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GAROL

A COMPUTER PROGRAM FOR EVALUATING RESONANCE
ABSORPTION INCLUDING RESONANCE OVERLAP

by

C. A. Stevens and C. V. Smith

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August 24, 1965

The GAROL computer code is described herein as it existed on August 24, 1965 .

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ABSTRACT

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A computer program, GAROL, has been written to study resonance absorption. The program is an improvement over other programs, presently in use, by virtue of its ability to handle overlap effects between resonances of a resonance absorber and of mixtures of resonance absorbers. In addition, a wide choice of geometry, energy mesh spacings, and cross section representation is available to the user.

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INTRODUCTION

Resonance absorption is a subject of considerable interest to designers of nuclear reactors. Accordingly, a considerable amount of work has been done in this area. For a good, up-to-date, summary the reader is referred to the work of Nordheim.⁽¹⁾

One of the assumptions which has been included in most treatments of resonance absorption is that, in a mixture of resonance absorbers, the total absorption may be obtained by summing the absorptions in each resonance of each nuclide, each being computed as if the other resonances were not present. The GAROL computer program does not make this assumption; it explicitly takes into account those effects which arise from resonance overlap of an individual resonance absorber and of mixtures of different resonance absorbers. It is conventional to consider the problem as a lattice of absorber imbedded in a purely scattering medium in which the flux is taken to be $\frac{1}{E}$. Thus the flux dips in the scattering medium due to absorptions in the lump are neglected. For tight lattices, this approximation can be poor. The GAROL program does not make this assumption; it solves two coupled integral equations for the fluxes in each region.

It is in these respects that this work represents an improvement over other computer programs used for computing resonance absorption; see for instance reference (2).

DESCRIPTION OF THE GAROL PROGRAM

General Features

The GAROL computer program is quite versatile. It allows an unlimited number of energy points, with flexibility regarding the layout of the mesh. The mesh may be chosen at equal energy or lethargy intervals; it may be chosen to be proportional to the neutron velocity ($\Delta E \sim \sqrt{E}$), or it may be an arbitrary table of mesh points. The program allows a choice of geometries: homogeneous, cylindrical, plane, spherical, or it can accept an arbitrary table of escape probabilities. Regardless of the geometry, a Dancoff correction may be used to account for shadowing effects in a tight lattice. The program can accommodate a mixture of up to ten isotopes. A cross section tape generated in a GAROL run can be used again in subsequent runs, thus allowing a saving of computer time. Cross sections may be $\frac{1}{v}$, constant, computed from single level Breit-Wigner resonance parameters, or they may be given in tabular form.

The output includes integrated fluxes over desired energy bands, for each region and for the cell. It contains average microscopic cross sections for capture, fission, and scattering for each isotope, for each region and for the cell. At the user's option, one can obtain pointwise values for the flux, source, total cross section, and collision density $[E\Sigma_t(E)\phi(E)]$ for each region. Also at the user's option, he may obtain graphical results, automatically generated on an electronic plotter.

Equations to be Solved

Consider a lattice of absorber lumps, denoted by the index 1, imbedded in another medium, not necessarily a pure scatterer, which is denoted by index 2. The average flux in the two media may be obtained as the solutions of the integral equation

$$\begin{aligned} V_1 \Sigma_{T1} \phi_1(E) = & (1 - P_1) V_1 \sum_{i=1}^M \frac{N_{1i}}{1 - \alpha_i} \int_E^{E/\alpha_i} \frac{\sigma_{s1}(E')}{E'} \phi_1(E') dE' \\ & + P_2 V_2 \sum_{i=1}^M \frac{N_{2i}}{1 - \alpha_i} \int_E^{E/\alpha_i} \frac{\sigma_{s1}(E')}{E'} \phi_2(E') dE' \\ & + V_1 (1 - P_1) Q_1(E) + V_2 P_2 Q_2(E) \end{aligned} \quad (1)$$

and another one just like it, but with the subscripts 1 and 2 reversed. The notation of Equation (1) is as follows:

V_k is the volume of region k.

$\Sigma_{tk}(E)$ is the total macroscopic cross section of region k.

$\phi_k(E)$ is the average flux in region k.

P_k is the escape probability from region k.

N_{ki} is the number density of isotope i in region k.

$\sigma_{si}(E')$ is the microscopic scattering cross section of isotope i.

$\alpha_i = \left(\frac{A_i - 1}{A_i + 1} \right)^2$, where A_i is the atomic weight of isotope i.

$Q_k(E)$ = source in region k.

We wish to restrict the energy range of interest to the interval (E_1, E_N) , with $E_1 > E_N$, such that below E_1 , we may ignore such high energy processes as inelastic scattering, anisotropic scattering in the center of mass coordinate system, and birth of neutrons from fission. In fact, we would like this to be true even for an energy range above E_1 so that in the absence of absorption in that range, we would have a $1/E$ flux. Above E_N , we assume that the velocity of the neutrons is sufficiently large so that the scattering kernel may be obtained from the mechanics of neutrons colliding with free and stationary atoms. In other words, upscattering and binding effects may be ignored, as is already implied by Equation (1).

By use of the Heaviside function $H(x)$, defined by

$$\begin{aligned} H(x) &= 1 \quad \text{for } x \geq 0 \\ &= 0 \quad \text{for } x < 0, \end{aligned}$$

we can rewrite Equation (1) in a more convenient form,

$$\begin{aligned}
V_1 \Sigma_{T1} \varphi_1(E) = & (1 - P_1) V_1 \sum_{i=1}^M \frac{N_{1i}}{1 - \alpha_i} \int_E^{E_1} \frac{\sigma_{si}(E')}{E'} H(E - \alpha_i E') \varphi_1(E') dE' \\
& + P_2 V_2 \sum_{i=1}^M \frac{N_{2i}}{1 - \alpha_i} \int_E^{E_1} \frac{\sigma_{si}(E')}{E'} H(E - \alpha_i E') \varphi_2(E') dE' \quad (2) \\
& + V_1 (1 - P_1) S_1(E) + V_2 P_2 S_2(E),
\end{aligned}$$

where we have removed the direct sources Q_k , and where

$$S_k(E) = \sum_{i=1}^M \frac{N_{ki}}{1 - \alpha_i} \int_{E_1}^{E/\alpha_i} \frac{\sigma_{si}(E')}{E'} H(E - \alpha_i E') \varphi_k(E') dE' \quad (3)$$

If we assume that in the interval $(E_1, E_1/\alpha)$ the flux has the magnitude $1/E$, that it is spatially flat and isotropic, and that the scattering cross section is independent of energy, we can easily evaluate the integral in Equation (3) to obtain

$$S_k(E) = \sum_{i=1}^M \frac{N_{ki} \sigma_{si}}{1 - \alpha_i} \left(\frac{1}{E_1} - \frac{\alpha_i}{E} \right) H(E - \alpha_i E_1) \quad (4)$$

The quantity $S_k(E)$ may now be considered as an external source which is normalized so that

$$\int_0^{E_1} S_k(E) dE = \sum_{i=1}^M \frac{N_{ki} \sigma_{si}}{1 - \alpha_i} \int_{\alpha E_1}^{E_1} \left(\frac{1}{E_1} - \frac{\alpha_i}{E} \right) dE = \sum_{i=1}^M N_{ki} \sigma_{si} \xi_i \quad (5)$$

where ξ_i is the usual

$$\xi_i = 1 + \frac{\alpha_i}{1 - \alpha_i} \ln \alpha_i \quad (6)$$

From Equation (5), we see that the integrated source from each isotope is proportional to $\sigma_s \xi$ for that isotope. In addition to this source, another source of arbitrary energy dependence may be superposed on it by the user of the GAROL program.

Collision Probabilities

The manner by which the collision probabilities ($1.0 - P_k$) are computed is based upon the frequently used assumption that they may be computed for a flat source in each region. For standard geometries, these are obtained directly from Case, de Hoffmann, and Placzek.⁽³⁾ For more complicated geometries it is possible to generate collision probabilities by other means, usually with one velocity transport theory solutions, and to use these directly in the GAROL program.

The collision probabilities for the two regions are related in a very simple manner. In order to see this, let $G(x, x')$ be the flux at the point x due to a unit source at point x' in a one velocity problem. The well known reciprocity theorem⁽³⁾ states that

$$G(x, x') = G(x', x) \quad (7)$$

If we consider a two region problem in which region 1 has a source $S_1(x)$, the total flux at any point x will be

$$\varphi(x) = \int_{V_1} S_1(x') G(x, x') d^3x'$$

where V_1 denotes that the integral is carried out over region 1.

The collision rate in region 2, which is equal to the escape rate from region 1 since all collisions effectively remove neutrons from the velocity of interest, is

$$\int_{V_2} \Sigma_{t2} \varphi(x) d^3x = \int_{V_2} d^3x \int_{V_1} d^3x' \Sigma_{t2}(x) S_1(x') G(x, x')$$

The escape probability is given by

$$P_1 = \frac{\int_{V_2} \Sigma_{t2} \varphi(x) d^3x}{\int_{V_1} S_1(x) d^3x} = \frac{\int_{V_2} d^3x \int_{V_1} d^3x' \Sigma_{t2}(x) S_1(x') G(x, x')}{\int_{V_1} S_1(x) d^3x} \quad (10)$$

If Σ_{t2} and S_1 are constants, the escape probability becomes

$$P_1 = \frac{\Sigma_{t2} \int_{V_2} d^3x \int_{V_1} d^3x' G(x, x')}{V_1} \quad (11)$$

or

$$\int_{V_2} d^3x \int_{V_1} d^3x' G(x, x') = \frac{P_1 V_1}{\Sigma_{t2}} \quad (12)$$

In exactly the same way, we obtain

$$\int_{V_1} d^3x \int_{V_2} d^3x' G(x, x') = \int_{V_2} d^3x \int_{V_1} d^3x' G(x', x) = \frac{P_2 V_2}{\Sigma_{t1}} \quad (13)$$

Now, by using the reciprocity relation, Equation (7), and comparing Equations (12) and (13), we obtain

$$P_1 V_1 \Sigma_{t1} = P_2 V_2 \Sigma_{t2} \quad (14)$$

So, once P_1 has been computed, P_2 may be obtained simply by use of Equation (14).

The escape probabilities in the GAROL program are computed from the flat source assumption. For the simple geometries, these have been developed by Case, et. al.⁽³⁾ We summarize their results as they are applicable to the GAROL program.

Let $\bar{\ell}_1$ denote the mean chord length of region 1, and Σ_{t1} be the total macroscopic cross section in the region.

For a sphere of radius r :

$$r = \frac{3}{4} \bar{\ell}_1 \quad (15)$$

With $x = r \Sigma_{t1}$, we have for

$$x \leq 0.02$$

$$P_1(x) = 1 - \frac{3x}{4} \quad (16)$$

$$\underline{0.02 < x < 5.0}$$

$$P_1(x) = \frac{3}{8x^3} [2x^2 - 1 + (1 + 2x)e^{-2x}] \quad (17)$$

$$\underline{x \geq 5.0}$$

$$P_1(x) = \frac{3}{4x} [1 - \frac{1}{2x^2}] \quad (18)$$

For an infinite cylinder with radius r :

$$r = \frac{\bar{l}_1}{2} \quad (19)$$

With $x = r\Sigma_{t1}$, we have for

$$\underline{x < 0.1}$$

$$P_1(x) = 1 - \frac{4x}{3} + \frac{x^2}{2} \ln \frac{2}{x} + \frac{x^2}{2} (\frac{5}{4} - \gamma) \quad (20)$$

in which Euler's constant $\gamma = 0.577216 \dots$

$$\underline{0.1 \leq x \leq 6.0}$$

Interpolation from tables.

$$\underline{x \geq 6.0}$$

$$P_1(x) = \frac{1}{2x} - \frac{3}{32x^3} \quad (21)$$

For a slab of half thickness a :

$$a = \frac{\bar{l}_1}{4} \quad (22)$$

With $x = a\Sigma_{t1}$, we have for

$$\underline{x < 0.05}$$

$$P_1(x) = 1 - x \ln \frac{1}{2x} - x(\frac{3}{2} - \gamma) - \frac{2x^2}{3} \quad (23)$$

again with $\gamma = 0.577216 \dots$

$$\underline{0.05 \leq x \leq 5.0}$$

Interpolation from tables.

$$\underline{x > 5.0}$$

$$P_1(x) = \frac{1}{4x} \quad (24)$$

For an arbitrary geometry:

$$\text{with } x = \frac{\bar{\ell}_1 \Sigma_{t1}}{2}$$

we use for

$$\underline{0.0 \leq x \leq 6.0}$$

Interpolation from tables which are supplied by the user.

$$\underline{x \geq 6.0}$$

$$P_1(x) = \frac{C_1}{x} + \frac{C_2}{x^2} + \frac{C_3}{x^3} \quad (25)$$

in which the constants C_1 , C_2 , and C_3 are supplied by the user.

A Dancoff correction factor, C , can be applied for tight lattice calculations. It is used to modify the escape probability P_1 by the formula

$$P_1^* = P_1 \frac{1 - C}{1 - (1 - \Sigma_t \bar{\ell}_1 P_1) C} \quad (26)$$

where $\bar{\ell}_1$ is the mean chord length of region 1. Equation (26) is due to Nordheim.⁽⁴⁾ It is a good approximation for lumps of any degree of grayness. If region 2 contains cross sections which vary with energy, the factor C depends upon energy. The GAROL program at present allows only one constant number for C , so it should be used with reservation on a tight lattice problem with a variable cross section in region 2.

Cross Sections

Cross sections may be used in a number of ways. These include:

- 1) one number, to represent a $\frac{1}{v}$ capture cross section, or a constant scattering cross section

- 2) a tabulated set of pointwise cross sections
- 3) a set of single level Breit-Wigner parameters, from which the GAROL program computes pointwise cross sections.

If it is desired to have the program compute cross sections from resonance parameters, the following computations are carried out within the computer program.

The cross sections are given by the usual formulae,

$$\sigma_a = \frac{\Gamma_y}{\Gamma} \sqrt{\frac{E_0}{E}} \sigma_0 \psi(\xi, x), \quad (27)$$

$$\sigma_f = \frac{\Gamma_f}{\Gamma} \sqrt{\frac{E_0}{E}} \sigma_0 \psi(\xi, x), \quad (28)$$

$$\sigma_s = \frac{\Gamma_n^0 \sqrt{E_0}}{\Gamma} \sigma_0 \psi(\xi, x) + \left(\sigma_0 \sigma_p g \frac{\Gamma_n^0 \sqrt{E_0}}{\Gamma} \right)^{1/2} \chi(\xi, x) + \sigma_p \quad (29)$$

where

$$\xi = \frac{\Gamma}{\Gamma_D} = \sqrt{\frac{A \Gamma^2}{4 E k T}} \quad (30)$$

is the ratio of the natural width to the Doppler width,

$$\sigma_0 = \frac{2.6 \times 10^6}{\sqrt{E_0}} g \frac{\Gamma_n^0}{\Gamma} \quad (31)$$

is the value of the peak of the total cross section at zero temperature,

$$\Gamma_n = \Gamma_n^0 \sqrt{E} \quad (32)$$

is the neutron width, Γ_n^0 being the reduced neutron width. Γ_y , Γ_f , and Γ are the capture, fission and total widths, respectively. g is the statistical factor,

$$g = \frac{2J + 1}{2(2I + 1)} \quad (33)$$

where I is the nuclear spin and J is the spin of the compound nucleus. σ_p is the potential cross section and the shape functions ψ and χ are given by

$$\psi(\xi, x) = \frac{\xi}{\sqrt{4\pi}} \int_{-\infty}^{\infty} \frac{e^{-(x-y)^2 \xi^2/4}}{1+y^2} dy \quad (34)$$

and

$$\chi(\xi, x) = \frac{2\xi}{\sqrt{4\pi}} \int_{-\infty}^{\infty} \frac{y e^{-(x-y)^2 \xi^2/4}}{1+y^2} dy. \quad (35)$$

x is given by

$$x = \frac{2(E - E_0)}{\Gamma}, \quad (36)$$

E_0 is the position of the center of the resonance, E is the neutron energy and T is the absolute temperature.

The method used to evaluate the shape functions is one devised by Triplett, Merrill, and Burr.⁽⁵⁾

Whenever accuracy permits it, five terms of an asymptotic series expansion are used to evaluate the line shapes.

The asymptotic series for ψ is

$$\psi(x, \xi) = \sum_{k=0}^{\infty} \alpha_k \left(\frac{4}{\xi^2}\right)^k (x^2 + 1)^{-\left(\frac{2k+1}{2}\right)} \sin[(2k+1) \sin^{-1}(x^2 + 1)^{-\frac{1}{2}}] \quad (37)$$

where

$$\alpha_0 = 1$$

$$\alpha_k = \frac{1.3.5 \dots (2k-1)}{2^k}, \quad k=1, 2, \dots \quad (38)$$

From the relation,

$$\chi(x, \xi) = 2x\psi(x, \xi) + \frac{4}{\xi^2} \frac{\partial \psi}{\partial x}(x, \xi) \quad (39)$$

we obtain

$$\chi(x, \xi) = \sum_{k=0}^{\infty} 2\alpha_k \left(\frac{4}{\xi^2}\right)^k (x^2 + 1)^{-\frac{2k+1}{2}} \left\{ \frac{-2(2k+1)}{\xi^2(1+x^2)} \cos[(2k+1)\sin^{-1}(x^2+1)^{-\frac{1}{2}}] \right. \\ \left. + x \left(1 - \frac{2(2k+1)}{\xi^2(1+x^2)} \sin[(2k+1)\sin^{-1}(x^2+1)^{-\frac{1}{2}}] \right) \right\} \quad (40)$$

If we set

$$J_k(x) = (x^2 + 1)^{-\frac{1}{2}} \sin[(2k+1)\sin^{-1}(x^2+1)^{-\frac{1}{2}}] \quad (41)$$

and

$$H_k(x) = (x^2 + 1)^{-\frac{1}{2}} \cos[(2k+1)\sin^{-1}(x^2+1)^{-\frac{1}{2}}], \quad (42)$$

we have

$$\psi(x, \xi) = \sum_{k=0}^{\infty} \alpha_k \left[\frac{4}{\xi^2(x^2+1)} \right]^k J_k(x) \quad (43)$$

and

$$\chi(x, \xi) = \sum_{k=0}^{\infty} 2\alpha_k \left[\frac{4}{\xi^2(x^2+1)} \right]^k x J_k(x) - \frac{2}{\xi^2} \frac{(2k+1)}{(1+x^2)} (x J_k(x) + H_k(x)) \quad (44)$$

By using elementary trigonometric formulae, it can be shown that Equations (41) and (42) are easily evaluated by the recursion equations

$$J_0(x) = \frac{1}{1+x^2} \quad (45)$$

$$H_0(x) = \frac{x}{1+x^2} \quad (46)$$

$$J_{k+1}(x) = \frac{x^2-1}{x^2+1} J_k(x) + \frac{2x}{x^2+1} H_k(x) \quad (47)$$

$$H_{k+1}(x) = \frac{x^2 - 1}{x^2 + 1} H_k(x) - \frac{2x}{x^2 + 1} J_k(x) \quad (48)$$

In the GAROL program, the first five terms of Equations (43) and (44) are used, and Equations (45) to (48) are used to compute individual terms of the series.

When it is not sufficiently accurate to use the asymptotic series, a convergent series is used. The latter is not used for all x and ξ values because of computer time considerations.

The convergent series for ψ is

$$\psi(x, \xi) = \exp[-x^2 z] \sum_{k=0}^{\infty} \frac{1}{k!} (xz)^{2k} \Gamma_k(z) \quad (49)$$

where

$$z = \frac{\xi^2}{4}$$

and

$$\Gamma_k(z) = \sqrt{z} e^z \int_z^{\infty} e^{-u} u^{-(k+\frac{1}{2})} du \quad (50)$$

By using Equation (39), we also have

$$\chi(x, \xi) = 2xz \exp[-x^2 z] \sum_{k=0}^{\infty} \frac{1}{k!} (xz)^{2k} \Gamma_{k+1}(z) . \quad (51)$$

$\Gamma_k(z)$ may be obtained from the recursion relation

$$\Gamma_{k+1}(z) = \frac{2}{2k+1} \left[\left(\frac{1}{z}\right)^k - \Gamma_k(z) \right] \quad (52)$$

and

$$\Gamma_0(z) = z^{\frac{1}{2}} e^z \int_z^{\infty} e^{-u} u^{-\frac{1}{2}} du \quad (53)$$

The quantity $\Gamma_0(z)$ may also be written as

$$\Gamma_0(z) = z^{\frac{1}{2}} e^z (\sqrt{\pi} - \gamma(\frac{1}{2}, z)) \quad (54)$$

where

$$\gamma(a, z) = \int_0^z e^{-u} u^{a-1} du \quad (55)$$

is the incomplete gamma function, or it may be expressed in terms of the normalized error function as

$$\Gamma_0(z) = \sqrt{\pi z} e^z (1 - \text{erf}(\sqrt{z})) \quad (56)$$

In the GAROL computer program $\Gamma_0(z)$ is computed from Equation (56) using the expansion

$$\text{erf}(x) = \frac{2}{\sqrt{\pi}} \left(x - \frac{x^3}{1!3} + \frac{x^5}{2!5} - \frac{x^7}{3!7} + \dots \right) \quad (57)$$

whenever $z \leq 8.4$.

$\Gamma_0(z)$ is computed from the continued fraction

$$\Gamma_0(z) = \frac{1}{1 + \frac{1}{2z + \frac{2}{z + \frac{3}{2z + \frac{4}{z + \frac{5}{2z + \frac{6}{z + \frac{7}{2z + 2.5}}}}}}}}}} \quad (58)$$

if $z > 8.4$.

When the convergent series is used for a given x and ξ , $\Gamma_0(z)$ needs to be computed only once. The remaining $\Gamma_k(z)$ are obtained rapidly from Equation (52).

The regions in the x, ξ plane for which the convergent or asymptotic series are to be used must be determined experimentally. The division which is given in Reference (5) has been found to be unsatisfactory. In the GAROL program, the convergent series is used whenever

$$\begin{array}{ll}
0 \leq x < 1.2 & \text{and} \quad \frac{4}{\xi^2} \geq 0.275 x^2 + 0.05 \\
1.2 \leq x < 10 & \text{and} \quad \frac{4}{\xi^2} \geq 0.12 x^2 + 0.28 \\
10 \leq x < 100 & \text{and} \quad \frac{4}{\xi^2} > 0.08 x^2 + 1.8 \\
100 \leq x < 500 & \text{and} \quad \frac{4}{\xi^2} > 0.0717 x^2 + 83 \\
500 < x < 2500 & \text{and} \quad \frac{4}{\xi^2} > 0.0635 x^2 + 2100 \\
x > 2500 & \text{and} \quad \frac{4}{\xi^2} \geq 0.111 x^{1.93}
\end{array} \tag{59}$$

For other values the asymptotic series has good accuracy and is therefore used.

Cross sections are computed in this manner for a finite interval around each resonance; that is, the method just described is used whenever

$$|x| \min(\xi, 1) < 150 \tag{60}$$

Outside of this interval, the scattering cross section is taken to be constant and equal to the potential cross sections. When computing the capture cross section for $x \min(\xi, 1) < -150$ the line shape ψ is taken to be first term of its asymptotic series, or

$$\psi(x, \xi) = \frac{1}{1 + x^2} . \tag{61}$$

For neutron energies such that $x \min(\xi, 1) > 150$, the capture cross section is assumed to be zero.

The Numerical Flux Computation

Let us first evaluate the integral

$$\int_E^{E_1} \frac{\sigma_s(E')}{E'} H(E - \alpha E') \varphi(E') dE'$$

numerically. This integral is typical of the type which appears in Equation (2). Break up the integral into a sum of integrals,

$$\int_E^{\frac{E}{\alpha}} \frac{\sigma_s(E')}{E'} H(E - \alpha E') \varphi(E') dE' = \sum_{j=p+1}^i \int_{E_j}^{E_{j-1}} \frac{\sigma_s(E')}{E'} \varphi(E') dE' + \int_{E_p}^{E_1} \frac{\sigma_s(E')}{E'} H(E_1 - \alpha E') \varphi(E') dE' \quad (62)$$

where the discrete variable E_i replaces E , and E_p is the discrete energy mesh point just below E_1/α . Note that if $E_1/\alpha > E_1$, $p=1$, and the last integral contributes nothing. For each interval (E_j, E_{j-1}) assume that $\sigma_s(E)\varphi(E)$ is linear; that is

$$\sigma_s(E)\varphi(E) = \frac{1}{E_{j-1} - E_j} [(E - E_j)\sigma_{s,j-1}\varphi_{j-1} + (E_{j-1} - E)\sigma_{s,j}\varphi_j] \quad (63)$$

where $\sigma_{s,j}$ and φ_j are the scattering cross section and flux at the energy E_j .

For the integral whose limits are (E_p, E_1) assume that $\sigma_s\varphi$ is linear in the interval $(E_p, E_1/\alpha)$,

$$\sigma_s(E)\varphi(E) = \frac{1}{E_1/\alpha - E_p} [(E - E_p)\sigma_s(\frac{E_1}{\alpha})\varphi(\frac{E_1}{\alpha}) + (\frac{E_1}{\alpha} - E)\sigma_{s,p}\varphi_p] \quad (64)$$

But E_1/α generally does not correspond to a mesh point and so we express $\sigma_s(\frac{E_1}{\alpha})\varphi(\frac{E_1}{\alpha}) \equiv \sigma_{s,p}^*\varphi_p^*$, by linear interpolation, in terms of its value at the two surrounding mesh points p and $p-1$. Then

$$\sigma_{s,p}^*\varphi_p^* = \frac{1}{E_{p-1} - E_p} [(E_{p-1} - \frac{E_1}{\alpha})\sigma_{s,p}\varphi_p + (\frac{E_1}{\alpha} - E_p)\sigma_{s,p-1}\varphi_{p-1}] \quad (65)$$

Inserting Equations (63) and (64) into Equation (62) gives

$$\int_E^{E/\alpha} \frac{\sigma_s(E')}{E'} H(E - \alpha E') \varphi(E') dE' = \sigma_{s,p} \varphi_p \beta_p + \sigma_{s,i} \varphi_i \gamma_i + \sum_{j=p+1}^{i-1} \sigma_{s,j} \varphi_j \delta_j + C_p \quad (66)$$

where

$$\beta_k = 1 - \frac{E_{k+1}}{E_k - E_{k+1}} \ln \frac{E_k}{E_{k+1}} \quad (67)$$

$$\gamma_k = \frac{E_{k-1}}{E_{k-1} - E_k} \ln \frac{E_{k-1}}{E_k} - 1 \quad (68)$$

$$\delta_k = \beta_k + \gamma_k \quad (69)$$

and

$$C_p = \frac{1}{2} \left(\frac{E_i}{\alpha} - E_p \right) \left(\frac{\sigma_{s,p} \varphi_p}{E_p} + \frac{\sigma_{s,p}^* \varphi_p^* \alpha}{E_i} \right) \quad (70)$$

unless $p = 1$, in which case

$$C_p = 0. \quad (71)$$

C_p is the evaluation of the last integral of Equation (62).

The special case for which $p=i$ corresponds to mesh points that are spaced sufficiently wide apart so that, for some isotope, $\alpha E_{i-1} > E_i$. For this case, the integral on the left hand side of Equation (62) is

$$\int_E^{E/\alpha} \frac{\sigma_s(E')}{E'} H(E - \alpha E') \varphi(E') dE' = C_i = \frac{1}{2} \left(\frac{1}{\alpha} - 1 \right) (\sigma_{s,i} \varphi_i + \sigma_{s,i}^* \varphi_i^* \alpha) \quad (72)$$

and, from Equation (65),

$$\sigma_{s,i}^* \varphi_i^* = \frac{1}{E_{i-1} - E_i} \left[(E_{i-1} - \frac{E_i}{\alpha}) \sigma_{s,i} \varphi_i + E_i \left(\frac{1}{\alpha} - 1 \right) \sigma_{s,i-1} \varphi_{i-1} \right] \quad (73)$$

Insertion of Equation (73) into Equation (72) gives, for the special case $p=i$,

$$\int_E^{E/\alpha} \frac{\sigma_s(E')}{E'} H(E - \alpha E') \varphi(E') dE' = a_i \sigma_{s,i} \varphi_i + b_i \sigma_{s,i-1} \varphi_{i-1} \quad (74)$$

where

$$a_i = \frac{1 - \alpha}{2\alpha} \left[1 + \frac{\alpha E_{i-1} - E_i}{E_{i-1} - E_i} \right] \quad (75)$$

and

$$b_i = \frac{(1 - \alpha)^2}{2\alpha} \frac{E_i}{E_{i-1} - E_i} \quad (76)$$

We are now ready to write Equation (2) in its finite differenced form. The equation is

$$\begin{aligned} V_{1\Sigma_{t1,i}} \varphi_{1i} &= (1 - P_1) V_1 \sum_{k=1}^M \frac{N_{1k}}{1 - \alpha_k} (Z_{1ki} + W_{1ki} \varphi_{1i}) \\ &+ P_2 V_2 \sum_{k=1}^M \frac{N_{2k}}{1 - \alpha_k} (Z_{2ki} + W_{2ki} \varphi_{2i}) \\ &+ V_1 (1 - P_1) S_{1i} + V_2 P_2 S_{2i} \end{aligned} \quad (77)$$

where

$$Z_{nki} = \sigma_{s,kp} \varphi_p \beta_p + \sum_{j=p+1}^{i-1} \sigma_{s,kj} \varphi_j \delta_j + C_{pk} \quad (78)$$

and

$$W_{nki} = \sigma_{s,ki} \gamma_i \quad (79)$$

if $p \neq i$. If $p = i$, that is if $\alpha_k E_{i-1} > E_i$, we have instead

$$Z_{nki} = b_{ik} = \frac{(1 - \alpha_k)^2}{2\alpha_k} \frac{E_i}{E_{i-1} - E_i} \quad (80)$$

and

$$W_{nki} = \frac{1 - \alpha_k}{2\alpha_k} \left[1 + \frac{\alpha_k E_{i-1} - E_i}{E_{i-1} - E_i} \right] \quad (81)$$

In Equations (78) and (81) the subscripts n and k denote the region and the isotope, respectively. With some additional abbreviated notation, we can write Equation (77) in a more compact manner. Define

$$D_{ni} = V_n \left\{ \Sigma_{tn,i} - (1 - P_n) \sum_{k=1}^M \frac{N_{nk}}{1 - \alpha_k} W_{nki} \right\} \quad (82)$$

$$Q_{ni} = V_n P_n \sum_{k=1}^M \frac{N_{nk}}{1 - \alpha_k} W_{nki} \quad (83)$$

and

$$\begin{aligned} T_{nmi} = & V_n (1 - P_n) \sum_{k=1}^M \frac{N_{nk}}{1 - \alpha_k} Z_{nki} + V_m P_m \sum_{k=1}^M \frac{N_{mk}}{1 - \alpha_k} Z_{mki} \\ & + V_n (1 - P_n) S_{ni} + V_m P_m S_{mi} \end{aligned} \quad (84)$$

In terms of these, Equation (77) becomes

$$D_{1i} \phi_{1i} - Q_{2i} \phi_{2i} = T_{12i} \quad (85)$$

As was mentioned below Equation (1), there exists another equation like it, but with the subscripts 1 and 2 reversed. In the notation of Equation (85) that second equation is

$$D_{2i} \phi_{2i} - Q_{1i} \phi_{1i} = T_{21i} \quad (86)$$

We may solve Equations (85) and (86) simultaneously to obtain

$$\phi_{1i} = \frac{T_{12i}D_{2i} + Q_{2i}T_{21i}}{D_{2i}D_{1i} - Q_{1i}Q_{2i}} \quad (87)$$

and

$$\phi_{2i} = \frac{T_{21i}D_{1i} + Q_{1i}T_{12i}}{D_{2i}D_{1i} - Q_{1i}Q_{2i}}. \quad (88)$$

The GAROL computer program evaluates Equations (87) and (88) for each i , one at a time beginning with $i=1$, until the complete flux solution has been obtained.

Averaging of Cross Sections

With the GAROL computer program, it is possible to obtain flux weighted cross sections over any desired energy bands. In addition a one group average, covering the entire range of the calculation, is always obtained. All of the integrals are carried out by the trapezoidal approximation. Let Σ_{α} denote the cross section for any reaction. This may be capture, scattering, or fission. Quite generally, a cell averaged macroscopic cross section may be defined by

$$\Sigma_{\alpha} = \frac{\int dE \int dV \int d\Omega \Sigma_{\alpha}(r, E, \Omega) \phi(r, E, \Omega)}{\int dE \int dV \int d\Omega \phi(r, E, \Omega)}, \quad (89)$$

where the angular integration is carried out over the full range, the volume is taken over the entire cell, and the energy integration is carried out over the energy group limits of interest.

For our two region cell, we define the integrated quantities

$$V_1 \phi_1(E) = \int_{V_1} dV \int d\Omega \phi(r, E, \Omega) \quad (90)$$

$$V_2 \varphi_2(E) = \int_{V_2} dV \int d\Omega \varphi(r, E, \Omega). \quad (91)$$

The energy dependent fluxes $\varphi_1(E)$ and $\varphi_2(E)$ are the fluxes of Equation (1). If $\Sigma_\alpha(r, E)$ has the simple form

$$\Sigma_\alpha(r, E) = N_1 \sigma_\alpha(E) \quad (92)$$

in V_1 and

$$\Sigma_\alpha(r, E) = N_2 \sigma_\alpha(E) \quad (93)$$

in V_2 , in which the number densities of the isotopes of interest are constant in each region, Equation (89) may be greatly simplified. Usually Equations (92) and (93) are satisfied; in fact, most often $N_2 = 0$. Using Equations (90) to (93) in (89) gives

$$\bar{\Sigma}_\alpha = \frac{N_1 V_1 \int \sigma_\alpha(E) \varphi_1(E) dE + N_2 V_2 \int \sigma_\alpha(E) \varphi_2(E) dE}{V_1 \int \varphi_1(E) dE + V_2 \int \varphi_2(E) dE} \quad (94)$$

If we define a flux weighted cross section for each region i by

$$\bar{\sigma}_{\alpha, i} = \frac{\int \sigma_\alpha(E) \varphi_i(E) dE}{\bar{\varphi}_i} \quad (95)$$

where $\bar{\varphi}_i$ is the group integrated flux

$$\bar{\varphi}_i = \int \varphi_i(E) dE, \quad (96)$$

Equation (94) becomes

$$\bar{\Sigma}_\alpha = \frac{N_1 V_1 \bar{\sigma}_{\alpha, 1} \bar{\varphi}_1 + N_2 V_2 \bar{\sigma}_{\alpha, 2} \bar{\varphi}_2}{V_1 \bar{\varphi}_1 + V_2 \bar{\varphi}_2} \quad (97)$$

We wish to compute a cell averaged microscopic cross section such that when it is multiplied by the number density of the isotope, homogenized over the entire cell, we obtain the correct macroscopic cross section. Thus we want $\bar{\sigma}_\alpha$ to satisfy

$$\bar{\Sigma}_\alpha = \frac{N_1 V_1 + N_2 V_2}{V_1 + V_2} \bar{\sigma}_\alpha \quad (98)$$

Hence, the cell averaged microscopic cross section is

$$\bar{\sigma}_\alpha = \frac{N_1 V_1 \bar{\sigma}_{\alpha,1} \bar{\phi}_1 + N_2 V_2 \bar{\sigma}_{\alpha,2} \bar{\phi}_2}{V_1 \bar{\phi}_1 + V_2 \bar{\phi}_2} \frac{V_1 + V_2}{N_1 V_1 + N_2 V_2} \quad (99)$$

The GAROL output includes the groupwise averages of capture, scattering and, if present, fission cross sections as given by Equations (95), for each region, and by Equation (99) for the cell. In the presence of fission, the quantity α , the ratio of capture to fission cross sections is also computed. If, as is usually the case, $N_2 = 0$ (the resonance absorber is present only in region 1), Equation (99) simplifies to

$$\bar{\sigma}_\alpha = \frac{\bar{\sigma}_{\alpha,1} \bar{\phi}_1}{\bar{\phi}_c} \quad (100)$$

where $\bar{\phi}_c$ is the average flux in the cell given by

$$\bar{\phi}_c = \frac{V_1 \bar{\phi}_1 + V_2 \bar{\phi}_2}{V_1 + V_2} \quad (101)$$

An Application of the GAROL Program

As an application of the GAROL computer program, we include a study of the effect of overlap of the resonances of the thorium doublet on the resonance integral and on the Doppler effect for thorium and thorium oxide rods.

The two resonances which were investigated had the parameters

$$E_o = 21.8 \text{ eV}$$

$$E_o = 23.47$$

$$\Gamma_n = 2.1 \text{ mv}$$

$$\Gamma_n = 4.0 \text{ mv}$$

$$\Gamma_\gamma = 24.5 \text{ mv}$$

$$\Gamma_\gamma = 24.5 \text{ mv}$$

$$g = 1.0$$

$$g = 1.0$$

In order to compute the resonance overlap, the cross sections for three thorium "isotopes" were computed: one isotope had both resonances, another had only the 21.8 eV resonance, while the third had only the 23.47 eV resonance. Separate problems were run for each of these isotopes. The resonance integral for the first isotope was compared with the sum of the resonance integrals of the second and third isotopes. The latter corresponds to the usual methods of computation. This comparison gives a direct indication of the influence of resonance overlap.

The results are summarized in Tables I to IV. All of the total resonance integrals referred to have been evaluated by standard procedures.⁽⁴⁾ The GAROL computer program was used only for an energy range covering the resonance doublet. It can be seen that the usual neglect of resonance overlap is justified for thin rods. But for larger rods the errors introduced can be significant.

Table I

Resonance Integral of Thorium Doublet
in Th Metal Rods

Rod Size (cm)	T = 300°K				T = 2000°K		
	No Overlap	With Overlap	% Diff.	% Diff. in Total Resonance Integral	No Overlap	With Overlap	% Diff.
0.138	6.05	6.00	1	0.25	9.08	9.44	1
0.275	4.02	3.94	1.8	0.5	5.85	5.74	1.9
0.55	2.72	2.62	3.5	0.8	3.58	3.45	3.7
1.1	1.87	1.75	6.7	1.3	2.24	2.09	7.3
2.2	1.30	1.15	12.6	2	1.45	1.27	13.6

Table II

Doppler Effect in Thorium Doublet
for Th Metal Rods

<u>Rod Size (cm)</u>	<u>(ΔI)₂₀₀₀₋₃₀₀ With No Overlap</u>	<u>(ΔI)₂₀₀₀₋₃₀₀ With Overlap</u>	<u>% Diff.</u>
0.138	3.47	3.45	0.9
0.275	1.87	1.80	2
0.55	0.86	0.83	4.5
1.1	0.37	0.34	10
2.2	0.15	0.12	23

Table III

Resonance Integral of Thorium Doublet in ThO₂ Rods

T = 300°K

T = 2000°K

<u>Rod Size (cm)</u>	<u>No Overlap</u>	<u>With Overlap</u>	<u>% Diff.</u>	<u>% Diff. in Total Resonance Integral</u>	<u>No Overlap</u>	<u>With Overlap</u>	<u>% Diff.</u>
0.25	6.35	6.28	1	0.3	10.0	9.9	1
0.50	4.30	4.21	2	0.6	6.33	6.18	2.4
1.0	3.02	2.90	4	0.9	4.09	3.90	5
2.0	2.21	2.05	8	1.6	2.78	2.55	9

Table IV

Doppler Effect in Thorium Doublet for ThO₂ Rods

<u>Rod Size (cm)</u>	<u>(ΔI)₂₀₀₀₋₃₀₀ With No Overlap</u>	<u>(ΔI)₂₀₀₀₋₃₀₀ With Overlap</u>	<u>% Diff.</u>
0.25	3.66	3.62	1.3
0.50	2.03	1.97	3
1.0	1.07	1.00	7
2.0	0.57	0.50	14

Output from GAROL

Standard output from a GAROL problem includes a description of the nuclides present on the cross section tape, if one has been generated, and a listing of the input options and limits specified for the calculation.

Further printed output is given if requested. This includes:

1. Pointwise cross-sections calculated from resonance parameters or interpolated from input cross sections, by isotope.
2. Pointwise flux, source, total macroscopic cross section, and collision density, all by region.
3. Broad group averaged cross sections.
4. Plotting description.

Output from the sample problem selects all of these options.

Two types of plotting may be done automatically from a GAROL problem. For region 1, the pointwise flux, total cross section, and collision density may be plotted. As an additional option, graphs of capture and fission rates, for each material, may be obtained. Samples of each of these are included. The plotting routines in GAROL were adapted from the two-dimensional plot routine described in reference 6.

Efficient Use of GAROL

Some hints regarding the efficient use of GAROL are included here. There are a number of ways in which the program may be used to do a homogeneous calculation. The most efficient is to choose the no geometry option, put the homogeneous mixture into region 1, and put 0.0 for the mean chord length of region 2 and for the number density of all materials in region 2. It is possible to run two homogeneous problems simultaneously by using the no geometry option, and by putting one mixture into each region. In such cases the mean chord lengths may be chosen to be equal to unity.

Generally speaking, the computer time is greatest for lighter materials. The only exception is for $A=1.0$ which is fastest of all because it is programmed differently. In practical applications, one frequently has a case in which he wants the flux to be $\frac{1}{E}$ in region 2. In such a case, it can be shown that the resonance integral of the isotopes in region 1 is independent of the choice of moderator in region 2. Thus, to simulate a $\frac{1}{E}$ flux in

region 2, it is best to let it be a large region in which the only material present has $A=1.0$, a constant scattering cross section, and no capture cross section.

OPERATING INSTRUCTIONS

Computer and Tape Requirements

The GAROL program is run on the IBM 7044 (32K) computer from a program tape and a starter deck, behind which is placed punched card input describing the problem(s) to be run.

In addition to the tapes required by the GA system, GAROL makes use of three special tapes: B4 for the GAROL Program Tape, B5 for GAROL cross section storage, and C6 for plotting. The B4 and B5 tapes must be mounted in all cases, and the B5 tape may be saved for subsequent runs. Thus, the tape configuration is as follows:

<u>GA Tape Unit</u>	<u>Fortran Logical Tape Number</u>	<u>Tape Function</u>
C1	1	General Atomic version of the IBM 7044 IBSYS Monitor (Version 9)
C2	5	Standard input tape
C3	6	Standard output tape
B4	7	GAROL program tape
B5	9	GAROL cross section tape
C6	11	GAROL plot tape, if any

If any plotting is done, instructions for the Stromberg-Carlson S-C 4020 High Speed Microfilm Recorder are written on tape C6. The number of graphs for which instructions have been generated will be printed on the on-line printer and will be transferred by the GA computer operator to the tape label provided by the user. The tape will then be sent to the S-C 4020 for plotting.

Thus, the deck setup for a sample GAROL problem consists of a six card starter deck followed by data cards prepared according to the Input Specifications for GAROL.

INPUT SPECIFICATIONS FOR GAROL

CARD	COLUMNS	FORMAT	NAME	DESCRIPTION
1	12	I12	INDEX	Source of cross sections for this problem(s) 0 = cross sections have been calculated and written on tape during an earlier run. This tape will be mounted on unit (B5). 1 = cross-sections will be calculated and written on tape (B5). This tape may be saved and reused for future calculations, if desired.
2	1-72	12A6	TLABEL	Tape label for data tape (B5). If INDEX = 0, this card must be identical to that used when the data tape was written.
If INDEX = 0, go to card 13.				
3	12	I12	NINDEX	Energy specification index 1 = Energies will be read from input cards (card 4A) 2 = Energies will be calculated by equal mesh spacing (card 4B) 3 = Energies will be calculated with mesh spacing proportion to velocity (card 4C) 4 = Energies will be calculated with equal lethargy mesh spacing (card 4D) 5 = Energies will be generated by a special subroutine ENRG (NPTS,E) supplied by the user (card 4E).
	13-24	I12	NPTS	Number of energy points. This value is needed for NINDEX = 1, and may be used when NINDEX = 5, if desired.
If NINDEX = 1, card 4A is needed.				
4A		6E12.6	E(i)	Energy points, in eV, from high to low. (NPTS entries)
If NINDEX = 2, card 4B is needed.				
4B	1-12	E12.6	EMAX	Maximum energy, eV
	13-24	E12.6	EMIN	Minimum energy, eV
	25-36	E12.6	DELTA E	ΔE , eV

INPUT SPECIFICATIONS FOR GAROL

CARD	COLUMNS	FORMAT	NAME	DESCRIPTION
If NINDEX = 3, card 4C is needed.				
4C	1-12	E12.6	EMAX	Maximum energy, eV
	13-24	E12.6	EMIN	Minimum energy, eV
	25-36	E12.6	CONST	C, where $E_{i+1} = E_i - C\sqrt{E_i}$ (equal velocity intervals)
If NINDEX = 4, card 4D is needed.				
4D	1-12	E12.6	EMAX	Maximum energy, eV
	13-24	E12.6	EMIN	Minimum energy, eV
	25-36	E12.6	DELTAU	Δu
If NINDEX = 5, the user supplies his own ENRG (NPTS,E) subroutine to compute, or read, his energy mesh. The number of energy points, NPTS, must not exceed 8000. The array E, which must be dimensioned, contains the energy points which are returned to the main program. If any input cards are required by the user's subroutine, they are inserted here (card 4E).				
4E				Variables and formats determined by the user.
5	1-12	I12	MAT	Number of nuclides for which cross sections will be calculated and written on tape (≤ 20)
	13-24	I12	JHYD	Will an A = 1.0 isotope be included on this tape? 0 = no 1 = yes
Cards 6 to 8 are repeated for each nuclide (MAT times).				
6	1-12	F12.6	TID	Identification number of this nuclide, given by Z and A, in the form 92.235000 for uranium 235. Nuclides should be given in ascending numerical order. Different sets of data for one nuclide may be distinguished in the fourth through six decimal places.
	13-42	5A6	CNAME	Nuclide description.
7	1-12	E12.6	AMASS	Atomic mass
	13-24	E12.6	ASYMSC	Asymptotic scattering cross section, used for computing source only.

INPUT SPECIFICATIONS FOR GAROL

CARD	COLUMNS	FORMAT	NAME	DESCRIPTION
	25-36	E12.6	SCAP	Capture cross section index. If SCAP ≥ 0.0, SCAP is the value of the capture cross section at 0.0253 eV, and the cross section is $1/v$. If SCAP = -1.0, pointwise capture cross sections will be calculated from resonance parameters. If SCAP = -2.0, pointwise cross sections will be read from cards (card 12).
	37-48	E12.6	SFIS	Fission cross section index. If SFIS ≥ 0.0, no fission. If SFIS = -1.0, pointwise fission will be calculated from resonance parameters. If SCAP = -2.0, this index is not used; pointwise fission cross sections will be read from cards (card 12).
	49-60	E12.6	SCAT	Scattering cross section index. If SCAT ≥ 0.0, scattering is constant at that value. If SCAT = -1.0, pointwise scattering cross sections will be calculated from resonance parameters. If SCAP = -2.0, this index is not used; pointwise scattering cross sections will be read from cards (card 12).
	61-72	E12.6	PRINT	Print index, for this nuclide. 0.0 = no printing 1.0 = the calculated or read capture, scattering, and fission (if present) cross sections for this nuclide will be printed. Up to nine sets of cross sections may be printed; if more than nine are specified, only the first nine will be printed. If any printing is done, the computer time estimate is doubled.
If SCAP = -2.0, card 8 is required.				
8	1-12	E12.6	ENPTS	Number of energies at which cross sections will be read.

Cards 9-11 (resonance parameters) are required for each material for which any cross sections will be calculated, and in the order specified by cards 6 and 7.

INPUT SPECIFICATIONS FOR GAROL

CARD	COLUMNS	FORMAT	NAME	DESCRIPTION
9	1-12	E12.6	WGT	Atomic mass. (This number will be checked against card 7, col. 1-12, to be sure that resonance parameters are given in the order specified).
	13-24	E12.6	STAT	Statistical factor indicator. If the statistical factor, g , is to have a constant value for all resonances, then STAT is the value used for the statistical factor. If $STAT \leq 0.0$, the statistical factor must be specified for each resonance.
	25-36	E12.6	SPOT	Potential scattering cross-section, barns.
	37-48	E12.6	TEMP	Temperature, $^{\circ}K$.
10	1-12	I12	NEZ	Number of resolved resonances (maximum = 500).
	24	I12	NFIS	Will fission widths be specified? 0 - No. 1 - Yes.
	36	I12	NGN	Γ_n form index. 0 - Neutron half-widths to be specified are standard values, not reduced. 1 - Neutron half-widths to be specified are reduced widths, Γ_n^0 .
Card 11 is given for each resonance. The format of card 11 is one of four types, depending on the NFIS and STAT values.				
If NFIS = 0 and $STAT \leq 0.0$, supply one card 11A for each resonance.				
11A	1-12	E12.6	EO	Resonance energy, eV.
	13-24	E12.6	GI	Either the spin (I) of the target nucleus, or the statistical factor, g , for this resonance, depending on the specification for GJ in the next field of this input card.
	25-36	E12.6	GJ	If $GJ > 0.0$, it is taken to be the spin (J) of the compound nucleus for this resonance, and the statistical factor is calculated as:

INPUT SPECIFICATIONS FOR GAROL

CARD	COLUMNS	FORMAT	NAME	DESCRIPTION
				$g = \frac{1}{2} \frac{(2J + 1)}{(2I + 1)}$ If $GJ < 0.0$, then GI in the previous field is taken to be the statistical factor, g, for this resonance.
	37-48	E12.6	GG	Γ_{γ} in millivolts.
	49-60	E12.6	GN	Γ_n , or Γ_n^0 , mv, depending on NGN specified on card 10, Col. 36.
If NFIS = 0 and STAT > 0.0, supply one card 11B for each resonance.				
11B	1-12	E12.6	EO	Resonance energy, eV.
	13-24	E12.6	GG	Γ_{γ} , mv.
	25-36	E12.6	GN	Γ_n or Γ_n^0 , mv.
If NFIS = 1, and STAT ≤ 0.0, supply one card 11C for each resonance.				
11C	1-12	E12.6	EO	Resonance energy, eV.
	13-24	E12.6	GI	As on card 11A.
	25-36	E12.6	GJ	As on card 11A.
	37-48	E12.6	GG	Γ_{γ} , mv.
	49-60	E12.6	GN	Γ_n or Γ_n^0 , mv.
	61-72	E12.6	GF	Γ_F , mv.
If NFIS = 1 and STAT > 0.0, supply one card 11D for each resonance.				
11D	1-12	E12.6	EO	Resonance energy, eV.
	13-24	E12.6	GG	Γ_{γ} , mv.
	25-36	E12.6	GN	Γ_n or Γ_n^0 , mv.
	37-48	E12.6	GF	Γ_F , mv.
If cross-sections will be read from cards, (SCAP = -2.0), for any nuclide, card 12, repeated at each energy, is required.				
Cross sections for up to 3 nuclides may be read from cards, and must be in the order specified by cards 6 to 8.				

INPUT SPECIFICATIONS FOR GAROL

CARD	COLUMNS	FORMAT	NAME	DESCRIPTION
12	1-12	E12.6	E	Energy, eV (high to low)
	13-24	E12.6	CAP	Capture cross section (barns)
	25-36	E12.6	SCAT	Scatter cross section (barns)
	37-48	E12.6	FISS	Fission cross section (barns)
Cross sections on the GAROL mesh are computed from this table by linear interpolation.				
13	1-72	12A6	TITLE	Problem description for flux calculation.
14	1-12	E12.6	EST	Upper boundary of energy range of interest (eV). If EST = 0.0, the first energy point present on the data tape will be used.
	13-24	E12.6	EEND	Lower boundary of energy range of interest (eV). If EEND = 0.0, the last energy point present on the data tape will be used.
	25-36	F12.1	GEOM	Geometry 1.0 = none (homogeneous) 2.0 = slab 3.0 = cylinder 4.0 = sphere 5.0 = Read your own escape probability table and coefficients (cards 18 and 19). 6.0 = Use the previously read tables.
	37-48	F12.1	ELEMS	Number of nuclides.
	49-60	F12.1	PRINT	Shall pointwise flux, external source, total cross section, and collision density be printed? 0.0 = no 1.0 = yes
	61-72	F12.1	PLOT	Shall flux, total cross section and collision density be plotted? 0.0 = no 1.0 = yes

INPUT SPECIFICATIONS FOR GAROL

CARD	COLUMNS	FORMAT	NAME	DESCRIPTION
15	1-12	E12.6	ELBAR(1)	$\bar{\ell}_1$ = Mean chord length, region 1
	13-24	E12.6	ELBAR(2)	$\bar{\ell}_2$ = Mean chord length, region 2: $\bar{\ell}_2 = 4V_2/S$ where V_2 is volume and S is common surface.
	25-36	E12.6	CC	Dancoff correction factor, if any.
	37-48	E12.6	XSORC	Will extra source terms be read? 0.0 = no 1.0 = yes
16	1-12	F12.1	ENBG	Number of broad groups. If ENBG = 0.0, there is no group averaging.
If ENBG $\neq$ 0.0, card 17 is needed.				
17		6E12.6	BEG(i)	Broad group lower boundaries in eV, from high to low.
Card 18 is repeated for each nuclide.				
18	1-12	F12.6	TID	Tape identification number for nuclide wanted.
	13-24	E12.6	DENS(1)	Density of this nuclide in region 1.
	25-36	E12.6	DENS(2)	Density of this nuclide in region 2.
	37-48	E12.6	PLOTS	0.0 = absorption rate for this isotope will not be plotted. 1.0 = absorption rate for this isotope will be plotted.
If GEOM = 5.0, cards 19 and 20 are needed.				
19	1-12	E12.6	C1	The constants C_1 , C_2 and C_3 .
	13-24	E12.6	C2	
	25-36	E12.6	C3	
		6E12.6	CYLT(i)	Special escape probability tables as a function of $\frac{\bar{\ell}_1 \Sigma_{t1}}{2}$. (302 entries from $\frac{\bar{\ell}_1 \Sigma_{t1}}{2} = 0.00$ to 6.02 in steps of 0.02.)
If XSORC = 1.0, cards 21 and 22 are needed.				
21	1-12	E12.6	ZSORC	Number of source points to be read. (ZSORC $\geq$ 2.0)

INPUT SPECIFICATIONS FOR GAROL

<u>CARD</u>	<u>COLUMNS</u>	<u>FORMAT</u>	<u>NAME</u>	<u>DESCRIPTION</u>
22	1-12	E12.6		Energy of source point
	13-24	E12.6		Source, region 1
	25-36	E12.6		Source, region 2
Repeat card 22 for each source point.				
Repeat input from card 13 until all problems have been specified.				

GAROL Error Table

<u>Link No.</u>	<u>Error No.</u>	<u>Description of Error</u>
1	1	Tape label card (input card 2) and label on data tape mounted on B5 do not agree.
1	2	Number of materials specified for data tape is not between 1 and 20.
1	3	More than 3 nuclides have been specified for the data tape with cross sections to be read from input cards.
1	7	A nuclide, other than the first, has been specified for the data tape with atomic mass A = 1.0.
1	4	Energy index (input card 3) is less than 1.
1	5	Energy index (input card 3) is greater than 5.
1	6	Number of energy points, using energy option 5, is greater than 8000, the core-contained limit.
2	1	Resonance parameters are either missing or out of order for a nuclide for which cross sections are to be calculated.
4	1	Number of materials for resonance calculation is not between 1 and 10.
4	2	Number of broad groups for averaging is not between 1 and 50.
4	3	Nuclide requested for resonance calculation is not present on data tape.

GAROL STARTER DECK AND SAMPLE PROBLEM

```

$IBJOB GAROL      NDSOURCE
$DUMP             TYPE1,00000-77777,ERROR
$*MOUNT          U07, (GAROL PROGRAM TAPE ON (B4))
$*MOUNT          U09, (GAROL DATA TAPE ON (B5))
$*HOLD           U11, (C6) PLOT TAPE
$RELOAD          U07,NAME=GAROL
    
```

U

1
THORIUM TAPE FOR GAROL SAMPLE PROBLEMS

8-65

```

4
29.023214 17.603469 0.00125
5
1.0 HYDROGEN
1.0 20.0 0.0 0.0 20.0 1.0
6.0 GRAPHITE
12.0 4.7102 0.0 0.0 4.7102 1.0
8.0 OXYGEN
16.0 3.7 0.0 0.0 3.7 1.0
90.232 TH232 300K, GAM=24.5, TWO RES
232.0 12.6 -1.0 0.0 -1.0 1.0
90.2321 TH232 2000K, GAM=24.5, TWO RES
232.0 12.6 -1.0 0.0 -1.0 1.0
232.0 1.0 12.6 300.0
2
21.8 24.5 2.1
23.47 24.5 4.0
232.0 1.0 12.6 2000.0
2
21.8 24.5 2.1
23.47 24.5 4.0
THORIUM R=2.2 T=300
29.023214 17.603469 3.0 2.0 1.0 1.0
4.4 10000.0 0.0
2.0
22.603302 17.603469
1.0 0.0 1.0 1.0
90.2320 0.03037 0.0 1.0
    
```

8-65

GAROL DATA TAPE, LABELED THORIUM TAPE FOR GAROL SAMPLE PROBLEMS

NUCLIDE TABLE OF CONTENTS

NUCLIDE I.D.	NAME	A	ASYMPTOTIC SCATTERING	CAPTURE	FISSION	SCATTER	NUMBER OF ARRAYS
1.0	HYDROGEN	1.000	20.00000	0.	0.	2.00000 C1	0
6.0	GRAPHITE	12.000	4.71020	0.	0.	4.71020 00	0
8.0	OXYGEN	16.000	3.70000	0.	0.	3.70000 00	0
90.232	TH232 300K, GAM=24.5, TWO RES	232.000	12.60000	COMPUTED	0.	COMPUTED	2
90.2321	TH232 2000K, GAM=24.5, TWO RES	232.000	12.60000	COMPUTED	0.	COMPUTED	2

GAROL DATA TAPE, LABELED THORIUM TAPE FOR GAROL SAMPLE PROBLEMS

DOPPLER BROADENING CALCULATIONS FOR TH232 300K, GAM=24.5, TWO RES
 ABSORBER MASS = 232.000
 POTENTIAL SCATTERING = 12.600 (BARNs)
 TEMPERATURE = 300.000 (K)

RESONANCE PARAMETER INPUT

NUMBER	RESONANCE ENERGY-EV	STATISTICAL FACTORS			HALF-WIDTHS - MV	
		I	J	G	GAMMA N	GAMMA F
1	21.800	0.0	0.0	1.000	2.1000	0.0000
2	23.470	0.0	0.0	1.000	4.0000	0.0000

GAROL DATA TAPE, LABELED THORIUM TAPE FOR GAROL SAMPLE PROBLEMS

8-65

DOPPLER BROADENING CALCULATIONS FOR TH232 2000K, GAM=24.5, TWO RES

ABSORBER MASS = 232.000

POTENTIAL SCATTERING = 12.600 (BARNs)

TEMPERATURE = 2000.000 (K)

RESONANCE PARAMETER INPUT

NUMBER	RESONANCE ENERGY-EV	STATISTICAL FACTORS			HALF-WIDTHS - MV		GAMMA F
		I	J	G	GAMMA	GAMMA	
1	21.800	0.0	0.0	1.000	2.1000	24.5000	0.0000
2	23.470	0.0	0.0	1.000	4.0000	24.5000	0.0000

GAROL DATA TAPE, LABELED THORIUM TAPE FOR				TH232 3000		TH232 2000		PROBLEMS	
ENERGY-EV				CAPTURE	SCATTER	CAPTURE	SCATTER		
1	2.90232	01	1.05696-01	1.38357	01	1.05968-01	1.38358	01	
2	2.89870	01	1.07078-01	1.38434	01	1.07358-01	1.38445	01	
3	2.89507	01	1.08485-01	1.38512	01	1.08773-01	1.38523	01	
4	2.89146	01	1.09918-01	1.38590	01	1.10213-01	1.38602	01	
5	2.88785	01	1.11377-01	1.38670	01	1.11680-01	1.38681	01	
6	2.88424	01	1.12863-01	1.38750	01	1.13174-01	1.38762	01	
7	2.88064	01	1.14377-01	1.38832	01	1.14696-01	1.38844	01	
8	2.87704	01	1.15918-01	1.38914	01	1.16246-01	1.38926	01	
9	2.87344	01	1.17489-01	1.38997	01	1.17826-01	1.39010	01	
10	2.86985	01	1.19089-01	1.39081	01	1.19435-01	1.39094	01	
11	2.86627	01	1.20719-01	1.39167	01	1.21075-01	1.39180	01	
12	2.86269	01	1.22381-01	1.39253	01	1.22747-01	1.39266	01	
13	2.85911	01	1.24074-01	1.39340	01	1.24450-01	1.39354	01	
14	2.85554	01	1.25800-01	1.39429	01	1.26187-01	1.39442	01	
15	2.85197	01	1.27559-01	1.39518	01	1.27957-01	1.39532	01	
16	2.84841	01	1.29353-01	1.39609	01	1.29762-01	1.39623	01	
17	2.84485	01	1.31182-01	1.39700	01	1.31603-01	1.39715	01	
18	2.84130	01	1.33047-01	1.39793	01	1.33480-01	1.39808	01	
19	2.83775	01	1.34949-01	1.39887	01	1.35335-01	1.39903	01	
20	2.83420	01	1.36890-01	1.39983	01	1.37348-01	1.39998	01	
21	2.83066	01	1.38869-01	1.40079	01	1.39341-01	1.40095	01	
22	2.82713	01	1.40888-01	1.40177	01	1.41374-01	1.40193	01	
23	2.82359	01	1.42949-01	1.40276	01	1.43449-01	1.40292	01	
24	2.82007	01	1.45052-01	1.40376	01	1.45567-01	1.40393	01	
25	2.81654	01	1.47198-01	1.40477	01	1.47729-01	1.40495	01	
26	2.81303	01	1.49389-01	1.40580	01	1.49936-01	1.40598	01	
27	2.80951	01	1.51625-01	1.40684	01	1.52189-01	1.40703	01	
28	2.80600	01	1.53909-01	1.40790	01	1.54490-01	1.40809	01	
29	2.80250	01	1.56242-01	1.40897	01	1.56840-01	1.40916	01	
30	2.79900	01	1.58624-01	1.41006	01	1.59241-01	1.41025	01	
31	2.79550	01	1.61057-01	1.41116	01	1.61693-01	1.41136	01	
32	2.79201	01	1.63543-01	1.41227	01	1.64199-01	1.41248	01	
33	2.78852	01	1.66083-01	1.41340	01	1.66760-01	1.41361	01	
34	2.78504	01	1.68678-01	1.41455	01	1.69377-01	1.41476	01	
35	2.78156	01	1.71331-01	1.41571	01	1.72053-01	1.41593	01	
36	2.77808	01	1.74043-01	1.41689	01	1.74788-01	1.41711	01	
37	2.77461	01	1.76816-01	1.41809	01	1.77585-01	1.41832	01	
38	2.77115	01	1.79652-01	1.41930	01	1.80446-01	1.41953	01	
39	2.76768	01	1.82552-01	1.42053	01	1.83372-01	1.42077	01	
40	2.76423	01	1.85518-01	1.42178	01	1.86366-01	1.42203	01	
41	2.76077	01	1.88553-01	1.42305	01	1.89429-01	1.42330	01	
42	2.75732	01	1.91658-01	1.42433	01	1.92563-01	1.42459	01	
43	2.75388	01	1.94836-01	1.42564	01	1.95772-01	1.42590	01	
44	2.75044	01	1.98089-01	1.42696	01	1.99057-01	1.42723	01	
45	2.74700	01	2.01419-01	1.42831	01	2.02421-01	1.42859	01	
46	2.74357	01	2.04829-01	1.42967	01	2.05866-01	1.42996	01	
47	2.74014	01	2.08321-01	1.43106	01	2.09394-01	1.43135	01	
48	2.73672	01	2.11899-01	1.43247	01	2.13009-01	1.43277	01	
49	2.73330	01	2.15564-01	1.43390	01	2.16714-01	1.43421	01	
50	2.72989	01	2.19319-01	1.43535	01	2.20511-01	1.43567	01	
51	2.72648	01	2.23168-01	1.43683	01	2.24403-01	1.43715	01	

GAROL DATA TAPE, LABELED THORIUM TAPE FOR				GAROL SAMPLE PROBLEMS			
ENERGY-EV		TH232 300		TH232 2000			
		CAPTURE	SCATTER	CAPTURE	SCATTER		
52	2.72307 01	2.27114-01	1.43833 01	2.28394-01	1.43866 01		
53	2.71967 01	2.31160-01	1.43985 01	2.32487-01	1.44020 01		
54	2.71627 01	2.35309-01	1.44140 01	2.36685-01	1.44175 01		
55	2.71288 01	2.39565-01	1.44298 01	2.40992-01	1.44334 01		
56	2.70949 01	2.43932-01	1.44458 01	2.45413-01	1.44495 01		
57	2.70611 01	2.48413-01	1.44621 01	2.49950-01	1.44659 01		
58	2.70273 01	2.53012-01	1.44786 01	2.54608-01	1.44826 01		
59	2.69935 01	2.57734-01	1.44955 01	2.59392-01	1.44995 01		
60	2.69598 01	2.62583-01	1.45126 01	2.64305-01	1.45168 01		
61	2.69261 01	2.67563-01	1.45300 01	2.69353-01	1.45343 01		
62	2.68925 01	2.72680-01	1.45478 01	2.74540-01	1.45522 01		
63	2.68589 01	2.77938-01	1.45658 01	2.79873-01	1.45704 01		
64	2.68253 01	2.83342-01	1.45842 01	2.85355-01	1.45889 01		
65	2.67918 01	2.88899-01	1.46029 01	2.90994-01	1.46077 01		
66	2.67583 01	2.94613-01	1.46220 01	2.96794-01	1.46269 01		
67	2.67249 01	3.00491-01	1.46414 01	3.02763-01	1.46465 01		
68	2.66915 01	3.06539-01	1.46611 01	3.08906-01	1.46664 01		
69	2.66582 01	3.12764-01	1.46813 01	3.15231-01	1.46867 01		
70	2.66249 01	3.19172-01	1.47018 01	3.21744-01	1.47074 01		
71	2.65916 01	3.25771-01	1.47227 01	3.28454-01	1.47285 01		
72	2.65584 01	3.32569-01	1.47440 01	3.35359-01	1.47500 01		
73	2.65252 01	3.39573-01	1.47658 01	3.42497-01	1.47720 01		
74	2.64921 01	3.46793-01	1.47879 01	3.49846-01	1.47943 01		
75	2.64590 01	3.54236-01	1.48106 01	3.57426-01	1.48172 01		
76	2.64259 01	3.61913-01	1.48336 01	3.65247-01	1.48405 01		
77	2.63929 01	3.69832-01	1.48572 01	3.73320-01	1.48643 01		
78	2.63600 01	3.78006-01	1.48812 01	3.81655-01	1.48885 01		
79	2.63270 01	3.86444-01	1.49058 01	3.90264-01	1.49133 01		
80	2.62941 01	3.95157-01	1.49308 01	3.99158-01	1.49387 01		
81	2.62613 01	4.04159-01	1.49564 01	4.08352-01	1.49646 01		
82	2.62285 01	4.13462-01	1.49826 01	4.17858-01	1.49910 01		
83	2.61957 01	4.23080-01	1.50093 01	4.27691-01	1.50180 01		
84	2.61630 01	4.33027-01	1.50367 01	4.37866-01	1.50457 01		
85	2.61303 01	4.43318-01	1.50646 01	4.48400-01	1.50740 01		
86	2.60977 01	4.53970-01	1.50932 01	4.59309-01	1.51029 01		
87	2.60651 01	4.65000-01	1.51224 01	4.70612-01	1.51325 01		
88	2.60325 01	4.76425-01	1.51523 01	4.82329-01	1.51628 01		
89	2.60000 01	4.88264-01	1.51829 01	4.94479-01	1.51938 01		
90	2.59675 01	5.00540-01	1.52143 01	5.07085-01	1.52256 01		
91	2.59351 01	5.13272-01	1.52464 01	5.20171-01	1.52582 01		
92	2.59027 01	5.26484-01	1.52793 01	5.33760-01	1.52916 01		
93	2.58703 01	5.40201-01	1.53130 01	5.47879-01	1.53258 01		
94	2.58380 01	5.54449-01	1.53476 01	5.62558-01	1.53609 01		
95	2.58057 01	5.69255-01	1.53831 01	5.77825-01	1.53970 01		
96	2.57735 01	5.84650-01	1.54195 01	5.93714-01	1.54340 01		
97	2.57413 01	6.00666-01	1.54568 01	6.10259-01	1.54719 01		
98	2.57091 01	6.17335-01	1.54951 01	6.27497-01	1.55110 01		
99	2.56770 01	6.34696-01	1.55345 01	6.45468-01	1.55510 01		
100	2.56449 01	6.52785-01	1.55750 01	6.64215-01	1.55923 01		
101	2.56129 01	6.71647-01	1.56166 01	6.83784-01	1.56347 01		
102	2.55809 01	6.91324-01	1.56594 01	7.04224-01	1.56783 01		
103	2.55489 01	7.11866-01	1.57034 01	7.25589-01	1.57232 01		

CAROL DATA TAPE, LABELED THORIUM TAPE FOR				CAROL SAMPLE PROBLEMS			
		TH232 300		TH232 2000			
ENERGY-EV		CAPTURE		SCATTER		CAPTURE	
						SCATTER	
104	2.55170 01	7.33323-01	1.57487 01	7.47936-01	1.57695 01	1.57695 01	1.57695 01
105	2.54851 01	7.55753-01	1.57953 01	7.71328-01	1.58171 01	1.58171 01	1.58171 01
106	2.54533 01	7.79214-01	1.58433 01	7.95831-01	1.58663 01	1.58663 01	1.58663 01
107	2.54215 01	8.03772-01	1.58929 01	8.21520-01	1.59170 01	1.59170 01	1.59170 01
108	2.53898 01	8.29496-01	1.59440 01	8.48473-01	1.59693 01	1.59693 01	1.59693 01
109	2.53580 01	8.56463-01	1.59967 01	8.76776-01	1.60234 01	1.60234 01	1.60234 01
110	2.53264 01	8.84754-01	1.60511 01	9.06522-01	1.60792 01	1.60792 01	1.60792 01
111	2.52947 01	9.14459-01	1.61073 01	9.37814-01	1.61370 01	1.61370 01	1.61370 01
112	2.52631 01	9.45673-01	1.61653 01	9.70763-01	1.61967 01	1.61967 01	1.61967 01
113	2.52316 01	9.78503-01	1.62254 01	1.00549 00	1.62586 01	1.62586 01	1.62586 01
114	2.52000 01	1.01306 00	1.62876 01	1.04213 00	1.63227 01	1.63227 01	1.63227 01
115	2.51686 01	1.04948 00	1.63920 01	1.08083 00	1.63892 01	1.63892 01	1.63892 01
116	2.51371 01	1.08788 00	1.64187 01	1.12175 00	1.64582 01	1.64582 01	1.64582 01
117	2.51057 01	1.12842 00	1.64878 01	1.16506 00	1.65298 01	1.65298 01	1.65298 01
118	2.50744 01	1.17127 00	1.65596 01	1.21097 00	1.66042 01	1.66042 01	1.66042 01
119	2.50430 01	1.21661 00	1.66342 01	1.25969 00	1.66817 01	1.66817 01	1.66817 01
120	2.50118 01	1.26462 00	1.67117 01	1.31147 00	1.67623 01	1.67623 01	1.67623 01
121	2.49805 01	1.31553 00	1.67922 01	1.36656 00	1.68463 01	1.68463 01	1.68463 01
122	2.49493 01	1.36958 00	1.68762 01	1.42527 00	1.69340 01	1.69340 01	1.69340 01
123	2.49181 01	1.42704 00	1.69636 01	1.48793 00	1.70255 01	1.70255 01	1.70255 01
124	2.48870 01	1.48821 00	1.70548 01	1.55492 00	1.71212 01	1.71212 01	1.71212 01
125	2.48559 01	1.55340 00	1.71500 01	1.62666 00	1.72214 01	1.72214 01	1.72214 01
126	2.48249 01	1.62299 00	1.72495 01	1.70363 00	1.73264 01	1.73264 01	1.73264 01
127	2.47939 01	1.69739 00	1.73537 01	1.78637 00	1.74366 01	1.74366 01	1.74366 01
128	2.47629 01	1.77705 00	1.74628 01	1.87549 00	1.75524 01	1.75524 01	1.75524 01
129	2.47319 01	1.86250 00	1.75772 01	1.97169 00	1.76743 01	1.76743 01	1.76743 01
130	2.47010 01	1.95430 00	1.76973 01	2.07579 00	1.78028 01	1.78028 01	1.78028 01
131	2.46702 01	2.05312 00	1.78236 01	2.31151 00	1.79384 01	1.79384 01	1.79384 01
132	2.46394 01	2.15969 00	1.79567 01	2.44546 00	1.80819 01	1.80819 01	1.80819 01
133	2.46086 01	2.27487 00	1.80970 01	2.44546 00	1.82340 01	1.82340 01	1.82340 01
134	2.45779 01	2.39961 00	1.82452 01	2.59203 00	1.83956 01	1.83956 01	1.83956 01
135	2.45471 01	2.53501 00	1.84020 01	2.75294 00	1.85675 01	1.85675 01	1.85675 01
136	2.45165 01	2.68235 00	1.85682 01	2.93027 00	1.87510 01	1.87510 01	1.87510 01
137	2.44859 01	2.84309 00	1.87447 01	3.12646 00	1.89472 01	1.89472 01	1.89472 01
138	2.44553 01	3.01891 00	1.89325 01	3.34450 00	1.91578 01	1.91578 01	1.91578 01
139	2.44247 01	3.21181 00	1.91328 01	3.58802 00	1.93843 01	1.93843 01	1.93843 01
140	2.43942 01	3.42409 00	1.93469 01	3.87623 00	1.96378 01	1.96378 01	1.96378 01
141	2.43637 01	3.65848 00	1.95763 01	4.19731 00	1.99077 01	1.99077 01	1.99077 01
142	2.43333 01	3.91820 00	1.98229 01	4.57146 00	2.02039 01	2.02039 01	2.02039 01
143	2.43029 01	4.20710 00	2.00885 01	5.01656 00	2.05320 01	2.05320 01	2.05320 01
144	2.42725 01	4.52977 00	2.03757 01	5.56009 00	2.08997 01	2.08997 01	2.08997 01
145	2.42422 01	4.89180 00	2.06872 01	6.24473 00	2.13177 01	2.13177 01	2.13177 01
146	2.42119 01	5.29994 00	2.10263 01	7.13695 00	2.18018 01	2.18018 01	2.18018 01
147	2.41817 01	5.76253 00	2.13970 01	8.33956 00	2.23743 01	2.23743 01	2.23743 01
148	2.41515 01	6.28989 00	2.18041 01	1.00092 01	2.30578 01	2.30578 01	2.30578 01
149	2.41213 01	6.89493 00	2.22534 01	1.23799 01	2.39284 01	2.39284 01	2.39284 01
150	2.40912 01	7.59404 00	2.27519 01	1.57921 01	2.50206 01	2.50206 01	2.50206 01
151	2.40611 01	8.40827 00	2.33084 01	2.07277 01	2.64324 01	2.64324 01	2.64324 01
152	2.40310 01	9.36502 00	2.39342 01	2.78453 01	2.82803 01	2.82803 01	2.82803 01
153	2.40010 01	1.05006 01	2.46432 01	3.80137 01	3.07133 01	3.07133 01	3.07133 01
154	2.39710 01	1.18641 01	2.54540 01	5.23315 01	3.39142 01	3.39142 01	3.39142 01
155	2.39411 01	1.35234 01	2.63908 01	7.21252 01	3.80966 01	3.80966 01	3.80966 01

GAROL DATA TAPE, LABELED THORIUM TAPE FOR GAROL SAMPLE PROBLEMS

	ENERGY-EV		TH232 300		TH232 2000		SCATTER			
	CAPTURE	SCATTER	CAPTURE	SCATTER	CAPTURE	SCATTER				
156	2.39112	01	1.55745	01	2.74867	01	9.89104	01	4.34955	01
157	2.38813	01	1.81588	01	2.87878	01	1.34306	02	5.03507	01
158	2.38515	01	2.14914	01	3.03603	01	1.79896	02	5.88806	01
159	2.38217	01	2.60072	01	3.23372	01	2.37027	02	6.92484	01
160	2.37919	01	3.23666	01	3.48764	01	3.06578	02	8.15235	01
161	2.37622	01	4.22065	01	3.83630	01	3.88689	02	9.56407	01
162	2.37325	01	5.94243	01	4.36035	01	4.82524	02	1.11366	02
163	2.37029	01	9.33845	01	5.23653	01	5.86079	02	1.28272	02
164	2.36732	01	1.64412	02	6.82111	01	6.96111	02	1.45742	02
165	2.36437	01	3.09283	02	9.71553	01	8.08201	02	1.62984	02
166	2.36141	01	5.78375	02	1.46730	02	9.16994	02	1.79037	02
167	2.35846	01	1.01240	03	2.21695	02	1.01659	03	1.93091	02
168	2.35552	01	1.59737	03	3.16782	02	1.10107	03	2.04379	02
169	2.35258	01	2.22522	03	4.11528	02	1.16507	03	2.11271	02
170	2.34964	01	2.70816	03	4.74700	02	1.20438	03	2.14114	02
171	2.34670	01	2.86611	03	4.79882	02	1.21636	03	2.12340	02
172	2.34377	01	2.63563	03	4.22276	02	1.20027	03	2.06008	02
173	2.34084	01	2.11129	03	3.22514	02	1.15735	03	1.95494	02
174	2.33792	01	1.48296	03	2.13790	02	1.09066	03	1.81448	02
175	2.33500	01	9.25114	02	1.23392	02	1.00463	03	1.64728	02
176	2.33208	01	5.24768	02	6.25598	01	9.04771	02	1.46303	02
177	2.32917	01	2.81936	02	2.85251	01	7.96894	02	1.27152	02
178	2.32626	01	1.52558	02	1.24879	01	6.86665	02	1.08222	02
179	2.32335	01	8.89883	01	6.15007	00	5.79111	02	9.02593	01
180	2.32045	01	5.81527	01	4.18103	00	4.78292	02	7.38647	01
181	2.31755	01	4.21796	01	3.90597	00	3.87124	02	5.94256	01
182	2.31465	01	3.28713	01	4.20881	00	3.07353	02	4.71322	01
183	2.31176	01	2.67807	01	4.68304	00	2.39655	02	3.70332	01
184	2.30888	01	2.24271	01	5.19619	00	1.83823	02	2.89233	01
185	2.30599	01	1.92079	01	5.69504	00	1.38999	02	2.26845	01
186	2.30311	01	1.67115	01	6.17154	00	1.03910	02	1.80274	01
187	2.30023	01	1.47342	01	6.62188	00	7.70847	01	1.46750	01
188	2.29736	01	1.31420	01	7.04603	00	5.70209	01	1.23596	01
189	2.29449	01	1.18428	01	7.44562	00	4.23101	01	1.08396	01
190	2.29162	01	1.07717	01	7.82288	00	3.17121	01	9.90954	00
191	2.28876	01	9.88163	00	8.18025	00	2.41890	01	9.40281	00
192	2.28590	01	9.13781	00	8.52016	00	1.89093	01	9.18995	00
193	2.28305	01	8.51413	00	8.84492	00	1.52319	01	9.17446	00
194	2.28019	01	7.99071	00	9.15671	00	1.26786	01	9.28704	00
195	2.27735	01	7.55230	00	9.45758	00	1.09040	01	9.47980	00
196	2.27450	01	7.18713	00	9.74948	00	9.66538	00	9.72091	00
197	2.27166	01	6.88611	00	1.00342	01	8.79629	00	9.99013	00
198	2.26882	01	6.64232	00	1.03136	01	8.19512	00	1.02799	01
199	2.26599	01	6.45054	00	1.05894	01	7.77769	00	1.05767	01
200	2.26316	01	6.30702	00	1.08632	01	7.50635	00	1.08809	01
201	2.26033	01	6.20929	00	1.11368	01	7.35832	00	1.11924	01
202	2.25751	01	6.15603	00	1.14119	01	7.32719	00	1.15133	01
203	2.25469	01	6.14704	00	1.16905	01	7.42184	00	1.18474	01
204	2.25187	01	6.18322	00	1.19746	01	7.65912	00	1.22034	01
205	2.24906	01	6.26671	00	1.22664	01	8.10897	00	1.25820	01
206	2.24625	01	6.40096	00	1.25683	01	8.83476	00	1.29982	01
207	2.24344	01	6.59105	00	1.28832	01	9.95594	00	1.34669	01

GAROL DATA TAPE, LABELED THORIUM TAPE FOR GAROL SAMPLE PROBLEMS									
TH232 300					TH232 2000				
ENERGY-EV	CAPTURE	SCATTER	SCATTER	CAPTURE	SCATTER	CAPTURE	SCATTER	SCATTER	SCATTER
208	2.24064 01	6.84400 00	1.32144 01	1.16472 01	1.40380 01	1.40380 01	1.40380 01	1.40380 01	1.40380 01
209	2.23784 01	7.16928 00	1.35656 01	1.41561 01	1.46480 01	1.46480 01	1.46480 01	1.46480 01	1.46480 01
210	2.23504 01	7.57963 00	1.39417 01	1.78219 01	1.54210 01	1.54210 01	1.54210 01	1.54210 01	1.54210 01
211	2.23225 01	8.09217 00	1.43483 01	2.30940 01	1.63699 01	1.63699 01	1.63699 01	1.63699 01	1.63699 01
212	2.22946 01	8.73001 00	1.47925 01	3.05450 01	1.75466 01	1.75466 01	1.75466 01	1.75466 01	1.75466 01
213	2.22668 01	9.52492 00	1.52835 01	4.08749 01	1.90112 01	1.90112 01	1.90112 01	1.90112 01	1.90112 01
214	2.22390 01	1.05213 01	1.58333 01	5.48992 01	2.08299 01	2.08299 01	2.08299 01	2.08299 01	2.08299 01
215	2.22112 01	1.17826 01	1.64576 01	7.35151 01	2.30703 01	2.30703 01	2.30703 01	2.30703 01	2.30703 01
216	2.21834 01	1.34031 01	1.71784 01	9.76410 01	2.57952 01	2.57952 01	2.57952 01	2.57952 01	2.57952 01
217	2.21557 01	1.55276 01	1.80263 01	1.28128 02	2.90538 01	2.90538 01	2.90538 01	2.90538 01	2.90538 01
218	2.21280 01	1.84816 01	1.90701 01	1.65645 02	3.28712 01	3.28712 01	3.28712 01	3.28712 01	3.28712 01
219	2.21004 01	2.27328 01	2.03756 01	2.10543 02	3.72378 01	3.72378 01	3.72378 01	3.72378 01	3.72378 01
220	2.20728 01	2.95199 01	2.21213 01	2.62722 02	4.20987 01	4.20987 01	4.20987 01	4.20987 01	4.20987 01
221	2.20452 01	4.17359 01	2.46531 01	3.21505 02	4.73468 01	4.73468 01	4.73468 01	4.73468 01	4.73468 01
222	2.20177 01	6.60330 01	2.86704 01	3.85561 02	5.28196 01	5.28196 01	5.28196 01	5.28196 01	5.28196 01
223	2.19902 01	1.16011 02	3.54510 01	4.52881 02	5.83025 01	5.83025 01	5.83025 01	5.83025 01	5.83025 01
224	2.19627 01	2.14686 02	4.69227 01	5.20836 02	6.35392 01	6.35392 01	6.35392 01	6.35392 01	6.35392 01
225	2.19353 01	3.91327 02	6.51504 01	5.86322 02	6.82487 01	6.82487 01	6.82487 01	6.82487 01	6.82487 01
226	2.19079 01	6.66800 02	9.08689 01	6.45980 02	7.21435 01	7.21435 01	7.21435 01	7.21435 01	7.21435 01
227	2.18805 01	1.02854 03	1.21446 02	6.96479 02	7.49806 01	7.49806 01	7.49806 01	7.49806 01	7.49806 01
228	2.18532 01	1.41107 03	1.49872 02	7.34824 02	7.65377 01	7.65377 01	7.65377 01	7.65377 01	7.65377 01
229	2.18259 01	1.70616 03	1.66634 02	7.58654 02	7.66857 01	7.66857 01	7.66857 01	7.66857 01	7.66857 01
230	2.17986 01	1.81079 03	1.64424 02	7.66484 02	7.53792 01	7.53792 01	7.53792 01	7.53792 01	7.53792 01
231	2.17714 01	1.68559 03	1.42682 02	7.57862 02	7.26680 01	7.26680 01	7.26680 01	7.26680 01	7.26680 01
232	2.17442 01	1.37897 03	1.08272 02	7.33407 02	6.86926 01	6.86926 01	6.86926 01	6.86926 01	6.86926 01
233	2.17170 01	9.96761 02	7.15752 01	6.94740 02	6.36709 01	6.36709 01	6.36709 01	6.36709 01	6.36709 01
234	2.16899 01	6.43217 02	4.11197 01	6.44302 02	5.78761 01	5.78761 01	5.78761 01	5.78761 01	5.78761 01
235	2.16628 01	3.77578 02	2.05477 01	5.85101 02	5.16104 01	5.16104 01	5.16104 01	5.16104 01	5.16104 01
236	2.16357 01	2.08306 02	9.08865 00	5.20415 02	4.51775 01	4.51775 01	4.51775 01	4.51775 01	4.51775 01
237	2.16087 01	1.13667 02	3.90451 00	4.53496 02	3.88579 01	3.88579 01	3.88579 01	3.88579 01	3.88579 01
238	2.15817 01	6.53533 01	2.17366 00	3.87310 02	3.28884 01	3.28884 01	3.28884 01	3.28884 01	3.28884 01
239	2.15547 01	4.15397 01	1.99539 00	3.24340 02	2.74503 01	2.74503 01	2.74503 01	2.74503 01	2.74503 01
240	2.15278 01	2.93697 01	2.37787 00	2.66470 02	2.26629 01	2.26629 01	2.26629 01	2.26629 01	2.26629 01
241	2.15009 01	2.25062 01	2.90115 00	2.14940 02	1.85862 01	1.85862 01	1.85862 01	1.85862 01	1.85862 01
242	2.14741 01	1.81522 01	3.41934 00	1.70378 02	1.52271 01	1.52271 01	1.52271 01	1.52271 01	1.52271 01
243	2.14472 01	1.50855 01	3.89779 00	1.32881 02	1.25505 01	1.25505 01	1.25505 01	1.25505 01	1.25505 01
244	2.14204 01	1.28513 01	4.32050 00	1.02131 02	1.04916 01	1.04916 01	1.04916 01	1.04916 01	1.04916 01
245	2.13937 01	1.11161 01	4.69968 00	7.75167 01	8.96761 00	8.96761 00	8.96761 00	8.96761 00	8.96761 00
246	2.13670 01	8.61602 00	5.34866 00	5.82565 01	7.86883 00	7.86883 00	7.86883 00	7.86883 00	7.86883 00
247	2.13403 01	9.73572 00	5.34866 00	4.35014 01	7.16684 00	7.16684 00	7.16684 00	7.16684 00	7.16684 00
248	2.13136 01	7.69305 00	5.62808 00	3.24147 01	6.72052 00	6.72052 00	6.72052 00	6.72052 00	6.72052 00
249	2.12870 01	6.92179 00	5.88277 00	2.42276 01	6.47947 00	6.47947 00	6.47947 00	6.47947 00	6.47947 00
250	2.12604 01	6.26970 00	6.11596 00	1.82704 01	6.38550 00	6.38550 00	6.38550 00	6.38550 00	6.38550 00
251	2.12338 01	5.71271 00	6.33034 00	1.09282 01	6.39257 00	6.39257 00	6.39257 00	6.39257 00	6.39257 00
252	2.12073 01	5.23263 00	6.52819 00	1.09282 01	6.46566 00	6.46566 00	6.46566 00	6.46566 00	6.46566 00
253	2.11808 01	4.81553 00	6.71143 00	8.75196 00	6.57918 00	6.57918 00	6.57918 00	6.57918 00	6.57918 00
254	2.11543 01	4.45053 00	6.88172 00	7.19838 00	6.71511 00	6.71511 00	6.71511 00	6.71511 00	6.71511 00
255	2.11279 01	4.12904 00	7.04044 00	6.07856 00	6.86131 00	6.86131 00	6.86131 00	6.86131 00	6.86131 00
256	2.11015 01	3.84421 00	7.19881 00	5.25803 00	7.00995 00	7.00995 00	7.00995 00	7.00995 00	7.00995 00
257	2.10752 01	3.59050 00	7.32786 00	4.64307 00	7.15625 00	7.15625 00	7.15625 00	7.15625 00	7.15625 00
258	2.10488 01	3.36340 00	7.45850 00	4.16955 00	7.29750 00	7.29750 00	7.29750 00	7.29750 00	7.29750 00
259	2.10225 01	3.15919 00	7.58151 00	3.79420 00	7.43235 00	7.43235 00	7.43235 00	7.43235 00	7.43235 00

GAROL DATA TAPE, LABELED THORIUM TAPE FOR			GAROL SAMPLE			PROBLEMS		
ENERGY-EV			TH232 300			TH232 2000		
	CAPTURE	SCATTER		CAPTURE	SCATTER		CAPTURE	SCATTER
260	2.09963 01	2.97481 00	7.69760 00	3.48809 00	7.56029 00			
261	2.09701 01	2.80768 00	7.80736 00	3.23194 00	7.68131 00			
262	2.09439 01	2.65565 00	7.91133 00	3.01287 00	7.79568 00			
263	2.09177 01	2.51688 00	8.01000 00	2.82218 00	7.90379 00			
264	2.08916 01	2.38982 00	8.10379 00	2.64720 00	8.00848 00			
265	2.08655 01	2.27315 00	8.19306 00	2.49964 00	8.10430 00			
266	2.08394 01	2.16571 00	8.27817 00	2.36602 00	8.19630 00			
267	2.08134 01	2.06654 00	8.35943 00	2.24451 00	8.28336 00			
268	2.07874 01	1.97475 00	8.43710 00	2.13356 00	8.36631 00			
269	2.07614 01	1.88962 00	8.51144 00	2.03188 00	8.44544 00			
270	2.07355 01	1.81049 00	8.58267 00	1.93840 00	8.52103 00			
271	2.07096 01	1.73678 00	8.65099 00	1.85219 00	8.59333 00			
272	2.06837 01	1.66798 00	8.71650 00	1.77246 00	8.66257 00			
273	2.06578 01	1.60367 00	8.77966 00	1.69852 00	8.72895 00			
274	2.06320 01	1.54342 00	8.84034 00	1.62979 00	8.79266 00			
275	2.06063 01	1.48691 00	8.89876 00	1.56576 00	8.85388 00			
276	2.05805 01	1.43380 00	8.95508 00	1.50597 00	8.91276 00			
277	2.05548 01	1.38382 00	9.00940 00	1.45004 00	8.96945 00			
278	2.05291 01	1.33672 00	9.06183 00	1.39761 00	9.02407 00			
279	2.05035 01	1.29227 00	9.11249 00	1.34839 00	9.07674 00			
280	2.04779 01	1.25026 00	9.16147 00	1.30209 00	9.12759 00			
281	2.04523 01	1.21052 00	9.20885 00	1.25847 00	9.17670 00			
282	2.04268 01	1.17287 00	9.25472 00	1.21732 00	9.22418 00			
283	2.04012 01	1.13716 00	9.29916 00	1.17844 00	9.27011 00			
284	2.03757 01	1.10326 00	9.34223 00	1.14166 00	9.31457 00			
285	2.03503 01	1.07104 00	9.38400 00	1.10681 00	9.35764 00			
286	2.03249 01	1.04038 00	9.42453 00	1.07376 00	9.39939 00			
287	2.02995 01	1.01118 00	9.46389 00	1.04238 00	9.43938 00			
288	2.02741 01	9.83343-01	9.50212 00	1.01255 00	9.47918 00			
289	2.02488 01	9.56785-01	9.53928 00	9.84154-01	9.51733 00			
290	2.02235 01	9.31422-01	9.57541 00	9.57107-01	9.55440 00			
291	2.01982 01	9.07181-01	9.61056 00	9.31315-01	9.59343 00			
292	2.01730 01	8.83993-01	9.64478 00	9.06698-01	9.62547 00			
293	2.01478 01	8.61794-01	9.67809 00	8.83179-01	9.65957 00			
294	2.01226 01	8.40526-01	9.71054 00	8.60692-01	9.69275 00			
295	2.00975 01	8.20136-01	9.74217 00	8.39172-01	9.72507 00			
296	2.00724 01	8.00572-01	9.77300 00	8.18561-01	9.75556 00			
297	2.00473 01	7.81790-01	9.80307 00	7.98806-01	9.78725 00			
298	2.00223 01	7.63745-01	9.83240 00	7.79857-01	9.81717 00			
299	1.99973 01	7.46397-01	9.86103 00	7.61668-01	9.84636 00			
300	1.99723 01	7.29709-01	9.88899 00	7.44196-01	9.87434 00			
301	1.99473 01	7.13647-01	9.91629 00	7.27402-01	9.90255 00			
302	1.99224 01	6.98177-01	9.94296 00	7.11249-01	9.92979 00			
303	1.98975 01	6.83270-01	9.96903 00	6.95703-01	9.95631 00			
304	1.98727 01	6.68897-01	9.99451 00	6.80732-01	9.98223 00			
305	1.98478 01	6.55032-01	1.00194 01	6.66306-01	1.00076 01			
306	1.98230 01	6.41649-01	1.00438 01	6.52397-01	1.00323 01			
307	1.97983 01	6.28726-01	1.00677 01	6.38980-01	1.00565 01			
308	1.97736 01	6.16240-01	1.00910 01	6.26030-01	1.00802 01			
309	1.97488 01	6.04171-01	1.01139 01	6.13525-01	1.01034 01			
310	1.97242 01	5.92499-01	1.01362 01	6.01442-01	1.01261 01			
311	1.96995 01	5.81207-01	1.01582 01	5.89763-01	1.01484 01			

GAROL DATA TAPE, LABELED THORIUM TAPE FOR GAROL SAMPLE PROBLEMS

	ENERGY-EV	CAPTURE	SCATTER	CAPTURE	SCATTER
112	1.96749 01	5.70277-01	1.01796 01	5.78468-01	1.01701 01
113	1.96504 01	5.59694-01	1.02007 01	5.67539-01	1.01915 01
114	1.96258 01	5.49441-01	1.02213 01	5.55961-01	1.02124 01
115	1.96013 01	5.39505-01	1.02415 01	5.46717-01	1.02328 01
116	1.95768 01	5.29872-01	1.02614 01	5.36792-01	1.02529 01
117	1.95523 01	5.20528-01	1.02808 01	5.27173-01	1.02726 01
118	1.95279 01	5.11463-01	1.02999 01	5.17847-01	1.02919 01
119	1.95035 01	5.02665-01	1.03186 01	5.03801-01	1.03109 01
120	1.94792 01	4.94122-01	1.03379 01	5.00022-01	1.03295 01
121	1.94548 01	4.85824-01	1.03550 01	4.91502-01	1.03477 01
122	1.94305 01	4.77762-01	1.03728 01	4.83227-01	1.03656 01
123	1.94063 01	4.69926-01	1.03902 01	4.75190-01	1.03832 01
124	1.93820 01	4.62307-01	1.04072 01	4.67379-01	1.04005 01
125	1.93578 01	4.54898-01	1.04240 01	4.59787-01	1.04174 01
126	1.93336 01	4.47689-01	1.04405 01	4.52405-01	1.04341 01
127	1.93095 01	4.40674-01	1.04567 01	4.45224-01	1.04505 01
128	1.92853 01	4.33845-01	1.04727 01	4.38237-01	1.04666 01
129	1.92612 01	4.27196-01	1.04883 01	4.31437-01	1.04824 01
130	1.92372 01	4.20719-01	1.05037 01	4.24817-01	1.04979 01
131	1.92132 01	4.14409-01	1.05189 01	4.18369-01	1.05132 01
132	1.91892 01	4.08260-01	1.05338 01	4.12089-01	1.05282 01
133	1.91652 01	4.02266-01	1.05484 01	4.05969-01	1.05430 01
134	1.91412 01	3.96421-01	1.05629 01	4.00004-01	1.05576 01
135	1.91173 01	3.90721-01	1.05770 01	3.94189-01	1.05719 01
136	1.90934 01	3.85159-01	1.05910 01	3.88518-01	1.05860 01
137	1.90696 01	3.79733-01	1.06048 01	3.82986-01	1.05998 01
138	1.90458 01	3.74437-01	1.06183 01	3.77589-01	1.06135 01
139	1.90220 01	3.69266-01	1.06316 01	3.72321-01	1.06269 01
140	1.89982 01	3.64218-01	1.06447 01	3.67180-01	1.06401 01
141	1.89745 01	3.59286-01	1.06575 01	3.62160-01	1.06531 01
142	1.89508 01	3.54469-01	1.06704 01	3.57257-01	1.06659 01
143	1.89271 01	3.49762-01	1.06829 01	3.52468-01	1.06786 01
144	1.89035 01	3.45162-01	1.06952 01	3.47788-01	1.06910 01
145	1.88798 01	3.40665-01	1.07074 01	3.43216-01	1.07033 01
146	1.88563 01	3.36268-01	1.07194 01	3.38746-01	1.07153 01
147	1.88327 01	3.31968-01	1.07312 01	3.34376-01	1.07272 01
148	1.88092 01	3.27762-01	1.07429 01	3.30103-01	1.07390 01
149	1.87857 01	3.23648-01	1.07543 01	3.25923-01	1.07505 01
150	1.87622 01	3.19622-01	1.07657 01	3.21834-01	1.07619 01
151	1.87388 01	3.15682-01	1.07768 01	3.17834-01	1.07732 01
152	1.87154 01	3.11825-01	1.07878 01	3.13919-01	1.07842 01
153	1.86920 01	3.08048-01	1.07987 01	3.10087-01	1.07952 01
154	1.86686 01	3.04351-01	1.08094 01	3.06335-01	1.08059 01
155	1.86453 01	3.00729-01	1.08199 01	3.02662-01	1.08166 01
156	1.86220 01	2.97182-01	1.08304 01	2.99064-01	1.08270 01
157	1.85988 01	2.93707-01	1.08406 01	2.95540-01	1.08374 01
158	1.85755 01	2.90301-01	1.08508 01	2.92088-01	1.08476 01
159	1.85523 01	2.86964-01	1.08608 01	2.88705-01	1.08576 01
160	1.85291 01	2.83692-01	1.08707 01	2.85390-01	1.08676 01
161	1.85060 01	2.80485-01	1.08804 01	2.82141-01	1.08774 01
162	1.84829 01	2.77340-01	1.08900 01	2.78955-01	1.08871 01
163	1.84598 01	2.74257-01	1.08995 01	2.75832-01	1.08966 01

GAROL DATA TAPE, LABELED THORIUM TAPE FOR GAROL SAMPLE PROBLEMS
TH232 300 TH232 2000

	ENERGY-EV	CAPTURE	SCATTER	CAPTURE	SCATTER
364	1.84367 01	2.71232-01	1.09089 01	2.72769-01	1.09060 01
365	1.84137 01	2.68265-01	1.09182 01	2.69765-01	1.09153 01
366	1.83907 01	2.65354-01	1.09273 01	2.66819-01	1.09245 01
367	1.83677 01	2.62498-01	1.09363 01	2.63928-01	1.09336 01
368	1.83448 01	2.59695-01	1.09452 01	2.61091-01	1.09426 01
369	1.83219 01	2.56944-01	1.09541 01	2.58308-01	1.09514 01
370	1.82990 01	2.54243-01	1.09627 01	2.55576-01	1.09602 01
371	1.82761 01	2.51591-01	1.09713 01	2.52894-01	1.09688 01
372	1.82533 01	2.48988-01	1.09798 01	2.50261-01	1.09773 01
373	1.82305 01	2.46431-01	1.09882 01	2.47675-01	1.09858 01
374	1.82077 01	2.43920-01	1.09965 01	2.45136-01	1.09941 01
375	1.81850 01	2.41454-01	1.10047 01	2.42643-01	1.10023 01
376	1.81622 01	2.39030-01	1.10128 01	2.40194-01	1.10105 01
377	1.81396 01	2.36649-01	1.10208 01	2.37787-01	1.10185 01
378	1.81169 01	2.34310-01	1.10287 01	2.35423-01	1.10264 01
379	1.80943 01	2.32011-01	1.10365 01	2.33100-01	1.10343 01
380	1.80717 01	2.29751-01	1.10442 01	2.30817-01	1.10420 01
381	1.80491 01	2.27529-01	1.10519 01	2.28573-01	1.10497 01
382	1.80265 01	2.25345-01	1.10594 01	2.26367-01	1.10573 01
383	1.80040 01	2.23198-01	1.10669 01	2.24199-01	1.10648 01
384	1.79815 01	2.21086-01	1.10743 01	2.22066-01	1.10722 01
385	1.79591 01	2.19010-01	1.10816 01	2.19970-01	1.10795 01
386	1.79366 01	2.16968-01	1.10888 01	2.17908-01	1.10868 01
387	1.79142 01	2.14959-01	1.10959 01	2.15880-01	1.10940 01
388	1.78918 01	2.12982-01	1.11030 01	2.13885-01	1.11011 01
389	1.78695 01	2.11038-01	1.11100 01	2.11923-01	1.11081 01
390	1.78472 01	2.09124-01	1.11169 01	2.09992-01	1.11150 01
391	1.78249 01	2.07242-01	1.11237 01	2.08092-01	1.11219 01
392	1.78026 01	2.05389-01	1.11305 01	2.06223-01	1.11286 01
393	1.77804 01	2.03565-01	1.11372 01	2.04383-01	1.11354 01
394	1.77582 01	2.01770-01	1.11438 01	2.02572-01	1.11420 01
395	1.77360 01	2.00002-01	1.11503 01	2.00789-01	1.11485 01
396	1.77138 01	1.98262-01	1.11568 01	1.99034-01	1.11551 01
397	1.76917 01	1.96549-01	1.11632 01	1.97306-01	1.11615 01
398	1.76696 01	1.94862-01	1.11696 01	1.95605-01	1.11679 01
399	1.76475 01	1.93200-01	1.11759 01	1.93930-01	1.11742 01
400	1.76255 01	1.91564-01	1.11821 01	1.92280-01	1.11804 01
401	1.76035 01	1.89953-01	1.11882 01	1.90656-01	1.11866 01

TAPE COMPLETE.

TIME = 7.403 MH

GAROL PROBLEM# 1. THORIUM R=2.2 T=300
 GEOMETRY = CYLIN.
 MEAN CHORD LENGTH OF REGION 1 = 4.400000 00
 REGION 2 = 1.000000 05

DANCOFF CORRECTION = 0.

PLOTTING OF THE RESULTS OF THIS PROBLEM HAS BEEN REQUESTED.

UPPER ENERGY LIMIT = 2.902321 01 EV

LOWER ENERGY LIMIT = 1.760347 01 EV

NUMBER OF BROAD GROUPS = 2

BROAD GROUP BOUNDARIES (EV)

1 2.902321 01 TO 2.260330 01
 2 2.260330 01 TO 1.760347 01

NUMBER OF MATERIALS = 2

MATERIAL I.D.	DESCRIPTION	D E N S I T Y	
		REGION 1	REGION 2
1	1.0 HYDROGEN	0.	1.000000 00
2	90.232 TH232 300K, GAM=24.5, TWO RES	3.037000-02	0.

GAROL PROBLEM 1, THORIUM R=2.2 T=300

POINT	ENERGY-EV	FLUX		SOURCE	REGION		TOTAL CROSS SECTION		COLLISION		DENSITY
		REGION 1	REGION 2		REGION 1	REGION 2	REGION 1	REGION 2	REGION 1	REGION 2	
1	2.902321	01	3.255428-02	1.318468-02	1.566144	04	4.234015-01	2.000000	4.000423-01	2.000000	01
2	2.898696	01	3.263290-02	3.4445518-02	1.566144	04	4.236767-01	2.000000	4.007679-01	2.000000	01
3	2.895075	01	3.271380-02	3.454142-02	1.566144	04	4.239553-01	2.000000	4.015234-01	2.000000	01
4	2.891458	01	3.279707-02	3.458462-02	1.566144	04	4.242374-01	2.000000	4.023100-01	2.000000	01
5	2.887846	01	3.289283-02	3.462788-02	1.566144	04	4.245230-01	2.000000	4.031294-01	2.000000	01
6	2.884238	01	3.297119-02	3.467119-02	1.566144	04	4.248123-01	2.000000	4.039828-01	2.000000	01
7	2.880635	01	3.306227-02	3.471456-02	1.566144	04	4.251052-01	2.000000	4.048718-01	2.000000	01
8	2.877037	01	3.315620-02	3.475798-02	1.566144	04	4.254020-01	2.000000	4.057977-01	2.000000	01
9	2.873443	01	3.323308-02	3.480145-02	1.566144	04	4.257025-01	2.000000	4.067623-01	2.000000	01
10	2.869853	01	3.333070-02	3.484498-02	1.566144	04	4.260070-01	2.000000	4.077671-01	2.000000	01
11	2.866258	01	3.343628-02	3.498856-02	1.566144	04	4.263154-01	2.000000	4.088137-01	1.999999	01
12	2.862638	01	3.356286-02	3.493220-02	1.566144	04	4.266279-01	2.000000	4.099040-01	1.999999	01
13	2.859111	01	3.367294-02	3.497599-02	1.566144	04	4.269445-01	2.000000	4.110395-01	1.999999	01
14	2.855540	01	3.378672-02	3.501964-02	1.566144	04	4.272654-01	2.000000	4.122227-01	1.999999	01
15	2.851973	01	3.389401-02	3.506344-02	1.566144	04	4.275906-01	2.000000	4.133295-01	1.999999	01
16	2.848410	01	3.396379-02	3.510729-02	1.566144	04	4.279201-01	2.000000	4.139819-01	1.999999	01
17	2.844852	01	3.403308-02	3.515121-02	1.566144	04	4.282542-01	2.000000	4.146317-01	1.999999	01
18	2.841298	01	3.410176-02	3.519517-02	1.566144	04	4.285929-01	2.000000	4.152776-01	1.999999	01
19	2.837748	01	3.416970-02	3.523919-02	1.566144	04	4.289362-01	2.000000	4.159180-01	1.999999	01
20	2.834203	01	3.423676-02	3.528327-02	1.566144	04	4.292843-01	2.000000	4.165515-01	1.999999	01
21	2.830663	01	3.430277-02	3.532740-02	1.566144	04	4.296373-01	2.000000	4.171759-01	1.999999	01
22	2.827127	01	3.436757-02	3.537159-02	1.566144	04	4.299952-01	2.000000	4.177897-01	1.999999	01
23	2.823598	01	3.443098-02	3.541583-02	1.566144	04	4.303583-01	2.000000	4.183907-01	1.999999	01
24	2.820068	01	3.449282-02	3.546012-02	1.566144	04	4.307265-01	2.000000	4.189767-01	1.999999	01
25	2.816545	01	3.455286-02	3.550448-02	1.566144	04	4.311001-01	2.000000	4.195453-01	1.999999	01
26	2.813024	01	3.461094-02	3.554888-02	1.566144	04	4.314791-01	2.000000	4.200945-01	1.999999	01
27	2.809512	01	3.466676-02	3.559335-02	1.566144	04	4.318636-01	2.000000	4.206208-01	1.999999	01
28	2.806007	01	3.472009-02	3.563787-02	1.566144	04	4.322538-01	2.000000	4.211218-01	1.999999	01
29	2.802492	01	3.477100-02	3.568244-02	1.566144	04	4.326498-01	2.000000	4.215982-01	1.999999	01
30	2.798996	01	3.482055-02	3.572707-02	1.566144	04	4.330517-01	2.000000	4.220634-01	1.999999	01
31	2.795500	01	3.486915-02	3.577176-02	1.566144	04	4.334597-01	2.000000	4.225222-01	1.999999	01
32	2.792007	01	3.491682-02	3.581650-02	1.566144	04	4.338738-01	2.000000	4.229751-01	1.999999	01
33	2.788520	01	3.496352-02	3.586130-02	1.566144	04	4.342944-01	2.000000	4.234217-01	1.999999	01
34	2.785036	01	3.500924-02	3.590615-02	1.566144	04	4.347214-01	2.000000	4.238671-01	1.999999	01
35	2.781557	01	3.505402-02	3.595106-02	1.566144	04	4.351550-01	2.000000	4.242968-01	1.999999	01
36	2.778082	01	3.509779-02	3.599602-02	1.566144	04	4.355955-01	2.000000	4.247254-01	1.999999	01
37	2.774612	01	3.514062-02	3.604105-02	1.566144	04	4.360429-01	2.000000	4.251487-01	1.999999	01
38	2.771146	01	3.518253-02	3.608613-02	1.566144	04	4.364974-01	2.000000	4.255811-01	1.999999	01
39	2.767684	01	3.522353-02	3.613126-02	1.566144	04	4.369593-01	2.000000	4.259811-01	1.999999	01
40	2.764226	01	3.526366-02	3.617645-02	1.566144	04	4.374286-01	2.000000	4.263912-01	1.999999	01
41	2.760773	01	3.530298-02	3.622170-02	1.566144	04	4.379055-01	2.000000	4.267982-01	1.999999	01
42	2.757325	01	3.534154-02	3.626701-02	1.566144	04	4.383904-01	2.000000	4.272031-01	1.999999	01
43	2.753880	01	3.537943-02	3.631237-02	1.566144	04	4.388833-01	2.000000	4.276071-01	1.999999	01
44	2.750440	01	3.541663-02	3.635778-02	1.566144	04	4.393845-01	2.000000	4.280102-01	1.999999	01
45	2.747004	01	3.545323-02	3.640326-02	1.566144	04	4.398941-01	2.000000	4.284135-01	1.999999	01
46	2.743572	01	3.548919-02	3.644849-02	1.566144	04	4.404124-01	2.000000	4.288170-01	1.999999	01
47	2.740145	01	3.552451-02	3.649438-02	1.566144	04	4.409396-01	2.000000	4.292208-01	1.999999	01
48	2.736722	01	3.555922-02	3.654003-02	1.566144	04	4.414759-01	2.000000	4.296253-01	1.999999	01
49	2.733303	01	3.559332-02	3.658573-02	1.566144	04	4.420215-01	2.000000	4.300310-01	1.999999	01
50	2.729889	01	3.562866-02	3.663149-02	1.566144	04	4.425769-01	2.000000	4.304387-01	1.999999	01
51	2.726478	01	3.566598-02	3.667731-02	1.566144	04	4.431422-01	2.000000	4.308478-01	1.999999	01
52	2.723072	01	3.569215-02	3.672318-02	1.566144	04	4.437176-01	2.000000	4.312593-01	1.999999	01

GAROL PROBLEM 1. THORIUM R=2.2 T=300

POINT	ENERGY-EV	FLUX		SOURCE		TOTAL CROSS SECTION		COLLISION		DENSITY
		REGION 1	REGION 2	REGION 1	REGION 2	REGION 1	REGION 2	REGION 1	REGION 2	
53	2.719671	01	3.572395-02	0.	1.566144	4.443034-01	2.000000	4.316735-01	1.999998	01
54	2.716273	01	3.575519-02	0.	1.566144	4.449000-01	2.000000	4.320907-01	1.999997	01
55	2.712880	01	3.578588-02	0.	1.566144	4.455075-01	2.000000	4.325111-01	1.999997	01
56	2.709491	01	3.581601-02	0.	1.566144	4.461264-01	2.000000	4.329351-01	1.999997	01
57	2.706106	01	3.584558-02	0.	1.566144	4.467573-01	2.000000	4.333629-01	1.999997	01
58	2.702726	01	3.587457-02	0.	1.566144	4.473995-01	2.000000	4.337947-01	1.999997	01
59	2.699349	01	3.590301-02	0.	1.566144	4.480544-01	2.000000	4.342309-01	1.999997	01
60	2.695977	01	3.593090-02	0.	1.566144	4.487220-01	2.000000	4.346720-01	1.999997	01
61	2.692610	01	3.595819-02	0.	1.566144	4.494026-01	2.000000	4.351177-01	1.999997	01
62	2.689246	01	3.598490-02	0.	1.566144	4.500957-01	2.000000	4.355687-01	1.999997	01
63	2.685886	01	3.601101-02	0.	1.566144	4.508047-01	2.000000	4.360249-01	1.999997	01
64	2.682531	01	3.603652-02	0.	1.566144	4.515269-01	2.000000	4.364869-01	1.999997	01
65	2.679180	01	3.606139-02	0.	1.566144	4.522639-01	2.000000	4.369546-01	1.999997	01
66	2.675833	01	3.608563-02	0.	1.566144	4.530161-01	2.000000	4.374283-01	1.999997	01
67	2.672490	01	3.610925-02	0.	1.566144	4.537839-01	2.000000	4.379088-01	1.999997	01
68	2.669152	01	3.613218-02	0.	1.566144	4.545679-01	2.000000	4.383957-01	1.999997	01
69	2.665818	01	3.615444-02	0.	1.566144	4.553686-01	2.000000	4.388895-01	1.999997	01
70	2.662487	01	3.617600-02	0.	1.566144	4.561865-01	2.000000	4.393904-01	1.999997	01
71	2.659161	01	3.619685-02	0.	1.566144	4.570222-01	2.000000	4.398987-01	1.999997	01
72	2.655839	01	3.621693-02	0.	1.566144	4.578762-01	2.000000	4.404145-01	1.999997	01
73	2.652522	01	3.623625-02	0.	1.566144	4.587493-01	2.000000	4.409381-01	1.999997	01
74	2.649208	01	3.625480-02	0.	1.566144	4.596420-01	2.000000	4.414701-01	1.999997	01
75	2.645899	01	3.627254-02	0.	1.566144	4.605550-01	2.000000	4.420106-01	1.999997	01
76	2.642593	01	3.628944-02	0.	1.566144	4.614890-01	2.000000	4.425597-01	1.999996	01
77	2.639292	01	3.630544-02	0.	1.566144	4.624448-01	2.000000	4.431177-01	1.999996	01
78	2.635995	01	3.632050-02	0.	1.566144	4.634231-01	2.000000	4.436850-01	1.999996	01
79	2.632702	01	3.633474-02	0.	1.566144	4.644247-01	2.000000	4.442619-01	1.999996	01
80	2.629413	01	3.634794-02	0.	1.566144	4.654505-01	2.000000	4.448485-01	1.999996	01
81	2.626129	01	3.636013-02	0.	1.566144	4.665014-01	2.000000	4.454533-01	1.999996	01
82	2.622848	01	3.637126-02	0.	1.566144	4.675783-01	2.000000	4.460524-01	1.999996	01
83	2.619571	01	3.638134-02	0.	1.566144	4.686822-01	2.000000	4.466707-01	1.999996	01
84	2.616299	01	3.639028-02	0.	1.566144	4.698141-01	2.000000	4.473000-01	1.999996	01
85	2.613031	01	3.640458-02	0.	1.566144	4.709752-01	2.000000	4.479406-01	1.999996	01
86	2.609766	01	3.641981-02	0.	1.566144	4.721665-01	2.000000	4.485934-01	1.999996	01
87	2.606506	01	3.643572-02	0.	1.566144	4.733893-01	2.000000	4.492579-01	1.999996	01
88	2.603250	01	3.645132-02	0.	1.566144	4.746448-01	2.000000	4.499349-01	1.999996	01
89	2.599998	01	3.646732-02	0.	1.566144	4.759344-01	2.000000	4.506250-01	1.999996	01
90	2.596750	01	3.648374-02	0.	1.566144	4.772595-01	2.000000	4.513285-01	1.999996	01
91	2.593506	01	3.649967-02	0.	1.566144	4.786216-01	2.000000	4.520456-01	1.999996	01
92	2.590266	01	3.651687-02	0.	1.566144	4.800222-01	2.000000	4.527770-01	1.999996	01
93	2.587031	01	3.653486-02	0.	1.566144	4.814630-01	2.000000	4.535227-01	1.999996	01
94	2.583799	01	3.655278-02	0.	1.566144	4.829459-01	2.000000	4.542840-01	1.999996	01
95	2.580571	01	3.657102-02	0.	1.566144	4.844725-01	2.000000	4.550609-01	1.999995	01
96	2.577347	01	3.658947-02	0.	1.566144	4.860451-01	2.000000	4.558534-01	1.999995	01
97	2.574128	01	3.660797-02	0.	1.566144	4.876655-01	2.000000	4.566625-01	1.999995	01
98	2.570912	01	3.662622-02	0.	1.566144	4.893361-01	2.000000	4.574890-01	1.999995	01
99	2.567700	01	3.664486-02	0.	1.566144	4.910593-01	2.000000	4.583329-01	1.999995	01
100	2.564493	01	3.666324-02	0.	1.566144	4.928375-01	2.000000	4.591953-01	1.999995	01
101	2.561289	01	3.668120-02	0.	1.566144	4.946735-01	2.000000	4.600762-01	1.999995	01
102	2.558090	01	3.669864-02	0.	1.566144	4.965701-01	2.000000	4.609767-01	1.999995	01
103	2.554894	01	3.671646-02	0.	1.566144	4.985304-01	2.000000	4.618976-01	1.999995	01
104	2.551702	01	3.673468-02	0.	1.566144	5.005576-01	2.000000	4.628391-01	1.999995	01

GAROL PROBLEM 1, THORIUM R=2.2 I=300

POINT	ENERGY-EV	FLUX		SOURCE		TOTAL CROSS SECTION		COLLISION		DENSITY
		REGION 1	REGION 2	REGION 1	REGION 2	REGION 1	REGION 2	REGION 1	REGION 2	
105	2.548515	01	3.620560-02	0.	1.566144	04	5.026553-01	2.000000	01	1.999995
106	2.545331	01	3.617164-02	0.	1.566144	04	5.048271-01	2.000000	01	1.999995
107	2.542151	01	3.613439-02	0.	1.566144	04	5.070771-01	2.000000	01	1.999995
108	2.538976	01	3.609375-02	0.	1.566144	04	5.094096-01	2.000000	01	1.999995
109	2.535804	01	3.604949-02	0.	1.566144	04	5.118291-01	2.000000	01	1.999995
110	2.532636	01	3.600144-02	0.	1.566144	04	5.143407-01	2.000000	01	1.999995
111	2.529472	01	3.594938-02	0.	1.566144	04	5.169496-01	2.000000	01	1.999995
112	2.526312	01	3.589308-02	0.	1.566144	04	5.196617-01	2.000000	01	1.999995
113	2.523156	01	3.583233-02	0.	1.566144	04	5.224832-01	2.000000	01	1.999995
114	2.520004	01	3.576681-02	0.	1.566144	04	5.254208-01	2.000000	01	1.999994
115	2.516856	01	3.569629-02	0.	1.566144	04	5.284817-01	2.000000	01	1.999994
116	2.513712	01	3.562040-02	0.	1.566144	04	5.316740-01	2.000000	01	1.999994
117	2.510572	01	3.553890-02	0.	1.566144	04	5.350061-01	2.000000	01	1.999994
118	2.507436	01	3.545140-02	0.	1.566144	04	5.384874-01	2.000000	01	1.999994
119	2.504303	01	3.535753-02	0.	1.566144	04	5.421281-01	2.000000	01	1.999994
120	2.501175	01	3.525693-02	0.	1.566144	04	5.459393-01	2.000000	01	1.999994
121	2.498051	01	3.514917-02	0.	1.566144	04	5.499331-01	2.000000	01	1.999994
122	2.494930	01	3.503376-02	0.	1.566144	04	5.541230-01	2.000000	01	1.999994
123	2.491813	01	3.491015-02	0.	1.566144	04	5.585236-01	2.000000	01	1.999994
124	2.488700	01	3.477785-02	0.	1.566144	04	5.631508-01	2.000000	01	1.999994
125	2.485591	01	3.463629-02	0.	1.566144	04	5.680227-01	2.000000	01	1.999994
126	2.482486	01	3.448483-02	0.	1.566144	04	5.731587-01	2.000000	01	1.999994
127	2.479385	01	3.432278-02	0.	1.566144	04	5.785808-01	2.000000	01	1.999994
128	2.476288	01	3.414935-02	0.	1.566144	04	5.843130-01	2.000000	01	1.999994
129	2.473195	01	3.396379-02	0.	1.566144	04	5.903825-01	2.000000	01	1.999994
130	2.470105	01	3.376517-02	0.	1.566144	04	5.968193-01	2.000000	01	1.999994
131	2.467019	01	3.355250-02	0.	1.566144	04	6.036572-01	2.000000	01	1.999994
132	2.463937	01	3.332480-02	0.	1.566144	04	6.109341-01	2.000000	01	1.999994
133	2.460859	01	3.308101-02	0.	1.566144	04	6.186928-01	2.000000	01	1.999993
134	2.457785	01	3.281975-02	0.	1.566144	04	6.269819-01	2.000000	01	1.999993
135	2.454715	01	3.253968-02	0.	1.566144	04	6.358561-01	2.000000	01	1.999993
136	2.451648	01	3.223947-02	0.	1.566144	04	6.453784-01	2.000000	01	1.999993
137	2.448586	01	3.191728-02	0.	1.566144	04	6.556203-01	2.000000	01	1.999993
138	2.445527	01	3.157144-02	0.	1.566144	04	6.666643-01	2.000000	01	1.999993
139	2.442472	01	3.120001-02	0.	1.566144	04	6.786057-01	2.000000	01	1.999993
140	2.439421	01	3.080090-02	0.	1.566144	04	6.915551-01	2.000000	01	1.999993
141	2.436373	01	3.037173-02	0.	1.566144	04	7.056415-01	2.000000	01	1.999993
142	2.433330	01	2.991006-02	0.	1.566144	04	7.210162-01	2.000000	01	1.999993
143	2.430290	01	2.941297-02	0.	1.566144	04	7.378579-01	2.000000	01	1.999993
144	2.427254	01	2.887745-02	0.	1.566144	04	7.563797-01	2.000000	01	1.999993
145	2.424222	01	2.830029-02	0.	1.566144	04	7.768237-01	2.000000	01	1.999993
146	2.421193	01	2.767771-02	0.	1.566144	04	7.995285-01	2.000000	01	1.999993
147	2.418169	01	2.700594-02	0.	1.566144	04	8.248344-01	2.000000	01	1.999993
148	2.415148	01	2.628073-02	0.	1.566144	04	8.532156-01	2.000000	01	1.999993
149	2.412131	01	2.549742-02	0.	1.566144	04	8.852341-01	2.000000	01	1.999992
150	2.409118	01	2.465129-02	0.	1.566144	04	9.216055-01	2.000000	01	1.999992
151	2.406108	01	2.373707-02	0.	1.566144	04	9.632162-01	2.000000	01	1.999992
152	2.403102	01	2.274987-02	0.	1.566144	04	1.011296 00	2.000000	01	1.999992
153	2.400100	01	2.168397-02	0.	1.566144	04	1.067318 00	2.000000	01	1.999992
154	2.397102	01	2.053394-02	0.	1.566144	04	1.133350 00	2.000000	01	1.999992
155	2.394108	01	1.929513-02	0.	1.566144	04	1.212193 00	2.000000	01	1.999992
156	2.391117	01	1.796262-02	0.	1.566144	04	1.307771 00	2.000000	01	1.999992

POINT	CAROL PROBLEM	1, ENERGY-EV	THORIUM R=2.2		T=300	SOURCE		TOTAL CROSS SECTION		COLLISION		DENSITY
			REGION 1	REGION 2		REGION 1	REGION 2	REGION 1	REGION 2	REGION 1	REGION 2	
157	2.388130	01	1.653285-02	4.187360-02	0.	1.566144	04	1.425768 00	2.000000 01	5.629304-01	1.999992 01	
158	2.385147	01	1.500319-02	4.192591-02	0.	1.566144	04	1.574737 00	2.000000 01	5.635165-01	1.999992 01	
159	2.382167	01	1.334777-02	4.197841-02	0.	1.566144	04	1.771920 00	2.000000 01	5.634107-01	1.999992 01	
160	2.379191	01	1.157358-02	4.203091-02	0.	1.566144	04	2.042169 00	2.000000 01	5.623268-01	1.999992 01	
161	2.376219	01	9.634381-03	4.208349-02	0.	1.566144	04	2.445896 00	2.000000 01	5.601776-01	1.999992 01	
162	2.373251	01	7.496622-03	4.213612-02	0.	1.566144	04	3.128956 00	2.000000 01	5.566543-01	1.999992 01	
163	2.370286	01	5.249934-03	4.218892-02	0.	1.566144	04	4.426420 00	2.000000 01	5.508168-01	1.999991 01	
164	2.367325	01	3.235904-03	4.224159-02	0.	1.566144	04	7.064778 00	2.000000 01	5.411927-01	1.999991 01	
165	2.364368	01	1.805631-03	4.229442-02	0.	1.566144	04	1.234352 01	2.000000 01	5.269666-01	1.999991 01	
166	2.361414	01	9.788079-04	4.234732-02	0.	1.566144	04	2.202142 01	2.000000 01	5.089966-01	1.999991 01	
167	2.358464	01	5.530087-04	4.240023-02	0.	1.566144	04	3.747956 01	2.000000 01	4.888276-01	1.999991 01	
168	2.355518	01	3.415327-04	4.245332-02	0.	1.566144	04	5.813277 01	2.000000 01	4.676701-01	1.999991 01	
169	2.352575	01	2.368779-04	4.250642-02	0.	1.566144	04	8.037792 01	2.000000 01	4.462527-01	1.999991 01	
170	2.349636	01	1.871217-04	4.255958-02	0.	1.566144	04	9.566346 01	2.000000 01	4.249982-01	1.999991 01	
171	2.346701	01	1.694894-04	4.261282-02	0.	1.566144	04	1.016178 02	2.000000 01	4.041755-01	1.999991 01	
172	2.343770	01	1.764206-04	4.266611-02	0.	1.566144	04	9.286864 01	2.000000 01	3.840017-01	1.999991 01	
173	2.340842	01	2.107620-04	4.271948-02	0.	1.566144	04	7.391452 01	2.000000 01	3.646650-01	1.999991 01	
174	2.337917	01	2.875044-04	4.277291-02	0.	1.566144	04	5.153019 01	2.000000 01	3.463662-01	1.999991 01	
175	2.334997	01	4.429184-04	4.282641-02	0.	1.566144	04	3.184314 01	2.000000 01	3.293259-01	1.999991 01	
176	2.332080	01	7.544975-04	4.287993-02	0.	1.566144	04	1.783715 01	2.000000 01	3.138533-01	1.999991 01	
177	2.329167	01	1.366933-03	4.293361-02	0.	1.566144	04	9.428705 00	2.000000 01	3.001925-01	1.999991 01	
178	2.326257	01	2.472445-03	4.298731-02	0.	1.566144	04	5.012454 00	2.000000 01	2.882934-01	1.999991 01	
179	2.323351	01	4.137257-03	4.304108-02	0.	1.566144	04	2.899351 00	2.000000 01	2.777331-01	1.999991 01	
180	2.320449	01	6.102974-03	4.309491-02	0.	1.566144	04	1.893075 00	2.000000 01	2.680904-01	1.999993 01	
181	2.317550	01	7.996345-03	4.314881-02	0.	1.566144	04	1.399618 00	2.000000 01	2.593761-01	1.999990 01	
182	2.314655	01	9.654020-03	4.320278-02	0.	1.566144	04	1.126122 00	2.000000 01	2.516401-01	1.999990 01	
183	2.311763	01	1.108658-02	4.325682-02	0.	1.566144	04	9.555544-01	2.000000 01	2.449043-01	1.999990 01	
184	2.308875	01	1.234768-02	4.331092-02	0.	1.566144	04	8.389201-01	2.000000 01	2.391699-01	1.999990 01	
185	2.305991	01	1.344748-02	4.336509-02	0.	1.566144	04	7.563022-01	2.000000 01	2.345275-01	1.999990 01	
186	2.303110	01	1.442793-02	4.341933-02	0.	1.566144	04	6.949570-01	2.000000 01	2.309280-01	1.999990 01	
187	2.300233	01	1.530807-02	4.347364-02	0.	1.566144	04	6.485855-01	2.000000 01	2.283808-01	1.999990 01	
188	2.297360	01	1.610617-02	4.352802-02	0.	1.566144	04	6.131110-01	2.000000 01	2.268613-01	1.999990 01	
189	2.294490	01	1.684101-02	4.358246-02	0.	1.566144	04	5.857898-01	2.000000 01	2.263581-01	1.999990 01	
190	2.291623	01	1.752846-02	4.363697-02	0.	1.566144	04	5.647175-01	2.000000 01	2.268393-01	1.999990 01	
191	2.288761	01	1.818389-02	4.369155-02	0.	1.566144	04	5.485393-01	2.000000 01	2.282942-01	1.999990 01	
192	2.285902	01	1.881844-02	4.374620-02	0.	1.566144	04	5.362725-01	2.000000 01	2.306889-01	1.999990 01	
193	2.283046	01	1.943636-02	4.380091-02	0.	1.566144	04	5.271942-01	2.000000 01	2.339377-01	1.999990 01	
194	2.280194	01	2.003135-02	4.385570-02	0.	1.566144	04	5.207671-01	2.000000 01	2.378623-01	1.999990 01	
195	2.277346	01	2.059365-02	4.391055-02	0.	1.566144	04	5.165903-01	2.000000 01	2.422750-01	1.999990 01	
196	2.274501	01	2.111445-02	4.396547-02	0.	1.566144	04	5.143649-01	2.000000 01	2.470228-01	1.999990 01	
197	2.271659	01	2.158875-02	4.402047-02	0.	1.566144	04	5.138712-01	2.000000 01	2.520142-01	1.999990 01	
198	2.268821	01	2.201423-02	4.407552-02	0.	1.566144	04	5.149520-01	2.000000 01	2.571998-01	1.999990 01	
199	2.265987	01	2.238990-02	4.413066-02	0.	1.566144	04	5.175018-01	2.000000 01	2.625556-01	1.999990 01	
200	2.263156	01	2.271469-02	4.418585-02	0.	1.566144	04	5.214584-01	2.000000 01	2.680656-01	1.999990 01	
201	2.260329	01	2.298764-02	4.424112-02	0.	1.566144	04	5.267994-01	2.000000 01	2.737230-01	1.999990 01	
202	2.257506	01	2.320770-02	4.429645-02	0.	1.566144	04	5.335387-01	2.000000 01	2.795250-01	1.999990 01	
203	2.254685	01	2.337247-02	4.435186-02	0.	1.566144	04	5.417272-01	2.000000 01	2.854770-01	1.999990 01	
204	2.251869	01	2.348005-02	4.440733-02	0.	1.566144	04	5.514540-01	2.000000 01	2.915758-01	1.999990 01	
205	2.249056	01	2.352658-02	4.446287-02	0.	1.566144	04	5.628505-01	2.000000 01	2.978187-01	1.999990 01	
206	2.246246	01	2.350782-02	4.451849-02	0.	1.566144	04	5.760973-01	2.000000 01	3.042044-01	1.999990 01	
207	2.243440	01	2.341887-02	4.457417-02	0.	1.566144	04	5.914338-01	2.000000 01	3.107324-01	1.999990 01	
208	2.240638	01	2.325311-02	4.462992-02	0.	1.566144	04	6.091725-01	2.000000 01	3.173898-01	1.999990 01	

GAROL PROBLEM 1. THORIUM R=2.2 I=300

POINT	ENERGY-EV	FLUX		SOURCE		TOTAL CROSS SECTION		COLLISION		DENSITY
		REGION 1	REGION 2	REGION 1	REGION 2	REGION 1	REGION 2	REGION 1	REGION 2	
209	2.237839	01	2.300486-02	0.	0.	6.297194-01	2.000000	3.241868-01	1.999989	01
210	2.235043	01	2.266626-02	0.	0.	6.536027-01	2.000000	3.311156-01	1.999989	01
211	2.232251	01	2.222870-02	0.	0.	6.815159-01	2.000000	3.381685-01	1.999989	01
212	2.229462	01	2.168299-02	0.	0.	7.143789-01	2.000000	3.453409-01	1.999989	01
213	2.226677	01	2.101837-02	0.	0.	7.534331-01	2.000000	3.526152-01	1.999989	01
214	2.223896	01	2.022313-02	0.	0.	8.003874-01	2.000000	3.599673-01	1.999989	01
215	2.221117	01	1.928330-02	0.	0.	8.576563-01	2.000000	3.673383-01	1.999989	01
216	2.218343	01	1.818534-02	0.	0.	9.287586-01	2.000000	3.746735-01	1.999989	01
217	2.215572	01	1.691333-02	0.	0.	1.019033	2.000000	3.818591-01	1.999989	01
218	2.212804	01	1.561093-02	0.	0.	1.140444	2.000000	3.889069-01	1.999989	01
219	2.210040	01	1.367080-02	0.	0.	1.309232	2.000000	3.955491-01	1.999989	01
220	2.207279	01	1.160309-02	0.	0.	1.568343	2.000000	4.016723-01	1.999989	01
221	2.204521	01	9.154517-03	0.	0.	2.016235	2.000000	4.069031-01	1.999989	01
222	2.201767	01	6.476127-03	0.	0.	2.876144	2.000000	4.101073-01	1.999989	01
223	2.199017	01	4.049387-03	0.	0.	4.599888	2.000000	4.096050-01	1.999989	01
224	2.196270	01	2.319311-03	0.	0.	7.945043	2.000000	4.047071-01	1.999989	01
225	2.193526	01	1.302934-03	0.	0.	1.386323	2.000000	3.962139-01	1.999989	01
226	2.190786	01	7.646107-04	0.	0.	2.301040	2.000000	3.854468-01	1.999989	01
227	2.188049	01	4.886406-04	0.	0.	3.492521	2.000000	3.734098-01	1.999989	01
228	2.185316	01	3.481765-04	0.	0.	4.740572	2.000000	3.606986-01	1.999989	01
229	2.182586	01	2.800635-04	0.	0.	5.687682	2.000000	3.476668-01	1.999989	01
230	2.179859	01	2.558397-04	0.	0.	5.998726	2.000000	3.345458-01	1.999989	01
231	2.177136	01	2.659727-04	0.	0.	5.552468	2.000000	3.215206-01	1.999989	01
232	2.174417	01	3.143874-04	0.	0.	4.316739	2.000000	3.087684-01	1.999989	01
233	2.171700	01	4.207815-04	0.	0.	3.244537	2.000000	2.964894-01	1.999989	01
234	2.168987	01	6.320492-04	0.	0.	2.078331	2.000000	2.849198-01	1.999989	01
235	2.166278	01	1.046759-03	0.	0.	1.209109	2.000000	2.749151-01	1.999989	01
236	2.163572	01	1.856327-03	0.	0.	6.602263	2.000000	2.651665-01	1.999989	01
237	2.160869	01	3.332613-03	0.	0.	3.570642	2.000000	2.571340-01	1.999989	01
238	2.158169	01	5.638109-03	0.	0.	2.500795	2.000000	2.495406-01	1.999989	01
239	2.155473	01	8.472858-03	0.	0.	1.322159	2.000000	2.414662-01	1.999989	01
240	2.152781	01	1.121553-02	0.	0.	9.641735-01	2.000000	2.327955-01	1.999989	01
241	2.150091	01	1.353289-02	0.	0.	7.716197-01	2.000000	2.245178-01	1.999989	01
242	2.147406	01	1.544531-02	0.	0.	6.551269-01	2.000000	2.172882-01	1.999989	01
243	2.144723	01	1.707918-02	0.	0.	5.765215-01	2.000000	2.111805-01	1.999989	01
244	2.142044	01	1.847226-02	0.	0.	5.215086-01	2.000000	2.063526-01	1.999989	01
245	2.139368	01	1.971553-02	0.	0.	4.533265-01	2.000000	2.025958-01	1.999989	01
246	2.136695	01	2.084236-02	0.	0.	4.487598-01	2.000000	1.998496-01	1.999989	01
247	2.134026	01	2.188195-02	0.	0.	4.241074-01	2.000000	1.980440-01	1.999989	01
248	2.131360	01	2.285908-02	0.	0.	4.045625-01	2.000000	1.971666-01	1.999989	01
249	2.128698	01	2.379390-02	0.	0.	3.888745-01	2.000000	1.969650-01	1.999989	01
250	2.126038	01	2.470379-02	0.	0.	3.761524-01	2.000000	1.975597-01	1.999989	01
251	2.123382	01	2.559994-02	0.	0.	3.657472-01	2.000000	1.988146-01	1.999989	01
252	2.120730	01	2.648520-02	0.	0.	3.571761-01	2.000000	2.006185-01	1.999989	01
253	2.118081	01	2.735229-02	0.	0.	3.500739-01	2.000000	2.028131-01	1.999989	01
254	2.115435	01	2.819047-02	0.	0.	3.441603-01	2.000000	2.052403-01	1.999989	01
255	2.112792	01	2.899184-02	0.	0.	3.392171-01	2.000000	2.077831-01	1.999989	01
256	2.110153	01	2.975522-02	0.	0.	3.350727-01	2.000000	2.103856-01	1.999989	01
257	2.107517	01	3.048088-02	0.	0.	3.315905-01	2.000000	2.130103-01	1.999989	01
258	2.104884	01	3.117193-02	0.	0.	3.286610-01	2.000000	2.156453-01	1.999989	01
259	2.102254	01	3.183131-02	0.	0.	3.261957-01	2.000000	2.182817-01	1.999989	01
260	2.099628	01	3.246164-02	0.	0.	3.241211-01	2.000000	2.209125-01	1.999989	01

GAROL PROBLEM 1, THORIUM R=2.2 T=300

POINT	ENERGY-EV	FLUX		SOURCE		TOTAL CROSS SECTION		COLLISION DENSITY	
		REGION 1	REGION 2	REGION 1	REGION 2	REGION 1	REGION 2	REGION 1	REGION 2
261	2.097005	3.306532-02	4.768675-02	0.	0.	1.556144	3.223789-01	2.000000	2.253315-01
262	2.094386	3.336441-02	4.774639-02	0.	0.	1.566144	3.209192-01	2.000000	2.241319-01
263	2.091769	3.419965-02	4.780611-02	0.	0.	1.566144	3.197013-01	2.000000	2.237072-01
264	2.089156	3.473349-02	4.786591-02	0.	0.	1.566144	3.186907-01	2.000000	2.232538-01
265	2.086546	3.524641-02	4.792577-02	0.	0.	1.566144	3.174897-01	2.000000	2.227637-01
266	2.083940	3.573898-02	4.798572-02	0.	0.	1.566144	3.171899-01	2.000000	2.22297-01
267	2.081337	3.621180-02	4.804574-02	0.	0.	1.566144	3.166365-01	2.000000	2.218457-01
268	2.078737	3.666567-02	4.810583-02	0.	0.	1.566144	3.162088-01	2.000000	2.214003-01
269	2.076140	3.710125-02	4.816600-02	0.	0.	1.566144	3.158801-01	2.000000	2.209545-01
270	2.073546	3.751974-02	4.822625-02	0.	0.	1.566144	3.156400-01	2.000000	2.205098-01
271	2.070956	3.792213-02	4.828656-02	0.	0.	1.566144	3.154765-01	2.000000	2.200651-01
272	2.068369	3.830930-02	4.834696-02	0.	0.	1.566144	3.153798-01	2.000000	2.196204-01
273	2.065785	3.868214-02	4.840743-02	0.	0.	1.566144	3.153417-01	2.000000	2.191757-01
274	2.063204	3.904118-02	4.846798-02	0.	0.	1.566144	3.153543-01	2.000000	2.187310-01
275	2.060627	3.938740-02	4.852860-02	0.	0.	1.566144	3.154128-01	2.000000	2.182863-01
276	2.058053	3.972142-02	4.858930-02	0.	0.	1.566144	3.155102-01	2.000000	2.178416-01
277	2.055482	4.004384-02	4.865007-02	0.	0.	1.566144	3.156421-01	2.000000	2.173969-01
278	2.052914	4.035523-02	4.871092-02	0.	0.	1.566144	3.158041-01	2.000000	2.169522-01
279	2.050349	4.065597-02	4.877185-02	0.	0.	1.566144	3.159927-01	2.000000	2.165075-01
280	2.047788	4.094567-02	4.883285-02	0.	0.	1.566144	3.162044-01	2.000000	2.160628-01
281	2.045230	4.122793-02	4.889393-02	0.	0.	1.566144	3.164303-01	2.000000	2.156181-01
282	2.042675	4.150016-02	4.895508-02	0.	0.	1.566144	3.166860-01	2.000000	2.151734-01
283	2.040123	4.176384-02	4.901631-02	0.	0.	1.566144	3.169510-01	2.000000	2.147287-01
284	2.037575	4.201942-02	4.907762-02	0.	0.	1.566144	3.172294-01	2.000000	2.142840-01
285	2.035029	4.226715-02	4.913900-02	0.	0.	1.566144	3.175193-01	2.000000	2.138393-01
286	2.032480	4.249676-02	4.920047-02	0.	0.	1.566144	3.178193-01	2.000000	2.133946-01
287	2.029948	4.274081-02	4.926262-02	0.	0.	1.566144	3.181277-01	2.000000	2.129499-01
288	2.027412	4.296764-02	4.932362-02	0.	0.	1.566144	3.184435-01	2.000000	2.125052-01
289	2.024880	4.318815-02	4.938532-02	0.	0.	1.566144	3.187655-01	2.000000	2.120605-01
290	2.022350	4.340252-02	4.944708-02	0.	0.	1.566144	3.190926-01	2.000000	2.116158-01
291	2.019824	4.361115-02	4.950893-02	0.	0.	1.566144	3.194239-01	2.000000	2.111711-01
292	2.017300	4.381437-02	4.957079-02	0.	0.	1.566144	3.197587-01	2.000000	2.107264-01
293	2.014780	4.401228-02	4.963266-02	0.	0.	1.566144	3.200963-01	2.000000	2.102817-01
294	2.012263	4.420523-02	4.969453-02	0.	0.	1.566144	3.204359-01	2.000000	2.098370-01
295	2.009750	4.439350-02	4.975709-02	0.	0.	1.566144	3.207771-01	2.000000	2.093923-01
296	2.007239	4.457728-02	4.981933-02	0.	0.	1.566144	3.211193-01	2.000000	2.089476-01
297	2.004732	4.475675-02	4.988164-02	0.	0.	1.566144	3.214621-01	2.000000	2.085029-01
298	2.002227	4.493216-02	4.994403-02	0.	0.	1.566144	3.218050-01	2.000000	2.080582-01
299	1.999726	4.510368-02	5.000650-02	0.	0.	1.566144	3.221477-01	2.000000	2.076135-01
300	1.997228	4.527135-02	5.006904-02	0.	0.	1.566144	3.224898-01	2.000000	2.071688-01
301	1.994733	4.543548-02	5.013167-02	0.	0.	1.566144	3.228312-01	2.000000	2.067241-01
302	1.992241	4.559623-02	5.019437-02	0.	0.	1.566144	3.231714-01	2.000000	2.062794-01
303	1.989752	4.575378-02	5.025715-02	0.	0.	1.566144	3.235104-01	2.000000	2.058347-01
304	1.987267	4.590824-02	5.032001-02	0.	0.	1.566144	3.238478-01	2.000000	2.053900-01
305	1.984784	4.605973-02	5.038295-02	0.	0.	1.566144	3.241835-01	2.000000	2.049453-01
306	1.982305	4.620841-02	5.044595-02	0.	0.	1.566144	3.245174-01	2.000000	2.045006-01
307	1.979828	4.635438-02	5.050909-02	0.	0.	1.566144	3.248492-01	2.000000	2.040559-01
308	1.977355	4.649777-02	5.057224-02	0.	0.	1.566144	3.251790-01	2.000000	2.036112-01
309	1.974885	4.663862-02	5.063549-02	0.	0.	1.566144	3.255065-01	2.000000	2.031665-01
310	1.972418	4.677707-02	5.069882-02	0.	0.	1.566144	3.258316-01	2.000000	2.027218-01
311	1.969954	4.691329-02	5.076223-02	0.	0.	1.566144	3.261543-01	2.000000	2.022771-01
312	1.967493	4.704735-02	5.082573-02	0.	0.	1.566144	3.264745-01	2.000000	2.018324-01

GAROL PROBLEM 1, THORIUM R=2.2 T=300

POINT	ENERGY-EV	FLUX		FLUX		SOURCE		TOTAL CROSS SECTION		COLLISION		DENSITY
		REGION 1	REGION 2	REGION 1	REGION 2	REGION 1	REGION 2	REGION 1	REGION 2	REGION 1	REGION 2	
313	1.965035	01	4.717932-02	5.088930-02	0.	1.566144	04	3.267923-01	2.000000	01	3.029659-01	1.999985
314	1.962580	01	4.730930-02	5.095295-02	0.	1.566144	04	3.271074-01	2.000000	01	3.037136-01	1.999985
315	1.960129	01	4.743731-02	5.101668-02	0.	1.566144	04	3.274198-01	2.000000	01	3.044455-01	1.999985
316	1.957680	01	4.756356-02	5.108049-02	0.	1.566144	04	3.277295-01	2.000000	01	3.051629-01	1.999985
317	1.955235	01	4.768798-02	5.114437-02	0.	1.566144	04	3.280366-01	2.000000	01	3.058652-01	1.999985
318	1.952792	01	4.781073-02	5.120834-02	0.	1.566144	04	3.283409-01	2.000000	01	3.065535-01	1.999985
319	1.950353	01	4.793188-02	5.127239-02	0.	1.566144	04	3.286424-01	2.000000	01	3.072282-01	1.999985
320	1.947916	01	4.805147-02	5.133652-02	0.	1.566144	04	3.289411-01	2.000000	01	3.078897-01	1.999985
321	1.945483	01	4.816957-02	5.140073-02	0.	1.566144	04	3.292371-01	2.000000	01	3.085382-01	1.999985
322	1.943052	01	4.828624-02	5.146502-02	0.	1.566144	04	3.295303-01	2.000000	01	3.091742-01	1.999985
323	1.940625	01	4.840156-02	5.152939-02	0.	1.566144	04	3.298207-01	2.000000	01	3.097982-01	1.999985
324	1.938201	01	4.851555-02	5.159384-02	0.	1.566144	04	3.301083-01	2.000000	01	3.104103-01	1.999985
325	1.935780	01	4.862829-02	5.165838-02	0.	1.566144	04	3.303931-01	2.000000	01	3.110111-01	1.999985
326	1.933361	01	4.873981-02	5.172299-02	0.	1.566144	04	3.306751-01	2.000000	01	3.116007-01	1.999985
327	1.930946	01	4.885009-02	5.178768-02	0.	1.566144	04	3.309544-01	2.000000	01	3.121791-01	1.999985
328	1.928534	01	4.895933-02	5.185246-02	0.	1.566144	04	3.312309-01	2.000000	01	3.127474-01	1.999985
329	1.926125	01	4.906741-02	5.191731-02	0.	1.566144	04	3.315047-01	2.000000	01	3.133050-01	1.999985
330	1.923719	01	4.917453-02	5.198225-02	0.	1.566144	04	3.317758-01	2.000000	01	3.138532-01	1.999985
331	1.921315	01	4.928066-02	5.204727-02	0.	1.566144	04	3.320442-01	2.000000	01	3.143917-01	1.999985
332	1.918915	01	4.938583-02	5.211237-02	0.	1.566144	04	3.323099-01	2.000000	01	3.149208-01	1.999985
333	1.916518	01	4.948999-02	5.217755-02	0.	1.566144	04	3.325729-01	2.000000	01	3.154403-01	1.999985
334	1.914124	01	4.959528-02	5.224281-02	0.	1.566144	04	3.328333-01	2.000000	01	3.159509-01	1.999985
335	1.911733	01	4.969568-02	5.230815-02	0.	1.566144	04	3.330910-01	2.000000	01	3.164527-01	1.999985
336	1.909345	01	4.979727-02	5.237358-02	0.	1.566144	04	3.333462-01	2.000000	01	3.169460-01	1.999985
337	1.906959	01	4.989806-02	5.243908-02	0.	1.566144	04	3.335988-01	2.000000	01	3.174312-01	1.999985
338	1.904577	01	4.999807-02	5.250467-02	0.	1.566144	04	3.338488-01	2.000000	01	3.179081-01	1.999985
339	1.902198	01	5.009736-02	5.257034-02	0.	1.566144	04	3.340963-01	2.000000	01	3.183774-01	1.999985
340	1.899822	01	5.019594-02	5.263610-02	0.	1.566144	04	3.343413-01	2.000000	01	3.188390-01	1.999985
341	1.897448	01	5.029383-02	5.270193-02	0.	1.566144	04	3.345839-01	2.000000	01	3.192932-01	1.999985
342	1.895078	01	5.039105-02	5.276785-02	0.	1.566144	04	3.348239-01	2.000000	01	3.197400-01	1.999985
343	1.892711	01	5.048756-02	5.283385-02	0.	1.566144	04	3.350616-01	2.000000	01	3.201794-01	1.999985
344	1.890346	01	5.058345-02	5.289993-02	0.	1.566144	04	3.352969-01	2.000000	01	3.206117-01	1.999985
345	1.887985	01	5.067875-02	5.296610-02	0.	1.566144	04	3.355298-01	2.000000	01	3.210373-01	1.999985
346	1.885626	01	5.077354-02	5.303234-02	0.	1.566144	04	3.357604-01	2.000000	01	3.214567-01	1.999985
347	1.883271	01	5.086777-02	5.309848-02	0.	1.566144	04	3.359886-01	2.000000	01	3.218697-01	1.999985
348	1.880918	01	5.096148-02	5.316509-02	0.	1.566144	04	3.362146-01	2.000000	01	3.222764-01	1.999985
349	1.878568	01	5.105461-02	5.323159-02	0.	1.566144	04	3.364383-01	2.000000	01	3.226766-01	1.999985
350	1.876222	01	5.114727-02	5.329817-02	0.	1.566144	04	3.366598-01	2.000000	01	3.230709-01	1.999985
351	1.873878	01	5.123943-02	5.336483-02	0.	1.566144	04	3.368790-01	2.000000	01	3.234593-01	1.999985
352	1.871537	01	5.133110-02	5.343158-02	0.	1.566144	04	3.370961-01	2.000000	01	3.238417-01	1.999985
353	1.869199	01	5.142240-02	5.349840-02	0.	1.566144	04	3.373111-01	2.000000	01	3.242190-01	1.999985
354	1.866864	01	5.151322-02	5.356532-02	0.	1.566144	04	3.375239-01	2.000000	01	3.245905-01	1.999985
355	1.864532	01	5.160370-02	5.363232-02	0.	1.566144	04	3.377346-01	2.000000	01	3.249572-01	1.999985
356	1.862203	01	5.169374-02	5.369940-02	0.	1.566144	04	3.379432-01	2.000000	01	3.253184-01	1.999985
357	1.859876	01	5.178339-02	5.376656-02	0.	1.566144	04	3.381498-01	2.000000	01	3.256744-01	1.999985
358	1.857553	01	5.187268-02	5.383381-02	0.	1.566144	04	3.383543-01	2.000000	01	3.260255-01	1.999985
359	1.855232	01	5.196162-02	5.390115-02	0.	1.566144	04	3.385569-01	2.000000	01	3.263718-01	1.999985
360	1.852915	01	5.205015-02	5.396856-02	0.	1.566144	04	3.387575-01	2.000000	01	3.267129-01	1.999985
361	1.850600	01	5.213839-02	5.403607-02	0.	1.566144	04	3.389561-01	2.000000	01	3.270496-01	1.999985
362	1.848288	01	5.222631-02	5.410365-02	0.	1.566144	04	3.391528-01	2.000000	01	3.273818-01	1.999985
363	1.845979	01	5.231391-02	5.417132-02	0.	1.566144	04	3.393476-01	2.000000	01	3.277094-01	1.999985
364	1.843673	01	5.240123-02	5.423908-02	0.	1.566144	04	3.395405-01	2.000000	01	3.280327-01	1.999993

GAROL PROBLEM 1,		THORIUM R=2.2		T=300
GROUP FLUXES				
GROUP	ENERGY-EV LOWER LIMIT	REGION 1	REGION 2	CELL AVERAGE
1	2.260329 01	1.883591-01	2.499997-01	2.499970-01
2	1.762547 01	1.864222-01	2.493729-01	2.493701-01
ONE GROUP FLUX		3.747813-01	4.993726-01	4.993671-01

GAROL PROBLEM 1, THORIUM R=2.2 T=300

BROAD GROUP AVERAGED CROSS SECTIONS

MATERIAL 1 1.0 HYDROGEN

GROUP	ENERGY-EV LOWER LIMIT	R E G I O N 1		R E G I O N 2		CELL	
		CAPTURE	SCATTER	CAPTURE	SCATTER	CAPTURE	AVERAGE SCATTER
1	2.260329 01	0.	2.000000 01	0.	2.000000 01	0.	2.000021 01
2	1.762547 01	0.	2.000000 01	0.	2.000000 01	0.	2.000022 01
ONE GROUP AVERAGE		0.	2.000000 01	0.	2.000000 01	0.	2.000022 01

GAROL PROBLEM 1, THORIUM R=2.2 I=300

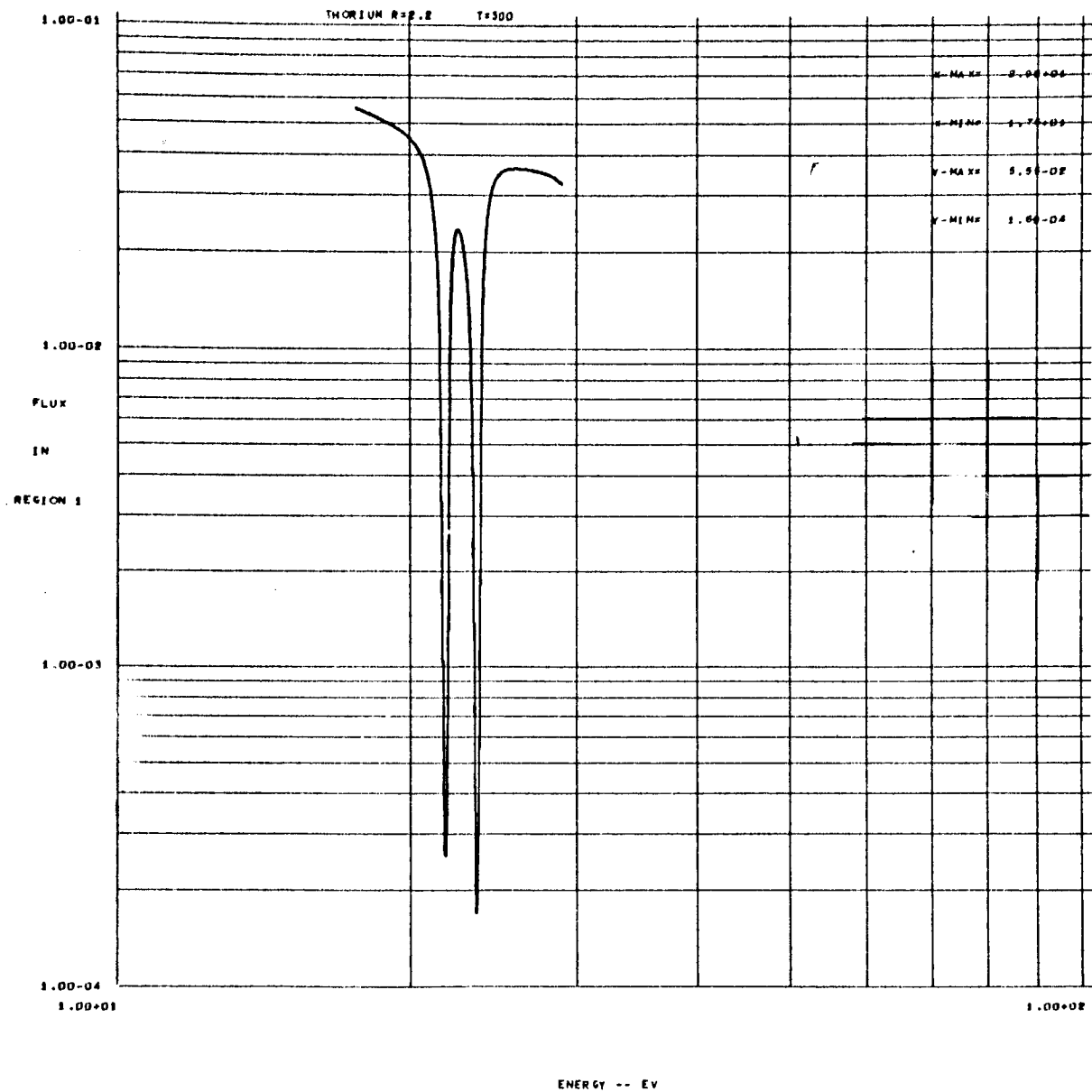
BROAD GROUP AVERAGED CROSS SECTIONS

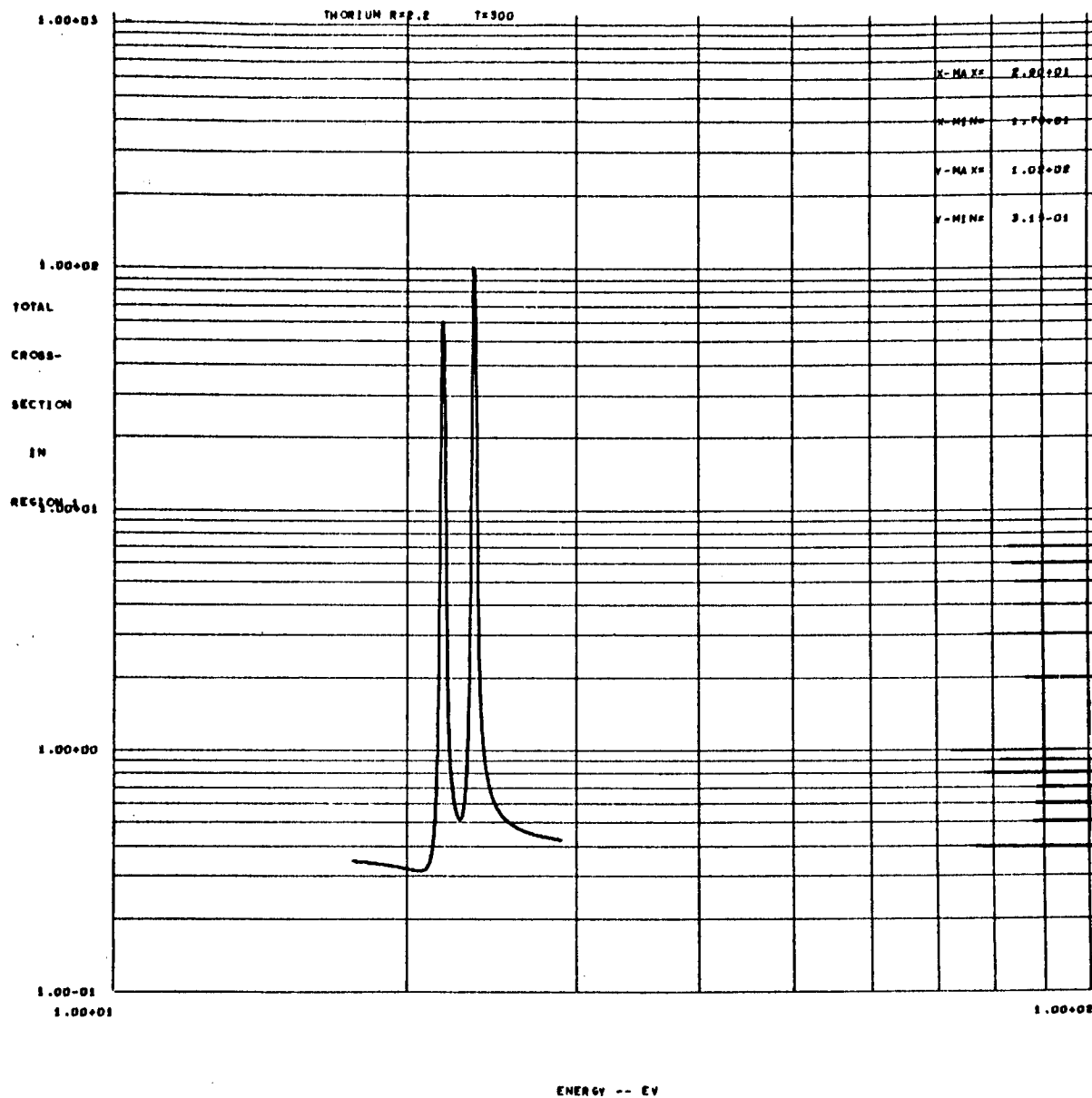
MATERIAL 2 90.232 TH232 300K, GAM=24.5, TWO RES

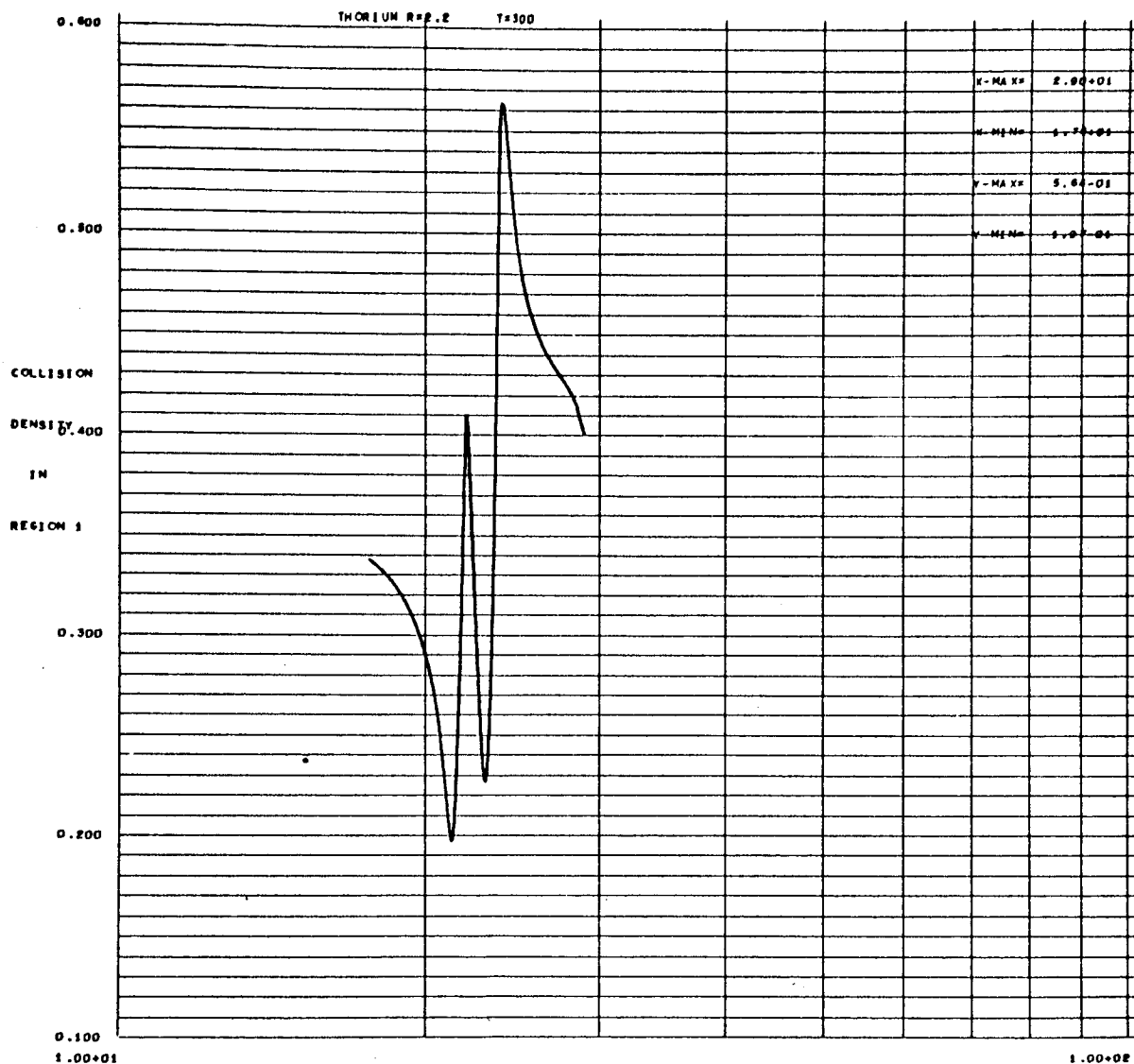
GROUP	ENERGY-EV LOWER LIMIT	R E G I O N 1		R E G I O N 2		C E L L		AVERAGE
		CAPTURE	SCATTER	CAPTURE	SCATTER	CAPTURE	SCATTER	
1	2.260329 01	3.265843 00	1.563582 01	1.025817 02	3.157013 01	2.460635 00	1.178074 01	
2	1.762547 01	2.858973 00	1.035968 01	6.745096 01	1.574598 01	2.137289 00	7.744608 00	
ONE GROUP AVERAGE		3.063460 00	1.301138 01	8.503838 01	2.366799 01	2.299165 00	9.765205 00	

GAROL PROBLEM	1.	THORIUM R=2.2	T=300				
		GENERAL ATOMIC, TPLOT,091565, S01 SMITH			-GAROL		
FRAME NO.	1	SERIES IDENTIFICATION					
		BEGIN PLOT SETUP	15.5926 MH				
		BEGIN PLOTTING	15.7269 MH				
		END PLOTTING	16.0694 MH				
FRAME NO.	2	THORIUM R=2.2	T=300	FLUX	IN	REGION 1	
		BEGIN PLOT SETUP	16.0741 MH				
		BEGIN PLOTTING	16.2083 MH				
		END PLOTTING	16.5417 MH				
FRAME NO.	3	THORIUM R=2.2	T=300	TOTAL CROSS-SECTION	IN	REGION 1	
		BEGIN PLOT SETUP	16.5463 MH				
		BEGIN PLOTTING	16.6204 MH				
		END PLOTTING	16.9769 MH				
FRAME NO.	4	THORIUM R=2.2	T=300	COLLISION DENSITY	IN	REGION 1	
		NO PLOTTING FOR THIS FRAME. Y IS CONSTANT FOR ALL X AT 0.					
		THORIUM R=2.2	T=300	CAPTURE	RATE		
		BEGIN PLOT SETUP	18.0231 MH				
		BEGIN PLOTTING	18.0972 MH				
		END PLOTTING	18.4398 MH				
FRAME NO.	5	THORIUM R=2.2	T=300	CAPTURE	RATE		

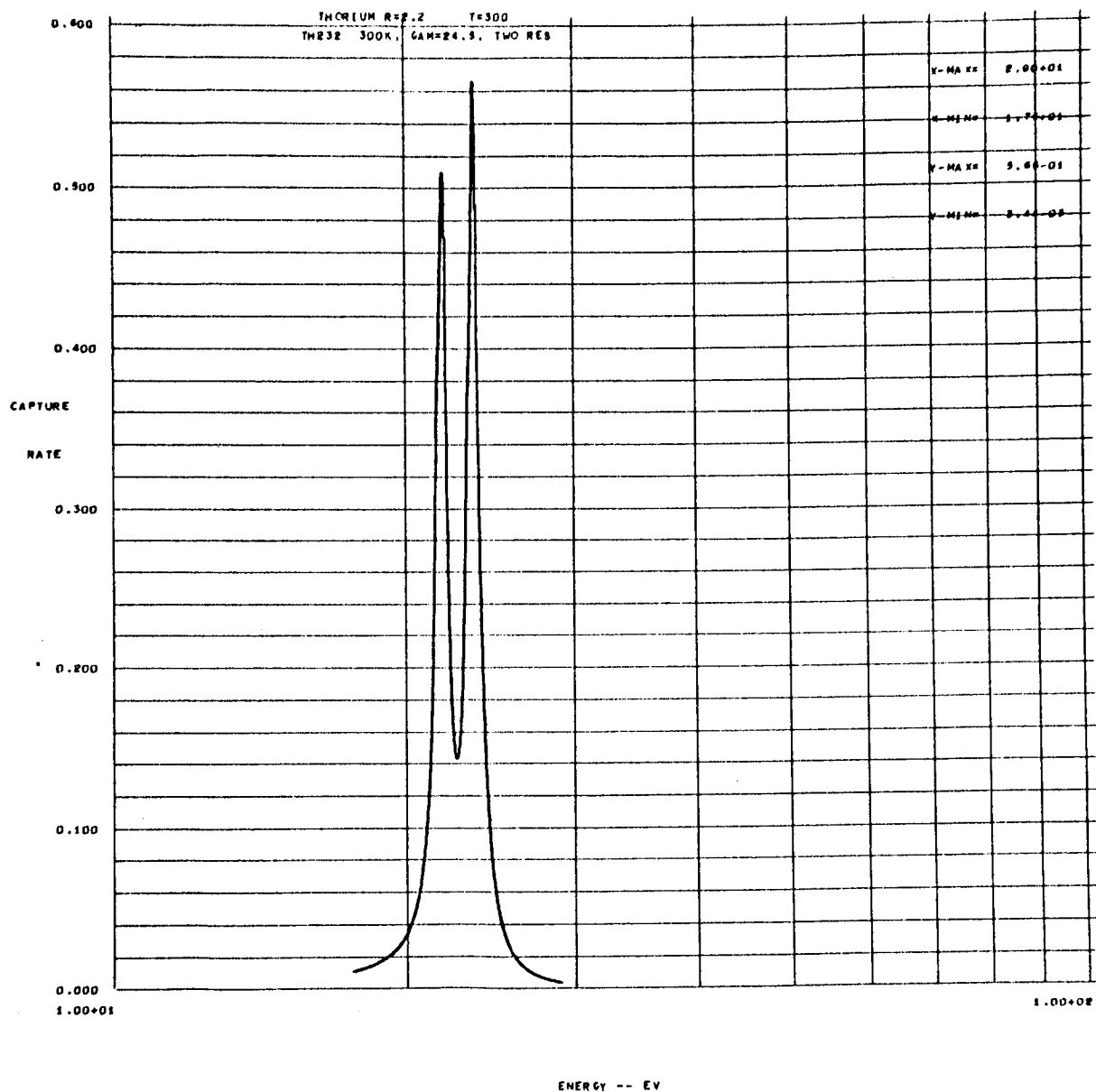
END-OF-DATA







ENERGY -- EV



LISTING OF THE GAROL PROGRAM

```

$IBFTC GAROL LIST,DECK,REF                                08-09-65MAIN0000
C MAIN LINK FOR GAROL MAIN0010
C 7-15-65 C V SMITH MAIN0020
C MAIN0030
COMMON /ALL/ NIN,NOUT,NDATA,NIN1,NIN3,JHYD,NEL,NARRAY,NPAGE,LINES MAIN0040
1,NPROB,NPTS,INDEX,NPLOT,TITLE(12),TID(10,20),CNAME(5,20),LINEPP MAIN0050
2 ,MAT,MFRAME MAIN0060
COMMON /TABLES/ CS1,CS2,CS3,SLABT(505),CYLT(305) MAIN0070
COMMON /PLOTT/ TLABEL(12),XLABEL(12),YLABEL(12),TT2(12),NFRAME MAIN0080
CALL CHAIN(1) MAIN0090
END MAIN0100

```

```

$IBMAP DUMFIL LIST,DECK,REF                                08-09-65DUMF0000
EXTERN UTVAR. DUMF0010
ENTRY FIL04. DUMF0020
ENTRY FIL07. DUMF0030
ENTRY FIL10. DUMF0040
ENTRY FIL11. DUMF0050
ENTRY FIL13. DUMF0060
ENTRY FIL14. DUMF0070
ENTRY FIL15. DUMF0080
ENTRY FIL16. DUMF0090
FIL04. EQU * DUMF0100
FIL07. EQU * DUMF0110
FIL10. EQU * DUMF0120
FIL11. EQU * DUMF0130
FIL13. EQU * DUMF0140
FIL14. EQU * DUMF0150
FIL15. EQU * DUMF0160
FIL16. EQU * DUMF0170
BSS 1 DUMF0180
END DUMF0190

```

```

$IBFTC ERRORS LIST,DECK,REF                                08-09-65ERRS0000
SUBROUTINE ERRORS(N1,N2) ERRS0010
WRITE (6,601) N1,N2 ERRS0020
PRINT 601, N1,N2 ERRS0030
601 FORMAT (22H0ERROR IN GAROL, LINK I2,14H, ERROR NUMBER I4,1H. ) ERRS0040
CALL EXIT ERRS0050
END ERRS0060

```

```

$IBFTC BOOLER LIST,REF BOOL0000
SUBROUTINE BOOLER(A1,A2) BOOL0010
A2=A1 BOOL0020
RETURN BOOL0030
END BOOL0040

```

SIBFTC TABSET LIST,REF

08-09-65 TABS0000

SETS UP SLAB AND CYLINDER TABLES
DATA FROM CASE, K., F. DE HOFFMANN, AND G. PLACZEK (1953)

BLOCK DATA

COMMON /TABLES/ CS1,CS2,CS3,SLABT(505),CYLT(305)

DIMENSION B1(89), B2(88), B3(88), B4(88), B5(88), B6(61)

DIMENSION C1(79), C2(78), C3(78), C4(67)

EQUIVALENCE (B1(1),SLABT(1)), (B2(1),SLABT(90)),

1 (B3(1),SLABT(178)), (B4(1),SLABT(266)), (B5(1),SLABT(354)),

2 (B6(1),SLABT(442))

EQUIVALENCE (C1(1),CYLT(1)), (C2(1),CYLT(80)), (C3(1),CYLT(158)),

1 (C4(1),CYLT(236))

DATA B1/0.0,0.04840,0.0831,0.1127,0.1390,0.1629,0.1849,0.2054,

1 0.2246,0.2427,0.2597,0.2759,0.2913,0.3060,0.3200,0.3335,0.3464,

2 0.3588,0.3707,0.3821,0.3932,0.4039,0.4142,0.4242,0.4339,0.4432,

3 0.4523,0.4611,0.4696,0.4779,0.4859,0.4937,0.5013,0.5087,0.5159,

4 0.5229,0.5298,0.5364,0.5429,0.5492,0.5554,0.5614,0.5673,0.5730,

5 0.5786,0.5841,0.5895,0.5947,0.5998,0.6048,0.6097,0.6145,0.6192,

6 0.6237,0.6282,0.6326,0.6369,0.6411,0.6453,0.6493,0.6533,0.6572,

7 0.6610,0.6647,0.6684,0.6720,0.6755,0.6790,0.6824,0.6857,0.6890,

8 0.6922,0.6954,0.6985,0.7015,0.7045,0.7074,0.7103,0.7132,0.7159,

9 0.7187,0.7214,0.7240,0.7266,0.7292,0.7317,0.7342,0.7366,0.7390/

DATA B2/0.7414,0.7437,0.7460,0.7483,0.7505,0.7527,0.7548,

1 0.7569,0.7590,0.7611,0.7631,0.7651,0.7670,0.7690,0.7709,0.7727,

2 0.7746,0.7764,0.7782,0.7800,0.7817,0.7834,0.7851,0.7868,0.7884,

3 0.7901,0.7917,0.7932,0.7948,0.7963,0.7978,0.7993,0.8008,0.8023,

4 0.8037,0.8051,0.8065,0.8079,0.8093,0.8106,0.8119,0.8132,0.8145,

5 0.8158,0.8171,0.8183,0.8196,0.8202,0.8220,0.8232,0.8243,0.8255,

6 0.8266,0.8278,0.8289,0.8300,0.8311,0.8321,0.8332,0.8342,0.8353,

7 0.8363,0.8373,0.8383,0.8393,0.8403,0.8413,0.8422,0.8432,0.8441,

8 0.8450,0.8460,0.8469,0.8478,0.8486,0.8495,0.8504,0.8512,0.8521,

9 0.8529,0.8538,0.8546,0.8554,0.8562,0.8570,0.8578,0.8586,0.8593/

DATA B3/0.8601,0.8608,0.8616,0.8623,0.8631,0.8638,0.8645,

1 0.8652,0.8659,0.8666,0.8673,0.8680,0.8687,0.8693,0.8700,0.8707,

2 0.8713,0.8720,0.8726,0.8732,0.8738,0.8745,0.8751,0.8757,0.8763,

3 0.8769,0.8775,0.8781,0.8786,0.8792,0.8798,0.8804,0.8809,0.8815,

4 0.8820,0.8826,0.8831,0.8836,0.8842,0.8847,0.8852,0.8857,0.8863,

5 0.8868,0.8873,0.8878,0.8883,0.8887,0.8892,0.8897,0.8902,0.8907,

6 0.8911,0.8916,0.8921,0.8925,0.8930,0.8934,0.8939,0.8943,0.8948,

7 0.8952,0.8956,0.8961,0.8965,0.8969,0.8973,0.8977,0.8982,0.8986,

8 0.8990,0.8994,0.8998,0.9002,0.9006,0.9010,0.9013,0.9017,0.9021,

9 0.9025,0.9029,0.9032,0.9036,0.9040,0.9043,0.9047,0.9051,0.9054/

DATA B4/0.9058,0.9061,0.9065,0.9068,0.9072,0.9075,0.9078,

1 0.9082,0.9085,0.9089,0.9092,0.9095,0.9098,0.9102,0.9105,0.9108,

2 0.9111,0.9114,0.9117,0.9120,0.9124,0.9127,0.9130,0.9133,0.9136,

3 0.9139,0.9141,0.9144,0.9147,0.9150,0.9153,0.9156,0.9159,0.9162,

4 0.9164,0.9167,0.9170,0.9173,0.9175,0.9178,0.9181,0.9183,0.9186,

5 0.9189,0.9191,0.9194,0.9196,0.9199,0.9202,0.9204,0.9207,0.9209,

6 0.9212,0.9214,0.9217,0.9219,0.9221,0.9224,0.9226,0.9229,0.9231,

TABS0010
TABS0020
TABS0030
TABS0040
TABS0050
TABS0060
TABS0070
TABS0080
TABS0090
TABS0100
TABS0110
TABS0120
TABS0130
TABS0140
TABS0150
TABS0160
TABS0170
TABS0180
TABS0190
TABS0200
TABS0210
TABS0220
TABS0230
TABS0240
TABS0250
TABS0260
TABS0270
TABS0280
TABS0290
TABS0300
TABS0310
TABS0320
TABS0330
TABS0340
TABS0350
TABS0360
TABS0370
TABS0380
TABS0390
TABS0400
TABS0410
TABS0420
TABS0430
TABS0440
TABS0450
TABS0460
TABS0470
TABS0480
TABS0490
TABS0500

7	0.9233,0.9236,0.9238,0.9240,0.9243,0.9245,0.9247,0.9249,0.9252,	TABS0510
8	0.9254,0.9256,0.9258,0.9261,0.9263,0.9265,0.9267,0.9269,0.9271,	TABS0520
9	0.9273,0.9276,0.9278,0.9280,0.9282,0.9284,0.9286,0.9288,0.9290/	TABS0530
	DATA B5/0.9292,0.9294,0.9296,0.9298,0.9300,0.9302,0.9304,	TABS0540
1	0.9306,0.9308,0.9309,0.9311,0.9313,0.9315,0.9317,0.9319,0.9321,	TABS0550
2	0.9323,0.9324,0.9326,0.9328,0.9330,0.9332,0.9333,0.9335,0.9337,	TABS0560
3	0.9339,0.9340,0.9342,0.9344,0.9346,0.9347,0.9349,0.9351,0.9352,	TABS0570
4	0.9354,0.9356,0.9357,0.9359,0.9361,0.9362,0.9364,0.9366,0.9367,	TABS0580
5	0.9369,0.9370,0.9372,0.9373,0.9375,0.9377,0.9378,0.9380,0.9381,	TABS0590
6	0.9383,0.9384,0.9386,0.9387,0.9389,0.9390,0.9392,0.9393,0.9395,	TABS0600
7	0.9396,0.9398,0.9399,0.9401,0.9402,0.9403,0.9405,0.9406,0.9408,	TABS0610
8	0.9409,0.9410,0.9412,0.9413,0.9415,0.9416,0.9417,0.9419,0.9420,	TABS0620
9	0.9421,0.9423,0.9424,0.9425,0.9427,0.9428,0.9429,0.9431,0.9432/	TABS0630
	DATA B6/0.9433,0.9434,0.9436,0.9437,0.9438,0.9439,0.9441,	TABS0640
1	0.9442, 0.9443,0.9444,0.9446,0.9447,0.9448,0.9449,0.9451,0.9452,	TABS0650
2	0.9453,0.9454,0.9455,0.9457,0.9458,0.9459,0.9460,0.9461,0.9462,	TABS0660
3	0.9464,0.9465,0.9466,0.9467,0.9468,0.9469,0.9470,0.9471,0.9473,	TABS0670
4	0.9474,0.9475,0.9476,0.9477,0.9478,0.9479,0.9480,0.9481,0.9482,	TABS0680
5	0.9483,0.9485,0.9486,0.9487,0.9488,0.9489,0.9490,0.9491,0.9492,	TABS0690
6	0.9493,0.9494,0.9495,0.9496,0.9497,0.9498,0.9499,0.9500,0.9501/	TABS0700
	DATA C1/0.0,0.2561,0.04967,0.07248,0.09421,0.11498,0.13487,	TABS0710
10.	15396,0.17231,0.18996,0.20697,0.22336,0.23918,0.25446,0.26923,	TABS0720
20.	28351,0.29733,0.31070,0.32366,0.33621,0.34838,0.36019,0.37164,	TABS0730
30.	38276,0.39356,0.40405,0.41424,0.42414,0.43377,0.44314,0.45225,	TABS0740
40.	46112,0.46975,0.47816,0.48634,0.49432,0.50209,0.50966,0.51704,	TABS0750
50.	52424,0.53126,0.53811,0.54479,0.55131,0.55767,0.56389,0.56996,	TABS0760
60.	57588,0.58167,0.58733,0.59285,0.59826,0.60354,0.60870,0.61375,	TABS0770
70.	61869,0.62352,0.62825,0.63287,0.63740,0.64183,0.64616,0.65041,	TABS0780
80.	65457,0.65864,0.66263,0.66654,0.67038,0.67413,0.67781,0.68142,	TABS0790
90.	68495,0.68842,0.69182,0.69516,0.69843,0.70164,0.70479,0.70788/	TABS0800
	DATA C2/0.71091,0.71389,0.71681,0.71968,0.72250,0.72526,	TABS0810
10.	72798,0.73065,0.73327,0.73585,0.73833,0.74087,0.74331,0.74572,	TABS0820
20.	74808,0.75040,0.75269,0.75493,0.75714,0.75931,0.76145,0.76355,	TABS0830
30.	76562,0.76765,0.76966,0.77163,0.77357,0.77548,0.77736,0.77921,	TABS0840
40.	78103,0.78282,0.78459,0.78633,0.78805,0.78974,0.79140,0.79304,	TABS0850
50.	79465,0.79624,0.79781,0.79936,0.80088,0.80239,0.80387,0.80532,	TABS0860
60.	80677,0.80818,0.80958,0.81096,0.81233,0.81367,0.81500,0.81630,	TABS0870
70.	81759,0.81886,0.82012,0.82136,0.82258,0.82379,0.82498,0.82616,	TABS0880
80.	82732,0.82847,0.82960,0.83071,0.83182,0.83291,0.83399,0.83505,	TABS0890
90.	83610,0.83714,0.83816,0.83917,0.84017,0.84116,0.84214,0.84310/	TABS0900
	DATA C3/0.84405,0.84500,0.84593,0.84685,0.84776,0.84866,	TABS0910
10.	84955,0.85043,0.85130,0.85216,0.85301,0.85385,0.85468,0.85550,	TABS0920
20.	85632,0.85712,0.85792,0.85870,0.85948,0.86025,0.86101,0.86177,	TABS0930
30.	86251,0.86325,0.86398,0.86471,0.86542,0.86613,0.86683,0.86752,	TABS0940
40.	86821,0.86889,0.86956,0.87023,0.87089,0.87154,0.87219,0.87283,	TABS0950
50.	87346,0.87409,0.87471,0.87533,0.87594,0.87654,0.87714,0.87773,	TABS0960
60.	87832,0.87890,0.87947,0.88004,0.88061,0.88117,0.88173,0.88228,	TABS0970
70.	88282,0.88336,0.88389,0.88443,0.88495,0.88547,0.88598,0.88650,	TABS0980
80.	88701,0.88751,0.88801,0.88850,0.88899,0.88948,0.88996,0.89044,	TABS0990
90.	89091,0.89138,0.89184,0.89230,0.89276,0.89321,0.89366,0.89411/	TABS1000

DATA	C4/0.89455,0.89499,0.89542,0.89585,0.89628,0.89671,	TABS1010
10.89713,0.89755,0.89796,0.89837,0.89878,0.89919,0.89959,0.89999,		TABS1020
20.90038,0.90077,0.90116,0.90155,0.90193,0.90231,0.90268,0.90306,		TABS1030
30.90343,0.90381,0.90417,0.90453,0.90489,0.90525,0.90560,0.90595,		TABS1040
40.90631,0.90665,0.90700,0.90734,0.90768,0.90802,0.90835,0.90868,		TABS1050
50.90902,0.90934,0.90967,0.90999,0.91031,0.91063,0.91095,0.91126,		TABS1060
60.91157,0.91188,0.91219,0.91250,0.91280,0.91310,0.91340,0.91369,		TABS1070
70.91399,0.91429,0.91457,0.91487,0.91515,0.91544,0.91572,0.91600,		TABS1080
80.91628,0.91656,0.91684,0.91711,0.91738/		TABS1090
END		TABS1100

\$IBMAP	TIDCO	LIST,DECK,REF	08-09-65	TIDC0000
*				TIDC0010
*		CALLING SEQUENCE -		TIDC0020
*				TIDC0030
*		CALL TIDCO(TID(1))		TIDC0040
*				TIDC0050
	ENTRY	TIDCO		TIDC0060
*				TIDC0070
	EXTERN	ERROR		TIDC0080
	EXTERN	EXIT		TIDC0090
*				TIDC0100
*				TIDC0110
*		CONSTANTS NEEDED		TIDC0120
	ZERO	OCT 0		TIDC0130
	NERR	OCT 3		TIDC0140
	TEN	OCT 12		TIDC0150
*				TIDC0160
*		TEST SYMBOLS		TIDC0170
	B6	OCT 60		TIDC0180
	BB	OCT 606060606060		TIDC0190
	B0	OCT 006060606060		TIDC0200
*				TIDC0210
*		INDEX REGISTER AND INTERIM STORAGE		TIDC0220
	XX4	BSS 1		TIDC0230
	T1	BSS 1		TIDC0240
	T2	BSS 1		TIDC0250
	T3	BSS 1		TIDC0260
	T4	BSS 1		TIDC0270
	F1	BSS 1		TIDC0280
	F2	BSS 1		TIDC0290
	Y1	TRA **		TIDC0300
	Y2	TRA **		TIDC0310
	Y3	TRA **		TIDC0320
*				TIDC0330
	PT1	PZE **		TIDC0340
*		ENTRY FOR ID CONVERSION		TIDC0350
	TIDCO	SAVE 1,2,4		TIDC0360
		STZ T1		TIDC0370
		STZ T2		TIDC0380
		STZ T3		TIDC0390
		STZ T4		TIDC0400
		CAL BB		TIDC0410
		SLW F1		TIDC0420
		CAL 3,4		TIDC0430
		STA PC1		TIDC0440
		STA A1		TIDC0450
		ADD =1		TIDC0460
		STA A2		TIDC0470
		ADD =1		TIDC0480
		STA B1		TIDC0490
		LXA NUMB-1,1		TIDC0500

	SXA	Y2,1	TIDC0510
	SXA	Y3,1	TIDC0520
	TXI	*+1,1,5	TIDC0530
	SXA	Y1,1	TIDC0540
	LXA	ZERO,2	TIDC0550
LP2	LXA	ZERO,1	TIDC0560
LP1	PXA	,1	TIDC0570
	SAC	PC1,,2	TIDC0580
	PXA	,0	TIDC0590
PC1	PCS	**,2,0	TIDC0600
	PAX	,4	TIDC0610
	TXL	NUMB,4,9	TIDC0620
	TXH	MISP,4,48	TIDC0630
	TXH	Y3,4,47	TIDC0640
	TXH	MISP,4,27	TIDC0650
	TXH	Y1,4,26	TIDC0660
	TXH	MISP,4,16	TIDC0670
	TXH	Y2,4,15	TIDC0680
	TRA	MISP	TIDC0690
CONT	TXI	*+1,1,1	TIDC0700
	TXL	LP1,1,5	TIDC0710
	TXI	*+1,2,-1	TIDC0720
	TXH	LP2,2,-2	TIDC0730
	TRA	FINAL	TIDC0740
DEC	STO	T1	TIDC0750
	STO	T2	TIDC0760
	TSX	SET,4	TIDC0770
	STZ	T3	TIDC0780
	CAL	PC1+3	TIDC0790
	STA	Y1	TIDC0800
	CAL	DEC-1	TIDC0810
	STA	Y3	TIDC0820
	CAL	F1	TIDC0830
	SLW	F2	TIDC0840
	CAL	BB	TIDC0850
	SLW	F1	TIDC0860
	TRA	CONT	TIDC0870
NUMB	STO	T1	TIDC0880
	TSX	MPLY,4	TIDC0890
	TSX	SET,4	TIDC0900
	CLA	T2	TIDC0910
	TNZ	CONT	TIDC0920
	CAL	PC1+2	TIDC0930
	STA	Y2	TIDC0940
	STA	Y3	TIDC0950
	TRA	CONT	TIDC0960
MPLY	LDQ	T4	TIDC0970
	MPY	TEN	TIDC0980
	STQ	T4	TIDC0990
	CLA	T4	TIDC1000

	ADD	T1	TIDC1010
	STO	T4	TIDC1020
	TRA	1,4	TIDC1030
SET	CLA	T3	TIDC1040
	ADD	=1	TIDC1050
	STO	T3	TIDC1060
	CAL	F1	TIDC1070
	ALS	6	TIDC1080
	ADD	T1	TIDC1090
	SLW	F1	TIDC1100
	TOV	*+1	TIDC1110
	TRA	1,4	TIDC1120
FINAL	LXA	T3,1	TIDC1130
	TXH	FIX,1,5	TIDC1140
	STZ	T1	TIDC1150
	CLA	=6	TIDC1160
	SUB	T3	TIDC1170
	PAX	,1	TIDC1180
	SXA	PT1,1	TIDC1190
	TSX	MPLY,4	TIDC1200
	TIx	*-1,1,1	TIDC1210
	CAL	B6	TIDC1220
	SLW	T1	TIDC1230
	LXA	PT1,1	TIDC1240
	TXH	REPL,1,5	TIDC1250
	TSX	SET,4	TIDC1260
	TIx	*-1,1,1	TIDC1270
	TRA	FIX	TIDC1280
REPL	CAL	B0	TIDC1290
	SLW	F1	TIDC1300
	TRA	OUT	TIDC1310
FIX	CLA	=5	TIDC1320
	PAX	,1	TIDC1330
LP4	PXA	,1	TIDC1340
	SAC	PT2,,2	TIDC1350
	SAC	PT3,,2	TIDC1360
	SAC	PT4,,2	TIDC1370
	CAL	B6	TIDC1380
PT2	CCS	F1,,5	TIDC1390
	TRA	*+2	TIDC1400
	TRA	CC2	TIDC1410
	PXA	,0	TIDC1420
PT3	PCS	F1,,5	TIDC1430
	TNZ	OUT	TIDC1440
	CAL	B6	TIDC1450
PT4	SAC	F1,,5	TIDC1460
CC2	TIx	LP4,1,1	TIDC1470
OUT	CAL	F1	TIDC1480
A2	SLW	**	TIDC1490
	CAL	F2	TIDC1500

```

A1    SLW    **
      CLA    T4
B1    STO    **
      RETURN TIDCO
MISP  CALL   ERROR(NERR)
      CALL   EXIT
      END

```

```

TIDC1510
TIDC1520
TIDC1530
TIDC1540
TIDC1550
TIDC1560
TIDC1570

```

```
$IBFTC ERROR LIST,DECK,REF
```

```
08-09-65ERR 0000
```

```
  SUBROUTINE ERROR(N)
```

```
ERR 0010
```

```
C      ERROR SUBROUTINE FOR TIDCO
```

```
ERR 0020
```

```
  WRITE (6,1)
```

```
ERR 0030
```

```
1  FORMAT (1H0///34H0ERROR STOP---MISPUNCHED ID NUMBER )
```

```
ERR 0040
```

```
  CALL EXIT
```

```
ERR 0050
```

```
  END
```

```
ERR 0060
```

* * * * *
 G A R D L L I N K 1
 * * * * *

\$IBMAP	COMSET	LIST,REF	08-09-65	1COM0000
B	BOOL	37333		1COM0010
BSET	CONTRL	A,C		1COM0020
A	BSS	B		1COM0030
C	EQU	*		1COM0040
	END			1COM0050

\$IBFTC	LINK1	LIST,DECK,REF	08-09-65	1LNK0000
C				1LNK0010
C		LINK 1		1LNK0020
C		SET UP CONSTANTS AND INITIALIZE DATA TAPE		1LNK0030
C				1LNK0040
	COMMON /ALL/	NIN,NOUT,NDATA,NIN1,NIN3,JHYD,NEL,NARRAY,NPAGE,LINES		1LNK0050
	1,NPROB,NPTS,INDEX,NPLOT,TITLE(12),TID(10,20),CNAME(5,20),LINEPP			1LNK0060
	2 ,MAT,MFRAME			1LNK0070
	COMMON /TABLES/	CS1,CS2,CS3,SLABT(505),CYLT(305)		1LNK0080
	COMMON /BSET/	LIMST,LIM1,LIM2,NPRINT,JPRINT(10),DUM(200),DE1,DE2		1LNK0090
	1 ,DE3,EEZERO,E(8000),SCAP(20),SF(20),SSC(20),SA(20),ALPHA(20)			1LNK0100
	2 ,KTAPE(3),KPTS(10)			1LNK0110
	3	,NORES(20),LLIM(20),SPO(20),EZERO(600),RHGT(600)		1LNK0120
	4 ,FACT1(600),FACT2(600),FACT3(600),FRAT(600),XI(600)			1LNK0130
	5	,GI(500),GJ(500),GF(500),EO(500),GG(500),GN(500)		1LNK0140
	6 ,SPIN(500)			1LNK0150
	COMMON /PLOTT/	TLABEL(12),XLABEL(12),YLABEL(12),TT2(12),NFRAME		1LNK0160
	EQUIVALENCE	(TID,NTID),(DUM,LIM),(NPT,NPTS),(NDATA,NDATA1)		1LNK0170
	DIMENSION	NTID(10,20), LIM(200)		1LNK0180
	DIMENSION	KT(3)		1LNK0190
	DIMENSION	FMT(12)		1LNK0200
C				1LNK0210
C		SET CONSTANTS		1LNK0220
	NIN=5			1LNK0230
	NOUT=6			1LNK0240
	LIMST=8000			1LNK0250
	NPROB=0			1LNK0260
	CS1=0.5			1LNK0270
	CS2=0.0			1LNK0280
	CS3=-0.09375			1LNK0290
	MFRAME=0			1LNK0300
	NPAGE=0			1LNK0310
	LINEPP=52			1LNK0320
	NKT=0			1LNK0330
	KT(1)=NIN			1LNK0340
	KT(2)=3			1LNK0350
	KT(3)=2			1LNK0360
	NDATA1=9			1LNK0370
	READ (NIN,902) INDEX			1LNK0380

REWIND NDATA1	1LNK0390
READ (5,901){TLABEL(I),I=1,12}	1LNK0400
901 FORMAT (12A6)	1LNK0410
IF (INDEX.LE.0) GO TO 710	1LNK0420
C START PREPARING A NEW DATA TAPE	1LNK0430
READ (NIN,902) NINDEX,NPTS	1LNK0440
CALL ENERGY(NINDEX)	1LNK0450
CALL BOOLER(6H(2A6, ,FMT(1))	1LNK0460
CALL BOOLER(6H2X5A6,,FMT(2))	1LNK0470
CALL BOOLER(6HOPF10.,FMT(3))	1LNK0480
CALL BOOLER(6H3,F12.,FMT(4))	1LNK0490
CALL BOOLER(6H5,2X1P,FMT(5))	1LNK0500
CALL BOOLER(6HI10) ,FMT(12))	1LNK0510
CALL BOOLER(6HE13.5,,EFMT)	1LNK0520
CALL BOOLER(6H1X ,XFMT1)	1LNK0530
CALL BOOLER(6H2X ,XFMT2)	1LNK0540
CALL BOOLER(6H2A6, ,AFMT)	1LNK0550
CALL BOOLER(6H CO,C1)	1LNK0560
CALL BOOLER(6HMPUTED,C2)	1LNK0570
CALL BOOLER(6H INPUT,C3)	1LNK0580
CALL BOOLER(6H CARDS,C4)	1LNK0590
CALL HEAD	1LNK0600
READ (NIN,902) MAT,JHYD	1LNK0610
902 FORMAT (6I12)	1LNK0620
IF (MAT.LT.1.OR.MAT.GT.20) CALL ERRORS(1,2)	1LNK0630
NEL=MAT	1LNK0640
NSUM=0	1LNK0650
NPRINT=0	1LNK0660
DO 10 K=1,NEL	1LNK0670
KPTS(K)=0	1LNK0680
READ (5,903) TID(1,K),TID(2,K),(CNAME(I,K),I=1,5),(TID(J,K),J=4,8)	1LNK0690
1 ,TID(10,K)	1LNK0700
CALL TIDCO(TID(1,K))	1LNK0710
903 FORMAT (2A6,5A6/6E12.6)	1LNK0720
IF (TID(6,K).GT.-2.0) GO TO 5	1LNK0730
TID(7,K)=-2.0	1LNK0740
TID(8,K)=-2.0	1LNK0750
NKT=NKT+1	1LNK0760
READ (NIN,902) KPTS(NKT)	1LNK0770
NT=3	1LNK0780
GO TO 6	1LNK0790
5 NT=0	1LNK0800
IF (TID(6,K).LT.0.0) NT=NT+1	1LNK0810
IF (TID(7,K).LT.0.0) NT=NT+1	1LNK0820
IF (TID(8,K).LT.0.0) NT=NT+1	1LNK0830
6 NTID(9,K)=NT	1LNK0840
NSUM=NSUM+NT	1LNK0850
IF (TID(10,K).LE.0.0) GO TO 10	1LNK0860
IF (NT.LE.0) GO TO 10	1LNK0870
NPRINT=NPRINT+1	1LNK0880

JPRINT(NPRINT)=K	1LNK0890
10 CONTINUE	1LNK0900
IF (NKT.LE.0) GO TO 12	1LNK0910
IF (NKT.GT.3) CALL ERRORS(1,3)	1LNK0920
DO 8 K=2,NEL	1LNK0930
IF (TID(4,K).EQ.1.0) CALL ERRORS(1,7)	1LNK0940
8 CONTINUE	1LNK0950
N=1	1LNK0960
DO 11 K=1,NEL	1LNK0970
IF (TID(6,K).GT.-2.0) GO TO 11	1LNK0980
KTAPE(N)=KT(NKT)	1LNK0990
MTAPE=KTAPE(N)	1LNK1000
IF (NKT.GT.1) REWIND MTAPE	1LNK1010
N=N+1	1LNK1020
NKT=NKT-1	1LNK1030
11 CONTINUE	1LNK1040
12 CONTINUE	1LNK1050
NARRAY=NSUM	1LNK1060
WRITE (6,904)	1LNK1070
904 FORMAT (26H0NUCLIDE TABLE OF CONTENTS/13H0NUCLIDE I.D. 7X,4HNAME	1LNK1080
1 26X 1HA 5X 10HASYPOTIC 7X 7HCAPTURE 7X 7HFISSION 7X 7HSCATTER	1LNK1090
2 5X 9HNUMBER OF/56X 10HSCATTERING 48X 6HARRAYS/)	1LNK1100
DO 30 K=1,NEL	1LNK1110
N=0	1LNK1120
L=6	1LNK1130
DO 35 JK=6,8	1LNK1140
IF (TID(JK,K).LT.0.0) GO TO 31	1LNK1150
N=N+1	1LNK1160
DUM(N)=TID(JK,K)	1LNK1170
FMT(L)=EFMT	1LNK1180
FMT(L+1)=XFMT1	1LNK1190
GO TO 34	1LNK1200
31 FMT(L)=AFMT	1LNK1210
FMT(L+1)=XFMT2	1LNK1220
IF (TID(JK,K).LT.-1.0) GO TO 32	1LNK1230
DUM(N+1)=C1	1LNK1240
DUM(N+2)=C2	1LNK1250
GO TO 33	1LNK1260
32 DUM(N+1)=C3	1LNK1270
DUM(N+2)=C4	1LNK1280
DUM(N+3)=C3	1LNK1290
DUM(N+4)=C4	1LNK1300
DUM(N+5)=C3	1LNK1310
N=N+6	1LNK1320
DUM(N)=C4	1LNK1330
FMT(L+2)=AFMT	1LNK1340
FMT(L+3)=XFMT2	1LNK1350
FMT(L+4)=AFMT	1LNK1360
FMT(L+5)=XFMT2	1LNK1370
GO TO 36	1LNK1380

33	N=N+2	1LNK1390
34	L=L+2	1LNK1400
35	CONTINUE	1LNK1410
36	NO=N	1LNK1420
	WRITE (6,FMT) TID(1,K),TID(2,K),(CNAME(I,K),I=1,5),TID(4,K),	1LNK1430
	1 TID(5,K),(DUM(N),N=1,NO),NTID(9,K)	1LNK1440
30	CONTINUE	1LNK1450
C		1LNK1460
C		1LNK1470
40	IF (INDEX.GT.1) GO TO 50	1LNK1480
	WRITE (NDATA)(TLABEL(I),I=1,12)	1LNK1490
	WRITE (NDATA1) NPT,NEL,NARRAY,JHYD	1LNK1500
	WRITE (NDATA1)((TID(I,K),I=1,10),(CNAME(J,K),J=1,5),K=1,NEL)	1LNK1510
	WRITE (NDATA)(SLABT(I),I=1,505),(CYLT(J),J=1,305)	1LNK1520
	GO TO 100	1LNK1530
50	READ (NDATA) (DUM(I),I=1,12)	1LNK1540
	DO 60 I=1,12	1LNK1550
	IF (TLABEL(I).NE.DUM(I)) CALL ERRORS(1,8)	1LNK1560
60	CONTINUE	1LNK1570
	DO 70 I=1,3	1LNK1580
70	READ (NDATA) DUM1	1LNK1590
	READ (NIN,902) JPT	1LNK1600
	JHYD=JPT	1LNK1610
	DO 80 J=1,JPT	1LNK1620
80	READ (NDATA) DUM1	1LNK1630
	READ (10,500)(DUM2,J=1,JPT)	1LNK1640
500	FORMAT (E12.6)	1LNK1650
	IF (ABS(DUM1-DUM2).GT.1.0E-5*DUM1) CALL ERRORS(1,9)	1LNK1660
100	CALL CHAIN(2)	1LNK1670
C	READ FROM A DATA TAPE PREVIOUSLY PREPARED	1LNK1680
710	NERR=1	1LNK1690
C	CHECK LABEL ON A DATA TAPE WRITTEN ON AN EARLIER RUN	1LNK1700
	READ (NDATA)(DUM(I),I=1,12)	1LNK1710
	DO 720 I=1,12	1LNK1720
	IF (DUM(I).NE.TLABEL(I)) CALL ERRORS(1,1)	1LNK1730
720	CONTINUE	1LNK1740
	NERR=2	1LNK1750
C	STORE -TABLE OF CONTENTS- AND OTHER DATA FROM	1LNK1760
C	BEGINNING OF DATA TAPE	1LNK1770
	READ (NDATA1) NPT,NEL,NARRAY,JHYD	1LNK1780
	READ (NDATA1) ((TID(J,K),J=1,10),(CNAME(I,K),I=1,5),K=1,NEL)	1LNK1790
	DO 730 K=1,NEL	1LNK1800
	IF (TID(6,K).GT.0.0) TID(6,K)=TID(6,K)*0.159	1LNK1810
	IF (TID(6,K).GT.-2.0) GO TO 730	1LNK1820
	TID(7,K)=-2.0	1LNK1830
	TID(8,K)=-2.0	1LNK1840
730	CONTINUE	1LNK1850
	READ (NDATA1) DUMMY	1LNK1860
	CALL CHAIN(4)	1LNK1870
	END	1LNK1880

		08-09-65	ENER0000
	\$IBFTC ENERGY LIST,DECK,REF		ENER0010
	SUBROUTINE ENERGY(NINDEX)		ENER0020
C			ENER0030
C	SET UP ENERGY MESH		ENER0040
C			ENER0050
	COMMON /ALL/ NIN,NOUT,NDATA,NIN1,NIN3,JHYD,NEL,NARRAY,NPAGE,LINES		ENER0060
	1,NPROB,NPTS,INDEX,NPLOT,TITLE(12),TID(10,20),CNAME(5,20),LINEPP		ENER0070
	2,MAT,MFRAME		ENER0080
	COMMON /TABLES/ CS1,CS2,CS3,SLABT(505),CYLT(305)		ENER0090
	COMMON /BSET/ LIMST,LIM1,LIM2,NPRINT,JPRINT(10),DUM(200),DE1,DE2		ENER0100
	1,DE3,EEZERO,E(8000),SCAP(20),SF(20),SSC(20),SA(20),ALPHA(20)		ENER0110
	2,KTAPE(3),KPTS(10)		ENER0120
	3,NORES(20),LLIM(20),SPO(20),EZERO(600),RHGT(600)		ENER0130
	4,FACT1(600),FACT2(600),FACT3(600),FRAT(600),XI(600)		ENER0140
	5,GI(500),GJ(500),GF(500),EO(500),GG(500),GN(500)		ENER0150
	6,SPIN(500)		ENER0160
	COMMON /PLOTT/ TLABEL(12),XLABEL(12),YLABEL(12),TT2(12),NFRAME		ENER0170
	EQUIVALENCE (TID,NTID),(DUM,LIM),(NPT,NPTS),(NDATA,NDATA1)		ENER0180
	DIMENSION NTID(10,20), LIM(200)		ENER0190
C			ENER0200
	IF (NINDEX.LT.1) CALL ERRORS(1,4)		ENER0210
	IF (NINDEX.GT.5) CALL ERRORS(1,5)		ENER0220
	LIMST=7998		ENER0230
	M2=LIMST		ENER0240
	NT=1		ENER0250
	LIM1=M2		ENER0260
C	INTERMEDIATE STORAGE OF ENERGIES ON INTERMEDIARY TAPE 8		ENER0270
	NIN1=8		ENER0280
	REWIND NIN1		ENER0290
100	GO TO (1,2,3,4,5,5),NINDEX		ENER0300
C	READ ENERGIES FROM INPUT CARDS		ENER0310
	1 M2=MIN0(NPTS,LIMST)		ENER0320
	LIM2=NPTS		ENER0330
	READ (NIN,901)(E(I),I=1,M2)		ENER0340
901	FORMAT (6E12.6)		ENER0350
	IF (M2.GE.NPTS) GO TO 10		ENER0360
	WRITE (NIN1)(E(I),I=1,M2)		ENER0370
101	NT=NT+1		ENER0380
	M2=MIN0(NPTS-(NT-1)*LIMST,LIMST)		ENER0390
	READ (NIN,901)(E(I),I=1,M2)		ENER0400
	DO 102 I=1,M2		ENER0410
	WRITE (NIN1) E(I)		ENER0420
102	CONTINUE		ENER0430
	IF (M2.LT.NPTS-NT*LIMST) GO TO 101		ENER0440
	GO TO 8		ENER0450
C	EQUAL ENERGY SPACING		ENER0460
C	READ E-MAX AND DELTA-E		ENER0470
	2 READ (NIN,901) EMAX,EMIN,DELTA-E		ENER0480
	E(1)=EMAX		ENER0490
	DO 201 I=2,M2		ENER0500
	E(I)=E(I-1)-DELTA-E		

```

      IF (E(I).GT.EMIN) GO TO 201
      NPTS=I
      IF (E(I).LT.EMIN) E(I)=EMIN
      GO TO 10
201  CONTINUE
      WRITE (NIN1)(E(I),I=1,M2)
      ENEXT=E(M2)
      M3=20000
      DO 202 I=1,M3
      ENEXT=ENEXT-DELTA E
      IF (ENEXT.GT.EMIN) GO TO 202
      NPTS=M2+I
      IF (ENEXT.LT.EMIN) ENEXT=EMIN
      WRITE (NIN1) ENEXT
      GO TO 7
202  WRITE (NIN1) ENEXT
      CALL ERRORS(1,7)
C      EQUAL VELOCITY SPACING
C      READ EMAX AND CONSTANT
3  READ (NIN,901) EMAX,EMIN,CONST
      E(1)=EMAX
      DO 301 I=2,M2
      E(I)=E(I-1)-CONST*SQRT(E(N-1))
      IF (E(I).GT.EMIN) GO TO 301
      NPTS=I
      IF (E(I).LT.EMIN) E(I)=EMIN
      GO TO 10
301  CONTINUE
      WRITE (NIN1)(E(I),I=1,M2)
      M3=20000
      ENEXT=E(M2)
      DO 302 I=1,M3
      ENEXT=ENEXT-CONST*SQRT(ENEXT)
      IF (ENEXT.GT.EMIN) GO TO 302
      NPTS=M2+I
      IF (ENEXT.LT.EMIN) ENEXT=EMIN
      WRITE (NIN1) ENEXT
      GO TO 7
302  WRITE (NIN1) ENEXT
      CALL ERRORS(1,7)
C      EQUAL LETHARGY SPACING
C      READ EZERO AND DELTA-U
4  READ (NIN,901) EMAX,EMIN,DELTAU
      E(1)=EMAX
      EDU=EXP(-DELTAU)
      DO 401 I=2,M2
      E(I)=E(I-1)*EDU
      IF (E(I).GT.EMIN) GO TO 401
      NPTS=I
      IF (E(I).LT.EMIN) E(I)=EMIN

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ENER0510
ENER0520
ENER0530
ENER0540
ENER0550
ENER0560
ENER0570
ENER0580
ENER0590
ENER0600
ENER0610
ENER0620
ENER0630
ENER0640
ENER0650
ENER0660
ENER0670
ENER0680
ENER0690
ENER0700
ENER0710
ENER0720
ENER0730
ENER0740
ENER0750
ENER0760
ENER0770
ENER0780
ENER0790
ENER0800
ENER0810
ENER0820
ENER0830
ENER0840
ENER0850
ENER0860
ENER0870
ENER0880
ENER0890
ENER0900
ENER0910
ENER0920
ENER0930
ENER0940
ENER0950
ENER0960
ENER0970
ENER0980
ENER0990
ENER1000

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GO TO 10	ENER1010
401 CONTINUE	ENER1020
WRITE (NIN1)(E(I),I=1,M2)	ENER1030
M3=20000	ENER1040
ENEXT=E(M2)	ENER1050
DO 402 I=1,M3	ENER1060
ENEXT=ENEXT*EDU	ENER1070
IF (ENEXT.GT.EMIN) GO TO 402	ENER1080
NPTS=M2+I	ENER1090
IF (ENEXT.LT.EMIN) ENEXT=EMIN	ENER1100
WRITE (NIN1) ENEXT	ENER1110
GO TO 7	ENER1120
402 WRITE (NIN1) ENEXT	ENER1130
CALL ERRORS(1,7)	ENER1140
C USE YOUR OWN SUBROUTINE ENRG TO GENERATE ENERGY POINTS	ENER1150
C WHERE NPTS IS LESS THAN 8001 AND ENERGIES ARE CORE CONTAINED	ENER1160
5 CALL ENRG(NPTS,E)	ENER1170
LIM1=NPTS	ENER1180
LIM2=NPTS	ENER1190
IF (NPTS.GT.8000) CALL ERRORS(1,6)	ENER1200
GO TO 10	ENER1210
7 REWIND NIN1	ENER1220
READ (NIN1) DUMMY	ENER1230
GO TO 10	ENER1240
8 REWIND NIN1	ENER1250
9 READ (NIN1)(E(I),I=1,LIM1)	ENER1260
10 RETURN	ENER1270
END	ENER1280
\$IBFTC ENRG LIST,DECK,REF	08-09-65ENRG0000
SUBROUTINE ENRG(NPTS,E)	ENRG0010
DIMENSION E(8000)	ENRG0020
WRITE (6,601)	ENRG0030
601 FORMAT (39HODUMMY SUBROUTINE ENRG HAS BEEN ENTERED/113HOIN ORDER T	ENRG0040
10 USE THE OPTION OF GENERATING YOUR OWN ENERGIES, PLEASE REPLACE T	ENRG0050
2HIS SUBROUTINE WITH ONE OF YOUR OWN.)	ENRG0060
CALL ERRORS(1,6)	ENRG0070
END	ENRG0080
\$IBFTC HEAD LIST,DECK,REF	08-09-65HEAD0000
SUBROUTINE HEAD	HEAD0010
COMMON /ALL/ NIN,NOUT,NDATA,NIN1,NIN3,JHYD,NEL,NARRAY,NPAGE,LINES	HEAD0020
1,NPROB,NPTS,INDEX,NPLOT,TITLE(12),TID(10,20),CNAME(5,20),LINEPP	HEAD0030
2 ,MAT,MFRAME	HEAD0040
COMMON /PLOTT/ TLABEL(12),XLABEL(12),YLABEL(12),T2(12)	HEAD0050
NPAGE=NPAGE+1	HEAD0060
WRITE (6,601)(TLABEL(I),I=1,12),NPAGE	HEAD0070
601 FORMAT(26H1GAROL DATA TAPE, LABELED 12A6, 22X 4HPAGE 16)	HEAD0080
RETURN	HEAD0090
END	HEAD0100

* * * * *
 G A R O L L I N K 2
 * * * * *

\$IBMAP	COMSET	LIST,REF	08-09-652COM0000
B	BOOL	37333	2COM0010
BSET	CONTRL	A,C	2COM0020
A	BSS	B	2COM0030
C	EQU	*	2COM0040
	END		2COM0050

\$IBFTC	LINK2	LIST,DECK,REF	08-09-652LNK0000
C		LINK 2	2LNK0010
C		READ RESONANCE PARAMETERS	2LNK0020
C		COMPUTE RESONANCE VARIABLES AND INDICES	2LNK0030
C		FOR CALCULATING CROSS SECTIONS	2LNK0040
C			2LNK0050
	COMMON /ALL/	NIN,NOUT,NDATA,NIN1,NIN3,JHYD,NEL,NARRAY,NPAGE,LINES	2LNK0060
	1,NPROB,NPTS,INDEX,NPLOT,TITLE(12),TID(10,20),CNAME(5,20),LINEPP		2LNK0070
	2 ,MAT,MFRAME		2LNK0080
	COMMON /TABLES/	CS1,CS2,CS3,SLABT(505),CYLT(305)	2LNK0090
	COMMON /BSET/	LIMST,LIM1,LIM2,NPRINT,JPRINT(10),DUM(200),DE1,DE2	2LNK0100
	1 ,DE3,EEZERO,E(8000),SCAP(20),SF(20),SSC(20),SA(20),ALPHA(20)		2LNK0110
	2 ,KTAPE(3),KPTS(10)		2LNK0120
	3 ,NORES(20),LLIM(20),SPO(20),EZERO(600),RHGT(600)		2LNK0130
	4 ,FACT1(600),FACT2(600),FACT3(600),FRAT(600),XI(600)		2LNK0140
	5 ,GI(500),GJ(500),GF(500),EO(500),GG(500),GN(500)		2LNK0150
	6 ,SPIN(500)		2LNK0160
	COMMON /PLOTT/	TLABEL(12),XLABEL(12),YLABEL(12),TT2(12),NFRAME	2LNK0170
	EQUIVALENCE (TID,NTID),(DUM,LIM),(NPT,NPTS),(NDATA,NDATA1)		2LNK0180
	DIMENSION NTID(10,20), LIM(200)		2LNK0190
			2LNK0200
	LIM3=LIM1		2LNK0210
	LIM1=0		2LNK0220
	NKT=0		2LNK0230
	DO 10 K=1,MAT		2LNK0240
	IF (TID(6,K).GE.0.0.AND.TID(7,K).GE.0.0.AND.TID(8,K).GE.0.0)		2LNK0250
	1 GO TO 10		2LNK0260
	IF (TID(6,K).EQ.-1.0) GO TO 5		2LNK0270
	IF (TID(8,K).EQ.-1.0) GO TO 5		2LNK0280
	IF (TID(7,K).EQ.-1.0) GO TO 5		2LNK0290
	NKT=NKT+1		2LNK0300
	GO TO 10		2LNK0310
	5 CALL DSET(K)		2LNK0320
	LIM1=234		2LNK0330
	10 CONTINUE		2LNK0340
	LIM1=LIM3		2LNK0350
	IF (NKT.LE.1) GO TO 30		2LNK0360
	NKTM1=NKT-1		2LNK0370
	DO 25 J=1,NKTM1		2LNK0380
	JTAPE=KTAPE(J)		2LNK0390
	KTO=KPTS(J)		2LNK0400

DO 20 I=1,KTO	2LNK0410
READ (NIN,500)EE, CAP, SCAT, FIS	2LNK0420
WRITE (JTAPE,500)EE, CAP, SCAT, FIS	2LNK0430
500 FORMAT (4E12.6)	2LNK0440
20 CONTINUE	2LNK0450
REWIND JTAPE	2LNK0460
25 CONTINUE	2LNK0470
30 CALL CHAIN(3)	2LNK0480
END	2LNK0490

\$IBFTC DSET	LIST,DECK,REF	08-09-65DSET0000
SUBROUTINE DSET(NMAT)		DSET0010
C		DSET0020
C	READ AND SET UP RESONANCE PARAMETERS AND CONSTANTS	DSET0030
C	FOR DOPPLER BROADENING CALCULATION	DSET0040
C	ADAPTED FOR GAROL FROM THE FASDOP PROGRAM (GAMD-6562)	DSET0050
C		DSET0060
	COMMON /ALL/ NIN,NOUT,NDATA,NIN1,NIN3,JHYD,NEL,NARRAY,NPAGE,LINES	DSET0070
	1,NPROB,NPTS,INDEX,NPLOT,TITLE(12),TID(10,20),CNAME(5,20),LINEPP	DSET0080
	2 ,MAT,MFRAME	DSET0090
	COMMON /TABLES/ CS1,CS2,CS3,SLABT(505),CYLT(305)	DSET0100
V	COMMON /BSET/ LIMST,LIM1,LIM2,NPRINT,JPRINT(10),DUM(200),DE1,DE2	DSET0110
	1 ,DE3,EEZERO,E(8000),SCAP(20),SF(20),SSC(20),SA(20),ALPHA(20)	DSET0120
	2 ,KTAPE(3),KPTS(10)	DSET0130
	3 ,NORES(20),LLIM(20),SPO(20),EZERO(600),RHGT(600)	DSET0140
	4 ,FACT1(600),FACT2(600),FACT3(600),FRAT(600),XI(600)	DSET0150
	5 ,GI(500),GJ(500),GF(500),EO(500),GG(500),GN(500)	DSET0160
	6 ,SPIN(500)	DSET0170
	COMMON /PLOTT/ TLABEL(12),XLABEL(12),YLABEL(12),TT2(12),NFRAME	DSET0180
	EQUIVALENCE (TID,NTID),(DUM,LIM),(NPT,NPTS),(NDATA,NDATA1)	DSET0190
	DIMENSION NTID(10,20), LIM(200)	DSET0200
	INTEGER GAMN	DSET0210
	DIMENSION GAMN(1)	DSET0220
	IF (LIM1.EQ.234) GO TO 2	DSET0230
	KST=1	DSET0240
	GO TO 3	DSET0250
2	KST=KEND+1	DSET0260
3	CONTINUE	DSET0270
20	READ (5,510) WGT,STAT,SPOT,TEMP	DSET0280
	IF (WGT.NE.TID(4,NMAT)) CALL ERRORS(2,1)	DSET0290
	READ (5,520) NEZ,NFIS,NGN	DSET0300
	NRR=NEZ	DSET0310
	NORES(NMAT)=NRR	DSET0320
	LLIM(NMAT)=KST	DSET0330
	KEND=KST+NRR-1	DSET0340
	AMASS=WGT	DSET0350
	SPO(NMAT)=SPOT	DSET0360

CALL HEAD	DSET0370
WRITE (6,602) (CNAME(I,NMAT),I=1,5),AMASS,SPOT,TEMP	DSET0380
602 FORMAT (1H08X,37H DOPPLER BROADENING CALCULATIONS FOR 5A6/	DSET0390
118X,24H ABSORBER MASS = F8.3/	DSET0400
318X,24H POTENTIAL SCATTERING = F8.3,8H (BARN)/	DSET0410
418X,24H TEMPERATURE = F8.3,4H (K)/)	DSET0420
DO 30 K=1,NRR	DSET0430
GI(K)=0.0	DSET0440
GJ(K)=0.0	DSET0450
30 GF(K)=0.0	DSET0460
IF (NFIS.GT.0) GO TO 80	DSET0470
IF (STAT.GT.0.0) GO TO 70	DSET0480
READ (5,530) (EO(J),GI(J),GJ(J),GG(J),GN(J),J=1,NRR)	DSET0490
40 DO 60 K=1,NRR	DSET0500
IF (GJ(K).GE.0.0) GO TO 50	DSET0510
SPIN(K)=GI(K)	DSET0520
GO TO 60	DSET0530
50 SPIN(K)=(2.0*GJ(K)+1.0)/(2.0*GI(K)+1.0)*0.5	DSET0540
60 CONTINUE	DSET0550
GO TO 120	DSET0560
70 READ (5,540) (EO(J),GG(J),GN(J),J=1,NRR)	DSET0570
GO TO 100	DSET0580
80 IF (STAT.GT.0.0) GO TO 90	DSET0590
READ (5,510) (EO(J),GI(J),GG(J),GN(J),GF(J),J=1,NRR)	DSET0600
GO TO 40	DSET0610
90 READ (5,550) (EO(J),GG(J),GN(J),GF(J),J=1,NRR)	DSET0620
100 DO 110 K=1,NRR	DSET0630
110 SPIN(K)=STAT	DSET0640
120 IF (NGN.GT.0) GO TO 302	DSET0650
301 GAMN(1)= - 4903602544	DSET0660
GO TO 303	DSET0670
302 GAMN(1)= - 4903602496	DSET0680
303 CONTINUE	DSET0690
304 WRITE(6,305) GAMN(1)	DSET0700
305 FORMAT(39X,26H RESONANCE PARAMETER INPUT//17X,11H RESONANCE 5X,21HDSET0710	
1 STATISTICAL FACTORS 12X,17H HALF-WIDTHS - MV/11X,49H NUMBER	ENDSET0720
2ERGY-EV I J G GA A6,27H GAMMA GAMMA	GADSET0730
3MMA F//)	DSET0740
WRITE(6,306) (K,EO(K),GI(K),GJ(K),SPIN(K),GN(K),GG(K),GF(K)	DSET0750
1,K=1,NEZ)	DSET0760
306 FORMAT(I16,F13.3,F10.1,F6.1,F8.3,2F13.4,F14.4)	DSET0770
IF (NGN.LE.0) GO TO 142	DSET0780
DO 141 K=1,NRR	DSET0790
141 GN(K)=GN(K)*SQRT(EO(K))	DSET0800
142 DO 143 K=1,NRR	DSET0810
GG(K)=GG(K)*0.001	DSET0820
GN(K)=GN(K)*0.001	DSET0830
143 GF(K)=GF(K)*0.001	DSET0840
RAKT=SQRT(AMASS/(8.6167E-05*TEMP))	DSET0850
CON1=((AMASS+1.0)/AMASS)**2	DSET0860
CON2=2.6029E+06*CON1	DSET0870

CON3=1.6133505E+03*CON1	DSET0880
RSPO=SQRT(SPOT)	DSET0890
DO 200 J=1,NRR	DSET0900
JJ=KST+J-1	DSET0910
EZERO(JJ)=E0(J)	DSET0920
GPF=GG(J)+GF(J)	DSET0930
REO=1.0/E0(J)	DSET0940
GT=1.0/(GN(J)+GPF)	DSET0950
RREO=SQRT(REO)	DSET0960
GNGT=GN(J)*GT	DSET0970
FACT=GNGT*RREO*SPIN(J)	DSET0980
FACT1(JJ)=FACT*RSPO*CON3	DSET0990
FACT2(JJ)=FACT*GPF*GT*CON2	DSET1000
FACT3(JJ)=GNGT*GNGT*SPIN(J)*REO*CON2	DSET1010
FRAT(JJ)=GF(J)/GPF	DSET1020
HGT=0.5/GT	DSET1030
RHGT(JJ)=2.0*GT	DSET1040
XI(JJ)=HGT*RREO*RAKT	DSET1050
200 CONTINUE	DSET1060
RETURN	DSET1070
160 WRITE (6,560)	DSET1080
CALL EXIT	DSET1090
510 FORMAT(6E12.6)	DSET1100
520 FORMAT(6I12)	DSET1110
530 FORMAT(5E12.6)	DSET1120
540 FORMAT(3E12.6)	DSET1130
550 FORMAT(4E12.6)	DSET1140
560 FORMAT(1H1///10X,54H * * * * * ERROR STOP - INPUT LIST TOO LARGE	DSET1150
1 * * * * *)	DSET1160
END	DSET1170

\$IBFTC HEAD	LIST,DECK,REF	08-09-65	HEAD0000
SUBROUTINE HEAD			HEAD0010
COMMON /ALL/	NIN,NOUT,NDATA,NIN1,NIN3,JHYD,NEL,NARRAY,NPAGE,LINES		HEAD0020
1,NPROB,NPTS,INDEX,NPLOT,TITLE(12),TID(10,20),CNAME(5,20),LINEPP			HEAD0030
2,MAT,MFRAME			HEAD0040
COMMON /PLOTT/	TLABEL(12),XLABEL(12),YLABEL(12),T2(12)		HEAD0050
NPAGE=NPAGE+1			HEAD0060
WRITE (6,601)(TLABEL(I),I=1,12),NPAGE			HEAD0070
601 FORMAT(26H1GAROL DATA TAPE, LABELED 12A6, 22X 4HPAGE 16)			HEAD0080
RETURN			HEAD0090
END			HEAD0100

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G A R O L L I N K 3

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\$IBMAP	COMSET	LIST,REF	08-09-653COM0000
B	BOOL	37333	3COM0010
BSET	CONTRL	A,C	3COM0020
A	BSS	B	3COM0030
C	EQU	*	3COM0040
	END		3COM0050

\$IBFTC	LINK3	LIST,DECK,REF	08-09-653LNK0000
C		LINK 3	3LNK0010
C		CALCULATE CROSS SECTIONS	3LNK0020
C		AND WRITE DATA TAPE ON (B5)	3LNK0030
C			3LNK0040
		COMMON /ALL/ NIN,NOUT,NDATA,NIN1,NIN3,JHYD,NEL,NARRAY,NPAGE,LINES	3LNK0050
		1,NPROB,NPTS,INDEX,NPLOT,TITLE(12),TID(10,20),CNAME(5,20),LINEPP	3LNK0060
		2 ,MAT,MFRAME	3LNK0070
		COMMON /TABLES/ CS1,CS2,CS3,SLABT(505),CYLT(305)	3LNK0080
		COMMON /BSET/ LIMST,LIM1,LIM2,NPRINT,JPRINT(10),DUM(200),DE1,DE2	3LNK0090
		1 ,DE3,EEZERO,E(8000),SCAP(20),SF(20),SSC(20),SA(20),ALPHA(20)	3LNK0100
		2 ,KTAPE(3),KPTS(10)	3LNK0110
		3 ,NDRES(20),LLIM(20),SPO(20),EZERO(600),RHGT(600)	3LNK0120
		4 ,FACT1(600),FACT2(600),FACT3(600),FRAT(600),XI(600)	3LNK0130
		5 ,GI(500),GJ(500),GF(500),EO(500),GG(500),GN(500)	3LNK0140
		6 ,SPIN(500)	3LNK0150
		COMMON /PLOTT/ TLABEL(12),XLABEL(12),YLABEL(12),TT2(12),NFRAME	3LNK0160
		EQUIVALENCE (TID,NTID),(DUM,LIM),(NPT,NPTS),(NDATA,NDATA1)	3LNK0170
		DIMENSION NTID(10,20), LIM(200)	3LNK0180
		DO 20 JK=1,50	3LNK0190
		GI(JK)=0.0	3LNK0200
		GJ(JK)=0.0	3LNK0210
20		CONTINUE	3LNK0220
		IF (NPRINT.GT.0) GO TO 21	3LNK0230
		ASSIGN 4 TO NGO	3LNK0240
		GO TO 22	3LNK0250
21		ASSIGN 10 TO NGO	3LNK0260
		CALL HEAD	3LNK0270
22		CONTINUE	3LNK0280
		IF (JHYD.LE.1) GO TO 23	3LNK0290
		JST=JHYD	3LNK0300
		JHYD=1	3LNK0310
24		IF (JST.LE.LIMST) GO TO 25	3LNK0320
		JST=JST-LIMST	3LNK0330
		NT=NT+1	3LNK0340
		GO TO 24	3LNK0350
23		JST=1	3LNK0360

25	I=JST	3LNK0370
	JEND1=MIN0(NPTS,LIMST)	3LNK0380
	NT=1	3LNK0390
	NTLIM=0	3LNK0400
	NTLIMP=LIMST	3LNK0410
	DO 1 K=1,MAT	3LNK0420
	ALPHA(K)=((TID(4,K)-1.0)/(TID(4,K)+1.0))**2	3LNK0430
1	CONTINUE	3LNK0440
	IF (JEND1.LT.NPTS) GO TO 2	3LNK0450
	ASSIGN 6 TO NP1	3LNK0460
	ASSIGN 8 TO NP2	3LNK0470
	GO TO 3	3LNK0480
2	ASSIGN 5 TO NP1	3LNK0490
	ASSIGN 9 TO NP2	3LNK0500
	EEZERO=E(LIMST)	3LNK0510
3	CONTINUE	3LNK0520
	IF (JST.GT.1) GO TO 4	3LNK0530
	DE1=0.0	3LNK0540
	DE2=E(2)/(E(1)-E(2))*ALOG(E(1)/E(2))	3LNK0550
	DE3=(E(1)-E(2))*0.5	3LNK0560
	ND=1	3LNK0570
	CALL FASDOP(1)	3LNK0580
	DO 40 K=1,NEL	3LNK0590
	ETO=E(1)*ALPHA(K)	3LNK0600
	DO 30 J=1,NPT	3LNK0610
	IF (E(J).GT.ETO) GO TO 30	3LNK0620
	LIM(ND)=J-I-1	3LNK0630
	JJ=J-1	3LNK0640
	GO TO 31	3LNK0650
30	CONTINUE	3LNK0660
	LIM(ND)=NPT-I	3LNK0670
	JJ=NPT	3LNK0680
31	ND=ND+1	3LNK0690
	NCORT=0	3LNK0700
33	LIM(ND)=NCORT	3LNK0710
	ND=ND+NCORT+1	3LNK0720
	IF (TID(6,K).GE.0.0) GO TO 34	3LNK0730
	DUM(ND)=SCAP(K)	3LNK0740
	ND=ND+1	3LNK0750
34	IF (TID(7,K).GE.0.0) GO TO 35	3LNK0760
	DUM(ND)=SF(K)	3LNK0770
	ND=ND+1	3LNK0780
35	IF (TID(8,K).GE.0.0) GO TO 40	3LNK0790
	DUM(ND)=SSC(K)	3LNK0800
	ND=ND+1	3LNK0810
40	CONTINUE	3LNK0820
	ND=ND-1	3LNK0830
	WRITE (NDATA1) E(1),DE1,DE2,DE3,ND,(DUM(J),J=1,ND)	3LNK0840
	IF (NPRINT.GT.0) CALL PRINT(JST,E(JST))	3LNK0850
4	JST=JST+1	3LNK0860

I=JST	3LNK0870
GO TO NP2,(8,9)	3LNK0880
9 IF (JST.LE.LIMST) GO TO 8	3LNK0890
JST=1	3LNK0900
I=JST	3LNK0910
NT=NT+1	3LNK0920
NTLIM=(NT-1)*LIMST	3LNK0930
NTLIMP=NTLIM+LIMST	3LNK0940
8 CONTINUE	3LNK0950
IF (JST+NTLIM.GE.NPTS) GO TO 11	3LNK0960
DE1=E(I-1)/(E(I-1)-E(I))*ALOG(E(I-1)/E(I))	3LNK0970
DE2=E(I+1)/(E(I)-E(I+1))*ALOG(E(I)/E(I+1))	3LNK0980
DE3=(E(I)-E(I+1))*0.5	3LNK0990
CALL FASDOP(JST)	3LNK1000
CALL NUTZ(JST,NT)	3LNK1010
GO TO NP1,(5,6)	3LNK1020
5 IF (NTLIMP+JST-1.GE.NPTS) ASSIGN 6 TO NP1	3LNK1030
READ (NIN1) E(JST-1)	3LNK1040
IF (JST.EQ.1) E(LIMST)=EEZERO	3LNK1050
IF (JST.EQ.2) E(LIMST+1)=E(1)	3LNK1060
6 CONTINUE	3LNK1070
GO TO NGO,(4,10)	3LNK1080
10 CALL PRINT(JST,E(JST))	3LNK1090
GO TO 4	3LNK1100
11 CONTINUE	3LNK1110
DE1=E(I-1)/(E(I-1)-E(I))*ALOG(E(I-1)/E(I))	3LNK1120
DE2=0.0	3LNK1130
DE3=0.0	3LNK1140
CALL FASDOP(JST)	3LNK1150
CALL NUTZ(JST,NT)	3LNK1160
IF (NPRINT.GT.0) CALL PRINT(JST,E(JST))	3LNK1170
EE=0.0	3LNK1180
ND=1	3LNK1190
WRITE (NDATA) EE,DE1,DE1,DE3,ND,EE	3LNK1200
END FILE NDATA	3LNK1210
CALL TICKER(TIME)	3LNK1220
TIME=TIME/216.0	3LNK1230
PRINT 601, TIME	3LNK1240
601 FORMAT (1H0/15HOTAPE COMPLETE. 15X,6HTIME = F10.3,3H MH)	3LNK1250
REWIND NDATA	3LNK1260
DO 12 I=1,4	3LNK1270
12 READ (NDATA) DUMMY	3LNK1280
CALL CHAIN(4)	3LNK1290
END	3LNK1300

*\$IBFTC FASDOP LIST,DECK,REF
SUBROUTINE FASDOP(JK)

08-09-65FASD0000

C		FASD0010
C		FASD0020
C	FAST AND EPITHERMAL ENERGY RANGE DOPPLER BROADENING CALCULATION	FASD0030
C	ADAPTED FOR GAROL FROM THE FASDOP PROGRAM (GAMD-6562)	FASD0040
C	'FASDOP' COMPUTES THE TOTAL CONTRIBUTION FROM ALL RESOLVED	FASD0050
C	RESONANCES TO THE ABSORPTION, FISSION, AND SCATTERING	FASD0060
C	CROSS-SECTIONS AT SPECIFIED ENERGIES.	FASD0070
C	OR CALCULATES CROSS-SECTIONS BY INTERPOLATION FROM INPUT	FASD0080
C		FASD0090
	COMMON /ALL/ NIN,NOUT,NDATA,NIN1,NIN3,JHYD,NEL,NARRAY,NPAGE,LINES	FASD0100
	1,NPROB,NPTS,INDEX,NPLOT,TITLE(12),TID(10,20),CNAME(5,20),LINEPP	FASD0110
	2 ,MAT,MFRAME	FASD0120
	COMMON /TABLES/ CS1,CS2,CS3,SLABT(505),CYLT(305)	FASD0130
	COMMON /BSET/ LIMST,LIM1,LIM2,NPRINT,JPRINT(10),DUM(200),DE1,DE2	FASD0140
	1 ,DE3,EEZERO,E(8000),SCAP(20),SF(20),SSC(20),SA(20),ALPHA(20)	FASD0150
	2 ,KTAPE(3),KPTS(10)	FASD0160
	3 ,NORES(20),LLIM(20),SPO(20),EZERO(600),RHGT(600)	FASD0170
	4 ,FACT1(600),FACT2(600),FACT3(600),FRAT(600),XI(600)	FASD0180
	5 ,GI(500),GJ(500),GF(500),EO(500),GG(500),GN(500)	FASD0190
	6 ,SPIN(500)	FASD0200
	EQUIVALENCE (TID,NTID),(DUM,LIM),(NPT,NPTS),(NDATA,NDATA1)	FASD0210
	DIMENSION NTID(10,20), LIM(200)	FASD0220
	DIMENSION A(4)	FASD0230
	EQUIVALENCE (GI(1),ELAST(1)), (GI(11),SCAPL(1)), (GI(21),SSCL(1))	FASD0240
	1 , (GI(31),SFL(1)), (GI(41),JPTS(1))	FASD0250
	EQUIVALENCE (GJ(1),ENEXT(1)), (GJ(11),SCAPN(1)), (GJ(21),SSCN(1))	FASD0260
	1 , (GJ(31),SFN(1))	FASD0270
	DIMENSION ELAST(10), SCAPL(10), SSCL(10), SFL(10), JPTS(10)	FASD0280
	DIMENSION ENEXT(10), SCAPN(10), SSCN(10), SFN(10)	FASD0290
C		FASD0300
	RE=SQRT(1.0/E(JK))	FASD0310
	N=0	FASD0320
	DO 300 I=1,MAT	FASD0330
	IF (TID(6,I).LE.-2.0) GO TO 245	FASD0340
	SA(I)=0.0	FASD0350
	SF(I)=0.0	FASD0360
	SSC(I)=SPO(I)	FASD0370
	IF (TID(6,I).GE.0.0.AND.TID(7,I).GE.0.0.AND.TID(8,I).GE.0.0)	FASD0380
	1 GO TO 300	FASD0390
	JST=LLIM(I)	FASD0400
	JEND=JST+NORES(I)-1	FASD0410
	DO 240 J=JST,JEND	FASD0420
	X=RHGT(J)*(E(JK)-EZERO(J))	FASD0430
	XTEST=ABS(X)	FASD0440
	IF (XI(J).LT.1.0) XTEST=XTEST*XI(J)	FASD0450
	IF (XTEST.LE.150.0) GO TO 220	FASD0460
	IF (X.GT.0.0) GO TO 240	FASD0470
	PSI=1.0/(1.0+X*X)	FASD0480
	GO TO 230	FASD0490

C	CALCULATE PSI(X,XI) AND CHI(X,XI)	FASD0500
C	SHALL WE USE ASYMPTOTIC OR CONVERGENT SERIES	FASD0510
220	THE=4.0/(XI(J)*XI(J))	FASD0520
	AXI=ABS(X)	FASD0530
	IF(AXI-1.2)21,12,12	FASD0540
12	IF(AXI-10.0)23,14,14	FASD0550
14	IF(AXI-100.0)25,16,16	FASD0560
16	IF (AXI-500.0) 27,18,18	FASD0570
18	IF (AXI-2500.0) 29,29,31	FASD0580
21	IF(0.275*AXI*AXI+0.05-THE)78,78,59	FASD0590
23	IF(0.12*AXI*AXI +0.28-THE)78,78,59	FASD0600
25	IF (0.08*AXI*AXI+1.8-THE) 78,78,59	FASD0610
27	IF (0.0717*AXI*AXI+83.0-THE) 78,78,59	FASD0620
29	IF (0.0635*AXI*AXI+2100.0-THE) 78,78,59	FASD0630
31	IF (0.111*AXI**1.93-THE) 78,78,59	FASD0640
C	TO 59 FOR ASYMPTOTIC SERIES	FASD0650
59	SQ = X*X+1.0	FASD0660
	AJ=1.0/SQ	FASD0670
	BB=THE*AJ	FASD0680
	A(1)=0.5	FASD0690
	A(2)=0.75	FASD0700
	A(3)=1.875	FASD0710
	A(4)=6.5625	FASD0720
	AH=X*AJ	FASD0730
	T1=(SQ-2.0)*AJ	FASD0740
	T2=2.0*AH	FASD0750
	PSI=AJ	FASD0760
	CHI=(1.0-BB)*AH	FASD0770
	B=1.0	FASD0780
	DO 10 K=1,4	FASD0790
	B=B*BB	FASD0800
	AB=A(K)*B	FASD0810
	AT=T2*AJ	FASD0820
	AJ=AJ*T1+T2*AH	FASD0830
	AH=T1*AH-AT	FASD0840
	PSI=PSI+AB*AJ	FASD0850
	S1=2*K+1	FASD0860
	XAJ=X*AJ	FASD0870
	CHI=CHI+AB*(XAJ-0.5*S1*BB*(XAJ+AH))	FASD0880
10	CONTINUE	FASD0890
	CHI=CHI*2.0	FASD0900
	GO TO 230	FASD0910
	TO 78 FOR CONVERGENT SERIES	FASD0920
	CALCULATE GAMMA INCOMPLETE(0)	FASD0930
78	TT=1.0/THE	FASD0940
	IF(TT-8.4)81,81,82	FASD0950
81	CALL GAMINC(TT,FR)	FASD0960
	G1C=FR*EXP(TT)*SQRT(TT)	FASD0970
	GO TO 83	FASD0980
82	V=0.5*XI(J)	FASD0990

TWOV=XI(J)	FASD1000
G1C=V/(V+1.0/(TWOV+2.0/(V+3.0/(TWOV+4.0/(V+5.0/(TWOV+6.0/	FASD1010
1 (V+7.0/(TWOV+2.5)))))))))	FASD1020
83 RAT=X*X	FASD1030
G2C= 2.0*(1.0-G1C)	FASD1040
C1=RAT*TT	FASD1050
C11=C1	FASD1060
TEP=G1C+C1*TT*G2C	FASD1070
TEC=G2C	FASD1080
FQ1=1.0	FASD1090
C2=X /THE	FASD1100
C3=EXP(-X *C2)	FASD1110
T9=1.0	FASD1120
DO 91 KZ=1,100	FASD1130
FQ1=FQ1+1.0	FASD1140
T9=T9+2.0	FASD1150
G2C=2.0/T9*(1.0-TT*G2C)	FASD1160
TR=C11*G2C	FASD1170
C11=C1*C11/FQ1	FASD1180
TR1=C11*TT*G2C	FASD1190
TEP=TEP+TR1	FASD1200
TEC=TEC+TR	FASD1210
IF (ABS (TR/TEC)-0.00001)93,93,91	FASD1220
91 CONTINUE	FASD1230
WRITE (6,603)	FASD1240
603 FORMAT (83H0IN CALCULATION OF PSI AND CHI, CONVERGENT SERIES UNCON	FASD1250
1VERGED AFTER 100 ITERATIONS.)	FASD1260
93 PSI =C3*TEP	FASD1270
CHI =C2*C3*TEC*2.0	FASD1280
230 Y=FACT2(J)*PSI*RE	FASD1290
SA(I)=SA(I)+Y	FASD1300
SF(I)=SF(I)+FRAT(J)*Y	FASD1310
IF (XTEST.GT.150.0) GO TO 240	FASD1320
SSC(I)=SSC(I)+FACT3(J)*PSI+FACT1(J)*CHI	FASD1330
240 CONTINUE	FASD1340
SCAP(I)=SA(I)-SF(I)	FASD1350
IF (SSC(I).LT.0.0) SSC(I)=0.0	FASD1360
GO TO 300	FASD1370
C	FASD1380
C READ CROSS-SECTIONS FROM CARDS AND INTERPOLATE	FASD1390
245 CONTINUE	FASD1400
N=N+1	FASD1410
JTAPE=KTAPE(N)	FASD1420
IF (ELAST(I).GT.0.0) GO TO 248	FASD1430
246 READ (JTAPE,500) ELAST(I),SCAPL(I),SSCL(I),SFL(I)	FASD1440
500 FORMAT (4E12.6)	FASD1450
JPTS(I)=JPTS(I)+1	FASD1460
247 READ (JTAPE,500) ENEXT(I),SCAPN(I),SSCN(I),SFN(I)	FASD1470
JPTS(I)=JPTS(I)+1	FASD1480
248 IF (ENEXT(I).GT.E(JK)) GO TO 250	FASD1490

IF (ABS(ELAST(I)-E(JK)).LE.1.0E-5*ELAST(I)) GO TO 252	FASD1500
249 IF (ELAST(I).GT.E(JK))GO TO 251	FASD1510
GO TO 252	FASD1520
250 ELAST(I)=ENEXT(I)	FASD1530
SCAPL(I)=SCAPN(I)	FASD1540
SSCL(I) = SSCN(I)	FASD1550
SFL(I) = SFN(I)	FASD1560
IF (JPTS(I).LT.KPTS(N)) GO TO 247	FASD1570
GO TO 252	FASD1580
251 ERATIO = (E(JK)-ENEXT(I))/(ELAST(I)-ENEXT(I))	FASD1590
SCAP(I)=SCAPN(I) + ERATIO*(SCAPL(I)-SCAPN(I))	FASD1600
SSC(I) = SSCN(I) + ERATIO*(SSCL(I)-SSCN(I))	FASD1610
SF(I) = SFN(I) + ERATIO*(SFL(I)-SFN(I))	FASD1620
GO TO 253	FASD1630
252 SCAP(I)=SCAPL(I)	FASD1640
SSC(I) = SSCL(I)	FASD1650
SF(I) = SFL(I)	FASD1660
253 IF (JK.LT.NPTS) GO TO 300	FASD1670
IF (JPTS(I).GE.KPTS(N)) GO TO 300	FASD1680
J1=JPTS(I)+1	FASD1690
J2=KPTS(N)	FASD1700
DO 254 K=J1,J2	FASD1710
254 READ (JTAPE) DUMMY	FASD1720
300 CONTINUE	FASD1730
RETURN	FASD1740
END	FASD1750

\$IBFTC	NUTZ	LIST,DECK,REF	08-09-65	NUTZ0000
		SUBROUTINE NUTZ(I,MT)		NUTZ0010
C				NUTZ0020
C		COMPUTE NUMBER OF DOWNSCATTERINGS		NUTZ0030
C		AND WRITE DATA ON CROSS SECTION TAPE (NDATA)		NUTZ0040
C				NUTZ0050
	COMMON /ALL/	NIN,NOUT,NDATA,NIN1,NIN3,JHYD,NEL,NARRAY,NPAGE,LINES		NUTZ0060
	1,NPROB,NPTS,INDEX,NPLOT,TITLE(12),TID(10,20),CNAME(5,20),LINEPP			NUTZ0070
	2 ,MAT,MFRAME			NUTZ0080
	COMMON /TABLES/	CS1,CS2,CS3,SLABT(505),CYLT(305)		NUTZ0090
	COMMON /BSET/	LIMST,LIM1,LIM2,NPRINT,JPRINT(10),DUM(200),DE1,DE2		NUTZ0100
	1 ,DE3,EZERO,E(8000),SCAP(20),SF(20),SSC(20),SA(20),ALPHA(20)			NUTZ0110
	2 ,KTAPE(3),KPTS(10)			NUTZ0120
	3	,NORES(20),LLIM(20),SPO(20),EZERO(600),RHGT(600)		NUTZ0130
	4 ,FACT1(600),FACT2(600),FACT3(600),FRAT(600),XI(600)			NUTZ0140
	5	,GI(500),GJ(500),GF(500),EO(500),GG(500),GN(500)		NUTZ0150
	6 ,SPIN(500)			NUTZ0160
	EQUIVALENCE	(TID,NTID),(DUM,LIM),(NPT,NPTS),(NDATA,NDATA1)		NUTZ0170
	DIMENSION	NTID(10,20), LIM(200)		NUTZ0180
	ND=1			NUTZ0190
	NT=MT			NUTZ0200
	LIMM1=LIMST*(NT-1)			NUTZ0210
	DO 40 K=1,NEL			NUTZ0220
	ETO=E(I)*ALPHA(K)			NUTZ0230
	ETL=E(I-1)*ALPHA(K)			NUTZ0240
	NST=I			NUTZ0250
	NEND=MINO(LIMST,NPTS-LIMM1)			NUTZ0260
20	DO 30 J=NST,NEND			NUTZ0270
	IF (E(J).GT.ETO) GO TO 30			NUTZ0280
	LIM(ND)=J-I-1			NUTZ0290
	IF (LIM(ND).LT.0) LIM(ND)=LIM(ND)+LIMM1			NUTZ0300
	JJ=J-1			NUTZ0310
	GO TO 31			NUTZ0320
30	CONTINUE			NUTZ0330
	IF (NEND.GE.NPTS-LIMM1) GO TO 25			NUTZ0340
	IF (NEND.EQ.I-1) GO TO 25			NUTZ0350
	NST=1			NUTZ0360
	LIMM1=LIMST*NT			NUTZ0370
	NEND=MINO(I-1,NPTS-LIMM1)			NUTZ0380
	NT=NT+1			NUTZ0390
	GO TO 20			NUTZ0400
25	LIM(ND)=NEND-I			NUTZ0410
	IF (LIM(ND).LT.0) LIM(ND)=LIM(ND)+LIMM1			NUTZ0420
	JJ=NEND			NUTZ0430
31	ND=ND+1			NUTZ0440
	NCORT=0			NUTZ0450
320	IF (JJ.GE.1) GO TO 32			NUTZ0460
	JJ=LIMST			NUTZ0470
32	IF (ETL.LT.E(JJ))GO TO 33			NUTZ0480

```

NCORT=NCORT+1
NDC=NCORT+ND
DUM(NDC)=E(JJ)
JJ=JJ-1
GO TO 320
33 LIM(ND)=NCORT
ND=ND+NCORT+1
IF (TID(6,K).GE.0.0) GO TO 34
DUM(ND)=SCAP(K)
ND=ND+1
34 IF (TID(7,K).GE.0.0) GO TO 35
DUM(ND)=SF(K)
ND=ND+1
35 IF (TID(8,K).GE.0.0) GO TO 40
DUM(ND)=SSC(K)
ND=ND+1
40 CONTINUE
ND=ND-1
WRITE (NDATA1) E(I),DE1,DE2,DE3,ND,(DUM(J),J=1,ND)
RETURN
END

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NUTZ0490
NUTZ0500
NUTZ0510
NUTZ0520
NUTZ0530
NUTZ0540
NUTZ0550
NUTZ0560
NUTZ0570
NUTZ0580
NUTZ0590
NUTZ0600
NUTZ0610
NUTZ0620
NUTZ0630
NUTZ0640
NUTZ0650
NUTZ0660
NUTZ0670
NUTZ0680
NUTZ0690

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\$IBFTC PRINT LIST,DECK,REF
 SUBROUTINE PRINT(JST,EE)

08-09-65PRIN0000

PRINT ROUTINE FOR GAROL DATA

COMMON /ALL/ NIN,NOUT,NDATA,NINI,NIN3,JHYD,NEL,NARRAY,NPAGE,LINES	PRIN0050
1,NPROB,NPTS,INDEX,NPLOT,TITLE(12),TID(10,20),CNAME(5,20),LINEPP	PRIN0060
2 ,MAT,MFRAME	PRIN0070
COMMON /TABLES/ CS1,CS2,CS3,SLABT(505),CYLT(305)	PRIN0080
COMMON /BSET/ LIMST,LIM1,LIM2,NPRINT,JPRINT(10),DUM(200),DE1,DE2	PRIN0090
1 ,DE3,EEZERO,E(8000),SCAP(20),SF(20),SSC(20),SA(20),ALPHA(20)	PRIN0100
2 ,KTAPE(3),KPTS(10)	PRIN0110
3 ,NORES(20),LLIM(20),SPO(20),EZERO(600),RHGT(600)	PRIN0120
4 ,FACT1(600),FACT2(600),FACT3(600),FRAT(600),XI(600)	PRIN0130
5 ,GI(500),GJ(500),GF(500),EO(500),GG(500),GN(500)	PRIN0140
6 ,SPIN(500)	PRIN0150
EQUIVALENCE (TID,NTID),(DUM,LIM),(NPT,NPTS),(NDATA,NDATA1)	PRIN0160
DIMENSION NTID(10,20), LIM(200)	PRIN0170
DIMENSION FMT(24), DUM1(9), DUM2(9), NSUB(9), NFMT(1)	PRIN0180
1 , T(20)	PRIN0190
EQUIVALENCE (FMT,NFMT)	PRIN0200
IF (NCODE.EQ.2345) GO TO 100	PRIN0210
CALL BOOLER(6HCAPTUR,CAP)	PRIN0220
CALL BOOLER(6HE ,TURE)	PRIN0230
CALL BOOLER(6HFISSIO,FIS)	PRIN0240
CALL BOOLER(6HNS ,SION)	PRIN0250
CALL BOOLER(6HSCATTE,SCAT)	PRIN0260
CALL BOOLER(6HRS ,TER)	PRIN0270
CALL BOOLER(6H(20X, ,FMT(1))	PRIN0280
CALL BOOLER(6HA6,A4, ,A6A4)	PRIN0290
CALL BOOLER(6H ,BLANK)	PRIN0300
CALL BOOLER(6H2X ,TWOX)	PRIN0310
CALL BOOLER(6H X ,X)	PRIN0320
CALL BOOLER(6H) ,ENDFMT)	PRIN0330
NCODE=2345	PRIN0340
N=1	PRIN0350
NF=2	PRIN0360
ND=0	PRIN0370
L=0	PRIN0380
DO 50 K=1,MAT	PRIN0390
IF (K.NE.JPRINT(N)) GO TO 50	PRIN0400
FMT(NF)=A6A4	PRIN0410
FMT(NF+1)=TWOX	PRIN0420
NF=NF+2	PRIN0430
NSPACE=(NTID(9,K)-1)*12	PRIN0440
NS=NSPACE/10	PRIN0450
NFMT(NF)=NS*64+NSPACE-NS*10	PRIN0460
IF (NFMT(NF).EQ.0) GO TO 10	PRIN0470
FMT(NF+1)=X	PRIN0480
NF=NF+2	PRIN0490

10 IF (TID(6,K).GE.0.0) GO TO 20	PRIN0500
ND=ND+1	PRIN0510
NSUB(ND)=K	PRIN0520
T(L+1)=CAP	PRIN0530
T(L+2)=TURE	PRIN0540
L=L+2	PRIN0550
IF (ND.GE.9) GO TO 60	PRIN0560
IF (TID(6,K).LE.-2.0) GO TO 21	PRIN0570
20 IF (TID(7,K).GE.0.0) GO TO 30	PRIN0580
21 ND=ND+1	PRIN0590
NSUB(ND)=K+20	PRIN0600
T(L+1)=FIS	PRIN0610
T(L+2)=SION	PRIN0620
L=L+2	PRIN0630
IF (ND.GE.9) GO TO 60	PRIN0640
IF (TID(6,K).LE.-2.0) GO TO 31	PRIN0650
30 IF (TID(8,K).GE.0.0) GO TO 40	PRIN0660
31 ND=ND+1	PRIN0670
NSUB(ND)=K+40	PRIN0680
T(L+1)=SCAT	PRIN0690
T(L+2)=TER	PRIN0700
L=L+2	PRIN0710
IF (ND.GE.9) GO TO 60	PRIN0720
40 CONTINUE	PRIN0730
N=N+1	PRIN0740
IF (N.GT.NPRINT) GO TO 60	PRIN0750
50 CONTINUE	PRIN0760
60 IF (FMT(NF-1).EQ.X) NF=NF-2	PRIN0770
FMT(NF)=ENDFMT	PRIN0780
IF(NF.GE.24) GO TO 80	PRIN0790
NF=NF+1	PRIN0800
DO 70 NJ=NF,24	PRIN0810
70 FMT(NJ)=BLANK	PRIN0820
80 CONTINUE	PRIN0830
GO TO 105	PRIN0840
100 IF (MOD(JST,52).GT.0) GO TO 115	PRIN0850
CALL HEAD	PRIN0860
105 DO 110 I=1,NPRINT	PRIN0870
J=JPRINT(I)	PRIN0880
DUM1(I)=CNAME(1,J)	PRIN0890
DUM2(I)=CNAME(2,J)	PRIN0900
110 CONTINUE	PRIN0910
WRITE (6,FMT)(DUM1(I),DUM2(I),I=1,NPRINT)	PRIN0920
WRITE (6,601)(T(I),I=1,L)	PRIN0930
601 FORMAT (8X,9HENERGY-EV 3X 18A6)	PRIN0940
115 WRITE (6,600)	PRIN0950
600 FORMAT (1X)	PRIN0960
DO 120 I=1,ND	PRIN0970
J=NSUB(I)	PRIN0980
120 DUM1(I)=SCAP(J)	PRIN0990

```

WRITE (6,602) JST,EE,(DUM1(LL),LL=1,ND)
602 FORMAT (I6,1P10E12.5)
RETURN
END

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PRIN1000
PRIN1010
PRIN1020
PRIN1030

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$IBFTC GAMINC LIST,DECK,REF
SUBROUTINE GAMINC(X1,FR)
C
C CALCULATE INCOMPLETE GAMMA-FUNCTION , G(A,X) FOR A=0.5)
C ADAPTED FOR GAROL FROM THE ZUT PROGRAM (GA-2525)
C
C=0.0
EX=1.0
SUM=1.0
DO 20 K=1,20
DO 15 J=1,5
C=C+1.0
EX=-X1*EX/C
TERM=EX/(2.0*C+1.0)
15 SUM=SUM+TERM
IF(ABS(TERM/SUM)-1.0E-5)22,22,20
20 CONTINUE
22 FR=2.0*SQRT(X1)*SUM
FR=1.7724539-FR
RETURN
END

```

```

08-09-65GAM10000
GAM10010
GAM10020
GAM10030
GAM10040
GAM10050
GAM10060
GAM10070
GAM10080
GAM10090
GAM10100
GAM10110
GAM10120
GAM10130
GAM10140
GAM10150
GAM10160
GAM10170
GAM10180
GAM10190
GAM10200

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$IBFTC HEAD LIST,DECK,REF
SUBROUTINE HEAD
COMMON /ALL/ NIN,NOUT,NDATA,NIN1,NIN3,JHYD,NEL,NARRAY,NPAGE,LINES
1,NPROB,NPTS,INDEX,NPLOT,TITLE(12),TID(10,20),CNAME(5,20),LINEPP
2 ,MAT,MFRAME
COMMON /PLOT/ TLABEL(12),XLABEL(12),YLABEL(12),T2(12)
NPAGE=NPAGE+1
WRITE (6,601)(TLABEL(I),I=1,12),NPAGE
601 FORMAT(26H1GAROL DATA TAPE, LABELED 12A6, 22X 4HPAGE I6)
RETURN
END

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08-09-65HEAD0000
HEAD0010
HEAD0020
HEAD0030
HEAD0040
HEAD0050
HEAD0060
HEAD0070
HEAD0080
HEAD0090
HEAD0100

```

* * * * *
 * G A R D L L I N K 4 *
 * * * * *

\$IBMAP	COMSET	LIST,REF	08-09-654COM0000
B	BOOL	7022	4COM0010
BSET	CONTRL	A,C	4COM0020
A	BSS	B	4COM0030
C	EQU	*	4COM0040
	END		4COM0050

\$IBFTC	LINK4	LIST,DECK,REF	08-09-654LNK0000
C			4LNK0010
C		LINK 4	4LNK0020
C		RESONANCE OVERLAP CALCULATION	4LNK0030
C			4LNK0040
	COMMON /ALL/	NIN,NOUT,NDATA,NIN1,NIN3,JHYD,NEL,NARRAY,NPAGE,LINES	4LNK0050
	1,NPROB,NPTS,INDEX,NPLOT,TITLE(12),TID(10,20),CNAME(5,20),LINEPP		4LNK0060
	2 ,MAT,MFRAME		4LNK0070
	COMMON /BSET/	V(2), R, IGEOM, EC, EST, EEND, NHYD, HYD(2)	4LNK0080
	1 , E, DE1, DE2, DE3, DE4, SUM(2), SUMA, SUMB, T(2), S(2)		4LNK0090
	2 , TERM, CC, MORDER(10), ELBAR(2)		4LNK0100
	3 , ZID(10,10), CAP(10), SCAT(10), FIS(10), LIM(10), DENS(10,2)		4LNK0110
	4 , DENSTY(10,2), ALPHA(10), TOTAL(2), P(2), D(2), Q(2), DDQQ		4LNK0120
	5 , PHI(2), SORC(2)		4LNK0130
	6 , NBG, BEG(50), BPHI(50,2), BCAP(50,10,2), BSCAT(50,10,2)		4LNK0140
	7 , BFIS(50,10,2), CELLS(50), CELLC(50), CELLF(50), OGPFI(2)		4LNK0150
	8 , OGSCAT(3), OGCAP(3), OGFIS(3)		4LNK0160
	9 ,TNAME(5,10)		4LNK0170
	COMMON /PLOTT/	TLABEL(12),XLABEL(12),YLABEL(12),TT2(12),NFRAME	4LNK0180
	EQUIVALENCE (TID,NID), (ZID,ID), (DUM,NDUM), (NDATA,NDATA1)		4LNK0190
	DIMENSION DUM(100)		4LNK0200
	DIMENSION NID(10,50), ID(10,10), NDUM(1)		4LNK0210
	DIMENSION EJ(5,10), NCORT(10),PHIL(2), SCATL(10), LIML(10)		4LNK0220
	1 ,DETP(2), TA(8000,2)		4LNK0230
	DIMENSION XS(2)		4LNK0240
C			4LNK0250
C		READ PROBLEM INPUT CARDS	4LNK0260
	LIMST=8000		4LNK0270
100	CALL INPUT		4LNK0280
	NPRINT=INDEX		4LNK0290
	NXSORC=NHYD		4LNK0300
	IF (NXSORC.GE.1) CALL XSORC(1,DA,DA)		4LNK0310
	IF (NPLOT.LT.1) GO TO 160		4LNK0320
	NIN3=3		4LNK0330
	REWIND NIN3		4LNK0340
	WRITE (NIN3)((TNAME(I,K),I=1,5),K=1,MAT)		4LNK0350
	NIN1=2		4LNK0360
	REWIND NIN1		4LNK0370

ASSIGN 321 TO NGOP	4LNK0380
ASSIGN 400 TO NGOQ	4LNK0390
GO TO 170	4LNK0400
160 ASSIGN 326 TO NGOP	4LNK0410
ASSIGN 500 TO NGOQ	4LNK0420
170 NERR=4	4LNK0430
NHYD=0	4LNK0440
ASSIGN 771 TO JGO	4LNK0450
DO 180 N=1,LIMST	4LNK0460
DO 180 NR=1,2	4LNK0470
180 TA(N,NR)=0.0	4LNK0480
DE4=0.0	4LNK0490
DEC=1.0/EC	4LNK0500
DO 185 NG=1,NBG	4LNK0510
DO 185 NR=1,2	4LNK0520
BPHI(NG,NR)=0.0	4LNK0530
DO 185 K=1,MAT	4LNK0540
BCAP(NG,K,NR)=0.0	4LNK0550
BFIS(NG,K,NR)=0.0	4LNK0560
BSCAT(NG,K,NR)=0.0	4LNK0570
185 CONTINUE	4LNK0580
IF (JHYD.GT.0.AND.MORDER(1).EQ.1) GO TO 190	4LNK0590
GO TO 195	4LNK0600
190 NHYD=1	4LNK0610
HYD(1)=0.0	4LNK0620
HYD(2)=0.0	4LNK0630
C READ THROUGH DATA TAPE UNTIL STARTING ENERGY (EST) IS FOUND	4LNK0640
195 IF (EST.GT.0.0) GO TO 201	4LNK0650
READ (NDATA1) E,DE1,DE2,DE3,NENTRY,(DUM(J),J=1,NENTRY)	4LNK0660
EST=E	4LNK0670
EC=E	4LNK0680
DEC=1.0/E	4LNK0690
GO TO 203	4LNK0700
201 READ (NDATA1) E,DE1,DE2,DE3,NENTRY,(DUM(J),J=1,NENTRY)	4LNK0710
202 IF (E.GT.EST) GO TO 201	4LNK0720
203 JST=0	4LNK0730
EC=E	4LNK0740
DEC=1.0/EC	4LNK0750
JPRINT=0	4LNK0760
NG=1	4LNK0770
DE12=1.0-DE2	4LNK0780
DO 204 K=1,MAT	4LNK0790
204 LIML(K)=1	4LNK0800
CALL TICKER(TIME)	4LNK0810
TIME=TIME/216.0	4LNK0820
WRITE (6,3001) TIME,NHYD	4LNK0830
3001 FORMAT (90X 26HSTART SPECTRUM CALCULATION F8.3,3H MH/ 90X	4LNK0840
1 6HNHYD = I3)	4LNK0850
ASSIGN 221 TO NGO1	4LNK0860
ASSIGN 231 TO NGO2	4LNK0870

ASSIGN 2481 TO NG05	4LNK0880
2049 ASSIGN 291 TO NG06	4LNK0890
205 DO 206 NR=1,2	4LNK0900
SUM(NR)=0.0	4LNK0910
206 TOTAL(NR)=0.0	4LNK0920
JST=JST+1	4LNK0930
IF (JST.GT.LIMST) JST=1	4LNK0940
READ MICROSCOPIC DATA	4LNK0950
NN=0	4LNK0960
M=1	4LNK0970
DO 220 K=1,NAT	4LNK0980
MC=MORDER(K)	4LNK0990
210 NN=NN+1	4LNK1000
LIM(K)=NDUM(M)	4LNK1010
M=M+1	4LNK1020
NCORT(K)=NDUM(M)	4LNK1030
M=M+1	4LNK1040
IF (NCORT(K).LE.0) GO TO 212	4LNK1050
NC=NCORT(K)	4LNK1060
DO 211 J=1,NC	4LNK1070
EJ(J,K)=DUM(M)	4LNK1080
M=M+1	4LNK1090
211 CONTINUE	4LNK1100
212 IF (MC.LE.1) GO TO 213	4LNK1110
MC=MC-1	4LNK1120
M=M+NID(9,NN)	4LNK1130
GO TO 210	4LNK1140
213 IF (ZID(6,K).GE.0.0) GO TO 214	4LNK1150
CAP(K)=DUM(M)	4LNK1160
M=M+1	4LNK1170
GO TO 215	4LNK1180
214 CAP(K)=ZID(6,K)/SQRT(E)	4LNK1190
215 IF (ZID(7,K).GE.0.0) GO TO 216	4LNK1200
FIS(K)=DUM(M)	4LNK1210
M=M+1	4LNK1220
GO TO 217	4LNK1230
216 FIS(K)=0.0	4LNK1240
217 IF (ZID(8,K).GE.0.0) GO TO 218	4LNK1250
SCAT(K)=DUM(M)	4LNK1260
M=M+1	4LNK1270
GO TO 219	4LNK1280
218 SCAT(K)=ZID(8,K)	4LNK1290
COMPUTE TOTAL CROSS SECTION FOR REGIONS 1 AND 2	4LNK1300
219 S1=CAP(K)+FIS(K)+SCAT(K)	4LNK1310
IF (LIML(K).LE.0) GO TO 2191	4LNK1320
SS=SCAT(K)*(DE1-1.0)	4LNK1330
GO TO 2193	4LNK1340
2191 AA=1.0-ALPHA(K)	4LNK1350
SS=(SCAT(K)*AA*(ELAST*(1.0+ALPHA(K))-2.0*E))/(2.0*ALPHA(K)*(ELAST-	4LNK1360
1 E))	4LNK1370

	BB=0.5*(E/(ELAST-E))*AA**2/ALPHA(K)*SCATL(K)	4LNK1380
	DO 2192 NR=1,2	4LNK1390
	IF (DENS(K,NR).LE.0.0) GO TO 2192	4LNK1400
	TA(JST,NR)=TA(JST,NR)+BB*PHIL(NR)*DENSTY(K,NR)	4LNK1410
2192	CONTINUE	4LNK1420
2193	DO 220 NR=1,2	4LNK1430
	IF (DENS(K,NR).LE.0.0) GO TO 220	4LNK1440
	TOTAL(NR)=TOTAL(NR)+S1*DENS(K,NR)	4LNK1450
	SUM(NR)=SUM(NR)+SS*DENSTY(K,NR)	4LNK1460
220	CONTINUE	4LNK1470
	ARG=ELBAR(1)*TOTAL(1)	4LNK1480
C	COMPUTE ESCAPE PROBABILITY FOR REGIONS 1 AND 2	4LNK1490
	GO TO (4,6,1,2,1,1,222),IGEOM	4LNK1500
6	ARG1=ARG*0.25	4LNK1510
	GO TO 3	4LNK1520
1	ARG1=ARG*.5	4LNK1530
	GO TO 3	4LNK1540
2	ARG1=ARG*.75	4LNK1550
3	CALL PROB(ARG1,IGEOM,P(1))	4LNK1560
C	APPLY DANC OFF CORRECTION, IF ANY, TO ESCAPE PROBABILITY TERM	4LNK1570
	IF (CC.GT.0.0) P(1)=P(1)*(1.0-CC)/(1.0-CC*(1.0-ARG*P(1)))	4LNK1580
	P(2)=P(1)*ARG/(TOTAL(2)*ELBAR(2))	4LNK1590
	GO TO 5	4LNK1600
4	P(1)=0.0	4LNK1610
	P(2)=0.0	4LNK1620
	ASSIGN 772 TO JGO	4LNK1630
	IGEOM=7	4LNK1640
5	GO TO NG01,(221,222)	4LNK1650
221	IF (MORDER(1).GT.1.AND.LIM(1).GT.LIMST) GO TO 350	4LNK1660
	ASSIGN 222 TO NG01	4LNK1670
C	COMPUTE FLUXES FOR REGIONS 1 AND 2	4LNK1680
222	DO 223 NR=1,2	4LNK1690
	MR=3-NR	4LNK1700
	D(NR)=V(MR)*(TOTAL(MR)-(1.0-P(MR))*SUM(MR))	4LNK1710
	Q(NR)=V(MR)*SUM(MR)*P(MR)	4LNK1720
	SORC(NR)=0.0	4LNK1730
223	CONTINUE	4LNK1740
	DDQQ=1.0/(D(1)*D(2)-Q(1)*Q(2))	4LNK1750
	DO 230 K=1,MAT	4LNK1760
	DO 230 NT=1,2	4LNK1770
	IF (DENS(K,NT).LE.0.0) GO TO 230	4LNK1780
	IF (E.LT.ALPHA(K)*EC) GO TO 230	4LNK1790
	SORC(NT)=SORC(NT)+DENSTY(K,NT)*ZID(5,K)*(DEC-ALPHA(K)/E)	4LNK1800
230	CONTINUE	4LNK1810
	IF (NXSORC.NE.1) GO TO 2300	4LNK1820
	CALL XSORC(2,E,XS)	4LNK1830
	SORC(1)=SORC(1)+XS(1)	4LNK1840
	SORC(2)=SORC(2)+XS(2)	4LNK1850
2300	SORC(1)=SORC(1)*V(1)	4LNK1860
	SORC(2)=SORC(2)*V(2)	4LNK1870

	SPD=SORC(1)*P(1)-SORC(2)*P(2)	4LNK1880
	GO TO NG02,(231,233,234)	4LNK1890
231	T(1)=SORC(2)+SPD	4LNK1900
	T(2)=SORC(1)-SPD	4LNK1910
	DO 2310 NR=1,2	4LNK1920
	MR=3-NR	4LNK1930
	D(NR)=TOTAL(MR)*V(MR)	4LNK1940
	PHI(MR)=T(NR)/D(NR)	4LNK1950
	S(MR)=E*PHI(MR)*TOTAL(MR)	4LNK1960
	DETP(MR)=DE12*PHI(MR)	4LNK1970
2310	CONTINUE	4LNK1980
	LINES=60	4LNK1990
	IF (NHYD.GT.0) GO TO 232	4LNK2000
	ASSIGN 234 TO NG02	4LNK2010
	GO TO 2401	4LNK2020
232	ASSIGN 233 TO NG02	4LNK2030
	ASSIGN 244 TO NG04	4LNK2040
	GO TO 2401	4LNK2050
233	DO 2330 NR=1,2	4LNK2060
2330	TA(JST,NR)=TA(JST,NR)+HYD(NR)	4LNK2070
	ASSIGN 244 TO NG04	4LNK2080
234	T(1)=TA(JST,2)*V(2)*(1.0-P(2))+TA(JST,1)*V(1)*P(1)+SORC(2)+SPD	4LNK2090
	T(2)=TA(JST,1)*V(1)*(1.0-P(1))+TA(JST,2)*V(2)*P(2)+SORC(1)-SPD	4LNK2100
	TA(JST,1)=0.0	4LNK2110
	TA(JST,2)=0.0	4LNK2120
240	DO 2400 NR=1,2	4LNK2130
	MR=3-NR	4LNK2140
	GO TO JGO,(771,772)	4LNK2150
772	PHI(NR)=T(MR)/D(MR)	4LNK2160
	GO TO 773	4LNK2170
771	PHI(NR)=(Q(NR)*T(NR)+T(MR)*D(NR))*DDQQ	4LNK2180
773	S(NR)=E*PHI(NR)*TOTAL(NR)	4LNK2190
	DETP(NR)=DE12*PHI(NR)	4LNK2200
2400	CONTINUE	4LNK2210
C	PRINT FLUXES FOR REGIONS 1 AND 2	4LNK2220
2401	IF (NPRINT.LE.0) GO TO 242	4LNK2230
	LINES=LINES+1	4LNK2240
	JPRINT=JPRINT+1	4LNK2250
	IF (LINES.GT.LINEPP) CALL HEAD	4LNK2260
	WRITE (NOUT,603) JPRINT,E,PHI(1),PHI(2),SORC(1),SORC(2),TOTAL(1),	4LNK2270
	1 TOTAL(2),S(1),S(2)	4LNK2280
	603 FORMAT (I5,1P9E14.6)	4LNK2290
C	COMPUTE SOURCES FROM THIS ENERGY TO ALL SUCCEEDING	4LNK2300
C	ENERGIES FOR THIS MATERIAL	4LNK2310
242	DO 250 K=1,MAT	4LNK2320
	GO TO NG04,(243,244)	4LNK2330
244	ASSIGN 243 TO NG04	4LNK2340
	DO 2440 NR=1,2	4LNK2350
2440	HYD(NR)=HYD(NR)+SCAT(K)*DETP(NR)*DENSTY(K,NR)	4LNK2360
	GO TO 250	4LNK2370

243	IF (LIM(K).LE.0) GO TO 250	4LNK2380
	DO 2500 NR=1,2	4LNK2390
	IF (DENS(K, NR).LE.0.0) GO TO 2500	4LNK2400
	SUMA=SCAT(K)*DETP(NR)*DENSTY(K, NR)	4LNK2410
245	NST=JST+1	4LNK2420
	IF (NST.GT.LIMST) NST=1	4LNK2430
	NEND=NST+LIM(K)-1	4LNK2440
	IF (NEND.LE.LIMST) GO TO 247	4LNK2450
	DO 246 N=NST, LIMST	4LNK2460
	TA(N, NR)=TA(N, NR)+SUMA	4LNK2470
246	CONTINUE	4LNK2480
	NST=1	4LNK2490
	NEND=NEND-LIMST	4LNK2500
247	DO 248 N=NST, NEND	4LNK2510
	TA(N, NR)=TA(N, NR)+SUMA	4LNK2520
248	CONTINUE	4LNK2530
	JJ=0	4LNK2540
	NC=NCORT(K)	4LNK2550
	GO TO NG05, (2481, 249)	4LNK2560
2481	ASSIGN 249 TO NG05	4LNK2570
	GO TO 2500	4LNK2580
C	COMPUTE CORRECTION TERMS, IF ANY, AND ADD THEM IN	4LNK2590
249	IF (INC.LE.0) GO TO 2500	4LNK2600
C	COMPUTE CAROL-S CORRECTION	4LNK2610
	R1=(1.0-DE1)*SCAT(K)	4LNK2620
	TA(NEND, NR)=TA(NEND, NR)+R1*PHI(NR)*DENSTY(K, NR)	4LNK2630
	JJ=JJ+1	4LNK2640
C	COMPUTE CHARLIE-S CORRECTION	4LNK2650
	EBAR=EJ(JJ, K)/ALPHA(K)	4LNK2660
	FLAST=SCATL(K)*PHIL(NR)	4LNK2670
	F=SCAT(K)*PHI(NR)	4LNK2680
	FBAR=((EBAR-E)*FLAST+(ELAST-EBAR)*F)/(ELAST-E)	4LNK2690
	CTERM=(EBAR-E)*0.5*(FBAR/EBAR+F/E)	4LNK2700
	TA(NEND, NR)=TA(NEND, NR)+CTERM*DENSTY(K, NR)	4LNK2710
	NC=NC-1	4LNK2720
	NEND=NEND-1	4LNK2730
	IF (NEND.LE.0) NEND=LIMST	4LNK2740
	GO TO 249	4LNK2750
2500	CONTINUE	4LNK2760
250	CONTINUE	4LNK2770
C	ADD TERMS FOR THIS ENERGY INTO SUMMATIONS FOR	4LNK2780
C	BROAD GROUP AVERAGES	4LNK2790
	DE=DE3+DE4	4LNK2800
	IF (E.GT.BEG(NG)) GO TO 280	4LNK2810
	IF (E.EQ.BEG(NG)) GO TO 270	4LNK2820
260	NG=NG+1	4LNK2830
	IF (NG.GT.NBG) GO TO 290	4LNK2840
	IF (E.LT.BEG(NG)) GO TO 260	4LNK2850
	DO 255 NT=1,2	4LNK2860
	DETPX=PHI(NT)*DE3	4LNK2870

BPHI(NG,NT)=DETPX	4LNK2880
DO 255 K=1,MAT	4LNK2890
BSCAT(NG,K,NT)=SCAT(K)*DETPX	4LNK2900
BCAP(NG,K,NT)=CAP(K)*DETPX	4LNK2910
IF (ZID(7,K).LT.0.0) BFIS(NG,K,NT)=FIS(K)*DETPX	4LNK2920
255 CONTINUE	4LNK2930
GO TO 290	4LNK2940
270 DE=DE4	4LNK2950
280 DO 285 NT=1,2	4LNK2960
DETPX=PHI(NT)*DE	4LNK2970
BPHI(NG,NT)=BPHI(NG,NT)+DETPX	4LNK2980
DO 285 K=1,MAT	4LNK2990
BSCAT(NG,K,NT)=BSCAT(NG,K,NT)+SCAT(K)*DETPX	4LNK3000
BCAP(NG,K,NT)=BCAP(NG,K,NT)+CAP(K)*DETPX	4LNK3010
IF (ZID(7,K).LT.0.0) BFIS(NG,K,NT)=BFIS(NG,K,NT)+FIS(K)*DETPX	4LNK3020
285 CONTINUE	4LNK3030
IF (E.EQ.BEG(NG)) GO TO 260	4LNK3040
C STORE ENERGY, FLUXES, AND SCATTERING TERMS FOR USE	4LNK3050
C AT NEXT ENERGY	4LNK3060
290 GO TO NG06,(291,2049,329)	4LNK3070
291 DE4=DE3	4LNK3080
ELAST=E	4LNK3090
DO 310 NR=1,2	4LNK3100
310 PHIL(NR)=PHI(NR)	4LNK3110
DO 320 K=1,MAT	4LNK3120
LIML(K)=LIM(K)	4LNK3130
320 SCATL(K)=SCAT(K)	4LNK3140
GO TO NG0P,(321,326)	4LNK3150
321 DO 325 K=1,MAT	4LNK3160
CAP(K)=CAP(K)*PHI(1)	4LNK3170
FIS(K)=FIS(K)*PHI(1)	4LNK3180
325 CONTINUE	4LNK3190
WRITE (NIN3) E,PHI(1),TOTAL(1)	4LNK3200
WRITE (NIN1)(CAP(K),FIS(K),K=1,MAT)	4LNK3210
326 CONTINUE	4LNK3220
READ (NDATA1) E,DE1,DE2,DE3,NENTRY,(DUM(J),J=1,NENTRY)	4LNK3230
DE12=DE1-DE2	4LNK3240
IF (E.LE.EEND) GO TO 327	4LNK3250
IF (E.GT.BEG(NG)) GO TO 205	4LNK3260
IF (ELAST-BEG(NG).GT.BEG(NG)-E) GO TO 341	4LNK3270
ASSIGN 2049 TO NG06	4LNK3280
GO TO 328	4LNK3290
327 ASSIGN 329 TO NG06	4LNK3300
328 BEG(NG)=ELAST	4LNK3310
GO TO 260	4LNK3320
341 BEG(NG)=E	4LNK3330
GO TO 205	4LNK3340
C FINISH COMPUTING BROAD GROUP AVERAGES AND PRINT RESULTS	4LNK3350
329 CONTINUE	4LNK3360
CALL TICKER(TIME)	4LNK3370

TIME=TIME/216.0	4LNK3380
WRITE (6,3002) TIME	4LNK3390
3002 FORMAT (90X 26H END SPECTRUM CALCULATION F8.3,3H MH)	4LNK3400
IF (NG.GE.NBG) GO TO 300	4LNK3410
NGP1=NG+1	4LNK3420
DO 330 N=NGP1,NBG	4LNK3430
DO 330 NT=1,2	4LNK3440
BPHI(N,NT)=0.0	4LNK3450
DO 330 K=1,MAT	4LNK3460
BCAP(N,K,NT)=0.0	4LNK3470
BSCAT(N,K,NT)=0.0	4LNK3480
BFIS(N,K,NT)=0.0	4LNK3490
330 CONTINUE	4LNK3500
300 IF (NXSORC.GE.1) CALL XSORC(3,DA,DA)	4LNK3510
GO TO NGOQ,(400,500)	4LNK3520
400 REWIND NIN3	4LNK3530
NPTS=JPRINT	4LNK3540
IF (NBG.LE.0) CALL CHAIN(6)	4LNK3550
500 IF (NBG.LE.0) GO TO 100	4LNK3560
CALL CHAIN(5)	4LNK3570
350 WRITE (6,600) LIM(1)	4LNK3580
600 FORMAT(113HOCHAIN 3 IS NOT YET AVAILABLE. PROBLEMS ARE LIMITED, T	4LNK3590
HEREFORE, TO MATERIALS FOR WHICH SOURCES AFFECT LESS THAN/	4LNK3600
2 62H08000 SUCCEEDING ENERGIES. FOR MATERIAL 1, THESE TERMS AFFECT	4LNK3610
3 18, 8HENERGIES)	4LNK3620
CALL EXIT	4LNK3630
END	4LNK3640

\$IBFTC INPUT LIST,DECK,REF
SUBROUTINE INPUT

08-09-65 INPT0000

INPT0010

INPT0020

READ PROBLEM INPUT CARDS AND PRINT PROBLEM SPECIFICATIONS

INPT0030

CHECK SOME OF THE INPUT AGAINST DIMENSIONED LIMITS

INPT0040

INPT0050

COMMON /ALL/ NIN,NDUT,NDATA,NIN1,NIN3,JHYD,NEL,NARRAY,NPAGE,LINES

INPT0060

1,NPROB,NPTS,INDEX,NPLOT,TITLE(12),TID(10,20),CNAME(5,20),LINEPP

INPT0070

2,MAT,NFRAME

INPT0080

COMMON /TABLES/ CS1,CS2,CS3,SLABT(505),CYLT(305)

INPT0090

COMMON /BSET/ V(2), R, 1GEOM, EC, EST, EEND, NHYD, HYD(2)

INPT0100

1, E, DE1, DE2, DE3, DE4, SUM(2), SUMA, SUMB, T(2), S(2)

INPT0110

2, TERM, CC, MORDER(10), ELBAR(2)

INPT0120

3, ZID(10,10), CAP(10), SCAT(10), FIS(10), LIM(10), DENS(10,2)

INPT0130

4, DENSTY(10,2), ALPHA(10), TOTAL(2), P(2), D(2), Q(2), DDQQ

INPT0140

5, PHI(2), SCRC(2)

INPT0150

6, NBG, BEG(50), BPHI(50,2), BCAP(50,10,2), BSCAT(50,10,2)

INPT0160

7, BFIS(50,10,2), CELLS(50), CELLC(50), CELLF(50), OGPFI(2)

INPT0170

8, OGSCAT(3), OGCAP(3), OGFIS(3)

INPT0180

9, TNAME(5,10)

INPT0190

COMMON /PLOTT/ TLABEL(12),XLABEL(12),YLABEL(12),TT2(12),NFRAME

INPT0200

EQUIVALENCE (TID,NID), (ZID,ID), (DUM,NDUM), (NDATA,NDATA1)

INPT0210

DIMENSION NID(10,50), ID(10,10)

INPT0220

INPT0230

1 READ (NIN,901)(TITLE(I),I=1,12)

INPT0240

901 FORMAT (12A6)

INPT0250

NPROB=NPROB+1

INPT0260

NCT=0

INPT0270

IF (NPROB.EQ.1) GO TO 3

INPT0280

REWIND NDATA1

INPT0290

DO 2 J=1,3

INPT0300

2 READ (NDATA1) DUMMY

INPT0310

IF (GEOM.GE.5.0) NCT=1

INPT0320

3 READ (NIN,902) EST,EEND,GEOM,ELEMS,PRINT,PLOTTZ

INPT0330

INDEX=PRINT+.1

INPT0340

NPLOT=PLOTTZ+.1

INPT0350

IF (NPLOT.GT.0) NPLOT=10

INPT0360

902 FORMAT (6E12.6)

INPT0370

MAT=ELEMS+.1

INPT0380

1GEOM=GEOM+.1

INPT0390

NERR=1

INPT0400

IF (MAT.GT.10.DR.MAT.LT.1) GO TO 420

INPT0410

READ (NIN,902) (ELBAR(L),L=1,2),CC,ZXSCRC

INPT0420

NHYD=ZXSCRC+.1

INPT0430

V(1)=1.0

INPT0440

V(2)=ELBAR(2)/ELBAR(1)

INPT0450

R=V(2)

INPT0460

READ (NIN,902) ENBG

INPT0470

NBG=ENBG+.1

INPT0480

NERR=NERR+1

INPT0490

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      IF (NBG.LE.0) GO TO 14
      IF (NBG.GT.50) GO TO 420
      READ (NIN,902)((BEG(I),I=1,NBG)
      GO TO 15
14    BEG(1)=0.0
15    CONTINUE
      READ (NIN,903)((ZID(N,K),N=1,2),(DENS(K,NT),NT=1,2),TT2(K),
1    K=1,MAT)
903   FORMAT (2A6,3E12.6)
      PL=0.0
      DO 4 K=1,MAT
4     PL=PL+TT2(K)
      NPL=PL+.1
      IF (NPL.GT.0) NPLOT=NPLOT+1
      NERR=NERR+1
      J=1
      NSP=1
      DO 150 K=1,MAT
      CALL TIDCO(ZID(1,K))
110   IF (NID(3,J)-ID(3,K)) 120,130,420
120   J=J+1
      NSP=NSP+1
      IF (J.GT.NEL) GO TO 420
      GO TO 110
130   MORDER(K)=NSP
      DO 140 I=4,10
      ZID(I,K)=TID(I,J)
140   CONTINUE
      DO 145 I=1,5
145   TNAME(I,K)=CNAME(I,J)
      J=J+1
      NSP=1
      ALPHA(K)=((ZID(4,K)-1.0)/(ZID(4,K)+1.0))**2
      DO 150 NT=1,2
      DENSITY(K,NT)=DENS(K,NT)/(1.0-ALPHA(K))
150   CONTINUE
      NPAGE=NPAGE+1
      WRITE (NOUT,611) NPROB,(TITLE(I),I=1,12),NPAGE
611   FORMAT (15H1GAROL PROBLEM I4,1H,3X 12A6,27X 4HPAGE I6)
      IF (IGECM.GT.4) GO TO 175
      IF (IGECM.GE.3) GO TO 160
      IF (IGECM.GT.1) GO TO 155
      CALL BOOLER(6HNONE ,A1)
      GO TO 170
155   CALL BOOLER(6HSLAB ,A1)
      GO TO 170
160   IF (IGECM.GT.3) GO TO 165
      CALL BOOLER(6HCYLIN.,A1)
      GO TO 170
165   CALL BOOLER(6HSPHERE,A1)

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INPT0500
INPT0510
INPT0520
INPT0530
INPT0540
INPT0550
INPT0560
INPT0570
INPT0580
INPT0590
INPT0600
INPT0610
INPT0620
INPT0630
INPT0640
INPT0650
INPT0660
INPT0670
INPT0680
INPT0690
INPT0700
INPT0710
INPT0720
INPT0730
INPT0740
INPT0750
INPT0760
INPT0770
INPT0780
INPT0790
INPT0800
INPT0810
INPT0820
INPT0830
INPT0840
INPT0850
INPT0860
INPT0870
INPT0880
INPT0890
INPT0900
INPT0910
INPT0920
INPT0930
INPT0940
INPT0950
INPT0960
INPT0970
INPT0980
INPT0990

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170 WRITE (NOUT,612) A1	INPT1000
612 FORMAT (14HOGOMETRY = A6)	INPT1010
175 WRITE (NOUT,6121) ELBAR(1),ELBAR(2),CC	INPT1020
6121 FORMAT {36HOMEAN CHORD LENGTH OF REGION 1 = 1PE14.6/	INPT1030
1 1H0 21X 14HREGION 2 = 1PE14.6/	INPT1040
2 24HODANCOFF CORRECTION = 1PE14.6)	INPT1050
IF (NHVD.EQ.1) WRITE (NOUT,701)	INPT1060
701 FORMAT (108HOEXTRA SOURCE TERMS WILL BE READ FROM INPUT CARD	INPT1070
1S, INTERPOLATED WHERE NEEDED, AND ADDED TO COMPUTED SOURCES.)	INPT1080
IF (NPLT.GT.0) WRITE (NOUT,702)	INPT1090
702 FORMAT (61HOPLOTTING OF THE RESULTS OF THIS PROBLEM HAS BEEN	INPT1100
1 REQUESTED.)	INPT1110
IF (EST.LE.0.0) GO TO 210	INPT1120
WRITE (NOUT,613) EST	INPT1130
613 FORMAT (24HOUPPER ENERGY LIMIT = 1PE14.6,4H EV)	INPT1140
GO TO 220	INPT1150
210 WRITE (NOUT,211)	INPT1160
211 FORMAT (62HOUPPER ENERGY LIMIT WILL BE THE FIRST ENERGY ON T	INPT1170
1HE DATA TAPE.)	INPT1180
220 IF (EEND.LE.0.0) GO TO 230	INPT1190
WRITE (NOUT,221) EEND	INPT1200
221 FORMAT (24HOWER ENERGY LIMIT = 1PE14.6,4H EV)	INPT1210
GO TO 240	INPT1220
230 WRITE (NOUT,231)	INPT1230
231 FORMAT (61HOWER ENERGY LIMIT WILL BE THE LAST ENERGY ON TH	INPT1240
1E DATA TAPE.)	INPT1250
240 IF (NBG.GT.0) GO TO 250	INPT1260
WRITE (NOUT,245)	INPT1270
245 FORMAT (60HOBROAD GROUP AVERAGED CROSS SECTIONS WILL NOT BE	INPT1280
1CALCULATED.)	INPT1290
GO TO 260	INPT1300
250 J=1	INPT1310
IF (NBG.GT.1) GO TO 255	INPT1320
WRITE (NOUT,615) NBG,J,EST,BEG(1)	INPT1330
GO TO 260	INPT1340
255 CONTINUE	INPT1350
WRITE (6,615) NBG,J,EST,BEG(1),(I,BEG(I-1),BEG(I),I=2,NBG)	INPT1360
615 FORMAT (26HONUMBER OF BROAD GROUPS = I4/1H0 7X 27HBROAD GROU	INPT1370
1P BOUNDARIES (EV)/(I6,1PE14.6,4H TO 1PE14.6))	INPT1380
260 CONTINUE	INPT1390
WRITE (NOUT,614) MAT,(K,ZID(1,K),ZID(2,K),(TNAME(I,K),I=1,5),	INPT1400
1 DENS(K,1),DENS(K,2),K=1,MAT)	INPT1410
614 FORMAT{1H0 22HNUMBER OF MATERIALS = I4/1H0 1X13HMATERIAL I.D.	INPT1420
1 5X 11HDESCRIPTION 27X 13HD E N S I T Y /55X 9HREGION 1 6X 9HREGI	INPT1430
2ON 2/(I3,2X,2A6,2X,5A6,1P2E15.6))	INPT1440
IF (IGOM.LE.4) GO TO 180	INPT1450
IF (IGOM.GE.6) GO TO 185	INPT1460
READ (NIN,902) CS1,CS2,CS3	INPT1470
READ (NIN,902)(CYLT(I),I=2,305)	INPT1480
CYLT(1)= 0.0	INPT1490

NPAGE=NPAGE+1	INPT1500
WRITE (NOUT,611) NPROB,(TITLE(I),I=1,12),NPAGE	INPT1510
WRITE (NOUT,616)	INPT1520
616 FORMAT(47HOSPECIAL ESCAPE PROBABILITY TABLES WILL BE USED /)	INPT1530
DO 176 I=1,50	INPT1540
I2=I+50	INPT1550
I3=I2+50	INPT1560
I4=I3+50	INPT1570
I5=I4+50	INPT1580
I6=I5+50	INPT1590
WRITE (NOUT,617) I,CYLT(I),I2,CYLT(I2),I3,CYLT(I3),I4,CYLT(I4),I5,	INPT1600
1CYLT(I5),I6,CYLT(I6)	INPT1610
617 FORMAT (I5,F10.5,5(I6,F10.5))	INPT1620
176 CONTINUE	INPT1630
I=301	INPT1640
I2=302	INPT1650
WRITE (NOUT,618) I,CYLT(I),CS1,CS2,CS3,I2,CYLT(I2)	INPT1660
618 FORMAT (79X,I6,F10.5/22H COEFFICIENTS-- CS1 = E12.6,3X 5HCS2 =	INPT1670
1E12.6,3X 5HCS3 =E12.6,5X,I6,F10.5)	INPT1680
IF (NPROB.GT.1) GO TO 190	INPT1690
GO TO 200	INPT1700
180 IF (NPROB.LE.1) GO TO 200	INPT1710
IF (NCT.LE.0) GO TO 190	INPT1720
READ (NDATA1)(SLABT(I),I=1,505),(CYLT(J),J=1,305)	INPT1730
CS1=0.5	INPT1740
CS2=0.0	INPT1750
CS3=-0.09375	INPT1760
GO TO 200	INPT1770
185 WRITE (NOUT,186)	INPT1780
186 FORMAT (71HOSPECIAL ESCAPE PROBABILITY TABLES FROM PRECEDING PROBL	INPT1790
1EM WILL BE USED.)	INPT1800
190 READ (NDATA1) DUMMY	INPT1810
200 RETURN	INPT1820
420 CALL ERRORS(4,NERR)	INPT1830
END	INPT1840

41BFTC	XSORC	LIST,DECK,REF	08-09-65	XSOR0000
	SUBROUTINE	XSORC(N,E,XS)		XSOR0010
C				XSOR0020
C		READ AND INTERPOLATE BACKGROUND SOURCE FROM INPUT CARDS		XSOR0030
	DIMENSION	XS(2)		XSOR0040
	NIN=5			XSOR0050
	GO TO	(10,20,30),N		XSOR0060
10	READ	(NIN,500) SORCES		XSOR0070
500	FORMAT	(6E12.6)		XSOR0080
	KPTS=	SORCES+.1		XSOR0090
	READ	(NIN,500) E1,SA1,SB1		XSOR0100
	READ	(NIN,500) E2,SA2,SB2		XSOR0110
	JPTS=	2		XSOR0120
	GO TO	40		XSOR0130
15	READ	(NIN,500) E2,SA2,SB2		XSOR0140
	JPTS=	JPTS+1		XSOR0150
20	IF	(E2.GT.E) GO TO 22		XSOR0160
	IF	(ABS(E1-E).LE.1.0E-5*E1) GO TO 24		XSOR0170
21	IF	(E1.GT.F) GO TO 23		XSOR0180
	GO TO	24		XSOR0190
22	EJ=	E2		XSOR0200
	SA1=	SA2		XSOR0210
	SB1=	SB2		XSOR0220
	IF	(JPTS.LT.KPTS) GO TO 15		XSOR0230
	GO TO	24		XSOR0240
23	ERATIO=	(E-E2)/(E1-E2)		XSOR0250
	XS(1)=	SA2+ERATIO*(SA1-SA2)		XSOR0260
	XS(2)=	SB2+ERATIO*(SB1-SB2)		XSOR0270
	GO TO	40		XSOR0280
24	XS(1)=	SA1		XSOR0290
	XS(2)=	SB1		XSOR0300
	GO TO	40		XSOR0310
30	IF	(JPTS.GE.KPTS) GO TO 40		XSOR0320
	J1=	JPTS+1		XSOR0330
	DO	31 J=J1,KPTS		XSOR0340
31	READ	(NIN,500) DA		XSOR0350
40	RETURN			XSOR0360
	END			XSOR0370

-\$IBFTC	PROB	LIST,DECK,REF	08-09-65	PROB0000
	SUBROUTINE	PROB(ARG,IGEOM,PZERO)		PROB0010
C				PROB0020
C		COMPUTE ESCAPE PROBABILITIES FOR REGION 1		PROB0030
C		ADAPTED FOR GAROL FROM THE ZUT PROGRAM (GA-2525)		PROB0040
C		THE CONSTANT 0.577216 DEFINES EULERS NUMBER		PROB0050
C				PROB0060
C	COMMON	/TABLES/ CS1,CS2,CS3,SLABT(505),CYLT(305)		PROB0070
C				PROB0080
C	GO TO	(940,720,620,820,640,640,640), IGEOM		PROB0090
C				PROB0100
C		CYLINDRICAL GEOMETRY		PROB0110
	620 IF	(ARG-0.1) 660,680,640		PROB0120
	640 IF	(ARG-6.0) 680,680,700		PROB0130
C		/ARG LESS THAN 0.1/		PROB0140
	660	PZERO=1.0-1.3333333*ARG+0.5*(-ALOG(ARG)+1.3659312)*ARG*ARG		PROB0150
		GO TO 920		PROB0160
C		/ARG GREATER THAN OR EQUAL TO 0.1, LESS THAN OR EQUAL TO 6.0/		PROB0170
	680	CALL NEWCYL(ARG,PC)		PROB0180
		PZERO=1.0-PC		PROB0190
		GO TO 920		PROB0200
C		/ARG GREATER THAN 6.0/		PROB0210
	700	PZERO=(CS1+CS2/ARG+CS3/(ARG*ARG))/ARG		PROB0220
		GO TO 920		PROB0230
C				PROB0240
C		SLAB GEOMETRY		PROB0250
	720 IF	(ARG-0.05) 760,780,740		PROB0260
	740 IF	(ARG-5.0) 780,780,800		PROB0270
C		/ARG LESS THAN 0.05/		PROB0280
	760	PZERO=1.0+ARG*(+ALOG(ARG)-0.66666667*ARG-0.2296368)		PROB0290
		GO TO 920		PROB0300
C		/ARG GREATER THAN OR EQUAL TO 0.05, LESS THAN OR EQUAL TO 5.0/		PROB0310
	780	CALL NEWSLB(ARG,PC)		PROB0320
		PZERO=1.0-PC		PROB0330
		GO TO 920		PROB0340
C		/ARG GREATER THAN 5.0/		PROB0350
	800	PZERO=0.25/ARG		PROB0360
		GO TO 920		PROB0370
C				PROB0380
C		SPHERICAL GEOMETRY		PROB0390
	820 IF	(ARG-0.02) 860,860,840		PROB0400
	840 IF	(ARG-5.0) 880,900,900		PROB0410
C		/ARG LESS THAN OR EQUAL TO 0.02/		PROB0420
	860	PZERO=1.0-0.75*ARG		PROB0430
		GO TO 920		PROB0440
C		/ARG GREATER THAN 0.02, LESS THAN 5.0/		PROB0450
	880	PZERO=3.0*((2.0*ARG)*ARG-1.0+(1.0+(2.0*ARG))*EXP(-(2.0*ARG)))		PROB0460
	1	/(2.0*ARG)**3		PROB0470
		GO TO 920		PROB0480

C /ARG GREATER THAN OR EQUAL TO 5.0/
 900 PZERO=3.0*{(2.0*ARG)*ARG-1.0)/(2.0*ARG)**3
 C
 920 RETURN
 C
 C NO GEOMETRY
 940 PZERO=0.0
 GO TO 920
 END

PROB0490
 PROB0500
 PROB0510
 PROB0520
 PROB0530
 PROB0540
 PROB0550
 PROB0560
 PROB0570

\$IBFTC HEAD	LIST,DECK,REF	08-09-65	HEAD0000
	SUBROUTINE HEAD		HEAD0010
	COMMON /ALL/ NIN,NOUT,NDATA,NIN1,NIN3,JHYD,NEL,NARRAY,NPAGE,LINES		HEAD0020
	1,NPROB,NPTS,INDEX,NPLOT,TITLE(12),TID(10,20),CNAME(5,20),LINEPP		HEAD0030
	2 ,MAT		HEAD0040
C	PAGE HEADING ROUTINE		HEAD0050
	NPAGE=NPAGE+1		HEAD0060
	WRITE (NOUT,601) NPROB,(TITLE(I),I=1,12),NPAGE		HEAD0070
601	FORMAT (15H1GAROL PROBLEM I4,1H,3X 12A6, 27X 4HPAGE I6/		HEAD0080
	1 6HOPPOINT 4X 9HENERGY-EV 8X 4HFLUX 10X 4HFLUX 8X 6HSOURCE 8X		HEAD0090
	2 6HSOURCE 9X 19HTOTAL CROSS SECTION 9X 18HCOLLISION DENSITY/		HEAD0100
	3 24X 9HREGION 1 5X 9HREGION 2 5X 9HREGION 1 5X 9HREGION 2 5X		HEAD0110
	4 9HREGION 1 5X 9HREGION 2 5X 9HREGION 1 5X 9HREGION 2/)		HEAD0120
	LINES=1		HEAD0130
	RETURN		HEAD0140
	END		HEAD0150

\$IBFTC NEWCYL	LIST,DECK,REF	08-09-65	NEWC0000
	SUBROUTINE NEWCYL(ARG,FARG)		NEWC0010
C	ADAPTED FOR GAROL FROM THE ZUT PROGRAM (GA-2525)		NEWC0020
	COMMON /TABLES/ CS1,CS2,CS3,SLABT(505),CYLT(305)		NEWC0030
	DEL=0.02		NEWC0040
	RINK=ARG/DEL		NEWC0050
	IN=RINK		NEWC0060
	FIN=IN		NEWC0070
	RINK=RINK-FIN		NEWC0080
	FARG=CYLT(IN+1)+RINK*(CYLT(IN+2)-CYLT(IN+1))-RINK*(RINK-1.0)/4.0		NEWC0090
	1*(CYLT(IN+2)+CYLT(IN+1)-CYLT(IN)-CYLT(IN+3))		NEWC0100
220	RETURN		NEWC0110
	END		NEWC0120

\$IBFTC NEWSLB	LIST,DECK,REF	08-09-65	NEWS0000
	SUBROUTINE NEWSLB(ARG,FARG)		NEWS0010
C			NEWS0020
C	ADAPTED FOR GAROL FROM THE ZUT PROGRAM (GA-2525)		NEWS0030
	COMMON /TABLES/ CS1,CS2,CS3,SLABT(505),CYLT(305)		NEWS0040
	DEL=0.01		NEWS0050
	RINK=ARG/DEL		NEWS0060
	IN=RINK		NEWS0070
	FIN=IN		NEWS0080
	RINK=RINK-FIN		NEWS0090
	FARG=SLABT(IN+1)+RINK*(SLABT(IN+2)-SLABT(IN+1))-RINK*(RINK-1.0)/4.		NEWS0100
	10*(SLABT(IN+2)+SLABT(IN+1)-SLABT(IN)-SLABT(IN+3))		NEWS0110
220	RETURN		NEWS0120
	END		NEWS0130

* * * * *

G A R D L L I N K 5

* * * * *

\$IBMAP	COMSET	LIST,REF	08-09-65	5COM0000
B	BOOL	7022		5COM0010
BSET	CONTRL	A,C		5COM0020
A	BSS	B		5COM0030
C	EQU	*		5COM0040
	END			5COM0050

\$IBFTC	LINK5	LIST,REF	08-09-65	5LNK0000
	COMMON /ALL/	NIN,NOUT,NDATA,NIN1,NIN3,JHYD,NEL,NARRAY,NPAGE,LINES		5LNK0010
	1,NPROB,NPTS,INDEX,NPLOT,TITLE(12),TID(10,20),CNAME(5,20),LINEPP			5LNK0020
	2 ,MAT,MFRAME			5LNK0030
	CALL AVRG			5LNK0040
	IF (NPLOT.LE.0) CALL CHAIN (4)			5LNK0050
C		TRANSFER TO PLOT ROUTINES (LINK 6)		5LNK0060
	CALL CHAIN (6)			5LNK0070
	END			5LNK0080

\$IBFTC AVRG LIST,DECK,REF
 SUBROUTINE AVRG

08-09-65AVRG0000

C		AVRG0010
C		AVRG0020
C		AVRG0030
C	COMPLETE BROAD GROUP AVERAGES, COMPUTE CELL AND ONE-GROUP	AVRG0040
C	AVERAGES, AND PRINT RESULTS	AVRG0050
		AVRG0060
	COMMON /ALL/ NIN,NOUT,NDATA,NINI,NIN3,JHYD,NEL,NARRAY,NPAGE,LINES	AVRG0070
	1,NPROB,NPTS,INDEX,NPLOT,TITLE(12),TID(10,20),CNAME(5,20),LINEPP	AVRG0080
	2 ,MAT,MFRAME	AVRG0090
	COMMON /TABLES/ CS1,CS2,CS3,SLABT(505),CYLT(305)	AVRG0100
	COMMON /BSET/ V(2), R, IGEOM, EC, EST, EEND, NHYD, HYD(2)	AVRG0110
	1 , E, DE1, DE2, DE3, DE4, SUM(2), SUMA, SUMB, T(2), S(2)	AVRG0120
	2 , TERM, CC, MORDER(10), ELBAR(2)	AVRG0130
	3 , ZID(10,10), CAP(10), SCAT(10), FIS(10), LIM(10), DENS(10,2)	AVRG0140
	4 , DENSTY(10,2), ALPHA(10), TOTAL(2), P(2), D(2), Q(2), DDQQ	AVRG0150
	5 , PHI(2), SORC(2)	AVRG0160
	6 , NBG, BEG(50), BPHI(50,2), BCAP(50,10,2), BSCAT(50,10,2)	AVRG0170
	7 , BFIS(50,10,2), CELLS(50), CELLC(50), CELLF(50), OGPFI(2)	AVRG0180
	8 , OGSCAT(3), OGCAP(3), OGFIS(3)	AVRG0190
	9 ,TNAME(5,10)	AVRG0200
	COMMON /PLOTT/ TLABEL(12),XLABEL(12),YLABEL(12),TT2(12),NFRAME	AVRG0210
	EQUIVALENCE (TID,NID), (ZID,ID)	AVRG0220
	DIMENSION NID(10,50), ID(10,10)	AVRG0230
	DIMENSION CPHI(50)	AVRG0240
	NPAGE=NPAGE+1	AVRG0250
	VA=V(1)	AVRG0260
	VB=V(2)	AVRG0270
	WRITE (6,601) NPROB,(TITLE(I),I=1,12),NPAGE	AVRG0280
601	FORMAT (15H1GAROL PROBLEM 14,1H, 3X 12A6,27X 4HPAGE 16)	AVRG0290
	DO 300 NT=1,2	AVRG0300
	OGPFI(NT)=0.0	AVRG0310
	DO 300 N=1,NBG	AVRG0320
	OGPFI(NT)=OGPFI(NT)+BPHI(N,NT)	AVRG0330
300	CONTINUE	AVRG0340
	AK=1.0/(VA+VB)	AVRG0350
	OGPFI3=0.0	AVRG0360
	DO 301 N=1,NBG	AVRG0370
	CPHI(N)=(BPHI(N,1)*VA+BPHI(N,2)*VB)*AK	AVRG0380
	OGPFI3=OGPFI3+CPHI(N)	AVRG0390
301	CONTINUE	AVRG0400
	WRITE (6,602)	AVRG0410
602	FORMAT (13HOGROUP FLUXES/6HOGROUP 3X 9HENERGY-EV 5X 9HREGION 1	AVRG0420
	1 5X 9HREGION 2 4X 12HCELL AVERAGE/8X 11HLOWER LIMIT/)	AVRG0430
	WRITE (6,603)(I,BEG(I),BPHI(I,1),BPHI(I,2),CPHI(I),I=1,NBG)	AVRG0440
603	FORMAT (14,1X,1P4E14.6)	AVRG0450
	WRITE (6,604)(OGPFI(I),I=1,2),OGPFI3	AVRG0460
604	FORMAT (15HOONE GROUP FLUX 1PE18.6,2E14.6)	AVRG0470
	DO 400 K=1,MAT	AVRG0480
	NPAGE=NPAGE+1	AVRG0490

WRITE (6,601) NPROB,(TITLE(I),I=1,12),NPAGE	AVRG0500
RR=DENS(K,2)*R	AVRG0510
TERM=(1.0+R)/(DENS(K,1)+RR)	AVRG0520
DO 305 NT=1,3	AVRG0530
OGSCAT(NT)=0.0	AVRG0540
OGCAP(NT)=0.0	AVRG0550
OGFIS(NT)=0.0	AVRG0560
305 CONTINUE	AVRG0570
DO 310 N=1,NBG	AVRG0580
BBR=1.0/(BPHI(N,1)+BPHI(N,2)*R)	AVRG0590
CELLS(N)=(DENS(K,1)*BSCAT(N,K,1)+RR*BSCAT(N,K,2))*TERM*BBR	AVRG0600
CELLC(N)=(DENS(K,1)*BCAP(N,K,1)+RR*BCAP(N,K,2))*TERM*BBR	AVRG0610
DO 310 NT=1,2	AVRG0620
OGSCAT(NT)=OGSCAT(NT)+BSCAT(N,K,NT)	AVRG0630
OGCAP(NT)=OGCAP(NT)+BCAP(N,K,NT)	AVRG0640
BSCAT(N,K,NT)=BSCAT(N,K,NT)/BPHI(N,NT)	AVRG0650
BCAP(N,K,NT)=BCAP(N,K,NT)/BPHI(N,NT)	AVRG0660
310 CONTINUE	AVRG0670
BBR=1.0/(OGPHI(1)+OGPHI(2)*R)	AVRG0680
OGSCAT(3)=(DENS(K,1)*OGSCAT(1)+RR*OGSCAT(2))*TERM*BBR	AVRG0690
OGCAP(3)=(DENS(K,1)*OGCAP(1)+RR*OGCAP(2))*TERM*BBR	AVRG0700
DO 315 NT=1,2	AVRG0710
OGCAP(NT)=OGCAP(NT)/OGPHI(NT)	AVRG0720
OGSCAT(NT)=OGSCAT(NT)/OGPHI(NT)	AVRG0730
315 CONTINUE	AVRG0740
IF (ZID(7,K).GE.0.0) GO TO 350	AVRG0750
IF (ZID(7,K).EQ.-1.0) GO TO 319	AVRG0760
DO 316 NT=1,2	AVRG0770
DO 316 N=1,NBG	AVRG0780
IF (BFIS(N,K,NT).NE.0.0) GO TO 319	AVRG0790
316 CONTINUE	AVRG0800
GO TO 350	AVRG0810
319 DO 320 N=1,NBG	AVRG0820
BBR=1.0/(BPHI(N,1)+BPHI(N,2)*R)	AVRG0830
CELLF(N)=(DENS(K,1)*BFIS(N,K,1)+RR*BFIS(N,K,2))*TERM*BBR	AVRG0840
DO 320 NT=1,2	AVRG0850
OGFIS(NT)=OGFIS(NT)+BFIS(N,K,NT)	AVRG0860
BFIS(N,K,NT)=BFIS(N,K,NT)/BPHI(N,NT)	AVRG0870
320 CONTINUE	AVRG0880
BBR=1.0/(OGPHI(1)+OGPHI(2)*R)	AVRG0890
OGFIS(3)=(DENS(K,1)*OGFIS(1)+RR*OGFIS(2))*TERM*BBR	AVRG0900
DO 325 NT=1,2	AVRG0910
OGFIS(NT)=OGFIS(NT)/OGPHI(NT)	AVRG0920
325 CONTINUE	AVRG0930
WRITE (NOUT,701) K,ZID(1,K),ZID(2,K),(TNAME(JKL,K),JKL=1,5)	AVRG0940
701 FORMAT (36HOBROAD GROUP AVERAGED CROSS SECTIONS /10HOMATERIAL 12,	AVRG0950
1 2X,2A6,5X,5A6)	AVRG0960
WRITE (NOUT,702)	AVRG0970

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702 FORMAT (6H0GROUP 3X 9HENERGY-EV 18X 22HR E G I O N 1 34X AVR0980
1 22HR E G I O N 2 /8X 11HLOWER LIMIT 5X 7HCAPTURE 7X AVR0990
2 7HSCATTER 7X 7HFISSION 8X 5HALPHA 8X 7HCAPTURE 7X 7HSCATTER 7X AVR1000
3 7HFISSION 8X 5HALPHA /) AVR1010
DO 330 N=1,NBG AVR1020
A1=BCAP(N,K,1)/BFIS(N,K,1) AVR1030
A2=BCAP(N,K,2)/BFIS(N,K,2) AVR1040
WRITE (NOUT,703) N,BEG(N),BCAP(N,K,1),BSCAT(N,K,1),BFIS(N,K,1),A1, AVR1050
1 BCAP(N,K,2),BSCAT(N,K,2),BFIS(N,K,2),A2 AVR1060
703 FORMAT (I4,1X,1P9E14.6) AVR1070
330 CONTINUE AVR1080
A1=OGCAP(1)/OGFIS(1) AVR1090
A2=OGCAP(2)/OGFIS(2) AVR1100
WRITE (NOUT,704) OGCAP(1),OGSCAT(1),OGFIS(1),A1,OGCAP(2),OGSCAT(2) AVR1110
1 ,OGFIS(2),A2 AVR1120
704 FORMAT (19H0ONE GROUP AVERAGE 1P8E14.6) AVR1130
WRITE (NOUT,705) AVR1140
705 FORMAT (6H0GROUP 3X 9HENERGY-EV 18X 25HC E L L A V E R A G E/ AVR1150
1 8X 11HLOWER LIMIT 5X 7HCAPTURE 7X 7HSCATTER 7X 7HFISSION 8X AVR1160
2 5HALPHA/ ) AVR1170
DO 340 N=1,NBG AVR1180
A1=CELLC(N)/CELLF(N) AVR1190
WRITE (NOUT,703) N,BEG(N),CELLC(N),CELLS(N),CELLF(N),A1 AVR1200
340 CONTINUE AVR1210
A1=OGCAP(3)/OGFIS(3) AVR1220
WRITE (NOUT,704) OGCAP(3),OGSCAT(3),OGFIS(3),A1 AVR1230
GO TO 400 AVR1240
350 CONTINUE AVR1250
WRITE (NOUT,701) K,ZID(1,K),ZID(2,K),(TNAME(JKL,K),JKL=1,5) AVR1260
WRITE (NOUT,706) AVR1270
706 FORMAT (6H0GROUP 3X 9HENERGY-EV 9X 15HR E G I O N 1 13X 15HR E G AVR1280
1 I O N 2 14X 13HCELL AVERAGE /8X 11HLOWER LIMIT 5X 7HCAPTURE 7X AVR1290
2 7HSCATTER 7X 7HCAPTURE 7X 7HSCATTER 7X 7HCAPTURE 7X 7HSCATTER /) AVR1300
DO 360 N=1,NBG AVR1310
WRITE (NOUT,703) N,BEG(N),(BCAP(N,K,NT),BSCAT(N,K,NT),NT=1,2), AVR1320
1 CELLC(N),CELLS(N) AVR1330
360 CONTINUE AVR1340
WRITE (NOUT,704) (OGCAP(NT),OGSCAT(NT),NT=1,3) AVR1350
400 CONTINUE AVR1360
RETURN AVR1370
END AVR1380

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* * * * *
 G A R O L L I N K 6
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\$IBMAP	COMSET	LIST,REF	08-09-656	COM0000
BSET	CONTRL	A,C		6COM0010
A	BSS	18050		6COM0020
C	EQU	*		6COM0030
	END			6COM0040

\$IBFTC	LINK6	LIST,REF	08-09-656	LNK0000
		LINK 6		6LNK0010
		PLGT ROUTINES		6LNK0020
				6LNK0030
		COMMON /ALL/ NIN,NCUT,NDATA,NIN1,NIN3,JHYD,NEL,NARRAY,NPAGE,LINES		6LNK0040
		1,NPROB,NPTS,INDEX,NPLOT,TITLE(12),TID(10,20),CNAME(5,20),LINEPP		6LNK0050
		2 ,MAT,MFRAME		6LNK0060
		COMMON /PLOT/ TLABEL(12),XLABEL(12),YLABEL(12), T2(12),NFRAME		6LNK0070
		COMMON /BSET/ TNAME(5,10),E(1000),CAP(1000,8),FIS(1000,8)		6LNK0080
		EQUIVALENCE (PHI(1),CAP(1,1)),(TOTAL(1),CAP(1,2)),(CD(1),CAP(1,3))		6LNK0090
		DIMENSION PHI(1000),TOTAL(1000),CD(1000)		6LNK0100
		DIMENSION KPLT(10)		6LNK0110
				6LNK0120
		REWIND NIN1		6LNK0130
		NTWO=2		6LNK0140
		DO 5 K=1,MAT		6LNK0150
		5 KPLT(K)=T2(K)+.1		6LNK0160
		READ (NIN3)((TNAME(I,K),I=1,5),K=1,MAT)		6LNK0170
		CALL TPLUT(1,N,N,N,D,D,D)		6LNK0180
		CALL BCCLER(6H ,BLANK)		6LNK0190
		NXSCL=2		6LNK0200
		NYSCL=1		6LNK0210
		MPTS=NPTS		6LNK0220
		KMAT=MINO(MAT,8)		6LNK0230
		10 JEND=MPTS		6LNK0240
		IF (JEND.GT.1000) JEND=1000		6LNK0250
		DO 30 J=1,12		6LNK0260
		TLABEL(J)=TITLE(J)		6LNK0270
		T2(J)=BLANK		6LNK0280
		XLABEL(J)=BLANK		6LNK0290
		YLABEL(J)=BLANK		6LNK0300
		30 CONTINUE		6LNK0310
		CALL BCCLER(6HENERGY,XLABEL(6))		6LNK0320
		CALL BCCLER(6H -- EV,XLABEL(7))		6LNK0330
		IF (NPLOT.EQ.1)GO TO 49		6LNK0340
		DO 20 I=1,JEND		6LNK0350
		READ (NIN3) E(I),PHI(I),TOTAL(I)		6LNK0360
		CD(I)=E(I)*PHI(I)*TOTAL(I)		6LNK0370
		20 CONTINUE		6LNK0380

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CALL BCCLER(6H FLUX,YLABEL(5))
CALL BCCLER(6H IN ,YLABEL(7))
CALL BCCLER(6H REGION,YLABEL(9))
CALL BCCLER(6H 1 ,YLABEL(10))
CALL TPLOT(2,NXSCL,NTWO,JEND,E,PHI,PHI)
CALL BCCLER(6H TOTAL ,YLABEL(1))
CALL BCCLER(6H CROSS-,YLABEL(3))
CALL BCCLER(6H SECTIO,YLABEL(5))
CALL BCCLER(6H HN ,YLABEL(6))
CALL TPLOT(2,NXSCL,NTWO,JEND,E,TOTAL,PHI)
CALL BCCLER(6H COLLIS,YLABEL(3))
CALL BCCLER(6H ION ,YLABEL(4))
CALL BCCLER(6H DENSIT,YLABEL(5))
CALL BCCLER(6H Y ,YLABEL(6))
YLABEL(1)=BLANK
CALL TPLOT(2,NXSCL,NYSCL,JEND,E,CD,PHI)
DO 40 J=1,12
YLABEL(J)=BLANK
40 CONTINUE
IF (NPLCT-10.LE.0) GO TO 70
49 DO 50 I=1,JEND
50 READ (NIN1)(CAP(I,K),FIS(I,K),K=1,KMAT)
CALL BCCLER(6H CAPTUR,YLABEL(5))
CALL BCCLER(6H E ,YLABEL(6))
CALL BCCLER(6H RATE,YLABEL(7))
DO 100 K=1,KMAT
IF (KPLCT(K).LE.0) GO TO 100
DO 60 J=1,5
60 T2(J)=TNAME(J,K)
CALL TPLOT(2,NXSCL,NYSCL,JEND,E,CAP(1,K),PHI)
IF (TID(7,K).GE.0.0) GO TO 100
CALL BCCLER(6H FISSIO,YLABEL(5))
CALL BCCLER(6H HN ,YLABEL(6))
CALL TPLOT(2,NXSCL,NYSCL,JEND,E,FIS(1,K),PHI)
CALL BCCLER(6H CAPTUR,YLABEL(5))
CALL BCCLER(6H E ,YLABEL(6))
100 CONTINUE
70 IF (JEND.GE.MPTS) GO TO 200
MPTS=MPTS-1000
GO TO 10
200 CALL END(1)
CALL BACK
MFRAME=NFRAME
PRINT 908,MFRAME
908 FORMAT (1H0 I6,26H FRAMES HAVE BEEN PLOTTED. )
CALL CHAIN(4)
END

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6LNK0390
6LNK0400
6LNK0410
6LNK0420
6LNK0430
6LNK0440
6LNK0450
6LNK0460
6LNK0470
6LNK0480
6LNK0490
6LNK0500
6LNK0510
6LNK0520
6LNK0530
6LNK0540
6LNK0550
6LNK0560
6LNK0570
6LNK0580
6LNK0590
6LNK0600
6LNK0610
6LNK0620
6LNK0630
6LNK0640
6LNK0650
6LNK0660
6LNK0670
6LNK0680
6LNK0690
6LNK0700
6LNK0710
6LNK0720
6LNK0730
6LNK0740
6LNK0750
6LNK0760
6LNK0770
6LNK0780
6LNK0790
6LNK0800
6LNK0810
6LNK0820
6LNK0830
6LNK0840
6LNK0850

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5IBFTC	TPLCT LIST,DECK,REF	08-10-65	TPL00000
	SUBROUTINE TPLCT(NNNN,NXSCL,NYSCL,NPT,XQX,YQY,Y)		TPL00010
			TPL00020
	ADAPTED FOR GARCL FROM THE TPLCT PROGRAM (GAMD-4346 REVISED)		TPL00030
			TPL00040
	COMMON /PLOTT/ TITLE(12),XLABEL(12),YLABEL(12),T2(12),MFRAME		TPL00050
	DIMENSION X(1000), Y(1000), A(682), CHR(3), HEAD(10)		TPL00060
	1,XQX(1000), YQY(1000)		TPL00070
	DIMENSION ZNAME(5)		TPL00080
	DIMENSION TYP(2)		TPL00090
			TPL00100
	GO TO (1000,2000),NNNN		TPL00110
1000	CF=0.43429448		TPL00120
	NTAPE=6		TPL00130
	IF (MFRAME.GT.1) NTAPE=-6		TPL00140
	CALL BOCLER (6HX-MAX=,BXMAX)		TPL00150
	CALL BOCLER (6HY-MAX=,BYMAX)		TPL00160
	CALL BOCLER (6HX-MIN=,BXMIN)		TPL00170
	CALL BOCLER (6HY-MIN=,BYMIN)		TPL00180
	CALL BOCLER (6H X,BXXX)		TPL00190
	CALL BOCLER (6H Y,BYYY)		TPL00200
	NCHRS=8		TPL00210
	INDEX=4		TPL00220
	INTENS=3		TPL00230
	AKAR=BXXX		TPL00240
	ICHAR=55		TPL00250
	CALL SETUP(A,682,NTAPE)		TPL00260
	CALL RST		TPL00270
	CALL SC1		TPL00280
	CALL HEADER		TPL00290
	IF (MFRAME.GT.1) GO TO 101		TPL00300
	MFRAME=1		TPL00310
	CALL BIGBEN(DATE,ZNAME)		TPL00320
	CALL BCDCON(HEAD)		TPL00330
	WRITE (0,205) DATE,{ZNAME(I),I=1,4)		TPL00340
205	FORMAT (23H GENERAL ATOMIC, TPLCT, A6,2H, 4A6)		TPL00350
	CALL FRAME(0.0,5.0,5.0,0.0)		TPL00360
	CALL TSP(1.0,2.5,HEAD(1),60)		TPL00370
	WRITE (6,902)(HEAD(I),I=1,10)		TPL00380
	WRITE (6,910)MFRAME		TPL00390
	CALL ADF		TPL00400
101	RETURN		TPL00410
			TPL00420
2000	CALL TICKER(TIME)		TPL00430
	TIME=TIME/216.0		TPL00440
	MFRAME=MFRAME+1		TPL00450
	NPTS=NPT		TPL00460
	DO 116 I=1,NPT		TPL00470
	X(I)=XQX(I)		TPL00480
	Y(I)=YQY(I)		TPL00490

116	CONTINUE	TPL00500
117	XMAXX=-1.E+35	TPL00510
	XMINN=1.E+35	TPL00520
	YMAXX=-1.E+35	TPL00530
	YMINN=1.E+35	TPL00540
	DO 118 IJ=1,NPTS	TPL00550
	XMAXX=AMAX1(XMAXX,X(IJ))	TPL00560
	XMINN=AMIN1(XMINN,X(IJ))	TPL00570
	YMAXX=AMAX1(YMAXX,Y(IJ))	TPL00580
	YMINN=AMIN1(YMINN,Y(IJ))	TPL00590
118	CONTINUE	TPL00600
	IF (XMAXX-XMINN) 120,120,121	TPL00610
120	WRITE (6,941)XMAXX	TPL00620
941	FORMAT(58HOND PLOTTING FOR THIS FRAME. X IS CONSTANT FOR ALL Y	TPL00630
	1AT 1PE12.6)	TPL00640
	GO TO 100	TPL00650
121	IF (YMAXX-YMINN) 122,122,130	TPL00660
122	WRITE (6,942)YMAXX	TPL00670
942	FORMAT (58HOND PLOTTING FOR THIS FRAME. Y IS CONSTANT FOR ALL X	TPL00680
	1AT 1PE12.6)	TPL00690
	GO TO 100	TPL00700
130	X1PR=XMAXX	TPL00710
	X2PR=XMINN	TPL00720
	Y1PR=YMAXX	TPL00730
	Y2PR=YMINN	TPL00740
132	GO TO (11,21),NXSCL	TPL00750
11	Z1=ABS(XMINN)	TPL00760
	Z2=ABS(XMAXX)	TPL00770
	Z=ALOG10(AMAX1(Z1,Z2))	TPL00780
	N=-Z	TPL00790
	IF (N) 15,13,14	TPL00800
13	IF (Z) 14,16,15	TPL00810
14	N=N+1	TPL00820
15	SCFX=10.0**N	TPL00830
	IF (XMAXX.LE.0.0) GO TO 1511	TPL00840
	LX2=XMAXX*SCFX+.999	TPL00850
	GO TO 1512	TPL00860
1511	LX2=XMAXX*SCFX	TPL00870
1512	X2=FLCAT(LX2)	TPL00880
	GO TO 17	TPL00890
16	SCFX=10.0**N	TPL00900
	X2=XMAXX*SCFX	TPL00910
	LX2=X2+.999	TPL00920
17	DO 18 J=1,NPT	TPL00930
18	X(J)=X(J)*SCFX	TPL00940
	IF (XMINN) 1811,1810,1812	TPL00950
1810	LXMIN=0	TPL00960
	XX=0.0	TPL00970
	GO TO 1813	TPL00980
1811	LXMIN=XMINN*SCFX-.999	TPL00990

XX=FLCAT(LXMIN)-.2E-6	TPL01000
GO TO 1813	TPL01010
1812 LXMIN=XMINN*SCFX	TPL01020
XX=FLCAT(LXMIN)+.2E-6	TPL01030
1813 X10=ABS(X2-XX)	TPL01040
X1=XX-0.1*X10	TPL01050
X1TYP=XX-0.08*X10	TPL01060
NDIST=LX2-LXMIN	TPL01070
IF (NDIST-5) 19,20,20	TPL01080
19 NX=NDIST*10+1	TPL01090
SX=0.1	TPL01100
GO TO 30	TPL01110
20 NX=NDIST*5+1	TPL01120
SX=0.2	TPL01130
GO TO 30	TPL01140
21 IF (XMINN) 210,210,212	TPL01150
210 WRITE (6,211)BXXX,BXXX	TPL01160
GO TO 101	TPL01170
212 DO 22 J=1,NPT	TPL01180
22 X(J)=ALOG10(X(J))	TPL01190
XMAXX=ALOG10(XMAXX)	TPL01200
XMINN=ALOG10(XMINN)	TPL01210
IF (XMINN)24,23,23	TPL01220
23 NX1=XMINN	TPL01230
GO TO 25	TPL01240
24 NX1=XMINN-1.0	TPL01250
IF (XMAXX) 26,25,25	TPL01260
25 NX2=XMAXX+1.0	TPL01270
GO TO 27	TPL01280
26 NX2=XMAXX	TPL01290
27 NXC=NX2-NX1	TPL01300
XX=FLCAT(NX1)	TPL01310
X2=FLCAT(NX2)	TPL01320
X10=X2-XX	TPL01330
X1=XX-0.1*X10	TPL01340
X1TYP=XX-0.08*X10	TPL01350
30 GO TO (31,41),NYSCL	TPL01360
31 Z1=ABS(YMINN)	TPL01370
Z2=ABS(YMAXX)	TPL01380
ZY=ALOG10(AMAX1(Z1,Z2))	TPL01390
NY=-ZY	TPL01400
IF (NY) 35,33,34	TPL01410
33 IF (ZY) 34,36,35	TPL01420
34 NY=NY+1	TPL01430
35 SCFY=10.0**NY	TPL01440
IF (YMAXX.LE.0.) GO TO 3511	TPL01450
LY1=YMAXX*SCFY+.999	TPL01460
GO TO 3512	TPL01470
3511 LY1=YMAXX*SCFY	TPL01480
3512 Y1=FLCAT(LY1)	TPL01490

GO TO 37	TPL01500
36 SCFY=10.0**NY	TPL01510
Y1=YMAXX*SCFY	TPL01520
LY1=Y1+.999	TPL01530
37 DO 38 J=1,NPT	TPL01540
38 Y(J)=Y(J)*SCFY	TPL01550
IF (YMINN) 381,380,382	TPL01560
380 LYMIN=0	TPL01570
YY=0.0	TPL01580
GO TO 383	TPL01590
381 LYMIN=YMINN*SCFY-.999	TPL01600
YY=FLCAT(LYMIN)-.2E-6	TPL01610
GO TO 383	TPL01620
382 LYMIN=YMINN*SCFY	TPL01630
YY=FLOAT(LYMIN) +.2E-06	TPL01640
383 Y10=ABS(Y1-YY)	TPL01650
Y22=YY-C.1*Y10	TPL01660
Y2TYP=YY-0.02*Y10	TPL01670
MDIST=LY1-LYMIN	TPL01680
IF (MDIST-5) 39,39,40	TPL01690
39 NY=MDIST*10+1	TPL01700
SY=0.1	TPL01710
GO TO 60	TPL01720
40 NY=MDIST*5+1	TPL01730
SY=0.2	TPL01740
GO TO 60	TPL01750
41 IF (YMINN) 410,410,412	TPL01760
410 WRITE (6,211)BYYY,BYYY	TPL01770
GO TO 101	TPL01780
412 DO 42 J=1,NPT	TPL01790
42 Y(J)=ALOG10(Y(J))	TPL01800
YMAXX=ALOG10(YMAXX)	TPL01810
YMINN=ALOG10(YMINN)	TPL01820
IF (YMINN) 44,43,43	TPL01830
43 NY2=YMINN	TPL01840
GO TO 45	TPL01850
44 NY2=YMINN-1.0	TPL01860
IF (YMAXX) 46,45,45	TPL01870
45 NY1=YMAXX+1.0	TPL01880
GO TO 47	TPL01890
46 NY1=YMAXX	TPL01900
47 NYC=NY1-NY2	TPL01910
Y1=FLOAT(NY1)	TPL01920
YY=FLCAT(NY2)	TPL01930
Y10=Y1-YY	TPL01940
Y22=YY-0.1*Y10	TPL01950
Y2TYP=YY-0.02*Y10	TPL01960
60 Y1T=0.01*Y10+Y1	TPL01970
XRSIDE=X2+0.01*X10	TPL01980
WRITE (6,922)TIME	TPL01990

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CALL TICKER (TIME)
TIME=TIME/216.0
WRITE (6,923)TIME
603 CALL FRAME (X1,Y1T,XRSIDE,Y22)
GO TO (61,62),NYSCL
61 CALL GXA (NY,XX,YY,SY)
GO TO 70
62 SY=Y10/FLOAT(NYC)
IF (NYC-5) 64,64,63
63 NY=NYC+1
CALL GXA (NY,XX,YY,SY)
GO TO 70
64 NY=NYC+1
VY=YY
DO 65 J=1,9
CALL GXA (NY,XX,VY,SY)
NY=NYC
AK=J+1
65 VY=YY+ALOG(AK)*CF*SY
70 GO TO (71,72),NXSCL
71 CALL GYA (NX,XX,YY,SX)
GO TO 76
72 SX=X10/FLOAT(NXC)
IF (NXC-5) 74,74,73
73 NX=NXC+1
CALL GYA (NX,XX,YY,SX)
GO TO 76
74 NX=NXC+1
VX=XX
DO 75 J=1,9
CALL GYA (NX,VX,YY,SX)
NX=NXC
AK=J+1
75 VX=XX+ALOG(AK)*CF*SX
76 XCENT=XX+0.2*X10
CALL TSP(XCENT,Y1T,TITLE(1),72)
XL=X1
Y11=Y1T-0.02*(Y1T-YY)
CALL TSP(XCENT,Y11,T2(1),72)
Y11=0.05*(Y1T-YY)
YL=Y1T-Y11*5.0
CALL TSP(XCENT,Y22,XLABEL(1),72)
DO 1235 J=1,12,2
YL=YL-Y11
1235 CALL TSP(XL,YL,YLABEL(J),12)
XPT=XX+C.85*X10
YPT=Y1-0.05*Y10
CALL BCDCON(CHR)
WRITE (0,911) BXMAX,X1PR
CALL TSP(XPT,YPT,CHR(1),18)

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TPL0200C
TPL02010
TPL02020
TPL02030
TPL02040
TPL02050
TPL02060
TPL02070
TPL02080
TPL02090
TPL02100
TPL02110
TPL02120
TPL02130
TPL02140
TPL02150
TPL02160
TPL02170
TPL02180
TPL02190
TPL02200
TPL02210
TPL02220
TPL02230
TPL02240
TPL02250
TPL02260
TPL02270
TPL02280
TPL02290
TPL02300
TPL02310
TPL02320
TPL02330
TPL02340
TPL02350
TPL02360
TPL02370
TPL02380
TPL02390
TPL02400
TPL02410
TPL02420
TPL02430
TPL02440
TPL02450
TPL02460
TPL02470
TPL02480
TPL02490

```

WRITE (0,911) BXMIN,X2PR	TPL02500
YPT=YPT-0.05*Y10	TPL02510
CALL TSP(XPT,YPT,CHR(1),18)	TPL02520
WRITE (0,911) BYMAX,Y1PR	TPL02530
YPT=YPT-0.05*Y10	TPL02540
CALL TSP(XPT,YPT,CHR(1),18)	TPL02550
WRITE (0,911) BYMIN,Y2PR	TPL02560
YPT=YPT-0.05*Y10	TPL02570
CALL TSP(XPT,YPT,CHR(1),18)	TPL02580
80 CALL BCDCON(TYP)	TPL02590
GO TO (82,81),NXSCL	TPL02600
82 IF (NX-10) 821,821,822	TPL02610
821 NQXJ=2	TPL02620
GO TO 825	TPL02630
822 IF (NX-40) 823,823,824	TPL02640
823 NQXJ=5	TPL02650
GO TO 825	TPL02660
824 NQXJ=10	TPL02670
825 DO 83 IK=1,NX,NQXJ	TPL02680
QX =XX+SX*FLOAT(IK)-SX	TPL02690
X2TYP=QX-X10/16.0	TPL02700
QX=QX/SCFX	TPL02710
IF (ABS(QX)-999.0) 827,827,826	TPL02720
826 WRITE (0,1006) QX	TPL02730
GO TO 83	TPL02740
827 IF (ABS(QX)-.1) 830,829,829	TPL02750
830 TTX=ABS(QX)*SCFX	TPL02760
IF (TTX-.2E-6) 829,829,826	TPL02770
829 WRITE (0,1008) QX	TPL02780
83 CALL TSP (X2TYP,Y2TYP,TYP,NCHRS)	TPL02790
GO TO 90	TPL02800
81 JNX=NXC+1	TPL02810
DO 183 IK=1,JNX	TPL02820
X2TYP=XX+SX*FLOAT(IK)-SX	TPL02830
IX=(X2TYP)/SX	TPL02840
XLX=10.0**IX	TPL02850
X2TYP=X2TYP-X10/16.0	TPL02860
WRITE (0,1006) XLX	TPL02870
183 CALL TSP (X2TYP,Y2TYP,TYP,NCHRS)	TPL02880
90 GO TO (92,91),NYSCL	TPL02890
92 IF(NY-10)1921,1921,1922	TPL02900
1921 NQYJ=2	TPL02910
GO TO 1925	TPL02920
1922 IF(NY-40)1923,1923,1924	TPL02930
1923 NQYJ=5	TPL02940
GO TO 1925	TPL02950
1924 NQYJ=10	TPL02960
1925 DO 93 IJ=1,NY,NQYJ	TPL02970
Y1TYP=YY+SY*FLOAT(IJ)-SY	TPL02980
QY=Y1TYP	TPL02990

QY=QY/SCFY	TPL03000
IF (ABS(QY)-999.0) 1927,1927,1926	TPL03010
1926 WRITE (0,1006) QY	TPL03020
GO TO 93	TPL03030
1927 IF (ABS(QY)-.1) 1930,1929,1929	TPL03040
1930 TTY=ABS(QY)*SCFY	TPL03050
IF (TTY-.1E-3) 1929,1929,1926	TPL03060
1929 WRITE (0,1008) QY	TPL03070
93 CALL TSP (X1TYP,Y1TYP,TYP,NCHRS)	TPL03080
GO TO 889	TPL03090
91 JNY=NYC+1	TPL03100
DO 193 IJ=1,JNY	TPL03110
Y1TYP=YY+SY*FLOAT(IJ)-SY	TPL03120
IY=(Y1TYP)/SY	TPL03130
YLY=10.0**IY	TPL03140
WRITE (0,1006) YLY	TPL03150
193 CALL TSP (X1TYP,Y1TYP,TYP,NCHRS)	TPL03160
889 CONTINUE	TPL03170
NVRS=NPTS-1	TPL03180
DO 98 JKL=1,INTENS	TPL03190
98 CALL DVR(NVRS,1,X,Y,1)	TPL03200
CALL END	TPL03210
CALL ADF	TPL03220
CALL TICKER (TIME)	TPL03230
TIME=TIME/216.0	TPL03240
WRITE (6,924)TIME	TPL03250
WRITE (6,909)MFRAME,(TITLE(I),I=1,12)	TPL03260
GO TO 99	TPL03270
100 MFRAME=MFRAME-1	TPL03280
WRITE (6,600)(TITLE(I),I=1,12)	TPL03290
99 CONTINUE	TPL03300
WRITE (6,600)(YLABEL(I),I=1,12)	TPL03310
600 FORMAT (22X 12A6)	TPL03320
GO TO 101	TPL03330
	TPL03340
	TPL03350
901 FORMAT(12A6)	TPL03360
902 FORMAT (11H 20X 12A6)	TPL03370
909 FORMAT (11H04X,10H FRAME NO. 14,3X,12A6)	TPL03380
910 FORMAT (11H04X,10H FRAME NO. 14,3X,22H SERIES IDENTIFICATION)	TPL03390
911 FORMAT (A6,1PE10.2,2X)	TPL03400
922 FORMAT(80X,17H BEGIN PLOT SETUP F10.4,3H MH)	TPL03410
923 FORMAT(80X,17H BEGIN PLOTTING F10.4,3H MH)	TPL03420
924 FORMAT(80X,17H END PLOTTING F10.4,3H MH)	TPL03430
1001 FORMAT (I6)	TPL03440
1002 FORMAT (A6)	TPL03450
1006 FORMAT (1PE8.2,4X)	TPL03460
1008 FORMAT (F8.3,4X)	TPL03470
211 FORMAT (11H0/1H019X,20H * * * ERROR * * * //20X,16H THE LOGARITHM	TPL03480
11C A6,31H-SCALE OPTION HAS BEEN SELECTED//20X,15H BUT A VALUE OF	TPL03490

2 A6,49H LESS THAN OR EQUAL TO ZERO HAS BEEN ENCOUNTERED.//20X,
 332H THIS GRAPH CANNOT BE CONTINUED.)
 END

TPLO3500
 TPLO3510
 TPLO3520

\$IBFTC HEADER LIST,DECK,REF

08-09-65HEAD0000

SUBROUTINE HEADER

HEAD0010

COMMON /ALL/ NIN,NDUT,NDATA,NIN1,NIN3,JHYD,NEL,NARRAY,NPAGE,LINESHEAD0020

1,NPROB,NPTS,INDEX,NPLOT,TITLE(12),TID(10,20),CNAME(5,20),LINEPP HEAD0030

2 ,MAT,MFRAME HEAD0040

NPAGE=NPAGE+1 HEAD0050

WRITE (6,601) NPROB,(TITLE(I),I=1,12),NPAGE HEAD0060

601 FORMAT (15H1GAROL PROBLEM 14,1H, 3X 12A6, 27X 4HPAGE 16) HEAD0070

RETURN HEAD0080

END HEAD0090

\$IBMAP BACKUP LIST,DECK,REF

08-11-65BACK0000

ENTRY BACK

BACK0010

BACK TXI **,0,0

BACK0020

SXA AXT,4

BACK0030

TSX S.100P,4

BACK0040

IOSKP B1

BACK0050

PZE S.SU11

BACK0060

AXT AXT **,4

BACK0070

TRA* BACK

BACK0080

B1 MZE 1

BACK0090

END

BACK0100

A number of routines which are used in GAROL are not included in the listing. These are machine language subroutines which are part of the General Atomic Plot Package.⁽⁷⁾ These routines are:

ADF	advances film
DVR	draw vector
END	writes end of file on plot tape
FRAME	establishes frame limits
GXA	generates x-axes
GYA	generates y-axes
RST	reset
SCI	select camera 1
SETUP	sets up plot buffer storage
TSP	types information on frame.

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