

USER'S MANUAL FOR A FORTRAN IV PROGRAM
FOR COMPUTING FLUTTER BOUNDARIES OF FLAT
PANEL ARRAYS IN SUPERSONIC FLOW

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MIDWEST RESEARCH INSTITUTE

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by

D. R. Kobett
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PREFACE

This manual was prepared by Midwest Research Institute under Contract No. NAS1-4900, "Research Relating to the Flutter of Flat Panels in a Supersonic Air Stream," for the Langley Research Center of the National Aeronautics and Space Administration.

Approved for:

MIDWEST RESEARCH INSTITUTE



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8 July 1966

ABSTRACT

The computer program is a by-product of research efforts that have produced NASA TN D-2227, CR-80, CR-538, and AFOSR TN 1952. The report material is arranged for two distinct types of readers, namely, the engineer who wishes to use the program as is, and the programmer who may be required to modify the program for a specific application.

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I. INTRODUCTION

The computer program described in this report is a by-product of panel flutter research efforts conducted under NASA and AFOSR sponsorship. It was developed to facilitate the calculation of flutter characteristics for multi-bay, flat panel arrays exposed on one side to a uniform supersonic air-stream. The program is written in FORTRAN IV for running on the IBM 7094 under IBSYS.

The computation technique employed is straightforward in the sense that a computer-run directly obtains, as output, points on the boundary separating stable from unstable regions in a generalized flutter-parameter-plane. (More conventional techniques require cross-plotting or machine interpolation under manual direction to obtain the "flutter points".) Although the program presented here is tailored to the case of a flat panel array, the technique can be conveniently adapted to related applications, for example, the flutter of a cylindrical shell or a wing-body configuration.

The report material is arranged for two distinct types of reader, namely, the engineer who wishes to use the program as is, and the programmer who may be required to modify the program for a specific application. The engineer will want to become familiar with the first six sections through the interpretation of output; the programmer with the main body of the report and those appendices that apply to the intended modification.

The computer program is based on the analytical model developed in [1].* A brief summary description of the model is given in Section II of this report; the reader interested in detail is referred to [1].

* Numbers in brackets refer to the bibliography.

II. BACKGROUND INFORMATION FOR THE PROGRAM USER

This section is divided into two parts, viz., a description of the analytical model employed and a discussion of the parametric options available to the program user.

A. Analytical Model

The computer program is based on the analysis described in [1], the salient features of which are summarized below.

Four different types of panel array configurations can be analyzed. Each configuration has an arbitrary number of chordwise bays; the distinction between configurations is associated with spanwise features. The first, and most general, array is one with finite span and arbitrary number of spanwise bays typified by Fig. 1.* The second configuration is one in which the array span is divided into equal width bays extending to infinity. The third configuration is an array with one spanwise bay whose side edges are free to deflect. The final configuration consists of the third array above, flanked at a distance by vertical surfaces representing wind tunnel walls.

All configurations have certain features in common. The upper surface of the panels is exposed to a uniform supersonic flow and the lower surface to a constant pressure equal to the static pressure in the undisturbed freestream. Acoustic effects on the lower surface and membrane stresses due to static pressure differential across the panel are not included.

To clarify the differences in the analyses of the different configurations, the case typified by Fig. 1 will first be discussed in some detail. Then those aspects peculiar to the other configurations will be pointed out.

The array is composed of geometrically identical panels; it has L chordwise and N spanwise bays, and is bordered by an inflexible surface. A nondimensional equation of motion for the vertical displacement of the panel surface is obtained using small deflection plate theory and exact, linearized, three-dimensional, potential aerodynamic theory. In formulating boundary and compatibility conditions the array is assumed to be supported at its perimeter and along the interior lines delineating the individual panels by a structure that does not deflect perpendicular to the plane of the array, but that does

* See Appendix I for Figures 1 - 6.

supply torsional restraint. At the leading and trailing edges the moment imposed by the supporting structure is equal to a proportionality factor, ϵ_x , multiplying the local panel slope. At the interior, spanwise directed members, the imposed moment is proportional to $2 \epsilon_x$ times the local panel slope; i.e., the interior members are twice as stiff, torsionally, as the ones at the perimeter.

The above torsional properties hold also for the chordwise directed supporting members, with the exception that the proportionality constant, ϵ_y , can be different from ϵ_x . The slope across the interior panel boundaries is assumed to be continuous.

The equation of motion is in essence a self-excited forced vibration equation where the aerodynamic pressure induced by the panel displacement is the forcing function. It is assumed that conditions for which the equation has harmonic solutions are conditions of neutral stability; this criterion is used in calculating the flutter boundaries for the panel array.

Harmonic solutions are obtained using a Galerkin approach. The chordwise variation of the panel displacement is approximated by a finite summation of natural vibration modes of a beam with L bays and boundary conditions the same as on the spanwise directed panel edges. The spanwise variation is approximated by one natural vibration mode* of a beam with N bays and boundary conditions the same as on the chordwise directed panel edges. Application of the Galerkin procedure requires integration of the aerodynamic pressure over the panel surface. This integration is performed by expanding the spanwise deflection shape in a sine series; then numerically integrating term by term using the unsteady pressure solution derived in [2] for sinusoidal spanwise and arbitrary chordwise deflection shape.

The above procedure leads to a set of simultaneous, complex, algebraic equations (see [1], Eq. (39)) for the amplitude and phasing of the approximating modes. An effect of structural damping is introduced by multiplying the stiffness matrix by the complex damping factor $(1 + jg)$. Solutions to the equations for real values of the basic parameters l/μ and $Z^{1/3}$

* Coupling between spanwise modes is neglected; the mode number is arbitrary.

are obtained by the procedure described in Section III*. The preceding is a brief description of analytical details for the panel array typified by Fig. 1. The analysis for the other three configurations are similar to that described above, with the exceptions noted in the following paragraph.

For the array which extends to infinity in the spanwise direction (second configuration) the mode approximating the spanwise deflection is automatically taken to be the lowest frequency natural vibration mode of a beam with an infinite number of bays. For the array with free side edges (third configuration) the panels are assumed to deflect two-dimensionally, i.e., with no spanwise variation in the deflection shape. The two-dimensionality assumption is incorporated by using the sine series expansion for a rectangular half wave. The fourth configuration, the one with simulated wind tunnel walls, is also handled simply by introducing an appropriate expansion. In this case, the expansion is one which simulates the effect of fictitious image panels, thereby obtaining no cross flow at the walls. Mach wave reflections from the walls are intrinsically included by this technique.

B. Parametric Options Available to the Program User

Within the framework of the four geometrical configurations described earlier, there are options available for what will be called analytical and physical parameters. The analytical parameters are:

1. Number of modes in the approximation of the chordwise deflection shape.
2. Mode numbers of the chordwise approximating terms.
3. Number of terms in the sine series expansion of the spanwise approximating mode.
4. Mode number of the spanwise approximating term (first configuration only).

$$* \quad \frac{1}{\mu} = \text{mass ratio parameter} = \frac{\rho a}{\rho_s h}$$

$Z^{1/3}$ = a parameter involving dynamic pressure and bending stiffness

$$= \frac{h}{a} \left[\frac{E}{q(1 - \nu^2)} \right]^{1/3}$$

where

ρ = free stream density
 ρ_s = panel material density
 a = panel chord
 h = panel thickness

E = modulus of elasticity
 q = freestream dynamic pressure
 ν = Poisson's ratio

The physical parameters are:

1. Mach number
2. Aspect ratio
3. Torsional restraint proportionality factors ϵ_x and ϵ_y
4. Number of chordwise panels
5. Number of spanwise panels (first configuration only)
6. Distance from panel edge to wind tunnel wall (fourth configuration only)
7. Structural damping coefficient.

Permissible ranges for the analytical parameters are defined in the following paragraphs.

The number of modes used to approximate the chordwise deflection shape must be at least 2 and at most 10. The lower limit is set by the analytical techniques employed and the upper limit by dimensioned array sizes in the program. Numerical considerations are expected to reduce the permissible upper limit to less than 10. With an earlier version of the program, numerical inaccuracy was encountered in increasing from 4 to 6 modes. The present, improved, version has been used extensively for up to 6 mode analyses [3]; it has not been applied to analyses requiring the use of more than 6 modes. The modes may be any combination of the first 30 natural vibration modes of a beam with the appropriate number of bays.

Up to 20 nonzero terms may be used in the sine series expansion of the approximating spanwise mode. Since the expansion always has zero alternate terms (odd or even numbered depending on mode number and number of spanwise bays), the above condition actually corresponds to a 40 term series expansion.

The spanwise approximating mode (first geometrical configuration only) may be any one of the first 30 natural vibration modes of a beam with N bays, N being the number of spanwise bays in the panel array. The above is a mechanical bound set by the program; practically, the mode number must be selected in cognizance of the number of spanwise bays, N , the spanwise mode number, and the 40 term bound on the sine series expansion.

This completes the definition of permissible ranges for the analytical parameters. Ranges for the physical parameters are discussed in the succeeding paragraphs.

Mach number must be confined to the supersonic regime (i.e., > 1) for compatibility with the analytical model.

The computer program imposes no restriction on aspect ratio. However, a practical bound (a judgment of the user) is imposed by the permissible number of modes in the approximation of the chordwise deflection shape.

The nondimensional torsional restraint proportionality factors ϵ_x and ϵ_y can be independently varied from zero to any maximum desired*. On a practical basis, however, $\epsilon = 0$ corresponds to pinned edge conditions and $\epsilon = 1,000$ has been found to very closely approximate the clamped edge case (a judgment made on the bases of both modal frequencies and computed flutter boundaries). Further, it has been observed that flutter boundaries computed using $\epsilon = 100$ and $\epsilon = 1,000$ are nearly identical, while $\epsilon = 10$ yields results approximately midway between the pinned and clamped edge cases.

Panel arrays with up to 4 chordwise bays can be analyzed. Again, however, a practical bound must be recognized, associated with the permissible number of modes in the approximation of the chordwise deflection shape.

Up to 6 spanwise bays can be used in analyses of finite span arrays (first geometrical configuration). As noted earlier, however, the number must be selected in cognizance of the spanwise mode number and the 40 term bound on the sine series expansion of the spanwise deflection shape.

For the fourth geometrical configuration, the distance from the panel side edges to the wind tunnel wall must be greater than zero to be compatible with the theory. Practically, it should be equal to or greater than about 10 per cent of the panel span in order to obtain a satisfactory sine series expansion of the spanwise deflection shape.

Finally, there is no program restriction on values for the structural damping coefficient.

This completes the overall description of parametric options available to the program user. Related recommendations for optimum program usage are provided in Section IV.

III. GENERAL PROGRAM DESCRIPTION

The method used to find flutter points is essentially that described on pages 15 - 17 of [1]. A few slight modifications are used, however, in the interest of saving either computer running time or storage.

* See Appendix VIII for description of a mild restriction on admissible values for ϵ_y .

The program makes use of a magnetic tape to store a number of arrays which depend only on the number of spanwise and chordwise bays, the corresponding mode numbers allowed and the parameters ϵ_x and ϵ_y describing edge conditions. If such a tape has not already been generated it can be generated as the first step of any flutter run. If it has been generated on a previous run it may be mounted as an input tape. Since the program may take around 12 min. to produce a tape when 3 chordwise bays are needed, it is advisable to save the tape if it might be used again. Details of the tape format are given in Appendix III.

Because of the size of the program it is necessary to use the overlay feature of the loader during execution. The first overlay generates the tape described in the preceding paragraph, if necessary. The second overlay reads data until a flutter problem has been defined, reads data from the tape generated previously for the specified number of chordwise bays, prints out heading information describing the problem and generates matrices which can be used by a more or less general subroutine, EUCLID, to compute flutter points and vectors. Subroutine EUCLID is loaded as the third overlay.

The flutter matrix used by the program is equivalent to but slightly different from that shown in [1]. Let $E = \{E_{\bar{m},m}\}$, $J = \{J_{\bar{m},m}\}$ and $C = \{C_{\bar{m},m}\}$ to simplify notation. Then since Eq. 39 of Ref. [1] can be premultiplied by any nonsingular matrix, we can premultiply by $\beta(1-jg)E^{-1}$, for E is nonsingular and β is not zero for Mach number greater than 1. The new form of Eq. 40 then becomes

$$\text{Det} \left\{ \frac{Z\beta(1+g^2)I}{24} - \mu\beta k^2(1-jg)E^{-1}J + (1-jg)E^{-1}C \right\} = 0$$

where I is the identity matrix. The argument list for subroutine EUCLID includes g , $-\beta k^2$, $12/\beta(1+g^2)$, and a table of μ -values in addition to the matrices $E^{-1}J$ and $E^{-1}C$. If we let λ denote $\frac{Z\beta(1+g^2)}{24}$ and $\bar{C}(\mu)$ be the matrix $\mu\beta k^2(1-jg)E^{-1}J - (1-jg)E^{-1}C$, the problem to be solved is that of finding real parameters λ and μ such that $|\lambda I - \bar{C}(\mu)| = 0$.

If μ is assigned a numerical value, then $|\lambda I - \bar{C}(\mu)|$ is the characteristic equation of the complex matrix $\bar{C}(\mu)$. The condition that the determinant vanish requires that real and imaginary parts of the characteristic equation have a common root. This occurs if and only if the Sylvester resultant [4] between the real and imaginary parts of the characteristic equation vanishes. Thus if for two distinct values of μ , the corresponding Sylvester resultants have opposite signs, there is a μ value between the original two for which the resultant vanishes.

Subroutine EUCLID first tabulates the Sylvester resultant corresponding to each value in the μ - table.* A search is then made for sign changes of the resultant as μ varies. When a sign change is detected, the program interpolates until the flutter value of μ is found to the required degree of accuracy. Then the corresponding value of λ and the flutter vector are found. The results are converted to the parameters of interest, namely $Z^{1/3}$ and $1/\mu$ and printed. The program then repeats the steps above until all sign changes in the resultant table have been processed, whereupon the second overlay is called again to read data for the next problem.

IV. COMPUTATION PROCEDURE

The purpose of a typical application of the computer program is to calculate stability boundaries for a particular geometrical configuration, and fixed values of Mach number, aspect ratio, torsional edge restraint, spanwise mode number (where applicable), and structural damping coefficient. The stability boundaries are obtained via a series of calculations as described below.**

In a discrete calculation, values are assigned to the analytical and physical parameters, a reduced frequency is specified, a table of μ values defined, and the program then computes the flutter points lying within the range of μ defined by the table.*** (For clarity of ensuing discussions a computation case is here defined as a series of discrete calculations for a selected set of reduced frequencies and damping coefficients.) Every computation case yields a number of points on the stability boundaries, each point being characterized by a particular frequency and flutter vector. Distinct stability boundaries are obtained by constructing continuous curves through the computed points, using continuity of reduced frequency and flutter vector as associative criteria.

* A table of μ values is defined by input data.

** In general, a number of computer runs will be required to completely define the boundaries.

*** If two flutter points lie within one increment of the μ table neither will be detected. However, experience with the program has shown that this event seldom occurs when a μ table with moderate increment sizes is employed (see Fig. 2 for recommended table). Further, when it does occur it creates little difficulty because the points can be obtained, if desired, by repeating the calculation using a μ table with finer increment sizes. In most instances the repetition is unnecessary because adjacent points on the boundaries are available from calculations made using slightly different frequencies.

The input μ table may be tailored to restrict the range through which the program searches for flutter points. In some instances, this tactic can be profitably employed to reduce computation time. In general, however, a range in $1/\mu$ from 0.01 to 0.20 is of practical interest and the μ table in Fig. 2 has therefore been used extensively in application of the computer program.

It has also been found economical to limit each computation case to between 5 and 10 reduced frequencies, and more or less construct the boundaries step by step.

Computation time can be reduced through judicious use of the intermediate data tape. The data arrays stored on the tape depend on

Number of spanwise bays - N
Spanwise mode number - NGBAR
Torsional edge restraints - ϵ_x and ϵ_y
Number of chordwise bays* - L.

The tape also contains data for 10 chordwise modes which may be any 10 of the first 30 natural vibration modes of a beam with L bays (see Section V on Input Preparation). The data tape, on the other hand, is independent of Mach number, aspect ratio and structural damping coefficient.

Since an appreciable amount of time is required to generate the data arrays stored on the tape (particularly for $L > 1$) it is advisable to reserve the tape for use as an auxiliary input tape in subsequent runs. This is true whether or not Mach number, aspect ratio and structural damping are varied. To emphasize the above point it may be noted that the results reported in [3] were obtained using a tape generated in the first computer run, whereas a total of approximately 15 runs were made in all.

Some final comments are required concerning the case where a computed flutter point(s) is incorrect (indicated by program checks included in the printed output). If this occurs the input data should be double checked first, because improper input can cause erroneous results. (For example, the mode numbers may not be in ascending order.) If the data are correct the specified error bound on μ (TESTR; see Appendix IX) may be too large. Experience with the program has indicated that a value of TESTR equal 10^{-7} is adequate in general for analyses using up to 6 chordwise modes, but numerical peculiarities could occasionally require an even smaller error bound.

* Data for up to 4 chordwise bays can be stored on 1 tape. However, no penalty in computation time is incurred if the user chooses to generate separate tapes for each L value.

Another possible cause of erroneous results is the use of too many chordwise modes in the analysis. As previously noted, with an earlier version of the program numerical inaccuracy was encountered when the number of modes was increased from 4 to 6. Improvement of one of the program routines (FLUT) eliminated this difficulty but it is possible that the use of more than 6 modes may similarly overtax a critical routine.

V. INPUT PREPARATION

A data deck may contain data sets for one or more computation cases, the only restriction being that the cases must all require the same intermediate data tape*, which may be available from a previous run or generated as part of the first case of the current run.

The first card of a data deck refers to the intermediate tape. If the tape is available from a previous run the first card is blank; if the tape is to be generated in the current run the first card is as follows.

<u>Cols.</u>	<u>Format</u>	<u>Symbol</u>	<u>Description</u>
1-2	I2	IMIN	(see IMAX)
3-4	I2	IMAX	Data arrays will be generated and stored for values of L from IMIN to IMAX inclusive ($IMIN \leq IMAX$).
5-24	10I2	MODE(I)	Array of 10 chordwise mode numbers between 1 and 30 in ascending order. Data arrays will be generated and stored for the 10 modes specified.**
25-26	I2	NSP	Number of spanwise bays.
27-28	I2	NGBAR	Spanwise mode number.
29-38	F10.0	EPY	Torsional restraint proportionality factor for spanwise directed panel edges (ϵ_x in Section II and [1]).

* See discussions of the intermediate tape in Section IV and Appendix III.

** Ten modes are required here even though some are not later used.

<u>Cols.</u>	<u>Format</u>	<u>Symbol</u>	<u>Description</u>
39-48	F10.0	EPK	Torsional restraint proportionality factor for chordwise directed panel edges (e_y in Section II and [1]). This item is irrelevant for options 4 and 5 (see option identification in later description of number 11 data card).

Data for the first case follow the intermediate tape card. This first data set must contain all of the cards described below (and illustrated in Fig. 4 which is provided for user reference) plus a blank terminating card. Subsequent data sets need only include the cards containing input information to be redefined for the new case. Each data set following the first is terminated by a blank card.

The individual data cards each have an identification number (between 1 and 12) in columns 1 and 2. This number is used for reference in the following description of input data details.*

01 Card

<u>Cols.</u>	<u>Format</u>	<u>Symbol</u>	<u>Description</u>
1-2	I2	-	Identification number (01 on this card).
11-20	E10.5	TESTR	Upper bound on acceptable decimal per cent error in computed μ (Appendix IX).

02 Card

<u>Cols.</u>	<u>Format</u>	<u>Symbol</u>	<u>Description</u>
1-2	I2	-	Identification number (02 on this card).
11-20	E10.5	S	Reciprocal of aspect ratio.

03 Card

<u>Cols.</u>	<u>Format</u>	<u>Symbol</u>	<u>Description</u>
1-2	I2	-	Identification number (03 on this card).

* Sample data listings (Figs. 2a, 2b and 3) are discussed at the end of this section.

03 Card (Concluded)

<u>Cols.</u>	<u>Format</u>	<u>Symbol</u>	<u>Description</u>
3-4	I2	MMAx	Number of chordwise modes.
5-6	I2	-	If zero, consecutive modes starting with the first are used; if not zero see next item.
61-80	10I2	MODE(I)	This field is blank if columns 5 - 6 contain zero. If columns 5 - 6 are not zero, this field contains the mode numbers to be used in the analysis, in ascending order. (The modes listed must be ones that are included on the intermediate tape.)

04 Card

<u>Cols.</u>	<u>Format</u>	<u>Symbol</u>	<u>Description</u>
1-2	I2	-	Identification number (04 on this card).
11-20	E10.5	EMSQ	Mach number squared.

05 Card

<u>Cols.</u>	<u>Format</u>	<u>Symbol</u>	<u>Description</u>
1-2	I2	-	Identification number (05 on this card).
3-4	I2	NG	Number of damping coefficients to be processed (maximum of 5). Blank or zero is taken as 1.
11-60	5E10.5	GT(I)	Damping coefficients.

06 Card

<u>Cols.</u>	<u>Format</u>	<u>Symbol</u>	<u>Description</u>
1-2	I2	-	Identification number (06 on this card).

06 Card (Concluded)

<u>Cols.</u>	<u>Format</u>	<u>Symbol</u>	<u>Description</u>
3-4	I2	L	Number of chordwise bays in panel array. (The number specified must be one of those included on the intermediate tape.)
11-20	E10.5	SAVE(1)	Blank or zero causes the inverse of the elastic matrix times the inertia and aerodynamic matrices to be printed. A nonzero value suppresses the printing.

07 Card

A series of 07 cards are used to read in the μ table. The table must contain a minimum of 2 and a maximum of 50 values arranged in monotonic order. Details of a typical 07 card are as follows.

<u>Cols.</u>	<u>Format</u>	<u>Symbol</u>	<u>Description</u>
1-2	I2	-	Identification number (07 on this card).
3-4	I2	-	Index of first μ on this card.
5-6	I2	-	Index of last μ on this card.
11-60	5E10.5	ALPHA(I)	Values of μ (up to five values).

08 Card

<u>Cols.</u>	<u>Format</u>	<u>Symbol</u>	<u>Description</u>
1-2	I2	-	Identification number (08 on this card).
3-4	I2	MAXAL	Total number of values in the μ table.

09 Card

A series of 09 cards are used to read in the reduced frequencies to be processed. A maximum of 30 frequencies can be read, in any desired order. Details of a typical 09 card are as follows.

<u>Cols.</u>	<u>Format</u>	<u>Symbol</u>	<u>Description</u>
1-2	I2	-	Identification number (09 on this card).

09 Card (Concluded)

<u>Cols.</u>	<u>Format</u>	<u>Symbol</u>	<u>Description</u>
3-4	I2	-	Index of first frequency on this card.
5-6	I2	-	Index of last frequency on this card.
11-60	SE10.5	CKAY(I)	Frequencies (up to five values).

10 Card

<u>Cols.</u>	<u>Format</u>	<u>Symbol</u>	<u>Description</u>
1-2	I2	-	Identification number (10 on this card).
3-4	I2	NK	Total number of frequencies read.

11 Card

This card identifies which of the 4 geometrical configurations described in Section II is to be analyzed. An option number is used for this purpose. The correlation between option number and geometrical configuration is as follows.

Option 1 - The finite array typified by Fig. 1.

Option 2 - The array with infinite span divided into equal width bays.

Option 4 - The array with one spanwise bay and free side edges.

Option 5 - The option 4 array flanked by vertical surfaces representing wind tunnel walls.

The omission of 3 in the option sequence results from the fact that a fifth geometrical configuration included in the analysis [1] has not been programmed. Details of the 11 card are as follows.

<u>Cols.</u>	<u>Format</u>	<u>Symbol</u>	<u>Description</u>
1-2	I2	-	Identification number (11 on this card).
3-4	I2	NCASE	Option number.

11 Card (Concluded)

<u>Cols.</u>	<u>Format</u>	<u>Symbol</u>	<u>Description</u>
11-20	E10.5	A/2	Distance from panel edge to wind tunnel wall, measured in panel spans. (Relevant to Option 5 only.)

12 Card

<u>Cols.</u>	<u>Format</u>	<u>Symbol</u>	<u>Description</u>
1-2	I2	-	Identification number (12 on this card).
3-4	I2	NNN	Number of nonzero terms in sine series expansion of spanwise deflection shape (maximum of 20). For Option 2 and $\epsilon_y = 0$ this number must be 1.

This completes the description of data card details. Sample data deck listings are given in Figs. 2 and 3 to complement the above description. The data listed in Fig. 2a cause two cases to be executed, both using an intermediate tape generated in the current run. The first case is an analysis of a finite array with 2 chordwise bays and 1 spanwise bay, and with

Mach number = 1.35
Aspect ratio = 4
Damping coefficient = 0.01
 $\epsilon_x = \epsilon_y = 0$
Spanwise mode number = 1 .

The analysis uses the first 4 chordwise modes, 20 nonzero terms in the sine series expansion, and 2 frequencies, 1.0 and 1.5 are processed.

The second case is an analysis of an Option 2 array with 3 chordwise bays and with

Mach number = 1.2
Aspect ratio = 2
Damping coefficient = 0.015
 $\epsilon_x = \epsilon_y = 0$.

The analysis uses chordwise modes 1, 4, 7, and 9, and 2 frequencies, 0.7 and 0.8 are processed.

The data listed in Fig. 2b also cause two cases to be executed, both using an intermediate tape generated in a previous run (assumed to be the run of Fig. 2a). The first case is an analysis of an Option 5 array with 1 chordwise bay and with

Mach number = 1.3
Aspect ratio = 1
Damping coefficient = 0
 $\epsilon_y = 0$

The analysis uses the first 4 chordwise modes, and 15 nonzero terms in the sine series expansion. The distance from the panel edge to the wind tunnel wall is one-quarter of the panel span. Three frequencies, 1.0, 1.2 and 1.4, are processed. The second case is identical with the first except Mach number is changed to 1.2.

The data listed in Fig. 3 will cause the sample output of Fig. 5 to be generated.

VI. INTERPRETATION OF OUTPUT

The output listing from a typical computer run illustrated in Fig. 5 is the implied reference for this section.

The output listing includes several checks on the validity of computed results and it is therefore pertinent to begin this discussion with the following brief reiteration of the overall computational technique employed. The purpose of a computer run is to calculate real-valued pairs of the parameters μ and Z which satisfy Eq. (40) of [1], that is, values for which the flutter determinant vanishes. The technique employed is not one of direct iteration of the complex flutter determinant. Instead, the Sylvester determinant composed of the coefficients of the real and imaginary characteristic polynomials of the flutter matrix, is tabulated with respect to the parameter μ *. The μ for which the Sylvester determinant vanishes, together with the corresponding Z obtained by operating on the characteristic polynomials, comprise a real-valued $\mu - Z$ pair for which the flutter determinant vanishes. These pairs are listed in the output in the converted form $1/\mu$ and $Z^{1/3}$ together with the flutter vector, program checks and associated identifying information.

* The elements of the Sylvester determinant are real-valued functions of μ ; they do not depend on Z .

Referring now to Fig. 5 the first line of output is a self-explanatory identification heading. The next block of output is a summarization of input parameters as follows:

- M - Mach number
- S - Reciprocal of aspect ratio
- E (SPAN) - Torsional restraint proportionality factor for spanwise directed edges (ϵ_x)
- E (CHORD) - Torsional restraint proportionality factor for chordwise directed edges (ϵ_y)
- TESTR - A precision factor imposed on the iteration of the Sylvester determinant (Appendix IX)
- L - Number of chordwise bays
- MMAX - Number of chordwise modes used in the analysis
- N - Number of spanwise bays (relevant only to Option 1 configuration)
- UMAX - Number of nonzero terms in the sine series expansion of the spanwise deflection shape
- SPANWISE MODE - Number of the spanwise approximating mode
- CASE - Geometrical configuration option number
- A/2 - Distance, in panel spans, from panel edge to wind tunnel wall (relevant only to Option 5)
- 1/DPHI - Number of equal increments (per bay) used in the chordwise numerical integration of the aerodynamic pressure (fixed at 16 in the program)
- K - Reduced frequency
- G - Structural damping coefficient

The next block of output contains intermediate computed results as follows:

- GAMMA BAR - Frequency of spanwise mode
- CHORDWISE MODE - Mode numbers and frequencies of chordwise modes
- BN(U) - Nonzero coefficients of sine-series expansion of spanwise deflection shape; listed in order of decreasing wavelength
- INVERSE OF ELASTIC MATRIX TIMES INERTIA MATRIX - The matrix $E^{-1}J$ (see Section III)
- INVERSE OF ELASTIC MATRIX TIMES REAL PART AEROD MATRIX - The matrix $\text{Real} \{E^{-1}C\}$ (see Section III)
- INVERSE OF ELASTIC MATRIX TIMES IMAG PART AEROD MATRIX - The matrix $\text{Imag} \{E^{-1}C\}$ (see Section III)

The input μ table is printed next, with the corresponding computed values of the Sylvester determinant. RES denotes the value of the determinant. SFA and SFR are scale factors on RES (see Appendix II). Sign changes in RES indicate the presence of a flutter point.

The preceding output constitutes general information; the remainder of the output is composed of blocks of computed flutter data, repeated for each flutter point that is found. The first item is the number of iterative interpolations of the Sylvester determinant required to obtain the flutter μ . Following this is a three-rowed tabulation containing the computed flutter point in the first row and the first of the program checks in the second and third rows. In the first row, $Z^{1/3}$ and $1/\mu$ are the computed flutter point pair, IAMDA is the negative of the common root of the characteristic polynomials at flutter, and RES (together with SFA and SFR) is the value of the Sylvester determinant for the flutter μ . The next two rows contain the same data as above except the μ 's are the last two bracketing μ 's in the iterative interpolation of the Sylvester determinant.* The test criterion is that RES in the second and third rows should be of opposite sign.

The next item printed is the flutter vector in polar form, normalized on the maximum component. R denotes the moduli and THETA the relative phase angles in radians. The vector elements are listed in order of ascending mode number.

The tabulation labelled COMPLEX RESIDUALS is a second program check, obtained by premultiplying the flutter vector by the flutter matrix. The test criterion here is that the "COMPLEX RESIDUALS" vector elements should uniformly be small (ideally zero).

The print-out labelled CHARACTERISTIC EQUATION AT FLUTTER are the coefficients of the real and imaginary characteristic polynomials at flutter. The coefficients of the real polynomial are listed first, beginning with the constant term and progressing toward the higher order terms. The real polynomial is of order MMAX and the leading coefficient is always unity. The imaginary polynomial, printed next, is of order MMAX-1.

The next line of output (containing P, Q, P/PIA and Q/QIA) is a numerical precision check of the computed flutter point, based on the criterion that the real and imaginary characteristic polynomials must have a common root at flutter. The theoretical basis for this check is described in Appendix IX.

* In the print-out these three values of μ (and/or $1/\mu$) will sometimes be identical because only six digits to the right of the decimal are printed.

The last output block (three lines) is a check to verify that the flutter determinant changes sign in the neighborhood of the computed flutter point. The first line contains the flutter λ and the corresponding value of the complex flutter determinant (real part printed first). The next two lines contain, respectively, 1.02 λ and 0.98 λ with the corresponding values of the flutter determinant. The test criteria are that the determinant must be of opposite sign in the last two lines, and the absolute value of the determinant in the first line should be less than that in the other two lines.

This completes the description of general output and specific output for a computed flutter point. In the general case, more than one flutter point will be obtained for a given reduced frequency, and there will be a corresponding number of output blocks containing the specific information just described. The output illustrated in Fig. 5, for example, contains three flutter points.

VII. PROGRAM ORGANIZATION

The main program (Deck name GHFLUT) is a dummy program used to control program overlay. It calls two subroutines, GHDUMP and CONTRL. The subprograms called by these two routines are shown in Fig. 6a and b.

Subroutine GHDUMP will generate a tape containing a number of arrays depending only on the elastic constraint properties and the number of bays in spanwise and chordwise directions and the corresponding mode shapes to be used in the analysis. There is no direct (in core) transfer of data from this routine to CONTRL; all information is transferred via the intermediate data tape.

Subroutine CONTRL is the control program for the major part of the flutter calculation. It reads input data describing the cases to be run, computes matrices and other parameters that are needed and calls subroutine EUCLID to find the actual flutter points.

Subroutine EUCLID is a specialization of a general purpose routine for finding pairs of real parameters for which a complex matrix vanishes. A slightly different version of the subroutine has been used to determine stability boundaries in a wing-body flutter analysis [5]. Subroutines CBAR, WROUT and VECNRM are written especially for the present panel flutter analysis. The other subroutines called by EUCLID are general purpose and would likely be suitable for use in other types of flutter calculations. The program still contains some of the control parameters which served to differentiate between the two flutter applications, although for all practical purposes these parameters are constants.

Another vestige of a previous application of the program is seen in the symbols used for μ , i.e., ALPHA, ALP, ALS, AP, AN, AL and for λ (formerly α) i.e., U, UN, UP. This, perhaps confusing, interchange should be noted carefully by the programmer.

In an earlier program version the role of the parameters μ , λ were given to α and μ . The present version is to be preferred, however, in spite of an additional matrix inversion required, because it is much easier for the user to choose a suitable range of tabulated μ values than of the old α values.

A list of all routines and a brief description of the purpose of each is given below.

GHFLUT is the main routine. It is a dummy routine used to control program overlay.

GHDUMP reads the mode numbers, number of spanwise bays, ϵ_x , ϵ_y and the range of values of L, the number of chordwise bays. For each L in the range, information is written on logical tape 9. This information is needed by subroutine CONTRL to set up flutter equations.

FREQEQ finds frequencies and generalized coordinates of the chordwise or spanwise modes.

CDFIND transfers the frequencies of modes requested into an array to be written on tape and finds the quantities $C_{m,l}$ and $D_{m,l}$. For chordwise modes it also generates the matrices $J_{\bar{m},m}$, $K_{\bar{m},m}$ and $R_{\bar{m},m}$.

GMML finds $G_{\bar{m},m,\ell}(\varphi)$. (See [1], page 52.)

HMML finds $H_{\bar{m},m,\ell}(\varphi)$. (See [1], page 53.)

CONTRL is effectually the main program. It has been made into a subroutine to facilitate program overlay. It calls INK to read one set of data. If necessary GPLUSH is called to read required data from logical tape 9. When the mode numbers required are not taken in sequence from the array on tape 9, the matrices read from tape are compressed to delete undesired modes. The routine then calls BFQST and computes $E^{-1}J$ and $E^{-1}R$. Then for each entry in the table of reduced frequencies (k) the matrices AER and AEI are computed, a value of structural damping (g) is chosen from the table and subroutine EUCLID is called to calculate flutter points. After the return from EUCLID, INK is called and the cycle is repeated.

INK reads input cards for the problems being run. Since problems subsequent to the first may be specified by reading only those parameters which change, control parameters are set in this routine which suppress parts of the computation which would be unnecessarily repetitious.

GPLUSH reads from logical tape 9 values for mode numbers, number of spanwise bays, ϵ_x and ϵ_y . Also read are mode frequencies and several matrices which depend on the number of chordwise bays specified.

BFQST calculates the quantities Q, S and T and the array $B_{n,u} F(u)$ for various values of u. (See [1], Appendices D and E.)

UMKEHR inverts a real matrix.

FINDP calculates $P_u(\xi)$. (See [1], page 46.)

FINDI computes the arrays EYER and EYEI where $EYER(MBAR,M) = \text{Real} \left\{ \sum_u B_{n,u} F(u) I_{\bar{m},m,u} \right\}$ and $EYEI(MBAR,M) = \text{Imag} \left\{ \sum_u B_{n,u} F(u) I_{\bar{m},m,u} \right\}$. These are also premultiplied by E^{-1} and stored as AER and AEI. (See [1], page 15.) The integrals $I_{\bar{m},m,u}$ are evaluated using the Newton-Coates five point formula (Bode's rule) [6] four times for each bay.

HD1063 prints a heading for each case, prints parameters identifying the case and that portion of output which is common to all flutter points for the given case.

CLOCK interrogates the internal clock and returns date and time coded as four alphameric words.

EUCLID uses values of μ from a table read into the program to construct the complex \bar{C} matrix. For each of these matrices, Sylvester's resultant is found and tabulated versus μ . This table is then searched for sign changes and for each sign change the program interpolates to find a μ value for which Sylvester's resultant vanishes. A corresponding Z value is found and the pair of values μ, Z represent a flutter point. Some checks are performed and the flutter point data along with flutter vector and figures of merit are printed out.

CBAR generates the matrix \bar{C} .

EQCHAR finds the characteristic equation of a double precision matrix. The routine handles 1 x 1 and 2 x 2 matrices as special cases. Larger matrices are first reduced to Hessenberg form [7] then subroutine CHAR is called to find the characteristic equation (see Appendix VII).

CHAR uses a recursion scheme to find coefficients of the characteristic equation of a matrix which is in Hessenberg form.

SCALE generates a matrix whose determinant vanishes when real and imaginary parts of the characteristic equation of the flutter matrix have common roots. In the process of generating this matrix two scale factors are removed, one on the roots of the characteristic equation, the other on the determinant of the matrix. This is necessary because of the enormous magnitude fluctuations encountered without scaling. A recursion based on pivotal reduction is used to allow the resultant to be computed as a determinant of order n rather than $2n-1$.

DETERM finds the determinant of a double precision matrix and scales it to prevent underflow. The true value of the determinant is $RES \times 2^{NSUM}$, where RES and NSUM are subroutine arguments.

WRITER prints a table of μ versus Sylvester's resultant from the real and imaginary parts of the characteristic equation. Flutter points are indicated where this resultant changes sign. Two scale factors are also printed which do not affect the sign.

FLUT finds the second flutter parameter, α , corresponding to the flutter value of μ .*

WROUT prints the flutter point data. The same routine also prints surrounding points used in interpolating for the final flutter point.*

VECTOR computes the flutter vector. The vector is premultiplied by the flutter matrix to give the residuals. Polar form of the vector and residuals are printed. Figures of merit are found for the real and imaginary parts of the characteristic equation at flutter. These are printed along with the characteristic equations. Finally, the determinant is computed for the flutter matrix and again for the same matrix where the eigenvalue which was subtracted on the main diagonal is increased and decreased by 2 per cent. These three determinants are printed.

INVCX inverts a complex matrix.

VECNRM normalizes the flutter vector in accordance with a scheme where each mode shape has unit rms amplitude.

* Note as mentioned earlier that the program symbols used for μ suggest α rather than μ .

CXDET finds the determinant of a complex matrix. The determinant is $X + iY$ where X and Y are subroutine arguments.

FMM finds $F_{\bar{m},m}(a_1, a_2, \alpha)$. (See [1], pages 51 - 52.)

FMKT finds the k^{th} derivative of $f_m(v)$ evaluated at $v = t$. (See page 51, [1]). The derivative of order zero is considered to be the function itself. This function has three arguments, k , m and t .

BFV evaluates the Bessel function $J_\nu(x)$ where $\nu = 0$ or 1 .

SUMM is called by BFV to evaluate $J_\nu(x)$ when x is greater than or equal to 4.

VIII. SUBMITTING A COMPUTER RUN

The program requires that logical tape 9 be available to the program. Hence, the user must either give instructions to mount a previously generated tape, or to mount a tape to be reserved following the current run, or to mount a scratch tape for use as logical tape 9.

Program deck structure, excluding ID or JOB cards for the particular installation, is shown in the following list.

\$IBJOB	card	
Deck	GHFLUT	
Deck	FMKT.	- subroutine FMKT
\$ORIGIN	EINS	
Deck	GHDUM.	- subroutine GHDUMP
Deck	GMML.	- subroutine GMML
Deck	HMML.	- subroutine HMML
Deck	FMM.	- function FMM
Deck	CDFIN.	- subroutine CDFIND
Deck	FREQE.	- subroutine FREQEQ
\$ORIGIN	EINS	
Deck	CLOCK.	- subroutine CLOCK
Deck	LANGLY	- subroutine CONTRL
\$ORIGIN	ZWEI	
Deck	INK.	- subroutine INK
Deck	GPLUSH.	- subroutine GPLUSH
Deck	BFQST.	- subroutine BFQST
Deck	UMKEH.	- subroutine UMKEHR
Deck	SUMM.	- function SUMM
Deck	BFV.	- function BFV

Deck	PFind	- subroutine FINDP
Deck	IFIND	- subroutine FINDI
Deck	HD1063	- subroutine HD1063
\$ORIGIN	ZWEI	
Deck	CBAR.	- subroutine CBAR
Deck	CHAR.	- subroutine CHAR
Deck	EQCHA.	- subroutine EQCHAR
Deck	SCALE.	- subroutine SCALE
Deck	DETER.	- subroutine DETERM
Deck	WRITE.	- subroutine WRITER
Deck	AFLUT	- subroutine FLUT
Deck	WROUT.	- subroutine WROUT
Deck	INVCX.	- subroutine INVCX
Deck	VECNR.	- subroutine VECNRM
Deck	CXDET.	- subroutine CXDET
Deck	PVECT	- subroutine VECTOR
Deck	EUCLI.	- subroutine EUCLID
\$ENTRY	GHFLUT	
	Intermediate tape data card	
	Data for first case	
	Blank card	
	Data for second case	
	Blank card	
	.	
	.	
	.	
	Data for last case	
	Blank card	
	Extra blank card or end of file	

Computer running time depends on a variety of factors. The following guidelines may be useful in estimating running time until the user has enough experience with his own type of applications to make better estimates.

A four-mode calculation (one frequency-damping combination) takes approximately 30 seconds (based on an expected average of 2 - 3 flutter points). A corresponding six-mode calculation requires about 60 to 75 seconds (4 - 5 flutter points on the average). If logical tape 9 is not available from a previous run, the running time estimate should include, in addition to the above, about L^2 minutes for each value of L for which a set of data will be written on tape 9.

APPENDIX I

FIGURES 1 - 6

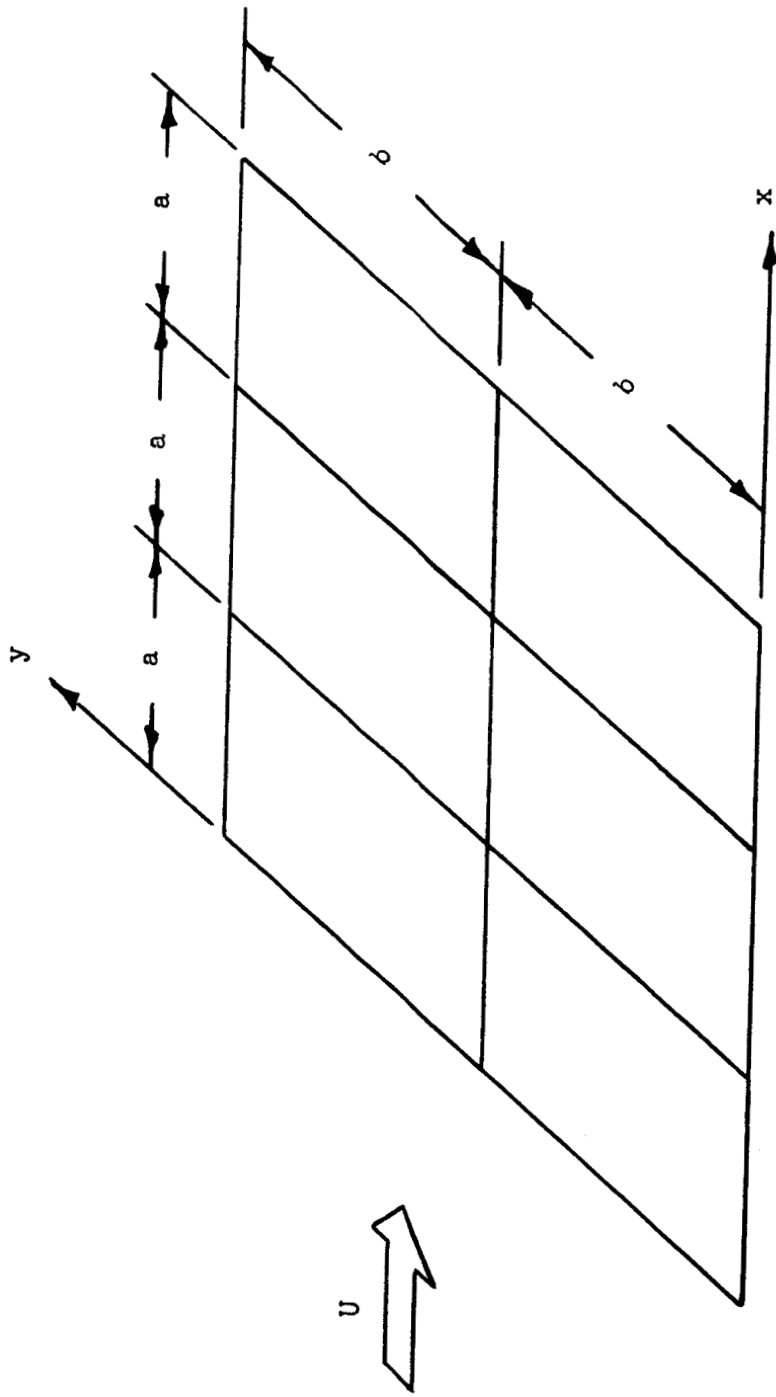


Fig. 1 - Typical Finite Panel Array

0103010203040708091011120101	0.	0.	0.
01	.0000001		
02	.25		
0304			
04	1.8225		
05	.01		
0602			
070105	2.	3.	5.
070610	7.	8.	10.
071115	12.	14.	18.
071620	22.	24.	28.
072125	32.	35.	41.
072630	47.	50.	58.
073135	66.	70.	78.
073640	86.	90.	95.
074144	110.	125.	135.
0844			
090102	1.0	1.5	
1002			
1101			
1220			
(BLANK)			
02	.5		
030401			
04	1.44		
05	.015		
0603			
090102	.7	.8	
1002			
1102			
1201			
(BLANK)			
(BLANK)			

01040709

Fig. 2a - Sample Input Data Set 1

(BLANK)	01	.00000001			
	02	1.			
	0304				
	04	1.69			
	05	0.			
	0601				
	070105	2.	3.	4.	5.
	070610	7.	8.	9.	10.
	071115	12.	14.	16.	18.
	071620	22.	24.	26.	28.
	072125	32.	35.	38.	41.
	072630	47.	50.	54.	58.
	073135	66.	70.	74.	78.
	073640	86.	90.	95.	100.
	074144	110.	125.	135.	150.
	0844				
	090103	1.0	1.2	1.4	
	1003				
	1105	.25			
	1215				
(BLANK)	04	1.44			
(BLANK)					
(BLANK)					

Fig. 2b - Sample Input Data Set 2

```

0101010203040506070809100102
01 .0000001
02 .25
0304
04 1.8225
05 .01
0601
070105 2.
070610 7.
071115 12.
071620 22.
072125 32.
072630 47.
073135 66.
073640 86.
074144 110.
0844
090101 1.5
1001
1101
1220

```

```

(BLANK )
(BLANK )

```

```

3.
4.
5.
6.
7.
8.
9.
10.
11.
12.
14.
16.
18.
20.
22.
24.
26.
28.
30.
32.
35.
38.
41.
44.
47.
50.
54.
58.
62.
66.
70.
74.
78.
82.
86.
90.
95.
100.
105.
110.
125.
135.
150.

```

Fig. 3 - Input Data Listing for Sample Output Case (Fig. 5)

INTERMEDIATE TAPE CARD

(Blank if tape is available from a previous run)

COLUMNS						
1-2	3-4	5-24	25-26	27-28	29-38	39-48
IMIN	IMAX	10 chordwise mode numbers in ascending order	Number of spanwise bays	Spanwise mode number	ϵ_x	ϵ_y

NUMBERED DATA CARDS

1-2	3-4	5-6	7-10	11-20	21-30	31-40	41-50	51-60	61-80
01				TESTR					
02				Inverse of aspect ratio					
03	Number of chordwise modes	If zero or blank, consecutive modes starting with first are used							Chordwise mode numbers in ascending order if cols. 5-6 are not blank or zero
04				Mach number squared					
05	Number of g values (blank taken as 1)			ϵ	ϵ	ϵ	ϵ	ϵ	
06	Number of chordwise bays			Nonzero will suppress print out of matrices					
07	Index of first μ on this card	Index of last μ on this card		μ	μ	μ	μ	μ	
08	Total number of entries in μ table								
09	Index of first k on this card	Index of last k on this card		k	k	k	k	k	
10	Total number of k's								
11	Option number (must be 1,2,4 or 5)			Distance from panel edge to tunnel wall in panel spans					
12	Number of nonzero terms in spanwise expansion								

Fig. 4 - Data Format for User Reference

```

M.R.I. FLUTTER PROGRAM DATE=00000000 TIME=00000000
M S E(SPAN) E(CHORD) FESTR L MMAX U UMAX SPANWISE MODE
1.3500 0.2500 0. 0. 0.10E-06 1 4 1 20 2 1

CASE A/Z 1/UPHI K G
1 1.0000 16 1.5000 0.0100

GAMMA-BAR= 6.2831853

CHORD-WISE MODE 1 2 3 4
3.1415924 6.2831853 9.4247772 12.5663706

BN(U)
1.757877 -0.483447 -0.197721 -0.095521 -0.040572 -0.008510 0.009204 0.017047 0.018142 0.015011
0.009754 0.004050 -0.000883 -0.004308 -0.005952 -0.005927 -0.004627 -0.002593 -0.000411 0.001449

INVERSE OF ELASTIC MATRIX TIMES INERTIA MATRIX
6.5702300E-03 0.
-0. 5.6835890E-04 -0. -6.7842637E-10 0.
6.3923710E-10 -0. 1.1998231E-04 0.
-0. 5.1632369E-13 -0. 3.8877094E-05

INVERSE OF ELASTIC MATRIX TIMES REAL PART AEROD MATRIX
-4.8284101E-03 -1.4912236E-02 3.4849315E-03 -5.4058474E-03
1.2898855E-03 -1.0846157E-03 -3.2866663E-03 -1.2090123E-04
6.3639989E-05 6.9382390E-04 -9.2668995E-05 -9.2554983E-04
3.1987256E-05 -8.2699311E-06 2.9989975E-04 -2.7647084E-06

INVERSE OF ELASTIC MATRIX TIMES IMAG PART AEROD MATRIX
9.1891894E-03 6.9303840E-03 1.5778516E-03 1.0541539E-03
-5.9951404E-04 8.5195765E-05 6.4234972E-04 3.7153926E-04
2.8814861E-05 -1.3560132E-04 -1.4406262E-04 -7.9678388E-06
-6.2376079E-06 2.5414165E-05 2.5818019E-06 -2.3953760E-05

MU RES. SFA SFR MU RES. SFA SFR MU RES. SFA SFR
2.00E 00 -1.56E 00 -8 -6 1.40E 01 4.43E-01 -6 -9 3.80E 01 -1.20E 00 -4 -25 7.80E 01 1.48E 00 -3 -24
3.00E 00 -2.10E 00 -7 -19 1.60E 01 1.14E 00 -5 -24 4.10E 01 -1.94E 00 -4 -24 8.20E 01 8.98E-01 -1 -22
4.00E 00 -1.28E 00 -7 -15 1.80E 01 1.12E 00 -5 -22 4.40E 01 -8.99E-01 -4 -22 8.60E 01 5.18E-01 -3 -20
5.00E 00 -6.72E-01 -7 -11 2.00E 01 1.73E 00 -5 -21 4.70E 01 -7.52E-01 -4 -21 9.00E 01 1.14E 00 -3 -20
6.00E 00 -8.77E-01 -7 -9 2.20E 01 5.44E-01 -5 -18 5.00E 01 -8.29E-01 -4 -21 9.50E 01 7.21E-01 -3 -18
7.00E 00 -6.03E-01 -7 -7 2.40E 01 1.07E 00 -5 -18 5.40E 01 6.25E-01 -4 -18 1.00E 02 8.65E-01 -3 -17
8.00E 00 8.86E-01 -6 -25 2.60E 01 7.00E-01 -5 -17 5.80E 01 1.11E 00 -4 -16 1.05E 02 9.87E-01 -3 -16
9.00E 00 7.18E-01 -6 -19 2.80E 01 -8.36E-01 -5 -20 6.20E 01 1.20E 00 -4 -16 1.10E 02 5.40E-01 -3 -14
1.00E 01 1.09E 00 -6 -17 3.00E 01 -2.23E 00 -5 -16 6.60E 01 2.11E 00 -3 -29 1.25E 02 5.69E-01 -3 -11
1.10E 01 2.27E 00 -6 -16 3.20E 01 -5.79E-01 -5 -12 7.00E 01 1.63E 00 -3 -27 1.35E 02 2.03E 00 -2 -27
1.20E 01 9.51E-01 -6 -13 3.50E 01 -1.39E 00 -4 -27 7.40E 01 1.14E 00 -3 -25 1.50E 02 1.44E 00 -2 -24
48 ITERATIONS

MU Z**1/3 LAMDA RES. SFA SFR 1/MU
7.923775 0.28041100 8.33269000E-04 5.248E-01 -6 -39 0.126202
7.923775 0.28041099 8.33268988E-04 -7.830E-01 -6 -42 0.126202
7.923775 0.28041100 8.33269000E-04 5.248E-01 -6 -39 0.126202

VECTOR R THETA COMPLEX RESIDUALS
0.097796 3.069003 -4.66E-10 7.28E-11
0.200997 6.236609 -3.82E-11 1.09E-11
0.658708 3.084337 -2.91E-11 4.55E-13
1.000000 0. -8.37E-11 -1.82E-11

CHARACTERISTIC EQUATION AT FLUTTER
1.9e83872E-09 3.5110776E-06 1.4812592E-03 1.239098E-01 1.000000E 00

```

Fig. 5 - Sample Output Listing

```

-1.9117971E-10 -3.5286575E-07 -1.5675161E-04 -1.0346376E-02
P= 1.4583E-16 Q= 1.1065E-17 P/PIA=-1.3460E-07 G/QIA= 1.1732E-07
LAMDA= 0.0008 DET= 1.3125E-16 1.3747E-17
LAMDA= 0.0008 DET= -2.1131E-11 1.8500E-12
LAMDA= 0.0008 DET= 2.1964E-11 -1.9227E-12
43 ITERATIONS

MU          Z**1/3      LAMDA      RES          SFA SFR      1/MU
27.883657  0.39191253  2.27492735E-03  -1.292E 00  -5 -34  0.035863
27.883657  0.39191253  2.27492738E-03  -1.154E 00  -5 -33  0.035863
27.883655  0.39191251  2.27492720E-03  1.063E 00  -5 -38  0.035863

VECTOR R      THETA      LAMDA      RES          SFA SFR      1/MU
0.017096     3.049019   -2.91E-10    4.37E-11
0.017926     0.455866   6.37E-12    1.09E-11
0.196811     3.121018  -1.46E-11   -8.53E-14
1.000000     0.         2.48E-10    8.90E-12

COMPLEX RESIDUALS
-2.91E-10    4.37E-11
6.37E-12    1.09E-11
-1.46E-11   -8.53E-14
2.48E-10    8.90E-12

CHARACTERISTIC EQUATION AT FLUTTER
1.9957785E-07 1.2297253E-04 1.6444874E-02 4.2113063E-01 1.0000000E 00
-8.2005277E-09 -5.1338555E-06 -7.0245779E-04 -1.3318586E-02

P=-1.3527E-14 Q= 9.4869E-18 P/PIA= 1.0882E-07 G/QIA= 1.9445E-09
LAMDA= 0.0023 DET= -1.3759E-14 5.4410E-17
LAMDA= 0.0023 DET= -2.4580E-09 9.6310E-11
LAMDA= 0.0022 DET= 2.5143E-09 -9.8841E-11
35 ITERATIONS

MU          Z**1/3      LAMDA      RES          SFA SFR      1/MU
50.830359  0.69252619  1.25518787E-02  -7.530E-01  -4 -32  0.019673
50.830359  0.69252619  1.25518787E-02  -7.530E-01  -4 -32  0.019673
50.830360  0.69252620  1.25518790E-02  7.288E-01  -4 -33  0.019673

VECTOR R      THETA      LAMDA      RES          SFA SFR      1/MU
0.006969     0.199852   -5.18E-09   -1.30E-09
0.070176     2.956780   4.40E-09   -5.49E-10
1.000000     0.         -2.91E-11   1.14E-11
0.035277    -3.151118  1.56E-07   5.86E-09

COMPLEX RESIDUALS
-5.18E-09   -1.30E-09
4.40E-09   -5.49E-10
-2.91E-11   1.14E-11
1.56E-07    5.86E-09

CHARACTERISTIC EQUATION AT FLUTTER
2.1021598E-06 7.2234060E-04 5.3622967E-02 7.6282816E-01 1.0000000E 00
-8.7196063E-08 -2.5618670E-05 -1.7293702E-03 -1.67355561E-02

P=-1.4753E-13 Q= 2.9833E-15 P/PIA=-4.3347E-08 G/QIA=-2.4642E-08
LAMDA= 0.0126 DET= -1.6315E-13 2.9936E-15
LAMDA= 0.0128 DET= 6.9688E-08 -2.5505E-09
LAMDA= 0.0123 DET= -6.6431E-06 2.4120E-09

```

Fig. 5 - (Concluded)

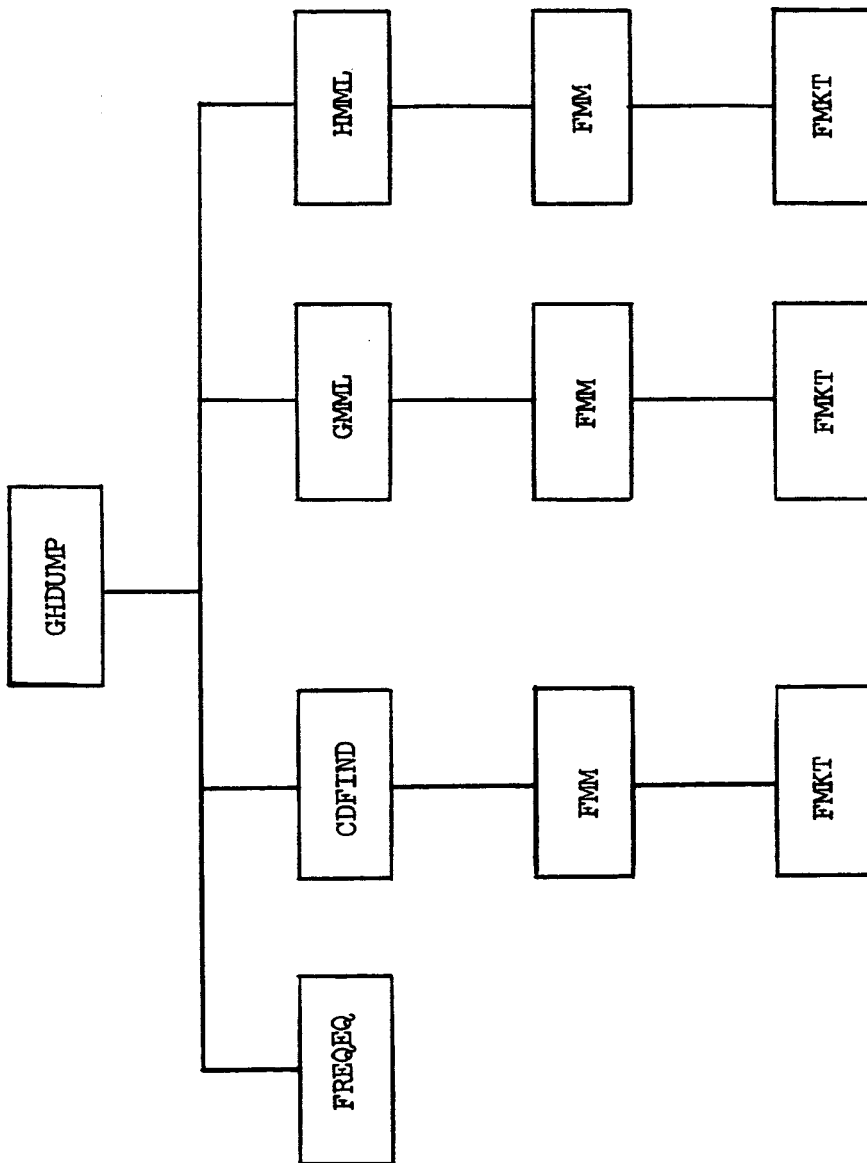


Fig. 6a - Hierarchy of Subroutines

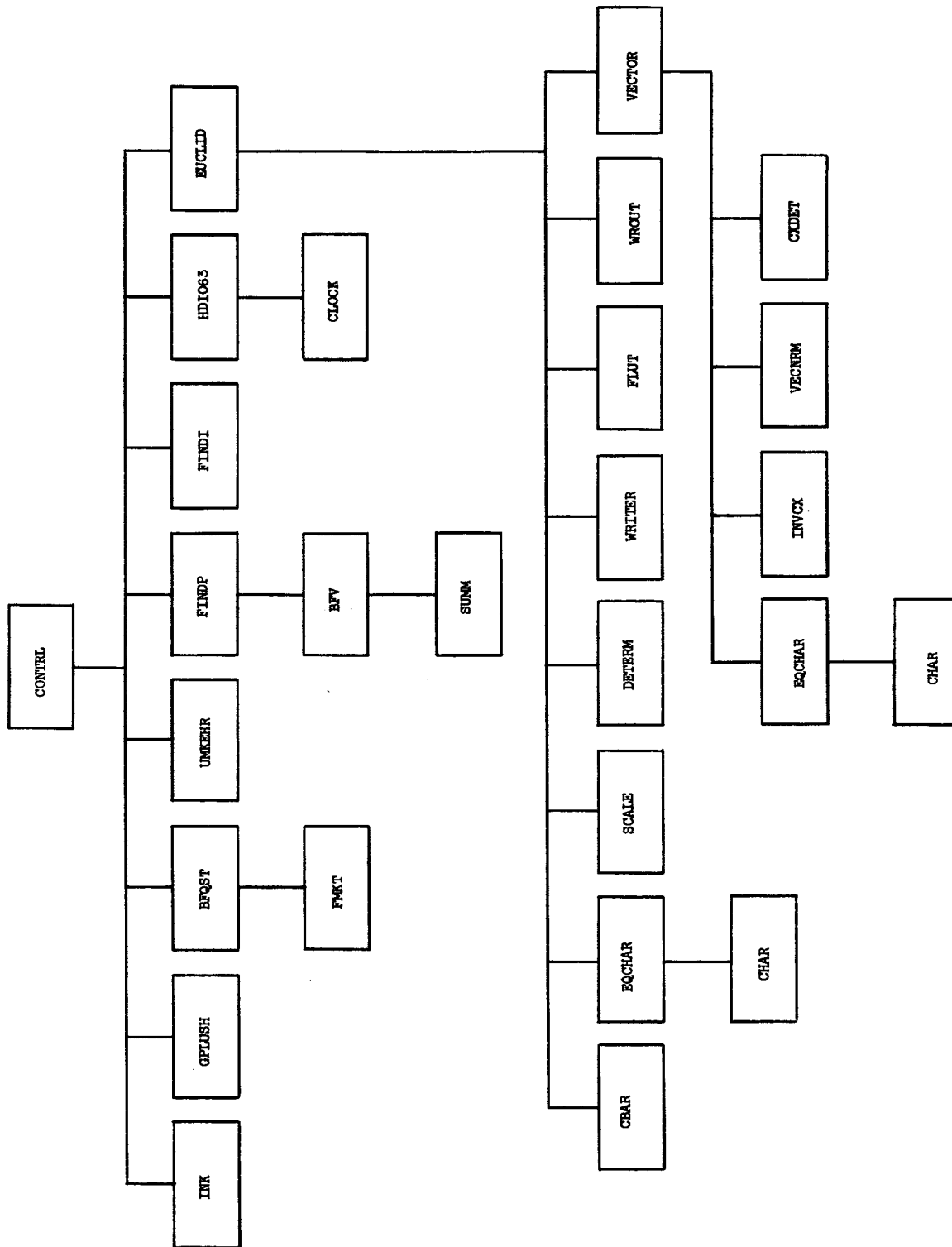


Fig. 6b - Hierarchy of Subroutines (Concluded)

APPENDIX II

DESCRIPTION OF SCALING ROUTINES

Experience with an earlier version of the program showed that the range of magnitudes of Sylvester's resultant of the real and imaginary parts of the characteristic equation can be extremely wide. The object of the program is to find μ values which will cause the resultant to vanish. Yet for the initial values read into the μ table the resultant may be so large as to cause overflow. Hence scaling has been used to keep these numbers in a range that the machine can handle. Binary scaling was used to avoid any loss of accuracy in scaling.

Two kinds of scale factors are used. One of these scales the roots of the characteristic equation; the other scales the reduced determinant. The scale factor applied to the roots of the characteristic equation is based on the real part of the equation and is chosen so that the magnitudes of the non-zero polynomial coefficients cluster around unity. The scale factor applied to the determinant is the product of several scale factors -- one for each row of the determinant except the last -- and is likewise chosen so that the calculated resultant is of the order of magnitude of unity.

The program prints the base 2 logarithms of these two scale factors along with a scaled resultant value. The logarithms of the scale factor for the characteristic equation and the determinant are labeled SFA and SFR, respectively. The true value of the resultant can be obtained from the printed (scaled) resultant from

$$RES_{\text{true}} = RES_{\text{scaled}} \cdot 2^{n^2\text{SFA}+\text{SFR}}$$

where n is the number of modes used in the analysis. No attempt is made to print out the true resultant since much of the time this number is outside the range of magnitudes which the machine can handle.

APPENDIX III

INTERMEDIATE TAPE FORMAT

The program obtains certain essential information from a binary intermediate tape. The program references this tape as logical tape 9. If no previously generated tape containing the required data is mounted, an input card must be punched which will cause the program to generate the tape at the beginning of the current run.

Information on logical tape 9 consists of one or more sets of data, one for each value of L from IMIN to IMAX. The upper bound for IMAX is 4 in the present program. The symbol L represents the number of chordwise bays in the panel array under study. Each set of data on the tape consists of the following sequence of seven records:

<u>Record</u>	<u>Length</u>	<u>List</u>	<u>Description</u>
1	16 words	L (MODE(J), J=1,10) NSP NGBAR ε chord ε span 16	Number of chordwise bays Chordwise mode numbers Number of spanwise bays Spanwise mode number Chordwise stiffness parameter Spanwise stiffness parameter Intervals used in integration
2	77 words	(GAMMA(J), J=1,11) ((C(M,K), M=1,11), K=1,6)	Frequencies γ_j , and $\bar{\gamma}$ $C_{m,\bar{\ell}}$
3	66 words	((D(M,K), M=1,11), K=1,6)	$D_{m,\bar{\ell}}$
4	100 words	((DJAY(MB,M), MB=1,10), M=1,10)	$J_{\bar{m},m}$
5	100 words	((CAY(MB,M), MB=1,10), M=1,10)	$K_{\bar{m},m}$
6	100 words	((ARE(MB,M), MB=1,10), M=1,10)	$R_{\bar{m},m}$
7	8,000 words	((GH(MB,M,K), MB=1,10), M=1,10), K=1,80)	$\sum_{\ell=1}^L [G_{\bar{m},m,\ell}(K\Delta\varphi) + H_{\bar{m},m,\ell-1}(K\Delta\varphi)]$

In the arrays GAMMA, C and D the subscript value of 11 refers to the spanwise mode while subscripts 1 - 10 refer to chordwise modes.

In order to form the integrals $I_{\bar{m},m,u}$ (See [1], page 52) it is necessary to integrate the products of $P_u(\ell-1+\varphi)$ times $G_{\bar{m},m,\ell}(\varphi)$ and $H_{\bar{m},m,\ell}(\varphi)$.

To conserve storage the sum of $G_{\bar{m},m,\ell}^-$ and $H_{\bar{m},m,\ell}^-$ is generated and stored. For $\ell = L$, note that $H_{\bar{m},m,\ell}^-$ is zero. The subscripts of $GH(MB,M,K)$ correspond respectively to \bar{m},m and an index representing the distance from the panel array leading edge measured in terms of the increment used in the numerical integration. Thus since $\Delta\varphi = 1/16$, K ranges from 1 to $16L$. Since the program does not presently have the capability of analyzing 5-bay configurations, the dimension of the array GH could be reduced to $GH(10,10,64)$ to gain additional storage space for the program.

Following the data corresponding to $L = L_{\max}$, the tape has one 16-word record indicating $L = 5$. This is presently used to signal end of file.

When data for a flutter case have been read, the program searches logical tape 9 for the data set corresponding to the value of L specified on the 06 data card.

APPENDIX IV

EXPLANATION OF EXCEPTIONAL COMMON STATEMENTS

Routines SUMM, FMKT, FMM, GMML and HMML have short COMMON tables since these routines reference only a few symbols near the beginning of the COMMON list.

In routines GMML, HMML, FREQEQ, CDFIND and GHDUMP an "O" is used in place of "L" in the COMMON table since L is used either in argument lists or as a DO loop index.

In routines FREQEQ and GHDUMP an "ON" is used in place of "BN" since BN is used in FREQEQ as a scratch variable.

Since data generated by GHDUMP are preserved on logical tape 9, and not in COMMON storage, the COMMON table for the overlay link containing GHDUMP does not agree with that of the later overlay links. In particular, the later routines do not contain the arrays CC, CD, DD.

APPENDIX V

LIST OF COMMON AND ARGUMENT LIST QUANTITIES ALTERED BY VARIOUS SUBPROGRAMS

Subroutine GHDUMP and the subprograms it calls communicate with the rest of the program through logical tape 9 and not through COMMON storage. Therefore, the list below is divided to show these routines separate from the other routines.

Subroutines in Overlay Containing GHDUMP

GHDUMP - reads MODE (1 - 10), NSP, NGBAR, EPY, EPX and minimum and maximum values of L. It also defines NODP = 16.

FREQEQ - computes FREQ, QMM arrays.

CDFIND - computes DJAY, CAY, ARE, C, D, CC, CD, DD arrays.

GMLL - computes GMM.

HMML - computes HMM.

Subroutines not in Overlay Containing GHDUMP

CONTRL - is effectually the main routine. It does not alter any quantities.

INK - is the input routine. Quantities defined are: EMSQ, EM, BSQ, BETA, BFOR, S, L, MMAX, NNN, A, TESTR, NEWP, NEWGAM, NEWC, NEWEIV, NEWMOD, NNST, NEWGMB, NEWDPH, MAXAL, NK, NG, and the arrays ALPHA, CKAY, GT, MODE, and SAVE.

GPLUSH - reads appropriate data from logical tape 9 into the program. This includes NSP, NGBAR, EPY, EPX, NODP, and the arrays MODE, GAMMA, C, D, DJAY, CAY, ARE and GH.

BFQST - defines Q, SS, T, BN, BUF.

UMKEHR - inverts matrix R in argument list.

PFIND - defines PREAL, PIMAG.

IFIND - defines AER, AEI, EYER, EYEI.

HD1063 - increments NSEQ.

EUCLID - computes array REST in the argument list.

CBAR - defines array CR in the argument list.

EQCHAR - defines array PRE in the argument list.

CHAR - defines array D in the argument list.

SCALE - defines NS, KRUB and array RR in the argument list.

DETERM - redefines NSUM, RES in the argument list.

FLUT - defines U, RES in the argument list.

INVCX - inverts complex matrix R in argument list.

CXDET - computes X, Y in argument list.

VECTOR - redefines array C in argument list.

VECNRM - defines array VM in argument list.

APPENDIX VI

TABLE OF PROGRAM SYMBOLS

<u>Program Symbol</u>	<u>Noncommon Reference</u>	<u>Report Notation</u>	<u>Comment</u>
A		A	Twice the distance from panel edge to wind tunnel wall.
AEI(MB,M)		$\text{Im}(E^{-1}C)$	See Section III.
AER(MB,M)		$\text{Re}(E^{-1}C)$	See Section III.
ALPHA(J)			Table of μ values.
ARE(MB,M)		$R_{\bar{m},m}$	See page 12, [1]*.
BETA		β	$\sqrt{M^2-1}$
BFOR		β^4	
BN(N)		$B_{n,u}$	Coefficients of spanwise mode expansion. See Appendix E, [1].
BSQ		β^2	
BUF(N)		$B_{n,u}F(u)$	See Appendix E, [1].
C(M,L)		$C_{m,\ell}$	See pages 43 - 44, [1].
CAY(MB,M)		$K_{\bar{m},m}$	See page 4, [1].
CC(M,N)		$\sum C_{m,\ell} C_{n,\ell}$	Summation over chordwise bays.
CD(M,N)		$\sum C_{m,\ell} D_{n,\ell}$	Summation over chordwise bays.
CK		k	Reduced frequency.
CKAY(J)			Table of k values.
CR(MB,M)	EUCLID	$\text{Re}(\bar{C})$ and $\text{Im}(\bar{C})$	Flutter matrix. See Section III.
D(M,L)		$D_{m,\ell}$	See pages 43 - 44, [1].
DD(M,N)		$\sum D_{m,\ell} D_{n,\ell}$	Summation over chordwise bays.
DJAY(MB,M)		$J_{\bar{m},m}$	See page 4, [1].
EIJ(MB,M)		$E^{-1}J$	Matrix product $EINV * DJAY$
EINV(MB,M)		$E^{-1} = (E_{\bar{m},m}^{-1})^{-1}$	See page 15, [1].
EIR(MB,M)		$E^{-1}R$	Matrix product $EINV * ARE$
EM		M	Mach number.
EMSQ		M^2	
EPX		ϵ_y	Torsional proportionality constant (Section II).
EPY		ϵ_x	Torsional proportionality constant (Section II).
EYEI(MB,M)		$S \cdot R_{\bar{m},m}$	See page 15, [1].
EYER(MB,M)		$S \cdot A_{\bar{m},m}$	See page 15, [1].*

* $R_{\bar{m},m}$ and $A_{\bar{m},m}$ are misprinted in [1]. They should read as follows:

$$R_{\bar{m},m} = \int_0^L \bar{\phi}_m^{(x)}(x) \bar{\phi}_m(x) dx$$

$$\left\{ A_{\bar{m},m} \right\} = \text{Real} \left\{ \sum_u B_{n,u} F(u) I_{\bar{m},m,u} / S \right\}$$

<u>Program Symbol</u>	<u>Noncommon Reference</u>	<u>Report Notation</u>	<u>Comment</u>
FREQ(M)			Frequencies of all modes in range of interest.
G		g	Structural damping coefficient.
GAMMA(M)		γ_m	Frequencies of modes used. See pages 40 - 41, [1].
GH(MB,M,K)			See Appendix III.
JEST(J)	EUCLID		Scale factor table (SFR table).
KRUB	EUCLID		Scale factor SFA.
KIT	EUCLID		Count of iterative interpolations needed to find flutter.
L		L	Number of chordwise bays.
LEST(J)	EUCLID		Scale factor table (SFA table).
MMAK			Number of chordwise modes.
MODE(J)			Chordwise mode numbers.
NCASE			Edge condition option number. See Section V.
NGBAR			Spanwise mode number.
NNN		U_{max}	Number of terms in spanwise mode expansion.
NODP			Constant = 16.
NS	EUCLID		Scale factor SFR.
NSP			Number of spanwise bays.
PIMAG		$\text{Im}(P_u(\xi))$	See page 10, [1].
PREAL		$\text{Re}(P_u(\xi))$	See page 10, [1].
PRE(J)	EUCLID		Characteristic equation.
Q		Q	See page 4, [1].
QMM(M)		q_m	See pages 39 - 41, [1].
REST(J)	CONTRL		Resultant table.
S		s	Reciprocal of aspect ratio.
SFOR		s^4	
SQK		k^2	
SQS		s^2	
SS		S	See page 4, [1].
T		T	See page 4, [1].
TESTR			Flutter precision control parameter. See Appendix IX.

APPENDIX VII

CHARACTERISTIC EQUATION ROUTINE

To set up the Sylvester determinant it is necessary to calculate the characteristic polynomial of the flutter matrix. An earlier version of the program made use of the Danilewski method [8], which was found to be numerically unstable [7]. The present routine calculates the polynomial in two steps. The flutter matrix is first converted to the almost triangular, or Hessenberg, form via a series of numerically stable operations [7].* The coefficients of the characteristic polynomial are then obtained using a recurrence relation derived from the general induction formula given in [9]. The two-step process proceeds as follows.

The flutter matrix is a full $m \times m$ matrix which is represented as

$$F = \begin{pmatrix} A_{11} & A_{12} & A_{13} & \dots & A_{1m} \\ A_{21} & \dots & \dots & \dots & A_{2m} \\ \cdot & & & & \cdot \\ \cdot & & & & \cdot \\ \cdot & & & & \cdot \\ \cdot & & & & \cdot \\ \cdot & & & & \cdot \\ A_{m1} & \dots & \dots & \dots & A_{mm} \end{pmatrix}$$

This matrix is first transformed to the Hessenberg form

$$S = \begin{pmatrix} s_{11} & s_{12} & s_{13} & \dots & s_{1m} \\ s_{21} & s_{22} & \dots & \dots & s_{2m} \\ 0 & s_{32} & s_{33} & \dots & \cdot \\ 0 & 0 & & & \cdot \\ \cdot & \cdot & & & \cdot \\ \cdot & \cdot & & & \cdot \\ \cdot & \cdot & & & \cdot \\ \cdot & \cdot & & & \cdot \\ 0 & 0 & \dots & \dots & s_{m,m-1} & s_{mm} \end{pmatrix}$$

* The operations consist in similarity transformations which do not alter the characteristic polynomial.

Now let $d_{n,p}$ be the coefficient of λ^p in the characteristic polynomial of the $n \times n$ submatrix taken from the upper left hand corner of S . The recurrence relation for computing the coefficients is

$$d_{n,p} = d_{n-1,p-1} - \sum_{k=1}^{n-p} v_{n-1,n-k+1} s_{n-k+1,n} d_{n-k,p} \quad (\text{VII-1})$$

where $d_{j,j} = 1$ (including $j = 0$)

$$d_{j,k} = 0 \quad \text{for } j < k$$

$$d_{j,k} = 0 \quad \text{for } k < 0$$

$$d_{j,j-1} = - \sum_{i=1}^m s_{i,i}$$

$$v_{j-1,j} = 1$$

$$v_{j,k} = \prod_{i=k}^j s_{i+1,i}$$

An $m \times m + 1$ d matrix is obtained by application of Eq. VII-1 through the ranges

$$n = 1, 2, 3 \dots m$$

$$p = 0, 1, 2 \dots m$$

The $m + 1$ elements of the m^{th} row of the d matrix are the required coefficients of the characteristic polynomial of the $m \times m$ matrix F .

APPENDIX VIII

ADMISSIBLE VALUES FOR THE TORSIONAL RESTRAINT PROPORTIONALITY FACTOR ϵ_y

In the case of the finite span array (Option 1) a restriction is imposed on ϵ_y by the sine series expansion of the spanwise deflection shape. The coefficients in the expansion are of the form*

$$B_{n,u} = \frac{2 B^3}{B \bar{\gamma}_n^{-u} \pi^4} \bar{\Phi}$$

where

- 2B = wavelength of expansion = $\lambda + 2N$
- $\lambda = sL/2M$
- s = inverse of aspect ratio
- L = number of chordwise panels
- M = Mach number
- N = number of spanwise panels
- $\bar{\gamma}_n$ = frequency of spanwise mode
- n = number of the spanwise mode
- u = summation index
- $\bar{\Phi}$ = a transcendental function whose form is not relevant to this discussion

The frequency $\bar{\gamma}_n$ depends on ϵ_y and N whereas B depends on N, s, L and M. It is obviously possible to choose values for the above quantities such that the denominator $B \bar{\gamma}_n^{-u} \pi^4$ vanishes, in which case the computer program will give an erroneous result. An inadvertent choice of such a combination of parameters will be indicated in the print-out of the expansion coefficients.

The restriction on ϵ_y (or more precisely on the combination ϵ_y, N, s, L, M) could be eliminated by causing the program to detect such a situation and artificially set B to a somewhat greater value. It is felt, however, that this modification is unwarranted because of the small probability that the situation will occur.

For the array with span extending to infinity (Option 2) the expansion coefficients contain the term $\bar{\gamma}_n^{-u} \pi^4$ in the denominator which vanishes for $\epsilon_y \equiv 0; u = n$. This degenerate case is taken care of by program logic. However, it is recommended that values $0 < \epsilon_y \ll 1$ be avoided to avert possible numerical difficulties associated with a vanishingly small (but not precisely zero) value of the denominator.

* See [1], Appendix E, Equation (E-7).

APPENDIX IX

DESCRIPTION OF A PROGRAM CHECK AND THE PRECISION FACTOR TEST

The purpose of this Appendix is to discuss the program check denoted in the output listing by the quantities P, Q, P/PLA and Q/QIA (following the characteristic equation print out), and the precision factor TESTR.

The basis for the check is the fact that, at flutter, the real and imaginary characteristic polynomials of the flutter matrix must have a common root. Referring to Section III, the flutter matrix may be written as

$$\left\{ \lambda I - \mu \beta k^2 (1-jg) E^{-1} J + (1-jg) E^{-1} C \right\}$$

where $\lambda = Z\beta(1+g^2)/24$ (as handled in the program). Since μ and λ can be considered independent variables with all other quantities fixed, the characteristic polynomials may be written as

$$\text{Real polynomial} = P(\lambda, \mu) = a_m \lambda^m + \dots + a_1 \lambda + a_0$$

$$\text{Imag. polynomial} = Q(\lambda, \mu) = b_{m-1} \lambda^{m-1} + \dots + b_1 \lambda + b_0$$

where the a_i and b_i are real-valued functions of μ only.

Let $\lambda_F = \lambda$ at flutter

$\mu_F = \mu$ at flutter

Then the check criteria stated above may be written as

$$P(\lambda_F, \mu_F) = Q(\lambda_F, \mu_F) = 0$$

The quantities appearing in the program check can now be defined as follows:

$$P = P(\lambda_F, \mu_F)$$

$$Q = Q(\lambda_F, \mu_F)$$

$$\frac{P}{PLA} = \frac{P(\lambda_F, \mu_F)}{\lambda_F \left. \frac{\partial P}{\partial \lambda} \right|_{\lambda_F, \mu_F}}$$

$$\frac{Q}{QIA} = \frac{Q(\lambda_F, \mu_F)}{\lambda_F \left. \frac{\partial Q}{\partial \lambda} \right|_{\lambda_F, \mu_F}}$$

Now P/PIA and Q/QIA represent the Newton-Raphson recurrence relation for iteration of the polynomials with respect to λ . For example, if P is iterated holding μ fixed at μ_F , and λ_F is the current estimate for λ , then the Newton-Raphson next approximation for λ is $\lambda_F (1 - P/PIA)$.

The quantities P/PIA and Q/QIA cannot be interpreted as a percentage error. However, experience with the computer program has shown that values less than about 10^{-3} imply at least four-digit accuracy in the computed values of $1/\mu$ and $z^{1/3}$. On the other hand, values of the order 10^{-1} imply breakdown of the computational techniques employed.

The input parameter TESTR is an upper bound on the acceptable decimal per cent error in μ . It is used in the program as follows. In searching for a zero of the Sylvester determinant the current bracketing values of μ are used to interpolate for the next approximation for μ . If

μ_1 = current μ value for which determinant is positive

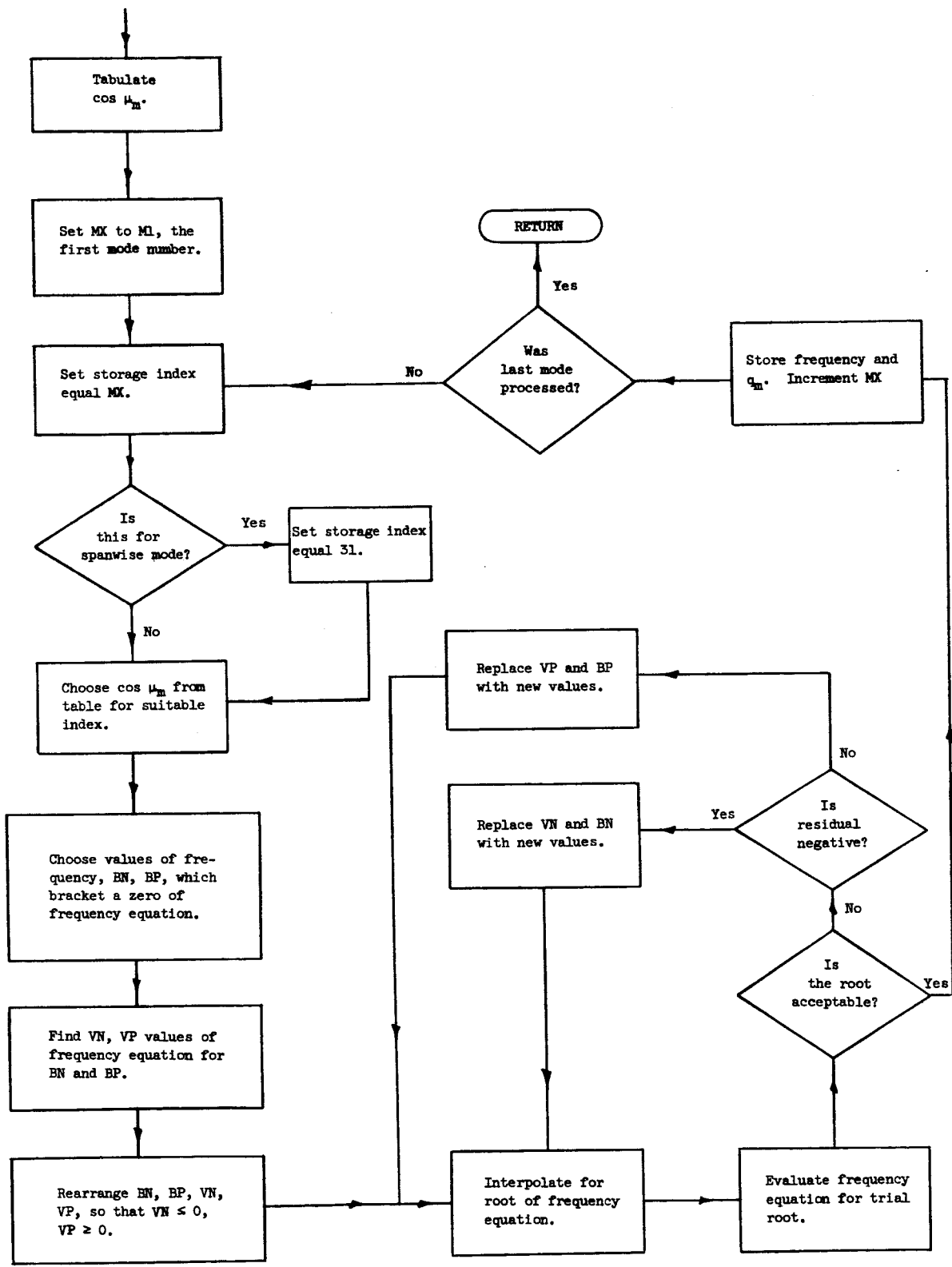
μ_2 = current μ value for which determinant is negative

μ_1 and μ_2 are used to interpolate for the next approximation μ_E . If the absolute value of the range $\mu_1 - \mu_2$ is less than or equal to μ_E times TESTR, μ_E is accepted as the flutter μ .

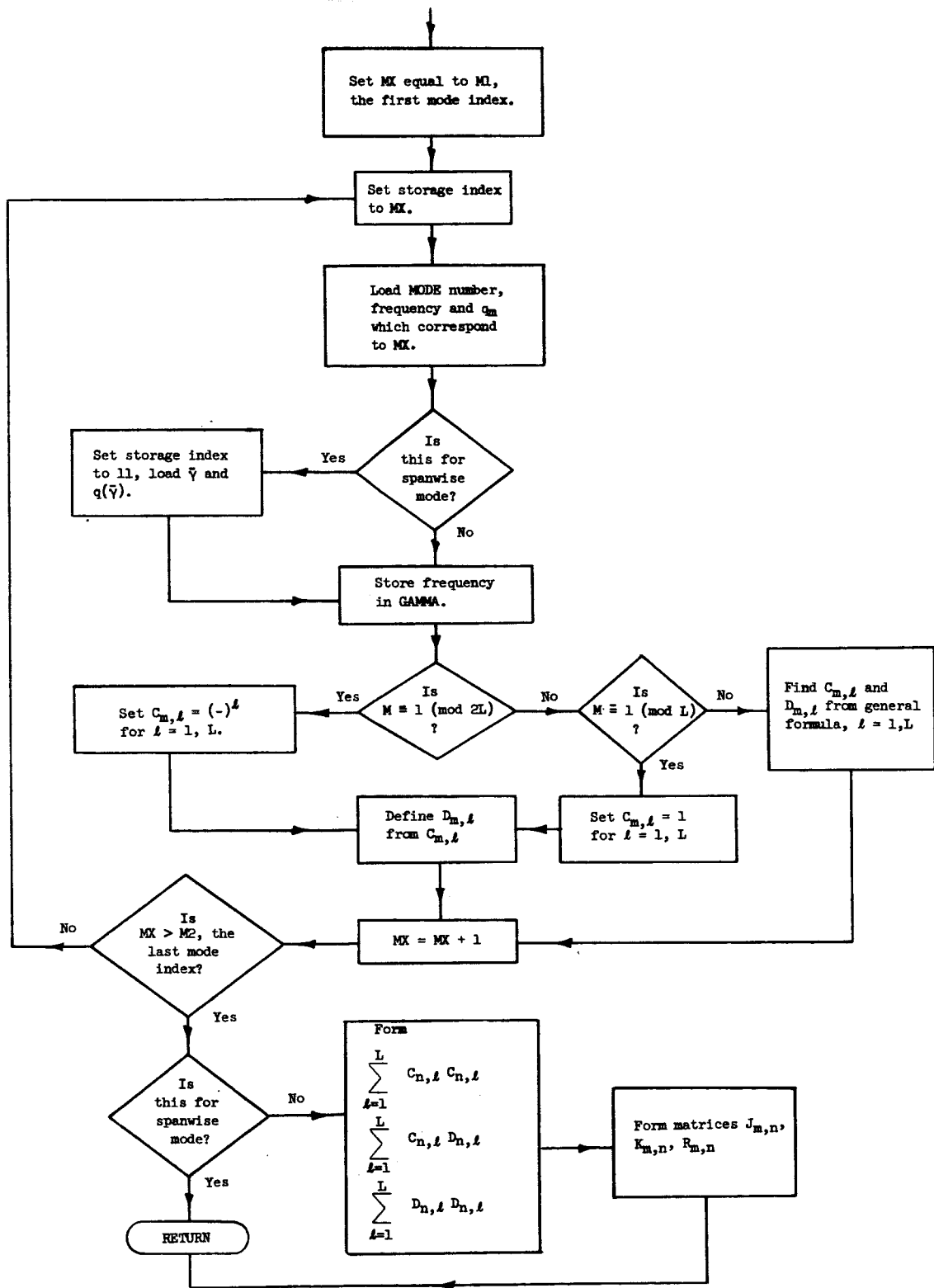
In application of the computer program a value of 10^{-7} has been used for TESTR. The effect of using other values has not been explored.

APPENDIX X

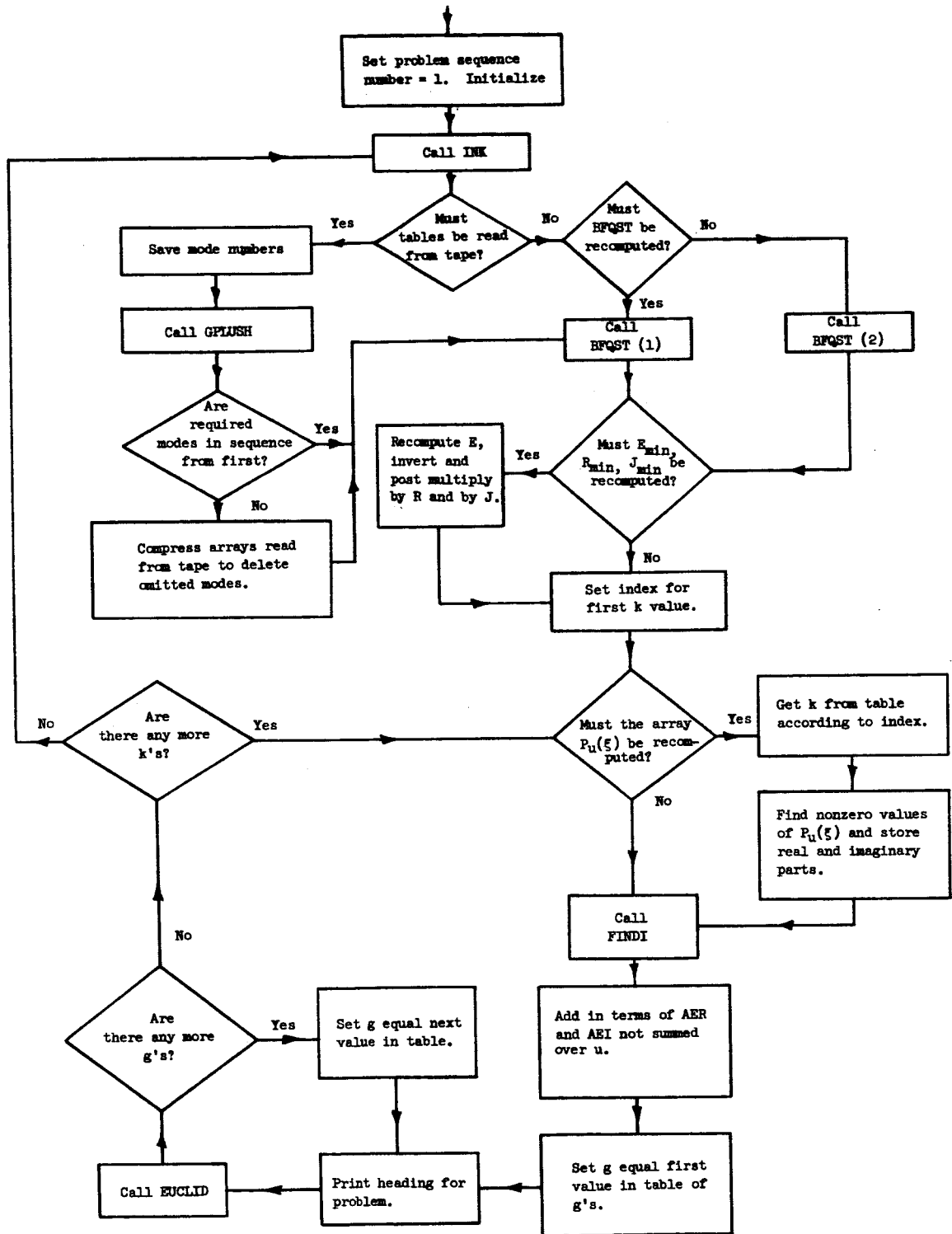
FLOW DIAGRAMS



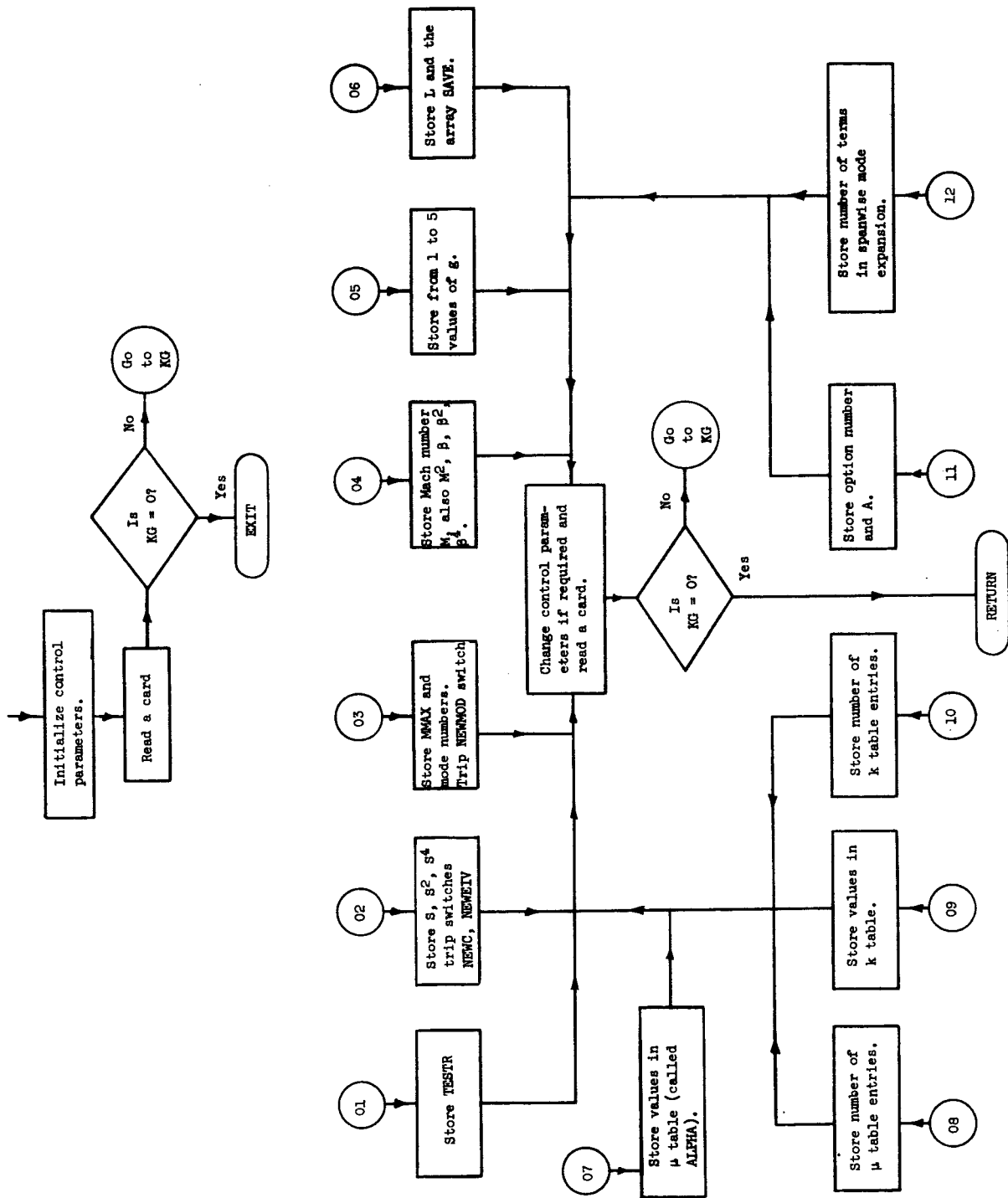
Subroutine FREQEQ



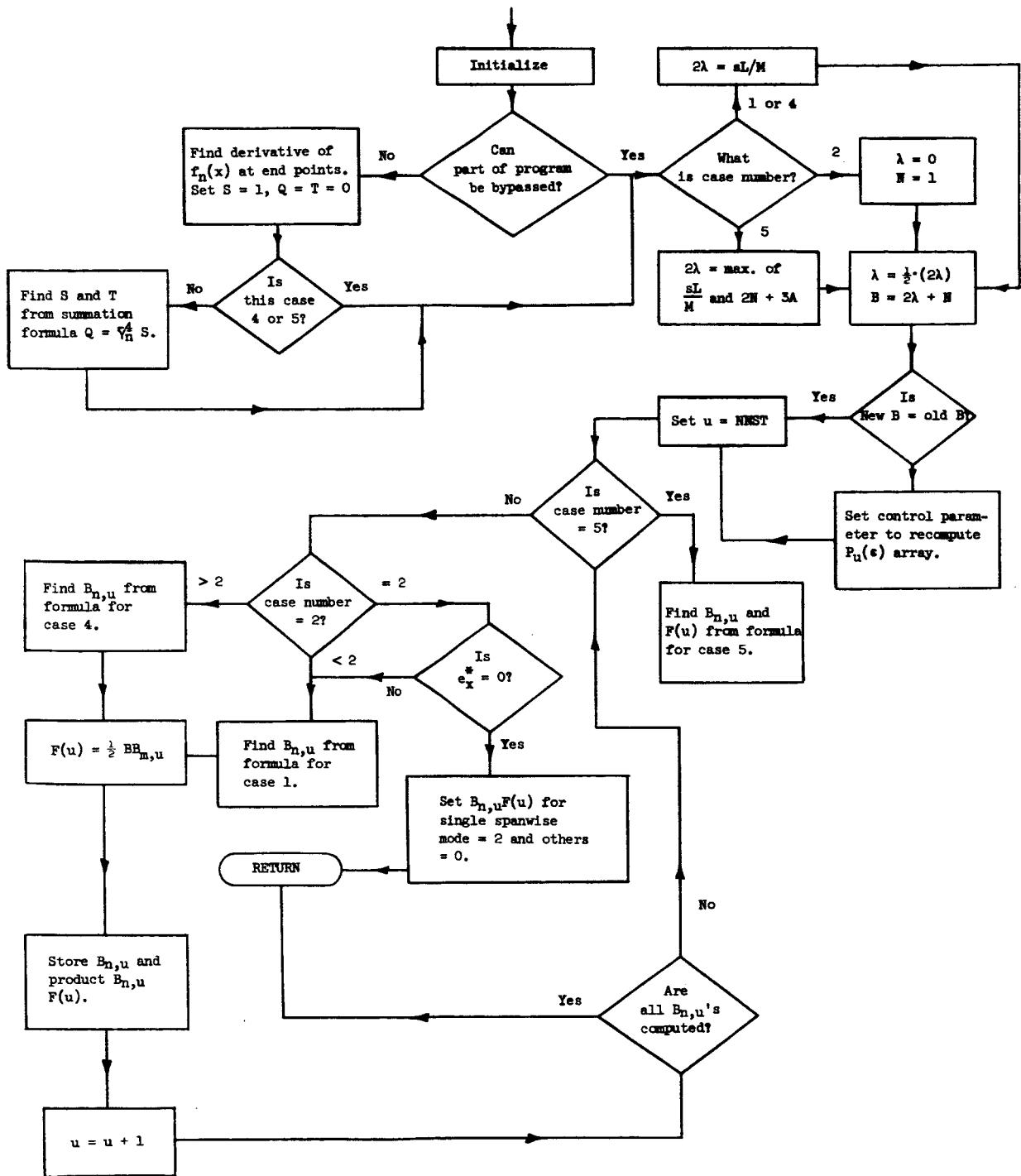
Subroutine CDFIND



Subroutine CONTRL

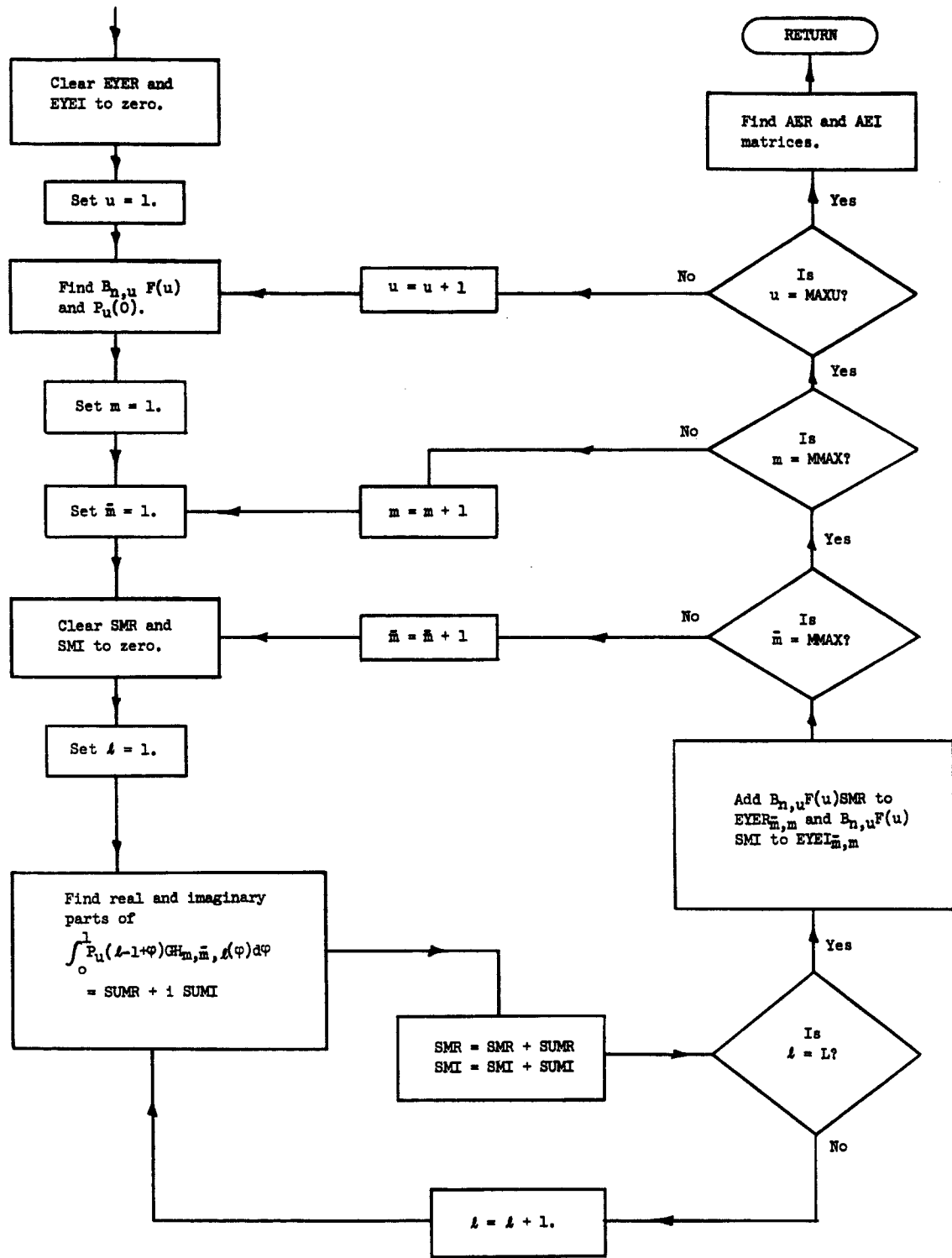


Subroutine INK

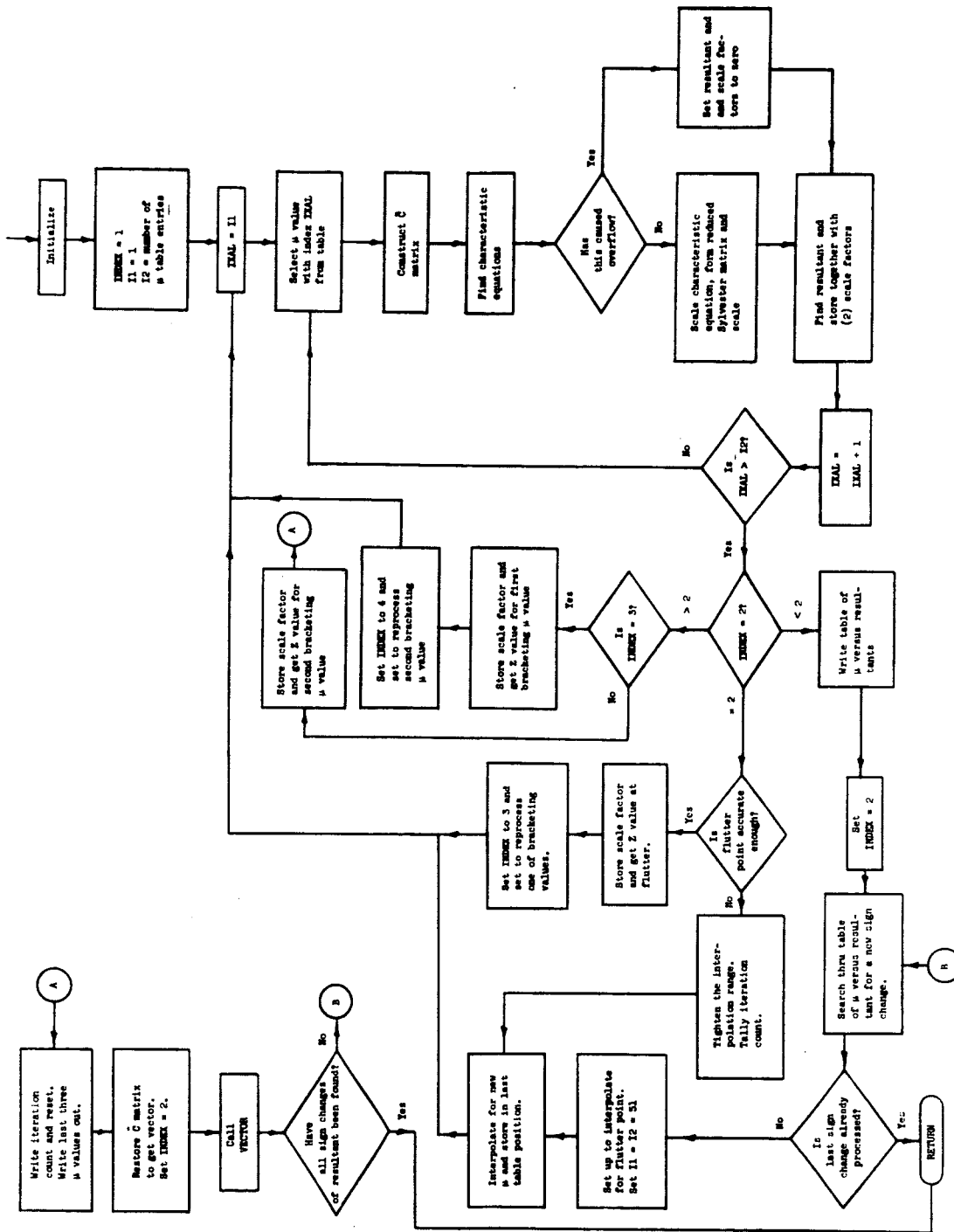


Note: ϵ_x and ϵ_y in the program are interchanged with reference to the notation in NASA CR-80 (Ref (1)).

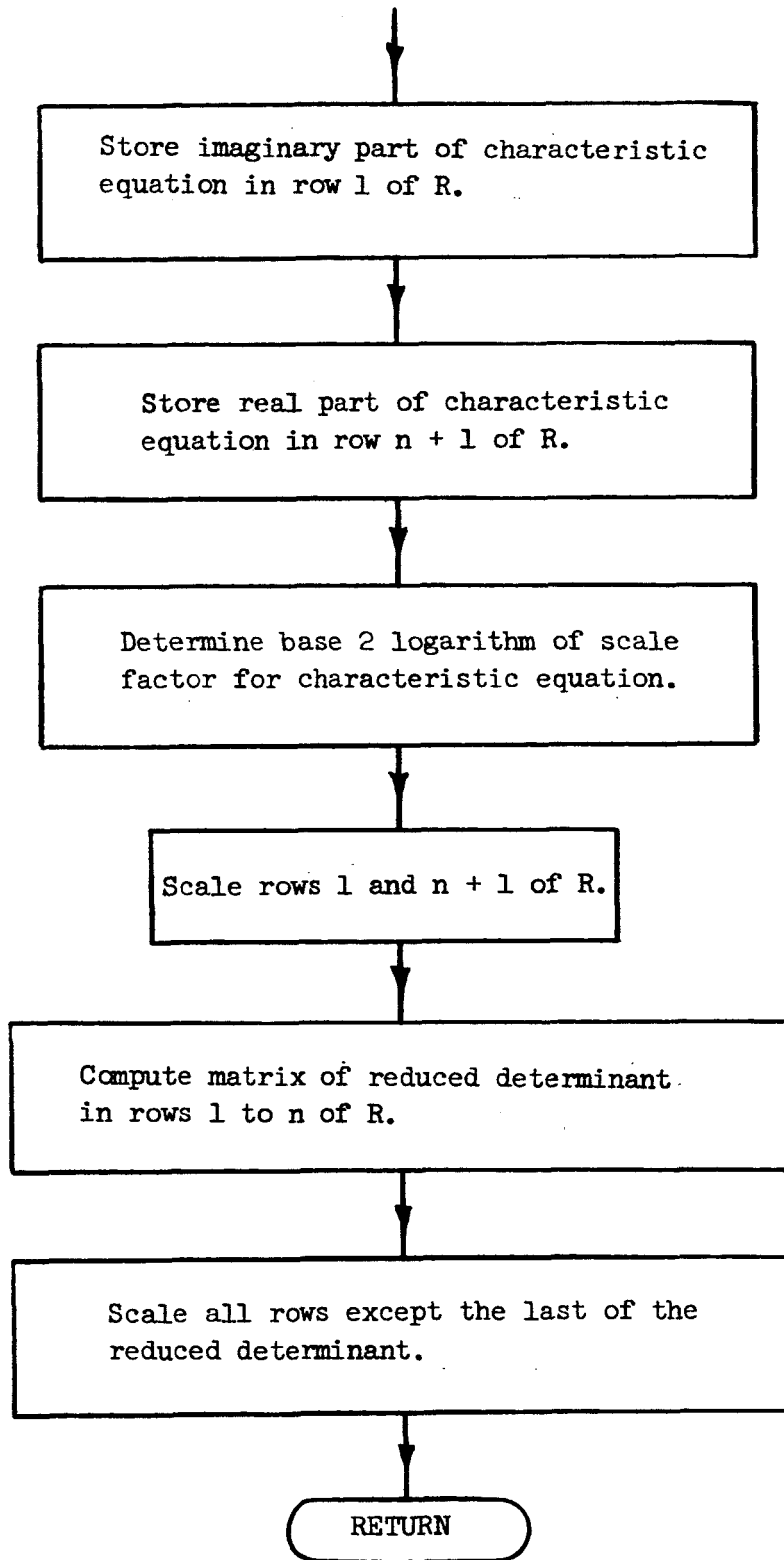
Subroutine BFGST



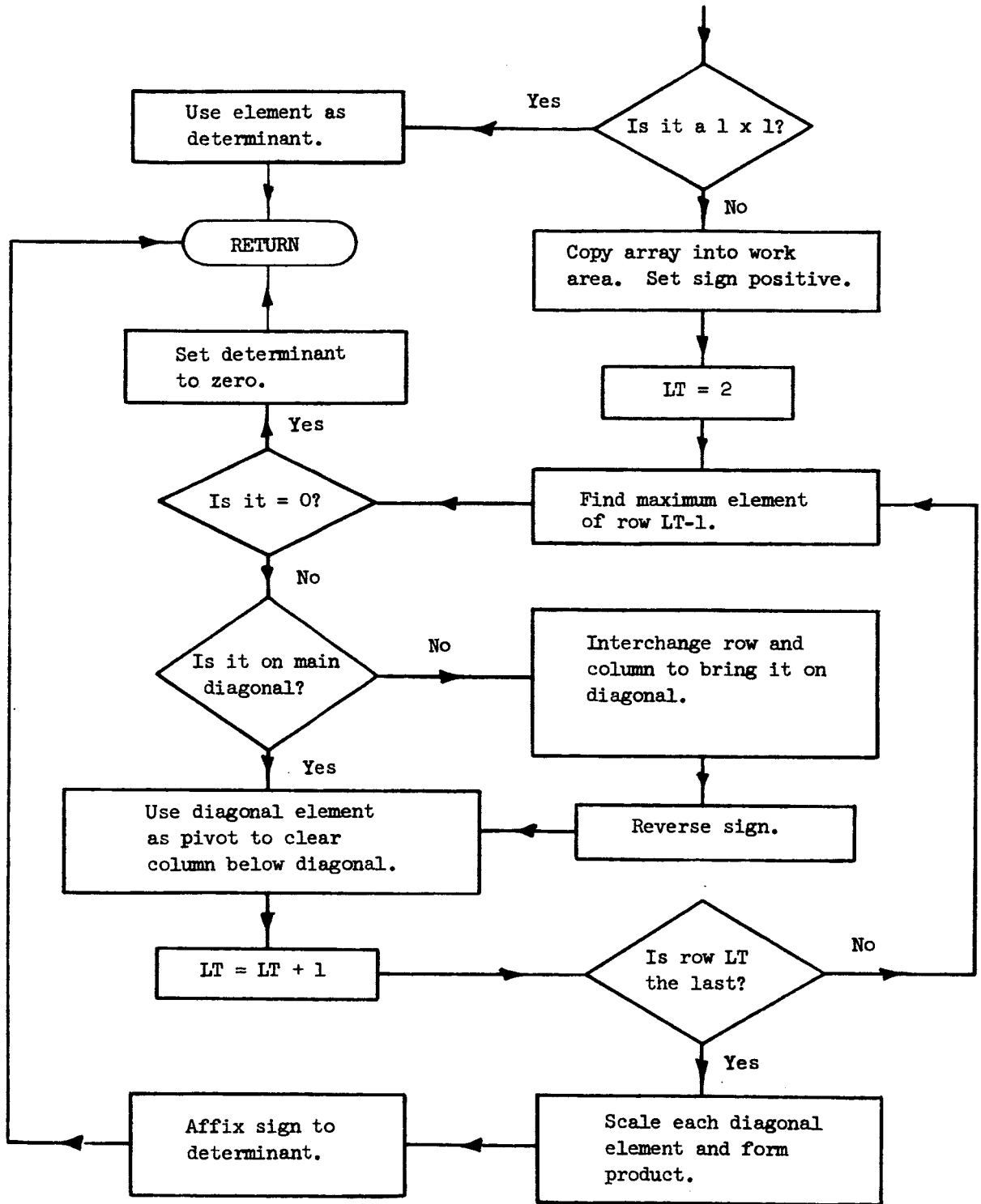
Subroutine FINDI



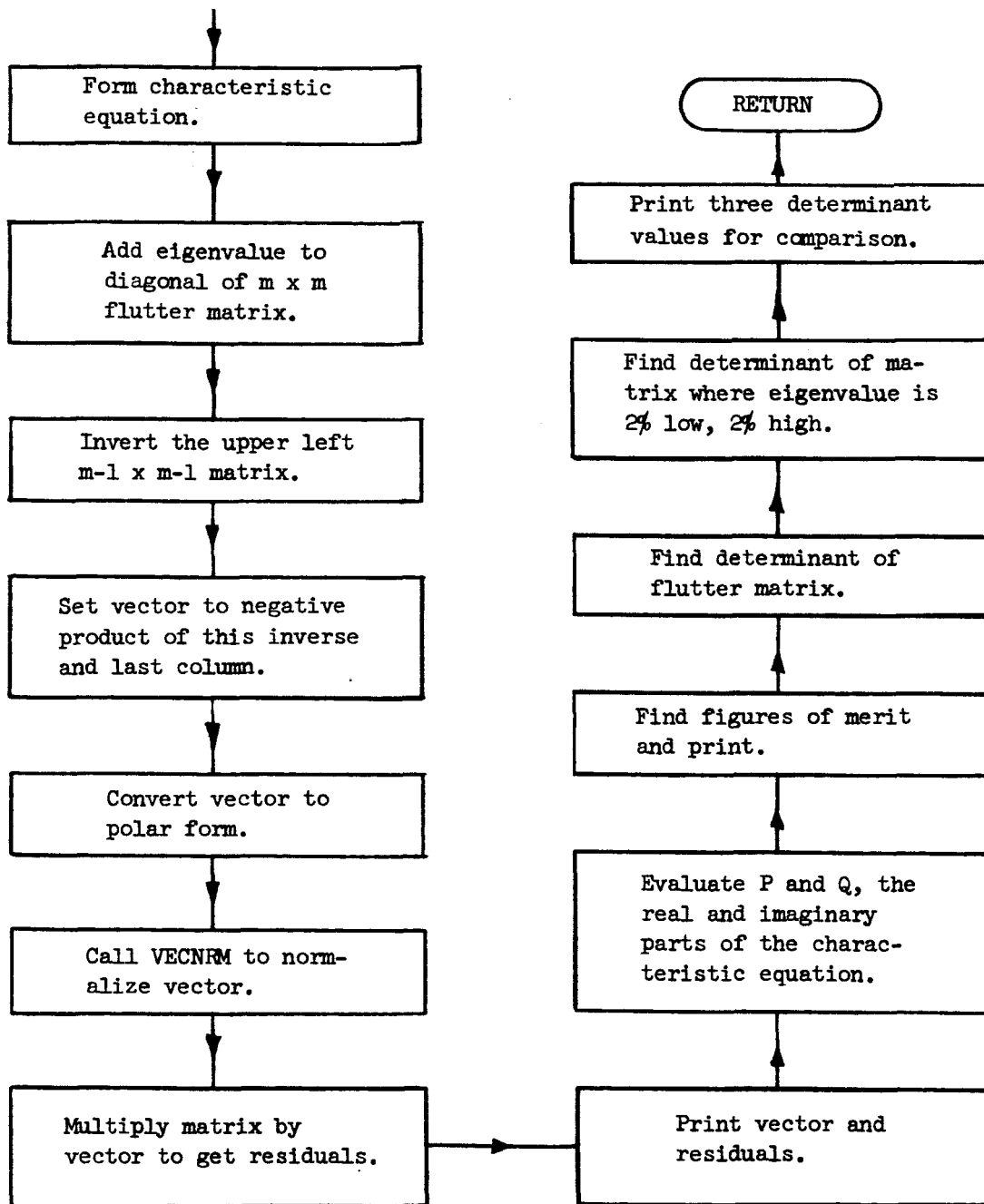
Subroutine EUCLID



Subroutine SCALE



Subroutine DETERM



Subroutine VECTOR

APPENDIX XI

PROGRAM LISTINGS

C*** MAIN PROGRAM FOR PROJECT NO. 2852-P

```
CALL GHDUMP                                GHFLUT20
CALL CONTRL                                GHFLUT30
RETURN                                       GHFLUT40
END                                           GHFLUT60
```

```

SUBROUTINE GHDUMP                                GHDU0020
COMMON GAMMA,EPY,EPX,GMM,SS,T,Q,FREQ,SAVE,COEFS,BFOR,BETA,BSQ,SWK,GHDU0030
1EM,CK,S,PI,PREAL,PIMAG,HMM,DPHI,MMAX,O,XL,SMR,SMI,EYER,EYEI,CC,CD,GHDU0040
2DD,C,D,PUR,PUI,GH,BUF,DJAY,CAY,ARE,NNN,EMSQ,NODP,XNODP,BEE,NEWP, GHDU0050
3NEWGH,NEWGAM,NEWGMB,NEWDPH,ALPHA,CKAY,NEWIV,NEW,NNST, GHDU0060
4DPNO,EINV,SQS,SFOR,EIJ,EIR,AER,AEI,NK,A,LNDP,QMM,MODE GHDU0070
COMMON G,TESTR,MAXAL,MMM,NCASE,NGBAR,NSP,NG,GT,NEWMOD,ON GHDU0080
DIMENSION GAMMA(11),FREQ(31),COEFS(24),EYER(10,10),EYEI(10,10), GHDU0090
1EIJ(10,10),EIR(10,10),AER(10,10),AEI(10,10),EINV(10,10),CKAY(30), GHDU0100
2ALPHA(51),DJAY(10,10),CAY(10,10),ARE(10,10),BUF(20),GH(10,10,80),GHDU0110
3PUR(20,80),PUI(20,80),CC(10,10),CD(10,10),DD(10,10),C(11,6),D(11GHDU0120
4,6),QMM(31),MODE(10),GT(5)
DIMENSION SAVE(14)                                GHDU0140
DIMENSION ON(20)                                GHDU0150
NODP=16                                           GHDU0170
DPHI=.0625                                       GHDU0180
PI = 3.1415927                                   GHDU0190
MMAX=10                                           GHDU0200
READ(5,600) LMIN,LMAX,MODE,NSP,NGBAR,EPY,EPX    GHDU0210
600 FORMAT(I4I2,2F10.0)                          GHDU0220
C*** IF THE CARD IS BLANK, TAPE WAS GENERATED PREVIOUSLY GHDU0222
IF(LMAX.LT.1) RETURN                             GHDU0225
C*** FIND SPANWISE FREQUENCIES AND MODE SHAPES GHDU0227
CALL FREQEQ(NSP,NGBAR,NGBAR,EPX,FREQ)           GHDU0230
CALL CDFIND(1,NSP,NGBAR,NGBAR)                  GHDU0240
DO 900 L=LMIN,LMAX                               GHDU0250
LNDP=L*NCDP                                       GHDU0260
C*** FIND CHORDWISE FREQUENCIES AND MODE SHAPES GHDU0265
21 CALL FREQEQ(L,1,MODE(10),EPY,FREQ)           GHDU0270
23 CALL CDFIND(1,L,1,MMAX)                       GHDU0280
C*** GENERATE G PLUS H MATRIX                    GHDU0285
31 DO 46 J=1,LNDP                                 GHDU0290
XT=J                                              GHDU0300
DARG=XT*DPHI                                     GHDU0310
32 IF(DARG-1.001) 35,33,33                       GHDU0320
33 DARG=DARG-1.                                  GHDU0330
GO TO 32                                         GHDU0340
35 JM=LNDP-NODP-J                                GHDU0350
JX=(J-1)/NODP+1                                  GHDU0360
DO 46 M=1,MMAX                                   GHDU0370
DO 46 MB=1,MMAX                                  GHDU0380
CALL GMML(M,MB,JX,L,DARG)                       GHDU0390
GH(MB,M,J)=GMM                                   GHDU0400
IF(JM) 46,44,44                                  GHDU0410
44 CALL HMML(M,MB,JX,L,DARG)                     GHDU0420
GH(MB,M,J)=GH(MB,M,J)+HMM                       GHDU0430
46 CONTINUE                                       GHDU0440
WRITE( 9)L,MODE,NSP,NGBAR,EPY,EPX,NODP         GHDU0450
WRITE( 9)GAMMA,C                                 GHDU0460
WRITE( 9) D                                       GHDU0470
WRITE( 9) DJAY                                   GHDU0480
WRITE( 9) CAY                                    GHDU0490
WRITE( 9) ARE                                    GHDU0500
500 WRITE( 9) GH                                  GHDU0510
900 CONTINUE                                       GHDU0520
C*** WRITE RECORD TO SIGNAL END OF DATA        GHDU0525
50 L=5                                           GHDU0530
WRITE( 9) L,MODE,NSP,NGBAR,EPY,EPX,NODP        GHDU0540
END FILE 9                                        GHDU0545
REWIND 9                                         GHDU0546
RETURN                                           GHDU0550
END                                               GHDU0560
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SUBROUTINE FREQEQ(LUL,MM1,MM2,EP,FREQ)
COMMON GAMMA,EPY,EPX,GMM,SS,T,Q,FREQ,SAVE,COEFS,RFOR,BETA,BSQ,SQK,
1EM,CK,S,PI,PREAL,PIMAG,HMM,DPHI,MMAX,O,XL,SMR,SMI,EYER,EYEI,CC,CD,
2DD,C,D,PUR,PUI,GH,BUF,DJAY,CAY,ARE,NNN,EMSQ,NODP,XNODP,BEE,NEWP,
3NEWGH,NEWGAM,NEWGMB,NEWDPH,ALPHA,CKAY,NEWEIF,NEWNC,NNST,
4DPNO,EINV,SQS,SFOR,EIJ,EIR,AER,AEI,NK,A,LNDP,QMM,MODE
COMMON G,TESTR,MAXAL,MMM,NCASE,NGBAR,NSP,NG,GT,NEWMOD,ON
DIMENSION GAMMA(11),FREQ(31),COEFS(24),EYER(10,10),EYEI(10,10),
1EIJ(10,10),EIR(10,10),AER(10,10),AEI(10,10),EINV(10,10),CKAY(30),
2ALPHA(51),DJAY(10,10),CAY(10,10),ARE(10,10),BUF(20),GH(10,10,80),FREQ(110
3PUR(20,80),PUI(20,80),CC(10,10),CD(10,10),DD(10,10),C(11,6),D(11
4,6),QMM(31),MODE(10),GT(5)
DIMENSION SAVE(14)
DIMENSION ON(20)
DIMENSION CST(7)
L=LUL
M1=MM1
M2=MM2
670 DO 671 J=2,6
671 CST(J)=0.
CST(1)=-1.
702 GO TO (750,750,703,704,705,706),L
703 CST(2)=-.5
GO TO 750
704 CST(2)=-.70710678
GO TO 750
705 CST(2)=-.80901699
CST(3)=-.30901699
GO TO 750
706 CST(2)=-.86602540
CST(3)=-.5
750 L2=L+2
LH=(L+1)/2
DO 753 J=1,LH
K=L2-J
753 CST(K)=-CST(J)
C SOLVE FREQUENCY EQUATION
755 DO 760 MX=M1,M2
MK=MX
M=MK
IF(M1-M2) 7553,7551,7551
7551 MK=31
7553 FML=(M-1)/L+1
MQ=(M-1)/(2*L)
MR=M-2*L*MQ
IF(MR-L-1) 752,752,751
751 MR=L+L+2-MR
752 COSMU=CST(MR)
BN=3.1415*FML
BP= BN+1.6
756 BA=BN
I=1
GO TO 90
10 VN=V
BA=BP
I=2
GO TO 90
11 VP=V
IF(VN) 13,13,12
12 V=VN
BA=BN
VN=VP
BN=BP
VP=V
BP=BA
13 GO TO 15
15 RAT=VP/(VP-VN)
DINT=BN-BP
IF(RAT-.9) 152,152,151

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```

151 RAT=.9
GO TO 154
152 IF(RAT-.1) 154,154,153
153 RAT=.1
154 BA=BP+RAT*DINT
I=3
GO TO 90
150 IF(BN-BA) 180,20,180
180 IF(BP-BA) 18,20,18
18 IF(V) 16,20,17
16 VN=V
BN=BA
GO TO 15
17 VP=V
BP=BA
GO TO 15
20 FREQ(MK)=BA
QMM(MK)=EP*(SH-SI)/(2.*BA*SI*SH-EP*(SH*CO-SI*CH))
760 CONTINUE
99 RETURN
90 SI=SIN(BA)
CO=COS(BA)
EX=EXP(BA)
EXM=1./EX
SH=0.5*(EX-EXM)
CH=SH+EXM
V=EP*(1.-CO*CH)+BA*(COSMU*(SH-SI)+SI*CH-CO*SH)
GO TO (10,11,150),I
END

```

```

FREQ0710
FREQ0720
FRFQ0730
FREQ0740
FREQ0750
FREQ0760
FREQ0770
FREQ0780
FRFQ0790
FREQ0800
FREQ0810
FREQ0820
FREQ0830
FREQ0840
FREQ0850
FREQ0860
FREQ0870
FREQ0880
FREQ0890
FREQ0900
FREQ0910
FREQ0920
FREQ0930
FREQ0940
FREQ0950
FREQ0960
FREQ0970
FREQ0980
FREQ0990

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```

SUBROUTINE CDFIND(L1,LUL,MM1,MM2)
COMMON GAMMA,EPY,EPX,GMM,SS,T,Q,FREQ,SAVE,COEFS,BFDR,BETA,BSQ,SQK,COFI0020
IEM,CK,S,PI,PREAL,PIMAG,HMM,DPHI,MMAX,D,XL,SMR,SMI,EYER,EYEI,CC,CD,COFI0030
2DD,C,D,PUR,PUI,GH,BUF,DJAY,CAY,ARE,NNN,EMSQ,NODP,XNODP,BEE,NEWP,COFI0040
3NEWGH,NEWGAM,NEWGMB,NEWDPH,ALPHA,CKAY,NEWIV,NEW,NNST,COFI0050
4DPNC,EINV,SQS,SFOR,EIJ,EIR,AER,AEI,NK,A,LNDP,QMM,MODECOFI0060
COMMON G,TESTR,MAXAL,MMM,NCASE,NGBAR,NSP,NG,GT,NEWMOD,BNCOFI0070
DIMENSION GAMMA(11),FREQ(31),COEFS(24),EYER(10,10),EYEI(10,10),COFI0080
IEIJ(10,10),EIR(10,10),AER(10,10),AEI(10,10),EINV(10,10),CKAY(30),COFI0090
2ALPHA(51),DJAY(10,10),CAY(10,10),ARE(10,10),BUF(20),GH(10,10,80),COFI0100
3PUR(20,80),PUI(20,80),CC(10,10),CD(10,10),DD(10,10),C(11,6),D(11COFI0110
4,6),QMM(31),MODE(10),GT(5)COFI0120
DIMENSION SAVE(14)COFI0130
DIMENSION BN(20)COFI0140
L=LULCOFI0150
EL=LCOFI0160
M1=MM1COFI0170
M2=MM2COFI0180
MM=MMAXCOFI0190
DO 36 MX=M1,M2COFI0200
MK=MXCOFI0210
M=MODE(MK)COFI0220
BA=FREQ(M)COFI0230
QM=QMM(M)COFI0240
IF(M1-M2) 20,17,17COFI0250
17 M=MKCOFI0260
BA=FREQ(31)COFI0270
QM=QMM(31)COFI0280
MK=11COFI0290
20 LMOD= MOD(M-1,2*L)COFI0300
GAMMA(MK)=BACOFI0310
IF(LMOD)24,22,24COFI0320
C M IS CONGRUENT TO 1 MOD 2LCOFI0330
22 C(MK,1)=1.COFI0340
IF(L-2) 231,221,221COFI0350
221 DO 23 J=2,LCOFI0360
23 C(MK,J)=-C(MK,J-1)COFI0370
231 SIGND=1.COFI0380
GO TO 28COFI0390
24 IF(LMOD-L)30,26,30COFI0400

```

```

C          M IS CONGRUENT TO 1 MOD L
26 DO 27 J=1,L
27 C(MK,J)=1.
   SIGND=-1.
28 DO 29 J=1,L
29 D(MK,J)=SIGND*C(MK,J)
   GO TO 36
C FORM C AND D
30 DO 35 J=L1,L
   FJ=J
   ZAHL=L+M-1
   UM=PI*ZAHL/EL
   UML=UM*FJ
   SLUM=SIN(UML-UM)
   SLU=SIN(UML)
   C(MK,J)=SLU-QM*SLUM
35 D(MK,J)=SLUM-QM*SLU
36 CONTINUE
   IF(MK-11) 40,99,99
C FORM SUM OF PRODUCTS OF C AND D
40 DO 5J=1,MM
   DO 5K=1,MM
   CC(J,K)=0.
   CD(J,K)=0.
   DD(J,K)=0.
   DO 5I=1,L
   CC(J,K)=CC(J,K)+C(J,I)*C(K,I)
   CD(J,K)=CD(J,K)+C(J,I)*D(K,I)
5 DD(J,K)=DD(J,K)+D(J,I)*D(K,I)
C FORM F TABLE FOR J,K,R
DO 9 J=1,MM
DO 9 K=1,MM
F1 =FMM(1.,1.,J,K,0.)-FMM(0.,0.,J,K,0.)
F2 =FMM(0.,-1.,J,K,0.)-FMM(1.,0.,J,K,0.)
F3 =FMM(1.,1.,J,K,2.)-FMM(0.,0.,J,K,2.)
F4 =FMM(0.,-1.,J,K,2.)-FMM(1.,0.,J,K,2.)
F5 =FMM(1.,1.,J,K,1.)-FMM(0.,0.,J,K,1.)
F6 =FMM(0.,-1.,J,K,1.)-FMM(1.,0.,J,K,1.)
C          TRANSPOSE MATRICES TO AGREE WITH REPORT NOTATION
DJAY(K,J)=F1*(CC(J,K)+DD(J,K))+F2*(CD(J,K)+CD(K,J))
CAY(K,J)=F3*(CC(J,K)+DD(J,K))+F4*(CD(J,K)+CD(K,J))
9 ARE(K,J)=F5*(CC(J,K)-DD(J,K))+F6*(CD(J,K)-CD(K,J))
99 RETURN
END

```

```

COFI0420
COFI0430
COFI0440
COFI0450
COFI0460
COFI0470
COFI0480
COFI0490
COFI0500
COFI0510
COFI0520
COFI0530
COFI0540
COFI0550
COFI0560
COFI0570
COFI0580
COFI0590
COFI0600
COFI0610
COFI0620
COFI0630
COFI0640
COFI0650
COFI0660
COFI0670
COFI0680
COFI0690
COFI0700
COFI0710
COFI0720
COFI0730
COFI0740
COFI0750
COFI0760
COFI0770
COFI0780
COFI0790
COFI0800
COFI0810
COFI0820
COFI0830
COFI0840
COFI0850

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SUBROUTINE GMML(M,MBAR,LL,L1,PHI)
DIMENSION GAMMA(11),FREQ(31),COEFS(24),SAVE(14)
DIMENSION C(11,6),D(11,6),DD(10,10),CD(10,10),CC(10,10),EYER(10,
110),EYEI(10,10)
COMMON GAMMA,EPY,EPX,GMM,SS,T,Q,FREQ,SAVE,COEFS,BFOR,BETA,BSQ,SQK,
1EM,CK,S,PI,PREAL,PIMAG,HMM,DPHI,MMAX,O,XL,SMR,SMI,EYER,EYEI,CC,CD,
2DD,C,D
L = L1
SUMCD1=0.0
SUMCD3=0.0
SUMCD5=0.0
SUMCD7=0.0
DO 10 LBAR=LL,L
J1=LBAR-LL+1
SUMCD1=SUMCD1+C(M,J1)*C(MBAR,LBAR)
SUMCD3=SUMCD3+C(M,J1)*D(MBAR,LBAR)
SUMCD5=SUMCD5+D(M,J1)*C(MBAR,LBAR)
10 SUMCD7=SUMCD7+D(M,J1)*D(MBAR,LBAR)
F1=FMM(1.0-PHI,1.0,M,MBAR,0.0)
F2=FMM(0.0,PHI,M,MBAR,0.0)
F3=FMM(0.0,1.0-PHI,M,MBAR,0.0)
F4=FMM(PHI-1.0,0.0,M,MBAR,0.0)
F5=FMM(-PHI,1.0,M,MBAR,0.0)
F6=FMM(-1.0,PHI,M,MBAR,0.0)
F7=FMM(1.0,1.0-PHI,M,MBAR,0.0)
GMML0020
GMML0030
GMML0040
GMML0050
GMML0060
GMML0070
GMML0080
GMML0090
GMML0100
GMML0110
GMML0120
GMML0130
GMML0140
GMML0150
GMML0160
GMML0170
GMML0180
GMML0190
GMML0200
GMML0210
GMML0220
GMML0230
GMML0240
GMML0250
GMML0260

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```

F8=FMM(PHI,0.0,M,MBAR,0.0)
F1=F1-F2
F3=F3-F4
F5=F5-F6
F7=F7-F8
GMM=F1*SUMCD1-F3*SUMCD3
1-F5*SUMCD5+F7*SUMCD7
999 RETURN
END

```

GMMLO270
GMMLO280
GMMLO290
GMMLO300
GMMLO310
GMMLO320
GMMLO330
GMMLO340
GMMLO350

```

SUBROUTINE HMML(M,MBAR,LL,L1,PHI)
DIMENSION GAMMA(11),FREQ(31),COEFS(24),SAVE(14)
DIMENSION C(11,6),D(11,6),DD(10,10),CD(10,10),CC(10,10),EYER(10,
110),EYEI(10,10)
COMMON GAMMA,EPY,EPX,GMM,SS,T,Q,FREQ,SAVE,COEFS,BFOR,BETA,BSQ,SQK,
LEM,CK,S,PI,PREAL,PIMAG,HMM,DPHI,MMA,XL,SMR,SMI,EYER,EYEI,CC,CD,
2DD,C,D
L=L1
SUMCD1=0.0
SUMCD3=0.0
SUMCD5=0.0
SUMCD7=0.0
LL1=LL+1
DO 20 LBAR=L1,L
J1=LBAR-LL
SUMCD1=SUMCD1+C(M,J1)*C(MBAR,LBAR)
SUMCD3=SUMCD3+C(M,J1)*D(MBAR,LBAR)
SUMCD5=SUMCD5+D(M,J1)*C(MBAR,LBAR)
20 SUMCD7=SUMCD7+D(M,J1)*D(MBAR,LBAR)
F1=FMM(1.0,PHI,M,MBAR,0.0)
F2=FMM(1.0-PHI,0.0,M,MBAR,0.0)
F3=FMM(PHI-1.0,1.0,M,MBAR,0.0)
F4=FMM(-1.0,1.0-PHI,M,MBAR,0.0)
F5=FMM(0.0,PHI,M,MBAR,0.0)
F6=FMM(-PHI,0.0,M,MBAR,0.0)
F7=FMM(PHI,1.0,M,MBAR,0.0)
F8=FMM(0.0,1.0-PHI,M,MBAR,0.0)
F1=F1-F2
F3=F3-F4
F5=F5-F6
F7=F7-F8
HMM=F1*SUMCD1-F3*SUMCD3-F5*SUMCD5+F7*SUMCD7
999 RETURN
END

```

HMML0020
HMML0030
HMML0040
HMML0050
HMML0060
HMML0070
HMML0080
HMML0090
HMML0100
HMML0110
HMML0120
HMML0130
HMML0140
HMML0150
HMML0160
HMML0170
HMML0180
HMML0190
HMML0200
HMML0210
HMML0220
HMML0230
HMML0240
HMML0250
HMML0260
HMML0270
HMML0280
HMML0290
HMML0300
HMML0310
HMML0320
HMML0330
HMML0340
HMML0350

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SUBROUTINE CONTRL
ONE MODE PROBLEMS NOT ALLOWED
DIMENSION KODE(10)
COMMON GAMMA,EPY,EPX,GMM,SS,T,Q,FREQ,SAVE,COEFS,BFOR,BETA,BSQ,SGK,
1EM,CK,S,PI,PREAL,PIMAG,HMM,DPHI,MMA,L,XL,SMR,SMI,EYER,EYEI,
2 C,D,PUR,PUI,GH,BUF,DJAY,CAY,ARE,NNN,EMSQ,NODP,XNODP,REE,NEWP,
3NEWGH,NEWGAM,NEWGMB,NEWDPH,ALPHA,CKAY,NEWIV,NEWC,NNST,
4DPNO,EINV,SQS,SFOR,EIJ,EIR,AER,AEI,NK,A,LNDP,QMM,MODE
COMMON G,TESTR,MAXAL,MMM,NCASE,NGBAR,NSP,NG,GT,NEWMOD,BN
DIMENSION GAMMA(11),FREQ(31),COEFS(24),EYER(10,10),EYEI(10,10),
1EIJ(10,10),EIR(10,10),AER(10,10),AEI(10,10),EINV(10,10),CKAY(30),
2ALPHA(51),DJAY(10,10),CAY(10,10),ARE(10,10),BUF(20),GH(10,10,80),
3PUR(20,80),PUI(20,80),
4,6),QMM(31),MODE(10),GT(5)
DIMENSION SAVE(14)
DIMENSION BN(20)
DIMENSION REST(51)
PI=3.1415927
COEFS(1)=.999999997
COEFS(2)=-.004394275
COEFS(3)=.000434725
COEFS(4)=-.000122226
COEFS(5)=.000043506

```

CONT0020
CONT0030
CONT0040
CONT0050
CONT0060
CONT0070
CONT0080
CONT0090
CONT0100
CONT0110
CONT0120
CONT0130
CONT0140
CONT0150
CONT0160
CONT0170
CONT0180
CONT0190
CONT0200
CONT0210
CONT0220
CONT0230
CONT0240

	COEFS(6)=-.000009285	CONT0250
	COEFS(7)=-.031249995	CONT0260
	COEFS(8)= .001144106	CONT0270
	COEFS(9)=-.000218024	CONT0280
	COEFS(10)=.000085844	CONT0290
	COEFS(11)=-.000035614	CONT0300
	COEFS(12)= .000008099	CONT0310
	COEFS(13)=1.000000004	CONT0320
	COEFS(14)=.007323931	CONT0330
	COEFS(15)=-.000559487	CONT0340
	COEFS(16)=.000145575	CONT0350
	COEFS(17)=-.000050363	CONT0360
	COEFS(18)=.000010632	CONT0370
	COEFS(19)=.093749994	CONT0380
	COEFS(20)=-.001601836	CONT0390
	COEFS(21)=.000266891	CONT0400
	COEFS(22)=-.000099941	CONT0410
	COEFS(23)=.000040658	CONT0420
	COEFS(24)=-.000009173	CONT0430
	NSEQ=1	CONT0440
	SAVE(1)=0.	CONT0445
20	CALL INK	CONT0450
	IF(MMAX.LE.0) RETURN	CONT0460
H2	LNDP=L*16	CONT0470
	IF(NEWGAM+NEWMOD+NEWDPH+NEWGMB) 50,50,25	CONT0480
C	PULL TABLES OF G+H OFF OF TAPE 9.	CONT0490
25	DO 26 J=1,MMAX	CONT0500
26	KODE(J)=MODE(J)	CONT0510
	CALL GPLUSH	CONT0520
	IF(MODE(MMAX)-KODE(MMAX)) 27,51,51	CONT0530
C***	IF MODES REQUESTED DISAGREE WITH MODES ON TAPE, COMPRESS ARRAYS	CONT0534
C***	TO GIVE AGREEMENT	CONT0535
27	DO 35 IM=1,MMAX	CONT0540
	IF(MODE(IM).EQ.KODE(IM)) GO TO 35	CONT0542
	DO 272 K=IM,9	CONT0544
	IF(MODE(K+1).NE.KODE(IM)) GO TO 272	CONT0546
	IK=K+1	CONT0548
	GO TO 275	CONT0550
272	CONTINUE	CONT0552
	WRITE(6,273) KODE(IM)	CONT0554
273	FORMAT(16HMOREREQUESTED MODE I3,14H NOT ON TAPE 9)	CONT0556
	GO TO 20	CONT0558
275	GAMMA(IM)=GAMMA(IK)	CONT0560
	DO 28 J=1,L	CONT0580
	C(IM,J)=C(IK,J)	CONT0590
28	D(IM,J)=D(IK,J)	CONT0600
	DO 32 LK=1,MMAX	CONT0610
	KM=MODE(LK)	CONT0620
	KK=KODE(LK)	CONT0630
	DJAY(KM,IM)=DJAY(KK,IK)	CONT0640
	CAY(KM,IM)=CAY(KK,IK)	CONT0650
	ARE(KM,IM)=ARE(KK,IK)	CONT0660
	LGH=20*L	CONT0670
	DO 32 JGH=1, LGH	CONT0680
32	GH(KM,IM,JGH)=GH(KK,IK,JGH)	CONT0690
35	CONTINUE	CONT0700
	GO TO 51	CONT0710
50	IF(NEWC) 60,60,51	CONT0720
51	CALL BFQST(1)	CONT0730
	GO TO 70	CONT0740
60	IF(NNST-1) 70,70,61	CONT0750
61	CALL BFQST(2)	CONT0760
70	IF(NEWIV) 80,80,71	CONT0770
71	DO 72 J=1,MMAX	CONT0780
	SG=SS*GAMMA(J)**4	CONT0790
C	FORM E INVERSE, PREMULIPLY R AND J	CONT0800
	DO 72 K=1,MMAX	CONT0810
72	EINV(J,K)=(DJAY(J,K)*(SG+Q*SFOR)+(T+T)*SQS*CAY(J,K))/SS	CONT0820
73	GO TO 74	CONT0830
74	CALL UMKEHR(EINV,MMAX)	CONT0840
	DO 75 J=1,MMAX	CONT0850
	DO 75 K=1,MMAX	CONT0860

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75      EIJ(J,K)=0.                                CONT0870
      EIR(J,K)=0.                                CONT0880
      DO 76 J=1,MMAX                             CONT0890
      DO 76 K=1,MMAX                             CONT0900
      DO 76 I=1,MMAX                             CONT0910
      EIJ(J,K)=EIJ(J,K)+EINV(J,I)*DJAY(I,K)    CONT0920
76      EIR(J,K)=EIR(J,K)+EINV(J,I)*ARE(I,K)    CONT0930
80      JK=1                                       CONT0940
      IF(NNST+NK+NEWP -3) 90,81,81             CONT0950
C***    CHOOSE REDUCED FREQUENCY FROM TABLE    CONT0955
81      CK=CKAY(JK)                               CONT0960
      SQK=CK*CK                                   CONT0970
C      CALCULATE AND STORE P                    CONT0980
83      DO 84 J=1,LNDP                             CONT0990
      ARG=J                                       CONT1000
      ARG=ARG*DPHI                               CONT1010
      DO 84 K=NNST,NNN                           CONT1020
      U=2*K- MOD(NGBAR*NSP,2)                   CONT1030
      CALL FINDP(U,ARG)                          CONT1040
      PUR(K,J)=PREAL                             CONT1050
84      PUI(K,J)=PIMAG                             CONT1060
90      CALL FINDI(NNN)                           CONT1070
C      ADD IN TERMS NOT SUMMED OVER U          CONT1080
      COA=CK-CK/BSQ                              CONT1090
      DO 91 J=1,MMAX                             CONT1100
      DO 91 K=1,MMAX                             CONT1110
      AER(J,K)=AER(J,K)/SS+EIR(J,K)            CONT1120
91      AEI(J,K)=AEI(J,K)/SS+COA*EIJJ(J,K)    CONT1130
      DO 960 JG=1,NG                             CONT1140
C***    CHOOSE STRUCTURAL DAMPING FROM TABLE  CONT1145
      G=GT(JG)                                   CONT1150
      CALL HD1063(INSEQ,JK,KODE)                CONT1160
95      FACTR=-SQK*BETA                          CONT1170
96      F12=12./(BETA*(1.+G*G))                CONT1180
      CALL EUCLID(MMAX,G,EIJ,AER,AEI,ALPHA,REST,FACTR,MAXAL,TESTR,L,F12,CONT1190
      IDJAY)                                     CONT1200
960    CONTINUE                                  CONT1210
97      JK=JK+1                                   CONT1220
      IF(JK-NK) 81,81,20                       CONT1230
      END                                         CONT1240

SUBROUTINE INK                                INK 0020
COMMON GAMMA,EPY,EPX,GMM,SS,T,Q,FREQ,SAVE,COEFS,BFOR,BETA,BSQ,SQK, INK 0030
1EM,CK,S,PI,PREAL,PIMAG,HMM,DPHI,MMAX,L,XL,SMR,SMI,EYER,EYEI, INK 0040
2  C,D,PUR,PUI,GH,BUF,DJAY,CAY,ARE,NNN,EMSQ,NODP,XNODP,BEE,NEWP, INK 0050
3NEWGH,NEWGAM,NEWGMB,NEWDPH,ALPHA,CKAY,NEWEIF,NEWC,NNST, INK 0060
4DPND,EINV,SQS,SFOR,EIJ,EIR,AER,AEI,NK,A,LNDP,QMM,MODE INK 0070
COMMON G,TESTR,MAXAL,MMM,NCASE,NGBAR,NSP,NG,GT,NEWMOD INK 0080
DIMENSION GAMMA(11),FREQ(31),COEFS(24),EYER(10,10),EYEI(10,10), INK 0090
1EIJ(10,10),EIR(10,10),AER(10,10),AEI(10,10),EINV(10,10),CKAY(30), INK 0100
2ALPHA(51),DJAY(10,10),CAY(10,10),ARE(10,10),BUF(20),GH(10,10,80), INK 0110
3PUR(20,80),PUI(20,80), C(11,6),D(11 INK 0120
4,6),QMM(31),MODE(10),GT(5) INK 0130
DIMENSION SAVE(14) INK 0140
DIMENSION W(5),KW(3),KM(10) INK 0150
NEWDPH=0 INK 0160
NEWEIF=0 INK 0170
NNST=1 INK 0180
NEWC=0 INK 0190
NEWP=0 INK 0200
NEWGAM=0 INK 0210
NEWGMB=0 INK 0220
NEWMOD=0 INK 0230
40 READ (5,41)KG,KW,W,KM INK 0240
41 FORMAT(4I2,2X5E10.5,10I2) INK 0250
C*** IF FIRST CARD OF CASE IS BLANK, CALL EXIT INK 0255
IF(KG)42,42,44 INK 0260
42 CALL EXIT INK 0270
C*** BRANCH TO STORE AS INDICATED BY CARD CODE INK 0275
44 GO TO (1,2,3,4,5,6,7,8,9,10,11,12),KG INK 0280

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1	TESTR=W(1)	INK 0290
	GO TO 52	INK 0300
2	S=W(1)	INK 0310
	SQS=S*S	INK 0320
	SFOR=SQS*SQS	INK 0330
	NEWIV=1	INK 0340
	NEWC=1	INK 0350
	GO TO 93	INK 0360
3	MMAK=KW(1)	INK 0370
	NEWMOD=1	INK 0380
	IF(KW(2))35,35,30	INK 0390
30	DO 31 J=1,10	INK 0400
31	MODE(J)=KM(J)	INK 0410
	GO TO 37	INK 0420
35	DO 36 J=1,MMAK	INK 0430
36	MODE(J)=J	INK 0440
37	GO TO 62	INK 0450
4	EMSQ=W(1)	INK 0460
	BSQ=EMSQ-1.	INK 0470
	EM=SQRT(EMSQ)	INK 0480
	BETA=SQRT(BSQ)	INK 0490
	BFOR=BSQ*BSQ	INK 0500
	GO TO 93	INK 0510
5	NG=KW(1)	INK 0520
	DO 505 J=1,5	INK 0530
505	GT(J)=W(J)	INK 0540
	IF(NG) 506,506,52	INK 0550
506	NG=1	INK 0560
	GO TO 52	INK 0570
6	DO 61 J=1,5	INK 0580
61	SAVE(J)=W(J)	INK 0590
	L=KW(1)	INK 0595
	GO TO 52	INK 0600
62	NEWGAM=1	INK 0640
63	NEWIV=1	INK 0650
	GO TO 52	INK 0660
7	NK1=KW(1)	INK 0670
	NK2=KW(2)	INK 0680
	NKL=NK1-1	INK 0690
	DO 71 J=NK1,NK2	INK 0700
	K=J-NKL	INK 0710
71	ALPHA(J)=W(K)	INK 0720
	GO TO 52	INK 0730
8	MAXAL=KW(1)	INK 0740
	GO TO 52	INK 0750
9	NK1=KW(1)	INK 0760
	NK2=KW(2)	INK 0770
	NKL=NK1-1	INK 0780
	DO 91 J=NK1,NK2	INK 0790
	K=J-NKL	INK 0800
91	CKAY(J)=W(K)	INK 0810
93	NEWP=1	INK 0840
	GO TO 52	INK 0850
10	NK=KW(1)	INK 0860
	GO TO 52	INK 0870
11	NCASE=KW(1)	INK 0910
C		INK 0920
	A=W(1)+W(1)	INK 0930
	NEWC=1	INK 0940
	GO TO 93	INK 0950
12	GO TO 124	INK 0960
124	NEWP=1	INK 0970
125	NNN=KW(1)	INK 0980
	GO TO 52	INK 0990
52	READ (5,41)KG,KW,W,KM	INK 1090
	IF(KG)99,99,44	INK 1100
C***	A BLANK CARD SIGNALS END OF DATA FOR THIS CASE	INK 1105
99	RETURN	INK 1120
	END	INK 1140


```

SUBROUTINE GPLUSH
COMMON GAMMA,EPY,EPX,GMM,SS,T,Q,FREQ,SAVE,COEFS,BFOR,BETA,BSQ,SQK,
1EM,CK,S,PI,PREAL,PIMAG,HMM,DPHI,MMAX,L,XL,SMR,SMI,EYER,EYEI,
2 C,D,PUR,PUI,GH,BUF,DJAY,CAY,ARE,NNN,EMSQ,NODP,XNODP,BEE,NEWP,
3NEWGH,NEWGAM,NEWGMB,NEWDPH,ALPHA,CKAY,NEWIV,NEWNC,NNST,
4DPND,EINV,SQS,SFOR,EIJ,EIR,AER,AEI,NK,A,LNDP,QMM,MODE
COMMON G,TESTR,MAXAL,MMM,NCASE,NGBAR,NSP,NG,GT,NEWMOD,BN
DIMENSION GAMMA(11),FREQ(31),COEFS(24),EYER(10,10),EYEI(10,10),
1EIJ(10,10),EIR(10,10),AER(10,10),AEI(10,10),EINV(10,10),CKAY(30),
2ALPHA(51),DJAY(10,10),CAY(10,10),ARE(10,10),BUF(20),GH(10,10,80),
3PUR(20,80),PUI(20,80),
4,6),QMM(31),MODE(10),GT(5)
DIMENSION SAVE(14)
DIMENSION BN(20)
10 READ (9)LL,MODE,NSP,NGBAR,EPY,EPX,NODP
IF(LL-L) 80,80,50
80 READ (9)GAMMA,C
READ (9) D
READ (9) DJAY
READ(9) CAY
READ(9) ARE
READ(9) GH
IF(LL-L) 10,90,50
90 IF(L-3) 999,999,998
998 REWIND 9
999 RETURN
50 REWIND 9
GO TO 10
END

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SUBROUTINE BFQST(NN)
COMMON GAMMA,EPY,EPX,GMM,SS,T,Q,FREQ,SAVE,COEFS,BFOR,BETA,BSQ,SQK,
1EM,CK,S,PI,PREAL,PIMAG,HMM,DPHI,MMAX,L,XL,SMR,SMI,EYER,EYEI,
2 C,D,PUR,PUI,GH,BUF,DJAY,CAY,ARE,NNN,EMSQ,NODP,XNODP,BEE,NEWP,
3NEWGH,NEWGAM,NEWGMB,NEWDPH,ALPHA,CKAY,NEWIV,NEWNC,NNST,
4DPND,EINV,SQS,SFOR,EIJ,EIR,AER,AEI,NK,A,LNDP,QMM,MODE
COMMON G,TESTR,MAXAL,MMM,NCASE,NGBAR,NSP,NG,GT,NEWMOD,BN
DIMENSION GAMMA(11),FREQ(31),COEFS(24),EYER(10,10),EYEI(10,10),
1EIJ(10,10),EIR(10,10),AER(10,10),AEI(10,10),EINV(10,10),CKAY(30),
2ALPHA(51),DJAY(10,10),CAY(10,10),ARE(10,10),BUF(20),GH(10,10,80),
3PUR(20,80),PUI(20,80),
4,6),QMM(31),MODE(10),GT(5)
DIMENSION SAVE(14)
DIMENSION BN(20)
N=NN
JSP=11
ENN=NSP
EL=L
G4=GAMMA(11)**4
GO TO (540,620),N
540 COES=.25/G4
FIN3=FMKT(3,JSP,1.)
FON3=FMKT(3,JSP,0.)
FIN1=FMKT(1,JSP,1.)
FON1=FMKT(1,JSP,0.)
FIN2=FMKT(2,JSP,1.)
FON2=FMKT(2,JSP,0.)
T=0.
Q=0.
SS=1.
IF(NCASE-3) 546,546,620
546 SS=0.
DO 550 K=1,NSP
CNKB=C(11,K)
DNKB=D(11,K)
RUB=(CNKB*FON1-DNKB*FIN1)*(CNKB*FON2+DNKB*FIN2)
RAB=CNKB*FIN1-DNKB*FON1
ROB=CNKB*FIN2+DNKB*FON2
RIB=CNKB*FIN3-DNKB*FON3
SS=SS+COES*(RUB-2.*RIB*RAB+ROB*(ROB-RAB))

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	RUB=(CNKB*FON2+DNKB*FIN2)*(CNKB*FON3-DNKB*FIN3)	BFQS0440
550	T=T-0.25*RAB*RAB+COES*(RIB*(ROB-RIB)-RUB)	BFQS0450
	Q=SS*G4	BFQS0460
C	FIND LAMDA AND B	BFQS0470
620	GO TO (81,82,83,81,83),NCASE	BFQS0480
81	WHAT=S*EL/EM	BFQS0490
	GO TO 90	BFQS0500
82	WHAT=0.	BFQS0510
	ENN=1.	BFQS0520
	GO TO 90	BFQS0530
83	WHAT=S*EL/EM	BFQS0540
	WAS=3.*A+ENN+ENN	BFQS0550
	IF(WHAT-WAS)831,90,90	BFQS0560
831	WHAT=WAS	BFQS0570
90	AMDA=0.5*WHAT	BFQS0580
	WAS=WHAT+ENN	BFQS0590
	IF(BEE-WAS) 138,140,138	BFQS0600
138	REE=WAS	BFQS0610
	NFWP=1	BFQS0620
C	FIND BU AND FU	BFQS0630
140	DO 147 JU=NNST,NNN	BFQS0640
	U=2*JU-MOD(NGBAR*NSP,2)	BFQS0650
	UPB=U*PI/BEE	BFQS0660
	COEB=2./(G4-UPB**4)/BEE	BFQS0670
	GO TO (91,92,93,94,95),NCASE	BFQS0680
91	BNU=0.	BFQS0690
	DO 916 K=1,NSP	BFQS0700
	CNKB=C(11,K)	BFQS0710
	DNKB=D(11,K)	BFQS0720
	CPL=K	BFQS0730
	CPL=(CPL+AMDA)*UPB	BFQS0740
	CPLM=CPL-UPB	BFQS0750
	SINUK=SIN(CPL)	BFQS0760
	COSUK=COS(CPL)	BFQS0770
	SINUM=SIN(CPLM)	BFQS0780
	COSUM=COS(CPLM)	BFQS0790
	RUB=CNKB*FIN3-DNKB*FON3-UPB**2*(CNKB*FIN1-DNKB*FON1)	BFQS0800
	RAB=CNKB*FON3-DNKB*FIN3-UPB**2*(CNKB*FON1-DNKB*FIN1)	BFQS0810
	ROB=(CNKB*FON2+DNKB*FIN2)*COSUM-(CNKB*FIN2+DNKB*FON2)*COSUK	BFQS0820
916	BNU=BNU+COEB*(RUB*SINUK+ROB*UPB-RAB*SINUM)	BFQS0830
918	FU=BNU*BEE*0.5	BFQS0840
	GO TO 98	BFQS0850
92	IF(EPX)921,921,91	BFQS0860
921	DO 922 K=NNST,NNN	BFQS0870
	BN(K)=0.	BFQS0875
922	BUF(K)=0.	BFQS0880
	BN(NGBAR)=2.	BFQS0885
	BUF(NGBAR)=2.	BFQS0890
	GO TO 99	BFQS0900
93	PAUSE	BFQS0910
	GO TO 91	BFQS0920
94	GO TO 941	BFQS0930
941	BNU =4./(PI*U)*COS(0.5*UPB*(BEE-1.))	BFQS0940
945	GC TO 918	BFQS0950
95	ABAR=AMDA-ENN-A	BFQS0960
	COEB=2./(U*PI)	BFQS0970
	RUB=UPB*(1.+A)	BFQS0980
	ROB=RUB+UPB*ABAR	BFQS0990
	RAB=ROB+UPB	BFQS1000
	BNU=COEB*(1.+2.*COS(RUB))*(COS(ROB)-COS(RAB))	BFQS1010
	FU=(COS(AMDA*UPB)-COS(UPB*(AMDA+1.)))/UPB	BFQS1020
98	BUF(JU)=BNU*FU	BFQS1030
147	BN(JU)=BNU	BFQS1040
99	RETURN	BFQS1050
	END	BFQS1060

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SUBROUTINE UMKEHR(R,IF)
DIMENSION R(10,10)
N=IF
IF(N-1)31,31,38

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UMKE0020
UMKF0030
UMKE0040
UMKE0050

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31 R(1,1)=1./R(1,1) UMKE0060
GO TO 99 UMKE0070
38 DO 41 K=1,N UMKE0080
D=R(K,K) UMKE0090
R(K,K)=1.0 UMKE0100
50 DO 42 J=1,N UMKE0110
42 R(K,J)=R(K,J)/D UMKE0120
56 IF(K-N)43,44,44 UMKE0130
43 KPLUS=K+1 UMKE0140
51 DO 41 I=KPLUS,N UMKE0150
D=R(I,K) UMKE0160
R(I,K)=0.0 UMKE0170
52 DO 41 J=1,N UMKE0180
41 R(I,J)=R(I,J)-D*R(K,J) UMKE0190
44 MINUS=N-1 UMKE0200
53 DO 45 K=1,MINUS UMKE0210
KPLUS=K+1 UMKE0220
54 DO 45 I=KPLUS,N UMKE0230
D=R(K,I) UMKE0240
R(K,I)=0.0 UMKE0250
55 DO 45 J=1,N UMKE0260
45 R(K,J)=R(K,J)-D*R(I,J) UMKE0270
99 RETURN UMKE0280
END UMKE0290

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SUBROUTINE FINDP (U,ZETA) PFIN0020
COMMON GAMMA,EPY,EPX,GMM,SS,T,Q,FREQ,SAVE,COEFS,BFOR,BETA,BSQ,SQK,PFIN0030
IEM,CK,S,PI,PREAL,PIMAG,HMM,DPHI,MMAX,L,XL,SMR,SMI,EYER,EYEI, PFIN0040
2 C,D,PUR,PUI,GH,BUF,DJAY,CAY,ARE,NNN,EMSQ,NODP,XNODP,BEE,NEWP, PFIN0050
3NEWGH,NEWGAM,NEWGMB,NEWDPH,ALPHA,CKAY,NEWEIF,NEWNC,NNST, PFIN0060
4DPND,EINV,SQS,SFOR,EIJ,EIR,AER,AEI,NK,A,LNDP,QMM,MODE PFIN0070
COMMON G,TESTR,MAXAL,MMM,NCASE,NGBAR,NSP,NG,GT,NEWMOD,BN PFIN0080
DIMENSION GAMMA(11),FREQ(31),COEFS(24),EYER(10,10),EYEI(10,10), PFIN0090
1EIJ(10,10),EIR(10,10),AER(10,10),AEI(10,10),EINV(10,10),CKAY(30), PFIN0100
2ALPHA(51),DJAY(10,10),CAY(10,10),ARE(10,10),BUF(20),GH(10,10,80),PFIN0110
3PUR(20,80),PUI(20,80), C(11,6),D(11,6) PFIN0120
4,6),QMM(31),MODE(10),GT(5) PFIN0130
DIMENSION SAVE(14) PFIN0140
DIMENSION BN(20) PFIN0150
BIGK=CK*EM/BSQ PFIN0160
GAMUSQ=BIGK*BIGK+(U*PI*S/(BETA*BEE))**2 PFIN0170
GAMU=SQRT(GAMUSQ) PFIN0180
ARG=GAMU*ZETA PFIN0190
CO = 0.5*GAMUSQ + SQK/BFOR PFIN0200
C1=2.0*CK*GAMU/BSQ PFIN0210
C2=GAMUSQ*0.5 PFIN0220
B0=BFV(0,ARG) PFIN0230
B1=BFV(1,ARG) PFIN0240
IF(B1)10,11,10 PFIN0250
11 B2=0.0 PFIN0260
GO TO 12 PFIN0270
10 B2=2.0*B1/ARG-B0 PFIN0280
12 EV=C2*B2-C0*B0 PFIN0290
ODD=C1*B1 PFIN0300
AA=BIGK*EM*ZETA PFIN0310
SINA=SIN(AA) PFIN0320
COSA=COS(AA) PFIN0330
PREAL=COSA*EV+SINA*ODD PFIN0340
PIMAG=COSA*ODD-SINA*EV PFIN0350
999 RETURN PFIN0360
END PFIN0370

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SUBROUTINE FINDI(MAXU) IFIN0030
COMMON GAMMA,EPY,EPX,GMM,SS,T,Q,FREQ,SAVE,COEFS,BFOR,BETA,BSQ,SQK,IFIN0040
IEM,CK,S,PI,PREAL,PIMAG,HMM,DPHI,MMAX,L,XL,SMR,SMI,EYER,EYEI, IFIN0050
2 C,D,PUR,PUI,GH,BUF,DJAY,CAY,ARE,NNN,EMSQ,NODP,XNODP,BEE,NEWP, IFIN0060
3NEWGH,NEWGAM,NEWGMB,NEWDPH,ALPHA,CKAY,NEWEIF,NEWNC,NNST, IFIN0070
4DPND,EINV,SQS,SFOR,EIJ,EIR,AER,AEI,NK,A,LNDP,QMM,MODE(10) IFIN0080

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COMMON G,TESTR,MAXAL,MMM,NCASE,NGBAR,NSP,NG,GT,NEWMOD,BN      IFIN0090
DIMENSION GAMMA(11),FREQ(31),COEFS(24),EYFR(10,10),EYEI(10,10),  IFIN0100
1EIJ(10,10),EIR(10,10),AER(10,10),AEI(10,10),EINV(10,10),CKAY(30), IFIN0110
2ALPHA(51),DJAY(10,10),CAY(10,10),ARE(10,10),BUF(20),GH(10,10,80),IFIN0120
3PUR(20,80),PUI(20,80),      C(11,6),D(11)IFIN0130
4,6),QMM(31)      IFIN0140
DIMENSION SAVE(14),GT(5)      IFIN0150
DIMENSION X(5),Y(5)      IFIN0160
RUR=-SQK*(0.5*EMSQ+1.)/BFOR      IFIN0170
ROB=0.5*(PI*S/BEE)**2/BSQ      IFIN0180
J=NODP      IFIN0190
DO 47 K=1,MMAX      IFIN0200
DO 47 KB=1,MMAX      IFIN0210
EYER(K,KB)=0.      IFIN0220
47 EYEI(K,KB)=0.      IFIN0230
C*** LOOP TO SUM OVER INDEX U      IFIN0235
DO 201 JU=1,MAXU      IFIN0240
BUFJU=BUF(JU)      IFIN0250
U=2*JU- MOD(NGBAR,2)      IFIN0260
C*** LCCPS TO FIND CONTRIBUTION OF TERM FOR EACH MATRIX ELEMENT      IFIN0265
PZERO=RUB-U*U*ROB      IFIN0270
DO 200 M=1,MMAX      IFIN0280
DO 199 MBAR=1,MMAX      IFIN0290
SMR=0.      IFIN0300
SMI=0.      IFIN0310
PASTPI=0.      IFIN0320
PASTPR=PZERO      IFIN0330
PASTGH=DJAY(M,MBAR)      IFIN0340
C*** LOOP TO SUM OVER ALL CHORDWISE PANELS      IFIN0345
DO 56 LL=1,L      IFIN0350
ILL=(LL-1)*J      IFIN0360
SUMR=0.      IFIN0370
SUMI=0.      IFIN0380
C*** NUMERICAL INTEGRATION LOOP      IFIN0385
DO 20 I=1,J,4      IFIN0390
IND=ILL+I-1      IFIN0400
DO 17 N=1,4      IFIN0410
IS=IND*N      IFIN0420
GMM=GH(M,MBAR,IS)      IFIN0430
X(N+1)=GMM*PUR(JU,IS)      IFIN0440
17 Y(N+1)=GMM*PUI(JU,IS)      IFIN0450
ANSR=(7.*(PASTPR*PASTGH+X(5))+32.*(X(2)+X(4))+12.*X(3))/22.5      IFIN0460
ANSI=(7.*(PASTPI*PASTGH+Y(5))+32.*(Y(2)+Y(4))+12.*Y(3))/22.5      IFIN0470
SUMR=SUMR+DPHI*ANSR      IFIN0480
SUMI=SUMI+DPHI*ANSI      IFIN0490
PASTGH=GMM      IFIN0500
PASTPI=PUI(JU,IS)      IFIN0510
20 PASTPR=PUR(JU,IS)      IFIN0520
SMR=SMR+SUMR      IFIN0530
56 SMI=SMI+SUMI      IFIN0540
EYER(M,MBAR)=EYER(M,MBAR)+SMR*BUFJU      IFIN0550
199 EYEI(M,MBAR)=EYEI(M,MBAR)+SMI*BUFJU      IFIN0560
200 CONTINUE      IFIN0570
201 CONTINUE      IFIN0580
C      FORM E INVERSE I= AER AND AEI      IFIN0590
106 DO 203 J=1,MMAX      IFIN0600
DO 203 K=1,MMAX      IFIN0610
AER(J,K)=0.      IFIN0620
203 AEI(J,K)=0.      IFIN0630
DO 205 J=1,MMAX      IFIN0640
DO 205 K=1,MMAX      IFIN0650
DO 205 I=1,MMAX      IFIN0660
AER(J,K)=AER(J,K)+EINV(J,I)*EYER(I,K)      IFIN0670
205 AEI(J,K)=AEI(J,K)+EINV(J,I)*EYEI(I,K)      IFIN0680
99 RETURN      IFIN0690
END      IFIN0700

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SUBROUTINE HD1063(INSEQ,JK,KODE)      HEAD0020
COMMON GAMMA,EPY,EPX,GMM,SS,T,Q,FREQ,SAVE,COEFS,BFOR,BETA,BSQ,SQK,HEAD0030
1EM,CK,S,PI,PREAL,PIMAG,HMM,DPHI,MMAX,L,XL,SMR,SMI,EYER,EYEI,      HEAD0040

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2   C,D,PUR,PUI,GH,BUF,DJAY,CAY,ARE,NNN,EMSQ,NDDP,XNDDP,BEE,NEWP, HE AJO050
3NEWGH,NEWGAM,NEWGMB,NEWDPH,ALPHA,CKAY,NEWIV,NEWIC,NNST, HE ADO060
4DPND,EINV,SQS,SFOR,EIJ,EIR,AER,AEI,NK,A,LNDP,QMM,MODE HLA00070
COMMON G,TESTR,MAXAL,MMM,NCASE,NGBAR,NSP,NG,GT,NEWMOD,BN HE ADO080
DIMENSION GAMMA(11),FREQ(31),COEFS(24),EYER(10,10),EYEI(10,10), HF ADO090
1EIJ(10,10),EIR(10,10),AER(10,10),AEI(10,10),EINV(10,10),CKAY(30), HE ADO100
2ALPHA(51),DJAY(10,10),CAY(10,10),ARE(10,10),BUF(20),GH(10,10,80),HE ADO110
3PUR(20,80),PUI(20,80), C(11,6),D(11)HE ADO120
4,6),CMM(31),MODE(10),GT(5) HE ADO130
DIMENSION SAVE(14) HE ADO140
DIMENSION BN(20),KODE(10) HE ADO150
A2=A*0.5 HE ADO160
20 CALL CLOCK(TIME1,TIME2,DATE1,DATE2) HE ADO170
WRITE (6,21)DATE1,DATE2,TIME1,TIME2,NSEQ HE ADO180
21 FORMAT(32H1M.R.I. FLUTTER PROGRAM DATE=,A6,A2,5X5HTIME=A6,A1,50HE ADO190
1X,I4) HE ADO200
NSEQ=NSEQ+1 HE ADO210
WRITE (6,22)EM,S,EPY,EPX,TESTR,L,MMAX,NSP,NNN,NGBAR HE ADO220
22 FORMAT(5X1HM9X1HS6X7HE(SPAN)2X8HE(CHORD)4X5HTESTR6X1HL6X4HMMAX9X1HHE ADO230
IN6X4HUMAX3X13HSPANWISE MODE/4F10.4,E10.2,I6,4I10) HE ADO240
WRITE (6,23)NCASE,A2,NDDP,CK,G HE ADO250
23 FORMAT(5HOCASE5X3HA/25X6H1/DPHI4X1HK9X1HG/I4,F10.4,I8,2F10.4) HE ADO260
IF(NEWGAM+NEWGMB)92,92,24 HE ADO270
24 WRITE (6,25)GAMMA(11) HE ADO280
25 FORMAT(11HOGAMMA-BAR=F11.7) HE ADO290
WRITE (6,26)(KODE(J),J=1,MMAX) HE ADO300
26 FORMAT(16HOCORD-WISE MODEI3,9I11) HE ADO310
WRITE (6,27)(GAMMA(J),J=1,MMAX) HE ADO320
27 FORMAT(8X10F11.7) HE ADO330
WRITE (6,948)(BN(J),J=1,NNN) HE ADO340
948 FORMAT(6HOBNU)/(1X10F10.6)) HE ADO350
92 IF(SAVE(1)) 99,93,99 HE ADO360
93 IF(JK-2) 94,95,95 HE ADO370
94 WRITE (6,941) HE ADO380
DO 942 J=1,MMAX HE ADO390
942 WRITE (6,943)(EIJ(J,K),K=1,MMAX) HE ADO400
95 WRITE (6,944) HE ADO410
DO 945 J=1,MMAX HE ADO420
945 WRITE (6,943)(AER(J,K),K=1,MMAX) HE ADO430
WRITE (6,946) HE ADO440
DO 947 J=1,MMAX HE ADO450
947 WRITE (6,943)(AEI(J,K),K=1,MMAX) HE ADO460
941 FORMAT(47HOINVERSE OF ELASTIC MATRIX TIMES INERTIA MATRIX) HE ADO470
943 FORMAT(1PBE15.7) HE ADO480
944 FORMAT(55HOINVERSE OF ELASTIC MATRIX TIMES REAL PART AERCD MATRIX) HE ADO490
946 FORMAT(55HOINVERSE OF ELASTIC MATRIX TIMES IMAG PART AERCD MATRIX) HE ADO500
99 RETURN HE ADO510
END HE ADO520

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SUBROUTINE CLOCK(TIME1,TIME2,DATE1,DATE2) CLOC0020
C DUMMY ROUTINE TO BE REPLACED BY CLOCK ROUTINE APPROPRIATE TO CLOC0030
C PARTICULAR INSTALLATION CLOC0040
TIME1=0. CLOC0050
TIME2=0. CLOC0060
DATE1=0. CLOC0070
DATE2=0. CLOC0080
RETURN CLOC0090
END CLOC0100

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SUBROUTINE EUCLID(M,G,E,AK,AI,ALS,REST,FACTR,MAXAL,TESTR,L,F12,DJ)EUC 0010
C THIS VERSION OF EUCLID CALLS FLUT SUBROUTINE WHICH EUC 0020
C REDUCES CHARACTERISTIC POLYNOMIALS TO LINEAR AND QUADRATIC FACTORSEUC 0030
C FOR CALCULATION OF ALPHA(EUCLIDIAN ALGORITHM MODIFIED) EUC 0040
DOUBLE PRECISION R(11,10),CR(10,20),PRE(22),ALP(51),AP,AN,AL,DUB, EUC 0050
IDET,RANGE EUC 0060
C FLUTTER DETERMINATION USING SYLVESTERS RESULTANT EUC 0070
DIMENSION REST(51) ,LEST(51),JEST(51) EUC 0080
DIMENSION ALS(50) EUC 0090

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	DIMENSION E(10,10),AR(10,10),AI(10,10),DJ(10,10)	EUC 0110
	J7=51	EUC 0130
	JPRE=11	EUC 0140
	DO 802 J=1,MAXAL	EUC 0150
802	ALP(J)=ALS(J)	EUC 0160
	N=M	EUC 0180
	MP=N+1	EUC 0190
803	INDEX=1	EUC 0200
	I1=1	EUC 0210
	I2=MAXAL	EUC 0220
804	DO 30 IXAL=I1,I2	EUC 0230
805	AL=ALP(IXAL)	EUC 0240
C***	SET UP MATRIX CBAR	EUC 0245
	CALL CBAR(AL,G,AR,AI,E,N,CR,FACTR)	EUC 0250
807	CALL OVERFL(JO)	EUC 0260
C***	FIND CHARACTERISTIC EQUATION	EUC 0265
809	CALL EQCHAR(CR,PRE,N)	EUC 0280
C	SYLVESTER RESULTANT	EUC 0290
	CALL OVERFL(JO)	EUC 0300
	GO TO (8100,810),JO	EUC 0305
810	IF(N) 8100,8100,811	EUC 0310
8100	DET=0.	EUC 0320
	N=M	EUC 0330
	GO TO 30	EUC 0340
811	CALL SCALE(R,PRE,N,JPRE,NS,KRUB)	EUC 0350
	CALL OVERFL(JO)	EUC 0360
	GO TO (8100,7),JO	EUC 0365
7	CALL DETERM(N,DET,R,NJL)	EUC 0370
C	STORE RESULTANT	EUC 0380
	LEST(IXAL)=NS	EUC 0390
	JEST(IXAL)=KRUB+NJL	EUC 0400
	CALL OVERFL(JO)	EUC 0410
	GO TO (8100,30),JO	EUC 0415
30	REST(IXAL)=DET	EUC 0420
	GO TO (31,38,501,506),INDEX	EUC 0430
31	CALL WRITER(ALP,REST,LEST,MAXAL,JEST)	EUC 0440
C	SEARCH FOR SIGN CHANGE OF REMAINDER	EUC 0450
	JSUB=2	EUC 0460
	INDEX=2	EUC 0470
32	DO 33 J=JSUB,MAXAL	EUC 0480
	IF(ABS(REST(J))/REST(J)*REST(J-1)) 325,33,33	EUC 0490
325	JSUB=J+1	EUC 0500
	GO TO 35	EUC 0510
33	CONTINUE	EUC 0520
34	RETURN	EUC 0530
C	INTERPOLATE FOR FLUTTER POINT	EUC 0540
35	J=JSUB-1	EUC 0550
	I1=J7	EUC 0560
	I2=J7	EUC 0570
	KIT=0	EUC 0580
	AP=ALP(J)	EUC 0590
	AN=ALP(J-1)	EUC 0600
	RP=REST(J)	EUC 0610
	RN=REST(J-1)	EUC 0620
	JP=JEST(J)	EUC 0630
	JN=JEST(J-1)	EUC 0640
	LP=LEST(J)	EUC 0650
	LN=LEST(J-1)	EUC 0660
	IF(RP) 36,365,365	EUC 0670
36	DUB=AP	EUC 0680
	AP=AN	EUC 0690
	AN=DUB	EUC 0700
	RUB=RP	EUC 0710
	RP=RN	EUC 0720
	RN=RUB	EUC 0730
	LUB=LN	EUC 0740
	LN=LP	EUC 0750
	LP=LUB	EUC 0760
	LUB=JN	EUC 0770
	JN=JP	EUC 0780
	JP=LUB	EUC 0790
365	LDIF=(LN-LP)*N+JN-JP	EUC 0800

	TWOL=2.**LDIF	EUC 0810
37	RANGE=AN-AP	EUC 0820
	DUB =RN/RP*TWOL	EUC 0830
	RATIO=1./(1.-DUB)	EUC 0850
	IF(RATIO-.9) 372,372,371	EUC 0860
371	RATIO=.9	EUC 0870
	GO TO 374	EUC 0880
372	IF(RATIO-.1) 373,374,374	EUC 0890
373	RATIO=.1	EUC 0900
374	ALP(J7)=AP+RATIO*RANGE	EUC 0910
	GO TO 804	EUC 0920
C	TEST FOR ACCEPTANCE OF ALPHA	EUC 0930
38	IF(ABS(RANGE)-TESTR*AN) 42,42,39	EUC 0940
39	IF(REST(J7)) 40,41,41	EUC 0950
40	RN=REST(J7)	EUC 0960
	KIT=KIT+1	EUC 0970
	LN=LEST(J7)	EUC 0980
	JN=JEST(J7)	EUC 0990
	IF (AN-AL) 401,42,401	EUC 1000
401	AN=AL	EUC 1010
	GO TO 37	EUC 1020
41	RP=REST(J7)	EUC 1030
	KIT=KIT+1	EUC 1040
	LP=LEST(J7)	EUC 1050
	JP=JEST(J7)	EUC 1060
	IF(AP-AL) 411,42,411	EUC 1070
411	AP=AL	EUC 1080
	GO TO 37	EUC 1090
C	WRITE FLUTTER DATA AND LOOP	EUC 1100
42	LSC=LEST(J7)	EUC 1110
43	CALL FLUT(PRE,N,LSC,U,RES,JPRE,1)	EUC 1120
50	INDEX=3	EUC 1130
	AF=AL	EUC 1140
	LF=LEST(J7)	EUC 1150
	JF=JEST(J7)	EUC 1160
	RF=REST(J7)	EUC 1170
	ALP(J7)=AN	EUC 1180
	GO TO 804	EUC 1190
501	LSC=LEST(J7)	EUC 1200
	CALL FLUT(PRE,N,LSC,UN,RES,JPRE,1)	EUC 1210
	INDEX=4	EUC 1220
	ALP(J7)=AP	EUC 1230
	GO TO 804	EUC 1240
506	LSC=LEST(J7)	EUC 1250
	CALL FLUT(PRE,N,LSC,UP,RES,JPRE,1)	EUC 1260
	WRITE(6,507) KIT	EUC 1270
507	FORMAT(1X15,11H ITERATIONS)	EUC 1280
	KIT=0	EUC 1290
508	CALL WR0UT(AF, U,RF,LF,0,JF,F12)	EUC 1300
	CALL WR0UT(AN,UN,RN,LN,1,JN,F12)	EUC 1310
	CALL WR0UT(AP,UP,RP,LP,1,JP,F12)	EUC 1320
55	CALL CBAR(AL,G,AR,AI,E,N,CR,FACTR)	EUC 1330
56	INDEX=2	EUC 1340
57	CALL VECTOR(U,CR,N,L,DJ)	EUC 1350
58	IF(JSUB-MAXAL) 32,32,34	EUC 1370
	END	EUC 1380

C***	SUBROUTINE CBAR(AL,G,AR,AI,E,N,CR,FACTR)	CBAR0020
	SET UP MATRIX CBAR	CBAR0025
	DOUBLE PRECISION CR(10,20)	CBAR0030
	DIMENSION E(10,10),AR(10,10),AI(10,10)	CBAR0040
	P=FACTR	CBAR0050
	ALF=AL*P	CBAR0060
	DO R06 J=1,N	CBAR0070
	DO R06 K=1,N	CBAR0080
	P=E(J,K)	CBAR0090
	Q=AR(J,K)	CBAR0100
	R=AI(J,K)*G	CBAR0110
	S=AI(J,K)	CBAR0120
	T=AR(J,K)*G	CBAR0130

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      U=E(J,K)*G
      CR(J,K)=ALF*P+Q+R
806 CR(J,K+10)=S-T-ALF*U
99  RETURN
      END
      CBAR0140
      CBAR0150
      CBAR0160
      CBAR0170
      CBAR0180

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      SUBROUTINE EQCHAR(AA,PRE,N1)
      DOUBLE PRECISION AA(10,20),A(10,20),D(11,22),X(20),TEMP,TEMP1,DENOCHEQ0010
      DOUBLE PRECISION PRE(22)
      N=N1
      M=N
      M1=M-1
      M2=M-2
      PRE(N)=0.
      PRE(N+11)=0.
130 IF(M2)140,130,143
      PRE(1)=AA(1,1)*AA(2,2)-AA(1,2)*AA(2,1)-AA(1,11)*AA(2,12)+AA(1,12)*CHEQ00120
      IAA(2,11)
      PRE(12)=AA(1,1)*AA(2,12)+AA(1,11)*AA(2,2)-AA(1,2)*AA(2,11)-AA(2,1)CHEQ00130
      I*AA(1,12)
      PRE(2)=-AA(2,2)
      PRE(13)=-AA(2,12)
140 PRE(N)=PRE(N)-AA(1,1)
      PRE(N+11)=PRE(N+11)-AA(1,11)
      GO TO 92
143 DO 144 J=1,N
      DO 144 K=1,N
      A(J,K)=AA(J,K)
144 A(J,K+10)=AA(J,K+10)
      C INSURE MAXIMUM SUB-DIAGONAL ELEMENT AT PIVOT
100 REFM=A(M,M1)**2+A(M,M1+10)**2
      I=M1
      DO 104 J=1,M2
      REFT=A(M,J)**2+A(M,J+10)**2
      IF(REFM-REFT)101,104,104
101 I=J
      REFM=REFT
104 CONTINUE
      IF(I-M1)210,105,105
105 IF(REFM)106,106,22
      C DECOUPLED
106 WRITE(6,107)
      WRITE(6,108) ((A(J,K),K=1,N),J=1,N)
      WRITE(6,107)
      WRITE(6,108) ((A(J,K+10),K=1,N),J=1,N)
107 FORMAT(10H DECOUPLED)
      N1=0
      GO TO 92
108 FORMAT(6(D11.3,2X))
      C INTERCHANGE ROWS AND COLUMNS
210 DO 212 J=1,M
      TEMP=A(J,I)
      TEMPI=A(J,I+10)
      A(J,I)=A(J,M1)
      A(J,I+10)=A(J,M1+10)
      A(J,M1+10)=TEMPI
212 A(J,M1)=TEMP
      DO 213 J=1,N
      TEMP=A(M1,J)
      TEMPI=A(M1,J+10)
      A(M1,J)=A(I,J)
      A(M1,J+10)=A(I,J+10)
      A(I,J+10)=TEMPI
213 A(I,J)=TEMP
      C SIMILARITY TRANSFORM
22 DENO=A(M,M1)**2+A(M,M1+10)**2
      TEMP=A(M,M1)/DENO
      TEMPI=-A(M,M1+10)/DENO
      DO 30 J=1,M2
      X(J+10)=A(M,J)*TEMPI+A(M,J+10)*TEMP
      CHEQ0010
      CHEQ0030
      CHEQ0040
      CHEQ0050
      CHEQ0060
      CHEQ0070
      CHEQ0080
      CHEQ0090
      CHEQ0100
      CHEQ0110
      CHEQ0120
      CHEQ0130
      CHEQ0140
      CHEQ0150
      CHEQ0160
      CHEQ0170
      CHEQ0180
      CHEQ0190
      CHEQ0200
      CHEQ0210
      CHEQ0220
      CHEQ0230
      CHEQ0240
      CHEQ0250
      CHEQ0260
      CHEQ0270
      CHEQ0280
      CHEQ0290
      CHEQ0300
      CHEQ0310
      CHEQ0320
      CHEQ0330
      CHEQ0340
      CHEQ0350
      CHEQ0360
      CHEQ0370
      CHEQ0380
      CHEQ0390
      CHEQ0400
      CHEQ0410
      CHEQ0420
      CHEQ0430
      CHEQ0440
      CHEQ0450
      CHEQ0460
      CHEQ0470
      CHEQ0480
      CHEQ0490
      CHEQ0500
      CHEQ0510
      CHEQ0520
      CHEQ0530
      CHEQ0540
      CHEQ0550
      CHEQ0560
      CHEQ0570
      CHEQ0580
      CHEQ0590
      CHEQ0600
      CHEQ0610
      CHEQ0620
      CHEQ0630
      CHEQ0640
      CHEQ0650

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30	X(J)=A(M,J)*TEMP-A(M,J+10)*TEMPI	CHEQ0660
	X(M1)=1.	CHEQ0670
	X(M1+10)=0.	CHEQ0680
	DO 31 J=M,N	CHEQ0690
	X(J+10)=0.	CHEQ0700
31	X(J)=0.	CHEQ0710
	DO 42 K=1,M2	CHEQ0720
	DO 41 J=1,N	CHEQ0730
	A(J,K+10)=A(J,K+10)-X(K)*A(J,M1+10)-X(K+10)*A(J,M1)	CHEQ0740
41	A(J,K)=A(J,K)-X(K)*A(J,M1)+X(K+10)*A(J,M1+10)	CHEQ0750
	A(M,K+10)=0.	CHEQ0760
42	A(M,K)=0.	CHEQ0770
	DO 52 J=1,M2	CHEQ0780
	DO 52 K=1,N	CHEQ0790
	A(M1,K+10)=A(M1,K+10)+X(J)*A(J,K+10)+X(J+10)*A(J,K)	CHEQ0800
52	A(M1,K)=A(M1,K)+X(J)*A(J,K)-X(J+10)*A(J,K+10)	CHEQ0810
	IF(M2-1,99,99,62	CHEQ0820
62	M=M1	CHEQ0830
	M1=M2	CHEQ0840
	M2=M2-1	CHEQ0850
	GO TO 100	CHEQ0860
99	GO TO 990	CHEQ0870
990	CALL CHAR(A,D,N)	CHEQ0880
90	NP=N+1	CHEQ0890
	DO 91 J=1,NP	CHEQ0900
	PRE(J+11)=D(NP,J+11)	CHEQ0910
91	PRE(J)=D(NP,J)	CHEQ0920
92	RETURN	CHEQ0930
	END	CHEQ0940

	SUBROUTINE CHAR(A,D,L)	CHAR0010
	DOUBLE PRECISION A(10,20),D(11,22),SUM,SUMI,FAC,FACI,ZR,ZI,TERM,	CHAR0015
	1TERM1,RUB	CHAR0020
	MAX=L	CHAR0030
	NP=MAX+1	CHAR0040
	DO 1 J=1,NP	CHAR0050
	D(J,J)=1.	CHAR0060
1	D(J,J+11)=0.	CHAR0070
	DO 10 N=1,MAX	CHAR0080
	N10=N+10	CHAR0090
	DO 10 K=1,N	CHAR0100
	NK=N-K	CHAR0110
	NK1=NK+1	CHAR0120
	NK12=NK1+11	CHAR0130
	SUM=0.	CHAR0140
	SUMI=0.	CHAR0150
	FAC=1.	CHAR0160
	FACI=0.	CHAR0170
	DO 5 M=1,K	CHAR0180
	NM=N-M	CHAR0190
	NM1=NM+1	CHAR0200
	NM10=NM+10	CHAR0210
	ZR=A(NM1,N)*D(NM1,NK1)-A(NM1,N10)*D(NM1,NK12)	CHAR0220
	ZI=A(NM1,N)*D(NM1,NK12)+A(NM1,N10)*D(NM1,NK1)	CHAR0230
	TERM=FAC*ZR-FACI*ZI	CHAR0240
	TERM1=FAC*ZI+FACI*ZR	CHAR0250
	SUM=SUM+TERM	CHAR0260
	SUMI=SUMI+TERM1	CHAR0270
	IF(K-M) 51,51,4	CHAR0280
4	RUB=FAC*A(NM1,NM)-FACI*A(NM1,NM10)	CHAR0290
	FACI=FAC*A(NM1,NM10)+FACI*A(NM1,NM)	CHAR0300
5	FAC=RUB	CHAR0310
51	IF(NK) 8,8,6	CHAR0320
6	D(N+1,NK1)=D(N,NK)-SUM	CHAR0330
	D(N+1,NK12)=D(N,NK12-1)-SUMI	CHAR0340
	GO TO 10	CHAR0350
8	D(N+1,1)=-SUM	CHAR0360
	D(N+1,12)=-SUMI	CHAR0370
10	CONTINUE	CHAR0380
99	RETURN	CHAR0390

	END	CHAR0400
	SUBRCUTINE SCALE(IRR,P,NN,JPRE,NS,KRUB)	SCAL2210
	DCUBLE PRECISICN RR(11,10),R(11,10),P(22),SF,RUB	SCAL2230
	N=NN	SCAL2260
700	EN=N	SCAL2270
	NP=N+1	SCAL2280
	DC 1 J=1,N	SCAL2290
	K=NP-J	SCAL2300
	JPR=JPRE+J	SCAL2310
	R(1,K)=P(JPR)	SCAL2320
1	R(NP,K)=P(J)	SCAL2330
701	SUMN2=(N*NP*(N+NP))/6	SCAL2340
	SCA=0.	SCAL2350
	DC 410 J=1,N	SCAL2360
	C=J	SCAL2370
	AB=DABS(R(NP,J))	SCAL2380
	IF(AB) 410,410,409	SCAL2390
409	RCG2=C*ALCG(AB)	SCAL2400
	SCA=SCA+RCG2	SCAL2410
410	CCONTINUE	SCAL2420
	NS=ABS(1.44270*SCA/SUMN2)+.5	SCAL2430
	IF(SCA) 410C,4101,4101	SCAL2440
4100	NS=-NS	SCAL2450
4101	FAC=1.0	SCAL2460
	SF=0.5**NS	SCAL2470
	DC 411 K=1,N	SCAL2480
	FAC=FAC*SF	SCAL2490
	R(1,K)=R(1,K)*FAC	SCAL2500
411	R(NP,K)=R(NP,K)*FAC	SCAL2510
	DC 5 K=2,N	SCAL2530
	RUB=-R(K-1,1)	SCAL2540
	R(K,N)=RUB*R(NP,N)	SCAL2550
	DC 5 J=2,N	SCAL2560
5	R(K,J-1)=R(K-1,J)+RUB*R(NP,J-1)	SCAL2570
60	KRUB=0	SCAL2580
	NM=N-1	SCAL2590
C	DC NCT SCALE LAST ROW UNLESS YOU WANT TROUBLE	SCAL2600
	DC 307 J=1,NM	SCAL2610
	RUB=0.	SCAL2620
	DC 304 K=1,N	SCAL2630
	AB=DABS(R(J,K))	SCAL2640
	IF(AB) 301,304,301	SCAL2650
301	RCG2=ALCG(AB)*1.4427	SCAL2660
	RUB=RUB+RCG2	SCAL2670
304	CCONTINUE	SCAL2680
	LRUB=RUB/EN+.5	SCAL2690
	KRUB=KRUB+LRUB	SCAL2700
305	SF=0.5**LRUB	SCAL2710
	DC 306 K=1,N	SCAL2720
306	RR(J,K)=R(J,K)*SF	SCAL2730
307	CCONTINUE	SCAL2740
	DC 308 K=1,N	SCAL2750
308	RR(N,K)=R(N,K)	SCAL2760
99	RETURN	SCAL2770
	END	SCAL2780
	SUBRCUTINE DETERM(MM,RES,R,NSUM)	DETE0650
C***	DCUBLE PRECISION DETERMINANT	DETE0660
	DCUBLE PRECISION R(11,10),A(10,10),DET,RES,DSIGN,AB,RUB,RA	DETE0670
	M=MM	DETE0680
	NSUM=0	DETE0690
	IF(M-1) 26,26,27	DETE0700
26	DET=R(1,1)	DETE0710
	GC TC 99	DETE0720
27	DC 28 J=1,M	DETE0730
	DC 28 K=1,M	DETE0740
28	A(J,K)=R(J,K)	DETE0750

	DSIGN=1.		DETE0760
C	K LCOP		DETE0770
	DO 30 LT=2,M		DETE0780
	K=LT-1		DETE0790
	L=0		DETE0800
	BIG=0.		DETE0810
	DO 100 I=K,M		DETE0820
	AR=DABS(A(K,I))		DETE0830
	IF(BIG-AR) 150,100,100		DETE0840
150	L=I		DETE0850
	BIG=AB		DETE0860
100	CONTINUE		DETE0870
	IF(L) 16,16,13		DETE0880
13	IF(K-L) 14,5,5		DETE0890
C	IF DIAGONAL ELEMENT IS NOT MAX, INTERCHANGE COLUMNS		DETE0900
14	DO 8 J=K,M		DETE0910
	RUB=A(J,K)		DETE0920
	A(J,K)=A(J,L)		DETE0930
8	A(J,L)=RUB		DETE0940
	DSIGN=-DSIGN		DETE0950
	IF(A(K,K)) 5,13,5		DETE0960
C	REDUCTION LOOP		DETE0970
5	RA=1./A(K,K)		DETE0980
	DO 3 I=LT,M		DETE0990
	AB=RA*A(I,K)		DETE1000
	DO 3 J=LT,M		DETE1010
3	A(I,J)=A(I,J)-AB*A(K,J)		DETE1020
30	CONTINUE		DETE1030
C	FORM PRODUCT OF DIAGONAL ELEMENTS		DETE1040
4	DO 6 J=2,M		DETE1050
C	SCALE TO PREVENT UNDERFLOW		DETE1060
	B=DABS(A(J,J))		DETE1070
	IF(B) 16,16,50		DETE1080
50	N=1.4427*ALOG(B)		DETE1090
	NSUM=NSUM+N		DETE1100
6	A(J,J)=A(J,J)*(.5**N)*A(J-1,J-1)		DETE1110
98	DET=DSIGN*A(M,M)		DETE1120
49	RES=DET		DETE1130
	RETURN		DETE1140
C	MATRIX IS SINGULAR, UNREMOVABLE ZERO ON DIAGONAL		DETE1150
16	DSIGN=0.		DETE1160
	GO TO 98		DETE1170
	END		DETE1180
C***	SUBROUTINE WRITER(A,R,L,ML,JE)		WRIT0020
	WRITE MU VERSUS RESULTANT TABLES		WRIT0025
	DIMENSION A(51),R(51),L(51),JE(51)		WRIT0030
	WRITE (6,600)		WRIT0040
	NR=ML/4		WRIT0050
	IF(4*NR-ML)7,8,8		WRIT0060
7	NR=NR+1		WRIT0070
8	DO 10 J=1,NR		WRIT0080
10	WRITE (6,601)(A(2*K-1),R(K),L(K),JE(K),K=J,ML,NR)		WRIT0090
99	RETURN		WRIT0100
600	FORMAT(5X2HMU8X3HRES4X7HSFA SFR5X2HMU8X3HRES4X7HSFA SFR5X2HMU8X3HR		WRIT0110
	IES4X7HSFA SFR5X2HMU8X3HRES4X7HSFA SFR)		WRIT0120
601	FOR*AT(4(1PE11.2,E11.2,I3,I4))		WRIT0130
	END		WRIT0140
C	SUBROUTINE FLUT(PRE,NR,NS,U,RES,JPRE,I)		FLUT0070
	DOUBLE PRECISION PRE(22),A(11),B(11),C(11),DENOM,ROOT,UU,PSUM,		FLUT0080
	IPDSUM,QSUM,QDSUM,REST		FLUT0090
	IN=I		FLUT0140
	N=NR		FLUT0150
	JPR=JPRE		FLUT0160
C	COPY THE CHARACTERISTIC POLYNOMIALS		FLUT0170
	JJ=N+1		FLUT0180
	DO 2 J=1,JJ		FLUT0190

```

A(J)=PRE(J)
J11=J+1
2 B(J)=PRE(J11)
NN=N-1
DENOM=B(N)
DO 3 K=1,NN
3 B(K)=B(K)/DENOM
B(N)=1.
6 NO=N-1
AA=A(1)/B(1)
DENOM=A(NO+1)-B(NO)-B(NO+1)*AA
DO 10 K=1,NO
10 C(K)=(A(K+1)-B(K)-B(K+1)*AA)/DENOM
IF(N-3)30,30,14
14 A(N)=B(N)
DO 15 J=1,NO
A(J)=B(J)
15 B(J)=C(J)
N=N-1
GO TO 6
30 ROOT=-C(1)
IF(IN)25,20,25
20 REST=B(2)+B(1)/ROOT+ROOT
RES=REST
100 RETURN
C CALCULATE SECOND ORDER ESTIMATE OF ROOT
25 DO 32 J=1,JJ
A(J)=PRE(J)
J11=J+1
32 B(J)=PRE(J11)
PSUM=A(NR+1)
PDSUM=0.
QSUM=B(NR+1)
QDSUM=0.
DO 35 K=1,NR
L=NR-K+1
XL=L
PSUM=ROOT*PSUM+A(L)
PDSUM=ROOT*PDSUM+A(L+1)*XL
QSUM=ROOT*QSUM+B(L)
35 QDSUM=ROOT*QDSUM+B(L+1)*XL
UU=(.5*(PSUM/PDSUM+QSUM/QDSUM)-ROOT)
U=UU
GO TO 100
END

```

```

FLUT0200
FLUT0210
FLUT0220
FLUT0230
FLUT0240
FLUT0250
FLUT0260
FLUT0270
FLUT0280
FLUT0290
FLUT0300
FLUT0310
FLUT0320
FLUT0330
FLUT0340
FLUT0350
FLUT0360
FLUT0370
FLUT0380
FLUT0390
FLUT0400
FLUT0410
FLUT0420
FLUT0430
FLUT0440
FLUT0450
FLUT0460
FLUT0470
FLUT0480
FLUT0490
FLUT0500
FLUT0510
FLUT0520
FLUT0530
FLUT0540
FLUT0550
FLUT0560
FLUT0570
FLUT0580
FLUT0590
FLUT0600
FLUT0610
FLUT0620
FLUT0630
FLUT0640

```

```

SUBROUTINE WROUT(A,U,R,L,N,JL,FAC)
C FLUTTER POINTS FOR PANEL
A3=(U*FAC*2.)**.33333333
RU=1./A
IF(N ) 617,617,619
617 WRITE (6,618)
618 FORMAT(1H07X2HMU10X6HZ**1/315X5HLAMDA10X3HRES7X7MSFA SFR4X4H1/MU)
C BEWARE-- SYMBOLS FOR MU AND ALPHA ARE INTERCHANGED BACK
619 WRITE (6,620)A,A3,U,R,L,JL,RU
620 FORMAT(F14.6,F16.8,1PE19.8,E14.3,I6,I4,OPF11.6)
RETURN
END

```

```

WROU0020
WROU0030
WROU0040
WROU0050
WROU0060
WROU0070
WROU0080
WROU0090
WROU0100
WROU0110
WROU0120
WROU0130

```

```

SUBROUTINE VECTOR(EW,C,I,L,DJ)
DOUBLE PRECISION P(22),C(10,20)
COMPLEX R(10),CK(10),S(10,10),SS
DIMENSION VM(10),VT(10),DJ(10,10)
M=I
CALL EQCHAR(C,P,M)
MN=M-1
C FORM CB=C+EIGENVALUE*I
DO 5 J=1,M

```

```

VECT1180
VECT1190
VECT1200
VECT1210
VECT1220
VECT1240
VECT1250
VECT1260
VECT1270

```

```

5   C(J,J)=C(J,J)+EW
C   COPY CB MATRIX
   DO 199 J=1,M
   DO 199 K=1,M
199 S(J,K)=CMPLX(C(J,K),C(J,K+10))
C   INVERT REDUCED CB MATRIX
   CALL INVCX(S,MN)
C   MULTIPLY INVERSE*(-LAST COLUMN)
   DO 10 J=1,MN
   R(J)=0.
   DO 10 K=1,MN
10  R(J)=R(J)-S(J,K)*S(K,M)
   R(M)=1.
   WRITE(6,12)
12  FORMAT(9HVECTOR R,9X5HTHETA,11X17HCOMPLEX RESIDUALS)
C   CONVERT TO POLAR FORM
   DO 16 J=1,MN
   VM(J)=ABS(R(J))
   VT(J)=ATAN2(AIMAG(R(J)),REAL(R(J)))
16  VT(J)=AMOD(VT(J)+6.2831953,6.2831953)
   CALL VECNRM(VM,L,M,DJ)
   VM(M)=1.
   VT(M)=0.
   IMAX=0
   VMAX=1.
   DO 20 J=1,MN
   IF(VMAX-VM(J)) 17,20,20
17  VMAX=VM(J)
   IMAX=J
   VTHET=VT(IMAX)
20  CONTINUE
   IF(IMAX) 23,23,21
21  DO 22 J=1,M
   VM(J)=VM(J)/VMAX
22  VT(J)=VT(J)-VTHET
C   MULTIPLY VECTOR BY MATRIX FOR CHECK
23  DO 24 J=1,M
   CK(J)=0.
   DO 200 K=1,M
   SS = CMPLX(C(J,K),C(J,K+10))
200 CK(J)=CK(J)+SS*R(K)
   DC 201 N=1,M
   DO 201 K=1,M
201 S(N,K)=CMPLX(C(N,K),C(N,K+10))
24  WRITE (6,25)VM(J),VT(J),CK(J)
25  FORMAT(2F12.6, 1PE18.2,E11.2)
C*** FIND FIGURES OF MERIT
   E=EW
   U=-EW
   PMU=U+P(M)
   PMUP=M
   QMU=P(M+11)
   QMUP=0.
   MM1=M-1
   DO 108 J=1,MM1
   K=M-J
   CAA=K
   PMU=PMU*U+P(K)
   QMU=QMU*U+P(K+11)
   PMUP=PMUP*U+P(K+1)*CAA
108 QMUP=QMUP*U+P(K+12)*CAA
   R3=PMU/(PMUP*U)
   R4=QMU/(QMUP*U)
   MP=M+1
   WRITE(6,628)
   WRITE(6,629) (P(J),J=1,MP)
   WRITE(6,629) (P(J+11),J=1,M)
628 FORMAT(35HOCCHARACTERISTIC EQUATION AT FLUTTER)
629 FORMAT(1P8E16.7)
   WRITE(6,631) PMU,QMU,R3,R4
630 FORMAT(7H LAMDA=F10.4,8H DET= 1P2E11.4)
631 FORMAT(3HOP=1PE11.4,3H Q=E11.4,7H P/PIA=E11.4,7H Q/QIA=E11.4)

```

```

VECT1280
VECT1290
VECT1300
VECT1310
VECT1330
VECT1340
VECT1350
VECT1360
VECT1370
VECT1380
VECT1390
VECT1400
VECT1410
VECT1420
VECT1430
VECT1440
VECT1450
VECT1460
VECT1465
VECT1480
VECT1530
VECT1540
VECT1550
VECT1560
VECT1570
VECT1580
VECT1590
VECT1600
VECT1610
VECT1620
VECT1630
VECT1640
VECT1650
VECT1660
VECT1670
VECT1680
VECT1690
VECT1700
VECT1710
VECT1730
VECT1740
VECT1750
VECT1760
VECT1780
VECT1790
VECT1800
VECT1805
VECT1820
VECT1830
VECT1840
VECT1850
VECT1860
VECT1870
VECT1880
VECT1890
VECT1900
VECT1910
VECT1920
VECT1930
VECT1940
VECT1950
VECT1960
VECT1970
VECT1980
VECT1990
VECT2000
VECT2010
VECT2020
VECT2030
VECT2070
VECT2080
VECT2090

```

```

C          EVALUATE DETERMINANT FOR FLUTTER ALPHA AND MU*(1,1.02,.98)VECT2095
      DO 28 J=1,3                                VECT2100
      FL=J*(7-J-J)-5                              VECT2110
      FL=.02*FL                                    VECT2120
      DO 26 K=1,M                                  VECT2130
26      S(K,K)=S(K,K)+FL*EW                       VECT2140
      E=E*(1.+FL)                                  VECT2150
      CALL CXDET(M,X,Y,S)                          VECT2160
      U=ABS(E)                                      VECT2170
28      WRITE(6,630) U,X,Y                        VECT2180
99      RETURN                                     VECT2190
      END                                          VECT2200

```

```

C***      SUBROUTINE INVCX(R,N)                   INVC0020
      COMPLEX MATRIX INVERSION                   INVC0025
      COMPLEX R(10,10),D                       INVC0030
40      IF(N-1) 37,37,38                        INVC0040
37      R(1,1)=1./R(1,1)                        INVC0050
      GO TO 99                                   INVC0060
38      DO 41 K=1,N                              INVC0070
      D=R(K,K)                                   INVC0080
      R(K,K)=1.                                  INVC0090
50      DO 42 J=1,N                              INVC0100
42      R(K,J)=R(K,J)/D                         INVC0110
56      IF (K-N) 43,44,44                       INVC0120
43      KPLUS=K+1                               INVC0130
51      DO 41 I=KPLUS,N                         INVC0140
      D=R(I,K)                                   INVC0150
      R(I,K)=0.                                  INVC0160
52      DO 41 J=1,N                              INVC0170
41      R(I,J)=R(I,J)-D*R(K,J)                 INVC0180
44      NMINUS=N-1                              INVC0190
53      DO 45 K=1,NMINUS                        INVC0200
      KPLUS=K+1                                  INVC0210
54      DO 45 I=KPLUS,N                         INVC0220
      D=R(K,I)                                   INVC0230
      R(K,I)=0.                                  INVC0240
55      DO 45 J=1,N                              INVC0250
45      R(K,J)=R(K,J)-D*R(I,J)                 INVC0260
99      RETURN                                     INVC0270
      END                                          INVC0280

```

```

C          SUBROUTINE VECNRN(VM,L,MMAJ,DJAY)     VECN0020
      TO NORMALIZE VECTOR ON BASIS OF EQUAL MODAL RMS VECN0030
      DIMENSION VM(10),DJAY(10,10)             VECN0040
      EL=L                                       VECN0050
      VM(MMAJ)=1.                                VECN0060
      DO 20 J=1,MMAJ                             VECN0070
      VPM=DJAY(J,J)/EL                           VECN0080
      VPM=SQRT(VPM)                               VECN0090
20      VM(J)=VM(J)*VPM                          VECN0100
      MINUS=MMAJ-1                               VECN0110
      DO 30 J=1,MINUS                             VECN0120
30      VM(J)=VM(J)/VM(MMAJ)                    VECN0130
      RETURN                                     VECN0140
      END                                          VECN0150

```

```

C***      SUBROUTINE CXDET(MM,X,Y,R)            CXDT0401
      COMPLEX DETERMINANT                       CXDT0402
      COMPLEX R(10,10),A(10,10),DET,DSIGN,RUB,RA,AB CXDT0402
      M=MM                                       CXDT0404
      IF(M-1) 26,26,27                          CXDT0405
26      DET=R(1,1)                               CXDT0406
      GO TO 99                                   CXDT0407
27      DO 28 J=1,M                              CXDT0408
      DO 28 K=1,M                              CXDT0409

```

28	A(J,K)=R(J,K)	CXDT0410
	DSIGN=1.	CXDT0411
C	K LOOP	CXDT0412
	DO 30 LT=2,M	CXDT0413
	K=LT-1	CXDT0414
	IF(CABS(A(K,K)))5,7,5	CXDT0415
C	ZERO ON MAIN DIAGONAL, INTERCHANGE ROWS	CXDT0416
7	IF(M-K) 16,16,71	CXDT0417
71	L=LT	CXDT0418
14	DO 8 J=K,M	CXDT0419
	RUB=A(J,K)	CXDT0420
	A(J,K)=A(J,L)	CXDT0421
8	A(J,L)=RUB	CXDT0422
	DSIGN=-DSIGN	CXDT0423
	IF(CABS(A(K,K)))5,13,5	CXDT0424
C	ZERO STILL ON DIAGONAL	CXDT0425
13	L=L+1	CXDT0426
	IF(L-M)14,14,16	CXDT0427
C	REDUCTION LOOP	CXDT0428
5	RA= 1. /A(K,K)	CXDT0429
	DO 3 I=LT,M	CXDT0430
	AB=RA*A(I,K)	CXDT0431
	DO 3 J=LT,M	CXDT0432
3	A(I,J)=A(I,J)-AB*A(K,J)	CXDT0433
30	CONTINUE	CXDT0434
C	FORM PRODUCT OF DIAGONAL ELEMENTS	CXDT0435
4	DO 6 J=2,M	CXDT0436
6	A(J,J)=A(J,J)*A(J-1,J-1)	CXDT0437
98	DET=DSIGN*A(M,M)	CXDT0438
	X=REAL(DET)	CXDT0439
	Y=AIMAG(DET)	CXDT0440
99	RETURN	CXDT0441
C	MATRIX IS SINGULAR, UNREMOVABLE ZERO ON DIAG	CXDT0442
16	DSIGN=0.	CXDT0443
	GO TO 98	CXDT0444
	END	CXDT0445

	FUNCTION FMM(A1,A2,M,MBAR,ALPHA)	FMM 0070
	DIMENSION GAMMA(11)	FMM 0030
	COMMON GAMMA	FMM 0040
	GAM4=GAMMA(M)**4	FMM 0050
	FM01=FMKT(0,M,A1)	FMM 0060
	FM11=FMKT(1,M,A1)	FMM 0070
	FM21=FMKT(2,M,A1)	FMM 0080
	FM31=FMKT(3,M,A1)	FMM 0090
	IALF=ALPHA+1.	FMM 0100
	GO TO (5,3,4),IALF	FMM 0110
5	FMA01=FM01	FMM 0120
	FMA11=FM11	FMM 0130
	FMA21=FM21	FMM 0140
	FMA31=FM31	FMM 0150
	GO TO 2	FMM 0160
3	FMA01=FM11	FMM 0170
	FMA11=FM21	FMM 0180
	FMA21=FM31	FMM 0190
	FMA31=FMKT(4,M,A1)	FMM 0200
	GO TO 2	FMM 0210
4	FMA01=FM21	FMM 0220
	FMA11=FM31	FMM 0230
	FMA21=FMKT(4,M,A1)	FMM 0240
	FMA31=FMKT(5,M,A1)	FMM 0250
2	IF(M-MBAR)10,1,10	FMM 0260
1	FM02=FMKT(0,M,A2)	FMM 0270
	FM12=FMKT(1,M,A2)	FMM 0280
	FM22=FMKT(2,M,A2)	FMM 0290
	FM32=FMKT(3,M,A2)	FMM 0300
6	TERM1=0.25*A2*FMA01*FM02	FMM 0310
	TERM2=0.25*A2*(FMA11*FM32+FMA31*FM12)	FMM 0320
	TERM3=0.125*(FMA21*FM12+FMA11*FM22)	FMM 0330
	TERM4=0.25*A2*FMA21*FM22	FMM 0340

```

TERMS=0.375*(FMA01*FM32+FMA31*FM02)
FMM=TERM1+(TERM4+TERMS-TERM2-TERM3)/GAM4
RETURN
10 FM02=FMKT(0,MBAR,A2)
    FM12=FMKT(1,MBAR,A2)
    FM22=FMKT(2,MBAR,A2)
    FM32=FMKT(3,MBAR,A2)
    GAMB4=GAMMA(MBAR)**4
    FMM=(FMA31*FM02-FMA01*FM32+FMA11*FM22-FMA21*FM12)/(GAM4-GAMB4)
999 RETURN
END

```

```

FMM 0350
FMM 0360
FMM 0370
FMM 0380
FMM 0390
FMM 0400
FMM 0410
FMM 0420
FMM 0430
FMM 0440
FMM 0450

```

```

FUNCTION FMKT(K,M,T)
DIMENSION GAMMA(11)
COMMON GAMMA
SINH(EX)=0.5*(EX-1.0/EX)
COSH(EX)=0.5*(EX+1.0/EX)
GAM=GAMMA(M)
ARG=T*GAM
EX=EXP(GAM)
SH=(EX-1.0/EX)*0.5
EX=EXP(ARG)
K1=K+1
GO TO (1,2,3,4,1,2),K1
1 FMKT=(SIN(ARG)-SIN(GAM)*SINH(EX)/SH)*GAM**K
  GO TO 99
2 FMKT=(COS(ARG)-SIN(GAM)*COSH(EX)/SH)*GAM**K
  GO TO 99
3 FMKT=(-SIN(ARG)-SIN(GAM)*SINH(EX)/SH)*GAM**K
  GO TO 99
4 FMKT=(-COS(ARG)-SIN(GAM)*COSH(EX)/SH)*GAM**K
99 RETURN
END

```

```

FMKT0020
FMKT0030
FMKT0040
FMKT0050
FMKT0060
FMKT0070
FMKT0080
FMKT0090
FMKT0100
FMKT0110
FMKT0120
FMKT0130
FMKT0140
FMKT0150
FMKT0160
FMKT0170
FMKT0180
FMKT0190
FMKT0200
FMKT0210
FMKT0220

```

```

C*** FUNCTION BVF(NU,Z)
      BESSEL FUNCTION J0,J1
      DIMENSION BF(30)
      IF(Z-4.0)200,201,201
201 BVF = SUMM(NU,Z)
      RETURN
200 IF(Z)202,205,202
205 IF(NU)204,204,203
204 BVF=1.0
      RETURN
203 BVF=0.0
      RETURN
202 M=1.4*Z+6.5
      ERR=.000001
      NCODE=1
60 BVF=0.0
      X = 2.0/ Z
      FLG=ALOG(.5*Z)
2 C=-1.0
50 N=NU+M
      BF(N+1)=1.0
      BF(N+2)=0.0
      BF(N+3)=0.0
      A=1.0
53 CR=0.0
      DO 6 J=1,M
        I=N+1-J
        F=I
        BF(I)=F*X*A+C*CR
        CR=A
6 A=BF(I)
      IF (NU) 7,7,8
7 CM=1.0
  CN=2.0

```

```

BVF 0020
BVF 0025
BVF 0030
BVF 0040
BVF 0050
BVF 0060
BVF 0070
BVF 0080
BVF 0090
BVF 0100
BVF 0110
BVF 0120
BVF 0130
BVF 0140
BVF 0150
BVF 0160
BVF 0170
BVF 0180
BVF 0190
BVF 0200
BVF 0210
BVF 0220
BVF 0230
BVF 0240
BVF 0250
BVF 0260
BVF 0270
BVF 0280
BVF 0290
BVF 0300
BVF 0310
BVF 0320
BVF 0330
BVF 0340

```


	GO TO 13	BVF 0350
H	CM=1.0	BVF 0360
	DO 9 J=1,NU	BVF 0370
	F=J	BVF 0380
9	CM=CM*F	BVF 0390
10	CN=CM*(F+2.0)	BVF 0400
13	GO TO (14,20),NCODE	BVF 0410
14	SUM=CM*BF(NU+1)+CN*BF(NU+3)	BVF 0420
	K=NU+5	BVF 0430
	J=2	BVF 0440
12	F=J	BVF 0450
	G=NU	BVF 0460
	CN=CN*(G+2.*F)*(G+F-1.0)/(F*(G+2.*F-2.))	BVF 0470
	SUM=SUM+CN*BF(K)	BVF 0480
	IF (N-K) 30,16,16	BVF 0490
16	J=J+1	BVF 0500
	K=K+2	BVF 0510
	GO TO 12	BVF 0520
20	SUM=CM*BF(NU+1)+CN*BF(NU+2)	BVF 0530
	J=2	BVF 0540
	K=NU+3	BVF 0550
19	F=J	BVF 0560
	G=NU	BVF 0570
	CN=CN*(G+F)*(2.*G+F-1.0)/(F*(G+F-1.))	BVF 0580
	SUM=SUM+CN*BF(K)	BVF 0590
	IF (N-K) 30,17,17	BVF 0600
17	J=J+1	BVF 0610
	K=K+1	BVF 0620
	GO TO 19	BVF 0630
30	F=FLG	BVF 0640
	AM=NU	BVF 0650
	F=AM*F	BVF 0660
	GO TO (32,31),NCODE	BVF 0670
31	G=X	BVF 0680
	GO TO 33	BVF 0690
32	G=0.0	BVF 0700
33	AMF=F+G	BVF 0710
	AMF=EXP(AMF)	BVF 0720
	G = AMF/SUM	BVF 0730
	AMR=BF(NU+1)	BVF 0740
	BF(NU+1)=AMR*G	BVF 0750
	ER=BF(NU+1)-BFV	BVF 0760
	ER=ABS(ER)	BVF 0770
	BFV=BF(NU+1)	BVF 0780
	IF (ERR-ER) 43,34,34	BVF 0790
43	M=M+1	BVF 0800
	GO TO 50	BVF 0810
34	RETURN	BVF 0820
	END	BVF 0830

	FUNCTION SUMM(NU,X)	SUMM0020
	DIMENSION GAMMA(11),FREQ(31),COEFS(24),SAVE(14)	SUMM0030
	COMMON GAMMA,EPY,EPX,GMM,SS,T,Q,FREQ,SAVE,COEFS,BFDR,BETA,BSQ,SQK,	SUMM0040
	IEM,CK,S,PI	SUMM0050
	AR=4.0/X	SUMM0060
	ARG=AR*AR	SUMM0070
	INU=NU+1	SUMM0080
	GO TO (1,100),INU	SUMM0090
C	JC TO BE COMPUTED.	SUMM0100
1	THETA=X-PI*0.25	SUMM0110
	I=1	SUMM0120
	J=7	SUMM0130
101	PN=ARG*(ARG*(ARG*(ARG*(ARG*COEFS(I)+COEFS(I+1))+COEFS(I+2))+COEFS(I+3))+COEFS(I+4))+COEFS(I+5)	SUMM0140
	QN=AR*(ARG*(ARG*(ARG*(ARG*COEFS(J)+COEFS(J+1))+COEFS(J+2))+COEFS(J+3))+COEFS(J+4))+COEFS(J+5)	SUMM0150
	SUM*=SQRT(AR*0.5/PI)*(COS(THETA)*PN-SIN(THETA)*QN)	SUMM0160
999	RETURN	SUMM0170
C	J1 TO BE COMPUTED.	SUMM0180
100	THETA=X-0.75*PI	SUMM0190
	I=13	SUMM0200
	J=19	SUMM0210
	GO TO 101	SUMM0220
	END	SUMM0230
		SUMM0240
		SUMM0250

BIBLIOGRAPHY

1. Kobett, D. R., "Research on Panel Flutter," NASA CR-80 (1964).
2. Luke, Y. L., and A. D. St. John, "Supersonic Panel Flutter," WADC Technical Report 57-252 (1957).
3. Kobett, D. R., "Flutter of Multiple Streamwise Bay Panels at Low Supersonic Mach Number," NASA CR-538 (1966).
4. Bocher, M., "Introduction to Higher Algebra," The MacMillan Company (1936).
5. Yates, J. E., "A Study of Aeroelastic (Flutter) Behavior of Slender F Flexible Wing-Body Configurations in Hypersonic Flow," Midwest Research Institute Phase Report No. 1, Contract No. NAS1-2620 (1964).
6. "Handbook of Mathematical Functions," U. S. Department of Commerce publication (AMS55), p. 886 (1964).
7. Hansen, E. R., "On the Danilewski Method," J. Assn. Comput. Mach., January 1963.
8. Faddeeva, V. N., "Computational Methods of Linear Algebra," (Translated by C. D. Benster), Dover Publications, Inc., New York (1959).
9. Givens, W., "The Characteristic Value - Vector Problem," J. Assn. Comput. Mach., July, 1957.