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STUDY OF APOLLO WATER IMPACT

FINAL REPORT

VOLUME 6

USER'S MANUAL - INTERACTION

(Contract NAS9-4552, G.O. 5264)

May 1967



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Prepared by

J. P. D. Wilkinson

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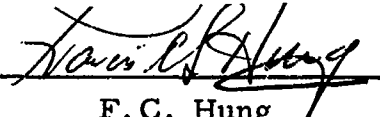
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FOREWORD

This report was prepared by North American Aviation, Inc., Space Division, under NASA Contract NAS9-4552, for the National Aeronautics and Space Administration, Manned Space Flight Center, Houston, Texas, with Dr. F. C. Hung, Program Manager and Mr. P. P. Radkowski, Assistant Program Manager. This work was administered under the direction of Structural Mechanics Division, MSC, Houston, Texas with Dr. F. Stebbins as the technical monitor.

This report is presented in eleven volumes for convenience for handling and distribution. All volumes are unclassified.

The objective of the study was to develop methods and Fortran IV computer programs to determine by the techniques described below, the hydro-elastic response of representation of the structure of the Apollo Command Module immediately following impact on the water. The development of theory, methods and computer programs is presented as Task I Hydrodynamic Pressures, Task II Structural Response and Task III Hydroelastic Response Analysis.

Under Task I - Computing program to extend flexible sphere using the Spencer and Shiffman approach has been developed. Analytical formulation by Dr. Li using nonlinear hydrodynamic theory on structural portion is formulated. In order to cover a wide range of impact conditions, future extensions are necessary in the following items:

- a. Using linear hydrodynamic theory to include horizontal velocity and rotation.
- b. Nonlinear hydrodynamic theory to develop computing program on spherical portion and to develop nonlinear theory on toroidal and conic sections.

Under Task II - Computing program and User's Manual were developed for nonsymmetrical loading on unsymmetrical elastic shells. To fully develop the theory and methods to cover realistic Apollo configuration the following extensions are recommended:

- a. Modes of vibration and modal analysis.
- b. Extension to nonsymmetric short time impulses.

c. Linear buckling and elasto-plastic analysis

These technical extensions will not only be useful for Apollo and future Apollo growth configurations, but they will also be of value to other aeronautical and spacecraft programs.

The hydroelastic response of the flexible shell is obtained by the numerical solution of the combined hydrodynamic and shell equations. The results obtained herein are compared numerically with those derived by neglecting the interaction and applying rigid body pressures to the same elastic shell. The numerical results show that for an axially symmetric impact of the particular shell studied, the interaction between the shell and the fluid produces appreciable differences in the overall acceleration of the center of gravity of the shell, and in the distribution of the pressures and responses. However the maximum responses are within 15% of those produced when the interaction between the fluid and the shell is neglected. A brief summary of results is shown in the abstracts of individual volumes.

The volume number and authors are listed on the following page.

The contractor's designation for this report is SID 67-498.

INDEX FOR FINAL REPORT

"Apollo Water Impact"

<u>Volume No.</u>	<u>Volume Title</u>	<u>Authors</u>
1	Hydrodynamic Analysis of Apollo Water Impact	T. Li and T. Sugimura
2	Dynamic Response of Shells of Revolution During Vertical Impact Into Water - No Interaction	A. P. Cappelli, and J. P. D. Wilkinson
3	Dynamic Response of Shells of Revolution During Vertical Impact Into Water - Hydroelastic Interaction	J. P. D. Wilkinson, A. P. Cappelli, and R. N. Salzman
4	Comparison With Experiments	J. P. D. Wilkinson
5	User's Manual - No Interaction	J. P. D. Wilkinson
6	User's Manual - Interaction	J. P. D. Wilkinson and R. N. Salzman
7	Modification of Shell of Revolution Analysis	A. P. Cappelli and S. C. Furuie
8	Unsymmetric Shell of Revolution Analysis	A. P. Cappelli, T. Nishimoto, P. P. Radkowski and K. E. Pauley
9	Mode Shapes and Natural Frequencies Analysis	A. P. Cappelli
10	User's Manual for Modification of Shell of Revolution Analysis	A. P. Cappelli and S. C. Furuie
11	User's Manual for Unsymmetric Shell of Revolution Analysis	E. Carrion, S. C. Furuie and T. Nishimoto

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TABLE OF CONTENTS

	Page
LIST OF ILLUSTRATIONS	xi
LIST OF TABLES	xi
1.1 INTRODUCTION	1
1.2 Load Map	3
1.3 Iterative Process Within Each Time Interval for the Pressure Determination	9
2.1 PROGRAM FLOW	13
2.2 Program Deck Setup	20
3.1 TAPE USAGE	23
4.1 INPUT DATA FORMAT	29
4.2 DECRD Subroutine	30
4.3 Data Deck Setup	32
4.4 Call DECRD (DA)	33
4.5 Boundary Conditions	35
4.5.1 Top Boundary	35
4.5.2 Bottom Boundary	38
4.6 Call DECRD (GDA)	41
4.7 Call DECRD (CDA)	42
5.1 SAMPLE PROBLEM	47
5.2 Sample Input Data and Tape Usage for the Start from Zero	49
5.3 Sample Input Data and Tape Usage for the Restart	59
5.4 Sample Output	68
6.1 WARNINGS AND RECOMMENDATIONS	105
6.1.1 6.1.1 Choice of Time Interval	105
6.1.2 Number of Iterations	105
6.1.3 DECRD	105
7.1 PROGRAM LISTINGS	107

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LIST OF ILLUSTRATIONS

Figure No.		Page
1	Iterative Procedure to Find Pressure and Response at Time t_i	11
2	Flow of executive program 157DR	14
3	Tape Usage for a Start from 0 Time	24
4	Contents of Tape B, Created on Logical Unit 8	25
5	Tape Usage for a Restart at 1.0 ms., to 2.0 ms.	27
6	Model of Sample Problem	48

LIST OF TABLES

Table No.		Page
1	Description of Links	2
2	KODES for a Start from Zero	75
3	KODES for a Restart	75

1.1 INTRODUCTION

The hydroelastic computer program is written entirely in FORTRAN IV and makes use of the overlay feature of that language. The program has been checked out in NAASYS, the NAA adaptation of the IBM 7090/7094 IBSYS/IBJOB system; and uses the NAASYS library routines shown in the load map, pages 4 to 8 inclusive, of Section 1.2.

The NAASYS input tape is Unit 5, the output tape is Unit 6. In addition to these files, the program uses Units 8, 9, 12, and 13 for reserve tapes, Units 10 and 11 as scratch tapes, and Unit 7 as the overlay tape. NAASYS itself is stored on Unit 1.

The program is made up of an executive program and eight links, all of which are called by the executive program. A brief description of each link is shown in Table I below.

Table I. Description of Links

Link No.	Name	Purpose
0	Executive	Reads general data, DA, and controls flow of execution of other links
1	GEOM	Reads geometric parameters. Prints all geometric input and calculated values
2	CDAFIT	Sets up stiffness parameters
3	ACCN	Computes hydrodynamic pressures on the shell
4	DEFLTN	Calculates the deflections due to the pressures
5	PATH	Controls flow after computation of deflections. Computes velocities and accelerations
6	INTLDS	Computes internal loads
7	FSUMS	Outputs all computer quantities
8	PIX	A dummy subroutine for a CRT Plotter

1.2 Load Map

OVERLAY ORIGIN CARDS AND ASSIGNED LINK NUMBERS

\$ORIGIN	CHAIN	IS LINK	1, PARENT LINK IS	0
\$ORIGIN	CHAIN	IS LINK	2, PARENT LINK IS	0
\$ORIGIN	CHAIN	IS LINK	3, PARENT LINK IS	0
\$ORIGIN	CHAIN	IS LINK	4, PARENT LINK IS	0
\$ORIGIN	CHAIN	IS LINK	5, PARENT LINK IS	0
\$ORIGIN	CHAIN	IS LINK	6, PARENT LINK IS	0
\$ORIGIN	CHAIN	IS LINK	7, PARENT LINK IS	0
\$ORIGIN	CHAIN, SYSUT2, REW	IS LINK	8, PARENT LINK IS	0

[illegible]

UN06	22614	.UN06.	22614	.BUFSZ	22615		
UN12	22620	.UN12.	22620				
UN13	22621	.UN13.	22621				
FLOG	22622	ALOG10	22622	ALOG	22623		
FXPF	23026	EXP	23026				
FSCD	23147	COSD	23147	SIND	23151		
FSCN	23200	COS	23200	SIN	23201		
FSQR	23374	SQRT	23374				
FXP2	23447	.XP2.	23447				
FXP3	23565	.XP3.	23565				
FRWT	23712	.FRWT.	23712				
FSLD1	24031	.FSL1.	24047	.FSD1.	24055 *		
FSLI	24066	.SLI.	24066	.SLI1.	24073	.SDI.	24101
FSLD0	24122	.FSLO.	24140	.FSD0.	24146 *		
FSL0	24157	.SLO.	24157	.SLO2.	24165	.SDO.	24172
DECRD	24213	DECRD	(24213)				
FASC	24331	ARCOS	24331 *	ARSIN	24332		
//	47246						
1 GMTRY	24462	///	/(47246)	EVEN	24463	GFOM	33034
CF3P	33055	CODIMA	34070				
2 CDAFIT	24462	///	/(47246)	EVEN	24463	CRVFIT	31213
COOS	31231	CODIM4	32244				
ENTP	32372	EVEN	32373	ENTERP	32572		
3 ACCN2	24462	///	/(47246)	EVEN	24463	ACCN	30566
4 157DR1	24462	///	/(47246)	EVEN	24463	DEFLTN	37412
MSU	37441	MSU	(37441)				
INVR5	37551	INV	40240				
5 WHERE	24462	///	/(47246)	EVEN	24463	PATH	25317
6 157DR2	24462	///	/(47246)	EVEN	24463	INTLDS	26603
7 FSUMS	24462	///	/(47246)	EVEN	24463	SUMS	25720

8	LNK6	24462	EVEN	24463	PIX	24476
	I/O BUFFERS			40313	THRU	47117
	UNUSED CORE			47120	THRU	47245
	BEGIN EXECUTION	32				00-00-42

1.3 Iterative Process Within Each Time Interval for the Pressure Determination

According to Equation (24) of Volume 3 of this report, the pressures on the penetrating shell of revolution during vertical axisymmetric impact into a fluid are given by

$$\begin{aligned}
 p = \frac{2}{\pi} \rho \left[\frac{RV^2}{c} + c\mu \frac{\partial V}{\partial t} \right] \\
 + \frac{\rho}{2} \sum_{s=0}^{\infty} f_s \left\{ \frac{RV}{c} \left[p_m(\mu) + \frac{1-\mu^2}{\mu} \frac{\partial}{\partial \mu} p_m(\mu) \right] \int_0^1 \eta v(\eta, t) p_m(\eta) d\eta \right. \\
 \left. + c p_m(\mu) \int_0^1 \eta p_m(\eta) \frac{\partial v}{\partial t}(\eta, t) d\eta \right\} \quad (1)
 \end{aligned}$$

Here,

ρ mass density of fluid

R radius of curvature of shell at impact point

V instantaneous velocity of center of gravity

c radius of wetted surface

$v(\eta, t)$ instantaneous velocity of shell surface

$p_m(\mu)$ is a Legendre polynomial

$$\mu = \left(1 - r^2/c^2 \right)^{1/2}$$

r radial coordinate

$$f_s = \frac{4s+3}{\pi} \left[\frac{(s!)^2 2^{2s+1}}{(2s+1)!} \right]^2$$

$$m = 2s + 1$$

In the computer program, the series is truncated at $s = 3$, satisfactory convergence having been achieved. It can be seen that the pressures are dependent on the overall velocity V of the center of gravity, and on the structural velocities v and their time derivatives. Thus, the pressures are coupled closely to the shell deformations.

In the computer program, an iterative process is used within each time increment in order to compute both the pressures and the shell responses so that they satisfy all the given equations to within some given convergence criterion. The iterative process is shown in diagrammatic form in Figure 1. The controlling input data for the iterations are CONV, the convergence criterion, and IVX, the maximum allowable number of iterations per time cycle. If the number of iterations exceeds IVX, the program considers the iteration cycle complete and simply goes on to the next time. Should this happen, the responses of the subsequent time cycles may not be satisfactory, and the job should be restarted with a larger IVX.

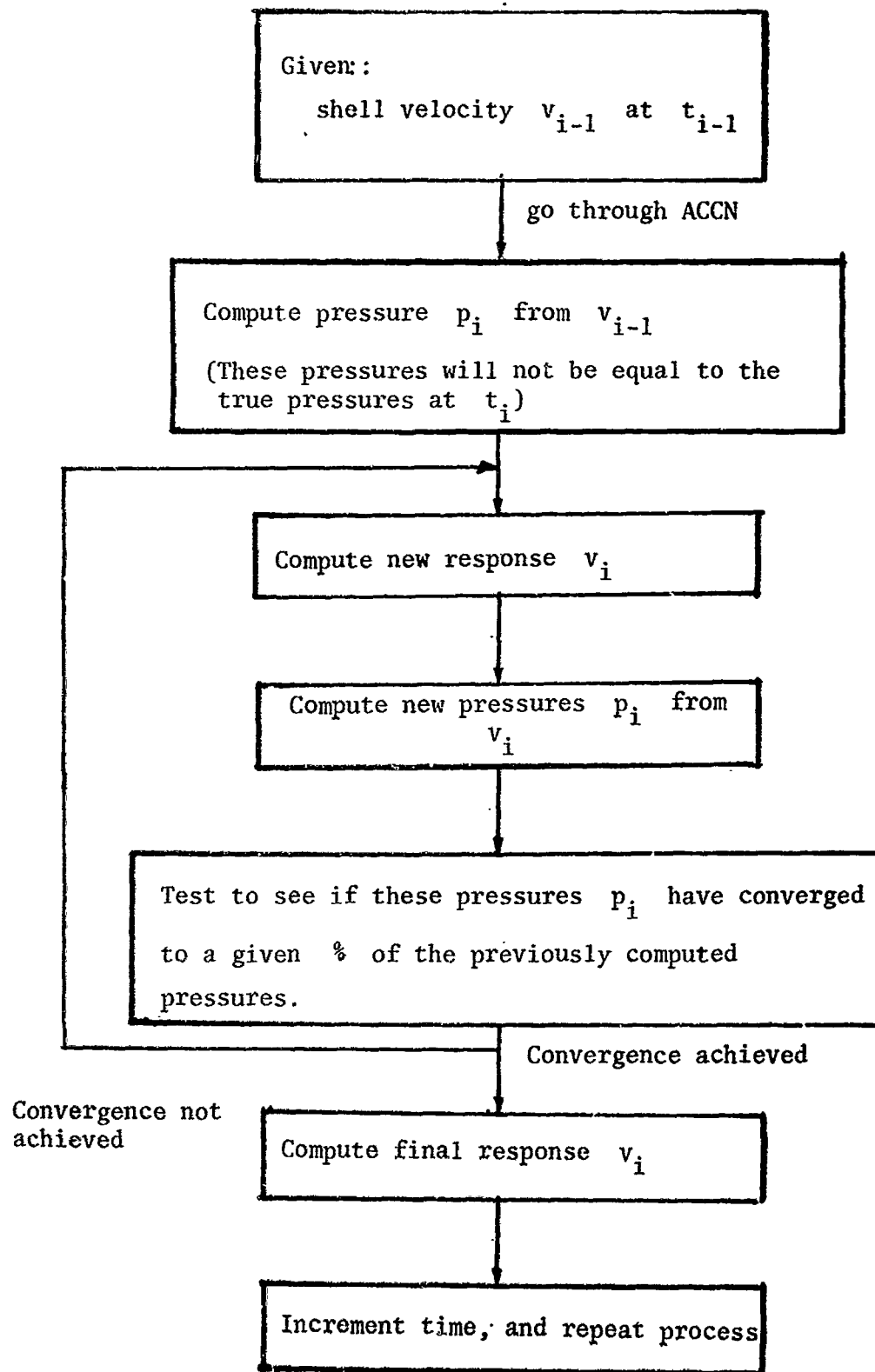


Figure 1. Iterative Procedure to Find Pressure and Response at Time t_i

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2.1 PROGRAM FLOW DESCRIPTION

An overall flow diagram of the executive program 157DR is shown in Figure 2. A listing of the complete program is shown in Section 7.1.

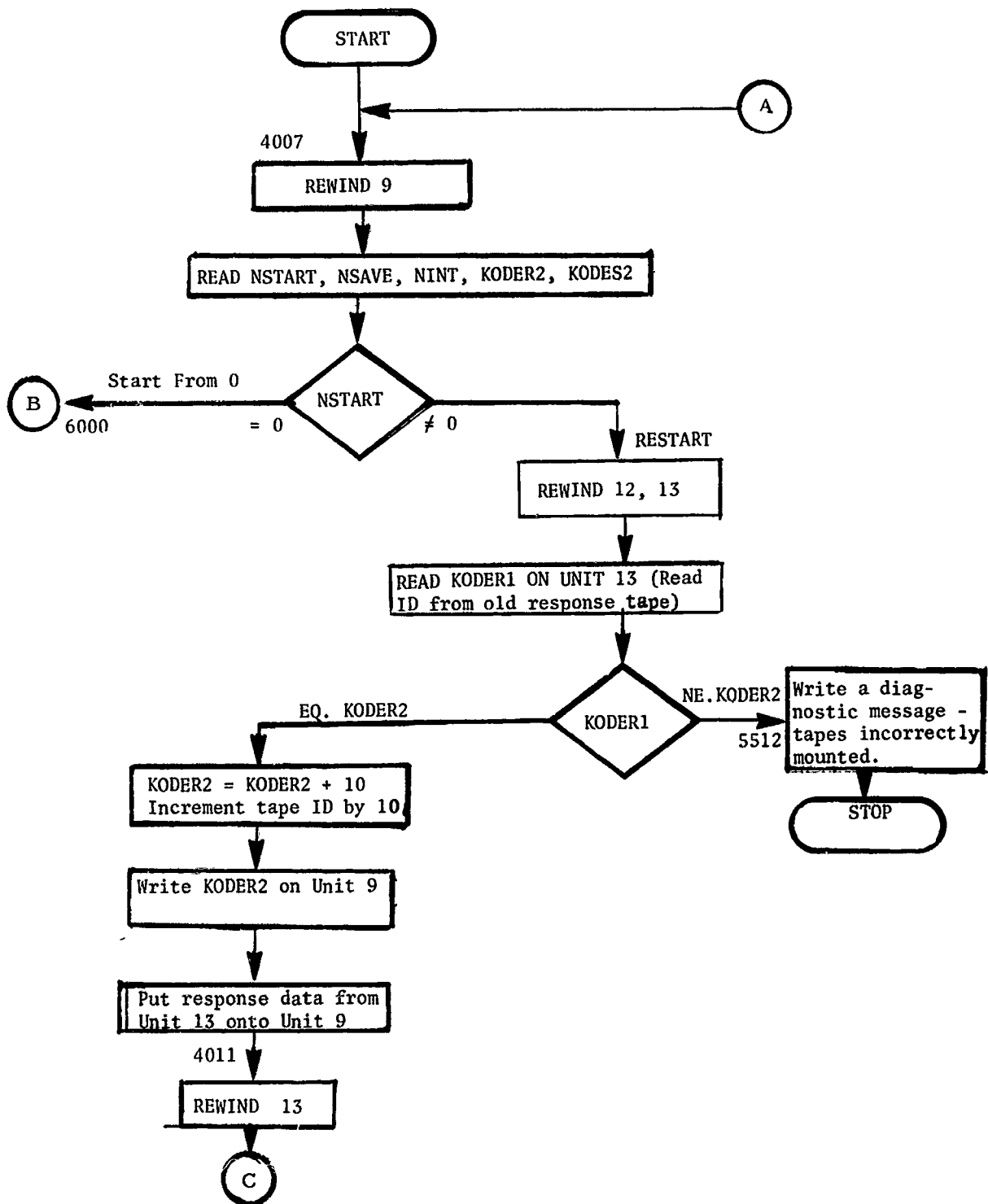


Figure 2. Flow of Executive Program 157DR (Sheet 1 of 6)

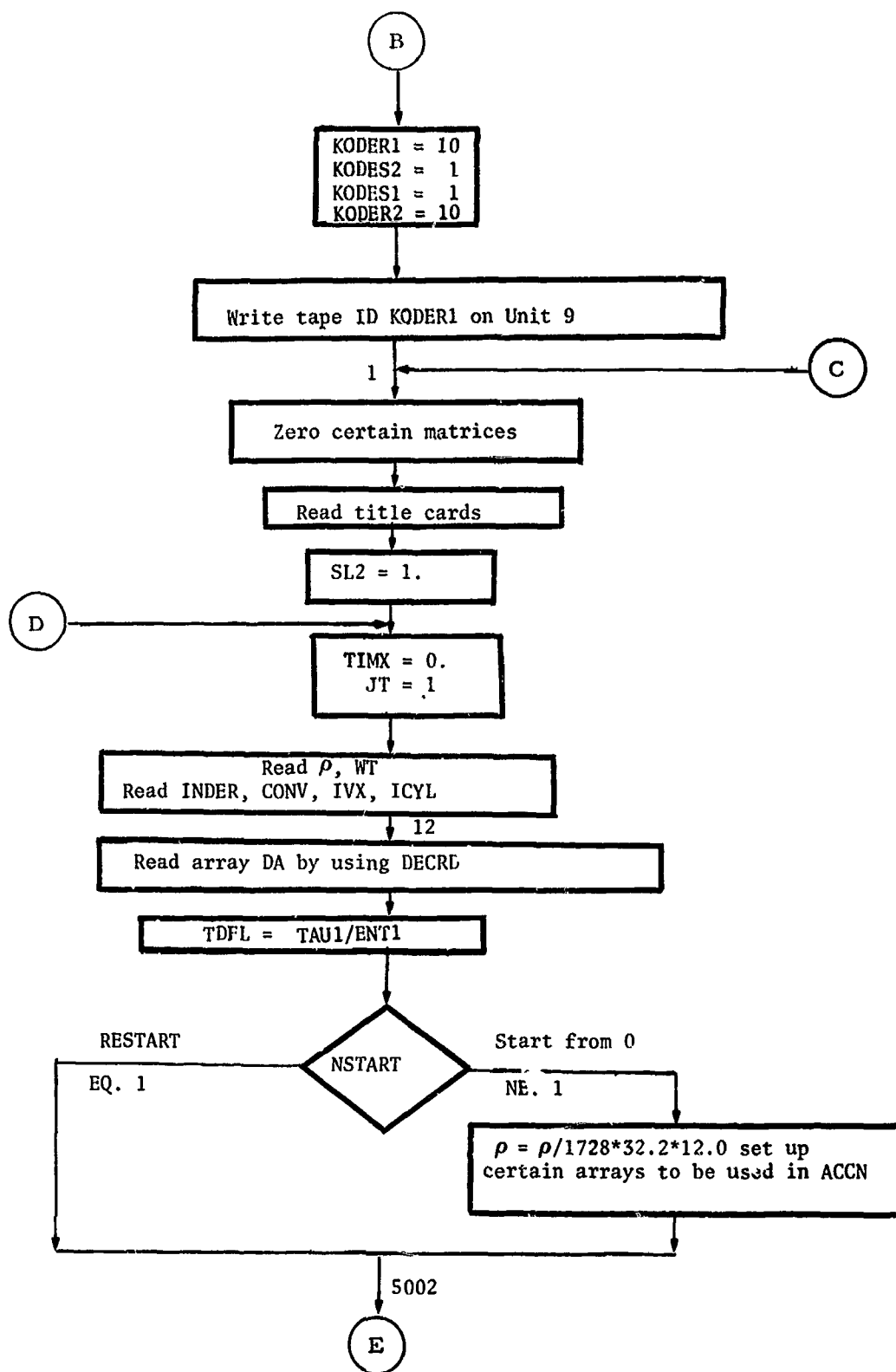


Figure 2. Flow of Executive Program 157DR (Sheet 2 of 6)

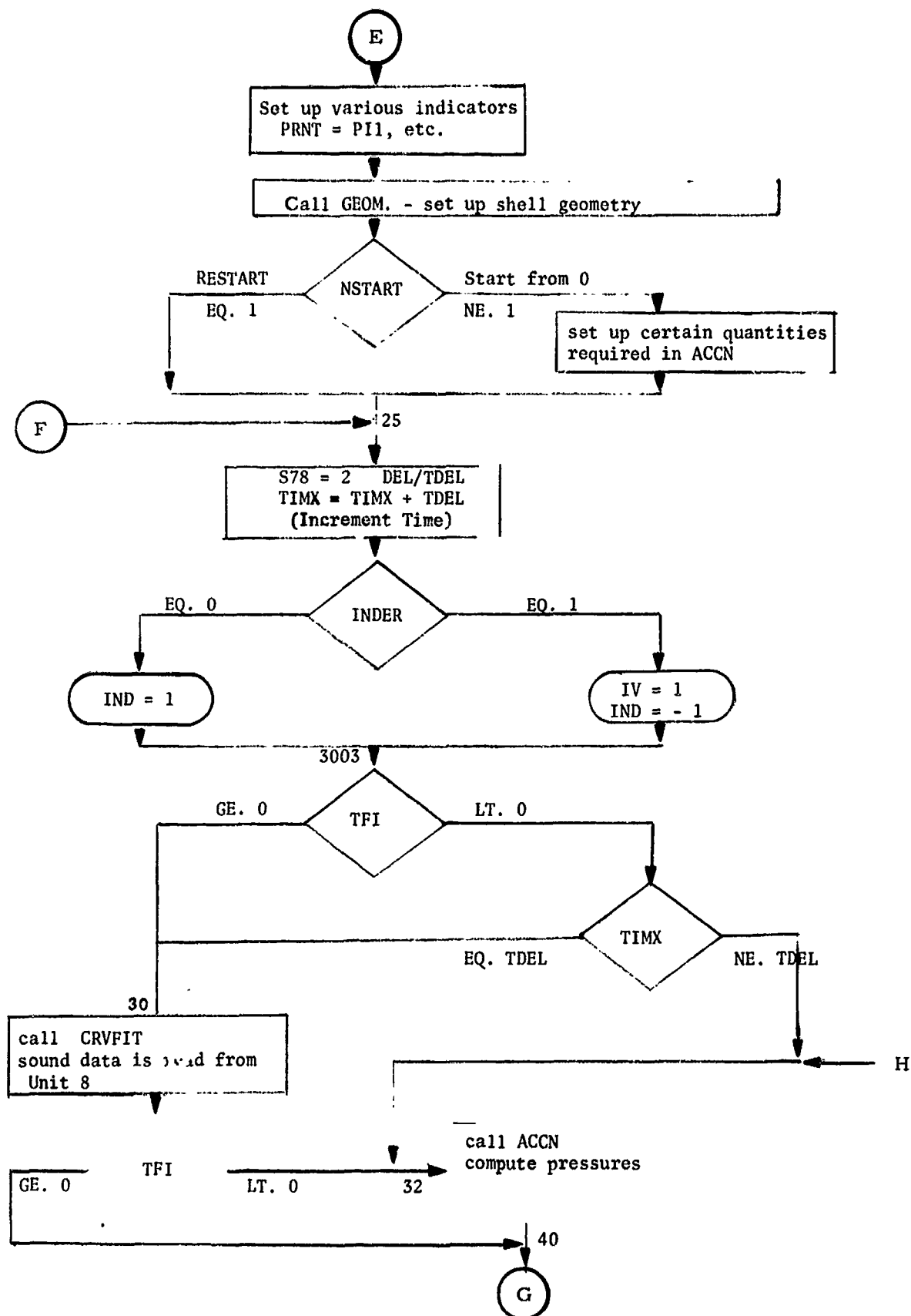


Figure 2. Flow of Executive Program 157DR (Sheet 3 of 6)

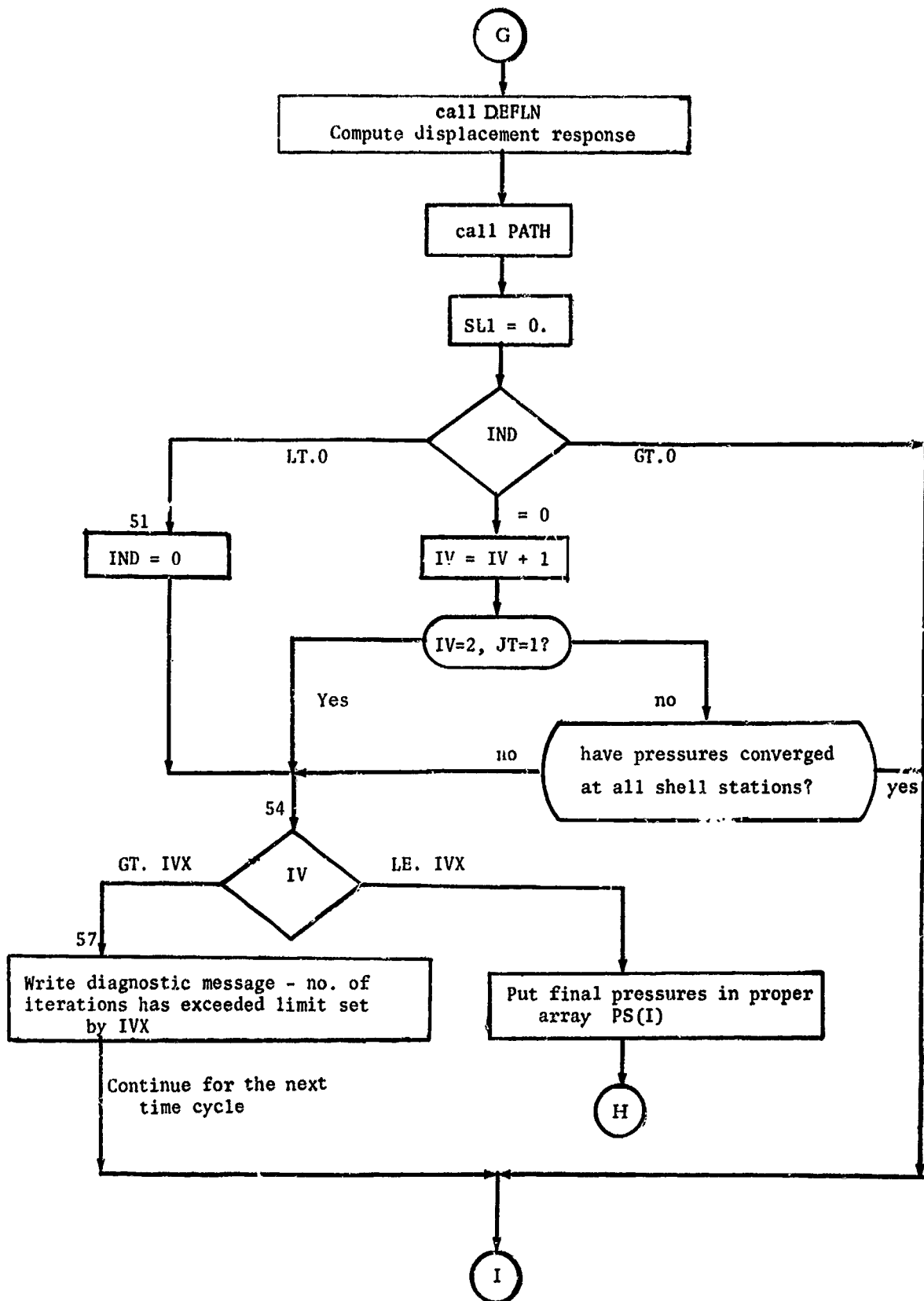


Figure 2. Flow of Executive Program 157DR (Sheet 4 of 6)

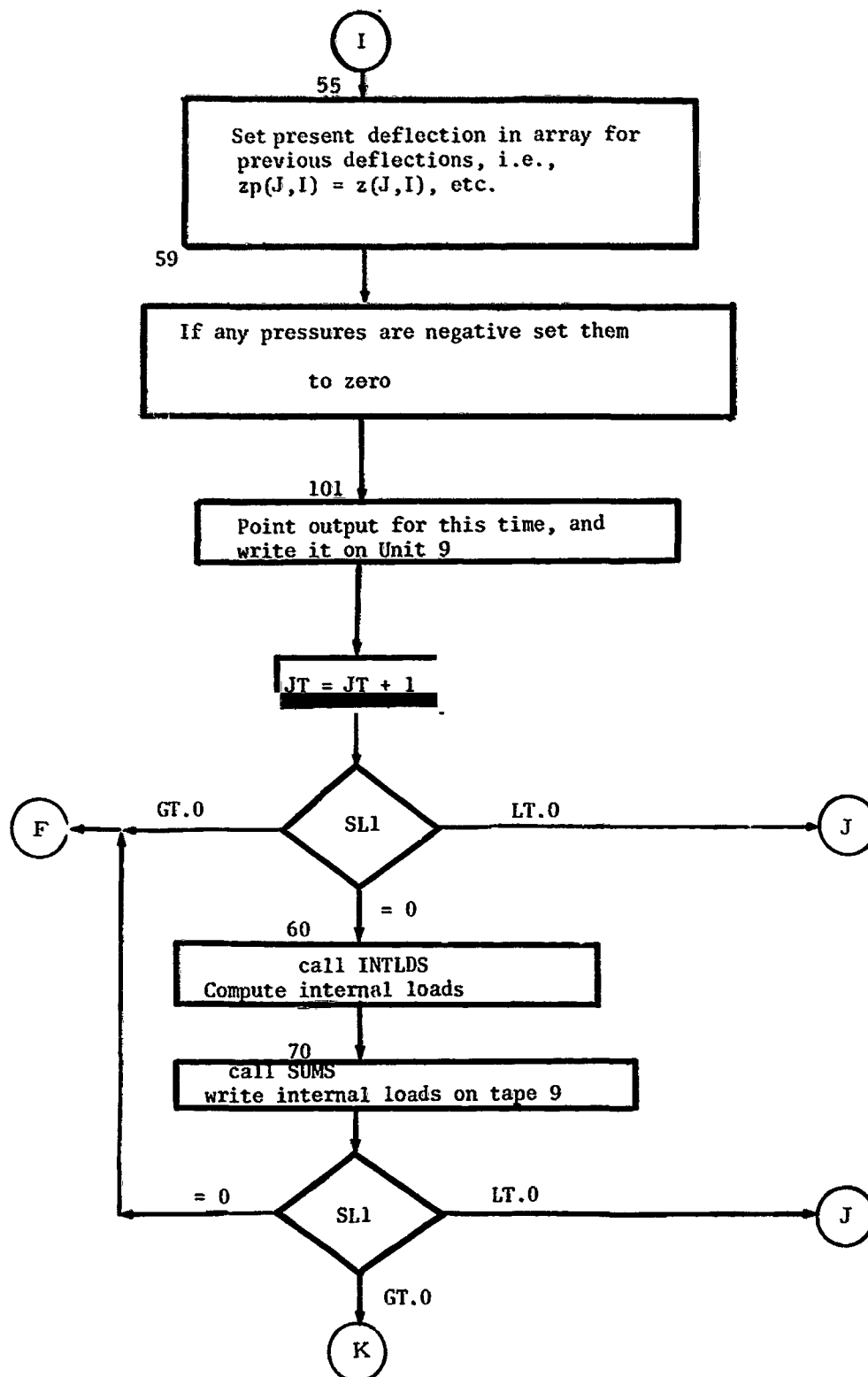


Figure 2. Flow of Executive Program 157DR (Sheet 5 of 6)

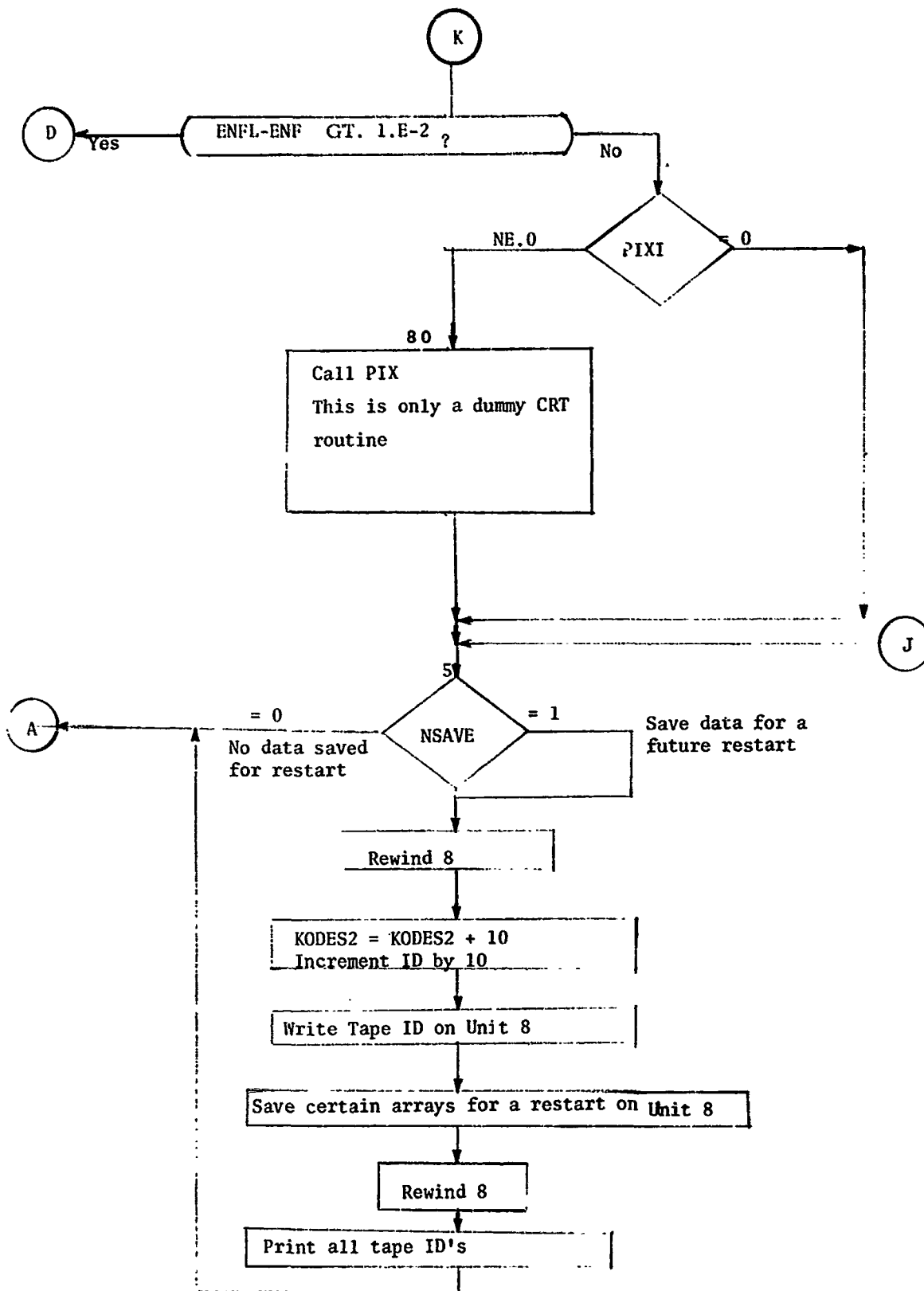


Figure 2. Flow of Executive Program 157DR (Sheet 6 of 6)

2.2 Program Deck Setup

As explained in Section 1.1, the deck is set up in overlay regions. Each region is denoted by a \$ORIGIN control card. A list of the setup is shown below. It includes the control cards and deck names. The order of these decks must be kept in the given sequence.

Control Cards		Subroutines
\$IBJOB		
\$IBFTC	157 DR	Main program
\$IBFTC	MMPY	MMY
\$IBFTC	MADD	ADD
\$ORIGIN	CHAIN	
\$IBFTC	GMTRY	GEOM
\$IBFTC	CF3P	CODIMA
\$ORIGIN	CHAIN	
\$IBFTC	CDAFIT	CRVFIT
\$IBFTC	CODS	CODIM4
\$IBFTC	ENTP	ENTERP
\$ORIGIN	CHAIN	
\$IBFTC	ACCN2	ACCN
\$ORIGIN	CHAIN	
\$IBFTC	157DR1	DEFLTIN
\$IBFTC	MSUB	MSU
\$IBFTC	INVRS	INV
\$ORIGIN	CHAIN	
\$IBFTC	WHERE	PATH
\$ORIGIN	CHAIN	
\$IBFTC	157DR2	INTLDS
\$ORIGIN	CHAIN	
\$OBFTC	FSUMS	SUMS
\$ORIGIN	CHAIN, SYSUT2, REW	
\$IBFTC	LNK6	PIX
\$DATA		

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3.1 TAPE USAGE

In order to permanently preserve the computer output in an easily accessible form, it is put out on a reserve tape. In addition, to enable the user to continue a job after the program has been run to a certain time (say 1.0 ms.), certain arrays are saved on another tape so that a restart can be subsequently made for calculations from 1.0 ms. to, say, 2.0 ms. This saving of certain arrays avoids the complete recalculation from 0 to 1.0 ms.

Because the mounting of reserve tapes is subject to human error, the first word on each tape is an identification code. This identification is automatically written on the tape when it is created and is printed on the final printed output at the end of the job. Before a tape is read by the computer, its identification is checked with a code which is part of the card input - KODER2 and KODES2. If the identification checks, the job proceeds; if not, then a diagnostic printout is made stating which tape is incorrectly mounted, and the job is stopped. It is therefore important to know the correct tape identification and keep track of it throughout all restart conditions.

To start a job from time zero, any two available tapes are mounted on logical units 8 and 9 (See Figure 3). The tape on unit 8 will be denoted by Tape A, and that on 9 will be denoted by Tape B. At the end of the job, Tape A will contain the saved arrays necessary for a restart. Tape B will contain the response in the order shown in Figure 4, where each line denotes a single record of the tape. As each tape is created, the identification code is written on it as the first record. Thus, Tape A, the "saved-data" tape, has the identification.

EDPM JOB REQUEST SUPPLEMENT

JOB NO. _____ REQUESTED BY _____ PHONE _____

ADDITIONAL INSTRUCTIONS

MOUNT ANY AVAILABLE TAPE ON LOGICAL UNIT 8

PUT FILE RING IN

Comment: This tape will hold the saved data for a future restart. Denote this tape by Tape No. A. Its identification word KODES2 = 10.

MOUNT ANY AVAILABLE TAPE ON LOGICAL UNIT 9

PUT FILE RING IN

Comment: This tape will hold the shell response Remote tape by B. Its identification No. is KODER2 = 11.

☐ SEE BACK OF FORM

TAPE USAGE

AUTH NO. _____ NAME _____
 JOB NO. _____ DATE _____
 PHONE _____ DEPT _____ GROUP _____

UNIT	REEL NO.	TAPE ID	DESCRIPTION	MINIMUM LENGTH	RESERVE THIS TAPE	FILE THIS TAPE	RETURN WITHDRAWN TAPE	RELEASE RESERVE TAPE	WITHDRAW UNRESERVED TAPE	WITHDRAW RESERVED TAPE
8	A	10	Saved data at 1.0 ms.		✓					
9	B	11	Response 0 - 1.0 ms.		✓					

Figure 3. Tape Usage for a Start from 0 Time

KODER2	
JT, TIMX, AP, VEL, ACC, BP, N, NOT	} This information is repeated for each time interval
PN(I), I = 1, NOT	
PM(I), I = 1, NOT	
PE2(I), I = 1, NOT	
USUM(I), I = 1, N	
WSUM(I), I = 1, N	
EMFE(I), I = 1, N	
EMTH(I), I = 1, N	
QFE(I), I = 1, N	
QTH(I), I = 1, N	
ENFE(I), I = 1, N	
ENTH(I), I = 1, N	
SIGFE(I), I = 1, N	
SIGTH(I), I = 1, N	
ZDOT(1, I), I = 1, N	
ZDOT(3, I), I = 1, N	
Z2DOT(1, I), I = 1, N	
Z2DOT(3, I), I = 1, N	

Figure 4. Contents of Tape B, Created on Logical Unit 8

KODER2 = 10,

while Tape B, the response tape, has the identification

KODES2 = 11.

Let us say that the job was stopped at $t = 1.0$ ms. In order to restart it, and run to $t = 2.0$ ms, the following tape manipulations are required. Any two available tapes are mounted onto logical units 8 and 9 (See Figure 5). Let us denote the tape on unit 8 by Tape C, and that on unit 9 by Tape D. Tape C will contain the "saved data" at the end of the job at $t = 2.0$ ms, while Tape D will contain the complete response from 0 to 2.0 ms. In addition to these two new tapes, Tapes A and B from the previous run are mounted on logical units 12 and 13, respectively (See Figure 5). At the beginning of the job, the identification number KODER2 of Tape B is read and if it is the correct number, the information on Tape B is placed on Tape D. Thus, Tape C now contains the response from 0 to 1.0 ms. Then, the identification number of Tape A is checked, and if it is correct, the "saved data" on Tape A is placed in common storage, and the job is started. At the end of the job, Tape D on logical unit 9 will contain the response from 0 to 2.0, while Tape C on logical unit 8 will contain the "saved data" at $t = 2.0$ ms, for a subsequent restart.

The identification numbers of the response tapes and the "saved data" tapes are incremented by 10 during each restart. Thus, the identification numbers of the newly created Tapes C and D are

KODER2 = 20

KODES2 = 21

respectively.

For a subsequent restart, new tapes are mounted on logical units 8 and 9 and, now, tapes C and D are mounted on logical units 12 and 13.

EDPM JOB REQUEST SUPPLEMENT

JOB NO.	REQUESTED BY	PHONE
---------	--------------	-------

ADDITIONAL INSTRUCTIONS

MOUNT ANY AVAILABLE TAPE ON LOGICAL UNIT 8

PUT FILE RING IN

Comment: This tape will hold saved data for a future restart. Denote this tape by Tape No. C. Its identification number will be KODES2 = 20.

MOUNT ANY AVAILABLE TAPE ON LOGICAL UNIT 9

PUT FILE RING IN

Comment: This tape will hold response from 0 to 2 ms. Denote this tape by Tape No. D. Identification KODES2 = 21.

MOUNT TAPE A ON LOGICAL UNIT 12

Comment: This tape is for the restart.

MOUNT TAPE B ON LOGICAL UNIT 13

Comment: This tape holds the response from 0 to 1 ms., and its information is put onto Tape C at beginning of job.

☐ SEE BACK OF FORM

TAPE USAGE

AUTH NO. _____ NAME _____
 JOB NO. _____ DATE _____
 PHONE _____ DEPT _____ GROUP _____

UNIT	REEL NO.	TAPE ID	DESCRIPTION	MINIMUM LENGTH	RESERVE THIS TAPE	FILE THIS TAPE	RETURN WITHDRAWN TAPE	RELEASE RESERVE TAPE	WITHDRAW UNRESERVED TAPE	WITHDRAW RESERVED TAPE
8	C	20	Saved data at 2.0 ms.		✓					
9	D	21	Response 0 - 2.0 ms.		✓					
12	A	10	Saved data at 1.0 ms.					✓		
13	B	11	Response 0 - 1.0 ms.					✓		

Figure 5. Tape Usage for a Restart at 1.0 ms., to 2.0 ms.

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4.1 INPUT DATA FORMAT

Data are entered into the program by three subroutines. The executive program 157DR reads the hydrodynamic data, and the DA region of the shell data. Subroutine GEOM reads the GDA region of shell data, and subroutine CDAFIT reads the CDA region of the shell data. The regions DA, GDA, and CDA are read by means of the DECRD subroutine.

The data in regions DA, GDA, and CDA is read by means of the DECRD subroutine. A description of the subroutine follows, together with a listing in FORTRAN IV.

1. **Description.** When a minus sign is encountered in column 1 of a DECRD data card, that card will be read and then reading will be terminated.

3. Call statement: CALL
DECRD (ARRAY)

4. Error indication: If the index field is zero or blank, the comment "BAD DATA CARD" and the contents columns 73-80 of the defective card will be printed. The job will be terminated.

- [illegible]

ARR(1)	-0.7063E 01	ARR(3)	0.2435E-00	ARR(5)	0.4649E 04
ARR(2)	Unchanged	ARR(4)	0.2065E 04		

```
ARR(11) 0.7896E 21 (Exponent mislocated or incomplete.)
ARR(12) Unchanged (Treated as a blank.)          ARR(14) 0.2975E 04
ARR(13) Unchanged (Treated as a blank.)          ARR(15) 0.1234E 03
```

- 30 -

\$IBFIC DECRD		DECRD0000
SUBROUTINE DECRD(D)		DECRD0005
DIMENSION FLT(5), ID(2), D(1)		DECRD010
10 READ (5,100) LOC, FLT, ID		DECRD015
100 FORMAT (I12, 5E12.0, 1A6, 1A2)		DECRD020
IF (LOC.EQ. 0) GO TO 500		DECRD025
15 K = IABS(LOC) - 1		DECRD030
DO 20 I = 1,5		DECRD035
IF (SIGN(1.0,FLT(I)).LT.0.0 .AND. FLT(I) .EQ. 0.0) GO TO 20		DECRD040
J = K + I		DECRD045
D(J) = FLT(I)		DECRD050
20 CONTINUE		DECRD055
IF (LOC.LT. 0) GO TO 1000		DECRD060
GO TO 10		DECRD065
500 WRITE (6,200) ID		DECRD070
200 FORMAT(10H0BAD DATA 1A6,1A2)		DECRD075
CALL EXIT		DECRD080
1000 RETURN		DECRD085
END		DECRD090

4.3 Data Deck Setup

Data decks should be stacked as follows:

1. Indicator card with NSTART, etc.
2. Three title cards (which may be blank, if necessary).
3. A card with RHO, WT.
4. An indicator card with INDER, etc.
5. DA, general shell data, read by executive program.
6. GDA, geometry data, read by GEOM subroutine.
7. CDA, section properties data, read by CDAFIT subroutine.

The data in groups 5, 6 and 7 should have a minus sign in column 1 of the last card.

The following tables show the nature of the DA, GDA, and CDA decks.

4.4 Call DECRD (DA)

DECRD Index	Name	Description
1	EN	No. of points along shell meridian
2	AO	Reference length (in.)
3	HO	Reference thickness (in.)
4	EO	Reference Young's Modulus (psi)
5	SIGO	Reference stress (psi)
8	POI	Poisson's ratio
11	SPRL	Location of spring along meridian
12	UK	Spring value in ξ direction
14	WK	Spring value in normal direction
16	TAUI	Length of total time interval from zero
17	ENT1	Total no. of time intervals from zero to TAUI
18	PI1	Print interval (will always print last interval)
25	MASS	Mass density of shell, lbs. sec ² /in ⁴
26	CFE	Coefficient of viscous damping at each station in ξ direction
27	CZ	Coefficient of viscous damping in normal direction.
28	SKFE	Spring constants of shell under elastic restraint in ξ direction.
29	SKZ	Spring constant at each station in normal direction.
30	SUM	Fourier summing increment (always -1.)

For most
cases set
to 1.0

DECRD Index	Name	Description
33	TFI	(Always - 1)
34	VIN	Initial impact velocity, in./sec.
36	RESTR.	0. for start from zero, 1. for restart
4440	EM1	See description of top boundary conditions in Section 4.5.1
4476	EM1N	See description of bottom boundary conditions in Section 4.5.2

Last card must have a - sign in Column 1.

4.5 Boundary Conditions

4.5.1 Top Boundary

When the boundary conditions on the top boundary are of the following kind, a special flag can be used to specify them:

free: $\left(N_{\xi} = \hat{N}_{\xi\theta} = \hat{F}_{\xi} = M_{\xi} = 0 \right) = 1.$

roller: $\left(N_{\xi} = u_{\theta} = W = M_{\xi} = 0 \right) = 2.$

fixed: $\left(u_{\xi} = u_{\theta} = W = \phi_{\xi} = 0 \right) = 3.$

simply supported: $\left(u_{\xi} = u_{\theta} = W = M_{\xi} = 0 \right) = 4.$

complete: $\left(u_{\xi} = u_{\theta} = \hat{F}_{\xi} = \phi_{\xi} = 0 \right) = 5.$

In these cases, DA(4440) = 1. E10, and DA(4441) is given the value 1., 2., 3., 4., or 5. as shown above. Other special boundary conditions may also be specified. As an example, the full boundary (which is also given above) can be specified as shown in the following data sheets.

FORTRAN FIXED 10 DIGIT DECIMAL DATA

DECK NO.	PROGRAMMER	DATE	PAGE	of	DESCRIPTION	DO NOT KEY PUNCH
1						
13	4 4 4 0				Diagonal Boundary Force Matrix	
25	1 .				EMI (4 × 4), omega at top of shell.	
37						
49					e.g. (free boundary)	$\begin{bmatrix} 1 & & & \\ & 1 & & \\ & & 1 & \\ & & & 0 \end{bmatrix}$
61						
1					EXAMPLE,	
13	4 4 4 5				EMI (contd)	
25	1 .					
37						
49						
61						
1	4 4 5 0				EXAMPLE	
13	1 .				EMI (contd)	
25						
37						
49						
61						

FORTRAN FIXED IO DIGIT DECIMAL DATA

DECK NO. _____ PROGRAMMER _____ DATE _____ PAGE _____ of _____

NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
1		Diagonal Boundary Displacement Matrix	
13		EM3(4 × 4) Lambda at top of shell	
25			
37			
49		e.g. (for free boundary) $\begin{bmatrix} 0 & & & \\ & 0 & & \\ & & 0 & \\ & & & 1 \end{bmatrix}$	
61			
1		EXAMPLE	
13		EM3 (cont'd)	
25			
37			
49			
61			
1		Column Boundary Matrix	
13		EM5(4 × 1), L, at top of shell.	
25			
37		e.g. $L = \begin{Bmatrix} 0 \\ 0 \\ 0 \\ 0 \end{Bmatrix}$	
4			
61			

4.5.2 Bottom Boundary

The same selection of boundary conditions is available here as for the top boundary. This time, the indicator specifying the free, roller, fixed, simply supported, and complete conditions are set as follows:

$$DA (4476) = 1.E10$$

$$DA (4477) = 1., 2., 3., 4., 5.,$$

according to the boundary condition desired. An example of other possible boundary conditions is given in the data sheets below. The example here is the free boundary (the same as in Section 4.5.1).

FORTRAN FIXED IO DIGIT DECIMAL DATA

DECK NO.	PROGRAMMER	DATE	PAGE	of	DESCRIPTION	DO NOT KEY PUNCH
1	4 4 7 6				Diagonal Boundary Force Matrix	
13	0 • 0				EMIN(4 × 4) OMEGA at Bottom of shell.	
25						
37						
49					e.g. (fixed boundary)	$\begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix}$
61						$\begin{bmatrix} 4476 \\ 15 \\ 4491 \end{bmatrix}$
1	4 4 9 1				EXAMPLE	
13					EMIN (cont.'d)	
25	1 • 0					
37						
49						
61						
1	4 4 9 2				Diagonal Boundary Displacement Matrix	
13	1 • 0				EMIN(4 × 4), LAMBDA at Bottom of shell.	
25						
37					e.g. (for fixed case),	$\begin{bmatrix} 1 \\ 1 \\ 1 \\ 0 \end{bmatrix}$
49						
61						

FORTRAN FIXED IO DIGIT DECIMAL DATA

DECK NO.	PROGRAMMER	DATE	PAGE	of	DESCRIPTION	DO NOT KEY PUNCH
1					EXAMPLE	
13	4 4 9 7				EM3N (cont'd)	
25	1 • 0					
37						
49						
61						
1					EM3N (cont'd)	
13	4 5 0 2					
25	1 •					
37						
49						
61						
1					Column Boundary Matrix	
13	4 5 0 5				EM5N (4 × 1), L, at Bottom of shell.	
25	0 • 0					
37					e.g. $L = \begin{Bmatrix} 0 \end{Bmatrix}$	
49						
61						

4.6 Call DECRD (GDA)

DECRD Index	Name	Description
1	GMI	Geometry indicator: 1. = cone - cylinder 2. = sphere - toroid 3. = general discrete point 4. = arbitrary functions
2	EN	No. of station points
3	PFLAG	print indicator; $\neq 0.$, prints all data
4	RA1	for GMI = 1.; radius at station 1
	RC	for GMI = 2.; radius of curvature
5	AXL	for GMI = 1.; axial surface length
	ROFF	for GMI = 2.; off-set distance to center of curvature
6	ANX	for GMI = 1.; angle between generator and axis of revolution.
	PHIO	for GMI = 2.; initial opening angle from vertical axis, in degrees.
7	PHIN	for GMI = 2.; final opening angle from vertical axis, in degrees.
8	EM	for GMI = 3.; number of RI points given
9-208	RIPT	for GMI = 3.; Discrete radii (200 points maximum)
209-409	XIPT	for GMI = 3.; Discrete XI - arc lengths, (200 points maximum)

The last card must have a - in Column 1.

4.7 Call DECRD (CDA)

The various tables are set up in this region as follows:

TAB (1) = No. of stations given along meridian (i. e. , stations at which values change).

TAB (2) = Station No. 1.

TAB (3) = Parameter value at Station No. 1

TAB (4) = Next station no.

TAB (5) = Next parameter value

Stations and parameter values interlaced.

The last station must be the Nth station parameter value because CODIMA interpolation routine will not extrapolate.

If $+1.0 \times 10^{10}$ is placed in TAB (1) the following parameter value is constant (uniform over all stations EN) and its value is placed in TAB (2).

DECRD Index	Name	Description
		<u>Extensional Rigidity</u>
1	DB	No. of stations given if = 1. E10, then a constant extensional rigidity is given in 2
2		Station No. 1 if CDA (1) = 1. E10, then this is a constant value of extensional rigidity.
3		Value of extensional rigidity between Station 1 and next station
4		Station No. 2
5		Value of extensional rigidity
6-41		Follows same pattern to DTB (20), value of last rigidity.

DFCRD Index	Name	Description
		<u>Flexural Rigidity</u>
42	EXTB	No. of stations given if = 1. E10, then a constant flexural rigidity is given in 43
43		Station No. 1 if CDA (42) = 1. E10, then this is the constant value of flexural rigidity
44		Value of flexural rigidity between station 1 and next station
45		Station No. 2
46		Value of flexural rigidity
47-81		Follows same pattern to EXTB (20), value of last rigidity.
		<u>Continue as above for the following quantities:</u>
83-123	EITB	Young's modulus (E)
124-164	ALFTB	Coefft of thermal expansion (α)
165-205	DNATB	1/2 shell thickness (h/2)
206-246	TTB	Temperature gradient through shell (T)
247-287	ENTB	Membrane thermal load

DECRD Index	Name	Description
288-328	EMTB	Bending thermal load
329-369	PNTB	Normal pressure on shell (at reference surface)
370-410	PFETB	Meridional surface pressure (at reference surface)
452-492	DZOTB	Initial displacement in normal direction.
493-533	VZOTB	Initial velocity in normal direction
534-574	QZOTB	Initial acceleration in normal direction
575-615	DFOTB	Initial displacement in ξ direction
616-665	VFOTB	Initial velocity in ξ direction.
657-691	QFOTB	Initial acceleration in ξ direction.

The last card must have a - sign in Column 1.

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5.1 SAMPLE PROBLEM

To demonstrate the use of the computer program, and to illustrate the format of the input and output data, the sample problem shown in Figure 6 has been calculated.

The problem concerns the vertical impact of a flexible body of revolution consisting of a shallow spherical shell to which is rigidly attached a heavier mass so that their combined weight is 10,000 lbs. The radius of curvature of the shell middle surface is 175.6 ins., and the opening angle is 19.53°. The shell extensional and flexural stiffnesses are both set equal to 3.33×10^6 lbs/in., which corresponds to a sandwich shell having 0.05 in. steel facings and 1.95 in. honeycomb core. Other shell properties are as follows: Mass per unit surface area = 9.7×10^{-4} lbs. sec.²/in.³; Poisson's ratio = 0.33, and modulus of elasticity $E = 29.7 \times 10^6$ psi. The initial impact velocity is 30 fps.

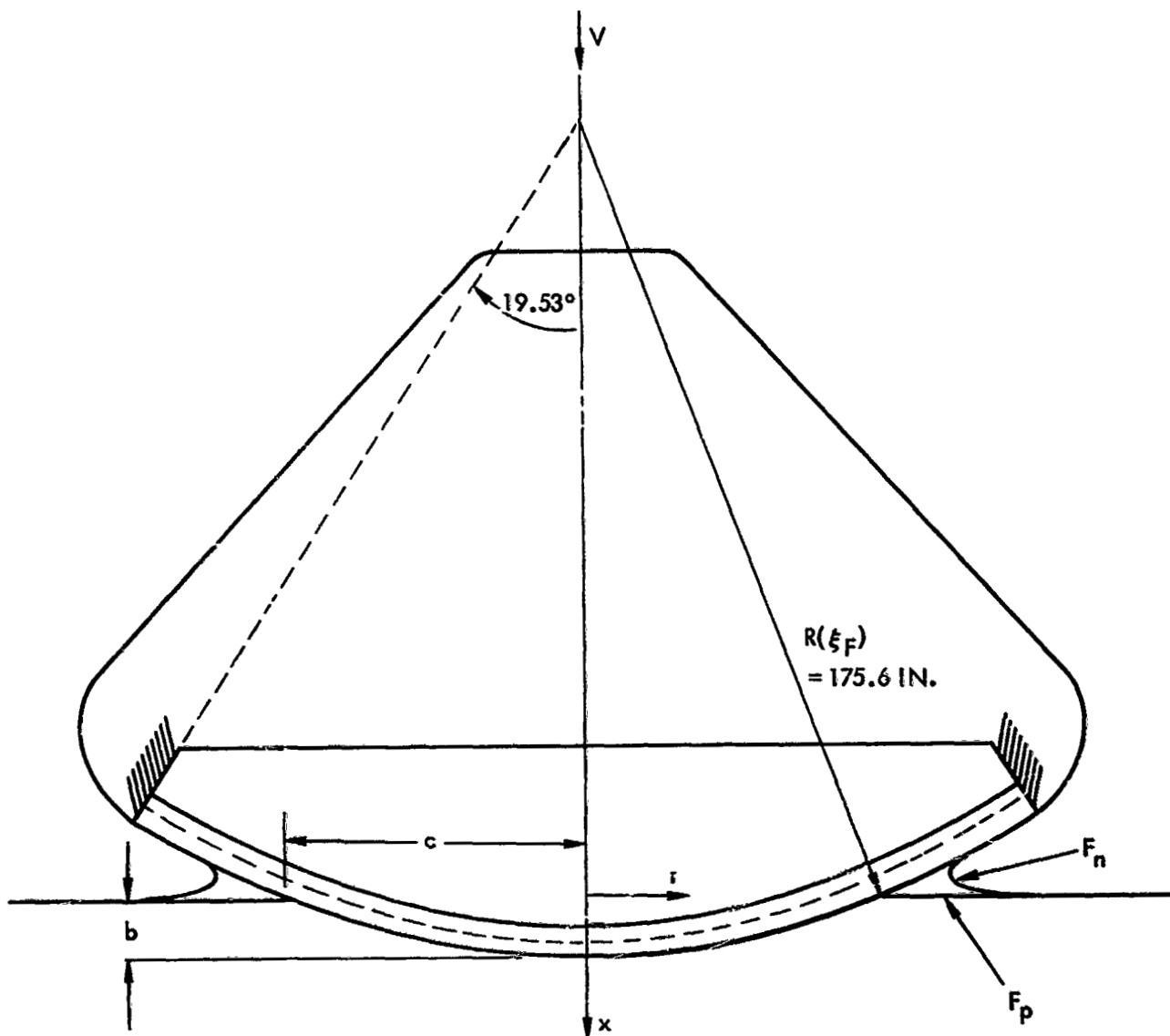


Figure 6. Model of Sample Problem.

5.2 Sample Input Data and Tape Usage

Because of the amount of computer time consumed in a single hydro-elastic computer run, it is well to split the total run into small subsections in order to be able to progressively check the output data as it is calculated. This is done by restarting the problem at various times as described in Section 3.1 on tape manipulations.

The present sample problem will be run to 2.0 ms, (although a usual run would be in the order of 8 to 15 ms.). It will be run in two sections; the first, a start from zero, from 0 to 1.0 ms; and the second, a restart, from 1.0 ms. to 2.0 ms. The time increment (TAU1/ENT1) was chosen as .1 ms, and the convergence criterion was chosen as .01, meaning that the pressure at the last iteration should be within 1% of that of the previous iteration.

Sample input sheets for the start from zero are shown below.

The symbols have the following meaning:

NSTART		0 for a start from zero
		1 for a restart
NSAVE		0 when no data will be saved
		1 when data will be saved for a future restart
NINT		Total no. of time intervals already computed: (= 0 for a start from zero)
KODER2		Tape codes (See Section 3.1)
KODES2		
RHO		Mass density of fluid in lbs. /cu. ft.
WT		Weight of vehicle in lbs.
INDER		Always = 1
CONV		Convergence criterion (see Section 1.3)
IVX		Maximum allowable no. of iterations per time cycle (see Section 1.3)
ICYL		= 0, always

All other symbols have been discussed in Section 4.

EDPM JOB REQUEST SUPPLEMENT

JOB NO. _____ REQUESTED BY _____ PHONE _____

ADDITIONAL INSTRUCTIONS

MOUNT ANY AVAILABLE TAPE ON LOGICAL UNIT 8

PUT FILE RING IN

MOUNT ANY AVAILABLE TAPE ON LOGICAL UNIT 9

PUT FILE RING IN

☐ SEE BACK OF FORM

TAPE USAGE

AUTH NO. _____ NAME _____
 JOB NO. _____ DATE _____
 PHONE _____ DEPT _____ GROUP _____

UNIT	REEL NO.	TAPE	DESCRIPTION	MINIMUM LENGTH	RESERVE	FILE	THIS TAPE	RETURN	WITHDRAWN TAPE	RELEASE	RESERVE TAPE	WITHDRAW UNRE-	SERVED TAPE	WITHDRAW	RESERVED TAPE
					THIS TAPE	THIS TAPE	THIS TAPE	THIS TAPE	THIS TAPE	THIS TAPE	THIS TAPE	THIS TAPE	THIS TAPE	THIS TAPE	THIS TAPE
8	A	10	Saved data at 1.0 ms.		✓										
9	B	11	Response 0 - 1.0 ms.		✓										

Start from zero time and run at
increment $t = .1$ ms to 1.0 ms.

FORTRAN FIXED IO DIGIT DECIMAL DATA

DECK NO.	PROGRAMMER	DATE	PAGE	of
NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH	
1	0	NSTART		
13	1	NSAVE		
25	0	NINT		
37	0	KODER2		
49	1	KODES2		
61				
1				
13				
25				
37				
49				
61				
1				
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37				
49				
61				
1				
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25				
37				
49				
61				

FORTRAN FIXED IO DIGIT DECIMAL DATA

DECK NO. _____ PROGRAMMER _____ DATE _____ PAGE _____ of _____

NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
1 T I T L E	73 80		
13			
25			
37			
49			
61			
1 6 2 . 5	73 80	RHO	
13 1 0 0 0 0 . 0		WT	
25			
37			
49			
61			
1 1	73 80	INDER	
13 0 . 0 1		CONV	
25 2 . 5		IVX	
37 0		ICYL	
49			
61			

FORTRAN FIXED IO DIGIT DECIMAL DATA

DECK NO. _____ PROGRAMMER _____ DATE _____ PAGE _____ of _____

NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
1			
13			
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37			
49			
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61			
1			
13			
25			

FORTRAN FIXED IO DIGIT DECIMAL DATA

DECK NO. _____ PROGRAMMER _____ DATE _____ of _____ PAGE _____ of _____

NUMBER		IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH	
1	2	73 80			
13					
25					
37					
49					
61	9 7 5 - 3		MASS		
1	3 0	73 80			
13	- 1 •			SUM	
25					
37					
49					
61					
1	3 3	73 80			
13	- 1 •			TFI	
25	3 6 0 •			VIN	
37					
49	0 • 0			RESTR	
61					

FORTRAN FIXED 10 DIGIT DECIMAL DATA

DECK NO. _____ PROGRAMMER _____ DATE _____ PAGE _____ of _____

NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
1	4 4 7 6		
13	1 0 + 1 0	EMIN	
25	3 0 0	EM3N	
37			
49			
61			
1	1		GDA
13	2 0 0	GMI	
25	1 2 0 0	EN	
37	- 1 0 0	PFLAG	
49	1 7 5 6	RC	
61	0 0 0	ROFF	
1	6		
13	0 0 0	PHIC	
25	1 9 5 3 0	PHIN	
37			
49			
61			

FORTKAN FIXED 10 DIGIT DECIMAL DATA

DECK NO. _____ PROGRAMMER _____ DATE _____ PAGE _____ of _____

NUMBER		IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
1	1	73 80		CDA
15	1 • 0 + 1 0		DTB	
25	3 • 3 3 + 6			
37				
49				
61				
1	4 2	73 80		
13	1 • 0 + 1 0		EKTB	
25	3 • 3 3 + 6			
37				
49				
61				
1	8 3	73 80		
13	1 • 0 + 1 0		EITR	
25	2 9 • 7 + 6			
37				
49				
61				

FORTRAN FIXED 10 DIGIT DECIMAL DATA

DECK NO.	PROGRAMMER	DATE	PAGE	of	DESCRIPTION	DO NOT KEY PUNCH
1						
13						
25						
37						
49						
61						
1						
13						
25						
37						
49						
61						
1						
13						
25						
37						
49						
61						

DNATB

73

80

73

80

73

80

5.3 Sample Data and Tape Usage for the Restart

In order to restart the problem at 1.0 ms., the following input is required. Note that the time interval must be the same in all runs.

The output quantities will be identical to those from the start from zero.

EDPM JOB REQUEST SUPPLEMENT

JOB NO. _____ REQUESTED BY _____ PHONE _____

ADDITIONAL INSTRUCTIONS

MOUNT ANY AVAILABLE TAPE ON LOGICAL UNIT 8
PUT FILE RING IN

MOUNT ANY AVAILABLE TAPE ON LOGICAL UNIT 9
PUT FILE RING IN

MOUNT TAPE A ON LOGICAL UNIT 12

MOUNT TAPE B ON LOGICAL UNIT 13

☐ SEE BACK OF FORM

TAPE USAGE

AUTH NO. _____ NAME _____
JOB NO. _____ DATE _____
PHONE _____ DEPT _____ GROUP _____

UNIT	REEL NO.	TAPE ID	DESCRIPTION	MINIMUM LENGTH	RESERVE THIS TAPE	FILE THIS TAPE	RETURN WITHDRAWN TAPE	RELEASE RESERVE TAPE	WITHDRAW UNRESERVED TAPE	WITHDRAW RESERVED TAPE
8	C	20	Saved data at 2.0 ms		✓					
9	D	21	Response 0 - 2.0 ms		✓					
12	A	10	Saved data at 1.0 ms					✓		
13	B	11	Response 0 - 1.0 ms					✓		

FORTRAN FIXED IO DIGIT DECIMAL DATA

Changes are denoted by
ar

DECK NO. _____ PROGRAMMER _____ DATE _____ PAGE _____ of _____

NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
1	1	NSTART	←
13	1	NSAVE	
25	1 0	NINT	←
37	1 0	KODER2	←
49	1 1 73 80	KODES2	←
61			
1			←
13			
25			
37			
49	73 80		
61			
1			
13			
25			
37			
49			
61			
1			
13			←
25			
37			
49			
61			

FORTRAN FIXED 10 DIGIT DECIMAL DATA

DECK NO. _____ PROGRAMMER _____ DATE _____ PAGE _____ of _____

NUMBER		IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
1	T I T L E		←	
13				
25				
37				
49		73		
61		80		
1	6 2 . 5		RHO	Same
13	1 0 0 0 0 . 0		WT	
25				
37				
49		73		
61		80		
1	1		INDER	Same
13	0 . 0 1		CONV	
25	2 5		IVX	
37	0		ICYL	
49		73		
61		80		

FORTRAN FIXED IO DIGIT DECIMAL DATA

DECK NO. _____ PROGRAMMER _____ DATE _____ PAGE _____ of _____

NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
1			Same
13		AO	
25		HO	
37		EO	
49		SIG	
61		INFO	
1			Same
13		ENFL	
25		POI	
37		THETA	
49		PIXI	
61			
1			
13		TAUL	←
25		ENTI	←
37		PII	
49			
61			

FORTRAN FIXED 10 DIGIT DECIMAL DATA

DECK NO. _____ PROGRAMMER _____ DATE _____ PAGE _____ of _____

NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
1			Same
13			
25			
37			
49			
61			
1		MASS	
13			Same
25		SUM	
37			
49			
61			
1			
13		TFI	
25		VIN	
37			
49		RESTART	←
61		PUNCH	

FORTRAN FIXED 10 DIGIT DECIMAL DATA

DECK NO. _____ PROGRAMMER _____ DATE _____ PAGE _____ of _____

NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
1 -			Same
13 1 . 0		EMIN	
25 + 1 0		EM3N	
37 3 . 0			
49	73		
61	80		
1 1			Same
13 2 . 0		GMI	
25 1 2 0 . 0		EN	
37 - 1 . 0		PFLAG	
49 1 7 5 . 6	73	RA1, RC	
61 0 . 0	80	AXL, ROFF	
1 -			Same
13 0 . 0		ANX, PHIO	
25 1 9 . 5 3 0		PHIN	
37			
49	73		
61	80		

FORTRAN FIXED 10 DIGIT DECIMAL DATA

DECK NO.	PROGRAMMER	DATE	PAGE	of	DESCRIPTION	DO NOT KEY PUNCH
1	1					Same
13	1 . 0 + 1 0				DTB	
25	3 . 3 3 + 6					
37						
49						
61						
1	4 2					Same
13	1 . 0 + 1 0				EKTB	
25	3 3 3 6					
37						
49						
61						
1	8 3					Same
13	1 . 0 + 1 0				EITB	
25	2 9 . 7 + 6					
37						
49						
61						

FORTRAN FIXED IO DIGIT DECIMAL DATA

DECK NO. _____ PROGRAMMER _____ DATE _____ PAGE _____ of _____

NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
1			Same
13		DI/ATB	
25			
37			
49			
61			
1			
13			
25			
37			
49			
61			
1			
13			
25			
37			
49			
61			

5.4 Sample Output

The following pages show the output resulting from the start from zero of the sample problem. Letters in circles correspond to descriptions below.

- (A) First Title Card
- (B) Second Title card
- (C) Third Title card
- (D) No. of Stations EN
- (E) Radius of curvature, ins.
- (F) Offset distance from center of curvature = 0
- (G) Closed apex, therefore PHIO initial opening angle is zero
- (H) PHIN, final opening angle is 19.53°
- (I) Station number
- (J) R(I), normal distance from shell to axis
- (K) W(THETA) nondimensional curvature in θ direction
- (L) W(XI) nondimensional curvature in ξ direction
- (M) RHOX(I) $R(I)/AO = \rho/AO$
- (N) GAMMA (I) ρ'/ρ
- (O) DTB, the extensional rigidity (constant over shell)
- (P) EKTB, the flexural rigidity (constant over shell)
- (Q) EITB, the Young's modulus (constant over shell)
- (R) ALFTB, thermal expansion coefficient (zero)

- Ⓢ DNATB, 1/2 shell thickness (constant over shell)
- Ⓣ TTB, temperature gradient (zero)
- Ⓤ ENTB, membrane thermal load (zero)
- Ⓥ EMTB, bending thermal load (zero)
- Ⓦ All these other quantities, read by CDR, are set to zero.
- ⓧ See Sections 4.4 to 4.7 for descriptions

EN = number of stations

AO = reference length

HO = Reference thickness

EO = Reference Young's modulus

SIGO = Reference stress level

ENFO = always zero

ENFL = always zero

POI = Poisson's ratio

THETA = always zero

PIXI = always zero

SPRL = location of spring along meridian

UK = spring value in ξ direction

VK = always zero

WK = spring value in normal direction

EMK = always zero

TAU1 = total length of time from zero

ENTI	= Total no. of time intervals from zero to TAU1
PI1	= point interval. Here PI1 = 1, and output is pointed at end of each interval
TAU2	= 0
ENT2	= 0
PI2	= 0
TAU3	= 0
ENT3	= 0
PI3	= 0
	(always zero)
MASS	= mass density
CFE	= coefficient of viscous damping at each station in ξ direction
CZ	= coefficient of viscous damping at each station in normal direction.
SKFE	= spring constant of shell under elastic restraint in ξ direction
SUM	= -1. always
EN1	= 1., open shell; = 2., closed shell; set in GEOM
DEL	= distance between station points
BCITP	= boundary condition indicator - top boundary
BCIBM	= boundary condition indicator - bottom boundary
Y	Full Tables of
D	Extensional rigidity
EK	Flexural rigidity
E1	Young's modulus
ALF	Coefficient of thermal expansion (zero here)

DNA . 1/2 shell thickness

T temperature gradient through shell (zero here)

ENT membrane thermal load (zero here)

EMT Bending thermal load (zero here)

(Z) Full Tables of

PN, PFE, DZO, VZO, AZO, DFO, VFO, AFO, all of which were read as zero in CDA. [See Section 4.7 for their descriptions].

(AA) This page is a diagnostic output which is made during each cycle in order to check the manner in which the iterations (described in Section 1.3) are made. Each row is denoted by a numeral in a circle (1) to (10). Column (AB) denotes the pressure component at the apex computed from the second term (the summation) of Equation 1 of Section 1.3.

Column (AC) denotes an intermediate average pressure at the apex derived from Column (AB) during each iteration. Column (AD) denotes the total pressure at the apex of the shell after each iteration. Column (AE) denotes the velocity of the shell after each iteration.

Element [(AE), (1)] is zero because this is the first calculation from an initial condition of zero. Rows (2) through (10) follow from each individual iteration. It is seen that for this time cycle there are a total of 9 iterations.

- Ⓐ is self-explanatory. It shows the time (t), maximum radius of the pressure profile (c), overall vehicle velocity (V), overall acceleration of the center of gravity (A), and depth of penetration (b).
- Ⓑ is a column showing the station number from the apex (1) to the boundary (120).
- Ⓒ is a column of the total pressure acting at each station point. Because the maximum radius of the wetted surface is 3.56 ins., and the distance between each station point (DEL, see ⓧ) is .503 ins., the wetted surface only extends to station 8. Beyond this station, no pressure is applied. Note that the maximum pressure always occurs at the edge of the wetted surface, in this case at station 8.
- Ⓓ is a column of pressures derived from the first term of Equation 1 of Section 1.3. Because they depend only on the overall velocity v, they have been here called the rigid-body components of pressure.
- Ⓔ is a column of pressures derived from the second term of Equation 1 of Section 1.3. They are called the elastic components because they also depend on the structural velocities.
- Ⓕ This page contains columns of response output. The columns are as follows:

I	Station points along shell meridian
U(I)	Tangential displacement (ins) of middle surface in ξ direction
V(I)	Tangential displacement of middle surface in θ direction. Here zero because problem is axially symmetric.
W(I)	Transverse displacement (ins.) of middle surface (positive outward).
M(PHI)	Meridional bending moment M_ξ (in lbs/in.)
M(THETA)	Circumferential bending moment M_θ (in lbs/in.)
M(PHI, THETA)	Twisting moment $M_{\xi\theta}$. Zero here because problem is axially symmetric.
Q(PHI)	Shear force Q_ξ (lbs/in.)
Q(THETA)	Shear force Q_θ . Zero here because problem is axially symmetric.
ⒹA	Additional columns of response.
I	Station point along meridian
N(PHI)	Meridional membrane force N_ξ (lbs/in.)
N(THETA)	Circumferential membrane force N_θ (lbs/in.)
N(PHI, THETA)	Twisting force $N_{\xi\theta}$. Zero here because problem is axially symmetric.
SIG(PHI)	Stress σ_ξ (psi) on outer fiber of shell.
SIG(THETA)	Stress σ_θ (psi) on outer fiber of shell.
SIG(PHI, THETA)	Stress $\sigma_{\xi\theta}$ on outer fiber of shell. Zero here because problem is axisymmetric.
ⒺA	Additional columns of response.

VEL(U)	Tangential velocity in ξ direction (ins. /sec.)
VEL(V)	Tangential velocity in θ direction. Zero here because problem is axially symmetric
VEL(W)	Transverse velocity (ins. /sec.), positive in outward direction.
ACC(U)	Tangential acceleration in ξ direction (ins. /sec. ²)
ACC(V)	Tangential acceleration in θ direction (ins. /sec. ²).
ACC(W)	Transverse acceleration (ins. /sec. ²), positive in outward direction.
ⒻA	The above output of the response quantities ⒶA to ⒺA is repeated with each time cycle. After a complete run these output quantities will be stored also on a tape as described in Section 3. 1. The appropriate KODES of each reserve tape are pointed at the end of all the output. In this case, the symbols have the following meanings. For a start from zero, see Table 2, for a restart, see Table 3.

KODE	ID	Tape Description
KODER1	10	Tape containing response at 1.0 ms
KODER2	0	Here a dummy tape
KODES1	1	Here a dummy tape
KODES2	11	Tape containing saved data for a restart

Table 2. KODES for a start from zero

KODE	ID	Tape Description
KODER1	10	Tape containing response at 1.0 ms.
KODER2	20	Tape containing response at 2.0 ms.
KODES1	11	Tape containing saved data at 1.0 ms.
KODES2	21	Tape containing saved data at 2.0 ms for a future restart.

Table 3. KODES for a restart

- (A) HYDROELASTIC RESPONSE APOLLO SPHERE ** FIXED BND.- P(N) IN ANALYTIC FORM
- (B) 5 ITERATIONS TO 0.5 MS ** POI=.33, EN=120., RHO=.000975
- (C) OPEN ANGLE=19.53, D=3.33E+6, K=3.33E+6, E=29.7E+6, DNA=1.025IN, RC=175.6

GEOMETRY DATA FOR REGION... (SPHERE - TOROID)

(D) NUMBER OF STATIONS - 120		(F) ROFF = 0.0000E-39		(G) PHIO = 0.0000E-39		(H) PHIN = 1.9530E 01	
(I) I	(J) R(I)	(K) W(THETA)	(L) W(XI)	(M) RHOX(I)	(N) GAMMA(I)		
1	0.0000000E-39	5.6947608E-03	5.6947608E-03	0.0000000E-39	1.0000000E 10		
2	5.0298677E-01	5.6947608E-03	5.6947608E-03	5.0298677E-01	1.9881132E 00		
3	1.0059694E 00	5.6947608E-03	5.6947608E-03	1.0059694E 00	9.9404847E-01		
4	1.5089438E 00	5.6947608E-03	5.6947608E-03	1.5089438E 00	6.6268992E-01		
5	2.0119058E 00	5.6947608E-03	5.6947608E-03	2.0119058E 00	4.9700793E-01		
6	2.5148512E 00	5.6947608E-03	5.6947608E-03	2.5148512E 00	3.9759653E-01		
7	3.0177760E 00	5.6947608E-03	5.6947608E-03	3.0177760E 00	3.3132047E-01		
8	3.5206761E 00	5.6947608E-03	5.6947608E-03	3.5206761E 00	2.8397889E-01		
9	4.0235473E 00	5.6947608E-03	5.6947608E-03	4.0235473E 00	2.4847133E-01		
10	4.5263854E 00	5.6947608E-03	5.6947608E-03	4.5263854E 00	2.2085313E-01		
11	5.0291864E 00	5.6947608E-03	5.6947608E-03	5.0291864E 00	1.9875748E-01		
12	5.5319462E 00	5.6947608E-03	5.6947608E-03	5.5319462E 00	1.8067824E-01		
13	6.0346605E 00	5.6947608E-03	5.6947608E-03	6.0346605E 00	1.6561129E-01		
14	6.5373253E 00	5.6947608E-03	5.6947608E-03	6.5373253E 00	1.5286151E-01		
15	7.0399365E 00	5.6947608E-03	5.6947608E-03	7.0399365E 00	1.4193236E-01		
16	7.5424901E 00	5.6947608E-03	5.6947608E-03	7.5424901E 00	1.3245968E-01		
17	8.0449816E 00	5.6947608E-03	5.6947608E-03	8.0449816E 00	1.2417040E-01		
18	8.5474072E 00	5.6947608E-03	5.6947608E-03	8.5474072E 00	1.1685570E-01		
19	9.0497625E 00	5.6947608E-03	5.6947608E-03	9.0497625E 00	1.1035314E-01		
20	9.5520437E 00	5.6947608E-03	5.6947608E-03	9.5520437E 00	1.0453448E-01		
21	1.0054246E 01	5.6947608E-03	5.6947608E-03	1.0054246E 01	9.9297155E-02		
22	1.0556367E 01	5.6947608E-03	5.6947608E-03	1.0556367E 01	9.4558103E-02		
23	1.1058400E 01	5.6947608E-03	5.6947608E-03	1.1058400E 01	9.0249382E-02		
24	1.1560343E 01	5.6947608E-03	5.6947608E-03	1.1560343E 01	8.6314849E-02		
25	1.2062191E 01	5.6947608E-03	5.6947608E-03	1.2062191E 01	8.2707722E-02		
26	1.2563940E 01	5.6947608E-03	5.6947608E-03	1.2563940E 01	7.9388759E-02		
27	1.3065586E 01	5.6947608E-03	5.6947608E-03	1.3065586E 01	7.6324672E-02		
28	1.3567125E 01	5.6947608E-03	5.6947608E-03	1.3567125E 01	7.3487151E-02		
29	1.4068553E 01	5.6947608E-03	5.6947608E-03	1.4068553E 01	7.0851913E-02		
30	1.4569865E 01	5.6947608E-03	5.6947608E-03	1.4569865E 01	6.8398048E-02		
31	1.5071057E 01	5.6947608E-03	5.6947608E-03	1.5071057E 01	6.6107434E-02		
32	1.5572126E 01	5.6947608E-03	5.6947608E-03	1.5572126E 01	6.3964210E-02		
33	1.6073067E 01	5.6947608E-03	5.6947608E-03	1.6073067E 01	6.1954599E-02		
34	1.6573876E 01	5.6947608E-03	5.6947608E-03	1.6573876E 01	6.0066465E-02		
35	1.7074549E 01	5.6947608E-03	5.6947608E-03	1.7074549E 01	5.8289090E-02		

36	1.7575083E 01	5.6947608E-03	5.6947608E-03	1.7575083E 01	5.6612959E-02
37	1.8075472E 01	5.6947608E-03	5.6947608E-03	1.8075472E 01	5.5029624E-02
38	1.8575712E 01	5.6947608E-03	5.6947608E-03	1.8575712E 01	5.3531597E-02
39	1.9075800E 01	5.6947608E-03	5.6947608E-03	1.9075800E 01	5.2112132E-02
40	1.9575732E 01	5.6947608E-03	5.6947608E-03	1.9575732E 01	5.0765160E-02
41	2.0075503E 01	5.6947608E-03	5.6947608E-03	2.0075503E 01	4.9485280E-02
42	2.0575110E 01	5.6947608E-03	5.6947608E-03	2.0575110E 01	4.8267571E-02
43	2.1074547E 01	5.6947608E-03	5.6947608E-03	2.1074547E 01	4.7107559E-02
44	2.1573812E 01	5.6947608E-03	5.6947608E-03	2.1573812E 01	4.6001273E-02
45	2.2072900E 01	5.6947608E-03	5.6947608E-03	2.2072900E 01	4.4945026E-02
46	2.2571806E 01	5.6947608E-03	5.6947608E-03	2.2571806E 01	4.3935454E-02
47	2.3070527E 01	5.6947608E-03	5.6947608E-03	2.3070527E 01	4.2969562E-02
48	2.3569060E 01	5.6947608E-03	5.6947608E-03	2.3569060E 01	4.2044541E-02
49	2.4067398E 01	5.6947608E-03	5.6947608E-03	2.4067398E 01	4.1157818E-02
50	2.4565540E 01	5.6947608E-03	5.6947608E-03	2.4565540E 01	4.0307058E-02
51	2.5063479E 01	5.6947608E-03	5.6947608E-03	2.5063479E 01	3.9490103E-02
52	2.5561213E 01	5.6947608E-03	5.6947608E-03	2.5561213E 01	3.8705000E-02
53	2.6058737E 01	5.6947608E-03	5.6947608E-03	2.6058737E 01	3.7949885E-02
54	2.6556047E 01	5.6947608E-03	5.6947608E-03	2.6556047E 01	3.7223042E-02
55	2.7053140E 01	5.6947608E-03	5.6947608E-03	2.7053140E 01	3.6722899E-02
56	2.7550010E 01	5.6947608E-03	5.6947608E-03	2.7550010E 01	3.5848037E-02
57	2.8046654E 01	5.6947608E-03	5.6947608E-03	2.8046654E 01	3.5197090E-02
58	2.8543068E 01	5.6947608E-03	5.6947608E-03	2.8543068E 01	3.4568784E-02
59	2.9039249E 01	5.6947608E-03	5.6947608E-03	2.9039249E 01	3.3961948E-02
60	2.9535190E 01	5.6947608E-03	5.6947608E-03	2.9535190E 01	3.3375504E-02
61	3.0030890E 01	5.6947608E-03	5.6947608E-03	3.0030890E 01	3.2808419E-02
62	3.0526343E 01	5.6947608E-03	5.6947608E-03	3.0526343E 01	3.2259739E-02
63	3.1021546E 01	5.6947608E-03	5.6947608E-03	3.1021546E 01	3.1728597E-02
64	3.1516494E 01	5.6947608E-03	5.6947608E-03	3.1516494E 01	3.1214120E-02
65	3.2011183E 01	5.6947608E-03	5.6947608E-03	3.2011183E 01	3.0715557E-02
66	3.2505610E 01	5.6947608E-03	5.6947608E-03	3.2505610E 01	3.0232179E-02
67	3.2999770E 01	5.6947608E-03	5.6947608E-03	3.2999770E 01	2.9763259E-02
68	3.3493659E 01	5.6947608E-03	5.6947608E-03	3.3493659E 01	2.9308202E-02
69	3.3987274E 01	5.6947608E-03	5.6947608E-03	3.3987274E 01	2.8866366E-02
70	3.4480610E 01	5.6947608E-03	5.6947608E-03	3.4480610E 01	2.8437149E-02
71	3.4973663E 01	5.6947608E-03	5.6947608E-03	3.4973663E 01	2.8020337E-02
72	3.5466428E 01	5.6947608E-03	5.6947608E-03	3.5466428E 01	2.7614533E-02
73	3.5958903E 01	5.6947608E-03	5.6947608E-03	3.5958903E 01	2.7220150E-02
74	3.6451083E 01	5.6947608E-03	5.6947608E-03	3.6451083E 01	2.6836408E-02
75	3.6942964E 01	5.6947608E-03	5.6947608E-03	3.6942964E 01	2.6462874E-02
76	3.7434541E 01	5.6947608E-03	5.6947608E-03	3.7434541E 01	2.6099165E-02
77	3.7925812E 01	5.6947608E-03	5.6947608E-03	3.7925812E 01	2.5744906E-02
78	3.8416771E 01	5.6947608E-03	5.6947608E-03	3.8416771E 01	2.5399677E-02

79	3.8907415E 01	5.6947608E-03	5.6947608E-03	3.8907415E 01	2.5063158E-02
80	3.9397740E 01	5.6947608E-03	5.6947608E-03	3.9397740F 01	2.4735016E-02
81	3.9887742E 01	5.6947608E-03	5.6947608E-03	3.9887742E 01	2.4414950E-02
82	4.0377416E 01	5.6947608E-03	5.6947608E-03	4.0377416E 01	2.4102658E-02
83	4.0866759E 01	5.6947608E-03	5.6947608E-03	4.0866759E 01	2.3797824E-02
84	4.1355767E 01	5.6947608E-03	5.6947608E-03	4.1355767E 01	2.3500199E-02
85	4.1844435E 01	5.6947608E-03	5.6947608E-03	4.1844435E 01	2.3209540E-02
86	4.2332760E 01	5.6947608E-03	5.6947608E-03	4.2332760E 01	2.2925626E-02
87	4.2820738E 01	5.6947608E-03	5.6947608E-03	4.2820738E 01	2.2648142E-02
88	4.3308365E 01	5.6947608E-03	5.6947608E-03	4.3308365E 01	2.2376895E-02
89	4.3795635E 01	5.6947608E-03	5.6947608E-03	4.3795635E 01	2.2111716E-02
90	4.4282547E 01	5.6947608E-03	5.6947608E-03	4.4282547E 01	2.18527390E-02
91	4.4769096E 01	5.6947608E-03	5.6947608E-03	4.4769096E 01	2.1598657E-02
92	4.5255277E 01	5.6947608E-03	5.6947608E-03	4.5255277E 01	2.1350387E-02
93	4.5741087E 01	5.6947608E-03	5.6947608E-03	4.5741087E 01	2.1107409E-02
94	4.6226521E 01	5.6947608E-03	5.6947608E-03	4.6226521E 01	2.0869534E-02
95	4.6711577E 01	5.6947608E-03	5.6947608E-03	4.6711577E 01	2.0636598E-02
96	4.7196249F 01	5.6947608E-03	5.6947608E-03	4.7196249E 01	2.0408445E-02
97	4.7680534E 01	5.6947608E-03	5.6947608E-03	4.7680534E 01	2.0184935E-02
98	4.8164428E 01	5.6947608E-03	5.6947608E-03	4.8164428E 01	1.9965885E-02
99	4.8647925E 01	5.6947608E-03	5.6947608E-03	4.8647925E 01	1.9751217E-02
100	4.9131024E 01	5.6947608E-03	5.6947608E-03	4.9131024E 01	1.9540797E-02
101	4.9613720E 01	5.6947608E-03	5.6947608E-03	4.9613720E 01	1.9334451E-02
102	5.0096010E 01	5.6947608E-03	5.6947608E-03	5.0096010E 01	1.9132085E-02
103	5.0577888E 01	5.6947608E-03	5.6947608E-03	5.0577888E 01	1.8933564E-02
104	5.1059351F 01	5.6947608E-03	5.6947608E-03	5.1059351E 01	1.8738803E-02
105	5.1540396E 01	5.6947608E-03	5.6947608E-03	5.1540396E 01	1.8547656E-02
106	5.2021016E 01	5.6947608E-03	5.6947608E-03	5.2021016E 01	1.8360049E-02
107	5.2501211F 01	5.6947608E-03	5.6947608E-03	5.2501211E 01	1.8175906E-02
108	5.2980975E 01	5.6947608E-03	5.6947608E-03	5.2980975E 01	1.7995078E-02
109	5.3460304E 01	5.6947608E-03	5.6947608E-03	5.3460304E 01	1.7817498E-02
110	5.3939195E 01	5.6947608E-03	5.6947608E-03	5.3939195E 01	1.7643060E-02
111	5.4417642E 01	5.6947608E-03	5.6947608E-03	5.4417642E 01	1.7471686E-02
112	5.4895643E 01	5.6947608E-03	5.6947608E-03	5.4895643E 01	1.7303327E-02
113	5.5373195E 01	5.6947608E-03	5.6947608E-03	5.5373195E 01	1.7137860E-02
114	5.5850291E 01	5.6947608E-03	5.6947608E-03	5.5850291E 01	1.6975209E-02
115	5.6326930E 01	5.6947608E-03	5.6947608E-03	5.6326930E 01	1.6815315E-02
116	5.6803105E 01	5.6947608E-03	5.6947608E-03	5.6803105E 01	1.6658115E-02
117	5.7278816E 01	5.6947608E-03	5.6947608E-03	5.7278816E 01	1.6503547E-02
118	5.7754057E 01	5.6947608E-03	5.6947608E-03	5.7754057E 01	1.6351485E-02
119	5.8228823E 01	5.6947608E-03	5.6947608E-03	5.8228823E 01	1.6201908E-02
120	5.8703112E 01	5.6947608E-03	5.6947608E-03	5.8703112E 01	1.6054856E-02

[illegible]

34	0.00E-39	0.00E-39	0.00F-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39
35	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39
36	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39
37	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39
38	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39
39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39
40	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39
41	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39

(X)

INITIAL DATA

EN = 1.200E 02 AQ = 1.000E 00 HQ = 1.00E 00 EO = 1.000E 00
SIGO = 1.000E 00 ENFO = 0.000E-39 ENFL = 0.000E-39 POI = 3.300E-01
THETA = 0.000E-39 PIX1 = 0.000E-39 SPRL = 0.000E-39 UK = 0.000E-39
VK = 0.000E-39 WK = 0.000E-39 EMK = 0.000E-39 TAU1 = 5.000E-04
ENT1 = 5.000E 00 P11 = 1.000E 00 TAU2 = 0.000E-39 ENT2 = 0.000E-39
P12 = 0.000E-39 TAU3 = 0.000E-39 ENT3 = 0.000E-39 P13 = 0.000E-39
MASS = 9.750E-04 CFE = 0.000E-39 CZ = 0.000E-39 SKFE = 0.000E-39
SKZ = 0.000E-39 SUM = -1.000E 00 EN1 = 2.000E 00 DEL = 5.030E-01
BCITP = 0.000E-39 BCIBM = 3.000E 00

83

(Y)

	D	EK	F1	ALF	DNA	T	ENT	EMT
1	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39
2	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39
3	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39
4	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39
5	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39
6	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39
7	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39
8	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39
9	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39
10	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39
11	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39
12	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39
13	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39
14	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39
15	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39
16	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39
17	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39
18	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39
19	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39

- 84 -

110	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39
111	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39
112	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39
113	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39
114	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39
115	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39
116	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39
117	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39
118	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39
119	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39
120	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39	0.00E-39

(AB)

EL PRES

0.00000E-38
0.15770E 03
0.13935E 03
0.13465E 03
0.13257E 03
0.13141E 03
0.13069E 03
0.13020E 03
0.12984E 03

(AC)

AV EL PRES

0.00000E-38
0.78851E 02
0.99019E 02
0.10793E 03
0.11285E 03
0.11595E 03
0.11805E 03
0.11957E 03
0.12071E 03

(AD)

TOT PRES

-0.38140E 03
-0.30255E 03
-0.28238E 03
-0.27347E 03
-0.26855E 03
-0.26545E 03
-0.26335E 03
-0.26183E 03
-0.26069E 03

(AE)

SHELL VEL

0.00000E-38
-0.53046E 02
-0.46794E 02
-0.45191E 02
-0.44482E 02
-0.44089E 02
-0.43843E 02
-0.43674E 02
-0.43553E 02

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(AA)

WATER IMPACT PRESSURE LOADS

TIME =	0.10000000E-03SEC		
MAX RAD OF PRESSURE PROFILE =	0.35557278E 01INS		
VEHICLE VELOCITY =	0.360000000E 03INS/SEC		
VEHICLE ACCELERATION =	0.000000000E-38G		
DEPTH OF PENETRATION =	0.360000000E-01INS		
(BB) STATION	(EC) TOTAL PRESSURE	RIGID-BODY COMPONENT	ELASTIC COMPONENT
1	-0.2607E 03	-0.3814E 02	0.1207E 03
2	-0.2651E 03	-0.3853E 03	0.1202E 03
3	-0.2790E 03	-0.3976E 03	0.1187E 03
4	-0.3050E 03	-0.4212E 03	0.1162E 03
5	-0.3495E 03	-0.4626E 03	0.1131E 03
6	-0.4295E 03	-0.5395E 03	0.1100E 03
7	-0.6099E 03	-0.7212E 03	0.1113E 03
8	-0.9771E 03	-0.1090E 04	0.1127E 03
9	0.0000E-38		
10	0.0000E-38		
11	0.0000E-38		
12	0.0000E-38		
13	0.0000E-38		
14	0.0000E-38		
15	0.0000E-38		
16	0.0000E-38		
17	0.0000E-38		
18	0.0000E-38		
19	0.0000E-38		
20	0.0000E-38		
21	0.0000E-38		
22	0.0000E-38		
23	0.0000E-38		
24	0.0000E-38		

111	0.0000E-38
112	0.0000E-38
113	0.0000E-38
114	0.0000E-38
115	0.0000E-38
116	0.0000E-38
117	0.0000E-38
118	0.0000E-38
119	0.0000E-38
120	0.0000E-38

UNDRFLOW AT 26463 IN MQ

DEFLECTIONS AND INTERNAL LOADS, TIME = 1.0000E-04

I	U(I)	V(I)	W(I)	M(PHI)	M(THETA)	M(PHI, THETA)	Q(PHI)	Q(THETA)
1	7.2760E-12	0.0000E-39	-4.3462E-03	-8.5440E 02	-8.5440E 02	-0.0000E-39	1.1021E 00	-0.0000E-39
2	6.5491E-06	0.0000E-39	-4.3218E-03	-8.5384E 02	-8.5384E 02	0.0000E-39	2.2229E 00	0.0000E-39
3	1.2993E-05	0.0000E-39	-4.2486E-03	-8.5215E 02	-8.5215E 02	0.0000E-39	8.6606E 00	0.0000E-39
4	1.9204E-05	0.0000E-39	-4.1268E-03	-8.4591E 02	-8.4965E 02	0.0000E-39	2.5055E 01	0.0000E-39
5	2.5056E-05	0.0000E-39	-3.9567E-03	-8.2944E 02	-8.4125E 02	0.0000E-39	5.8265E 01	0.0000E-39
6	3.0421E-05	0.0000E-39	-3.7395E-03	-7.9320E 02	-8.2310E 02	0.0000E-39	1.2033E 02	0.0000E-39
7	3.5163E-05	0.0000E-39	-3.4778E-03	-7.2035E 02	-7.8732E 02	0.0000E-39	2.4116E 02	0.0000E-39
8	3.9135E-05	0.0000E-39	-3.1769E-03	-5.7292E 02	-7.1705E 02	0.0000E-39	4.8400E 02	0.0000E-39
9	4.2169E-05	0.0000E-39	-2.8473E-03	-2.7462E 02	-5.7889E 02	0.0000E-39	5.8030E 02	0.0000E-39
10	4.4212E-05	0.0000E-39	-2.5106E-03	-6.5196E 01	-4.5537E 02	0.0000E-39	4.3917E 02	0.0000E-39
11	4.5360E-05	0.0000E-39	-2.1811E-03	8.0480E 01	-3.4985E 02	0.0000E-39	3.2842E 02	0.0000E-39
12	4.5722E-05	0.0000E-39	-1.8683E-03	1.7914E 02	-2.6208E 02	0.0000E-39	2.4092E 02	0.0000E-39
13	4.5410E-05	0.0000E-39	-1.5781E-03	2.4264E 02	-1.9055E 02	0.0000E-39	1.7174E 02	0.0000E-39
14	4.4534E-05	0.0000E-39	-1.3141E-03	2.7974E 02	-1.3328E 02	0.0000E-39	1.1726E 02	0.0000E-39
15	4.3200E-05	0.0000E-39	-1.0776E-03	2.9710E 02	-8.8277E 01	0.0000E-39	7.4706E 01	0.0000E-39
16	4.1506E-05	-0.0000E-39	-8.6890E-04	2.9988E 02	-5.3434E 01	0.0000E-39	4.1855E 01	0.0000E-39
17	3.9541E-05	-0.0000E-39	-6.8730E-04	2.9212E 02	-2.7138E 01	0.0000E-39	1.6916E 01	0.0000E-39
18	3.7385E-05	-0.0000E-39	-5.3138E-04	2.7701E 02	-7.7823E 00	0.0000E-39	-1.5930E 00	0.0000E-39
19	3.5106E-05	-0.0000E-39	-3.9931E-04	2.5704E 02	5.9848E 00	0.0000E-39	-1.4905E 01	0.0000E-39
20	3.2764E-05	-0.0000E-39	-2.8898E-04	2.3415E 02	1.5316E 01	0.0000E-39	-2.4051E 01	0.0000E-39
21	3.0409E-05	-0.0000E-39	-1.9820E-04	2.0983E 02	2.1182E 01	0.0000E-39	-2.9895E 01	0.0000E-39
22	2.8983E-05	-0.0000E-39	-1.2472E-04	1.8523E 02	2.4395E 01	0.0000E-39	-3.3156E 01	0.0000E-39
23	2.5816E-05	-0.0000E-39	-6.6349E-05	1.6118E 02	2.5620E 01	0.0000E-39	-3.4435E 01	0.0000E-39
24	2.3637E-05	-0.0000E-39	-2.1007E-05	1.3828E 02	2.5401E 01	0.0000E-39	-3.4227E 01	0.0000E-39
25	2.1562E-05	-0.0000E-39	1.3254E-05	1.1695F 02	2.4174E 01	0.0000E-39	-3.2940E 01	0.0000E-39
26	1.9605E-05	-0.0000E-39	3.8218E-05	9.7427E 01	2.2285E 01	0.0000E-39	-3.0903E 01	0.0000E-39
27	1.7776E-05	-0.0000E-39	5.5497E-05	7.9858E 01	2.0003E 01	0.0000E-39	-2.8381E 01	0.0000E-39
28	1.6077E-05	-0.0000E-39	6.6525E-05	6.4281E 01	1.7534E 01	0.0000E-39	-2.5585E 01	0.0000E-39
29	1.4512E-05	-0.0000E-39	7.2561E-05	5.0665E 01	1.5029E 01	0.0000E-39	-2.2676E 01	0.0000E-39
30	1.3076E-05	-0.0000E-39	7.4696E-05	3.8930E 01	1.2599E 01	0.0000E-39	-1.9777E 01	-0.0000E-39
31	1.1768E-05	0.0000E-39	7.3862E-05	2.8958E 01	1.0320E 01	-0.0000E-39	-1.6979E 01	-0.0000E-39
32	1.0581E-05	0.0000E-39	7.0847E-05	2.0609E 01	8.2390F 00	-0.0000E-39	-1.4347E 01	-0.0000E-39
33	9.5085E-06	0.0000E-39	6.6302E-05	1.3730E 01	6.3834E 00	-0.0000E-39	-1.1921E 01	-0.0000E-39
34	8.5440E-06	0.0000E-39	6.0764E-05	8.1595E 00	4.7638E 00	-0.0000E-39	-9.7263E 00	-0.0000E-39
35	7.6793E-06	0.0000E-39	5.4661E-05	3.7401E 00	3.3792E 00	-0.0000E-39	-7.7741E 00	-0.0000E-39
36	6.9063E-06	0.0000E-39	4.8333E-05	3.1777E-01	2.2196E 00	-0.0000E-39	-6.0649E 00	-0.0000E-39
37	6.2171E-06	0.0000E-39	4.2037E-05	-2.2527E 00	1.2695E 00	-0.0000E-39	-4.5913E 00	-0.0000E-39
38	5.6038E-06	0.0000E-39	3.5968E-05	-4.1060E 00	5.0960E-01	-0.0000E-39	-3.3407E 00	-0.0000E-39
39	5.0597E-06	0.0000E-39	3.0261E-05	-5.3648E 00	-8.1213E-02	-0.0000E-39	-2.2964E 00	-0.0000E-39

40	4.5755E-06	0.0000E-39	2.5008E-05	-6.1391E 00	-5.2472E-01	-0.0000E-39	-1.4396E 00	-0.0000E-39
41	4.1466E-06	0.0000E-39	2.0262E-05	-6.5263E 00	-8.4235E-01	-0.0000E-39	-7.5051E-01	-0.0000E-39
42	3.7662E-06	0.0000E-39	1.6048E-05	-6.6112E 00	-1.0545E 00	-0.0000E-39	-2.0881E-01	-0.0000E-39
43	3.4786E-06	0.0000E-39	1.2367E-05	-6.4666E 00	-1.1801E 00	-0.0000E-39	2.0518E-01	-0.0000E-39
44	3.1286E-06	0.0000E-39	9.2029E-06	-6.1542E 00	-1.2762E 00	-0.0000E-39	5.1022E-01	-0.0000E-39
45	2.8617E-06	0.0000E-39	6.5281E-06	-5.7257E 00	-1.2381E 00	-0.0000E-39	7.2380E-01	-0.0000E-39
46	2.6236E-06	0.0000E-39	4.3058E-06	-5.2232E 00	-1.1990E 00	-0.0000E-39	8.6190E-01	-0.0000E-39
47	2.4108E-06	0.0000E-39	2.4949E-06	-4.6808E 00	-1.1302E 00	-0.0000E-39	9.3887E-01	-0.0000E-39
48	2.2048E-06	0.0000E-39	1.0499E-06	-4.1252E 00	-1.0414E 00	-0.0000E-39	9.6740E-01	-0.0000E-39
49	2.0484E-06	0.0000E-39	-7.2758E-08	-3.5772E 00	-9.4020E-01	-0.0000E-39	9.5856E-01	-0.0000E-39
50	1.8935E-06	0.0000E-39	-9.1738E-07	-3.0518E 00	-8.3305E-01	-0.0000E-39	9.2183E-01	-0.0000E-39
51	1.7531E-06	0.0000E-39	-1.5257E-06	-2.5599E 00	-7.2488E-01	-0.0000E-39	8.6521E-01	-0.0000E-39
52	1.6254E-06	0.0000E-39	-1.9365E-06	-2.1085E 00	-6.1943E-01	-0.0000E-39	7.9535E-01	-0.0000E-39
53	1.5088E-06	0.0000E-39	-2.1853E-06	-1.7018E 00	-5.1948E-01	-0.0000E-39	7.1769E-01	-0.0000E-39
54	1.4020E-06	0.0000E-39	-2.3040E-06	-1.3414E 00	-4.2693E-01	-0.0000E-39	6.3655E-01	-0.0000E-39
55	1.3039E-06	0.0000E-39	-2.3206E-06	-1.0272E 00	-3.4296E-01	0.0000E-39	5.5531E-01	-0.0000E-39
56	1.2134E-06	-0.0000E-39	-2.2595E-06	-7.5763E-01	-2.6820E-01	0.0000E-39	4.7652E-01	-0.0000E-39
57	1.1297E-06	-0.0000E-39	-2.1417E-06	-5.3017E-01	-2.0283E-01	0.0000E-39	4.0204E-01	-0.0000E-39
58	1.0521E-06	-0.0000E-39	-1.9846E-06	-3.4160E-01	-1.4668E-01	0.0000E-39	3.3313E-01	-0.0000E-39
59	9.7995E-07	-0.0000E-39	-1.8027E-06	-1.8827E-01	-9.9321E-02	0.0000E-39	2.7057E-01	-0.0000E-39
60	9.1285E-07	-0.0000E-39	-1.6077E-06	-6.6368E-02	-6.0146E-02	0.0000E-39	2.1477E-01	-0.0000E-39
61	8.5030E-07	-0.0000E-39	-1.4090E-06	2.7985E-02	-2.8435E-02	0.0000E-39	1.6580E-01	-0.0000E-39
62	7.9194E-07	-0.0000E-39	-1.2136E-06	9.8561E-02	-3.4027E-03	0.0000E-39	1.2353E-01	-0.0000E-39
63	7.3744E-07	-0.0000E-39	-1.0269E-06	1.4895E-01	1.5759E-02	0.0000E-39	8.7652E-02	-0.0000E-39
64	6.8652E-07	-0.0000E-39	-8.5256E-07	1.8249E-01	2.9852E-02	0.0000E-39	5.7718E-02	-0.0000E-39
65	6.3893E-07	-0.0000E-39	-6.9310E-07	2.0222E-01	3.9643E-02	0.0000E-39	3.3220E-02	-0.0000E-39
66	5.9445E-07	-0.0000E-39	-5.4991E-07	2.1088E-01	4.5855E-02	0.0000E-39	1.3601E-02	-0.0000E-39
67	5.5289E-07	-0.0000E-39	-4.2353E-07	2.1088E-01	4.9146E-02	0.0000E-39	-1.7104E-03	-0.0000E-39
68	5.1406E-07	-0.0000E-39	-3.1386E-07	2.0432E-01	5.0111E-02	0.0000E-39	-1.3282E-02	-0.0000E-39
69	4.7780E-07	-0.0000E-39	-2.2031E-07	1.9298E-01	4.9275E-02	0.0000E-39	-2.1657E-02	-0.0000E-39
70	4.4396E-07	-0.0000E-39	-1.4192E-07	1.7836E-01	4.7094E-02	0.0000E-39	-2.7348E-02	-0.0000E-39
71	4.1238E-07	-0.0000E-39	-7.7514E-08	1.6171E-01	4.3957E-02	0.0000E-39	-3.0825E-02	-0.0000E-39
72	3.8294E-07	-0.0000E-39	-2.5743E-08	1.4403E-01	4.0189E-02	0.0000E-39	-3.2514E-02	-0.0000E-39
73	3.5551E-07	-0.0000E-39	1.4798E-08	1.2612E-01	3.6060E-02	0.0000E-39	-3.2792E-02	-0.0000E-39
74	3.2997E-07	-0.0000E-39	4.5524E-08	1.0858E-01	3.1783E-02	0.0000E-39	-3.1990E-02	-0.0000E-39
75	3.0620E-07	-0.0000E-39	6.7817E-08	9.1862E-02	2.7527E-02	0.0000E-39	-3.0392E-02	-0.0000E-39
76	2.8409E-07	-0.0000E-39	8.2987E-08	7.6290E-02	2.3420E-02	0.0000E-39	-2.8237E-02	-0.0000E-39
77	2.6354E-07	-0.0000E-39	9.2250E-08	6.2068E-02	1.9555E-02	0.0000E-39	-2.5726E-02	-0.0000E-39
78	2.4444E-07	-0.0000E-39	9.6715E-08	4.9310E-02	1.5993E-02	0.0000E-39	-2.3021E-02	-0.0000E-39
79	2.2671E-07	0.0000E-39	9.7373E-08	3.8058E-02	1.2775E-02	-0.0000E-39	-2.0251E-02	-0.0000E-39
80	2.1024E-07	0.0000E-39	9.5096E-08	2.8300E-02	9.9180E-03	-0.0000E-39	-1.7518E-02	-0.0000E-39
81	1.9496E-07	0.0000E-39	9.0640E-08	1.9978E-02	7.4257E-03	-0.0000E-39	-1.4896E-02	-0.0000E-39
82	1.8079E-07	0.0000E-39	8.4648E-08	1.3006E-02	5.2888E-03	-0.0000E-39	-1.2440E-02	-0.0000E-39

83	1.6764E-07	0.0000E-39	7.7656E-08	7.2769E-03	3.4896E-03	-0.0000E-39	-1.0185E-02	-0.0000E-39
84	1.5544E-07	0.0000E-39	7.0106E-08	2.6702E-03	2.0039E-03	-0.0000E-39	-8.1518E-03	-0.0000E-39
85	1.4413E-07	0.0000E-39	6.2350E-08	-9.3936E-04	8.0352E-04	-0.0000E-39	-5.3508E-03	-0.0000E-39
86	1.3363E-07	0.0000E-39	5.4667E-08	-3.6778E-03	-1.4167E-04	-0.0000E-39	-4.7815E-03	-0.0000E-39
87	1.2390E-07	0.0000E-39	4.7263E-08	-5.6679E-03	-8.6270E-04	-0.0000E-39	-3.4369E-03	-0.0000E-39
88	1.1487E-07	0.0000E-39	4.0292E-08	-7.0258E-03	-1.3901E-03	-0.0000E-39	-2.3046E-03	-0.0000E-39
89	1.0648E-07	0.0000E-39	3.3856E-08	-7.8594E-03	-1.7532E-03	-0.0000E-39	-1.3688E-03	-0.0000E-39
90	9.8699E-08	0.0000E-39	2.8018E-08	-8.2669E-03	-1.9794E-03	-0.0000E-39	-5.1152E-04	-0.0000E-39
91	9.1470E-08	0.0000E-39	2.2807E-08	-8.3363E-03	-2.0939E-03	-0.0000E-39	-1.3400E-05	-0.0000E-39
92	8.4753E-08	0.0000E-39	1.8228E-08	-8.1448E-03	-2.1193E-03	-0.0000E-39	4.4503E-04	-0.0000E-39
93	7.8508E-08	0.0000E-39	1.4265E-08	-7.7592E-03	-2.0756E-03	-0.0000E-39	7.8292E-04	-0.0000E-39
94	7.2699E-08	0.0000E-39	1.0889E-08	-7.2365E-03	-1.9802E-03	-0.0000E-39	1.0185E-03	-0.0000E-39
95	6.7290E-08	0.0000E-39	8.0569E-09	-6.6242E-03	-1.8481E-03	-0.0000E-39	1.1689E-03	-0.0000E-39
96	6.2252E-08	0.0000E-39	5.7231E-09	-5.9614E-03	-1.6917E-03	-0.0000E-39	1.2497E-03	-0.0000E-39
97	5.7554E-08	0.0000E-39	3.8360E-09	-5.2794E-03	-1.5213E-03	-0.0000E-39	1.2749E-03	-0.0000E-39
98	5.3169E-08	0.0000E-39	2.3433E-09	-4.6026E-03	-1.3453E-03	-0.0000E-39	1.2568E-03	-0.0000E-39
99	4.9074E-08	0.0000E-39	1.1929E-09	-3.9496E-03	-1.1700E-03	-0.0000E-39	1.2062E-03	-0.0000E-39
100	4.5244E-08	0.0000E-39	3.3503E-10	-3.3339E-03	-1.0005E-03	-0.0000E-39	1.1323E-03	-0.0000E-39
101	4.1658E-08	0.0000E-39	-2.7738E-10	-2.7647E-03	-8.4041E-04	-0.0000E-39	1.0427E-03	-0.0000E-39
102	3.8296E-08	0.0000E-39	-6.8765E-10	-2.2476E-03	-6.9220E-04	-0.0000E-39	9.4367E-04	-0.0000E-39
103	3.5141E-08	0.0000E-39	-9.3512E-10	-1.7854E-03	-5.5745E-04	-0.0000E-39	8.4033E-04	-0.0000E-39
104	3.2174E-08	0.0000E-39	-1.0548E-09	-1.3789E-03	-4.3696E-04	-0.0000E-39	7.3657E-04	-0.0000E-39
105	2.9380E-08	0.0000E-39	-1.0775E-09	-1.0267E-03	-3.3098E-04	-0.0000E-39	6.3535E-04	-0.0000E-39
106	2.6744E-08	0.0000E-39	-1.0297E-09	-7.2672E-04	-2.3929E-04	-0.0000E-39	5.3876E-04	-0.0000E-39
107	2.4253E-08	0.0000E-39	-9.3406E-10	-4.7573E-04	-1.6136E-04	0.0000E-39	4.4820E-04	-0.0000E-39
108	2.1892E-08	-0.0000E-39	-8.0933E-10	-2.7010E-04	-9.6447E-05	0.0000E-39	3.6442E-04	0.0000E-39
109	1.9651E-08	-0.0000E-39	-6.7087E-10	-1.0599E-04	-4.3693E-05	0.0000E-39	2.8773E-04	0.0000E-39
110	1.7518E-08	-0.0000E-39	-5.3087E-10	2.0468E-05	-2.1896E-06	0.0000E-39	2.1803E-04	0.0000E-39
111	1.5482E-08	-0.0000E-39	-3.9865E-10	1.1294E-04	2.8962E-05	0.0000E-39	1.5490E-04	0.0000E-39
112	1.3533E-08	-0.0000E-39	-2.8095E-10	1.7482E-04	5.0599E-05	0.0000E-39	9.7726E-05	0.0000E-39
113	1.1661E-08	-0.0000E-39	-1.8221E-10	2.0909E-04	6.3470E-05	0.0000E-39	4.5742E-05	0.0000E-39
114	9.8579E-09	-0.0000E-39	-1.0477E-10	2.1832E-04	6.8209E-05	0.0000E-39	-1.9078E-06	0.0000E-39
115	8.1137E-09	-0.0000E-39	-4.9101E-11	2.0461E-04	6.5322E-05	0.0000E-39	-4.6099E-05	0.0000E-39
116	6.4206E-09	-0.0000E-39	-1.3966E-11	1.6959E-04	5.5189E-05	0.0000E-39	-8.7683E-05	-0.0000E-39
117	4.7704E-09	-0.0000E-39	3.4744E-12	1.1448E-04	3.8062E-05	-0.0000E-39	-1.2744E-04	-0.0000E-39
118	3.1553E-09	0.0000E-39	7.5483E-12	4.0123E-05	1.4087E-05	-0.0000E-39	-1.6602E-04	-0.0000E-39
119	1.5676E-09	0.0000E-39	4.0108E-12	-5.2958E-05	-1.6686E-05	-0.0000E-39	-2.0394E-04	-0.0000E-39
120	0.0000E-39	-0.0000E-39	-0.0000E-39	-1.6444E-04	-5.3864E-05	-0.0000E-39	-2.4172E-04	-0.0000E-39

I	N(PHI)	N(THETA)	N(PHI,THETA)	SIG(PHI)	SIG(THETA)	SG(PHI,THETA)
1	-5.1952E 01	-5.1952E 01	-0.0000E-39	-9.2853E 03	-9.2853E 03	0.0000E-39
2	-5.1685E 01	-5.1452E 01	-0.0000E-39	-9.2770E 03	-9.2746E 03	0.0000E-39
3	-5.1074E 01	-5.0324E 01	-0.0000E-39	-9.2535E 03	-9.2540E 03	0.0000E-39
4	-5.0166E 01	-4.8527E 01	-0.0000E-39	-9.1804E 03	-9.2024E 03	0.0000E-39
5	-4.8977E 01	-4.6071E 01	-0.0000E-39	-8.9995E 03	-9.0915E 03	0.0000E-39
6	-4.7570E 01	-4.2999E 01	-0.0000E-39	-8.6136E 03	-8.8747E 03	0.0000E-39
7	-4.6068E 01	-3.9402E 01	-0.0000E-39	-7.8512E 03	-8.4716E 03	0.0000E-39
8	-4.4721E 01	-3.5465E 01	-0.0000E-39	-6.3253E 03	-7.7112E 03	0.0000E-39
9	-4.3495E 01	-3.1377E 01	-0.0000E-39	-3.2527E 03	-6.2523E 03	0.0000E-39
10	-4.2029E 01	-2.7320E 01	-0.0000E-39	-1.0895E 03	-4.9452E 03	0.0000E-39
11	-4.0103E 01	-2.3338E 01	-0.0000E-39	4.2426E 02	-3.8227E 03	0.0000E-39
12	-3.7878E 01	-1.9558E 01	-0.0000E-39	1.4587E 03	-2.8844E 03	0.0000E-39
13	-3.5471E 01	-1.6058E 01	-0.0000E-39	2.1343E 03	-2.1156E 03	0.0000E-39
14	-3.2976E 01	-1.2887E 01	-0.0000E-39	2.5398E 03	-1.4964E 03	0.0000E-39
15	-3.0463E 01	-1.0068E 01	-0.0000E-39	2.7430E 03	-1.0059E 03	0.0000E-39
16	-2.7985E 01	-7.6039E 00	0.0000E-39	2.7963E 03	-6.2429E 02	-0.0000E-39
17	-2.5582E 01	-5.4872E 00	0.0000E-39	2.7409E 03	-3.3334E 02	-0.0000E-39
18	-2.3284E 01	-3.6999E 00	0.0000E-39	2.6089E 03	-1.1687E 02	-0.0000E-39
19	-2.1109E 01	-2.2179E 00	0.0000E-39	2.4257E 03	3.9200E 01	-0.0000E-39
20	-1.9071E 01	-1.0137E 00	0.0000E-39	2.2113E 03	1.4698E 02	-0.0000E-39
21	-1.7178E 01	-5.7787E-02	0.0000E-39	1.9808E 03	2.1673E 02	-0.0000E-39
22	-1.5431E 01	6.7983E-01	0.0000E-39	1.7459E 03	2.5707E 02	-0.0000E-39
23	-1.3830E 01	1.2285E 00	0.0000E-39	1.5151E 03	2.7513E 02	-0.0000E-39
24	-1.2372E 01	1.6162E 00	0.0000E-39	1.2948E 03	2.7676E 02	-0.0000E-39
25	-1.1050E 01	1.8691E 00	0.0000E-39	1.0892E 03	2.6671E 02	-0.0000E-39
26	-9.8580E 00	2.0112E 00	0.0000E-39	9.0085E 02	2.4875E 02	-0.0000E-39
27	-8.7872E 00	2.0639E 00	0.0000E-39	7.3133E 02	2.2587E 02	-0.0000E-39
28	-7.8292E 00	2.0464E 00	0.0000E-39	5.8110E 02	2.0036E 02	-0.0000E-39
29	-6.9751E 00	1.9753E 00	0.0000E-39	4.4997E 02	1.7396E 02	-0.0000E-39
30	-6.2159E 00	1.8650E 00	0.0000E-39	3.3717E 02	1.4792E 02	-0.0000E-39
31	-5.5429E 00	1.7274E 00	-0.0000E-39	2.4161E 02	1.2316E 02	-0.0000E-39
32	-4.9476E 00	1.5727E 00	-0.0000E-39	1.6191E 02	1.0027E 02	-0.0000E-39
33	-4.4221E 00	1.4092E 00	-0.0000E-39	9.6594E 01	7.9592E 01	-0.0000E-39
34	-3.9588E 00	1.2433E 00	-0.0000E-39	4.4086E 01	6.1317E 01	-0.0000E-39
35	-3.5507E 00	1.0802E 00	-0.0000E-39	2.8315E 00	4.5479E 01	-0.0000E-39
36	-3.1915E 00	9.2376E-01	-0.0000E-39	-2.8683E 01	3.2017E 01	-0.0000E-39
37	-2.8752E 00	7.7676E-01	-0.0000E-39	-5.1888E 01	2.0798E 01	-0.0000E-39
38	-2.5966E 00	6.4106E-01	-0.0000E-39	-6.8113E 01	1.1644E 01	-0.0000E-39
39	-2.3511E 00	5.1781E-01	-0.0000E-39	-7.8570E 01	4.3496E 00	-0.0000E-39
40	-2.1343E 00	4.0754E-01	-0.0000E-39	-8.4344E 01	-1.3042E 00	-0.0000E-39
41	-1.9425E 00	3.1028E-01	-0.0000E-39	-8.6396E 01	-5.5362E 00	-0.0000E-39
42	-1.7724E 00	2.2572E-01	-0.0000E-39	-8.5564E 01	-8.5590E 00	0.0000E-39

43	-1.6212E 00	1.5326F-01	-0.0000F-39	-8.2567E 01	-1.0572E 01	0.0000E-39
44	-1.4863E 00	9.2105E-02	-0.0000E-39	-7.8013E 01	-1.1760E 01	0.0000E-39
45	-1.3655E 00	4.1344E-02	-0.0000E-39	-7.2408E 01	-1.2288E 01	0.0000E-39
46	-1.2571E 00	-1.8740E-05	-0.0000E-39	-6.6167E 01	-1.2301E 01	0.0000E-39
47	-1.1593E 00	-3.3001E-02	-0.0000E-39	-5.9624E 01	-1.1925E 01	0.0000E-39
48	-1.0707E 00	-5.8618E-02	-0.0000E-39	-5.3038E 01	-1.1270E 01	0.0000E-39
49	-9.9027E-01	-7.7847E-02	-0.0000E-39	-4.6610E 01	-1.0425E 01	0.0000E-39
50	-9.1692E-01	-9.1618E-02	-0.0000E-39	-4.0486E 01	-9.4634E 00	0.0000E-39
51	-8.4980E-01	-1.0079E-01	-0.0000E-39	-3.4768E 01	-8.4454E 00	0.0000E-39
52	-7.8820E-01	-1.0615E-01	-0.0000E-39	-2.9520E 01	-7.4173E 00	0.0000E-39
53	-7.3149E-01	-1.0841E-01	-0.0000E-39	-2.4780E 01	-6.4145E 00	0.0000E-39
54	-6.7916E-01	-1.0819E-01	-0.0000E-39	-2.0559E 01	-5.4628E 00	0.0000E-39
55	-6.3076E-01	-1.0605E-01	-0.0000E-39	-1.6851E 01	-4.5799E 00	0.0000E-39
56	-5.8591E-01	-1.0246E-01	0.0000E-39	-1.3637E 01	-3.7770E 00	0.0000E-39
57	-5.4430E-01	-9.7826E-02	0.0000E-39	-1.0887E 01	-3.0600E 00	0.0000E-39
58	-5.0564E-01	-9.2480E-02	0.0000E-39	-8.5654E 00	-2.4304E 00	0.0000E-39
59	-4.6969E-01	-8.6704E-02	0.0000E-39	-6.6326E 00	-1.8868E 00	0.0000E-39
60	-4.3625E-01	-8.0723E-02	0.0000E-39	-5.0472E 00	-1.4250E 00	0.0000E-39
61	-4.0511E-01	-7.4717E-02	0.0000E-39	-3.7676E 00	-1.0395E 00	0.0000E-39
62	-3.7613E-01	-6.8822E-02	0.0000E-39	-2.7535E 00	-7.2374E-01	0.0000E-39
63	-3.4915E-01	-6.3142E-02	0.0000E-39	-1.9665E 00	-4.7031E-01	0.0000E-39
64	-3.2404E-01	-5.7751E-02	0.0000E-39	-1.3711E 00	-2.7178E-01	0.0000E-39
65	-3.0067E-01	-5.2698E-02	0.0000E-39	-9.3475E-01	-1.2074E-01	0.0000E-39
66	-2.7893E-01	-4.8010E-02	0.0000E-39	-6.2830E-01	-1.0101E-02	0.0000E-39
67	-2.5871E-01	-4.3701F-02	0.0000E-39	-4.2595E-01	6.6788E-02	-0.0000E-39
68	-2.3992E-01	-3.9772E-02	0.0000E-39	-3.0526E-01	1.1602E-01	-0.0000E-39
69	-2.2247E-01	-3.6211E-02	0.0000E-39	-2.4694E-01	1.4308E-01	-0.0000E-39
70	-2.0627E-01	-3.3004E-02	0.0000E-39	-2.3470E-01	1.5281E-01	-0.0000E-39
71	-1.9123E-01	-3.0128E-02	0.0000E-39	-2.5499E-01	1.4941E-01	-0.0000E-39
72	-1.7728E-01	-2.7558E-02	0.0000E-39	-2.9675E-01	1.3648E-01	-0.0000E-39
73	-1.6435E-01	-2.5269E-02	0.0000E-39	-3.5109E-01	1.1702E-01	-0.0000E-39
74	-1.5236E-01	-2.3234E-02	0.0000E-39	-4.1108E-01	9.3518E-02	-0.0000E-39
75	-1.4126E-01	-2.1426E-02	0.0000E-39	-4.7143E-01	6.7956E-02	-0.0000E-39
76	-1.3098E-01	-1.9819E-02	0.0000E-39	-5.2828E-01	4.1901E-02	-0.0000E-39
77	-1.2146E-01	-1.8390E-02	0.0000E-39	-5.7892E-01	1.6544E-02	-0.0000E-39
78	-1.1265E-01	-1.7117E-02	0.0000E-39	-6.2165F-01	-7.2479E-03	-0.0000E-39
79	-1.0450E-01	-1.5979E-02	-0.0000E-39	-6.5549E-01	-2.8876E-02	-0.0000E-39
80	-9.6960E-02	-1.4958E-02	-0.0000E-39	-6.8013E-01	-4.7967E-02	-0.0000E-39
81	-8.9984E-02	-1.4038E-02	-0.0000E-39	-6.9568E-01	-6.4327E-02	-0.0000E-39
82	-8.3532E-02	-1.3205E-02	-0.0000F-39	-7.0263E-01	-7.7907E-02	-0.0000E-39
83	-7.7564E-02	-1.2446E-02	-0.0000E-39	-7.0167E-01	-8.8768E-02	-0.0000E-39
84	-7.2044E-02	-1.1750E-02	-0.0000E-39	-6.9369E-01	-9.7051E-02	-0.0000E-39
85	-6.693' -02	-1.1110E-02	-0.0000E-39	-6.7962E-1	-1.0296E-01	-0.0000E-39

86	-6.2217E-02	-1.0517E-02	-0.0000E-39	-6.6045E-01	-1.0672E-01	-0.0000E-39
87	-5.7849E-02	-9.9650E-03	-0.0000E-39	-6.3715E-01	-1.0859E-01	-0.0000E-39
88	-5.3809E-02	-9.4491E-03	-0.0000E-39	-6.1065E-01	-1.0884E-01	-0.0000E-39
89	-5.0072E-02	-8.9650E-03	-0.0000E-39	-5.8180E-01	-1.0772E-01	-0.0000E-39
90	-4.6615E-02	-8.5095E-03	-0.0000E-39	-5.5138E-01	-1.0548E-01	-0.0000E-39
91	-4.3417E-02	-8.0798E-03	-0.0000E-39	-5.2008E-01	-1.0235E-01	-0.0000E-39
92	-4.0459E-02	-7.6740E-03	-0.0000E-39	-4.8851E-01	-9.8550E-02	-0.0000E-39
93	-3.7723E-02	-7.2903E-03	-0.0000E-39	-4.5717E-01	-9.4261E-02	-0.0000E-39
94	-3.5192E-02	-6.9275E-03	-0.0000E-39	-4.2648E-01	-8.9651E-02	-0.0000E-39
95	-3.2853E-02	-6.5846E-03	-0.0000E-39	-3.9678E-01	-8.4864E-02	-0.0000E-39
96	-3.0690E-02	-6.2610E-03	-0.0000E-39	-3.6833E-01	-8.0021E-02	-0.0000E-39
97	-2.8691E-02	-5.9559E-03	-0.0000E-39	-3.4133E-01	-7.5220E-02	-0.0000E-39
98	-2.6845E-02	-5.6691E-03	-0.0000E-39	-3.1590E-01	-7.0542E-02	-0.0000E-39
99	-2.5141E-02	-5.4000E-03	-0.0000E-39	-2.9215E-01	-6.6052E-02	-0.0000E-39
100	-2.3568E-02	-5.1485E-03	-0.0000E-39	-2.7010E-01	-6.1795E-02	-0.0000E-39
101	-2.2120E-02	-4.9141E-03	-0.0000E-39	-2.4976E-01	-5.7807E-02	-0.0000E-39
102	-2.0786E-02	-4.6968E-03	-0.0000E-39	-2.3110E-01	-5.4111E-02	-0.0000E-39
103	-1.9559E-02	-4.4961E-03	-0.0000E-39	-2.1408E-01	-5.0720E-02	-0.0000E-39
104	-1.8434E-02	-4.3119E-03	-0.0000E-39	-1.9865E-01	-4.7640E-02	-0.0000E-39
105	-1.7402E-02	-4.1439E-03	-0.0000E-39	-1.8471E-01	-4.4871E-02	-0.0000E-39
106	-1.6459E-02	-3.9919E-03	-0.0000E-39	-1.7219E-01	-4.2409E-02	-0.0000E-39
107	-1.5599E-02	-3.8556E-03	-0.0000E-39	-1.6101E-01	-4.0245E-02	-0.0000E-39
108	-1.4818E-02	-3.7347E-03	-0.0000E-39	-1.5109E-01	-3.8370E-02	-0.0000E-39
109	-1.4111E-02	-3.6291E-03	-0.0000E-39	-1.4233E-01	-3.6771E-02	-0.0000E-39
110	-1.3475E-02	-3.5384E-03	-0.0000E-39	-1.3465E-01	-3.5438E-02	-0.0000E-39
111	-1.2904E-02	-3.4625E-03	-0.0000E-39	-1.2800E-01	-3.4358E-02	-0.0000E-39
112	-1.2397E-02	-3.4010E-03	-0.0000E-39	-1.2229E-01	-3.3521E-02	-0.0000E-39
113	-1.1951E-02	-3.3539E-03	-0.0000E-39	-1.1747E-01	-3.2917E-02	-0.0000E-39
114	-1.1562E-02	-3.3208E-03	-0.0000E-39	-1.1349E-01	-3.2538E-02	-0.0000E-39
115	-1.1229E-02	-3.3017E-03	-0.0000E-39	-1.1030E-01	-3.2376E-02	-0.0000E-39
116	-1.0950E-02	-3.2964E-03	-0.0000E-39	-1.0786E-01	-3.2427E-02	-0.0000E-39
117	-1.0722E-02	-3.3047E-03	-0.0000E-39	-1.0614E-01	-3.2686E-02	-0.0000E-39
118	-1.0545E-02	-3.3266E-03	-0.0000E-39	-1.0513E-01	-3.3151E-02	-0.0000E-39
119	-1.0417E-02	-3.3620E-03	-0.0000E-39	-1.0480E-01	-3.3821E-02	-0.0000E-39
120	-1.0312E-02	-3.4030E-03	-0.0000E-39	-1.0490E-01	-3.4612E-02	-0.0000E-39

VELOCITIES AND ACCELERATIONS

	VEL(U)	VEL(V)	VEL(W)	ACC(U)	ACC(V)	ACC(W)
7.276E-08	0.000E-39	-4.346E 01	7.276E-04	0.000E-39	-4.346E 05	

6.549E-02	0.000E-39	-4.322E-01	6.549E-02	0.000E-39	-4.322E-05
1.299E-01	0.000E-39	-4.249E-01	1.299E-03	0.000E-39	-4.249E-05
1.920E-01	0.000E-39	-4.127E-01	1.920E-03	0.000E-39	-4.127E-05
2.506E-01	0.000E-39	-3.957E-01	2.506E-03	0.000E-39	-3.957E-05
3.042E-01	0.000E-39	-3.739E-01	3.042E-03	0.000E-39	-3.739E-05
3.516E-01	0.000E-39	-3.478E-01	3.516E-03	0.000E-39	-3.478E-05
3.914E-01	0.000E-39	-3.177E-01	3.914E-03	0.000E-39	-3.177E-05
4.217E-01	0.000E-39	-2.847E-01	4.217E-03	0.000E-39	-2.847E-05
4.421E-01	0.000E-39	-2.511E-01	4.421E-03	0.000E-39	-2.511E-05
4.536E-01	0.000E-39	-2.181E-01	4.536E-03	0.000E-39	-2.181E-05
4.572E-01	0.000E-39	-1.868E-01	4.572E-03	0.000E-39	-1.868E-05
4.541E-01	0.000E-39	-1.578E-01	4.541E-03	0.000E-39	-1.578E-05
4.453E-01	0.000E-39	-1.314E-01	4.453E-03	0.000E-39	-1.314E-05
4.320E-01	0.000E-39	-1.078E-01	4.320E-03	0.000E-39	-1.078E-05
4.151E-01	0.000E-39	-8.689E-00	4.151E-03	0.000E-39	-8.689E-04
3.954E-01	0.000E-39	-6.873E-00	3.954E-03	0.000E-39	-6.873E-04
3.738E-01	0.000E-39	-5.314E-00	3.738E-03	0.000E-39	-5.314E-04
3.511E-01	0.000E-39	-3.993E-00	3.511E-03	0.000E-39	-3.993E-04
3.276E-01	0.000E-39	-2.890E-00	3.276E-03	0.000E-39	-2.890E-04
3.041E-01	0.000E-39	-1.982E-00	3.041E-03	0.000E-39	-1.982E-04
2.808E-01	0.000E-39	-1.247E-00	2.808E-03	0.000E-39	-1.247E-04
2.582E-01	0.000E-39	-6.635E-01	2.582E-03	0.000E-39	-6.635E-03
2.364E-01	0.000E-39	-2.101E-01	2.364E-03	0.000E-39	-2.101E-03
2.156E-01	0.000E-39	1.325E-01	2.156E-03	0.000E-39	1.325E-03
1.961E-01	0.000E-39	3.822E-01	1.961E-03	0.000E-39	3.822E-03
1.778E-01	0.000E-39	5.550E-01	1.778E-03	0.000E-39	5.550E-03
1.608E-01	0.000E-39	6.652E-01	1.608E-03	0.000E-39	6.652E-03
1.451E-01	0.000E-39	7.256E-01	1.451E-03	0.000E-39	7.256E-03
1.308E-01	0.000E-39	7.470E-01	1.308E-03	0.000E-39	7.470E-03
1.177E-01	0.000E-39	7.386E-01	1.177E-03	0.000E-39	7.386E-03
1.058E-01	0.000E-39	7.085E-01	1.058E-03	0.000E-39	7.085E-03
9.509E-02	0.000E-39	6.630E-01	9.509E-02	0.000E-39	6.630E-03
8.544E-02	0.000E-39	6.076E-01	8.544E-02	0.000E-39	6.076E-03
7.679E-02	0.000E-39	5.466E-01	7.679E-02	0.000E-39	5.466E-03
6.906E-02	0.000E-39	4.833E-01	6.906E-02	0.000E-39	4.833E-03
6.217E-02	0.000E-39	4.204E-01	6.217E-02	0.000E-39	4.204E-03
5.604E-02	0.000E-39	3.597E-01	5.604E-02	0.000E-39	3.597E-03
5.059E-02	0.000E-39	3.026E-01	5.059E-02	0.000E-39	3.026E-03
4.576E-02	0.000E-39	2.501E-01	4.576E-02	0.000E-39	2.501E-03
4.147E-02	0.000E-39	2.026E-01	4.147E-02	0.000E-39	2.026E-03
3.766E-02	0.000E-39	1.605E-01	3.766E-02	0.000E-39	1.605E-03
3.429E-02	0.000E-39	1.237E-01	3.429E-02	0.000E-39	1.237E-03
.129E-02	0.000E-39	9.203E-02	3.129E-02	0.000E-39	9.20E-02

2.862E-02	0.000E-39	2.862E-02	0.000E-39	6.528E-02	6.528E-02
2.624E-02	0.000E-39	2.624E-02	0.000E-39	4.306E-02	4.306E-02
2.411E-02	0.000E-39	2.411E-02	0.000E-39	2.495E-02	2.495E-02
2.220E-02	0.000E-39	2.220E-02	0.000E-39	1.050E-02	1.050E-02
2.048E-02	0.000E-39	2.048E-02	0.000E-39	-7.276E-00	-7.276E-00
1.893E-02	0.000E-39	1.893E-02	0.000E-39	-9.174E-01	-9.174E-01
1.753E-02	0.000E-39	1.753E-02	0.000E-39	-1.526E-02	-1.526E-02
1.625E-02	0.000E-39	1.625E-02	0.000E-39	-1.936E-02	-1.936E-02
1.509E-02	0.000E-39	1.509E-02	0.000E-39	-2.185E-02	-2.185E-02
1.402E-02	0.000E-39	1.402E-02	0.000E-39	-2.304E-02	-2.304E-02
1.304E-02	0.000E-39	1.304E-02	0.000E-39	-2.321E-02	-2.321E-02
1.213E-02	0.000E-39	1.213E-02	0.000E-39	-2.260E-02	-2.260E-02
1.130E-02	0.000E-39	1.130E-02	0.000E-39	-2.142E-02	-2.142E-02
1.052E-02	0.000E-39	1.052E-02	0.000E-39	-1.985E-02	-1.985E-02
9.800E-01	0.000E-39	9.800E-01	0.000E-39	-1.803E-02	-1.803E-02
9.128E-01	0.000E-39	9.128E-01	0.000E-39	-1.608E-02	-1.608E-02
8.503E-01	0.000E-39	8.503E-01	0.000E-39	-1.409E-02	-1.409E-02
7.919E-01	0.000E-39	7.919E-01	0.000E-39	-1.214E-02	-1.214E-02
7.374E-01	0.000E-39	7.374E-01	0.000E-39	-1.027E-02	-1.027E-02
6.865E-01	0.000E-39	6.865E-01	0.000E-39	-8.526E-01	-8.526E-01
6.389E-01	0.000E-39	6.389E-01	0.000E-39	-6.931E-01	-6.931E-01
5.945E-01	0.000E-39	5.945E-01	0.000E-39	-5.499E-01	-5.499E-01
5.529E-01	0.000E-39	5.529E-01	0.000E-39	-4.235E-01	-4.235E-01
5.141E-01	0.000E-39	5.141E-01	0.000E-39	-3.139E-01	-3.139E-01
4.778E-01	0.000E-39	4.778E-01	0.000E-39	-2.203E-01	-2.203E-01
4.440E-01	0.000E-39	4.440E-01	0.000E-39	-1.419E-01	-1.419E-01
4.124E-01	0.000E-39	4.124E-01	0.000E-39	-7.751E-00	-7.751E-00
3.829E-01	0.000E-39	3.829E-01	0.000E-39	-2.574E-00	-2.574E-00
3.555E-01	0.000E-39	3.555E-01	0.000E-39	1.410E-00	1.410E-00
3.300E-01	0.000E-39	3.300E-01	0.000E-39	4.552E-00	4.552E-00
3.062E-01	0.000E-39	3.062E-01	0.000E-39	6.782E-00	6.782E-00
2.841E-01	0.000E-39	2.841E-01	0.000E-39	8.299E-00	8.299E-00
2.635E-01	0.000E-39	2.635E-01	0.000E-39	9.225E-00	9.225E-00
2.444E-01	0.000E-39	2.444E-01	0.000E-39	9.671E-00	9.671E-00
2.267E-01	0.000E-39	2.267E-01	0.000E-39	9.737E-00	9.737E-00
2.102E-01	0.000E-39	2.102E-01	0.000E-39	9.510E-00	9.510E-00
1.950E-01	0.000E-39	1.950E-01	0.000E-39	9.064E-00	9.064E-00
1.808E-01	0.000E-39	1.808E-01	0.000E-39	8.465E-00	8.465E-00
1.676E-01	0.000E-39	1.676E-01	0.000E-39	7.766E-00	7.766E-00
1.554E-01	0.000E-39	1.554E-01	0.000E-39	7.011E-00	7.011E-00
1.441E-01	0.000E-39	1.441E-01	0.000E-39	6.235E-00	6.235E-00
1.336E-01	0.000E-39	1.336E-01	0.000E-39	5.467E-00	5.467E-00
1.239E-01	0.000E-39	1.239E-01	0.000E-39	4.726E-00	4.726E-00

1.149E-03	0.000E-39	4.029E-04	1.149E 01	0.000E-39	4.029E 00
1.065E-03	0.000E-39	3.386E-04	1.065E 01	0.000E-39	3.386E 00
9.870E-04	0.000E-39	2.802E-04	9.870E 00	0.000E-39	2.802E 00
9.147E-04	0.000E-39	2.281E-04	9.147E 00	0.000E-39	2.281E 00
8.475E-04	0.000E-39	1.823E-04	8.475E 00	0.000E-39	1.823E 00
7.851E-04	0.000E-39	1.427E-04	7.851E 00	0.000E-39	1.427E 00
7.270E-04	0.000E-39	1.089E-04	7.270E 00	0.000E-39	1.089E 00
6.729E-04	0.000E-39	8.057E-05	6.729E 00	0.000E-39	8.057E-01
6.225E-04	0.000E-39	5.723E-05	6.225E 00	0.000E-39	5.723E-01
5.755E-04	0.000E-39	3.836E-05	5.755E 00	0.000E-39	3.836E-01
5.317E-04	0.000E-39	2.343E-05	5.317E 00	0.000E-39	2.343E-01
4.907E-04	0.000E-39	1.193E-05	4.907E 00	0.000E-39	1.193E-01
4.524E-04	0.000E-39	3.350E-06	4.524E 00	0.000E-39	3.350E-02
4.166E-04	0.000E-39	-2.774E-06	4.166E 00	0.000E-39	-2.774E-02
3.830E-04	0.000E-39	-6.877E-06	3.830E 00	0.000E-39	-6.877E-02
3.514E-04	0.000E-39	-9.351E-06	3.514E 00	0.000E-39	-9.351E-02
3.217E-04	0.000E-39	-1.055E-05	3.217E 00	0.000E-39	-1.055E-01
2.938E-04	0.000E-39	-1.077E-05	2.938E 00	0.000E-39	-1.077E-01
2.674E-04	0.000E-39	-1.030E-05	2.674E 00	0.000E-39	-1.030E-01
2.425E-04	0.000E-39	-9.341E-06	2.425E 00	0.000E-39	-9.341E-02
2.189E-04	0.000E-39	-8.093E-06	2.189E 00	0.000E-39	-8.093E-02
1.965E-04	0.000E-39	-6.709E-06	1.965E 00	0.000E-39	-6.709E-02
1.752E-04	0.000E-39	-5.309E-06	1.752E 00	0.000E-39	-5.309E-02
1.548E-04	0.000E-39	-3.987E-06	1.548E 00	0.000E-39	-3.987E-02
1.353E-04	0.000E-39	-2.810E-06	1.353E 00	0.000E-39	-2.810E-02
1.166E-04	0.000E-39	-1.822E-06	1.166E 00	0.000E-39	-1.822E-02
9.858E-05	0.000E-39	-1.048E-06	9.858E-01	0.000E-39	-1.048E-02
8.114E-05	0.000E-39	-4.910E-07	8.114E-01	0.000E-39	-4.910E-03
6.421E-05	0.000E-39	-1.397E-07	6.421E-01	0.000E-39	-1.397E-03
4.770E-05	0.000E-39	3.474E-08	4.770E-01	0.000E-39	3.474E-04
3.155E-05	0.000E-39	7.548E-08	3.155E-01	0.000E-39	7.548E-04
1.568E-05	0.000E-39	4.011E-08	1.568E-01	0.000E-39	4.011E-04
0.000E-39	-0.000E-39	-0.000E-39	0.000E-39	0.000E-39	-0.000E-39

TAPE CODES KODER1,KODER2,KODES1,KODES2=

10 10 1 11

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6.1 WARNINGS AND RECOMMENDATIONS

6.1.1 Choice of Time Interval

The proper choice of the appropriate time interval Δt is important for obtaining good results. If Δt is too large, the response will be highly damped and inaccurate. On the other hand, if Δt is too small, the program will take a large amount of time to run. In addition, it appears that having too small a Δt may give rise to numerical instabilities in the pressure calculations. In the sample problem Δt of 0.1 ms was used, which gave good results.

6.1.2 Number of Iterations

There is an unidentifiable bug in the program which makes it necessary that a restart be made after about 140 iterations through the shell program. Should 160 iterations be exceeded, the program will "blow up." Therefore, it is recommended that the job be run in segments of roughly 1 ms. between restarts. The method of restarting is explained in Sections 1.3 and 5.3. In the calculations made for the sample problem, the index IVX was set to about 25, and a restart was made every 1.0 ms. to 7 ms. Thereafter, because of the increase in the number of iterations to convergence in each time cycle, restarts were made at intervals of 0.5 ms.

6.1.3 DECRD

The subroutine DECRD is in the NAA program library and consequently does not appear specifically in the source decks. In installations without this program in their library, the subroutine should be inserted in the zero link behind the subroutine MMY.

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7.1

PROGRAM LISTING

\$IBJOB			
\$IBFTC 157DR			00000010
C	HYDROELASTIC RESPONSE OF SHELLS OF REVOLUTION		00000020
C			00000030
C	REFERENCE ** AIAA JOURNAL, VOL. 1, NO. 8, AUGUST 1963, PG. 1833FF		00000040
C	AND VOL. 2, NO. 3, MARCH 1964, PG. 590FF		00000050
C			00000060
C	NOMENCLATURE		00000070
C	EN	NUMBER OF POINTS	00000080
C	* AO	REFERENCE LENGTH (IN)	00000090
C	* HO	REFERENCE THICKNESS (IN)	00000100
C	* EO	REFERENCE YOUNGS MODULUS (PSI)	00000110
C	* SIGO	REFERENCE STRESS (PSI)	00000120
C	* ENFO	INITIAL VALUE OF THE FOURIER COMPONENT	00000130
C	* ENFL	LAST FOURIER COMPONENT	00000140
C	* POI	POISSONS RATIO	00000150
C	* THETA	HORIZONTAL ANGLE (0.-) THETA VALUES COMPLETED	00000160
C	* PIXI	CRT INDICATOR PLOTS CURVE WHEN NON-ZERO	00000170
C	* SPRL	LOCATION OF SPRING	00000180
C	* UK	SPRING VALUE - PHI DIRECTION	00000190
C	* VK	DIITTO * * * - THETA DIRECTION	00000200
C	* WK	DIITTO * * * - N DIRECTION	00000210
C	* EMK	DIITTO * * * - MOMENT	00000220
C	* TAU1	LENGTH OF FIRST TIME INTERVAL	00000230
C	* ENI1	NO. OF INCREMENTS IN FIRST TIME INTERVAL	00000240
C	* P11	PRINT INTERVAL. WILL ALWAYS PRINT LAST INTERVAL VALUES	00000250
C	* TAU2,ENT2,P12	** DIITTO ** FOR THE 2ND TIME INTERVAL	00000260
C	* TAU3,ENT3,P13	** DIITTO ** FOR THE 3RD TIME INTERVAL	00000270
C	* MASS	MASS DENSITY OF THE MATERIAL	00000280
C	* CFE,CZ	COEFFICIENTS OF VISCOUS DAMPING AT EA. STATION	00000290
C	* SKEE,SKZ	SPRING CONSTANTS OF SHELL UNDER ELAST. RESTRAINT	00000300
C	* SUM	FOURIER SUMMING INCREMENT	00000310
C	ENI	1. = OPEN SHELL 2. = CLOSED SET IN GEOM	00000320
C	DEL	FINITE DIFFERENCE INTERVAL	00000330
C	* TFI	TIME FUNCTION IND. (-)=CALL ACCN (+)=TIME FUNCTIONS	00000340
C	* VIN	INITIAL IMPACT VELOCITY	00000350
C	RESIRT	NON-ZERO, THIS IS A RESTART	00000360
C	PNCH	NON-ZERO, PUNCH CARDS FOR POSSIBLE RESTART	00000370
C			00000380
C	R(I)	DISTANCE FROM AXIS (IN) COMPUTED BY SUBR. GEOM	00000390
C	WTHD(I)	NON-DIMENSIONAL CURVATURE - THETA DIRECTION	00000400
C	WFE(I)	DIITTO * * * - PHI DIRECTION	00000410
C	GAMA(I)	RHO' / RHOX	00000420

C	RHOX(1)	R / A0		0.0000430
C	D(1)	MEMBRANE STIFFNESS (DIMENSIONLESS)		0.0000440
C	EK(1)	BENDING STIFFNESS (DIM)		0.0000450
C	E1(1)	MODULUS OF ELASTICITY		0.0000460
C	ALF(1)	THERMAL EXPANSION COEFFICIENT	* * DITTO * *	0.0000470
C	DNA(1)	DISTANCE FROM NEUTRAL AXIS		0.0000480
C	T(1)	TEMPERATURE CHANGE		0.0000490
C	ENT(1)	TEMPERATURE LOAD (DIM)		0.0000500
C	EMI(1)	TEMPERATURE LOAD (DIM)		0.0000510
C	PFE(1)	FOURIER COMPONENT FOR LOAD - PHI DIRECTION		0.0000520
C	PTH(1)	DITTO * * *	- THETA DIRECTION	0.0000530
C	PN(1)	DITTO * * *	- N DIRECTION	0.0000540
C	DZ0,VZ0,AZ0	COEF. OF INITIAL VALUES OF DISPLACEMENT, VELOCITY, LD,0.0000550		
C	DF0,VF0,AF0	** DITTO **		0.0000560
C	* EM1(4,4)	DIAGONAL BOUNDARY FORCE MATRIX (OMEGA)		0.0000570
C	* EM3(4,4)	DIAGONAL BOUNDARY DISPLACEMENT MATRIX (LAMBDA)		0.0000580
C	* EM5(4)	COLUMN BOUNDARY MATRIX (L)		0.0000590
C	* EM1N(4,4)	DIAGONAL BOUNDARY FORCE MATRIX AT BOTTOM		0.0000600
C	* EM3N(4,4)	DIAGONAL BOUNDARY DISPLACEMENT MATRIX AT BOTTOM		0.0000610
C	* EM5N(4)	COLUMN BOUNDARY MATRIX AT BOTTOM		0.0000620
C	MO(1)	MASS PER UNIT AREA OF SHELL = 2.*DNA(1) * MASS		0.0000630
C	TDEL	TIME INCREMENT, CURRENT. E.G. TAU1 / ENT1		0.0000640
C	NJT	NUMBER OF TIME INCREMENTS DESIRED, CURRENT		0.0000650
C	TIME	RUNNING TIME COUNT		0.0000660
C	PRNT	CURRENT PRINT INTERVAL		0.0000670
C	* PARAMETERS PRECEDED BY *	ARE READ IN EXECUTIVE PROGRAM, OTHERS		0.0000680
C		ARE SET IN GEOM OR CRVFIT.		0.0000690
C				0.0000700
C				0.0000710
C				0.0000720
C				0.0000730
C				0.0000740
C				0.0000750
C	REAL	MASS, LM11,LM22,LM33, NM11,NM22,NM33, NM11,NM22,NM33, MO		
C	1	EQUIVALENCE	(DA(1), EN),(DA(2), AU),(DA(3), HC),(DA(4), F0),(DA(5), SIG0),(DA(6), ENF0),(DA(7), FNFL),(DA(8), POI),(DA(9), THETA),(DA(10), PIX1),(DA(11), SPRL),(DA(12), UK),(DA(13), VK),(DA(14), WK),(DA(15), EMK),(DA(16), LAU1),(DA(17), ENT1),(DA(18), P11),(DA(19), TAU2),(DA(20), ENT2),(DA(21), P12),(DA(22), TAU3),(DA(23), FNT3),(DA(24), P13),(DA(25), MASS),(DA(26), CFE),(DA(27), CZ),(DA(28), SKFE),(DA(29), SKZ),(DA(30), SUM),(DA(31), EN1),(DA(32), DEL),(DA(33), IFI),(DA(34), VIN),(DA(35), IND),(DA(36), PN(200)	


```

      READ (13) (DA(K),K=1,NOT)
4012 WRITE( 9) (DA(K),K=1,NOT)
      DO 4013 J=1,14
      READ (13) (DA(K),K=1,N)
4013 WRITE( 9) (DA(K),K=1,N)
4011 CONTINUE
      REWIND 13
      GO TO 1
5 IF(NSAVE.EQ.0) GO TO 4007
C RESTART--- SAVE TIMX,ZPREV,OMEG
      REWIND 8
      KODES2=KODES2+10
      WRITE( 8) KODES2
      WRITE(8) (OMG2(I),I=1,2002),
1 INDER,ICYL,JELLO,IVX,CONV,NO,IV,NOT,(PE2(I),I=1,918),
2 (DA(I),I=2640,2839),
3 (DA(I),I=3240,3439),(DA(I),I=3840,4039)
      REWIND 8
      WRITE(6,6002) KODER1,KODER2,KODES1,KODES2
6002 FORMAT(1H0,40HTAPE CODES KODER1,KODER2,KODES1,KODES2=,4I12)
      GO TO 4007
6000 CONTINUE
      KODER1=10
      KODER2=10
      KODES2=1
      KODES1=1
      WRITE( 9) KODER1
1 DO 2 I = 1,4511
2 DA(I) = 0.
      DO 4 K = 1,3
      DO 4 L = 1,200
      ZP(K,L) = 0.
      Z2P(K,L) = 0.
      Z3P(K,L) = 0.
4
C READ(5,6) BCD
6 FORMAT( 12A6 )
      WRITE
7 FORMAT(1H1 / (18X, 12A6 /) )
      SL2 = 1.
10 TIMX = 0.
      JT = 1
      READ(5,3004) RHO,WT
3004 FORMAT(2E12.8)

```

00001300
00001310
00001320
00001330
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00001360
00001370
00001380
00001390
00001400
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00001735

READ AND PRINT TITLE CARDS

C	RHO= FLUID DENSITY -- LBS/CU FT	00001730
C	WT = BODY WEIGHT -- LBS	00001740
C	VIN = INITIAL IMPACT VELOCITY -- INCHES PER SECOND	00001750
	READ(5,3000)INDR,CONV,IVX,ICYL	00001760
	3000 FORMAT(I12,E12.8,2I12)	00001770
C	IF INDR = 0, NO ITERATION	00001780
C	CONV=PRESSURE CONVERGENCE CRITERION	00001790
C	VX=MAX NO OF ITERATIONS CYCLES	00001800
C	IF ICYL = 0, IMPACT OF A SPHERE	00001810
C	IF ICYL = 1, IMPACT OF A CYLINDER	00001820
C	FOR A STSIC CASE, TAU1=.1 MS, ENTI=1, PI=1, MASS=0.0	00001830
C		00001840
	12 CALL DECRD(DA)	00001850
C		00001860
	IDEL = TAU1 / ENTI	00001870
	IF(NSTART.EQ.1) GO TO 5002	00001880
	RHO=RHO/1728.0	00001890
	RH = RHO / (32.2*12.)	00001900
	P(1,1)= 1.	00001910
	P(2,1)= 1.	00001920
	P(3,1)= 1.	00001930
	P(4,1)= 1.	00001940
	PP(1,1)= 1.	00001950
	PP(2,1)= 6.	00001960
	PP(3,1)= 15.	00001970
	PP(4,1)= 28.	00001980
	GMU(1) = 1.	00001990
	PIE = 3.14159265	00002000
	FUN(1)= -2./PIE *3.	00002010
	FUN(2)= -7./(2.*PIE)*(2.**3/6.)** 2	00002020
	FUN(3)= -31./(2.*PIE)*(4.*2.**5/ 120.)**2	00002030
	FUN(4)= -15./(2.*PIE)*(36.*2.**7 / (7.*6.*120.))** 2	00002040
	JELLO=0	00002050
	5002 CONTINUE	00002060
	PRNT = PI1	00002070
	ENF = ENFO	00002080
	NJT = ENTI	00002090
	PI1 = PI1	00002100
	NTH = 0	00002110
	ELAM = H0 /A0	00002120
	ELAM2 = ELAM **2	00002130
	S1 = 1. - POI	00002140
	S2 = 1. + POI	00002150

S77 = A0/E0 * A0/H0	00002160
C	00002170
C	00002180
20 CALL GEOM	00002190
IF(INSTRT.EQ.1) GO TO 25	00002200
RADIUS=1./WFE	00002210
GAM=8.*2.**.5*RHO*RADIUS**1.5/(3.*WT)	00002220
C	00002230
25 S78 = 2. * DEL /TDEL	00002240
TIMX = TIMX + TDEL	00002250
IF(INDER)3002,3002,3001	00002260
3002 IND=1	00002270
GO TO 3003	00002280
3001 CONTINUE	00002290
IV=1	00002300
IND=-1	00002310
3003 CONTINUE	00002320
IF(IFI .GE. 0.) GO TO 30	00002330
IF(TIMX .NE. TDEL) GO TO 32	00002340
C	00002350
30 CALL CRVFIT	00002360
C	00002370
IF(IFI .GE. 0.) GO TO 40	00002380
32 CALL ACCN	00002390
C	00002400
40 CALL DEFLTIN	00002410
C	00002420
50 CALL PATH	00002430
SL1=0.0	00002440
IF(IND)51,52,55	00002450
51 IND=0	00002460
GO TO 54	00002470
52 IV=IV+1	00002480
IF(IV.EQ.2.AND.JT.EQ.1) GO TO 54	00002490
NOP=NOT-1	00002500
DO 102 I=1,NOP	00002510
IF(ABS(1.0-PE2(I)/PS(I)).GT.CONV) GO TO 54	00002520
102 CONTINUE	00002530
GO TO 55	00002540
54 IF(IV.GT.IVX) GO TO 57	00002550
NOP=NOT-1	00002560
DO 103 I=1,NOP	00002570
103 PS(I)=PE2(I)	00002580

GO TO 32	00002590
57 WRITE(6,58)IVX	00002600
58 FORMAT(1H0,39HNO OF ITERATIONS HAS EXCEED LIMIT IVX=,I3)	00002610
59 CONTINUE	00002620
DO 59 I = 1,N	00002630
DO 59 J = 1,3	00002640
Z3P(J,I) = Z2P(J,I)	00002650
Z2P(J,I) = ZP(J,I)	00002660
ZP(J,I) = Z(J,I)	00002670
DO 5050 I=1,NOT	00002680
IF(PN(I),LE,0.0) GO TO 101	00002690
5050 PN(I)=0.0	00002700
101 CONTINUE	00002710
NOD=NO+2	00002720
NODD=NO+3	00002730
WRITE(6,33)TIMX,AP,VEL,ACC,BP,(I,PN(I),PM1(I),PF2(I),I=1,NOD)	00002740
FORMAT(1H1,///37X,2/HWATER IMPACT PRESSURE LOADS ///	00002750
11H0,34H MAX RAD OF PRESSURE PROFILE = ,F17.8,3HSEC, /	00002760
21H0,34H VEHICLE VELOCITY = ,E17.8,3HINS, /	00002770
61H0,34H VEHICLE ACCELERATION = ,E17.8,7HINS/SEC, /	00002780
41H0,34H DEPTH OF PENETRATION = ,E17.8,1HG, /	00002790
51H0,34H DEPTH OF PENETRATION = ,E17.8,3HINS, /	00002800
61H0,5X,7HSTALION,10X,14HIOIAL PRESSURE,10X,20HRIQID-BODY COMPONENT,00002810	00002810
7 10X,17HELASTIC COMPONENT,/(19,15X,F12.4,18X,F12.4,15X,F12.4)	00002820
WRITE(6,34)(I,PN(I),I=NODD,N)	00002830
34 FORMAT(19,15X,F12.4)	00002840
WRITE(9)JT,TIMX,AP,VEL,ACC,BP,N,NOT	00002850
WRITE(9)(PN(I),I=1,NOT)	00002860
WRITE(9)(PM1(I),I=1,NOT)	00002870
WRITE(9)(PE2(I),I=1,NOT)	00002880
JT=JT+1	00002890
IF(SL1) 5,60,25	00002900
C	00002910
60 CALL INTLDS	00002920
C	00002930
70 CALL SUMS	00002940
IF(SL1) 5,25,72	00002950
C	00002960
72 IF(ENF - ENF .GT. 1.E-2) GO TO 10	00002970
IF(PXI .EQ. 0.) GO TO 90	00002980
C	00002990
80 CALL PIX	00003000
90 GO TO 5	00003010

5512	WRITE(6,5513) KODER1,KODER2	00003020
5513	FORMAT(1H0,58HINPUT RESPONSE TAPES WPONG-CHECK TAPE NOS.---KODER1,00003030	00003030
	1KODER2=,2I12)	00003040
	STOP	00003050
	END	00003060

SIBFC MPMY	DECK NO. 8K-901	0003070
C MATRIX MULTIPLY SUBROUTINE		0003080
C		0003090
C ARGUMENTS		0003100
C L NO. OF ROWS X MATRIX		0003120
C M NO. OF COLS X MATRIX		0003130
C N NO. OF COLS Y MATRIX		0003140
C X(I,K) MRA		0003150
C Y(K,J) MMY		0003160
C Z(I,J) MSR		0003170
C SUBROUTINE MMY(L,N,X,Y,Z)		0003180
C DIMENSION X(4,4), Y(4,4), Z(4,4)		0003190
DO 30 I=1,L		0003200
DO 30 J=1,N		0003210
Z(I,J)=0.0		0003220
DO 30 K=1,M		0003230
30 Z(I,J)=Z(I,J)+X(I,K)*Y(K,J)		0003240
RETURN		0003250
END		0003260

SIBFC MADD	00003270
C MATRIX ADD SUBROUTINE	00003280
C	00003290
C ARGUMENTS	00003300
C L NO. OF ROWS	00003310
C M NO. OF COLS	00003320
C A(I,J) MRA	00003330
C B(I,J) MAD	00003340
C C(I,J) MSR	00003350
SUBROUTINE MAD(L,M,A,B,C)	00003360
DIMENSION A(4,4), B(4,4), C(4,4)	00003370
DO 30 I=1,L	00003380
DO 30 J=1,M	00003390
30 C(I,J)=A(I,J)+B(I,J)	00003400
RETURN	00003410
END	00003420

SORIGIN	CHAIN	00003430
SIBFTC	GMTRY	00003440
C	GEOMETRY COMPUTATION SUBROUTINE	6J-157DR *LINK 1A
C		00003450
C	SUBROUTINE GEOM	00003460
C		00003470
C		00003480
C	NOMENCLATURE	00003490
C	GMI = GEOMETRY INDICATOR	00003500
C	= 1.0 - CONE - CYLINDER	00003510
C	= 2.0 - SPHERL - TOROID	00003520
C	= 3.0 - GENERAL DISCRETE POINTS	00003530
C	= 4.0 - ARBITRARY FUNCTIONS	00003540
C		00003550
C	EN NO. OF POINTS / REGION	00003560
C	PFLAG PRINT INDICATOR, NON-ZERO PRINTS ALL INPUT DATA	00003570
C	**	00003580
C	GMI = 1.0	00003590
C	RA1 = RADIUS AT STATION 1	00003600
C	AXL = AXIAL SURFACE LENGTH	00003610
C	ANX = ANGLE - GENERATOR AND AXIS OF REVOLUTION	00003620
C	**	00003630
C	GMI = 2.0	00003640
C	RC = RADIUS OF CURVATURE	00003650
C	ROFF = OFFSET DISTANCE TO CENTER OF CURVATURE	00003660
C	PHIO = INITIAL OPENING ANGLE FROM VERTICAL AXIS	00003670
C	PHIN = FINAL OPENING ANGLE FROM VERTICAL AXIS	00003680
C	**	00003690
C	GMI = 3.0 (-3.0 DISCRETE ARCLENGTHS)	00003700
C	FM = NO. OF RIPT'S GIVEN	00003710
C	RIPT = DISCRETE RADII	00003720
C	XIPT = DISCRETE XI'S (OR ARCLENGTHS)	00003730
C	**	00003740
C		00003750
C	DIMENSION RIPT(200), XIPT(200), R(200), XSI(200), WITH(200),	00003760
C	1 WFE(200), RHOX(200), GAMMA(200), SARB(200), SURF(200),	00003770
C	2 GDA(408), RHOP(200)	00003780
C	DIMENSION XJ(400), RJ(400), DER(400)	00003790
C		00003800
C	EQUIVALENCE (GDA(1), GMI), (GDA(2), EN),	00003810
C	1 (GDA(3), PFLAG), (GDA(4), RA1,RC),	00003820
C	2 (GDA(5), AXL, ROFF), (GDA(6), ANX, PHIO),	00003830
C	3 (GDA(7), PHIN), (GDA(8), EM),	00003840
C	4 (GDA(9), RIPT), (GDA(20), XIPT)	00003850


```

20 IF (PFLAG.NE.0.0) WRITE(6,22)
22 FORMAT(1H1,3X,24HGEOMETRY DATA FOR CONE OR CYLINDER// 35X,22HNUMB0004310
1ER OF STATIONS - ,14//6X,7HRA1 =,1PE13.4,7X,7HAXL =,E13.4,7X,00004320
2 7HANX =,E13.4)
00004330
00004340
C
DEL = AXL/(EN - 1.0)
SINFI = SIND(ANX)
COSFI = COSD(ANX)
WTH(1) = A0 * COSFI/RA1
WFE(1) = 0.0
RHOX(1) = RA1/A0
R(1) = RA1
00004350
00004360
00004370
00004380
00004390
00004400
00004410
00004420
C
DO 30 I = 2,N
R(I) = R(I-1) + DEL * SINFI
WTH(I) = A0 * COSFI / R(I)
WFE(I) = 0.0
30 RHOX(I) = R(I)/A0
GO TO 95
00004430
00004440
00004450
00004460
00004470
00004480
00004490
00004500
00004510
00004520
00004530
C
35 IF (PFLAG.NE.0.0) WRITE(6,37) IRGN,N,RC,ROFF,PHIO,PHIN
37 FORMAT(1H1,3X,24HGEOMETRY DATA FOR REGION, 13,18,1 (SPHERE - TOROID
XD) // 35X,22HNUMB0004540
1ER OF STATIONS - ,14//6X,7HRC =,1PE13.4,7X,7HROFF =,E13.4,7X,00004550
2 7HPHIO =,E13.4,7X,7HPHIN =,E13.4 )
ANGSP = PHIN - PHIO
00004560
00004570
00004580
00004590
00004600
00004610
00004620
00004630
00004640
00004650
00004660
00004670
00004680
00004690
00004700
00004710
00004720
C
DO 40 I = 1,NN
APHI = BPHI + DEL
ASINP = SIND(APHI)
ACOSP = COSD(APHI)
R(I+1) = R(I) + RC * (ASINP - RSINP)
WFE(I) = AU/RC
IF(ROFF.EQ.0.0) GO TO 38
WTH(I) = A0 * RSINP / R(I)

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GO TO 39	00004730
38 WTH(I) = WFE(I)	00004740
39 RHOX(I) = R(I)/AO	00004750
BPHI = APhi	00004760
BSINP = ASINP	00004770
BCOSP = ACOSP	00004780
40 CONTINUE	00004790
DEL = ARS(DEL)	00004800
WFE(N) = AO/RC	00004810
IF(ROFF.EQ.0.0) GO TO 45	00004820
WTH(N) = AO * RSINP / R(N)	00004830
GO TO 46	00004840
45 WTH(N) = WFE(N)	00004850
46 RHOX(N) = R(N)/AO	00004860
DEL = DEL * RC * 0.01745329	00004870
IF(ICYL.EQ.0) GO TO 95	00004880
DO 47 I=1,N	00004890
47 WTH(I)=0.0	00004900
GO TO 95	00004910
C	00004920
50 IF(GMI - 4.0) 75, 51, 51	00004930
C	00004940
51 WRITE (6,55)	00004950
55 FORMAT (/// 5X, 44HARBITRARY FUNCTIONS AND CONICS NOT AVAILABLE)	00004960
C	00004970
CALL EXIT	00004980
STOP	00004990
C	00005000
C	00005010
75 M = EM	00005020
MM = M - 1	00005030
MM2 = M - 2	00005040
C	00005050
IF (PFLAG.NE.0.0) WRITE(6,76)IRGN,N, (RIPT(I), XIPT(I), I = 1,M)00005060	
76 FORMAT(1H,31X,24HGEOMETRY DATA FOR REGION,13,18H (DISCRETE POINT00005070	
15) //35X,20HNUMBER OF STATIONS - ,14//16X,1HR,16X,2HX1 //	00005080
2 (3X,1P2E20.71.)	00005090
C	00005100
SARB(1) = 0.0	00005110
IF (GMI) 81, 77, 77	00005120
77 DXI = XIPT(M) - XIPT(1)	00005130
DO 80 IL = 1,MM	00005140
SURB = 0.0	00005150

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DLI = XIPT(IL+1) - XIPT(IL)
K = (DLI/DLXI * FN + 1.0) * 5.0
AK = K
DDL = DLI/AK
KP1 = K + 1
DO 78 JI = 1, KP1
AJI = JI - 1
XJ(JI) = XIPT(IL) + AJI * DDL
78 CONTINUE
C
CALL CODIMA(KP1, XJ, RJ, XIPT, RIPT, M, -1.0)
C
DO 79 JR = 1, K
DLR(JR) = RJ(JR+1) - RJ(JR)
DLS = SQRT(DLR(JR)**2 + DDL**2)
79 SURB = SURB + DLS
SARB(IL+1) = SARB(IL) + SURB
80 CONTINUE
GO TO 82
C
R1 SARB(M) = XIPT(M) - XIPT(1)
82 DEL = SARB(M)/(FN-1.0)
SURF(1) = 0.0
DO 85 I = 1, NN
85 SURF(I+1) = SURF(I) + DEL
C
CALL CODIMA (N, SURF, R, SARB, RIPT, M, -1.0)
C
RHOX(1) = R(1)/A0
DELSQ = DEL * DFL
DO 86 I = 1, NN
86 RHOX(I+1) = R(I+1)/A0
C
**
95 DEL = DEL/A0
DELSQ = DEL * DFL
DO 105 I = 1, N
DFNM = 2. * RHOX(I) * DFL
IF(RHOX(I).EQ.0.) GO TO 97
IF (I.NE.1) GO TO 98
GAMA(I) = (2. * (RHOX(I+1) - RHOX(I)) + RHOX(I+1) - RHOX(I+2))/DENM
GO TO 105
97 GAMA(I) = 1. * F+10
GO TO 105
98 IF (I.FQ. N) GO TO 100

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GAMA(I) = (RHOX(I+1) - RHOX(I-1)) / DENM
GO TO 105
100 GAMA(I) = (3. * (RHOX(I) - RHOX(I-1)) + RHOX(I-2) - RHOX(I-1)) / DENM
105 CONTINUE
C
IGM = GMI
GO TO (125,125,110,100,100), IGM
C
110 DO 122 I = 1,N
IF(RHOX(I) .EQ. 0.) GO TO 116
WTH(I) = (SQRT(1. - (GAMA(I) * RHOX(I)) ** 2)) / RHOX(I)
DENOM = RHOX(I) * WTH(I) * DELSQ
F(I,NE,1) GO TO 112
WFE(I) = (-2. * RHOX(I) + 5. * RHOX(I+1) - 4. * RHOX(I+2) + RHOX(I+3)) / DENOM
GO TO 122
112 IF (I .EQ. N) GO TO 115
WFE(I) = (2. * RHOX(I) - RHOX(I-1) - RHOX(I+1)) / DENOM
GO TO 122
115 WFE(I) = (-2. * RHOX(I) + 5. * RHOX(I-1) - 4. * RHOX(I-2) + RHOX(I-3)) / DENOM
GO TO 122
116 IF(I .EQ. 1) GO TO 122
118 WFE(N) = WFE(N-1)
WTH(N) = WFE(N)
122 CONTINUE
C
IF(RHOX(1) .NE. 0.) GO TO 125
WFE(1) = WFE(2)
WTH(1) = WFE(1)
C
125 IF (PFLAG .EQ. 0.0) GO TO 1000
WRITE (6,130) (I, R(I), WTH(I), WFE(I), RHOX(I), GAMA(I),
1 I = 1,N)
130 FORMAT (1H-,9X,1H1,9X,4HR(I), 10X,8HW(THETA),11X,
1 5HW(XI),11X,7HRHOX(I),10X,7HGAMA(I) // (111,1P5E17.7) )
C
1000 DEL2 = 2. * DEL
BTAT1 = -577 * CFE * DEL
BTAT3 = -577 * CZ * DEL
C
EN1 = 1.
1005 IF(R(1) .NE. 0.) GO TO 2000
C

```

EN1 = 2.	00006020
DO 1010 I = 1,4	00006030
FM6(I) = 0.	00006040
DO 1010 J = 1,4	00006050
FM2(I,J) = 0.	00006060
1010 FM4(I,J) = 0.	00006070
C FORM UPPER BOUNDARY MATRICES FOR CLOSED SHELL	00006080
FM4(1,1) = 1.	00006090
IF(ENF - 1.) 1120,1130,1140	00006100
1120 EM2(4,4) = 1. /DEL	00006120
1121 EM2(3,3) = 1. /DEL	00006130
FM4(2,2) = 1.	00006140
GO TO 2000	00006150
1130 EM2(2,1) = 1. /DEL	00006160
EM4(1,2) = 1.	00006170
1135 EM4(3,3) = 1.	00006180
EM4(4,4) = 1.	00006190
GO TO 2000	00006200
1140 IF(ENF.NF.2.) GO TO 1150	00006210
FM4(4,3) = 1.	00006220
GO TO 1121	00006230
1150 FM4(2,2) = 1.	00006240
GO TO 1135	00006250
C	00006260
2000 RETURN	00006270
FND	00006280

\$IBFIC CF3P	0006290
C PARABOLIC CURVE FITTING SUBROUTINE (THREE POINTS)	0006300
C	0006310
C SUBROUTINE CODIM4 (N1, X, Y, XI, YI, N2, SHAPE)	0006320
C	0006330
C ARGUMENTS	0006340
C N1 NO. OF POINTS TO INTERPOLATE	0006350
C X LOCATION OF POINTS TO BE INTERPOLATED	0006360
C Y ANSWERS	0006370
C XI INDEPENDENT ARGUMENT	0006380
C YI DEPENDENT ARGUMENT	0006390
C N2 NO. OF ARGUMENTS	0006400
C SHAPE 0 = FITS END WITH STRAIGHT LINE 1 = CURVE, LAST 3 PTS.	0006410
C	0006420
C DIMENSION X(1),Y(1),XI(1),YI(1),D(2),A(2),R(2),C(2)	0006430
C	0006440
100 IN = 0	0006450
XK = SHAPE	0006460
C	0006470
C DO 800 N = 1,N1	0006480
C	0006490
IF (N2-2) 110,115,120	0006500
110 Y(N) = YI(N2)	0006510
GO TO 800	0006520
C	0006530
115 Y(N) = (YI(2)-YI(1))/(XI(2)-XI(1))* (X(N)-XI(1))+YI(1)	0006540
GO TO 800	0006550
C	0006560
120 J = 1	0006570
125 IF(XI(J)-X(N)) 130,140,150	0006580
140 Y(N) = YI(J)	0006590
GO TO 800	0006600
C	0006610
130 J = J+1	0006620
IF(J-N2) 125,125,145	0006630
145 Y(N) = (YI(N2)-YI(N2-1))/(XI(N2)-XI(N2-1))*(X(N)-XI(N2-1))	0006640
1 + YI(N2 - 1)	0006650
GO TO 800	0006660
C	0006670
150 IF(J-2) 115,155,160	0006680
155 K = 3	0006690
JJ = 1	0006700
GO TO 185	0006710

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160 IF(J-N2) 170,165,145
165 K = N2-1
    JJ = 2
    GO TO 185
170 IF(J-IN) 180,200,180
180 JJ = 3
    K = J
C
185 DO 200 M = 1,2
    X1 = XI(K-1)-XI(K)
    X2 = XI(K)-XI(K-2)
    X3 = XI(K-2)-XI(K-1)
    Y1 = YI(K-1)-YI(K)
    Y2 = YI(K)-YI(K-2)
    Y3 = YI(K-2)-YI(K-1)
    XX1 = XI(K-2)**2
    XX2 = XI(K-1)**2
    XX3 = XI(K)**2
    D(M) = XX1*X1 + XX2*X2 + XX3*X3
    A(M) = (YI(K-2)*X1 - YI(K-1)*X2 + YI(K)*X3)/D(M)
    B(M) = (XX1*Y1 + XX2*Y2 + XX3*Y3)/D(M)
    C(M) = YI(K-2) - A(M)*XX1 - B(M)*XI(K-2)
    200 K = K+1
300 P1 = X(N)*(A(1)*X(N)+B(1)) + C(1)
    P2 = X(N)*(A(2)*X(N)+B(2)) + C(2)
    AL = (X(N)-XI(J-1))/(XI(J)-XI(J-1))
    S = YI(J)*AL + YI(J-1)*(1.0-AL)
    GO TO (320,330,350),JJ
C
320 P2 = P1
    AL = (X(N)-XI(1))/(XI(2)-XI(1))
    S = AL*YI(2) + (1.0-AL)*YI(1)
    IF (SHAPE) 321,322, 322
321 XM1 = ARS (YI(2) - YI(1)) / (XI(2) - XI(1))
    XM2 = ARS (YI(3) - YI(2)) / (XI(3) - XI(2))
    XK = 1.0 - ARS (XM1 - XM2) / (XM1 + XM2)
322 P1 = S + XK *(P2-S)
    GO TO 350
C
330 P1 = P2
    AL = (X(N)-XI(N2-1))/(XI(N2)-XI(N2-1))
    S = AL* YI(N2) + (1.0-AL)*YI(N2-1)
    IF (SHAPE) 331,332, 332

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331	X-1) = ABS (YI(N2 - 1) - YI(N2)) / (X1(N2 - 1) - X1(N2))	00007160
	XM2 = ABS (YI(N2 - 2) - YI(N2 - 1)) / (X1(N2 - 2) - X1(N2 - 1))	00007170
	XK = 1. - ABS (XM1 - XM2) / (XM1 + XM2)	00007180
332	P2 = S + XK*(P1-S)	00007190
		00007200
350	E1 = ABS (F1-S)	00007210
	F2 = ABS (P2-S)	00007220
	IN = J	00007230
	IF(E1+E2) 700,700,750	00007240
700	Y(N) = S	00007250
	GO TO 800	00007260
750	YNUM = E1 * AL * P2 + (1. - AL) * E2 * P1	00007270
	YDEN = E1 * AL + (1. - AL) * E2	00007280
	Y(N) = YNUM / YDEN	00007290
800	CONTINUE	00007300
		00007310
900	RETURN	00007320
	END	00007330

SORIGIN	CHAIN	00007340
SIRFTC CDAFIT		00007350
C	CURVE FIT SUBROUTINE	00007360
C		00007370
C	SUBROUTINE CRVFIT	00007380
C		00007390
C	THE NOMENCLATURE IS VERY SIMILAR TO THAT IN THE DA DATA REGION	00007400
C	AS EXPLAINED IN THE EXECUTIVE PROGRAM. THE SUFFIX TB (TABLE)	00007410
C	HAS BEEN ADDED TO EACH PARAMETER.	00007420
C		00007430
C	THE TABLES ARE SET UP AS FOLLOWS	00007440
C	TAB(1) NO. OF STATIONS GIVEN	00007450
C	TAB(2) STATION NO. = 1.	00007460
C	TAB(3) PARAMETER VALUE AT STATION 1.	00007470
C	TAB(4)FF STATIONS AND VALUES INTERLACED.	00007480
C	THE LAST STATION MUST BE N BECAUSE CODIMA WILL NOT EXTRAPOLATE	00007490
C		00007500
C	REAL MASS, MO	00007510
C		00007520
C	DIMENSION CDA(697), DTB(41), FKTR(41), EITR(41), ALFTR(41),	00007530
C	1 DNATB(41), ITB(41), ENTB(41), EMIB(41), PNTR(41), PFETB(41),	00007540
C	2 PHTB(41), DZOTR(41), VZOTR(41), QZOTB(41), DFOTB(41),	00007550
C	3 VFOTB(41), QFOTB(41),	00007560
C	4 D(200), EK(200), EI(200), ALF(200), DNA(200), T(200), ENT(200),	00007570
C	5 EMT(200), PN(200), PFE(200), PTH(200), DZ0(200), VZ0(200),	00007580
C	6 AZ0(200), DF0(200), VF0(200), AF0(200), X(200),	00007590
C	7 STA(20), VAL(20)	00007600
C		00007610
C	EQUIVALENCE	00007620
C	1(CDA(83), EITB), (CDA(124), ALFTR), (CDA(165), DNATB),	00007630
C	2(CDA(206), ITB), (CDA(247), ENTB), (CDA(288), EMIB),	00007640
C	3(CDA(329), PNTR), (CDA(370), PFETR), (CDA(411), PHTB),	00007650
C	4(CDA(452), DZOTB), (CDA(493), VZOTB), (CDA(534), QZOTB),	00007660
C	5(CDA(575), DFOTR), (CDA(616), VFOTB), (CDA(657), QFOTB)	00007670
C		00007680
C	EQUIVALENCE	00007690
C	1(DA(1240), EK),(DA(1440), EI),(DA(1640), ALF),(DA(1840), DNA),	00007700
C	2(DA(2040), T),(DA(2240), ENT), (DA(2440), MT),(DA(2640), PN),	00007710
C	3(DA(2840), PFE),(DA(3040), PTH), (DA(3240), Z0),(DA(3440), VZ0),	00007720
C	4(DA(3640), AZ0),(DA(3840), DF0), (DA(4040), VF0),(DA(4240), AF0),	00007730
C	5(DA(4400), H0),(DA(4600), EU),(DA(4800), PO1),(DA(5000), ENFO),	00007740
C	6(DA(5200), RESTRT)	00007750
C		00007760

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COMMON DA(4511), EM2(4,4), FMA(4,4), FM6(4), S1, S2, ELAM2,
1 Z(4,200), XX(4,200), A2(4,4), B2(4,4), C2(4,4), E(4,4),
2 F(4,4), GA(4,4), A(4,4), B(4,4), C(4,4), G(4), EC(4), DEL2,
3 SL1, SL2, N, NTH, NTPR, NTPW, I, K, L,
4 S77, S78, BTAL1, BTA33, MC(20), OMG2(200), ZP(3,200),
5 Z2P(3,200), Z3P(3,200), TIMX, IDEL, PRM1, FNF, PRI, JT, NJT, V1
6 XXX(2800), INDER, ICYL,
1 JELLO, IVX, CONV, NO, IV, NOT, PE2( 75), PS( 75), PM1( 75),
2 P(4, 75), PP(4, 75), FUN(4), RH, RHO, WT, GAM, GMU( 75), BP, AP,
3 VEL, ACC, R1, ZAP, PIE, RADIUS, NSTART, NSAVE
4 , KODES1, KODES2, KOVER1, KODER2
C
N = FN
S3 = FO * H0 * (1. - POI **2)
DO 50 I = 1, 697
50 CDA(I) = 0.
C
IF(INSTART.EQ.0) GO TO 65
READ(12) KODE S1
IF(KODES1.NE.KODEF52) GO TO 5513
READ(12) OMG2(I), I=1, 2002, INDER, ICYL, JFLLQ, IVX, CONV, NO, IV, NOT,
1 (PE2(I), I=1, 918),
3 (DA(I), I=2640, 42839),
2 (DA(I), I=3240, 3639), (DA(I), I=3840, 4039)
REWIND 12
IV=1
JELLO=0
TIMX = TIMX + IDEL
JI = JIMX / IDEL + 1.E-6
PRNT = JT
C
65 CALL DECRD ( CDA )
PRINT TABLES ON NEG. IMD.
C
IF(DTR.EQ.0) GO TO 90
WRITE ( 6,70) (I, DTR(I), EKTR(I), ELTB(I), ALFTB(I), DNATR(I),
1 TIB(I), ENIB(I), EMIB(I), I = 1, 41)
70 FORMAT(///10X, 16HCURVE FIT TABLES ///14X, 3HDTB, 8X, 4HFKTB, 8X,
1 4HELIB, 8X, 5HALEIB, 7X, 5HDNAIB, 8X, 3HTIB, 8X, 4HENIB, 8X, 4HEMIB /
2 (18, 1P8F17.3) )
C
WRITE ( 6,72) (I, PNTR(I), PFETB(I), PTHTR(I), DZOTB(I),
1 VZOTB(I), QZOTB(I), DEOIB(I), VFOIB(I), QFOIB(I), I = 1, 41)

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72 FORMAT(// 11X,4HENTB, 6X,5HREFTB, 6X,5HRTITB, 6X,5HDTOTB, 6X, 000008200		FORM COL. OF STATION NOS.	
1	5HVZOTB, 6X,5HQZOTB, 6X,5HDFOTB, 6X,5HVFOTB, 6X,5HQFOTB //		000008210
2	(16, 1P9E11.2) ,		000008220
C			
90	DO 92 I = 1,N		000008230
92	X(I) = I		000008240
C			
100	IF(DVB.NE. 1.E+10) GO TO 120		000008250
DO	105 I = 1,N		000008260
105	D(I) = DVB(2)		000008270
GO	TO 200		000008280
C			
120	IF(OTB..EQ. U.) GO TO 600		000008290
NOSTA	= OTB		000008300
ICDA	= 1		000008310
IDA	= 1040		000008320
IXX	= 1		000008330
GO	TO 2000		000008340
C			
200	IF(EKTB.NE. 1.E+10) GO TO 220		000008350
DO	205 I = 1,N		000008360
205	EK(I) = EKTB(2)		000008370
GO	TO 300		000008380
C			
220	NOSTA = EKTB		000008390
ICDA	= 42		000008400
IDA	= 1240		000008410
IXX	= 2		000008420
GO	TO 2000		000008430
C			
300	IF(E1TB.NE. 1.E+10) GO TO 320		000008440
DO	305 I = 1,N		000008450
305	E1(I) = E1TB(2)		000008460
GO	TO 400		000008470
C			
320	NOSTA = E1TB		000008480
ICDA	= 83		000008490
IDA	= 1440		000008500
IXX	= 3		000008510
GO	TO 2000		000008520
C			
320	NOSTA = E1TB		000008530
ICDA	= 83		000008540
IDA	= 1440		000008550
IXX	= 3		000008560
GO	TO 2000		000008570
C			
400	IF(ALFTB.NE. 1.E+10) GO TO 420		000008580
DO	405 I = 1,N		000008590
405	AL(I) = ALFTB(2)		000008600
GO	TO 2000		000008610
C			
420	NOSTA = ALTB		000008620
ICDA	= 83		000008630
IDA	= 1440		000008640
IXX	= 3		000008650
GO	TO 2000		000008660
C			
420	NOSTA = ALTB		000008670
ICDA	= 83		000008680
IDA	= 1440		000008690
IXX	= 3		000008700
GO	TO 2000		000008710
C			
420	NOSTA = ALTB		000008720
ICDA	= 83		000008730
IDA	= 1440		000008740
IXX	= 3		000008750
GO	TO 2000		000008760
C			
420	NOSTA = ALTB		000008770
ICDA	= 83		000008780
IDA	= 1440		000008790
IXX	= 3		000008800
GO	TO 2000		000008810
C			
420	NOSTA = ALTB		000008820
ICDA	= 83		000008830
IDA	= 1440		000008840
IXX	= 3		000008850
GO	TO 2000		000008860
C			
420	NOSTA = ALTB		000008870
ICDA	= 83		000008880
IDA	= 1440		000008890
IXX	= 3		000008900
GO	TO 2000		000008910
C			
420	NOSTA = ALTB		000008920
ICDA	= 83		000008930
IDA	= 1440		000008940
IXX	= 3		000008950

405	ALF(I) = ALFTR(2)	00008630
	GO TO 500	00008640
C		
420	IF(ALFTR.EQ.0.) GO TO 500	00008650
	NOSTA = ALFTR	00008660
	ICDA = 124	00008670
	IDA = 1640	00008680
	IXX = 4	00008690
	GO TO 2000	00008700
C		
500	IF(DNATR.NE.1.E+10) GO TO 520	00008710
	DO 505 I = 1,N	00008720
	DNAT(I) = DNATR(2)	00008730
	505 MNT(I) = MASS * D(I) / EI(I) * S3	00008740
	GO TO 600	00008750
C		
520	NOSTA = DNATR	00008760
	ICDA = 165	00008770
	IDA = 1840	00008780
	IXX = 5	00008790
	GO TO 2000	00008800
C		
580	DO 582 I = 1,N	00008810
	582 MNT(I) = MASS * D(I) / EI(I) * S3	00008820
C		
600	IF(TTR.NE.1.E+10) GO TO 620	00008830
	DO 605 I = 1,N	00008840
	605 T(I) = TTR(2)	00008850
	GO TO 700	00008860
C		
620	IF(TTR) 622,900,630	00008870
	622 NOSTA = -TTR	00008880
	ICDA = 206	00008890
	IDA = 2040	00008900
	IXX = 6	00008910
	GO TO 2000	00008920
C		
630	DO 632 I = 1,N	00008930
	632 T(I) = ENTERP(X(I), TTR)	00008940
C		
700	IF(ENTR.NE.1.E+10) GO TO 720	00008950
	DO 705 I = 1,N	00008960
	705 ENT(I) = ENTR(2)	00008970
		00008980
		00008990
		00009000
		00009010
		00009020
		00009030
		00009040
		00009050

GO TO 800	00009060
C	00009070
720 IF(ENTR) 722,800,730	00009080
722 NOSTA = -ENTR	00009090
ICDA = 247	00009100
IDA = 2240	00009110
IXX = 7	00009120
GO TO 2000	00009130
C	00009140
730 DO 732 I = 1,N	00009150
732 EMT(I) = ENTERP(X(I), FMTB)	00009160
C	00009170
800 IF(EMTB.NE. 1.E+10) GO TO 820	00009180
DO 805 I = 1,N	00009190
805 EMT(I) = EMTB(2)	00009200
GO TO 900	00009210
C	00009220
820 IF(EMTB) 822,900,830	00009230
822 NOSTA = -EMTB	00009240
ICDA = 288	00009250
IDA = 2440	00009260
IXX = 8	00009270
GO TO 2000	00009280
C	00009290
830 DO 832 I = 1,N	00009300
832 EMT(I) = ENTERP(X(I), FMTB)	00009310
C	00009320
900 IF(PNTR.NE. 1.F+10) GO TO 920	00009330
DO 905 I = 1,N	00009340
905 PN(I) = PNTR(2)	00009350
GO TO 1000	00009360
C	00009370
920 IF(PNTR) 922,1000,930	00009380
922 NOSTA = -PNTR	00009390
ICDA = 329	00009400
IDA = 2640	00009410
IXX = 9	00009420
GO TO 2000	00009430
C	00009440
930 DO 932 I = 1,N	00009450
932 PN(I) = ENTERP(X(I), PNTR)	00009460
C	00009470
1000 IF(PFEIB.NE. 1.F+10) GO TO 1020	00009480

DO 1005	I = 1,N	00009490
1005 PFF(I) = PFFTR(2)		00009500
GO TO 1100		00009510
C		00009520
1020 IF(PFFTR)	1022,1100,1030	00009530
1022 NOSTA = -PFFTR		00009540
ICDA = 370		00009550
IDA = 2840		00009560
IXX = 10		00009570
GO TO 2000		00009580
C		00009590
1030 DO 1032	I = 1,N	00009600
1032 PFE(I) = ENTERP(X(I), PFFTR)		00009610
C		00009620
1100 IF(PTHIR,NF,1,F+10) GO TO 1120		00009630
DO 1105	I = 1,N	00009640
1105 PTH(I) = PTHIR(2)		00009650
GO TO 1200		00009660
C		00009670
1120 IF(PTHIR)	1122,1200,1130	00009680
1122 NOSTA = -PTHIR		00009690
ICDA = 411		00009700
IDA = 3040		00009710
IXX = 11		00009720
GO TO 2000		00009730
C		00009740
1130 DO 1132	I = 1,N	00009750
1132 PTH(I) = ENTERP(X(I), PTHIR)		00009760
C		00009770
1200 IF(DZ0IR,NF,1,F+10) GO TO 1220		00009780
DO 1205	I = 1,N	00009790
1205 DZ0(I) = DZ0IR(2)		00009800
GO TO 1300		00009810
C		00009820
1220 IF(DZ0IR)	1222,2100,1230	00009830
1222 NOSTA = -DZ0IR		00009840
ICDA = 452		00009850
IDA = 3240		00009860
IXX = 12		00009870
GO TO 2000		00009880
C		00009890
1230 DO 1232	I = 1,N	00009900
1232 DZ0(I) = ENTERP(X(I), DZ0IR)		00009910

C	1300 IF(VZOTR,NF,1,F+10) GO TO 1320	00009920
	DO 1305 I = 1,N	00009930
	1305 VZ0(I) = VZOTR(2)	00009940
	GO TO 1400	00009950
C		00009960
		00009970
		00009980
	1320 IF(VZOTB) 1322,1400,1330	00009990
	1322 NOSTA = -VZOTR	00010000
	ICDA = 493	00010010
	IDA = 3440	00010020
	IXX = 13	00010030
	GO TO 2000	00010040
C		00010050
		00010060
		00010070
	1400 IF(QZOTR,NF,1,F+10) GO TO 1420	00010080
	DO 1405 I = 1,N	00010090
	1405 AZ0(I) = QZOTR(2) /MO(I)	00010100
	GO TO 1500	00010110
C		00010120
	1420 IF(QZOTB) 1422,1500,1430	00010130
	1422 NOSTA = -QZOTR	00010140
	ICDA = 534	00010150
	IDA = 3640	00010160
	IXX = 14	00010170
	GO TO 2000	00010180
C		00010190
	1430 DO 1432 I = 1,N	00010200
	QZ0 = ENTRP(X(I), QZOTB)	00010210
	1432 AZ0(I) = QZ0 /MO(I)	00010220
	GO TO 1500	00010230
C		00010240
	1480 DO 1482 I = 1,N	00010250
	1482 AZ0(I) = AZ0(I) /MO(I)	00010260
C		00010270
	1500 IF(DF0TB,NF,1,F+10) GO TO 1520	00010280
	DO 1505 I = 1,N	00010290
	1505 DF0(I) = DF0TB(2)	00010300
	GO TO 1600	00010310
C		00010320
	1520 IF(DF0TB) 1522,1600,1530	00010330
	1522 NOSTA = -DF0TB	00010340

ICDA = 575	00010350
IDA = 3840	00010360
IXX = 15	00010370
GO TO 2000	00010380
C	00010390
1530 DO 1532 I = 1,N	00010400
1532 DF0(I) = FINTERP(X(I), DF0IR)	00010410
C	00010420
1600 IF(VF0IR *NF * J.F+10) GO TO 1620	00010430
DO 1605 I = 1,N	00010440
1605 VF0(I) = VF0IR(2)	00010450
GO TO 1700	00010460
C	00010470
1620 IF(VF0IR) 1622,1700,1630	00010480
1622 NOSTA = -VF0IR	00010490
ICDA = 616	00010500
IDA = 4040	00010510
IXX = 16	00010520
GO TO 2000	00010530
C	00010540
1630 DO 1632 I = 1,N	00010550
1632 VF0(I) = FINTERP(X(I), VF0IR)	00010560
C	00010570
1700 IF(QF0IR *NF * J.F+10) GO TO 1720	00010580
DO 1705 I = 1,N	00010590
1705 AF0(I) = QF0IR(2) /MO(I)	00010600
GO TO 2100	00010610
C	00010620
1720 IF(QF0IR) 1722,2100,1730	00010630
1722 NOSTA = -QF0IR	00010640
IDA = 657	00010650
JA = 4240	00010660
IXX = 17	00010670
GO TO 2000	00010680
C	00010690
1730 DO 1732 I = 1,N	00010700
QF0 = FINTERP(X(I), QF0IR)	00010710
1732 AF0(I) = QF0 /MO(I)	00010720
GO TO 2100	00010730
C	00010740
1780 DO 1782 I = 1,N	00010750
1782 AF0(I) = AF0(I) /MO(I)	00010760
GO TO 2100	00010770

```

C
2000 K0 = 0
K2 = 2 * NOSTA
DO 2005 I = 2, K2, 2
K0 = K0 + 1
KX = ICDA + I - 1
STA(K0) = CDA(KX)
2005 VAL(K0) = CDA(KX+1)
CALL CODIM4 (N,X,DA(IDA), STA,VAL,NOSTA, 1.)
C
GO TO (200, 300, 400, 500, 580, 700, 800, 900, 1000, 1100, 1200,
1 1300, 1400, 1480, 1600, 1700, 1780), IXX
C
2100 IF(TIMX.NE.IDEL) GO TO 3050
IF(ENF.NE.ENFO) GO TO 5000
IDEL2 = IDEL **2
DO 2110 I = 1,N
OMG2(I) = S77 * MO(I) * S78
ZP(1,I) = DFO(I)
ZP(3,I) = DZO(I)
Z2P(1,I) = AFO(I) * IDEL2 + 2. * DFO(I)
Z2P(3,I) = AZO(I) * IDEL2 + 2. * DZO(I)
Z3P(1,I) = 6. * (AFO(I)*IDEL2 + VFO(I)*IDEL) + 9. * DFO(I)
2110 Z3P(3,I) = 6. * (AZO(I)*IDEL2 + VZO(I)*IDEL) + 9. * DZO(I)
C
WRITE (6,3000) (DA(I), I=1,32), DA(4441), DA(4477), (I, P(I),
1 EK(I), EL(I), ALF(I), DNA(I), J(I), ENJ(I), I = 1,N)
3000 FORMAT( 1H1//10X, 12HINITIAL DATA// 6X,7HEN =,1PE12.3, 8X,
1 7HAQ =,E12.3, 8X,7HHQ =,E12.3, 8X,7HENFL =,E12.3, 8X,
2 7HSIGO =,E12.3, 8X,7HENFO =,E12.3, 8X,7HENFL =,E12.3, 8X,
3 7HPOI =,E12.3// 6X,7HHEIA =,E12.3, 8X,7HPLXI =,E12.3, 8X,
4 7HSPRL =,E12.3, 8X,7HUK =,E12.3// 6X,7HVK =,E12.3, 8X,
5 7HMK =,E12.3, 8X,7HEMK =,E12.3, 8X,7HTAU1 =,E12.3, 8X,
6 7HENT1 =,E12.3, 8X,7HP11 =,E12.3, 8X,7HTAU2 =,E12.3, 8X,
7 7HENT2 =,E12.3// 6X,7HP12 =,E12.3, 8X,7HTAU3 =,E12.3, 8X,
8 7HENT3 =,E12.3, 8X,7HP13 =,E12.3, 8X,7HMASS =,E12.3, 8X,
9 7HCFE =,E12.3, 8X,7HCZ =,E12.3, 8X,7HSKEF =,E12.3, 8X,
X 7HSKZ =,E12.3, 8X,7HSUM =,E12.3, 8X,7HEN1 =,E12.3, 8X,
1 7HDEL =,E12.3// 6X,7HBCIIP =,E12.3, 8X,7HSCIBM =,E12.3// 15X,
2 1HD, 10X,7HEK, 10X,7HE1, 10X,3HALF, 9X,3HDNA, 10X,1HT, 10X,
3 3HENT, 9X,3HEMT // (18, 8E12.3) )
WRITE (6,3015) (I, PN(I), PFF(I), PTH(I), DZO(I), VZO(I),
1 AZO(I), DFO(I), VFO(I), AFO(I), I = 1,N)

```

3005	FORMAT(/// 12X,2HPN, 8X,3HPFE, 8X,3HPTH, 8X,3HDZ0, 8X,3HVZ0, 8X,	00011210
I	3HAZ0, 8X,3HDF0, 8X,3HVFO, 8X,3HAF0 // (16, 1P9F11.2))	00011230
C		00011240
	GO TO 5000	00011250
3050	CONTINUE	00011260
5000	RETURN	00011270
5513	WRITE(6,5514) KODES1,KODES2	00011280
5514	FORMAT(1H0,54HINPUT COMMON IS WRONG--CHECK TAPE NOS.--KODES1,KODES2,1290	00011300
	1S2=,2112)	00011310
	STOP	00011320
	END	

```

SIBFIC CODES
C PARABOLIC CURVE FITTING SUBROUTINE (THREE POINTS)
C
C SUBROUTINE CODIMA (N1, X, Y, X1, Y1, N2, SHAPE)
C
C ARGUMENTS
C N1 NO. OF POINTS TO INTERPOLATE
C X LOCATION OF POINTS TO BE INTERPOLATED
C Y ANSWERS
C X1 INDEPENDENT ARGUMENT
C Y1 DEPENDENT ARGUMENT
C N2 NO. OF ARGUMENTS
C SHAPE 0 = FITS END WITH STRAIGHT LINE 1 = CURVE, LAST 3 PTS.
C
C DIMENSION X(1),Y(1),X1(1),Y1(1),D(2),A(2),B(2),C(2)
C
C 100 IN = 0
C XK = SHAPE
C DO 800 N = 1,N1
C
C IF (N2-2) 110,115,120
C 110 Y(N) = Y1(N2)
C GO TO 800
C
C 115 Y(N) = (Y1(7)-Y1(1))/(X1(2)-X1(1))* (X(N)-X1(1))+Y1(1)
C GO TO 800
C
C 120 J = 1
C 125 IF(X1(J)-X(N)) 130,140,150
C 140 Y(N) = Y1(J)
C GO TO 800
C
C 150 J = J+1
C IF(J-N2) 125,125,142
C 145 Y(N) = (Y1(N2)-Y1(N2-1))/(X1(N2)-X1(N2-1))*(X(N)-X1(N2-1))
C + Y1(N2-1)
C GO TO 800
C
C 150 IF(J-2) 115,155,160
C 155 K = 3
C JJ = 1
C GO TO 185

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160 IF(J-N2) 170,165,142
165 K = N2-1
      JJ = 2
      GO TO 185
170 IF(J-IN) 180,300,180
180 JJ = 3
      K = J
C
185 DO 200 M = 1,2
      X1 = XI(K-1)-XI(K)
      X2 = XI(K)-XI(K-2)
      X3 = XI(K-2)-XI(K-1)
      Y1 = YI(K-1)-YI(K)
      Y2 = YI(K)-YI(K-2)
      Y3 = YI(K-2)-YI(K-1)
      XX1 = XI(K-2)**2
      XX2 = XI(K-1)**2
      XX3 = XI(K)**2
      D(M) = XX1*X1 + XX2*X2 + XX3*X3
      A(M) = (YI(K-2)*X1 + YI(K-1)*X2 + YI(K)*X3)/D(M)
      B(M) = (X1*Y1 + X2*Y2 + X3*Y3)/D(M)
      C(M) = YI(K-2) - A(M)*X1 - B(M)*X2 - C(K-2)
200 K = K+1
300 P1 = X(N)*(A(1)*X(N)+B(1)) + C(1)
      P2 = X(N)*(A(2)*X(N)+B(2)) + C(2)
      AL = (X(N)-XI(J-1))/(XI(J)-XI(J-1))
      S = YI(J)*AL + YI(J-1)*(1-AL)
      GO TO (320,330,340),JJ
C
370 P2 = P1
      AL = (X(N)-XI(1))/(XI(2)-XI(1))
      S = AL*YI(2) + (1-AL)*YI(1)
      IF (SHAPE) 321,322,322
321 XM1 = ABS (YI(2) - YI(1)) / (XI(2) - XI(1))
      XM2 = ABS (YI(3) - YI(2)) / (XI(3) - XI(2))
      XK = 1. - ABS (XM1 - XM2) / (XM1 + XM2)
322 P1 = S + XK *(P2-S)
      GO TO 350
C
390 P1 = P2
      AL = (X(N)-XI(N2-1))/(XI(N2)-XI(N2-1))
      S = AL*YI(N2) + (1-AL)*YI(N2-1)
      IF (SHAPE) 331,332,332

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331 XM1 = ABS (X1AN2 - 1) - Y1(N2) / (X1(N2 - 1) - X1(N2)) 0012190
XM2 = ABS (Y1(N2 - 2) - Y1(N2 - 1)) / (X1(N2 - 2) - X1(N2 - 1)) 0012200
XK = 1 - ABS (XM1 - XM2) / (X1 + XM2) 0012210
332 P2 = S + XK * (P1 - S) 0012220
C 0012230
350 E1 = ABS (P1 - S) 0012240
E2 = ABS (P2 - S) 0012250
IN = J 0012260
IF (E1 + E2) 700, 700, 750 0012270
700 Y(N) = S 0012280
GO TO 800 0012290
750 YNUM = E1 * AL * P2 + (1 - AL) * E2 * P1 0012300
YDEN = E1 * AL + (1 - AL) * E2 0012310
Y(N) = YNUM / YDEN 0012320
800 CONTINUE 0012330
C 0012340
900 RETURN 0012350
END 0012360

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SIBFC ENTP	00012370
C LINEAR INTERPOLATION SUBROUTINE **ENTERP**	6J-997
C	00012380
C	00012390
C SELECTS THE VALUE AT EITHER END OF TABLE WHEN ARGUMENT EXCEEDS	00012400
C LIMIT, THEN CONTINUES	00012410
C	00012420
C SUBROUTINE ARGUMENTS	00012430
C X	00012440
C	00012450
C TAB(1) NO. OF PAIRS OF ARGUMENTS AND VALUES IN TABLE	00012460
C TAB(2), ETC ARGUMENTS AND FUNCTIONS INTERLACED	00012470
C	00012480
C FUNCTION ENTERP (X,TAB)	00012490
C	00012500
C DIMENSION TAB(101)	00012510
C IF (TAB) 9,9,8	00012520
9 ENTERP = - TAB	00012530
RETURN	00012540
8 N = TAB	00012550
DO 5 I=1,N	00012560
1 IF (TAB(2*I)-X) 5,4,3	00012570
3 IF (I-1) 6,6,7	00012580
7 ENTERP = TAB(2*I-1) + (X-TAB(2*I-2)) * (TAB(2*I+1) - TAB(2*I-1))	00012590
V / (TAB(2*I) - TAB(2*I-2))	00012600
RETURN	00012610
4 ENTERP = TAB(2*I+1)	00012620
RETURN	00012630
5 CONTINUE	00012640
M = 2*N+1	00012650
K = M	00012660
105 WRITE (6,10) X, TAB(K)	00012670
10 FORMAT (// 10X, 39H LIMITS OF TABLE EXCEEDED BY ARGUMENT = 1PE12.4	00012680
I / 10X, E12.4, 24H = VALUE USED FROM TABLE)	00012690
ENTERP = TAB(K)	00012700
RETURN	00012710
6 M = 2*N+1	00012720
K = 3	00012730
GO TO 105	00012740
END	

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SORIGIN          CHAIN          00012750
SYBFC ACCN2      00012760
C                CALCULATION OF SYMMETRIC HYDRO-ELASTIC IMPACT
SUBROUTINE ACCN 00012770
DIMENSION PM(200), ZDOT(3,200), COM2(4), COM3(4), RA(200) 00012780
1, DETINT(4), VINT(4), PM2(75), ZDO2(3,200), CON2(4), 00012790
2, CON3(4) 00012800
COMMON DATA(200), V, TDEL, PRNT(3), JT, NJT, V1, X(200), INDR, ICYL, 00012810
1, JELCO, IVX, CONV, NO, IV, NOT, PE2(75), PS(75), PM1(75), 00012820
2, P1(75), P2(75), P3(75), P4(75), P5(75), P6(75), P7(75), P8(75), P9(75), 00012830
3, VEL, ACC, RI, Z, P1E, R 00012840
EQUIVALENCE (PA(32), DEL), (DA(34), VIN), (DA(44), WFF), (DA(264), PV), 00012850
1, DA(324), ZDOT), (DA(35), TNU), (DA(384), ZDO2), (DA(41), RA) 00012860
VIN IS THE INITIAL VELOCITY, 1/5*DEL IS THE RADIAL INCREMENT 00012870
THE RADIUS OF CURVATURE, R, IS EQUAL TO 1/WFF. RHO IS THE LIQUID 00012880
DENSITY, LBS/IN**3. WT IS THE WEIGHT OF THE ENTERING BODY. 00012890
IF (IND.EQ.0) GO TO 300 00012900
IF (JT.GT.1) GO TO 900 00012910
B=0. 00012920
ACC=0. 00012930
VEL=VIN 00012940
GO TO 940 00012950
900 FORCE = PI*RA(1)**2/4.*PM(1) 00012960
DO 910 I=2,NOT 00012970
VEL = (PA(1)-RA(1-1))/2. 00012980
910 FORCE = FORCE + 4.*PI*VEL*RA(1)*PM(1) 00012990
ACC = FORCE/WT 00013000
940 VEL=VEL+ TDEL*ACC*32.2*12. 00013010
B=B+ VEL*TDEL +ACC*32.2*6.*TDEL**2 00013020
A= (2.*R*B)**.5 00013030
NO=A/DEL+1. 00013040
IF (NO.EQ.1) GO TO 10 00013050
DO I N=2,NO 00013060
GMU(N)=(1.-(RA(N)/A)**2)**.5 00013070
P(1,N)=GMU(N) 00013080
PP(1,N)=1. 00013090
P(2,N)=.5*(15.*GMU(N)**3-3.*GMU(N)) 00013100
P(3,N)=.5*(15.*GMU(N)**2-3.) 00013110
P(4,N)=.125*(15.*GMU(N)**5-75.*GMU(N)**3+15.*GMU(N)) 00013120
P(5,N)=.125*(15.*GMU(N)**4-21.*GMU(N)**2+15.) 00013130
P(6,N)= 1./16.*(42.*GMU(N)**7-593.*GMU(N)**5+315.*GMU(N)**3-75.* 00013140
GMU(N)) 00013150
1 PP(4,N)=1./16.*(7.*429.*GMU(N)**6-2.*567.*GMU(N)**4+315.*3.*GMU(N)) 00013160
00013170

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1**2-35.)
10 IF( A-RA(NO) .LT. DEL/2.) GO TO 100
   NOT = NO + 1
   GO TO 102
100 NOT = NO
   IF ( NO .GT. 1) GO TO 102
   R1=0.
   Z=1.
   GO TO 103
102 R1 = RA(NOT) - DEL/2.
   Z = (1.-(R1/A1**2)**.5
   LET = NOT - 1
   DO 110 I = 1,LET
   CON = 2./PIE*(VEL**2*R1/A/GMU(1) + A*GMU(1) * ACC )
110 PM1(I) = RH * CON
103 PM1(NOT) = -2./PIE*VEL**2/DEL*RRH*(PIE/2.-ARSIN(R1/A))
1 -1./PIE*ACC*A*RH/DEL*(-R1*Z+ A*PIE/2.- A*ARSIN(R1/A))
   NOP=NO+2
   DO 120 L = 1, NOP
120 ZDOT(3,L) = ZDOT(3,L) + (DEL*ZDOT(3,L)
300 IF (NO .LT. 2) GO TO 302
   IF (NO.GT. 3) GO TO 310
   BE=(ZDOT(3,NO)-ZDOT(3,1))/(GMU(NO)-1.)
   AE = ZDOT(3,1) - BE
   CE = 0.
   DE = 0.
   BA=(ZDOT(3,NO)-ZDOT(3,1))/(GMU(NO)-1.)
   AA = ZDOT(3,1) - BA
   CA = 0.
   DA = 0.
   GO TO 320
305 AF = ZDOT(3,1)
   BE = 0.
   DE = 0.
   CE = 0.
   AA = ZDOT(3,1)
   BA = 0.
   CA = 0.
   DA = 0.
   GO TO 330
310 N1= NO/3 + 1
   N2= 2*NO/3 + 1
   E2=(ZDOT(3,N1)-ZDOT(3,1))/(GMU(N1)-1.)- (ZDOT(3,N2)-ZDOT(3,1))/(

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1 GMU(N2)-1. ) 00013620
E3= (ZD01(3,N1)-ZD01(3,1))/(GMU(N1)-1. ) - (ZD01(3,N0)-ZD01(3,1))/(GMU(N0)-1. ) 00013630
1/(GMU(N0)-1. ) 00013640
E4= ( GMU(N1)**3-1. )/(GMU(N1)-1. ) - ( GMU(N2)**3-1. )/( GMU(N2)-1. ) 00013650
1-1. ) 00013660
E5= ( GMU(N1)**3-1. )/(GMU(N1)-1. ) - (GMU(N0)**3-1. )/(GMU(N0)-1. ) 00013670
1-1. ) 00013680
A2=(ZD02(3,N1)-ZD02(3,1))/(GMU(N1)-1. ) - (ZD02(3,N0)-ZD02(3,1))/( GMU(N0)-1. ) 00013690
1 GMU(N2)-1. ) 00013700
A3= (ZD02(3,N1)-ZD02(3,1))/(GMU(N1)-1. ) - (ZD02(3,N0)-ZD02(3,1))/(GMU(N0)-1. ) 00013710
1/(GMU(N0)-1. ) 00013720
A4= ( GMU(N1)**3-1. )/(GMU(N1)-1. ) - ( GMU(N2)**3-1. )/( GMU(N2)-1. ) 00013730
1-1. ) 00013740
A5= ( GMU(N1)**3-1. )/(GMU(N1)-1. ) - (GMU(N0)**3-1. )/(GMU(N0)-1. ) 00013750
1-1. ) 00013760
DE=(E2/(GMU(N1)-GMU(N2)) -E3/(GMU(N1)-GMU(N0)) )/( GMU(N1)-GMU(N0)) ) / 00013770
1 (E4/( GMU(N1)-GMU(N2)) -E5/( GMU(N1)-GMU(N0)) ) / 00013780
CF=(E2-DE**24)/(GMU(N1)-GMU(N2)) 00013790
BE=(ZD01(3,N1)-ZD01(3,1))/(GMU(N1)-1. ) -CE*(GMU(N1)**2-1. )/(GMU(N1)-1. ) 00013800
1(GMU(N1)-1. ) -DE*(GMU(N1)**3-1. )/( GMU(N1)-1. ) 00013810
AE=ZD01(3,1)-BE-CE-DE 00013820
DA=(A2/(GMU(N1)-GMU(N2)) -A3/(GMU(N1)-GMU(N0)) )/( GMU(N1)-GMU(N0)) ) / 00013830
1 (A4/( GMU(N1)-GMU(N2)) -A5/( GMU(N1)-GMU(N0)) ) / 00013840
CA=(A2-DA**A4)/(GMU(N1)-GMU(N2)) 00013850
BA=(ZD02(3,N1)-ZD02(3,1))/(GMU(N1)-1. ) -CA*(GMU(N1)**2-1. )/(GMU(N1)-1. ) 00013860
1(GMU(N1)-1. ) -DA*(GMU(N1)**3-1. )/( GMU(N1)-1. ) 00013870
AA=ZD02(3,1)-RA-CA-DA 00013880
320 TINI(1)=AE/3.+BE/4.+CF/5.+DE/6. 00013890
TINI(2)=BE/24.+2.*CE/35.+3.*DE/48. 00013900
TINI(3)=-FE/(8.**24.)+DE/(8.**20.) 00013910
TINI(4)=BE/(16.**40.)-DE/(16.**120.) 00013920
DETINI(1)=AA/3.+BA/4.+CA/5.+DA/6. 00013930
DETINI(2)=BA/24.+2.*CA/35.+3.*DA/48. 00013940
DETINI(3)=-RA/(8.**24.)+DA/(8.**20.) 00013950
DETINI(4)=BA/(16.**40.)-DA/(16.**120.) 00013960
IF (NOT .EQ. 1) GO TO 350 00013970
LET=NOT-1 00013980
DO 50 I=1,LET 00013990
PM2(I)=0.0 00014000
DO 45 M=1,4 00014010
CON2(M)=R/A*VEL* ( P(M,1) + ( RA(1)/A)**2/GMU(1) * PP(M,1) ) 00014020
CON3(M)=A*P(M,1) 00014030
45 PM2(I)=PM2(I)+RH*FUN(M)*(CON2(M)*TINI(1)+CON3(M)) 00014040

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```

1*DEFINT(M)
50 CONTINUE
350 CONTINUE
ALF=0.
AL2=0.
AL3=0.
AL4=1.
CON2I(1)=R*VEL/A/DEL*(A*ARSIN(2)*(35./64.*ALF +5./8.*AL2
1 +3./4.*AL3 +AL4) -R1*Z*(ALF/8. *( -6.*Z**6 +7./3.*Z**4
2 +35./12.*Z**2 +35./8.)* +AL2/6.*( -4.*Z**4 +
3 5./2.*Z**2 +15./4.)* +AL3/4.*( -2.*Z**2 +3.))
CON3I(1)=A**2*ARSIN(Z)/2./DEL*(35./64.*ALF +5./8.*AL2
1 +3./4.*AL3 +AL4) -A*Z*R1/2.*(ALF/4.*(Z**6 +7./6.*Z**4
2 +35./24.*Z**2 +35./16.)* +AL2/3.*(Z**4 +5./4.*Z**2
3 +15./8.)* +AL3/2.*(Z**2 +3./2.)* +AL4)/DEL
ALF=0.
AL2=0.
AL3=5./2.
AL4=-3./2.
CON2I(2)=R*VEL/A/DEL*(A*ARSIN(2)*(35./64.*ALF +5./8.*AL2
1 +3./4.*AL3 +AL4) -R1*Z*(ALF/8. *( -6.*Z**6 +7./3.*Z**4
2 +35./12.*Z**2 +35./8.)* +AL2/6.*( -4.*Z**4 +
3 5./2.*Z**2 +15./4.)* +AL3/4.*( -2.*Z**2 +3.))
CON3I(2)=A**2*ARSIN(Z)/2./DEL*(35./64.*ALF +5./8.*AL2
1 +3./4.*AL3 +AL4) -A*Z*R1/2.*(ALF/4.*(Z**6 +7./6.*Z**4
2 +35./24.*Z**2 +35./16.)* +AL2/3.*(Z**4 +5./4.*Z**2
3 +15./8.)* +AL3/2.*(Z**2 +3./2.)* +AL4)/DEL
ALF=0.
AL2=63./8.
AL3=-70./8.
AL4=15./8.
CON2I(3)=R*VEL/A/DEL*(A*ARSIN(2)*(35./64.*ALF +5./8.*AL2
1 +3./4.*AL3 +AL4) -R1*Z*(ALF/8. *( -6.*Z**6 +7./3.*Z**4
2 +35./12.*Z**2 +35./8.)* +AL2/6.*( -4.*Z**4 +
3 5./2.*Z**2 +15./4.)* +AL3/4.*( -2.*Z**2 +3.))
CON3I(3)=A**2*ARSIN(Z)/2./DEL*(35./64.*ALF +5./8.*AL2
1 +3./4.*AL3 +AL4) -A*Z*R1/2.*(ALF/4.*(Z**6 +7./6.*Z**4
2 +35./24.*Z**2 +35./16.)* +AL2/3.*(Z**4 +5./4.*Z**2
3 +15./8.)* +AL3/2.*(Z**2 +3./2.)* +AL4)/DEL
ALF=429./16.
AL2=-693./16.
AL3=315./16.
AL4=-35./16.

```

CON2I(4) = R*VEL/A/DEL*(A*ARSIN(Z)*(35./64.*ALF + 5./8.*AL2			00014490
1	+ 3./4.*AL3 + AL4) - R1*Z*(ALF/8. *(-6.*Z**6 + 7./3.*Z**4		00014500
2	+ 35./12.*Z**2 + 35./8.) + AL2/6.*(-4.*Z**4 +		00014510
3	5./2.*Z**2 + 15./4.) + AL3/4.*(-2.*Z**2 + 3.)) \		00014520
CON3I(4) = A**2*ARSIN(Z)/2./DEL*(35./64.*ALF + 7./8.*AL2			00014530
1	+ 3./4.*AL3 + AL4) - A*Z*R1/2.*(ALF/4.*(Z**6 + 7./6.*Z**4		00014540
2	+ 35./24.*Z**2 + 35./16.) + AL2/3.*(Z**4 + 5./4.*Z**2		00014550
3	+ 15./8.) + AL3/2.*(Z**2 + 3./2.) + AL4) /DEL		00014560
PM2(NOT) = 0.0			00014570
DO 115 M=1,4			00014580
115 PM2(NOT)= RH*FUN(M)*(CON2I(M)* TINTI(M)			00014590
1 + CON3I(M) * DETINT(M)) + PM2(NOT)			00014600
IF (IND.EQ.0) GO TO 230			00014610
WRITE (6,220)			00014620
220 FORMAT (1H, 8H EL PRES 10X, 10HAV EL PRES 7X, 8HTOT PRES 9X,			00014630
1 10HSHELL VEL //)			00014640
230 WRITE (6,240) ZDOI(3,1) , PM2(1)			00014650
240 FORMAT (1H+ 52X, E12.5 / 1X, E12.5)			00014660
IF (IND.NE.0) GO TO 180			00014670
DO 160 I= 1,NOT			00014680
PM2(I) = (FLOAT(IV)*PE2(I) + PM2(I)) / FLOAT(IV + 1)			00014690
160 PE2(I) = PM2(I)			00014700
GO TO 200			00014710
180 DO 190 I=1,NOT			00014720
190 PE2(I) = PM2(I)			00014730
200 DO 210 I= 1,NOT			00014740
210 PM(I) = PM2(I) + PM1(I)			00014750
WRITE (6,61) PM2(1), PM(1)			00014760
61 FORMAT (1H+ 18X, E12.5, 5X, E12.5)			00014770
RETURN			00014780
END			00014790

\$ORIGIN C:CHAIN		00014800
\$IRFTC 157DR1		00014810
C	6J-157DR	00014820
C		00014830
SUBROUTINE DEFLTN		00014840
C		00014850
DIMENSION R(200), D(200), EK(200), ENI(200), EMT(200), PFE(200), WTHD(200),		00014860
1	PTH(200), PN(200), WFE(200), ALF(200), DNA(200), WTHD(200),	00014870
2	RHOX(200), GAMA(200), EI(200), I(200), P(4,4,200), EML(4,4),	00014880
3	EM3(4,4), EM5(4), EVIN(4,4), EM3N(4,4), EM5N(4)	00014890
C		00014900
REAL MASS, LM11, LM22, LM33, NM11, NM22, NM33,		00014910
1	MO	00014920
C		00014930
EQUIVALENCE (DA(1), EN), (DA(2), A), (DA(3), HO),		00014940
1	(DA(4), EO), (DA(5), SIGO), (DA(6), ENFO), (DA(7), ENFL),	00014950
2	(DA(8), POI), (DA(9), ITHETA), (DA(10), PIXI), (DA(11), SPRL),	00014960
3	(DA(12), UK), (DA(13), VK), (DA(14), WK), (DA(15), FMK),	00014970
4	(DA(16), TAU1), (DA(17), ENI1), (DA(18), P11), (DA(19), TAU2),	00014980
5	(DA(20), FNT2), (DA(21), F12), (DA(22), TAU3), (DA(23), FNT3),	00014990
6	(DA(24), P13), (DA(25), MASS), (DA(26), CFF), (DA(27), CZ),	00015000
7	(DA(28), SKFE), (DA(29), SKZ), (DA(30), SUM), (DA(31), EN1),	00015010
8	(DA(32), DEL), (DA(33), IND), (DA(36), RESIRI)	00015020
EQUIVALENCE (DA(4), R), (DA(240), WTHD), (DA(440), WFE),		00015030
1	(DA(640), GAMA), (DA(840), RHUX), (DA(1040), D), (DA(1240), EK),	00015040
2	(DA(1440), EI), (DA(1640), ALF), (DA(1840), DNA), (DA(2040), T),	00015050
3	(DA(2240), ENI), (DA(2440), EMI), (DA(2640), PN), (DA(2840), PFE),	00015060
4	(DA(3040), PTH), (DA(3240), DZ), (DA(3440), VZU), (DA(3640), AZO),	00015070
5	(DA(3840), DFO), (DA(4040), VEU), (DA(4240), AEJ), (DA(4440), EMI),	00015080
6	(DA(4456), EM3), (DA(4472), EM5), (DA(4476), EMIN), (DA(4492), EM3N),	00015090
7	(DA(4508), EM5N)	00015100
C		00015110
COMMON DA(4511), EM2(4,4), EM4(4,4), EM6(4,4), S1, S2, ELAN2,		00015120
1	Z(4,200), X(4,200), A2(4,4), B2(4,4), C2(4,4), G2(4,4), E(4,4),	00015130
2	F(4,4), GA(4,4), A(4,4), B(4,4), C(4,4), G(4,4), EC(4,4), DEL2,	00015140
3	SL1, SL2, N, NTH, NTPR, NTPW, I, K, L,	00015150
4	S77, S78, BTALL, BTAB3, NUC(200), OMG2(200), ZP(3,200),	00015160
5	Z2P(3,200), Z3P(3,200), TIME, IDEL, PRNT, ENF, PRI, JT, NJT, VI	00015170
6	XX(2800), INDER	00015180
C		00015190
C		00015200
N2 = SPRL		00015210
DO 300 I = 1,N		00015220

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      WITH = WTHD(I)
      GAM = GAMA(I)
      RHO = RHOX(I)
      S4 = ELAY2 * FK(I) * S1
      S6 = 3. * WFF(I) - WTH
      S7 = 3. * WTH - WFF(I)
      S80 = -4. * OMG2(I)
      S79 = -5. * OMG2(I)
      LM11 = S79 + 6. * BTAL1
      LM22 = S79
      LM33 = S79 + 6. * BTA33
      MM11 = -(S80 + 3. * BTAL1)
      MM22 = -S80
      MM33 = -(S80 + 3. * BTA33)
      NM11 = -OMG2(I) + .66666667 * BTAL1
      NM22 = -OMG2(I)
      NM33 = -OMG2(I) + .66666667 * BTA33
      IF(I - 1) 100, 2, 100
2 IF(ENI .GE. 2.) GO TO 95
      C
      BP = (-D(3) + 4.*D(2) - 3.*D(1)) / DEL2
      WFFP = (-WFF(3) + 4.*WFF(2) - 3.*WFF(1)) / DEL2
      TTP = (-ENT(3) + 4.*ENT(2) - 3.*ENT(1)) / DEL2
      DP = (-FK(3) + 4.*FK(2) - 3.*FK(1)) / DEL2
      EMTP = (-EMI(3) + 4.*EMI(2) - 3.*EMI(1)) / DEL2
      IRCX = 0
      IF(EMI .NE. 1.E+10) GO TO 20
      IRCX = FMI(2,1)
      IRM = 4439
      C
      20 S9 = ENF / RHO
      S3 = GAM * D(I)
      S5 = D(I) / 2. * S9
      S8 = S4 * S9 / 8. * S6 * S7
      S15 = S4 * S9 / 2.
      S9 = S9 ** 2
      S10 = S4 * (S2 * GAM**2 * WFF(I) + S9 / 2. * S6)
      S11 = S4 * S5 / D(I)
      IF(IRCX .EQ. 0) GO TO 83
      DO 22 K = 1, 32
      IX = IRM + K
      22 DA(IX) = 0.
      GO TO (21, 32, 33, 34, 35), IRCX

```

C	31	DA(I RM+1) = 1.	FREE BOUNDARY	00015660
		DA(I RM+6) = 1.		00015670
		DA(I RM+11) = 1.		00015680
		DA(I RM+32) = 1.		00015690
		GO TO 83		00015700
C	32	DA(I RM+1) = 1.	ROLLER BOUNDARY	00015710
		DA(I RM+22) = 1.		00015720
		DA(I RM+27) = 1.		00015730
		DA(I RM+32) = 1.		00015740
		GO TO 83		00015750
C	33	DA(I RM+16) = 1.	FIXED OR CLAMPED BOUNDARY	00015760
		DA(I RM+17) = 1.		00015770
		DA(I RM+22) = 1.		00015780
		DA(I RM+27) = 1.		00015810
		GO TO 83		00015820
C	34	DA(I RM+17) = 1.	SIMPLY SUPPORTED (HINGED)	00015830
		DA(I RM+22) = 1.		00015840
		DA(I RM+27) = 1.		00015850
		DA(I RM+32) = 1.		00015870
		GO TO 83		00015880
C	35	DA(I RM+11) = 1.	COMPLETE (CLOSED)	00015890
		DA(I RM+16) = 1.		00015910
		DA(I RM+17) = 1.		00015920
		DA(I RM+22) = 1.		00015930
		GO TO 83		00015940
C	83	DO 84 K = 1,4		00015950
		EM6(K) = 0.		00015960
		DO 84 L = 1,4		00015970
		EM2(K,L) = 0.		00015980
		EM4(K,L) = 0.		00015990
C	84	EM2(I,1) = D(I)/DEL		00016000
		EM4(I,1) = POI * S3		00016010
		EM4(I,2) = POI * CNF / RHO * U(I)		00016020
		EM4(I,3) = D(I) * (WFF(I) + POI * WFF(I))		00016030
		EM4(I,4) = -S5 * S1 = S8		00016040
		EM4(I,5) = D(I) * S1 / 2 + S4 / 8 * S / * 2		00016050
		EM4(I,6) = - GAM * EM2(I,2)		00016060
				00016070
				00016080

EM2(2,2) = EM2(2,2) /DEL	00016090
EM2(2,3) = S15 * S7	00016100
EM4(2,3) = - GAM * EM2(2,3)	00016120
EM2(2,3) = EM2(2,3) /DEL	00016130
EM4(3,1) = - S10	00016140
EM2(3,2) = S11 * S7 /DEL	00016150
EM4(3,2) = -S11 * GAM *(S7 + 2.*S2*WTH)	00016160
EM2(3,3) = S4 * (2.*S9 + S2 * GAM **2) /DEL	00016170
EM4(3,3) = -S4 *(3. + POI) * GAM * S9	00016180
EM2(3,4) = ELAM2 /DEL	00016190
EM4(3,4) = ELAM2 * S1 * GAM	00016200
EM2(4,3) = - 1. /DEL	00016210
EM4(4,1) = WFE(I)	00016220
EM6(I) = - ENT(I)	00016230
EM6(I) = ELAM2 * GAM * S1 * EMT(I)	00016240
DO 90 K = 1,4	00016250
DO 90 L = 1,4	00016260
90 EM2(K,L) = - EM2(K,L) /2.	00016270
GO TO 121	00016280
C	
95 IF(REST * NE. 0.) GO TO 94	00016290
IF(TIME * NE. TDEL) GO TO 97	00016300
IF(INDER.EQ.U) GO TO 94	00016310
IF(IND.GE.0) GO TO 97	00016320
94 DO 96 K = 1,4	00016330
DO 96 L = 1,4	00016340
EM1(K,L) = EM2(K,L)	00016350
96 EM3(K,L) = EM4(K,L)	00016360
REST = 0.	00016370
97 DO 98 K = 1,4	00016380
G2(K) = 0.	00016390
DO 98 L = 1,4	00016400
A2(K,L) = 2. * EM1(K,L)	00016410
C2(K,L) = -.25 * A2(K,L)	00016420
98 EM1(K,L) = 1.5 * EM1(K,L)	00016430
CALL MSU (4,4, EM3, L1, B2)	00016440
GO TO 300	00016450
100 IF(I - N) 102, 101, 102	00016460
101 BP = (D(N-2) - 4.*D(N-1) + 3.*D(N)) /DEL2	00016470
WFE = (WFE(N-2) - 4.*WFE(N-1) + 3.*WFE(N)) /DEL2	00016480
DP = (EK(N-2) - 4.*EK(N-1) + 3.*EK(N)) /DEL2	00016490
TP = (ENT(N-2) - 4.*ENT(N-1) + 3.*ENT(N)) /DEL2	00016500
EMTP = (EMT(N-2) - 4.*EMT(N-1) + 3.*EMT(N)) /DEL2	00016510
	00016520

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IRCX = 0
IF(FMIN.NF.1.E+10) GO TO 20
IRCX = F4M(2,1)
IRM = 4475
GO TO 20

C
102 BP = (D(1,1) - D(1-1)) / DEL2
WFFP = (WFF(1,1) - WFF(1-1)) / DEL2
DP = (ER(1,1) - ER(1-1)) / DEL2
ITP = (ENT(1,1) - ENT(1-1)) / DEL2
FMTP = (EMI(1,1) - EMI(1-1)) / DEL2
ALL EXCEPT CLOSED APEX

120 S3 = GAM * D(1)
S5 = D(1) / 2 * ENF / RHO
S8 = S4 * ENF / 8 * RHO * S5 * S7
S9 = (ENF / RHO) ** 2
S10 = S4 * (S2 * GAM ** 2 * WFF(1) + S9 / 2 * S5)
S11 = S4 * S5 / D(1)

C
121 DO 125 K = 1,4
DO 125 L = 1,4
125 E(K,L) = 0
E(1,1) = D(1) / DEL
F(1,1) = S3 + BP
S12 = WITH * WFF(1)
GAM2 = GAM ** 2
GA(1,1) = POI * RP * GAM - D(1) * (POI * S12 + GAM2 + S1 * S9 / 2)
1 - S4 * (S2 * GAM2 * WFF(1) ** 2 + S6 ** 2 * S9 / 8)
F(1,2) = S2 * S3 + S8
GA(1,2) = POI * ENF / RHO * BP - (3 - POI) * S5 * GAM - S11 * 2
1 * GAM * (S6 * S7 / 8 + S2 * S12)
F(1,3) = D(1) * (WFF(1) + POI * WITH) + S1
GA(1,3) = D(1) * (WFFP + GAM * (WFF(1) - WITH) + RP * (WFF(1) + POI *
1 WITH - S4 * S9 * GAM * (S6 / 2 + S2 * WFF(1))
F(1,4) = FLAM2 * WFF(1)
GA(1,4) = F(1,4) * S1 * GAM
F(2,1) = - F(1,2)
GA(2,1) = - S5 * GAM * (3 - POI) - S1 * ENF / 2 * BP / RHO + S11 * 2
1 * (- S2 * GAM * S12 + GAM / 8 * (6 * S12 - 7 * WFF(1) ** 2 - 3 * WITH
2 ** 2) - WFFP / 4 * (5 * WITH - 3 * WFF(1)) - S11 * DP / ER(1) / 4 * S6 * S7
F(2,2) = (D(1) / 2 * S1 + S4 / 8 * S7 ** 2) / DEL
F(2,2) = S1 / 2 * (GAM * D(1) + RP) - S4 / 8 * S7 * (2 * WFFP - GAM
1 * (5 * WFF(1) - 3 * WITH) + FLAM2 / 8 * DP * S1 * S7 ** 2

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GA(2,2) = - GAM * F(2,2) + D(I) * (S1/2 * S12 - S2) - S4 * (S2 * S5
1 * WTH**2 - S12/8 * S7**2)
00016960
E(2,3) = S11 * S7 / DEL
00016980
F(2,3) = S11 * (2 * S2 * GAM * WTH - WFFP + 3 * GAM * (WFE(I) -
00016990
1 * WTH) + S11 / EK(I) * DP * S7
00017000
GA(2,3) = - S5 * 2 * (WTH + POI * WFE(I)) + S4 * S5 / D(I) * (GAM *
00017010
1 * WFFP - 2 * GAM2 * WFE(I) - 2 * S2 * S9 * WTH + S7 * (GAM2 + S12)) - S11 /
00017020
2 * EK(I) * DP * GAM * S7
00017030
GA(2,4) = - POI * ELAM2 * WTH * ENF / RHO
00017040
F(2,4) = 0
00017050
F(3,1) = - F(1,3)
00017060
S13 = WTH + POI * WFE(I)
00017070
GA(3,1) = - D(I) * GAM * S13 + ELAM2 * EK(I) * S1 * (GAM * S2 * GAM2
00017080
1 * WFE(I) - GAM * WFFP - WFE(I) * (S9 - 2 * S12)) + S9 / 2 * (GAM
00017090
2 * (WFE(I) - WTH) - 3 * WFFP) - ELAM2 * DP * S1 * (S2 * GAM2 * WFE(I) + S9
00017100
3 / 2 * S6)
00017120
E(3,2) = F(2,3)
00017130
F(3,2) = S11 * (GAM * (WFE(I) * 3 - WTH * (5 + 2 * POI)) - WFFP)
00017140
1 + S11 * DP / EK(I) * S7
00017150
GA(3,2) = - D(I) * ENF / RHO * S13 + S11 * (2 * S2 * (S12 * WTH - GAM2 *
00017160
1 * (WFE(I) - 2 * WTH) - S2 * WTH) + GAM * WFFP + 3 * GAM2 * (WTH - WFE(I))
00017170
2 * (S12 * S7) - S11 * DP / EK(I) * (GAM * (2 * S2 * WTH + S7) )
00017180
E(3,3) = S4 * (2 * S9 + S2 * GAM2) / DEL
00017190
F(3,3) = - S4 * (S2 * GAM * (2 * S12 + GAM2) + 2 * GAM * S9) + ELAM2
00017200
1 * DP * S1 * (S2 * GAM2 + 2 * S9)
00017210
GA(3,3) = - D(I) * (WFE(I) * 2 + 2 * POI * S12 * WTH ** 2) + S4 * S9 * (S2 * (S12 -
00017220
1 * S9 + 2 * GAM2) + 2 * (GAM2 + S12) - S1 * S9 * DP * ELAM2 * (3 * POI) * GAM
00017230
E(3,4) = ELAM2 / DEL
00017240
F(3,4) = ELAM2 * GAM * (2 * - POI)
00017250
GA(3,4) = - FLAM2 * (S1 * S12 + POI * S9)
00017260
F(4,1) = EK(I) * WFE(I)
00017270
GA(4,1) = EK(I) * (WFFP + POI * GAM * WFE(I))
00017280
GA(4,2) = EK(I) * POI * ENF * WTH / RHO
00017290
E(4,3) = - EK(I) / DEL
00017300
F(4,2) = 0
00017310
F(4,3) = - EK(I) * POI * GAM
00017320
F(4,4) = 0
00017330
GA(4,3) = EK(I) * POI * S9
00017340
140 GA(1,1) = GA(1,1) - S77 * SKKE
00017350
GA(3,3) = GA(3,3) - S77 * SKZ
00017360
IF(1 * NE * N2) GO TO 142
00017370
S3 = A0 / EU * A0 / H0
00017380
GA(1,1) = GA(1,1) - UK * S3
00017390

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GA(2,2) = GA(2,2) - VK * S3
GA(3,3) = GA(3,3) - WK * S3
S3 = S3 / AV * EMK * WFF(I)
F(1,3) = F(1,3) - S3
GA(1,1) = GA(1,1) + S3 * WFF(I)
142 GA(4,4) = -1.
G(1) = (-PFE(I) + TIP - ELAW2 * S1 * GAMMA * FE(I) * EMT(I)) * DEL2
G(2) = (-PTH(I) - ENF/RHU * (ENT(I) + FLAW2 * S1 * WITH * WI(I)) * DEL2
G(3) = (-PN(I) - (WFF(I) + WITH) * ENT(I) - FLAW2 * S1 * (GAP * F * ATP
1 - EMT(I) * (S12 - S9)) * DEL2
G(4) = EMT(I) * DEL2
DO 150 K = 1,4
DO 150 L = 1,4
150 E(K,L) = 2. * F(K,L)
CALL MAD (4,4, E, F, A)
CALL MSU (4,4, E, F, C)
DO 160 K = 1,4
DO 160 L = 1,4
E(K,L) = -2. * E(K,L)
160 GA(K,L) = DEL2 * GA(K,L)
CALL MAD (4,4, E, GA, B)
DO 162 K = 1,4
G(K) = G(K) * IDEL
DO 162 L = 1,4
A(K,L) = A(K,L) * IDEL
B(K,L) = B(K,L) * IDEL
162 C(K,L) = C(K,L) * IDEL
IF(JT - 2) 163, 164, 165
163 S79 = -6. * QMG2(I)
S80 = 6.
GO TO 166
164 LM11 = S80 + 5.3333333 * BTALL
LM22 = S80
LM33 = S80 + 5.3333333 * HTA33
165 S79 = -2. * QMG2(I)
S80 = 11. / 3.
166 B(1,1) = B(1,1) + S79 + S80 * BTALL
B(2,2) = B(2,2) + S79
B(3,3) = B(3,3) + S79 + S8. * BTA33
G(1) = G(1) + LM11 * ZP(1,1) + NM11 * Z2P(1,1) + NM11 * Z3P(1,1)
G(2) = G(2) + LM22 * ZP(2,1) + NM22 * Z2P(2,1) + NM22 * Z3P(2,1)
G(3) = G(3) + LM33 * ZP(3,1) + NM33 * Z2P(3,1) + NM33 * Z3P(3,1)
IF(I - 2) 210, 170, 169

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169 IF(I - N) 185,200,185
C
170 CALL INV (4, C, PI, IERR)
CALL MMY (4,4,4, B2,C,EM4)
CALL MMY (4,4,4, EM4,B,B2)
CALL MSU (4,4, B2,A2,B2)
CALL INV (4, B2, PI, IERR)
IF(EN1 - 2) 176,172,172
172 CALL MMY (4,4,4, EM4,A,A2)
CALL MSU (4,4, A2,C2,A2)
CALL MMY (4,4,4, B2,A2,P(1,1,2))
GO TO 178
176 CALL MMY (4,4,4, B2,EM4,A2)
CALL MMY (4,4,4, A2,A,P(1,1,2))
178 CALL MMY (4,4,1, EM4,G,EM6)
CALL MSU (4,1, EM6,G2,G2)
CALL MMY (4,4,1, B2,G2,X(1,2))
C
DO 180 K = 1,4
G2(K) = G(K)
DO 180 L = 1,4
A2(K,L) = A(K,L)
B2(K,L) = B(K,L)
180 C2(K,L) = C(K,L)
GO TO 300
185 CALL MMY (4,4,4, C,P(1,1,I-1),EM4)
CALL MSU (4,4, B,EM4,EM4)
CALL INV (4, EM4, PI, IERR)
CALL MMY (4,4,1, C,X(1,I-1),EM6)
CALL MSU (4,1, G,EM6,EM6)
IF(I - N) 190,220,190
190 CALL MMY (4,4,4, EM4,A,P(1,1,I))
CALL MMY (4,4,1, EM4,EM6,X(1,I))
GO TO 300
C
200 CALL INV (4, A, PI, IERR)
CALL MMY (4,4,4, EM1N,EM2,GA)
CALL MMY (4,4,4, GA,A,EM2)
CALL MMY (4,4,4, EM1N,EM4,A)
CALL MAD (4,4, EM3N,A,A)
CALL MMY (4,4,4, EM2,B,E)
CALL MAD (4,4, A,E,R)
CALL MMY (4,4,4, EM2,C,F)

```

CALL MAD (4,4, GA, F, C)	00018260
CALL MMY (4,4,1, EM1, F, 46, EC)	00018270
CALL MSU (4,1, FM5N, EC, EC)	00018280
CALL MMY (4,4,1, EM2, G, E)	00018290
CALL MAD (4,1, EC, E, G)	00018300
DO 205 K = 1,4	00018310
DO 205 L = 1,4	00018320
GA(K,L) = 0.	00018330
205 E(K,L) = 0.	00018340
GO TO 185	00018350
I = 1, OPEN APEX	
210 CALL INV (4, C, PI, IERR)	00018360
CALL MMY (4,4,4, EM1, EM2, GA)	00018370
CALL MMY (4,4,4, GA, C, EM2)	00018380
CALL MMY (4,4,4, EM1, EM4, C)	00018390
CALL MAD (4,4, EM3, C, C)	00018400
CALL MMY (4,4,4, EM2, R, E)	00018410
CALL MSU (4,4, C, E, R2)	00018420
CALL MMY (4,4,4, FM2, A, E)	00018430
CALL MAD (4,4, GA, E, A)	00018440
DO 215 K = 1,4	00018450
DO 215 L = 1,4	00018460
215 A2(K,L) = -A(K,L)	00018470
CALL MMY (4,4,1, EM1, EM6, EC)	00018480
CALL MSU (4,1, FM5, EC, EC)	00018490
CALL MMY (4,4,1, EM2, G, F)	00018500
CALL MSU (4,1, EC, E, G2)	00018510
DO 217 K = 1,4	00018520
DO 217 L = 1,4	00018530
GA(K,L) = 0.	00018540
217 E(K,L) = 0.	00018550
GO TO 300	00018560
220 CALL MMY (4,4,1, EM4, EM6, Z(1,N))	00018570
300 CONTINUE	00018580
DEFLECTIONS	
DO 305 I = 1, N	00018590
I2 = N - I	00018600
IF(I2 - 1) 304, 310, 304	00018610
304 CALL MMY (4,4,1, P(1,1, I2, Z(1, I2+1), EM6)	00018620
305 CALL MSU (4,1, X(1, I2), EM6, Z(1, I2))	00018630
I = 1	
310 CALL MMY (4,4,1, R2, Z(1,2), FM6)	00018640
CALL MSU (4,1, G2, EM6, G2)	00018650
	00018660
	00018670
	00018680

00018690
00018700
00018710
00018720
00018730
00018740

CALL MMY (4,4,1, A2,Z(1,3),EM6)
CALL MSU (4,1, G2,EM6,G2)
CALL MMY (4,4,1, C2,G2,Z(1,1))
C
1000 RETURN
END

\$IBFIC MSUB		DECK NO. 8K-904	
C	MATRIX SUBTRACT SUBROUTINE		00018750
C			00018760
C	ARGUMENTS		00018770
C	L NO. OF ROWS		00018780
C	M NO. OF COLS		00018790
C	A(I,J) MRA		00018800
C	R(I,J) MSR		00018810
C	C(I,J) MSR		00018820
C	SUBROUTINE MSU(L,M,A,B,C)		00018830
	DIMENSION A(4,4), B(4,4), C(4,4)		00018840
	DO 30 I=1,L		00018850
	DO 30 J=1,M		00018860
	30 C(I,J)=A(I,J)-B(I,J)		00018870
	RETURN		00018880
	END		00018890

```

$IRFTC INVR5
C MATRIX INVERSION SUBROUTINE
C
C DECK NO. 8K-900
C
C MODIFICATION OF F1,4R444 BY D.J.HALLMAN,DEPT. 56,LA
C
C ARGUMENTS
C
C IOM INDICATOR OF ORDER (N) OF MATRIX A COMPILED FOR 4 X 4
C
C IERR INDICATOR OF ERROR RETURN =1,NORMAL. NUT=1,ERR
C
C MATRICES
C
C A(I,J) INPUT MATRIX N,N I,J
C
C LR(M) MATRIX OF LOCATIONS OF MAX ROW M,1
C
C LC(M) MATRIX OF LOCATIONS OF MAX COL 1,M
C
C SUBSCRIPTS
C
C I ROW OF A
C
C J COL OF A
C
C MI LOCATION OF PIVOT BEFORE INTERCHANGE,ROW OF MAX
C
C MJ LOCATION OF PIVOT BEFORE INTERCHANGE,COL OF MAX
C
C M LOCATION OF PIVOT,ROW AND COL
C
C N ORDER OF MATRIX
C
C VARIABLES
C
C P PIVOT ELEMENT,MAX ELEMENT BEFORE INTERCHANGE
C
C PI PI PRODUCT OF P(M) =VALUE OF DETERMINANT
C
C TEMPORARY
C
C TEMP INTERCHANGE AND REORDERING OF ELEMENTS OF A
C
C * * *
C
C SURROUTINE INV(IOM,A,PI,IERROR)
C
C DIMENSION A(4,4), LR(4), LC(4)
C
C SFTUP
C
C M=1
C
C N=IOM
C
C PI=1.0
C
C SEARCH REDUCED ARRAY FOR MAXIMUM ELEMENT
C
C 1000 P=0.0
C
C DO 1010 I=M,N
C
C DO 1010 J=M,N
C
C IF( ABS(P) - ABS( A(I,J) ) ) 1005,1010,1010
C
C 1005 P=A(I,J)

```

MI=I	00019340
MJ=J	00019350
1010 CONTINUE	00019360
LR(M)=MI	00019370
LC(M)=MJ	00019380
C INTERCHANGE MAXIMUM ROW WITH PIVOT ROW	00019390
2000 IF(MI-M)2100,2200,2100	00019400
2100 DO 2110 J=1,N	00019410
TEMP=A(MI,J)	00019420
A(MI,J)=-A(M,J)	00019430
2110 A(M,J)=TEMP	00019440
C INTERCHANGE MAXIMUM COL WITH PIVOT COL	00019450
2200 IF(MJ-M)2205,3000,2205	00019460
2205 DO 2210 I=1,N	00019470
TEMP=A(I,MJ)	00019480
A(I,MJ)=-A(I,M)	00019490
2210 A(I,M)=TEMP	00019500
C DIVIDE PIVOT COL BY PIVOT ELEMENT	00019510
3000 DO 3010 I=1,N	00019520
IF(I-M)3005,3010,3005	00019530
3005 A(I,M)=-A(I,M)/P	00019540
3010 CONTINUE	00019550
C ELIMINATE	00019560
4000 DO 4210 I=1,N	00019570
IF(I-M)4005,4210,4005	00019580
4005 DO 4110 J=1,N	00019590
IF(J-M)4105,4110,4105	00019600
4105 A(I,J)=A(I,M)*A(M,J)+A(I,J)	00019610
4110 CONTINUE	00019620
4210 CONTINUE	00019630
C DIVIDE PIVOT ROW BY PIVOT ELEMENT	00019640
5000 DO 5010 J=1,N	00019650
IF(J-M)5005,5010,5005	00019660
5005 A(M,J)=A(M,J)/P	00019670
5010 CONTINUE	00019680
A(M,M)=1.0/P	00019690
M=M+1	00019700
IF(M-N)1000,5020,5999	00019710
5020 P=A(M,M)	00019720
GO TO 3000	00019730
5999 M=N-1	00019740
6000 MI=LC(M)	00019750
MJ=LR(M)	00019760

C	RE-ORDER ROWS OF INVERSE	00019770
	IF(MI-M)6005,6200,6005	00019780
6005	DO 6010 J=1,N	00019790
	TEMP=A(M,J)	00019800
	A(I,J)=-A(MI,J)	00019810
6010	A(MI,J)=TEMP	00019820
C	RE ORDER COLS OF INVERSE	00019830
6200	IF(MJ-M)6205,7000,6205	00019840
6205	DO 6210 I=1,N	00019850
	TEMP=A(I,M)	00019860
	A(I,N)=-A(I,MJ)	00019870
6210	A(I,MJ)=TEMP	00019880
7000	M=M-1	00019890
	IF(M)9002,9001,6000	00019900
9001	IFERROR=1	00019910
	GO TO 9999	00019920
C	M IS LESS THAN ZERO	00019930
9002	IFERROR=2	00019940
9999	RETURN	00019950
	FND	00019960

ORIGIN	CHAIN	00019970
SIRFC WHERE		00019980
C 6-J-1570R	DTFRMINES PROGRAM FLOW	00019990
C		00020000
C	SUBROUTINE PATH	00020010
C		00020020
C	DIMENSION ZDOT(3,200), Z2DOT(3,200), PFF(200), PN(200)	00020030
C	REAL MASS, LM11, LM22, LM33, NM11, MM22, MM33, NM11, NM22, NM33,	00020040
C	MO	00020050
C	1	00020060
C	EQUIVALENCE (DA(1), EN), (DA(2), -AO), (DA(3), HO), (DA(4), EO), (DA(5), SIG), (DA(6), FNFO), (DA(7), FNFL), (DA(8), POI), (DA(9), THETA), (DA(10), PIX1), (DA(11), SPRL), (DA(12), UK), (DA(13), VK), (DA(14), WK), (DA(15), EMK), (DA(16), TAU1), (DA(17), EN1), (DA(18), P11), (DA(19), TAU2), (DA(20), EN2), (DA(21), P12), (DA(22), TAU3), (DA(23), EN3), (DA(24), P13), (DA(25), MASS), (DA(26), CFE), (DA(27), CZ), (DA(28), SKFF), (DA(29), SKZ), (DA(30), SUM), (DA(31), EN1), (DA(32), DEL), (DA(35), IND), (DA(39), DRW)	00020070
C	EQUIVALENCE (DA(40), R), (DA(240), WTHD), (DA(440), WFF), (DA(640), GAMA), (DA(840), RHGX), (DA(1040), D), (DA(1240), EK), (DA(1440), E1), (DA(1640), ALF), (DA(1840), DNA), (DA(2040), T), (DA(2240), EN1), (DA(2440), EN2), (DA(2640), PN), (DA(2840), PFF), (DA(3040), PTH), (DA(3240), ZDOT), (DA(3440), VZ), (DA(3640), AZ), (DA(3840), Z2DOT), (DA(4040), VEU), (DA(4240), AF), (DA(4440), EM1), (DA(4508), EM3), (DA(4472), EM5), (DA(4476), EM1N), (DA(4492), EM3N), (DA(4508), FM5N)	00020080
C	COMMON DA(4511), EM2(4,4), EM4(4,4), EM6(4), S1, S2, ELAM2,	00020090
C	1 Z(4,200), X(4,200), A2(4,4), B2(4,4), C2(4,4), G2(4), E(4,4),	00020100
C	2 F(4,4), GA(4,4), A(4,4), B(4,4), C(4,4), G(4), EC(4), DEL2,	00020110
C	3 SL1, SL2, N, NTH, NTPR, NTPW, I, K, L,	00020120
C	4 S77, S78, B1A11, B1A33, M0(200), OMG2(200), ZP(3,200),	00020130
C	5 Z2P(3,200), Z3P(3,200), TIMX, IDEL, PRNT, ENF, PRI, JT, NJT	00020140
C	IPRNT = PRNT	00020150
C	SL1 = 0.	00020160
C	IF(IPRNT.EQ. JT) GO TO 90	00020170
C	IF(JT.EQ. NJT) GO TO 90	00020180
C	SL1 = 1.	00020190
C	IF(DRW.EQ. 0.1) GO TO 90	00020200
C	SL1 = -1.	00020210
C	COMPUTE VELOCITIES, ACCELER.	00020220
C		00020230
C		00020240
C		00020250
C		00020260
C		00020270
C		00020280
C		00020290
C		00020300
C		00020310
C		00020320
C		00020330
C		00020340
C		00020350
C		00020360
C		00020370
C		00020380
C		00020390

```

90 S3 = 11.
S4 = 18.
S5 = 2.
S6 = 5.
S0=0.
S10=2.
S11=4.
S12=1.
IF(JT-2) 100,110,120
100 S3=6.
S4=6.
S0=0.
S10=0.
S5=0.
S6=0.
S11=0.
S12=0.
GO TO 120
110 S3=6.
S4=6.
S0=0.
S10=0.
S5=1.
S6=2.
S11=1.
S12=0.
120 S7 = 6. * IDEL
IDEL? = IDEL **2
C
DO 150 L = 1,N
DO 150 K = 1,2
ZDOT(K,L) = (S3 * Z(P(K,L)) - 4 * Z(P(K,L)) + S0 * Z2P(K,L) -
1 S10 * Z2P(K,L)) / S7
150 Z2DOT(K,L) = (S5 * Z(K,L) - S6 * ZP(K,L) + S11 * Z2P(K,L) -
1 S12 * Z3P(K,L)) / IDEL2
IF(JT.GT.1) GO TO 170
DO 160 L=1,N
Z2DOT(1,L)=ZDOT(1,L) / IDEL
Z2DOT(2,L)=0.
160 Z2DOT(3,L)=Z2DOT(3,L) / IDEL
170 CONTINUE
C
IF(SL1.LT.0.0) GO TO 100
00020400
00020410
00020420
00020430
00020440
00020450
00020460
00020470
00020480
00020490
00020500
00020510
00020520
00020530
00020540
00020550
00020560
00020570
00020580
00020590
00020600
00020610
00020620
00020630
00020640
00020650
00020660
00020670
00020680
00020690
00020700
00020710
00020720
00020730
00020740
00020750
00020760
00020770
00020780
00020790
00020800
00020810
00020820

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```

IF(JT.EQ.NJT) GO TO 200
IF(IND.FO.O) GO TO 50
PRNT = PRNT + PRI
GO TO 50
C
200 IF(TAU1 + TAU2 - TIMX.LE. 1.F-8) GO TO 210
      SFT UP NEW INTFVAL
      SECJND
C
      TDEL = TAU2 / FNT2
      PRNT = PRI2
      NJT = FNT2
      PRI = PRI2
      TIMX = TAU1
      GO TO 220
C
210 IF(TAU1 + TAU2 + TAU3 - TIMX.LE. 1.F-8) GO TO 50
      TDEL = TAU3 / FNT3
      PRNT = PRI3
      NJT = FNT3
      PRI = PRI3
      TIMX = TAU2 + TAU1
      THRD
C
220 JT = 1
      TDEL2 = TDEL **2
      DO 250 K = 1,3
      DO 250 I = 1,N
      IF(K-2) 231,232,233
      231 S8 = PFE(I) / MO(I)
      GO TO 240
      232 S8 = 0.
      GO TO 240
      233 S8 = PN(I) / MO(I)
      240 ZP(K,I) = Z(K,I)
      22P(K,L) = S8 * TDEL2 + 2. * Z(K,L)
      250 23P(K,L) = 6. * (S8 * TDEL2 + ZDOT(K,L) * TDEL) + 9. * Z(K,L)
      GO TO 80
C
300 WRITE (6,310) ((ZDOT(K,L), K=1,3), (Z2DOT(K,L), K=1,3), L=1,N)
310 FORMAT(//10X,28HVELOCITIES AND ACCELERATIONS // 15X,6HVEL(U),
      1 10X,6HVEL(V), 10X,6HVEL(W), 10X,6HACC(U), 10X,6HACC(V), 10X,
      2 6HACC(W) // (6X, 1P6E16.3) )
C
50 CONTINUE
80 RETURN
      END

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ORIGIN		CHAIN		
SIRFTC 157DR2				00021280
C 6J-157DR			COMPUTES INTERNAL LOADS	00021290
C				00021300
C				00021310
C				00021320
C				00021330
C				00021340
C				00021350
C				00021360
C				00021370
C				00021380
C				00021390
C				00021400
C				00021410
C				00021420
C				00021430
C				00021440
C				00021450
C				00021460
C				00021470
C				00021480
C				00021490
C				00021500
C				00021510
C				00021520
C				00021530
C				00021540
C				00021550
C				00021560
C				00021570
C				00021580
C				00021590
C				00021600
C				00021610
C				00021620
C				00021630
C				00021640
C				00021650
C				00021660
C				00021670
C				00021680
C				00021690
C				00021700

```

C
490 S3 = 1. - POI **2
491 S4 = S1 / 2.
492 S12 = SIGO / EO / S3
493 S20 = (HO / AO) **2
494 IF (ENI - 2.) 496,497,497
496 L1 = 1
497 GO TO 498
497 L1 = 2
498 WP = (-Z(3,3) + 4.*Z(3,2) - 3.*Z(3,1)) / DFL2
499 FETH(1) = ENF * WP + WTHD * Z(2,1)
500 DO 500 I = L1,N
500 FETH(I) = ENF / RHOX(I) * Z(3,I) + WTHD(I) * Z(2,I)
502 DO 1000 I = 1,N
502 IF (I - 1) 520,504,520
504 IF (ENI - 2.) 510,506,506
506 ENFEX = D(1) * ((S2 * Z(1,2) - Z(1,1)) + ENF * POI * (Z(2,2) - Z(2,1))) / DFL2
506 ENFEX = D(1) * ((S2 * Z(3,1)) - ENF * Z(2,1)) - ENF * Z(2,1)
506 ENFEX = 2. * ENF **2
507 ENTHX = 2. * ENFEX / S6
508 ENFTX = ENF * ENFEX / S6
509 FMFTX = ENF * Z(4,1) / S6
510 FMTHX = 2. * Z(4,1) / S6
511 GO TO 552
C
510 ROP = (-RHOX(3) + 4. * RHOX(2) - 3. * RHOX(1)) / DFL2
511 WP = (-Z(3,3) + 4. * Z(3,2) - 3. * Z(3,1)) / DFL2
512 FETHP = (-FETH(3) + 4. * FETH(2) - 3. * FETH(1)) / DFL2
513 VP = (-Z(2,3) + 4. * Z(2,2) - 3. * Z(2,1)) / DFL2
514 UP = (-Z(1,3) + 4. * Z(1,2) - 3. * Z(1,1)) / DFL2
515 FM6(4) = (-Z(4,3) + 4. * Z(4,2) - 3. * Z(4,1)) / DFL2
516 FM6(2) = VP
517 FM6(3) = WP
518 FM6(1) = UP
519 GO TO 550
520 IF (I - N) 540,530,540
C
530 WP = (Z(3,N-2) - 4. * Z(3,N-1) + 3. * Z(3,N)) / DFL2
531 FETHP = (FETH(N-2) - 4. * FETH(N-1) + 3. * FETH(N)) / DFL2
532 VP = (Z(2,N-2) - 4. * Z(2,N-1) + 3. * Z(2,N)) / DFL2
533 UP = (Z(1,N-2) - 4. * Z(1,N-1) + 3. * Z(1,N)) / DFL2
534 FM6(4) = (Z(4,N-2) - 4. * Z(4,N-1) + 3. * Z(4,N)) / DFL2

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```

ROP = (RHOX(N-2) - 4.*RHOX(N-1) + 3.*RHOX(N)) / DEL2
GO TO 515
C
540 WP = (Z(3,I+1) - Z(3,I-1)) / DEL2
FFTHP = (FFTH(I+1) - FFTH(I-1)) / DFL2
ROP = (RHOX(I+1) - RHOX(I-1)) / DEL2
VP = (Z(2,I+1) - Z(2,I-1)) / DEL2
UP = (Z(1,I+1) - Z(1,I-1)) / DEL2
FM6(4) = (Z(4,I+1) - Z(4,I-1)) / DEL2
GO TO 515
550 FFFE = -WP + WFF(I) * Z(1,I)
X(3,I) = FFFE
S11 = FNF / RHOX(I)
S5 = S11 * Z(2,I) + GAMA(I) * Z(1,I) + WTHD(I) * Z(3,I)
S6 = UP + WFF(I) * Z(3,I)
EKTH = S11 * FFTH(I) + GAMA(I) * FFFE
ENFEX = D(I) * (S6 + POI * S5) - ENI(I)
EMTHX = POI * Z(4,I) + FK(I) * S3 * EKTH - S1 * FMT(I)
ENTHX = D(I) * (S5 + POI * S6) - ENI(I)
ENFTX = D(I) * S4 * (VP - GAMA(I) * Z(2,I) - S11 * Z(1,I))
FMFIX = EK(I) * S4 * (-S11 * FFFE + FFTHP - GAMA(I) * FFTH(I) + .5 *
1 WTHD(I) - WFF(I)) * (S11 * Z(1,I) + VP + GAMA(I) * Z(2,I))
552 S15 = DNA(I) / AU
S7 = S15 * S3
S9 = E1(I) * ALF(I) * T(I) / S1
SR = S12 * E1(I)
S10 = S8 * S15 * EMT(I) / EK(I)
IF(RHOX(I)) 551,555,551
551 IF(I-1) 554,553,554
553 S13 = 2.
GO TO 559
554 S13 = 1.
GO TO 559
555 S6 = S15 / EK(I) * (Z(4,I) + EMT(I))
S11 = (Z(2,I) - Z(2,I-1)) / DEL2
S13 = (Z(1,I) - Z(1,I-1)) / DEL2
IF(ENF - 1.) 556,557,558
556 G(1) = S8 * (S2 * (S13 + WFF * Z(3,I)) + S6) - S9
G(2) = G(1)
G(3) = 0.
GO TO 578
557 G(1) = S8 * (POI * S11 + S6) - S9
G(2) = S8 * (S11 + S6 / POI) - S9

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```

G(3) = 0.
GO TO 578
558 G(1) = S8 * (S2*S13 + POI*FNF*S11 + S6) - S9
G(2) = S8 * (S2*S13 + ENF*S11 + S6 / POI) - S9
G(3) = S8*ENF * (S15 / (2.*FNF**2) * Z(4,1) / FK(1) - S13 * S1/2.)
GO TO 578
559 S6 = S4 * (S15/2. * (1. * WTHD(1) - WFF(1)) + 1.)
GFFX = S20 * (GAMA(1) * (Z(4,1) - FMTHX) + FMA(4) + FNF/PHOX(1) *
1 EMFTX * S13)
565 DO 560 K = 1,3
DO 560 L = 1,4
560 EM4(K,L) = 0.
FM4(1,1) = S8
FM4(2,1) = POI * S8
FM4(2,3) = -S7 * GAMA(1) * S8
FM4(3,2) = S6 * S8
FM4(3,3) = S15 * S1 * S11 * S8
G2(1) = S10 - S9
G2(2) = POI * S10 - S9
G2(3) = 0.
B2(1,1) = POI * GAMA(1) * S8
B2(1,2) = POI * S11 * S8
B2(1,3) = (WFF(1) + POI * WTHD(1)) * S8
B2(1,4) = S15 / FK(1) * S8
B2(2,1) = GAMA(1) * (1. + S7*WFF(1)) * S8
B2(2,2) = S8 * S11 * (1. + S7*WTHD(1))
B2(2,3) = S8 * (WTHD(1) + POI*WFF(1) + S7 * S11 **2)
B2(2,4) = B2(1,4) * POI
B2(3,1) = S8 * S4 * S11 * (S15/2. * (WTHD(1) - 3.*WFF(1)) - 1.)
B2(3,2) = -EM4(3,2) * GAMA(1)
B2(3,3) = -S8 * S1 * S11 * S15 * GAMA(1)
B2(3,4) = 0.
CALL MMY (3,4,1,EM4,EM6,G)
CALL MMY (3,4,1,B2,2(1,1),EC)
CALL MAD (3,1,G,EC,G)
CALL MAD (3,1,G,G2,G)
C
578 USUM(1) = Z(1,1)
VSUM(1) = Z(2,1)
WSUM(1) = Z(3,1)
FMFE(1) = Z(4,1)
FMTH(1) = FMTHX
FMFT(1) = EMFTX
SAVE FOURIER COEFFICIENTS
00022577
00022580
00022590
00022600
00022610
00022620
00022630
00022640
00022650
00022660
00022670
00022680
00022690
00022700
00022710
00022720
00022730
00022740
00022750
00022760
00022770
00022780
00022790
00022800
00022810
00022820
00022830
00022840
00022850
00022860
00022870
00022880
00022890
00022900
00022910
00022920
00022930
00022940
00022950
00022960
00022970
00022980
00022990

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ENFE(I) = ENFEI
FNTH(I) = FNTHX
ENFI(I) = ENFTX
SIGFF(I) = G(1)
SIGTH(I) = G(2)
SIGFT(I) = G(3)
QFE(I) = QFFX
X(1,I) = 2 * ROP * EMFTX - ENF * EMTHX
X(2,I) = EMFTX
1000 CONTINUE
DO 599 I = 1,N
  IF(I.NE.1) GO TO 593
  FMFTP = (FMFT(2) - FMFT(1)) / DEL
  IF( RHOX(I) ) 596,592,596
C
  592 EMFEP = (FMFE(2) - FMFE(1)) / DEL
  EMTHP = (FMTH(2) - FMTH(1)) / DEL
  QFE(1) = ELAM2 * (EMFEP + ENF * EMFTP)
  QTH(1) = FLAM2 * (FMFTP - ENF * EMTHP)
  GO TO 599
  593 IF(I - N) 595,594,595
  594 FMFTP = (FMFT(N) - FMFT(N-1)) / DEL
  GO TO 596
  595 EMFTP = (FMFT(I+1) - FMFT(I-1)) / DEL2
  596 QTH(I) = ELAM2 / RHOX(I) * (X(1,I) + RHOX(I) * EMFTP)
  599 CONTINUE
700 CONTINUE
  RETURN
  END
0023000
0023010
0023020
0023030
0023040
0023050
0023060
0023070
0023080
0023090
0023100
0023120
0023130
0023140
0023150
0023160
0023170
0023180
0023190
0023200
0023210
0023220
0023230
0023240
0023250
0023260
0023270
0023280
0023290

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\$ORIGIN	CHAIN		00023350
\$IRFTC FSUMS			00023350
C	6J-157DR	FOURIER SUMMING	00023320
C			00023330
C	SUBROUTINE SUMS		00023340
C			00023350
	DIMENSION	R(200), D(200), FK(200), ENI(200), FMT(200), PFF(200), WTHD(200),	00023360
1	PTH(200), PN(200), WFF(200), ALF(200), DNA(200),		00023370
2	RHOX(200), GAMA(200), E1(200), T(200), ETH(200)		00023380
	DIMENSION	USUM(200), VSUM(200), WSUM(200), EMEF(200), EMTH(200),	00023390
1	EMFI(200), FNEF(200), ENTH(200), FNET(200), SIGFE(200),		00023400
2	SIGTH(200), SIGFT(200), QFF(200), QTH(200),		00023410
3	ZDOI(3,200), ZDOI(3,200)		00023420
C			00023430
	REAL	MASS, LM11, LM22, LM33, MM11, MM22, MM33, NM11, NM22, NM33,	00023440
1	MO		00023450
C			00023460
	EQUIVALENCE	(DA(1), EN), (DA(2), AU), (DA(3), HO), (DA(4), EO), (DA(5), SIGU), (DA(6), FNEU), (DA(7), ENFI), (DA(8), POT), (DA(9), THETA), (DA(10), PIXI), (DA(11), SPRL), (DA(12), UK), (DA(13), VK), (DA(14), WK), (DA(15), EMK), (DA(16), TAU1), (DA(17), ENI1), (DA(18), PI1), (DA(19), TAU2), (DA(20), ENI2), (DA(21), PI2), (DA(22), TAU3), (DA(23), ENI3), (DA(24), PI3), (DA(25), MASS), (DA(26), CFE), (DA(27), CZ), (DA(28), SKFE), (DA(29), SKZ), (DA(30), SUM), (DA(31), ENI), (DA(32), DFL), (DA(39), DRW)	00023470
	EQUIVALENCE	(DA(40), R), (DA(240), WTHD), (DA(440), WEE), (DA(640), GAMA), (DA(840), RHOX), (DA(1040), D), (DA(1240), FK), (DA(1440), E1), (DA(1640), ALE), (DA(1840), DNA), (DA(2040), T), (DA(2240), ENI), (DA(2440), FMT), (DA(2640), PN), (DA(2840), PFF), (DA(3040), PIH), (DA(3240), ZDOI), (DA(3440), VZO), (DA(3640), AZO), (DA(3840), ZDOI), (DA(4040), VFU), (DA(4240), AFU), (DA(4440), EM1), (DA(4456), EM3), (DA(4472), EM5), (DA(4476), EMI1), (DA(4492), EMI3), (DA(4508), EM5N)	00023480
C			00023490
	COMMON	DA(4511), EM2(4,4), FM4(4,4), FM6(4), S1, S2, FLAM2,	00023500
1	Z(4,200), X(4,200), A2(4,4), B2(4,4), C2(4,4), G2(4), E(4,4),		00023510
2	F(4,4), GA(4,4), A(4,4), B(4,4), C(4,4), G(4), EC(4), DEL2,		00023520
3	SL1, SL2, N2, NTH, NIPK, NIPW, I, K, L,		00023530
4	S77, S78, BT11, HTA93, MO(200), OMG2(200), ZP(3,200),		00023540
5	Z2P(3,200), Z3P(3,200), T1X, TD-L, PRNI, ENF, PRI, JT, NJT, VI		00023550
	COMMON		00023560
1	USUM, VSUM, WSUM, EMEF, EMTH, ENFI, ENFF, ENTH, ENFI, SIGFE,		00023570
			00023580
			00023590
			00023600
			00023610
			00023620
			00023630
			00023640
			00023650
			00023660
			00023670
			00023680
			00023690
			00023700
			00023710
			00023720

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2 SIGTH, SIGFI, QFE, QTH
C
C
755 S13 = A0 * SIGO / E0
S14 = SIGO * H0 **3 / A0
S16 = SIGO * H0
DO 756 I = 1, N
  USUM(I) = S13 * USUM(I)
  VSUM(I) = S13 * VSUM(I)
  WSUM(I) = S13 * WSUM(I)
  EMFE(I) = S14 * EMFE(I)
  FMTH(I) = S14 * FMTH(I)
  EMFT(I) = S14 * EMFT(I)
  OFF(I) = S16 * OFF(I)
  QTH(I) = S16 * QTH(I)
  FNFE(I) = S16 * FNFE(I)
  FNTH(I) = S16 * FNTH(I)
  ENFT(I) = S16 * ENFT(I)
756 ENFT(I) = S16 * ENFT(I)
730 WRITE (6, 733) TIMX, (I, USUM(I), VSUM(I), WSUM(I),
1 EMFE(I), FMTH(I), EMFT(I), QFE(I), QTH(I), I = 1, N)
733 FORMAT(1H1, 28X, 39HDEFLECTIONS AND INTERNAL LOADS, TIME =, 1P6E12, 40H23920
1 // 3X, 1H1, 5X, 4H0(I), 9X, 4HV(I), 9X, 4HW(I), 8X, 6HM(PHI), 6X,
2 8HM(THETA), 3X, 12HM(PHI, THETA), 4X, 6HQ(PHI), 6X, 8HQ(THETA) //
3 (14, 8F13.4) )
WRITE (6, 735) (I, ENFE(I), FNTH(I), ENFT(I), SIGFE(I),
1 SIGTH(I), SIGFT(I), I = 1, N)
735 FORMAT(1H1, 2X, 1H1, 4X, 6HN(PHI), 6X, 8HN(THETA), 3X, 12HN(PHI, THETA), 40H23990
1 3X, 8HSIG(PHI), 4X, 10HSIG(THETA), 2X, 13HSG(PHI, THETA) //
2 (14, 1P6E13.4) )
WRITE (6, 738) ((ZDOT(K, L), K=1, 3), (ZDOT(K, L), K=1, 3), L=1, N)
738 FORMAT(/// 10X, 28HVELOCITIES AND ACCELERATIONS // 15X, 6HVEL(U),
1 10X, 6HVEL(V), 10X, 6HVEL(W), 10X, 6HACC(U), 10X, 6HACC(V), 10X,
2 6HACC(W) // (6X, 1P6F16.3) )
C
WRITE(9)(USUM(I), I=1, N)
WRITE(9)(VSUM(I), I=1, N)
WRITE(9)(WSUM(I), I=1, N)
WRITE(9)(EMFE(I), I=1, N)
WRITE(9)(FMTH(I), I=1, N)
WRITE(9)(EMFT(I), I=1, N)
WRITE(9)(QTH(I), I=1, N)
WRITE(9)(ENFE(I), I=1, N)
WRITE(9)(FNTH(I), I=1, N)
WRITE(9)(SIGFE(I), I=1, N)

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WRITE(9)(SIGH(I),I=1,N)	00024170
WRITE(9)(ZDOT(1,I),I=1,N)	00024180
WRITE(9)(ZDOT(3,I),I=1,N)	00024190
WRITE(9)(Z2DOT(1,I),I=1,N)	00024200
WRITE(9)(Z2DOT(3,I),I=1,N)	00024210
880 SL2 = 0.0	00024220
IF(IAU1 + IAU2 + IAU3 - TIMX .GT. 1.E-8) GO TO 890	00024230
888 SL1 = 1.	00024240
C	00024250
890 IF(DRW .NF. 0.) SL1 = -2.	00024260
RETURN	00024270
END	00024280

\$ORIGIN	CHAIN.SYSUT2.REW	00024290
\$BFTC LNK6		00024300
C 6J-148 ** LINK6	PSEUDO CRT SUBROUTINE	00024310
C		00024320
SUBROUTINE PIX		00024330
C		00024340
LO = 0		00024350
RETURN		00024360
END		00024370

SDATA									
	1	75	80	81					
HYDROELASTIC RESPONSE APOLLO SPHERE ** FIXED BIND.- P(....) IN ANALYTIC FORM									
10 ITERATIONS TO 2.0 MS RESTA.T ** POI=.33, EN=120., KHJ=.000975									
OPEN ANGLE=19.53, D=3.33E+6, K=3.33E+6, E=29.7E+6, DNA=1.025IN, RC=175.600024420									
62.5 10000.0									
1	0.01	25	0						00024430
2	1.	1.	1.	1.	0.0				00024430
7	0.0	0.33	0.0	0.0					00024460
16	2.0	20.	1.						00024470
21					.975				00024480
30	-1.								00024490
33	-1.	360.	1.0	0.					00024500
4476	1.0	3.0							00024510
1	2.0	120.0	-1.0	175.6	0.0				00024520
6	0.0	19.530							00024530
1	1.0	3.33	+6						00024540
42	1.0	3.33	+6						00024550
83	1.0	29.7	+6						00024560
165	1.0	1.025							00024570

\$IBFTC DECRD	DECRD000
SUBROUTINE DECRD(D)	DECRD005
DIMENSION FLT(5), ID(2), D(1)	DECRD010
10 READ (5,100) LOC, FLT, ID	DECRD015
100 FORMAT (I12, 5E12.0, 1A6, 1A2)	DECRD020
IF (LOC.EQ. 0) GO TO 500	DECRD025
15 K = IABS(LOC) - 1	DECRD030
D0 20 I = 1,5	DECRD035
IF (SIGN(1.0,FLT(I)).LT.0.0 .AND. FLT(I).EQ. 0.0) GO TO 20	DECRD040
J = K + 1	DECRD045
D(J) = FLT(I)	DECRD050
20 CONTINUE	DECRD055
IF (LOC.LT. 0) GO TO 1000	DECRD060
GO TO 10	DECRD065
500 WRITE (6,200) ID	DECRD070
200 FORMAT(10HOBAD DATA 1A6,1A2)	DECRD075
CALL EXIT	DECRD080
1000 RETURN	DECRD085
END	DECRD090