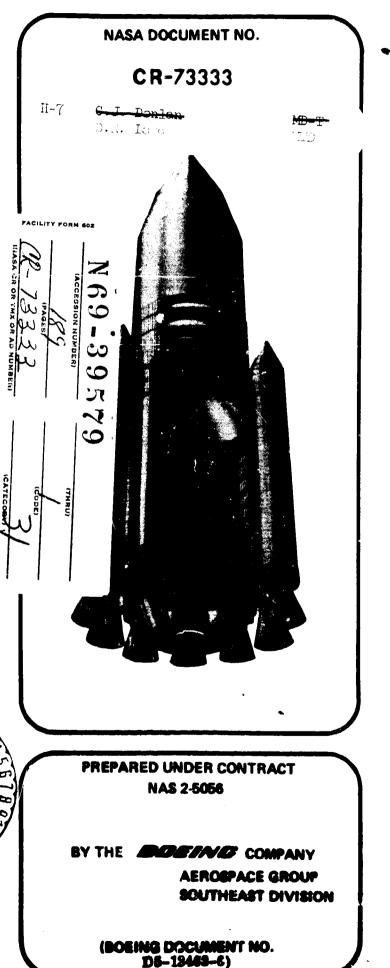
COST STUDIES OF MULTIPURPOSE LARGE LAUNCH VEHICLES

VOLUME VI

COST IMPLICATIONS OF VEHICLE SIZE, TECHNOLOG CONFIGURATION AND PROGRAM OPTIONS





FINAL REPORT FOR COST STUDIES OF MULTIPURPOSE LARGE LAUNCH VEHICLES

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VOLUME VI COST IMPLICATIONS OF VEHICLE SIZE, TECHNOLOGY, CONFIGURATION, AND PROGRAM OPTIONS

PRE PARED UNDER CONTRACT NAS2-5056 FOR NATIONAL AERONAUTICS AND SPACE ADMINISTRATION OFFICE OF ADVANCE RESEARCH AND TECHNOLOGY MISSION ANALYSIS DIVISION SEPTEMBER 15, 1969

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ABSTRACT

Nine volumes including this volume present the final report documentation outlining the accomplishments for the "Cost Studies of the Multipurpose Large Launch Vehicles" (MLLV). NASA/OART Contract NAS2-5056. This volume presents an assessment of and application for the overall study results to show cost implications of vehicle size, technology, configuration and program options.

The MLLV family will consist of a single-stage-to-orbit configuration plus other configurations consisting of a main stage (as used for the single-stage-to-orbit configuration) with various quantities of 260 inch diameter solid rocket motor (SRM) strap-on stages and/or injection stage modules. The main stage will employ LOX/LH_2 propellant with either a multichamber/plug or toroidal/aerospike engine system. The single-stage-to-orbit configuration will have a payload capability of approximately 500,000 pounds to a 100 nautical mile earth orbit. With the addition of the st_rap-on SRM stages and/or LOX/LH_2 injection stage modules this payload capability can be increased incrementally to as much as 1.850,000 pounds.

The contract consisted of four study phases. The Phase I activity was a detailed cost analysis of an Advanced Multipurpose Large Launch Vehicle (AMLLV) family as previously defined in NASA/OART Contract NAS2-4079. Costs for vehicle design, test, transportation, manufacture and launch were defined. Resource implications for the AMLLV configurations were determined to support the cost analysis.

The Phase II study activity consisted of the conceptual design and resource analysis of a smaller or half size Multipurpose Large Launch Vehicle (MLLV) family.

The Phase III activity consisted of a detailed cost analysis of the smaller Multipurpose Large Launch Vehicle configurations as defined in Phase II. Costs for vehicle design, test, transportation, manufacture and launch were determined.

The Phase IV activity (as reported in this Volume) assessed the results of the study including the implications on performance, resources and cost of vehicle size, program options, and vehicle configuration options. The study results provided data in sufficient depth to permit analysis of the cost/performance potential of the various options and/or advanced technologies.

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ABSTRACT (Continued)

KEY WORDS

Advanced Multipurpose Large Launch Vehicles (AMLLV) Half Size Multipurpose Large Launch Vehicles (MLLV) Single-Stage-to-Orbit Multichamber/Plug Engine System 7oroidal/Aerospike Engine System 260 Inch Solid Propellant Rocket Motor (SRM) 260 Inch Solid Propellant Rocket Motor (SRM) Orbital Injection Stage Contract NAS2-4079 Contract NAS2-5056 Payload to 100 NM Orbit Cost Resources Zero Stage Vehicles Parallel Stage Vehicles

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FOREWORD

This volume. Cost Implications of Vehicle Size, Technology, Configuration, and Program Options, is one of nine volumes documenting the results of a twelve month study program "Cost Studies of Multipurpose Large Launch Vehicles". NASA/OART Contract NAS2-5056. The objective of this study was to define cost. cost sensitivities, and cost/size sensitivities of potential future launch vehicles to aid in the guidance of current and future technology programs. The baseline vehicles utilized to make this assessment were:

- 1. The Advanced Multipurpose Large Launch Vehicles (AMLLV) as defined under NASA/OART Contract NAS2-4079.
- 2. The Multipurpose Large Launch Vehicles (MLLV) as defined under this contract and described in Volume II, "Half Size Vehicle (MLLV) Conceptual Design".

The program documentation includes this volume plus a Summary Volume, a Design Volume, a Resources Volume, Cost Volumes, an Advanced Technology Implications Volume, and Appendices Volumes. Individual designations for these volumes are as follows:

Volume I	Summary		
Volume II	Half-Size Vehicle (MLLV) Conceptual Design		
Volume III	Resource Implications		
Volume IV	Baseline AMLLV Costs		
Volume V	Baseline MLLV Costs		
Volume VI	Cost Implications of Vehicle Size, Technology, Configuration, and Program Options		
Volume VII	Advanced Technology Implications		
Volume VIII	Flight Control and Separation, and Stress Analysis (Unclassified Appendices)		

Volume IX Propulsion Data and Trajectories (Classified Appendices)

Data on the 260 inch diameter solid propellant rocket motor were obtained from the Aerojet General Corporation. Data on the multichamber/plug propulsion system were obtained from the Pratt and Whitney Division of the United Aircraft Corporation

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and the Rocketdyne Division of the North American Rockwell Corporation. Data on the toroidal/aerospike propulsion system were obtained from the Rocketdyne Division of the North American Rockwell Corporation.

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These propulsion data were obtained from the propulsion contractors at no cost to the contract. The material received encompassed not only the technical data, but resources, costs, schedules and advanced technology information. This support materially aided The Boeing Company in the preparation of a complete and meaningful study and is gratefully acknowledged.

This study was administered under the direction of NASA/OART Mission Analysis Division, Ames Research Center, Moffett Field, California under the direction of the technical monitor, Mr. Edward W. Gomersall.

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1.0 INTRODUCTION

This study was directed to define the economic aspects of a future launch vehicle system. This work complements the previously completed technological study, "Advanced Multipurpose Large Launch Vehicles", Contract NAS2-4079. (This study is hereinafter referred to as the reference study. The vehicle family defined by this prior study is hereinafter referred to as the baseline AMLLV family.)

The economic aspects to be defined included:

- a. The non-recurring and recurring costs for implementation and operation of the baseline AMLLV family.
- b. The non-recurring and recurring costs for implementation and operation of a half size (MLLV) vehicle family. (Payload capability half that of the base-line AMLLV family.)
- c. Cost effectiveness of program and configuration options.
- d. Cost/size implications, and performance/cost implications of advanced technology applications.

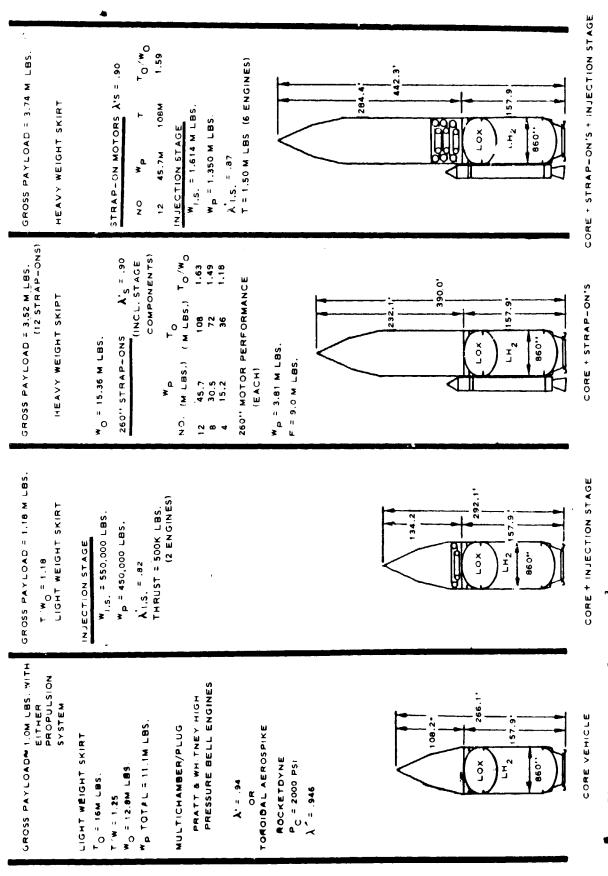
The baseline AMLLV family as defined by the referenced contracted study consisted of:

- a. A single stage to orbit baseline vehicle capable of injecting one million pounds of payload into a 100 n. mi. low-earth orbit.
- b. Injection stage modules which are additive to the main stage for increased payload capability and payload maneuvering.
- c. Strap-on solid or liquid propellant rocket motors for main stage thrust augmentation to improve payload capability.

The design, test, manufacturing, handling and transportation, facilities and launch plans developed under the referenced contracted study were used as a basis for cost definition.

The baseline AMLLV vehicle family is depicted in Figure 1.0.0.0-1. Payload performance for this family is summarized in Figure 1.0.0.0-2.

The baseline MLLV family was that family defined by this study and shown in Volume II. The basic MLLV vehicle configuration employed the following components:



ALL PAYLOADS SHOWN FOR A = 5 LBS FT³ 100 NAUTICAL MILE CIRCULAR ORBIT ETCITEDE 1 0 0.1 ADV/ANCED MATT TIDIDDOCE I ADCE I A

FIGURE 1.0.0.0-1 ADVANCED MULTIPURPOSE LARGE LAUNCH VEHICLE BASELINE FAMILY ļ

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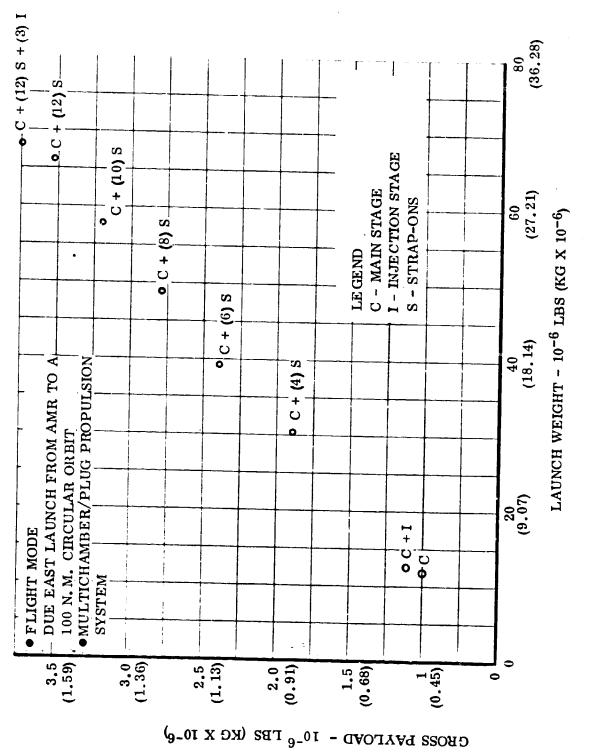


FIGURE 1.0.0.0-2 AMLLIV PAYLOAD VERSUS LAUNCH WEIGHT

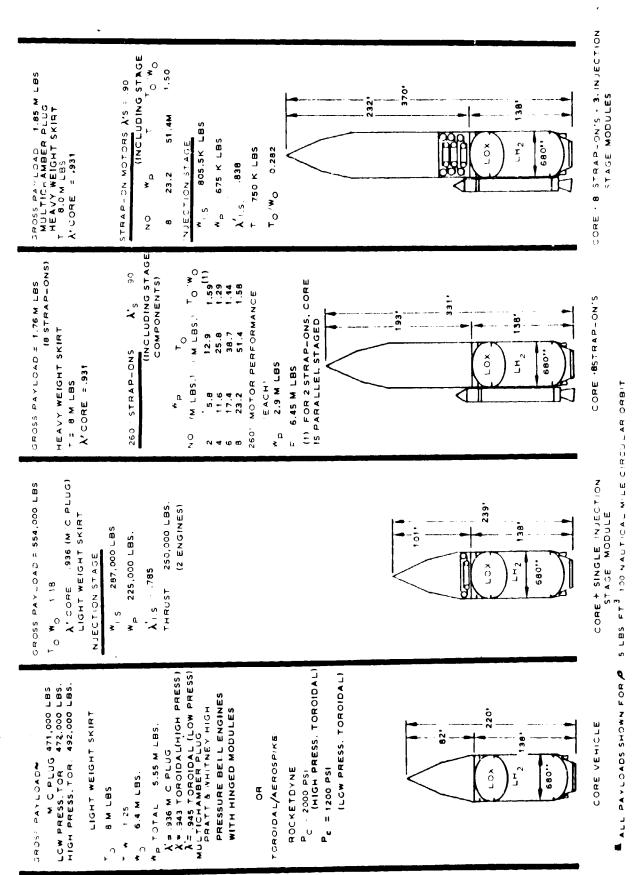
- a. Main (Core) Stage Sized to provide a single-stage-to-orbit payload of approximately 500,000 pounds. Propellants will be liquid oxygen (LOX) and liquid hydrogen (LH₂). Two different engine systems, the multi-chamber/plug (Pratt and Whitney) and the toroidal/aerospike (Rocketdyne) were considered for the main stage.
- b. Injection Stage A modular stage for increased payload capability and maneuvering. The number of modules will vary from one to three. The propulsion system will use high pressure bell engines of Pratt and Whitney design. The propellants will use LOX/LH₂.
- c. Strap-On Stages Sized to provide a payload to a 100 N.M. orbit of approximately 2,000,000 pounds when used to augment the main stage with injection stage modules. Solid rocket motors of 156 inch and 260 inch diameters were considered.

The baseline MLLV vehicle family is depicted in Figure 1.0.0.0-3. Payload performance for this family is summarized in Figure 1.0.0.0-4.

This volume, Cost Implications of Vehicle Size, Technology Configuration and Program Options, presents an assessment of and applications for the overall study results. The detailed cost analyses developed for the AMLLV and the MLLV and reported in Volumes IV and V were utilized to conduct cost effectiveness and parametric analyses of program, configuration, size and technology alternatives.

This volume is divided into eight sections. The first two sections outline and summarize the remaining sections of the document. Section 3.0 presents the objectives, ground rules, guidelines and assumptions. As the cost data presented here were strongly influenced by the utilization of specific design, resources and cost ground rules, these ground rules (which were also reported in previous volumes) are contained herein for ready reference. Section 4.0 presents the cost magnitudes and distributions relative to program phases, vehicle stages and elements, and cost categories. The effects of learning curves on the recurring costs of the various vehicle components are tabulated for both the AMLLV and the MLLV families. Methods for obtaining program cost for a specific vehicle configuration or for a series of vehicles in a program are illustrated by representative examples.

Section 5.0 illustrates the method of using the cost information to determine the cost effectiveness of the program and configuration options. Overall program costs are shown for different program sizes utilizing different vehicles of both the AMLLV and the MLLV configurations. The cost impact of providing manufacturing, test and launch facilities for the largest vehicle configuration (and then utilizing the same facilities for a full range of vehicle configurations in the vehicle family)



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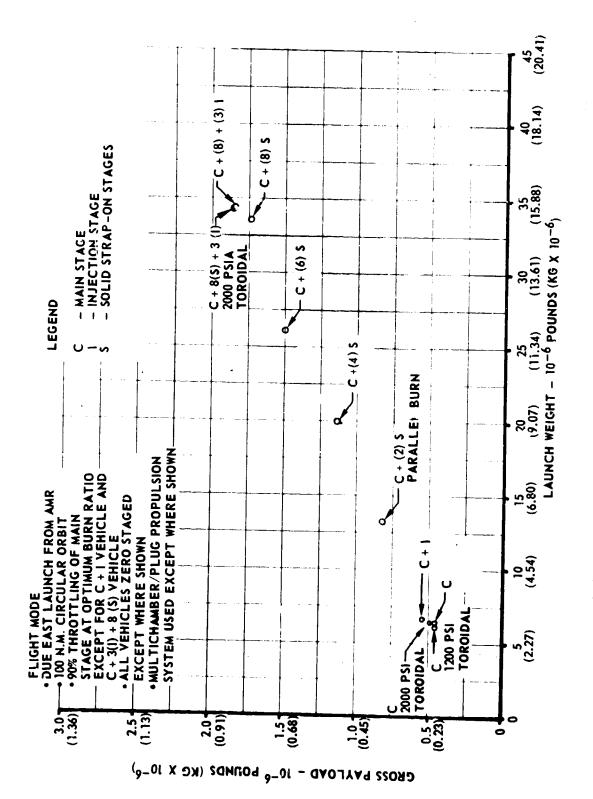
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FIGURE 1.0.0.0-3 HALF SIZE (MLLV) BASELINE VEHICLE FAMILY





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is compared to costs for providing similar facilities sized for a specific vehicle configuration. The effects of the manufacturing and launch rate on overall program cost, estimated on the basis of historical data on the Saturn V program, are presented. Performance and cost potential of various main stage engine options, including various configurations of the multichamber/plug propulsion system and the toroidal/aerospike propulsion system are discussed. Other propulsion system trades, as presented, included the use of liquid strap-on stages versus solid propellant strap-on stages, the use of 156 versus 260 inch solid propellant rocket motor stages and the effect of staged 260" SRM stages versus non-stages 260" SRM stages.

Section 6. 0 contains the methodology for cost effectiveness evaluation of alternative technology applications. Parametric data which can be used to determine whether the development of advanced technology is cost effective is presented. Technology improvements are related to either improved mass fraction (weight improvements) or propulsion performance (I_{sp}). Parametric cost curves as a function of performance, size, etc., for the baseline vehicles are shown. Costs of the major baseline vehicle components (structure, engines, propellant, subsystems, etc.) are defined or modeled in terms of dollars per pound of baseline vehicle dry weight or launch weight. The resulting parametric curves and associated data are used in representative examples to assess the cost-effectiveness of potential technology improvements.

Section 7.0, Risks and Deletions, contains an estimation of those activities and program options which may be deleted from the program thus improving the cost effectiveness. With these deletions, of course, a greater risk is assumed. These have been placed in order of probable increasing risk.

Section 8.0, Program Managers Assessment, presents a critical review of the data and study results by the program manager and the members of the study team. PRECEDING PAGE BLANK NOT FILMED.

2.0 SUMMARY

This volume presents a critical assessment of the overall study results to provide an understanding of the cost implications of launch vehicle size, technology, configuration and program options.

2.1 COST DISTRIBUTIONS AND SIZE IMPLICATIONS

To define the relative cost relationships for development, procurement, and operation of the baseline MLLV and AMLLV families, the "modularized" costs (and supporting resource data) of the two vehicle families were collected and categorized, during the course of the study activity, by three program phases, i.e.:

Phase A "Get Ready" Phase

This category includes non-recurring costs for vehicle design, and for the tooling, equipment and facilities required for production and launch.

Phase B Development Test Phase

This category includes the non-recurring costs for all development test activity required to develop and qualify the launch vehicle, its components and the associated support hardware for manned flight.

Phase C Operational Program Phase

This category includes all of the recurring costs for manufacture and launch of the operational vehicles.

The distributions of program costs showed that the percentage of overall program costs attributable to each of these phases was approximately the same for both the AMLLV and MLLV programs. This is indicative that the relative distribution of costs by program phase will be independent of vehicle size. Generally, the non-recurring costs (the sum of the A and B costs) will be approximately 11 times those of the first operational unit cost. The Phase A costs will be approximately 4 1/2 times and the Phase B costs will be 6 1/2 times those of the first operational unit. respectively. The relative distribution of costs by program phase does not appear to be sensitive to complexity, as the relative distribution of the costs for the three program phases were generally the same for the main stage, the injection stage and the solid rocket motor strap-on stages.

Magnitude of overall cost appears to be primarily influenced by the complexity of the structure or system to be built and secondarily influenced by the difference in size. For example, the cost for the injection stage module will be approximately

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the same as that for a strap-on solid rocket motor (SRM) stage even through the weight of an individual SRM stage will be approximately seven times that of a fueled injection stage module.

The overall magnitude of the costs will be significantly larger for the main stage as the main stage not only is the more complex stage but is also the primary stage of the launch vehicle and, therefore, must absorb a significant portion of the costs for program management, system engineering, launch facilities and liquid stage manufacturing and test facilities.

Further, the <u>magnitudes of the costs</u> in Phases A, B, and C <u>will not be significantly</u> <u>sensitive to the relative size of similar articles</u>. For example, the half size (MLLV) main stage costs for these phases will be approximately 85 percent those of the full size (AMLLV) main stage.

The magnitude of component costs in Phases A and C will, however, be more nearly directly related to the quantity required per operation vehicle. For example, the magnitude of engine and SRM costs per vehicle will be almost directly related to the number required per vehicle.

The magnitude of the component costs for Phase B will not be sensitive to the quantity required per vehicle. For example, the development test costs for the SRM stage will be approximately the same regardless of the quantity to be used per vehicle.

As will be discussed subsequently, the magnitude of the A and C costs for a vehicle program will be strongly influenced by the anticipated production and launch rate. The magnitude of the development test or B costs, however, will be insensitive to the anticipated production and launch rate.

The two R&D flight tests specified for the development test program will represent approximately 25% of the overall non-recurring costs required for either of the two vehicle systems. If useful payloads could be flown on the R&D test flight vehicles, program costs could be substantially reduced.

The addition of either injection stages or SRM stages to the primary main stage will not significantly increase the magnitude of the non-recurring program costs. For example, non-recurring costs for the main stage alone will be 36 percent of those for the main stage and SRM stages.

The distribution of Phase A costs by cost categories (i.e., manpower, material, tooling, facilities and equipment) indicates that a significant portion of the A costs will be attributable to facilities and equipment. The next largest cost category will be tooling. The tooling costs will be the most sensitive cost category relative to vehicle size, even though they will be reduced by only 28 percent as the vehicle size is reduced by 50 percent.

A major portion of the Phase A costs will be involved in the provision of the launch facility. These costs will represent approximately 45 percent of the total get ready costs for the MLLV and AMLLV single-stage-to-orbit vehicles. As the injection stage will be the same diameter as the main stage, and will fit atop the main stage without significantly increasing the length of the vehicle, its effect on launch facility costs will be negligible. For use of the SRM strap-on stages, however, a significant increase in the launch facility will occur.

The relative distribution of costs by program cost categories and elements (i e., structures, engines, systems, etc.) will be generally the same as that of the two stage Saturn V for both the MLLV and AMLLV single-stage-to-orbit vehicles. The engine systems, however, for the AMLLV and MLL? vehicles will represent a larger percentage of the overall operational program costs than do those of the Saturn V. This is attributable to the number of engines involved. For the MLLV and the AMLLV. 24 individual engines will be used for each main stage. By comparison, the two stage Saturn V has a total of 10 engines for both stages.

2.2 COST EFFECTIVENESS OF PROGRAM AND CONFIGURATION OPTIONS

The specific payload requirements, in terms of required payload weight per laurch will have a major influence on the choice of the vehicle configuration to provide the most cost effective program. However, the cost per pound of delivered payload generally will decrease as the required payload weight per launch is increased. In other words, the lower payload single-stage-to-orbit vehicles will be the least cost effective vehicles in the MLLV and AMLLV families. Cost effectiveness will improve as SRM strap-on rocket motors are added to the main stage.

Only small operational programs will be required to amortize the additional nonrecurring costs for development and implementation of the strap-on stages (i.e., programs requiring three million pounds of payload to orbit for the MLLV and six million pounds of payload to orbit for the AMLLV).

Use of the injection stage as a propulsive element to increase payload to a 100 N. M. orbit will never be as cost effective as utilization of the SRM strap-on stages or an increase in the size of the main stage. For this reason, use of the injection stage should be considered only, after achievement of orbit, for payload maneuvering or for missions beyond earth orbit. (The injection stage should be considered

as part of the payload to orbit rather than as part of the propulsion system to achieve orbit.)

The operational cost effectiveness values of all of the possible configurations in the MLLV family were compared (1) to those of configurations in the AMLLV family and (2) to those of the two stage Saturn V vehicle and its potential uprated deriva – tives employing 156 inch and 260 inch diameter SRM strap-on stages. This comparison lead to the very significant study conclusion that, for a given payload per launch requirement. operational costs will not be significantly influenced by the choice of any specific launch vehicle configuration with the capability of providing the required payload. Operational costs do not appear to be sensitive to design or configuration options. (Costs are, however, sensitive to payload size as discussed below.) This conclusion assumes that all possible configurations will be produced and operated within the same program philosophy, limitations and ground rules.

The data showed that <u>improved cost effectiveness</u> (as stated above) <u>will be obtained</u> as the payload per launch requirement in increased. In other words, there appears to be a "quantity discount" relative to larger sized payloads. This quantity discount is based on the assumption that whatever size vehicle is used, the same production and launch rate will be maintained.

This study, as well as prior experience with the Saturn V and other programs, showed that the cost of a launch vehicle will be significantly effected by the production and launch rate. A primary factor causing increased cost at low rates is the inflexibility within the current manufacturing and launch philosophy relative to the use of personnel and skills. The costs for a full complement of personnel and skills, (required at the production and launch facilities regardless of the rate) will significantly increase the unit cost at low rates. A major factor in reducing costs would be an increase in the production and launch rate from approximately two vehicles per year to approximately six vehicles per year.

The cost trades of engine options showed that program costs were only slightly effected by the various possible adaptations to either the multichamber/plug or toroidal/aerospike engine systems in terms of size of the engine systems, operating pressure, number of modules, etc.

The engine option trades indicated that <u>lower operational cost will result from the</u> use of the larger and/or higher performance engine options with both the single-stageto orbit vehicles and vehicles containing strap-on stages. For example, operationally it will be more cost effective to use the higher performance 2000 psi toroidal/aerospike engine with eight modules, each rated at 2 million pounds thrust than to use the lower performance 1200 psi modules rated at 2 million pounds thrust or the higher performance 2000 psi toroidal/ aerospike engine with 16 modules rated at 1 million pounds thrust each.

The above conclusion assumes a moderate or large operation. However, for small operational program sizes which cannot effectively amortize the higher non-recurring cost of the larger nigher performance systems, the lower performance, lower thrust, systems will be more cost effective.

If low cost liquid stages can be developed and procured at the same price as the SRM strap-on stages, a minor reduction in program cost will occur, attributable to easier transportation and handling of the lighter weight (empty) liquid stage. The transportation and handling costs for use of either of these stages will be so nearly the same, however, that no significant cost advantages can be attributed to either system.

The use of 260 inch diameter SRM's will be more cost effective than the use of equivalent performance 156 inch diameter SRM's for an operational program. Although the non-recurring costs for the 156 inch SRM's will be less than that of the 260 inch SRM's, the lower production costs of the 260 inch SRM's will make them become more cost effective as program size increases. Again, as with the liquid engines. the cost trades tend to favor the larger sizes over the smaller sizes.

The baseline program calls for use of the solid rocket motor strap-on stages in a "zero" stage mode wherein all of the SRM's will be ignited at liftoff and separated at the same time after burn out. A sequential staging concept such that approximately 3/4 of the quantity of SRM's would be ignited at launch and the remaining 1/4 ignited after burnout of the initial 3/4 would in effect provide a three stage vehicle and increase the payload capability by better than 10%. This alternative concept would only slightly increase the program cost but would provide a significant improvement in payload and, therefore, is an attractive option for the vehicle system.

2.3 COST EFFECTIVENESS OF ALTERNATE TECHNOLOGY APPLICATIONS

Parametric cost and performance data and its application show the maximum dollars that can be spent for an alternative technology for any specified vehicle program. These data (1) relate the required main stage size for a given payload to specific impulse and mass fraction, and (2) show the relationships of program cost to main stage size.

The data relative to improvements in structural efficiency indicate that the programs with single-stage-to-orbit vehicles will be more cost sensitive to improvement or degradation in mass fraction than those programs employing vehicles with strap-on stages. Similar analyses showed that the AMLLV and MLLV single-stage-to-orbit

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configurations will be more cost sensitive to changes in specific impulse than will configurations with strap-on stages.

Application of the mass fraction and specific impulse changes show the following cost effects for a program to place 20 million pounds of payload in orbit. For the AMLLV single-stage-to-orbit vehicle, a 0.02 improvement in mass fraction will result in a program cost reduction of seven percent. Similarly, a five percent improvement in specific impulse will reduce the program costs by five percent. A degradation of five percent in specific impulse will increase the program cost 6.5 percent.

2.4 COST REDUCTION ANALYSIS

Cost reduction of the baseline programs can be achieved through configuration modifications and/or changes in program philosophy relative to design, manufacturing, and test and launch. <u>Changes in program philosophy will</u>, however, <u>be much more</u> <u>effective in reducing costs</u>. Philosophy changes include such things as utilization of the two R&D flights to deliver unmanned but useful payloads; modification to the manufacturing and launch procedures used with low production and launch rates, to provide more effective utilization of personnel and skills; deletion of the facility checkout vehicle (the first R&D flight vehicle would be used for facility checkout); reduction in instrumentation; deletion of redundant components; reduction of postmanufacturing checkout; deletion of dynamic tests; deletion of static firing acceptance tests; reduction of tolerances; and reduction of the safety factor from 1.40 to 1.25. (The above are listed in order of increasing risk as the list progresses.)

A cost reduction of approximately 40% appears possible for a typical program to develop and launch 36 MLLV single-stage-to-orbit vehicles. The resource and cost analyses of this study were accomplished on the basis of the existing techniques utilized for the Saturn V launch vehicle. Similar cost reduction methods have been proposed for the Saturn V but have yet to be implemented.

3.0 GROUND RULES, GUIDELINES AND ASSUMPTIONS

The guidelines and assumptions for this study were developed from the contractual requirements, the previous AMLLV study (NAS2-4079), and applicable data from previous and current studies. Where special circumstances dictated an arbitrary assumption, The Poeing Company and the NASA technical monitor concurred on a suitable guideline.

The resource plans were based on current Saturn V philosphies to the maximum extent possible. No attempt was made to tailor the program for cost optimization.

Where possible, the cost estimates were based on direct costs with burden costs added as separate items.

Resource inputs for recurring and non-recurring items were received from functional organizations within The Boeing Company and from propulsion contractors (Aerojet General, Pratt and Whitney, and Rocketdyne). Most of the direct inputs were in terms of manhours: however, total dollar costs were also received for several items, i.e., material, equipment, engines, etc.

The Boeing Manufacturing Departments at the Michoud Assembly Facility and at Huntsville provided manhours and material estimates for the following items: 1) Fabrication, Major and Minor Assembly of the Sub-System Components, 2) Manufacturing Test Manhours, 3) Raw and Production Material, 4) Planning manhours, 5) Tool Design manhours, 6) Tool Fabrication and Erection hours, 7) Manufacturing Development hours, and 8) MGSE and Handling/Transportation Equipment hours and dollars.

The Boeing Huntsville Engineering Department provided basic engineering design and sustaining engineering manhours. The Boeing Facilities Department at Huntsville, BATC and Michoud provided costs of the brick, and mortar facilities for production, test and launch: transportation and handling equipment: capital equipment and maintenance costs. The Boeing Test Organization at Huntsville provided manhours and costs for conducting Developmental Testing, Structural Tests, Systems Development (Systems Breadboard), Systems Tests, Dynamic Tests, Manufacturing Development and Wind Tunnel Tests.

The Boeing Engineering Department at BATC provided costs for Launch Operations and Launch Vehicle Ground Support Equipment (LVGSE) and Test Equipment.

The propulsion contractors provided costs for the solid rocket motors, toroidal/ aerospike engine and the multichamber/plug engines. The liquid engine data was supplemented with data received from the Propulsion Office at NASA/MSFC.

The details associated with these direct inputs are displayed and summarized in the "Resources Implications" Volume III of this report.

The following ground rules, guidelines, and assumptions were utilized for this study activity, "Cost Studies of Multipurpose Large Launch Vehicles" Contract NAS2-5056:

a. Design

- 1. Direct ascent to 100 nautical mile circular earth orbit was the primary mission used to size and establish the baseline vehicle design, to establish the trajectory for heating and control analyses, and as the reference for performance comparisons.
- 2. The vehicles will be launched due east from AMR.
- 3. Payload configurations will be as follows:
 - a. The payload, exclusive of the nose cone, will have a constant diameter.
 - b. Uniform distribution of mass within payload envelope was assumed.
- 4. Stages and vehicle subsystems will be expendable.
- 5. All study vehicles will be manrated. The design criteria and the necessary combination of ground and flight testing were defined based on those established for the Saturn IB/Gemini and Saturn V/Apollo systems.

b. Test

- 1. Present NASA/MSFC and KSC test philosophies will be continued.
- 2. Two R&D flight tests will be required to qualify the vehicle. The development test program for either the AMLLV or the MLLV will provide for two unmanned flight tests of the maximum size configuration in the selected vehicle family.

- 3. A facility checkout vehicle will be provided for initial checkout of the manufacturing, test, and launch operations, tooling, equipment and facilities.
- 4. A dynamic test will be included in each program (either AMLLV or MLLV) for the maximum size vehicle (strap-ons will be simulated).
- 5. Development testing of the main stage and injection stage will be conducted in new dynamic and structural test facilities constructed adjacent to the factory building.
- 6. The solid motors will require a development program and qualification testing.
- 7. Engine acceptance test firing and trim by engine contractor will be required.
- 8. Static test firing will be required for final acceptance of the main stage and injection stage.
- 9. Static test firing will be conducted on the launch pad.
- 10. All subsystems functional and acceptance testing will be performed by the vendor except as noted.
- c. Manufacturing
 - 1. All stages will be built in factories adjacent to navigable waterways.
 - 2. Main stages and injection stages will be fabricated at the NASA Michoud site (or its equivalent located on a navigable waterway) in a new factory building.
 - 3. The 260 inch diameter solid rocket motors (SRMs) will be manufactured at the Aerojet General Facility in Dade County, Florida.
 - 4. The 260 inch SRM strap-on stage structural assemblies, consisting of the nose cone, forward skirt, aft skirt and attachment fittings will be fabricated at Michoud and sent to the SRM contractors facility at Homestead, Florida for assembly to the solid rocket motor.
- d. Transportation
 - 1. The vehicle elements will be transported from the manufacturing facilities to the launch facility on towed barges.

- 2. Land transportation will be required for the main and injection stages at the manufacturing facility (but not at the launch site).
- 3. At the launch facility all stages will be lifted directly off their barges and placed in the selected location by a large traveling gantry hoist; therefore, no additional transportation equipment will be required.
- 4. The requirements for transporting and handling the elements of the half size (MLLV) vehicle will be the same as those of the full size (AMLLV).
- 5. No land transportation of the SRM stage will be required, as it will be lifted directly from the manufacturing pit and placed aboard the towed barge used for transport to the launch facility.
- 6. The barges used to transport the SRM stages from the manufacturing site to the launch pad will also serve as storage facilities. These barges will be anchored in protected, yet remote locations, and towed to the launch pad as required for vehicle assembly.
- 7. At the launch site, the SRM's will be lifted directly from the barge and placed in position on the launch pad by a mobile overhead gantry crane. This same track mounted gantry will also be used to lift the main and injection stages.
- e. Launch
 - 1. The launch pad will serve as the static firing stand for main and injection stages, the refurbishment facility, the vertical assembly and checkout facility and finally the launch pad.
 - 2. The launch site will be in the vicinity of Cape Kennedy to share the utilization of the available support facilities, support personnel, and existing tracking networks.
 - 3. Although the acoustic siting criteria indicate that an off-shore site is required, an on-shore site was specified to provide comparable facility, equipment, tooling and cost requirements to those of existing systems.
 - 4. Mating of the SRM and injection stages to the main stage will be at the launch pad. Final vehicle assembly and checkout will be in the launch position.

f. Cost

1. All propulsion costing, performance, and design data necessary in the evaluation were compiled from appropriate propulsion contractors (i.e., the contractors specifically working on the respective systems).

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- 2. Costs were based on 1968 dollars without an inflationary factor. Funds were assumed to be available as required.
- 3. Launch and production rates will be two vehicles per year.
- 4. All cost values in this report are contractors cost values only and do not include profit or fee, with the exception of the Solid Rocket Motors and liquid engines.
- 5. The first unit has been defined as the first flight vehicle: (the first R&D flight test) effects of learning curve(s) enter after that unit.

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COST DISTRIBUTIONS, SIZE IMPLICATIONS, LEARNING CURVE EFFECTS AND METHODS FOR COMPILING PROGRAM COST

This section summarizes the input cost data and shows the distribution of costs by 1) program phases, 2) vehicle stages and elements, and 3) cost categories. The implications of vehicle size on the costs and their distribution are illustrated and discussed. The effects of learning on recurring costs are tabulated and graphically illustrated to provide tools for conducting cost effectiveness analyses as discussed in subsequent Sections 5.0 and 6.0. Methods are given for compiling overall program costs.

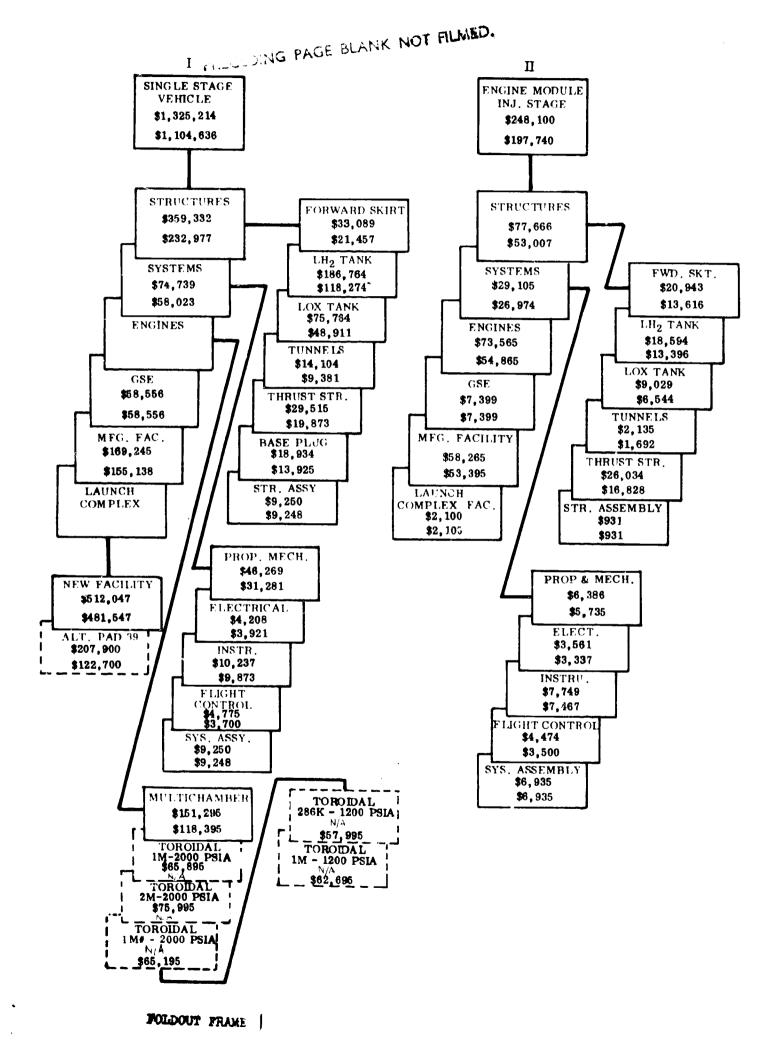
The "modularized" cost data shown in detail in Volumes IV and V are summarized by program phases and stage and program elements in Figures 4. 0. 0. 0-1 through 4. 0. 0. 0-3. The costs shown are additive i. e., the Phase A costs for an MLLV vehicle incorporating a main stage plus an injection stage engine module plus two injection stage fuel modules plus four strap-on stages can be determined by adding the main stage costs (Column I) plus the injection stage engine module costs (Column II) plus twice the injection stage fuel module costs (two times Column III) plus the strap-on stage fixed cost (Column IV) plus one-half the variable cost of eight strap-on stages (one-half of Column V). The same addition is possible to determine the program buildup for Phase B costs. To determine the overall program costs for Phase C, however, learning effects must be applied to the multiples of stages required for the program. These effects and their application are shown and discussed in Sections 4. 2 and 4. 3.

The results of adding the various elements (with appropriate learning curve factors as applicable) to determine Phase A, B and C costs are summarized in Figure 4.0.0.0-4. This chart shows, for example, that the total non-recurring costs (Phase A costs plus Phase B costs) for an MLLV vehicle consisting of a main stage plus eight SRM stages plus a three module injection stage will be 4.09 billion dollars. The recurring cost of the first operational vehicle will be 372 thousand dollars. Similarly, the recurring cost of the first operational MLLV single-stageto-orbit vehicle will be 251 thousand dollars. The non-recurring costs for development of this vehicle (not shown on figure) will be 2.78 billion dollars.

4.1 COST DISTRIBUTIONS AND VEHICLE SIZE IMPLICATIONS

The detailed "modularized" cost data shown in Volumes IV and V were analyzed to determine the distribution of costs relative to:

- a. Program Phases
 - 1. "Get Ready" costs (A costs)
 - 2. Development test costs (B costs)
 - 3. First operational unit costs (C costs for the 3rd flight unit)



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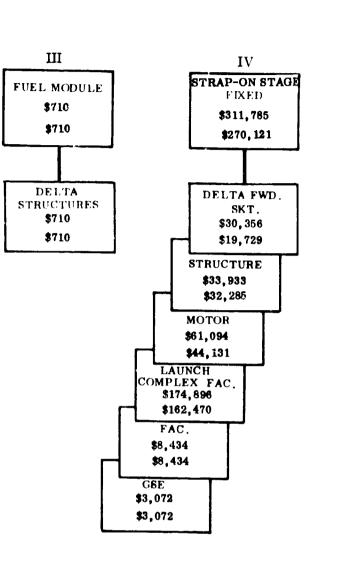
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• AMLLV COST SHOWN ON TOP

- MLLV COSTS SHOWN ON BOTTOM

- •DOLLARS ARE IN THOUSANDS.
- NOTES: []]] ALTERNATE SYSTEMS.





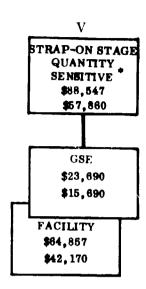
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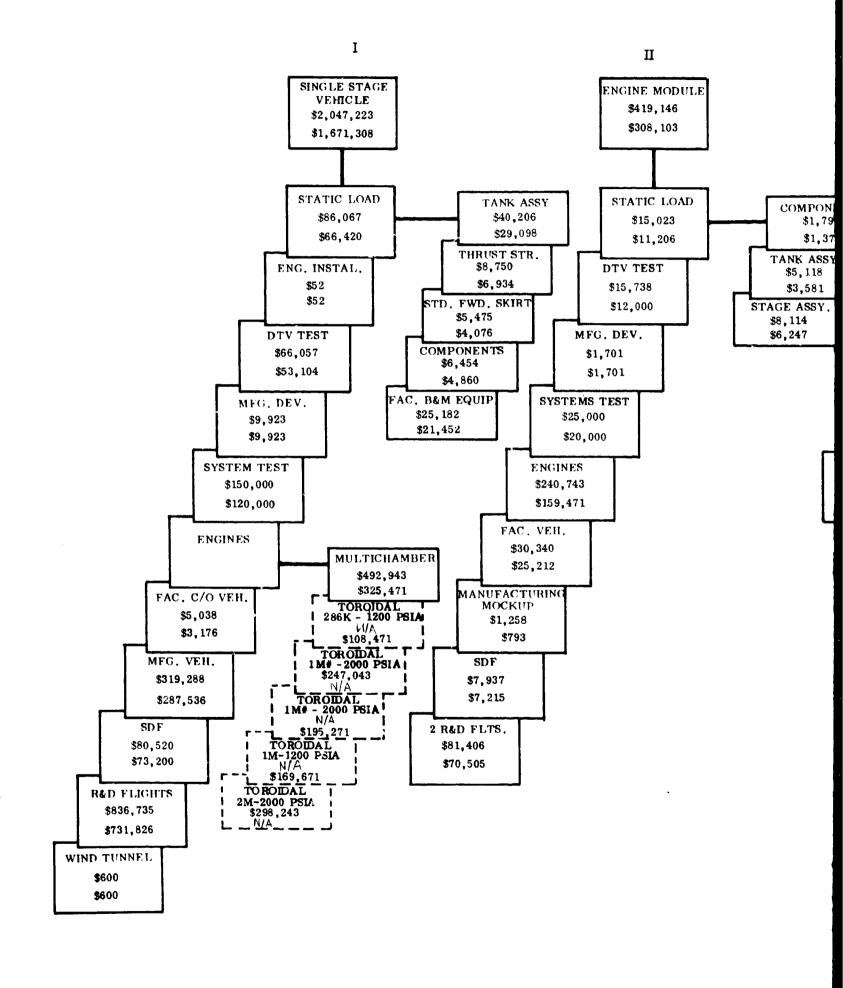
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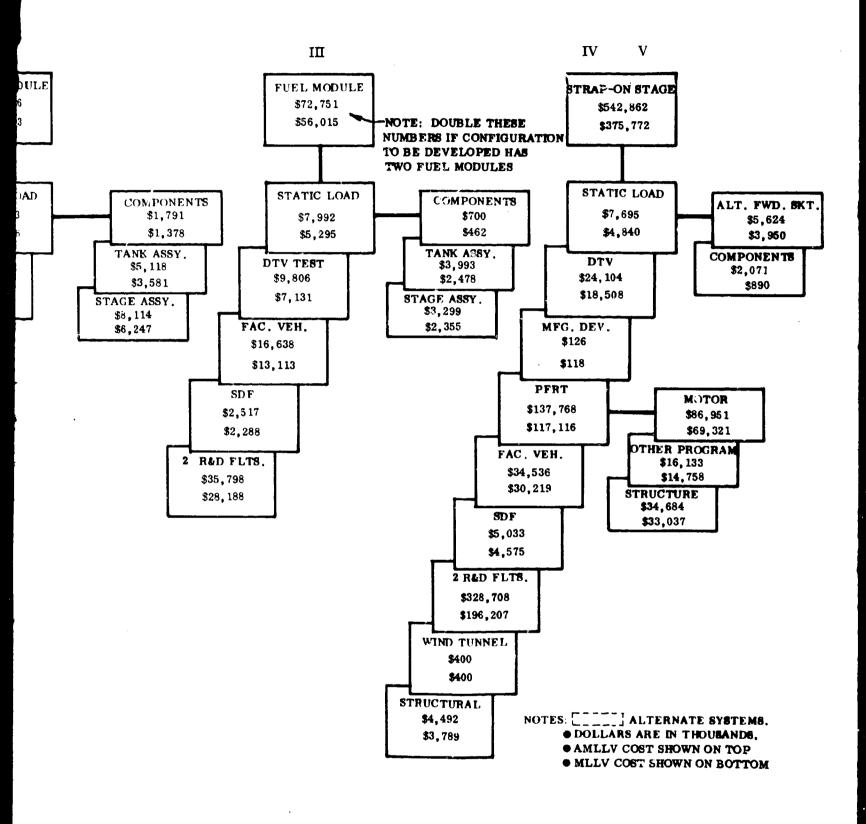
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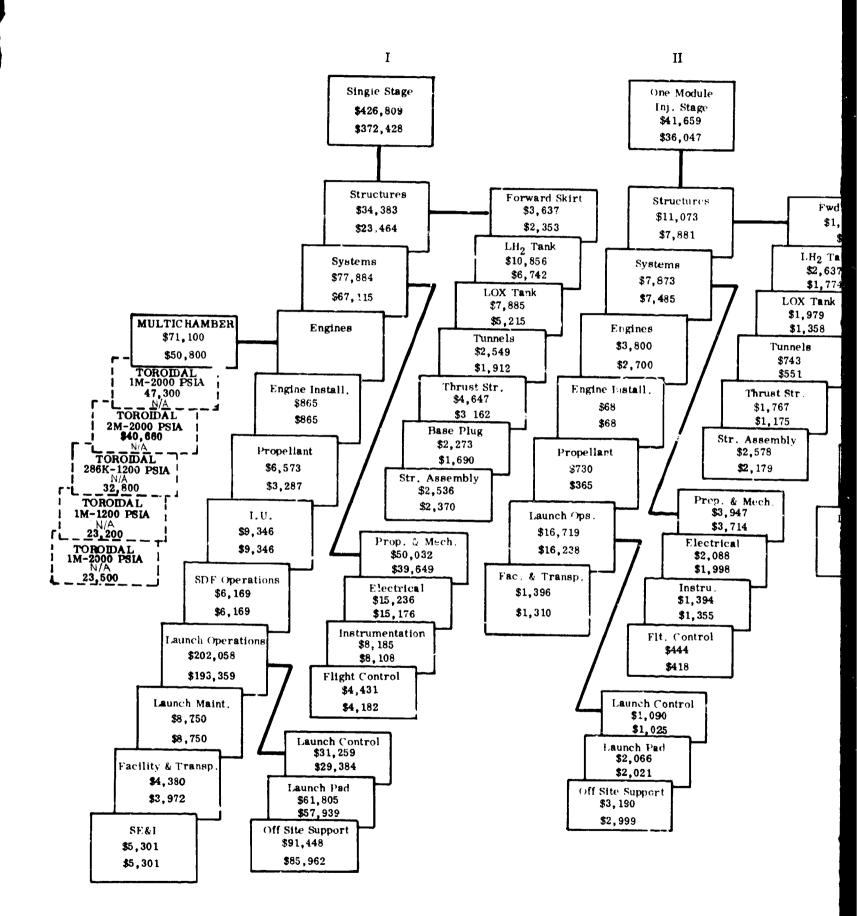
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FIGURE 4.0.0.0-2 DEVELOPMENT TEST COST ("B" COST) SUMMARY

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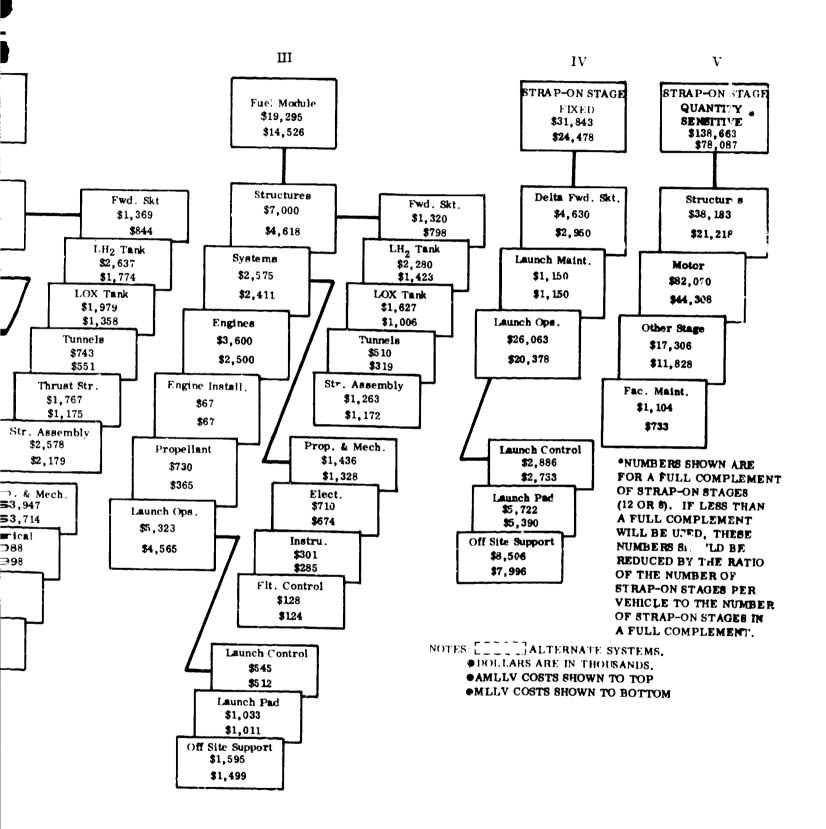
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FIGURE 4.0.0.0-3 FIRST UNIT COST ("C" COST) SUMMARY (APPLICABLE TO FIRST R&D FLIGHT VEHICLE ONLY)

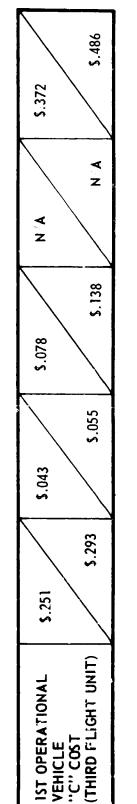
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(DOLLARS IN BILLIONS)	TOTAL	\$1.630 \$1.974	\$2.462 \$3.150	\$4.092 \$5.124
	2 R&D FLIGHTS	N Å N Å	\$1.049 \$1.313	\$1.049 \$1.313
	FULL COMPLEMENT OF STRAP-ON STAGES	\$.328 \$.400	5.180 5.214	\$.508 5.614
	THREE MODULE INJECTION STAGE	5.198 5.249	5.294 5.413	5 .492 5 .662
	MAIN STAGE	\$1.104 \$1.325	5.939 51.210	\$2.043 \$2.535
		GET READY "A" COSTS	DEVELOPMENT TEST "B" COSTS	TOTAL NON-RECURRING

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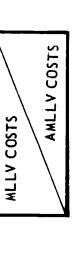


FIGURE 4.0.0.0-4 COST SUMMARY - AMLLV/MLLV BASELINE FAMILY

b. Program Elements

- 1. Stage costs Main stage, injection stage, strap-on stage, etc.
- 2. Component costs Structures, propulsion and mechanical, electrical and electronic, etc.
- 3. Operations costs Manufacturing, test, transportation, launch, etc.

e. Cost Categories

- 1. Labor
- 2. Material
- 3. Tooling
- 4. Equipment
- 5. Facilities

The resulting data is summarized in Figures 4.1.0.0-1 through 4.1.0.0-10. Figure 4.1.0.0-1 shows the apportionment of stage costs by program phases. Figure 4.1.0.0-2 shows the stage cost distribution by program phases for the maximum size AMLLV and MLLV vehicles. These figures indicate that the costs for the main stage development and operation with an MLLV or AMLLV maximum size (1) vehicle will be approximately two-thirds of the total A, B and/or C costs. Costs for the three module injection stage and for the full complement of strap-on stage will be approximately one-fifth and one-eighth of the total costs respectively.

The majority of the costs are attributable to the main stage because the main stage is the primary stage of the launch vehicle and, therefore, must absorb a significant portion of the fixed program costs associated with:

- a. Program Management and System Engineering.
- b. Liquid stage manufacturing and test facilities (construction, checkout, operation and maintenance).
- c. Launch facility (construction, checkout, operation and maintenance).

The apportionment of costs by program phases and stages provided the following relationships:

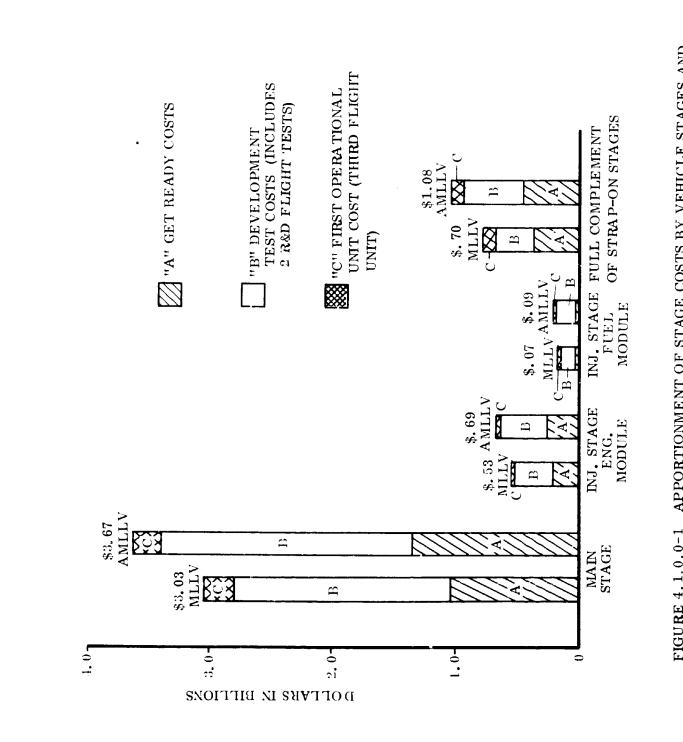
MLLV AMLLV

a. Main Stage

A C (3rd Flight Unit)

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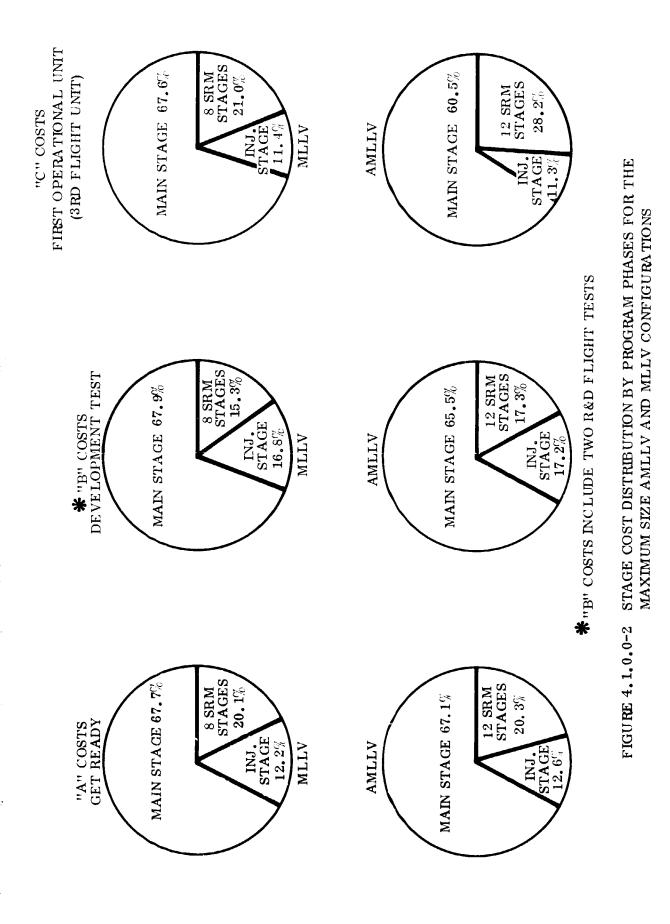
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	B C (3rd Flight Unit)	6.66	6.99
	A + B C (3rd Flight Unit)	11.06	11.51
	AB	0.66	0.65

NOTE: (1) Maximum size vehicle refers to a vehicle incorporating a main stage plus a three module injection stage plus a full complement of strap-on stages.

b.	Injection Stage (Three Module)	MLLV	AMLLV
	A C (3rd Flight Unit)	4.68	3. 42
	B C (3rd Flight Unit)	8.92	7.18
	A + B C (3rd Flight Unit)	13.60	10.60
	$\frac{A}{B}$	0.52	0.48
с.	Strap-On Stages (Full Complement)	MLLV	AMLLV
	A C (3rd Flight Unit)	4.22	2.92
	B C (3rd Flight Unit)	4.83	3.95
	$\frac{A + B}{C \text{ (3rd Flight Unit)}}$	9. 05	6.87
	A B	0.87	0.74

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(Continued)

AMLLV MLLV Maximum Size Vehicle A C (3rd Flight Unit) 4.35 4.07 B C (3rd Flight Unit) 6.63 6.44 $\frac{A + B}{C \text{ (3rd Flight Unit)}}$ 10.98 10.51 $\frac{A}{B}$ 0.66 0.63

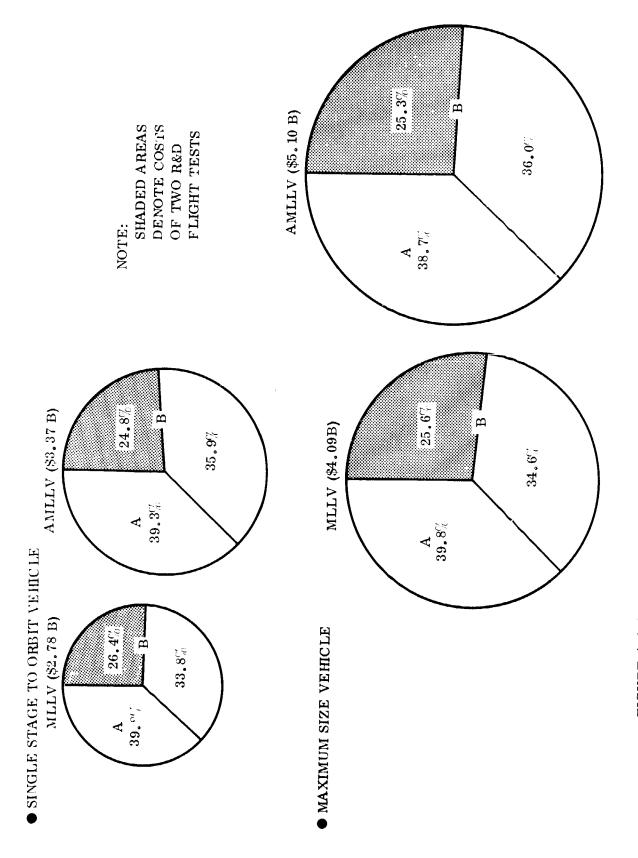
B costs used for the above ratios include the costs of two R&D flight tests of a vehicle incorporating a main stage plus a three module injection stage plus the maximum complement of strap-on stages. The cost data presented in Figure 4.1.0.0-3 shows that the costs of the two R&D flight tests represent approximately one-fourth of the non-recurring costs for either the MLLV or AMLLV vehicle families.

If useful payloads could be flown on these R&D flight test vehicles, the non-recurring costs would, therefore, be reduced by a factor of 25%. This overall savings would not, however, be realized within the total program costs as the costs of the first two flight units would increase by approximate'y 10% to account for position on the learning curve, the additional time for the initial launch cycles and the additional instrumentation requirements.

Figure 4.1.0.0-4 shows the stage costs for phase A distributed by the major program elements. These costs are modularized and presented in such a manner that they can be added. The solid rocket motor strap-on stage "A" costs are for the maximum vehicle configurations, i.e., eight MLLV and twelve AMLLV strap-on stages. "A" costs for the injection stage fuel modules are for design effort only, as the facilities provided for the engine module of the injection stage will be adequate for production and operation of the fuel modules.

The "B" costs for the various vehicle stages are displayed in Figure 4.1.0.0-5. These costs are distributed by costs attributable to each of the major development tests.

The basic approach used in compiling the non-recurring cost data shown in Figures 4.1.0.0-6 through 4.1.0.0-9 assumed that all launches will be made using only one of the several possible MLLV configurations shown. All included costs relate to facilities, equipment and tooling sized for production and launch of only the configuration being used. The two R&D flight test vehicles are of the specific operational vehicle to be flown.



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FIGURE 4.1.0.0-3 FLIGHT TEST COSTS RELATIVE TO NON-RECURRING COSTS

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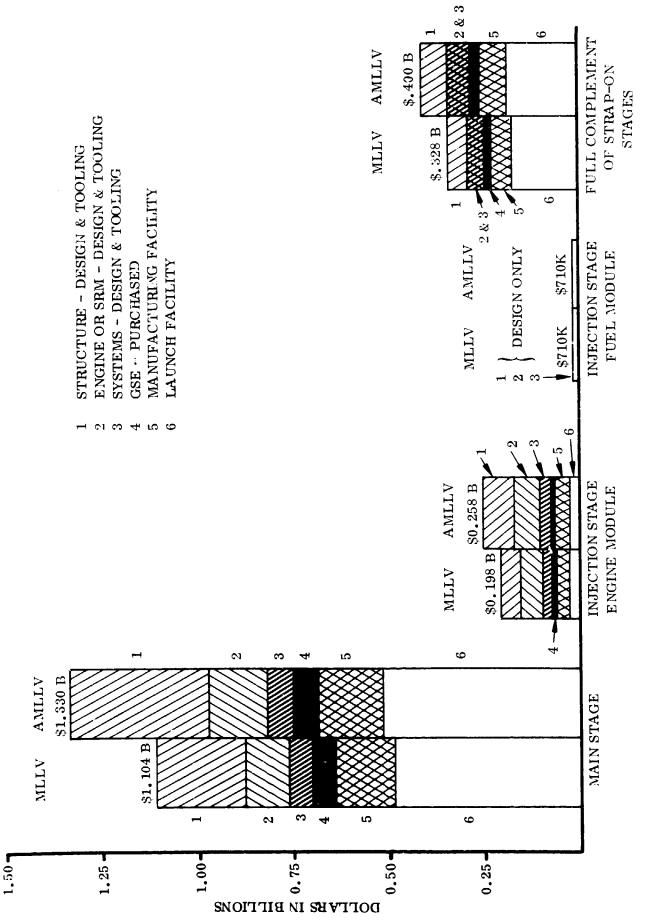
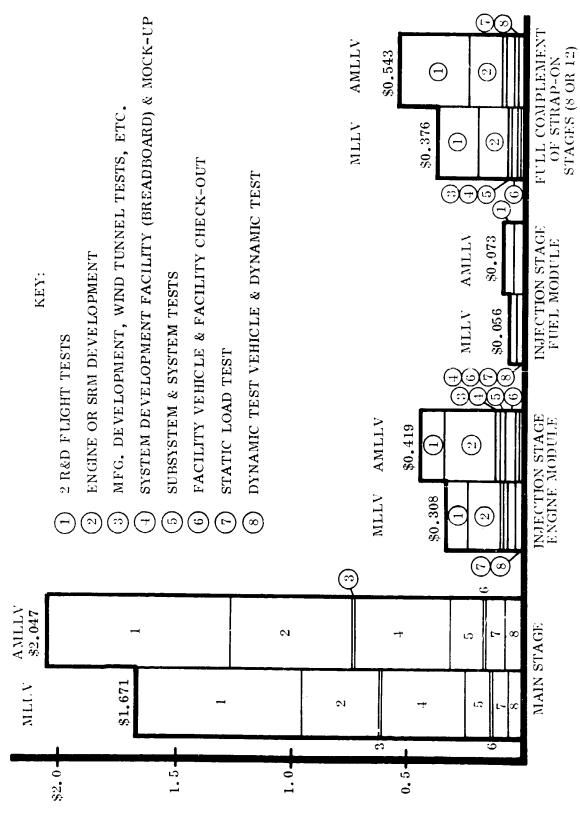


FIGURE 4 1.0.0-4 STAGE ELEMENT COST DISTRIBUTION FOR PHASE A

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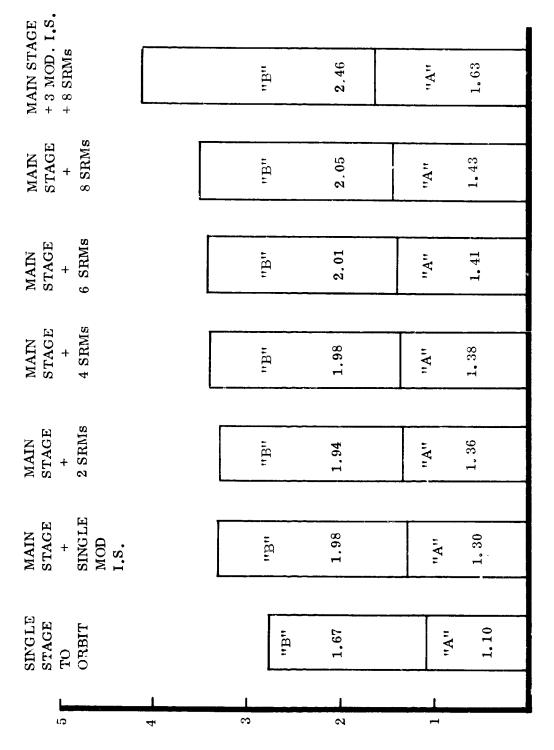
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FIGURE 4. 1. 0. 0-5 STAGE ELEMENT COST DISTRIBUTION FOR PHASE B

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FIGURE 4.1.0.0-6 MLLV NON-RECURRING COST SUMMARY

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+ 3 MOD. I.S. MAIN STAGE + 12 SRMs "B" 3.13 "A" 1.97 + 10 SFMs + 12 SRMs2.591.73 "B" "A" STAGE MAIN STAGE MAIN 2.551.70 'nA'n "B" + 8 SRMs STAGE MAIN 1.67 2.51uВu "A" + 6 SRMsSTAGE 2.461.65 MAIN "B" "A" + 4 SRMsSTAGE MAIN 2.421.62 пВп "A" STAGE + 2 SRMS 1.60 "A" MAIN 2.37"B" MOD. I.S. + SINGLE STAGE "B" 2.47 1.57 "A" MAIN SINGLE STAGE ORBIT 2.05"A" 1.32 "B" TO**ل** 9 ß 4 က 2 ---COSTS - DOLLARS IN BILLIONS

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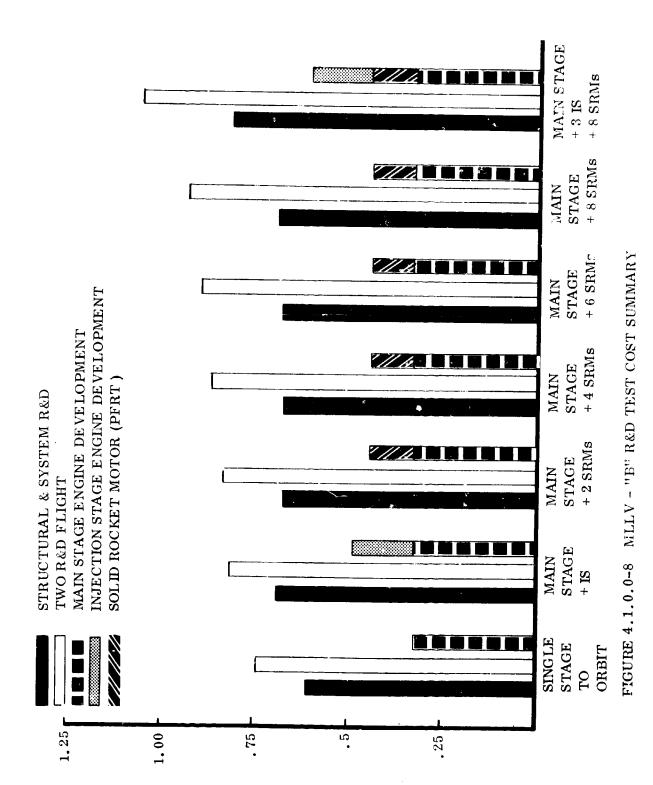
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FIGURE 4.1.0.0-7 AMLLV NON-RECURRING COST SUMMARY



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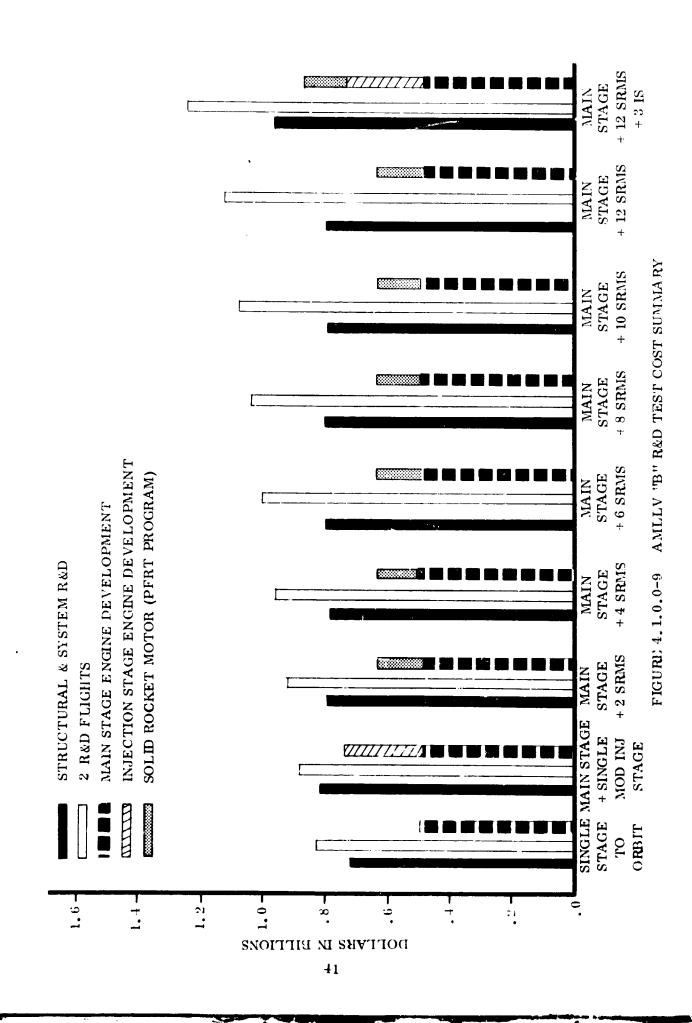
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These figures show that the non-recurring cost for implementation of the injection stage are basically the same as for the solid rocket motor stages. They further show that the non-recurring costs will be relatively insensitive to the number of injection stage modules and/or the number of SRM stages to be used for the vehicle configurations.

The costs for flight test portion of the development test program will exceed the development test costs for either structures and systems or the propulsion systems. The flight test costs are approximately 40 to 50 percent higher than the test costs for structures and systems development and 100 to 160 percent higher than the costs for propulsion system development. The development test costs for the structures and systems exceeds the development test costs for the propulsion systems by approximately 50 percent for the single-stage-to-orbit configuration and by 30 to 50 percent for the other configuration.

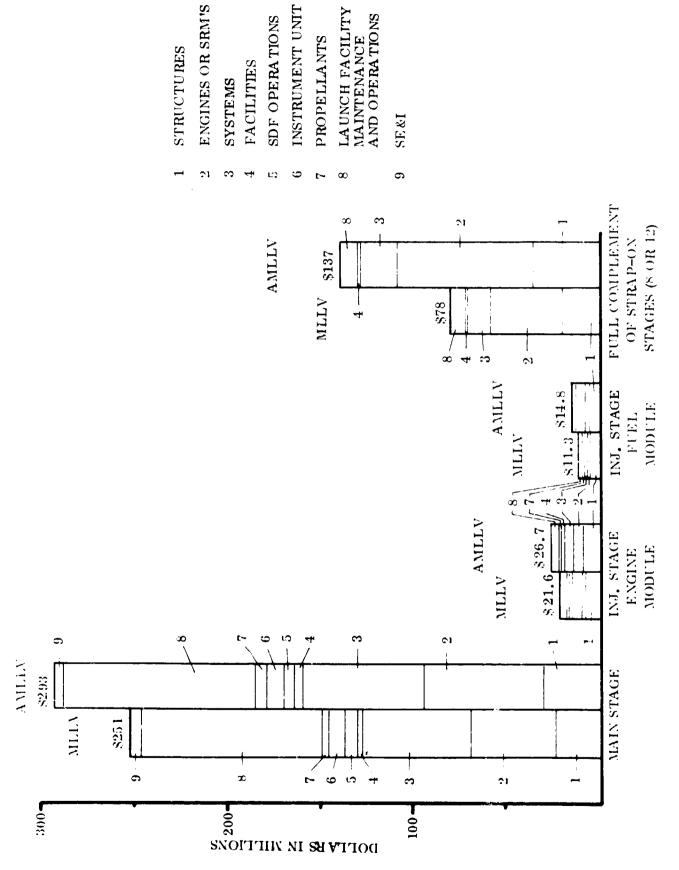
Another approach (not shown) would assume that all program support elements will be sized for the maximum configuration and that all other configurations can be produced and launched for various mixes of launch vehicle within a program. The two R&D flight vehicles are of the maximum payload configuration.

For this approach which would assume that capability for launching the maximum configuration must be maintained, the "A" and "B" costs will be constant for all configurations and the same as those shown for the maximum configuration in the afcrementioned figures.

"C" costs by program element for the first units of both vehicle families are shown in Figure 4.1.0.0-10. (To use these data in development of a total program cost, that requires multiple launches, appropriate learning curves must be used for obtaining the overall program operational costs.)

The above referenced figures also show the relationship of the cost distributions to vehicle size. From these data the following cost/size/phase relationships were determined.

		Phases	
	Α	В	С
MLLV Main Stage AMLLV Main Stage	. 832	. 817	. 855
MLLV Injection Stage Engine Module AMLLV Injection Stage Engine Module	. 799	. 737	. 799
MLLV Injection Stage Fuel Module AMLLV Injection Stage Fuel Module	1.000	.772	. 742



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FIGURE 4.1.0.0-10 STAGE ELEMENT COST DISTRIBUTION FOR FIRST OPERATIONAL UNIT (3RD FLIGHT UNIT) "C" COST

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4.1	(Continued)		PHASES	5
	MLLV Three Module Injection Stage	А	В	С
	AMLLV Three Module Injection Stage	. 799	.730	.779
	MLLV Strap-On Stage AMLLV Strap-On Stage	. 868	. 693	. 844
	MLLV Full Complement of Strap-on Stag AMLLV Full Complement of Strap-on Sta	<u>es</u> ges. 817	. 692	. 565

NOTE:

All of the above relationships relate to a 50% size reduction except for that of the individual strap-on stage which relates to a 23% size reduction.

As these numbers indicate, a 50 percent reduction in the main stage size will result in only a 15 percent reduction in the main stage recurring costs while a 50 percent reduction in the injection stage size will result in approximately a 20 percent reduction in injection stage recurring cost and a 23 percent size reduction for an individual strap-on stage will result in a 16 percent reduction in cost (a 55%) cost reduction for a 50 percent size reduction). The basis for this anomaly (as stated above) is that the main stage, as a primary vehicle stage, must absorb a significant portion of the fixed non-size sensitive cost associated with facility, maintenance and operations. The cost of the full complement of strap-on stages for the half size vehicle will be only 60 percent that for the full size vehicle. This significant reduction in strap-on stage costs is due to the combination of: (1) the effects of size reduction of the individual stages and (2) the reduction in number of required strap-on stages from 12 to 8.

Figure 4.1.0.0-11 through 4.1.0.0-13 show the distribution of costs by cost categories by stage by program phase. The distribution of costs to the cost categories was accomplished by reviewing each individual entry in the back-up detailed cost sheets in the AMLLV and MLLV baseline costs contained in Volumes IV and V, respectively. Assignment of a specific cost entry to a given cost category was based on an individual judgement of each entry. Some of these assignments required arbitrary assumptions which would effect the total distributions shown. For example, manpower and vehicle material as shown, relate only to that manpower and vehicle material to be expended to design, test, build and operate the vehicle. Manpower required in support of the other categories, i.e., tooling, material, facilities and equipment is included in the cost of those items as applicable. For example, manpower for tool design is shown as a tooling cost. Similarly, material required for tooling is shown as a tooling cost. Material costs as assigned to the vehicle material category reflect all costs for purchases material (inclusive of purchased assemblies and subsystems) to be used to design, test, manufacture and operate the vehicle. SRM and liquid engines for this distribution were not considered purchased

4.1 (Continued)

assemblies (vehicle material) but were further broken down into the manpower, material, tooling, fabrication and equipment by categories. All systems and subsystems, on the other hand, were classified as vehicle material exclusively.

The distribution of Phase A costs by cost category as shown in Figure 4.1.0.0-11, indicates that a significant portion of the "Get Ready" costs will be attributable to Facilities and Equipment. The next largest cost category will be tooling. Of the cost categories shown, the tooling costs appear to be the most sensitive to vehicle size. Tooling costs will be reduced by 28 percent as the vehicle size is reduced by 50 percent while the total A costs will be reduced by only approximately 17% for a similar size reduction. The costs for vehicle material will be negligible. Program management and engineering design costs will represent approximately only 1.2 percent and 5.0 percent respectively of the total Phase A costs.

The ratio of MLLV costs to AMLLV costs for the main stage, for the three module injection stage, and the full complement of strap-on stages will vary between 80 and 83.5 percent. This is indicative of the fact that the major cost elements are relatively independent of size. Only a slight difference in the costs for equipment and the facilities, tooling, and material will occur between the MLLV and the AMLLV sizes. The manpower requirements will be essentially the same regardless of the size.

Figure 4.1.0.0-12 illustrates the distribution of costs by categories for Phase B. These costs include not only the costs for conducting the test, but also the costs. required to provide the test specimens. The development test costs for the MLLV single-stage-to-orbit will be 81.5 percent those of the AMLLV. Similar comparisons of the development test costs of the MLLV and AMLLV three module injection stages and full complements of strap-on stages showed the ratios will be 74.1 and 69.2 percent, respectively. For all stages of the vehicle, the tooling and facilities equipment costs will be essentially identical regardless of the size. A relatively significant increase will occur for material costs for the larger vehicle. The major difference in MLLV and AMLLV SRM stage costs can be attributed almost entirely to the increased propellant that will be required in each test SRM. The manpower costs which represent the major portion (70°) of the liquid stage B costs will increase only slightly as the size goes up. This is the effect of increased manpower requirements for manufacturing operations, test and quality and reliability assurance. As most of the SRM stage test components will be purchased, material costs for the SRM exceed the manpower costs. The management and administration and the vehicle engineering are essentially the same.

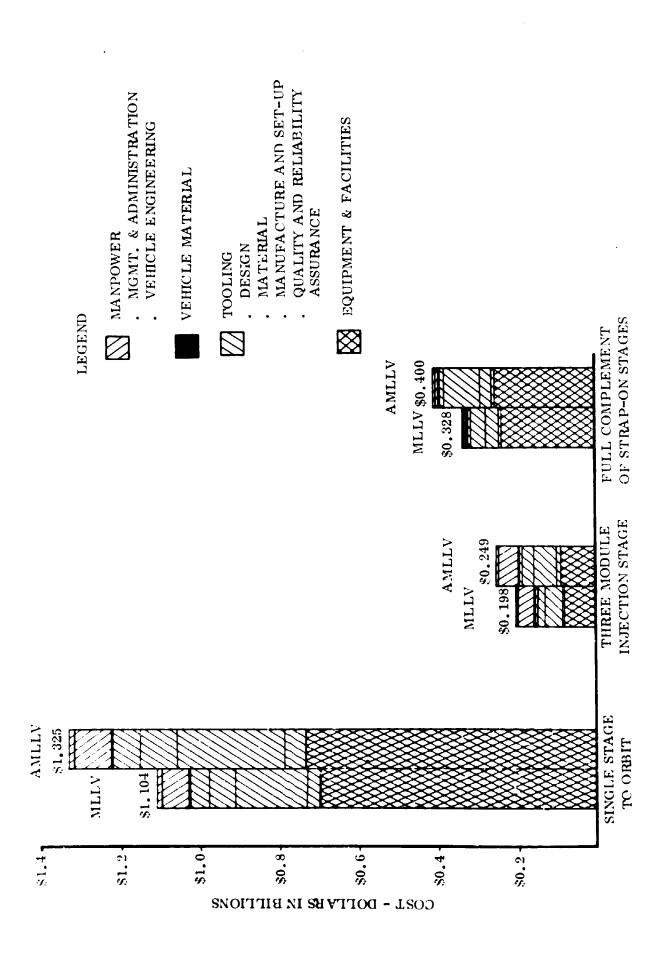


FIGURE 4.1.0.0-11 DISTRIBUTION OF COST BY COST CATEGORY FOR PHASE A

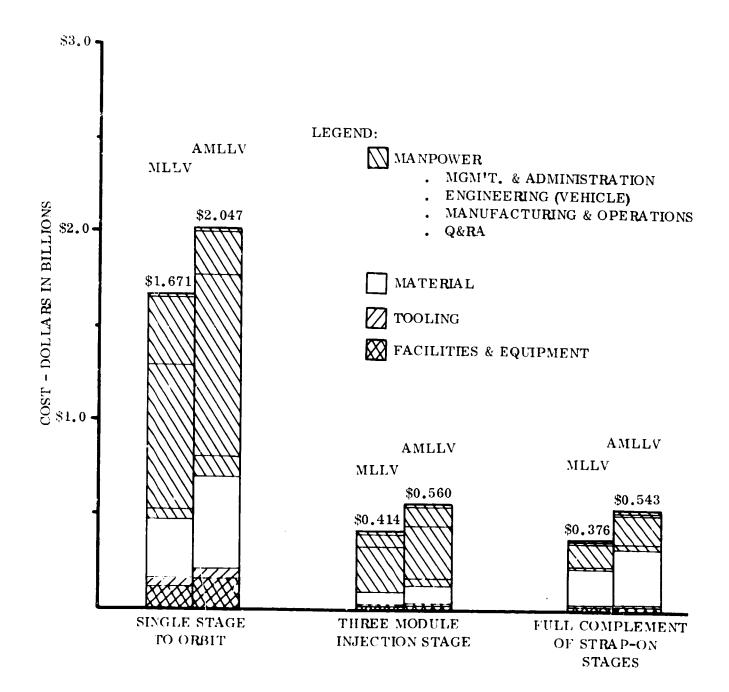
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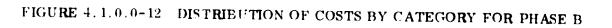
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4.1 (Continued)

Figure 4.1.0.0-13 shows the distribution of costs by category for the first operational unit (C cost). The costs of the MLLV stages as ratioed to those of the AMLLV stages will be 86.5 percent, 77.8 percent, and 87.2 percent for the single-stage-to-orbit (main stage), three module injection stage, and full complement of strap-on stages, respectively. As was observed for the costs for Phase B, the facility, tooling and equipment will be essentially the same regardless of size. The material costs will be relatively higher for the AMLLV single-stage-to-orbit vehicles and for the AMLLV full complement of strap-on stages. For the single-stage-to-orbit vehicle, this will be a direct effect of the size increase. For the strap-on stages, it will be principally due to the twelve SRM's for the AMLLV versus the 8 SRM's for the MLLV as well as the increased propellant loading for the AMLLV SRM's of approximately 1,000,000 pounds each. The material costs for the three module injection stage will not be significantly affected by size. The costs for manpower will represent by far the majority of the liquid stage production and launch costs. Manpower costs will be a smaller percentage of SRM stage costs because of the high percentage of purchased propellant materials and stage components. The differences in costs for manpower between each of the MLLV and AMLLV stages will be principally due to the manufacturing and operations test and quality and reliability assurance. The management and administration and vehicle engineering manpower will be essentially the same regardless of vehicle size.

Figure 4.1.0.0-14 and 15 illustrate the AMLLV and MLLV main stage production and launch cost distributions compared to the Saturn V cost distributions. Figure 4.1.0.0-14 shows that the main stage manufacturing cost distributions by cost categories of the AMLLV and the MLLV will be similarly comparable to those of the S-IC stage of the Saturn V.

As shown in Figure 4.1.0.0-15, the costs distributions by cost elements will be generally comparable except for the engine cost. For the MLLV and AMLLV, the engine costs will be a significantly larger percentage of vehicle costs than will the engine costs for the Saturn V. This can be attributed principally to the number of engines involved. For the MLLV and the AMLLV twenty-four engines will be used per main stage whereas, for the two stage Saturn V a total of ten engines are utilized.

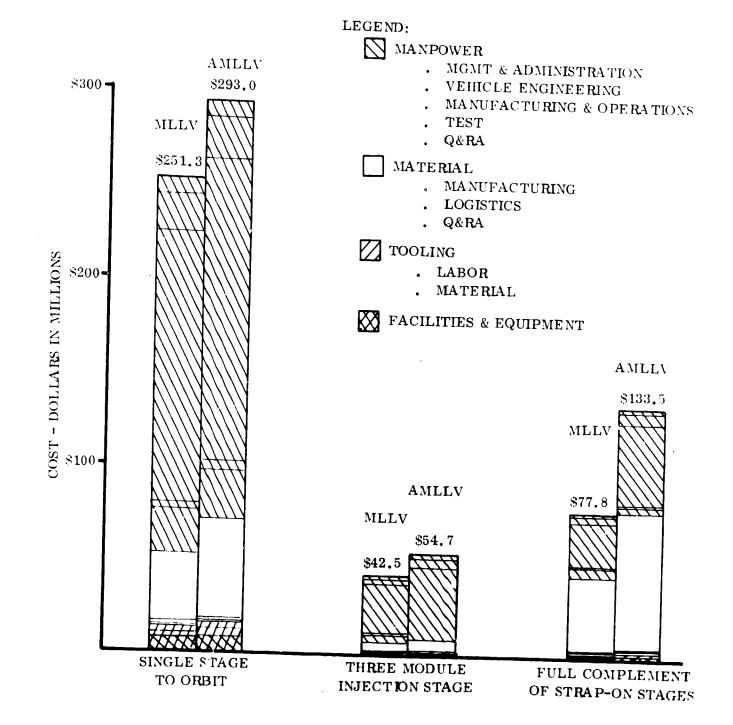
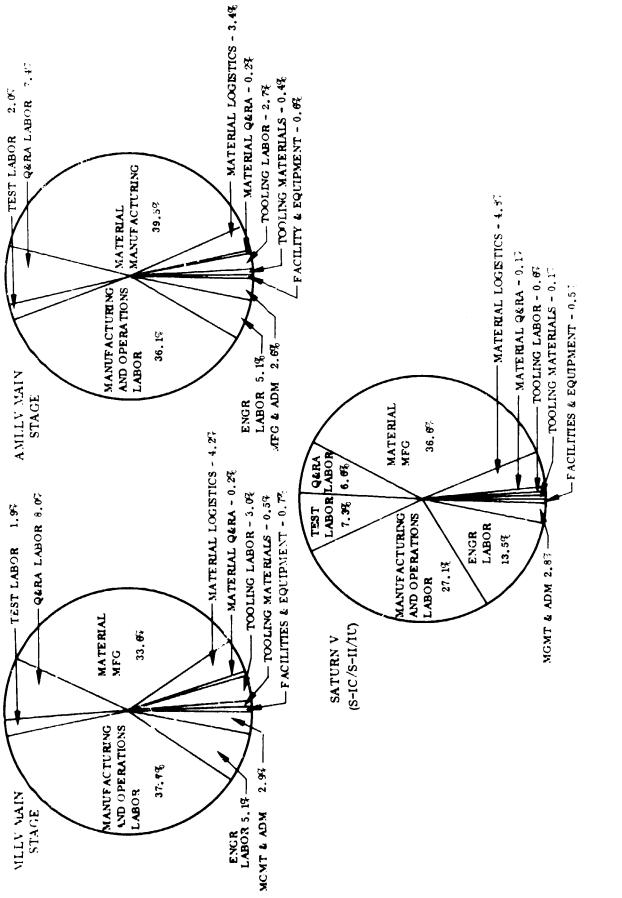


FIGURE 4, 1.0.0-13 DISTRIBUTION OF COSTS BY CATEGORY FOR FIRST OPERATIONAL UNIT (3RD FLIGHT UNIT)



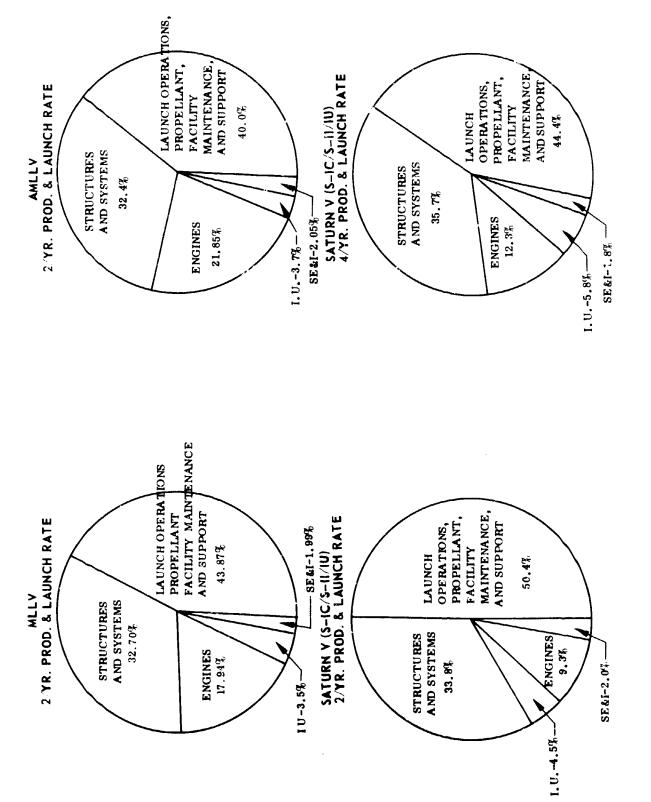


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FIGURE 4.1.0.0-15 AMLLV AND MLLV MAIN STAGE PRODUCTION AND LAUNCH COSTS ("C" COSTS) COST ELEMEN'TS COMPARED TO SATURN V COST ELEMENTS

4.2 LEARNING CURVE EFFECTS ON RECURRING COSTS FOR PRODUCTION AND LAUNCH

The preceding data show only recurring costs for the first flight stages. To evaluate overall program costs, (as required for cost effectiveness analyses of program, configuration and technology alternatives) it is necessary that recurring cost be computed for varying production quantities of the individual stages. To accomplish these computations, learning curve effects on the cost of the various stages and stage elements must be applied. For the purpose of applying the learning curve data, the first stage produced for flight (the first R&D flight test) was considered as the number one unit.

The first unit costs and learning curve values shown on Table 4.2.0.0-I were defined for the various stage and stage elements. (See Book C of Volumes IV or V.)

As shown in Table 4.2.0.0-I, two learning curve rates were utilized in determining the cost of the variable cost AMLLV/MLLV components. These learning rates were: 1) 91% for the main stage structure, injection stage engine module, injection stage fuel module, and delta cost for the heavy weight alternate forward skirt and 2) 95% for the main stage engine, injection stage engine and solid propellant motors.

For reference, improvement curve (learning rate) tables are provided in Tables 4.2.0.0-II through 4.2.0.0-V. Tables 4.2.0.0-II and 4.2.0.0-III show the unit progressive curves for the 91% and 95% learning curves, respectively. Tables 4.2.0.0-IV and 4.2.0.0-V show the cumulative progressive curves for 91% and 95% learning curves, respectively. An application of each type of these curves are shown below.

<u>Unit Progressive Curve Application</u> - The first unit cost of the AMLLV main stage learning curve sensitive elements (exclusive of engines) are 118 million dollars. To determine the costs of these elements for the sixth unit, the 91% unit progressive curve tables are used. The first unit costs of 118 million dollars are multiplied by the factor .78365300. This product is equal to 92.47 million dollars. If the costs of the sixth unit are known, i.e., 92.47 million dollars, the costs of the first unit may be obtained by dividing the sixth unit factor from the unit progressive curve table, i.e., 92.47 divided by .78365300 equals 118 million dollars.

<u>Cumulative Progressive Curve Application</u> - If it is desired to obtain the cumulative costs of the first six units, the cumulative progressive tables must be utilized. For example: the first unit costs of the AMLLV SRM stage learning curve sensitive elements are 13.05 million dollars. The SRM stage learning curve sensitive elements costs are on a 95% learning curve. If it is desired to determine the cumulative costs of these elements for the first six units, the first unit costs of 13.05 million dollars are multiplied by the cumulative progressive table factor for the sixth unit, 5.537962. The product is equal to 72.27 million dollars. If the total costs of the six units are

	ELEMENTS	IND ARS IN	(DOLLARS IN THOUSANDS)		
	AM	WITTON ATTIME	W	MLLV	
	IST R&D 16 FLIGHT	1st OPERATIONAL FLIGHT	IST R&D IS FLIGHT	1st OPERATIONAL FLIGHT	LEAKNING CURVE
MAIN STAGE - VARIABLE COSTS	(118,000)	(101,616)	(95,000)	(81,810)	
Structures Systems Facility and Transportation	34, 383 77, 884 4, 380 865	29,609 67,070 3,772 745	23,464 67,115 3,972 865	20,206 57,797 3,421 745	91% Composite
MAIN STAGE - FIXED COSTS	(238,500)	(130,000)	(226,000)	(125,000)	
	6,573 9,346 6,169	6,573 9,346 6,169	3,287 9,346 6,169	3,287 9,346 6,169	
	ļ	94_164	I	88,506	100 %
	8.750	8.750	8,750	8,750	
	5,301	5,301	5,301	5,301	
	202,361	١	193,147	1	
MAIN STAGE – ENGINE COSTS					
	(71,100)	(66,065)	(50,800)	(47,203)	
	I	1	(32,800)	(30,477)	ENGINE
	I	1	(32,200)	(21,557)	ALTERNATIVES
	(65,900) (76,000)	(61,234) (70,618)	(23,500)	(21,836)	90.6
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TABLE 4.2.0.0-I LEARNING CURVE AND ASSOCIATED COSTS FOR AMLLV/MLLV ELEMENTS

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TABLE 4.2.0.0-I LEARNING CURVE AND ASSOCIATED COSTS FOR AMLLV/MLLV ELEMENTS (Continued)

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E	ELEMENTS (Continued)	itinued)		(DOLLARS IN THOUSANDS)	OUSANDS)
	AM		Z	(LLV 1st OPERATIONAL	LEARNING
PROGRAM ELEMENTS	FLIGHT	FLIGHT	FLIGHT	FLIGHT	CURVE
ENGINE MODULE - V ARIABLE COSTS	(20,400)	(17,826)	(16,700)	(14, 381)	
Structures Systems	11,073 7,873	9,536 6,780 1,202	7,881 7,485 1 310	6, 787 6, 446 1 128	91%
Faculty and Transp. Engine Installation	083 83	59 59	68 68	29	
ENGINE MODULE - ENGINE COSTS	(3,800)	(3,530)	(2,700)	(2,509)	95 %
ENGINE MODULE - FIXED COSTS	(17,400)	(5,800)	(16,600)	(4,700)	
Propellant	730	730	365	365	
Uperational Venture Launch Operations	I	5,044	I	4,311	100 %
neur Launch Operations Delta SE &I, Inst.	16,670	١	16,238	١	
FUEL MODULE - VARIABLE COSTS	(009 * 6)	(8,267)	(7,100)	(6,114)	
Structures Systems Engine Installation	7,000 2,575 67	6,028 2,217 58	4,618 2,411 67	3,977 2,076 58	91% Composite
FUEL MODULE - ENGINE COSTS	(3,600)	(3,345)	(2,500)	(2,323)	95 %
FUEL MODULE - FIXED COSTS	(6,000)	(3,300)	(4,900)	(2,700)	
Fropellant	730	730	265	365	
Operational Venicle Launch Operations	ł	3,523	i	2,374	> 100 [°]
R&D Launch Operations Delta SE&I, Inst.	5,270	t	4,535	۲	

TABLE 4.2.0.0-I LEARNING CURVE AND ASSOCIATED COSTS FOR AMLLV/MLLV ELEMENTS (Continued)

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(DOLLARS IN THOUSANDS)

		NI MINITION			
	A	AMLLV	N	MLLV	
PROGRAM ELEMENT	1st R&D 1s FLIGHT	lst OPERATIONAL FLIGHT	lst R&D ls FLIGHT	lst OPERATIONAL FLIGHT	LEARTING CURVE
ALTERNATE FWD SKIRT COSTS	(4,600)	(3,961)	(2,900)	(2,497)	91 ⁽⁷
SRM STAGE - FIXED COSTS	(27,400)	(7, 900)	(20, 600)	(6,500)	
Launch Maintenance	1,150	1, 150	1, 150	1, 160	
Operational Vehicle Launch Operations	I	6,725	1	5,305	> 100%
R&D Launch Operations Delta SE&I, Inst.	26,250	١	18,450	i	
SRM STAGE - VARLABLE COSTS	(136, 663)*	(128,844)*	(78,087)**	(72,558)**	·
Structures SRM Motors Facility Maintenance Other Stage Hardware	38,183 82,070 1,104 17,306	35,479 76,257 1,026 16,081	21, 218 94, 308 733 11, 828	19, 716 87, 623 681 10, 990	95% Composite
	*Block of 12 SRM's	*Block of 12 SRM's	**Block of 8 SRM's	**Block of 8 SRM's	

4.2 (Continued)

known, i.e., 72.27 million dollars, that number divided by the above factor (5.537962) will give the first unit costs of 13.05 million dollars.

To aid in application of the learning curve effects to the cost analyses, the MLLV data was tabulated as shown in Tables 4.2.0.0-VI through 4.2.0.0-XII. Similar data for the AMLLV is shown in Tables 4.2.0.0-XIII through 4.2.0.0-XVIII. (NOTE: These cost data apply <u>only</u> to a production and launch rate of two per year.)

Examples showing the use of these tables are provided in the following Section 4.3.

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR.

TABLE 4.2.0.0-II91% UNIT PROGRESSIVE CURVE TABLE

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	0 916	UN IT	PROGRESS CLIVIA	E TABLE	918 4		915 3	1 MU	PROGRESS CURV	E TABLE	
1 2 3	.73103500 .64524200 .62953600 .60537000	1+00000000 +72161700 +66084100 +62673400 +60334000	+91000000 +71312400 +65867100 +62403200 +60136500	.84115700 .70539900 .65271100 .62142500 .59844300	+82810000 +84832300 +8484300 +81890600 -59757100	1 2 3	. 80333600 . 60179006 . 64534600 . 61647000 . 59574600	.76365300 .64575000 .64191400 .61411100 .59396700	•76736700 •68011600 •63862800 •61182800 •59223200	+75357100 +67484+00 +83547300 +80981000 +59053800	•74154100 •64497.00 •63244700 •63244700 •60745900 •30765900 •56665300
5 6 7 8	\$58726700 \$57287800 \$56098700 \$55088700 \$56088700	.58568700 .57159100 .53990600 .54995700 .54131500	+58+14100 +57332800 +55884100 +54803200 +54051000	•58262900 •56908700 •55779300 •54813500 •53971600	-58114900 -56786900 -55676200 -55676200 -55676200 -55693100	5 6 7 8	- 5 7970000 - 5666 7300 - 55574600 - 54686200 - 53813600	.57828100 .56549700 .55474500 .54548300 .58738900	. 57889000 556334,00 553375900 554483600 53663200	+57552400 +56320400 +55278800 +55278800 +54578900 +53588400	+57414400 5 +56208700 6 +55183100 7 +54295400 8 +5351+600 9
10 11 12 13 14	•53041300 •52752700 •52131900 •51567200 •51547200	.53369000 .52687800 .52073000 .51513500 .51000400	+53207500 +52623606 +52014800 +5204800 +51460200 +50951400	.53228800 .52560080 .51857000 .51857000 .51807400 .50902800	+53154900 +52407000 +5180800 +51355000 +50854800	10 11 12 13 14	+53087700 +52434600 +51843106 +51383106 +50806700	+53019300 +52372000 +51766906 +51251600 +50756200	+52951600 -52314800 +51731300 +51200500 +50712100	+5288+600 +52251200 +51676100 +511+9900 +50465300	.52818300 10 .52191500 11 .91821+00 12 .51999700 13 .50818900 14
15 16 17 18 19	50572900 50130700 40718900 40333800 48872200	. 50527200 . 50088200 . 40578500 . 49286600 . 4837200	• 50 + 61 800 • 500 + 61 90 • + 65 39900 • + 62 59600 • + 6902 + 00	. 504 348 00 . 500042 00 . 45600 700 . 492 228 00 . 4864 78 00	.90902100 .40902600 .40961800 .4093800 .4093800	15 16 17 18 19	.50347800 .49523200 .49523200 .49523200 .49150260 .48799400	.50303700 .40880300 .49884880 .49114100 .48763400	+ 50260000 + 6839500 + 69446700 + 69078300 + 68731700	+90216600 +99799000 +99608800 +99642700 +8898100	+50173500 15 +49758800 14 +49371200 17 +49007300 18 +4864730 19
20 21 22 23 24	.48631600 .48309800 .48005000 .47715500 .4740000	+45596600 +4278600 +47975400 +4787400 +47815200	.46545800 .4247500 .47945900 .47386500 .47386500	.48533200 .48216700 .47816600 .47631500 .47539900	. 48500700 . 48185900 . 47887400 . 4783700 . 4733400	20 21 22 23 24			+4404500 +48094800 +47800800 +47521300 +47254800	+ n8372700 + n8066700 + n7772300 + u7466100 + n7228800	.48341.00 20 .48034700 21 .47741600 22 .47741600 22 .47747000 23 .47203000 24
25 26 27 28 29	+7177200 +66926200 +6685400 +6685400 +6635400 +66234100	.47151600 .46901700 .46432800 .46432800 .46212400	. 47126100 . 46877300 . 46638900 . 46638900 . 46190900	+47100700 +4853000 +4615700 +4615700 +46388100 +4169400	. 47075500 . 468 28800 . 46592500 . 46395500 . 46365800	25 26 27 28 29	+47050300 +46804780 +45599400 +4343600 +4126700	• •7(25300 • • •70700 • • •5•6•00 • • •521500 • • •105=00	. + 7000300 + + 756800 - + 6523500 - + 6289600 - + 608+300	++6975500 +46733100 +46500700 +46277600 +46063200	
10 31 32 33	++++++++++++++++++++++++++++++++++++++	• + 6000500 • + 5796400 • + 5599600 • + 5409700 • + 5226100	.45979700 .45776-00 .45580300 .45391000 .45208100	•45959100 •45756500 •45561100 •45372500 •45190200	.45938500 .45736600 .45541900 .45545900 .45172300	30 31 32 33 34	.45917600 .45716600 .45522800 .45335500 .45154400	.45897500 .45697100 .45503800 .4531/100 .45136700	++5+77100 ++5+8+800 ++5+8+800 ++5118900	+ + 5856800 + + 5657900 + + 546000 + + 5280500 + + 5101300	.45836000-30 .45638400-31 .65547100 32 .45262400 33 .65083700 36
35 30 37 38 39	.45060100 .46793700 .46726700 .46566700 .44607400	. 650 48600 . 44876800 . 66710200 . 46548700 . 46392000	. 450 31 200 . 468 59900 . 468 93900 . 46 53 2900 . 46 376 500	+4013800 +44843000 +4677500 +46517000 +44361200	. 44 996500 . 44626300 . 44661300 . 44561200 . 44345800	35 36 37 38 39		. ++962000 . ++792900 . ++628900 . ++628900 . ++315300	.44944900 .44776200 .44612800 .44654100 .44554100	.44927800 .44759700 .44596700 .44596700 .44284900	
•0 •1 •2 •3	.4425=100 .4425=100 .43401400 .442400 .442400 .4401400	+4+239700 +4+091700 +4447700 +43807500 ++3671000	+4224700 +44077100 +43933500 +4393700 +43657600	++209800 ++062600 ++3919400 ++3780000 +436++200	• 44 194900 • 440 48 100 • 43905 300 • 437662 00 • 436 308 00 • 43498800	40 \ 41 43 43	+44180000 +44033600 +43891200 +43617400	+44165200 +44019200 +43877200 +43778990 +43604100	++150+00 ++400+800 ++3863200 ++3725200 ++3590800	+ 64135 300 + 63440300 + 63844200 + 63711600 + 6377600	• • • 12.00 • 6 • • 3976206 • 1 • • 363500 • 2 • • 3648100 • 3 • • 3564600 • •
45 47 47		•44538000 •45408300 •45281700 •45281700 •45158200 •€-,32500	+++324+00 +++344500 +++344200 +++344000 ++4024600	+ 3511800 + 3342700 + 3256800 + 3133800 + 3013700	4370000 43264400 43121700 43001900	45 46 47 48 49	+43485700 +43357300 +45232000 +43109600 +42990000	+43+72800 +4334+600 +43219600 +43097500 +43097500	643454800 643332000 643207300 643285500 642966300	**3**6400 **3314*30 **319*400 **3073*00 **3073*00	μα3φ3τμητια κά330,0πμΩ° 40 φά31927.05 47 κά30,0140,05 46 φά20μά30,0° 49
	41 % 0	1	TT PROGRESS CU	HVE TAPLE	915		91 % 5	UN 6	IT PROGRESS CU	RVE TAHLE B	
50 51 52 53	• 42931300 • 42815800 • 42702800 • 42592300 • 42454100	+ 291-600 + 2804400 + 2691600 + 2581300 + 2473400	+ 2 y0 8000 + 2 7 9 300 0 + 2 6 80 500 + 2 5 7 0 500 + 2 4 6 2 7 00	• • 2896 • 00 • • 278 1600 • • 266 94 00 • • 255 96 00 • • 245 2100	+ 42 88 4800 + 42 770300 + 42656300 + 426563700 + 42641400	50 51 52 53 54	+2073200 +2759000 +2247200 +2237900 +2230800	+2861700 +62747700 +2636200 +2527100 +62420300	+2850200 +2736400 +2825200 +2516300 +2409700	• 42838700 • 4272500 • 42614200 • 42505500 • 42399200	6474 (68282600 - 1 682802 () 1 882802802 () 68238480 () 56
55 56 57 58 59	. 42378200 . 42274400 . 42172700 . 42073000 . 41975300	•42367700 •42264100 •42162600 •42063200 •41965600	++2357200 ++2253900 ++2152600 ++2053300 ++1956000	++23+6800 ++22+3700 ++21+2600 ++20+3500 ++19+6300	++ 2336400 ++2233500 +2132600 +42033700 +41936700	55 56 57 58 59	•42326000 •42223300 •42122600 •42023900 •41927100	+42315600 +42213100 +42112700 +42014100 +41917500	+42305300 +42203000 +42102700 +42004400 +41908000	.42295000 .42192400 .42092800 .41994700 .41994700	•422347
60 61 62 63 64	.41874400 .41785300 .41693000 .41602300 .41513300	.41869900 .41776000 .41683800 .41593300 .41593300	.41860400 .41766700 .41674700 .41584400 .41495600	.41851900 .41757400 .41665600 .41575400 .41686900	+41841600 +41748200 +41656500 +41566500 +41478100	60 61 62 63 64	.41832100 .417,8900 .41647400 .41557600 .41469300	.41822700 .41720700 .41530400 .41540700 .41540700 .41460600	+1813400 +1720500 +1629300 +1539800 +1451900	+4160+000 +41711300 +41620300 +41630900 +41643100	.417443(0 80 .41702100 81 .4161(1 0 52 .41522100 83 .41434530 84
85 66 67 68 69	.41425800 .41339800 .41255300 .41172200 .41090500	.41417100 .41331300 .41246900 .41164000 .41082400	+1408500 +1322800 +1238600 +1155800 +1155800	.41399800 .41314300 .41230200 .41147600 .41066300	++1391200 ++1305800 ++1221900 ++1139400 ++1058200	45 67 68	++1582600 ++1297400 ++1213400 ++1131200 ++1050200	+41374000 +41288900 +41205300 +41123100 +41042200	+1365400 +1280500 +1197000 +1114900 +1034100	+1358900 +1272100 +41188700 +41108800 +41028100	.4134A300 65 .41263700 66 .41180500 67 .41098600 68 .41018100 69
70 71 72 73 74	.41010200 .40931100 .40853300 .40776700 .40701300		+0915400 +40915400 +40837800 +40761500 +40686300	.+0986300 .+0907600 .+0830200 .+0753900 .+0678900	• 40 9784 00 • 40 8998 00 • 40 82 25 00 • 40 82 25 00 • 40 67 14 00	70 71 72 73 74	+0970500 +0892000 +081+800 +0738800 +0864000	+40962600 +40864300 +40807200 +40731300 +40856600	+40954700 +40876500 +40799500 +40723800 +40723800	. 40946800 . 45 465 700 . 40791900 . 40716300 . 4094 \ 800	+40 434900 70 +40861060 71 +40 784300 72 +40 704300 73 +40834-00 7-
75 76 77 78 79	++0627000 ++0553400 ++0481800 ++0410800 ++0340800	.40619600 .40546600 .40474600 .40403700 .40333800	+40 \$12300 +40 539300 +40 48 7500 +40 396 700 +40 326900	+40604900 +40532100 +40460400 +40389700 +40320000	• +0597600 • +0524900 • +053300 • +0382700 • +0313100	75 76 77 78 70	+0540300 +40517700 +40446100 +40375700 +40306200	++0583000 ++0510500 ++0439000 ++0368700 ++0299300	++0 \$7 5700 ++0 50 3300 ++0 432000 ++0 36 1700 ++0 292+50	+40568400 +40496100 +40424980 +40354700 +40285500	+40561163 75 +40486900 76 +50417400 77 +40347790 78 +40278700 79
80 81 82 83	++0271800 ++0203800 ++0136700 ++0070600 ++0005300	+0265000 +40197000 +40190100 +0064000 -39998900	+40258100 +40190300 +40123400 +40057500 +39992400	+40251300 +40183600 +40116800 +40050900 +39985900	.60264500 .60176900 .60110200 .60044600 .39979500	80 61 63 63 64	+40237700 +40170100 +4013500 +40037900 +30973100	+40237900 +40163400 +6096900 +60031300 +39966600	+ 40 22 4 100 + 40 156 700 + 400 90 300 + 400 2 4800 + 39960 200	+40217300 +40150190 +40083700 +40018300 +39953800	+40210FC3 H0 +40143+00 A1 +400/7207 A2 +40011800 A3 +39947+70 A4
85 84 87 88 89	- 39941000 - 34877500 - 34814800 - 39752400 - 34891400	+ 39934600 + 39871200 + 39808600 - 39746800 + 39685800	• 39928200 • 39864900 • 39802400 • 39740700 • 39679700	+ 39821800 + 39858600 + 39796100 + 39734500 + 39873700	• 39915500 • 39852300 • 39790000 • 39728400 • 39667600	85 86 87 88 89	.30000100 .30844000 .50783400 .30723300 .30722300	• 3990 2800 • 398 39800 • 397 7600 • 397 14200 • 396 5400	.39896400 .39833500 .38771400 .39710108 .39649600	+ 39890100 + 39827300 + 39785200 + 39704000 + 3964 3600	.398838455 .39821040 88 .39754108 88 .39697900 88 .39697900 89
40 91 92 43	• 396 31600 • 395 72000 • 395 13200 • 39455100 • 39397800	• 39625600 • 19566100 • 19507400 • 39449400 • 39392100	+ 39619600 + 39560200 + 39501500 + 39643600 + 39386+00	• 30013600 • 30554300 • 30605700 • 30605700 • 30637000 • 30360700	+ 3960 77 80 + 39548+00 + 39489900 + 394371 80 + 39375600	60 91 92 93	- 30601700 - 39542500 - 39464100 - 39426400 - 39369300	•39595780 •39534780 •9478300 •3420600 •39363700	+ 39589800 + 39530800 + 39472500 + 39414900 + 39359000	• 3958 3900 • 3952 4900 • 39466 700 • 39466 700 • 39469 700 • 3952 400	.36577600 40 .36114100 91 .39660-00 92 .3960 500 93 .38366700 95
95 96 97 98 99	. 39341100 . 39285100 . 39229700 . 39175000 . 39120400	• 39335500 • 39278500 • 39224200 • 39189600 • 39119600	.34329800 .39273900 .39218700 .39184100 .39184100	+ 34324200 + 34264400 + 34213200 + 34154700 + 34154700 + 34104800	.39318600 .39282900 .39207800 .39153300 .39099500	87 87 88 88	.30313000 .30257300 .50202300 .30147800 .30094100	+ 3930 7400 + 3925 1400 + 39194800 + 39142500 + 39088800	+ 3430 1400 + 34246300 + 34141400 + 34137100 + 34083500	+30200200 +30240706 +30165000 +30131700 +30076100	+39290602 95 +39235200 96 +39180700 97 +39126100 96 +39072800 99

TABLE 4.2.0.0-III 95% UNIT PROGRESSIVE CURVE TABLE

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	1° 3	JNJT	рыракыса сонаң	Abut	454		47 8	NIT.	PROGRESS HV	° ≜∺_ s	471 7
	•44334443 •4714834 •1748530		- 95 3001130 - n3203/00 - 14559630 - 14559630	.42141400 .42111400 .14242-00 .17202000 .17202000	+02+000 +822+4500 +190+3000 +1103+100 +75515400	i.	- MB\$1,000 - 3.840001 - 7840001 - 784000 - 76401 - 76401405		10 ASH44), 4-10 AF JU 4-10 AF JU 4-ASA1-JU 4-ASA1-JU 4-754-754,00	++5737500 +26763430 +78166500 +7841030 +7841030 +7534,900	-869935.0° -866424000 - -779639 20 0 -7629363 -7629363
6,7	***** *744644-30 *73401-30 *73021300 *72405100	- 15471433 - 164530 - 13773860 - 12365730 - 122865730	• '5836610 • 76647600 • 73682100 • '2871300 • 7217300	.74542310 .73544400 .72746400 .72746400 .72104600 .71504100	74434200 73509200 72723700 7236700 71467600		•7453n0 •73624-00 •7265.500 •71981-00 •71391000	• •2 •47 30 • 7 5 \$ •. 500 • 7 5 \$ •. 900 • 7 5 \$ •. 900 • 7 1 \$ \$ \$ 0 \$ 00 • 00	.74142.00 .77251000 .7251000 .71857000 .71251000	.74388803 .73180130 .73180130 .7248340 .71797133 .71227630	.7345-300 5 .731011-0 6 .72572730 7 .71737100 8 .711737100 4
.0 	.714//800 .714//800 .70621470 .70168700 .54753700 .54372.30	.7164420 .7158420 .70774300 .70125000 .69116130 .69333530	-71561430 -71317000 -70527200 -7082370 -54874900 -54244400	.70965800 .70480800 .7039400 .69636000 .69263400	.70915000 .70434900 .6998000 .69597400 .69227700	10 12 13 14	.7084420 .70384400 .8445400 .84554.00 .84554.00	.7081520 .70364470 .69915200 .69952122. .69157100	.707A4090 .32299800 .8487+300 .4483530 .4483530 .44122730	.107173-0 .732554-5 .6983375 .69846-50 .69087555	- 1066-130 - 1021.507 - 1021.507 - 10 - 10
15 16 17 18	.543.2.30 .64643.00 .9838.603 .66094300 .66094300	10773500 - 58965000 - 58352600 - 68352600 - 68355600 - 6835500	+68 +5 1 3 00 -6# 62 69 30 +6# 32 3+ 30 +6# 0 3# 300 +6 7 76 95 30	.68917800 .68595700 .68294100 .680.0790 .67743500	•65884500 •68564700 •68265000 •67483300 •67717600	15 16 17 18 19	.68851000 .68533000 .68236.00 .67954000 .67691800	•66818402 •66503200 •66207300 •67928400 •67928400	.64786303 .68872700 .68170700 .67902000 .67640700	.03754300 .08442540 .08150300 .07475200 .07615=30	+68721400 15 +68812400 46 +6812400 47 +67844500 16 +67540200 14
20 21 22 23 24	67565.00 67321600 67321600 67392100 66669930 66669930	675+0200 .67297900 .67067700 .66649+000 .66639.00	167515400 167274400 167045300 66827100 156618700	.67490700 .67251000 .67273000 .54305800 .54305800	•67465200 •67227700 •6720800 •67184500 •66578200	20 21 22 23 24	.67.4, -30 .6727-500 .66978990 .66763600 .66558000	.0741"500 .07101400 .8695860 .8695860 .86742600 .68537420	+57793300 +6715+400 +64934900 +65721700 +66514000	. 67369300 . 67;35430 . 64913;00 . 66990;00 . 66998;00	.87345+10 2 .67117910 2 .664643230 23 .66474330 2- .66284410 24
25 26 27 28 29	.6645cf 20 .66266300 .66081200 .65903600 .45737630	388434900 68247100 886083100 885888200 885715900	-56419-00 -66228400 -66045100 -65868900 -65699200	.66309900 .6672320 .66723100 .6585160 .6585160	+64380600 +64191100 +66009300 +65834400 +65834400	25 26 27 28 29	.00301300 .00172030 .05991500 .05941500 .059417300 .05044300	+663+2300 +6615+210 +65974+003 +65800201 +65800201 +6563+-04	.66322400 .66135800 .65956.00 .659783200 .65616700	.66333920 .66117500 .65938500 .65938500 .65765300 .65630440	- 062/04/300 20 - 460/04/300 20 - 659921007 27 - 65746+10 28 - 65584-230 44 - 45524717 30
90 31 32 33	.65587430 - 85404000 .85255500 .85107100 .64483-00	.0555180C .05343500 .652~3500 .652~2500 .64944300	. #5535700 . #5577900 . #5225500 . #527800 . #4935300	+65519700 +65362400 +65210500 +65263500 +65263500	+ 65503700 + 65367000 + 65195600 + 65049100 + 64907200	10 31 32 33	.65487500 .65331600 .65180700 .65034700 .64843300	.6547.400 .65316300 .65165930 .65322400 .64574490	.65450.00 .65301300 .65151100 .65306130 .54865630	_6%***C**CC _6%7#%#30 _6%391*50 _6%391*50 _6%851700	- 65270700 11 - 65221700 32 - 64477620 33 - 64477620 34 - 64702600 35
35 36 37 38 39	- 0402+200 + 64684300 + 64554200 + 64554200 + 6430 + 200	. 648.3600 . 64876300 . 64945300 . 644.4430 . 644.4430	. 64 796930 . 64682700 . 64532530 . 544 33930 . 64282930	.04743300 .04544530 .64514700 .64514700 .6454700	* 8*769800 *8*536*00 *6*336200 *6*381300 *6*381300	35 36 37 36 39	. 6 4 75 % 20 . 6 4 6 2 3 300 . 6 4 8 9 4 100 . 6 4 3 6 8 6 0 . 6 4 2 4 6 6 00	064762800 066610200 066610200 066756300 066356300 066236600	.6+729300 +6+597100 +6+468800 +6+34+000 +6+322600	+64719400 +64964+00 +64950-00 +64331700 +64331700	64-71220 36 46-443521 37 46-443521 37 46-314412 38 46414721 34
40 41 42 43	+5+186#00 +6+069700 +63955-00+ +638++300 +63735730	44:7-000 +64368120 +63944300 +63833300 +61725000	.64163200 .640-6600 .63933000 .63822320 .63822320	+6+15:400 +6+035:300 +6392:630 +638:11=30 -638:31=30	- 64139600 - 64923700 - 63910700 - 63900500 - 63693100	40 42 43 44	+64127400 +64012200 +63784100 +63784100 +63784100	•A+116205 •6+0000000 •63888+000 •43778600 •6367140.	+4104900 +63464500 +43877300 +43764000 +63661300	+46042411 +53476100 +53466100 +6375721 +6365011	.433667.5
40 40 41 44	.0302/-00 .03720+00 .03427+00 .033.0100+ .032.0000	+*30+++00 +*39++20 +**15+20 +**15+20 ***5400 ******	- 63636400 - 6350600 - 6340500 - 6367200 - 63211100	-63598530 -63595300 -63395530 -63297530 -63271800	• 63548200 • 63485700 • 63385600 • 63385600 • 63192100	45 46 47 48 47	+0357/400 +03475600 +53375600 +53278100 +54282600	66374 °20 66366550 6536554°2 £6324870° €6324870° 64328320	4039970,0 663695000 663296000 6632960000 66329600000	• N3N4ANUUU • N3N4ANUUU • K3N4ANUU • M324 ++ • M324 ++	48-6456 40 46-3364 42 483-84 42 483-84 48 49-842 46
	¥58	UN	IT PROGRESS CUP	ANE TABLE	958		95 % 5	ان 6	NIT PROGRESS C	URVĘ TAHLE ð	95% 9
50 51 52 53	0 • 63130400 • 63043200 • 62452700 • 62864900	4 6 10 4 100 6 10 4 100 6 29 4 3 7 00 6 2 8 5 5 2 00 6 2 7 6 4 5 0 0	2 • 631:7000 • 63026900 • 62936800 • 62936800 • 62759900	.63107700 .63015600 .62925900 .62837700 .62751400	.63098400 .63005600 .62917000 .62829000 .62742800	50 51 52 53 54	+63089200 +62997700 +62908100 +62820300 +62734300	63079900 62948700 62894370 62811700 62775900	63070700 62479030 62440400 62440400 62603000 62717300	++++++++++++++++++++++++++++++++++++++	+63352400 50 +62961600 51 +62872400 52 +62785730 53 +62700400 54
54 55 57 58 59	.62777.00 .62641~00 .6264400 .62526400 .625460000 .62367100	+62683500 +62630100 +62536300 +62538300 +62538100	.62675100 .62510200 .62510200	.62666700 .62583630 .62502200 .62422200 .52343700	+62658300 +62575400 +62694100 +62614300 +62935900	55 56 57 58 59	.62649900 .62567200 .62485000 .52405400 .62328100	.626+1600 .62559000 .62478000 .623799500 .62320+00	.52633300 .62550900 .62473000 .62390600 .62312700	+62625000 +62542700 +62462000 +62382700 +62382700	+62616700 55 +62534620 56 +62454000 57 +62374900 58 +62297200 59
60 61 62 63	+62284500 +6221340 +6213860C +62065100	+62281900 +62205900 +62131200 +62057800 +61985600	62274200 62194300 62123800 62123800 62050500 61978500	+6226660C +62190800 +62116400 +62043200 +61971306	.62256900 .42183300 .62109000 .62036000 .81864200	60 61 62 63 64	.62251300 .62175800 .62101700 .62028800 .61957100	.62243700 .62168400 .62094300 .62021500 .61950000	.62236100 .62161900 .62081000 .62081000 .62019300 .61942900	+82228500 +82153400 +82079700 +82007100 +81935890	+62221000 60 +62146000 61 +62072400 62 +61999900 63 +51928700 64
64 66 57 68 69	.6199200 .61921700 .61651800 .61783000 .617.5300 .617.5300	+6191+600 +618+4800 +61776200 +61708600 +614+2000	.4.407600 .41837900 .61769300 .61701900 .61635400	+61900600 +61831060 +61762600 +61695200 +61628900	.61893600 .61824100 .61755600 .61625300 .61622300	65 66 67 68 69	<pre>61886600 61817200 61749000 61749000 61749000 61681800 61615700</pre>	.61879000 .61810400 .61742200 .61675200 .61609200	61872600 61803500 61735500 51668500 61802600	.61865700 .61796600 .61728700 .61661400 .61596100	.61858700 65 .61789500 66 .61722000 67 .61655300 68 .61589600 69
70 74 72 73 74	+61545000 +61515400 +61654600 +61392100 +61330300	+01576500 +01512000 +01448590 +61385900 +61324200	+61570000 +61505609 +61462200 +61379700 +61318100	+61563500 +61499200 +81435900 +81373500 +61312000	.61557100 .61462900 .61429600 .61567300 .61557300	70 71 72 73 74	.61550600 .61486500 .61423300 .61361100 .61299600	61544200 61480100 61417100 61354900 61293700	+61537700 +61+73800 +61410800 +61348800 +61287600	+61531300 +61447400 +61404600 +61342600 +61281500	+41524800 7C +61441130 71 +61398300 72 +61336500 73 +61275500 74 +61215400 75
75 74 17 78 79	•61269400 •61209400 •61150200 •61091400 •61034300	.61263400 .61203400 .61164300 .61086100 .61028600	+61257400 +61197500 +61138500 +61080300 +61022900	.61251300 .61191600 .61132600 .61076500 .61017200	.61245300 .61185400 .6124600 .61068700 .61068700	75 76 77 70 79	.61239300 .61179700 .61120900 .61063000 .61005870	.61233300 .61173800 .61115100 .61057200 .61000100	+51227300 +61167900 +61109900 +61051900 +60994500	.61221300 .61162090 .61103500 .61065700 .60588800	.61213400 76 .61097700 77 .61040000 78 .60981.00 79 .60927000 60
80 61 82 83 84	+60977500 +60921500 +60846200 +60811600 +60757700	.00571900 .00515900 .0060700 .0006200 .00752400	++++++++++++++++++++++++++++++++++++++	. 60 950 600 . 50 90 48 90 . 50 84 97 90 . 50 7954 00 . 50 7954 00 . 60 74 1 700	+ 60 95 5000 + 60 899 306 + 60 884 300 + 60 790 900 + 60 7364 00	60 61 82 83 84		.60943800 .60888200 .60833400 .60779203 .60725800	+60938200 +60882700 +608827900 +60773800 +60720400	+60877200 +80822500 +60768500 +60715100	- 60871700 81 - 60817000 82 - 60763100 83 - 60709800 84
85 86 87 88	+8070+600 +80652000 +60600200 +6058400 +60588400	+ 60546800 + 60595000 + 60543900	+60 894000 +60 84 1800 +60 589900 +60 588900 +60 488 300	. 60688700 . 60636400 . 60584700 . 60533700 . 60483300	+50683500 +50631200 +50579500 +50528500 +50428300	85 86 87 88 89	+60678200 +80626000 +60574500 +60574500 +60523600 +60473500	.60673000 .60622800 .60568400 .60518500 .60468300	+60667700 +60615700 +60564200 +60513500 +60463300	.60610500 .60559100 .60508400 .60458300	+60405300 M6 +60554000 87 +60503400 88 +60453300 89 +60403800 90
90 91 92 93 94	+60448300 +60398400 +60350100 +603501800 +60351800	.60394000 .60345200 .60297000	00438400 004086400 10040400 10040400 10040400 10040400 10040400 10040400	+ 604 335 00 + 60 3842 00 + 60 3856 00 + 60 2875 00 + 60 2875 00	•00 628500 •00 379300 •00 330790 •00 282793 •00 233200	90 91 93 93	.60423600 .60314400 .60325900 .60277900 .60270500	+60366600 +60321100 +60273100 +60273100	.50413700 .60364700 .60316300 .60268400 .60271100	+00359800 +00311400 +00263600 +00216400	.60355000 91 .60306600 92 .60258900 93 .60211700 94
95 96 97 98	+00207000 +0114200 +00114200 +00088000 +00023500		+60107600 +63151100 +60105000 +60059500 +60014500	. 401 92900 . 401 444 00 . 401 08500 . 409 55000 . 409 101 40	.60141800 .60099900 .60099900	95 94 97 98 99	.60183600 .60137200 .60091300 .60066000 .60991100	+60132600 +60086800 +60041500	+80124000 +8012200 +60032200 +50032200	.60123400 .60077700 .60032400	+40118800 90 +40073100 97 +40028000 98

TABLE 4.2.0.0-IV 91% CUMULATIVE PROGRESSIVE CURVE TABLE

	918		E MOGRESS CUR	VE TABLE	918		, 915 5		VE PROGRESS CU	RVE TABLE	418. G
2	0 8.17983000 15.0594800 21.52845800 21.52845800 2.7.68440100	1 8.v01m4700 15.74678900 22.15519200 28.28774100	. 6. 40346000	2+77115700 10+31997000 17+05617100 23+40064900	3.59925700 11.01829300 17.70511400 24.0195500 30.08612000	1 2 3	4.40259300 11.71009100 18.35046200 24.43602500 30.48186600	5.16624600 12.39584100 18.99237600 25.25013600 31.27583300	5.95363300 13.07595700 19.63100200 25.86196200 31.84406500	6+70720400 13+75080500 20+26647500 26+47157200 32+45860300	7++487950C 14+82070600 1 20+89892200 2 27+07903100 3 53+04748600 4
5 6 7 8 9	53,63475300 39,42582300 -5,08748700 50,64054500 56,10028100	34,22044000 39,99741400 45,64739300 51,19050200 56,64159600	34,80458100 40,56774200 46,20823400 51,73954100 57,18210600	46.76402700	35.06835900 41.70469800 47.32078900 52.83491800 58.26075390	5 6 7 8 9	36.54805900 42.27137100 47.87633500 53.38128000 58.79880900	37+12634000 42+8368600 48+43128000 53+92677300 59+33629800	37,70323000 43,40120900 48,98503900 54,47140900 59,67293000	38.27875600 43.96441300 49.53782700 55.01519800 60.40881400	38+85294500 5 44+52550000 6 50+J8985800 7 55+55815200 6 6/1+94395800 9
10 11 12 13	61++7837100 56+78401500 72+02463600 77+.0634200 82+33+25000	62.01206100 67.31089300 72.54536600 77.72147700 82.84425400	62+54503600 67+83712900 73+06551400 78+23607906 83+35376800	63.07730400 68.36272900 73.58508400 78.75015300 83.86279600	63+60887300 68+88769900 74+10408200 79+26370300 84+37134200	10 11 12 13	64.13975000 69.41204500 74.62251300 79.77673400 84.87840900	64.66994300 69.93577400 75.14034200 80.28925000 83.38700100	65.1944:900 70.45889200 75.65769500 80.80125500 85.69412200	65.72830500 70.98140400 76.17445600 81.31275400 86.40077500	66-25668800 10 71:50331700 11 76:59067000 12 81:82375100 13 86:90606400 14
15 16 17 18	87.41269300 42.44534500 47.41558400 102.38608600 107.29438400	87.41796500 42.44627700 47.43237700 102.87905200 107.78876100	88.42278300 93.44673800 98.42877600 103.37164800 108.27778500	108.76546400	80+43107230 94+44640600 99+42040100 104+35574100 109+25475900	15 16 17 18 19	104.84724300 109.74279300	90,43758700 93,4442200 100,41048100 105,33838400 110,23044700	105.82916700	106-31959600	91.94408800 15 96.93839500 16 101.89274800 17 106.80966 00 18 111.69139200 19
21	117. 12302200 1213710500 126.32156200	117.50580800	117.98828300 122.79631800 127.57502900	118.47045000	114.11989100 118.95230900 123.75455800 128.52738100 133.27278200	20 21 22 23 24	119.43386300 124.23294200 129.00314200 133.74585300	124.71123800 129.47862800 134.21866200	120.39606100 125.18924000 129.95384100 134.89121000	120.87670500 125.66696900 130.42878200 135.16349800	116+53992400 20 121+35705500 21 126+14440700 72 130+90345200 3 135+63552800 75
25 26 27 28 24			141,71891300 146,42344800 151,07469600	146.21744300 145.88960500 151.53857700 156.16528400	137+99183900 142+66573100 147+39553000 152+00223500 156+62076+00	25 26 27 28 29	143.15377800 147.82122400 152.46567100 157.08803100		144.08915300 148.75192300 153.39188200 158.00992800	144.55648400 149.21693000 153.85465800 158.47056000	140.34186100 25 145.02357800 26 149.68171000 27 154.31721600 28 158.93098200 29
30 51 53	108.57272300	159-85120000 164-43996100 169-30871900 173-55817800 178-08899600	160+31099700 164+99772500 169+46452200 174+01208800 178+54107900	165.35529000 169.92013300 174.46581300 178.99298100	161+22997300 165+81265600 170+37555200 174+91935200 179+64670600	30 31 32 33 34	170+83078000 175+37270700 179+89624800	166.72679500 171.28581800 175.82587800 180.34761500	180.79880+00	167.64014900 172.19532600 176.73167100 181.74681700	163.52383200 30 168.09653300 31 172.64979700 3. 177.184.0500 33 181.70065400 34
15 10 17 18	182.15131500 180.64834400 191.12854000 195.54225700 _00.04003800	182+60180100 187+09716780 191+57564200 196+03774400 200+481~5830	183+05211300 187+*4575600 192+02258100 196+48307300 200+92772300		183+95221600 188+4+245900 192+91596900 197+37325500 201+81+79300	35 36 37 38 39	188.890354v0 193.36242000 197.81811000 202.25809800	184,85142800 189,33848300 193,80870900 198,26280800 202,70125100	185.30107700 189.78624500 194.25483700 198.70734900 203.14425200	190.23384200 194.70080400 199.15173400 203.58710100	168.19946200 35 190.68127300 36 195.14661000 37 199.59566400 38 204.02979900 39
-0	204 + 723+600 208 + 88962300 213 + 2 4728000 217 + 6 4071400 222 + 3 5 5 2 400	204.91474300 204.33054000 213.73175700 218.11878900 222.449200600	205+35699000 209+77131100 21+17109200 218+55672600 222+92858200	210+21193700 214+61028600 218+99452600 223+36502400	208-24103700 210+65241800 215+04933900 219+43218800 223+80133200	40 41 42 43 44	211.09275400 215.46825100 219.86971300 224.23750000	215.92702300 220.30710200 224.67354700	216+36565500 220+74435400 225+10945500	212.41289900 216.80414700 221.18147000 225.54523100	208.4456000 40 212.85266100 41 217.24250000 42 221.61845100 43 225.93087500 44
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TABLE 4.2.0.0-V 95% CUMULATIVE PROGRESSIVE CURVE TABLE

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TABLE 4.2.0.0-VI TOTAL UNIT AND CUMULATIVE COST

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MLLV SINGLE STAGE VEHICLE LESS ENGINES (DOLLARS IN MILLIONS)

	—r																	7
	COST	CUM	\$ 321	634	841	1,045	1,247	1,447	1,645	1,842	2,038	2,232	3.194	4,141	5,078	6,006	6,927	\$7,843
	TOTAL COST	UNIT	\$321	313	207	204	202	200	198	197	196	195	191	188	187	185	184	\$183
<u> </u>	COST	CUM	\$ 226	452	577	702	827	952	1,077	1,202	1,327	1,452	2_077	2,702	3,327	3,952	4,577	\$5,202
(2) FIXED COST	FIXED	UNIT	\$226	226	125	-						125	125				-	\$125
(1) E STAGE	VEHICLE COST	CUM	ફ 95	182	264	343	420	495	568	640	711	780	211 12	1.439	1,751	2,054	2,350	\$2,641
) SINGLA	VEHICL	UNIT	\$95	87	82	79	77	75	73	72	71	70	уy	63	62	60	59	\$58
		UNIT	1	73	က	4	ວ	9	7	80	6	10	ц Т	20	25	30	35	40

- engine installation. The composite learning curve value is 91%. First unit cost is \$95.000,000. Single stage includes cost of structures, system, maintenance, and transportation and (<u>1</u>) NOTE:
- Fixed costs for each single stage vehicle include: propellant, IU. SDF operations, launch operations, and maintenance and SE&I costs. No learning curve effects were applied in developing these costs. (2)

TABLE 4, 2, 0, 0-VII TOTAL UNIT AND CUMULATIVE COST MULTICHAMBER/PLUC AND TOROIDAL FNGINES FOR THE MLLV SINCLE STAGE VEHICLE

(DOLLARS IN MILLIONS)

	(1)	((2) TORO	(2) TOROIDAL		
	* MULTIC	* MULTICHAMBER	**286К ТНВ	286K THRUST 1200 PSI	***1M THR	***1M THRUST 1200 PSI	***1M THRUST 2000 PSI	ST 2000 PSI
VEH	PLUG EN	CUM CUM	UNIT	CUM	UNIT	CUM	TINIT	CUM
								8
-	0 0 1 4	\$ 50.8	\$32.8	\$ 32.8	\$23.2	\$ 23.2	\$23.5	\$ 23.5
	0,06		20.8	62.6	21.3	44.5	21.6	45.1
63	46.0	20.0	0.02 0.02	6 10	90 5	65.0	20.7	65.8
en	44.3	141.1	0.02	3.1.5		O O	20.2	86.0
4	43.2	184.3	27.9	119.1	20.02	0.00		105.0
• ư	42.5	226.8	27.4	146.5	19.6	104.6	19.9	100.01
.	11.0	268 6	27.0	173.5	19.3	123.9	19.6	C.C21
٥	0,14	0 000	26 7	200.2	19.1	143.0	19.3	144.8
7	41.3			996 6	18 9	161.9	19.1	163.9
80	40.8	350.7	50.4	077		100 6	10 0	182.9
σ	40.1	391.2	26.1	252.7	18.7	100.0		6 1064
, C	\$40.1	\$ 431.3	\$25.9	\$ 278.6	\$18.6	\$199.2	\$18.8	1.1026
2								
			\$95 A	\$ 405.8	\$18.2	\$290.3	\$18.4	\$293.9
15	\$39.3	T-070 ¢			10 7	270 1	17_9	383.8
20	38.3	820.0	24.7	1.620	11.1		9 U F	472.0
25	37.6	1.008.4	24.3	651.4	17.4	400.2	0.11	
	0 16	1 193 4	23.9	771.2	17.1	552.1	17.4	0.800
30	0.10	1 001 0	99 6	889.6	16.9	636.9	17.1	644.9
35	36.7	7.110.1				\$ U6490 8	\$16.9	\$729.8
40	\$36.2	\$1,558.5	\$23.4	\$1,006.8	۲01¢	0.0216	0.0Te	
	*Blocks of 24 each	f 24 each	**Blocks of 28	of 28	***Blocks of 8	ks of 8	*** Blocks of	is of 8

- Multichamber/plug engines are based on an estimated first unit cost of \$2,500,000 and a learning curve value of 95%. NOTE: (1)
- First unit costs for toroidal engines are \$1,400,000, \$3,200,000 and \$3,240,000, respectively. The learning curve value is 95%. (3)

TABLE 4.2.0.0-VIII TOTAL UNIT AND CUMULATIVE COST MLLV INJECTION STAGE ENGINE MODULE LESS ENGINES

(DOLLARS IN MILLIONS)

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COST	I CUM		\$ 33.3	65.1	84.2	102.7	120.8	138.6	156.1	173.4	190.5	\$ 207.4	\$ 289.9		447.8	524.3	599.7	\$674.1	
TOTAL COST	IINIT	TIMO	\$33.3	31.8	19.1	18.5	18.1	17.8	17.5	17.3	17.1	\$16.9	\$16.3	15.8		15.2	15.0	\$14.8	
	CINE	MOO	\$ 16.6	33.2	37.9	42.6	47.3	F2.0	50.7	61.4	66.1	\$ 70.8	с 64 3 2		141 3	164.8	188.3	\$211.8	
(2) ETXED COST	TINIT'T T	TINIO	\$16.6	16.6	4.7						-	\$ 4.7	5 7 8		•			\$ 4.7	_
		CUM	s 16.7		46.3	60.1	73.5	86.6	99.4	112.0	124.4	\$136.6	с ЦСГФ Ф	0.351¢	5.162 500 E	350 F	411 4	\$462.3	
(1)	21	LINU	\$16.7	4 TC -	7 71	33.00	13.4	13.1	12.8	12.6	12.4	\$12.2	¢ 7	0.11	1.11	10.6	0°01	\$10.1	
		TINU	,	- 6	4 6	ۍ ۲	- u:			- a) c	10		15 1	20	52 50	ο Ο Γ	δ. 0 4 0 4	21

- Maintenance and Transportation. The composite learning curve value is 91%. The first Costs for one engine module include: Structures, Engine Installation, Systems Facility, unit cost is \$16,700,000. (1) NOTE:
- Fixed cost for one engine module include: Propeliant and Launch Operations Cost. No learning curve effects were applied in developing these costs. 6

TABLE 4.2.0.0-IX TOTAL UNIT AND CUMULATIVE COST MLLV INJECTION STAGE FUEL MODULE LESS ENGINES

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(DOLLARS IN MILLIONS)

																				_			
	, COST	CUM		\$ 1Z.0	23.4	32.2	40.8	49.2	57.4	65.6	73.6	81.6	\$ 89.5	\$ 128.0	165.5	202.2	238.3	273.8	309.0	378.2	446.3	513.5	\$ 579.9
	TOTAL COST	UNIT	(\$12.0	11.4	80 90	8.6	8.4	8.3	8.1	8.0	8.0	\$ 7.9	\$ 7.6	7.4	7.3	7.2	7.1	7.0	6.9	6.8	6.7	\$ 6.6
	FIXED COST	CUM		\$ 4.9	9.8	12.5	15.2	17.9	20.6	23.3	26.0	28.7	\$ 31.4	\$ 44.9		71.9	85.4	98.9	112.4	139.4	166.4	193.4	\$220.4
(2)	FIXEI	UNIT		\$4.9	4.9	2.7	-					-	\$2.7	2 2 3									\$2.7
	(1) DDULE COST	CUM		\$ 7.1	13.6	19.7	25.6	31.3	36.8	42.3	47.6	52.9	\$ 58.1	\$ 23 1	107 1	130.3	152.9	174.9	196.6	238.8	279.9	320.1	\$359.5
(1)	FUEL MODU	TINU		\$7.1	6.5	6.1	5.9	5.7	5.6	5.4	5.3	5.3	\$5.2	0 13	5 F 4	4.6	4.5	4.4	4.3	4.2	4.1	4.0	\$3.9
		TINU			2		→ 4	- LC) (j		. oc		10	Li T		25	30	35	40	50	60	20	80

- Maintenance and Transportation. The composite learning curve value is 91%. The first Structures, Engine Installation, Systems Facility, Costs for one fuel module include: unit cost is \$7,100,000. Ð NOTE:
- Fixed cost for one fuel module include: Propellant and Launch Operations 30st. No learning curve effects were applied in developing these costs. (5)

TABLE 4.2.0.0-X TOTAL COST MLLV INJECTION STAGE ENGINES (DOLLARS IN MILLIONS)

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The learning curve value is 95% . The first unit cost of the 125,000 pounds thrust ergine is \$1,370,000. NOTE:

TABLE 4.2.0.0-XI TOTAL COST MLLV COST FOR THE ALTERNATE FORWARD SKIRT AND SRM FIXED COSTS (DOLLARS IN MILLIONS)

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II (1) AT TE	ERNATE	(2) 2	SRM		
	D SKIRT COST	FIXED COS	FIXED COST PER FLIGHT	TOTAL COST	TOTAL COST PER FLIGHT
UNIT		TINU	CUM	UNIT	CUM
\$2.9	\$2.9	\$20.6	\$20.6	\$23.5	\$23.5
2.6	5.5	20.6	41.2	23.2	46.7
2.5	8.0	6.5	47.7	0.6	55.7
2.4	10.4	-	54.2	8.9	64.6
2.3	12.8		60.7	8.8	73.5
2.3	15.0		67.2	8.8	82.2
2.2	17.3		73.7	8.7	91.0
2.2	19.5		80.2	8.7	99.7
2.2	21.6		86.7	8.7	108.3
\$2.1	\$23.7	\$ 6,5	\$93.2	\$ 8.6	\$116.9
\$2.0	\$34.0	\$ 6.5	\$125.7	\$ 8.5	\$159.7
1.9	43.7		158.2	8.4	201.9
1.9	53.2		190.7	8.4	243.9
1.8	62.4		223.2	8.3	285.6
1.8	71.4	-	255.7	8.3	327.1
\$1.8	\$80.3	\$ 6.5	\$288.2	\$ 8.3	\$368.5

- Costs associated with the alternate forward skirt are "Delta" costs, over and above those costs required for a standard forward skirt. The composite learning curve value is 91%. The first unit delta cost is \$2,900,000. (1) NOTE:
- (2) SRM fixed costs include: Launch Operations and Launch Maintenance cost. No learning curve effects were applied in developing these costs.

TABLE 4.2.0.0-XII TOTAL COST MLLV SOLID ROCKET MOTOR STAGE QUANTITY SENSITIVE COST (DOLLARS IN MILLIONS)

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K COST CUM COST NBR(S) .0 \$ 21.0 44 .6 40.6 44 .6 59.6 46 .78.1 59.6 46 .9 78.1 50 .8 114.2 54 .9 132.0 56 .44 132.0 56 .45 149.6 64 .46 149.6 64 .149.6 167.0 88 .22 201.4 64 .28 235.3 80 .29 235.3 80 .9 235.1 96 .9 302.1 112 .12 318.6 104 .351.5 112 128 .144 26 335.1 144		AC TIN'I			UNIT OR	
\$21.0 \$21.0 \$44 19.6 \$40.6 \$40.6 19.0 59.6 \$46 19.0 59.6 \$48 18.5 78.1 50.6 18.5 78.1 50.6 18.2 96.3 50.6 17.9 114.2 52 17.4 156.6 \$48 17.4 167.0 56 17.4 184.2 64 17.2 218.4 72 17.2 218.4 72 17.0 218.4 72 16.9 235.1 88 16.6 302.1 104 16.5 335.1 104 16.5 335.1 120 16.5 335.1 128 16.5 335.1 128	NBR(S)	BLOCK COST	CUM COST	NBR(S)	BLOCK COST	CUM COST
96.5 19.6 40.6 46.5 19.6 59.6 59.6 48 18.2 96.3 59.6 48 17.9 17.8 114.2 56 17.6 114.2 56 46 17.6 149.6 149.6 56 17.1 114.2 556 54 17.2 201.4 64 56 17.2 201.4 64 56 16.6 235.3 80 235.3 16.6 235.3 88 88 16.6 335.1 104 16.5 335.1 104 16.5 335.1 112 16.5 335.1 128 16.5 335.1 128 16.5 128 128 16.5 128 128 16.5 128 128 16.4 128 128 16.5 128 128 16.5 128 128 16.6 128 128 16.8		1	5	44	\$16.3	\$ 384.1
19.6 40.6 18.5 78.1 18.5 78.1 18.2 96.3 17.9 117.8 17.6 132.0 17.6 149.6 17.2 184.2 17.2 201.4 17.2 218.4 17.2 218.4 17.2 218.4 17.2 218.4 17.2 218.4 16.5 235.1 16.5 335.1 16.5 335.1 16.5 335.1 16.5 104 16.5 1104 16.5 1104 16.5 1104 16.5 1120 16.5 1120	7-1	•				
19.0 59.6 18.5 78.1 18.2 96.3 17.9 17.9 17.6 114.2 17.6 132.0 17.6 149.6 17.2 184.2 17.2 184.2 17.2 184.2 17.2 184.2 17.2 184.2 17.2 184.2 16.6 235.1 16.5 302.1 16.5 335.1 16.5 335.1 16.5 335.1 16.4 120 16.5 104 16.5 120 16.5 335.1 16.4 128	4	19.6	40.6	46	16.2	400.3
18.5 78.1 50 17.9 17.9 114.2 52 17.8 114.2 54 54 17.6 114.2 54 54 17.6 17.4 167.0 56 17.2 201.4 64 56 17.2 201.4 64 64 17.2 218.4 72 64 16.9 235.3 80 96 16.8 252.1 88 96 16.6 235.3 80 96 16.6 302.1 1104 16.5 335.1 120 16.5 335.1 123 16.5 335.1 122	9	19.0	59.6	48	16.2	416.5
18.2 96.3 52 17.9 114.2 54 17.6 132.0 556 17.6 149.6 149.6 17.4 167.0 149.6 17.2 184.2 56 17.2 201.4 64 17.2 218.4 72 17.2 218.4 72 16.9 235.3 80 16.8 252.1 88 16.8 252.1 88 16.6 302.1 112 16.5 318.6 104 16.5 335.1 120 16.4 355.5 104 16.5 335.1 128 16.4 355.5 114	00	18.5	78.1	50	16.1	432.6
17.9 114.2 54 17.6 149.6 132.0 56 17.4 167.0 149.6 56 17.2 149.6 167.0 56 17.2 184.2 167.0 56 17.2 201.4 64 56 17.2 201.4 64 72 17.0 218.4 72 80 16.9 235.3 80 88 16.6 235.3 80 96 16.6 302.1 104 120 16.5 318.6 104 112 16.4 351.5 104 128 16.4 351.5 120 128	10	18.2	96.3	52	16.0	448.6
17.8 132.0 56 17.6 149.6 167.0 17.4 167.0 167.0 17.2 184.2 64 17.2 201.4 64 17.2 201.4 64 17.2 201.4 64 17.2 218.4 72 16.9 235.3 80 16.8 252.1 88 16.8 252.1 88 16.6 285.5 104 16.6 302.1 112 16.5 318.6 120 16.4 351.5 104 16.5 335.1 128 16.4 351.5 144	12	17.9	114.2	54	16.0	464.6
17.6 149.6 17.4 167.0 17.2 184.2 17.2 184.2 17.2 201.4 17.0 218.4 17.0 235.3 16.9 235.3 16.8 235.3 16.8 235.1 16.8 235.3 16.8 235.1 16.8 235.1 16.8 235.1 16.8 235.1 16.8 235.1 16.8 235.1 16.8 268.9 16.6 302.1 16.5 318.6 16.5 335.1 16.4 351.5 16.4 351.5	14	17.8	132.0	56	\$16.0	480.6
17.4 167.0 17.2 184.2 17.2 201.4 17.2 201.4 17.0 218.4 17.0 235.3 16.9 235.3 16.8 235.3 16.8 235.1 16.8 235.1 16.8 235.1 16.8 235.1 16.8 235.1 16.8 252.1 16.8 235.1 16.6 302.1 16.5 318.6 16.5 335.1 16.4 351.5 16.4 351.5 16.4 351.5	16	17.6	149.6			
17.2 184.2 17.2 201.4 17.2 201.4 17.0 218.4 17.0 218.4 16.9 235.3 16.9 235.3 16.8 235.1 16.8 252.1 16.8 252.1 16.8 268.9 16.6 302.1 16.5 318.6 16.5 318.6 16.5 335.1 16.4 351.5 16.5 335.1 16.4 351.5	18	17.4	167.0			
17.2 201.4 64 17.0 218.4 72 16.9 235.3 80 16.9 235.1 88 16.8 235.1 88 16.8 235.1 88 16.8 235.1 88 16.8 252.1 88 16.6 285.5 104 16.6 302.1 112 16.5 318.6 120 16.5 335.1 120 16.4 351.5 144	20	17.2	184.2			
17.0 218.4 72 16.9 235.3 80 16.8 252.1 88 16.8 252.1 88 16.8 255.1 88 16.6 268.9 96 16.6 285.5 104 16.6 302.1 112 16.5 318.6 120 16.5 335.1 120 16.4 351.5 144	22	17.2	201.4	64	15.8	544.1
16.9 235.3 80 16.8 252.1 88 16.8 252.1 88 16.8 258.9 96 16.6 285.5 104 16.6 302.1 112 16.5 318.6 120 16.5 335.1 120 16.4 351.5 144	24	17.0	218.4	72	15.7	607.1
16.8 252.1 88 16.8 268.9 96 16.6 285.5 104 16.6 302.1 112 16.5 318.6 120 16.5 335.1 120 16.5 335.1 128 16.5 351.5 144 26.4 351.5 144	26	16.9	235.3	80	15.6	669.5
16.8 268.9 96 16.6 285.5 104 16.6 302.1 112 16.5 318.6 120 16.5 335.1 128 16.4 351.5 144 26.9 835.1 144	28	16.8	252.1	88	15.4	731.4
16.6 285.5 104 16.6 302.1 112 16.5 318.6 120 16.5 335.1 128 16.4 351.5 144 *16.3 351.5 144	30	16.8	268.9	96	15.3	793.0
16.6 302.1 112 16.5 318.6 120 16.5 335.1 128 16.4 351.5 144 *16.9 \$367.8	32	16.6	285.5	104	15.2	854.1
16.5 318.6 120 16.5 335.1 128 16.4 351.5 144 *16.3 \$357 8	34	16.6	302.1	112	15.1	915.0
16.5 335.1 128 16.4 351.5 144 *16.9 \$367.8	36	16.5	318.6	120	15.1	975.5
16.4 351.5 144 ©16.9 \$367.8	30 13	16.5	335.1	128	15.0	1,035.7
6 JL 9	40	16.4	351.5	144	15.0	\$1,155.3
	42	\$16.3	\$367.8			

stage hardware and facility maintenance. The composite learning curve value is 95%. The first unit cost is \$10,754,000. Costs associated with the SRM stage cost include: structures, SRM motor, other NOTE:

TABLE 4.2.0.0-XIII TOTAL UNIT AND CUMULATIVE COST AMLLV SINGLE STAGE VEHICLE W/MULTICHAMBER/PLUG ENGINES

(DOLLARS IN MILLIONS) 4,422 5,738 7,035 8,319 \$10,852 1,418 1,702 1,983 2,261 2,537 9,590 1,130 2,811 3,033 428837 CUM TOTAL COST Ś 284 281 278 278 276 275 272 265 261 258 258 256 2533251 UNIT 293288 409 \$428 2,817 3,467 4,117 4,767 \$5,417 2,167 997 1,127 1,257 1,387 607 737 867 1,517 239 477 CUM FIXED COST Ś (3) UNIT \$130 130 130 \$239 238130 1,672 1,928 1,412 879 1,148 \$2,182 549BLOCKS OF 24 EACH) 197 258 318377 435492605 135 71 CUM MULTICHAMBER ŝ PLUG ENGINE ରି UNIT 54 52 52 52 51 53 53 62 61 59 57 57 57 57 \$71 43 2,530 2,156 \$3,253 1,376 1,773 2,895 225 326 423517 609669 788 875 961 118 SINGLE STAGE CUM \$ E UNIT 81 78 76 77 72 71 71 97 94 92 92 89 87 86 \$118 107 101 \$ UNIT 15 20 25 30 35 35 **6 4 6 0** 6 10 03 **6 4**

transportation and engine installation. The composite curve value is 91%. The first unit cost is \$118,000,000. Single stage includes cost of structures, systems, maintenance, E NOTE:

- Multichamber/plug engines are based on an estimated first unit cost of \$3,500,000 and a learning curve value of 95%. <u>ନ୍</u>
- and maintenance and SE&I costs. Units 1 and 2 include R&D instrumentation. No learning curve effects Fixed costs for each single stage vehicle include: propellant, IU, SDF operations, launch operations were applied in developing these costs. <u>(</u>?)

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TOTAL UNIT AND CUMULATIVE COST **TABLE 4.2.0.0-XIV**

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A the second second Ī AMLLV SINGLE STAGE VEHICLE W/TOROIDAL ENGINES

(DOLLARS IN MILLIONS)

	TOTAL COST	CUM	\$404	794	1,069	1,339	1,605	1,768	2,129	2,389	2,646	2,902	4 162		5,400	6,621	7,830	9,027	
	TOTA	UNIT	\$404	390	295	270	266	263	261	260	257	256	250	1	246	243	241	238	
	(3) FIXED COST	CUM	\$239	477	607	737	867	266	1,127	1,257	1,387	1,517	9 167	- 1 OT 6 -	2,817	3,467	4,117	4,767	•
) () FIXEI	UNIT	\$239	238	130	-						130	130	7001	-			-	-
	(2) FOROIDAL ENGINES	CUM	\$ 47	92	136	179	221	262	303	344	384	424	810 8	eto	810	998	1,183	1,365	
	(2) TOROIDAL	TINU	\$47	45	44	43	42	41	41	41	40	40	Ç	00	38	37	37	36	
	(1) SINGLE STAGE	CUM	\$ 118		326	423	517	609	669	788	875	19C	010G F	1,370	1,773	2,156	2,530	2,895	
I	(1) SINGLE	UNIT	\$118	107	101	2.6	94	92	06	68	87	86	ţ	81	78	76	74	72	
		UNIT	1	0	e	4	5	9	7	00	6	10	L T	CT	20	25	30	35	

Single Stage includes cost of structures, systems, maintenance and transportation and engine installation. The composite curve value is 91%. The first unit cost is \$118,000,000. **E** NOTE:

\$10,216

\$237

\$130

\$1,546

\$36

\$ 3,253

\$ 71

30 35 40

3,4674,117 4,767 \$5,417

- Toroidal engines are based on an estimated first unit cost of \$47,300,000. This consists of a 16 module, 2,000 PSI (1.0m lb thrust per module) engine. The learning curve value is 95%. (5
- (3) Fixed costs for each single stage vehicle include: Propellant, IU, SDF operations. launch operations and maintenance and SE&I costs. No learning curve effects wore applied in developing these costs.

TABLE 4.2.0.0-XV 'rOTAL UNIT AND CUMULATIVE COST AMLLV INJECTION STAGE ENGINE MODULE LESS HIGH PRESSURE ENGINES

. У.Ц. (DOLLARS IN MILLIONS)

L COST	CUM		\$ 37.8	73.8	07 1		119.8	142.0	163.8	185.3	006	1.002	227.4	248.1		349.2	447.2	E40 9	0.44.0	636.2	729.2	\$ 0.55 P	
(3) TOTAL COST	UNIT		\$37.8	36.0		23.3	22.7	22.2	20.8	21.5		21.12	21.0	20.7		19.9	19 4		13°0	18.6	18.4	¢10 1	T.014
COST	CIIM		\$ 17.4			40.6	46.4	52.2	58.0	0 6 9	0.00	69.6	75.4	C F0	7.10	110.2	190.9	7°601	163.2	197.2	2.9.6 2		\$ 500.4
(2) FIXED COST		TINIO	\$17.4	V 41	L/.4	5.8								-	۵. x	α L	• •	-					۵.6 ۴
CODIT F		CUM	V 00 Ø	4 5 5 5 6 6	39.0	56.5	73.4	0 00	0000	100.0	121.5	136.8	152 0	0.101	166.9	0.000	0.602	308.0	374.0	439 0		0.300	\$565.0
THOME MODILE	(I) FINCINE	UNIT		\$20.4	18.6	17.5	0 21	10.0	10.4	16.0	15.7	15.3	6 11	1 2.61	14.9		14.1	13.6	13.2		14.0	12.6	\$12.3
		UNIT			67	c	2	4, 1	5 C	9	7	a	0 0	<u>5</u>	10		15	20	25		30	35	40

- Maintenance and Transportation. The composite learning curve value is 91%. The first Costs for one engine module include: Structures, Engine Installation, Systems, Facility unit cost is \$20,400,000. **E** NOTE:
- Fixed cost for one engine module include: Propellant and Launch Operations cost. No learning curve effects were applied in developing these costs. 6
- (3) Refer to Table 4.2.0.0-XVII for Engine cost.

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TABLE 4.2.0.0-XVI TOTAL UNIT AND CUMULATIVE COST AMLLV INJECTION STAGE FUEL MODULE LESS HIGH PRESSURE ENGINES

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(DOLLARS IN MILLIONS)

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(3) TOTAL COST	CUM	С 1 1 2 2	30.3	41.9	53.2	64.2	75.0	85.7	96.2	106.6	116.9	 167.3	216.2	264.1	311.1	357.4	403.2	493.3	581.9	669.2	\$755.5
) TOTAI	UNIT	۵ ۱۳ ۵	14.7	11.6	11.3	11.0	10.8	10.7	10.5	10.4	10.3	 9.9	9.7	9.5	9.3	9.2	9.1	8.9	8.8	8.7	\$ 8.6
(2) FIXED COST	CUM	ि ४ २	12.0	15.3	18.6	21.9	25.2	28.5	31.8	35.1	38.4	54.9	71.4	87.9	104.4	120.9	137.4	170.4	203.4	236.4	\$269.4
(2) FIXED	UNIT	۲ ۵۵	6.0	3.3						-	3.3	3.3	-	•						-	\$3.3
(1) FUEL MODULE	CUM	9 U 4	18.3	26.6	34.6	42.3	49.8	57.2	64.4	71.5	78.5	112.4	144.8	176.2	206.7	236.5	265.8	322.9	378.5	432.8	\$486.1
CIELN	UNIT'	8 U \$	8.7	8.3	8.0	7.7	7.5	7.4	7.2	7.1	7.0	6.6	6.4	6.2	6.0	5.9	5.8	5.6	5.5	5.4	\$5.3
	UNIT		 ~7	сл	4	5	9	7	œ	6	10	 15	20	25	30	35	40	50	60	70	80

- Costs for one fuel module include: Structure, Engine Installation, and Systems cost. The composite learning curve value is 91%. The first unit cost is \$9,600,000. **E** NOTE:
- Fixed costs include: Propellant and Launch Operations. No learning curve effects were applied in developing these costs. (3)
- (3) Refer to Taple 4.2.0.0-XVII for Engine cost.

TABLE 4.2. 0. 0-XVII TOTAL COST AMLLV INJECTION STAGE ENGINES

(DOLLARS IN MILLIONS)

CUM	COST	\$ 67.0	70.0	73.0	75.9	2 00 0 00 0 00	81.8	84.7	87.6	90.5	93.4	107.8	199 0	1 201	1.051	177.0	218.7	259.0	298.8	\$338.2		
	UNIT	42	44	46	94	40 70		54	95	0 00	909	0.5		80 00	90	120	150	180	210	240		
F		T					<u>.</u>															
MIN	COST	c e	0 - 1 0 - 1	7.4	10.9	14.2	17.6	20.8	24.1	21.3	30.4	33.0	36.7	39.8	42.9	46.0	49.0	52.0	55.1	58.1	61.1	\$64.1
	TINU		N	4	9	æ	10	12	14	16	18	20	22	24	26	28	30	32	34	36	38	40

NOTE: The learning curve value is 95%. The first unit cost of the 250,000 pound thrust engine is \$1,960,000.

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AMLLV SRM COST - FIXED AND VARIABLE TOTAL CUMULATIVE COST TABLE 4.2.0.0-XVIII

(DOLLARS IN (SNOFITIN

	TOTAL SKIRT + FIXED	CUM	\$ 32.0		75.5	87.3	98.9	110.4	121.9	133.3	144.6	155.9		211.7	266.8	321.5	375.7	429.6	\$483.2			
	TO' SKIRT	UNIT	32.0	31.6	11.9	11.8	•	•	11.5	11.4	11.3	11.3		24	23.	23.	22.	22.	22.0			
Q	PER H (SRM)	CUM	\$ 27.4		62.7	70.6	78.5	86.4	94.3	102.2	110.1	118.0		157.5	197.0	236.5	276.0	315.5	355.0			
(3) FIXED	COST PER LAUNCH (SRM)	UNIT	27.4	27.4	7.9	-						6.4		2.9					612			
(2) d cost for	ALTERNATE FWD SKIRT	CUM	\$ 4 6		12.8	16.7	20.4	24.0	27.6	31.1	34.5	37.9		54.2	69.8	85.0	99.7	114.1	\$125.2			
A COS	ALTE FWD :	UNIT	4.6	4.2	4.0	3.9	3.7	3.6	3.6	3.5	3.4	3.4		16.3	15.6	15.2	14.7	14.4	14.1			
		UNIT	+	1 01	ۍ م	4	5	9	2	8	6	10		15	20	25	30	35	40			
		CUM	\$ 446 4	-	485.8	505.4	525.0	544.5	563.9	583.3	602.7	622.0		1,183.9	1,724.6	2,251.8	2,769.3	3,279.2	3,782.8	4,281.1		
	ST	UNIT	10 R		10.6			19.5	19.4	19.4	19.4	19.3		18.3	17.8	17.4	17.1	16.9	16.7	16.5		
	(1) SRM STAGE COST	TINU	67	44	46	48	50	52	54	56	58	60		120	180	240	300	360	420	480		
	SRM	CUM	1	4 20.4 49 3	72.3		116.9	138.7	160.2	181.5	202.6	223.6	244.4	265.1	285.6	306.0	326.3	346.6	366.7	386.7	406.7	\$426.6
		UNIT	2 	4.07 9.3.9	23.0	22.5	22.1	21.8	21.5		21.1	21.0	20.8	20.7	20.5	20.4	20.3	20.3	20.1	20.1	20.1	19.9
		UNIT	c	7 7	+ 9	00	10	12	14	16	18	20	22	24	26	28	30	32	34	36	38	40

Costs associated with the SRM stage cost include: Structures, SRM Motor, other stage hardware, and Fability Maintenance. The composite learning curve is 95%. The first unit cost is \$13,050,000. <u>(1</u>) NOTE:

- Delta costs associzted with the alternate forward skirt include all production costs over and above that of a standard forward skirt. The composite learning curve is 91%. The first unit cost is 84,600,000. 6
 - SRM fixed costs include Launch Operations and Launch Maintenance. No learning curve effects were (c)

applied in developing these costs.

4.3 METHODS FOR DETERMINING UNIT COSTS AND FOR COMPILING OVERALL PROGRAM COSTS

This section presents examples showing the use of the learning curve tables, provided in Section 4.2, to determine: (1) the operational cost of a tenth AMLLV representative vehicle configuration and (2) the overall program costs for a sample program consisting of a mix of AMLLV configurations. The overall program costs determined for the latter example include not only the operational costs, but the non-recurring costs also.

The cost of producing and launching a 10th unit AMLLV vehicle consisting of (1) a main stage with multichamber/plug engines, (2) one injection stage engine module, and (3) twelve strap-on stages can be determined as follows:

10th Unit Description	Unit Price	Ref. Table
Main Stage		
Single Stage Vehicle (No. 10)	\$ 86.0M	4.2.0.0-XIII
Multichamber/ Plug Engines No.'s 217-240 (Block of 24)	56.0M	4.2.0.0-XIII
Fixed Cost	130.0M	4.2.0.0-XIII
	\$271.	0 M
Injection Stage Engine Module		
Engine Module (No. 10)	\$ 14.9M	4.2.0.0-XV
Fixed Cost	5.8M	4.2.0.0-XV
High Pressure Engines (No.'s 19 and 20)	<u>3.2M</u>	4.2.0.0-XVII
Sub-Total	\$ 23	.9M

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4.3 (Continued)		
10th Unit Description	Unit Price	Ref. Table
Strap-On Stage(s)		
SRM Stage Cost (No.'s 109-120)	\$110.3M	4.2.0.0-XVIII
Alternate Fwd. Skt. (No. 10)	3. 4M	4.2.0.0-XVIII
Fixed Cost	7.9M	4.2.0.0-XVIII
Sub-Total	\$121.	6M
TOTAL COST	<u>\$416.</u>	<u>5 M</u>

Use of the learning curve tables to determine overall program costs is illustrated considering a twelve vehicle AMLLV program consisting of the following:

I "Get Ready" Phase

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II Development Test Phase (exclusive of R&D flight tests)

III Two R&D flight vehicles (Max. payload config) followed by:

IV six single-stage-to-orbit vehicles followed by :

V One maximum payload AMLLV vehicle followed by:

VI Three vehicles consisting of a main stage with four SRM's.

		Cumulative Cost	Ref. Table
Ι.	"Get Ready, A costs		
	Main Stage	\$13 2 5.2M	4.0.0.0-I
	Injection Stage Engine Module	248.1M	4 0.0.0-I
	Two Injection Stage Fuel Modules	1.4M	4 0.0.0-I
	SRM Fixed	311.8M	4.0.0.0-I
	SRM Variable	88.5M	4.0.0.0-I
	Total A Costs	\$1,975	6.0M

4.3 (Continued)

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		Cumulative Cost	Ref. Table
Π.	Development Test. B Costs (Exclusive of Two R&D Flight Tests)		
	Main Stage	\$1,210 .5M	4.0 0 0-II
	Injection Stage Engine Module	337.7M	4.0.0.0-II
	Two Injection Stage Fuel Modules	73.9M	4.0.0.0-II
	SRM Stage	214.1M	4.0.0.0-II
	Total B Costs	\$1,836	. 2M
ш.	Two R&D Flight Vehicles		
	Main Stage		
	Single Stage Vehicle (No.'s 1-2	e) \$ 225.0M	4.2.0.0-XIII
	Multichamber/Plug Engines (No.'s 1-48)	135.0M	4.2.0.0-XIII
	Fixed Cost	477.0M	4.2.0.0-XIII
	Sub-Total	\$837.	0 M
	Injection Stage - Engine Modules		
	Engine Modules (No.'s 1-2)	\$39. 0M	4.2.0.0-XV
	Fixed Cost	34.8M	4.2.0.0-XV
	125K Thrust Engine (No.'s 1-2 & 7-8)	7.1M	4.2.0.0-XVII
	Sub-Total	\$80. 9	ЭМ

4.3	(Continued)	Cumulative	
	Two R&D Flight Vehicles	Cost	Ref. Table
	Injection Stage - Fuel Module		
	Fuel Module (No.'s 1-4)	34.6M	4.2.0.0-XVI
	Fixed Cost	18.6M	4.2.0.0-XVI
	125K Thrust Engine (No.'s 3-6 & 9-12)	_13.7M_	4.2.0.0-XVII
	Sub-Total	\$66.9	Μ
	SRM Strap-On Stage		
	SRM Stage (No. 's 1-24)	\$265 . 1M	4.2.0.0-XVIII
	Alt. Fwd. Skt. (No. 's 1-2)	8.8M	4.2.0.0-XVIII
	SRM Fixed Cost	54.8M	4.2.0.0-XVIII
	Sub-Total	\$328.	7M
	TOTAL	\$1,313.	5M
۲V.	Six Single Stage Vehicles	Cumulative Cost	Ref. Table
	Main Stage		
	Single Stage Vehicle (No. 's 3-8	\$ 563. 0M	4.2.0.0-XIII
	Multichamber/Plug (No.'s 49-192)	357.0M	4.2.0.0-XIII
	Fixed Cost	780. OM	4.2.0.0-XIII
	TOTAL	<u>\$1,7</u>	00. 0M

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4.3	(Continued)	Cumulative	
ν.	One Maximum Payload Vehicle	Cost	Ref. Table
	Main Stage		
	Single Stage Vehicle (No. 9)	\$ 87.0M	4.2.0.0-XIII
	Multichamber/Plug (No.'s 193-216)	57. OM	4.2.0.0-XIII
	Fixed Cost	<u>130.0M</u>	4.2.0.0-XIII
	Sub-Total	\$274.0M	
	Injection Stage - Engine Module		
	Engine Module (No. 3)	\$ 17.5M	4.2.0.0-XV
	Fixed Cost	5.8M	4.2.0.0-XV
	High Pressure Engines (No.'s 13-14)	<u>3. 3M</u>	4.2.0.0-XVII
	Sub-Total	\$ 26.6M	
	Injection Stage - Fuel Modules - (Tw o)	
	Fuel Module (No.'s 5-6)	\$15.2M	4.2.0.0-XVI
	Fixed Cost	6.6M	4.2.0.0-XVI
	High Pressure Engines (No.'s 15-18)	6.3M	4.2.0.0-XVII
	Sub-Total	\$28.1M	
	SRM Strap-On Stage		
	SRM Stage (No. 's 25-36)	\$121.6M	4.2.0.0-XVIII
	Alt. Fwd. Skt. (No. 3)	4. OM	4.2.0.0-XVIII
	SRM Fixed Cost	7.9M	4.2.0.9-XVIII
	Sub-Total	\$133. 5M	
	TOTAL	<u>\$462.2M</u>	

1.0	(continued)		
VI.	Three Vehicles Consisting of a Main Stage with Four SRM's	Cumulative Cost	Ref. Table
	Main Stage		
	Single Stage Vehicle (No.'s 10-12)	\$255 . 0M	4.2.0.0-XIII
	Multichamber/Plug Engines (No.ºs 217-288)	167.0M	4.2.0.0-XIII
	Fixed Cost	390. OM	4.2.0.0-XIII
	Sub-Total	\$812.0M	
	SRM Strap-On Stage		
	SRM Stage (No.'s 37-48)	\$118.7M	4.2.0.0-XVIII
	Alt. Fwd. Skt. (No.'s 4-6)	11.2M	4.2.0.0-XVIII
	Fixed Cost	<u>23.</u> 7 <u>M</u>	4.2.0.0-XVIII
	Sub-Total	\$153 . 6M	
	TOTAL	\$965. 6M	
Sum	mary Total Program		
I. II. IV. V. VI.	"Get Ready", A Costs Development Test, B Costs R&D Flight Vehicles Single Stage Vehicle Full Size Vehicle Single Stage W/Four SRM's Each	\$1,975.0M 1,836.2M 1,313.5M 1,700.0M 462.2M 956.5M	
GRA	ND TOTAL	\$8,234.4M	

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(Continued)

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The above representative examples used the multichamber/plug propulsion system on the main stage. The same type of cost data can be developed for vehicles with the toroidal/aerospike propulsion system on the main stage by using the toroidal/ aerospike data shown in Table 4.2.0.0-XIV in lieu of the multichamber/plug propulsion data. The MLLV data, contained in Tables 4.2.0.0-VI through 4.2.0.0-XII, may

4.3 (Continued)

be used to develop vehicle cost data and/or vehicle program costs in the same manner as shown above for the AMLLV.

Similar calculations can be performed to determine the costs of larger or smaller size programs for both the AMLLV and the MLLV vehicle configurations as discussed in the following Section 5.1.

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5.0 COST EFFECTIVENESS OF PROGRAM AND CONFIGURATION OPTIONS

This section of Volume VI show methods for application of the "modularized" cost data shown in Volumes IV and V (and summarized in the preceding Section 4.0 of this Volume) to evaluate:

1. The overall program costs for specific programs.

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- 2. The effects of program size on overall program costs and cost effectiveness.
- 3. The relative cost effectiveness of the AMLLV and MLLV sizes as applied to specific program requirements.
- 4. The cost effectiveness of various AMLLV and MLLV configuration options.

As the number of possible combinations between program and configuration options is significantly large, this section does not attempt to evaluate all of the alternatives. Representative program and configuration trades are presented to demonstrate how such trades can be conducted and how the required input data can be found and applied. These trades also indicate significant trends and the major influencing factors causing these trends.

In all of the cost data presented and discussed, the <u>costs</u> for development production, checkout and launch of the payload are omitted. Similarly, no costs are shown for payload or vehicle operations, such as down range tracking and communications, after vehicle liftoff from the launch pad.

5.1 COST EFFECTIVENESS OF STAGE AND PROGRAM OPTIONS

To show the application of the "modularized" cost data to the evaluation of the overall program cost and cost effectiveness, two different specific program types were defined and costed for both of the vehicle families (the MLLV and the AMLLV families), i.e.;

a. An "unbiased" program - For an unbiased program, the payload size and packaging is assumed to be flexible so it can be adapted to any of the possible vehicle configurations. (Payload size and packaging requirements do not bias the choice of the launch vehicle.) With an unbiased program the manufacturing facilities, test facilities, and the launch complex are sized for the specific vehicle configuration utilized to deliver the payload to orbit.

5.1 (Continued)

b. A "biased" program - For a biased program, any or all of the payload sizes are fixed and, therefore, bias the choice of the launch vehicle. For a biased program, the manufacturing facilities, test facilities and launch complex, therefore, are sized by the maximum size vehicle configuration necessary to deliver the largest specified payload package to orbit.

The resulting data (as discussed and shown below) indicate that the cost effectiveness choices of configurations for a specific program are not only dependent on the total quantity of payload to be launched, but on the bias created by specific fixed payload sizes.

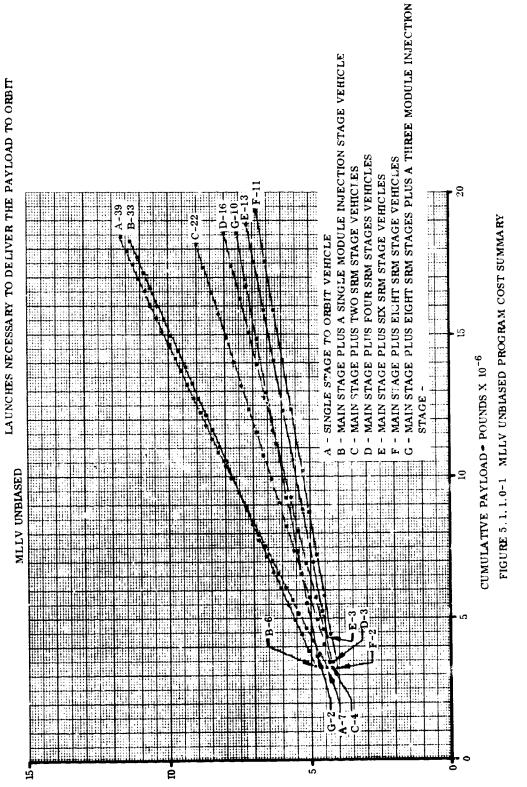
NOTE: For these analyses, a constant production and launch rate of two per year was assumed. Therefore, program duration will vary inversely with vehicle size.

5.1.1 MLLV Unbiased Program Cost Summary

To evaluate the most cost effective combination of MLLV stages for various required total quantities of delivered payload, the total program costs (including all non-recurring costs) for delivering between three million and eighteen million pounds of payload to a 100 NM orbit were determined. The plot of cumulative payload versus total program costs for various MLLV configurations is shown in Figure 5.1.1.0-1.

Each of the seven lines shown on the Figure 5.1.1.0-1 represents one specific vehicle configuration delivering the payload to orbit at a launch rate of two launches per year. The costs were developed based on providing manufacturing, test, launch and other supporting facilities for this manufacturing and launch rate. The specific points shown on each of the lines indicate specific payload increments that can be obtained with each of these configurations.

As shown, seven launches of the MLLV single stage to orbit vehicle are required to deliver three million pounds to a 100 NM orbit. With the same vehicle configuration 39 launches are required to deliver eighteen million pounds to orbit. Two launches of the vehicle configuration consisting of a main stage plus eight SRM stages and a three module injection stage are required to deliver three million pounds. To deliver eighteen million pounds, 10 launches of this larger configuration are required. The figure shows that the most costly ways to deliver the payload to orbit will be with the single stage to orbit vehicle configuration or the vehicle configuration consisting of a main stage plus a single module injection stage. The addition of an injection stage, however, will be a more cost effective option than the use of a single stage to orbit vehicle alone for programs requiring more than nine million pounds.



2 NUMBERS SHOWN TO THE RIGHT OF LETTER INDICATES THE NUMBER OF

1 PAYLOADS USED ARE FOR VEHICLES WITH THE MULTICHAMBER/PLUG

PROPULSION SYSTEM ON THE MAIN STAGE

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FIGURE 5.1.1.0-1 MLLV UNBIASED PROGRAM COST SUMMARY

TOTAL PROGRAM COST - DOLLARS IN BILLIONS

1	1	MAIN	HUUSANDS	' 1	1	1	MAIN
ITEM	SINGLE STAGE VEHICLE	STAGE + INJ. STAGE VEHICLE	MAIN STAGE + 2 SRM's VEHICLE	MAIN STAGE + 4 SRM's VEHIC LE	MAIN STAGE + 6 SRM's VEHICLE	MAIN STAGE + 8 SRM's VEHICLE	STAGE + (3M)1NJ, + 8 SRM's VEHICLE
"A" CATEGORY							
	\$1,104,636			\$1, 104,636	\$1,104,636		
INJECTION STAGE	0	197,740	0	0	0	0	198,450
SOLIDS	0	0	254,051				328, 441
"A" TOTAL	\$1,104,636	\$1,302,376	\$1,358,687	\$1, 382, 686	\$1,408,449	\$1,433,077	\$1,631,527
"B" CATEGORY	-						
MODEL TESTS	\$ 600	\$ 600	\$ 1,000	\$ 1,000	\$ 1,000	\$ 1,000	\$ 1,000
SYSTEMS TEST	120,000	140,000	120,000	120,000	120,000	120,000	140,000
SDF	73,200	80,415	77, 775	77,775	77,775	77, 775	1 1
MFG, DEV	9, 923	11,624	10,041	10,041	10,041	1	
ENGINE	325, 523	484, 994	442,639	442,439	442,639	442,639	602,110
STRUCT, DEV. & TEST	66, 420	77, 626	75, 049	75,049	75,049	75,049	96,845
DTV	53,104	65,104	71,612	71,612	71,612	71,612	97, 874
"F" & MOCK-UP	290, 712	316, 717	320, 931	320, 931	320, 931	320,931	373,162
R&D FLIGHTS	731, 826	802, 331	819, 126	856,626	892,726	928,126	1,048,831
"B" TOTAL	\$1,671,308	\$1, 979, 411	\$1,938,173	\$1,975,673	\$2,011,773	\$2,047,173	\$2,461,130
"C" CATEGORY							
MAIN STAGE	\$ 251,300	\$ 251,300	\$251,300	\$251,300	\$251,300	\$251,300	1
INJECTION STAGE	0	21, 400	0	0	0	0	42,600
SOLIDS	0	0	28,000	45,100	61,800	77,800	77,800
1ST OPERATIONAL VEHICLE (THIRD FLIGHT UNIT)		\$ 272,700				<u> </u>	
A + B	\$2, 775, 944	\$3, 281, 787	\$3,296,860	\$3, 358, 359	\$3, 420, 222	\$3,480,250	\$4, 092, 657
	251, 300	1 .		1		1	
A + B + C	\$3,027,244	\$3, 554, 487	\$3, 576, 160	\$3,654,759	\$3, 733, 322	2 \$3, 809, 350	54,464,357
PAYLOADS - VEHICLES WITH: MULTICHAMBER/PLUG WITH SINGLE POSITION NOZZLE ON MAIN STAGE	471,645	553, 593	824, 478	3 1,159,48	9 1,458,179	9 1,756,86	9 1, 851, 441
NUMBER OF LAUNCHES OF VEHICLES WITH MULTICHAMBE PLUG SINGLE POSITION NOZZLI ON MAIN STAGE REQUIRED FOR A PROGRAM OF :	ε						
3 MILIION	7	6	4	3	3	2	2
6 MILLION	13	11	8	6	5	4	4
12 MILLION	26	22	16	11	9	7	7
18 MILLION	39	33	22	16	13	11	10
LBS. TO 100 N.M. EARTH ORBIT	r						
	the second s						

TABLE 5, 1, 1, 0-1 MELV UNBIASED PROGRAM COSTS

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NO BIAS IN PROGRAM ELEMENTS (DOLLARS IN THOUSANDS)

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TABLE 5.1.1.0-II MLLV UNBIASED PROGRAM COST SUMMARY

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VEHICLE DESCRIPTION PAYLOAD/LAUNCH	NUMBER OF LAUNCHES	TOTAL PAYLOAD	PROGRAM COST (\$ IN MILLIONS)
	*2 + 7	3,301,543	4,474.3
Single Stage	$\frac{1}{2} + 13$	6,131,437	5,867.2
(471,649 lbs)	2 + 13 2 + 20	12,262,874	8,863.2
	2 + 20 2 + 39	18,394,311	11,665.8
	2 T 33	10,001,011	,
Main Stage	2 + 6	3,321,558	4, 865. 9
Plus a Single Module	-	-	-
Injection Stage	-	-	-
(553, 593 lbs)	2 + 33	18,268,569	11,459.9
Main Stage	2 + 4	3,297,912	4,389.7
Plus (2) SRM	-	-	
Stages	-	-	-
(824, 478 lbs)	2 + 22	18,138,516	8, 992.4
	0 / 0	3, 478, 467	4,233,9
Main Stage	2 + 3	5,410,401	_
Plus (4) SRM	-	_	-
Stages	$\frac{1}{2}$ + 16	- 18,551,824	7,940.1
(1,159,489 lbs)	2 + 10	10,001,0-1	
Main Stage	2 + 3	4, 374, 537	4,353.7
Plus (6) SRM	-	-	-
Stages	-	-	-
(1, 458, 179 lbs)	2 + 13	18,956,327	7,281.5
(_, _, _, _, _, _, _, _, _, _, _, _, _, _	,		
Main Stage	2 + 2	3, 513, 738	4,131.5
Plus (8) SRM	-	-	-
Stages	_	-	-
(1,756,869 lbs)	2 + 11	19,325,559	6,910.7
		0 700 000	4.825.4
Main Stage	2 + 2	3,702,882	5,540.5
Plus a Three Module	2 + 4	7,405,762	6,586,8
Injection Stage	2 + 7	12,960,087	7,616.2
Plus (8) SRM	2 + 10	18, 514, 410	(010 • 4
Stages			
(1,851,441 lbs)			

*(2) R&D Flights - Do not contribute to total payload

5.1.1 (Continued)

in a lesser number of launches and a lower program costs. (Assuming that the same launch rate can be maintained.) The lowest cost programs (over the payload range investigated) will utilize a vehicle consisting of a main stage plus eight strap-on SRM stages. A review of the cost data showed that the savings in recurring cost accrued for a single launch of such a vehicle will amortize the higher recurring cost required for its implementation. The use of the injection stage is not as cost effective as the use of strap-on SRM stages.

Table 5.1.1.0-I tabulates the data for the seven vehicles used in the unbiased MLLV program cost analysis. Get ready costs, development test costs, and first unit vehicle costs are shown. The payloads for each configuration are identified and the associated number of launches necessary to deliver various quantities of payload are shown.

Table 5.1.1.0-II shows a tabulation of the input data used to prepare Figure 5.1.1.0-1. Included in this table are the total program costs, total payload, and the number of launches necessary to place three million, six million, twelve million, and eighteen million pounds of payload into 100 NM orbit. Shown under the description of each of the vehicles in parenthesis are the payload capability associated with each of the vehicles.

5.1.2 MLLV Biased Program Cost Summary

In the unbiased program option discussed above, costs were determined for vehicles in which the manufacturing, test and launch facilities were specifically sized for a specific vehicle configuration. All of the payloads in the program were delivered by the same configuration. The representative MLLV biased program, discussed in this section, includes the requirement for placing one 1.85 million pound payload package in orbit with a single launch plus additional optional size payload packages. This requires one launch of a maximum payload vehicle configuration (main stage plus eight SRM stages plus a three module injection stage) coupled with launch of other optional vehicle configurations to deliver the remainder of the payload in the program. With this launch vehicle bias included, the total program costs for delivering between three and eighteen million pounds to a 100 NM orbit were determined. Figure 5.1.2.0-1 illustrates the total program costs versus the cumulative payload delivered to a 100 NM orbit for various MLLV configuration launch options.

As shown in Figure 5.1.2. 0-1 the most cost effective option is that which consists of one launch of the maximum payload vehicle coupled with the remainder of launches being conducted with vehicles consisting of a main stage plus eight SRM stages. This option is only slightly more cost effective than the option with continuous use of the maximum payload vehicle configuration. The other options will result in considerably more expensive programs. As would be expected, from the previous



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- 1 PAYLOADS USED ARE FOR VEHICLES WITH THE MULTICHAMBER/PLUG PROPULSION SYSTEM ON THE MAIN STAGE
- 2 ONE MAX PAYLO'D VEHICLE MUST BE ADDED TO NUMBERS SHOWN TO RIGHT OF LETT'ERS TO SHOW TOTAL NUMBER OF LAUNCHES REQUIRED

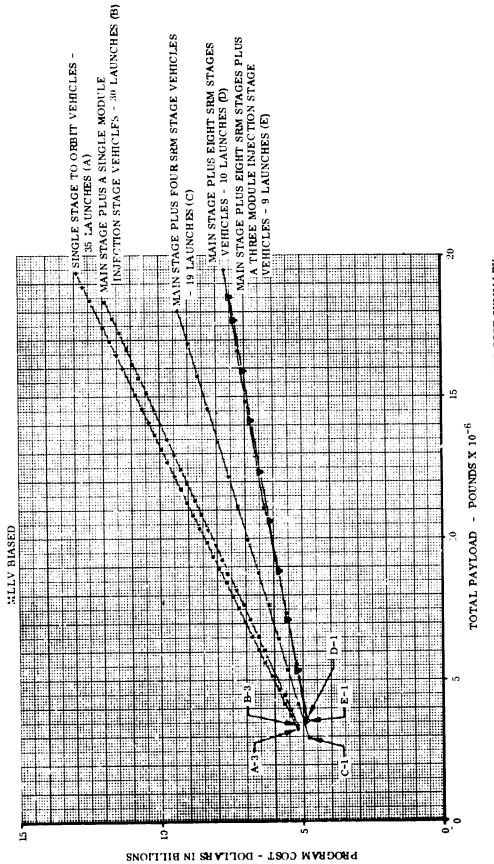


FIGURE 5.1.2.0-1 MILLV BLASED PROGRAM COST SUMMARY

FIGURE 5.1.2.0-1 MLLV BLASED PROGRAM COST SUMMARY

TABLE 5. 1. 2. 0-I PROGRAM	5. 1. 2. 0-1 MLLV BIASED PROGRAM COSTS PROGRAM REQUIRES 2 MAX. SIZE R&D FLIGHTS AND ONE MAX. SIZE OPERATIONAL FLIGHT (DOLLARS IN THOUSAND)	MLLV BIASED PROGRAM COSTS EQUIRES 2 MAX. SIZE R&D FLIG OPERATIONAL FLIGHT	RAM COSTS E R&D FLIC AL FLIGHT	HTS AND O DOLLARS	HTS AND ONE MAX. SIZE (DOLLARS IN THOUSANDS)	IZE (NDS)	MAIN STAGE +
ITEM	SINGLE STAGE VEHICLE	MAIN STAGE + INJ. STAGE VEHICLE	MAIN STAGE + 2 SRMS VEHICLE	MAIN STAGE + 4 SRMS VEHICLE	MAIN STAGE + 6 SRMS VEHICLE	MAIN STAGE + 8 SRMs VEHICLE	STAGE +8 SRMS VEHICLE
"A" CATEGORY MAIN STAGE INJECTION S'FAGE SOLIDS							1, 104, 636 198, 450 328 , 441
"A" TOTAL	1,631,527						1, 631, 527
"B" CATEGORY							
"B" TOTAL	2,461,130						- 2,461,130
"C" CA TEGORY MAIN STAGE	251, 300	251, 300	251, 300	251, 300	251, 300	251, 300	251, 300
INJECTION STAGE	-0-	21,400	-0-	-0-	-0- 61 800	-0- 77_800	42,600 77 800
SOLIDS	-0-		28,000	40, 100	000 1 0		
IST OPERATIONAL VEHICLE (THIRD FLIGHT UNIT)	251, 300	272,700	279, 300	296,400	313, 100	329,100	
A + F C	4, 092, 657 251, 300	4, 092, 657 272, 700	4, 092, 657 279, 300	4, 092, 657 296, 400	4,092,657 313,100 4,405,757	4, 092, 657 329, 100 4 421 757	4,092,657 371,700 4,464,357
$\mathbf{A} + \mathbf{B} + \mathbf{C}$	4, 343, 957	4, 365, 357	4, 371, 337	100 ,000 ,1	101 601 .		
PAYLOAD VEHICLE WITH MULTI- CHAMBER/ PLUC WITH SINGLE POSITION ON MAIN STAGE	I- 471,649	553 , 590	824,478	1, 159, 489	1,458,179	1,756,869	1,851,441
NUMBER OF LAUNCHES OF PROG REQUIRED FOR A PROGRAM (GRAM OPTION	on vehicles	ES				
3M	n	e	01			-	1
6M	5	œ	5	↔	÷	••	ر ه
12M	22	19	13	6	2	ల	9
18M	35	30	20	14	12	10	с.
LBS TO 100 N.M. EARTH ORBIT	L						

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VEHICLE DESC RIPTIO N PAYLOAD/LAUNCH	NUMBER OF LAUNCHES	TOTAL PAYLOAD (LBS)	PROGRAM COST (\$ IN MILLIONS)
Single Stage	* ** 2 + 1 + 3	3,266,388	5,196.4
(471,649 lbs)	2 + 1 + 35	18,359,156	12, 445. 3
Main Stage Plus a Single Module Injection Stage	2 + 1 + 3	3,452,220	5,257.4
(533, 593 lbs)	2 + 1 + 30	18,459,231	11,886.1
Main Stage Plus (4) SRM Stages	2 + 1 + 1	3,010,930	4,752.7
(1,159,489 lbs)	2 + 1 + 14	18,084,287	8, 332. 9
Main Stage Plus (8) SRM Stages	2 + 1 + 1	3,608,310	4,786.1
(1,756,869 lbs)	2 + 1 + 10	19, 420, 131	7,567.4
Main Stage Plus (3) Module Injection Stage Plus (8) SRM Stages	2 + 2 2 + 4 2 + 7 2 + 10	3,702,882 7,405,762 12,960,087 18,514,410	4,827.4 5,542.5 6,588.8 7,614.2
(1,851,441)			

TABLE 5.1.2.0-II MLLV BIASED PROGRAM SUMMARY

*(2) R&D flights - Do not contribute to total payload

**One payload of the maximum configuration

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5.1.2 (Continued)

enbiased program discussion, a single launch of the maximum payload vehicle configuration coupled with the remainder of the launches being conducted with single-stage-to-orbit vehicle configurations is the most expensive program option. The continued use of the injection stage after the launch of the maximum payload vehicle does not appear to be a cost effective option.

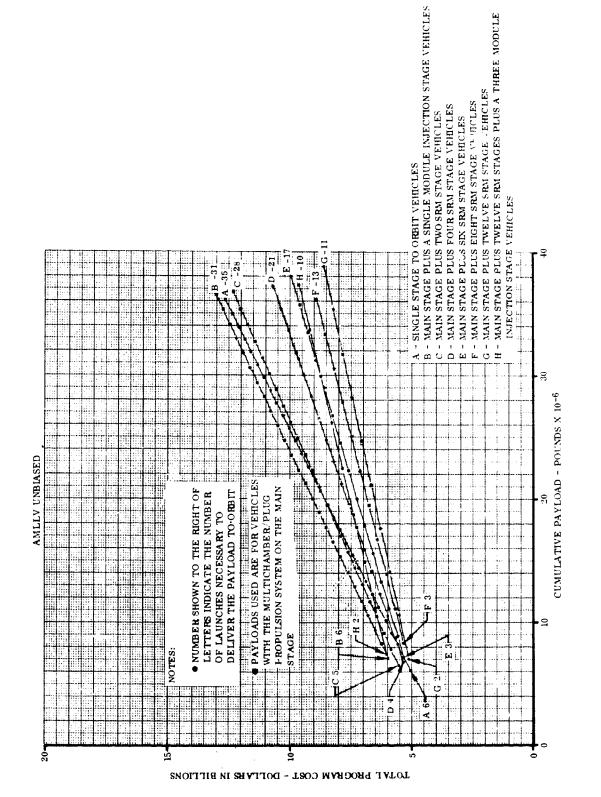
Table 5.1.2.0-I lists the input MLLV biased program costs including the "A" get ready costs, the "B" development test costs, and the "C" first unit costs. Since the biased program includes one launch of the maximum payload vehicle configuration, the "A" and the "B" program costs are constant and are the costs for the maximum payload vehicle regardless of what other vehicle configuration options are utilized for the remainder of the launch program. Also shown in this table are the payload capability of the vehicles. It was assumed for all of the vehicle configurations that the main stage would use the multichamber/plug propulsion system with the single position nozzle. The number of launches shown are those launches of the alternative vehicles which must be launched in addition to the maximum vehicle to deliver the payload weights indicated. To obtain the total number of launches in a specific program one maximum payload capability launch plus two R&D flights of the maximum payload vehicle must be added to the number shown.

Table 5.1.2. 0-II tabulates the program costs for the costs shown graphically in Figure 5.1.2.0-1.

5.1.3 AMLLV Unbiased Program Cost Summary

To evaluate the most cost effective combination of AMLLV stages for various required total quantities of delivered payload, the total program costs for delivering between six million and thirty-six million pounds of payload to a 100 NM orbit were determined. The plot of cumulative payload versus total program costs for various AMLLV configurations is shown in Figure 5.1.3.0-1.

As was observed with the MLLV unbiased program, the most cost effective vehicle (least program cost to put up total payload) is the configuration consisting of the main stage plus the maximum number of strap-on solid motor stages. The most expensive vehicle programs are those which use either the single stage to orbit vehicle or the main stage plus a single injection stage vehicle. The use of the injection stage does not become cost effective (when compared to the single stage to orbit vehicle) until approximately 28 million pounds are placed into orbit. Then it becomes slightly more effective than delivering the same payload with the single stage to orbit vehicle.



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IFEM "A" CAFFGORY MAIN STAGE 1%FCTION STAGE 1%FCTION STAGE SOLIDS "A" TOTAL "B" CATEGORY MODEL TESTS SYSTEMS FEST SDF	SINGLE STAGE VEHICLE 1,325,214 0 1,325,214 600 150,000 80,520	MAIN STAGE + A SINGLE MODULE INJ STAGE VEHICLF 1, 325, 214 248, 100 0 1,573, 314 600 175, 000 88, 457	MAIN STAGE + 2 SRM STAGE VEHICLE 1, 325, 214 0 273, 941 1, 599, 155 1,000 150,000 85, 553	MAIN STAGE + 1 SRM STAGE VEHICLE 1, 325, 214 0 299, 449 1, 624, 663 1, 000 150, 000 85, 553	MAIN STAGE + 6 SRM STAGE VEHICLE 1, 325, 214 0 324, 558 1, 649, 772 1, 000 156, 000 85, 553	MAIN STAGE + * SRM STAGE VEHICLE 1, 325, 214 0 349, 695 1, 674, 909 1, 000 150, 000 85, 553	MAIN STAGE + 10 SRM STAGE + VEHICLE 1, 325, 214 0 375, 157 1, 700, 371 1, 000 150, 000 85, 553 10	MAIN STAGE + 12 SRM STAGE VEHICLE 1, 325, 214 0 400, 332 1, 725, 546 1,000 150,000 85, 553	249,520 400,332 1,975,060 1,000 175,000 98,524
MFG. DEV.	9,923 192 995	11,624 733,738	10,149 630,763	10,049 630,763	10,049 630,762	10,049 630,763	10,049 630,763	10,049 630,763	11,750 871,506
ENGINES (AND/OR PFRT) Struct, dev. & test dtv	492,995 86,067 66,057	101,090 81,795	98,254 90,161	98,254 90,161	98,254 90,161	98,254 90,161	98,254 90,161	98,254 90,161	$129,261 \\ 125,511$
"F" & MOCK-UP	324,326	355,924	358,862	358,862	358,862 1,039,035	358,862 1,081,835	358,862 1,123,935	358,862 1,165,435	423,736 1,313,435
R&D FLIGHTS	836,735	<u>918, 141</u> 2, 466, 369	949,635	the second s	2,463,677		2, 548, 577	2,590,077	3, (49, 723
"B" TOTAL " <u>C" CATEGOR:</u> MAIN STAGE INJECTION STAGE	2,041,223 293,000 0	293,000 26,800	293, 000		293,000 0	293,000 0	293,000 6	293,000 0	293,000 54,700
SOLIDS	0	0	38,900	59, 800	79, 800	99, 500	118,600	137,500	137,500
IST OPERATIONAL VEHICLE (THIRD FLIGHT UNIT)	293,000	319, 800	331,900	352, 800	372,800	392,500	411,600	430,500	485,200
NON-RECURRING "A" + "B"	3, 372, 437	4, 039, 683	3, 973, 432	4, 044, 440	4,113,449	4,181,386	4,248,948	4, 315, 623	5,124,789
RECURRING "C" (ABOVE)	293,000	31 9, 800	331, 900	352, 800	372,800	392,500	411,600	430, 500	485,200
"A" + "B" + "C"	3, 665, 437	4, 359, 483	4, 305, 332	4,397,240	4,486,249	4,573,886	4,660,548	4, 746, 123	5,609,989
PAYLOAD VEHICLE WITH MULTICHAMBER/ PLUG ON MAIN STAGE VEHICLE WITH 2000 PSIA TOROIDAL/AEROSPIKE	1,028,887 980,652		1,310,000	1,770,000	2,230,000	2,780,000	3,180,000	3,527,290	3,737,738
NUMBER OF LAUNCHES OF A VEH WITH A MULTICHAMBER/FLUG SIN POSITION NOZZLE ON THE MAIN STAGE REQUIRED FOR A PROGRAM OF: 6M 12M 24M 36M LBS TO FARTH ORBIT		6 10 21 31	5 11 19 28	4 7 14 21	3 6 11 17	3 5 9 13	2 4 8 12	2 4 7 11	2 4 7 10

TABLE 5. 1. 3. 0-1 AMLLV UNBIASED PROGRAM COSTS (DOLLARS IN THOUSANDS) NO BIAS IN PROGRAM ELEMENTS MAIN STATE A

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TABLE 5.1.3.0-H AMLLV UNBIASED PROGRAM SUMMARY

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	NUMBER OF LAUNCHES	TOTAL PAYLOAD	PROGRAM COST (\$ IN MILLIONS)
	* 2 + 6 2 + 35	6,173,322 36,011,045	5,072.7 12,631.8
Main Stage Plus a Single Module Injection Stage	2 + 6	7,070,136	5,892.2
	2 + 31	36, 529, 036	12 , 998.6
Main Stage Plus (2) SRM Stages	2 + 5	6, 550, 000	5,566.6
(1, 310, 000)	2 + 28	36,680,000	12,340.2
Main Stage Plus (4) SRM Stages	2 + 4	7,080,000	5,407.6
(1, 770, 000)	2 + 21	37,170,000	10,830,4
Main Stage Plus (6) SRM Stages	2 + 3	6,690,000	5,201.3
(2, 230, 000)	2 + 17	37, 910, 000	9,922.2
Main Stage Plus (8) SRM Stages	2 + 3	8, 340, 000	5,327.1
(2, 780, 000)	2 + 13	36, 140, 000	8, 916. 9
Main Stage Plus (12) SRM Stagos	2 + 2	7,054,580	5,159.6
Stages (3, 527, 290)	2 + 11	38,800,190	8,750.6
Main Stage Plus a Three module Injection Stage Plus (12)	2 + 2	7,475,476	6,077.8
SRM Stages (3, 740, 000)	2 + 10	37, 377, 380	9,667.7

*(2) R&D flights - Do not contribute to total payload

5.1.3 (Continued)

Table 5.1.3.6-1 presents the AMLLV unbiased program costs. Shown on this table are nine vehicle configurations and the costs associated with the get ready, development test and first unit costs. The payload capabilities of each vehicle are shown. The main stage contains a multichamber/plug propulsion system with a single position nozzle. The total number of launches required for the range of program sizes is also shown.

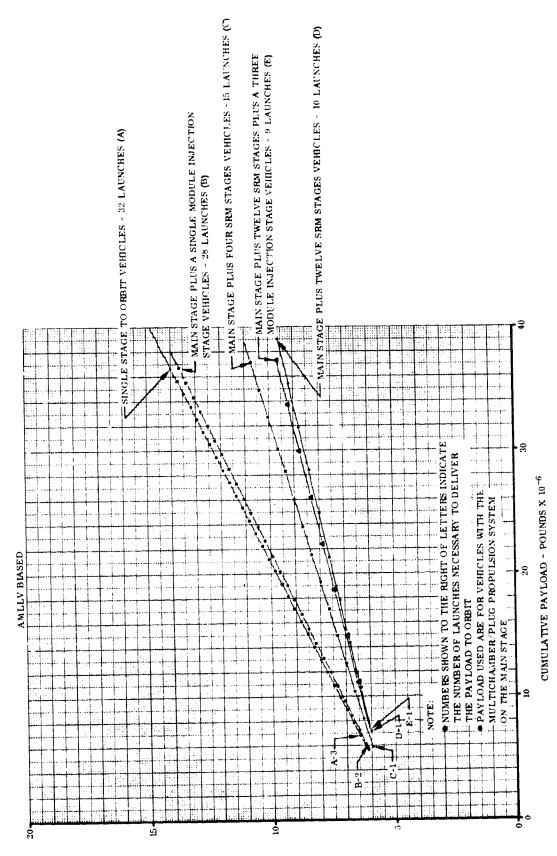
Table 5.1.3.0-II shows the program costs for the six million pound payload program and for the 36 million pound payload program for the nine vehicle configurations. The number of launches and the total payload placed into orbit by each of these configurations is also shown on this table. Two launches were included for the RND flight test. The payload that could be delivered by these R&D flight test vehicles was not included in the total payload capability shown.

5.1.4 AMLLV Biased Program Cost Summary

The representative AMLLV biased program, discussed in this section, includes the requirement for placing a singular 3.7 million pound payload package in orbit with a single launch. This requires one launch of a maximum payload configuration vehicle configuration coupled with launch of other optional vehicle configurations to deliver the remainder of the payload in the program. With this launch vehicle bias included, the total program costs for delivering between six and thirty-six million pounds to a 100 NM orbit were determined. Figure 5.1.4.0-1 illustrates the total program costs versus the cumulative payload delivered to a 100 NM orbit for various MLLV configuration launch options.

As shown in Figure 5.1.4.0-1, the lowest program cost option for the AMLLV biased program is the use of a vehicle consisting of a main stage plus 12 strap-on solid stages. Because of the program bias, the use of an injection stage is always more cost effective when compared to use of a single stage to orbit vehicle. In all instances, use of the vehicles without strap-on stages is considerably more expensive than use of those vehicle configurations utilizing strap-on SRM stages. Use of injection stages with vehicles having strap-on SRM stages will slightly increase program costs.

Table 5.1.4.0-1 shows the AMLLV biased program cost summary (with a multichamber/ plug engine system on the main stage). As the manufacturing test and launch facilities must be sized for the maximum vehicle configuration, the get ready cost and the development test cost are a constant (fixed) cost for any of the nine vehicle



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TOTAL PROGRAM COST - DOLLARS IN BILLIOUS

TABLE 5.1.4.0-1 AMLLV BIAS PROGRAM REQUIRES 2 MAX. SIZE	l. 4. 0-1 AM QUIRES 2 M	لعز	D PROGRAM	D PROGRAM CUS IS 2D FLIGHTS AND ONE MAX.	AX.	SIZE OPERATIONAL FLIGHT	VAL FLIGH	 	
ITEM	SINGLE STAGE VEHICLE	(D) MAIN STAGE A SINGLE MODULE INJECTION STAGE VEHICLE	OLLARS IN MAIN STAGE + 2 SRM STAGE VEHICLES	(DOLLARS IN THOUSANDS) E MAIN MAIN STAGE + STAGE + S N 2 SRM 4 SRM STAGE STAGE VEHICLE V) MAIN STAGE + 6 SRM STAGE VEHICLE	MAIN STAGE + 8 SRM STAGE VEHICLE	MAIN S FAGE + 10 SRM VEHICLE	MAIN STAGE + 12 SEM STAGE VEHICLE	ATIN STAGE • A THREE MODULE INJECTION STAGE + 12 SRM STAGE + 12 SRM
"A" CATEGORY MAIN STAGE INJECTION STAGE SOLDS									1, 325, 214 249, 520 40< 332
"A" TOTAL	1, 975, 066								1, 975, 066
"B" CATEGORY MODEL TESTS SYSTEMS TEST SDF MFG, DEV. ENGINES (OR PFRT) STRUCT, DEV. & TEST DTV "F" & MOCK-UP R&D FLIGHTS									1,000 175,000 98,524 11,750 871,506 129,261 129,261 129,261 123,736 1,313,435
'B" TOTAL	3, 149, 723								- 3, 149, (23
"C" CATEGORY MAIN STAGE INJECTION STAGE SOLIDS	293, 000	293, 000 26, 800	293 , 000 38, 900	293, 000 59, 806	293, 000 79, 800	293, 000 99, 500	293, 000 118, 600	293, 000 137, 500	293, 000 54, 700 137, 500
IST OPERATIONAL VEHICLE (THIRD FLIGHT UNIT)	293, 000	319,800	331,900	352,800	371,800	392,500	411,600	430,500	485,200
A+B C A+B+C	5, 103, 989 243, 000 5, 396, 989	5, 103, 989 319, 800 5, 423, 789	5, 103, 989 331, 900 5, 435, 889	5, 103, 989 352, 800 5, 456, 789	5, 103, 989 371, 800 5, 475, 789	5, 103, 989 392, 500 5, 496, 489	5, 103, 989 <u>411, 600</u> 5, 515, 589	5, 103, 989 430, 500 5, 534, 489	5, 124, 789 485, 200 5, 609, 989
PAYLOADS VEHICLE WITH MULTICHAMBER/ PLUG ON MAIN STAGE VEHICLE WITH TOROIDAL	1,028,887 980,652	1, 178, 356	1, 310, 000	1,770,000	2,230,000	2, 780, 000	3, 180,000	3, 527, 290	3, 737, 739
AEROSPIKE ON MAIN STAGE I AUNCHES OF VEHICLES WITH MULTICHAMBER/PLUG PROPULSION NUMBER OF LAUNCHES OF VEHICLES WITH MULTICHAMBER/PLUG PROPULSION SYSTEM ON MAIN STAGE REQUIRED FOR A PROGRAM OF	AUNCHES O DN MAIN ST	AUNCHES OF VEHICLES WITH MULTICHAMBER/ ON MAIN STAGE REQUIRED FOR A PROGRAM OF	S WITH MUI RED FOR A	TICHAMBE	R/PLUG PR DF	OPULSION		•	-
		c1 F	01 1-	e) 16	ণ ব			- ~	 ۲
24M 36M	32 0	81 81	9 %	51 61	10 13	<u>କ</u> ମ୍ର	- 1	y G	6 57
LBS TO EARTH ORBIT									

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TABLE 5.1.4.0-II AMLLV BIASED PROGRAM SUMMARY

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VEHICLE DESCRIPTION PAYLOAD/LAUNCH	NUMBER OF LAUNCHES	TOTAL PAYLOAD	PROGRAM COST (\$ IN MILLIONS)
Single Stage	** * 2 + 1 + 3	6, 824, 399	6,459.0
(1,028,878 lbs)	2 + 1 + 32	36, 662, 122	14,066.0
Main Stage Plus a Single	2 + 1 + 2	6,094,450	6,229,2
Injection Stage (1,178,356 lbs)	2 + 1 + 28	36,731,706	13,690,6
Main Stage Plus (6) SRM Stages	2 + 1 + 1	5, 967, 738	5,965.5
(2,230,000 lbs)	2 + 1 + 15	37,187,738	10,705.1
Main Stage Plus (12) SRM Stages	2 + 1 + 1	7,265,028	6 , 0 24. 5
(3, 527, 290 lbs)	2 + 1 + 10	39, 010, 638	9,605.1
Main Stage Plus a Three Module Injection Stage + (12) SRM Stages	2 + 2	7,475,476	6,077.8
(3, 740, 000 lbs)	2 + 10	37, 377, 380	9, 668. 7

*One payload of the largest configuration required

**(2) R&D flights of the largest configuration - does not contribute to total payload

5.1.4 (Continued)

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configurations shown. Only the production first unit cost varies with the vehicle configuration. Shown in this table are the payload capabilities of the vehicle with the multichamber/plug propulsion system with the single position nozzle on the first stage. Also shown on this chart are the number of launches required to deliver the six million, 12 million, 24 million, and 36 million pounds of payload to 100 NM orbit. The number of launches required as shown are the number of launches required of the vehicle options in addition to the two R&D flight tests of the maximum size vehicle configuration plus one operational launch of a maximum size vehicle.

Table 5.1.4.0-II presents the payload and program cost tabulations for the five vehicle configuration options presented in Figure 5.1.4.0-1. Note that no useful payload was considered from the two R&D flights.

5.1.5 Configuration Influence on Program Cost

This section summarizes the MLLV and AMLLV program cost data shown in the previous sections 5.1.1.0 through 5.1.4.0 to illustrate the effects of configuration selection on overall program cost. Figure 5.1.5.0-1 shows the total program cost for a representative program considering utilization of all of the AMLLV and MLLV vehicle configurations. The representative program shown includes development, implementation and operation of sufficient vehicles to deliver 20,000,000 pounds to a 100 N.M. earth orbit. All non-recurring and recurring program cost were included and there was no restriction on the sizes of the individual payloads. This figure shows that as the payload capability of the vehicle increases that the total program costs will generally decrease. For the size program shown, the maximum payload capability MLLV vehicle, however, is almost as cost effective as the maximum payload capability AMLLV vehicle and is more cost effective than the majority of the AMLLV configurations. As discussed earlier and shown on this figure, the use of the injection stage (as a propulsion unit to achieve orbit) is generally not cost effective. Similar analyses of other program sizes also showed that the use of the injection stage would never be the most cost effective option. For this reason, use of the injection stage, as a propulsive stage to achieve a 100 N.M. earth orbit, was no longer considered and excluded from further cost trades. The injection stage will be a useful stage for use in orbit and for missions beyond a 100 N.M. earth orbit. The injection stage should, therefore, be considered as part of the payload package rather than as part of the orbital injection vehicle.

The trends discussed above were biased by the size of the selected operational program relative to amortization of the non-recurring costs. Figure 5.1.5.0-2 shows the same type data for an operational program only (non-recurring cost excluded). This figure not only confirms the trends discussed above but leads to

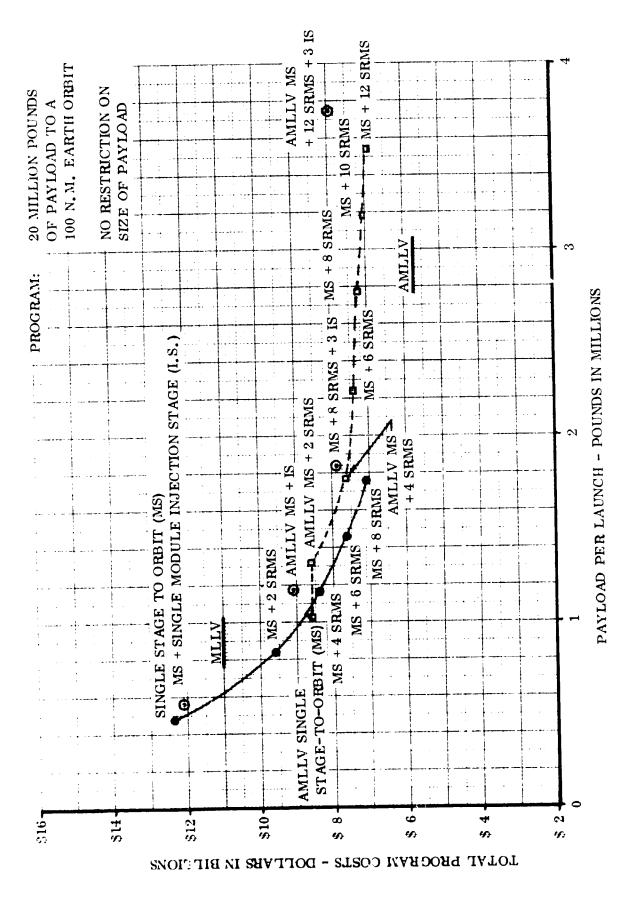


FIGURE 5.1.5.0-1 TOTAL PROGRAM COST VERSUS VEHICLE CONFIGURATION FOR UNBIASED PROGRAM

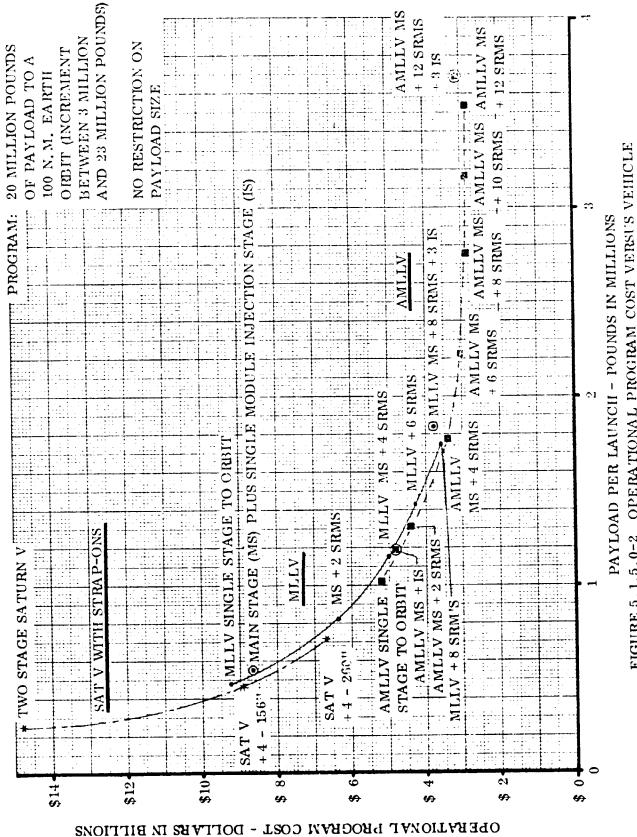


FIGURE 5.1.5.0-2 OPERATIONAL PROGRAM COST VERSUS VEHICLE CONFIGURA TION FOR UNBIASED PROGRAM

5.1.5 (Continued)

a significant conclusion, i.e.: for a given payload per launch requirement, recurring costs will not be significantly influenced by the choice of the launch vehicle configuration. For example, for a payload size requirement of approximately 1.8 million pounds per launch, either the MLLV main stage plus 8 strap-on stage vehicle or the AMLLV main stage plus 4 strap-on stage vehicle can be used for basically the same operational cost. Similarly, for a payload size requirement of approximately 1.2 million pounds, an MLLV main stage plus 4 strap-on stages vehicle or an AMLLV main stage plus injection stage vehicle can be used with no significant difference in operational program cost. To further confirm this effect, existing cost data for two stage Saturn V vehicles and for two stage Saturn V vehicles with either 4-156 inch or 4-260 inch diameter SRM strap-ons were normalized for a production and launch rate of two per year. This data, which are also shown in Figure 5.1.5.0-2, further indicate that for a specific payload per launch requirement, costs will be insensitive to configuration selection. For example, for a payload per launch requirement of 500,000 pounds, the MLLV single-stage-to-orbit vehicle or the Saturn V vehicle with four 156 inch SRM strap-ons can be used without a significant difference in cost.

As discussed above, for a given fixed payload per launch requirement, operational program costs will be insensitive to the choice of the launch vehicle configuration. A specific amount of energy, in whatever package, will cost the same amount. This conclusion assumes that all possible configurations will be produced and operated within the same program philosophy, limitations and ground rules.

The data in Figure 5.1.5.0-2 further shows that for increased payload per launch requirements, program cost will decrease. In other words, there appears to be a 'quantity discount' relative to size of the payload package. This ''quantity discount'' is based on the assumption that, whatever size vehicle is used, a production and launch rate of two vehicles per year can be maintained. The effect of this assumption on the ''quantity discount'' trend is further discussed in Section 5.1.6.

5.1.6 Rate Influence on Unit Cost

The cost effectiveness trades discussed in the preceding sections were accomplished assuming a production and launch rate of two vehicles per year. Prior experience with the Saturn V and other programs has shown that the cost of a launch vehicle is significantly effected by the production and launch rate. This launch rate/cost relationship is such that it could invalidate the trends indicated. The range of size of the vehicles considered is such that a common launch rate may not be applicable. If payload development time is a limiting factor, a program to launch a given weight of payload may require a minimum time for accomplishment. For example, a program to launch 20 million pounds of payload could require a minimum of ten years for accomplishment (two million pounds per year). This rate

5.1.6 (Continued)

limitation on payload would impose the following vehicle production and launch rates:

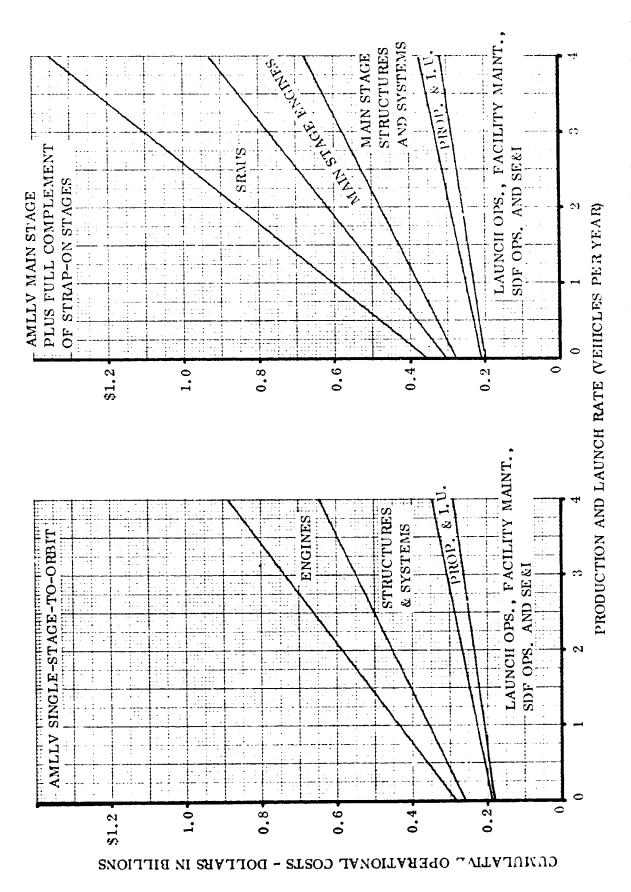
MLLV Single-Stage-To-Orbit	4.28 launches/yr
MLLV Main Stage Plus Eight Strap-Ons	1.14 launches/yr
AMLLV Single-Stage-To-Orbit	1.94 launches/yr
AMLLV Main Stage Plus Twelve Strap-Ons	0.57 launches/yr

If the unit costs for launch vehicles will be a function of the production and launch rate, a payload limitation on rate will reduce the costs of the smaller vehicles and increase the costs of the larger vehicles. To quantitatively evaluate the rate effect on unit cost, the following activities were accomplished:

- a. A review of the rate/unit cost sensitivity of Saturn V/S-IC costs as defined by the Chrysler National Space Booster Study, Contract NASW-1740 (1968) and by additional Boeing in-house studies.
- b. A review of the AMLLV/MLLV cost data to define the rate sensitive cost elements.

These reviews resulted in the data shown in Figure 5.1.6.0-1 and 5.1.6.0-2. Figure 5.1.6.0-1 shows cumulative annual recurring program costs as a function of launch rate. This data plus similar non-recurring cost data curves are shown on Figure 5.1.6.0-2. These latter curves show that the unit costs of the AMLLV/ MLLV vehicles will be strongly influenced by the production launch rate and show the appropriate factors to be applied to the individual vehicle costs to account for variations in the launch rate from the nominal of two per year.

Figure 5.1.6.0-3 shows how application of these launch rate cost bias factors would effect the results of the program and configuration cost effectiveness studies shown on the preceding Figure 5.1.5.0-2. This figure proposes another significant study conclusion, i.e.: choice of vehicle configuration for any size payload per launch requirement will not significantly effect program costs. The rate bias on costs, as shown on this figure, neutralizes the indicated reduced costs for the larger payload vehicles (neutralizes the "quantity discount" effect). Figure 5.1.6.0-4 shows a matrix of operational costs versus vehicle size (payload per launch) as a function of either various fixed launch rates or variable fixed rates of payload launched per year. This data shows that the above conclusion basically holds for any required quantity of payload per year. There are, however, some minor cost advantages for selection of specific size vehicles for specific payload per year requirements. For example: for a payload per year requirement of 2.0 million pounds, the least expensive vehicle would be that configuration with approximately 2 million pounds of payload capability. Choice of either larger or smaller vehicles would tend to increase the operational program costs. Similarly,



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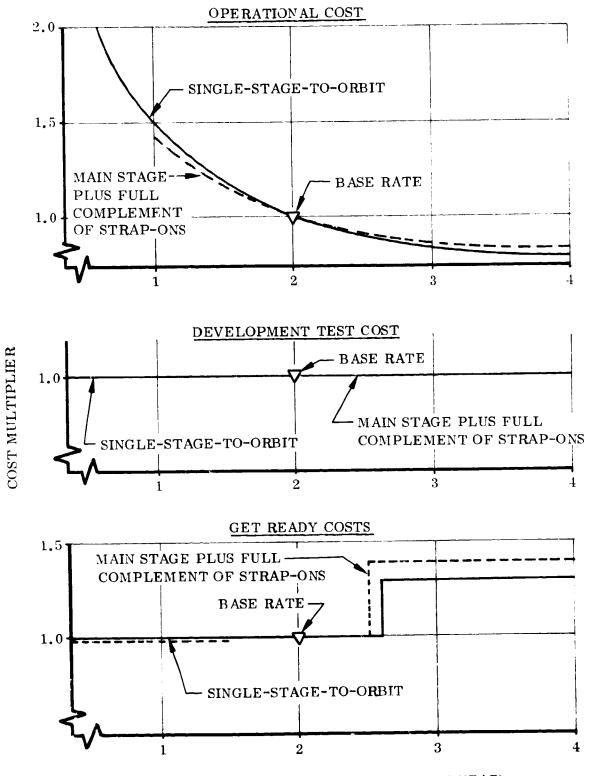
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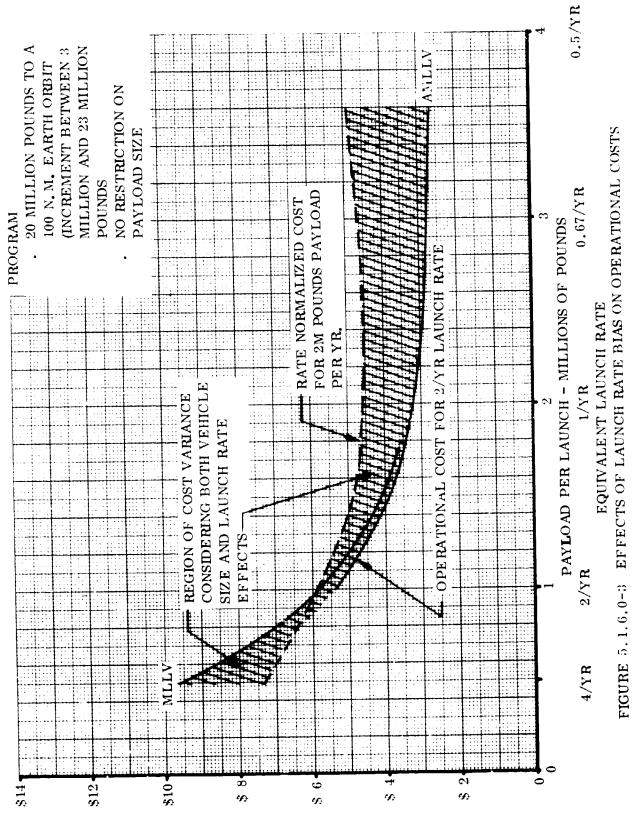


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PRODUCTION AND LAUNCH RATE (UNITS PER YEAR)

FIGURE 5.1.6.0-2 PRODUCTION AND LAUNCH RATE EFFECTS ON COSTS



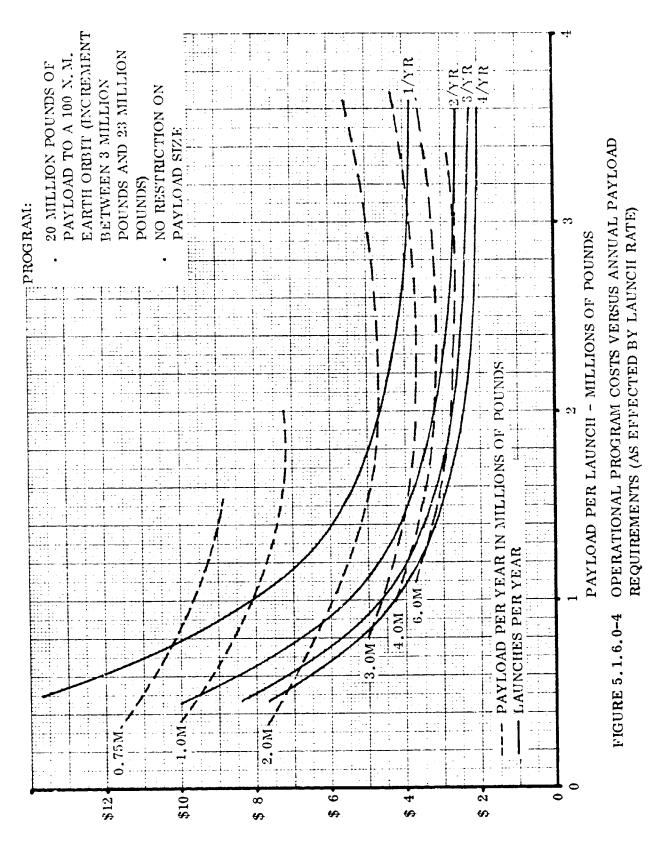
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OPERATIONAL PROGRAM COSTS - DOLLARS IN BILLIOUS



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OPERATIONAL PROCRAM COST - DOLLARS IN BILLIONS

Continued)

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rograms which require larger quantities of payload per year will have lower costs if they utilize vehicles with payload capabilities of slighly in excess of 2.0M pounce.

The data shown on the aforementioned figures, while indicative of trenes, should not be applied directly for quantitative comparisons. For lower launch rates, modifications of operational procedures and philosophy could reduce the rate impact on cost.

D.2 PERFORMANCE/COST POTENTIAL OF ENGINE OPTIONS

In the previously completed AMLLV study (Contract NAS2-4079), two different propulsion systems were evaluated for application to the main stage, i.e.: 1) the high pressure multichamber/plug propulsion system and 2) the 2000 psia toroidal/aerospike propulsion system. The propulsion system alternatives investig ted for the MLLV main stage, in this study, were:

- a. The high pressure multichamber/plug propulsion system with a single position nozzle.
- b. A high pressure multichamber/plug propulsion system with a two position nozzle.
- c. The 2000 psia chamber pressure toroidal/aerospike with 8 modules (each producing one million pounds of thrust).
- d. A 1200 psia chamber pressure toroidal/aerospike with 28 modules (each producing 286,000 pounds of thrust).
- e. A 1200 psia toroidal/aerospike with 8 modules (each producing one million pounds of thrust).

The performance analyses of these various propulsion system options are presented in Volume II. In general, the multichamber/plug propulsion systems will provide the highest engine performance while the toroidal/aerospike propulsion systems will have the lowest weight. As a result of vehicle payload performance analyses, it was determined that the 2000 psia (high pressure) toroidal/aerospike engine will provide the best compromise between engine performance and engine weight. The use of either high pressure multichamber/plug or the 1200 psia (low pressure) toroidal/aerospike propulsion systems will result in lower vehicle payload capability.

This section reviews the performance data relative to the costs of the various engine systems to assess the performance/cost potential of the engine options. Section 2.2.1 assesses the relationship to program cost of the module size of the AMLLV

5.2 (Continued)

2000 psi toroidal/aerospike engine. Section 5.2.2 assesses relationship to program cost of the module size and chamber pressure of the MLLV toroidal/ aerospike. Section 5.2.3 analyzes the relationship to program cost of the AMLLV multichamber/plug module size.

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The multichamber/plug propulsion system costs were provided to The Boeing Company by the Pratt and Whitney Division of United Aircraft Corporation. The toroidal/aerospike propulsion system costs were supplied by the Rocketdyne Division of North American Rockwell Corporation.

5.2.1 Effects of AMLLV Toroidal/Aerospike Engine Module Size on Program Cost

The get ready, development test, and first unit costs for the toroidal/aerospike propulsion system were provided for two different 2000 psia toroidal/aerospike propulsion systems: 1) an eight module system with a total thrust of 16 million pounds (two million pounds thrust per module), and 2) a sixteen module system with a total thrust of 16,000,000 pounds (one million pounds thrust per module).

Figure 5.2.1.0-1 illustrates program costs relative to quantity of operational payload delivered to a 100 nautical mile orbit by various AMLLV configurations employing the two different engine module sizes. The costs for the single-stageto-orbit vehicle indicate that use of the smaller module (one million pound thrust module) will result in slightly lower program costs for small quantities of operational payload than will the use of the propulsion system with the two million pound thrust module. As the amount of payload to be delivered to orbit is increased beyond approximately twelve million pounds use of the larger module will, however, become more economical.

Two other vehicle configurations are also shown: 1) an AMLLV vehicle consisting of a main stage plus six SRM strap-on stages and 2) an AMLLV vehicle consisting of a main stage plus 12 SRM stages. Each of these configurations were also costed with the eight two million pound thrust module and the sixteen one million pound thrust toroidal/aerospike propulsion system. In both instances, the costs for the vehicles with the two million pound modules will be initially slightly higher than those of the vehicles with the one million pound modules. The two million pound module vehicles will become more cost effective as the required total payload increases beyond 27 and 42 million pounds for the main stages plus six SRM vehicles and the main stage plus twelve SRM vehicles, respectively.

Use of either the larger or smaller modules will not significantly effect the overall program cost. The costs of the two million pound module toroidal/ acrospike propulsion system for any configuration will be 68 million dollar.

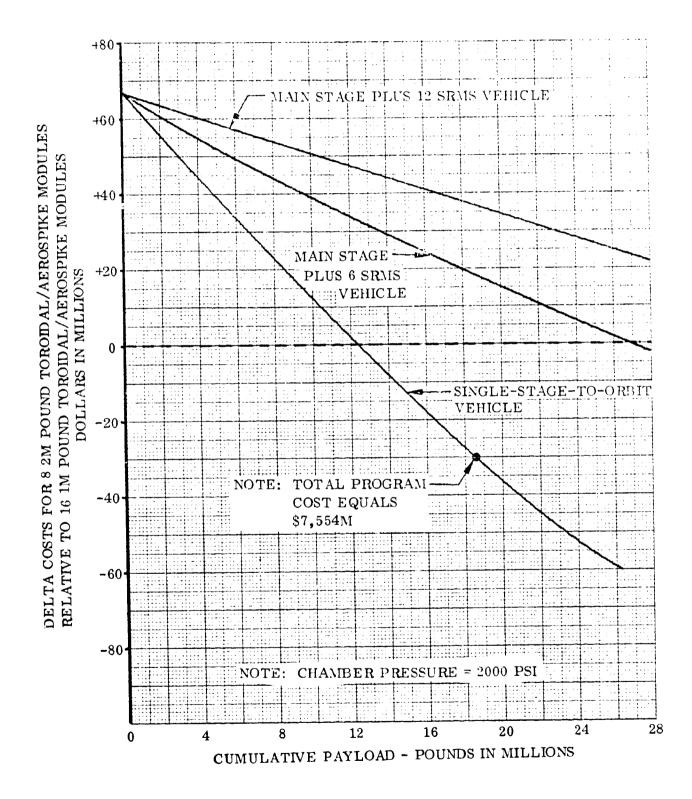


FIGURE 5.2.1.0-1

RELATIVE PROGRAM COSTS FOR AMLLV CONFIGURATIONS WITH TOROIDAL/AEROSPIKE PROPULSION SYSTEM OPTIONS ON THE MAIN STAGE

5.2.1. (Continued)

greater than that of the one million pound module thrust toroidal/aerospike propulsion system during the get ready and the development test phases. This difference will be amortized by the lower production cost of the two million pound thrust modules such that the larger modules become more cost effective for the larger programs. The program cost savings attributable to use of the larger modules will be approximately 30 million dollars for a program consisting of 18 launches of the AMLLV single-stage-to-orbit vehicle. This saving will represent a total program cost saving, however, of only 0.4 percent as the overall program cost for development and launch of 18 operational vehicles will be 7,554 million dollars. ſ

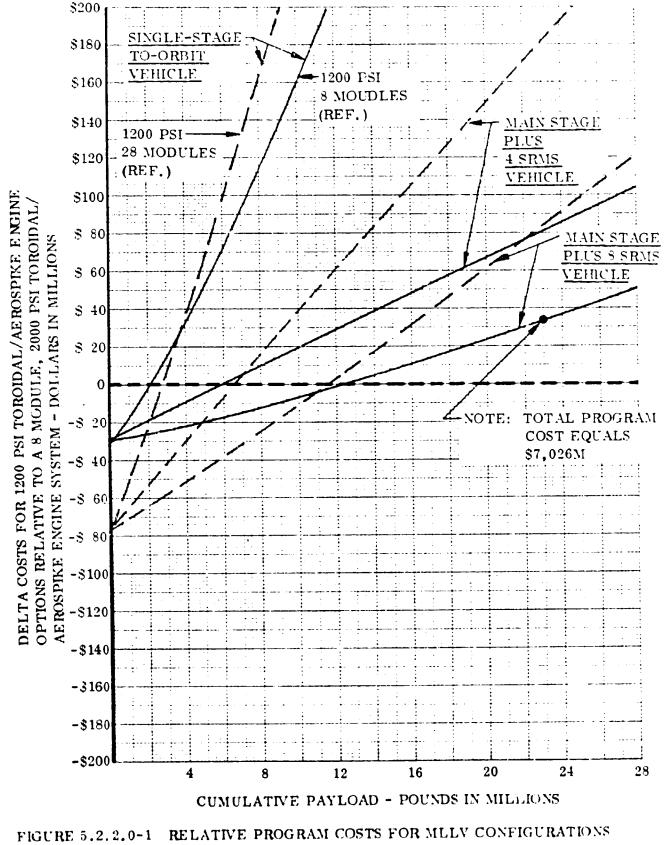
5.2.2 Effect of MLLV Toroidal/Aerospike Engine Module Size and Chamber Pressure on Program Costs

The three different toroidal/aerospike engine systems investigated for the main stage of the half size MLLV vehicle were:

- a. A 2000 psia chamber pressure system with eight modules, each producing one million pounds of thrust.
- b. A 1200 psia chamber pressure system with eight modules, each producing one million pounds of thrust.
- c. A 1200 psia chamber pressure system with 28 modules, each producing 286,000 pounds of thrust.

Figure 5.2.2.0-1 shows relative total program cost as a function of the cumulative amount of payload delivered to 100 NM earth orbit for three different MLLV configurations for the three engine systems. The configurations shown are (1) a single-stage-to-orbit vehicle, (2) a vehicle consisting of a main stage plus four strap-on stages and (3) a vehicle consisting of a main stage plus eight strap-on stages.

For all of the three vehicle configurations, the differences in costs attributable to the various engine systems employed on the main stage will be only a minor portion of the overall program costs. With the single-stage-to-orbit vehicle, the 1200 psia engine systems will be the more cost effective for programs with total payload requirements of less than two to three million pounds. Beyond this point, the 2000 psi toroidal/aerospike propulsion system will be more cost effective. While the 1200 psia propulsion system can use existing J-2 turbo pump technology, the higher performance that can be obtained with the 2000 psi propulsion system will soon offset the higher costs required for development of the new turbo machinery. Similar trends, which favor the 2000 psi engine system, are shown for the configurations employing strap-on SRM stages.



with TOROIDAL/ AEROSPIKE PROPULSION SYSTEM OPTIONS ON MAIN STAGE

5.2.2 (Continued)

Compared to the 28 module 1200 psia system, the reduced production cost attributable to the larger module size will give the 8 module 1200 psia engine system a cost advantage.

The single-stage-to-orbit configurations will be more cost sensitive to the engine options than will be configurations employing strap-on stages. Overall program costs, in any case, however, will not be significantly effected. For example, a program cost differential of \$200 million dollars between engine options for the single-stage-to-orbit vehicle will represent a change in total program costs of approximately 2.4 percent.

5.2.3 Effects of Multichamber/Plug Module Size on Costs

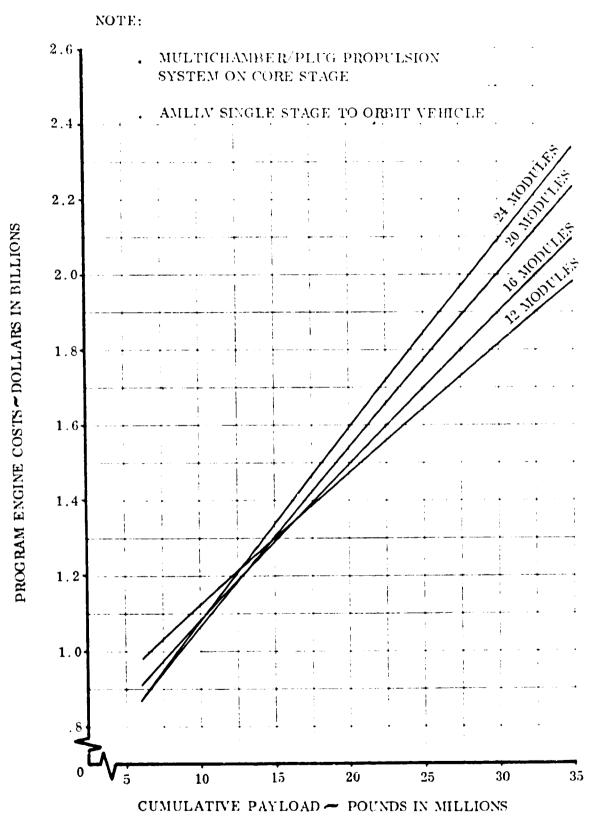
During the AMLLV study program, the multichamber/plug module size effects on engine performance and weight were investigated. Some degradation in the amount of payload delivered to orbit by the single-stage-to-orbit vehicle was shown to occur as the engine module size was increased (with total stage thrust held constant). This decrease was due 1) to the increased stage structural weight required to react the more concentrated engine thrust loads and 2) the sea level effects of the required overespanded nozzle.

It would, therefore, be advantageous from the performance standpoint to have as many modules as possible. Cost trades were conducted, considering the AMLLV single-stage-to-orbit, the number of modules to optimize cost/ performance. Figure 5.2.3.0-1 shows that the overall program costs for engine systems incorporating the larger modules generally will be slightly less than those of engine systems with the smaller modules. While the non-recurring costs of engines with smaller modules will be considerably less than those of engines with larger modules, the production costs will be less for the engines with the larger modules.

5.3 STRAP-ON STAGE CONFIGURATION PERFORMANCE COST TRADES

In the prior AMLLV study, the payload capability of the core vehicle was found to be significantly increased through the utilization of strap-on stages. The vehicle performance with both liquid propellant strap-on stages and solid rocket moter (SRM) strap-on stages was investigated. The strap-on stage diameter and amount of propellant carried in these stages as well as the number of stages were investigated.

For the MLLV half size vehicle configuration investigated in this current study activity, only SRM strap-on stages were investigated. Strap-on stage



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FIGURE 5.2.3.0-1 PROPULSION SYSTEM PROGRAM COSTS FOR VARIABLE NUMBER OF MODULES

5.3 (Continued)

diameters of 156 and 260 inches and the method of staging these SRM strap-on stages were examined. This performance trades activity is reported in Volume II.

This section reports the results of performance/cost trades relative to size, type and staging sequence of strap-on stage propulsion systems,

5.3.1 Liquid Propellant Strap-On Stages vs., Solid Rocket Motor (SRM) Stages

The liquid propellant strap-on stages are an alternative for the solid rocket motor (SRM) stages. For the purpose of this comparison, it was assumed that the costs for development, test and manufacture of the liquid stage would be the same as those for the SRM stage. The comparison of the liquid strap-on stage to the SRM stage was, therefore, based on relating comparable postmanufacturing tests, procedures and operations. The liquid propellant strap-on stages for this comparison were assumed to be 260 inches in diameter.

The SRM stage is described from development through manufacture and usage in Volume III, paragraph 4.2.9 - SRM Development Tests, paragraph 4.2.10 - Flight Tests, Section 5.4 - SRM Manufacturing Plan and Section 7.0 - Launch Plan.

Table 5.3.1.0-1 outlines the processing of the SRM stage and a comparable liquid stage from the manufacturing site to the launch facility and through launch. Costs for most of the operations will be similar for the two stages, and are not listed. Where substantial differences will exist, either in "get ready" non-recurring costs or operating and maintenance recurring costs, these costs are noted. The prime assumption is as stated above that the costs of the two stages, upon reaching the manufacturing facility dock site, will be equal. This includes the cost of the liquid fuel for the liquid stages. Major differences occurring in processing after this established baseline, are noted as delta costs.

Weights will be a factor in transporation and handling costs. The 260 inch SRM stage for the full size AMLLV will weigh approximately 4,200,000 pounds, while the dry weight of a comparable liquid stage will be approximately 172,000 pounds. Storage requirements at the launch site will also affect transportation and handling costs. The weight and safety requirements of the SRM stages dictate that they will remain on the barge, moored in a protected location until needed for launch.

Recurring processing costs for the two configurations will differ very little, and will be generally more or less compensating. An exception is the increased TABLE V. B. P. OF. SEM STAGE VERSUS LIQUID PROPELLANT STRAPON STAGE POST-MANUFACTURING TO LAUNCH COST COMPARISONS

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rtorn.	l∿rform Marceiving [nspection on Marge		Same		3 Unload Stage Onto Pad W. Crane Hoist	1.510
ы 2	score on Barge I ntil Bequired on Liquid Stage		•		 Transfer to Shop Area & Conduct Receiving Inspection. 	Accessing inspection.
र विकास	Unload SRM from Barge onto Pad W. Roll Hamp Actuators				. Store и Pad Storkki Ата	
vit nie	Move to Ganter Create to Romation slip 6. Romate		-		e. Mowe to Silo and Insert for Vehicle Stacking	- Stacking
07 - 10	Nove to Sido and Insert				 Align Stage and Attach to Main Stage 	
Kn S	Align SRM Stage and Attach to Core Stage				 Vehicle Integration, 2x - 4x4 wheekov 	ь О.:-
-li÷	Vehicle Integration, Test and Checkout				9 CDD - Fueling and Defueling Operations	ration.
100.)			-		10. Prepare for Launch - Countdown Sequence	equence.
1.1951-1	Pressre for Launch - Countdown Sequence				11 Launch	
q.umerj			Same			
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			(246,000)	246, 000	3. Tow Vehicles A Required	
L L L	Cantry Equipment and Enloading Crane For SRM Stages	000,155,000	17,135,000	12,000,000	4. Gantin Crane W. O.SRM Londs	
ropril	Propeilant Storage & Distribution	53,250,000	(000,000),11,	100,250,000	 Propellant Storage, etc. Increased for Loguid Stages 	for Logued Stages
	DELTA TOTAL FOR NOV-RECURNING COSTS		-100 67 0 12			

5.3.1 (Continued)

SRM transportation costs which are attributable to the requirement to store the SRM stages on the barges until all the stages have been received, and the vehicle is scheduled for launch. This will necessitate one barge for each SRM stage, plus one spare. (Only two liquid strap-on stage barges will be required, as liquid stages will be off loaded immediately upon arrival at the launch facility. The two barges can each make two round trips per month, if required.) The SRM barge operating and maintenance costs for each launch cycle of six months will exceed the liquid stage barge operating and maintenance costs by \$95,000.

The initial non-recurring costs of the 13 SRM stage barges will be \$20,816,000 more than the cost of the two liquid stage barges.

It will take more time and equipment to lift the heavier SRM stages. This difference will be partially compensated for by the fact that the SRM stage will undergo only one handling sequence after barge off-loading and will be placed directly in the silo for mating to the main stage. The liquid strap-on stages will first go to the receiving area on the pad, and then will be placed in a subterranean storage room on the pad until needed for stacking the vehicle. While the operating costs of handling the SRM's and the liquid stage on the launch pad will, therefore, be approximately the same, there will be a \$10,610,000 additional cost for the larger gantry required to lift and transport the SRM stages.

Propollant storage and distribution capacities must be increased at the launch facility, if liquid propellant stages are to be used. The cost of a Hitional fuel storage barges, pumping and distribution facilities is estimated at \$17,000,000.

As shown (considering the prime assumption), these differences will result in an approximate \$17M (1.37) savings in the AMLLV non-recurring get ready costs attributable to use of the liquid strap-on stages. Similarly, the recurring costs for the AMLLV maximum payload vehicle would be reduced by \$95K (0.027).

5.3.2 Dollars Available for Strap-On Stage Options

The strap-on stage options investigated during the AMLLV and MLLV vehicle conceptual design studies were the 260 inch and the 156 inch solid propellant rocket motor stages, and the 260 inch liquid propellant strap-on stages.

Costs for the entire SRM stage program were developed for both the AMLLV and MLLV. These costs include the costs of design, development and test, facilities, manufacture, transportation, and launch costs.

A summary of all costs associated with the 260" SRM stage, from drawing board to launch pad, appear in Figures 5.3.2.0-1 and 5.3.2.0-2 as dollars available for AMLLV or MLLV strap-on stage options. These figures contain individual data for specific program sizes considering the maximum payload vehicles.

(2 OPERATIONAL) (6 OPERATIONAL) (10 OPERATIONAL) (14 OPERATIONAL 52.5 M. LBS. 16 FLIGHTS OTHER s 614,486 1,830,662 165,400 2,610,548 \$ 9,889,685 7,279,137 SRM VEHICLE - 3.75 M LBS PAYLOAD PER LAUNCH 37.5 M. LBS. 12 FLIGHTS \$ 8,346,340 OTHER s 614,486 1,401,917 133,800 2,150,203 6, 196, 137 *** DOLLARS AVAILABLE FOR STRAP-ON STAGES, SOLID OR LIQUID FUELED SRM BASIS - MAIN STAGE PLUS TWELVE SRM STAGE DOLLARS IN THOUSANDS 22.5 M. LBS. **THER** \$6,782,598 SRM **8 FLIGHTS** 614,486 962,285 102,200 5,103,537 1,678,971 LAUNCH) CLARGEAELE TO SRM'S. (RECURING) a sum server and a construction of the server and the server and S: 7.5 M. LBS. \$5,150,623 4 FLIGHTS s 614,486 505,400 70, 100 3,960,137 1,190,486 OTHER SRM \$4,315,623 \$ 614,486 273,900 54,800 94:3, 186 3, 372, 437 OTHER SRM KIWIW.1G 2 R&D 12.0] 10.0s. 0 -6.01 10.7 2.0-: | Vehicle Totais (Less SRM's) Totals SRM Non-Recurring Costs PAYLOAD IN MILLIONS PROCRAM COSTS SNOFTIN NI AMLLV FLIGHTS DOLLARS GRAND TOTAL AMLLV OF POUNDS -Wars *** н.) ** 'ن ب

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** C_{F} : COST OF FACILITIES (MANUFACTURING, TRANSPORTATION, TEST AND

+ $c_{\rm S}$ = COST OF SOLID ROCKET MOTOR STRAP-ON STAGES (RECURRING)

FIGURE 5, 3, 2, 0+1 DOLLARS AVAILABLE FOR AMILY STRAP-ON STAGES

· C_S COST OF SOLID ROCALET - JOFOR STRAP-ON STAGES (RECURRING)

- •• C_F == 0ST OF FACILITIES (MANUFACTORING, TRANSPORTATION, TEST AND LAUNCH) CHARGEABLE TO SRAPS. (RECURRING = 0&M)
 - +++ DOLLARE AVAILABLE FOR STRAP-ON STAGES, SOLID OR LIQUID FUELED

PROGRAM COSTS 10. 0-	BASIS:	MAIN STAGE PLUS EIGHT SRM STAGE VEHICLE 1.757 MLBS PAYLOAD PER LAUNCH	D PER LAUNCH		
S				SRM	SRM
SN			SRM		
	OTHER	SRM OTHER	OTHER	OTHER	OTHER
MLLV FLIGHTS PAYLOAD IN MILLIONS OF LBS	2 R&D DUMMY	4 FLJGHTS (2 OPERATIONAL) 3.70 M. LBS.	4 FLIGHTS 8 FLIGHTS 12 FLIGHTS 16 FLIGHTS 16 FLIGHTS (2 OPERATIONAL) (6 OPERATIONAL) (10 OPERATIONAL) (14 OPERATIONAL) 3.70 M. LBS. 11.10 M. LBS. 18.50 M. LBS. 26.90 M. LBS.	12 FLIGHTS (10 OPERATIONAL 18.50 M. LBS.	16 FLIGHTS 0(14 OPERATIONA 26, 90 M. 1.JJS.
MLLN UNTS			SUNVERSION SUPPORT	S(I)	
SRM Non-Recurring Costs *SRM C ₅ Costs **SRM C _F Costs *** SRM Totals Vehicle Totals (Less SRMs)	<pre>\$ 507,446 155,660 41,200 704,306 2,775,944</pre>	\$ 507,446 285,500 54,200 847,146 3,283,818	8 507,446 544,100 80,200 1,131,746 4,256,318	\$ 507, 446 793,000 106, 200 1,406, 646 5, 826, 918	\$ 507,446 1,035,700 132,200 1,675,346 6,131,718
GRAND TOTAL	\$3,480,250	<u>84,1:30,964</u>	<u>\$5,388,064</u>	<u>87,233,564</u>	<u>S_7,807,664</u>

FIGURE 5, 3, 2, 0-2 DOLLARS AVAILABLE FOR MLLV STRAP-ON STAGES

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Each MLLV or AMLLV vehicle as costed has a main stage and a full compliment of SRM strap-ons; e.g., 8 for the MLLV and 12 for the AMLLV.

The tables appearing on each figure show the total program costs (less SRM's), the SRM strap-on stage non-recurring costs and the SRM strap-on stage recurring (C_s and C_F) costs. The totals of the SRM stage costs appears on the table and on each bar on the bar charts. These SRM totals (as designated by a triple asterisk) represents amounts available within each program for implementation and operation of any alternative strap-on stage.

5.3.3Cost Comparison of MLLV Vehicle Configuration with Strap-On156 Inch or 260 Inch SRM Strap-On Options

During the MLLV half size vehicle conceptual design study activity as reported in Volume II of this final report, it was concluded that the 156 inch strap-on stage with one half the thrust level and one half the propellant weight of the 260 inch SRM stage would be an acceptable option for the MLLV strap-on family. Twice the number of strap-on stages would be required for the maximum vehicle configuration with the 156 inch SRM's as required for that with the 260 inch SRM stages.

In Volume III, Resources Implications, a comparison was made of the method of transportation of the 156 inch motor segments to the launch site versus delivery of the completed 156 inch stage. The various launch operational procedures and sequence options for the 156 inch stage were also analyzed. The transportation and facility requirements were identified. This data, coupled with cost data obtained for 156 inch strap-on motors by Boeing and other contractors on previous studies provided the input data for the cost comparison.

Table 5.3.3.0-I shows comparable costs for get ready and development test costs associated with the 260 inch and 156 inch MLLV SRM strap-on stages.

The <u>fixed</u> get ready costs for the 156 inch SRM stage will be approximately \$45,000,000 less than those shown for the 260 inch SRM stage. The principal cost differences will be due to:

- a. Slightly reduced launch complex facility costs. These will be the result of lower cost handling and lifting devices required for the 156" SRM segments. (These segments weigh less than one half million pounds per segment versus the approximate three and one half million pounds of the monolithic 260 inch SRM stages.)
- b. Reduced SRM facility and tooling costs. Approximately \$19,000,000 less will be required for the 156 inch SRM stage. As the 260 inch SRM stage will be delivered as a complete stage versus the 156 inch motor being

TABLE 5.3.3.0-I GET READY AND DEVELOPMENT TEST COSTS FOR MLLV CONFIGURATION WITH EIGHT 260" SRM STRAP-ON STAGES VERSUS SIXTEEN 156" SRM STRAP-ON STAGES (DOLLARS IN THOUSANDS)

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FUNCTION OR COMPONENT	156" SRM STAGE	260'' SRM STAGE
Fixed Get Ready Costs		
GSE	3 3,100	8 3,072
Michoud Facility	7,420	8,434
Launch Complex Facility	151,000	162,470
SRM Facility and Tooling		
Plus Design	25,000	44,131
Stage Structure Design		
and Tooling	19,500	32,745
Forward Skirt	19,729	19,729
Subtotal	225,749	270,581
Quantity Sensitive - Get Ready Costs		
GSE	14,000	17,690
Facility, Manufacturing and		
Launch	32,000	42,170
Subtotal	46,000	57,860
Development Test Costs		
Stage Structural Test	2,287	3,789
Manufacturing Development	118	118
PFRT SRM	42,900	69,321
Other	9,500	14,758
Stage Structure	21,000	33,037
Wind Tunnel and SDF	4,975	4,975
Facility Test	15,820	30,219
DTV	18,508	18,508
R&D Flights (2)	224,443	196,207
Static Load	2,880	4,810
Subtotal	342,431	375,772
TOTAL	<u>\$614,180</u>	\$704,213

. 156" SRM Stage Contains 1.45 Million Pounds of Propellant . 260" SRM Stage Contains 2.90 Million Pounds of Propellant

5.3.3(Continued)

delivered in segments, considerably less tooling will be required for assembly and checkout at the SRM facility.

c. Smaller diameters and lower weight for the associated stage structure design and tooling. Approximately thirteen million dollars lower cost will result with smaller 156 inch SRM stage structures.

Other get ready costs are those items of ground support equipment and facility manufacturing and launch equipment which are sensitive to the quantity of solid motor segments and/or motors to be fabricated and to the number of SRM stages to be launched. The GSE costs for the 156 inch SRM will be approximately the same as the 260 inch SRM. Although there will be a considerable difference in the weight of the items to be handled by the ground support equipment, the larger quantities and number of subassemblies (segments) that will be required for the 156 inch SRM will make their costs comparable to the 260 inch SRM GSE costs. There will be a decrease of approximately \$12,000,000 between the 156 inch stage and the 260 inch stage costs for the quantity sensitive elements of the facilities for manufacturing and launch. The 156 inch motors can be manufactured in a simpler manufacturing facility than those required for the 260 inch motors. The 260 inch motors will require cast, cure and test facilities which cost between two to three million dollars apiece. At least four would be required to meet the launch rate required by the program. For the 156 inch motors, the segments will be cast in smaller increments and require less complex facilities.

A difference of approximately \$33,000,000 will exist between the 156 inch SRM stage and the 260 inch SRM stage development test costs. The major differences will be in the PFRT costs where approximately \$45,000,000 more will be required for the 260 inch SRM stage tests. The same number of SRM's will be involved in the test program, however, the propellant in the 156 inch motors will be half that required for the 260 inch motors. In addition, all other structures will be reduced in size and weight and, therefore, cost considerably less. A cost difference of approximately \$15,000,000 will exist in the facility test vehicle costs. The structural elements, transportation costs, and launch operation costs for the 156 inch motors will make up the major portion of this difference. These costs will be considerably less for the 156 inch SRM stage as it goes through the facility, handling and checkout procedures than those for the 260 inch SRM stage. All of the other costs shown in the development test program will be approximately the same for the two configurations (except for the R&D flights).

Vehicle programs with increasing payload requirements were costed to determine the break even point between the two configurations. Three different size vehicle programs were examined. These programs consisted of four vehicles which placed 7,000,000 pounds of payload into 100 NM orbit, nine vehicles which put up 15,800,000 million pounds of payload, and 20 vehicles which put up 35,100,000

5.3.3 (Continued)

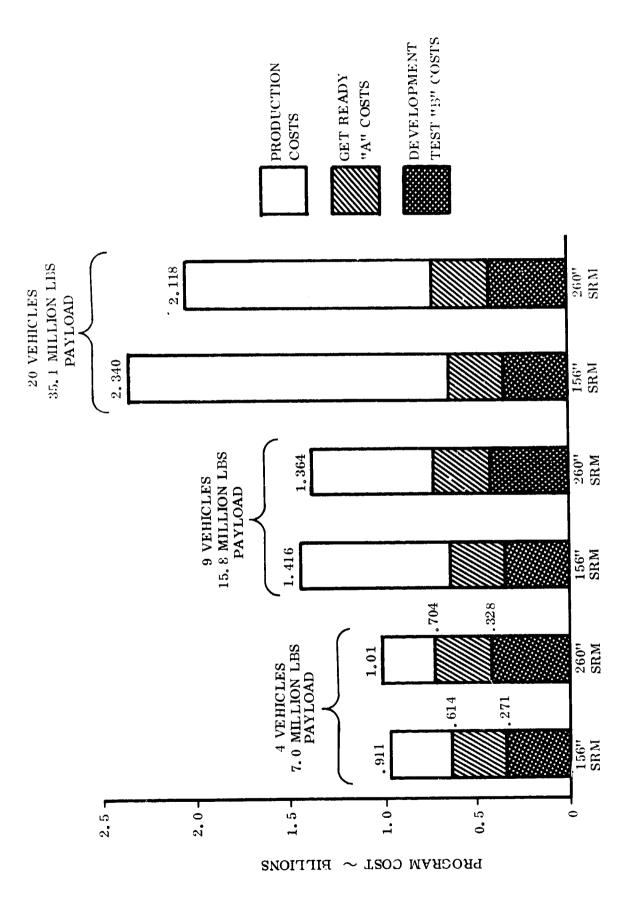
million pounds of payload. With only four vehicles, the 156 inch SRM program cost will be 117 less than the program cost for 260 inch strap-ons. The cost difference is the result of the greater "get ready" and development test costs for the 260 inch SRM stages as compared to the 156 inch SRM stage. At approximately nine vehicles or 15,800,000 pounds of payload, the lower get ready and development test costs for the 156 inch SRM will be offset by the lower production costs for the 260 inch SRM stages. At this point, the overall cost of the 260 inch SRM program will be slightly lower than that of the 156 inch SRM. When the program is increased to 20 vehicles, there will be a considerable savings with the vehicle configuration having 260 inch SRM strap-ons. These comparative results are shown in Figure 5.3.3.0-1.

5.3.4 Cost Comparison of MLLV Configuration with Eight Strap-On 260 Inch SRM's - Sequentially Staged SRM's Versus Non-Sequentially Staged SRM's

The MLLV configuration consisting of a main stage plus eight strap-on 260 inch SRM's, operating in a zero stage mode, will have a payload capability to 100 NM of 1,757,000 pounds. In Volume II, the performance advantage of sequentially staging the 260 inch SRM stages was presented. For the sequential staging mode, six of the eight SRM stages would be ignited at liftoff, burned and separated after propellant depletion. The remaining two SRM stages would be then ignited. After their propellant depletion, they would be separated and then the main stage ignited. The payload with the sequentially staged SRM's would be approximately 1,950,000 pounds. (This payload value is a conservative approximation. The effects of drag losses and vehicle structural penalties induced by the SRM stages that are not ignited at launch must be considered in more detail analyses to better define the vehicle performance for this mode.)

The effects of sequentially staging the SRM's on the get ready costs, development tests costs and first unit costs were determined. It was determined that the following vehicle elements will be affected:

- a. Instrument Unit The instrument unit must be modified to provide the modified ignition and separation sequence of the SRM stages.
- b. Main Stage The main stage exclusive of the forward skirt must be structurally modified to withstand the greater payload weight and length. The base plug will require a significant increase in the ablative insulation since it now must withstand the solid motor exhaust gases for 260 seconds rather than for 130 seconds as with the non-staged configuration. The forward skirt structure will be significantly affected. During operation of the six SRM stages, six of the points at which the SRM stages are attached to the core vehicle will react the positive loads induced by the thrust of the



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5.3.4 (Continued)

SRM stages while the remaining two SRM stage attachment points will react the negative loads due to the non-operation of these stages and to the drag induced by their weight. This will create unusual loads paths within the forward skirt and will necessitate some increase in its weight.

In addition to the vehicle changes, there are several areas which should be investigated during the get ready and development test phases. These include:

- a. Wind tunnel analyses of the local aerodynamics and separation dynamics during staging. As the SRM stages will not be separated simultaneously, the spacings between the two remaining and the six being expended will be more critical than when all eight SRM stages are staged simultaneously.
- b. Analyses of the separation motor requirements. With the tight clearance between the SRM stages being separated and those remaining, it may be necessary to modify the separation motors.
- c. Increased structures testing of the main stage and strap-on stage forward skirts to account for the uneven load distribution.
- d. Modification to the dynamic test activities to simulate for the condition of six SRM stages being ignited at launch, followed by ignition of the remaining two SRM stages after the six SRM stages are expended and separated. This will cause a minor modification to the dynamic test vehicle, tooling, equipment, tests and operations.

Table 5.3.4.0-I lists the various elements of get ready and development test costs showing those elements which will be modified. In addition, the cost of the non-sequentially staged standard condiguration is shown for comparison. The increase in the get ready and development test costs will be \$1,788,000 (0.25 percent).

The recurring (first flight test unit) costs effects are summarized in Table 5.3.4.0-II.

The first unit cost for the SRM stage will be increased by approximately \$600,000. Cost increases of \$160,000 for the core stage will include those for modification of the forward skirt, a slight modification to the thickness of the tank walls, an increase in the base plug insulation, and slight modifications to the breadboard and the launch operations.

To provide a comparison of the cost effectiveness, a vehicle program consisting of 20 vehicles (2 R&D flights, 18 operational flights) using the sequentially staged method versus the non-sequentially stage method was costed. The vehicle

TABLE 5.3.4.0-IGET READY AND DEVELOPMENT TEST COSTS FOR MLLV
CONFIGURATION WITH EIGHT 260'' SRM STRAP-ON STAGES
STANDARD VERSUS SEQUENTIALLY STAGED
(DOLLARS IN THOUSANDS)

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FUNCTION OR COMPONENT	260'' SRM STAGE (USING SEQUENTIALLY STAGED SRMS)	260'' SRM ' S (ZERO STAGED)
Fixed Get Ready Costs		
	\$ 3,072	\$ 3,072
GSE Michard Engility	8,454	8,434
Michoud Facility Launch Complex Facility	162,470	162,470
SRM Facility and Tooling	— · · · ·	
Plus Design	44,131	44,131
Stage Structure Design.		
and Tooling	32,335	32,285
Forward Skirt	19,729	19,729
r of ward Skilt	and the second	
Subtotal	\$270,191	\$270,121
Quantity Sensitive - Get Ready Costs ()	Excluding R&D Flight Tests)	15,690
GSE	10,000	,
Facility Manufacturing and Launch	42,210	42,170
Subtotal	\$ 57,900	\$ 57,860
Development Test Costs		
at a stars to a 1 To at	3,809	3,789
Stage Structural Test	118	118
Manufacturing Development PFRT SRM	69,321	69,321
Other	14,758	14,758
Stage Structure	33,037	33,037
Wind Tunnel and SDF	5,533	4,975
Facility Test	30,219	30,219
DTV	19,508	18,508
Static Load	4,940	4,830
Subtotal	\$181,243	\$179,565
TOTAL	\$509 , 334	\$507,546

TABLE 5.3.4.0-11FIRST FLIGHT TEST UNIT COST COMPARISON OF
SEQUENTIALLY STAGED MODE VERSUS STANDARD
STAGED MODE FOR THE MLLV CONFIGURATION
CONSISTING OF A MAIN STAGE PLUS EIGHT STRAP-ON
260 INCH SRM'S

,	SEQUENTIALLY STAGED MODE	ZERO STAGED MODE
8 SRM Stages Main Stage	\$103,165,000 372,638,000	\$102,565,000 372,478,000
MLLV Configuration Consisting of a Main Stage Plus Eight Strap-On Stages (Total Vehicle)	\$475,803,000	\$475,043,000

5.3.4 (Continued)

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configuration used for this comparison consisted of a main stage plus eight 260 inch SRM stages. This analysis showed that the total cost of the program will be 8,987,900,000 for the vehicle configurations using ignition of all eight SRM stages at launch. This gave a cost effectiveness of \$284 per pound of payload placed into orbit. Using the staged SRM sequentially staged concept, the total program cost will increase by approximately 15 million dollars to \$9,002,900,000. In terms of cost effectiveness, the staged vehicle concept will, however, deliver payload to orbit at a cost of \$256 per pound.

In summary, the staged vehicle concept will significantly increase the payload capability at only a minor increase in cost. This will result in a much more cost effective vehicle.

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6.0 COST EFFECTIVENESS EVALUATION OF ALTERNATIVE TECH-NOLOGY APPLICATIONS

This section presents parametric cost and performance data and illustrates the methodology for its application to evaluate the cost effectiveness of alternative technology applications to the baseline MLLV and AMLLV families. Such evaluations can be used to determine the maximum dollars which can be expanded. for an advanced technology alternative to replace the technology specified for the baseline vehicle, without increasing overall cost for a specified program.

Application of technology alternatives to the main stage of either the MLLV or AMLLV families should result in a change of the overall vehicle weight for a given payload requirement. This change in vehicle weight will be reflected in the weight or size (and associated costs) of the major elements comprising the vehicle and of the required supporting facilities, equipment and tooling. Application of the relationships of technology, size and cost with the proper methodology will give the cost/performance potential of alternative technologies.

The following tools for evaluation of the cost/performance potential of alternative technology applications to the baseline MLLV and AMLLV families are provided and discussed in the subsequent sub-sections:

- a. Relationship of required main stage size, for a given payload, as a function of specific impulse (I_{sp}) and mass fraction (λ').
- b. Relationship of costs to main stage size.
- c. Methodology for cost effectiveness evaluation with representative examples and conclusions.

6.1 RELATIONSHIPS OF REQUIRED MAIN STAGE SIZE TO TECHNOLOGY IMPROVEMENTS

Application of technology improvements, such as increasing the mass fraction or increasing the specific impulse will result in reduction of the required overall vehicle launch weight to place a given payload in orbit. Figure 6.1.0.0-1 through Figure 6.1.0.0-8 illustrate the relationships of mass fraction (λ'), and specific impulse (I_{sp}) as a function of the vehicle weight for a specified payload capability.

Figure 6.1.0.0-1 shows the required main stage weight of the AMLLV singlestage-to-orbit vehicle as a function of the main stage mass fraction (λ') for various values of specific impulse (I_{sp}). The baseline AMLLV main stage (with multichamber/plug propulsion system) is identified by the triangle which corresponds to the baseline stage weight of 11.8 million pounds, the associated

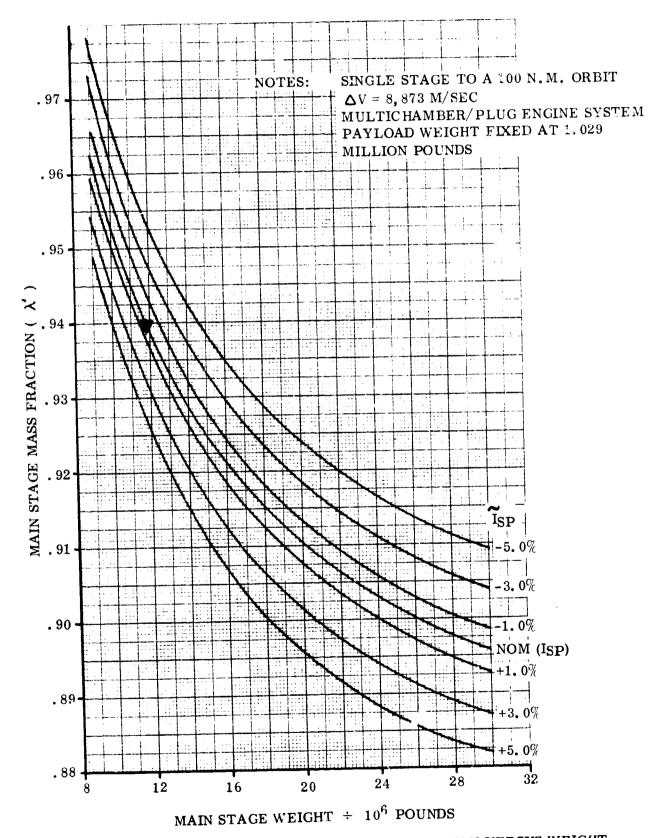
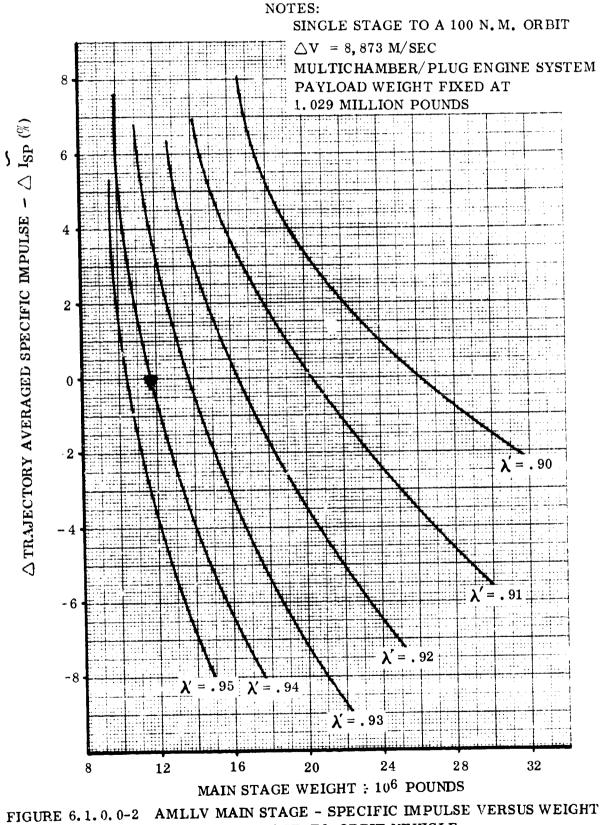


FIGURE 6.1.0.0-1 AMLLV MAIN STAGE - MASS FRACTION VERSUS WEIGHT FOR SINGLE-STAGE-TO-CRBIT VEHICLE



FOR SINGLE-STAGE-TO-ORBIT VEHICLE

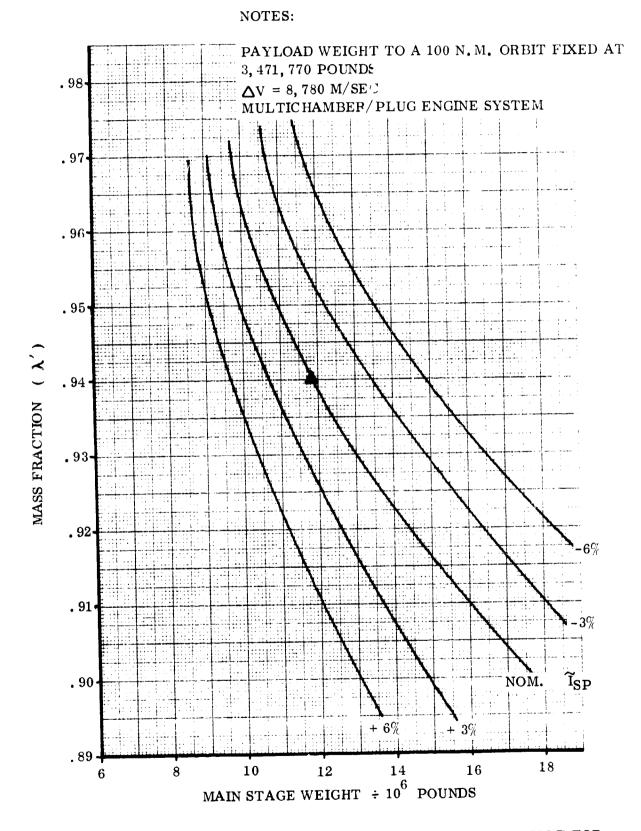
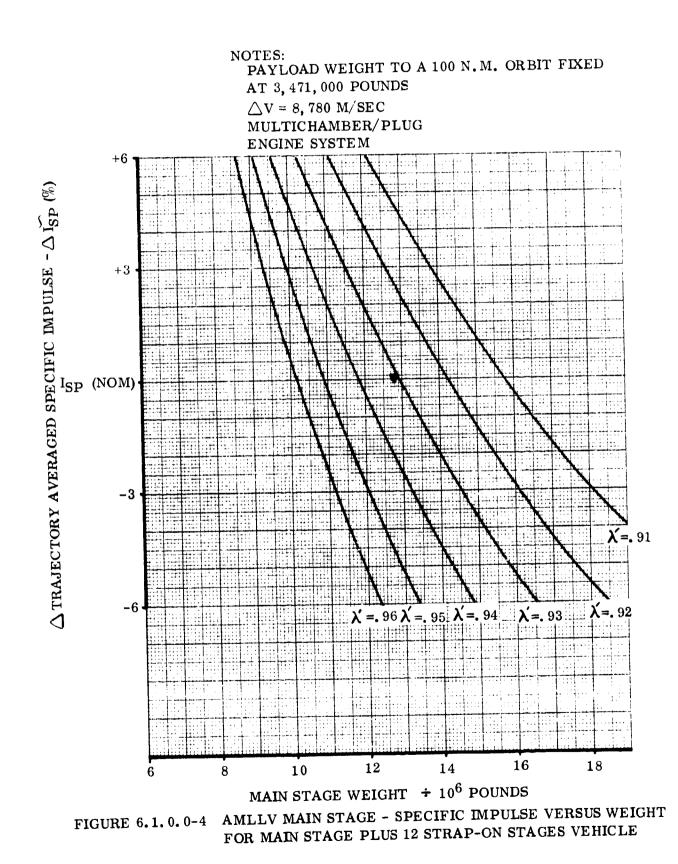


FIGURE 6.1.0.0-3 AMLLV MAIN STAGE - MASS FRACTION VERSUS WEIGHT FOR MAIN STAGE PLUS 12 STRAP-ON STAGES VEHICLE



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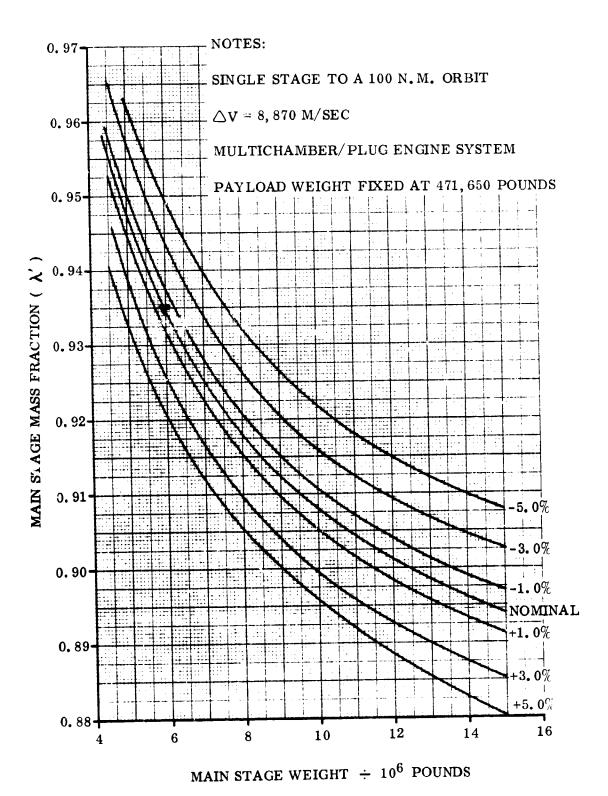
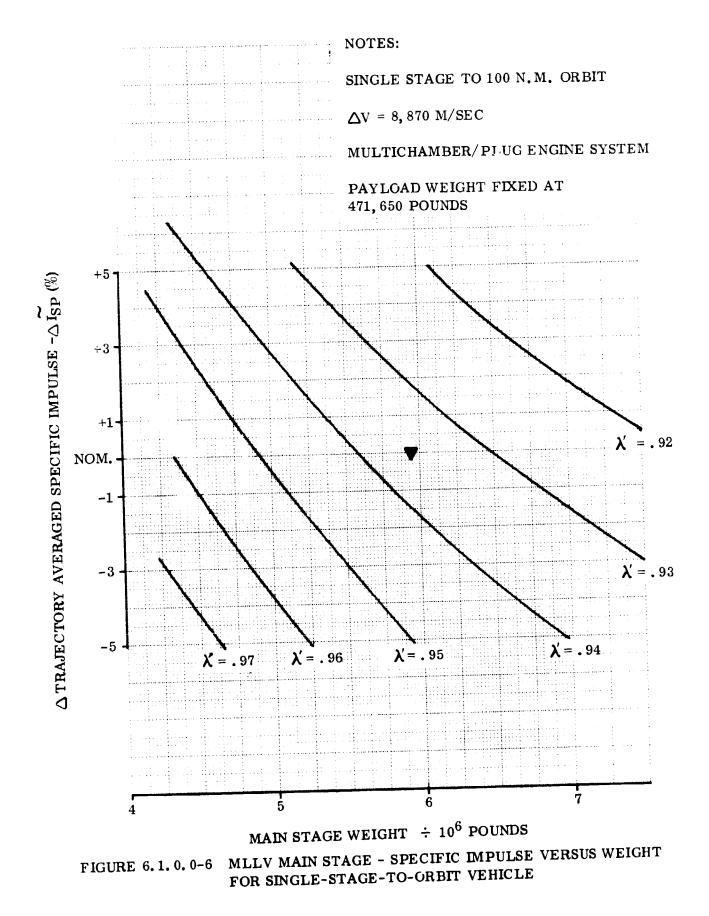


FIGURE 6.1.0.0-5 MLLV MAIN STAGE - MASS FRACTION VERSUS WEIGHT FOR SINGLE-STAGE-TO-ORBIT VEHICLE



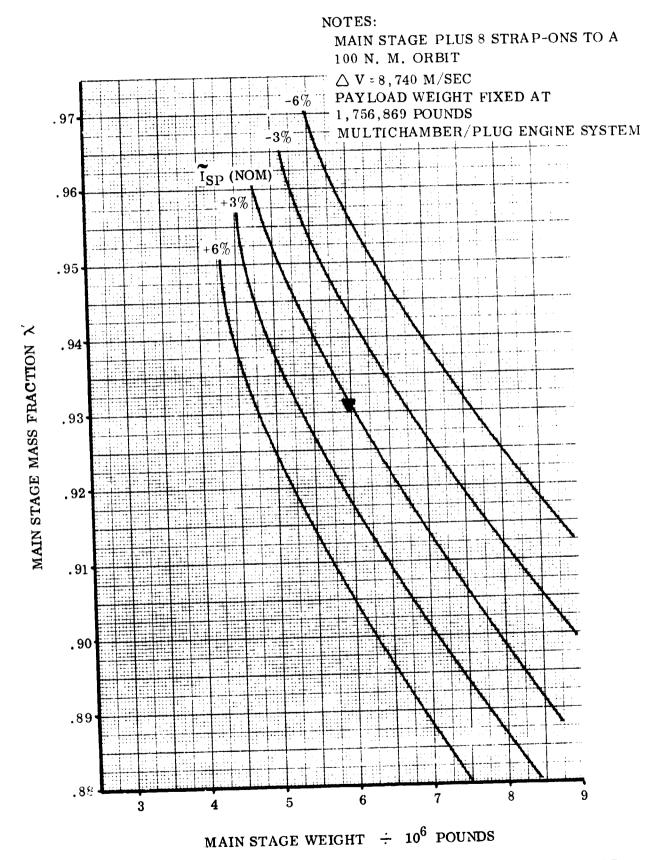


FIGURE 6.1.0.0-7 MLLV MAIN STAGE - MAES FRACTION VERSUS WEIGHT FOR MAIN STAGE PLUS 8 STRAP-ON STAGES VEHICLE

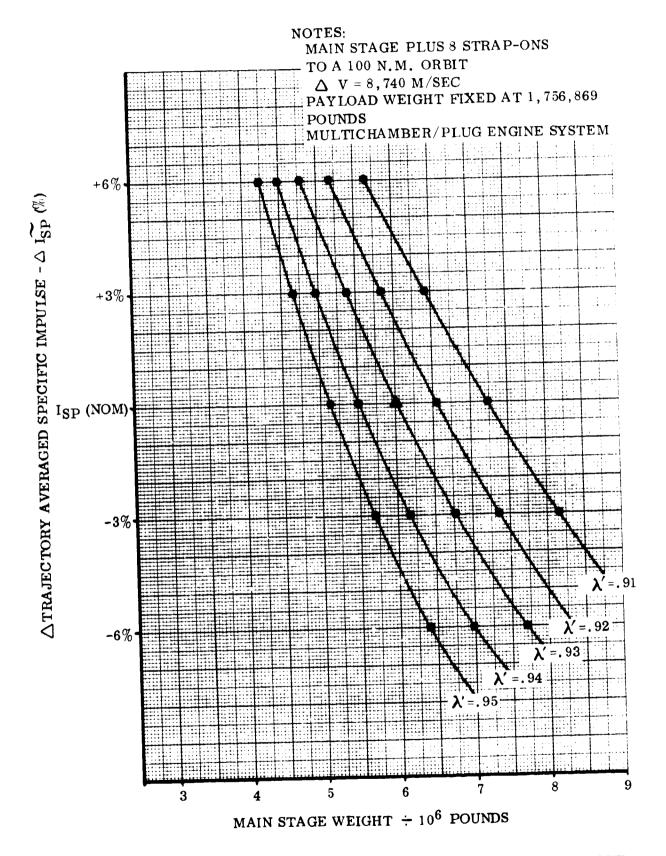
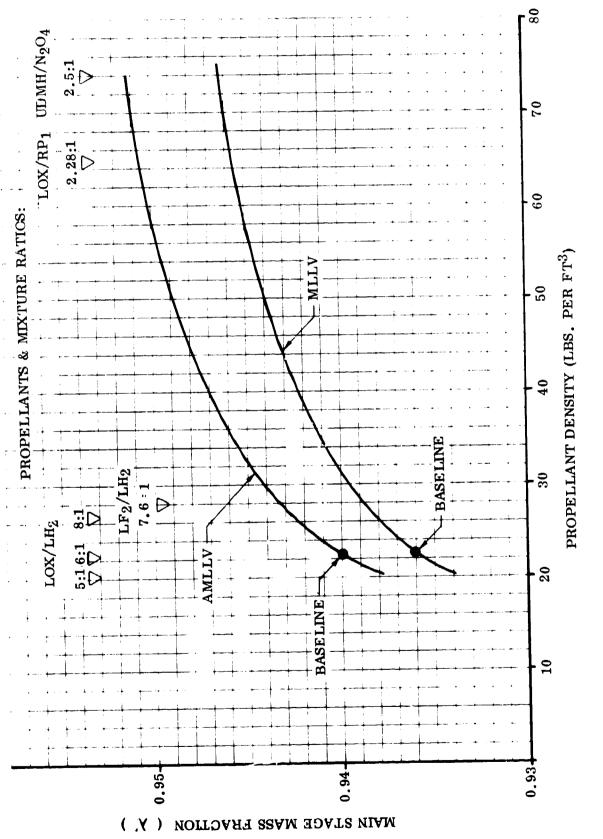


FIGURE 6.1.0.0-8

MLLV MAIN STAGE - SPECIFIC IMPULSE VERSUS WEIGHT FOR MAIN STAGE PLUS 8 STRAP-ON STAGE VEHICLE







6.1 (Continued)

 λ' of .94 and the nominal trajectory averaged I_{sp}. This figure shows, for example, that if the λ' is increased from .94 to .95 and the I_{sp} remains constant, the required main stage weight will decrease to 10.4 million pounds.

Figure 6.1.0.0-2 shows the required weight of the AMLLV main stage as a function of trajectory averaged I_{sp} for various values of λ . The baseline vehicle is again identified by the triangle. If the trajectory averaged I_{sp} is increased by 5% at a constant λ of 0.94, the required main stage weight will decrease from 11.8 million pounds to 10.0 million pounds.

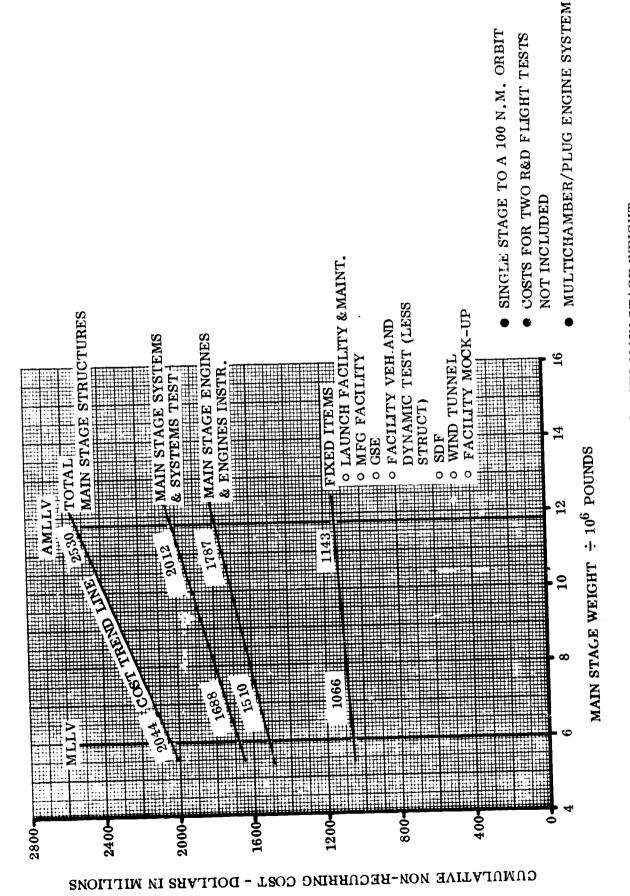
Figures 6.1.0.0-3 and 6.1.0.0-4 show similar relationships for the main stage of the AMLLV main stage plus twelve strap-on stages vehicle configuration. Figures 6.1.0.0-5 through 6.1.0.0-8 show similar relationships for the main stage of the MLLV single-stage-to-orbit vehicle and the main stage of the MLLV main stage plus eight strap-on stages vehicle configurations.

Figure 6.1.0.0-9 shows the effect of propellant density on stage mass fraction. For this analysis the stage thrust and propellant weight were held constant. To prepare the chart, it was assumed that changes in propellant density would effect the length (and weight) of the propellant tank cylindrical sections only. As the propellant density was increased, the required length (and weight) of the cylindrical section was reduced. Mixture ratios for LOX/LH₂, LF₂/LH₂, LOX/RP-1 and UDMH/N₂O₄ propellants are shown for reference. This curve used in conjunction with the curves of mass fraction and specific impulse versus main stage launch weight, shown in Figures 6.1.0.0-1 through 6.1.0.0-8, can be used to determine the effects of a change of propellant density (and specific impulse) on the required main stage weight to deliver a specified payload weight to orbit.

6.2 SIZE / COST RELATIONSHIPS

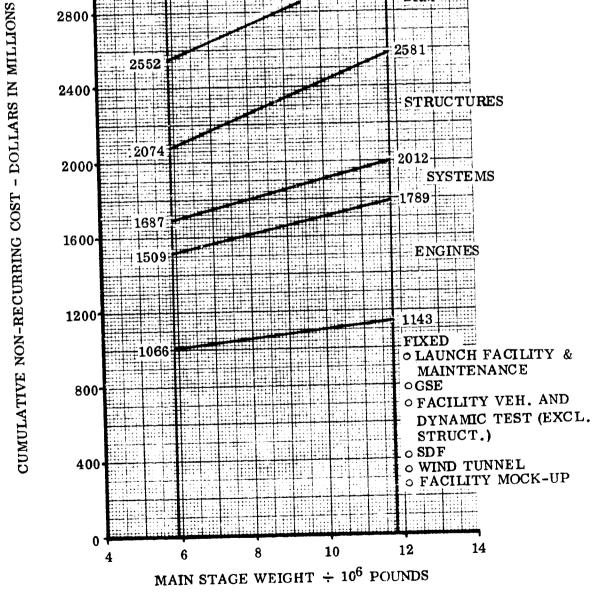
The change in main stage weight as described above is reflected in changes in the weight of the major vehicle systems and subsystems such as structure, engines and propellants and in the size of supporting facilities, equipment and tooling.

Figures 6.2.0.0-1 and 6.2.0.0-2 show the non-recurring ("get ready" and development test) costs for the MLLV and AMLLV single-stage-to-orbit vehicles and for the ! LLV and AMLLV main stage plus full complement of strapon stage vehicles. The lines connecting the cost points show the cost trends relative to main stage weights. <u>Costs for the two R&D flights tests are not</u> <u>included</u>. To aid in application of the methodology defined in the following section 6.3, the costs are grouped by the following categories:





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SRM

1.

• COST FOR TWO R&D FLIGHTS NOT INCLUDED

• SOLID MOTOR SIZES FOR AMLLV AND MLLV FIXED

• MULTICHAMBER/PLUG ENGINE SYSTEMS

• 100 N.M. ORBIT

32001

2800

• MAIN STAGE PLUS FULL COMPLEMENT OF SRM STRAP-ON STAGES

FIGURE 6.2.0.0-2 NON-RECURRING COSTS VERSUS MAIN STAGE WEIGHT

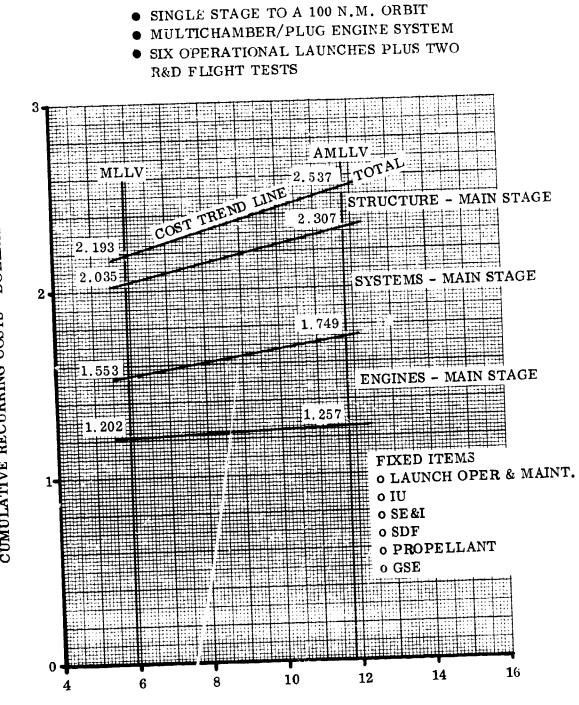
6.2 (Continued)

- a. Main Stage Structure Includes, as applicable to non-recurring or recurring costs, production costs of all main stage structures, structures for Dynamic and Facility Checkout Vehicles, static and dynamic load tests and manufacturing development. Also included (as applicable) are the delta costs for the heavyweight forward skirt.
- b. Main Stage System and System Installation Includes, as applicable to non-recurring or recurring costs, production costs of all main stage systems, system test, system development, and engine installation.
- c. Main Stage Engines Includes, as applicable to non-recurring or recurring costs, production costs of all main stage engines.
- d. SR M Strap-On Stages (as applicable) Includes as applicable to nonrecurring or recurring costs, production costs of SR Ms structures and motors, SR M GSE, SR M facilities, SR M manufacturing development, SDF, static load, PFRT and wind tunnel.
- e. Fixed Costs Includes launch and manufacturing facilities, transportation, GSE, Systems Breadboard (SDF), SE&I, Instrumentation Unit, wind tunnel tests, manufacturing mockup and propellants.

Similarly, Figures 6.2.0.0-3 through 6.2.0.0-10 show the recurring (production and launch) costs for the MLVV and AMLLV single-stage-to-orbit vehicle configurations and for the MLLV and AMLIV main stage plus full complement of strap-on stage vehicle configurations. The cumulative recurring costs are shown for various program sizes (6, 12, 24, and 36 operational launches plus two R&D flight tests). Learning curve effects are included.

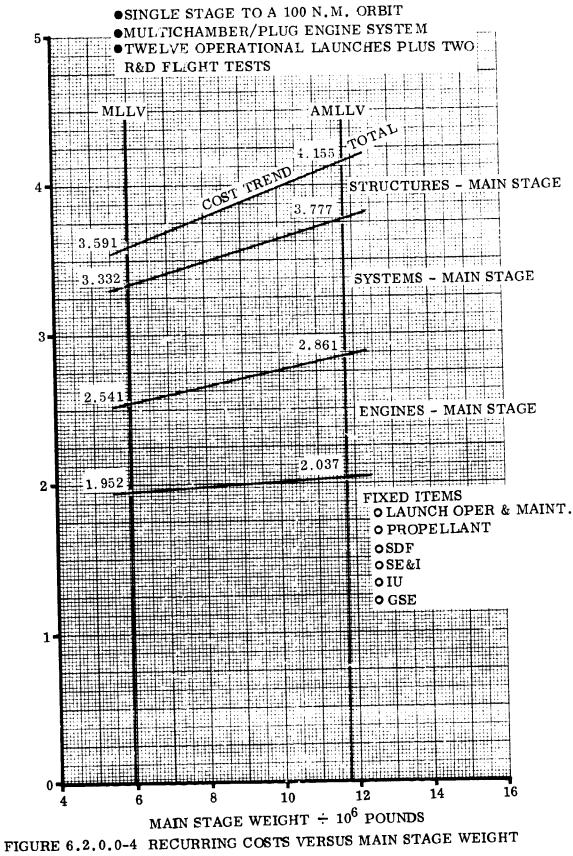
As shown by Figures 6.2.0.0-1 through Figure 6.2.0.0-10, there will be ϵ minimal cost reduction associated with reduction in size for main stage systems and for fixed items such as facilities, launch operations, GSE, etc.

The most appreciable cost/size relationship will be for main stage structure and for main stage engines. The costs of these two elements will reduce by approximately 30% as the vehicle size is reduced from the full size AMLLV to the half size MLLV configuration. The total reduction in cost for this size change will be approximately 19%.



MAIN STAGE WEIGHT \div 10⁶ POUNDS FIGURE 6.2.0.0-3 RECURRING COSTS VERSUS MAIN STAGE WEIGHT

CUMULATIVE RECURRING COSTS - DOLLARS IN BILLIONS



CUMULATIVE RECURRING COSTS - L'LLARS IN BILLIONS

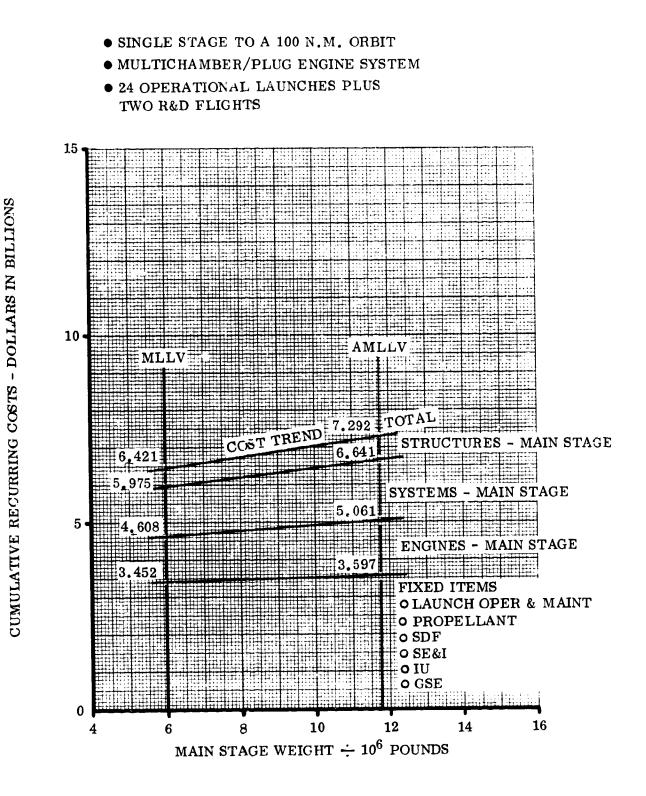
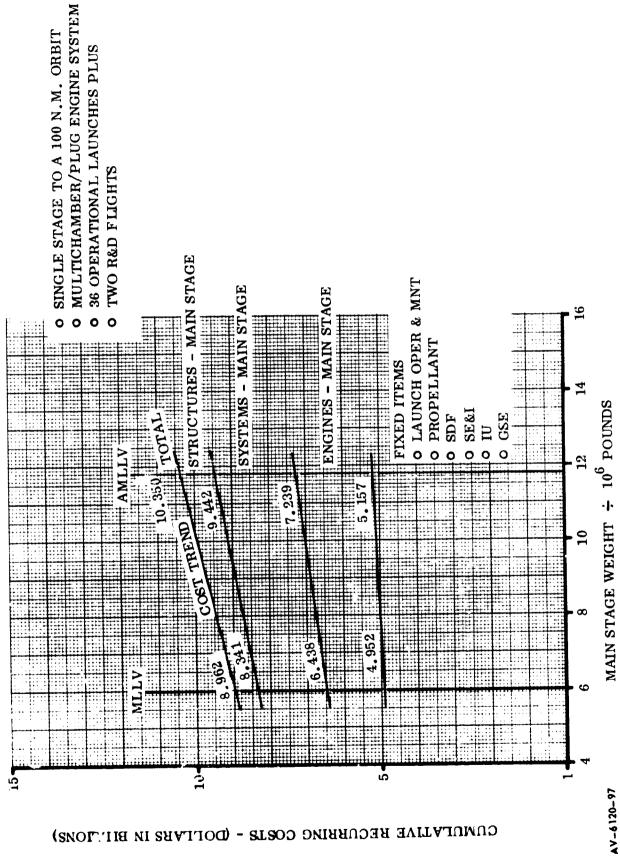


FIGURE 6.2.0.0-5 DECURRING COSTS VERSUS MAIN STAGE WEIGHT



CUMULATIVE RECURRING COSTS - (DOLLARS IN BIL.JONS)

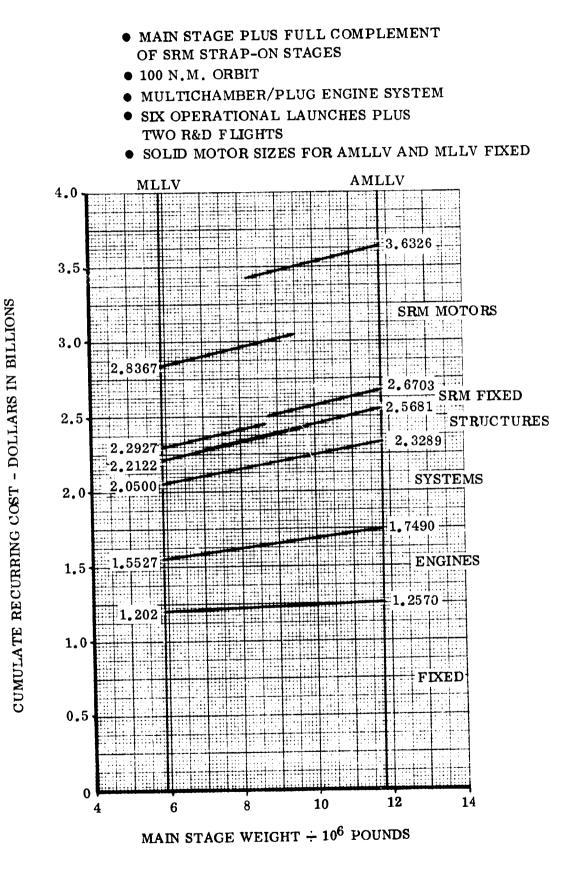
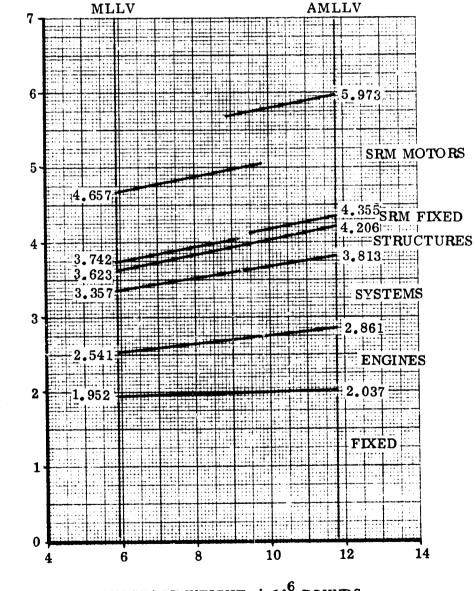
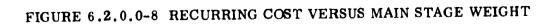


FIGURE 6.2.0.0-7 RECURRING COST VERSUS MAIN STAGE WEIGHT

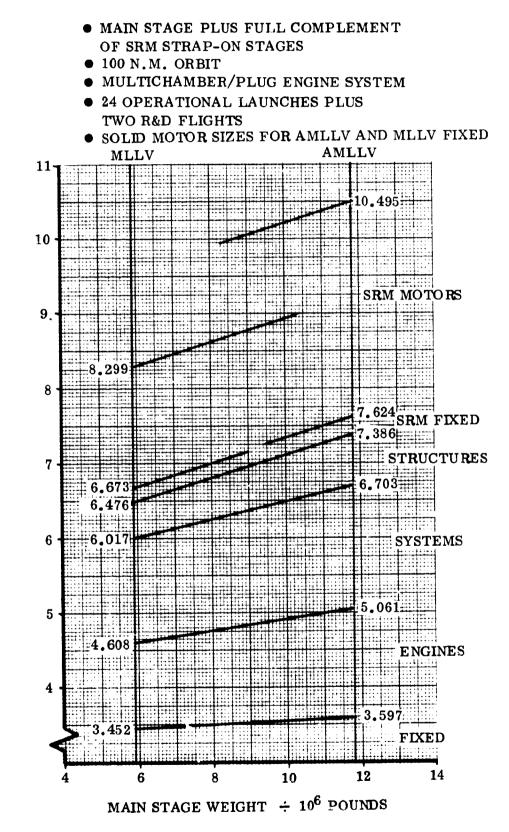


MAIN STAGE WEIGHT \div 10⁶ POUNDS



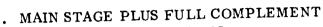
CUMULATIVE RECURRING COSTS - DOLLARS IN BILLIONS

- TWO R&D FLIGHTS • SOLID MOTOR SIZES FOR AMLLV AND MLLV FIXED
- TWELVE OPERATIONAL LAUNCHES PLUS
- MULTICHAMBER/PLUG ENGINE SYSTEM
- 100 N.M. ORBIT
- MAIN STAGE PLUS FULL COMPLEMENT OF SRM STRAP-ON STAGES

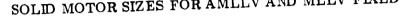


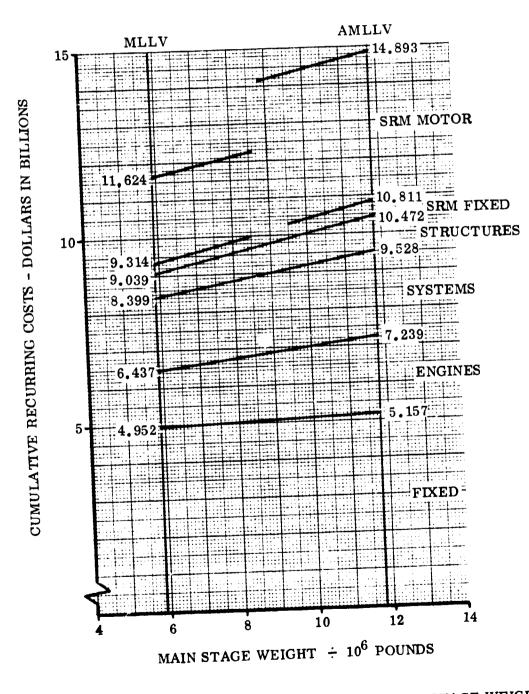


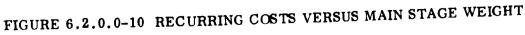
CUMULATIVE RECURRING COSTS - DOLLARS IN BILLIONS



- OF SRM STRAP-ON STAGES
- 100 N.M. ORBIT
- MULTICHAMBER/PLUG ENGINE SYSTEM
- 36 OPERATIONAL LAUNCHES PLUS TWO R&D FLIGHTS
- SOLID MOTOR SIZES FOR AMLLV AND MLLV FIXED







6.3 METHODOLOGY FOR COST EFFECTIVENESS EVALUATIONS

The preceding Figures 6.1.0.0-1 through 6.1.0.0-9 show the effect of technology variables on main stage weight. These data plus the cost versus size data from the preceding Figures 6.2.0.0-1 through 6.2.0.0-10 provide the required input data for evaluating the cost effectiveness of alternative technology applications to the primary stage of the baseline MLLV and AMLLV families. The following representative examples show the methodology for applying this data.

6.3.1 Effects on Cost of Changes in Main Stage Mass Fraction

A representative example of the methodology for application of this data for evaluation of alternative structure is shown in Figure 6.3.1.0-1. This figure shows the maximum dollars, for R&D and a 36 AMLLV single stage to orbit production and launch program, which can be expended for R&D and for production of the advanced structure alternative (to replace the structure specified for the baseline vehicle) without increasing the overall program cost.

For this particular example, the following conditions were considered or assumed:

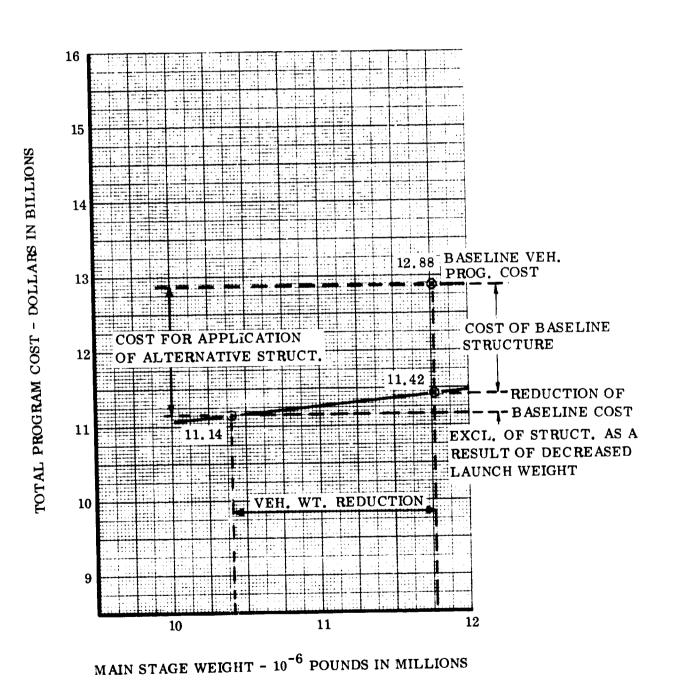
- a. Vehicle: AMLLV single-stage-to-orbit vehicle Main stage weight = 11.805 X 10⁶ lbs.
- b. Program Size: 36 launches @ 1,029,000 pounds of payload per launch.
- c. System Investigated: Structures
- d. Technology change: Change in mass fraction from $\lambda' = .94$ to $\lambda' = .95$.

The procedure was as follows:

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- a. The total cumulative AMLLV non-recurring cost of \$2.53 billion was determined from Figure 6.2.0.0-1.
- b. The total cumulative AMLLV recurring cost of \$10.35 billion was determined from Figure 6.2.0.0-6.
- c. These costs (a and b above) were added to determine the total accumulative costs of \$12.88 billion. (Plot point "A" in Figure 6.3.1.0-1).
- d. The structure system cost was determined from Figure 6.2.0.0-1 and 6.2.0.0-6 as in steps a, b, and c above to be \$1.46 billion.

FIGURE 6.3.1.0-1 COST EFFECTIVENESS EVALUATION OF ALTERNATIVE STRUCTURE TECHNOLOGY



. AMLLV SINGLE-STAGE TO A 100 N.M. EARTH ORBIT . MULTICHAMBER/PLUG ENGINE SYSTEM

PROGRAM - 36 OPERATIONAL LAUNCHES

CHANGE IN λ FROM 0.94 TO 0.95

6.3.1 (Continued)

- e. The total baseline program cost (excluding structures) was determined to be \$11.42 billion (Plot point B in Figure 6.3.1.0-1) by subtracting step (d) from step (c).
- f. From Figure 6.1.0.0-1, using a λ^{\prime} of 0.95 and the nominal trajectory averaged I_{sp}, the new AMLLV main stage weight of 10.4 X 10⁶ lbs. was determined.
- g. From Figure 6.2.0.0-1 and 6.2.0.0-6, the total cumulative program costs (excluding structure) for the new vehicle weight was determined to be \$11.14 billion (Plot point "C" in Figure 6.3.1.0-1).

Points A, B and C as derived by the above technique and plotted in Figure 6.3.1.0-1 formed the cost effectiveness parameters of the alternative structural technology to be investigated. The line connecting points B and C is the cost reduction line; the slope of which indicates the degree of cost reduction relative to size of the main stage. (The steeper this slope, the more cost reduction will be realized.)

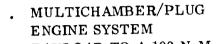
The cost difference between points B and C of \$280 million is the amount that the total program costs, (exclusive of the cost of structures) for a program of 36 launches, will be reduced as a result of a decrease in vehicle launch weight due to a change in mass fraction from $\lambda' = .94$ to $\lambda' = .95$. The cost difference between points A and B of \$1,460 million is the sum of the non-recurring and recurring cost of the old structure to be replaced.

The total cost difference between points A and C is \$1,720 million which is then the maximum amount which can be expended for development and application of the alternative structures if they are to be cost effective. The cost for developing and producing of the alternative structures should, therefore, not exceed the \$1,720 million, otherwise, the new technology will not be economically feasible and should warrant no further in-depth consideration.

Through the use of data presented in Figure 6.1.0.0-1 through 6.1.0.0-9 and Figures 6.2.0.0-1 through 6.2.0.0-10, other similar analyses were conducted for other vehicle configurations and other program sizes. The results of these other analyses are shown in Table 6.3.1.0-1 and Figure 6.3.1.0-2.

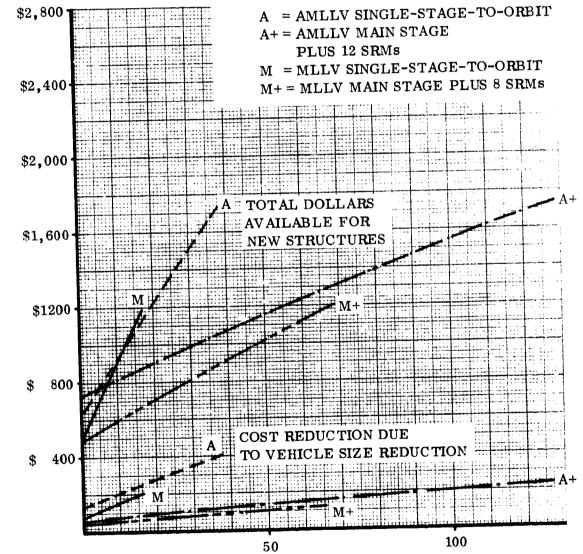
Table 6.3.1.0-1 shows: 1) the cost reduction due to size reduction for improved structure (excluding the cost of the baseline structures), 2) the cost of the baseline structure and 3) the total dollars available for replacement of the old baseline structural technology (cost reduction due to size reduction excluding cost of structures plus cost of the baseline structure). Cost data are

NOTES:



- PAYLOAD TO A 100 N.M.
- E ARTH ORBIT . CHANGE IN $\lambda' = +0.01$

LEGEND:



DOLLARS IN MILLIONS

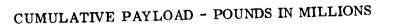


FIGURE 6.3.1.0-2 COST IMPLICATIONS OF A 0.01 IMPROVEMENT IN MASS FRACTION

	ů.	MLLV SINGLE- STAGE-TO-ORBUT	- 11	AMLLV SINGLE- STACE-TO-ORBIT	LE- LBTT	MLLV MAIN STACE + 8 SRM's	i M's	AMLLV MAIN STAGE + 12 SRM's	к, в К
	OPER.	SNOITTEI NI	6%	IN BILLIONS	8 ²²	\$ \$	8 4	s BILLIONS	*
Cost Reduction Due to Size Reduction									
	N.	0. 057	2.8	0.108	4.3	0.034	L. 3	0, 064	2.0
Pines C	9	0. 036	1.7	0.069	2.7	0.022	8 °	0.041	
(Incivites 2	12	0.060	1.7	0.113		0.066		0, 117	11
RAD Fits.) (Exchudes Cost of Structures)	24 36	0. 1 09 0. 1 49	1. 7 1. 7	0. 280		060.0	6.9	Q. 157	1:1
Cost of Baseline Biracture									
	N	0, 356	17.3	0. 424	16.7	0. 387	15.1	0. 569	1.8.1
	1 4	0.158	7.2	0.230	9.1	0.162	5. 7	0, 239	• •
	5 21	0.259	7.2	0.378	9.1	0.266	2.1	0.393	0 4
	2	0. 446	7.0	0.651	8. 9	0.459		0.67	* * 6 v
	8	0. 621	7.0	0. 908	8.8	0.640	5.5	0. 344	
Total Dollars Awilable for New Technology									
	a	0.607	14.3	0. 631	16.4	0, 605	8,9	0.913	16.9
Phases A, B & C	• <u>•</u>	0.732	13.0	L. 023	15. 3	0.723	7.9	1.093	15.2
	1 2	0.968	11.4	1.353	13.8	0.946	6°9	1.427	13.2
	1 46	1 183	10.7	1.720	13.3	1.151	6.4	I.734	12.3

BLE 6.3.1.0-I COST IMPLICATIONS OF A 0.01 IMPROVEMENT IN MAIN STAGE MASS FRACTION

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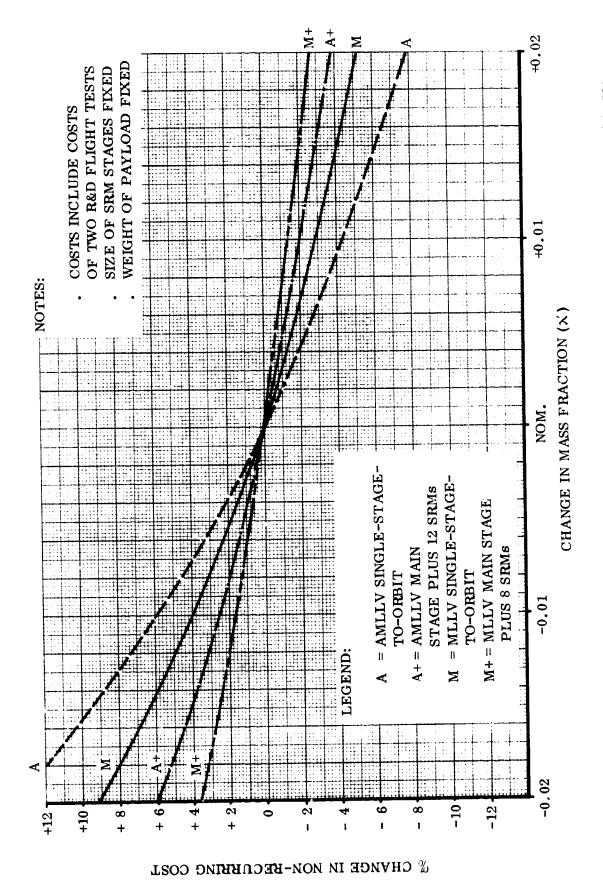
6.3.1 (Continued)

shown for Phases A and B (less flight tests) and operational programs of 6. 12. 24, and 36 (plus two flight tests each). The vehicles for which data are depicted are the MLLV single-stage-to-orbit vehicle, the MLLV main stage plus 8 SRMs vehicle, the AMLLV single-stage-to-orbit vehicle and the AMLLV main stage plus 12 SRMs vehicle. This table is somewhat difficult to interpret because of the large variance in payloads between the various vehicle sizes. For example, 36 flights of the MLLV single-stage-to-orbit vehicle will deliver something less than 18 million pounds to orbit while 36 flights of the AMLLV main stage plus 12 SR Ms vehicle will deliver 144 million pounds of payload to orbit.

Figure 6.3.1.0-2 was prepared to provide better visibility of the dollars available for new technology (for a 0.01 improvement in the main stage mass fraction) relative to comparative payload programs. This figure shows the overall program cost reduction due to vehicle size reduction and the total dollars available within the program for new structure to provide an improvement in main stage mass fraction of 0.01. This figure shows that the single-stage-to-orbit vehicles are more sensitive to technology improvements, i.e., more cost reduction can be realized with the single-stage-to-orbit vehicles through technology improvements than for the vehicles consisting of main stages plus a full complement of strap-on stages. For a smaller program which requires a few pounds of payload to orbit, Figure 6.3.1.0-2 indicates that the larger (AMLLV) vehicles will have more dollars available for new structures technology than will the smaller (MLLV) vehicles. However, this chart further indicates, that for larger payload programs, the smaller (MLLV) vehicles will have more dollars available for new structures technology. (The tabulated data on 6.3.1.0-1 explains why this is so. The cost savings attributable to technology changes for the AMLLV type vehicles during the A and B phases will be considerably larger than the cost savings attributable to those on the MLLV vehicles. Conversely, the size reduction resulting from alternative structure applications and the cost of the baseline structures will result in more available recurring dollars per pound of delivered payload for the MLLV vehicles than for the AMLLV vehicles.)

The data discussed above relates only to an improvement in main stage mass fraction of 0.01 through the replacement of the baseline structure with an alternative advanced technology type structure. Similar trades can be performed to define the dollars available for other values of main stage mass fraction attributable to structural changes or to weight changes in engine systems, subsystems, etc. The same methodology as described above would be used.

To provide a better understanding of the cost implications of mass fraction. Figures 6.3.1.0-3 through 6.3.1.0-5 are provided. These figures show the

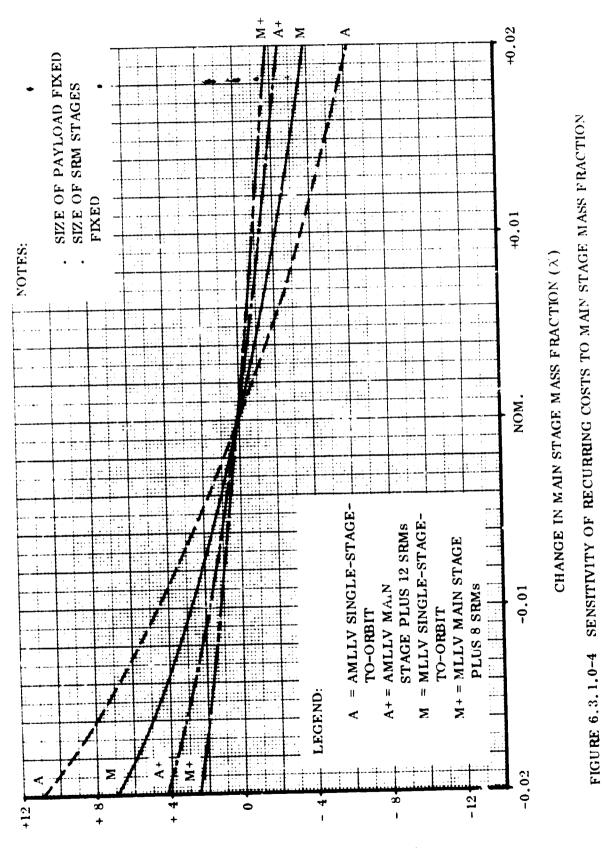


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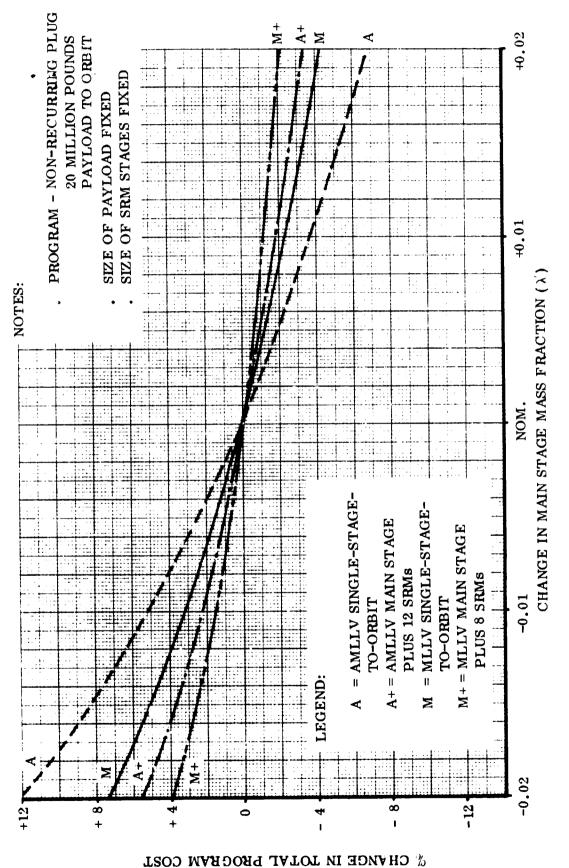


FIGURE 6.3.1.0-5 SENSITIVITY OF OVERALL PROGRAM COST TO MAIN STAGE MASS FRACTION

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6.3.1 (Continued)

percent change in various program costs as a function of various changes in mass fraction. Figure 6.3.1.0-3 which shows the cost sensitivity of <u>non-re-</u> <u>curring costs</u> to main stage mass fraction, indicates that the largest savings (as stated above) will accrue to the AMLLV type vehicles as opposed to similar MLLV type vehicles. The single stage to orbit vehicles will have a more significant cost sensitivity to mass fraction during Phases A and B than will the vehicles with the full complements of strap-on stages.

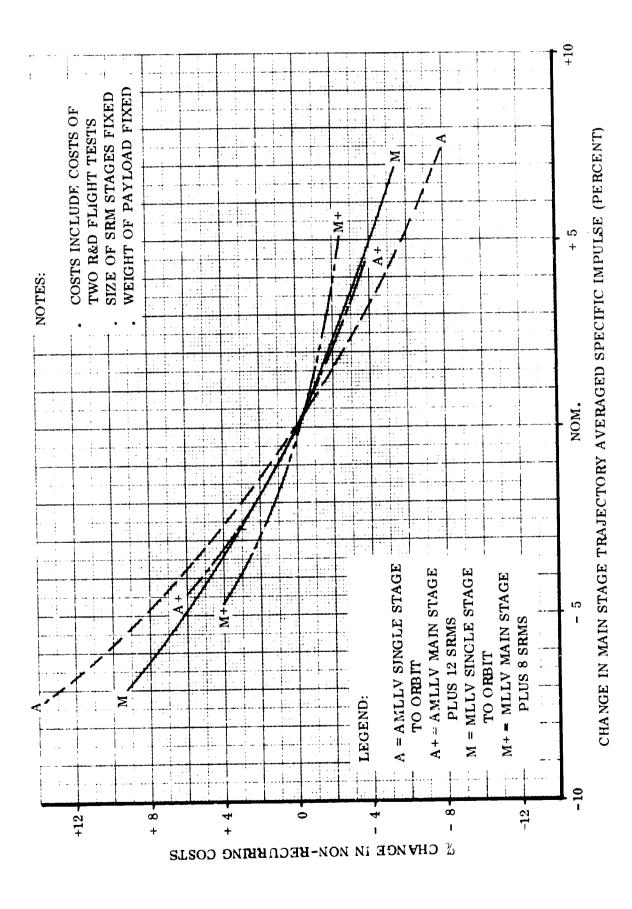
A review of the sensitivity of <u>recurring costs</u> to main stage mass fraction. as shown in Figure 6.3.1.0-4, also indicates that the larger (AMLLV) vehicles will be more cost sensitive to changes in mass fractions than the smaller (MLLV) vehicles. The single-stage-to-orbit vehicles will be more cost sensitive than the vehicles with the strap-ons to changes in mass fraction.

A combination of the two prior charts to provide the sensitivity of <u>total program</u> <u>costs</u> to main stage mass fraction is shown in Figure 6.3.1.0-5. This figure generally shows the same trends indicated above wherein the AMLLV configurations will be more sensitive than comparable MLLV configurations to the changes in mass fraction and wherein the single stage to orbit vehicles will be more sensitive to changes in mass fraction than the vehicles with strap-on stages. For the program size indicated (i.e., Phases A and B plus 20 million pounds of operational payload to orbit), it appears that an improvement of 0.02 in main stage mass fraction for the AMLLV single-stage-to-orbit will result in an approximate reduction in overall program costs of 7%. A reduction of 0.02 in main stage mass fraction for this vehicle would increase program cost by approximately 12%.

6.3.2 Effect on Program Cost of Changes in Specific Impulse

For a two percent improvement in main stage specific impulse, Table 6.3.2.0-I shows: 1) the program cost reduction due to main stage size reduction for the improved specific impulse (excluding the cost of the baseline multichamber / plug engines), 2) the cost of the baseline engines and 3) the total dollars available for replacement of the baseline engine technology (cost reduction due to size reduction excluding cost of engine plus cost of the baseline engine). Cost data are tabulated for Phase A and B (less flight tests) and operational programs of 6. 12, 24, and 36 (plus two flight tests each). The vehicles for which data are depicted are the MLLV single-stage-to-orbit vehicle, the MLLV main stage plus 8 SR Ms vehicle, the AMLLV single-stage-to-orbit vehicle and the AMLLV main stage plus 12 SR Ms vehicle.

To provide a better understanding of the cost implications of specific impulse. Figures 6.3.2.0-1 through 6.5.2.0-3 are provided. These figures show the percent change in various program costs as a function of changes in specific

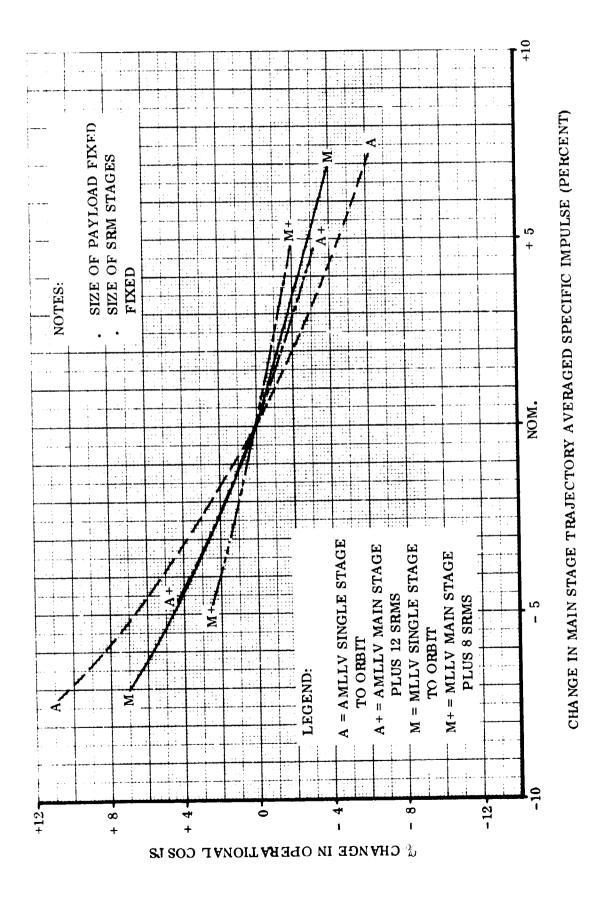


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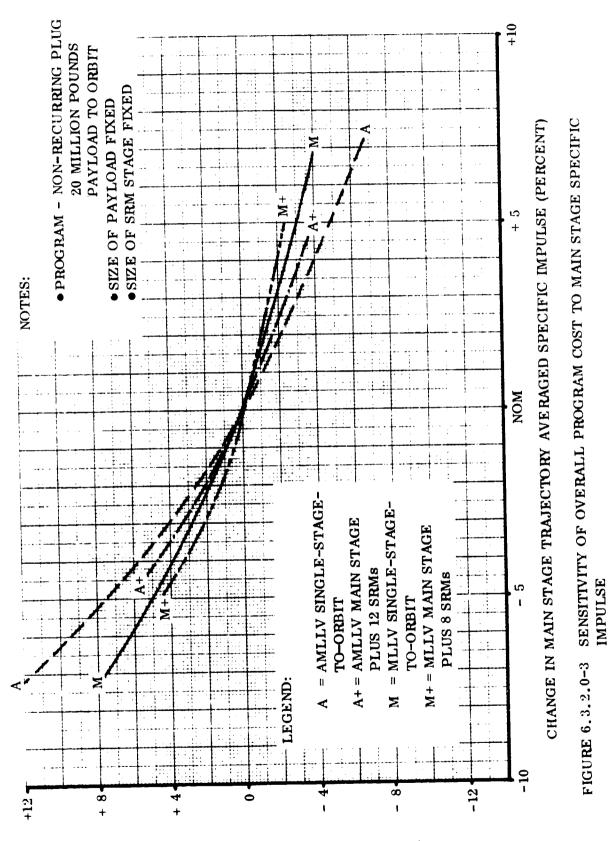
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7 СНАИСЕ IN ТОТАL РЯОСКАМ СОЗТ

TABLE 6.1.2.0-1 COST IMPLICATIONS OF A 2 PERCENT IMPROVEMENT IN MAIN STAGE TRAJECTORY AVERAGED SPECIFIC IMPULSE

Cost Reduction	NO.	MITA SINGLE		AMLLV SINGLE- STAGE-TO-ORBIT	BIT	MLLV MAIN STAGE + 8 SRM's	M's	AMLLV MAIN STAGE + 12 SRM's	t M' 3
Cost Reduction	OFR.	THUR TO-OT-TO-NIS	140	IN BITTIONS		\$ IN BILLIONS	£×	SNOITTIA NI \$	4
Due to Size Reduction									
			5	0.0409	1.61	0.0123	0.48	0.0243	0.77
Phases A & B	ž	0.040	35	0 0275	1, 08	0.0083	0.29	0. 0164	0. 45
	•	0.10.0	3	0.0446	1. 07	0.0135	0. 29	0.0266	0.45
(Inches 2	Z	0.0445		0 0763	1.05	0.0232	0.28	0.0455	0.43
RAD Flue.)	5 8	0. 0537	3 5 5 6	0. 1073	1. 04	0. 0325	0.28	0. 0638	0.43
Cost of Baseline Engines									
		0. 4540	22.20	0.6440	25.40	0. 4430	17.60	0.6440	20.40
Mana A ab	<u>۽</u>	14507	16.10	0.4920	19.40	0. 3507	12.40	0.4915	13, 60
	•	0.000	01.01	0 2240	19.70	0.5890	12.60	0.8240	12 36
	12	0. 2690	00 - 91	0.010	20.10	1. 0560	13.90	1.4640	14.00
	8 8	1. 4860 1. 4860	16.60	2.0820	20.20	1.4850	12.80	2.0820	14.10
Tem! Dollars Awilable for New Technology									
		0.8389	19.8	1.2044	23.60	0. 8068	11.9	1.1762	21.8
		1.0857	19.3	1. 5535	22.90	1.0503	11.5	1.5189	20.8
	12		18.6	2. 2252	22.60	1.5270	11.2	2.1778	20.1
	(¥	2.0141	18.2	2.8742	22.20	1.9653	10.9	2.8141	19.8
	3						ē		

6.3.2 (Continued)

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impulse. These figures indicate that the largest savings, from improvements in specific impulse, will accrue to the AMLLV type vehicles as opposed to similar MLLV type vehicles. The single-stage-to-orbit vehicles will have a more significant cost sensitivity to specific impulse than will the vehicles with a full complement of strap-on stages.

For the program size indicated on Figure 6.3.2.0-3 (i.e., Phases A and B plus 20 million pounds of operational payload to orbit), it appears that an improvement of five percent in main stage engine specific impulse for the AMLLV single-stage-to-orbit vehicle will result in an approximate reduction in overall program costs of 5 percent. A reduction of five in main stage engine specific impulse for this vehicle would increase program cost by approximately 7.5 percent.

6.3.3 Evaluation of Main Stage Engine Alternatives

A representative example of the methodology for evaluation of main stage engine alternatives is shown in Figure 6.3.3.0-1. This figure shows the maximum dollars; for R&D, production and launch of thirty-six MLLV single-stage-toorbit vehicles; which can be expended for R&D and production of the 2000 psi chamber pressure toroidal/aerospike (to replace the multichamber 'plug engine on the main stage) without increasing the overall program cost.

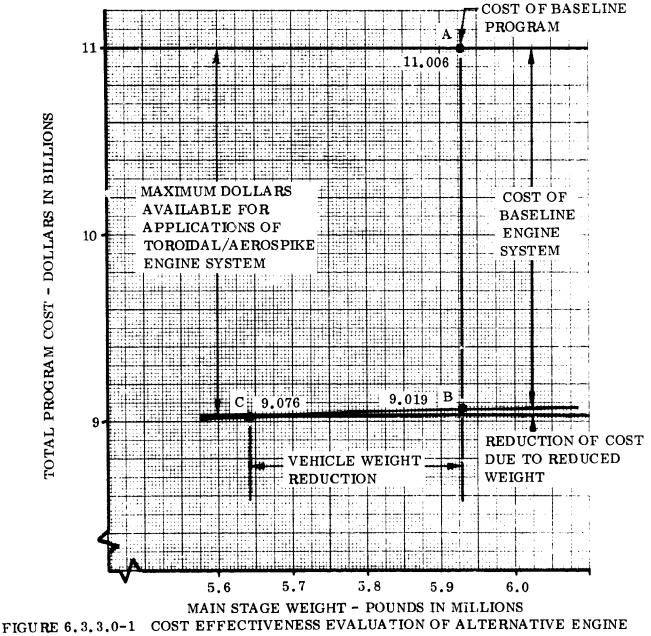
For this particular example the following conditions were assumed:

- a. Vehicle: MLLV single-stage-to-orbit vehicle main stage weight = 5.931 X 10⁶ pounds.
- b. Program Size: 36 launches @ 472,000 pounds of payload per launch.
- c. System Investigated: Engines
- d. Technology Change: Removal of the multichamber/plug engine system and replacement with a 2000 psi toroidal/aerospike engine (with eight modules). This latter engine will provide a 1.17% lower value for trajectory averaged specific impulse but its lower weight will result in an increase in the main stage mass fraction from 0.936 to 0.943.

The procedure was as follows:

a. The MLLV single-stage-to-orbit non-recurring cost of \$2.044 billion was determined from Figure 6.2.0.0-1.

- MLLV SINGLE STAGE TO A 100 N.M. EARTH ORBIT
- . PROGRAM NON-RECURRING PLUS 36 OPERATIONAL LAUNCHES
- , CHANGE OF ENGINE SYSTEM FROM MULTICHAMBER/ PLUG TO TOROIDAL/AEROSPIKE (2000 PSIA)



TECHNOLOGY

6.3.3 (Continued)

- b. The total MLLV single-stage-to-orbit recurring cost for thirty-six vehicles was determined from Figure 6.2.0.0-6 to be \$8.962 billion.
- c. These costs (a and b above) were then added to determine the total program costs for the baseline vehicle of \$11.006 billion (Plot point "A" in Figure 6.3.3.0-1).
- d. The cost of the multichamber/plug engine system was determined from Figures 6.2.0.0-1 and 6.2.0.0-6 (as in steps a, b and c above) to be \$1.930 billion.
- e. The total baseline program cost (excluding cost of the engine system) was determined to be \$9.076 billion by subtracting step d from step c. (Plot point B of Figure 6.3.2.0-1).
- f. From Figures 6.1.0.0-5 and/or 6.1.0.0-6, using the new values of I_{sp} and λ' (minus 1.0% and 0.943 respectively), the required new main stage weight was determined to be 5.64 million pounds.
- g. From Figures 6.2.0.0-1 and 6.2.0.0-6, the total accumulative new program costs (excluding the costs of the new engine system) were determined to be \$9.019 billion (Plot point C on Figure 6.3.3.0-1).

The cost difference between points B and C of \$57.0 million is the amount that the total program costs (exclusive of the costs of engines) will be reduced as a result of the decrease in main stage weight due to use of the alternative engine system. The cost difference between points A and B of \$1.930 billion is the sum of the non-recurring and recurring costs of the multichamber/plug engine to be replaced.

The total cost difference between points A and C of \$1.987 billion, then is the maximum amount which can be expended for development and application of the alternative engine system if it is to be cost effective.

Similar MLLV trades considering the 1200 psia toroidal/aerospike engine (28 modules) showed that with the lower Isp (3.07% lower) and the improved mass fraction (from 0.936 to 0.945), the required main stage weight would decrease to 5.905 X 10⁶ pounds. The maximum available dollars for development and application of this engine system (for a thirty-six unit operation program) is 1,936 billion dollars.

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7.0 COST REDUCTION ANALYSIS

The AMLLV/MLLV design, resource and cost studies were based upon the Saturn V design, development and production philosophies. No attempt was made to cost optimize the vehicles. The design, resources, and cost activities followed the Saturn V/S-IC philosophies to provide realistic output and to assure that the resulting cost data would be relatively comparable to actual historical Saturn V/S-IC data. The Saturn V philosophies to date have emphasized reliability with cost as a secondary consideration. Through the successful flights of the Apollo program, the reliability aspects have been proven and cost reduction is now receiving more emphasis. Currently, there are numerous activities underway to reduce the cost of the Saturn V vehicle systems. These studies have shown that costs may be reduced by from twenty-five to fifty percent of the current costs as the program matures and as the design, manufacture, test and launch philosophies are adjusted to better conform to the actual requirements of the operational phase.

The Saturn V cost reduction data in conjunction with a review of the MLLV / AMLLV study data was used to identify potential cost reduction areas for the MLLV single-stage-to-orbit vehicle. Similar analyses can be conducted for any of the MLLV/AMLLV configurations.

In the cost reduction analyses it was found that the results would be heavily biased by the initial assumptions or limitations established for conducting the analyses, i.e.:

- a. Almost any modification to the vehicle which will increase its payload capability will reduce the costs for a program requiring a fixed total amount of payload to orbit (if the additional payload capability can be utilized). This may not necessarily be the case.
- b. If the required payload per launch of the vehicle is fixed, improvements to the vehicle must be reflected by a reduced launch weight. This reduced launch weight will also be reflected in reduced program cost. This latter cost reduction (for the fixed payload per launch case) will, however, be only approximately 25 percent of that cost reduction possible if an increase in is allowable.

Either of the above assumptions could be valid depending on the specific circumstances. <u>A review of any of the data in this book should be accomplished</u> considering both of these assumptions.

7.1 POTENTIAL AREAS FOR COST REDUCTION

7.1.1 R&D Flight Tests

The baseline development test plan specifies two vehicles for R&D flight testing prior to manned flight. Each R&D flight test will consist of the launch of a highly instrumented launch vehicle with a dummy payload. If these R&D test vehicles could be utilized to deliver useful unmanned payloads, a significant reduction in program costs would be achieved. These payloads should be such that they would not be critical and could be replaced should the R&D tests be unsuccessful. The two R&D flight tests costs for the MLLV single-stage-to-crbit vehicle will be 731.8 million dollars. If useful payloads could be flown, the majority of this cost could be saved, i.e., \$529.8 million. Certain costs due to the longer launch cycle and to the increased instrumentation requirements, etc., would, however, still be attributed to these tests.

7.1.2 Dynamic Tests

Dynamic tests are specified to verify the structural and vibration characteristics of the launch vehicle by simulated flight dynamic loads. These tests will require a dynamic test stand and structurally complete stages less electrical and hydraulic components, engines and subsystems. (These latter elements will be simulated with appropriately mounted lump masses.) The structural components utilized in these tests will not be reused in the baseline flight program. For cost reduction, 1) the dynamic tests could possibly be deleted or 2) the dynamic tests could be conducted and the vehicle structural elements later used in a future noncritical unmanned vehicle launch. With the first approach, 53.1 million dollars could be saved from the MELV single-stage-to-orbit development test program or with the second approach, 23.5 million dollars could be saved from the optrational program.

7.1.3 Facilities Checkout Vehicle

A facilities checkout vehicle ("F" vehicle) was specified in the baseline program to determine the physical and functional compatibility of the stages and vehicle to the production, test and launch facilities; the equipment; the tooling and the procedures. The "F" vehicle will be essentially a complete vehicle with only the engines and some minor systems deleted. If the "F" vehicle could be deleted from the program, the savings would not be too significant as the tests performed using the facilities checkout vehicle would still have to be performed. If, however, the first R&D vehicle could be used for these tests, the deletion of the requirement for the separate facilities checkout vehicle hardware would reduce the non-recurring MLLV single-stage-to-orbit costs by 41 million dollars.

7.1.4 Static Tests

Static test firings of the main stage will be used in the baseline program to verify propulsion and control systems and to verify capability of all systems to function under the environment generated with full thrust. Under the AMLLV MLLV test and launch concept, the static firing tests will be performed at the launch site in the launch position. Deletion of static testing, therefore, would not significantly reduce facility, equipment or tooling requirements nor delete the major costs associated with the test stand as these elements would still be required for launch. However, deletion of static testing would reduce the time line for the launch cycle by 14.1 2 weeks, i.e.: 4.1 2 weeks required for static testing of the stage, three additional weeks required for silo refurbishment, and seven weeks required for stage refurbishment. The total baseline launch cycle with static testing is 32 weeks. Deletion of the static tests would reduce this time to 17 1 2 weeks and permits the launching of three vehicles per year from one launch pad instead of the two specified by the baseline program. (This could result in a cost savings of 373 million dollars for an additional launch complex should a rate of three per year be required. Recurring cost savings from better facility utilization would be 62 million doilars per launch.) If the launch rate remains at two per year, then these savings would not be achieved. Approximately 27 million dollars per MLLV single-stage-to-orbit would be saved by the deletion of the static firing tests. This assumes that the launch facility manhours can be reduced by the manhours required for static test (allowable variable launch facility headcount.) If a constant headcount is required, the only cost savings would be that associated with the reduction in instrumentation, parts refurbishment, and fuel. This cost savings would be only one million dollars per vehicle.

7.1.5 Main Stage Propulsion System (Two Position Nozzle)

The baseline multichamber plug engine propulsion system will contain a single position nozzle. Utilization of the two position nozzle (see Section 4.3.1.1. Volume ID would reduce the cost of the aft portion of the nozzle exit cone and at the same time reduce the size of the required engine system by providing improved sea level performance. The combination of lower weight and improved performance would not only reduce the cost of the engine but would also provide an increase of 2,556 pounds in orbital payload capability for the MLLV single-stage-to-orbit vehicle. This would have a significant effect on the recurring costs of programs where payload size was not limited. The cost savings on a 36 vehicle production program of the MLLV single-stage-to-orbit vehicle configuration for example would be approximately 50 million dollars. This value includes the savings resulting from the lower cost smaller engine system. and the savings that can be attributed to the increased payloads put up by the vehicles containing this engine system. (Note: If the payload capability of the vehicle is held constant at the baseline value and the overall vehicle size is reduced to compensate for the improved performance as discussed in Section 6.0. the resulting cost saving for the program will be \$13 million.)

7.1.6 Base Plug

With the use of the 24 multichamber/plug engine modules (each having the two position nozzle), it may be possible to delete the base plug with only a minor loss in engine performance. A preliminary estimate of the savings is 55.4 million dollars for a vehicle program consisting of 36 launches of the MLLV single-stage-to-orbit vehicle configuration. Further performance trades are required to verify this estimate.

7.1.7 Instrumentation

The systems portion of the MLLV vehicle costs will be significantly greater than the cost of the structure. An analysis of these system costs indicate that while the majority of the systems are required, a portion of the costs are attributable to redundant and/or excessive instrumentation. A reduction in this instrumentation could reduce the recurring costs by approximately 6.6 million dollars for the 36 vehicle MLLV single-stage-to-orbit vehicle program.

7.1.8 Major Component Tests

The sub-components and the major components that make up the main stage of the MLLV vehicle will each be subjected to separate tests and to extensive quality and reliability assurance operations. For example, the individual components of the hydrogen and LOX tanks will be subjected to numerous interim tests prior to the ultimate hydrostatic and mating tests. Similarly, the engines will be tested by the engine manufacture several times prior to receipt at the assembly facility. At the assembly facility, they will then be subjected to subsystems and interface tests and later to actual static firing test at the launch site. Similar type tests will be performed at successive levels of assembly on the electrical and hydraulic components. A reduction in the amount of testing through test deletion and 'or by combined systems testing would significantly reduce the costs of a stage. This number is not readily available without an extensive detailed analysis of historical data. However, a best engineering estimate of this cost saving is 4.1 million dollars per vehicle. For a 36 MLLV single-stage-to-orbit vehicle program, this would amount to a saving of 108 million dollars.

7.1.9 Design Philosophy

The design philosophy utilized for the AMLLV/MLLV was based upon that used in the Saturn V program which maximized the safety and reliability. Reducing this reliability slightly by increasing fabrication tolerances, reducing safety factors, and changing some of the design formula utilized to determine the size and shape of the structures could result in a significant decrease in stage weight and or complexity. This could have effects of decreasing the cost of fabrication

7.1.9 (Continued)

and for increasing the payload capability for a fixed vehicle size. For example, a reduction in the safety factor from 1.4 to 1.25 for load carrying structures would increase the payload of the MLLV single stage to orbit vehicle by approximately 6 percent. For a given program payload requirement equivalent to launch of 36 baseline vehicles, the estimated cost saving is \$928.7 million. (Note: If the payload capability of the vehicle is held constant at the baseline value and the overall vehicle size is reduced to compensate for the reduced structure weight; as discussed in Section 6.0; the resulting cost saving to the program will be \$228 million.)

7.1.10 Manufacturing Procedures

The production concept utilized in the fabrication of the Saturn V vehicles to date is one which provides specific areas for each type operation on each major component with separately assigned workers to each of these areas. While this concept improves reliability, by giving each worker a limited specific job to accomplish, and is efficient and cost effective for fabrication of large quantities of vehicles, it does not lend itself to low cost with a small production rate. Also with the concurrent changes in part design for successive units, flow through the production sequence must be paced by the time required to implement the change orders as they result from tests of similar earlier parts. Significant cost reductions at low production rates may be realized if the production is handled on a "model shop" basis where the workers have several different but related functions such that when a function is completed the workers can then accomplish the next successive similar operation. This approach would result in a minimum "idle" time with a significant reduction in the manufacturing manhours required to do a job. For the production and launch rate of two per year. it is estimated that savings of approximately 1,130 million dollars could be realized for a 36 MLLV single-stage-to-orbit vehicle program.

7.1.11 On-Board Test and Checkout

An on-board test and checkout system was described in Volume II (MLLV Design) of this report. In addition, its impact on the schedule and launch was discussed in Volume III, (Resource Implications). However, all of the cost data was generated without regard to having on-board test and checkout capability as the impact of these systems could not be realistically assessed. It is obvious that utilization of the on-board tests and checkout systems while increasing direct production costs would significantly reduce the large number of personnel required for pre-flight test and checkout operations. In addition, there would be some reduction in the test costs associated with interim manufacturing test operations. An estimate of savings that could possibly be realized with this system is approximately 150 million dollars for a thirty-six MLLV single-stageto-orbit vehicle program.

7.2 PROGRAM IMPACT OF COST REDUCTIONS

To assess the combined impact of all of the above cost reduction techniques, a program consisting of the "get ready", development test, manufacture and launch of 36 MLLV single stage to orbit vehicles was made. The baseline cost for this program will be \$11 billion. The 36 operational launches will put into orbit 16,979,000 pounds of payload at a total program cost of 648 dollars per pound.

Table 7.2.0.0-I lists the cost elements, as discussed above, where cost savings potential exist. The elements are listed in a sequence progressing from those which have the least potential risk to those which have the most potential risk. The amount of dollars that can be saved with each of these elements, as shown, include savings in both non-recurring and recurring costs. The overall included non-recurring cost savings of \$1.6 billion encompass deletion of the facilities checkout vehicle, deletion of dynamic test, base plug deletion for Phases A and B, design philosophy simplification and the use of the first two R&D flights for delivery of unmanned non-critical payload. The overall recurring includes cost savings for the 36 vehicle operational program of \$2.4 billion encompass static test deletion, major component test reduction, instrumentation reduction, base plug production deletion, engine nozzle modifications, changes to the manufacturing procedures and to the addition of the on-board test and checkout system to the vehicle. The total maximum potential cost savings is \$4.0 billion for the Phases A and B plus 36 launches. This reduction would result in a total program cost of delivered payload of \$412 per pound.

The data shown in Table 7.2.0.0-I shows that the majority of the program cost savings that can be realized will result from changes in design, manufacture. test and launch philosophies. Application of design or configuration alternatives will result in only minor cost savings if the current philosophies are maintained. Of the potential savings of \$4 billion, only the following savings are not attributable to changes in program philosophy:

Item	Potential Savings
Use of On-Board Test and Checkout	\$150M
Engine Nozzle Modification	50 M
Base Plug Deletion	55 M
Instrumentation Reduction	7 M
TOTAL	\$262 M

The sum of these elements represents only 6 1 '2 percent of the overall potential savings shown.

TABLE 7.2.0.0-ICOST REDUCTION FOR SINGLE STAGE TO ORBIT MLLVPROGRAM CONSISTING OF 36 VEHICLES

RISK RATING	COST ELEMENT	COST REDUCTION
1	2 R&D Flights	\$ 530 Million
2	On Board Test & Checkout	150 Million
3	Manufacturing Procedures	1,130 Million
4	Engine Nozzle Modification	50 Million (13M*)
5	Base Plug Deletion	55 Million
6	Facilities Checkout Vehicle Deleted	41 Million
7	Instrumentation, Reduction	7 Million
8	Major Component Test Reduction	108 Million
9	Dynamic Test Vehicle Deletion	53 Million
10	Static Test Deletion	970 Million
11	Design Philosophy	929 Million (228M*)
	TOTAL	\$4, 023 Million

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*As applicable, numbers in parentheses represent program cost savings if payload of each vehicle is maintained constant and overall size of the vehicle is reduced to compensate for the lower inert weight and/or increased performance. Other numbers represent cost savings if payload capability is allowed to increase and that this increased capability per launch can be used to reduce the number of launches or increase the effectiveness of the program by providing more payload per launch. Finance of the state best that a kit the

8.0 PROGRAM MANAGER'S ASSESSMENT

The final portion of the study activity consisted of a critical review of the data and study results by the program manager and members of the study team. This review indicated that this study (and the reference study) had resulted in a detailed conceptual design for launch vehicles which is attractive in terms of both cost performance and payload potential. This concept makes use of the operational simplicity of a single stage vehicle to transport payload to earth orbit. The Saturn V/Apollo program and related activities have advanced the technology base to the point that such a system is now feasible and can be developed and implemented within the current stage-of-the-art. The use of strap-on stages and injection stage modules in conjunction with the main stage (as developed for the single-stage-to-orbit application) will provide a series of vehicles capable of providing a range of payloads extending from that of the single-stage-to-orbit configuration up to four times that of the single-stage-to-orbit configuration. The flexibility and simplicity offered by these configuration options can provide significant cost advantages relative to previously considered systems for boosting large heavy payloads.

These studies, which investigated size effects, indicate that the single-stageto-orbit concept (with its various payload augmentation options) is applicable to a wide range of payload requirements and as such, a specific vehicle family could be tailored to accomplish any spectrum of missions.

This study also resulted in a comprehensive plan for implementation and operation of such vehicle systems with supporting cost detail. As the resource and cost data were developed in accordance with current operational philosophies and costing procedures, the results are directly comparable to existing data for current systems. The results define a fixed yardstick against which future improvements to improve performance or minimize cost can be measured. With the resulting data and the methodology developed for its use, the priorities for improving technology can be assessed relative to their cost/performance potential.

The results of this study and the detailed data developed are in sufficient depth to provide a comprehensive reference for follow-on Phase B activities. The method of presenting the data should provide a detailed format and guide for subsequent Phases B. C and D activities.

The study review indicated, however, that certain areas of the study received a disproportionate emphasis. The review also indicated certain minor inconsistencies between the design, resource and cost data.

Of the resource data generated, for example, the vehicle structures received far more emphasis than the other vehicle systems. Even though the estimated cost for the launch facility implementation and operation represented between

Continued)

30 to 50 percent of the total program cost, less emphasis was placed on detail ir this area than any of the areas. A more detailed breakdown of the costs associated with the launch facility and operations is required. While the estimates were provided from people actively working the launch area, it is felt that the estigates more nearly relate to current operations rather than to the AMLLV and MLLV vehicles. For example, according to the Chrysler "National Space Booster Study", the launch cost for a three stage Saturn V at the rate of two per year will be approximately \$84,000,000. While the MLLV single-stage-to-orbit vehicle will deliver twice the payload to orbit of a two stage Saturn V vehicle. its liftoff weight will be almost identical to that of the two stage Saturn V vehicle. The single-stage-to-orbit vehicle has only one stage wherein the Saturn V reference vehicle has three stages. The Saturn V also consists of two different probellant systems; a LOX/RP-1 and a LOX/LH₂ system. The cost estimates, however, despite the weight similarities and fewer number of components attributable to the MLLV, show that the launch operations cost for the MLLV singlestage-to-orbit vehicle, at a rate of two per year, will be \$88,500,000 per vehicle as compared to \$84,000,000 for the three stage Saturn V vehicle. Logic indicates that the MLLV launch costs should be on the order of 20 to 25 percent less than those shown. A more detailed study of the launch facility would provide cost estimates to a greater depth and would improve the confidence in the numbers generated.

By study groundrules, the location for the launch facility will be on land in the Launch Complex 39 area. The acoustical studies showed that many of the different possible configurations for the MLLV and AMLLV families could not be launched from such a site without creating a severe acoustical problem in the surrounding inhabited areas. As little can be done to reduce the launch noise that would occur from the rocket exhaust, the only practical solution would be to move the launch facility to a more remote site. This could be accomplished by locating the facility on some of the sand bars off shore at Cape Kennedy. locating the facility on offshore islands, or use of a floating launch facility. The launch complex shown was defined as a feasible facility, however, no detail studies were accomplished to optimize such a facility and its operations. There are many alternative ways for launching the vehicles other than the ones shown which may be more adaptable to location at these alternative sites.

Even though an on-board test and checkout system was specified by the design concept, the impact of such a system on the resource requirements could not adequately be assessed by this study. In the area of launch operations, such a system should drastically reduce the costs. Incorporation of such a system, however, would increase the initial cost for the design and development of the systems and would also increase costs for manufacturing and installation of the systems. Additional studies are required to define in detail: (1) the specific requirements for each of the on-board test and checkout elements as they relate

8.0 (Continued)

to their assigned subsystems, (2) the interface and integrated operation of the combined on-board test and checkout elements and (3) the necessary procedures and operations which should be associated with producing, testing and launching vehicles incorporating such systems.

Additional study is required to more adequately define the thermal environment in the base region during the flight regime. The best method of cooling this region should be defined through further design studies.

A review of the stress analysis showed that the toroidal tanks of the injection stage modules were designed for the cut-off acceleration of the maximum payload vehicles (i.e., main stage plus eight SR M stages plus a three module injection stage) of approximately 3.9 g's. The vehicle consisting of a main stage and a single module injection stage will fly a trajectory, however, such that the vehicle acceleration at cutoff of the main stage will be approximately 8 g's. This cutoff condition will, therefore, be beyond the design capability of toroidal tanks. Additional stress analysis and design detail is required to modify the design of the injection stage tankage such that it is adaptable to all of the potential vehicle configurations.

The review also showed that the specified design would not adapt to all of the possible eighteen configurations. To provide this total flexibility some additional studies are required to slightly modify the trajectories to minimize the loads for certain specific configurations (such as the main stage plus two strapon stages in the parallel burn mode). These trajectory modifications can be made such that the current design is acceptable to all of the potential configurations without seriously degrading the performance of any of the particular configurations.

Several numerical errors in the recording and buildup of cost data were uncovered during the assessment. Those errors which would have resulted in a significant variance in the study results, were corrected and the costing analyses and methodology were updated to incorporate these corrections. Certain small errors, which would not significantly effect the study results, were left uncorrected in order to avoid redoing the detailed compilation from raw data inputs through the detail cost buildups to the costing methodology.

The preparation of the figures and tables in this document was accomplished through considerable effort in abstracting the specific data from the bulk of data available. Lengthy computations were required to compile this data in a meaningful manner. These computations for the most part were accomplished manually. As stated above, many errors resulted during the detailed manual computation and transcribing of the data. These required extensive correction

8.0 (Continued)

and rework of the cost analyses. To improve the facility for similar cost analyses in the future, it is recommended that computer storage of the cost data be provided with the provision for easy access and updating of the data as required. In conjunction with the storage, a computer program with the capability of performing at least all of the calculations required for this volume should be provided. With this tool and the methodology developed by this report, detailed cost analyses could be run on a variety of systems in a matter of hours with minimal error (as compared to manual computation). The effects of changing costs due to improved design, different philosophy or changes in pricing factors could be evaluated expeditiously by changing the data in storage, machine computation of the problems, and selected data print-out. Ī

The studies indicated, that while costs can be affected by certain design or configuration improvements, operational and implementation philosophies primarily will determine the program costs. The one time use of the expendable vehicle components is a major cost driver. Further studies should be accomplished to cost optimize the vehicle design, to define low cost implementation and operational philosophies and to consider the potential of recovery and re-use of the main stage hardware.

Prior to implementation of systems such as the AMLLV and MLLV, many advances probably will be made in new materials and processes. The potential of these materials should be identified and studies conducted to show the proper methods for incorporation of these materials into the vehicle systems. Detailed resource plans similar to those provided for the baseline vehicles (with aluminum structures) should be prepared for selected structural material alternatives. Associated costs should then be determined and compared to the baseline costs. Such studies should be accomplished on a recurring periodic basis.

