

NASA CONTRACTOR REPORT



NASA CR-599

NASA CR-599

GPO PRICE \$ _____

CESTI PRICE(S) \$ 2.50

Hard Copy (HC) _____

Microfiche (MF) .75

ATTITUDE DETERMINATION USING A KALMAN FILTER

VOLUME II

by James L. Farrell

N 66 36301
(ACCESS CN NUMBER)
77
(PAGES)
CR-599
(NASA CR OR TRX CR AD NUMBER)

(CATEGORY)
1
(ACCESS)
14
(CATEGORY)

Prepared by
WESTINGHOUSE ELECTRIC CORPORATION
Baltimore, Md.
for Goddard Space Flight Center

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION • WASHINGTON, D. C. • SEPTEMBER 1966

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Prepared under Contract No. NAS 5-9195 by
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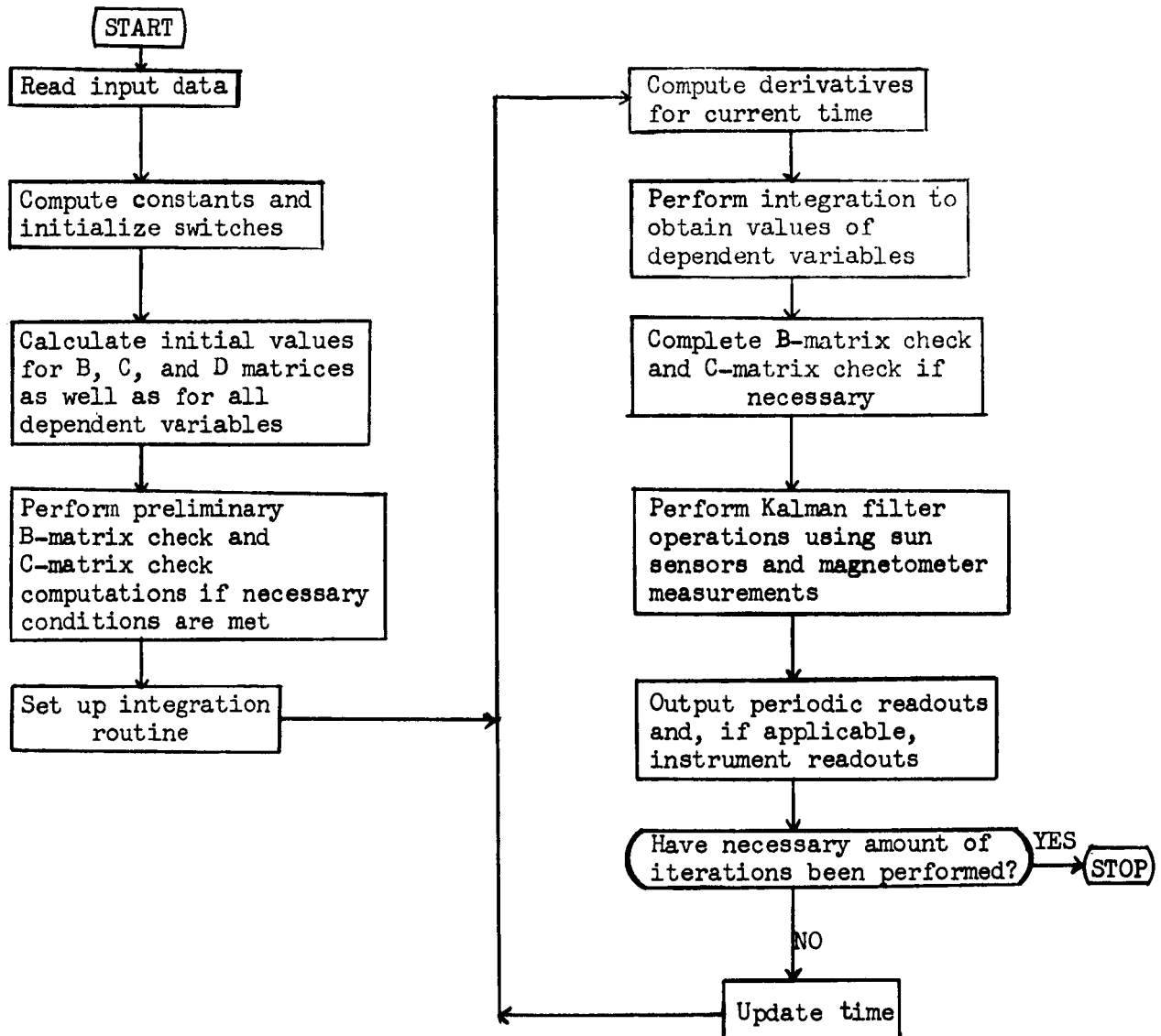
Section I. Introduction

This volume contains documentation of the computer program written under contract NAS5-9195. The program determines the attitude of an orbiting vehicle using a Kalman filter according to the analysis performed in Volume I of this report.

The program is written in FORTRAN IV with subroutines in FORTRAN and MAP. It is written for an IBM 7094 and has been successfully run on the Moonlight System at NASA. The naming of variables follows FORTRAN II conventions as to fixed and floating point names with most floating point variables being typed double precision. One large main program with a few small subroutines was originally intended but, due to compiler limitations, the creation of several other subroutines was necessary.

In addition to a description of the program and its usage, Volume II also contains a sample set of input data and a portion of the results generated from this data.

BLOCK DIAGRAM



Section II. Description of Routines

A. MAIN PROGRAM: JF

The main program performs the majority of the work required by the analysis. After the data is read-in and all necessary initialization is done, the initial values of the dependent variables are calculated.

The integration loop is then entered. The derivatives are calculated in BOX A (see part B of this section); the integration is performed by sub-routine DICE and the results of the integration are used in the Kalman filter logic in BOX C, followed by the periodic and instrument readouts.

When the required number of iterations have been performed, the program begins to process the next case.

B. SUBROUTINE DICE (P,T,TP,E1,E2,N,Y,DY,F,L,INDEX,I)

PURPOSE: DICE is a double precision routine designed to be used in conjunction with an integration subroutine (DINTEG) to provide a numerical solution of an Nth order system of linear and/or non-linear differential equations expressed as a system of N first order equations:

$$\dot{Y}_n = f_n(t, Y_1, Y_2, \dots, Y_n) \quad Y_n(t_0) = Y_{n,0}; \quad n = 1, 2, 3, \dots, N$$

where Y_n are the N dependent variables and t is the independent variable. The local error generated by the numerical process is controlled by adjusting the integration step size based on the relative error as estimated by extrapolation to zero step size.

The basic method of the DICE routine can be summarized as follows:

1. Use initial conditions for the N dependent variables as solutions at $t = t_0$ and adopt the maximum step size permissible.
2. Perform the computation (integration subroutine) to find the single step solution for the new value of the independent variable, t.
3. Halve the integration step size.
4. Solve the problem again (integration subroutine) from the last convergent point using two applications of the reduced step size.
5. Compute an extrapolated solution making use of both solutions.
6. Compare the two-step solution with the extrapolated solution.
7. If the two solutions are sufficiently close, the procedure is continued using the extrapolated solution as initial values at the updated time t.

8. If the two solutions are not sufficiently close, the reduced step size is again halved and the procedure restarted from step 4 using the conditions at the last convergent point.
9. If the two solutions agree too closely then the basic step is doubled and the procedure restarted at step 1 using the extrapolated solution at the new value of the independent variable.

The above briefly describes the method; however, additional details are given below.

The superscripts (I) and (II) refer to the one-step and two-step approximations respectively. The subscript $i + 1$ refers to the solution at the new value of the independent variable, i referring to the old value. $h = t_{i+1} - t_i$ is the step size. The one-step approximation is found by the method in the integration subroutine. The two-step approximation is found by halving the step size and computing a one-step approximation at time $t_i + h/2$. This approximation is then used as the starting point for another one-step approximation again using the halved value of step size. This two-step approximation then can be thought of as two one-step approximations.

The procedure used to automatically control the error is as follows:

1. An error estimate for each of the N dependent variables using extrapolation to zero step size is expressed as:

$$E_{n,i+1} = \frac{\begin{matrix} \text{(II)} \\ Y_{n,i+1} \end{matrix} - \begin{matrix} \text{(I)} \\ Y_{n,i+1} \end{matrix}}{2^A - 1}$$

where A is the order of integration.

2. These values of $E_{n,i+1}$ are added to the two-step results to obtain the extrapolated solutions:

$$(II) \\ Y_{n,i+1} = Y_{n,i+1} + E_{n,i+1}$$

3. A relative error term is next defined and computed for each variable:

$$R_{n,i+1} = \frac{E_{n,i+1}}{Y_{n,i+1}}$$

4. The maximum relative error $(R_{n,i+1})_{\max}$ is designated E and is tested against two bounds E1 and E2. E1 is to keep the integration step size from remaining too small and E2 is used to keep the interval from becoming too large. The program then halves the interval and repeats the step, continues at the same interval, or continues at twice the interval.
5. The subscript n of the maximum relative error is recorded in INDEX, an argument of the calling sequence, and if printed out, can be helpful in locating the trouble point in cases of non-convergence.

The arguments in the calling sequence are defined as:

- P - maximum allowable step size.
- T - independent variable.
- TP - value of independent variable at which DICE will provide entry to BOXC.
- E1 - lower error bound for controlling step size.
- E2 - upper error bound for controlling step size.
- N - number of dependent variables expressed as a fixed point variable or constant.
- Y - first dependent variable followed by the remaining N-1 dependent variables (must be dimensioned).
- DY - derivative of first dependent variable followed by the remaining N-1 derivatives in the same order as the corresponding dependent variables (must be dimensioned).

F - the first cell of at least 7N cells required by DICE for storage
(must be dimensioned).

L - a fixed point variable controlled by DICE to exit to the proper
section of the program calling DICE.

INDEX - records the subscript of the variable having the greatest relative
error.

I - order of integration (2, 3, or 4).

BOXA - statement number for derivative computations.

BOXB - statement number for supplementary computations after valid integration
step. Checks for end-of-case based on conditions of dependent variables
should be done in BOXB.

BOXC - statement number for print routine.

BOXD - statement number for non-convergence.

All floating point arguments are double precision.

The basic setup necessary to use the routine is as follows:

```

      .
      .
      .
      L = 4
S      CALL DICE(P, . . . . ., I)
      GO TO (BOXA, BOXB, BOXC, BOXD), L

BOXA   Evaluate N derivatives
      GO TO S

BOXB   Perform any necessary calculations after a valid integration step
      GO TO S

```

BOXC Print normal output

TP = TP+P

GO TO S

BOXD Dump or check print to determine reason for non-convergence

GO TO next case

This is a standard Westinghouse routine which has been used
locally for several years.

C. SUBROUTINE DINTEG (T, DT, N, Y, DY, F, J, I)

PURPOSE: DINTEG is a double precision routine designed to be used in conjunction with DICE to provide a second, third, or fourth order Runge-Kutta solution of an Nth order system of linear and/or non-linear differential equations expressed as a system of N first order equations.

The basic method of the DINTEG routine can be summarized as follows:

Given the initial conditions of the N dependent variables at time t_i , and their derivatives at time t_i , this routine will calculate a one-step approximation for each of the N dependent variables at time $t_i + h$, where h is the step size. Given the function

$$Y_n = f_n(t, Y_1, Y_2, Y_3, \dots, Y_n)$$

and the initial values

$$t_i; Y_{1,i}; Y_{2,i}; Y_{3,i}; \dots, Y_{n,i})$$

then a second order Runge-Kutta solution gives a one-step approximation of:

$$Y_{n,i+1} = Y_{n,i} + 1/2(K_{0,n} + K_{1,n})$$

where:

$$K_{0,n} = hf_n(t_i; Y_{1,i}; Y_{2,i}; \dots; Y_{n,i})$$

$$K_{1,n} = hf_n(t_{i+1}; Y_{1,i} + K_{0,1}; Y_{2,i} + K_{0,2}; \dots; Y_{n,i} + K_{0,n})$$

The third order Runge-Kutta solution gives an approximation of:

$$Y_{n,i+1} = Y_{n,i} + 1/6 (K_{0,n} + 4K_{1,n} + K_{2,n})$$

where:

$$K_{0,n} = hf_n(t_i; Y_{1,i}; Y_{2,i}; \dots; Y_{n,i})$$

$$K_{1,n} = hf_n(t_i + h/2; Y_{1,i} + 1/2 K_{0,1}; \dots; Y_{n,i} + 1/2 K_{0,n})$$

$$K_{2,n} = hf_n (t_i + h; Y_{1,i} + 2K_{1,1} - K_{0,1}; Y_{2,i} + 2K_{1,2} - K_{0,2}; \dots; Y_{n,i} + 2K_{1,n} - K_{0,n})$$

and the fourth order Runge-Kutta solution gives a one-step approximation of:

$$Y_{n,i+1} = Y_{n,i} + 1/6 (K_{0,n} + 2K_{1,n} + 2K_{2,n} + K_{3,n})$$

where

$$K_{0,n} = hf_n (t_i; Y_{1,i}; Y_{2,i}; \dots; Y_{n,i})$$

$$K_{1,n} = hf_n (t_{i+h/2}; Y_{1,i} + 1/2K_{0,1}; Y_{2,i} + 1/2K_{0,2}; \dots; Y_{n,i} + 1/2K_{0,n})$$

$$K_{2,n} = hf_n (t_{i+h/2}; Y_{1,i} + 1/2K_{1,1}; Y_{2,i} + 1/2K_{1,2}; \dots; Y_{n,i} + 1/2K_{1,n})$$

$$K_{3,n} = hf_n (t_{i+h}; Y_{1,i} + K_{2,1}; Y_{2,i} + K_{2,2}; \dots; Y_{n,i} + K_{2,n})$$

The arguments of the calling sequence are defined as:

T - independent variable - controlled by DINTEG

DT - step size - controlled by calling program

N - number of dependent variables

Y - dependent variables

DY - derivative of dependent variables

F - storage cells used by DICE and DINTEG (must be dimensioned)

J - fixed point variable controlled by DICE to enter proper section of DINTEG

I - order of integration (2, 3, or 4)

This is a standard Westinghouse routine which has been used locally for several years. In this program it is called exclusively by DICE.

D. FUNCTION RANNUM (SIGMA, XMEAN,I)

PURPOSE: To produce a normally distributed random number. A set of such numbers has the characteristics of a set of normally distributed random numbers with a given mean and standard deviation.

A uniformly distributed number U_j in the interval (0,1) is generated by UDRNRT. The normally distributed number, X_n , having a mean (m) and standard deviation (σ) is computed by the routine as follows:

$$V_i = \sqrt{-2 \log_e .5 (1 - |1 - 2 U_j|)}$$

$$X_n = m + \sigma \left[\text{sign}(U_j - .5) \left(V_i - \frac{a_0 + a_1 V_i + a_2 V_i^2}{1 + b_1 V_i + b_2 V_i^2 + b_3 V_i^3} \right) \right]$$

where $a_0 = 2.515517$	$b_1 = 1.432788$
$a_1 = .802853$	$b_2 = .189269$
$a_2 = .010328$	$b_3 = .001308$

The calling sequence is

$$XN = \text{RANNUM} (\text{SIGMA}, \text{XMEAN}, I)$$

where SIGMA is the standard deviation (floating point),

XMEAN is the mean of the sample (floating point),

I is the initial random number as a fixed point odd integer and

XN is the normally distributed random number.

This is a standard Westinghouse routine which has been used locally for several years.

E. FUNCTION UDRNRT (I)

PURPOSE: To produce a random number uniformly distributed in the interval (0,1) having a period of 2^{33} .

The routine is given a starter, I, from which it computes a uniformly distributed random number, U_j , in the interval (0,1) as follows:

$$I_j = M I_{j-1} \pmod{2^{35}} \text{ where } M = 5^{13}$$

$$\text{Then } U_j = I_j / 2^{35}$$

The calling sequence is

$$UJ = \text{UDRNRT}(I) \text{ where}$$

I is the initial random number as a fixed point odd integer and

UJ is the uniformly distributed random number (floating point)

This is a standard Westinghouse routine which has been used locally for several years.

F. FUNCTION ECCAN (EMM,E)

PURPOSE: To compute eccentric anomaly

The function subroutine ECCAN solves Kepler's equation

$EA = EMM + E \sin EA$ as follows:

$$E_0 = EMM + E \sin EMM (1 + E \cos EMM) \quad (1)$$

$$\Delta E = \frac{EMM - E_0 + E \sin E_0}{1 - E \cos E_0} \quad (2)$$

$$E_1 = E_0 + \Delta E \quad (3)$$

If E_0 and E_1 agree to within $.5 \times 10^{-13}$, then E_1 is accepted as the eccentric anomaly, EA. Otherwise, E_0 is replaced by E_1 , a new E_1 is computed, and the iteration continues.

This is a standard Westinghouse routine which has been used locally for several years.

G. SUBROUTINE CEE (A1, A2, A3, XMAT)

PURPOSE: To perform coordinate transformations

The routine performs a coordinate transformation based on the angles A1, A2, A3 and returns the resulting 3 x 3 matrix, XMAT, to the calling program. It is used to compute the matrixes C, HC, G, and HG.

H. SUBROUTINE EXTRA (B, HB, G, HG, SPRM, HSPRM, HSDP)

PURPOSE: To compute and write the error matrix.

The routine computes the error matrix, $B^T \cdot HB$, and outputs it along with the matrix HB. During checkout, additional output was obtained from EXTRA by means of the last five arguments in the calling sequence. These arguments could now be dropped without introducing any ill effects.

I. SUBROUTINE CHECK1

PURPOSE: To determine whether to use numerical integration or closed-form solution for the transition matrix, whether to compute the B-matrix check and the C-matrix check, and to perform preliminary calculations on the B-matrix and C-matrix check if they are to be computed.

The conditions are examined for the closed-form solution of the transition matrix as well as for the B-matrix and C-matrix checks and the corresponding switches are set accordingly. If the B-matrix check is to be used, the matrix EM is computed for later use. If the criteria for the C-matrix check are met, further calculations produce PSI11, PSI13, PSI21, PSI23.

If the C-matrix check is to be omitted, the reason for omission will appear in the output. The interpretation of this reason may be found in Section IV.

The variables required by this routine are contained in the named COMMON regions GET, GIVE, and OMEGA.

J. SUBROUTINE HELP

PURPOSE: To compute the closed form solution of the transition matrix.

If the closed form solution for PH is to be used, the necessary partial derivatives are computed and used to calculate the transition matrix.

In either case, several other matrices are computed in this routine in order to keep the size of the main program within the bounds of the compiler.

The variables required by this routine are contained in the named COMMON regions GET, GIVE, OMEGA, and XCIN.

SECTION III. Input

All input to the program is made from data cards which are expected to be read from FORTRAN logical unit 5. Each case requires exactly 5 cards.

A. Makeup of Data Cards

<u>Data Card #1</u>		Format 7F10.0	
FIELD #1	OIZ	Orbital inclination angle	radians
FIELD #2	OOZ	Longitude of ascending node	radians
FIELD #3	OWZ	Argument of perigee in vehicle orbit	radians
FIELD #4	OAPZ	Semi-major axis of orbit	Astronomical units in sun orbiter case. Statute miles in earth or- biter case.
FIELD #5	OEZ	Eccentricity of orbit	
FIELD #6	OTPZ	Time of perigee relative to start time of simulation	hours
FIELD #7	CTP	Total duration of simulation	
<u>Data Card #2</u>		Format 7F10.0	
FIELD #1	VI(1)	Principal moment of inertia about x-axis	kilogram- meters ²
FIELD #2	VI(2)	Principal moment of inertia about y-axis	kilogram- meters ²
FIELD #3	VI(3)	Principal moment of inertia about z-axis	kilogram- meters ²
FIELD #4	VQ	Displacement from center of pressure meters to center of gravity	
FIELD #5	VLQ	Vehicular elevation of the displace- ment vector from c.p. to c.g.	radians

FIELD #6	VPQ	Vehicular azimuth of the displacement vector from c.p. to c.g.	radians
----------	-----	--	---------

FIELD #7	VAV	Effective area of the vehicle	square meters
----------	-----	-------------------------------	---------------

Data Card #3

Format 7F10.0

FIELD #1	OBZD	Minimum allowable angle between sun line and sensor slit for which a sun sensor measurement will be allowed	radians
----------	------	---	---------

FIELD #2	OBYD	Maximum allowable deviation from right angle for which a sun sensor measurement will be allowed	radians
----------	------	---	---------

FIELD #3	SIGZ	Standard deviation of initial angular position uncertainty in each axis	radians
----------	------	---	---------

FIELD #4	SIGW	Standard deviation of initial angular rate uncertainty in each axis	radians/second
----------	------	---	----------------

FIELD #5	SIGS	Standard deviation of sun sensor error uncertainty in each axis	radians
----------	------	---	---------

FIELD #6	SIGB	Standard deviation of magnetometer error uncertainty in each axis	webers/sq. meter
----------	------	---	------------------

FIELD #7	TSO	Initial angular displacement of sun beyond vernal equinox (applies only to earth orbiter)	radians
----------	-----	---	---------

Data Card #4

Format 7F10.0

FIELD #1	ZI	Initial local Euler angle displacement about roll axis	radians
----------	----	--	---------

FIELD #2	Z2	Initial local Euler angle displacement about pitch axis	radians
----------	----	---	---------

FIELD #3	Z3	Initial local Euler angle displacement about yaw axis	radians
----------	----	---	---------

FIELD #4	WO1	Initial angular rate about roll axis	radians
----------	-----	--------------------------------------	---------

FIELD #5	WO2	Initial angular rate about pitch axis	radians
----------	-----	---------------------------------------	---------

FIELD #6	WO3	Initial angular rate about yaw axis	radians
----------	-----	-------------------------------------	---------

FIELD #7	PBO	Initial celestial longitude of the earth's magnetic pole (applies only to earth orbiter)	radians
----------	-----	--	---------

Data Card #5

Format 7110

FIELD #1	NS	Number of sun sensors (12 is the upper limit)
FIELD #2	M	Total number of measurement intervals
FIELD #3	NZ	=0 sun orbiter is simulated =1 earth orbiter is simulated
FIELD #4	NT	=0 transition matrix computed under torque free conditions =1 transition matrix computed with torques included
FIELD #5	NRS	Random number starter; must be a positive, odd integer
FIELD #6	not used	
FIELD #7	not used	

B. Illegal Practices - There are several input conditions which will result in erroneous results or will cause the program to halt. These inputs usually involve unrealistic or contradictory combinations of parameters.

1) Program stops

- a) Semi-major axis of orbit less than the radius of earth for an earth satellite.
- b) Nonrealisable combination of inertias (I_1, I_2, I_3).
(See Reference 28 of Volume I)

2) Practices leading to erroneous results

- a) $N_t = 0$ with high spin rates causes an inaccurate transition matrix.
- b) Significant oscillation angle rates with $N_c = 1$. (See condition 7 of Appendix F, Volume I.)
- c) High eccentricity for a sun orbiter introduces error in the solar pressure calculation.
- d) Either ω_{01} or both ω_{02} and ω_{03} chosen equal to zero causes inaccuracies in the closed form solution of the transition matrix. The zero condition may be satisfactorily simulated by giving the quantities a value on the order of 10^{-12} .

C. Inputs for Sample Case - The following are the input quantities used in obtaining the output seen in Section IV.

Col. 10	Col. 20	Col. 30	Col. 40	Col. 50	Col. 60	Col. 70
0.	0.	0.	4000.	0.	0.	.16666666
150.	200.	100.	0.	0.	0.	0.
1.	.7854	.1	.0001	.01	.000001	0.
.05	.03	.04	-.000049	.00122	.000061	0.
12	20	1	1	101		

SECTION IV. OUTPUT

All output appears on the printer (FORTRAN logical unit 6). There is no need for any operator action such as tape handling, on-line messages or key-ins.

A. Normal output for every run

- 1) Inputs - The 33 input values are output and labeled, both with their specific name and under the more general headings of ORBIT, VEHICLE, OBSERVATION, STATISTICAL, INITIAL CONDITIONS, and CONTROL.
- 2) Initial conditions - Prior to entering the integration loop, the initial values of several quantities are seen.
 - a) CROSI - Cross product of vectors POLI and VERI
 - b) POLI - Orbit pole unit vector in inertial coordinates
 - c) VERI - Local vertical unit vector in inertial coordinates
 - d) SUNI - Unit vector along sunline in inertial coordinates
(for earth orbiter only)
 - e) MAGI - Unit vector along magnetic field in inertial coordinates (for earth orbiter only)
 - f) CROSV - Cross product of vectors POLV and VERV
 - g) POLV - Orbit pole unit vector in vehicle coordinates
 - h) VERV - Local vertical unit vector in vehicle coordinates
 - i) SUNV - Unit vector along sunline in vehicle coordinates
(for earth orbiter only)
 - j) MAGV - Unit vector along magnetic field in vehicle coordinates (for earth orbiter only)
 - k) XA - Actual position and velocity of the vehicle
 - l) XO - Difference between actual and observed position and velocity. Position components are initialized at every

interval for both actual and observed values. Thus, the differences in position are zero at the start of the simulation.

- m) C-MATRIX CHECK OMITTED DUE TO XX - If the conditions for the computation of the C-matrix check have not been met, the number of the first test which failed appears in this message. There are twelve such tests arranged in the following order:

- i. Earth orbiter
- ii. Effective area of the vehicle equals zero
- iv. $z_1^2 + z_2^2 + z_3^2 \leq .01$
- v. $|\omega_{\theta 2} - \eta_0| \leq 0.1 \sqrt{3} \xi_2$
- vi. $I_1 > I_3$
- vii. $\xi_1 \xi_3 < 0$
- viii. $F_1 = (1 - 3\xi_1 - \xi_1 \xi_3) > 0$
- ix. $F_2 = F_1^2 + 16 \xi_1 \xi_3 > 0$
- x. $z_{11} \leq .1; z_{13} \leq .1; z_{21} \leq .1; z_{23} \leq .1$
- xi. $|\omega_{\theta 1} + \eta_0 z_3| < .01 (r_1 z_{11} + r_2 z_{21})$
- xii. $|\omega_{\theta 3} - \eta_0 z_1| < .01 (r_1 z_{13} + r_2 z_{23})$

- 3) Periodic readouts - The frequency of this type of output is determined by the user and is equal to the duration of the simulation in seconds (3600 times CTP) divided by the number of iterations (M)

- a) TIME - Number of seconds since start of simulation

M - Iteration count

GX, GY, GZ - Roll, pitch, and yaw angular displacement since last interval

- b) VERI - Current local vertical unit vector in inertial coordinates

- c) CROSV - Current cross product of vectors POLV and VERV. If the C-matrix check has been computed, the fourth number on this line represents the closed-form solution for the second value in the cross product. Otherwise, it is set to zero.
- d) POLV - Current orbital pole unit vector in vehicle coordinates. If the C-matrix check has been computed, the fourth number on this line represents the closed-form solution for the third component of the vector. Otherwise, it is set to zero.
- e) VERV - Current local vertical unit vector in vehicle coordinates. If the C-matrix check has been computed, the fourth number on this line represents the closed-form solution for the first component of the vector. Otherwise, it is set to zero.
- f) SUNV - Current unit vector along sunline in vehicle coordinates (for earth orbiter only).
- g) MAGV - Current unit vector along magnetic field in vehicle coordinates (for earth orbiter only).
- h) TRANSITION MATRIX - The 6×6 transition matrix appears under the heading .
- i) B-MATRIX - The 3×3 B matrix appears under the heading .
- j) B-MATRIX CHECK - The 3×3 matrix appears under the heading. If the B-matrix check has been computed, the matrix represents the closed form solution for the B-matrix. In a torque free case, it should equal the B-matrix; they should be approximately equal when torques are present. The matrix is set to zero if the computation of the B-matrix check has been omitted.

- k) XA - Actual position and velocity of the vehicle. The two numbers on the next line represent the magnitudes of the position and velocity vectors.
 - l) XR - Square root of the diagonal elements of the 6×6 uncertainty covariance matrix. The two numbers on the next line are the square root of the sum of the first three and last three values on the above line.
 - m) XP - Errors in Euler angles and angular rates. Since these are referenced to the coordinate frame corresponding to the preceding interval, the Euler angle uncertainties take on a meaning less significant than the off-diagonal terms of the error matrix (to be discussed later in this section). The two numbers on the next line are the magnitudes of the position and velocity vector errors respectively.
4. Instrument readouts - This output occurs at every iteration for each magnetometer which is in position with respect to the magnetic field and for each sun sensor which is in position with respect to the sunline. If no instrument is in position, this type of output is omitted for the current iteration.
- a) The first six lines are not labeled since they were originally intended only for debug purposes but were later deemed useful. They represent the 6×6 uncertainty covariance matrix.
 - b) INST. NO. = XX. For a magnetometer readout, instruments 1, 2, and 3 indicate roll, pitch, and yaw respectively. The sun sensors are arranged as follows:

Instrument Number	Field of View Axis	Direction of Slit
1	+ Roll	Pitch
2	+ Pitch	Yaw
3	+ Yaw	Roll
4	- Roll	Pitch
5	- Pitch	Yaw
6	- Yaw	Roll
7	+ Roll	Yaw
8	+ Pitch	Roll
9	+ Yaw	Pitch
10	- Roll	Yaw
11	- Pitch	Roll
12	- Yaw	Pitch

YA - In magnetometer readout, actual earth dipole flux density in webers/sq. meter.

- In sun sensor readout, actual measured value of angle Y (defined in Volume I).

NOTE: The first three sun sensor readouts are easily distinguished from the magnetometer readouts because the value of YA for the magnetometers is on the order of 10^{-5} while its value for the sun sensors normally ranges from 2.0 to 0.1.

H1A, H2A, H3A- Partial derivatives of the observable with respect to the rotational position state variables as computed from the actual vehicle orientation. These three values currently appear in the output as zero because the necessary calculations overloaded the compiler. The equations may be added as a subroutine at any time.

c) NR - Random number used in the computation of the observed position and velocity vectors.

YP - In magnetometer readout, predicted earth dipole flux density in webers/sq. meter.

- In sun sensor readout, predicted measured value of angle Y.

H1,H2,H3 - Partial derivatives of the observable with respect to the rotational position state variables as computed from the predicted vehicle orientation.

d) XR - Same as the XR discussed above with the exception that it is now computed from uncertainty covariance matrix, which is updated after each instrument readout.

e) XO - Difference between the actual and observed position and velocity vectors. The two numbers of the next line are the magnitudes of the position and velocity vector differences respectively.

f) W - Vector of optimum linear estimator coefficients.

5. End of Iteration - After each iteration, even when there was no instrument readout, the following printout occurs;

a) HB-MATRIX - Observed orthogonal transformation from vehicle to fixed inertial coordinates.

b) ERROR MATRIX - Product of B^{-1} times HB.

NOTE: Since the observed transformation and the actual transformation in this case are defined relative to the same inertial reference, the error matrix contains the net effect of all attitude errors present up to the current interval.

- c) The number that appears under the error matrix is the square root of the sum of the squares of terms (1,2), (2,3), and (3,1) of the error matrix where the first index is the row indicator and the second is the column indicator.

B. Diagnostic Messages

The program checks for certain undesirable conditions and outputs an explanatory message when one of these situations is detected. It then goes on to the next case.

1) Errors caused by illegal input

- a) TEST = XXXX WHEN SR = XXXX. The current value of TEST would result in attempting to compute the square root of a negative number. This erroneous value can only occur when the semi-major axis of the orbit (input variable OAPZ) is less than the radius of the earth in statute miles.
- b) INPUT MOMENTS OF INERTIA NOT REALIZABLE. The difference between any two moments of inertia cannot be greater than the third in a rigid body. The moments of inertia (inputs VI(1), VI(2), VI(3)) are printed out following the message.

2) Unrealistic trigonometric values

Several places throughout the program, an arccosine is calculated from the computed value of a cosine. Clearly, these cosines cannot be greater than 1. The following messages were useful in debugging the mathematical model as well as the program itself. They have remained in the program in order to prohibit analysis with meaningless data should some malfunction occur.

- a) $N = XX$. $LOOP = XXX$, $SLIU = XXX$. N is the instrument number; $LOOP$ is the iteration count and $SLIU$ is an intermediate variable in the computation of YA (actual angle between sun line and instrument) and must be less than 1.
- b) $N = XX$. $LOOP = XXX$, $SLIN = XXX$, $ZETAS = XXX$. N and $LOOP$ are as above; $SLIN$ divided by $ZETAS$ forms the cosine of YA and must be less than 1.
- c) $N = XX$. $LOOP = XXX$, $SDPU = XXX$. N and $LOOP$ are as above; $SDPU$ is an intermediate value in the computation of YP (predicted angle between sun line and instrument) and must be less than 1.
- d) $N = XX$. $LOOP = XXX$, $SDPL = XXX$, $HZS = XXX$. N and $LOOP$ are as above; $SDPL$ divided by HZS forms the cosine of YP and must be less than 1.
- e) TROUBLE IN ARCCOS. The cosine of $\angle_{hv}$ has been calculated to be greater than 1 in subroutine CHECK1. In addition to the message, the ten quantities that go into the computation are also printed out.

3. If the integration routine cannot converge, a PDUMP results.

C. Output from Sample Case

The following pages contain a portion of the results generated from the data cards listed in Section III. All the preliminary output is shown as well as the periodic and instrument readouts from the first and last (twentieth) iteration.

*** INPUTS ***

ORBIT	012=	0.	002=	0.	0M2=	0.	OATP=	4000.00000000
	0E2=	0.	0TP2=	0.				
VEHICLE	11=	150.00000000	12=	200.00000000	13=	100.00000000	VQ=	0.
	VLQ=	0.	VPQ=	0.	VAV=	0.		
OBSERVATION	NS=	12	0B2D=	1.00000000	0BYD=	0.78540000	M=	20
STAT.	SIGZ=	0.09999999	SIGW=	0.00000000	SIGS=	0.01000000	SIGB=	0.000000100
INIT.	Z1=	0.05000000	Z2=	0.02999999	Z3=	0.04000000	P80=	0.
	W02=	-0.00004900	W02=	0.00120000	W03=	0.00006100	T50=	0.
CONTROL	NZ=	1	NT=	1	CTP=	0.16666666	NRS=	101
CROSSI		-0.		1.00000000		0.		
POLI		0.		-0.		1.00000000		
VERI		1.00000000		0.		0.		
SUNI		1.00000000		0.		0.		
MAGI		0.19252197		0.		0.98129266		
CROSSV		0.99675049		0.04143731		-0.02793542		
POLV		-0.03997134		0.99789141		0.05113719		
VERV		0.02999549		-0.04995668		0.99830085		
SUNV		0.02999549		-0.04995668		0.99830085		
MAGV		-0.03344879		0.96960577		0.24237540		
XA		0.		0.		0.	-0.00004900	0.00122000
XD		0.		0.		0.	0.00011010	0.00005222
								-0.00000307

TIME=	29.9999833	M=	1	CX=	-0.00130654	GM=	0.03680594	GZ=	0.00181516
VERI	0.99932450				0.03684070	0.			
CROSV	0.99875060				0.04146658	-0.02789525	C11	0.03998602	C13
POLV	-0.04000519				0.99789449	0.05105063	C21	C22	0.04991054
VERV	0.02995341				-0.04987088	0.99830641	0.03003379	C32	C33
SUN0	-0.00065623				-0.05135416	0.99865832			
MAGV	-0.04011349				0.96935594	0.24236245			

TRANSITION MATRIX

0.99942919	0.00176237	0.00018770	-29.99184449	-0.04387668	-0.95734597
-0.00174256	0.99951407	-0.00003576	0.03224137	-29.99512768	0.03712121
0.03836773	0.00013714	0.99993790	-0.28855269	-0.01645527	-30.01691461
0.00008677	-0.00000077	-0.00001305	0.99842108	0.00113906	0.02566102
-0.00000030	0.00003228	0.00000238	-0.00041799	0.99951552	-0.00052785
-0.00009937	-0.00000469	0.00000106	-0.01897722	-0.00001541	0.99974332

B-MATRIX			B-MATRIX CHECK		
XA	0.00134744	-0.03661566	-0.00181636	-0.00004393	0.00122102
	0.03663644		0.00122334		0.00000000
XR	0.09993811	0.09999655	0.10011737	0.00010026	0.00010000
	0.17326402		0.00017335		0.00009999
KP	-0.00333004	-0.00161228	0.00006863	0.00011183	0.00005545
	0.00370046		0.00012495		-0.00000000
	0.0099762	0.00000020	0.00038571	0.00000057	-0.00000000
	0.00000020	0.00999931	0.00000000	-0.00000001	0.00000002
	0.00038571	0.00000034	0.01002348	-0.00000010	0.00000002
	0.00000057	-0.00000001	-0.00000010	0.00000001	0.00000000
	-0.00000000	0.00000002	0.00000002	0.00000000	-0.00000000
	-0.00000010	-0.00000004	-0.00000029	0.00000000	0.00000001
INST. NO.=	I	YA=	0.00000171	M1A=	-0.00000000
				M2A=	-0.00000003
NR=	-0.00000071	WP=	0.00000188	M1=	0.
				M2=	0.0000019
XR	0.03992648	0.09602190	0.04130232	0.00010026	0.00010000
	0.14460771		0.00017333		0.00009996
X0	-0.00427401	-0.00911893	-0.02445851	0.00011210	0.00005537
					-0.00000491

0.02645072

```

1066.31451416  8475.58911133  27706.13891602  0.00012513  0.08498897  -0.84913993
0.00998530    -0.00003777    0.00006559    0.00000057    -0.00000000    -0.00000008
-0.00009777    0.00922021    -0.00254330    0.00000001    0.00000001    0.00000003
0.00006539    -0.00254530    0.00170588    -0.00000001    -0.00000000    -0.00000004
0.00000057    0.00000001    -0.00000001    0.00000001    0.00000000    0.00000000
-0.00000000    0.00000001    -0.00000000    0.00000000    0.00000001    -0.00000000
-0.00000008    0.00000003    -0.00000004    0.00000000    -0.00000000    0.00000001

INST. NO.= 3      YA= 1.51941842  M1A= -0.00000000  M2A= -0.00000000  M3A= -0.00000000
NR= -0.00318899  YP= 1.49842587  M1 = -0.99999999  M2 = -0.00621978  M3 = 0.12808057
XR  0.01164067  0.09597985  0.04126818  0.00010009  0.00010000  0.00009995

```

0.10510035

```

X0  -0.01988449  -0.00956579  -0.02419449  0.00011121  0.00005538  -0.00000478
W   -0.98778310  -0.02827623  0.01670609  -0.00005675  0.00000034  0.00000818
0.00013088    -0.00037986    0.00023226    0.00000000    -0.00000000    -0.00000000
-0.00037986    0.00921213    -0.00254053    0.00000000    0.00000001    0.00000003
0.00023226    -0.00250053    0.00170306    -0.00000000    -0.00000000    -0.00000000
0.00000000    0.00000000    -0.00000000    0.00000001    0.00000000    0.00000000
-0.00000000    0.00000001    -0.00000000    0.00000000    0.00000001    -0.00000000
-0.00000000    0.00000003    -0.00000004    0.00000000    -0.00000000    0.00000001

INST. NO.= 9      YA= 1.57746141  M1A= -0.00000000  M2A= -0.00000000  M3A= -0.00000000
NR= 0.01330772  YP= 1.48859671  M1 = -0.00444664  M2 = -0.99878273  M3 = -0.07463337
XR  0.01078133  0.01044849  0.03243642  0.00010009  0.00010000  0.00009995

```

0.03574254

```

X0  -0.01574127  -0.11283800  0.00342166  0.00011119  0.00005520  -0.00000514
W   0.11398206
0.04053539    -1.01036856  0.27018404  -0.00000025  -0.00000168  -0.00000349

```

HB-MATRIX

ERROR MATRIX

```

-0.01891927    -0.05702077    0.99819371    0.99970139    -0.02180577    0.01102854
0.99964295    0.01762777    0.01996142    0.02173974    0.99974522    0.00607175
-0.01886890    0.99821496    0.05666436    -0.01115012    -0.00503018    0.99992075

```

0.02523612

TIME=	599.99996943	M=	20	CX=	0.00152341	GY=	0.03713800	GZ=	0.00175871
VER1	0.74318501			0.65708597	0.				
CRUSV	0.99919731			0.03270868	-0.02312732	C11	0.03078592	C13	
PULV	-0.03225874			0.99928799	0.01956759	C21	C22	0.01889952	
VERV	0.02375069			-0.01880582	0.99954101		C32	C33	
SUNV	-0.65031399			-0.03581221	0.75839042				
MAGV	-0.15046063			0.97379526	0.17056145				
TRANSITION MATRIX									
	0.99971369	0.00018587	-0.00062907	-29.99529386	-0.00510046	-0.84125425			
	-0.00022113	0.9996196	-0.00001293	0.00372640	-29.99867368	0.03838499			
	0.03334866	0.00003419	0.99965001	-0.24717700	-0.01569536	-30.00974438			
	0.00005635	0.00001174	0.00004130	0.99998001	0.00008047	0.02191122			
	0.00000066	0.00003584	0.00000038	-0.00005003	0.99987298	-0.00052549			
	0.00003141	-0.00000182	0.00000220	-0.01737799	-0.00093773	0.99945277			
B-MATRIX									
	-0.65039761	-0.03586113	0.75931806	0.	0.	0.			
	0.75047984	0.01172589	0.65159100	0.	0.	0.			
	-0.03225874	0.99928799	0.01956759	0.	0.	0.			
B-MATRIX CHECK									
XA	-0.00152447	-0.03714396	-0.00175992	0.00005131	0.00123856	0.00005724			
	0.03721695			0.00124095					
XR	0.00857292	0.00479179	0.01344602	0.00001847	0.00001387	0.00003858			
	0.01664800			0.00004496					
XP	-0.00052679	0.00332821	0.00154828	0.00001316	-0.00011926	-0.00005124			
	0.00370833			0.00013107					
	0.00007349	0.00000521	-0.00005759	-0.00000013	-0.00000000	0.00000011			
	0.00000521	0.00002286	-0.00001269	-0.00000000	-0.00000005	0.00000003			
	-0.000005759	-0.00001269	0.00018079	0.00000004	0.00000002	-0.00000045			
	-0.000000213	-0.00000000	0.00000004	0.00000000	-0.00000000	-0.00000000			
	-0.000000000	-0.00000005	0.00000002	-0.00000000	0.00000000	-0.00000000			
	0.000000011	0.00000003	-0.00000005	-0.00000000	-0.00000000	0.00000000			
INST. #3= 1	YA=	0.00000480	H1A=	-0.00000000	H2A=	-0.00000000	H3A=	-0.00000000	
YR=	0.00000151	YR=	0.00000527	H1 =	0.	H2 =	0.00000850	H3 =	0.00002907
XR	0.00843587	0.00477902	0.01255819	0.00001842	0.00001386	0.00003665			
	0.01586594			0.00004330					
XO	-0.00201473	0.00316899	0.00624797	0.00001945	-0.00011893	-0.00006302			

0.00728953									
-1419.68252563	-151.91398811	4484.07849121	0.00013600	1.23030491	0.32222372	-11.24645090			
0.00007118	0.00000496	-0.00005028	-0.00000013	-0.00000000	-0.00000000	0.00000000			
0.00000496	0.00002284	-0.00001191	-0.00000000	0.00000000	-0.00000005	0.00000003			
-0.000005028	-0.00001191	0.00015771	0.00000004	0.00000000	0.00000002	-0.00000039			
-0.00000013	-0.00000000	0.00000004	0.00000000	0.00000000	-0.00000000	-0.00000000			
-0.00000000	-0.00000005	0.00000002	-0.00000000	-0.00000000	0.00000000	-0.00000000			
0.00000009	0.00000003	-0.00000039	-0.00000000	-0.00000000	-0.00000000	0.00000000			
INST. NO. = 9 YA = 2.28000534 H1A = -0.00000000 H2A = -0.00000000 H3A = -0.00000000									
NR = -0.00159872	YP = 2.27273029	H1 = 0.02339360	H2 = -0.99989582	H3 = -0.03198076					
XR 0.00843549	0.00433038	0.01254765	0.00001842	0.00001290		0.00003661			
0.01572747									
X0 -0.00209326	0.00213057	0.00651231	0.00001949	-0.00011633		-0.000006379			
0.00716459									
W -0.01383517	-0.18293860	0.04656979	0.00000601	0.00045828		-0.00013521			
HB-MATRIX									
-0.64613497	-0.03636406	0.76235638	0.99980085	0.01918313		-0.00550101			
0.76149011	0.03655954	0.64714465	-0.01926733	0.99959132		-0.01568504			
-0.05140421	0.99865964	0.00406846	0.00519842	0.01578791		0.99986184			
ERROR MATRIX									
0.02531870									

APPENDIX A: GLOSSARY

The purpose of this glossary is to relate program names to the engineering symbols defined in Volume I and to define those variables which are introduced in the program itself. It is meant to contain all major parameters of interest as well as most of the intermediate variables.

The Glossary in Volume I is referenced for all variables defined in that volume. Section III of Volume II (Input) is referenced for the description of all input quantities.

<u>PROGRAM SYMBOL</u>	<u>ENGINEERING SYMBOL</u>	<u>DESCRIPTION</u>
A(I,J)	$a_{i,j}$	Volume I
ABC	A_c	Cosine of $\omega_A \tau$
ABSI	A_s	Sine of $\omega_A \tau$
ABETA	$ \beta $	Magnitude of magnetic flux density
ACP	A'_c	Cosine of $(\omega'_A t + \alpha_{kh})$
AHV	α_{hv}	Angle between the angular momentum vector and vector V
ALSC		Cosine of angle between spin axis and angular momentum vector as computed from observed attitude (for transition matrix)
ALSS		Sine of angle between spin axis and angular momentum vector as computed from observed attitude (for transition matrix)
ASCP	α_c	Cosine of angle between spin axis and angular momentum vector
ASKH	α_{kh}	Angle between initial yaw axis and angular momentum vector
ASKV	α_{kv}	Angle between initial yaw axis and vector V
ASSP	α_s	Sine of angle between spin axis and angular momentum vector
ASUBK	α_k	Difference between α_{kv} and α_{kh}
ASUEM	A_m	Mean anomaly of satellite
ASP	A'_s	Sine of $(\omega'_A t + \alpha_{kh})$
AZ	a_o	Semi-major axis in meters
B(I,J)	$B_{i,j}$	Volume I
BBC	B_c	Cosine of $\omega_s \tau$
BBS	B_s	Sine of $\omega_s \tau$
BCHK (I,J)		B-check matrix
BCP	B'_c	Cosine of $(\omega'_s t - \alpha_k)$

<u>PROGRAM SYMBOL</u>	<u>ENGINEERING SYMBOL</u>	<u>DESCRIPTION</u>
BDUM(I,J)		Intermediate array used in the computation of BDUM
BETA(I)	β_i	Volume I
BETAP(I)	β''_i	Volume I
BSP	B'_s	Sine of $(\omega'_B t - \alpha_k)$
BTSP(I)	β_i	Volume I
C(I,J)	$C_{i,j}$	Volume I
CAHV		Cosine of α_{hv}
CAK		Cosine of α_k
CAKH		Cosine of α_{kh}
CAPEZ		Eccentric anomaly
CCHK1		First term in the C-matrix check
CCHK2		Second term in the C-matrix check
CCHK3		Third term in the C-matrix check
CHX(I)		Cosines of the observed position state variables
CIC	i_c	Volume I
CIS	i_s	Volume I
COMC	α_c	Cosine of α_c
COSAKV		Cosine of α_{kv}
CSUBB	c_β	Earth magnetic field constant
CSUBH	c_h	Solar measurement sensitivity constant
CTHDS	$\dot{\theta}_s$	Time derivative of solar true anomaly
CTHE		Cosine of θ
CTP	T'	Input

<u>PROGRAM SYMBOL</u>	<u>ENGINEERING SYMBOL</u>	<u>DESCRIPTION</u>
CUEM	$[\omega_B/m]$	Earth magnetic field constant
CUC		Cosine of $(\omega_0 + \theta_0)$
CWS		Volume I
D(I,J)	$D_{i,j}$	Volume I
DELA(I)		Variables of differentiation in transition matrix derivation
DELBA(I)		Variables of differentiation in transition matrix derivation
DELF1(I)		Variables of differentiation in transition matrix derivation
DELF2(I)		Variables of differentiation in transition matrix derivation
DELG1(I)		Variables of differentiation in transition matrix derivation
DELG2(I)		Variables of differentiation in transition matrix derivation
DELG3(I)		Variables of differentiation in transition matrix derivation
DELK(I)		Variables of differentiation in transition matrix derivation
DELL(I)		Variables of differentiation in transition matrix derivation
DELX1(I)		Variables of differentiation in transition matrix derivation
DELX2(I)		Variables of differentiation in transition matrix derivation
DELX3(I)		Variables of differentiation in transition matrix derivation
EL(I,J)	$L_{i,j}$	Volume I
ELL(I,J)	$Ll_{i,j}$	Volume I
EM(I,J)	$M(I,J)$	Intermediate array in the computation of B-matrix check

<u>PROGRAM SYMBOL</u>	<u>ENGINEERING SYMBOL</u>	<u>DESCRIPTION</u>
ERR1		Lower error limit for the integration routine
ERR2		Upper error limit for the integration routine
ETAZ	η_0	Volume I
FG(I)	f_{γ_i}	Scalar products in non-homogeneous transition matrix derivation
FS(I)	f_{s_i}	Scalar products in non-homogeneous transition matrix derivation
F1	F_1	Intermediate variable in closed form transition matrix solution
F2	F_2	Intermediate variable in closed form transition matrix solution
F7N(I)		Storage array required by DICE
G(I,J)	$G_{i,j}$	Volume I
GAM(I,J)	$\Gamma_{i,j}$	Volume I
GNU(I,J)	$V_{i,j}$	Volume I
HB(I,J)	$B_{i,j}$	Volume I
HBTSP(I)	$\hat{\beta}_i$	Volume I
HC(I,J)	$\hat{C}_{i,j}$	Volume I
HCAPF(I,J)	$\hat{F}_{i,j}$	Parameters in the observed equations of motion
HCAPN(I)	N_i	Volume I
HCSUBH	$\hat{c}_h$	Solar measurement sensitivity constant using observed quantities
HDUM(I)		Intermediate array used in the calculation of PP
HFG(I)	$\hat{f}_{\gamma_i}$	Scalar products in non-homogeneous transition matrix (computed from observed values)
HFS(I)	$\hat{f}_{s_i}$	Scalar products in non-homogeneous transition matrix (computed from observed values)

<u>PROGRAM SYMBOL</u>	<u>ENGINEERING SYMBOL</u>	<u>DESCRIPTION</u>
HG(I,J)	$\hat{G}_{i,j}$	Volume I
HGAM(I,J)	$\hat{r}_{i,j}$	Volume I
HGNU(I,J)	$\hat{g}_{i,j}$	Volume I
HIA(I)	$H_i A$	Measurement sensitivities computed from actual attitude (Actual computations not in present program)
HH(I)	$\hat{H}_i$	Volume I
HLOWF(I,J)	$\hat{f}_{i,j}$	Parameters in the observed equations of motion
HSDP(I)	$\hat{s}''_i$	Volume I
HSPRM(I)	$\hat{s}'_i$	Volume I
HU	$\hat{\mu}$	Volume I
HW01	$\hat{\omega}_{o1}$	Observed angular rate about roll axis
HW02	$\hat{\omega}_{o2}$	Observed angular rate about pitch axis
HW03	$\hat{\omega}_{o3}$	Observed angular rate about yaw axis
HX(I)	$\hat{x}_i$	Observed position and velocity state variables
HXD(I)	$\hat{\dot{x}}_i$	Derivatives of observed position and velocity state variables
HZETAS	$\hat{J}_s$	Sine of the observed angle, $\mathcal{J}$
HZ1	$\hat{z}_1$	Observed local Euler angle displacement about roll axis
HZ2	$\hat{z}_2$	Observed local Euler angle displacement about pitch axis
HZ3	$\hat{z}_3$	Observed local Euler angle displacement about yaw axis
INDEX		Index of the most widely varying dependent variable
IORD		Order of integration

<u>PROGRAM SYMBOL</u>	<u>ENGINEERING SYMBOL</u>	<u>DESCRIPTION</u>
IWHY		Indicator of the reason for omission of the C-matrix check
KTR		Magnetometer counter
LOOP	m	Iteration counter
LQQQ		Control variable in the integration routine
M	M	Input
MAG		Switch set in program =1; use magnetometers =2; skip magnetometers
N		Sun sensor index
NRS	NRS	Input
NS	N_s	Input
NSUBB	N_b	=1; compute the B-matrix check =2; omit the B-matrix check
NSUBC	N_c	=1; compute the C-matrix check =2; omit the C-matrix check
NSUBM	N_m	=1; compute closed form transition matrix =2; integrate to solve for the transition matrix
NT	N_t	Input
NVAR		Number of dependent variables
NZ	N_o	Input
OAPZ	a_o	Input
OBYD	Y_{Δ}	Input
OBZD	J_{Δ}	Input
OEZ	e_o	Input
OIZ	i_o	Input
OOZ	ω_o	Input
OSA	ω_A	Spin rate as computed from observed state

<u>PROGRAM SYMBOL</u>	<u>ENGINEERING SYMBOL</u>	<u>DESCRIPTION</u>
OSB	ω_B	Precession as computed from observed state
OTPZ	t'_0	Input
OWZ	ω_0	Input
OYZ	ω_{yz}	$\sqrt{\omega_2^2 + \omega_3^2}$
PBO	ψ_{β_0}	Input
PH(I,J)	$\phi_{i,j}$	Transition matrix; Volume I
PHD(I,J)	$\dot{\phi}_{i,j}$	Derivative of transition matrix
PI	π	Pi, to 16 significant digits
PM(I,J)	$P^{(-)}_{i,j}$	Volume I
PMDUM(I,J)		Intermediate array used in the computation of PM
PP(I,J)	$P^{(+)}_{i,j}$	Volume I
PSIB	ψ_{β}	Volume I
PSI2	ψ_2	Volume I
PSI11	ψ_{11}	Volume I
PSI13	ψ_{13}	Volume I
PSI21	ψ_{21}	Volume I
PSI23	ψ_{23}	Volume I
PSUBC	P_c	Cosine of $\omega_p t$
PSUBP	P_p	Volume I
PSUBS	P_s	Sine of $\omega_p t$
PZ	P_0	Parameter of orbit
Q(I)	q_i	Volume I
QKB(I)	k_{β_i}	Volume I
QKBDR	$K_{\beta} \cdot R$	Dot product of K_{β} and R

<u>PROGRAM SYMBOL</u>	<u>ENGINEERING SYMBOL</u>	<u>DESCRIPTION</u>
QLBC	λ_{bc}	Cosine of λ_b
QQ(I,J)		Intermediate array in the calculation of the B-matrix check
QSC	k_c	Cosine of $\hat{\omega}_{o3}/\omega_{yz}$
QSS	k_s	Sine of $\hat{\omega}_{o2}/\omega_{yz}$
R(I)	r_i	Volume I
RANDOM	N_R	Random number
RHO	ρ	Volume I
RHOX(I)	pXi	Predicted state
RR(I,J)		Intermediate array in the computation of the B-matrix check
RT1	r_1	Volume I
RT2	r_2	Volume I
R11	R_{11}	Parameter in libration analysis
R13	R_{13}	Parameter in libration analysis
R21	R_{21}	Parameter in libration analysis
R23	R_{23}	Parameter in libration analysis
R31	R_{31}	Parameter in libration analysis
R33	R_{33}	Parameter in libration analysis
R41	R_{41}	Parameter in libration analysis
R43	R_{43}	Parameter in libration analysis
SAHV		Sine of α_{hv}
SAK		Sine of α_k
SAKH		Sine of α_{kh}
SDPL(I)	$\hat{s}'' \cdot L$	Dot product of $\hat{s}''$ and L
SDPU(I)	$\hat{s}'' \cdot U$	Dot product of $\hat{s}''$ and U

<u>PROGRAM SYMBOL</u>	<u>ENGINEERING SYMBOL</u>	<u>DESCRIPTION</u>
SHX(I)		Sines of the observed position state variables
SIC	i_f	Sine of i_o
SIGB	σ_B	Input
SIGS	σ_S	Input
SIGW	σ_w	Input
SIGZ	σ_z	Input
SOMC	Ω_c	Sine of Ω_o
SPRM(I)	s'_i	Volume I
SR	r	Volume I
SSRL(I)	s_i	Volume I
SSP(I)	s''_i	Volume I
STHE		Sine of θ
SX(I)		Sines of the position state variables
SUF	μ_i	Sine of $(\omega_o + \theta_o)$
T	T	Duration of simulation in seconds
TAU	τ	Interval between measurements
TERM1		Intermediate variable used in several calculations
TERM2		Intermediate variable used in several calculations
TESL		Intermediate value used in the test for shadow
TESR		Intermediate value used in the test for shadow
TEST		Intermediate value used in the test for shadow
THES	θ_s	Volume I

<u>PROGRAM SYMBOL</u>	<u>ENGINEERING SYMBOL</u>	<u>DESCRIPTION</u>
THETA	θ	Volume I
THETAL	θ_{m-1}	Volume I
TM	t	Time; independent variable in the integration
TP		Box C entry time; see Volume II, Section II, B
TSO	θ_{so}	Input
TZ	t_o	Time at perigee in seconds (relative to reference time at start of simulation)
U	μ	Volume I
UA(I,J)	$U_{i,j}$	Volume I
VAV	A_v	Input
V(I)		Vector about which the angular momentum precesses
VDP(I)		Vector V in vehicle coordinates
VI(I)	I_i	Input
VLQ	λ_Q	Input
VPQ	ψ_Q	Input
VQ	q	Input
VXH		Magnitude of the cross product of V and H
W(I)	W_i	Volume I
WDUM(I)		Intermediate array used in the computation of W
WSAP	ω'_A	Volume I
WSBP	ω'_B	Volume I
WSUBP	ω_f	Volume I
WOI	ω_{o1}	Input

<u>PROGRAM SYMBOL</u>	<u>ENGINEERING SYMBOL</u>	<u>DESCRIPTION</u>
W02	ω_{02}	Input
W03	ω_{03}	Input
X(I)	X_i	Position and velocity state variables
XD(I)	$\dot{X}_i$	Derivatives of position and velocity state variables
XDIFF(I)		Difference between actual and observed position and velocity
XIC	J_c	Cosine of limiting plane angle, J
YA	Y_A	Actual value of observable
YP	Y_P	Predicted value of observable
YOUc		Cosine of $(\omega_0 + \theta)$
YOUF		Sine of $(\omega_0 + \theta)$
ZB11	Z_{11}	Parameter in libration analysis
ZB13	Z_{13}	Parameter in libration analysis
ZB21	Z_{21}	Parameter in libration analysis
ZB23	Z_{23}	Parameter in libration analysis
ZE1	ξ_1	Volume I
ZE2	ξ_2	Volume I
ZE3	ξ_3	Volume I
ZETAS		Sine of J
ZMEAN		Mean for the computed random numbers
ZSQ		ZE2 for symmetric vehicle
Z1	Z_1	Input
Z2	Z_2	Input
Z3	Z_3	Input

APPENDIX B: Program Listings

Due to the volume of the listings, this table of contents is provided as an aid in finding the listing of any particular routine.

Main Program	B-2
DICE	B-19
DINTEG	B-23
RANNUM	B-25
UDRNRT	B-28
ECCAN	B-29
CEE	B-30
EXTRA	B-31
CHECK1	B-32
HELP	B-37

C MAIN PROGRAM
\$EXECUTE IBJOB
\$IBJOB
\$IBFTG JF

COMMON/OMEGA/ HW01,HW02,HW03,RT1,RT2,ZB11,ZB13,ZB21,ZB23
COMMON/XCIN/X,TAU,CHX,SHX,HG,GAM,STHE,CTHE,THETA,COMC,SOMC,
ICIC,SIC,G,SPRM,PM,PP,PMOUM,IM,CWS,PBO,QKB,QLBC,QKBP,R,SR,QKBDR,
2BETA,CSUBB,SRUB,BETAP,OWZ
COMMON/GIVE/NT,NZ,OAPZ,VAV,VQ,OEZ,ZE1,ZE2,ZE3,D,VI,
IETAZ,T,SSP,B,C,PSUBP,Z1,Z2,Z3,W01,W02,W03
COMMON/GET/NSUBB,NSUBC,NSUBM,NVAR,EM,PSI11,PSI13,PSI21,PSI23
1,WSAP,WSBP,ASKH,ASUBK,WSUBP,ASCP,ASSP,CAHV,SAHV
DOUBLE PRECISION V,VDP,QQ,RR,EM,BCHK,ECCAN,CAPEZ,TERM1
DOUBLE PRECISION PSI11,PSI13,PSI21,PSI23,DUM,RT1,RT2,
IZB11,ZB13,ZB21,ZB23,8TSP,8BTSP,ABETA,HBETAP,
3ASP,ACP,BCP,BSP,PSUBC,PSUBS,PSI2,CCHK1,CCHK2,CCHK3
DOUBLE PRECISION WSAP,WSBP,ASKH,ASUBK,WSUBP,ASCP,ASSP,CAHV,SAHV
DOUBLE PRECISION PI,CIS,CTHDS,CWS,CUBM,QLBC,ACON,PSUBP,AZ,TZ,T,U,
IETAZ,CSUBB,PZ,COMC,SOMC,CIC,SIC,ZE1,ZE2,ZE3,RHO,UC,QM,TAU,
2XIC,ASUBM,THETA,CUC,SUF,
3HW01,HW02,HW03,
4TDIFF,THETA,THDIF,CTHE,STHE,SR,THES,THX2,SRUB,YOUUC,YOUUF,PSIB,
5QKBDR,TEST,IESL,TESR,OUTA,OUTB,OUTC,OUTD,OUTE,OUTF,OUTG,OUTH,
6OUTI,OUTJ,OUTK,OUTL,C64,SLIN,SLIU,ZDUM,ZETAS,YA,CSUBH,SDPU,
7SDPL,HZETAS,YP,HCSUBH,SCALAR,PSUM1,PSUM2,APXM1,APXM2
DOUBLE PRECISION OQZ,DIZ,Z1,Z2,Z3,VLQ,VPQ,OBZD,PBO,TSD
DOUBLE PRECISION GNU,Q,HGNU,HH,D,C,B,X,XD,HC,HB,HX,HXD,PH,PHD,
1PP,SSP,QKB,QKBP,SS,XDIFF,F7N,GAM,SSRL,SPRM,G,SCX,CHX,CHX,
2FS,FG,HGAM,HSPRM,HG,HFS,HFG,HGAPF,HLOWF,A,ZEE,RHOX,BDUM,PM,
3PMOUM,R,CAPN,HIA,HSDP,HCAPN,M,ADUM,WDUM,HDUM,PDIAG,APX
4,BETA,BETAP,VI
DIMENSION V(3),VDP(3),QQ(3,3),RR(3,3),EM(3,3),BCHK(3,3)
DIMENSION GNU(3,3),Q(3),VI(3),HGNU(3,3),HH(6),EL(12,3),
1D(3,3),C(3,3),B(3,3),X(48),XD(48),HC(3,3),HB(3,3),HX(6),HXD(6),
2PH(6,6),PHD(6,6),PP(6,6),SSP(3),QKB(3),QKBP(3),SS(3),XDIFF(6),
3F7N(350),GAM(3,3),SSRL(3),SPRM(3),G(3,3),SX(3),SHX(3),CX(3),
4CHX(3),FG(3),FS(3),HGAM(3,3),HSPRM(3),HG(3,3),HFG(3),HFS(3),
5HCAPF(3,3),HLOWF(3,3),A(3,3),ZEE(3),RHOX(6),BDUM(3,3),PM(6,6),
6PMOUM(6,6),R(3),UA(12,3),CAPN(3),HIA(6),HSDP(3),HCAPN(3),W(6),
7ADUM(6),WDUM(6,6),HDUM(6,6),PDIAG(6),APX(6),BTSP(3),HBTSP(3)

```

8,BETA(3),BETAP(3),EL(12,3),HBETAP(3)
DATA((EL(I,J),J=1,3),I=1,12)/1.,0.,0.,0.,1.,0.,0.,0.,1.,
1.,0.,0.,0.,-1.,0.,0.,0.,-1.,0.,0.,0.,0.,1.,0.,0.,0.,1.,
2.,0.,0.,0.,-1.,0.,0.,0.,-1.,/
DATA((EL(I,J),J=1,3),I=1,12)/0.,0.,-1.,-1.,0.,0.,-1.,0.,0.,
10.,1.,0.,0.,0.,1.,0.,0.,0.,0.,1.,0.,0.,0.,-1.,
20.,0.,0.,-1.,-1.,0.,0./
EQUIVALENCE (X(7),HX(1)),(XD(7),HDX(1)),(X(13),PH(1)),(XD(13),
1PHD(1)),(ZEI,ZEE(1))
DATA((UA(I,J),J=1,3),I=1,12)/0.,1.,0.,0.,0.,1.,0.,0.,1.,0.,
10.,0.,1.,1.,0.,0.,0.,0.,1.,1.,0.,0.,1.,0.,0.,1.,1.,
20.,0.,0.,1.,0./

```

C SETTING CONSTANTS

```

PI = 3.141592653589793
CIS = 23.5*PI/180.
CTHDS = 2.*PI/(365.*24.*3600.)
CMS = 7.292E-05
CUBM = 1.E 17
DUM = 78.9*PI/180.
QLBC = DCOS(DUM)
ZMEAN = 0.0
C64 = DCOS(64.*PI/180.)

```

C READING DATA

```

999 CONTINUE
READ(5,1000) DAV,FRA,OMZ,OAPZ,DEZ,OTPZ,CTP,(VI(I),I=1,3),VQ,VLQ,
1VPQ,VAV,OBZD,OBZD,SIGZ,SIGW,SIGS,SIG8,TSO,Z1,Z2,Z3,W01,W02,
2W03,P80
READ(5,1001) NS,M,NZ,NT,NRS
OIZ = DAV
DOZ = FRA
WRITE(6,1002) OIZ,DOZ,OMZ,OAPZ,DEZ,OTPZ,(VI(I),I=1,3),VQ,VLQ,
1VPQ,VAV,NS,OBZD,OBZD,M,SIGZ,SIGW,SIGS,SIG8,Z1,Z2,Z3,P80,
2W01,W02,W03,TSO,NZ,NT,CTP,NRS
LOOP = 0
IF(NZ) 1,1,2
NZ = 2
PSUBP = .9E-05/(OAPZ**2)
AZ = OAPZ*9.E 07*1610.
TZ = OTPZ*3600.
T = CTP*3600.

```

```

19  U = 0.0
    ETAB = DSQRT(1.325E 20)/DSQRT(AZ**3)
    DO 19 I = 1,3
    SS(I) = 0.0
    QK8(I) = 0.0
    QKBP(I) = 0.0
    GO TO 3
2   PSUBP = .9E-05
    QK8(3) = DSIN(DUM)
    AZ = OAPZ*1610.
    TZ = OTPZ*3600.
    T = CTP*3600.
    U = 3.986E 14
3   ETAB = DSQRT(U)/DSQRT(AZ**3)
    CSUBB = -CUBM/(4.*PI)
    PZ = AZ*(1.-OEZ**2)
    COMC = DCOS(OOZ)
    SOMC = DSIN(OOZ)
    CIC = DCOS(OIZ)
    SIG = DSIN(OIZ)
    ZE1 = (VI(3)-VI(2))/VI(1)
    ZE2 = (VI(1)-VI(3))/VI(2)
    ZE3 = (VI(2)-VI(1))/VI(3)
    DO 15 K=1,3
    IF(DABS(ZEE(K))-1.) 15,15,16
    WRITE(6,1019)(ZEE(I),I=1,3)
    GO TO 400
15  CONTINUE
    RHO = PSUBP*VAV
    Q(1) = VQ*DCOS(VLQ)*DCOS(VPQ)
    Q(2) = VQ*DCOS(VLQ)*DSIN(VPQ)
    Q(3) = VQ*DSIN(VLQ)
    DO 4 I = 1,3
    DO 4 J = 1,3
    IF(I-J) 5,6,5
5   GNU(I,J) = RHO*Q(I)/VI(J)
    GO TO 4
6   GNU(I,J) = 0.0
4   CONTINUE
    IF(NT) 7,7,8

```

```

7  HU = 0.0
   DO 10 I = 1,3
   DO 10 J = 1,3
10  HGNU(I,J) = 0.0
   GO TO 11
8  HU = U
   DO 9 I = 1,3
   DO 9 J = 1,3
9  HGNU(I,J) = GNU(I,J)
11  QM = M
   TAU = T/QM
   XIC = DCOS(OBZD)
   HH(4) = 0.0
   HH(5) = 0.0
   HH(6) = 0.0
   ASUBM = -ETAZ*TZ
   CAPEZ = ECCAN(ASUBM,OEZ)
   TERM1 = (DCOS(CAPEZ)-OEZ)/(1.-OEZ*DCOS(CAPEZ))
   IF(TERM1)5401,5402,5401
5402 THETA = (CAPEZ*PI)/(2.*DABS(CAPEZ))
      GO TO 5405
5401 IF(DABS(TERM1)-1.)5403,5403,5404
5404 WRITE(6,1041)
1041 FORMAT(27HTROUBLE IN ARCCOS FOR THETA)
      GO TO 999
5403 THETA = (CAPEZ/DABS(CAPEZ))*DATAN(DSQRT(1.-TERM1**2)/TERM1)
5405 CONTINUE
   CUC = DCOS(OMZ+THETA)
   SUF = DSIN(OMZ+THETA)
   D(1,1) = -COMC*SUF-SOMC*CIC*CUC
   D(1,2) = SOMC*SIC
   D(1,3) = COMC*CUC-SOMC*CIC*SUF
   D(2,1) = -SOMC*SUF+COMC*CIC*CUC
   D(2,2) = -COMC*SIC
   D(2,3) = SOMC*CUC+COMC*CIC*SUF
   D(3,1) = SIC*CUC
   D(3,2) = CIC
   D(3,3) = SIC*SUF
   CALL CEE(Z1,Z2,Z3,C)
   DO 25 I = 1,3

```

```

25      DO 25 J = 1,3
         B(I,J) = D(I,1)*C(1,J)+D(I,2)*C(2,J)+D(I,3)*C(3,J)
26      DO 26 L = 1,3
         X(L) = 0.0
         X(4) = W01
         X(5) = W02
         X(6) = W03
         HZ1 = RANUM(SIGZ,ZMEAN,NRS)+Z1
         HZ2 = RANUM(SIGZ,ZMEAN,NRS)+Z2
         HZ3 = RANUM(SIGZ,ZMEAN,NRS)+Z3
         HW01 = RANUM(SIGW,ZMEAN,NRS)+W01
         HW02 = RANUM(SIGW,ZMEAN,NRS)+W02
         HW03 = RANUM(SIGW,ZMEAN,NRS)+W03
         CALL CEE(HZ1,HZ2,HZ3,HC)
         DO 30 I = 1,3
         DO 30 J = 1,3
30      HB(I,J) = D(I,1)*HC(1,J)+D(I,2)*HC(2,J)+D(I,3)*HC(3,J)
31      DO 31 L = 1,3
         HX(L) = 0.0
         HX(4) = HW01
         HX(5) = HW02
         HX(6) = HW03
         DO 50 IJ = 1,6
50      XDIF(IJ) = HX(IJ)-X(IJ)
         DO 35 I = 1,6
         DO 35 J = 1,6
35      PP(I,J) = 0.0
         SIGZ2 = SIGZ**2
         DO 36 I = 1,3
36      PP(I,I) = SIGZ2
         SIGW2 = SIGW**2
         DO 37 I = 4,6
37      PP(I,I) = SIGW2
         GO TO (41,42),NZ
42      SSP(1) = -C(3,1)
         SSP(2) = -C(3,2)
         SSP(3) = -C(3,3)
         GO TO 45
41      QK8(1) = QLBC*DCOS(PB0)
         QK8(2) = QLBC*DSIN(PB0)

```

```

46      DO 46 I = 1,3
         QKBP(I) = B(1,I)*QKB(1)+B(2,I)*QKB(2)+B(3,I)*QKB(3)
         SS(1) = DCOS(TSO)
         SS(2) = DCOS(CIS)*DSIN(TSO)
         SS(3) = DSIN(CIS)*DSIN(TSO)
         DO 47 I = 1,3
            SSP(I) = B(1,I)*SS(1)+B(2,I)*SS(2)+B(3,I)*SS(3)
47      WRITE(6,1003) ((D(I,J),I=1,3),J=1,3),SS,QKB,((C(K,L),L=1,3),
45      1K=1,3),SSP,QKBP,((X(I1),I1=1,6),(XDIF(IJ),IJ=1,6)
         CALL CHECK1
         BEGINNING OF RECURSION LOOP
C
C
C      SETTING UP ICE CALLING SEQUENCE
         TM = 0.0
         TP = 0.0
         ERR1 = 1.E-10
         ERR2 = 1.E-08
         IORD = 4
C      INITIALIZE PHI ARRAY
         DO 54 I = 1,6
         DO 54 J = 1,6
         IF(I-J) 52,53,52
52      PH(I,J) = 0.0
         GO TO 54
53      PH(I,J) = 1.0
54      CONTINUE
55      LQQQ=4
60      CALL DICE(TAU, TM, TP, ERR1, ERR2, NVAR, X, XD, F7N, LQQQ, INDEX, IORD)
         GO TO (100,200,300,400),LQQQ
C      BOX A
100      TDIFF = ETAB*(TM-TZ)
         CAPEZ = ECCAN(TDIFF,OEZ)
         TERM1 = (DCOS(CAPEZ)-OEZ)/(1.-OEZ*DCOS(CAPEZ))
         IF(TERM1) 5406,5407,5406
5407      THETA = (CAPEZ*PI)/(2.*DABS(CAPEZ))
         GO TO 5410
5406      IF(DABS(TERM1)-1.)5408,5408,5409
5409      WRITE(6,1042)
1042      FORMAT(29H8D ARCCOS FOR THETA IN BOX A)
         GO TO 999

```

```

5408 THETA = (CAPEZ/DABS(CAPEZ))*DATAN(DSQRT(1.-TERM1**2)/TERM1)
5410 CONTINUE
      THDIF = THETA-THETA
      CTHE = DCOS(THDIF)
      STHE = DSIN(THDIF)
      DO 101 I = 1,3
101   GAM(I,3) = C(3,I)*CTHE+C(1,I)*STHE
      GO TO (102,103),NZ
102   SR = PZ/(1.+OEZ*DCOS(THETA))
      THES = TSO+CTHDS*TM
      SSR(1) = DCOS(THES)
      SSR(2) = DCOS(CIS)*DSIN(THES)
      SSR(3) = DSIN(CIS)*DSIN(THES)
      DO 104 I = 1,3
104   SPRM(I) = B(1,I)*SSRL(1)+B(2,I)*SSRL(2)+B(3,I)*SSRL(3)
      GO TO 107
103   SR = 1.0
      DO 106 I = 1,3
106   SPRM(I) = -GAM(1,3)
107   DO 110 I = 1,3
      SX(I) = DSIN(X(I))
      CX(I) = DCOS(X(I))
      CALL CEE (X(1),X(2),X(3),G)
      DO 111 I = 1,3
111   FG(I) = G(1,I)*GAM(1,3)+G(2,I)*GAM(2,3)+G(3,I)*GAM(3,3)
      FS(I) = G(1,I)*SPRM(1)+G(2,I)*SPRM(2)+G(3,I)*SPRM(3)
      SRCUB = SR**3
      XD(1) = -X(4)+(SX(2)/CX(2))*(X(6)*CX(1)-X(5)*SX(1))
      XD(2) = -X(5)*CX(1)-X(6)*SX(1)
      XD(3) = -(1./CX(2))*(X(6)*CX(1)-X(5)*SX(1))
      XD(4) = ZE1*(-X(5)*X(6)+3.*U*FG(3)*FG(2)/SRCUB)+GNU(2,1)*FS(3)-
      GNU(3,1)*FS(2)
      XD(5) = ZE2*(-X(6)*X(4)+3.*U*FG(1)*FG(3)/SRCUB)+GNU(3,2)*FS(1)-
      GNU(1,2)*FS(3)
      XD(6) = ZE3*(-X(4)*X(5)+3.*U*FG(2)*FG(1)/SRCUB)+GNU(1,3)*FS(2)-
      GNU(2,3)*FS(1)
      C      OBSERVED QUANTITIES
      DO 115 I = 1,3
115   HGAM(I,3) = HC(3,I)*CTHE+HC(1,I)*STHE
      GO TO (116,118),NZ

```

```

116 DO 117 J = 1,3
117 HSPRM(J) = HB(1,J)*SSRL(1)+HB(2,J)*SSRL(2)+HB(3,J)*SSRL(3)
GO TO 120
118 DO 122 I = 1,3
122 HSPRM(I) = -HGAM(1,3)
120 DO 125 I = 1,3
SHX(I) = DSIN(HX(I))
CHX(I) = DCOS(HX(I))
CALL CEE (HX(1),HX(2),HX(3),HG)
DO 128 I = 1,3
HFG(I) = HG(1,I)*HGAM(1,3)+HG(2,I)*HGAM(2,3)+HG(3,I)*HGAM(3,3)
HFS(I) = HG(1,I)*HSPRM(1)+HG(2,I)*HSPRM(2)+HG(3,I)*HSPRM(3)
HXD(1) = -HX(4)+(SHX(2)/CHX(2))*HX(6)*CHX(1)-HX(5)*SHX(1)
HXD(2) = -HX(5)*CHX(1)-HX(6)*SHX(1)
HXD(3) = -(1./CHX(2))*HX(6)*CHX(1)-HX(5)*SHX(1)
HXD(4) = ZE1*(-HX(5)*HX(6)+3.*HU*HFG(3)*HFG(2)/SRCUB)+HGNU(2,1)*
1HFS(3)-HGNU(3,1)*HFS(2)
HXD(5) = ZE2*(-HX(6)*HX(4)+3.*HU*HFG(1)*HFG(3)/SRCUB)+HGNU(3,2)*
1HFS(1)-HGNU(1,2)*HFS(3)
HXD(6) = ZE3*(-HX(4)*HX(5)+3.*HU*HFG(2)*HFG(1)/SRCUB)+HGNU(1,3)*
1HFS(2)-HGNU(2,3)*HFS(1)
C PHI EQUATIONS - SET UP
IF(NT) 130,130,131
131 HCAPF(1,1) = 0.0
HCAPF(1,2) = HFS(3)*CHX(1)-HFS(2)*SHX(1)
HCAPF(1,3) = HSPRM(1)*HG(2,1)-HSPRM(2)*HG(1,1)
HCAPF(2,1) = -HFS(3)
HCAPF(2,2) = HFS(1)*SHX(1)
HCAPF(2,3) = HSPRM(1)*HG(2,2)-HSPRM(2)*HG(1,2)
HCAPF(3,1) = HFS(2)
HCAPF(3,2) = -HFS(1)*CHX(1)
HCAPF(3,3) = HSPRM(1)*HG(2,3)-HSPRM(2)*HG(1,3)
HLOWF(1,1) = 0.0
HLOWF(1,2) = HFG(3)*CHX(1)-HFG(2)*SHX(1)
HLOWF(1,3) = HGAM(1,3)*HG(2,1)-HGAM(2,3)*HG(1,1)
HLOWF(2,1) = -HFG(3)
HLOWF(2,2) = HFG(1)*SHX(1)
HLOWF(2,3) = HGAM(1,3)*HG(2,2)-HGAM(2,3)*HG(1,2)
HLOWF(3,1) = HFG(2)
HLOWF(3,2) = -HFG(1)*CHX(1)

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```

HLOWF(3,3) = HGAM(1,3)*HG(2,3)-HGAM(2,3)*HG(1,3)
ACON = 3.*HU/SRCUB
DO 135 K = 1,3
  K1 = MOD(K,3)+1
  K2 = MOD(K+1,3)+1
  DO 135 L = 1,3
    135 A(K,L) = ZEE(K)*ACON*(HFG(K2)*HLOWF(K1,L)+HFG(K1)*HLOWF(K2,L))+
      HGNU(K1,K)*HCAPF(K2,L)-HGNU(K2,K)*HCAPF(K1,L)
      GO TO 140
130 DO 138 I = 1,3
  DO 138 J = 1,3
138 A(I,J) = 0.0
      PHI EQUATIONS - DERIVATIVES
140 THX2 = SHX(2)/CHX(2)
      GO TO (60,145),NSUBM
145 CONTINUE
      DO 150 I = 1,6
        PHD(1,I) = HXD(2)*THX2*PH(1,I)-(HXD(3)/CHX(2))*PH(2,I)-PH(4,I)-
          1THX2*SHX(1)*PH(5,I)+THX2*CHX(1)*PH(6,I)
        PHD(2,I) = HXD(3)*CHX(2)*PH(1,I)-CHX(1)*PH(5,I)-SHX(1)*PH(6,I)
        PHD(3,I) = (-HXD(2)/CHX(2))*PH(1,I)+HXD(3)*THX2*PH(2,I)+
          1(SHX(1)/CHX(2))*PH(5,I)-(CHX(1)/CHX(2))*PH(6,I)
        PHD(4,I) = A(1,I)*PH(1,I)+A(1,2)*PH(2,I)+A(1,3)*PH(3,I)-ZE1*
          1HX(6)*PH(5,I)-ZE1*HX(5)*PH(6,I)
        PHD(5,I) = A(2,I)*PH(1,I)+A(2,2)*PH(2,I)+A(2,3)*PH(3,I)-ZE2*
          1HX(6)*PH(4,I)-ZE2*HX(4)*PH(6,I)
        PHD(6,I) = A(3,I)*PH(1,I)+A(3,2)*PH(2,I)+A(3,3)*PH(3,I)-ZE3*
          1HX(5)*PH(4,I)-ZE3*HX(4)*PH(5,I)
        GO TO 60
      BOX B
200 CONTINUE
      GO TO 60
      BOX C
300 IF(DABS(TM)-.0001) 4093,4093,3332
3332 DO 301 I = 1,6
301 RHOX(I) = HX(I)
      CALL HELP
      DO 672 I = 1,3
      BTSP(I) = G(I,1)*BETAP(1)+G(I,2)*BETAP(2)+G(I,3)*BETAP(3)
      HBTSP(I) = HB(1,I)*BETA(1)+HB(2,I)*BETA(2)+HB(3,I)*BETA(3)
672

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321 ABETA = DSQRT(BETA(1)**2+BETA(2)**2+BETA(3)**2)
    GO TO (321,322),NZ
    TEST = 1.-(6.4E 06/SR)**2
    IF(TEST) 329,330,330
329 WRITE(6,1005) TEST,SR
    GO TO 999
330 TESR = -DSQRT(TEST)
    TESL = D(1,3)*SSRL(1)+D(2,3)*SSRL(2)+D(3,3)*SSRL(3)
    IF(TESL-TESR) 331,331,332
331 DO 333 I = 1,3
    DO 333 J = 1,3
    GNU(I,J) = 0.0
333 HGNU(I,J) = 0.0
    GO TO 322
332 DO 334 I = 1,3
    DO 334 J = 1,3
    IF(I-J) 335,336,335
335 GNU(I,J) = RHO*Q(I)/VI(J)
    GO TO 334
336 GNU(I,J) = 0.0
334 CONTINUE
    IF(NT) 337,337,338
337 DO 339 I = 1,3
    DO 339 J = 1,3
    HGNU(I,J) = 0.0
339 DO 340 K = 1,3
    DO 340 L = 1,3
    HGNU(K,L) = GNU(K,L)
    C PERIODIC READOUTS
340 LOOP = LOOP+1
322 OUTA = DSQRT(X(1)**2+X(2)**2+X(3)**2)
    OUTB = DSQRT(X(4)**2+X(5)**2+X(6)**2)
    OUTC = DSQRT(PM(1,1))
    OUTD = DSQRT(PM(2,2))
    OUTE = DSQRT(PM(3,3))
    OUTF = DSQRT(PM(4,4))
    OUTG = DSQRT(PM(5,5))
   OUTH = DSQRT(PM(6,6))
    OUTI = DSQRT(PM(1,1)+PM(2,2)+PM(3,3))
    OUTJ = DSQRT(PM(4,4)+PM(5,5)+PM(6,6))

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```

DO 341 L = 1,6
  XDIFF(L) = RHOX(L)-X(L)
  OUTK = DSQRT(XDIFF(1)**2+XDIFF(2)**2+XDIFF(3)**2)
  OUTL = DSQRT(XDIFF(4)**2+XDIFF(5)**2+XDIFF(6)**2)
  GO TO (801,802), NSUBB
801 ACP=DCOS(WSAP*TM+ASKH)
    ASP=DSIN(WSAP*TM+ASKH)
    BCP=DCOS(WSBP*TM-ASUBK)
    BSP=DSIN(WSBP*TM-ASUBK)
    PSUBC=DCOS(WSUBP*TM)
    PSUBS = DSIN(WSUBP*TM)
    QQ(1,1)=ASCP
    QQ(1,2)=ASSP*ASP
    QQ(1,3)=ASSP*ACP
    QQ(2,1)=0.0
    QQ(2,2)=ACP
    QQ(2,3)=-ASP
    QQ(3,1)=-ASSP
    QQ(3,2)=ASCP*ASP
    QQ(3,3)=ASCP*ACP
    RR(1,1)=QQ(1,1)
    RR(1,2)=QQ(1,2)
    RR(1,3)=QQ(1,3)
    RR(2,1)=BCP*QQ(2,1)+BSP*QQ(3,1)
    RR(2,2)=BCP*QQ(2,2)+BSP*QQ(3,2)
    RR(2,3)=BCP*QQ(2,3)+BSP*QQ(3,3)
    RR(3,1)=-BSP*QQ(2,1)+BCP*QQ(3,1)
    RR(3,2)=-BSP*QQ(2,2)+BCP*QQ(3,2)
    RR(3,3)=-BSP*QQ(2,3)+BCP*QQ(3,3)
    QQ(1,1)=CAHV*RR(1,1)+SAHV*RR(3,1)
    QQ(1,2)=CAHV*RR(1,2)+SAHV*RR(3,2)
    QQ(1,3)=CAHV*RR(1,3)+SAHV*RR(3,3)
    QQ(2,1)=RR(2,1)
    QQ(2,2)=RR(2,2)
    QQ(2,3)=RR(2,3)
    QQ(3,1)=-SAHV*RR(1,1)+CAHV*RR(3,1)
    QQ(3,2)=-SAHV*RR(1,2)+CAHV*RR(3,2)
    QQ(3,3)=-SAHV*RR(1,3)+CAHV*RR(3,3)
    RR(1,1)=QQ(1,1)
    RR(1,2)=QQ(1,2)

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```

RR(1,3)=QQ(1,3)
RR(2,1)=PSUBC*QQ(2,1)-PSUBS*QQ(3,1)
RR(2,2)=PSUBC*QQ(2,2)-PSUBS*QQ(3,2)
RR(2,3)=PSUBC*QQ(2,3)-PSUBS*QQ(3,3)
RR(3,1)=PSUBS*QQ(2,1)+PSUBC*QQ(3,1)
RR(3,2)=PSUBS*QQ(2,2)+PSUBC*QQ(3,2)
RR(3,3)=PSUBS*QQ(2,3)+PSUBC*QQ(3,3)
DO 803 I=1,3
DO 803 J=1,3
803 BCHK(I,J)=EM(I,1)*RR(1,J)+EM(I,2)*RR(2,J)+EM(I,3)*RR(3,J)
GO TO 805
802 DO 804 I=1,3
DO 804 J=1,3
804 BCHK(I,J)=0.0
805 GO TO (807,808),NSUBC
807 PS12=DATAN2(W02-ETAZ,ETAZ*Z2*DSQRT(3.*ZE2))
CCHK1=ZB13*DCOS(RT1*TM+PSI13)-ZB23*DCOS(RT2*TM+PSI23)
CCHK2=ZB11*DCOS(RT1*TM+PSI11)-ZB21*DCOS(RT2*TM+PSI21)
CCHK3=DSQRT(Z2**2+(ETAZ-W02)**2/(3.*ZE2*ETAZ**2))*DCOS(PSI2+DSQRT
1(3.*ZE2)*ETAZ*TM)
GO TO 810
808 CCHK1=0.0
CCHK2=0.0
CCHK3=0.0
810 WRITE(6,1006)TM,LOOP,G(3,2),G(1,3),G(2,1),D(I,3),I=1,3),(C(1,I),
1I=1,3),CCHK1,(C(2,J),J=1,3),CCHK2,(C(3,K),K=1,3),CCHK3,(SSP(L),
2L=1,3),(QKBP(I),I=1,3),(PH(J,K),K=1,6),J=1,6)
WRITE (6,1023) ((B(I,J),J=1,3),(BCHK(I,K),K=1,3),I=1,3),
1(X(I),I=1,6),OUTA,OUTB,OUTC,OUTD,OUTE,OUTF,OUTG,OUTH,OUTI,OUTJ,
2(XDIFF(J),J=1,6),OUTK,OUTL
GO TO (345,346),NZ
345 MAG = 1
KTR = 1
5412 IF(DABS(BETAP(KTR)/ABETA)-.200)5413,5425,5425
5413 CONTINUE
5417 RANDOM = RANNUM(SIGB,ZMEAN,NRS)
DO 5418 I=1,3
5418 HBETAP(I) = HG(1,I)*HBTSP(1)+HG(2,I)*HBTSP(2)+HG(3,I)*HBTSP(3)
YA = BETAP(KTR)
YP = HBETAP(KTR)

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5421 GO TO (5421,5422,5423),KTR
      HH(1) = 0.
      HH(2) = HBETAP(3)*CHX(1)-HBETAP(2)*SHX(1)
      HH(3) = HBTSP(1)*HG(2,1)-HBTSP(2)*HG(1,1)
      GO TO 5424
5422 HH(1) = -HBETAP(3)
      HH(2) = HBETAP(1)*SHX(1)
      HH(3) = HBTSP(1)*HG(2,2)-HBTSP(2)*HG(1,2)
      GO TO 5424
5423 HH(1) = HBETAP(2)
      HH(2) = -HBETAP(1)*CHX(1)
      HH(3) = HBTSP(1)*HG(2,3)-HBTSP(2)*HG(1,3)
5424 DO 5426 I=1,3
5426 ADUM(I) = HH(1)*PM(1,I)+HH(2)*PM(2,I)+HH(3)*PM(3,I)
      SCALAR = 1./((ADUM(1)*HH(1)+ADUM(2)*HH(2)+ADUM(3)*HH(3)+SIGB**2)
      DO 5427 J=1,6
5427 W(J) = (PM(J,1)*HH(1)+PM(J,2)*HH(2)+PM(J,3)*HH(3))*SCALAR
      GO TO 3371
5429 IF(TESL-TESR) 375,375,346
346 N = 1
      MAG = 2
347 SLIN = SSP(1)*EL1(N,1)+SSP(2)*EL1(N,2)+SSP(3)*EL1(N,3)
      IF(SLIN-C64) 348,349,349
348 N = N+1
      IF(N-NSI) 347,347,375
349 SLIU = SSP(1)*UA(N,1)+SSP(2)*UA(N,2)+SSP(3)*UA(N,3)
      IF(DABS(SLIU)-XIC) 350,350,348
350 ZDUM = 1.-SLIU**2
      IF(ZDUM) 351,352,352
351 WRITE(6,1008) N,LOOP,SLIU
      GO TO 999
352 ZETAS = DSORT(ZDUM)
      SLN = SSP(1)*EL (N,1)+SSP(2)*EL (N,2)+SSP(3)*EL (N,3)
      ZDUM = SLN/ZETAS
      IF(ABS(ZDUM)-1.) 353,353,354
354 WRITE(6,1009) N,LOOP,SLN ,ZETAS
      GO TO 999
353 YA =DATAN2(DSORT(1.-ZDUM**2),ZDUM)
      IF(ABS(YA-PI/2.)-OBYD) 356,356,348
356 DO 357 I = 1,3

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357 CAPN(I) = ZETAS*EL(N,I)+DCOS(YA)*SLIU*UA(N,I)
   CSUBH = -1./((ZETAS**2*DSIN(YA))
   RANDOM = RANUM(SIGS,ZMEAN,NRS)
   DO 360 J = 1,3
360   HSDP(J) = HG(1,J)*HSPRM(1)+HG(2,J)*HSPRM(2)+HG(3,J)*HSPRM(3)
   SDPU = HSDP(1)*UA(N,1)+HSDP(2)*UA(N,2)+HSDP(3)*UA(N,3)
   ZDUM = 1.-SDPU**2
   IF(ZDUM) 361,362,362
361   WRITE(6,1010) N,LOOP,SDPU
   GO TO 999
362   HZETAS = DSQRT(ZDUM)
   SDPL = HSDP(1)*EL(N,1)+HSDP(2)*EL(N,2)+HSDP(3)*EL(N,3)
   ZDUM = SDPL/HZETAS
   IF(ABS(ZDUM)-1.) 363,363,364
364   WRITE(6,1011) N,LOOP,SDPL,HZETAS
   GO TO 999
363   YP = DATAN2(DSQRT(1.-ZDUM**2),ZDUM)
   DO 365 I = 1,3
365   HCAPN(I) = HZETAS*EL(N,I)+DCOS(YP)*SDPU*UA(N,I)
   HCSUBH = -1./((HZETAS**2*DSIN(YP))
   HH(1) = HCSUBH*(HCAPN(3)*HSDP(2)-HCAPN(2)*HSDP(3))
   HH(2) = HCSUBH*((CHX(1)*HSDP(3)-SHX(1)*HSDP(2))*HCAPN(1)+
   1HSDP(1)*(SHX(1)*HCAPN(2)-CHX(1)*HCAPN(3)))
   HH(3) = HCSUBH*((HSPRM(1)*HG(2,1)-HSPRM(2)*HG(1,1))*HCAPN(1)+
   1(HSPRM(1)*HG(2,2)-HSPRM(2)*HG(1,2))*HCAPN(2)+(HSPRM(1)*
   2HG(2,3)-HSPRM(2)*HG(1,3))*HCAPN(3))
   DO 367 I = 1,3
367   ADUM(I) = HH(1)*PM(1,I)+HH(2)*PM(2,I)+HH(3)*PM(3,I)
   SCALAR = 1./((ADUM(1)*HH(1)+ADUM(2)*HH(2)+ADUM(3)*HH(3)+SIGS**2)
   DO 369 J = 1,6
369   W(J) = (PM(J,1)*HH(1)+PM(J,2)*HH(2)+PM(J,3)*HH(3))*SCALAR
3371 DO 371 I = 1,6
   DO 371 J = 1,6
371   WDUM(I,J) = W(I)*HH(J)
   DO 373 K = 1,6
   DO 373 L = 1,6
377   IF(K-L) 374,377,374
   HDUM(K,L) = 1.-WDUM(K,L)
   GO TO 373
374   HDUM(K,L) = -WDUM(K,L)

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373 CONTINUE
DO 379 I = 1,6
DO 379 J = 1,6
379 PP(I,J) = HDUM(I,1)*PM(I,J)+HDUM(I,2)*PM(2,J)+HDUM(I,3)*
1PM(3,J)+HDUM(I,4)*PM(4,J)+HDUM(I,5)*PM(5,J)+HDUM(I,6)*PM(6,J)
WRITE (6,1073) ((PM(I,J),J=1,6),I=1,6)
1073 FORMAT(1H0,6F18.8)
DO 381 K = 1,6
381 PDIAG(K) = DSQRT(PP(K,K))
PSUM1 = DSQRT(PP(1,1)+PP(2,2)+PP(3,3))
PSUM2 = DSQRT(PP(4,4)+PP(5,5)+PP(6,6))
DO 383 J = 1,6
383 HX(J) = RHOX(J)+W(J)*(YA-YP+RANDOM)
APX(J) = HX(J)-X(J)
APXM1 = DSQRT(APX(1)**2+APX(2)**2+APX(3)**2)
APXM2 = DSQRT(APX(4)**2+APX(5)**2+APX(6)**2)
GO TO(3383,3384),MAG
3383 N = KTR
3384 CONTINUE
WRITE (6,1015) N,YA,(HIA(K),K=1,3),RANDOM,YP,(HH(I),I=1,3),
1(PDIAG(K),K=1,6),PSUM1,PSUM2,(APX(J),J=1,6),APXM1,APXM2,
2(W(L),L=1,6)
DO 385 K = 1,6
385 RHOX(K) = HX(K)
DO 386 I = 1,3
386 SHX(I) = DSIN(HX(I))
CHX(I) = DCOS(HX(I))
CALL CEE (HX(1),HX(2),HX(3),HG)
DO 389 I = 1,6
DO 389 J = 1,6
389 PM(I,J) = PP(I,J)
GO TO (5425,348),MAG
5425 IF(KTR-3) 5428,5429,5429
5428 KTR = KTR+1
GO TO 5412
375 THETA = THETA
DO 387 I = 1,3
DO 387 J = 1,3
387 C(I,J) = GAM(I,I)*G(1,J)+GAM(2,I)*G(2,J)+GAM(3,I)*G(3,J)
X(I) = 0.0

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X(2) = 0.0
X(3) = 0.0
DO 392 I = 1,3
DO 392 J = 1,3
392 HC(I,J) = HGAM(1,I)*HG(1,J)+HGAM(2,I)*HG(2,J)+HGAM(3,I)*HG(3,J)
DO 393 K = 1,3
DO 393 L = 1,3
393 BDUM(K,L) = HB(K,1)*HG(1,L)+HB(K,2)*HG(2,L)+HB(K,3)*HG(3,L)
DO 394 I = 1,3
DO 394 J = 1,3
394 HB(I,J) = BDUM(I,J)
HX(1) = 0.0
HX(2) = 0.0
HX(3) = 0.0
DO 409 I = 1,6
DO 409 J = 1,6
410 IF(I-J) 410,411,410
PH(I,J) = 0.0
GO TO 409
411 PH(I,J) = 1.0
409 CONTINUE
CALL EXTRA (B,HB,G,HG,SPRM,HSPRM,HSDP)
4093 CONTINUE
TP = TP+TAU
IF(TP-T1 55,55,999
      BOX D
C 400 CALL PDUMP
      GO TO 999
1000 FORMAT(7F10.0)
1001 FORMAT(7I10)
1002 FORMAT(1H,14H*** INPUTS ***/
      16HOORBIT,6H OIZ=F16.8,6H OIZ=F16.8,6H OATP=F16.8/
      21H ,5X ,6H OEZ=F16.8,6H OIPZ=F16.8/
      38HOVEHICLE,4H I1=F16.8,6H I2=F16.8,6H
      41H ,5X ,6H VLQ=F16.8,6H VPQ=F16.8,6H VAV=F16.8/
      512HOBSERVATION,4H NS=I4,6H OBZD=F16.8,6H OBYD=F16.8,4H M=I7/
      66HOSTAT,6H SIGZ=F16.8,6H SIGW=F16.8,6H SIGS=F16.8,6H SIGB=F16.8/
      76H0INIT,6H Z1=F16.8,6H Z2=F16.8,6H Z3=F16.8,6H P80=F16.8/
      81H ,5X ,6H WD1=F16.8,6H WD2=F16.8,6H WD3=F16.8,6H TSO=F16.8/
      98HOCNTROL,4H NZ=I5,4H NT=I5,6H CTP=F16.8,6H NRS=I5)

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1003 FORMAT(1H0,6HCROSI ,3F16.8/1H0,6H POLI , 3F16.8/1H0,5H VERI,3F16.8/
1 1H0,6H SUNI ,3F16.8/1H0,6H MAGI , 3F16.8/1H0,5HCROSV,3F16.8/
2 1H0,6H POLV ,3F16.8/1H0,6H VERV , 3F16.8/1H0,5H SUNV,3F16.8/
3 1H0,6H MAGV ,3F16.8/1H0,6H XA ,6F16.8/1H0,5H XO ,6F16.8)
1005 FORMAT(1H0,5HTEST=F16.8,8HWHEN SR=F16.8)
1008 FORMAT(1H0,2HN=I3,7H LOOP=,I5,7H SLIU=F16.8)
1009 FORMAT(1H0,2HN=I3,7H LOOP=,I5,7H SLIN=F16.8,7H ZETAS=F16.8)
1011 FORMAT(1H0,2HN=I3,7H LOOP=,I5,7H SDPL=F16.8,7H HZS=F16.8)
1010 FORMAT(1H0,2HN=I3,7H LOOP=,I5,7H SDPU=F16.8)
1006 FORMAT(1H1,5HTIME=F16.8,2X,2HM=I5,2X,3HGX=F16.8,2X,3HGY=F16.8,
12X,3HGZ=F16.8/6H0 VERI,2X,3(F16.8,2X)/6HOCROSV,2X,3(F16.8,2X),
27X,3HC11,6X,F16.8,7X,3HC13/6H0 POLV,2X,3(F16.8,2X),7X,3HC21,13X,
33HC22,F16.8/6H0 VERV,2X,3(F16.8,2X),F16.8,7X,3HC32,13X,3HC33/
46H0 SUNV,2X,3(F16.8,2X)/6H0 MAGV,2X,3(F16.8,2X)/1H0,30X,17HTRANSIT
5ION MATR1X/1H0,6(F16.8,/1H ))
1019 FORMAT(40H0INPUT MOMENTS OF INERTIA NOT REALIZABLE/1H0,3F18.8)
1023 FORMAT(1H0,23X,8HB-MATR1X,43X,14HB-MATR1X CHECK/1H0,3(6F18.8/1H )/
15H0 XA ,2X,6F16.8/1H0,10X,F16.8,30X,F16.8/5H0 XR ,2X,6F18.8/1H0,
210X,F16.8,30X,F16.8/6H0 XP ,2X,6F18.8/1H0,10X,F16.8,30X,F16.8)
1015 FORMAT (1H0,10HINST. NO.=I3,9X,3HYA=F16.8,2X,4HH1A=F16.8,2X,4HH2A=
1,F16.8,2X,4HH3A=F16.8/1H0,3HNR=F14.8,2X,3HYP=F16.8,2X,4HH1 =F16.8,
22X,4HH2 =F16.8,2X,4HH3 =F16.8/1H0,2HXR,2X,6(F16.8,2X)/1H0,10X,
3F16.8,30X,F16.8/1H0,2HXO,2X,6(F16.8,2X)/1H0,10X,F16.8,30X,F16.8/
41H0,1HW,3X,6(F16.8,2X))
STOP
END

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```

$IBFTC DICE DECK
CDICE DOUBLE PRECISION ICE
SUBROUTINE DICE(P,TT,TP,E1,E2,NN,Y,DY,F,LL,INDEX,I)
DIMENSION Y(50),DY(50),F(350)

C
DOUBLE PRECISION Y , DY , F , TT
DOUBLE PRECISION TS , H , DT , E1
DOUBLE PRECISION E2 , H1 , P , T2 , TP
DOUBLE PRECISION H2
L = LL
T = TT
GO TO (100,200,300,400),L
100 IG=IG
GO TO (101,102),IG
101 J = 1
L = 2
M = 0
TS = T
DO 106 K = 1,N
K1 = K+3*N
K2 = K1+N
K3 = N + K
F(K1) = Y(K)
F(K3) = F(K1)
F(K2) = DY(K)
GO TO 402
106
102 CALL DINTG(T,DT,N,Y,DY,F,J,I)
J = J+1
IF(J-I ) 103,103,104
103 L = 1
GO TO 402
104 M = M+1
105 GO TO (110,120,130),M
110 DO 111 K = 1,N
K1 = K+N+N
F(K1) = Y(K)
111 DO 113 K = 1,N
K1 = K+3*N
K2 = K1+N
K3 = N + K

```

DICE0000
 DICE0010
 DICE0020
 DICE0040
 DICE0050
 DICE0060
 DICE0070
 DICE0080
 DICE0100
 DICE0110
 DICE0120
 DICE0130
 DICE0140
 DICE0150
 DICE0160
 DICE0170
 DICE0180
 DICE0190
 DICE0200
 DICE0210
 DICE0220
 DICE0230
 DICE0240
 DICE0250
 DICE0260

 DICE0290
 DICE0300
 DICE0310
 DICE0320
 DICE0330
 DICE0340
 DICE0350
 DICE0360
 DICE0370
 DICE0380
 DICE0390
 DICE0400
 DICE0410

DICE0420
DICE0430
DICE0440
DICE0450
DICE0460
DICE0470
DICE0480
DICE0490
DICE0500
DICE0510
DICE0520
DICE0530
DICE0540
DICE0550
DICE0560
DICE0570
DICE0580
DICE0590
DICE0600
DICE0610
DICE0620
DICE0630
DICE0640
DICE0650
DICE0660
DICE0670
DICE0680
DICE0690
DICE0700
DICE0710
DICE0720
DICE0730
DICE0740
DICE0750
DICE0760
DICE0770
DICE0780
DICE0790
DICE0800
DICE0810

```

Y(K) = F(K1)
F(K3) = F(K1)
113 DY(K) = F(K2)
T = TS
114 IF(PART(I,T,1)) 114,116,114
115 IF(DABS(H/T)-.00001D0) 115,115,116
M = 0
L = 4
GO TO 402
116 DT = .5D0*H
M = 1
J = 1
GO TO 300
120 DO 121 K = 1,N
K1 = K+N
121 F(K1) = Y(K)
M = 2
J = 1
IG = 2
L = 1
GO TO 402
130 DO 131 K = 1,N
K1 = K+2*N
F(K) = (Y(K)-F(K1))/(2.D0**I-1.D0)
Y(K) = Y(K) +F(K)
IF(DABS(Y(K))-0.0001D0)139,139,140
139 F(K) = 0.D0
GO TO 131
140 F(K) = DABS(F(K)/Y(K))
131 CONTINUE
E = F
INDEX = 1
IF (N-1)1335,1335,1315
1315 DO 133 K = 2,N
IF(E-F(K)) 132,133,133
132 INDEX = K
E = F(K)
133 CONTINUE
1335 IF(E -E1) 134,135,135
134 H = H+H

```

DICE0820
DICE0830
DICE0840
DICE0850
DICE0860
DICE0870
DICE0880
DICE0890
DICE0900
DICE0910
DICE0920
DICE0930
DICE0940
DICE0950
DICE0960
DICE0970
DICE0980
DICE0990
DICE1000
DICE1010
DICE1020
DICE1030
DICE1040
DICE1050
DICE1060
DICE1070
DICE1080
DICE1090
DICE1100
DICE1110
DICE1120
DICE1130
DICE1140
DICE1150
DICE1160
DICE1170
DICE1180
DICE1190
DICE1200
DICE1210

DICE1220
DICE1230
DICE1240
DICE1250
DICE1260
DICE1270
DICE1280
DICE1290
DICE1300

H = P
DT = H
N = NN
401 IG = 1
L = 1
402 TT = T
LL = L
RETURN
END

```

$18FTC DING DECK
CDING DICE INTEGRATION SUBROUTINE
C I = 2 SECOND ORDER RUNGE-KUTTA DING0000
C I = 3 THIRD ORDER RUNGE-KUTTA DING0010
C I = 4 FOURTH ORDER RUNGE-KUTTA DING0020
C STORAGE F1 = E = Z1 DING0030
C F2 = YHAF1 TEMPORARY STORAGE REQUIRED= DING0040
C F3 = YFULL DIMENSION OF F ARRAY = DING0050
C F4 = YSAVE N*(3+I) DING0060
C F5 = DYSAVE WHERE N = NO OF DERIVATIVES DING0070
C F6 = Z2 AND I = ORDER OF INTEGRATION DING0080
C F7 = Z3 PROCESS DING0090
C SUBROUTINE DINTG (I,TD,N,Y,DY,F,J,II) DING0100
C DIMENSION Y(50),DY(50),F(350) DING0110
C THE FOLLOWING STATEMENT(S) HAVE BEEN MANUFACTURED BY THE TRANSLATOR----DING0120
C DING0130
C DING0140
C DOUBLE PRECISION Y , DY , F , DT , TD DING0150
C DOUBLE PRECISION T DING0160
C DIMENSION Y(50),DY(50),F(350) DING0170
C I = II DING0180
C DT = TD DING0190
C DO 100 K = 1,N DING0200
C K1 = K DING0210
C K2 = K+5*N DING0220
C K3 = K2+N DING0230
C K4 = K + N DING0240
C GO TO (99,85,95,95),I DING0250
C GO TO (86,2,999,999),J DING0260
C F(K1) = DY(K)*DT DING0270
C Y(K) = F(K4) + F(K1) DING0280
C GO TO 100 DING0290
C GO TO (1,2,3,4),J DING0300
C F(K1) = DY(K)*DT DING0310
C Y(K) = F(K4)+.5D0*F(K1) DING0320
C GO TO 100 DING0330
C F(K2) = DY(K)*DT DING0340
C GO TO (99,22,23,24),I DING0350
C F(K3) = DY(K)*DT DING0360
C GO TO (99,33,33,34),I DING0370
C Y(K) = F(K4)+(F(K1)+2.0D0*(F(K2)+F(K3))+DY(K)*DT)/6.0 DING0380

```

```

22      GO TO 100
      Y(K) = .500*(F(K1)+F(K2))
23      GO TO 25
      Y(K) = 2.00*F(K2)-F(K1)
24      GO TO 25
      Y(K) = .500*F(K2)
25      Y(K) = Y(K)+F(K4)
      GO TO 100
33      Y(K) = F(K4)+(F(K1)+4.00*F(K2)+F(K3))/6.00
      GO TO 100
34      Y(K) = F(K4)+F(K3)
100     CONTINUE
      GO TO (110,120,130,140),J
110     GO TO (999,131,132,132),I
120     GO TO (999,140,132,140),I
130     GO TO (999,140,140,132),I
131     T = DT + T
      GO TO 140
132     T = T + .500*DT
140     RETURN
999     PAUSE
      GO TO 140
      END

```

```

DING0390
DING0400
DING0410
DING0420
DING0430
DING0440
DING0450
DING0460
DING0470
DING0480
DING0490
DING0500
DING0510
DING0520
DING0530
DING0540
DING0550
DING0560
DING0570
DING0580
DING0590
DING0600
DING0610

```

\$IBMAP	RANN	DECK
RANNUM	ENTRY	RANNUM
	SXD	CHRIS,4
	CLA	3,4
	STA	A
	CLA	4,4
	STA	B
	CLA	5,4
	STO	C
	TSX	UDRNRT,4
	TXI	4+3,0
	PZE	26,0,0
C	HTR	O
	STO	D
	LRS	35
	FMP	E
	FAD	F
	SSH	
	FAD	F
S	LRS	35
	FMP	G
	STO	ARG
	TSX	ALOG,4
	TXI	4+3,0
	PZE	27,0,0
	HTR	ARG
	LRS	35
	FMP	E
	STO	H
	TSX	SORT,4
	TXI	4+3,0
	PZE	28,0,0
	HTR	H
	STO	P
	LRS	35
	FMP	H
	STO	Q
	CLA	F
	STO	R
	LXA	S,4

SIGMA

X MEAN

COMPUTE UI

COMPUTE NI

SRNRT0018

SRNRT0020

SRNRT0022

SRNRT0023

SRNRT0025

SRNRT0026

SRNRT0027

SRNRT0028

SRNRT0029

SRNRT0030

SRNRT0031

SRNRT0032

SRNRT0034

SRNRT0035

SRNRT0036

SRNRT0037

SRNRT0038

SRNRT0039

SRNRT0040

SRNRT0041

SRNRT0042

SRNRT0043

SRNRT0044

SRNRT0045
 SRNRT0046
 SRNRT0047
 SRNRT0048
 SRNRT0049
 SRNRT0050
 SRNRT0051
 SRNRT0052
 SRNRT0053
 SRNRT0054
 SRNRT0055
 SRNRT0056
 SRNRT0057
 SRNRT0058
 SRNRT0059
 SRNRT0060
 SRNRT0061
 SRNRT0062
 SRNRT0063
 SRNRT0064
 SRNRT0065
 SRNRT0066
 SRNRT0067
 SRNRT0068
 SRNRT0069
 SRNRT0070

SRNRT0075
 SRNRT0076
 SRNRT0077
 SRNRT0078
 SRNRT0079
 SRNRT0080
 SRNRT0081
 SRNRT0082

V	LDQ T,4	
	FMP R,4	
	FAD R	
	STO R	
	TIX V,4,1	
	CLA T	
	STO W	
	LXA X,4	
Y	LDQ D,4	
	FMP Q,4	
	FAD W	
	STO W	
	TIX Y,4,1	
	FDP R	
	STQ R	
	CLA R	
X	CHS	
	FAD P	
	STO W	
	CLA D	
	FSB G	
	TPL Z	
	CLS W	
	TRA AA	
	CLA W	
Z	LRS 35	
AA	FMP O	
A	FAD O	
B	LXD CHRIS,4	
	TRA 1,4	
CHRIS	PZE	
ARG	PZE	
E	DEC -2.	
F	DEC 1.	
G	DEC .5	
	DEC 1.432788	
	DEC .189269	
	DEC .001308	
T	DEC 2.515517	
	DEC .802853	

SRNR T0083

SRNR T0090

DEC -010328

HYR 0
HTR 0
HTR 0
HTR 0
HTR 0
HTR 0
END

D P H Q R W

\$IBMAP	UDRN	ENTRY	UDRNRT	DECK
UDRNRT	SXD	CHRIS,4		
	CLA	3,4		
	STA	A		
	STA	B		
	STA	C		
	STA	D		
	STA	E		
	STA	K		
	CLA	0		
A	ANA	MASK		
	TNZ	C		
K	CLA	0		
	ARS	18		
B	STO	0		
C	LDQ	0		
	MPY	F		
D	STQ	0		
E	CLA	0		
	ARS	8		
	ADD	G		
	FAD	H		
	LXD	CHRIS,4		
	TRA	1,4		
CHRIS	PZE			
MASK	HTR	-1		
F	OCT	011060471625		
G	OCT	200000000000		
H	OCT	0		
	END			

UDRN0015
UDRN0016
UDRN0017
UDRN0018
UDRN0019
UDRN0020

UDRN0022
UDRN0023

UDRN0025

UDRN0028

UDRN0031
UDRN0032
UDRN0033

UDRN0036
UDRN0037
UDRN0038
UDRN0039
UDRN0040

```

$IBFTC ECCAN
C      SUBROUTINE ECCAN
      DOUBLE PRECISION FUNCTION ECCAN(XM,E)
      DOUBLE PRECISION EPSIL,XM,E,DELE
      EPSIL = .5*10.**{-13}
      ECCAN = XM+E*DSIN(XM)*(1.+E*DCOS(XM))
2     DELE = (XM-ECCAN+E*DSIN(ECCAN))/(1.-E*DCOS(ECCAN))
      ECCAN = ECCAN+DELE
      IF(DABS(DELE/ECCAN)-EPSIL) 1,1,2
1     RETURN
      END

```

```

$IBFIC CEE
SUBROUTINE CEE (Z1,Z2,Z3,C)
DOUBLE PRECISION Z1,Z2,Z3,C,CZ1,CZ2,CZ3,SZ1,SZ2,SZ3
DIMENSION C(3,3)
SZ1 = DSIN(Z1)
CZ1 = DCOS(Z1)
SZ2 = DSIN(Z2)
CZ2 = DCOS(Z2)
SZ3 = DSIN(Z3)
CZ3 = DCOS(Z3)
C(1,1) = CZ3*CZ2
C(1,2) = SZ3*CZ1+CZ3*SZ2*SZ1
C(1,3) = SZ3*SZ1-CZ3*SZ2*CZ1
C(2,1) = -SZ3*CZ2
C(2,2) = CZ3*CZ1-SZ3*SZ2*SZ1
C(2,3) = CZ3*SZ1+SZ3*SZ2*CZ1
C(3,1) = SZ2
C(3,2) = -CZ2*SZ1
C(3,3) = CZ2*CZ1
RETURN
END

```

```

$IBFIC EXTRA
SUBROUTINE EXTRA (B,HB,G,HG,SPRM,HSPRM,HSDP)
DOUBLE PRECISION B,HB,G,HG,SPRM,HSPRM,HSDP,RR,ESUM
DIMENSION B(3,3),HB(3,3),G(3,3),HG(3,3),SPRM(3),HSPRM(3),HSDP(3),
1RR(3,3)
DO 827 I = 1,3
DO 827 J = 1,3
827 RR(I,J) = B(1,I)*HB(1,J)+B(2,I)*HB(2,J)+B(3,I)*HB(3,J)
ESUM = DSQRT(RR(1,2)**2+RR(2,3)**2+RR(3,1)**2)
WRITE (6,1062) ((HB(I,J),J=1,3),( RR (I,K),K=1,3),I=1,3),ESUM
1062 FORMAT (1H0,22X,9HBB-MATRIX,45X,12HERROR MATRIX/1H0,3(6F18.8/1H )/
11H0,72X,F18.8)
1063 FORMAT (1H0,3F18.8)
RETURN
END

```

\$IBFTC CHECK1

```

SUBROUTINE CHECK1
COMMON/OMEGA/ HWO1,HWO2,HWO3,RT1,RT2,ZB11,ZB13,ZB21,ZB23
COMMON/GIVE/NT,NZ,OAPZ,VAV,VQ,OEZ,ZE1,ZE2,ZE3,D,VI,
1ETAZ,T,SSP,B,C,PSUBP,Z1,Z2,Z3,W01,W02,W03
COMMON/GET/NSUBB,NSUBC,NSUBM,NVAR,EM,PSI11,PSI13,PSI21,PSI23
1,WSAP,WSBP,ASKH,ASUBK,WSUBP,ASCP,ASSP,CAHV,SAHV
DIMENSION D(3,3),VI(3),SSP(3),B(3,3),EM(3,3),C(3,3),V(3),
1VDP(3),QQ(3,3),RR(3,3)
DOUBLE PRECISION TERM2,HWO1,HWO2,HWO3,VXH,COSAKV,PI
DOUBLE PRECISION V,VDP,QQ,RR,EM,ZE1,ZE2,ZE3,
1D,VI,ETAZ,T,SSP,B,C,PSUBP,Z1,Z2,Z3
DOUBLE PRECISION WSAP,WSBP,ASCP,ASSP,TERM1,CAHV,WSUBP,ASKH,
1ASKV,ASUBK,ASHV,SAHV,SAK,CAK,SAKH,CAKH,AHV,RT1,RT2,R11,R21,R31,
2R41,R13,R23,R33,R43,ZB11,ZB13,ZB21,ZB23,PSI11,PSI13,PSI21,PSI23
PI = 3.141592653589793
IF(NT)601,601,602
602 NSUBM=2
NSUBB = 2
NVAR=48
GO TO 650
601 IF(DABS(ZE1)-.0000001) 603,603,602
603 NSUBM=1
NVAR=12
WSAP=-ZE2*W01
WSBP=DSQRT((ZE2+1.)*2*W01**2+W02**2+W03**2)
WSBP = -WSBP
ASCP=-(ZE2+1.)*W01/WSBP
ASSP=DSQRT(1.-ASCP**2)
IF(VAV)604,604,605
605 GO TO(606,607),NZ
606 IF(OAPZ-40000.)608,608,607
608 NSUBB=2
GO TO 650
604 NSUBB=1
DO 610 I=1,3
V(I)=D(I,2)
VDP(I)=C(2,I)
610 TERM1=VI(2)*((W02*VDP(2)+W03*VDP(3))
CAHV=ASCP*((VI(1)*W01*VDP(1)+TERM1)/(VI(1)*W01)

```

```

TERM1=ASCP*(1.-1.5*ASSP**2)*ZE2
WSUBP = 0.0
GO TO 615
607 IF(I-1-E 06)616,616,617
617 NSUBB=2
GO TO 650
616 NSUBB=1
DO 618 I=1,3
VDP(I)=SSP(I)
618 V(I)=8(I,1)*SSP(1)+8(I,2)*SSP(2)+8(I,3)*SSP(3)
WSUBP = 0.0
615 ASKH=DATAN2(W02,W03)
TERM1 = VDP(3)*VI(1)*W01-VDP(1)*VI(3)*W03
VXH = DSQRT((VDP(2)*VI(3)*W03-VDP(3)*VI(2)*W02)**2+TERM1**2
I+(VDP(1)*VI(2)*W02-VDP(2)*VI(1)*W01)**2)
COSAKV = TERM1/VXH
TERM2 = (VDP(2)*VI(1)**2*W01**2)/ASCP**2-VI(2)*W02*
1(WDP(1)*VI(1)*W01+VDP(2)*VI(2)*W02+VDP(3)*VI(3)*W03)
IF (COSAKV) 620,6204,620
620 ASKV = (TERM2/DABS(TERM2))*DATAN2(DSQRT(1.-COSAKV**2),COSAKV)
GO TO 6203
6204 ASKV = (PI*TERM2)/(2.*DABS(TERM2))
6203 ASUBK = ASKV-ASKH
TERM1=VI(2)*(W02*VDP(2)+W03*VDP(3))
TERM2=ASCP*(VI(1)*W01*VDP(1)+TERM1)/(VI(1)*W01)
IF(DABS(TERM2)-1.) 6231,6231,624
624 WRITE(6,1022)TERM2,(VDP(1),I=1,3),W01,W02,W03,VI(1),VI(2),ASCP
GO TO 999
6231 IF(1TERM2) 623,6232,623
623 AHV = DATAN2(DSQRT(1.-TERM2**2),TERM2)
GO TO 6233
6232 AHV = PI/2.
6233 CAHV = DCOS(AHV)
SAHV=DSIN(AHV)
SAK=DSIN(ASUBK)
CAK=DCOS(ASUBK)
SAKH=DSIN(ASKH)
CAKH=DCOS(ASKH)
QQ(1,1)=CAHV
QQ(1,2)=0.0

```

```

QQ(1,3)=-SAHV
QQ(2,1)=SAK*SAHV
QQ(2,2)=CAK
QQ(2,3)=SAK*CAHV
QQ(3,1)=CAK*SAHV
QQ(3,2)=-SAK
QQ(3,3)=CAK*CAHV
RR(1,1)=ASCP*QQ(1,1)-ASSP*QQ(3,1)
RR(1,2)=ASCP*QQ(1,2)-ASSP*QQ(3,2)
RR(1,3)=ASCP*QQ(1,3)-ASSP*QQ(3,3)
RR(2,1)=QQ(2,1)
RR(2,2)=QQ(2,2)
RR(2,3)=QQ(2,3)
RR(3,1)=ASSP*QQ(1,1)+ASCP*QQ(3,1)
RR(3,2)=ASSP*QQ(1,2)+ASCP*QQ(3,2)
RR(3,3)=ASSP*QQ(1,3)+ASCP*QQ(3,3)
QQ(1,1)=RR(1,1)
QQ(1,2)=RR(1,2)
QQ(1,3)=RR(1,3)
QQ(2,1)=CAKH*RR(2,1)+SAKH*RR(3,1)
QQ(2,2)=CAKH*RR(2,2)+SAKH*RR(3,2)
QQ(2,3)=CAKH*RR(2,3)+SAKH*RR(3,3)
QQ(3,1)=-SAKH*RR(2,1)+CAKH*RR(3,1)
QQ(3,2)=-SAKH*RR(2,2)+CAKH*RR(3,2)
QQ(3,3)=-SAKH*RR(2,3)+CAKH*RR(3,3)
DO 627 I=1,3
DO 627 J=1,3
627 EM(I,J)=B(I,1)*QQ(1,J)+B(I,2)*QQ(2,J)+B(I,3)*QQ(3,J)
C-MATRIX CHECK
650 GO TO(651,652),NZ
652 IMHY=1
670 WRITE(6,1032)IMHY
NSUBC=2
GO TO 699
999 CALL EXIT
651 IF(VAV)653,653,672
653 IF(OEZ)654,654,673
654 IF(Z1+Z2+Z2+Z3-Z3-.01)655,655,674
655 TERM1=DABS(WO2-ETAZ)
TERM2=DSQRT(3.*ZE2)*.1*ETAZ

```

```

656 IF (TERM1-TERM2) 656, 656, 675
657 IF (VI(1)-VI(3)) 676, 676, 657
658 IF (ZE1*ZE3) 658, 677, 677
659 TERM1 = 1.-3.*ZE1-ZE1*ZE3
660 IF (TERM1) 678, 678, 659
661 TERM2=TERM1**2+16.*ZE1*ZE3
662 IF (TERM2) 679, 679, 680
663 IWHY=2
664 GO TO 670
665 IWHY=3
666 GO TO 670
667 IWHY=4
668 GO TO 670
669 IWHY=5
670 GO TO 670
671 IWHY=6
672 GO TO 670
673 IWHY=7
674 GO TO 670
675 IWHY=8
676 GO TO 670
677 IWHY=9
678 GO TO 670
679 GO TO 670
680 RT1 = ETAZ*DSQRT((TERM1+DSQRT(TERM2))/2.)
    RT2 = ETAZ*DSQRT((TERM1-DSQRT(TERM2))/2.)
    TERM1=RT1**2-RT2**2
    R11=(RT1**2-ETAZ**2*(1.+ZE1-ZE1*ZE3))/TERM1
    R21=(RT2**2-ETAZ**2*(1.+ZE1-ZE1*ZE3))/TERM1
    R31 = ((1.+ZE1)*ZE3*ETAZ**3)/(RT1*TERM1)
    R41 = ((1.+ZE1)*ZE3*ETAZ**3)/(RT2*TERM1)
    R13=(RT1**2-ETAZ**2*(1.-ZE3-3.*ZE1-ZE1*ZE3))/TERM1
    R23=(RT2**2-ETAZ**2*(1.-ZE3-3.*ZE1-ZE1*ZE3))/TERM1
    R33=(4.*(1.-ZE3)*ZE1*ETAZ**3)/(RT1*TERM1)
    R43=(4.*(1.-ZE3)*ZE1*ETAZ**3)/(RT2*TERM1)
    ZB11=DSQRT((R11*Z1)**2+(R31*Z3)**2)
    ZB13=DSQRT((R33*Z1)**2+(R13*Z3)**2)
    ZB21=DSQRT((R21*Z1)**2+(R41*Z3)**2)
    ZB23=DSQRT((R43*Z1)**2+(R23*Z3)**2)
    IF (ZB11-.1) 681, 681, 682
    IF (ZB13-.1) 683, 683, 682
681

```

```

683 IF(ZB21-.1)684,684,682
684 IF(ZB23-.1)685,685,682
682 IWHY=10
GO TO 670
685 TERM1=DABS(WO1+ETAZ*Z3)
TERM2=.01*(RT1*ZB11+RT2*ZB21)
IF(TERM1-TERM2)686,686,687
687 IWHY=11
GO TO 670
686 TERM1=DABS(WO3-ETAZ*Z1)
TERM2=.01*(RT1*ZB13+RT2*ZB23)
IF(TERM1-TERM2)688,688,689
689 IWHY=12
GO TO 670
688 NSUBC=1
TERM1= R31*Z3
TERM2=R11*Z1
PSI11=DATAN2(TERM1,TERM2)
TERM1= R33*Z1
TERM2=R13*Z3
PSI13=DATAN2(TERM1,TERM2)
TERM1= R41*Z3
TERM2=R21*Z1
PSI21=DATAN2(TERM1,TERM2)
TERM1= R43*Z1
TERM2=R23*Z3
PSI23=DATAN2(TERM1,TERM2)
699 CONTINUE
1021 FORMAT(1H0,18HTROUBLE IN 8-CHECK/1H0,7F16.8)
1022 FORMAT(1H0,17HTROUBLE IN ARCCOS/1H0,9F13.8)
1032 FORMAT(1H0,30HC-MATRIX CHECK OMITTED DUE TO ,I3)
RETURN
END

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\$1BFTC HELP

SUBROUTINE HELP

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COMMON/OMEGA/ HWO1,HWO2,HWO3,RT1,RT2,ZB11,ZB13,ZB21,ZB23
COMMON/GIVE/NT,NZ,OAPZ,YAV,VQ,OEZ,ZE1,ZE2,ZE3,D,VI,
1ETAZ,T,SSP,B,C,PSUBP,Z1,Z2,Z3,M01,M02,M03
COMMON/GET/NSUBB,NSUBC,NSUBM,NVAR,EM,PSI11,PSI13,PSI21,PSI23
1,WSAP,WSBP,ASKH,ASUBK,WSUBP,ASCP,ASSP,CAHV,SAHV
COMMON/XCIN/X,TAU,CHX,SHX,HG,GAM,STHE,CTHE,THETA,COMC,SOMC,
1CIC,SIC,G,SPRM,PM,PP,PMDUM,TM,CWS,PBO,QKB,QLBC,QKBP,R,SR,QKBDR,
2BETA,CSUBB,SRUB,BETAP,OMZ
DIMENSION X(48)
DIMENSION C(3,3),D(3,3),B(3,3),SSP(3),VI(3),EM(3,3),HX(6)
DIMENSION DELL(3),DELK(3),DELA(3),DELB(3),DELG1(3),DELG2(3),
1DELG3(3),DELF1(3),DELF2(3),DELX1(3),DELX2(3),DELX3(3),CHX(3),
2SHX(3),HG(3,3),PH(6,6),GAM(3,3),G(3,3),BDUM(3,3),SPRM(3),PM(6,6),
3PP(6,6),PMDUM(6,6),QKB(3),QKBP(3),R(3),BETA(3),BETAP(3)
DOUBLE PRECISION WSAP,WSBP,ASKH,ASUBK,WSUBP,ASCP,ASSP,CAHV,SAHV,
1HWO1,HWO2,HWO3,RT1,RT2,ZB11,ZB13,ZB21,ZB23
DOUBLE PRECISION X
DOUBLE PRECISION ZE1,ZE2,ZE3,TAU,HX, D,VI,ETAZ,T,SSP,B,C,
1PSUBP,Z1,Z2,Z3,EM,PSI11,PSI13,PSI21,PSI23
DOUBLE PRECISION OSA,OSB,ZSQ,ALSC,ALSS,OYZ,QSC,QSS,TTT,ABC,ABSI,
1BBC,BBS,F1,F2,CTHE,STHE,THETA,YOUC,YOUF,COMC,SOMC,CIC,SIG,
2TM,CWS,PBO,PSIB,QLBC,SR,QKBDR,CSUBB,SRUB
DOUBLE PRECISION DELL,DELK,DELA,DELB,DELG1,DELG2,DELG3,DELF1,
1DELF2,DELX1,DELX2,DELX3,CHX,SHX,HG,PH,GAM,G,BDUM,SPRM,PM,PP,
2PMDUM,QKB,QKBP,R,BETA,BETAP
EQUIVALENCE (X(7),HX(1)),(PH(1),X(13))
GO TO (821,822),NSUBM
821 ZSQ=ZE2
OSA=-ZSQ*HWO1
OSB=DSQRT((ZSQ+1.))*2*HWO1*2+HWO2*2+HWO3*2)
OSB = -OSB
ALSC=-(ZSQ+1.)*HWO1/OSB
ALSS=DSQRT(1.-ALSC*2)
OYZ=DSQRT(HWO2*2+HWO3*2)
QSC=HWO3/OYZ
QSS=HWO2/OYZ
TTT = TAU
ABC=DCOS(OSA*TTT)

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      ABSI=DSIN(OSA*TTT)
      BBC=DCOS(OSB*TTT)
      BBS=DSIN(OSB*TTT)
      DELL(1) = -(OYZ*ALSC**2)/((ZSQ+1.)*HW01**2)
      DELL(2) = ( HW02*ALSC**2)/((ZSQ+1.)*HW01*OYZ)
      DELL(3) = ( HW03*ALSC**2)/((ZSQ+1.)*HW01*OYZ)
      DELK(1)=0.0
      DELK(2)=HW03/OYZ**2
      DELK(3)=-HW02/OYZ**2
      DELA(1)=-ZSQ*TTT
      DELA(2)=DELK(2)
      DELA(3)=DELK(3)
      DELB(1) = ((ZSQ+1.)***2*HW01*TTT)/OSB
      DELB(2)=HW02*TTT/OSB
      DELB(3)=HW03*TTT/OSB
      DO 824 J=1,3
      DELG1(J)=-2.*ALSC*ALSS*DELL(J)*(1.-BBC)-ALSS**2*BBS*DELB(J)
      DELG2(J)=ALSS*ALSC*QSS*BBS*DELB(J)+(1.-BBC)*(ALSC**2*DELL(J)*QSS-
      1ALSS**2*DELL(J)*QSS+ALSS*ALSC*QSC*DELK(J))-(ALSC*DELL(J)*QSC*
      2BBS-ALSS*QSS*DELK(J)*BBS+ALSS*QSC*BBC*DELB(J))
      DELG3(J)=ALSS*ALSC*QSC*BBS*DELB(J)+(1.-BBC)*(ALSC**2*DELL(J)*QSC-
      1ALSS**2*DELL(J)*QSC-ALSS*ALSC*QSS*DELK(J))+(ALSC*DELL(J)*QSS*
      2BBS+ALSS*QSC*DELK(J)*BBS+ALSS*QSS*BBC*DELB(J))
      CONTINUE
824  F1=ALSS**2*QSC*(1.-BBC)+QSC*BBC-ALSC*QSS*BBS
      F2=QSS*BBC+ALSC*QSC*BBS
      DO 825 J=1,3
      DELF1(J)=ALSS**2*QSC*BBS*DELB(J)+(1.-BBC)*(-ALSS**2*QSS*DELK(J)+
      12.*ALSS*ALSC*DELL(J)*QSC)-QSC*BBS*DELB(J)-QSS*DELK(J)*BBC+ALSS*
      2DELL(J)*QSS*BBS-ALSC*QSC*DELK(J)*BBS-ALSC*QSS*BBC*DELB(J)
      DELF2(J)=-QSS*BBS*DELB(J)+QSC*DELK(J)*BBC-ALSS*DELL(J)*QSC*BBS-
      1ALSC*QSS*DELK(J)*BBS+ALSC*QSC*BBC*DELB(J)
      CONTINUE
825  DO 826 J=1,3
      DELX1(J)=(F1*DELF2(J)-F2*DELF1(J))-(F1*F1+F2*F2)*DELA(J))/CHX(2)**2
      DELX2(J)=DELG3(J)/CHX(2)
826  DELX3(J)=(HG(2,1)*DELG1(J)-HG(1,1)*DELG2(J))/CHX(2)**2
      PH(1,1)=CHX(3)/CHX(2)
      PH(1,2)=-SHX(3)/CHX(2)
      PH(1,3)=0.0

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PH(2,1)=SHX(3)
PH(2,2)=CHX(3)
PH(2,3)=0.0
PH(3,1)=-CHX(3)*SHX(2)/CHX(2)
PH(3,2)=SHX(3)*SHX(2)/CHX(2)
PH(3,3)=1.0
DO 827 K=4,6
  PH(1,K)=DELX1(K-3)
  PH(2,K)=DELX2(K-3)
  PH(3,K)=DELX3(K-3)
  PH(4,4)=1.0
  PH(4,5)=0.0
  PH(4,6)=0.0
  PH(5,4)=ZSQ*HM02*TTT*ABSI-ZSQ*HM03*TTT*ABC
  PH(5,5)=ABC
  PH(5,6)=ABSI
  PH(6,4)=ZSQ*HM03*TTT*ABSI+ZSQ*HM02*TTT*ABC
  PH(6,5)=-ABSI
  PH(6,6)=ABC
  HM01=HX(4)
  HM02=HX(5)
  HM03=HX(6)
END OF CLOSED FORM TRANSITION MATRIX
C 822 CONTINUE
DO 302 I = 1,3
  GAM(1,1) = -C(3,1)*STHE+C(1,1)*CTHE
  GAM(1,2) = C(2,1)
  YOUC = DCOS(OMZ+THETA)
  YOUF = DSIN(OMZ+THETA)
  D(1,1) = -COMC*YOUF-SOMC*CIC*YOUC
  D(1,2) = SOMC*SIC
  D(1,3) = COMC*YOUC-SOMC*CIC*YOUF
  D(2,1) = -SOMC*YOUF+COMC*CIC*YOUC
  D(2,2) = -COMC*SIC
  D(2,3) = SOMC*YOUC+COMC*CIC*YOUF
  D(3,1) = SIC*YOUC
  D(3,2) = CIC
  D(3,3) = SIC*YOUF
DO 305 I = 1,3
DO 305 J = 1,3

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305 C(I,J) = GAM(I,I)*G(I,J)+GAM(2,I)*G(2,J)+GAM(3,I)*G(3,J)
DO 306 I = 1,3
DO 306 J = 1,3
306 BDUM(I,J) = B(I,I)*G(I,J)+B(I,2)*G(2,J)+B(I,3)*G(3,J)
DO 308 K = 1,3
DO 308 L = 1,3
308 B(K,L) = BDUM(K,L)
DO 310 I = 1,3
310 SSP(I) = G(I,I)*SPRM(1)+G(2,I)*SPRM(2)+G(3,I)*SPRM(3)
DO 314 I = 1,6
DO 314 J = 1,6
314 PMDUM(I,J) = PH(I,I)*PP(I,J)+PH(I,2)*PP(2,J)+PH(I,3)*PP(3,J)+
1PH(I,4)*PP(4,J)+PH(I,5)*PP(5,J)+PH(I,6)*PP(6,J)
DO 316 I = 1,6
DO 316 J = 1,6
316 PM(I,J) = PMDUM(I,I)*PH(J,1)+PMDUM(I,2)*PH(J,2)+PMDUM(I,3)*
1PH(J,3)+PMDUM(I,4)*PH(J,4)+PMDUM(I,5)*PH(J,5)+PMDUM(I,6)*PH(J,6)
GO TO (321,322),NZ
321 PSIB = PBO+CWS*TM
QK8(1) = QLBC*DCOS(PSIB)
QK8(2) = QLBC*DSIN(PSIB)
DO 325 I = 1,3
325 QK8P(I) = B(1,I)*QK8(1)+B(2,I)*QK8(2)+B(3,I)*QK8(3)
DO 326 I = 1,3
326 R(I) = SR*D(I,3)
QK8DR = QK8(1)*R(1)+QK8(2)*R(2)+QK8(3)*R(3)
DO 327 J = 1,3
327 BETA(J) = CSUBB*(QK8(J)/SRCUB-3.*QK8DR*(J)/(SRCUB*SR**2))
DO 328 L = 1,3
328 BETAP(L) = B(1,L)*BETA(1)+B(2,L)*BETA(2)+B(3,L)*BETA(3)
322 RETURN
END

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