = OMEGA*.017453296	INPT0440

Page Intentionally Left Blank

Subroutine: INTR, INTRI

Purpose: The purpose of INTR is to interpolate as a function of the central body on the coordinates of the other bodies, to the given time, and return the interpolated position values. The purpose of INTRI is the same as INTR, but in addition it numerically differentiates the positions to obtain the velocities and also return them.

Calling Sequence:

CALL INTR, INTRI (TW, TF, NB, PO, NV, VE, DIS)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	TW	1		whole days	Time in days since 1950.0
I	TF	1		fractional days	Time in fractional days since TW
I	NB	1			Central body
O	PO	22		Km	Array of position values
I	NV	1			Dummy variable
O	VE	22		Km/sec	Array of velocity values
I	DIS	1		Km	Jupiter included if DIS > 10 ⁶

Common storages used or required:

C

Subroutines required:

FIX, FLOAT

Functions required:

Approximate number of storages required: 2063 OCTAL

For interpolation, the following formula is used:

$$y(t) = \left\{ u y_0 + t y_1 \right\} + \left\{ \frac{u(u^2-1)}{3!} \delta^2 y_0 + \frac{t(t^2-1)}{3!} \delta^2 y_1 \right\} \\ + \left\{ \frac{u(u^2-1)(u^2-4)}{5!} \delta^4 y_0 + \frac{t(t^2-1)(t^2-4)}{5!} \delta^4 y_1 \right\}$$

where $y_0 = y(T_j)$

$y_1 = y(T_j + h)$

$h = \text{ephemeris interval}$

$$t = \frac{T - T_j}{h}$$

$u = 1 - t$

$T_j \leq T < T + h$

For the velocity values, the following is used:

$$\dot{y}(T) = \frac{1}{h} \left\{ -y_0 + y_1 \right\} + \frac{1}{h} \left\{ -\frac{3u^2-1}{3!} \delta^2 y_0 + \frac{3t^2-1}{3!} \delta^2 y_1 \right\} \\ + \frac{1}{h} \left\{ -\frac{5u^4-15u^2+4}{5!} \delta^4 y_0 + \frac{5t^4-15t^2+4}{5!} \delta^4 y_1 \right\}$$

The locations of variables in the position and velocity arrays are as follows:

PO(5)	Z value of Jupiter
PO(6)	Y value of Jupiter
PO(7)	X value of Jupiter

PO(8) - PO(10) values of Mars
PO(11) - PO(13) values of Venus
PO(14) - PO(16) values of the Sun
PO(17) - PO(19) values of the Moon
PO(20) - PO(22) values of the Earth

The VE array is arranged the same as the PO array with velocity values in place of positions.

INTR, INTR1

FAP
 TTL JPL EPHEMERIS LOOKUP NEW ERP 6/63
 LBL INTR
 COUNT 530
 ENTRY INTR
 ENTRY INTR1
 REM CALL INTR A,B,C,D,E,F,G POSITIONS AND VELOCITIES
 REM A=ARG INTEGRAL DAYS SINCE 1950.0
 REM B=FRACTION OF DAY
 REM C=CENTRAL BODY 0=EARTH 1=MOON 2=SUN 3=VEN 4=MARS
 REM D=OUTPUT TABLE STARTING ADDRESS
 REM E=IGNORED (VELOCITY OPTION INDICATOR)
 REM F=ADDRESS OF VELOCITY TABLE
 REM G=RADIUS FROM CENTRAL BODY
 REM EPHEMERIS TAPE MUST BE MOUNTED ON A6
 INTR TXL **3,**
 INTR1 SXD VEL,4
 TXL **2,**
 STZ VEL
 CLA 1,4
 STA TAR
 CLA 2,4 FRA
 STA FRA
 CLA 3,4 CEN
 STA CEN
 CLA 4,4 OUP
 STA OUP
 CLA 6,4 VELOCITY
 STA XN,V
 CLA 7,4
 STA RADS
 TAR CLA **
 STO TARG
 FRA CLA **
 STO TARG+1
 CEN CLA **
 ARS 18
 STO CENTER
 RADS CLA **
 STO R
 SXD TRAP,4
 SXD TRAP+1,2
 SXD HELIO-1,1
 CLA VEL
 TNZ NEU : MUST INTERPOLATE TO
 REM OBTAIN VELOCITY
 CLA CENTER
 SUB KERNO
 TNZ NEU : MUST INTERPOLATE FOR
 REM NEW CENTRAL BODY
 CLA TARG

INTR
 INTR0000
 INTR0010
 INTR0020
 INTR0030
 INTR0040
 INTR0050
 INTR0060
 INTR0070
 INTR0080
 INTR0090
 INTR0100
 INTR0110
 INTR0120
 INTR0130
 INTR0140
 INTR0150
 INTR0160
 INTR0170
 INTR0180
 INTR0190
 INTR0200
 INTR0210
 INTR0220
 INTR0230
 INTR0240
 INTR0250
 INTR0260
 INTR0270
 INTR0280
 INTR0290
 INTR0300
 INTR0310
 INTR0320
 INTR0330
 INTR0340
 INTR0350
 INTR0360
 INTR0370
 INTR0380
 INTR0390
 INTR0400
 INTR0410
 INTR0420
 INTR0430
 INTR0440
 INTR0450
 INTR0460
 INTR0470
 INTR0480
 INTR0490

INTR, INTRI(Cont'd)

SUB TARGO
 TNZ NEU
 CLA TARG+1
 SUB TARGO+1
 TZE FLEE+6
 REM
 REM
 REM
 REM
 NEU CLA TARG
 FSB TABLE
 TMI LOOKUP
 STO COM+19
 SUB 20,
 TPL LOOKUP
 CLA COM+19
 FDH 4.
 STQ COM+18
 CLA COM+18
 CALL FIX
 CALL FLOAT
 STO COM+17
 CHS
 FAD COM+18
 STO COM+1
 CLA TARG+1
 FDH 4.
 STQ COM
 CLA COM
 FAD COM+1
 STO TARG+2
 LDQ COM+19
 FMP =9,
 CALL FIX
 ADD KERNO+1
 STA GG
 LDQ COM+17
 FMP =54,
 CALL FIX
 ADD KERNO+2
 STA HH
 AXT 2*SEP,4
 STZ XN+2*SEP,4
 TIX +-1,4,1
 AXT BSEP,4
 STZ KBO+BSEP,4
 TIX +-1,4,1
 LXA CENTER,4
 PXD ,4
 COM
 PDX ,2

TIME HAS CHANGED

ANALYZE TABLE
 NEEDS AS A
 FUNCTION OF
 CENTRAL BODY

POSITION EPHEMERIS TAPE
 T-TO

(T-TO)/4.

MUST INTERPOLATE
 SO CLEAR STORAGE

SET GRAVITATIONAL
 COEFFICIENTS
 TO ZERO

INTR050
 INTR051
 INTR052
 INTR053
 INTR054
 INTR055
 INTR056
 INTR057
 INTR058
 INTR059
 INTR060
 INTR061
 INTR062
 INTR063
 INTR064
 INTR065
 INTR066
 INTR067
 INTR068
 INTR069
 INTR070
 INTR071
 INTR072
 INTR073
 INTR074
 INTR075
 INTR076
 INTR077
 INTR078
 INTR079
 INTR080
 INTR081
 INTR082
 INTR083
 INTR084
 INTR085
 INTR086
 INTR087
 INTR088
 INTR089
 INTR090
 INTR091
 INTR092
 INTR093
 INTR094
 INTR095
 INTR096
 INTR097
 INTR098
 INTR099
 INTR100

NTR, INTRI (Cont'd)

GEO	TXH	HELIO,4,1		INTR1010
	AXT	3,1		INTR1020
	CLA	GRAV+3,1		INTR1030
	STO	KBO+3,1		INTR1040
	TIX	*-2,1,1		INTR1050
	STZ	KBO-1,2		INTR1060
	CLA	EWORTO		INTR1070
	STO	EWORT		INTR1080
	CLA	HWORTE		INTR1090
	STO	HWORT		INTR1100
	TXH	GG12,4,0		INTR1110
	CLA	RJ	TEST FOR	INTR1120
	SUB	R	INCLUSION OF.	INTR1130
	TPL	GG12	JUPITER IF	INTR1140
	CLA	HWORTJ	EARTH IS	INTR1150
	STO	HWORT	CENTRAL BODY	INTR1160
	CLA	GRAV+6		INTR1170
	STO	KB6		INTR1180
	TXL	GG12,,**		INTR1190
HELIO	AXT	BSEP,1		INTR1200
	CLA	GRAV+BSEP,1		INTR1210
	STO	KBO+BSEP,1		INTR1220
	TIX	*-2,1,1		INTR1230
	STZ	KB2-3,2		INTR1240
ORTHO	CLA	EWORTO		INTR1250
	STO	EWORT		INTR1260
	CLA	HWORTO		INTR1270
	STO	HWORT		INTR1280
GG12	CLA	VEL	CHECK	INTR1290
	TZE	GG6	FOR VELOCITY	INTR1300
	CLA	EWORTO	OPTIONS	INTR1310
	STO	EWORT		INTR1320
	CLA	HWORTV		INTR1330
	STO	HWORT		INTR1340
GG6	CLA	EWORT		INTR1350
	TZE	GG+2		INTR1360
	CLA	EVEL		INTR1370
	STO	VEL+1		INTR1380
	CLA	TARG+1	GEOCENTRIC	INTR1390
	TSX	TAB,4	INTERPOLATION	INTR1400
GG	PZE	**,,9		INTR1410
	PZE	XN,,EWORT+1		INTR1420
	CLA	HWORT		INTR1430
	TZE	HH+2		INTR1440
	CLA	HVEL		INTR1450
	STO	VEL+1		INTR1460
	CLA	TARG+2	HELIOCENTRIC	INTR1470
	TSX	TAB,4	INTERPOLATION	INTR1480
HH	PZE	**,,54		INTR1490
	PZE	XN+3,,HWORT+1		INTR1500
RESET	AXT	3,4	PLACE	INTR1510

INTR, INTRI (Cont'd)

CLA XN+6,4
 FDH EVEL
 STQ XN,+18,4
 CLA XN+9,4
 FDH EVEL
 STQ XN,+12,4
 LDQ XN+3,4
 STQ XN+6,4
 FMP MU
 FSB XN+18,4
 STO XN+9,4
 STZ XN+3,4
 LDQ XN,+3,4
 STQ XN,+6,4
 FMP MU
 FSB XN,+18,4
 STO XN,+9,4
 STZ XN,+3,4
 TIX RESET+1,4,1
 LXA CENTER,4
 LXD VEL,2
 TXH RVPRT,2,0
 TXH TESTM,4,0
 NZT KB6
 TRA FLEE
 AXT 3,1
 CLA XN+21,1
 FAD XN+9,1
 STO XN+21,1
 TIX +-3,1,1
 TXL FLEE
 TESTM TXH RVPRT,4,1
 AXT 3,1
 CLS XN+6,1
 STO XN+3,1
 CLA XN+9,1
 FSB XN+6,1
 STO XN+9,1
 STZ XN+6,1
 TIX +-6,1,1
 FLEE CLA CENTER
 STO KERNO
 CLA TARG
 STO TARGO
 CLA TARG+1
 STO TARGO+1
 AXT 21,1
 CLA XN+21,1
 OUP STO **,1
 TIX OUP-1,1,1
 CLA VEL

COORDINATES
 IN OLD
 FORMAT

POSITION OF SUN

VELOCITY OF SUN

IX2 NOT ZERO IF VELOCITY OPTION
 GET COORDINATES FOR PRINTING

EARTH-CENTERED

MOON-CENTERED

TRANSFER POSITIONS

INTR1520
 INTR1530
 INTR1540
 INTR1550
 INTR1560
 INTR1570
 INTR1580
 INTR1590
 INTR1600
 INTR1610
 INTR1620
 INTR1630
 INTR1640
 INTR1650
 INTR1660
 INTR1670
 INTR1680
 INTR1690
 INTR1700
 INTR1710
 INTR1720
 INTR1730
 INTR1740
 INTR1750
 INTR1760
 INTR1770
 INTR1780
 INTR1790
 INTR1800
 INTR1810
 INTR1820
 INTR1830
 INTR1840
 INTR1850
 INTR1860
 INTR1870
 INTR1880
 INTR1890
 INTR1900
 INTR1910
 INTR1920
 INTR1930
 INTR1940
 INTR1950
 INTR1960
 INTR1970
 INTR1980
 INTR1990
 INTR2000
 INTR2010
 INTR2020

INTR, INTRI (Cont'd)

	TZE	OUT	DO NOT TRANSFER VELOCITY	INTR2030
	AXT	21,1		INTR2040
	CLA	XN,+21,1	TRANSFER VELOCITIES	INTR2050
(N.V	STO	**,1		INTR2060
	TIX	XN,V-1,1,1		INTR2070
OUT	LXD	HELIO-1,1		INTR2080
	LXD	TRAP+1,2		INTR2090
	LXD	TRAP,4		INTR2100
	TRA	8,4		INTR2110
	REM	TSX TAB,4	(AC)=INTERPOLATIVE ARGUMENT	INTR2120
	REM	PZE B,,K		INTR2130
	REM	PZE A,,C		INTR2140
	REM		B=START OF DATA BLOCK	INTR2150
	REM		K=WORDS PER SUB BLOCK	INTR2160
	REM		A=START OF RESULT BLOCK	INTR2170
	REM		C=SKIP CODE WORD LOCATION	INTR2180
AB	SXD	COM+9,4		INTR2190
	SXD	COM+8,2		INTR2200
	SXD	COM+7,1		INTR2210
	STO	ARG		INTR2220
	CLA	1,4		INTR2230
	STA	TAB18		INTR2240
	LRS	18		INTR2250
	ADD	1,4		INTR2260
	STA	TAB21		INTR2270
	CLA	2,4		INTR2280
	PAX	,1		INTR2290
	TXI	**+1,1,SEP		INTR2300
	SXA	TAB29,1		INTR2310
	ARS	18		INTR2320
	STA	VELOP		INTR2330
	AXT	2,1		INTR2340
	CLA	VEL		INTR2350
	TNZ	VELOP		INTR2360
	TXI	VELOP,1,-1		INTR2370
VELOP	CLA	**,1	PICK UP SKIP	INTR2380
	STO	VEL+2	CODE WORD	INTR2390
	TXL	POSOP,1,1		INTR2400
	REM		VELOCITY OPTION	INTR2410
	CLA	ARG		INTR2420
	TSX	COEFF.,4	FORM THE	INTR2430
	AXT	3,4	E1(2J).	INTR2440
	CLS	COM+13,4		INTR2450
	STO	COM+16,4		INTR2460
	TIX	*-2,4,1		INTR2470
	CLA	1,	FORM THE	INTR2480
	FSB	ARG	E0(2J).	INTR2490
	TSX	COEFF.,4		INTR2500
	TRA	TAB1-1		INTR2510
	REM		POSITION OPTION	INTR2520
OSOP	CLA	ARG		INTR2530

INTR, INTRI (Cont'd)

	TSX	COEFF, 4	FORM THE	INTR254
	AXT	3, 4	E1(2J)	INTR255
	CLA	COM+13, 4		INTR256
	STO	COM+16, 4		INTR257
	TIX	*-2, 4, 1		INTR258
	CLA	1.	FORM THE	INTR259
	FSB	ARG	E0(2J)	INTR260
	TSX	COEFF, 4		INTR261
	LXA	TAB29, 4		INTR262
	TXI	**+1, 4, -SEP		INTR263
	SXA	TAB29, 4		INTR264
	SXD	COM+4, 1		INTR265
TAB1	AXT	0, 3		INTR266
	LDQ	VEL+2		INTR267
	PXD			INTR268
	LGL	2.		INTR269
	PAX	, 4		INTR270
	STQ	VEL+2		INTR271
	CAL	=03		INTR272
	ORS	VEL+2		INTR273
	TXH	END, 4, 2		INTR274
	TXH	FORT, 4, 0		INTR275
	TXI	**+1, 1, -3		INTR276
	TXI	TAB1+1, 2, -1		INTR277
FORT	AXT	3, 4		INTR278
TAB18	LDQ	**, 1	X(0)	INTR279
	FMP	COM+13, 4		INTR280
	STO	COM		INTR281
TAB21	LDQ	**, 1	X(1)	INTR282
	FMP	COM+16, 4		INTR283
	FAD	COM		INTR284
	STO	COM+4, 4		INTR285
	TXI	**+1, 1, -1		INTR286
	TIX	*-8, 4, 1		INTR287
	FAD	COM+2		INTR288
	FAD	COM+1		INTR289
TAB29	STO	**, 2	X(T)	INTR290
	TXI	TAB1+1, 2, -1		INTR291
END	LXD	COM+4, 1		INTR292
	TIX	VELOP, 1, 1		INTR293
	LXD	COM+9, 4		INTR294
	LXD	COM+8, 2		INTR295
	LXD	COM+7, 1		INTR296
	TRA	3, 4		INTR297
COEFF	STO	COM+10	CALCULATE	INTR298
	LDQ	COM+10	POSITION	INTR299
	FMP	COM+10	COEFFICIENTS	INTR300
	STO	COM+12	FOR EVERETT, S	INTR301
	FSB	1.	INTERPOLATION	INTR302
	FDH	6.	FORMULA	INTR303
	FMP	COM+10		INTR304

INTR, INTRI (Cont'd)

STO COM+11
 CLA COM+12
 FSB 4.
 FDH 20.
 FMP COM+11
 STO COM+12
 TRA 1,4
 COEFF, STO COM
 CLS 1.
 FDH VEL+1
 STQ COM+10
 LDQ COM
 FMP COM
 STO COM+12
 XCA
 FMP 3.
 FSB 1.
 FDH 6.
 FMP COM+10
 STO COM+11
 CLA COM+12
 FSB 3.
 XCA
 FMP 5.
 XCA
 FMP COM+12
 FAD 4.
 FDH 120.
 FMP COM+10
 STO COM+12
 TRA 1,4
 RVPRT AXT 0,2
 AXT 3,5
 CLA XN+9,2
 FAD XN+9,4
 STO XN+9,2
 CLA VEL
 TZE ++4
 CLA XN,+9,2
 FAD XN,+9,4
 STO XN,+9,2
 TXI ++1,2,-1
 TIX RVPRT+2,4,1
 TXH RVPRT+1,2,9-SEP
 CLA CENTER
 ALS 1
 ADD CENTER
 PAC ,4
 CLA XN,4
 STO COM+3,1
 CLA XN,,4

CALCULATE
 VELOCITY
 COEFFICIENTS
 FOR EVERETT,S
 INTERPOLATION
 FORMULA

EXPRESS ALL
 BODIES GEOCENTRICALLY

BUFFER
 CENTRAL
 BODY

INTR3050
 INTR3060
 INTR3070
 INTR3080
 INTR3090
 INTR3100
 INTR3110
 INTR3120
 INTR3130
 INTR3140
 INTR3150
 INTR3160
 INTR3170
 INTR3180
 INTR3190
 INTR3200
 INTR3210
 INTR3220
 INTR3230
 INTR3240
 INTR3250
 INTR3260
 INTR3270
 INTR3280
 INTR3290
 INTR3300
 INTR3310
 INTR3320
 INTR3330
 INTR3340
 INTR3350
 INTR3360
 INTR3370
 INTR3380
 INTR3390
 INTR3400
 INTR3410
 INTR3420
 INTR3430
 INTR3440
 INTR3450
 INTR3460
 INTR3470
 INTR3480
 INTR3490
 INTR3500
 INTR3510
 INTR3520
 INTR3530
 INTR3540
 INTR3550

INTR, INTRI (Cont'd)

	STO	COM+6,1		INTR356
	TXI	++1,4,-1		INTR357
	TIX	*-5,1,1		INTR358
RVPRT1	AXT	0,2	EXPRESS ALL	INTR359
	AXT	3,4	BODIES IN TERMS	INTR360
	CLA	XN,2	OF THE CENTRAL	INTR361
	FSB	COM+3,4	BODY	INTR362
	STO	XN,2		INTR363
	CLA	VEL		INTR364
	TZE	++4		INTR365
	CLA	XN,,2		INTR366
	FSB	COM+6,4		INTR367
	STO	XN,,2		INTR368
	TXI	++1,2,-1		INTR369
	TIX	RVPRT1+2,4,1		INTR370
	TXH	RVPRT1+1,2,-SEP		INTR371
	TXL	FLEE		INTR372
LOOKUP	CLA	TLAST		INTR373
	FSB	TARG		INTR374
	TNZ	++2		INTR375
	TRA	ERR1		INTR376
	TMI	*-1		INTR377
	CLA	TARG		INTR378
	FSB	TFIRST		INTR379
	TPL	++2		INTR380
	TRA	ERR1		INTR381
	FDH	20,		INTR382
	XCA			INTR383
	CALL	FIX		INTR384
	CALL	FLOAT		INTR385
	XCA			INTR386
	FMP	20,		INTR387
	FAD	TFIRST		INTR388
	STO	COM+1	TIME ON RECORD	INTR389
	CLA	TABLE		INTR390
	FSB	COM+1		INTR391
	TMI	FINDIT		INTR392
	FDH	20,		INTR393
	XCA			INTR394
	CALL	FIX		INTR395
	ADD	1F	RECORDS TO	INTR396
	PAX	,4	BE BACKED	INTR397
	TEFA	++1		INTR398
	TXL	++3,4,20	OVER	INTR399
	REWA	6		INTR400
	TRA	FINDIT		INTR401
	BSRA	6		INTR402
	TIX	*-1,4,1		INTR403
FINDIT	AXT	10,2		INTR404
	SDHA	6		INTR405
	RTBA	6		INTR406

INTR, INTRI (Cont'd)

	RCHA	IO		INTR4070
	TCOA	*		INTR4080
	TEFA	ERR1		INTR4090
	CLA	TABLE		INTR4100
	SUB	COM+1		INTR4110
	TMI	++2		INTR4120
	TNZ	LOOKUP	TAPE NOT POSITIONED PROPERLY	INTR4130
	TNZ	FINDIT		INTR4140
	AXT	513,4		INTR4150
	CAL	TABLE	CHECK	INTR4160
	ACL	A+513,4	SUM	INTR4170
	TIX	*-1,4,1		INTR4180
	TRCA	BSRA		INTR4190
	LAS	C		INTR4200
	TRA	++2		INTR4210
	TRA	SCALE		INTR4220
3SRA	BSRA	6		INTR4230
	TIX	FINDIT+1,2,1		INTR4240
	CALL	ERP		INTR4250
IO	IOCD	TABLE,,515		INTR4260
ERR1	CALL	ERPT		INTR4270
	PZE	TARG		INTR4280
	REM		SCALING	INTR4290
	REM		LOOP	INTR4300
SCALE	AXT	189,4		INTR4310
	LDQ	A+189,4	SCALE	INTR4320
	FMP	SCALE1	GEOCENTRIC	INTR4330
	STO	A+189,4	EPHEMERIS	INTR4340
	TIX	*-3,4,1		INTR4350
	AXT	324,4		INTR4360
	LDQ	B+324,4	SCALE	INTR4370
	FMP	SCALE2	HELIOCENTRIC	INTR4380
	STO	B+324,4	EPHEMERIS	INTR4390
	TIX	*-3,4,1		INTR4400
	CLA	GRAV	COMPUTE	INTR4410
	FAD	GRAV+1	MASS RATIO	INTR4420
	STO	COM	OF MOON	INTR4430
	CLA	GRAV+1	TO EARTH-MOON	INTR4440
	FDH	COM	BARYCENTER	INTR4450
	STQ	MU	FOR POSITION OF EARTH	INTR4460
	TRA	NEU		INTR4470
SCALE1	DEC	6378.150	EARTH RADIUS	INTR4480
SCALE2	DEC	149598500.	ASTRONOMICAL UNIT (JPL, JULY 1961	INTR4490
IFIRST	DEC	3892.0	0 HR AUG 28, 1960 JD = 2437174,5	INTR4500
FLAST	DEC	7292.0	0 HR DEC 19, 1969 JD = 2440554,5	INTR4510
TRAP	PZE			INTR4520
	PZE			INTR4530
RJ	DEC	1E6	JUPITER TEST DISTANCE	INTR4540
TEMPDT	DEC	34,	E.T.=U.T.	INTR4550
	PZE			INTR4560
GRAV	DEC	3.98602E5	EARTH	INTR4570

INTR, INTRI (Cont'd)

DEC	4.8983349E3	MOON	INTR458
DEC	1.3252312E11	SUN	INTR459
DEC	3.2429889E5	VENUS	INTR460
DEC	4.2915518E4	MARS	INTR461
DEC	0	REMOVE BARYCENTER	INTR462
DEC	1.2652701E8	JUPITER	INTR463
EVEL	DEC 86400.		INTR464
HVEL	DEC 345600.		INTR465
MU	PZE	MASS RATIO OF MOON TO BARYCENTER	INTR466
OCT	000000520052	MARS, JUPITER VELOCITY	INTR467
HWORT	OCT 0		INTR468
OCT	527777777777	MOON VELOCITY	INTR469
OCT	0		INTR470
HWORTJ	OCT 000000005252	BARYCENTER, JUPITER	INTR471
HWORTE	OCT 000000005200	BARYCENTER	INTR472
EWORTO	OCT 527777777777		INTR473
HWORTO	OCT 000052525252		INTR474
HWORTV	OCT 525252525252		INTR475
TARGO	DEC 20.,.0	FORMER TIME	INTR476
KERNO	PZE	FORMER CENTER	INTR477
PZE	A	GEOCENTRIC REFERENCE	INTR478
PZE	B	HELIOCENTRIC REFERENCE	INTR479
ARG	PZE 0		INTR480
1F	DEC 1		INTR481
1.	DEC 1.		INTR482
3.	DEC 3.		INTR483
4.	DEC 4.		INTR484
5.	DEC 5.		INTR485
6.	DEC 6.		INTR486
20.	DEC 20.		INTR487
120.	DEC 120.		INTR488
86400.	DEC 86400.		INTR489
VEL	BSS 3	VELOCITY OPTION,H,SKIP CODE:	INTR490
*			INTR491
TABLE	DEC 0	RESERVE.	INTR492
A	BSS 189	FOR	INTR493
B	BSS 324	WORKING	INTR494
C	BSS 1	EPHEMERIS	INTR495
*			INTR496
TARG	PZE		INTR497
PZE			INTR498
PZE			INTR499
CENTER	PZE		INTR500
COM	BSS 21		INTR501
VAFLG	PZE		INTR502
FQFLG	BSS 3		INTR503
KB0	PZE		INTR504
KB1	PZE		INTR505
KB2	PZE		INTR506
KB3	PZE		INTR507
KB4	PZE		INTR508

INTR, INTRI (Cont'd)

KB5	PZE	
KB6	PZE	
XN	BSS	21
XN.	BSS	21
T	PZE	
	PZE	
R	PZE	
BSEP	SYN	7
SEP	SYN	XN ₁ - XN
	END	

INTR5090
INTR5100
INTR5110
INTR5120
INTR5130
INTR5140
INTR5150
INTR5160
INTR5170
INTR

Subroutine: INV3

Purpose: To invert a matrix of any dimension up to a 6 by 6.

Calling Sequence:

CALL INV3 (A, N, DETERM)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
IO	A	6,6			A(I) Matrix to be inverted
					A(O) Inverse of input matrix
I	N	1			Dimension of input matrix
O	DETERM	1			Matrix determinant

Common storages used or required: None

Subroutines required: None

Functions required: ABS

Approximate number of storages required:

INV3

```

* LABEL INV3
C SUBROUTINE FOR INVERTING SQUARE MATRICES WHICH ARE 6 BY 6 OR LESS INV30000
C (TO INVERT LARGER MATRICES, SAY M BY M, DIMENSION IPIVOT(M), A(M*M), INV30010
C INDEX(M,2), PIVOT(M) AND RECOMPILE) INV30020
C A IS THE SQUARE MATRIX TO BE INVERTED INV30030
C N IS THE SIZE OF A (A IS AN N BY N MATRIX) INV30040
C THE SUBROUTINE RETURNS A INVERSE IN PLACE OF A AND THE DETERMINANT INV30050
C IN DETERM. INV30060
SUBROUTINE INV3(A,N,DETERM) INV30070
DIMENSION IPIVOT(6), A(36), INDEX(6,2), PIVOT(6) INV30080
EQUIVALENCE (IROW,JROW), (ICOLUM,JCOLUM), (AMAX,T,SWAP) INV30090
DETERM=1.0 INV30100
DO 20 J=1,N INV30110
20 IPIVOT(J)=0 INV30120
DO 550 I=1,N INV30130
AMAX=0.0 INV30140
DO 105 J=1,N INV30150
IF(IPIVOT(J)-1) 60,105,60 INV30160
60 DO 100 K=1,N INV30170
IF(IPIVOT(K)-1) 80,100,740 INV30180
80 M = N*(K-1)+J INV30190
IF (ABSF(AMAX)-ABSF(A(M))) 85,100,100 INV30200
85 IROW=J INV30210
ICOLUM=K INV30220
AMAX = A(M) INV30230
100 CONTINUE INV30240
105 CONTINUE INV30250
IPIVOT(ICOLUM)=IPIVOT(ICOLUM)+1 INV30260
IF(IROW-ICOLUM) 140,260,140 INV30270
140 DETERM=-DETERM INV30280
DO 200 L=1,N INV30290
M = N*(L-1) INV30300
M1 = M+ICOLUM INV30310
M = M+IROW INV30320
SWAP = A(M) INV30330
A(M) = A(M1) INV30340
200 A(M1) = SWAP INV30350
260 INDEX(I,1)=IROW INV30360
INDEX(I,2)=ICOLUM INV30370
M = N*(ICOLUM-1)+ICOLUM INV30380
PIVOT(I) = A(M) INV30390
DETERM=DETERM*PIVOT(I) INV30400
A(M) = 1.0 INV30410
DO 350 L=1,N INV30420
M = N*(L-1)+ICOLUM INV30430
350 A(M) = A(M)/PIVOT(I) INV30440
DO 550 L1=1,N INV30450
IF(L1-ICOLUM) 400,550,400 INV30460
400 M = N*(ICOLUM-1)+L1 INV30470
T = A(M) INV30480
A(M) = 0. INV30490

```

INV3 (Cont'd)

```

DO 450 L=1,N
M = N*(L-1)
M1 = M+ICOLUM
M = M+L1
450 A(M) = A(M)-A(M1)*T
550 CONTINUE
DO 710 I=1,N
L=N+1-I
IF(INDEX(L,1)=INDEX(L,2)) 630,710,630
630 JROW=INDEX(L,1)
JCOLUM=INDEX(L,2)
M = N*(JROW-1)
M1 = N*(JCOLUM-1)
DO 705 K=1,N
M = M+1
M1 = M1+1
SWAP = A(M)
A(M) = A(M1)
A(M1) = SWAP
705 CONTINUE
710 CONTINUE
740 RETURN
END

```

```

INV3050
INV3051
INV3052
INV3053
INV3054
INV3055
INV3056
INV3057
INV3058
INV3059
INV3060
INV3061
INV3062
INV3063
INV3064
INV3065
INV3066
INV3067
INV3068
INV3069
INV3070
INV3071
INV3

```

Page Intentionally Left Blank

Subroutine: INVAO

Purpose: To form the inverse of a transition matrix for a linear, conservative dynamic system. If Φ is a partitioned matrix such as

$$\Phi = \begin{pmatrix} \Phi_1 & \Phi_2 \\ \Phi_3 & \Phi_4 \end{pmatrix} \text{ then INVAO computes } \Phi^{-1} = \begin{pmatrix} \Phi_4^T & -\Phi_2^T \\ -\Phi_3^T & \Phi_1^T \end{pmatrix}$$

Calling Sequence:

CALL INVAO (AO, AOI)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	AO	6,6	$\Phi(t_2, t_1)$		Transition Matrix
O	AOI	6,6	$\Phi^{-1}(t_2, t_1)$		Inverse Transition Matrix

Common storages used or required: None

Subroutines required: None

Functions required: None

Approximate number of storages required: _____

INVAO

```

* LABEL
* SYMBOL TABLE
SUBROUTINE INVAO(AO,AOI)
DIMENSION AO(6,6),AOI(6,6)
DO 1 I=1,3
  II=I+3
  DO 1 J=1,3
    JJ=J+3
    AOI(I,J)=AO(JJ,II)
    AOI(II,J)=-AO(JJ,I)
    AOI(II,JJ)=AO(J,I)
1  AOI(I,JJ)=-AO(J,II)
RETURN
END

```

```

INVA
INVA
INVA0000
INVA0010
INVA0020
INVA0030
INVA0040
INVA0050
INVA0060
INVA0070
INVA0080
INVA0090
INVA0100
INVA

```


LOADO

```

* LABEL
* SYMBOL TABLE
SUBROUTINE LOADO(AC)
COMMON T
DIMENSION T(1360),AO(6,6)
K=6
JJ=27
DO1 I=1,6
DO 1 J=1,3
K=K+1
KK=J+3
JJ=JJ+1
AO(KK,I)=T(JJ)
AO(J,I)=T(K)
1 CONTINUE
RETURN
END

```

```

LOAD
LOAD
LOAD0000
LOAD0010
LOAD0020
LOAD0030
LOAD0040
LOAD0050
LOAD0060
LOAD0070
LOAD0080
LOAD0090
LOAD0100
LOAD0110
LOAD0120
LOAD0130
LOAD

```

Subroutine: LOADT

Purpose: To place unit initial conditions in the T block for the
variational equations which are being used to generate the transition matrix.

Calling Sequence:

CALL LOADT

Input and Output

Common storages used or required:	T
Subroutines required:	None
Functions required:	None
Approximate number of storages required:	

LOADT

```

* LABEL
* SYMBOL TABLE
SUBROUTINE LOADT
C SUBROUTINE LOADT PUTS UNIT ICS ON PERTURBATION EQUATIONS
COMMON T
DIMENSION T(1360),X(3,6),V(3,6)
EQUIVALENCE (T(7), X),(T(28),V)
DO 2 I=1,3
L=I+3
DO 1 J=1,3
K=J+3
X(I,J)=0.
V(I,K)=0.
X(I,K)=0.
V(I,J)=0.
1 CONTINUE
X(I,I)=1.
V(I,L)=1.
2 CONTINUE
RETURN
END

```

```

LOAT
LOAT
LOAT0000
LOAT0010
LOAT0020
LOAT0030
LOAT0040
LOAT0050
LOAT0060
LOAT0070
LOAT0080
LOAT0090
LOAT0100
LOAT0110
LOAT0120
LOAT0130
LOAT0140
LOAT0150
LOAT0160
LOAT0170
LOAT

```

Subroutine: MASS

Purpose: To find the relevant gravitational constants to be used in computing planetary perturbations for a given central body. MASS also chooses the initial integration step size as a function of central body.

Calling Sequence:

CALL MASS (NOR, UM, VKB, X, ACCP)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	NOR	1			Central Body Indicator.
					1=Earth; 2, Moon; 3, Sun; 4, Venus; 5, Mars; 6, Jupiter
I	UM	6	μ_i	Km ³ /sec ²	Gravitational constants, arranged as above
O	VKB	6	μ_i	Km ³ /sec ²	μ_i for bodies
I	X	3	X, Y, Z	Km	Position coordinates
O	ACCP	1		seconds	Initial integration step size

Common storages used or required: None

Subroutines required: None

Functions required: FNORM

Approximate number of storages required: _____

Method of Establishing Integration Step Size and Perturbing Bodies

Central Body	Integration Step Size	Other Bodies to be Considered
Earth	60.0	Moon, Sun. If $ X \geq 10^6$ Km, Jupiter.
Moon	60.0	Earth, Sun.
Sun	43200.0	All
Venus, Mars, Jupiter	60.0	All

The bodies which are not to be used in calculation of perturbation accelerations are eliminated from consideration by placing zeros in array VKB(6). For the bodies which are being considered, the appropriate gravitational constant is placed in VKB(6).

MASS

```

* LABEL
* SYMBOL TABLE
SUBROUTINE MASS(NOR,UM,VKB,X,ACCP)
DIMENSION UM(6),VKB(6),X(3)
N = NOR
DO 1 I=1,6
1 VKB(I) = 0.
GO TO (2,3,6,4,4,4),N
2 VKB(2) = UM(2)
ACCP = 60.
DIS = FNORM(X)
VKB(3) = UM(3)
IF (DIS=10.000000.) 11,10,10
10 VKB(6) = UM(6)
GO TO 12
11 VKB(6) = 0.
12 RETURN
3 VKB(1) = UM(1)
VKB(3) = UM(3)
ACCP = 60.
RETURN
6 ACCP = 43200.
GO TO 7
4 ACCP = 60.
7 DO 5 I=1,6
5 VKB(I) = UM(I)
VKB(N) = 0.
RETURN
END

```

```

MASS
MASS
MASS000
MASS001
MASS002
MASS003
MASS004
MASS005
MASS006
MASS007
MASS008
MASS009
MASS010
MASS011
MASS012
MASS013
MASS014
MASS015
MASS016
MASS017
MASS018
MASS019
MASS020
MASS021
MASS022
MASS023
MASS024
MASS025
MASS

```

Page Intentionally Left Blank

Subroutine: MATRX

Purpose: To perform matrix multiplications of matrices with any dimensions up to maximum dimensions of 10 by 10. A zero in the call sequence (J) yields an output matrix $C = A \cdot B$. A one in the call sequence (J) yields an output matrix $C = A \cdot B \cdot A^T$. The matrix products are obtained in double precision.

Calling Sequence:

CALL MATRX (A, B, C, NRA, NCA, NCB, J)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	A	(10,10)			Input Matrix
I	B	(10,10)			Input Matrix
O	C	(10,10)			Output Matrix
I	NRA	1			Number of Rows of A
I	NCA	1			Number of Columns of A
I	NCB	1			Number of Columns of B
I	J	1			Type of multiplication desired

Common storages used or required:

None

Subroutines required:

None

Functions required:

None

Approximate number of storages required:

MATRIX

* LABEL	MATX
* SYMBOL TABLE	MATX
CEC2000 SUBROUTINE MATRX	MATX
SUBROUTINE MATRX(A,B,C,NRA,NCA,NCB,J)	MATX0000
C J=0 A*B=C	MATX0010
C J=1 A*B*AT=C T MEANS TRANSPOSE	MATX0020
C NRA=NUMBER OF ROWS OF A	MATX0030
C NCA=COLUMNS OF A	MATX0040
C NCB=COLUMNS OF B	MATX0050
C ACCUMULATION OF PRODUCTS IN DOUBLE PRECISION	MATX0060
DIMENSION A(100),B(100),C(100),D(100)	MATX0080
D DUD=0.	MATX0090
D DUM=0.	MATX0100
DO 1 I=1,NRA	MATX0110
DO 1 K=1,NCB	MATX0120
NC=I+(K-1)*NRA	MATX0130
D CRUD=0.	MATX0140
DO 2 L=1,NCA	MATX0150
NA=I+(L-1)*NRA	MATX0160
NB=L+(K-1)*NCA	MATX0170
DUD=A(NA)	MATX0180
DUM=B(NB)	MATX0190
D CRUD=CRUD+DUD*DUM	MATX0200
2 CONTINUE	MATX0210
D(NC)=CRUD	MATX0220
1 CONTINUE	MATX0230
IF(J)3,3,4	MATX0240
3 CONTINUE	MATX0250
KK=NCB*NRA	MATX0260
DO 5 I=1,KK	MATX0270
5 C(I)=D(I)	MATX0280
GO TO 10	MATX0290
4 CONTINUE	MATX0300
DO 6 I=1,NRA	MATX0310
DO 6 K=1,NRA	MATX0320
NC=I+(K-1)*NRA	MATX0340
D CRUD=0.	MATX0350
DO 7 L=1,NCA	MATX0360
NA=I+(L-1)*NRA	MATX0370
NB=K+(L-1)*NRA	MATX0380
DUM=D(NA)	MATX0390
DUD=A(NB)	MATX0400
D CRUD=CRUD+DUM*DUD	MATX0410
7 CONTINUE	MATX0420
C(NC)=CRUD	MATX0430
6 CONTINUE	MATX0440
10 CONTINUE	MATX0510
RETURN	MATX0520
END	MATX

Subroutine: MATSUB

Purpose: The subroutine is primarily logic which controls (1) trajectory and data printout, (2) updating of the state covariance matrix for observations by calling subroutines EARTR, ONBTR, and MONBTR, and (3) updating of the guidance covariance matrix by calling subroutine GUID.

Calling Sequence:

CALL MATSUB

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I					Quantities obtained from common
O					Quantities returned to common

Common storages used or required:

T, S, C, IC

Subroutines required:

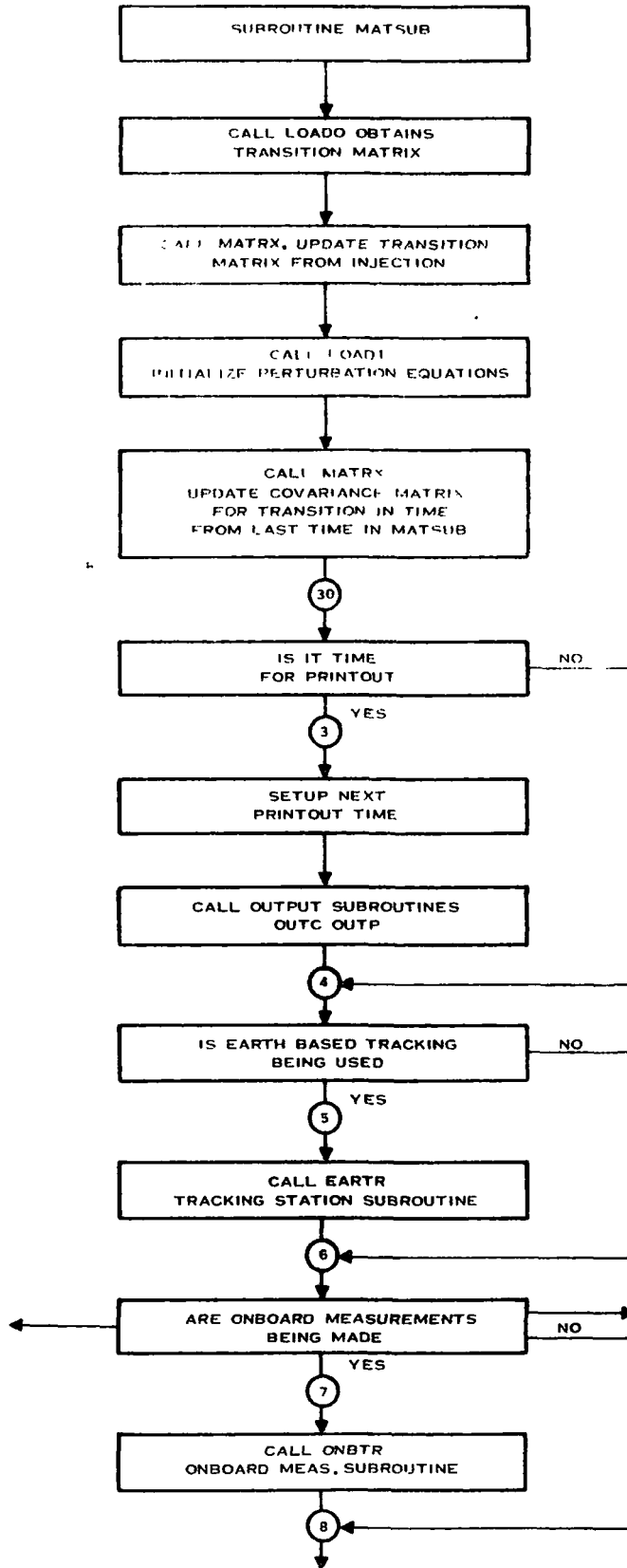
EARTR, GUID, INVAO, LOADO, LOADT, MATRX, MONBTR, ONBTR, OUTC, OUTP

Functions required:

SQRT (FIL) (STH)

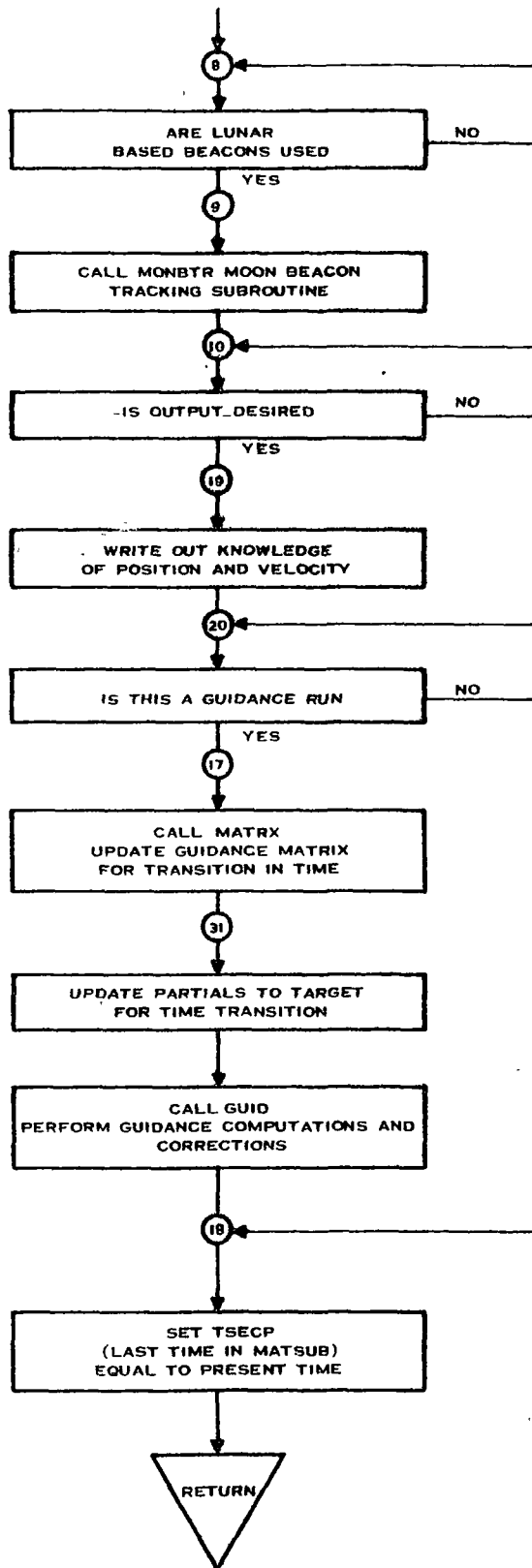
Approximate number of storages required:

346 DEC



MATSUB -2

S-262



* LABEL	MATS
* SYMBOL TABLE	MATS
CEC2006 SUBROUTINE MATSUB	MATS
SUBROUTINE MATSUB	MATS0000
COMMON T,S,C,IC	MATS0010
DIMENSION T(1360),S(1000),C(1000),IC(1),AN(3,3),PO(22),VE(22),	MATS0020
1EM(3,3),XP(3),VXP(3),EA(3,3),XED(3),VED(3),AO(6,6),P(6,6),	MATS0030
2TFTA(3,6),PFTA(6,6),AOS(6,6),AOI(6,6)	MATS0040
EQUIVALENCE (T ,TDUM),(S ,SDUM),(C ,CDUM),	MATS0050
1(C(138),AN),(C(13),TP1),(C(14),TP2),(C(62),PO),(C(84),VE),	MATS0060
2(C(120),EM),(C(650),TPRINT),(C(651),TSTRT),(C(30),TSEC),	MATS0070
3(C(15),XP),(C(18),VXP),(C(10),TW),(C(11),TF) ,(C(129),EA),	MATS0080
4(C(652),P),(C(752),AOS),(C(850),AOI)	MATS0090
5,(C(460),PFTA),(C(568),TFTA),(C(647),TOUT)	MATS0100
EQUIVALENCE (IC(2),IOR),(IC(7),KOUT),(IC(6),ITARG),(IC(9),LPRINT),	MATS0110
1(IC(190),LSTAT),(IC(191),LONB),(IC(192),LMB),(IC(193),IGUID),	MATS0120
2(IC(214),NOUT),(C(649),TSECP)	MATS0130
CALL SETN(NIN,NUTS)	MATS0131
NOUT=1	MATS0140
CALL LOADU(AO)	MATS0145
CALL MATRX(AO,AOS,AOS,6,6,6,0)	MATS0150
CALL LOADT	MATS0155
CALL MATRX(AO,P,P,6,6,6,1)	MATS0160
DO 30 I=1,6	MATS0165
DO 30 J=I,6	MATS0170
P(I,J)=(P(I,J)+P(J,I))/2.	MATS0175
P(J,I)=P(I,J)	MATS0180
30 CONTINUE	MATS0185
IF(TOUT=TSEC) 3,3,4	MATS0220
3 CONTINUE	MATS0230
TOUT=TOUT+TPRINT	MATS0240
NOUT=2	MATS0250
C NOUT IS USED TO INDICATE OTHER OUTPUT WANTED WHEN = 2	MATS0260
CALL OUTC	MATS0270
CALL OUTP	MATS0280
4 CONTINUE	MATS0290
C LSTAT IS SET 2 BY INPUT CARDS IF ANY EARTH BASED TRACKING	MATS0300
LSTAT=LSTAT	MATS0310
GO TO (6,5),LSTAT	MATS0320
5 CONTINUE	MATS0330
CALL EARTH	MATS0340
C EARTH UDDATS COV MATRIX P FOR EARTH BASED TRACKING	MATS0350
6 CONTINUE	MATS0360
LONB=LONB	MATS0370
GO TO (8,7),LONB	MATS0380
C LONB IS SET 2 BY INPUT CARDS IF ANY ONBOARD MEASUREMENTS MADE	MATS0390
7 CONTINUE	MATS0400
C ONBTR UPDATES COV MATRIX P FOR THE ONBOARD MEASUREMENTS	MATS0410
CALL ONBTR	MATS0420
8 CONTINUE	MATS0430
LMB=LMB	MATS0440

MATSUB (Cont'd)

	GO TO (10,9),LMB	MATS045
C	LMB IS SET 2 BY INPUT CARDS IF MOON BASED BEACONS USED	MATS046
	9 CONTINUE	MATS047
	CALL MONBTR	MATS048
C	MONBTR UPDATS COV MATRIX P FOR BEACONS ON MOON	MATS049
	10 CONTINUE	MATS050
	GO TO (20,19), NOUT	MATS051
	19 CONTINUE	MATS052
	RMSP=SQRTF (P (1,1)+P (2,2)+P (3,3))	MATS053
	RMSVP=SQRTF(P (4,4)+P (5,5)+P (6,6))	MATS054
	WRITE OUTPUT TAPE :NUTS,700,RMSP,RMSVP	MATS055
700	FORMAT(42H KNOWLEDGE OF STATE AFTER ALL OBSERVATIONS,/ 124H RMS POSITION=,E15.8,25H RMS VELOCITY=, 2E15.8)	MATS056
	20 CONTINUE	MATS058
	NUMBERS 11-16 RESERVED FOR FUTURE MEASUREMENTS	MATS059
C	IGUID=IGUID	MATS060
	GO TO (18,17),IGUID	MATS061
C	IGUID IS SET BY INPUT TO MAIN PROGRAM IF GUIDANCE CALCULATIONS ARE MADE	MATS062
C	17 CONTINUE	MATS063
	CALL MATRX(AO,PFTA,PFTA,6,6,6,1)	MATS064
	DO 31 I=1,6	MATS065
	DO 31 J=I,6	MATS066
	PFTA(I,J)=(PFTA(I,J)+PFTA(J,I))/2.	MATS067
	PFTA(J,I)=PFTA(I,J)	MATS067
31	CONTINUE	MATS068
	CALL INVAO(AO,AOI)	MATS068
	CALL MATRX(TFTA,AOI,TFTA,3,6,6,0)	MATS069
	CALL GUID	MATS071
C	GUID PERFORMS THE GUIDANCE CALCULATIONS	MATS072
	18 CONTINUE	MATS073
	TSECP=TSEC	MATS074
	RETURN	MATS075
	END	MATS

Page Intentionally Left Blank

(Cont'd.)

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
O	RO	1	ρ		Libration term
O	G	1	g	radians	Mean anomaly of the moon
O	GP	1	g	radians	Mean anomaly of the sun
O	WW	1	ω	radians	Argument of the perigee of the moon
O	EMN	3,3			Rotation matrix

Transformation From Earth's True Equator to Moon's True Equator.

The two rectangular systems are related through Λ , Ω' , and i by the rotation:

$$\begin{pmatrix} x \\ y \\ z \end{pmatrix}_{\text{MOON}} = \begin{pmatrix} b_{11} & b_{12} & b_{13} \\ b_{21} & b_{22} & b_{23} \\ b_{31} & b_{32} & b_{33} \end{pmatrix} \begin{pmatrix} X' \\ Y' \\ Z' \end{pmatrix}_{\text{EARTH}}$$

where

$$b_{11} = \cos \Lambda \cos \Omega' - \sin \Lambda \sin \Omega' \cos i$$

$$b_{12} = \cos \Lambda \sin \Omega' + \sin \Lambda \cos \Omega' \cos i$$

$$b_{13} = \cos \Lambda \sin i$$

$$b_{21} = -\sin \Lambda \cos \Omega' - \cos \Lambda \sin \Omega' \cos i$$

$$b_{22} = -\sin \Lambda \sin \Omega' + \cos \Lambda \cos \Omega' \cos i$$

$$b_{23} = \cos \Lambda \sin i$$

$$b_{31} = \sin \Omega' \sin i$$

$$b_{32} = -\cos \Omega' \sin i$$

$$b_{33} = \cos i$$

i is the inclination of the moon's true equator to the earth's equator

Ω' is the right ascension of the ascending node of the moon's true equator

Λ is the anomaly from the node to the X axis

$$\Lambda = \Delta + (\textcircled{\text{C}} + \Upsilon) - (\Omega + \sigma)$$

Δ is the anomaly from the node to the ascending node of the moon's true equator on the ecliptic

Ω is the mean longitude of the descending node of the moon's mean equator on the ecliptic

$\textcircled{\text{C}}$ is the mean longitude of the moon

σ is the libration in the node

Υ is the libration in the mean longitude

ρ is the libration in the inclination.

$\delta\psi$, ϵ , Ω , and $\textcircled{\text{C}}$ are input quantities obtained from NUTAIT. The remainder are computed from the following equations.

I = inclination of moon's equator to ecliptic

$$I = 1.535^\circ$$

g = mean anomaly of moon

$$g = 215.54013 + 13.064992 d$$

g' = mean anomaly of sun

g' = $358.009067 + .9856005 d$

ω = argument of perigee of moon

ω = $196.745632 + .1643586 d$

where d = days from 1950.

$$\sigma \sin I = -.0302777 \sin g + .0102777 \sin (g + 2\omega) - .00305555 \sin (2g + 2\omega)$$

$$\tau = -.003333 \sin g + .0163888 \sin g' + .005 \sin 2\omega$$

$$\rho = -.0297222 \cos g + .0102777 \cos (g + 2\omega) - .00305555 \cos (2g + 2\omega)$$

$$\cos i = \cos (\Omega + \sigma + \delta\psi) \sin \epsilon \sin (I + \rho)$$

$$+ \cos \epsilon \cos (I + \rho)$$

$$0 < i < 90^\circ$$

$$\sin \Omega' = -\sin (\Omega + \sigma + \delta\psi) \sin (I + \rho) \csc i$$

$$-90^\circ < \Omega' < 90^\circ$$

$$\sin \Delta = -\sin (\Omega + \sigma + \delta\psi) \sin \epsilon \csc i$$

$$\cos \Delta = -\sin (\Omega + \sigma + \delta\psi) \sin \Omega' \cos \epsilon$$

$$-\cos (\Omega + \sigma + \delta\psi) \cos \Omega'$$

$$0^\circ \leq \Delta < 360^\circ$$

Reference: JPL Technical Report No. 32-223

* LABEL
* SYMBOL TABLE

CEC20AH

SUBROUTINE MNA(TIME,OM,CR,DT,EPSIL,RO,G,GP,WW,EM)

DIMENSION EM(3,3),DF(3)

D = TIME

T = D/36525.

T2 = T*T

T3 = T2*T

A=13.064992

DO 6 I=1,3

DD=D

D - DD=DD*(A/360.)

D DD=DD-INTF(DD)

DF(I)=DD

GO TO (4,5,6),I

4 A=.9856005

GO TO 6

5 A=.1643586

6 CONTINUE

G=215.54013*360.*DF(1)

GP=358.009067*360.*DF(2)

WW=196.745632*360.*DF(3)

G = G*.017453296

GP = GP*.017453296

WW = WW*.017453296

YN = 1.535*.017453296

RO = -.0297222*COSF(G) + .01020777*COSF(G+2.*WW)

1 -.00305555*COSF(2.*G+2.*WW)

TA = -.003333*SINF(G) + .0163888*SINF(GP)

1 +.005*SINF(2.*WW)

SG = -.0302777*SINF(G) + .0102777*SINF(G+2.*WW)

1 -.00305555*SINF(2.*G+2.*WW)

SG = (SG*.017453296)/SINF(YN)

RO = RO*.017453296

TA = TA*.017453296

YN = YN + RO

RO = OM + SG + DT

CI = COSF(RO)*SINF(EPSIL)*SINF(YN)

1 *COSF(EPSIL)*COSF(YN)

SI = 1. - CI**2

SI = SQRTF(SI)

SO = -SINF(RO)*SINF(YN)/SI

CO = 1. - SO**2

CO = SQRTF(CO)

SD = -SINF(RO)*SINF(EPSIL)/SI

CD = -SINF(RO)*SO*COSF(EPSIL) - COSF(RO)*CO

DL = ACOSF(CD)

IF(SD)1,3,3

1 DL = 6.283185306 - DL

3 CONTINUE

SMNA

SMNA

SMNA

SMNA000

SMNA001

SMNA002

SMNA003

SMNA004

SMNA005

SMNA006

SMNA007

SMNA008

SMNA009

SMNA010

SMNA011

SMNA012

SMNA013

SMNA014

SMNA015

SMNA016

SMNA017

SMNA018

SMNA019

SMNA020

SMNA021

SMNA022

SMNA023

SMNA024

SMNA025

SMNA026

SMNA027

SMNA028

SMNA029

SMNA030

SMNA031

SMNA032

SMNA033

SMNA034

SMNA035

SMNA036

SMNA037

SMNA038

SMNA039

SMNA040

SMNA041

SMNA042

SMNA043

SMNA044

SMNA045

SMNA046

SMNA047

MNA (Cont'd)

```

CA = DL + (CR + TA) - (OM + SG)
SA = SINF(CA)
CA = COSF(CA)
RO = COSF(RO)*SINF(EPSIL)/(SI*CD)
EM(1,1) = CA*CO - SA*SO*CI
EM(1,2) = CA*SO + SA*CO*CI
EM(1,3) = SA*SI
EM(2,1) = -SA*CO - CA*SO*CI
EM(2,2) = -SA*SO + CA*CO*CI
EM(2,3) = CA*SI
EM(3,1) = SO*SI
EM(3,2) = -CO*SI
EM(3,3) = CI
RETURN
END

```

```

SMNA048
SMNA049
SMNA050
SMNA051
SMNA052
SMNA053
SMNA054
SMNA055
SMNA056
SMNA057
SMNA058
SMNA059
SMNA060
SMNA061
SMNA

```

Subroutine: MNAND

Purpose: To compute the matrix M used to perform the velocity transformation corresponding to the position transformation described in MNA.

Calling Sequence:

CALL MNAND (TIME, RO, G, GP, WW, EM, DM)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	TIME	1	d	days	Days since 1950.0
I	RO	1	ρ	radians	Output from MNA; see description
I	G	1	g	radians	Output from MNA; see description
I	GP	1	g'	radians	Output from MNA; see description
I	WW	1	ω	radians	Output from MNA; see description
I	EM	3,3	M		Output from MNA; matrix M
O	DM	3,3	\dot{M}		Matrix \dot{M}

Common storages used or required:

None

Subroutines required:

None

Functions required:

COS

Approximate number of storages required:

Theory and Equations

In transforming lunacentric position coordinates relative to the earth's equator and equinox of 1950.0 to coordinates relative to the moon's true equator, three matrices are computed. Matrix A (from ROTEQ) rotates the coordinates to equinox of date, matrix N (from NUTAIT) accounts for the nutation of the earth about its precessing mean equator, and matrix M (from MNA) transforms to the position relative to the moon's true equator.

$$\text{Then } \begin{pmatrix} X \\ Y \\ Z \end{pmatrix}_{\text{moon}} = \text{MNA} \begin{pmatrix} X \\ Y \\ Z \end{pmatrix}_{\text{earth, 1950.0}}$$

Assuming that $\dot{N} = \dot{A} = 0$

$$\begin{pmatrix} \dot{X} \\ \dot{Y} \\ \dot{Z} \end{pmatrix}_{\text{moon}} = \text{MNA} \begin{pmatrix} \dot{X} \\ \dot{Y} \\ \dot{Z} \end{pmatrix}_{\text{earth, 1950}} + \dot{\text{MNA}} \begin{pmatrix} X \\ Y \\ Z \end{pmatrix}_{\text{earth, 1950}}$$

The $\dot{\text{M}}$ matrix is computed from the equations:

$$\dot{\text{M}} = \begin{pmatrix} M_{21}\dot{\Lambda} & M_{22}\dot{\Lambda} & M_{23}\dot{\Lambda} \\ -M_{11}\dot{\Lambda} & -M_{12}\dot{\Lambda} & -M_{13}\dot{\Lambda} \\ 0 & 0 & 0 \end{pmatrix}$$

where M_{ij} are the elements of M, and

$$\dot{\Lambda} = \dot{\Delta} + \dot{\zeta} + \dot{\epsilon} - \dot{\Omega} - \dot{\sigma}$$

$$\dot{\Delta} = -\rho (\dot{\Omega} + \dot{\sigma})$$

$$\dot{\Delta} = 0.266170762 \times 10^{-5} - 0.12499171 \times 10^{-13} T \text{ rad/sec; } T = d/36525$$

$$\dot{\Omega} = -0.1069698435 \times 10^{-7} + 0.23015329 \times 10^{-3} T \text{ rad/sec}$$

$$\begin{aligned} \dot{\sigma} = & -0.1535272946 \times 10^{-9} \cos g \\ & +0.569494067 \times 10^{-10} \cos g \\ & +0.579473484 \times 10^{-11} \cos 2g \text{ rad/sec} \end{aligned}$$

$$\begin{aligned} \dot{\sigma} = & -0.520642191 \times 10^{-7} \cos g \\ & +0.1811774451 \times 10^{-7} \cos (g+2g) \\ & -0.1064057858 \times 10^{-7} \cos (2g+2g) \text{ rad/sec} \end{aligned}$$

Reference: JPL Technical Report No. 32-223

MNAND

```

* LABEL
* SYMBOL TABLE
SUBROUTINE MNAND(TIME,RO,G,GP,WW,EM,DM)
DIMENSION DM(3,3),EM(3,3)
T = TIME/36525.
CRD = .266170762E-5 * .12499171E-13*T
OMD = -.1069698435E-7 + .23015329E-13*T
TAD = -1.535272946*COSF(G) + .569494067*COSF(GP)
1 + .0579473484*COSF(2.*WW)
TAD = .1E-9*TAD
SGD = -.520642191*COSF(G) + .1811774451*COSF(G+2.*WW)
1 -.1064057858*COSF(2.*WW+2.*G)
SGD = .1E-6*SGD
DLD = -RO*(OMD + SGD)
CAD = DLD + CRD + TAD - OMD - SGD
DM(1,1) = EM(2,1)*CAD
DM(1,2) = EM(2,2)*CAD
DM(1,3) = EM(2,3)*CAD
DM(2,1) = -EM(1,1)*CAD
DM(2,2) = -EM(1,2)*CAD
DM(2,3) = -EM(1,3)*CAD
DM(3,1) = 0.0
DM(3,2) = 0.0
DM(3,3) = 0.0
RETURN
END

```

```

MNAN
MNAN
MNAN0000
MNAN0010
MNAN0020
MNAN0030
MNAN0040
MNAN0050
MNAN0060
MNAN0070
MNAN0080
MNAN0090
MNAN0100
MNAN0110
MNAN0120
MNAN0130
MNAN0140
MNAN0150
MNAN0160
MNAN0170
MNAN0180
MNAN0190
MNAN0200
MNAN0210
MNAN0220
MNAN

```

Subroutine: MONBTR

Purpose: To obtain the position and velocity vectors of the vehicle relative to the beacon and determine if the beacon is in view of the vehicle. The station location partials are computed and subroutine COMPHQ called to update the state covariance matrix for the measurements being made. The types of measurements possible are range, range rate, right ascension, and declination.

Calling Sequence:

CALL MONBTR

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I					Quantities obtained from common
O					Quantities placed in common

Common storages used or required:

T, S, C, IC

Subroutines required:

COMPHQ, DOT, INTRI, MATRX, MNAND, MNA, NUTAIT, TRAC

Functions required:

ASIN, ATAN, FNORM, SQRT (FIL)(SLO)(STH)

Approximate number of storages required:

495 DEC

MONBTR Partial Derivatives

MONBTR computes two partial matrices which are used in COMPHQ to evaluate station location errors. The matrices are the following:

$$\text{STPARS} = \begin{pmatrix} \frac{\partial x_1}{\partial \text{LAT}} & \frac{\partial x_1}{\partial \text{LON}} & \frac{\partial x_1}{\partial \text{ALT}} \\ \frac{\partial x_2}{\partial \text{LAT}} & \frac{\partial x_2}{\partial \text{LON}} & \frac{\partial x_2}{\partial \text{ALT}} \\ \frac{\partial x_3}{\partial \text{LAT}} & \frac{\partial x_3}{\partial \text{LON}} & \frac{\partial x_3}{\partial \text{ALT}} \end{pmatrix}$$

$$\text{STPARD} = \begin{pmatrix} \frac{\partial \dot{x}_1}{\partial \text{LAT}} & \frac{\partial \dot{x}_1}{\partial \text{LON}} & \frac{\partial \dot{x}_1}{\partial \text{ALT}} \\ \frac{\partial \dot{x}_2}{\partial \text{LAT}} & \frac{\partial \dot{x}_2}{\partial \text{LON}} & \frac{\partial \dot{x}_2}{\partial \text{ALT}} \\ \frac{\partial \dot{x}_3}{\partial \text{LAT}} & \frac{\partial \dot{x}_3}{\partial \text{LON}} & \frac{\partial \dot{x}_3}{\partial \text{ALT}} \end{pmatrix}$$

where $\vec{X} = \begin{pmatrix} x_1 \\ x_2 \\ x_3 \end{pmatrix} = -\vec{X}_V + \vec{X}_B \quad \Xi \text{ XREL (FORTRAN)}$

$\vec{\dot{X}} = \begin{pmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{pmatrix} = -\vec{\dot{X}}_V + \vec{\dot{X}}_B \quad \Xi \text{ VREL (FORTRAN)}$

$$\frac{\partial x_i}{\partial \text{LAT}} = \frac{\partial x_{B1}}{\partial \text{LAT}} \quad \frac{\partial \dot{x}_i}{\partial \text{LAT}} = \frac{\partial \dot{x}_{B1}}{\partial \text{LAT}} \quad i = 1, 2, 3$$

$$\vec{X}_B = (MNA)^T \vec{X}_{BM}$$

$$\dot{\vec{X}}_B = (MNAND)^T \dot{\vec{X}}_{BM} + (MNA)^T \dot{\vec{X}}_{BM} \quad (=0)$$

where subscripts BM indicate beacon moon-fixed coordinates.

The transformations MNA and MNAND are obtained by calling the sub-routines MNA and MNAND.

$$\vec{X}_{BM} = (R + ALT) \begin{pmatrix} \cos LAT \cos LON \\ \cos LAT \sin LON \\ \sin LAT \end{pmatrix}$$

3 x 1

3 x 3

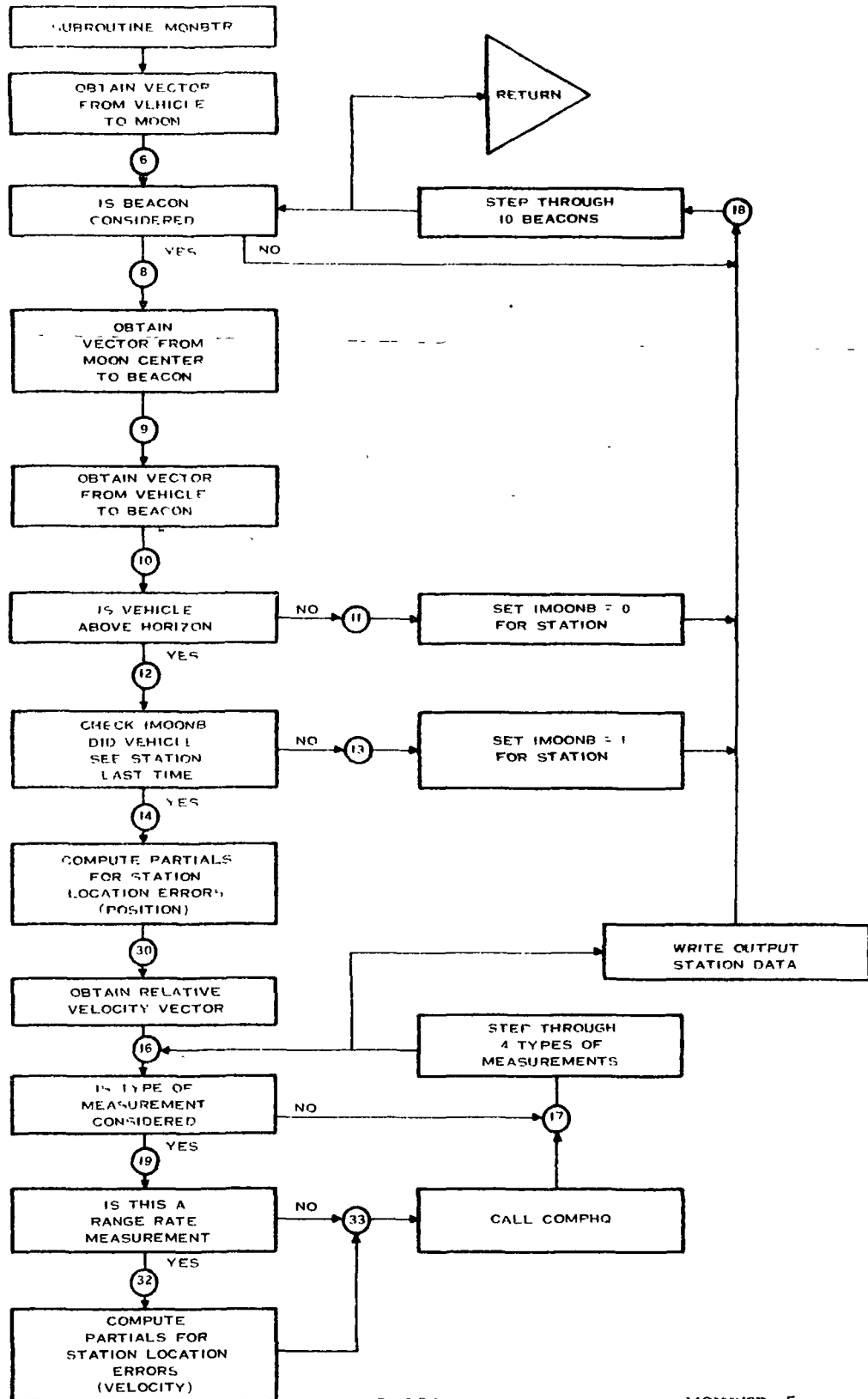
3 x 1

$$\begin{pmatrix} \frac{\partial x_1}{\partial PAR} \\ \frac{\partial x_2}{\partial PAR} \\ \frac{\partial x_3}{\partial PAR} \end{pmatrix} = (MNA)^T \begin{pmatrix} \frac{\partial x_{BM}}{\partial PAR} \\ \frac{\partial y_{BM}}{\partial PAR} \\ \frac{\partial z_{BM}}{\partial PAR} \end{pmatrix}$$

$$\begin{pmatrix} \frac{\partial \dot{x}_1}{\partial PAR} \\ \frac{\partial \dot{x}_2}{\partial PAR} \\ \frac{\partial \dot{x}_3}{\partial PAR} \end{pmatrix} = (MNAND)^T \begin{pmatrix} \frac{\partial x_{BM}}{\partial PAR} \\ \frac{\partial y_{BM}}{\partial PAR} \\ \frac{\partial z_{BM}}{\partial PAR} \end{pmatrix}$$

S-279

MONBTR-3



S-281

MONSTR-5

MONBTR

* LABEL	MONB
* SYMBOL TABLE	MONB
CEC2012 SUBROUTINE MONBTR	MONB
SUBROUTINE MONBTR	MONB0000
COMMON T,S,C,IC	MONB0010
DIMENSION	MONB0020
1T(1360),S(1000),C(1000),IC(1),XREL(3),VREL(3)	MONB0030
1,PO(22),VE(22),AN(3,3),EM(3,3),ISBCON(10),U(3),EN(3)	MONB0040
2,RT(3),E(3),ETM(3,3),IMOOONB(10),DM(3,3),DUM(3,3)	MONB0050
3,RMB(3),TYMEAS(4,10),X(3),VX(3),OUTPUT(6)	MONB0060
DIMENSION STPARS(3,3),DUD(3,3),STPARD(3,3)	MONB0065
EQUIVALENCE (T,TDUM),(S,SDUM),(C,CDUM),(IC,ICDUM)	MONB0070
1,(C(895),XREL),(C(898),VREL),(C(894),OBNO),(C(893),XMAG),	MONB0080
2(C(892),DEX),(C(891),DEN1),(C(890),DEN2)	MONB0090
3,(C(889),DEX2),(C(888),DEX3),(C(652),P),(C(973),OUTPUT)	MONB0100
1,(C(13),TW),(C(14),TF),(C(62),PO),(IC(3),NOR)	MONB0110
2,(IC(190),LSTAT),(C(138),AN),(S(24),A),(C(120),EM)	MONB0120
3,(IC(140),ISBCON),(S(72),DR),(IC(220),IMOOONB),(C(649),TSECP)	MONB0130
4,(C(30),TSEC),(IC(140),TYMEAS),(C(15),X),(C(18),VX)	MONB0140
EQUIVALENCE (C(800),STPARD),(C(788),STPARS)	MONB0145
CALL SETN(NIN,NUTS)	MONB0147
DELTT=TSEC-TSECP	MONB0150
LSTAT=LSTAT	MONB0160
GO TO(1,2),LSTAT	MONB0170
1 CONTINUE	MONB0180
NB=NOR-1	MONB0190
DIS=1.E10	MONB0200
CALL INTR1(TW,TF,NB,PO,1,VE,DIS)	MONB0210
2 CONTINUE	MONB0220
TIME=TW+TF	MONB0230
CALL NUTAIT(TIME,OM,CR,DT,EM,EPSIL)	MONB0240
CALL MNA(TIME,OM,CR,DT,EPSIL,RO,G,GP,WW,ETM)	MONB0250
CALL MNAND(TIME,RO,G,GP,WW,ETM,DM)	MONB0260
IF(NOR-2)3,5,3	MONB0270
3 CONTINUE	MONB0280
DO 4 I=1,3	MONB0290
J=20-I	MONB0300
XREL(I)=PO(J)-X(I)	MONB0310
VREL(I)=VE(J)-VX(I)	MONB0320
4 CONTINUE	MONB0330
GO TO 7	MONB0340
5 CONTINUE	MONB0350
DO 6 I=1,3	MONB0360
XREL(I)=-X(I)	MONB0370
VREL(I)=-VX(I)	MONB0380
6 CONTINUE	MONB0390
C XREL POSITION VECTOR FROM VEHICLE TO MOON CENTER 1950	MONB0400
C VREL RELATIVE VELOCITY OF MOON CENTER 1950	MONB0410
7 CONTINUE	MONB0420
NN=485	MONB0430
DO 18 III=1,10	MONB0440

INTR, INTRI(Cont'd)

SUB TARGO
TNZ NEU
CLA TARG+1
SUB TARGO+1
TZE FLEE+6

TIME HAS CHANGED

INTR050

INTR051

INTR052

INTR053

INTR054

INTR055

INTR056

INTR057

INTR058

INTR059

NEU

CLA TARG
FSB TABLE
TMI LOOKUP
STO COM+19
SUB 20.

ANALYZE TABLE
NEEDS AS A
FUNCTION OF
CENTRAL BODY

INTR060

INTR061

INTR062

INTR063

INTR064

INTR065

INTR066

INTR067

INTR068

INTR069

INTR070

INTR071

INTR072

INTR073

INTR074

INTR075

INTR076

INTR077

INTR078

INTR079

INTR080

INTR081

INTR082

INTR083

INTR084

INTR085

INTR086

INTR087

INTR088

INTR089

INTR090

INTR091

INTR092

INTR093

INTR094

INTR095

INTR096

INTR097

INTR098

INTR099

INTR100

TPL LOOKUP
CLA COM+19
FDH 4.

POSITION EPHEMERIS TAPE
T-TO

STQ COM+18
CLA COM+18
CALL FIX
CALL FLOAT
STO COM+17

(T-TO)/4.

CHS
FAD COM+18
STO COM+1
CLA TARG+1
FDH 4.

STQ COM
CLA COM
FAD COM+1
STO TARG+2
LDQ COM+19
FMP =9.

CALL FIX
ADD KERNO+1
STA GG
LDQ COM+17
FMP =54.

CALL FIX
ADD KERNO+2
STA HH
AXT 2*SEP,4

MUST INTERPOLATE
SO CLEAR STORAGE

STZ XN+2*SEP,4
TIX *-1,4,1
AXT BSEP,4
STZ KBO*BSEP,4
TIX *-1,4,1
LXA CENTER,4

SET GRAVITATIONAL
COEFFICIENTS
TO ZERO

PXD ,4
COM
PDX ,2

INTR, INTRI (Cont'd)

INTR1010
 INTR1020
 INTR1030
 INTR1040
 INTR1050
 INTR1060
 INTR1070
 INTR1080
 INTR1090
 INTR1100
 INTR1110
 INTR1120
 INTR1130
 INTR1140
 INTR1150
 INTR1160
 INTR1170
 INTR1180
 INTR1190
 INTR1200
 INTR1210
 INTR1220
 INTR1230
 INTR1240
 INTR1250
 INTR1260
 INTR1270
 INTR1280
 INTR1290
 INTR1300
 INTR1310
 INTR1320
 INTR1330
 INTR1340
 INTR1350
 INTR1360
 INTR1370
 INTR1380
 INTR1390
 INTR1400
 INTR1410
 INTR1420
 INTR1430
 INTR1440
 INTR1450
 INTR1460
 INTR1470
 INTR1480
 INTR1490
 INTR1500
 INTR1510

TEST FOR
 INCLUSION OF
 JUPITER IF
 EARTH IS
 CENTRAL BODY

CHECK
 FOR VELOCITY
 OPTIONS

GEOCENTRIC
 INTERPOLATION

HELIOCENTRIC
 INTERPOLATION

PLACE

GEO TXH HELIO,4,1
 AXT 3,1
 CLA GRAV+3,1
 STO KBO+3,1
 TIX *-2,1,1
 STZ KBO-1,2
 CLA EWORTO
 STO EWORT
 CLA HWORTE
 STO HWORT
 TXH GG12,4,0
 CLA RJ
 SUB R
 TPL GG12
 CLA HWORTJ
 STO HWORT
 CLA GRAV+6
 STO KB6
 TXL GG12,,**
 HELIO AXT BSEP,1
 CLA GRAV+BSEP,1
 STO KBO+BSEP,1
 TIX *-2,1,1
 STZ KB2-3,2
 ORTHO CLA EWORTO
 STO EWORT
 CLA HWORTO
 STO HWORT
 GG12 CLA VEL
 TZE GG6
 CLA EWORTO
 STO EWORT
 CLA HWORTV
 STO HWORT
 GG6 CLA EWORT
 TZE GG+2
 CLA EVEL
 STO VEL+1
 CLA TARG+1
 TSX TAB,4
 GG PZE **,9
 PZE XN,,EWORT+1
 CLA HWORT
 TZE HH+2
 CLA HVEL
 STO VEL+1
 CLA TARG+2
 TSX TAB,4
 HH PZE **,54
 PZE XN+3,,HWORT+1
 RESET AXT 3,4

INTR, INTRI (Cont'd)

CLA XN+6,4
 FDH EVEL
 STQ XN,+18,4
 CLA XN+9,4
 FDH EVEL
 STQ XN,+12,4
 LDQ XN+3,4
 STQ XN+6,4
 FMP MU
 FSB XN+18,4
 STO XN+9,4
 STZ XN+3,4
 LDQ XN,+3,4
 STQ XN,+6,4
 FMP MU
 FSB XN,+18,4
 STO XN,+9,4
 STZ XN,+3,4
 TIX RESET+1,4,1
 LXA CENTER,4
 LXD VEL,2
 TXH RVPRT,2,0
 TXH TESTM,4,0
 NZT KB6
 TRA FLEE
 AXT 3,1
 CLA XN+21,1
 FAD XN+9,1
 STO XN+21,1
 TIX *-3,1,1
 TXL FLEE
 TESTM TXH RVPRT,4,1
 AXT 3,1
 CLS XN+6,1
 STO XN+3,1
 CLA XN+9,1
 FSB XN+6,1
 STO XN+9,1
 STZ XN+6,1
 TIX *-6,1,1
 FLEE CLA CENTER
 STO KERNO
 CLA TARG
 STO TARGO
 CLA TARG+1
 STO TARGO+1
 AXT 21,1
 CLA XN+21,1
 OUP STO **,1
 TIX OUP-1,1,1
 CLA VEL

COORDINATES
 IN OLD
 FORMAT

POSITION OF SUN

VELOCITY OF SUN

IX2 NOT ZERO IF VELOCITY OPTION
 GET COORDINATES FOR PRINTING

EARTH-CENTERED

MOON-CENTERED

TRANSFER POSITIONS

INTR152
 INTR153
 INTR154
 INTR155
 INTR156
 INTR157
 INTR158
 INTR159
 INTR160
 INTR161
 INTR162
 INTR163
 INTR164
 INTR165
 INTR166
 INTR167
 INTR168
 INTR169
 INTR170
 INTR171
 INTR172
 INTR173
 INTR174
 INTR175
 INTR176
 INTR177
 INTR178
 INTR179
 INTR180
 INTR181
 INTR182
 INTR183
 INTR184
 INTR185
 INTR186
 INTR187
 INTR188
 INTR189
 INTR190
 INTR191
 INTR192
 INTR193
 INTR194
 INTR195
 INTR196
 INTR197
 INTR198
 INTR199
 INTR200
 INTR201
 INTR202

INTR, INTRI (Cont'd)

	TZE	OUT	DO NOT TRANSFER VELOCITY	INTR2030
	AXT	21,1		INTR2040
	CLA	XN,+21,1	TRANSFER VELOCITIES	INTR2050
(N,V)	STO	++,1		INTR2060
	TIX	XN,V-1,1,1		INTR2070
OUT	LXD	HELIO-1,1		INTR2080
	LXD	TRAP+1,2		INTR2090
	LXD	TRAP,4		INTR2100
	TRA	8,4		INTR2110
	REM	TSX TAB,4	(AC)=INTERPOLATIVE ARGUMENT	INTR2120
	REM	PZE B,,K		INTR2130
	REM	PZE A,,C		INTR2140
	REM		B=START OF DATA BLOCK	INTR2150
	REM		K=WORDS PER SUB BLOCK	INTR2160
	REM		A=START OF RESULT BLOCK	INTR2170
	REM		C=SKIP CODE WORD LOCATION	INTR2180
TAB	SXD	COM+9,4		INTR2190
	SXD	COM+8,2		INTR2200
	SXD	COM+7,1		INTR2210
	STO	ARG		INTR2220
	CLA	1,4		INTR2230
	STA	TAB18		INTR2240
	LRS	18		INTR2250
	ADD	1,4		INTR2260
	STA	TAB21		INTR2270
	CLA	2,4		INTR2280
	PAX	,1		INTR2290
	TXI	++1,1,SEP		INTR2300
	SXA	TAB29,1		INTR2310
	ARS	18		INTR2320
	STA	VELOP		INTR2330
	AXT	2,1		INTR2340
	CLA	VEL		INTR2350
	TNZ	VELOP		INTR2360
	TXI	VELOP,1,-1		INTR2370
ELOP	CLA	++,1	PICK UP SKIP	INTR2380
	STO	VEL+2	CODE WORD	INTR2390
	TXL	POSOP,1,1		INTR2400
	REM		VELOCITY OPTION	INTR2410
	CLA	ARG		INTR2420
	TSX	COEFF.,4	FORM THE	INTR2430
	AXT	3,4	E1(2J).	INTR2440
	CLS	COM+13,4		INTR2450
	STO	COM+16,4		INTR2460
	TIX	*-2,4,1		INTR2470
	CLA	1.	FORM THE	INTR2480
	FSB	ARG	E0(2J).	INTR2490
	TSX	COEFF.,4		INTR2500
	TRA	TAB1-1		INTR2510
	REM		POSITION OPTION	INTR2520
OSOP	CLA	ARG		INTR2530

INTR, INTRI (Cont'd)

	TSX	COEFF,4	FORM THE	INTR254
	AXT	3,4	E1(2J)	INTR255
	CLA	COM+13,4		INTR256
	STO	COM+16,4		INTR257
	TIX	*-2,4,1		INTR258
	CLA	1.	FORM THE	INTR259
	FSB	ARG	E0(2J)	INTR260
	TSX	COEFF,4		INTR261
	LXA	TAB29,4		INTR262
	TXI	++1,4,-SEP		INTR263
	SXA	TAB29,4		INTR264
	SXD	COM+4,1		INTR265
TAB1	AXT	0,3		INTR266
	LDQ	VEL+2		INTR267
	PXD			INTR268
	LGL	2		INTR269
	PAX	,4		INTR270
	STQ	VEL+2		INTR271
	CAL	=05		INTR272
	ORS	VEL+2		INTR273
	TXH	END,4,2		INTR274
	TXH	FORT,4,0		INTR275
	TXI	++1,1,-3		INTR276
	TXI	TAB1+1,2,-1		INTR277
FORT	AXT	3,4		INTR278
TAB18	LDQ	++,1	X(0)	INTR279
	FMP	COM+13,4		INTR280
	STO	COM		INTR281
TAB21	LDQ	++,1	X(1)	INTR282
	FMP	COM+16,4		INTR283
	FAD	COM		INTR284
	STO	COM+4,4		INTR285
	TXI	++1,1,-1		INTR286
	TIX	*-8,4,1		INTR287
	FAD	COM+2		INTR288
	FAD	COM+1		INTR289
TAB29	STO	++,2	X(T)	INTR290
	TXI	TAB1+1,2,-1		INTR291
END	LXD	COM+4,1		INTR292
	TIX	VELOP,1,1		INTR293
	LXD	COM+9,4		INTR294
	LXD	COM+8,2		INTR295
	LXD	COM+7,1		INTR296
	TRA	3,4		INTR297
COEFF	STO	COM+10	CALCULATE	INTR298
	LDQ	COM+10	POSITION	INTR299
	FMP	COM+10	COEFFICIENTS	INTR300
	STO	COM+12	FOR EVERETT,S	INTR301
	FSB	1.	INTERPOLATION	INTR302
	FDH	6.	FORMULA	INTR303
	FMP	COM+10		INTR304

INTR, INTRI (Cont'd)

	STO	COM+11		INTR3050
	CLA	COM+12		INTR3060
	FSB	4.		INTR3070
	FDH	20.		INTR3080
	FMP	COM+11		INTR3090
	STO	COM+12		INTR3100
	TRA	1,4		INTR3110
COEFF.	STO	COM	CALCULATE	INTR3120
	CLS	1.	VELOCITY	INTR3130
	FDH	VEL+1	COEFFICIENTS	INTR3140
	STO	COM+10	FOR EVERETT,S	INTR3150
	LDQ	COM	INTERPOLATION	INTR3160
	FMP	COM	FORMULA	INTR3170
	STO	COM+12		INTR3180
	XCA			INTR3190
	FMP	3.		INTR3200
	FSB	1.		INTR3210
	FDH	6.		INTR3220
	FMP	COM+10		INTR3230
	STO	COM+11		INTR3240
	CLA	COM+12		INTR3250
	FSB	3.		INTR3260
	XCA			INTR3270
	FMP	5.		INTR3280
	XCA			INTR3290
	FMP	COM+12		INTR3300
	FAD	4.		INTR3310
	FDH	120.		INTR3320
	FMP	COM+10		INTR3330
	STO	COM+12		INTR3340
	TRA	1,4		INTR3350
RVPRT	AXT	0,2	EXPRESS ALL	INTR3360
	AXT	3,5	BODIES GEOCENTRICALLY	INTR3370
	CLA	XN+9,2		INTR3380
	FAD	XN+9,4		INTR3390
	STO	XN+9,2		INTR3400
	CLA	VEL		INTR3410
	TZE	++4		INTR3420
	CLA	XN,+9,2		INTR3430
	FAD	XN,+9,4		INTR3440
	STO	XN,+9,2		INTR3450
	TXI	++1,2,-1		INTR3460
	TIX	RVPRT+2,4,1		INTR3470
	TXH	RVPRT+1,2,9-SEP		INTR3480
	CLA	CENTER	BUFFER	INTR3490
	ALS	1	CENTRAL	INTR3500
	ADD	CENTER	BODY	INTR3510
	PAC	,4		INTR3520
	CLA	XN,4		INTR3530
	STO	COM+3,1		INTR3540
	CLA	XN,,4		INTR3550

INTR, INTRI (Cont'd)

	STO	COM+6,1		INTR3560
	TXI	++1,4,-1		INTR3570
	TIX	*-5,1,1		INTR3580
RVPRT1	AXT	0,2	EXPRESS ALL	INTR3590
	AXT	3,4	BODIES IN TERMS	INTR3600
	CLA	XN,2	OF THE CENTRAL	INTR3610
	FSB	COM+3,4	BODY	INTR3620
	STO	XN,2		INTR3630
	CLA	VEL		INTR3640
	TZE	++4		INTR3650
	CLA	XN,,2		INTR3660
	FSB	COM+6,4		INTR3670
	STO	XN,,2		INTR3680
	TXI	++1,2,-1		INTR3690
	TIX	RVPRT1+2,4,1		INTR3700
	TXH	RVPRT1+1,2,-SEP		INTR3710
	TXL	FLEE		INTR3720
LOOKUP	CLA	TLAST		INTR3730
	FSB	TARG		INTR3740
	TNZ	++2		INTR3750
	TRA	ERR1		INTR3760
	TMI	*-1		INTR3770
	CLA	TARG		INTR3780
	FSB	TFIRST		INTR3790
	TPL	++2		INTR3800
	TRA	ERR1		INTR3810
	FDH	20,		INTR3820
	XCA			INTR3830
	CALL	FIX		INTR3840
	CALL	FLOAT		INTR3850
	XCA			INTR3860
	FMP	20,		INTR3870
	FAD	TFIRST		INTR3880
	STO	COM+1	TIME ON RECORD	INTR3890
	CLA	TABLE		INTR3900
	FSB	COM+1		INTR3910
	TMI	FINDIT		INTR3920
	FDH	20,		INTR3930
	XCA			INTR3940
	CALL	FIX		INTR3950
	ADD	1F	RECORDS TO	INTR3960
	PAX	,4	BE BACKED	INTR3970
	TEFA	++1		INTR3980
	TXL	++3,4,20	OVER	INTR3990
	REWA	6		INTR4000
	TRA	FINDIT		INTR4010
	BSRA	6		INTR4020
	TIX	*-1,4,1		INTR4030
FINDIT	AXT	10,2		INTR4040
	SDHA	6		INTR4050
	RTBA	6		INTR4060

INTR, INTRI (Cont'd)

INTR4070
 INTR4080
 INTR4090
 INTR4100
 INTR4110
 INTR4120
 INTR4130
 INTR4140
 INTR4150
 INTR4160
 INTR4170
 INTR4180
 INTR4190
 INTR4200
 INTR4210
 INTR4220
 INTR4230
 INTR4240
 INTR4250
 INTR4260
 INTR4270
 INTR4280
 INTR4290
 INTR4300
 INTR4310
 INTR4320
 INTR4330
 INTR4340
 INTR4350
 INTR4360
 INTR4370
 INTR4380
 INTR4390
 INTR4400
 INTR4410
 INTR4420
 INTR4430
 INTR4440
 INTR4450
 INTR4460
 INTR4470
 INTR4480
 INTR4490
 INTR4500
 INTR4510
 INTR4520
 INTR4530
 INTR4540
 INTR4550
 INTR4560
 INTR4570

TAPE NOT POSITIONED PROPERLY

CHECK
 SUM

SCALING
 LOOP

SCALE
 GEOCENTRIC
 EPHEMERIS

SCALE
 HELIOCENTRIC
 EPHEMERIS

COMPUTE
 MASS RATIO
 OF MOON
 TO EARTH-MOON
 BARYCENTER
 FOR POSITION OF EARTH

EARTH RADIUS
 ASTRONOMICAL UNIT (JPL, JULY 1961
 0 HR AUG 28, 1960 JD = 2437174.5
 0 HR DEC 19, 1969 JD = 2440554.5

JUPITER TEST DISTANCE
 E.T.=U.T.

EARTH

RCHA IO
 TCOA *
 TEFA ERR1
 CLA TABLE
 SUB COM+1
 TMI **2
 TNZ LOOKUP
 TNZ FINDIT
 AXT 513,4
 CAL TABLE
 ACL A+513,4
 TIX *-1,4,1
 TRCA BSRA
 LAS C
 TRA **2
 TRA SCALE
 BSRA BSRA 6
 TIX FINDIT+1,2,1
 CALL ERP
 IO IOCD TABLE,,515
 ERR1 CALL ERPT
 PZE TARG
 REM
 REM
 SCALE AXT 189,4
 LDQ A+189,4
 FMP SCALE1
 STO A+189,4
 TIX *-3,4,1
 AXT 324,4
 LDQ B+324,4
 FMP SCALE2
 STO B+324,4
 TIX *-3,4,1
 CLA GRAV
 FAD GRAV+1
 STO COM
 CLA GRAV+1
 FDH COM
 STQ MU
 TRA NEU
 SCALE1 DEC 6378.150
 SCALE2 DEC 149598500.
 TFIRST DEC 3892.0
 TLAST DEC 7292.0
 TRAP PZE
 PZE
 RJ DEC 1E6
 TEMPDT DEC 34.
 PZE
 GRAV DEC 3.98602E5

INTR, INTRI (Cont'd)

DEC	4.8983349E3	MOON	INTR458
DEC	1.3252312E11	SUN	INTR459
DEC	3.2429889E5	VENUS	INTR460
DEC	4.2915518E4	MARS	INTR461
DEC	0	REMOVE BARYCENTER	INTR462
DEC	1.2652701E8	JUPITER	INTR463
EVEL	DEC 86400.		INTR464
HVEL	DEC 345600.		INTR465
MU	PZE	MASS RATIO OF MOON TO BARYCENTER	INTR466
OCT	000000520052	MARS, JUPITER VELOCITY	INTR467
HWORT	OCT 0		INTR468
OCT	527777777777	MOON VELOCITY	INTR469
OCT	0		INTR470
HWORTJ	OCT 000000005252	BARYCENTER, JUPITER	INTR471
HWORTE	OCT 000000005200	BARYCENTER	INTR472
EWORTO	OCT 527777777777		INTR473
HWORTO	OCT 000052525252		INTR474
HWORTV	OCT 525252525252		INTR475
TARGO	DEC 20.,0	FORMER TIME	INTR476
KERNO	PZE	FORMER CENTER	INTR477
PZE	A	GEOCENTRIC REFERENCE	INTR478
PZE	B	HELIOCENTRIC REFERENCE	INTR479
ARG	PZE 0		INTR480
1F	DEC 1		INTR481
1.	DEC 1.		INTR482
3.	DEC 3.		INTR483
4.	DEC 4.		INTR484
5.	DEC 5.		INTR485
6.	DEC 6.		INTR486
20.	DEC 20.		INTR487
120.	DEC 120.		INTR488
86400.	DEC 86400.		INTR489
VEL	BSS 3	VELOCITY OPTION,H,SKIP CODE	INTR490
*			INTR491
TABLE	DEC 0	RESERVE	INTR492
A	BSS 189	FOR	INTR493
B	BSS 324	WORKING	INTR494
C	BSS 1	EPHEMERIS	INTR495
*			INTR496
TARG	PZE		INTR497
PZE			INTR498
PZE			INTR499
CENTER	PZE		INTR500
COM	BSS 21		INTR501
VAFLG	PZE		INTR502
FQFLG	BSS 3		INTR503
KBO	PZE		INTR504
KB1	PZE		INTR505
KB2	PZE		INTR506
KB3	PZE		INTR507
KB4	PZE		INTR508

INTR, INTRI (Cont'd)

KB5	PZE	
KB6	PZE	
XN	BSS	21
XN.	BSS	21
T	PZE	
	PZE	
R	PZE	
BSEP	SYN	7
SEP	SYN	XN, -XN
	END	

INTR5090
INTR5100
INTR5110
INTR5120
INTR5130
INTR5140
INTR5150
INTR5160
INTR5170
INTR

Subroutine: INV3

Purpose: To invert a matrix of any dimension up to a 6 by 6.

Calling Sequence:

CALL INV3 (A, N, DETERM)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
IO	A	6,6			A(I) Matrix to be inverted
					A(O) Inverse of input matrix
I	N	1			Dimension of input matrix
O	DETERM	1			Matrix determinant

Common storages used or required: None

Subroutines required: None

Functions required: ABS

Approximate number of storages required:

INV3

```

* LABEL INV3
C SUBROUTINE FOR INVERTING SQUARE MATRICES WHICH ARE 6 BY 6 OR LESS INV30000
C (TO INVERT LARGER MATRICES, SAY M BY M, DIMENSION IPIVOT(M),A(M*M), INV30010
C INDEX(M,2),PIVOT(M) AND RECOMPILE) INV30020
C A IS THE SQUARE MATRIX TO BE INVERTED INV30030
C N IS THE SIZE OF A (A IS AN N BY N MATRIX) INV30040
C THE SUBROUTINE RETURNS A INVERSE IN PLACE OF A AND THE DETERMINANT INV30050
C IN DETERM. INV30060
SUBROUTINE INV3(A,N,DETERM) INV30070
DIMENSION IPIVOT(6),A(36) ,INDEX(6,2),PIVOT(6) INV30080
EQUIVALENCE (IROW,JROW), (ICOLUM,JCOLUM),(AMAX,T,SWAP) INV30090
DETERM=1.0 INV30100
DO 20 J=1,N INV30110
20 IPIVOT(J)=0 INV30120
DO 550 I=1,N INV30130
AMAX=0.0 INV30140
DO 105 J=1,N INV30150
IF(IPIVOT(J)-1) 60,105,60 INV30160
60 DO 100 K=1,N INV30170
IF(IPIVOT(K)-1) 80,100,740 INV30180
80 M = N*(K-1)+J INV30190
IF (ABSF(AMAX)-ABSF(A(M))) 85,100,100 INV30200
85 IROW=J INV30210
ICOLUM=K INV30220
AMAX = A(M) INV30230
100 CONTINUE INV30240
105 CONTINUE INV30250
IPIVOT(ICOLUM)=IPIVOT(ICOLUM)+1 INV30260
IF(IROW-ICOLUM) 140,260,140 INV30270
140 DETERM=-DETERM INV30280
DO 200 L=1,N INV30290
M = N*(L-1) INV30300
M1 = M+ICOLUM INV30310
M = M+IROW INV30320
SWAP = A(M) INV30330
A(M) = A(M1) INV30340
200 A(M1) = SWAP INV30350
260 INDEX(I,1)=IROW INV30360
INDEX(I,2)=ICOLUM INV30370
M = N*(ICOLUM-1)+ICOLUM INV30380
PIVOT(I) = A(M) INV30390
DETERM=DETERM*PIVOT(I) INV30400
A(M) = 1.0 INV30410
DO 350 L=1,N INV30420
M = N*(L-1)+ICOLUM INV30430
350 A(M) = A(M)/PIVOT(I) INV30440
DO 550 L1=1,N INV30450
IF(L1-ICOLUM) 400,550,400 INV30460
400 M = N*(ICOLUM-1)+L1 INV30470
T = A(M) INV30480
A(M) = 0. INV30490

```

INV3 (Cont'd)

```

DO 450 L=1,N
M = N*(L-1)
M1 = M+ICOLUM
M = M+L1
450 A(M) = A(M)-A(M1)+T
550 CONTINUE
DO 710 I=1,N
L=N+1-I
IF(INDEX(L,1)=INDEX(L,2)) 630,710,630
630 JROW=INDEX(L,1)
JCOLUM=INDEX(L,2)
M = N*(JROW-1)
M1 = N*(JCOLUM-1)
DO 705 K=1,N
M = M+1
M1 = M1+1
SWAP = A(M)
A(M) = A(M1)
A(M1) = SWAP
705 OONTINUE
710 OONTINUE
740 RETURN
END

```

INV3050
INV3051
INV3052
INV3053
INV3054
INV3055
INV3056
INV3057
INV3058
INV3059
INV3060
INV3061
INV3062
INV3063
INV3064
INV3065
INV3066
INV3067
INV3068
INV3069
INV3070
INV3071
INV3

Page Intentionally Left Blank

Subroutine: INVAO

Purpose: To form the inverse of a transition matrix for a linear, conservative dynamic system. If Φ is a partitioned matrix such as

$$\Phi = \begin{pmatrix} \Phi_1 & \Phi_2 \\ \Phi_3 & \Phi_4 \end{pmatrix} \text{ then INVAO computes } \Phi^{-1} = \begin{pmatrix} \Phi_4^T & -\Phi_2^T \\ -\Phi_3^T & \Phi_1^T \end{pmatrix}$$

Calling Sequence:

CALL INVAO (AO, AOI)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	AO	6,6	$\Phi(t_2, t_1)$		Transition Matrix
O	AOI	6,6	$\Phi^{-1}(t_2, t_1)$		Inverse Transition Matrix

Common storages used or required:

None

Subroutines required:

None

Functions required:

None

Approximate number of storages required:

INVAO

```
* LABEL
* SYMBOL TABLE
SUBROUTINE INVAO(AO,AOI)
DIMENSION AO(6,6),AOI(6,6)
DO 1 I=1,3
  II=I+3
  DO 1 J=1,3
    JJ=J+3
    AOI(I,J)=AO(JJ,II)
    AOI(II,J)=-AO(JJ,I)
    AOI(II,JJ)=AO(J,I)
1  AOI(I,JJ)=-AO(J,II)
RETURN
END
```

```
INVA
INVA
INVA0000
INVA0010
INVA0020
INVA0030
INVA0040
INVA0050
INVA0060
INVA0070
INVA0080
INVA0090
INVA0100
INVA
```


Subroutine: LOADO

Purpose: To transfer the transition matrix from its storage in the integration package's T block to the matrix in the call list.

Calling Sequence:

CALL LOADO (AO)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
0	AO	(6,6)	$\Phi(t_2 t_1)$		Transition Matrix

Common storages used or required: T

Subroutines required: None

Functions required: None

Approximate number of storages required:

LOADO

```

* LABEL
* SYMBOL TABLE
SUBROUTINE LOADO(AC)
COMMON T
DIMENSION T(1360),AO(6,6)
K=6
JJ=27
DO1 I=1,6
DO 1 J=1,3
K=K+1
KK=J+3
JJ=JJ+1
AO(KK,I)=T(JJ)
AO(J,I)=T(K)
1 CONTINUE
RETURN
END

```

```

LOAD
LOAD
LOAD0000
LOAD0010
LOAD0020
LOAD0030
LOAD0040
LOAD0050
LOAD0060
LOAD0070
LOAD0080
LOAD0090
LOAD0100
LOAD0110
LOAD0120
LOAD0130
LOAD

```

Subroutine: LOADT

Purpose: To place unit initial conditions in the T block for the variational equations which are being used to generate the transition matrix.

Calling Sequence:

CALL LOADT

Input and Output

Common storages used or required:	T
Subroutines required:	None
Functions required:	None
Approximate number of storages required:	

LOADT

```

* LABEL
* SYMBOL TABLE
SUBROUTINE LOADT
C SUBROUTINE LOADT PUTS UNIT ICS ON PERTURBATION EQUATIONS
COMMON T
DIMENSION T(1360),X(3,6),V(3,6)
EQUIVALENCE (T(7), X),(T(28),V)
DO 2 I=1,3
L=I+3
DO 1 J=1,3
K=J+3
X(I,J)=0.
V(I,K)=0.
X(I,K)=0.
V(I,J)=0.
1 CONTINUE
X(I,I)=1.
V(I,L)=1.
2 CONTINUE
RETURN
END

```

```

LOAT
LOAT
LOAT0000
LOAT0010
LOAT0020
LOAT0030
LOAT0040
LOAT0050
LOAT0060
LOAT0070
LOAT0080
LOAT0090
LOAT0100
LOAT0110
LOAT0120
LOAT0130
LOAT0140
LOAT0150
LOAT0160
LOAT0170
LOAT

```

Subroutine: MASS

Purpose: To find the relevant gravitational constants to be used in computing planetary perturbations for a given central body. MASS also chooses the initial integration step size as a function of central body.

Calling Sequence:

CALL MASS (NOR, UM, VKB, X, ACCP)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	NOR	1			Central Body Indicator.
					1=Earth; 2, Moon; 3, Sun; 4,
					Venus; 5, Mars; 6, Jupiter
I	UM	6	μ_i	Km^3/sec^2	Gravitational constants, arranged
					as above
O	VKB	6	μ_i	Km^3/sec^2	μ_i for bodies
I	X	3	X, Y, Z	Km	Position coordinates
O	ACCP	1		seconds	Initial integration step size

Common storages used or required: None

Subroutines required: None

Functions required: FNORM

Approximate number of storages required:

Method of Establishing Integration Step Size and Perturbing Bodies

Central Body	Integration Step Size	Other Bodies to be Considered
Earth	60.0	Moon, Sun. If $ X \geq 10^6$ Km, Jupiter.
Moon	60.0	Earth, Sun.
Sun	43200.0	All
Venus, Mars, Jupiter	60.0	All

The bodies which are not to be used in calculation of perturbation accelerations are eliminated from consideration by placing zeros in array VKB(6). For the bodies which are being considered, the appropriate gravitational constant is placed in VKB(6).

Page Intentionally Left Blank

Subroutine: MATRX

Purpose: To perform matrix multiplications of matrices with any dimensions up to maximum dimensions of 10 by 10. A zero in the call sequence (J) yields an output matrix $C = A \cdot B$. A one in the call sequence (J) yields an output matrix $C = A \cdot B \cdot A^T$. The matrix products are obtained in double precision.

Calling Sequence:

CALL MATRX (A, B, C, NRA, NCA, NCB, J)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	A	(10,10)			Input Matrix
I	B	(10,10)			Input Matrix
O	C	(10,10)			Output Matrix
I	NRA	1			Number of Rows of A
I	NCA	1			Number of Columns of A
I	NCB	1			Number of Columns of B
I	J	1			Type of multiplication desired

Common storages used or required:

None

Subroutines required:

None

Functions required:

None

Approximate number of storages required:

MATRIX

* LABEL	MATX
* SYMBOL TABLE	MATX
CEC2000 SUBROUTINE MATRX	MATX
SUBROUTINE MATRX(A,B,C,NRA,NCA,NCB,J)	MATX0000
C J=0 A*B=C	MATX0010
C J=1 A*B*AT=C T MEANS TRANSPOSE	MATX0020
C NRA=NUMBER OF ROWS OF A	MATX0030
C NCA=COLUMNS OF A	MATX0040
C NCB=COLUMNS OF B	MATX0050
C ACCUMULATION OF PRODUCTS IN DOUBLE PRECISION	MATX0060
C DIMENSION A(100),B(100),C(100),D(100)	MATX0080
D DUD=0.	MATX0090
D DUM=0.	MATX0100
DO 1 I=1,NRA	MATX0110
DO 1 K=1,NCB	MATX0120
NC=I+(K-1)*NRA	MATX0130
D CRUD=0.	MATX0140
DO 2 L=1,NCA	MATX0150
NA=I+(L-1)*NRA	MATX0160
NB=L+(K-1)*NCA	MATX0170
DUD=A(NA)	MATX0180
DUM=B(NB)	MATX0190
D CRUD=CRUD+DUD*DUM	MATX0200
2 CONTINUE	MATX0210
D(NC)=CRUD	MATX0220
1 CONTINUE	MATX0230
IF(J)3,3,4	MATX0240
3 CONTINUE	MATX0250
KK=NCB*NRA	MATX0260
DO 5 I=1,KK	MATX0270
5 C(I)=D(I)	MATX0280
GO TO 10	MATX0290
4 CONTINUE	MATX0300
DO 6 I=1,NRA	MATX0310
DO 6 K=1,NRA	MATX0320
NC=I+(K-1)*NRA	MATX0340
D CRUD=0.	MATX0350
DO 7 L=1,NCA	MATX0360
NA=I+(L-1)*NRA	MATX0370
NB=K+(L-1)*NRA	MATX0380
DUM=D(NA)	MATX0390
DUD=A(NB)	MATX0400
D CRUD=CRUD+DUM*DUD	MATX0410
7 CONTINUE.	MATX0420
C(NC)=CRUD	MATX0430
6 CONTINUE.	MATX0440
10 CONTINUE	MATX0510
RETURN	MATX0520
END	MATX

Subroutine: MATSUB

Purpose: The subroutine is primarily logic which controls (1) trajectory and data printout, (2) updating of the state covariance matrix for observations by calling subroutines EARTR, ONBTR, and MONBTR, and (3) updating of the guidance covariance matrix by calling subroutine GUID.

Calling Sequence:

CALL MATSUB

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I					Quantities obtained from common
O					Quantities returned to common

Common storages used or required:

T, S, C, IC

Subroutines required:

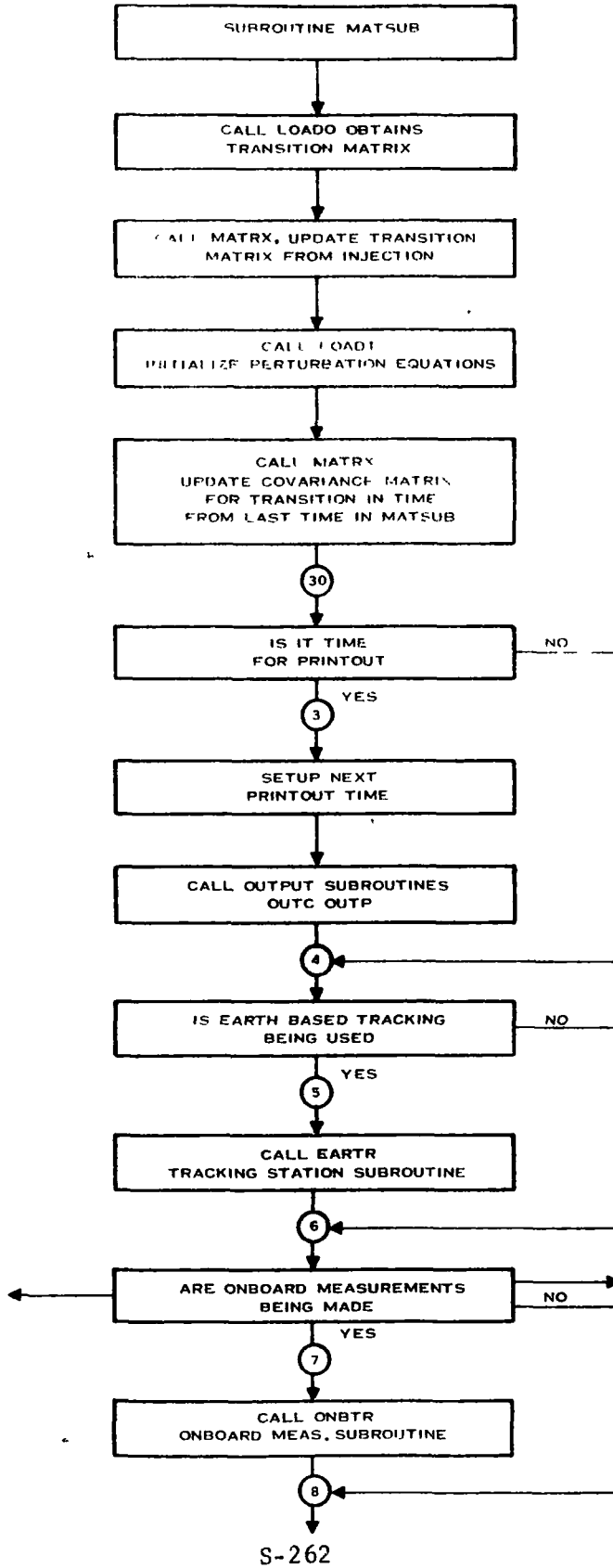
EARTR, GUID, INVAO, LOADO, LOADT, MATRX, MONBTR, ONBTR, OUTC, OUTP

Functions required:

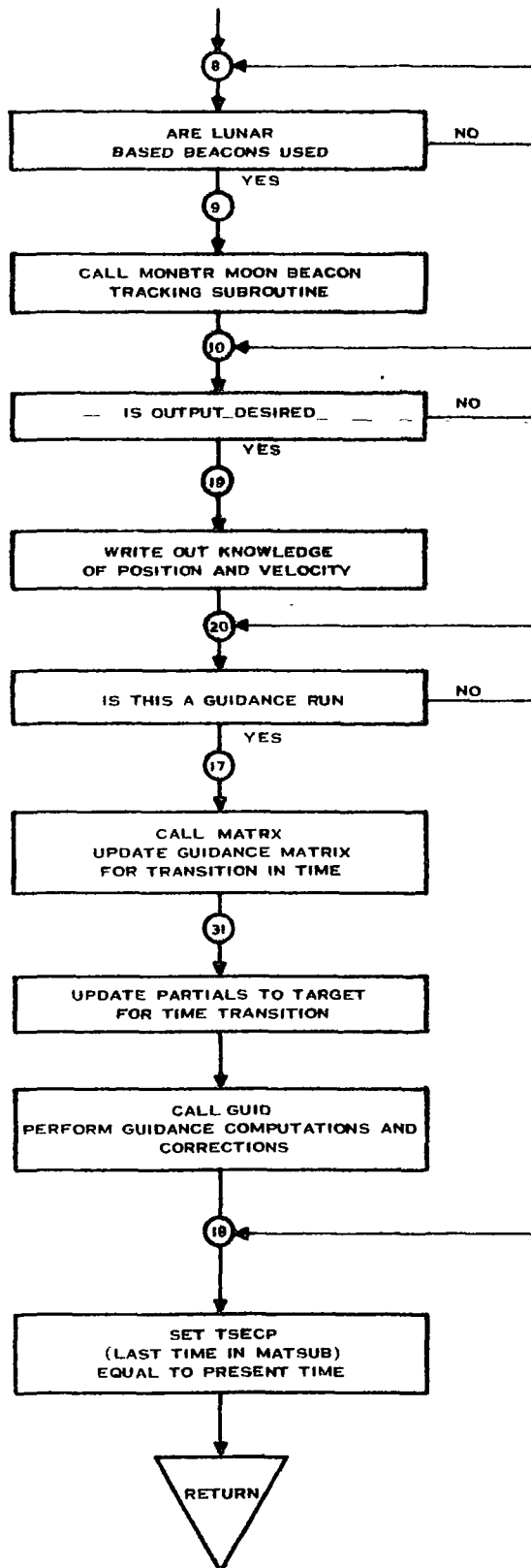
SQRT (FIL) (STH)

Approximate number of storages required:

346 DEC



MATSUB -2



* LABEL	MATS
* SYMBOL TABLE	MATS
CEC2006 SUBROUTINE MATSUB	MATS
SUBROUTINE MATSUB	MATS0000
COMMON T,S,C,IC	MATS0010
DIMENSION T(1360),S(1000),C(1000),IC(1),AN(3,3),PO(22),VE(22),	MATS0020
1EM(3,3),XP(3),VXP(3),EA(3,3),XED(3),VED(3),AO(6,6),P(6,6),	MATS0030
2TFTA(3,6),PFTA(6,6),AOS(6,6),AOI(6,6)	MATS0040
EQUIVALENCE (T ,TDUM),(S ,SDUM),(C ,CDUM),	MATS0050
1(C(138),AN),(C(13),TP1),(C(14),TP2),(C(62),PO),(C(84),VE),	MATS0060
2(C(120),EM),(C(650),TPRINT),(C(651),TSTRT),(C(30),TSEC),	MATS0070
3(C(15),XP),(C(18),VXP),(C(10),TW),(C(11),TF) ,(C(129),EA),	MATS0080
4(C(652),P),(C(752),AOS),(C(850),AOI)	MATS0090
5,(C(460),PFTA),(C(568),TFTA),(C(647),TOUT)	MATS0100
EQUIVALENCE (IC(2),IOR),(IC(7),KOUT),(IC(6),ITARG),(IC(9),LPRINT),	MATS0110
1(IC(190),LSTAT),(IC(191),LONB),(IC(192),LMB),(IC(193),IGUID),	MATS0120
2(IC(214),NOUT),(C(649),TSECP)	MATS0130
CALL SETN(NIN,NUTS)	MATS0131
NOUT=1	MATS0140
CALL LOADU(AO)	MATS0145
CALL MATRX(AO,AOS,AOS,6,6,6,0)	MATS0150
CALL LOADT	MATS0155
CALL MATRX(AO,P,P,6,6,6,1)	MATS0160
DO 30 I=1,6	MATS0165
DO 30 J=I,6	MATS0170
P(I,J)=(P(I,J)+P(J,I))/2.	MATS0175
P(J,I)=P(I,J)	MATS0180
30 CONTINUE	MATS0185
IF(TOUT=TSEC) 3,3,4	MATS0220
3 CONTINUE	MATS0230
TOUT=TOUT+TPRINT	MATS0240
NOUT=2	MATS0250
C NOUT IS USED TO INDICATE OTHER OUTPUT WANTED WHEN = 2	MATS0260
CALL OUTC	MATS0270
CALL OUTP	MATS0280
4 CONTINUE	MATS0290
C LSTAT IS SET 2 BY INPUT CARDS IF ANY EARTH BASED TRACKING	MATS0300
LSTAT=LSTAT	MATS0310
GO TO (6,5),LSTAT	MATS0320
5 CONTINUE	MATS0330
CALL EARTR	MATS0340
C EARTR UDDATS COV MATRIX P FOR EARTH BASED TRACKING	MATS0350
6 CONTINUE	MATS0360
LONB=LONB	MATS0370
GO TO (8,7),LONB	MATS0380
C LONB IS SET 2 BY INPUT CARDS IF ANY ONBOARD MEASUREMENTS MADE	MATS0390
7 CONTINUE	MATS0400
C ONBTR UPDATES COV MATRIX P FOR THE ONBOARD MEASUREMENTS	MATS0410
CALL ONBTR	MATS0420
8 CONTINUE	MATS0430
LMB=LMB	MATS0440

MATSUB (Cont'd)

	GO TO (10,9),LMB	MATS0450
C	LMB IS SET 2 BY INPUT CARDS IF MOON BASED BEACONS USED	MATS0460
	9 CONTINUE	MATS0470
	CALL MONBTR	MATS0480
C	MONBTR UPDATS COV MATRIX P FOR BEACONS ON MOON	MATS0490
	10 CONTINUE	MATS0500
	GO TO (20,19), NOUT	MATS0510
	19 CONTINUE	MATS0520
	RMSP=SQRTF (P (1,1)+P (2,2)+P (3,3))	MATS0530
	RMSVP=SQRTF(P (4,4)+P (5,5)+P (6,6))	MATS0540
	WRITE OUTPUT TAPE NUTS,700,RMSP,RMSVP	MATS0550
700	FORMAT(42H KNOWLEDGE OF STATE AFTER ALL OBSERVATIONS,/ 124H RMS POSITION=,E15.8,25H RMS VELOCITY=, 2E15.8)	MATS0560
	20 CONTINUE	MATS0580
C	NUMBERS 11-16 RESERVED FOR FUTURE MEASUREMENTS	MATS0590
	IGUID=IGUID	MATS0600
	GO TO (18,17),IGUID	MATS0610
C	IGUID IS SET BY INPUT TO MAIN PROGRAM IF GUIDANCE CALCULATIONS ARE MADE	MATS0620
	17 CONTINUE	MATS0630
	CALL MATRX(AO,PFTA,PFTA,6,6,6,1)	MATS0640
	DO 31 I=1,6	MATS0650
	DO 31 J=I,6	MATS0655
	PFTA(I,J)=(PFTA(I,J)+PFTA(J,I))/2.	MATS0660
	PFTA(J,I)=PFTA(I,J)	MATS0665
	31 CONTINUE	MATS0670
	CALL INVAO(AO,AOI)	MATS0675
	CALL MATRX(TFTA,AOI,TFTA,3,6,6,0)	MATS0680
	CALL GUID	MATS0685
C	GUID PERFORMS THE GUIDANCE CALCULATIONS	MATS0690
	18 CONTINUE	MATS0700
	TSECP=TSEC	MATS0710
	RETURN	MATS0720
	END	MATS0730
		MATS0740
		MATS0750
		MATS

Page Intentionally Left Blank

Subroutine: MNA

Purpose: To provide the rotation matrix EMN which transforms moon centered coordinates in the earth's true equator and equinox to moon centered coordinates in the moon's true equator.

Calling Sequence:

CALL MNA (TIME, OM, CR, DT, EPSIL, RO, G, GP, WW, EMN)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	TIME	1	d	days	Days since 1950.0
I	OM	1	Ω		Output from NUTAIT: (Arg. Descending node)
I	CR	1	ζ	radians	Output from NATAIT: (mean long. of the moon)
I	DT	1	$\Delta\psi + d\psi$	radians	Output from NUTAIT: (nutation in longitude)
I	EPSIL	1	$\bar{e} + \Delta e + de$	radians	Output from NUTAIT: (mean obliquity and nutation in obliquity)

(Cont'd)

Common storages used or required:

None.

Subroutines required:

System double precision routines.

Functions required:

INTF, SORT, SIN, COS, ACOS

Approximate number of storages required:

(Cont'd.)

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
0	RO	1	ρ		Libration term
0	G	1	g	radians	Mean anomaly of the moon
0	GP	1	g	radians	Mean anomaly of the sun
0	WW	1	ω	radians	Argument of the perigee of the moon
0	EMN	3,3			Rotation matrix

Transformation From Earth's True Equator to Moon's True Equator.

The two rectangular systems are related through Λ , Ω' , and i by the rotation:

$$\begin{pmatrix} x \\ y \\ z \end{pmatrix}_{\text{MOON}} = \begin{pmatrix} b_{11} & b_{12} & b_{13} \\ b_{21} & b_{22} & b_{23} \\ b_{31} & b_{32} & b_{33} \end{pmatrix} \begin{pmatrix} x' \\ y' \\ z' \end{pmatrix}_{\text{EARTH}}$$

where

$$b_{11} = \cos \Lambda \cos \Omega' - \sin \Lambda \sin \Omega' \cos i$$

$$b_{12} = \cos \Lambda \sin \Omega' + \sin \Lambda \cos \Omega' \cos i$$

$$b_{13} = \cos \Lambda \sin i$$

$$b_{21} = -\sin \Lambda \cos \Omega' - \cos \Lambda \sin \Omega' \cos i$$

$$b_{22} = -\sin \Lambda \sin \Omega' + \cos \Lambda \cos \Omega' \cos i$$

$$b_{23} = \cos \Lambda \sin i$$

$$b_{31} = \sin \Omega' \sin i$$

$$b_{32} = -\cos \Omega' \sin i$$

$$b_{33} = \cos i$$

i is the inclination of the moon's true equator to the earth's equator

Ω' is the right ascension of the ascending node of the moon's true equator

Λ is the anomaly from the node to the X axis

$$\Lambda = \Delta + (\text{C} + \Upsilon) - (\Omega + \sigma)$$

Δ is the anomaly from the node to the ascending node of the moon's true equator on the ecliptic

Ω is the mean longitude of the descending node of the moon's mean equator on the ecliptic

C is the mean longitude of the moon

σ is the libration in the node

Υ is the libration in the mean longitude

ρ is the libration in the inclination.

$\delta\psi$, ϵ , Ω , and C are input quantities obtained from NUTAIT. The remainder are computed from the following equations.

I = inclination of moon's equator to ecliptic

$$I = 1.535^\circ$$

g = mean anomaly of moon

$$g = 215.54013 + 13.064992 d$$

g' = mean anomaly of sun

g' = $358.009067 + .9856005 d$

ω = argument of perigee of moon

ω = $196.745632 + .1643586 d$

where d = days from 1950.

$$\sigma \sin I = -.0302777 \sin g + .0102777 \sin (g + 2\omega) - .00305555 \sin (2g + 2\omega)$$

$$\tau = -.003333 \sin g + .0163888 \sin g' + .005 \sin 2\omega$$

$$\rho = -.0297222 \cos g + .0102777 \cos (g + 2\omega) - .00305555 \cos (2g + 2\omega)$$

$$\cos i = \cos (\Omega + \sigma + \delta\psi) \sin \epsilon \sin (I + \rho)$$

$$+ \cos \epsilon \cos (I + \rho)$$

$$0 < i < 90^\circ$$

$$\sin \Omega' = -\sin (\Omega + \sigma + \delta\psi) \sin (I + \rho) \csc i$$

$$-90^\circ < \Omega' < 90^\circ$$

$$\sin \Delta = -\sin (\Omega + \sigma + \delta\psi) \sin \epsilon \csc i$$

$$\cos \Delta = -\sin (\Omega + \sigma + \delta\psi) \sin \Omega' \cos \epsilon$$

$$-\cos (\Omega + \sigma + \delta\psi) \cos \Omega'$$

$$0^\circ \leq \Delta < 360^\circ$$

Reference: JPL Technical Report No. 32-223

MNA

* LABEL
* SYMBOL TABLE

CEC20AH

SUBROUTINE MNA(TIME,OM,CR,DT,EPSIL,RO,G,GP,WW,EM)

DIMENSION EM(3,3),DF(3)

D = TIME

T = D/36525,

T2 = T*T

T3 = T2*T

A=13.064992

DO 6 I=1,3

DD=D

DD=DD*(A/360.)

DD=DD-INTF(DD)

DF(I)=DD

GO TO (4,5,6),I

4 A=,9856005

GO TO 6

5 A=,1643586

6 CONTINUE

G=215.54013*360.*DF(1)

GP=358.009067*360.*DF(2)

WW=196.745632*360.*DF(3)

G = G*,017453296

GP = GP*,017453296

WW = WW*,017453296

YN = 1.535*,017453296

RO = -.0297222*COSF(G) + .01020777*COSF(G+2.*WW)

1 -.00305555*COSF(2.*G+2.*WW)

TA = -.003333*SINF(G) + .0163888*SINF(GP)

1 +.005*SINF(2.*WW)

SG = -.0302777*SINF(G) + .0102777*SINF(G+2.*WW)

1 -.00305555*SINF(2.*G+2.*WW)

SG = (SG*,017453296)/SINF(YN)

RO = RO*,017453296

TA = TA*,017453296

YN = YN + RO

RO = OM + SG + DT

CI = COSF(RO)*SINF(EPSIL)*SINF(YN)

1 *COSF(EPSIL)*COSF(YN)

SI = 1. - CI**2

SI = SQRTF(SI)

SO = -SINF(RO)*SINF(YN)/SI

CO = 1. - SO**2

CO = SQRTF(CO)

SD = -SINF(RO)*SINF(EPSIL)/SI

CD = -SINF(RO)*SO*COSF(EPSIL) - COSF(RO)*CO

DL = ACOSF(CD)

IF(SD)1,3,3

1 DL = 6.283185306 - DL

3 CONTINUE

SMNA

SMNA

SMNA

SMNA000

SMNA001

SMNA002

SMNA003

SMNA004

SMNA005

SMNA006

SMNA007

SMNA008

SMNA009

SMNA010

SMNA011

SMNA012

SMNA013

SMNA014

SMNA015

SMNA016

SMNA017

SMNA018

SMNA019

SMNA020

SMNA021

SMNA022

SMNA023

SMNA024

SMNA025

SMNA026

SMNA027

SMNA028

SMNA029

SMNA030

SMNA031

SMNA032

SMNA033

SMNA034

SMNA035

SMNA036

SMNA037

SMNA038

SMNA039

SMNA040

SMNA041

SMNA042

SMNA043

SMNA044

SMNA045

SMNA046

SMNA047

MNA (Cont'd)

```

CA = DL + (CR + TA) - (OM + SG)
SA = SINF(CA)
CA = COSF(CA)
RO = COSF(RO)*SINF(EPSIL)/(SI*CD)
EM(1,1) = CA*CO - SA*SO*CI
EM(1,2) = CA*SO + SA*CO*CI
EM(1,3) = SA*SI
EM(2,1) = -SA*CO - CA*SO*CI
EM(2,2) = -SA*SO + CA*CO*CI
EM(2,3) = CA*SI
EM(3,1) = SO*SI
EM(3,2) = -CO*SI
EM(3,3) = CI
RETURN
END

```

```

SMNA048
SMNA049
SMNA050
SMNA051
SMNA052
SMNA053
SMNA054
SMNA055
SMNA056
SMNA057
SMNA058
SMNA059
SMNA060
SMNA061
SMNA

```

Subroutine: MNAND

Purpose: To compute the matrix M used to perform the velocity transformation corresponding to the position transformation described in MNA.

Calling Sequence:

CALL MNAND (TIME, RO, G, GP, WW, EM, DM)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	TIME	1	d	days	Days since 1950.0
I	RO	1	ρ	radians	Output from MNA; see description
I	G	1	g	radians	Output from MNA; see description
I	GP	1	g'	radians	Output from MNA; see description
I	WW	1	ω	radians	Output from MNA; see description
I	EM	3,3	M		Output from MNA; matrix M
O	DM	3,3	\dot{M}		Matrix \dot{M}

Common storages used or required:

None

Subroutines required:

None

Functions required:

COS

Approximate number of storages required:

Theory and Equations

In transforming lunacentric position coordinates relative to the earth's equator and equinox of 1950.0 to coordinates relative to the moon's true equator, three matrices are computed. Matrix A (from ROTEQ) rotates the coordinates to equinox of date, matrix N (from NUTAIT) accounts for the nutation of the earth about its precessing mean equator, and matrix M (from MNA) transforms to the position relative to the moon's true equator.

$$\text{Then } \begin{pmatrix} X \\ Y \\ Z \end{pmatrix}_{\text{moon}} = \text{MNA} \begin{pmatrix} X \\ Y \\ Z \end{pmatrix}_{\text{earth, 1950.0}}$$

Assuming that $\dot{N} = \dot{A} = 0$

$$\begin{pmatrix} \dot{X} \\ \dot{Y} \\ \dot{Z} \end{pmatrix}_{\text{moon}} = \text{MNA} \begin{pmatrix} \dot{X} \\ \dot{Y} \\ \dot{Z} \end{pmatrix}_{\text{earth, 1950}} + \dot{\text{MNA}} \begin{pmatrix} X \\ Y \\ Z \end{pmatrix}_{\text{earth, 1950}}$$

The $\dot{\text{M}}$ matrix is computed from the equations:

$$\dot{\text{M}} = \begin{pmatrix} M_{21}\dot{\Lambda} & M_{22}\dot{\Lambda} & M_{23}\dot{\Lambda} \\ -M_{11}\dot{\Lambda} & -M_{12}\dot{\Lambda} & -M_{13}\dot{\Lambda} \\ 0 & 0 & 0 \end{pmatrix}$$

where M_{ij} are the elements of M, and

$$\dot{\Lambda} = \dot{\Delta} + \dot{\zeta} + \dot{\epsilon} - \dot{\Omega} - \dot{\sigma}$$

$$\dot{\Delta} = -\rho (\dot{\Omega} + \dot{\sigma})$$

$$\dot{\zeta} = 0.266170762 \times 10^{-5} - 0.12499171 \times 10^{-13} T \text{ rad/sec; } T = d/36525$$

$$\dot{\Omega} = -0.1069698435 \times 10^{-7} + 0.23015329 \times 10^{-3} T \text{ rad/sec}$$

$$\begin{aligned} \dot{\iota} = & -0.1535272946 \times 10^{-9} \cos g \\ & +0.569494067 \times 10^{-10} \cos g \\ & +0.579473484 \times 10^{-11} \cos 2\omega \text{ rad/sec} \end{aligned}$$

$$\begin{aligned} \dot{\sigma} = & -0.520642191 \times 10^{-7} \cos g \\ & +0.1811774451 \times 10^{-7} \cos (g+2\omega) \\ & -0.1064057858 \times 10^{-7} \cos (2\omega+2g) \text{ rad/sec} \end{aligned}$$

Reference: JPL Technical Report No. 32-223

MNAND

```

* LABEL
* SYMBOL TABLE
SUBROUTINE MNAND(TIME,RO,G,GP,WW,EM,DM)
DIMENSION DM(3,3),EM(3,3)
T = TIME/36525.
CRD = .266170762E-5 = .12499171E-13*T
OMD = -.1069698435E-7 + .23015329E-13*T
TAD = -1.535272946*COSF(G) + .569494067*COSF(GP)
1 + .0579473484*COSF(2.*WW)
TAD = .1E-9*TAD
SGD = -.520642191*COSF(G) + .1811774451*COSF(G+2.*WW)
1 -.1064057858*COSF(2.*WW+2.*G)
SGD = .1E-6*SGD
DLD = -RO*(OMD + SGD)
CAD = DLD + CRD + TAD - OMD - SGD
DM(1,1) = EM(2,1)*CAD
DM(1,2) = EM(2,2)*CAD
DM(1,3) = EM(2,3)*CAD
DM(2,1) = -EM(1,1)*CAD
DM(2,2) = -EM(1,2)*CAD
DM(2,3) = -EM(1,3)*CAD
DM(3,1) = 0,0
DM(3,2) = 0,0
DM(3,3) = 0,0
RETURN
END

```

```

MNAN
MNAN
MNAN0000
MNAN0010
MNAN0020
MNAN0030
MNAN0040
MNAN0050
MNAN0060
MNAN0070
MNAN0080
MNAN0090
MNAN0100
MNAN0110
MNAN0120
MNAN0130
MNAN0140
MNAN0150
MNAN0160
MNAN0170
MNAN0180
MNAN0190
MNAN0200
MNAN0210
MNAN0220
MNAN

```

Subroutine: MONBTR

Purpose: To obtain the position and velocity vectors of the vehicle relative to the beacon and determine if the beacon is in view of the vehicle. The station location partials are computed and subroutine COMPHQ called to update the state covariance matrix for the measurements being made. The types of measurements possible are range, range rate, right ascension, and declination.

Calling Sequence:

CALL MONBTR

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I					Quantities obtained from common
O					Quantities placed in common

Common storages used or required:

T, S, C, IC

Subroutines required:

COMPHQ, DOT, INTRI, MATRX, MNAND, MNA, NUTAIT, TRAC

Functions required:

ASIN, ATAN, FNORM, SQRT
(FIL)(SLO)(STH)

Approximate number of storages required:

495 DEC

MONBTR Partial Derivatives

MONBTR computes two partial matrices which are used in COMPHQ to evaluate station location errors. The matrices are the following:

$$\text{STPARS} = \begin{pmatrix} \frac{\partial x_1}{\partial \text{LAT}} & \frac{\partial x_1}{\partial \text{LON}} & \frac{\partial x_1}{\partial \text{ALT}} \\ \frac{\partial x_2}{\partial \text{LAT}} & \frac{\partial x_2}{\partial \text{LON}} & \frac{\partial x_2}{\partial \text{ALT}} \\ \frac{\partial x_3}{\partial \text{LAT}} & \frac{\partial x_3}{\partial \text{LON}} & \frac{\partial x_3}{\partial \text{ALT}} \end{pmatrix}$$

$$\text{STPARD} = \begin{pmatrix} \frac{\partial \dot{x}_1}{\partial \text{LAT}} & \frac{\partial \dot{x}_1}{\partial \text{LON}} & \frac{\partial \dot{x}_1}{\partial \text{ALT}} \\ \frac{\partial \dot{x}_2}{\partial \text{LAT}} & \frac{\partial \dot{x}_2}{\partial \text{LON}} & \frac{\partial \dot{x}_2}{\partial \text{ALT}} \\ \frac{\partial \dot{x}_3}{\partial \text{LAT}} & \frac{\partial \dot{x}_3}{\partial \text{LON}} & \frac{\partial \dot{x}_3}{\partial \text{ALT}} \end{pmatrix}$$

$$\text{where } \vec{x} = \begin{pmatrix} x_1 \\ x_2 \\ x_3 \end{pmatrix} = -\vec{x}_V + \vec{x}_B \quad \equiv \text{XREL (FORTRAN)}$$

$$\vec{\dot{x}} = \begin{pmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{pmatrix} = -\vec{\dot{x}}_V + \vec{\dot{x}}_B \quad \equiv \text{VREL (FORTRAN)}$$

$$\frac{\partial x_i}{\partial \text{LAT}} = \frac{\partial x_{Bi}}{\partial \text{LAT}} \quad \frac{\partial \dot{x}_i}{\partial \text{LAT}} = \frac{\partial \dot{x}_{Bi}}{\partial \text{LAT}} \quad i = 1, 2, 3$$

$$\vec{X}_B = (MNA)^T \vec{X}_{BM}$$

$$\vec{X}_B = (MNAND)^T \vec{X}_{BM} + \cancel{(MNA)^T \vec{X}_{BM}} \quad (=0)$$

where subscripts BM indicate beacon moon-fixed coordinates.

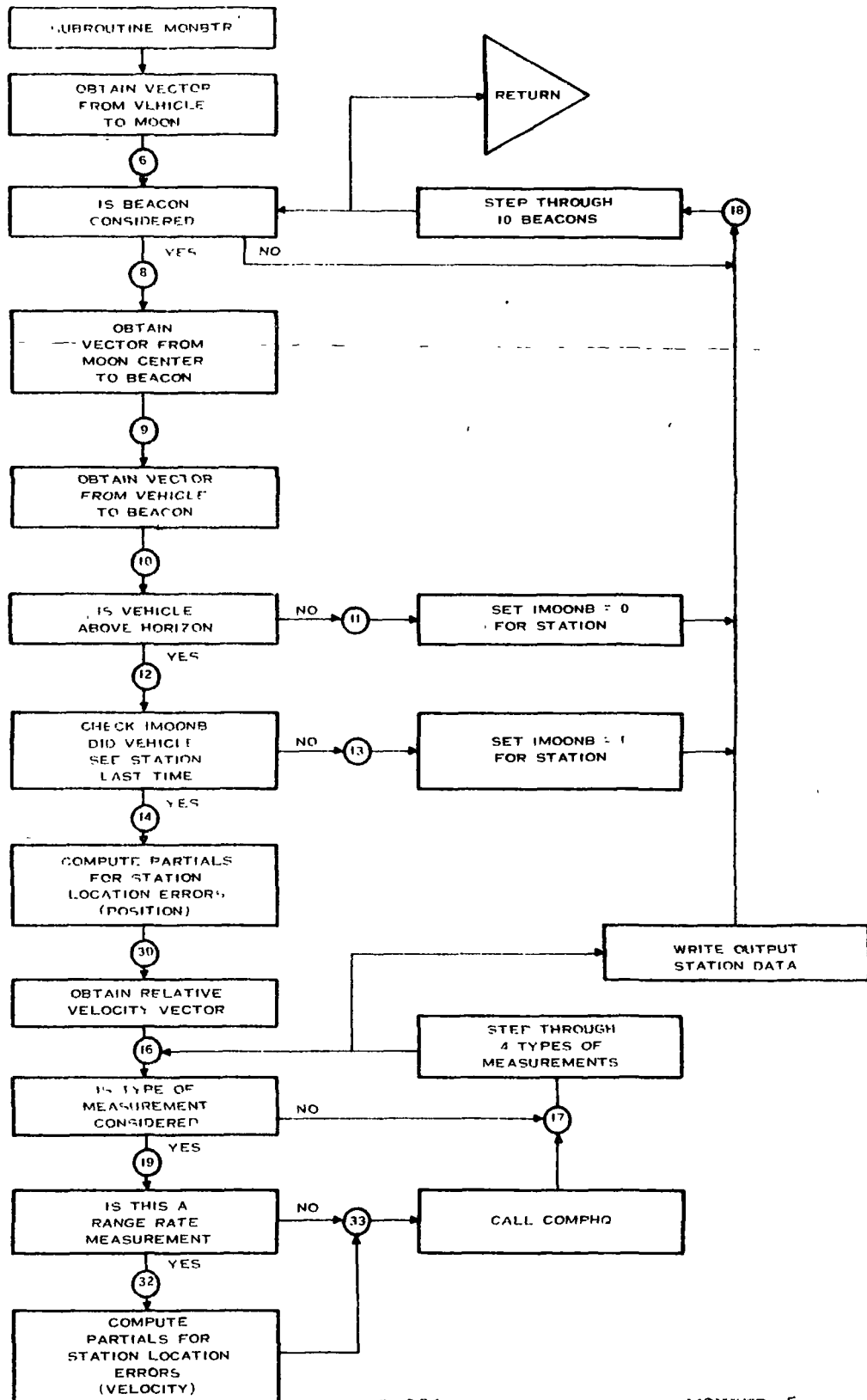
The transformations MNA and MNAND are obtained by calling the sub-routines MNA and MNAND.

$$\vec{X}_{BM} = (R + ALT) \begin{pmatrix} \cos LAT \cos LON \\ \cos LAT \sin LON \\ \sin LAT \end{pmatrix}$$

$3 \times 1 \quad 3 \times 3 \quad 3 \times 1$

$$\begin{pmatrix} \frac{\partial X_1}{\partial PAR} \\ \frac{\partial X_2}{\partial PAR} \\ \frac{\partial X_3}{\partial PAR} \end{pmatrix} = (MNA)^T \begin{pmatrix} \frac{\partial X_{BM}}{\partial PAR} \\ \frac{\partial Y_{BM}}{\partial PAR} \\ \frac{\partial Z_{BM}}{\partial PAR} \end{pmatrix}$$

$$\begin{pmatrix} \frac{\partial \dot{X}_1}{\partial PAR} \\ \frac{\partial \dot{X}_2}{\partial PAR} \\ \frac{\partial \dot{X}_3}{\partial PAR} \end{pmatrix} = (MNAND)^T \begin{pmatrix} \frac{\partial X_{BM}}{\partial PAR} \\ \frac{\partial Y_{BM}}{\partial PAR} \\ \frac{\partial Z_{BM}}{\partial PAR} \end{pmatrix}$$



MONBTR

* LABEL	MONB
* SYMBOL TABLE	MONB
CEC2012 SUBROUTINE MONBTR	MONB
SUBROUTINE MONBTR	MONB0000
COMMON T,S,C,IC	MONB0010
DIMENSION	MONB0020
1T(1360),S(1000),C(1000),IC(1),XREL(3),VREL(3)	MONB0030
1,PO(22),VE(22),AN(3,3),EM(3,3),ISBOON(10),U(3),EN(3)	MONB0040
2,RT(3),E(3),ETM(3,3),IMOONB(10),DM(3,3),DUM(3,3)	MONB0050
3,RMB(3),TYMEAS(4,10),X(3),VX(3),OUTPUT(6)	MONB0060
DIMENSION STPARS(3,3),DUD(3,3),STPARD(3,3)	MONB0065
EQUIVALENCE (T,TDUM),(S,SDUM),(C,CDUM),(IC,ICDUM)	MONB0070
1,(C(895),XREL),(C(898),VREL),(C(894),OBNO),(C(893),XMAG),	MONB0080
2(C(892),DEX),(C(891),DEN1),(C(890),DEN2)	MONB0090
3,(C(889),DEX2),(C(888),DEX3),(C(652),P),(C(973),OUTPUT)	MONB0100
1,(C(13),TW),(C(14),TF),(C(62),PO),(IC(3),NOR)	MONB0110
2,(IC(190),LSTAT),(C(138),AN),(S(24),A),(C(120),EM)	MONB0120
3,(IC(140),ISBCON),(S(72),DR),(IC(220),IMOONB),(C(649),TSECP)	MONB0130
4,(C(30),TSEC),(IC(140),TYMEAS),(C(15),X),(C(18),VX)	MONB0140
EQUIVALENCE (C(800),STPARD),(C(788),STPARS)	MONB0145
CALL SETN(NIN,NUTS)	MONB0147
DELTT=TSEC-TSECP	MONB0150
LSTAT=LSTAT	MONB0160
GO TO(1,2),LSTAT	MONB0170
1 CONTINUE	MONB0180
NB=NOR-1	MONB0190
DIS=1.E10	MONB0200
CALL INTR1(TW,TF,NB,PO,1,VE,DIS)	MONB0210
2 CONTINUE	MONB0220
TIME=TW+TF	MONB0230
CALL NUTAIT(TIME,OM,CR,DT,EM,EPSIL)	MONB0240
CALL MNA(TIME,OM,CR,DT,EPSIL,RO,G,GP,WW,ETM)	MONB0250
CALL MNAND(TIME,RO,G,GP,WW,ETM,DM)	MONB0260
IF(NOR-2)3,5,3	MONB0270
3 CONTINUE	MONB0280
DO 4 I=1,3	MONB0290
J=20-I	MONB0300
XREL(I)=PO(J)-X(I)	MONB0310
VREL(I)=VE(J)-VX(I)	MONB0320
4 CONTINUE	MONB0330
GO TO 7	MONB0340
5 CONTINUE	MONB0350
DO 6 I=1,3	MONB0360
XREL(I)=-X(I)	MONB0370
VREL(I)=-VX(I)	MONB0380
6 CONTINUE	MONB0390
C XREL POSITION VECTOR FROM VEHICLE TO MOON CENTER 1950	MONB0400
C VREL RELATIVE VELOCITY OF MOON CENTER 1950	MONB0410
7 CONTINUE	MONB0420
NN=485	MONB0430
DO 18 III=1,10	MONB0440

MONETR (Cont'd)

15	CONTINUE	MONB0810
C	RMB ROTATIONAL VELOCITY OF MOON BEACON 1950	MONB0820
	DO 16 I=1,3	MONB0830
	VREL(I)=VREL(I)+RMB(I)	MONB0840
C	VREL RELATIVE VELOCITY OF MOON BEACON WRT THE VEHICLE	MONB0850
16	CONTINUE	MONB0860
	OBNO=DELTT/S(NN+13)	MONB0870
	XMAG=FNORM(XREL)	MONB0880
	DEX=XREL(1)**2+XREL(2)**2	MONB0890
	DEN1=1./SQRTF(DEX)/XMAG**2	MONB0900
	DEN2=1./DEX	MONB0910
	DEX2=XMAG*XMAG	MONB0920
	DEX3=1./XMAG	MONB0930
C	THE ABOVE QUANTITIES ARE USED IN COMPUTATIONS OF H MATRIX	MONB0940
	DEC=ASINF(DEX3*XREL(3))	MONB0942
	OUTPUT(5)=DEC/DR	MONB0944
	RA=ATANF(XREL(2)/XREL(1))	MONB0946
	OUTPUT(3)=RA/DR	MONB0948
	OUTPUT(1)=XMAG	MONB0949
	DO 17 JJJ=1,4	MONB0950
	IF(TYMEAS(JJJ,III))17,17,19	MONB0960
19	CONTINUE	MONB0962
	IF(JJJ=4)33,32,33	MONB0964
32	CONTINUE	MONB0966
	DO 34 I=1,3	MONB0968
	DO 34 J=1,3	MONB0970
	STPARD(I,J)=0.	MONB0972
	DO 34 K=1,3	MONB0974
34	STPARD(I,J)=STPARD(I,J)+DUM(K,I)*DUD(K,J)	MONB0975
33	CONTINUE	MONB0976
	CALL COMPHQ(JJJ,2,NN)	MONB0978
17	CONTINUE	MONB0980
	WRITE OUTPUT TAPE NUTS,700,III,OUTPUT	MONB0982
700	FORMAT(13H MOON BEACON ,I2,	MONB0983
	1/4H RNGE15.8,5H RGRE15.8,	MONB0984
	25H RAE15.8,5H RARE15.8,5H DECE15.8,5H DCRE15.8)	MONB0985
	DO 20 I=1,6	MONB0986
20	OUTPUT(I)=0.	MONB0987
18	CONTINUE	MONB0990
	RETURN	MONB1000
	END	MONB

Subroutine: MULT

Purpose: To find the product matrix of two 3 x 3 matrices.

Calling Sequence:

CALL MULT (A, B, C)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	A	3,3			First input matrix
I	B	3,3			Second input matrix
O	C	3,3			C = AB

Common storages used or required: None

Subroutines required: None

Functions required: None

Approximate number of storages required: _____

MULT

```
* LABEL
* SYMBOL TABLE
SUBROUTINE MULT(A,B,C,N)
DIMENSION A(3,3),B(3,3),C(3,3)
DO 1 I=1,3
DO 1 J=1,3
C(I,J) = 0.
DO 1 K=1,3
1 C(I,J) = C(I,J) + A(I,K)*B(K,J)
3 RETURN
END
```

```
MULT
MULT
MULT0000
MULT0010
MULT0020
MULT0030
MULT0040
MULT0050
MULT0060
MULT0070
MULT
```

Subroutine: NUTAIT

Purpose: To evaluate the elements of the nutation matrix which relates the Cartesian coordinates expressed in the true equator and equinox to those in the mean equator and equinox.

Calling Sequence:

CALL NUTAIT (TIME, OM, CR, DT, EN, EPSIL)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	TIME	1	T	days	Total number days from ref.epoch
O	OM	1	Ω	radians	Argument of moon's descending node
O	CR	1	CR	radians	Mean longitude of moon
O	DT	1	$\Delta\psi + d\psi$	radians	Nutation in longitude of equinox
O	EN	3,3	N	(-)	Nutation matrix
O	EPSIL	1	$\bar{\epsilon} + d\epsilon$	radians	True obliquity

Common storages used or required:

None

Subroutines required:

None

Functions required:

INTF, SINF, COSF

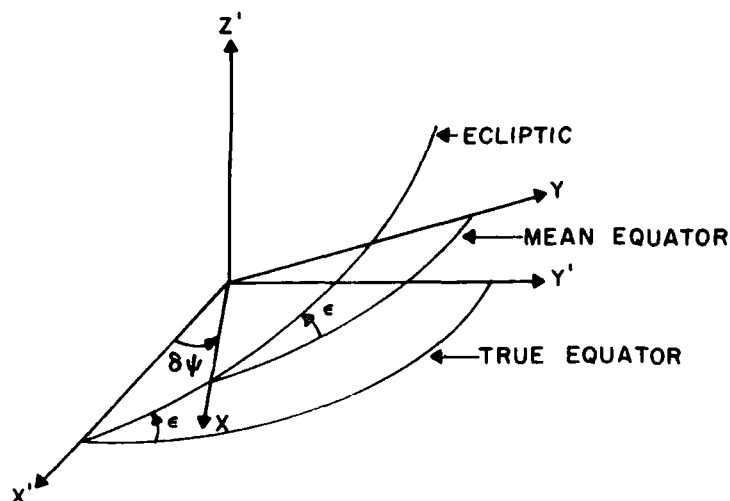
Approximate number of storages required:

NUTAIT

Method and Theory

The input time is converted to Julian centuries of 36525 days past the reference epoch (currently, 0^h January 1, 1950, E.T.). Where the computed angles are likely to be extremely large, the largest contributing term is reduced to the first revolution by the internal function DF(X). By using double precision arithmetic, this technique also helps to control round-off errors more closely as well as to keep the computed angles reasonable.

The relationship between the Cartesian coordinates expressed in the true equator and equinox and those expressed in the mean equator and equinox is shown in the following sketch:



The nutations are given by the following:

$$\text{For obliquity} \quad \delta\epsilon = \Delta\epsilon + d\epsilon$$

$$\text{For longitude} \quad \delta\Psi = \Delta\Psi + d\Psi$$

In the above equations, $\Delta\epsilon$, $\Delta\Psi$ express the long-period contributions and $d\epsilon$, $d\Psi$ the short-period contributions.

Both ϵ and Ψ are computed as functions of Ω , CR, Γ' , L, Γ where

$$\Omega = 12.112790 - 360*DF(1) + .0020795T + .002081T^2 + .000002T^3$$

$$CR = 64.375452 + 360*DF(2) - .001131575T - .00113015T^2 - .0000019T^3$$

$$\Gamma' = 208.84399 + 360*DF(3) - .010334T - .010343T^2 - .000012T^3$$

$$\Gamma = 282.08053 + .0000470684D + .00045525T + .0004575T^2 + .000003T^3$$

$$L = 280.08121 + 360*DF(4) + .000303 (T + T^2)$$

T in the above equations is the number of Julian years past the reference epoch and the function DF(X) is

$$DF(X) = d \frac{a}{360}$$

where $a = .052953922, 13.176397, .11140408, .98564734$

and d is the number of days past the reference epoch.

$$\text{Then } \Delta\epsilon \times 10^4 = 25.5844 \cos \Omega - .2511 \cos 2\Omega$$

$$+ 1.5336 \cos 2L + .0666 \cos (3L - \Gamma)$$

$$- .0258 \cos (L + \Gamma) - .0183 \cos (2L - \Omega)$$

$$- .0067 \cos (2\Gamma' - \Omega)$$

$$\Delta\epsilon \times 10^4 = .2456 \cos 2CR + .0508 \cos (2CR - \Omega)$$

$$+ .0369 \cos (3CR - \Gamma') - .0139 \cos (CR + \Gamma')$$

$$- .0086 \cos (CR - \Gamma' + \Omega) + .0083 \cos (CR - \Gamma' - \Omega)$$

$$+ .0061 \cos (3CR + \Gamma' - 2L) + .0064 \cos (3CR - \Gamma' - \Omega)$$

$$\Delta\Psi \times 10^4 = -(47.8927 + .0482T) \sin \Omega$$

$$+ .5800 \sin 2\Omega - 3.5361 \sin 2L - .1378 \sin (3L - \Gamma)$$

$$+ .0594 \sin (L + \Gamma) + .0344 \sin (2L - \Omega) + .0125 \sin (2\Gamma' - \Omega)$$

$$+ .3500 \sin (L - \Gamma) + .0125 \sin (2L - 2\Gamma')$$

$$\begin{aligned}
d\psi \times 10^4 = & -.5658 \sin 2CR - .0950 \sin (2CR - \Omega) \\
& -.0725 \sin (3CR - \Gamma') + .0317 \sin (CR + \Gamma') \\
& + .0161 \sin (CR - \Gamma' + \Omega) + .0158 \sin (CR - \Gamma' - \Omega) \\
& -.0144 \sin (3CR + \Gamma' - 2L) - .0122 \sin (3CR - \Gamma' - \Omega) \\
& + .1875 \sin (CR - \Gamma') + .0078 \sin (2CR - 2\Gamma') \\
& + .0414 \sin (CR + \Gamma' - 2L) + .0167 \sin (2CR - 2L) \\
& -.0089 \sin (4CR - 2L).
\end{aligned}$$

The mean obliquity is calculated by

$$\bar{\epsilon} = 23.4457587 - .01309404T - .00000088T^2 + .00000050T^3$$

and the true obliquity by

$$\epsilon = \bar{\epsilon} + \delta\epsilon$$

The nutation matrix N relates the Cartesian coordinates expressed in the true equator and equinox to those in the mean equator and equinox by

$$\begin{vmatrix} X' \\ Y' \\ Z' \end{vmatrix} = N \begin{vmatrix} X \\ Y \\ Z \end{vmatrix}$$

where the primed system is the true equator and equinox and the unprimed is the mean equator and equinox.

Thus

$$\begin{aligned}
N_{11} &= \cos \delta\psi \\
N_{12} &= -\sin \delta\psi \cos \bar{\epsilon} \\
N_{13} &= \sin \delta\psi \sin \bar{\epsilon} \\
N_{21} &= \sin \delta\psi \cos \epsilon
\end{aligned}$$

$$N_{22} = \cos \delta\psi \cos \epsilon \cos \bar{\epsilon} + \sin \epsilon \sin \bar{\epsilon}$$

$$N_{23} = \cos \delta\psi \cos \epsilon \sin \bar{\epsilon} - \sin \epsilon \cos \bar{\epsilon}$$

$$N_{31} = \sin \delta\psi \sin \epsilon$$

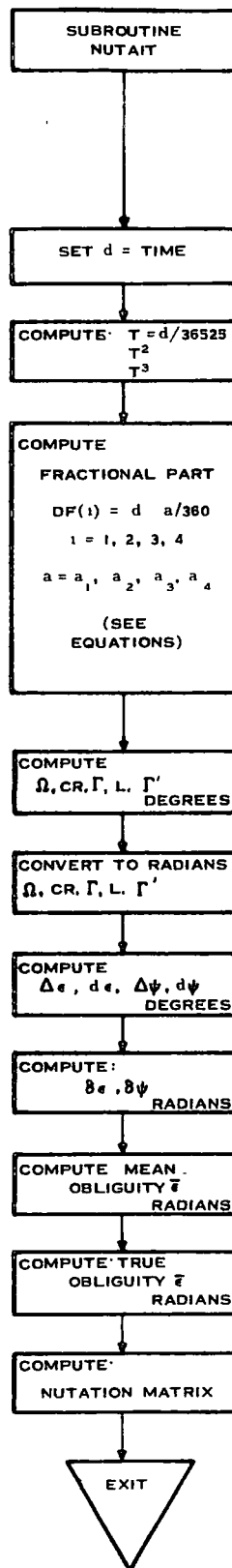
$$N_{32} = \cos \delta\psi \sin \epsilon \cos \bar{\epsilon} - \cos \epsilon \sin \bar{\epsilon}$$

$$N_{33} = \cos \delta\psi \sin \epsilon \sin \bar{\epsilon} + \cos \epsilon \cos \bar{\epsilon}$$

For numerical calculation, the above N matrix is expanded to the first order in $\delta\psi$ and $\delta\epsilon$:

$$N = \begin{vmatrix} 1 & -\delta\psi \cos \bar{\epsilon} & -\delta\psi \sin \bar{\epsilon} \\ \delta\psi \cos \bar{\epsilon} & 1 & -\delta\epsilon \\ \delta\psi \sin \bar{\epsilon} & \delta\epsilon & 1 \end{vmatrix}$$

Reference: JPL Technical Report No. 32-223



NUTAIT

WDL-TR2184

```

* LABEL NUTA
* SYMBOL TABLE NUTA
SUBROUTINE NUTAIT (TIME,OM,CR,DT,EN,ERSIL) NUTA00
DIMENSION EN(3,3) NUTA00
D = TIME NUTA00
T = D/36525. NUTA00
T2 = T*T NUTA00
T3 = T2*T NUTA00
OM = 12.112790-.052953922*D+.0020795*T+.002081*T2+.000002*T3 NUTA00
CR = 64.375452+13.176397*D-.001131575*T-.00113015*T2+.0000019*T3 NUTA00
GP = 208.84399+.11140408*D-.010334*T-.010343*T2-.000012*T3 NUTA00
VL = 280.08121+.98564734*D+.000303*(T+T2) NUTA00
G = 282.08053+.0000470684*D+.00045525*T+.0004575*T2+.000003*T3 NUTA01
OM = OM*.017453296 NUTA01
CR = CR*.017453296 NUTA01
GP = GP*.017453296 NUTA01
VL = VL*.017453296 NUTA01
G = G*.017453296 NUTA01
DE = .255844*COSF(OM)-.2511*COSF(2.*OM)+1.5336*COSF(2.*VL) NUTA01
1 +.0666*COSF(3.*VL-G)-.0258*COSF(VL+G)-.0183*COSF(2.*VL-OM) NUTA01
2 -.0067*COSF(2.*GP-OM) NUTA01
DD = .2456*COSF(2.*CR)+.0508*COSF(2.*CR-OM)+.0369*COSF(3.*CR-GP) NUTA01
1 -.0139*COSF(CR+GP)+.0086*COSF(CR-GP+OM)+.0083*COSF(CR-GP-OM) NUTA02
2 +.0061*COSF(3.*CR+GP-2.*VL)+.0064*COSF(3.*CR-GP-OM) NUTA02
DT = -(47.8927+.0482*T)*SINF(OM)+.58*SINF(2.*OM) NUTA02
1 -3.5361*SINF(2.*VL)-.1378*SINF(3.*VL-G)+.0594*SINF(VL+G) NUTA02
2 +.0344*SINF(2.*VL-OM)+.0125*SINF(2.*GP-OM)+.35*SINF(VL-G) NUTA02
3 +.0125*SINF(2.*VL-2.*GP) NUTA02
DS = -.5658*SINF(2.*CR)-.095*SINF(2.*CR-OM)-.0725*SINF(3.*CR-GP) NUTA02
1 +.0317*SINF(CR+GP)+.0161*SINF(CR-GP+OM)+.0158*SINF(CR-GP-OM) NUTA02
2 -.0144*SINF(3.*CR+GP-2.*VL)-.0122*SINF(3.*CR-GP-OM) NUTA02
3 +.1875*SINF(CR-GP)+.0078*SINF(2.*CR-2.*GP) NUTA02
4 +.0414*SINF(CR+GP-2.*VL)+.0167*SINF(2.*CR-2.*VL) NUTA03
5 -.0089*SINF(4.*CR-2.*VL) NUTA03
DE = .17453296E-5*(DE+DD) NUTA03
DT = .17453296E-5*(DT+DS) NUTA03
EB = 23.4457587-.01309404*T+.00000088*T2+.0000005*T3 NUTA03
EB = EB*.017453296 NUTA03
ERSIL = EB+DE NUTA03
EN(1,1) = 1. NUTA03
EN(1,2) = -DT*COSF(EB) NUTA03
EN(1,3) = -DT*SINF(EB) NUTA03
EN(2,1) = -EN(1,2) NUTA04
EN(2,2) = 1. NUTA04
EN(2,3) = -DE NUTA04
EN(3,1) = -EN(1,3) NUTA04
EN(3,2) = DE NUTA04
EN(3,3) = 1. NUTA04
RETURN NUTA04
END NUTA

```

Page Intentionally Left Blank

Subroutine: OBLN

Purpose: To compute the perturbing acceleration due to the earth's oblateness. The formula for the earth's potential includes the second, third and fourth spherical harmonics. Part of the input is a rotation matrix to equator and equinox of date, obtained by successive calls to ROTEQ, NUTAIT, and MULT. It also computes the first variation of the perturbing acceleration for the variational equations.

Calling Sequence:

CALL OBLN (XP, U, A, VJ, H, D, PO, AN, B, NEQ)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	XP	3	\bar{R}	Kilometers	Position vector
I	U	1	μ	Km^3/sec^2	Gravitational constant
I	A	1	R_E	Kilometers	Equatorial radius of the earth
I	VJ	1	J		Coefficient of second harmonic
I	H	1	H		Coefficient of third harmonic
I	D	1	D		Coefficient of fourth harmonic
O	PO	3	∇U		Perturbing acceleration
I	AN	3,3			Rotation matrix to equator and equinox of date

(Cont'd.)

Common storages used or required: None

Subroutines required: None

Functions required: SORT

Approximate number of storages required: 480 DEC

(Cont'd.)

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
O	B	3,3	$\partial \ddot{x}_i / \partial x_i$		Derivatives of ∇U
I	NEQ	1			Number of differential equations being integrated

OBLN computes the perturbing acceleration due to the earth's oblateness. The oblate potential of the earth is assumed to contain the second, third, and fourth spherical harmonics:

$$U = \frac{\mu}{R} \left\{ \frac{JR_E}{3R^2} (1 - 3 \sin^2 \phi) + \frac{HR_E^3}{5R^3} (3 \sin \phi - 5 \sin^3 \phi) + \frac{DR_E^4}{35R^4} (3 - 30 \sin^2 \phi + 35 \sin^4 \phi) \right\}$$

where R_E is the equatorial radius of the earth and ϕ is the geocentric latitude, $\bar{R} = (X_1, X_2, X_3)$ is expressed in the mean equator and equinox of 1950.

The position vector $\bar{r} = (X, Y, Z)$ expressed in the true equator and equinox of date must be obtained to determine $\sin \phi$. The proper rotation matrix AN has been computed. Then,

$$\bar{r} = AN \bar{R}$$

and

$$\sin \phi = \frac{Z}{R} .$$

The perturbing acceleration is equal to ∇U :

$$\frac{\partial U}{\partial X_j} = -J\mu \frac{R_E^2}{R^4} \left\{ \left(1 - \frac{5Z^2}{R^2} \right) \frac{X_j}{R} + 2 \frac{Z}{R} AN_{3j} \right\}$$

$$-H\mu \frac{R_E^3}{R^5} \left\{ \left(3 - \frac{7Z^2}{R^2} \right) \frac{Z}{R} \frac{X_j}{R} + \left(-\frac{3}{5} + \frac{3Z^2}{R^2} \right) AN_{3j} \right\}$$

$$-D\mu \frac{R_E^4}{R^6} \left\{ \left(\frac{3}{7} - \frac{6Z^2}{R^2} + \frac{9Z^4}{R^4} \right) \frac{X_j}{R} + \left(\frac{12}{7} - \frac{4Z^2}{R^2} \right) \frac{Z}{R} AN_{3j} \right\}$$

for $j = 1, 2, 3$.

If the number of second order differential equations is less than or equal to three, RETURN is called at this point.

OBLN also computes the derivatives of the perturbing acceleration for use in the integration package. For this purpose, only the term arising from the second harmonic is retained; also, the coordinates are regarded as being expressed in the reference system of the mean equator and equinox of 1950.

Starting with

$$\nabla U_a = \left(\varepsilon_1 \frac{X_1}{R}, \varepsilon_1 \frac{X_2}{R}, \varepsilon_2 \frac{X_3}{R} \right)$$

where

$$\varepsilon_1 = -J\mu \frac{R_E^2}{R^4} \left(1 - \frac{5Z^2}{R^2} \right)$$

$$\varepsilon_2 = -J\mu \frac{R_E^2}{R^4} \left(3 - \frac{5Z^2}{R^2} \right)$$

yields

$$\frac{\partial \ddot{x}_1}{\partial x_j} = \varepsilon_1 \frac{x_1}{R} \left(\frac{1}{x_1} \frac{\partial x_1}{\partial x_j} - \frac{3}{R^2} \bar{R} \cdot \frac{\partial \bar{R}}{\partial x_j} \right) \\ + J\mu R_E^2 \frac{x_1}{R^7} \left\{ 10x_3 \frac{\partial x_3}{\partial x_j} + 2 \left(1 - 10 \frac{x_3^2}{R^2} \right) \bar{R} \cdot \frac{\partial \bar{R}}{\partial x_j} \right\}$$

$$\frac{\partial \ddot{x}_2}{\partial x_j} = \varepsilon_1 \frac{x_2}{R} \left(\frac{1}{x_2} \frac{\partial x_2}{\partial x_j} - \frac{3}{R^2} \bar{R} \cdot \frac{\partial \bar{R}}{\partial x_j} \right) \\ + J\mu R_E^2 \frac{x_2}{R^7} \left\{ 10x_3 \frac{\partial x_3}{\partial x_j} + 2 \left(1 - 10 \frac{x_3^2}{R^2} \right) R \cdot \frac{\partial R}{\partial x_j} \right\}$$

$$\frac{\partial \ddot{x}_3}{\partial x_j} = \varepsilon_2 \frac{x_3}{R} \left(\frac{1}{x_3} \frac{\partial x_3}{\partial x_j} - \frac{3}{R^2} \bar{R} \cdot \frac{\partial \bar{R}}{\partial x_j} \right) \\ + J\mu R_E^2 \frac{x_3}{R^7} \left\{ 10x_3 \frac{\partial x_3}{\partial x_j} + 2 \left(3 - 10 \frac{x_3^2}{R^2} \right) R \cdot \frac{\partial R}{\partial x_j} \right\}$$

Expanding the dot products and collecting terms gives

$$B_{11} = \varepsilon_1 \left(\frac{1}{R} - \frac{3x_1^2}{R^3} \right) + 2J\mu R_E^2 \frac{x_1^2}{R^7} \left(1 - 10 \frac{x_3^2}{R^2} \right)$$

$$B_{12} = \varepsilon_1 \left(-\frac{3x_1 x_2}{R^3} \right) + 2 J\mu R_E^2 \frac{x_1 x_2}{R^7} \left(1 - 10 \frac{x_3^2}{R^2} \right)$$

$$B_{13} = g_1 \left(-\frac{3X_1 X_3}{R^3} \right) + 2 J\mu R_E^2 \frac{X_1 X_3}{R^7} \left(6 - 10 \frac{X_3^2}{R^2} \right)$$

$$B_{21} = B_{12}$$

$$B_{22} = g_1 \left(\frac{1}{R} - \frac{3X_2^2}{R^3} \right) + 2 J\mu R_E^2 \frac{X_2^2}{R^7} \left(1 - 10 \frac{X_3^2}{R^2} \right)$$

$$B_{23} = g_1 \left(-\frac{3X_2 X_3}{R^3} \right) + 2 J\mu R_E^2 \frac{X_2 X_3}{R^7} \left(6 - 10 \frac{X_3^2}{R^2} \right)$$

$$B_{31} = B_{13}$$

$$B_{32} = B_{23}$$

$$B_{33} = g_2 \left(\frac{1}{R} - \frac{3X_3^2}{R^3} \right) + 2 J\mu R_E^2 \frac{X_3^2}{R^7} \left(8 - 10 \frac{X_3^2}{R^2} \right)$$

where $B\lambda_j = \frac{\partial \ddot{X}_i}{\partial X_j}$

For $R > 3R_E$, B is set equal to zero.

```

* LABEL
* SYMBOL TABLE
CEC2031 SUBROUTINE OBLN
SUBROUTINE OBLN(XP,U,A,VJ,H,D,PO,AN,B,NEQ)
DIMENSION X(3),PO(3),AN(3,3),XP(3),B(3,3)
RE=6378.15
DO 2 I=1,3
X(I) = 0.
DO 2 J=1,3
2 X(I) = X(I) + AN(I,J)*XP(J)
R2 = X(1)**2+X(2)**2+X(3)**2
R = SQRTF(R2)
UR2 = U/R2
AR = A/R
AR2 = AR*AR
AR3 = AR*AR2
AR4 = AR*AR3
ZR = X(3)/R
ZR2 = ZR*ZR
ZR4 = ZR2*ZR2
TM1 = (1.-5.*ZR2)/R
TM2 = 2.*ZR
TM3 = (3.-7.*ZR2)*ZR/R
TM4 = -.6+3.*ZR2
TM5 = (.42857143-6.*ZR2+9.*ZR4)/R
TM6 = (1.7142857-4.*ZR2)*ZR
T01 = -VJ*UR2*AR2
T02 = -H*UR2*AR3
T03 = -D*UR2*AR4
DO 1 I=1,3
1 PO(I) = T01*(TM1*XP(I)+TM2*AN(3,I))
1 +T02*(TM3*XP(I)+TM4*AN(3,I))
2 +T03*(TM5*XP(I)+TM6*AN(3,I))
IF(NEQ=3)3,3,4
3 CONTINUE
RETURN
4 CONTINUE
IF(R=3.*RE)5,5,6
6 CONTINUE
DO 7 I=1,3
DO 7 J=1,3
B(I,J)=0.
7 CONTINUE
GO TO 3
5 CONTINUE
G5=-T01/R
G6=5.*ZR2
G1=-G5*(1.-G6)
G2=-G5*(3.-G6)
G7=2.*G6
G8=X(1)/R

```

```

OBLN
OBLN
OBLN
OBLN0000
OBLN0010
OBLN0020
OBLN0030
OBLN0040
OBLN0050
OBLN0060
OBLN0070
OBLN0080
OBLN0090
OBLN0100
OBLN0110
OBLN0120
OBLN0130
OBLN0140
OBLN0150
OBLN0160
OBLN0170
OBLN0180
OBLN0190
OBLN0200
OBLN0210
OBLN0220
OBLN0230
OBLN0240
OBLN0250
OBLN0260
OBLN0270
OBLN0280
OBLN0290
OBLN0300
OBLN0310
OBLN0320
OBLN0330
OBLN0340
OBLN0350
OBLN0360
OBLN0370
OBLN0380
OBLN0390
OBLN0400
OBLN0410
OBLN0420
OBLN0430
OBLN0440
OBLN0450
OBLN0460
OBLN0470

```

```

.G9=X(2)/R
.G10=X(3)/R
B(1,1)=G1*(1,-3,*G8**2)*2.*G5*G8**2*(1,-G7)
B(1,2)=-3.*G1*G8*G9+2.*G5*G8*G9*(1,-G7)
B(1,3)=-3.*G1*G8*G10+2.*G5*G8*G10*(6,-G7)
B(2,1)=B(1,2)
B(2,2)=G1*(1,-3,*G9**2)+2.*G5*G9**2*(1,-G7)
B(2,3)=-3.*G1*G9*G10+2.*G5*G9*G10*(6,-G7)
B(3,1)=B(1,3)
B(3,2)=B(2,3)
B(3,3)=G2*(1,-3,*G10**2)+2.*G5*G10**2*(8,-G7)
GO TO 3
END

```

```

OBLN048
OBLN049
OBLN050
OBLN051
OBLN052
OBLN053
OBLN054
OBLN055
OBLN056
OBLN057
OBLN058
OBLN059
OBLN

```

OBLN -

S-301

Page Intentionally Left Blank

Subroutine: ONBTR

WDL-TR2184

Purpose: The subroutine obtains the relative position and velocity vectors from the vehicle to any of the six following bodies; Earth, Moon, Sun, Venus, Mars, and Jupiter. The bodies to be observed are established by input data. The types of observation which can be made on the body are range, range rate, right ascension, and declination. The selection of types of measurements to be made is also by input data. ONBTR calls subroutine COMPHO to perform the updating of the covariance matrix for observations being made.

Calling Sequence:

CALL ONBTR

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I					Quantities obtained from common
O					Quantities placed in common

Common storages used or required:

T, S, C, IC

Subroutines required:

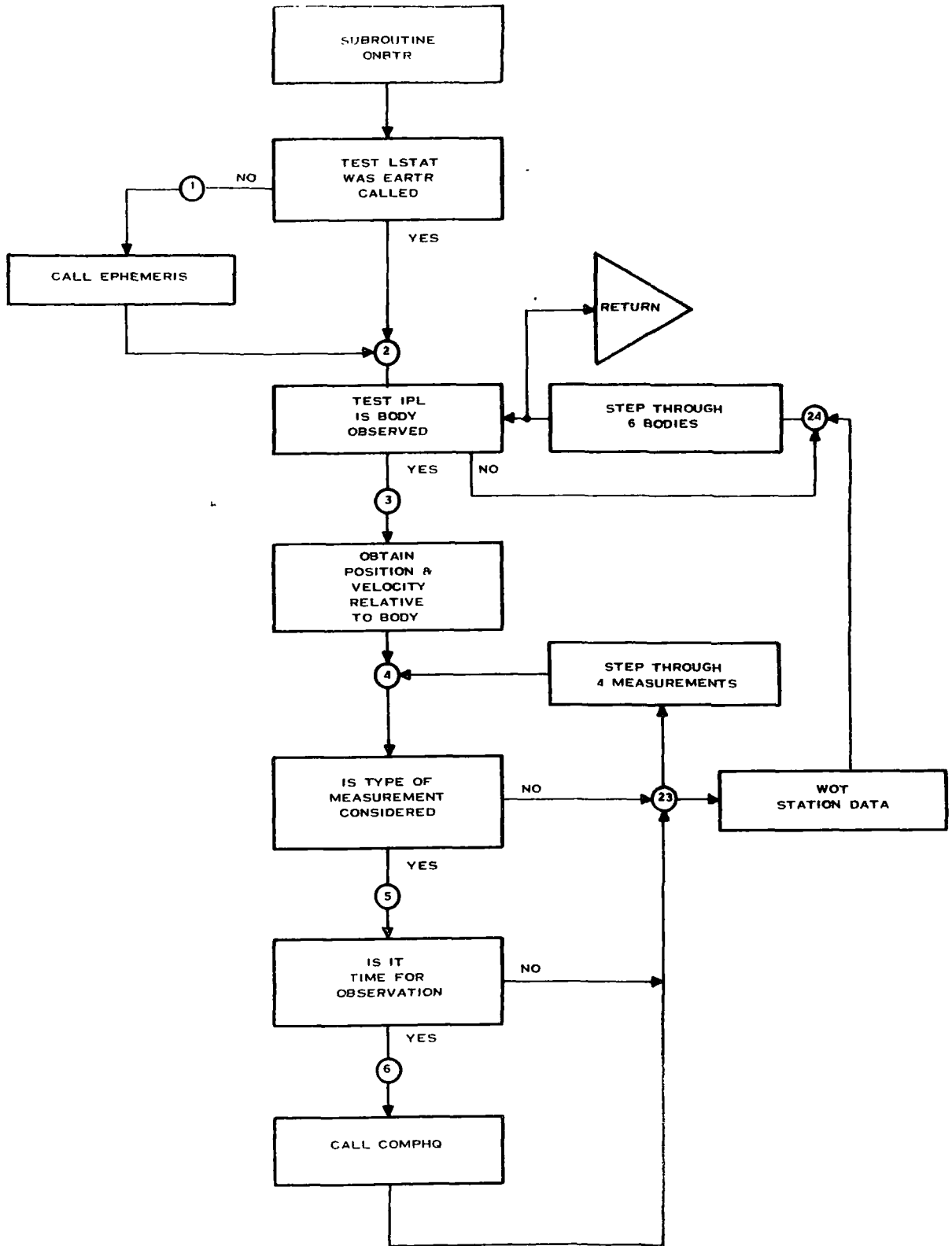
COMPHO, INTRI

Functions required:

ASIN, ATAN, FNORM, SQRT,
(FIL)(SLO)(STH)

Approximate number of storages required:

267 DEC



```

* LABEL ONBT
* SYMBOL TABLE ONBT
CEC2007 ONBT
SUBROUTINE ONBTR ONBT000
SUBROUTINE ONBTR UPDATES CONVARIANCE MATRIX FOR ONBOARD ONBT001
MEASUREMENTS OF RANGE, RIGHT ASCENSION, DECLINATION, AND ONBT002
RANGE RATE RELATIVE TO THE 6 CELESTIAL BODIES ONBT003
COMMON T, S, C, IC ONBT004
DIMENSION PO(22), VE(22), IMPLAN(4,6), IPL(6), X(3), VX(3) ONBT005
1, T(1360), S(1000), C(1000), IC(1), XREL(3), VREL(3) ONBT006
2, TLAST(4,6), OBRATE(4,6), H(6), P(6,6), OUTPUT(6) ONBT007
EQUIVALENCE (T, TDUM), (S, SDUM), (C, CDUM) ONBT008
1, (IC(110), IPL), (IC(116), IMPLAN), (C(15), X), (C(18), VX) ONBT009
2, (IC(3), NOR), (C(13), TW), (C(14), TF), (IC(190), LSTAT) ONBT010
3, (C(649), TSECP), (C(30), TSEC), (S(437), OBRATE), (C(652), P) ONBT011
4, (C(622), TLAST), (C(62), PO), (C(84), VE) ONBT012
1, (C(895), XREL), (C(898), VREL), (C(894), OBNO), (C(893), XMAG), ONBT013
2(C(892), DEX), (C(891), DEN1), (C(890), DEN2), (S(72), DR) ONBT014
3, (C(889), DEX2), (C(888), DEX3), (C(652), P), (C(973), OUTPUT) ONBT015
CALL SETN(NIN, NUTS) ONBT015
LSTAT=LSTAT ONBT016
GO TO (1,2), LSTAT ONBT017
1 CONTINUE ONBT018
NB=NOR-1 ONBT019
DIS=1.E10 ONBT020
CALL INTR1(TW, TF, NB, PO, 1, VE, DIS) ONBT021
2 CONTINUE ONBT022
DO 24 JJ=1,6 ONBT023
JJ DETERMINES BODY TO BE OBSERVED 1, EARTH 2, MOON 3, SUN ONBT024
4, VENUS 5, MARS 6, JUPITER ONBT025
IF(IPL(JJ))24,24,3 ONBT026
3 CONTINUE ONBT027
LM=26-3*(JJ) ONBT028
DO 4 I=1,3 ONBT029
MM=LM-I ONBT030
XREL(I)=PO(MM)-X(I) ONBT031
VREL(I)=VE(MM)-VX(I) ONBT032
4 CONTINUE ONBT033
XREL=VECTOR FROM VEHICLE TO JJ-TH PLANET, EQUINOX 1950 ONBT034
VREL=RELATIVE VELOCITY VECTOR ONBT035
XMAG=FNORM(XREL) ONBT036
DEX=XREL(1)**2+XREL(2)**2 ONBT037
DEN1=1./SQRTF(DEX)/XMAG**2 ONBT038
DEN2=1./DEX ONBT039
DEX2=XMAG*XMAG ONBT040
DEX3=1./XMAG ONBT041
C THE ABOVE QUANTITIES ARE USED IN COMPUTATIONS OF H MATRIX ONBT042
DELTT=TSEC-TSECP ONBT043
DEC=ASINF(DEX3*XREL(3)) ONBT043
OUTPUT(5)=DEC/DR ONBT043
RA=ATANF(XREL(2)/XREL(1)) ONBT043

```

```

OUTPUT(3)=RA/DR
OUTPUT(1)=XMAG
DO 23 JJJ=1,4
IF(IMPLAN(JJJ, JJ))23,23,5
5 CONTINUE
TLAST(JJJ, JJ)=TLAST(JJJ, JJ)+DELTT
C TLAST STORES TIME SINCE LAST JJJ TYPE OF OBSERVATION OF JJ BODY
C JJJ DETERMINES TYPE OF OBS. 1=RANGE, 2=RIGHT ASCENSION,
C 3=DECLINATION, 4=RANGE RATE
NOB=TLAST(JJJ, JJ)/OBRATE(JJJ, JJ)
OBNO=NOB
IF(NOB)23,23,6
6 CONTINUE
JJJ=JJJ
NN=426
CALL COMPHQ(JJJ, 1, NN)
TLAST(JJJ, JJ)=TLAST(JJJ, JJ)+OBNO*OBRATE(JJJ, JJ)
23 CONTINUE
WRITE OUTPUT TAPE NUTS, 700, JJ, OUTPUT
700 FORMAT(16H CELESTIAL BODY , I2,
1/4H RNGE15.8, 5H RGRE15.8,
25H RAE15.8, 5H RARE15.8, 5H DECE15.8, 5H DCRE15.8)
DO 20 I=1,6
20 OUTPUT(I)=0.
24 CONTINUE
RETURN
END

```

ONBT0438
ONBT0439
ONBT0440
ONBT0450
ONBT0460
ONBT0470
ONBT0480
ONBT0490
ONBT0500
ONBT0510
ONBT0520
ONBT0530
ONBT0540
ONBT0550
ONBT0560
ONBT0570
ONBT0580
ONBT0590
ONBT0591
ONBT0592
ONBT0593
ONBT0594
ONBT0595
ONBT0596
ONBT0600
ONBT0610
ONBT

Subroutine: ORTC

Purpose: To convert Cartesian coordinates to conic elements for the output subroutines and to provide other auxiliary results used in computations in the output subroutine.

Calling Sequence:

CALL ORTC (X, DX, U, SMA, ECC, RCA, OINC, OMG, BEP, B, B2, R2, V2, A, C3, BET, THT)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	X	3	\vec{R}	Km	Position vector
I	VX	3	\vec{V}	Km/sec	Velocity vector
I	U	1	μ	Km ³ /sec ²	Central body gravitational constant
O	SMA	1	a	Km	Semi-Major Axis
O	ECC	1	e		Eccentricity
O	RCA	1	V_p	Km	Radius of closest approach
O	OINC	1	i	RAD	Orbital inclination

(Cont'd.)

Common storages used or required: _____

Subroutines required: _____

Functions required: _____

Approximate number of storages required: _____

(Cont'd.)

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
O	OMG	1	Ω	RAD	Argument of ascending node
O	BEP	1	ω	RAD	
O	B	3	$\vec{R} \times \vec{V}$		Quantities used in output subroutine computations
O	B2	1	$ \vec{R} \times \vec{V} ^2$		
O	R2	1	$ \vec{R} ^2$	Km ²	
O	V2	1	$ \vec{V} ^2$	(Km/sec) ²	
O	A	1	$\vec{R} \cdot \vec{V}$		
O	C3	1	$v^2 - \frac{2\mu}{R}$	(Km/sec) ²	
O	BET	1	η	RAD	
O	THT	1	θ	RAD	

The orbital elements determined by the subroutine are the following:

$$C3 = v^2 - \frac{2\mu}{R} \quad \vec{R} \times \vec{v} = \vec{h}$$

Semi-Major Axis

$$a = \text{SMA} = \frac{\mu}{|C3|}$$

Eccentricity

$$e = \text{ECC} = \sqrt{1 + \frac{C3 |\vec{R} \times \vec{v}|^2}{\mu^2}} = \sqrt{1 + \frac{C3 |\vec{h}|^2}{\mu^2}}$$

Radius of Closest Approach

$$v_p = RCA = \frac{|\vec{R} \times \vec{U}|^2}{\mu(1+e)} = \frac{|\vec{h}|^2}{\mu(1+e)}$$

Orbital Inclination

$$i = OINC = \tan^{-1} \frac{\sqrt{h^2(1) + h^2(2)}}{h(3)}$$

Argument of the Ascending node

$$\Omega = OMG = \tan^{-1} \frac{h(1)}{-h(2)}$$

True Anomaly

$$\theta = THT = \tan^{-1} \frac{(\vec{X} \cdot \vec{U}) |\vec{h}|}{|\vec{h}|^2 - \mu R}$$

Argument of Periapsis plus True Anomaly

$$n = BET = \frac{X(3) |\vec{h}|}{X(2) h(1) - X(1) h(2)}$$

Argument of Periapsis

$$\omega = BEP = BET - THT$$

```

* LABEL
* SYMBOL TABLE.
SUBROUTINE ORTC(X,DX,U,SMA,ECC,RCA,OINC,OMG,BEP
1,B,B2,R2,V2,A,C3,BET,THT)
DIMENSION X(3),DX(3),B(3)
CALL CROSS(X,DX,B)
R2 = DOT(X,X)
V2 = DOT(DX,DX)
B2 = DOT(B,B)
A = DOT(X,DX)
BB = SQRTF(B2)
R = SQRTF(R2)
C3 = V2-2.*U/R
SMA = U/ABSF(C3)
ECC = SQRTF(1.+C3*B2/U**2)
OINC = ARKTNS(180,B(3),SQRTF(B(1)**2+B(2)**2))
OMG = ARKTNS(360,-B(2),B(1))
RCA = B2/(U*(1.+ECC))
P = B2/U
THT = ARKTNS(360,U*(P-R),BB*A)
BET = ARKTNS(360,X(2)*B(1)-X(1)*B(2),X(3)*BB)
BEP = BET-THT
IF(BEP) 2,3,3
2 BEP=BEP+6.2831853
3 CONTINUE
RETURN
END
    
```

```

ORTC
ORTC
ORTC0000
ORTC0010
ORTC0020
ORTC0030
ORTC0040
ORTC0050
ORTC0060
ORTC0070
ORTC0080
ORTC0090
ORTC0100
ORTC0110
ORTC0120
ORTC0130
ORTC0140
ORTC0150
ORTC0160
ORTC0170
ORTC0180
ORTC0190
ORTC0200
ORTC0210
ORTC0220
ORTC0230
ORTC
    
```

Subroutine: OUTC

Purpose: OUTC writes out the trajectory elements in a coordinate system and reference system specified by an input quantity (KOUT). OUTC also writes out the orbital parameters found in ORTC, and writes out the selenographic latitude and longitude if the system is moon-centered.

Calling Sequence:

CALL OUTC

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
KOUT	IC(7)				0 for output in date
					1 for output in 1950
					2 for output in ecliptic coord.

Common storages used or required: T, S, C, IC

Subroutines required: see next page

Functions required: see next page

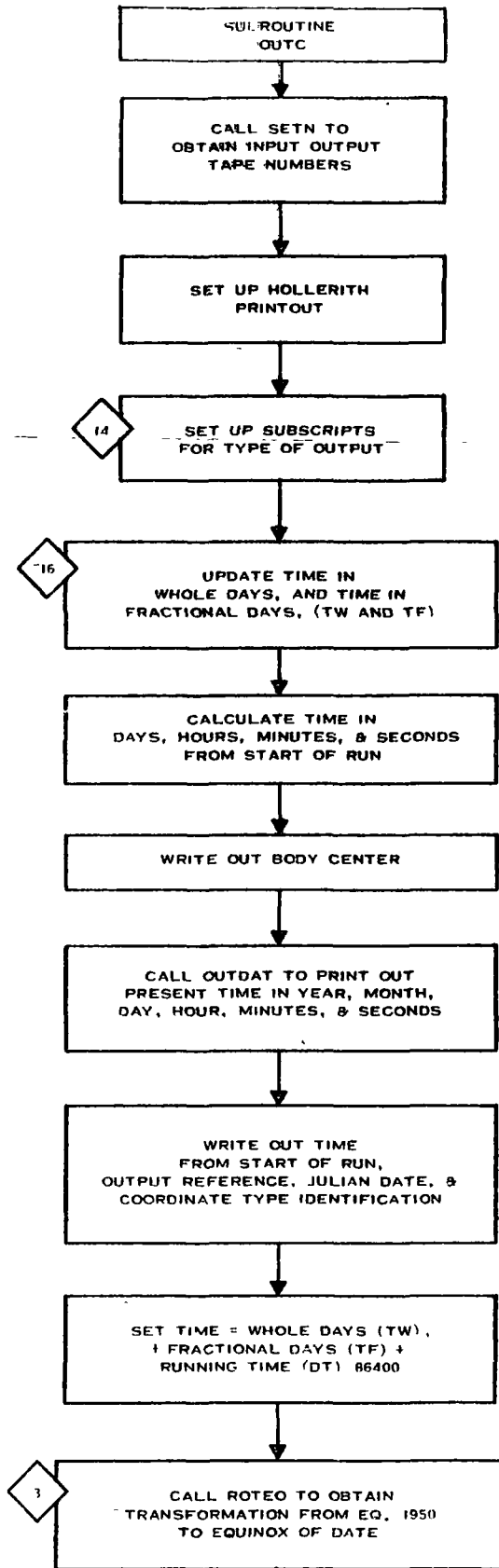
Approximate number of storages required: decimal 940; octal 1654

Subroutines Required

ECLIP
GHA
INTRI
MNAND
NMA
MULT
NUTAIT
ORTC
OUTDAT
ROTATE
ROTEQ
RVOUT
SETN

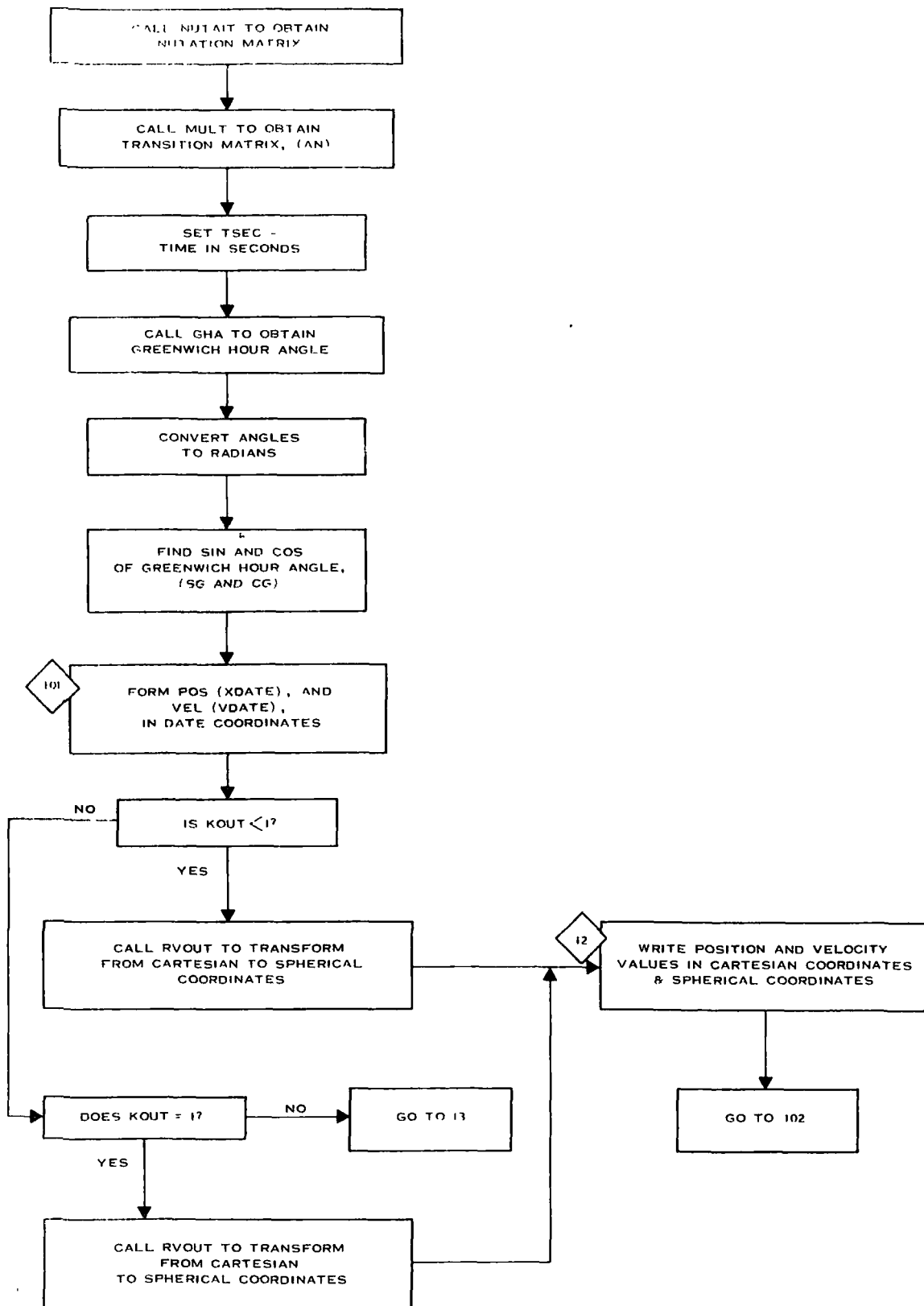
Functions Required

ARKTNS
ATAN
COS
SIN
SORT



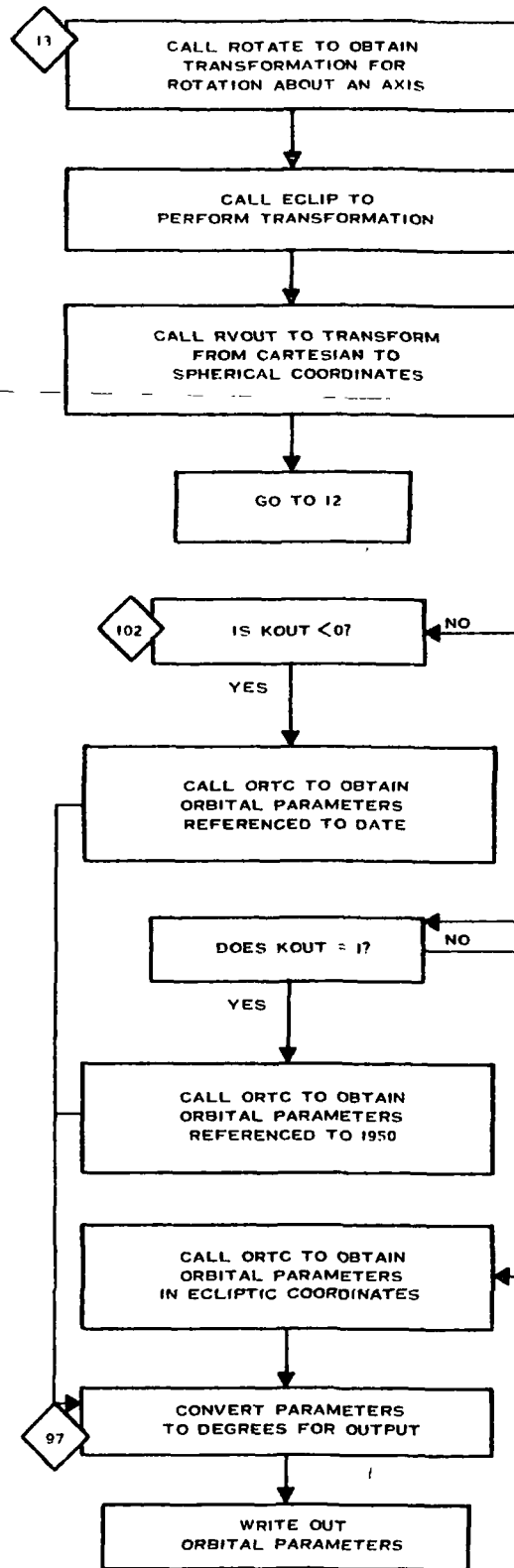
S-313

OUTC - 3



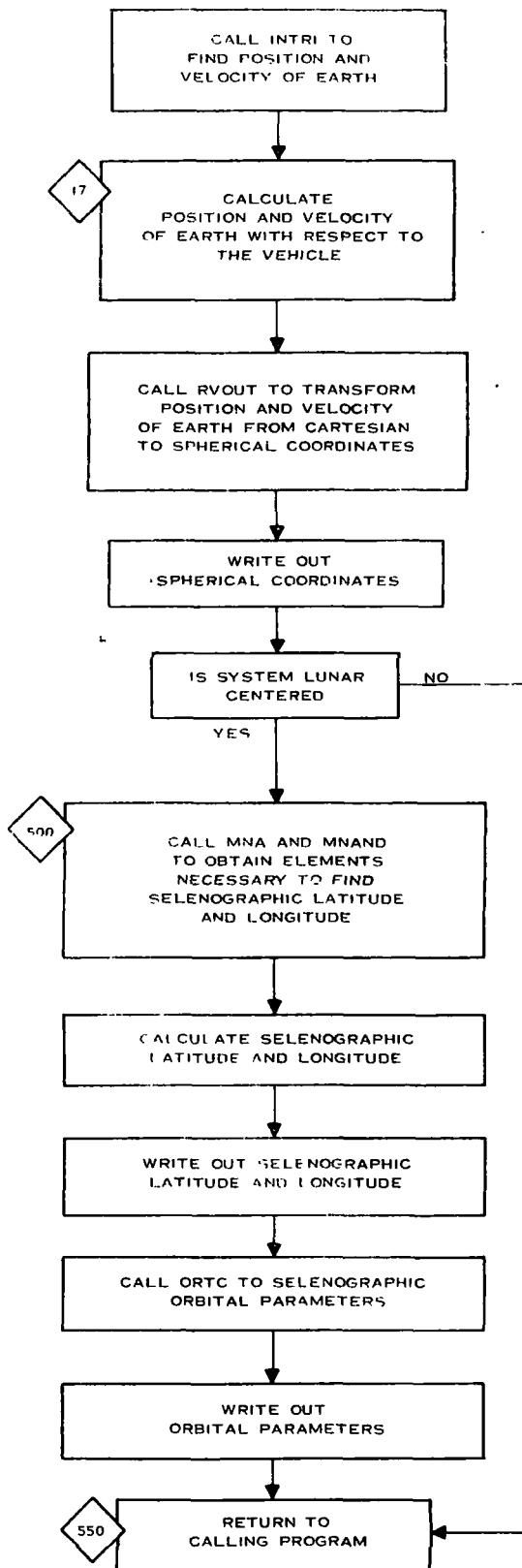
S-314

OUTC - 4



OUTC - 5

S-315



```

* LABEL OUTC
* SYMBOL TABLE OUTC
CEC2015 SUBROUTINE OUTC OUTC
SUBROUTINE OUTC OUTC000
COMMON T,S,C,IC OUTC001
EQUIVALENCE (T,TDUM),(S,SDUM),(C,CDUM),(IC,IGDUM) OUTC002
EQUIVALENCE (T(2),DT),(C(15),XP),(C(18),VXP),(C(129),EA) OUTC003
1,(C(120),EN),(C(138),AN),(C(62),PO),(C(84),VE),(C(10),TW) OUTC004
2,(C(11),TF),(IC(3),NOR),(IC(6),ITARG),(IC(7),KOUT),(C(55),U) OUTC005
3,(S(73),RTD),(C(180),SMA),(C(181),ECC),(C(182),RCA),(C(183),OINC) OUTC006
4,(C(184),OMG),(C(185),BEP),(C(186),XED),(C(189),VED) OUTC007
5,(C(156),ECX),(C(159),ECV),(C(147),ECL),(C(30),T2) OUTC008
6,(C(192),RCV),(C(195),RCV2),(C(196),R2),(C(197),V2),(C(198),RDV) OUTC009
7,(C(199),C3),(C(162),BET),(C(163),THT) OUTC010
-----
DIMENSION T(1360),S(1000),C(1000),IC(1) OUTC011
DIMENSION XP(3),VXP(3),EA(3,3),EN(3,3),B(3,3),AN(3,3), OUTC012
1 BAN(3,3),PO(22),VE(22),XDATE(3),VDATE(3),XEARTH(3),VEARTH(3), OUTC013
2SPDATE(6),ECX(3),ECV(3),CNAME(6),VEV(3) OUTC014
DIMENSION XED(3),VED(3),PEV(3),RCV(3),RCVM(3) OUTC015
DIMENSION ANAME(2) OUTC016
DIMENSION BNAME(4) OUTC017
DIMENSION ECL(3,3) OUTC018
DIMENSION POS(3),VES(3),POM(3),VEM(3),POT(3),VET(3) OUTC019
CALL SETN(NIN,NOUT) OUTC019
ANAME(1) = 6H DATE OUTC020
ANAME(2) = 6H1950.0 OUTC021
BNAME(1) = 6H EC OUTC022
BNAME(2) = 6H LIPTIC OUTC023
BNAME(3) = 6H EQUA OUTC024
BNAME(4) = 6H TORIAL OUTC025
CNAME(1)=6H EARTH OUTC026
CNAME(2)=6H MOON OUTC027
CNAME(3)=6H SUN OUTC028
CNAME(4)=6H VENUS OUTC029
CNAME(5)=6H MARS OUTC030
CNAME(6)=6H JUPITR OUTC031
202 CONTINUE OUTC032
KO=KOUT OUTC033
NOR = NOR OUTC034
IF (KOUT-1) 14,14,15 OUTC035
14 KT = 3 OUTC036
GO TO 16 OUTC037
15 KT = 1 OUTC038
KO=0 OUTC039
16 CONTINUE OUTC040
TP2 = TF+DT/86400. OUTC041
TWGN=0. OUTC042
32 CONTINUE OUTC043
IF(TP2) 33,34,34 OUTC044
33 CONTINUE OUTC045
TP2=TP2+1. OUTC046

```

	TWGN=TWGN-1.	OUTC0470
	GO TO 32	OUTC0480
34	CONTINUE	OUTC0490
	TFP = INTF(TP2)	OUTC0500
	TP2 = TP2-TFP	OUTC0510
	TP1=TW+TFP+TWGN	OUTC0520
	IT1=T2/86400.	OUTC0530
	DT1=IT1	OUTC0540
	DT1=T2-DT1*86400.	OUTC0550
	IT2=DT1/3600.	OUTC0560
	DT2=IT2	OUTC0570
	DT2=DT1-DT2*3600.	OUTC0580
	IT3=DT2/60.	OUTC0590
	DT3=IT3	OUTC0600
	DT3=DT2-DT3*60.	OUTC0610
	TT = INTF(TP2+.5)	OUTC0620
	TP2P = TP2+.5-TT	OUTC0630
	TP1P = TP1 + TT + 2433282.	OUTC0640
	WRITE OUTPUT TAPE NOUT,702,CNAME(NOR)	OUTC0650
702	FORMAT (/1H0A6,10H CENTERED)	OUTC0660
	CALL OUTDAT(TP1,TP2)	OUTC0670
	WRITE OUTPUT TAPE NOUT,2,IT1,IT2,IT3,DT3,ANAME(KO +1),TP1P,TP2P	OUTC0680
	1 ,BNAME(KT),BNAME(KT+1)	OUTC0690
	2 FORMAT(I4,5H DAYSI4,5H HRS.I4,5H MIN.F7.2,5H SEC.4XA6,3X12HJULIAN	OUTC0700
	1 DATE:F8.0,F8.8,10X2A6,12H COORDINATES)	OUTC0710
	N = NOR	OUTC0720
	TIME = TW+TF+DT/86400.	OUTC0730
	DIS = 1.E10	OUTC0740
	NR1 = N-1	OUTC0750
	NV = 1	OUTC0760
3	CALL ROTEQ(TIME,EA)	OUTC0770
	CALL NUTAIT(TIME,WM,CR,DA,EN,EPSIL)	OUTC0780
	CALL MULT(EN,EA,AN,0)	OUTC0790
	TSEC = 86400.*TP2	OUTC0800
	CALL GHA(TSEC,TP1,GHAN,EN(2,1),OMEGA)	OUTC0810
	GHAN = GHAN*.017453296	OUTC0820
	OMEGA = OMEGA*.017453296	OUTC0830
	SG = SINP(GHAN)	OUTC0840
	CG = COSP(GHAN)	OUTC0850
	DO 1 I=1,3	OUTC0860
	XDATE(I) = 0.	OUTC0870
	VDATE(I) = 0.	OUTC0880
	DO 101 J=1,3	OUTC0890
	XDATE(I) = XDATE(I) + AN(I,J)*XP(J)	OUTC0900
	VDATE(I) = VDATE(I) + AN(I,J)*VXP(J)	OUTC0910
101	CONTINUE	OUTC0920
	XED(I)=XDATE(I)	OUTC0930
	VED(I)=VDATE(I)	OUTC0940
1	CONTINUE	OUTC0950
	IF (KOUT-1) 11,10,13	OUTC0960
10	CALL RVOUT(XP,VXP,SPDATE)	OUTC0970

```

WRITE OUTPUT TAPE NOUT,5,XP,VXP,SPDAT
GO TO 102
11 CALL RVOUT(XDATE,VDATE,SPDATE)
12 WRITE OUTPUT TAPE NOUT,5,XDATE,VDATE,SPDATE
GO TO 102
13 CALL ROTATE(1,EPSIL,ECL,1)
CALL ECLIP(XDATE,VDATE,ECL)
CALL RVOUT(XDATE,VDATE,SPDATE)
DO 103 I=1,3
  ECX(I)=XDATE(I)
103 ECV(I)=VDATE(I)
GO TO 12
102 CONTINUE
5 FORMAT(4H __XE15.8,5H __YE15.8,5H __ZE15.8,5H DXE15.8,
1 5H DYE15.8,5H DZE15.8/4H RE15.8,5H DECE15.8,5H RAE15.8,
2 5H VE15.8,5H PTHE15.8,5H AZE15.8)
IF (KOUT-1) 105,106,107
105 CALL ORTC(XED,VED,U,SMA,ECC,RCA,OINC,OMG,BEP
1,RCV,RCV2,R2,V2,RDV,C3,BET,THT)
GO TO 97
106 CALL ORTC(XP,VXP,U,SMA,ECC,RCA,OINC,OMG,BEP
1,RCV,RCV2,R2,V2,RDV,C3,BET,THT)
GO TO 97
107 CALL ORTC(ECX,ECV,U,SMA,ECC,RCA,OINC,OMG,BEP
1,RCV,RCV2,R2,V2,RDV,C3,BET,THT)
97 CONTINUE
ORIN =OINC*RTD
OMEG =OMG*RTD
APF =BEP*RTD
WRITE OUTPUT TAPE NOUT,4,SMA,ECC,ORIN,OMEG,APF,RCA
CALL INTR1(TP1,TP2,NR1,PO,NV,VE,DIS)
DO 17 I=1,3
  I4=23-I
  PEV(I)=PO(I4)-XP(I)
  VEV(I)=VXP(I)-VE(I4)
17 CONTINUE
DO 108 I=1,3
  XDATE(I)=0.
  VDATE(I)=0.
DO 108 J=1,3.
  XDATE(I)=XDATE(I)-AN(I,J)*PEV(J)
108 VDATE(I)=VDATE(I)+AN(I,J)*VEV(J)
22 XEARTH(3) = XDATE(3)
VEARTH(3) = VDATE(3)
XEARTH(1) = XDATE(1)*CG + XDATE(2)*SG
XEARTH(2) = -XDATE(1)*SG + XDATE(2)*CG
VEARTH(1)=VDATE(1)*CG+VDATE(2)*SG
VEARTH(2)=-VDATE(1)*SG+VDATE(2)*CG
CALL RVOUT(XEARTH,VEARTH,SPDATE)
WRITE OUTPUT TAPE NOUT,31,SPDATE
31 FORMAT(4H RTEE15.8,5H LATE15.8,

```

3.5H	LONE15.8,5H	VEE15.8,5H	PTEE15.8,5H	AZEE15.8)	OUTC1490
29	CONTINUE.				OUTC1500
	IF(N-2)550,500,550				OUTC1510
500	CALL MNA(TIME,WM,CR,DA,EPSIL,RR,G,GP,WW,BAN)				OUTC1520
	DO 510 I=1,3				OUTC1540
	XDATE(I)=0.				OUTC1550
	VDATE(I)=0.				OUTC1560
	DO 510 J=1,3				OUTC1570
	XDATE(I)=XDATE(I)+BAN(I,J)*XED(J)				OUTC1580
510	VDATE(I)=VDATE(I)+BAN(I,J)*VED(J)				OUTC1590
	SLAT=XDATE(3)/SQRTF(XDATE(1)**2+XDATE(2)**2)				OUTC1600
	SLAT=ATANF(SLAT)*RTD				OUTC1610
	SLNG=ARKTNS(360,XDATE(1),XDATE(2))*RTD				OUTC1620
	WRITE OUTPUT TAPE NOUT,701,SLNG,SLAT				OUTC1630
701	FORMAT(19H SELENOGRAPHIC LON=,E17.8,5H LAT=,E17.8)				OUTC1640
	CALL ORTC(XDATE,VDATE,U,AMS,EPS,RP,ORIN,OMEG,APF				OUTC1650
	1,RCVM,RCVM2,R2M,V2M,RDVM,C3M,BETM,THTM)				OUTC1660
	OMEG = OMEG*RTD				OUTC1670
	ORIN = ORIN*RTD				OUTC1680
C	GIVES CALENDER DATE FROM T1(WHOLE DAYS FROM 1950)				OUTC1690
C	ANDT2(FRACT OF DAY)				OUTC1700
	APF = APF*RTD				OUTC1710
	WRITE OUTPUT TAPE NOUT,4,AMS,EPS,ORIN,OMEG,APF,RP				OUTC1720
4	FORMAT(4H SMAE15.8,5H ECCE15.8,5H INCE15.8,5H LANE15.8,				OUTC1730
1	5H APFE15.8,5H RCAE15.8)				OUTC1740
550	RETURN				OUTC1750
	END				OUTC

Subroutine: OUTDAT

Purpose: OUTDAT finds and outputs the calendar date and Julian date, given the number of days since 1950.0.

Calling Sequence:

CALL OUTDAT (T1, T2)

Input and Output

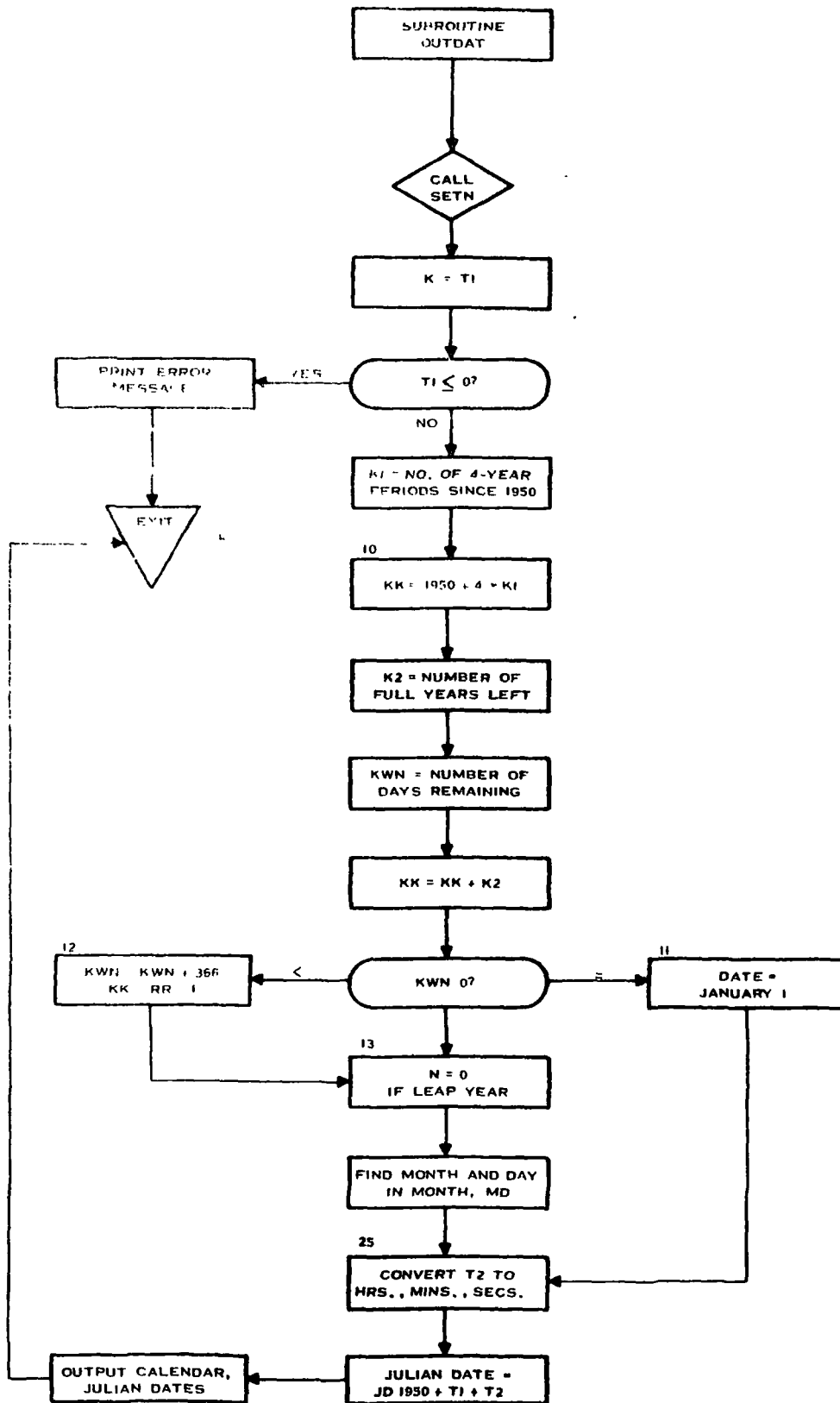
I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	T1	1		days	Integral number of days from 1950.0.
I	T2	1		days	Fraction of day past T1

Common storages used or required: None

Subroutines required: SETN

Functions required: XMODF, INTF

Approximate number of storages required: 351 DEC



S-322

OUTDAT - 2


```

* LABEL
* SYMBOL TABLE
CEC20DT
SUBROUTINE OUTDAT (T1,T2)
C GIVES CALENDER DATE FROM T1(WHOLE DAYS FROM 1950)
C ANDT2(FRACT OF DAY)
CALL SETN(NIN,NOUT)
MD=0
K=T1
IF(T1)6,6,7
6 WRITE OUTPUT TAPE NOUT,100
8 RETURN
100 FORMAT(23H DATE IS 1950 OR BEFORE)
7 K1=K/1461
10 KK=K1*4+1950
K1=XMODF(K,1461)
K2=K1/365
KWN=XMODF(K1,365)-K2/3
KK=KK+K2
IF(KWN)12,11,13
11 MONTH=1
MD=1
GO TO 25
12 KWN=KWN+366
KK=KK-1
13 N=XMODF(KK,4)
KNW=0
JJ=0
135 JJ=JJ+1
IF(12=JJ)23,23,137
C J,F,M,A,M,J,J,A,S,O,N,MONTHS FOR GO TO
137 GO TO (14,15,14,16,14,16,14,14,16,14,16,14),JJ
14 CONTINUE
KNW=KNW+31
GO TO 17
15 CONTINUE
IF(N)18,18,19
18 KNW=KNW+1
19 KNW=KNW+28
GO TO 17
16 KNW=KNW+30
17 CONTINUE
IF(KWN=KNW)20,21,22
22 CONTINUE
MD=KNW
GO TO 135
20 CONTINUE
MONTH=JJ
MD=KWN-MD+1
GO TO 25

```

```

OUTD
OUTD
OUTD
OUTD000
OUTD001
OUTD002
OUTD003
OUTD004
OUTD005
OUTD006
OUTD007
OUTD008
OUTD009
OUTD010
OUTD011
OUTD012
OUTD013
OUTD014
OUTD015
OUTD016
OUTD017
OUTD018
OUTD019
OUTD020
OUTD021
OUTD022
OUTD023
OUTD024
OUTD025
OUTD026
OUTD027
OUTD028
OUTD029
OUTD030
OUTD031
OUTD032
OUTD033
OUTD034
OUTD035
OUTD036
OUTD037
OUTD038
OUTD039
OUTD040
OUTD041
OUTD042
OUTD043
OUTD044
OUTD045
OUTD046
OUTD047
OUTD048

```

OUTDAT (cont'd)

WDL-TR2184

```
21 CONTINUE
  MONTH=JJ+1
  MD=1
  GO TO 25
23 MONTH =12
  MD=KWN-MD+1
25 CONTINUE
  TH=T2*24.
  THP=INTF(TH)
  NHOUR=THP
  THP=(TH-THP)*60.
  TH=INTF(THP)
  NMIN=TH
  THP=(THP-TH)*60.
  NSEC=THP
  TSEC=NSEC
  THP=(THP-TSEC)*1000.
  NFSEC=THP
  TT=INTF(T2+.5)
  TP2=T2+.5-TT
  TP1=T1+TT+2433282.
  WRITE OUTPUT TAPE NOUT,101, KK, MONTH, MD, NHOUR, NMIN, NSEC, NFSEC
  1, TP1, TP2
101 FORMAT(6H YEAR=, I4, 8H MONTH=, I2, 6H DAY=, I2, 7H HOUR=, I2,
  1.6H MIN=, I2, 6H SEC=, I2, 1H., I3, 10X, 12H JULIAN DATE=,
  2F8.0, F8.8)
  GO TO 8
  END
```

OUTD0480
OUTD0490
OUTD0500
OUTD0510
OUTD0520
OUTD0530
OUTD0540
OUTD0550
OUTD0560
OUTD0570
OUTD0580
OUTD0590
OUTD0600
OUTD0610
OUTD0620
OUTD0630
OUTD0640
OUTD0650
OUTD0660
OUTD0670
OUTD0680
OUTD0690
OUTD0700
OUTD0710
OUTD0720
OUTD0730
OUTD0740
OUTD

Subroutine: OUTP

Purpose: Obtain the error data in the desired coordinate system for output purposes. The three coordinate systems available are: (1) Equator of Date, (2) Equator of 1950, and (3) Ecliptic. The coordinate system is determined by an input quantity KOUT.

Calling Sequence:

CALL OUTP

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I					Quantities obtained from common
O					Quantities printed out

Common storages used or required:

T, S, C, IC

Subroutines required:

CROSS, HPHT, INV3, MATRX, PTRAN

Functions required:

COS, FNORM, SIN, SQRT

Approximate number of storages required:

1179 DEC

A. Derivation of Partials Used in Subroutine

In order to determine the RMS error in knowledge of orbital elements, the partials which relate the elements and the vehicle state are required. The derivation of these partials follows. The angular elements are shown below in Fig. 1.

i = ORBITAL INCLINATION
 Ω = ARGUMENT OF THE ASCENDING NODE
 ω = ARGUMENT OF PERIGEE
 θ = TRUE ANOMALY
 h = ANGULAR MOMENTUM VECTOR
 $n = \theta + \omega$

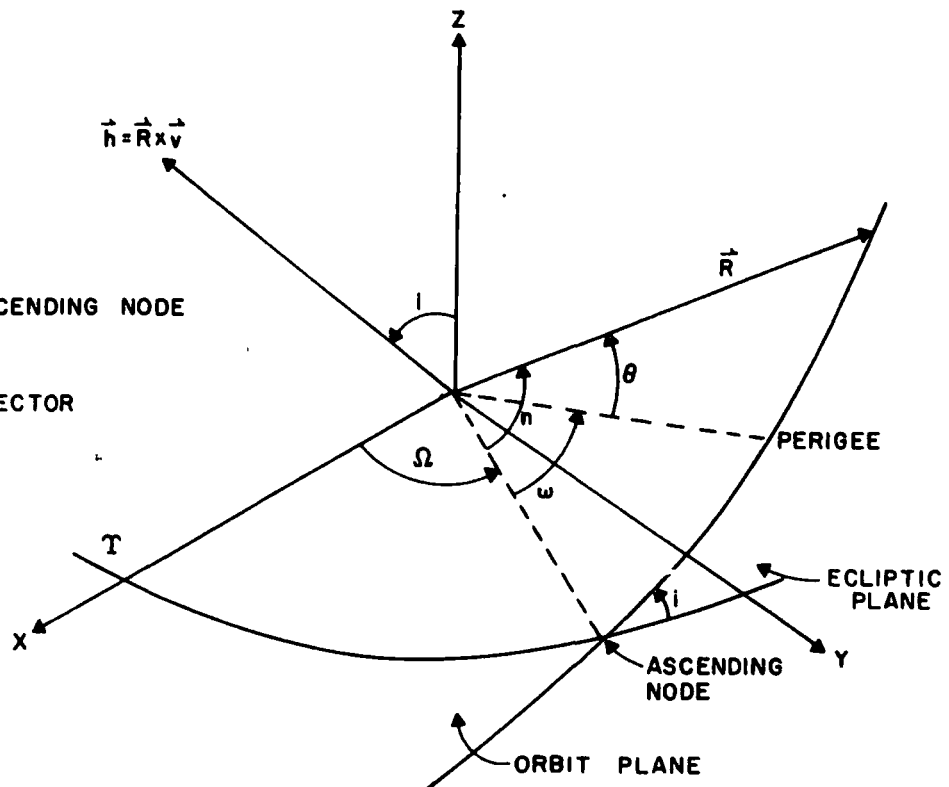


FIG. 1

1. Derivation of partial for eccentricity

$$e = \sqrt{1 + \frac{h^2 C3}{\mu^2}}$$

$$\nabla e = \frac{1}{\mu^2 e} \left\{ C3 [v^2 \vec{r} - (\vec{r} \cdot \vec{v}) \vec{v}] + h^2 \mu \frac{\vec{r}}{r^3} \right\}$$

$$\text{where } \nabla = \left(\frac{\partial}{\partial x} ; \frac{\partial}{\partial y} ; \frac{\partial}{\partial z} \right)$$

$$C3 = v^2 - \frac{2\mu}{r}$$

$$h^2 = |\vec{r} \times \vec{v}|^2$$

$$D\epsilon = \frac{1}{\mu^2 \epsilon} \left\{ h^2 \vec{v} + c3 [r^2 \vec{v} - (\vec{r} \cdot \vec{v}) \vec{r}] \right\}$$

$$\text{where } D = \left(\frac{\partial}{\partial \dot{x}} ; \frac{\partial}{\partial \dot{y}} ; \frac{\partial}{\partial \dot{z}} \right)$$

2. Derivation of partials for radius of closest approach

$$r_p = \frac{h^2}{\mu(1+\epsilon)}$$

$$\nabla r_p = \frac{1}{\mu \epsilon} \left\{ v^2 \vec{r} - (\vec{r} \cdot \vec{v}) \vec{v} - \mu r_p^2 \frac{\vec{r}}{r^3} \right\}$$

$$Dr_p = \frac{1}{\mu \epsilon} \left\{ (r^2 - r_p^2) \vec{v} - (\vec{r} \cdot \vec{v}) \vec{r} \right\}$$

3. Derivation of partials for semi-major axis

$$a = - \frac{\mu}{|c3|}$$

$$\frac{\partial a}{\partial X_k} = 2a^2 \frac{X_k}{r^3}$$

for k = 1, 2, 3

$$X_1 = X \quad X_2 = Y \quad X_3 = Z$$

$$\frac{\partial a}{\partial \dot{X}_k} = 2a^2 \frac{\dot{X}_k}{\mu}$$

$$\dot{X}_1 = \dot{X} \quad \dot{X}_2 = \dot{Y} \quad \dot{X}_3 = \dot{Z}$$

4. Derivation of partials for longitude of the ascending node

$$\Omega = \text{Tan}^{-1} \frac{h(1)}{-h(2)}$$

$$\frac{\partial \Omega}{\partial x} = - \sin \Omega \frac{\dot{z}}{h \sin i}$$

$$\frac{\partial \Omega}{\partial \dot{x}} = \sin \Omega \frac{z}{h \sin i}$$

$$\frac{\partial \Omega}{\partial y} = \cos \Omega \frac{z}{h \sin i}$$

$$\frac{\partial \Omega}{\partial \dot{y}} = - \cos \Omega \frac{z}{h \sin i}$$

$$\frac{\partial \Omega}{\partial z} = -\cos i \frac{\dot{z}}{h \sin i} \quad \frac{\partial \Omega}{\partial \dot{z}} = \cos i \frac{z}{h \sin i}$$

5. Derivation of partials for inclination

$$i = \tan^{-1} \frac{\sqrt{h(1)^2 + h(2)^2}}{h(3)}$$

$$\frac{\partial i}{\partial X_k} = \frac{\sin i \cos n}{\sin n} \frac{\partial \Omega}{\partial X_k} \quad \text{for } k = 1, 2, \dots, 6$$

$$X_1 = X \quad X_2 = Y \quad X_3 = Z$$

$$X_4 = \dot{X} \quad X_5 = \dot{Y} \quad X_6 = \dot{Z}$$

6. Derivation of partials for argument of periapsis

$$\omega = n - \theta = \tan^{-1} \frac{zh}{yh(1) - xh(2)} - \tan^{-1} \frac{(\hat{r} \cdot \hat{v}) h}{h^2 - \mu r}$$

$$\frac{\partial \omega}{\partial X_k} = -\frac{1}{e^2} (\alpha \cos n + \beta \sin n) \frac{\partial n}{\partial X_k} + \frac{1}{he^2} \left\{ (\alpha \sin n - \beta \cos n) \right\}$$

$$\left\{ \frac{\partial h}{\partial X_k} - (\alpha + \cos n) \frac{\cos i}{\sin n} h \frac{\partial \Omega}{\partial X_k} \right\}$$

for $k = 1, 2, 3$

$$\frac{\partial \omega}{\partial \dot{X}} = -\frac{1}{e^2} (\alpha \cos n + \beta \sin n) \frac{\partial n}{\partial \dot{X}} + \frac{1}{he^2} (\alpha \sin n - \beta \cos n) \left\{ \frac{\partial h}{\partial \dot{X}} \right.$$

$$\left. - (\alpha + \cos n) \frac{\cos i}{\sin n} h \frac{\partial \Omega}{\partial \dot{X}} \right\} - \frac{h}{e^2 \mu} \alpha \cos \Omega$$

$$\frac{\partial n}{\partial y} = -\frac{1}{\epsilon^2} (\alpha \cos n + \beta \sin n) \frac{\partial n}{\partial y} + \frac{1}{h\epsilon^2} (\alpha \sin n - \beta \cos n) \left\{ \frac{\partial h}{\partial y} \right. \\ \left. - (\alpha + \cos n) \frac{\cos i}{\sin n} h \frac{\partial \Omega}{\partial y} \right\} - \frac{1}{\mu\epsilon^2} \alpha \sin \Omega$$

$$\frac{\partial n}{\partial z} = -\frac{1}{\epsilon^2} (\alpha \cos n + \beta \sin n) \frac{\partial n}{\partial z} + \frac{1}{h\epsilon^2} (\alpha \sin n - \beta \cos n) \left\{ \frac{\partial h}{\partial z} \right. \\ \left. - (\alpha + \cos n) \frac{\cos i}{\sin n} h \frac{\partial \Omega}{\partial z} \right\} - \frac{h}{\mu\epsilon^2} \frac{\beta}{\sin i}$$

where

$$\alpha = \epsilon \cos \omega$$

$$\beta = \epsilon \sin \omega$$

$$\frac{\partial h}{\partial x_k} = \frac{h \sin^2 i \cos n}{\cos i \sin n} \frac{\partial \Omega}{\partial x_k} \quad k = 1, 2, \dots, 6$$

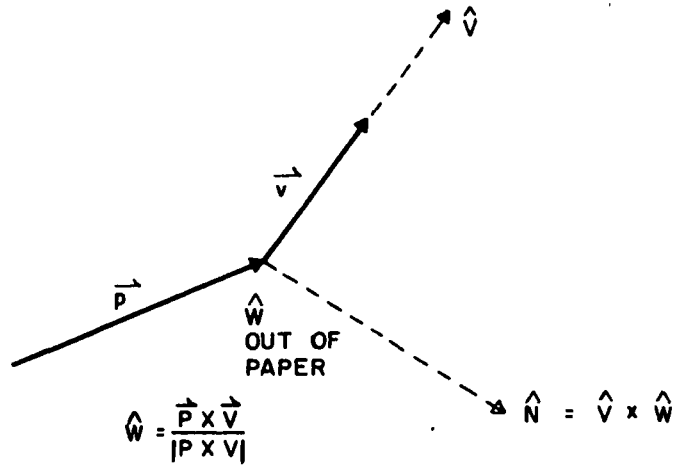
$$\frac{\partial n}{\partial x} = -\cos i \frac{\partial \Omega}{\partial x} - \frac{1}{r} \sin n \cos \Omega \quad \frac{\partial n}{\partial x} = -\cos i \frac{\partial \Omega}{\partial x}$$

$$\frac{\partial n}{\partial y} = -\cos i \frac{\partial \Omega}{\partial y} - \frac{1}{r} \sin n \sin \Omega \quad \frac{\partial n}{\partial y} = -\cos i \frac{\partial \Omega}{\partial y}$$

$$\frac{\partial n}{\partial z} = -\cos i \frac{\partial \Omega}{\partial z} + \frac{1}{r} \frac{\cos n}{\sin i} \quad \frac{\partial n}{\partial z} = -\cos i \frac{\partial \Omega}{\partial z}$$

B. Derivation of Transformation from Cartesian x, y, z to Cartesian N, V, W coordinates

The coordinates N, V, and W represent unit vectors shown in Fig. 2 following.



(PAPER IS ORBIT PLANE)

\vec{p} AND \vec{v} ARE POSITION AND VELOCITY VECTORS

FIG. 2

\hat{W} is in the direction of the angular momentum vector, \hat{V} is along the velocity vector, and \hat{N} forms an orthogonal coordinate system in the sense of $\hat{N} = \hat{V} \times \hat{W}$. The three unit vectors may be written as follows:

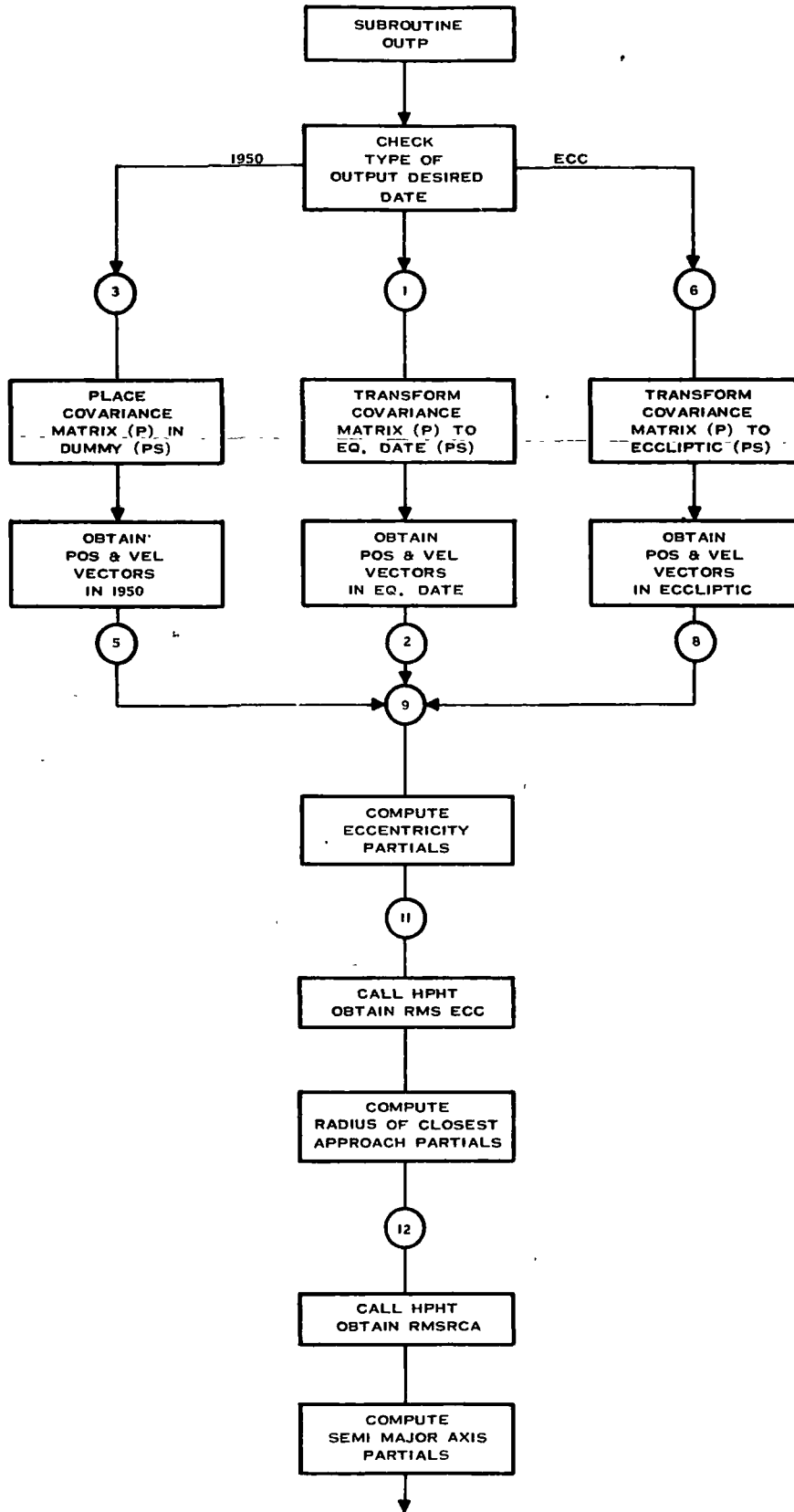
$$\hat{W} = \frac{\vec{R} \times \vec{v}}{|\vec{R} \times \vec{v}|}$$

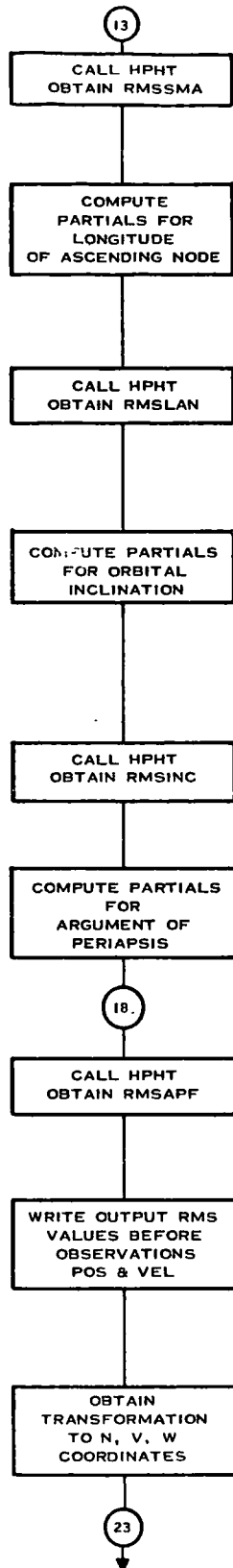
$$\hat{V} = \frac{\vec{v}}{|\vec{v}|}$$

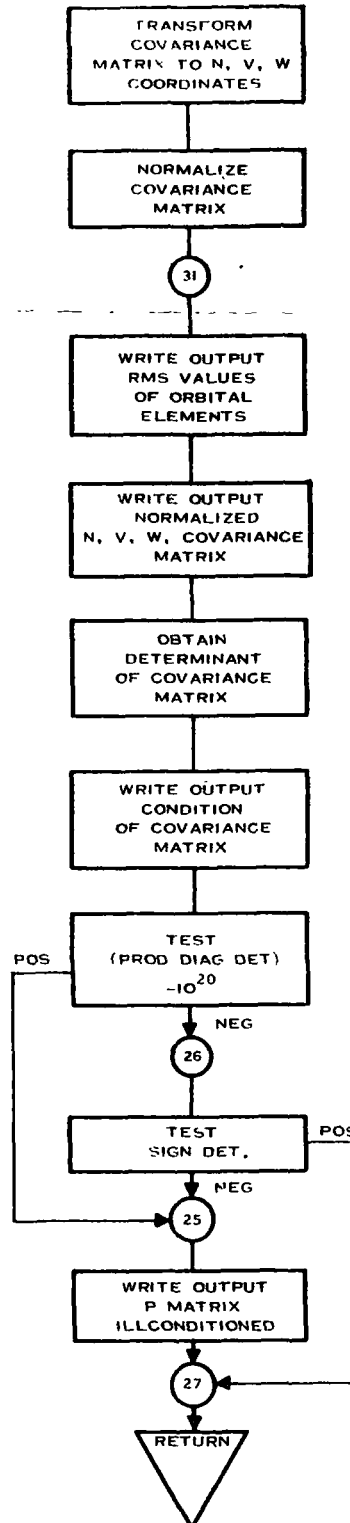
$$\hat{N} = \frac{\vec{v}}{|\vec{v}|} \times \frac{\vec{R} \times \vec{v}}{|\vec{R} \times \vec{v}|}$$

Writing the transposed vectors in matrix form yields the desired transformation from $\hat{i}, \hat{j}, \hat{k}$ to $\hat{N}, \hat{V}, \hat{W}$

$$\begin{pmatrix} N \\ V \\ W \end{pmatrix}_{3 \times 1} = \begin{pmatrix} \hat{N}^T \\ \hat{V}^T \\ \hat{W}^T \end{pmatrix}_{3 \times 3} \begin{pmatrix} x \\ y \\ z \end{pmatrix}_{3 \times 1}$$







S-333

OUPT - 9

```

* LABEL
CEC2016 SUBROUTINE OUTP
SUBROUTINE OUTP
COMMON T,S,C,IC
DIMENSION T(1360),S(1000),C(1000),IC(1),P(6,6),AN(3,3),ECL(3,3)
1,ECX(3),ECV(3),XED(3),VED(3),XP(3),VXP(3),PS(6,6),X(3),VX(3)
2,DUM(3,3), H (6),DUMC(3,3),DELH2(3),DELC3(3),DELECC(3),DELVH2(3)
3,DELVEC(3),DELRP(3),DELRP(3),DELSMA(3),DELYSA(3),Q(6)
DIMENSION Q1(6),RCV(3),DAG(6)
EQUIVALENCE (T,TDUM),(S,SDUM),(C,CDUM),(IC,ICDUM)
1,(C(652),P ),(C(138),AN),(C(147),ECL),(C(156),ECX),(C(159),ECV)
2,(C(180),SMA),(C(181),ECC),(C(182),RCA),(C(183),OINC),(C(184),OMG)
3,(C(185),APF),(C(186),XED),(C(189),VED),(C(192),RCV),(C(195),RCV2)
4,(C(196),R2),(C(197),V2) ,(C(198),RDV),(C(199),C3),(C(15),XP)
5,(C(18),VXP),(IC(7),KOUT),(C(55) ,U),(C(162),BET),(C(163),THT)
6,(S(73),RTD)
CALL SETN(NIN,NUTS)
C KOUT=TYPE OUTPUT DESIRED 0=EQ OF DATE 1= EQ OF 1950 2=ECCLIPTIC
IF(KOUT=1) 1,3,6
1 CONTINUE
CALL PTRAN(P,AN,PS,2)
DO 2 I=1,3
X(I)=XED(I)
2 VX(I)=VED(I)
GO TO 9
3 CONTINUE
DO 4 I=1,6
DO 4 J=1,6
4 PS(I,J)=P(I,J)
DO 5 I=1,3
X(I)=XP(I)
5 VX(I)=VXP(I)
GO TO 9
6 CONTINUE
DO 7 I=1,3
DO 7 J=1,3
DUM(I,J)=0.
DO 7 K=1,3
7 DUM(I,J)=DUM(I,J) + ECL(I,K)*AN(K,J)
CALL PTRAN( P,DUM,PS,2)
DO 8 I=1,3
X(I)=ECX(I)
8 VX(I)=ECV(I)
9 CONTINUE
R=SQRTF(R2)
CALL CROSS(VX,RCV,DELH2)
CALL CROSS(RCV,X,DELVH2)
DO 10 I=1,3
10 DELC3(I)=(U/R2/R)*X(I)
C FOLLOWING IS COMPUTATION OF ECCENTRICITY PARTIALS
CONST= 1./(ECC*U**2)

```

```

OUTP
OUTP
OUTP0000
OUTP0010
OUTP0020
OUTP0030
OUTP0040
OUTP0050
OUTP0060
OUTP0070
OUTP0080
OUTP0090
OUTP0100
OUTP0110
OUTP0120
OUTP0130
OUTP0138
OUTP0140
OUTP0150
OUTP0160
OUTP0170
OUTP0180
OUTP0190
OUTP0200
OUTP0210
OUTP0220
OUTP0230
OUTP0240
OUTP0250
OUTP0260
OUTP0270
OUTP0280
OUTP0290
OUTP0300
OUTP0310
OUTP0320
OUTP0330
OUTP0340
OUTP0350
OUTP0360
OUTP0370
OUTP0380
OUTP0390
OUTP0400
OUTP0410
OUTP0420
OUTP0430
OUTP0440
OUTP0450
OUTP0460
OUTP0470

```

```

DO 11 I=1,3
II=I+3
DELECC(I)=CONST*(C3*DELH2(I)+RCV2*DELVC3(I))
DELVEC(I)=CONST*(C3*DELVH2(I)+RCV2*VX(I))
H(I)=DELECC(I)
H(II)=DELVEC(I)
11 CONTINUE
CALL HPHT(H,PS,RMSECC)
FOLLOWING FOR PARTIALS OF RADIUS CLOSEST APPROACH =RCA
CON=1.+ECC
CONST=U*CON
CONS =RCV2/(CONST*CON)
CON=2./CONST
DO 12 I=1,3
II= I+3
DELRP(I)=CON*DELH2(I)-CONS*DELECC(I)
DELVRP(I)=CON*DELVH2(I)-CONS*DELVEC(I)
H(I)=DELRP(I)
H(II)=DELVRP(I)
12 CONTINUE
CALL HPHT(H,PS,RMSRCA)
FOLLOWING FOR PARTIALS OF SEMI MAJOR AXIS =SMA
CONST= 1./( ECC-1.)
CON= RCA*CONST**2
DO 13 I=1,3
II=I+3
DELSMA(I)=CONST*DELRP(I)-CON*DELECC(I)
DELVSA(I)=CONST*DELVRP(I)-CON*DELVEC(I)
H(I)=DELSMA(I)
H(II)=DELVSA(I)
13 CONTINUE
CALL HPHT(H,PS,RMSSMA)
CI=COSF(OINC)
SI=SINF(OINC)
CW=COSF(OMG)
SW=SINF(OMG)
FOLLOWING FOR LINE OF MODES =LAN PARTIALS
CON =SQRTF(RCV2)
CONST=1./(CON*SI)
CONS =VX(3)*CONST
G(1) =-SW*CONS
G(2) =CW *CONS
G(3) =-CI*CONS/SI
CONS =X(3)*CONST
G(4) =SW*CONS
G(5) =-CW*CONS
G(6) = CI*CONS/SI
CALL HPHT(O,PS,RMSLAN)
THE FOLLOWING FOR INCLINATION
CONS=1./CON
H(1)=CONS*(VX(2)*SI + VX(3)*CW*CI)
    
```

OUTP048
 OUTP049
 OUTP050
 OUTP051
 OUTP052
 OUTP053
 OUTP054
 OUTP055
 OUTP056
 OUTP057
 OUTP058
 OUTP059
 OUTP060
 OUTP061
 OUTP062
 OUTP063
 OUTP064
 OUTP065
 OUTP066
 OUTP067
 OUTP068
 OUTP069
 OUTP070
 OUTP071
 OUTP072
 OUTP073
 OUTP074
 OUTP075
 OUTP076
 OUTP077
 OUTP078
 OUTP084
 OUTP085
 OUTP086
 OUTP087
 OUTP088
 OUTP089
 OUTP090
 OUTP091
 OUTP092
 OUTP093
 OUTP094
 OUTP095
 OUTP096
 OUTP097
 OUTP098
 OUTP099
 OUTP100
 OUTP101
 OUTP102
 OUTP103

H(2)=CONS*(VX(1)*SI + VX(3)*SW*CI)	OUTPUT1040
H(3)=-CONS*CI*(VX(1)*CW+VX(2)*SW)	OUTPUT1050
H(4)=CONS*(X(2)*SI-X(3)*CW*CI)	OUTPUT1060
H(5)=-CONS*(X(1)*SI+X(3)*SW*CI)	OUTPUT1070
H(6)= CONS*CI*(X(1)*CW + X(2)*SW)	OUTPUT1080
CALL HPHT(H,PS,RMSINC)	OUTPUT1090
C THE FOLLOWING ARE PARTIALS OF ARG. OF PERIAPSIS = APF	OUTPUT1100
SN =SINF(BET)	OUTPUT1110
CN = COSF(BET)	OUTPUT1120
DO 17 I=1,6	OUTPUT1130
Q1(I) = -CI*Q(I)	OUTPUT1140
17 CONTINUE	OUTPUT1150
Q1(1) = Q1(1)-SN*CW/R	OUTPUT1160
Q1(2) = Q1(2)-SN*SW/R	OUTPUT1170
Q1(3) = Q1(3)+CN/(R*SI)	OUTPUT1180
CP = COSF(APF)	OUTPUT1190
SP = SINF(APF)	OUTPUT1200
RAGHI = 1./SQRTF(RCV2)	OUTPUT1210
CON = ECC*CP	OUTPUT1220
CONST = ECC*SP	OUTPUT1230
CONS = -(CON*CN+CONST*SN)/(ECC**2)	OUTPUT1240
CONS1 = (CON*SN-CONST*CN)*RAGHI/(ECC**2)	OUTPUT1250
CONS2 = CON+CN	OUTPUT1260
CONS2 = CONS2*RAGHI*CI/SN	OUTPUT1270
DO 18 I=1,3	OUTPUT1280
II = I+3	OUTPUT1290
H(I) = CONS*Q1(I)+CONS1*(RAGHI*DELH2(I)-CONS2*Q(I))	OUTPUT1300
H(II) = CONS*Q1(II)+CONS1*(RAGHI*DELH2(II)-CONS2*Q(II))	OUTPUT1310
18 CONTINUE	OUTPUT1320
CONS = -1./((RAGHI*U)*(ECC**2))	OUTPUT1330
H(4) = H(4)+CONS*CW*CON	OUTPUT1340
H(5) = H(5)+CONS*SW*CON	OUTPUT1350
H(6) = H(6)+CONS*CONST/SI	OUTPUT1360
CALL HPHT(H,PS,RMSAPF)	OUTPUT1370
WRITE OUTPUT TAPE NUTS,700	OUTPUT1380
700 FORMAT(44X,31H RMS VALUES BEFORE OBSERVATIONS)	OUTPUT1390
DO 21 I=1,6	OUTPUT1400
21 H(I) =SQRTF(PS(I,I))	OUTPUT1410
WRITE OUTPUT TAPE NUTS,701,H	OUTPUT1420
701 FORMAT(4H XE15.8,5H YE15.8,5H ZE15.8,5H DXE15.8,	OUTPUT1430
15H DYE15.8,5H DZE15.8)	OUTPUT1440
R50=FNORM(VXP)	OUTPUT1580
CALL CROSS(XP,VXP,DUM(1,3))	OUTPUT1590
R51=FNORM(DUM(1,3))	OUTPUT1600
DO 22 I=1,3	OUTPUT1610
DUM(I,2)=VXP(I)/R50	OUTPUT1620
22 DUM(I,3)= DUM(I,3)/R51	OUTPUT1630
CALL CROSS(DUM(1,2),DUM(1,3),DUM(1,1))	OUTPUT1640
DO 23 I=1,3	OUTPUT1650
DO 23 J=1,3	OUTPUT1660
23 DUMC(I,J)=DUM(J,I)	OUTPUT1670

```

CALL PTRAN(P,DUMC,PS,2)
DO 30 I=1,6
DAG(I)=SQRTF(PS(I,I))
30 CONTINUE
DO 31 I=1,6
DO 32 J=I,6
PS(I,J)=PS(I,J)/DAG(I)/DAG(J)
32 CONTINUE
PS(I,I)=1.
31 CONTINUE
RMSINC = RMSINC*RTD
RMSAPF = RMSAPF*RTD
RMSLAN = RMSLAN*RTD
WRITE OUTPUT TAPE NUTS,702,RMSSMA, RMSECC,RMSINC,RMSLAN,RMSAPF,
1RMSRCA
702 FORMAT(4H SMAE15.8,5H ECCE15.8,5H INCE15.8,5H LANE15.8,
15H APFE15.8,5H RCAE15.8)
WRITE OUTPUT TAPE NUTS,703,DAG
703 FORMAT(50X,22H RMS N,V,W COORDINATES,/21X,17H RMS POSITION, KM,
142X,20H RMS VELOCITY KM/SEC,/7X,7H NORMAL, 12X,9H VELOCITY,11X,
29H MOMENTUM,12X,7H NORVEL,14X,7H VELVEL,11X,9H MOMENVEL,/4H
3.8,(5E20.8))
WRITE OUTPUT TAPE NUTS,704,((PS(I,J),J=1,6),I=1,6)
704 FORMAT(30X,58H NORMALIZED STATE COVARIANCE MATRIX IN N,V,W COORD
1INATES,/4H E15.8,(5E20.8)/19X,(5E20.8)/39X,(4E20.8)/59X,
2(3E20.8)/79X,(2E20.8)/99X,E20.8)
CON = 1.
CALL INV3(PS,6,DETER)
CONST = CON/DETER
WRITE OUTPUT TAPE NUTS,705,DETER,CON,CONST
705 FORMAT(37H CONDITION OF STATE COVARIANCE MATRIX,/
124H DETERMINANT OF MATRIX =,E15.8,3X,
222H PRODUCT OF DIAGONAL =,E15.8,1X,
324H RATIO PROD,DIAG,/DET. =,E15.8)
IF (ABSF(CONST)-1.E20) 26,25,25
26 IF (DETER) 25,25,27
WRITE OUTPUT TAPE NUTS,706
706 FORMAT(33H ***P MATRIX IS ILLCONDITIONED***)
27 CONTINUE
RETURN
END

```

OUTP168
 OUTP169
 OUTP170
 OUTP171
 OUTP172
 OUTP173
 OUTP174
 OUTP175
 OUTP176
 OUTP177
 OUTP178
 OUTP179
 OUTP180
 OUTP181
 OUTP182
 OUTP183
 OUTP184
 OUTP185
 OUTP186
 OUTP187
 OUTP188
 OUTP189
 OUTP190
 OUTP191
 OUTP192
 OUTP193
 OUTP194
 OUTP195
 OUTP196
 OUTP197
 OUTP198
 OUTP199
 OUTP200
 OUTP201
 OUTP202
 OUTP203
 OUTP

Page Intentionally Left Blank

Subroutine: PTRAN

Purpose: To compute the transformation of the state covariance matrix from one inertial coordinate system to another. The transformation which is obtained with KK = 2 is the following:

$$PS = \begin{pmatrix} B & 0 \\ 0 & B \end{pmatrix} \begin{pmatrix} P \end{pmatrix} \begin{pmatrix} B^T & 0 \\ 0 & B^T \end{pmatrix}$$

6x6 6x6 6x6 6x6

If KK is set 1 only, the diagonal 3x3's are computed.

Calling Sequence:

CALL PTRAN (P, B, PS, KK)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	P	(6,6)			Covariance Matrix
I	B	(3,3)			Transformation Matrix
O	PS	(6,6)			Transformed Matrix
I	KK	1			Logic Key

Common storages used or required: None

Subroutines required: None

Functions required: None

Approximate number of storages required: _____

PTRAN

WDL-TR

```

* LABEL
* SYMBOL TABLE
SUBROUTINE PTRAN( P,B,PS,KK)
DIMENSION P(6,6),B(3,3),PS(6,6),DUM(6,6)
C SUBROUTINE CALCULATES THE 6X6 MATRIX PS FROM
C P IS SYMMETRIC PS=( B 0 )( P )( BT 0 ) T=TRANPOSE
C ( 0 B )( ) ( 0 BT) K=1 OBTAINS ONLY DIAG 3X3
DO 1 I=1,6
DO 1 J=1,6
PS(I,J)=0.
1 DUM(I,J)=0.
DO 2 I=1,3
I3=I+3
DO 2 J=1,3
J3=J+3
DO 2 K=1,3
K3 = K+3
DUM(I,J)=DUM(I,J)+ B(I,K)*P(K,J)
DUM(I3,J3)=DUM(I3,J3)+ B(I,K)*P(K3,J3)
GO TO(2,3), KK
3 DUM(I,J3) =DUM(I,J3) + B(I,K)*P(K,J3)
2 CONTINUE
DO 5 I=1,3
I3=I+3
DO 5 J=1,3
J3=J+3
DO 4 K=1,3
K3=K+3
PS(I,J)=PS(I,J) + DUM(I,K)*B(J,K)
PS(I3,J3)=PS(I3,J3) +DUM(I3,K3)*B(J,K)
GO TO(4,6), KK
6 PS(I,J3) =PS(I,J3) +DUM(I ,K3)*B(J,K)
4 CONTINUE
GO TO(5,7),KK
7 PS(J3,I)=PS(I,J3)
5 CONTINUE
8 CONTINUE
RETURN
END

```

PTRN
PTRN
PTRN000
PTRN0010
PTRN0020
PTRN0030
PTRN0035
PTRN0040
PTRN0050
PTRN0060
PTRN0070
PTRN0080
PTRN0090
PTRN0100
PTRN0110
PTRN0120
PTRN0130
PTRN0140
PTRN0150
PTRN0160
PTRN0170
PTRN0180
PTRN0190
PTRN0200
PTRN0210
PTRN0220
PTRN0230
PTRN0240
PTRN0250
PTRN0260
PTRN0270
PTRN0280
PTRN0290
PTRN0300
PTRN0310
PTRN0320
PTRN0330
PTRN0340
PTRN

Subroutine: RETRO

Purpose: To take the P and PAR covariance matrices through a retro maneuver into a circular orbit.

Calling Sequence:

CALL RETRO

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I					Quantities obtained from common
O					Quantities returned to common

Common storages used or required:

T, S, C, IC

Subroutines required:

MATRX, SETN

Functions required:

DOT, FNORM, SQRT

Approximate number of storages required:

779 DEC

Derivation of Guidance Law Through Retro Maneuver

The vehicle is assumed to be at periapsis at the time the subroutine is called. The maneuver is then carried out such that the vehicle is in circular orbit after retro fire.

The required velocity at periapsis for a circular orbit is:

$$v_p = \sqrt{\frac{\mu}{R_p}}$$

The required incremental velocity correction along the nominal trajectory is the following

$$\Delta \vec{v} = \left(\frac{v_p}{v_n} - 1 \right) \vec{v}_n \quad v_n = |\vec{v}_n| \quad (1)$$

where v_n is the nominal periapsis velocity vector for the incoming trajectory.

The guidance law which governs the deviations from the nominal is obtained in the following manner. The deviation from nominal periapsis velocity (assuming linear theory) may be written as:

$$\delta \vec{v}_p = \dot{\underline{x}} + A \underline{x} \quad (2)$$

3x1 3x1(3x3) (3x1)

where

$$A = \begin{pmatrix} \frac{\partial v_p}{\partial x_1} & 0 & 0 \\ 0 & \frac{\partial v_p}{\partial x_2} & 0 \\ 0 & 0 & \frac{\partial v_p}{\partial x_3} \end{pmatrix}$$

and $\underline{\hat{X}}$ and $\dot{\underline{\hat{X}}}$ are the vehicle deviation state.

The partial derivatives in matrix A are the following:

$$\frac{\partial U_p}{\partial X_i} = - \frac{\mu X_i}{2U_p R^3} \quad i = 1, 2, 3$$

The estimate of periapsis velocity deviation from equation (2) is

$$\delta \underline{\hat{U}}_p = \underline{\hat{X}} + A \underline{\hat{X}} \quad (3)$$

and the guidance law is obtained as follows:

$$\delta \underline{\hat{U}}_p + \underline{\dot{\hat{X}}}_{g_t} = 0 = \underline{\hat{X}} + A \underline{\hat{X}} + \underline{\dot{\hat{X}}}_{g_t}$$

or

$$\underline{\dot{\hat{X}}}_{g_t} = - (A \ I) \begin{pmatrix} \underline{\hat{X}} \\ \underline{\hat{X}} \\ \underline{\dot{\hat{X}}} \end{pmatrix} \quad (4)$$

3x1 3x6 6x1

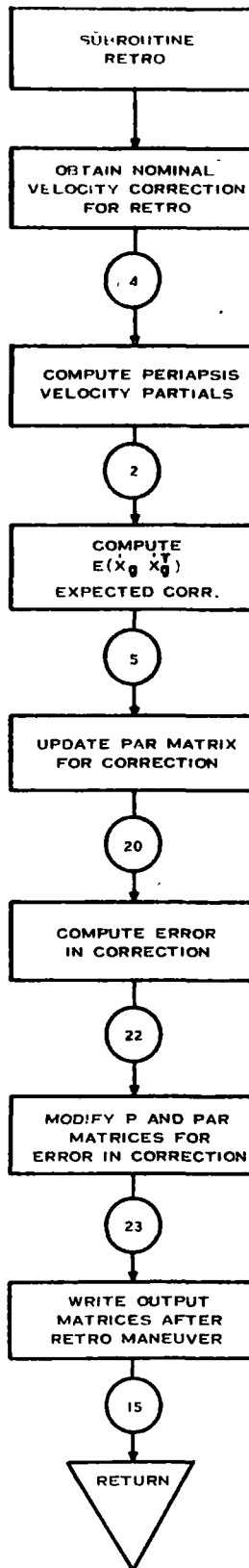
The total guidance correction is the sum of equations (1) and (4).

$$\underline{\dot{\hat{X}}}_{gt} = - (A \ I) \begin{pmatrix} \underline{\hat{X}} \\ \underline{\hat{X}} \\ \underline{\dot{\hat{X}}} \end{pmatrix} + \Delta \underline{\hat{V}} \quad (5)$$

The guidance law expressed by equation (4) corresponds to equation (6) in the guidance correction derivation in subroutine GUID. The P and PAR covariance matrices are then updated as shown by the derivation in the GUID subroutine writeup. The additional term, $\Delta \underline{\hat{V}}$, present in the total guidance correction required is treated as being independent of the deviation state. Therefore, the $E(\underline{\dot{\hat{X}}}_{gt} \underline{\dot{\hat{X}}}_{gt}^T)$ may be written as:

$$E(\underline{\dot{\hat{X}}}_{gt} \underline{\dot{\hat{X}}}_{gt}^T) = E(\underline{\dot{\hat{X}}}_g \underline{\dot{\hat{X}}}_g^T) + \Delta \underline{\hat{V}} \Delta \underline{\hat{V}}^T$$

since $E(\underline{\dot{\hat{X}}}_g \Delta \underline{\hat{V}}^T) = 0$



S-344

RETRO - 4

```

* LABEL
* SYMBOL TABLE
CEC2030 SUBROUTINE RETRO
SUBROUTINE RETRO
COMMON T,S,C,IC
DIMENSION T(1360),S(1000),C(1000),IC(1)
1,TPAR(3,6),PAR(6,6),P(6,6),DUP(3,3)
2,TGUID(6),DUM(3,3),DUN(3,3),DUMM(6,6)
DIMENSION XP(3),VXP(3),CV(3)
EQUIVALENCE (T,TDUM),(S,SDUM),(C,CDUM)
1,(IC,ICDUM),(C(568),TPAR),(C(460),PAR)
2,(C(652),P),(IC(218),N),(C(648),TGUIDE)
3,(IC(219),IGD),(IC(217),IGDTP),(IC(214),NOUT)
4,(C(30),TSEC),(S(476),TGUID),(S(483),RATIO)
5,(S(473),QQPT),(S(471),QQSO),(S(484),DMONIT)
EQUIVALENCE (C(15),XP),(C(18),VXP),(C(55),U)
CALL SETN(NIN,NUTS)
WRITE OUTPUT TAPE NUTS,701
701 FORMAT(94H THE DOLLOWING DATA ARE CONDITIONS AFTER RETRO INTO CIRCULAR ORBIT ASSUMING VEHICLE AT PERIGEE)
R2=DOT(XP,XP)
R=FNORM(XP)
VM=FNORM(VXP)
VP=SQRTF(U/R)
DELV=VP/VM
DO 1 I=1,3
1 CV(I)=DELV*VXP(I)
WRITE OUTPUT TAPE NUTS,700,CV
700 FORMAT(35H CIRCULAR VELOCITY COMPONENTS X,Y,Z/(3E17,8))
DO 4 I=1,3
4 CV(I)=(CV(I)-VXP(I))**2
CONS=-U/(2.*VP*R2*R)
DO 2 I=1,3
II=I+3
DO 3 J=1,3
JJ=J+3
TPAR(I,J)=0.
3 TPAR(I,JJ)=0.
TPAR(I,I)=CONS*XP(I)
2 TPAR(I,II)=-1.
CALL MATRX(TPAR,P,DUM,3,6,6,1)
CALL MATRX(TPAR,PAR,DUN,3,6,6,1)
DO 5 I=1,3
DO 6 J=1,3
6 DUM(I,J)=DUN(I,J)-DUM(I,J)
5 DUM(I,I)=DUM(I,I)+CV(I)
RMSV2=DUM(1,1)+DUM(2,2)+DUM(3,3)
RMSV=SQRTF(RMSV2)
C FOLLOWING IS UPDATING OF PAR MATRIX FOR GUIDANCE CORRECTION
DO 17 I=1,6
DO 17 J=I,6

```

RETR
RETR
RETR
RETR000
RETR001
RETR002
RETR003
RETR004
RETR005
RETR006
RETR007
RETR008
RETR009
RETR010
RETR011
RETR012
RETR013
RETR014
RETR015
RETR016
RETR017
RETR018
RETR019
RETR020
RETR021
RETR022
RETR023
RETR024
RETR025
RETR026
RETR027
RETR028
RETR029
RETR030
RETR031
RETR032
RETR033
RETR034
RETR035
RETR036
RETR037
RETR038
RETR039
RETR040
RETR041
RETR042
RETR043
RETR044
RETR045
RETR046
RETR047

RETRO (cont'd)

WDL-TR2

```

PAR(I,J)=PAR(I,J)-P(I,J)
PAR(J,I)=PAR(I,J)
17 CONTINUE
DO 19 I=1,3
II=I+3
DO 18 J=1,3
JJ=J+3
DUMM(II,J)=TPAR(I,J)
DUMM(I,JJ)=0.
DUMM(II,JJ)=0.
18 DUMM(I,J)=0.
19 DUMM(I,I)=1.
CALL MATRX(DUMM,PAR,PAR,6,6,6,1)
DO 20 I=1,6
DO 20 J=I,6
PAR(I,J)=PAR(I,J)+P(I,J)
PAR(J,I)=PAR(I,J)
20 CONTINUE
CRUD=QQPT*RMSV2
QQ=QQSO-QQPT
DO 22 I=1,3
DO 21 J=I,3
DUN(I,J)=QQ*DUM(I,J)
DUN(J,I)=DUN(I,J)
21 CONTINUE
DUN(I,I)=DUN(I,I)+CRUD
22 CONTINUE
RMSERR=SQRTF(DUN(1,1)+DUN(2,2)+DUN(3,3))
DO 23 I=1,3
II=I+3
DO 23 J=I,3
JJ=J+3
PAR(II,JJ)=PAR(II,JJ)+DUN(I,J)
PAR(JJ,II)=PAR(II,JJ)
P(II,JJ)=P(II,JJ)+DMONIT*DUN(I,J)
P(JJ,II)=P(II,JJ)
23 CONTINUE
WRITE OUTPUT TAPE NUTS,702,RMSV,RMSERR
702 FORMAT(24H RETRO GUID DATA FOLLOWS/
115H RMS VEL REQ=,E15.8,10X,18H RMSERR IN CORR=,E15.8)
WRITE OUTPUT TAPE NUTS,703,P
703 FORMAT(9H P MATRIX/(6E17.8))
WRITE OUTPUT TAPE NUTS,704,PAR
704 FORMAT(11H PAR MATRIX/(6E17.8))
15 RETURN
END

```

RETR048
 RETR049
 RETR050
 RETR051
 RETR052
 RETR053
 RETR054
 RETR055
 RETR056
 RETR057
 RETR058
 RETR059
 RETR060
 RETR061
 RETR062
 RETR063
 RETR064
 RETR065
 RETR066
 RETR067
 RETR068
 RETR069
 RETR070
 RETR071
 RETR072
 RETR073
 RETR074
 RETR075
 RETR076
 RETR077
 RETR078
 RETR079
 RETR080
 RETR081
 RETR082
 RETR083
 RETR084
 RETR085
 RETR086
 RETR087
 RETR088
 RETR089
 RETR090
 RETR091
 RETR092
 RETR

Subroutine: ROTATE

Purpose: To compute a 3 x 3 rotation matrix for a transformation of coordinates about axis i ($i = 1, 2, 3$) through an angle $\pm \theta$.

[For example: rotation about axis 1, matrix =
$$\begin{pmatrix} 1 & 0 & 0 \\ 0 & \cos \theta & -\sin \theta \\ 0 & \sin \theta & \cos \theta \end{pmatrix}$$

Calling Sequence:

CALL ROTATE (NCOORD, ANG, RMTRIX, IROT)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	NCOORD	1	$i, i = 1, 2, 3$		Axis of rotation
I	ANG	1	θ	radians	Angle for rotation
O	RMTRIX	3,3			Resulting rotation matrix
I	IROT	1			If IROT < 0, use $-\theta$.

Common storages used or required: None

Subroutines required: None

Functions required: None

Approximate number of storages required: _____

ROTATE

WDL-TR21

```
* LABEL
* SYMBOL TABLE
SUBROUTINE ROTATE(NCOORD,ANG,RMATRIX,IROT)
DIMENSION RMATRIX(3,3)
SANG = SIN(ANG)
CANG = COS(ANG)
IF (IROT) 1,2,2
1 SANG = -SANG
2 DO 3 I=1,3
  DO 3 J=1,3
3 RMATRIX(I,J) = 0.
  GO TO (4,5,6), NCOORD
4 I = 2
  J = 3
  GO TO 7
5 I = 1
  J = 3
  GO TO 7
6 I = 1
  J = 2
7 RMATRIX(NCOORD,NCOORD) = 1.
  RMATRIX(I,I) = CANG
  RMATRIX(I,J) = SANG
  RMATRIX(J,I) = -SANG
  RMATRIX(J,J) = CANG
RETURN
END
```

ROTA
ROTA
ROTA0000
ROTA0010
ROTA0020
ROTA0030
ROTA0040
ROTA0050
ROTA0060
ROTA0070
ROTA0080
ROTA0090
ROTA0100
ROTA0110
ROTA0120
ROTA0130
ROTA0140
ROTA0150
ROTA0160
ROTA0170
ROTA0180
ROTA0190
ROTA0200
ROTA0210
ROTA0220
ROTA0230
ROTA

Subroutine: ROTEQ

Purpose: ROTEQ evaluates elements of the rotation matrix which relate the general precession of the earth's equator and the consequent retrograde motion of the equinox on the ecliptic. It is used to provide the transformation from mean equator and equinox of 1950.0 to mean equator and equinox of date.

Calling Sequence:

CALL ROTEQ (TIME, A)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	TIME	1	T	days	Total number days from reference epoch (1950.0)
O	A	3,3	A		Rotation matrix

Common storages used or required: None

Subroutines required: None

Functions required: None

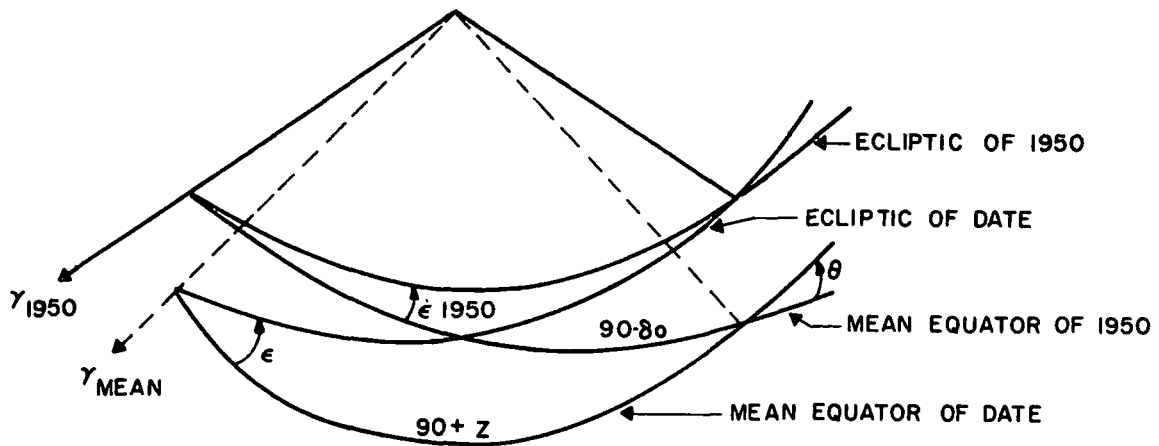
Approximate number of storages required: _____

Elements of Transformation

The rotation matrix may be represented as

$$\begin{pmatrix} x' \\ y' \\ z' \end{pmatrix} = \begin{pmatrix} a_{11} & a_{12} & a_{13} \\ a_{21} & a_{22} & a_{23} \\ a_{31} & a_{32} & a_{33} \end{pmatrix} \begin{pmatrix} X \\ Y \\ Z \end{pmatrix}$$

where X, Y, Z are expressed in the mean equator and equinox of 1950.0 and x', y', z' are the coordinates in the mean equator and equinox of date.



The geometry of the precession has been represented by the three small parameters δ_0 , z , and θ . γ_{1950} is the mean equinox of 1950; $\bar{\epsilon}_{1950}$ is the mean obliquity of 1950; γ_{mean} is the mean equinox of date; $\bar{\epsilon}$ is the mean obliquity of date. Measured in the mean equator of 1950 from the mean equinox of 1950, $90^\circ - \delta_0$ is the right ascension of the ascending node of the mean equator of date on the mean equator of 1950.

$90^\circ + z$ is the right ascension of the node measured in the mean equator of date from the mean equinox of date. θ is the inclination of the mean equator of date to the mean equator of 1950.

In terms of δ_o , z , and θ , (a_{ij}) is given by:

$$a_{11} = -\sin \delta_o \sin z + \cos \delta_o \cos z \cos \theta$$

$$a_{12} = -\cos \delta_o \sin z - \sin \delta_o \cos z \cos \theta$$

$$a_{13} = -\cos z \sin \theta$$

$$a_{21} = \sin \delta_o \cos z + \cos \delta_o \sin z \cos \theta$$

$$a_{22} = \cos \delta_o \cos z - \sin \delta_o \sin z \cos \theta$$

$$a_{23} = -\sin z \sin \theta$$

$$a_{31} = \cos \delta_o \sin \theta$$

$$a_{32} = -\sin \delta_o \sin \theta$$

$$a_{33} = \cos \theta$$

$$\delta_o = 2304'' 997T + ''302T^2 + ''0179T^3$$

$$z = 2304'' 997T + ''093T^2 + ''0192T^3$$

$$\theta = 2004'' 298T - ''426T^2 - ''0416T^3$$

with T the number of Julian centuries of 36,525 days past the epoch 1950.0.

The actual computational form of (a_{ij}) is obtained by expanding the a_{ij} in power series in δ_0 , z , θ and replacing the arguments by the above time series. The results are:

$$a_{11} = 1 - .00029697T^2 - .00000013T^3$$

$$a_{12} = -a_{21} = -.02234988T - .00000676T^2 + .00000221T^3$$

$$a_{13} = -a_{31} = -.00971711T + .00000207T^2 + .00000096T^3$$

$$a_{22} = 1 - .00024976T^2 - .00000015T^3$$

$$a_{23} = a_{32} = -.00010859T^2 - .00000003T^3$$

$$a_{33} = 1 - .00004721T^2 + .00000002T^3$$

```

* LABEL
* SYMBOL TABLE
SUBROUTINE ROTEQ(TIME,A)
DIMENSION A(3,3)
T = TIME/36525.
T2 = T*T
T3 = T2*T
A(1,1) = 1. - .00029697*T2 - .00000013*T3
A(1,2) = -.02234988*T - .00000676*T2 + .00000221*T3
A(2,1) = -A(1,2)
A(1,3) = -.00971711*T + .00000207*T2 + .00000096*T3
A(3,1) = -A(1,3)
A(2,2) = 1. - .00024976*T2 - .00000015*T3
A(2,3) = -.00010859*T2 - .00000003*T3
A(3,2) = A(2,3)
A(3,3) = 1. - .00004721*T2 + .00000002*T3
RETURN
END

```

```

ROTO
ROTO
ROTO000
ROTO001
ROTO002
ROTO003
ROTO004
ROTO005
ROTO006
ROTO007
ROTO008
ROTO009
ROTO010
ROTO011
ROTO012
ROTO013
ROTO014
ROTO

```

Page Intentionally Left Blank

Subroutine: RVIN

Purpose: To transform inertial equatorial spherical to Cartesian coordinates.

Calling Sequence:

CALL RVIN (A, B, C)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	A	5	$A(1) = R$		Magnitude of Position Vector
			$A(2) = \phi$	deg	Declination
			$A(3) = \theta$	deg	Right Ascension
			$A(4) = V$		Magnitude of Velocity Vector
			$A(5) = \Gamma$	deg	Flight Path Angle
			$A(6) = \Sigma$	deg	Azimuth
O	B	3			X, Y, Z
O	C	3			\dot{X} , \dot{Y} , \dot{Z}

Common storages used or required:

None

Subroutines required:

None

Functions required:

SIN, COS

Approximate number of storages required:

RVIN

The calling sequence consists of

CALL RVIN (XIN, XOUT, VOUT)

where: XIN is a vector with dimension six. The vector contains the spherical set in the following order

$$\text{XIN} = \begin{pmatrix} |R| \\ 0 \\ \theta \\ |V| \\ \gamma \\ \sigma \end{pmatrix} \quad \begin{array}{l} |R| = \text{Magnitude position vector} \\ 0 = \text{Declination} \\ \theta = \text{Right ascension} \\ |V| = \text{Magnitude velocity vector} \\ \gamma = \text{Flight path angle} \\ \sigma = \text{Azimuth} \end{array}$$

6x1

XOUT is a vector with dimension three. The vector contains the Cartesian components of position

$$\text{XOUT} = \begin{pmatrix} x \\ y \\ z \end{pmatrix}$$

3x1

VOUT is a vector with dimension three. The vector contains the Cartesian components of velocity

$$\text{VOUT} = \begin{pmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \end{pmatrix}$$

3x1

RVIN TRANSFORMATIONS

The position transformation is obtained as follows (see Fig. 1 below).

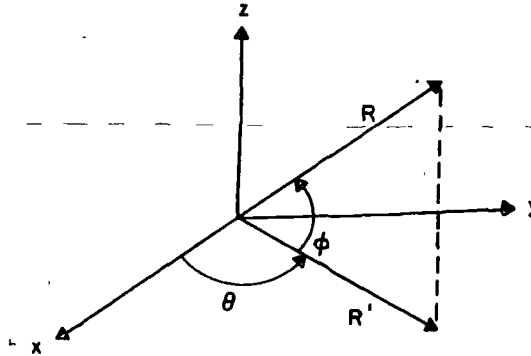


FIG 1

Projecting \vec{R} on the x-y plane, θ is the angle from the x axis to the projection measured counterclockwise. The elevation of \vec{R} above the x-y plane is the angle ϕ . The formulas are

$$\text{XOUT} = \begin{pmatrix} x \\ y \\ z \end{pmatrix}_{3 \times 1} = |R| \begin{pmatrix} \cos \phi \cos \theta \\ \cos \phi \sin \theta \\ \sin \phi \end{pmatrix}_{3 \times 1} \quad (1)$$

The velocity transformation is obtained as follows. The azimuth and flight path angles refer to the tangent plane which is normal to the \vec{R} vector (see Fig. 2).

$$\begin{matrix} \begin{pmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \end{pmatrix} \\ 3 \times 1 \end{matrix} = \begin{matrix} \begin{pmatrix} \hat{U} & \hat{E} & \hat{N} \end{pmatrix} \\ 3 \times 3 \end{matrix} \begin{matrix} \begin{pmatrix} \dot{U} \\ \dot{E} \\ \dot{N} \end{pmatrix} \\ 3 \times 1 \end{matrix} = \begin{matrix} \begin{pmatrix} \cos \phi \cos \theta \sin \theta & -\sin \phi \cos \theta \\ \cos \phi \sin \theta \cos \theta & -\sin \phi \sin \theta \\ \sin \phi & 0 & \cos \phi \end{pmatrix} \\ 3 \times 3 \end{matrix} \begin{matrix} \begin{pmatrix} \dot{U} \\ \dot{E} \\ \dot{N} \end{pmatrix} \\ 3 \times 1 \end{matrix} \quad (5)$$

The velocity vector in the tangent plane coordinates (Fig. 2) is

$$\begin{matrix} \vec{V} \\ 3 \times 1 \end{matrix} = \begin{matrix} \begin{pmatrix} \dot{U} \\ \dot{E} \\ \dot{N} \end{pmatrix} \\ 3 \times 1 \end{matrix} = |V| \begin{matrix} \begin{pmatrix} \sin \gamma \\ \cos \gamma \sin \sigma \\ \cos \gamma \cos \sigma \end{pmatrix} \\ 3 \times 1 \end{matrix} \quad (6)$$

Substituting equation (6) into (5) yields the desired transformation

$$\begin{matrix} V_{OUT} \\ 3 \times 1 \end{matrix} = \begin{matrix} \begin{pmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \end{pmatrix} \\ 3 \times 1 \end{matrix} = |V| \begin{matrix} \begin{pmatrix} \hat{U} & \hat{E} & \hat{N} \end{pmatrix} \\ 3 \times 3 \end{matrix} \begin{matrix} \begin{pmatrix} \sin \gamma \\ \cos \gamma \sin \sigma \\ \cos \gamma \cos \sigma \end{pmatrix} \\ 3 \times 1 \end{matrix}$$

```

* LABEL
* SYMBOL TABLE
SUBROUTINE RVIN(A,B,C)
DIMENSION A(6),B(3),C(3),D(3,3),E(3)
A(2) = A(2)*.017453293
A(3) = A(3)*.017453293
A(5) = A(5)*.017453293
A(6) = A(6)*.017453293
CP = COSF(A(2))
SP = SIN F(A(2))
CT = COSF(A(3))
ST = SIN F(A(3))
CG = COSF(A(5))
SG = SIN F(A(5))
CS = COSF(A(6))
SS = SIN F(A(6))
SPCT = SP*CT
SPST = SP*ST
CGSS = CG*SS
CGCS = CG*CS
CPCT = CP*CT
CPST = CP*ST
D(1,1) = CPCT
D(1,2) = -ST
D(1,3) = -SPCT
D(2,1) = CPST
D(2,2) = CT
D(2,3) = -SPST
D(3,1) = SP
D(3,2) = 0.
D(3,3) = CP
B(1) = A(1)*CPCT
B(2) = A(1)*CPST
B(3) = A(1)*SP
E(1) = A(4)*SG
E(2) = A(4)*CGSS
E(3) = A(4)*CGCS
DO 1 I=1,3
C(I) = 0.
DO 1 J=1,3
1 C(I) = C(I) + D(I,J)*E(J)
RETURN
END

```

```

RVIN
RVIN
RVIN0000
RVIN0010
RVIN0020
RVIN0030
RVIN0040
RVIN0050
RVIN0060
RVIN0070
RVIN0080
RVIN0090
RVIN0100
RVIN0110
RVIN0120
RVIN0130
RVIN0140
RVIN0150
RVIN0160
RVIN0170
RVIN0180
RVIN0190
RVIN0200
RVIN0210
RVIN0220
RVIN0230
RVIN0240
RVIN0250
RVIN0260
RVIN0270
RVIN0280
RVIN0290
RVIN0300
RVIN0310
RVIN0320
RVIN0330
RVIN0340
RVIN0350
RVIN0360
RVIN0370
RVIN0380
RVIN0390
RVIN

```

Subroutine: RVOUT

Purpose: To convert Cartesian position and velocity coordinates to inertial equatorial spherical coordinates.

Calling Sequence: -----

CALL RVOUT (A, B, C)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	A	3	X, Y, Z		Position coordinates
I	B	3	$\dot{X}, \dot{Y}, \dot{Z}$		Velocity coordinates
O	C	6	C(1) = R		Magnitude of position vector
			C(2) = ϕ	degrees	Declination
			C(3) = α	degrees	Right ascension
			C(4) = V		Magnitude of velocity vector
			C(5) = Γ	degrees	Flight path angle
			C(6) = Σ	degrees	Azimuth

Common storages used or required:

None

Subroutines required:

CORSS

Functions required:

ATANF, SORTF, ARKTNS, DOT,
ACOS, FNORM

Approximate number of storages required:

RVOUT

The transformations required to convert Cartesian coordinates to inertial equatorial spherical are the inverse of those required by, and described under, RVIN.

For the position coordinates:

$$R = \sqrt{X^2 + Y^2 + Z^2}$$

$$\phi = \sin^{-1} \frac{Z}{R} \quad -90^\circ \leq \phi \leq 90^\circ$$

$$\theta = \tan^{-1} \frac{Y}{X} \quad \left. \begin{array}{l} + 0 \text{ for } X > 0 \\ + 180^\circ \text{ for } X \leq 0 \end{array} \right\}$$

For the velocity coordinates, \dot{X}' , \dot{Y}' , \dot{Z}' are obtained by applying the inverse of the transformation matrix $\begin{bmatrix} \hat{U} & \hat{E} & \hat{N} \\ 3 \times 3 \end{bmatrix}$ given in RVIN. Then:

$$|V| = \sqrt{\dot{X}'^2 + \dot{Y}'^2 + \dot{Z}'^2}$$

$$\Gamma = \sin^{-1} \frac{\dot{X}'}{V} \quad -90^\circ \leq \Gamma \leq 90^\circ$$

$$\Sigma = \tan^{-1} \frac{\dot{Y}'}{\dot{Z}'} \quad \left. \begin{array}{l} + 0 \text{ for } \dot{Z}' > 0 \\ + 180 \text{ for } \dot{Z}' \leq 0 \end{array} \right\}$$

* LABEL	RVOT
* SYMBOL TABLE	RVOT
CEC2017 SUBROUTINE RVOUT	RVOT
SUBROUTINE RVOUT(A,B,C)	RVOT000
DIMENSION A(3),B(3), C(6),E(3),G(3),H(3)	RVOT001
ACOSF(X) = ATANF(SQRTF(1.-X**2)/X)	RVOT002
C(1) = FNORM(A)	RVOT003
C(4) = FNORM(B)	RVOT004
C(2) = ATANF(A(3)/SQRTF(A(1)**2+A(2)**2))	RVOT005
C(3)=ARKTNS(360,A(1),A(2))	RVOT006
4 F = DOT(A,B)	RVOT007
ARG = F/(C(1)*C(4))	RVOT008
C(5) = ACOSF(ARG)	RVOT009
IF (ARG) 5,6,6	RVOT010
5 C(5) = -1.5707963 - C(5)	RVOT011
GO TO 7	RVOT012
6 C(5) = 1.5707963 - C(5)	RVOT013
7 CALL CROSS(A,B,E)	RVOT014
EN=FNORM(E)	RVOT015
DO 12 I=1,3	RVOT016
12 E(I)=E(I)/EN	RVOT017
CALL CROSS(E,A,G)	RVOT018
GN = FNORM(G)	RVOT019
DO 8 I=1,3	RVOT020
8 G(I) = G(I)/GN	RVOT021
H(1) = 0.	RVOT022
H(2) = 0.	RVOT023
H(3) = 1.	RVOT024
CALL CROSS(H,A,E)	RVOT025
ARG = DOT(E,G)	RVOT026
EN = FNORM(E)	RVOT027
ARG = ARG/EN	RVOT028
C(6) = ACOSF(ARG)	RVOT029
IF (G(3)) 9,10,10	RVOT030
9 C(6) = C(6) + 1.5707963	RVOT031
GO TO 11	RVOT032
10 C(6) = -C(6) + 1.5707963	RVOT033
11 CONTINUE	RVOT034
C(2) = C(2)*57.29578	RVOT035
C(3) = C(3)*57.29578	RVOT036
C(5) = C(5)*57.29578	RVOT037
C(6) = C(6)*57.29578	RVOT038
RETURN	RVOT039
END	RVOT

Page Intentionally Left Blank

Subroutine: SDEC

Purpose: To compute the total perturbation accelerations due to earth's oblateness, perturbing bodies, and Encke perturbations due to deviations from reference conic. These perturbations are obtained by calling OBLN, BODY, and ENCKE and placed in the T block for use in the integration package.

Calling Sequence:

CALL _____

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I					Quantities obtained from common
O					Quantities placed in common

Common storages used or required:

T, S, C, IC

Subroutines required:

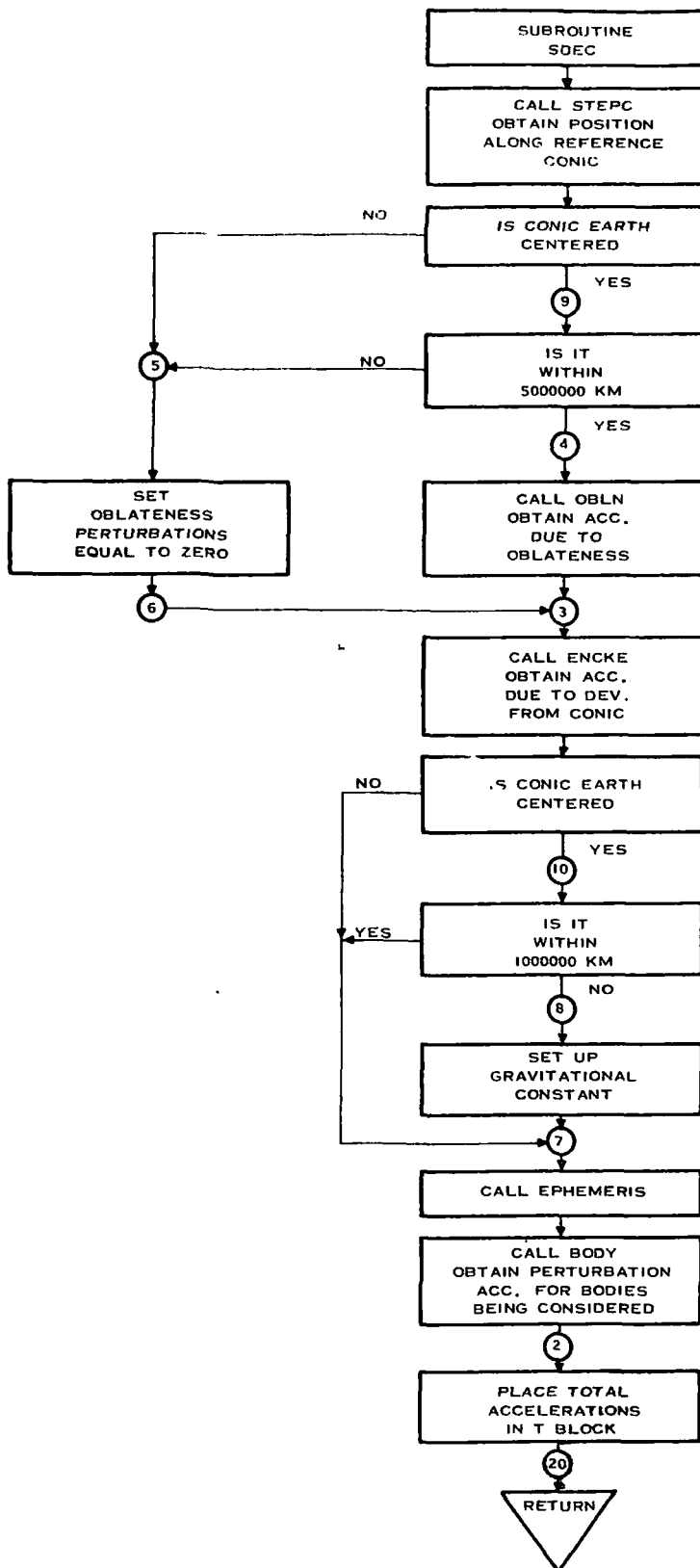
BODY, ENCKE, INTR, OBLN, STEPC

Functions required:

None

Approximate number of storages required:

195 DEC



* LABEL	SDEC
* SYMBOL TABLE	SDEC
CEC2024 SUBROUTINE SDEC	SDEC
SUBROUTINE SDEC	SDEC000
DIMENSION T(1360),S(1000),C(1000),IC(1)	SDEC001
DIMENSION RAD(3), X(3),VX(3),XP(3),	SDEC002
1 AE(3),AO(3),AP(3),PO(22),VE(22),CA(3),VKB(6),	SDEC003
2 RBO(6),RBOP(6) ,UM(6),VXP(3),AN(3,3),EN(3,3),EA(3,3)	SDEC004
3,BP(3,3) ,XSO(3),VXSO(3)	SDEC005
COMMON T,S,C,IC	SDEC006
EQUIVALENCE (T,TDUM),(S,SDUM),(C,CDUM)	SDEC007
EQUIVALENCE (S(11),VJ),(S(12),H),(S(13),D),(S(900),RAD)	SDEC008
EQUIVALENCE (C(10),TW),(C(11),TF),(C(13),TP1),(C(14),TP2)	SDEC009
1,(C(15),XP),(C(18),VXP),(C(21),AE),(C(24),AO),(C(27),CA)	SDEC010
2,(C(33),X),(C(36),VX)	SDEC011
4,(C(55),U),(C(56),VKB),(C(62),PO),(C(84),VE),(C(106),RBO) - -	SDEC012
5,(C(112),RBOP),(C(120),EN),(C(129),EA),(C(138),AN),(C(171),BP)	SDEC013
7,(IC(1),N),(IC(2),IOR),(IC(3),NOR),(IC(4),KSTP),(IC(5),KTYPE)	SDEC014
8,(IC(6),ITARG),(S(14),RE),(C(46),XSO),(C(49),VXSO),(IC(231),NSTEP)	SDEC015
NEQ=3*N	SDEC016
CALL STEPC(NSTEP,T(2),XSO,VXSO,U,X,VX)	SDEC017
DO 1 I=1,3	SDEC018
1 XP(I) = X(I) + T(I+3)	SDEC019
IF(NOR-1)5,9,5	SDEC020
9 IF (RBOP-500000.) 4,5,5	SDEC021
4 CALL OBLN(XP,U,RE,VJ,H,D,AO,AN,BP,NEQ)	SDEC022
GO TO 3	SDEC023
5 DO 6 I=1,3	SDEC024
AO(I)=0.	SDEC025
DO 6 J=1,3	SDEC026
BP(I,J)=0.	SDEC027
6 CONTINUE	SDEC028
3 CALL ENCKE(U,X,T(4),AE)	SDEC029
IF(NOR-1)7,10,7	SDEC030
10 IF (RBOP-1000000.) 7,8,8	SDEC031
8 VKB(6) = UM(6)	SDEC032
7 NV = 0	SDEC033
NR1=NOR-1	SDEC034
TP2 = TF+T(2)/86400.	SDEC035
TWGN=0.	SDEC036
21 CONTINUE	SDEC037
IF(TP2)22,23,23	SDEC038
22 CONTINUE	SDEC039
TP2=TP2+1.	SDEC040
TWGN=TWGN-1.	SDEC041
GO TO 21	SDEC042
23 CONTINUE	SDEC043
TFP = INTF(TP2)	SDEC044
TP2 = TP2-TFP	SDEC045
TP1=TW+TFP+TWGN	SDEC046
CALL INTR(TP1,TP2,NR1,PO,NV,VE,RBOP)	SDEC047

SDEC (cont'd)

WDL-TR218

```
CALL BODY(XP,PO,VKB,RBO,RBOP,CA,NOR,BP,T,NEQ,U)
KJ=2*NEQ+3
DO 2 I=1,3
KI=KJ+I
2 T(KI) = AO(I) + AE(I) -CA(I)
20 RETURN
END
```

SDEC0480
SDEC0490
SDEC0500
SDEC0510
SDEC0520
SDEC0530
SDEC

S-368

SDEC - 4

Subroutine: SETN

Purpose: SETN sets the logical tape numbers for input and output to conform with the system unit table.

Calling Sequence:

CALL SETN (NIN, NOUT)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
0	NIN	1			Logical input tape unit
0	NOUT	1			Logical output tape unit

Common storages used or required: None

Subroutines required: None

Functions required: None

Approximate number of storages required: _____

SETN

WDL-TR

* LABEL
CEC2023
SUBROUTINE SETN(NIN,NOUT)
C CALLING THIS SUBROUTINE RESULTS IN THE USE OF
C INPUT TAPE 2 AND OUTPUT TAPE 3
C USER MUST READ INPLT TAPE NIN, AND WRITE OUTPUT NOUT,
NIN=2
NOUT=3
RETURN
END

SETN
SETN0000
SETN0001
SETN0002
SETN0030
SETN004
SETN005
SETN0060
SETN0070
SETN

Subroutine: SHIFTP

Purpose: To change position and velocity coordinates from a coordinate system centered at body IOR to one centered at body NOR. SHIFTP also returns the new gravitational constant and the position and velocity of all bodies on the ephemeris tape referenced to the new center. (The latter is done by calling the ephemeris subroutine INTRI)

Calling Sequence:

CALL SHIFTP (IOR, NOR, U, UM, X, VX, PO, VE, TP1, TP2)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	IOR	1			Index of old central body
I	NOR	1			Index of new central body
O	U	1	μ	Km ³ /sec ²	Gravitational constant, body NOR
I	UM	6			Array of gravitational constants
I-O	X	3	X, Y, Z	Km	Positions } input: * w.r.t. body IOR
I-O	VX	3	$\dot{X}, \dot{Y}, \dot{Z}$	Km/sec	Velocities } output: w.r.t. body NOR
O	PO	22		Km	Positions } of bodies on tape w.r.t.
O	VE	22		Km/sec	Velocities } body NOR
I	TP1	1		seconds	Double precision time in sec-
I	TP2	1		seconds	onds since 1950.

Common storages used or required:

None

Subroutines required:

INTRI

Functions required:

None

Approximate number of storages required:

* with respect to

The sequence used in shifting centers is the following:

IOR (NOR)	CENTRAL BODY
1	Earth
2	Moon
3	Sun
4	Venus
5	Mars
6	Jupiter

* LABEL	SHTP
* SYMBOL TABLE	SHTP
SUBROUTINE SHIFTP(IOR,NOR,U,UM,X,VX,PO,VE,TF,TW,T2)	SHTP000
COMMON T,S,C,IC	SHTP001
DIMENSION T(1360),S(1000),C(1000),IC(1)	SHTP002
DIMENSION UM(6),X(3),VX(3),PO(22),VE(22)	SHTP003
EQUIVALENCE (T,TDUM),(S,SDUM),(C,CDUM),(C(14),TP2),(C(13),TP1)	SHTP004
N = NOR	SHTP005
IO = IOR	SHTP006
IOR = NOR	SHTP007
U = UM(N)	SHTP008
NV = 1	SHTP009
DIS = 1.E10	SHTP010
NR1 = NOR-1	SHTP011
CALL INTR1(TP1,TP2,NR1,PO,NV,VE,DIS)	SHTP012
DO 1 I=1,3	SHTP013
J = 26-3*I0-I	SHTP014
X(I) = X(I)+PO(J)	SHTP015
1 VX(I) = VX(I)+VE(J)	SHTP016
RETURN	SHTP017
END	SHTP

Page intentionally left blank

Page intentionally left blank

Subroutine: STEPC

Purpose: To obtain the state, i.e., radius vector, R, and velocity vector, V, of a probe which is separated by a time increment, t, from a specified state, R_0 and V_0 , assuming an inverse-square central force law with gravitational constant u.

Calling Sequence:

CALL STEPC (N, T, R, V, U, RR, VV)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	N	1			Initializing index
I	T	1	Δt	sec	Incremental time
I	R	3	\vec{X}_0	Km	Initial Conic position (t_0)
I	V	3	$\dot{\vec{X}}_0$	Km/sec	Initial Conic Velocity (t_0)
I	U	1	μ	Km^3/sec^2	Gravitational constant
O	RR	3	\vec{X}	Km	Position on Conic ($t_0 + \Delta t$)
O	VV	3	$\dot{\vec{X}}$	Km/sec	Velocity on Conic ($t_0 + \Delta t$)

Common storages used or required:

None

Subroutines required:

DOT, GOTOR

Functions required:

ARKTNS, SQRT

Approximate number of storages required:

255 DEC

*Discussion

The inverse-square central force law is characterized by the equations

$$\begin{aligned}\dot{R} &= \frac{dR}{dt} = V \\ \dot{V} &= \frac{dV}{dt} = -\frac{u}{r^3} R\end{aligned}\quad (1)$$

where r is defined to be $+(R \cdot R)^{1/2}$.

The angular momentum vector, H , defined by the vector cross-product

$$H = R \times V \quad (2)$$

is a constant with respect to time, as seen by

$$\dot{H} = \dot{R} \times V + R \times \dot{V} = V \times V + R \times \left(\frac{-u}{r^3} R \right) = 0, \text{ so that } H = H_0 = R_0 \times V_0.$$

Because the magnitude, h_0 , of H_0 is generally nonzero, the plane equations

$$\begin{aligned}R \cdot H &= R \cdot H_0 = 0 \\ V \cdot H &= V \cdot H_0 = 0\end{aligned}\quad (3)$$

which follow from the definition of H , lead to the conclusion that all motion occurs in the plane normal to H_0 . That is, if R_0 and V_0 are non-zero and noncollinear vectors, any other vectors, such as R and V , must lie in the plane formed by R_0 and V_0 . Algebraically, one says that R and V may be expressed as linear combinations of R_0 and V_0 .

$$\begin{aligned}R &= f R_0 + g V_0 \\ V &= \dot{f} R_0 + \dot{g} V_0\end{aligned}\quad (4)$$

* Vectors will be denoted by capital letters and scalars by lower-case letters with the single exception of the rather standard symbol, E , for eccentric anomaly.

The second of equations (4) follows from (1) and from the fact that R_0 and V_0 are not functions of the time increment, t . The scalars, f , \dot{f} , g , and \dot{g} , are functions of R_0 , V_0 , and t . The discussion which follows concerns the determination of these scalars.

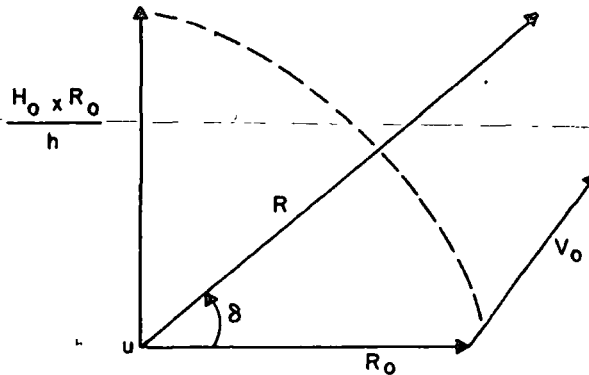


FIG 1

The vector $(H_0 \times R_0)/h$ is seen to be perpendicular to R_0 and to have the same magnitude, r_0 , as R_0 . Figure 1 shows that R may be written as the linear combination,

$$R = \frac{r}{r_0} \left[R_0 \cos \delta + \frac{H_0 \times R_0}{h} \sin \delta \right] \quad (5)$$

Equation (5) may be rewritten by expanding the vector triple cross-product,

$$H_0 \times R_0 = (R_0 \times V_0) \times R_0 = V_0 (R_0 \cdot R_0) - R_0 (R_0 \cdot V_0).$$

$$R = \frac{r}{r_0} \left[R_0 \left(\cos \delta - \frac{R_0 \cdot V_0}{h} \sin \delta \right) + V_0 \frac{r_0^2}{h} \sin \delta \right] \quad (5a)$$

Comparing equation (5a) with equation (4),

$$f = \frac{r}{r_0} \left(\cos \delta - \frac{R_0 \cdot V_0}{h} \sin \delta \right)$$

$$g = \frac{r r_0}{h} \sin \delta. \quad (6)$$

At this point, the reader should note that while r_0 , $R_0 \cdot V_0$, and h are computable directly from R_0 and V_0 , the quantities r and δ have not been specifically defined in terms of R_0 , V_0 , and t . In order to do so, it is necessary to examine the conic solution to the inverse-square law equations of motion.

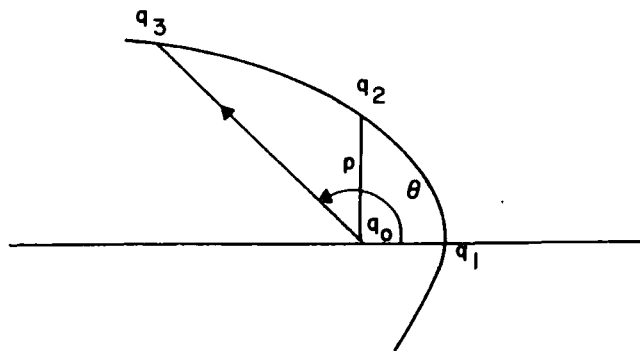


FIG 2

Figure 2 shows a conic section with focus at q_0 and pericenter at q_1 . The point q_3 on the conic is specified, in polar coordinates originating at q_0 , by the radius, r , and true anomaly, θ , θ being measured positive counter-clockwise from the line $\overline{q_0q_1}$. The length $\overline{q_0q_2}$ is called the semi-latus rectum and is denoted by p . The parameter specifying the shape of the conic is the eccentricity, e , which may be calculated from the equation

$$e = \frac{\overline{q_0q_2}}{\overline{q_0q_1}} - 1. \quad \text{The conic equation in an often-used form is,}$$

$$r = \frac{p}{1 + e \cos \theta} \quad (7)$$

S-378

STPEC - 4

Conic sections are characterized by eccentricity as follows:

circular	if	$e = 0$
elliptical	if	$0 < e < 1$
parabolic	if	$e = 1$
hyperbolic	if	$e > 1$

The two cases of great interest here are the elliptical and hyperbolic cases. Figure 3 below shows an ellipse.

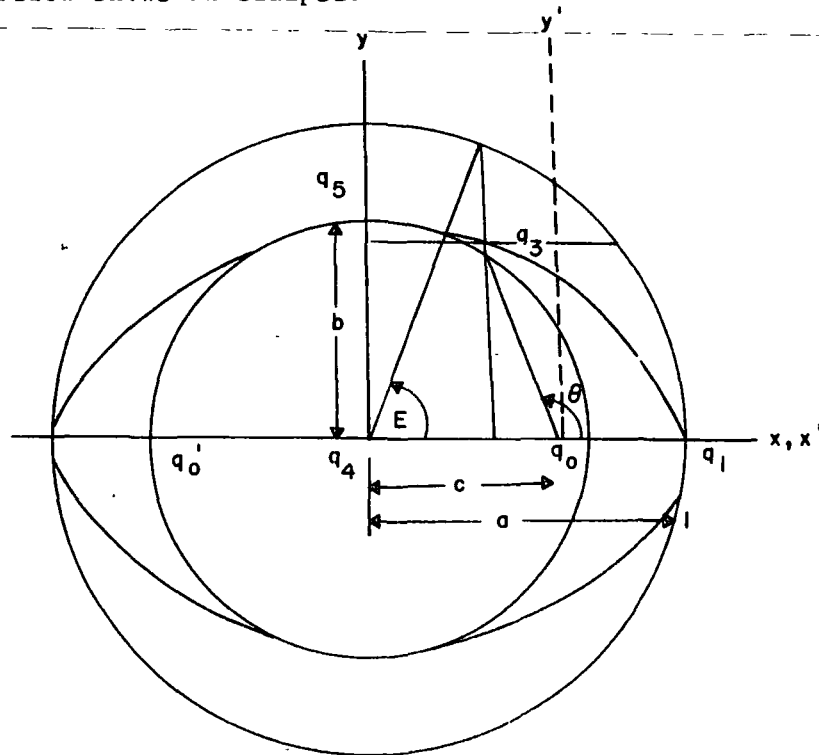


FIG. 3

The semi-major axis, a , is the distance from the point of symmetry, q_4 , to the pericenter, q_1 . The semi-minor axis, b , is the length $\overline{q_4q_5}$. The eccentricity is equal to the ratio

$$c/a = \frac{\sqrt{a^2 - b^2}}{a}$$

The eccentric anomaly, E , is the argument of the projection of the point, q_3 , from the line $\overline{q_4q_1}$ onto a circle of radius, a , concentric with the ellipse. That is, the Cartesian coordinates of q_3 relative to q_4 are

$$\begin{aligned} x &= a \cos E \\ y &= b \sin E \end{aligned} \quad (8)$$

Equations (8) give rise to the familiar equation of the ellipse

$$\frac{x^2}{a^2} + \frac{y^2}{b^2} = \cos^2 E + \sin^2 E = 1.$$

Relative to coordinates centered at q_0 , q_3 is described by

$$\begin{aligned} x' &= r \cos \theta = a \cos E - ea \\ y' &= y = r \sin \theta = b \sin E = a \sqrt{1-e^2} \sin E. \\ r &= x'^2 + y'^2 = a(1 - e \cos E) \end{aligned} \quad (8a)$$

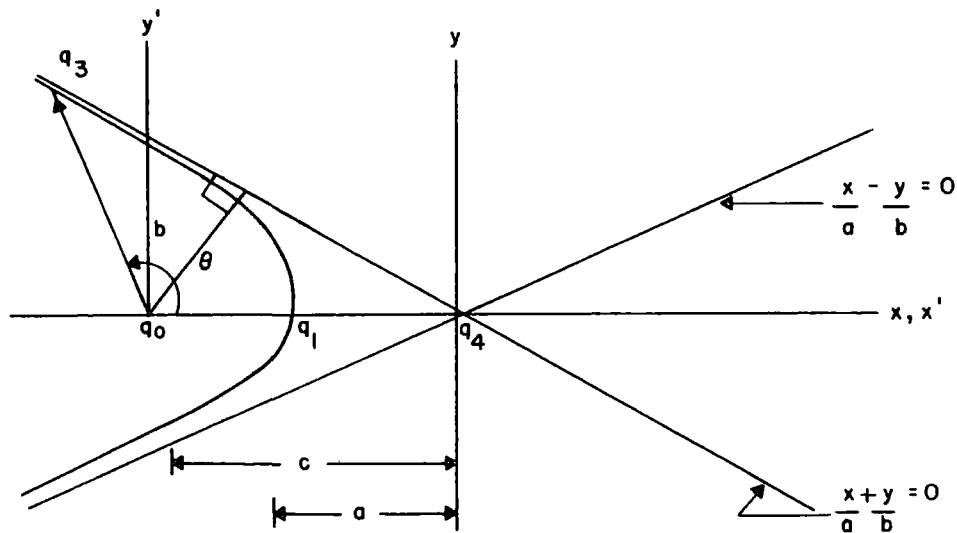


FIG 4

Figure 4 shows a conic section which is hyperbolic. The lines $\frac{x}{a} - \frac{y}{b} = 0$ and $\frac{x}{a} + \frac{y}{b} = 0$ are the asymptotes of the hyperbola. The semi-major axis, a , is again the distance from the point of symmetry, q_4 , to the pericenter, q_1 . The semi-minor axis, b , is defined as the distance from the focus, q_0 , to one of the asymptotes. Eccentricity is given by the ratio

$$c/a = \sqrt{\frac{a^2 + b^2}{a^2}}$$

The eccentric anomaly, E , (sometimes called F) is too difficult to picture to be included in Fig. 4. E is defined in such a way that q_3 is described in Cartesian coordinates by

$$\begin{aligned} x &= -a \cosh E \\ y &= b \sinh E, \end{aligned} \tag{9}$$

leading to the familiar hyperbolic equation

$$\frac{x^2}{a^2} - \frac{y^2}{b^2} = \cosh^2 E - \sinh^2 E = 1$$

The Cartesian coordinates of q_3 relative to q_0 are given by

$$\begin{aligned} x' &= r \cos \theta = ea - a \cosh E \\ y' &= r \sin \theta = b \sinh E = a \sqrt{e^2 - 1} \sinh E. \\ r &= \sqrt{x'^2 + y'^2} = a(e \cosh E - 1) \end{aligned} \tag{9a}$$

Solution of the differential equations (1) yields p , a , and e as constants of the motion.

It is easily verified that

$$h = \sqrt{r_o^2 v_o^2 - (R_o \cdot v_o)^2} = r^2 \dot{\theta} \quad \text{angular momentum magnitude}$$

$$p = h^2/u \quad \text{semi-latus rectum}$$

$$a = \frac{r_o}{\left| 2 - \frac{r_o v_o^2}{u} \right|} \quad \text{semi-major axis}$$

$$e^2 = 1 - p/a \quad \text{eccentricity}$$

$$n = \sqrt{u/a^3} \quad \text{mean motion}$$

It should be observed that p is non-negative so that a negative semi-major axis corresponds to an eccentricity greater than one; that is, to the hyperbolic case. Some useful identities are listed as equations (11).

$$\frac{R \cdot V}{r} = \frac{d}{dt} (R \cdot R)^{1/2} = \dot{r} = \frac{ep\theta \sin\theta}{(1+e\cos\theta)^2} = \frac{ue}{h} \sin\theta$$

$$\cos\theta = \mp \frac{a}{r} (cE - e)$$

$$\sin\theta = \frac{a}{r} \sqrt{|e^2 - 1|} \quad sE = \sqrt{\frac{a}{u}} \frac{h}{r} \quad sE$$

$$esE = \frac{R \cdot V}{\sqrt{ua}}$$

$$ecE = 1 \pm \frac{r}{a} \quad (11)$$

The convention has been adopted that when a double sense sign \pm is used, the upper pertains to the hyperbolic case and the lower to the elliptical.

The symbols sE and cE mean $\sin E$ and $\cos E$ for the elliptical case, but $\sinh E$ and $\cosh E$ for the hyperbolic case. Hence, if we let

$\phi = E - E_0$, it follows that

$$s\phi = sEcE_0 - cEsE_0$$

$$c\phi = cEcE_0 + sEsE_0$$

and

$$sE = s\phi cE_0 + c\phi sE_0$$

$$cE = c\phi cE_0 + s\phi sE_0 \quad (12)$$

This angle, δ , of equation (5) is seen to represent the incremental true anomaly on the conic section containing R_0 and R . Thus, we can

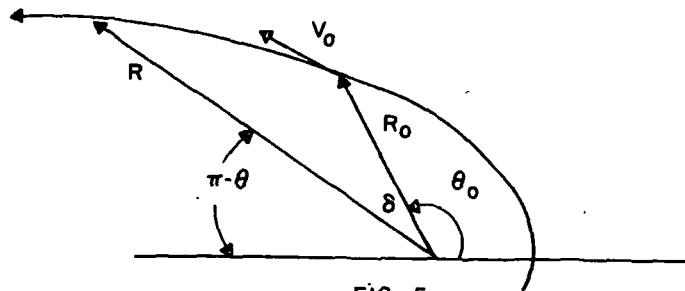


FIG. 5

find expressions for $\sin \delta$ and $\cos \delta$ in terms of θ and θ_0 .

$$\sin \delta = \sin (\theta - \theta_0) = \sin \theta \cos \theta_0 - \cos \theta \sin \theta_0$$

$$\cos \delta = \cos (\theta - \theta_0) = \cos \theta \cos \theta_0 + \sin \theta \sin \theta_0. \quad (13)$$

The incremental true anomaly may now be related to R_0 and V_0 through substitution of equations (11) and (12) into (13).

$$\begin{aligned}
\sin \delta &= \sin \theta \cos \theta_o - \cos \theta \sin \theta_o \\
&= \sqrt{\frac{a^3}{u}} \frac{h}{rr_o} (\bar{r} s E c E_o \pm e s E \bar{r} e s E_o \pm c E s E_o) \\
&= \frac{h}{n r r_o} (\bar{r} s \phi \pm e s E \bar{r} e s E_o) \\
&= \frac{h}{n r r_o} (\bar{r} s \phi \pm e c E_o s \phi \pm e s E_o c \phi \bar{r} e s E_o) \\
&= \frac{h}{n r r_o} \left(\frac{r_o}{a} s \phi \pm \frac{R_o \cdot V_o}{\sqrt{ua}} (c \phi - 1) \right)
\end{aligned}$$

$$\begin{aligned}
\cos \delta &= \cos \theta \cos \theta_o + \sin \theta \sin \theta_o \\
&= \frac{a^2}{r r_o} \left[c E c E_o - e c E - e c E_o + e^2 \pm (e^2 - 1) s E s E_o \right] \\
&= \frac{a^2}{r r_o} \left[c \phi - e c E - e c E_o + e^2 \pm e^2 s E s E_o \right] \\
&= \frac{a^2}{r r_o} \left[c \phi - e c \phi c E_o \bar{r} e s \phi s E_o - e c E_o + e^2 \pm e^2 s E_o c E_o s \phi \pm e^2 s^2 E_o c \phi \right] \\
&= \frac{a^2}{r r_o} \left[\bar{r} \frac{r_o}{a} c \phi + \frac{r_o}{a} \frac{R_o \cdot V_o}{\sqrt{ua}} s \phi + 1 \pm \frac{R_o \cdot V_o}{a} - 1 \bar{r} \frac{r_o}{a} \pm \frac{(R_o \cdot V_o)^2}{ua} c \phi \right] \\
&= \frac{a^2}{r r_o} \left[\bar{r} \frac{r_o}{a} (c \phi + 1) + \frac{r_o}{a} \frac{R_o \cdot V_o}{\sqrt{ua}} s \phi \pm \frac{r_o^2 v_o^2}{ua} \pm \frac{(R_o \cdot V_o)^2}{ua} (c \phi - 1) \right] \\
&= \frac{a^2}{r r_o} \left[\bar{r} \frac{r_o}{a} (c \phi - 1) + \frac{r_o}{a} \frac{R_o \cdot V_o}{\sqrt{ua}} s \phi + \frac{r_o}{a} \left(\frac{r_o v_o^2}{u} - 2 \right) \right. \\
&\quad \left. \pm \frac{(R_o \cdot V_o)^2}{ua} (c \phi - 1) \right] \\
&= \frac{a^2}{r r_o} \left[\bar{r} \left[\frac{(R_o \cdot V_o)^2}{ua} - \frac{r_o}{a} \right] (c \phi - 1) + \frac{r_o}{a} \frac{R_o \cdot V_o}{\sqrt{ua}} s \phi + \frac{r_o^2}{a^2} \right]
\end{aligned}$$

The coefficients, f and g , of equation (6) are finally found to be:

$$\begin{aligned}
 f &= \frac{r}{r_o} \left(\cos \delta - \frac{R_o \cdot V_o}{h} \sin \delta \right) \\
 &= \frac{a^2}{r_o^2} \left[+ \left[\frac{(R_o \cdot V_o)^2}{ua} - \frac{r_o}{a} - \frac{(R_o \cdot V_o)^2}{ua} \right] (c\phi - 1) + \frac{r_o}{a} \left[\frac{R_o \cdot V_o}{\sqrt{ua}} - \frac{R_o \cdot V_o}{\sqrt{ua}} \right] s\phi \right. \\
 &\quad \left. + \frac{r_o^2}{a^2} \right] = \mp \frac{a}{r_o} (c\phi - 1) + 1 \tag{14}
 \end{aligned}$$

$$\begin{aligned}
 g &= \frac{rr_o}{h} \sin \delta \\
 &= \frac{1}{n} \frac{r_o}{a} s\phi + \frac{R_o \cdot V_o}{\sqrt{ua}} (c\phi - 1) \tag{15}
 \end{aligned}$$

The velocity coefficients, \dot{f} and \dot{g} , are found by noting that

$$\dot{\phi} = \dot{E} = \sqrt{\frac{u}{a}} \frac{1}{r}$$

$$\text{and therefore } \dot{f} = \mp \frac{a}{r_o} \frac{d}{dt} (c\phi) = - \frac{a}{r_o} \dot{E} s\phi = - \frac{\sqrt{ua}}{rr_o} s\phi \tag{16}$$

$$\begin{aligned}
 \dot{g} &= \frac{\dot{E}}{n} \left(\frac{r_o}{a} c\phi + \frac{R_o \cdot V_o}{\sqrt{ua}} s\phi \right) \\
 &= \frac{a}{r} \left(\frac{r_o}{a} c\phi + \frac{R_o \cdot V_o}{\sqrt{ua}} s\phi \right) \tag{17}
 \end{aligned}$$

where

$$\begin{aligned}
 \frac{r}{a} &= \mp (1 - ecE) = \mp (1 - ec\phi cE_o \mp es\phi sE_o) \\
 &= \mp \left(1 - c\phi \left(1 \pm \frac{r_o}{a} \right) \mp s\phi \frac{R_o \cdot V_o}{\sqrt{ua}} \right) \\
 &= \pm (c\phi - 1) + \frac{r_o}{a} c\phi + \frac{R_o \cdot V_o}{\sqrt{ua}} s\phi \tag{18}
 \end{aligned}$$

Kepler's equation presents the incremental time, t , in terms of Φ

$$\begin{aligned}
 nt &= \bar{\tau} (E - esE) \pm (E_0 - esE_0) \\
 &= \bar{\tau} (\Phi - esE + esE_0) \\
 &= \bar{\tau} (\Phi - es\Phi cE_0 - ec\Phi sE_0 + esE_0) \\
 &= \bar{\tau} \left[\Phi - s\Phi \left(1 \pm \frac{r_0}{a} \right) - (c\Phi - 1) \frac{R_0 \cdot V_0}{\sqrt{ua}} \right] \\
 &= \bar{\tau} (\Phi - s\Phi) + \frac{r_0}{a} s\Phi \pm \frac{R_0 \cdot V_0}{\sqrt{ua}} (c\Phi - 1) \tag{19}
 \end{aligned}$$

In order to solve equation (19) for Φ as a function of R_0 , V_0 and t , an iterative method is required. Any solution obtained is necessarily unique, since the right side of (19) is seen to be monotonically increasing for all Φ .

Equation (19) may be used to simplify equations (15) and (17).

$$\begin{aligned}
 g &= \frac{1}{n} \left[\frac{r_0}{a} s\Phi + nt \pm (\Phi - s\Phi) - \frac{r_0}{a} s\Phi \right] \\
 &= t \pm \frac{1}{n} (\Phi - s\Phi) \tag{15a}
 \end{aligned}$$

$$\begin{aligned}
 \dot{g} &= 1 \pm \frac{\dot{E}}{n} (1 - c\Phi) \\
 &= 1 \mp \sqrt{\frac{u}{a}} \frac{1}{nr} (c\Phi - 1) \\
 &= 1 \mp \frac{a}{r} (c\Phi - 1) \tag{17a}
 \end{aligned}$$

Subroutine Description

The subroutine will calculate

$$(1) R = R(R_o, V_o, t)$$

$$V = V(R_o, V_o, t)$$

$$\delta = \delta(R_o, V_o, t)$$

The first time STEP is called with a given R_o and V_o ($N=1$), those coefficients which are dependent only on R_o and V_o are calculated. Thereafter, these coefficients are considered to be constants with respect to t .

<u>Calculation</u>	<u>FORTAN Name</u>
$r_o = \sqrt{R_o \cdot R_o}$	RM
$v_o = \sqrt{V_o \cdot V_o}$	VM
$a = \frac{r_o}{\left 2 - \frac{r_o v_o^2}{u} \right }$	A
$n = \frac{1}{a} \sqrt{\frac{u}{a}}$	RAT
$R_o \cdot V_o = R_o \cdot V_o$	RV
$h = \sqrt{r_o^2 v_o^2 - (R_o \cdot V_o)^2}$	H

STEPC calls Subroutine GOTOR to solve equation (19),

$$nt = \bar{r} (\bar{\phi} - s\bar{\phi}) + \frac{r_o}{a} s\bar{\phi} + \frac{R_o \cdot V_o}{\sqrt{ua}} (c\bar{\phi} - 1) \text{ for } \bar{\phi}.$$

GOTOR returns a vector F where

	<u>Elliptical</u>	<u>Hyperbolic</u>
F(1) =	$\bar{\phi} - \sin \bar{\phi}$	$\sinh \bar{\phi} - \bar{\phi}$
F(2) =	$1 - \cos \bar{\phi}$	$\cosh \bar{\phi} - 1$
F(3) =	$\sin \bar{\phi}$	$\sinh \bar{\phi}$
F(4) =	$\cos \bar{\phi}$	$\cosh \bar{\phi}$

The coefficients, f, g, \dot{f} and \dot{g} , are then calculated.

<u>Calculation</u>	<u>FORTTRAN Name</u>
$f = -\frac{r_o}{a} F(2) + 1$	EF
$g = -\frac{F(1)}{n} + t$	GE
$\frac{r}{a} = F(2) + \frac{r_o}{a} F(4) + \frac{R_o \cdot V_o}{\sqrt{ua}} F(3)$	ROA
$\dot{f} = -anF(3) / \frac{(r_o r)}{a}$	EFD
$\dot{g} = -\frac{a}{r} F(2) + 1$	GED
$\delta = \tan^{-1} \frac{hg}{f_o^2 f + R_o \cdot V_o g}$	TA
$R = fR_o + gV_o$	RR
$V = \dot{f}R_o + \dot{g}V_o$	VV

Reference: NASA X-640-63-71, ITEM Program Manual, Goddard Space Flight Center, Greenbelt, Maryland.

LABEL	STPC
* SYMBOL TABLE	STPC
CEC2023 SUBROUTINE STEPC	STPC
SUBROUTINE STEPC(N,T,R,V,U,RR,VV)	STPC000
DIMENSION R(3),V(3),RR(3),VV(3),C(2),F(4)	STPC001
GO TO (1,2),N	STPC002
1 CONTINUE	STPC003
PI=3.141592654	STPC004
R2=DOT(R,R)	STPC005
RM=SQRTF(R2)	STPC006
V2=DOT(V,V)	STPC007
RV=DOT(R,V)	STPC008
VM=SQRTF(V2)	STPC009
A=RM/(2.-RM*V2/U)	STPC010
ABA=ABSF(A)	STPC011
RAT=SQRTF(U/ABA)/ABA	STPC012
C(1)=RM/ABA	STPC013
C(2)=RV/SQRTF(U+ABA)	STPC014
IF(A)3,3,4	STPC015
4 CONTINUE	STPC016
K=1	STPC017
E1=RAT*T	STPC018
GO TO 15	STPC019
3 CONTINUE	STPC020
K=2	STPC021
E1=0.	STPC022
15 CONTINUE	STPC023
2 CONTINUE	STPC024
T IS THE INCREMENTAL TIME IN ORBIT	STPC025
EMDT=RAT*T	STPC026
CALL GOTOR(K,EMDT,C,F,E1)	STPC027
EF=-F(2)/C(1)+1.	STPC028
GE=-F(1)/RAT*T	STPC029
TA=ARKTNS(360,R2*EF+RV*GE,H*GE)	STPC030
ROA=F(2)+C(1)*F(4)+C(2)*F(3)	STPC031
EFD=-ABA*RAT*F(3)/(RM*ROA)	STPC032
GED=-F(2)/ROA+1.	STPC033
8 CONTINUE	STPC034
DO 10 I=1,3	STPC035
RR(I)=EF*R(I)+GE*V(I)	STPC036
VV(I)=EFD*R(I)+GED*V(I)	STPC037
10 CONTINUE	STPC038
RETURN	STPC039
END	STPC

Page Intentionally Left Blank

Subroutine: TIMEC

Purpose: To compute whole days and fractional days since January 1, 1950, from calendar date input. This input is in the form (Years from 1900) $\times 10^2 +$ (Month of Year) + (Day of Month) $\times 10^{-2}$, and (Hour of Day) $\times 10^2 +$ (Minutes of Hour) + (Seconds of Minute) $\times 10^{-2}$. [See examples under input description]. The input date must be 1961 or later.

Calling Sequence:

CALL TIMEC (T1, T2, T3, T4)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	T1	1			Year, month, day. Jan. 12, 1965 = 6501.12.
I	T2	1			Hour, minutes, seconds. 1 PM, 1 min, 30.3 sec = 1301.303
O	T3	1		days	Whole number of days since 1950.
O	T4	1		days	Fractional number of days past T3.

Common storages used or required:

None

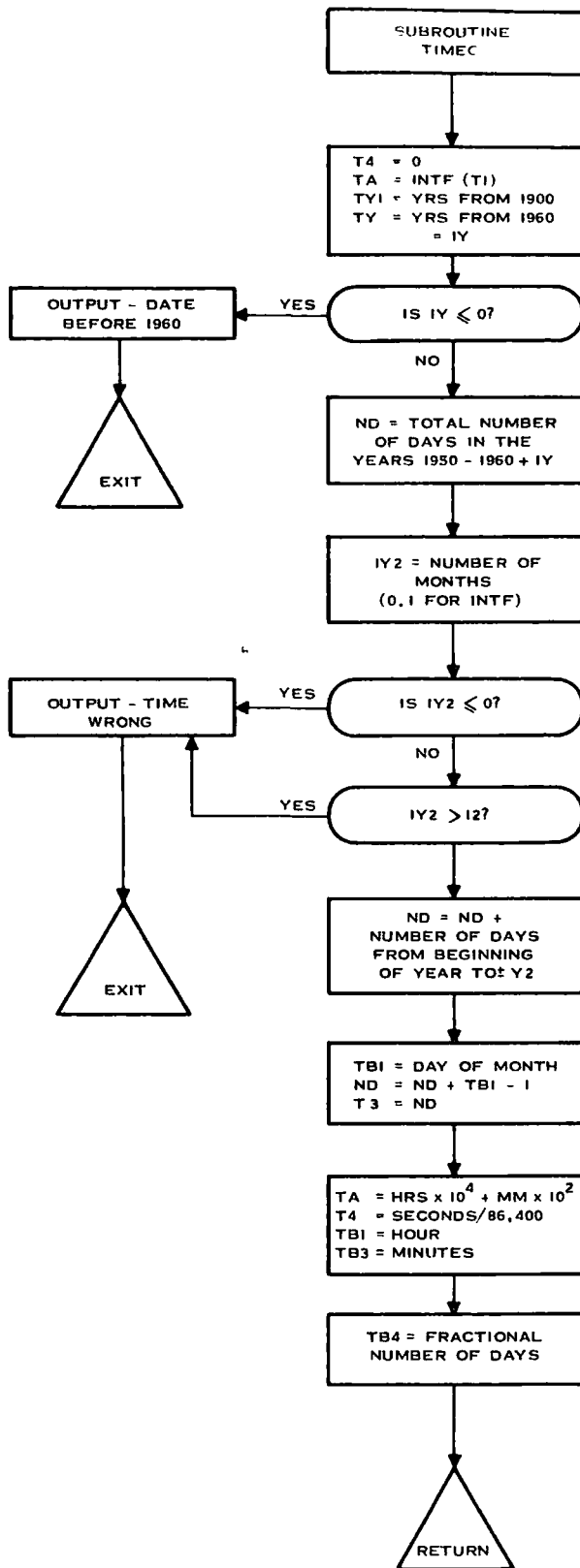
Subroutines required:

EXIT

Functions required:

INTF

Approximate number of storages required:



```

* LABEL
* SYMBOL TABLE
SUBROUTINE TIMEC(T1,T2,T3,T4)
T1 IS AN INPUT IN FORM (YEARS FROM 1900)(MONTH OF YEAR)
(DAY OF MONTH
WRITTEN AS 6501,12 FOR JAN. 12, 1965
T2 IS AN INPUT IN FORM (HOUR OF DAY)(MINUTE OF HOUR)
(SECOND OF MINUTE)
WRITTEN AS 1301,3032 FOR 1PM, 1 MINUTE, 30.32 SECOND
T3 IS WHOLE DAYS FROM 1950 OUTPUT
CALL SETN(NIN,NOUT)
T4=0.
TA=INTF(T1)
TA1=TA/100.+.01
TY1=INTF(TA1)
TY=TY1-60.
IY=TY
IF (IY) 15,15,16
15 CONTINUE
WRITE OUTPUT TAPE NOUT,17
17 FORMAT (37H EXIT FROM TIMEC. DATE 1960 OR BEFORE)
CALL EXIT
16 CONTINUE
ND=3652
K=1
DO 1 I=1, IY
KK=K-I
IF (KK) 2,2,3
2 CONTINUE
ND=ND + 366
K=K+4
GO TO 1
3 CONTINUE
ND=ND +365
1 CONTINUE
TY2=TA-TY1*100.+.1
IY2=INTF(TY2)
IF (IY2) 10,10,11
11 CONTINUE
IF (12-IY2) 10,12,12
10 CONTINUE
WRITE OUTPUT TAPE NOUT,13
13 FORMAT(37H INPUT TIME IS WRONG. EXIT FROM TIMEC)
CALL EXIT
12 CONTINUE
DO 4 I=1,IY2
I=I
JAN FEB MAR APRIL MAY JUNE JULY AUG SEPT OCT NOV
GO TO (4,6,7,6,8,6,8,6,6,8,6,8),I
6 CONTINUE
ND=ND + 31

```

```

TIMC
TIMC
TIMC000
TIMC001
TIMC002
TIMC003
TIMC004
TIMC005
TIMC006
TIMC007
TIMC007
TIMC008
TIMC009
TIMC010
TIMC011
TIMC012
TIMC013
TIMC014
TIMC015
TIMC016
TIMC017
TIMC018
TIMC019
TIMC020
TIMC021
TIMC022
TIMC023
TIMC024
TIMC025
TIMC026
TIMC027
TIMC028
TIMC029
TIMC030
TIMC031
TIMC032
TIMC033
TIMC034
TIMC035
TIMC036
TIMC037
TIMC038
TIMC039
TIMC040
TIMC041
TIMC042
TIMC043
TIMC044
TIMC045
TIMC046
TIMC047

```

```

GO TO 4
7 CONTINUE
IF (KK-1) 9, 14, 9
14 CONTINUE
ND=ND +29
GO TO 4
9 CONTINUE
ND=ND +28
GO TO 4
8 CONTINUE
ND=ND +30
4 CONTINUE
TB1=(T1-TA)*100.+.1
ND=ND +XINTF(TB1)
ND=ND-1
T3=ND
TA=INTF(T2)
T4=(T2-TA)/864.
TB=TA/100.+.1
TB1=INTF(TB)
TB2=TA-TR1*100.+.1
TB3= INTF(TB2)
T4=T4+TB1/24.+TB3/24./60.
RETURN
END

```

```

TIMC0480
TIMC0490
TIMC0500
TIMC0510
TIMC0520
TIMC0530
TIMC0540
TIMC0550
TIMC0560
TIMC0570
TIMC0580
TIMC0590
TIMC0600
TIMC0610
TIMC0620
TIMC0630
TIMC0640
TIMC0650
TIMC0660
TIMC0670
TIMC0680
TIMC0690
TIMC0700
TIMC0710
TIMC

```


Subroutine: TIMED

Purpose: To convert an input time from the format DAYS HOURS·MIN SEC to seconds. If the input is negative, it is assumed to be in seconds, and returned positive.

Calling Sequence:

CALL TIMED (T1, T2)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	T1	1		-seconds	or (DAYS + 10 ² + HOURS + MIN x 10 ⁻² + SEC x 10 ⁻⁴)
O	T2	1		seconds	

Common storages used or required: None

Subroutines required: None

Functions required: INTF

Approximate number of storages required:

TIMED

WDL-TR2

*	LABEL	TIMD
*	SYMBOL TABLE	TIMD
	SUBROUTINE TIMED (T1,T2)	TIMD0000
	IF(T1)1,1,2	TIMD0010
1	CONTINUE	TIMD0020
	T2=-T1	TIMD0030
	RETURN	TIMD0040
C	SUBROUTINE ACCEPTS T1 IN SEC IF THE SIGN IS INPUT NEGATIVE AND	TIMD0050
C	GIVES T2 IN + SEC IF T1 IS + AND ARRANGED AS (DAYS HOURS.MIN SEC)	TIMD0060
C	IT CONVERTS OUTPUT T2 TO SEC	TIMD0070
2	CONTINUE	TIMD0080
	TDH=INTF(T1)	TIMD0090
	TMS=T1-TDH	TIMD0100
	TM1=TMS+100,+.01	TIMD0110
	TM=INTF(TM1)	TIMD0120
	TS=(TMS*100,-TM)*100,+.01	TIMD0130
	TD=INTF(TDH/100,+.01)	TIMD0140
	TH=TDH-TD*100,+.01	TIMD0150
	TH=INTF(TH)	TIMD0160
	TS=INTF(TS)	TIMD0170
	T2=TD*86400, +TH*3600, +TM*60, +TS	TIMD0180
	RETURN	TIMD0190
	END	TIMD

Subroutine: TRAC

Purpose: To obtain the vector from a body center to a tracking station and the unit up, east, and north vectors. The coordinate system is a rotating body fixed system. The body may be treated as an oblate spheroid.

Calling Sequence:

CALL TRAC (TO, AT, H, GHA, U, E, EN, RT, AC, SL, CL, ST, CT, A, B)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	TO	1		RAD	Tracker longitude
I	AT	1		RAD	Tracker latitude
I	H	1		Km	Tracker Altitude
I	GHA	1		RAD	Greenwich hour angle
O	U	3	\hat{U}		Up unit vector
O	E	3	\hat{E}		East unit vector
O	EN	3	\hat{N}		North unit vector
O	RT	3			Radius vector to tracker

(Cont'd.)

Common storages used or required: None

Subroutines required: None

Functions required: SIN, COS, SORT

Approximate number of storages required: 194 DEC

(Cont 'd.)

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
O	AC	1			Constant used in program
O	SL	1			Sin LAT
O	CL	1			Cos LAT
O	ST	1			Sin LONG
O	CT	1			Cos LONG
I	A	1	R_E	Km	Body's equatorial radius
I	B	1	R_p	Km	Body's polar radius

Derivation of Vectors obtained in TRAC

A. Derivation of Unit U, E, and N

The coordinate system of concern is shown in Fig. 1 below.

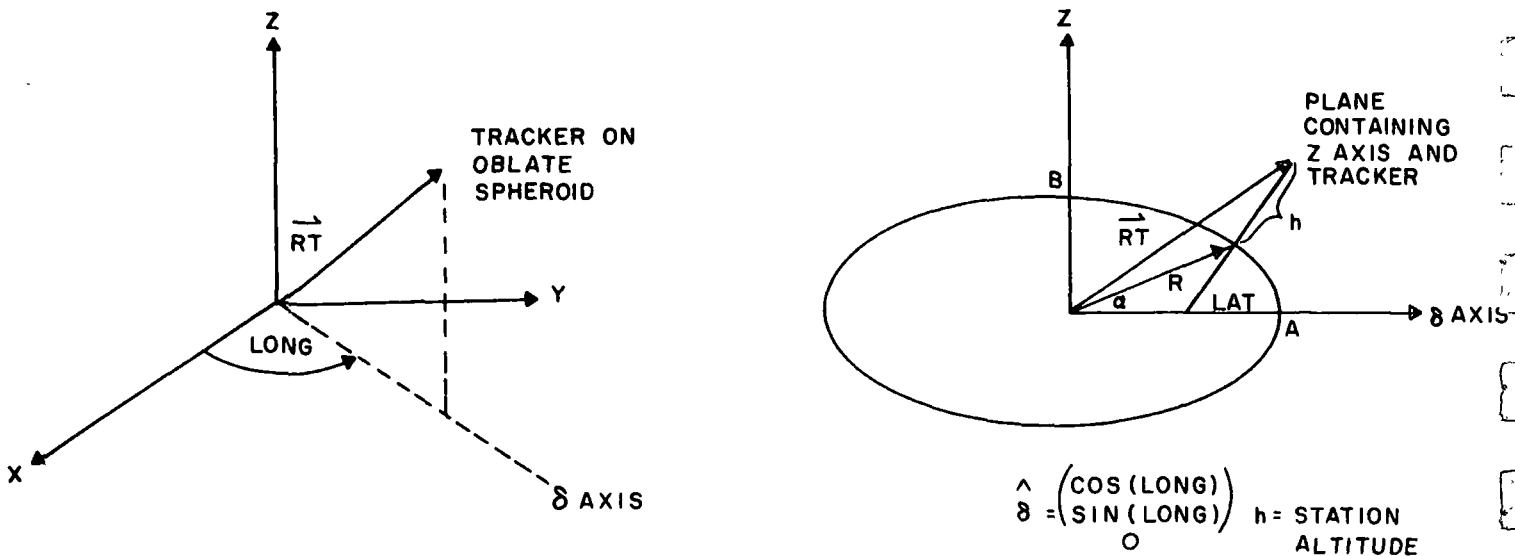


FIG 1

The unit up vector, U, may be written as:

$$\hat{U} = \begin{pmatrix} \cos(\text{LAT}) \cos(\text{LONG}) \\ \cos(\text{LAT}) \sin(\text{LONG}) \\ \sin(\text{LAT}) \end{pmatrix}$$

The unit east vector, E, is:

$$\hat{E} = \frac{\hat{K} \times \hat{U}}{|\hat{K} \times \hat{U}|} = \begin{pmatrix} -\sin(\text{LONG}) \\ \cos(\text{LONG}) \\ 0 \end{pmatrix}$$

The unit north vector, N, is:

$$\hat{N} = \hat{U} \times \hat{E} = \begin{pmatrix} -\sin(\text{LAT}) \cos(\text{LONG}) \\ -\sin(\text{LAT}) \sin(\text{LONG}) \\ \cos(\text{LAT}) \end{pmatrix}$$

B. Derivation of Radius Vector, RT, to Tracker.

$$\vec{RT} = \vec{R} + h \hat{U}$$

$$\vec{R} = |R| \cos \alpha \begin{pmatrix} \cos(\text{LONG}) \\ \sin(\text{LONG}) \\ 0 \end{pmatrix} + |R| \sin \alpha \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}$$

Equation of ellipse in Z- δ plane

$$\frac{Z^2}{B^2} + \frac{\delta^2}{A^2} = 1$$

Substituting for Z, δ

$$R^2 \left(\frac{\sin^2 \alpha}{B^2} + \frac{\cos^2 \alpha}{A^2} \right) = 1$$

$$\frac{dZ}{d\delta} = -\frac{B^2}{A^2} \frac{\delta}{Z}$$

$$\tan(\text{LAT}) = \frac{A^2}{B^2} \frac{Z}{\delta}$$

$$\tan \alpha = \frac{Z}{\delta}$$

$$R = \frac{AB}{(A^2 \sin^2 \alpha + B^2 \cos^2 \alpha)^{1/2}} \quad \therefore \tan \alpha = \frac{B^2}{A^2} \tan(\text{LAT})$$

$$R \cos \alpha = \frac{A}{\left(\frac{A^2}{B^2} \tan^2 \alpha + 1\right)^{1/2}} \quad R \sin \alpha = \frac{B}{\left(1 + \frac{B^2}{A^2} \cot^2 \alpha\right)^{1/2}}$$

Substituting for $\tan \alpha$ yields

$$R \cos \alpha = \frac{A}{\left(\frac{B^2}{A^2} \tan^2(\text{LAT}) + 1\right)^{1/2}} \quad R \sin \alpha = \frac{B}{\left(1 + \frac{A^2}{B^2} \cot^2(\text{LAT})\right)^{1/2}}$$

$$\text{RT}(1) = \left\{ \frac{A}{\left[\frac{B^2}{A^2} \sin^2(\text{LAT}) + \cos^2(\text{LAT})\right]^{1/2}} + h \right\} U(1)$$

$$\text{RT}(2) = \left\{ \frac{A}{\left[\frac{B^2}{A^2} \sin^2(\text{LAT}) + \cos^2(\text{LAT})\right]^{1/2}} + h \right\} U(2)$$

$$\text{RT}(3) = \left\{ \frac{B^2}{\left[B^2 \sin^2(\text{LAT}) + A^2 \cos^2(\text{LAT})\right]^{1/2}} + h \right\} U(3)$$



* LABEL	TRAC
* SYMBOL TABLE	TRAC
CEC2009	TRAC
SUBROUTINE TRAC (TO,AT,H,GHA,U,E,EN,RT,AC,SL,CL,ST,CT,A,B)	TRAC0000
DIMENSION RT(3),U(3),E(3),EN(3)	TRAC0010
C TO AND LAT MUST BE INPUTED IN RAD,H IS ALTITUDE IN KM	TRAC0020
SL=SINF(AT)	TRAC0030
CL=COSE(AT)	TRAC0040
TA=TO+GHA	TRAC0050
C GHA IS GREENWICH HOUR ANGLE,U IS 'UP,E IS EAST,	TRAC0060
C EN IS NORTH UNIT VECTORS	TRAC0070
ST = SINF(TA)	TRAC0080
CT = COSE(TA)	TRAC0090
C = SQRTF(CL*CL+B*B*SL*SL/(A*A))	TRAC0100
AC=A/C	TRAC0110
U(1) = CL*CT	TRAC0120
U(2) = CL*ST	TRAC0130
U(3) = SL	TRAC0140
RT(1) = (A/C+H)*U(1)	TRAC0150
RT(2) = (A/C+H)*U(2)	TRAC0160
RT(3) = (B*B/(A*C)+H)*U(3)	TRAC0170
4 E(1) = -ST	TRAC0180
E(2) = CT	TRAC0190
E(3) = 0.	TRAC0200
EN(1) = -SL*CT	TRAC0210
EN(2) = -SL*ST	TRAC0220
EN(3) = CL	TRAC0230
RETURN	TRAC0240
END	TRAC

Page Intentionally Left Blank

TRANSH

WDL-TR 4

```
* LABEL
* SYMBOL TABLE
SUBROUTINE TRANSH(H,LL)
C SUBROUTINE TRANSFORMS H MATRIX TO EQUINOX 1950
EQUIVALENCE(T,TDUM),(S,SDUM),(C,CDUM),(C(138),AN)
DIMENSION H(6),AN(3,3),DUM(1,6),T(1360),S(1000),C(1000),IC(1)
COMMON T,S,C,IC
LL=LL
DO 1 I=1,3
K=I+3
DUM(I)=0.
DUM(K)=0.
DO 1 J=1,3
DUM(I)=DUM(I)+AN(J,I)*H(J)
GO TO(1,2),LL
2 CONTINUE
L=J+3
DUM(K)=DUM(K)+AN(J,I)*H(L)
1 CONTINUE
DO 3 I=1,6
H(I)=DUM(I)
3 CONTINUE
RETURN
END
```

TRAN
TRAN
TRAN000
TRAN001
TRAN0020
TRAN003
TRAN004
TRAN0050
TRAN0060
TRAN007
TRAN008
TRAN0090
TRAN010
TRAN011
TRAN0120
TRAN013
TRAN014
TRAN0150
TRAN0160
TRAN017
TRAN018
TRAN0190
TRAN020
TRAN

DISTRIBUTION LIST

<u>Address</u>	<u>Number of Copies</u>
National Aeronautics and Space Administration Goddard Space Flight Center Greenbelt, Maryland Attn: Dr. F. O. Vonbun	30
Philco Corporation WDL Division Palo Alto, California	70
	100