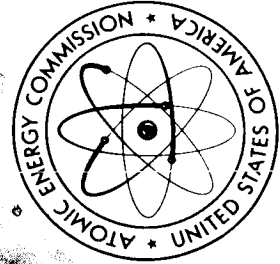


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11D-23639

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RN-S-0114



NO 303 RN .65

REPORT NO. RN-S-0114

TO

AEC-NASA SPACE NUCLEAR PROPULSION OFFICE

TRANSIENT ENGINE SIMULATION PROGRAM



SPACE ENGINE OPERATIONS - NUCLEAR

CONTRACT SNP-1 AUGUST 1964 NERVA PROGRAM

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RELEASE FOR ABSTRACTING

IN BUTLER INDEX ABSTRACTS

AEROJET-GENERAL CORPORATION
A SUBSIDIARY OF THE GENERAL TIRE & RUBBER COMPANY

ABSTRACT

This report describes the Transient Engine Simulation Program showing logic and the derivation of equations. Operating instructions are also given.

The program will calculate metal and fluid temperatures and stagnation pressure distributions as functions of time and distance. The overall engine system is represented by combining several separate existing mathematical models of engine subsystems (e.g. turbopump, reflector, shield, core, nozzle, hot-bleed port). The program is general and capable of handling design modifications.

Program accuracy is shown to be a direction function of input. Good agreement with NEX-A1 and other test data has been shown. The program is in production and is coded in SCAT for the IBM 7094 computer using the Aerojet Kismet monitor.

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TABLE OF CONTENTS

I. PURPOSE	3
II. SUMMARY	7
A. Method of Solution	7
B. Capabilities and Accuracies	9
III. TECHNICAL DISCUSSION	13
A. Derivation of Equations	13
1. Turbopump	13
2. General Heat-Transfer Equations	17
3. Pressure-Drop Calculation	20
4. Flow Rate Capacitance Effects	21
5. Hot-Bleed-Port and Nozzle-Tube Model	21
B. Logical Order of Operation	22
IV. GLOSSARY OF TERMS	45
A. Symbols	45
B. Subscripts	46

TABLE OF CONTENTS (cont.)

V. FIGURES	Page	
No.		
1 AZM	12013	Master Control Region and Input Initialization
2 AYA		Iterate to Find $\dot{V}_h$ Closing on P_8
3 AYB		Find Actual Turbine Work
4 AYD		Find Pump Flow Rate
5 AYE		Find Inlet Pressure and Flow Rate Change for One Part
6 AYEA		Find Outlet Pressure and Flow Rate Change for One Part
7 AYG		Region to Compute Part of Corrector Equations
8 AYGA		Compute Some Corrector Equations
9 AYII		Look Up Isentropic Values
10 AYL		Compute Work Required by the Pump
11 AYX		Compute Heat Resistance Term, M, for Each Node
12 AYPA		Pump and Turbine Master Control (Corrector)
13 AYPB		Turbopump Master Control Time i + 1 (Predictor)
14 AYR		Find Values for One Node
15 AYT		Check for Cool-Down Reached
16 AZA		Set Values for One Time Step
17 AZAA		Obtain Values for Next Time Point
18 AZAB		Find Values at Zero Time
19 AZAC		Initialize Program
20 AZB		Main Engine Heat Transfer and Fluid Flow
21 AZC		Compute Some Values for One-Node, Metal Temperatures
22 AZG		Compute Some Values for One-Node, Metal Temperatures
23 AZI		Heat Transfer Iteration Master Control
24 AZJ		Compute Metal Temperatures for One Time Point
25 AZK		Move Current Values to Past-Time Values for Each Part
26 AZNI		Initialize Nozzle Tube Program
27 AZT		Fluid Node Calculations

TABLE OF CONTENTS (cont.)

APPENDICES

- A. NERVA Engine Transient Program
- B. Sample Case
- C. Typical Program Printout
- D. Program Listing

Page
79
91
95
99

I. PURPOSE

The Transient Engine Simulation Program is designed to predict the transient operation of the NERVA rocket engine with minimum run time on the computer; however, the mathematical model is flexible enough to determine the thermal and hydrodynamic characteristics of a wide range of mono-fluid flow systems. Therefore while the Logical Order of Solution, Sec. III, B, is tied into the NERVA engine, it is also applicable to other systems.

II. SUMMARY

A. METHOD OF SOLUTION

The transient engine simulation program is a finite-difference, explicit solution, digital-computer program that calculates solid temperature, liquid temperature, and pressure distribution as functions of distance and time throughout the engine system. Separate analyses of the turbopump, hot-bleed port, reflector, shield, core, nozzle, and various tanks and lines are combined to represent the transient performance of the complete engine.

The turbopump assembly model consists primarily of an energy balance, including an energy storage term to account for the angular energy of the rotating machinery.

The analytical representation of the reflector, shield, and core (identified as parts in the program) is a one-fluid-channel finite-difference energy balance. The single-channel representation allows computation simplicity and improves computing speed but necessitates utilization of several unique analysis techniques. The flow channels in the various components are of different size and shape and thus requires incorporation of a "void fraction"* in the heat-transfer analysis. The void fraction, when used properly, quite satisfactorily simulates the heat transfer of a many-channelled heat exchanger with a one-channel representation. However, this method destroys the hydrodynamic characteristics.

* The void fraction is defined as the flow area divided by the total heat-transfer area (flow area plus metal area) of the heat exchanger.

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The fluid-pressure distribution is obtained by analyzing the various flow channels and calculating a bulk friction factor for use with the one-channel representation. This method has been tested for nuclear power engine cases and with test data for liquid, cold gas, and ambient gas flows; good results have been obtained in all cases for both heat-transfer and pressure-drop characteristics.

The nozzle, being a counter-current heat exchanger, is not adaptable to the basic model used for the reflector, shield, and core. Therefore, a model was developed treating the nozzle as a single-pass counter-current heat exchanger. The tubes are divided into finite distance increments for pressure-drop and heat-transfer calculations. Calculations are made for flow, heat-transfer coefficients, unique metal conductivities, and exit, entrance and turning pressure losses. Heat-transfer areas, wetted perimeter, and pressure-loss coefficients are required as input. The nozzle-tube representation is accurate for a nuclear transient run since the largest heat addition to the nozzle coolant is due to core exit gases; however this method gives poor results for a nozzle cool-down due to large heat additions from the nozzle tube jacket. A revised nozzle-tube program is presently being developed.

The hot-bleed port subroutine is also a counter-current finite difference routine which balances the turbine flow rate from both the diluent and hot inlet pressures. Entrance loss, exit loss, vena contracta, and angle of diluent injection are considered. The diluent extraction point can be varied within the engine. The representation of the hot bleed is moderately rigorous and agrees well with early tests run on a 2.5-in. hot-bleed port.

A linear predictor routine is used to project the program to the succeeding time point. The predictor is accurate enough to eliminate a closure on the pump discharge pressure, which greatly reduces the overall program running time.

At present a set of eight simultaneous partial differential equations are being programmed for inclusion in this program. The addition of these equations will enable the program to handle any transient fluid flow situation, including two-phase flow.

B. CAPABILITIES AND ACCURACIES

The program is designed so that the physical characteristics of the system may be input; therefore, the program is extremely flexible and is capable of handling major design modifications.

The single-flow channel, however, somewhat limits the program since this does not permit prediction of the metal temperatures in the tie-rod channel. A model of the tie-rod channel is presently being "checked out", for the inclusion in the program, and it will correct this deficiency.

The program accuracy is a direct function of the input. The closure tolerances, increments for finite differences, pressure-drop constants, and the constants used by the program to calculate convective heat-transfer-film coefficients are input. However, reasonably large time and distance nodes result in only a small error, but greatly improve the program operating time*. However, if proper input is applied to the program, the results will provide good agreement with test data.

Comparison of this program with data from NKK-A1 showed that the calculated values fell within the test data bandwidth (with the exception, as previously explained, of the nozzle chilldown, where there is a large heat addition to the fluid from the nozzle jacket).

* For example, $\Delta t = 1$ sec, and $\Delta t = 0.2$ sec,
 $\dot{V}_p = 4.36$ $\dot{V}_p = 4.44$
 This illustrates a difference of 1.8%.

III. TECHNICAL DISCUSSION

A. DERIVATION OF EQUATIONS*

1. Turbopump

The turbopump model consists of four basic equations:

- (1) the turbine work
- (2) the pump work
- (3) a calculation of the pressure ratio across the turbine
- (4) the energy balance on the turbopump assembly.

a. Turbine Work Done

The turbine work is found by calculating the isentropic turbine work and multiplying it by a turbine efficiency factor.

Turbine work = Turbine efficiency x turbine isentropic work, or

$$W_{T \text{ act}} = \eta_T \left[\dot{V}_T C_P (T_{11} - T_{12}) \right] \text{ isen} \quad (1)$$

Considering isentropic and ideal gas relationships,

$$T_{12} = T_{11} \left(\frac{P_{11}}{P_{12}} \right)^{\frac{\gamma-1}{\gamma}} \quad (2)$$

where

$$\frac{\gamma-1}{\gamma} = \frac{R}{\gamma C_P} \quad (3)$$

therefore,

$$T_{12} = T_{11} \left(\frac{P_{11}}{P_{12}} \right)^{\frac{R}{\gamma C_P}} \quad (4)$$

* A glossary of terms appears as Section IV of this volume.

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Now, substituting pressures for temperature and rearranging algebraically.

$$\dot{W}_T \text{ act} = \eta_T \dot{W}_T C_p T_{11} \left[1 - \left(\frac{P_{11}}{P_{12}} \right)^{\frac{R}{\gamma C_p}} \right] \quad (5)$$

b. Pump Work Done

The pump work done is the flow times the enthalpy difference across the pump divided by the pump's efficiency

$$\dot{W}_P \text{ act} = \frac{\dot{W}_P \Delta h}{\eta_P}, \quad (6)$$

c. Pressure Ratio Across the Turbine

The pressure drop across the turbine is controlled by two choked nozzles, the turbine inlet nozzle (A_{tn}) and the last-stage rotor of the turbine (A_{rn}). Using the isentropic choked equation,* to calculate P_{12} and P_{11} from the turbine flow rate as functions of T_{12} and T_{11} :

$$P_{12} = \frac{\dot{W}_T \sqrt{T_{12}}}{A_{rn} (.1596)} \quad \text{and} \quad P_{11} = \frac{\dot{W}_T \sqrt{T_{11}}}{K_t} \quad (7)$$

where

$$K_t = (.1596 A_{tn})$$

By equating $\dot{W}_T$, we obtain

$$\frac{P_{12}}{P_{11}} = \frac{K_t}{A_{rn} (.1596)} \sqrt{\frac{T_{12}}{T_{11}}} \quad (8)$$

*Acher Shapiro, Dynamics and Thermodynamics of Compressible Fluid Flow, page 63, Ronald Press Co.

Actual temperature differential across the turbine is equal to the product of turbine isentropic temperature differential and turbine efficiency:

$$\Delta T = \eta_T \Delta T_{\text{isen}} \quad (9)$$

$$(T_{12} - T_{11}) = \eta_T (T_{12 \text{ isen}} - T_{11}) \quad (10)$$

solving for

$$\frac{T_{12}}{T_{11}} = 1 - \eta_T \left(1 - \frac{T_{12 \text{ isen}}}{T_{11}} \right) \quad (11)$$

Now, since

$$\frac{T_{12 \text{ isen}}}{T_{11}} = \left(\frac{P_{12}}{P_{11}} \right)^{\frac{R}{\gamma C_p}} \quad (12)$$

then

$$\frac{T_{12}}{T_{11}} = \left(\frac{P_{12}}{P_{11}} \right)^{\frac{R}{\gamma C_p}} \quad (13)$$

Now, substituting for $\frac{T_{12}}{T_{11}}$ in Equation 8, we obtain

$$\frac{P_{12}}{P_{11}} = \frac{K_t}{A_{rn} (.1596)} \sqrt{1 - \eta_T \left[1 - \left(\frac{P_{12}}{P_{11}} \right)^{\frac{R}{\gamma C_p}} \right]} \quad (14)$$

The above equation lends itself to a digital iteration solution.

d. Energy Balance on the Turbopump Assembly

To obtain the pump work at time $(i+1)$, the average pump work between this time $(i+1)$, and i , plus the change in rotational energy over that time difference is equated to the average turbine work for the same time period, as given by

$$\frac{W_{p \text{ act}}(i) + W_{p \text{ act}}(i+1)}{2} + \frac{d \left(\frac{I \omega^2}{2} \right)}{dt} = \frac{W_{T \text{ act}}(i) + W_{T \text{ act}}(i+1)}{2} \quad (15)$$

rearranging,

$$W_{p \text{ act}}(i+1) = W_{p \text{ act}}(i) - \frac{d(I \omega^2)}{dt} + W_{T \text{ act}}(i) + W_{T \text{ act}}(i+1) \quad (16)$$

Using finite difference integration on $\frac{d(I \omega^2)}{dt}$ and solving for

$$\omega^2 = \frac{2\pi}{60} \left(N^2 \right) \quad (16a)$$

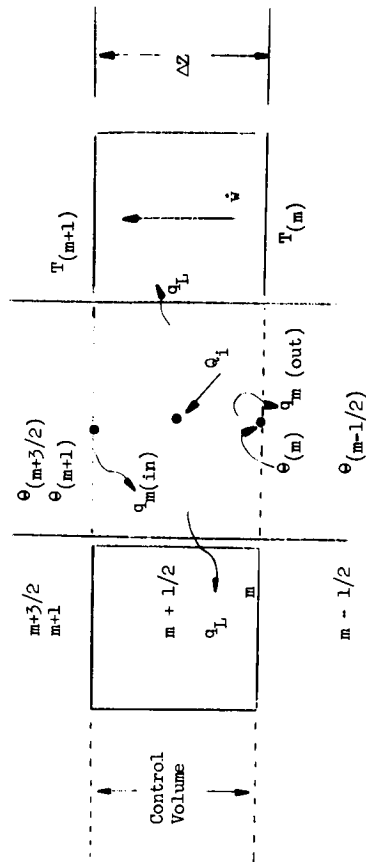
$$\frac{d(I \omega^2)}{dt} = \frac{I \frac{2\pi}{60} \left(N^2(i+1) - N^2(i) \right)}{12g \Delta t 778} \quad (17)$$

Substituting into the above, the equation for $W_{p \text{ act}}(i+1)$ is obtained as

$$W_{p \text{ act}}(i+1) = -W_{p \text{ act}}(i) - \frac{I}{12g \Delta t} \left(\frac{2\pi}{60} \right)^2 \left(\frac{N^2(i+1) - N^2(i)}{778} \right) + W_{T \text{ act}}(i+1) + W_{T \text{ act}}(i) \quad (18)$$

2. General Heat-Transfer Equations

The general heat-transfer model consists of two energy balances, one on a liquid node and one on a metal node. A control volume is assumed as follows:



The energy into the control volume is equated to the energy out of the control volume

$$\frac{\partial E}{\partial t}_{in} = \frac{\partial E}{\partial t}_{out}$$

The energy balance on the liquid assumes steady flow and steady-state over the distance increment, and thus no energy storage in the liquid. Therefore,

$$h_f \Delta Z F_p \left[\theta_{(m+1/2, n)} - T_{(m+1/2, n)} \right] = \dot{V} C_p \left[T_{(m+1, n)} - T_{(m, n)} \right] \quad (19)$$

Define

$$M = \frac{\dot{V} C_p}{h_f \Delta Z F_p} \quad (20)$$

and substitute into the above. Then,

$$T_{(m+1, n)} - T_{(m, n)} = \frac{1}{M} \left[\theta_{(m+1/2, n)} - T_{(m+1/2, n)} \right] \quad (21)$$

Assuming the temperature distribution in the fluid control volume varies linearly with distance, the average temperature of the fluid node becomes

$$T_{(m+\frac{1}{2}, n)} = \frac{T_{(m+1, n)} + T_{(m, n)}}{2} \quad (22)$$

Now, substituting into the above and rearranging to solve for $T_{(m+1, n)}$ we obtain the next fluid temperature

$$T_{(m+1, n)} = \frac{2\theta_{(m+\frac{1}{2}, n)} + (2M-1) T_{(m, n)}}{2M+1} \quad (23)$$

The energy balance on the metal control volume is more complex than that of the liquid; the energy from the previous node, plus the nuclear energy, minus the energy lost to the next node and the fluid, is equated to the energy storage,

$$\frac{\partial E_{in}}{\partial t} - \frac{\partial E_{out}}{\partial t} = \frac{\partial E_{storage}}{\partial t}$$

Substituting equivalent values,

$$q_{m(in)} + q_1 - q_{m(out)} - q_L = \frac{\partial E_{storage}}{\partial t} \quad (24)$$

Substituting and gathering terms,

$$\begin{aligned} \frac{2k(1-f) A_F}{f \Delta Z} \theta_{(m, n)} - \theta_{(m+\frac{1}{2}, n)} + q_1 - \frac{2k(1-f) A_F}{f \Delta Z} \theta_{(m+\frac{1}{2}, n)} - \theta_{(m+1, n)} \\ - \dot{v} C_P T_{(m+1, n)} - T_{(m, n)} = \frac{\Delta Z(1-f) A_F C_P R}{\Delta t f} \theta_{(m+\frac{1}{2}, n+1)} - \theta_{(m+\frac{1}{2}, n)} \end{aligned} \quad (25)$$

Define N as equal to

$$\frac{\Delta Z(1-f) A_F C_P R}{f \Delta t \dot{v} C_P} \quad (26)$$

Substituting and gathering terms

$$\begin{aligned} \theta_{(m+\frac{1}{2}, n+1)} - \theta_{(m+\frac{1}{2}, n)} \\ = \frac{1}{N} \left[T_{(m, n)} - T_{(m+1, n)} \right] + \frac{2K \Delta t}{(\Delta Z)^2 \rho_R C_R} \left[\theta_{(m+1, n)} - 2\theta_{(m+\frac{1}{2}, n)} + \theta_{(m, n)} \right] + \frac{q_1}{\dot{v} C_P N} \end{aligned} \quad (27)$$

Define S as equal to

$$\frac{2K \Delta t}{(\Delta Z)^2 \rho_R C_R} \quad (28)$$

Assuming the temperature gradient in the metal node varies linearly with distance,

$$\theta_{(m+1, n)} = \frac{\theta_{(m+\frac{3}{2}, n)} + \theta_{(m+\frac{1}{2}, n)}}{2} \quad (29a)$$

and

$$\theta_{(m, n)} = \frac{\theta_{(m+\frac{1}{2}, n)} + \theta_{(m-\frac{1}{2}, n)}}{2} \quad (29b)$$

Now, substituting Equations (29a) and (29b) into Equation (27),

$$\theta_{(m+\frac{1}{2}, n+1)} = \frac{1}{N} \left[T_{(m, n)} - T_{(m+1, n)} \right] + \frac{S}{2} \left[\theta_{(m+\frac{3}{2}, n)} - 2\theta_{(m+\frac{1}{2}, n)} + \theta_{(m-\frac{1}{2}, n)} \right] + \frac{q_1}{\dot{v} C_P N} \quad (30)$$

From Equation (25),

$$\theta_{(m+\frac{1}{2}, n)} = \frac{(2M+1) T_{(m+1, n)} - (2M-1) T_{(m, n)}}{2} \quad (31)$$

Substituting in the above and gathering terms

$$\theta_{(m+\frac{1}{2},n+1)} = \theta_{(m+\frac{1}{2},n)} \left[1 - \frac{2}{N(2M+1)} \right] + T_{(m,n)} \left[\frac{1}{N} - \frac{2M-1}{N(2M+1)} \right] + \frac{S}{2} \theta_{(m+\frac{3}{2},n)} - 2\theta_{(m+\frac{1}{2},n)} + \theta_{(m-\frac{1}{2},n)} + \frac{Q_1}{\dot{w} C_P N} \quad (32)$$

Let

$$U = \frac{Q_1}{\dot{w} C_P N} = \frac{H \Delta T}{\rho_R C_R} \quad (33)$$

and substituting Equation (26) into (33), and $Q_1 = \frac{H \Delta Z (1-f) A_F}{f}$

$$U = \frac{Q_1 f \Delta t}{\rho_R C_R \Delta Z (1-f) A_F}$$

Therefore,

$$\theta_{(m+\frac{1}{2},n+1)} = \theta_{(m+\frac{1}{2},n)} \left[1 - \frac{2}{N(2M+1)} \right] + T_{(m,n)} \left[\frac{1}{N} - \frac{2M-1}{N(2M+1)} \right] + \frac{S}{2} \theta_{(m+\frac{3}{2},n)} - 2\theta_{(m+\frac{1}{2},n)} + \theta_{(m-\frac{1}{2},n)} + U \quad (34)$$

3. Pressure-Drop Calculation

The pressure-drop calculation is a combination friction and heat-transfer pressure drop that is proportional to $\frac{\dot{w}^2}{A^2 \rho}$

$$\Delta P = \frac{\dot{w}^2}{A_F^2 \rho \Delta g} \frac{T_{(m+1,n)} - T_{m,n}}{T_{m,n}} + \frac{4\phi \Delta Z}{\dot{w}^2} \quad (35)$$

Rearranging,

$$P_{(m,n)} - P_{(m+1,n)} = \frac{\dot{w}^2}{A_F^2 \Delta g} \frac{T_{(m+1,n)} - T_{(m,n)}}{T_{(m,n)}} + \frac{4\phi \Delta Z}{\dot{w}^2} \quad (36)$$

and

$$P_{(m+1,n)} = P_{(m,n)} - \frac{\dot{w}^2}{A_F^2 \rho \Delta g} \left[\frac{T_{(m+1,n)} - T_{(m,n)}}{T_{(m,n)}} \right] + \frac{4\phi \Delta Z}{\dot{w}^2} \quad (37)$$

4. Flow Rate Capacitance Effects

The change in flow rate over the next time point is equated to the change in flow rate over the previous time point, plus the mass change

$$\dot{w}_{(m+1,n)} - \dot{w}_{(m,n)} = \dot{w}_{(m,n-1)} + \frac{A_F \Delta Z}{\Delta t} \left[\rho_{(m,n-1)} - \rho_{(m,n)} \right] \quad (38)$$

Therefore,

$$\dot{w}_{(m+1,n)} = \dot{w}_{(m,n)} + \frac{A_F \Delta Z}{\Delta t} \left[\rho_{(m,n-1)} - \rho_{(m,n)} \right] + \dot{w}_{(m,n-1)} - \dot{w}_{(m+1,n-1)} \quad (39)$$

5. Hot-Bleed-Port and Nozzle-Tube Model

The heat-transfer and pressure-drop equations explained in paragraphs 2 and 3, above, are basically the same as those used in the hot-bleed-port and nozzle-tube programs. Complete descriptions of the equations used in the hot-bleed-port and nozzle-tube programs are available in REON Reports 8209-64-2 and 8209-64-5, respectively. Copies of these reports may be obtained by contacting the Manager, Contracting Division, REON.

B. LOGICAL ORDER OF OPERATION

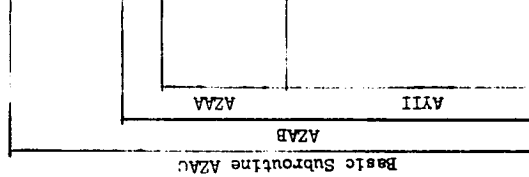
Covering subroutines are referenced by comparable letters in enclosing brackets. Unless otherwise referenced, see Figure 1, AZM.

Steps

1. Read in AGC-modified LASL (PRPTY) hydrogen properties subroutine.
2. Set up curves for the pump under investigation of $\frac{\Delta H}{N^2}$ as a function of Q and N^2 for interpolation.
3. Read standard case, which details the parameters describing the physical system. See AZXC. If an error is detected, print "ERROR IN STANDARD INPUT" and stop. If a tape check occurs, print "BAD TAPE - FLUSH," and stop.
4. Set counter to begin storing at first part (ref. II,A in text). See AZXA.
5. Test next card to see if a standard input is desired. If there is no input remaining, print "END OF INPUT" and stop. If tape check occurs, print "BAD TAPE - FLUSH," and stop.
6. Read in the input for the next part. If no input cards remain, print, "END OF INPUT," and stop, transferring to AZM-12. If the same number of parts as contained in the standard case are read in and no final "T" card is encountered, to flag end of input, print "ZERO T CARD MISSING," and stop.
7. If the final "T" card has been read, go to step 18; if not, continue.
8. Print input for this part.
9. Prepare to set up the input curves (AZM-7). If this is the first part, all input curves are expected. If this is not the first part, the number of curves for one part will be expected.
10. Check the next curve. If the number of points is -1, go to step 12. If the number of points is greater than the maximum number or less than 2, print "ERROR IN PTS/CURVE" and go to step 237.

11. Set up the curve for linear interpolation. See AZM-8.
12. If the required number of curves are not read in, go to step 10.
13. If the number of nodes input for this part is greater than the maximum, print "TOO MANY NODES" and go to step 237.
14. Set inlet and outlet plenum densities and the density for each node to $\rho = f(\theta_o \text{ and } P_o \text{ min})$; thus the density is determined by the initial metal temperature and the minimum outlet pressure. Set all metal temperatures equal to θ_o and all flow rates to zero.
15. Compute total distance from AZM-19.

$$Z_{\max} = (\text{Number of nodes} + \frac{1}{2}) \Delta Z$$
16. If there is not enough storage for this part, go to step 236.
17. Set the counter to read in the next part, and go to step 6.
18. If no parts have been read in and the final "T" card is read in, stop.
19. Set counter to compute input number of time points.
20. Begin program initialization.
21. If the diluent extraction point is zero or beyond the last part, print "NO DILUENT REMOVED" and stop.
22. Set time $t_i = -\Delta t$.
23. Time $t_{i+1} = \Delta t + \text{time } t_i$.
24. If input P_1 is not zero, go to step 31.
25. Interpolate input curves for P_1 and T_1 at time 0.
26. Find $h_1 = f(P_1, T_1)$ in hydrogen properties subroutine.
27. Find $\rho_1 = f(P_1, T_1)$ in hydrogen properties subroutines. If error occurs, print "BAD TANK PRESS, TEMP" and stop the program.
28. Find $S = f(P_2 \text{ and } T_1 + \Delta T)$ in perhydrogen properties subroutine.
29. Find vapor pressure at pump inlet. If the pressure is greater than the total pressure at the pump inlet, print "GAS AT PUMP INLET" and stop.



30. Find pump inlet saturated vapor head.

$$H_{sv} = \frac{P_1 - P_1 \text{ vapor ft-lbf}}{12 \rho_1 \text{ lbm}} \quad (\text{Eq. PR34})$$
31. If the input gate position is not zero, go to step 33.
32. Interpolate input curve for gate position at time zero.
33. If input tank pressure is zero, go to step 35.
34. For functions of $P_{1,i+1}$ at $P_{1,i}$ and $T_{1,i}$, find entropy and hydrogen properties at P_1 and T_1 . If an error occurs in the hydrogen properties subroutine, print "BAD TANK TEMP, PRS" and stop the problem.
35. If input gate position is zero, go to step 37.
36. G.P. = G. F. input.
37. $P_1 = P_{1,c} - \bar{P}_{1,i+1}$, $T_1 = T_2 = T_{2,o} = T_{2,i+1}$, Pump-outlet conditions at zero time are set equal to pump-inlet conditions.
38. Set $P_{o \text{ min}}$ equal to the input minimum outlet pressure
39. Set $M_{(i+1)}$ equal to input initial turbine speed
40. Set $\dot{W}_{T(i+1)}$ equal to input pump flow-rate guess
41. Set $\dot{W}_{c(i+1)}$ equal to input diluent flow-rate guess
42. Set $\dot{W}_{h(i+1)}$ equal to input not-bleed-port flow-rate guess
43. The predicted values for $P_0, P_8, T_8, P_{11}, T_{11}, T_{12}, Q_p, W_{p \text{ act}}$, $W_{T \text{ act}}$, and ΔH are not used in the initial computations and are therefore set equal to zero.
44. Place input not-bleed-port parameters in storage for hot bleed port program.
45. Set initial T_0 for nozzle tubes equal to the input initial metal temperature.

42. If the nozzle tube subroutine is not required, go to step 46.
43. Find T_0 ; if $T_0 < 0$, stop the problem.
44. If input $P_{o \text{ min}}$ is not zero, set P_0 equal to input $P_{o \text{ min}}$. If input $P_{o \text{ min}}$ is zero, interpolate input curve for $P_{o \text{ min}}$ at initial time and set P_0 equal to this value.
45. Set the initial q_1 guess equal to the input initial q_1 guess.
46. If input P_{11} is not zero, set flag to proceed with turbopump calculations as though the hot-bleed port were replaced with a star bottle.
47. Set flags to print nozzle tube and/or hot-bleed port iterations if desired.
48. Set flag to print only inlet and outlet distance nodes for each part if desired.
49. Flag option to ignore nozzle tube choking.
50. Move print-out paper to a new page. Return to AZM-31 and go to AZA
51. Set t_i equal to $t_{(i+1)}$, and proceed to next time point.
52. If $P_{o \text{ min}}$ input is zero, interpolate input curve for $P_{o \text{ min}}$ at next time point.
53. Set the following values at the current time point equal to the predicted values from the preceding time point: $P_1, T_1, P_2, T_2, G.P., N, \rho_1, \Delta H, \dot{W}_p, \dot{W}_c, H_{sv}$.
54. Print inlet conditions for this time point.
55. Begin iteration to find pump flow ($\dot{W}_{P_i}$) by closing on the calculated pressure in comparison with the pressure required to choke the main nozzle.
56. Set diluent flow rate to the value computed by the hot-bleed-port program. Note that initially this value is that predicted in the previous time interval.
- Set temperature equal to T_2 , pressure equal to P_2 , and flow rate equal to $\dot{W}_p$.

57. Deactivate " P_6 too low" and "diluent removed" flags.
58. If the diluent is to be removed at the pump outlet, subtract $\dot{w}_c$ from the flow rate, and activate "diluent removed" flag. If $\dot{w}_c$ is greater than the current flow rate, go to step 96.
59. Find the nozzle tube inlet conditions P_3 and T_3 setting T_3 equal to T_2 , and T_3 equal to T_2 (Eq. T1)

$$P_3 \text{ equal to } P_2 - K_2 \frac{(\dot{w}_R)^2}{(A_2)^2 \rho_2^2} \text{ psia} \quad (\text{Eq. T2})$$
60. If the diluent is to be removed at the nozzle tube inlet, subtract $\dot{w}_c$ from the flow rate and activate the "diluent removed" flag. If $\dot{w}_c$ is greater than the current flow rate, go to step 96.
61. If the nozzle tube subroutine is desired, enter the nozzle-tube program to find P_4 , T_4 , the choked-flow rate, and the tube metal temperatures. If a negative pressure occurs in the nozzle tubes, go to step 88. If some other error occurs, print "NOZZLE TUBE ERROR," ignore the nozzle tubes, and continue.
62. Set counter to first part.
63. If the diluent is to be removed at the inlet to this part, subtract $\dot{w}_c$ from the flow rate, and activate the "diluent removed" flag. If $\dot{w}_c$ is greater than the current flow rate, go to step 96.
64. Set inlet pressure and temperature equal to the current pressure and temperature.
65. Find inlet plenum flow-rate change by:

$$\dot{w}_{\text{out}} = \dot{w}_{\text{in}} + \frac{V_{\text{inlet plenum}}}{\Delta t} \left[\rho_{(i-1)} - \rho_i \right] + \dot{w}_{\text{in}} - \dot{w}_{\text{out}} \quad \text{lb/sec} \quad (i-1)$$

 If $\dot{w}_{\text{out}} = 0$, go to step 96.
 If current $P = 0$, go to step 88.

66. In the input inlet orifice K is not zero, compute the inlet pressure drop by:

$$P_{\text{out}} = P_{\text{in}} - \frac{\dot{w}^2 K_{\text{orifice}}}{\rho^2 g} \text{ psia}$$

 If $P_{\text{out}} = 0$, go to step 88.
 Initial $Z = 1/2 (\Delta Z)$
67. Find the parahydrogen properties for the pressure and temperature at this node. If $P = 0$, go to step 88. If some other error occurs, print "BAD FLUID TEMP, PHS," and stop program. Interpolate input curves to find flow area (A_p) and wetted perimeter (F_p) at this distance node.
68. Find the hydraulic diameter by

$$\bar{D} = \frac{4 A_p}{F_p} \text{ in inches.} \quad (\text{Eq. HT4})$$
69. Find the film coefficient by

$$h_f = \frac{k Z}{\bar{D}} \left[\frac{4 \dot{w}}{\pi F_p} \right]^{0.8} \frac{\pi}{\theta} \alpha \frac{\bar{D}}{p+Z} \frac{C_p}{k} \frac{0.4}{\text{in.}^2 \text{-sec}} \frac{\text{Btu}}{\text{R}} \quad (\text{Eq. HT6})$$
70. If an error occurs, print "CHECK DUMP FOR NEG" and stop the program.
71. Interpolate input curves to find the thermal conductivity (k) at this metal temperature.
72. If input wall thickness is zero, find M by:

$$M = \frac{\dot{w} C_p}{h_f \Delta Z F_p}$$

 If input wall thickness is not zero, find M by:

$$M = \frac{\dot{w} C_p}{F_p \Delta Z} \left[\frac{1}{h_f} + \frac{X}{2k} \right] \quad (\text{Eq. HT1a})$$

74. If $M < 1/2$, activate "M too small" flag.
75. Find fluid temperature for the next node by setting
- $$T_{(m+1,n)} = \frac{2\theta_{(m+1/2,n)} + (2M-1) T_{(m,n)} + \theta_R}{2M+1} \quad (\text{Eq. HT9})$$
76. Find the fluid pressure for the next node by:
- $$P_{(m+1,n)} = P_{(m,n)} - \frac{\dot{V}^2}{A_p^2 \rho} \frac{2g}{\Delta z} + \frac{T_{(m+1,n)} - T_{(m,n)}}{T_{(m,n)}} \left(\frac{\dot{V}^2}{p} + \frac{\dot{V}^2}{p} \right) \text{ psia} \quad (\text{Eq. HT6})$$
- If $P_{(m+1,n)}$ is < 0 , go to step 88.
77. Find the capacitance flow rate change by setting
- $$\dot{V}_{(m+1,n)} = \dot{V}_{(m,n)} + \frac{A_f \Delta Z}{\Delta t} \left[\frac{\rho_{(m,n-1)} - \rho_{(m,n)}}{\Delta t} \right] + \left[\dot{V}_{(m,n-1)} - \dot{V}_{(m+1,n-1)} \right] \text{ lb/sec} \quad (\text{Eq. HT13})$$
- If $\dot{V}_{(m+1,n)} < 0$, go to step 96.
78. Set $Z = Z + \Delta Z$ (meaning, proceed to next distance node)
79. If all nodes for this part have not been processed, to to step 68.
80. If input outlet orifice K is not zero, find the pressure drop by:
- $$P_{\text{out}} = P_{\text{in}} - \frac{\dot{V}^2 K_{\text{outlet orifice}}}{\rho} \text{ psia} \quad (\text{Eq. HT12})$$
- If $P_{\text{out}} < 0$, go to step 88.
81. Set outlet pressure equal to the current pressure.

AZB
AZC
AZD

AZB
AZC
AZD

Basic Subroutine AZI

82. Find the outlet flow rate change by:
- $$\dot{V}_{\text{out}} = \dot{V}_{\text{in}} + \frac{\text{outlet plenum}}{\Delta t} \left[\rho_{(i-1)} - \rho_{(i)} \right] + \dot{V}_{\text{in}(i-1)} - \dot{V}_{\text{out}(i-1)} \quad (\text{Eq. HT13a})$$
- If $\dot{V}_{\text{out}} < 0$, go to step 96.
83. Set outlet flow rate equal to the current flow rate.
84. Set increment counter to process next part. If all parts have not been processed, go to step 63.
85. Set P_6 and T_6 to current pressure and temperature.
86. If P_6 is less than P_0 min, activate "P₆ too low" flag.
87. Go to step 89. (Exit AZB)
88. If the current pressure is negative, go to step 97. If not, print "HEAT TRANSFER ERROR" and stop the program. (AZB, AZFF)
89. If a start bottle is used, go to step 99.
90. Enter hot-bleed port program to find $\dot{V}_c$, $\dot{V}_h$, $\dot{V}_m$, and P_8 . If a negative pressure occurs, go to step 101. If $\dot{V}_h$ is negative somewhere, go to step 99.
91. If $\dot{V}_m$ from the hot-bleed port program and the calculated $\dot{V}_m$ agree within the input tolerance, go to step 93.
92. Calculate a new $\dot{V}_p$ guess and adjust if necessary to arrive at a value between the given maximum and minimum values. If the maximum number of iterations has been exceeded, go to step 98. If not, go to step 56.
93. If the diluent flow rate used does not agree with $\dot{V}_c$ from the hot-bleed port program within the input tolerance, and the maximum number of iterations has not been exceeded, go to step 56. If the maximum number of iterations has been exceeded, go to step 98.
94. Store the number of iterations for printing.
95. Go to step 102 and exit AZI.

AZB
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Basic Subroutine AZI

96. A negative flow rate has occurred somewhere in the system.
If the "DILUENT REMOVED" flag is active, subtract the diluent flow from the current pump flow, and use this as a lower limit on $\dot{V}_p$. If not, use the current $\dot{V}_p$ as the lower limit. Go to step 92.

97. A negative pressure has occurred somewhere in the system.
If the "DILUENT REMOVED" flag is active, add the diluent flow from the current pump flow and use this as an upper limit on $\dot{V}_p$. If not, use the current $\dot{V}_p$ as an upper limit. Go to step 92.

98. Print "WR, WC NOT CLOSED"; set number of iterations to the maximum and go to step 95.

99. Compute nozzle choke flow as follows, assuming $\dot{V}_h = 0$:

$$\dot{V}_N \text{ choke} = \frac{0.1396 A^* P_6}{\sqrt{T_6}} \text{ lb/sec} \quad (\text{Eq. HT11})$$

100. If $\dot{V}_N$ choke and $\dot{V}_N$ calculated agree within the input tolerance, go to step 94. If not, go to step 92.

101. Halve the diluent flow rate. If the maximum number of iterations has been exceeded, go to step 98. If not, go to step 50.

102. Print the main engine system parameters. The following error messages are printed if applicable: "LIQ IN TUBE THROAT," "M TOO SMALL," "TEMP EXCEEDED MAX," "PG TOO LOW."

103. Set counter to first part. Prepare to transfer current values to past time values.

104. Set past time point inlet and outlet plenum densities and flow rates equal to current values.

105. Set past time point densities and flow rates for each node equal to current values.

106. If all parts have not been processed, set counter to next part and go to step 104.

AZFP

AYGA

Basic Subroutine AYPA

AXB

AZH

NFWB

107. Print Values predicted from the preceding time point.

108. Find Q_{p1} from the following equations:

$$Q_{p1} = \frac{\dot{V}_p}{\rho_1 (0.0028)(1728)} \text{ gal/min} \quad (\text{Eq. PT18})$$

$$\beta = \frac{P_6}{\dot{V}_p} \quad (\text{Eq. PT13})$$

$$\alpha = (P_2 - P_6) \dot{V}_p^2 \quad (\text{Eq. PT14})$$

109. If a start bottle is not being used, go to step 127.

110. Set P_{11} and T_{11} equal to the input P_{11} and T_{11} .

111. Find T_{11} . If $T_{11} < 0$, stop the program.

112. Find P_{11} from the following:

$$P_{11} = \dot{V}_T \frac{\sqrt{T_6}}{K_c} \text{ psi} \quad (\text{Eq. PT7})$$

113. De-activate "P₁₂ not closed" flag.

$$114. \text{ Find } \eta_t = \left[-6318076 \times 10^{-6} \frac{N_1}{T_{11}} + \left(.11039226 \times 10^{-2} \right) \frac{N_1}{\sqrt{T_{11}}} \right]$$

115. Set the upper limit on P_{12} equal to P_{11} .

116. Find C_{p11} from P_{11} , T_{11} . If an error occurs, stop.

117. Begin the iteration to find P_{12} by closing on $\left(\frac{P_{12}}{P_{11}} \right)_i$

$$118. \text{ Find } T_{12} = T_{11} \left[\frac{P_{12}}{P_{11}} \right]^{0.7} \quad (\text{Eq. PT44})$$

$$119. \text{ Find } \eta_T = \eta_T^* \left[1 + \frac{7}{(7+1)} C_{p11} \left(\frac{T_{11} - T_{12}}{T_{11}} \right) \right] \quad (\text{Eq. PT45})$$

Basic Subroutine

AZK

AZPI

NEMA

RAPA

AZFI

BDXA

$$120. \text{ Find } \left(\frac{P_{12}}{P_{11}} \right) = \frac{K_t}{2 A_{rn} (.1396)} \sqrt{1 - \eta_p \left[1 - \left(\frac{P_{12}}{P_{11}} \right) \right] \left[\frac{R}{778 C_p 11} \right]} \quad (\text{Eq. PT9})$$

121. If $\left(\frac{P_{12}}{P_{11}} \right)$ and $\left(\frac{P_{12}}{P_{11}} \right)$ are within the input closure tolerance, continue. If not, calculate a new P_{12} guess and adjust, if necessary, so it lies between the given minimum and maximum values. If the maximum number of iterations has been exceeded, activate the "P₁₂ not closed" flag and continue. If not, go to step 118.

$$122. \text{ Find } \dot{W}_{T \text{ act } i} = \dot{W}_T i \eta_T C_p 11 T_{11} \left[1 - \left(\frac{P_{12}}{P_{11}} \right) \right] \left[\frac{R}{778 C_p 11} \right] \text{ Btu/sec} \quad (\text{Eq. PT10})$$

123. Find η_p from program curves as a function of Q_p/W and $NPSP/W^2$.

124. If $\eta_p = 0$, set $\dot{W}_p \text{ act } i = 0$, and go to step 127.

$$125. \text{ Find } \dot{W}'_p \text{ act } i = \dot{W}_p \text{ act } i = \frac{\dot{W}_p \Delta h}{\eta_p} \text{ Btu/sec} \quad (\text{Eq. PT21})$$

126. Go to step 140. (Exit AYL).

$$127. \text{ Find } \dot{W}_{T i} = \dot{W}_h i + \dot{W}_c i \text{ lb/sec} \quad (\text{Eq. PT27a})$$

$$128. \text{ Find } K_6 = \frac{T_8 i \dot{W}_T i}{T_2 i \dot{W}_c i + T_6 i \dot{W}_h i} \text{ unitless} \quad (\text{Eq. PT27})$$

$$129. \text{ Find } K_{10} = \frac{\dot{W}_c}{\sqrt{P_2 - P_{HM}}} \text{ lb/sec, psia}^{1/2} \quad (\text{Eq. PT36})$$

$$130. \text{ Find } K_{16} = \frac{\dot{W}_h}{\sqrt{P_6 - P_{HM}}} \text{ lb/sec, psia}^{1/2} \quad (\text{Eq. PT35})$$

131. Find $K_{12} = \frac{\dot{W}_T}{V_8} \text{ lb/in.} \quad (\text{Eq. PT37})$
132. Find $K_{13} = \frac{\dot{W}_h}{V_{HM}} \text{ lb/in.} \quad (\text{Eq. PT38})$
133. Find $K_{14} = \frac{\dot{W}_c}{V_{CM}} \text{ lb/in.} \quad (\text{Eq. PT39})$
134. Find $K_{15} = \frac{\dot{W}_c}{\sqrt{P_2 - P_{CM}}} \text{ lb/sec, psia}^{1/2} \quad (\text{Eq. PT40})$
135. Find $K_{V(i+1)} = A \left[\frac{C_F(i+1)}{C_F(i+1)} \right] - B \quad (\text{Eq. PT33})$
136. Find $K_3 = 1/K_t^2 + K_{1(i+1)} + K_2 \frac{\text{lb}^2 \text{ sec}^2}{\text{lbm}^2 \text{ in.}^4} \quad (\text{Eq. PT30})$

where

$$K_{1(i+1)} = \frac{R (2 \rho_{H_2O})}{K_{V(i+1)}^2} \frac{\text{lb}^2 \text{ sec}^2}{\text{lbm}^2 \text{ in.}^4} \quad (\text{Eq. PT30a})$$

$$K_2 = \frac{R (K_{11} + K_9) (12)}{A^2 g} \frac{\text{lb}^2 \text{ sec}^2}{\text{lbm}^2 \text{ in.}^4} \quad (\text{Eq. PT30b})$$

$$K_t = A_{tn} \sqrt{\frac{Z_g}{R(12)}} \frac{2}{(7+1)} \quad (\text{Eq. PT6})$$

137. Find $T_{11 i} = T_8 i, ^\circ R \quad (\text{Eq. PT6})$
138. Find $\dot{W}_{T i} = P_{11 i} \frac{K_t}{\sqrt{T_{11}}} \text{ lbm/sec} \quad (\text{Eq. PT7})$

139. Go to step 113.
140. Print corrected values.
141. If all of the desired number of time points have been computed, go to step 4.

142. Set counter to compute metal temperatures for the first part at the next time.
143. Deactivate "maximum temperature exceeded" flag for this part.
144. Set time to time at which last fluid computations were made.
145. Set the node counter to the first node for this part.

$$A = 1/2 (\Delta Z)$$

146. Find the average flow rate for this node

$$\dot{V}_{(m+1/2)} = 1/2 [\dot{V}_{(m)} + \dot{V}_{(m+1)}]$$

147. Interpolate the input curves to find A_F and F_P at this distance node.

148. Find the average pressure, temperature, and specific heat for this node.

$$T_{(m+1/2)} = 1/2 [T_{(m)} + T_{(m+1)}]$$

$$P_{(m+1/2)} = [P_{(m)} + P_{(m+1)}]$$

$$C_P (m+1/2) = 1/2 [C_{Pm} + C_{P(m+1)}]$$

149. Interpolate the input curves to find C_R and k for the metal temperature at this node.

150. Interpolate input curves for total heat-generation coefficient at this time point and fraction of total for this distance node. The internal heat-generation coefficient for this node will be the product of the total and the fraction.

151. If input wall thickness is 0, find M

$$M = \frac{\dot{V} C_P}{F_f \Delta Z F_P} \quad (\text{Eq. HT1})$$

If not,

$$M = \frac{\dot{V} C_P}{F_P \Delta Z} \left[\frac{1}{h_f} + \frac{X}{2k} \right] \quad (\text{Eq. HT1a})$$

152. If $M = 1/2$, activate "m too small" flag.

153. If input wall thickness is 0, find N

$$N = \frac{\Delta Z (1-f) A_F \rho_R C_R}{f \Delta t \dot{V} C_P} \quad (\text{Eq. HT2})$$

If not,

$$N = \frac{\Delta Z \pi (p-x) \rho_R C_R}{\Delta t \dot{V} C_P} \quad (\text{Eq. HT2a})$$

154. If $M \geq N$, go to step 165.

155. Find $S/2 = \frac{k_R \Delta t}{(\Delta Z)^2 \rho_R C_R}$ (Eq. HT3)

156. Find $U = \frac{H \Delta t}{\rho_R C_R}, O_R$ (Eq. HT5)

157. Find metal temperature for the next time point.

$$\theta_{(m+1/2, n+1)} = \left[\frac{1}{N} - \frac{2M-1}{N(2M+1)} \right] T_{(m, n)} + \left[1 - \frac{2}{N(2M+1)} \right] \theta_{(m+1/2, n)}$$

$$+ \frac{S}{2} \left[\theta_{(m+3/2, n)} - 2\theta_{(m+1/2, n)} + \theta_{(m-1/2, n)} \right] + U, O_R \quad (\text{Eq. HT10})$$

158. If $\theta_{(m+1/2, n+1)} \geq T_{\max}$, activate the "maximum temperature exceed" flag.

159. Set increment counter to compute the next node

$$Z = Z + \Delta Z$$

160. If all nodes for this part have not been computed, go to step 145.

161. Extrapolate metal temperatures at the ends of parts:

$$\theta_{(m-1/2)} = 2\theta_{(m+1/2)} - \theta_{(m+3/2)}$$

$$\theta_{(m \max + 3/2)} = 2\theta_{(m \max + 1/2)} - \theta_{(m \max + 5/2)}$$

162. Add the metal-temperature time-increment of this part to the current time. If it is less than the next fluid computation time, go to step 145.

163. Set the increment counter to compute the next part. If all the parts have not been computed, go to step 143.

164. Go to 166. (Exit AZJ)

165. Halve the time increment for this part. If $\Delta t = \Delta t_{\min}$ print "DELTA T TOO SMALL" and stop. If not go to step 145.

166. If the outlet metal temperature of the last part is less than $t_{\min}$ and this time point has already been printed, print "COOLDOWN REACHED," and go to step 4.

167. $\text{Time}_{(i+1)} = \text{Time}_{(i)} + \Delta t$

168. If input tank pressure (P_1) is not zero, go to step 175.

169. Interpolate the input curves of P_1 and T_1 for P_1 and T_1 at this time point.

170. Find the entropy at P_1 and T_1 .

171. Find the hydrogen properties of P_1 and T_1 . If an error occurs, print "BAD TANK PRS, TMP" and stop.

172. Find entropy at P_1 and $T_1 + \Delta T$, where ΔT is a temperature increment used in finding isentropic temperature changes across the pump.

173. Find vapor pressure at P_1 and T_1 . If the vapor pressure is greater than the total pressure, print "GAS AT PUMP INLET" and stop.

174. Find $H_{\text{ev}}(i+1) = \frac{P_1 - P_1 \text{ vapor}}{12 \rho_1}$, $\frac{\text{ft, lbf}}{\text{lbm}}$ (Eq. PT34)

175. If input gate position is 0, interpolate input curves for G.P. at this time point.

176. If $N_1 = 0$, set $N_{(i+1)} \text{ guess} = 5000$. If not, set $N_{(i+1)} \text{ guess} = N_1$.

177. Begin iteration to find $N_{(i+1)}$ by closing on $W_p \text{ act}(i+1)$ computed by energy balance and work required.

178. Interpolate $\psi_{p(i+1)}$ not closed flag.

179. $\psi_{p(i+1)} \text{ guess} = \psi_p(1)$.

180. Begin iteration to find $\psi_p(i+1)$ by closing on $\Delta H_{(i+1)}$.

181. Find $\dot{V}_{p(i+1)} = Q_{p(i+1)} \rho_1$ (0.602228) (1728) lbm/sec (Eq. PT18)

182. Find $P_{2(i+1)} = \alpha \dot{V}_{p(i+1)}^2 + \beta \dot{V}_{p(i+1)}$, psia (Eq. PT17)

183. Find $T_{2(i+1)}$ from P_2 , P_1 , and T_1 isentropically

$$T_{2(i+1)} = T_1(i+1) + \frac{\Delta T}{(S - S')} \frac{(S'' - S)}{(S - S')}, \quad ^\circ R$$

where

$$S = S(P_1 \text{ and } T_1)$$

$$S' = S'(P_1 \text{ and } T_1 + \Delta T)$$

$$S'' = S(P_2 \text{ and } T_1)$$

$$\Delta T = \text{small temperature increment, in. } ^\circ R$$

184. Find parahydrogen properties at P_2 and T_2 . If an error occurs, go to step 191.

185. Find $\Delta H_{(i+1)} = 776 \left[h(P_2, T_2) - h(P_1, T_1) \right]$, $\frac{\text{ft, lbf}}{\text{lbm}}$ (Eq. PT16)

If $\Delta H_{(i+1)} < 0$, go to step 192.

186. Find $\Delta H/N^2 = f(Q/N \text{ and } NFSP/N^2)$ from the turbopump curves.

187. Find $\Delta H_{(i+1)} = \left[\frac{\Delta H}{N^2} \right]_{(i+1)} N_{(i+1)}^2$, $\frac{\text{ft, lbf}}{\text{lbm}}$ (Eq. PT20)

188. If $\Delta H_{(i+1)}$ and $\Delta H'_{(i+1)}$ are within the input closure tolerance, go to step 193.

189. Compute a new $Q_{p(i+1)}$ guess, and adjust, if necessary, so that it is between the given maximum and minimum values.

190. If the maximum number of iterations has been exceeded, activate the $Q_{p(i+1)}$ not closed flag and go to step 193. If not, go to step 181.

191. If $T_2(i+1)$ is too low, go to step 192. If $P_2(i+1)$ is too large, use the current value of $Q_{p(i+1)}$ as an upper limit on $Q_{p(i+1)}$ and go to step 189.

Basic Subroutine AYPB

AYD

192. Use the current value of $\dot{Q}_p(i+1)$ as a lower limit on $\dot{Q}_p(i+1)$ and go to step 189.

193. If a start assistance is being used, find

$$\dot{v}_T(i+1) = \frac{P_{11}(i+1) K_t}{\sqrt{T_{11}(i+1)}} \text{ lb/sec, and go to step 216}$$

If $T_{11}(i+1) < 0$, stop.

194. Deactivate $\dot{v}_H$ not closed flag.

195. Find $P_0(i+1) = \beta \dot{v}_p(i+1)$, psia (Eq. PT21)

196. Set $\dot{v}_h(i+1)$ guess = $\dot{v}_h(i)$

197. Begin iteration to find $\dot{v}_h(i+1)$ by closing on $P_8(i+1)$

198. Find $P_{HM} = \left[\frac{\dot{v}_h(i+1)}{K_{16}} \right]^2 - P_0(i+1)$, psia (Eq. PT35)

If $P_{HM} < 0$, go to step 212.

199. Find $\dot{v}_c = K_{10} \sqrt{P_2(i+1) - P_{HM}(i+1)}$, lb/sec (Eq. PT36)

If $P_2(i+1) < P_{HM}(i+1)$, stop.

200. Find $\dot{v}_T(i+1) = \dot{v}_h(i+1) + \dot{v}_c(i+1)$, lb/sec (Eq. PT27a)

201. Find $\dot{v}_8(i+1) = K_{12} \dot{v}_T(i+1)$, in./sec (Eq. PT37)

202. Find $\dot{v}_{HM}(i+1) = K_{13} \dot{v}_h(i+1)$, in./sec (Eq. PT38)

203. Find $\dot{v}_{CM}(i+1) = K_{14} \dot{v}_c(i+1)$, in./sec (Eq. PT39)

204. Find $P_{CM}(i+1) = \left[\frac{\dot{v}_c(i+1)}{K_{15}} \right]^2 - P_2(i+1)$, psia (Eq. PT40)

$P_{CM}(i+1) < 0$, go to step 212.

205. Find $T_8(i+1) = K_6 \left(\frac{T_2 \dot{v}_c + T_6 \dot{v}_h}{\dot{v}_T} \right) (i+1)$, $^{\circ}R$ (Eq. PT28)

and $T_8(i+1)$ static = $\left(\frac{T_8(i+1)}{Z-1 M^2 + 1} \right)^{\frac{\gamma}{\gamma-1}}$, $^{\circ}R$ (Eq. PT41)

206. Find $P_8(i+1)$ static

$$= \frac{P_{HM} + (P_{CM} - P_{HM}) A_{cm} \cos \theta + \frac{1}{2} (V_{CM} \cos \theta - V_8)(V_{HM} - V_8)}{f V_8 P_{D_H} L} \left[\frac{2}{Z-1 M^2 + 1} \right]^{\frac{\gamma}{\gamma-1}}$$

psia (Eq. PT42)

207. Find $P_8(i+1) = P_8(i+1)$ static $\left[\frac{Z-1 M^2 + 1}{2} \right]^{\frac{\gamma}{\gamma-1}}$, psia (Eq. PT43)

208. Find $P'_8(i+1) = \dot{v}_T(i+1) \sqrt{T_8(i+1)^{K_5}}$, psia (Eq. PT29)

209. If $P_8(i+1)$ agrees with $P'_8(i+1)$ within the input tolerance, go to step 213.

210. Compute a new $\dot{v}_h(i+1)$ guess and adjust, if necessary, so that it lies between the given maximum and minimum values.

211. If the maximum number of iterations has been exceeded, activate the $\dot{v}_h(i+1)$ not closed flag and go to step 213; if not, go to step 198.

212. Use the current $\dot{v}_h(i+1)$ value as an upper limit on $\dot{v}_h(i+1)$ and go to step 210.

213. Find $\sqrt{T_{11}(i+1)}$; if $T_{11}(i+1) < 0$, stop.

214. Find $P_{11}(i+1) = \frac{\dot{v}_T(i+1)}{K_t} \sqrt{T_{11}(i+1)}$, psia

215. Deactivate the $P_{12}(i+1)$ not closed flag.

$$216. \text{ Find } \eta_T = -(0.5318076 \times 10^{-6}) \left[\frac{N_{i+1}}{\sqrt{T_{11}(i+1)}} \right] + (0.11039226 \times 10^{-2})$$

217. Set upper limit of $P_{12}(i+1)$ equal to $P_{11}(i+1)$

218. Find C_{P11} at $P_{11}(i+1)$ and $T_{11}(i+1)$. If error occurs, stop.

219. Begin iteration to find $P_{12}(i+1)$ closing on $P_{12}/P_{11}(i+1)$

$$220. \text{ Find } T_{12}(i+1) = T_{11}(i+1) \frac{P_{12}(i+1)}{P_{11}(i+1)}, \text{ or } \quad (\text{Eq. PT44})$$

$$221. \eta_T = \eta_T' \left[\frac{7 R T_{12}(i+1)}{1 + (7+1) C_{P11}(i+1) T_{11}(i+1)} - T_{11}(i+1) \right], \text{ unitless} \quad (\text{Eq. PT45})$$

$$222. \text{ Find } P_{12}/P_{11} = \frac{K_t}{2 A_{rn}(0.1396)} \left[1 - \eta_T \right] \frac{P_{12}(i+1)}{P_{11}(i+1)}, \text{ unless} \quad (\text{Eq. PT9})$$

223. If $(P_{12}/P_{11})(i+1)$ and $P_{12}(i+1)/P_{11}(i+1)$ agree within the input tolerance, go to step 226.

224. Compute a new $P_{12}(i+1)$ guess and adjust, if necessary so that it lies between the given maximum and minimum values.

225. If the maximum number of iterations have been exceeded, activate the $P_{12}(i+1)$ not closed flag and go to step 228. If not, go to step 220.

$$226. \text{ Find } W_T \text{ act}(i+1) = \frac{R}{778 C_{P11}} \frac{P_{12}}{P_{11}}, \text{ Btu/sec} \quad (\text{Eq. PT10})$$

AYK	AYL	AYM	KRPA	AZEP
Basic Subroutine AYB				
227. Find η_p from program curves as a function of $Q_p/N(i+1)$ and $NFSP/N^2(i+1)$. If $\eta_p = 0$, set $W_p \text{ act}(i+1) = 0$, and go to step 229. 228. Find $W_p \text{ act}(i+1) = \frac{W_p(i+1) \Delta h(i+1)}{\eta_p}$, Btu/sec (Eq. PT21) 229. Find $W_p \text{ act}(i+1) = W_p \text{ act}(i) - \frac{I_{PT}}{(776) L2g \Delta t} \frac{2\pi^2}{60} N^2(i+1) - N^2(i) + W_T \text{ act}(i+1) + W_T \text{ act}(i)$, Btu/sec (Eq. PT11) 230. If $W_p \text{ act}(i+1)$ and $W_p \text{ act}(i+1)$ are within the input tolerance, to go to step 234. 231. Compute a new $N(i+1)$ guess, and adjust it if necessary so that it lies between the given maximum and minimum values. 232. If the maximum number of iterations have been exceeded, go to step 233; if not, go to step 178. 233. Print "PREDICTOR FAILED," and go to step 235. 234. If $Q_p(i+1)$ is not closed, and/or $W_h(i+1)$ is not closed, and/or $P_{12}(i+1)$ is not closed, flags are activated. Go to step 233. 235. Go to step 51. 236. Print, "TOO MANY PARTS." 237. Read next input card. If a tape error has occurred print, "HELP HELP HEKILLIP" and stop. 238. If the last card read was the final "T" card, go to step 4; if not go to step 237.				

IV. GLOSSARY OF TERMS

A. SYMBOLS

Symbol	Unit	Definition
T	$^{\circ}\text{R}$	Temperature - Fluid
P	$\text{lb}/\text{in.}^2$	Pressure
ρ	$\text{lb}/\text{in.}^3$	Density
h_f	$\text{Btu}/\text{sec}-^{\circ}\text{R}-\text{in.}^2$	Convective Heat Transfer Film Coefficient
θ	$^{\circ}\text{R}$	Temperature - Metal
f	Unitless	Void Fraction
P_p	in.	Wetted Perimeter
A_F	in.^2	Flow Area
ΔZ	in.	Distance node
M	Unitless	Equation Coefficient
N	Unitless, RPM	Defined in Equation 26 Turbine Speed
Δt	sec	Time increment
k	$\text{Btu}/\text{in.}-\text{sec}-^{\circ}\text{R}$	Thermal Conductivity
q	Btu/sec	Heat Flow
H	$\text{Btu}/\text{sec}-\text{in.}^3$	Internal Heat Generation
ν	$^{\circ}\text{R}$	Temperature Rise Due to Internal Heat Generation
S	--	Axial Conduction Coefficient
C_p-C_R	$\text{Btu}/\text{in.}-^{\circ}\text{R}$	Specific Heat Fluid, Metal
E	$\text{in.}-\text{lb}/\text{lb}-\text{sec}^2$	Gravitational Constant
$\dot{v}$	$\text{lb}/\text{m}/\text{sec}$	Flow Rate
W	Btu/sec	Work
ϕ	in.	Hydraulic Diameter

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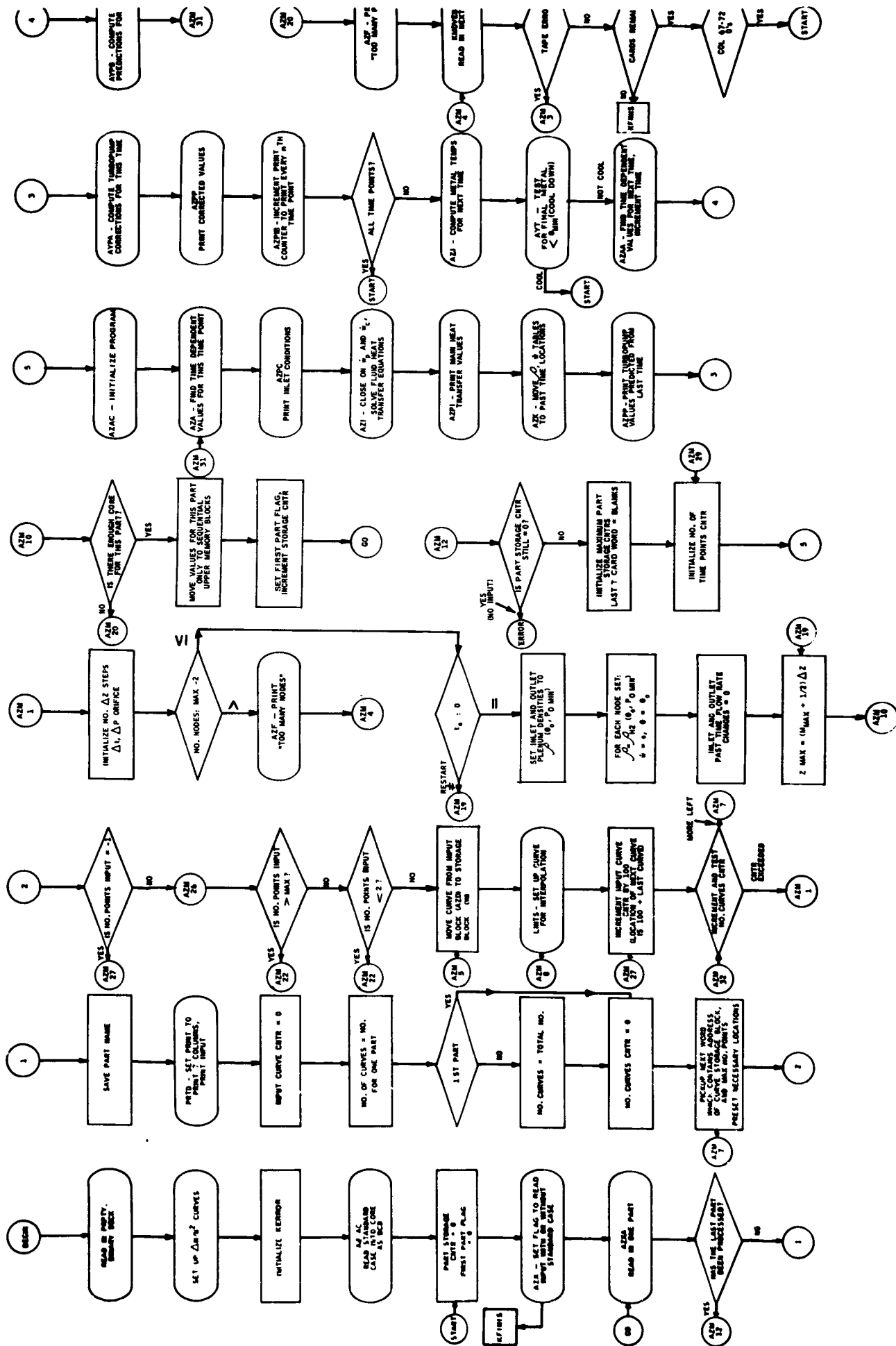
Symbol	Unit	Definition
I	in. ² -lbm	Moment of Inertia
Q _p	gal/min	Flow Rate
Q _i	Btu/sec	Internal Heat Generated
H	ft lbf/lbm	Pump Head Rise
h	Btu/lb	Enthalpy
S	Btu/lb-°R	Entropy
φ	Unitless	Friction Factor
η _T	Unitless	Turbine Efficiency
η _P	Unitless	Pump Efficiency
γ	Unitless	Ratio of Specific Heats
ω	rad/sec	Rotational Speed

B. SUBSCRIPTS

Subscripts	Description
1	Pump Inlet
2	Pump Outlet
3	Nozzle Tube Inlet
4	Nozzle Tube Outlet
6	Nozzle Chamber - Core Outlet
8	Hot Bleed Port Outlet
11	Turbine Inlet
12	Turbine Outlet
m	Distance Node
n, i	Time
T act	Actual Turbine
P act	Actual Pump
isen	Isentropic

Subscripts	Description
HM	Hot Mixture
CM	Cold Mixture
c	Cold
h	Hot
N	Nozzle
T	Turbine

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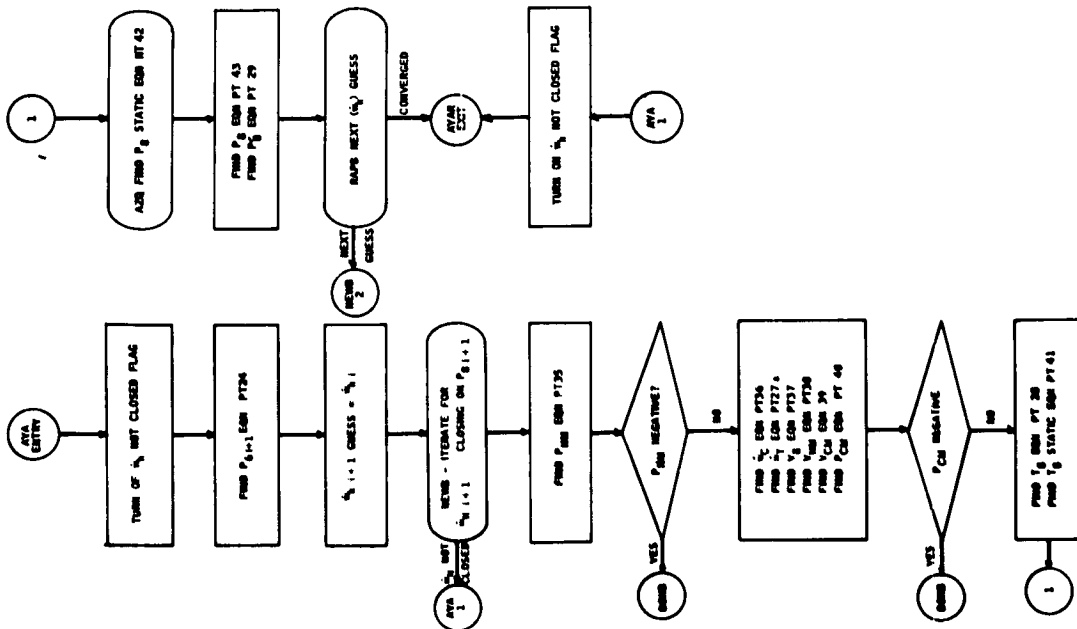


Figure 2
AYA
Iterate to Find v_h Closing on P
Page 50

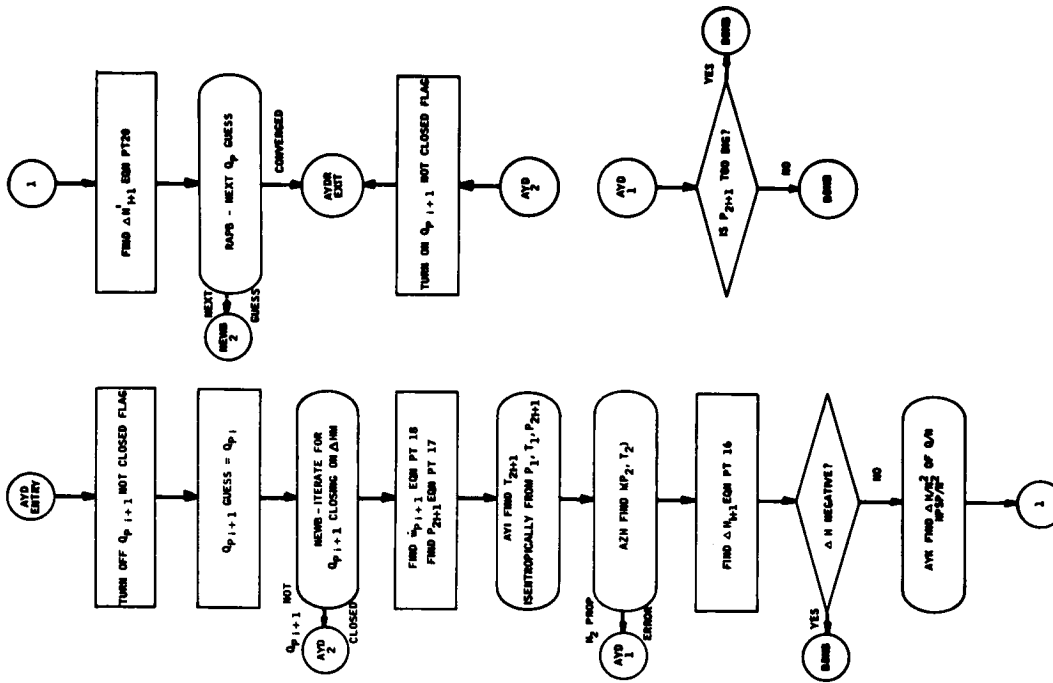


Figure 4
AYA
Find Pump Flow Rate
Page 52

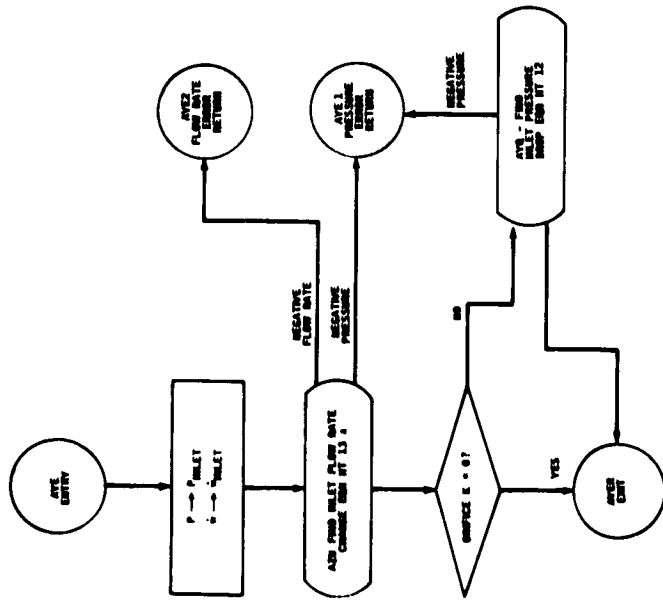


Figure 5
 AYE
 Find Inlet Pressure and Flow Rate Changes for One Part
 Page 53

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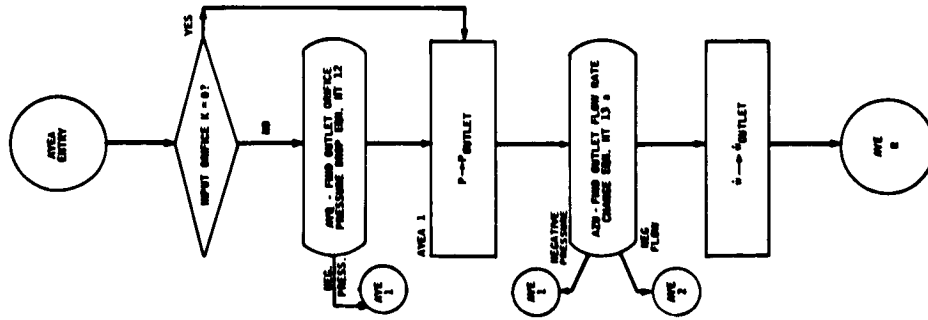


Figure 6
Find Outlet Pressure and Flow Rate for One Part
Page 54

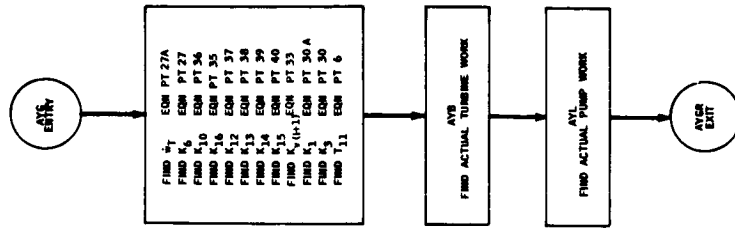


Figure 7
Region to Compute Part of Corrector Equations
Page 55

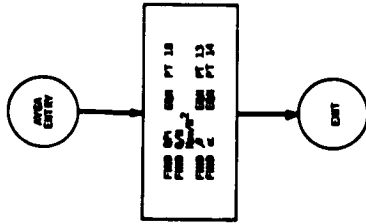


Figure 8
AYR
Compute Some Corrector Equations
Page 56

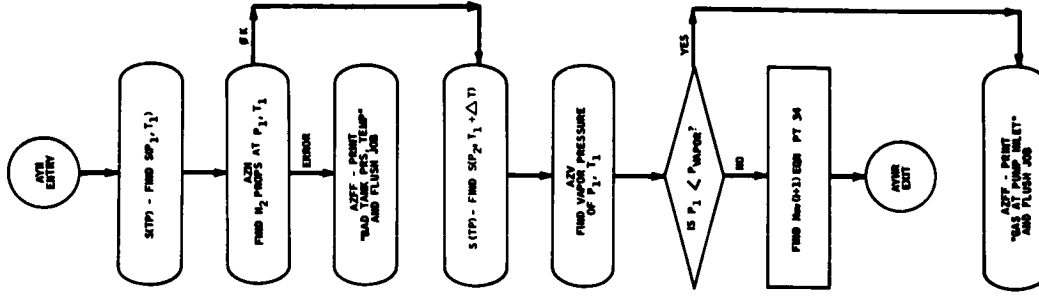


Figure 9
AYR
Look-Up Isentropic Values
Page 57

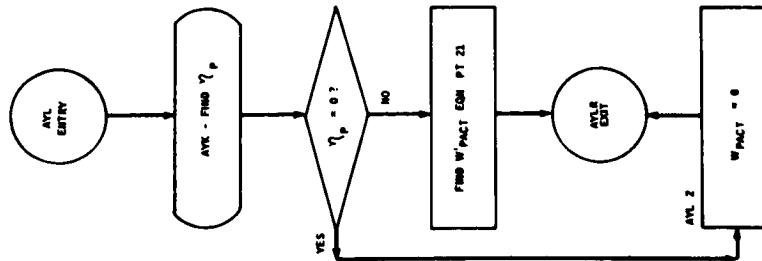


Figure 10
AVL
Compute Work Required by the Pump
Page 58

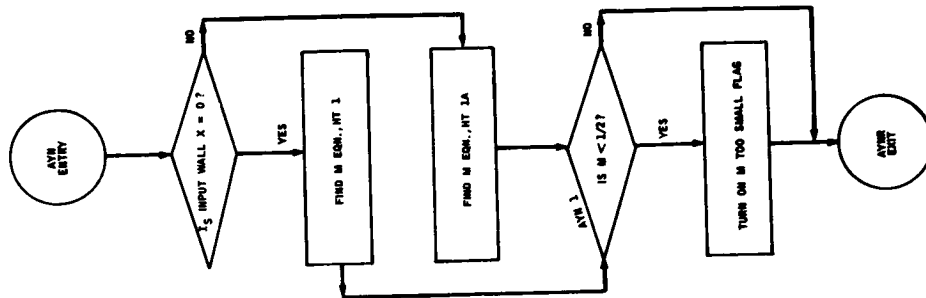


Figure 11
AVL
Compute Heat Resistance Term, M, for One Mode
Page 59

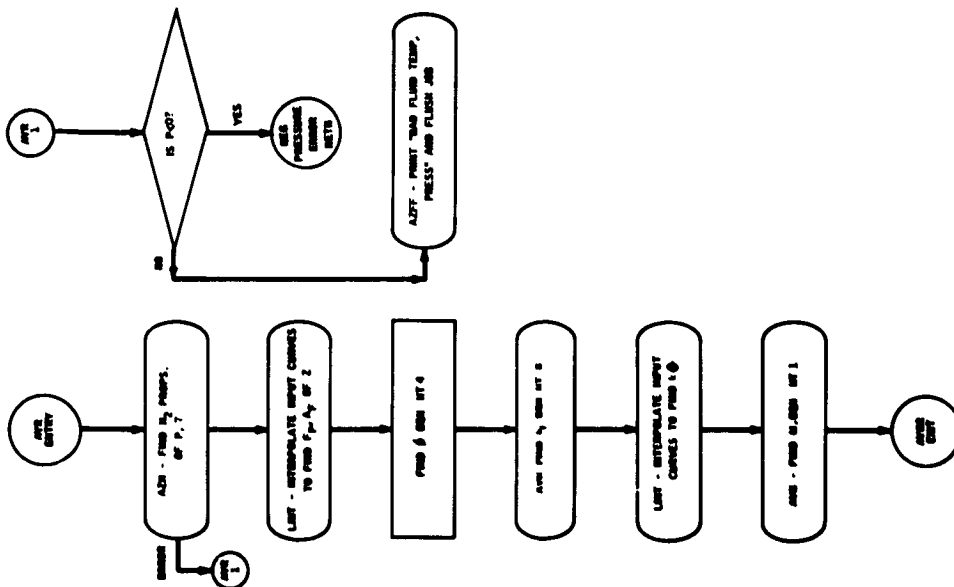


Figure 14
ATP
Fluid Values for One Mode
Page 62

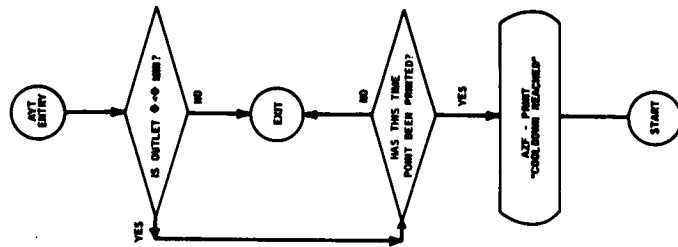


Figure 15
ATP
Check for Cool-Down Reached
Page 63

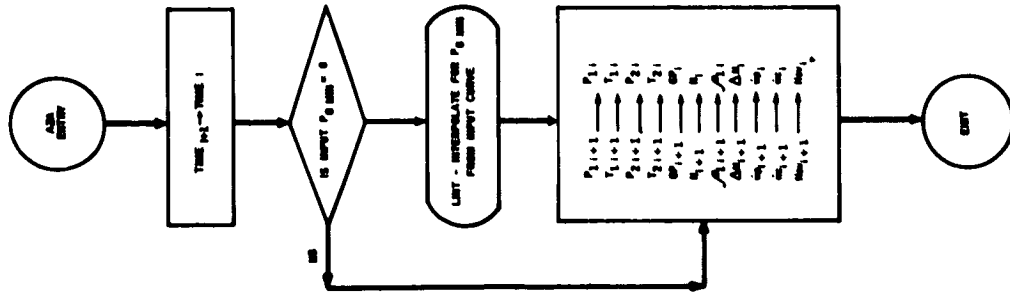


Figure 16
AZA
Set Values for One Time Step
Page 64

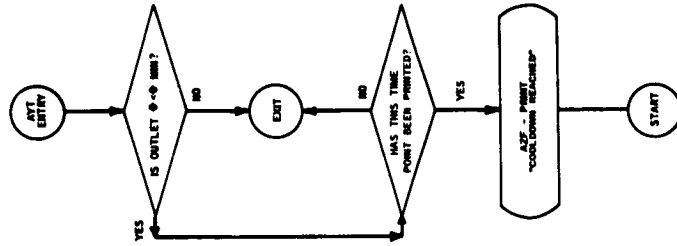


Figure 15
AZT
Check for Cool-Down Reached
Page 63

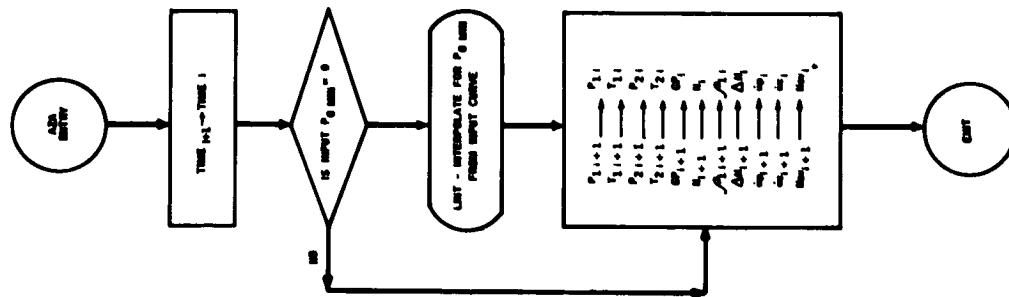


Figure 16
AZAA
Set Values for One Time Step
Page 64

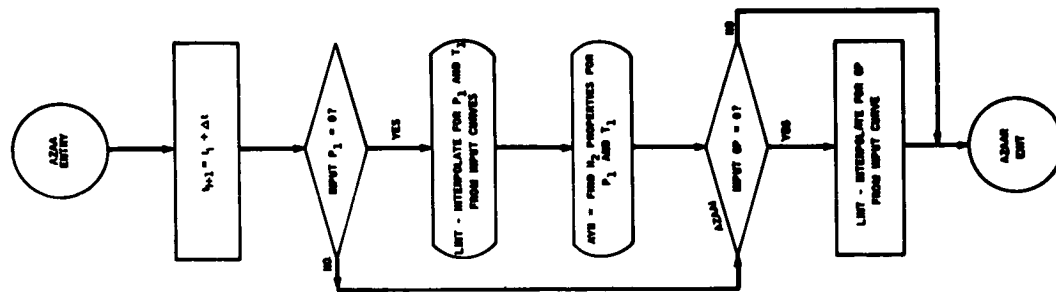


Figure 17
AZAA
Obtain Values for Next Time Point
Page 65

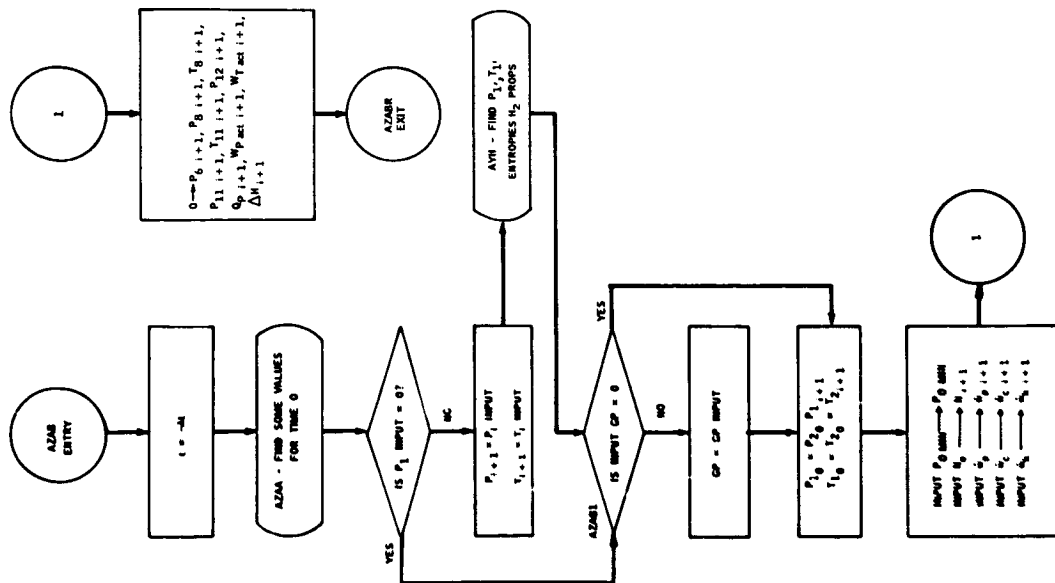


Figure 18
AZAB
Find Values at Zero Time

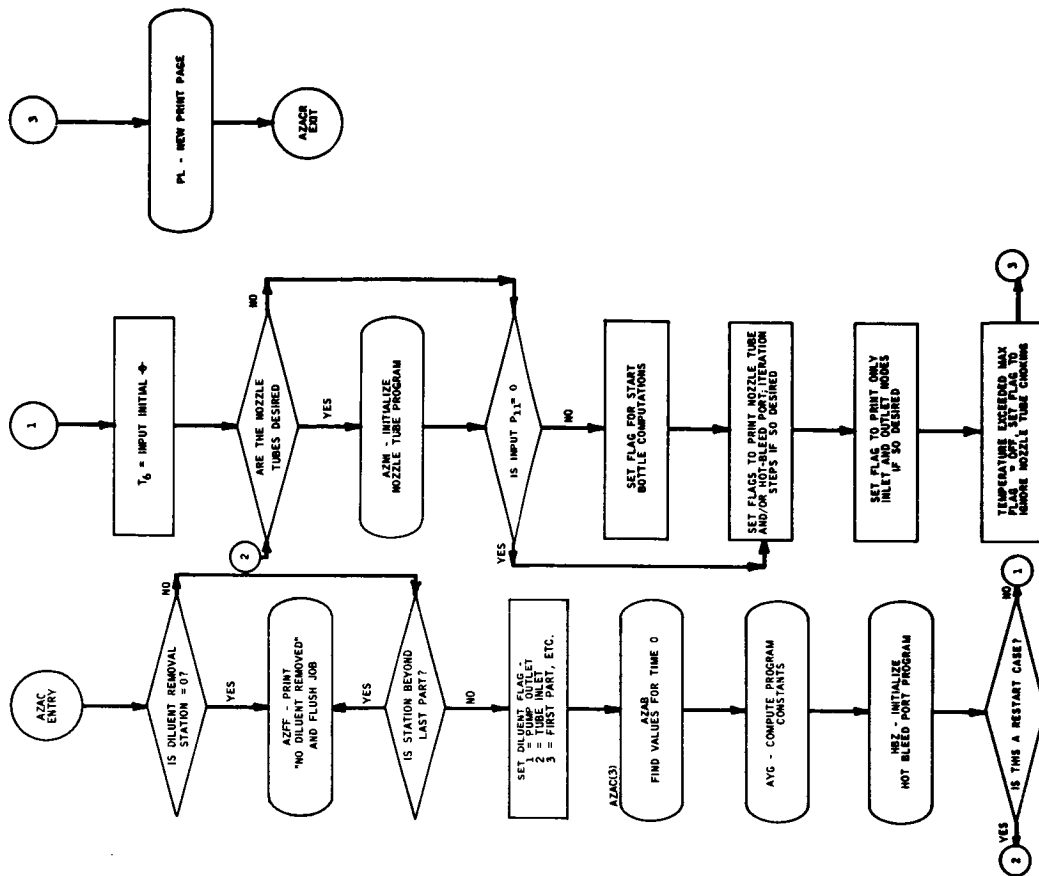


Figure 19
AZAC
Initialise Program

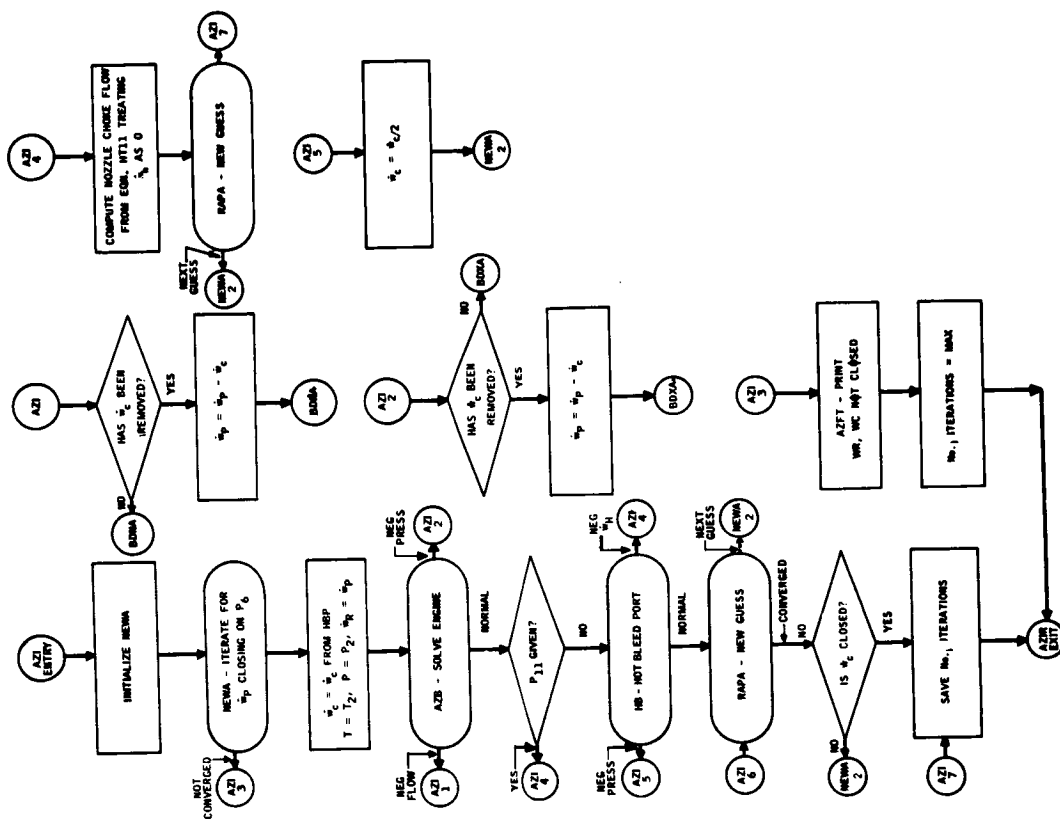


Figure 23
AZI
Heat-Transfer Iteration Master Control

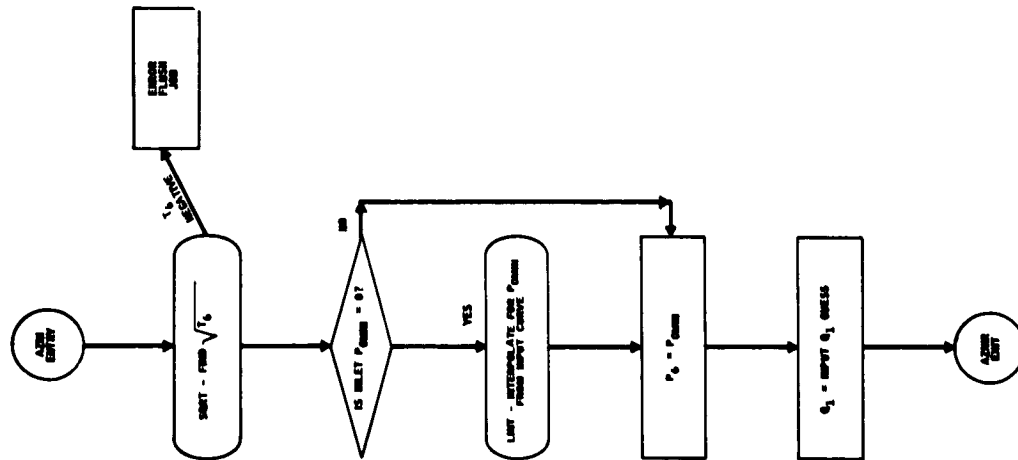


Figure 26
AZMI
Initialize Nozzle Tube Program

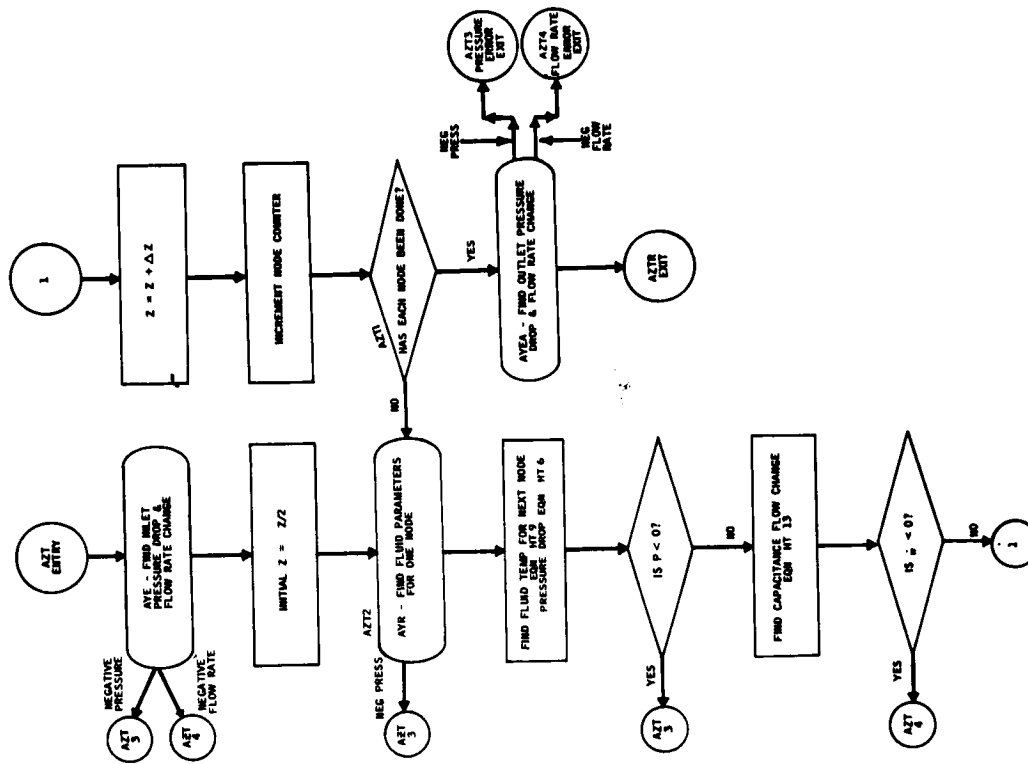


Figure 27
AZT
Fluid Node Corrections

Report No. NE-8-0114

APPENDIX A
NEVA ENGINE TRANSIENT PROGRAM

Page 77

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A. INPUT

1. General Input

VALUES ARE ENTERED ON DATA CARDS ANYWHERE BETWEEN COLUMNS 1 AND 72 INCLUSIVE. EACH VALUE MUST BE PRECEDED BY A SIGN (+ OR -). THE FOLLOWING ARE THE ONLY ALLOWABLE SYMBOLS ON DATA CARDS.

0-9 THE INTEGERS. NOTE THAT THE ZERO IS PUNCHED WITH THE (0-7) KEY

. THE DECIMAL POINT IS PERMITTED BUT NOT NECESSARY. FOR EXAMPLE
+10-10-+10-0

+ OR - EACH VALUE MUST BE PRECEDED BY A SIGN. NOTE THAT THE MINUS SIGN IS PUNCHED WITH THE (-SKIP,-) KEY.

E THIS IS USED TO INDICATE A POWER OF TEN. FOR EXAMPLE, +1000-+1E3
+10000E-1-+1E4

L THIS INDICATES A RELATIVE LOCATION. IF NO L IS SUPPLIED, THE RELATIVE LOCATION IS ASSUMED TO BE ZERO. ALL SUCCESSIVE VALUES AFTER AN L ARE ASSUMED TO BE IN SEQUENCE. THE LOCATION INCREASING BY 1. IF TWO OR MORE VALUES ARE SUPPLIED WITH THE SAME RELATIVE LOCATION, THE LAST ONE ENCOUNTERED IS THE ONE USED. FOR EXAMPLE IF THE SIXTH AND SEVENTH INPUT VALUES (RELATIVE LOCATIONS = 6 AND 6) WERE 21 AND 13-5, THESE VALUES WOULD BE ENTERED AS L6+21+13-5

BLANKS ARE COMPLETELY IGNORED EXCEPT BETWEEN THE DIGITS OF A SINGLE NUMBER.

EXCEPT FOR SPECIFIED COLUMNS, THERE ARE NO ILLEGAL SYMBOLS ON Y CARDS.

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3. Description

S = THIS VALUE IS SUPPLIED BY THE STANDARD CASE
0 = THIS VALUE AFFECTS THE LOGICAL SEQUENCE OF THE PROGRAM

h. Input

a. Input for Each Part

SYMBOL	UNITS	DESCRIPTION
DELTA Z	IN	SDISTANCE INCREMENT.
M MAX	NONE	SMNO. DELTA Z STEPS. IF THIS VALUE IS 0 THIS PART WILL BE IGNORED.
PHI	NONE	SFRICITION FACTOR.
F	NONE	SVOID FRACTIO .
RHO R	LB/IN3	SNETAL DENSITY.
X	IN	SQWALL THICKNESS. IF THIS VALUE IS NOT 0 THE PIPE OPTION WILL BE USED.
KPRESS IN	1/IN4	SPRESSURE DROP K FOR INLET ORFICE.
KPRESS OUT	1/IN4	SPRESSURE DROP K FOR OUTLET ORFICE.
V INLET	IN3	SINLET PLENUM VOLUME.
V OUTLET	IN3	SOUTLET PLENUM VOLUME.

b. Input for Entire System

PRINT INTL	NONE	SUPRINT INTERVAL. THIS VALUE IS OF THE FORM 1000A+B. IF A IS 0 EACH MODE WILL BE PRINTED. IF A IS NOT 0 ONLY THE FIRST AND LAST MODES FOR EACH PART WILL BE PRINTED. A PRINTOUT WILL BE MADE EVERY B TIMES DELTA T SECONDS.
TIME 0	SEC	SINITIAL TIME. IF THIS VALUE IS NOT 0 THIS CASE WILL BE TREATED AS A RESTART CASE AND ADDITIONAL INPUT WILL BE REQUIRED.
DELTA T	SEC	STIME INCREMENT.
NO. DEL T	NONE	NUMBER OF TIME POINTS DESIRED.
DEL T MIN	SEC	SMINIMUM ALLOWABLE TIME INCREMENT.

2. Cases

a. Input Case

AN INPUT CASE CONSISTS OF DATA FOR EACH PART FOLLOWED BY THE NOZZLE (SEE INPUT (IF ANY)). AND A FINAL T CARD. THE DATA FOR EACH PART CONSISTS OF THE DATA CARDS FOR THAT PART FOLLOWED BY A DATA CARD. THE PART CARD CONSISTS OF (1) T IN COL 1, (2) PART NAME IN COL 2-7, (3) ANY IDENTIFYING INFORMATION IN COL 8-72. THE FINAL INPUT WITH TWO EXCEPTIONS. (1) WHEN USING THE STANDARD CASE THE NUMBER OF PARTS MUST BE THE SAME AS IN THE STANDARD CASE. NOTE- SOME PARTS MAY BE IGNORED BY SETTING THE NUMBER OF MODES TO ZERO. (2) THE REQUIRED AMOUNT OF STORAGE MUST NOT EXCEED THE CAPACITY OF THE MACHINE. THE PROGRAM PRINTS A MESSAGE AND STOPS WHEN THIS OCCURS.

b. Standard Case

THE STANDARD CASE IS A FOUR PART CASE. INFORMATION IN THE INPUT CASE OVERRIDES THE STANDARD CASE BUT THE STANDARD CASE VALUES ARE RESET AT THE BEGINNING OF EACH NEW CASE. THOSE VALUES NOT IN THE STANDARD CASE ARE NOT RESET. IF THE STANDARD CASE IS NOT DESIRED, A CARD WHICH IS BLANK EXCEPT FOR AN X IN COL 1 AND T IN COL 1 AND T IN COL 1 ARE THE FIRST CARD OF THE INPUT CASE. THE PROGRAM PRINTS A MESSAGE AND STOPS WHEN THE STANDARD CASE IS USED WITH OTHER THAN A FOUR PART CASE.

125	THETA 0	DEGR	SPINENTIAL METAL TEMP. IF THIS VALUE IS NEGATIVE, THE PROGRAM WILL EXPECT METAL TEMPS TO BE INPUT FOR EACH MODE. METAL TEMPS ARE INPUT AS SPECIFIED FOR THE RESTART CASE.	135	ITER FLAG	NONE	THIS VALUE IS OF THE FORM 1000A/B. IF A IS NOT ZERO, EACH NOZZLE TUBE ITERATION STEP WILL BE PRINTED. IF B IS NOT ZERO, EACH HOT BLEED PORT ITERATION STEP WILL BE PRINTED.
	T MIN	DEGR	MINIMUM ALLOWABLE FLUID OUTLET TEMP.		GATE POS	PERCENT	STURBINE LINE VALVE GATE POSITION. IF THIS VALUE IS ZERO, THE PROGRAM WILL USE THE GATE POSITION CURVE.
	T MAX	DEGR	MAXIMUM ALLOWABLE TEMPERATURE.		A(KV)	NONE	SCONSTANT FOR K SUB V.
	B/L STA	NONE	POSITION OF INLET TO DILUENT LINE. 1=AT PUMP DISCHARGE, 2=AT NOZZLE TUBE INLET, 3=AT FIRST PART INLET, ETC.		B(KV)	NONE	SCONSTANT FOR K SUB V.
	P1	PSIA	STANK PRESSURE. IF THIS VALUE IS ZERO, THE PROGRAM WILL USE THE INLET PRESSURE AND TEMPERATURE CURVES.		GAMMA	NONE	RATIO OF SPECIFIC HEATS.
120	T1	DEGR	STANK TEMP.		K2	NONE	SK FOR NOZZLE TUBE INLET LINE PRESSURE DROP.
	P OUT MIN	PSIA	MINIMUM ALLOWABLE OUTLET PRESSURE. IF THIS VALUE IS 0 THE PROGRAM WILL USE THE P OUT MIN CURVE WHICH IN THIS CASE, MUST BE INPUT		C2	IN	DIAMETER OF NOZZLE TUBE INLET LINE.
	EPS P0	NONE	SHOT BLEED PORT OUTLET PRESSURE CLOSURE TOLERANCE.		DM	IN	DIAMETER OF HOT BLEED PORT.
	EPS P12	NONE	STURBINE OUTLET PRESSURE CLOSURE TOLERANCE.		DTL	IN	DIAMETER OF TURBINE LINE
	WOOTP GUESS LB/SEC		INITIAL PUMP FLOW RATE GUESS.		DTN	IN	DIAMETER OF TURBINE NOZZLE.
	WCOIC GUESS LB/SEC		INITIAL DILUENT FLOW RATE GUESS.	145	DRN	IN	DIAMETER OF ROLL CONTROL NOZZLE.
	WOOTH GUESS LB/SEC		INITIAL HOT BLEED PORT FLOW RATE GUESS.		IPT	LB-IN2	MOMENT OF PUMP AND TURBINE ROTOR.
	EPS WOOTC	NONE	DILUENT FLOW RATE CLOSURE TOLERANCE.		N INIT	RPM	INITIAL TURBINE SPEED.
	EPS WOOTR	NONE	SCORE OUTLET FLOW RATE CLOSURE TOLERANCE.		EPS H	NONE	PUMP HEAD RISE CLOSURE TOLERANCE.
	A6	IN2	AREA OF CONE OUTLET.		EPS WP ACT	NONE	PUMP ACTUAL WORK CLOSURE TOLERANCE.
130	A STAR	IN2	MINIMUM NOZZLE THROAT AREA.	150	L	IN	LENGTH OF HOT BLEED PORT.
	PHI(IN7)	NONE	NOZZLE TUBE FRICTION FACTOR. IF THIS VALUE IS 0 THE NOZZLE TUBES WILL BE IGNORED.		N	NONE	NUMBER OF PORTION STEPS IN HOT BLEED PORT.
	NO. PARTS	NONE	NO. OF SEGMENTS IN NOZZLE TUBES (DISTANCE MODES).		DCO	IN	DIAMETER OF HOT BLEED PORT COLD FLOW HOLES.
	WT WALL X	IN	NOZZLE TUBE WALL THICKNESS.		NCO	NONE	NUMBER OF HOT BLEED PORT COLD FLOW HOLES.
	G1 INIT	BTU/SEC-IN2	INITIAL W-T TRANSFER GUESS FOR NOZZLE TUBES.		T	IN	THICKNESS OF HOT BLEED PORT COLD FLOW ANNULUS.
				155	R	IN	THICKNESS OF METAL BETWEEN HOT AND COLD FLOWS IN HOT BLEED PORT.
					THETA	DEG	DILUENT IMPINGENT ANGLE.
					L50	NONE	SHOT BLEED PORT COLD FLOW FILM COEFF PARAMETER.
					A COLD	NONE	SHOT BLEED PORT COLD FLOW FILM COEFF PARAMETER.
					B COLD	NONE	SHOT BLEED PORT COLD FLOW FILM COEFF PARAMETER.

160 C COLD NONE SHOT BLEED PORT COLD FLOW FILM COEFF PARAMETER.
 161 A HOT NONE SHOT BLEED PORT HOT FLOW FILM COEFF PARAMETER.
 162 B HOT NONE SHOT BLEED PORT HOT FLOW FILM COEFF PARAMETER.
 163 C HOT NONE SHOT BLEED PORT HOT FLOW FILM COEFF PARAMETER.
 164 F COLD NONE SHOT BLEED PORT COLD FLOW FRICTION FACTOR.
 165 F HOT NONE SHOT BLEED PORT HOT FLOW FRICTION FACTOR.
 166 K FOR PWR-P00-CMB.CC.
 167 K FOR PCH. CC.
 168 K IN NONE SHOT BLEED PORT INLET PRESSURE DROP.
 169 K CC NONE INCOMPRESSIBLE FLOW K.
 170 K CI NONE INCOMPRESSIBLE FLOW K.
 171 B COLD FT-LBP/LB-DEGR SCOLD GAS CONSTANT.
 172 B HOT FT-LBP/LB-DEGR SHOT GAS CONSTANT.
 173 K II NONE K FOR P00.
 174 K S NONE K FOR P00.
 175 K E NONE K FOR P00.
 176 P II PSIA SUPPLEMENTARY IN TURBINE INLET START BOTTLE. IF THIS VALUE IS ZERO, THE PROGRAM WILL ASSUME THAT THERE IS NO START BOTTLE.
 177 Y II DEGR TURBINE START BOTTLE TEMPERATURE.
 178 BELLONS FLAG NONE SHOT THIS VALUE IS ZERO. THE BELLONS SECTIONS WILL BE IGNORED.
 179 BELLONS K NONE STABLE OF BELLONS SECTION PRESSURE DROP K VALUES VS DISTANCE (IN) INPUT AS 0.0. A MAXIMUM OF TEN PAIRS OF VALUES IS ALLOWED. THE DISTANCES MUST BE IN ASCENDING ORDER AND THE LAST DISTANCE SHOULD BE GREATER THAN OR EQUAL TO THE LENGTH OF THE HOT BLEED PORT.

5. Input Curves

a. General

EACH CURVE IS INPUT AS A SERIES OF NUMBERS, EACH PRECEDED BY A SIGN. THE FIRST NUMBER IS THE NUMBER OF POINTS IN THE CURVE. EACH FOLLOWING PAIR OF NUMBERS REPRESENTS A POINT ON THE CURVE. THE INDEPENDENT VARIABLE FIRST. FOR EXAMPLE, THE POINTS (1.1), (1.2), (2.0) ARE INPUT AS 2.1, 1.1, 2.0. THE NUMBER OF POINTS PER CURVE MUST BE GREATER THAN OR EQUAL TO 2, OR EQUAL TO -1. IF THE NUMBER OF POINTS IS -1 THE CURVE WILL BE IGNORED. NOTE THAT A CURVE WHICH IS IGNORED IS NOT THE SAME AS A CURVE WHOSE DEPENDENT VARIABLE IS EVERYWHERE 0. A MAXIMUM NO. OF POINTS IS GIVEN FOR EACH CURVE. ALL CURVES MUST BE IN ASCENDING ORDER OF THE INDEPENDENT VARIABLE.

b. For Each Part

1100 A SUB F IN2 SFLOW AREA VS DISTANCE (IN) 10
 1200 F SUB P IN SMETTED PERIMETER VS DISTANCE (IN) 10
 1300 FRACT H NONE SFRACTION (PERCENT/100) OF INTERNAL HEAT GENERATION VS DISTANCE (IN) 10
 1400 H BTU/IN3-SEC INTERNAL HEAT GENERATION COEFF VS TIME (SEC) 49
 1500 K SUB R BTU/SEC-IN-DEGR SMETAL THERMAL CONDUCTIVITY VS TEMP (DEGR) 49
 1600 C SUB R BTU/LB-DEGR SMETAL HEAT CAPACITY VS TEMP (DEGR) 49

c. For Entire System

1700 T I DEGR STANK TEMP VS TIME (SEC) 49
 1800 P I PSIA STANK PRESSURE VS TIME (SEC) 49
 1900 P OUT MIN PSIA MINIMUM OUTLET PRESSURE VS TIME (SEC) 49
 2000 CP PERCENT SCATE POSITION OF TURBINE LINE VALVE VS TIME (SEC) 10

6. Nozzle Tube Input

A SET OF NOZZLE TUBE INPUT VALUES IS CONTAINED IN THE STANDARD CASE BUT IS NOT RESET FOR EACH INPUT CASE. THE DATA CARDS FOR NOZZLE TUBE INPUT VALUES ARE PLACED BETWEEN THE LAST PART T CARD AND THE FINAL T CARD OF AN INPUT CASE.

10	AF COLD	IN2	TABLE OF COLD FLOW AREA VS DISTANCE (IN) INPUT AS SEVEN PAIRS OF VALUES OF THE FORM +Z+NF.
114	FP COLD	IN	TABLE OF COLD FLOW WETTED PERIMETER VS DISTANCE (IN) INPUT AS SEVEN PAIRS OF VALUES OF THE FORM +Z+PP.
128	D	IN	TABLE OF DIAMETER VS DISTANCE (IN) INPUT AS FOUR PAIRS OF VALUES OF THE FORM +Z+D.
136	RF	NONE	TABLE OF RECOVERY FACTOR VS DISTANCE (IN) INPUT AS FOUR PAIRS OF VALUES OF THE FORM +Z+RF.
144	AF HOT	IN2	TABLE OF HOT FLOW AREA VS DISTANCE (IN) INPUT AS SEVEN PAIRS OF VALUES OF THE FORM +Z+AF.
158	SIGMA	NONE	TABLE OF STATIC TO STAGNATION TEMP RATIO VS DISTANCE (IN) INPUT AS NINE PAIRS OF VALUES OF THE FORM +Z+SIGMA.

NOTE- THE ABOVE TABLES MUST BE IN ASCENDING ORDER OF DISTANCE.

176	K(P IN)	NONE	INLET PRESSURE DROP K
180	LENGTH	IN	LENGTH OF NOZZLE TUBES
184	K	NONE	THERMAL CONDUCTIVITY CONSTANT
188	SKRM	NONE	THERMAL CONDUCTIVITY CONSTANT
192	CKRM	NONE	THERMAL CONDUCTIVITY CONSTANT
196	AKMF	NONE	FILM COEFF CONSTANT
200	BKMF	NONE	FILM COEFF CONSTANT
204	TEXT	BUMP NONE	INITIAL EXIT TEMP GUESS BUMPER
208	Z THRAT	IN	DISTANCE TO MINIMUM THROAT AREA
212	A THRAT	IN2	MINIMUM THROAT AREA

3. Restarting Program

AT THE PRESENT TIME, THE PROGRAM MAY NOT BE RESTARTED. THE FORMAT FOR INPUTTING METAL TEMPERATURES FOLLOWS.

LCC	SYMBOL	UNITS	DESCRIPTION
1-156	THETA	DEGR	METAL TEMPS FOR EACH NODE. THE FIRST VALUE IS A LINEAR EXTRAPOLATION OF THE FIRST TWO PRINTED NODES. THE SECOND VALUE IS EQUAL TO THE PRINTED TEMP FOR THE FIRST NODE. THE THIRD VALUE IS THE TEMP FOR THE SECOND NODE. ETC. THE LAST VALUE IS A LINEAR EXTRAPOLATION OF THE LAST TWO PRINTED NODES. TOTAL OF NMAX+2 VALUES.

C. PROGRAM MESSAGES

BAD FLUID TEMP-PROS PROPERTY ROUTINES. FLUID TEMP OR PRESSURE OUTSIDE RANGE OF HYDROGEN PROPERTY ROUTINES. USUALLY INDICATES DRASTIC ERROR IN INPUT OR CONVERGENCE

BAD TIME PROS. TMP P1 OR T1 NOT IN RANGE OF HYDROGEN PROPERTY ROUTINE

BAD TAP- PLUM RTT CHECK ON INPUT TAP

CHECK PUMP FOR NEG CONVERGENCE SOME QUANTITY NEGATIVE. DRASTIC ERROR IN INPUT OR CONVERGENCE

COOLDOWN REACHED OUTLET METAL TEMP LESS THAN THETA MIN

DELTA T TOO SMALL TIME INCREMENT LESS THAN MIN

END OF INPUT NO CASES REMAINING OR TCARD MISSING

ERROR IN PTS/CURVE NUMBER OF POINTS MUST BE GREATER THAN 1 AND LESS THAN MAXIMUM. CURVE MAY BE MISSING ALTOGETHER

ERROR IN STD INPUT TOO MANY CARDS OR TCARD MISSING IN STANDARD CASE

GAS AT PUMP INLET PRESSURE AND TEMP AT PUMP INLET DETERMINE GAS. PUMP OVERSPEEDS. MSV IS NEGATIVE

HEAT TRANSFER ERROR ERROR IN HEAT TRANSFER OTHER THAN NEGATIVE PRESSURE ON FLOW

HELP HELP HELLLLPP SOMETHING DRASTICALLY WRONG WITH INPUT OR INPUT TAP- SEE PROGRAMMER.

ILLEGAL CHARACTER ILLEGAL CHARACTER ON ONE OR MORE DATA CARDS. CARDS WITH ERRORS WILL BE PRINTED OUT. IF NO ILLEGAL CHARACTERS ARE FOUND. SEE PROGRAMMER.

LIG IN TUBE THROAT FLUID IN NOZZLE TUBE THROAT WAS LIQUID ON LAST PASS PRINTS ONLY AT PRINTED TIME POINTS

P TCC SMALL P LESS THAN 1/2 AT SCV. NOCE. PRINTED AT END OF P1P: WHEN OCCURRED. MAY HAVE OCCURRED AT SOME TIME POINT BETWEEN PRINTING BUT PRINTED AT LATER POINT

NO DILUENT REMOVED NO INPUT DILUENT REMOVAL STATION

NOZZLE TUBE ERROR ERROR ON LAST PASS THROUGH NOZZLE TUBES. TUBES THEREFORE IGNORED.

P4 TOO LOW P4 LESS THAN P0MIN

PREDICTOR FAILED SOME ITERATION FAILED TO CLOSE IN TURBOPUMP PREDICT

TEMP EXCEEDED MAX METAL OR FLUID TEMPERATURE GREATER THAN THAL. PRINTED AFTER PART WHEN OCCURRED. MAY HAVE OCCURRED BETWEEN PRINTED TIME POINTS BUT PRINTED LATER

TOO MANY MOSES NUMBER OF MOSES EXCEEDS MAXIMUM IN ONE OR MORE PART

TOO MANY PARTS NOT ENOUGH S-ORANGE AVAILABLE FOR THIS MANY PARTS

WE. WC NOT CLOSED MAX ITERATIONS IN HEAT TRANSFER EXCEEDED

ZERO TCARD MISSING OCCURS ONLY WITH CASE USING STANDARD INPUT. TCARD LEFT OFF OR MORE PARTS THAN STANDARD CASE

***** NOT CLOSED THE SPECIFIED HOT BLEED PORT ITERATION DID NOT CLOSE

APPENDIX B

SAMPLE CASE - NERVA ENGINE TRANSIENT PROGRAM

PROGRAM INPUT													
DEL Z	1.00000	2. P15	1.00000	PRCT	1.00000	WID P	1.00000	MAL R	1.00000	ENT A	1.00000	ENT V	1.00000
PRIM	1.00000	TIME 0	1.00000	DEL T	1.00000	T P15	1.00000	OT RIN	1.00000	HE TAP	1.00000	DELUT	1.00000
T1	1.00000	NO MIN	1.00000	P1 CLS	1.00000	WID P	1.00000	WID C	1.00000	HE CLS	1.00000	HE CLS	1.00000
A STAR	1.00000	RTD PF	1.00000	PARTS	1.00000	MAL Z	1.00000	OT RIN	1.00000	WID P	1.00000	WID C	1.00000
R 2	1.00000	D 2	1.00000	D H	1.00000	D TL	1.00000	D TH	1.00000	PI	1.00000	WID C	1.00000
HE LTH	1.00000	NO Z	1.00000	D CO	1.00000	NO HLS	1.00000	T	1.00000	THETA	1.00000	A CLD	1.00000
C CLD	1.00000	A HOT	1.00000	B HOT	1.00000	C HOT	1.00000	PRCT C	1.00000	REPRM	1.00000	REPRM	1.00000
AC CAP	1.00000	SC INC	1.00000	R CLD	1.00000	R HOT	1.00000	R 11	1.00000	R 11	1.00000	R 11	1.00000
SEC 1	1.00000	R 1	1.00000	SEC 2	1.00000	R 2	1.00000	SEC 3	1.00000	R 3	1.00000	SEC 5	1.00000
SEC A	1.00000	R A	1.00000	SEC 7	1.00000	R 7	1.00000	SEC 8	1.00000	R 8	1.00000	SEC 10	1.00000
FLW AREA VS DISTANCE	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000
METED PERIMETER VS Z	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000
PRCT HEAT GEN VS DIST	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000
INT HEAT GEN VS TIME	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000
THERMAL CONDUCTIVITY	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000
C. SW R VS TEMPERATURE	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000
INLET TEMP VS TIME	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000
INLET PRESSURE VS TIME	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000
OUTLET PRESSURE VS TIME	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000
GATE POSITION VS TIME	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000
1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000

PROGRAM INPUT													
DEL Z	1.00000	2. P15	1.00000	PRCT	1.00000	WID P	1.00000	MAL R	1.00000	ENT A	1.00000	ENT V	1.00000
FLW AREA VS DISTANCE	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000
METED PERIMETER VS Z	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000
PRCT HEAT GEN VS DIST	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000
INT HEAT GEN VS TIME	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000
THERMAL CONDUCTIVITY	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000
C. SW R VS TEMPERATURE	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000
INLET TEMP VS TIME	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000
INLET PRESSURE VS TIME	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000
OUTLET PRESSURE VS TIME	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000
GATE POSITION VS TIME	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000
1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000

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1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	
00121	12374	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52
00121	12374	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52
00121	12374	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52
00121	12374	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52
00121	12374	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52
00121	12374	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52
00121	12374	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52
00121	12374	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52
00121	12374	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28																								

163*MASTER CONTROL REGION
24416 0 60000 0 40316 164 BEGIN STZ PP41
24417 0 76000 0 00016 165 +1 LMTM
24420 0 07401 4 00053 166 +2 TSX KBINLD,4,1 READ IN PRPTY
24421 0 07400 4 40710 167 +3 TSX ICURV,4
24422 0 00061 0 00005 168 +4 PZE S,,49
24423 0 00000 0 00020 169 +5 PZE 16
24424 0 00000 0 31113 170 +6 PZE AYK01
24425 -0 50000 0 32576 171 +7 CAL ENDO
24426 0 60200 0 00056 172 +8 SLW KERROR
24427 0 07400 4 27323 173 +9 TSX AZXC,4 READ STANDARD CASE
24430 0 63400 0 24603 174 START SXA AZM10,0
24431 0 60000 0 32721 175 +1 STZ X+3
24432 0 07400 4 27161 176 +2 TSX AZX,4 TEST INPUT FOR NEW CASE
24433 0 07400 4 27236 177 GO TSX AZXA,4 INPUT
24434 -0 52000 0 32612 178 +1 NZT TCARD+11
24435 0 02000 0 24615 179 +2 TRA AZM12 END OF CASE
24436 -0 50000 0 32577 180 +3 CAL TCARD
24437 0 56000 0 32600 181 +4 LDQ TCARD+1
24440 -0 76300 0 00006 182 +5 LGL 6
24441 0 60200 0 34555 183 +6 SLW FX PART NAME
24442 0 07400 4 32113 184 +7 TSX PRTD,4
24443 0 63400 0 24500 185 +8 SXA AZM8,0
24444 -0 77400 1 00006 186 +9 AXC NCTMP,1
24445 -0 52000 0 32721 187 +10 NZT X+3 O= 1ST PART
24446 -0 77400 1 00012 188 +11 AXC NCURV,1
24447 0 77400 2 00000 189 +12 AXT 0,2
24450 -0 63400 1 24507 190 +13 SXD AZM32,1
24451 0 77400 1 00000 191 +14 AXT 0,1
24452 -0 50000 1 24703 192 AZM7 CAL AZM01,1
24453 0 62100 0 24472 193 +1 STA AZM24
24454 0 62100 0 24502 194 +2 STA AZM6 TABLE STORAGE ADDRESS
24455 0 62200 0 24465 195 +3 STD AZM26 LINTS
24456 0 36100 0 40200 196 +4 ACL FX1
24457 0 62100 0 24474 197 +5 STA AZM25
24460 0 63400 1 24505 198 +6 SXA AZM28,1
24461 0 50000 2 36230 199 +7 CLA AZD,2 NO. PTS
24462 -0 12000 0 24503 200 +8 TMI AZM27 -- CURVE NOT NEEDED
24463 -0 30000 0 40306 201 +9 UFA FIX
24464 0 73400 4 00000 202 +10 PAX ,4
24465 3 00000 4 24676 203 AZM26 TXH AZM22,4,**0 TOO MANY PTS
24466 -3 00001 4 24676 204 +1 TXL AZM22,4,1 TOO FEW PTS.
24467 -0 63400 4 24502 205 +2 SXD AZM6,4
24470 0 77400 1 00000 206 +3 AXT 0,1
24471 0 50000 2 36231 207 AZM5 CLA AZD+1,2
24472 0 60100 1 00000 208 AZM24 STO **0,1
24473 0 50000 2 36232 209 +1 CLA AZD+2,2
24474 0 60100 1 00000 210 AZM25 STO **0,1
24475 1 77776 1 24476 211 +1 TXI **1,1,-2
24476 1 77776 2 24477 212 +2 TXI **1,2,-2
24477 2 00001 4 24471 213 +3 TIX AZM5,4,1
24478 0 77400 1 00000 214 AZM2 TXI **2

JOB 12013.

25/09/64

PAGE

3

24501 0 07400 4 42511 215 +1 TSX LINTS,4
24502 0 00000 0 00000 216 AZM6 PZE **0,**0
24503 1 77634 2 24504 217 AZM27 TXI **1,2,-100
24504 0 63400 2 24500 218 +1 SXA AZM8,2
24505 0 77400 1 00000 219 AZM28 AXT **0,1
24506 1 77777 1 24507 220 +1 TXI **1,1,-1
24507 3 00000 1 24452 221 AZM32 TXH AZM7,1,**0
24510 0 50000 0 36065 222 AZM1 CLA DMHAX
24511 -0 30000 0 40306 223 +1 UFA FIX
24512 0 62100 0 34556 224 +2 STA FX+1 NO. DEL 2 PTS
24513 0 50000 0 40200 225 +3 CLA FX1
24514 0 60100 0 34562 226 +4 STO FX+5
24515 0 50000 0 36100 227 +5 CLA DELT
24516 0 60100 0 35625 228 +6 STO PT+11
24517 0 60000 0 35616 229 +7 STZ PT+4
24520 0 60000 0 35617 230 +8 STZ PT+5
24521 0 77400 2 00000 231 +9 AXT 0,2
24522 0 53400 1 34556 232 +10 LXA FX+1,1
24523 -3 00060 1 24526 233 +11 TXL **3,1,NZMAX-2
24524 -1 24670 0 25421 234 +12 SYR AZF,,AZM11 TOO MANY NODES
24525 0 02000 0 24654 235 +13 TRA AZM4 FLUSH CASE
24526 1 00001 1 24527 236 +14 TXI **1,1,1
24527 0 52000 0 36077 237 +15 ZET DTMI INITIAL TIME
24530 0 02000 0 24573 238 +16 TRA AZM19
239*RESTART CASE TRANSFERS AROUND HERE
24531 0 50000 0 32640 240 +17 CLA P+18
24532 0 52000 0 32721 241 +18 ZET X+3
24533 0 02000 0 24542 242 +19 TRA AZM17
24534 0 50000 0 36111 243 +20 CLA DPO
24535 -0 10000 0 24541 244 +21 TNZ AZM17-1
24536 0 75400 0 00000 245 +22 PXA ,0
24537 0 07400 4 42437 246 +23 TSX LINT,4
24540 0 00000 0 33441 247 +24 PZE WPO
24541 0 60100 0 32640 248 +25 STO P+18
24542 0 50000 0 36103 249 AZM17 CLA DTHO
24543 0 12000 0 24546 250 +1 TPL **3
24544 0 50000 2 35636 251 +2 CLA AZO1,2
24545 0 02000 0 24547 252 +3 TRA **2
24546 3 00000 2 24556 253 +4 TXH AZM9,2,0
24547 0 56000 0 32640 254 +5 LDQ P+18
24550 0 07400 4 25564 255 +6 TSX AZH,4
24551 0 07400 4 42602 256 +7 TSX ERROR,4
24552 0 56000 0 33730 257 +8 LDQ WPR+6 RHO
24553 0 50000 0 36103 258 +9 CLA DTHO
24554 3 00000 2 24556 259 +10 TXH AZM9,2,0
24555 -0 60000 0 35620 260 +11 STQ PT+6 INLET
24556 -0 60000 2 35720 261 AZM9 STQ AZO6,2
24557 -0 12000 0 24561 262 +1 TMI **2
24560 0 60100 2 35636 263 +2 STO AZO1,2
24561 0 60000 2 36002 264 +3 STZ AZO8,2
24562 1 77777 2 24563 265 +4 TXI **1,2,-1
24563 2 00001 1 24562 266 +5 TIX AZM17,1,1
24564 -0 60000 0 35634 267 +6 STQ PT+18 OUTLET DENSITY

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24566 0 60100 2 35636 269 +8 STO AZ01,2
24567 0 50000 2 35636 270 +9 CLA AZ01,2
24570 0 60100 0 32633 271 +10 STO P+13
24571 0 60000 0 35626 272 +11 STZ PT+12
24572 0 60000 0 35627 273 +12 STZ PT+13
24573 0 50200 0 36064 274 AZM19 CLS DELZ
24574 0 24100 0 40214 275 +1 FDP FL2
24575 -0 60000 0 35615 276 +2 STQ PT+3
24576 0 50000 0 36065 277 +3 LDQ DMMAx
24577 0 26000 0 36064 278 +4 FHP DELZ
24600 0 30000 0 35615 279 +5 FAD PT+3
24601 0 60100 0 35615 280 +6 STO PT+3
281*MOVE DATA TO STORAGE
282 +7 AXT AZMTS,2
283 AZM10 AXT *0,4
284 +1 TXL *+2,4,0
285 +2 TXL AZM20,4,AZMT+AZMTS+206
286 +3 CLA AZMTE,2
287 +4 STO AZMT,4
288 +5 TXI *+1,4,-1
289 +6 TIX *-3,2,1
290 +7 SXA AZM10,4
291 +8 STL X+3
292 +9 TRA GO
293*END OF MULTI-PHASE INPUT
294 AZM12 XEC AZM10
295 +1 TXL ERROR,4,0
296 +2 TXI *+1,4,-AZMTG
297 +3 SXD AZB3,4
298 +4 SXD AZPI4,4
299 +5 SXD AZK4,4
300 +6 SXD AZJ9,4
301 +7 SXD AZAC7,4
302 +8 CAL BLANK
303 +9 SLW TCARD+11
304*INITIALIZE FOR SINGLE AND MULTIPLE PARTS
305 AZM29 CLA ONDT
306 +1 UFA FIX
307 +2 ACL FX1
308 +3 PAX ,1
309 +4 TSX AZAC,4
310 AZM31 TSX AZA,4
311 +1 TSX AZPC,4
312 +2 TSX AZI,4
313 +3 TSX AZPI,4
314 +4 TSX AZK,4
315 +5 TSX AZPP,4
316 +6 TSX AYPA,4
317 +7 TSX AZPP,4,1
318 +8 TSX AZPI8,4
319 +9 TNX START,1,1
320 AZM2 TSX AZJ,4
321 +1 TSX AYT,4
322 +2 TSX AZA,4
24615 0 52200 0 24603 294
24616 -3 00000 4 42602 295
24617 1 62717 4 24620 296
24620 -0 63400 4 25321 297
24621 -0 63400 4 26543 298
24622 -0 63400 4 26217 299
24623 -0 63400 4 26056 300
24624 -0 63400 4 25217 301
24625 -0 50000 0 40304 302
24626 0 60200 0 32612 303
24627 0 50000 0 36101 305
24630 -0 30000 0 40306 306
24631 0 36100 0 40200 307
24632 0 73400 1 00000 308
24633 0 07400 4 25201 309
24634 0 07400 4 25034 310
24635 0 07400 4 26324 311
24636 0 07400 4 25633 312
24637 0 07400 4 26462 313
24640 0 07400 4 26170 314
24641 0 07400 4 26664 315
24642 0 07400 4 31601 316
24643 0 07401 4 26664 317
24644 0 07400 4 26617 318
24645 -2 00001 1 24430 319
24646 0 07400 4 25752 320
24647 0 07400 4 32006 321
24648 0 07400 4 36075 322
24651 0 07400 4 31627 323
24652 0 02000 0 24634 324
325*EL FLUSH FOR INPUT ERRORS-- TOO MANY PARTS
326 AZM20 STR AZF,,AZM21
327 AZM4 TSX KMOVEB,4,62
328 +1 FVE TCARD,,12
329 +2 TQP AZM3
330 +3 TPL *+2
331 +4 TSX KFINIS,4
332 +5 CAL TCARD+11
333 +6 TNZ AZM20+1
334 +7 TRA START
335 AZM3 STR AZFF,,AZM30
336 AZM21 BCI 3,TOO MANY PARTS
337 AZM11 BCI 3,TOO MANY NODES
338 AZM30 BCI 3,HELP HELP HEELLLL
339*EL FLUSH FOR MISSING CURVE OR TOO MANY POINTS
340 AZM22 STR AZF,,AZM23
341 +1 TRA AZM20+1
342 AZM23 BCI 3,ERROR IN PTS/CURVE
343 AZM01 PZE WAF,,10
344 +1 PZE WFP,,10
345 +2 PZE WH,,10
346 +3 PZE WHT,,49
347 +4 PZE WK,,49
348 +5 PZE WCR,,49
349 +6 PZE WTI,,49
350 +7 PZE WPI,,49
351 +8 PZE WPO,,49
352 +9 PZE WGP,,10
24715 0 63400 4 25025 355
24716 0 63400 2 25026 356
24717 0 50000 1 34556 357
24720 0 73700 4 00000 358
24721 -0 63400 1 24722 359
24722 1 00000 4 24723 360
24723 0 75400 1 00000 361
24724 0 73400 2 00000 362
24725 -0 63400 4 25017 363
24726 0 07400 4 30155 364
24727 0 02000 0 25032 365
24730 0 02000 0 25030 366
24731 0 50000 0 32620 367
24732 0 60100 2 34163 368
24733 0 50000 0 32631 369
24734 0 60100 2 34101 370
24735 0 50000 0 32621 371
24736 0 60100 2 34245 372
24737 0 50000 1 36064 373
354*REGION TO EVALUATE FINITE DIFFERENCE TEMPERATURE EQUATIONS
355 AZT SXA AZTR,4
356 +1 SXA AZTR+1,2
357 +2 CLA FX+1,1
358 +3 PAC ,4
359 +4 SXD *+1,1
360 +5 TXI *+1,4,*0
361 +6 PAX ,1
362 +7 PAX ,2
363 +8 SXD AZT1,4
364 +9 TSX AVE,4
365 +10 TRA AZT3
366 +11 TRA AZT4
367 +12 CLA P+2
368 +13 STO AZ03,2
369 +14 CLA P+11
370 +15 STO AZ02,2
371 +16 CLA P+3
372 +17 STO AZ04,2
373 +18 CLA DEI Z,1
T6
MAXIMUM Z
READ IN NEXT PART
NO INPUT
NO. TIME POINTS
HEAT TRNS AND HBP ITERATION
PRINT HT TRNS
MOVE METAL TMS TO PERM STO
PRINT PREDICTED VALUES
I TURBO-PUMP VALUES
PRINT CORRECTED VALUES
BUMP PRINT COUNTER
COMPUTE METAL TEMPS FOR NWXT TIME
TEST FOR COOLDOWN REACHED
INLET CONDITIONS FOR TIME +1
TURBOPUMP PREDICTOR
PART FLAG
NEW CASE
MULTI-PART
ERROR
ERROR
INLET TEMP
WDOT
INLET PRESS
```

24741	0	13100	0	00000	375	+20	XCA		INITIAL Z IN AC
24742	0	60100	0	32616	376	AZT2	STO	P	Z
24743	0	50000	2	35637	377	+1	CLA	AZ01+1,2	
24744	0	60100	0	32617	378	+2	STO	P+1	
24745	0	07400	4	31722	379	+3	TSX	AYR,4	
24746	0	02000	0	25032	380	+4	TRA	AZT3	
24747	0	56000	0	33746	381	+5	LDQ	TP+9	2M-1
24750	0	26000	0	32620	382	+6	FMP	P+2	T
24751	0	30000	0	32617	383	+7	FAD	P+1	METAL TEMP
24752	0	30000	0	32617	384	+8	FAD	P+1	
24753	0	24100	0	33745	385	+9	FDP	TP+8	
24754	0	13100	0	00000	386	+10	XCA		
24755	0	60100	2	34164	387	+11	STO	AZ03+1,2	T M+1,N
24756	0	60100	0	32620	388	+12	STO	P+2	
24757	0	30200	2	34163	389	+13	FSB	AZ03,2	
24760	0	24100	2	34163	390	+14	FDP	AZ03,2	
24761	0	13100	0	00000	391	+15	XCA		
24762	0	30000	0	33766	392	+16	FAD	TP+25	
24763	0	13100	0	00000	393	+17	XCA		
24764	0	26000	0	34002	394	+18	FMP	TP+37	
24765	0	60100	0	33772	395	+19	STO	TP+29	PRESSURE DROP TERM
24766	0	50000	0	32621	396	+20	CLA	P+3	
24767	0	30200	0	33772	397	+21	FSB	TP+29	
24770	0	60100	0	32621	398	+22	STO	P+3	PRESSURE
24771	0	60100	2	34246	399	+23	STO	AZ04+1,2	P M+1,N
24772	-0	12000	0	25032	400	+24	TMI	AZT3	
24773	0	50000	0	32623	401	+25	CLA	P+5	RHO M,N EQN HT13
24774	0	60100	2	34411	402	+26	STO	AZ07,2	
24775	0	30200	2	35720	403	+27	FSB	AZ06,2	RHO M,N-1
24776	0	13100	0	00000	404	+28	XCA		
24777	0	26000	0	34074	405	+29	FMP	TP+95	
25000	0	30000	0	32631	406	+30	FAD	P+11	
25001	0	30200	2	36003	407	+31	FSB	AZ08+1,2	
25002	0	30000	2	36002	408	+32	FAD	AZ08,2	
25003	-3	62716	1	25005	409	+33	TXL	**2,1,-AZMTG-1	*****
25004	0	50000	0	32631	410	+34	CLA	P+11	
25005	0	60100	2	34102	411	+35	STO	AZ02+1,2	WOOD M+1,N
25006	0	60100	0	32631	412	+36	STO	P+11	
25007	-0	12000	0	25030	413	+37	TMI	AZT4	HF
25010	0	50000	0	32622	414	+38	CLA	P+4	
25011	0	60100	2	34327	415	+39	STO	AZ05,2	
25012	0	50000	0	33731	416	+40	CLA	WPR+7	
25013	0	60100	2	34473	417	+41	STO	AZ09,2	
25014	0	50000	0	32616	418	+42	CLA	P	
25015	0	30000	1	36064	419	+43	FAD	DELZ,1	
25016	1	77777	2	25017	420	+44	TXI	**1,2,-1	
25017	3	00000	2	24742	421	AZT1	TXH	AZT2,2,**0	
25020	0	07400	4	30201	422	+1	TSX	AYEA,4	
25021	0	02000	0	25032	423	+2	TRA	AZT3	ERROR
25022	0	02000	0	25030	424	+3	TRA	AZT4	ERROR
25023	0	50000	0	33731	425	+4	CLA	WPR+7	
25024	0	60100	2	34473	426	+5	STO	AZ09,2	
25025	0	77400	4	00000	427	AZTR	AXT	**0,4	
25026	0	77400	4	00000	428	+1	AXT	**0,2	
25027	0	02000	4	00003	429	+2	TRA	3,4	
25030	0	52200	0	25025	430	AZT4	XEC	AZTR	
25031	1	00002	4	25026	431	+1	TXI	AZTR+1,4,2	ERROR EXIT FOR NEGATIVE FLOW RATE
25032	0	52200	0	25025	432	AZT3	XEC	AZTR	ERROR EXIT
25033	1	00001	4	25026	433	+1	TXI	AZTR+1,4,1	

435*REGION TO COMPUTE CONSTANTS FOR ONE TIME STEP									
25034	0	50000	0	34072	436	AZA	CLA	TP+93	
25035	0	60100	0	32630	437	+1	STO	P+10	NEW TIME
25036	0	52000	0	36111	438	+2	ZET	DPD	
25037	0	02000	0	25046	439	+3	TRA	AZAI+1	
25040	0	63400	4	25045	440	+4	SXA	AZAI,4	NEW POMIN
25041	0	50000	0	32630	441	+5	CLA	P+10	
25042	0	07400	4	42437	442	+6	TSX	LINT,4	
25043	0	00000	0	33441	443	+7	PZE	WPD	
25044	0	60100	0	32640	444	+8	STO	P+18	
25045	0	77400	4	00000	445	AZAI	AXT	**0,4	
25046	0	50000	0	34064	446	+1	CLA	TP+87	P1
25047	0	60100	0	32652	447	+2	STO	P+28	
25050	0	50000	0	34065	448	+3	CLA	TP+88	T1
25051	0	60100	0	32653	449	+4	STO	P+29	
25052	0	50000	0	32674	450	+5	CLA	P+46	P2
25053	0	60100	0	32654	451	+6	STO	P+30	
25054	0	50000	0	32675	452	+7	CLA	P+47	T2
25055	0	60100	0	32655	453	+8	STO	P+31	
25056	0	50000	0	34073	454	+9	CLA	TP+94	GP
25057	0	60100	0	32657	455	+10	STO	P+33	
25060	0	50000	0	32666	456	+11	CLA	P+40	N
25061	0	60100	0	32665	457	+12	STO	P+39	
25062	0	50000	0	34017	458	+13	CLA	TP+50	RHO 1
25063	0	60100	0	34060	459	+14	STO	TP+83	
25064	0	50000	0	34056	460	+15	CLA	TP+81	DELH (BTU/LB)
25065	0	60100	0	34066	461	+16	STO	TP+89	
25066	0	50000	0	32677	462	+17	CLA	P+49	WOODP
25067	0	60100	0	32643	463	+18	STO	P+21	
25070	0	50000	0	34046	464	+19	CLA	TP+73	WOODC
25071	0	60100	0	32644	465	+20	STO	P+22	
25072	0	50000	0	32636	466	+21	CLA	P+16	HSV
25073	0	60100	0	32635	467	+22	STO	P+15	
25074	0	02000	4	00001	468	+23	TRA	1,4	

470*REGION TO OBTAIN CONSTANTS FOR TIME I+1									
25075	0	50000	0	32630	471	AZAA	CLA	P+10	
25076	0	30000	0	32637	472	+1	FAD	P+17	
25077	0	60100	0	34072	473	+2	STO	TP+93	NEW TIME
25100	0	63400	4	25122	474	+3	SXA	AZAA,4	
25101	0	52000	0	36107	475	+4	ZET	DPI	
25102	0	02000	0	25114	476	+5	TRA	AZAA1	
25103	0	50000	0	34072	477	+6	CLA	TP+93	
25104	0	07400	4	42437	478	+7	TSX	LINT,4	
25105	0	00000	0	33216	479	+8	PZE	WPI	
25106	0	60100	0	34064	480	+9	AXT	**0,4	

25110	0	07400	4	42437	482	+11	TSX	LINT,4	
25111	0	00000	0	32773	483	+12	PZE	MTI	
25112	0	60100	0	34065	484	+13	STO	TP+88	T1
25113	0	07400	4	30453	485	+14	TSX	AYII,4	
25114	0	52000	0	36130	486	AZAA1	ZET	OGP	
25115	0	03000	0	25122	487	+1	TRA	AZAA8	
25116	0	50000	0	34072	488	+2	CLA	TP+93	
25117	0	07400	4	42437	489	+3	TSX	LINT,4	
25120	0	00000	0	33644	490	+4	PZE	WGP	GP
25121	0	60100	0	34073	491	+5	STO	TP+94	
25122	0	77400	4	00000	492	AZAA8	AXT	000,4	
25123	0	02900	4	00001	493	+1	TRA	1,4	

495*REGION TO FIND VALUES AT ZERO TIME

25124	0	63400	4	25174	494	AZAB	SXA	AZABR,4	
25125	0	50200	0	36100	497	+1	CLS	DELT	
25126	0	60200	0	32637	498	+2	SLW	P+17	
25127	0	60100	0	32630	499	+3	STO	P+10	
25130	0	07400	4	25073	500	+4	TSX	AZAA,4	READ CURVES
25131	0	50000	0	36107	501	+5	CLA	DPI	
25132	0	10000	0	25137	502	+6	TZE	AZAB1	P1
25133	0	60100	0	34064	503	+7	STO	TP+87	
25134	0	50000	0	36110	504	+8	CLA	DTI	T1
25135	0	60100	0	34065	505	+9	STO	TP+88	
25136	0	07400	4	30453	506	+10	TSX	AYII,4	
25137	0	50000	0	36130	507	AZAB1	CLA	OGP	
25140	0	10000	0	25142	508	+1	TZE	0+2	GP
25141	0	60100	0	34073	509	+2	STO	TP+94	P1
25142	0	50000	0	34064	510	+3	CLA	TP+87	
25143	0	60100	0	32674	511	+4	STO	P+46	
25144	0	60100	0	32652	512	+5	STO	P+28	
25145	0	50000	0	34065	513	+6	CLA	TP+88	
25146	0	60100	0	32675	514	+7	STO	P+47	
25147	0	60100	0	32653	515	+8	STO	P+29	
25150	0	50000	0	36111	516	+9	CLA	OPD	
25151	0	60100	0	32640	517	+10	STO	P+18	
25152	0	50000	0	36143	518	+11	CLA	DNI	
25153	0	60100	0	32666	519	+12	STO	P+40	
25154	0	50000	0	36114	520	+13	CLA	DWP	
25155	0	60100	0	32677	521	+14	STO	P+49	
25156	0	50000	0	36115	522	+15	CLA	DWC	
25157	0	60100	0	34066	523	+16	STO	TP+73	
25160	0	50000	0	36116	524	+17	CLA	DWH	
25161	0	60100	0	34045	525	+18	STO	TP+72	
25162	0	60000	0	34042	526	+19	STZ	TP+69	
25163	0	60000	0	34043	527	+20	STZ	TP+70	
25164	0	60000	0	34052	528	+21	STZ	TP+77	
25165	0	60000	0	32662	529	+22	STZ	P+36	
25166	0	60000	0	34053	530	+23	STZ	TP+78	
25167	0	60000	0	32664	531	+24	STZ	P+38	
25170	0	60000	0	32700	532	+25	STZ	P+50	
25171	0	60000	0	32670	533	+26	STZ	P+42	
25172	0	60000	0	32672	534	+27	STZ	P+44	

25174	0	77400	4	00000	536	AZABR	AXT	000,4	
25175	0	02000	4	00001	537	+1	TRA	1,4	
25176	2	22124	4	06321	538	AZAB2	BCI	3,BAD TANK PRS, TMP	

540*REGION TO INITIALIZE PROGRAM

25201	0	63400	4	25260	541	AZAC	SXA	AZACR,4	
25202	0	63400	1	25261	542	+1	SXA	AZACR+1,1	
25203	0	50000	0	36106	543	+2	CLA	DDIL	DILUENT REMOVAL FLAG
25204	-0	30000	0	40306	544	+3	UFA	FIX	
25205	0	73700	4	00000	545	+4	PAC	1,4	
25206	3	00000	4	25210	546	+5	TXH	0+2,4,0	
25207	-1	25263	0	25617	547	AZAC5	STR	AZFF,1,AZAC4	
25210	-3	77775	4	25213	548	+1	TXL	AZAC1,4,-3	
25211	-0	62500	4	32715	549	+2	STL	X-1,4	
25212	0	02000	0	25222	550	+3	TRA	AZAC3	
25213	-0	77400	1	15061	551	AZAC1	AXC	AZMTG,1	
25214	1	00003	4	25215	552	+1	TXI	0+1,4,3	
25215	-3	00000	4	25221	553	AZAC6	TXL	AZAC2,4,0	
25216	1	76003	1	25217	554	+1	TXI	0+1,1,-AZMTS	
25217	-3	00000	1	25207	555	AZAC7	TXL	AZAC5,1,000	
25220	1	00001	4	25215	556	+1	TXI	AZAC6,4,1	
25221	-0	62500	1	34557	557	AZAC2	STL	FX+2,1	IN CORRECT PART
25222	0	07400	4	25124	558	AZAC3	TSX	AZAB,4	
25223	0	07400	4	27657	559	+1	TSX	AYC,4	
25224	0	07400	4	44724	560	+2	TSX	HBZ,4	
25225	0	50000	0	36077	561	+3	CLA	DTMI	
25226	0	10000	0	25231	562	+4	TZE	0+3	
25227	0	50000	0	36103	563	+5	CLA	DTHO	
25230	0	60100	0	32633	564	+6	STO	P+13	T6
25231	0	52000	0	36123	565	+7	ZET	DNEFF	
25232	0	07400	4	26247	566	+8	TSX	AZNI,4	
25233	0	50000	0	36201	567	+9	CLA	DP11	
25234	0	60100	0	32742	568	+10	STO	X+20	
25235	0	50000	0	36127	569	+11	CLA	DS+T	
25236	-0	30000	0	40306	570	+12	UFA	FIX	
25237	0	32200	0	40306	571	+13	ERA	FIX	
25240	0	13100	0	00000	572	+14	XCA	0	
25241	0	75400	0	00000	573	+15	PXA	0	
25242	0	22100	0	40212	574	+16	DVP	FXIE3	
25243	0	60100	0	47714	575	+17	STO	HB6	PRINT HOT BLEED PORT
25244	-0	60000	0	44475	576	+18	STO	AZNS	PRINT NOZZLE TUBES
25245	0	50000	0	36076	577	+19	CLA	DPRI	
25246	-0	30000	0	40306	578	+20	UFA	FIX	
25247	0	32200	0	40306	579	+21	ERA	FIX	
25250	0	13100	0	00000	580	+22	XCA	0	
25251	0	75400	0	00000	581	+23	PXA	0	
25252	0	22100	0	40212	582	+24	DVP	FXIE3	
25253	-0	60000	0	32725	583	+25	STO	X+7	SKIP PRINT FLAG
25254	0	62100	0	32726	584	+26	STY	X+8	
25255	0	60000	0	32727	585	+27	STZ	X+9	
25256	-0	62500	0	32737	586	+28	STL	X+17	
25257	0	07401	4	32541	587	+29	TSX	PL,4,1	RESTORE PAGE
25260	0	77400	4	00000	588	AZACR	AXT	000,4	
25261	0	77400	1	00000	589	+1	AXT	000,1	

25262 0 02000 4 00001 590 +2 TRA 1,4
25263 -0 54660 2 43143 591 AZAC4 BCI 3,NO DILUENT REMOVED

593*REGION TO COMPUTE MAIN ENGINE HEAT TRANSFER
25264 0 63400 4 25331 594 AZB SXA AZBR,4
25267 0 63400 1 25332 595 +1 SXA AZBR+1,1
25270 0 60000 0 32722 596 +2 STZ X+4
25271 0 60000 0 32744 597 +3 STZ X+22
25272 -0 52000 0 32716 598 +4 NZT X
25273 0 02000 0 25274 599 +5 TRA **3
25274 0 07400 4 27353 600 +6 TSX AZV,4 DILUENT AT PUMP DISCHARGE
25275 0 02000 0 25337 601 +7 TRA AZB12 MOUTR -
25276 0 07400 4 27367 602 +8 TSX AZZ,4 P3 AND T3
25277 -0 52000 0 32717 603 +9 NZT X+1
25300 0 02000 0 25303 604 +10 TRA **3
25301 0 07400 4 27353 605 +11 TSX AZV,4 DILUENT AT TUBE INLET
25302 0 02000 0 25337 606 +12 TRA AZB12
25303 -0 52000 0 36123 607 +13 NZT DNZFF
25304 0 02000 0 25310 608 +14 TRA AZB5
25305 0 07400 4 42636 609 +15 TSX AZN,4
25306 0 02000 0 25343 610 +16 TRA AZB11
25307 0 02000 0 25341 611 +17 TRA AZB9 NEG PRESS
25310 -0 77400 1 15061 612 AZB5 AXC AZMTG,1
25311 -0 52000 1 34557 613 AZB2 NZT FX+2,1
25312 0 02000 0 25315 614 +1 TRA **3
25313 0 07400 4 27353 615 +2 TSX AZV,4
25314 0 02000 0 25337 616 +3 TRA AZB12
25315 0 07400 4 24715 617 +4 TSX AZT,4 HEAT TRANS
25316 0 02000 0 25337 618 +5 TRA AZB12
25317 0 02000 0 25334 619 +6 TRA AZB8
25320 1 76003 1 25321 620 +7 TXI **1,1,-AZMTS
25321 3 00000 1 25311 621 AZB3 TXH AZB2,1,**0
25322 0 50000 0 32620 622 +1 CLA P+2 T
25323 0 60100 0 32633 623 +2 STO P+13
25324 0 50000 0 32621 624 +3 CLA P+3 P6
25325 0 60100 0 32656 625 +4 STO P+32 MIN P0
25326 0 56000 0 32640 626 +5 LOQ P+18
25327 0 04000 0 25331 627 +6 TLQ **2 P6 TOO LOW
25330 -0 62500 0 32722 628 +7 STL X+4
25331 0 77400 4 00000 629 AZBR AXT **0,4
25332 0 77400 1 00000 630 +1 AXT **0,1
25333 0 02000 4 00003 631 +2 TRA 3,4
25334 0 50000 0 32621 632 AZB8 CLA P+3
25335 -0 12000 0 25341 633 +1 TMI AZB9
25336 -1 25345 0 25417 634 +2 STR AZFF,,AZB7
25337 0 52200 0 25331 635 AZB12 XEC AZBR
25340 1 00002 4 25332 636 +1 TXI AZBR+1,4,2
25341 0 52200 0 25331 637 AZB9 XEC AZBR
25342 1 00001 4 25332 638 +1 TXI AZBR+1,4,1 NEG PRESSURE
25343 -1 43573 0 25421 639 AZB11 STR AZF,,BUG1
25344 0 02000 0 25310 640 +1 TRA AZB5
25345 3 02521 6 36063 641 AZB7 BCI 3,HEAT TRANSFER ERROR
25346 -0 54660 2 43143 642 AZB7 BCI 3,NO DILUENT REMOVED

644*REGION TO COMPUTE SOME CONSTANTS
25353 0 63400 4 25377 645 AZC SXA AZCR,4
25354 0 50000 0 32616 646 +1 CLA P Z
25355 0 07400 4 42437 647 +2 TSX LINT,4
25356 0 00000 1 34567 648 +3 PZE WAF,1
25357 0 60100 0 33757 649 +4 STO TP+18 AF
25360 0 50000 0 32616 650 +5 CLA P
25361 0 07400 4 42437 651 +6 TSX LINT,4
25362 0 00000 1 34625 652 +7 PZE WFP,1
25363 0 60100 0 33760 653 +8 STO TP+19 FP
654*PIPE OPTION BRANCHES OUT HERE TO AZC1
25364 0 52000 1 36071 655 +9 ZET DPX,1 NOT 0=PIPE OPTION
25365 0 02000 0 25401 656 +10 TRA AZC2
25366 0 50000 0 40213 657 +11 CLA FL1
25367 0 30200 1 36067 658 +12 FSB DVF,1
25370 0 24100 1 36067 659 +13 FDP DVF,1
25371 0 26000 1 36064 660 +14 FMP DELZ,1
25372 0 24100 1 35625 661 +15 FDP TP+11,1
25373 0 26000 0 33757 662 +16 FMP TP+18
25374 0 60100 0 33765 663 AZC1 STO TP+24
25375 0 24100 0 32631 664 +1 FDP P+11
25376 -0 60000 0 33771 665 +2 STQ TP+28
25377 0 77400 4 00000 666 AZCR AXT **0,4
25400 0 02000 4 00001 667 +1 TRA 1,4
25401 0 50000 0 33757 668 AZC2 CLA TP+18 AF -- PIPE OPTION
25402 0 24100 0 40275 669 +1 FDP PI
25403 0 26000 0 40216 670 +2 FMP FL4
25404 0 07400 4 24364 671 +3 TSX SQRT,4
25405 0 07400 4 42602 672 +4 TSX ERROR,4
25406 0 60100 0 33735 673 +5 STO TP
25407 0 30200 1 36071 674 +6 FSB DPX,1 DI
25410 0 24100 1 35625 675 +7 FDP TP+11,1 DELT
25411 0 26000 1 36071 676 +8 FMP DPX,1
25412 0 13100 0 00000 677 +9 XCA PI
25413 0 26000 0 40275 678 +10 FMP
25414 0 13100 0 00000 679 +11 XCA
25415 0 26000 1 36064 680 +12 FMP DELZ,1
25416 0 02000 0 25374 681 +13 TRA AZC1

683*REGION TO PRINT ERROR MESSAGES
25417 -0 50000 0 25437 684 AZFF CAL AZF2 PRINT AND FLUSH
25420 0 02000 0 25422 685 +1 TRA **2

687*PRINT MESSAGE AND RETURN
25421 -0 50000 0 00000 688 AZF CAL 0 PRINT AND RETURN
25422 0 60000 0 25432 689 +1 STZ AZF1+1
25423 0 62100 0 25436 690 AZF3 STA AZFR+1
25424 0 63400 4 25435 691 +1 SXA AZFR,4
25425 -0 50060 0 00046 692 +2 CAL* K1CSTR

25430	0	07400	4	00052	495	+5	TSX	DOU7,4
25431	3	04000	0	00000	496	AZF1	PTM	000,3072
25432	0	00000	0	00000	497	+1	PZE	000
25433	-1	00012	0	00012	498	+2	FVE	10,,10
25434	0	07401	4	32941	499	+3	TSX	PL,4,1
25435	0	77400	4	00000	700	AZFR	AXT	000,4
25436	0	02000	0	00000	701	+1	TRA	000
25437	0	00000	0	42602	702	AZF2	PZE	ERROR

25440	-0	50000	0	25444	704	PRINT TIME WITH MESSAGE		
25441	0	40200	0	25432	705	AZFT	CAL	AZFT1
25442	-0	50000	0	00000	706	+1	SLW	AZF1+1
25443	0	02000	0	25423	707	+2	CAL	0
25444	-2	13702	0	32630	708	+3	TRA	AZF3
					709	AZFT1	SIX	P+10,,6082

25445	0	63400	4	25560	711	REGION TO COMPUTE CONSTANTS FOR ONE POSITION STEP		
25446	0	50000	2	34101	712	AZG	SXA	AZGR,4
25447	0	30000	2	34102	713	+1	CLA	AZ02,2
25450	C	24100	0	40214	714	+2	FAD	AZ02+1,2
25451	-0	60000	0	32631	715	+3	FDP	FL2
25452	0	07400	4	25353	716	+4	STQ	P+11
25453	0	50000	2	34163	717	+5	TSX	AZC,4
25454	0	30000	2	34164	718	+6	CLA	AZ03,2
25455	C	24100	0	40214	719	+7	FAD	AZ03+1,2
25456	-0	60000	0	32620	720	+8	FDP	FL2
25457	0	50000	2	34245	721	+9	STQ	P+2
25460	0	30000	2	34246	722	+10	CLA	AZ04,2
25461	0	24100	0	40214	723	+11	FAD	AZ04+1,2
25462	-0	60000	0	32621	724	+12	FDP	FL2
25463	0	50000	2	34473	725	+13	STQ	P+3
25464	0	30000	2	34474	726	+14	CLA	AZ09,2
25465	0	24100	0	40214	727	+15	FAD	AZ09+1,2
25466	-0	60000	0	33731	728	+16	FDP	FL2
25467	0	50000	2	35637	729	+17	STQ	WPR+7
25470	0	07400	4	42437	730	+18	CLA	AZ01+1,2
25471	C	00000	1	35367	731	+19	TSX	LINT,4
25472	0	13100	0	00000	732	+20	PZE	WCR,1
25473	0	26000	1	36070	733	+21	XCA	
25474	0	60100	0	33776	734	+22	FMP	DRHOR,1
25475	0	50000	2	35637	735	+23	STQ	TP+33
25476	0	07400	4	42437	736	+24	CLA	AZ01+1,2
25477	0	00000	1	35144	737	+25	TSX	LINT,4
25500	0	60100	0	33761	738	+26	PZE	WK,1
25501	0	50000	0	33736	739	+27	STQ	TP+20
25502	0	07400	4	42437	740	+28	CLA	TP+1
25503	0	00000	1	34721	741	+29	TSX	LINT,4
25504	0	60100	0	34075	742	+30	PZE	WHT,1
25505	0	50000	0	32616	743	+31	STQ	TP+96
25506	0	07400	4	42437	744	+32	CLA	P
25507	C	00000	1	34663	745	+33	TSX	LINT,4
25508	0	13100	0	00000	746	+34	PZE	WH,1
					747	+35		

LSUBP
METAL TEMP

RHO SUB R * C SUB R

K

Z, IN

25511	C	26000	0	34075	748	+36	FMP	TP+96	FRACTION OF HEAT GEN COEFF
25512	0	60100	0	33777	749	+37	STQ	TP+34	H
25513	0	50000	2	34327	750	+38	CLA	AZ05,2	
25514	0	60100	0	32622	751	+39	STQ	P+4	
25515	0	07400	4	31545	752	+40	TSX	AYN,4	
25516	0	50000	0	33776	753	+41	CLA	TP+33	RHO C R
25517	0	24100	0	33731	754	+42	FDP	WPR+7	C P
25520	0	26000	0	33771	755	+43	FMP	TP+28	
25521	0	60100	0	32624	756	+44	STQ	P+6	
25522	0	34000	0	32627	757	+45	CAS	P+9	M
25523	0	02000	0	25526	758	+46	TRA	*+3	
25524	0	02000	0	25526	759	+47	TRA	*+2	
25525	0	02000	0	25562	760	+48	TRA	AZG1	
25526	0	50000	0	33761	761	+49	CLA	TP+20	K
25527	0	24100	0	33776	762	+50	FDP	TP+33	
25530	0	26000	1	35625	763	+51	FMP	PT+11,1	DELT
25531	0	24100	1	36064	764	+52	FDP	DELZ,1	
25532	0	13100	0	00000	765	+53	XCA		
25533	0	24100	1	36064	766	+54	FDP	DELZ,1	
25534	0	13100	0	00000	767	+55	XCA		
25535	0	24100	0	40214	768	+56	FDP	FL2	
25536	-0	60000	0	32625	769	+57	STQ	P+7	S/2
25537	0	50000	0	33777	770	+58	CLA	TP+34	H
25540	0	24100	0	33776	771	+59	FDP	TP+33	
25541	0	26000	1	35625	772	+60	FMP	PT+11,1	
25542	0	60100	0	32626	773	+61	STQ	P+8	
25543	0	50200	0	33746	774	+62	CLS	TP+9	
25544	0	24100	0	33745	775	+63	FDP	TP+8	
25545	0	13100	0	00000	776	+64	XCA		
25546	0	30000	0	40213	777	+65	FAD	FL1	
25547	0	24100	0	32624	778	+66	FDP	P+6	
25550	-0	60000	0	33747	779	+67	STQ	TP+10	
25551	0	50200	0	40214	780	+68	CLS	FL2	
25552	0	24100	0	33745	781	+69	FDP	TP+8	
25553	0	13100	0	00000	782	+70	XCA		
25554	0	24100	0	32624	783	+71	FDP	P+6	
25555	0	13100	0	00000	784	+72	XCA		
25556	0	30000	0	40213	785	+73	FAD	FL1	
25557	0	60100	0	33744	786	+74	STQ	TP+7	
25560	0	77400	4	00000	787	AZGR	AXT	000,4	
25561	0	02000	4	00002	788	+1	TRA	2,4	
25562	0	52200	0	25560	789	AZG1	XEC	AZGR	
25563	0	02000	4	00001	790	+1	TRA	1,4	

25564	0	63400	4	25625	792	REGION TO COMPUTE PARA HYDROGEN PROPERTIES, TEMP IN AC, PRESS IN MQ		
25565	-0	12000	4	00001	793	AZH	SXA	AZHR,4
25566	0	16200	0	25571	794	+1	TMI	1,4
25567	0	52200	0	25625	795	+2	TQP	AZH2
25570	0	02000	4	00001	796	AZH3	XEC	AZHR
					797	+1	TRA	1,4

25574	0	02000	0	25602	801	+3	TRA	AZM4	
25575	0	13100	0	00000	802	+4	XCA		
25576	0	34000	0	33722	803	+5	CAS	WPR	
25577	0	02000	0	25601	804	+6	TRA	*+2	
25600	0	02000	0	25625	805	+7	TRA	AZMR	
25601	0	13100	0	00000	806	+8	XCA		SAME PRESSURE
25602	0	77400	4	00012	807		AZM4	AXT	10.4
25603	0	60000	0	33734	808	+1	STZ	WPR+10.4	
25604	2	00001	4	25603	809	+2	TIX	*-1.4,1	
25605	0	60100	0	33727	810	+3	STO	WPR+5	TEMP
25606	-0	60000	0	33722	811	+4	STQ	WPR	PRESS
25607	0	07400	4	32022	812	+5	TSX	PRP.4	
25610	0	02000	0	25567	813	+6	TRA	AZM3	
25611	0	56000	0	33723	814	+7	LDQ	WPR+1	SP VOL FT**3/LB
25612	0	26000	0	40245	815	+8	FMP	FLCUP	IN3/FT3
25613	0	60100	0	33723	816	+9	STO	WPR+1	IN**3/LB
25614	0	50000	0	25627	817	+10	CLA	AZM1	
25615	0	56000	0	33727	818	+11	LDQ	WPR+5	
25616	0	04000	0	25625	819	+12	TLQ	AZMR	
25617	0	50000	0	25630	820	+13	CLA	AZM1+1	
25620	0	04000	0	25622	821	+14	TLQ	*+2	
25621	0	02000	0	25625	822	+15	TRA	AZMR	
25622	0	26000	0	25631	823	+16	FMP	AZM1+2	
25623	0	30000	0	25632	824	+17	FAD	AZM1+3	
25624	0	60100	0	33731	825	+18	STO	WPR+7	
25625	0	77400	4	00000	826		AZMR	AXT	**0.4
25626	0	02000	4	00002	827	+1	TRA	2.4	
25627	2	10550	0	00000	828		AZM1		
25630	2	11404	0	00000	829	+1			
25631	1	71763	5	54427	830	+2			
25632	2	01755	3	41217	831	+3			

833*REGION TO ITERATE ON FLOW RATE FOR MULTIPLE PART CASE AT ONE TIME PT.

25633	0	63400	4	25705	834		AZ1	SXA	AZ1R.4	
25634	0	50000	0	40305	835	+1	CLA	BIG		
25635	0	60100	0	40471	836	+2	STO	NEWA9		
25636	0	60000	0	40472	837	+3	STZ	NEWA9+1		
25637	0	50000	0	32644	838	+4	CLA	P+22		
25640	0	60100	0	47403	839	+5	STO	PR+50		INITIAL WDOTC GUESS
25641	0	50000	0	36120	840	+6	CLA	DWRE		WDOTR CLOSURE
25642	0	07400	4	40407	841	+7	TSX	NEWA.4		
25643	0	47406	0	32643	842	+8	PZE	P+21,PR+53		
25644	0	00024	0	32631	843	+9	PZE	P+11,NHIT		
25645	0	02000	0	25723	844	+10	TRA	AZ13		NIT CONVERGED
25646	0	50000	0	47403	845	+11	CLA	PR+50		
25647	0	60100	0	32644	846	+12	STO	P+22		WDOTC= VALUE OBTAINED BY HOT BLEED P
25648	0	50000	0	32655	847	+13	CLA	P+31		
25651	0	60100	0	32620	848	+14	STO	P+2		T2
25652	0	50000	0	32654	849	+15	CLA	P+30		
25653	0	60100	0	32621	850	+16	STO	P+3		P2
25654	0	50000	0	32643	851	+17	CLA	P+21		
25655	0	60100	0	32631	852	+18	STO	P+11		WDOTR=WDOTP
25656	0	00000	0	32666	853					WEATNSR 2 TAIN

JOB 12013.

25/09/64

PAGE 15

25657	0	02000	0	25707	854	+20	TRA	AZ11		NEG FLOW
25660	0	02000	0	25715	855	+21	TRA	AZ12		NEG PRESS
25661	0	52000	0	32742	856	+22	ZET	X+20		
25662	0	02000	0	25732	857	+23	TRA	AZ14		P11, T11 GIVEN- SKIP HOT BLEED PORT
25663	0	07400	4	44757	858	+24	TSX	H8.4		HOT BLEED PORT PROGRAM
25664	0	02000	0	25732	859	+25	TRA	AZ14		WDOTC NEG, TREAT AS ZERO THIS PASS
25665	0	02000	0	25746	860	+26	TRA	AZ15		NEG PRESSURE, LOWER WDOTC
25666	0	07400	4	40477	861		AZ16	TRAP.4		CLOSE
25667	0	50000	0	32644	862	+1	CLA	P+22		
25670	0	56000	0	47403	863	+2	LDQ	PR+50		
25671	-0	60000	0	32644	864	+3	STQ	P+22		
25672	0	30200	0	47403	865	+4	FSB	PR+50		
25673	0	24100	0	47403	866	+5	FDP	PR+50		
25674	0	76000	0	00012	867	+6	DCT			
25675	0	07400	4	42602	868	+7	TSX	ERROR.4		WDOTC IN HBP=0
25676	0	13100	0	00000	869	+8	XCA			
25677	-0	34000	0	36117	870	+9	LAS	DWCE		
25700	0	02000	0	40427	871	+10	TRA	NEWA2+1		NOT CONVERGED TRY AGAIN WITH SAME WP
25701	0	02000	0	25702	872	+11	TRA	*+1		
25702	0	52200	0	40427	873		AZ17	XEC	NEWA2+1	
25703	1	77754	4	25704	874	+1	TXI	*+1.4,-NHIT		
25704	0	63600	4	32732	875	+2	SCA	X+12.4		NO. ITERATIONS
25705	0	77400	4	00000	876		AZ1R	AXT	**0.4	
25706	0	02000	4	00001	877	+1	TRA	1.4		EXIT
25707	-0	52000	0	32744	878					878*NEGATIVE FLOW RATE- WDOTP TOO SMALL
25710	0	02000	0	40466	879		AZ11	NZT	X+22	
25711	0	50000	0	32643	880	+1	TRA	BDNA		
25712	0	30200	0	32644	881	+2	CLA	P+21		IF WDOTC HAS BEEN REMOVED LOWER
25713	0	60100	0	32643	882	+3	FSB	P+22		MINIMUM BY WDOTC
25714	0	02000	0	40466	883	+4	STO	P+21		
25715	-0	52000	0	32744	884	+5	TRA	BDNA		885*NEGATIVE PRESSURE- WDOTP TOO BIG
25716	0	02000	0	40463	886		AZ12	NZT	X+22	
25717	0	50000	0	32643	887	+1	TRA	BDXA		
25720	0	30000	0	32644	888	+2	CLA	P+21		IF DILUENT HAS BEEN REMOVED RAISE
25721	0	60100	0	32643	889	+3	FAD	P+22		NEW MAXIMUM BY WDOTC
25722	0	02000	0	40463	890	+4	STO	P+21		
25723	-1	25727	0	25440	891	+5	TRA	BDXA		
25724	0	77400	4	00024	892					892*NOT CONVERGED
25725	0	63400	4	32732	893		AZ13	STR	AZFT, AZ101	
25726	0	02000	0	25705	894	+1	AXT	NHIT.4		
25727	-2	65173	6	06623	895	+2	SXA	X+12.4		
25732	0	50000	0	32620	896	+3	TRA	AZ1R		
25733	0	07400	4	24364	897		AZ101	BCI	3,WR, WC NOT CLOSED	
25734	0	07400	4	42602	898					898*P11, T11 GIVEN- WDOTC =0, HOT BLEED PORT CLOSED
25735	0	60100	0	12512	899		AZ14	CLA	P+2	
25736	0	56000	0	36122	900	+1	TSX	SQRT.4		
25737	0	26000	0	32621	901	+2	TSX	ERROR.4		ROOT T6
25740	0	24100	0	12512	902	+3	STO	COMMON		
25741	0	76000	0	40241	903	+4	LDQ	DASTR		
					904	+5	FMP	P+3		P6
					905	+6	FDP	COMMON		
					906	+7	FMP	FL139		

25743 0 60100 0 34007 908 +9 STO TP+42 WOOTN CHOKE
25744 0 07400 4 40477 909 +10 TSX RAPA+4
25745 0 02000 0 25702 910 +11 TRA AZI7
911*NEG PRESSURE IN HOT BLEED PORT, LOWER WOOTC NEW WOOTC= .5 WOOTC
25746 0 50000 0 32644 912 AZI5 CLA P+22
25747 0 24100 0 40214 913 +1 FDP FL2
25750 -0 60000 0 32644 914 +2 STO P+22
25751 0 02000 0 40427 915 +3 TRA NEWA2+1

917*REGION TO COMPUTE MAIN ENGINE METAL TEMPS
25752 0 63400 4 26057 918 AZJ SXA AZJR+4
25753 0 63400 1 26060 919 +1 SXA AZJR+1,1
25754 0 63400 2 26061 920 +2 SXA AZJR+2,2
25755 0 63400 3 26062 921 +3 SXA AZJR+3,3
25756 0 63400 5 26063 922 +4 SXA AZJR+4,5
25757 -0 77400 1 15061 923 +5 AXS AZMTG,1
25760 0 60000 1 34561 924 AZJ8 STZ FX+4,1
25761 0 50000 1 34562 925 +1 CLA FX+5,1
25762 0 73400 5 00000 926 +2 PAX ,5
25763 0 50000 0 32630 927 +3 CLA P+10
25764 0 60100 0 33736 928 +4 STO TP+1
25765 0 77400 3 00000 929 AZJ7 AXT 0,3
25766 0 75400 1 00000 930 +1 PAX ,1
25767 0 73400 2 00000 931 +2 PAX ,2
25770 0 50000 1 34556 932 +3 CLA FX+1,1
25771 0 73700 4 00000 933 +4 PAC ,4
25772 -0 63400 4 26030 934 +5 SKD AZJ4,4
25773 -0 63400 4 26044 935 +6 SKD AZJ5,4
25774 0 50000 1 36064 936 +7 CLA DELZ,1
25775 0 24100 0 40214 937 +8 FDP FL2
25776 0 13100 0 00000 938 +9 XCA
25777 0 60100 0 32616 939 AZJ3 STO P
26000 0 07400 4 25445 940 +1 TSX AZG,4
26001 0 02000 0 26065 941 +2 TRA AZJ2
26002 0 50000 2 35640 942 +3 CLA AZO1+2,2
26003 0 30000 2 35636 943 +4 FAD AZO1,2
26004 0 30200 2 35637 944 +5 FSB AZO1+1,2
26005 0 30200 2 35637 945 +6 FSB AZO1+1,2
26006 0 13100 0 00000 946 +7 XCA
26007 0 26000 0 32625 947 +8 FMP P+7
26010 0 60100 0 12512 948 +9 STO COMMON
26011 0 56000 2 35637 949 +10 LDQ AZO1+1,2
26012 0 26000 0 33744 950 +11 FMP TP+7
26013 0 60100 0 12513 951 +12 STO COMMON+1
26014 0 56000 2 34163 952 +13 LDQ AZO3,2
26015 0 26000 0 13747 953 +14 FMP TP+10
26016 0 30000 0 12512 954 +15 FAD COMMON
26017 0 30000 0 12513 955 +16 FAD COMMON+1
26020 0 30000 0 32626 956 +17 FAD P+8
26021 0 56000 0 36105 957 +18 LDQ DTMAX
26022 0 04000 0 26100 958 +19 TLQ AZJ12
26023 0 60100 3 26106 959 AZJ13 STO AZJ1,3
26024 0 60100 3 26106 960 AZJ1 STO AZJ1,3

26025 0 30000 1 36064 961 +2 FAD DELZ,1
26026 1 77777 2 26027 962 +3 TXI **1,2,-1
26027 1 77777 3 26030 963 +4 TXI **1,3,-1
26030 3 00000 3 25777 964 AZJ4 TXH AZJ3,3,**0
26031 0 77400 3 00000 965 +1 AXT 0,3
26032 0 75400 1 00000 966 +2 PAX ,1
26033 0 73400 2 00000 967 +3 PAX ,2
26034 0 50000 0 26106 968 +4 CLA AZJ1
26035 0 36100 0 40301 969 +5 ACL 188
26036 0 30200 0 26107 970 +6 FSB AZJ1+1
26037 0 60100 2 35636 971 +7 STO AZO1,2
26040 0 50000 3 26106 972 AZJ6 CLA AZJ1,3
26041 0 60100 2 35637 973 +1 STO AZO1+1,2
26042 1 77777 2 26043 974 +2 TXI **1,2,-1
26043 1 77777 3 26044 975 +3 TXI **1,3,-1
26044 3 00000 3 26040 976 AZJ5 TXH AZJ6,3,**0
26045 0 50000 2 35636 977 +1 CLA AZO1,2
26046 0 30000 2 35636 978 +2 FAD AZO1,2
26047 0 30200 2 35635 979 +3 FSB AZO1-1,2
26050 0 60100 2 35637 980 +4 STO AZO1+1,2
26051 0 50000 0 33736 981 +5 CLA TP+1
26052 0 30000 1 35625 982 +6 FAD PT+11,1
26053 0 60100 0 33736 983 +7 STO TP+1
26054 2 00001 5 25765 984 +8 TXI AZJ7,5,1
26055 1 76003 1 26056 985 +9 TXI **1,1,-AZHTS
26056 3 00000 1 25760 986 AZJ9 TXH AZJ8,1,**0
26057 0 77400 4 00000 987 AZJR AXT **0,4
26060 0 77400 1 00000 988 +1 AXT **0,1
26061 0 77400 2 00000 989 +2 AXT **0,2
26062 0 77400 3 00000 990 +3 AXT **0,3
26063 0 77400 5 00000 991 +4 AXT **0,5
26064 0 02000 4 00001 992 +5 TRA 1,4
26065 0 50000 1 35625 993 AZJ2 CLA PT+11,1
26066 0 24100 0 40214 994 +1 FDP FL2
26067 -0 60000 1 35625 995 +2 STO PT+11,1
26070 0 50000 0 36102 996 +3 CLA DMDT
26071 0 04000 0 26102 997 +4 TLQ AZJ10
26072 0 75400 5 00000 998 +5 PAX ,5
26073 0 56000 1 34562 999 +6 LDQ FX+5,1
26074 0 76300 0 00001 1000 +7 LLS 1
26075 0 73400 5 00000 1001 +8 PAX ,5
26076 -0 60000 1 34562 1002 +9 STO FX+5,1
26077 0 02000 0 25765 1003 +10 TRA AZJ7
26100 -0 62500 1 34561 1004 AZJ12 STL FX+4,1
26101 0 02000 0 26023 1005 +1 TRA AZJ13
26102 -1 26103 0 25417 1006 AZJ10 STR AZFF,,AZJ11
26103 2 42543 4 32160 1007 AZJ11 BCI 3,DELTA T TOO SMALL
1008 AZJ1 BSS NZMAX,F

26170 0 63400 4 26220 1010*REGION TO MOVE METAL TEMPS FROM TEMPORARY TO PERMANENT STORAGE
26171 0 63400 2 26221 1011 AZK SXA AZKR,4
26172 0 77400 4 42717 1012 +1 SXA AZKR+1,2
1013 +2 AXT AZMTB-AZMT 4 REFERENCE TO PART STORAGE

26173	0	63400	4	26215	1014	AZK3	SXA	AZK1,4	
26174	0	50000	4	34556	1015	+1	CLA	FX+1,4	NO. DELZ POINTS
26175	0	73400	2	00000	1016	+2	PAX	,2	
26176	1	00001	2	26177	1017	+3	TXI	**1,2,1	
26177	0	90000	4	35621	1018	+4	CLA	PT+7,4	
26200	0	60100	4	35620	1019	+5	STO	PT+6,4	
26201	0	90000	4	35623	1020	+6	CLA	PT+9,4	
26202	0	60100	4	35622	1021	+7	STO	PT+8,4	
26203	0	90200	4	35630	1022	+8	CLS	PT+14,4	
26204	0	60100	4	35626	1023	+9	STO	PT+12,4	
26205	0	90200	4	35631	1024	+10	CLS	PT+15,4	
26206	0	60100	4	35627	1025	+11	STO	PT+13,4	
26207	0	90000	4	34101	1026	AZK2	CLA	AZ02,4	TEMPORARY
26210	0	60100	4	34002	1027	+1	STO	AZ08,4	PERMANENT
26211	0	90000	4	34411	1028	+2	CLA	AZ07,4	
26212	0	60100	4	35720	1029	+3	STO	AZ06,4	
26213	1	77777	4	26214	1030	+4	TXI	**1,4,-1	
26214	2	00001	2	26207	1031	+5	TXI	AZK2,2,1	
26215	0	77400	4	00000	1032	AZK1	AXT	**0,4	
26216	1	76003	4	26217	1033	+1	TXI	**1,4,-AZMTS	
26217	3	00000	4	26173	1034	AZK4	TXM	AZK3,4,**0	PRESET TO MAX STOR+1+AZMTB-AZMT
26220	0	77400	4	00000	1035	AZKR	AXT	**0,4	
26221	0	77400	2	00000	1036	+1	AXT	**0,2	
26222	0	02000	4	00001	1037	+2	TRA	1,4	

26223	0	63400	4	26245	1040	AZL	SXA	AZLR,4	
26224	0	50000	0	33731	1041	+1	CLA	WPR+7	C P
26225	0	24100	0	33732	1042	+2	FDP	WPR+8	K
26226	0	26000	0	33733	1043	+3	FMP	WPR+9	
26227	0	56000	0	40224	1044	+4	LDQ	FL,4	
26230	0	07400	4	27021	1045	+5	TSX	AZE,4	
26231	0	60100	0	12524	1046	+6	STO	COMMON+10	
26232	0	50000	0	40216	1047	+7	CLA	FL4	
26233	0	24100	0	40275	1048	+8	FDP	PI	
26234	0	13100	0	00000	1049	+9	XCA		
26235	0	24100	0	33733	1050	+10	FDP	WPR+9	
26236	0	13100	0	00000	1051	+11	XCA		
26237	0	56000	0	40254	1052	+12	LDQ	FL,8	
26240	0	07400	4	27021	1053	+13	TSX	AZE,4	
26241	0	13100	0	00000	1054	+14	XCA		
26242	0	26000	0	33732	1055	+15	FMP	WPR+8	K
26243	0	13100	0	00000	1056	+16	XCA		
26244	0	26000	0	12524	1057	+17	FMP	COMMON+10	
26245	0	77400	4	00000	1058	AZLR	AXT	**0,4	
26246	0	02000	4	00001	1059	+1	TRA	1,4	

1061*NOZZLE TUBE ROUTINES 1062*NOZZLE TUBE INITIALIZATION REGION

26247	0	63400	4	26264	1063	AZNI	SXA	AZNIR,4	
26250	0	50000	0	32633	1064	+1	CLA	P+13	T6
26251	0	02000	4	00001	1065	+2	TRA	1,4	

26252	0	07400	4	42602	1066	+3	TSX	ERROR,4	BAD THETA 0
26253	0	60100	0	32634	1067	+4	STO	P+14	
26254	0	50000	0	36111	1068	+5	CLA	DPO	
26255	-C	10000	0	26261	1069	+6	TN2	AZN11	
26256	0	50000	0	36077	1070	+7	CLA	DTMI	
26257	0	07400	4	42437	1071	+8	TSX	LINT,4	
26260	0	00000	0	33441	1072	+9	PZE	WPO	
26261	0	60100	0	32656	1073	AZN11	STO	P+32	
26262	0	50000	0	36126	1074	+1	CLA	DQINT	
26263	0	60100	0	32641	1075	+2	STO	QINT	
26264	0	77400	4	00000	1076	AZNIR	AXT	**0,4	
26265	0	02000	4	00001	1077	+1	TRA	1,4	

26266	0	63400	4	26321	1080	AZNM	SXA	AZNR,4	
26267	0	50000	0	44463	1081	+1	CLA	AZN2	
26270	0	30200	0	44233	1082	+2	F58	AZN3	Z
26271	0	60100	0	33743	1083	+3	STO	TP+6	
26272	0	50000	0	44442	1084	+4	CLA	PSUBC	P1
26273	0	30200	0	44443	1085	+5	F58	PSUBC+1	P2
26274	0	24100	0	44461	1086	+6	FDP	DELTAZ	
26275	0	26000	0	33743	1087	+7	FMP	TP+6	Z-Z1
26276	0	30000	0	44442	1088	+8	FAD	PSUBC	P1
26277	0	60100	0	33752	1089	+9	STO	TP+13	
26300	0	50000	0	44444	1090	+10	CLA	TSUBC	T1
26301	0	30200	0	44445	1091	+11	F58	TSUBC+1	T2
26302	0	24100	0	44461	1092	+12	FDP	DELTAZ	
26303	0	26000	0	33743	1093	+13	FMP	TP+6	
26304	0	30000	0	44444	1094	+14	FAD	TSUBC	T1
26305	0	56000	0	26323	1095	+15	LDQ	AZNM1	H2 CRITICAL TEMP
26306	0	60000	0	32737	1096	+16	STZ	X+17	
26307	0	04000	0	26311	1097	+17	TLQ	AZNM2	H2 GAS
26310	-0	62500	0	32737	1098	+18	STL	X+17	FLAG TO IGNORE NOZZLE TUBE CHOKE
26311	0	07400	4	26364	1099	AZNM2	TSX	SORT,4	
26312	0	07400	4	42602	1100	+1	TSX	ERROR,4	
26313	0	60100	0	33756	1101	+2	STO	TP+17	
26314	0	56000	0	44234	1102	+3	LDQ	AZN3+1	AREA OF NOZZLE TUBE THROAT
26315	0	26000	0	33752	1103	+4	FMP	TP+13	
26316	0	24100	0	33756	1104	+5	FDP	TP+17	
26317	0	26000	0	40241	1105	+6	FMP	FL139	.1396
26320	0	60100	0	32651	1106	+7	STO	P+27	
26321	0	77400	4	00000	1107	AZNR	AXT	**0,4	
26322	0	02000	4	00001	1108	+1	TRA	1,4	
26323	2	06740	0	00000	1109	AZNM1	DEC	60.	

1111*PRINT REGIONS

26324	0	52000	0	32727	1113	AZPC	ZET	X+9	
26325	0	02000	4	00001	1114	+1	TRA	1,4	
26326	0	63400	4	26355	1115	+2	SXA	AZPCR,4	
26327	0	07412	4	32541	1116	+3	TSX	PL,4,10	
26330	0	07400	4	00052	1117	+4	TSX	DOUT,4	
26331	3	02033	0	26372	1118	+5	PTM	AZPC3,,1051	

26332	0	11616	0	00000	1119	+6	PZE	0.,5006
26333	-1	47064	0	00012	1120	+7	FVE	KPRINT.,20020
26334	0	07400	4	00052	1121	+8	TSX	DOUT.,4
26335	3	05772	0	26357	1122	+9	PTM	AZPC1.,3066
26336	3	02064	0	26455	1123	+10	PTM	AZPS1+2.,1078
26337	-2	13672	0	32630	1124	+11	SIX	P+10.,6074
26340	-1	00024	0	00012	1125	+12	FVE	10.,20
26341	0	07400	4	00052	1126	+13	TSX	DOUT.,4
26342	3	01765	0	26362	1127	+14	PTM	AZPC2.,1013
26343	0	13545	0	00001	1128	+15	PZE	1.,7013
26344	-1	00012	0	00012	1129	+16	FVE	10.,10
26345	0	07400	4	00052	1130	+17	TSX	DOUT.,4
26346	-2	13576	0	32632	1131	+18	SIX	P+28.,6014
26347	0	05705	0	00001	1132	+19	PZE	1.,3013
26350	-2	13662	0	32665	1133	+20	SIX	P+39.,6066
26351	-2	13677	0	32657	1134	+21	SIX	P+33.,6079
26352	-2	13714	0	32676	1135	+22	SIX	P+48.,6092
26353	-2	13731	0	32637	1136	+23	SIX	P+17.,6105
26354	-1	47052	0	00012	1137	+24	FVE	KPRINT.,20010
26355	0	77400	4	00000	1138		AZPCR	AXT
26356	0	02000	4	00001	1139	+1	TRA	1.,4
26357	3	14543	2	56360	1140		AZPC1	BCI
26362	-2	04760	0	10660	1141		AZPC2	BCI
26372	-1	45454	5	45454	1142		AZPC3	BCI

					1144	REGION TO PRINT INLET AND OUTLET PRESSURE DROPS			
26373	0	63400	4	26424	1145		AZPD	SXA	AZPDR.,4
26374	0	44100	4	00000	1146	+1	LDI		0.,4
26375	-0	05700	7	77774	1147	+2	RIL		777774
26376	0	60400	0	00001	1148	+3	STI		KINDX4
26377	0	07400	4	00052	1149	+4	TSX		DOUT.,4
26400	3	01772	1	34555	1150	+5	PTM		FX.,1,1018
26401	3	02001	4	26430	1151	+6	PTM		AZPD1+2.,4,1025
26402	3	05764	0	26430	1152	+7	PTM		AZPD2.,3044
26403	3	05773	0	26435	1153	+8	PTM		AZPD4.,3067
26404	3	02071	0	26435	1154	+9	PTM		AZPD4.,1081
26405	3	04056	0	26456	1155	+10	PTM		AZPS3.,2094
26406	3	04104	0	26444	1156	+11	PTM		AZPD7.,2116
26407	3	02154	0	26446	1157	+12	PTM		AZPD7+2.,1132
26410	1	13674	4	26442	1158	+13	PON		AZPD5+2.,4,6076
26411	1	13662	4	26435	1159	+14	PON		AZPD3+2.,4,6050
26412	1	13727	4	26451	1160	+15	PON		AZPD8+2.,4,6103
26413	1	13755	4	26453	1161	+16	PON		AZPD9+2.,4,6125
26414	1	00000	4	26444	1162	+17	PON		AZPD6+2.,4
26415	0	07401	4	32541	1163	+18	TSX		PL.,4,1
26416	0	44100	0	00061	1164	+19	LDI		KINDX4
26417	-0	05400	0	00001	1165	+20	LFT		1
26420	0	02000	0	26424	1166	+21	TRA		AZPDR
26421	0	07402	4	32541	1167	+22	TSX		PL.,4,2
26422	0	07400	4	32563	1168	+23	TSX		PC.,4
26423	-1	00012	0	00012	1169	+24	FVE		KPRINT.,10
26424	0	77400	4	00000	1170		AZPDR	AXT	0.,4
26425	0	02000	4	00001	1171	+1	TRA		1.,4
26426	-2	00005	0	00005	1172		AZPD1	BCI	3,INLET OUTLET

PART NAME
IN OR OUTDROP
FLOW
RHO
FVE

26430	-0	75125	6	26264	1173		AZPD2	BCI	3,PRESSURE DROP=
26433	-2	00000	1	35616	1174		AZPD3	SIX	PT+4,1
26434	-2	00000	1	35617	1175	+1	SIX		PT+5,1
26435	-2	06047	6	23121	1176		AZPD4	BCI	3, PSIA, PRESSURE=
26440	-2	00000	1	35612	1177		AZPD5	SIX	PT.,1
26441	-2	00000	1	35613	1178	+1	SIX		PT+1,1
26442	-1	00024	0	00012	1179		AZPD6	FVE	10.,20
26443	-1	00012	0	00012	1180	+1	FVE		10.,10
26444	-0	32261	6	22523	1181		AZPD7	BCI	3, LB/SEC RHO= LB/IN3
26447	-2	00000	1	35624	1182		AZPD8	SIX	PT+10,1
26450	-2	00000	1	35614	1183	+1	SIX		PT+2,1
26451	-2	00000	1	35621	1184		AZPD9	SIX	PT+7,1
26452	-2	00000	1	35623	1185	+1	SIX		PT+9,1
26453	-2	33144	2	51360	1186		AZPS1	BCI	3, TIME=
26456	2	64346	6	66051	1187		AZPS3	BCI	2, FLOW RATE =
26460	2	33046	4	22560	1188		AZP3	BCI	2, CHOKE FLOW=

FLOW
RHO

SEC

NO. 2 POINTS THIS PART

					1190	ITERATION PRINT REGION			
26462	0	52000	0	32727	1191		AZPI	ZET	X+9
26463	0	02000	4	00001	1192	+1	TRA		1.,4
26464	0	63400	1	26573	1193	+2	SXA		AZPIR.,1
26465	0	63400	2	26574	1194	+3	SXA		AZPIR+1,2
26466	0	63400	4	26575	1195	+4	SXA		AZPIR+2,4
26467	0	52000	0	36123	1196	+5	ZET		DNZFF
26470	0	07400	4	26625	1197	+6	TSX		AZPN.,4
26471	0	77400	1	62717	1198	+7	AXT		AZHTB-AZHT.,1
26472	0	63400	1	26534	1199		AZPI3	SXA	AZPI1.,1
26473	0	07402	4	26373	1200	+1	TSX		AZPD.,4,2
26474	0	50000	1	34556	1201	+2	CLA		FX+1,1
26475	0	73400	2	00000	1202	+3	PAX		,2
26476	0	50000	1	36064	1203	+4	CLA		DELZ.,1
26477	0	60100	0	26610	1204	+5	STO		AZPI6
26500	0	24100	0	40214	1205	+6	FDP		FL2
26501	-0	60000	0	32616	1206	+7	STO		P
26502	0	50000	1	35637	1207		AZPI2	CLA	AZ01+1,1
26503	0	60100	0	32617	1208	+1	STO		P+1
26504	0	50000	1	34163	1209	+2	CLA		AZ03,1
26505	0	30000	1	34164	1210	+3	FAD		AZ03+1,1
26506	0	24100	0	40214	1211	+4	FDP		FL2
26507	-0	60000	0	32620	1212	+5	STO		P+2
26510	0	50000	1	34245	1213	+6	CLA		AZ04,1
26511	0	30000	1	34246	1214	+7	FAD		AZ04+1,1
26512	0	24100	0	40214	1215	+8	FDP		FL2
26513	-0	60000	0	32621	1216	+9	STO		P+3
26514	0	50000	1	34327	1217	+10	CLA		AZ05,1
26515	0	60100	0	32622	1218	+11	STO		P+4
26516	0	50000	1	34411	1219	+12	CLA		AZ07,1
26517	0	60100	0	32623	1220	+13	STO		P+5
26520	0	50000	1	34101	1221	+14	CLA		AZ02,1
26521	0	30000	1	34102	1222	+15	FAD		AZ02+1,1
26522	0	24100	0	40214	1223	+16	FDP		FL2
26523	-0	60000	0	32631	1224	+17	STO		P+11
26524	0	07400	4	32642	1225	+18	TSX		PRINT.,4
26525	0	52000	0	32725	1226	+19	ZET		X+7

METAL TEMP

METAL TEMP

PRESSURE

HF

RHO

FLOW RATE

26526	1	77777	2	26577	1227	+20	TXI	AZPI8,2,-1	
26527	C	50000	0	32616	1228	+21	CLA	P	
26530	0	30000	0	26610	1229	+22	FAD	AZPI6	DEL 2
26531	0	60100	0	32616	1230	+23	STO	P	
26532	1	77777	1	26533	1231	+24	TXI	*+1,1,-1	
26533	2	00001	2	26502	1232	+25	TXI	AZPI2,2,1	
26534	0	77400	1	00000	1233		AZPI1	AXT	*+0,1
26535	0	07401	4	26373	1234	+1	TSX	AZPD,4,1	OUTLET PRES DROP
26536	0	52000	1	34560	1235	+2	ZET	FX+3,1	
26537	-1	26611	0	25421	1236	+3	STR	AZF,,AZPI7	
26540	0	52000	1	34561	1237	+4	ZET	FX+4,1	
26541	-1	26614	0	25421	1238	+5	STR	AZF,,AZPI9	
26542	1	76003	1	26543	1239	+6	TXI	*+1,1,-AZMT5	
26543	3	00000	1	26472	1240		AZPI4	TXM	AZPI3,1,*+0
26544	0	50000	0	32631	1241	+1	CLA	P+11	PRESET TO MAX STOR+1+D-AZMT
26545	0	30200	0	32644	1242	+2	FSB	P+22	WDOTR
26546	0	30200	0	32645	1243	+3	FSB	P+23	WDOTC
26547	0	60100	0	32646	1244	+4	STO	P+24	WDOTH
2655C	0	30200	0	34007	1245	+5	FSB	TP+42	WDOTN
26551	0	24100	0	34007	1246	+6	FDP	TP+42	WDOTNCHOKE
26552	-0	60000	0	34024	1247	+7	STQ	TP+55	
26553	0	07400	4	00052	1248	+8	TSX	DOUT,4	ERROR
26554	3	01772	0	26647	1249	+9	PTH	AZPN1,,1018	
26555	3	02001	0	26461	1250	+10	PTH	AZP3+1,,1025	
26556	3	02022	0	26647	1251	+11	PTH	AZPN1,,1042	
26557	3	04007	C	26460	1252	+12	PTH	AZP3,,2055	
26560	3	06017	0	26605	1253	+13	PTH	AZPI5,,3087	
26561	3	06055	0	26453	1254	+14	PTH	AZPS1,,3117	
26562	-2	13622	0	32646	1255	+15	SIX	P+24,,6034	FLOW
26563	-2	13660	C	34007	1256	+16	SIX	TP+42,,6064	CHOKE FLOW
26564	-0	00104	0	32732	1257	+17	FOR	X+12,,68	
26565	-3	13721	0	34024	1258	+18	SVN	TP+55,,6097	ERROR
26566	-3	06051	0	32630	1259	+19	SVN	P+10,,3113	
26567	-1	23444	0	00012	1260	+20	FVE	10,,10020	
26570	0	07403	4	32541	1261	+21	TSX	PL,4,3	
26571	0	52000	0	32722	1262	+22	ZET	X+4	
26572	-1	25350	0	25421	1263	+23	STR	AZF,,AZB10	P6 TOO LOW
26573	0	77400	1	00000	1264		AZPIR	AXT	*+0,1
26574	0	77400	2	00000	1265	+1	AXT	*+0,2	
26575	0	77400	4	00000	1266	+2	AXT	*+0,4	
26576	0	02000	4	00001	1267	+3	TRA	1,4	
26577	-3	00000	2	26534	1269		AZPI8	TXL	AZPI1,2,0
2660C	0	50000	1	35615	1270	+1	CLA	PT+3,1	M MAX
26601	0	60100	0	32616	1271	+2	STO	P	
26602	-0	63600	2	26604	1272	+3	SCD	*+2,2	
26603	0	77400	2	00001	1273	+4	AXT	1,2	
26604	1	00000	1	26502	1274	+5	TXI	AZPI2,1,*+0	
26605	3	16325	5	12163	1275		AZPI5	BCI	2,ITERATIONS
26607	2	55151	4	65113	1276	+2	BCI	1,ERROR=	
				26610	1277		AZPI6	BSS	1,F
26611	-0	46063	4	64660	1278		AZPI7	BCI	3,M TOO SMALL
26614	-2	32544	4	76025	1279		AZPI9	BCI	3,TEMP EXCEEDED MAX

26617	0	50000	0	32727	1282	AZPI8	CLA	X+9	
2662C	-0	10000	0	26622	1283	+1	TNZ	*+2	
26621	0	50000	0	32726	1284	+2	CLA	X+8	
26622	0	40200	0	40200	1285	+3	SUB	FX1	
26623	0	60100	0	32727	1286	+4	STO	X+9	
26624	0	02000	4	00001	1287	+5	TRA	1,4	

26625	0	63400	4	26645	1290	AZPN	SXA	AZPNR,4	
26626	0	07402	4	32541	1291	+1	TSX	PL,4,2	
26627	0	07400	4	00052	1292	+2	TSX	DOUT,4	
26630	3	23530	0	26647	1293	+3	PTH	AZPN1,,10072	
26631	3	02101	0	26461	1294	+4	PTH	AZP3+1,,1089	
26632	3	04100	0	26460	1295	+5	PTH	AZP3,,2112	
26633	-2	13636	0	32703	1296	+6	SIX	P+53,,6046	
26634	-2	13660	0	32702	1297	+7	SIX	P+52,,6064	
26635	-2	13701	0	32630	1298	+8	SIX	P+10,,6081	
26636	-2	13751	C	32651	1299	+9	SIX	P+27,,6121	
26637	-2	13722	0	34063	1300	+10	SIX	TP+86,,6098	CHOKE FLOW
26640	-1	00024	0	00012	1301	+11	FVE	10,,20	
26641	0	52000	0	32724	1302	+12	ZET	X+6	
26642	-1	43573	0	25421	1303	+13	STR	AZF,,BUG1	NOZZLE TUBE ERROR
26643	0	52000	0	32737	1304	+14	ZET	X+17	
26644	-1	26661	0	25421	1305	+15	STR	AZF,,AZPN2	
26645	0	77400	4	00000	1306		AZPNR	AXT	*+0,4
26646	0	02000	4	00001	1307	+1	TRA	1,4	
26647	-0	54671	7	14325	1308		AZPN1	BCI	,NOZZLE TUBE INPUT TEMP=
26661	-0	33150	6	03145	1309		AZPN2	BCI	3,LIQ IN TUBE THROAT

26664	0	52000	0	32727	1312	AZPP	ZET	X+9	
26665	0	02000	4	00001	1313	+1	TRA	1,4	
26666	0	63400	4	26740	1314	+2	SXA	AZPPR,4	
26667	0	63400	1	26741	1315	+3	SXA	AZPPR+1,1	
2667C	0	44100	4	00000	1316	+4	LDI	0,4	
26671	-0	05700	7	77776	1317	+5	RIL	777776	
26672	-0	04600	0	00000	1318	+6	PIA		
26673	-0	73700	1	00000	1319	+7	PDC	,1	PRED OR CORR
26674	0	07406	4	32541	1320	+8	TSX	PL,4,6	
26675	0	50260	1	26767	1321	+9	CLS*	AZPP6+2,1	WC
26676	0	30260	1	26771	1322	+10	FSB*	AZPP6+4,1	WM
26677	0	60260	1	26775	1323	+11	SLW*	AZPP6+8,1	WT
267CC	C	30000	0	32631	1324	+12	FAD	P+11	WDOTR
267C1	0	60160	1	26773	1325	+13	STO*	AZPP6+6,1	WN
26702	0	07400	4	00052	1326	+14	TSX	DOUT,4	
26703	3	02044	1	26743	1327	+15	PTH	AZPP1,1,1060	
26704	3	04030	0	26745	1328	+16	PTH	AZPP2,,2072	
26705	-1	00024	0	00012	1329	+17	FVE	10,,20	
26706	0	07400	4	00052	1330	+18	TSX	DOUT,4	
26707	3	01765	C	26747	1331	+19	PTH	AZPP4,,1013	

PAGE 25

25/04/64

PAGE 25

P0 -- STATIC PRESSURE

1440*REGION TO COMPUTE INLET AND OUTLET CAPACITANCE FLOW RATE CHANGE

27075	0	63400	4	27123	1441	AZU	SKA	AZUR,4	
27076	0	63400	2	27124	1442		+1 SKA	AZUR+1,2	
27077	0	56000	0	32621	1443		+2 LOG	P+3	
27100	0	16200	0	27102	1444		+3 TOP	P+2	
27101	0	02000	4	00001	1445		+4 TRA	1,4	
27102	0	44100	4	00000	1446		+5 LDI	0,4	NEGATIVE PRESSURE
27103	-0	05700	7	77776	1447		+6 RIL	777776	
27104	-0	04400	0	00000	1448		+7 PIA		
27105	-0	73700	2	00000	1449		+8 PDC	.2	
27106	0	50000	0	32620	1450		+9 CLA	P+2	T
27107	0	07400	4	25544	1451		+10 TSH	AZM,4	
27110	0	07400	4	42602	1452		+11 TSH	ERROR,4	
27111	0	50200	0	33730	1453		+12 CLS	WPR+6	NEW RHO EOM MT13
27112	0	60260	2	27130	1454		+13 SLW	AZU1,2	
27113	0	30060	2	27132	1455		+14 FAD	AZU2,2	OLD RHO
27114	0	24100	0	32637	1456		+15 FDP	P+17	DELT
27115	0	24040	2	27134	1457		+16 FMP	AZU3,2	PLENUM VOLUME
27116	0	30060	2	27136	1458		+17 FAD	AZU5,2	OLD DELWDOT
27117	0	60160	2	27140	1459		+18 STO	AZU6,2	-CURRENT DELWDOT
27120	0	30000	0	32631	1460		+19 FAD	P+11	
27121	0	60100	0	32631	1461		+20 STO	P+11	
27122	-0	12000	0	27126	1462		+21 TMI	AZU4	NEGATIVE FLOW RATE
27123	0	77400	4	00000	1463	AZUR	AXT	000,4	
27124	0	77400	2	00000	1464		+1 AXT	000,2	
27125	0	02000	4	00003	1465		+2 TRA	3,4	
27126	0	52200	0	27123	1466	AZU4	XEC	AZUR	
27127	1	00001	4	27124	1467		+1 TXI	AZUR+1,4,1	ERROR RETURN
27130	0	00000	1	35621	1468	AZU1	PZE	PT+7,1	
27131	0	00000	1	35623	1469		+1 PZE	PT+9,1	
27132	0	00000	1	35620	1470	AZU2	PZE	PT+6,1	
27133	0	00000	1	35622	1471		+1 PZE	PT+8,1	
27134	0	00000	1	36074	1472	AZU3	PZE	DVI,1	
27135	0	00000	1	36075	1473		+1 PZE	DVO,1	
27136	0	00000	1	35626	1474	AZU5	PZE	PT+12,1	PAST TIME DELWDOT
27137	0	00000	1	35627	1475		+1 PZE	PT+13,1	
27140	0	00000	1	35630	1476	AZU6	PZE	PT+14,1	-CURRENT DELWDOT
27141	0	00000	1	35631	1477		+1 PZE	PT+15,1	

1479*REGION TO COMPUTE VAPOR PRESSURE VS TEMP

27142	0	63400	4	27152	1480	AZV	SKA	AZVR,4	
27143	0	77400	4	00005	1481		+1 AXT	5,4	
27144	0	75400	0	00000	1482		+2 PXA	.0	
27145	0	30000	4	27161	1483	AZV2	FAD	AZV1+5,4	
27146	-2	00001	4	27152	1484		+1 TNX	AZVR,4,1	
27147	0	13100	0	00000	1485		+2 XCA		
27150	0	26000	0	33742	1486		+3 FMP	TP+5	
27151	0	02000	0	27145	1487		+4 TRA	AZV2	
27152	0	77400	4	00000	1488	AZVR	AXT	000,4	
27153	0	02000	4	00001	1489		+1 TRA	1,4	
27154	1	62526	4	30773	1490	AZV1	DEC	40835E-9,-.0037617,.238625,-7.92,96.38	

1492*INPUT SUBROUTINES

1493*TEST NEXT CASE FOR STANDARD INPUT DESIRED

27161	0	63400	4	27177	1494	AZX	SKA	AZX,4	
27162	0	63400	0	27304	1495		+1 SKA	AZX82,0	INITIALIZE XR FOR NEW CASE
27163	0	07476	4	00102	1496		+2 TSH	KTAKES,4,62	
27164	-1	00001	0	27215	1497		+3 FVE	AZX1,.1	
27165	0	12000	0	27170	1498		+4 TPL	P+3	
27166	-1	27217	0	25421	1499	AZX4	STR	AZF,,AZX3	
27167	0	07400	4	00076	1500		+1 TSH	KFINIS,4	
27170	0	16200	0	27201	1501		+2 TOP	AZX4	
27171	-0	50000	0	27215	1502		+3 CAL	AZX1	
27172	0	32200	0	27216	1503		+4 ERA	AZX2	
27173	0	60200	0	27215	1504		+5 SLW	AZX1	
27174	-0	10000	0	27177	1505		+6 TNZ	AZX	N CARD SAYS IGNORE STD INPUT
27175	0	07476	4	00101	1506		+7 TSH	KMOVES,4,62	PASS N CARD
27176	-1	00016	0	00000	1507		+8 FVE	0,,14	
27177	0	77400	4	00000	1508	AZX	AXT	000,4	
27200	0	02000	4	00001	1509		+1 TRA	1,4	
27201	-1	27222	0	25421	1510	AZX4	STR	AZF,,AZX5	
27202	0	07400	4	00052	1511		+1 TSH	DOUT,4	
27203	3	21544	0	27225	1512		+2 PTH	AZX7,,9060	
27204	-1	00024	0	00000	1513		+3 FVE	KONLIN,,20	
27205	0	07400	4	00076	1514		+4 TSH	KFINIS,4	
27206	0	07400	4	00055	1515	AZX8	TSH	KDEBUE,4	
27207	0	16200	0	27201	1516		+1 TOP	AZX4	
27210	-1	27212	0	25421	1517		+2 STR	AZF,,AZX9	
27211	0	02000	0	24654	1518		+3 TRA	AZX4	
27212	3	14343	2	52721	1519	AZX9	BCI	3,ILLEGAL CHARACTER	
				27215	1520	AZX1	BSS	1,0	NOT 0= STD CASE
27216	-0	56060	6	06060	1521	AZX2	BCI	1,N	
27217	2	54524	6	04626	1522	AZX3	BCI	3,END OF INPUT	
27222	2	22124	6	06321	1523	AZX5	BCI	3,BAD TAPE- FLUSH	
27225	-2	32147	2	56023	1524	AZX7	BCI	9,TAPE CHECK ON KISMET INPUT TAPE, PLEASE SAVE TAPE	

1526*READ IN ONE PART

27236	0	63400	4	27257	1527	AZX4	SKA	AZXAR,4	
27237	-0	52000	0	27215	1528		+1 NZT	AZX1	
27240	0	02000	0	27250	1529		+2 TRA	AZX1	IGNORE STD CASE
27241	-0	62500	0	27322	1530		+3 STL	AZX81	INPUT FROM CORE
27242	0	07400	4	41664	1531		+4 TSH	A558,4	
27243	0	32577	0	36064	1532		+5 PZE	0,,TCARD	
27244	0	07400	4	00056	1533		+6 TSH	KERROR,4	
27245	0	07400	4	00056	1534		+7 TSH	KERROR,4	
27246	-0	52000	0	32612	1535		+8 NZT	TCARD+11	
27247	0	02000	0	27261	1536		+9 TRA	AZX2	
27250	0	60000	0	27322	1537	AZX1	STZ	AZX81	INPUT FROM TAPE
27251	0	07400	4	41664	1538		+1 TSH	A558,4	
27252	0	32577	0	36064	1539		+2 PZE	0,,TCARD	
27253	0	02000	0	27206	1540		+3 TRA	AZX8	
27254	0	02000	0	27166	1541		+4 TRA	AZX6	EOF
27255	-0	52000	0	36065	1542		+5 NZT	DMAX	0= IGNORE THIS PART
27256	0	02000	0	27237	1543		+6 TRA	AZX+1	
27257	0	77400	4	00000	1544	AZXAR	AXT	000,4	
27258	0	02000	4	00001	1545				

27261	0	60000	0	27322	1946	AZXA2	STZ	AZXBI	
27262	0	07400	4	41664	1947	+1	TSX	AS50,4	READ TUBE INPUT, IF ANY
27263	0	32577	0	44107	1948	+2	PZE	LVSAC,,TCARD	
27264	0	02000	0	27204	1949	+3	TRA	AZX8	
27265	0	02000	0	27166	1950	+4	TRA	AZX8	
27266	-0	50000	0	27277	1951	+5	CAL	AZXRA4	
27267	0	32000	0	32577	1952	+6	AMS	TCARD	
27270	-0	52000	0	32612	1953	+7	NZT	TCARD+11	
27271	0	02000	0	27257	1954	+8	TRA	AZXAR	
27272	-1	27274	0	29421	1955	AZXAS	STR	AZF,,AIXA3	
27273	0	07400	4	00076	1956	+1	TSX	KFINIS,4	
27274	-3	12551	4	66063	1957	AZXAS	BCI	3,ZERO TCARD MISSING	
27277	-2	07777	7	77777	1958	AZXAS	OCT	-20777777777	

27300	-0	52000	0	27322	1960	READ ONE CARD FROM CORE			
27301	0	02000	0	00101	1961	AZX8	NZT	AZXBI	INPUT FROM TAPE
27302	0	63400	4	27317	1962	+1	TRA	KMOV8	
27303	0	63400	1	27320	1963	+2	SXA	AZXBR,4	
27304	0	77400	4	00000	1964	+3	SXA	AZXBR+1,1	
27305	0	77400	1	00000	1965	AZXB2	AXT	000,4	
27306	-0	90000	4	50032	1966	+1	AXT	0,1	
27307	0	60200	1	32577	1967	AZXB3	CAL	AZXI,4	
27310	1	77777	4	27311	1968	+1	SLB	TCARD,1	
27311	1	77777	1	27312	1969	+2	TXI	0+1,4,-1	
27312	3	77764	1	27306	1970	+3	TXI	0+1,1,-1	
27313	0	63400	4	27304	1971	+4	TXM	AZXB3,1,-12	ADDRESS FOR NEXT CARD
27314	-0	76000	0	00003	1972	+5	SXA	AZXB2,4	
27315	0	13100	0	00000	1973	+6	SSM		
27316	0	76000	0	00003	1974	+7	XCA		TO SIMULATE KMOV8
27317	0	77400	4	00000	1975	+8	SSP		
27320	0	77400	1	00000	1976	AZXBR	AXT	000,4	
27321	0	02000	4	00002	1977	+1	AXT	000,1	
				27322	1978	+2	TRA	2,4	
					1979	AZXBI	BSS	1,0	NOT 0= INPUT FROM CORE

27323	0	63400	4	27345	1982	AZXC	SXA	AZXCR,4	
27324	0	63400	1	27346	1983	+1	SXA	AZXCR+1,1	
27325	0	77400	1	00000	1984	+2	AXT	0,1	
27326	0	07476	4	00101	1985	AZXC2	TSX	KMOV8,4,62	INPUT STORAGE
27327	-1	00014	1	50032	1986	+1	PVE	AZXI,1,12	
27330	0	16200	0	27201	1987	+2	TQP	AZX4	
27331	-0	12000	0	27334	1988	+3	YMI	AZXC1	
27332	-0	50000	1	50045	1989	+4	CAL	AZXI+11,1	COL 67-72
27333	0	10000	0	27340	1990	+5	TZE	AZXC4	
27334	1	77764	1	27335	1991	+6	TXI	0+1,1,-12	
27335	3	76650	1	27326	1992	+7	TXM	AZXC2,1,-12*CARDS	TEST CARDS VS AVAILABLE STORAGE
27336	-1	27350	0	25421	1993	AZXC1	STR	AZF,,AIXC3	
27337	0	07400	4	00076	1994	+1	TSX	KFINIS,4	
27340	0	60000	0	27322	1995	AZXC4	STZ	AZXBI	
27341	0	07400	4	41664	1996	+1	TSX	AS50,4	
27342	0	32577	0	44107	1997	+2	PZE	LVSAC,,TCARD	NOZZLE TUBE PARAMETERS
27343	0	02000	0	27334	1998	+3	TRA	AZXC1	
27344	0	02000	4	00002	1999	+4	TRA		

27345	0	77400	4	00000	1600	AZXCR	AXT	000,4	
27346	0	77400	1	00000	1601	+1	AXT	000,1	
27347	0	02000	4	00001	1602	+2	TRA	1,4	
27350	2	55151	4	65160	1603	AZXC3	BCI	3,ERROR IN STD INPUT	

27353	0	52000	0	32742	1606	AZY	ZET	X+20	
27354	0	02000	4	00002	1607	+1	TRA	2,4	DILUENT SET TO ZERO
27355	0	50000	0	32620	1608	+2	CLA	P+2	
27356	0	60100	0	32705	1609	+3	STO	P+55	TC
27357	0	50000	0	32621	1610	+4	CLA	P+3	
27360	0	60100	0	32704	1611	+5	STO	P+54	PC
27361	0	50000	0	32631	1612	+6	CLA	P+11	
27362	0	30200	0	32644	1613	+7	F50	P+22	WOOTC
27363	0	60100	0	32631	1614	+8	STO	P+11	WOOTR
27364	-0	62500	0	32744	1615	+9	STL	X+22	DILUENT REMOVED FLAG
27365	-0	12000	4	00001	1616	+10	TMI	1,4	ERROR RETURN FOR NEGATIVE WOOTR
27366	0	02000	4	00002	1617	+11	TRA	2,4	

27367	0	50000	0	32655	1620	AZZ	CLA	P+31	INLET
27370	0	60100	0	32703	1621	+1	STO	P+53	T2
27371	0	60100	0	32620	1622	+2	STO	P+2	T3
27372	0	56000	0	32757	1623	+3	LQD	C+8	CURRENT FLUID TEMP
27373	0	26000	0	32631	1624	+4	FNP	P+11	EQN T2
27374	0	24100	0	34071	1625	+5	FOP	TP+92	WOOTR
27375	0	26000	0	32631	1626	+6	FNP	P+11	ANO2 PREDICTED
27376	0	30000	0	32654	1627	+7	FAD	P+30	
27377	0	60100	0	32702	1628	+8	STO	P+52	
27400	0	60100	0	32621	1629	+9	STO	P+3	P3
27401	0	02000	4	00001	1630	+10	TRA	1,4	CURRENT PRESSURE

27402	0	63400	4	27525	1633	AYA	SXA	AYAR,4	
27403	0	60000	0	32733	1634	+1	STZ	X+13	ERROR FLAG
27404	0	56000	0	32677	1635	+2	LQD	P+49	WOOTP
27405	0	26000	0	32632	1636	+3	FNP	P+12	EQN PT24
27406	0	60100	0	34042	1637	+4	STO	TP+69	
27407	0	60000	0	40633	1638	+5	STZ	NEWB9+1	P6
27410	0	50000	0	40305	1639	+6	CLA	BIG	MINWOOTH
27411	0	60100	0	40632	1640	+7	STO	NEWB9	
27412	0	50000	0	32645	1641	+8	CLA	P+23	MAX WOOTH
27413	0	60100	0	34045	1642	+9	STO	TP+72	
27414	0	50000	0	34112	1643	+10	CLA	DP8E	WOOTH(I+1) GUESS = WOOTH(I)
27415	0	07400	4	40547	1644	+11	TSX	NEWB,4	
27416	0	34043	0	34045	1645	+12	PZE	TP+72,,TP+70	
27417	0	00017	0	34044	1646	+13	PZE	TP+71,,15	
27420	0	02000	0	27527	1647	+14	TRA	AYA1	NON CONVERGENCE
27421	0	50000	0	34045	1648	+15	CLA	TP+72	WOOTH
27422	0	24100	0	33753	1649	+16	FOP	TP+14	EQN PT35
27423	-0	60000	0	12512	1650	+17	STO	COMMON	

27424	0	24000	0	12512	1651	+18	FMP	COMMON		
27425	0	30200	0	34042	1652	+19	FSD	TP+69		
27426	0	12000	0	40624	1653	+20	TPL	BDX8	WOOTH TOO BIG	
27427	0	60200	0	47333	1654	+21	SLW	PR+10	PHM	
27430	0	90000	0	32674	1655	+22	CLA	P+44	P2	EQN PT36
27431	0	30200	0	47333	1656	+23	FSD	PR+10	PHM	
27432	0	07400	4	24364	1657	+24	TSX	SGRT,4		
27433	0	07400	4	42602	1658	+25	TSX	ERROR,4		
27434	0	13100	0	00000	1659	+26	XCA			
27435	0	24000	0	33740	1660	+27	FMP	TP+3		
27436	0	60100	0	34044	1661	+28	STO	TP+73	WOOTC	
27437	0	60100	0	47403	1662	+29	STO	PR+50		
27440	0	30000	0	34045	1663	+30	FAD	TP+72	WOOTH	EQN PT27A
27441	0	60100	0	34051	1664	+31	STO	TP+76	WOOTY	
27442	0	24100	0	33754	1665	+32	FDP	TP+15	K12	EQN PT37
27443	-0	60000	0	47447	1666	+33	STQ	PR+06	V8	
27444	0	30000	0	34045	1667	+34	CLA	TP+72	WOOTH	EQN PT38
27445	0	60100	0	47404	1668	+35	STQ	PR+51		
27446	0	24100	0	33755	1669	+36	FDP	TP+16		
27447	-0	60000	0	47446	1670	+37	STQ	PR+05	VHM	
27450	0	30000	0	34046	1671	+38	CLA	TP+73	WOOTC	EQN PT39
27451	0	24100	0	33762	1672	+39	FDP	TP+21		
27452	-0	60000	0	47445	1673	+40	STQ	PR+04	VCM	
27453	0	30000	0	34046	1674	+41	CLA	TP+73	WCOYC	EQN PT40
27454	0	24100	0	33763	1675	+42	FDP	TP+22		
27455	-0	60000	0	12513	1676	+43	STQ	COMMON+1		
27456	0	24000	0	12513	1677	+44	FMP	COMMON+1		
27457	0	30200	0	32674	1678	+45	FSD	P+44	P2	
27460	0	12000	0	40624	1679	+46	TPL	BDX8	WOOTC, THEREFORE WOOTH TOO BIG	
27461	0	60200	0	47332	1680	+47	SLW	PR+9	PCM	
27462	0	50000	0	32633	1681	+48	LDQ	P+13	T6(1)	EQN PT28
27463	0	26000	0	34045	1682	+49	FMP	TP+72	WOOTH	
27464	0	67100	0	12514	1683	+50	STO	COMMON+2		
27465	0	50000	0	32675	1684	+51	LDQ	P+47		
27466	0	26000	0	34046	1685	+52	FMP	TP+73		
27467	0	30000	0	12514	1686	+53	FAD	COMMON+2		
27470	0	24100	0	34051	1687	+54	FDP	TP+76		
27471	0	26000	0	34056	1688	+55	FMP	TP+65		
27472	0	60100	0	34052	1689	+56	STQ	TP+77	T8	
27473	0	60100	0	34053	1690	+57	STQ	TP+78	T11	
27474	0	50000	0	47400	1691	+58	LDQ	PR+47	MH8(1)	EQN PT41
27475	0	26000	0	47400	1692	+59	FMP	PR+47		
27476	0	13100	0	00000	1693	+60	XCA			
27477	0	24000	0	32760	1694	+61	FMP	C+9		
27500	0	30000	0	40213	1695	+62	FAD	FL1		
27501	0	60100	0	33737	1696	+63	STQ	TP+2		
27502	0	50000	0	34052	1697	+64	CLA	TP+77		
27503	0	24100	0	33737	1698	+65	FDP	TP+2		
27504	-0	60000	0	47355	1699	+66	STQ	PR+28	T8 STATIC, ASSUME MH8 SAME AS TIME 1	
27505	0	07400	4	27034	1700	+67	TSX	AZQ,4	P8 STATIC	EQN PT42
27506	0	00000	0	36175	1701	+68	PZE	DRH		
27507	0	50000	0	33737	1702	+69	CLA	TP+2		
27510	0	50000	0	32764	1703	+70	LDQ	C+13	MACH NO. TERM	EQN PT43
27511	0	07400	4	27021	1704	+71	TSX	AZE,4		

27512	0	13100	0	00000	1705	+72	XCA			
27513	0	24000	0	47324	1706	+73	FMP	PR+3	P8 STATIC	
27514	0	60100	0	34043	1707	+74	STQ	TP+70	P8 STAGNATION	
27515	0	50000	0	34052	1708	+75	LDQ	TP+77	T8	EQN PT29
27516	0	26000	0	34033	1709	+76	FMP	TP+62		
27517	0	07400	4	24364	1710	+77	TSX	SGRT,4		
27520	0	07400	4	42602	1711	+78	TSX	ERROR,4		
27521	0	13100	0	00000	1712	+79	XCA			
27522	0	24000	0	34051	1713	+80	FMP	TP+76		
27523	0	60100	0	34044	1714	+81	STQ	TP+71	P8 PRIME	
27524	0	07400	4	40640	1715	+82	TSX	RAP8,4		
27525	0	77400	4	00000	1716	AYAR	AXT	000,4		
27526	0	02000	4	00001	1717	+1	TRA	L,4		
27527	-0	62500	0	32733	1718	AYAL	STL	X+13		
27530	0	02000	0	27525	1719	+1	TRA	AYAR		

1721*REGION TO SOLVE FOR ACTUAL WORK IN THE PUMP AND TURBINE									
27531	0	63400	4	27641	1722	AYB	SKA	AYBR,4	
27532	0	50000	1	27643	1723	+1	CLA*	AYBT,1	T11
27533	0	07400	4	24364	1724	+2	TSX	SGRT,4	EQN PT7
27534	0	07400	4	42602	1725	+3	TSX	ERROR,4	
27535	0	60100	0	34006	1726	+4	STO	TP+41	
27536	0	52000	0	32742	1727	+5	ZET	X+20	
27537	0	02000	0	27647	1728	+6	TRA	AYB2	P11 GIVEN
27540	0	24100	0	34037	1729	+7	FDP	TP+66	K T
27541	0	26000	1	27645	1730	+8	FMP*	AYBM,1	WOOTY
27542	0	60100	0	32662	1731	+9	STO	P+36	P11
27543	0	60000	1	32740	1732	AYB1	ST2	X+18,1	ERROR FLAGS
27544	0	24100	0	40224	1733	+1	FDP	FL10	
27545	-0	60000	0	32664	1734	+2	STQ	P+38	P12 GUESS = P11/10
27546	0	50000	1	32665	1735	+3	CLA	P+39,1	EQN PT8
27547	0	24100	0	34006	1736	+4	FDP	TP+41	
27550	0	13100	0	00000	1737	+5	XCA		
27551	0	07400	4	30516	1738	+6	TSX	AYJ,4	
27552	0	60100	0	34003	1739	+7	STQ	TP+38	ETAT PRIME
27553	0	50000	1	27643	1740	+8	CLA*	AYJ,1	T11
27554	0	50000	0	32662	1741	+9	LDQ	P+3	EQN PT9A
27555	-0	60000	0	40632	1742	+10	STQ	NEWB9	P11
27556	0	60000	0	40633	1743	+11	ST2	NEWB9+1	
27557	0	07400	4	25564	1744	+12	TSX	AZN,4	
27560	0	07400	4	42602	1745	+13	TSX	ERROR,4	
27561	0	50000	0	32750	1746	+14	CLA	C+1	R/776
27562	0	24100	0	33731	1747	+15	FDP	MPR+7	CP(T11,P11)
27563	-0	60000	0	34012	1748	+16	STQ	TP+45	
27564	0	50000	0	36113	1749	+17	CLA	DP12E	P12 EPSILON
27565	0	07400	4	40547	1750	+18	TSX	NEWB,4	
27566	0	34011	0	32664	1751	+19	PZE	P+38,TP+44	
27567	0	00062	0	34013	1752	+20	PZE	TP+46,,50	
27570	0	02000	0	27655	1753	+21	TRA	AYB3	
27571	0	50000	0	32664	1754	+22	CLA	P+38	P12
27572	0	24100	0	32662	1755	+23	FDP	P+36	P11
27573	-0	60000	0	34013	1756	+24	STQ	TP+46	
27574	0	13100	0	00000	1757	+25	XCA		

27375	0	54000	0	34012	1758	+26	LDC	TP+45			
27376	0	07400	4	27021	1759	+27	TSX	AZE,4			
27377	0	60100	0	12512	1760	+28	STQ	COMMON			
27600	0	13100	0	00000	1761	+29	XCA		PRESS RATIO	EQN PT44	
27601	0	26060	1	27643	1762	+30	FMP	AYBT,1	T11		
27602	0	60100	0	34001	1763	+31	STQ	TP+36	T12		
27603	0	30240	1	27643	1764	+32	FSD	AYBT,1	T11		
27604	0	60100	0	12513	1765	+33	STQ	COMMON+1	T12-T11	EQN PT45	
27605	0	50200	0	32766	1766	+34	CLS	C+15			
27606	0	24100	0	12513	1767	+35	FDP	COMMON+1			
27607	0	26000	0	40240	1768	+36	FMP	FLR0			
27610	0	24100	0	33731	1769	+37	FDP	WPR+7	CSUBP		
27611	0	26000	0	34001	1770	+38	FMP	TP+36	T12		
27612	0	30000	0	40213	1771	+39	FAD	FL1			
27613	0	13100	0	00000	1772	+40	XCA				
27614	0	26000	0	34003	1773	+41	FMP	TP+38			
27615	0	60100	0	34010	1774	+42	STQ	TP+43			
27616	0	50000	0	12512	1775	+43	CLA	COMMON	ETAT		
27617	0	30200	0	40213	1776	+44	FSD	FL1	PRESS RATIO	EQN PT9	
27620	0	13100	0	00000	1777	+45	XCA				
27621	0	26000	0	34010	1778	+46	FMP	TP+43	ETA 7		
27622	0	60100	0	34014	1779	+47	STQ	TP+47			
27623	0	30000	0	40213	1780	+48	FAD	FL1			
27624	0	07400	4	24364	1781	+49	TSX	SORT,4			
27625	0	07400	4	42602	1782	+50	TSX	ERROR,4			
27626	0	24100	0	32747	1783	+51	FDP	C	K T TERM		
27627	-0	60000	0	34011	1784	+52	STQ	TP+44	P12/P11 PRIME		
27630	0	07400	4	40640	1785	+53	TSX	RAPD,4			
27631	0	50200	0	34014	1786		CLS	TP+47			
27632	0	13100	0	00000	1787	+1	XCA				
27633	0	26060	1	27645	1788	+2	FMP	AYBM,1	WOOTY		
27634	0	13100	0	00000	1789	+3	XCA				
27635	0	26000	0	33731	1790	+4	FMP	WPR+7	CP(T11,P11)		
27636	0	13100	0	00000	1791	+5	XCA				
27637	0	26060	1	27643	1792	+6	FMP	AYBT,1			
27640	0	60100	1	32671	1793	+7	STQ	P+43,1	WTACT		
27641	0	77400	4	00000	1794		AXT	000,4			
27642	0	02000	4	00001	1795	+1	TRA	1,4			
27643	0	00000	0	32643	1796		PZE	P+37			
27644	0	00000	0	34053	1797	+1	PZE	TP+78			
27645	0	00000	0	32647	1798		PZE	P+25			
27646	0	00000	0	34051	1799	+1	PZE	TP+76			
27647	0	50000	0	32662	1800		CLA	P+36	P11		
27650	0	24100	0	34006	1801	+1	FDP	TP+41			
27651	0	26000	0	34037	1802	+2	FMP	TP+66	KT		
27652	0	60140	1	27645	1803	+3	STQ	AYBM,1	WOOT		
27653	0	50000	0	32662	1804	+4	CLA	P+36			
27654	0	02000	0	27543	1805	+5	TRA	AYB1			
27655	-0	62500	1	32740	1806		STL	X+18,1			
27656	0	02000	0	27631	1807	+1	TRA	AYB4			

1809*REGION TO COMPUTE PROGRAM CONSTANTS

27660	0	50000	0	36133	1811	+1	CLA	DK			
27661	0	30200	0	40213	1812	+2	FSD	FL1			
27662	0	60100	0	12512	1813	+3	STQ	COMMON	K-1		
27663	0	30000	0	40214	1814	+4	FAD	FL2			
27664	0	60100	0	12513	1815	+5	STQ	COMMON+1	K+1		
27665	0	24100	0	12512	1816	+6	FDP	COMMON			
27666	-0	60000	0	12514	1817	+7	STQ	COMMON+2	K+1/K-1		
27667	0	50000	0	36133	1818	+8	CLA	DK			
27670	0	24100	0	12513	1819	+9	FDP	COMMON+1			
27671	-0	60000	0	32766	1820	+10	STQ	C+15	K/(K+1)		
27672	0	50000	0	40214	1821	+11	CLA	FL2			
27673	0	24100	0	12513	1822	+12	FDP	COMMON+1			
27674	0	13100	0	00000	1823	+13	XCA				
27675	0	54000	0	12514	1824	+14	LDC	COMMON+2			
27676	0	07400	4	27021	1825	+15	TSX	AZE,4			
27677	0	24100	0	40225	1826	+16	FDP	FL12			
27700	0	26000	0	40236	1827	+17	FMP	FLG	GRAY		
27701	0	24100	0	40237	1828	+18	FDP	FLR			
27702	0	26000	0	36133	1829	+19	FMP	DK			
27703	0	07400	4	24364	1830	+20	TSX	SORT,4			
27704	0	07400	4	42602	1831	+21	TSX	ERROR,4			
27705	0	60100	0	34037	1832	+22	STQ	TP+66			
27706	0	56000	0	36140	1833	+23	LDC	DDTN			
27707	0	07400	4	30047	1834	+24	TSX	AYCA,4			
27710	0	60100	0	47431	1835	+25	STQ	PR+72	ATN FOR MB		
27711	0	13100	0	00000	1836	+26	XCA				
27712	0	26000	0	34037	1837	+27	FMP	TP+66			
27713	0	60100	0	34037	1838	+28	STQ	TP+66	KT		
27714	0	56000	0	36141	1839	+29	LDC	DDTN			
27715	0	07400	4	30047	1840	+30	TSX	AYCA,4			
27716	0	24100	0	34037	1841	+31	FDP	TP+66			
27717	0	26000	0	40241	1842	+32	FMP	FL139			
27720	0	13100	0	00000	1843	+33	XCA				
27721	0	26000	0	40214	1844	+34	FMP	FL2			
27722	0	60100	0	32747	1845	+35	STQ	C			
27723	0	50000	0	40237	1846	+36	CLA	FLR			
27724	0	24100	0	40242	1847	+37	FDP	FL776			
27725	-0	60000	0	32750	1848	+38	STQ	C+1	R/776		
27726	0	50000	0	40275	1849	+39	CLA	PI			
27727	0	24100	0	40246	1850	+40	FDP	FL108			
27730	0	26000	0	40275	1851	+41	FMP	PI			
27731	0	24100	0	40242	1852	+42	FDP	FL776			
27732	0	26000	0	36142	1853	+43	FMP	DIPY			
27733	0	24100	0	40236	1854	+44	FDP	FLG			
27734	-0	60000	0	32751	1855	+45	STQ	C+2			
27735	0	50000	0	40213	1856	+46	CLA	FL1			
27736	0	24100	0	40243	1857	+47	FDP	FLGAL			
27737	0	13100	0	00000	1858	+48	XCA				
27740	0	24100	0	40245	1859	+49	FDP	FLCUF			
27741	-0	60000	0	32752	1860	+50	STQ	C+3			
27742	0	50000	0	40237	1861	+51	CLA	FLR			
27743	0	24100	0	40244	1862	+52	FDP	FL144			
27744	0	26000	0	40247	1863	+53	FMP	FL2RM			
27745	0	60100	0	32753	1864	+54	STQ	C+4			

27746	0	50000	0	40234	1865	+55	CLA	FLR	
27747	0	24100	0	40236	1866	+56	FDP	FLG	
27750	0	26000	0	40225	1867	+57	FMP	FL12	
27751	0	60100	0	32754	1868	+58	STQ	C+5	
27752	0	56000	0	36137	1869	+59	LDQ	DDTL	
27753	0	07400	4	30047	1870	+60	TSX	AYCA,4	
27754	0	60100	0	32755	1871	+61	STQ	C+6	
27755	0	13100	0	00000	1872	+62	XCA		
27756	0	26000	0	32755	1873	+63	FMP	C+6	
27757	0	60100	0	32755	1874	+64	STQ	C+6	
27760	0	56000	0	40225	1875	+65	LDQ	FL12	
27761	0	26000	0	40242	1876	+66	FMP	FL776	
27762	0	60100	0	32756	1877	+67	STQ	C+7	
27763	0	56000	0	36135	1878	+68	LDQ	DD2	
27764	0	07400	4	30047	1879	+69	TSX	AYCA,4	EON T2A
27765	0	60100	0	12515	1880	+70	STQ	COMMON+3	
27766	0	50200	0	36134	1881	+71	CLS	DK2	
27767	0	24100	0	12515	1882	+72	FDP	COMMON+3	
27770	0	13100	0	00000	1883	+73	XCA		
27771	0	24100	0	12515	1884	+74	FDP	COMMON+3	
27772	0	13100	0	00000	1885	+75	XCA		
27773	0	24100	0	40236	1886	+76	FDP	FLG	
27774	0	13100	0	00000	1887	+77	XCA		
27775	0	24100	0	40214	1888	+78	FDP	FL2	
27776	-0	60000	0	32757	1889	+79	STQ	C+8	
27777	0	50000	0	36176	1890	+80	CLA	DK11	
30000	0	30000	0	36177	1891	+81	FAD	DK9	
30001	0	24100	0	32755	1892	+82	FDP	C+6	
30002	0	26000	0	32754	1893	+83	FMP	C+5	
30003	0	60100	0	34032	1894	+84	STQ	TP+61	
30004	0	50000	0	36167	1895	+85	CLA	DKPHM	
30005	0	30200	0	40213	1896	+86	FSB	FL1	
30006	0	60100	0	12516	1897	+87	STQ	COMMON+4	
30007	0	24100	0	40214	1898	+88	FDP	FL2	
30010	-0	60000	0	32760	1899	+89	STQ	C+9	(K-1)/2
30011	0	50000	0	36167	1900	+90	CLA	DKPHM	
30012	0	24100	0	12516	1901	+91	FDP	COMMON+4	
30013	-0	60000	0	32764	1902	+92	STQ	C+13	
30014	0	56000	0	36136	1903	+93	LDQ	DDH	
30015	0	07400	4	30047	1904	+94	TSX	AYCA,4	
30016	0	13100	0	00000	1905	+95	XCA		
30017	0	26000	0	40272	1906	+96	FMP	FLGF	
30020	0	60100	0	32761	1907	+97	STQ	C+10	G*AH
30021	0	56000	0	36154	1908	+98	LDQ	DTMET	
30022	0	26000	0	40277	1909	+99	FMP	RAD	
30023	0	07400	4	42374	1910	+100	TSX	COS,4	
30024	0	60100	0	32765	1911	+101	STQ	C+14	COS TETA
30025	0	56000	0	36150	1912	+102	LDQ	DDCO	
30026	0	07400	4	30047	1913	+103	TSX	AYCA,4	
30027	0	13100	0	00000	1914	+104	XCA		
30030	0	26000	0	36151	1915	+105	FMP	DNH	
30031	0	13100	0	00000	1916	+106	XCA		
30032	0	26000	0	32765	1917	+107	FMP	C+14	
30033	0	13100	0	00000	1918	+108	XCA		

30034	0	26000	0	40272	1919	+109	FMP	FLGF	
30035	0	60100	0	32762	1920	+110	STQ	C+11	G*ACN+COS(THETA)
30036	0	56000	0	36165	1921	+111	LDQ	DFHOT	
30037	0	26000	0	40275	1922	+112	FMP	PI	
30040	0	24100	0	40214	1923	+113	FDP	FL2	
30041	0	26000	0	36136	1924	+114	FMP	DDH	
30042	0	13100	0	00000	1925	+115	XCA		
30043	0	26000	0	36146	1926	+116	FMP	DL	
30044	0	60100	0	32763	1927	+117	STQ	C+12	F*PI*DH*L/2
30045	0	77400	4	00000	1928	AYCR	AXT	**0,4	
30046	0	02000	4	00001	1929	+1	TRA	L,4	

30047	-0	60000	0	30054	1932	AYCA	STQ	AYCA1	1931*REGION TO COMPUTE AREA FROM DIAMETER
30050	0	26000	0	30054	1933	+1	FMP	AYCA1	
30051	0	24100	0	40216	1934	+2	FDP	FL4	
30052	0	26000	0	40275	1935	+3	FMP	PI	
30053	0	02000	4	00001	1936	+4	TRA	L,4	
				30054	1937	AYCA1	BSS	L,F	

30055	0	63400	4	30142	1940	AYD	SXA	AYDR,4	1939*REGION TO COMPUTE PUMP FLOW
30056	0	60000	0	32736	1941	+1	STZ	X+16	
30057	0	50000	0	40305	1942	+2	CLA	BIG	
30060	0	60100	0	40632	1943	+3	STQ	NEWB9	
30061	0	60000	0	40633	1944	+4	STZ	NEWB9+1	
30062	0	56000	0	32666	1945	+5	LDQ	P+40	N I+1
30063	0	26000	0	30154	1946	+6	FMP	AYD01	
30064	0	60100	0	32700	1947	+7	STQ	P+50	
30065	0	50000	0	36144	1948	+8	CLA	DHE	Q/N GUESS = .37
30066	0	07400	4	40547	1949	+9	TSX	NEWB,4	
30067	0	32676	0	32700	1950	+10	PZE	P+50, P+48	
30070	0	00031	0	34027	1951	+11	PZE	TP+58, +25	
30071	0	02000	0	30147	1952	+12	TRA	AYD2	
30072	0	56000	0	32700	1953	+13	LDQ	P+50	EON PT18
30073	0	26000	0	34017	1954	+14	FMP	TP+50	RH01
30074	0	24100	0	32752	1955	+15	FDP	C+3	
30075	-0	60000	0	32677	1956	+16	STQ	P+49	WDDTP(I+1)
30076	0	26000	0	32673	1957	+17	FMP	P+45	ALPHA
30077	0	30000	0	32632	1958	+18	FAD	P+12	BETA
30100	0	13100	0	00000	1959	+19	XCA		EON PT17
30101	0	26000	0	32677	1960	+20	FMP	P+49	
30102	0	60100	0	32674	1961	+21	STQ	P+46	
30103	0	07400	4	30437	1962	+22	TSX	AYI,4	P2(I+1)
30104	0	60100	0	32675	1963	+23	STQ	P+47	FIND T2 ISOENTROPICALLY
30105	0	56000	0	32674	1964	+24	LDQ	P+46	T2(I+1)
30106	0	07400	4	25564	1965	+25	TSX	AZH,4	
30107	0	02000	0	30151	1966	+26	TRA	AYD1	
30110	0	50000	0	33724	1967	+27	CLA	WPR+2	H2(I+1)
30111	0	30200	0	34070	1968	+28	FSB	TP+91	H1(I+1)
30112	0	60100	0	34056	1969	+29	STQ	TP+81	
30113	0	13100	0	00000	1970	+30	XCA		
30114	0	26000	0	40242	1971	+31	FMP	FL776	

30115	0	30000	0	40264	1972	+32	FAD	FL100		
30116	0	60100	0	32676	1973	+33	STO	P+48		DELTA H (1+1)
30117	0	10000	0	30121	1974	+34	TSE	P+2		
30120	-0	12000	0	40627	1975	+35	TRI	BDNB	P2 TOO LOW	
30121	0	50000	0	32700	1976	+36	CLA	P+50	Q	EQN PT19
30122	0	24100	0	32644	1977	+37	FDP	P+40	N	
30123	-0	60000	0	34000	1978	+38	STQ	TP+35	Q/N	
30124	0	50000	0	32634	1979	+39	CLA	P+14	MSV	
30125	0	24100	0	32644	1980	+40	FDP	P+40	N	
30126	0	13100	0	00000	1981	+41	XCA			
30127	0	24100	0	32644	1982	+42	FDP	P+40		
30130	-0	60000	0	33773	1983	+43	STQ	TP+30		
30131	0	07401	4	30527	1984	+44	TSX	AYK,4,1	MSV/MSQ.	
30132	0	00000	0	34017	1985	+45	PZE	TP+50,0		
30133	0	13100	0	00000	1986	+46	XCA			EQN PT20
30134	0	26000	0	32644	1987	+47	FMP	P+40		
30135	0	13100	0	00000	1988	+48	XCA			
30136	0	26000	0	32644	1989	+49	FMP	P+40		
30137	0	30000	0	40264	1990	+50	FAD	FL100		
30140	0	60100	0	34027	1991	+51	STO	TP+58		
30141	0	07400	4	40640	1992	+52	TSX	RAPB,4		
30142	0	77400	4	00000	1993		AYDR	AXT		
30143	0	50000	0	32676	1994	+1	CLA	P+48		
30144	0	30200	0	40264	1995	+2	FSB	FL100		
30145	0	60100	0	32676	1996	+3	STO	P+4P		
30146	0	02000	4	00001	1997	+4	TRA	1,4		
30147	-0	62500	0	32736	1998		AYD2	STL	X+16	
30150	0	02000	0	30142	1999	+1	TRA	AYDR		
30151	-0	73400	4	00000	2000		AYD1	PDX	,4	
30152	-3	00001	4	40624	2001	+1	TXL	BDXB,4,1		P2 TOO HIGH
30153	0	02000	0	40627	2002	+2	TRA	BDNB		T2 TOO LOW
30154	1	77572	7	02437	2003		AYD01	DEC	.37	

30155	0	63400	4	30173	2004		2005*REGION TO FIND INLET VALUES FOR ONE PART AT ONE TIME			
30156	0	50000	0	32621	2007	+1	CLA	P+3		
30157	0	60100	1	35612	2008	+2	STO	PT,1		INLET PRESSURE
30160	0	50000	0	32631	2009	+3	CLA	P+11		
30161	0	60100	1	35624	2010	+4	STO	PT+10,1		INLET FLOW
30162	0	07400	4	27075	2011	+5	TSX	AZU,4,0		
30163	0	02000	0	30177	2012	+6	TRA	AYE1		
30164	0	02000	0	30175	2013	+7	TRA	AYE2		
30165	-0	52000	1	34072	2014	+8	NZT	DKDPI,1		
30166	0	02000	0	30173	2015	+9	TRA	AYER		
30167	0	07400	4	31674	2016	+10	TSX	AYG,4,0		ORFICE DROP
30170	0	02000	0	30177	2017	+11	TRA	AYE1		ERROR RETN
30171	0	50000	0	12512	2018	+12	CLA	COMMON		
30172	0	60100	1	35614	2019	+13	STO	PT+4,1		
30173	0	77400	4	00000	2020		AYER	AXT		
30174	0	02000	4	00003	2021	+1	TRA	3,4		
30175	0	52200	0	30173	2022		AYER2	XEC	AYER	
30176	0	02000	4	00002	2023	+1	TRA	2,4		
30177	0	02000	4	00002	2023		AY			

30200	0	02000	4	00001	2025	+1	TRA	1,4		
30201	0	63400 <td>4</td> <td>30173</td> <td>2026</td> <td></td> <td>AYERA</td> <td>SXA</td> <td>AYER,4</td> <td></td>	4	30173	2026		AYERA	SXA	AYER,4	
30202	-0	52000	1	36073	2029	+1	NZT	DKDPI,1		
30203	0	02000	0	30210	2030	+2	TRA	AYERA1		
30204	0	07401	4	31674	2031	+3	TSX	AYG,4,1		ORFICE DROP
30205	0	02000	0	30177	2032	+4	TRA	AYER1		EQN HT12
30206	0	50000	0	12512	2033	+5	CLA	COMMON		
30207	0	60100	1	35617	2034	+6	STO	PT+5,1		
30210	0	50000	0	32621	2035		AYERA1	CLA	P+3	
30211	0	60100	1	35613	2036	+1	STO	PT+1,1		OUTLET PRESSURE
30212	0	07401	4	27075	2037	+2	TSX	AZU,4,1		
30213	0	02000	0	30177	2038	+3	TRA	AYER1		
30214	0	02000	0	30175	2039	+4	TRA	AYER2		
30215	0	50000	0	32631	2040	+5	CLA	P+11		
30216	0	60100	1	35614	2041	+6	STO	PT+2,1		
30217	0	02000	0	30173	2042	+7	TRA	AYER		

30220	0	63400	4	30324	2045		2044*REGION TO COMPUTE SEVERAL QUANTITIES FOR TIME I			
30221	0	54000	0	32655	2046	+1	LDQ	P+31		
30222	0	26000	0	32644	2047	+2	FMP	P+22	T2	EQN 27
30223	0	60100	0	34047	2048	+3	STO	TP+74	WDOOTC	
30224	0	54000	0	32633	2049	+4	LDQ	P+13	T6	
30225	0	26000	0	32645	2050	+5	FMP	P+23	WDOOT H	
30226	0	30000	0	34047	2051	+6	FAD	TP+74		
30227	0	60100	0	34050	2052	+7	STO	TP+75		
30230	0	50000	0	32645	2053	+8	CLA	P+23	WDOOTH	EQN 27A
30231	0	30000	0	32644	2054	+9	FAD	P+22	WDOOTC	
30232	0	60100	0	32647	2055	+10	STO	P+25	WDOOT	
30233	0	24100	0	34050	2056	+11	FDP	TP+75		
30234	0	26000	0	32641	2057	+12	FMP	P+35	T8	
30235	0	60100	0	34036	2058	+13	STO	TP+65	K6	
30236	0	50000	0	32654	2059	+14	CLA	P+30	P2	EQN PT36
30237	0	30200	0	47333	2060	+15	FSB	PR+10	PHN	
30240	0	07400	4	24364	2061	+16	TSX	SQRT,4		
30241	0	07400	4	42602	2062	+17	TSX	ERROR,4		
30242	0	60100	0	12512	2063	+18	STO	COMMON		
30243	0	50000	0	32644	2064	+19	CLA	P+22	WDOOTC	
30244	0	24100	0	12512	2065	+20	FDP	COMMON		
30245	-0	60000	0	33740	2066	+21	STQ	TP+3	K10	
30246	0	50000	0	32656	2067	+22	CLA	P+32	P6	EQN PT35
30247	0	30200	0	47333	2068	+23	FSB	PR+10		
30250	0	07400	4	24364	2069	+24	TSX	SQRT,4		
30251	0	07400	4	42602	2070	+25	TSX	ERROR,4		
30252	0	60100	0	12512	2071	+26	STO	COMMON		
30253	0	50000	0	32645	2072	+27	CLA	P+23	WDOOTH	
30254	0	24100	0	12512	2073	+28	FDP	COMMON		
30255	-0	60000	0	33753	2074	+29	STQ	TP+14	K11	
30256	0	50000	0	32647	2075	+30	CLA	P+25	WDOOT	EQN PT37
30257	0	24100	0	47447	2076	+31	FDP	PR+86	V8	
30260	-0	60000	0	33754	2077	+32	STQ	TP+15	K12	

30261	0	50000	0	32648	2078	+33	CLA	P+23	WOOTH	EQN PT38
30262	0	24100	0	47444	2079	+34	FDP	PR+85	VHM	
30263	-0	60000	0	33755	2080	+35	STQ	TP+16	K13	
30264	0	50000	0	32644	2081	+36	CLA	P+22	WOOTC	EQN PT39
30265	0	24100	0	47445	2082	+37	FDP	PR+84	VCM	
30266	-0	60000	0	33762	2083	+38	STQ	TP+21	K14	
30267	0	50000	0	32654	2084	+39	CLA	P+30	P2	EQN PT40
30270	0	30200	0	47332	2085	+40	FSB	PR+9		
30271	0	07400	4	24344	2086	+41	TSX	SOFT,4		
30272	0	07400	4	42402	2087	+42	TSX	ERROR,4		
30273	0	60100	0	12512	2088	+43	STQ	COMMON		
30274	0	50000	0	32644	2089	+44	CLA	P+22		
30275	0	24100	0	12512	2090	+45	FDP	COMMON		
30276	-0	60000	0	33763	2091	+46	STQ	TP+22	K15	
30277	0	54000	0	34131	2092	+47	LDQ	DAKV	EQN PT33	
30300	0	24000	0	34073	2093	+48	FMP	TP+94		
30301	0	30200	0	34132	2094	+49	FSB	DBKV		
30302	0	60100	0	34040	2095	+50	STQ	TP+67	KV(1+1)	
30303	0	50000	0	32753	2096	+51	CLA	C+4	4GR/12	EQN 30A
30304	0	24100	0	34040	2097	+52	FDP	TP+67		
30305	0	13100	0	00000	2098	+53	XCA			
30306	0	24100	0	34040	2099	+54	FDP	TP+67		
30307	-0	60000	0	34031	2100	+55	STQ	TP+60	K1	
30310	0	50000	0	40213	2101	+56	CLA	FL1	EQN 30	
30311	0	24100	0	34037	2102	+57	FDP	TP+66	K7	
30312	0	13100	0	00000	2103	+58	XCA			
30313	0	24100	0	34037	2104	+59	FDP	TP+66		
30314	0	13100	0	00000	2105	+60	XCA			
30315	0	30000	0	34031	2106	+61	FAD	TP+60	K1	
30316	0	30000	0	34032	2107	+62	FAD	TP+61	K2	
30317	0	60100	0	34033	2108	+63	STQ	TP+62	K3	
30320	0	50000	0	32641	2109	+64	CLA	P+35	T8	EQN 6
30321	0	60100	0	32643	2110	+65	STQ	P+37	T11	
30322	0	07400	4	27531	2111	+66	TSX	AYB,4	TIME 1	EQN PT7-10
30323	0	07400	4	31501	2112	+67	TSX	AYL,4		EQN PT21
30324	0	77400	4	00000	2113	AYGR	AXT	**0,4		
30325	0	07000	4	00001	2114	+1	TRA	L,4		

2116*REGION TO COMPUTE					ADDITIONAL QUANTITIES AT TIME 1					
30326	0	50000	0	32643	2117	AYGA	CLA	P+21	WOOTP	EQN PT18
30327	0	24100	0	34060	2118	+1	FDP	TP+83	RHO1	
30330	0	26000	0	32752	2119	+2	FMP	C+3		
30331	0	60100	0	34061	2120	+3	STQ	TP+84	QP(1)	
30332	0	24100	0	32645	2121	+4	FDP	P+39		
30333	-0	60000	0	34000	2122	+5	STQ	TP+35	Q/N	
30334	0	50000	0	32635	2123	+6	CLA	P+15		
30335	0	24100	0	32645	2124	+7	FDP	P+39		
30336	0	13100	0	00000	2125	+8	XCA			
30337	0	24100	0	32645	2126	+9	FDP	P+39		
30340	-0	60000	0	33773	2127	+10	STQ	TP+30	HSV/NSQ.	
30341	0	50000	0	32656	2128	+11	CLA	P+32	P6	EQN PT13
30342	0	24100	0	32643	2129	+12	FDP	P+21		
30343	-0	60000	0	32632	2130	+13	STQ	P+12	BETA	
30344	0	30000	0	32654	2131	+14	CLA	P+22	EQN PT14	

30345	0	30200	0	32656	2132	+15	FSB	P+32	P6	
30346	0	24100	0	32643	2133	+16	FDP	P+21		
30347	0	13100	0	00000	2134	+17	XCA			
30350	0	24100	0	32643	2135	+18	FDP	P+21		
30351	-0	60000	0	32673	2136	+19	STQ	P+45	ALPHA	
30352	0	02000	4	00001	2137	+20	TRA	L,4		

2139*REGION TO COMPUTE FILM COEFFICIENT										
30353	0	63400	4	30430	2140	AYH	SXA	AYHR,4		
30354	0	63400	1	30431	2141	+1	SXA	AYHR+1,1		
30355	0	50000	0	32620	2142	+2	CLA	P+2	T	
30356	0	24140	4	00001	2143	+3	FDP	L,4	THETA	
30357	-0	50000	4	00001	2144	+4	CAL	L,4		
30360	-0	73700	1	00000	2145	+5	PDC	+1		
30361	0	13100	0	00000	2146	+6	XCA			
30362	0	56000	1	00000	2147	+7	LDQ	0,1	ALPHA	
30363	-0	12000	0	30433	2148	+8	TMI	AYH1		
30364	0	07400	4	27021	2149	+9	TSX	AZE,4		
30365	0	60100	0	12524	2150	+10	STQ	COMMON+10		
30366	0	50000	0	33741	2151	+11	CLA	TP+4		
30367	0	24100	0	33764	2152	+12	FDP	TP+23	D+DELZ	
30370	0	13100	0	00000	2153	+13	XCA			
30371	0	56000	1	00001	2154	+14	LDQ	L,1	BETA	
30372	-0	12000	0	30433	2155	+15	TMI	AYH1		
30373	0	07400	4	27021	2156	+16	TSX	AZE,4		
30374	0	60100	0	12525	2157	+17	STQ	COMMON+11		
30375	0	50000	0	32631	2158	+18	CLA	P+11	WOOT	
30376	0	36100	0	40302	2159	+19	ACL	288		
30377	0	24100	0	33760	2160	+20	FDP	TP+19	F	
30400	0	13100	0	00000	2161	+21	XCA			
30401	0	24100	0	33733	2162	+22	FDP	WPR+9		
30402	0	13100	0	00000	2163	+23	XCA			
30403	0	56000	0	40256	2164	+24	LDQ	FL,8		
30404	-0	12000	0	30433	2165	+25	TMI	AYH1		
30405	0	07400	4	27021	2166	+26	TSX	AZE,4		
30406	0	60100	0	12526	2167	+27	STQ	COMMON+12		
30407	0	50000	0	33731	2168	+28	CLA	WPR+7		
30410	0	24100	0	33732	2169	+29	FDP	WPR+8		
30411	0	26000	0	33733	2170	+30	FMP	WPR+9		
30412	0	56000	0	40226	2171	+31	LDQ	FL,4		
30413	-0	12000	0	30433	2172	+32	TMI	AYH1		
30414	0	07400	4	27021	2173	+33	TSX	AZE,4		
30415	0	13100	0	00000	2174	+34	XCA			
30416	0	26000	0	12526	2175	+35	FMP	COMMON+12		
30417	0	24100	0	33741	2176	+36	FDP	TP+4	D	
30420	0	26000	0	12524	2177	+37	FMP	COMMON+10		
30421	0	13100	0	00000	2178	+38	XCA			
30422	0	26000	0	12525	2179	+39	FMP	COMMON+11		
30423	0	13100	0	00000	2180	+40	XCA			
30424	0	26000	0	33732	2181	+41	FMP	WPR+8	K	
30425	0	13100	0	00000	2182	+42	XCA			
30426	0	26000	1	00002	2183	+43	FMP	2,1	GAMMA	
30427	0	60100	0	32622	2184	+44	STQ	P+4	MF	

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30430 0 77400 4 00000 2185 AYMR AXT 000,4
30431 0 77400 1 00000 2186 +1 AXT 000,1
30432 0 02000 4 00002 2187 +2 TRA 2,4
30433 -1 30434 0 25417 2188 AYH1 STR AZPF,,AYH2
30434 2 33025 2 34260 2189 AYH2 BCI 3,CHECK DUMP FOR NEG
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2191*REGION TO COMPUTE TEMP CHANGE IN AN ISOENTROPIC PRESS CHANGE
30437 0 63400 4 30450 2192 AYI SXA AYIR,4
30440 0 60100 0 34016 2193 +1 STO TP+49 P2
30441 0 50000 0 34065 2194 +2 CLA TP+88 T1
30442 0 54000 0 32674 2195 +3 LDQ P+46 P2
30443 0 07400 4 41043 2196 +4 TSX S(TP),4
30444 0 30200 0 34062 2197 +5 FSB TP+85 S
30445 0 24100 0 34005 2198 +6 FDP TP+40 S-SP
30446 0 26000 0 30452 2199 +7 FMP AYI1 DELT
30447 0 30000 0 34065 2200 +8 FAD TP+88 T1
30450 0 77400 4 00000 2201 AYIR AXT 000,4
30451 0 02000 4 00001 2202 +1 TRA 1,4
30452 2 02400 0 00000 2203 AYI1 DEC 2.
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2205*REGION TO COMPUTE CONSTANT ENTROPIES FOR AYI
30453 0 63400 4 30511 2206 AYI1 SXA AYIIR,4
30454 0 50000 0 34065 2207 +1 CLA TP+88 T1
30455 0 54000 0 34064 2208 +2 LDQ TP+87 P1
30456 0 07400 4 41043 2209 +3 TSX S(TP),4
30457 0 60100 0 34062 2210 +4 STO TP+85 S
30460 0 50000 0 34065 2211 +5 CLA TP+88 T1(I+1)
30461 0 60100 0 33742 2212 +6 STO TP+5 P1(I+1)
30462 0 54000 0 34064 2213 +7 LDQ TP+87
30463 0 07400 4 25564 2214 +8 TSX AZH,4
30464 -1 25176 0 25417 2215 +9 STR AZFF,,AZAB2
30465 0 50000 0 33730 2216 +10 CLA WPR+6
30466 0 60100 0 34017 2217 AYI11 STO TP+50
30467 0 50000 0 33724 2218 +1 CLA WPR+2
30470 0 60100 0 34070 2219 +2 STO TP+91 H1(I+1)
30471 0 50000 0 34065 2220 +3 CLA TP+88 T1
30472 0 30000 0 30452 2221 +4 FAD AYI1 DELT
30473 0 54000 0 34064 2222 +5 LDQ TP+87 P1
30474 0 07400 4 41043 2223 +6 TSX S(TP),4
30475 0 30200 0 34062 2224 +7 FSB TP+85 S
30476 0 76000 0 00002 2225 +8 CMS
30477 0 60100 0 34005 2226 +9 SYO TP+40 S-SP
30500 0 07400 4 27142 2227 +10 TSX AZV,4 VAPOR PRESSURE
30501 0 30200 0 34064 2228 +11 FSB TP+87 P1
30502 -0 12000 0 30504 2229 +12 TMI *+2
30503 -1 30513 0 25417 2230 +13 STR AZFF,,AYI12
30504 0 76000 0 00002 2231 +14 CMS
30505 0 24100 0 34017 2232 +15 FDP TP+50 RHQ1
30506 0 13100 0 00000 2233 +16 XCA
30507 0 24100 0 40225 2234 +17 FDP FL12
30510 -0 60000 0 32636 2235 +18 STO P+16 HSV(I+1)
30511 0 77400 4 00000 2236 AYIIR AXT 000,4
30512 0 02000 0 00001 2237 +1 TRA 1,4
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30513 2 72162 6 02163 2238 AYI12 BCI 3,GAS AT PUMP INLET
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2240*REGION TO COMPUTE ETA T -- N/ROOT T IN AC
30516 0 60100 0 34023 2241 AYJ STO TP+54
30517 0 54000 0 30525 2242 +1 LDQ AYJ1
30520 0 26000 0 34023 2243 +2 FMP TP+54
30521 0 30000 0 30526 2244 +3 FAD AYJ1+1
30522 0 13100 0 00000 2245 +4 XCA
30523 0 26000 0 34023 2246 +5 FMP TP+54
30524 0 02000 4 00001 2247 +6 TRA 1,4
30525 -1 54523 1 45747 2248 AYJ1 DEC -6318076E-13,11039226E-10
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2250*REGION TO COMPUTE PUMP CHARACTERISTICS
30527 0 63400 4 30603 2251 AYK SXA AYKR,4
30530 0 63400 1 30604 2252 +1 SXA AYKR+1,1
30531 0 44100 4 00000 2253 +2 LDI 0,4
30532 -0 05700 0 00002 2254 +3 RIL 2 RESET PARABOLA FLAG
30533 -0 77400 1 31023 2255 +4 AXK AYK1,1
30534 -0 05400 0 00001 2256 +5 LFT 1 1 IN DECREMENT OF TSX = HEAD DESIRED
30535 0 02000 0 31076 2257 +6 TRA AYK9 MARK 4 MOD 4 PUMP
30536 0 50000 0 33773 2258 +7 CLA TP+30 HSV/NSQ.
30537 0 54000 0 31065 2259 +8 LDQ AYK3 HSV/NSQ MAX
30540 0 04000 0 30542 2260 +9 TLQ *+2
30541 0 13100 0 00000 2261 +10 XCA
30542 0 26000 0 40235 2262 +11 FMP FL12E8
30543 0 13100 0 00000 2263 +12 XCA
30544 0 26060 4 00001 2264 +13 FMP+ 1,4 RHO
30545 0 30000 0 40214 2265 +14 FAD FL2
30546 0 60100 0 12512 2266 +15 STO COMMON
30547 0 50000 0 40213 2267 +16 CLA FL1
30550 0 24100 0 12512 2268 +17 FDP COMMON
30551 -0 60000 0 12512 2269 +18 STO COMMON X2
30552 0 50000 0 31066 2270 +19 CLA AYK3+1 .36
30553 0 30200 0 34000 2271 +20 FSB TP+35 Q/N
30554 0 60100 0 12513 2272 +21 STO COMMON+1 X1
30555 -0 12000 0 30606 2273 +22 TMI AYK4 IF PLUS USE -A- CURVE
30556 0 56000 1 00005 2274 +23 LDQ 5,1 A5
30557 0 26000 0 12512 2275 +24 FMP COMMON X2
30560 0 30000 1 00004 2276 +25 FAD 4,1 A4
30561 0 13100 0 00000 2277 +26 XCA
30562 0 26000 0 12513 2278 +27 FMP COMMON+1 X1
30563 0 60100 0 12514 2279 +28 STO COMMON+4
30564 0 56000 1 00003 2280 +29 LDQ 3,1 A3
30565 0 26000 0 12512 2281 +30 FMP COMMON
30566 0 30000 1 00001 2282 +31 FAD 1,1
30567 0 30000 0 12516 2283 +32 FAD COMMON+4
30570 0 13100 0 00000 2284 +33 XCA
30571 0 26000 0 12513 2285 +34 FMP COMMON+1 X1
30572 0 60100 0 12517 2286 +35 STO COMMON+5
30573 0 56000 1 00002 2287 +36 LDQ 2,1
30574 0 26000 0 12512 2288 +37 FMP COMMON .2
30575 0 30000 1 00000 2289 +38 FAD 0,1 A0
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30576	0	30000	0	12517	2290	+39	FAD	COMMON+5	
30577	-0	05600	0	00001	2291	AYK8	LNT	1	
30600	0	02000	0	30603	2292	+1	TRA	AYKR	..O-EFFICIENCY DESIRED
30601	0	24100	0	40234	2293	+2	FDP	PLIES	
30602	0	13100	0	00000	2294	+3	XCA		
30603	0	77400	4	00000	2295	AYKR	ANT	000,4	
30604	0	77400	1	00000	2296	+1	ANT	000,1	
30605	0	02000	4	00002	2297	+2	TRA	2,4	
30606	0	56000	0	31070	2298	AYK4	LDQ	AYK3+3	1.31
30607	0	26000	0	12512	2299	+1	FMP	COMMON	
30610	0	60100	0	12520	2300	+2	STO	COMMON+6	1.31X2
30611	0	50000	0	31067	2301	+3	CLA	AYK3+2	.9448
30612	0	30200	0	12520	2302	+4	FSB	COMMON+6	
30613	0	60100	0	12521	2303	+5	STO	COMMON+7	Q/N MAX
30614	0	13100	0	00000	2304	+6	XCA		
30615	0	26000	0	31071	2305	+7	FMP	AYK3+4	
30616	0	60100	0	12541	2306	+8	STO	COMMON+23	
30617	0	56000	0	34000	2307	+9	LDQ	TP+35	Q/N
30620	0	04000	0	30623	2308	+10	TLQ	AYK5	
30621	0	75400	0	00000	2309	+11	PXA	,0	
30622	0	02000	0	30603	2310	+12	TRA	AYKR	PUMP TOO SLOW TO PUMP
30623	-0	60000	0	12523	2311	AYK5	STQ	COMMON+9	Q/N PRIME
30624	0	56000	0	12521	2312	+1	LDQ	COMMON+7	
30625	0	26000	0	31072	2313	+2	FMP	AYK3+5	.95
30626	0	56000	0	34000	2314	+3	LDQ	TP+35	
30627	0	04000	0	30632	2315	+4	TLQ	AYK6	
30630	-0	05500	0	00002	2316	+5	SIL	2	
30631	0	60100	0	12523	2317	+6	STO	COMMON+9	Q/N PRIME = .9K(Q/N)MAX
30632	0	50000	0	31073	2318	AYK6	CLA	AYK3+6	.44
30633	0	04000	0	30636	2319	+1	TLQ	AYK7	
30634	-0	05500	0	00002	2320	+2	SIL	2	SET PARABOLA FLAG
30635	0	60100	0	12523	2321	+3	STO	COMMON+9	Q/N PRIME = .44
30636	0	50000	0	31066	2322	AYK7	CLA	AYK3+1	.36
30637	0	30200	0	12523	2323	+1	FSB	COMMON+9	Q/N PRIME
30640	0	60100	0	12513	2324	+2	STO	COMMON+1	X1
30641	0	30000	0	31074	2325	+3	FAD	AYK3+7	.5848
30642	0	30200	0	12520	2326	+4	FSB	COMMON+6	
30643	0	60100	0	12522	2327	+5	STO	COMMON+8	
30644	0	50000	0	12512	2328	+6	CLA	COMMON	X2
30645	0	24100	0	12520	2329	+7	FDP	COMMON+6	
30646	-0	60000	0	12514	2330	+8	STQ	COMMON+2	X3
30647	0	50000	0	12513	2331	+9	CLA	COMMON+1	X1
30650	0	30200	0	31075	2332	+10	FSB	AYK3+8	.02
30651	0	60100	0	12524	2333	+11	STQ	COMMON+10	
30652	0	56000	1	00020	2334	+12	LDQ	16,1	DD
30653	0	26000	0	12512	2335	+13	FMP	COMMON	
30654	0	30000	1	00017	2336	+14	FAD	15,1	
30655	0	60100	0	12525	2337	+15	STO	COMMON+11	
30656	0	56000	1	00014	2338	+16	LDQ	12,1	86
30657	0	26000	0	12512	2339	+17	FMP	COMMON	
30660	0	60100	0	12526	2340	+18	STO	COMMON+12	
30661	0	56000	1	00016	2341	+19	LDQ	14,1	88
30662	0	26000	0	12514	2342	+20	FMP	COMMON+2	X3
30663	0	00000	0	00000	2343				
30664	0	30000	0	12526	2344	+22	FAD	COMMON+12	
30665	0	30000	1	00013	2345	+23	FAD	11,1	85
30666	0	13100	0	00000	2346	+24	XCA		
30667	0	26000	0	12513	2347	+25	FMP	COMMON+1	X1
30670	0	30000	1	00007	2348	+26	FAD	7,1	81
30671	0	60100	0	12527	2349	+27	STQ	COMMON+13	
30672	0	56000	1	00012	2350	+28	LDQ	10,1	84
30673	0	26000	0	12512	2351	+29	FMP	COMMON	
30674	0	60100	0	12530	2352	+30	STO	COMMON+14	
30675	0	56000	1	00015	2353	+31	LDQ	13,1	87
30676	0	26000	0	12514	2354	+32	FMP	COMMON+2	
30677	0	60100	0	12534	2355	+33	STO	COMMON+18	
30700	0	30000	0	12530	2356	+34	FAD	COMMON+14	
30701	0	30000	0	12527	2357	+35	FAD	COMMON+13	
30702	0	13100	0	00000	2358	+36	XCA		
30703	0	26000	0	12513	2359	+37	FMP	COMMON+1	X1
30704	0	30000	1	00006	2360	+38	FAD	6,1	80
30705	0	60100	0	12531	2361	+39	STQ	COMMON+15	
30706	0	56000	1	00010	2362	+40	LDQ	8,1	82
30707	0	26000	0	12512	2363	+41	FMP	COMMON	
30710	0	60100	0	12532	2364	+42	STQ	COMMON+16	
30711	0	56000	1	00011	2365	+43	LDQ	9,1	
30712	0	26000	0	12514	2366	+44	FMP	COMMON+2	X3
30713	0	30000	0	12532	2367	+45	FAD	COMMON+16	
30714	0	30000	0	12531	2368	+46	FAD	COMMON+15	
30715	0	24100	0	12524	2369	+47	FDP	COMMON+10	
30716	0	26000	0	12513	2370	+48	FMP	COMMON+1	X1
30717	0	30000	0	12525	2371	+49	FAD	COMMON+11	
30720	-0	05600	0	00002	2372	+50	LNT	2	
30721	0	02000	0	30577	2373	+51	TRA	AYK8	IF PARABOLA FLAG IS OFF, EXIT
30722	0	60100	0	12537	2374	+52	STO	COMMON+21	
30723	0	50200	0	12514	2375	+53	CLS	COMMON+2	
30724	0	24100	0	12522	2376	+54	FDP	COMMON+8	
30725	-0	60000	0	12515	2377	+55	STQ	COMMON+3	X4
30726	0	26000	1	00011	2378	+56	FMP	9,1	
30727	0	60100	0	12536	2379	+57	STO	COMMON+20	
30730	0	56000	1	00016	2380	+58	LDQ	14,1	
30731	0	26000	0	12513	2381	+59	FMP	COMMON+1	
30732	0	30000	1	00015	2382	+60	FAD	13,1	87
30733	0	13100	0	00000	2383	+61	XCA		
30734	0	26000	0	12515	2384	+62	FMP	COMMON+3	X4
30735	0	60100	0	12535	2385	+63	STO	COMMON+19	
30736	0	50200	1	00013	2386	+64	CLS	11,1	85
30737	0	30200	0	12526	2387	+65	FSB	COMMON+12	
30740	0	30200	0	12533	2388	+66	FSB	COMMON+17	
30741	0	36100	0	40301	2389	+67	ACL	188	
30742	0	30000	0	12535	2390	+68	FAD	COMMON+19	
30743	0	13100	0	00000	2391	+69	XCA		
30744	0	26000	0	12513	2392	+70	FMP	COMMON+1	X1
30745	0	30200	1	00007	2393	+71	FSB	7,1	81
30746	0	30200	0	12530	2394	+72	FSB	COMMON+14	
30747	0	30200	0	12534	2395	+73	FSB	COMMON+18	
30750	0	30200	0	12536	2396	+74	FSB	COMMON+20	
30751	0	24100	0	12524	2397	+75	FDP	COMMON+10	

30752	0	26000	0	12513	2398	+76	FMP	COMMON+1	X1
30753	0	60100	0	12540	2399	+77	STO	COMMON+22	PARTIAL 2 WRT Q/N AT Q/N PRIME
30754	0	50000	0	12523	2400	+78	CLA	COMMON+9	0
30755	0	30200	0	12541	2401	+79	F38	COMMON+23	G
30756	0	60100	0	12542	2402	+80	STO	COMMON+24	
30757	0	13100	0	00000	2403	+81	XCA		
30760	0	26000	0	12542	2404	+82	FMP	COMMON+24	
30761	0	60100	0	12543	2405	+83	STO	COMMON+27	DENOMINATOR
30762	0	50200	0	12540	2406	+84	CLS	COMMON+22	E
30763	0	13100	0	00000	2407	+85	XCA		
30764	0	26000	0	12523	2408	+86	FMP	COMMON+9	D
30765	0	30000	0	12537	2409	+87	FAD	COMMON+21	F
30766	0	60100	0	12543	2410	+88	STO	COMMON+25	
30767	0	30000	0	12537	2411	+89	FAD	COMMON+21	F
30770	0	13100	0	00000	2412	+90	XCA		
30771	0	26000	0	12523	2413	+91	FMP	COMMON+9	0
30772	0	60100	0	12544	2414	+92	STO	COMMON+26	
30773	0	50000	0	12543	2415	+93	LQO	COMMON+25	
30774	0	26000	0	12541	2416	+94	FMP	COMMON+23	
30775	0	30200	0	12544	2417	+95	F38	COMMON+26	
30776	0	24100	0	12545	2418	+96	FDP	COMMON+27	
30777	0	26000	0	12541	2419	+97	FMP	COMMON+23	G
31000	0	60100	0	12550	2420	+98	STO	COMMON+30	C
31001	0	50000	0	12541	2421	+99	LQO	COMMON+23	G
31002	0	26000	0	12541	2422	+100	FMP	COMMON+23	
31003	0	13100	0	00000	2423	+101	XCA		
31004	0	26000	0	12540	2424	+102	FMP	COMMON+22	E
31005	0	30000	0	12544	2425	+103	FAD	COMMON+26	
31006	0	24100	0	12545	2426	+104	FDP	COMMON+27	DENOM
31007	-0	60000	0	12547	2427	+105	STQ	COMMON+29	B
31010	0	50000	0	12542	2428	+106	LQO	COMMON+24	
31011	0	26000	0	12540	2429	+107	FMP	COMMON+22	E
31012	0	30200	0	12537	2430	+108	F38	COMMON+21	F
31013	0	24100	0	12545	2431	+109	FDP	COMMON+27	DENOM
31014	-0	60000	0	12544	2432	+110	STQ	COMMON+28	A
31015	0	26000	0	34000	2433	+111	FMP	TP+35	Q/N
31016	0	30030	0	12547	2434	+112	FAD	COMMON+29	B
31017	0	13100	0	00000	2435	+113	XCA		
31020	0	26000	0	34000	2436	+114	FMP	TP+35	Q/N
31021	0	30000	0	12550	2437	+115	FAD	COMMON+30	C
31022	0	02000	0	30577	2438	+116	TRA	AYK8	
31023	2	00576	1	40005	2439	AYK1	DEC	.74646,.07456,-.28222,-.74307,1.52787,-19.22319,.00335	
31032	1	77523	7	00334	2440	+7	DEC	.33191,-.00636,.0011,-2.75204,-.67221,-18.35352,.16571	
31041	2	01656	4	37300	2441	+14	DEC	1.68188,.74646,-.28222	
31044	2	03577	6	50135	2442	AYK2	DEC	5.99732,1.64067,-.93201,-10.25526,3.80415,-62.58795	
31052	-1	76413	5	30704	2443	+6	DEC	-.1307,.53358,.71196,-.01868,-2.30298,7.1731,-111.58496	
31061	-1	77531	5	47502	2444	+13	DEC	-.33760,-2.20862,5.99732,-.93201	
31065	1	56414	3	36750	2445	AYK3	DEC	2E-6	MAXIMUM DELHSV/NSQ.
31066	1	77540	5	07534	2446	+1	DEC	.36	Q/N DIVISION PT BETWEEN CURVES A, B
31067	2	00743	5	71515	2447	+2	DEC	.9448	Q/N MAX CNST
31070	2	01517	2	70244	2448	+3	DEC	1.31	X3 CNST
31071	2	00765	6	05075	2449	+4	DEC	.98	Z=0 AT .98(Q/N MAX)
31072	2	00746	3	14632	2450	+5	DEC	.95	USE PARABOLA ABOVE .95(Q/N MAX)
31073	1	77702	4	36561	2451	+6	DEC	.44	USE PARABOLA BEYOND .44

31074	2	00453	3	25637	2452	+7	DEC	.5848	X3 CNST
31075	1	73507	5	34122	2453	+8	DEC	.02	EQN B CNST
31076	0	50000	0	33773	2454	AYK9	LQO	TP+30	HSV/N**2
31077	0	26060	4	00001	2455	+1	FMP*	1.4	RHO1
31100	0	13100	0	00000	2456	+2	XCA		
31101	0	26000	0	40225	2457	+3	FMP	FL12	NPSP/NSQ
31102	0	56000	0	31500	2458	+4	LQO	AYK02	MAXIMUM NPSP/NSQ
31103	0	04000	0	31105	2459	+5	TLQ	**2	
31104	0	13100	0	00000	2460	+6	XCA		
31105	0	50000	0	34000	2461	+7	CLA	TP+35	Q/N
31106	0	07400	4	40734	2462	+8	TSX	SCURV,4	
31107	0	00061	0	00005	2463	+9	PZE	5,.49	
31110	0	00000	0	00020	2464	+10	PZE	16	
31111	0	00000	0	31113	2465	+11	PZE	AYK01	
31112	0	02000	0	30603	2466	+12	TRA	AYKR	
31113	1	45467	2	31151	2467	AYK01	DEC	453E-11,0.,0.,.16,0.,.18,573E-7,.21,596E-7,.22,606E-7,.24	
31127	1	63402	2	74774	2468	+12	DEC	616E-7,.26,625E-7,.28,628E-7,.283,633E-7,.3,636E-7,.32	
31141	1	63411	3	77556	2469	+22	DEC	633E-7,.33,627E-7,.36,0.,.4,0.,.5,0.,.1,0.	
				31154	2470	BSS		16	
31174	1	45635	5	41727	2471	DEC		602E-11,0.,0.,.15,0.,.18,58E-6,.21,598E-7,.22,607E-7,.24	
31210	1	63402	6	23573	2472	DEC		617E-7	
31211	1	77412	1	72703	2473	DEC		.26,627E-7,.28,635E-7,.29,638E-7,.31,643E-7,.33,636E-7	
31223	1	77527	0	24366	2474	DEC		.335,632E-7,.342,625E-7,.38,582E-7,.4,0.,.1,0.	
				31235	2475	BSS		16	
31255	1	47401	5	45312	2476	DEC		15E-9,0.,0.,.13,0.,.18,594E-7,.21,609E-7,.22,617E-7,.24	
31271	1	63406	4	40364	2477	DEC		626E-7,.26,634E-7,.28,641E-7,.29,643E-7,.31,645E-7,.33	
31303	1	63415	2	14347	2478	DEC		642E-7,.35,639E-7,.37,631E-7,.4,617E-7,.45,0.,.1,0.	
				31316	2479	BSS		16	
31336	1	50402	4	35146	2480	DEC		301E-10,0.,0.,.12,0.,.18,607E-7,.21,621E-7,.22,629E-7,.24	
31352	1	63413	1	32553	2481	DEC		637E-7,.26,642E-7,.28,646E-7,.29,647E-7,.31,647E-7,.33	
31364	1	63416	7	47343	2482	DEC		646E-7,.35,644E-7,.37,64E-6,.39,635E-7,.45,0.,.1,0.	
				31377	2483	BSS		16	
31417	1	51402	4	35146	2484	DEC		602E-10,0.,0.,.1,0.,.16,616E-7,.206,634E-7,.22,639E-7,.24	
31433	1	63416	0	71745	2485	DEC		644E-7,.26,647E-7,.28,649E-7,.29,65E-6,.31,651E-7,.33	
31445	1	63420	5	02340	2486	DEC		65E-6,.35,647E-7,.37,644E-7,.41,633E-7,.46,0.,.1,0.	
				31460	2487	BSS		16	
31500	1	51402	4	35146	2488	AYK02	DEC	602E-10	MAXIMUM NPSP/NSQ

31501	0	63400	4	31514	2491	AYL	SXA	AYLR,4	
31502	0	50000	1	31524	2492	+1	CLA	AYLP,1	
31503	0	62100	0	31505	2493	+2	STA	*+2	
31504	0	07400	4	30527	2494	+3	TSX	AYK,4,0	
31505	0	00000	0	00000	2495	+4	PZE	**0,0	
31506	0	10000	0	31516	2496	+5	TZE	AYL2	
31507	0	60100	0	12512	2497	+6	STO	COMMON	
31510	0	50060	1	31526	2498	+7	CLA*	AYLN,1	WDOTP
31511	0	24100	0	12512	2499	+8	FDP	COMMON	
31512	0	26060	1	31522	2500	+9	FMP*	AYLO,1	
31513	0	60160	1	31520	2501	+10	STO*	AYLA,1	DELH
31514	0	77400	4	00000	2502	AYLR	AXT	**0,4	
31515	0	02000	4	00001	2503	+1	TRA	1.4	

2490*REGION TO COMPUTE

WORK REQUIRED TO DRIVE THE PUMP

31517	0	02000	0	31514	2505	+1	TRA	AYLR	
31520	0	00000	0	32667	2506		AYLA	PZE	P+41
31521	0	00000	0	34057	2507	+1	PZE	TP+82	
31522	0	00000	0	34066	2508		AYLO	PZE	TP+89
31523	0	00000	0	34096	2509	+1	PZE	TP+81	
31524	0	00000	0	34060	2510		AYLP	PZE	TP+83
31525	0	00000	0	34017	2511	+1	PZE	TP+50	RMOL
31526	0	00000	0	32643	2512		AYLM	PZE	P+21
31527	0	00000	0	32677	2513	+1	PZE	P+49	

31530	0	56000	0	32666	2515*REGION TO COMPUTE ACTUAL WORK IN THE PUMP				
31531	0	28000	0	32666	2516	AYM	LDQ	P+40	N(I+1) EQN PT11
31532	0	60100	0	34015	2517	+1	FMP	P+40	
31533	0	56000	0	32665	2518	+2	STQ	TP+48	
31534	0	26000	0	32665	2519	+3	LDQ	P+39	
31535	0	30200	0	34015	2520	+4	FMP	P+39	
31536	0	24100	0	32637	2521	+5	FSB	TP+48	N(I+1)*2
31537	0	26000	0	32751	2522	+6	FDP	P+17	DELT
31540	0	30200	0	32667	2523	+7	FMP	C+2	
31541	0	30000	0	32672	2524	+8	FSB	P+41	WPACT(I)
31542	0	30000	0	32671	2525	+9	FAD	P+44	WTACT(I+1)
31543	0	60100	0	32670	2526	+10	FAD	P+43	WTACT(I)
31544	0	02000	4	00001	2527	+11	STQ	P+42	WPACT(I+1)
					2528	+12	TRA	1,4	

31545	0	56000	0	32622	2530*REGION TO COMPUTE HEAT RESISTANCE TERM, M, FOR ONE NODE				
31546	-0	52000	1	36071	2531	AYN	LDQ	P+4	HF
31547	0	02000	0	31560	2532	+1	NZT	DPX,1	
31550	0	26000	1	36071	2533	+2	TRA	AYN1	
31551	0	30000	0	33761	2534	+3	FMP	DPX,1	
31552	0	30000	0	33761	2535	+4	FAD	TP+20	K
31553	0	60100	0	33751	2536	+5	FAD	TP+20	
31554	0	56000	0	32622	2537	+6	STQ	TP+12	
31555	0	26000	0	33761	2538	+7	LDQ	P+4	HF
31556	0	36100	0	40301	2539	+8	FMP	TP+20	
31557	0	24100	0	33751	2540	+9	ACL	188	
31560	-0	60000	0	33751	2541	+10	FDP	TP+12	
31561	0	50000	0	33731	2542	AYN1	STQ	TP+12	
31562	0	24100	0	33751	2543	+1	CLA	WPR+7	CP
31563	0	26000	0	32631	2544	+2	FDP	TP+12	
31564	0	24100	1	36064	2545	+3	FMP	P+11	WOODY
31565	0	13100	0	00000	2546	+4	FDP	DEL2,1	
31566	0	24100	0	33760	2547	+5	XCA		
31567	0	13100	0	00000	2548	+6	FDP	TP+19	FP
31570	0	60100	0	32627	2549	+7	XCA		
31571	0	36100	0	40301	2550	+8	STQ	P+9	M
31572	0	30000	0	40213	2551	+9	ACL	188	
31573	0	60100	0	33745	2552	+10	FAD	FL1	
31574	0	30200	0	40214	2553	+11	STQ	TP+8	2M+1
31575	0	60100	0	33746	2554	+12	FSB	FL2	
31576	0	13000	0	00001	2555	+13	STQ	TP+9	2M-1
					2556	+14	TRA	1,4	

31577	-0	62500	1	34560	2557	+15	STL	FX+3,1	
31600	0	02000	4	00001	2558	+16	TRA	1,4	

31601	0	63400	4	31610	2560*MASTER CONTROL FOR PUMP AND TURBINE FOR TIME I (CORRECTIONS)				
31602	0	63400	1	31611	2561	AYPA	SXA	AYPAR,4	
31603	0	77400	1	00000	2562	+1	SXA	AYPAR+1,1	
31604	0	07400	4	30326	2563	+2	AXT	0,1	XRI= TIME I
31605	0	52000	0	32742	2564	+3	TSX	AYGA,4	
31606	0	02000	0	31613	2565	+4	ZET	X+20	
31607	0	07400	4	30220	2566	+5	TRA	AYPA1	
31610	0	77400	4	00000	2567	+6	TSX	AYG,4	
31611	0	77400	1	00000	2568	AYPAR	AXT	**0,4	
31612	0	02000	4	00001	2569	+1	AXT	**0,1	
					2570	+2	TRA	1,4	
31613	0	50000	0	36201	2571*P11 GIVEN				
31614	0	60100	0	32662	2572	AYPA1	CLA	DP11	
31615	0	50000	0	36202	2573	+1	STQ	P+36	
31616	0	60100	0	32663	2574	+2	CLA	DT11	
31617	0	60100	0	34053	2575	+3	STQ	P+37	
31620	0	07400	4	27531	2576	+4	STQ	TP+78	
31621	0	07400	4	31501	2577	+5	TSX	AYB,4	
31622	0	60000	0	32645	2578	+6	TSX	AYL,4	
31623	0	60000	0	32647	2579	+7	STZ	P+23	
31624	0	60000	0	32660	2580	+8	STZ	P+25	
31625	0	60000	0	32661	2581	+9	STZ	P+34	
					2582	+10	STZ	P+35	
31626	0	02000	0	31610	2583	+11	TRA	AYPAR	

31627	0	63400	4	31663	2585*REGION TO PREDICT ENGINE AND TURBOPUMP PERFORMANCE FOR NEXT TIME POINT				
31630	0	63400	1	31664	2586	AYPB	SXA	AYPBR,4	
31631	-0	77400	1	00001	2587	+1	SXA	AYPBR+1,1	
31632	0	50000	0	32665	2588	+2	AXC	1,1	
31633	-0	10000	0	31635	2589	+3	CLA	P+39	
31634	0	50000	0	31670	2590	+4	TNZ	*+2	
31635	0	60100	0	32666	2591	+5	CLA	AYPB1	
31636	0	50000	0	40305	2592	+6	STQ	P+40	N(I+1) GUESS
31637	0	60100	0	40471	2593	+7	CLA	BIG	
31640	0	60000	0	40472	2594	+8	STQ	NEWA9	
31641	0	50000	0	36145	2595	+9	STZ	NEWA9+1	
31642	0	07400	4	40407	2596	+10	CLA	DNPE	
31643	0	32670	0	32666	2597	+11	TSX	NEWA,4	
31644	0	00031	0	34057	2598	+12	PZE	P+40,,P+42	
31645	0	02000	0	31666	2599	+13	PZE	TP+82,,25	
31646	0	07400	4	30055	2600	+14	TRA	AYPB2	
31647	-0	52000	0	32742	2601	+15	TSX	AYD,4	NOT CONVERGED
31650	0	07400	4	27402	2602	+16	NZT	X+20	FIND QP(I+1)
31651	0	07400	4	27531	2603	+17	TSX	AYA,4	NOT O= P11 GIVEN
31652	0	07400	4	31501	2604	+18	TSX	AYB,4	FIND PB
31653	0	07400	4	31530	2605	+19	TSX	AYL,4	FIND WTACT
31654	0	07400	4	40477	2606	+20	TSX	AYM,4	FIND WPACTPRIME
31655	0	52000	0	32736	2607	+21	TSX	RAPA,4	FIND WPACT
					2608	+22	ZET	X+16	
					2609	+23	TRA	1,4	

31697	0	92000	0	32733	2610	+24	ZRT	X+13	
31698	0	02000	0	31666	2611	+25	TRA	AYPB2	
31699	0	92000	0	32741	2612	+26	ZRT	X+19	
31699	0	02000	0	31666	2613	+27	TRA	AYPB2	
31693	0	77400	4	00000	2614		AYPBR	AXT	000,4
31694	0	77400	1	00000	2615	+1	AXT	000,1	
31695	0	02000	4	00001	2616	+2	TRA	L,4	
31696	-1	31671	0	25440	2617		AYPB2	STR	AZPT,,AYPB3
31697	0	02000	0	31663	2618	+1	TRA	AYPBR	
31670	2	15470	4	00000	2619		AYPB1	DEC	5000.
31671	-0	75125	2	43123	2620		AYPB3	BCI	3,PREDICTOR FAILED

INITIAL N GUESS

2622*REGION TO COMPUTE INLET AND OUTLET PRESSURE DROPS FOR ONE PART

31674	0	63400	4	31701	2623		AYQ	SXA	AYQR,4	
31675	0	50000	0	32620	2624	+1	CLA	P+2		FLUID TEMP
31676	0	56000	0	32621	2625	+2	LDQ	P+3		PRESSURE
31677	0	07400	4	25564	2626	+3	TSX	AZH,4		
31700	0	02000	0	31720	2627	+4	TRA	AYQ1		
31701	0	77400	4	00000	2628		AYQR	AXT	000,4	
31702	0	44100	4	00000	2629	+1	LDI	0,4		
31703	0	50200	1	34072	2630	+2	CLS	DKDPI,1		
31704	-0	05400	0	00001	2631	+3	LFT	1		
31705	0	50200	1	34073	2632	+4	CLS	DKDPO,1		
31706	0	24100	0	33730	2633	+5	FDP	WPR+6		DENSITY
31707	0	26000	0	32631	2634	+6	FMP	P+11		FLOW RATE
31710	0	24100	0	40214	2635	+7	FDP	FL2		
31711	0	26000	0	32631	2636	+8	FMP	P+11		
31712	0	24100	0	40236	2637	+9	FDP	FLG		
31713	0	13100	0	00000	2638	+10	XCA			
31714	0	40200	0	12512	2639	+11	SLW	COMMON		DELTA P
31715	0	30000	0	32621	2640	+12	FAD	P+3		NEW PRESSUE
31716	0	60100	0	32621	2641	+13	STO	P+3		
31717	0	02000	4	00002	2642	+14	TRA	2,4		
31720	0	52200	0	31701	2643		AYQ1	XEC	AYQR	
31721	0	02000	4	00001	2644	+1	TRA	L,4		

2646*REGION TO COMPUTE VALUES FOR AZT

31722	0	63400	4	31775	2647		AYR	SXA	AYRR,4	
31723	0	50000	0	32620	2648	+1	CLA	P+2		T
31724	0	56000	0	32621	2649	+2	LDQ	P+3		
31725	0	07400	4	25564	2650	+3	TSX	AZH,4		
31726	0	02000	0	31777	2651	+4	TRA	AYR1		
31727	0	50000	0	32616	2652	+5	CLA	P		
31730	0	07400	4	42437	2653	+6	TSX	LINT,4		
31731	0	00000	1	34625	2654	+7	PZE	WFP,1		
31732	0	60100	0	33760	2655	+8	STO	TP+19		
31733	0	50000	0	32616	2656	+9	CLA	P		
31734	0	07400	4	42437	2657	+10	TSX	LINT,4		
31735	0	00000	1	34567	2658	+11	PZE	WAF,1		
31736	0	60100	0	33757	2659	+12	STO	TP+18		
31737	0	24100	0	33760	2660	+13	FDP	TP+19		
31738	0	26000	0	40214	2661	+14	EMP	FL4		

31741	0	60100	0	33741	2662	+15	STO	TP+4		D
31742	0	30000	1	34064	2663	+16	FAD	DELZ,1		
31743	0	60100	0	33764	2664	+17	STO	TP+23		
31744	0	07400	4	30353	2665	+18	TSX	AYH,4		
31745	0	36156	2	35637	2666	+19	PZE	AZ01+1,2,DA		
31746	0	50000	2	35637	2667	+20	CLA	AZ01+1,2		
31747	0	07400	4	42437	2668	+21	TSX	LINT,4		
31750	0	00000	1	35144	2669	+22	PZE	WK,1		
31751	0	60100	0	33761	2670	+23	STO	TP+20		
31752	0	07400	4	31545	2671	+24	TSX	AYN,4		
31753	0	56000	0	40214	2672	+25	LDQ	FL4		
31754	0	26000	1	34064	2673	+26	FMP	DFP,1		
31755	0	24100	0	33741	2674	+27	FDP	TP+4		D
31756	0	26000	1	34064	2675	+28	FMP	DELZ,1		
31757	0	60100	0	33766	2676	+29	STO	TP+25		
31760	0	50000	0	32631	2677	+30	CLA	P+11		
31761	0	24100	0	33757	2678	+31	FDP	TP+18		
31762	-0	60000	0	12512	2679	+32	STQ	COMMON		
31763	0	26000	0	12512	2680	+33	FMP	COMMON		
31764	0	24100	0	40274	2681	+34	FDP	FL2GI		
31765	0	26000	0	33723	2682	+35	FMP	WPR+1		
31766	0	60100	0	34002	2683	+36	STO	TP+37		
31767	0	50200	0	33757	2684	+37	CLS	TP+18		AF
31770	0	24100	0	32637	2685	+38	FDP	P+17		DELT
31771	0	26000	1	34064	2686	+39	FMP	DELZ,1		
31772	0	60100	0	34074	2687	+40	STO	TP+95		
31773	0	50000	0	33730	2688	+41	CLA	WPR+6		
31774	0	60100	0	32623	2689	+42	STO	P+5		
31775	0	77400	4	00000	2690		AYRR	AXT	000,4	
31776	0	02000	4	00002	2691	+1	TRA	2,4		
31777	0	16200	0	32002	2692		AYR1	TQP	AYR2	
32000	0	52200	0	31775	2693	+1	XEC	AYRR		
32001	0	02000	4	00001	2694	+2	TRA	L,4		
32002	-1	32003	0	25417	2695		AYR2	STR	AZFF,,AYR3	
32003	2	22124	6	02643	2696		AYR3	BCI	3,BAD FLUID TNP, PRS	

2698*REGION TO CHECK FOR MINIMUM OUTLET METAL TEMPERATURE

32006	0	50000	0	32617	2699		AYT	CLA	P+1	M TEMP
32007	0	56000	0	34104	2700	+1	LDQ	DTNIN		
32010	0	04000	4	00001	2701	+2	TLQ	L,4		NOT COOL
32011	0	50000	0	32726	2702	+3	CLA	X+8		PRINT INTERVAL
32012	0	40200	0	32727	2703	+4	SUB	X+9		PRINT COUNTER
32013	0	40200	0	40200	2704	+5	SUB	FX1		
32014	-0	10000	4	00001	2705	+6	TNZ	L,4		WAIT UNTIL PRINT
32015	-1	32017	0	25421	2706	+7	STR	AZF,,AYT1		
32016	0	02000	0	24430	2707	+8	TRA	START		
32017	2	34446	4	32446	2708		AYT1	BCI	3,COOLDOWN REACHED	

2710*REGION TO COMPUTE PARA HYDROGEN PROPERTIES

32022	0	63400	4	32070	2711		PRP	SXA	PRP1,4	
32023	0	50000	0	33722	2712	+1	CLA	WPR		PRESSURE
32024	0	56000	0	32111	2713	+2	LDQ	PRP4+1		1500

32025	0	04000	0	32072	2714	+3	TLO	PRP7	ERROR RETURN FOR PRESS TOO BIG
32026	0	60000	0	32100	2715	+4	STZ	PRP8	
32027	0	56000	0	32107	2716	+5	LDO	PRP6+3	14.7
32030	0	04000	0	32033	2717	+4	TLO	PRP9	
32031	0	60100	0	32100	2718	+7	STO	PRP8	PRESS
32032	-0	60000	0	33722	2719	+8	STQ	WPR	14.7
32033	0	50000	0	33727	2720	PRP4	CLA	WPR+5	TEMPERATURE
32034	0	30200	0	32110	2721	+1	FSD	PRP4	36
32035	-0	12000	0	32074	2722	+2	THI	PRP10	ERROR RETN TEMP TOO SMALL
32036	0	07400	4	13257	2723	+3	TSX	THAL,4	
32037	0	00000	0	33727	2724	+4	PZE	WPR+5	TEMP
32040	0	00000	0	33722	2725	+5	PZE	WPR	PRESS
32041	0	50000	0	32102	2726	+6	CLA	PRP8+2	0
32042	0	00000	0	33730	2727	+7	PZE	WPR+6	DENSITY
32043	0	00000	0	32103	2728	+8	PZE	PRP8+3	0
32044	0	00000	0	33731	2729	+9	PZE	WPR+7	C P
32045	0	00000	0	33724	2730	+10	PZE	WPR+2	M
32046	0	07400	4	22027	2731	+11	TSX	VIS,4	
32047	0	00000	0	33727	2732	+12	PZE	WPR+5	TEMP
32050	0	00000	0	33722	2733	+13	PZE	WPR	PRESS
32051	0	00000	0	33730	2734	+14	PZE	WPR+6	DENS
32052	0	50000	0	32102	2735	+15	CLA	PRP8+2	
32053	0	00000	0	33733	2736	+16	PZE	WPR+9	VISC
32054	0	00000	0	33732	2737	+17	PZE	WPR+8	K
32055	0	50000	0	32100	2738	+18	CLA	PRP8	
32056	0	10000	0	32063	2739	+19	TZE	PRP11	
32057	0	60100	0	33722	2740	+20	STO	WPR	PRESS
32060	0	24100	0	32107	2741	+21	FDP	PRP6+3	14.7
32061	0	26000	0	33730	2742	+22	FMP	WPR+6	DENSITY
32062	0	60100	0	33730	2743	+23	STO	WPR+6	
32063	0	50000	0	32106	2744	PRP11	CLA	PRP6+2	FL1
32064	0	24100	0	33730	2745	+1	FDP	WPR+6	DEN
32065	0	13100	0	00000	2746	+2	XCA		
32066	0	24100	0	32112	2747	+3	FDP	PRP4+2	1728
32067	-0	60000	0	33723	2748	+4	STQ	WPR+1	SPECIFIC VOLUME
32070	0	77400	4	00000	2749	PRP1	AXT	**0,4	
32071	0	02000	4	00002	2750	+1	TRA	2,4	
32072	0	50000	0	32104	2751	PRP7	CLA	PRP6	
32073	0	76500	0	00000	2752	+1	LRS	0	
32074	0	52200	0	32070	2753	+2	XEC	PRP1	
32075	0	02000	4	00001	2754	+3	TRA	1,4	
32076	0	50000	0	32105	2755	PRP10	CLA	PRP6+1	
32077	0	02000	0	32073	2756	+1	TRA	PRP7+1	
				32100	2757	PRP8	BSS	4,F	
32104	0	00001	0	00000	2758	PRP6	PZE	0,,1	PRESSURE TOO BIG
32105	0	00002	0	00000	2759	+1	PZE	0,,2	TEMP TOO SMALL
32106	2	01400	0	00000	2760	+2	DEC	1.	
32107	2	04726	3	14632	2761	+3	DEC	14.7	
32110	2	06440	0	00000	2762	PRP4	DEC	36.	
32111	2	13567	0	00000	2763	+1	DEC	1500.	
32112	2	13660	0	00000	2764	+2	DEC	1728.	

32113	0	63400	4	32222	2767	PRTD	SXA	PR99,4	
32114	0	63400	2	32221	2768	+1	SXA	PR98,2	
32115	0	63400	1	32220	2769	+2	SXA	PR971,1	
32116	-0	62500	0	33734	2770	+3	STL	COLUM	
32117	0	60000	0	32575	2771	+4	STZ	COUNT	
32120	0	07400	4	00052	2772	+5	TSX	DOUT,4	
32121	3	27451	0	32577	2773	+6	PTH	TCARD,,12073	
32122	3	04110	0	00036	2774	+7	PTH	KDATEA,,2120	
32123	3	04124	0	32573	2775	+8	PTH	PL2,,2132	
32124	-1	00001	0	00012	2776	+9	FVE	KPRINT,,1	
32125	0	07400	4	00052	2777	+10	TSX	DOUT,4	
32126	3	05773	0	40311	2778	+11	PTH	PR60,,3067	
32127	-1	00024	0	00012	2779	+12	FVE	KPRINT,,20	
32130	0	50000	0	40314	2780	+13	CLA	PR61	
32131	0	62100	0	32134	2781	+14	STA	PRO2	
32132	0	60000	0	40310	2782	+15	STZ	CUT	
32133	0	77400	2	00000	2783	+16	AXT	.,2	
32134	0	52000	2	36064	2784	PRO2	ZET	D,2	
32135	0	02000	0	32150	2785	+1	TRA	PRO3	
32136	1	77777	2	32137	2786	+2	TXI	**1,2,-1	
32137	3	77766	2	32134	2787	+3	TXH	PRO2,2,-10	
32140	0	07400	4	32214	2788	+4	TSX	PRO23,4	
32141	0	53400	4	32134	2789	PRO24	LXA	PRO2,4	
32142	1	00012	4	32143	2790	+1	TXI	**1,4,10	
32143	0	63400	4	32134	2791	+2	SXA	PRO2,4	
32144	0	52000	0	32721	2792	+3	ZET	X+3	
32145	3	37357	4	32220	2793	+4	TXH	PR971,4,AZMTP	
32146	-3	40177	4	32133	2794	+5	TXL	PRO2-1,4,AZMTC	
32147	0	02000	0	32220	2795	+6	TRA	PR971	
32150	0	50000	0	32134	2796	PRO3	CLA	PRO2	
32151	0	62100	0	32207	2797	+1	STA	PRO4	
32152	0	53400	4	32207	2798	+2	LXA	PRO4,4	
32153	0	63400	4	32172	2799	+3	SXA	PR10,4	
32154	1	41550	4	32155	2800	+4	TXI	**1,4,-AZD	
32155	3	77633	4	32175	2801	+5	TXH	PR12,4,D-AZD-1	
32156	0	75400	4	00000	2802	+6	PXA	,4	
32157	0	13100	0	00000	2803	+7	XCA	,0	
32160	0	75400	0	00000	2804	+8	PXA	PR11	
32161	0	22100	0	32224	2805	+9	DVP	PRO4-1	
32162	-0	10000	0	32206	2806	+10	TNZ		FX150
32163	0	13100	0	00000	2807	+11	XCA		
32164	0	76700	0	00002	2808	+12	ALS	2	
32165	0	73400	4	00000	2809	+13	PAX	,4	
32166	-0	63600	4	00061	2810	+14	SCD	KINDX4,4	
32167	0	07400	4	00052	2811	+15	TSX	DOUT,4	
32170	3	07675	4	32225	2812	+16	PTH	PR13,4,4029	
32171	3	02060	0	32275	2813	+17	PTH	PR14,,1072	
32172	-3	00101	0	00000	2814	PR10	SVN	**0,,65	
32173	-1	00024	0	00012	2815	+1	FVE	10,,20	
32174	0	02000	0	32206	2816	+2	TRA	PRO4-1	
32175	0	53500	4	40310	2817	PR12	LAC	CUT,4	
32176	-3	00000	4	32201	2818	+1	TXL	**3,4,0	
32177	0	52000	0	32721	2819	+2	ZET	X+3	
32200	-3	77766	4	32212	2820	+3	TXL	PRO1,4,D-AZMTE	

PRINT ONLY PART

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32201 -0 63400 4 00061 2821 +4 SXO KENDX4,4
32202 0 07400 4 00052 2822 +5 TSX DOUT,4
32203 3 01743 4 32274 2823 +6 PTH PR19,4,1011
32204 0 21445 0 00001 2824 +7 PZE 1,,9013
32205 -1 00024 0 00012 2825 +8 FVE 10,,20
32206 0 07400 4 00052 2826 +9 TSX DOUT,4
32207 -2 13574 0 00000 2827 PRO4 SIX 0,,6012
32210 0 21445 0 00001 2828 +1 PZE 1,,9013
32211 -1 00012 0 00012 2829 +2 FVE KPRINT,,10
32212 0 07400 4 32214 2830 PRO1 TSX PRO23,4
32213 0 02000 0 32141 2831 +1 TRA PRO24
32214 0 50000 0 40310 2832 PRO23 CLA CUT
32215 0 40000 0 40211 2833 +1 ADD FX10
32216 0 60100 0 40310 2834 +2 STO CUT
32217 0 02000 4 00001 2835 +3 TRA 1,4
32220 0 77400 1 00000 2836 PRO71 AXT 0,1
32221 0 77400 2 00000 2837 PRO8 AXT ,2
32222 0 77400 4 00000 2838 PRO9 AXT ,4
32223 0 02000 4 00001 2839 +1 TRA 1,4
32224 0 00000 0 00144 2840 PR11 PZE 100
32225 2 64346 6 66021 2841 PR13 BCI 4,FLOW AREA VS DISTANCE
32231 -2 62563 6 32524 2842 +4 BCI 4,WETTED PERIMETER VS Z
32235 2 65121 2 36360 2843 +8 BCI 4,FRACT HEAT GEN VS DIST
32241 3 14563 6 03025 2844 +12 BCI 4,INT HEAT GEN VS TIME
32245 -2 33025 5 14421 2845 +16 BCI 4,THERMAL CONDUCTIVITY
32251 2 36062 6 42260 2846 +20 BCI 4,C SUB R VS TEMPERATURE
32255 3 14543 2 56360 2847 +24 BCI 4,INLET TEMP VS TIME
32261 3 14543 2 56360 2848 +28 BCI 4,INLET PRESSURE VS TIME
32265 -0 66463 4 32563 2849 +32 BCI 4,OUTLET PRESSURE VS TIME
32271 2 72163 2 56047 2850 +36 BCI 4,GATE POSITION VS TIME
32275 -0 74631 4 56362 2851 PR14 BCI 1,POINTS
32276 2 42543 6 07160 2852 PR15
32277 -3 16047 6 36260 2853 +1
32300 2 65131 2 36360 2854 +2
32301 -2 54631 2 46024 2855 +3
32302 -1 13046 6 05160 2856 +4
32303 -2 62143 4 36067 2857 +5
32304 2 54563 7 06042 2858 +6
32305 2 56731 6 36042 2859 +7
32306 3 14543 6 36065 2860 +8 BCI 2,INLT VOTLT V
32310 -0 75131 4 56360 2861 +10
32311 -2 33144 2 56000 2862 +11
32312 2 42543 6 06360 2863 +12
32313 -2 36047 6 36260 2864 +13
32314 2 46360 4 43145 2865 +14
32315 -0 46343 6 06300 2866 +15
32316 -0 44560 6 34447 2867 +16
32317 -0 46760 6 34447 2868 +17
32320 2 43143 6 44563 2869 +18 BCI 2,DILUNTP1
32322 -2 30160 6 06060 2870 +20 BCI 1,T1
32323 -0 74660 4 43145 2871 +21
32324 -0 70260 2 34362 2872 +22
32325 -0 71060 2 34362 2873 +23
32327 -2 62446 6 36023 2874 +24
32327 -2 62446 6 36023 2875 +25
32330 -2 62446 6 36030 2876 +26
32331 -2 62360 2 34362 2877 +27
32332 -2 65160 2 34362 2878 +28
32333 2 16006 6 06060 2879 +29
32334 2 16062 6 32151 2880 +30 BCI ,A STARNTB FFPARTS WALL TQ1 INTSWT GATE PA(KV) B(KV) K(KT)
32344 -0 26002 6 06060 2881 +40 BCI 3,K 2 D 2 D H
32351 2 46063 4 36060 2882 +43
32352 2 46063 4 56060 2883 +44
32353 2 46051 4 56060 2884 +45
32354 3 16047 6 36060 2885 +46
32355 -2 24725 2 52460 2886 +47
32356 3 06023 4 36260 2887 +48 BCI 2,H CLS WP CLS
32360 3 02260 4 36330 2888 +50
32361 -0 50060 6 06760 2889 +51
32362 2 46023 4 66060 2890 +52
32363 -0 50060 3 04362 2891 +53
32364 -2 06360 6 06060 2892 +54 BCI , T R THETA A COLDB COLDC COLDA HOT B HOT C HOT
32376 2 65123 6 36023 2893 +64 BCI ,FRCT CFRCT H K(PHM)K(PCMK)(DLP)K(CMPKC INCR COLDR HOT
32410 -0 26001 0 16060 2894 +74
32411 -0 26011 6 06060 2895 +75
32412 -0 26025 6 06060 2896 +76
32413 -0 76001 0 16060 2897 +77 BCI ,3,P 11 T 11 O=NO B
32416 -2 22523 6 00160 2898 +80 BCI ,SEC 1 K 1 SEC 2 K 2 SEC 3 K 3 SEC 4 K 4 SEC 5 K 5
32430 -2 22523 6 00660 2899 +90 BCI ,SEC 6 K 6 SEC 7 K 7 SEC 8 K 8 SEC 9 K 9 SEC 10 K 10
2900*PRINT REGION
32442 0 63400 4 32522 2901 PRINT SXA PP97,4
32443 0 63400 2 32523 2902 +1 SXA PP98,2
32444 0 63400 1 32524 2903 +2 SXA PP99,1
32445 0 52000 0 33734 2904 +3 ZET COLUM
32446 0 02000 0 32526 2905 +4 TRA PZ
32447 0 53400 4 40315 2906 +5 LXA PP40,4
32450 0 63400 4 32470 2907 +6 SXA PP06,4
32451 -0 53400 4 40315 2908 +7 LXD PP40,4
32452 0 63400 4 32504 2909 +8 SXA PP075,4
32453 -0 53400 2 40316 2910 +9 LXD PP41,2
32454 3 00000 2 32461 2911 +10 TXH PP04,2,0
32455 0 07400 4 00052 2912 PP01 TSX DOUT,4
32456 3 27451 0 32577 2913 +1 PTH TCARD,,12073
32457 3 04110 0 00036 2914 +2 PTH KDATEA,,2120
32460 -1 00001 0 00012 2915 +3 FVE KPRINT,,1
32461 1 77777 2 32462 2916 PP04 TXI *+1,2,-1
32462 3 77767 2 32465 2917 +1 TXH *+3,2,-9
32463 0 60000 0 40316 2918 +2 STZ PP41
32464 0 02000 0 32453 2919 +3 TRA PP01-2
32465 -0 63400 2 40316 2920 +4 SXD PP41,2
32466 0 77400 2 00010 2921 +5 AXT X/B-P/8,2
32467 0 77400 1 00000 2922 PP05 AXT 0,1
32470 0 52000 1 32616 2923 PP06 ZET P,1
32471 0 02000 0 32501 2924 +1 TRA PP07
32472 1 77777 1 32473 2925 +2 TXI *+1,1,-1
32473 3 77770 1 32470 2926 +3 TXH PP06,1,-8
32474 -0 53400 4 40316 2927 +4 LXD PP41,4
32475 3 77776 4 32513 2928 +5 TXH PP09,4,-2
```

OK SINCE P IS A MULTIPLE OF 8

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32476 1 00001 4 32477 2929 +6 TXI 0+1,4,1
32477 -0 63400 4 40316 2930 +7 SKD PP41,4
32500 0 02000 0 32513 2931 +8 TRA PP09
32501 0 53400 4 32470 2932 PP07 LXA PP04,4
32502 0 63400 4 32510 2933 +1 SKA PP08,4
32503 0 07400 4 00052 2934 +2 TSX DOUT,4
32504 3 01757 0 40317 2935 PP075 PTH HEDER,,1007
32505 0 15547 0 00001 2936 +1 PZE 1,,7015
32506 -1 00024 0 00012 2937 +2 FVE KPRINT,,20
32507 0 07400 4 00052 2938 +3 TSX DOUT,4
32510 -2 17515 0 32616 2939 PP08 SIX P,,8013
32511 0 15547 0 00001 2940 +1 PZE 1,,7015
32512 -1 00012 0 00012 2941 +2 FVE KPRINT,,10
32513 0 53400 4 32504 2942 PP09 LXA PP075,4
32514 1 00010 4 32515 2943 +1 TXI 0+1,4,8
32515 0 63400 4 32504 2944 +2 SKA PP075,4
32516 0 53400 4 32470 2945 +3 LXA PP06,4
32517 1 00010 4 32520 2946 +4 TXI 0+1,4,8
32520 0 63400 4 32470 2947 +5 SKA PP06,4
32521 2 00001 2 32467 2948 +6 TIX PP05,2,1
32522 0 77400 4 00000 2949 PP97 AXT ,4
32523 0 77400 2 00000 2950 PP98 AXT ,2
32524 0 77400 1 00000 2951 PP99 AXT ,1
32525 0 02000 4 00001 2952 +1 TRA 1,4
32526 0 07401 4 32541 2953 PZ TSX PL,4,1
32527 -0 53400 4 32575 2954 +1 LXD COUNT,4
32530 3 00001 4 32533 2955 +2 TXH PA,4,1
32531 0 07400 4 32563 2956 +3 TSX PC,4
32532 -1 00024 0 00012 2957 +4 FVE KPRINT,,20
32533 0 07400 4 00052 2958 PA TSX DOUT,4
32534 -2 13621 0 32616 2959 +1 SIX P,,6033
32535 0 11625 0 00001 2960 +2 PZE 1,,5013
32536 -2 13737 0 32631 2961 +3 SIX P+11,,6111
32537 -1 00012 0 00012 2962 +4 FVE 10,,10
32540 0 02000 0 32522 2963 +5 TRA PP97
2964*SUBROUTINE TO TEST LINE COUNT AND PRINT PAGE HEAD
32541 0 63400 4 32561 2965 PL SKA PLR,4
32542 0 44100 4 00000 2966 +1 LDI 0,4
32543 -0 05700 7 77700 2967 +2 RIL 777700
32544 -0 04600 0 00000 2968 +3 PIA
32545 0 62200 0 32556 2969 +4 STD PF
32546 -0 53400 4 32575 2970 +5 LXD COUNT,4
32547 3 00000 4 32556 2971 +6 TXH PF,4,0
32550 0 07400 4 00052 2972 PL1 TSX DOUT,4
32551 3 27451 0 32577 2973 +1 PTH TCARD,,12073
32552 3 04110 0 00036 2974 +2 PTH KDATEA,,2120
32553 3 04124 0 32573 2975 +3 PTH PL2,,2132
32554 -1 00001 0 00012 2976 +4 FVE KPRINT,,1
32555 0 77400 4 00000 2977 +5 AXT 0,4
32556 1 00000 4 32557 2978 PF TXI 0+1,4,000
32557 3 00067 4 32550 2979 +1 TXH PL1,4,NLMAX
32560 -0 63400 4 32575 2980 PG SKD COUNT,4
32561 0 77400 4 00000 2981 PLR AXT 00,4
32562 0 02000 0 00001 2982 +1 LDI 0,4

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PRINT COLUMN HEADS

```

32563 -0 63400 4 00061 2983*SUBROUTINE TO PRINT COLUMN HEADS
32564 0 07400 4 00052 2984 PC SKD KINDEX,4
32565 3 02011 0 40317 2985 +1 TSX DOUT,4
32566 0 11625 0 00001 2986 +2 PTH HEDER,,1033
32567 3 02127 0 40332 2987 +3 PZE 1,,5013
32570 1 00000 4 00001 2988 +4 PTH HEDER+11,,1111
32571 -0 53400 4 00061 2989 +5 PON 1,4
32572 0 02000 4 00002 2990 +6 LXD KINDEX,4
32573 -2 06633 6 04633 2991 +7 TRA 2,4
2992 PL2 BCI 2, W. 0.= 0718

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CONFIDENTIAL R D WORK ORDER NO.

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32575 0 00000 0 00000 2994 COUNT PZE 0,,0
32576 0 02000 0 42566 2995 ENDO TRA END

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32577 2997 TCARD BSS 15,0
32616 2998 P BSS 64,0
32716 2999 X BSS 25,0
32747 3000 C BSS 20,0
32773 3001 WTI BSS 147,F
33216 3002 WPI BSS 147,F
33441 3003 WPO BSS 147,F
33664 3004 WGP BSS 30,F
33722 3005 WPR BSS 10,F
33734 3006 COLUM BSS 1,F
33735 3007 TP BSS 100,F
34101 3008 AZMTB EQU 0+1
3009*BEGINNING OF PART STORAGE
34101 3010 AZ02 BSS NZMAX,F
34163 3011 AZ03 BSS NZMAX,F
34245 3012 AZ04 BSS NZMAX,F
34327 3013 AZ05 BSS NZMAX,F
34411 3014 AZ07 BSS NZMAX,F
34473 3015 AZ09 BSS NZMAX,F
34555 3016 FX BSS 10,0
34567 3017 WAF BSS 30,F
34625 3018 WFP BSS 30,F
34663 3019 WH BSS 30,F
34721 3020 WMT BSS 147,F
35144 3021 WK BSS 147,F
35367 3022 WCR BSS 147,F
3023*THE FOLLOWING CELLS ARE RELATIVE TO D
35612 3024 PT BSS 20,F
35636 3025 AZ01 BSS NZMAX,F
35720 3026 AZ06 BSS NZMAX,F
36002 3027 AZ08 BSS NZMAX,F
36064 3028 D EQU 0+1
36064 3029 DELZ BSS 1,F
36065 3030 DNMAX BSS 1,F
36066 3031 DFF BSS 1,F
36067 3032 DVF BSS 1,F
36070 3033 DRHOR BSS 1,F

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PERMANENT STORAGE
FIXED POINT AND OCTAL STORAGE
SOME PROG CNSTS (FLOATING PT)
INLET TEMP
INLET PRESS
OUTLET PRESS
GATE POSITION
PROPERTIES OF PARA HYDROGEN

TEMPORARY STORAGE
BEGINNING OF PART STORAGE

TEMPORARY FLOW RATE, LB/SEC
FLUID TEMPS, DEGR
PRESSURE, PSIA
FILM COEFF, BTU/IN²-SEC-DEGR
NEW FLUID DENSITIES, LB/IN³
CSUBP

FLOW AREA
WETTED PERIMETER
FRACT HEAT GEN VS DISTANCE
INT HEAT GEN VS TIME
THERMAL CONDUCTIVITY
HEAT CAPACITY OF METAL

FLOATING POINT STORAGE, EACH PART
OLD METAL TEMPS, DEGR
OLD DENSITIES, LB/IN³
PERMANENT FLOW RATE, LB/SEC
INPUT STORAGES
POSITION INCREMENT, IN
*NO. POSITION PTS, 3= IGNORE THIS PT
FRICTION FACTOR
VOID FRACTION
METAL DENSITY

36071 3034 OPX BSS 1,F
 36072 3035 OKDPI BSS 1,F
 36073 3036 OKDPO BSS 1,F
 36074 3037 OVI BSS 1,F
 36075 3038 OVO BSS 1,F
 36076 3039 AZMTE EQU *+1
 3040*PART STORAGE ENDS HERE
 36076 3041 ORG D+10
 36076 3042 DPR1 BSS 1,F
 36077 3043 DTMI BSS 1,F
 36100 3044 DELT BSS 1,F
 36101 3045 DMOT BSS 1,F
 36102 3046 DMOT BSS 1,F
 36103 3047 DTHO BSS 1,F
 36104 3048 DTMIN BSS 1,F
 36105 3049 DTMAX BSS 1,F
 36106 3050 DOIL BSS 1,F
 36107 3051 OPI BSS 1,F
 36110 3052 OTI BSS 1,F
 36111 3053 OPO BSS 1,F
 36112 3054 OPBE BSS 1,F
 36113 3055 OP12E BSS 1,F
 36114 3056 OMP BSS 1,F
 36115 3057 OMC BSS 1,F
 36116 3058 DMH BSS 1,F
 36117 3059 DMCE BSS 1,F
 36120 3060 DMRE BSS 1,F
 36121 3061 DA6 BSS 1,F
 36122 3062 CASTR BSS 1,F
 36123 3063 DNZFF BSS 1,F
 36124 3064 DNP BSS 1,F
 36125 3065 DMT BSS 1,F
 36126 3066 DQINT BSS 1,F
 36127 3067 DSWT BSS 1,F
 36130 3068 DGP BSS 1,F
 36131 3069 DAKV BSS 1,F
 36132 3070 DBKV BSS 1,F
 36133 3071 DK BSS 1,F
 36134 3072 DK2 BSS 1,F
 36135 3073 DD2 BSS 1,F
 36136 3074 ODH BSS 1,F
 36137 3075 ODTL BSS 1,F
 36140 3076 ODTN BSS 1,F
 36141 3077 DORN BSS 1,F
 36142 3078 DIPT BSS 1,F
 36143 3079 DNI BSS 1,F
 36144 3080 DHE BSS 1,F
 36145 3081 DMPE BSS 1,F
 36146 3082 OL BSS 1,F
 36147 3083 ONX BSS 1,F
 36150 3084 ODCO BSS 1,F
 36151 3085 DNH BSS 1,F
 36152 3086 DT BSS 1,F
 36153 3087 DT BSS 1,F

SUB 12013.

25/09/69

PAGE 57

36154 3088 DTHET BSS 1,F
 36155 3089 TK EQU *+1
 36155 3090 BSS 1
 36156 3091 DA BSS 1,F
 36157 3092 DB BSS 1,F
 36160 3093 DC BSS 1,F
 36161 3094 DAHOT BSS 1,F
 36162 3095 DBHOT BSS 1,F
 36163 3096 DCHOT BSS 1,F
 36164 3097 DFCLD BSS 1,F
 36165 3098 DFHOT BSS 1,F
 36166 3099 BSS 1
 36167 3100 DKPHM BSS 1,F
 36170 3101 DKPCM BSS 1,F
 36171 3102 DKIN BSS 1,F
 36172 3103 DKCC BSS 1,F
 36173 3104 DKCI BSS 1,F
 36174 3105 DRC BSS 1,F
 36175 3106 DRH BSS 1,F
 36176 3107 DK11 BSS 1,F
 36177 3108 DK9 BSS 1,F
 36200 3109 DKE BSS 1,F
 36201 3110 DP11 BSS 1,F
 36202 3111 DT11 BSS 1,F
 36203 3112 DKFLG BSS 1,F
 36204 3113 ORG D+80
 36204 3114 BELLO BSS 20,F
 36230 3115 ORG D+100
 36230 3116 AZD BSS 100*NCURV,F
 40177 3117 AZMTC EQU *

*WALL THICK, IN, NOT 0= PIPE OPTION
 K FOR INLET PRESS DROP, 1/IN4
 K FOR OUTLET PRESS DROP, 1/IN4
 INLET PLENUM, IN3
 OUTLET PLENUM, IN3
 END OF PART STORAGE

WHOLE ENGINE SYSTEM INPUT
 PRINT INTERVAL
 *INIT TIME, NOT 0= RESTART PROGRAM
 TIME INCREMENT, SEC
 NO. TIME INCREMENTS
 MINIMUM TIME INTERVAL, SEC
 INITIAL METAL TEMP, DEGR
 MIN OUTLET METAL TEMP, DEGR
 MAX ALLOWABLE FLUID TEMP, DEGR
 STATION FOR REMOVAL OF DILUENT
 *TANK PRESSURE, PSIA, 0= USE CURVE
 TANK TEMPERATURE, DEGR
 *MIN OUTLET PRESS, 0= USE CURVE
 P8 CLOSURE
 P12 CLOSURE
 INITIAL PUMP FLOW GUESS, LB/SEC
 INITIAL DILUENT FLOW GUESS, LB/SEC
 INITIAL HOT BLEED FLOW GUESS, LB/SEC
 WOOT C CLOSURE
 WOOT R CLOSURE
 AREA OF CCORE OUTLET, IN2
 NOZZLE THROAT AREA, IN
 *NOZ TUBE FRIC FACTOR, 0= NO TUBES
 NO. NOZ TUBE SEGMENTS
 NOZ TUBE WALL THICKNESS, IN
 INIT P1 FOR NOZ TUBES
 *7= PRINT NOZZLE TUBE ITERATIONS
 *GATE POSITION, PERCENT, 0=USE CURVE
 CNST FOR KV COMP
 CNST FOR KV COMP
 K FOR KT COMPUTATION
 K FOR NOZ TUBE INLET LINE
 DIAM OF NOZ TUBE INLET LINE, IN
 DIAM OF HOT BLEED PORT, IN
 DIAM OF TURBINE LINE, SQIN
 DIAM OF TURBINE NOZZLE, IN
 DIAM OF ROLL CONTROL NOZZLE, IN
 MOMENT OF PUMP AND TURBINE, LB-SQIN
 INITIAL TURBINE SPEED, RPM
 PUMP HEAD CLOSURE
 PUMP WORK CLOSURE
 LENGTH OF HOT BLEED PORT, IN
 NO. POSITION STEPS IN HBP
 DIAM OF COLD FLOW HOLES, IN
 NO. COLD FLOW HOLES
 THICKNESS OF COLD FLOW ANNULUS, IN
 *THICKNESS OF COLD FLOW ANNULUS, IN

402C0 0 00000 0 00001 3119 FX1 PZE 1
 40201 0 00000 0 00002 3120 FX2 PZE 2
 402C2 0 00000 0 00003 3121 FX3 PZE 3
 40203 0 00000 0 00004 3122 FX4 PZE 4
 40204 0 00000 0 00005 3123 FX5 PZE 5
 40205 0 00000 0 00006 3124 FX6 PZE 6
 40206 0 00000 0 00007 3125 FX7 PZE 7
 40207 0 00000 0 00010 3126 FX8 PZE 8
 4021C 0 00000 0 00011 3127 FX9 PZE 9
 40211 0 00000 0 00012 3128 FX10 PZE 10
 40212 0 00000 0 01750 3129 FX1E3 PZE 1000
 40213 2 01400 0 00000 3130 FL1
 40214 2 02400 0 00000 3131 FL2
 40215 2 02600 0 00000 3132 FL3
 40216 2 03400 0 00000 3133 FL4
 40217 2 03500 0 00000 3134 FL5
 40220 2 03600 0 00000 3135 FL6
 40221 2 03700 0 00000 3136 FL7
 40222 2 04400 0 00000 3137 FL8
 40223 2 04440 0 00000 3138 FL9
 40224 2 04500 0 00000 3139 FL10

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40226 1 77631 4 63146 3141 FL.4 DEC .4
40227 2 00714 6 31463 3142 FL.9 DEC .9
40230 2 01431 4 63146 3143 FL1.1 DEC 1.1
40231 2 01463 1 46315 3144 FL1.2 DEC 1.2
40232 2 01600 0 00000 3145 FL1.5 DEC 1.5
40233 2 00746 3 14632 3146 FL.95 DEC .95
40234 2 21606 5 00000 3147 FL1E5 DEC 1E5
40235 2 37436 0 44300 3148 FL12E8 DEC 12E8
40236 2 11601 5 77627 3149 FL6 DEC 385.7496
40237 2 12602 2 00000 3150 FLR DEC 772.5
40240 2 00774 3 15101 3151 FLR8 DEC .99297
40241 1 76435 7 15153 3152 FL139 DEC .1396
40242 2 12604 7 70244 3153 FL776 DEC 777.97
40243 1 70444 0 16431 3154 FLGAL DEC .002228
40244 2 10440 0 00000 3155 FL144 DEC 144.
40245 2 13660 0 00000 3156 FLCUF DEC 1728.
40246 2 16521 4 00000 3157 FL108 DEC 10800.
40247 2 07763 1 46315 3158 FL2RW DEC 124.8
40250 1 75631 4 63146 3159 FL.1 DEC .1
40251 1 76631 4 63146 3160 FL.2 DEC .2
40252 1 76700 4 06112 3161 FL.219 DEC .219
40253 1 77400 0 00000 3162 FL.25 DEC .25
40254 2 00400 0 00000 3163 FL.5 DEC .5
40255 2 00463 1 46315 3164 FL.6 DEC .6
40256 2 00631 4 63146 3165 FL.8 DEC .8
40257 2 02671 4 63146 3166 FL3.45 DEC 3.45
40260 2 06602 1 72703 3167 FL48.2 DEC 48.28
40261 2 06720 0 00000 3168 FL58 DEC 58.0
40262 2 02731 4 63146 3169 FL3.7 DEC 3.7
40263 2 07410 0 00000 3170 FL66 DEC 66.
40264 2 07620 0 00000 3171 FL100 DEC 100.
40265 2 10401 4 63146 3172 FL128. DEC 128.8
40266 2 10550 0 00000 3173 FL180 DEC 180.
40267 2 11440 0 00000 3174 FL288 DEC 288.
40270 2 12764 0 00000 3175 1000. DEC 1000.
40271 2 02622 0 77327 3176 FLPI DEC 3.1415927
40272 2 06401 3 10721 3177 FLGF DEC 32.17405
40273 2 07401 3 10721 3178 FL2G DEC 64.3481
40274 2 12601 5 77627 3179 FL2GI DEC 771.4992
40275 2 02622 0 77324 3180 PI
40276 2 03622 0 77325 3181 2PI
40277 1 73435 7 50646 3182 RAD
40300 2 06712 2 73406 3183 DEG
3184*OCTAL CONSTANTS
40301 0 01000 0 00000 3185 188 DEC 188
40302 0 02000 0 00000 3186 288 DEC 288
40303 0 00000 0 00000 3187 ZERO PZE 0,,0
40304 -2 06060 6 06060 3188 BLANK
40305 3 77777 7 77777 3189 BIG OCT 37777777777
40306 2 33000 0 00000 3190 FIX OCT 233000000000

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GRAVITY, IN-LB/LBF-SEC
 GAS CNST, FT-LBF/LB-DEGR
 GAS CNST, BTU/LB-DEGR
 LB-DEGR**5/SEC-LBF
 FT-LBF/BTU
 FT**3-MIN/GAL-SEC
 SQIN/SQFT
 CUIN/CUFT

2* DENSITY OF WATER, LB/FT3

GRAVITY, FT-LB/LBF-SEC2

2* GRAVITY, IN-LB/LBF-SEC2

40307 2 12250 6 00060 3192 BCDD BC 1
 TVM ARMA'S 43/11/64 PAGE 59

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40310 0 00000 0 00000 3193 CUT PZE 0
40311 -0 75146 2 75121 3194 PR60
40312 -0 46031 4 54764 3195 +1
40313 -2 36060 6 06060 3196 +2
40314 0 40307 0 36064 3197 PR61 PZE D,,BCDD
40315 0 40317 0 32616 3198 PP40 PZE P,,HEDER
40316 0 00000 0 00000 3199 PP41 PZE 0,,0
40317 -3 16024 3 16263 3200 HEDER
40320 -0 42563 4 36063 3201 +1
40321 2 64364 2 46063 3202 +2
40322 -0 75125 6 26260 3203 +3
40323 2 63143 4 46023 3204 +4
40324 -2 05130 4 66060 3205 +5 BCI 1, RHO
40325 -2 06045 6 06060 3206 +6
40326 -2 06261 0 26060 3207 +7
40327 3 06360 2 72545 3208 +8
40330 -2 06044 6 06060 3209 +9 BCI 1, M
40331 -2 33144 2 56060 3210 +10
40332 -2 62446 6 36051 3211 +11
40333 -2 02225 6 32160 3212 +12
40334 -2 06360 0 66060 3213 +13
40335 -1 16360 6 30660 3214 +14
40336 3 06265 6 03160 3215 +15 BCI 2,HSV I HSVI+1
40340 2 42543 6 06360 3216 +17
40341 -0 74660 4 43145 3217 +18
40342 -1 00131 4 53163 3218 +19
40343 -2 06060 6 06060 3219 +20
40344 -2 62446 6 36047 3220 +21
40345 -2 62446 6 36023 3221 +22
40346 -2 62446 6 36030 3222 +23
40347 -2 62446 6 36045 3223 +24 BCI 8,NDOT NWDOT T
40357 -2 04760 0 66060 3224 +32 BCI 8, P 6 G P P 8 NT CHK P 1 T 1 P 2 T 2
40367 -0 57431 2 00134 3225 +40 8, P 6 G P P 8 T 8 P 11 T 11 P 12 N(I)
40370 -2 64721 2 36360 3226 +41
40371 -2 64721 3 12001 3227 +42
40372 -2 66321 2 36360 3228 +43
40373 -2 66321 3 12001 3229 +44
40374 2 14347 3 02160 3230 +45
40375 -0 70260 3 12001 3231 +46
40376 -2 30260 3 12001 3232 +47
40377 2 43060 3 12001 3233 +48
40400 -2 64760 3 12001 3234 +49
40401 -1 04760 3 12001 3235 +50
40402 -2 06060 6 06060 3236 +51
40403 -2 04760 0 36060 3237 +52
40404 -2 06360 0 36060 3238 +53
40405 -2 04760 2 36060 3239 +54
40406 -2 06360 2 36060 3240 +55

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3242*NEWTONS ITERATION ROUTINE FOR ONE VARIABLE
 3243*CLOSURE IN AC, MAX AND MIN SET
 3244* TSX NEWA,4
 3245* P7C

3246* PZE LIVPRIME),,MAX NO. ITERATIONS
3247* NON-CONVERGENCE EXIT
3248* EVALUATE
3249* TSX RAPA,4
3250* CONVERGED
CLOSURE IN AC
40407 0 60100 0 40473 3251 NEMA STO NEMA1
40410 0 60000 0 40475 3252 +1 STZ NEMA1+2
40411 -0 50000 4 00001 3253 +2 CAL 1,4 X
40412 0 62100 0 40524 3254 +3 STA RAPAS
40413 0 62100 0 40533 3255 +4 STA RAPA6
40414 0 62100 0 40537 3256 +5 STA RAPA1
40415 0 62100 0 40542 3257 +6 STA RAPA7
40416 0 62100 0 40433 3258 +7 STA NEMA8
40417 0 77100 0 00022 3259 +8 ARS 18 Y1
40420 0 62100 0 40477 3260 +9 STA RAPA
40421 0 62100 0 40504 3261 +10 STA RAPAS
40422 -0 50000 4 00002 3262 +11 CAL 2,4 Y2
40423 0 62100 0 40504 3263 +12 STA RAPA+5
40424 0 77100 0 00022 3264 +13 ARS 18 MAX NO. ITERATIONS
40425 0 62100 0 40427 3265 +14 STA NEMA2+1
40426 0 63400 4 40432 3266 NEMA2 SXA NEMA+4
40427 0 77400 4 00000 3267 +1 AXT **0,4
40430 -2 00001 4 40461 3268 +2 THX NEMA7,4,1
40431 0 63400 4 40427 3269 +3 SXA *2,4
40432 0 77400 4 00000 3270 NEMA8 AXT **0,4
40433 0 50000 0 00000 3271 NEMA8 CLA **0 GUESS
40434 0 56000 0 40471 3272 +1 LDQ NEMA9 MAX
40435 0 04000 0 40450 3273 +2 TLQ NEMA6
40436 0 56000 0 40472 3274 +3 LDQ NEMA9+1 MIN
40437 0 04000 4 00004 3275 +4 TLQ 4,4
40440 0 50000 0 40251 3276 +5 CLA FL.2
40441 -0 52000 0 40475 3277 NEMA3 NZT NEMA1+2
40442 0 02000 0 40452 3278 +1 TRA NEMA5
40443 0 13100 0 00000 3279 +2 XCA
40444 0 30000 0 40474 3280 +3 FAD NEMA1+1
40445 0 24100 0 40214 3281 +4 FDP FL2
40446 -0 60060 0 40433 3282 +5 STQ* NEMA8
40447 0 02000 0 40427 3283 +6 TRA NEMA2+1
40450 0 50200 0 40253 3284 NEMA6 CLS FL.25
40451 0 02000 0 40441 3285 +1 TRA NEMA3
40452 0 60100 0 12512 3286 NEMA5 STO COMMON
40453 0 50060 0 40433 3287 +1 CLA* NEMA8
40454 -0 13000 0 00000 3288 +2 XCL
40455 0 26000 0 12512 3289 +3 FMP COMMON
40456 0 30060 0 40433 3290 +4 FAD* NEMA8
40457 0 60160 0 40433 3291 +5 STQ* NEMA8
40460 0 02000 0 40427 3292 +6 TRA NEMA2+1
40461 0 52200 0 40432 3293 NEMA7 XEC NEMA8
40462 0 02000 4 00003 3294 +1 TRA 3,4 NON-CONVERGENCE
40463 0 56060 0 40433 3295 BDXA LDQ* NEMA8
40464 -0 60000 0 40471 3296 +1 STQ NEMA9
40465 0 02000 0 40450 3297 +2 TRA NEMA6
40466 0 56060 0 40433 3298 BDNA LDQ* NEMA8
40467 -0 60000 0 50472 3299 +1 STQ NEMA9+1

40470 0 02000 0 40440 3300 +2 TRA NEMA3-1
40471 0 40471 3301 NEMA9 BSS 2,F MAX,MIN
40473 0 40473 3302 NEMA1 BSS 3,F
40476 2 00746 3 14632 3303 -1 DEC -.95
40477 0 50000 0 00000 3304 RAPA CLA **0 Y1
40500 -0 34000 0 40473 3305 +1 LAS NEMA1
40501 0 02000 0 40504 3306 +2 TRA **3
40502 0 02000 0 40504 3307 +3 TRA **2
40503 0 02000 0 40544 3308 +4 TRA RAPA9
40504 0 30200 0 00000 3309 +5 FSB **0 Y2
40505 0 60100 0 12514 3310 +6 STO COMMON+2
40506 0 24100 0 00000 3311 RAPA8 FDP **0 NEW E
40507 0 13100 0 00000 3312 +1 XCA Y1
40510 -0 34000 0 40473 3313 +2 LAS NEMA1
40511 0 02000 0 40514 3314 +3 TRA **3 CLOSURE
40512 0 02000 4 00001 3315 +4 TRA 1,4
40513 0 02000 4 00001 3316 +5 TRA 1,4
40514 0 50000 0 40475 3317 +6 CLA NEMA1+2
40515 0 10000 0 40537 3318 +7 TZE RAPAS
40516 0 30200 0 12514 3319 +8 FSB COMMON+2
40517 0 10000 0 40537 3320 +9 TZE RAPAS
40520 0 60100 0 12512 3321 +10 STO COMMON
40521 0 56000 0 12514 3322 +11 LDQ COMMON+2
40522 0 26000 0 40474 3323 +12 FMP NEMA1+1
40523 0 60100 0 12513 3324 +13 STO COMMON+1
40524 0 56000 0 00000 3325 RAPA5 LDQ **0 NEWX
40525 -0 60000 0 40474 3326 +1 STQ NEMA1+1
40526 0 26000 0 40475 3327 +2 FMP NEMA1+2
40527 0 30200 0 12513 3328 +3 FSB COMMON+1
40530 0 24100 0 12512 3329 +4 FDP COMMON
40531 0 76000 0 00012 3330 +5 DCT
40532 0 02000 0 40537 3331 +6 TRA RAPAS
40533 -0 60000 0 00000 3332 RAPA6 STQ **0 NEW GUESS
40534 0 50000 0 12514 3333 RAPA2 CLA COMMON+2
40535 0 60100 0 40475 3334 +1 STO NEMA1+2
40536 0 02000 0 40427 3335 +2 TRA NEMA2+1
40537 0 56000 0 00000 3336 RAPA1 LDQ **0 X
40540 -0 60000 0 40474 3337 +1 STQ NEMA1+1
40541 0 26000 0 40476 3338 +2 FMP NEMA1+3
40542 0 60100 0 00000 3339 RAPA7 STO **0 OLD X
40543 0 02000 0 40534 3340 +1 TRA RAPAS BUMPER
40544 0 30260 0 40504 3341 RAPA9 FSB* RAPAS
40545 0 60100 0 12514 3342 +1 STO COMMON+2
40546 0 02000 0 40510 3343 +2 TRA RAPAS+2
40547 0 60100 0 40634 3344 NEMA8 STO NEMA1
40550 0 60000 0 40636 3345 +1 STZ NEMA1+2
40551 -0 50000 4 00001 3346 +2 CAL 1,4
40552 0 62100 0 40665 3347 +3 STA RAPAS
40553 0 62100 0 40674 3348 +4 STA RAPAS
40554 0 62100 0 40700 3349 +5 STA RAPAS
40555 0 62100 0 40703 3350 +6 STA RAPAS
40556 0 62100 0 40574 3351 +7 STA NEMA8
40557 0 77100 0 00022 3352 +8 ARS 18
40560 0 62100 0 40640 3353 +9 STA RAPAS

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40941 0 42100 0 40647 3354 +10 STA RAP88
40942 -0 30000 4 00002 3355 +11 CAL 2,4
40943 0 42100 0 40649 3356 +12 STA RAP83
40944 0 42100 0 40705 3357 +13 STA RAP89
40945 0 77100 0 00022 3358 +14 ARS 18
40946 0 42100 0 40570 3359 +15 STA NEWB2+1
40947 0 43400 4 40573 3360 NEWB2 SXA NEWB4,4
40970 0 77400 4 00000 3361 +1 AXT 000,4
40971 -2 00001 4 40622 3362 +2 TNX NEWB7,4,1
40972 0 43400 4 40570 3363 +3 SXA 0-2,4
40973 0 77400 4 00000 3364 NEWB4 AXT 000,4
40974 0 90000 0 00000 3365 NEWB8 CLA 000
40975 0 94000 0 40632 3366 +1 LDQ NEWB9
40976 0 04000 0 40611 3367 +2 TLQ NEWB6
40977 0 94000 0 40633 3368 +3 LDQ NEWB9+1
40980 0 04000 4 00004 3369 +4 TLQ 4,4
40981 0 90000 0 40251 3370 +5 CLA FL,2
40982 -0 52000 0 40636 3371 NEWB3 NZT NEWB1+2
40983 0 02000 0 40613 3372 +1 TRA NEWB5
40984 0 13100 0 00000 3373 +2 XCA
40985 0 30000 0 40635 3374 +3 PAD NEWB1+1
40986 0 24100 0 40214 3375 +4 FDP FL2
40987 -0 40060 0 40574 3376 +5 STO* NEWB8
40988 0 02000 0 40570 3377 +6 TRA NEWB2+1
40989 0 90200 0 40253 3378 NEWB6 CLS FL,25
40990 0 02000 0 40602 3379 +1 TRA NEWB3
40991 0 60100 0 12512 3380 NEWB5 STO COMMON
40992 0 90060 0 40574 3381 +1 CLA* NEWB8
40993 -0 13000 0 00000 3382 +2 XCL
40994 0 26000 0 12512 3383 +3 FMP COMMON
40995 0 30060 0 40574 3384 +4 PAD* NEWB8
40996 0 60160 0 40574 3385 +5 STO* NEWB8
40997 0 02000 0 40570 3386 +6 TRA NEWB2+1
40998 0 52200 0 40573 3387 NEWB7 XEC NEWB4
40999 0 02000 4 00003 3388 +1 TRA 3,4
41000 0 56060 0 40574 3389 BDXB LDQ* NEWB8
41001 -0 60000 0 40632 3390 +1 STQ NEWB9
41002 0 02000 0 40611 3391 +2 TRA NEWB6
41003 0 56060 0 40574 3392 BDNB LDQ* NEWB8
41004 -0 60000 0 40633 3393 +1 STQ NEWB9+1
41005 0 02000 0 40601 3394 +2 TRA NEWB3-1
41006 0 40632 3395 NEWB9 BSS 2,F
41007 0 40634 3396 NEWB1 BSS 3,F
41008 2 00746 3 14432 3397 -1 DEC .95
41009 0 50000 0 00000 3398 RAPB CLA 000
41010 -0 34000 0 40634 3399 +1 LAS NEWB1
41011 0 02000 0 40645 3400 +2 TRA 0+3
41012 0 02000 0 40645 3401 +3 TRA 0+2
41013 0 02000 0 40705 3402 +4 TRA RAPB9
41014 0 30200 0 00000 3403 RAPB3 FSB 000
41015 0 60100 0 12514 3404 +1 STO COMMON+2
41016 0 24100 0 00000 3405 RAPB8 FDP 000
41017 0 13100 0 00000 3406 +1 XCA
41018 -0 74000 0 40634 3407 +2 LFC

```

GUESS

MAX

MIN

NON-CONVERGENCE

MAX,MIN

```

40452 0 02000 0 40655 3408 +3 TRA 0+3
40453 0 02000 4 00001 3409 +4 TRA 1,4
40454 0 02000 4 00001 3410 +5 TRA 1,4
40455 0 50000 0 40636 3411 +6 CLA NEWB1+2
40456 0 10000 0 40700 3412 +7 TZE RAPB1
40457 0 30200 0 12514 3413 +8 FSB COMMON+2
40458 0 10000 0 40700 3414 +9 TZE RAPB1
40459 0 60100 0 12512 3415 +10 STO COMMON
40460 0 56000 0 12514 3416 +11 LDQ COMMON+2
40461 0 26000 0 40635 3417 +12 FMP NEWB1+1
40462 0 60100 0 12513 3418 +13 STO COMMON+1
40463 0 56000 0 00000 3419 RAPB5 LDQ 000
40464 -0 60000 0 40635 3420 +1 STQ NEWB1+1
40465 0 26000 0 40636 3421 +2 FMP NEWB1+2
40466 0 30200 0 12513 3422 +3 FSB COMMON+1
40467 0 24100 0 12512 3423 +4 FDP COMMON
40468 0 76000 0 00012 3424 +5 DCT
40469 0 02000 0 40700 3425 +6 TRA RAPB1
40470 -0 60000 0 00000 3426 RAPB6 STQ 000
40471 0 50000 0 12514 3427 RAPB2 CLA COMMON+2
40472 0 60100 0 40636 3428 +1 STO NEWB1+2
40473 0 02000 0 40570 3429 RAPB4 TRA NEWB2+1
40474 0 56000 0 00000 3430 RAPB1 LDQ 000
40475 -0 60000 0 40635 3431 +1 STQ NEWB1+1
40476 0 26000 0 40637 3432 +2 FMP NEWB1+3
40477 0 60100 0 00000 3433 RAPB7 STO 000
40478 0 02000 0 40675 3434 +1 TRA RAPB2
40479 0 30200 0 00000 3435 RAPB9 FSB 000
40480 0 60100 0 12514 3436 +1 STO COMMON+2
40481 0 02000 0 40651 3437 +2 TRA RAPB8+2
40482 0 63400 1 40777 3438 ICURV SXA CURVR,1
40483 0 63400 2 41000 3439 +1 SXA CURVR+1,2
40484 0 63400 4 41001 3440 +2 SXA CURVR+2,4
40485 0 50000 4 00001 3441 +3 CLA 1,4
40486 0 10000 4 00004 3442 +4 TZE 4,4
40487 -0 73400 2 00000 3443 +5 PDX 2
40488 -0 63600 2 40731 3444 +6 SCD CURV1+1,2
40489 0 73400 2 00000 3445 +7 PAX 0,2
40490 0 50000 4 00002 3446 +8 CLA 2,4
40491 0 73400 1 00000 3447 +9 PAX 0,1
40492 -0 63400 1 40730 3448 +10 SKD CURV1,1
40493 0 50000 4 00003 3449 +11 CLA 3,4
40494 0 40000 0 41004 3450 +12 ADD CURVC+1
40495 0 62100 0 40730 3451 +13 STA CURV1
40496 0 77400 1 00000 3452 +14 AXT 0,1
40497 0 07400 4 42511 3453 +15 TSX LINTS,4
40498 0 00000 1 00000 3454 CURV1 PZE 000,1,000
40499 1 77552 1 40732 3455 +1 TXI 0+1,1,-150
40500 2 00001 2 40727 3456 +2 TIX 0-3,2,1
40501 0 02000 0 40777 3457 +3 TRA CURV3
40502 0 63400 1 40777 3458 SCURV SXA CURVR,1
40503 0 63400 2 41000 3459 +1 SXA CURVR+1,2
40504 0 63400 4 41001 3460 +2 SXA CURVR+2,4
40505 0 60100 0 41005 3461 +3 STO CURVC+2

```

TO INITIALIZE
 TSX ICURV,4
 PZE NO. Z CURVES (ADDRESS),,DELTA
 PZE NO. X,Y PAIRS (ADDRESS)
 PZE TABLE (Z1,X1,Y1,X2,Y2,...)

TO INTERPOLATE X IN AC
 Z IN MQ
 TSX SCURV,4
 PZE SAME
 PZE SAME
 PZE SAME
 Y IN ACC.

Z2 TABLE MUST BE 150 GREATER

X

```

40740 -0 60000 0 41006 3462 +4 STQ CURVC+3
40741 0 50000 4 00001 3463 +5 CLA 1,4
40742 0 10000 4 00004 3464 +6 TZE 4,4
40743 -0 73400 2 00000 3465 +7 PDX ,2
40744 -0 63600 2 40767 3466 +8 SCD CURV7-1,2
40745 0 73400 2 00000 3467 +9 PAX 0,2
40746 0 63400 2 40754 3468 +10 SXA CURV4,2
40747 -0 63400 2 40773 3469 +11 SXD CURV8,2
40750 0 50000 4 00003 3470 +12 CLA 3,4
40751 0 62100 0 40760 3471 +13 STA CURV5
40752 0 40000 0 41004 3472 +14 ADD CURVC+1
40753 0 62100 0 40764 3473 +15 STA CURV6
40754 0 77400 4 00000 3474 CURV4 AXT **0,4 **=NO Z CURVES
40755 0 77400 1 00000 3475 +1 AXT 0,1
40756 0 77400 2 00000 3476 +2 AXT 0,2
40757 0 63400 4 40770 3477 +3 SXA CURV7,4
40760 0 50000 1 00000 3478 CURV5 CLA **0,1
40761 0 60100 2 41007 3479 +1 STO CURVC+4,2
40762 0 50000 0 41005 3480 +2 CLA CURVC+2
40763 0 07400 4 42437 3481 +3 TSX LINT,4
40764 0 00000 1 00000 3482 CURV6 PZE **0,1
40765 0 60100 2 41010 3483 +1 STO CURVC+5,2
40766 1 77776 2 40767 3484 +2 TXI **1,2,-2
40767 1 77552 1 40770 3485 +3 TXI **1,1,-150 DELTA Z(CURVES)
40770 0 77400 4 00000 3486 CURV7 AXT **0,4
40771 2 00001 4 40757 3487 +1 TIX CURV5-1,4,1
40772 0 07400 4 42511 3488 +2 TSX LINTS,4
40773 0 00000 0 41007 3489 CURV8 PZE CURVC+4,,**0 ,NO. OF Z CURVES
40774 0 50000 0 41006 3490 +1 CLA CURVC+3
40775 0 07400 4 42437 3491 +2 TSX LINT,4
40776 0 00000 0 41007 3492 +3 PZE CURVC+4
40777 0 77400 1 00000 3493 CURVR AXT **0,1
41000 0 77400 2 00000 3494 +1 AXT **0,2
41001 0 77400 4 00000 3495 +2 AXT **0,4
41002 0 02000 4 00004 3496 +3 TRA 4,4
41003 2 33000 0 00000 3497 CURVC OCT 233000000000
41004 0 00000 0 00001 3498 +1 PZE 1
3499 BSS 30

```

3502*ENTROPY ROUTINE, TEMP IN AC, PRESS IN MQ

3503* TSX S(TP),4

3504*ENTROPY IN AC

3505 S(TP) SXA STPEX,4

3506 UNLIST

3892 LIST

41043 0 63400 4 41153

3894*AS58 HAS BEEN MODIFIED (SEE AZX)

3895 AS58 CLS 1,4

3896 UNLIST

41664 0 50200 4 00001

```

42374 0 30000 0 42435 4148 LIST
4149 COS PAD SIN+32 ADD PI/2 FOR COS
4150 UNLIST
4181 LIST
42437 0 60100 0 12512 4182 LINT STO COMMON STORE ARGUMENT
4183 UNLIST
4270 LIST

```

```

42566 -0 62500 0 04171 4272 UNLESS 1
END STL 2169
42572 -0 62500 0 04171 4273 CORE AZN, LAST
+4 STL 2169
42576 -0 62500 0 04171 4274 CORE HBI, KSUBM
+8 STL 2169
42602 0 02000 0 42603 4275 ERROR TRA **1
42603 -0 62500 0 04171 4276 UNLESS 1
+1 STL 2169
42607 -0 62500 0 04171 4277 CORE BEGIN, PRTO
+5 STL 2169
42613 -0 62500 0 04171 4278 CORE NEWA, RAP89
+9 STL 2169
42617 -0 63400 4 00061 4279 +13 SXD KINDEX, 4
4280 CORE -10, 10, S, 4, 4
+14 STL 2169
42624 -0 62500 0 04171 4281 +18 TSX KDEBUG, 4
42625 -1 01163 0 32716 4282 +19 FVE X,, AZMTB-X
42626 -1 07764 0 51162 4283 +20 FVE AZMT, 4*AZMTS
42627 -1 00165 0 44277 4284 +21 FVE TY,, LQ1-TY
42630 -1 23421 0 44514 4285 +22 FVE LAST,, 10001
42631 -1 00226 0 47321 4286 +23 FVE PR,, 150
42632 0 60000 0 33734 4287 +24 STZ COLUM
42633 0 07400 4 32442 4288 +25 TSX PRINT, 4
42634 0 07400 4 47024 4289 +26 TSX HBP, 4
42635 0 02000 0 24430 4290 +27 TRA START

```

4292*NOZZLE TUBE PROGRAM ' HUDSON

```

42636 0 63400 4 43552 4293 AZN SXA AZNR, 4
42637 0 63400 1 43553 4294 +1 SXA AZNR+1, 1
42640 0 63400 2 43554 4295 +2 SXA AZNR+2, 2
42641 0 76000 0 00012 4296 +3 OCT
42642 0 02000 0 42643 4297 +4 TRA **1
42643 0 50000 0 44475 4298 +5 CLA AZN5
42644 0 60100 0 44105 4299 +6 STO SHT
42645 0 77400 4 00012 4300 +7 AXT 10, 4
42646 -0 63400 4 43745 4301 +8 SXD ITER5, 4
42647 0 77400 4 43556 4302 +9 AXT BUG, 4
42650 0 63400 4 44020 4303 +10 SXA ITER9, 4
42651 0 50000 0 32631 4304 +11 CLA P+11
42652 0 60100 0 34063 4305 +12 STO WR
42653 0 76000 0 00012 4306 +13 OCT

```

ITER PRINT FLAG

NO. ITERATIONS

ERROR RETURN
CURRENT FLOW RATE

42654 U 02000 0 42654 4307 +14 TRA 0+1
4308 NOZZLE FLOW COMPUTED IGNORING CAPACITANCE
42655 0 50000 0 32643 4309 +15 CLA P+21
42656 0 30200 0 32644 4310 +16 FSB P+22
42657 0 30200 0 34045 4311 +17 FSB TP+72
42660 0 60100 0 32646 4312 +18 STD P+24
42661 0 60000 0 32724 4313 +19 STZ X+6
42662 0 60000 0 32731 4314 +20 STZ X+11
42663 0 50000 0 44224 4315 +21 CLA NTOTL
42664 0 24100 0 34124 4316 +22 FDP NUMBR
42665 0 76000 0 00012 4317 +23 DCT
42666 0 07400 4 44235 4318 +24 TSX DIVCK,4
42667 -0 60000 0 44461 4319 +25 STD DELTAZ
42670 -0 63400 0 43262 4320 +26 SKD CNT6,0
42671 -0 63400 0 43377 4321 +27 SKD CNT7,0
42672 -0 63400 0 43460 4322 +28 SKD CNT8,0
42673 -0 63400 0 43536 4323 +29 SKD CNT9,0
42674 0 50000 0 32633 4324 +30 CLA T6
42675 0 30200 0 32620 4325 +31 FSB T3
42676 0 13100 0 00000 4326 +32 XCA
42677 0 26000 0 44467 4327 +33 FHP KON11
42700 0 60100 0 44513 4328 +34 STD MAXER
42701 0 56000 0 32633 4329 +35 LDQ T6
42702 0 26000 0 44154 4330 +36 FHP LVSRN+1
42703 0 13100 0 00000 4331 +37 XCA
42704 0 26000 0 44232 4332 +38 FHP KON55
42705 0 60100 0 44373 4333 +39 STD THINT
42706 0 60100 0 44440 4334 +40 STD TSUBH
42707 0 50000 0 32620 4335 +41 CLA T3
42710 0 56000 0 32621 4336 +42 LDQ P3
42711 0 07400 4 25564 4337 +43 TSX AZH,4
42712 0 02000 0 43576 4338 +44 TRA AZN1
42713 0 50200 0 33723 4339 +45 CLS WPR+1
42714 0 24100 0 40246 4340 +46 FDP FLCUF
42715 0 26000 0 34063 4341 +47 FHP WR
42716 0 13100 0 00000 4342 +48 XCA
42717 0 26000 0 34063 4343 +49 FHP WR
42720 0 13100 0 00000 4344 +50 XCA
42721 0 26000 0 44223 4345 +51 FHP KON39
42722 0 30000 0 32621 4346 +52 FAD P3
42723 0 60100 0 44462 4347 +53 STD PIN
42724 0 77400 4 00060 4348 AZN4 AKT 48,4
42725 0 60000 4 44357 4349 +1 STZ TV+48,4
42726 2 00001 4 42725 4350 +2 TIX 0-1,4,1
42727 0 50000 0 44462 4351 NUTH1 CLA PIN
42730 0 60100 0 44442 4352 +1 STD PSUBC
42731 0 50000 0 32620 4353 +2 CLA T3
42732 0 60100 0 44444 4354 +3 STD TSUBC
42733 0 60100 0 44453 4355 +4 STD TCH
42734 0 50000 0 44373 4356 +5 CLA THINT
42735 0 60100 0 44454 4357 +6 STD TWH
42736 0 50000 0 32641 4358 +7 CLA QINT
42737 0 60100 0 44476 4359 +8 STD Q1
42740 0 50000 0 44144 4360 +9 CLA LVSRN+1

LOWER 01 GUESS FLAG
TOTAL LENGTH

LENGTH OF DELTA Z

MAX ERROR OF CLOSURE BETWEEN T6
INPUT AND COMPUTED T6

.98

INITIAL GUESS OF EXIT TEMP

.025

RETURN HERE AFTER 01 LOWERED

INITIAL GUESS OF COLD WALL TEMP

INITIAL GUESS OF HOT WALL TEMP
RESET 01 WITH INITIAL GUESS

42741 0 60100 0 44434 4361 +10 STD DSUBH
42742 0 50000 0 44154 4362 +11 CLA LVSRN+1
42743 0 60100 0 44434 4363 +12 STD RSUBH
42744 0 50000 0 34124 4364 +13 CLA NUMBR
42745 0 60100 0 44367 4365 +14 STD NLEFT
42746 0 50000 0 44461 4366 +15 CLA DELTAZ
42747 0 60100 0 44460 4367 +16 STD NUM
42750 0 50000 0 44460 4368 DHRN CLA NUM
42751 0 07400 4 44515 4369 +1 TSX TIN1,4
42752 0 00000 0 44143 4370 +2 HTR LVSDH,0,0
42753 0 00004 0 00001 4371 +3 HTR 1,0,4
42754 0 60100 0 44435 4372 +4 STD DSUBH+1
42755 0 30000 0 44434 4373 +5 FAD DSUBH
42756 0 13100 0 00000 4374 +6 XCA
42757 0 26000 0 44472 4375 +7 FHP KON8
42760 0 60100 0 44413 4376 +8 STD DSUBH1
42761 0 50000 0 44460 4377 +9 CLA NUM
42762 0 07400 4 44515 4378 +10 TSX TIN1,4
42763 0 00000 0 44153 4379 +11 HTR LVSRN,0,0
42764 0 00004 0 00001 4380 +12 HTR 1,0,4
42765 0 60100 0 44437 4381 +13 STD RSUBH+1
42766 0 50000 0 44460 4382 +14 CLA NUM
42767 0 07400 4 44515 4383 +15 TSX TIN1,4
42770 0 00000 0 44163 4384 +16 HTR LVSDH,0,0
42771 0 00007 0 00001 4385 +17 HTR 1,0,7
42772 0 60100 0 44412 4386 +18 STD CH
42773 0 50000 0 44440 4387 FINQ1 CLA TSUBH
42774 0 56000 0 32656 4388 +1 LDQ P+32
42775 0 07400 4 25564 4389 +2 TSX AZH,4
42776 0 02000 0 43576 4390 +3 TRA AZN1
42777 0 56000 0 33731 4391 +4 LDQ WPR+7
43000 0 26000 0 32646 4392 +5 FHP P+24
43001 0 60100 0 12512 4393 +6 STD COMMON
43002 0 50000 0 44476 4394 +7 CLA Q1
43003 0 24100 0 12512 4395 +8 FDP COMMON
43004 0 76000 0 00012 4396 +9 DCT
43005 0 07400 4 44235 4397 +10 TSX DIVCK,4
43006 -0 60000 0 12512 4398 +11 STD COMMON
43007 0 50000 0 44440 4399 +12 CLA TSUBH
43010 0 24100 0 44436 4400 +13 FDP RSUBH
43011 0 76000 0 00012 4401 +14 DCT
43012 0 07400 4 44235 4402 +15 TSX DIVCK,4
43013 0 13100 0 00000 4403 +16 XCA
43014 0 30000 0 12512 4404 +17 FAD COMMON
43015 0 13100 0 00000 4405 +18 XCA
43016 0 26000 0 44437 4406 +19 FHP RSUBH+1
43017 0 60100 0 44441 4407 +20 STD TSUBH+1
43020 0 30000 0 44440 4408 +21 FAD TSUBH
43021 0 13100 0 00000 4409 +22 XCA
43022 0 26000 0 44472 4410 +23 FHP KON8
43023 0 60100 0 44446 4411 +24 STD TSUBH1
43024 0 50000 0 44444 4412 +25 CLA TSUBC
43025 0 56000 0 44442 4413 +26 LDQ PSUBC
43026 0 07400 4 25564 4414 +27 TSX AZH,4

DIAMETER AT POINT N

RECOVERY FACTOR AT POINT N
NUMBER OF DELTA Z

TOTAL LENGTH USE TO POINT N+M
FIND DIAMETER AT POINT N+M N=1,2...

AVERAGE

FIND RECOVERY FACTOR AT POINT N+M

FIND CIRCUM. HOT

P6

FIND C SUB P HOT

NOZZLE FLOW (HOT SIDE)
C SUB P (WR)
FIND TEMP AT NEXT SEGMENT OF
HOT SIDE

TEMP AT BEGIN OF NEXT SEGMENT

MEAN HOT TEMP OF THE SEGMENT

C SUB P COLD

43027	0	02C00	0	43574	4415	+28	TRA	AZN1		
43030	0	50000	0	33731	4416	+29	CLA	WPR+7		
43031	0	13100	0	00000	4417	+30	XCA		C P	
43032	0	26000	0	34063	4418	+31	FMP	WA		C SUB P COLD
43033	0	40100	0	12512	4419	+32	STO	COMMON		
43034	0	50000	0	44474	4420	+33	CLA	Q1		FIND TEMP OF NEXT SEGMENT OF COLD SIDE
43035	0	24100	0	12512	4421	+34	FDP	COMMON		
43036	0	76C00	0	00012	4422	+35	DCT			
43037	0	07400	4	44235	4423	+36	TSX	DIVCK,4		
43040	0	13100	0	00000	4424	+37	XCA			
43041	0	30000	0	44444	4425	+38	FAD	TSUBC		
43042	0	60100	0	44443	4426	+39	STO	TSUBC+1		TEMP BEGIN OF NEXT SEGMENT
43043	0	30000	0	44444	4427	+40	FAD	TSUBC		
43044	0	13100	0	00000	4428	+41	XCA			
43045	0	26000	0	44472	4429	+42	FMP	KON8		
43046	0	60100	0	44447	4430	+43	STO	TSUBC1		MEAN COLD TEMP OF THE SEGMENT
43047	0	50000	0	44460	4431	+44	CLA	NUM		
43050	0	30200	0	44461	4432	+45	F58	DELTAZ		
43051	0	60100	0	44500	4433	+46	STO	TEMP		
43052	0	07400	4	44515	4434	+47	TSX	TINI,4		FIND WETTED PERIMETER NEEDED
43053	0	00000	0	44125	4435	+48	HTR	LVSAC,0,0		
43054	0	00007	0	00001	4436	+49	HTR	1,0,7		
43055	0	60100	0	44451	4437	+50	STO	CCI		
43056	0	50000	0	44500	4438	+51	CLA	TEMP		
43057	0	07400	4	44515	4439	+52	TSX	TINI,4		FIND COLD FLOW HEAT TRANSFER AREA
43060	0	00000	0	44107	4440	+53	HTR	LVSAC,0,0		
43061	0	00007	0	00001	4441	+54	HTR	1,0,7		
43062	0	60100	0	44450	4442	+55	STO	ACI		COLD FLOW HEAT TRANSFER AREA
43063	0	24100	0	44451	4443	+56	FDP	CCI		WETTED PERIMETER OF COLD FLOW
43064	0	76000	0	00012	4444	+57	DCT			
43065	0	07400	4	44235	4445	+58	TSX	DIVCK,4		
43066	0	26000	0	40216	4446	+59	FMP	KON40		4
43067	0	60100	0	44452	4447	+60	STO	DSUBC		COLD FLOW HYDRAULIC DIAMETER
43070	0	13100	0	00000	4448	+61	XCA			
43071	0	26000	0	44473	4449	+62	FMP	KON5		64.4 = 2 G
43072	0	13100	0	00000	4450	+63	XCA			
43073	0	26000	0	44450	4451	+64	FMP	ACI		
43074	0	13100	0	00000	4452	+65	XCA			
43075	0	26000	0	44450	4453	+66	FMP	ACI		
43076	0	60100	0	44502	4454	+67	STO	TEMP+2		
43077	0	50000	0	44447	4455	+68	CLA	TSUBC1		
43100	0	56000	0	44442	4456	+69	LDQ	PSUBC		
43101	0	07400	4	25564	4457	+70	TSX	AZH,4		
43102	0	02000	0	43576	4458	+71	TRA	AZN1		
43103	0	50000	0	33723	4459	+72	CLA	WPR+1	1/RHO	
43104	0	24100	0	40245	4460	+73	FDP	FLCUF		
43105	0	26000	0	44465	4461	+74	FMP	KON1		144
43106	0	13100	0	00000	4462	+75	XCA			
43107	0	26000	0	34063	4463	+76	FMP	WR		COLD FLOW
43110	0	13100	0	00000	4464	+77	XCA			
43111	0	26000	0	34063	4465	+78	FMP	WR		COLD FLOW
43112	0	24100	0	44502	4466	+79	FDP	TEMP+2		
43113	0	76000	0	00012	4467	+80	DCT			
43114	0	07400	4	44235	4468	+81	TSX	DIVCK,4		
43115	0	26000	0	44461	4469	+82	FMP	DELTAZ		LENGTH OF SEGMENT
43116	0	13100	0	00000	4470	+83	XCA			
43117	0	26000	0	40216	4471	+84	FMP	KON40		4
43120	0	13100	0	00000	4472	+85	XCA			
43121	0	26000	0	36123	4473	+86	FMP	FRICT		FRICTION FACTOR
43122	0	76C00	0	00002	4474	+87	CHS			
43123	0	30C00	0	44442	4475	+88	FAD	PSUBC		
43124	0	60100	0	44443	4476	+89	STO	PSUBC+1		PRESS AT NEXT SEGMENT
43125	0	56C00	0	44450	4477	+90	LDQ	ACI		
43126	0	26C00	0	40216	4478	+91	FMP	KON40		4
43127	0	60100	0	44500	4479	+92	STO	TEMP		4(ACI)
43130	0	50000	0	44447	4480	+93	CLA	TSUBC1		AVERAGE COLD TEMP
43131	0	56000	0	44442	4481	+94	LDQ	PSUBC		
43132	0	07400	4	25564	4482	+95	TSX	AZH,4		
43133	0	02000	0	43576	4483	+96	TRA	AZN1		
43134	0	07400	4	26223	4484	+97	TSX	AZL,4		L
43135	0	13100	0	00000	4485	+98	XCA			L SUB CI
43136	0	26000	0	43605	4486	+99	FMP	GAMMAC		FIND HEAT TRANSFER COEFFICIENT COLD
43137	0	24100	0	44500	4487	+100	FDP	TEMP		FOR COLD SIDE
43140	0	76000	0	00012	4488	+101	DCT			
43141	0	07400	4	44235	4489	+102	TSX	DIVCK,4		
43142	-0	60000	0	44502	4490	+103	STQ	TEMP+2		
43143	0	50000	0	40275	4491	+104	CLA	KON44		PI
43144	0	07400	4	24307	4492	+105	TSX	LN,4		
43145	0	07400	4	44243	4493	+106	TSX	ERLN,4		
43146	0	13100	0	00000	4494	+107	XCA			
43147	0	26000	0	40256	4495	+108	FMP	KON41		.8
43150	0	07400	4	24240	4496	+109	TSX	EXP,4		
43151	0	07400	4	44254	4497	+110	TSX	EREXP,4		
43152	0	13100	0	00000	4498	+111	XCA			
43153	0	26000	0	44502	4499	+112	FMP	TEMP+2		
43154	0	60100	0	44502	4500	+113	STO	TEMP+2		
43155	0	50000	0	34063	4501	+114	CLA	WR		COLD FLOW
43156	0	07400	4	24307	4502	+115	TSX	LN,4		
43157	0	07400	4	44243	4503	+116	TSX	ERLN,4		
43160	0	13100	0	00000	4504	+117	XCA			
43161	0	26000	0	40256	4505	+118	FMP	KON41		.8
43162	0	07400	4	24240	4506	+119	TSX	EXP,4		
43163	0	07400	4	44254	4507	+120	TSX	EREXP,4		
43164	0	13100	0	00000	4508	+121	XCA			
43165	0	26000	0	44502	4509	+122	FMP	TEMP+2		
43166	0	60100	0	44502	4510	+123	STO	TEMP+2		
43167	0	50000	0	44451	4511	+124	CLA	CCI		
43170	0	07400	4	24307	4512	+125	TSX	LN,4		
43171	0	07400	4	44243	4513	+126	TSX	ERLN,4		
43172	0	13100	0	00000	4514	+127	XCA			
43173	0	26000	0	40251	4515	+128	FMP	KON42		.2
43174	0	07400	4	24240	4516	+129	TSX	EXP,4		
43175	0	07400	4	44254	4517	+130	TSX	EREXP,4		
43176	0	13100	0	00000	4518	+131	XCA			
43177	0	26000	0	44502	4519	+132	FMP	TEMP+2		
43200	0	60100	0	44502	4520	+133	STO	TEMP+2		
43201	0	50000	0	44452	4521	+134	CLA	DSUBC		

43203	0	60100	0	12512	4523	+134	STO	COMMON	
43204	0	50000	0	44452	4524	+137	CLA	DSUBC	
43205	0	24100	0	12512	4525	+138	FDP	COMMON	
43206	0	76000	0	00012	4526	+139	DCY		
43207	0	07400	4	44235	4527	+140	TSX	DIVCK,4	
43210	0	13100	0	00000	4528	+141	XCA		
43211	0	07400	4	24307	4529	+142	TSX	LN,4	
43212	0	07400	4	44243	4530	+143	TSX	ERLN,4	
43213	0	13100	0	00000	4531	+144	XCA		
43214	0	26000	0	43604	4532	+145	FMP	BETAC	
43215	0	07400	4	24240	4533	+146	TSX	EXP,4	
43216	0	07400	4	44254	4534	+147	TSX	EREXP,4	
43217	0	13100	0	00000	4535	+148	XCA		
43220	0	26000	0	44502	4536	+149	FMP	TEMP+2	
43221	0	60100	0	44502	4537	+150	STO	TEMP+2	
43222	0	50000	0	44447	4538	NUTCH	CLA	TSUBCI	AVERAGE COLD TEMP
43223	0	24100	0	44453	4539	+1	FDP	TCW	COLD WALL TEMP
43224	0	76000	0	00012	4540	+2	DCY		
43225	0	07400	4	44235	4541	+3	TSX	DIVCK,4	
43226	0	13100	0	00000	4542	+4	XCA		
43227	0	07400	4	24307	4543	+5	TSX	LN,4	
43230	0	07400	4	44243	4544	+6	TSX	ERLN,4	
43231	0	13100	0	00000	4545	+7	XCA		
43232	0	26000	0	43603	4546	+8	FMP	ALPHAC	
43233	0	07400	4	24240	4547	+9	TSX	EXP,4	
43234	0	07400	4	44254	4548	+10	TSX	EREXP,4	
43235	0	13100	0	00000	4549	+11	XCA		
43236	0	26000	0	44502	4550	+12	FMP	TEMP+2	
43237	0	60100	0	44455	4551	+13	STO	HCI	HEAT TRANSFER COEFFICIENT COLD SIDE
43240	0	13100	0	00000	4552	+14	XCA		
43241	0	26000	0	44461	4553	+15	FMP	DELTA2	LENGTH OF SEGMENT
43242	0	13100	0	00000	4554	+16	XCA		
43243	0	26000	0	44412	4555	+17	FMP	CH	HOT CIRCUM. AREA
43244	0	60100	0	12512	4556	+18	STO	COMMON	
43245	0	50000	0	44474	4557	+19	CLA	Q1	HEAT TRANSFER RATE
43246	0	24100	0	12512	4558	+20	FDP	COMMON	
43247	0	76000	0	00012	4559	+21	DCY		
43250	0	07400	4	44235	4560	+22	TSX	DIVCK,4	
43251	0	13100	0	00000	4561	+23	XCA		
43252	0	30000	0	44447	4562	+24	FAD	TSUBCI	
43253	0	13100	0	00000	4563	+25	XCA		TEMP COLD WALL PRIME
43254	0	50000	0	44453	4564	+26	CLA	TCW	TEMP COLD WALL
43255	0	07401	2	43624	4565	+27	TSX	ITER,2,1	
43256	-0	44446	0	44324	4566	+28	MZE	TY+21,,KON17	
43257	0	44447	0	44325	4567	+29	PZE	TY+22,,KON11	
43260	0	44474	0	44326	4568	+30	PZE	TY+23,,KON10	
43261	3	44453	0	44266	4569	+31	PTH	LTCW,,TCW	
43262	3	00000	0	44266	4570	CNT6	PTH	LTCW	
43263	0	44470	0	44471	4571	+1	PZE	KON13,,KON12	
43264	0	02000	0	43267	4572	+2	TRA	TCWOK	CLOSED
43265	0	60100	0	44453	4573	+3	STO	TCW	NEW GUESS COLD WALL TEMP
43266	0	02000	0	43222	4574	+4	TRA	NUTCH	
43267	0	50000	0	44413	4575	TCWOK	CLA	DSUBHI	AVERAGE DIAMETER
43270	0	07400	4	24307	4576	+1	TSX	LN,4	
43271	0	07400	4	44243	4577	+2	TSX	ERLN,4	
43272	0	13100	0	00000	4578	+3	XCA		
43273	0	26000	0	44230	4579	+4	FMP	KON53	1.8
43274	0	07400	4	24240	4580	+5	TSX	EXP,4	
43275	0	07400	4	44254	4581	+6	TSX	EREXP,4	
43276	0	60100	0	44500	4582	+7	STO	TEMP	
43277	0	50000	0	44446	4583	+8	CLA	TSUBHI	AVERAGE HOT TEMP
43300	0	56000	0	32656	4584	+9	LDQ	P+32	P6
43301	0	07400	4	25564	4585	+10	TSX	AZH,4	
43302	0	02000	0	43556	4586	+11	TRA	BUG	
43303	0	07400	4	26223	4587	+12	TSX	AZL,4	
43304	0	13100	0	00000	4588	+13	XCA		
43305	0	26000	0	44231	4589	+14	FMP	KON54	L SUB HI
43306	0	60100	0	44511	4590	+15	STO	TEMP+9	.026
43307	0	50000	0	34063	4591	+16	CLA	WR	HOT FLOW
43310	0	07400	4	24307	4592	+17	TSX	LN,4	
43311	0	07400	4	44243	4593	+18	TSX	ERLN,4	
43312	0	13100	0	00000	4594	+19	XCA		
43313	0	26000	0	40256	4595	+20	FMP	KON41	.8
43314	0	07400	4	24240	4596	+21	TSX	EXP,4	
43315	0	07400	4	44254	4597	+22	TSX	EREXP,4	
43316	0	13100	0	00000	4598	+23	XCA		
43317	0	26000	0	44511	4599	+24	FMP	TEMP+9	
43320	0	24100	0	44500	4600	+25	FDP	TEMP	
43321	0	76000	0	00012	4601	+26	DCY		
43322	0	07400	4	44235	4602	+27	TSX	DIVCK,4	
43323	-0	60000	0	44511	4603	+28	STQ	TEMP+9	
43324	0	50000	0	44460	4604	+29	CLA	NUM	
43325	0	30200	0	44461	4605	+30	FSB	DELTA2	LENGTH OF SEGMENT
43326	0	07400	4	44515	4606	+31	TSX	TINI,4	
43327	0	00000	0	44201	4607	+32	HTR	LVSTIG,0,0	
43330	0	00011	0	00001	4608	+33	HTR	1,0,9	
43331	0	60100	0	44512	4609	+34	STO	SIGMA	
43332	0	50000	0	44446	4610	NUTHM	CLA	TSUBHI	AVERAGE HOT TEMP
43333	0	30000	0	44454	4611	+1	FAD	THW	HOT WALL TEMP
43334	0	60100	0	12512	4612	+2	STO	COMMON	
43335	0	56000	0	44512	4613	+3	LDQ	SIGMA	
43336	0	26000	0	44446	4614	+4	FMP	TSUBHI	
43337	0	24100	0	12512	4615	+5	FDP	COMMON	
43340	0	76000	0	00012	4616	+6	DCY		
43341	0	07400	4	44235	4617	+7	TSX	DIVCK,4	
43342	0	13100	0	00000	4618	+8	XCA		
43343	0	07400	4	24307	4619	+9	TSX	LN,4	
43344	0	07400	4	44243	4620	+10	TSX	ERLN,4	
43345	0	13100	0	00000	4621	+11	XCA		
43346	0	26000	0	40256	4622	+12	FMP	KON41	
43347	0	07400	4	24240	4623	+13	TSX	EXP,4	
43350	0	07400	4	44254	4624	+14	TSX	EREXP,4	
43351	0	13100	0	00000	4625	+15	XCA		
43352	0	26000	0	44511	4626	+16	FMP	TEMP+9	
43353	0	60100	0	44456	4627	+17	STO	HHI	HEAT TRANSFER COEFFICIENT HOT
43354	0	13100	0	00000	4628	+18	XCA		
43355	0	26000	0	44412	4629	+19	FMP	CH	
43356	0	13100	0	00000	4630	+20	YCA		

43357	0	26000	0	44461	4631	+21	FMP	DELTAZ		LENGTH OF SEGMENT
43360	0	60100	0	12512	4632	+22	STO	COMMON		
43361	0	50000	0	44476	4633	+23	CLA	Q1		HEAT TRANSFER RATE
43362	0	24100	0	12512	4634	+24	FDP	COMMON		
43363	0	76000	0	00012	4635	+25	DCT			
43364	0	07400	4	44235	4636	+26	TSX	DIVCK,4		
43365	0	13100	0	00000	4637	+27	XCA			
43366	0	76000	0	00002	4638	+28	CMS			
43367	0	30000	0	44446	4639	+29	FAD	TSUBHI		AVERAGE HOT TEMP
43370	0	13100	0	00000	4640	+30	XCA			HOT WALL TEMP PRIME
43371	0	50000	0	44454	4641	+31	CLA	THW		HOT WALL TEMP
43372	0	07402	2	43624	4642	+32	TSX	ITER,2,2		
43373	0	44466	0	44327	4643	+33	PZE	TY+24,,KON17		
43374	0	44467	0	44330	4644	+34	PZE	TY+25,,KON11		
43375	0	44474	0	44331	4645	+35	PZE	TY+26,,KON10		
43376	3	44454	0	44265	4646	+36	PTH	LTHW,,THW		
43377	3	00000	0	44265	4647					
43400	0	44470	0	44471	4648					
43401	0	02000	0	43404	4649	+1	PZE	KON13,,KON12		
43402	0	60100	0	44454	4650	+2	TRA	THWOK		CLOSED
43403	0	02000	0	43332	4651	+3	STO	THW		NEW GUESS HOT WALL TEMP
43404	0	50000	0	44454	4652	+4	TRA	NUTHW		
43405	0	30000	0	44453	4653					
43406	0	13100	0	00000	4654					
43407	0	26000	0	44472	4655	+1	FAD	TCW		
43410	0	13100	0	00000	4656	+2	XCA			.5
43411	0	26000	0	44226	4657	+3	FMP	KON51		
43412	0	30000	0	44225	4658	+6	FAD	KON50		
43413	0	13100	0	00000	4659	+7	XCA			
43414	0	26000	0	44227	4660	+8	FMP	KON52		
43415	0	60100	0	44457	4661	+9	STO	KM		THERMAL CONDUCTIVITY
43416	0	50000	0	36125	4662	+10	CLA	XTHIK		METAL THICKNESS
43417	0	24100	0	44457	4663	+11	FDP	KM		
43420	0	76000	0	00012	4664	+12	DCT			
43421	0	07400	4	44235	4665	+13	TSX	DIVCK,4		
43422	-0	60C00	0	12512	4666	+14	STQ	COMMON		
43423	0	50000	0	44474	4667	+15	CLA	KON10		1
43424	0	24100	0	44456	4668	+16	FDP	HHI		HOT SIDE HEAT TRANSFER COEFFICIENT
43425	0	76000	0	00012	4669	+17	DCT			
43426	0	07400	4	44235	4670	+18	TSX	DIVCK,4		
43427	0	13100	0	00000	4671	+19	XCA			
43430	0	30000	0	12512	4672	+20	FAD	COMMON		
43431	0	60100	0	12512	4673	+21	STO	COMMON		
43432	0	50000	0	44474	4674	+22	CLA	KON10		1
43433	0	24100	0	44455	4675	+23	FDP	HCI		COLD SIDE HEAT TRANSFER COEFFICIENT
43434	0	76000	0	00012	4676	+24	DCT			
43435	0	07400	4	44235	4677	+25	TSX	DIVCK,4		
43436	0	13100	0	00000	4678	+26	XCA			
43437										

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43533 0 44467 0 44336 4739 +11 PZE TY+31,,KON11
43534 0 44474 0 44337 4740 +12 PZE TY+32,,KON10
43535 3 44373 0 43623 4741 +13 PTH LT6,,THINT
43536 3 00000 0 43622 4742 CNT9 PTH LTH
43537 0 44470 0 44471 4743 +1 PZE KON13,,KON12
43540 0 02000 0 43544 4744 +2 TRA CLOSD
43541 0 60100 0 44373 4745 +3 STO THINT
43542 0 60100 0 44440 4746 +4 STO TSUBH
43543 0 02000 0 42727 4747 +5 TRA NUTHI
43544 0 50000 0 44445 4748 CLOSD CLA TSUBC+1
43545 0 56000 0 44443 4749 +1 LDQ PSUBC+1
43546 0 60100 0 32620 4750 +2 STO T3
43547 -0 60000 0 32621 4751 +3 STQ P3
43550 0 50000 0 44476 4752 +4 CLA Q1
43551 0 60100 0 32641 4753 +5 STO QLINT
43552 0 77400 4 00000 4754 AZNR AXT **0,4
43553 0 77400 1 00000 4755 +1 AXT **0,1
43554 0 77400 2 00000 4756 +2 AXT **0,2
43555 0 02000 4 00003 4757 +3 TRA 3,4
43556 0 52000 0 32731 4758 BUG ZET X+11
43557 0 02000 0 43567 4759 +1 TRA BUG2
43560 0 50000 0 32641 4760 +2 CLA QLINT
43561 0 24100 0 40224 4761 +3 FDP FL10
43562 -0 60000 0 32641 4762 +4 STQ QLINT
43563 -0 62500 0 32731 4763 +5 STL X+11
43564 0 50000 0 32703 4764 +6 CLA P+53
43565 0 60100 0 32620 4765 +7 STO T3
43566 0 02000 0 42724 4766 +8 TRA AZN4
43567 -0 62500 0 32724 4767 BUG2 STL X+6
43570 -0 63400 4 00061 4768 +1 SXD KINDX4,4
43571 0 52200 0 43552 4769 +2 XEC AZNR
43572 1 00002 4 43553 4770 +3 TXI AZNR+1,4,2
43573 -0 54671 7 14325 4771 BUG1 BCI 3,NOZZLE TUBE ERROR
43576 0 16200 0 43556 4772 AZN1 TQP BUG
43577 -0 62500 0 32724 4773 +1 STL X+6
43600 -0 63400 4 00061 4774 +2 SXD KINDX4,4
43601 0 52200 0 43552 4775 +3 XEC AZNR
43602 1 00001 4 43553 4776 +4 TXI AZNR+1,4,1
43603 1 77534 1 21727 4781 KON40 EQU FL4
43604 0 00000 0 00000 4782 KON41 EQU FL.8
43605 1 73543 4 20626 4783 KON42 EQU FL.2
43606 0 77400 1 00000 4784 KON44 EQU PI
43607 3 00000 1 44243 4785 ALPHAC DEC .34
43610 1 00001 1 43611 4786 BETAC DEC 0
43611 0 63400 1 43606 4787 GAMMAC DEC .0217
43612 0 50000 0 32641 4788 QINU AXT 0,1
43613 0 60100 0 44476 4789 +1 TXH ERLN,1,0
43614 0 50000 0 44373 4790 +2 TXI **1,1,1
43615 0 60100 0 44454 4791 +3 SXA *-3,1
43616 0 60000 0 44327 4792 +4 CLA QLINT
43617 0 60000 0 44330 4793 +5 STO Q1
43620 0 60000 0 44331 4794 +6 CLA THINT
43621 0 02000 0 42773 4795 +7 STO TMW
43622 -2 36025 6 73163 4796 +8 STZ TY+24
43623 -2 30660 6 06060 4797 +9 STZ TY+25
43624 0 63400 4 44010 4799 +10 STZ TY+26
43625 0 63400 1 44011 4800 +11 TRA FINQ1
43626 0 60000 0 32735 4801 LTH BCI 1,T EXIT
43627 0 60100 0 44073 4802 LT6 BCI 1,T6
43630 -0 60000 0 44074 4803 G E N E R A L N E W T O N T Y P E I T E R A T I O N S C H E M E
43631 0 30200 0 44074 4804 ITER SXA ITERX,4
43632 0 60100 0 44076 4805 +1 SXA ITERX+1,1
43633 0 24100 0 44074 4806 +2 STZ X+15
43634 -0 60000 0 44077 4807 +3 STO Q
43635 0 50000 2 00004 4808 +4 STQ Q+1
43636 -0 73700 4 00000 4809 +5 FSB Q+1
43637 0 50000 4 00000 4810 +6 STO Q+3
43640 0 60100 0 44075 4811 +7 FDP Q+1
43641 0 50000 2 00001 4812 +8 STQ Q+4
43642 -0 73700 4 00000 4813 +9 CLA 4,2
43643 0 50000 4 00000 4814 +10 PDC 0,4
43644 0 76500 0 00000 4815 +11 CLA 0,4
43645 0 04000 0 43765 4816 +12 STO Q+2
43646 0 50000 2 00001 4817 +13 CLA 1,2
43647 -0 12000 0 43723 4818 +14 PDC 0,4
43650 -0 32000 0 44046 4819 +15 CLA 0,4
43651 -0 10000 0 43662 4820 +16 LRS 0
43652 0 50000 2 00002 4821 +17 TLQ ITER7
43653 -0 73700 4 00000 4822 ITER1 CLA 1,2
43654 0 56000 4 00000 4823 +1 SXA ITER4
43655 0 26000 0 44075 4824 +2 STZ X+15
43656 0 24100 0 44074 4825 +3 STO Q
43657 0 26000 0 44073 4826 +4 STQ Q+1
43660 0 60100 0 44102 4827 +5 FSB Q+3
43661 0 02000 0 43720 4828 +6 STO Q+2
43662 -0 52060 2 00001 4829 +7 FDP Q+1
43663 0 02000 0 43652 4830 +8 STQ Q+7
43664 0 50000 2 00004 4831 +9 TRA ITER3
43665 -0 73700 4 00000 4832 ITER2 NZT* 1,2
43666 0 50000 2 00006 4833 +1 TRA ITER1
43667 -0 73700 1 00000 4834 +2 CLA 4,2
43670 0 50000 4 00000 4835 +3 PDC 0,4
43671 0 60100 0 44075 4836 +4 CLA 6,2
43672 0 30260 2 00003 4837 +5 PDC 0,1
43673 0 60100 0 44100 4838 +6 CLA 0,4
43674 0 50060 2 00001 4839 +7 STO Q+2
43675 0 30260 2 00002 4840 +8 FSB* 3,2
43676 0 30200 0 44076 4841 +9 STO Q+5
43677 0 60100 0 44101 4842 +10 CLA* 1,2
43700 0 50000 2 00003 4843 +11 FSB* 2,2
43701 -0 73700 4 00000 4844 +12 FSB Q+3
43702 0 56000 4 00000 4845 +13 STC Q+6
43703 0 26000 0 44100 4846 +14 CLA 3,2
+15 PDC 0,4
+16 LDQ 0,4
+17 FMP Q+5
```

43704	0	24100	0	44101	4847	+18	FDP	Q+6
43705	0	26000	0	44076	4848	+19	FMP	Q+3
43706	0	60100	0	44102	4849	+20	STO	Q+7
43707	0	56060	2	00006	4850	+21	LDO*	6,2
43710	0	76500	0	00000	4851	+22	LRS	0
43711	-0	60000	0	44103	4852	+23	STQ	Q+8
43712	0	56000	1	00000	4853	+24	LDO	0,1
43713	0	76300	0	00000	4854	+25	LLS	0
43714	0	04000	0	43720	4855	+26	TLQ	ITER3
43715	0	50000	0	44075	4856	+27	CLA	Q+2
43716	0	30000	0	44103	4857	+28	FAD	Q+8
43717	0	02000	0	43722	4858	+29	TRA	ITER3+2
43720	0	50000	0	44075	4859	ITER3	CLA	Q+2
43721	0	30000	0	44102	4860	+1	FAD	Q+7
43722	0	60100	0	44104	4861	+2	STO	Q+9
43723	0	50000	2	00005	4862	ITER4	CLA	5,2
43724	-0	73400	4	00000	4863	+1	PDX	0,4
43725	1	00001	4	43726	4864	+2	TXI	**1,4,1
43726	-0	75400	4	00000	4865	+3	PXD	0,4
43727	0	60000	0	44100	4866	+4	STZ	Q+5
43730	0	63400	4	44100	4867	+5	SXA	Q+5,4
43731	0	62200	2	00005	4868	+6	STD	5,2
43732	0	50000	2	00000	4869	+7	CLA	Q+2
43733	0	77100	0	00022	4870	+8	ARS	18
43734	-0	32000	0	40206	4871	+9	ANA	FX7
43735	0	60100	0	44076	4872	+10	STO	Q+3
43736	0	50000	0	44105	4873	+11	CLA	SWT
43737	0	32200	0	40206	4874	+12	ERA	FX7
43740	0	10000	0	43743	4875	+13	TZE	*+3
43741	0	50000	0	44076	4876	+14	CLA	Q+3
43742	0	40200	0	44105	4877	+15	SUB	SWT
43743	3	00050	4	43745	4878	+16	TXH	ITER5,4,40
43744	-0	10000	0	43750	4879	+17	TNZ	ITER6
					4880*MAX NO. ITERATIONS IN DECREMENT			
43745	3	00012	4	44071	4881	ITER5	TXH	ITER+3,4,10
43746	0	77400	1	00000	4882	+1	AXT	0,1
43747	0	07400	4	44021	4883	+2	TSX	ITERP,4
43750	0	50000	0	44073	4884	ITER6	CLA	Q
43751	0	60160	2	00001	4885	+1	STO*	1,2
43752	0	50000	0	44074	4886	+2	CLA	Q+1
43753	0	60160	2	00002	4887	+3	STO*	2,2
43754	0	50000	0	44075	4888	+4	CLA	Q+2
43755	0	60160	2	00003	4889	+5	STO*	3,2
43756	0	60000	0	44075	4890	+6	STZ	Q+2
43757	0	50000	2	00001	4891	+7	CLA	1,2
43760	0	12000	0	43763	4892	+8	TPL	*+3
43761	0	50000	0	44074	4893	+9	CLA	Q+1
43762	1	77777	2	44010	4894	+10	TXI	ITERX,2,-1
43763	0	50000	0	44104	4895	+11	CLA	Q+9
43764	1	77777	2	44010	4896	+12	TXI	ITERX,2,-1
43765	0	50000	0	44105	4897	ITER7	CLA	SWT
43766	0	10000	0	44003	4898	+1	TZE	ITER8
43767	0	50000	2	00000	4899	+2	CLA	Q+2
43770	0	77100	0	00022	4900	+3	ARS	18

FX BUMPER

TEST E LESS THAN DELTA X3

LOOP NO.

PRINT ITERATION

NO PRINT

43771	-0	32000	0	40206	4901	+4	ANA	FX7
43772	0	60100	0	44076	4902	+5	STD	Q+3
43773	0	50000	0	44105	4903	+6	CLA	SWT
43774	0	40200	0	40206	4904	+7	SUB	FX7
43775	0	10000	0	44001	4905	+8	TZE	ITER7A
43776	0	50000	0	44076	4906	+9	CLA	Q+3
43777	0	40200	0	44105	4907	+10	SUB	SWT
44000	-0	10000	0	44003	4908	+11	TNZ	ITER8
44001	0	77400	1	00001	4909	ITER7A	AXT	1,1
44002	0	07400	4	44021	4910	+1	TSX	ITERP,4
44003	0	60060	2	00001	4911	ITER8	STZ*	1,2
44004	0	60060	2	00002	4912	+1	STZ*	2,2
44005	0	60060	2	00003	4913	+2	STZ*	3,2
44006	-0	75400	0	00000	4914	+3	PXD	
44007	0	62200	2	00005	4915	+4	STD	5,2
44010	0	77400	4	00000	4916	ITERX	AXT	**0,4
44011	0	77400	1	00000	4917	+1	AXT	**0,1
44012	0	76000	0	00012	4918	+2	DCT	
44013	0	02000	0	44014	4919	+3	TRA	*+1
44014	-0	76000	0	00144	4920	+4	SLT	4
44015	0	02000	2	00007	4921	+5	TRA	7,2
44016	-0	50060	2	00005	4922	+6	CAL*	5,2
44017	0	60200	0	32735	4923	+7	SLW	X+15
44020	0	02000	0	00000	4924	ITER9	TRA	**0
44021	0	63400	4	44042	4925	ITERP	SXA	ITERPX,4
44022	0	07400	4	00052	4926	+1	TSX	DOUT,4
44023	3	01757	0	44047	4927	+2	PTH	ANA+1,,1007
44024	3	01770	0	44050	4928	+3	PTH	ANA+2,,1016
44025	3	02105	0	44051	4929	+4	PTH	ANA+3,,1093
44026	1	02004	2	00005	4930	+5	PON	5,2,1028
44027	1	02031	2	00004	4931	+6	PON	4,2,1049
44030	1	02057	2	00004	4932	+7	PON	4,2,1071
44031	3	02065	0	44052	4933	+8	PTH	ANA+4,,1077
44032	-0	00007	0	44076	4934	+9	FOR	Q+3,,7
44033	-0	00023	0	44100	4935	+10	FOR	Q+5,,19
44034	-3	11660	0	44075	4936	+11	SVN	Q+2,,5040
44035	-3	11706	0	44073	4937	+12	SVN	Q,,5062
44036	-3	11734	0	44074	4938	+13	SVN	Q+1,,5084
44037	-3	17647	0	44077	4939	+14	SVN	Q+4,,8103
44040	1	02133	1	44045	4940	+15	PON	ITBCD+1,1,1115
44041	1	00012	0	44106	4941	+16	PON	MODE,,10
44042	0	77400	4	00000	4942	ITERPX	AXT	**0,4
44043	0	02000	4	00001	4943	+1	TRA	1,4
44044	3	02133	0	44053	4944	ITBCD	PTH	ANA+5,,1115
44045	3	02133	0	40304	4945	+1	PTH	BLANK,,1115
44046	0	00000	0	77777	4946	ANA	PZE	0-1
44047	-0	34646	4	76060	4947	+1	BCI	5,LOOP ITERS.ERROR *
44054	-2	33031	6	26022	4948	ITEXP	BCI	CLOSED
44066	0	07400	4	00052	4949	ITERR	TSX	DOUT,4
44067	3	23610	0	44054	4950	+1	PTH	ITEXP,,10120
44070	1	00012	0	44106	4951	+2	PON	MODE,,10
44071	0	76000	0	00144	4952	+3	SLN	4
44072	0	02000	0	43765	4953	+4	TRA	ITER7
				44073	4954	Q	BSS	10,0

LOOP NO

PRINT ALL LOOP

IR4
IR1

OFF NORMAL RETURN
NAME OF LOOP

PRESET ERROR RETURN

*

THIS BALANCE FAILED TO CONVERGE ** IT MUST BE SUM INPUT **

```

44106 -1 00012 0 00012 44106 4955 SMT BSS 1,X
44106 4956 MODE FVE KPRINT,,10
44107 4957 DISTANCE VS COLD FLOW HEAT TRANSFER AREA
44107 4958 LVSAC BSS 14,F
44125 4959 DISTANCE VS COLD FLOW WETTED PERIMETER
44125 4960 LVSCC BSS 14,F
44143 4961 DISTANCE VS DIAMETER TABLE
44143 4962 LVSDM BSS 8,F
44153 4963 DISTANCE VS RECOVERY FACTOR TABLE
44153 4964 LVSRM BSS 8,F
44163 4965 DISTANCE VS CIRCUMFERENCE TABLE OF HOT FLOW AREA
44163 4966 LVSCM BSS 14,F
44201 4967 DISTANCE VS SIGMA
44201 4968 LVSIG BSS 18,F
44223 4969 KON39 BSS 1,F
44224 4970 NTOTL BSS 1,F
44225 4971 KON50 BSS 1,F
44226 4972 KON51 BSS 1,F
44227 4973 KON52 BSS 1,F
44230 4974 KON53 BSS 1,F
44231 4975 KON54 BSS 1,F
44232 4976 KON55 BSS 1,F
44233 4977 AZN3 BSS 2,F
44235 0 63600 4 44514 4978 DIVCK SCA LAST,4
44236 0 02000 0 43556 4979 +1 TRA BUG
44237 2 43165 3 12631 4980 +2 BCI 4, DIVIDING BY 0 AT LOC
44243 0 63600 4 44514 4981 ERLN SCA LAST,4
44244 0 02000 0 43556 4982 +1 TRA BUG
44245 2 55151 4 65160 4983 +2 BCI 7, ERROR WHEN TAKING LN OF A NUMBER LOC
44254 0 63600 4 44514 4984 EREXP SCA LAST,4
44255 0 02000 0 43556 4985 +1 TRA BUG
44256 2 55151 4 65160 4986 +2 BCI 7, ERROR WHEN GETTING EXP. OF A NUMBER LOC
44256 -2 33066 6 06060 4987 LTMW BCI 1, TMW
44256 -2 33066 6 06060 4988 LTCM BCI 1, TCM
44267 -2 33033 3 14563 4989 +1 BCI 1, TM,INT
44270 2 16367 3 02160 4990 +2 BCI 1, ALPHA
44271 2 72144 4 42160 4991 +3 BCI 1, GAMMA
44272 2 22563 2 16060 4992 +4 BCI 1, BETA
44273 -2 62143 4 36063 4993 +5 BCI 2, WALL THICK.
44275 2 65131 2 33360 4994 +7 BCI 2, FRIC. FACTOR
44277 4995 TY BSS 48,H
44277 4996 INDAT BSS 8,H
44277 4997 MLEFT BSS 1,D
44277 4998 THENT BSS 3
44277 5000 THENT BSS 1,H
44277 5001 PRICY EQU DNZFF
44277 5002 QINT EQU P+19
44277 5003 CM BSS 1,D
44277 5004 NUMBR EQU DNP
44277 5005 DSUBM BSS 1,D
44277 5006 DSUBM BSS 6
44277 5007 DSUBM BSS 10
44277 5008 XTHIK EQU DMT
44277 5009 XTHIK EQU DMT

I AT THROAT, THROAT AREA
STORAGE USE WITH ITERATION ROUTINE
INITIAL GUESS OF EXIT TEMP
NOZZLE TUBE FRICTION FACTOR
INITIAL Q1 GUESS
NO. PARTS
AVERAGE OF DIAMETERS N AND N+1
WALL THICKNESS

44434 5009 DSUBM BSS 2,H
44436 5010 RSUBM BSS 2,H
44440 5011 TSUBM BSS 2,H
44442 5012 PSUBC BSS 2,H
44444 5013 TSUBC BSS 2,H
44446 5014 TSUBM BSS 1,H
44447 5015 TSUBCI BSS 1,H
44450 5016 ACI BSS 1,H
44451 5017 CCI BSS 1,H
44452 5018 DSUBC BSS 1,H
44453 5019 TCM BSS 1,H
44454 5020 TMW BSS 1,H
44455 5021 HCI BSS 1,H
44456 5022 HHI BSS 1,H
44457 5023 KM BSS 1,H
44460 5024 NUM BSS 1,H
44461 5025 DELTAZ BSS 1,H
44462 5026 PIN BSS 1,F
44463 5027 AZN2 BSS 1,F
44464 -1 00160 6 06060 5028* TEMPORARY STORAGE AND CONSTANTS FOR CHECKOUT
44465 2 10440 0 00000 5029 LQ1 BCI 1,Q1
44466 1 67406 1 11565 5030 KON1 DEC 144.
44467 1 72507 5 34122 5031 KON17 DEC .001
44470 1 60517 4 26542 5032 KON11 DEC .01
44471 1 37667 6 33766 5033 KON12 DEC .00001
44472 2 00400 0 00000 5034 KON13 DEC .0000000001
44473 2 07401 4 63146 5035 KON8 DEC .5
44474 2 01400 0 00000 5036 KON5 DEC 64.4
44475 5037 KON10 DEC 1.
44475 5038 AZN5 BSS 1,X
44475 5039 P3 EQU P+3
44475 5040 T3 EQU P+2
44475 5041 WR EQU TP+86
44475 5042 Q1 BSS 1,X
44475 5043 T6 EQU P+13
44475 5044 RHO4 BSS 1,X
44475 5045 TEMP BSS 10,X
44475 5046 SIGMA BSS 1,D
44475 5047 MAXER BSS 1,D
44475 5048 LAST BSS 1,X
44475 5049 TINI STO TINI+98
44475 5050 +1 SXD TINI+87,1
44475 5051 +2 SXD TINI+88,2
44475 5052 +3 SXD TINI+89,4
44475 5053 +4 CLA 2,4
44475 5054 +5 STO TINI+94
44475 5055 +6 ADD TINI+91
44475 5056 +7 PAX 0,1
44475 5057 +8 SXD TINI+29,1
44475 5058 +9 ALS 1
44475 5059 +10 STA TINI+95
44475 5060 +11 CLA TINI+94
44475 5061 +12 ARS 17
44475 5062 +13 SUB TINI+95

COLD FLOW HEAT TRANSFER AREA
WETTED PERIMETER COLD FLOW
HYDRAULIC DIAMETER OF COLD FLOW
TEMP COLD WALL
TEMP HOT WALL
HEAT TRANSFER COEFFICIENT COLD SIDE
HEAT TRANSFER COEFFICIENT HOT SIDE
THERMAL CONDUCTIVITY
INLET PRESSURE

```

```

44533 0 73400 1 00000 5063
44534 -0 43400 1 44534 5064
44535 0 40700 0 44534 5065
44536 0 73400 1 00000 5066
44537 0 40000 4 00001 5067
44540 0 62100 0 44544 5068
44541 0 62100 0 44566 5069
44542 0 62100 0 44570 5070
44543 0 50000 0 44557 5071
44544 0 34000 1 00000 5072
44545 2 00002 1 44544 5073
44546 0 02000 0 44547 5074
44547 0 50000 0 44553 5075
44550 0 76000 0 00001 5076
44551 0 02000 0 44566 5077
44552 2 00000 1 44554 5078
44553 -0 53400 1 44647 5079
44554 -3 00000 1 44554 5080
44555 -0 53400 1 44554 5081
44556 -0 75400 1 00000 5082
44557 0 77100 0 00022 5083
44560 0 76000 0 00002 5084
44561 0 40000 0 44544 5085
44562 0 62100 0 44603 5086
44563 0 40000 0 44650 5087
44564 0 62100 0 44601 5088
44565 0 02000 0 44577 5089
44566 0 50000 1 00000 5090
44567 1 00002 1 44570 5091
44570 0 30000 1 00000 5092
44571 0 76500 0 00043 5093
44572 0 26000 0 44651 5094
44573 0 34000 0 44657 5095
44574 1 77777 1 44552 5096
44575 1 77777 1 44552 5097
44576 1 77775 1 44552 5098
44577 -0 53400 2 44647 5099
44600 0 53400 1 44654 5100
44601 0 50000 1 00000 5101
44602 0 60100 2 12513 5102
44603 0 50000 1 00000 5103
44604 0 30200 0 44657 5104
44605 0 60100 2 12512 5105
44606 1 77776 2 44607 5106
44607 2 00002 1 44601 5107
44610 0 50000 0 12512 5108
44611 0 60100 2 12512 5109
44612 0 53400 4 44653 5110
44613 -0 53400 2 44652 5111
44614 1 77776 2 44615 5112
44615 -0 75400 2 00000 5113
44616 -0 73400 1 00000 5114
44617 0 50000 1 12514 5115
44620 0 30200 2 12512 5116

```

BEGIN SEARCH FOR
K+1 BEST POINTS

TEST EVEN/ODD K

K EVEN
K ODD

BEGIN AITKENS INTERPOLATION

```

44621 0 10000 0 44634 5117
44622 0 60100 0 44656 5118
44623 0 56000 2 12512 5119
44624 0 26000 1 12515 5120
44625 0 60100 0 44655 5121
44626 0 56000 1 12514 5122
44627 0 26000 2 12513 5123
44630 0 30200 0 44655 5124
44631 0 24100 0 44656 5125
44632 -0 60000 1 12515 5126
44633 1 77776 1 44617 5127
44634 0 50000 2 12514 5128
44635 0 60100 1 12514 5129
44636 2 00001 4 44614 5130
44637 0 50000 1 12513 5131
44640 -0 53400 1 44644 5132
44641 -0 53400 2 44645 5133
44642 -0 53400 4 44646 5134
44643 0 02000 4 00003 5135
44644 0 00000 0 00000 5136
44652 0 00002 0 00000 5137
44653 0 00000 0 00000 5138

```

ESCAPE

5140*HOT BLEED PORT ROUTINES

5141*REGION TO INITIALIZE HOT BLEED PORT FOR EACH TIME POINT

```

44660 0 50000 0 32704 5142 HBI CLA P+54 PC
44661 -0 10000 0 44663 5143 +1 TNZ *+2 *CHECKOUT ONLY
44662 0 50000 0 32702 5144 +2 CLA P+52 *CHECKOUT ONLY
44663 0 60100 0 47321 5145 +3 STO PR
44664 0 60100 0 47325 5146 +4 STO PR+4
44665 0 60000 0 47322 5147 +5 STZ PR+1
44666 0 50000 0 32656 5148 +6 CLA P+32 PH
44667 0 60100 0 47323 5149 +7 STO PR+2 P6
44670 0 60000 0 47324 5150 +8 STZ PR+3
44671 0 60000 0 47334 5151 +9 STZ PR+11 P8
44672 0 50000 0 32705 5152 +10 CLA P+55 P08
44673 -0 10000 0 44675 5153 +11 TNZ *+2 TC
44674 0 50000 0 32703 5154 +12 CLA P+53 *CHECKOUT ONLY
44675 0 60100 0 47352 5155 +13 STO PR+25 *CHECKOUT ONLY
44676 0 60100 0 47356 5156 +14 STO PR+29
44677 0 60000 0 47353 5157 +15 STZ PR+26 TH
44700 0 50000 0 32633 5158 +16 CLA P+13 T6
44701 0 60100 0 47354 5159 +17 STO PR+27
44702 0 60000 0 47355 5160 +18 STZ PR+28 T8
44703 0 60000 0 47365 5161 +19 STZ PR+36 T08
44704 0 50000 0 32644 5162 +20 CLA P+22
44705 0 60100 0 47403 5163 +21 STO PR+50
44706 0 50000 0 34045 5164 +22 CLA TP+72
44707 0 60100 0 47404 5165 +23 STO PR+51
44710 0 50000 0 32657 5166 +24 CLA P+33
44711 0 60100 0 47350 5167 +25 STO PR+23 G.P.

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5169*REGION TO OUTPUT HB QUANTITIES

44713	0	50000	0	47334	5170	HBO	CLA	PR+11	
44714	0	60100	0	32640	5171		+1 STO	P+34	P08
44715	0	50000	0	47345	5172		+2 CLA	PR+36	
44716	0	60100	0	32641	5173		+3 STO	P+35	T08
44717	0	50000	0	47404	5174		+4 CLA	PR+51	
44720	0	60100	0	32645	5175		+5 STO	P+23	W00TH
44721	0	50000	0	47407	5176		+6 CLA	PR+54	
44722	0	60100	0	34007	5177		+7 STO	TP+42	W00TNCHOME
44723	0	02000	4	00001	5178		+8 TRA	1,4	

5179*REGION TO INITIALIZE INPUT FOR HOT BLEED PORT

44724	0	50000	0	36152	5180	H02	CLA	DT	
44725	0	60100	0	47341	5181		+1 STO	P+16	
44726	0	50000	0	36136	5182		+2 CLA	DLH	
44727	0	60100	0	47340	5183		+3 STO	PR+15	
44730	0	50000	0	36133	5184		+4 CLA	DR	
44731	0	60100	0	47342	5185		+5 STO	PR+17	
44732	0	50000	0	36130	5186		+6 CLA	ODCO	
44733	0	60100	0	47343	5187		+7 STO	PR+18	
44734	0	50000	0	36131	5188		+8 CLA	DNH	
44735	0	60100	0	47344	5189		+9 STO	PR+19	
44736	0	50000	0	36134	5190		+10 CLA	OTHET	
44737	0	60100	0	47345	5191		+11 STO	PR+20	
44740	0	50000	0	36147	5192		+12 CLA	DNX	
44741	0	60100	0	47370	5193		+13 STO	PR+39	
44742	0	50000	0	36146	5194		+14 CLA	DL	
44743	0	60100	0	47372	5195		+15 STO	PR+41	
44744	0	50000	0	36121	5196		+16 CLA	DA6	
44745	0	60100	0	47422	5197		+17 STO	PR+65	
44746	0	50000	0	36122	5198		+18 CLA	DASTR	
44747	0	60100	0	47430	5199		+19 STO	PR+71	
44750	0	50000	0	36203	5200		+20 CLA	DKFLG	
44751	0	60100	0	47455	5201		+21 STO	PR+92	
44752	0	50000	0	36131	5202		+22 CLA	DAKV	
44753	0	60100	0	47456	5203		+23 STO	PR+93	
44754	0	50000	0	36132	5204		+24 CLA	DBKV	
44755	0	60100	0	47457	5205		+25 STO	PR+94	
44756	0	02000	4	00001	5206		+26 TRA	1,4	

5207*HOT BLEED PORT PROGRAM -- KEN NAGASAWA

44757	0	63400	4	47051	5208	HB	SXA	HBR,4	
44760	0	63400	2	47052	5209		+1 SXA	HBR+1,2	
44761	0	63400	3	47053	5210		+2 SXA	HBR+2,3	
44762	0	63400	1	47054	5211		+3 SXA	HBR+3,1	
44763	0	63400	5	47055	5212		+4 SXA	HBR+4,5	
44764	0	63400	6	47056	5213		+5 SXA	HBR+5,6	
44765	0	63400	7	47057	5214		+6 SXA	HBR+6,7	
44766	0	77400	1	00000	5215		+7 AXT	O,1	
44767	0	77400	2	00000	5216		+8 AXT	O,2	
44770	0	77400	3	00000	5217		+9 AXT	O,3	
44771	0	77400	5	00000	5218		+10 AXT	O,5	
44772	0	77400	6	00000	5219		+11 AXT	O,6	
44773	0	77400	7	00000	5220		+12 AXT	O,7	
44774	0	76000	0	00012	5221		+13 DCT		
44775	0	02000	0	44776	5222		+14 TRA	*+1	

44776	0	50000	0	47714	5223		+15 CLA	H86	
44777	0	60100	0	44105	5224		+16 STO	SWT	
45000	0	77400	4	00050	5225		+17 AXT	40,4	ITER PRINT FLAG
45001	-0	63400	4	43745	5226		+18 SKD	ITER5,4	NO. ITERATIONS
45002	0	77400	4	47065	5227		+19 AXT	H84,4	
45003	0	63400	4	44020	5228		+20 SXA	ITER9,4	ERROR RETURN
45004	0	07400	4	44660	5229		+21 TSX	H81,4	INPUT
45005	0	50000	0	47354	5230		+22 CLA	PR+27	T6
45006	0	56000	0	47323	5231		+23 LDQ	PR+2	P6
45007	0	07400	4	25564	5232		+24 TSX	AZH,4	
45010	0	07400	4	42602	5233		+25 TSX	ERROR,4	
45011	0	50000	0	33724	5234		+26 CLA	WPR+2	
45012	0	60100	0	47524	5235		+27 STO	Z+31	H06
45013	0	50000	0	47356	5236		+28 CLA	PR+29	T2C
45014	0	56000	0	47325	5237		+29 LDQ	PR+4	P2C
45015	0	07400	4	25564	5238		+30 TSX	AZH,4	
45016	0	07400	4	42602	5239		+31 TSX	ERROR,4	
45017	0	50000	0	33724	5240		+32 CLA	WPR+2	
45020	0	60100	0	47525	5241		+33 STO	Z+32	H02C
45021	0	56000	0	47404	5242		+34 LDQ	PR+51	WH
45022	0	26000	0	40262	5243		+35 FMP	FL3,7	
45023	0	60100	0	47453	5244		+36 STO	PR+90	
45024	0	50000	0	47372	5245		+37 CLA	PR+41	Q INITIAL GUESS
45025	0	24100	0	47370	5246		+38 FDP	PR+39	LENGTH
45026	-0	60000	0	47371	5247		+39 STQ	PR+40	NO OF DELTAS
45027	0	50000	0	47370	5248		+40 CLA	PR+39	DELTA X
45030	0	60100	0	47546	5249		+41 STO	Z+49	
45031	0	77400	7	00002	5250		+42 AXT	Z,7	
45032	0	50000	0	47323	5251	20.00	CLA	PR+2	P6
45033	0	56000	0	47354	5252		+1 LDQ	PR+27	T6= THIC
45034	-3	00000	6	45037	5253		+2 TXL	*+3,6,0	MR HOT NOT INPUT
45035	0	07400	4	47733	5254		+3 TSX	RHOMR,4	CALC. DENSITY = (P*144)/(IRH*T)
45036	0	02000	0	45045	5255		+4 TRA	*+7	
45037	0	13100	0	00000	5256		+5 XCA		
45040	0	07400	4	25564	5257		+6 TSX	AZH,4	
45041	0	07400	4	42602	5258		+7 TSX	ERROR,4	
45042	0	56000	0	33730	5259		+8 LDQ	WPR+6	
45043	0	26000	0	40245	5260		+9 FMP	FLCUP	
45044	0	60100	0	47522	5261		+10 STO	Z+29	COMPUTE WN ,K=1.4
45045	0	76000	0	00142	5262		+11 SLN	Z	K-1
45046	0	50000	0	36167	5263		+12 CLA	TK+10	K+1
45047	0	30200	0	40213	5264		+13 FSR	FL1	
45050	0	60100	0	47465	5265		+14 STO	Z	
45051	0	30000	0	40214	5266		+15 FAD	FL2	
45052	0	60100	0	47466	5267		+16 STO	Z+1	
45053	0	24100	0	47465	5268		+17 FDP	Z	
45054	-0	60000	0	47467	5269		+18 STQ	Z+2	
45055	0	50000	0	40214	5270		+19 CLA	FL2	
45056	0	24100	0	47466	5271		+20 FDP	Z+1	
45057	0	13100	0	00000	5272		+21 XCA		
45060	0	56000	0	47467	5273		+22 LDQ	Z+2	
45061	0	07400	1	47752	5274		+23 TSX	POWER,1	
45062	0	13100	0	00000	5275		+24 XCA		

45064	0	24100	0	36175	5277	+26	FDP	TK+16	
45065	0	26000	0	40272	5278	+27	FMP	FLGF	
45066	0	60100	0	47530	5279	+28	STO	Z+35	
45067	0	24100	0	47354	5280	+29	FDP	PR+27	
45070	0	13100	0	00000	5281	+30	XCA		T6
45071	0	07400	4	24364	5282	+31	TSX	SQRT,4	
45072	0	07400	4	42602	5283	+32	TSX	ERROR,4	
45073	0	13100	0	00000	5284	+33	XCA		
45074	0	26000	0	47323	5285	+34	FMP	PR+2	P6
45075	0	13100	0	00000	5286	+35	XCA		
45076	0	26000	0	47430	5287	+36	FMP	PR+71	AN
45077	0	60100	0	47407	5288	+37	STO	PR+54	WN
45100	0	30000	0	47404	5289	+38	FAD	PR+51	WH
45101	0	60100	0	47404	5290	20.01	STO	PR+53	WR
45102	0	50000	0	47404	5291	+1	CLA	PR+53	WR
45103	0	24100	0	47522	5292	+2	FDP	Z+29	
45104	0	26000	0	40244	5293	+3	FMP	FL144	
45105	0	24100	0	47422	5294	+4	FDP	PR+65	A6
45106	-0	60000	0	47450	5295	+5	STQ	PR+87	V6
45107	0	50000	0	40254	5296	20.50	CLA	FL.5	
45110	-0	52000	0	47401	5297	+1	NZT	PR+48	
45111	0	60100	0	47401	5298	+2	STO	PR+48	MACH HOT MIX
45112	0	50000	0	47354	5299	+3	CLA	PR+27	
45113	0	60100	0	47367	5300	+4	STO	PR+38	THIC=T6
45114	0	50000	0	36167	5301	+5	CLA	TK+10	
45115	0	30200	0	40213	5302	+6	FSB	FL1	
45116	0	24100	0	40214	5303	+7	FDP	FL2	
45117	-0	60000	0	47472	5304	+8	STQ	Z+5	K-1/2
45120	0	26000	0	47401	5305	+9	FMP	PR+48	
45121	0	13100	0	00000	5306	+10	XCA		
45122	0	26000	0	47401	5307	+11	FMP	PR+48	
45123	0	30000	0	40213	5308	+12	FAD	FL1	
45124	0	60100	0	47473	5309	+13	STO	Z+6	
45125	0	50000	0	47367	5310	+14	CLA	PR+38	
45126	0	24100	0	47473	5311	+15	FDP	Z+6	
45127	-0	60000	0	47364	5312	+16	STQ	PR+35	THM
45130	0	26000	0	40272	5313	20.55	FMP	FLGF	
45131	0	13100	0	00000	5314	+1	XCA		
45132	0	26000	0	36167	5315	+2	FMP	TK+10	
45133	0	13100	0	00000	5316	+3	XCA		
45134	0	26000	0	36175	5317	+4	FMP	TK+16	R HOT
45135	0	07400	4	24364	5318	+5	TSX	SQRT,4	
45136	0	07400	4	42602	5319	+6	TSX	ERROR,4	
45137	0	60100	0	47521	5320	+7	STO	Z+28	C HOT
45140	0	13100	0	00000	5321	+8	XCA		
45141	0	26000	0	47401	5322	+9	FMP	PR+48	
45142	0	60100	0	47446	5323	+10	STO	PR+85	VHM
45143	0	56000	0	47340	5324	20.56	LDQ	PR+15	DH
45144	0	26000	0	47340	5325	+1	FMP	PR+15	
45145	0	24100	0	40216	5326	+2	FDP	FL4	
45146	0	26000	0	40271	5327	+3	FMP	FLPI	
45147	0	60100	0	47424	5328	+4	STO	PR+67	AM
45150	0	52000	0	47454	5329	+5	ZET	PR+91	HEAT TRANSFER FLAG
45151	0	02000	0	45507	5330	+6	TRA	Z1.99	NON ZERO

45152	0	50000	0	47404	5331	20.58	CLA	PR+51	
45153	0	76000	0	00003	5332	+1	SSP		WH
45154	0	24100	0	47446	5333	+2	FDP	PR+85	PAKE ABSOLUTE
45155	0	26000	0	40244	5334	+3	FMP	FL144	
45156	0	24100	0	47424	5335	+4	FDP	PR+67	
45157	-0	60000	0	47523	5336	+5	STO	Z+30	AM
45160	0	56000	0	47446	5337	+6	LDQ	PR+85	VHM
45161	0	26000	0	47446	5338	20.60	FMP	PR+85	
45162	0	60100	0	47466	5339	+1	STO	Z+1	
45163	0	56000	0	47450	5340	+2	LDQ	PR+87	V6
45164	0	26000	0	47450	5341	+3	FMP	PR+87	
45165	0	30000	0	47466	5342	+4	FAD	Z+1	
45166	0	60100	0	47465	5343	+5	STO	Z	
45167	0	07400	4	24364	5344	+6	TSX	SQRT,4	
45170	0	07400	4	42602	5345	+7	TSX	ERROR,4	
45171	0	60100	0	47451	5346	+8	STO	PR+88	VIN
45172	0	50000	0	47522	5347	20.65	CLA	Z+29	
45173	0	30000	0	47523	5348	+1	FAD	Z+30	
45174	0	24100	0	40214	5349	+2	FDP	FL2	
45175	-0	60000	0	47474	5350	+3	STQ	Z+7	RHO IN
45176	0	56000	0	36171	5351	20.70	LDQ	TK+12	KIN = .5
45177	0	26000	0	47465	5352	+1	FMP	Z	VIN 2
45200	0	60100	0	47465	5353	+2	STO	Z	
45201	0	50000	0	47451	5354	+3	CLA	PR+88	VIN
45202	0	30200	0	47446	5355	+4	FSB	PR+85	VAM
45203	0	60100	0	47466	5356	+5	STO	Z+1	
45204	0	13100	0	00000	5357	+6	XCA		
45205	0	26000	0	47466	5358	+7	FMP	Z+1	
45206	0	30000	0	47465	5359	+8	FAD	Z	
45207	0	24100	0	40273	5360	+9	FDP	FL2G	
45210	0	26000	0	47474	5361	+10	FMP	Z+7	RHO IN
45211	0	24100	0	40244	5362	+11	FDP	FL144	DELTA P
45212	-0	60000	0	47335	5363	+12	STQ	PR+12	P6
45213	0	50000	0	47323	5364	20.75	CLA	PR+2	
45214	0	30200	0	47335	5365	+1	FSB	PR+12	
45215	0	60100	0	47336	5366	+2	STO	PR+13	PHM O
45216	0	50000	0	36167	5367	20.76	CLA	TK+10	K
45217	0	30200	0	40213	5368	+1	FSB	FL1	
45220	0	60100	0	47465	5369	+2	STO	Z	
45221	0	50000	0	36167	5370	+3	CLA	TK+10	
45222	0	24100	0	47465	5371	+4	FDP	Z	
45223	-0	60000	0	47513	5372	+5	STQ	Z+22	K/K-1
45224	0	50000	0	47473	5373	+6	CLA	Z+6	
45225	0	07400	1	47752	5374	+7	TSX	POWER,1	
45226	0	60100	0	47465	5375	+8	STO	Z	
45227	0	50000	0	47336	5376	+9	CLA	PR+13	PHM O
45230	0	24100	0	47465	5377	+10	FDP	Z	
45231	-0	60000	0	47333	5378	+11	STQ	PR+10	PHM
45232	0	50000	0	36167	5379	20.77	CLA	TK+10	1.4
45233	0	30000	0	40213	5380	+1	FAD	FL1	
45234	0	60100	0	47466	5381	+2	STO	Z+1	
45235	0	50000	0	40214	5382	+3	CLA	FL2	
45236	0	24100	0	47466	5383	+4	FDP	Z+1	
45237	-0	60000	0	47465	5384	+5	STQ	Z	2/K+1

45240	0	50000	0	36167	5385	+6	CLA	TK+10	
45241	0	30200	0	40213	5386	+7	FSB	FL1	
45242	0	60100	0	47467	5387	+8	STO	Z+2	
45243	0	50000	0	47466	5388	+9	CLA	Z+1	
45244	0	24100	0	47467	5389	+10	PDP	Z+2	K+1/K-1
45245	0	50000	0	47465	5390	+11	CLA	Z	
45246	0	07400	1	47752	5391	+12	TSX	POWER,1	
45247	0	24100	0	36175	5392	+13	PDP	TK+16	772.
45250	0	26000	0	40272	5393	+14	FMP	FLGF	
45251	0	13100	0	00000	5394	+15	XCA		
45252	0	26000	0	36167	5395	+16	FMP	TK+10	
45253	0	24100	0	47367	5396	+17	PDP	PR+38	
45254	0	13100	0	00000	5397	+18	XCA		
45255	0	07400	4	24364	5398	+19	TSX	SQRT,4	
45256	0	07400	4	42602	5399	+20	TSX	ERROR,4	
45257	0	13100	0	00000	5400	+21	XCA		
45260	0	26000	0	47336	5401	+22	FMP	PR+13	
45261	0	13100	0	00000	5402	+23	XCA		
45262	0	26000	0	47424	5403	+24	FMP	PR+67	
45263	0	34000	0	47404	5404	+25	CAS	PR+51	WM
45264	0	02000	0	45271	5405	+26	TRA	20.80	
45265	0	02000	0	45352	5406	+27	TRA	20.90	
45266	0	60100	0	47404	5407	+28	STO	PR+51	WMHAX = WM
45267	0	50000	0	40213	5408	+29	CLA	FL1	
45270	0	02000	0	45111	5409	+30	TRA	20.50+2	
45271	0	56000	0	47472	5410	20.80	LDQ	Z+5	
45272	0	26000	0	47404	5411	+1	FMP	PR+51	
45273	0	13100	0	00000	5412	+2	XCA		
45274	0	26000	0	47404	5413	+3	FMP	PR+51	
45275	0	60100	0	47466	5414	+4	STO	Z+1	
45276	0	50000	0	47333	5415	20.85	CLA	PR+10	PHM
45277	0	56000	0	47364	5416	+1	LDQ	PR+35	THM
45300	-3	00000	6	45303	5417	+2	TXL	*+3,6,0	MR HOT NOT INPUT
45301	0	07400	4	47733	5418	+3	TSX	RHOMR,4	CALC. DENSITY = (P*144)/(RHOT)
45302	0	02000	0	45311	5419	+4	TRA	*+7	
45303	0	13100	0	00000	5420	+5	XCA		
45304	0	07400	4	25564	5421	+6	TSX	AZH,4	
45305	0	07400	4	42602	5422	+7	TSX	ERROR,4	
45306	0	56000	0	33730	5423	+8	LDQ	WPR+6	
45307	0	26000	0	40245	5424	+9	FMP	FLCUF	
45310	0	60100	0	47465	5425	+10	STO	Z	RHO PRIME HM
45311	0	24100	0	40244	5426	+11	PDP	FL144	
45312	0	26000	0	47465	5427	+12	FMP	Z	
45313	0	24100	0	40244	5428	+13	PDP	FL144	
45314	0	26000	0	47424	5429	+14	FMP	PR+67	AM
45315	0	13100	0	00000	5430	+15	XCA		
45316	0	26000	0	47424	5431	+16	FMP	PR+67	
45317	0	13100	0	00000	5432	+17	XCA		
45320	0	26000	0	47367	5433	+18	FMP	PR+38	THM 0
45321	0	13100	0	00000	5434	+19	XCA		
45322	0	26000	0	36175	5435	+20	FMP	TK+16	
45323	0	13100	0	00000	5436	+21	XCA		
45324	0	26000	0	36167	5437	+22	FMP	TK+10	
45325	0	13100	0	00000	5438	+23	XCA		
45326	0	26000	0	40272	5439	+24	FMP	FLGF	
45327	0	30200	0	47466	5440	+25	FSB	Z+1	
45330	0	07400	4	24364	5441	+26	TSX	SQRT,4	
45331	0	07400	4	42602	5442	+27	TSX	ERROR,4	
45332	0	60100	0	47465	5443	+28	STO	Z	
45333	0	50000	0	47404	5444	+29	CLA	PR+51	WM
45334	0	76000	0	00003	5445	+30	SSP		MAKE ABSOLUTE
45335	0	24100	0	47465	5446	+31	FDP	Z	
45336	0	50000	0	47401	5447	+32	CLA	PR+48	
45337	0	07400	2	43624	5448	5448*WMH ITERATION			
45340	-0	47755	0	47573	5449	+33	TSX	ITER,2,2	
45341	0	47754	0	47574	5450	+34	NZE	IT+20,CLS2	
45342	0	40213	0	47575	5451	+35	PZE	IT+21,CLS1	
45343	3	47401	0	47307	5452	+36	PZE	IT+22,FL1	
45344	3	00000	0	47275	5453	+37	PTH	YHD,PR+48	
45345	0	47757	0	47757	5454	+38	PTH	XHD	
45346	0	02000	0	45352	5455	+39	PZE	CLS4,CLS4	
45347	0	12000	0	45351	5456	+40	TRA	20.90	
45350	0	50000	0	40256	5457	+41	TPL	*+2	
45351	0	02000	0	45111	5458	+42	CLA	FL,8	
45352	-3	00000	6	45367	5459	+43	TRA	20.50+2	
45353	0	77400	7	00001	5460	20.90	TXL	21.00,6,0	MR HOT NOT INPUT
45354	0	50000	0	47461	5461	+1	AXT	1,7	INITIALIZE FOR MR MIX
45355	0	30000	0	40213	5462	+2	CLA	PR+96	COMPUTE MR MIX MR HOT
45356	0	13100	0	00000	5463	+3	FAD	FL1	
45357	0	26000	0	47403	5464	+4	XCA		
45360	0	30000	0	47404	5465	+5	FMP	PR+50	W C
45361	0	60100	0	12512	5466	+6	FAD	PR+51	WM
45362	0	50000	0	47461	5467	+7	STO	KOM	
45363	0	24100	0	12512	5468	+8	CLA	PR+96	MR H INPUT
45364	0	26000	0	47404	5469	+9	FDP	KOM	
45365	0	60100	0	47462	5470	+10	FMP	PR+51	WM
45366	0	07400	4	47715	5471	+11	STO	PR+97	MR MIX
45367	0	56000	0	47404	5472	+12	TSX	NEWRCP,4	COMPUTE NEW R AND C SUB P FOR MIX
45370	0	26000	0	47524	5473	21.00	LDQ	PR+51	WM
45371	0	60100	0	47465	5474	+1	FMP	Z+31	
45372	0	50000	0	47403	5475	+2	STO	Z	
45373	0	30000	0	47404	5476	+3	CLA	PR+50	WC
45374	0	60100	0	47405	5477	+4	FAD	PR+51	WM
45375	0	56000	0	47403	5478	+5	STO	PR+52	WT
45376	0	26000	0	47525	5479	+6	LDQ	PR+50	WC
45377	0	30000	0	47465	5480	+7	FMP	Z+32	HO2
45400	0	24100	0	47405	5481	+8	FAD	Z	WH(HO6)
45401	0	76000	0	00012	5482	+9	FDP	PR+52	WT
45402	0	07400	4	42602	5483	+10	DCT		
45403	-0	60000	0	47526	5484	+11	TSX	ERROR,4	
45404	0	13100	0	00000	5485	+12	STQ	Z+33	
45405	-3	00000	6	45412	5486	+13	XCA		HO8
45406	0	24160	7	47752	5487	+14	TXL	*+5,6,0	
45407	0	13100	0	00000	5488	+15	FDP	NEWCP+2,7	MR HCT NOT INPUT
45410	0	30000	0	40263	5489	+16	XCA		HO8 IN AC IR7=1 C SUB P MIX
45411	0	02000	0	45415	5490	+17	FAD	FL66	TO8 IN AC
					5491	+18	TRA	*+4	
					5492	5492*CAVENAN INTERPOLATION			

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45412 0 07400 4 44513 5493 +19 TSX TIN1,4 MOB VS. T08
45413 0 00000 0 47760 5494 +20 HTR THOT,0,0
45414 0 00022 0 00001 5495 +21 HTR 1,0,18
45415 0 60100 0 47365 5496 +22 STO PR+36 T08
45416 0 60100 0 47353 5497 +23 STO PR+26 TH
5498*COMPUTE PO 8 ON EACH PASS
45417 0 50000 0 47530 5499 +24 CLA Z+35 CALCULATE PO 8
45420 -3 00000 6 45423 5500 +25 TXL *+3,6,0 MR HOT NOT INPUT
45421 0 24160 7 47750 5501 +26 FDP* NEWR+2,7 IR=2 RHOT,IR=1 R MIX IR7=1
45422 0 26060 7 47747 5502 +27 FMP* NEWR+1,7 IR=2 RHOT,IR=1 R MIX IR7=1
45423 0 07400 4 24364 5503 +28 TSX SQRT,4
45424 0 07400 4 42602 5504 +29 TSX ERROR,4
45425 0 13100 0 00000 5505 +30 XCA
45426 0 26000 0 47431 5506 +31 FMP PR+72 ATN
45427 0 60100 0 47531 5507 +32 STO Z+36 KT
45430 0 13100 0 00000 5508 +33 XCA
45431 0 26000 0 47531 5509 +34 FMP Z+36
45432 0 60100 0 47532 5510 +35 STO Z+37
45433 0 56000 0 47350 5511 +36 LDQ PR+23 KT2
45434 0 26000 0 47456 5512 +37 FMP PR+93 GATE POS
45435 0 30200 0 47457 5513 +38 FSB PR+94 A
45436 0 60100 0 47460 5514 +39 STO PR+95 B
45437 0 13100 0 00000 5515 +40 XCA KV
45440 0 26000 0 47460 5516 +41 FMP PR+95
45441 0 60100 0 47533 5517 +42 STO Z+38 KV SQUARE
45442 0 50000 0 40265 5518 +43 CLA FL128.
45443 0 24100 0 47533 5519 +44 FDP Z+38 KV2
45444 0 26060 7 47750 5520 +45 FMP* NEWR+2,7 R HOT IR=2, R MIX IR=1
45445 0 24100 0 40244 5521 +46 FDP FL144
45446 0 26000 0 47532 5522 +47 FMP Z+37
45447 0 60100 0 47534 5523 +48 STO Z+39 KT2
45450 0 30000 0 36176 5524 +49 CLA TK+17 F
45451 0 30000 0 36177 5525 +50 FAD TK+18 K11
45452 0 60100 0 47466 5526 +51 STO Z+1 K9
45453 0 56000 0 47340 5527 +52 LDQ PR+15 DTL EQU. DH
45454 0 26000 0 47340 5528 +53 FMP PR+15 DTL EQU. DH
45455 0 24100 0 40216 5529 +54 FDP FL4
45456 0 26000 0 40271 5530 +55 FMP FLPI
45457 0 60100 0 47535 5531 +56 STO Z+40 ATL
45460 0 13100 0 00000 5532 +57 XCA
45461 0 26000 0 47535 5533 +58 FMP Z+40 ATL
45462 0 60100 0 47535 5534 +59 STO Z+40 ATL SQUARE
45463 0 50060 7 47750 5535 +60 CLA* NEWR+2,7 R HOT IR=2, R MIX IR=1
45464 0 24100 0 47535 5536 +61 FDP Z+40 ATL SQUARE
45465 0 26000 0 47532 5537 +62 FMP Z+37 KT2
45466 0 24100 0 40272 5538 +63 FDP FLGF
45467 -0 60000 0 47536 5539 +64 STO Z+41 L
45470 0 26000 0 47466 5540 +65 FMP Z+1 K11+K9
45471 0 30000 0 47534 5541 +66 FAD Z+39 F
45472 0 30000 0 40213 5542 +67 FAD FL1
45473 0 07400 4 24364 5543 +68 TSX SQRT,4
45474 0 07400 4 42602 5544 +69 TSX ERROR,4
45475 0 60100 0 47537 5545 +70 STO Z+42
45476 0 50000 0 47365 5546 +71 CLA PR+36 T08

45477 0 07400 4 24364 5547 +72 TSX SQRT,4
45500 0 07400 4 42602 5548 +73 TSX ERROR,4
45501 0 24100 0 47531 5549 +74 FDP Z+36 KT
45502 0 26000 0 47405 5550 +75 FMP PR+52 WT
45503 0 13100 0 00000 5551 +76 XCA
45504 0 26000 0 47537 5552 +77 FMP Z+42
45505 0 60100 0 47322 5553 +78 STO PR+1 NEW PH
45506 0 60100 0 47334 5554 21.05 STO PR+11 POB
45507 0 60000 0 47545 5555 21.99 STZ Z+48 INITIALIZE FOR BELLOW SECTIONS
45510 0 77400 1 00000 5556 +1 AXT 0,1
45511 0 63400 1 46220 5557 +2 SXA 23.93,1
5558* HEAT TRANSFER PROGRAM 8/23/63
45512 -3 00000 6 45515 5559 22.00 TXL *+3,6,0 MR HOT NOT INPUT
45513 0 50060 7 47752 5560 +1 CLA* NEWCP+2,7 C SUB P MIX
45514 0 02000 0 45522 5561 +2 TRA *+6
45515 0 50000 0 47353 5562 +3 CLA PR+26
45516 0 56000 0 47322 5563 +4 LDQ PR+1 TH I
45517 0 07400 4 25564 5564 +5 TSX AZH,4 PH I
45520 0 07400 4 42602 5565 +6 TSX ERROR,4
45521 0 50000 0 33731 5566 +7 CLA WPR+7
45522 0 60100 0 47465 5567 +8 STO Z
45523 0 50000 0 47453 5568 +9 CLA PR+90 CSUBP HOT
45524 0 24100 0 47465 5569 +10 FDP Z QI
45525 0 13100 0 00000 5570 +11 XCA
45526 0 24100 0 47405 5571 +12 FDP PR+52
45527 0 13100 0 00000 5572 +13 XCA
45530 0 30000 0 47353 5573 +14 FAD PR+26
45531 0 60100 0 47362 5574 +15 STO PR+33 TH I
45532 0 30000 0 47353 5575 22.10 FAD PR+26 TH I+1
45533 0 24100 0 40214 5576 +1 FDP FL2
45534 -0 60000 0 47413 5577 +2 STO PR+58
45535 0 50000 0 47352 5578 22.20 CLA PR+25 TH I+1/2
45536 0 56000 0 47321 5579 +1 LDQ PR TC I
45537 0 16200 0 45541 5580 +2 TQP *+2 PC I
45540 0 02000 0 47063 5581 +3 TRA HB3
45541 0 07400 4 25564 5582 +4 TSX AZH,4
45542 0 07400 4 42602 5583 +5 TSX ERROR,4
45543 0 50000 0 33731 5584 +6 CLA WPR+7
45544 0 60100 0 47465 5585 +7 STO Z
45545 0 50000 0 47453 5586 +8 CLA PR+90 CSUBP COLD
45546 0 24100 0 47465 5587 +9 FDP Z Q I
45547 0 13100 0 00000 5588 +10 XCA
45550 0 24100 0 47403 5589 +11 FDP PR+50
45551 0 13100 0 00000 5590 +12 XCA
45552 0 30000 0 47352 5591 +13 FAD PR+25 MC
45553 0 60100 0 47361 5592 +14 STO PR+32 TCI
45554 0 30000 0 47352 5593 22.30 FAD PR+25 TCI+1
45555 0 24100 0 40214 5594 +1 FDP FL2
45556 -0 60000 0 47412 5595 +2 STO PR+57 TC I+1/2
45557 0 56000 0 47340 5596 22.40 LDQ PR+15 DH
45558 0 26000 0 40271 5597 +1 FMP FLPI
45561 0 60100 0 47465 5598 +2 STO Z F PH
45562 0 56000 0 47424 5599 +3 LDQ PR+67 AH
45563 0 26000 0 40216 5600 +4 FMP FL4
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45564 0 24100 0 47405 5601 +5 FOP Z
45565 -0 60000 0 47347 5602 +6 STQ PR+22
45566 0 50000 0 47342 5603 +7 CLA PR+33
45567 0 30200 0 47353 5604 +8 FSB PR+26
45570 0 24100 0 47413 5605 +9 FOP PR+58
45571 -0 60000 0 47444 5606 +10 STQ Z+1
45572 0 54000 0 40214 5607 +11 LDQ FL4
45573 0 26000 0 36165 5608 +12 FMP TK+8
45574 0 24100 0 47347 5609 +13 FOP PR+22
45575 0 26000 0 47371 5610 +14 FMP PR+40
45576 0 30000 0 47444 5611 +15 FAD Z+1
45577 0 60100 0 47444 5612 +16 STQ Z+1
45600 0 50000 0 47322 5613 +17 CLA PR+1
45601 0 54000 0 47353 5614 +18 LDQ PR+26
45602 -3 00000 4 45605 5615 +19 TXL +3,6,0
45603 0 07400 4 47733 5616 +20 TSX RNDNR,4
45604 0 02000 0 45613 5617 +21 TRA +7
45605 0 13100 0 00000 5618 +22 XCA
45606 0 07400 4 25564 5619 +23 TSX AZH,4
45607 0 07400 4 42602 5620 +24 TSX ERROR,4
45610 0 54000 0 33730 5621 +25 LDQ WPR+6
45611 0 26000 0 40245 5622 +26 FMP FLCUF
45612 0 60100 0 47465 5623 +27 STQ Z
45613 0 50000 0 40244 5624 +28 CLA FL144
45614 0 24100 0 47465 5625 +29 FOP Z
45615 0 26000 0 47405 5626 +30 FMP PR+52
45616 0 24100 0 47424 5627 +31 FOP PR+67
45617 0 26000 0 47405 5628 +32 FMP PR+52
45620 0 24100 0 47424 5629 +33 FOP PR+67
45621 0 26000 0 47466 5630 +34 FMP Z+1
45622 0 24100 0 40273 5631 +35 FOP FL2G
45623 0 13100 0 00000 5632 +36 XCA
45624 0 30000 0 47322 5633 +37 FAD PR+1
45625 0 60100 0 47331 5634 +38 STQ PR+8
45626 0 30000 0 47322 5635 22.50 FAD PR+1
45627 0 24100 0 40214 5636 +1 FOP FL2
45630 -0 60000 0 47476 5637 +2 STQ Z+9
45631 0 50000 0 47413 5638 22.60 CLA PR+58
45632 0 07400 4 25564 5639 +1 TSX AZH,4
45633 0 07400 4 42602 5640 +2 TSX ERROR,4
45634 0 07400 4 26223 5641 +3 TSX AZL,4
45635 0 60100 0 47374 5642 22.70 STQ PR+45
45636 0 50000 0 47371 5643 +1 CLA PR+40
45637 0 30000 0 47340 5644 +2 FAD PR+15
45640 0 60100 0 47465 5645 +3 STQ Z
45641 0 50000 0 47340 5646 +4 CLA PR+15
45642 0 24100 0 47465 5647 +5 FOP Z
45643 0 13100 0 00000 5648 +6 XCA
45644 0 54000 0 36162 5649 +7 LDQ TK+5
45645 0 07400 1 47752 5650 +8 TSX POWER,1
45646 0 24100 0 47424 5651 +9 FOP PR+67
45647 0 26000 0 36163 5652 +10 FMP TK+6
45650 0 60100 0 47465 5653 +11 STQ Z
45651 0 50000 0 40270 5654 +12 CLA 1000.

45652 -0 52000 0 47416 5655 +13 NZY PR+61
45653 0 60100 0 47416 5656 +14 STQ PR+61
45654 0 50000 0 47413 5657 +15 CLA PR+58
45655 0 24100 0 47416 5658 +16 FOP PR+61
45656 0 13100 0 00000 5659 +17 XCA
45657 0 54000 0 36161 5660 +18 LDQ TK+4
45660 0 07400 1 47752 5661 +19 TSX POWER,1
45661 0 24100 0 40214 5662 +20 FOP FL4
45662 0 26000 0 47465 5663 +21 FMP Z
45663 0 60100 0 47465 5664 +22 STQ Z
45664 0 54000 0 47340 5665 +23 LDQ PR+15
45665 0 26000 0 40271 5666 +24 FMP FLPI
45666 0 60100 0 47500 5667 +25 STQ Z+11
45667 0 54000 0 40251 5668 +26 LDQ FL.2
45670 0 07400 1 47752 5669 +27 TSX POWER,1
45671 0 60100 0 47466 5670 +28 STQ Z+1
45672 0 54000 0 47405 5671 +29 LDQ PR+52
45673 0 26000 0 40271 5672 +30 FMP FLPI
45674 0 54000 0 40256 5673 +31 LDQ FL.8
45675 0 07400 1 47752 5674 +32 TSX POWER,1
45676 0 13100 0 00000 5675 +33 XCA
45677 0 26000 0 47466 5676 +34 FMP Z+1
45700 0 13100 0 00000 5677 +35 XCA
45701 0 26000 0 47465 5678 +36 FMP Z
45702 0 13100 0 00000 5679 +37 XCA
45703 0 26000 0 47376 5680 +38 FMP PR+45
45704 0 60100 0 47374 5681 +39 STQ PR+43
45705 0 50000 0 47453 5682 22.80 CLA PR+90
45706 0 24100 0 47374 5683 +1 FOP PR+43
45707 0 13100 0 00000 5684 +2 XCA
45710 0 24100 0 47371 5685 +3 FOP PR+40
45711 0 13100 0 00000 5686 +4 XCA
45712 0 24100 0 47500 5687 +5 FOP Z+11
45713 0 13100 0 00000 5688 +6 XCA
45714 0 76000 0 00002 5689 +7 CHS
45715 0 30000 0 47413 5690 +8 FAD PR+58
45716 0 60100 0 47416 5691 +9 STQ PR+61
45717 0 12000 0 45722 5692 +10 TPL 22.90
45720 0 60000 0 47416 5693 +11 STZ PR+61
45721 0 02000 0 45754 5694 +12 TRA 22.99
45722 0 50000 0 47414 5695 22.90 CLA PR+59
45723 -0 10000 0 45730 5696 +1 TNZ 22.95
45724 0 50000 0 47415 5697 +2 CLA PR+60
45725 0 30000 0 47416 5698 +3 FAD PR+61
45726 0 24100 0 40214 5699 +4 FOP FL2
45727 0 13100 0 00000 5700 +5 XCA
5701*CAVENAH INTERPOLATION
45730 0 07400 4 44515 5702 22.95 TSX TIN1,4
45731 0 00000 0 50024 5703 +1 HTR KSUBM,0,0
45732 0 00003 0 00001 5704 +2 HTR 1,0,3
45733 0 60100 0 47377 5705 +3 STQ PR+46
45734 0 50000 0 47340 5706 +4 CLA PR+15
45735 0 30000 0 47341 5707 +5 FAD PR+16
45736 0 24100 0 47341 5708 +6 FOP PR+16
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D SLA M
TH I+1
TH I
TH I+1/2

FRICTION NOT
D SLA M

PH I
TH I
MR NOT NOT INPUT
CALC. DENSITY = (P*144)/(RH*OT)

RHO HI
WT
AM

PH I
PH I+1

PH I+1/2
TH I+1/2

LH I+1/2
DELTA X
DH

DH+DELTA X

B NOT

AH
C NOT

THW I+1/2

TH I+1/2

A NOT

DH

WT

LH I+1/2
H M I+1/2
Q I

DELTA X

FPH

TH I+1/2
THW I+1/2

THW I+1/2 IS MINUS
GO TO LOWER Q GUESS
TH I+1/2

KM
DH
THICK.

45737	0	26000	0	47377	5709	+7	FMP	PR+46	
45740	0	60100	0	47445	5710	+8	STQ	Z	
45741	0	50000	0	47453	5711	+9	CLA	PR+90	Q I
45742	0	24100	0	47445	5712	+10	FDP	Z	
45743	0	13100	0	00000	5713	+11	XCA		DELTA X
45744	0	24100	0	47371	5714	+12	FDP	PR+40	
45745	0	13100	0	00000	5715	+13	XCA		
45746	0	24100	0	40271	5716	+14	FDP	FLP1	
45747	0	13100	0	00000	5717	+15	XCA		
45750	0	76000	0	00002	5718	+16	CHS		
45751	0	30000	0	47416	5719	+17	FAD	PR+61	TMW I+1/2
45752	0	60100	0	47415	5720	+18	STQ	PR+60	TCM I+1/2
45753	0	12000	0	45760	5721	+19	TPL	23.00	
45754	0	50000	0	47453	5722	22.99	CLA	PR+90	Q
45755	0	24100	0	40214	5723	+1	FDP	FL2	
45756	-0	60000	0	47453	5724	+2	STQ	PR+90	NEW Q GUESS
45757	0	02000	0	45512	5725	+3	TRA	22.00	
45760	0	50000	0	47341	5726	23.00	CLA	PR+16	THICK.
45761	0	30000	0	47341	5727	+1	FAD	PR+16	
45762	0	30000	0	47342	5728	+2	FAD	PR+17	RAD.
45763	0	30000	0	47340	5729	+3	FAD	PR+15	DM
45764	0	60100	0	47501	5730	+4	STQ	Z+12	DM+R+2T
45765	0	13100	0	00000	5731	+5	XCA		
45766	0	26000	0	47342	5732	+6	FMP	PR+17	
45767	0	13100	0	00000	5733	+7	XCA		
45770	0	26000	0	40271	5734	+8	FMP	FLP1	
45771	0	60100	0	47423	5735	+9	STQ	PR+66	AREA COLD
45772	0	56000	0	47501	5736	23.10	LDQ	Z+12	
45773	0	26000	0	40271	5737	+1	FMP	FLP1	
45774	0	24100	0	40254	5738	+2	FDP	FL.5	
45775	-0	60000	0	47502	5739	+3	STQ	Z+13	FPC
45776	0	50000	0	47352	5740	23.20	CLA	PR+25	TCI
45777	0	56000	0	47321	5741	+1	LDQ	PR	PC I
46000	0	07400	4	25564	5742	+2	TSX	AZH,4	
46001	0	07400	4	42602	5743	+3	TSX	ERROR,4	
46002	0	56000	0	33730	5744	+4	LDQ	WPR+6	
46003	0	26000	0	40245	5745	+5	FMP	FLCUF	
46004	0	60100	0	47465	5746	+6	STQ	Z	
46005	0	50000	0	47361	5747	+7	CLA	PR+32	TC I+1
46006	0	30200	0	47352	5748	+8	FSB	PR+25	TC I
46007	0	24100	0	47412	5749	+9	FDP	PR+57	TC I+1/2
46010	-0	60000	0	47466	5750	+10	STQ	Z+1	
46011	0	50000	0	36164	5751	+11	CLA	TK+7	FRICTION COLD
46012	0	24100	0	47342	5752	+12	FDP	PR+17	R
46013	0	13100	0	00000	5753	+13	XCA		
46014	0	26000	0	40214	5754	+14	FMP	FL2	
46015	0	26000	0	47371	5755	+15	FMP	PR+40	DELTA X
46016	0	30000	0	47466	5756	+16	FAD	Z+1	
46017	0	24100	0	47465	5757	+17	FDP	Z	
46020	0	26000	0	47403	5758	+18	FMP	PR+50	WC
46021	0	24100	0	47423	5759	+19	FJP	PR+66	AC
46022	0	26000	0	47403	5760	+20	FMP	PR+50	WC
46023	0	24100	0	47423	5761	+21	FDP	PR+66	
46024	0	26700	0	40244	5762	+22	FMP	FL144	

46025	0	24100	0	40273	5763	+23	FDP	FL2G	
46026	0	13100	0	00000	5764	+24	XCA		
46027	0	76000	0	00002	5765	+25	CHS		
46030	0	30000	0	47321	5766	+26	FAD	PR	PC I
46031	0	60100	0	47330	5767	+27	STQ	PR+7	PC I+1
46032	0	12000	0	46034	5768	+28	TPL	23.30	
46033	0	02000	0	47063	5769	+29	TRA	HB8	
46034	0	30000	0	47321	5770	23.30	FAD	PR	NEGATIVE PC (I+1)
46035	0	24100	0	40214	5771	+1	FDP	FL2	
46036	-0	60000	0	47477	5772	+2	STQ	Z+10	PC I+1/2
46037	0	50000	0	47342	5773	23.40	CLA	PR+17	RAD.
46040	0	30000	0	47342	5774	+1	FAD	PR+17	
46041	0	60100	0	47346	5775	+2	STQ	PR+21	D SLA C
46042	0	30000	0	47371	5776	+3	FAD	PR+40	
46043	0	60100	0	47465	5777	+4	STQ	Z	
46044	0	50000	0	47346	5778	+5	CLA	PR+21	
46045	0	24100	0	47465	5779	+6	FDP	Z	
46046	0	13100	0	00000	5780	+7	XCA		
46047	0	56000	0	36157	5781	+8	LDQ	TK+2	B COLD
46050	0	07400	1	47752	5782	+9	TSX	POWER,1	
46051	0	24100	0	47423	5783	+10	FDP	PR+66	
46052	0	26000	0	36160	5784	+11	FMP	TK+3	C COLD
46053	0	60100	0	47465	5785	+12	STQ	Z	
46054	0	50000	0	47412	5786	23.50	CLA	PR+57	
46055	0	56000	0	47477	5787	+1	LDQ	Z+10	PC I+1/2
46056	0	07400	4	25564	5788	+2	TSX	AZH,4	
46057	0	07400	4	42602	5789	+3	TSX	ERROR,4	
46060	0	07400	4	26223	5790	+4	TSX	AZL,4	
46061	0	60100	0	47375	5791	23.65	STQ	PR+44	LC I+1/2
46062	0	50000	0	47412	5792	+1	CLA	PR+57	TC I+1/2
46063	0	24100	0	47415	5793	+2	FDP	PR+60	TWC I+1/2
46064	0	13100	0	00000	5794	+3	XCA		
46065	0	56000	0	36156	5795	+4	LDQ	TK+1	A COLD
46066	0	07400	1	47752	5796	+5	TSX	POWER,1	
46067	0	60100	0	47466	5797	+6	STQ	Z+1	
46070	0	56000	0	47403	5798	+7	LDQ	PR+50	WC
46071	0	26000	0	40271	5799	+8	FMP	FLP1	
46072	0	56000	0	40256	5800	+9	LDQ	FL.8	
46073	0	07400	1	47752	5801	+10	TSX	POWER,1	
46074	0	13100	0	00000	5802	+11	XCA		
46075	0	26000	0	47466	5803	+12	FMP	Z+1	
46076	0	60100	0	47466	5804	+13	STQ	Z+1	
46077	0	50000	0	47502	5805	+14	CLA	Z+13	FPC
46100	0	56000	0	40251	5806	+15	LDQ	FL.2	
46101	0	07400	1	47752	5807	+16	TSX	POWER,1	
46102	0	24100	0	40216	5808	+17	FDP	FL4	
46103	0	26000	0	47466	5809	+18	FMP	Z+1	
46104	0	13100	0	00000	5810	+19	XCA		
46105	0	26000	0	47375	5811	+20	FMP	PR+44	LC I+1/2
46106	0	13100	0	00000	5812	+21	XCA	Z	
46107	0	26000	0	47465	5813	+22	FMP	Z	
46110	0	60100	0	47373	5814	+23	STQ	PR+42	H CI
46111	0	50000	0	47501	5815	23.70	CLA	Z+12	

46113	0	60100	0	47903	5817	+2	STO	Z+14	DM+27
46114	0	50000	0	47953	5818	+3	CLA	PR+90	Q I
46115	0	24100	0	47503	5819	+4	FDP	Z+14	
46116	0	13100	0	00000	5820	+5	XCA		
46117	0	24100	0	47373	5821	+6	FDP	PR+42	M CI
46120	0	13100	0	00000	5822	+7	XCA		
46121	0	24100	0	40271	5823	+8	FDP	FLPI	
46122	0	13100	0	00000	5824	+9	XCA		
46123	0	24100	0	47371	5825	+10	FDP	PR+40	DELTA X
46124	0	13100	0	00000	5826	+11	XCA		
46125	0	30000	0	47412	5827	+12	FAD	PR+57	TC I+1/2
46126	0	60100	0	47415	5828	+13	STO	PR+60	TCM I+1/2
46127	0	30000	0	47416	5829	23.80	FAD	PR+61	TNM I+1/2
46130	0	24100	0	40214	5830	+1	FDP	FL2	
46131	-0	60000	0	47414	5831	+2	STO	PR+59	TM I+1/2
46132	0	13100	0	00000	5832	+3	XCA		
5833*CAVENAN INTERPOLATION									
46133	0	07400	4	44915	5834	+4	TSX	TIN1,4	
46134	0	00000	0	50024	5835	+5	MTR	KSUBN,0,0	
46135	0	00003	0	00001	5836	+6	MTR	L,0,3	
46136	0	60100	0	47377	5837	+7	STO	PR+46	KM
46137	0	50000	0	40213	5838	23.90	CLA	FL1	
46140	0	24100	0	47371	5839	+1	FDP	PR+40	DELTA X
46141	0	13100	0	00000	5840	+2	XCA		
46142	0	24100	0	40271	5841	+3	FDP	FLPI	
46143	-0	60000	0	47466	5842	+4	STQ	Z+1	
46144	0	13100	0	00000	5843	+5	XCA		
46145	0	24100	0	47503	5844	+6	FDP	Z+14	DM+27
46146	0	13100	0	00000	5845	+7	XCA		
46147	0	24100	0	47373	5846	+8	FDP	PR+42	HCI
46150	-0	60000	0	47465	5847	+9	STQ	Z	
46151	0	50000	0	47466	5848	+10	CLA	Z+1	
46152	0	24100	0	47340	5849	+11	FDP	PR+15	OH
46153	0	13100	0	00000	5850	+12	XCA		
46154	0	24100	0	47374	5851	+13	FDP	PR+43	M HI
46155	0	13100	0	00000	5852	+14	XCA		
46156	0	30000	0	47465	5853	+15	FAD	Z	
46157	0	60100	0	47465	5854	+16	STO	Z	
46160	0	50000	0	47341	5855	+17	CLA	PR+16	THICK.
46161	0	30000	0	47340	5856	+18	FAD	PR+15	OH
46162	0	60100	0	47467	5857	+19	STO	Z+2	
46163	0	50000	0	47466	5858	+20	CLA	Z+1	
46164	0	24100	0	47467	5859	+21	FDP	Z+2	
46165	0	26000	0	47341	5860	+22	FMP	PR+16	
46166	0	24100	0	47377	5861	+23	FDP	PR+46	
46167	0	13100	0	00000	5862	+24	XCA		
46170	0	30000	0	47465	5863	+25	FAD	Z	
46171	0	60100	0	47465	5864	+26	STO	Z	
46172	0	50000	0	47413	5865	+27	CLA	PR+58	TH I+1/2
46173	0	30200	0	47412	5866	+28	FSB	PR+57	TC I+1/2
46174	0	24100	0	47465	5867	+29	FDP	Z	
46175	-0	60000	0	47465	5868	+30	STQ	Z	Q CALCULATED
46176	0	50000	0	47755	5869	+31	CLA	CLS2	
46177	0	24100	0	47465	5870	+32	FDP	Z	

46200	0	13100	0	00000	5871	+33	XCA		
46201	0	60200	0	12512	5872	+34	SLW	COMMON	
46202	0	56000	0	47465	5873	+35	LQ	Z	RESTORE NQ
46203	0	50000	0	47453	5874	+36	CLA	PR+90	
5875*Q ITERATION									
46204	0	07402	2	43624	5876	+37	TSX	ITER,2,2	
46205	0	12512	0	47547	5877	+38	PZE	IT,,COMMON	
46206	0	47754	0	47550	5878	+39	PZE	IT+1,,CLS1	NEWTON, ABSOLUTE CLOSURE
46207	0	40213	0	47551	5879	+40	PZE	IT+2,,FL1	
46210	3	47453	0	47310	5880	+41	PTH	YHD+1,,PR+90	
46211	3	00000	0	47276	5881	+42	PTH	XHD+1	
46212	0	47757	0	47757	5882	+43	PZE	CLS4,,CLS4	
46213	0	02000	0	46216	5883	+44	TRA	23.92	
46214	0	60100	0	47453	5884	23.91	STO	PR+90	Q GUESS
46215	0	02000	0	45512	5885	+1	TRA	22.00	
46216	-0	52000	0	47455	5886	23.92	NZT	PR+92	K VALUE FLAG
46217	0	02000	0	46262	5887	+1	TRA	24.00	
46220	0	77400	1	00000	5888	23.93	AXT	0,1	
46221	0	50000	0	47371	5889	+1	CLA	PR+40	DELTA FLAG
46222	0	30000	0	47545	5890	+2	FAD	Z+48	SUM DELTA X
46223	0	60100	0	47545	5891	+3	STO	Z+48	SUM DELTA X
46224	0	13100	0	00000	5892	+4	XCA		
46225	0	50000	1	36204	5893	+5	CLA	BELLO,1	
46226	0	04000	0	46256	5894	+6	TLQ	23.94	
46227	0	50000	0	47361	5895	+7	CLA	PR+32	TC I+1
46230	0	56000	0	47330	5896	+8	LQ	PR+7	PC I+1
46231	0	07400	4	25564	5897	+9	TSX	AZH,4	
46232	0	07400	4	42602	5898	+10	TSX	ERROR,4	
46233	0	56000	0	33730	5899	+11	LQ	WPR+6	
46234	0	26000	0	40245	5900	+12	FMP	FLCUF	
46235	0	60100	0	47465	5901	+13	STO	Z	
46236	0	50000	0	47403	5902	+14	CLA	PR+50	MC
46237	0	24100	0	47465	5903	+15	FDP	Z	
46240	0	26000	0	47403	5904	+16	FMP	PR+50	MC
46241	0	24100	0	40273	5905	+17	FDP	FL2G	
46242	0	26000	0	40244	5906	+18	FMP	FL144	
46243	0	24100	0	47423	5907	+19	FDP	PR+66	AC I
46244	0	26000	1	36205	5908	+20	FMP	BELLO+1,1	
46245	0	24100	0	47423	5909	+21	FDP	PR+66	AC I
46246	0	13100	0	00000	5910	+22	XCA		
46247	0	76000	0	00002	5911	+23	CHS		
46250	0	30000	0	47330	5912	+24	FAD	PR+7	
46251	0	60100	0	47330	5913	+25	STO	PR+7	
46252	1	77776	1	46253	5914	+26	TXI	*+1,1,-2	NEW PC I+1 DUE TO BELLONS SECTION
46253	3	77752	1	46255	5915	+27	TXH	*+2,1,-22	
46254	0	07400	4	42602	5916	+28	TSX	ERROR,4	10 PASSES MAXIMUM
46255	0	63400	1	46220	5917	+29	SXA	23.93,1	
46256	0	50000	0	47330	5918	23.94	CLA	PR+7	PC I+1
46257	0	60100	0	47326	5919	+1	STO	PR+5	PCIC
46260	0	50000	0	47361	5920	+2	CLA	PR+32	TC
46261	0	60100	0	47357	5921	+3	STO	PR+30	TCIC
46262	0	50000	0	47546	5922	24.00	CLA	Z+49	
46263	0	30200	0	40213	5923	+1	FSB	FL1	
46264	0	10000	0	46776	5924	+2	Y76		

46265 0 60100 0 47504 5925 +3 STO Z+49
46266 0 77400 1 00002 5926 +4 AXI Z+1
46267 0 90000 1 47332 5927 +5 CLA PR+9,1
46270 0 60100 1 47323 5928 +6 STO PR+2,1
46271 0 90000 1 47363 5929 +7 CLA PR+34,1
46272 0 60100 1 47354 5930 +8 STO PR+27,1
46273 2 00001 1 46267 5931 +9 TIX 0-4,1,1
46274 0 02000 0 45512 5932 +10 TRA 22.00
46275 0 90000 0 47370 5933 25.00 CLA PR+39
46276 0 60100 0 47546 5934 +1 STO Z+49
46277 0 90000 0 32704 5935 +2 CLA P+94
46300 0 60100 0 47321 5936 +3 STO PR
46301 0 60000 0 47322 5937 +4 STZ PR+1
46302 0 90000 0 32705 5938 +5 CLA P+55
46303 0 60100 0 47352 5939 +6 STO PR+25
46304 0 60000 0 47353 5940 +7 STZ PR+26
46305 0 90000 0 47361 5941 +8 CLA PR+32
46306 0 56000 0 47330 5942 +9 LDQ PR+7
46307 0 07400 4 25544 5943 +10 TSX AZH,4
46310 0 07400 4 42602 5944 +11 TSX ERROR,4
46311 0 56000 0 33730 5945 +12 LDQ WPR+6
46312 0 26000 0 40245 5946 +13 FMP FLCUF
46313 0 60100 0 47504 5947 +14 STO Z+15
46314 0 56000 0 47343 5948 25.10 LDQ PR+18
46315 0 26000 0 47343 5949 +1 FMP PR+18
46316 0 24100 0 40216 5950 +2 FDP FL4
46317 0 26000 0 47344 5951 +3 FMP PR+19
4632 0 13100 0 00000 5952 +4 XCA
46321 0 26000 0 40271 5953 +5 FMP FLPI
46322 0 60100 0 47427 5954 +6 STO PR+70
46323 0 56000 0 47504 5955 25.20 LDQ Z+15
46324 0 50000 0 40215 5956 +1 CLA FL3
46325 0 04000 0 46412 5957 +2 TLQ 26.00
5958* INCOMPRESSIBLE EQUATIONS
46326 0 50000 0 47361 5959 25.30 CLA PR+32
46327 0 60100 0 47363 5960 +1 STO PR+34
46330 0 34000 0 40261 5961 +2 CAS FL58
46331 0 02000 0 46342 5962 +3 TRA 25.40
46332 0 02000 0 46342 5963 +4 TRA 25.40
46333 0 60100 0 33742 5964 +5 STO TP+5
46334 0 07400 4 27142 5965 +6 TSX AZV,4
46335 0 13100 0 00000 5966 +7 XCA
46336 0 50000 0 47333 5967 +8 CLA PR+10
46337 0 04000 0 46342 5968 +9 TLQ 25.40
46340 0 60000 0 47332 5969 +10 STQ PR+9
46341 0 02000 0 46344 5970 +11 TRA 25.50
46342 0 50000 0 47333 5971 25.40 CLA PR+10
46343 0 60100 0 47332 5972 +1 STO PR+9
46344 0 50000 0 47363 5973 25.50 CLA PR+34
46345 0 56000 0 47332 5974 +1 LDQ PR+9
46346 0 07400 4 25544 5975 +2 TSX AZH,4
46347 0 07400 4 42602 5976 +3 TSX ERROR,4
46350 0 56000 0 33730 5977 +4 LDQ WPR+6
46351 0 26000 0 40245 5978 +5 FMP FLCUF

DELTA X

RESTORING DELTA FOR HEAT TRANSFER
PC. THIS ASSUMES PH, TM TO BE ZERO

PH

TC

TM

TC I+1
PC I+1

DCO

NO.

ACN

COMPRESSIBLE

TC I+1
TCMPHM
PCMV LESS THAN PHM
PCN=PCMVPCN=PHM
TCM
PCM

25/09/64

PAGE 97

46352 0 60100 0 47505 5979 +6 STO Z+16
46353 0 50000 0 36173 5980 +7 CLA TK+14
46354 0 30000 0 40213 5981 +8 FAD FL1
46355 0 60100 0 47465 5982 +9 STO Z
46356 0 50000 0 47330 5983 +10 CLA PR+7
46357 0 30200 0 47332 5984 +11 FSB PR+9
46360 0 24100 0 47465 5985 +12 FDP Z
46361 0 26000 0 40272 5986 +13 FMP FLGF
46362 0 24100 0 47505 5987 +14 FDP Z+16
46363 0 26000 0 40267 5988 +15 FMP FL288
46364 0 07400 4 24364 5989 +16 TSX SQRT,4
46365 0 07400 4 42602 5990 +17 TSX ERROR,4
46366 0 60100 0 47445 5991 +18 STO PR+84
46367 0 24100 0 40244 5992 25.60 FDP FL144
46370 0 26000 0 47427 5993 +1 FMP PR+70
46371 0 13100 0 00000 5994 +2 XCA
46372 0 26000 0 40255 5995 +3 FMP FL.6
46373 0 13100 0 00000 5996 +4 XCA
46374 0 26000 0 47505 5997 +5 FMP Z+16
46375 0 13100 0 00000 5998 +6 XCA
46376 0 50000 0 47403 5999 +7 CLA PR+50
6000*WC ITERATION
46377 0 07402 2 43624 6001 +8 TSX ITER,2,2
46400 0 47755 0 47576 6002 +9 MZE IT+23,,CLS2
46401 0 47754 0 47577 6003 +10 PZE IT+24,,CLS1
46402 0 40213 0 47600 6004 +11 PZE IT+25,,FL1
46403 3 47403 0 47314 6005 +12 PTH YHD+5,,PR+50
46404 3 00000 0 47302 6006 +13 PTH XHD+5
46405 0 47757 0 47757 6007 +14 PZE CLS4,,CLS4
46406 0 02000 0 46601 6008 +15 TRA 27.00
46407 0 60100 0 47403 6009 +16 STO PR+50
46410 -3 00000 6 45367 6010 +17 TXL 21.00,6,0
46411 0 02000 0 45352 6011 +18 TRA 20.90
6012* COMPRESSIBLE EQUATIONS
46412 0 50000 0 47333 6013 26.00 CLA PR+10
46413 0 60100 0 47332 6014 +1 STO PR+9
46414 0 34000 0 47330 6015 +2 CAS PR+7
46415 0 02000 0 46420 6016 +3 TRA 26.01
46416 0 02000 0 46423 6017 +4 TRA 26.02
46417 0 02000 0 46423 6018 +5 TRA 26.02
46420 0 56000 0 47403 6019 26.01 LDQ PR+50
46421 0 26000 0 40254 6020 +1 FMP FL.5
46422 0 02000 0 46576 6021 +2 TRA H83
46423 0 50000 0 47402 6022 26.02 CLA PR+49
46424 0 30200 0 40213 6023 +1 FSB FL1
46425 -0 10000 0 46427 6024 +2 TNZ 26.10
46426 0 60000 0 47402 6025 +3 STZ PR+49
46427 0 50000 0 40254 6026 26.10 CLA FL.5
46430 -0 52000 0 47402 6027 +1 NZT PR+49
46431 0 60100 0 47402 6028 +2 STO PR+49
46432 0 56000 0 47402 6029 26.20 LDQ PR+49
46433 0 26000 0 47402 6030 +1 FMP PR+49
46434 0 60100 0 47466 6031 +2 STO Z+1
46435 0 13100 0 00000 6032 +3 XCA

KC IN = .5

PCI 0
PCM

RHO CM

VCM

ACN

VENA CAVA EFFECT

RHO CM

MR HOT INPUT

PCM = PHM
PCI 0

LOWER WC

MACH CM

46436	0	26000	0	47472	6033	+4	FMP	Z+5	
46437	0	30000	0	40213	6034	+5	FAD	FL1	
46440	0	60100	0	47506	6035	+6	STO	Z+17	
46441	0	56000	0	47513	6036	+7	LDQ	Z+22	K/K-1
46442	0	07400	1	47752	6037	+8	TSX	POWER,1	
46443	0	60100	0	47465	6038	+9	STO	Z	
46444	0	56000	0	47466	6039	+10	LDQ	Z+1	
46445	0	26000	0	36167	6040	+11	FMP	TK+10	
46446	0	24100	0	40214	6041	+12	FDP	FL2	
46447	0	26000	0	36172	6042	+13	FMP	TK+13	KC IN = .5
46450	0	30000	0	40213	6043	+14	FAD	FL1	
46451	0	13100	0	00000	6044	+15	XCA	Z	
46452	0	26000	0	47465	6045	+16	FMP	Z	
46453	0	60100	0	47465	6046	+17	STO	Z	
46454	0	50000	0	47330	6047	+18	CLA	PR+7	PC I+1
46455	0	24100	0	47465	6048	+19	FDP	Z	
46456	-0	60000	0	47465	6049	+20	STO	Z	
46457	0	50000	0	47402	6050	+21	CLA	PR+49	M CM
46460	0	30200	0	40213	6051	+22	FSB	FL1	
46461	-0	10000	0	46465	6052	+23	TNZ	+4	
46462	0	50000	0	47465	6053	+24	CLA	Z	
46463	0	60100	0	47332	6054	+25	STO	PR+9	
46464	0	02000	0	46506	6055	+26	TRA	26.30	
46465	0	56000	0	47465	6056	+27	LDQ	Z	
46466	0	50000	0	47332	6057	+28	CLA	PR+9	

6058*MCN,PCM ITERATION

46467	0	07402	2	43624	6059	+29	TSX	ITER,2,2	
46470	0	47756	0	47553	6060	+30	PZE	IT+4,,CLS3	
46471	0	47754	0	47554	6061	+31	PZE	IT+5,,CLS1	
46472	0	40213	0	47555	6062	+32	PZE	IT+6,,FL1	
46473	3	47402	0	47315	6063	+33	PTH	YHD+6,,PR+49	
46474	3	00000	0	47303	6064	+34	PTH	XHD+6	
46475	0	47757	0	47757	6065	+35	PZE	CLS4,,CLS4	
46476	0	02000	0	46506	6066	+36	TRA	26.30	
46477	0	12000	0	46502	6067	+37	TPL	+3	
46500	0	50000	0	47402	6068	+38	CLA	PR+49	
46501	0	30000	0	40250	6069	+39	FAD	FL1	
46502	0	34000	0	40213	6070	+40	CAS	FL1	
46503	0	50000	0	40213	6071	+41	CLA	FL1	
46504	0	50000	0	40213	6072	+42	CLA	FL1	
46505	0	02000	0	46431	6073	+43	TRA	26.20-1	
46506	0	50000	0	47361	6074	26.30	CLA	PR+32	TC I+1
46507	0	60100	0	47357	6075	+1	STO	PR+30	TCM 0
46510	0	24100	0	47506	6076	+2	FDP	Z+17	
46511	-0	60000	0	47363	6077	+3	STQ	PR+34	TCM
46512	0	26000	0	40272	6078	26.40	FMP	FLGF	
46513	0	13100	0	00000	6079	+1	XCA		
46514	0	26000	0	36167	6080	+2	FMP	TK+10	K = 1.4
46515	0	13100	0	00000	6081	+3	XCA		
46516	0	26000	0	36174	6082	+4	FMP	TK+15	
46517	0	07400	4	24364	6083	+5	TSX	SORT,4	R = 772.
46520	0	07400	4	42602	6084	+6	TSX	ERROR,4	
46521	0	60100	0	47507	6085	+7	STO	Z+18	CCM
46522	0	13100	0	00000	6086	26.50	XCA		

46523	0	26000	0	47402	6087	+1	FMP	PR+49	
46524	0	60100	0	47445	6088	+2	STO	PR+84	VCM
46525	0	50000	0	36167	6089	+3	CLA	TK+10	K=1.4 COMPUTE ACN (PRIME)
46526	0	30200	0	40213	6090	+4	FSB	FL1	
46527	0	60100	0	47465	6091	+5	STO	Z	
46530	0	50000	0	40213	6092	+6	CLA	FL1	
46531	0	24100	0	47465	6093	+7	FDP	Z	
46532	0	50000	0	47506	6094	+8	CLA	Z+17	
46533	0	07400	1	47752	6095	+9	TSX	POWER,1	
46534	0	60100	0	47465	6096	+10	STO	Z	
46535	0	50000	0	40214	6097	+11	CLA	FL2	
46536	0	24100	0	47465	6098	+12	FDP	Z	
46537	0	13100	0	00000	6099	+13	XCA		
46540	0	30000	0	40271	6100	+14	FAD	FLP1	
46541	0	60100	0	47465	6101	+15	STO	Z	
46542	0	50000	0	40271	6102	+16	CLA	FLP1	
46543	0	24100	0	47465	6103	+17	FDP	Z	
46544	-0	60000	0	47465	6104	+18	STQ	Z	
46545	0	26000	0	47465	6105	+19	FMP	Z	
46546	0	13100	0	00000	6106	+20	XCA		
46547	0	26000	0	47427	6107	+21	FMP	PR+70	ACN
46550	0	60100	0	47527	6108	+22	STO	Z+34	ACN PRIME
46551	0	50000	0	47363	6109	26.60	CLA	PR+34	TCM
46552	0	56000	0	47332	6110	+1	LDQ	PR+9	PCN
46553	0	07400	4	25564	6111	+2	TSX	AZH,4	
46554	0	07400	4	42602	6112	+3	TSX	ERROR,4	
46555	0	56000	0	33730	6113	+4	LDQ	MPR+6	
46556	0	26000	0	40245	6114	+5	FMP	FLCUF	
46557	0	60100	0	47505	6115	+6	STO	Z+16	
46560	0	13100	0	00000	6116	+7	XCA		
46561	0	26000	0	47445	6117	+8	FMP	PR+84	VCM
46562	0	13100	0	00000	6118	+9	XCA		
46563	0	26000	0	47527	6119	+10	FMP	Z+34	ACN PRIME
46564	0	24100	0	40244	6120	+11	FDP	FL144	
46565	0	50000	0	47403	6121	+12	CLA	PR+50	
46566	0	07402	2	43624	6122	+13	TSX	ITER,2,2	
46567	-0	47755	0	47556	6123	+14	NZE	IT+7,,CLS2	
46570	0	47754	0	47557	6124	+15	PZE	IT+8,,CLS1	
46571	0	40213	0	47560	6125	+16	PZE	IT+9,,FL1	
46572	3	47403	0	47314	6126	+17	PTH	YHD+5,,PR+50	
46573	3	00000	0	47302	6127	+18	PTH	XHD+5	
46574	0	47757	0	47757	6128	+19	PZE	CLS4,,CLS4	
46575	0	02000	0	46601	6129	+20	TRA	27.00	
46576	0	60100	0	47403	6130	H83	STO	PR+50	
46577	-3	00000	6	45367	6131	+1	TXL	21.00,6,0	MR HOT INPUT
46600	0	02000	0	45352	6132	+2	TRA	20.90	CALCULATE NEW MR MIX
46601	0	50000	0	47400	6133	27.00	CLA	PR+47	MH8
46602	0	10000	0	46606	6134	+1	TZE	27.01	
46603	0	30200	0	40213	6135	+2	FSB	FL1	
46604	-0	10000	0	46606	6136	+3	TNZ	27.01	
46605	0	60000	0	47400	6137	+4	STZ	PR+47	
46606	0	50000	0	40254	6138	27.01	CLA	FL.5	
46607	-0	52000	0	47400	6139	+1	NZT	PR+47	MH8
46610	0	60100	0	47400	6140	+2	STO	PR+47	

44611	0	34000	0	47400	6141	27.10	LDQ	PR+47	
44612	0	26000	0	47400	6142	+1	FMP	PR+47	
44613	0	13100	0	00000	6143	+2	XCA		
44614	0	26000	0	47472	6144	+3	FMP	Z+5	K-1/2
44615	0	30000	0	40213	6145	+4	FAD	FL1	
44616	0	60100	0	47510	6146	+5	STO	Z+19	
44617	0	30000	0	36167	6147	+6	CLA	TK+10	
44620	0	30000	0	40213	6148	+7	FAD	FL1	
44621	0	24100	0	47472	6149	+8	FDP	Z+5	
44622	0	26000	0	40253	6150	+9	FMP	FL.25	
44623	0	13100	0	00000	6151	+10	XCA		
44624	0	30000	0	47510	6152	+11	CLA	Z+19	
44625	0	07400	1	47752	6153	+12	TSX	POWER,1	
44626	0	60100	0	47465	6154	+13	STO	Z	
44627	0	30000	0	36167	6155	27.20	CLA	TK+10	
44630	0	24100	0	47365	6156	+1	FDP	PR+36	TS 0
44631	0	26000	0	40272	6157	+2	FMP	FLGF	
44632	0	24160	7	47750	6158	+3	FDP*	NEWR+2,7	R HOT IR=2, R MIX IR=1
44633	0	13100	0	00000	6159	+4	XCA		
44634	0	07400	4	24364	6160	+5	TSX	SQRT,4	
44635	0	07400	4	42602	6161	+6	TSX	ERROR,4	
44636	0	13100	0	00000	6162	+7	XCA		
44637	0	26000	0	47400	6163	+8	FMP	PR+47	MHB
44640	0	24100	0	47465	6164	+9	FDP	Z	
44641	0	26000	0	47424	6165	+10	FMP	PR+67	AM
44642	0	13100	0	00000	6166	+11	XCA		
44643	0	26000	0	47334	6167	+12	FMP	PR+11	PS 0
44644	0	60100	0	47465	6168	+13	STO	Z	
44645	0	30000	0	47400	6169	+14	CLA	PR+47	
44646	0	30200	0	40213	6170	+15	FSB	FL1	
44647	0	10000	0	46671	6171	+16	TZE	27.30	MHB=1
44650	0	36000	0	47465	6172	+17	LDQ	Z	
44651	0	30000	0	47405	6173	+18	CLA	PR+52	WT
44652	0	07402	2	43624	6174	+19	TSX	ITER,2,2	
44653	0	47756	0	47561	6175	+20	PZE	IT+10,,CLS3	
44654	0	47754	0	47562	6176	+21	PZE	IT+11,,CLS1	
44655	0	40213	0	47563	6177	+22	PZE	IT+12,,FL1	
44656	3	47400	0	47316	6178	+23	PTH	YHD+7,,PR+47	
44657	3	00000	0	47304	6179	+24	PTH	XHD+7	
44660	0	47757	0	47757	6180	+25	PZE	CLS4,,CLS4	
44661	0	02000	0	46671	6181	+26	TRA	27.30	
44662	0	12000	0	46665	6182	+27	TPL	+03	
44663	0	36000	0	47400	6183	+28	LDQ	PR+47	
44664	0	26000	0	40250	6184	+29	FMP	FL.1	
44665	0	34000	0	40213	6185	+30	CAS	FL1	
44666	0	30000	0	40213	6186	+31	CLA	FL1	
44667	0	30000	0	40213	6187	+32	CLA	FL1	
44670	0	02000	0	46610	6188	+33	TRA	27.10-1	
44671	0	30000	0	47365	6189	27.30	CLA	PR+36	TS 0
44672	0	24100	0	47510	6190	+1	FDP	Z+19	
44673	-0	60000	0	47355	6191	+2	STQ	PR+28	TS
44674	0	26000	0	40272	6192	27.40	FMP	FLGF	
44675	0	13100	0	00000	6193	+1	XCA		
44676	0	27.30	0	47367	6194		FMP	TS	
44677	0	13100	0	00000	6195	+3	XCA		
446700	0	26060	7	47750	6196	+4	FMP*	NEWR+2,7	R HOT IR=2, R MIX IR=1
446701	0	07400	4	24364	6197	+5	TSX	SQRT,4	
446702	0	07400	4	42602	6198	+6	TSX	ERROR,4	
446703	0	60100	0	47511	6199	+7	STO	Z+20	CH 8
446704	0	13100	0	00000	6200	27.50	XCA		
446705	0	26000	0	47400	6201	+1	FMP	PR+47	MHB
446706	0	60100	0	47447	6202	+2	STO	PR+86	VB
446707	-0	50000	7	47750	6203	28.00	CAL	NEWR+2,7	
446710	0	62100	0	46712	6204	+1	STA	+02	
446711	0	07400	4	27034	6205	+2	TSX	AZ0,4	
446712	0	00000	0	00000	6206	+3	PZE	+00	COMPUTE PS
446713	0	50000	0	47510	6207	28.20	CLA	Z+19	
446714	0	56000	0	47513	6208	+1	LDQ	Z+22	K/K-1
446715	0	07400	1	47752	6209	+2	TSX	POWER,1	
446716	0	13100	0	00000	6210	+3	XCA		
446717	0	26000	0	47324	6211	+4	FMP	PR+3	PS
446720	0	60100	0	47514	6212	+5	STO	Z+23	PS 0 PRIME
446721	0	30000	0	47400	6213	28.30	CLA	PR+47	MACH H8
446722	0	30200	0	40213	6214	+1	FSB	FL1	
446723	-0	10000	0	46771	6215	+2	TNZ	28.50	
446724	0	50000	0	36167	6216	28.40	CLA	TK+10	
446725	0	30200	0	40213	6217	+1	FSB	FL1	
446726	0	60100	0	47465	6218	+2	STO	Z	K-1
446727	0	30000	0	40214	6219	+3	FAD	FL2	
446730	0	60100	0	47466	6220	+4	STO	Z+1	K+1
446731	0	24100	0	47465	6221	+5	FDP	Z	
446732	-0	60000	0	47465	6222	+6	STO	Z	K+1/K-1
446733	0	50000	0	40214	6223	+7	CLA	FL2	
446734	0	24100	0	47466	6224	+8	FDP	Z+1	K+1
446735	0	13100	0	00000	6225	+9	XCA		K+1/K-1
446736	0	56000	0	47465	6226	+10	LDQ	Z	
446737	0	07400	1	47752	6227	+11	TSX	POWER,1	
446740	0	13100	0	00000	6228	+12	XCA		
446741	0	26000	0	36167	6229	+13	FMP	TK+10	K
446742	0	24160	7	47750	6230	+14	FDP*	NEWR+2,7	R HOT IR=2, R MIX IR=1
446743	0	26000	0	40272	6231	+15	FMP	FLGF	
446744	0	24100	0	47365	6232	+16	FDP	PR+36	TS 0
446745	0	13100	0	00000	6233	+17	XCA		
446746	0	07400	4	24364	6234	+18	TSX	SQRT,4	
446747	0	07400	4	42602	6235	+19	TSX	ERROR,4	
446750	0	13100	0	00000	6236	+20	XCA		
446751	0	26000	0	47334	6237	+21	FMP	PR+11	PS 0
446752	0	13100	0	00000	6238	+22	XCA		AM
446753	0	26000	0	47424	6239	+23	FMP	PR+67	
446754	0	13100	0	00000	6240	+24	XCA		WT
446755	0	50000	0	47405	6241	+25	CLA	PR+52	
446756	0	07402	2	43624	6242	+26	TSX	ITER,2,2	
446757	-0	47755	0	47564	6243	+27	NZE	IT+13,,CLS2	
446760	0	47754	0	47565	6244	+28	PZE	IT+14,,CLS1	
446761	0	40213	0	47566	6245	+29	PZE	IT+15,,FL1	
446762	3	47405	0	47317	6246	+30	PTH	YHD+8,,PR+52	
446763	3	00000	0	47305	6247	+31	PTH	XHD+8	
446764	0	47757	0	47757	6248	+32	PZE	CLS4,,CLS4	

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46765 0 02000 0 47017 6249 +33 TRA HBI
46766 0 30200 0 47403 6250 +34 FSB PR=50
46767 0 60100 0 47404 6251 +35 STO PR=51
46770 0 02000 0 47014 6252 +36 TRA HBI+1
46771 0 50000 0 47334 6253 28.50 CLA PR=11
46772 0 56000 0 47514 6254 +1 LDQ Z+23
46773 0 07402 2 43624 6255 +2 TSB ITER,2,2
46774 0 47755 0 47567 6256 +3 PZE IT+10,,CL52
46775 0 47754 0 47570 6257 +4 PZE IT+17,,CL51
46776 0 40213 0 47571 6258 +5 PZE IT+10,,FL1
46777 3 47404 0 47320 6259 +6 PTH VMD+9,,PR+51
47000 3 00000 0 47306 6260 +7 PTH XMD+9
47001 0 47757 0 47757 6261 +8 PZE CL54,,CL54
47002 0 02000 0 47017 6262 +9 TRA HBI
47003 0 12000 0 47013 6263 28.60 TPL HBI
47004 0 77400 1 00003 6264 +1 AXT 3,1 INITIALIZE FOR NEW GUESS
47005 0 60000 1 47572 6265 +2 STZ IT+19,1
47006 2 00001 1 47005 6266 +3 TIX 0-1,1,1
47007 -0 76000 0 00142 6267 +4 SLT 2
47010 0 02000 0 47041 6268 +5 TRA HBI
47011 0 56000 0 47404 6269 +6 LDQ PR=51 WDOOTH NEG 2ND TIME
47012 0 26000 0 40254 6270 +7 FMP FL.8 LOWER WDOOTH GUESS
47013 0 60100 0 47404 6271 HBI+2 STO PR=51
47014 0 30000 0 47407 6272 +1 FAD PR=54 WN
47015 0 77400 7 00002 6273 +2 AXT 2,7
47016 0 02000 0 45101 6274 +3 TRA 20.01 NEW NR
47017 0 50000 0 47365 6275 HBI+1 CLA PR=36 TOB
47020 0 60100 0 47353 6276 +1 STO PR=26 TH
47021 0 52000 0 44105 6277 +2 ZET SWT
47022 0 07400 4 47024 6278 +3 TSB HBI+4 PRINT
47023 0 02000 0 47044 6279 +4 TRA HBI+5

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47024 0 63400 4 47041 6281 HBI+1 SKA HBI+4
47025 0 63400 1 47042 6282 +1 SKA HBI+1,1
47026 0 50000 0 47334 6283 +2 CLA PR=11
47027 0 10000 0 47031 6284 +3 TZE 0+2
47030 0 60100 0 47322 6285 +4 STO PR=1
47031 0 77400 1 00031 6286 +5 AXT 25,1
47032 0 07400 4 00052 6287 PRINI+1 TSB DOOTH,4
47033 3 02001 1 47136 6288 +1 PTH MD1+25,1,1025
47034 0 05722 0 00056 6289 +2 PZE 30,,3026
47035 -3 11655 1 47352 6290 +3 SVN PR+25,1,5037
47036 0 05722 0 00031 6291 +4 PZE 25,,3026
47037 1 00000 0 44106 6292 +5 PDN MODE
47040 2 00001 1 47032 6293 +6 TIX PRINI,1,1
47041 0 77400 4 00000 6294 HBI+1 AXT 00,4
47042 0 77400 1 00000 6295 +1 AXT 00,1
47043 0 02000 4 00001 6296 +2 TRA 1,4
47044 0 76000 0 00140 6297 +3 SLF
47045 0 77400 1 00144 6298 +4 AXT 100,1
47046 0 60000 1 47713 6299 +5 STZ IT+100,1
47047 2 00001 1 47046 6300 +6 TIX 0-1,1,1
47050 0 07400 4 44713 6301 +7 TSB HBI+4
47051 0 77400 4 00000 6302 HBI+1 AXT 00,4

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47052 0 77400 2 00000 6303 +1 AXT 00,2
47053 0 77400 3 00000 6304 +2 AXT 00,3
47054 0 77400 1 00000 6305 +3 AXT 00,1
47055 0 77400 5 00000 6306 +4 AXT 00,5
47056 0 77400 6 00000 6307 +5 AXT 00,6
47057 0 77400 7 00000 6308 +6 AXT 00,7
47060 0 02000 4 00003 6309 +7 TRA 3,4
47061 0 52200 0 47051 6310 HBI+1 XEC HBI
47062 1 00002 4 47052 6311 +1 TIX HBI+1,4,2 ERROR
47063 0 52200 0 47051 6312 HBI+1 XEC HBI RETURN FOR WDOOTH NEG
47064 1 00001 4 47052 6313 +1 TIX HBI+1,4,1 ERROR RETN FOR PC NEGATIVE
47065 0 60200 0 47070 6315 HBI+1 SLW HBI+5 NAME OF LOOP IN AC
47066 -1 47070 0 25421 6316 +1 STR AIF,,HBI5
47067 0 02000 2 00007 6317 +2 TRA 7,2 NORMAL ITER RETURN
47070 -2 06060 6 06060 6318 HBI+1 BCI 3, NOT CLOSED
47073 -0 52551 6 54644 6319 HBI+1 BCI 1, NERVOUS BALANCE
47105 -0 72560 6 06060 6320 HBI+1 BCI 1, PC PH P6 P8 P2C PC1C P11 PC I+1PH I+1PCM
47117 -0 73044 6 06060 6321 +10 BCI 1, PHM PO 8 DELTAPPHIC DM T R DCO NO.
47131 -2 33025 6 32160 6322 +20 BCI 1, THETA DSLA CDSL A HG POS T2C TC1C TC I+1TH I+1TCM
47143 -2 32360 6 06060 6323 +30 BCI 1, TC TH T6 T8 T2C TC1C TC I+1TH I+1TCM
47155 -2 33044 6 06060 6324 +40 BCI 1, THM TO 8 TH1C DELTASDELTALENGTHHMC+0F HMC+0F LCI
47167 -0 33031 6 06060 6325 +50 BCI 1, LHM KM M HBI M HM M CM
47201 -2 62360 6 06060 6326 HBI+1 BCI 1, MC WM WT WR WN TCI THI TMI
47213 -2 32366 3 16060 6327 +10 BCI 1, TCHI THWI A6 ACI AM WPCI WPHI
47225 2 12345 6 06060 6328 +20 BCI 1, ACN AN ATN A-COLOB-COLD
47237 2 34023 4 64324 6329 HBI+1 BCI 1, C-COLDA -HOTB -HOTC -HOTFRIC-HKIN KCIN-CKCIN-IVCM
47251 -2 53044 6 06060 6330 +10 BCI 1, VHM V8 V6 VIN2 OSUBI HT FLGK FLAGA B
47263 -0 26560 6 06060 6331 +20 BCI 1, KV MR MOTMR MIXMR FLG
47275 -0 43044 6 06060 6332 XHD BCI 1, HMM Q THW TCW THI MC MCM NHB WT WH
47307 -0 43044 6 06060 6333 YMD BCI 1, HMM Q THW TCW THI MC PCN WT WH P8 O
47321 6334 PR BSS 100,F
47345 6335 Z BSS 50,F
47347 6336 IT BSS 100,F
47371 6337 Y BSS 1,0
47374 6338 HBI+1 BSS 1,X
47390 6339 SUBROUTINES TO CALCULATE NEW R HOT,R MIX NEW HOB,NEW CSUB PIH,MIX)
47715 0 50000 7 47463 6340 NEWRCPLA PR+98,7 MR HOT IR=2, MR MIX IR=1
47716 0 30000 0 40213 6341 +1 FAD FL1
47717 0 60100 0 12512 6342 +2 STO KOM
47720 0 56000 0 40260 6343 +3 LDQ FL48,2
47721 0 26000 7 47463 6344 +4 FMP PR+98,7 MR HOT IR=2, MR MIX IR=1
47722 0 30000 0 40242 6345 +5 FAC FL776
47723 0 24100 0 12512 6346 +6 FDI KOM
47724 -0 60060 7 47750 6347 +7 STG+ NEWR+2,7
47725 0 56000 0 40252 6348 +8 LDQ FL.219 NEW RMOT AND R MIX
47726 0 26000 7 47463 6349 +9 FMP PR+98,7 MR HOT IR=2, MR MIX IR=1
47727 0 30000 0 40257 6350 +10 FAD FL3.45
47730 0 24100 0 12512 6351 +11 FDP KOM
47731 -0 60060 7 47752 6352 +12 STO+ NEWCP+2,7
47732 0 02000 4 00001 6353 +13 TRA 1,4
47733 0 60100 0 12512 6354 RHOMR STO KOM
47734 -0 60000 0 12513 6355 +1 STO KOM+1
47735 0 24160 7 47750 6356 +2 FDP+ NEWR+2,7

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47736	0	26000	0	40244	6357	+3	FMP	FL144		
47737	0	24100	0	12513	6358	+4	FDP	KOM+1		
47740	0	13100	0	00000	6359	+5	XCA			T
47741	0	02000	4	00001	6360	+6	TRA	1,4		
47742	0	30200	0	40263	6361		NEWM	FSB	FL66	TEMP. IN AC
47743	0	13100	0	00000	6362	+1	XCA			
47744	0	26060	7	47752	6363	+2	FMP*	NEWCP+2,7		C SUB P MIX
47745	0	02000	4	00001	6364	+3	TRA	1,4		
47746	0	00000	0	36175	6365		NEWM	HTR	TK+16	R HOT
47747	0	00000	0	47540	6366	+1	HTR		Z+43	R MIX
47750	0	00000	0	47541	6367		NEWCP	HTR	Z+44	CP HOT
47751	0	00000	0	47542	6368	+1	HTR		Z+45	CP MIX
				12512	6369		KOM	EQU	COMMON	
					6370*		POWER SUBROUTINE			
47752	0	07400	4	27021	6371		POWER	TSX	AZE,4	
47753	0	02000	1	00001	6372	+1	TRA		1,1	
47754	1	72507	5	34122	6373		CLS1	DEC	.01	
47755	1	67406	1	11565	6374		CLS2	DEC	.001	
47756	1	63643	3	34273	6375		CLS3	DEC	.0001	
47757	1	60517	4	26542	6376		CLS4	DEC	.00001	
					6377*		CAVEMAN ENTHALPY VS.	TEMP TABLE FOR HOT TEMPS		
47760	2	13651	0	00000	6378		THOT	DEC	1700.,510.,2000.,595.,2300.,680.,2700.,795.,3200.,940.	
47772	2	14764	0	00000	6379	+10	DEC		4000.,1155.,5500.,1600.,7500.,2150.,9000.,2550.,11000.	
50003	2	14575	2	00000	6380	+19	DEC		3050.,13000.,3555.,15000.,4050.,17000.,4500.,19100.,5000.	
50014	2	17470	4	00000	6381	+28	DEC		20000.,5200.,21000.,5400.,22000.,5600.,24000.,6000.	
					6382*		CAVEMAN TEMP VS.	SOME SORT OF THERMAL CONDUCTIVITY		
50024	0	00000	0	00000	6383		KSUBM	DEC	0.,0.,200.,115E-6,2000.,355E-6	
					50032		6385	AZXI	BSS	12*CARDS,H
51162	0	00000	0	00000	6386		AZMT	PZE		STORAGE FOR STANDARD CASE, BCD
				15061	6387		AZMTG	EQU	AZMT-AZMTB	TEMP STORAGE FOR EACH PHASE PART
				37357	6388		AZMTP	EQU	AZD+100*NCMP-1	GAP BETWEEN PART AND CURRENT STORAGE
				01775	6389		AZMTS	EQU	AZMTE-AZMTB	END OF PART CURVES
				00062	6390		CARDS	EQU	50	SIZE OF STORAGE FOR EACH PART
				00012	6391		NCURV	EQU	10	MAX NO. CARDS IN STD CASE
				00006	6392		NCMP	EQU	6	TOTAL NO. CURVES
				00024	6393		NHIT	EQU	20	NO. CURVES FOR ONE PART
				00067	6394		NLMAX	EQU	55	MAX NO. HEAT TRANSFER ITERATIONS
				00062	6395		NZMAX	EQU	50	MAX NO LINES/PAGE
				24416	6396			END	BEGIN	MAX NO. NODES/PART

SBCENT	*0065	*KPRINT	0001	22.70	*0090	2PI	*0058	AYE1	0036
S8YVAS	0065	*KPUNCH	*0001	22.80	*0091	58BCD	0065	AYE2	0036
ALPHAC	0074	KRBUFF	*0001	22.90	0091	58EOF	0065	AYEA	0037
AS50C1	0065	*KRTAPE	*0001	22.95	0091	58IR1	0065	AYEA1	0037
AS50C2	0065	KSERCH	*0001	22.99	0092	58IR2	0065	AYER	0036
AS50C3	0065	KSHORT	*0001	23.00	0092	58IR4	0065	AYG	0037
AS58D1	0065	KSQZRD	*0001	23.10	*0092	58MIL	0065	AYGA	0038
AS58F1	0065	KSTART	*0001	23.20	*0092	58ONE	0065	AYGR	0038
AS58F2	0065	KSTIME	*0001	23.30	0093	58TEN	*0065	AYH	0039
AS58Y1	0065	KSTUFF	*0001	23.40	*0093	ACI	0079	AYH1	0040
*COMMON	0001	KTAKB	0001	23.50	*0093	ANA	0077	AYH2	0040
DELTAZ	0079	KTIMEX	*0001	23.65	*0093	AS58	0064	AYHR	0040
DSUBHI	0078	KTUNIT	*0001	23.70	*0093	AS58A	0065	AYI	0040
FL128.	0058	KUNFLO	*0001	23.80	*0094	AS58B	0065	AYI1	0040
FL12E8	0058	KMBUFF	*0001	23.90	*0094	AS58C	0065	AYI2	0040
FL3.45	0058	KWITAP	*0001	23.91	*0095	AS58D	0065	AYI3	*0040
FL48.2	0058	*KWITAP	*0001	23.92	0095	AS58E	0065	AYI12	0041
FL.219	0058	NEWRCP	0103	23.93	7095	AS58F	0065	AYI1R	0040
GAMMAC	0074	ST1763	0064	23.94	0095	AS58G	0065	AYIR	0040
ITER7A	0077	ST59.4	0064	24.00	0095	AS58H	0065	AYJ	0041
ITERPX	0077	ST59.7	0064	25.00	0096	AS58J	0065	AYJ1	0041
KBINLD	0001	TSUBCI	0079	25.10	*0096	AS58K	0065	AYK	0041
KCLOCK	*0001	TSUBHI	0079	25.20	*0096	AS58P	0065	AYK01	0045
KDATEA	0001	1000.	0058	25.30	*0096	AS58Q	0065	AYK02	0045
KDATEN	*0001	188	0058	25.40	0096	AS58V	0065	AYK1	0044
KDEBUG	0001	20.00	*0083	25.50	0096	AS58W	0065	AYK2	*0044
*KDELAY	*0001	20.01	0084	25.60	*0097	AS58X	0065	AYK3	0044
KENTRY	*0001	20.50	0084	26.00	0097	AS58Y	0065	AYK4	0042
*KERROR	0001	20.55	*0084	26.01	0097	AS58Z	0065	AYK5	0042
*KFINIS	0001	20.56	*0084	26.02	0097	AYA	0029	AYK6	0042
KINDX1	*0001	20.58	*0085	26.10	0097	AYAL	0031	AYK7	0042
KINDX2	*0001	20.60	*0085	26.20	0097	AYAR	0031	AYK8	0042
*KINDX4	0001	20.65	*0085	26.30	0098	AYB	0031	AYK9	0045
KISBSF	*0001	20.70	*0085	26.40	*0098	AYB1	0031	AYKR	0042
*KISBSR	*0001	20.75	*0085	26.50	*0098	AYB2	0032	AYL	0045
KISETT	*0001	20.76	*0085	26.60	*0099	AYB3	0032	AYL2	0045
*KISORG	*0001	20.77	*0085	27.00	0099	AYB4	0032	AYLA	0046
*KISOUT	0001	20.80	0086	27.01	0099	AYBR	0032	AYLO	0046
KISREW	*0001	20.85	*0086	27.10	0100	AYBT	0032	AYLP	0046
KISRTT	*0001	20.90	0087	27.20	*0100	AYBW	0032	AYLR	0045
KISTAT	*0001	21.00	0087	27.30	0100	AYC	0032	AYLW	0046
KISNEF	*0001	21.05	*0089	27.40	*0100	AYCA	0035	AYM	0046
*KJOBND	*0001	21.99	0089	27.50	*0101	AYCA1	0035	AYN	0046
KLCSTR	0001	22.00	0C89	28.00	*0101	AYCR	0035	AYN1	0046
KLCCAT	*0001	22.10	*0C89	28.20	*0101	AYD	0035	AYPA	0047
KLRQUT	*0001	22.20	*0089	28.30	*0101	AYD01	0036	AYPA1	0047
*KMCVEB	0001	22.30	*0089	28.40	*0101	AYD1	0036	AYPAR	0047
KONLIN	0001	22.40	*0089	28.50	0102	AYD2	0036	AYPB	0047
*KOPINP	*0001	22.50	*0090	28.60	*0102	AYDR	0036	AYPB1	0048
*KCVFLO	0001	22.60	*0090	288	0058	AYE	0036	AYPB2	0048

AYPB3 0048	AZC 0011	AZK 0017	AZN11 0019	AZQ 0025
AYPBR 0048	AZC1 0011	AZK1 0018	AZN1R 0019	AZQR 0025
AYQ 0048	AZC2 0011	AZK2 0018	AZNR 0074	AZT 0005
AYQ1 0048	AZCR 0011	AZK3 0018	AZNV 0019	AZT1 0006
AYQR 0048	AZD 0057	AZK4 0018	AZNM1 0019	AZT2 0006
AYR 0048	AZE 0025	AZKR 0018	AZNM2 0019	AZT3 0007
AYR1 0049	AZE1 0025	AZL 0018	AZNR 0019	AZT4 0007
AYR2 0049	AZER 0025	AZLR 0018	AZP3 0021	AZTR 0006
AYR3 0049	AZF 0011	AZM01 0005	AZPC 0019	AZU 0026
AYRR 0049	AZF1 0012	AZM1 *0003	AZPC1 0020	AZU1 0026
AYT 0049	AZF2 0012	AZM10 0004	AZPC2 0020	AZU2 0026
AYT1 0049	AZF3 0011	AZM11 0005	AZPC3 0020	AZU3 0026
AZ01 0055	AZFF 0011	AZM12 0004	AZPCR 0020	AZU4 0026
AZ02 0055	AZFR 0012	AZM17 0003	AZPD 0020	AZU5 0026
AZ03 0055	AZFT 0012	AZM19 0004	AZPD1 0020	AZU6 0026
AZ04 0055	AZFT1 0012	AZM2 *0004	AZPD2 0021	AZUR 0026
AZ05 0055	AZG 0012	AZM20 0005	AZPD3 0021	AZV 0026
AZ06 0055	AZG1 0013	AZM21 0005	AZPD4 0021	AZV1 0026
AZ07 0055	AZGR 0013	AZM22 0005	AZPD5 0021	AZV2 0026
AZ08 0055	AZH 0013	AZM23 0005	AZPD6 0021	AZVR 0026
AZ09 0055	AZH1 0014	AZM24 0002	AZPD7 0021	AZX 0027
AZA 0007	AZH2 0013	AZM25 0002	AZPD8 0021	AZX1 0027
AZA1 0007	AZH3 0013	AZM26 0002	AZPD9 0021	AZX2 0027
AZAA 0007	AZH4 0014	AZM27 0003	AZPDR 0020	AZX3 0027
AZAA1 0008	AZHR 0014	AZM28 0003	AZP1 0021	AZX4 0027
AZAAAR 0008	AZI 0014	AZM29 *0004	AZP11 0022	AZX5 0027
AZAB 0008	AZI01 0015	AZM3 0005	AZP12 0021	AZX6 0027
AZAB1 0008	AZI1 0015	AZM30 0005	AZP13 0021	AZX7 0027
AZAB2 0009	AZI2 0015	AZM31 0004	AZP14 0022	AZX8 0027
AZABR 0009	AZI3 0015	AZM32 0003	AZP15 0022	AZX9 0027
AZAC 0009	AZI4 0015	AZM4 0005	AZP16 0022	AZXA 0027
AZAC1 0009	AZI5 0016	AZM5 0002	AZP17 0022	AZXA1 0027
AZAC2 0009	AZI6 *0015	AZM6 0003	AZP18 0022	AZXA2 0028
AZAC3 0009	AZI7 0015	AZM7 0002	AZP19 0022	AZXA3 0028
AZAC4 0010	AZIR 0015	AZM8 0002	AZP1B 0023	AZXA4 0028
AZAC5 0009	AZJ 0016	AZM9 0003	AZPIR 0022	AZXAS *0028
AZAC6 0009	AZJ1 0017	AZMT 0104	AZPN 0023	AZXAR 0027
AZAC7 0009	AZJ10 0017	AZMT8 0055	AZPN1 0023	AZXB 0028
AZACR 0009	AZJ11 0017	AZMTC 0057	AZPN2 0023	AZXB1 0028
AZB 0010	AZJ12 0017	AZMTE 0056	AZPNR 0023	AZXB2 0028
AZB10 0010	AZJ13 0016	AZMTG 0104	AZPP 0023	AZXB3 0028
AZB11 0010	AZJ2 0017	AZMTP 0104	AZPP1 0024	AZXB4 0028
AZB12 0010	AZJ3 0016	AZMTS 0104	AZPP2 0024	AZXC 0028
AZB2 0010	AZJ4 0017	AZN 0065	AZPP4 0024	AZXC1 0028
AZB3 0010	AZJ5 0017	AZN1 0074	AZPP5 0024	AZXC2 0028
AZB5 0010	AZJ6 0017	AZN2 0079	AZPP6 0024	AZXC3 0029
AZB7 0010	AZJ7 0016	AZN3 0078	AZPP7 0024	AZXC4 0028
AZB8 0010	AZJ8 0016	AZN4 0066	AZPPR 0024	AZXCR 0029
AZB9 0010	AZJ9 0017	AZN5 0079	AZPS1 0021	AZXI 0104
AZBR 0010	AZJR 0017	AZN1 0018	AZPS3 0021	AZXR 0027

AZY 0029	DA6 0056	DNX 0056	EQT3 0064	FL.8 0058
AZZ 0029	DAMOT *0057	DNZFF 0056	EQT3R 0064	FL.9 *0058
BA 0065	DAKV 0056	*DOUT 0001	EREXP 0078	FL.95 *0058
BCDD 0058	DASTR 0056	DP11 0057	ERLN 0078	FR 0065
BDNA 0060	DB *0057	DP12E 0056	ERROR 0065	FRICT 0078
BDNB 0062	DBHOT *0057	DP8E 0056	EXP 0001	FX 0055
BDXA 0060	DBKV 0056	DPD *0001	EXP13 *0001	FX1 0057
BDXB 0062	DC *0057	DPD1 *0001	FINQ1 0067	FX10 0057
BEGIN 0002	DCMOT *0057	DPDT *0001	FIX 0058	FX1E3 0057
BELLO 0057	DD2 0056	DPI 0056	FL1 0057	FX2 *0057
BETAC 0074	DDCO 0056	DPD 0056	FL10 0057	FX3 *0057
BIG 0058	DDH 0056	DPR1 0056	FL100 0058	FX4 *0057
BLANK 0058	DDIL 0056	DPX 0056	FL108 0058	FX5 *0057
BUG 0074	DDRN 0056	DQINT 0056	FL12 0057	FX6 *0057
BUG1 0074	DDTL 0056	DR 0056	FL139 0058	FX7 0057
BUG2 0074	DDTH 0056	DRC *0057	FL144 0058	FX8 *0057
C 0055	DEG *0058	DRH 0057	FL180 *0058	FX9 *0057
CARDS 0104	DEL 0056	DRHOR 0055	FL1E5 0058	F.A 0064
CCI 0079	DELZ 0055	DSA *0001	FL1.1 *0058	F.B 0064
CD 0065	DEN *0001	DSAT *0001	FL1.2 *0058	F.C 0064
CH 0078	DEN1 *0001	DST *0001	FL1.5 *0058	F.D 0064
CLOSD 0074	DENT *0001	DSTT *0001	FL2 0057	F.E 0064
CLS1 0104	DFCLD *0057	DSUBC 0079	FL288 0058	F.F 0064
CLS2 0104	DF 0055	DSUBH 0079	FL2G 0058	F.G 0064
CLS3 0104	DFHOT 0057	DSWT 0056	FL2GI 0058	F.H 0064
CLS4 0104	DGP 0056	DT 0056	FL2RW 0058	F.I 0064
CNT6 0070	DHE 0056	DT11 0057	FL3 0057	F.J 0064
CNT7 0072	DMRN 0067	DTHO 0056	FL3.7 0058	F.K 0064
CNT8 0073	DIPY 0056	DTHET 0057	FL4 0057	F.L 0064
CNT9 0074	DIVCK 0078	DTI 0056	FL5 *0057	GO 0002
COLUM 0055	DK 0056	DTMAX 0056	FL58 0058	H8 0082
COS 0065	DK11 0057	DTM1 0056	FL6 *0057	H81 0102
COUNT 0055	DK2 0056	DTMIN 0056	FL66 0058	H82 0102
CP3 *0001	DK9 0057	DVF 0055	FL7 *0057	H83 0099
CP31 *0001	DKCC *0057	DVI 0056	FL776 0058	H84 0103
CP3T *0001	DKCI *0057	DVO 0056	FL8 *0057	H85 0103
CPH *0001	DKDP1 0056	DWC 0056	FL9 *0057	H86 0103
CPH1 *0001	DKDPO 0056	DWE 0056	FLCUF 0058	H87 0103
CPHT *0001	DKE *0057	DWH 0056	FLG 0058	H88 0103
CURV1 0063	DKFLG 0057	DWP 0056	FLGAL 0058	H8I 0081
CURV4 0064	DKIN *0057	DWPE 0056	FLGF 0058	H8O 0082
CURV5 0064	DKPCM *0057	DWRE 0056	FLPI 0058	H8P 0102
CURV6 0064	DKPHM 0057	DWT 0056	FLR 0058	H8PR 0102
CURV7 0064	DL 0056	END 0065	FLRB 0058	H8R 0102
CURV8 0064	DMOT 0056	ENOO 0055	FL.1 0058	H8Z 0082
CURVC 0064	DMAX 0055	ENT *0001	FL.2 0058	HC1 0079
CURVR 0064	DMOT 0056	ENT1 *0001	FL.25 0058	HD1 0103
CUT 0059	DNH 0056	ENTT *0001	FL.4 0058	HD3 *0103
D 0055	DNI 0056	EQT1 0064	FL.5 0058	HD4 *0103
DA 0057	DNP 0056	EQT2 0064	FL.6 0058	HDMD *0103

MEDER	0039	LN	0001	NUTHE	0066	PR98	0052	RMD4	*0079
MHI	0079	LO	0065	NUTMH	0071	PR99	0052	RMDMR	0103
ICURV	0043	LQ1	0079	NZMAX	0104	PRES3	0064	ROTAT	*0073
IN	0065	LT6	0075	P	0055	PRIN1	0102	RSUM	0079
INDAT	*0078	LTCW	0078	P3	0079	PRINT	0053	SCURV	0063
INT	*0001	LTH	0075	PA	0054	PRP	0049	SET	0065
IR1	0065	LTHW	0078	PC	0055	PRP1	0050	SIGMA	0079
IR2	0065	LVSAC	0078	PEXP	*0001	PRP10	0050	SIN	0065
IR4	0065	LVSCH	0078	PF	0054	PRP11	0050	SPACE	0064
IT	0103	LVSCH	0078	PG	*0054	PRP4	0050	SORT	0001
ITDCD	0077	LVSCH	0078	PI	0058	PRP6	0050	ST102	0064
ITER	0075	LVSIS	0078	PIH	0079	PRP7	0050	ST108	0064
ITER1	0075	LVSIN	0078	PL	0054	PRP8	0050	ST220	0064
ITER2	0075	MAKER	0079	PL1	0054	PRP9	0050	ST293	0064
ITER3	0076	MODE	0078	PL2	0055	PRPT1	*0001	ST440	0064
ITER4	0076	NCTMP	0104	PLDG	*0001	PRPTY	*0001	ST8R1	0064
ITER5	0076	NCURV	0104	PLR	0054	PRTD	0051	START	0002
ITER6	0076	NE	0065	PNB	*0001	PSORT	*0001	STF72	0064
ITER7	0076	NEHA	0060	PNB1	*0001	PST	*0001	STP1	0064
ITER8	0077	NEHA1	0061	PNBT	*0001	PSTT	*0001	STPIC	0064
ITER9	0077	NEHA2	0060	POWER	0104	PSUBC	0079	STP2	0064
ITERP	0077	NEHA3	0060	PP01	0053	PT	0055	STP2C	0064
ITERR	0077	NEHA3	0060	PP04	0053	PVT	*0001	STP3	0064
ITERX	0077	NEHA4	0060	PP05	0053	PVT1	*0001	STP3C	0064
ITEXP	0077	NEHA7	0060	PP06	0053	PVYT	*0001	STP4	0064
KM	0079	NEHA8	0060	PP07	0054	PZ	0054	STP4C	0064
KCM	0104	NEHA9	0061	PP075	0054	Q	0077	STP5	0064
KCN1	0079	NEHAR	0060	PP08	0054	Q1	0079	STP5C	0064
KCN10	0079	NEHB	0061	PP09	0054	Q1INT	0078	STP6	0064
KCN11	0079	NEHB1	0062	PP40	0059	QINU	0074	STP6C	0064
KCN12	0079	NEHB2	0062	PP41	0059	Q1OK	0073	STP7	0064
KCN13	0079	NEHB3	0062	PP97	0054	RAD	0058	STP7C	0064
KCN17	0079	NEHB5	0062	PP98	0054	RAPA	0061	STP8	0064
KCN39	0078	NEHB6	0062	PP99	0054	RAPA1	0061	STP8C	0064
KCN40	0074	NEHB7	0062	PR	0103	RAPA2	0061	STP9	0064
KCN41	0074	NEHB8	0062	PRO1	0052	RAPA5	0061	STP9C	0064
KCN42	0074	NEHB9	0062	PRO2	0051	RAPA6	0061	STPEX	0064
KCN44	0074	NEHB9	0062	PRO23	0052	RAPA7	0061	STP6	0064
KONS	0079	NEHCP	0104	PRO24	0051	RAPA8	0061	STPG1	0064
KONS0	0078	NEHN	*0104	PRO3	0051	RAPA9	0061	STPG2	0064
KONS1	0078	NEHR	0104	PRO4	0052	RAPB	0062	STPG3	0064
KONS2	0078	NHIT	0104	PR10	0051	RAPB1	0063	STPG4	0064
KONS3	0078	NLEFT	0078	PR11	0052	RAPB2	0063	STPG5	0064
KONS4	0078	NLMAX	0104	PR12	0051	RAPB3	0062	STPZO	0064
KONS5	0078	NRA	*0001	PR13	0052	RAPB4	*0063	SWT	0078
KONS6	0079	NRA	*0001	PR14	0052	RAPB5	0063	S(TP)	0064
KSUBH	0104	NTOTL	0078	PR15	0052	RAPB6	0063	T3	0079
LAST	0079	NUM	0079	PR60	0059	RAPB7	0063	T6	0079
LINT	0065	NUMB	0078	PR61	0059	RAPB8	0062	TCARD	0055
LINTS	0065	NUTCW	0070	PR971	0052	RAPB9	0063	TCW	0079

TCMDK	0070	THINT	0078	TSUBH	0079	WH	0055	XHD	0103
TEMP	0079	THOT	0104	TY	0078	WHT	0055	XLC	*0001
TEMPR	0064	THW	0079	VIS	0001	WK	0055	XLC1	*0001
TES	0065	THWOK	0072	VIS1	*0001	WPI	0055	XLCT	*0001
TEST	*0073	TIN1	0079	VIST	*0001	WPD	0055	XTHIK	0078
THAL	0001	TK	0057	WAF	0055	WPR	0055	Y	*0103
THAL1	*0001	TLO	0065	WCR	0055	WR	0079	YHD	0103
THALT	*0001	TP	0055	WGP	0055	WTI	0055	Z	0103
THI	0065	TSUBC	0079			X	0055	ZERO	*0058