# <u>TITLE PAGE</u>

## DEVELOPMENT AND BUILD OF PROTOTYPE TOOLS FOR INDUCTION BRAZING OF STAINLESS STEEL TUBING AND FITTINGS FOR NASA APPLICATIONS

#### Final Report

Prepared for George C. Marshall Space Flight Center, Huntsville, Alabama.

Technical Information Series Report No. R66FPD47 March, 1966.

Prepared under Contract No. NAS8-11554 Control No. 1-4-8-00001 (IF) by the Braze Development Laboratory, Large Jet Engine Department, Flight Propulsion Division, General Electric Co., Evendale, Ohio

O.H. S

D. H. Greisl Author

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### FORWARD

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This final report covers the work performed under NASA Contract NAS8-11554, Control No. 1-4-8-0000 (IF). The contract work included the design and manufacture of sizing equipment for the tubing to be brazed; the design of couplings, elbows and tee type braze fittings; the development and manufacture of split type induction braze tools for these fittings; the design and manuvacture of debraze tooling; the evaluation of high frequency induction brazing on heavy wall large 0.D. tubing; and the training and instruction of Marshall Space Flight Center personnel in the use of these tools.

This program was conducted in the Braze Development Laboratory, Manufacturing Process Applications Development, Large Jet Engine Department, Flight Propulsion Division, General Electric Co., Evendale, Ohio. George F. Albers, Supervisor of the Braze Development Laboratory, was the Program Manager and Don H. Greisl of the Braze Development Laboratory was the Project Engineer for the program.

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### ABSTRACT

The design and manufacture of sizing tools for the tubing to be brazed; the design of couplings, elbows and tee type fittings; the design and manufacture of split type induction tools to braze these fittings to the tube ends; the design and manufacture of the debrazing tools; and the use of high frequency induction brazing of heavy wall tubing (.188 wall thickness -0.D. 2") are described in this report.

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#### INTRODUCTION

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The systems and components of rocket propulsion vehicles must function under severe environmental operating conditions. Rocket propulsion fluid systems, in particular, are subjected to extremes of temperature, pressure and vibration for short periods of time. The standard threaded type aircraft engine fittings currently being used for tubing connections in rocket propulsion fluid systems are inadequate. Leakage can occur when the vehicle is exposed to operating conditions. Advanced tube joining methods are required which will provide zero leakage and light weight with a high degree of operational reliability.

Techniques for making "on engine" tubing connections by induction brazing had been developed by the Brazing Development Laboratory, Large Jet Engine Department, Flight Propulsion Division, General Electric Company, Evendale, Ohio for use on the J93 Engine used to power the XB-70 air vehicle. This technique was considered feasible and worthy of further development for joining advanced rocket propulsion fluid tubing systems.

The purpose of this program was to design, develop, manufacture and demonstrate induction brazing and related tooling and connectors for fluid tubing systems on rocket propulsion vehicles.

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#### TOOLING

The NASA contract required the design and construction of six (6) split coil inductors (one of each size) for brazing 1/4", 3/4", 1 1/4", 1 1/2", 2" and 2 1/2" tubing using a straight coupling: the design and manufacture of five (5) split coil inductors (one of each) for brazing the pre-mentioned tubing sizes except the 2 1/2" for elbow and tee type fittings; the design and building of sizing equipment for sizing tubing to a controlled diameter in the following size tubing: 1/4", 3/8", 1/2", 3/4", 1", 1 1/4", 1 1/2", 2" and 2 1/2"; the design and building of debrazing equipment, (one of each) for 1/4", 3/4", 1 1/4", 1 1/2", 2" and 2 1/2";

The development of each type tool will be reviewed in detail. Each aspect of the process is defined and each applicable tool discussed.

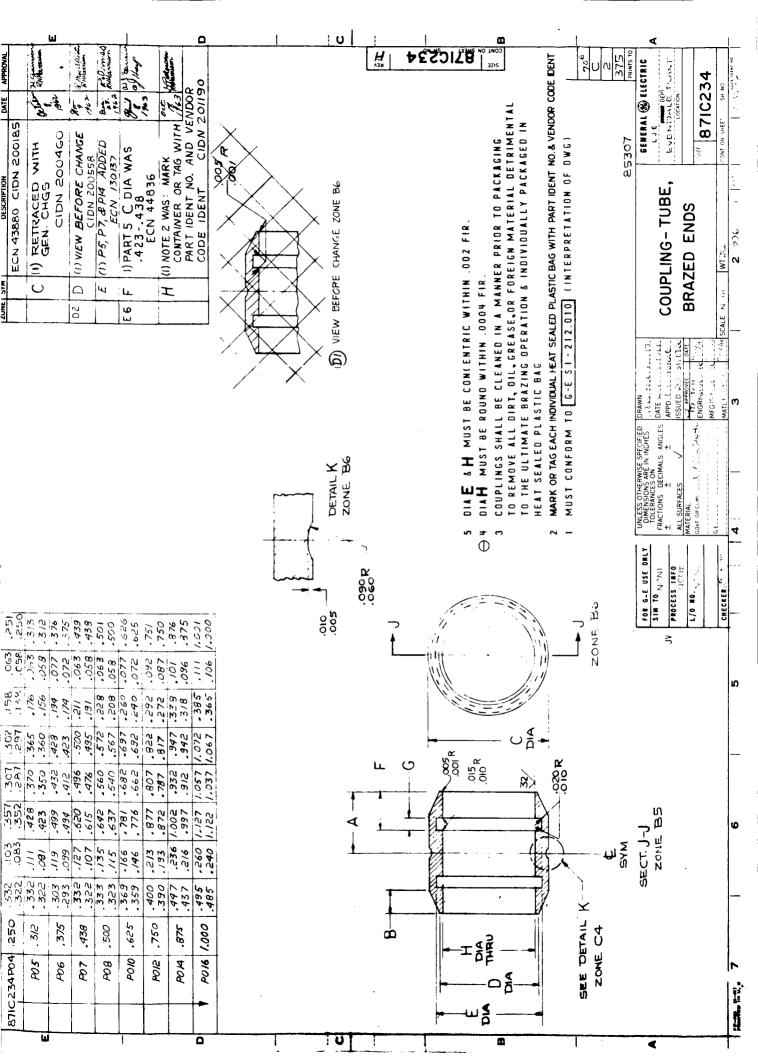
#### Split Inductors For Straight Couplings

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The basic process consists of induction brazing tubing and couplings together to produce a strong, leak-resistant joint. This is accomplished by assembling a coupling, containing preplaced braze alloy (print 871C234) equally over two tube ends and induction heating the area to the braze alloy flow temperature.

To satisfy these requirements the split coil inductors must exhibit the following characteristics: a split induction heating coil having the effect of one continuous wound coil, a split atmospheric chamber with inert gas inlets and outlets, and a chamber that houses the split coils with an air cooling manifold.

The split atmospheric chamber permits visual observation of the joint during the brazing operation. It also envelopes the joint providing an oxygen free atmosphere. An advantage of being able to see the joint during the brazing operations is that if the automatically alloted time does not produce a good braze joint, manual control of the heating cycle can be assumed until the alloy has flowed and formed a sound joint. Secondly, melting of the braze alloy can be observed or monitored visually. Melting is evident by a dark shadow seen on the coupling representing the braze alloy as it melts and starts to flow.



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## Manufacture Of Atmospheric Chamber

Pyrex tubing of the correct diameter is split off center lengthwise and lapped flat to the correct dimension. One half of the tube is scrapped for being undersize. This is compensated for, by the advantage that matched halves are not a requirement. One half can be replaced with another tube half with the assurance that an adequate atmospheric chamber is being obtained.

A water-cooled metallurgical cut-off machine utilizing a glass cutting wheel, was used to perform the splitting operation. Cutting dimensions were obtained by the use of a plexiglass guide block attached to the travel table on the cut-off machine. Little difficulty resulted with this cutting technique. The split tube contact surfaces were relatively chip free, but untrue. An aluminum oxide (grinding wheel - fine grit) served as the lapping plate to correct the contact surface. Dimensional checks were taken periodically to ascertain the quality of this operation. The lapping method is a light, even hand stroke in one direction at all times. The quality was exceptionally good, chipping was almost negative, and a ± .002" on altitude and a .005" F.I.R. on surface flatness could be maintained. This method is acceptable for producing the split atmospheric chamber. Table I lists the final configurations and dimensions.

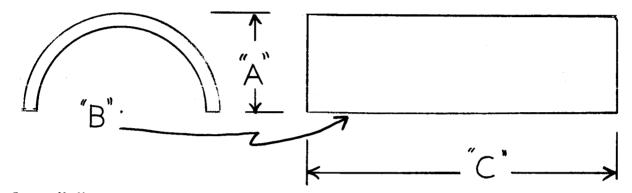
Splitting glass for the elbow and tee type tool is accomplished in the same manner as for the straight coupling tools. One difference exists between the two types of tool glass. For the elbow and tee type tools, the glass is molded to the required diameter by placing the split glass in a ceramic mold and yielding (forming) at a temperature of 1500°F for five (5) minutes.

This molding of the glass insures tighter control on glass dimensions, assuring more efficient sealing at the split line. Standard pyrex tubing in larger diameters has greater tolerances on the O.D. and I.D. than is needed for (split induction braze tools) sealing chambers. Molding of the glass also eliminates the problem of using several different size O'Rings to hold the glass in place. Table II lists the final configurations and dimensions.

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TABLE I. Tolerances For Glass Tools Used In Brazing Straight Couplings



Surface "B" to be flat w/in .0005 F.I.R. and surface "B" parallel to top of tubing w/in 003 in.

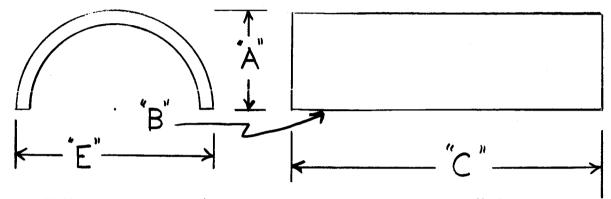
0.D. <u>Brazed Tube</u>	Tube 0.D. (MM)	Tube Wall (MM)	Dim. "A" <u>Inches</u>	Dim. "C" Inches
250	13.4	1.3	.266	2.26
	12.6	1.1	.251	2.24
750	28.7 27.3	1.7 1.3	•550 •535	2.26 2.24
1.250	46.0	2.2	.897	3.63
	44.0	1.8	.882	3.61
1.500	52.0 50.0	2.2 1.8	1.015	3.63 3.61
2.000	76.3 73.7	2.7 2.1	1.487 1.474	3.63 3.61
2.500	81.3 78.7	2.7 2.1	1.536 1.521	3.63 3.61

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Glass Tolerances For Elbow TABLE II. And Tee Type Tools



Surface "B" to be flat w/in .0005 F.I.R. and Surface "B' parallel to top of tubing w/in 003 in.

Brazed Tube 0.D.	Tube O.D. <u>Nom. (MM)</u>	Tube Wall Nom. (MM)	Dim. "A" Inches	Dim. "C" Inches	Dim. "E" <u>Inches</u>
.250	13.0	1.2	.260 .255	1.32	.520 .510
.750	28.0	1.5	.5675	1.57	1.135 1.125
1.250	45.0	2.0	.880 .875	1.95	1.760 1.750
1.500	51.0	2.0	1.005 1.000	1.95	2.010 2.000
2.000	70.0	2.4	1.400 1.395	2.32	2.800 2.790

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# Split Coil Inductors And Housing Block

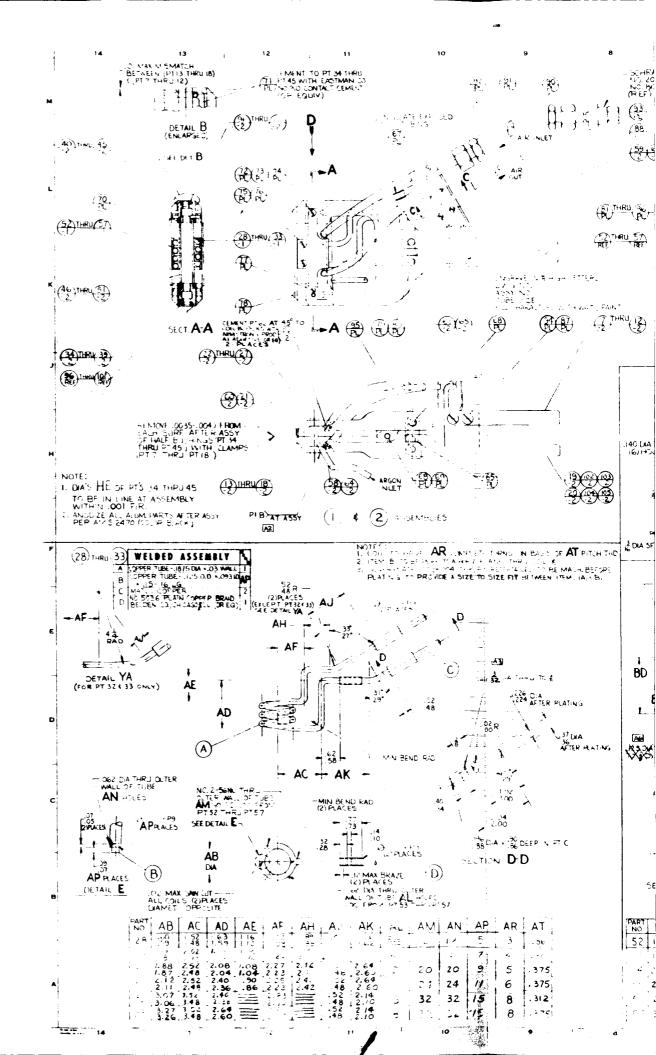
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The coils are supplied in equal halves, but function as one continuous wound coil. Coils are housed in a rigid chamber of RPD 150 (composed of preimpregnated long spinning grade chrysotile asbestos fibers and a high heat resistant phenolic resin system) material and containing an air manifold for cooling of all coil halves. The coil is so constructed that if one portion of the coil were accidently damaged it could easily be replaced, preventing the loss of a complete coil. The individual coil segments are contained and positioned in RPD 150 block by means of two small screws. Between the two screws is an air passage from the manifold to the coil segment, thus cooling each segment separately. Air is discharged on the 0.D. of each coil near the split line thru a small hole drilled in the coil segments as seen in Figure 1 and 1.A.

The cooling air in the 1/4" tool enters from one side of the coil and travels through the coil discharging at the opposite opening (See figures 2 & 2A). These particular split coil inductors are for brazing the 1/4", 3/4", 1 1/4", 1 1/2", 2" and 2 1/2" tube joints with straight connectors. Table III lists the split coil data for the above mentioned coils. Several other features of the split coil inductors are:

- 1. A flexible copper braided joint at the pivot point of the clamp allowing freedom of movement while in operation.
- 2. A special copper cable connecting pin, silver brazed to the end of each coil lead.
- 3. A double argon feed system to prevent a heat sink.
- 4. Ease of opening and closing of split coil.
- 5. Extra argon channel between O'Rings to prevent oxidation.

Figures I through 6A are the split inductors delivered to NASA for use in brazing straight couplings, print 4012180-651.



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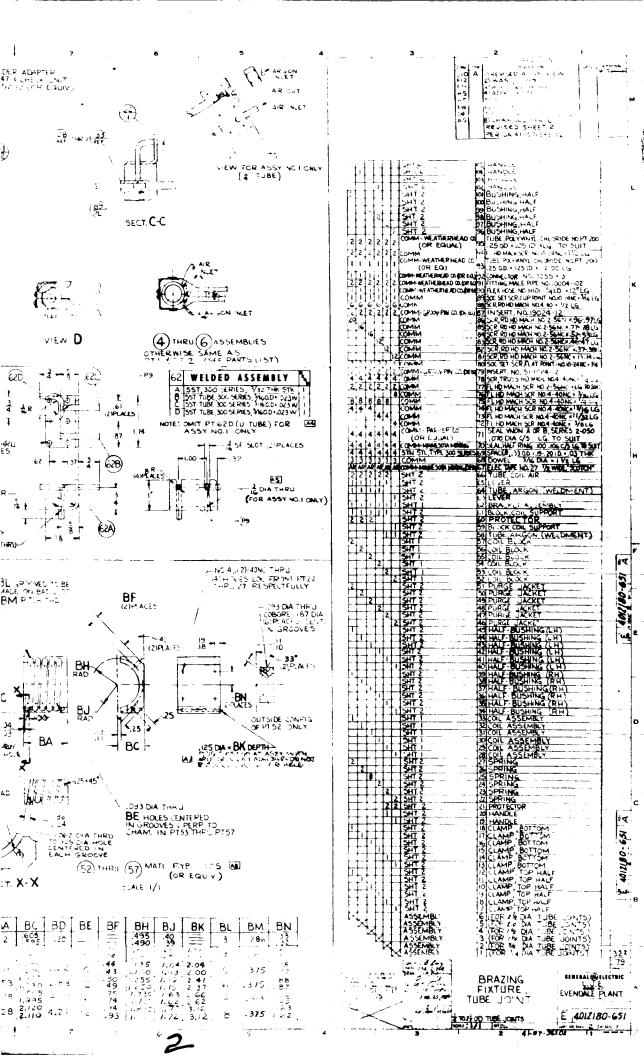




Figure 1

AIR DISCHARGE HOLES

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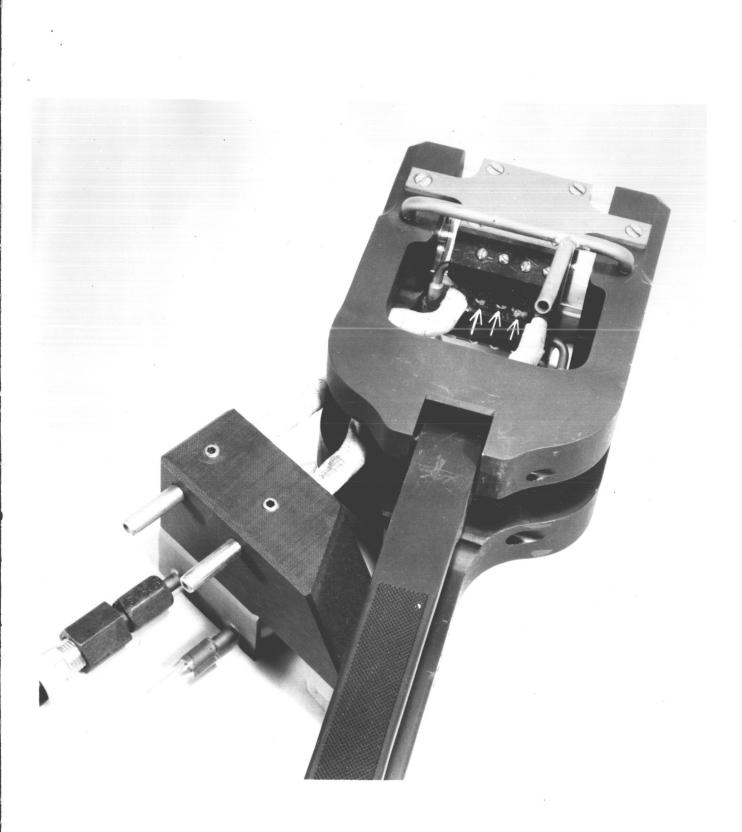


FIGURE 1 A

AIR DISCHARGE HOIES (3/4"Braze Tool)



FIGURE 2

l/4" BRAZE TOOL (A-Air Inlet)

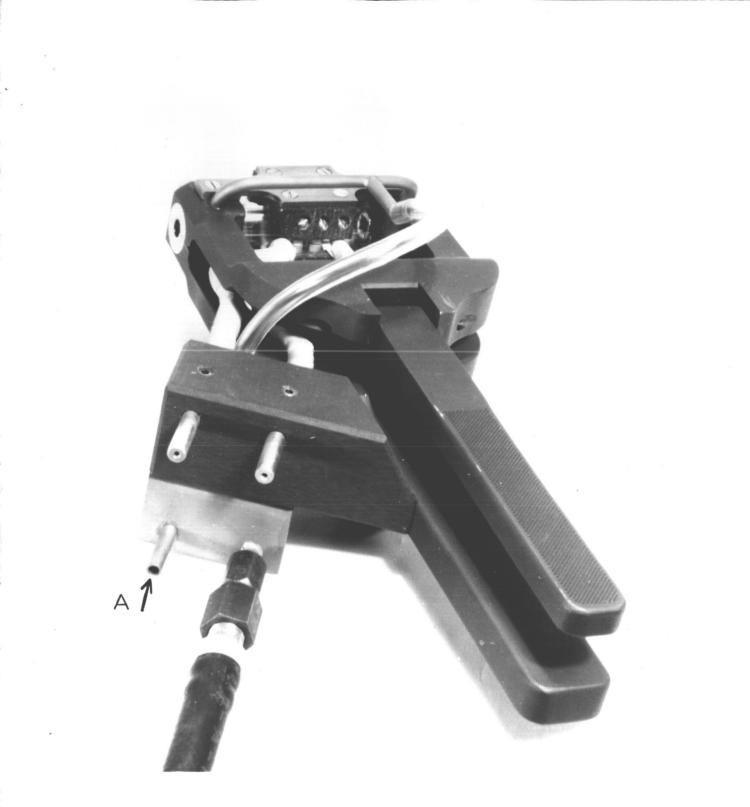


FIGURE 2A

l/4" BRAZE TCOL (A-Air Discharge)



. FIGURE 3

1 1/4" BRAZE TOOL



FIGURE 3A

1 1/4" BRAZE TCOL

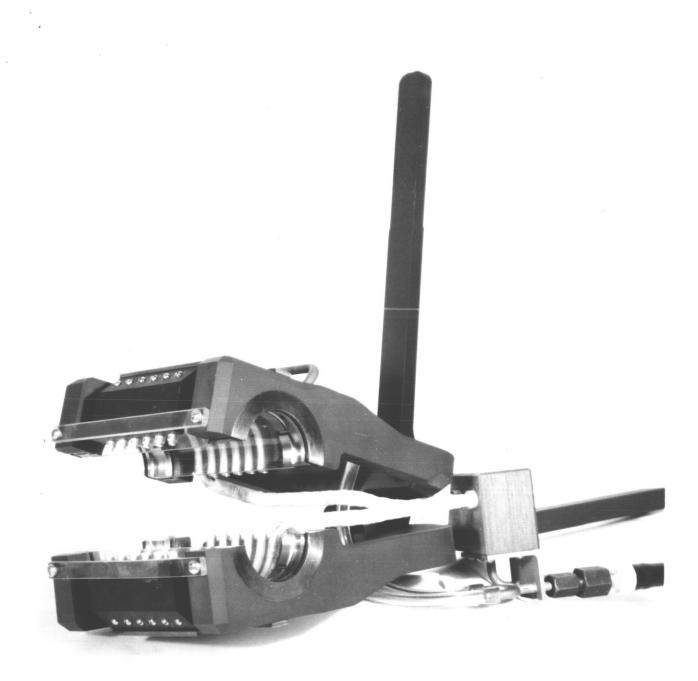


FIGURE 4

1 1/2" BRAZE TCOL

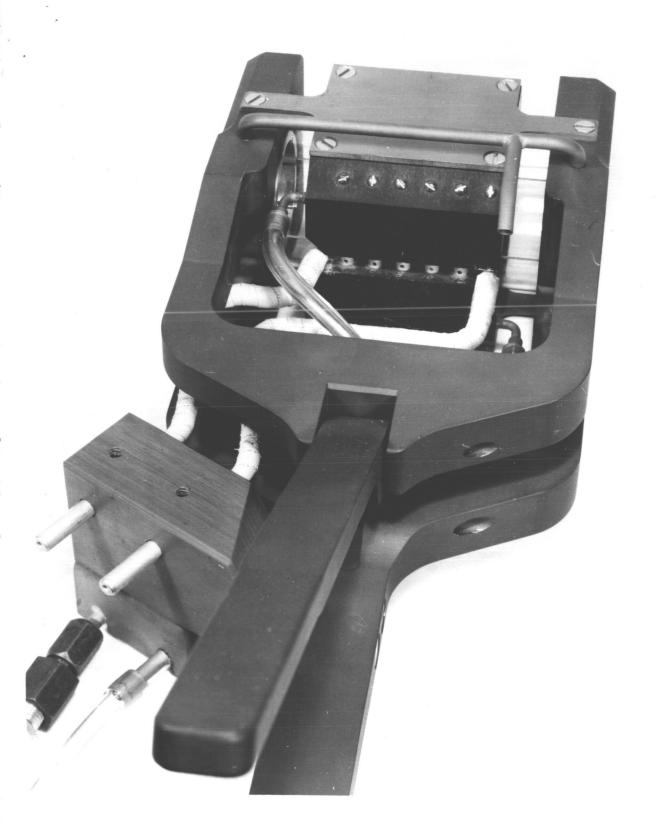


FIGURE LA

1 1/2" BRAZE TOOL

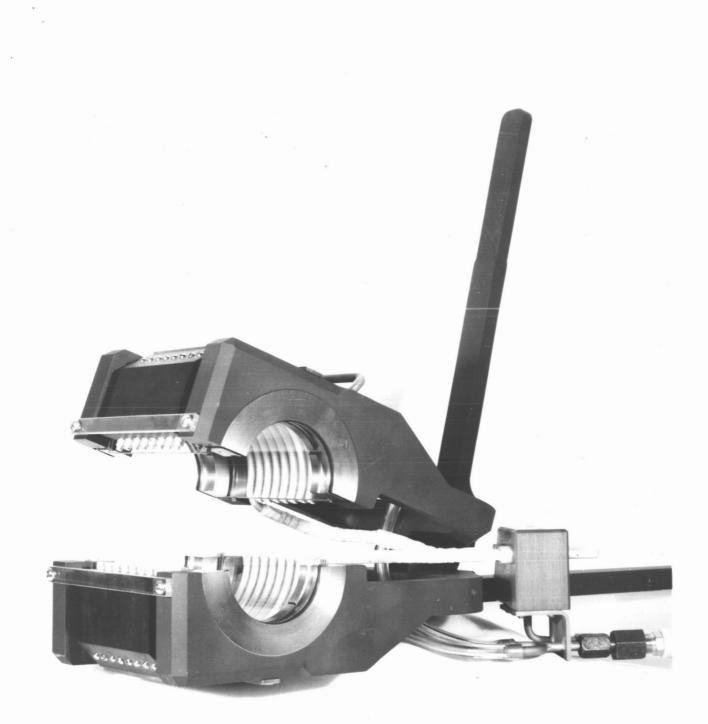


FIGURE 5

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2" BRAZE TOOL

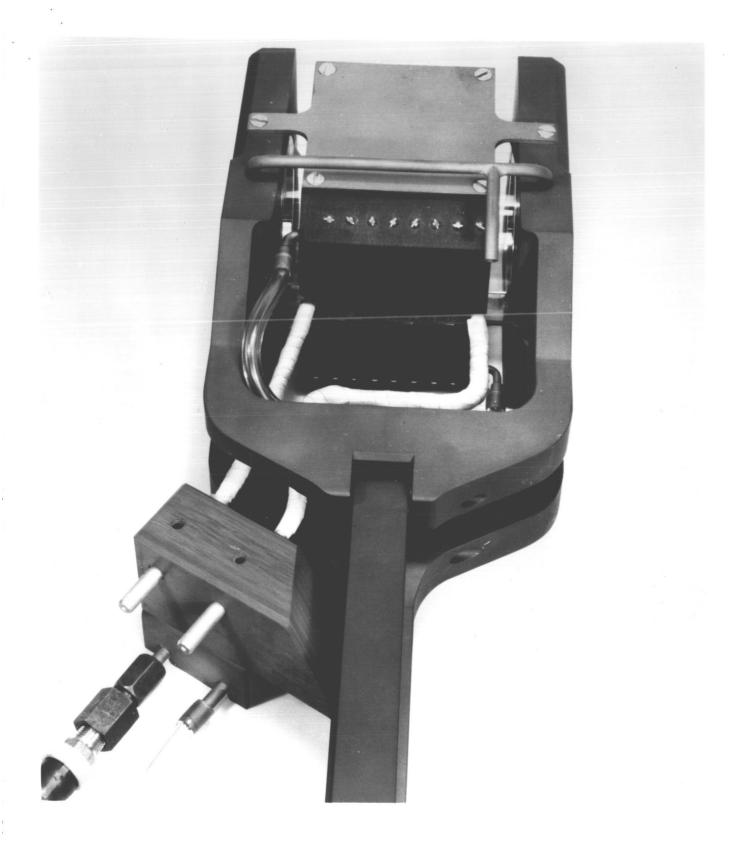


FIGURE 5A

2" BRAZE TCOL

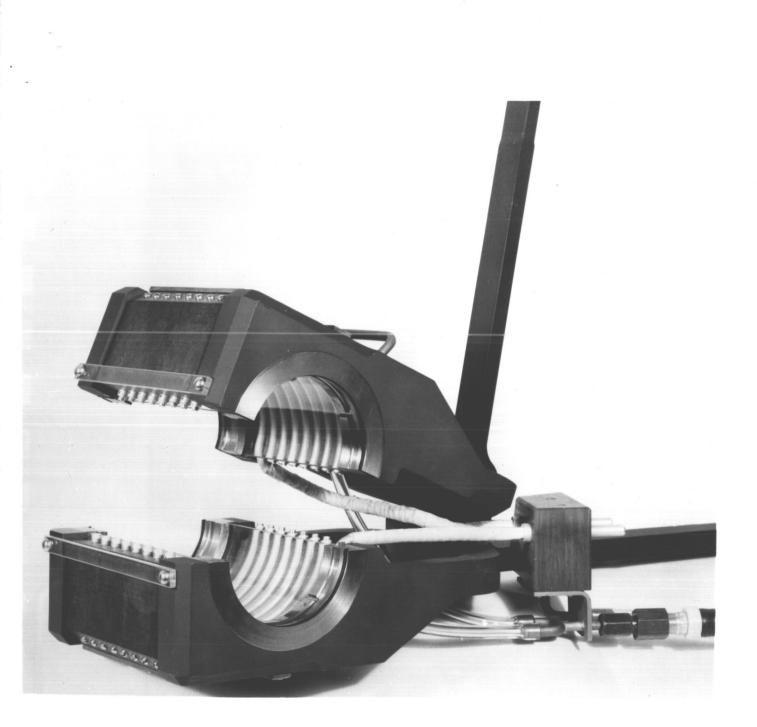


FIGURE 6

2 1/2" BRAZE TOOL

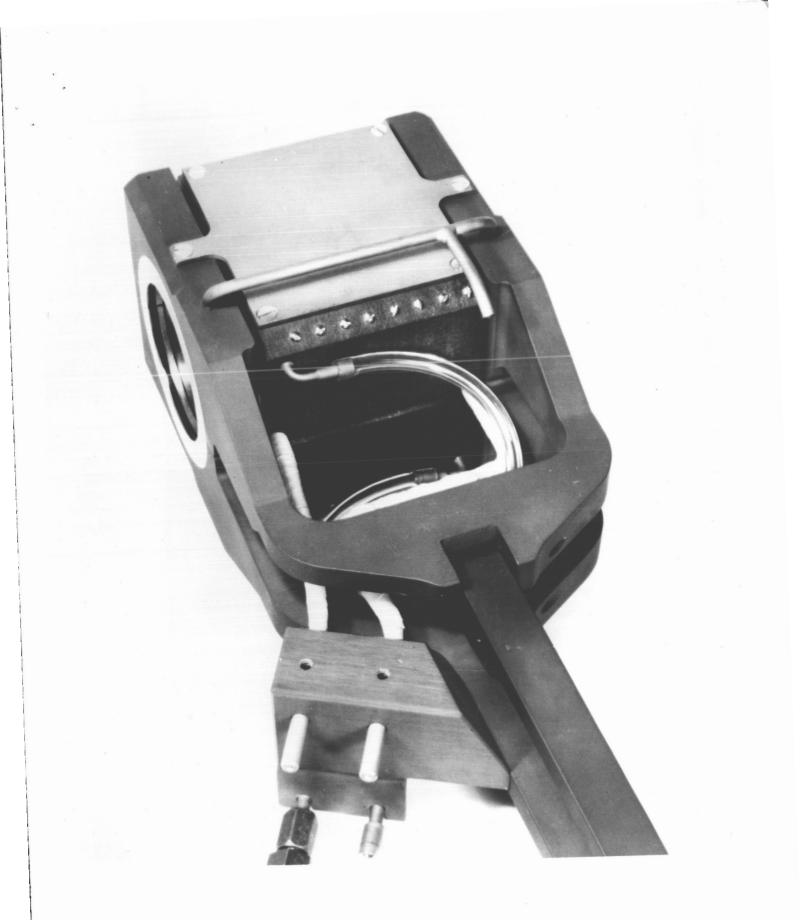


FIGURE 6A

2 1/2" BRAZE TOOL

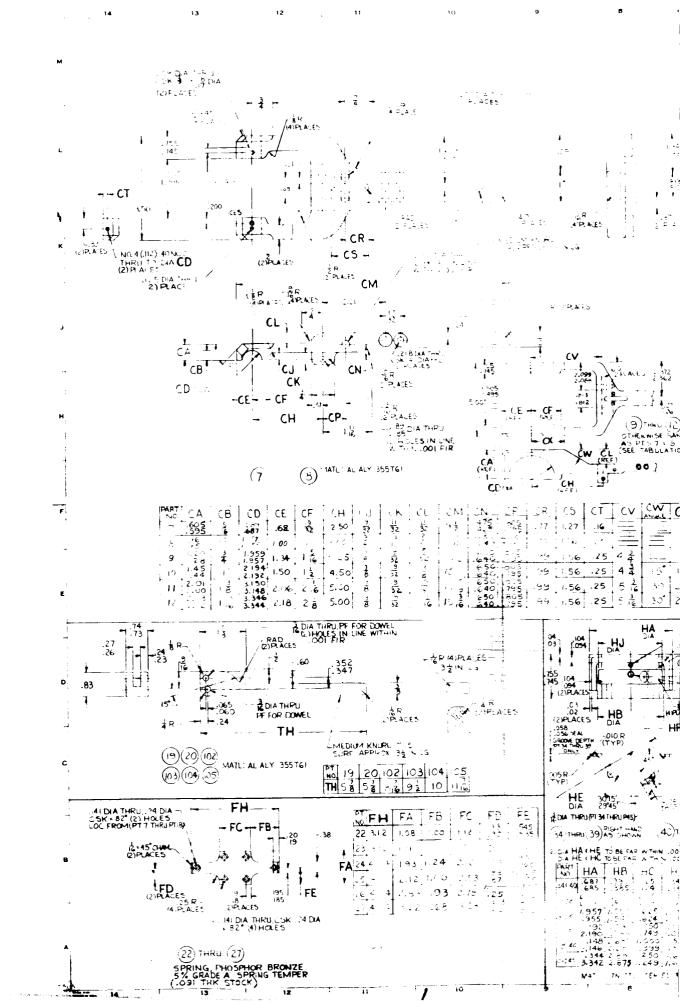
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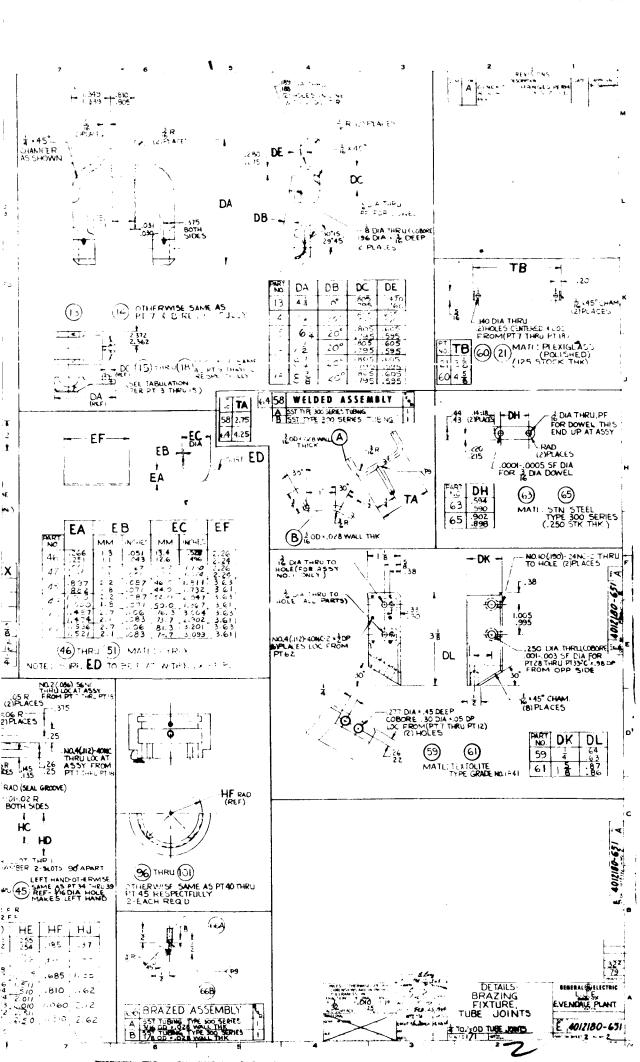
# INDUCTORS FOR ELBOW AND TEE FITTINGS

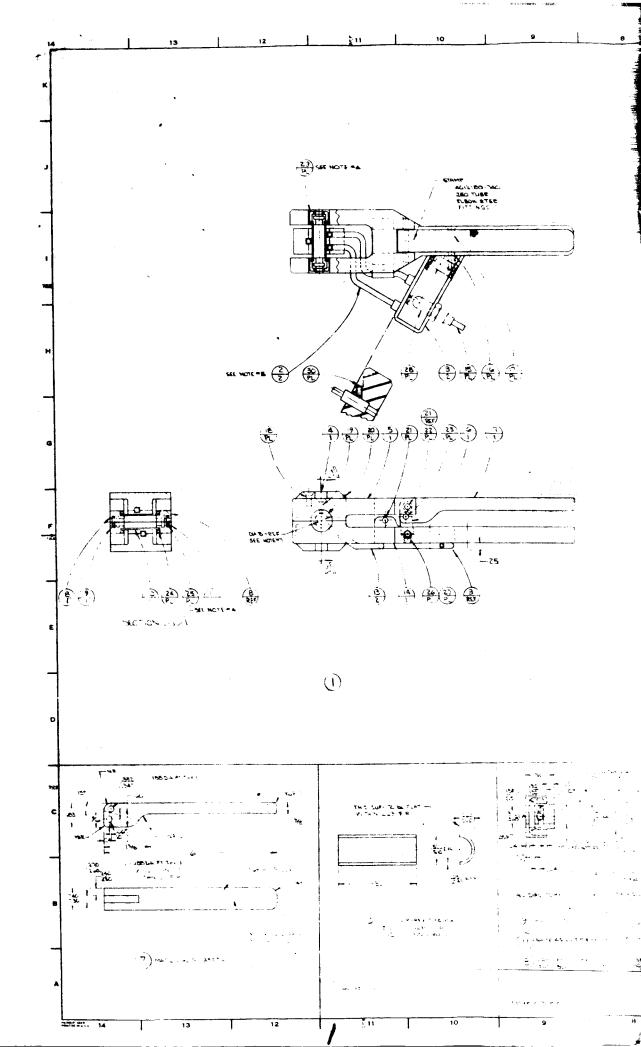
Housing of the split coil inductor for brazing elbow and tee type fittings is similar to that used for the coil for brazing straight couplings. The coil itself is made from square copper tubing instead of round which was used for straight couplings coil. Square copper tubing was used to gain additional surface area needed for efficient heating of these fittings. Greater efficiency could be achieved with coils having a larger surface area, due to the fact that high-frequency currents tend to flow along the surface of the metal. By using square copper tubing the number of turns were reduced, allowing shortening of the straight length required to make a coil for brazing elbow and tee type fittings. The width of the brazing tool was thus reduced. The coil itself has a safety wiper blade attached on the back side of the coil where the coil joins at the split line of the glass chamber. The wiper blade not only insures good electrical contact, but also acts as a shield which prevents back flow of discharged cooling air. As was mentioned previously, the glass for these tools is molded giving tighter control on tolerances and assuring a better atmosphere chamber. The sealing jaws of these tools are made of the RPD 150 material to reduce weight of the tool. The jaws themselves have a double O'Ring groove to insure better sealing. Figure 7 thru 11 show the 1/4" braze tool through the 2" braze tool for brazing the elbow and tee type fittings. Figure 12, 12A and 12B show the braze tools with their carrying case. For details of these tools see prints, 4012180-740 thru 744.

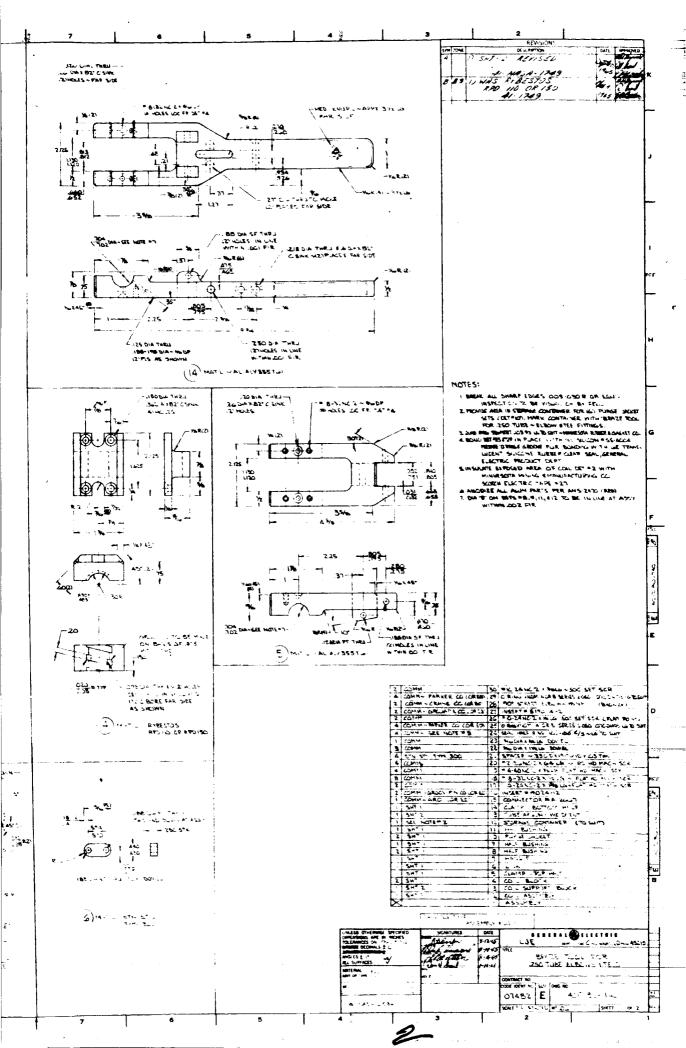
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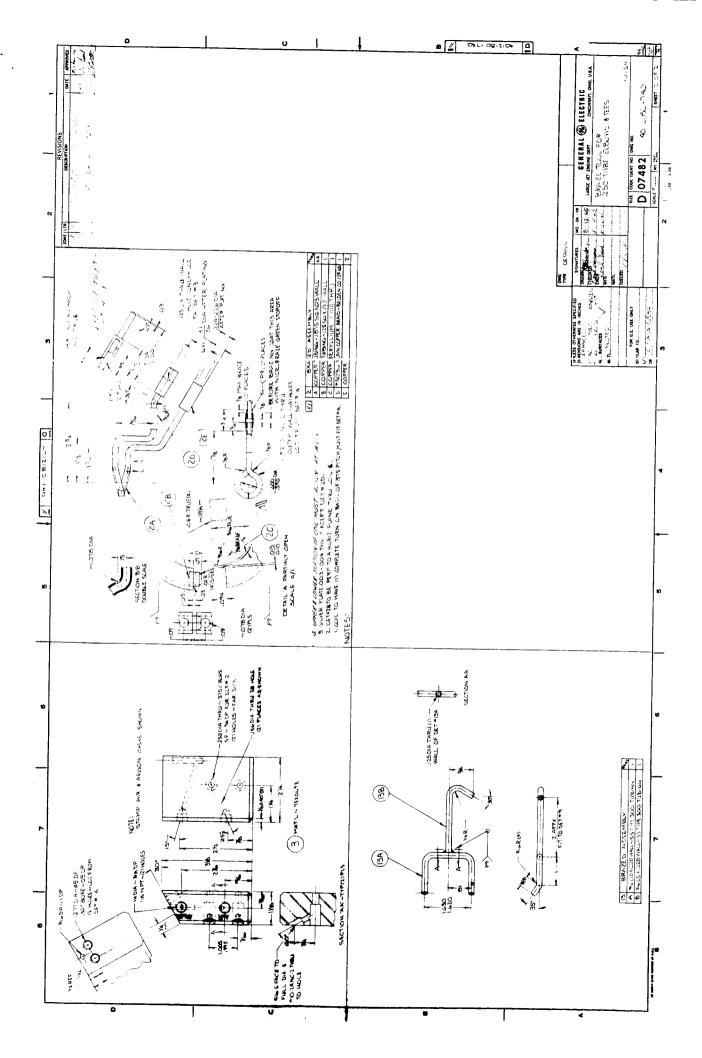
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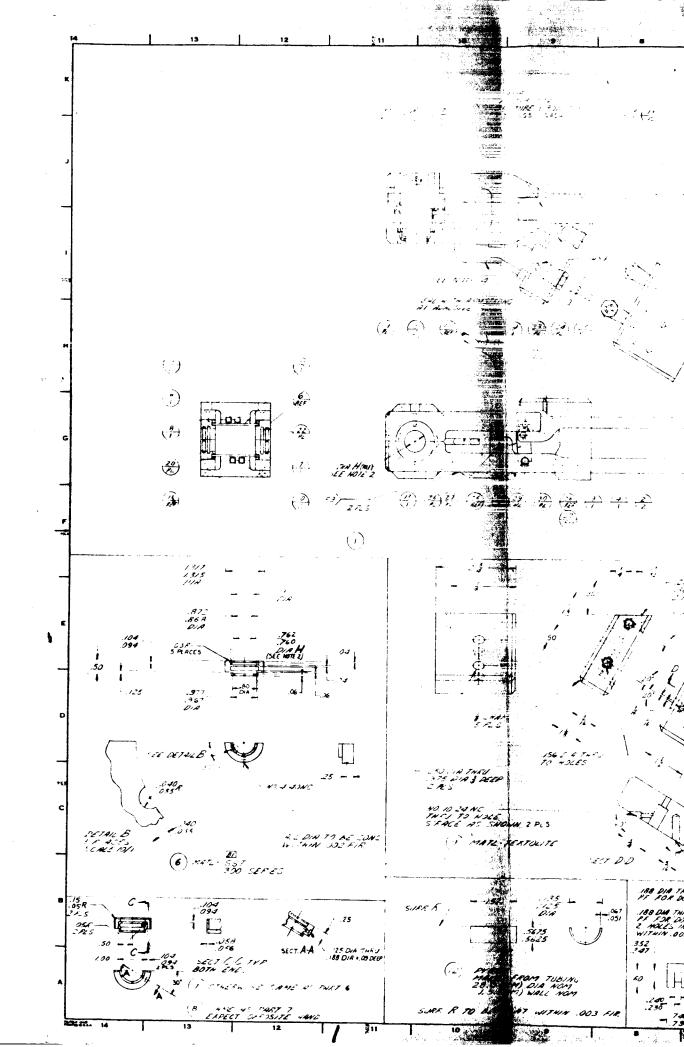


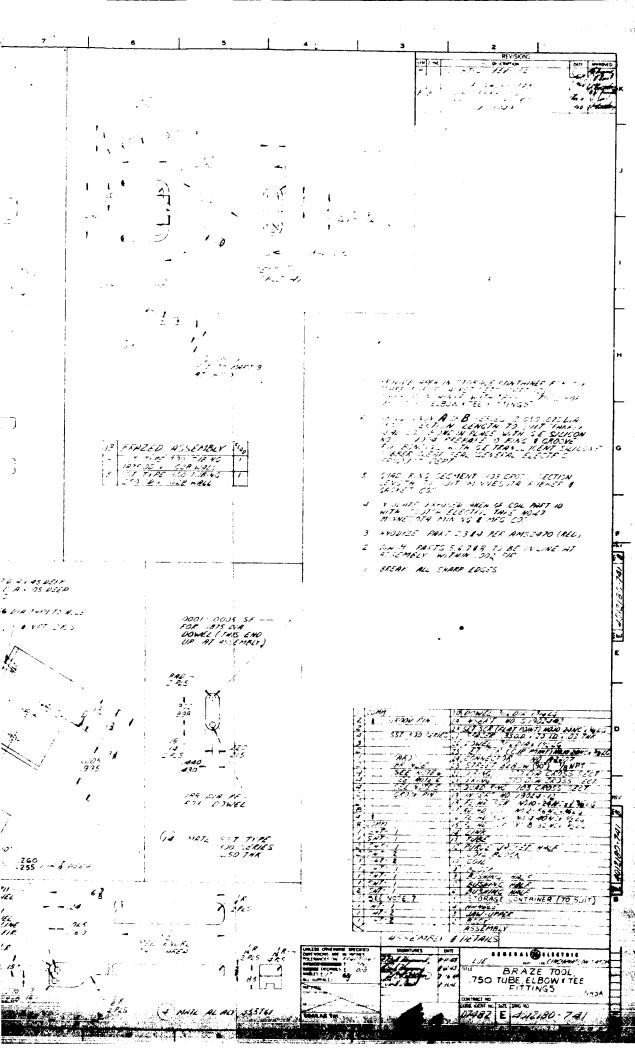


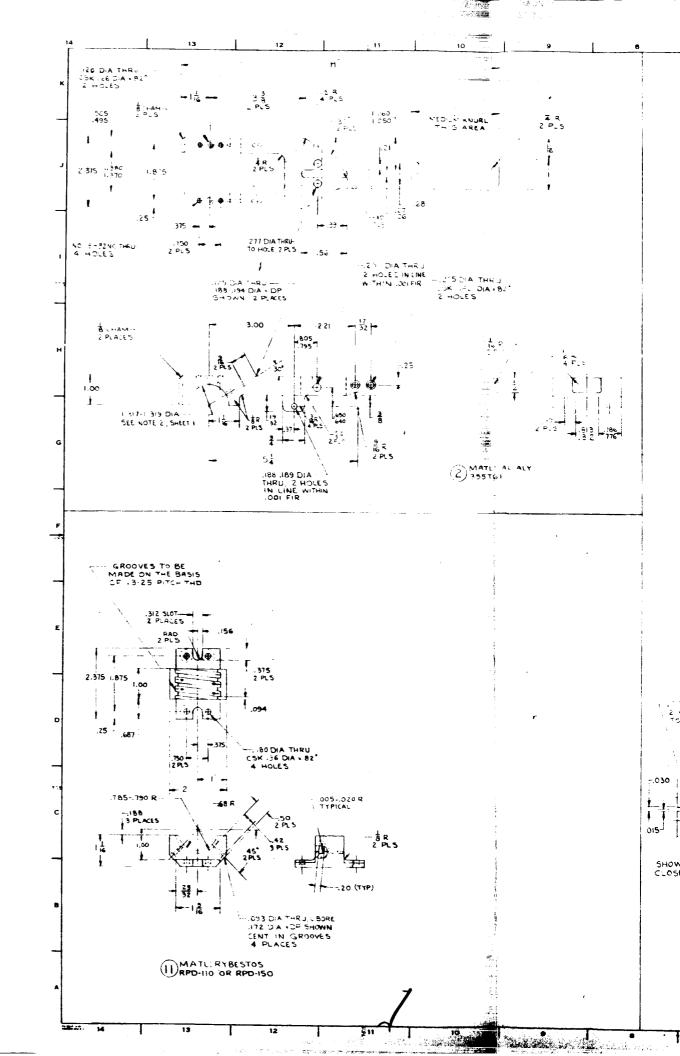


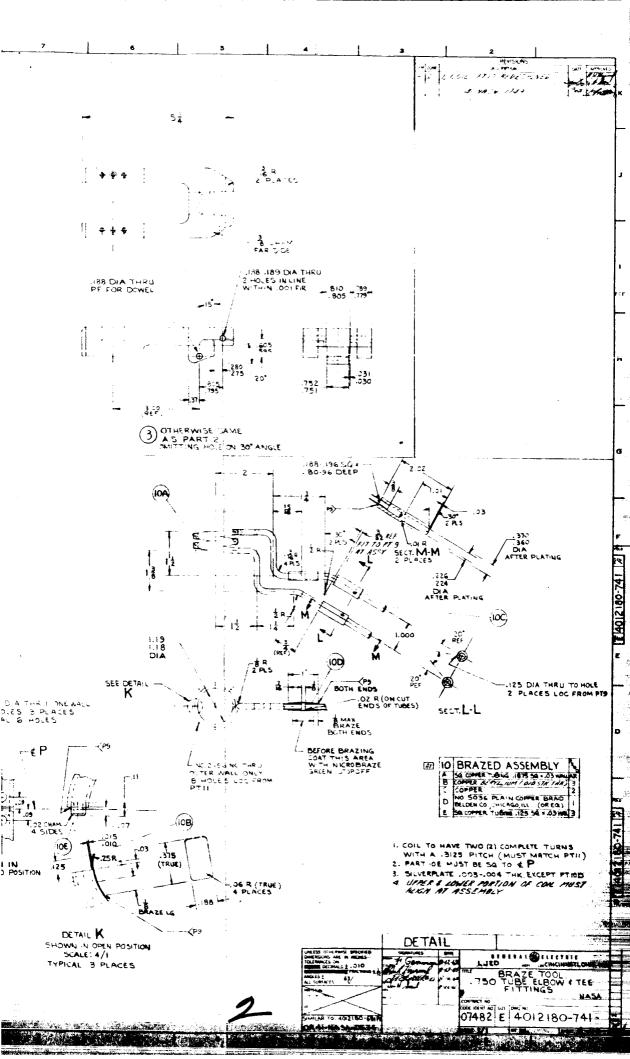


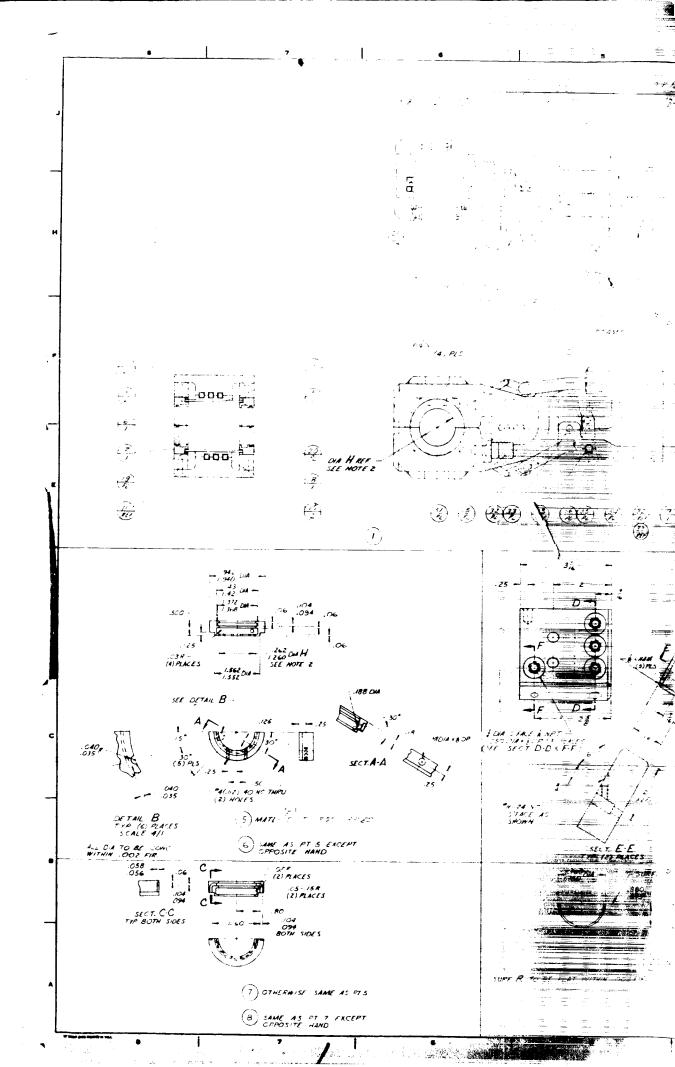


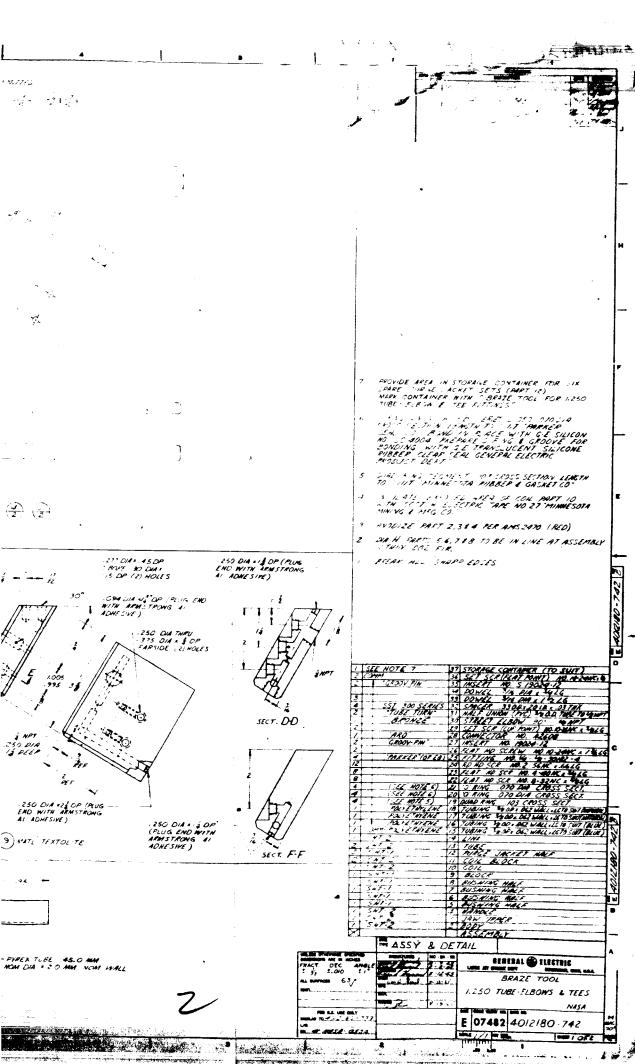


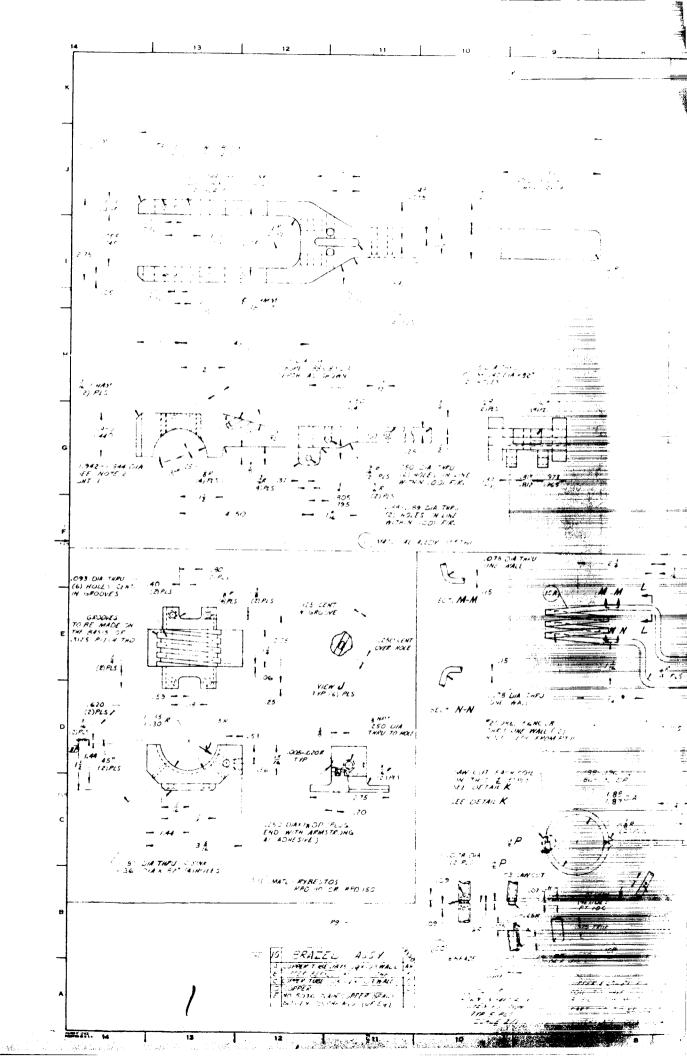


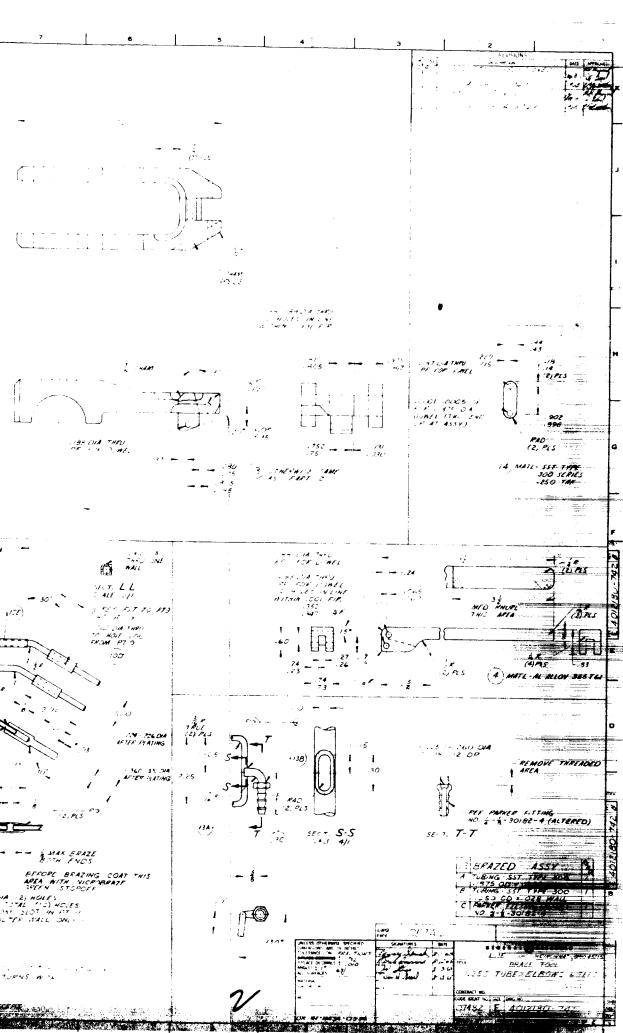


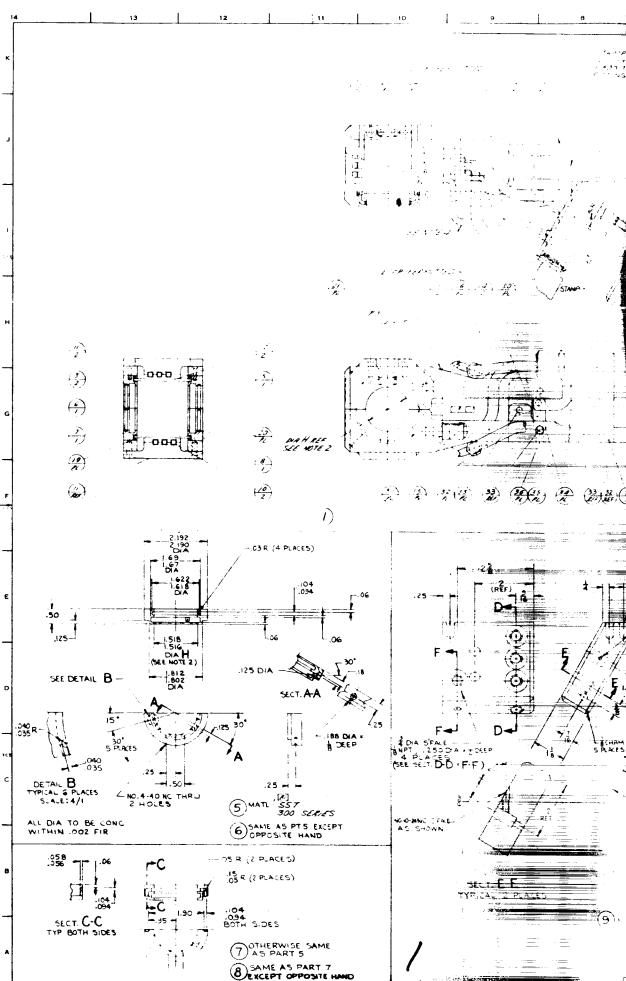




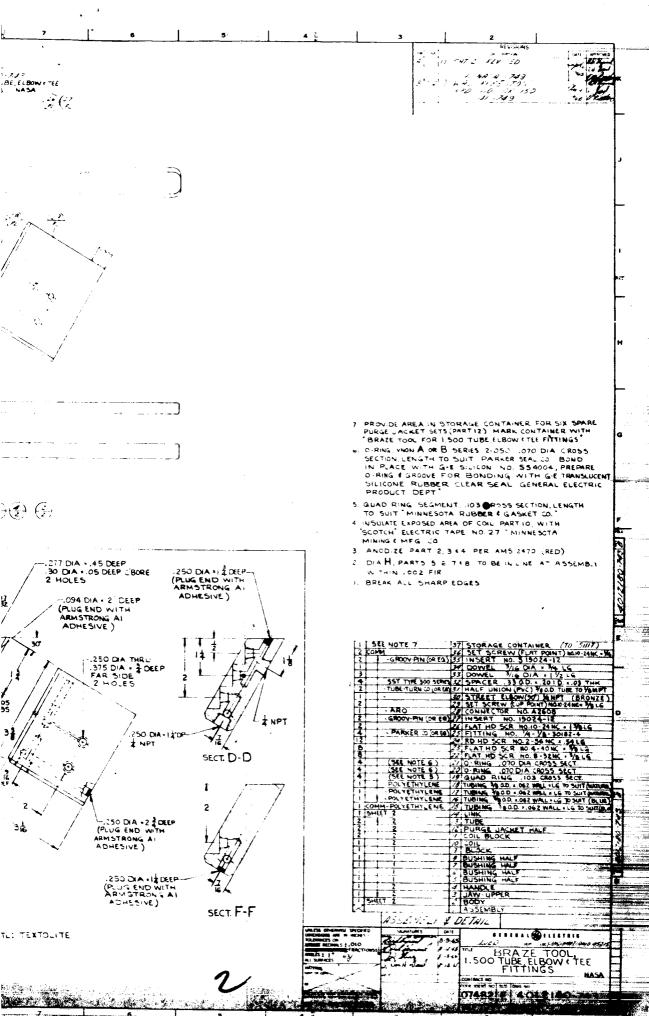




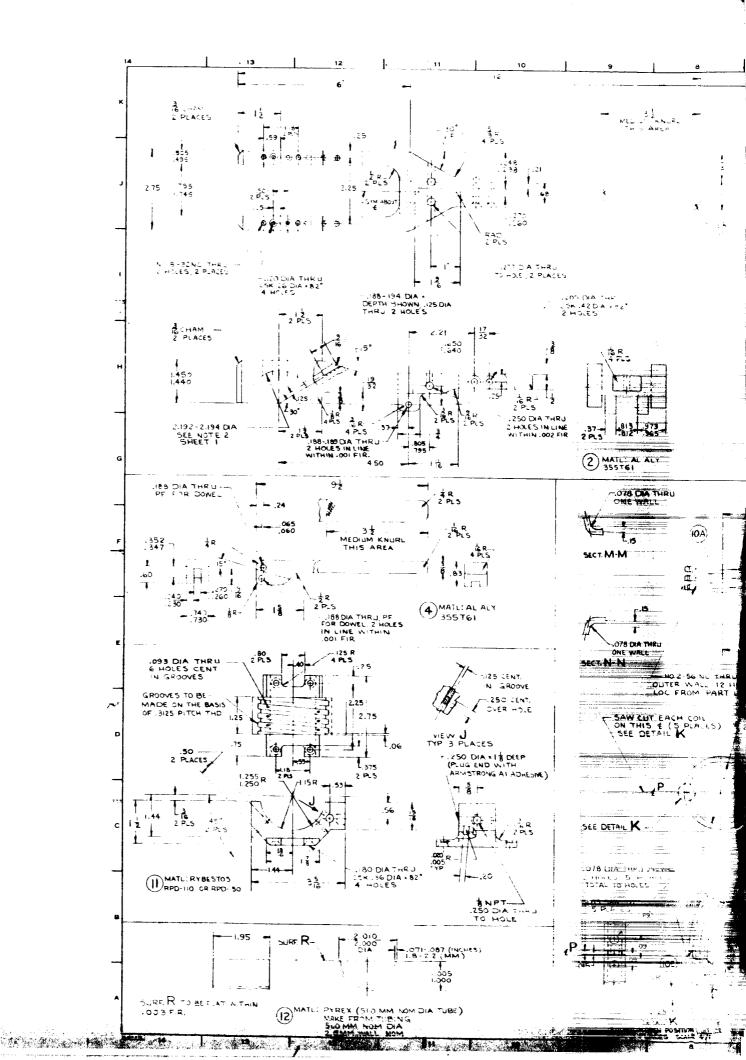


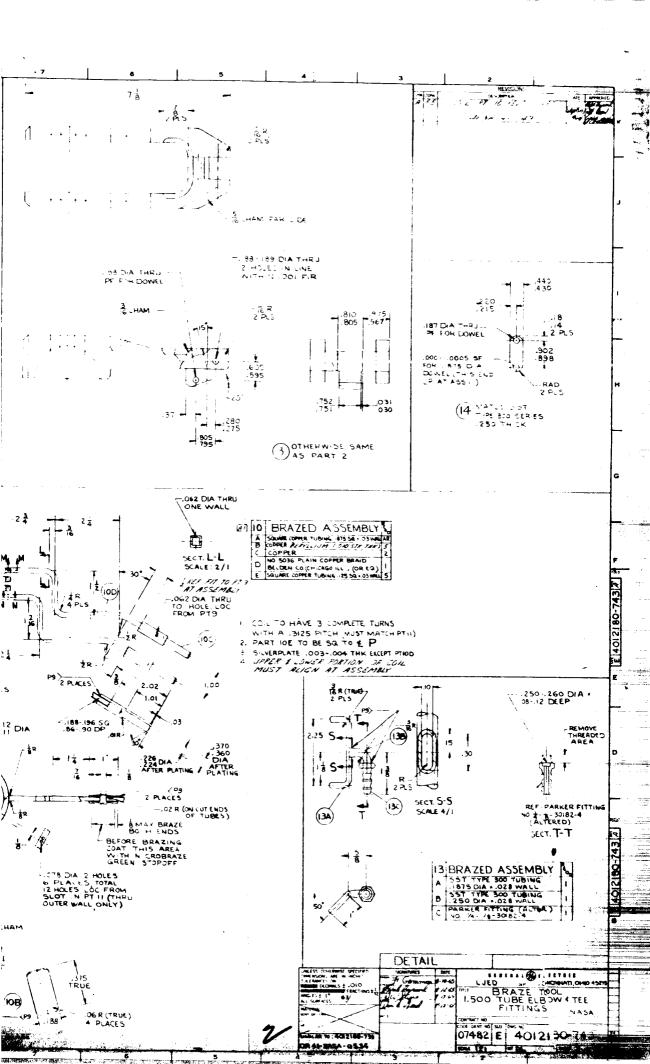


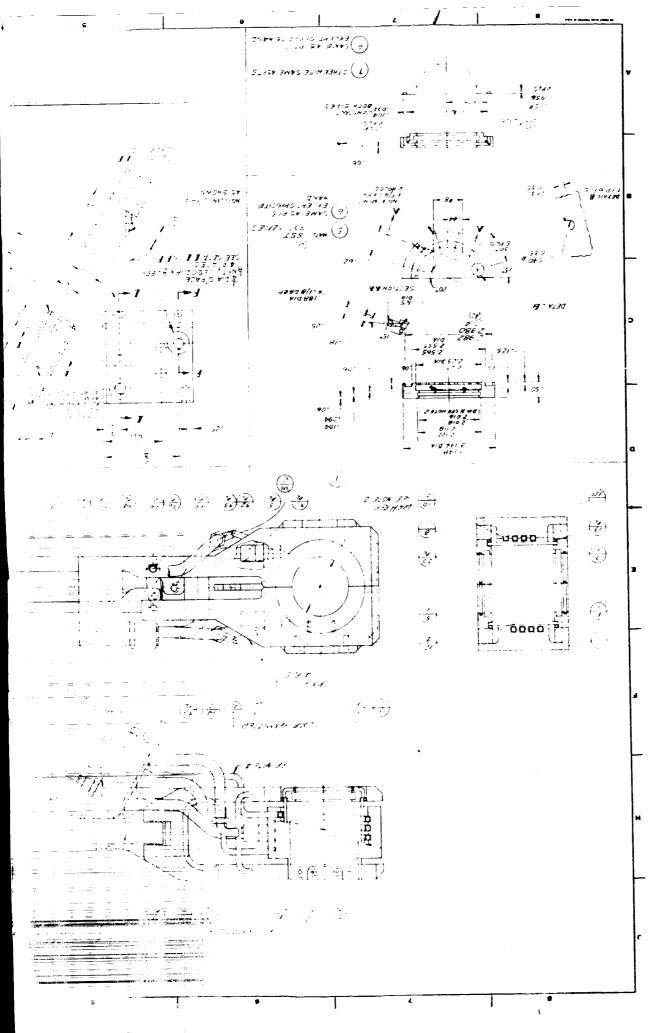
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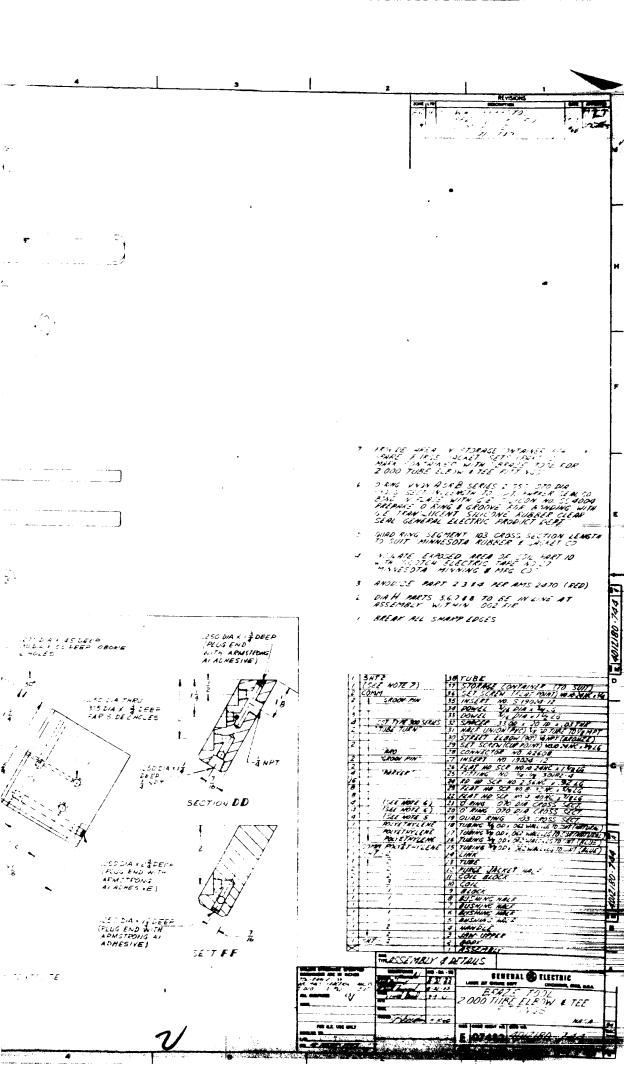


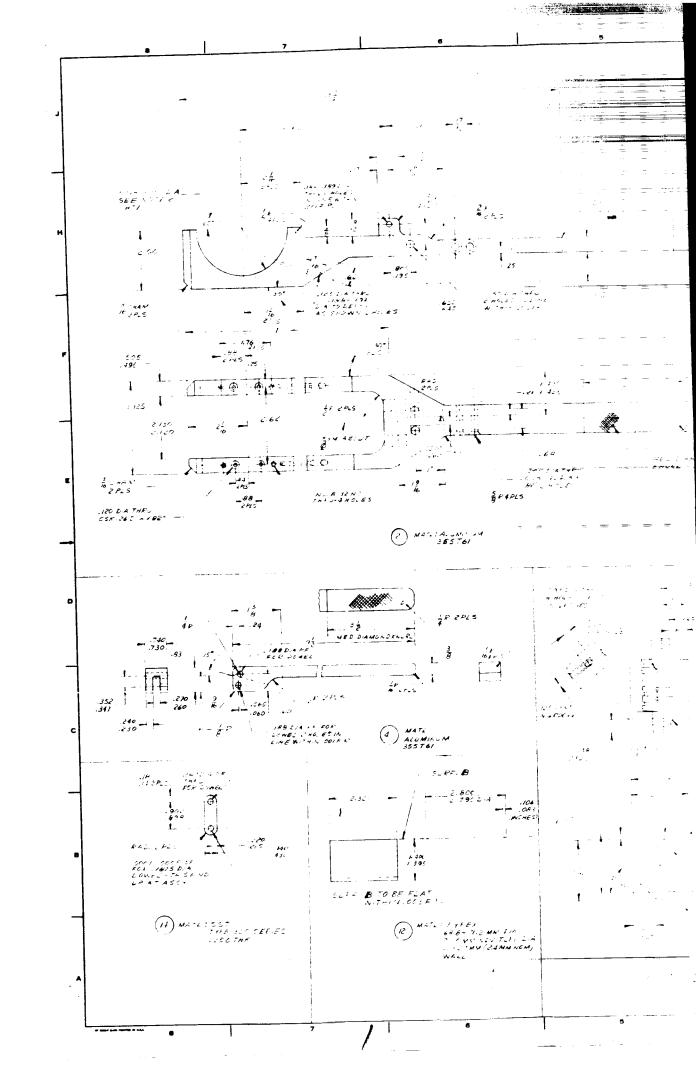
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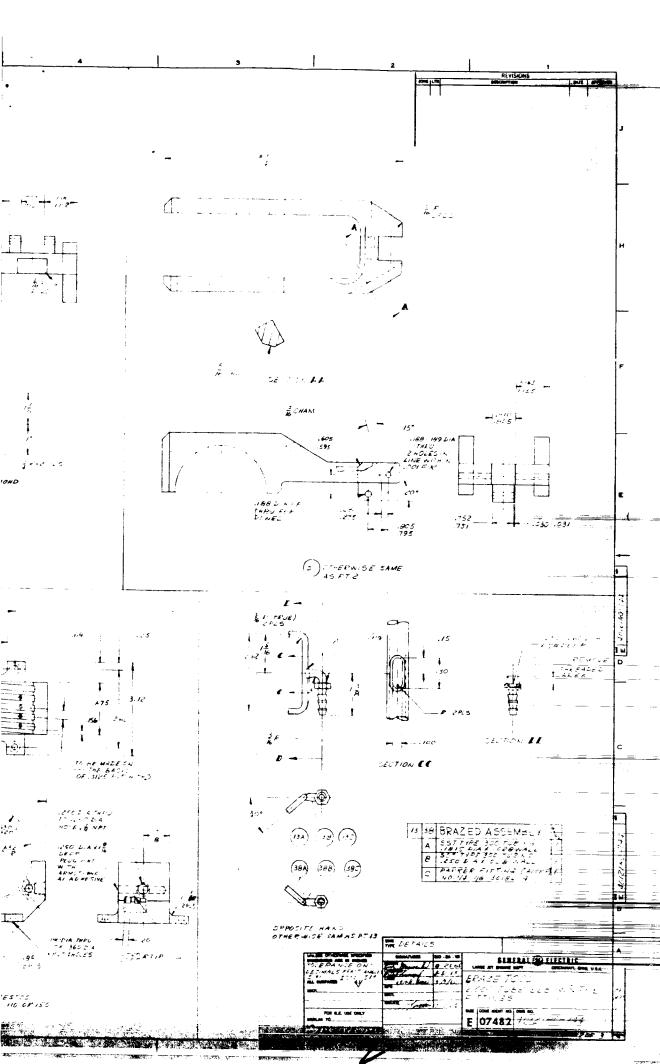


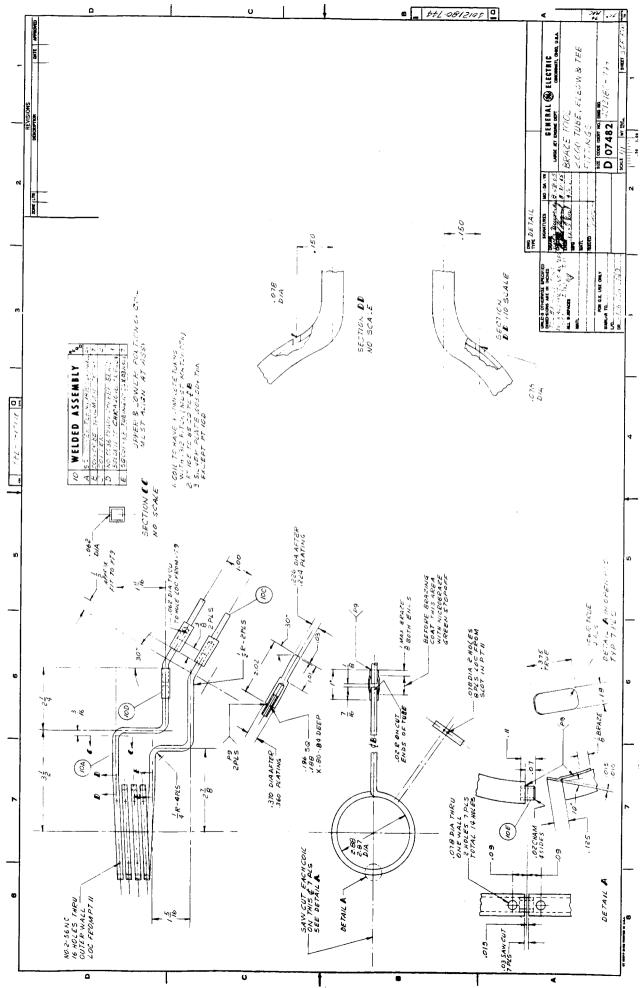












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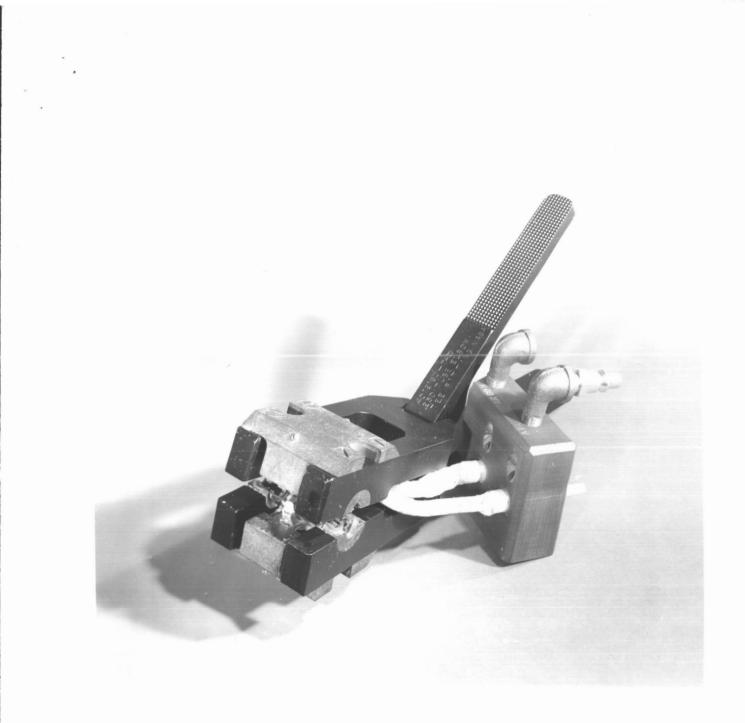


FIGURE 7 1/4" BRAZE TCOL FOR ELBOW & TEE FITTINGS

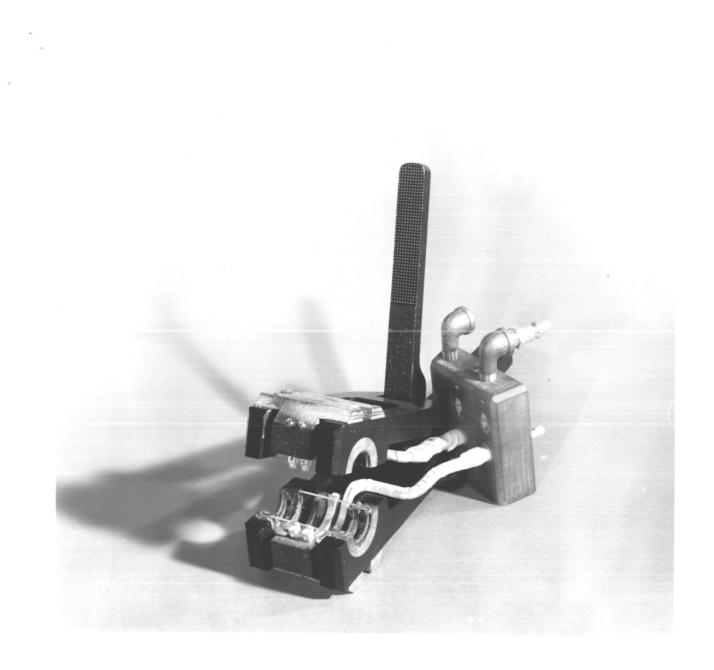


FIGURE 8

3/4" BRAZE TOOL FOR ELBOW & TEE FITTINGS

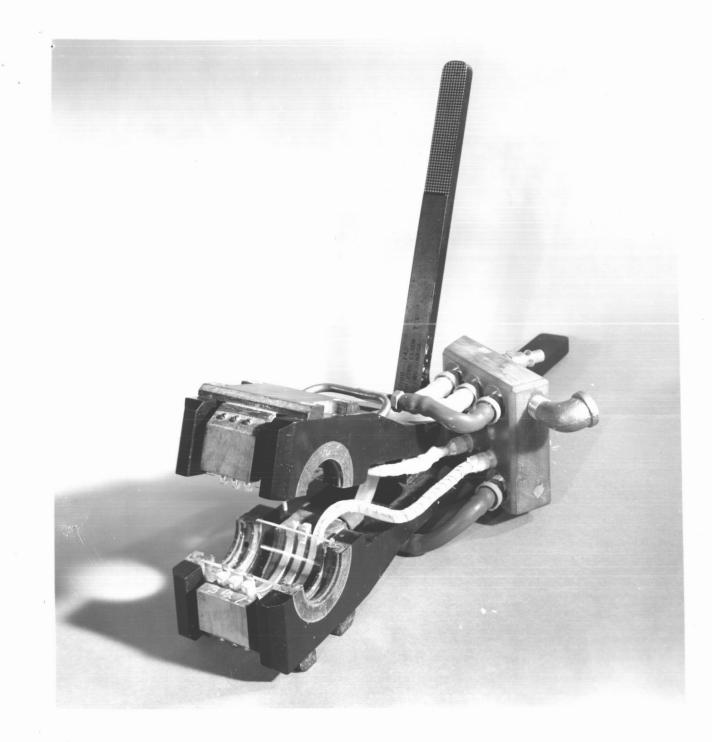


FIGURE 9 1 1/4" BRAZE TOOL FOR ELBOW & TEE FITTINGS

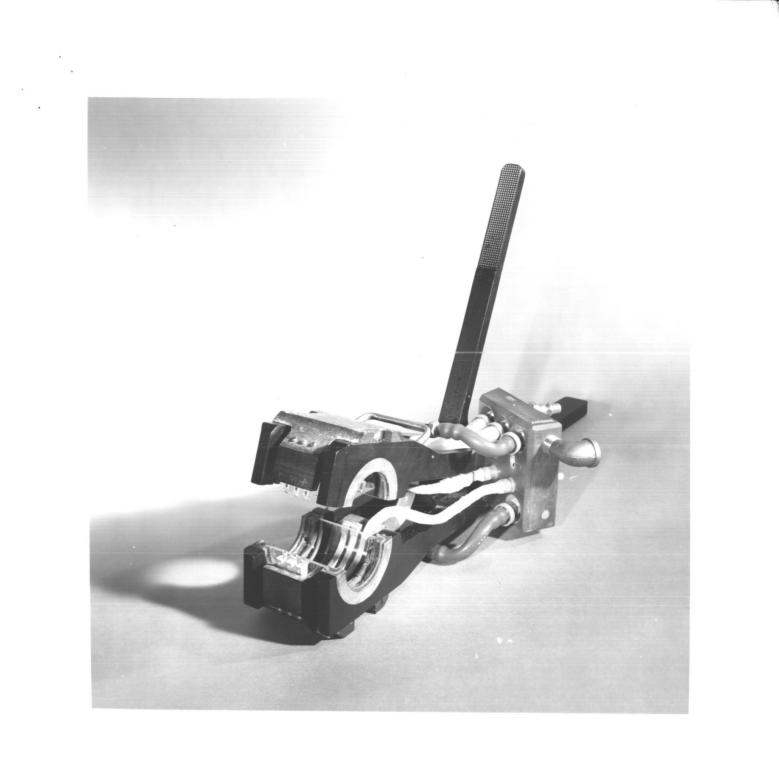


FIGURE 10 1 1/2" BRAZE TOOL FOR ELBOW & TEE FITTINGS MOL761

## FIGURE 11 2" BRAZE TCOL FOR ELBOW & TEE FITTINGS



FIGURE 12

CARRYING CASE

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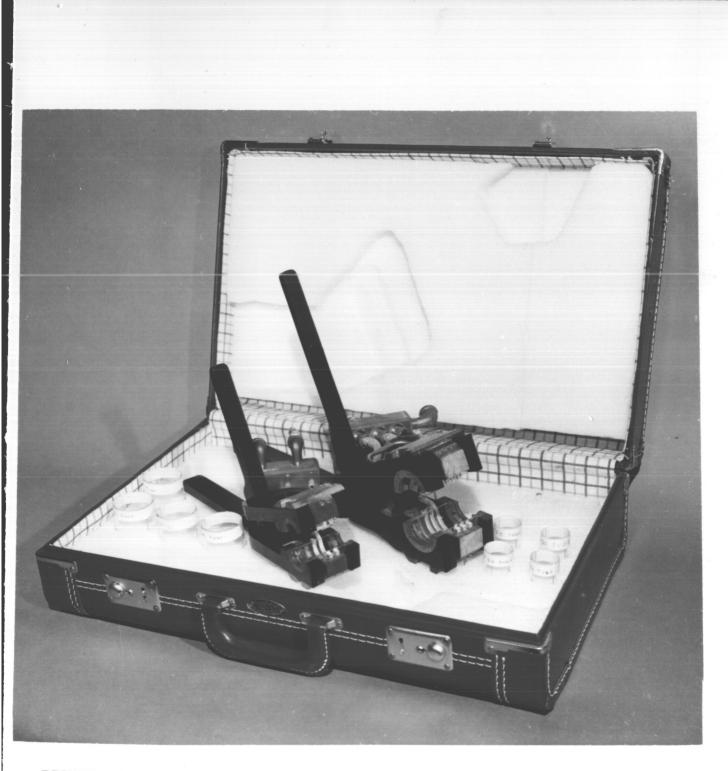


FIGURE 12A

CARRYING CASE

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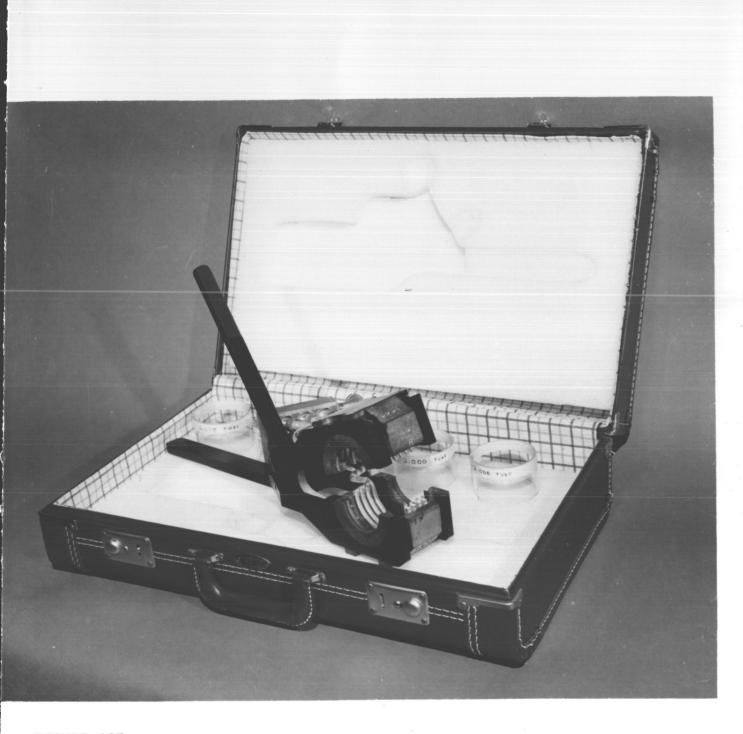


FIGURE 12B

CARRYING CASE

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### TABLE III. Split Coil Data For Straight Connectors

Tube Size	Coil I.D.	<u>Coil Turns</u>	<u>Coil Pitch</u>
.250	.60 .59	3	.286
.750	1.19 1.18	4	.286
1.250	1.88 1.87	5	.375
1.500	2.12 2.11	6	.375
2.000	3.07 3.06	8	.312
2.500	3.27 3.26	8	.375

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## TABLE IV. Split Coil Data For Elbow And Tee Type Fittings

Tube Size	<u>Coil I.D.</u>	<u>Coil Turns</u>	<u>Coil Pitch</u>
.250	.60 .59	1	.375
.750	1.19 1.18	2	.3125
1.250	1.88 1.87	3	.3125
1.500	2.12 2.11	3	.3125
2.000	2.88 2.87	4	.3125

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### ✓ Debraze Tool

The fitting must first be cut in half, then the debrazing tool is used to remove the remaining half coupling, elbow or tee type fitting. The removal of fittings are necessary when lines must be disconnected to replace a braze fitting, filters, or replace sections of tubing.

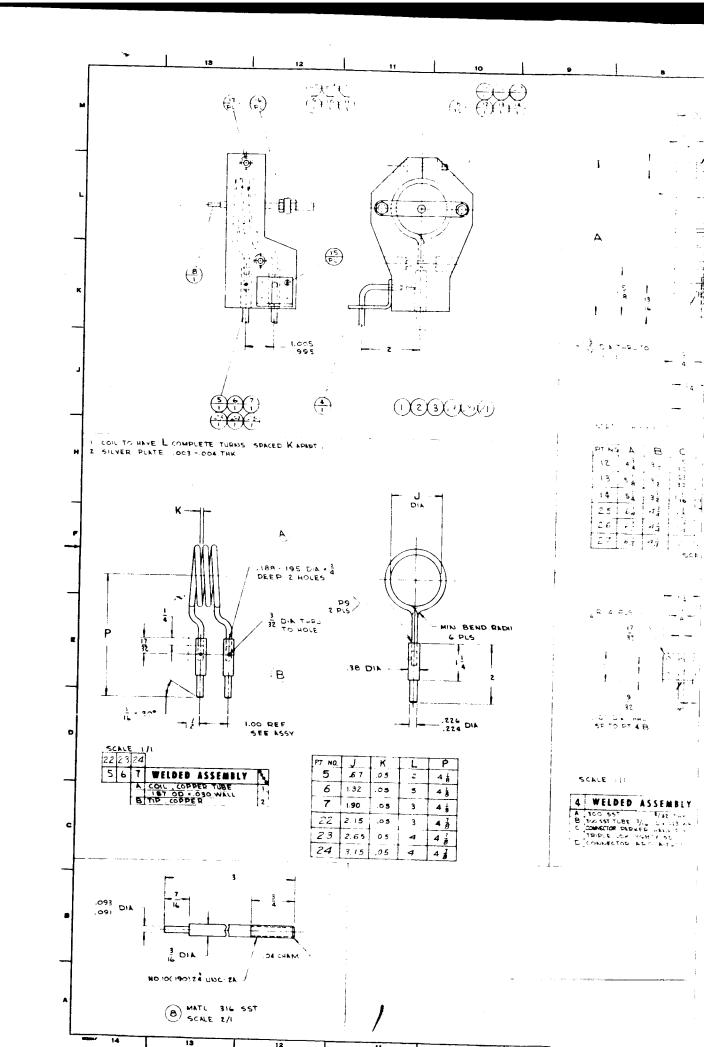
The debrazing fixture, Figure 13 is a semi-automatic tool which works in conjunction with its corresponding heating coil, Figure 14 and 14A. The coil itself is housed in a containing block which has guide sleeves for centering the coil to the fitting, an argon gas outlet that inserts into the tube and acts to catch the hot parted fitting when removed. The continuous wound heating coil for the debrazing fixture is used to remelt the braze alloy. This coil is made from soft copper tubing .187 x 030 wall with sufficient turns to overlap the brazed area by .070 minimum and the I.D. of the coil is at least .120 greater than the O.D. of the fitting.

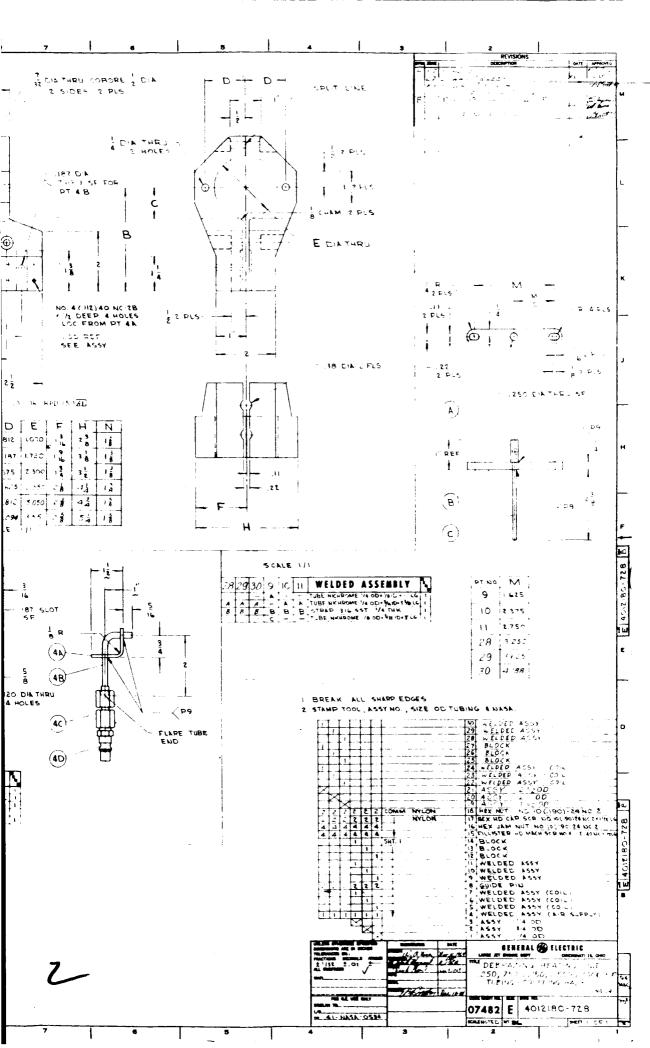
The other half of the debrazing fixture is air operated. An adjustable hardener split block sets next to the fitting to be removed. The extension to this block has tefelon sleeves to prevent binding when this is moved forward by the striking arm. The tool itself is held to the tubing by an adjustable split brass sleeve. Prints 4012180-728 detail all heating units and prints, 4012180-731 thru 736 detail the debrazing fixture.

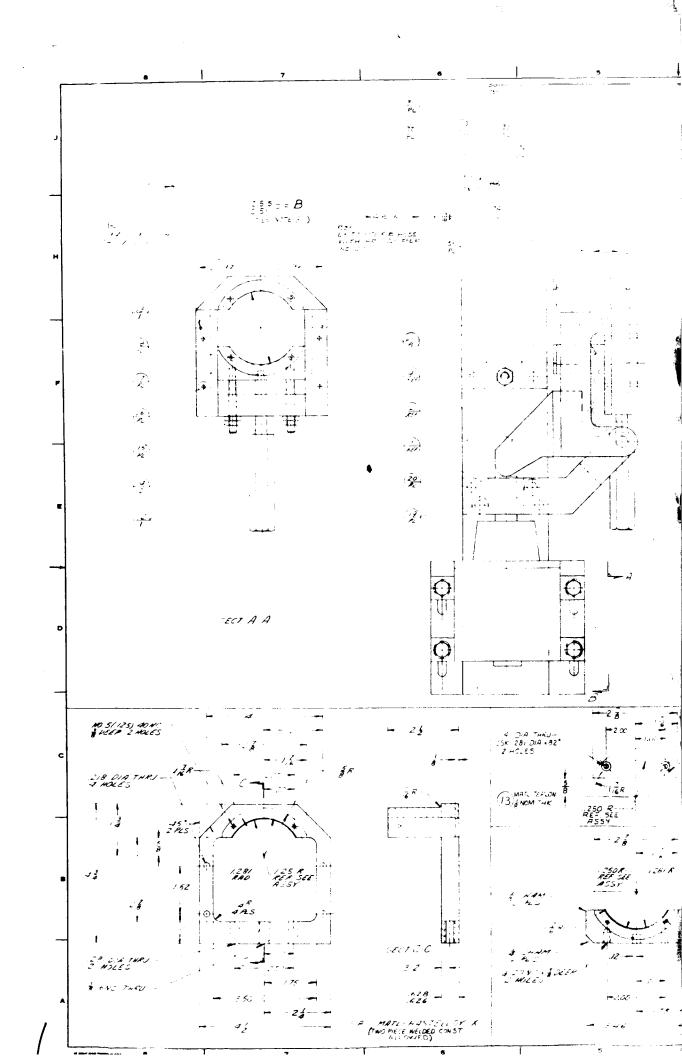
#### Sizing Tools

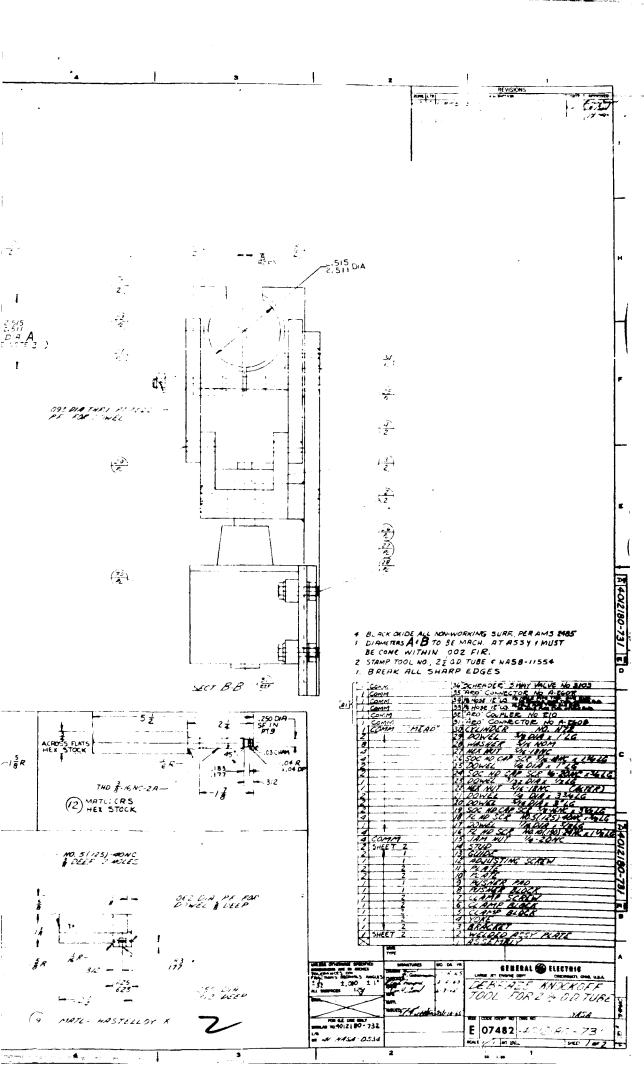
There are two methods of sizing tubing - expansion and reduction. Both methods were investigated during the initial braze program and reduction was chosen because closer tolerances could be achieved and it was a much simpler operation. Also, a more practical and compact tool could be designed for the reduction method. The tools designed, Figure 15, attach to a two-directional motor mounted on a table. Each sizing tool is interchangeable with the two-directional motor. Every sizing tool has a matching clamping block which slides on parallel bars and holds the tubing stationary during the sizing operation. Figures 16, 16A and 16B show three different sizing housings and matching clamping blocks. For details see print 4012180-729.

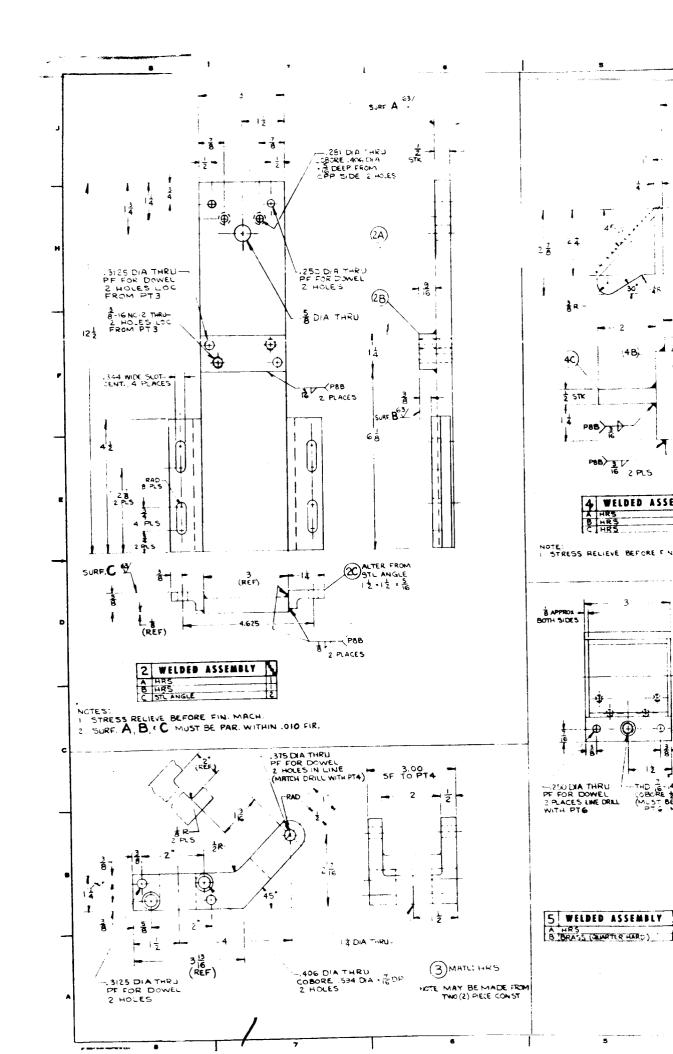
The design of the sizing tools for 1/4", 3/4", 1 1/4", 1 1/2" are all the same. Problems were encountered with the 2" and the 2 1/2" sizing tool, mainly a flaring condition on the end of the tube sized. Design of 2" and 2 1/2" sizing tool was altered to correct this.



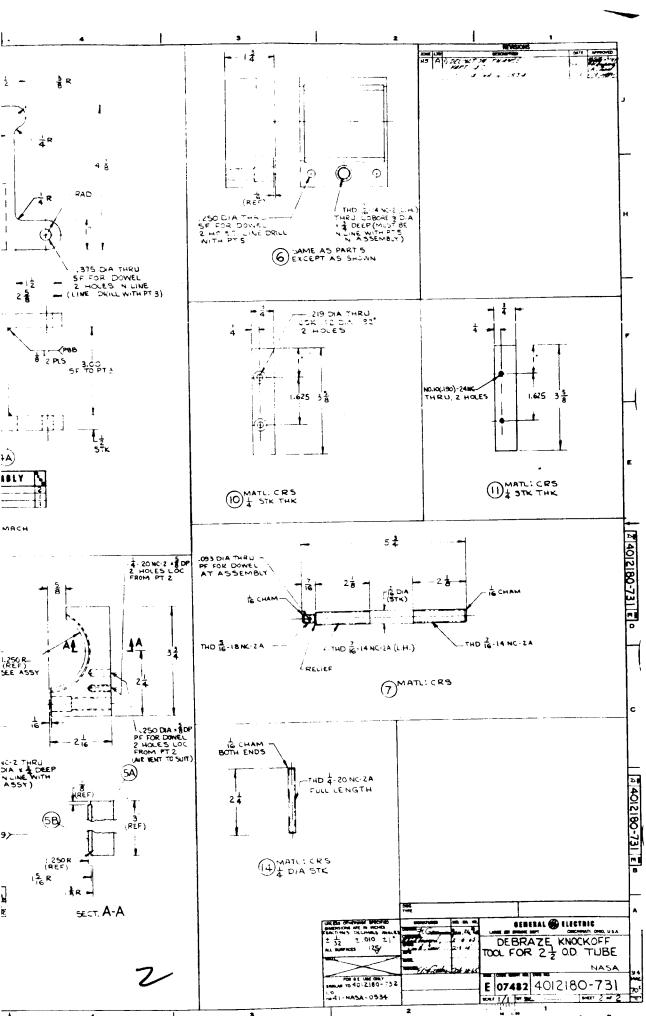




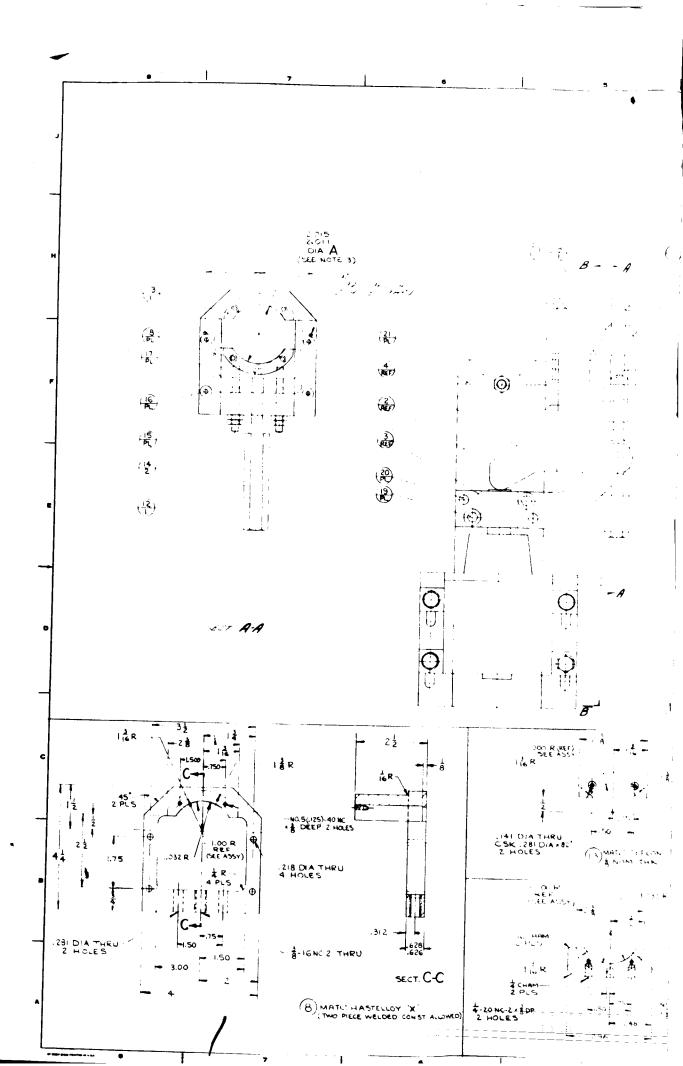


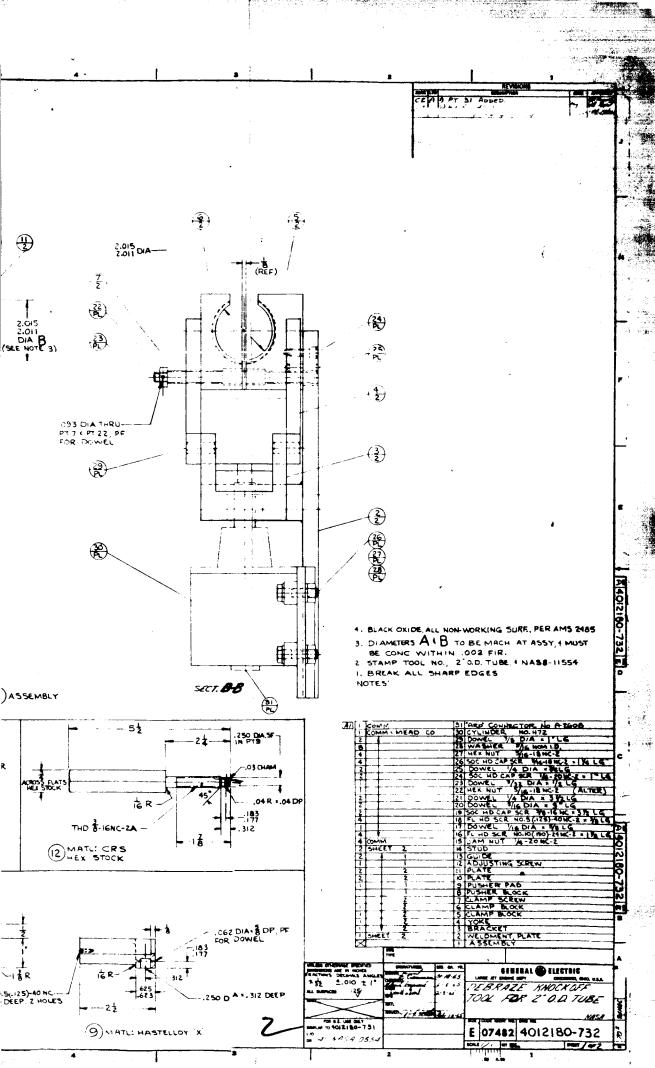


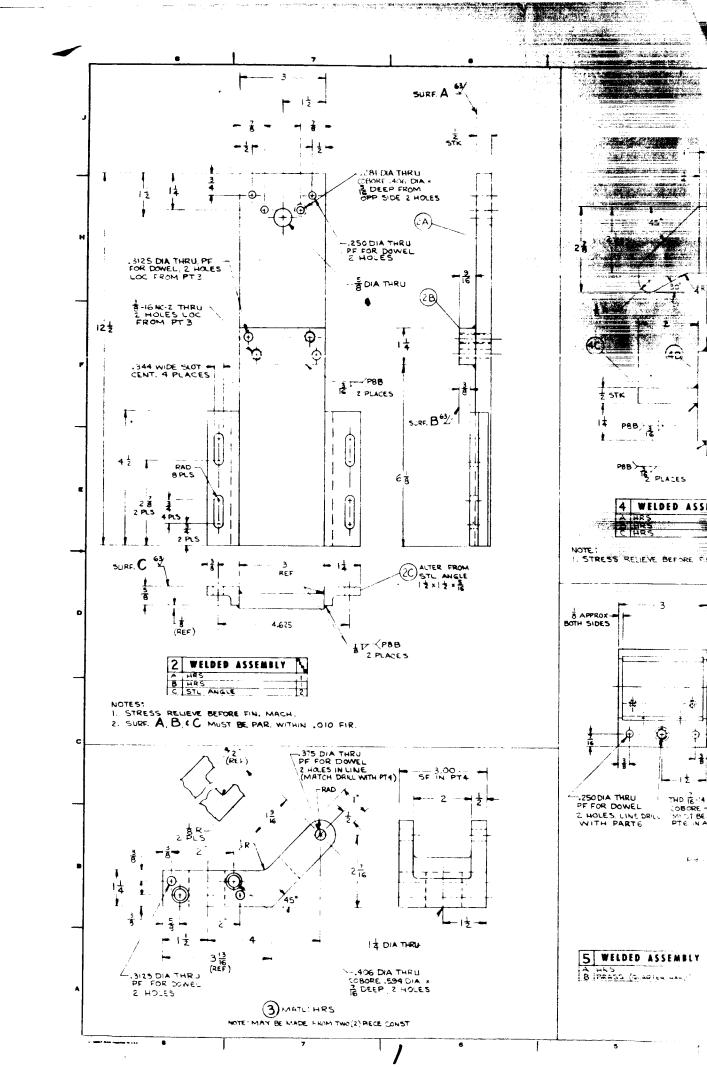
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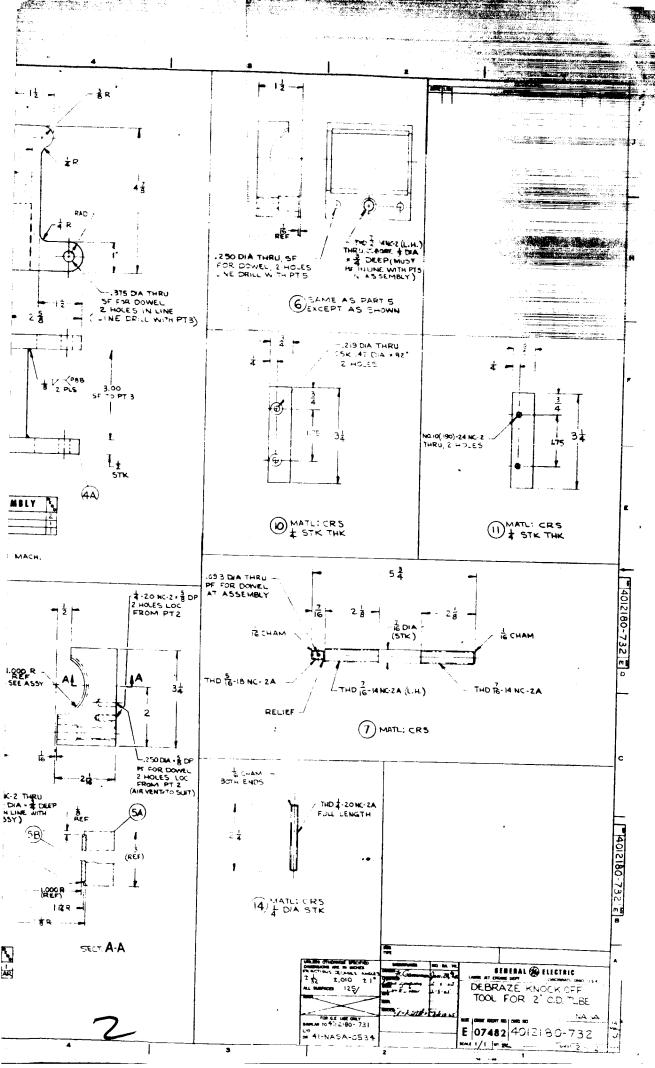


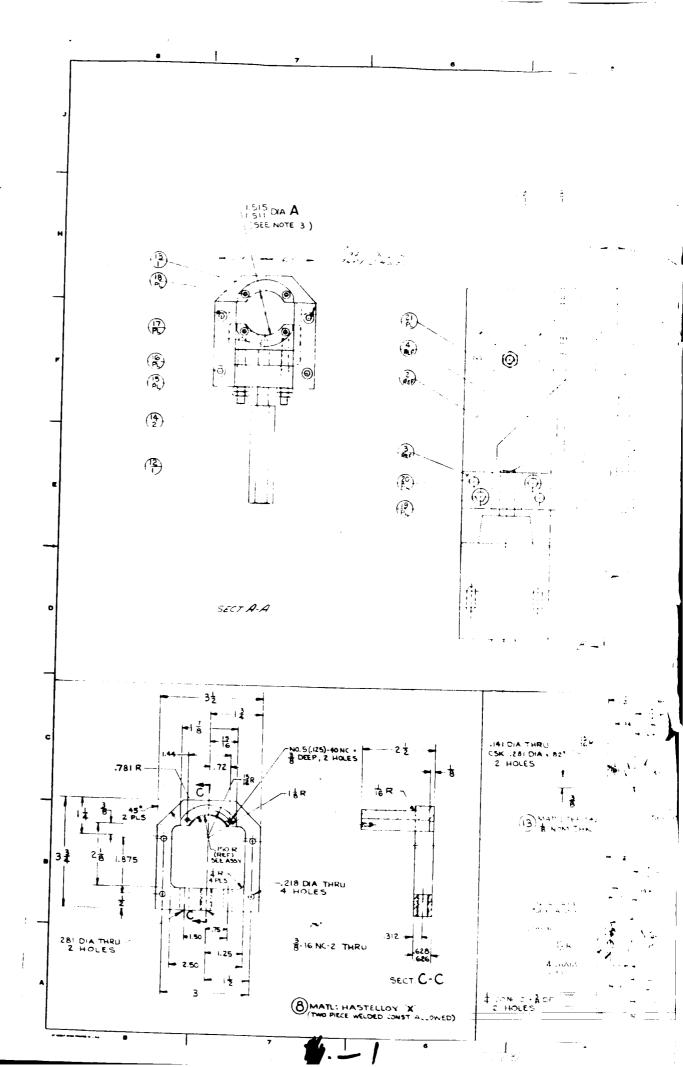
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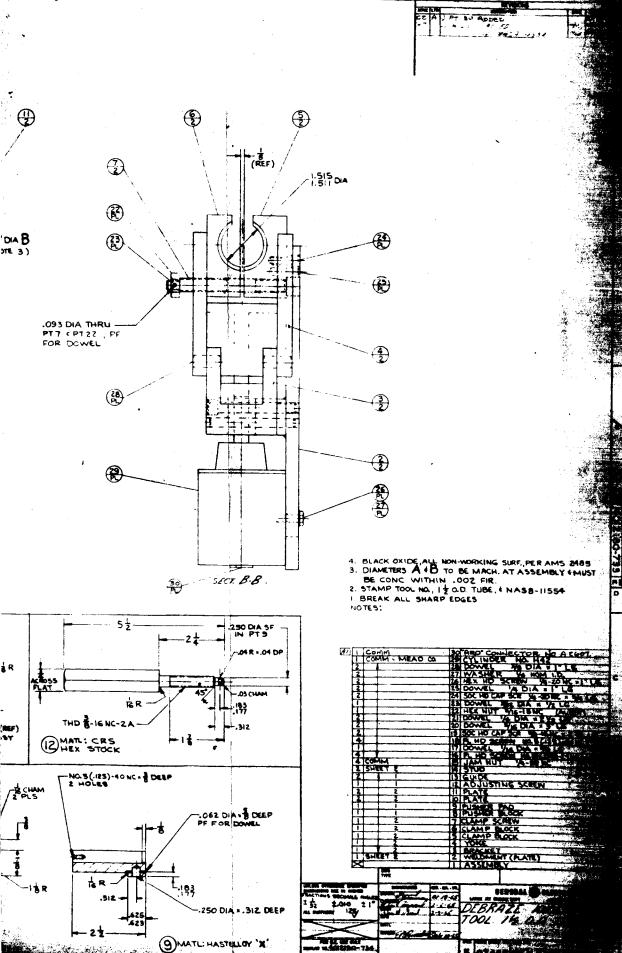


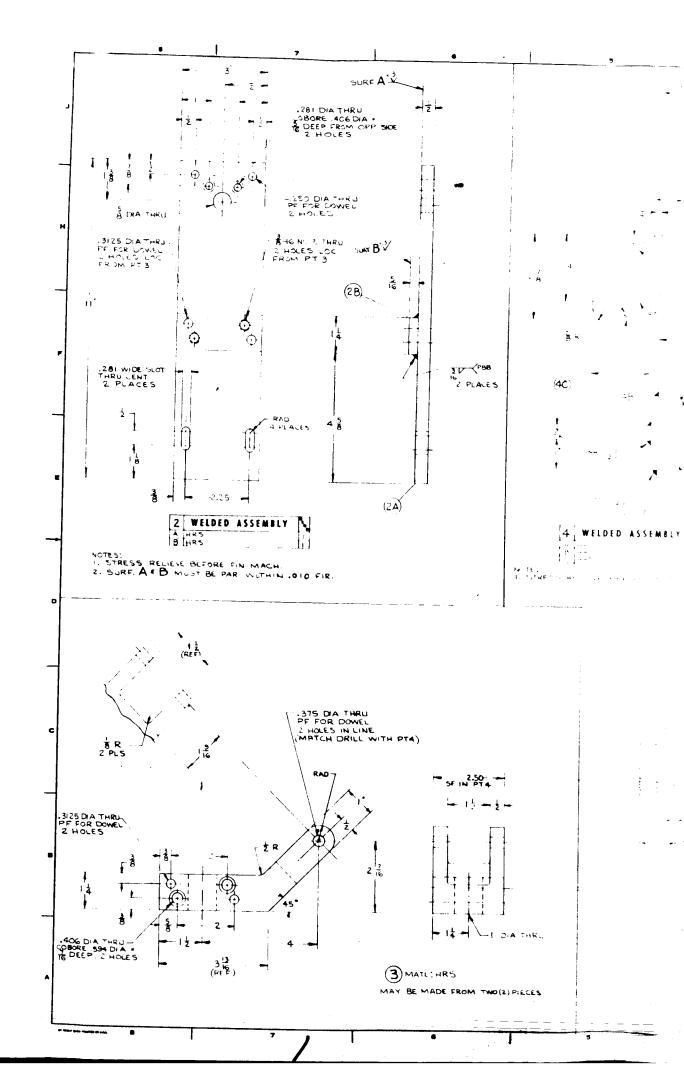


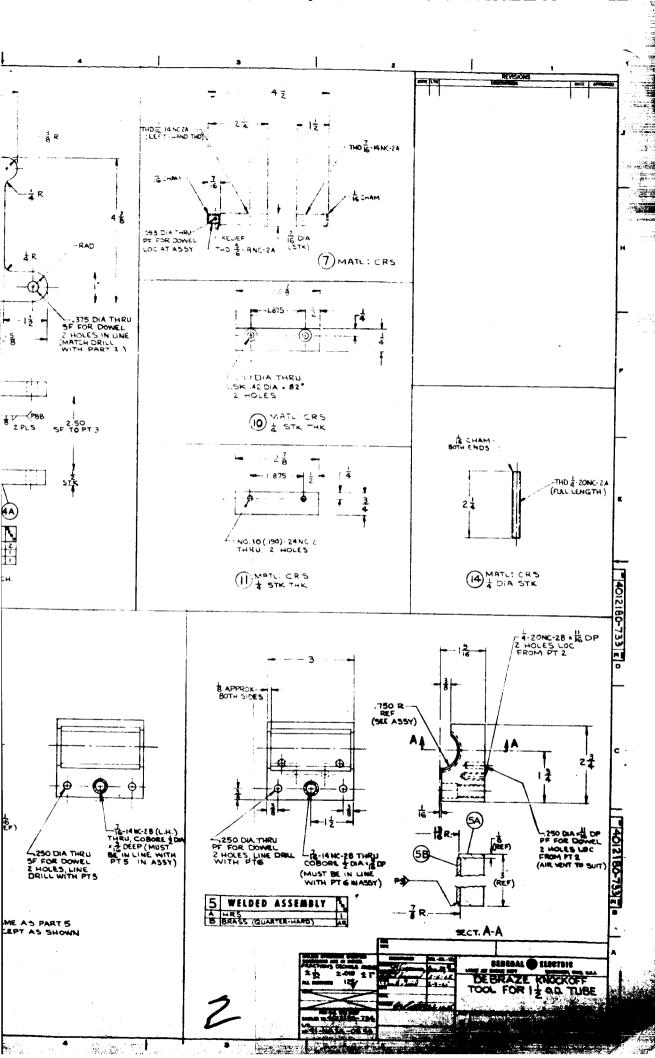


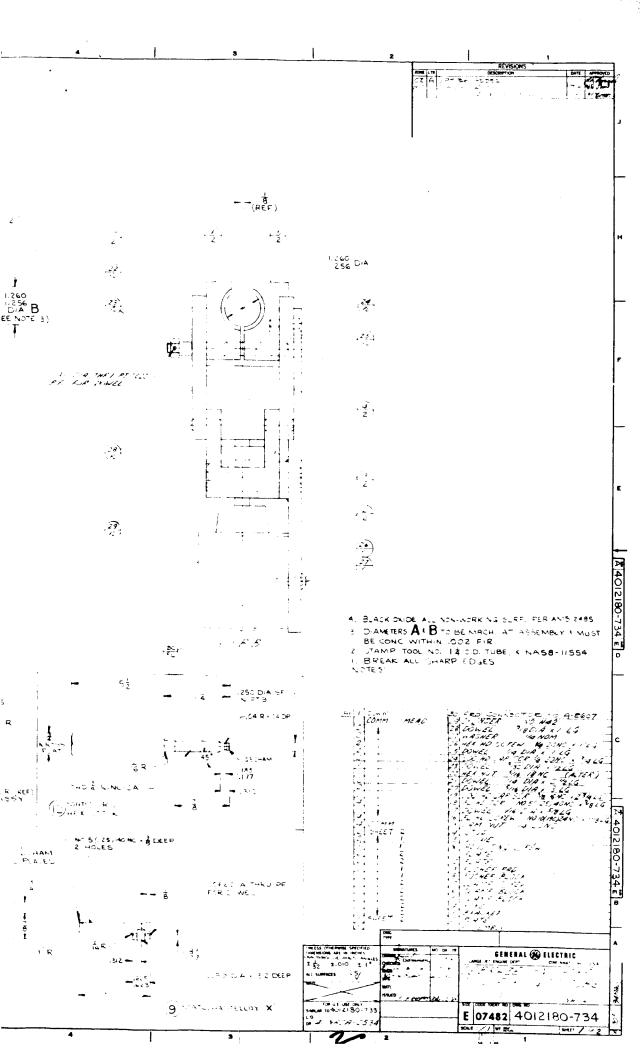


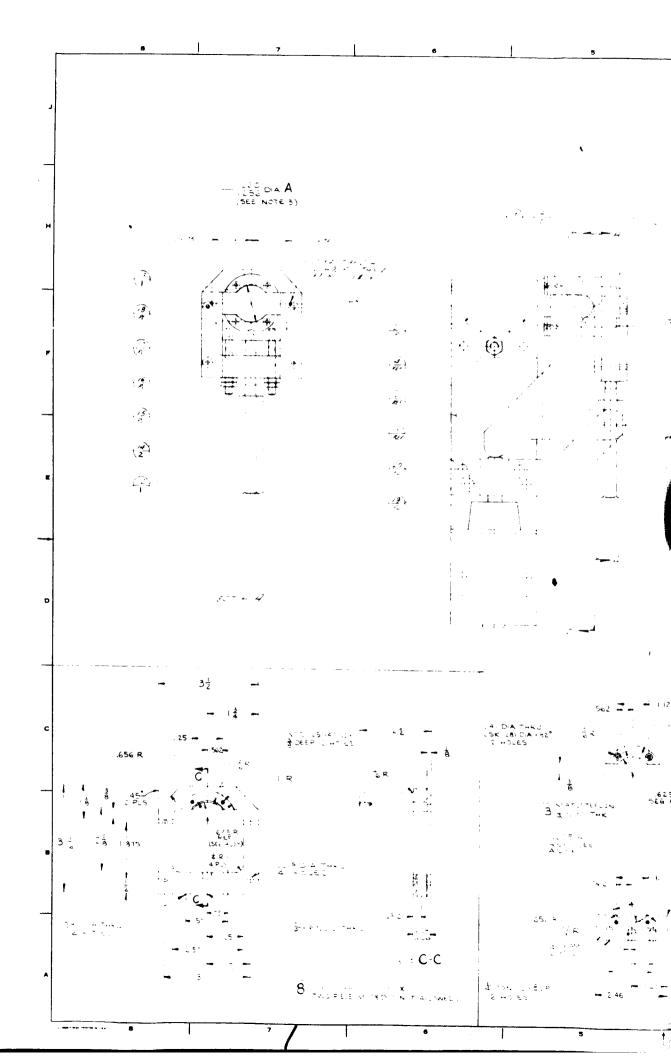
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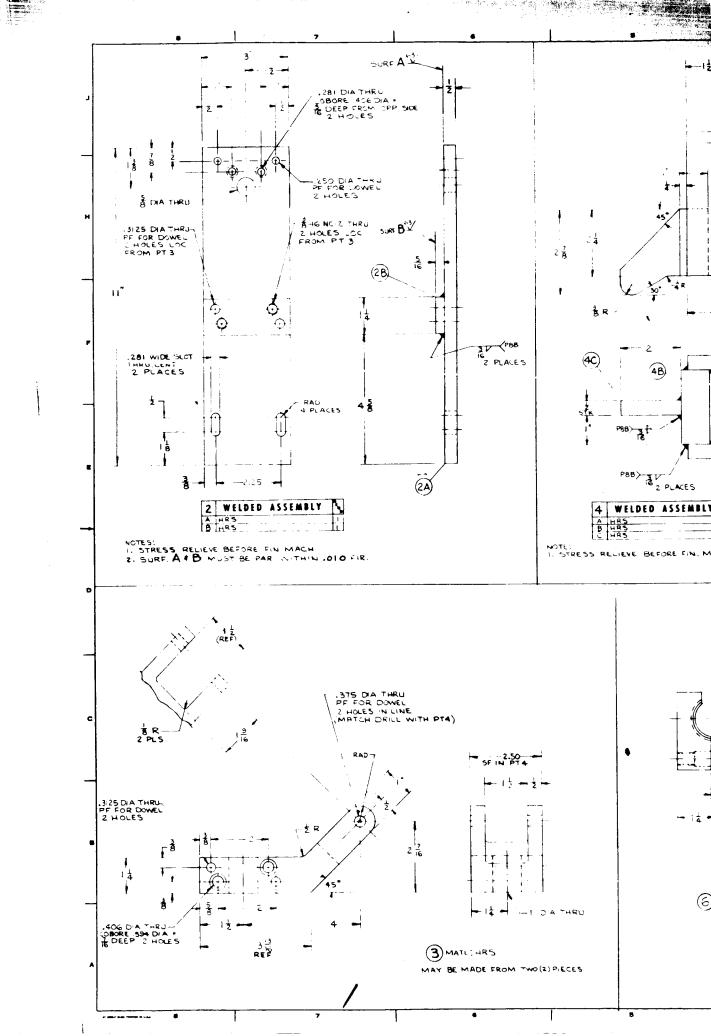




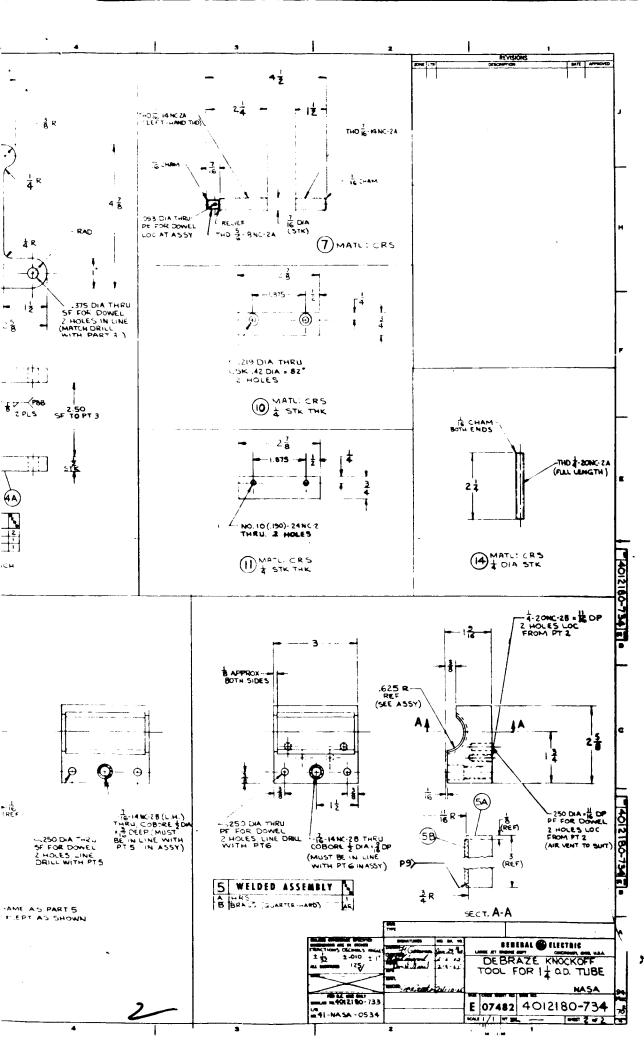


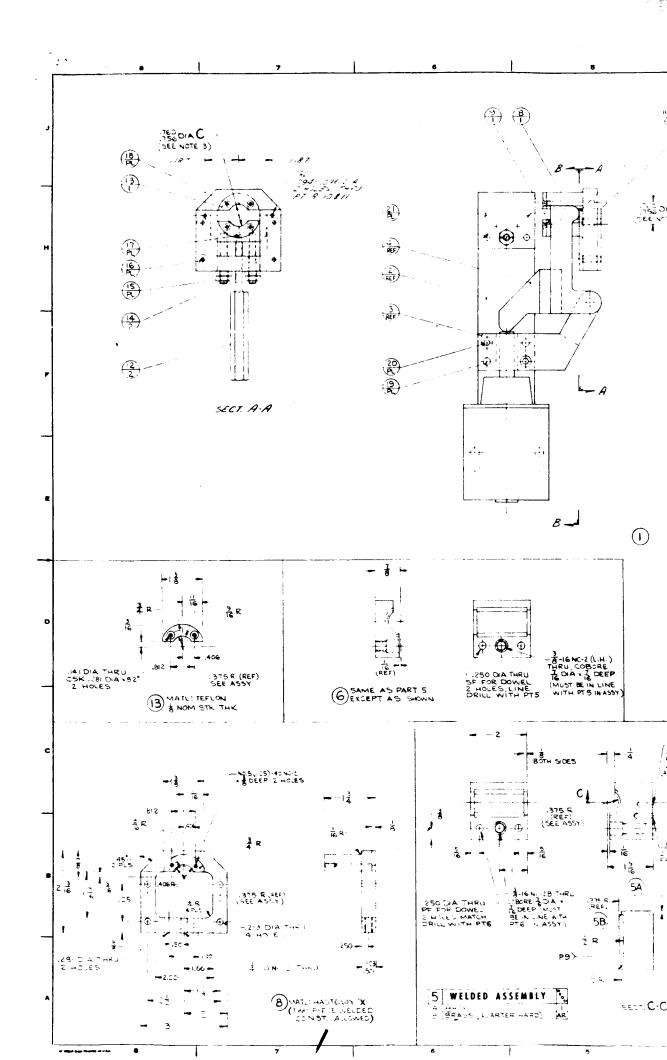


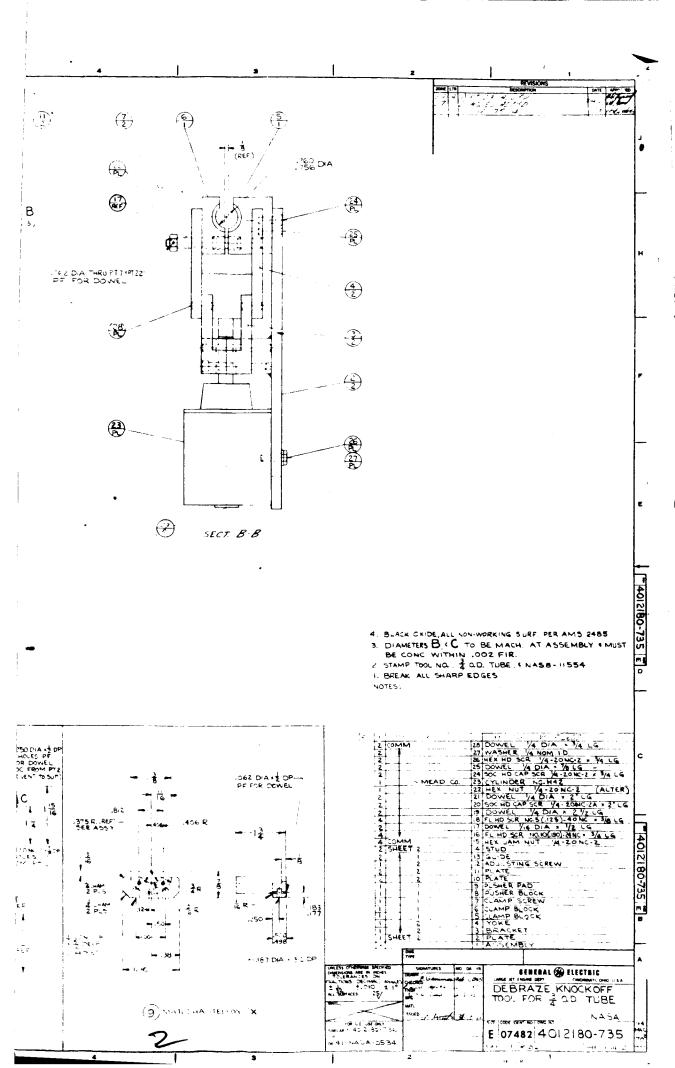


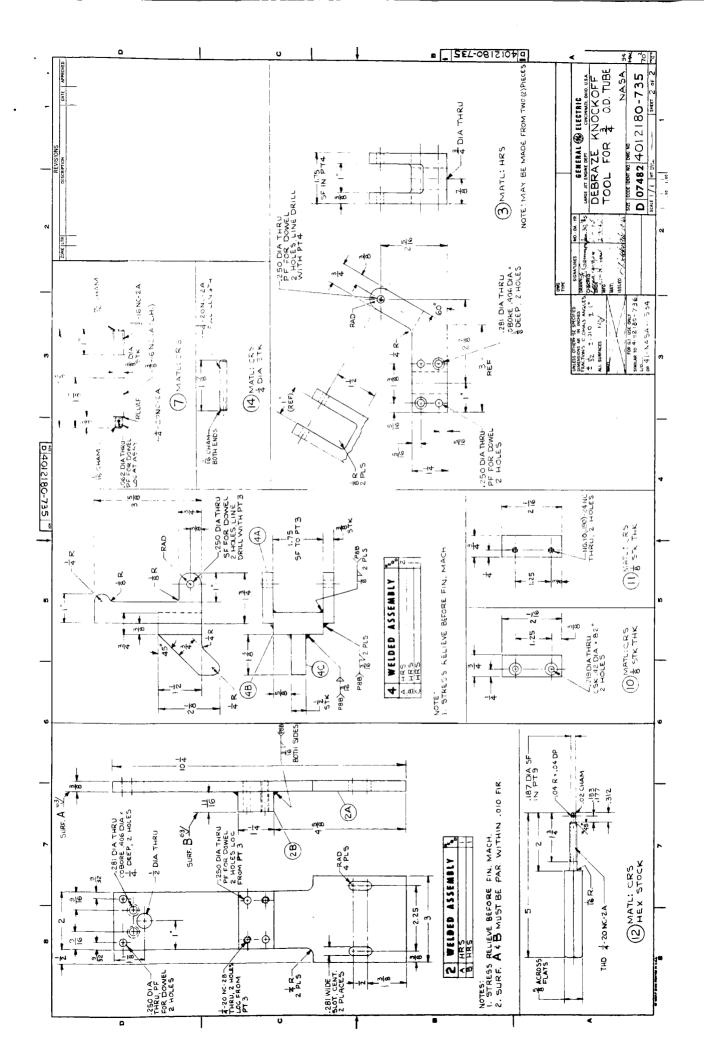


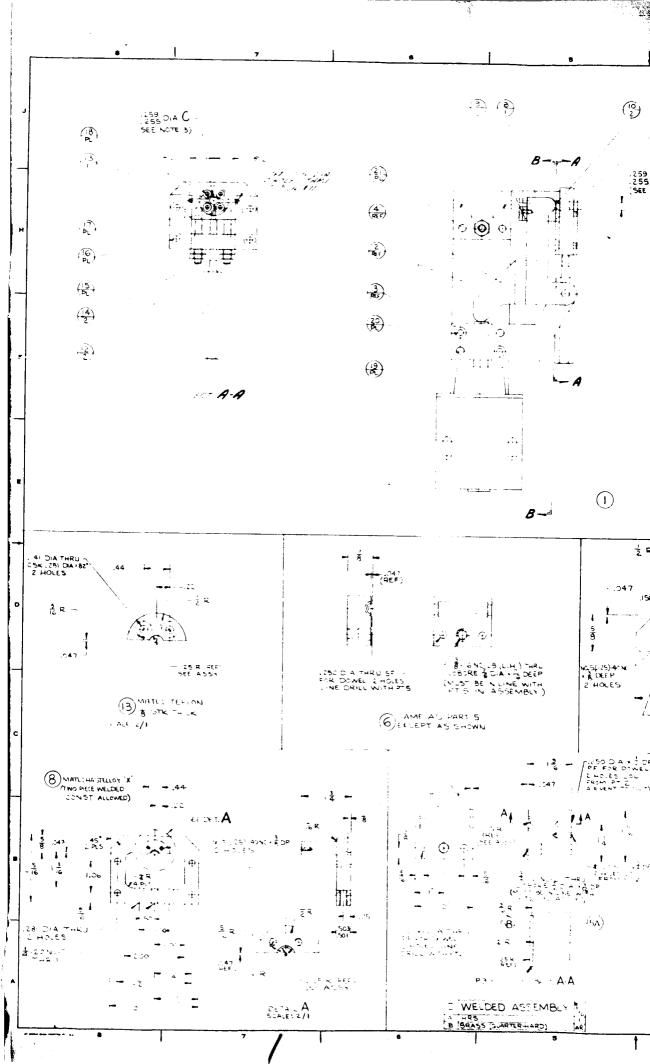
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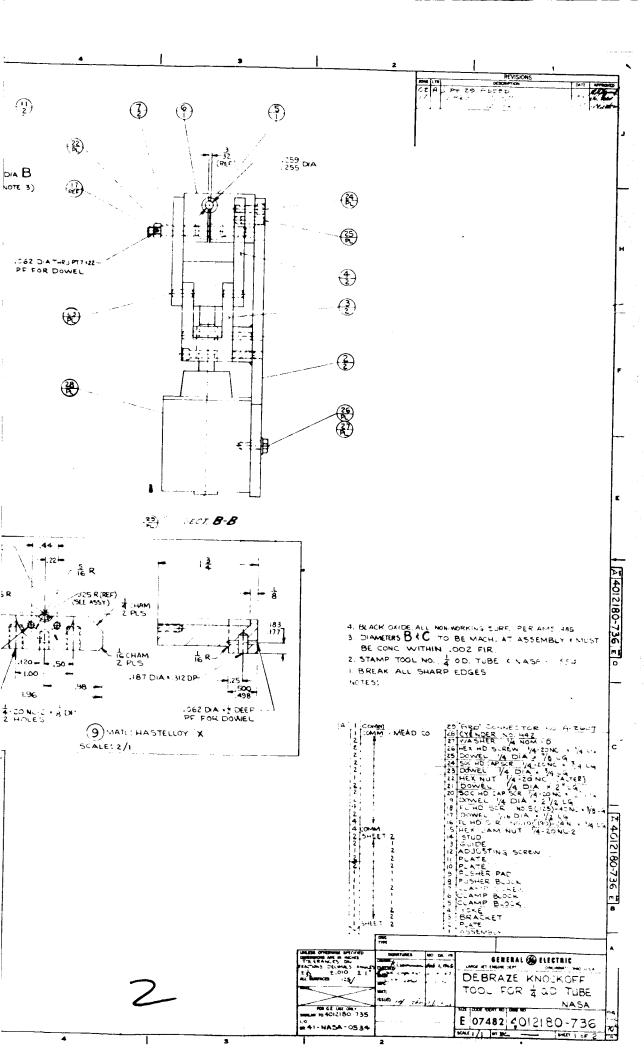


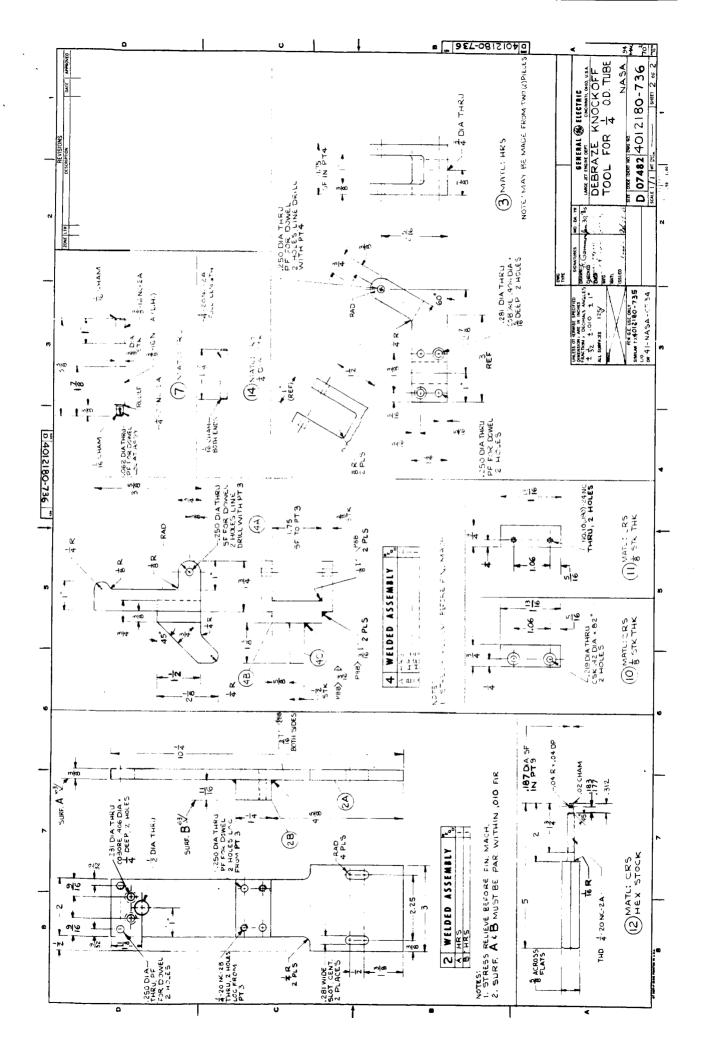


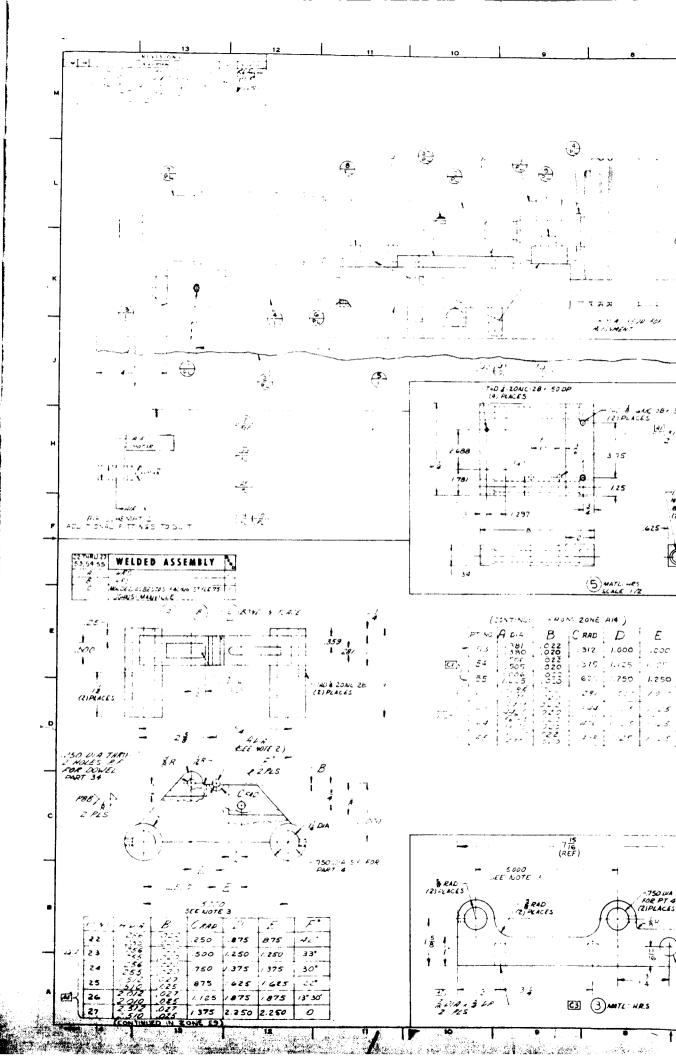


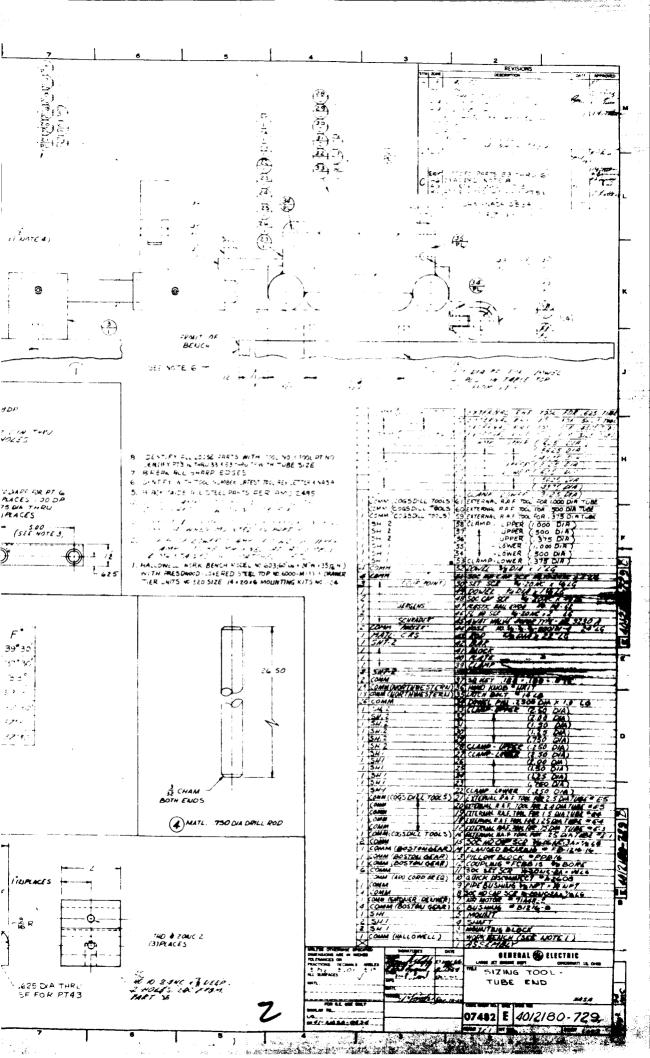


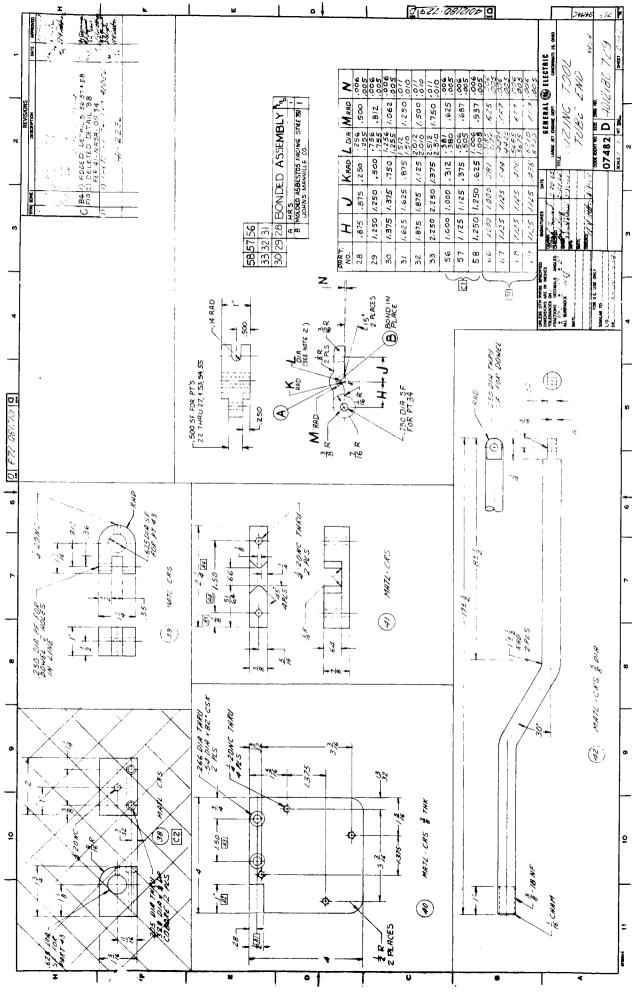








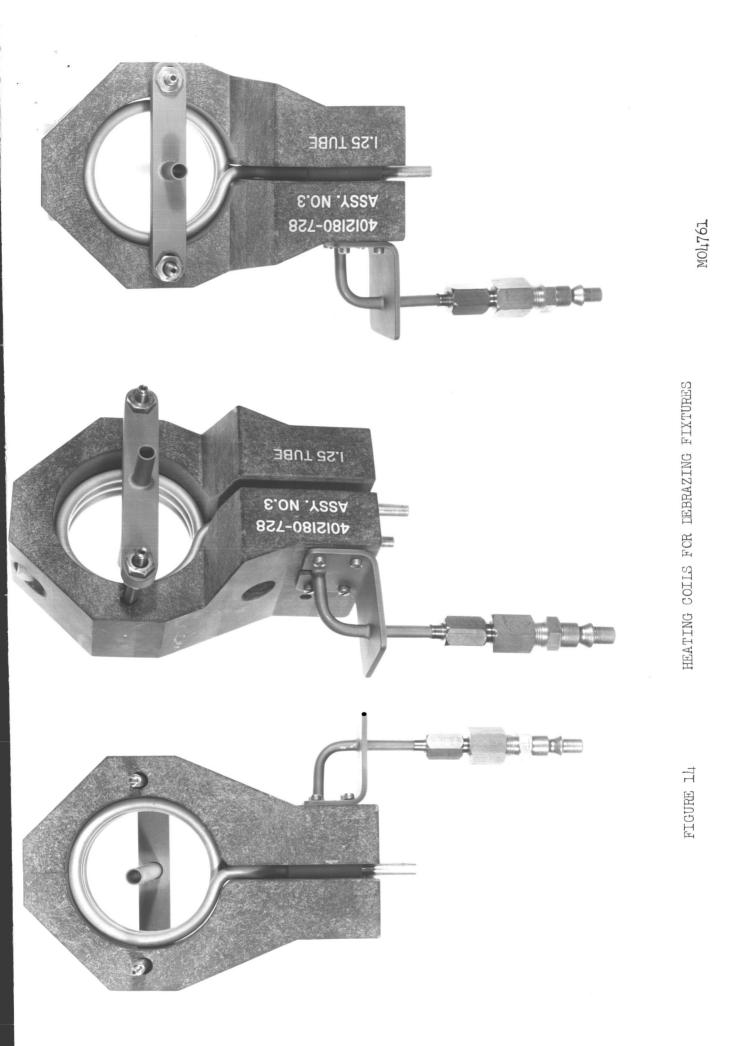


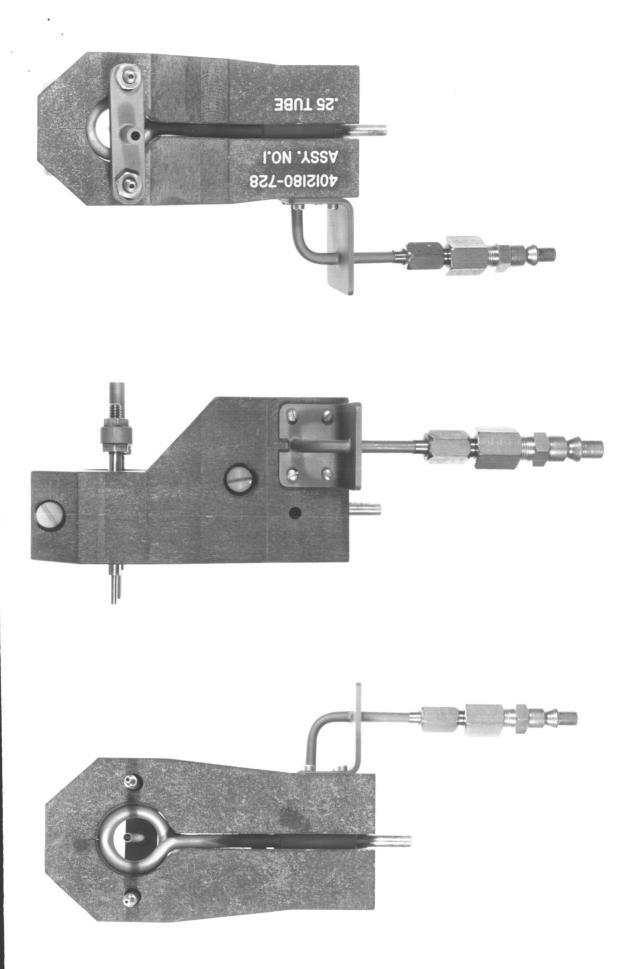


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HEATING COILS FOR DEBRAZING FIXTURES

FIGURE 14A



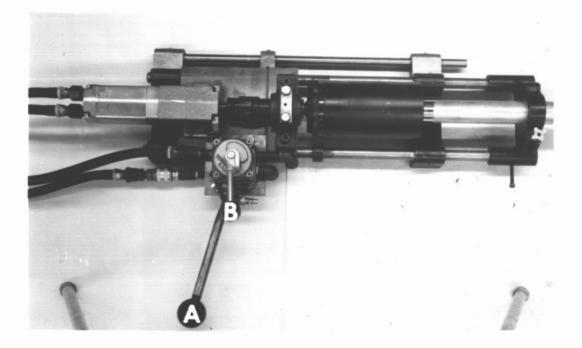


FIGURE 15

TOP & SIDE VIEW OF SIZING TCOL (A-Lever Arm B-Air Reversing Switch)



# FIGURE 16 1/4" SIZING HOUSING & CLAMPING BLOCK



FIGURE 16A

# 3/4" SIZING HOUSING & CLAMPING BLOCK



FIGURE 16B 1 1/4" SIZING HOUSING & CLAMPING BLOCK m04761

# GENERAL ELECTRIC COMPANY TECHNICAL INFORMATION SERIES NO. R66FPD47

### Sizing Tools (Cont'd)

The sizing of all tubing is accomplished by roll forgings (or forming). When the sizing tools are rotated at relatively high speeds, precision ground and hardened rolls bear on a cammed arbor; the rolls spin, rise and fall rapidly compressing the tube surface. These tools are adjustable in .0001 increments with a range from a nominal tube size dimension to  $\pm$  .005 inches.

The sizing operation procedure is as follows: Place a tube in the proper holder and tighten the clamp. Activate the motor. Turn to the forward position, which operates the sizing tool in a clockwise motion. The sizing tool is brought forward by means of the handle attached, while it is revolving. After initial engagement the tube will feed itself into the sizing tool. Upon completion of sizing, reverse the sizing tool rotation direction by reversing the air valve. The motor will turn the sizing tool counter clockwise immediately freeing the tubing from the hardened rolls. To disengage, pull the sizing tool back to its original position.

#### Coupling Elbow And Tee Designs

The design of the coupling, elbow, and tee fittings has evolved primarily from the fitting design used on the J93 Engine which powers the XB-70 aircraft. Sketch I and II are initial designs of a coupling first developed for the J93 fluid system. Drawing 871C234, illustrates the present coupling design for the J93 fluid system. Drawing 4012180-638 is the design of couplings used for NASA applications. The latter drawing is exactly the same as drawing 871C234 except for larger size fittings.

+.0010

The I.D. of the coupling has a critical dimension of -.0000 to control dimensional gaps with sized tubing. This controlled I.D. dimension is maintained on all fitting designs. Sketch I has spacers at each end of the coupling with a crown dimension of  $020 \times 030$ . these spacers are used for alignment. Sketch II shows the same basic design, only the spacers have been replaced with projections thru  $120^{\circ}$  apart. These projections were also used for alignment. Drawings 871C234 and 4012180-638 show the absence of spacers or projections. Later, it was found that with controlled I.D. dimensions on the coupling and controlled tubing, the brazing alloy acted as the alignment means during braze alloy flow. The recessed groove in each half of the coupling allows for

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#### SKETCH 1

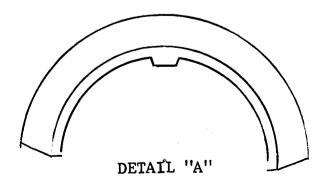
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SEE DETAIL "A"

**3 PROJECTIONS THRU** 

120° APART .040 - .080 WIDE

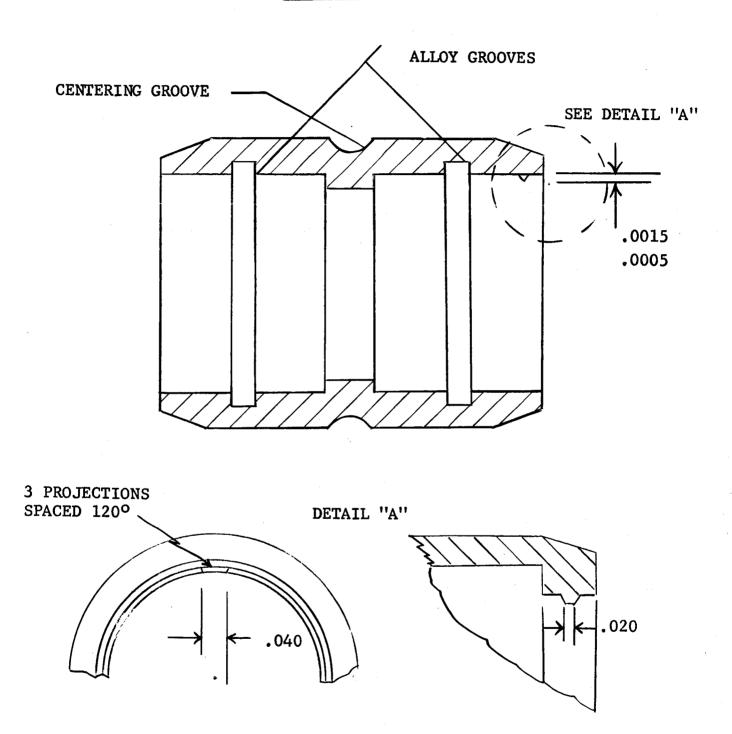


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**NO.** R66FPD47

# SKETCH 2



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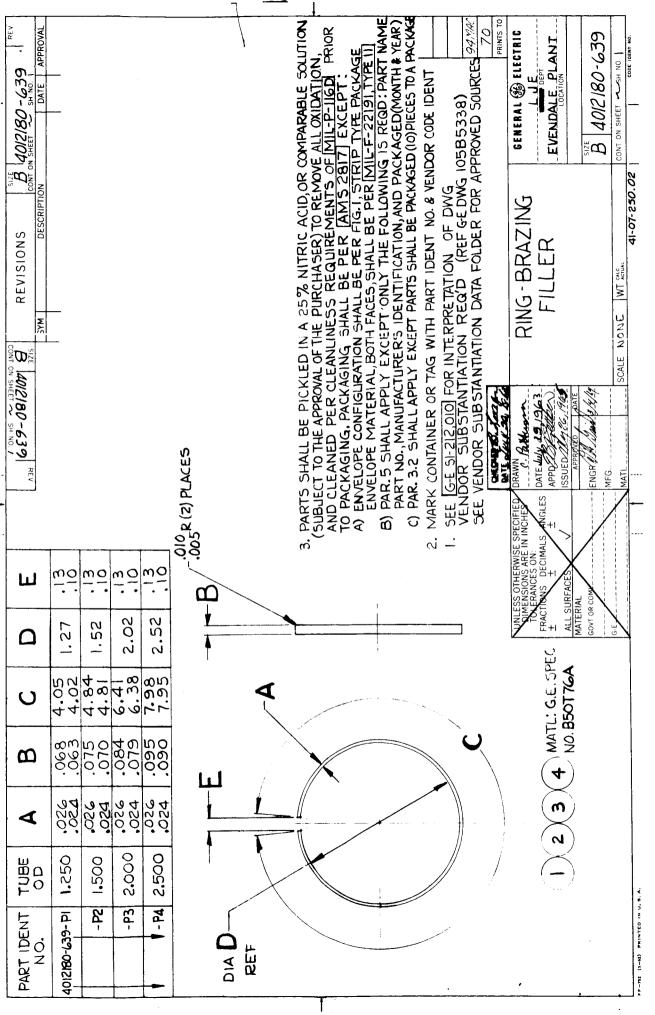
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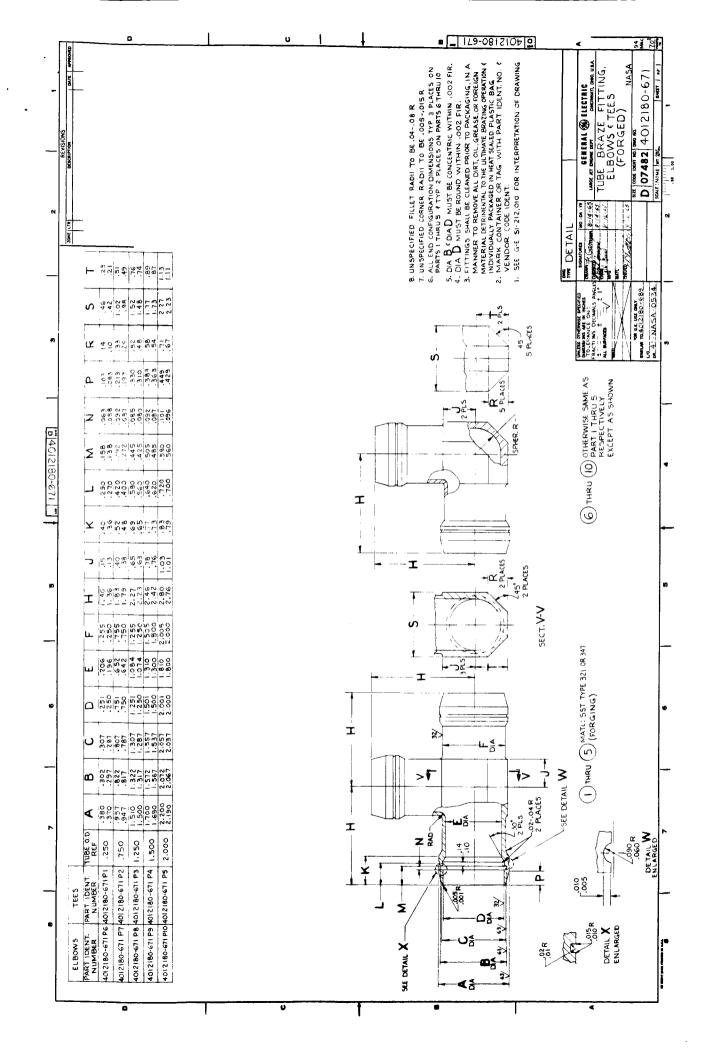
## Coupling Elbow And Tee Designs (Cont'd)

rectangular snap rings of braze alloy (print 4012180-639). Preplacing the alloy insures soundly brazed coupling, when the alloy has flowed out and formed a continuous fillet around the periphery of the coupling. If the alloy is preplaced externally there is no assurance that the alloy has flowed into the coupling joint. The shallow centering trough on the outside of the coupling is for parting purposes when it becomes desirable to disassemble. This coupling design is reliable and economical to manufacture compared to the other designs. Print 4012180-638 details production couplings.

Elbow and tee fittings were also evolved from the basic design of the J93 fluid system coupling. Both the elbow and the tee fittings have a internal shoulder to control insertion depth, shown as dimension "L" on print 4012180-671. The area aft of the internal shoulder on the 0.D. of the fitting is used as a sealing surface for the braze tool. There is also a shallow trough on these fittings for parting purposes.

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#### **NO.** R66FPD47

#### FEASIBILITY STUDY TO DETERMINE THE EFFECTS OF BRAZ-ING HEAVY WALL TUBING UTILIZING A HIGH FRE-QUENCY SOURCE INDUCTION GENERATOR

The purpose of this study was to determine if the induction braze tools, the high frequency induction source and related equipment specified for brazing the tubing of the NASA low pressure system (Table V) can be utilized for brazing tubing of wall thicknesses required for the NASA high pressure system (Table VI).

#### Conditions Of Test

Materials

Tubing A <u>Size</u>	Wall Thickness	Designat _AMS_	ion SAE
.250	0.026	5570G and 5571B	30321 and 50347
.750	0.075	5570G and 557IB	30321 and 30347
1.250	0.122	5570G and 5571B	30321 and 30347
1.500	0.113	5570G and 557IB	30321 and 30347
2.000	0.151	5570G and 557IB	30321 a <b>n</b> d 30347
2.500	0.188	5570G and 557IB	30321 and 30347

- B. Braze Alloy Gold 82% Nickel 18% in round rings of rectangular wire.
- C. Purge Gas High Purity Argon.
- D. Fittings 347 Stainless Steel straight couplings elbow and tees provided with an internal braze alloy groove. Drawings 4012180-638 and 4012180-629.

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#### TABLE V

# Low And High Pressure Systems

	Pressure Sys	stem Wall Thickness	
Tube 0.D.	Low	High	Diffuser
.250	.020	.026	.006
.750	.049	.075	.026
1.250	.083	.122	.039
1.500	.095	:113	.018
2.000	.095	.151	.056
2.500	.120	.188	.068

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# GENERAL ELECTRIC COMPANY TECHNICAL INFORMATION SERIES NO. R66FPD47

# TABLE VI

## POWER TIME CYCLES

Low	7 Pressure	Tubing	<u>High Pressure Tubing</u>					
Size	Power <u>Setting</u>	Time <u>Seconds</u>	Size	Power <u>Setting</u>	Time <u>Seconds</u>			
.250	12	20	.250	12	24			
.750	13	35	.750	•4	60			
1.250	15	60	1.250	18	120			
1.500	15	60	1.500	20	120			

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#### Fixturing

A lab. rig fixture, Figure No. 17-17A & 17B, was used for testing all sizes of tubing. This fixture is designed to provide argon protection during the brazing and cooling operations.

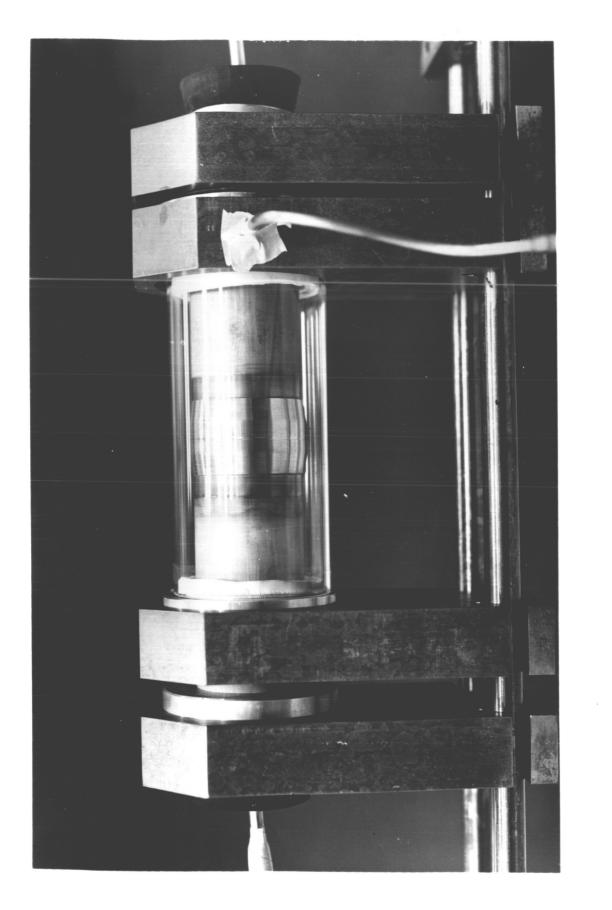
#### <u>Tests</u>

Sample joints of heavier wall thickness tubing were induction heated in the lab. rig fixture, using the power settings and time cycles previously established for brazing the low pressure system tubing. Two chromel-alumel therocouples were used to determine the temperature of the joint being brazed. Each thermocouple was tweezer weld tacked in place on the 1.D. of the tube being brazed. One thermocouple was located at the center of the coupling, the other thermocouple was located at the end of the coupling. Samples were inspected visually for brazing alloy flow. In the event, the joint did not reach braze temperature or braze alloy flow did not occur, the power setting and/or the time was increased in small increments, until a sound braze joint was obtained.

#### Test Results

The 1/4", 3/4". 1 1/4" and 1 1/2" braze joints exhibited good flow of braze alloy around the periphery of the fittings. The power time cycles used for obtaining these results were somewhat greater than those established for the low pressure system Table V. X-ray examination of these brazed samples revealed 80 to 100% coverage. Peel testing of these same samples verified the x-ray findings. Figure 18 is a 1 1/2" peeled joint. The 2" and 2 1/2" samples exhibited poor alloy flow for all power time cycles attempted. No acceptable couplings were obtained. X-ray and peel testing indicated 40 to 50% coverage. The powertime cycle required to obtain 40-50% braze coverage for the larger samples caused over heating of the power transmission cable. One to two hours was required to cool the cable before it could be used again.

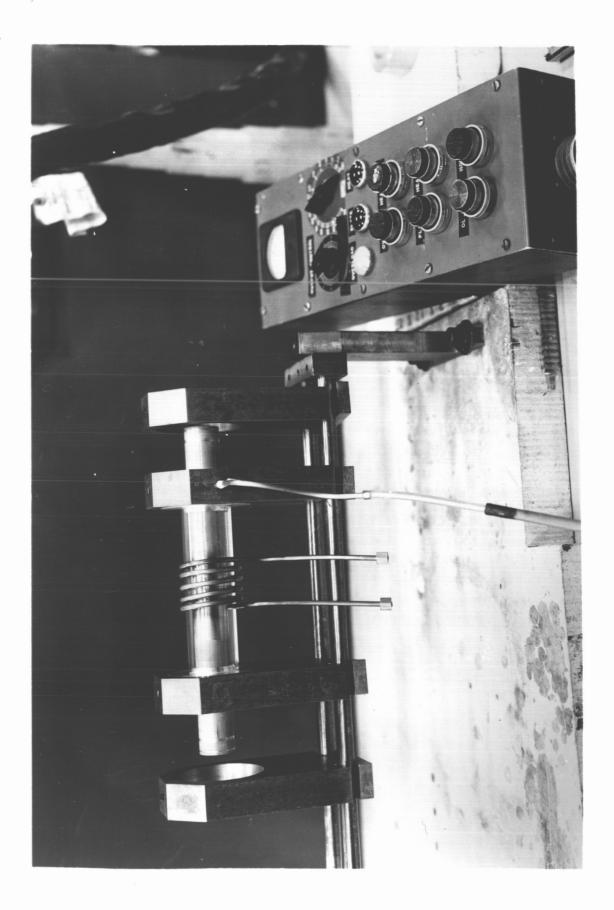
Distortion of the 2" and 2 1/2" couplings occurred during the heating cycles. Figure 19 shows a typical example. The distortion was located near the end of the coupling where the wall is tapered. It was not found at the same point on the periphery of the coupling of all the samples prepared indicating that it was not due to a hot spot during the heating cycle.



T9740M

LAB BRAZE FIXTURE

FIGURE 17



19240М

LAB BRAZE FIXTURE

FIGURE 17A



M04761

LAB BRAZE FIXTURE

FIGURE 17 B



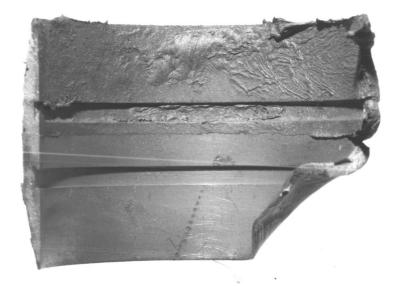


FIGURE 18 1/2" PEELED BRAZE JOINT



FIGURE 19

COUPLING DISTORTED AREA

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## <u>Conclusions</u>

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This investigation revealed that sound, high quality braze joints can be obtained in the 1/4", 3/4", 1 1/4" and 1 1/2" high pressure systems utilizing the present induction braze tools and related equipment. The 2" and 2 1/2" joints cannot be produced with our present braze tools and related equipment.

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### STEEL SEALING JAWS

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The RPD 150 sealing jaws in the 1 1/2", 2" and 2 1/2" straight couplings were replaced with a stainless steel jaw. The braze tools for brazing the elbow and tee type fittings were also modified in like manner. Enough heat reached the RPD 150 material to produce outgassing during continued use. The outgassing contaminated the atmosphere inside the chamber resulting in undesireable oxidation. The contamination problem was eliminated by the change to steel. It was felt that with the shorter width of tools for brazing elbow and tee fittings, it would be advisable to replace the plastic sealing jaws with stainless steel also. Replacements of these tools were completed and all tools tested. All braze tools tested satisfactory.

### **TECHNICAL INFORMATION SERIES**

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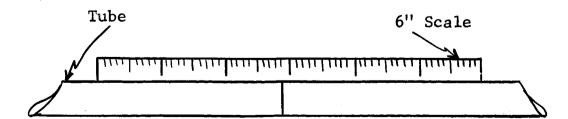
### RECOMMENDED OR SUGGESTED BRAZE PROCEDURE

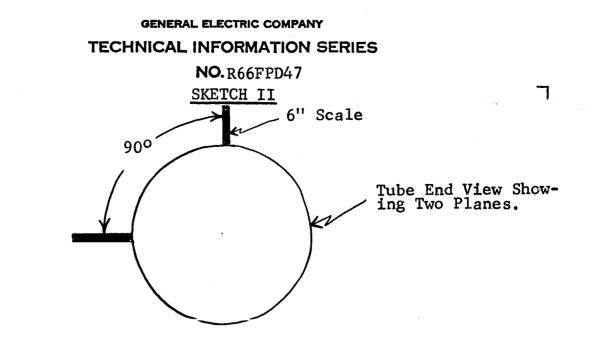
### Tubing Fit Up

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- 1.1 Purpose: To cut, trim and align tube ends before the braze operation.
- 1.2 Set-up and Parts Protection: Using a blue print accumlation list and (if possible) a photo book check for couting, clamping and bracketing of the tubing before fit-up. Keep the tube ends capped at all times, except during brazing. Handle tubing carefully. Avoid unnecessary contact with other piping structural material and tooling.
- 1.3 When tube fitter has marked the tube or tubes for cut off, remove it if necessary to facilitate cutting. Be sure to plug the tube before cutting.
- 1.4 On final fit tube ends should mate in free state, or maximum gap of .030.
- 1.5 To determine proper alignment, lay a six inch scale (or straight edge).



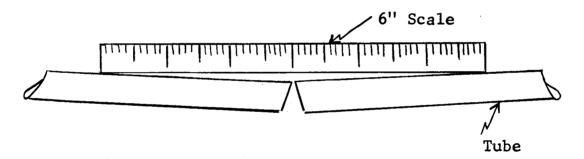


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## SKETCH III

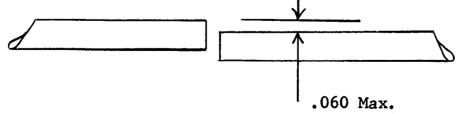
Warning - Do not assemble joint as shown in Sketch III.

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### SKETCH IV

1.6 After completion of step 1.5 and with tube ends in free state, misalignment must not exceed .060. See Sketch IV.



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Realign end tube which is removed or disturbed after final 1.7 alignment.

## Tube Preparation

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2.1 Purpose: Sizing is required to control the clearance between the coupling and the tube.

Masking is required to center the coupling on the joint and to assure control of the gap between tube ends.

A cleaning process is required to prepare the tube and tube ends for braze.

- 2.2 Sizing: The proper roll-a-finish size tool and split holding clamp should be set up on the sizing equipment. Secure tube in clamp and size tube ends. (A. sample piece of tubing should be run first to see if the roll-a-finish tool is set correctly to give the required diameter; this is especially true when sizing tubing of the same diameter, but of different wall thickness.)
- Tube end should be wiped clean of all oil. 2.3
- Tube end to be brazed should be roughened using 180 emery 2.4 cloth. Tube end after sizing has too smooth a finish for brazing.
- 2.5 Some means of marking the tube end prior to final clean should be done now. A suggested method for use is an electric etch similar to that used for putting an identifying number on a tube.
- 2.6 Tube and tube end should now be cleaned to your specification, capped and bagged for brazing.

# Inspection - Visual and Dimensional

3.1 Purpose: To provide the assembly inspector with an instruction by which to interpret and perform the various inspection functions necessary to assure successful processing of high integrity leak proof braze joints.

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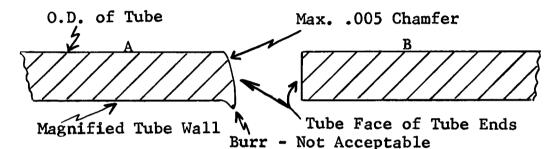
- 3.2 Preassembly Inspections Tubing Only: Visual, inspect the tubing for dents. No dents allowed over a 2" length measured from tube end. No radius within the dent or between the dent and its adjacent tube surface shall be less than three times the nominal tube wall-thickness. Depth of dents not to exceed 10% of outside tube diameter. No dents allowed in bend radii or within one tube diameter of tangent points. More than two dents in any given axial inch of tube length is not allowed except on high pressure tubing. On high pressure tubing more than two dents in any given three consecutive axial inches of tube length is not allowed.
- 3.3 Visual: Inspect the tube ends and tubing for nicks and scratches. Depth of 10% of wall thickness on all but high pressure tubing. On hydraulic tubing, use 5% of wall thick-ness or .002 whichever is smaller.
- 3.4 Visual: Out of roundness shall not exceed 10% of the tube diameter over 1.75" length measured from the tube end.

#### **TECHNICAL INFORMATION SERIES**

## **NO.** R66FPD47

3.5 Visual: Tube End - Inspect the trimmed tube end for squareness of the face, freedom of burrs in the I.D. and a maximum of .005 chamfer on the O.D. of the face. See Sketch V.

### SKETCH V



Note: A) Not Acceptable B) Acceptable

Use a brass scribe on the I.D. of tube ends if necessary to pick up the burr.

- 3.6 Visual: Corrosion Inspect for rust or any form of dirty scale on tube 0.D. not allowed.
- 3.7 Visual: Centering Marks Inspect the tube O.D. for presence of the coupling and tool centering marks. The marks (one per tube end) must be clear and distinct.

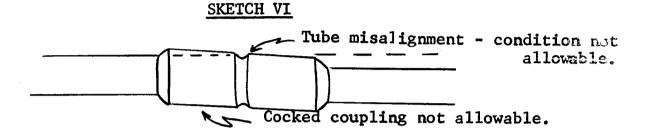
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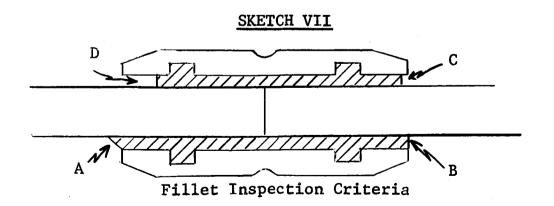
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3.8 Final Braze Inspection: Visual - Inspect the brazed joint for tube misalignment and cocked coupling. See Sketch VI.



Visual: Using a localized light and a plain or magnifying mirror as needed, inspect the joint for evidence of a braze alloy fillet around the external tube/coupling entrance periphery; no gaps, voids or pinholes allowed. See Sketch VII.



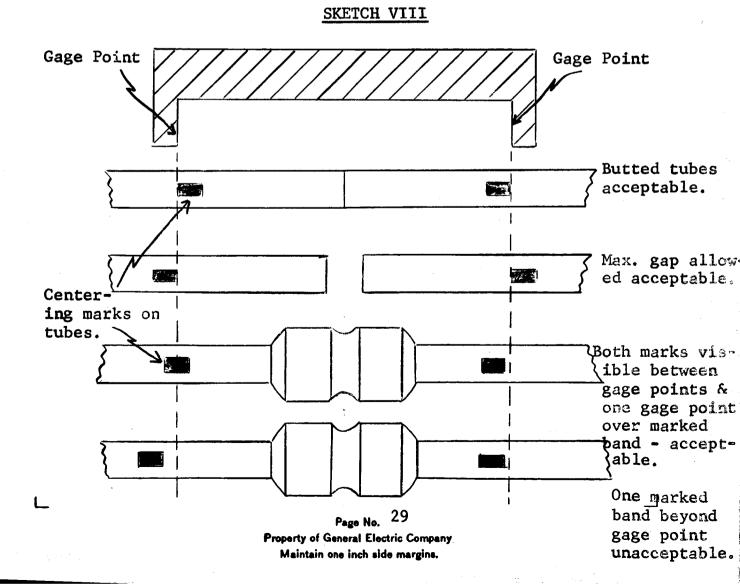
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### **NO.** R66FPD47

- A. Braze alloy extends beyond edge of coupling. Fillet is palinly visible. This is acceptable.
- B. Braze alloy extends to the edge of coupling. Fillet is acceptable, if visible through a light and/or 10X glass.
- C. Braze alloy extends to the edge of coupling. Fillet requires light and 10X glass to see it. This is acceptable. Under cut must not exceed .03125.
- D. Braze alloy is not visible with light and 10X glass. Braze joint is not acceptable.
- 3.9 Dimensional: On coupling centering and tube gap. Using a fixture as shown in Sketch VIII inspect brazed tube joint.



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- ۲ 4.1 Repair Procedure: This suggested repair procedure is for the repair of braze joints which after the first induction cycle with internally preplaced braze rings do not exhibit the presence of braze alloy completely around the tube/coupling interstice.
  - By visual inspection and measurements the sum total length 4.2 of all voids at one coupling tube intersection must be less than the following lengths as measured circumferentially around the tube.

<u>Joint Size</u>	Max. Limit Inches
1/4"	5/32"
3/4''	15/32"
1 1/4"	5/8''
1 1/2"	3/4"
2''	1"
2 1/2"	1"

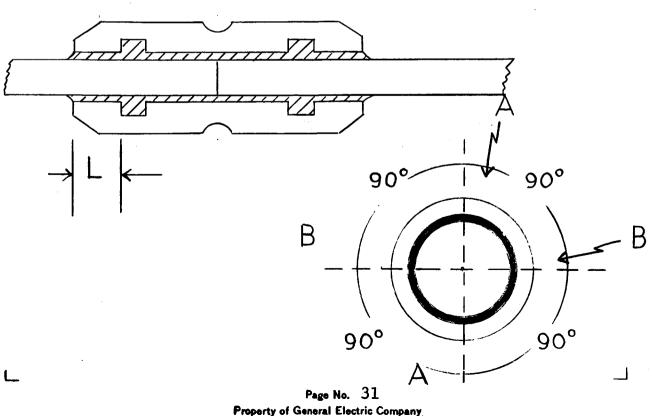
- 4.3 Locally clean the voided area flush with distilled water. Flush with suitable solvent and let dry.
- 4.4 Wearing clean lint free gloves place a braze ring on the tube adjacent to the coupling side which is voided. No more than one braze ring per coupling side allowed.

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- 4.5 Purge joint in question sufficient time to achieve a good argon atmosphere - being sure all of solvent has evaporated. Repeat the brazing procedure assuring flow of external ring. No more than one reheat per joint allowed.
  - 4.6 Visual Inspection: Visual inspect each joint using a localized light and a magnifying mirror. Joint must show evidence of a braze alloy fillet 360° around the external tube coupling entrance periphery; with no gaps, voids or pinholes. Examine questionable areas with a 10X magnifying glass. See Sketch VII of an acceptable joint.
  - 4.7 X-ray the joint in two planes 90° apart. Inspect for voids in length L shown in Sketch IX. X-ray acceptable limits are defined in Table I.

#### SKETCH IX



Maintain one inch side margins.

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X-ray inspection in plane A-A and B-B. The cumulative length of voids in one length "L" shall be considered one indication in Table I. Joints subjected to repair which do not meet this criteria after repair will be cut out and rebrazed.

TABLE I

Tubing Size	Allowable Limits
1/4" Dia.	One (1) .035" and three (3) .018 indications allowed per coupling end.
3/4" Dia.	One (1) .077" and three (3) .038 indications allowed per coupling end.
1 1/4" Dia.	One (1) .107" and three (3) .053 indications allowed per coupling end.
1 1/2" Dia.	One (1) .137" and three (3) .063 indications allowed per coupling end.
2" Dia.	One (1) .154" and three (3) .080 indications allowed per coupling end.
2 1/2" Dia.	One (1) .171" and three (3) .098 indications allowed per coupling end.

No voids allowed within .015" of outboard ends of coupling.

5.0 Debraze

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- 5.1 Purpose: To facilitate disassembly, repair or replacement of the brazed tubing.
- 5.2 Cut coupling in half and deburr tube ends.

Note: A nylon brush may be used to prevent entry of chips during the deburring operation.

5.3 Be sure tube is free of all fuel, oil or contaminants. Purge inside of tubing with argon until a good atmosphere is ach-ieved.

5.4 Clamp on debrazing tool and heat coupling until it is hot enough to be removed. After removal of half coupling the

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tube end must be cleaned prior to brazing.

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