

Technical Report TR-65-24 October, 1965

Subroutines for Digital Computation
of Chemical Engineering Problems*

Part I

by

Chan M. Park

* This work was supported by National Aeronautics and Space Administration Grant NSG-398 to the Computer Science Center, University of Maryland, College Park, Maryland.

CONTENTS

	Page
I. INTRODUCTION	1
II. DESCRIPTION OF ROUTINES.	2
A. Non-Mathematical Routines.	2
1) Unit Conversion Routine (CONVRT)	2
2) Log-log Plot Routine (LNPLT)	5
B. Mathematical Routines.	7
1) Lagrangian Interpolation Routine (LAGINT)	7
2) Gauss Elimination Routine (GAUSS)	8
3) Least-Squares Fit Routine (LEASQ)	9
4) Matrix Multiplication Routine (MATMPY)	9
5) Matrix Inversion Routine (MATINV)	10
6) Numerical Integration Routine by Simpson's Method (SIMPSN)	11
7) Modified Runge-Kutta Method Routine (RUNMOD)	12
APPENDIX 1. LISTING OF SUBROUTINE PROGRAMS	15
Disclaimer	16
Abbreviations Used for the Units (Table)	17
Subroutine CONVRT.	19
Subroutine LNPLT.	39
Subroutine LAGINT.	42
Subroutine GAUSS	44
Subroutine LEASQ.	45
Subroutine MATMPY.	46
Subroutine MATINV.	47
Subroutine SIMPSN.	48
Subroutine RUNMOD.	49
APPENDIX 2. LISTING OF CONTROL PROGRAMS AND NUMERICAL RESULTS.	50
CCNVRT (Case 1)	51
CCNVRT (Case 2)	53
CLNPLT	55
CLAGIN	57
CGAUSS	59
CLEASQ	61
CMTMPY	63
CMTINV	65
CSMPSN	67
CRUNMO	69
References.	74

I. INTRODUCTION

This report contains a collection of subroutine programs developed for chemical engineers and chemical engineering students to aid in the solution of their problems. Rather than developing all-purpose general routines with many options which often make them difficult to use, these subroutines were developed with emphasis on practical applicability in the chemical engineering field and organized to make them usable with a minimum of effort.

The subroutines described in this paper are basic and are frequently required in the reduction of experimental data to usable form as well as in the solution of computer-oriented chemical engineering problems. Both FORTRAN II and FORTRAN IV versions are provided so that a user can choose according to his control program. Control programs as well as numerical results are also included for each subroutine to illustrate its usage. Since there are only small differences between the programs in FORTRAN II and FORTRAN IV, only FORTRAN II program listings are given in the Appendices at the end of this report.

Some of the restrictions involved in the subroutines, such as dimension statements, may be easily removed by modifying the source deck. Both source and binary decks are available from the author.

Additional routines dealing with mathematical equations such as ordinary and partial differential equations, as well as some specific programs for solving complex chemical engineering problems such as kinetics, diffusion and unsteady-state transport phenomena, are presently being developed and will be the subject of Part II of this report.

A word of caution: The maximum number of elements in a two- or three-array variable specified in a dimension statement of a control program should be the same as that in a subroutine which is called by the control program. The user must therefore be careful when working with two- or three-dimensional variables.

II. DESCRIPTION OF ROUTINES

The routines are divided into two classes. The first class consists of non-mathematical routines which are useful in the treatment of chemical engineering problems. The second class consists of mathematical subroutines which are frequently employed in the solution of the problems. The theoretical and procedural aspects of the mathematical routines are described in standard works on numerical analysis such as those listed as references at the end of this report. Control programs have been used to illustrate practical applications of the subroutines in each case.

A. Non-Mathematical Routines

1) Unit Conversion Routine (Subroutine CONVRT)

Conversions of complex units from one scale to another are very often necessary in the solution of chemical engineering problems. For example, if a chemical engineer wants to use thermal conductivity data obtained by a physicist who often chooses Kcal/sec-cm-°C as its unit, he may want to convert the unit into Btu/hr-ft²/in-°F. Although it is not difficult to convert one unit into another, usually it takes time and effort, and there is the possibility of introducing errors. This routine has been written to make it possible to perform conversions with greater speed and accuracy than by manual methods. The routine is especially effective if the entire problem is being solved by the computer, as will be the case in most instances. CONVRT has been developed in such a way that any additional units required can be easily added. Most of the practical units employed by a chemical engineer are already included in the routine.

The calling sequence of the routine is

CALL CONVRT (N, A, B, FACTOR)

where

N = a zero or an integer number

A = original unit

B = desired unit

FACTOR = conversion factor

There are two ways of introducing the units into the machine, one as Hollerith arguments of the subroutine and the other as input data to the machine. The arguments N, A, and B will have somewhat different features depending upon the above two cases,

as shown in the following example.

Let us consider the conversion of $\text{KCAL}/(\text{SEC} \cdot \text{CM} \cdot \text{DEGC})$ into $\text{BTU}/(\text{HR} \cdot (\text{FT}^2/\text{INCH}) \cdot \text{DEGF})$.

a) If these units are introduced as Hollerith arguments, the calling sequence will have the form

```
CALL CONVRT (0, 19HbKCAL/(SEC*CM*DEGC),
              27HbBTU/(HR*(FT**2/INCH)*DEGF), FACTOR)
```

Hence $N = 0$

```
A = 19HbKCAL/(SEC*CM*DEGC)
B = 27HbBTU/(HR*(FT**2/INCH)*DEGF)
```

(b means a blank space)

In this case, N should have the value zero because this is an index to tell the machine that the units are introduced as Hollerith arguments. The numbers (19 and 27) in front of the units are the numbers of characters (including blank spaces) following the letter H, which stands for Hollerith field.

Some additional examples:

i) conversion of lb/gal into Kg/m^3

```
CALL CONVRT (0, 7H LB/GAL, 10H KG/(M**3), FACTOR)
```

ii) conversion of centipoise into lb/ft-sec

```
CALL CONVRT (0, 3H CP, 12H LB/(FT*SEC), FACTOR)
```

b) If the units are introduced as input data to the machine, the calling sequence is

```
CALL CONVRT (N, UNIT1, UNIT2, FACTOR)
```

where UNIT 1 and UNIT2 correspond to A and B, respectively. In this case UNIT1 and UNIT2 are variables with one-dimensional subscripts, and the following statements should be included in the control program before the subroutine CONVRT is called. (The following example is in FORTRAN II.)

```

        DIMENSION UNIT1(24), UNIT2(24)
        N = 12 (or 24, see below)
        READ INPUT TAPE 5, 1, (UNIT1(I), I = 1,N)
        READ INPUT TAPE 5, 1, (UNIT2(I), I = 1,N)
1  FORMAT(12A6)

        .....
        .....
        CALL CONVRT (N, UNIT1, UNIT2, FACTOR)
        .....
        .....

        END
*      DATA
        KCAL/(SEC*CM*DEGC)
        BTU/(HR*(FT**2/INCH)*DEGF)

```

The units, both original and desired, are punched on the separate cards as input data. If any one of the units has more than 72 characters (which means that one card is not enough for that unit), the value of N should be 24 and two cards should be given as data for each unit. If one of the units has less than 72 characters while the other has more than 72, then the former should have a blank card immediately following the data card to make two data cards. If a unit requires more than two cards, the dimension statement should be changed to increase the storage, and N may then be increased to read in more than two cards.

Notes:

- a) Whenever feasible, conventional abbreviations such as BTU, KG, etc. were used in the program. However, users are urged to check the list of abbreviations provided in front of the subroutine CONVRT before using it.
- b) The formation of a complex unit is very simple; it is similar to writing an arithmetic expression in FORTRAN. Some rules are:
 - (i) Parentheses may be used anywhere in the complex unit, so as to perform the computation of that part of the unit first, except in front of an exponentiation operator (**). This is not a serious restriction since in practice an exponential operation is performed on a simple unit (e.g. cm^2 , ft^3 , sec^2 , etc.) rather than on a compound unit in the formation of a complex unit.
 - (ii) The multiplication symbol (*) is used between simple units (e.g. SEC*CM*DEGC for sec-cm-°C) to separate them. (Actually, the simple units are multiplied to form the complex unit, even though the (-) symbol is used in the conventional expression.)

- (iii) Squares and cubes are expressed using the exponentiation operator (e.g. CM**2 for cm², and FT**3 for cubic foot).
- (iv) The exponent should be an integer whose value is less than 8. (Only 2 and 3 are used in most cases.)
- (v) No addition (+) or subtraction (-) symbols may be used.
- c) It should be noted that this routine computes a conversion factor from one unit to another. For example, it will give 1.8 as the conversion factor from °C into °F. However, the routine will not convert a temperature of 100°C into Fahrenheit temperature unless the appropriate equation is provided after the routine CONVRT is called. In this case the appropriate equation is:

$$FTEMP = 100. * FACTOR + 32.$$
- d) When an error is detected in the formation of a complex unit, an error message will be printed out, and the computation will stop.
- e) There are ten subprograms associated with subroutine CONVRT. Their names and functions are:
 - SEPCOMCalled by CONVRT. Separate a complex unit into simple units and operators and compute a characteristic number for the complex unit.
 - GETNOCalled by SEPCOM. Search the table of simple units and get a characteristic number for a simple unit separated from the complex unit.
 - ERROR1
throughCalled by SEPCOM. Write error messages
ERROR7 if there are any errors in the formation of a complex unit.
 - WRITE1Called by GETNO. Write an error message when a given simple unit is not found in the table of simple units.

Control Program (CCNVRT)

Two control programs are given in Appendix 2 to illustrate the two cases described above. In the first case, the factor for a conversion from Btu/sec into ft-lb/sec is computed. The second control program finds the conversion factor for a conversion from centipoise into lb/(ft-hr).

2) Log-log Plot Routine (Subroutine LNPLLOT)

A plot of experimental data or computed results on a log-log scale is often desired by a chemical engineer. A preliminary

analysis usually does not require a very fine curve, yet it takes considerable time and effort if large amounts of data are being treated. This log-log plot routine was written to free the researcher from the drudgery of a manual plot.

The calling sequence is

```
CALL LINPLOT (N, X, Y, SYMBOL)
```

where

N = number of points

X = array of abscissa values

Y = array of ordinate values

SYMBOL = a character to be used in the plot

The points do not have to be in any order. (In other words, the X-coordinates of the points need not be in an ascending or a descending order.)

SYMBOL is a character which is defined before the routine is called. The most frequently used are "*", and "+", although any character such as "A", "l", etc. may be used. The definition of SYMBOL will have the form

SYMBOL = 1H*

SYMBOL = 1H+ etc.

in a FORTRAN II program. An alternative calling sequence in FORTRAN II is to define the symbol as an argument of the sub-routine, e.g. CALL LNPLT (N, X, Y, 1H*). In a FORTRAN IV program, SYMBOL will be defined with a DATA statement.

Notes:

a) Limitation: $N \leq 200$

b) Dimensioned variables: X(200), Y(200)

Control Program (CLNPLT)

The sample problem considered here is that of plotting a curve of dispersion group vs. Reynolds number in a straight pipe, as compiled by Levenspiel (Industrial and Engineering Chemistry vol. 50, p. 343, 1958).

The equation used to compute the dispersion group for a Reynolds number less than 20,000 was obtained by the author by applying the least-squares fit method to the curve presented by Levenspiel.

$$\ln\left(\frac{D}{u d_t}\right) = 0.63082532 (\ln(N_{Re}))^2 - 12.5531745 (\ln(N_{Re})) + 61.25958824 \quad \text{for } N_{Re} \leq 20,000$$

The dispersion group for a Reynolds number greater than 20,000

was computed by use of the theoretical equation derived by Taylor.

$$\frac{D}{u d_t} = 3.57 \sqrt{0.0014 + 0.09 \left(\frac{1}{N_{Re}} \right)^{0.27}}$$

for $N_{Re} > 20,000$

B. Mathematical Routines

1) Lagrangian Interpolation Routine (Subroutine LAGINT)

This routine may be used in the evaluation of Y-coordinate values for given values on X-axis by use of the Lagrangian interpolation method.

The calling sequence is

CALL LAGINT (N, X, Y, NV, XV, YV)

where

N = number of points in a given table

X, Y = coordinates of the given points

NV = number of points to be approximated by the interpolation

XV = X-coordinates of points for which the Y-coordinates are sought

YV = Y-coordinates obtained from interpolations

The X-coordinates in the given table should be in ascending order.

Notes:

- a) Limitations: $N \leq 500$ and $NV \leq 500$
- b) Dimensioned variables: X(500), Y(500), XV(500), YV(500)
- c) If XV(I) is less than the smallest or greater than the largest value of X, a message will be printed out and no interpolation will be attempted for that particular XV.

Control Program (CLAGIN)

The control program is written to illustrate a computation of mass rates for given pressure drops in an orifice manometer.

Suppose that the following table is obtained from a calibration experiment of an orifice meter.

Pressure Drop (in.)	1.0	2.0	3.0	4.0	5.0	6.0	7.0
Mass Rate (lb/min)	1.32	1.87	2.29	2.64	2.96	3.23	3.49

It is desired to compute the mass rates for runs carried out with the pressure drop as follows:

Run No.	1	2	3	4
Pressure Drop (in.)	1.5	3.5	4.0	5.5

The control program listing in Appendix 2 shows how subroutine LAGINT is used.

2) Gauss Elimination Routine (Subroutine GAUSS)

This routine will solve linear simultaneous equations by a Gauss elimination method. It is also employed as a sub-program of other subroutines such as least-squares fit and matrix inversion routines.

The calling sequence is

CALL GAUSS (M, A, X)

where

M = number of unknowns

A = coefficients of unknowns

X = unknowns

Notes:

- Limitation: $M \leq 50$
- Dimensioned variables: A(50,51), X(50)
- If the matrix of coefficients is singular or not solvable because of zero coefficients generated in the process of elimination, a message is printed out and computation stops.
- The original matrix of coefficients is not altered during the process.

Control Program (CGAUSS)

The following equations show component balances of acetone, water and air for an acetone recovery system.

acetone $F(0.0295) = P(0.99) + W(0.05) + A(0)$

water $120 = P(0.01) + W(0.95) + A(0)$

air $F(0.9705) = P(0) + W(0) + A$

(over-all $F + 120 = F + W + A$)

where

F = rate of feed to absorber, lb/hr

A = air leaving absorber, lb/hr

P = product, lb/hr

W = waste, lb/hr

the control program computes P, W, and A for a given F. The numerical computation was done with $F = 50,000 \text{ lb/hr}$.

3) Least-Squares Fit Routine (Subroutine LEASQU)

The object of this routine is to find an Nth degree polynomial which will best fit a set of data using the least-squares criterion. The polynomial is expressed in the form

$$Y = C_1 X^N + C_2 X^{N-1} + C_3 X^{N-2} + \dots + C_N X + C_{N+1}$$

The routine will compute $C_1, C_2, \dots, C_{N+1}$ provided that a set of X and Y data is given.

The calling sequence is

CALL LEASQU (N, X, Y, MDEGRE, C)

where

N = number of points given

X, Y = coordinates of the given points

MDEGRE = highest degree desired for a fit

(e.g. MDEGRE = 1 for a straight line)

C = coefficients of the polynomial

Notes:

- a) Limitation: $MDEGRE \leq 50$
- b) Dimensioned variables: X(200), C(50), Y(200)
- c) Subroutine GAUSS is called by this routine. Therefore, a source or binary deck of GAUSS should be submitted together with this routine.

Control Program (CLEASQ)

In an experiment, a flow meter is being calibrated. The following table has been obtained.

Readings (GPH)	20	30	40	50	60	70	80	90	100	120
True Rate (GPH)	19.8	29.7	39.7	49.6	60.2	70.3	80.2	90.0	102.5	120.5

It is desired to obtain a straight line correlating the flow meter reading with the true rate. The equation for this line is to be found by the method of least squares.

4) Matrix Multiplication Routine (Subroutine MATMPY)

This routine computes the product of two square matrices.

The calling sequence is

CALL MATMPY (N, A, B, C)

where

N = number of elements in a row or column

A = matrix A

B = matrix B

C = matrix C, the product of A and B

Notes:

a) Limitation: $N \leq 50$

b) Dimensioned variables: A(50,51), B(50,51), C(50,51)

Control Program (CMTMPY)

In solution of an engineering problem, the following two matrices A and B are obtained.

$$A = \begin{vmatrix} 8.467 & 5.137 & 3.141 & 2.063 \\ 5.137 & 6.421 & 2.617 & 2.003 \\ 3.141 & 2.617 & 4.128 & 1.628 \\ 2.063 & 2.003 & 1.628 & 3.446 \end{vmatrix}$$

$$B = \begin{vmatrix} 0.25087 & -0.16214 & -0.08116 & -0.01760 \\ -0.16214 & 0.33074 & -0.05994 & -0.06686 \\ -0.08116 & -0.05994 & 0.37988 & -0.09604 \\ -0.01760 & -0.06686 & -0.09604 & 0.38497 \end{vmatrix}$$

It is desired to find out whether matrix B is the inverse of matrix A. An easy way of solving this problem is to take the product of A and B and to check if the resulting matrix is the identity matrix. This control program will find the product of A and B.

5) Matrix Inversion Routine (Subroutine MATINV)

This subroutine inverts a square matrix by the Gauss elimination method.

The calling sequence is

CALL MATINV (M, A, B)

where

M = number of elements in a row or column

A = original matrix

B = inverse matrix of A

Notes:

- a) Limitation: $M \leq 50$
- b) Dimensioned variables: A(50,51), B(50,51)
- c) Subroutine GAUSS is a subprogram of this routine.

Control Program (CMTINV)

One way of solving a system of linear equations is by use of the inverse matrix of the coefficients.

$$\begin{aligned} \text{i.e.:} \quad & \vec{A}\vec{x} = \vec{b} ; \\ \text{Multiplying by } A^{-1}, \quad & A^{-1}\vec{A}\vec{x} = A^{-1}\vec{b}. \\ \text{Since} \quad & A^{-1}A = I, \\ \text{there results} \quad & \vec{x} = A^{-1}\vec{b} \end{aligned}$$

This method is very effective when $\vec{b}$ changes with $\vec{x}$ while A is kept constant, because $\vec{x}$ can be found very easily for different sets of $\vec{b}$ once A^{-1} is computed.

In the illustration of this control program, the following matrix A is inverted.

$$A = \begin{vmatrix} 8.467 & 5.137 & 3.141 & 2.063 \\ 5.137 & 6.421 & 2.617 & 2.003 \\ 3.141 & 2.617 & 4.128 & 1.628 \\ 2.063 & 2.003 & 1.628 & 3.446 \end{vmatrix}$$

6) Numerical Integration Routine by Simpson's Method (Sub-routine SIMPSN)

This routine finds the area under a curve given in the form of numerical points by Simpson's integration method. In this program Simpson's method has been modified to make it possible to work with both even and odd numbers of increments.

The calling sequence is
CALL SIMPSN (N, Y, H, A)

where

N = number of points (= number of increments + 1)
Y = Y-coordinates of the points
H = size of an increment on the X-axis
A = area obtained from the integration

Notes:

- a) Limitation: $N \leq 200$
- b) Dimensioned variable: $Y(200)$
- c) The points should be equally spaced on the X-axis.

Control Program (CSMPSN)

In a dispersion experiment using the trace injection technique, Levenspiel and Smith obtained the following results (Chem. Engr. Sci. vol. 6, p. 227, 1957):

<u>Time (sec)</u>	<u>Conc. (arbitrary unit)</u>
0.0	0.0
2.0	11.0
4.0	53.0
6.0	64.0
8.0	58.0
10.0	48.0
12.0	39.0
14.0	29.0
16.0	22.0
18.0	16.0
20.0	11.0
22.0	9.0
24.0	7.0
26.0	5.0
28.0	4.0
30.0	2.0
32.0	2.0
34.0	2.0
36.0	1.0
38.0	1.0
40.0	1.0
42.0	1.0

In order to normalize the concentration data, it is desired to compute the area under the concentration curve. This control program also shows how the dimensionless variance can be calculated in the dispersion experiment.

7) Modified Runge-Kutta Method Routine (Subroutine RUNMOD)

Subroutine RUNMOD solves an ordinary differential equation (first order) by a Runge-Kutta method as modified by Gill. The ordinary differential equation has the form $y' = F(x, y)$ with an initial condition $y(x_0) = y_0$.

The calling sequence is

```
CALL RUNMOD (N, X, Y, H)
```

where

```
N = number of points
X = X-coordinates of points (equally spaced)
Y = Y-coordinates of points computed
H = size of an increment on the X-axis
```

The function $y' = F(x, y)$ should be given in the following form (Example in FORTRAN II):

```
FUNCTION FUNCT(X, Y)
FUNCT =  $\alpha(X) + \beta(Y) + \gamma(X*Y) + \delta*$ 
RETURN
END
```

* α , β , γ , δ are constants, functions such as sine, cosine, log, etc. or combinations of them. For example, if $y' = \sin x + 2\cos 3y$ then

```
FUNCT = SIN(X) + 2. * COS(3. * Y)
```

Notes:

- a) Limitation: $N \leq 500$
- b) Dimensioned variables: X(500), Y(500)
- c) Since X's are equally spaced, it is necessary to give only the value of X(1). The others will be computed by the routine.
- d) The initial value Y(1) should be defined before the routine is called.

Control Program (CRUNMO)

A mixing tank problem will be considered as an example. In a large tank equipped with a stirrer, salt solution is introduced at a rate of 5 gal/min. The concentration of salt is 2lb/gal. Initially, the tank contained 100 gal of pure water. Assuming that the system is a perfectly mixing system and that the solution leaves the tank at the bottom at a rate of 1 gal/min, it is desired to find the concentration of salt in the tank as a function of time. In this case, the mathematical equation to be solved is

$$\frac{dc}{dt} = \frac{10}{100 + 4t} - \frac{5c}{100 + 4t}$$

with an initial condition $c = 0$ when $t = 0$.

APPENDIX 1. LISTING OF SUBROUTINE PROGRAMS

Disclaimer

Although each program has been tested by the author, no warranty, express or implied, is made by the author, as to the accuracy and functioning of the programs and related program materials, nor shall the fact of distribution constitute any such warranty, and no responsibility is assumed by the author or the Computer Science Center in connection therewith.

ABBREVIATIONS USED FOR UNITS IN SUBROUTINE CONVRT

ACRE	ACRE
ANGSTROM	ANGST
ATMOSPHERE	ATM
BAR	BAR
BRITISH THERMAL UNIT	BTU
BUSHEL	BUSH
CALORIE (GRAM-)	CAL
CENTIMETER	CM
CENTIPOISE	CP
DAY	DAY
DEGREE CENTIGRADE	DEGC
DEGREE FAHRENHEIT	DEGF
DYNE	DYNE
ERG	ERG
FOOT	FT
FEET OF WATER (PRESSURE, AT 15 DEGREES C)	FTWAT
GALLON	GAL
GRAM	GR
GRAIN	GRAIN
GRAVITY	GRAVIT
HORSEPOWER	HP
HOURL	HR
INCH	INCH
INCHES OF MERCURY (PRESSURE, AT 0 DEGREES C)	INHG
INCHES OF WATER (PRESSURE, AT 15 DEGREES C)	IWATER
JOULE	JOULE
KELVIN (ABS. TEMP.)	KELVIN
KILOCALORIE	KCAL
KILOGRAM	KG
KILOMETER	KM
KILOWATT	KW
POUND	LB
LITER	LITER
METER	M
MEGABAR	MEGBAR
MICRON	MICRON
MILE	MILE
MINUTE	MIN
MILIMETER	MM
MM OF MERCURY (PRESSURE)	MMHG
MILIMICRON	MMICR
METERS OF WATER (PRESSURE, AT 15 DEGREES C)	MWATER
OUNCE (WEIGHT)	OUNCE
OUNCE (VOLUME)	OZ
POISE	POISE
QUART (DRY)	QUARTD
QUART (LIQUID)	QUARTL
RANKIN (ABS. TEMP.)	RANKIN
ROD	ROD
SECOND	SEC
TON (METRIC)	TONM
TON-REFRIGERATION	TONREF
TON (SHORT)	TONS
WATT	WATT
YARD	YD

PROGRAMS

*	FAP	
	LBL	CONVRT,2
	ENTRY	CONVRT
CONVRT	SXA	X1,1
	SXA	X2,2
	SXA	X4,4
	CLA*	1,4
	TZE	DIRECT
	PDC	,1
	CLA	2,4
	STA	RELOC1
	CLA	3,4
	STA	RELOC2
	CAL	ALLONE
	SLW	S1,1
	SLW	S2,1
	AXT	0,1
	AXT	0,2
TEST	CAL	S1,1
	LAS	ALLONE
	TRA	*+2
	TRA	FINISH+1
RELOC1	CAL	** ,2
	SLW	S1,1
RELOC2	CAL	** ,2
	SLW	S2,1
	TXI	*+1,1,-1
	TXI	TEST,2,1
FINISH	PZE	S1
	CLA	*-1
	STA	ARG2
	TRA	*+2
	PZE	S2
	CLA	*-1
	STA	ARG3
	TRA	COMMON
DIRECT	CLA	2,4
	STA	ARG2
	CLA	3,4
	STA	ARG3
COMMON	CLA	4,4
	STA	ANSWER
	TSX	SEPCOM,4
ARG2	PZE	**
	PZE	VALUE1
	TSX	SEPCOM,4
ARG3	PZE	**
	PZE	VALUE2
	CLA	VALUE2
	FDP	VALUE1
ANSWER	STQ	**
X1	AXT	** ,1
X2	AXT	** ,2
X4	AXT	** ,4
	TRA	5,4
VALUE1	BSS	1
VALUE2	BSS	1
S1	BSS	100
S2	BSS	100
ALLONE	OCT	777777777777

EXTERN SEPCOM
END

*	FAP	
	LBL	SEPCOM,2
	ENTRY	SEPCOM
SEPCOM	SXA	SAVE1,1
	SXA	SAVE2,2
	SXA	SAVE4,4
	AXT	100,1
	STZ	S+100,1
	TIX	*-1,1,1
	CLA	1,4
	STA	BIGLP
	CLA	2,4
	STA	ANSWER
	AXT	-30,1
	AXT	0,2
	ZAC	
BIGLP	LDQ	**
SMLP	LGL	6
	LAS	BLANK1
	TRA	*+2
	TRA	BRNCH2
	LAS	LEFTP
	TRA	CHECKM
	TRA	*+2
	TRA	CHECKM
	SLW	S,2
	TXI	BRNCH2,2,-1
CHECKM	LAS	MULTPL
	TRA	CHECKD
	TRA	*+2
	TRA	CHECKD
	TXI	*+1,2,-1
	SLW	S,2
	CAL	S-1,2
	TZE	*+2
	TRA	M
	CAL	S-2,2
	LAS	MULTPL
	CALL	ERROR1
	TRA	*+2
	CALL	ERROR1
	TXI	*+1,2,1
	CAL	EXPNT
	SLW	S-1,2
	TRA	BRNCH2
M	TXI	BRNCH1,2,-1
CHECKD	LAS	DIVIDE
	TRA	CHECKR
	TRA	*+2
	TRA	CHECKR
	TXI	*+1,2,-1
	SLW	S,2
	TXI	BRNCH1,2,-1
CHECKR	LAS	RIGHTP
	TRA	CHARCT
	TRA	*+2
	TRA	CHARCT
	TXI	*+1,2,-1
	SLW	S,2
	TRA	BRNCH3

CHARCT	ALS	0,1
	ORS	S,2
	TXI	BRNCH2,1,6
BRNCH1	CAL	S-2,2
	LAS	RIGHTP
	TRA	*+2
	TRA	BRNCH2
	ANA	MASK1
	TZE	NUMBER
	PXA	,1
	PAC	,1
	CAL	BLANK
	ARS	30,1
	ORS	S-2,2
	TRA	RESET1
BRNCH3	CAL	S-1,2
	LAS	RIGHTP
	TRA	*+2
	TRA	BRNCH2
	ANA	MASK1
	TZE	NUMBR2
	PXA	,1
	PAC	,1
	CAL	BLANK
	ARS	30,1
	ORS	S-1,2
	TRA	RESET1
NUMBR2	CAL	S-1,2
	ARS	30
	SLW	S-1,2
	TRA	RESET1
NUMBER	CAL	S-2,2
	ARS	30
	SLW	S-2,2
RESET1	AXT	-30,1
BRNCH2	XCL	
	TZE	*+4
	XCL	
	CLM	
	TRA	SMLP
	CAL	BIGLP
	ADD	=01
	STA	BIGLP
	STA	TEST2
TEST2	CAL	**
	LAS	=077777777777
	TRA	BIGLP-1
	TRA	*+2
	TRA	BIGLP-1
	PXA	,2
	STO	IR2
	CAL	S,2
	LAS	RIGHTP
	TRA	*+2
	TRA	RESET2
	ANA	MASK1
	TZE	NUMBR3
	PXA	,1

	PAC	,1
	CAL	BLANK
	ARS	30,1
	ORS	S,2
	TRA	RESET2
NUMBR3	CAL	S,2
	ARS	30
	SLW	S,2
RESET2	AXT	0,1
GETNOS	CAL	S,2
	ANA	MASK1
	TZE	REPEAT-1
	CAL	S,2
	SLW	A
	TSX	GETNO,4
	PZE	A
	PZE	B
	CLA	B
	STO	S,2
	TXI	*+1,1,1
REPEAT	TXL	CALC,2,0
	TXI	GETNOS,2,1
CALC	AXT	0,1
BIGLP2	CAL	S,1
	LAS	EXPNT
	TRA	*+2
	TRA	FIRST
	PXA	,1
	SUB	IR2
	TZE	SMLP2
	TXI	BIGLP2,1,-1
SMLP2	AXT	0,1
	CAL	S,1
	LAS	RIGHTP
	TRA	*+2
	TRA	SECOND
	PXA	,1
	SUB	IR2
	TZE	THIRD
	TXI	SMLP2+1,1,-1
FIRST	CLA	S-1,1
	STO	TEMP1
LOOP1	CLA	S+1,1
	SUB	=01
	STO	S+1,1
	TZE	*+5
	LDQ	S-1,1
	FMP	TEMP1
	STO	S-1,1
	TRA	LOOP1
	CAL	BLANK
	SLW	S,1
	SLW	S+1,1
	AXT	0,1
	TRA	BIGLP2
SECOND	TXI	*+1,1,1
	CAL	S,1
	LAS	LEFTP

	TRA	*+2
	TRA	LOOP2
	TIX	SECOND,1,0
	CALL	ERROR2
LOOP2	SXA	X1,1
	SXA	XX1,1
	CLA	S+1,1
	STO	TEMP2
	TXI	*+1,1,-1
	CAL	S+1,1
	LAS	BLANK
	TRA	*+2
	TRA	*-4
	LAS	MULTPL
	TRA	*+2
	TRA	PROD
	LAS	DIVIDE
	TRA	*+2
	TRA	DIVISN
	CAL	BLANK
	SLW	S+1,1
XX1	AXT	**,1
	SLW	S,1
	TRA	SMLP2
PROD	CAL	BLANK
	SLW	S+1,1
	TXI	*+1,1,-1
	CAL	S+1,1
	LAS	BLANK
	TRA	*+2
	TRA	PROD+2
	LDQ	S+1,1
	FMP	TEMP2
	STO	TEMP3
	CAL	BLANK
	SLW	S+1,1
X1	AXT	**,1
	CLA	TEMP3
	STO	S+1,1
	TRA	LOOP2
DIVISN	CAL	BLANK
	SLW	S+1,1
	TXI	*+1,1,-1
	CAL	S+1,1
	LAS	BLANK
	TRA	*+2
	TRA	DIVISN+2
	CLA	TEMP2
	FDP	S+1,1
	STQ	TEMP3
	CAL	BLANK
	SLW	S+1,1
	TRA	X1
THIRD	AXT	0,1
	CAL	S,1
	LAS	BLANK
	TRA	FINAL
	TRA	*+2

	TRA	FINAL
	PXA	,1
	SUB	IR2
	TZE	*+2
	TXI	THIRD+1,1,-1
	CALL	ERROR4
FINAL	CLA	S,1
	STO	RESULT
	PXA	,1
	SUB	IR2
	TZE	END
LOOP3	TXI	*+1,1,-1
	CAL	S,1
	LAS	BLANK
	TRA	*+2
	TRA	*+5
	LAS	LEFTP
	TRA	COMPUT
	CALL	ERROR3
	TRA	COMPUT
	PXA	,1
	SUB	IR2
	TZE	END
	TRA	LOOP3
COMPUT	LAS	MULTPL
	TRA	DCHECK
	TRA	*+2
	TRA	DCHECK
	SXA	XA1,1
LOOP4	TXI	*+1,1,-1
	CAL	S,1
	LAS	BLANK
	TRA	MPY
	TRA	*+2
	TRA	MPY
	PXA	,1
	SUB	IR2
	TZE	*+2
	TRA	LOOP4
	CALL	ERROR5
MPY	LAS	LEFTP
	TRA	*+2
	CALL	ERROR3
	LDQ	RESULT
	FMP	S,1
	STO	RESULT
	CAL	BLANK
	SLW	S,1
XA1	AXT	** ,1
	SLW	S,1
	TRA	LOOP3
DCHECK	LAS	DIVIDE
	CALL	ERROR6
	TRA	*+2
	CALL	ERROR6
	SXA	XXA1,1
LOOP5	TXI	*+1,1,-1
	CAL	S,1

	LAS	BLANK
	TRA	DIV
	TRA	*+2
	TRA	DIV
	PXA	,1
	SUB	IR2
	TZE	*+2
	TRA	LOOP5
	CALL	ERROR7
DIV	LAS	LEFTP
	TRA	*+2
	CALL	ERROR3
	CLA	RESULT
	FDP	S,1
	STQ	RESULT
	CAL	BLANK
	SLW	S,1
XXA1	AXT	**,1
	SLW	S,1
	TRA	LOOP3
END	CLA	RESULT
ANSWER	STO	**
SAVE1	AXT	**,1
SAVE2	AXT	**,2
SAVE4	AXT	**,4
	TRA	3,4
BLANK1	OCT	60
BLANK	OCT	606060606060
LEFTP	OCT	74
MULTPL	OCT	54
EXPNT	OCT	5454
DIVIDE	OCT	61
RIGHTP	OCT	34
MASK1	OCT	700000000000
A	BSS	1
B	BSS	1
S	BSS	100
IR2	BSS	1
TEMP1	BSS	1
TEMP2	BSS	1
TEMP3	BSS	1
RESULT	BSS	1
	EXTERN	GETNO
	EXTERN	ERROR1,ERROR2,ERROR3,ERROR4,ERROR5,ERROR6,ERROR7
	END	

*	FAP	
	LBL	GETNO,2
	ENTRY	GETNO
GETNO	SXA	X2,2
	SXA	X4,4
	SXA	X1,1
	CLA	2,4
	STA	NUMBER
	ZAC	
	LDQ*	1,4
	LGL	6
	LAS	=031
	TRA	MIDDLE
	TRA	*+1
	SUB	=021
MIDDLE	TRA	SETIND
	LAS	=051
	TRA	LAST
	TRA	*+1
	SUB	=030
LAST	TRA	SETIND
SETIND	SUB	=040
	PAC	,1
	CLA	COUNT,1
	SUB	COUNT-1,1
	PAX	,2
	CLA	COUNT,1
	PAC	,1
COMP	CAL*	1,4
	LAS	TABLE-1,1
	TRA	*+2
	TRA	FOUND
	TIX	*+2,2,1
	CALL	WRITE1
	TXI	COMP,1,1
FOUND	CLA	FACTOR-1,1
NUMBER	STO	**
X2	AXT	**,2
X4	AXT	**,4
X1	AXT	**,1
	TRA	3,4
STARTA	SYN	*
TABLE	BCI	1,ACRE
	BCI	1,ANGST
	BCI	1,ATM
AN	EQU	*-STARTA
STARTB	SYN	*
	BCI	1,BAR
	BCI	1,BTU
	BCI	1,BUSH
BN	EQU	*-STARTA
STARTC	SYN	*
	BCI	1,CAL
	BCI	1,CM
	BCI	1,CP
CN	EQU	*-STARTA
STARTD	SYN	*
	BCI	1,DAY
	BCI	1,DEGC
	BCI	1,DEGF

	BCI	1,DYNE
DN	EQU	*-STARTA
STARTE	SYN	*
	BCI	1,ERG
EN	EQU	*-STARTA
STARTF	SYN	*
	BCI	1,FT
	BCI	1,FTWAT
FN	EQU	*-STARTA
STARTG	SYN	*
	BCI	1,GAL
	BCI	1,GR
	BCI	1,GRAIN
	BCI	1,GRAVIT
GN	EQU	*-STARTA
STARTH	SYN	*
	BCI	1,HP
	BCI	1,HR
HN	EQU	*-STARTA
STARTI	SYN	*
	BCI	1,INCH
	BCI	1,INHG
	BCI	1,IWATER
IN	EQU	*-STARTA
STARTJ	SYN	*
	BCI	1,JOULE
JN	EQU	*-STARTA
STARTK	SYN	*
	BCI	1,KCAL
	BCI	1,KELVIN
	BCI	1,KG
	BCI	1,KM
	BCI	1,KW
KN	EQU	*-STARTA
STARTL	SYN	*
	BCI	1,LB
	BCI	1,LITER
LN	EQU	*-STARTA
STARTM	SYN	*
	BCI	1,M
	BCI	1,MEGBAR
	BCI	1,MICRON
	BCI	1,MILE
	BCI	1,MIN
	BCI	1,MM
	BCI	1,MMHG
	BCI	1,MMICR
	BCI	1,MWATER
MN	EQU	*-STARTA
STARTN	SYN	*
NN	EQU	*-STARTA
STARTO	SYN	*
	BCI	1,OUNCE
	BCI	1,OZ
ON	EQU	*-STARTA
STARTP	SYN	*
	BCI	1,POISE
PN	EQU	*-STARTA

STARTQ	SYN	*
	BCI	1,QUARTD
	BCI	1,QUARTL
QN	EQU	*-STARTA
STARTR	SYN	*
	BCI	1,RANKIN
	BCI	1,ROD
RN	EQU	*-STARTA
STARTS	SYN	*
	BCI	1,SEC
SN	EQU	*-STARTA
STARTT	SYN	*
	BCI	1,TONM
	BCI	1,TONREF
	BCI	1,TONS
TN	EQU	*-STARTA
STARTU	SYN	*
UN	EQU	*-STARTA
STARTV	SYN	*
VN	EQU	*-STARTA
STARTW	SYN	*
	BCI	1,WATT
WN	EQU	*-STARTA
STARTX	SYN	*
XN	EQU	*-STARTA
STARTY	SYN	*
	BCI	1,YD
YN	EQU	*-STARTA
STARTZ	SYN	*
ZN	EQU	*-STARTA
	PZE	0
COUNT	PZE	AN
	PZE	BN
	PZE	CN
	PZE	DN
	PZE	EN
	PZE	FN
	PZE	GN
	PZE	HN
	PZE	IN
	PZE	JN
	PZE	KN
	PZE	LN
	PZE	MN
	PZE	NN
	PZE	ON
	PZE	PN
	PZE	QN
	PZE	RN
	PZE	SN
	PZE	TN
	PZE	UN
	PZE	VN
	PZE	WN
	PZE	XN
	PZE	YN
	PZE	ZN
FACTOR	DEC	2.471E-08

DEC 1.0E+08
 DEC 0.9678E-03
 DEC 0.9807
 DEC 9.296F-08
 DEC 0.02838E-03
 DEC 2.344F-02
 DEC 1.
 DEC 0.27777778E-01
 DEC 0.041667
 DEC 1.0
 DEC 1.8
 DEC 980.655
 DEC 9.80665E+02
 DEC 0.032808
 DEC 32.84E-03
 DEC 0.2642E-03
 DEC 1.0
 DEC 15.432
 DEC 0.7868253E-10
 DEC 0.3653E-10
 DEC 1.0
 DEC 0.3937
 DEC 28.96E-03
 DEC 394.05E-03
 DEC 9.80665E-05
 DEC 2.344E-05
 DEC 1.0
 DEC 0.001
 DEC 1.0E-05
 DEC 0.2724E-10
 DEC 0.002205
 DEC 0.001
 DEC 0.01
 DEC 0.9807E-03
 DEC 1.0E+04
 DEC 6.2E-06
 DEC 60.
 DEC 10.
 DEC 735.559E-03
 DEC 1.0E+07
 DEC 10.01E-03
 DEC 0.03527
 DEC 33.81E-03
 DEC 0.27777778E-03
 DEC 0.9081E-03
 DEC 1.057E-03
 DEC 1.8
 DEC 0.0019884
 DEC 3600.
 DEC 0.1E-05
 DEC 7.74667E-12
 DEC 0.1102E-05
 DEC 0.2724E-07
 DEC 0.010936
 FND

ANGST
 ATM
 BAR
 BTU
 BUSH
 CAL
 CM
 CP
 DAY
 DEGC
 DEGF
 DYNE
 ERG
 FT
 FTWAT
 GAL
 GR
 GRAIN
 GRAVIT
 HP
 HR
 INCH
 INHG
 IWATER
 JOULE
 KCAL
 KELVIN
 KG
 KM
 KW
 LB
 LITER
 M
 MEGBAR
 MICRON
 MILE
 MIN
 MM
 MMHG
 MMICR
 MWATER
 OUNCE
 OZ
 POISE
 QUARTD
 QUARTL
 RANKIN
 ROD
 SEC
 TONM
 TONREF
 TONS
 WATT
 YD

```
SUBROUTINE ERROR1  
  WRITE OUTPUT TAPE 6, 1000,  
1000 FORMAT(1H0/1H05X,104H...ERROR1... TWO OPERATORS SUCH AS * AND / AR  
1E WRITTEN CONSECUTIVELY IN THE FORMATION OF A COMPLEX UNIT. )  
  CALL EXIT  
  END
```

```
SUBROUTINE ERROR2  
  WRITE OUTPUT TAPE 6, 1000  
1000 FORMAT(1H0/1H05X,75H...ERROR2... TOO MANY RIGHT PARENTHESES IN THE  
1 FORMATION OF A COMPLEX UNIT.  )  
  CALL EXIT  
  END
```

```
SUBROUTINE ERROR3  
  WRITE OUTPUT TAPE 6, 1000  
1000 FORMAT(1H0/1H05X,74H...ERROR3... TOO MANY LEFT PARENTHESES IN THE  
  INFORMATION OF A COMPLEX UNIT.  )  
  CALL EXIT  
  END
```

```
SUBROUTINE ERROR4  
  WRITE OUTPUT TAPE 6, 1000  
1000 FORMAT(1H0/1H05X,68H...ERROR4... THE UNIT IS NOT INTRODUCED PROPER  
1LY OR A PROGRAM ERROR.  )  
  CALL EXIT  
  END
```

```
SUBROUTINE ERRORS  
WRITE OUTPUT TAPE 6, 1000  
1000 FORMAT(1H0/1H05X,74H...ERROR5... NO SIMPLE UNIT IS PRESENT AFTER A  
1 MULTIPLICATION OPERATOR(*). )  
CALL EXIT  
END
```

```
SUBROUTINE ERROR6  
WRITE OUTPUT TAPE 6, 1000  
1000 FORMAT(1H0/1H05X,64H...ERROR6... NO PROPER OPERATOR EXISTS BETWEEN  
1 TWO SIMPLE UNITS. )  
CALL EXIT  
END
```

```
SUBROUTINE ERROR7  
  WRITE OUTPUT TAPE 6, 1000  
1000 FORMAT(1H0/1H05X,68H...ERROR7... THE UNIT IS NOT INTRODUCED PROPER  
      1LY OR A PROGRAM ERROR.  )  
      CALL EXIT  
      END
```

```
SUBROUTINE WRITE1  
  WRITE OUTPUT TAPE 6, 1.  
1 FORMAT(1H0/1H05X,89H...ERROR... CHECK THE LIST OF ABBREVIATION OF  
  1UNITS WHETHER YOU ARE USING THE RIGHT ONES.  )  
  CALL EXIT  
  END
```

```

C          SUBROUTINE - LNPLLOT
C          A LOG - LOG PLOT ROUTINE
C
C          SUBROUTINE LNPLLOT(N,X,Y,SYMBOL)
C
C          DIMENSION X(200),Y(200),XL(200),YL(200),POINT(121,97),YNUMB(97),
INSX(10),NSY(10),XNUMB(10)
C
C          DO 5 I=1,N
XL(I)=LOGF(X(I))*0.434294
YL(I)=LOGF(Y(I))*0.434294
5 CONTINUE
C
C          XMIN=XL(1)
XMAX=XL(1)
YMIN=YL(1)
YMAX=YL(1)
C
C          DO 50 I=2,N
IF(XMIN-XL(I)) 20,20,15
15 XMIN=XL(I)
20 IF(XMAX-XL(I)) 25,30,30
25 XMAX=XL(I)
30 IF(YMIN-YL(I)) 40,40,35
35 YMIN=YL(I)
40 IF(YMAX-YL(I)) 45,50,50
45 YMAX=YL(I)
50 CONTINUE
C
C          IF(INTF(XMIN)-XMIN)54,56,55
54 XMIN=INTF(XMIN)
GO TO 56
55 XMIN=INTF(XMIN)-1.0
56 IF(INTF(XMAX)-XMAX) 59,61,60
59 XMAX=INTF(XMAX)+1.0
GO TO 61
60 XMAX=INTF(XMAX)
61 IF(INTF(YMIN)-YMIN) 64,66,65
64 YMIN=INTF(YMIN)
GO TO 66
65 YMIN=INTF(YMIN)-1.0
66 IF(INTF(YMAX)-YMAX) 69,75,70
69 YMAX=INTF(YMAX)+1.0
GO TO 75
70 YMAX=INTF(YMAX)
C
C          75 XCYCLE=(XMAX-XMIN)+0.5
XSPACE=120./INTF(XCYCLE)
NXSPCE=XINTF(XSPACE+0.5)
C
C          YCYCLE=(YMAX-YMIN)+0.5
YSPACE=12.*XSPACE/20.
NYSPE=XINTF(YSPACE+0.5)
NYH=XINTF(YSPACE*INTF(YCYCLE)+0.5)+1
C
C          DO 80 I=1,121
DO 80 J=1,NYH
B          POINT(I,J)=606060606060
YNUMB(J)=0.0
80 CONTINUE

```

C

```

DO 85 I=1,8
AI=FLOATF(I)+1.0
YSCALE=LOGF(AI)*0.434294*YSPACE+0.5
NSY(I)=XINTF(YSCALE)
XSCALE=LOGF(AI)*0.434294*XSPACE+0.5
NSX(I)=XINTF(XSCALE)

```

85 CONTINUE

C

```

DO 95 I=1,121
DO 95 J=1,NYH,NYSPCE
NPOWER=(J-1)/NYSPCE
POINT(I,J)=1H-
YNUMB(J)=10.** (YMIN)*(10.**NPOWER)
IF(J-NYH) 86,95,95

```

86 DO 90 K=1,8

AK=K

JK=J+NSY(K)

90 YNUMB(JK)=(AK+1.0)*YNUMB(J)

95 CONTINUE

C

```

DO 105 J=1,NYH
DO 105 I=1,121,NXSPCE
POINT(I,J)=1HI

```

105 CONTINUE

C

```

DO 115 I=1,121,NXSPCE
DO 115 J=1,NYH,NYSPCE
POINT(I,J)=1H+
IF(I-121) 106,115,115

```

106 DO 110 K=1,8

JK=J+NSY(K)

POINT(I,JK)=1H+

IK=I+NSX(K)

110 POINT(IK,J)=1H+

115 CONTINUE

C

```

DO 120 K=1,N
AI=(XL(K)-XMIN)*XSPACE+0.5
I=XINTF(AI)+1
AJ=(YL(K)-YMIN)*YSPACE+0.5
J=XINTF(AJ)+1
POINT(I,J)=SYMBOL

```

120 CONTINUE

C

```

DO 135 JREV=1,NYH
J=NYH+1-JREV

```

IF(YNUMB(J)) 130,125,130

125 WRITE OUTPUT TAPE 6, 500, (POINT(I,J),I=1,121)

GO TO 135

130 WRITE OUTPUT TAPE 6, 501, YNUMB(J), (POINT(I,J),I=1,121)

135 CONTINUE

C

XNUMB(1)=10.** (XMIN)

NCYCLE=XINTF(XCYCLE)

IH=NCYCLE+1

DO 136 I=2,IH

XNUMB(I)=XNUMB(I-1)*10.

```
136 CONTINUE
    IF(NCYCLE-2) 145,150,140
140 IF(NCYCLE-4) 155,160,165
145 WRITE OUTPUT TAPE 6, 502, (XNUMB(I),I=1,IH)
    GO TO 200
150 WRITE OUTPUT TAPE 6, 503, (XNUMB(I),I=1,IH)
    GO TO 200
155 WRITE OUTPUT TAPE 6, 504, (XNUMB(I),I=1,IH)
    GO TO 200
160 WRITE OUTPUT TAPE 6, 505, (XNUMB(I),I=1,IH)
    GO TO 200
165 WRITE OUTPUT TAPE 6, 506, XNUMB(1),XNUMB(IH)
```

C

```
500 FORMAT(8X,121A1)
501 FORMAT(1PE8.1,(121A1))
502 FORMAT(6X,E8.1,110X,E8.1)
503 FORMAT(6X,E8.1,50X,E8.1,52X,E8.1)
504 FORMAT(6X,E8.1,5X,2H 2,5X,2H 3,3X,2H 4,2X,2H 5,3H 6,3H 7,1X,E8.1
    1,2(7X,2H 2,5X,2H 3,3X,2H 4,2X,2H 5,3H 6,3H 7,1X,E8.1))
505 FORMAT(6X,E8.1,20X,E8.1,3(22X,E8.1))
506 FORMAT(6X,E8.1,110X,E8.1)
```

C

```
200 RETURN
    END
```

SUBROUTINE - LAGINT
 A LAGRANGIAN INTERPOLATION METHOD USING ARBITRARY SET OF ORDINATES
 REFERENCE - HILDEBRAND, INTRODUCTION TO NUMERICAL ANALYSIS, 1956
 P60

SUBROUTINE LAGINT(N,X,Y,NV,XV,YV)

DIMENSION X(500),Y(500),XV(500),YV(500)

DO 17 K=1,NV

CHECK IF XV(K) IS INSIDE THE RANGE OF X VALUES

IF(XV(K)-X(1)) 13,4,3
 3 IF(XV(K)-X(N)) 4,4,14

CHECK IF XV(K) IS IDENTICAL TO ANY ONE OF THE VALUES OF X

4 DO 5 I=1,N
 IF(XV(K)-X(I)) 6,15,5
 5 CONTINUE

MAIN COMPUTATION

6 PAI=1.
 DO 7 I=1,N
 7 PAI=PAI*(XV(K)-X(I))
 BOT1=(XV(K)-X(1))
 DO 8 I=2,N
 8 BOT1=BOT1*(X(1)-X(I))
 TERM1=Y(1)/BOT1
 NL=N-1
 TERMIN=0.
 DO 11 J=2,NL
 BOTIN=(XV(K)-X(J))
 JL=J-1
 JH=J+1
 DO 9 I=1,JL
 9 BOTIN=BOTIN*(X(J)-X(I))
 DO 10 I=JH,N
 10 BOTIN=BOTIN*(X(J)-X(I))
 TERMIN=TERMIN+Y(J)/BOTIN
 11 CONTINUE
 BOTN=(XV(K)-X(N))
 DO 12 I=1,NL
 12 BOTN=BOTN*(X(N)-X(I))
 TERMN=Y(N)/BOTN

SIGMA=TERM1+TERMIN+TERMN
 YV(K)=PAI*SIGMA
 GO TO 17

13 WRITE OUTPUT TAPE 6,500,K,XV(K)
 GO TO 17
 14 WRITE OUTPUT TAPE 6, 501, K,XV(K)
 GO TO 17
 15 YV(K)=Y(I)
 17 CONTINUE

500 FORMAT(/11X8H WHEN K=13,8H, XV(K)=E14.7,37H IS LESS THAN THE SMALL

1EST VALUE OF X/)
501 FORMAT(/11X8H WHEN K=I3,8H, XV(K)=E14.7,38H IS LARGER THAN THE BIG
1GEST VALUE OF X/)

C

20 RETURN
END

SUBROUTINE - GAUSS

```

C
C
SUBROUTINE GAUSS(M,A,X)
C
C   DIMENSION A(50,51),B(50,51),X(50),AI(50,51)
C
C   N=M+1
C
C   DO 1 I=1,M
C   DO 1 J=1,N
C   AI(I,J)=A(I,J)
C   1 CONTINUE
C
C   DO 100 K=1,M
C   DO 100 I=1,M
C   IF(I-K) 100,5,40
C   5 DO 30 J=1,N
C   IF(J-I) 10,15,15
C   10 B(I,J)=0.0
C   GO TO 30
C   15 IF(AI(I,I)) 16,20,16
C   16 B(I,J)=AI(I,J)/AI(I,I)
C   GO TO 30
C   20 L=I+1
C   21 IF(AI(L,L)) 25,35,25
C   25 B(I,J)=AI(L,J)/AI(L,L)
C   AI(L,J)=AI(I,J)
C   GO TO 30
C   35 L=L+1
C   IF(L-M) 21,21,36
C   36 WRITE OUTPUT TAPE 6, 1003,K
C   GO TO 160
C   30 CONTINUE
C   GO TO 100
C   40 DO 80 J=1,N
C   IF(J-(K+1)) 80,45,45
C   45 AI(I,J)=AI(I,J)-B(K,J)*AI(I,K)
C   80 CONTINUE
C   100 CONTINUE
C
C   X(M)=B(M,N)
C   ML=M-1
C   DO 120 I=1,ML
C   K=M-I
C   SUM=0.0
C   KH=K+1
C   105 DO 110 J=KH,M
C   110 SUM=SUM+B(K,J)*X(J)
C   X(K)=B(K,N)-SUM
C   120 CONTINUE
C
C   1003 FORMAT(1H010X,46H NO SOLUTIONS BECAUSE OF ZERO COEFFICIENTS ON 14,
C   114HTH ELIMINATION)
C   150 RETURN
C   160 CALL EXIT
C   END

```

```
C          SUBROUTINE - LEASQU
C          POLYNOMIAL FIT BY THE LEAST-SQUARES METHOD
C          SUBROUTINE LEASQU(N,X,Y,MDEGRE,C)
C          DIMENSION A(50,51),X(200),Y(200),C(50),S(200),V(200)
C          M=MDEGRE+1
C          M1=M+1
C          MH=2*MDEGRE+1
C          DO 5 I=1,MH
C             S(I)=0.0
C             DO 5 K=1,N
C                S(I)=S(I)+X(K)**(MH-I)
C          5 CONTINUE
C          DO 10 I=1,M
C             V(I)=0.0
C             DO 10 K=1,N
C                V(I)=V(I)+Y(K)*(X(K)**(M-I))
C          10 CONTINUE
C          DO 20 I=1,M
C             A(I,M1)=V(I)
C             DO 20 J=1,M
C                IJL=I+J-1
C                A(I,J)=S(IJL)
C          20 CONTINUE
C          CALL GAUSS(M,A,C)
C          RETURN
C          END
```

```
C      SUBROUTINE - MATMPY
C      COMPUTING THE PRODUCT OF TWO SQUARE MATRICES
C
C      SUBROUTINE MATMPY(N,A,B,C)
C
C      DIMENSION A(50,51),B(50,51),C(50,51)
C
C      DO 30 I=1,N
C      DO 30 J=1,N
C      C(I,J)=0.0
C      DO 20 K=1,N
C      C(I,J)=C(I,J)+A(I,K)*B(K,J)
20 CONTINUE
30 CONTINUE
RETURN
END
```

```
C          SUBROUTINE - MATINV
C  COMPUTING THE INVERSE OF A SQUARE MATRIX BY USE OF GAUSS-
C  ELIMINATION METHOD
C
C  SUBROUTINE MATINV(M,A,B)
C  DIMENSION A(50,51),B(50,51),X(50)
C
C  N=M+1
C
C  DO 20 I=1,M
20  A(I,N)=0.0
C  DO 30 I=1,M
C  A(I,N)=1.0
C  CALL GAUSS(M,A,X)
C  DO 25 J=1,M
C  B(J,I)=X(J)
25  CONTINUE
C  DO 26 K=1,M
C  A(K,N)=0.0
26  CONTINUE
30  CONTINUE
C
C  RETURN
C  END
```

```
C          SUBROUTINE - SIMPSN
C  A SUBROUTINE TO COMPUTE INTEGRAL OF A FUNCTION BY THE SIMPSONS
C  RULE
C
C  SUBROUTINE SIMPSN(N,Y,H,A)
C
C  DIMENSION Y(200)
C
C  CHECK=FLOATF(N)/2.0
C  ICHECK=CHECK
C  IF(CHECK-FLOATF(ICHECK)) 1,15,1
C
C  1 K=1
C  2 NL=N-1
C    NLL=N-2
C    SUMEVE=0.0
C    SUMODD=0.0
C    DO 5 I=2,NL,2
C      SUMEVE=SUMEVE+Y(I)
C  5 CONTINUE
C    DO 10 I=3,NLL,2
C      SUMODD=SUMODD+Y(I)
C  10 CONTINUE
C
C    A=(Y(1)+SUMEVE*4.+SUMODD*2.+Y(N))*H/3.
C
C    GO TO (100,20),K
C
C  15 N=N-1
C    K=2
C    GO TO 2
C
C  20 N=N+1
C    ALAST=(Y(N-1)+Y(N))*H/2.0
C    A=A+ALAST
C
C  100 RETURN
C    END
```

```

C      SUBROUTINE - RUNMOD
C      A RUNGE-KUTTA METHOD MODIFIED BY GILL TO SOLVE AN ORDINARY
C      DIFFERENTIAL EQUATION
C      REFERENCE - RALSTON AND WILF, MATHEMATICAL METHOD FOR DIGITAL
C                      COMPUTERS, 1960, P110
C

```

```

C      SUBROUTINE RUNMOD(N,X,Y,H)
C      DIMENSION X(500),Y(500)

C      Q0=0.
C      NL=N-1
C      DO 2 I=1,NL
C      U=X(I)
C      V=Y(I)
C      T1=H*FUNCT(U,V)
C      Q1=Q0+3.*(T1-2.*Q0)/2.-T1/2.
C      Y2=Y(I)+(T1-2.*Q0)/2.
C      U=X(I)+H/2.
C      V=Y2
C      T2=H*FUNCT(U,V)
C      Q2=Q1+3.*(1.-SQRTF(0.5))*(T2-Q1)-(1.-SQRTF(0.5))*T2
C      Y3=Y2+(1.-SQRTF(0.5))*(T2-Q1)
C      V=Y3
C      T3=H*FUNCT(U,V)
C      Q3=Q2+3.*(1.+SQRTF(0.5))*(T3-Q2)-(1.+SQRTF(0.5))*T3
C      Y4=Y3+(1.+SQRTF(0.5))*(T3-Q2)
C      U=X(I)+H
C      V=Y4
C      T4=H*FUNCT(U,V)
C      Q4=Q3+(T4-2.*Q3)/2.-T4/2.
C      Y(I+1)=Y4+(T4-2.*Q3)/6.
C      X(I+1)=X(I)+H
C      Q0=Q4
C 2 CONTINUE

C      RETURN
C      END

```

APPENDIX 2. LISTING OF CONTROL PROGRAMS
AND NUMERICAL RESULTS

```
CCCNVRT      CONTROL PROGRAM FOR SUBROUTINE CONVRT (CCNVRT)
C
C   CASE1 ... THE UNITS ARE INTRODUCED AS HOLLERITH ARGUMENTS
C   PROBLEM ... FIND A CONVERSION FACTOR FOR A UNIT CONVERSION
C               FROM BTU/SEC TO FT-LB/SEC
C
C   CALL CONVRT(0, 8H BTU/SEC, 12H (FT*LB)/SEC, FACTOR)
C   WRITE OUTPUT TAPE 6, 100, FACTOR
C
C 100 FORMAT(1H1/1H015X,8H RESULTS/1H010X,24H ORIGINAL UNIT = BTU/SEC/1H
1010X,28H DESIRED UNIT = (FT*LB)/SEC/1H010X,20H CONVERSION FACTOR
2= E12.5)
C
C   CALL EXIT
C   END
```

RESULTS

ORIGINAL UNIT = BTU/SEC

DESIRED UNIT = (FT*LB)/SEC

CONVERSION FACTOR = 0.77820E 03

```
CCCNVRT      CONTROL PROGRAM FOR SUBROUTINE CONVRT (CCNVRT)
C
C   CASE2 ... THE UNITS ARE INTRODUCED AS INPUT DATA
C   PROBLEM ... FIND A CONVERSION FACTOR FOR A UNIT CONVERSION
C               FROM CENTI POISE(CP) TO LB/(FT-HR)
C
C   DIMENSION UNIT1(30),UNIT2(30)
C   N=12
C   READ INPUT TAPE 5, 100, (UNIT1(I),I=1,N)
C   READ INPUT TAPE 5, 100, (UNIT2(I),I=1,N)
C   CALL CONVRT(N,UNIT1,UNIT2,FACTOR)
C   WRITE OUTPUT TAPE 6, 101, (UNIT1(I),I=1,N),(UNIT2(I),I=1,N),FACTOR
C
100  FORMAT(12A6)
101  FORMAT(1H1/1H015X,8H RESULTS/1H010X,17H ORIGINAL UNIT = 12A6/1H010
      1X,17H DESIRED UNIT = 12A6/1H010X,20H CONVERSION FACTOR = E12.5)
C
      CALL EXIT
      END

*   DATA
      CP
      LB/(FT*HR)
```

RESULTS

ORIGINAL UNIT = CP

DESIRED UNIT = LB/(FT*HR)

CONVERSION FACTOR = 0.24195E 01

```
CCLNPLT      CONTROL PROGRAM FOR SUBROUTINE LNPLT (CLNPLT)
C
C   PROBLEM ... TO PLOT A DISPERSION GROUP VS. REYNOLDS NUMBER ON
C               A LOG - LOG SCALE
C
C   DIMENSION REYN(200),DISP(200)
C
C   WRITE OUTPUT TAPE 6, 1000
C
C   5 REYN(1)=2500.
C     DO 10 I=2,16
C       REYN(I)=REYN(I-1)+500.0
C   10 CONTINUE
C
C     DO 11 I=17,20
C       REYN(I)=REYN(I-1)+2500.
C   11 CONTINUE
C
C     DO 15 I=1,20
C       TERM=0.63082532*(LOGF(REYN(I))**2)-12.55317450*(LOGF(REYN(I)))+61.
C       125958824
C       DISP(I)=EXP(F(TERM))
C   15 CONTINUE
C
C     DO 20 I=21,40
C       REYN(I)=REYN(I-1)+5000.
C       F=0.0014+0.09*((1./REYN(I))**0.27)
C       DISP(I)=3.57*SQRTF(F)
C   20 CONTINUE
C
C     N=40
C     SYMBOL=1H*
C     CALL LNPLT(N,REYN,DISP,SYMBOL)
C
C   WRITE OUTPUT TAPE 6, 1001
C
C   1000 FORMAT(1H1/1H030X,47H A PLOT OF DISPERSION GROUP VS. REYNOLDS NUMB
C             1ER////)
C   1001 FORMAT(1H060X,16H REYNOLDS NUMBER)
C
C   CALL EXIT
C   END
```

The figure consists of two vertically stacked plots sharing a common X-axis labeled 'REYNOLDS NUMBER' with values 1.0E 03, 2, 3, 4, 5, 6, 7, 1.0E 04, 2, 3, 4, 5, 6, 7, 1.0E 05, 2, 3, 4, 5, 6, 7, 1.0E 06. The Y-axis for both plots ranges from 1.0E 01 at the top to 1.0E 00 at the bottom, with intermediate labels at 9.0E 00, 8.0E 00, 7.0E 00, 6.0E 00, 5.0E 00, 4.0E 00, 3.0E 00, 2.0E 00, 1.0E 00, 9.0E-01, 8.0E-01, 7.0E-01, 6.0E-01, 5.0E-01, 4.0E-01, 3.0E-01, 2.0E-01, and 1.0E-01.

Top Plot Data (Approximate):

Reynolds Number	Y-axis Value
1.0E 03	1.0E 01
2	1.0E 01
3	1.0E 01
4	1.0E 01
5	1.0E 01
6	1.0E 01
7	1.0E 01
1.0E 04	1.0E 01
2	1.0E 01
3	1.0E 01
4	1.0E 01
5	1.0E 01
6	1.0E 01
7	1.0E 01
1.0E 05	1.0E 01
2	1.0E 01
3	1.0E 01
4	1.0E 01
5	1.0E 01
6	1.0E 01
7	1.0E 01
1.0E 06	1.0E 01

Bottom Plot Data (Approximate):

Reynolds Number	Y-axis Value
1.0E 03	1.0E 01
2	1.0E 01
3	1.0E 01
4	1.0E 01
5	1.0E 01
6	1.0E 01
7	1.0E 01
1.0E 04	1.0E 01
2	1.0E 01
3	1.0E 01
4	1.0E 01
5	1.0E 01
6	1.0E 01
7	1.0E 01
1.0E 05	1.0E 01
2	1.0E 01
3	1.0E 01
4	1.0E 01
5	1.0E 01
6	1.0E 01
7	1.0E 01
1.0E 06	1.0E 01

```

CCLAGIN          CONTROL PROGRAM FOR SUBROUTINE LAGINT(CLAGIN)
C
C  PROBLEM ... FIND MASS RATES FROM PRESSURE DROP DATA IN AN ORIFICE
C                MANOMETER BY AN INTERPOLATION OF CALIBRATION CURVE
C                (SEE TEXT FOR NUMERICAL VALUES)
C
C  DIMENSION PDROP(20),RATE(20),PDROPV(20),RATEV(20)
C
C  READ INPUT TAPE 5, 100, N,(PDROP(I),I=1,N)
C  READ INPUT TAPE 5, 101, (RATE(I),I=1,N)
C  READ INPUT TAPE 5, 100, NV,(PDROPV(I),I=1,NV)
C
C  CALL LAGINT(N,PDROP,RATE,NV,PDROPV,RATEV)
C
C  WRITE OUTPUT TAPE 6, 102
C  WRITE OUTPUT TAPE 6, 103, (PDROP(I),RATE(I),I=1,N)
C  WRITE OUTPUT TAPE 6, 104
C  WRITE OUTPUT TAPE 6, 103, (PDROPV(I),RATEV(I),I=1,NV)
C
100 FORMAT(I4/(12F5.1))
101 FORMAT(12F5.2)
102 FORMAT(1H1/1H010X,20H    CALIBRATION TABLE/1H012X,18H PRESSURE
103     1MASS/15X,16H DROP      RATE/)
103 FORMAT(15X,F5.1,6X,F5.2)
104 FORMAT(////1H017X,8H RESULTS/1H012X,18H PRESSURE      MASS/15X,16H
105     1DROP      RATE/)
C
C  CALL EXIT
C  END

```

```

*  DATA
7
1.0  2.0  3.0  4.0  5.0  6.0  7.0
1.32 1.87 2.29 2.64 2.96 3.23 3.49
4
1.5  3.5  4.0  5.5

```

CALIPRATION TABLE

PRESSURE	MASS
DROP	RATE
1.0	1.32
2.0	1.87
3.0	2.29
4.0	2.64
5.0	2.96
6.0	3.23
7.0	3.49

RESULTS

PRESSURE	MASS
DROP	RATE
1.5	1.61
3.5	2.47
4.0	2.64
5.5	3.10

CCGAUSS CONTROL PROGRAM FOR SUBROUTINE GAUSS (CGAUSS)

```

C
C   PROBLEM ... COMPUTE THE RATE OF PRODUCT(P),WASTE(W), AND AIR
C   LEAVING ABSORBER (A) IN AN ACETONE RECOVERY SYSTEM
C   (FOR EQUATIONS, SEE TEXT)
C
C   DIMENSION COECNT(50,51),X(50)
C
C   READ INPUT TAPE 5, 100, M,((COECNT(I,J),J=1,M),I=1,M)
5  READ INPUT TAPE 5, 101, F
C
C   N=M+1
C   COECNT(1,N)=F*0.0295
C   COECNT(2,N)=120.
C   COECNT(3,N)=F*0.9705
C
C   CALL GAUSS(M,COECNT,X)
C
C   P=X(1)
C   W=X(2)
C   A=X(3)
C
C   WRITE OUTPUT TAPE 6, 102, F
C   WRITE OUTPUT TAPE 6, 103, ((COECNT(I,J),J=1,N),I=1,M)
C   WRITE OUTPUT TAPE 6, 104, P,W,A
C
100 FORMAT(I4/(3F5.2))
101 FORMAT(F10.0)
102 FORMAT(1H1/1H010X,21H THE RATE OF FEED IS F9.0,7H LB/HR. )
103 FORMAT(1H0/1H010X,23H ORIGINAL EQUATIONS ARE//(16X,F5.2,7H * P +
1F5.2,7H * W + F5.2,7H * A = F8.1))
104 FORMAT(1H0/1H010X,19H RESULTS (IN LB/HR)/1H015X,3H P=F8.1/16X,3H W
1=F8.1/16X,3H A=F8.1)
C
C   GO TO 5
C   END

```

* DATA

```

3
0.99 0.05 0.00
0.01 0.95 0.00
0.00 0.00 1.00
50000.0

```

THE RATE OF FEED IS 50000. LB/HR.

ORIGINAL EQUATIONS ARE

$$\begin{array}{rcll} 0.99 \bullet P + 0.05 \bullet W + 0. & \bullet A = & 1475.0 \\ 0.01 \bullet P + 0.95 \bullet W + 0. & \bullet A = & 120.0 \\ 0. & \bullet P + 0. & \bullet W + 1.00 \bullet A = & 48525.0 \end{array}$$

RESULTS (IN LB/HR)

$$\begin{array}{l} P = 1484.3 \\ W = 110.7 \\ A = 48525.0 \end{array}$$

```

CCLEASQ          CONTROL PROGRAM FOR SUBROUTINE LEASQU (CLEASQ)
C
C   PROBLEM ... FIND A STRAIGHT LINE FORMULA WHICH WILL BEST FIT THE
C                   DATA OBTAINED IN A CALIBRATION EXPERIMENT OF A FLOW
C                   METER
C                   (SEE TEXT FOR NUMERICAL VALUES)
C
C   DIMENSION READNG(200),OBSRVD(200),C(50)
C
C   READ INPUT TAPE 5, 100, N,(READNG(I),I=1,N)
C   READ INPUT TAPE 5, 101, (OBSRVD(I),I=1,N)
C
C   MDEGRE=1
C   CALL LEASQU(N,READNG,OBSRVD,MDEGRE,C)
C
C   WRITE OUTPUT TAPE 6, 102
C   WRITE OUTPUT TAPE 6, 103, (READNG(I),OBSRVD(I),I=1,N)
C   WRITE OUTPUT TAPE 6, 104, C(1),C(2)
C
C   100 FORMAT(I4/(12F6.1))
C   101 FORMAT(12F6.1)
C   102 FORMAT(1H1/1H012X,18H CALIBRATION TABLE/1H010X,22H READINGS      OB
C             1SERVED/13X,19H (GPH)          (GPH)//)
C   103 FORMAT(12X,F6.1,7X,F6.1)
C   104 FORMAT(1H0/1H0/1H015X,7H RESULT/1H010X,14H FLOW RATE = (E12.5,15H)
C             1 * READING + (E12.5,1H)  )
C
C   CALL EXIT
C   END

```

* DATA

10										
20.0	30.0	40.0	50.0	60.0	70.0	80.0	90.0	100.0	120.0	
19.8	29.7	39.7	49.6	60.2	70.3	80.2	90.0	102.5	120.5	

CALIBRATION TABLE

READINGS (GPH)	OBSERVED (GPH)
20.0	19.8
30.0	29.7
40.0	39.7
50.0	49.6
60.0	60.2
70.0	70.3
80.0	80.2
90.0	90.0
100.0	102.5
120.0	120.5

RESULT

FLOW RATE = (0.10161E 01) * READING + (-0.81428E 00)

```

CCMTMPY          CONTROL PROGRAM FOR SUBROUTINE MATMPY (CMTMPY)
C
C   PROBLEM ... FIND THE PRODUCT OF TWO MATRICES, A AND B
C                   (SEE TEXT FOR NUMERICAL VALUES)
C
C   DIMENSION A(50,51),B(50,51),C(50,51)
C
C   READ INPUT TAPE 5, 100, N
C   READ INPUT TAPE 5, 101, ((A(I,J),J=1,N),I=1,N)
C   READ INPUT TAPE 5, 101, ((B(I,J),J=1,N),I=1,N)
C
C   CALL MATMPY(N,A,B,C)
C
C   WRITE OUTPUT TAPE 6, 102, ((A(I,J),J=1,N),I=1,N)
C   WRITE OUTPUT TAPE 6, 103, ((B(I,J),J=1,N),I=1,N)
C   WRITE OUTPUT TAPE 6, 104, ((C(I,J),J=1,N),I=1,N)
C
C   100 FORMAT(I4)
C   101 FORMAT(4F10.5)
C   102 FORMAT(1H1/1H010X,18H ORIGINAL MATRICES/1H010X,5H A = 4F10.5/(16X,
C   14F10.5))
C   103 FORMAT(1H0/1H010X,5H B = 4F10.5/(16X,4F10.5))
C   104 FORMAT(////1H012X,7H RESULT/1H010X,19H THE PRODUCT MATRIX/1H010X,5
C   1H C = 4F10.5/(16X,4F10.5))
C
C   CALL EXIT
C   END

```

DATA

```

4
8.467      5.137      3.141      2.063
5.137      6.421      2.617      2.003
3.141      2.617      4.128      1.628
2.063      2.003      1.628      3.446
0.25087    -0.16214    -0.08116    -0.01760
-0.16214    0.33074    -0.05994    -0.06686
-0.08116    -0.05994    0.37988     -0.09604
-0.01760    -0.06686    -0.09604     0.38497

```

ORIGINAL MATRICES

A = 8.46700 5.13700 3.14100 2.06300
 5.13700 6.42100 2.61700 2.00300
 3.14100 2.61700 4.12800 1.62800
 2.06300 2.00300 1.62800 3.44600

B = 0.25087 -0.16214 -0.08116 -0.01760
 -0.16214 0.33074 -0.05994 -0.06686
 -0.08116 -0.05994 0.37988 -0.09604
 -0.01760 -0.06686 -0.09604 0.38497

RESULT

THE PRODUCT MATRIX

C = 0.99997 -0.00003 -0.00002 0.00005
 -0.00003 0.99998 -0.00002 0.00004
 -0.00002 -0.00002 1.00000 0.00002
 0.00000 -0.00000 -0.00000 1.00002

```

CCMTINV          CONTROL PROGRAM FOR SUBROUTINE MATINV (CMTINV)
C
C   PROBLEM ... INVERT MATRIX A
C               (SEE TEXT FOR NUMERICAL VALUES)
C
C   DIMENSION A(50,51),B(50,51)
C
C   READ INPUT TAPE 5, 100, N, ((A(I,J),J=1,N),I=1,N)
C
C   CALL MATINV(N,A,B)
C
C   WRITE OUTPUT TAPE 6, 101, ((A(I,J),J=1,N),I=1,N)
C   WRITE OUTPUT TAPE 6, 102, ((B(I,J),J=1,N),I=1,N)
C
C   100 FORMAT(I4/(4F8.5))
C   101 FORMAT(1H1/1H010X,16H ORIGINAL MATRIX/1H010X,5H A = 4F10.5/(16X,4F
C       110.5))
C   102 FORMAT(/////1H012X,7H RESULT/1H010X,15H INVERSE MATRIX/1H010X,5H B
C       1= 4F10.5/(16X,4F10.5))
C
C   CALL EXIT
C   END

```

* DATA

4			
8.467	5.137	3.141	2.063
5.137	6.421	2.617	2.003
3.141	2.617	4.128	1.628
2.063	2.003	1.628	3.446

ORIGINAL MATRIX

A =	8.46700	5.13700	3.14100	2.06300
	5.13700	6.42100	2.61700	2.00300
	3.14100	2.61700	4.12800	1.62800
	2.06300	2.00300	1.62800	3.44600

RESULT

INVERSE MATRIX

B =	0.25087	-0.16214	-0.08116	-0.01760
	-0.16214	0.33074	-0.05994	-0.06686
	-0.08116	-0.05994	0.37988	-0.09604
	-0.01760	-0.06686	-0.09604	0.38497

```

CCSMPSN          CONTROL PROGRAM FOR SUBROUTINE SIMPSN (CSMPSN)
C
C   PROBLEM ... FIND AN AREA UNDER THE CONCENTRATION CURVE OBTAINED
C                   BY LEVENSPIEL AND SMITH IN THEIR DISPERSION EXPERIMENT
C                   (SEE TEXT FOR CONCENTRATION DATA)
C                   ALSO, COMPUTE DIMENSIONLESS VARIANCE WHICH WILL BE
C                   USED TO DETERMINE A DISPERSION COEFFICIENT.
C                   SOME OTHER NECESSARY DATA ARE
C                   VELOCITY = 1.17 FT/SEC
C                   LENGTH   = 9.0 FT
C
C   DIMENSION CONC(200),TIME(200),TCONC(200),TSQCON(200)
C
C   READ INPUT TAPE 5, 100, N,VEL,AL
C   READ INPUT TAPE 5, 101, (TIME(I),I=1,N)
C   READ INPUT TAPE 5, 102, (CONC(I),I=1,N)
C
C   H=TIME(2)-TIME(1)
C
C   CALL SIMPSN(N,CONC,H,AREA)
C
C   DO 10 I=1,N
C     TCONC(I)=TIME(I)*CONC(I)
C     TSQCON(I)=TIME(I)**2*CONC(I)
10  CONTINUE
C
C   CALL SIMPSN(N,TCONC,H,FIRSTM)
C
C   CALL SIMPSN(N,TSQCON,H,SECNDM)
C
C   VAR=(SECNDM/AREA-((FIRSTM/AREA)**2))*((VEL/AL)**2)
C
C   WRITE OUTPUT TAPE 6, 103, VEL,AL
C   WRITE OUTPUT TAPE 6, 104, (TIME(I),CONC(I),I=1,N)
C   WRITE OUTPUT TAPE 6, 105, AREA,VAR
C
100  FORMAT(I4,2F5.2)
101  FORMAT(14F5.1)
102  FORMAT(7F10.5)
103  FORMAT(1H1/1H010X,18H EXPERIMENTAL DATA/1H012X,11H VELOCITY =F5.2,
17H FT/SEC/13X,11H LENGTH   =F5.2,3H FT/1H0/1H013X,14H TIME      CON
2C//)
104  FORMAT(14X,F5.1,4X,F5.1)
105  FORMAT(////1H010X,8H RESULTS/1H010X,30H AREA UNDER THE CONC. CURVE
1 = E12.5/1H010X,30H DIMENSIONLESS VARIANCE      = E12.5)
C
C   CALL EXIT
C   END
C
*   DATA
22  1.17 9.00
0.0  2.0  4.0  6.0  8.0 10.0 12.0 14.0 16.0 18.0 20.0 22.0 24.0 26.0
28.0 30.0 32.0 34.0 36.0 38.0 40.0 42.0
0.00000 11.00000 53.00000 64.00000 58.00000 48.00000 39.00000
29.00000 22.00000 16.00000 11.00000 9.00000 7.00000 5.00000
4.00000 2.00000 2.00000 2.00000 1.00000 1.00000 1.00000
1.00000

```

EXPERIMENTAL DATA

VELOCITY = 1.17 FT/SEC
LENGTH = 9.00 FT

TIME	CONC
0.	0.
2.0	11.0
4.0	53.0
6.0	64.0
8.0	58.0
10.0	48.0
12.0	39.0
14.0	29.0
16.0	22.0
18.0	16.0
20.0	11.0
22.0	9.0
24.0	7.0
26.0	5.0
28.0	4.0
30.0	2.0
32.0	2.0
34.0	2.0
36.0	1.0
38.0	1.0
40.0	1.0
42.0	1.0

RESULTS

AREA UNDER THE CONC. CURVE = 0.76400E 03

DIMENSIONLESS VARIANCE = 0.79132E 00

```

CCRUNMO      CONTROL PROGRAM FOR SUBROUTINE RUNMOD (CRUNMO)
C
C      PROBLEM ... FIND THE CONCENTRATION OF SALT IN A MIXING TANK AS
C      A FUNCTION OF TIME
C      (SEE TEXT FOR THE STATEMENT OF PROBLEM)
C
C      DIMENSION TIME(200),CONC(200)
C
C      N=181
C      H=1.0
C      TIME(1)=0.0
C      CONC(1)=0.0
C
C      CALL RUNMOD(N,TIME,CONC,H)
C
C      WRITE OUTPUT TAPE 6, 100
C      WRITE OUTPUT TAPE 6, 101, (TIME(I),CONC(I),I=1,N)
C
100 FORMAT(1H1/1H015X,20H MIXING TANK PROBLEM/1H010X, 14H SALT 2 LB/GA
1L/14X,18H 5 GAL/MIN -----+/30X,2H I/27X,5H I I,7X,2H I/27X,5H I
2 I,7X,2H I/27X,2H I,10X,2H I/27X,14H I-----I/27X,14H I V0=10
30GAL I/27X,2H I,4X,2H C,4X,8H I-----+/27X,14H -----4X,2H I
4/45X,2H I/43X,9H C LB/GAL/42X,10H 1 GAL/MIN////1H021X,7H RESULT/1H
5017X,5H TIME7X,5H CONC/18X,6H (MIN),4X,9H (LB/GAL)//)
101 FORMAT(17X,F6.1,5X,F9.5)
C
C      CALL EXIT
C      END

```

```

C      FUNCTION RPROGRAM FOR MIXING TANK PROBLEM
C
C      FUNCTION FUNCT(TIME,CONC)
C
C      FUNCT=(10.-5.0*CONC)/(100.0+4.0*TIME)
C
C      RETURN
C      END

```

MIXING TANK PROBLEM

SALT 2 LB/GAL

5 GAL/MIN -----+

```

      I
    I  I      I
    I  I      I
    I      I
    I-----I
    I VC=1CCGAL I
    I      C      I-----+
    -----
                        I
                        I
                    C LB/GAL
                    1 GAL/MIN

```

RESULT

TIME (MIN)	CONC (LB/GAL)
0.	0.
1.0	0.09569
2.0	0.18344
3.0	0.26417
4.0	0.33866
5.0	0.40760
6.0	0.47154
7.0	0.53101
8.0	0.58645
9.0	0.63822
10.0	0.68668
11.0	0.73212
12.0	0.77481
13.0	0.81498
14.0	0.85284
15.0	0.88858
16.0	0.92236
17.0	0.95433
18.0	0.98464
19.0	1.01340
20.0	1.04073
21.0	1.06673
22.0	1.09148
23.0	1.11508
24.0	1.13760
25.0	1.15910
26.0	1.17966
27.0	1.19933
28.0	1.21817
29.0	1.23623
30.0	1.25355
31.0	1.27017
32.0	1.28614
33.0	1.30149

34.0	1.31626
35.0	1.33048
36.0	1.34417
37.0	1.35736
38.0	1.37009
39.0	1.38237
40.0	1.39422
41.0	1.40567
42.0	1.41674
43.0	1.42744
44.0	1.43780
45.0	1.44782
46.0	1.45752
47.0	1.46692
48.0	1.47604
49.0	1.48487
50.0	1.49344
51.0	1.50176
52.0	1.50984
53.0	1.51768
54.0	1.52530
55.0	1.53270
56.0	1.53990
57.0	1.54691
58.0	1.55372
59.0	1.56035
60.0	1.56681
61.0	1.57309
62.0	1.57922
63.0	1.58519
64.0	1.59100
65.0	1.59668
66.0	1.60221
67.0	1.60761
68.0	1.61287
69.0	1.61801
70.0	1.62303
71.0	1.62794
72.0	1.63272
73.0	1.63740
74.0	1.64198
75.0	1.64645
76.0	1.65082
77.0	1.65509
78.0	1.65927
79.0	1.66336
80.0	1.66736
81.0	1.67128
82.0	1.67512
83.0	1.67887
84.0	1.68255
85.0	1.68615
86.0	1.68968
87.0	1.69314
88.0	1.69653
89.0	1.69986
90.0	1.70312
91.0	1.70631
92.0	1.70945
93.0	1.71252

94.0	1.71554
95.0	1.71850
96.0	1.72140
97.0	1.72426
98.0	1.72705
99.0	1.72980
100.0	1.73250
101.0	1.73515
102.0	1.73776
103.0	1.74032
104.0	1.74283
105.0	1.74530
106.0	1.74773
107.0	1.75011
108.0	1.75246
109.0	1.75477
110.0	1.75704
111.0	1.75927
112.0	1.76146
113.0	1.76362
114.0	1.76574
115.0	1.76783
116.0	1.76989
117.0	1.77191
118.0	1.77391
119.0	1.77587
120.0	1.77780
121.0	1.77970
122.0	1.78157
123.0	1.78341
124.0	1.78523
125.0	1.78702
126.0	1.78878
127.0	1.79051
128.0	1.79222
129.0	1.79391
130.0	1.79557
131.0	1.79721
132.0	1.79882
133.0	1.80041
134.0	1.80198
135.0	1.80352
136.0	1.80505
137.0	1.80655
138.0	1.80803
139.0	1.80950
140.0	1.81094
141.0	1.81236
142.0	1.81376
143.0	1.81515
144.0	1.81651
145.0	1.81786
146.0	1.81919
147.0	1.82051
148.0	1.82180
149.0	1.82308
150.0	1.82434
151.0	1.82559
152.0	1.82682
153.0	1.82804

154.0	1.82924
155.0	1.83042
156.0	1.83159
157.0	1.83275
158.0	1.83389
159.0	1.83502
160.0	1.83613
161.0	1.83723
162.0	1.83832
163.0	1.83939
164.0	1.84045
165.0	1.84150
166.0	1.84254
167.0	1.84356
168.0	1.84458
169.0	1.84558
170.0	1.84657
171.0	1.84754
172.0	1.84851
173.0	1.84947
174.0	1.85041
175.0	1.85135
176.0	1.85227
177.0	1.85318
178.0	1.85409
179.0	1.85498
180.0	1.85586

References:

- 1) Hamming, R. W., "Numerical Methods for Scientists and Engineers", McGraw-Hill (1962)
- 2) Hildebrand, F. B., "Introduction to Numerical Analysis", McGraw-Hill (1956)
- 3) Himmelblau, D. M., "Basic Principles and Calculations in Chemical Engineering", Prentice-Hall (1964)
- 4) Lapidus, L., "Digital Computation for Chemical Engineers", McGraw-Hill (1962)
- 5) Mickley, H. S., T. K. Sherwood, and C. E. Reed, "Applied Mathematics in Chemical Engineering" McGraw-Hill (1957)
- 6) Perry, J. H. ed., "Chemical Engineers' Handbook" 3rd edition McGraw-Hill (1950)
- 7) Ralston, A., and H. S. Wilf, "Mathematical Methods for digital Computers", Wiley (1962)
- 8) Richtmyer, R. D., "Difference Methods for Initial-Value Problems", Interscience (1962)