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SIMPLIFIED PROCEDURES FOR ESTIMATING FLAPWISE BENDING MOMENTS ON HELICOPTER ROTOR BLADES

Part II - Tables

by Anton J. Landgrebe

Prepared by
UNITED AIRCRAFT CORPORATION
East Hartford, Conn.
for Langley Research Center

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PART II - TABLES

By Anton J. Landgrebe
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SUMMARY

Procedures and charts for estimating flapwise bending moments on helicopter rotor blades were presented in Part I*. As a supplement, tables are presented herein of the bending moment transfer coefficient information presented in chart form in Part I. Tabulated transfer coefficients are presented for each independent parameter of blade bending moment for nine combinations of mass and frequency parameter, and six advance ratios (0.25 to 1.4). Additional information, not presented in Part I, includes coefficients for the fourth and fifth harmonics for the low advance ratios (0.25 to 0.5), and six blade stations, instead of two, for the hingeless blade coefficients.

INTRODUCTION

Charts for estimating flapwise bending moments on helicopter rotor blades were presented in Part I. These charts consist of transfer coefficients relating independent rotor parameters to harmonics of bending moment for a wide range of blade design parameters and operating conditions of interest. Detailed procedures for using the transfer coefficients in conjunction with the performance charts of NASA CR-114 were described and illustrated with sample calculations. While the charts provide sufficient information and accuracy for most bending moment or bending stress requirements, certain applications may require a greater degree of accuracy than that obtainable from the charts. This may be particularly true for those designs or flight conditions where moment components contributed by the various independent parameters are of such a size that the net bending moment on the blade forms a small difference of large numbers. Therefore, an accurate digital representation of the moment transfer coefficients used for the charts of Part I are presented herein. In addition to the data presented in Part I, the tables include the fourth and fifth harmonic transfer coefficients for the low advance ratios (0.25 to 0.5) and four additional blade stations for the hingeless blade charts.

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*See NASA CR-1440, 1969.

SYMBOLS

A_{1_s}	Cosine component of first harmonic cyclic pitch; coefficient of $-\cos\psi$ term in Fourier series expansion of the blade pitch angle with respect to the rotor shaft, deg
B_{1_s}	Sine component of first harmonic cyclic pitch; coefficient of $-\sin\psi$ term in Fourier series expansion of the blade pitch angle with respect to the rotor shaft, deg
c (or C)	Cosine component of n^{th} harmonic
c_o	Blade chord at reference station, ft
E	Young's modulus of elasticity, $lb/in.^2$
FP	Frequency parameter, $EI_o/m_o(\Omega R)^2R^2$
I	Flapwise section area moment of inertia, $in.^4$
I_o	Flapwise section area moment of inertia at reference station, $in.^4$
m_o	Mass per unit span at reference station, slug/ft
M	Flapwise bending moment, positive when upper surface is in compression, in.-lb
$\overline{M}_{(\ )}$	Transfer function relating nondimensional bending moment to independent parameter ( )
$\overline{M}_{(\ ),n,c \text{ or } s}$	Transfer coefficient relating the n^{th} cosine or sine harmonic of nondimensional bending moment to independent parameter ( ) where ( ) can represent θ_{75}, θ_1, λ_c, or λ_s, A_{1_s}, B_{1_s}, or β_B, 1/deg except nondimensional for λ_c and λ_s
MP	Mass parameter, $\rho R c_o/2m_o$
MU	Rotor advance ratio; ratio of forward velocity component in plane of rotor to ΩR (same as μ)
n (or N)	Harmonic number appearing in Fourier expansion

SYMBOLS (Continued)

n_{max}	Maximum harmonic number required for determining flapwise bending moment
$\bar{r}$	Ratio of local section radius to rotor radius
R	Rotor radius, ft or in.
s(or S)	Sine component of n^{th} harmonic
β_B	Preconing angle for hingeless blade, deg
θ_l	Amplitude of linear blade twist, positive when tip angle is larger, deg
θ_{75}	Blade pitch angle at the 0.75R station, deg
λ_c	Rotor inflow ratio; ratio of velocity parallel to control axis (axis of no feathering) to ΩR, positive up
λ_s	Rotor inflow ratio; ratio of velocity parallel to shaft axis to ΩR, positive up
μ	Rotor advance ratio; ratio of forward velocity component in plane of rotor to ΩR
ρ	Air density, $slug/ft^3$
ψ	Blade azimuth angle measured from downstream blade position in direction of advancing blade, deg
Ω	Rotor rotational frequency, rad/sec

RELATION BETWEEN TRANSFER COEFFICIENTS AND FLAPWISE BENDING MOMENT

As described in detail in Part I, the transfer coefficients relate the independent rotor parameters to the flapwise bending moment at a given radial station and azimuth position. The transfer function for each independent parameter ( ) is equal to a harmonic summation of the negative Fourier series of transfer coefficients as shown by the following equation.

$$\overline{M}_{(\ )} = \overline{M}_{(\ ),0} - \sum_{n=1}^{n_{MAX}} \left(\overline{M}_{(\ ),n,c} \cos n\psi + \overline{M}_{(\ ),n,s} \sin n\psi \right)$$

For an articulated blade, the independent parameters ( ) are collective pitch (θ_{75}), blade twist (θ_1), and inflow ratio (λ_C). For a hingeless blade, the independent parameters are collective pitch (θ_{75}), blade twist (θ_1), inflow ratio (λ_S), cyclic pitch (A_{1S}) and (B_{1S}), and preconing (β_B). The total bending moment is obtained by scaling the independent parameters by the transfer functions and superposing the independent contributions in the following manner.

For an articulated blade,

$$M = \frac{EI}{R} \left(\overline{M}_{\theta_{75}} \theta_{75} + \overline{M}_{\theta_1} \theta_1 + \overline{M}_{\lambda_C} \lambda_C \right)$$

For a hingeless blade,

$$M = \frac{EI}{R} \left(\overline{M}_{\theta_{75}} \theta_{75} + \overline{M}_{\theta_1} \theta_1 + \overline{M}_{\lambda_S} \lambda_S + \overline{M}_{A_{1S}} A_{1S} + \overline{M}_{B_{1S}} B_{1S} + \overline{M}_{\beta_B} \beta_B \right)$$

UNITS AND SCALE FACTORS FOR TABULATED TRANSFER COEFFICIENTS

The transfer coefficients presented in the tables have units of 1/degree except for the inflow ratio transfer coefficients which are nondimensional.

The transfer coefficients were tabulated from computer punch cards which were punched concurrently with the printing of the computer output. Due to format limitations of the printout a scale factor was used. This scale factor

was included in the punch cards, and thus is also incorporated in the tables presented herein. It must be removed when using the tabulated transfer coefficients. The scale factor used is 100,000 except for the inflow ratio transfer coefficients for which it is 1000. Thus,

$$\bar{M}_{(\ ),\, n,\, c \text{ or } s} = \frac{\text{TABULATED VALUE}}{100{,}000}$$

for transfer coefficients for which the independent parameter ( ) is θ_{75}, θ_I, A_{IS}, B_{IS}, or β_B and,

$$\bar{M}_{\lambda,\, n,\, c \text{ or } s} = \frac{\text{TABULATED VALUE}}{1000}$$

for inflow ratio transfer coefficients λ_c or λ_s.

The coefficients are presented in exponential format. Thus, for example, the tabulated coefficient 0.123 + 02 = $0.123 \times 10^2 = 12.3$.

LIMITATIONS AND SCOPE OF TABULATED TRANSFER COEFFICIENTS

The following is a listing of the assumptions described in Part I which also apply to the tabulated transfer coefficients. However, reasonable extensions beyond the limits imposed by some of these assumptions can be made with little error, as discussed in Part I.

1. Blades with uniform mass and stiffness distributions
2. Constant chord blades
3. Low stiffness blades
4. Unstalled blades
5. Small offset (for articulated blades)
6. Negligible chordwise and torsional coupling
7. Linear twist blades

8. Conventional helicopter tip speeds below $\mu = 0.5$ ($\Omega R \cong 670$ ft/sec)

9. Advancing tip Mach number = 0.9 for $\mu > 0.5$

The range of the parameters influencing the tabulated transfer coefficients are summarized below.

Advance ratio	μ	= 0.25, 0.4, 0.5, 0.7, 1.0, 1.4
Mass parameter	MP	= 0.1, 0.3, 0.5
Frequency parameter	FP	= 0.001, 0.0025, 0.01 (for $\mu \leq 0.5$)
	FP	= $0.000447(1+\mu)^2$, $0.00112(1+\mu)^2$, $0.00447(1+\mu)^2$ (for $\mu > 0.5$)

The transfer coefficients have been tabulated for the following sets of independent parameters, blade stations, and harmonics.

Articulated blades -

Independent parameters: $\theta_{75}, \theta_1, \lambda_c$
Blade stations: $\bar{r}$ = 0.21, 0.35, 0.45, 0.55, 0.75, 0.85
Harmonics: n = 0 to 5 cosine and sine components

Hingeless blades -

Independent parameters: $\theta_{75}, \theta_1, \lambda_s, A_{1s}, B_{1s}, \beta_B$
Blade stations: $\bar{r}$ = 0.0, 0.14, 0.325, 0.55, 0.75, 0.85
Harmonics: n = 0 to 5 cosine and sine components

ORGANIZATION OF TABLES

A total of nine basic tables of transfer coefficients are presented. These are divided into a set of three tables applicable to articulated blades and a set of six tables applicable to hingeless blades. Each of the nine basic tables applies to a specific independent parameter (θ_{75}, θ_1, etc.) and is subdivided into nine parts (A through I) corresponding to nine combinations of mass parameter and frequency parameter (i.e., blade design). A single page of tabulated transfer coefficients corresponds to one blade design, and results for six advance ratios, six radial stations, and five harmonics are presented

for each design. The transfer coefficients are listed in the following harmonic order (N, COR S): steady (0), first through fifth harmonic cosine components (1-5, C), and first through fifth harmonic sine components (1-5, S). Listings of the contents of the tables for articulated and hingeless rotors are presented below.

Listing of Transfer Coefficient Tables for Articulated Rotors

Table No.	Root Constraint	Independent Parameter	Mass Parameter MP	Frequency Parameter	
				FP (For μ = 0.25, 0.4, 0.5)	$FP/(1+\mu)^2$ (For μ = 0.7, 1.0, 1.4)
1A	Articulated	θ_{75}	0.1	0.001	0.000447
1B	↓	↓	↓	0.0025	0.00112
1C	↓	↓	↓	0.01	0.00447
1D	↓	↓	0.3	0.001	0.000447
1E	↓	↓	↓	0.0025	0.00112
1F	↓	↓	↓	0.01	0.00447
1G	↓	↓	0.5	0.001	0.000447
1H	↓	↓	↓	0.0025	0.00113
1I	↓	↓	↓	0.01	0.00447
2A	↓	θ_1	0.1	0.001	0.00447
2B	↓	↓	↓	0.0025	0.00112
2C	↓	↓	↓	0.01	0.00447
2D	↓	↓	0.3	0.001	0.000447
2E	↓	↓	↓	0.0025	0.00112
2F	↓	↓	↓	0.01	0.00447
2G	↓	↓	0.5	0.001	0.000447
2H	↓	↓	↓	0.0025	0.00112
2I	↓	↓	↓	0.01	0.00447
3A	↓	λ_C	0.1	0.001	0.00447
3B	↓	↓	↓	0.0025	0.00112
3C	↓	↓	↓	0.01	0.00447
3D	↓	↓	0.3	0.001	0.000447
3E	↓	↓	↓	0.0025	0.00112
3F	↓	↓	↓	0.01	0.00447
3G	↓	↓	0.5	0.001	0.000447
3H	↓	↓	↓	0.0025	0.00112
3I	↓	↓	↓	0.01	0.00447

Listing of Transfer Coefficient Tables for Hingeless Rotors

Table No.	Root Constraint	Independent Parameter	Mass Parameter MP	Frequency Parameter	
				FP (For μ = 0.25, 0.4, 0.5)	$FP/(1+\mu)^2$ (For μ = 0.7, 1.0, 1.4)
4A	Hingeless	θ_{75}	0.1	0.001	0.000447
4B				0.0025	0.00112
4C				0.01	0.00447
4D			0.3	0.001	0.000447
4E				0.0025	0.00112
4F				0.01	0.00447
4G			0.5	0.001	0.000447
4H				0.0025	0.00112
4I				0.01	0.00447
5A		θ_1	0.1	0.001	0.000447
5B				0.0025	0.00112
5C				0.01	0.00447
5D			0.3	0.001	0.000447
5E				0.0025	0.00112
5F				0.01	0.00447
5G			0.5	0.001	0.000447
5H				0.0025	0.00112
5I				0.01	0.00447
6A		λ_s	0.1	0.001	0.000447
6B				0.0025	0.00112
6C				0.01	0.00447
6D			0.3	0.001	0.000447
6E				0.0025	0.00112
6F				0.01	0.00447
6G			0.5	0.001	0.000447
6H				0.0025	0.00112
6I				0.01	0.00447
7A		A_{1_s}	0.1	0.001	0.000447
7B				0.0025	0.00112
7C				0.01	0.00447
7D			0.3	0.001	0.000447
7E				0.0025	0.00112
7F				0.01	0.00447
7G			0.5	0.001	0.000447
7H				0.0025	0.00112
7I				0.01	0.00447
8A		B_{1_s}	0.1	0.001	0.000447
8B				0.0025	0.00112
8C				0.01	0.00447
8D			0.3	0.001	0.000447
8E				0.0025	0.00112
8F				0.01	0.00447
8G			0.5	0.001	0.000447
8H				0.0025	0.00112
8I				0.01	0.00447
9A		β_B	0.1	0.001	0.000447
9B				0.0025	0.00112
9C				0.01	0.00447
9D			0.3	0.001	0.00447
9E				0.0025	0.00112
9F				0.01	0.00447
9G			0.5	0.001	0.00447
9H				0.0025	0.00112
9I				0.01	0.00447

TABLES OF TRANSFER COEFFICIENTS OF FLAPWISE BENDING MOMENTS

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**** CAUTION ****

Divide Tabulated Values by 100,000
to obtain transfer coefficients for
θ_{75} , θ_1, A_{1_s}, B_{1_s}, or β_B
Divide Tabulated Values by 1000
to obtain transfer coefficients for
λ_c and λ_s

****

TABLE 1.
COLLECTIVE PITCH TRANSFER COEFFICIENTS FOR AN ARTICULATED BLADE

(A) MP = 0.1
FP = 0.001 (FOR MU = 0.25,0.4,0.5)
FP = 0.000447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S — ADVANCE RATIO, MU = 0.25

(0.21)R

0	.1789+03				
1-5,C	-.3081+02	-.9661+02	-.3017+02	-.3065+02	-.6260+01
1-5,S	.1164+03	.5886+01	-.1323+02	.2106+02	-.3002+02

(0.35)R

0	.3809+03				
1-5,C	-.7257+02	-.7774+02	-.3764+02	-.3262+02	-.5697+01
1-5,S	.2225+03	.7895+01	-.3847+02	.1443+02	-.3517+02

(0.45)R

0	.4572+03				
1-5,C	-.1009+03	-.6856+02	-.3430+02	-.2230+02	-.4214+01
1-5,S	.2766+03	.6092+01	-.5975+02	-.2328+01	-.2636+02

(0.55)R

0	.3827+03				
1-5,C	-.1231+03	-.3359+02	-.2557+02	-.3864+01	-.3569+01
1-5,S	.3004+03	.5169-00	-.8194+02	-.2813+02	-.6780+01

(0.75)R

0	-.3469+03				
1-5,C	-.1038+03	.1034+03	.1351+01	.4049+02	-.8360+01
1-5,S	.1696+03	-.2001+02	-.9660+02	-.8115+02	.5159+02

(0.85)R

0	-.4947+03				
1-5,C	-.6015+02	.1114+03	.6896+01	.3803+02	-.8288+01
1-5,S	.6747+02	-.1990+02	-.6724+02	-.6816+02	.5093+02

N,C OR S — ADVANCE RATIO, MU = 0.4

(0.21)R

0	.1293+03				
1-5,C	-.3884+02	-.1473+03	-.1286+02	.2789+02	.1638+01
1-5,S	.2169+03	-.3068+02	-.1814+02	-.6036+01	.2087+02

(0.35)R

0	.3222+03				
1-5,C	-.1178+03	-.2099+03	-.1974+02	.3079+02	.5064+01
1-5,S	.4218+03	-.8274+02	-.5820+02	-.2706+01	.1653+02

(0.45)R

0	.3871+03				
1-5,C	-.1704+03	-.1914+03	-.1851+02	.1852+02	.6347+01
1-5,S	.5327+03	-.1023+03	-.8871+02	.2867+01	.6403+01

(0.55)R

0	.3109+03				
1-5,C	-.2242+03	-.1028+03	-.9602+01	-.7539+01	.5087+01
1-5,S	.5867+03	-.1238+03	-.1143+03	.1009+02	-.5580+01

(0.75)R

0	-.4106+03				
1-5,C	-.1915+03	.2681+03	.3109+02	-.8389+02	-.8098+01
1-5,S	.3061+03	-.1483+03	-.1013+03	.2046+02	-.1692+02

(0.85)R

0	-.5451+03				
1-5,C	-.1069+03	.2956+03	.3405+02	-.7865+02	-.1030+02
1-5,S	.1053+03	-.1096+03	-.5897+02	.1575+02	-.1129+02

N,C OR S — ADVANCE RATIO, MU = 0.5

(0.21)R

0	.7224+02				
1-5,C	-.5402+02	-.2829+03	-.3459+02	.5929+02	-.7517+01
1-5,S	.2773+03	-.9836+02	-.3980+02	-.4899+02	.5562+01

(0.35)R

0	.2430+03				
1-5,C	-.1648+03	-.4145+03	-.5571+02	.8100+02	.4803+01
1-5,S	.5769+03	-.1731+03	-.1168+03	-.4549+02	-.1939+01

(0.45)R

0	.3027+03				
1-5,C	-.2487+03	-.5989+03	-.5883+02	.6224+02	.1579+02
1-5,S	.7448+03	-.2221+03	-.1749+03	-.2049+02	-.5053+01

(0.55)R

0	.2253+03				
1-5,C	-.3198+03	-.2638+03	-.4784+02	.2279+01	.2290+02
1-5,S	.8316+03	-.2736+03	-.2246+03	.2114+02	.3899-00

(0.75)R

0	-.4913+03				
1-5,C	-.2877+03	.3583+03	.2368+02	-.2222+03	.4886+01
1-5,S	.4873+03	-.3178+03	-.2056+03	.1152+03	.4661+02

(0.85)R

0	-.5941+03				
1-5,C	-.1762+03	.4337+03	.3889+02	-.2206+03	-.6228+01
1-5,S	.1970+03	-.2296+03	-.1235+03	.1014+03	.4923+02

N,C OR S — ADVANCE RATIO, MU = 0.7

(0.21)R

0	-.1002+03				
1-5,C	-.1215+03	-.6178+03	-.2261+03	-.1868+03	-.7503+01
1-5,S	.4554+03	-.2053+03	-.4755+03	-.2249+03	-.3397+03

(0.35)R

0	-.8483+02				
1-5,C	-.3033+03	-.1008+04	-.3274+03	-.5609+02	.7171+01
1-5,S	.8634+03	-.3881+03	-.7149+03	-.2267+03	-.3453+03

(0.45)R

0	-.9441+02				
1-5,C	-.4270+03	-.1034+04	-.3520+03	.8089+02	.2927+02
1-5,S	.1061+04	-.5153+03	-.8257+03	-.1348+03	-.1856+03

(0.55)R

0	-.1779+03				
1-5,C	-.5144+03	-.7357+03	-.3444+03	.1679+03	.6108+02
1-5,S	.1190+04	-.6404+03	-.9213+03	.2155+02	.1087+03

(0.75)R

0	-.5410+03				
1-5,C	-.3963+03	.7660+03	-.2130+03	-.2501+02	.1162+03
1-5,S	.7846+03	-.6939+03	-.9203+03	.3556+03	.7997+03

(0.85)R

0	-.4763+03				
1-5,C	-.2148+03	.9310+03	-.1127+03	-.1143+03	.8951+02
1-5,S	.3890+03	-.4686+03	-.6245+03	.3060+03	.6901+03

N,C OR S — ADVANCE RATIO, MU = 1.0

(0.21)R

0	-.5298+03				
1-5,C	-.2402+03	-.1041+04	-.7555+03	-.5880+03	-.1690+03
1-5,S	.9043+03	-.4160+03	-.1717+04	-.6554+03	-.1748+04

(0.35)R

0	-.9198+03				
1-5,C	-.6075+03	-.1921+04	-.1177+04	-.4409+03	-.2337+03
1-5,S	.1426+04	-.6042+03	-.2507+04	-.7331+03	-.1389+04

(0.45)R

0	-.1137+04				
1-5,C	-.8333+03	-.2130+04	-.1382+04	-.3178+02	-.1204+03
1-5,S	.1518+04	-.1078+04	-.2677+04	-.4948+03	-.4601+03

(0.55)R

0	-.1262+04				
1-5,C	-.9379+03	-.1715+04	-.1527+04	.5667+03	.1958+03
1-5,S	.1399+04	-.1329+04	-.2523+04	-.1382+02	.7269+03

(0.75)R

0	-.1066+04				
1-5,C	-.5292+03	.7632+03	-.1348+04	.1517+04	.1072+04
1-5,S	.5511+03	-.1336+04	-.1236+04	.1086+04	.2192+04

(0.85)R

0	-.6279+03				
1-5,C	-.2145+03	.1117+04	-.8325+03	.1138+04	.8957+03
1-5,S	.1707+03	-.8459+03	-.5261+03	.9197+03	.1573+04

N,C OR S — ADVANCE RATIO, MU = 1.4

(0.21)R

0	-.1356+04				
1-5,C	-.1000+04	-.1259+04	-.2537+04	-.3847+03	-.1345+04
1-5,S	.2121+04	-.5849+03	-.2971+04	-.5849+03	-.2214+04

(0.35)R

0	-.2369+04				
1-5,C	-.1908+04	-.2237+04	-.3760+04	-.4494+02	-.1346+04
1-5,S	.2875+04	-.1128+04	-.4561+04	-.9276+03	-.1511+04

(0.45)R

0	-.2901+04				
1-5,C	-.2316+04	-.2376+04	-.4451+04	.6145+03	-.4925+03
1-5,S	.2809+04	-.1523+04	-.4848+04	-.7949+03	-.3499+03

(0.55)R

0	-.3157+04				
1-5,C	-.2323+04	-.1734+04	-.5141+04	.1577+04	.1106+04
1-5,S	.2240+04	-.1875+04	-.4223+04	-.1882+03	.7470+03

(0.75)R

0	-.2268+04				
1-5,C	-.9873+03	.1033+04	-.5150+04	.2894+04	.4189+04
1-5,S	.3198+03	-.1814+04	-.6924+03	.1552+04	.1136+04

(0.85)R

0	-.1211+04				
1-5,C	-.3107+03	.1233+04	-.3242+04	.2016+04	.3094+04
1-5,S	-.1431+03	-.1099+04	.1066+03	.1323+04	.5818+03

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 1.
COLLECTIVE PITCH TRANSFER COEFFICIENTS FOR AN ARTICULATED BLADE

(B) MR = 0.1
FP = 0.0025 (FOR MU ≤ 0.25,0.4,0.5)
FP = 0.00112(1+MU)**2 (FOR MU ≥ 0.7,1.0,1.4)

N,C OR S — ADVANCE RATIO, MU = 0.25

(0.21)R

0	.1869+03				
1-S,C	-.1698+02	-.3292+02	-.2515+02	-.1432+01	.3223+02
1-S,S	.1131+03	-.3381+01	-.1748+02	-.9716+01	.2325+02

(0.35)R

0	.3579+03				
1-S,C	-.5158+02	-.4291+02	-.4082+02	-.6208+01	.2423+02
1-S,S	.2121+03	-.2515+01	-.3476+02	-.1187+02	.1896+02

(0.45)R

0	.3902+03				
1-S,C	-.7769+02	-.3224+02	-.4922+02	-.1253+02	.2591+01
1-S,S	.2606+03	-.2086+01	-.4496+02	-.1085+02	.3496+01

(0.55)R

0	.2878+03				
1-S,C	-.9644+02	-.3283+01	-.5489+02	-.2057+02	-.2757+02
1-S,S	.2719+03	-.3013+01	-.5082+02	-.8387+01	-.1848+02

(0.75)R

0	-.1896+03				
1-S,C	-.7855+02	.6744+02	-.4616+02	-.3064+02	-.6793+02
1-S,S	.1492+03	-.7847+01	-.3481+02	-.2120+01	-.5087+02

(0.85)R

0	-.2233+03				
1-S,C	-.4286+02	.5578+02	-.2697+02	-.2033+02	-.4798+02
1-S,S	.6464+02	-.6284+01	-.1790+02	-.4069-00	-.3591+02

N,C OR S — ADVANCE RATIO, MU = 0.4

(0.21)R

0	.1504+03				
1-S,C	-.5004+02	-.1553+03	-.1431+02	.8697+01	.2715+02
1-S,S	.2156+03	-.4043+02	-.4146+02	-.6624+01	.8533+01

(0.35)R

0	.3068+03				
1-S,C	-.1232+03	-.2106+03	-.1779+02	.9718+01	.2535+02
1-S,S	.4116+03	-.6605+02	-.8598+02	-.3831+01	.6260+01

(0.45)R

0	.3338+03				
1-S,C	-.1723+03	-.1865+03	-.1231+02	.5042+01	.1253+02
1-S,S	.5072+03	-.8272+02	-.1160+03	-.1031+00	.1789+01

(0.55)R

0	.2270+03				
1-S,C	-.2020+03	-.1002+03	.1043+01	-.4738+01	-.6962+01
1-S,S	.5261+03	-.9865+02	-.1376+03	.2828+01	-.3132+01

(0.75)R

0	-.2458+03				
1-S,C	-.1468+03	.1397+03	.3184+02	-.2504+02	-.3730+02
1-S,S	.2734+03	-.9856+02	-.1152+03	.1942+01	-.6846+01

(0.85)R

0	-.2577+03				
1-S,C	-.7585+02	.1331+03	.2574+02	-.1942+02	-.2772+02
1-S,S	.1116+03	-.6143+02	-.6534+02	.3306-00	-.4283+01

N,C OR S — ADVANCE RATIO, MU = 0.5

(0.21)R

0	.9894+02				
1-S,C	-.6991+02	-.2921+03	-.5504+02	.7482+01	-.9042+02
1-S,S	.2901+03	-.6772+02	-.9371+02	-.4026+02	-.7769+01

(0.35)R

0	.2347+03				
1-S,C	-.1725+03	-.4103+03	-.7896+02	.1867+02	-.7415+02
1-S,S	.5691+03	-.1216+03	-.1870+03	-.4024+02	-.1490+02

(0.45)R

0	.2564+03				
1-S,C	-.2436+03	-.3855+03	-.7957+02	.1442+02	-.2070+02
1-S,S	.7148+03	-.1597+03	-.2581+03	-.2707+02	-.1469+02

(0.55)R

0	.1502+03				
1-S,C	-.2904+03	-.2618+03	-.6452+02	-.8774+01	.5538+02
1-S,S	.7595+03	-.1951+03	-.2981+03	-.8212+01	-.6714+01

(0.75)R

0	-.2987+03				
1-S,C	-.2244+03	.1639+03	-.5139+01	-.7734+02	.1615+03
1-S,S	.4328+03	-.1935+03	-.2594+03	.1993+02	.2125+02

(0.85)R

0	-.2875+03				
1-S,C	-.1203+03	.1826+03	.8142+01	-.6323+02	.1156+03
1-S,S	.1920+03	-.1192+03	-.1503+03	.1578+02	.1932+02

N,C OR S — ADVANCE RATIO, MU = 0.7

(0.21)R

0	-.6991+02				
1-S,C	-.1319+03	-.6040+03	-.4880+03	-.2457+03	-.9390+03
1-S,S	.4715+03	-.1408+03	-.6530+03	-.1854+03	.2899+03

(0.35)R

0	-.7943+02				
1-S,C	-.2911+03	-.9339+03	-.6972+03	-.1647+03	-.8124+03
1-S,S	.8398+03	-.2781+03	-.9884+03	-.1961+03	.2267+03

(0.45)R

0	-.1121+03				
1-S,C	-.3911+03	-.9229+03	-.7687+03	-.3886+02	-.2764+03
1-S,S	.1023+04	-.3794+03	-.1140+04	-.1529+03	.3943+02

(0.55)R

0	-.1929+03				
1-S,C	-.4430+03	-.6268+03	-.7884+03	.7118+02	.5118+03
1-S,S	.1080+04	-.4659+03	-.1247+04	-.1134+03	-.2213+03

(0.75)R

0	-.3461+03				
1-S,C	-.3049+03	.3542+03	-.5841+03	.9154+02	.1595+04
1-S,S	.6791+03	-.4319+03	-.1049+04	-.7112+02	-.5487+03

(0.85)R

0	-.2452+03				
1-S,C	-.1532+03	.3993+03	-.3254+03	.4020+02	.1120+04
1-S,S	.3315+03	-.2529+03	-.6088+03	-.4456+02	-.3769+03

N,C OR S — ADVANCE RATIO, MU = 1.0

(0.21)R

0	-.4948+03				
1-S,C	-.2767+03	-.1096+04	-.1872+04	-.4478+03	-.5403+03
1-S,S	.9165+03	-.3417+03	-.1785+04	-.3749+03	.7449+03

(0.35)R

0	-.8704+03				
1-S,C	-.5697+03	-.1848+04	-.2733+04	-.3014+03	-.4706+03
1-S,S	.1319+04	-.6988+03	-.2649+04	-.4401+03	.7269+03

(0.45)R

0	-.1067+04				
1-S,C	-.7301+03	-.1976+04	-.3113+04	-.2388+02	-.1134+03
1-S,S	.1377+04	-.9579+03	-.2884+04	-.4129+03	.1925+03

(0.55)R

0	-.1142+04				
1-S,C	-.7769+03	-.1574+04	-.3317+04	.2848+03	.4400+03
1-S,S	.1228+04	-.1154+04	-.2748+04	-.3648+03	-.7681+03

(0.75)R

0	-.7633+03				
1-S,C	-.4477+03	.8029+02	-.2595+04	.5126+03	.1175+04
1-S,S	.4975+03	-.9830+03	-.1454+04	-.2356+03	-.2203+04

(0.85)R

0	-.3843+03				
1-S,C	-.2014+03	.3389+03	-.1441+04	.3156+03	.7993+03
1-S,S	.1815+03	-.5458+03	-.6560+03	-.1294+03	-.1529+04

N,C OR S — ADVANCE RATIO, MU = 1.4

(0.21)R

0	-.1281+04				
1-S,C	-.1014+04	-.1514+04	-.5201+04	.1986+03	.5606+03
1-S,S	.1837+04	-.5888+03	-.2259+04	-.3049+03	-.1713+03

(0.35)R

0	-.2196+04				
1-S,C	-.1761+04	-.2641+04	-.7739+04	.5083+03	.5087+03
1-S,S	.2453+04	-.1097+04	-.3364+04	-.5225+03	-.2571+02

(0.45)R

0	-.2652+04				
1-S,C	-.2075+04	-.2919+04	-.8897+04	.7896+03	.2870+03
1-S,S	.2389+04	-.1422+04	-.3358+04	-.4204+03	-.1509+03

(0.55)R

0	-.2764+04				
1-S,C	-.1988+04	-.2477+04	-.9411+04	.1035+04	.1386+02
1-S,S	.1921+04	-.1617+04	-.2519+04	-.1274+02	-.6267+03

(0.75)R

0	-.1776+04				
1-S,C	-.8598+03	-.3688+03	-.6911+04	.9537+03	-.2725+03
1-S,S	.5033+03	-.1223+04	.8163+02	.8519+03	-.1514+04

(0.85)R

0	-.9675+03				
1-S,C	-.3140+03	.1300+03	-.3667+04	.5312+03	-.1813+03
1-S,S	.9809+02	-.6412+03	.4429+03	.6347+03	-.1037+04

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 1.
COLLECTIVE PITCH TRANSFER COEFFICIENTS FOR AN ARTICULATED BLADE

(C) MP = 0.1
FP = 0.01 (FOR MU = 0.25,0.4,0.5)
FP = 0.00447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S — ADVANCE RATIO, MU = 0.25

(0.21)R

0	.1729+03				
1-S,C	-.2292+02	-.2853+02	-.1143+01	.4505+01	.5882+01
1-S,S	.1019+03	-.1050+02	-.3970+01	.8207+01	.5887+01

(0.35)R

0	.2660+03				
1-S,C	-.4403+02	-.3181+02	-.9170-00	.5583+01	.6765+01
1-S,S	.1683+03	-.1540+02	-.8600+01	.1125+02	.6671+01

(0.45)R

0	.2636+03				
1-S,C	-.5660+02	-.2256+02	-.8250-00	.4342+01	.4841+01
1-S,S	.1929+03	-.1811+02	-.1116+02	.1207+02	.6202+01

(0.55)R

0	.1862+03				
1-S,C	-.6197+02	-.6012+01	-.1135+01	.1523+01	.1158+01
1-S,S	.1857+03	-.1997+02	-.1173+02	.1183+02	.5552+01

(0.75)R

0	-.3066+02				
1-S,C	-.4119+02	.1884+02	-.1801+01	-.3378+01	-.4566+01
1-S,S	.9047+02	-.1586+02	-.6430+01	.7553+01	.3697+01

(0.85)R

0	-.4851+02				
1-S,C	-.2014+02	.1369+02	-.1170+01	-.2561+01	-.3309+01
1-S,S	.3755+02	-.8526+01	-.2790+01	.3783+01	.1977+01

N,C OR S — ADVANCE RATIO, MU = 0.4

(0.21)R

0	.1406+03				
1-S,C	-.4876+02	-.1117+03	-.1322+03	-.2044+02	-.4441+01
1-S,S	.2024+03	-.2085+02	-.4548+02	.1211+01	.5058-00

(0.35)R

0	.2204+03				
1-S,C	-.9099+02	-.1390+03	-.1923+03	-.2632+02	-.3600+01
1-S,S	.3373+03	-.3172+02	-.8276+02	.2657+01	-.1128+01

(0.45)R

0	.2130+03				
1-S,C	-.1127+03	-.1171+03	-.2109+03	-.2880+02	-.1850+01
1-S,S	.3862+03	-.3782+02	-.1033+03	.3787+01	-.1992+01

(0.55)R

0	.1344+03				
1-S,C	-.1170+03	-.6431+02	-.2052+03	-.3110+02	-.2219-00
1-S,S	.3750+03	-.4168+02	-.1103+03	.4619+01	-.1725+01

(0.75)R

0	-.6664+02				
1-S,C	-.6756+02	.3690+02	-.1199+03	-.2621+02	.7311-00
1-S,S	.1833+03	-.3227+02	-.7058+02	.3771+01	.7093-00

(0.85)R

0	-.6705+02				
1-S,C	-.3076+02	.3383+02	-.5698+02	-.1457+02	.3831-00
1-S,S	.7611+02	-.1714+02	-.3403+02	.1995+01	.8545-00

N,C OR S — ADVANCE RATIO, MU = 0.5

(0.21)R

0	.9647+02				
1-S,C	-.6203+02	-.2053+03	-.2359+03	-.4364+02	-.2205+01
1-S,S	.2739+03	-.4193+02	-.4885+02	.4049+01	.2075+02

(0.35)R

0	.1560+03				
1-S,C	-.1172+03	-.2655+03	-.3473+03	-.5072+02	.2594-00
1-S,S	.4649+03	-.6668+02	-.9761+02	.1024+02	.1643+02

(0.45)R

0	.1458+03				
1-S,C	-.1463+03	-.2351+03	-.3829+03	-.5425+02	.1524+01
1-S,S	.5433+03	-.6123+02	-.1267+03	.1732+02	.5853+01

(0.55)R

0	.6949+02				
1-S,C	-.1530+03	-.1462+03	-.3728+03	-.6196+02	.7536-00
1-S,S	.5347+03	-.9019+02	-.1382+03	.2512+02	-.6107+01

(0.75)R

0	-.1047+03				
1-S,C	-.8967+02	.4260+02	-.2149+03	-.6201+02	-.3363+01
1-S,S	.2757+03	-.6901+02	-.8920+02	.2673+02	-.1543+02

(0.85)R

0	-.8531+02				
1-S,C	-.4110+02	.4866+02	-.1012+03	-.3636+02	-.2705+01
1-S,S	.1104+03	-.3635+02	-.4285+02	.1531+02	-.9339+01

N,C OR S — ADVANCE RATIO, MU = 0.7

(0.21)R

0	-.3922+02				
1-S,C	-.1313+03	-.5607+03	-.1164+04	-.1669+03	.8976+01
1-S,S	.4521+03	-.5677+02	.4583+03	.7766+02	.1056+03

(0.35)R

0	-.9193+02				
1-S,C	-.1959+03	-.6632+03	-.1696+04	-.2274+03	-.1076+01
1-S,S	.6607+03	-.8941+02	.6806+03	.1385+03	.6235+02

(0.45)R

0	-.1347+03				
1-S,C	-.2212+03	-.5890+03	-.1878+04	-.2368+03	-.1458+02
1-S,S	.7334+03	-.1053+03	.7659+03	.1774+03	-.1754+02

(0.55)R

0	-.1664+03				
1-S,C	-.2229+03	-.4347+03	-.1855+04	-.2188+03	-.2797+02
1-S,S	.7265+03	-.1105+03	.7692+03	.1996+03	-.1050+03

(0.75)R

0	-.1356+03				
1-S,C	-.1397+03	-.1098+03	-.1124+04	-.1168+03	-.3110+02
1-S,S	.4423+03	-.7367+02	.4791+03	.1463+03	-.1551+03

(0.85)R

0	-.7106+02				
1-S,C	-.6796+02	-.2714+02	-.5408+03	-.5356+02	-.1732+02
1-S,S	.2131+03	-.3657+02	.2327+03	.7465+02	-.8992+02

N,C OR S — ADVANCE RATIO, MU = 1.0

(0.21)R

0	-.4196+03				
1-S,C	-.2415+03	-.9095+03	-.1053+04	.2398+03	.6903+02
1-S,S	.6877+03	-.4224+02	.1545+04	.2164+03	-.2575+02

(0.35)R

0	-.6316+03				
1-S,C	-.3333+03	-.1114+04	-.1491+04	.4293+03	.3601+02
1-S,S	.9082+03	-.8020+02	.2397+04	.3928+03	-.1160+03

(0.45)R

0	-.7171+03				
1-S,C	-.3514+03	-.1037+04	-.1609+04	.5486+03	-.1992+02
1-S,S	.9173+03	-.8531+02	.2785+04	.5060+03	-.2009+03

(0.55)R

0	-.7227+03				
1-S,C	-.3281+03	-.8260+03	-.1540+04	.6115+03	-.7838+02
1-S,S	.8153+03	-.6290+02	.2868+04	.5674+03	-.2688+03

(0.75)R

0	-.4456+03				
1-S,C	-.1772+03	-.2971+03	-.8720+03	.4341+03	-.1049+03
1-S,S	.3971+03	-.3597+02	.1828+04	.4058+03	-.2301+03

(0.85)R

0	-.2139+03				
1-S,C	-.8165+02	-.1091+03	-.4061+03	.2173+03	-.5925+02
1-S,S	.1738+03	-.1681+02	.8863+03	.2035+03	-.1205+03

N,C OR S — ADVANCE RATIO, MU = 1.4

(0.21)R

0	-.1006+04				
1-S,C	-.4379+03	-.7927+03	.4140+03	.2759+04	.4783+03
1-S,S	.1155+04	.3949+02	.1747+04	-.2934+03	-.3336+03

(0.35)R

0	-.1462+04				
1-S,C	-.5670+03	-.8961+03	.6672+03	.3995+04	.5767+03
1-S,S	.1439+04	.4134+02	.2767+04	-.2747+03	-.4085+03

(0.45)R

0	-.1610+04				
1-S,C	-.5601+03	-.7543+03	.7947+03	.4389+04	.5276+03
1-S,S	.1367+04	.3094+02	.3256+04	-.1647+03	-.3806+03

(0.55)R

0	-.1568+04				
1-S,C	-.4866+03	-.5108+03	.8317+03	.4264+04	.4103+03
1-S,S	.1121+04	.1609+02	.3372+04	-.2762+02	-.3040+03

(0.75)R

0	-.9032+03				
1-S,C	-.2241+03	-.7954+02	.5346+03	.2447+04	.1371+03
1-S,S	.4447+03	-.4199+01	.2136+04	.1114+03	-.1112+03

(0.85)R

0	-.4206+03				
1-S,C	-.9506+02	-.2236+01	.2580+03	.1138+04	.4776+02
1-S,S	.1745+03	-.4139+01	.1026+04	.7254+02	-.4145+02

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 1.
COLLECTIVE PITCH TRANSFER COEFFICIENTS FOR AN ARTICULATED BLADE

(D) MP = 0.3
FF = 0.001 (FOR MU = 0.25,0.4,0.5)
FF = 0.000447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N/C OR S — ADVANCE RATIO, MU = 0.25

(0.21)R

0	.5142+03				
1-5/C	-.2169+03	-.1255+02	-.6668+02	-.6705+01	-.6397+01
1-5/S	.5041+03	-.3459+02	-.3364+02	-.6287+01	-.7274+01

(0.35)R

0	.1123+04				
1-5/C	-.5956+03	.4997+02	-.8353+02	-.1135+02	-.5159+01
1-5/S	.6540+03	-.6837+02	-.8337+02	-.4988+01	-.1100+02

(0.45)R

0	.1316+04				
1-5/C	-.8555+03	.1374+03	-.6869+02	-.1244+02	-.2060+01
1-5/S	.7757+03	-.8663+02	-.1294+03	-.5747+01	-.1008+02

(0.55)R

0	.1094+04				
1-5/C	-.1052+04	.2863+03	-.2967+02	-.1073+02	.1742+01
1-5/S	.7595+03	-.4361+02	-.1726+03	-.1213+02	-.4720+01

(0.75)R

0	-.1055+04				
1-5/C	-.8202+03	.5241+03	.9952+02	.3330+01	.5947+01
1-5/S	.2961+03	-.3956+02	-.2218+03	-.4387+02	.1891+02

(0.85)R

0	-.1474+04				
1-5/C	-.4304+03	.4264+03	.1038+03	.6859+01	.4236+01
1-5/S	.2874+02	-.7855+02	-.1616+03	-.4144+02	.2033+02

N/C OR S — ADVANCE RATIO, MU = 0.4

(0.21)R

0	.3563+03				
1-5/C	-.3692+03	-.7076+02	-.2412+03	.1934+02	.2744+02
1-5/S	.6855+03	-.2026+03	-.1096+03	-.1066+03	-.4498+02

(0.35)R

0	.9004+03				
1-5/C	-.9859+03	.1177+03	-.3229+03	.1420+02	.4497+02
1-5/S	.1244+04	-.3101+03	-.2878+03	-.7145+02	-.5299+02

(0.45)R

0	.1063+04				
1-5/C	-.1426+04	.3774+03	-.2853+03	-.7629+01	.4218+02
1-5/S	.1564+04	-.4292+03	-.4612+03	-.3121+02	-.3956+02

(0.55)R

0	.8666+03				
1-5/C	-.1749+04	.7435+03	-.1553+03	-.4970+02	.1844+02
1-5/S	.1555+04	-.2014+03	-.6883+03	-.2011+02	-.9124+01

(0.75)R

0	-.1166+04				
1-5/C	-.1344+04	.1413+04	.3461+03	-.1659+03	-.9352+02
1-5/S	.5940+03	-.2490+03	-.1040+04	-.1773+03	.8308+02

(0.85)R

0	-.1540+04				
1-5/C	-.7053+03	.1132+04	.3810+03	-.1471+03	-.9997+02
1-5/S	.6624+02	-.1938+03	-.8030+03	-.1950+03	.8186+02

N/C OR S — ADVANCE RATIO, MU = 0.5

(0.21)R

0	.1397+03				
1-5/C	-.4916+03	-.1799+03	-.4328+03	.1807+02	-.2316+01
1-5/S	.8666+03	-.4086+03	-.6208+02	-.4061+03	-.1734+03

(0.35)R

0	.5892+03				
1-5/C	-.1361+04	.1176+03	-.6601+03	.5410+02	.4522+02
1-5/S	.1692+04	-.7167+03	-.3204+03	-.3238+03	.2255+03

(0.45)R

0	.7513+03				
1-5/C	-.1659+04	.3312+03	-.6746+03	.2134+02	.6897+02
1-5/S	.2117+04	-.7932+03	-.6484+03	-.1442+03	-.1762+03

(0.55)R

0	.5407+03				
1-5/C	-.2270+04	.1092+04	-.5289+03	-.1131+03	.5757+02
1-5/S	.2295+04	-.8556+03	-.1137+04	.4642+02	-.3289+02

(0.75)R

0	-.1414+04				
1-5/C	-.1759+04	.4030+04	.2858+03	-.6777+03	-.1256+03
1-5/S	.1219+04	-.4376+03	-.2147+04	.1238+03	.4771+03

(0.85)R

0	-.1078+04				
1-5/C	-.9152+03	.1601+04	.4456+03	-.6510+03	-.1557+03
1-5/S	.4316+03	-.2893+03	-.1747+04	.3339+02	.4773+03

N/C OR S — ADVANCE RATIO, MU = 0.7

(0.21)R

0	-.5154+03				
1-5/C	-.9357+03	-.3123+03	-.1409+04	-.1027+04	-.1048+04
1-5/S	.1412+04	-.1001+04	-.6641+03	-.1581+04	-.1538+04

(0.35)R

0	-.6200+03				
1-5/C	-.2058+04	-.3725+03	-.2195+04	-.6525+03	-.9961+03
1-5/S	.2464+04	-.1685+04	-.1205+04	-.1559+04	-.1630+04

(0.45)R

0	-.6582+03				
1-5/C	-.2724+04	-.1662+03	-.2502+04	-.1998+03	-.4560+03
1-5/S	.2951+04	-.2096+04	-.1836+04	-.9327+03	-.9932+03

(0.55)R

0	-.7826+03				
1-5/C	-.3061+04	.7285+03	-.2617+04	.2713+02	.4700+03
1-5/S	.3106+04	-.2483+04	-.2876+04	.6702+02	.2189+03

(0.75)R

0	-.1256+04				
1-5/C	-.1900+04	.3532+04	-.1900+04	-.9227+03	.2480+04
1-5/S	.1967+04	-.2589+04	-.5130+04	.2022+04	.3147+04

(0.85)R

0	-.9963+03				
1-5/C	-.8724+03	.2904+04	-.1086+04	-.1061+04	.2091+04
1-5/S	.9551+03	-.1748+04	-.4031+04	.1716+04	.2764+04

N/C OR S — ADVANCE RATIO, MU = 1.0

(0.21)R

0	-.1929+04				
1-5/C	-.2292+04	-.5943+03	-.3610+04	-.3397+04	-.3816+04
1-5/S	.2894+04	-.2696+04	-.1653+04	-.4232+04	-.3876+04

(0.35)R

0	-.3165+04				
1-5/C	-.4146+04	-.1572+04	-.5753+04	-.3106+04	-.4191+04
1-5/S	.4123+04	-.3706+04	-.3084+04	-.4476+04	-.3044+04

(0.45)R

0	-.3667+04				
1-5/C	-.4965+04	-.1534+04	-.6892+04	-.1573+04	-.2270+04
1-5/S	.4218+04	-.4396+04	-.4115+04	-.2828+04	-.1261+04

(0.55)R

0	-.3653+04				
1-5/C	-.5023+04	-.1009+04	-.7791+04	.6516+03	.1731+04
1-5/S	.3657+04	-.4993+04	-.5128+04	.1759+03	.6401+03

(0.75)R

0	-.1958+04				
1-5/C	-.2209+04	.1745+04	-.7197+04	.4164+04	.1106+05
1-5/S	.8508+03	-.4841+04	-.5440+04	.6458+04	.1922+04

(0.85)R

0	-.8347+03				
1-5/C	-.7641+03	.1839+04	-.4513+04	.3208+04	.9105+04
1-5/S	-.4020+02	-.3109+04	-.3550+04	.5353+04	.1117+04

N/C OR S — ADVANCE RATIO, MU = 1.4

(0.21)R

0	-.4561+04				
1-5/C	-.7251+04	.2223+04	-.5306+04	-.5241+04	-.4041+04
1-5/S	.5907+04	-.4833+04	-.3731+04	-.3684+04	.3310+04

(0.35)R

0	-.6543+04				
1-5/C	-.1059+05	.2769+04	-.9169+04	-.4361+04	-.4920+04
1-5/S	.7502+04	-.5477+04	-.2583+04	-.4198+04	.4142+04

(0.45)R

0	-.7001+04				
1-5/C	-.1103+05	.2585+04	-.1190+05	-.1331+04	-.3030+04
1-5/S	.7040+04	-.4985+04	-.9174+03	-.2194+04	.2010+04

(0.55)R

0	-.6705+04				
1-5/C	-.1014+05	.2066+04	-.1455+05	.2997+04	.1395+04
1-5/S	.6504+04	-.4381+04	-.3002+03	.2104+04	-.3136+04

(0.75)R

0	-.3841+04				
1-5/C	-.8340+04	.6377+03	-.1476+05	.9037+04	.1121+05
1-5/S	.3743+03	-.3381+04	.3224+03	.1109+05	-.1462+05

(0.85)R

0	-.1013+04				
1-5/C	.7202+03	.1886+03	-.9188+04	.6463+04	.8838+04
1-5/S	-.5654+03	-.2131+04	.6710+03	.8578+04	-.1135+05

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 1.
COLLECTIVE PITCH TRANSFER COEFFICIENTS FOR AN ARTICULATED BLADE

(E) MP = 0.3
FP = 0.0025 (FOR MU = 0.25,0.4,0.5)
FP = 0.00112(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S					
ADVANCE RATIO, MU = 0.25					
		(0,1)R			
0	.5609+03				
1-S,C	-.2407+03	-.1697+02	-.6348+02	.1982-00	.1043+02
1-S,S	.3593+03	-.8781+02	-.4266+02	-.1452+02	-.4758+01
		(0,35)R			
0	.1066+04				
1-S,C	-.5710+03	.3886+02	-.8084+02	-.3399+01	.8916+01
1-S,S	.6341+03	-.9794+02	-.9036+02	-.1181+02	-.4260+01
		(0,45)R			
0	.1149+04				
1-S,C	-.7841+03	.1180+03	-.7189+02	-.8422+01	.2686+01
1-S,S	.7425+03	-.8685+02	-.1271+03	-.7608+01	-.2065+01
		(0,55)R			
0	.8373+03				
1-S,C	-.9021+03	.2218+03	-.4597+02	-.1520+02	-.6733+01
1-S,S	.7262+03	-.7309+02	-.1603+03	-.5810+01	.9802-00
		(0,75)R			
0	-.5866+03				
1-S,C	-.6241+03	.3382+03	.2215+02	-.2318+02	-.2103+02
1-S,S	.2972+03	-.5221+02	-.1577+03	-.1147+02	.5156+01
		(0,85)R			
0	-.6732+03				
1-S,C	-.3152+03	.2286+03	.2560+02	-.1575+02	-.1530+02
1-S,S	.9076+02	-.3270+02	-.9575+02	-.9519+01	.3740+01

N,C OR S					
ADVANCE RATIO, MU = 0.4					
		(0,1)R			
0	.4165+03				
1-S,C	-.4029+03	-.9079+02	-.2629+03	-.2900+02	-.1309+01
1-S,S	.6651+03	-.2547+03	.1454+03	-.1040+03	-.8511+02
		(0,35)R			
0	.8612+03				
1-S,C	-.9540+03	.6633+02	-.3501+03	-.3405+02	.1316+02
1-S,S	.1263+04	-.3350+03	-.3347+03	-.8631+02	-.8634+02
		(0,45)R			
0	.9397+03				
1-S,C	-.1300+04	.2952+03	-.3256+03	-.4439+02	.1930+02
1-S,S	.1426+04	-.3475+03	-.5049+03	-.5556+02	-.4926+02
		(0,55)R			
0	.6397+03				
1-S,C	-.1562+04	.5891+03	-.2267+03	-.7037+02	.1344+02
1-S,S	.1412+04	-.3425+03	-.6872+03	-.3883+02	.1405+02
		(0,75)R			
0	-.6939+03				
1-S,C	-.1030+04	.9067+03	.6529+02	-.1264+03	-.2631+02
1-S,S	.5890+03	-.2634+03	-.7781+03	-.6795+02	.1265+02
		(0,85)R			
0	-.7295+03				
1-S,C	-.5143+03	.8105+03	.9396+02	-.9182+02	-.2625+02
1-S,S	.1857+03	-.1558+03	-.4945+03	-.5678+02	.9720+02

N,C OR S					
ADVANCE RATIO, MU = 0.5					
		(0,1)R			
0	.2205+03				
1-S,C	-.5420+03	-.2173+03	-.5032+03	-.1722+03	-.1781+03
1-S,S	.8708+03	-.4730+03	-.1592+03	-.3227+03	-.2056+03
		(0,35)R			
0	.5810+03				
1-S,C	-.1249+04	.1262+02	-.7370+03	-.1540+03	-.1282+03
1-S,S	.1041+04	-.7269+03	-.4479+03	-.2739+03	-.2353+03
		(0,45)R			
0	.6599+03				
1-S,C	-.1697+04	.3667+03	-.7573+03	-.1276+03	-.1869+02
1-S,S	.2000+04	-.3445+03	-.7698+03	-.1416+03	-.1529+03
		(0,55)R			
0	.3481+03				
1-S,C	-.1959+04	.3159+03	-.6337+03	-.1421+03	.1167+03
1-S,S	.2073+04	-.9124+03	-.1176+04	.5432+01	.2018+02
		(0,75)R			
0	-.8764+03				
1-S,C	-.1329+04	.1295+04	-.9326+02	-.2612+03	.2617+03
1-S,S	.1084+04	-.7395+03	-.1572+04	.1325+03	.3848+02
		(0,85)R			
0	-.8264+03				
1-S,C	-.6604+03	.6712+03	.4657+02	-.2005+03	.1773+03
1-S,S	.4482+03	-.4294+03	-.1044+04	.8401+02	.3062+03

N,C OR S					
ADVANCE RATIO, MU = 0.7					
		(0,1)R			
0	-.4170+03				
1-S,C	-.9437+03	-.6362+03	-.2095+04	-.1727+04	-.2274+04
1-S,S	.1393+04	-.1022+04	-.6930+03	-.8673+03	.3515+02
		(0,35)R			
0	-.5516+03				
1-S,C	-.1902+04	-.9132+03	-.3133+04	-.1526+04	-.2037+04
1-S,S	.2348+04	-.1741+04	-.1252+04	-.8051+03	-.3409+02
		(0,45)R			
0	-.6295+03				
1-S,C	-.2425+04	-.9154+03	-.3535+04	-.9264+03	-.7838+03
1-S,S	.2701+04	-.2177+04	-.1047+04	-.4710+03	-.1862+03
		(0,55)R			
0	-.7426+03				
1-S,C	-.2664+04	-.2183+03	-.3652+04	-.3093+03	.1116+04
1-S,S	.2817+04	-.2494+04	-.2645+04	-.3502+02	-.4296+03
		(0,75)R			
0	-.8250+03				
1-S,C	-.1552+04	.1771+04	-.2603+04	.1513+03	.3838+04
1-S,S	.1634+04	-.2125+04	-.3385+04	.5007+03	-.7697+03
		(0,85)R			
0	-.5295+03				
1-S,C	-.7158+03	.1356+04	-.1410+04	.7369+02	.2723+04
1-S,S	.7643+03	-.1219+04	-.2195+04	.3574+03	-.5268+03

N,C OR S					
ADVANCE RATIO, MU = 1.0					
		(0,1)R			
0	-.1796+04				
1-S,C	-.2199+04	-.8154+03	-.4927+04	-.3388+04	-.1744+04
1-S,S	.2668+04	-.2414+04	-.2722+03	-.6837+03	.1496+04
		(0,35)R			
0	-.2933+04				
1-S,C	-.3739+04	-.1575+04	-.7556+04	-.3028+04	-.1618+04
1-S,S	.3659+04	-.3863+04	-.1065+04	-.7263+03	.1527+04
		(0,55)R			
0	-.3368+04				
1-S,C	-.4318+04	-.1763+04	-.8885+04	-.1694+04	-.7342+03
1-S,S	.3669+04	-.4601+04	-.1715+04	-.3302+03	.2302+03
		(0,55)R			
0	-.3317+04				
1-S,C	-.4172+04	-.1412+04	-.9675+04	-.9491+02	.5923+03
1-S,S	.3102+04	-.4972+04	-.2193+04	.4136+03	-.2255+04
		(0,75)R			
0	-.1748+04				
1-S,C	-.1868+04	-.2058+03	-.7647+04	.1554+04	.2359+04
1-S,S	.1019+04	-.3709+04	-.1817+04	.1613+04	-.6195+04
		(0,85)R			
0	-.7669+03				
1-S,C	-.7163+03	.4199+03	-.4232+04	.1042+04	.1627+04
1-S,S	.2919+03	-.1993+04	-.9739+03	.1142+04	-.4310+04

N,C OR S					
ADVANCE RATIO, MU = 1.4					
		(0,1)R			
0	-.3964+04				
1-S,C	-.6624+04	.9685+03	-.6316+04	-.1530+04	.3746+04
1-S,S	.5245+04	-.4611+04	.4390+04	.9027+03	.1259+03
		(0,35)R			
0	-.5744+04				
1-S,C	-.1069+05	.9961+03	-.1053+05	-.5616+03	.2734+04
1-S,S	.6751+04	-.5665+04	.4844+04	.7467+03	.2353+03
		(0,45)R			
0	-.6213+04				
1-S,C	-.1071+05	.1571+03	-.1301+05	.1189+04	.5068+03
1-S,S	.6351+04	-.5390+04	.4648+04	.1486+04	-.2455+03
		(0,55)R			
0	-.5931+04				
1-S,C	-.9307+04	-.4188+03	-.1448+05	.3322+04	-.2068+04
1-S,S	.4912+04	-.4578+04	.4681+04	.3420+04	-.1352+04
		(0,75)R			
0	-.3261+04				
1-S,C	-.2872+04	-.3083+03	-.1108+05	.4934+04	-.4126+04
1-S,S	.1063+04	-.2214+04	.4338+04	.6436+04	-.3071+04
		(0,85)R			
0	-.1523+04				
1-S,C	-.6868+03	-.4828+03	-.5899+04	.3020+04	-.2539+04
1-S,S	.1004+03	-.1017+04	.2601+04	.4267+04	-.2062+04

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 1.
COLLECTIVE PITCH TRANSFER COEFFICIENTS FOR AN ARTICULATED BLADE

(F) MP = 0.3
FP = 0.01 (FOR MU = 0.25,0.4,0.5)
FP = 0.00447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N:C OR S		ADVANCE RATIO, MU = 0.25			
		(0.21)R			
0	.5169+03				
1-S:C	-.2543+03	-.3074+02	-.9327+02	-.1022+022	-.5262-01
1-S:S	.3267+03	-.0615+02	-.2543+02	.7676-00	.1980+01
		(0.35)R			
0	.7945+03				
1-S:C	-.4641+03	-.0341+01	-.1285+03	-.1342+02	.1158+01
1-S:S	.5228+03	-.0339+02	-.5665+02	.1866+01	.1237+01
		(0.45)R			
0	.7336+03				
1-S:C	-.5084+03	.3448+02	-.1335+03	-.1510+02	.1612+01
1-S:S	.5827+03	-.0382+02	-.7832+02	.2392+01	.5796-00
		(0.55)R			
0	.5477+03				
1-S:C	-.5057+03	.0170+02	-.1215+03	-.1683+02	.1106+01
1-S:S	.5419+03	-.7812+02	-.9069+02	.2330+01	.5267-00
		(0.75)R			
0	-.1026+03				
1-S:C	-.3345+03	.1067+03	-.6062+02	-.1477+02	-.1080+01
1-S:S	.2301+03	-.4837+02	-.6549+02	.8309-00	.1407+01
		(0.85)R			
0	-.1514+03				
1-S:C	-.1917+03	.0386+02	-.2679+02	-.8282+01	-.9961-00
1-S:S	.9003+02	-.2448+02	-.3294+02	.2251-00	.1027+01

N:C OR S		ADVANCE RATIO, MU = 0.4			
		(0.21)R			
0	.4059+03				
1-S:C	-.4164+03	-.4288+03	-.4004+03	-.9959+02	-.3173+02
1-S:S	.6059+03	-.4936+03	-.8309+02	-.2980+01	.1154+00
		(0.35)R			
0	.6450+03				
1-S:C	-.7077+03	-.6473+02	-.5701+03	-.1270+03	-.2573+02
1-S:S	.9969+03	-.4691+03	-.2054+03	.2970+01	-.1073+02
		(0.45)R			
0	.6269+03				
1-S:C	-.9427+03	.1871+02	-.6065+03	-.1354+03	-.1451+02
1-S:S	.1116+04	-.2886+03	-.3919+02	.8005+01	-.1684+02
		(0.55)R			
0	.4010+03				
1-S:C	-.9726+03	.1486+03	-.5638+03	-.1407+03	-.5443+01
1-S:S	.1049+04	-.2795+03	-.3703+03	.1059+02	-.1646+02
		(0.75)R			
0	-.1445+03				
1-S:C	-.6566+03	.2529+03	-.2892+03	-.1111+03	-.1779+01
1-S:S	.4695+03	-.1695+03	-.2964+03	.6109+01	-.2005+01
		(0.85)R			
0	-.1960+03				
1-S:C	-.2517+03	.1536+03	-.1287+03	-.6072+02	-.1718+01
1-S:S	.1683+03	-.0281+02	-.1549+03	.2456+01	.1496+01

N:C OR S		ADVANCE RATIO, MU = 0.5			
		(0.21)R			
0	.2655+03				
1-S:C	-.3579+03	-.4927+03	-.7394+03	-.2590+03	-.7118+02
1-S:S	.6260+03	-.5566+03	-.4492+02	.7358+01	.5480+02
		(0.35)R			
0	.4483+03				
1-S:C	-.1013+04	-.4716+03	-.1088+04	-.3034+03	-.5311+02
1-S:S	.1371+04	-.5415+03	-.2147+03	.3635+02	.1747+02
		(0.45)R			
0	.4166+03				
1-S:C	-.1263+04	-.4294+03	-.1165+04	-.3015+03	-.2380+02
1-S:S	.1379+04	-.6143+03	-.3852+03	.6737+02	-.2790+02
		(0.55)R			
0	.2059+03				
1-S:C	-.1279+04	.7154+02	-.1126+04	-.2987+03	-.5100-00
1-S:S	.1332+04	-.6206+03	-.5389+03	.9737+02	-.6434+02
		(0.75)R			
0	-.2924+03				
1-S:C	-.7372+03	.4943+03	-.5988+03	-.2362+03	.5395+01
1-S:S	.7053+03	-.5899+03	-.5091+03	.9691+02	-.6151+02
		(0.85)R			
0	-.2400+03				
1-S:C	-.5363+03	.1967+03	-.2699+03	-.1313+03	.9418-00
1-S:S	.3202+03	-.4906+03	-.2793+03	.5405+02	-.3125+02

N:C OR S		ADVANCE RATIO, MU = 0.7			
		(0.21)R			
0	-.2151+03				
1-S:C	-.9568+03	-.1139+04	-.2567+04	-.8640+03	-.1392+03
1-S:S	.1308+04	-.6124+03	.6570+03	.4970+03	.4470+03
		(0.35)R			
0	-.3852+03				
1-S:C	-.1427+04	-.1340+04	-.3744+04	-.1105+04	-.1913+03
1-S:S	.1908+04	-.9160+03	.7767+03	.7977+03	.3157+03
		(0.45)R			
0	-.4903+03				
1-S:C	-.1598+04	-.1181+04	-.4149+04	-.1078+04	-.2009+03
1-S:S	.2114+04	-.1037+04	.6891+03	.9528+03	.3215+02
		(0.55)R			
0	-.5513+03				
1-S:C	-.1598+04	-.9608+03	-.4102+04	-.9172+03	-.1874+03
1-S:S	.2090+04	-.1047+04	.5079+03	.1012+04	-.2898+03
		(0.75)R			
0	-.4056+03				
1-S:C	-.9859+03	-.2019+03	-.2490+04	-.4018+03	-.1021+03
1-S:S	.1260+04	-.0581+03	.1273+03	.6867+03	-.5111+03
		(0.85)R			
0	-.2059+03				
1-S:C	-.4774+03	-.4372+02	-.1198+04	-.1676+03	-.4718+02
1-S:S	.6103+03	-.3206+03	.3111+02	.3427+03	-.3019+03

N:C OR S		ADVANCE RATIO, MU = 1.0			
		(0.21)R			
0	-.1345+04				
1-S:C	-.1871+04	-.1852+04	-.3683+04	.2494+03	.1665+03
1-S:S	.1944+04	-.9784+03	.3457+04	.1212+04	-.1107+03
		(0.35)R			
0	-.1976+04				
1-S:C	-.2542+04	-.2423+04	-.5329+04	.8667+03	.9017+02
1-S:S	.2604+04	-.1300+04	.5080+04	.2020+04	-.3752+03
		(0.45)R			
0	-.2203+04				
1-S:C	-.2840+04	-.2423+04	-.5857+04	.1424+04	-.4127+02
1-S:S	.2868+04	-.1321+04	.5657+04	.2468+04	-.6127+03
		(0.55)R			
0	-.2180+04				
1-S:C	-.2462+04	-.2128+04	-.5718+04	.1857+04	-.1793+03
1-S:S	.2413+04	-.1183+04	.5595+04	.2654+04	-.7966+03
		(0.75)R			
0	-.1366+04				
1-S:C	-.1267+04	-.1008+04	-.3347+04	.1555+04	-.2443+03
1-S:S	.1220+04	-.5859+03	.3349+04	.1799+04	-.6651+03
		(0.85)R			
0	-.6264+03				
1-S:C	-.5716+03	-.4357+03	-.1578+04	.8104+03	-.1382+03
1-S:S	.5401+03	-.2585+03	.1590+04	.8888+03	-.3465+03

N:C OR S		ADVANCE RATIO, MU = 1.4			
		(0.21)R			
0	-.3177+04				
1-S:C	-.3161+04	-.3684+03	.6312+03	.6034+04	.1471+04
1-S:S	.3463+04	-.0475+03	.7499+04	-.5572+03	-.1601+04
		(0.35)R			
0	-.4450+04				
1-S:C	-.3965+04	-.1730+03	.1021+04	.9301+04	.1632+04
1-S:S	.4414+04	-.7439+03	.1067+05	-.2085+03	-.1797+04
		(0.45)R			
0	-.4762+04				
1-S:C	-.3776+04	.1389+03	.1220+04	.1073+05	.1337+04
1-S:S	.4299+04	-.9758+03	.1196+05	.3171+03	-.1497+04
		(0.55)R			
0	-.4456+04				
1-S:C	-.3050+04	.1526+03	.1280+04	.1092+05	.8598+03
1-S:S	.3647+04	.0109+02	.1163+05	.8354+03.	-.9942+03
		(0.75)R			
0	-.2456+04				
1-S:C	-.1224+04	.9653+03	.8252+03	.6746+04	.7085+02
1-S:S	.1563+04	.4449+03	.6663+04	.9867+03	-.1278+03
		(0.85)R			
0	-.1143+04				
1-S:C	-.4856+03	.3126+03	.3986+03	.3215+04	-.3581+02
1-S:S	.0502+03	.2736+03	.3110+04	.5414+03	.1260+02

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 1.
COLLECTIVE PITCH TRANSFER COEFFICIENTS FOR AN ARTICULATED BLADE

(G) MP = 0.5
FP = 0.001 (FOR MU = 0.25,0.4,0.5)
FP = 0.000447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S	ADVANCE RATIO, MU = 0.25				
		(0.21)R			
0	.8367+03				
1-S,C	-.5775+03	.1886+03	-.1442+03	.2992+01	-.2454+01
1-S,S	.6000+03	-.1958+03	-.6544+02	-.2262+02	-.1225+02
		(0.35)R			
0	.1486+04				
1-S,C	-.1530+04	.4412+03	-.1612+03	-.6819+01	.3057+01
1-S,S	.9260+03	-.7653+02	-.1597+03	-.7799+01	-.1134+02
		(0.45)R			
0	.2114+04				
1-S,C	-.2167+04	.6314+03	-.1064+03	-.1700+02	.6151+01
1-S,S	.9861+03	.9162+02	-.2358+03	-.7158-00	-.6744+01
		(0.55)R			
0	.1749+04				
1-S,C	-.2069+04	.6151+03	.8591+01	-.2754+02	.4888+01
1-S,S	.8713+03	.2756+03	-.3158+03	-.1345+02	-.7213-00
		(0.75)R			
0	-.1741+04				
1-S,C	-.2008+04	.6754+03	.3396+03	-.3300+02	-.1802+02
1-S,S	.1722+02	.4009+03	-.3744+03	-.1217+03	.7238+01
		(0.85)R			
0	-.2406+04				
1-S,C	-.1067+04	.3905+03	.3221+03	-.2177+02	-.2127+02
1-S,S	-.2463+03	.2606+03	-.2640+03	-.1247+03	.5561+01

N,C OR S	ADVANCE RATIO, MU = 0.4				
		(0.21)R			
0	.5145+03				
1-S,C	-.8804+03	.4269+03	-.4808+03	.1045+03	-.4387+01
1-S,S	.1113+04	-.3674+03	-.1047+03	-.1915+03	-.1409+03
		(0.35)R			
0	.1355+04				
1-S,C	-.2364+04	.1176+04	-.6347+03	.7848+02	.8067+02
1-S,S	.1879+04	-.3776+03	-.4481+03	-.4121+02	-.1434+03
		(0.45)R			
0	.1654+04				
1-S,C	-.3348+04	.1764+04	-.5172+03	-.1863+02	.1140+03
1-S,S	.2163+04	-.2648+02	-.8031+03	.6392+02	-.8881+02
		(0.55)R			
0	.1348+04				
1-S,C	-.4073+04	.2327+04	-.1562+03	-.1939+03	.6938+02
1-S,S	.2015+04	.3884+03	-.1248+04	.3649+02	.4803+01
		(0.75)R			
0	-.1761+04				
1-S,C	-.3054+04	.2465+04	.1157+04	-.6442+03	-.3438+03
1-S,S	.3217+03	.7973+03	-.1886+04	-.6710+03	.2206+03
		(0.85)R			
0	-.2357+04				
1-S,C	-.1571+04	.1630+04	.1180+04	-.5653+03	-.3677+03
1-S,S	-.3320+03	.5546+03	-.1439+04	-.7476+03	.2008+03

N,C OR S	ADVANCE RATIO, MU = 0.5				
		(0.21)R			
0	.6447+02				
1-S,C	-.1224+04	.4586+03	-.7442+03	.2822+03	-.9418+02
1-S,S	.1430+04	-.9881+03	.1174+03	-.7960+03	-.4556+03
		(0.35)R			
0	.7345+03				
1-S,C	-.2971+04	.1659+04	-.1177+04	.3904+03	.9412+02
1-S,S	.2800+04	-.1072+04	-.3391+03	-.4642+03	-.5866+03
		(0.45)R			
0	.1025+04				
1-S,C	-.4118+04	.2648+04	-.1161+04	.2157+03	.2097+03
1-S,S	.3117+04	-.9386+03	-.1011+04	-.2813+02	-.4471+03
		(0.55)R			
0	.7855+03				
1-S,C	-.4916+04	.3576+04	-.7417+03	-.3012+03	.1884+03
1-S,S	.3226+04	-.4730+03	-.2030+04	.3048+03	-.5340+02
		(0.75)R			
0	-.1990+04				
1-S,C	-.3598+04	.3679+04	.1378+04	-.2199+04	-.5262+03
1-S,S	.1371+04	.2119+03	-.4164+04	-.1931+03	.1329+04
		(0.85)R			
0	-.2394+04				
1-S,C	-.1853+04	.2355+04	.1614+04	-.2100+04	-.6451+03
1-S,S	.2910+03	.2421+03	-.3421+04	-.4793+03	.1318+04

N,C OR S	ADVANCE RATIO, MU = 0.7				
		(0.21)R			
0	-.1164+04				
1-S,C	-.2262+04	.2884+03	-.1947+04	-.1205+04	-.2383+04
1-S,S	.2299+04	-.2605+04	.3052+02	-.3063+04	-.2372+04
		(0.35)R			
0	-.1463+04				
1-S,C	-.4248+04	.1057+04	-.3206+04	-.4496+03	-.2175+04
1-S,S	.3650+04	-.2803+04	-.6976+03	-.2920+04	-.2723+04
		(0.45)R			
0	-.1464+04				
1-S,C	-.5254+04	.1962+04	-.3764+04	.4434+02	-.9807+03
1-S,S	.4110+04	-.3049+04	-.1952+04	-.1559+04	-.1809+04
		(0.55)R			
0	-.1467+04				
1-S,C	-.5300+04	.2226+04	-.4003+04	-.2598+03	.9023+03
1-S,S	.4066+04	-.3203+04	-.4057+04	.6021+03	.2005+03
		(0.75)R			
0	-.1365+04				
1-S,C	-.2900+04	.3435+04	-.2816+04	-.3940+04	.4557+04
1-S,S	.2091+04	-.2976+04	-.8639+04	.4822+04	.5683+04
		(0.85)R			
0	-.9676+03				
1-S,C	-.1074+04	.4046+04	-.1542+04	-.5924+04	.3761+04
1-S,S	.8553+03	-.2004+04	-.6913+04	.4032+04	.5123+04

N,C OR S	ADVANCE RATIO, MU = 1.0				
		(0.21)R			
0	-.3561+04				
1-S,C	-.5012+04	.8194+03	-.3702+04	-.4571+04	-.6034+04
1-S,S	.4658+04	-.4782+04	.1398+04	-.6835+04	-.3049+04
		(0.35)R			
0	-.5148+04				
1-S,C	-.7752+04	.4472+03	-.6708+04	-.4044+04	-.7016+04
1-S,S	.5932+04	-.5818+04	-.4788+02	-.6906+04	-.2818+04
		(0.45)R			
0	-.5370+04				
1-S,C	-.8423+04	.8891+02	-.8609+04	-.2066+04	-.4314+04
1-S,S	.5544+04	-.5676+04	-.1978+04	-.3795+04	-.1262+04
		(0.55)R			
0	-.4801+04				
1-S,C	-.7775+04	.1595+02	-.1017+05	.5199+03	.1747+04
1-S,S	.4256+04	-.5413+04	-.4170+04	.1696+04	-.3364+03
		(0.75)R			
0	-.1591+04				
1-S,C	-.2560+04	.1018+04	-.9459+04	.3897+04	.1666+05
1-S,S	.3305+03	-.4760+04	-.6051+04	.1280+05	-.7479+03
		(0.85)R			
0	-.3399+03				
1-S,C	-.4517+03	.1013+04	-.5838+04	.2875+04	.1395+05
1-S,S	-.5162+03	-.3170+04	-.4047+04	.1036+05	-.9160+03

N,C OR S	ADVANCE RATIO, MU = 1.4				
		(0.21)R			
0	-.7646+04				
1-S,C	-.1379+05	.4128+04	-.2177+04	-.4598+04	-.3316+04
1-S,S	.8366+04	-.7620+04	.1147+05	-.6172+04	.5736+04
		(0.35)R			
0	-.8776+04				
1-S,C	-.1871+05	.4310+04	-.6212+04	-.3038+04	-.5836+04
1-S,S	.9077+04	-.5238+04	.1050+05	-.6169+04	.8649+04
		(0.45)R			
0	-.7727+04				
1-S,C	-.1858+05	.2980+04	-.9533+04	.6373+03	-.4677+04
1-S,S	.7394+04	-.1521+04	.7270+04	-.2312+04	.8207+04
		(0.55)R			
0	-.5988+04				
1-S,C	-.1492+05	.8449+03	-.1242+05	.5733+04	.5851+03
1-S,S	.4994+04	.1651+04	.4445+04	.4876+04	-.8882+04
		(0.75)R			
0	-.2532+04				
1-S,C	-.2753+04	-.2790+04	-.1187+05	.1236+05	.1814+05
1-S,S	.1182+04	.1770+04	.3653+04	.1833+05	-.1541+05
		(0.85)R			
0	-.1220+04				
1-S,C	.4377+03	-.2252+04	-.7008+04	.8428+04	.1249+05
1-S,S	.3700+03	.4237+03	.2909+04	.1360+05	-.1158+05

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 1.
COLLECTIVE PITCH TRANSFER COEFFICIENTS FOR AN ARTICULATED BLADE

(H) MP = 0.5
FP = 0.0025 (FOR MU = 0.25,0.4,0.5)
FP = 0.00112(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S — ADVANCE RATIO, MU = 0.25

	(0.21)R			
0	.9197+03			
1-5,C	-.6487+03	.1648+03	-.1412+03	-.1257+02	-.1070+02
1-5,S	.5771+03	-.1887+03	-.6791+02	-.2472+02	-.1314+02
	(0.35)R			
0	.1725+04			
1-5,C	-.1498+04	.3981+03	-.1585+03	-.1793+02	-.4920+01
1-5,S	.9062+03	-.1172+03	-.1626+03	-.1730+02	-.1409+02
	(0.45)R			
0	.1860+04			
1-5,C	-.2033+04	.3769+03	-.1125+03	-.2247+02	.1454+01
1-5,S	.9768+03	.2151+01	-.2406+03	-.1319+02	-.9213+01
	(0.55)R			
0	.1346+04			
1-5,C	-.2316+04	.7248+03	-.2305+02	-.2952+02	.5277+01
1-5,S	.8468+03	.1276+03	-.3134+03	-.2114+02	-.3817-00
	(0.75)R			
0	-.9634+03			
1-5,C	-.1566+04	.9664+03	.1580+03	-.3883+02	-.4583-00
1-5,S	.1550+03	.2078+03	-.3189+03	-.5978+02	.1634+02
	(0.85)R			
0	-.1106+04			
1-5,C	-.7758+03	.3905+03	.1292+03	-.2642+02	-.2735+01
1-5,S	-.4497+02	.1274+03	-.1948+03	-.4766+02	.1296+02

N,C OR S — ADVANCE RATIO, MU = 0.4

	(0.21)R			
0	.6259+03			
1-5,C	-.9882+03	.4003+03	-.4779+03	-.3271+02	-.9920+02
1-5,S	.1079+04	-.5552+03	-.1788+03	-.2306+03	-.1809+03
	(0.35)R			
0	.1325+04			
1-5,C	-.2285+04	.1089+04	-.6265+03	-.5014+02	-.3030+02
1-5,S	.1813+04	-.4950+03	-.5395+03	-.1393+03	-.1905+03
	(0.45)R			
0	.1465+04			
1-5,C	-.3101+04	.1632+04	-.5306+03	-.1037+03	.3518+02
1-5,S	.2031+04	-.2705+03	-.8934+03	-.4650+02	-.1112+03
	(0.55)R			
0	.1020+04			
1-5,C	-.3528+04	.2077+04	-.2438+03	-.2150+03	.6453+02
1-5,S	.1858+04	.6130+01	-.1281+04	-.2299+02	.3424+02
	(0.75)R			
0	-.1035+04			
1-5,C	-.2367+04	.1895+04	.5003+03	-.4340+03	-.3009+02
1-5,S	.4682+03	.3257+03	-.1511+04	-.2128+03	.3099+03
	(0.85)R			
0	-.1106+04			
1-5,C	-.1166+04	.1100+04	.4524+03	-.3168+03	-.5167+02
1-5,S	-.4024+01	.2286+03	-.9653+03	-.1960+03	.2405+03

N,C OR S — ADVANCE RATIO, MU = 0.5

	(0.21)R			
0	.2160+03			
1-5,C	-.1325+04	.4337+03	-.7980+03	-.2291+03	-.4516+03
1-5,S	.1422+04	-.9771+03	-.1366+03	-.7937+03	-.4601+03
	(0.35)R			
0	.7706+03			
1-5,C	-.2886+04	.1480+04	-.1223+04	-.1794+03	-.3220+03
1-5,S	.2505+04	-.1218+04	-.6651+03	-.5886+03	-.5631+03
	(0.45)R			
0	.9086+03			
1-5,C	-.3828+04	.2340+04	-.1220+04	-.2010+03	-.5646+02
1-5,S	.2943+04	-.1137+04	-.1333+04	-.2085+03	-.3874+03
	(0.55)R			
0	.5344+03			
1-5,C	-.4288+04	.3046+04	-.8671+03	-.3883+03	.2538+03
1-5,S	.2905+04	-.9085+03	-.2215+04	.1644+03	.2907+02
	(0.75)R			
0	-.1230+04			
1-5,C	-.2821+04	.2779+04	.4304+03	-.9567+03	.5441+03
1-5,S	.1271+04	-.2776+03	-.3192+04	.3439+03	.9754+03
	(0.85)R			
0	-.1177+04			
1-5,C	-.1360+04	.1600+04	.5320+03	-.7349+03	.3587+03
1-5,S	.4322+03	-.7856+02	-.2151+04	.1816+03	.7875+03

N,C OR S — ADVANCE RATIO, MU = 0.7

	(0.21)R			
0	-.9550+03			
1-5,C	-.2249+04	.9305+02	-.2882+04	-.3060+04	-.3831+04
1-5,S	.2277+04	-.1942+04	-.2928+03	-.1765+04	-.1683+03
	(0.35)R			
0	-.1270+04			
1-5,C	-.4063+04	.9907+03	-.4445+04	-.2707+04	-.3513+04
1-5,S	.3547+04	-.2677+04	-.1111+04	-.1594+04	-.3687+03
	(0.45)R			
0	-.1335+04			
1-5,C	-.4963+04	.1320+04	-.5071+04	-.1726+04	-.1518+04
1-5,S	.3940+04	-.3283+04	-.2301+04	-.7262+03	-.5237+03
	(0.55)R			
0	-.1306+04			
1-5,C	-.5021+04	.2274+04	-.5215+04	-.8137+03	.1528+04
1-5,S	.3777+04	-.3500+04	-.3993+04	.5279+03	-.6562+03
	(0.75)R			
0	-.9250+03			
1-5,C	-.4760+04	.3206+04	-.3514+04	-.3377+03	.5958+04
1-5,S	.1848+04	-.2780+04	-.5915+04	.2243+04	-.6111+03
	(0.85)R			
0	-.5145+03			
1-5,C	-.1175+04	.2092+04	-.1839+04	-.3037+03	.4254+04
1-5,S	.7720+03	-.1582+04	-.3922+04	.1590+04	-.3563+03

N,C OR S — ADVANCE RATIO, MU = 1.0

	(0.21)R			
0	-.3281+04			
1-5,C	-.4819+04	.8262+03	-.5168+04	-.5307+04	-.2949+04
1-5,S	.4257+04	-.4283+04	-.1658+04	-.1118+04	.2799+04
	(0.35)R			
0	-.4857+04			
1-5,C	-.7310+04	.8983+03	-.8481+04	-.4668+04	-.3086+04
1-5,S	.5270+04	-.5663+04	-.7880+03	-.8408+03	.2710+04
	(0.45)R			
0	-.5166+04			
1-5,C	-.7805+04	.7841+03	-.1035+05	-.2462+04	-.1788+04
1-5,S	.4870+04	-.5893+04	-.6505+03	.2694+03	.5944+03
	(0.55)R			
0	-.4707+04			
1-5,C	-.6930+04	.6508+03	-.1152+05	.1977+03	.4722+03
1-5,S	.3751+04	-.5716+04	-.2263+04	.2053+04	-.3194+04
	(0.75)R			
0	-.1977+04			
1-5,C	-.4357+04	.4295+03	-.9110+04	.2922+04	.4015+04
1-5,S	.6594+03	-.3896+04	-.3388+04	.4424+04	-.8929+04
	(0.85)R			
0	-.7562+03			
1-5,C	-.6463+03	.2476+03	-.5000+04	.1942+04	.2888+04
1-5,S	.1062+03	-.2093+04	-.2082+04	.2978+04	-.6184+04

N,C OR S — ADVANCE RATIO, MU = 1.4

	(0.21)R			
0	-.6753+04			
1-5,C	-.1227+05	.2425+04	-.3523+04	-.2307+04	.5848+04
1-5,S	.7451+04	-.6388+04	.8902+04	-.1438+03	.2512+04
	(0.35)R			
0	-.8372+04			
1-5,C	-.1714+05	.3374+04	-.7578+04	-.3151+03	.3724+04
1-5,S	.6340+04	-.8841+04	.8832+04	-.1312+02	.2167+04
	(0.45)R			
0	-.7953+04			
1-5,C	-.1710+05	.4077+04	-.1036+05	.2837+04	.4110+03
1-5,S	.6953+04	-.9281+04	.7956+04	.1632+04	.2911+03
	(0.55)R			
0	-.6552+04			
1-5,C	-.1390+05	.4491+04	-.1[illegible]	.4880+04	-.2610+04
1-5,S	.4864+04	-.7619+04	.[illegible]	.4872+04	-.2701+04
	(0.75)R			
0	-.2865+04			
1-5,C	-.5265+04	-.1[illegible]	-.[illegible]	.[illegible]	-.3651+04
1-5,S	.5835+03	.1087+04	.[illegible]	.[illegible]	-.6370+04
	(0.85)R			
0	-.1095+04			
1-5,C	-.5862+03	-.[illegible]	-.[illegible]	.[illegible]	-.1964+04
1-5,S	-.9913+02	.[illegible]	.[illegible]	.[illegible]	-.4183+04

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 1.
COLLECTIVE PITCH TRANSFER COEFFICIENTS FOR AN ARTICULATED BLADE

(I) MP = 0.5
FP = 0.01 (FOR MU = 0.25,0.4,0.5)
FP = 0.00447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S		ADVANCE RATIO, MU = 0.25			
		(0.21)R			
0	.8591+03				
1-S,C	-.6842+03	.1002+03	-.1641+03	-.3074+02	-.8553+01
1-S,S	.5077+03	-.1718+03	-.4507+02	.1447+01	.2626+01
		(0.35)R			
0	.1311+04				
1-S,C	-.1242+04	.2306+03	-.2169+03	-.4052+02	-.6910+01
1-S,S	.7696+03	-.1855+03	-.1110+03	.3221+01	-.1661-00
		(0.45)R			
0	.1289+04				
1-S,C	-.1514+04	.3259+03	-.2140+03	-.4412+02	-.3975+01
1-S,S	.8204+03	-.1524+03	-.1618+03	.2362+01	-.2433+01
		(0.55)R			
0	.8968+03				
1-S,C	-.1553+04	.3861+03	-.1804+03	-.4626+02	-.1739+01
1-S,S	.7216+03	-.1051+03	-.1961+03	-.1121+01	-.3204+01
		(0.75)R			
0	-.1763+03				
1-S,C	-.8767+03	.2913+03	-.6981+02	-.3606+02	-.1040+01
1-S,S	.2581+03	-.2802+02	-.1530+03	-.7717+01	-.5694-00
		(0.85)R			
0	-.2535+03				
1-S,C	-.3950+03	.1491+03	-.2604+02	-.1953+02	-.8263-00
1-S,S	.8210+02	-.9199+01	-.7916+02	-.5410+01	.2732-00

N,C OR S		ADVANCE RATIO, MU = 0.4			
		(0.21)R			
0	.6472+03				
1-S,C	-.1051+04	.2217+03	-.6399+03	-.1960+03	-.9350+02
1-S,S	.9509+03	-.9302+03	-.1338+03	.1268+02	.3884+02
		(0.35)R			
0	.1032+04				
1-S,C	-.1911+04	.5762+03	-.9019+03	-.2485+03	-.6875+02
1-S,S	.1481+04	-.9644+03	-.3863+03	.5393+02	.1292+02
		(0.45)R			
0	.1015+04				
1-S,C	-.2335+04	.6439+03	-.9364+03	-.2692+03	-.2860+02
1-S,S	.1607+04	-.8331+03	-.6073+03	.7461+02	-.1034+02
		(0.55)R			
0	.6664+03				
1-S,C	-.2402+04	.1014+04	-.8318+03	-.2896+03	.4138+01
1-S,S	.1437+04	-.5223+03	-.7843+03	.7079+02	-.1900+02
		(0.75)R			
0	-.2656+03				
1-S,C	-.1367+04	.7655+03	-.3601+03	-.2457+03	.1324+02
1-S,S	.5352+03	-.2086+03	-.6759+03	.1276+02	.3483+01
		(0.85)R			
0	-.2870+03				
1-S,C	-.6166+03	.3900+03	-.1436+03	-.1371+03	.4895+01
1-S,S	.1765+03	-.8259+02	-.3617+03	-.2808+01	.7685+01

N,C OR S		ADVANCE RATIO, MU = 0.5			
		(0.21)R			
0	.3571+03				
1-S,C	-.1363+04	.1452+03	-.1185+04	-.5330+03	-.2257+03
1-S,S	.1363+04	-.9298+03	-.8541+02	.5101+02	.1721+03
		(0.35)R			
0	.6567+03				
1-S,C	-.2401+04	.3838+03	-.1772+04	-.6150+03	-.1936+03
1-S,S	.2001+04	-.1324+04	-.4507+03	.1575+03	.7545+02
		(0.45)R			
0	.6353+03				
1-S,C	-.2941+04	.1496+03	-.1934+04	-.6065+03	-.1024+03
1-S,S	.2327+04	-.1403+04	-.8513+03	.2445+03	-.3780+02
		(0.55)R			
0	.3372+03				
1-S,C	-.3009+04	.1203+04	-.1819+04	-.6026+03	-.2978+01
1-S,S	.2184+04	-.1292+04	-.1247+04	.3055+03	-.1176+03
		(0.75)R			
0	-.4122+03				
1-S,C	-.1711+04	.9492+03	-.9101+03	-.4883+03	.7978+02
1-S,S	.9981+03	-.6384+03	-.1264+04	.2431+03	-.9249+02
		(0.85)R			
0	-.3462+03				
1-S,C	-.7765+03	.4877+03	-.3936+03	-.2739+03	.4933+02
1-S,S	.3977+03	-.2776+03	-.7088+03	.1260+03	-.3930+02

N,C OR S		ADVANCE RATIO, MU = 0.7			
		(0.21)R			
0	-.5442+03				
1-S,C	-.2262+04	-.6830+03	-.3697+04	-.1480+04	-.3790+03
1-S,S	.2064+04	-.1594+04	.1019+04	.1136+04	.1065+04
		(0.35)R			
0	-.6262+03				
1-S,C	-.3221+04	-.9365+03	-.5509+04	-.1844+04	-.4447+03
1-S,S	.2699+04	-.2263+04	.9622+03	.1755+04	.8610+03
		(0.45)R			
0	-.9340+03				
1-S,C	-.3551+04	-.7058+03	-.6215+04	-.1747+04	-.3906+03
1-S,S	.3108+04	-.2449+04	.5713+03	.2038+04	.3005+03
		(0.55)R			
0	-.9491+03				
1-S,C	-.3494+04	-.3620+03	-.6259+04	-.1427+04	-.2829+03
1-S,S	.2968+04	-.2362+04	.6410+02	.2109+04	-.3643+03
		(0.75)R			
0	-.6025+03				
1-S,C	-.2102+04	.1305+03	-.3915+04	-.5531+03	-.6393+02
1-S,S	.1691+04	-.1372+04	-.4832+03	.1379+04	-.9107+03
		(0.85)R			
0	-.2944+03				
1-S,C	-.1068+04	.1212+03	-.1904+04	-.2140+03	-.1280+02
1-S,S	.7958+03	-.6500+03	-.3197+03	.6800+03	-.5534+03

N,C OR S		ADVANCE RATIO, MU = 1.0			
		(0.21)R			
0	-.2360+04				
1-S,C	-.4162+04	-.1061+04	-.5241+04	.3817+03	.3278+03
1-S,S	.3049+04	-.2793+04	.4776+04	.2212+04	.1147+03
		(0.35)R			
0	-.3311+04				
1-S,C	-.5540+04	-.1503+04	-.7850+04	.1424+04	.2376+03
1-S,S	.3923+04	-.3557+04	.6642+04	.3547+04	-.3479+03
		(0.45)R			
0	-.3510+04				
1-S,C	-.5657+04	-.1622+04	-.8876+04	.2376+04	.4061+02
1-S,S	.3867+04	-.3459+04	.7051+04	.4223+04	-.8612+03
		(0.55)R			
0	-.3311+04				
1-S,C	-.5065+04	-.1653+04	-.8911+04	.3124+04	-.1788+03
1-S,S	.3369+04	-.2930+04	.6636+04	.4443+04	-.1315+04
		(0.75)R			
0	-.1819+04				
1-S,C	-.2559+04	-.6794+03	-.5463+04	.2634+04	-.3235+03
1-S,S	.1562+04	-.1268+04	.3637+04	.2922+04	-.1245+04
		(0.85)R			
0	-.8352+03				
1-S,C	-.1124+04	-.4896+03	-.2616+04	.1375+04	-.1888+03
1-S,S	.6350+03	-.5237+03	.1673+04	.1431+04	-.6655+03

N,C OR S		ADVANCE RATIO, MU = 1.4			
		(0.21)R			
0	-.4990+04				
1-S,C	-.7554+04	.1626+04	-.1151+04	.7066+04	.1567+04
1-S,S	.5450+04	-.3315+04	.1082+05	-.3726+03	-.2611+04
		(0.35)R			
0	-.6762+04				
1-S,C	-.9251+04	.2543+04	-.1604+04	.1151+05	.1590+04
1-S,S	.6768+04	-.5268+04	.1509+05	.3503+03	-.3043+04
		(0.45)R			
0	-.6913+04				
1-S,C	-.8813+04	.2966+04	-.1705+04	.1381+05	.1126+04
1-S,S	.6428+04	-.4230+04	.1604+05	.1197+04	-.2669+04
		(0.55)R			
0	-.6263+04				
1-S,C	-.6883+04	.3048+04	-.1601+04	.1454+05	.4954+03
1-S,S	.5209+04	-.3320+03	.1567+05	.1947+04	-.1943+04
		(0.75)R			
0	-.3160+04				
1-S,C	-.2562+04	.1909+04	-.8651+03	.9428+04	-.2918+03
1-S,S	.2067+04	.3057+03	.8154+04	.1872+04	-.4895+03
		(0.85)R			
0	-.1599+04				
1-S,C	-.9407+03	.7139+03	-.3937+03	.4561+04	-.2295+03
1-S,S	.6165+03	-.5835+03	.3711+04	.9932+03	-.1258+03

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 2.
BLADE FLAST TRANSFER COEFFICIENTS FOR AN ARTICULATED BLADE

(A) MP = 0.1
FM = 0.001 (FOR MU = 0.25,0.4,0.5)
FM = 0.000447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S — ADVANCE RATIO, MU = 0.25

(0,21)R

0	.4829+02				
1-S,C	.1203+02	.5420+02	.1176+02	.4152+01	-.3224+01
1-S,S	-.8575+02	.5453+01	.2156+02	.2043+02	.2561+01

(0,35)R

0	.1614+03				
1-S,C	.3171+02	.9066+02	.1564+02	.4346+01	-.1559+01
1-S,S	-.1905+03	.1742+02	.3568+02	.2495+02	.3820+01

(0,45)R

0	.2452+03				
1-S,C	.4513+02	.1101+03	.1798+02	.4054+01	.1908+01
1-S,S	-.2566+03	.2451+02	.4373+02	.2351+02	.6550+01

(0,55)R

0	.3164+03				
1-S,C	.5676+02	.1208+03	.2263+02	.4572+01	.7230+01
1-S,S	-.3023+03	.2725+02	.5060+02	.2060+02	.1276+02

(0,75)R

0	.2456+03				
1-S,C	.4077+02	.1204+03	.3761+02	.9396+01	.1825+02
1-S,S	-.2264+03	.6863+01	.5095+02	.1453+02	.3312+02

(0,85)R

0	.1296+03				
1-S,C	.2062+02	.6042+02	.3141+02	.8540+01	.1522+02
1-S,S	-.1200+03	-.3627+01	.3496+02	.9943+01	.2932+02

N,C OR S — ADVANCE RATIO, MU = 0.4

(0,21)R

0	.7924+02				
1-S,C	.1736+02	.1126+03	.8231+01	.2921+01	-.6873+01
1-S,S	-.1391+03	.6179+02	-.1120+02	.1258+02	-.5997-00

(0,35)R

0	.2173+03				
1-S,C	.4749+02	.1062+03	.1098+02	-.1371+01	-.6266+01
1-S,S	-.3107+03	.1221+03	-.2019+02	.1032+02	-.4729+01

(0,45)R

0	.3133+03				
1-S,C	.6749+02	.2235+03	.1614+02	-.5906+01	-.4145+01
1-S,S	-.4188+03	.1575+03	-.2582+02	.3892+01	-.6435+01

(0,55)R

0	.3839+03				
1-S,C	.8043+02	.2512+03	.2860+02	-.1012+02	-.2123+01
1-S,S	-.4925+03	.1816+03	-.3110+02	-.4706+01	-.4812+01

(0,75)R

0	.2913+03				
1-S,C	.5160+02	.2277+03	.7141+02	-.9705+01	-.2724+01
1-S,S	-.3628+03	.1405+03	-.3272+02	-.1742+02	.1264+02

(0,85)R

0	.1508+03				
1-S,C	.2195+02	.1404+03	.6326+02	-.5153+01	-.3178+01
1-S,S	-.1891+03	.7867+02	-.2256+02	-.1372+02	.1509+02

N,C OR S — ADVANCE RATIO, MU = 0.5

(0,21)R

0	.1030+03				
1-S,C	.2193+02	.1328+03	.2491+02	-.8448+01	-.1266+02
1-S,S	-.1885+03	.9944+02	-.1404+01	-.2598+02	.2014+02

(0,35)R

0	.2648+03				
1-S,C	.5035+02	.2216+03	.3471+02	-.1976+02	-.9166+01
1-S,S	-.4871+03	.1930+03	-.5999+01	-.3451+02	.1152+02

(0,45)R

0	.3714+03				
1-S,C	.8181+02	.2596+03	.4735+02	-.2394+02	-.3272+01
1-S,S	-.6390+03	.2459+03	-.1393+02	-.2907+02	-.3961+01

(0,55)R

0	.4823+03				
1-S,C	.9174+02	.2738+03	.7502+02	-.2078+02	.2032+01
1-S,S	-.6147+03	.2790+03	-.2824+02	-.1161+02	-.2370+02

(0,75)R

0	.3006+03				
1-S,C	.3864+02	.1747+03	.1649+03	.1660+02	-.5448-00
1-S,S	-.3799+03	.2036+03	-.6620+02	.5280+02	-.5028+02

(0,85)R

0	.1396+03				
1-S,C	.2909-00	.8731+02	.1432+03	.2466+02	-.3783+01
1-S,S	-.1623+03	.1089+03	-.5675+02	.5502+02	-.3820+02

N,C OR S — ADVANCE RATIO, MU = 0.7

(0,21)R

0	.1594+03				
1-S,C	.4115+02	.2076+03	.7758+02	.3192+02	.2072+02
1-S,S	-.3127+03	.1605+03	-.1655+02	-.4035+02	.6540+02

(0,35)R

0	.3585+03				
1-S,C	.9726+02	.3452+03	.1203+03	.1988+02	.2542+02
1-S,S	-.6827+03	.3049+03	-.2442+02	-.4188+02	.4804+02

(0,45)R

0	.6658+03				
1-S,C	.1200+03	.4104+03	.1640+03	.4990+01	.2031+02
1-S,S	-.7994+03	.3621+03	-.3187+02	-.1882+02	.1327+02

(0,55)R

0	.1033+04				
1-S,C	.1444+03	.4452+03	.2394+03	-.3522+01	.7649+01
1-S,S	-.8782+03	.4209+03	-.4506+02	.2791+02	-.2604+02

(0,75)R

0	.1256+04				
1-S,C	.7109+02	.3385+03	.4135+03	.2261+02	-.2943+02
1-S,S	-.5078+03	.2777+03	-.7651+02	.1484+03	-.5847+02

(0,85)R

0	.1625+04				
1-S,C	.2175+02	.1948+03	.3256+03	.2805+02	-.2853+02
1-S,S	-.2156+03	.1377+03	-.6030+02	.1285+03	-.3777+02

N,C OR S — ADVANCE RATIO, MU = 1.0

(0,21)R

0	.2069+03				
1-S,C	.9379+02	.2927+03	.1350+03	.7817+02	.1028+03
1-S,S	-.5703+03	.3808+03	-.1101+03	-.6709+02	.4259+02

(0,35)R

0	.3406+03				
1-S,C	.1886+03	.4652+03	.2427+03	.6450+02	.9938+02
1-S,S	-.1050+04	.6616+03	-.1596+03	-.6974+02	.6259+01

(0,45)R

0	.4669+03				
1-S,C	.2876+03	.5473+03	.3602+03	.3585+02	.5652+02
1-S,S	-.1270+04	.7868+03	-.1889+03	-.3362+02	-.2158+02

(0,55)R

0	.5955+03				
1-S,C	.2334+03	.5968+03	.5385+03	.1098+02	-.9827+01
1-S,S	-.1307+04	.8155+03	-.2256+03	.3679+02	-.2351+02

(0,75)R

0	.5577+03				
1-S,C	.9630+02	.4909+03	.8305+03	.1322+02	-.1251+03
1-S,S	-.6306+03	.4640+03	-.2655+03	.1926+03	.7003+02

(0,85)R

0	.1394+03				
1-S,C	.2501+02	.2925+03	.6025+03	.1732+02	-.9935+02
1-S,S	-.2349+03	.2092+03	-.1833+03	.1564+03	.7591+02

N,C OR S — ADVANCE RATIO, MU = 1.4

(0,21)R

0	.4941+03				
1-S,C	.2767+03	.5734+03	.1342+03	.2162+03	-.7823+02
1-S,S	-.1071+04	.9459+03	-.4115+03	-.1061+03	-.1147+03

(0,35)R

0	.8048+03				
1-S,C	.4116+03	.6145+03	.3434+03	.1832+03	-.5973+02
1-S,S	-.1833+04	.1516+04	-.5689+03	-.1307+03	-.1650+03

(0,45)R

0	.9091+03				
1-S,C	.4204+03	.6707+03	.5741+03	.8361+02	.4085+01
1-S,S	-.2108+04	.1715+04	-.6094+03	-.7708+02	-.1149+03

(0,55)R

0	.8737+03				
1-S,C	.3560+03	.6193+03	.8667+03	-.4025+02	.1048+03
1-S,S	-.2024+04	.1676+04	-.6100+03	.5047+02	.3711+02

(0,75)R

0	.3815+03				
1-S,C	.5027+02	.5783+03	.1150+04	-.1790+03	.2621+03
1-S,S	-.7762+03	.6414+03	-.4489+03	.3350+03	.4182+03

(0,85)R

0	.1355+03				
1-S,C	-.2857+02	.3604+03	.7616+03	-.1235+03	.1890+03
1-S,S	-.2177+03	.3530+03	-.2558+03	.2631+03	.3368+03

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 2.
BLADE TWIST TRANSFER COEFFICIENTS FOR AN ARTICULATED BLADE

(B) MP = 0.1
FP = 0.0025 (FOR MU = 0.25,0.4,0.5)
FP = 0.00112(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S		ADVANCE RATIO, MU = 0.25			
		(0.21)R			
0	.5908+02				
1-S,C	.1189+02	.4945+02	.1631+02	.4553+01	-.1523+02
1-S,S	-.9047+02	.3293+01	.2398+02	.1530+02	.1037+02
		(0.35)R			
0	.1621+03				
1-S,C	.2916+02	.8218+02	.2482+02	.6835+01	-.1013+02
1-S,S	-.1874+03	.1074+02	.3965+02	.2043+02	.1172+02
		(0.45)R			
0	.2352+03				
1-S,C	.3992+02	.9908+02	.2956+02	.7794+01	.1045+01
1-S,S	-.2455+03	.1483+02	.4864+02	.2210+02	.1129+02
		(0.55)R			
0	.2825+03				
1-S,C	.4496+02	.1085+03	.3382+02	.8268+01	.1571+02
1-S,S	-.2754+03	.1516+02	.5538+02	.2351+02	.1155+02
		(0.75)R			
0	.2135+03				
1-S,C	.2775+02	.8406+02	.3247+02	.6514+01	.3324+02
1-S,S	-.1899+03	.3204+01	.4859+02	.2189+02	.1287+02
		(0.85)R			
0	.1121+03				
1-S,C	.1273+02	.4715+02	.2014+02	.3754+01	.2293+02
1-S,S	-.9651+02	-.1040+01	.2883+02	.1376+02	.8817+01

N,C OR S		ADVANCE RATIO, MU = 0.4			
		(0.21)R			
0	.6834+02				
1-S,C	.2165+02	.1141+03	.6117+01	-.3429-00	-.1502+02
1-S,S	-.1477+03	.3090+02	-.1082+02	.8191+01	.4763+01
		(0.35)R			
0	.2130+03				
1-S,C	.4972+02	.1864+03	.9222+01	-.3818+01	-.1311+02
1-S,S	-.3063+03	.9604+02	-.1826+02	.7634+01	.2051+01
		(0.45)R			
0	.2959+03				
1-S,C	.6665+02	.2225+03	.1373+02	-.7243+01	-.6748+01
1-S,S	-.4012+03	.1208+03	-.2253+02	.5121+01	-.5581-00
		(0.55)R			
0	.3454+03				
1-S,C	.7424+02	.2417+03	.2188+02	-.1061+02	.1093+01
1-S,S	-.4501+03	.1319+03	-.2555+02	.2435+01	-.1530+01
		(0.75)R			
0	.2503+03				
1-S,C	.4570+02	.1857+03	.3568+02	-.1158+02	.9827+01
1-S,S	-.3096+03	.8874+02	-.2177+02	.2225-00	.2860+01
		(0.85)R			
0	.1293+03				
1-S,C	.2169+02	.1040+03	.2521+02	-.7098+01	.6820+01
1-S,S	-.1572+03	.4500+02	-.1272+02	.2468-00	.3272+01

N,C OR S		ADVANCE RATIO, MU = 0.5			
		(0.21)R			
0	.1140+03				
1-S,C	.2309+02	.1345+03	.1953+02	-.2297+02	.1229+02
1-S,S	-.1925+03	.6998+02	-.4355+01	-.2310+01	.1984+02
		(0.35)R			
0	.2599+03				
1-S,C	.5696+02	.2237+03	.3087+02	-.3355+02	.1088+02
1-S,S	-.3967+03	.1639+03	-.1182+02	-.8452+01	.1056+02
		(0.45)R			
0	.3498+03				
1-S,C	.7743+02	.2635+03	.4597+02	-.3175+02	.1454+01
1-S,S	-.5110+03	.2015+03	-.2337+02	-.1162+02	-.5440+01
		(0.55)R			
0	.3941+03				
1-S,C	.8662+02	.2745+03	.7164+02	-.1983+02	-.1505+02
1-S,S	-.5559+03	.2150+03	-.4150+02	-.1131+02	-.2431+02
		(0.75)R			
0	.2568+03				
1-S,C	.4951+02	.1760+03	.1124+03	.1824+02	-.4426+02
1-S,S	-.3368+03	.1360+03	-.6831+02	-.2886-01	-.4180+02
		(0.85)R			
0	.1240+03				
1-S,C	.2132+02	.8868+02	.7871+02	.1895+02	-.3280+02
1-S,S	-.1559+03	.8661+02	-.4773+02	.2809+01	-.2755+02

N,C OR S		ADVANCE RATIO, MU = 0.7			
		(0.21)R			
0	.1715+03				
1-S,C	.3715+02	.1995+03	.9754+02	.2135+02	.9544+02
1-S,S	-.3151+03	.1483+03	-.7277+02	-.1942+02	-.3753+02
		(0.35)R			
0	.3459+03				
1-S,C	.7758+02	.3254+03	.1558+03	.1342+02	.8543+02
1-S,S	-.5970+03	.2589+03	-.1117+03	-.2119+02	-.3991+02
		(0.45)R			
0	.4423+03				
1-S,C	.9719+02	.3801+03	.2013+03	.3969+01	.3580+02
1-S,S	-.7361+03	.3092+03	-.1388+03	-.1407+02	-.2205+02
		(0.55)R			
0	.4769+03				
1-S,C	.9831+02	.3922+03	.2541+03	-.1047+01	-.3712+02
1-S,S	-.7714+03	.3173+03	-.1684+03	-.9366-00	.1122+02
		(0.75)R			
0	.2894+03				
1-S,C	.4116+02	.2492+03	.2789+03	.7332+01	-.1383+03
1-S,S	-.4336+03	.1809+03	-.1758+03	.2276+02	.7029+02
		(0.85)R			
0	.1351+03				
1-S,C	.1277+02	.1246+03	.1751+03	.7843+01	-.9788+02
1-S,S	-.1930+03	.6283+02	-.1092+03	.1755+02	.5239+02

N,C OR S		ADVANCE RATIO, MU = 1.0			
		(0.21)R			
0	.2831+03				
1-S,C	.9565+02	.3183+03	.1306+03	.2423+02	-.6623+01
1-S,S	-.5578+03	.3286+03	-.2850+03	-.7615+02	-.8986+02
		(0.35)R			
0	.5014+03				
1-S,C	.1633+03	.5004+03	.2363+03	.1224+02	-.5516+01
1-S,S	-.9751+03	.5328+03	-.4261+03	-.8488+02	-.9680+02
		(0.45)R			
0	.5998+03				
1-S,C	.1843+03	.5743+03	.3252+03	-.1806+01	.5906+01
1-S,S	-.1143+04	.6062+03	-.5022+03	-.6619+02	-.5596+02
		(0.55)R			
0	.6079+03				
1-S,C	.1666+03	.6839+03	.4173+03	-.1112+02	.2767+02
1-S,S	-.1125+04	.6893+03	-.5600+03	-.3354+02	.1915+02
		(0.75)R			
0	.5264+03				
1-S,C	.5336+02	.6665+03	.4261+03	-.5225+01	.6095+02
1-S,S	-.5421+03	.2960+03	-.4789+03	.2349+02	.1415+03
		(0.85)R			
0	.1443+03				
1-S,C	.1129+02	.1816+03	.2536+03	-.2432-00	.4169+02
1-S,S	-.2172+03	.1255+03	-.2736+03	.2122+02	.1021+03

N,C OR S		ADVANCE RATIO, MU = 1.4			
		(0.21)R			
0	.4648+03				
1-S,C	.2404+03	.4522+03	.2273+02	-.1158+02	-.5932+02
1-S,S	-.9961+03	.7389+03	-.6764+03	-.8365+02	.1975+02
		(0.35)R			
0	.7233+03				
1-S,C	.3456+03	.6679+03	.1530+03	-.4335+02	-.4783+02
1-S,S	-.1622+04	.1121+04	-.9946+03	-.1025+03	-.1026+02
		(0.45)R			
0	.7969+03				
1-S,C	.3567+03	.7495+03	.2923+03	-.7608+02	.3136+01
1-S,S	-.1816+04	.1213+04	-.1130+04	-.6939+02	-.4541+02
		(0.55)R			
0	.7484+03				
1-S,C	.3067+03	.7603+03	.4304+03	-.1085+03	.8214+02
1-S,S	-.1669+04	.1110+04	-.1178+04	-.5813+02	-.7794+02
		(0.75)R			
0	.3440+03				
1-S,C	.1031+03	.5016+03	.4477+03	-.1113+03	.1754+03
1-S,S	-.6991+03	.4756+03	-.8429+03	.7873+01	-.8160+02
		(0.85)R			
0	.1379+03				
1-S,C	.3020+02	.2548+03	.2568+03	-.6383+02	.1142+03
1-S,S	-.2498+03	.1807+03	-.4435+03	.1317+02	-.4570+02

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 2.
BLADE TWIST TRANSFER COEFFICIENTS FOR AN ARTICULATED BLADE

(E) MP = 0.1
FP = 0.01 (FOR MU = 0.25,0.4,0.5)
FP = 0.00447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S		ADVANCE RATIO, MU = 0.25			
		(0.21)R			
0	.7273+02				
1-S,C	.9727+01	.3650+02	.3873+02	.3699+01	.1621+01
1-S,S	-.8800+02	.3831+01	.8777+01	.1196+02	.8316+01
		(0.35)R			
0	.1455+03				
1-S,C	.1788+02	.5591+02	.5794+02	.5093+01	.2564+01
1-S,S	-.1545+03	.7037+01	.1480+02	.1590+02	.9793+01
		(0.45)R			
0	.1883+03				
1-S,C	.2182+02	.6350+02	.6582+02	.5539+01	.2896+01
1-S,S	-.1866+03	.8086+01	.1778+02	.1649+02	.8877+01
		(0.55)R			
0	.2049+03				
1-S,C	.2222+02	.6361+02	.6718+02	.5630+01	.2528+01
1-S,S	-.1916+03	.7248+01	.1856+02	.1562+02	.7019+01
		(0.75)R			
0	.1302+03				
1-S,C	.1212+02	.3843+02	.4378+02	.3943+01	.9863+00
1-S,S	-.1113+03	.2050+01	.1169+02	.9133+01	.2762+01
		(0.85)R			
0	.6209+02				
1-S,C	.5335+01	.1840+02	.2180+02	.2048+01	.3191+00
1-S,S	-.5121+02	.3702-00	.5638+01	.4410+01	.1131+01

N,C OR S		ADVANCE RATIO, MU = 0.4			
		(0.21)R			
0	.9717+02				
1-S,C	.2153+02	.9174+02	.8327+01	-.9180-00	-.9438+00
1-S,S	-.1489+03	.1980+02	-.3271+01	.1479+02	.8581+01
		(0.35)R			
0	.1839+03				
1-S,C	.3722+02	.1404+03	.1223+02	-.3278+01	-.1[illegible]+01
1-S,S	-.2605+03	.3373+02	-.4195+01	.2020+02	.1032+02
		(0.45)R			
0	.2318+03				
1-S,C	.4430+02	.1591+03	.1465+02	-.5010+01	-.1[illegible]+01
1-S,S	-.3145+03	.3917+02	-.4407+01	.2142+02	.9968+01
		(0.55)R			
0	.2468+03				
1-S,C	.4465+02	.1588+03	.1666+02	-.5920+01	-.2372+01
1-S,S	-.3236+03	.3794+02	-.4424+01	.2099+02	.8985+01
		(0.75)R			
0	.1526+03				
1-S,C	.2468+02	.9507+02	.1404+02	-.3980+01	-.2686+01
1-S,S	-.1895+03	.1831+02	-.3230+01	.1247+02	.5364+01
		(0.85)R			
0	.7204+02				
1-S,C	.1105+02	.4533+02	.7691+01	-.1901+01	-.1589+01
1-S,S	-.8763+02	.7502+01	-.1722+01	.6111+01	.2707+01

N,C OR S		ADVANCE RATIO, MU = 0.5			
		(0.21)R			
0	.1166+03				
1-S,C	.2965+02	.1220+03	.2193+02	-.2041+02	-.4425+01
1-S,S	-.1917+03	.4060+02	-.1387+02	.1052+02	-.1423+01
		(0.35)R			
0	.2152+03				
1-S,C	.5094+02	.1876+03	.3255+02	-.3075+02	-.6184+01
1-S,S	-.3333+03	.6628+02	-.2173+02	.1334+02	-.1976+01
		(0.45)R			
0	.2655+03				
1-S,C	.6024+02	.2094+03	.3934+02	-.3248+02	-.7819+01
1-S,S	-.[illegible]+03	.7531+02	-.2864+02	.1462+02	-.5427+00
		(0.55)R			
0	.2755+03				
1-S,C	.6022+02	.2021+03	.4509+02	-.2862+02	-.9954+01
1-S,S	-.3987+03	.7186+02	-.3620+02	.1452+02	.2681+01
		(0.75)R			
0	.1599+03				
1-S,C	.3251+02	.1076+03	.3832+02	-.9229+01	-.1029+02
1-S,S	-.2170+03	.3419+02	-.3527+02	.1151+02	.7881+01
		(0.85)R			
0	.7308+02				
1-S,C	.1436+02	.4885+02	.2102+02	-.2619+01	-.5967+01
1-S,S	-.9616+02	.1398+02	-.2083+02	.6163+01	.4883+01

N,C OR S		ADVANCE RATIO, MU = 0.7			
		(0.21)R			
0	.1694+03				
1-S,C	.5751+02	.2047+03	-.3769+02	-.3812+02	-.5723+01
1-S,S	-.3179+03	.6348+02	-.4092+02	.2787+02	.1792+01
		(0.35)R			
0	.2542+03				
1-S,C	.8294+02	.2886+03	-.4847+02	-.5390+02	-.1085+02
1-S,S	-.4616+03	.8746+02	-.6945+02	.4458+02	.7860+01
		(0.45)R			
0	.2885+03				
1-S,C	.9104+02	.3103+03	-.4798+02	-.5813+02	-.1274+02
1-S,S	-.5096+03	.9286+02	-.8619+02	.5230+02	.1367+02
		(0.55)R			
0	.2921+03				
1-S,C	.8914+02	.2973+03	-.4085+02	-.5587+02	-.1422+02
1-S,S	-.5019+03	.8614+02	-.9459+02	.5560+02	.1884+02
		(0.75)R			
0	.1844+03				
1-S,C	.5318+02	.1765+03	-.1832+02	-.3228+02	-.1033+02
1-S,S	-.3026+03	.4716+02	-.6715+02	.3696+02	.1608+02
		(0.85)R			
0	.8993+02				
1-S,C	.2545+02	.8039+02	-.7740+01	-.1523+02	-.5254+01
1-S,S	-.1453+03	.2185+02	-.3395+02	.1838+02	.8807+01

N,C OR S		ADVANCE RATIO, MU = 1.0			
		(0.21)R			
0	.2541+03				
1-S,C	.4731+02	.2366+03	-.2930+03	-.6676+02	.1120+01
1-S,S	-.4859+03	.1175+03	-.1060+02	.4486+02	-.1128+02
		(0.35)R			
0	.3624+03				
1-S,C	.6488+02	.3289+03	-.4117+03	-.9698+02	-.5326+00
1-S,S	-.6775+03	.1590+03	-.2972+02	.6988+02	-.1795+02
		(0.45)R			
0	.3935+03				
1-S,C	.6798+02	.3328+03	-.4412+03	-.1069+03	-.2692+01
1-S,S	-.7208+03	.1646+03	-.4607+02	.8254+02	-.2126+02
		(0.55)R			
0	.3794+03				
1-S,C	.6306+02	.3051+03	-.4193+03	-.1047+03	-.4517+01
1-S,S	-.6809+03	.1586+03	-.5824+02	.8626+02	-.2226+02
		(0.75)R			
0	.2173+03				
1-S,C	.3361+02	.1589+03	-.2342+03	-.6162+02	-.4635+01
1-S,S	-.3744+03	.7806+02	-.4739+02	.5649+02	-.1484+02
		(0.85)R			
0	.1016+03				
1-S,C	.1529+02	.7160+02	-.1085+03	-.2910+02	-.2515+01
1-S,S	-.1726+03	.3542+02	-.2454+02	.2743+02	-.7106+01

N,C OR S		ADVANCE RATIO, MU = 1.4			
		(0.21)R			
0	.3501+03				
1-S,C	.1003+03	.3475+03	-.3347+03	-.9958+02	-.1728+02
1-S,S	-.7265+03	.2146+03	.1130+03	.2294+03	.2781+01
		(0.35)R			
0	.4791+03				
1-S,C	.1346+03	.4660+03	-.4569+03	-.1483+03	-.3513+02
1-S,S	-.9798+03	.2876+03	.1486+02	.3397+03	.4027+01
		(0.45)R			
0	.5008+03				
1-S,C	.1381+03	.4779+03	-.4764+03	-.1668+03	-.4781+02
1-S,S	-.1009+04	.2949+03	.1494+03	.3799+03	.4463+01
		(0.55)R			
0	.4613+03				
1-S,C	.1247+03	.4314+03	-.4383+03	-.1693+03	-.5536+02
1-S,S	-.9159+03	.2662+03	.1319+03	.3756+03	.4373+01
		(0.75)R			
0	.2414+03				
1-S,C	.6258+02	.2160+03	-.2279+03	-.9831+02	-.4033+02
1-S,S	-.4634+03	.1332+03	.6285+02	.2218+03	.2546+01
		(0.85)R			
0	.1084+03				
1-S,C	.2759+02	.9530+02	-.1022+03	-.4628+02	-.2015+02
1-S,S	-.2054+03	.5878+02	.2745+02	.1042+03	.1190+01

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 2.
BLADE HOST TRANSFER COEFFICIENTS FOR AN ARTICULATED BLADE

(D) MP = 0.3
FP = 0.001 (FOR MU = 0.25,0.4,0.5)
FP = 0.001447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S — ADVANCE RATIO, MU = 0.25

	(0,21)R			
0	.1625+03			
1-5,C	.3965+02	.0814+02	.1805+02	.7518+01	.2073+01
1-5,S	-.2453+03	.1160+03	-.1945+02	.3632+01	.9540-00
	(0,35)R			
0	.5202+03			
1-5,C	.1303+03	.0772+02	.3021+02	.5091+01	.2151+01
1-5,S	-.5306+03	.2206+03	-.2426+02	.2467+01	.5516-00
	(0,45)R			
0	.7803+03			
1-5,C	.1936+03	.4902+02	.4044+02	.1839+01	.1155+01
1-5,S	-.7143+03	.2768+03	-.1841+02	-.1076-02	-.1967-00
	(0,55)R			
0	.9767+03			
1-5,C	.2362+03	.2054+02	.5555+02	-.1153+00	-.7896-00
1-5,S	-.8207+03	.3081+03	-.3091+01	-.3312+01	-.1181+01
	(0,75)R			
0	.7472+03			
1-5,C	.1520+03	.7349+01	.8823+02	.6682+01	-.6082+01
1-5,S	-.5797+03	.2081+03	.4832+02	-.8386+01	-.2632+01
	(0,85)R			
0	.3824+03			
1-5,C	.6292+02	.0727+01	.7087+02	.8373+01	-.5587+01
1-5,S	-.2863+03	.1040+03	.4789+02	-.6599+01	-.2044+01

N,C OR S — ADVANCE RATIO, MU = 0.4

	(0,21)R			
0	.2041+03			
1-5,C	.9044+02	.1417+03	.7471+02	.5799+02	.3152+02
1-5,S	-.4099+03	.3230+03	-.6532+02	.3905+02	.1695+02
	(0,35)R			
0	.6999+03			
1-5,C	.2595+03	.1359+03	.1228+03	.5824+02	.3014+02
1-5,S	-.6691+03	.4087+03	-.8792+02	.3872+02	.1668+02
	(0,45)R			
0	.9920+03			
1-5,C	.3644+03	.9655+02	.1653+03	.1126+02	.1582+02
1-5,S	-.1145+04	.7600+03	-.7308+02	.2111+02	.9601+01
	(0,55)R			
0	.1191+04			
1-5,C	.4268+03	.5613+02	.2314+03	-.7193+01	-.7652+01
1-5,S	-.1320+04	.8421+03	-.2433+02	-.9745+01	-.2116+01
	(0,75)R			
0	.8262+03			
1-5,C	.2460+03	.5313+02	.3858+03	.3636+02	-.5908+02
1-5,S	-.9279+03	.5617+03	.1581+03	-.8377+02	-.2798+02
	(0,85)R			
0	.3927+03			
1-5,C	.8837+02	.5703+02	.3141+03	.5156+02	-.5218+02
1-5,S	-.4674+03	.2782+03	.1625+03	-.7551+02	-.2499+02

N,C OR S — ADVANCE RATIO, MU = 0.5

	(0,21)R			
0	.3457+03			
1-5,C	.1579+03	.1295+03	.1117+03	.1133+03	.3802+02
1-5,S	-.5567+03	.4964+03	-.3891+02	.3830+02	.7910+02
	(0,35)R			
0	.8467+03			
1-5,C	.3710+03	.9527+02	.1838+03	.6211+02	.4706+02
1-5,S	-.1134+04	.9089+03	-.4484+02	.2328+02	.6179+02
	(0,45)R			
0	.1160+04			
1-5,C	.4923+03	.2247+02	.2623+03	.3424-01	.3525+02
1-5,S	-.1448+04	.1109+04	-.1798+02	.6677-00	.1965+02
	(0,55)R			
0	.1342+04			
1-5,C	.5445+03	-.5067+02	.4007+03	-.4120+02	.4851+01
1-5,S	-.1663+04	.1191+04	.4684+02	-.2108+02	-.3432+02
	(0,75)R			
0	.1861+03			
1-5,C	.6263+03	-.1179+03	.7703+03	.6326+02	-.9626+02
1-5,S	-.9213+03	.8834+03	.2592+03	-.2013+02	-.1049+03
	(0,85)R			
0	.3006+03			
1-5,C	.3464+02	-.7394+02	.6467+03	.1044+03	-.9498+02
1-5,S	-.3656+03	.4855+03	.2415+03	-.4690+01	-.7937+02

N,C OR S — ADVANCE RATIO, MU = 0.7

	(0,21)R			
0	.5556+03			
1-5,C	.3375+03	.9023+02	.1014+03	.2971+03	.1904+03
1-5,S	-.9719+03	.9471+03	-.1799+03	.1366+03	.5785+02
	(0,35)R			
0	.1154+04			
1-5,C	.8218+03	-.3826+02	.2416+03	.2308+03	.2231+03
1-5,S	-.1761+04	.1599+04	-.2347+03	.1216+03	.5138+01
	(0,45)R			
0	.1436+04			
1-5,C	.7329+03	-.1433+03	.4287+03	.8742+02	.1510+03
1-5,S	-.2111+04	.1860+04	-.1982+03	.4865+02	-.3822+02
	(0,55)R			
0	.1658+04			
1-5,C	.7122+03	-.1866+03	.7335+03	-.7288+02	-.1379+02
1-5,S	-.2172+04	.1893+04	-.8745+02	-.6607+02	-.4921+02
	(0,75)R			
0	.7327+03			
1-5,C	.1464+03	.7010+02	.1379+04	-.1963+03	-.4761+03
1-5,S	-.9897+03	.9588+03	.2728+03	-.2885+03	.9090+02
	(0,85)R			
0	.2251+03			
1-5,C	-.7297+02	.1511+03	.1087+04	-.1208+03	-.4316+03
1-5,S	-.2991+03	.3691+03	.2724+03	-.2369+03	.1155+03

N,C OR S — ADVANCE RATIO, MU = 1.0

	(0,21)R			
0	.9591+03			
1-5,C	.7670+03	.1002+01	.4186+02	.8110+03	.3398+03
1-5,S	-.1851+04	.1941+04	-.6746+03	.2419+03	-.4022+03
	(0,35)R			
0	.1560+04			
1-5,C	.1001+04	-.3805+03	.3177+03	.6812+03	.4151+03
1-5,S	-.3044+04	.2900+04	-.7918+03	.1309+03	-.5332+03
	(0,45)R			
0	.1731+04			
1-5,C	.9219+03	-.6043+03	.6807+03	.3076+03	.3036+03
1-5,S	-.3416+04	.3097+04	-.6255+03	.1282+02	-.3512+03
	(0,55)R			
0	.1883+04			
1-5,C	.8441+03	-.8035+03	.1189+04	-.1551+03	.3299+02
1-5,S	-.3219+04	.2841+04	-.2706+03	-.3710+02	.1521+03
	(0,75)R			
0	.4302+03			
1-5,C	-.2148+03	.2218+03	.1925+04	-.6862+03	-.6674+03
1-5,S	-.1015+04	.1032+04	.5794+03	.1880+03	.1544+04
	(0,85)R			
0	-.3937+01			
1-5,C	-.3121+03	.3914+03	.1385+04	-.4857+03	-.5802+03
1-5,S	-.1190+03	.2652+03	.5372+03	.2098+03	.1314+04

N,C OR S — ADVANCE RATIO, MU = 1.4

	(0,21)R			
0	.1362+04			
1-5,C	.9558+03	-.2970+03	-.9846+03	.1723+04	-.1236+04
1-5,S	-.3541+04	.4429+04	-.1097+04	.6652+03	-.1045+04
	(0,35)R			
0	.1547+04			
1-5,C	.1788+03	-.1406+04	-.6921+03	.1316+04	-.8215+03
1-5,S	-.5200+04	.6209+04	-.1090+04	.1544+03	-.1317+04
	(0,45)R			
0	.1270+04			
1-5,C	-.7439+03	-.2035+04	-.1198+03	.5646+03	.1360+02
1-5,S	-.5345+04	.6531+04	-.4789+03	-.3050+02	-.8369+03
	(0,55)R			
0	.7721+03			
1-5,C	-.1554+04	-.2076+04	.5203+03	-.1236+03	.1033+04
1-5,S	-.4461+04	.5488+04	.6130+03	.4335+03	.3506+03
	(0,75)R			
0	-.2125+03			
1-5,C	-.1977+04	-.2315+03	.1073+04	-.3281+03	.2078+04
1-5,S	-.6249+03	.1787+04	.2594+04	.2554+04	.3062+04
	(0,85)R			
0	-.2701+03			
1-5,C	-.8507+03	.3276+03	.6914+03	-.1006+03	.1392+04
1-5,S	.3492+03	.4445+03	.1955+04	.2118+04	.2428+04

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 2.
BLADE TWIST TRANSFER COEFFICIENTS FOR AN ARTICULATED BLADE

(E) MP = 0.3
FP = 0.0025 (FOR MU = 0.25,0.4,0.5)
FP = 0.00112(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S		ADVANCE RATIO, MU = 0.25			
		(0.21)R			
0	.1926+03				
1-S,C	.4397+02	.7281+02	.1877+02	.5874+01	.8153-00
1-S,S	-.2570+03	.1076+03	-.2150+02	-.6045-01	-.1612+01
		(0.35)R			
0	.5182+03				
1-S,C	.1181+03	.8554+02	.3166+02	.3603+01	.5258-01
1-S,S	-.5275+03	.1976+03	-.2737+02	-.5751-00	-.1362+01
		(0.45)R			
0	.7436+03				
1-S,C	.1662+03	.7863+02	.4283+02	.1191+01	-.7414-00
1-S,S	-.6849+03	.2436+03	-.2398+02	-.1714+01	-.7046-00
		(0.55)R			
0	.8853+03				
1-S,C	.1904+03	.6664+02	.5691+02	.4063-00	-.1313+01
1-S,S	-.7568+03	.2597+03	-.1437+02	-.3699+01	.1468-01
		(0.75)R			
0	.6463+03				
1-S,C	.1199+03	.4007+02	.6949+02	.4739+01	-.8860-00
1-S,S	-.5005+03	.1622+03	.1047+02	-.7060+01	.6043-00
		(0.85)R			
0	.3331+03				
1-S,C	.5539+02	.2273+02	.4586+02	.4457+01	-.3359-00
1-S,S	-.2472+03	.7853+02	.1096+02	-.5058+01	.3738-00

N,C OR S		ADVANCE RATIO MU = 0.4			
		(0.21)R			
0	.2934+03				
1-S,C	.9427+02	.1480+03	.7334+02	.4418+02	.3046+02
1-S,S	-.4233+03	.3038+03	-.8474+02	-.2193-00	-.2170+02
		(0.35)R			
0	.6876+03				
1-S,C	.2291+03	.1770+03	.1300+03	.3332+02	.2822+02
1-S,S	-.8507+03	.3492+03	-.1182+03	-.2145+01	-.1934+02
		(0.45)R			
0	.9394+03				
1-S,C	.3108+03	.1690+03	.1815+03	.1721+02	.1385+02
1-S,S	-.1097+04	.3705+03	-.1151+03	-.8786+01	-.8379+01
		(0.55)R			
0	.1076+04				
1-S,C	.3953+03	.1544+03	.2462+03	.7494+01	-.7689+01
1-S,S	-.1214+04	.3985+03	-.8714+02	-.2179+02	.7615+01
		(0.75)R			
0	.7361+03				
1-S,C	.2010+03	.1158+03	.3046+03	.2036+02	-.4060+02
1-S,S	-.8115+03	.4336+03	.8394+01	-.4643+02	.3105+02
		(0.85)R			
0	.3671+03				
1-S,C	.8764+02	.7056+02	.2011+03	.1925+02	-.3006+02
1-S,S	-.4059+03	.2075+03	.2323+02	-.3393+02	.2266+02

N,C OR S		ADVANCE RATIO, MU = 0.5			
		(0.21)R			
0	.3721+03				
1-S,C	.1560+03	.1051+03	.1529+03	.7939+02	.1169+03
1-S,S	-.5736+03	.4725+03	-.6767+02	-.7555+01	.2484+02
		(0.35)R			
0	.8263+03				
1-S,C	.3403+03	.1949+03	.2546+03	.4361+02	.1098+03
1-S,S	-.1114+04	.6409+03	-.8339+02	-.1434+02	.1493+02
		(0.45)R			
0	.1096+04				
1-S,C	.4392+03	.1727+03	.3499+03	.4425+01	.5083+02
1-S,S	-.1393+04	.1011+04	-.7065+02	-.1656+02	.4000-00
		(0.55)R			
0	.1200+04				
1-S,C	.4643+03	.1289+03	.4796+03	-.1464+02	-.4277+02
1-S,S	-.1475+04	.1044+04	-.4032+02	-.1471+02	-.1267+02
		(0.75)R			
0	.7216+03				
1-S,C	.2264+03	.3097+02	.6205+03	.3498+02	-.1953+03
1-S,S	-.8360+03	.3859+03	.3300+02	-.5674-00	-.1490+02
		(0.85)R			
0	.3265+03				
1-S,C	.8450+02	.9251+01	.4159+03	.4075+02	-.1456+03
1-S,S	-.3699+03	.2624+03	.3319+02	.2805+01	-.7207+01

N,C OR S		ADVANCE RATIO, MU = 0.7			
		(0.21)R			
0	.5671+03				
1-S,C	.3160+03	.1644+03	.1988+03	.1955+03	.1240+03
1-S,S	-.[illegible]8+03	.8891+03	-.2694+03	-.8012+02	-.1899+03
		(0.35)R			
0	.1061+04				
1-S,C	.5631+03	.1519+03	.3889+03	.1457+03	.1252+03
1-S,S	-.1691+04	.1466+04	-.3649+03	-.9367+02	-.2003+03
		(0.45)R			
0	.1329+04				
1-S,C	.6946+03	.1251+03	.5883+03	.5471+02	.7498+02
1-S,S	-.1996+04	.1678+04	-.3711+03	-.8500+02	-.1032+03
		(0.55)R			
0	.1568+04				
1-S,C	.8220+03	.1266+03	.8432+03	-.3142+02	-.6348+01
1-S,S	-.1961+04	.1640+04	-.3330+03	-.6949+02	.7819+02
		(0.75)R			
0	.7109+03				
1-S,C	.2171+03	.1865+03	.1055+04	-.6923+02	-.1360+03
1-S,S	-.9440+03	.6000+03	-.1605+03	-.3495+02	.3992+03
		(0.85)R			
0	.2950+03				
1-S,C	.5104+02	.1348+03	.6785+03	-.3512+02	-.1014+03
1-S,S	-.3669+03	.3261+03	-.7103+02	-.1777+02	.2957+03

N,C OR S		ADVANCE RATIO, MU = 1.0			
		(0.21)R			
0	.9306+03				
1-S,C	.6569+03	.4189+02	.8664+02	.2844+03	-.2669+03
1-S,S	-.1756+04	.1808+04	-.7359+03	-.1933+03	-.3174+03
		(0.35)R			
0	.1461+04				
1-S,C	.8944+03	-.1661+03	.3982+03	.1840+03	-.2100+03
1-S,S	-.2833+04	.2722+04	-.9348+03	-.2376+03	-.3412+03
		(0.45)R			
0	.1803+04				
1-S,C	.1080+04	-.2627+03	.7531+03	.3495+02	.1017-01
1-S,S	-.3144+04	.2911+04	-.8889+03	-.1957+03	-.1939+03
		(0.55)R			
0	.1471+04				
1-S,C	.8600+03	-.1986+03	.1152+04	-.9084+02	.3179+03
1-S,S	-.2897+04	.2617+04	-.7212+03	-.9682+02	.7708+02
		(0.75)R			
0	.5755+03				
1-S,C	.5174+02	.2258+03	.1349+04	-.1096+03	.7205+03
1-S,S	-.1093+04	.9888+03	-.2406+03	.1078+03	.5175+03
		(0.85)R			
0	.1909+03				
1-S,C	-.6260+02	.2239+03	.8195+03	-.4954+02	.4835+03
1-S,S	-.3397+03	.3212+03	-.7770+02	.9441+02	.3725+03

N,C OR S		ADVANCE RATIO, MU = 1.4			
		(0.21)R			
0	.1292+04				
1-S,C	.7324+03	-.4724+03	-.3380+03	.8641+03	-.3392+03
1-S,S	-.3263+04	.4015+04	-.6503+03	.3766+03	.2955+03
		(0.35)R			
0	.1576+04				
1-S,C	.3773+03	-.1258+04	.1646+03	.7341+03	-.1419+03
1-S,S	-.4749+04	.5794+04	-.5467+03	.2926+03	.1080+03
		(0.45)R			
0	.1482+04				
1-S,C	-.1032+03	-.1566+04	.7595+03	.4665+03	.1813+03
1-S,S	-.4697+04	.6027+04	-.7363+02	.3804+03	-.7497+02
		(0.55)R			
0	.9647+03				
1-S,C	-.5101+03	-.1365+04	.1315+04	.2606+03	.5399+03
1-S,S	-.4084+04	.5262+04	.6407+03	.7497+03	-.1631+03
		(0.75)R			
0	.6816+02				
1-S,C	-.5575+03	-.1741+02	.1392+04	.1949+03	.7584+03
1-S,S	-.9899+03	.1928+04	.1478+04	.1412+04	-.1296+02
		(0.85)R			
0	-.7820+02				
1-S,C	-.2881+03	.2315+03	.7824+03	.1409+03	.4531+03
1-S,S	-.1150+03	.6347+03	.9647+03	.9452+03	.3733+02

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 2.
BLADE TWIST TRANSFER COEFFICIENTS FOR AN ARTICULATED BLADE

(F) MP = 0.3
FP = 0.01 (FOR MU = 0.25,0.4,0.5)
FP = 0.00447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S		ADVANCE RATIO, MU = 0.25			
		(0.21)R			
0	.2171+03				
1-S,C	.5958+02	.1030+03	.5397+02	.1962+02	.7806+01
1-S,S	-.2567+03	.3827+02	-.8889+01	.2979+02	.2716+02
		(0.35)R			
0	.4320+03				
1-S,C	.1130+03	.1545+03	.8540+02	.2634+02	.1218+02
1-S,S	-.4482+03	.9981+02	-.5297+01	.4276+02	.3332+02
		(0.45)R			
0	.5567+03				
1-S,C	.1359+03	.1727+03	.1015+03	.2844+02	.1443+02
1-S,S	-.5395+03	.1161+03	-.6204-00	.4619+02	.3196+02
		(0.55)R			
0	.6853+03				
1-S,C	.1440+03	.1703+03	.1082+03	.2883+02	.1545+02
1-S,S	-.5526+03	.1124+03	.2777+01	.4406+02	.2760+02
		(0.75)R			
0	.3852+03				
1-S,C	.7906+02	.1003+03	.7549+02	.2050+02	.1099+02
1-S,S	-.3200+03	.5389+02	.2395+01	.2450+02	.1408+02
		(0.85)R			
0	.1823+03				
1-S,C	.3525+02	.4763+02	.3840+02	.1074+02	.5645+01
1-S,S	-.1471+03	.2193+02	.8717-00	.1138+02	.6576+01

N,C OR S		ADVANCE RATIO, MU = 0.4			
		(0.21)R			
0	.3129+03				
1-S,C	.8134+02	.1816+03	-.4842+01	-.5680+01	-.5674+01
1-S,S	-.4248+03	.1723+03	-.1346+03	-.1975+02	-.8708+01
		(0.35)R			
0	.5835+03				
1-S,C	.1495+03	.2622+03	.9934+01	-.1219+02	-.3870+01
1-S,S	-.7369+03	.2805+03	-.1998+03	-.2418+02	-.8512+01
		(0.45)R			
0	.7282+03				
1-S,C	.1812+03	.2853+03	.2961+02	-.1651+02	-.7732-00
1-S,S	-.8843+03	.3207+03	-.2220+03	-.2577+02	-.5554+01
		(0.55)R			
0	.7677+03				
1-S,C	.1824+03	.2749+03	.5092+02	-.1879+02	.2185+01
1-S,S	-.9059+03	.3107+03	-.2182+03	-.2783+02	-.1625+01
		(0.75)R			
0	.4650+03				
1-S,C	.9513+02	.1567+03	.5816+02	-.1316+02	.3546+01
1-S,S	-.5224+03	.1576+03	-.1284+03	-.2451+02	.3030+01
		(0.85)R			
0	.2174+03				
1-S,C	.4069+02	.7368+02	.3339+02	-.6543+01	.1966+01
1-S,S	-.2400+03	.6750+02	-.6101+02	-.1388+02	.2140+01

N,C OR S		ADVANCE RATIO, MU = 0.5			
		(0.21)R			
0	.3779+03				
1-S,C	.1202+03	.2358+03	.5495+02	-.3099+02	-.6296+01
1-S,S	-.5548+03	.2787+03	-.2209+03	-.4691+02	-.3505+02
		(0.35)R			
0	.6860+03				
1-S,C	.2226+03	.3456+03	.1108+03	-.5214+02	-.1805+01
1-S,S	-.9473+03	.4427+03	-.3263+03	-.5609+02	-.3637+02
		(0.45)R			
0	.8371+03				
1-S,C	.2667+03	.3707+03	.1596+03	-.5715+02	.1746+01
1-S,S	-.1115+04	.4953+03	-.3707+03	-.5470+02	-.2432+02
		(0.55)R			
0	.8595+03				
1-S,C	.2567+03	.3416+03	.2037+03	-.4896+02	.2374+01
1-S,S	-.1108+04	.4669+03	-.3820+03	-.5061+02	-.5782+01
		(0.75)R			
0	.4867+03				
1-S,C	.1241+03	.1624+03	.1855+03	-.1134+02	-.2603+01
1-S,S	-.5864+03	.2182+03	-.2583+03	-.3383+02	.1903+02
		(0.85)R			
0	.2197+03				
1-S,C	.5654+02	.6820+02	.1021+03	-.8778-00	-.2618+01
1-S,S	-.2575+03	.8861+02	-.1309+03	-.1779+02	.1350+02

N,C OR S		ADVANCE RATIO, MU = 0.7			
		(0.21)R			
0	.5549+03				
1-S,C	.2414+03	.3352+03	-.1123+03	-.1313+03	-.4107+02
1-S,S	-.9169+03	.5098+03	-.4475+03	-.6135+02	-.3745+02
		(0.35)R			
0	.8161+03				
1-S,C	.3362+03	.4606+03	-.9953+02	-.1966+03	-.3868+02
1-S,S	-.1307+04	.6844+03	-.6751+03	-.8110+02	-.4687+02
		(0.45)R			
0	.9150+03				
1-S,C	.3575+03	.4838+03	-.4963+02	-.2227+03	-.2281+02
1-S,S	-.1419+04	.7027+03	-.7694+03	-.8195+02	-.4462+02
		(0.55)R			
0	.9153+03				
1-S,C	.3563+03	.4514+03	.1232+02	-.2251+03	-.2260+01
1-S,S	-.1374+04	.6385+03	-.7824+03	-.7303+02	-.3672+02
		(0.75)R			
0	.5631+03				
1-S,C	.1895+03	.2458+03	.7148+02	-.1418+03	.1978+02
1-S,S	-.8053+03	.3286+03	-.4973+03	-.3597+02	-.1456+02
		(0.85)R			
0	.2726+03				
1-S,C	.6857+02	.1136+03	.4508+02	-.6910+02	.1305+02
1-S,S	-.3816+03	.1484+03	-.2431+03	-.1592+02	-.5722+01

N,C OR S		ADVANCE RATIO, MU = 1.0			
		(0.21)R			
0	.7506+03				
1-S,C	.3899+03	.5721+03	-.5402+03	-.2801+03	-.5852+02
1-S,S	-.1439+04	.9435+03	-.6765+03	.1025+03	-.1355+02
		(0.35)R			
0	.1053+04				
1-S,C	.5052+03	.7709+03	-.6801+03	-.4297+03	-.5855+02
1-S,S	-.1962+04	.1226+04	-.9661+03	.1798+03	-.4295+02
		(0.45)R			
0	.1086+04				
1-S,C	.5005+03	.7953+03	-.6531+03	-.4951+03	-.4001+02
1-S,S	-.2044+04	.1218+04	-.1050+04	.2270+03	-.6896+02
		(0.55)R			
0	.1011+04				
1-S,C	.4343+03	.7397+03	-.5440+03	-.5059+03	-.1494+02
1-S,S	-.1884+04	.1061+04	-.1013+04	.2507+03	-.8886+02
		(0.75)R			
0	.5427+03				
1-S,C	.1998+03	.2135+03	-.2247+03	-.3188+03	.1541+02
1-S,S	-.9913+03	.4929+03	-.5816+03	.1759+03	-.7360+02
		(0.85)R			
0	.2477+03				
1-S,C	.8517+02	.9335+02	-.9038+02	-.1540+03	.1127+02
1-S,S	-.4467+03	.2110+03	-.2722+03	.8773+02	-.3827+02

N,C OR S		ADVANCE RATIO, MU = 1.4			
		(0.21)R			
0	.9825+03				
1-S,C	.3994+03	.4017+03	-.7314+03	.3083+03	.2010+03
1-S,S	-.2189+04	.2000+04	-.5273+03	.5342+03	-.1624+03
		(0.35)R			
0	.1256+04				
1-S,C	.4612+03	.5387+03	-.8260+03	.3875+03	.2922+03
1-S,S	-.2861+04	.2605+04	-.6537+03	.8421+03	-.2152+03
		(0.45)R			
0	.1228+04				
1-S,C	.4990+03	.5524+03	-.6943+03	.3718+03	.3220+03
1-S,S	-.2800+04	.2595+04	-.6177+03	.9875+03	-.2179+03
		(0.55)R			
0	.1046+04				
1-S,C	.2849+03	.4907+03	-.4089+03	.3092+03	.3138+03
1-S,S	-.2505+04	.2264+04	-.5052+03	.1020+04	-.1937+03
		(0.75)R			
0	.4508+03				
1-S,C	.6412+02	.2496+03	-.7128+02	.1274+03	.1810+03
1-S,S	-.1175+04	.1052+04	-.1950+03	.6432+03	-.9396+02
		(0.85)R			
0	.1904+03				
1-S,C	.1365+02	.1102+03	-.9621-00	.5111+02	.8433+02
1-S,S	-.5039+03	.4488+03	-.7580+02	.3086+03	-.4090+02

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 2.
BLADE TWIST TRANSFER COEFFICIENTS FOR AN ARTICULATED BLADE

(G) MP = 0.5
FP = 0.001 (FOR MU = 0.25,0.4,0.5)
FP = 0.000447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S — ADVANCE RATIO, MU = 0.25

(0.21)R

0	.2904+03				
1-S,C	.1024+03	.4338+02	.3163+02	.8505+01	.5345+01
1-S,S	-.4030+03	.2141+03	-.3590+02	.1336+02	.1241+01

(0.35)R

0	.9029+03				
1-S,C	.3241+03	-.3867+02	.5627+02	.2487+01	.4313+01
1-S,S	-.8474+03	.3734+03	-.3651+02	.1060+02	.2898+01

(0.45)R

0	.1338+04				
1-S,C	.4744+03	-.1212+03	.7113+02	-.1182+01	.1747+01
1-S,S	-.1108+04	.4387+03	-.1562+02	.3531+01	.3088+01

(0.55)R

0	.1654+04				
1-S,C	.5663+03	-.1955+03	.8442+02	.1651+01	-.1372+01
1-S,S	-.1265+04	.4474+03	.2650+02	-.5686+01	.1519+01

(0.75)R

0	.1197+04				
1-S,C	.3297+03	-.1764+03	.8537+02	.3681+02	-.4685+01
1-S,S	-.8466+03	.1903+03	.1457+03	-.1842+02	-.7855+01

(0.85)R

0	.5804+03				
1-S,C	.1151+03	-.9046+02	.5790+02	.3906+02	-.3282+01
1-S,S	-.4056+03	.4337+02	.1331+03	-.1419+02	-.8580+01

N,C OR S — ADVANCE RATIO, MU = 0.4

(0.21)R

0	.4859+03				
1-S,C	.2548+03	.5792+02	.9645+02	.5568+02	.6193+02
1-S,S	-.6731+03	.3859+03	-.1243+03	.1115+03	.1721+02

(0.35)R

0	.1234+04				
1-S,C	.5846+03	-.1437+03	.1842+03	.8479+01	.5341+02
1-S,S	-.1348+04	.1013+04	-.1446+03	.9957+02	.3045+02

(0.45)R

0	.1714+04				
1-S,C	.7905+03	-.3261+03	.2495+03	-.2491+02	.2289+02
1-S,S	-.1728+04	.4187+04	-.8726+02	.4410+02	.2799+02

(0.55)R

0	.2009+04				
1-S,C	.8843+03	-.4740+03	.3228+03	-.1899+02	-.2056+02
1-S,S	-.1946+04	.1213+04	.4711+02	-.4077+02	.7792+01

(0.75)R

0	.1249+04				
1-S,C	.3791+03	-.3468+03	.4039+03	.1899+03	-.9493+02
1-S,S	-.1290+04	.5403+03	.4735+03	-.2081+03	-.8777+02

(0.85)R

0	.5168+03				
1-S,C	.5408+02	-.1441+03	.2973+03	.2156+03	-.7818+02
1-S,S	-.6212+03	.1441+03	.4481+03	-.1777+03	-.9128+02

N,C OR S — ADVANCE RATIO, MU = 0.5

(0.21)R

0	.6333+03				
1-S,C	.3795+03	-.2213+02	.8566+02	.1253+03	.1033+03
1-S,S	-.9261+03	.3943+03	-.1422+03	.2086+03	.8877+02

(0.35)R

0	.1474+04				
1-S,C	.7868+03	-.3079+03	.2071+03	.1498+02	.1095+03
1-S,S	-.1743+04	.1491+04	-.1417+03	.1734+03	.9505+02

(0.45)R

0	.1966+04				
1-S,C	.9805+03	-.3460+03	.3338+03	-.7379+02	.6695+02
1-S,S	-.2141+04	.1697+04	-.4997+02	.6466+02	.5599+02

(0.55)R

0	.2267+04				
1-S,C	.1001+04	-.7415+03	.5131+03	-.8993+02	-.1497+02
1-S,S	-.2267+04	.1661+04	.1359+03	-.8751+02	-.2239+02

(0.75)R

0	.1108+04				
1-S,C	.1841+03	-.6011+03	.8581+03	.2886+03	-.2327+03
1-S,S	-.1183+04	.5343+03	.6664+03	-.3394+03	-.2405+03

(0.85)R

0	.3114+03				
1-S,C	-.1719+03	-.3070+03	.6843+03	.3615+03	-.2160+03
1-S,S	-.4094+03	.9201-00	.6065+03	-.2759+03	-.2235+03

N,C OR S — ADVANCE RATIO, MU = 0.7

(0.21)R

0	.9931+03				
1-S,C	.7635+03	-.2142+03	-.1059+03	.3137+03	.2798+03
1-S,S	-.1637+04	.1694+04	-.4641+03	.5682+03	-.5831+02

(0.35)R

0	.1660+04				
1-S,C	.1183+04	-.7022+03	.9021+02	.1743+03	.3865+03
1-S,S	-.2708+04	.2569+04	-.5012+03	.5282+03	-.6986+02

(0.45)R

0	.2245+04				
1-S,C	.1233+04	-.9899+03	.3810+03	-.1712+02	.2956+03
1-S,S	-.3072+04	.2753+04	-.3401+03	.2480+03	-.5105+02

(0.55)R

0	.2290+04				
1-S,C	.9978+03	-.1071+04	.7945+03	-.1847+03	.3989+01
1-S,S	-.2986+04	.2519+04	-.3949+02	-.2040+03	-.6649+01

(0.75)R

0	.8724+03				
1-S,C	-.2922+03	-.2140+03	.1489+04	-.1320+03	-.9778+03
1-S,S	-.1078+04	.6921+03	.6680+03	-.1109+04	.1203+03

(0.85)R

0	.1436+03				
1-S,C	-.5449+03	.1589+03	.1142+04	-.1400+02	-.9146+03
1-S,S	-.1788+03	-.1478+02	.5985+03	-.9231+03	.1113+03

N,C OR S — ADVANCE RATIO, MU = 1.0

(0.21)R

0	.1554+04				
1-S,C	.1395+04	-.2377+03	-.5601+03	.1259+04	.6171+02
1-S,S	-.3099+04	.3450+04	-.1380+04	.9232+03	-.9639+03

(0.35)R

0	.2111+04				
1-S,C	.1315+04	-.1027+04	-.2618+03	.9248+03	.2937+02
1-S,S	-.4632+04	.4582+04	-.1389+04	.6141+03	-.1078+04

(0.45)R

0	.2868+04				
1-S,C	.7496+03	-.1466+04	.2052+03	.2771+03	.3931+03
1-S,S	-.4888+04	.4410+04	-.9037+03	.1648+03	-.6446+03

(0.55)R

0	.1675+04				
1-S,C	-.6173+02	-.1487+04	.7375+03	-.4164+03	.3233+03
1-S,S	-.4331+ 4	.5494+04	-.1526+03	-.1881+03	.2671+03

(0.75)R

0	.1942+03				
1-S,C	-.1324+04	.3150+02	.1204+04	-.8908+03	-.3280+03
1-S,S	-.1051+04	.3168+03	.1154+04	.3941+01	.2412+01

(0.85)R

0	-.1751+03				
1-S,C	-.1030+04	.4867+03	.8022+03	-.5401+03	-.3932+03
1-S,S	.5513+02	-.4225+03	.9452+03	.1657+03	.2005+04

N,C OR S — ADVANCE RATIO, MU = 1.4

(0.21)R

0	.1633+04				
1-S,C	.7382+03	-.2499+02	-.2344+04	.3573+04	-.3216+04
1-S,S	-.5915+04	.7096+04	-.7738+03	.9829+03	-.1297+04

(0.35)R

0	.1156+04				
1-S,C	-.1739+04	-.1840+04	-.2117+04	.2379+04	-.2514+04
1-S,S	-.7772+04	.9244+04	-.1119+03	.9400+02	-.2064+04

(0.45)R

0	.3799+03				
1-S,C	-.3898+04	-.3107+04	-.1456+04	.7703+03	-.4967+03
1-S,S	-.7330+04	.6910+04	.1016+04	-.5835+02	-.1698+04

(0.55)R

0	-.3041+03				
1-S,C	-.5332+04	-.3591+04	-.9148+03	-.2987+03	.2306+04
1-S,S	-.5506+04	.7288+04	.2516+04	.1094+04	-.1751+03

(0.75)R

0	-.4025+03				
1-S,C	-.3652+04	-.1324+04	-.8814+03	.6775+03	.6030+04
1-S,S	-.2280+02	.2061+04	.4276+04	.5465+04	.4076+04

(0.85)R

0	-.1233+03				
1-S,C	-.1637+04	-.4786+03	-.7077+03	.9599+03	.4255+04
1-S,S	.9377+03	.4274+03	.2911+04	.4451+04	.3410+04

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 2.
BLADE TWIST TRANSFER COEFFICIENTS FOR AN articulated BLADE

(H) MP = 0.5
FP = 0.0025 (FOR MU = 0.25,0.4,0.5)
FP = 0.00112(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S — ADVANCE RATIO, MU = 0.25

(0.21)R

0	.3393+03				
1-5,C	.1102+03	.5124+02	.3232+02	.1178+02	.5334+01
1-5,S	-.4163+03	.2041+03	-.3337+02	.4072+01	-.2551+01

(0.35)R

0	.8931+03				
1-5,C	.2940+03	-.1067+01	.5798+02	.8109+01	.4698+01
1-5,S	-.8366+03	.3533+03	-.3452+02	.3084+01	-.8256-00

(0.45)R

0	.1206+04				
1-5,C	.4096+03	-.5882+02	.7603+02	.4456+01	.2174+01
1-5,S	-.1072+04	.4143+03	-.1736+02	-.4047-00	.9826-00

(0.55)R

0	.1409+04				
1-5,C	.4610+03	-.1071+03	.9274+02	.4444+01	-.1285+01
1-5,S	-.1172+04	.4134+03	.1454+02	-.6019+01	.2092+01

(0.75)R

0	.1651+04				
1-5,C	.2677+03	-.9916+02	.9170+02	.1488+02	-.5921+01
1-5,S	-.7463+03	.2005+03	.7517+02	-.1506+02	.5081-00

(0.85)R

0	.5301+03				
1-5,C	.1151+03	-.5173+02	.5644+02	.1257+02	-.4263+01
1-5,S	-.3626+03	.7847+02	.5758+02	-.1093+02	-.3471-00

N,C OR S — ADVANCE RATIO, MU = 0.4

(0.21)R

0	.5294+03				
1-5,C	.2359+03	.8242+02	.1133+03	.8724+02	.6543+02
1-5,S	-.6906+03	.5624+03	-.1129+03	.4119+02	-.3102+02

(0.35)R

0	.1206+04				
1-5,C	.5346+03	-.4332+02	.2112+03	.5826+02	.6051+02
1-5,S	-.1329+04	.9653+03	-.1330+03	.3582+02	-.1883+02

(0.45)R

0	.1617+04				
1-5,C	.6985+03	-.1655+03	.2878+03	.2177+02	.2812+02
1-5,S	-.1674+04	.1129+04	-.8632+02	.7722+01	.8051-00

(0.55)R

0	.1810+04				
1-5,C	.7424+03	-.2547+03	.3665+03	.2043+01	-.2162+02
1-5,S	-.1812+04	.1126+04	.1713+02	-.3855+02	.2085+02

(0.75)R

0	.1144+04				
1-5,C	.3598+03	-.1899+03	.3915+03	.4016+02	-.9959+02
1-5,S	-.1152+04	.5549+03	.2424+03	-.1158+03	.3200+02

(0.85)R

0	.5397+03				
1-5,C	.1293+03	-.8716+02	.2467+03	.4139+02	-.7381+02
1-5,S	-.5661+03	.2217+03	.1932+03	-.8524+02	.1912+02

N,C OR S — ADVANCE RATIO, MU = 0.5

(0.21)R

0	.6758+03				
1-5,C	.3628+03	.3709+01	.1639+03	.1675+03	.1682+03
1-5,S	-.9353+03	.3673+03	-.1150+03	.7743+02	-.1249+02

(0.35)R

0	.1444+04				
1-5,C	.7240+03	-.1869+03	.3248+03	.9228+02	.1648+03
1-5,S	-.1711+04	.1444+04	-.1131+03	.5627+02	-.9701+01

(0.45)R

0	.1867+04				
1-5,C	.8837+03	-.3563+03	.4744+03	.7506+01	.8296+02
1-5,S	-.2071+04	.1846+04	-.4207+02	.2922+01	-.1989+01

(0.55)R

0	.2061+04				
1-5,C	.9701+03	-.4888+03	.6533+03	-.3800+02	-.5422+02
1-5,S	-.2129+04	.1505+04	.8769+02	-.7008+02	.8556+01

(0.75)R

0	.1883+04				
1-5,C	.2869+03	-.1078+03	.7947+03	.5482+02	-.2919+03
1-5,S	-.1110+04	.6616+03	.3287+03	-.1647+03	.2231+02

(0.85)R

0	.4490+03				
1-5,C	.4552+02	-.2173+03	.5194+03	.7164+02	-.2208+03
1-5,S	-.4655+03	.2165+03	.2480+03	-.1155+03	.1573+02

N,C OR S — ADVANCE RATIO, MU = 0.7

(0.21)R

0	.1011+04				
1-5,C	.6921+03	-.1831+03	.8795+02	.3429+03	.1138+03
1-5,S	-.1593+04	.1597+04	-.4030+03	.7286+02	-.3853+03

(0.35)R

0	.1611+04				
1-5,C	.1060+04	-.5704+03	.3491+03	.2307+03	.1590+03
1-5,S	-.2623+04	.2438+04	-.4615+03	.2827+02	-.3899+03

(0.45)R

0	.2146+04				
1-5,C	.1135+04	-.7777+03	.6531+03	.4518+02	.1285+03
1-5,S	-.2961+04	.2623+04	-.3632+03	-.6121+02	-.1972+03

(0.55)R

0	.2122+04				
1-5,C	.9345+03	-.7851+03	.1020+04	-.1321+03	.3089+02
1-5,S	-.2863+04	.2368+04	-.1740+03	-.1849+03	.1395+03

(0.75)R

0	.9645+03				
1-5,C	.5844+02	-.4934+03	.1302+04	-.2072+03	-.2055+03
1-5,S	-.1135+04	.8291+03	.1955+03	-.3299+03	.7036+03

(0.85)R

0	.3534+03				
1-5,C	-.1278+03	.1762+02	.8312+03	-.1135+03	-.1683+03
1-5,S	-.3708+03	.2252+03	.1736+03	-.2214+03	.5172+03

N,C OR S — ADVANCE RATIO, MU = 1.0

(0.21)R

0	.1520+04				
1-5,C	.1157+04	-.5128+03	-.3404+03	.5867+03	-.6984+03
1-5,S	-.2938+04	.5179+04	-.1000+04	.1145+03	-.6674+03

(0.35)R

0	.2129+04				
1-5,C	.1199+04	-.1319+04	.1960+02	.3265+03	-.5325+03
1-5,S	-.4409+04	.4413+04	-.1005+04	-.5423+01	-.6720+03

(0.45)R

0	.2143+04				
1-5,C	.8257+03	-.1684+04	.4967+03	.1164+02	-.4472+02
1-5,S	-.4651+04	.4396+04	-.6477+03	-.5484+02	-.3658+03

(0.55)R

0	.1790+04				
1-5,C	.2442+03	-.1586+04	.9929+03	-.1968+03	.6311+03
1-5,S	-.4049+04	.3588+04	-.1169+03	.1812+02	.1388+03

(0.75)R

0	.4989+03				
1-5,C	-.6223+03	-.2740+03	.1222+04	-.7156+02	.1402+04
1-5,S	-.1262+04	.6100+03	.6328+03	.3337+03	.8892+03

(0.85)R

0	.9709+02				
1-5,C	-.4742+03	.9719+02	.7284+03	.2178+02	.9273+03
1-5,S	-.2828+03	.5209+02	.4643+03	.2664+03	.6313+03

N,C OR S — ADVANCE RATIO, MU = 1.4

(0.21)R

0	.1642+04				
1-5,C	.2674+03	-.1045+04	-.1400+04	.2209+04	-.1510+04
1-5,S	-.5409+04	.6781+04	.8893+02	.1151+04	.6031+03

(0.35)R

0	.1534+04				
1-5,C	-.1465+04	-.2746+04	-.9182+03	.1878+04	-.9975+03
1-5,S	-.7329+04	.9249+04	.9939+03	.1052+04	.1175+04

(0.45)R

0	.9828+03				
1-5,C	-.2861+04	-.3556+04	-.1950+03	.1326+04	.1130+03
1-5,S	-.7049+04	.9225+04	.2101+04	.1214+04	-.3664+03

(0.55)R

0	.3340+03				
1-5,C	-.3620+04	-.3421+04	.4152+03	.1073+04	.1468+04
1-5,S	-.5360+04	.7714+04	.3335+04	.1929+04	-.6516+03

(0.75)R

0	-.3504+03				
1-5,C	-.2269+04	-.9323+03	.5406+03	.1292+04	.2603+04
1-5,S	-.5930+03	.2516+04	.3841+04	.3146+04	-.3520+03

(0.85)R

0	-.2485+03				
1-5,C	-.1014+04	-.8862+02	.2580+03	.8840 03	.1613+04
1-5,S	.3280+03	.7400+03	.2269+04	.2071+04	-.1086+03

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 2.
BLADE TWIST TRANSFER COEFFICIENTS FOR AN ARTICULATED BLADE

(I) MP = 0.5
FP = 0.01 (FOR MU = 0.25,0.4,0.5)
FP = 0.00447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S		ADVANCE RATIO, MU = 0.25			
		(0,21)R			
0	.3905+03				
1-5,C	.9222+02	.8354+02	.1371+02	.6122-00	-.7838-00
1-5,S	-.4165+03	.1393+03	-.4591+02	-.5750+01	-.1472+01
		(0,35)R			
0	.7689+03				
1-5,C	.1791+03	.9970+02	.3010+02	-.4907-00	-.2912-00
1-5,S	-.7220+03	.2261+03	-.6238+02	-.7449+01	-.9268-00
		(0,45)R			
0	.9845+03				
1-5,C	.2222+03	.9233+02	.4320+02	-.1294+01	.3198-00
1-5,S	-.8630+03	.2672+03	-.6298+02	-.8548+01	-.2356-00
		(0,55)R			
0	.1057+04				
1-5,C	.2268+03	.7579+02	.5320+02	-.1501+01	.8134-00
1-5,S	-.8756+03	.2471+03	-.5442+02	-.9945+01	.2186-00
		(0,75)R			
0	.8555+03				
1-5,C	.1197+03	.3396+02	.4429+02	-.3368-00	.7921-00
1-5,S	-.4938+03	.1217+03	-.2227+02	-.9436+01	.8634-01
		(0,85)R			
0	.3087+03				
1-5,C	.5123+02	.1498+02	.2359+02	.4943-01	.4017-00
1-5,S	-.2237+03	.5109+02	-.8587+01	-.5400+01	-.4032-01

N,C OR S		ADVANCE RATIO, MU = 0.4			
		(0,21)R			
0	.5441+03				
1-5,C	.1930+03	.1998+03	.5055+02	.9757-00	-.1216+02
1-5,S	-.6809+03	.2797+03	-.1840+03	-.3572+02	-.2065+02
		(0,35)R			
0	.1062+04				
1-5,C	.3493+03	.2538+03	.1131+03	-.1108+02	-.7745+01
1-5,S	-.1102+04	.8092+03	-.2616+03	-.4499+02	-.1836+02
		(0,45)R			
0	.1257+04				
1-5,C	.4173+03	.2506+03	.1656+03	-.2045+02	-.1207+01
1-5,S	-.1380+04	.9872+03	-.2752+03	-.5050+02	-.1025+02
		(0,55)R			
0	.1268+04				
1-5,C	.4116+03	.2220+03	.2085+03	-.2506+02	.4296+01
1-5,S	-.1397+04	.8544+03	-.2500+03	-.5803+02	-.8530-00
		(0,75)R			
0	.7561+03				
1-5,C	.2015+03	.1155+03	.1804+03	-.1519+02	.5468+01
1-5,S	-.7918+03	.3150+03	-.1175+03	-.5510+02	.7942+01
		(0,85)R			
0	.3479+03				
1-5,C	.8252+02	.5370+02	.9737+02	-.6616+01	.2715+01
1-5,S	-.3606+03	.1304+03	-.4946+02	-.3164+02	.5090+01

N,C OR S		ADVANCE RATIO, MU = 0.5			
		(0,21)R			
0	.6618+03				
1-5,C	.2677+03	.2312+03	.1338+03	-.2291+02	-.2084+02
1-5,S	-.8897+03	.6001+03	-.2881+03	-.7815+02	-.6233+02
		(0,35)R			
0	.1182+04				
1-5,C	.4940+03	.2985+03	.2647+03	-.6116+02	-.9530+01
1-5,S	-.1480+04	.9377+03	-.4092+03	-.9569+02	-.6190+02
		(0,45)R			
0	.1423+04				
1-5,C	.5693+03	.2874+03	.3706+03	-.7883+02	.1154+01
1-5,S	-.1712+04	.1033+04	-.4445+03	-.9852+02	-.3870+02
		(0,55)R			
0	.1457+04				
1-5,C	.5394+03	.2341+03	.4582+03	-.7451+02	.5207+01
1-5,S	-.1671+04	.9547+03	-.4334+03	-.9971+02	-.5398+01
		(0,75)R			
0	.7779+03				
1-5,C	.2344+03	.7966+02	.3963+03	-.1964+02	-.4246+01
1-5,S	-.8535+03	.4178+03	-.2614+03	-.7800+02	.3557+02
		(0,85)R			
0	.3423+03				
1-5,C	.8761+02	.2655+02	.2142+03	-.2025+01	-.4974+01
1-5,S	-.3650+03	.1616+03	-.1268+03	-.4283+02	.2440+02

N,C OR S		ADVANCE RATIO, MU = 0.7			
		(0,21)R			
0	.9610+03				
1-5,C	.5199+03	.4253+03	-.7836-00	-.1762+03	-.1115+03
1-5,S	-.1491+04	.1114+04	-.6200+03	-.9711+02	-.5864+02
		(0,35)R			
0	.1364+04				
1-5,C	.6951+03	.4962+03	.1361+03	-.2820+03	-.1029+03
1-5,S	-.2068+04	.1468+04	-.9063+03	-.1415+03	-.6811+02
		(0,45)R			
0	.1516+04				
1-5,C	.7108+03	.4975+03	.2805+03	-.3361+03	-.5754+02
1-5,S	-.2191+04	.1478+04	-.1006+04	-.1567+03	-.5904+02
		(0,55)R			
0	.1485+04				
1-5,C	.6963+03	.4632+03	.4086+03	-.3563+03	.2714-00
1-5,S	-.2065+04	.1312+04	-.9972+03	-.1549+03	-.4174+02
		(0,75)R			
0	.8844+03				
1-5,C	.3269+03	.1274+03	.3848+03	-.2411+03	.5976+02
1-5,S	-.1147+04	.6401+03	-.6073+03	-.9392+02	-.7983+01
		(0,85)R			
0	.4229+03				
1-5,C	.1469+03	.9592+02	.2080+03	-.1202+03	.3871+02
1-5,S	-.5344+03	.2821+03	-.2927+03	-.4519+02	-.9494-00

N,C OR S		ADVANCE RATIO, MU = 1.0			
		(0,21)R			
0	.1258+04				
1-5,C	.6769+03	.5720+02	-.3738+03	-.2320+03	-.9967+02
1-5,S	-.2411+04	.2095+04	-.9714+03	.1368+03	-.4695+02
		(0,35)R			
0	.1653+04				
1-5,C	.8114+03	.4536+02	-.3291+03	-.3752+03	-.2987+02
1-5,S	-.3199+04	.2662+04	-.1308+04	.2385+03	-.1006+03
		(0,45)R			
0	.1674+04				
1-5,C	.7327+03	.1501+02	-.1646+03	-.4492+03	.7370+02
1-5,S	-.3247+04	.2582+04	-.1347+04	.3000+03	-.1411+03
		(0,55)R			
0	.1493+04				
1-5,C	.5576+03	-.1986+02	.3470+02	-.4750+03	.1775+03
1-5,S	-.2942+04	.2179+04	-.1226+04	.3303+03	-.1679+03
		(0,75)R			
0	.7326+03				
1-5,C	.1665+03	-.4620+02	.2160+03	-.3146+03	.2096+03
1-5,S	-.1431+04	.9340+03	-.6276+03	.2309+03	-.1285+03
		(0,85)R			
0	.3219+03				
1-5,C	.5322+02	-.2751+02	.1343+03	-.1543+03	.1163+03
1-5,S	-.6303+03	.3836+03	-.2809+03	.1151+03	-.6560+02

N,C OR S		ADVANCE RATIO, MU = 1.4			
		(0,21)R			
0	.1313+04				
1-5,C	.6939+02	-.3819+03	-.5939+02	.1346+04	.3173+03
1-5,S	-.3771+04	.4879+04	-.1460+03	.4239+03	-.7548+03
		(0,35)R			
0	.1573+04				
1-5,C	-.1390+03	-.4710+03	.3965+03	.1943+04	.6468+03
1-5,S	-.4727+04	.6306+04	.7071+02	.7187+03	-.1069+04
		(0,45)R			
0	.1424+04				
1-5,C	-.3713+03	-.4424+03	.8759+03	.2128+04	.8816+03
1-5,S	-.4523+04	.6235+04	.3352+03	.8852+03	-.1152+04
		(0,55)R			
0	.1090+04				
1-5,C	-.5717+03	-.3575+03	.1276+04	.2062+04	.1022+04
1-5,S	-.3747+04	.5368+04	.5743+03	.9524+03	-.1097+04
		(0,75)R			
0	.5456+03				
1-5,C	-.5311+03	-.1356+03	.1141+04	.1177+04	.7451+03
1-5,S	-.1524+04	.2449+04	.5687+03	.6355+03	-.6090+03
		(0,85)R			
0	.1159+03				
1-5,C	-.2800+03	-.3172+02	.5974+03	.5466+03	.3724+03
1-5,S	-.6056+03	.1034+04	.3034+03	.3100+03	-.2799+03

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 3.
INFLOW RATIO TRANSFER COEFFICIENTS FOR AN ARTICULATED BLADE

(A) MP = 0.1
FP = 0.001 (FOR MU = 0.25,0.4,0.5)
FP = 0.000447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S	ADVANCE RATIO, MU = 0.25				
			(0.21)R		
0	.4599+02				
1-S,C	-.2216+02	-.1027+02	-.6880+01	-.8627+01	-.4949+01
1-S,S	.1731+03	-.1332+02	.9363+01	.2144+02	-.1475+02
			(0.35)R		
0	.8449+02				
1-S,C	-.5540+02	-.8119+01	-.7993+01	-.1023+02	-.3808+01
1-S,S	.2784+03	-.2073+02	.2952+01	.2153+02	-.1559+02
			(0.45)R		
0	.6842+02				
1-S,C	-.7763+02	.4209+01	-.5120+01	-.7115+01	-.8856-00
1-S,S	.3132+03	-.2517+02	-.6013+01	.1280+02	-.8769+01
			(0.55)R		
0	-.2975+02				
1-S,C	-.9382+02	.2937+02	.1510+01	.2253-00	.3153+01
1-S,S	.3695+03	-.3052+02	-.1615+02	-.2100+01	.4820+01
			(0.75)R		
0	-.4359+03				
1-S,C	-.6041+02	.1027+03	.2223+02	.2339+02	.9727+01
1-S,S	.1532+03	-.3887+02	-.2477+02	-.3635+02	.4247+02
			(0.85)R		
0	-.4311+03				
1-S,C	-.3479+02	.9201+02	.2115+02	.2258+02	.7816+01
1-S,S	.3631+02	-.2959+02	-.1699+02	-.3286+02	.3927+02

N,C OR S	ADVANCE RATIO, MU = 0.4				
			(0.21)R		
0	.2326+02				
1-S,C	-.5020+02	-.7107+02	-.1215+02	.2269+02	-.6275-00
1-S,S	.2862+03	-.3779+02	.8820+01	.1769+02	-.5612+01
			(0.35)R		
0	.6333+02				
1-S,C	-.9634+02	-.7919+02	-.1547+02	.1975+02	.1774+01
1-S,S	.4313+03	-.6310+02	-.2550+02	.1975+02	-.7582+01
			(0.45)R		
0	.5011+02				
1-S,C	-.1374+03	-.5074+02	-.1180+02	.7791+01	.3791+01
1-S,S	.5105+03	-.7810+02	-.6271+02	.1178+02	-.5907+01
			(0.55)R		
0	-.3711+02				
1-S,C	-.1635+03	.9342+01	-.1715+01	-.1048+02	.5168+01
1-S,S	.5285+03	-.9309+02	-.1044+03	-.5553+01	-.6247-00
			(0.75)R		
0	-.4430+03				
1-S,C	-.1371+03	.1858+03	.3319+02	-.4657+02	.2351+01
1-S,S	.2594+03	-.1034+03	-.1419+03	-.5746+02	.1898+02
			(0.85)R		
0	-.4394+03				
1-S,C	-.7645+02	.1735+03	.3295+02	-.3961+02	.8753-01
1-S,S	.8037+02	-.7396+02	-.1004+03	-.5397+02	.1894+02

N,C OR S	ADVANCE RATIO, MU = 0.5				
			(0.21)R		
0	-.2612+02				
1-S,C	-.4297+02	-.1610+03	-.3447+02	.6775+02	.9200+01
1-S,S	.2673+03	-.7774+02	.3829+01	-.1531+02	.6770+01
			(0.35)R		
0	.1102+00				
1-S,C	-.1195+03	-.2048+03	-.5320+02	.7706+02	.1440+02
1-S,S	.5145+03	-.1365+03	-.5831+02	-.9809+01	.1812-00
			(0.45)R		
0	-.9102+01				
1-S,C	-.1741+03	-.1ad2+03	-.5888+02	.4663+02	.1308+02
1-S,S	.6392+03	-.1707+03	-.1213+03	-.1277+01	-.4391+01
			(0.55)R		
0	-.8346+02				
1-S,C	-.2162+03	-.6961+02	-.5822+02	-.2170+02	.5146+01
1-S,S	.6896+03	-.2001+03	-.1899+03	.6853+01	-.3715+01
			(0.75)R		
0	-.4456+03				
1-S,C	-.1744+03	.2665+03	-.3000+02	-.2315+03	-.3032+02
1-S,S	.3641+03	-.1963+03	-.2448+03	.5955+01	.2405+02
			(0.85)R		
0	-.4312+03				
1-S,C	-.9532+02	.2770+03	-.1231+02	-.2184+03	-.3199+02
1-S,S	.1288+03	-.1315+03	-.1703+03	.3853-00	.2781+02

N,C OR S	ADVANCE RATIO, MU = 0.7				
			(0.21)R		
0	-.1376+03				
1-S,C	-.7343+02	-.3565+03	-.1449+03	-.7099+02	.1815+02
1-S,S	.2906+03	-.1508+03	-.2119+03	-.1081+03	-.1617+03
			(0.35)R		
0	-.2822+03				
1-S,C	-.1730+03	-.5549+03	-.2111+03	.3177+01	.2047+02
1-S,S	.5588+03	-.2800+03	-.3436+03	-.1016+03	-.1768+03
			(0.45)R		
0	-.2414+03				
1-S,C	-.2465+03	-.5559+03	-.2387+03	.5703+02	.1902+02
1-S,S	.6642+03	-.3619+03	-.4343+03	-.5596+02	-.1052+03
			(0.55)R		
0	-.2943+03				
1-S,C	-.2914+03	-.3893+03	-.2619+03	.5794+02	.1838+02
1-S,S	.7291+03	-.4319+03	-.5454+03	.1198+02	.4222+02
			(0.75)R		
0	-.3838+03				
1-S,C	-.2105+03	.3919+03	-.2606+03	-.1769+03	.2263+02
1-S,S	.8953+03	-.4173+03	-.6913+03	.1316+03	.4256+03
			(0.85)R		
0	-.2831+03				
1-S,C	-.1176+03	.4752+03	-.1779+03	-.2046+03	.1789+02
1-S,S	.2542+03	-.2684+03	-.5024+03	.1081+03	.3758+03

N,C OR S	ADVANCE RATIO, MU = 1.0				
			(0.21)R		
0	-.3109+03				
1-S,C	-.1242+03	-.5060+03	-.4247+03	-.3265+03	-.2244+03
1-S,S	.3930+03	-.2337+03	-.7161+03	-.2338+03	-.8910+03
			(0.35)R		
0	-.5700+03				
1-S,C	-.2985+03	-.9438+03	-.6435+03	-.2723+03	-.2410+03
1-S,S	.5082+03	-.4344+03	-.1052+04	-.2602+03	-.7143+03
			(0.45)R		
0	-.7105+03				
1-S,C	-.3983+03	-.1084+04	-.7673+03	-.9351+02	-.1179+03
1-S,S	.4982+03	-.5657+03	-.1157+04	-.1791+03	-.2417+03
			(0.55)R		
0	-.7846+03				
1-S,C	-.4406+03	-.9636+03	-.8963+03	.1599+03	.1383+03
1-S,S	.4383+03	-.6759+03	-.1168+04	-.1921+02	.3702+03
			(0.75)R		
0	-.8638+03				
1-S,C	-.2367+03	.5164+02	-.9502+03	.5431+03	.7155+03
1-S,S	.2306+03	-.6382+03	-.8098+03	.3400+03	.1148+04
			(0.85)R		
0	-.3020+03				
1-S,C	-.9122+02	.2928+03	-.6389+03	.4080+03	.5844+03
1-S,S	.1104+03	-.3953+03	-.4509+03	.2896+03	.8295+03

N,C OR S	ADVANCE RATIO, MU = 1.4				
			(0.21)R		
0	-.5058+03				
1-S,C	-.4061+03	-.3728+03	-.1052+04	-.1279+03	-.1195+04
1-S,S	.7915+03	-.2285+03	-.7023+03	-.3522+02	-.4968+03
			(0.35)R		
0	-.9363+03				
1-S,C	-.8076+03	-.7239+03	-.1534+04	-.7357+02	-.1082+04
1-S,S	.6274+03	-.3423+03	-.1145+04	-.1055+03	-.2952+03
			(0.45)R		
0	-.1173+04				
1-S,C	-.9931+03	-.8468+03	-.1832+04	.7995+02	-.9102+03
1-S,S	.4994+03	-.4076+03	-.1285+04	-.1271+03	-.7342+02
			(0.55)R		
0	-.1279+04				
1-S,C	-.1014+04	-.7628+03	-.2180+04	.3267+03	.6519+03
1-S,S	.3259+03	-.4653+03	-.1213+04	-.9178+02	.2205+02
			(0.75)R		
0	-.8705+03				
1-S,C	-.4335+03	-.5599+02	-.2364+04	.7150+03	.2348+04
1-S,S	.6940+02	-.4815+03	-.4679+03	.1007+03	-.2918+03
			(0.85)R		
0	-.4457+03				
1-S,C	-.1335+03	.1228+03	-.1526+04	.5119+03	.1727+04
1-S,S	.2298+02	-.2720+03	-.1368+03	.1072+03	-.2967+03

NOTE- DIVIDE LISTED VALUES BY 1000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 3.
INFLOW RATIO TRANSFER COEFFICIENTS FOR AN ARTICULATED BLADE

(B) MP = 0.1
FP = 0.0025 (FOR MU = 0.25,0.4,0.5)
FP = 0.00112(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S — ADVANCE RATIO, MU = 0.25

(0.21)R

0	.4920+02				
1-5,C	-.1952+02	-.8220+01	.1923+01	.5612+01	.2931+02
1-5,S	.1673+03	-.1604+02	-.1014+01	-.2662+01	.1379+02

(0.35)R

0	.6886+02				
1-5,C	-.4950+02	-.6084+01	.2477+01	.4804+01	.2572+02
1-5,S	.2647+03	-.2290+02	-.6626+01	-.8666-00	.1318+02

(0.45)R

0	.3257+02				
1-5,C	-.7006+02	.3696+01	.3154+01	.1991+01	.1018+02
1-5,S	.2948+03	-.2542+02	-.1027+02	.2175+01	.6820+01

(0.55)R

0	-.6496+02				
1-5,C	-.8290+02	.2126+02	.4556+01	-.1824+01	-.1259+02
1-5,S	.2916+03	-.2672+02	-.1141+02	.6049+01	-.3144+01

(0.75)R

0	-.2967+03				
1-5,C	-.6149+02	.5273+02	.7169+01	-.6825+01	-.4603+02
1-5,S	.1200+03	-.2193+02	-.3854+01	.1028+02	-.1924+02

(0.85)R

0	-.2324+03				
1-5,C	-.3211+02	.3873+02	.5083+01	-.4869+01	-.3350+02
1-5,S	.4689+02	-.1300+02	-.3260-00	.6952+01	-.1443+02

N,C OR S — ADVANCE RATIO, MU = 0.4

(0.21)R

0	.2099+02				
1-5,C	-.3746+02	-.6672+02	-.1340+02	.1501+02	.4793+02
1-5,S	.2428+03	-.3406+02	-.1409+02	-.7784+01	.6829+01

(0.35)R

0	.5002+02				
1-5,C	-.6837+02	-.7085+02	-.1805+02	.1200+02	.4331+02
1-5,S	.4152+03	-.5473+02	-.5161+02	-.6924+01	.4828+01

(0.45)R

0	.1896+02				
1-5,C	-.1225+03	-.4320+02	-.1698+02	.1106+01	.1787+02
1-5,S	.4842+03	-.6557+02	-.8313+02	-.4842+01	.3650-00

(0.55)R

0	-.7413+02				
1-5,C	-.1436+03	.7457+01	-.1205+02	-.1586+02	-.2118+02
1-5,S	.4815+03	-.7277+02	-.1097+03	-.3462+01	-.5321+01

(0.75)R

0	-.3052+03				
1-5,C	-.1077+03	.1037+03	.2986+01	-.4231+02	-.8208+02
1-5,S	.2341+03	-.6091+02	-.1025+03	-.4505+01	-.1179+02

(0.85)R

0	-.2389+03				
1-5,C	-.5636+02	.8101+02	.4630+01	-.3068+02	-.6044+02
1-5,S	.9228+02	-.3558+02	-.5955+02	-.3602+01	-.8074+01

N,C OR S — ADVANCE RATIO, MU = 0.5

(0.21)R

0	-.1336+02				
1-5,C	-.4956+02	-.1617+03	-.4591+02	.2230+02	-.2446+02
1-5,S	.2727+03	-.6274+02	-.3598+02	-.1979+02	-.2193+02

(0.35)R

0	-.4437+01				
1-5,C	-.1131+03	-.2013+03	-.6784+02	.2535+02	-.1893+02
1-5,S	.5907+03	-.1094+03	-.1061+03	-.1769+02	-.2517+02

(0.45)R

0	-.3130+02				
1-5,C	-.1629+03	-.1653+03	-.7358+02	.8844+01	-.3721+01
1-5,S	.6072+03	-.1368+03	-.1665+03	-.1095+02	-.1481+02

(0.55)R

0	-.1135+03				
1-5,C	-.1488+03	-.7469+02	-.7059+02	-.2743+02	.1709+02
1-5,S	.6247+03	-.1556+03	-.2227+03	-.3898+01	.7425+01

(0.75)R

0	-.3108+03				
1-5,C	-.1346+03	.1436+03	-.3806+02	-.1045+03	.4424+02
1-5,S	.3279+03	-.1300+03	-.2263+03	.1291+01	.5461+02

(0.85)R

0	-.2369+03				
1-5,C	-.6911+02	.1290+03	-.1763+02	-.8019+02	.3117+02
1-5,S	.1368+03	-.7500+02	-.1371+03	.4371-00	.4287+02

N,C OR S — ADVANCE RATIO, MU = 0.7

(0.21)R

0	-.1177+03				
1-5,C	-.8431+02	-.3522+03	-.2924+03	+.1265+03	-.5266+03
1-5,S	.3020+03	-.1131+03	-.3297+03	-.9174+02	.1409+03

(0.35)R

0	-.1901+03				
1-5,C	-.1767+03	-.5291+03	-.4193+03	+.8082+02	-.4570+03
1-5,S	.5202+03	-.2138+03	-.5163+03	-.9157+02	.1001+03

(0.45)R

0	-.2372+03				
1-5,C	-.2312+03	-.5174+03	-.4704+03	+.2231+02	-.1558+03
1-5,S	.6261+03	-.2798+03	-.6324+03	-.7509+02	.6521+01

(0.55)R

0	-.2805+03				
1-5,C	-.2555+03	-.3536+03	-.4989+03	.1499+02	.2894+03
1-5,S	.6602+03	-.3272+03	-.7392+03	+.6325+02	-.1127+03

(0.75)R

0	-.2630+03				
1-5,C	-.1661+03	.1760+03	-.4057+03	-.1789+02	.9054+03
1-5,S	.4274+03	-.2742+03	-.7036+03	+.6117+02	-.2406+03

(0.85)R

0	-.1612+03				
1-5,C	-.8895+02	.2048+03	-.2344+03	-.2757+02	.6367+03
1-5,S	.2138+03	-.1546+03	-.4240+03	-.4171+02	-.1605+03

N,C OR S — ADVANCE RATIO, MU = 1.0

(0.21)R

1	-.2041+03				
1-5,C	-.1008+03	-.5126+03	-.1017+04	-.3131+03	-.3137+03
1-5,S	.3624+03	-.1943+03	-.7117+03	-.1291+03	.4669+03

(0.35)R

0	-.5365+03				
1-5,C	-.2657+03	-.8998+03	-.1495+04	-.2748+03	-.2802+03
1-5,S	.4572+03	-.3723+03	-.1078+04	+.1577+03	.4398+03

(0.45)R

0	-.6623+03				
1-5,C	-.3646+03	-.1012+04	-.1731+04	-.1623+03	-.9647+02
1-5,S	.4669+03	-.4900+03	-.1205+04	-.1698+03	.1136+03

(0.55)R

0	-.6954+03				
1-5,C	-.3870+03	-.8945+03	-.1890+04	-.4440+02	.1822+03
1-5,S	.3951+03	-.5690+03	-.1196+04	-.1922+03	-.4444+03

(0.75)R

0	-.6193+03				
1-5,C	-.2251+03	-.1834+03	-.1563+04	.5143+02	.5493+03
1-5,S	.2138+03	-.4556+03	-.7204+03	-.2027+03	-.1261+04

(0.85)R

0	-.1976+03				
1-5,C	-.1420+03	.1852+02	-.8843+03	.3130+02	.3751+03
1-5,S	.1095+03	-.2477+03	-.3519+03	+.1260+03	-.8705+03

N,C OR S — ADVANCE RATIO, MU = 1.4

(0.21)R

0	-.4092+03				
1-5,C	-.9140+03	-.4368+03	-.1709+04	.4925+02	.2458+03
1-5,S	.4986+03	-.2006+03	-.1258+03	.1160+03	.5626+02

(0.35)R

0	-.8356+03				
1-5,C	-.7231+03	-.6254+03	-.2543+04	.1026+03	.2259+03
1-5,S	.5391+03	-.3735+03	-.2617+03	.8821+02	.4992+02

(0.45)R

0	-.1090+04				
1-5,C	-.8333+03	-.9707+03	-.2943+04	.1375+03	.6831+02
1-5,S	.4833+03	-.4136+03	-.2287+03	.9696+02	-.7549+02

(0.55)R

0	-.1145+04				
1-5,C	-.7433+03	-.9047+03	-.3152+04	.1570+03	-.1809+03
1-5,S	.3177+03	-.4189+03	-.2398+02	.1750+03	-.3166+03

(0.75)R

0	-.7024+03				
1-5,C	-.3075+03	-.2996+03	-.2388+04	.1135+03	-.4945+03
1-5,S	.1112+03	-.2345+03	.4485+03	.3310+03	-.6478+03

(0.85)R

0	-.3336+03				
1-5,C	-.1004+03	-.7202+02	-.1202+04	.5793+02	-.3279+03
1-5,S	.4722+02	-.1471+03	.3394+03	.2231+03	-.4274+03

NOTE- DIVIDE LISTED VALUES BY 1000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 3.
INFLOW RATIO TRANSFER COEFFICIENTS FOR AN ARTICULATED BLADE

(C) MP = 0.1
FP = 0.01 (FOR MU = 0.25,0.4,0.5)
FP = 0.00447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S		ADVANCE RATIO, MU = 0.25			
		(0.21)R			
0	.3466+02				
1-S,C	-.2051+02	-.8012+01	-.1678+02	.2103+01	.3888+01
1-S,S	.1439+03	-.7351+01	-.1109+02	.2312-00	.9362-00
		(0.35)R			
0	.3045+02				
1-S,C	-.3901+02	-.6728+01	-.2479+02	.1324+01	.3593+01
1-S,S	.2121+03	-.1033+02	-.2068+02	.1891-00	.5295-00
		(0.45)R			
0	-.4077+01				
1-S,C	-.4940+02	-.1367+01	-.2802+02	-.6065-00	.1559+01
1-S,S	.2261+03	-.1141+02	-.2583+02	.7484-01	.6923-01
		(0.55)R			
0	-.6131+02				
1-S,C	-.5292+02	.6254+01	-.2860+02	-.3144+01	-.1381+01
1-S,S	.2046+03	-.1161+02	-.2726+02	-.5823-01	-.1911-00
		(0.75)R			
0	-.1267+03				
1-S,C	-.3325+02	.1406+02	-.1887+02	-.5285+01	-.4654+01
1-S,S	.8904+02	-.7957+01	-.1657+02	-.1697-00	.6105-02
		(0.85)R			
0	-.8064+02				
1-S,C	-.1582+02	.8861+01	-.9463+01	-.3228+01	-.3004+01
1-S,S	.3495+02	-.4083+01	-.7763+01	-.1042+00	.7991-01

N,C OR S		ADVANCE RATIO, MU = 0.4			
		(0.21)R			
0	.1821+02				
1-S,C	-.3223+02	-.4438+02	-.7713+02	.6717+01	.1613+01
1-S,S	.2143+03	-.2195+02	-.1341+02	.3274+01	.8713-00
		(0.35)R			
0	.1295+02				
1-S,C	-.6072+02	-.4472+02	-.1140+03	.1278+02	.1956+01
1-S,S	.3334+03	-.3282+02	-.3709+02	.5353+01	.7605-00
		(0.45)R			
0	-.1934+02				
1-S,C	-.7621+02	-.2718+02	-.1272+03	-.1873+02	.9370-00
1-S,S	.3602+03	-.3734+02	-.5421+02	.6367+01	.1184+01
		(0.55)R			
0	-.7420+02				
1-S,C	-.8074+02	-.6783-00	-.1265+03	-.2501+02	-.1172+01
1-S,S	.3436+03	-.3826+02	-.6376+02	.6651+01	.2338+01
		(0.75)R			
0	-.1352+03				
1-S,C	-.4933+02	.3277+02	-.7741+02	.2488+02	-.4229+01
1-S,S	.1582+03	-.2523+02	-.4486+02	.4294+01	.3898+01
		(0.85)R			
0	-.8530+02				
1-S,C	-.2315+02	.2228+02	-.3753+02	-.1409+02	-.2828+01
1-S,S	.6382+02	-.1262+02	-.2210+02	.2104+01	.2484+01

N,C OR S		ADVANCE RATIO, MU = 0.5			
		(0.21)R			
0	-.1343+02				
1-S,C	-.4509+02	-.1177+03	-.2039+03	-.3079+02	-.3132+01
1-S,S	.2503+03	-.3898+02	-.1266+02	.3587+01	.1386+02
		(0.35)R			
0	-.2739+02				
1-S,C	-.8259+02	-.1422+03	-.3021+03	.3986+02	-.1778+01
1-S,S	.4065+03	-.6119+02	-.4851+02	.7237+01	.9992+01
		(0.45)R			
0	-.5750+02				
1-S,C	-.1012+03	-.1173+03	-.3370+03	.4806+02	-.3945-00
1-S,S	.4621+03	-.7133+02	-.7726+02	.1063+02	.2780+01
		(0.55)R			
0	-.1043+03				
1-S,C	-.1041+03	-.6310+02	-.3343+03	.6023+02	.1709-00
1-S,S	.4433+03	-.7378+02	-.9588+02	.1391+02	-.4365+01
		(0.75)R			
0	-.1440+03				
1-S,C	-.5898+02	.3616+02	-.2028+03	-.6332+02	-.8571-00
1-S,S	.2167+03	-.4785+02	-.7250+02	.1322+02	-.8284+01
		(0.85)R			
0	-.8769+02				
1-S,C	-.2660+02	.3280+02	-.9789+02	.3707+02	-.7983-00
1-S,S	.9047+02	-.2361+02	-.3660+02	.7377+01	-.4699+01

N,C OR S		ADVANCE RATIO, MU = 0.7			
		(0.21)R			
0	-.9825+02				
1-S,C	-.8017+02	-.3137+03	-.6449+03	-.9148+02	.8022+01
1-S,S	.2740+03	-.5973+02	.3090+03	.6005+02	.5969+02
		(0.35)R			
0	-.1583+03				
1-S,C	-.1178+03	-.3736+03	-.9458+03	.1315+03	.4015+01
1-S,S	.4017+03	-.8690+02	.4402+03	.9909+02	.4006+02
		(0.45)R			
0	-.1895+03				
1-S,C	-.1313+03	-.3347+03	-.1053+04	-.1439+03	-.2813+01
1-S,S	.4471+03	-.9610+02	.4779+03	.1207+03	-.1383-01
		(0.55)R			
0	-.2018+03				
1-S,C	-.1306+03	-.2508+03	-.1047+04	-.1405+03	.1013+02
1-S,S	.4442+03	-.9483+02	.4626+03	.1304+03	-.4496+02
		(0.75)R			
0	-.1374+03				
1-S,C	-.8013+02	-.6854+02	-.6404+03	.8338+02	-.1381+02
1-S,S	.2716+03	-.5734+02	.2703+03	.9061+02	-.7414+02
		(0.85)R			
0	-.6662+02				
1-S,C	-.3871+02	-.1904+02	-.3092+03	.3982+02	-.7926+01
1-S,S	.1311+03	-.2756+02	.1284+03	.4553+02	-.4351+02

N,C OR S		ADVANCE RATIO, MU = 1.0			
		(0.21)R			
0	-.2560+03				
1-S,C	-.1304+03	-.4428+03	-.4505+03	.2683+02	.2246+02
1-S,S	.2512+03	-.5279+02	.7808+03	.1558+03	.2186+02
		(0.35)R			
0	-.3817+03				
1-S,C	-.1755+03	-.5629+03	-.6482+03	.8001+02	.4537+01
1-S,S	.3295+03	-.6791+02	.1183+04	.2512+03	-.1852+02
		(0.45)R			
0	-.4301+03				
1-S,C	-.1806+03	-.5462+03	-.7091+03	.1263+03	-.2106+02
1-S,S	.3305+03	-.6677+02	.1351+04	.3002+03	-.6708+02
		(0.55)R			
0	-.4302+03				
1-S,C	-.1641+03	-.4613+03	-.6889+03	.1613+03	-.4636+02
1-S,S	.2913+03	-.5737+02	.1368+04	.3169+03	-.1118+03
		(0.75)R			
0	-.2623+03				
1-S,C	-.8385+02	-.1981+03	-.4000+03	.1325+03	-.5298+02
1-S,S	.1391+03	-.2577+02	.8507+03	.2094+03	-.1118+03
		(0.85)R			
0	-.1254+03				
1-S,C	-.3750+02	-.8146+02	-.1880+03	.6878+02	-.2926+02
1-S,S	.6036+02	-.1085+02	.4092+03	.1027+03	-.6038+02

N,C OR S		ADVANCE RATIO, MU = 1.4			
		(0.21)R			
0	-.3836+03				
1-S,C	-.2383+03	-.3348+03	.1798+03	.7713+03	.9910+02
1-S,S	.2705+03	-.1034+02	.6143+03	.6102+01	-.1217+03
		(0.35)R			
0	-.5609+03				
1-S,C	-.3176+03	-.4170+03	.2741+03	.1121+04	.1133+03
1-S,S	.3273+03	-.1047+01	.9400+03	.1983+02	-.1557+03
		(0.45)R			
0	-.6210+03				
1-S,C	-.3238+03	-.3962+03	.3136+03	.1236+04	.9693+02
1-S,S	.3087+03	.1156+02	.1079+04	.4794+02	-.1523+03
		(0.55)R			
0	-.6081+03				
1-S,C	-.2904+03	-.3251+03	.3167+03	.1205+04	.6757+02
1-S,S	.2354+03	.2351+02	.1092+04	.7183+02	-.1298+03
		(0.75)R			
0	-.5535+03				
1-S,C	-.1433+03	-.1290+03	.1933+03	.6952+03	.1318+02
1-S,S	.8048+02	.2530+02	.6695+03	.6552+02	-.5787+02
		(0.85)R			
0	-.1652+03				
1-S,C	-.6287+02	-.5065+02	.9178+02	.3239+03	.1967+01
1-S,S	.2854+02	.1369+02	.3183+03	.3442+02	-.2378+02

NOTE- DIVIDE LISTED VALUES BY 1000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 3.
INFLOW RATIO TRANSFER COEFFICIENTS FOR AN ARTICULATED BLADE

(D) MP = 0.3
FP = 0.001 (FOR MU = 0.25,0.4,0.5)
FP = 0.000447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S — ADVANCE RATIO, MU = 0.25

(0.21)R

0	.1273+03				
1-S,C	-.1891+03	.7828+02	-.3272+02	.8633+01	-.2529+01
1-S,S	.5214+03	-.1061+03	-.1444+02	-.2834+01	-.2795+01

(0.35)R

0	.2314+03				
1-S,C	-.5024+03	.1748+03	-.4150+02	.1929+01	-.1396+01
1-S,S	.7957+03	-.1161+03	-.5016+02	.1523+01	-.4185+01

(0.45)R

0	.1669+03				
1-S,C	-.7141+03	.2527+03	-.3141+02	.5763+01	.1974-00
1-S,S	.8610+03	-.9246+02	-.8347+02	.2768+01	-.3387+01

(0.55)R

0	-.1135+03				
1-S,C	-.8614+03	.3388+03	-.3927+01	.1239+02	.1682+01
1-S,S	.8103+03	-.5559+02	-.1217+03	.1721+01	-.2257-00

(0.75)R

0	-.1300+04				
1-S,C	-.6135+03	.4230+03	.9072+02	.8418+01	.1368+01
1-S,S	.2673+03	.1239+02	-.1626+03	.3290+01	.1262+02

(0.85)R

0	-.1277+04				
1-S,C	-.2989+03	.3068+03	.8981+02	.1778+01	.2253-00
1-S,S	.2308+02	.1732+02	-.1188+03	.3392+02	.1268+02

N,C OR S — ADVANCE RATIO, MU = 0.4

(0.21)R

0	.2505+02				
1-S,C	-.2935+03	.7951+02	-.1338+03	.6761+02	.3209+02
1-S,S	.7609+03	-.2685+03	-.1103+02	-.5860+02	-.2535+02

(0.35)R

0	.1094+03				
1-S,C	-.7665+03	.3282+03	-.1912+03	.5187+02	.4377+02
1-S,S	.1273+04	-.3360+03	-.1435+03	-.2392+02	-.2571+02

(0.45)R

0	.6257+02				
1-S,C	-.1083+04	.5593+03	-.1765+03	.5022+01	.3456+02
1-S,S	.1454+04	-.3156+03	-.2928+03	.3770+01	-.1564+02

(0.55)R

0	-.1803+03				
1-S,C	-.1300+04	.8150+03	-.1009+03	.6809+02	.4680+01
1-S,S	.1435+04	-.2609+03	-.4858+03	.9838-00	.1686+01

(0.75)R

0	-.1264+04				
1-S,C	-.9148+03	.1046+04	.2207+03	-.2206+03	-.1076+03
1-S,S	.5058+03	-.9923+02	-.7818+03	.1622+03	.4193+02

(0.85)R

0	-.1230+04				
1-S,C	-.4409+03	.7480+03	.2479+03	-.1870+03	-.1077+03
1-S,S	.4435+02	-.3967+02	-.6032+03	-.1796+03	.3811+02

N,C OR S — ADVANCE RATIO, MU = 0.5

(0.21)R

0	-.1377+03				
1-S,C	-.3087+03	-.5102+02	-.2842+03	.7680+02	.4806+02
1-S,S	.6228+03	-.4369+03	.5657+02	-.2058+03	-.1117+03

(0.35)R

0	-.1031+03				
1-S,C	-.9534+03	.2710+03	-.4304+03	.9699+02	.7642+02
1-S,S	.1488+04	-.6412+03	-.1428+03	.1361+03	-.1368+03

(0.45)R

0	-.1377+03				
1-S,C	-.1320+04	.6201+03	-.4453+03	.3923+02	.6739+02
1-S,S	.1785+04	-.6979+03	-.4222+03	.3876+02	-.1009+03

(0.55)R

0	-.3339+03				
1-S,C	-.1563+04	.1023+04	-.3687+03	-.1141+03	.1850+02
1-S,S	.1858+04	-.6896+03	-.8287+03	.3165+02	-.1069+02

(0.75)R

0	-.1246+04				
1-S,C	-.1081+04	.1445+04	.8981+02	.6478+03	-.1964+03
1-S,S	.8475+03	-.4761+03	-.1620+04	.1045+03	.2853+03

(0.85)R

0	-.1174+04				
1-S,C	-.5172+03	.1047+04	.2003+03	-.6088+03	-.2030+03
1-S,S	.2275+03	-.2720+03	-.1312+04	-.1601+03	.2801+03

N,C OR S — ADVANCE RATIO, MU = 0.7

(0.21)R

0	-.5334+03				
1-S,C	-.6115+03	-.2382+03	-.7113+03	.3783+03	-.3988+03
1-S,S	.8994+03	-.7773+03	-.1287+03	-.7800+03	-.7466+03

(0.35)R

0	-.7811+03				
1-S,C	-.1261+04	-.1111+03	-.1133+04	.1417+03	-.3833+03
1-S,S	.1516+04	-.1273+04	-.4127+03	.7355+03	-.8407+03

(0.45)R

0	-.8808+03				
1-S,C	-.1617+04	.2107+03	-.1342+04	.1649+02	-.1819+03
1-S,S	.1785+04	-.1518+04	-.8432+03	.3981+03	-.5460+03

(0.55)R

0	-.9562+03				
1-S,C	-.1771+04	.7571+03	-.1497+04	-.6989+02	.1662+03
1-S,S	.1871+04	-.1682+04	-.1564+04	.1170+03	.7960+02

(0.75)R

0	-.9102+03				
1-S,C	-.9872+03	.1950+04	-.1369+04	.1195+04	.9286+03
1-S,S	.1160+04	-.1439+04	-.3138+04	.1062+04	.1742+04

(0.85)R

0	-.6101+03				
1-S,C	-.3933+03	.1586+04	-.8823+03	.1196+04	.7858+03
1-S,S	.5663+03	-.8915+03	-.2498+04	.8788+03	.1561+04

N,C OR S — ADVANCE RATIO, MU = 1.0

(0.21)R

0	-.1134+04				
1-S,C	-.1149+04	-.3100+03	-.1809+04	-.1638+04	-.2282+04
1-S,S	.1236+04	-.1334+04	-.4380+03	.1728+04	-.1590+04

(0.35)R

0	-.1929+04				
1-S,C	-.2012+04	-.7327+03	-.2833+04	-.1531+04	-.2401+04
1-S,S	.1468+04	-.2002+04	-.1020+04	-.1803+04	-.1242+04

(0.45)R

0	-.2241+04				
1-S,C	-.2351+04	-.8918+03	-.3443+04	-.8844+03	-.1271+04
1-S,S	.1292+04	-.2310+04	-.1540+04	-.1076+04	-.5222+03

(0.55)R

0	-.2235+04				
1-S,C	-.2318+04	-.7753+03	-.4062+04	.6991+01	.9237+03
1-S,S	.9335+03	-.2543+04	-.2123+04	.2468+03	.2194+03

(0.75)R

0	-.1043+04				
1-S,C	-.9143+03	.2906+03	-.4305+04	.1301+04	.5770+04
1-S,S	.9155+02	-.2331+04	-.2582+04	.3006+04	.6319+03

(0.85)R

0	-.3750+03				
1-S,C	-.2338+03	.4732+03	-.2848+04	.1000+04	.4710+04
1-S,S	-.7150+02	-.1474+04	-.1734+04	.2467+04	.3291+03

N,C OR S — ADVANCE RATIO, MU = 1.4

(0.21)R

0	-.1856+04				
1-S,C	-.2927+04	.6872+03	-.2136+04	.1315+04	-.2606+04
1-S,S	.1860+04	-.1952+04	.2092+04	.1115+04	.1645+04

(0.35)R

0	-.2710+04				
1-S,C	-.4445+04	.6377+03	-.3330+04	-.1052+04	-.2521+04
1-S,S	.1791+04	-.1953+04	.1763+04	.9857+03	.1767+04

(0.45)R

0	-.2891+04				
1-S,C	-.4719+04	.3515+03	-.4163+04	-.2680+03	-.1234+04
1-S,S	.1235+04	-.1487+04	.1086+04	.9266+02	.7165+03

(0.55)R

0	-.2693+04				
1-S,C	-.4147+04	-.4648+02	-.5109+04	.8145+03	.8883+03
1-S,S	.5797+03	-.9750+03	.5705+03	.1488+04	-.1420+04

(0.75)R

0	-.1278+04				
1-S,C	-.1047+04	-.5970+03	-.5595+04	.2244+04	.4470+04
1-S,S	-.1306+03	-.4735+03	.7038+03	.4286+04	-.5698+04

(0.85)R

0	-.5326+03				
1-S,C	-.4156+02	-.4381+03	-.3596+04	.1585+04	.3353+04
1-S,S	-.1070+03	-.3108+03	.6262+03	.3163+04	-.4340+04

NOTE- DIVIDE LISTED VALUES BY 1000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 3.
INFLOW RATIO TRANSFER COEFFICIENTS FOR AN ARTICULATED BLADE

(E) MP = 0.3
FP = 0.0025 (FOR MU = 0.25,0.4,0.5)
FP = 0.00112(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S		ADVANCE RATIO, MU = 0.25			
		(0,21)R			
0	.1469+03				
1-S,C	-.2098+03	.6059+02	-.3479+02	.3657+01	-.1992+01
1-S,S	.5031+03	-.1025+03	-.2378+02	.8030+01	-.7778+01
		(0,35)R			
0	.1969+03				
1-S,C	-.4827+03	.1464+03	-.3971+02	.1663+01	.1732+01
1-S,S	.7615+03	-.1226+03	-.6108+02	.4405+01	-.7234+01
		(0,45)R			
0	.8158+02				
1-S,C	-.6511+03	.2171+03	-.2866+02	.1246+01	.4855+01
1-S,S	.8187+03	-.1107+03	-.9222+02	.1146+01	-.2502+01
		(0,55)R			
0	-.2139+03				
1-S,C	-.7337+03	.2830+03	-.6318+01	.4238+01	.6466+01
1-S,S	.7478+03	-.8564+02	-.1211+03	.8799-00	.5536+01
		(0,75)R			
0	-.8990+03				
1-S,C	-.4752+03	.2866+03	.4017+02	.5886+01	.2459+01
1-S,S	.2759+03	-.2656+02	-.1223+03	.9504+01	.1948+02
		(0,85)R			
0	-.6997+03				
1-S,C	-.2283+03	.1747+03	.3307+02	-.3586+01	.1981-00
1-S,S	.7921+02	-.8643+01	-.7428+02	.8597+01	.1452+02

N,C OR S		ADVANCE RATIO, MU = 0.4			
		(0,21)R			
0	.5483+02				
1-S,C	-.3157+03	.7094+02	-.1482+03	.1532+02	.9311+01
1-S,S	.7385+03	-.2616+03	-.4256+02	-.5924+02	-.5912+02
		(0,35)R			
0	.9538+02				
1-S,C	-.7238+03	.2946+03	-.2082+03	.1709+01	.2025+02
1-S,S	.1214+04	-.3506+03	-.1800+03	-.3843+02	-.5673+02
		(0,45)R			
0	-.2175-00				
1-S,C	-.9745+03	.4995+03	-.2016+03	-.2839+02	.1867+02
1-S,S	.1369+04	-.3533+03	-.3200+03	-.1438+02	-.2614+02
		(0,55)R			
0	-.2640+03				
1-S,C	-.1096+04	.6939+03	-.1477+03	-.7575+02	.2671+01
1-S,S	.1301+04	-.3154+03	-.4722+03	-.427 01	.2472+02
		(0,75)R			
0	-.8919+03				
1-S,C	-.7053+03	.7243+03	.3304+02	-.1483+03	-.4917+02
1-S,S	.5094+03	-.1514+03	-.5613+03	-.3920+02	.1118+03
		(0,85)R			
0	-.6881+03				
1-S,C	-.3373+03	.4402+03	.5507+02	-.1053+03	-.4202+02
1-S,S	.1511+03	-.6768+02	-.3576+03	.3756+02	.8394+02

N,C OR S		ADVANCE RATIO, MU = 0.5			
		(0,21)R			
0	-.9281+02				
1-S,C	-.4039+03	-.3088+02	-.3100+03	.5201+02	-.7327+02
1-S,S	.8053+03	-.4394+03	-.1620+02	.1673+03	-.1476+03
		(0,35)R			
0	-.9093+02				
1-S,C	-.8895+03	.2540+03	-.4683+03	.4913+02	-.4508+02
1-S,S	.1409+04	-.6651+03	-.2208+03	.1222+03	-.1615+03
		(0,45)R			
0	-.1726+03				
1-S,C	-.1179+04	.5564+03	-.5007+03	-.7287+02	.1326+01
1-S,S	.1661+04	-.7418+03	-.4778+03	.4202+02	-.9205+02
		(0,55)R			
0	-.3947+03				
1-S,C	-.1312+04	.8653+03	-.4517+03	.1481+03	.4963+02
1-S,S	.1663+04	-.7427+03	-.8043+03	.3409+02	.4591+02
		(0,75)R			
0	-.9075+03				
1-S,C	-.8299+03	.9985+03	-.1512+03	.3323+03	.7915+02
1-S,S	.8044+03	-.4666+03	-.1138+04	.6300+02	.3235+03
		(0,85)R			
0	-.6792+03				
1-S,C	-.3937+03	.6201+03	-.3515+02	.2493+03	.4811+02
1-S,S	.3124+03	-.2583+03	-.7603+03	.3030+02	.2514+03

N,C OR S		ADVANCE RATIO, MU = 0.7			
		(0,21)R			
0	-.4643+03				
1-S,C	-.6233+03	-.3228+03	-.1104+04	.8012+03	-.1121+04
1-S,S	.9074+03	-.7493+03	-.2066+03	.4266+03	-.3425+02
		(0,35)R			
0	-.7182+03				
1-S,C	-.1191+04	-.3158+03	-.1670+04	.6743+03	-.1009+04
1-S,S	.1469+04	-.1242+04	-.5205+03	.3907+03	-.1155+03
		(0,45)R			
0	-.8317+03				
1-S,C	-.1475+04	-.8411+02	-.1929+04	-.4268+03	-.3950+03
1-S,S	.1692+04	-.1496+04	-.9249+03	-.2138+03	-.1777+03
		(0,55)R			
0	-.8805+03				
1-S,C	-.1540+04	.3426+03	-.2072+04	.2546+03	.5377+03
1-S,S	.1706+04	-.1623+04	-.1482+04	.2215+02	-.2204+03
		(0,75)R			
0	-.6519+03				
1-S,C	-.8527+03	.1072+04	-.1642+04	.3144+03	.1880+04
1-S,S	.9962+03	-.1209+04	-.2065+04	.3178+03	-.1736+03
		(0,85)R			
0	-.3570+03				
1-S,C	-.3742+03	.7761+03	-.9295+03	.2555+03	.1335+04
1-S,S	.4727+03	-.6560+03	-.1356+04	.2251+03	-.9203+02

N,C OR S		ADVANCE RATIO, MU = 1.0			
		(0,21)R			
0	-.1061+04				
1-S,C	-.1146+04	-.4106+03	-.2372+04	.1699+04	-.1234+04
1-S,S	.1116+04	-.1343+04	.1954+03	.4636+02	.1150+04
		(0,35)R			
0	-.1785+04				
1-S,C	-.1901+04	-.8452+03	-.3630+04	.1593+04	-.1113+04
1-S,S	.1288+04	-.2069+04	-.8562+02	-.2670+01	.1129+04
		(0,45)R			
0	-.2058+04				
1-S,C	-.2156+04	-.1026+04	-.4333+04	.1043+04	-.5119+03
1-S,S	.1129+04	-.2385+04	-.4050+03	.1554+0	.2851+03
		(0,55)R			
0	-.2000+04				
1-S,C	-.2042+04	-.9711+03	-.4861+04	.4035+03	.3316+03
1-S,S	.8440+03	-.2486+04	-.6938+03	.4320+03	-.1235+04
		(0,75)R			
0	-.9509+03				
1-S,C	-.8645+03	-.2787+03	-.4139+04	.2689+03	.1376+04
1-S,S	.2607+03	-.1730+04	-.7196+03	.8150+03	-.3553+04
		(0,85)R			
0	-.3801+03				
1-S,C	-.3080+03	-.3385+02	-.2354+04	.1971+03	.9394+03
1-S,S	.8994+02	-.9065+03	-.4054+03	.5466+03	-.2467+04

N,C OR S		ADVANCE RATIO, MU = 1.4			
		(0,21)R			
0	-.1661+04				
1-S,C	-.2599+04	.2526+03	-.2110+04	.1087+03	.1188+04
1-S,S	.1589+04	-.1838+04	.1971+04	.5266+03	.7392+03
		(0,35)R			
0	-.2475+04				
1-S,C	-.3964+04	-.3663+02	-.3395+04	.1812+03	.9585+03
1-S,S	.1609+04	-.2056+04	.2141+04	.6948+03	.5512+03
		(0,45)R			
0	-.2672+04				
1-S,C	-.4207+04	-.3741+03	-.4166+04	.5393+03	.1705+03
1-S,S	.1212+04	-.1754+04	.1995+04	.1073+04	.1091+02
		(0,55)R			
0	-.2473+04				
1-S,C	-.3647+04	-.6707+03	-.4691+04	.9104+03	-.9271+03
1-S,S	.7204+03	-.1275+04	.1928+04	.1778+04	-.7216+03
		(0,75)R			
0	-.1154+04				
1-S,C	-.1102+04	-.6783+03	-.3773+04	.1031+04	-.2106+04
1-S,S	.8067+02	-.3910+03	.1705+04	.2580+04	-.1463+04
		(0,85)R			
0	-.4750+03				
1-S,C	-.2524+03	-.3709+03	-.2053+04	.5992+03	-.1368+04
1-S,S	.5285-00	-.1400+03	.1017+04	.1639+04	-.9329+03

NOTE- DIVIDE LISTED VALUES BY 1000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 3.
INFLOW RATIO TRANSFER COEFFICIENTS FOR AN ARTICULATED BLADE

(F) MP = 0.3
FP = 0.01 (FOR MU ≤ 0.25,0.4,0.5)
FP = 0.00447(1+MU)**2 (FOR MU ≥ 0.7,1.0,1.4)

N,C OR S					
ADVANCE RATIO, MU = 0.25					
			(0.21)R		
0	.1055+03				
1-S,C	-.2074+03	.2689+02	-.5887+02	*.4909+01	-.1629-00
1-S,S	.4260+03	-.7369+02	-.1861+02	*.2207+01	.1638-00
			(0.35)R		
0	.9030+02				
1-S,C	-.3763+03	.6498+02	-.8167+02	*.8885+01	.1016+01
1-S,S	.6149+03	-.9481+02	-.4501+02	*.1418+01	-.6101-00
			(0.45)R		
0	-.1651+02				
1-S,C	-.4577+03	.9511+02	-.8528+02	*.1129+02	.1516+01
1-S,S	.6440+03	-.9329+02	-.6344+02	*.7726-00	-.9937-00
			(0.55)R		
0	-.1913+03				
1-S,C	-.4669+03	.1167+03	-.7805+02	*.1375+02	.1120+01
1-S,S	.5696+03	-.8073+02	-.7354+02	*.8411-00	-.8317-00
			(0.75)R		
0	-.3881+03				
1-S,C	-.2589+03	.9409+02	-.3928+02	-.1213+02	-.8894-00
1-S,S	.2310+03	-.3745+02	-.5180+02	*.1928+01	.3660-00
			(0.85)R		
0	-.2463+03				
1-S,C	-.1154+03	.4935+02	-.1741+02	-.6661+01	-.8629-00
1-S,S	.8599+02	-.1623+02	-.2566+02	-.1363+01	.4261-00
ADVANCE RATIO, MU = 0.4					
			(0.21)R		
0	.4187+02				
1-S,C	-.3151+03	-.1110+02	-.2501+03	-.5387+02	-.1870+02
1-S,S	.6518+03	-.1933+03	-.2822+02	.8129-00	-.4091-00
			(0.35)R		
0	.2073+02				
1-S,C	-.5702+03	.6918+02	-.3629+03	*.7785+02	-.1431+02
1-S,S	.9935+03	-.2706+03	-.1163+03	.8488+01	-.5301+01
			(0.45)R		
0	-.7405+02				
1-S,C	-.6930+03	.1526+03	-.3923+03	*.9273+02	-.7294+01
1-S,S	.1077+04	-.2840+03	-.1927+03	.1374+02	-.6722+01
			(0.55)R		
0	-.2308+03				
1-S,C	-.7070+03	.2245+03	-.3711+03	-.1057+03	-.2142+01
1-S,S	.9795+03	-.2606+03	-.2495+03	.1551+02	-.3982+01
			(0.75)R		
0	-.3973+03				
1-S,C	-.3928+03	.2096+03	-.1976+03	*.9030+02	-.1330+01
1-S,S	.4141+03	-.1306+03	-.2056+03	.7797+01	.5715+01
			(0.85)R		
0	-.2408+03				
1-S,C	-.1754+03	.1133+03	-.8945+02	-.4974+02	-.1411+01
1-S,S	.1567+03	-.5759+02	-.1075+03	.2976+01	.4902+01
ADVANCE RATIO, MU = 0.5					
			(0.21)R		
0	-.6504+02				
1-S,C	-.3961+03	-.1472+03	-.5069+03	-.1591+03	-.5072+02
1-S,S	.7474+03	-.3117+03	.2688+02	.2496+02	.3796+02
			(0.35)R		
0	-.1124+03				
1-S,C	-.7055+03	-.9213+02	-.7565+03	-.1984+03	-.4229+02
1-S,S	.1187+04	-.4664+03	-.8919+02	.4636+02	.1337+02
			(0.45)R		
0	-.1958+03				
1-S,C	-.8516+03	.1851+02	-.8384+03	*.2167+03	-.2500+02
1-S,S	.1328+04	-.5143+03	-.2188+03	.6337+02	-.1384+02
			(0.55)R		
0	-.3210+03				
1-S,C	-.8660+03	.1464+03	-.8162+03	*.2401+03	-.1046+02
1-S,S	.1253+04	-.4941+03	-.3383+03	.7770+02	-.3212+02
			(0.75)R		
0	-.4139+03				
1-S,C	-.4816+03	.2341+03	-.4631+03	-.2171+03	-.3060+01
1-S,S	.5869+03	-.2673+03	-.3361+03	.6758+02	-.2320+02
			(0.85)R		
0	-.2494+03				
1-S,C	-.2156+03	.1393+03	-.2158+03	*.1234+03	-.2587+01
1-S,S	.2387+03	-.1212+03	-.1851+03	.3680+02	-.9619+01

N,C OR S					
ADVANCE RATIO, MU = 0.7					
			(0.21)R		
0	-.3466+03				
1-S,C	-.5969+03	-.5996+03	-.1343+04	*.3910+03	-.6130+02
1-S,S	.8191+03	-.4879+03	.4813+03	.3081+03	.2862+03
			(0.35)R		
0	-.5200+03				
1-S,C	-.8659+03	-.6827+03	-.1990+04	*.5339+03	-.8784+02
1-S,S	.1106+04	-.6932+03	.5611+03	.4934+03	.1716+03
			(0.45)R		
0	-.6063+03				
1-S,C	-.9553+03	-.5753+03	-.2235+04	*.5573+03	-.9586+02
1-S,S	.1306+04	-.7507+03	.4888+03	.5884+03	.4060+02
			(0.55)R		
0	-.6210+03				
1-S,C	-.9404+03	-.3854+03	-.2240+04	*.5164+03	-.9331+02
1-S,S	.1283+04	-.7248+03	.3487+03	.6241+03	-.1112+03
			(0.75)R		
0	-.3993+03				
1-S,C	-.5662+03	-.4268+02	-.1390+04	*.2772+03	-.5987+02
1-S,S	.7699+03	-.4215+03	.7128+02	.4227+03	-.2253+03
			(0.85)R		
0	-.1959+03				
1-S,C	-.2718+03	.1135+02	-.6743+03	*.1274+03	-.2625+02
1-S,S	.3691+03	-.1999+03	.1090+02	.2108+03	-.1348+03
ADVANCE RATIO, MU = 1.0					
			(0.21)R		
0	-.8363+03				
1-S,C	-.9572+03	-.9131+03	-.1615+04	.1396+03	.1571+03
1-S,S	.7322+03	-.6018+03	.1747+04	.7996+03	.1261+03
			(0.35)R		
0	-.1211+04				
1-S,C	-.1283+04	-.1226+04	-.2387+04	.3982+03	.1175+03
1-S,S	.9541+03	-.7770+03	.2557+04	.1279+04	.2561+02
			(0.45)R		
0	-.1332+04				
1-S,C	-.1316+04	-.1259+04	-.2670+04	.6205+03	.2689+02
1-S,S	.9507+03	-.7667+03	.2837+04	.1520+04	-.1188+03
			(0.55)R		
0	-.1302+04				
1-S,C	-.1191+04	-.1142+04	-.2652+04	.7868+03	-.7509+02
1-S,S	.8310+03	-.6619+03	.2796+04	.1597+04	-.2599+03
			(0.75)R		
0	-.7632+03				
1-S,C	-.6037+03	-.5804+03	-.1598+04	.8420+03	-.1455+03
1-S,S	.3892+03	-.3008+03	.1664+04	.1048+04	-.2972+03
			(0.85)R		
0	-.3599+03				
1-S,C	-.2690+03	-.2590+03	-.7610+03	.3327+03	-.8541+02
1-S,S	.1673+03	-.1274+03	.7885+03	.5129+03	-.1641+03
ADVANCE RATIO, MU = 1.4					
			(0.21)R		
0	-.1192+04				
1-S,C	-.1692+04	-.4669+03	.1213+03	.2203+04	.4128+03
1-S,S	.8400+03	-.4663+03	.2710+04	*.6963+02	-.6413+03
			(0.35)R		
0	-.1646+04				
1-S,C	-.2195+04	-.5805+03	.2288+03	.3371+04	.4824+03
1-S,S	.1012+04	-.4517+03	.3852+04	.4678+02	-.8009+03
			(0.45)R		
0	-.1734+04				
1-S,C	-.2178+04	-.5503+03	.3000+03	.3868+04	.4247+03
1-S,S	.9253+03	-.2920+03	.4164+04	.1861+03	-.7631+03
			(0.55)R		
0	-.1614+04				
1-S,C	-.1891+04	-.4503+03	.3383+03	.3917+04	.3109+03
1-S,S	.7188+03	-.8661+02	.3981+04	.3109+03	-.6287+03
			(0.75)R		
0	-.8560+03				
1-S,C	-.8886+03	-.1773+03	.2393+03	.2401+04	.8063+02
1-S,S	.2392+03	.1399+03	.2222+04	.3036+03	-.2525+03
			(0.85)R		
0	-.3879+03				
1-S,C	-.3687+03	-.6927+02	.1186+03	.1142+04	.2159+02
1-S,S	.8307+02	.9590+02	.1023+04	.1615+03	-.9979+02

NOTE- DIVIDE LISTED VALUES BY 1000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 3.
INFLOW RATIO TRANSFER COEFFICIENTS FOR AN ARTICULATED BLADE

(G) MP = 0.5
FP = 0.001 (FOR MU = 0.25,0.4,0.5)
FP = 0.000447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S	ADVANCE RATIO, MU = 0.25				
			(0,21)R		
0	.1664+03				
1-S,C	-.5085+03	.2788+03	-.9316+02	.2295+02	.2732+01
1-S,S	.8657+03	-.2301+03	-.3718+02	+.1801+02	-.1308+02
			(0,35)R		
0	.3242+03				
1-S,C	-.1312+04	.5435+03	-.1023+03	.8790+01	.9576+01
1-S,S	.1189+04	-.1523+03	-.1170+03	+.2116+01	-.9033+01
			(0,45)R		
0	.2027+03				
1-S,C	-.1384+04	.7014+03	-.5968+02	-.1061+02	.1112+02
1-S,S	.1177+04	-.2256+01	-.1851+03	.5599+01	-.2163+01
			(0,55)R		
0	-.2566+03				
1-S,C	-.2282+04	.8161+03	.3074+02	+.3109+02	.5720+01
1-S,S	.9769+03	.1847+03	-.2556+03	+.5373+01	.4678+01
			(0,75)R		
0	-.2123+04				
1-S,C	-.1519+04	.6749+03	.2960+03	+.4144+02	-.3124+02
1-S,S	.5845+02	.4140+03	-.2988+03	+.1067+03	.5479+01
			(0,85)R		
0	-.2058+04				
1-S,C	-.7174+03	.3987+03	.2767+03	+.2532+02	-.3440+02
1-S,S	-.2022+03	.3072+03	-.2064+03	-.1117+03	.1245+01

N,C OR S	ADVANCE RATIO, MU = 0.4				
			(0,21)R		
0	-.3166+02				
1-S,C	-.7339+03	.4999+03	-.2817+03	.1587+03	.1348+02
1-S,S	.1271+04	-.5624+03	.2952+02	-.1269+03	-.1013+03
			(0,35)R		
0	.6011+02				
1-S,C	-.1841+04	.1200+04	-.3911+03	.1229+03	.7728+02
1-S,S	.1961+04	-.4729+03	-.2379+03	+.3238+01	-.9516+02
			(0,45)R		
0	-.1670+02				
1-S,C	-.2561+04	.1681+04	-.3232+03	.8536+01	.9393+02
1-S,S	.2109+04	-.1950+03	-.5416+03	.7715+02	-.5060+02
			(0,55)R		
0	-.3711+03				
1-S,C	-.3035+04	.2061+04	-.8432+02	-.1764+03	.4496+02
1-S,S	.1924+04	.1832+03	-.9175+03	.5032+02	.1833+02
			(0,75)R		
0	-.1919+04				
1-S,C	-.2052+04	.1754+04	.8388+03	-.5845+03	-.3051+03
1-S,S	.3207+03	.7648+03	-.1423+04	-.5202+03	.1555+03
			(0,85)R		
0	-.1837+04				
1-S,C	-.9515+03	.1021+04	.8549+03	-.5010+03	-.3336+03
1-S,S	-.2651+03	.6105+03	-.1074+04	+.5851+03	.1347+03

N,C OR S	ADVANCE RATIO, MU = 0.5				
			(0,21)R		
0	-.3559+03				
1-S,C	-.9497+03	.4620+03	-.4499+03	.3126+03	-.2819+01
1-S,S	.1350+04	-.8765+03	.2762+03	-.4099+03	-.2633+03
			(0,35)R		
0	-.3358+03				
1-S,C	-.2178+04	.1451+04	-.7345+03	.3471+03	.1247+03
1-S,S	.2267+04	-.9783+03	-.7693+02	+.1612+03	-.3299+03
			(0,45)R		
0	-.3629+03				
1-S,C	-.2931+04	.2202+04	-.7387+03	.1502+03	.1694+03
1-S,S	.2596+04	-.7708+03	-.6284+03	.9264+02	-.2419+03
			(0,55)R		
0	-.6005+03				
1-S,C	-.3387+04	.2834+04	-.4845+03	.3005+03	.9020+02
1-S,S	.2570+04	-.4038+03	-.1430+04	.2213+03	-.8891+01
			(0,75)R		
0	-.1804+04				
1-S,C	-.2168+04	.2527+04	.8671+03	+.1720+04	-.5692+03
1-S,S	.9265+03	.4354+03	-.2966+04	+.4167+03	.7825+03
			(0,85)R		
0	-.1678+04				
1-S,C	-.9594+03	.1481+04	.1026+04	+.1598+04	-.6303+03
1-S,S	.9850+02	.4647+03	-.2408+04	+.6040+03	.7673+03

N,C OR S	ADVANCE RATIO, MU = 0.7				
			(0,21)R		
0	-.1057+04				
1-S,C	-.1517+04	.2679+03	-.9016+03	+.1642+03	-.8389+03
1-S,S	.1485+04	-.1441+04	.4321+03	+.1476+04	-.1126+04
			(0,35)R		
0	-.1468+04				
1-S,C	-.2718+04	.9721+03	-.1548+04	.3256+03	-.7664+03
1-S,S	.2240+04	-.1980+04	.3077+02	+.1334+04	-.1472+04
			(0,45)R		
0	-.1540+04				
1-S,C	-.3231+04	.1664+04	-.1872+04	.4075+03	-.3393+03
1-S,S	.2458+04	-.2056+04	-.8200+03	+.6122+03	-.1088+04
			(0,55)R		
0	-.1487+04				
1-S,C	-.3290+04	.2474+04	-.2054+04	+.1767+03	.3418+03
1-S,S	.2418+04	-.1962+04	-.5238+04	.4884+03	.8500+01
			(0,75)R		
0	-.9802+03				
1-S,C	-.1412+04	.3336+04	-.1560+04	+.3337+04	.1686+03
1-S,S	.1358+04	-.1259+04	-.5275+04	.2516+04	.3511+04
			(0,85)R		
0	-.5573+03				
1-S,C	-.3743+03	.2373+04	-.8891+03	+.3215+04	.1395+04
1-S,S	.6422+03	-.7092+03	-.4250+04	.2056+04	.3258+04

N,C OR S	ADVANCE RATIO, MU = 1.0				
			(0,21)R		
0	-.2085+04				
1-S,C	-.2523+04	.3822+03	-.1775+04	+.1786+04	-.3118+04
1-S,S	.2011+04	-.2605+04	.1069+04	+.2852+04	-.1151+04
			(0,35)R		
0	-.3122+04				
1-S,C	-.3731+04	.1123+03	-.3089+04	+.1597+04	-.3493+04
1-S,S	.2039+04	-.3148+04	.4352+03	+.2806+04	-.1011+04
			(0,45)R		
0	-.3320+04				
1-S,C	-.3911+04	-.1798+03	-.4002+04	+.9214+03	-.2067+04
1-S,S	.1475+04	-.3034+04	-.5457+03	+.1350+04	-.6029+03
			(0,55)R		
0	-.3002+04				
1-S,C	-.3444+04	-.3819+03	-.4933+04	.1242+03	.9461+03
1-S,S	.7141+03	-.2829+04	-.1688+04	.1221+04	-.1806+03
			(0,75)R		
0	-.9298+03				
1-S,C	-.8226+03	-.1409+03	-.5340+04	.6820+03	.8060+04
1-S,S	-.3602+03	-.2360+04	-.2764+04	.6410+04	.6558+02
			(0,85)R		
0	-.1380+03				
1-S,C	.4950+02	.3416+02	-.3513+04	.4607+03	.6696+04
1-S,S	-.3275+03	-.1553+04	-.1868+04	.5136+04	-.1211+02

N,C OR S	ADVANCE RATIO, MU = 1.4				
			(0,21)R		
0	-.3230+04				
1-S,C	-.5391+04	.1208+04	-.1468+04	+.9878+03	-.2996+04
1-S,S	.2807+04	-.3219+04	.4902+04	+.2500+04	.2138+04
			(0,35)R		
0	-.3866+04				
1-S,C	-.7193+04	.6869+03	-.2773+04	+.5308+03	-.3318+04
1-S,S	.2203+04	-.2083+04	.4287+04	+.2003+04	.1744+04
			(0,45)R		
0	-.3487+04				
1-S,C	-.7001+04	-.2084+03	-.3783+04	.4336+03	-.1919+04
1-S,S	.1084+04	-.4166+03	.2800+04	+.1416+03	.3446+03
			(0,55)R		
0	-.2685+04				
1-S,C	-.5679+04	-.1230+04	-.4791+04	.1770+04	.9059+03
1-S,S	.1267+03	.9732+03	.1617+04	.2789+04	-.1755+04
			(0,75)R		
0	-.7924+03				
1-S,C	-.1208+04	-.2093+04	-.5006+04	.3988+04	.6609+04
1-S,S	.3528+02	.8950+03	.1695+04	.7375+04	-.4868+04
			(0,85)R		
0	-.2379+03				
1-S,C	.1766+02	-.1355+04	-.3121+04	.2420+04	.5138+04
1-S,S	.2348+03	.2315+03	.1432+04	.5334+04	-.3502+04

NOTE- DIVIDE LISTED VALUES BY 1000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 3.
INFLOW RATIO TRANSFER COEFFICIENTS FOR AN ARTICULATED BLADE

(H) MP = 0.5
FP = 0.0025 (FOR MU = 0.25,0.4,0.5)
FP = 0.00112(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S — ADVANCE RATIO, MU = 0.25

	(0.21)R			
0 .2219+03				
1-5,C -.5558+03	.2500+03	-.9038+02	.6175+01	-.3629+01
1-5,S .8216+03	-.2161+03	-.4515+02	.2191+02	-.1644+02
	(0.35)R			
0 .2812+03				
1-5,C -.1266+04	.4922+03	-.9964+02	.3638+01	.2802+01
1-5,S .1145+04	-.1753+03	-.1264+03	.1262+02	-.1442+02
	(0.45)R			
0 .6287+02				
1-5,C -.1697+04	.6389+03	-.6415+02	.1620+02	.6257+01
1-5,S .1146+04	-.6599+02	-.1947+03	.6905+01	-.6298+01
	(0.55)R			
0 -.3980+03				
1-5,C -.1696+04	.7248+03	.4883+01	-.3033+02	.4437+01
1-5,S .9466+03	.6994+02	-.2565+03	.1280+02	.5078+01
	(0.75)R			
0 -.1478+04				
1-5,C -.1192+04	.5427+03	.1429+03	-.4088+02	-.1249+02
1-5,S .1837+03	.2210+03	-.2545+03	-.4954+02	.2079+02
	(0.85)R			
0 -.1139+04				
1-5,C -.5604+03	.2919+03	.1132+03	.2633+02	-.1220+02
1-5,S -.2602+02	.1518+03	-.1530+03	-.4089+02	.1502+02

N,C OR S — ADVANCE RATIO, MU = 0.4

	(0.21)R			
0 .2433+02				
1-5,C -.8035+03	.4552+03	-.2910+03	.3363+02	-.5420+02
1-5,S .1217+04	-.5463+03	-.6780+02	-.1740+03	-.1410+03
	(0.35)R			
0 .5973+02				
1-5,C -.1790+04	.1090+04	-.3969+03	.7734+01	-.4757+01
1-5,S .1876+04	-.5599+03	-.3552+03	-.9956+02	-.1428+03
	(0.45)R			
0 -.8614+02				
1-5,C -.2375+04	.1528+04	-.3400+03	-.6120+02	.3467+02
1-5,S .2008+04	-.3836+03	-.6486+03	-.2504+02	-.7720+02
	(0.55)R			
0 -.4699+03				
1-5,C -.2634+04	.1819+04	-.1476+03	-.1773+03	.4302+02
1-5,S .1775+04	-.1139+03	-.9622+03	.4531+01	.3711+02
	(0.75)R			
0 -.1357+04				
1-5,C -.1627+04	.1421+04	.3722+03	-.3702+03	-.4705+02
1-5,S .4395+03	.3232+03	-.1132+04	-.1520+03	.2434+03
	(0.85)R			
0 -.1034+04				
1-5,C -.7563+03	.7683+03	.3331+03	-.2665+03	-.5652+02
1-5,S .5510+01	.2600+03	-.7168+03	-.1441+03	.1863+03

N,C OR S — ADVANCE RATIO, MU = 0.5

	(0.21)R			
0 -.2733+03				
1-5,C -.9947+03	.4585+03	-.4840+03	.2894+02	-.2242+03
1-5,S .1326+04	-.8612+03	.3875+02	.4497+03	-.3078+03
	(0.35)R			
0 -.3675+03				
1-5,C -.2063+04	.1337+04	-.7644+03	.1915+02	-.1360+03
1-5,S .2178+04	-.1079+04	-.3617+03	.2963+03	-.3622+03
	(0.45)R			
0 -.4101+03				
1-5,C -.2696+04	.1994+04	-.7835+03	-.1102+03	-.1950+01
1-5,S .2456+04	-.9856+03	-.8858+03	.6637+02	-.2304+03
	(0.55)R			
0 -.6856+03				
1-5,C -.2935+04	.2463+04	-.5872+03	-.3461+03	.1243+03
1-5,S .2333+04	-.7237+03	-.1554+04	.1282+03	.6180+02
	(0.75)R			
0 -.1304+04				
1-5,C -.1757+04	.2003+04	.2022+03	-.8833+03	.1643+03
1-5,S .9123+03	-.2568+02	-.2247+04	.1251+03	.6975+03
	(0.85)R			
0 -.9564+03				
1-5,C -.8031+03	.1094+04	.2887+03	-.6660+03	.8788+02
1-5,S .2700+03	.9756+02	-.1504+04	.3378+02	.5540+03

N,C OR S — ADVANCE RATIO, MU = 0.7

	(0.21)R			
0 -.9250+03				
1-5,C -.1499+04	.1916+03	-.1387+04	.1256+04	-.1754+04
1-5,S .1478+04	-.1389+04	.7803+02	.9286+03	-.1527+03
	(0.35)R			
0 -.1349+04				
1-5,C -.2591+04	.7310+03	-.2207+04	.1020+04	-.1634+04
1-5,S .2199+04	-.2006+04	-.3970+03	.7974+03	-.3631+03
	(0.45)R			
0 -.1456+04				
1-5,C -.3027+04	.1288+04	-.2583+04	.6574+03	-.7103+03
1-5,S .2391+04	-.2186+04	-.1178+04	.2929+03	-.4201+03
	(0.55)R			
0 -.1390+04				
1-5,C -.2932+04	.1888+04	-.2733+04	.4953+03	.7421+03
1-5,S .2277+04	-.2158+04	-.2299+04	.4207+03	-.3130+03
	(0.75)R			
0 -.7608+03				
1-5,C -.1402+04	.2173+04	-.1956+04	.8574+03	.2923+04
1-5,S .1183+04	-.1380+04	-.3622+04	.1357+04	.2083+03
	(0.85)R			
0 -.3569+03				
1-5,C -.5411+03	.1345+04	-.1049+04	.6772+03	.2098+04
1-5,S .5298+03	-.7146+03	-.2419+04	.9469+03	.2361+03

N,C OR S — ADVANCE RATIO, MU = 1.0

	(0.21)R			
0 -.1912+04				
1-5,C -.2494+04	.3309+03	-.2501+04	-.2402+04	-.1985+04
1-5,S .1793+04	-.2345+04	.1129+04	.2247+03	.1891+04
	(0.35)R			
0 -.2927+04				
1-5,C -.3662+04	.2495+03	-.4009+04	.2186+04	-.1928+04
1-5,S .1764+04	-.3039+04	.7713+03	.4359+02	.1798+04
	(0.45)R			
0 -.3162+04				
1-5,C -.3813+04	.7491+02	-.4927+04	.1295+04	-.1004+04
1-5,S .1309+04	-.3080+04	.5646+02	.6228+03	.5442+03
	(0.55)R			
0 -.2867+04				
1-5,C -.3263+04	-.1169+03	-.5637+04	-.2340+03	.4385+03
1-5,S .7334+03	-.2878+04	-.7620+03	.1486+04	-.1592+04
	(0.75)R			
0 -.1095+04				
1-5,C -.9741+03	-.2721+03	-.4854+04	.8738+03	.2468+04
1-5,S .3060+02	-.1902+04	-.1422+04	.2472+04	-.4721+04
	(0.85)R			
0 -.3596+03				
1-5,C -.2064+03	-.1689+03	-.2758+04	.5952+03	.1733+04
1-5,S -.2674+02	-.9394+03	-.8887+03	.1615+04	-.3266+04

N,C OR S — ADVANCE RATIO, MU = 1.4

	(0.21)R			
0 -.2840+04				
1-5,C -.4693+04	.1015+04	-.1595+04	.2037+03	.1459+04
1-5,S .2407+04	-.2828+04	.3557+04	.1327+03	.1801+04
	(0.35)R			
0 -.3670+04				
1-5,C -.6459+04	.7582+03	-.2885+04	.4266+03	.9905+03
1-5,S .1974+04	-.2336+04	.3499+04	.3183+03	.1278+04
	(0.45)R			
0 -.3525+04				
1-5,C -.6379+04	.1711+03	-.3746+04	.1171+04	.8065+02
1-5,S .1052+04	-.1236+04	.2774+04	.1227+04	.1037+03
	(0.55)R			
0 -.2858+04				
1-5,C -.5133+04	-.5126+03	-.4338+04	.1913+04	-.9201+03
1-5,S .1962+03	-.1720+03	.2133+04	.2545+04	-.1307+04
	(0.75)R			
0 -.9161+03				
1-5,C -.1171+04	-.1074+04	-.3481+04	.2085+04	-.1615+04
1-5,S -.2893+03	.5065+03	.1495+04	.3789+04	-.2493+04
	(0.85)R			
0 -.2766+03				
1-5,C -.1191+03	-.6639+03	-.1874+04	.1199+04	-.9727+03
1-5,S -.1359+03	.2749+03	.8981+03	.2373+04	-.1547+04

NOTE- DIVIDE LISTED VALUES BY 1000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 3.
INFLOW RATIO TRANSFER COEFFICIENTS FOR AN ARTICULATED BLADE

(I) MP = 0.5
FP = 0.01 (FOR MU = 0.25,0.4,0.5)
FP = 0.00447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S					
	ADVANCE RATIO, MU = 0.25				
	(0.21)R				
0	.1655+03				
1-S,C	-.5571+03	.1574+03	-.1106+03	+.1751+02	-.7991+01
1-S,S	.6800+03	-.1794+03	-.3381+02	+.1356+01	.5670-00
	(0.35)R				
0	.1315+03				
1-S,C	-.1805+04	.2903+03	-.1470+03	+.2762+02	-.5023+01
1-S,S	.9417+03	-.2035+03	-.8982+02	.1822+01	-.9215-00
	(0.45)R				
0	-.4873+02				
1-S,C	-.1217+04	.3641+03	-.1451+03	-.3369+02	-.1328+01
1-S,S	.9500+03	-.1720+03	-.1323+03	.2742+01	-.1522+01
	(0.55)R				
0	-.3366+03				
1-S,C	-.1234+04	.3896+03	-.1216+03	-.3769+02	.1009+01
1-S,S	.8011+03	-.1175+03	-.1593+03	.6265-00	-.8834-00
	(0.75)R				
0	-.6490+03				
1-S,C	-.6736+03	.2483+03	-.4482+02	+.2944+02	.1178+00
1-S,S	.2748+03	-.1782+02	-.1202+03	+.6076+01	.1821+01
	(0.85)R				
0	-.4094+03				
1-S,C	-.2975+03	.1194+03	-.1591+02	-.1563+02	-.4450-00
1-S,S	.8758+02	.2018-00	-.6117+02	+.4641+01	.1523+01

N,C OR S					
	ADVANCE RATIO, MU = 0.4				
	(0.21)R				
0	.3640+02				
1-S,C	-.8051+03	.2651+03	-.4246+03	-.1188+03	-.6269+02
1-S,S	.1034+04	-.4831+03	-.6854+02	.6934+01	.1973+02
	(0.35)R				
0	-.5713+01				
1-S,C	-.1441+04	.5840+03	-.6107+03	+.1650+03	-.4725+02
1-S,S	.1520+04	-.6223+03	-.2623+03	.3594+02	.4171+01
	(0.45)R				
0	-.1520+03				
1-S,C	-.1740+04	.7891+03	-.6437+03	+.1933+03	-.2104+02
1-S,S	.1594+04	-.5969+03	-.4357+03	.5242+02	-.7112+01
	(0.55)R				
0	-.3886+03				
1-S,C	-.1763+04	.8842+03	-.5806+03	+.2206+03	.8489-00
1-S,S	.1389+04	-.4825+03	-.5723+03	.5185+02	-.7665+01
	(0.75)R				
0	-.6265+03				
1-S,C	-.9649+03	.5881+03	-.2597+03	+.1937+03	.8360+01
1-S,S	.5008+03	-.1583+03	-.4903+03	.1238+02	.1160+02
	(0.85)R				
0	-.3892+03				
1-S,C	-.4273+03	.2849+03	-.1050+03	+.1080+03	.3250+01
1-S,S	.1635+03	-.5067+02	-.2605+03	.2956-01	.1078+02

N,C OR S					
	ADVANCE RATIO, MU = 0.5				
	(0.21)R				
0	-.1687+03				
1-S,C	-.9691+03	.2048+03	-.7695+03	-.2966+03	-.1445+03
1-S,S	.1175+04	-.7737+03	.1865+02	.7081+02	.1214+03
	(0.35)R				
0	-.2575+03				
1-S,C	-.1693+04	.5889+03	-.1167+04	+.3641+03	-.1166+03
1-S,S	.1794+04	-.1086+04	-.2385+03	.1574+03	.6717+02
	(0.45)R				
0	-.3768+03				
1-S,C	-.2020+04	.8710+03	-.1292+04	+.3925+03	-.5538+02
1-S,S	.1947+04	-.1125+04	-.5324+03	.2151+03	.4113+01
	(0.55)R				
0	-.5469+03				
1-S,C	-.2030+04	.1032+04	-.1238+04	+.4314+03	.5609+01
1-S,S	.1777+04	-.9972+03	-.8192+03	.2447+03	-.3464+02
	(0.75)R				
0	-.6409+03				
1-S,C	-.1101+04	.7340+03	-.6548+03	+.3903+03	.4589+02
1-S,S	.7611+03	-.4305+03	-.8413+03	.1689+03	-.1328+02
	(0.85)R				
0	-.3803+03				
1-S,C	-.4664+03	.3629+03	-.2922+03	+.2223+03	.2641+02
1-S,S	.2911+03	-.1709+03	-.4704+03	.8328+02	.1792+01

N,C OR S					
	ADVANCE RATIO, MU = 0.7				
	(0.21)R				
0	-.6718+03				
1-S,C	-.1398+04	-.3159+03	-.1884+04	+.5796+03	-.1122+03
1-S,S	.1292+04	-.1180+04	.6482+03	.6076+03	.4942+03
	(0.35)R				
0	-.9565+03				
1-S,C	-.1984+04	-.2261+03	-.2852+04	+.7754+03	-.1235+03
1-S,S	.1806+04	-.1617+04	.5911+03	.9812+03	.4233+03
	(0.45)R				
0	-.1036+04				
1-S,C	-.2147+04	-.2896+02	-.3260+04	+.7932+03	-.9882+02
1-S,S	.1928+04	-.1693+04	.3202+03	.1177+04	.1880+03
	(0.55)R				
0	-.1004+04				
1-S,C	-.2071+04	.1957+03	-.3324+04	+.7176+03	-.5929+02
1-S,S	.1832+04	-.1574+04	-.2215+02	.1255+04	-.9863+02
	(0.75)R				
0	-.5861+03				
1-S,C	-.1202+04	.3526+03	-.2122+04	-.3658+03	.4089+01
1-S,S	.1034+04	-.8508+03	-.3667+03	.8564+03	-.3564+03
	(0.85)R				
0	-.2783+03				
1-S,C	-.5698+03	.2087+03	-.1039+04	+.1645+03	.8651+01
1-S,S	.4850+03	-.3922+03	-.2354+03	.4281+03	-.2210+03

N,C OR S					
	ADVANCE RATIO, MU = 1.0				
	(0.21)R				
0	-.1469+04				
1-S,C	-.2127+04	-.5944+03	-.2424+04	.3161+03	.3434+03
1-S,S	.1166+04	-.1534+04	.2361+04	.1279+04	.2695+03
	(0.35)R				
0	-.2025+04				
1-S,C	-.2797+04	-.8752+03	-.3678+04	.7993+03	.3354+03
1-S,S	.1431+04	-.1932+04	.3295+04	.2062+04	.6181+02
	(0.45)R				
0	-.2132+04				
1-S,C	-.2813+04	-.9761+03	-.4202+04	.1197+04	.2181+03
1-S,S	.1334+04	-.1856+04	.3509+04	.2464+04	-.2377+03
	(0.55)R				
0	-.1988+04				
1-S,C	-.2488+04	-.9668+03	-.4259+04	.1484+04	.6388+02
1-S,S	.1066+04	-.1546+04	.3313+04	.2601+04	-.5348+03
	(0.75)R				
0	-.1071+04				
1-S,C	-.1197+04	-.5800+03	-.2652+04	.1185+04	-.1119+03
1-S,S	.3870+03	-.6395+03	.1828+04	.1719+04	-.6164+03
	(0.85)R				
0	-.4895+03				
1-S,C	-.5214+03	-.2757+03	-.1276+04	.6110+03	-.7753+02
1-S,S	.1431+03	-.2574+03	.8428+03	.8427+03	-.3409+03

N,C OR S					
	ADVANCE RATIO, MU = 1.4				
	(0.21)R				
0	-.2001+04				
1-S,C	-.3407+04	.1483+03	-.7740+03	.2726+04	.4009+03
1-S,S	.1436+04	-.1455+04	.3928+04	+.1370+02	-.9452+03
	(0.35)R				
0	-.2600+04				
1-S,C	-.4321+04	.1726+03	-.1067+04	.4263+04	.3672+03
1-S,S	.1655+04	-.1486+04	.5335+04	.2544+03	-.1287+04
	(0.45)R				
0	-.2564+04				
1-S,C	-.4186+04	.1511+03	-.1122+04	.4971+04	.2087+03
1-S,S	.1430+04	-.1065+04	.5538+04	.5297+03	-.1340+04
	(0.55)R				
0	-.2247+04				
1-S,C	-.3525+04	.1097+03	-.1042+04	.5107+04	.1469+02
1-S,S	.1015+04	-.4868+03	.5069+04	.7563+03	-.1230+04
	(0.75)R				
0	-.1036+04				
1-S,C	-.1502+04	.2720+02	-.5520+03	.3198+04	-.1724+03
1-S,S	.2230+03	.2474+03	.2609+04	.6665+03	-.6367+03
	(0.85)R				
0	-.4408+03				
1-S,C	-.6140+03	.6833+01	-.2492+03	.1531+04	-.1096+03
1-S,S	.4516+02	.2008+03	.1165+04	.3478+03	-.2849+03

NOTE- DIVIDE LISTED VALUES BY 1000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 4.
COLLECTIVE PITCH TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(A) MP = 0.1
FP = 0.001 (FOR MU ≤ 0.25,0.4,0.5)
FP = 0.000447(1+MU)**2 (FOR MU ≥ 0.7,1.0,1.4)

N,C OR S		ADVANCE RATIO, MU = 0.25				N,C OR S		ADVANCE RATIO, MU = 0.7			
				(0.0)R						(0.0)R	
0	-.1093+03					0	-.9535+03				
1-5,C	.3981+03	-.3545+03	-.9677+02	*.2189+02	.9549+01	1-5,C	.1113+04	-.1140+04	-.4997+03	*.5016+02	-.1824+03
1-5,S	.1345+04	-.1010+03	-.2039+03	*.1003+03	-.6024+02	1-5,S	.5175+04	-.1577+04	.5534+03	.1372+03	-.1032+03
				(0.14)R						(0.14)R	
0	.2022+02					0	.3976+02				
1-5,C	.2233+02	.1406+02	.4482+01	.2201+01	*.3304+01	1-5,C	.9725+02	.5135+02	-.7828-00	.1342+02	.2402+02
1-5,S	.7819+01	-.3757+01	.3118+01	.4116+01	.3681+01	1-5,S	.1528+03	-.2523+02	.8923+01	*.1148+02	.1982+02
				(0.325)R						(0.325)R	
0	.1362+03					0	.3232+03				
1-5,C	.2422+02	.7625+02	.2181+02	.7510+01	-.2928+01	1-5,C	.7864+02	.3074+03	.9051+02	.1310+02	.6284+02
1-5,S	-.1692+03	.8776+01	.3364+02	.1796+02	.1080+02	1-5,S	-.5523+03	.2406+03	-.7963+02	*.3549+02	.3585+02
				(0.55)R						(0.85)R	
0	.3003+03					0	.5084+03				
1-5,C	.5052+02	.1138+03	.3652+02	.9125+01	.9739+01	1-5,C	.1219+03	.4137+03	.2400+03	-.7488+01	-.8024-01
1-5,S	-.2872+03	.1699+02	.5836+02	.2502+02	.1204+02	1-5,S	-.8091+03	.3647+03	-.1704+03	*.5118+01	-.1813+02
				(0.75)R						(0.75)R	
0	.2567+03					0	.3531+03				
1-5,C	.3560+02	.1105+03	.4617+02	.6309+01	.1784+02	1-5,C	.6795+02	.3557+03	.4085+03	.2911+02	-.9473+02
1-5,S	-.2362+03	.2161+01	.6622+02	.3380+02	.2119+02	1-5,S	-.5426+03	.2442+03	-.2362+03	.3709+02	-.6003+02
				(0.85)R						(0.85)R	
0	.1402+03					0	.1709+03				
1-5,C	.1542+02	.7339+02	.3496+02	.3333+01	.1358+02	1-5,C	.2354+02	.2187+03	*.3223+03	.3661+02	-.8761+02
1-5,S	-.1321+03	-.5704+01	.4712+02	.2705+02	.1902+02	1-5,S	-.2591+03	.1149+03	*.1754+03	.3493+02	-.4710+02

N,C OR S		ADVANCE RATIO, MU = 0.4				N,C OR S		ADVANCE RATIO, MU = 1.0			
				(0.0)R						(0.0)R	
0	-.1805+03					0	-.1050+04				
1-5,C	.7071+03	-.8945+03	-.2168+02	.5100+01	.2150+02	1-5,C	.1253+04	-.1383+04	-.5578+03	-.1246+03	-.9385+02
1-5,S	.2229+04	-.7914+03	-.3106-03	*.8351+02	-.6435+02	1-5,S	.8671+04	-.2837+04	.1735+04	.3641+03	.2730+03
				(0.14)R						(0.14)R	
0	.3771+02					0	.7959+02				
1-5,C	.4104+02	.3040+02	.1415+01	.2595+01	-.4530+01	1-5,C	.1964+03	.6787+02	-.2818+02	.3376+02	.1369+02
1-5,S	.1438+02	-.1125+02	-.5087+01	.1154+01	.2992+01	1-5,S	.5131+03	-.8382+02	.6492+02	*.1523+02	-.1303+02
				(0.325)R						(0.325)R	
0	.1873+03					0	.4902+03				
1-5,C	.4192+02	.1740+03	.5806+01	.8409-00	-.7457+01	1-5,C	.1928+03	.4710+03	.1198+03	.5810+02	.3692+02
1-5,S	-.2767+03	.8208+02	.1476+02	.7132+01	.6106+01	1-5,S	-.9238+03	.5377+03	-.3023+03	*.9647+02	-.9916+02
				(0.55)R						(0.55)R	
0	.3658+03					0	.6513+03				
1-5,C	.8202+02	.2501+03	.2367+02	-.1055+02	-.2394+01	1-5,C	.2212+03	.6017+03	.4122+03	-.2298+02	.1225+02
1-5,S	-.4690+03	.1429+03	-.2615+02	.3285+01	-.2918+01	1-5,S	-.1217+04	.7173+03	-.5670+03	*.4317+02	-.2506+02
				(0.75)R						(0.75)R	
0	.3015+03					0	.4066+03				
1-5,C	.5803+02	.2404+03	.5625+02	*.1832+02	-.5376+01	1-5,C	.7755+02	.5128+03	.6445+03	-.5453+02	-.5797+01
1-5,S	-.3813+03	.1154+03	-.2800+02	.5378+01	.1052+01	1-5,S	-.7024+03	.4172+03	-.6380+03	.4408+02	.1787+03
				(0.85)R						(0.85)R	
0	.1629+03					0	.1900+03				
1-5,C	.2568+02	.1600+03	.5033+02	*.1411+02	-.6262+01	1-5,C	.8890+01	.3111+03	.4679+03	-.3473+02	-.5437+01
1-5,S	-.2109+03	.6285+02	-.1918+01	.5658+01	.4256+01	1-5,S	-.3037+03	.1801+03	-.4230+03	.4688+02	.1693+03

N,C OR S		ADVANCE RATIO, MU = 0.5				N,C OR S		ADVANCE RATIO, MU = 1.4			
				(0.0)R						(0.0)R	
0	-.4754+03					0	.6805+03				
1-5,C	.5501+03	-.9466+03	-.1095+03	.1208+03	-.1649+02	1-5,C	.4521+04	-.1016+04	.7109+03	-.3457+03	.5849+03
1-5,S	.3187+04	-.1316+04	-.2553+02	.4096+02	-.1233+03	1-5,S	.1594+05	-.5236+04	.3899+04	.4380+03	-.7705+02
				(0.14)R						(0.14)R	
0	.8170+02					0	.4196+03				
1-5,C	.4774+02	.4889+02	-.3466+01	*.9792+01	.2975+01	1-5,C	.8712+03	.1967+03	-.2101+02	.3673+02	-.1009+03
1-5,S	-.1796+02	.9320-00	.1144+01	*.1333+02	.1212+02	1-5,S	.1672+04	-.2625+03	.2742+03	-.2892+02	.3400+02
				(0.325)R						(0.325)R	
0	.2543+03					0	.7359+03				
1-5,C	.5592+02	.2149+03	.1945+02	-.3061+02	.4597+01	1-5,C	.4782+03	.6992+03	-.1464+03	.1074+03	-.3115+03
1-5,S	-.3876+03	.1481+03	-.2819+01	*.2795+02	.2802+02	1-5,S	-.1526+04	.1215+04	-.7904+03	*.1610+03	.3890+02
				(0.55)R						(0.55)R	
0	.3683+03					0	.7496+03				
1-5,C	.7881+02	.2725+03	.8449+02	-.1956+02	-.9618+01	1-5,C	.3826+03	.8484+03	.2647+03	-.5023+02	.1509+03
1-5,S	-.5217+03	.2123+03	-.3427+02	-.6744+01	-.1480+02	1-5,S	-.1891+04	.1432+04	-.1284+04	-.1848+02	-.7855+02
				(0.75)R						(0.75)R	
0	.3580+03					0	.3528+03				
1-5,C	.7366+02	.2193+03	.1488+03	.1026+02	-.2860+02	1-5,C	.1287+03	.8298+03	.5956+03	-.1154+03	.7033+03
1-5,S	-.4618+03	.2044+03	-.6901+02	.3335+02	-.7987+02	1-5,S	-.9225+03	.6905+03	-.1092+04	.1586+03	-.1071+03
				(0.85)R						(0.85)R	
0	.2396+03					0	.1364+03				
1-5,C	.4839+02	.1321+03	.1211+03	.1630+02	-.2534+02	1-5,C	.3091+02	.5288+03	.4259+03	*.7368+02	.5444+03
1-5,S	-.2944+03	.1362+03	-.5769+02	.3518+02	-.7456+02	1-5,S	-.3530+03	.2603+03	-.6242+03	.1307+03	-.6428+02

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 4.
COLLECTIVE PITCH TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(B) MP = 0.1
FP = 0.0025 (FOR MU = 0.25,0.4,0.5)
FP = 0.00112(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S	ADVANCE RATIO, MU = 0.25				
			(0.0)R		
0	-.1222+03				
1-S,C	.3265+03	-.1985+03	-.1371+03	*.1907+02	-.1214+02
1-S,S	.9010+03	-.7576+02	-.1409+03	*.6853+02	-.4986+02
			(0.14)R		
0	.3784+02				
1-S,C	.5573+02	-.3904+01	-.6289+01	*.4941-00	-.4512-00
1-S,S	.6368+02	-.7416+01	-.8640+01	-.3371+01	-.4146-00
			(0.325)R		
0	.1507+03				
1-S,C	.2549+02	.6099+02	.3613+02	.6340+01	.3689+01
1-S,S	-.1605+02	.7134+01	.3082+02	.1635+02	.1417+02
			(0.55)R		
0	.2524+03				
1-S,C	.3376+02	.9032+02	.6354+02	.1181+02	.7026+01
1-S,S	-.2442+03	.7883+01	.5374+02	.2576+02	.1295+02
			(0.75)R		
0	.2410+03				
1-S,C	.2981+02	.7607+02	.6162+02	.1198+02	.7213+01
1-S,S	-.2068+03	.3813+01	.5153+02	.2281+02	.4201+01
			(0.85)R		
0	.1456+03				
1-S,C	.1757+02	.4384+02	.3740+02	.7379+01	.4459+01
1-S,S	-.1194+03	.1531+01	.3115+02	.1340+02	.8608-00

N,C OR S	ADVANCE RATIO, MU = 0.4				
			(0.0)R		
0	-.1672+03				
1-S,C	.5208+03	-.5886+03	-.1558+02	.7024+01	-.1368+02
1-S,S	.1499+04	-.4473+03	-.3386+02	*.8289+02	-.5148+02
			(0.14)R		
0	.5111+02				
1-S,C	.9318+02	-.2098+02	-.1643+01	.1047+01	.3050-00
1-S,S	.1066+03	-.4246+02	-.7567+01	.7263+01	-.4858+01
			(0.325)R		
0	.1968+03				
1-S,C	.5111+02	.1557+03	.5863+01	.1946+01	.2482+01
1-S,S	-.2655+03	.5158+02	-.8211+01	.1102+02	.5687+01
			(0.55)R		
0	.3074+03				
1-S,C	.6760+02	.2277+03	.2259+02	.9434+01	-.6387+0.
1-S,S	-.4042+03	.7915+02	-.1471+02	.1654+02	.7745+01
			(0.75)R		
0	.2775+03				
1-S,C	.5808+02	.1884+03	.3060+02	.1338+02	-.1380+02
1-S,S	-.3423+03	.6576+02	-.1519+02	.1357+02	.5585+01
			(0.85)R		
0	.1644+03				
1-S,C	.3386+02	.1078+03	.2033+02	-.8973+01	-.9912+01
1-S,S	-.1 76+03	.3764+02	-.9420+01	.7731+01	.2995+01

N,C OR S	ADVANCE RATIO, MU = 0.5				
			(0.0)R		
0	-.3077+03				
1-S,C	.4099+03	-.6837+03	-.8544+02	.7628+02	-.7484+02
1-S,S	.2043+04	-.7356+03	-.1327+02	*.4461+02	-.1100+02
			(0.14)R		
0	.5025+02				
1-S,C	.8269+02	-.1033+02	-.6604+01	.1321+01	.1023+02
1-S,S	.1471+03	-.6403+02	.5238-00	*.7546+01	-.6801+01
			(0.325)R		
0	.2380+03				
1-S,C	.6239+02	.2062+03	.2471+02	*.2285+02	.3137+02
1-S,S	-.3455+03	.9713+02	-.5301+01	*.1667+01	-.1005+02
			(0.55)R		
0	.3471+03				
1-S,C	.8008+02	.2690+03	.7087+02	-.3063+02	-.2057+02
1-S,S	-.4917+03	.1403+03	-.4292+02	.3115+01	-.3970+01
			(0.75)R		
0	.2934+03				
1-S,C	.6423+02	.1962+03	.8808+02	.2311+02	-.7265+02
1-S,S	-.3871+03	.1105+03	-.6561+02	.6686+01	.5209+01
			(0.85)R		
0	.1694+03				
1-S,C	.3638+02	.1060+03	.57../+02	*.1269+02	-.5474+02
1-S,S	-.2167+03	.6182+02	-.4467+02	.4790+01	.4985+01

N,C OR S	ADVANCE RATIO, MU = 0.7				
			(0.0)R		
0	-.6512+03				
1-S,C	.9602+03	-.8522+03	.2397+02	.8626+02	.4226+02
1-S,S	.3308+04	-.9488+03	.8011+03	.9258+02	.7807+02
			(0.14)R		
0	.1229+02				
1-S,C	.2108+03	-.2851+02	-.7344+01	.4550+0	-.4620+01
1-S,S	.3777+03	-.9551+02	.7678+02	.7810-00	-.7607+01
			(0.325)R		
0	.3100+03				
1-S,C	.1031+03	.2943+03	-.3623+01	*.2612+02	-.1998+02
1-S,S	-.4831+03	.1659+03	-.1905+03	*.3353+02	-.3771+02
			(0.55)R		
0	.4237+03				
1-S,C	.1096+03	.4019+03	.7030+02	*.3710+02	.1799+01
1-S,S	-.6774+03	.2177+03	-.3756+03	*.3309+02	-.7124+01
			(0.75)R		
0	.3164+03				
1-S,C	.7685+02	.2957+03	.1139+03	*.2829+02	.2501+02
1-S,S	-.4796+03	.1448+03	-.3671+03	*.1396+02	.3076+02
			(0.85)R		
0	.1707+03				
1-S,C	.4060+02	.1584+03	.7592+02	*.1539+02	.1906+02
1-S,S	-.2520+03	.7374+02	-.2183+03	*.4998+01	.2508+02

N,C OR S	ADVANCE RATIO, MU = 1.0				
			(0.0)R		
0	-.6351+03				
1-S,C	.1460+04	-.1197+04	.8873+03	.2107+03	.5776+02
1-S,S	.5193+04	-.1548+04	.1546+04	.4972+02	-.7314+02
			(0.14)R		
0	.4710+02				
1-S,C	.4250+03	-.6960+02	.8763+02	.2588+02	-.1447+02
1-S,S	.8223+03	-.2050+03	.2002+03	*.1075+02	.2124+01
			(0.325)R		
0	.4355+03				
1-S,C	.2363+03	.4616+03	-.2409+03	*.6784+02	-.4145+02
1-S,S	-.7410+03	.3002+03	-.4086+03	*.4176+02	.2002+02
			(0.55)R		
0	.5306+03				
1-S,C	.2121+03	.609U...	-.2812+03	*.1463+0?	.1510+02
1-S,S	-.1019+04	.3547+03	-.7754+03	*.2420+02	-.4130+02
			(0.75)R		
0	.3326+03				
1-S,C	.1195+03	.4056+03	-.1520+03	*.1404+03	.6261+02
1-S,S	-.6240+03	.1838+03	-.6860+03	.6175+01	-.8035+02
			(0.85)R		
0	.1634+03				
1-S,C	.5610+02	.2050+03	-.6844+02	*.8107+02	.4399+02
1-S,S	-.3011+03	.8026+02	-.3864+03	.8341+01	5305+02

N,C OR S	ADVANCE RATIO, MU = 1.4				
			(0.0)R		
0	.7674+03				
1-S,C	.5048+04	-.1041+04	.3473+04	.8004+02	-.1893+03
1-S,S	.8507+04	-.2486+04	.1280+04	*.1512+03	-.5706+02
			(0.14)R		
0	.5244+03				
1-S,C	.1636+04	.1833+02	.5355+03	.2539+02	-.3070+02
1-S,S	.1853+04	-.4098+03	.2561+03	*.6518+02	.3845+02
			(0.325)R		
0	.6867+03				
1-S,C	.5666+03	.6743+03	-.9997+03	*.5812+02	.3713+02
1-S,S	-.1012+04	.5710+03	-.2522+03	.1506+02	.4382+02
			(0.55)R		
0	.6432+03				
1-S,C	.2792+03	.7796+03	-.1501+04	*.2561+03	.2316+02
1-S,S	-.1487+04	.6756+03	-.4720+03	.2211+0?	-.1788+03
			(0.75)R		
0	.3081+03				
1-S,C	.8929+02	.4303+03	-.1022+0*	*.2882+03	-.7682+01
1-S,S	-.8001+03	.3235+03	-.3662+0?	.2731+03	*.2654+03
			(0.85)R		
0	.1300+03				
1-S,C	.2824+02	*.966+03	-.5147+03	*.1689+03	-.8728+01
1-S,S	-.3557+03	.1342+03	-.1935+03	.1644+03	-.1686+03

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 4.
COLLECTIVE PITCH TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(C) MP = 0.1
FP = 0.01 (FOR MU = 0.25,0.4,0.5)
FP = 0.00447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S	ADVANCE RATIO, MU = 0.25				
		(0.0)R			
0	-.2467+02				
1-5,C	.2303+03	-.9699+02	-.6418+02	-.1832+02	-.9889+01
1-5,S	.3673+03	-.2624+02	.5846+02	-.8192+02	-.3871+02
		(0.14)R			
0	.4357+02				
1-5,C	.9639+02	-.1556+02	-.1306+02	-.3415+01	-.2020+01
1-5,S	.7966+02	-.1105+02	.1015+02	-.1704+02	-.8163+01
		(0.325)R			
0	.1316+03				
1-5,C	.4544+02	.3990+02	.2222+02	.6459+01	.3049+01
1-5,S	-.1032+03	.6324+01	-.2324+02	.2605+02	.1209+02
		(0.55)R			
0	.1898+03				
1-5,C	.3260+02	.5991+02	.4020+02	.1008+02	.4845+01
1-5,S	-.1695+03	-.7603+01	-.3758+02	.4486+02	.2103+02
		(0.75)R			
0	.1346+03				
1-5,C	.1866+02	.3899+02	.2957+02	.6640+01	.3176+01
1-5,S	-.1126+03	-.6051+01	-.2590+02	.3153+02	.1486+02
		(0.85)R			
0	.6023+02				
1-5,C	.8934+01	.1904+02	.1511+02	.3257+01	.1554+01
1-5,S	-.5634+02	-.3213+01	-.1294+02	.1584+02	.7478+01

N,C OR S	ADVANCE RATIO, MU = 0.4				
		(0.0)R			
0	-.5690+02				
1-5,C	.3753+03	-.2349+03	-.7182+01	.2970+02	-.2070+02
1-5,S	.6179+03	-.1462+03	-.1457+02	.1096+03	-.5449+02
		(0.14)R			
0	.4972+02				
1-5,C	.1553+03	-.4275+02	-.3093+01	-.7368+01	-.6225+01
1-5,S	.1353+03	-.5089+02	.1050+02	-.2648+02	-.1454+02
		(0.325)R			
0	.1692+03				
1-5,C	.6955+02	.8392+02	.2057-00	.5838+01	.1799+01
1-5,S	-.1713+03	-.5819+01	-.1407+02	.2600+02	.1009+02
		(0.55)R			
0	.2341+03				
1-5,C	.4674+02	.1274+03	.5514+01	.9777+01	.4618+01
1-5,S	-.2842+03	.4914+01	-.1805+02	.4854+02	.2159+02
		(0.75)R			
0	.1596+03				
1-5,C	.2536+02	.8205+02	.6236+01	.6128+01	.3247+01
1-5,S	-.1196+03	.2613+01	-.1255+02	.3463+02	.1618+02
		(0.85)R			
0	.7974+02				
1-5,C	.1226+02	.3989+02	.3562+01	.2933+01	.1618+01
1-5,S	-.9351+02	.1009+01	-.6332+01	.1747+02	.8294+01

N,C OR S	ADVANCE RATIO, MU = 0.5				
		(0.0)R			
0	-.1265+03				
1-5,C	.3092+03	-.2926+03	-.9171+01	.3687+02	-.1603+02
1-5,S	.4691+03	-.2250+03	.3403+02	-.1437+03	-.5291+02
		(0.14)R			
0	.3706+02				
1-5,C	.1357+03	-.4233+02	-.2832+01	.3357+01	-.4995+01
1-5,S	.1978+03	-.7528+02	.2731+01	.3481+02	-.1759+02
		(0.325)R			
0	.1917+03				
1-5,C	.7527+02	.1246+03	.4667+01	.2020+02	-.1295-00
1-5,S	-.2185+03	-.2575+01	-.2780+02	.3507+02	.4976+01
		(0.55)R			
0	.2580+03				
1-5,C	.6012+02	.1697+03	.1690+02	-.2658+02	-.9790-00
1-5,S	-.3069+03	.1356+02	-.5639+02	.6773+02	.2327+02
		(0.75)R			
0	.1636+03				
1-5,C	.4059+02	.1009+03	.1681+02	-.1578+02	-.1951+01
1-5,S	-.2234+03	.6672+01	-.4691+02	.4968+02	.2210+02
		(0.85)R			
0	.6263+02				
1-5,C	.1647+02	.4745+02	.9361+01	.7422+01	-.1228+01
1-5,S	-.1031+03	.2616+01	-.2496+02	.2532+02	.1213+02

N,C OR S	ADVANCE RATIO, MU = 0.7				
		(0.0)R			
0	-.2335+03				
1-5,C	.3481+03	-.3670+03	.1647+03	.2906+02	-.5865+02
1-5,S	.1129+04	-.3343+03	-.9271+02	.2481+03	-.7513+02
		(0.14)R			
0	.1667+02				
1-5,C	.1672+03	-.6172+02	.3590+02	.1157+02	-.1678+02
1-5,S	.2056+03	-.1234+03	-.2783+02	.6609+02	-.2643+02
		(0.325)R			
0	.2321+03				
1-5,C	.8866+02	.1575+03	-.5407+02	-.7438-00	.1082+02
1-5,S	-.2015+03	-.6911+01	.4604+01	.6520+02	.6790+01
		(0.55)R			
0	.3003+03				
1-5,C	.5697+02	.2112+03	-.8025+02	.6067+01	.2029+02
1-5,S	-.4470+03	.2193+02	-.5897+01	.1289+03	.2783+02
		(0.75)R			
0	.1803+03				
1-5,C	.2705+02	.1184+03	-.4749+02	.5931+01	.1295+02
1-5,S	-.2653+03	.1047+02	-.1579+02	.9221+02	.2367+02
		(0.85)R			
0	.8506+02				
1-5,C	.1187+02	.5394+02	-.2213+02	.3221+01	.6205+01
1-5,S	-.1235+03	.3971+01	-.1002+02	.4627+02	.1248+02

N,C OR S	ADVANCE RATIO, MU = 1.0				
		(0.0)R			
0	-.3534+03				
1-5,C	.3130+03	-.4531+03	.3094+03	-.2052+03	-.8326+02
1-5,S	.1571+04	-.4728+03	-.2945+03	.2830+03	-.1019-01
		(0.14)R			
0	-.9247+01				
1-5,C	.1715+03	-.8609+02	.7896+02	-.5666+02	-.2444+02
1-5,S	.4535+03	-.1840+03	-.7868+02	.8408+02	-.1030+02
		(0.325)R			
0	.2916+03				
1-5,C	.9648+02	.1976+03	-.9712+02	.6534+02	.2051+02
1-5,S	-.3655+03	.5524+01	.7886+02	.7919+02	-.2281+02
		(0.55)R			
0	.3650+03				
1-5,C	.5006+02	.2561+03	-.1486+03	.1245+03	.3709+02
1-5,S	-.5635+03	.5965+02	.1123+03	.1646+03	-.2574+02
		(0.75)R			
0	.2015+03				
1-5,C	.1612+02	.1319+03	-.8477+02	.8514+02	.2315+02
1-5,S	-.3182+03	.3151+02	.5628+02	.1165+03	-.1450+02
		(0.85)R			
120	.9115+02				
1-5,C	.5516+01	.5739+02	-.3863+02	.4178+02	.1095+02
1-5,S	-.1014+03	.1326+02	.2396+02	.5778+02	-.6665+01

N,C OR S	ADVANCE RATIO, MU = 1.4				
		(0.0)R			
0	-.4044+03				
1-5,C	.4566+03	-.6166+03	.3063+03	-.4103+03	.1631+01
1-5,S	.2273+04	-.4858+03	-.3277+03	.2333+03	.1647+03
		(0.14)R			
0	-.9493+01				
1-5,C	.2484+03	-.1279+03	.9265+02	-.1163+03	-.5793-00
1-5,S	.7636+03	-.1847+03	-.6875+02	.5750+02	.4015+02
		(0.325)R			
0	.3471+03				
1-5,C	.2112+03	.2833+03	-.7412+02	.1492+03	-.6561+01
1-5,S	-.4236+03	.4366+02	.1450+03	.9006+02	-.7428+02
		(0.55)R			
0	.4043+03				
1-5,C	.1331+03	.3724+03	-.1038+03	.2705+03	-.1626+02
1-5,S	-.7430+03	.1021+03	.1829+03	-.1282+03	-.1249+03
		(0.75)R			
0	.2045+03				
1-5,C	.5291+02	.1889+03	-.4510+02	.1749+03	-.1379+02
1-5,S	-.3831+03	.4800+02	.8717+02	.6796+02	-.7938+02
		(0.85)R			
0	.8045+02				
1-5,C	.2093+02	.8133+02	-.1749+02	.8364+02	-.7202+01
1-5,S	-.1642+03	.1919+02	.3626+02	-.2986+02	-.3778+02

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 4.
COLLECTIVE PITCH TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(D) MP = 0.3
FP = 0.001 (FOR MU = 0.25,0.4,0.5)
FP = 0.000447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S	ADVANCE RATIO, MU = 0.25				
			(0.0)R		
0	-.1944+03				
1-5,C	.4331+03	-.3671+03	-.1343+03	+.2285+02	-.5740+01
1-5,S	.5223+04	-.1216+04	.1331+03	.3700+01	.5735+01
			(0.14)R		
0	.7354+02				
1-5,C	.3750+02	.4199+02	.8510-00	.4259+01	.1609+01
1-5,S	.8309+02	.2707+01	-.9149+01	.1009+01	-.5018-00
			(0.325)R		
0	.4360+03				
1-5,C	.1015+03	.9542+02	.2173+02	.5212+01	.2169+01
1-5,S	-.4760+03	.1771+03	-.3101+02	.1074+01	-.8816-00
			(0.55)R		
0	.9414+03				
1-5,C	.2156+03	.5510+02	.5796+02	+.6359-00	-.1718+01
1-5,S	-.7824+03	.2829+03	-.1774+02	-.3272+01	-.2936-01
			(0.75)R		
0	.7747+03				
1-5,C	.1589+03	.4418+02	.9722+02	.8897+01	-.3697+01
1-5,S	-.6167+03	.2103+03	.1932+02	-.1012+02	-.7863-00
			(0.85)R		
0	.4077+03				
1-5,C	.7305+02	.3804+02	.7947+02	.1150+02	-.2646+01
1-5,S	-.3330+03	.1073+03	.2529+02	+.9168+01	-.1059+01

N,C OR S	ADVANCE RATIO, MU = 0.4				
			(0.0)R		
0	-.2305+03				
1-5,C	.1699+04	-.5710+03	-.5321+03	-.1851+03	-.1351+03
1-5,S	.9507+04	-.3515+04	.5367+03	+.2645+02	.6429+01
			(0.14)R		
0	.1427+03				
1-5,C	.1284+03	.1063+03	.4435+01	.3279+02	.2100+02
1-5,S	.1718+03	.3768+01	-.3008+02	.9504+01	-.8831-00
			(0.325)R		
0	.6075+03				
1-5,C	.2155+03	.2162+03	.9071+02	.4799+02	.4515+02
1-5,S	-.7748+03	.4934+03	-.1190+03	.2002+02	.1346+01
			(0.55)R		
0	.1140+04				
1-5,C	.3993+03	.1437+03	.2483+03	-.1280+01	-.3008+01
1-5,S	-.1245+04	.7764+03	-.8893+02	-.1117+02	.4994+01
			(0.75)R		
0	.6724+03				
1-5,C	.2702+03	.1539+03	.4224+03	.3154+02	-.7530+02
1-5,S	-.9908+03	.5656+03	.4201+02	-.7550+02	-.3288+01
			(0.85)R		
0	.4374+03				
1-5,C	.1145+03	.1353+03	.3465+03	+.4675+02	-.7261+02
1-5,S	-.5440+03	.2833+03	.7339+02	+.7357+02	-.6343+01

N,C OR S	ADVANCE RATIO, MU = 0.5				
			(0.0)R		
0	-.3796+03				
1-5,C	.2219+04	.1739+03	-.9115+03	+.3077+03	-.2515+03
1-5,S	.1306+05	-.5391+04	.4944+03	.6790+02	-.1603+03
			(0.14)R		
0	.1900+03				
1-5,C	.1926+03	.1559+03	.9801+01	.7071+02	.3548+02
1-5,S	.2329+03	.1826+02	-.2641+02	.7984+01	.3071+02
			(0.325)R		
0	.7468+03				
1-5,C	.3226+03	.2263+03	.1529+03	.8396+02	.8730+02
1-5,S	-.1022+04	.7622+03	-.1000+03	+.1093+01	.5579+02
			(0.55)R		
0	.1280+04				
1-5,C	.5185+03	.8513+02	.4531+03	+.3491+02	.6584+01
1-5,S	-.1500+04	.1121+04	-.4901+02	+.2605+02	-.1511+02
			(0.75)R		
0	.8522+03				
1-5,C	.2866+03	.4025+02	.8458+03	.6079+02	-.1544+03
1-5,S	-.1010+04	.7202+03	.8938+02	+.3225+02	-.9057+02
			(0.85)R		
0	.3631+03				
1-5,C	.8611+02	.4500+02	.7136+03	.1074+03	-.1577+03
1-5,S	-.4692+03	.3121+03	.1071+03	+.2096+02	-.8020+02

N,C OR S	ADVANCE RATIO, MU = 0.7				
			(0.0)R		
0	.3426+03				
1-5,C	.4245+04	.1565+04	-.7511+03	-.6961+03	-.5470+03
1-5,S	.2001+05	-.8876+04	.1784+04	.1799+03	.4845+03
			(0.14)R		
0	.3765+03				
1-5,C	.5100+03	.2919+03	-.3338+02	.1631+03	.6676+02
1-5,S	.6991+03	-.6737+02	-.2412+02	.2546+02	-.2862+02
			(0.325)R		
0	.1033+04				
1-5,C	.5957+03	.2231+03	.1498+03	.2700+03	.2201+03
1-5,S	-.1607+04	.1393+04	-.3343+03	.1132+02	-.1608+03
			(0.55)R		
0	.1453+04				
1-5,C	.6999+03	.7035+02	.7635+03	+.6716+02	.3912+02
1-5,S	-.1995+04	.1800+04	-.3644+03	+.7762+02	-.2555+02
			(0.75)R		
0	.8186+03				
1-5,C	.2566+03	.3247+03	.1453+04	-.1873+03	-.3971+03
1-5,S	-.1106+04	.9875+03	-.1728+03	-.1882+03	.4098+03
			(0.85)R		
0	.3085+03				
1-5,C	.2197+02	.3443+03	.1160+04	-.1128+03	-.3951+03
1-5,S	-.4413+03	.3760+03	-.5727+02	+.1555+03	.4123+03

N,C OR S	ADVANCE RATIO, MU = 1.0				
			(0.0)R		
0	.5309+04				
1-5,C	.8671+04	.5710+04	.1551+04	-.1020+04	.9788+03
1-5,S	.3564+05	-.1442+05	.5073+04	.5613+03	.2389+04
			(0.14)R		
0	.1184+04				
1-5,C	.1435+04	.8180+03	-.1915+02	.3145+03	-.1672+03
1-5,S	.2342+04	-.2163+03	.5319+02	.5251+02	-.1690+03
			(0.325)R		
0	.1489+04				
1-5,C	.1109+04	.1627+02	-.1603+03	.4937+03	-.3791+03
1-5,S	-.2761+04	.2829+04	-.1007+04	-.1368+03	-.8895+03
			(0.55)R		
0	.1430+04				
1-5,C	.6623+03	-.4696+03	.7102+03	-.2099+03	.2731+03
1-5,S	-.2950+04	.2945+04	-.9379+03	+.1507+03	-.6556+02
			(0.75)R		
0	.5065+03				
1-5,C	-.9057+02	.3746+03	.1554+04	-.3458+03	.9215+03
1-5,S	-.1261+04	.1171+04	-.2442+03	.2863+03	.1717+04
			(0.85)R		
0	.9867+02				
1-5,C	-.2119+03	.5605+03	.1182+04	+.1751+03	.7225+03
1-5,S	-.3903+03	.3046+03	.1207+02	.3209+03	.1562+04

N,C OR S	ADVANCE RATIO, MU = 1.4				
			(0.0)R		
0	.2359+05				
1-5,C	.2707+05	.1194+05	.1191+05	+.3286+04	.5199+04
1-5,S	.6295+05	-.2356+05	.3019+04	+.8222+03	.2539+03
			(0.14)R		
0	.4413+04				
1-5,C	.4592+04	.2536+04	.9201+03	.5935+03	-.7777+03
1-5,S	.6816+04	-.6969+03	.2519+03	+.8631-00	.6090+03
			(0.325)R		
0	.1819+04				
1-5,C	.4282+03	.5156+03	-.1522+04	.1283+04	-.2314+04
1-5,S	-.4564+04	.5866+04	-.3497+03	+.4785+02	.3462+03
			(0.55)R		
0	.5257+03				
1-5,C	-.1682+04	-.8234+03	-.1020+04	.1328+03	.9328+03
1-5,S	-.4104+04	.5697+04	.9150+03	.1252+04	-.8214+03
			(0.75)R		
0	-.5803+03				
1-5,C	-.1439+04	.5775+03	.8207+02	.5519+03	.3961+04
1-5,S	-.9199+03	.2289+04	.2738+04	.3802+04	-.2742+03
			(0.85)R		
0	-.5245+03				
1-5,C	-.6810+03	.8576+03	.2493+03	.5993+03	.2971+04
1-5,S	.3930+02	.7421+03	.2101+04	.2979+04	.8177+02

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 4.
COLLECTIVE PITCH TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(E) MP = 0.3
FP = 0.0025 (FOR MU = 0.25,0.4,0.5)
FP = 0.00112(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S	ADVANCE RATIO, MU = 0.25			
	(0.0)R			
0 -.2087+03				
1-5,C .3869+03	-.3852+03	-.2226+03	.2963+02	.5402+01
1-5,S .3473+04	-.6728+03	.7182+01	.9466+02	-.6698+02
	(0.14)R			
0 .1393+03				
1-5,C .1078+03	.7865+01	-.6217+01	.3422+01	.5127+01
1-5,S .3133+03	-.3899+02	.8971-00	.1224+01	.2508+01
	(0.325)R			
0 .4579+03				
1-5,C .1409+03	.1503+03	.7593+02	.2612+02	.1260+02
1-5,S -.4441+03	.1369+03	.6219+01	.3684+02	.2903+02
	(0.55)R			
0 .7525+03				
1-5,C .2139+03	.1986+03	.1502+03	.4343+02	.2272+02
1-5,S -.6832+03	.1920+03	.2913+02	.5394+02	.3864+02
	(0.75)R			
0 .7103+03				
1-5,C .1942+03	.1484+03	.1581+03	.4114+02	.2304+02
1-5,S -.5734+03	.1502+03	.4139+02	.4521+02	.2926+02
	(0.85)R			
0 .4274+03				
1-5,C .1153+03	.8121+02	.9846+02	.2479+02	.1420+02
1-5,S -.3297+03	.8388+02	.2778+02	.2601+02	.1610+02

N,C OR S	ADVANCE RATIO, MU = 0.4			
	(0.0)R			
0 -.3763+03				
1-5,C .1214+04	-.6449+03	-.2801+03	.4206+02	-.1825+02
1-5,S .6265+04	-.2174+04	.5849+03	.7266+02	.9515+02
	(0.14)R			
0 .1924+03				
1-5,C .2577+03	.1409+02	-.2988+02	.3633+01	.2344+01
1-5,S .6003+03	-.1454+03	.1726+02	.5881+01	-.9209+01
	(0.325)R			
0 .6355+03				
1-5,C .2213+03	.2446+03	.6463+02	.1984+02	.9268+01
1-5,S -.7079+03	.3960+03	-.1539+03	.1531+02	-.3779+02
	(0.55)R			
0 .9562+03				
1-5,C .3022+03	.2929+03	.2230+03	.1529+02	.3563+01
1-5,S -.1087+04	.5631+03	-.1942+03	.3641+02	.5580+01
	(0.75)R			
0 .8373+03				
1-5,C .2555+03	.1909+03	.2927+03	.1437+01	-.5297+01
1-5,S -.9023+03	.4448+03	-.1347+03	-.4180+02	.5546+02
	(0.85)R			
0 .4903+03				
1-5,C .1478+03	.9705+02	.1931+03	-.1829+01	-.4982+01
1-5,S -.5163+03	.2493+03	-.7087+02	-.2668+02	.4377+02

N,C OR S	ADVANCE RATIO, MU = 0.5			
	(0.0)R			
0 -.5483+03				
1-5,C .1578+04	-.3998+03	-.6519+03	-.9354+01	-.1741+03
1-5,S .8588+04	-.3515+04	.7745+03	.2050+03	.2313+03
	(0.14)R			
0 .2320+03				
1-5,C .3569+03	.7987+02	-.6402+02	.6855+01	.2030+02
1-5,S .8260+03	-.2310+03	.3530+02	.2820+01	-.2208+02
	(0.325)R			
0 .7705+03				
1-5,C .3307+03	.3057+03	.1546+03	.1814+02	.7740+02
1-5,S -.9236+03	.6327+03	-.1859+03	.5701+02	-.9181+02
	(0.55)R			
0 .1069+04				
1-5,C .4151+03	.3198+03	.4943+03	.1802+02	.8905-01
1-5,S -.1302+04	.8444+03	-.2745+03	-.5637+02	.1127+02
	(0.75)R			
0 .8624+03				
1-5,C .3180+03	.1659+03	.6348+03	.8408+01	-.9410+02
1-5,S -.9776+03	.6178+03	-.2285+03	-.2398+02	.1309+03
	(0.85)R			
0 .4887+03				
1-5,C .1764+03	.7164+02	.4167+03	.3279+01	-.7613+02
1-5,S -.5350+03	.3341+03	-.1310+03	-.8348+01	.1037+03

N,C OR S	ADVANCE RATIO, MU = 0.7			
	(0.0)R			
0 -.1249+03				
1-5,C .3182+04	.1527+03	-.1667+03	.2090+03	.3159+03
1-5,S .1271+05	-.5679+04	.1960+04	.5029+03	.4595+03
	(0.14)R			
0 .4037+03				
1-5,C .8250+03	.1913+03	-.6754+02	.4916+02	-.3451+02
1-5,S .1648+04	-.5110+03	.1675+03	.2641+02	-.2383+02
	(0.325)R			
0 .1013+04				
1-5,C .6174+03	.4008+03	.6667+02	.1387+01	-.1352+03
1-5,S -.1325+04	.1102+04	-.4763+03	.1457+03	-.1798+03
	(0.55)R			
0 .1244+04				
1-5,C .6202+03	.5163+03	.5840+03	-.9312+02	.7554+02
1-5,S -.1758+04	.1325+04	-.8106+03	-.1864+03	-.1489+02
	(0.75)R			
0 .8489+03				
1-5,C .3595+03	.3772+03	.8361+03	.1430+03	.2685+03
1-5,S -.1095+04	.7835+03	-.7182+03	.1254+03	.1780+03
	(0.85)R			
0 .4397+03				
1-5,C .1707+03	.2018+03	.5452+03	-.9441+02	.1948+03
1-5,S -.5371+03	.3734+03	-.4137+03	-.6437+02	.1405+03

N,C OR S	ADVANCE RATIO, MU = 1.0			
	(0.0)R			
0 .3370+04				
1-5,C .7320+04	.2857+04	.2112+04	.7882+03	.8046+03
1-5,S .2224+05	-.9297+04	.3520+04	.3836+03	-.5453+02
	(0.14)R			
0 .1403+04				
1-5,C .2157+04	.8063+03	.2266+03	.1643+03	-.9576+02
1-5,S .3999+04	-.1069+04	.4172+03	-.5786+01	.1009+03
	(0.325)R			
0 .1447+04				
1-5,C .1169+04	.4226+03	-.3629+03	-.1041+03	-.4124+03
1-5,S -.1909+04	.2106+04	-.8566+03	-.1435+03	.1332+03
	(0.55)R			
0 .1299+04				
1-5,C .8188+03	.4265+03	.8123+02	-.3951+03	.1593+03
1-5,S -.2607+04	.2257+04	-.1188+04	.1901+02	-.2311+03
	(0.75)R			
0 .5838+03				
1-5,C .2615+03	.2860+03	.5175+03	-.4484+03	.6422+03
1-5,S -.1308+04	.9984+03	-.8021+03	.1738+03	-.4603+03
	(0.85)R			
0 .2316+03				
1-5,C .6964+02	.1481+03	.3711+03	-.2700+03	.4505+03
1-5,S -.5530+03	.3844+03	-.4073+03	.1258+03	-.3046+03

N,C OR S	ADVANCE RATIO, MU = 1.4			
	(0.0)R			
0 .1595+05				
1-5,C .1937+05	.8926+04	.7995+04	-.1240+04	-.4229+02
1-5,S .4114+05	-.1600+05	.6764+03	-.1077+04	.1157+04
	(0.14)R			
0 .5524+04				
1-5,C .5875+04	.2858+04	.1623+04	-.1488+02	-.1223+03
1-5,S .1006+05	-.2309+04	.7278+02	-.5018+03	.4193+03
	(0.325)R			
0 .2360+04				
1-5,C .1175+04	.9542+03	-.9399+03	.8484+03	-.3637+02
1-5,S -.2369+04	.4355+04	.2143+03	.1915+03	.6930+02
	(0.55)R			
0 .8578+03				
1-5,C -.2725+03	.5302+03	-.5928+03	.1342+04	.5674+03
1-5,S -.3464+04	.4917+04	.1519+04	.2146+04	-.4577+03
	(0.75)R			
0 -.2276+03				
1-5,C -.6047+03	.2462+03	.3062+03	.1023+04	.7820+03
1-5,S -.1207+04	.2268+04	.1862+04	.2647+04	-.6213+03
	(0.85)R			
0 -.2669+03				
1-5,C -.3775+03	.1075+03	.3047+03	.5390+03	.4760+03
1-5,S -.3861+03	.9167+03	.1111+04	.1579+04	-.3764+03

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 4.
COLLECTIVE PITCH TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(F) MP = 0.3
FP = 0.01 (FOR MU = 0.25,0.4,0.5)
FP = 0.00447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S	ADVANCE RATIO, MU = 0.25			
	(0.0)R			
0	-.3603+02			
1-S,C	.3669+03	-.2179+03	-.5968+02	+.6615+02	-.2156+02
1-S,S	.1546+04	-.1563+03	.9300+02	-.8976+02	-.6262+02
	(0.14)R			
0	.1469+03			
1-S,C	.1749+03	-.2303+02	-.6483+01	-.6703+01	.6737-00
1-S,S	.4177+03	-.3687+02	.2212+02	-.1377+02	-.8651+01
	(0.325)R			
0	.4016+03			
1-S,C	.1242+03	.1164+03	.3986+02	.3780+02	.1949+02
1-S,S	-.2395+03	.3365+02	-.2151+02	.4096+02	.3074+02
	(0.55)R			
0	.5706+03			
1-S,C	.1203+03	.1646+03	.7572+02	.5744+02	.2872+02
1-S,S	-.4701+03	.5128+02	-.3712+02	.6669+02	.4905+02
	(0.75)R			
0	.4023+03			
1-S,C	.7548+02	.1047+03	.6039+02	.3912+02	.1974+02
1-S,S	-.3186+03	.2988+02	-.2479+02	.4692+02	.3423+02
	(0.85)R			
0	.2035+03			
1-S,C	.3695+02	.5071+02	.3173+02	.1948+02	.9875+01
1-S,S	-.1574+03	.1364+02	-.1219+02	.2362+02	.1719+02

N,C OR S	ADVANCE RATIO, MU = 0.4			
	(0.0)R			
0	-.1622+03			
1-S,C	.8199+03	-.4487+03	.3145+03	.6520+02	.1315+02
1-S,S	.2656+04	-.5892+03	.1789+03	+.3465+02	.3236+01
	(0.14)R			
0	.1610+03			
1-S,C	.3617+03	-.6053+02	.6155+02	.1612+02	.2097+01
1-S,S	.7343+03	-.1484+03	.3655+02	-.5223+01	.6939-01
	(0.325)R			
0	.5261+03			
1-S,C	.2023+03	.2002+03	-.9569+02	-.1966+02	-.4994+01
1-S,S	-.3723+03	.1114+03	-.6262+02	.1490+02	-.1122+01
	(0.55)R			
0	.7181+03			
1-S,C	.1590+03	.2684+03	-.1336+03	-.4660+02	-.6497+01
1-S,S	-.7567+03	.1907+03	-.1153+03	.2183+02	.1395+01
	(0.75)R			
0	.4849+03			
1-S,C	.8914+02	.1582+03	-.7677+02	-.3926+02	-.3599+01
1-S,S	-.5140+03	.1208+03	-.8594+02	.1398+02	.2709+01
	(0.85)R			
0	.2414+03			
1-S,C	.4197+02	.7405+02	-.3543+02	-.2092+02	-.1633+01
1-S,S	-.2537+03	.5809+02	-.4410+02	.6785+01	.1679+01

N,C OR S	ADVANCE RATIO, MU = 0.5			
	(0.0)R			
0	-.3442+03			
1-S,C	.9983+03	-.5407+03	.4665+03	.2393+03	.2922+02
1-S,S	.3531+04	-.9874+03	.4229+03	+.8450+02	.2693+02
	(0.14)R			
0	.1411+03			
1-S,C	.4589+03	-.4647+02	.8977+02	.4795+02	.6359+01
1-S,S	.9746+03	-.2504+03	.9872+02	+.1607+02	.1131+01
	(0.325)R			
0	.6076+03			
1-S,C	.2845+03	.2886+03	-.1366+03	-.8350+02	-.1051+02
1-S,S	-.4749+03	.1730+03	-.1298+03	.3311+02	-.1255+02
	(0.55)R			
0	.6014+03			
1-S,C	.2280+03	.3452+03	-.1693+03	-.1479+03	-.2217+02
1-S,S	-.9222+03	.2786+03	-.2765+03	.6069+02	-.3539+01
	(0.75)R			
0	.5173+03			
1-S,C	.1228+03	.1824+03	-.8243+02	-.1073+03	-.1791+02
1-S,S	-.5955+03	.1622+03	-.2213+03	.4561+02	.6329+01
	(0.85)R			
0	.2530+03			
1-S,C	.5651+02	.8092+02	-.3468+02	+.5458+02	-.9436+01
1-S,S	-.2877+03	.7496+02	-.1162+03	.2348+02	.4790+01

N,C OR S	ADVANCE RATIO, MU = 0.7				
	(0.0)R				
0	-.4014+03				
1-S,C	.1816+04	-.4950+03	.1197+04	.3409+03	.3895+02
1-S,S	.4573+04	-.1651+04	.1799+03	+.5613+03	-.6882+02
	(0.14)R				
0	.1804+03				
1-S,C	.9074+03	.2096+02	.2856+03	.9063+02	.9549+01
1-S,S	.1401+04	-.4807+03	.6089+02	-.1290+03	-.8885+01
	(0.325)R				
0	.7347+03				
1-S,C	.5339+03	.4351+03	-.3339+03	-.1020+03	-.1380+02
1-S,S	-.5764+03	.2516+03	-.4433+02	.2108+03	.3635+02
	(0.55)R				
0	.8875+03				
1-S,C	.3630+03	.5108+03	-.5065+03	-.2206+03	-.2851+02
1-S,S	-.1134+04	.4256+03	-.1547+03	.4061+03	.4927+02
	(0.75)R				
0	.5164+03				
1-S,C	.1705+03	.2728+03	-.2952+03	-.1697+03	-.2181+02
1-S,S	-.6640+03	.2290+03	-.1414+03	.3004+03	.2892+02
	(0.85)R				
0	.2408+03				
1-S,C	.7303+02	.1218+03	-.1364+03	-.8725+02	-.1120+02
1-S,S	-.3049+03	.1010+03	-.7629+02	.1527+03	.1348+02

N,C OR S	ADVANCE RATIO, MU = 1.0				
	(0.0)R				
0	.2580+03				
1-S,C	.3153+04	-.2421+03	.1896+04	-.5061+03	-.1819+03
1-S,S	.6799+04	-.2907+04	-.4983+03	+.1176+04	.1380+03
	(0.14)R				
0	.5837+03				
1-S,C	.1740+04	.2316+03	.5401+03	-.1007+03	-.3789+02
1-S,S	.2376+04	-.9898+03	-.1238+03	-.3199+03	.5756+02
	(0.325)R				
0	.1013+04				
1-S,C	.1019+04	.6884+03	-.4399+03	.2617+03	.8984+02
1-S,S	-.6725+03	.3233+03	.1731+03	.4315+03	-.1820+02
	(0.55)R				
0	.9830+03				
1-S,C	.6026+03	.7182+03	-.6624+03	.4539+03	.1573+03
1-S,S	-.1517+04	.6366+03	.2804+03	.8881+03	-.9597+02
	(0.75)R				
0	.4800+03				
1-S,C	.2434+03	.3542+03	-.3372+03	.3119+03	.1082+03
1-S,S	-.8191+03	.3133+03	.1724+03	.6499+03	-.8794+02
	(0.85)R				
0	.2062+03				
1-S,C	.9794+02	.1522+03	-.1445+03	.1537+03	.5335+02
1-S,S	-.3578+03	.1300+03	.8126+02	.3265+03	-.4695+02

N,C OR S	ADVANCE RATIO, MU = 1.4				
	(0.0)R				
0	.3315+04				
1-S,C	.5975+04	.6592+03	.2245+04	-.2096+04	.9784+03
1-S,S	.1240+05	-.4327+04	-.8135+03	.1255+04	.2120+04
	(0.14)R				
0	.2318+04				
1-S,C	.3469+04	.9153+03	.8791+03	+.4906+03	.2814+03
1-S,S	.5291+04	-.1527+04	-.1499+03	.3001+03	.6318+03
	(0.325)R				
0	.1793+04				
1-S,C	.1833+04	.1304+04	-.7241+02	.1002+04	-.3277+03
1-S,S	.3277-00	.6273+03	.4298+03	+.5076+03	-.7472+03
	(0.55)R				
0	.1129+04				
1-S,C	.8194+03	.1175+04	-.1570+03	.1681+04	-.5695+03
1-S,S	-.1701+04	.1126+04	.5883+03	+.7223+03	-.1473+04
	(0.75)R				
0	.4038+03				
1-S,C	.2455+03	.5476+03	.4631+02	.1076+04	-.3508+03
1-S,S	-.9094+03	.5200+03	.3218+03	+.3874+03	-.1001+04
	(0.85)R				
0	.1472+03				
1-S,C	.6315+02	.2304+03	.5158+02	.5137+03	-.1646+03
1-S,S	-.3825+03	.2077+03	.1440+03	+.1713+03	-.4872+03

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 4.
COLLECTIVE PITCH TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(G) MP = 0.5
FP = 0.001 (FOR MU = 0.25,0.4,0.5)
FP = 0.000447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S		ADVANCE RATIO, MU = 0.25				
		(0,0)R				
0	.6009+03					
1-S,C	-.3666+02	.1382+03	-.2339+03	+.3539+02	-.1630+02	
1-S,S	.9055+04	-.2151+04	.1796+03	+.2173+02	.4784+01	
		(0,14)R				
0	.1752+03					
1-S,C	.4357+02	.7141+02	-.7332-01	.6488+01	.3195+01	
1-S,S	.1525+03	.2174+02	-.2206+02	.5298+01	-.1242+01	
		(0,325)R				
0	.7579+03					
1-S,C	.2507+03	.3893+02	.4159+02	.6581+01	.5793+01	
1-S,S	-.7636+03	.3275+03	-.5254+02	.8741+01	-.9255-01	
		(0,55)R				
0	.1592+04					
1-S,C	.5162+03	-.1397+03	.9639+02	.1791+01	-.5422-00	
1-S,S	-.1200+04	.4436+03	.6454+01	-.6036+01	.2323+01	
		(0,75)R				
0	.1251+04					
1-S,C	.3488+03	-.1364+03	.1171+03	.3138+02	-.6277+01	
1-S,S	-.9146+03	.2458+03	.1088+03	-.2282+02	-.4593+01	
		(0,85)R				
0	.6276+03					
1-S,C	.1409+03	-.6148+02	.8335+02	.3557+02	-.5430+01	
1-S,S	-.4089+03	.8524+02	.1065+03	-.2007+02	-.6544+01	

N,C OR S		ADVANCE RATIO, MU = 0.4				
		(0,0)R				
0	.1531+04					
1-S,C	.1489+04	.9644+03	-.7744+03	-.2406+03	-.2379+03	
1-S,S	.1694+05	-.6142+04	.6774+03	-.2680+03	.2516+02	
		(0,14)R				
0	.3627+03					
1-S,C	.1941+03	.1803+03	-.6077+01	.5118+02	.3565+02	
1-S,S	.3248+03	.5143+02	-.7272+02	.4455+02	-.1262+02	
		(0,325)R				
0	.1078+04					
1-S,C	.4034+03	.6255+02	.1360+03	.5302+02	.7701+02	
1-S,S	-.1224+04	.8961+03	-.1968+03	.8925+02	-.2275+01	
		(0,55)R				
0	.1424+04					
1-S,C	.6234+03	-.3158+03	.3718+03	-.1763+02	-.6229+01	
1-S,S	-.1435+04	.1208+04	-.2669+02	-.3457+02	.2054+02	
		(0,75)R				
0	.1337+04					
1-S,C	.4511+03	-.2308+03	.5136+03	.1260+03	-.1305+03	
1-S,S	-.1394+04	.6833+03	.3309+03	-.2122+03	-.3837+02	
		(0,85)R				
0	.5906+03					
1-S,C	.1283+03	-.5767+02	.3856+03	.1634+03	-.1255+03	
1-S,S	-.7457+03	.2469+03	.3431+03	-.1976+03	-.5568+02	

N,C OR S		ADVANCE RATIO, MU = 0.5				
		(0,0)R				
0	.1869+04					
1-S,C	.2362+03	.4017+04	-.9760+03	-.1890+03	-.5338+03	
1-S,S	.2486+05	-.9651+04	.3464+03	-.4087+03	-.8502+02	
		(0,14)R				
0	.7023+03					
1-S,C	.4266+03	.1369+03	-.2661+02	.2641+02	.7896+02	
1-S,S	.3923+03	.1919+03	-.8134+02	.6496+02	.1264+02	
		(0,325)R				
0	.1468+04					
1-S,C	.7418+03	-.1772+03	.1558+03	.7645+02	.1790+03	
1-S,S	-.1684+04	.1409+04	-.1410+03	.1396+03	.2852+02	
		(0,55)R				
0	.1881+04					
1-S,C	.8999+03	-.4995+03	.6269+03	.7629+02	-.7672+01	
1-S,S	-.1908+04	.1561+04	.1417+03	-.3297+02	-.1809+01	
		(0,75)R				
0	.1549+04					
1-S,C	.6663+03	-.7749+03	.1084+04	.3346+02	-.3232+03	
1-S,S	-.1473+04	.9545+03	.5480+03	-.3101+03	-.5273+02	
		(0,85)R				
0	.9872+03					
1-S,C	.3791+03	-.6117+03	.8789+03	.9290+01	-.3180+03	
1-S,S	-.8382+03	.4572+03	.4990+03	-.2971+03	-.5172+02	

N,C OR S		ADVANCE RATIO, MU = 0.7				
		(0,0)R				
0	.4199+04					
1-S,C	.5791+04	.5829+04	.1025+03	+.9641+03	-.6041+03	
1-S,S	.3494+05	-.1508+05	.2535+04	+.1077+04	.1049+04	
		(0,14)R				
0	.9361+03					
1-S,C	.9314+03	.4934+03	-.1121+03	.2882+03	.4661+02	
1-S,S	.1201+04	.3991+02	-.1476+03	.1772+03	-.1039+03	
		(0,325)R				
0	.1753+04					
1-S,C	.1195+04	-.2246+03	-.2994+01	.4132+03	.2983+03	
1-S,S	-.2572+04	.2451+04	-.5912+03	.3911+03	-.3582+03	
		(0,55)R				
0	.2189+04					
1-S,C	.9744+03	-.7120+03	.8704+03	-.2194+03	.1224+03	
1-S,S	-.2713+04	.2585+04	-.3162+03	+.1358+03	-.1675+02	
		(0,75)R				
0	.1022+04					
1-S,C	-.4352+02	.7673+02	.1629+04	-.3808+03	-.7420+03	
1-S,S	-.1227+04	.9882+03	.1510+03	-.7995+03	.7380+03	
		(0,85)R				
0	.2792+03					
1-S,C	-.3223+03	.3988+03	.1262+04	-.2122+03	-.7837+03	
1-S,S	-.3826+03	.1725+03	.2113+03	-.6964+03	.7152+03	

N,C OR S		ADVANCE RATIO, MU = 1.0				
		(0,0)R				
0	.1358+05					
1-S,C	.1277+05	.1156+05	.4959+04	-.2046+04	.2173+04	
1-S,S	.5789+05	-.2326+05	.6515+04	-.1713+04	.3714+04	
		(0,14)R				
0	.2497+04					
1-S,C	.2405+04	.1377+04	.6042+02	.6519+03	-.3616+03	
1-S,S	.3580+04	.4689+02	-.2139+03	.2273+03	-.2479+03	
		(0,325)R				
0	.2213+04					
1-S,C	.1073+04	-.5203+03	-.5817+03	.9203+03	-.8023+03	
1-S,S	-.4514+04	.4832+04	-.1506+04	.3610+03	-.1410+04	
		(0,55)R				
0	.1474+04					
1-S,C	-.5039+02	-.1611+04	.2558+03	-.5037+03	.5533+03	
1-S,S	-.4031+04	.3889+04	-.5190+03	-.6373+01	-.1929+03	
		(0,75)R				
0	.2063+03					
1-S,C	-.1167+04	.1780+02	.8359+03	-.4137+03	.1768+04	
1-S,S	-.1381+04	.8619+03	.7137+03	.7414+03	.2666+04	
		(0,85)R				
0	-.1106+03					
1-S,C	-.2186+03	.6156+03	.6158+03	-.5527+02	.1363+04	
1-S,S	-.3127+03	-.1009+03	.6910+03	.7733+03	.2459+04	

N,C OR S		ADVANCE RATIO, MU = 1.4				
		(0,0)R				
0	.4208+05					
1-S,C	.4582+05	.1654+05	.2319+05	-.9650+04	.1169+05	
1-S,S	.9409+05	-.3725+05	-.2261+04	-.3628+04	.6818+03	
		(0,14)R				
0	.7812+04					
1-S,C	.7101+04	.3975+04	.1895+04	.1599+04	-.1318+04	
1-S,S	.9939+04	-.5654+03	-.3468+03	-.4726+03	.1279+04	
		(0,325)R				
0	.1957+04					
1-S,C	-.1463+04	.1170+04	-.2698+04	.3513+04	-.4966+04	
1-S,S	-.7578+04	.9622+04	.7099+03	-.7430+02	.4302+03	
		(0,55)R				
0	-.3465+03					
1-S,C	-.6022+04	-.1848+04	-.2618+04	.4845+03	.1818+04	
1-S,S	-.5259+04	.8564+04	.3615+04	.3131+04	-.2029+04	
		(0,75)R				
0	-.1007+04					
1-S,C	-.3906+04	-.3044+03	-.1925+04	.2166+04	.9594+04	
1-S,S	-.3351+03	.3551+04	.5274+04	.7922+04	-.1101+03	
		(0,85)R				
0	-.6079+03					
1-S,C	-.1602+04	.4944+03	-.1140+04	.2189+04	.7427+04	
1-S,S	.6007+03	.1376+04	.3559+04	.6028+04	.6645+03	

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 4.
COLLECTIVE PITCH TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(II) MP = 0.5
FP = 0.0025 (FOR MU = 0.25,0.4,0.5)
FP = 0.00112(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S	ADVANCE RATIO, MU = 0.25			
	(0.0)R			
0 .6270+02				
1-S,C .9349+02	-.5421+02	-.1583+03	-.1286+02	-.2951+01
1-S,S .6090+04	-.1427+04	.1680+03	.1282+02	.1080+02
	(0.14)R			
0 .3176+03				
1-S,C .1032+03	.2986+02	-.1401+02	-.4308-01	.7260-00
1-S,S .5736+03	-.6157+02	-.4361+01	.2434+01	-.7819-00
	(0.325)R			
0 .6257+03				
1-S,C .2374+03	.6499+02	.3523+02	.4883+01	.2113+01
1-S,S -.7035+03	.2843+03	-.5357+02	-.1422+01	-.3950+01
	(0.55)R			
0 .1312+04				
1-S,C .3660+03	-.2587-00	.9735+02	.8439+01	.6237-00
1-S,S -.1050+04	.3710+03	-.2454+02	-.1166+02	.9514-01
	(0.75)R			
0 .1211+04				
1-S,C .3305+03	-.7851+02	.1190+03	.8144+01	-.1509+01
1-S,S -.8477+03	.2653+03	.2474+02	-.1765+02	.4990+01
	(0.85)R			
0 .7228+03				
1-S,C .1956+03	-.6344+02	.7719+02	.4936+01	-.1342+01
1-S,S -.4794+03	.1418+03	.2482+02	-.1200+02	.4018+01

N,C OR S	ADVANCE RATIO, MU = 0.4			
	(0.0)R			
0 .6871+03				
1-S,C .1163+04	.2026+03	-.5775+03	-.1082+03	-.7081+02
1-S,S .1124+05	-.4155+04	.6405+03	.3881+02	.1438+03
	(0.14)R			
0 .5353+03				
1-S,C .3573+03	.1081+03	-.5732+02	.6319+01	.7133+01
1-S,S .1137+04	-.2552+03	-.1306+02	.1312+02	-.1647+02
	(0.325)R			
0 .1138+04				
1-S,C .4606+03	.1467+03	.1262+03	.4474+02	.3014+02
1-S,S -.1097+04	.7825+03	-.2062+03	-.1293+01	-.6188+02
	(0.55)R			
0 .1612+04				
1-S,C .6377+03	.3492+02	.3937+03	.3468+02	.2845+01
1-S,S -.1635+04	.1014+04	-.1307+03	-.6715+02	.6912+01
	(0.75)R			
0 .1386+04				
1-S,C .5070+03	-.1142+03	.5013+03	.3432+01	-.3198+02
1-S,S -.1298+04	.7158+03	.3446+02	-.1103+03	.8696+02
	(0.85)R			
0 .7740+03				
1-S,C .2856+03	-.9910+02	.3284+03	-.4014+01	-.2643+02
1-S,S -.7284+03	.3800+03	.5349+02	-.7607+02	.6899+02

N,C OR S	ADVANCE RATIO, MU = 0.5			
	(0.0)R			
0 .9371+03				
1-S,C .1925+04	.1226+04	-.9819+03	-.1445+03	-.2560+03
1-S,S .1556+05	-.6560+04	.7709+03	.1268+03	.3526+03
	(0.14)R			
0 .7029+03				
1-S,C .5658+03	.2513+03	-.1075+03	.2171+02	.2808+02
1-S,S .1586+04	-.3968+03	-.1120+02	.1425+02	-.3906+02
	(0.325)R			
0 .1389+04				
1-S,C .6943+03	.1253+03	.2146+03	.8135+02	.1113+03
1-S,S -.1417+04	.1217+04	-.2440+03	-.2975+02	-.1498+03
	(0.55)R			
0 .1789+04				
1-S,C .7979+03	-.7064+02	.7489+03	.3955+02	.2717+01
1-S,S -.1897+04	.1469+04	-.1746+03	-.1089+03	.1540+02
	(0.75)R			
0 .1347+04				
1-S,C .5287+03	-.2535+03	.9853+03	-.3248+02	-.1310+03
1-S,S -.1306+04	.9304+03	.7798+01	-.1453+03	.2083+03
	(0.85)R			
0 .7398+03				
1-S,C .2721+03	-.1909+03	.6503+03	-.3400+02	-.1065+03
1-S,S -.6828+03	.4645+03	.4051+02	-.9617+02	.1655+03

N,C OR S	ADVANCE RATIO, MU = 0.7			
	(0.0)R			
0 .2604+04				
1-S,C .8719+04	.3394+04	-.5826+02	.1959+03	.8034+03
1-S,S .2330+05	-.1046+05	.2054+04	.3171+03	.9216+03
	(0.14)R			
0 .1244+04				
1-S,C .1369+04	.5981+03	-.1042+03	.1153+03	-.7308+02
1-S,S .3148+04	-.6771+03	.1155+03	.3562+02	-.6646+02
	(0.325)R			
0 .1792+04				
1-S,C .1101+04	.1017+02	.3436+02	.9862+02	-.3387+03
1-S,S -.2043+04	.2099+04	-.5731+03	-.8961+02	-.3883+03
	(0.55)R			
0 .1972+04				
1-S,C .9871+03	-.2659+02	.8577+03	-.1806+03	.1039+03
1-S,S -.2470+04	.2264+04	-.7237+03	-.2503+03	-.1051+02
	(0.75)R			
0 .1196+04				
1-S,C .3534+03	-.1739+01	.1300+04	-.3842+03	.5399+03
1-S,S -.1260+04	.1093+04	-.4771+03	-.2885+03	.4168+03
	(0.85)R			
0 .5832+03				
1-S,C .1022+03	.4221+01	.8562+03	-.2658+03	.4001+03
1-S,S -.5362+03	.4472+03	-.2422+03	-.1795+03	.3248+03

N,C OR S	ADVANCE RATIO, MU = 1.0			
	(0.0)R			
0 .9909+04				
1-S,C .1152+05	.6819+04	.4395+04	.6718+03	.2420+04
1-S,S .3883+05	-.1602+05	.3020+04	-.6852+03	-.1552+03
	(0.14)R			
0 .3313+04				
1-S,C .3393+04	.1894+04	.5733+03	.2972+03	-.2020+03
1-S,S .7058+04	-.1647+04	.2124+03	-.1497+03	.1983+03
	(0.325)R			
0 .2366+04				
1-S,C .1679+04	-.1446+03	-.6806+03	.1844+03	-.1134+04
1-S,S -.3066+04	.3896+04	-.8119+03	.1495+03	.3073+03
	(0.55)R			
0 .1628+04				
1-S,C .6333+03	-.5647+03	-.2311+03	-.2963+03	.3233+03
1-S,S -.3663+04	.3646+04	-.3251+03	.6369+03	-.3361+03
	(0.75)R			
0 .3579+03				
1-S,C -.3775+03	-.4404+03	.4308+03	-.5833+03	.1606+04
1-S,S -.1323+04	.1118+04	.3837+03	.7557+03	-.7793+03
	(0.85)R			
0 .1650+02				
1-S,C -.3723+03	-.2343+03	.3563+03	-.3851+03	.1139+04
1-S,S -.3937+03	.2543+03	.3355+03	.4598+03	-.5243+03

N,C OR S	ADVANCE RATIO, MU = 1.4			
	(0.0)R			
0 .2545+05				
1-S,C .2743+05	.1347+05	.1385+05	-.5580+04	.2606+04
1-S,S .5967+05	-.2401+05	-.4670+04	-.2763+04	.5564+03
	(0.14)R			
0 .6590+04				
1-S,C .7718+04	.4198+04	.2735+04	-.3596+03	-.2127+03
1-S,S .1413+05	-.3076+04	-.1232+04	-.1309+04	.6785+03
	(0.325)R			
0 .3204+04				
1-S,C .1108+03	.1019+04	-.1770+04	.2874+04	-.1053+04
1-S,S -.3898+04	.7074+04	.1162+04	.2445+02	.6247+03
	(0.55)R			
0 .5994+03				
1-S,C -.2654+04	-.1150+03	-.1094+04	.4198+04	.1612+04
1-S,S -.4698+04	.7019+04	.4574+04	.3806+04	-.9422+03
	(0.75)R			
0 -.9135+03				
1-S,C -.2566+04	-.4904+03	.5608+03	.2952+04	.3121+04
1-S,S -.6810+03	.2473+04	.4919+04	.4926+04	-.1752+04
	(0.85)R			
0 -.7128+03				
1-S,C -.1433+04	-.3224+03	.5587+03	.1508+04	.1992+04
1-S,S .2091+03	.7662+03	.2852+04	.2965+04	-.1112+04

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 4.
COLLECTIVE PITCH TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(I) MP = 0.5
FP = 0.01 (FOR MU = 0.25,0.4,0.5)
FP = 0.00447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S		ADVANCE RATIO, MU = 0.25			
		(0.0)R			
0	.6426+02				
1-S,C	.3270+03	-.2451+03	.6110+02	.1836+02	.2936+01
1-S,S	.2694+04	-.4442+03	.1118+03	-.1685+01	-.4021-00
		(0.14)R			
0	.3087+03				
1-S,C	.1752+03	-.3104+02	.8806+01	.4510+01	.6114-00
1-S,S	.7474+03	-.1028+03	.1998+02	.4601-00	-.3066-01
		(0.325)R			
0	.7192+03				
1-S,C	.1554+03	.1068+03	-.1966+02	-.5489+01	-.8026-00
1-S,	-.3662+03	.1049+03	-.4135+02	.1043+01	.2593-00
		(0.55)R			
0	.9942+03				
1-S,C	.1608+03	.1254+03	-.1160+02	-.1278+02	-.1124+01
1-S,S	-.7416+03	.1689+03	-.6374+02	.1910+01	.4001-00
		(0.75)R			
0	.6932+03				
1-S,C	.1000+03	.6227+02	.3477+01	-.1066+02	-.6329-00
1-S,S	-.4960+03	.1065+03	-.4184+02	-.3201+01	.2786-00
		(0.85)R			
0	.3495+03				
1-S,C	.4861+02	.2662+02	.3885+01	-.5668+01	-.2888-00
1-S,S	-.2446+03	.5118+02	-.2050+02	.1949+01	.1399-00

N,C OR S		ADVANCE RATIO, MU = 0.4			
		(0.0)R			
0	.9302+02				
1-S,C	.8490+03	-.5944+03	.2816+03	.1251+03	.3119+02
1-S,S	.4744+04	-.1267+04	.4797+03	-.3620+02	-.4159+01
		(0.14)R			
0	.4206+03				
1-S,C	.4388+03	-.7049+02	.4133+02	.3098+02	.3896+01
1-S,S	.1356+04	-.3034+03	.9082+02	-.3033+01	-.2528+01
		(0.325)R			
0	.9389+03				
1-S,C	.3545+03	.2753+03	-.9356+02	.3932+02	-.1343+02
1-S,S	-.5501+03	.2707+03	-.1728+03	.1435+02	-.1339-00
		(0.55)R			
0	.1212+04				
1-S,C	.3293+03	.3368+03	-.6875+02	-.9566+02	-.1503+02
1-S,S	-.1185+04	.4346+03	-.2858+03	.4208+01	.6538+01
		(0.75)R			
0	.6001+03				
1-S,C	.1875+03	.1790+03	-.5561-00	-.8181+02	-.6896+01
1-S,S	-.7960+03	.2669+03	-.1980+03	.7326+01	.7903+01
		(0.85)R			
0	.3953+03				
1-S,C	.8797+02	.7957+02	.8491+01	-.4379+02	-.2802+01
1-S,S	-.3920+03	.1267+03	-.9906+02	.5564+01	.4575+01

N,C OR S		ADVANCE RATIO, MU = 0.5			
		(0.0)R			
0	-.1351+01				
1-S,C	.1164+04	-.6584+03	.4008+03	.3696+03	.7715+02
1-S,S	.6371+04	-.2106+04	.9005+03	.1001+03	.1427+02
		(0.14)R			
0	.4733+03				
1-S,C	.6269+03	-.3038+02	.5304+02	.8007+02	.1130+02
1-S,S	.1826+04	-.5090+03	.1905+03	.1742+02	-.4344+01
		(0.325)R			
0	.1106+04				
1-S,C	.5305+03	.3939+03	-.1285+03	-.1251+03	-.3213+02
1-S,S	-.6808+03	.4168+03	-.3005+03	.3417+02	-.1088+02
		(0.55)R			
0	.1354+04				
1-S,C	.4696+03	.4259+03	-.4694+02	-.2490+03	-.4285+02
1-S,S	-.1407+04	.6252+03	-.5638+03	.4364+02	.1117+02
		(0.75)R			
0	.8454+03				
1-S,C	.2466+03	.1976+03	.5828+02	-.1939+03	-.2483+02
1-S,S	-.8886+03	.3489+03	-.4228+03	.2309+02	.2248+02
		(0.85)R			
0	.4066+03				
1-S,C	.1111+03	.8110+02	.4607+02	-.1009+03	-.1153+02
1-S,S	-.4243+03	.1580+03	-.2174+03	.1022+02	.1397+02

N,C OR S		ADVANCE RATIO, MU = 0.7			
		(0.0)R			
0	.2976+03				
1-S,C	.2742+04	-.2481+03	.1719+04	.6402+03	.9490+02
1-S,S	.6735+04	-.3555+04	.8470+03	.9243+03	-.2280+03
		(0.14)R			
0	.7312+03				
1-S,C	.1465+04	.1893+03	.3963+03	.1905+03	.9734+01
1-S,S	.2627+04	-.9850+03	.2058+03	-.2187+03	-.2812+02
		(0.325)R			
0	.1376+04				
1-S,C	.9960+03	.5947+03	-.4779+03	.1705+03	-.3573+02
1-S,S	-.7239+03	.6248+03	-.2976+03	.3234+03	.1133+03
		(0.55)R			
0	.1462+04				
1-S,C	.7026+03	.6246+03	-.6451+03	.4509+03	-.1975+01
1-S,S	-.1853+04	.9380+03	-.6004+03	.6177+03	.1302+03
		(0.75)R			
0	.8179+03				
1-S,C	.3071+03	.3118+03	-.3277+03	.3765+03	.2818+02
1-S,S	-.9203+03	.4611+03	-.4527+03	.4506+03	.6170+02
		(0.85)R			
0	.3736+03				
1-S,C	.1286+03	.1349+03	-.1412+03	.1983+03	.1927+02
1-S,S	-.4098+03	.1934+03	-.2314+03	.2279+03	.2567+02

N,C OR S		ADVANCE RATIO, MU = 1.0			
		(0.0)R			
0	.3021+04				
1-S,C	.6217+04	.1227+04	.3330+04	.7977+03	-.2690+03
1-S,S	.1447+05	-.6526+04	-.5004+03	.2199+04	.3815+03
		(0.14)R			
0	.2193+04				
1-S,C	.3410+04	.1003+04	.9714+03	.1216+03	-.6545+02
1-S,S	.5445+04	-.2117+04	-.2050+03	.6446+03	.1822+03
		(0.325)R			
0	.2039+04				
1-S,C	.1936+04	.1057+04	-.6978+03	.5022+03	.1715+03
1-S,S	-.5533+03	.9076+03	.4833+02	.6972+03	-.5969+02
		(0.55)R			
0	.1528+04				
1-S,C	.1041+04	.8337+03	-.1022+04	.8348+03	.4183+03
1-S,S	-.2196+04	.1512+04	.2666+03	.1520+04	-.4203+03
		(0.75)R			
0	.6268+03				
1-S,C	.3606+03	.3485+03	-.4794+03	.5695+03	.3465+03
1-S,S	-.1136+04	.6794+03	.2376+03	.1126+04	-.4137+03
		(0.85)R			
0	.2462+03				
1-S,C	.1309+03	.1379+03	-.1954+03	.2801+03	.1809+03
1-S,S	-.4776+03	.2666+03	.1258+03	.5677+03	-.2248+03

N,C OR S		ADVANCE RATIO, MU = 1.4			
		(0.0)R			
0	.1178+05				
1-S,C	.1383+05	.5294+04	.4183+04	.5214+04	.3060+04
1-S,S	.2850+05	-.1057+05	-.2778+04	.2281+04	.5318+04
		(0.14)R			
0	.6984+04				
1-S,C	.7641+04	.3608+04	.2008+04	.1095+04	.8984+03
1-S,S	.1291+05	-.3506+04	-.8179+03	.3640+03	.1631+04
		(0.325)R			
0	.3791+04				
1-S,C	.3441+04	.2780+04	.7687+03	.2805+04	-.8890+03
1-S,S	.1634+04	.1963+04	.8903+03	.1352+04	-.1903+04
		(0.55)R			
0	.1498+04				
1-S,C	.1113+04	.1991+04	.9353+03	.4622+04	-.1408+04
1-S,S	-.2094+04	.3110+04	.1576+04	.1867+04	-.4024+04
		(0.75)R			
0	.2458+03				
1-S,C	.1949+03	.9035+03	.8863+03	.2971+04	-.7689+03
1-S,S	-.1089+04	.1402+04	.9754+03	.1052+04	-.2856+04
		(0.85)R			
0	.2180+02				
1-S,C	.3444+02	.3830+03	.4836+03	.1422+04	-.3416+03
1-S,S	-.4245+03	.5544+03	.4583+03	.4776+03	-.1411+04

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 5.
BLADE TWIST TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(A) MP = 0.1
FP = 0.001 (FOR MU = 0.25,0.4,0.5)
FP = 0.000447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S		ADVANCE RATIO, MU = 0.25			
		(0.0)R			
0	.1613+05				
1-5,C	.2927+05	.1234+04	.6498+02	-.7057+01	-.5645+02
1-5,S	.9465+03	-.4057+03	.1715+03	-.3261+02	.2049+02
		(0.14)R			
0	.7862+03				
1-5,C	.1325+04	.3156+02	-.2285+01	-.3330+01	.3898+01
1-5,S	.1265+03	-.2848+02	.2111+01	-.1083+01	-.8286+01
		(0.325)R			
0	.2834+03				
1-5,C	-.5080-00	-.3499+02	-.1205+02	-.6380+01	.1021+02
1-5,S	.2369+03	-.1654+02	-.2713+02	.9438-00	-.1515+02
		(0.55)R			
0	.3152+03				
1-5,C	-.4124+02	-.6545+01	-.2357+01	.1975+01	-.1542+00
1-5,S	.3208+03	-.2675+02	-.6242+02	-.2624+01	.1644+01
		(0.75)R			
0	-.3711+03				
1-5,C	-.9676+02	.1353+03	.2746+02	.2198+02	-.1265+02
1-5,S	.1997+03	-.6775+02	-.6460+02	-.1041+02	.2628+02
		(0.85)R			
0	-.5378+03				
1-5,C	-.8063+02	.1435+03	.2951+02	.2287+02	-.1183+02
1-5,S	.8165+02	-.6264+02	-.4145+02	-.9919+01	.2512+02

N,C OR S		ADVANCE RATIO, MU = 0.4			
		(0.0)R			
0	.1837+05				
1-5,C	.4856+05	.3398+04	.3531+03	-.6550+02	-.1289+03
1-5,S	.2161+04	-.9794+03	.6863+03	-.3336+02	-.4790+02
		(0.14)R			
0	.8516+03				
1-5,C	.2197+04	.8228+02	-.2199+01	.1997+01	.8140+01
1-5,S	.2537+03	-.7442+02	.2067+02	-.2887+01	-.3926+01
		(0.325)R			
0	.2154+03				
1-5,C	-.9890+01	-.1567+03	-.4694+02	.8558+01	.2588+02
1-5,S	.4390+03	-.5465+02	-.8029+02	-.1800+01	-.4118+01
		(0.55)R			
0	.2425+03				
1-5,C	-.8702+02	-.2314+02	-.3283+02	-.3919+01	.3115+01
1-5,S	.6268+03	-.9516+02	-.2176+03	-.5004+01	-.2836+00
		(0.75)R			
0	-.4735+03				
1-5,C	-.1773+03	.3522+03	.5165+02	-.2631+02	-.4151+02
1-5,S	.3944+03	-.1955+03	-.2399+03	-.1559+02	.1120+02
		(0.85)R			
0	-.6243+03				
1-5,C	-.1435+03	.3741+03	.6695+02	-.2528+02	-.4265+02
1-5,S	.1667+03	-.1751+03	-.1578+03	-.1492+02	.1180+02

N,C OR S		ADVANCE RATIO, MU = 0.5			
		(0.0)R			
0	.2005+05				
1-5,C	.6282+05	.6143+04	.1059+04	-.1169+03	-.7591+02
1-5,S	.3440+04	-.1587+04	.1585+04	.1998+03	.2589+03
		(0.14)R			
0	.1026+04				
1-5,C	.2822+04	.8223+02	-.2815+02	.8063+01	-.6931+01
1-5,S	.4261+03	-.9352+02	.1294+02	-.2224+02	-.4917+02
		(0.325)R			
0	.2078+03				
1-5,C	-.4689+02	-.3550+03	-.1596+03	.1990+02	-.3091+01
1-5,S	.6447+03	-.8383+02	-.1822+03	-.6179+02	-.1052+03
		(0.55)R			
0	-.2592+02				
1-5,C	-.1381+03	-.6775+02	-.1129+03	-.1788+02	.1531+02
1-5,S	.8329+03	-.2272+03	-.3988+03	-.3522+02	.4296+01
		(0.75)R			
0	-.4236+03				
1-5,C	-.2534+03	.4590+03	.2277+02	-.7283+02	.3833+02
1-5,S	.6877+03	-.3450+03	-.5480+03	.2992+02	.1893+02
		(0.85)R			
0	-.4169+03				
1-5,C	-.2051+03	.4765+03	.5796+02	-.6682+02	.3321+02
1-5,S	.4212+03	-.2710+03	-.4184+03	.4070+02	.1864+03

N,C OR S		ADVANCE RATIO, MU = 0.7			
		(0.0)R			
0	.2281+05				
1-5,C	.8814+05	.1144+05	.4410+04	.7573+03	.1562+04
1-5,S	.5169+04	-.2536+04	.6551+04	.1090+04	.2896+04
		(0.14)R			
0	.1362+04				
1-5,C	.5941+04	.3219+03	.4311+02	-.1401+03	-.2550+03
1-5,S	.7055+03	-.2732+03	.1099+03	-.6027+02	-.3813+03
		(0.325)R			
0	-.2136+03				
1-5,C	.8107+02	-.6887+03	-.6878+03	-.1946+03	-.5887+03
1-5,S	.9885+03	-.2442+03	-.9521+03	-.2671+03	-.1035+04
		(0.55)R			
0	-.2835+03				
1-5,C	-.1990+03	-.3591+03	-.9885+03	.9381+02	.1695+03
1-5,S	.1414+04	-.5520+03	-.1782+04	-.1304+03	.8540+02
		(0.75)R			
0	-.7220+03				
1-5,C	-.3675+03	.1207+04	-.6903+03	-.3548+02	.1221+04
1-5,S	.1024+04	-.9588+03	-.2028+04	.1837+03	.1969+04
		(0.85)R			
0	-.6531+03				
1-5,C	-.2794+03	.1317+04	-.3514+03	-.1199+03	.1084+04
1-5,S	.5345+03	-.7676+03	-.1393+04	.2095+03	.1828+04

N,C OR S		ADVANCE RATIO, MU = 1.0			
		(0.0)R			
0	.3320+05				
1-5,C	.1370+06	.2126+05	.1614+05	.2332+04	.1087+05
1-5,S	.1768+05	-.4071+04	.2285+05	.4074+04	.8949+04
		(0.14)R			
0	.2832+04				
1-5,C	.1393+05	.1818+04	.5586+03	-.4463+03	-.1518+04
1-5,S	.2615+04	-.5864+03	.8089+03	-.7785+02	-.1087+04
		(0.325)R			
0	-.1082+04				
1-5,C	.5573+03	-.1237+04	-.2889+04	-.1087+04	-.4486+04
1-5,S	.1931+04	-.5163+03	-.4018+04	-.1018+04	-.3171+04
		(0.55)R			
0	-.1586+04				
1-5,C	-.3643+03	-.1149+04	-.4696+04	.5446+03	.1162+04
1-5,S	.1952+04	-.1383+04	-.6387+04	-.7256+03	.3493+03
		(0.75)R			
0	-.1464+04				
1-5,C	-.7182+03	.1524+04	-.4213+04	.2133+04	.8957+04
1-5,S	.1028+04	-.2217+04	-.5683+04	.1525+03	.4182+04
		(0.85)R			
0	-.9198+03				
1-5,C	-.5260+03	.1773+04	-.2539+04	.1690+04	.7536+04
1-5,S	.4409+03	-.1636+04	-.3398+04	.3087+03	.3444+04

N,C OR S		ADVANCE RATIO, MU = 1.4			
		(0.0)R			
0	.7242+05				
1-5,C	.2355+06	.2988+05	.5656+05	-.7687+03	.5164+04
1-5,S	.4141+05	-.2759+04	.3355+05	.6528+04	-.2435+04
		(0.14)R			
0	.9297+04				
1-5,C	.3467+05	.4604+04	.3852+04	-.1130+04	-.1120+04
1-5,S	.7981+04	-.9954+03	.3131+04	.4767+03	.4292+03
		(0.325)R			
0	-.2570+04				
1-5,C	.1536+04	-.6574+03	-.1181+05	-.8526+03	-.2891+04
1-5,S	.4163+04	-.2000+04	-.5691+04	-.1366+04	.2055+04
		(0.55)R			
0	-.4252+04				
1-5,C	-.1821+04	-.1156+04	-.2048+05	.1043+04	.1393+04
1-5,S	.3102+04	-.4484+04	-.8315+04	-.1567+04	-.1162+04
		(0.75)R			
0	-.3588+04				
1-5,C	-.1939+04	.2425+04	-.1942+05	.5167+03	.5603+04
1-5,S	.1181+04	-.5228+04	-.3510+04	-.1658+03	-.7449+04
		(0.85)R			
0	-.2095+04				
1-5,C	-.1160+04	.2489+04	-.1167+05	.1664+01	.4237+04
1-5,S	.4022+03	-.3393+04	-.9080+03	.2420+03	-.6066+04

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 5.
BLADE TWIST TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(B) MP = 0.1
FP = 0.0025 (FOR MU = 0.25,0.4,0.5)
FP = 0.00112(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S	ADVANCE RATIO, MU = 0.25				
			(0.0)R		
0	.1090+05				
1-S,C	.2018+05	.7897+03	.1768+03	-.7667+01	-.1653+02
1-S,S	-.9978+03	-.4426+03	.1577+03	-.1885+02	-.4326+02
			(0.14)R		
0	.1740+04				
1-S,C	.2964+04	.9113+02	.9066+01	-.9884-00	-.1422+01
1-S,S	-.4196+02	-.6471+02	.1046+02	-.1900+01	.1032+01
			(0.325)R		
0	.4237+03				
1-S,C	.2921+03	-.2634+02	-.3922+02	-.1634+01	.8554+00
1-S,S	.2326+03	-.1282+02	-.3525+02	-.4535-00	.1096+02
			(0.55)R		
0	.1453+03				
1-S,C	.5139+02	.2703+02	-.5588+02	-.8052+01	-.3028+01
1-S,S	.2938+03	-.3272+02	-.6990+02	-.6881+01	-.5857+01
			(0.75)R		
0	-.1374+03				
1-S,C	-.3133+02	.6563+02	-.4468+02	-.1161+02	-.6273+01
1-S,S	.2027+03	-.4450+02	-.7308+02	-.1117+02	-.2336+02
			(0.85)R		
0	-.1375+03				
1-S,C	-.3176+02	.6410+02	-.2519+02	-.7813+01	-.4484+01
1-S,S	.1064+03	-.2967+02	-.4542+02	-.7694+01	-.1775+02

N,C OR S	ADVANCE RATIO, MU = 0.4				
			(0.0)R		
0	.1255+05				
1-S,C	.3386+05	.2271+04	.6472+03	.3628+01	-.1673+02
1-S,S	-.9808+03	-.1142+04	.7225+03	.9821+01	-.1677+02
			(0.14)R		
0	.1954+04				
1-S,C	.4966+04	.2554+03	.3666+02	.1082+01	-.6477+01
1-S,S	.4997+02	-.1696+03	.5775+02	-.2197+01	-.6664+01
			(0.325)R		
0	.3804+03				
1-S,C	.4727+03	-.9467+02	-.1308+03	-.6495+01	-.7784+01
1-S,S	.4482+03	-.4058+02	-.1369+03	-.1138+02	-.9289+01
			(0.55)R		
0	.5770+02				
1-S,C	.6618+02	.4459+02	-.1741+03	-.3460+02	-.2544+01
1-S,S	.5865+03	-.9739+02	-.2862+03	-.2377+02	-.7954+01
			(0.75)R		
0	-.2135+03				
1-S,C	-.6551+02	.2134+03	-.1278+03	-.4912+02	.4832+01
1-S,S	.4019+03	-.1276+03	-.3071+03	-.2688+02	-.2421+01
			(0.85)R		
0	-.1816+03				
1-S,C	-.5984+02	.1642+03	-.6923+02	-.3388+02	.4401+01
1-S,S	.2142+03	-.8433+02	-.1923+03	-.1644+02	-.4082-00

N,C OR S	ADVANCE RATIO, MU = 0.5				
			(0.0)R		
0	.1413+05				
1-S,C	.4417+05	.3910+04	.1644+04	.8498+02	.2970+02
1-S,S	-.5454+03	-.1788+04	.1191+04	.1357+03	-.2811+03
			(0.14)R		
0	.2150+04				
1-S,C	.6473+04	.4292+03	.9157+02	.7196+01	-.1767+02
1-S,S	.1864+03	-.2694+03	.1075+03	-.6665+01	.2167+02
			(0.325)R		
0	.3137+03				
1-S,C	.6044+03	-.1906+03	-.3424+03	-.3023+02	-.3785+02
1-S,S	.6387+03	-.8035+02	-.2013+03	-.5627+02	.9553+02
			(0.55)R		
0	-.5279+02				
1-S,C	.7178+02	.3428+02	-.4757+03	-.1013+03	.2987-00
1-S,S	.8322+03	-.1991+03	-.4578+03	-.5419+02	-.4603+02
			(0.75)R		
0	-.3005+03				
1-S,C	-.9515+02	.3293+03	-.3686+03	-.1324+03	.4595+02
1-S,S	.6241+03	-.2577+03	-.5119+03	-.2193+02	-.1941+03
			(0.85)R		
0	-.2302+03				
1-S,C	-.8306+02	.2602+03	-.2049+03	-.8728+02	.3710+02
1-S,S	.3421+03	-.1698+03	-.3244+03	-.7136+01	-.1480+03

N,C OR S	ADVANCE RATIO, MU = 0.7				
			(0.0)R		
0	.1567+05				
1-S,C	.6550+05	.8309+04	.8666+04	.1072+04	.4731+03
1-S,S	-.1405+04	-.3024+04	.4511+04	.6586+03	-.1426+04
			(0.14)R		
0	.2828+04				
1-S,C	.1200+05	.1166+04	.7514+03	.5724+02	-.7239+02
1-S,S	.1564+03	-.6026+03	.4976+03	.5031+02	.1913+03
			(0.325)R		
0	.7069+02				
1-S,C	.1464+04	-.4774+03	-.2011+04	-.3367+03	-.2462+03
1-S,S	.9851+03	-.2911+03	-.8665+03	-.1582+03	.6880+03
			(0.55)R		
0	-.4177+03				
1-S,C	.1968+03	-.1099+03	-.3253+04	-.4930+03	.7716+02
1-S,S	.1369+04	-.6571+03	-.1703+04	-.2198+03	-.3018+03
			(0.75)R		
0	-.4504+03				
1-S,C	-.1230+03	.4865+03	-.2761+04	-.3948+03	.3930+03
1-S,S	.9593+03	-.7648+03	-.1646+04	-.1612+03	-.1226+04
			(0.85)R		
0	-.2714+03				
1-S,C	-.1123+03	.3981+03	-.1566+04	-.2192+03	.2909+03
1-S,S	.5133+03	-.4780+03	-.9755+03	-.8621+02	-.8968+03

N,C OR S	ADVANCE RATIO, MU = 1.0				
			(0.0)R		
0	.2470+05				
1-S,C	.1150+06	.1677+05	.3271+05	.2094+04	-.5787+03
1-S,S	-.3120+04	-.5898+04	.2617+04	.1251+04	-.9391+03
			(0.14)R		
0	.5317+04				
1-S,C	.2764+05	.3220+04	.4083+04	.5477+02	-.2383+01
1-S,S	.8668+01	-.1650+04	.5962+03	.1078+03	.3835+03
			(0.325)R		
0	-.3662+03				
1-S,C	.4304+04	-.9213+03	-.8378+04	-.8833+03	.1748+03
1-S,S	.1599+04	-.1057+04	.2555+03	-.2384+03	.7364+03
			(0.55)R		
0	-.1519+04				
1-S,C	.5965+03	-.1105+04	-.1423+05	-.9147+03	-.1250+03
1-S,S	.1909+04	-.1755+04	.8357+03	.1348+03	-.1019+04
			(0.75)R		
0	-.1179+04				
1-S,C	-.1747+03	-.2693+03	-.1164+05	-.4289+03	-.3611+03
1-S,S	.1144+04	-.1676+04	.1029+04	.4530+03	-.2190+04
			(0.85)R		
0	-.6253+03				
1-S,C	-.1713+03	-.2043+02	-.6384+04	-.1689+03	-.2479+03
1-S,S	.5484+03	-.9702+03	.6324+03	.3147+03	-.1462+04

N,C OR S	ADVANCE RATIO, MU = 1.4				
			(0.0)R		
0	.4424+05				
1-S,C	.1345+06	.2006+05	.2744+05	-.3182+04	-.2632+04
1-S,S	-.9153+04	-.6593+04	-.3135+05	.7708+03	.1213+04
			(0.14)R		
0	.1211+05				
1-S,C	.3988+05	.5172+04	.5147+04	-.8747+03	.3427+03
1-S,S	-.1433+04	-.3133+04	-.4484+04	-.2362+02	.4620+03
			(0.325)R		
0	-.9334+02				
1-S,C	.7321+04	-.4089+03	-.6081+04	.4979+03	.1275+04
1-S,S	.2240+04	-.3104+04	.1154+05	.3899+03	.2879+02
			(0.55)R		
0	-.3169+04				
1-S,C	.6723+03	-.6188+03	-.1057+05	.2320+04	-.1612+04
1-S,S	.2542+04	-.3298+04	.2121+05	.2986+04	-.7320+03
			(0.75)R		
0	-.2461+04				
1-S,C	-.9069+02	.1646+02	-.7887+04	.2544+04	-.3308+04
1-S,S	.1148+04	-.2030+04	.1729+05	.3666+04	-.9493+03
			(0.85)R		
0	-.1273+04				
1-S,C	-.6268+02	.1391+03	-.4112+04	.1481+04	-.2125+04
1-S,S	.4558+03	-.9881+03	.9304+04	.2187+04	-.5711+03

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 5.
BLADE TWIST TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(2) MB = 0.1
FP = 0.01 (FOR MB ≤ 0.25,0.4,0.5)
FP = 0.00447(1+MU)**2 (FOR MB = 0.7,1.0,1.4)

N,C OR S		ADVANCE RATIO, MU = 0.25			
		(0,0)R			
0	.5848+04				
1-S,C	.1029+05	.3350+03	.3644+02	-.1933+01	-.4074+01
1-S,S	-.2921+04	-.3958+03	-.7286+02	-.1666+02	-.5263+01
		(0,1)R			
0	.2333+04				
1-S,C	.3983+04	.1168+03	.1040+02	-.1278+01	-.1614+01
1-S,S	-.1037+04	-.1522+03	-.1238+02	-.3526+01	-.1338+01
		(0,25)R			
0	.6178+03				
1-S,C	.1234+04	.2481+02	-.3634+01	-.1799+01	-.8825+00
1-S,S	-.1407+03	-.5345+02	.2891+02	.5365+01	.8476+00
		(0,5)R			
0	.2446+03				
1-S,C	.3853+03	.3028+02	-.6800+01	-.2859+01	-.1481+01
1-S,S	.1228+03	-.4286+02	.4320+02	.9718+01	.1228+01
		(0,75)R			
0	.6336+01				
1-S,C	.1055+03	.3653+02	-.3794+01	-.2283+01	-.1283+01
1-S,S	.1003+03	-.3406+02	.2856+02	.7091+01	.6052+00
		(0,85)R			
0	-.1961+02				
1-S,C	.3549+02	.2154+02	-.1669+01	-.1283+01	-.7058+00
1-S,S	.4995+02	-.1836+02	.1484+02	.3612+01	.2543+00

N,C OR S		ADVANCE RATIO, MU = 0.4			
		(0,0)R			
0	.6859+04				
1-S,C	.1780+05	.1003+04	.2657+03	.1696+02	-.1031+02
1-S,S	-.4258+04	-.1113+04	-.2936+03	-.7878+02	-.1223+02
		(0,1)R			
0	.2695+04				
1-S,C	.6862+04	.3473+03	.7150+02	.1976+01	-.5223+01
1-S,S	-.1474+04	-.4252+03	-.4749+02	-.1628+02	-.5767+01
		(0,25)R			
0	.8695+03				
1-S,C	.2118+04	.6610+02	-.4087+02	-.1183+02	-.4839+01
1-S,S	-.1183+03	-.1484+03	.1178+03	.2761+02	-.1990+01
		(0,5)R			
0	.1973+03				
1-S,C	.6516+03	.7492+02	-.7785+02	-.2120+02	-.6602+01
1-S,S	.2835+03	-.9949+02	.1723+03	.5280+02	.3614+01
		(0,75)R			
0	-.3715+02				
1-S,C	.1774+03	.9611+02	-.5139+02	-.1699+02	-.5078+01
1-S,S	.2106+03	-.7725+02	.1091+03	.3930+02	.5257+01
		(0,85)R			
0	-.4228+02				
1-S,C	.5977+02	.5739+02	-.2509+02	-.8938+01	-.2656+01
1-S,S	.1037+03	-.4158+02	.5270+02	.2026+02	.3125+01

N,C OR S		ADVANCE RATIO, MU = 0.5			
		(0,0)R			
0	.7792+04				
1-S,C	.2365+05	.1870+04	.4185+03	.1183+03	-.5950+02
1-S,S	-.4884+04	-.1823+04	-.5952+03	-.4467+02	-.1643+02
		(0,1)R			
0	.3020+04				
1-S,C	.9153+04	.6400+03	.1176+03	.1861+02	-.9935+01
1-S,S	-.1647+04	-.6952+03	-.9079+02	-.1692+02	-.5285+01
		(0,25)R			
0	.8963+03				
1-S,C	.2792+04	.9732+02	-.4218+02	-.5161+02	.1210+02
1-S,S	-.2347+02	-.2305+03	.2489+03	.1187+02	-.3150+01
		(0,5)R			
0	.1254+03				
1-S,C	.8405+03	.8627+02	-.6888+02	-.8182+02	-.6973+01
1-S,S	.4866+03	-.1730+03	.3554+03	.6014+02	-.1124+02
		(0,75)R			
0	-.9598+02				
1-S,C	.2202+03	.1327+03	-.3136+02	-.5612+02	-.2061+02
1-S,S	.3568+03	-.1386+03	.2212+03	.6270+02	-.1234+02
		(0,85)R			
0	-.7244+02				
1-S,C	.7204+02	.8193+02	-.1236+02	-.2799+02	-.1327+02
1-S,S	.1775+03	-.7506+02	.1061+03	.3526+02	-.7041+01

N,C OR S		ADVANCE RATIO, MU = 0.7			
		(0,0)R			
0	.8906+04				
1-S,C	.3300+05	.3858+04	.9195+03	.3182+03	-.9782+02
1-S,S	-.7709+04	-.3582+04	-.1735+04	-.3028+03	-.7934+02
		(0,1)R			
0	.3728+04				
1-S,C	.1429+05	.1479+04	.3324+03	.5987+02	-.8095+01
1-S,S	-.2990+04	-.1561+04	-.3233+03	-.6414+02	.1396+02
		(0,25)R			
0	.1016+04				
1-S,C	.4955+04	.2820+03	.2168+02	-.9380+02	.3477+02
1-S,S	-.3545+03	-.6293+03	.7418+03	.1528+03	.5737+02
		(0,5)R			
0	-.1761+02				
1-S,C	.1563+04	.1761+03	-.2819+02	-.7950+02	-.1461+02
1-S,S	.5992+03	-.4471+03	.1162+04	.3302+03	-.2166+02
		(0,75)R			
0	-.1852+03				
1-S,C	.4162+03	.2467+03	.6823+01	-.9765+01	-.4726+02
1-S,S	.4872+03	-.3099+03	.7556+03	.2664+03	-.7019+02
		(0,85)R			
0	-.1108+03				
1-S,C	.1392+03	.1499+03	.9159+01	.3239+01	-.3011+02
1-S,S	.2454+03	-.1589+03	.3669+03	.1392+03	-.4464+02

N,C OR S		ADVANCE RATIO, MU = 1.0			
		(0,0)R			
0	.1249+05				
1-S,C	.4940+05	.6414+04	.9820+03	-.1415+04	-.8111+02
1-S,S	-.1117+05	-.7474+04	-.2581+04	.3686+04	.1358+04
		(0,1)R			
0	.5653+04				
1-S,C	.2419+05	.2835+04	.6295+03	-.3743+03	.8634+01
1-S,S	-.4985+04	-.3813+04	-.4723+03	.9332+03	.3986+03
		(0,25)R			
0	.1379+04				
1-S,C	.9584+04	.7245+03	.6335+03	.6641+03	.4290+02
1-S,S	-.1118+04	-.1936+04	.1372+04	-.1191+04	-.4329+03
		(0,5)R			
0	-.4064+03				
1-S,C	.3220+04	.2071+03	.8351+03	.1522+04	-.5467+02
1-S,S	.3917+03	-.1390+04	.2227+04	-.2006+04	-.9085+03
		(0,75)R			
0	-.4906+03				
1-S,C	.8750+03	.2111+03	.6083+03	.1209+04	-.9581+02
1-S,S	.3961+03	-.8451+03	.1467+04	-.1262+04	-.6596+03
		(0,85)R			
0	-.2567+03				
1-S,C	.2975+03	.1267+03	.3087+03	.6285+03	-.5716+02
1-S,S	.1983+03	-.4133+03	.7120+03	-.5999+03	-.3303+03

N,C OR S		ADVANCE RATIO, MU = 1.4			
		(0,0)R			
0	.1998+05				
1-S,C	.6251+05	.6892+04	.1101+04	.8297+04	.3088+04
1-S,S	-.1138+05	-.1159+05	-.1433+04	.4995+04	.2825+04
		(0,1)R			
0	.1004+05				
1-S,C	.3410+05	.3427+04	.1280+04	.2288+04	.8744+03
1-S,S	-.5560+04	-.6916+04	.8061+02	.1486+04	.6832+03
		(0,25)R			
0	.2877+04				
1-S,C	.1494+05	.1010+04	.1626+04	-.3089+04	-.1228+04
1-S,S	-.1448+04	-.4220+04	.1730+04	-.1540+04	-.8096+03
		(0,5)R			
0	-.5041+03				
1-S,C	.5112+04	.6076+02	.1736+04	-.4788+04	-.2390+04
1-S,S	.2503+03	-.2935+04	.2629+04	-.2692+04	-.1533+04
		(0,75)R			
0	-.7635+03				
1-S,C	.1349+04	-.1499+02	.1003+04	-.2784+04	-.1643+04
1-S,S	.2840+03	-.1553+04	.1727+04	-.1635+04	-.9743+03
		(0,85)R			
0	-.4015+03				
1-S,C	.4509+03	-.2396+01	.4665+03	-.1260+04	-.8034+03
1-S,S	.1340+03	-.7157+03	.8360+03	-.7621+03	-.4620+03

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 5.
BLADE TWIST TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(B) MR = 0.3
FP = 0.001 (FOR MU = 0.25,0.4,0.5)
FP = 0.000447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S	ADVANCE RATIO, MU = 0.25				
	(0.0)R				
0	.4896+05				
1-S,C	.3359+05	.1649+04	.6018+03	.3079+02	.1871+02
1-S,S	.1295+05	-.5888+03	.4840+03	.5397+02	.1037+02
	(0.14)R				
0	.2381+04				
1-S,C	.1413+04	.8379+02	-.1704+02	.5669+01	-.1676+01
1-S,S	.8827+03	-.1091+03	.1551+02	-.2886+01	.7377+01
	(0.325)R				
0	.8177+03				
1-S,C	-.4695+03	.8201+02	-.9770+02	.2864-00	-.5196+01
1-S,S	.7174+03	-.1144+03	-.6182+02	-.4102+01	-.1660+01
	(0.55)R				
0	.8934+03				
1-S,C	-.9963+03	.3394+03	-.6923+02	-.1994+02	-.1704+01
1-S,S	.8876+03	-.3676+02	-.1987+03	-.9965+01	-.3589+01
	(0.75)R				
0	-.1142+04				
1-S,C	-.9106+03	.8009+03	.4945+02	-.2770+02	.7369+01
1-S,S	.4233+03	-.8593+02	-.2685+03	-.4967+02	-.3661+01
	(0.85)R				
0	-.1621+04				
1-S,C	-.5309+03	.4910+03	.7480+02	-.1917+02	.8118+01
1-S,S	.1097+03	-.7763+02	-.1969+03	-.5068+02	-.2346+01

N,C OR S	ADVANCE RATIO, MU = 0.4				
	(0.0)R				
0	.5339+05				
1-S,C	.5577+05	.4104+04	.2543+04	.2670+03	-.6128+02
1-S,S	.1961+05	-.1218+04	.1935+04	.5129+03	.3209+03
	(0.14)R				
0	.2449+04				
1-S,C	.2343+04	.1741+03	-.6812+02	.2306+02	.6322+01
1-S,S	.1368+04	-.2927+03	.8536+02	-.3449+02	-.3043+02
	(0.325)R				
0	.5563+03				
1-S,C	-.7937+03	.1856+03	-.4140+03	.3276+01	.3892+02
1-S,S	.1348+04	-.3775+03	-.2033+03	-.6148+02	-.7611+02
	(0.55)R				
0	.6365+03				
1-S,C	-.1674+04	.9370+03	-.3195+03	-.1023+03	.2116+02
1-S,S	.1729+04	-.2559+03	-.8285+03	-.5042+02	-.9540+01
	(0.75)R				
0	-.1356+04				
1-S,C	-.1567+04	.1612+04	.1654+03	-.2477+03	-.1127+03
1-S,S	.8553+03	-.3440+03	-.1269+04	-.2495+03	.8781+02
	(0.85)R				
0	-.1767+04				
1-S,C	-.8671+03	.1293+04	.2830+03	-.2163+03	-.1302+03
1-S,S	.2367+03	-.3181+03	-.9771+03	-.2589+03	.8721+02

N,C OR S	ADVANCE RATIO, MU = 0.5				
	(0.0)R				
0	.5723+05				
1-S,C	.7073+05	.6329+04	.4898+04	.6754+03	.2535+03
1-S,S	.2186+05	-.1244+04	.2510+04	.1551+04	.9899+03
	(0.14)R				
0	.2443+04				
1-S,C	.2935+04	.2019+03	-.7551+02	.9667+01	-.7743+02
1-S,S	.1643+04	-.4613+03	.1976+03	-.1993+03	-.1045+03
	(0.325)R				
0	.2073+03				
1-S,C	-.1073+04	.2098+03	-.7866+03	-.9283+01	-.6733+02
1-S,S	.1831+04	-.7803+03	-.1767+03	-.3632+03	-.3248+03
	(0.55)R				
0	.2948+03				
1-S,C	-.2178+04	.1436+04	-.8539+03	-.2083+03	.1062+03
1-S,S	.2564+04	-.8637+03	-.1484+04	-.1247+02	-.7187+02
	(0.75)R				
0	-.1656+04				
1-S,C	-.1956+04	.2390+04	-.2284+02	-.7444+03	.1602+02
1-S,S	.1556+04	-.1022+04	-.2589+04	.5250+02	.6413+03
	(0.85)R				
0	-.1978+04				
1-S,C	-.1132+04	.1877+04	.3060+03	-.7178+03	-.5986+02
1-S,S	.6350+03	-.8075+03	-.2020+04	-.1425+02	.6894+03

N,C OR S	ADVANCE RATIO, MU = 0.7				
	(0.0)R				
0	.5627+05				
1-S,C	.1010+06	.1423+05	.1792+05	.7359+04	.8266+04
1-S,S	.2226+05	-.1068+04	.8480+04	.6078+04	.5942+04
	(0.14)R				
0	.3141+04				
1-S,C	.6263+04	.7996+03	.1287+03	-.6460+03	-.1178+04
1-S,S	.2594+04	-.6473+03	.3681+03	-.6888+03	-.6064+03
	(0.325)R				
0	-.1047+04				
1-S,C	-.1575+04	-.2516+03	-.2995+04	-.1632+04	-.2965+04
1-S,S	.2835+04	-.1759+04	-.1042+04	-.1825+04	-.1945+04
	(0.55)R				
0	-.1182+04				
1-S,C	-.2868+04	.1145+04	-.4661+04	-.5844+03	.5176+03
1-S,S	.3605+04	-.2723+04	-.3860+04	-.2849+03	-.2874+03
	(0.75)R				
0	-.1790+04				
1-S,C	-.2201+04	.3690+04	-.3938+04	-.7363+03	.5790+04
1-S,S	.2419+04	-.3444+04	-.6578+04	.1693+04	.3092+04
	(0.85)R				
0	-.1471+04				
1-S,C	-.1180+04	.3233+04	-.2396+04	-.7714+03	.5254+04
1-S,S	.1109+04	-.2543+04	-.5117+04	.1541+04	.3026+04

N,C OR S	ADVANCE RATIO, MU = 1.0				
	(0.0)R				
0	.7366+05				
1-S,C	.1555+06	.2103+05	.4610+05	.1859+05	.2134+05
1-S,S	.2601+05	.4377+04	.1525+05	.1158+05	.7063+04
	(0.14)R				
0	.5673+04				
1-S,C	.1414+05	.2533+04	.1980+04	-.1657+04	-.2659+04
1-S,S	.5021+04	-.1360+04	.1511+04	-.9323+03	-.4560+03
	(0.325)R				
0	-.3755+04				
1-S,C	-.3326+04	.2325+03	-.8181+04	-.5691+04	-.8763+04
1-S,S	.5203+04	-.3830+04	-.1615+04	-.3759+04	-.1337+04
	(0.55)R				
0	-.4631+04				
1-S,C	-.4832+04	.2604+03	-.1476+05	-.9570+03	.1246+04
1-S,S	.4847+04	-.5348+04	-.6276+04	-.5184+03	-.1340+04
	(0.75)R				
0	-.3204+04				
1-S,C	-.3152+04	.2567+04	-.1424+05	.3441+04	.1675+05
1-S,S	.2350+04	-.6245+04	-.8135+04	.4225+04	-.4250+04
	(0.85)R				
0	-.1724+04				
1-S,C	-.1565+04	.2400+04	-.8759+04	.2917+04	.1443+05
1-S,S	.9667+03	-.4344+04	-.5471+04	.3763+04	-.3746+04

N,C OR S	ADVANCE RATIO, MU = 1.4				
	(0.0)R				
0	.1147+06				
1-S,C	.1829+06	.9122+02	.5526+05	.1558+05	.1624+05
1-S,S	.1233+05	.2634+05	-.2099+05	.5744+04	-.1064+05
	(0.14)R				
0	.1287+05				
1-S,C	.2152+05	.2810+04	.6446+04	-.2252+04	.2215+03
1-S,S	.7037+04	-.1207+04	.2026+04	-.2856+03	.2240+04
	(0.325)R				
0	-.7037+04				
1-S,C	-.1025+05	.5682+04	-.8459+04	-.6073+04	-.3217+03
1-S,S	.9705+04	-.9400+04	.7694+04	-.2643+04	.7380+04
	(0.55)R				
0	-.7929+04				
1-S,C	-.1086+05	.4330+04	-.2167+05	.2345+04	-.1474+04
1-S,S	.6303+04	-.8563+04	.4485+04	.3259+04	-.2623+04
	(0.75)R				
0	-.5841+04				
1-S,C	-.3778+04	.9121+03	-.2147+05	.7476+04	-.9751+03
1-S,S	.1909+04	-.9337+04	.4532+04	.1324+05	-.1775+05
	(0.85)R				
0	-.3376+04				
1-S,C	-.9165+03	-.8066+02	-.1271+05	.5203+04	-.3952+03
1-S,S	.5875+03	-.3782+04	.3395+04	.1044+05	-.1422+05

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 5.
BLADE TWIST TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(E) MR = 0.3
FP = 0.0025 (FOR MU = 0.25,0.4,0.5)
FP = 0.00112(1+MU)**2 (FOR MU = 0.7,&.0,1.4)

N,C OR S					
ADVANCE RATIO, MU = 0.25					
		(0.0)R			
0	.3324+05				
1-S,C	.2386+05	.1356+04	.5822+03	.7120+02	.3593+02
1-S,S	.8538+04	-.5916+03	.3211+03	.2764+02	.1384+02
		(0.14)R			
0	.5288+04				
1-S,C	.3300+04	.1981+03	.2434+02	.3682+01	-.3680+01
1-S,S	.1585+04	-.1318+03	.3373+02	.3764+01	-.4219+00
		(0.325)R			
0	.1257+04				
1-S,C	-.1803+03	.8348+02	-.1241+03	-.1582+02	-.1463+02
1-S,S	.8859+03	-.1096+03	-.5684+02	-.3031+01	-.4265+01
		(0.55)R			
0	.4034+03				
1-S,C	-.7110+03	.3030+03	-.1175+03	-.2290+02	.2083+01
1-S,S	.8758+03	-.1056+03	-.1729+03	-.1277+02	-.7697+00
		(0.75)R			
0	-.4458+03				
1-S,C	-.7010+03	.4227+03	-.4189+02	-.1862+02	.2133+02
1-S,S	.5064+03	-.5275+02	-.2177+03	-.1742+02	.3958+01
		(0.85)R			
0	-.4317+03				
1-S,C	-.4238+03	.2828+03	-.1084+02	-.1053+02	.1685+02
1-S,S	.2408+03	-.2215+02	-.1422+03	-.1159+02	.3336+01

N,C OR S					
ADVANCE RATIO, MU = 0.4					
		(0.0)R			
0	.3681+05				
1-S,C	.3989+05	.3432+04	.2489+04	.4447+03	.1781+03
1-S,S	.1323+05	-.1257+04	.1331+04	.2797+03	.2563+03
		(0.14)R			
0	.5704+04				
1-S,C	.5514+04	.4925+03	.1117+03	.4084+02	-.1166+02
1-S,S	.2564+04	-.3351+03	.1654+03	.2318+02	-.1090+02
		(0.325)R			
0	.1054+04				
1-S,C	-.3086+03	.1997+03	-.5157+03	-.7737+02	-.6274+02
1-S,S	.1632+04	-.3710+03	-.1990+03	-.4567+02	-.8297+02
		(0.55)R			
0	.1202+03				
1-S,C	-.1195+04	.7843+03	-.5394+03	-.1884+03	.2562+01
1-S,S	.1674+04	-.4183+03	-.7542+03	-.8310+02	-.9462+01
		(0.75)R			
0	-.6345+03				
1-S,C	-.1174+04	.1113+04	-.2594+03	-.2044+03	.8111+02
1-S,S	.1006+04	-.2717+03	-.1008+04	-.8287+02	.8601+02
		(0.85)R			
0	-.5299+03				
1-S,C	-.7089+03	.7473+03	-.1040+03	-.1380+03	.6511+02
1-S,S	.4869+03	-.1383+03	-.6679+03	-.5009+02	.7143+02

N,C OR S					
ADVANCE RATIO, MU = 0.5					
		(0.0)R			
0	.4001+05				
1-S,C	.5124+05	.5415+04	.4793+04	.1122+04	.7611+03
1-S,S	.1541+05	-.1518+04	.1695+04	.6541+03	.2606+03
		(0.14)R			
0	.6032+04				
1-S,C	.7061+04	.7478+03	.2417+03	.7490+02	-.9448+02
1-S,S	.3098+04	-.5216+03	.2913+03	-.1436+02	-.7565+01
		(0.325)R			
0	.7756+03				
1-S,C	-.4440+03	.2405+03	-.1006+04	-.2379+03	-.3331+03
1-S,S	.2203+04	-.7635+03	-.1834+03	-.2047+03	-.8845+02
		(0.55)R			
0	-.2327+03				
1-S,C	-.1585+04	.1130+04	-.1223+04	-.4483+03	.6913+02
1-S,S	.2445+04	-.1016+04	-.1279+04	-.9876+02	-.5613+02
		(0.75)R			
0	-.8559+03				
1-S,C	-.1535+04	.1665+04	-.7907+03	-.4433+03	.5213+03
1-S,S	.1640+04	-.8064+03	-.1901+04	.8630+02	.1484+02
		(0.85)R			
0	-.6395+03				
1-S,C	-.9229+03	.1126+04	-.3999+03	-.2719+03	.4082+03
1-S,S	.8517+03	-.4540+03	-.1287+04	.8918+02	.2276+02

N,C OR S					
ADVANCE RATIO, MU = 0.7					
		(0.0)R			
0	.4018+05				
1-S,C	.7639+05	.1444+05	.1849+05	.7188+04	.4687+04
1-S,S	.1592+05	-.2186+04	.1922+04	.2994+03	-.3629+04
		(0.14)R			
0	.6951+04				
1-S,C	.1335+05	.2190+04	.1695+04	.2964+03	-.4216+03
1-S,S	.4212+04	-.1028+04	.6281+03	-.3891+02	.5984+03
		(0.325)R			
0	-.2612+03				
1-S,C	-.1204+03	-.3608+03	-.4195+04	-.2118+04	-.2084+04
1-S,S	.3369+04	-.1737+04	.4143+02	-.1031+03	.1862+04
		(0.55)R			
0	-.1420+04				
1-S,C	-.2075+04	.6290+03	-.6818+04	-.2326+04	.5650+02
1-S,S	.3698+04	-.2715+04	-.2053+04	.2273+03	-.1081+04
		(0.75)R			
0	-.1233+04				
1-S,C	-.1772+04	.1620+04	-.5899+04	-.1228+04	.2488+04
1-S,S	.2425+04	-.2485+04	-.3213+04	.4710+03	-.3671+04
		(0.85)R			
0	-.6954+03				
1-S,C	-.9887+03	.1149+04	-.3370+04	-.5420+03	.1886+04
1-S,S	.1235+04	-.1388+04	-.2128+04	.3249+03	-.2663+04

N,C OR S					
ADVANCE RATIO, MU = 1.0					
		(0.0)R			
0	.5533+05				
1-S,C	.1180+06	.2386+05	.4088+05	.1036+05	.9531+03
1-S,S	.1744+05	-.1570+03	-.4218+04	-.9236+03	-.2159+04
		(0.14)R			
0	.1134+05				
1-S,C	.2609+05	.5118+04	.5810+04	.3979+03	.1183+03
1-S,S	.6373+04	-.1844+04	.2798+03	-.3898+03	.1167+04
		(0.325)R			
0	-.2014+04				
1-S,C	.2256+03	-.2116+03	-.9189+04	-.3576+04	-.3570+03
1-S,S	.5646+04	-.4334+04	.2629+04	.3889+03	.2146+04
		(0.55)R			
0	-.4396+04				
1-S,C	-.3686+04	-.7374+03	-.1704+05	-.2095+04	-.8794+03
1-S,S	.5256+04	-.5418+04	.2659+04	.2949+04	-.2842+04
		(0.75)R			
0	-.2939+04				
1-S,C	-.2379+04	-.2256+03	-.1497+05	.6585+03	-.9084+03
1-S,S	.2660+04	-.3680+04	.1215+04	.3847+04	-.5608+04
		(0.85)R			
0	-.1468+04				
1-S,C	-.1136+04	-.4280+02	-.8263+04	.8164+03	-.5291+03
1-S,S	.1168+04	-.1882+04	.4844+03	.2387+04	-.3770+04

N,C OR S					
ADVANCE RATIO, MU = 1.4					
		(0.0)R			
0	.8672+05				
1-S,C	.1318+06	.1523+05	.4012+05	.1432+04	-.2621+04
1-S,S	.1906+05	.7606+04	-.3353+05	-.5510+04	.4686+04
		(0.14)R			
0	.2279+05				
1-S,C	.3367+05	.5586+04	.8953+04	-.1156+04	.8362+03
1-S,S	.9919+04	-.2052+04	-.4546+04	-.1536+04	.1347+04
		(0.325)R			
0	-.2028+04				
1-S,C	-.3631+04	.3186+04	-.6787+04	-.9240+03	.2085+04
1-S,S	.9802+04	-.8365+04	.1192+05	.2123+04	-.1781+03
		(0.55)R			
0	-.7426+04				
1-S,C	-.8516+04	.2187+04	-.1598+05	.6171+04	-.1876+04
1-S,S	.7283+04	-.6969+04	.1867+05	.9012+04	-.1485+04
		(0.75)R			
0	-.4840+04				
1-S,C	-.3218+04	.8854+03	-.1406+05	.9019+04	-.4269+04
1-S,S	.2187+04	-.1953+04	.1367+05	.9973+04	-.1539+04
		(0.85)R			
0	-.2344+04				
1-S,C	-.1011+04	.3360+03	-.7733+04	.5543+04	-.2770+04
1-S,S	.5568+03	-.4158+03	.7091+04	.5822+04	-.8933+03

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 5.
BLADE TWIST TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(F) MP = 0.3
FP = 0.01 (FOR MU = 0.25,0.4,0.5)
FP = 0.00447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S — ADVANCE RATIO, MU = 0.25

(0.0)R

0	.1800+05				
1-S,C	.1372+05	.9487+03	.3644+03	.4040+02	.6424+01
1-S,S	.3827+04	-.6884+03	-.1664+03	-.3429+02	.4581+01

(0.14)R

0	.7168+04				
1-S,C	.5139+04	.3650+03	.8531+02	.1122+02	.1792+01
1-S,S	.1808+04	-.2904+03	-.2753+02	-.5692+01	.1002+01

(0.325)R

0	.2483+04				
1-S,C	.1223+04	.1521+03	-.8592+02	-.8089+01	-.1522+01
1-S,S	.1166+04	-.1450+03	.5437+02	.1534+02	-.6335-00

(0.55)R

0	.7173+03				
1-S,C	-.4489+02	.1906+03	-.1434+03	-.2080+02	-.4230+01
1-S,S	.9124+03	-.1036+03	.5517+02	.2685+02	.2687+00

(0.75)R

0	-.1056+01				
1-S,C	-.2329+03	.1718+03	-.9344+02	-.1743+02	-.3730+01
1-S,S	.4620+03	-.5619+02	.1885+02	.1983+02	.1035+01

(0.85)R

0	-.6996+02				
1-S,C	-.1381+03	.9461+02	-.4552+02	-.9265+01	-.2012+01
1-S,S	.2060+03	-.2621+02	.5813+01	.1016+02	.6781-00

N,C OR S — ADVANCE RATIO, MU = 0.4

(0.0)R

0	.2081+05				
1-S,C	.2346+05	.2643+04	.1636+04	.2742+03	.5786+02
1-S,S	.6453+04	-.1741+04	-.6797+03	-.2933+03	-.4053+01

(0.14)R

0	.8071+04				
1-S,C	.8779+04	.9976+03	.3858+03	.7886+02	.1079+02
1-S,S	.3097+04	-.7610+03	-.9514+02	-.4884+02	.1593+01

(0.325)R

0	.2554+04				
1-S,C	.2065+04	.3774+03	-.3846+03	-.5056+02	-.1718+02
1-S,S	.2111+04	-.4067+03	.2468+03	.1306+03	.1303+02

(0.55)R

0	.5302+03				
1-S,C	-.6916+02	.4721+03	-.6565+03	-.1364+03	-.1990+02
1-S,S	.1722+04	-.2937+03	.2169+03	.2238+03	.3168+02

(0.75)R

0	-.1452+03				
1-S,C	-.3843+03	.4405+03	-.4358+03	-.1157+03	-.8711+01
1-S,S	.8975+03	-.1525+03	.4838+02	.1629+03	.2905+02

(0.85)R

0	-.1422+03				
1-S,C	-.2270+03	.2449+03	-.2139+03	-.6167+02	-.3404+01
1-S,S	.4054+03	-.6945+02	.5270+01	.8301+02	.1588+02

N,C OR S — ADVANCE RATIO, MU = 0.5

(0.0)R

0	.2283+05				
1-S,C	.3104+05	.4677+04	.3186+04	.7366+03	.6513+02
1-S,S	.8165+04	-.2727+04	-.1617+04	-.6710+03	-.6332+02

(0.14)R

0	.8866+04				
1-S,C	.1100+05	.1713+04	.7638+03	.1919+03	.1903+02
1-S,S	.3967+04	-.1215+04	-.2281+03	-.1356+03	.1468+02

(0.325)R

0	.2534+04				
1-S,C	.2728+04	.5316+03	-.7305+03	-.1574+03	-.9005+01
1-S,S	.2863+04	-.7025+03	.6004+03	.2761+03	.6712+02

(0.55)R

0	.2880+03				
1-S,C	-.1125+03	.6307+03	-.1283+04	-.3428+03	-.2408+02
1-S,S	.2561+04	-.3703+03	.5763+03	.5771+03	.4717+02

(0.75)R

0	-.3147+03				
1-S,C	-.5119+03	.6287+03	-.8682+03	-.2658+03	-.1948+02
1-S,S	.1397+04	-.3258+03	.1793+03	.4693+03	.5061+01

(0.85)R

0	-.2225+03				
1-S,C	-.3009+03	.3558+03	-.4293+03	-.1379+03	-.1023+02
1-S,S	.6467+03	-.1544+03	.4888+02	.2477+03	-.2486+01

N,C OR S — ADVANCE RATIO, MU = 0.7

(0.0)R

0	.2415+05				
1-S,C	.4816+05	.1169+05	.7629+04	.9179+03	-.1225+03
1-S,S	.8059+04	-.7896+04	-.8613+04	-.4252+04	-.9233+03

(0.14)R

0	.9921+04				
1-S,C	.2029+05	.4562+04	.2218+04	.2537+03	.4737+02
1-S,S	.4715+04	-.3624+04	-.1943+04	-.9829+03	.1596+02

(0.325)R

0	.2356+04				
1-S,C	.5919+04	.9970+03	-.1444+04	.2161+02	.1474+03
1-S,S	.4024+04	-.1662+04	.2759+04	.1593+04	.5849+03

(0.55)R

0	-.4413+03				
1-S,C	.8138+03	.5991+03	-.2967+04	.4219+03	.3566+02
1-S,S	.3756+04	-.9636+03	.4314+04	.3095+04	.2623+03

(0.75)R

0	-.6908+03				
1-S,C	-.2203+03	.7264+03	-.2047+04	.5398+03	-.6738+02
1-S,S	.2143+04	-.4664+03	.2669+04	.2299+04	-.1510+03

(0.85)R

0	-.3783+03				
1-S,C	-.1765+03	.4324+03	-.1012+04	.3139+03	-.4960+02
1-S,S	.1004+04	-.2096+03	.1268+04	.1170+04	-.1336+03

N,C OR S — ADVANCE RATIO, MU = 1.0

(0.0)R

0	.3272+05				
1-S,C	.6956+05	.1671+05	.5361+04	-.6477+04	.3131+03
1-S,S	.1285+05	-.1193+05	-.1319+05	.4173+04	.5220+04

(0.14)R

0	.1417+05				
1-S,C	.3325+05	.7637+04	.2517+04	-.1512+04	.2638+03
1-S,S	.7959+04	-.6599+04	-.3118+04	.1050+04	.1508+04

(0.325)R

0	.2304+04				
1-S,C	.1165+05	.2525+04	.8919+03	.3440+04	.2586+03
1-S,S	.6068+04	-.4022+04	.5036+04	-.1244+04	-.1504+04

(0.55)R

0	-.2268+04				
1-S,C	.3079+04	.1462+04	.3984+03	.7307+04	.1325+03
1-S,S	.4704+04	-.2772+04	.8171+04	-.1693+04	-.2960+04

(0.75)R

0	-.1831+04				
1-S,C	.6420+03	.1187+04	.2472+03	.5641+04	.4645+01
1-S,S	.2310+04	-.1374+04	.5122+04	-.8303+03	-.2033+04

(0.85)R

0	-.8942+03				
1-S,C	.1936+03	.6463+03	.1271+03	.2886+04	-.1134+02
1-S,S	.1015+04	-.6140+03	.2435+04	-.3498+03	-.9986+03

N,C OR S — ADVANCE RATIO, MU = 1.4

(0.0)R

0	.5862+05				
1-S,C	.9558+05	.2687+05	.1905+04	.4427+04	.9519+04
1-S,S	.3659+05	-.1200+05	-.1179+05	.2643+05	.8390+04

(0.14)R

0	.2871+05				
1-S,C	.4976+05	.1344+05	.3366+04	.1363+04	.2681+04
1-S,S	.2208+05	-.7832+04	-.2188+04	.7557+04	.2640+04

(0.325)R

0	.6868+04				
1-S,C	.1812+05	.4928+04	.5156+04	-.3686+03	-.3728+04
1-S,S	.1396+05	-.3807+04	.6517+04	-.8873+04	-.2340+04

(0.55)R

0	-.2770+04				
1-S,C	.3661+04	.1617+04	.4515+04	.8169+03	-.6601+04
1-S,S	.8123+04	-.3866+04	.9588+04	-.1524+05	-.4418+04

(0.75)R

0	-.2682+04				
1-S,C	.3110+03	.7932+03	.1966+04	.1467+04	-.4252+04
1-S,S	.3174+04	-.1760+04	.5658+04	-.9384+04	-.2784+04

(0.85)R

0	-.1328+04				
1-S,C	.6241+01	.3936+03	.7941+03	.8745+03	-.2032+04
1-S,S	.1258+04	-.7509+03	.2619+04	-.4349+04	-.1315+04

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 5.
BLADE TWIST TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(G) MP = 0.5
FP = 0.001 (FOR MU = 0.25,0.4,0.5)
FP = 0.000447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S		ADVANCE RATIO, MU = 0.25			
		(0.8)R			
0	.8166+05				
1-S,C	.3977+05	.1212+03	.9938+03	.8063+02	.2820+02
1-S,S	.2318+05	-.7653+03	.7280+03	.1033+03	.6468+02
		(0.14)R			
0	.3956+04				
1-S,C	.1466+04	.1292+03	-.6372+02	.8459+01	-.6788+01
1-S,S	.1530+04	-.2406+03	.2804+02	-.1275+02	-.8294+01
		(0.325)R			
0	.1360+04				
1-S,C	-.1364+04	.4416+03	-.2041+03	-.3856+01	-.4464+01
1-S,S	.1079+04	-.1993+03	-.1086+03	-.1112+02	-.1862+02
		(0.55)R			
0	.1400+04				
1-S,C	-.2708+04	.9251+03	-.4312+02	-.4089+02	.7816+01
1-S,S	.1019+04	.2639+03	-.3662+03	-.1438+02	-.2722+01
		(0.75)R			
0	-.1900+04				
1-S,C	-.2304+04	.1042+04	.2823+03	-.5883+02	-.1506+02
1-S,S	.1961+03	.3776+03	-.4714+03	-.1267+03	.1832+02
		(0.85)R			
0	-.2661+04				
1-S,C	-.1277+04	.7179+03	.2968+03	-.4385+02	-.2250+02
1-S,S	-.1367+03	.2226+03	-.3356+03	-.1292+03	.1803+02

N,C OR S		ADVANCE RATIO, MU = 0.4			
		(0.8)R			
0	.8549+05				
1-S,C	.6470+05	-.1143+04	.3827+04	.2317+03	.9860+02
1-S,S	.3075+05	-.1469+04	.2346+04	.5643+03	.6672+03
		(0.14)R			
0	.3873+04				
1-S,C	.2418+04	.2186+03	-.2102+03	.9160+02	-.5271+02
1-S,S	.2278+04	-.6761+03	.1811+03	-.1142+03	-.9310+02
		(0.325)R			
0	.7798+03				
1-S,C	-.2098+04	.1168+04	-.8062+03	.9144+02	.1741+02
1-S,S	.2110+04	-.7478+03	-.2628+03	-.7078+02	-.2134+03
		(0.55)R			
0	.9509+03				
1-S,C	-.4157+04	.2654+04	-.3556+03	-.2814+03	.9142+02
1-S,S	.2229+04	.2978+03	-.1494+04	.1783+02	-.9369+01
		(0.75)R			
0	-.2071+04				
1-S,C	-.3469+04	.2914+04	.9274+03	-.7897+03	-.3178+03
1-S,S	.6639+03	.6478+03	-.2300+04	-.6724+03	.3238+03
		(0.85)R			
0	-.2701+04				
1-S,C	-.1907+04	.1954+04	.1072+04	-.6982+03	-.4065+03
1-S,S	-.1056+03	.3836+03	-.1752+04	-.7799+03	.3212+03

N,C OR S		ADVANCE RATIO, MU = 0.5			
		(0.8)R			
0	.8557+05				
1-S,C	.8266+05	-.2711+04	.6375+04	-.1074+03	.4506+03
1-S,S	.3042+05	-.1737+04	.2831+04	.2029+04	.2496+04
		(0.14)R			
0	.4169+04				
1-S,C	.2509+04	.4637+03	-.3638+03	.2724+03	-.7028+02
1-S,S	.2694+04	-.7383+03	.3690+03	-.2154+03	-.3445+03
		(0.325)R			
0	.4595+03				
1-S,C	-.3010+04	.1751+04	-.1264+04	.3689+03	-.1569+03
1-S,S	.2971+04	-.1312+04	-.4665+02	-.5939+03	-.7964+03
		(0.55)R			
0	-.4233+03				
1-S,C	-.4379+04	.3627+04	-.6111+03	-.6261+03	.9283+01
1-S,S	.3282+04	-.7783+03	-.2352+04	-.2803+03	.2337+02
		(0.75)R			
0	-.1749+04				
1-S,C	-.4325+04	.4817+04	.8454+03	-.1968+04	.2887+03
1-S,S	.1962+04	.5730+03	-.4991+04	.4129+03	.1414+04
		(0.85)R			
0	-.1598+04				
1-S,C	-.2914+04	.3640+04	.1030+04	-.1759+04	.2834+03
1-S,S	.9190+03	.3116+03	-.4212+04	.4972+03	.1395+04

N,C OR S		ADVANCE RATIO, MU = 0.7			
		(0.8)R			
0	.7749+05				
1-S,C	.1105+06	.3346+04	.2130+05	.9832+04	.1288+05
1-S,S	.2050+05	.3449+04	.4646+04	.9383+04	.6116+04
		(0.14)R			
0	.3935+04				
1-S,C	.5904+04	.5929+03	.2314+03	-.8492+03	-.1744+04
1-S,S	.3235+04	-.1518+04	.8481+03	-.1471+04	-.4914+03
		(0.325)R			
0	-.2160+04				
1-S,C	-.3977+04	.1471+04	-.3745+04	-.1914+04	-.4535+04
1-S,S	.4288+04	-.3333+04	.3059+02	-.3295+04	-.2226+04
		(0.55)R			
0	-.2017+04				
1-S,C	-.5568+04	.4085+04	-.6244+04	-.1117+04	.4383+03
1-S,S	.4734+04	-.3546+04	-.4836+04	.3771+03	-.7864+03
		(0.75)R			
0	-.2221+04				
1-S,C	-.3591+04	.5983+04	-.5031+04	-.3425+04	.8153+04
1-S,S	.2747+04	-.3957+04	-.1095+05	.4323+04	.3992+04
		(0.85)R			
0	-.1708+04				
1-S,C	-.1675+04	.4458+04	-.2785+04	-.3366+04	.7480+04
1-S,S	.1255+04	-.2950+04	-.8065+04	.3739+04	.4168+04

N,C OR S		ADVANCE RATIO, MU = 1.0			
		(0.8)R			
0	.9178+05				
1-S,C	.1582+06	.5114+04	.4597+05	.2321+05	.2560+05
1-S,S	.8924+04	.1694+05	-.2441+04	.1582+05	.2225+04
		(0.14)R			
0	.6023+04				
1-S,C	.1186+05	.2156+04	.2578+04	-.2222+04	-.2670+04
1-S,S	.4868+04	-.2431+04	.2213+04	-.2299+04	.3219+03
		(0.325)R			
0	-.6298+04				
1-S,C	-.8227+04	.2974+04	-.7884+04	-.7039+04	-.1064+05
1-S,S	.7477+04	-.7075+04	.2682+04	-.6234+04	.5640+03
		(0.55)R			
0	-.6066+04				
1-S,C	-.8256+04	.2422+04	-.1636+05	-.1027+04	-.4196+02
1-S,S	.5498+04	-.5792+04	-.4317+04	.1633+04	-.2082+04
		(0.75)R			
0	-.3439+04				
1-S,C	-.3842+04	.2038+04	-.1539+05	.3654+04	.2015+05
1-S,S	.2434+04	-.5994+04	-.8489+04	.1089+05	-.7664+04
		(0.85)R			
0	-.1719+04				
1-S,C	-.1494+04	.1377+04	-.9162+04	.2950+04	.1799+05
1-S,S	.1107+04	-.4386+04	-.6026+04	.8953+04	-.6465+04

N,C OR S		ADVANCE RATIO, MU = 1.4			
		(0.8)R			
0	.1328+06				
1-S,C	.1792+06	-.1986+05	.3623+05	.8283+04	.1180+04
1-S,S	.3833+05	-.1741+04	-.4906+05	.1216+05	-.1907+05
		(0.14)R			
0	.1255+05				
1-S,C	.1544+05	.1691+04	.6370+04	-.2525+04	.1360+04
1-S,S	.7950+04	-.3204+04	.2194+04	-.2388+04	.3165+04
		(0.325)R			
0	-.1045+05				
1-S,C	-.1941+05	.9697+04	-.3543+04	-.3628+04	-.1247+04
1-S,S	.1299+05	-.1234+05	.1498+05	-.6580+04	.1031+05
		(0.55)R			
0	-.6937+04				
1-S,C	-.1457+05	.7399+04	-.1567+05	.6918+04	-.2291+04
1-S,S	.5490+04	-.3312+04	.6809+04	.5650+04	-.2613+04
		(0.75)R			
0	-.4439+04				
1-S,C	-.3345+04	-.7581+02	-.1440+05	.1182+05	.6787+04
1-S,S	.1633+04	-.1462+04	.4885+04	.1985+05	-.1883+05
		(0.85)R			
0	-.2869+04				
1-S,C	-.2550+03	-.1556+04	-.7884+04	.7789+04	.6738+04
1-S,S	.1012+04	-.1589+04	.3646+04	.1442+05	-.1485+05

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 5.
BLADE TWIST TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(M) MP = 0.5
FP = 0.0025 (FOR MU = 0.25,0.4,0.5)
FP = 0.00112(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S	ADVANCE RATIO, MU = 0.25			
	(0.0)R			
0 .5575+05				
1-S,C .2835+05	.4392+03	.8470+03	.1261+03	.4090+02
1-S,S .1614+05	-.3956+03	.4898+03	.3072+02	.2675+02
	(0.14)R			
0 .8838+04				
1-S,C .3568+04	.1993+03	.1229+02	.1113+02	-.2829+01
1-S,S .2869+04	-.2040+03	.5256+02	.5598+01	-.1795+01
	(0.325)R			
0 .2041+04				
1-S,C -.1110+04	.4171+03	-.2096+03	-.2355+02	-.1525+02
1-S,S .1379+04	-.2092+03	-.9953+02	-.4611+01	-.1020+02
	(0.55)R			
0 .6235+03				
1-S,C -.2128+04	.8041+03	-.1199+03	-.5675+02	-.2564+01
1-S,S .1126+04	.8300+01	-.3310+03	-.3157+02	-.3116+01
	(0.75)R			
0 -.7529+03				
1-S,C -.1911+04	.8526+03	.5903+02	-.6539+02	.1435+02
1-S,S .4444+03	.2564+03	-.4293+03	-.4695+02	.7253+01
	(0.85)R			
0 -.7205+03				
1-S,C -.1125+04	.9525+03	.7128+02	-.4178+02	.1211+02
1-S,S .1401+03	.2056+03	-.2824+03	-.3179+02	.6477+01

N,C OR S	ADVANCE RATIO, MU = 0.4			
	(0.0)R			
0 .5947+05				
1-S,C .4624+05	.1115+02	.3370+04	.6978+03	.4043+03
1-S,S .2220+05	-.8891+03	.1820+04	.2120+03	.4351+03
	(0.14)R			
0 .9159+04				
1-S,C .5863+04	.3670+03	.5232+02	.9162+02	-.3676+02
1-S,S .4265+04	-.5414+03	.2575+03	.8029+01	-.4654+02
	(0.325)R			
0 .1661+04				
1-S,C -.1694+04	.1130+04	-.8542+03	-.9883+02	-.1626+03
1-S,S .2595+04	-.8056+03	-.3056+03	-.6648+02	-.1848+03
	(0.55)R			
0 .1601+03				
1-S,C -.3280+04	.2251+04	-.5972+03	-.4084+03	-.4510+01
1-S,S .2272+04	-.3580+03	-.1431+04	-.1332+03	.5911+01
	(0.75)R			
0 -.9600+03				
1-S,C -.2938+04	.2418+04	.5794+02	-.5572+03	.1909+03
1-S,S .1008+04	.3513+03	-.2007+04	-.1410+03	.2351+03
	(0.85)R			
0 -.7968+03				
1-S,C -.1727+04	.1516+04	.1640+03	-.3707+03	.1553+03
1-S,S .3795+03	.3538+03	-.1344+04	-.8801+02	.1890+03

N,C OR S	ADVANCE RATIO, MU = 0.5			
	(0.0)R			
0 .6141+05				
1-S,C .5817+05	-.2494+03	.6275+04	.1960+04	.1861+04
1-S,S .2304+05	.1348+03	.2492+04	.1132+04	.9106+03
	(0.14)R			
0 .9155+04				
1-S,C .7334+04	.4607+03	.1783+03	.1596+03	-.2135+03
1-S,S .4726+04	-.7271+03	.5364+03	-.1082+03	-.7394+02
	(0.325)R			
0 .9947+03				
1-S,C -.2165+04	.1592+04	-.1532+04	-.3831+03	-.7978+03
1-S,S .3413+04	-.1593+04	-.2278+03	-.4696+03	-.3598+03
	(0.55)R			
0 -.4304+03				
1-S,C -.4049+04	.3327+04	-.1487+04	-.9192+03	.1065+03
1-S,S .3454+04	-.1345+04	-.2547+04	-.9944+02	-.5090+02
	(0.75)R			
0 -.1203+04				
1-S,C -.3502+04	.3664+04	-.5882+03	-.1059+04	.1150+04
1-S,S .1971+04	-.3494+03	-.3960+04	.4063+03	.3542+03
	(0.85)R			
0 -.8777+03				
1-S,C -.2031+04	.2313+04	-.1843+03	-.6763+03	.9097+03
1-S,S .9239+03	-.1994+02	-.2784+04	.3481+03	.2965+03

N,C OR S	ADVANCE RATIO, MU = 0.7			
	(0.0)R			
0 .5591+05				
1-S,C .8277+05	.8089+04	.2158+05	.1095+05	.8779+04
1-S,S .1760+05	.1099+04	.1702+03	-.1159+04	-.5962+04
	(0.14)R			
0 .9331+04				
1-S,C .1340+05	.1688+04	.2007+04	.3843+03	-.7255+03
1-S,S .5249+04	-.1171+04	.9139+03	-.4317+03	.8206+03
	(0.325)R			
0 -.1031+04				
1-S,C -.2540+04	.1181+04	-.4852+04	-.3376+04	-.3864+04
1-S,S .4965+04	-.3278+04	.7328+03	-.8443+02	.2903+04
	(0.55)R			
0 -.2340+04				
1-S,C -.4763+04	.2943+04	-.8437+04	-.3525+04	-.1301+03
1-S,S .5073+04	-.4143+04	-.3436+04	.1375+04	-.1154+04
	(0.75)R			
0 -.1574+04				
1-S,C -.3253+04	.3463+04	-.7568+04	-.1680+04	.4102+04
1-S,S .2865+04	-.2921+04	-.6142+04	.2214+04	-.5023+04
	(0.85)R			
0 -.7935+03				
1-S,C -.1664+04	.2169+04	-.4378+04	-.6809+03	.3201+04
1-S,S .1351+04	-.1537+04	-.4155+04	.1474+04	-.3688+04

N,C OR S	ADVANCE RATIO, MU = 1.0			
	(0.0)R			
0 .7131+05				
1-S,C .1194+06	.1278+05	.3895+05	.1447+05	.2252+04
1-S,S .1553+05	.6387+04	-.9287+04	-.3004+04	-.6456+04
	(0.14)R			
0 .1385+05				
1-S,C .2404+05	.3960+04	.6111+04	.2527+03	.2260+03
1-S,S .7062+04	-.1767+04	.2425+03	-.1279+04	.1636+04
	(0.325)R			
0 -.4022+04				
1-S,C -.4600+04	.2477+04	-.7905+04	-.5238+04	-.6875+03
1-S,S .7744+04	-.6869+04	.4163+04	.1754+03	.4372+04
	(0.55)R			
0 -.6253+04				
1-S,C -.7494+04	.1885+04	-.1703+05	-.1828+04	-.1055+04
1-S,S .6171+04	-.6676+04	.1689+04	.5111+04	-.2904+04
	(0.75)R			
0 -.3279+04				
1-S,C -.3236+04	.0985+03	-.1594+05	.2730+04	-.8048+03
1-S,S .1933+04	-.2967+04	-.1770+04	.7184+04	-.8499+04
	(0.85)R			
0 -.1424+04				
1-S,C -.1179+04	.2299+03	-.9133+04	.2389+04	-.4306+03
1-S,S .4795+03	-.1112+04	-.1575+04	.4460+04	-.5838+04

N,C OR S	ADVANCE RATIO, MU = 1.4			
	(0.0)R			
0 .1188+06				
1-S,C .1521+06	.1197+05	.3132+05	.4848+04	-.1016+05
1-S,S .4263+05	.3311+04	-.3638+05	-.6350+04	.6300+04
	(0.14)R			
0 .3022+05				
1-S,C .3412+05	.6247+04	.8748+04	-.1641+04	.1075+04
1-S,S .1873+05	-.3832+04	-.4730+04	-.3308+04	.1180+04
	(0.325)R			
0 -.4367+04				
1-S,C -.1323+05	.0989+04	-.1418+04	-.2010+04	.6312+04
1-S,S .1403+05	-.7393+04	.1237+05	.5733+03	-.6645+03
	(0.55)R			
0 -.1012+05				
1-S,C -.1372+05	.7750+04	-.8694+04	.1076+05	.8224+03
1-S,S .8502+04	.9966+03	.1758+05	.1268+05	.4676+03
	(0.75)R			
0 -.5234+04				
1-S,C -.1305+04	.4892+04	-.9153+04	.1616+05	-.4583+04
1-S,S .9193+03	.7641+04	.1158+05	.1611+05	.1418+04
	(0.85)R			
0 -.2228+04				
1-S,C .1079+04	.2405+04	-.5266+04	.9971+04	-.3371+04
1-S,S -.4942+03	.5283+04	.5755+04	.9665+04	.9434+03

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 5.
BLADE TWIST TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(I) MR = 0.5
FP = 0.01 (FOR MU = 0.25,0.4,0.5)
FP = 0.00447(1+MU)**2 (FOR MU = 0.7,0.9,1.1,1.4)

N,C OR S		ADVANCE RATIO, MU = 0.25			
		(0.0)R			
0	.3049+05				
1-5,C	.1603+05	.9201+03	.6188+03	.8226+02	.1943+02
1-5,S	.8692+04	-.5466+03	-.1504+03	-.9068+02	-.7587+01
		(0.14)R			
0	.1212+05				
1-5,C	.5661+04	.4349+03	.1342+03	.2673+02	.7311+01
1-5,S	.3861+04	-.3180+03	-.1857+02	-.1419+02	.9577+00
		(0.325)R			
0	.4159+04				
1-5,C	.6594+03	.3556+03	-.1635+03	-.9674+01	.1856+01
1-5,S	.2157+04	-.2576+03	.3721+02	.3729+02	.7877+01
		(0.55)R			
0	.1173+04				
1-5,C	-.1052+04	.4872+03	-.2473+03	-.3974+02	.1747+00
1-5,S	.1462+04	-.1609+03	-.3188+02	.5499+02	.9698+01
		(0.75)R			
0	-.1827+02				
1-5,C	-.9325+03	.3842+03	-.1503+03	-.3729+02	-.1293+01
1-5,S	.6620+03	-.3639+02	-.7349+02	.3594+02	.5694+01
		(0.85)R			
0	-.1245+03				
1-5,C	-.4875+03	.2026+03	-.7112+02	-.2042+02	-.8834+01
1-5,S	.2796+03	-.5420+01	-.4646+02	.1711+02	.2671+01

N,C OR S		ADVANCE RATIO, MU = 0.4			
		(0.0)R			
0	.3390+05				
1-5,C	.2670+05	.2308+04	.2698+04	.4577+03	.7783+02
1-5,S	.1331+05	-.1059+04	-.6862+03	-.7019+03	-.1310+03
		(0.14)R			
0	.1325+05				
1-5,C	.9501+04	.1063+04	.5699+03	.1390+03	.4955+01
1-5,S	.6132+04	-.7573+03	-.6821+02	-.1397+03	-.2452+02
		(0.325)R			
0	.4145+04				
1-5,C	.1144+04	.8437+03	-.7718+03	-.9357+02	-.3375+02
1-5,S	.3726+04	-.8258+03	.1979+03	.2460+03	.5066+02
		(0.55)R			
0	.8500+03				
1-5,C	-.1664+04	.1203+04	-.1287+04	-.3120+03	-.1068+02
1-5,S	.2709+04	-.8144+03	-.1335+03	.4212+03	.8932+02
		(0.75)R			
0	-.2238+03				
1-5,C	-.1499+04	.9760+03	-.7705+03	-.2898+03	.1588+02
1-5,S	.1277+04	-.2010+03	-.3498+03	.2989+03	.6536+02
		(0.85)R			
0	-.2209+03				
1-5,C	-.7838+03	.5190+03	-.3726+03	-.1584+03	.1226+02
1-5,S	.5494+03	-.6192+02	-.2202+03	.1509+03	.3335+02

N,C OR S		ADVANCE RATIO, MU = 0.5			
		(0.0)R			
0	.3627+05				
1-5,C	.3467+05	.4126+04	.5314+04	.1101+04	.1449+03
1-5,S	.1558+05	-.1194+04	-.1882+04	-.1730+04	-.4477+03
		(0.14)R			
0	.1393+05				
1-5,C	.1230+05	.1761+04	.1183+04	.3045+03	.2748+01
1-5,S	.7316+04	-.1087+04	-.1952+03	-.3873+03	-.3402+02
		(0.325)R			
0	.3923+04				
1-5,C	.1460+04	.1143+04	-.1466+04	-.2444+03	-.6281+02
1-5,S	.4886+04	-.1460+04	.6492+03	.5817+03	.2206+03
		(0.55)R			
0	.4154+03				
1-5,C	-.2118+04	.1606+04	-.2529+04	-.6581+03	.1792+02
1-5,S	.3935+04	-.1259+04	.7707+02	.1224+04	.1920+03
		(0.75)R			
0	-.4695+03				
1-5,C	-.1861+04	.1346+04	-.1742+04	-.5595+03	.7593+02
1-5,S	.2057+04	-.5803+03	-.4832+03	.9814+03	.4934+02
		(0.85)R			
0	-.3318+03				
1-5,C	-.9681+03	.7233+03	-.8683+03	-.2998+03	.4975+02
1-5,S	.9179+03	-.2358+03	-.3415+03	.5156+03	.9283+01

N,C OR S		ADVANCE RATIO, MU = 0.7			
		(0.0)R			
0	.3571+05				
1-5,C	.2413+05	.1366+05	.1262+05	-.1184+02	-.8788+03
1-5,S	.1410+05	-.7256+04	-.1333+05	-.8372+04	-.2261+04
		(0.14)R			
0	.1449+05				
1-5,C	.2184+05	.5258+04	.3495+04	.5994+02	-.4275+02
1-5,S	.8107+04	-.4024+04	-.3094+04	-.2066+04	-.9248+02
		(0.325)R			
0	.3144+04				
1-5,C	.4496+04	.1489+04	-.2998+04	.4780+03	.5674+03
1-5,S	.6635+04	-.2892+04	.3871+04	.2783+04	.1188+04
		(0.55)R			
0	-.8785+03				
1-5,C	-.1436+04	.1123+04	-.6145+04	.1374+04	.6295+03
1-5,S	.5885+04	-.1966+04	.5706+04	.5540+04	.4890+03
		(0.75)R			
0	-.1054+04				
1-5,C	-.1534+04	.1088+04	-.4427+04	.1293+04	.2939+03
1-5,S	.3218+04	-.7611+03	.3257+04	.4117+04	-.3819+03
		(0.85)R			
0	-.5543+03				
1-5,C	-.7851+03	.6149+03	-.2225+04	.7048+03	.1219+03
1-5,S	.1461+04	-.2877+03	.1492+04	.2099+04	-.3172+03

N,C OR S		ADVANCE RATIO, MU = 1.0			
		(0.0)R			
0	.4710+05				
1-5,C	.7146+05	.1631+05	.8311+04	-.1067+05	.1260+04
1-5,S	.1922+05	-.8057+04	-.2283+05	.1643+04	.6193+04
		(0.14)R			
0	.2002+05				
1-5,C	.3249+05	.7844+04	.3555+04	-.2662+04	.7519+03
1-5,S	.1204+05	-.6082+04	-.5803+04	.1038+03	.1831+04
		(0.325)R			
0	.2597+04				
1-5,C	.8856+04	.3445+04	.2990+03	.5293+04	.4447+03
1-5,S	.9269+04	-.5849+04	.7533+04	-.8786+03	-.1940+04
		(0.55)R			
0	-.3836+04				
1-5,C	.2975+03	.2814+04	-.1352+04	.1163+05	.7428+02
1-5,S	.6840+04	-.4296+04	.1214+05	-.3706+03	-.4287+04
		(0.75)R			
0	-.2784+04				
1-5,C	-.4480+03	.2162+04	-.1157+04	.9077+04	-.1167+03
1-5,S	.3107+04	-.1655+04	.7347+04	.2576+03	-.3194+04
		(0.85)R			
0	-.1324+04				
1-5,C	-.2065+03	.1097+04	-.5965+03	.4657+04	-.8321+02
1-5,S	.1318+04	-.6286+03	.3439+04	.2144+03	-.1613+04

N,C OR S		ADVANCE RATIO, MU = 1.4			
		(0.0)R			
0	.7503+05				
1-5,C	.9376+05	.3072+05	.4149+03	-.7186+04	.1234+05
1-5,S	.4590+05	-.2069+04	-.2670+05	.3155+05	.1294+05
		(0.14)R			
0	.3538+05				
1-5,C	.4521+05	.1651+05	.4331+04	-.1709+04	.3638+04
1-5,S	.2955+05	-.3572+04	-.6640+04	.8626+04	.3854+04
		(0.325)R			
0	.6474+04				
1-5,C	.1059+05	.7268+04	.8243+04	.4939+04	-.4226+04
1-5,S	.1999+05	-.4917+04	.1039+05	-.1160+05	-.4370+04
		(0.55)R			
0	-.5072+04				
1-5,C	-.2833+04	.3527+04	.7213+04	.1122+05	-.7943+04
1-5,S	.1192+05	-.2985+04	.1525+05	-.1964+05	-.8314+04
		(0.75)R			
0	-.3716+04				
1-5,C	-.2310+04	.1827+04	.2932+04	.8787+04	-.5206+04
1-5,S	.4460+04	-.4377+03	.8369+04	-.1289+05	-.5481+04
		(0.85)R			
0	-.1716+04				
1-5,C	-.1066+04	.8688+03	.1128+04	.4486+04	-.2581+04
1-5,S	.1765+04	.5368+02	.3739+04	-.5673+04	-.2638+04

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 6.
INFLOW RATIO TRANSFER COEFFICIENTS FOR AN ARTICULATED BLADE

(A) MP = 0.1
FP = 0.001 (FOR MU = 0.25,0.4,0.5)
FP = 0.000447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S — ADVANCE RATIO, MU = 0.25

(0.0)R

0	.1287+05				
1-S,C	.1264+05	.6396+03	.1357+03	.1286+02	-.2823+03
1-S,S	-.6155+03	-.6876+03	.8778+02	.3611+02	-.1754+03

(0.14)R

0	.5755+03				
1-S,C	.5686+03	.2268+02	-.6806+01	-.6118+01	.2219+02
1-S,S	.9395+02	-.3416+02	-.1048+02	-.2836+02	.1293+02

(0.325)R

0	.3761+02				
1-S,C	-.1994+02	-.6839+01	-.2080+02	-.7629+01	.5631+02
1-S,S	.2707+03	-.8351+01	-.4819+02	-.4287+02	.3829+02

(0.55)R

0	-.4920+02				
1-S,C	-.6058+02	.2222+02	-.1640+02	-.1107+01	-.7895+01
1-S,S	.2990+03	-.1593+01	-.8355+02	-.1930+02	-.1857+02

(0.75)R

0	-.4521+03				
1-S,C	-.1115+03	.6158+02	-.1797+02	-.1845+02	-.1279+03
1-S,S	.1917+03	-.7426+01	-.6655+02	.3421+02	-.7944+02

(0.85)R

0	-.4677+03				
1-S,C	-.9199+02	.5434+02	-.1504+02	-.1275+02	-.1263+03
1-S,S	.9788+02	-.9309+01	-.3581+02	.4826+02	-.7135+02

N,C OR S — ADVANCE RATIO, MU = 0.4

(0.0)R

0	.1308+05				
1-S,C	.2118+05	.1549+04	.1478+03	-.1721+03	-.6911+02
1-S,S	.6672+03	-.5960+03	.1983+03	-.1853+03	-.1812+03

(0.14)R

0	.5599+03				
1-S,C	.9507+03	.4661+02	-.4639-00	.1725+02	-.3150+01
1-S,S	.2116+03	-.3348+02	.1432+02	-.6186+01	.7628+01

(0.325)R

0	.3926+01				
1-S,C	-.3631+02	-.3644+02	-.2129+02	.3830+02	.1114+01
1-S,S	.4363+03	-.3452+02	-.3488+02	-.7398-00	.2678+02

(0.55)R

0	-.7810+02				
1-S,C	-.1077+03	.5547+02	-.2882+02	-.1579+02	.1687+01
1-S,S	.5256+03	-.7835+02	-.1446+03	-.7431+01	-.5571+01

(0.75)R

0	-.4763+03				
1-S,C	-.1487+03	.2141+03	-.1085+02	-.8795+02	-.2561+01
1-S,S	.3194+03	-.1121+03	-.1767+03	-.3062+02	-.5888+02

(0.85)R

0	-.4900+03				
1-S,C	-.1084+03	.1992+03	.1866-00	-.8076+02	-.3584+01
1-S,S	.1458+03	-.9144+02	-.1201+03	-.3010+02	-.5678+02

N,C OR S — ADVANCE RATIO, MU = 0.5

(0.0)R

0	.1304+05				
1-S,C	.2760+05	.3129+04	.6612+03	-.1580+03	-.7328+02
1-S,S	.1641+04	-.4401+03	.8568+03	.7684+02	.8861+02

(0.14)R

0	.6805+03				
1-S,C	.1223+04	.4332+02	-.1487+02	.2744+02	.4115+01
1-S,S	.3072+03	-.5113+02	.2196+02	-.4859+01	-.1865+02

(0.325)R

0	-.1954+02				
1-S,C	-.6275+02	-.1672+03	-.9888+02	.5442+02	.1373+02
1-S,S	.5392+03	-.8834+02	-.7982+02	-.1855+02	-.3888+02

(0.55)R

0	-.2065+03				
1-S,C	-.1216+03	.2120+02	-.9895+02	-.3086+02	.3658+01
1-S,S	.6537+03	-.1679+03	-.2534+03	-.2014+02	.4874+01

(0.75)R

0	-.4234+03				
1-S,C	-.1703+03	.3305+03	-.4548+02	-.1597+03	-.1561+02
1-S,S	.4835+03	-.2108+03	-.4897+03	-.1164+02	.7638+02

(0.85)R

0	-.3539+03				
1-S,C	-.1295+03	.3211+03	-.1409+02	-.1487+03	-.1662+02
1-S,S	.2748+03	-.1557+03	-.3268+03	-.5236+01	.7346+02

N,C OR S — ADVANCE RATIO, MU = 0.7

(0.0)R

0	.1301+06				
1-S,C	.3460+05	.5467+04	.2346+04	.2888+03	.7736+03
1-S,S	.2857+04	-.4250+03	.3216+04	.4448+03	.1461+04

(0.14)R

0	.7314+03				
1-S,C	.2311+04	.2882+03	.1166+02	-.5058+02	-.1864+03
1-S,S	.4116+03	-.1181+03	.7858+02	-.2587+02	-.1988+03

(0.325)R

0	-.2833+03				
1-S,C	-.3398+02	-.4125+03	-.3848+03	-.5085+02	-.2998+03
1-S,S	.5826+03	-.1676+03	-.4538+03	-.1075+03	-.5341+03

(0.55)R

0	-.3109+03				
1-S,C	-.1871+03	-.2307+03	-.5886+03	.1082+02	.7856+02
1-S,S	.8102+03	-.3476+03	-.1015+04	-.9229+02	.1617+02

(0.75)R

0	-.4737+03				
1-S,C	-.2347+03	.5212+03	-.5359+03	-.2846+03	.6206+03
1-S,S	.6163+03	-.5028+03	-.1298+04	-.5654+02	.9942+03

(0.85)R

0	-.3838+03				
1-S,C	-.1610+03	.5863+03	-.3329+03	-.2283+03	.5578+03
1-S,S	.3401+03	-.3795+03	-.9266+03	-.3201+02	.9355+03

N,C OR S — ADVANCE RATIO, MU = 1.0

(0.0)R

0	.1598+05				
1-S,C	.4687+05	.8238+04	.7991+04	.1946+04	.6548+04
1-S,S	.8455+04	-.1251+04	.9372+04	.1443+04	.3388+04

(0.14)R

0	.1332+04				
1-S,C	.4748+04	.6627+03	.2388+03	-.1833+03	-.8898+03
1-S,S	.1194+04	-.2189+03	.3289+03	-.4617+02	-.4243+03

(0.325)R

0	-.6197+02				
1-S,C	.1247+03	-.6133+03	-.1486+04	-.5307+03	-.2661+04
1-S,S	.7019+03	-.2439+03	-.1676+04	-.3821+03	-.1202+04

(0.55)R

0	-.8900+03				
1-S,C	-.2528+03	-.7277+03	-.2505+04	.4055+02	.5954+03
1-S,S	.6052+03	-.6043+03	-.2787+04	-.3253+03	.9419+02

(0.75)R

0	-.7309+03				
1-S,C	-.3618+03	.2642+03	-.2573+04	.6998+03	.5071+04
1-S,S	.3933+03	-.9182+03	-.2696+04	-.1379+03	.1813+04

(0.85)R

0	-.4290+03				
1-S,C	-.2478+03	.4710+03	-.1653+04	.5797+03	.4275+04
1-S,S	.2224+03	-.6689+03	-.1688+04	-.5191+02	.1158+04

N,C OR S — ADVANCE RATIO, MU = 1.4

(0.0)R

0	.2744+05				
1-S,C	.5955+05	.5694+04	.1943+05	.7371+03	.2434+04
1-S,S	.1304+05	.6410+03	.5265+04	.6638+03	-.4515+04

(0.14)R

0	.3546+04				
1-S,C	.8589+04	.9723+03	.1252+04	-.2985+03	-.4099+03
1-S,S	.2484+04	-.1861+03	.8148+03	.4122+02	.6677+03

(0.325)R

0	-.9779+03				
1-S,C	-.1397+02	.3181+02	-.4138+04	-.4836+03	-.1193+04
1-S,S	.1052+04	-.7592+03	-.5228+03	-.1537+03	.2448+04

(0.55)R

0	-.1720+04				
1-S,C	-.8354+03	-.2438+03	-.7309+04	-.2063+02	.3051+03
1-S,S	.4591+03	-.1411+04	-.1114+04	-.4969+02	-.1106+04

(0.75)R

0	-.1466+04				
1-S,C	-.6073+03	.2481+03	-.7390+04	-.1639+03	.1766+04
1-S,S	.1166+03	-.1537+04	.7687+02	.2665+03	-.6096+04

(0.85)R

0	-.8518+03				
1-S,C	-.3120+03	.3075+03	-.4567+04	-.1968+03	.1346+04
1-S,S	.4995+02	-.9734+03	.3968+03	.2395+03	-.4828+04

NOTE- DIVIDE LISTED VALUES BY 1000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 6.
INFLOW RATIO TRANSFER COEFFICIENTS FOR A HINGELESS BLADE
(B) MP = 0.1

FP = 0.0025 (FOR MU = 0.25,0.4,0.5)
FP = 0.00112(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S		ADVANCE RATIO, MU = 0.25			
		(0.0)R			
0	.8639+04				
1-S,C	.8632+04	.3334+03	.1409+03	-.3484+02	-.8663+02
1-S,S	-.7524+03	-.4636+03	.6857+02	-.2216+02	.6479+02
		(0.14)R			
0	.1295+04				
1-S,C	.1263+04	.4942+02	.7823+01	-.1196+01	.1537+01
1-S,S	.4873+01	-.7134+02	-.9598+01	-.1623+02	-.2366+02
		(0.325)R			
0	.1388+03				
1-S,C	.1866+03	.1231+02	-.3433+02	.3298+01	.2105+02
1-S,S	.2518+03	-.1491+02	-.5184+02	-.2626+02	-.5644+02
		(0.55)R			
0	-.1255+03				
1-S,C	-.2829+02	.3143+02	-.6331+02	-.1429+02	-.1164+02
1-S,S	.2838+03	-.1288+02	-.8099+02	-.1537+02	.1741+01
		(0.75)R			
0	-.2755+03				
1-S,C	-.6228+02	.4171+02	-.6335+02	-.2812+02	-.4554+02
1-S,S	.1656+03	-.8948+01	-.7382+02	.5358+01	.7092+02
		(0.85)R			
0	-.1967+03				
1-S,C	-.4479+02	.2765+02	-.3884+02	-.1995+02	-.3457+02
1-S,S	.7849+02	-.4818+01	-.4387+02	.7322+01	.5782+02

N,C OR S		ADVANCE RATIO, MU = 0.4			
		(0.0)R			
0	.8809+04				
1-S,C	.1476+05	.1831+04	.3198+03	-.2928+02	-.2595+02
1-S,S	-.3993+03	-.6244+03	.2498+03	-.6539+02	-.5310+01
		(0.14)R			
0	.1318+04				
1-S,C	.2149+04	.1258+03	.1284+02	-.2056+01	-.1884+02
1-S,S	.1287+03	-.1847+03	.1716+02	-.1244+02	-.1874+02
		(0.325)R			
0	.1158+03				
1-S,C	.1675+03	-.1457+02	-.7716+02	-.2369+01	-.1282+02
1-S,S	.4271+03	-.4746+02	-.6598+02	-.8596+01	-.3876+02
		(0.55)R			
0	-.1578+03				
1-S,C	-.2173+02	.7702+02	-.1814+03	-.2683+02	-.1857+01
1-S,S	.4863+03	-.7487+02	-.1612+03	-.1258+02	.2568+01
		(0.75)R			
0	-.3012+03				
1-S,C	-.6712+02	.1579+03	-.7388+02	-.4235+02	.1322+02
1-S,S	.2996+03	-.7444+02	-.1882+03	-.1153+02	.6889+02
		(0.85)R			
0	-.2111+03				
1-S,C	-.4739+02	.1129+03	-.3989+02	-.2981+02	.1889+02
1-S,S	.1472+03	-.4584+02	-.1287+03	-.6883+01	.3256+02

N,C OR S		ADVANCE RATIO, MU = 0.5			
		(0.0)R			
0	.9079+04				
1-S,C	.1949+05	.2878+04	.9613+03	.1959+02	.3283+02
1-S,S	-.1274+02	-.6492+03	.7929+03	.8058+02	-.9072+02
		(0.14)R			
0	.1321+04				
1-S,C	.2840+04	.2264+03	.5396+02	.1538+02	-.9718+01
1-S,S	.2217+03	-.1158+03	.7625+02	-.4559-00	.5793+01
		(0.325)R			
0	.5792+02				
1-S,C	.2267+03	-.9476+02	-.2838+03	.6413+01	-.2481+02
1-S,S	.5283+03	-.7585+02	-.1164+03	-.2715+02	.2872+02
		(0.55)R			
0	-.2891+03				
1-S,C	-.2511+02	.5244+02	-.2944+03	-.7117+02	.3775+01
1-S,S	.6356+03	-.1423+03	-.3167+03	-.3136+02	-.1498+02
		(0.75)R			
0	-.3149+03				
1-S,C	-.6928+02	.2243+03	-.2394+03	-.1264+03	.3531+02
1-S,S	.4330+03	-.1558+03	-.3825+03	-.1917+02	-.6826+02
		(0.85)R			
0	-.2122+03				
1-S,C	-.6388+02	.1715+03	-.1359+03	-.8833+02	.2782+02
1-S,S	.2281+03	-.9769+02	-.2473+03	-.9364+01	-.4582+02

N,C OR S		ADVANCE RATIO, MU = 0.7			
		(0.0)R			
0	.8963+04				
1-S,C	.2588+05	.3833+04	.4293+04	.4827+03	.2675+03
1-S,S	.1036+03	-.1005+04	.2025+04	.2663+03	-.6198+03
		(0.14)R			
0	.1543+04				
1-S,C	.4768+04	.5075+03	.3695+03	.4518+02	-.3738+02
1-S,S	.2576+03	-.2313+03	.2473+03	.1845+02	.7958+02
		(0.325)R			
0	-.8271+02				
1-S,C	.5287+03	-.2774+03	-.1017+04	-.1388+03	-.1293+03
1-S,S	.5847+03	-.1807+03	-.3651+03	-.6910+02	.2885+03
		(0.55)R			
0	-.3642+03				
1-S,C	.1386+02	-.7315+02	-.1681+04	-.2879+03	.3369+02
1-S,S	.7602+03	-.3525+03	-.8398+03	-.9713+02	-.1347+03
		(0.75)R			
0	-.3227+03				
1-S,C	-.9455+02	.2508+03	-.1454+04	-.3088+03	.1968+03
1-S,S	.5591+03	-.3731+03	-.8821+03	-.7259+02	-.5388+03
		(0.85)R			
0	-.1837+03				
1-S,C	-.6863+02	.2888+03	-.8304+03	-.1818+03	.1458+03
1-S,S	.2999+03	-.2275+03	-.5355+03	-.3914+02	-.3875+03

N,C OR S		ADVANCE RATIO, MU = 1.0			
		(0.0)R			
0	.1154+05				
1-S,C	.3859+05	.6399+04	.1268+05	.1234+04	-.1966+03
1-S,S	.8961+03	-.1506+04	.7650+03	.1017+02	-.1175+04
		(0.14)R			
0	.2424+04				
1-S,C	.9181+04	.1109+04	.1575+04	.6979+02	-.2283+02
1-S,S	.4637+03	-.5063+03	.1986+03	-.2933+02	.1932+03
		(0.325)R			
0	-.3185+03				
1-S,C	.1358+04	-.4411+03	-.3386+04	-.4716+03	.2348+02
1-S,S	.6014+03	-.4985+03	.1316+03	.6652+01	.6338+03
		(0.55)R			
0	-.8597+03				
1-S,C	.1107+03	-.5844+03	-.5698+04	-.5965+03	-.3866+02
1-S,S	.6138+03	-.7727+03	.3111+03	.2475+03	-.4737+03
		(0.75)R			
0	-.6348+03				
1-S,C	-.9797+02	-.2515+03	-.4718+04	-.3772+03	-.8385+02
1-S,S	.3353+03	-.6854+03	.3428+03	.3498+03	-.1314+04
		(0.85)R			
0	-.3311+03				
1-S,C	-.7269+02	-.9255+02	-.2688+04	-.1859+03	-.5551+02
1-S,S	.1532+03	-.3877+03	.2056+03	.2283+03	-.8991+03

N,C OR S		ADVANCE RATIO, MU = 1.4			
		(0.0)R			
0	.1593+05				
1-S,C	.3119+05	.4676+04	.7519+04	-.8864+03	-.8316+03
1-S,S	.1941+04	-.6595+03	-.7843+04	-.7485+03	.4132+03
		(0.14)R			
0	.4322+04				
1-S,C	.9806+04	.1195+04	.1376+04	-.2468+03	.3598+02
1-S,S	.9211+03	-.5752+03	-.1056+04	-.1986+03	.2042+03
		(0.325)R			
0	-.1185+03				
1-S,C	.1179+04	-.1682+03	-.1824+04	.1586+03	.3494+03
1-S,S	.8265+03	-.8732+03	.2987+04	.3064+03	.3082+02
		(0.55)R			
0	-.1224+04				
1-S,C	-.3493+03	-.4194+03	-.3294+04	.7025+03	-.2931+03
1-S,S	.6347+03	-.8701+03	.5285+04	.1213+04	-.4875+03
		(0.75)R			
0	-.9192+03				
1-S,C	-.2575+03	-.2369+03	-.2557+04	.7657+03	-.7859+03
1-S,S	.2246+03	-.4489+03	.4213+04	.1325+04	-.6571+03
		(0.85)R			
0	-.4713+03				
1-S,C	-.1123+03	-.1067+03	-.1352+04	.4452+03	-.4607+03
1-S,S	.7284+02	-.1984+03	.2251+04	.7712+03	-.3982+03

NOTE- DIVIDE LISTED VALUES BY 1000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 6.
INFLOW RATIO TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(C) MP = 0.1
FP = 0.01 (FOR MU = 0.25,0.4,0.5)
FP = 0.00447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S		ADVANCE RATIO, MU = 0.25			
		(0.0)R			
0	.4408+04				
1-5,C	.4567+04	.1140+03	.6468+02	-.5066+02	-.4205+02
1-5,S	-.9058+03	-.2906+03	-.1579+03	.1266+02	-.6730+01
		(0.14)R			
0	.1691+04				
1-5,C	.1760+04	.3736+02	.3823+01	-.1876+02	-.1639+02
1-5,S	-.2467+03	-.1131+03	-.4509+02	-.8681+01	-.1021+02
		(0.325)R			
0	.4635+03				
1-5,C	.5132+03	.2588+01	-.4489+02	-.4546+01	-.4950+01
1-5,S	.1108+03	-.3753+02	.1927+02	-.3039+02	-.1784+0;
		(0.55)R			
0	.9001+01				
1-5,C	.1265+03	.2507+01	-.6970+02	-.1160+01	-.5777-00
1-5,S	.1884+03	-.1731+02	.4281+02	-.3904+02	-.1925+02
		(0.75)R			
0	-.9818+02				
1-5,C	.1884+02	.7181+01	-.4903+02	-.7432-00	.7227-00
1-5,S	.1017+03	-.8905+01	.3001+02	-.2483+02	-.1082+02
		(0.85)R			
0	-.6322+02				
1-5,C	.2215+01	.4716+01	-.2472+02	-.4193-00	.5184-00
1-5,S	.4498+02	-.4247+01	.1498+02	-.1208+02	-.4999+01

N,C OR S		ADVANCE RATIO, MU = 0.4			
		(0.0)R			
0	.4652+04				
1-5,C	.7892+04	.4764+03	.8766+02	.7385+01	-.2474+02
1-5,S	-.1561+04	-.5604+03	-.2379+03	-.7935+02	-.2873+02
		(0.14)R			
0	.1772+04				
1-5,C	.3040+04	.1742+03	.1909+02	-.2291+01	-.1091+02
1-5,S	-.4396+03	-.2208+03	-.4987+02	-.2382+02	-.1457+02
		(0.325)R			
0	.4611+03				
1-5,C	.9138+03	.5487+02	-.2520+02	-.1708+02	-.7731+01
1-5,S	.1719+03	-.8260+02	.6632+02	.8891+01	-.8196+01
		(0.55)R			
0	-.1803+02				
1-5,C	.2589+03	.6869+02	-.4304+02	-.3649+02	-.1085+02
1-5,S	.3174+03	-.5556+02	.9779+02	.2531+02	.1317+01
		(0.75)R			
0	-.1167+03				
1-5,C	.6021+02	.6897+02	-.2961+02	-.3180+02	-.8925+01
1-5,S	.1804+03	-.3683+02	.5857+02	.2032+02	.6143+01
		(0.85)R			
0	-.7222+02				
1-5,C	.1766+02	.3905+02	-.1476+02	-.1716+02	-.4768+01
1-5,S	.8189+02	-.1885+02	.2754+02	.1063+02	.3997+01

N,C OR S		ADVANCE RATIO, MU = 0.5			
		(0.0)R			
0	.4895+04				
1-5,C	.1049+05	.1055+04	.2711+03	.7828+02	-.2828+02
1-5,S	-.1909+04	-.7929+03	-.3926+03	-.4897+02	-.1490+02
		(0.14)R			
0	.1843+04				
1-5,C	.4042+04	.3625+03	.7197+02	.1920+02	-.4329+01
1-5,S	-.5411+03	-.3098+03	-.5616+02	-.1285+02	-.4536+01
		(0.325)R			
0	.4423+03				
1-5,C	.1213+04	.6307+02	-.4114+02	-.2581+02	.6561+01
1-5,S	.2142+03	-.1163+03	.1662+03	.1731+02	.1109+01
		(0.55)R			
0	-.5426+02				
1-5,C	.3411+03	.7008+02	-.7173+02	-.6325+02	-.2590+01
1-5,S	.4240+03	-.9134+02	.2201+03	.4873+02	.3028+01
		(0.75)R			
0	-.1345+03				
1-5,C	.7799+02	.9511+02	-.4340+02	-.5446+02	-.9505+01
1-5,S	.2618+03	-.6817+02	.1269+03	.4445+02	.2112+01
		(0.85)R			
0	-.7959+02				
1-5,C	.2246+02	.5737+02	-.2040+02	-.2921+02	-.6197+01
1-5,S	.1238+03	-.3604+02	.5876+02	.2422+02	.1048+01

N,C OR S		ADVANCE RATIO, MU = 0.7			
		(0.0)R			
0	.4814+04				
1-5,C	.1313+05	.1896+04	.4495+03	.1792+03	-.5344+02
1-5,S	-.2547+04	-.1424+04	-.9858+03	-.2339+03	-.6503+02
		(0.14)R			
0	.1964+04				
1-5,C	.5671+04	.6993+03	.1498+03	.3760+02	-.1047+02
1-5,S	-.9029+03	-.6308+03	-.1826+03	-.5501+02	-.2765+01
		(0.325)R			
0	.4430+03				
1-5,C	.1933+04	.8738+02	-.2848+02	-.6140+02	.9180+01
1-5,S	.7703+02	-.2697+03	.4107+03	.9313+02	.2866+02
		(0.55)R			
0	-.1087+03				
1-5,C	.5819+03	.5320+02	-.7639+02	-.8846+02	-.1072+02
1-5,S	.4273+03	-.1922+03	.6157+03	.1953+03	-.5247+01
		(0.75)R			
0	-.1438+03				
1-5,C	.1446+03	.1173+03	-.4339+02	-.5123+02	-.2228+02
1-5,S	.2977+03	-.1268+03	.3840+03	.1523+03	-.3001+02
		(0.85)R			
0	-.7704+02				
1-5,C	.4601+02	.7498+02	-.1945+02	-.2365+02	-.1375+02
1-5,S	.1457+03	-.6424+02	.1834+03	.7874+02	-.1960+02

N,C OR S		ADVANCE RATIO, MU = 1.0			
		(0.0)R			
0	.5719+04				
1-5,C	.1636+05	.2778+04	.4253+03	-.4723+03	-.1087+03
1-5,S	-.2491+04	-.2423+04	-.1302+04	.4566+03	.3065+03
		(0.14)R			
0	.2546+04				
1-5,C	.7983+04	.1181+04	.2370+03	-.1327+03	-.1884+02
1-5,S	-.1042+04	-.1246+04	-.2590+03	.1234+03	.1069+03
		(0.325)R			
0	.5446+03				
1-5,C	.3115+04	.2118+03	.1763+03	.2170+03	.3788+02
1-5,S	-.1015+03	-.6460+03	.6404+03	-.1167+03	-.8488+02
		(0.55)R			
0	-.2639+03				
1-5,C	.1008+04	-.2097+02	.2056+03	.5327+03	.1854+02
1-5,S	.2380+03	-.4619+03	.1052+04	-.1622+03	-.2588+03
		(0.75)R			
0	-.2570+03				
1-5,C	.2618+03	.3162+02	.1493+03	.4331+03	-.1105+02
1-5,S	.1640+03	-.2751+03	.6923+03	-.7727+02	-.2184+03
		(0.85)R			
0	-.1301+03				
1-5,C	.8659+02	.2790+02	.7603+02	.2248+03	-.9559+01
1-5,S	.7715+02	-.1334+03	.3358+03	-.3190+02	-.1144+03

N,C OR S		ADVANCE RATIO, MU = 1.4			
		(0.0)R			
0	.7995+04				
1-5,C	.1745+05	.2613+04	.1367+03	.1896+04	.9055+03
1-5,S	-.4195+01	-.2776+04	-.4560+03	.2351+04	.1646+04
		(0.14)R			
0	.3993+04				
1-5,C	.9456+04	.1280+04	.2640+03	.5094+03	.2529+03
1-5,S	.1684+03	-.1656+04	.7404+02	.6689+03	.4771+03
		(0.325)R			
0	.1107+04				
1-5,C	.4035+04	.3533+03	.4511+03	-.6564+03	-.3863+03
1-5,S	.3393+03	-.1008+04	.6472+03	-.8154+03	-.5744+03
		(0.55)R			
0	-.2375+03				
1-5,C	.1296+04	.2081+02	.4885+03	-.9965+03	-.7735+03
1-5,S	.3038+03	-.6921+03	.9237+03	-.1427+04	-.1056+04
		(0.75)R			
0	.3174+03				
1-5,C	.3151+03	.9973+01	.2727+03	-.5486+03	-.5456+03
1-5,S	.1266+03	-.3613+03	.5863+03	-.8903+03	-.6841+03
		(0.85)R			
0	-.1645+03				
1-5,C	.1001+03	.9509+01	.1248+03	-.2452+03	-.2693+03
1-5,S	.4949+02	-.1657+03	.2804+03	-.4199+03	-.3273+03

NOTE- DIVIDE LISTED VALUES BY 1000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 6.
INFLOW RATIO TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(D) MP = 0.3
FP = 0.001 (FOR MU = 0.25,0.4,0.5)
FP = 0.000447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S	ADVANCE RATIO, MU = 0.25				
	(0.0)R				
0	.3773+05				
1-5,C	.1664+05	.3605+03	.2919+03	-.3118+02	-.1208+02
1-5,S	.6368+04	.8280+02	.2680+03	.2472+02	-.3612+01
	(0.14)R				
0	.1670+04				
1-5,C	.6511+03	.6495+02	-.9225+01	.9813+01	-.6619-01
1-5,S	.6756+03	-.8127+02	.1492+02	-.5640+01	-.1042+01
	(0.325)R				
0	.6851+02				
1-5,C	-.4192+03	.1632+03	-.5040+02	.1220+02	.2244+01
1-5,S	.8354+03	-.1365+03	-.3434+02	-.4413+01	-.1683+01
	(0.55)R				
0	-.2109+03				
1-5,C	-.8289+03	.3583+03	-.2726+02	-.1336+02	.2337+01
1-5,S	.8196+03	-.0247+02	-.1409+03	.8113-00	.6587-00
	(0.75)R				
0	-.1400+04				
1-5,C	-.6878+03	.4616+03	.5541+02	-.2626+02	.3387+01
1-5,S	.3670+03	-.2244+02	-.1905+03	-.2615+02	.5645+01
	(0.85)R				
0	-.1425+04				
1-5,C	-.3712+03	.3415+03	.6710+02	-.1882+02	-.4683+01
1-5,S	.1123+03	-.1847+02	-.1376+03	-.3077+02	.5563+01

N,C OR S	ADVANCE RATIO, MU = 0.4				
	(0.0)R				
0	.3719+05				
1-5,C	.2637+05	.1025+04	.1376+04	.1011+02	-.1358+03
1-5,S	.8341+04	.2870+03	.9806+03	.2430+03	.1382+03
	(0.14)R				
0	.1576+04				
1-5,C	.1034+04	.1029+03	-.3885+02	.3989+02	.1518+02
1-5,S	.9523+03	-.2007+03	.7795+02	-.2604+02	-.2105+02
	(0.325)R				
0	-.6247+02				
1-5,C	-.6432+03	.3149+03	-.2372+03	.4703+02	.5215+02
1-5,S	.1332+04	-.3757+03	-.8655+02	-.2891+02	-.3842+02
	(0.55)R				
0	-.2925+03				
1-5,C	-.1255+04	.8760+03	-.1880+03	-.8676+02	.9144+01
1-5,S	.1453+04	-.2674+03	-.5559+03	-.1623+02	.7393+01
	(0.75)R				
0	-.1397+04				
1-5,C	-.1032+04	.1149+04	.1122+03	-.2443+03	-.1331+03
1-5,S	.6845+03	-.1863+03	-.8809+03	-.1768+03	.4302+02
	(0.85)R				
0	-.1402+04				
1-5,C	-.5536+03	.8391+03	.1846+03	-.2121+03	-.1430+03
1-5,S	.2037+03	-.1339+03	-.6773+03	-.1950+03	.3533+02

N,C OR S	ADVANCE RATIO, MU = 0.5				
	(0.0)R				
0	.3677+05				
1-5,C	.3215+05	.2293+04	.2981+04	.2309+03	.8699+01
1-5,S	.8923+04	.1069+04	.1315+04	.7885+03	.6547+03
	(0.14)R				
0	.1429+04				
1-5,C	.1234+04	.6258+02	-.5610+02	.5095+02	-.1722+02
1-5,S	.1012+04	-.2742+03	.1924+03	-.9718+02	-.7354+02
	(0.325)R				
0	-.2955+03				
1-5,C	-.8156+03	.2472+03	-.4968+03	.7091+02	.1871+02
1-5,S	.1534+04	-.0522+03	-.1415+02	-.1533+03	-.1974+03
	(0.55)R				
0	-.4422+03				
1-5,C	-.1516+04	.1140+04	-.5704+03	-.1784+03	.4568+02
1-5,S	.1910+04	-.0860+03	-.9546+03	-.1148+01	-.2029+02
	(0.75)R				
0	-.1413+04				
1-5,C	-.1233+04	.1587+04	-.1400+03	-.6794+03	-.1312+03
1-5,S	.1065+04	-.0044+03	-.1756+04	-.1286+03	.3562+03
	(0.85)R				
0	-.1383+04				
1-5,C	-.6616+03	.1159+04	.7084+02	-.6402+03	-.1699+03
1-5,S	.4044+03	-.4159+03	-.1406+04	-.1775+03	.3675+03

N,C OR S	ADVANCE RATIO, MU = 0.7				
	(0.0)R				
0	.3272+05				
1-5,C	.3997+05	.4929+04	.8485+04	.2882+04	.3443+04
1-5,S	.8747+04	.2329+04	.3312+04	.2677+04	.2655+04
	(0.14)R				
0	.1686+04				
1-5,C	.2303+04	.2069+03	.6171+02	-.2245+03	-.4769+03
1-5,S	.1286+04	-.3462+03	.3463+03	-.2931+03	-.2140+03
	(0.325)R				
0	-.9478+03				
1-5,C	-.1095+04	-.6301+02	-.1441+04	-.4967+03	-.1212+04
1-5,S	.1703+04	-.1153+04	-.1517+03	-.7630+03	-.8999+03
	(0.55)R				
0	-.1046+04				
1-5,C	-.1733+04	.9109+03	-.2407+04	-.3421+03	.1886+03
1-5,S	.2117+04	-.1612+04	-.1906+04	-.5870+02	-.2522+03
	(0.75)R				
0	-.1153+04				
1-5,C	-.1238+04	.2082+03	-.2303+04	-.1239+04	.2304+04
1-5,S	.1472+04	-.1694+04	-.3657+04	.7315+03	.1594+04
	(0.85)R				
0	-.8522+03				
1-5,C	-.6213+03	.1705+04	-.1453+04	-.1213+04	.2094+04
1-5,S	.7769+03	-.1166+04	-.2889+04	.6559+03	.1631+04

N,C OR S	ADVANCE RATIO, MU = 1.0				
	(0.0)R				
0	.3565+05				
1-5,C	.5588+05	.7676+04	.2150+05	.8642+04	.1216+05
1-5,S	.1187+05	.5159+04	.5501+04	.4360+04	.2419+04
	(0.14)R				
0	.2613+04				
1-5,C	.4823+04	.9118+03	.7748+03	-.7095+03	-.1547+04
1-5,S	.2233+04	-.4021+03	.7291+03	-.5064+03	-.1456+03
	(0.325)R				
0	-.2165+04				
1-5,C	-.1769+04	-.7853+02	-.3975+04	-.2615+04	-.5034+04
1-5,S	.1915+04	-.1932+04	-.3615+03	-.1580+04	-.3958+03
	(0.55)R				
0	-.2599+04				
1-5,C	-.2332+04	-.3838+03	-.7327+04	-.8980+03	.6465+03
1-5,S	.1284+04	-.2559+04	-.2531+04	.1206+03	-.6757+03
	(0.75)R				
0	-.1615+04				
1-5,C	-.1369+04	.4309+03	-.7720+04	.7514+03	.9380+04
1-5,S	.6010+03	-.2821+04	-.3552+04	.2241+04	-.2272+04
	(0.85)R				
0	-.7952+03				
1-5,C	-.6249+03	.5643+03	-.4967+04	.7271+03	.8084+04
1-5,S	.3100+03	-.1933+04	-.2428+04	.1890+04	-.1973+04

N,C OR S	ADVANCE RATIO, MU = 1.4				
	(0.0)R				
0	.4022+05				
1-5,C	.4309+05	-.3571+04	.1623+05	.2678+04	.1971+04
1-5,S	.4732+04	.1395+05	-.1004+05	.8006+02	-.7381+04
	(0.14)R				
0	.4311+04				
1-5,C	.4039+04	.3219+03	.1604+04	-.6938+03	-.2525+03
1-5,S	.2491+04	.1075+03	.9096+03	-.4942+03	.1312+04
	(0.325)R				
0	-.2794+04				
1-5,C	-.4442+04	.1618+04	-.2749+04	-.1220+04	-.8522+03
1-5,S	.2760+04	-.3374+04	.3633+04	-.5027+03	.4029+04
	(0.55)R				
0	-.2829+04				
1-5,C	-.4028+04	.9454+03	-.6383+04	.8718+03	-.4283+03
1-5,S	.8678+03	-.2522+04	.2215+04	.2465+04	-.1374+04
	(0.75)R				
0	-.1852+04				
1-5,C	-.1228+04	-.2727+03	-.6796+04	.1462+04	-.2212+03
1-5,S	.1184+03	-.1465+04	.2213+04	.5217+04	-.7831+04
	(0.85)R				
0	-.1027+04				
1-5,C	-.2319+03	-.3919+03	-.4200+04	.8684+03	-.1470+03
1-5,S	.1095+03	-.8269+03	.1635+04	.3773+04	-.6106+04

NOTE- DIVIDE LISTED VALUES BY 1000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 6.
INFLOW RATIO TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(E) MP = 0.3
FP = 0.0025 (FOR MU = 0.25,0.4,0.5)
FP = 0.00112(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S	ADVANCE RATIO, MU = 0.25				
		(0.0)R			
0	.2561+05				
1-5,C	.1184+05	.4655+03	.3137+03	.2314+02	.1788+02
1-5,S	.4520+04	-.4682+02	.2143+03	.1403+02	.8201+01
		(0.14)R			
0	.3830+04				
1-5,C	.1560+04	.1084+03	.1104+02	.2544+01	-.3683+01
1-5,S	.1032+04	-.6331+02	.2252+02	.1058+01	-.1673+01
		(0.325)R			
0	.3814+03				
1-5,C	-.2813+03	.1397+03	-.6975+02	-.3795+01	-.9751+01
1-5,S	.8852+03	-.1216+03	-.4056+02	-.3577+01	-.4804+01
		(0.55)R			
0	-.4251+03				
1-5,C	-.6148+03	.2896+03	-.5999+02	-.1198+02	.4450+01
1-5,S	.8271+03	-.1038+03	-.1275+03	-.9240+01	.4047-00
		(0.75)R			
0	-.8725+03				
1-5,C	-.5574+03	.3231+03	-.1360+02	-.1525+02	.1927+02
1-5,S	.3798+03	-.2923+02	-.1624+03	-.1103+02	.6497+01
		(0.85)R			
0	-.6180+03				
1-5,C	-.3286+03	.2048+03	.7697-00	-.9989+01	.1471+02
1-5,S	.1465+03	-.3376+01	-.1064+03	-.7112+01	.5175+01

N,C OR S	ADVANCE RATIO, MU = 0.4				
		(0.0)R			
0	.2554+05				
1-5,C	.1867+05	.1200+04	.1369+04	.2020+03	.4213+02
1-5,S	.6118+04	.1007+02	.7520+03	.1285+03	.1564+03
		(0.14)R			
0	.3764+04				
1-5,C	.2499+04	.2433+03	.5806+02	.3237+02	-.1826+01
1-5,S	.1490+04	-.1547+03	.1049+03	.1019+02	-.1441+01
		(0.325)R			
0	.2637+03				
1-5,C	-.4164+03	.2817+03	-.2996+03	-.1978+02	-.1400+02
1-5,S	.1424+04	-.3496+03	-.1081+03	-.2383+02	-.6167+02
		(0.55)R			
0	-.5188+03				
1-5,C	-.9286+03	.6763+03	-.3187+03	-.1244+03	-.2926+01
1-5,S	.1409+04	-.3556+03	-.4963+03	-.4789+02	.5437+01
		(0.75)R			
0	-.8897+03				
1-5,C	-.8406+03	.8089+03	-.1602+03	-.1821+03	.1227+02
1-5,S	.7288+03	-.1778+03	-.6925+03	-.5021+02	.8438+02
		(0.85)R			
0	-.6136+03				
1-5,C	-.4951+03	.5222+03	-.6707+02	-.1229+03	.1050+02
1-5,S	.3154+03	-.7437+02	-.4630+03	-.3122+02	.6720+02

N,C OR S	ADVANCE RATIO, MU = 0.5				
		(0.0)R			
0	.2555+05				
1-5,C	.2334+05	.2306+04	.2908+04	.5976+03	.4251+03
1-5,S	.6826+04	.4437+03	.9970+03	.3545+03	.2803+03
		(0.14)R			
0	.3665+04				
1-5,C	.3084+04	.3500+03	.1460+03	.7120+02	-.4403+02
1-5,S	.1683+04	-.1950+03	.2069+03	.2586+01	-.1494+02
		(0.325)R			
0	.5587+02				
1-5,C	-.5238+03	.2325+03	-.6261+03	-.9083+02	-.1742+03
1-5,S	.1674+04	-.6083+03	-.6074+02	-.9334+02	-.9681+02
		(0.55)R			
0	-.6770+03				
1-5,C	-.1134+04	.8235+03	-.8176+03	-.3204+03	.2329+02
1-5,S	.1801+04	-.7370+03	-.8194+03	-.5552+02	-.1410+02
		(0.75)R			
0	-.9065+03				
1-5,C	-.1004+04	.1126+04	-.5854+03	-.4206+03	.2515+03
1-5,S	.1095+04	-.5024+03	-.1286+04	.2248+02	.9502+02
		(0.85)R			
0	-.5963+03				
1-5,C	-.5867+03	.7503+03	-.3132+03	-.2775+03	.1989+03
1-5,S	.5346+03	-.2623+03	-.8801+03	.2906+02	.7963+02

N,C OR S	ADVANCE RATIO, MU = 0.7				
		(0.0)R			
0	.2324+05				
1-5,C	.3010+05	.5516+04	.8394+04	.2804+04	.2080+04
1-5,S	.7003+04	.1022+04	.5634+03	.6331+02	-.1397+04
		(0.14)R			
0	.3875+04				
1-5,C	.5063+04	.7996+03	.7819+03	.1979+03	-.1862+03
1-5,S	.2024+04	-.2524+03	.3790+03	-.2877+02	.2476+03
		(0.325)R			
0	-.4676+03				
1-5,C	-.5035+03	-.1293+03	-.1869+04	-.7549+03	-.9274+03
1-5,S	.1894+04	-.1079+04	.2620+03	-.1561+02	.7425+03
		(0.55)R			
0	-.1114+04				
1-5,C	-.1335+04	.5567+03	-.3299+04	-.1169+04	.2571+02
1-5,S	.2145+04	-.1511+04	-.9709+03	.2296+03	-.4131+03
		(0.75)R			
0	-.8299+03				
1-5,C	-.1016+04	.1103+04	-.2968+04	-.9637+03	.1073+04
1-5,S	.1433+04	-.1180+04	-.1786+04	.3759+03	-.1466+04
		(0.85)R			
120	-.4413+03				
1-5,C	-.5451+03	.7583+03	-.1719+04	-.5408+03	.8265+03
1-5,S	.7365+03	-.6487+03	-.1213+04	.2509+03	-.1063+04

N,C OR S	ADVANCE RATIO, MU = 1.0				
		(0.0)R			
0	.2612+05				
1-5,C	.4084+05	.9086+04	.1706+05	.4737+04	.8395+03
1-5,S	.8282+04	.2348+04	-.2601+04	-.1839+04	-.3251+04
		(0.14)R			
0	.5176+04				
1-5,C	.8688+04	.1917+04	.2432+04	.2861+03	-.1006+01
1-5,S	.2759+04	-.3558+03	.7814+02	-.3430+03	.6605+03
		(0.325)R			
0	-.1337+04				
1-5,C	-.6344+03	-.2271+03	-.3929+04	-.1588+04	-.4238+03
1-5,S	.2033+04	-.2038+04	.1411+04	.5604+03	.1988+04
		(0.55)R			
0	-.2434+04				
1-5,C	-.1892+04	-.6654+03	-.7684+04	-.1491+04	-.4960+03
1-5,S	.1660+04	-.2478+04	.1422+04	.1963+04	-.1212+04
		(0.75)R			
0	-.1536+04				
1-5,C	-.1033+04	-.4998+03	-.6866+04	-.5102+03	-.2886+03
1-5,S	.6761+03	-.1565+04	.6363+03	.2241+04	-.3718+04
		(0.85)R			
0	-.7471+03				
1-5,C	-.4529+03	-.2625+03	-.3879+04	-.1441+03	-.1361+03
1-5,S	.2463+03	-.7721+03	.2489+03	.1352+04	-.2563+04

N,C OR S	ADVANCE RATIO, MU = 1.4				
		(0.0)R			
0	.3135+05				
1-5,C	.3446+05	.3463+04	.1282+05	-.1714+04	-.1991+04
1-5,S	.9466+04	.5580+04	-.1110+05	-.2966+04	.9619+03
		(0.14)R			
0	.7977+04				
1-5,C	.7942+04	.1324+04	.2737+04	-.6311+03	.2019+03
1-5,S	.3976+04	.2014+03	-.1277+04	-.9117+03	.6044+03
		(0.325)R			
0	-.1201+04				
1-5,C	-.2847+04	.6461+03	-.2417+04	.4040+03	.1068+04
1-5,S	.2817+04	-.2476+04	.4352+04	.8091+03	.3646+03
		(0.55)R			
0	-.2861+04				
1-5,C	-.3864+04	-.8410+02	-.5396+04	.2735+04	-.4457+03
1-5,S	.1622+04	-.1622+04	.6569+04	.4012+04	-.8080+03
		(0.75)R			
0	-.1592+04				
1-5,C	-.1426+04	-.5202+03	-.4647+04	.3227+04	-.1563+04
1-5,S	.1555+03	.1337+03	.4649+04	.4533+04	-.1341+04
		(0.85)R			
0	-.7114+03				
1-5,C	-.4526+03	-.3548+03	-.2540+04	.1909+04	-.1048+04
1-5,S	-.1074+03	.3232+03	.2381+04	.2658+04	-.8385+03

NOTE- DIVIDE LISTED VALUES BY 1000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 6.
INFLOW RATIO TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(F) MP = 0.3
FP = 0.01 (FOR MU = 0.25,0.4,0.5)
FP = 0.00447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S		ADVANCE RATIO, MU = 0.25			
		(0.0)R			
0	.1361+05				
1-S,C	.6762+04	.4859+03	.2076+03	.2327+02	.3811+01
1-S,S	.2401+04	-.2556+03	-.8911+02	-.2708+02	-.7724-00
		(0.14)R			
0	.5206+04				
1-S,C	.2476+04	.2132+03	.4790+02	.7119+01	.7474-00
1-S,S	.1259+04	-.1317+03	-.1363+02	-.5092+01	-.3824-00
		(0.325)R			
0	.1393+04				
1-S,C	.4715+03	.1376+03	-.5026+02	-.4391+01	-.1388+01
1-S,S	.9890+03	-.1003+03	.2909+02	.1076+02	.3755-00
		(0.55)R			
0	-.1603+02				
1-S,C	-.1832+03	.1665+03	-.8251+02	-.1482+01	-.2478+01
1-S,S	.7749+03	-.7756+02	.2305+02	.1967+02	.2195+01
		(0.75)R			
0	-.3285+03				
1-S,C	-.2159+03	.1285+03	-.5325+02	-.1373+02	-.1816+01
1-S,S	.3485+03	-.3474+02	.2139+01	.1477+02	.2376+01
		(0.85)R			
0	-.2071+03				
1-S,C	-.1170+03	.6753+02	-.2565+02	-.7498+01	-.9269-00
1-S,S	.1441+03	-.1434+02	-.1508+01	.7606+01	.1348+01

N,C OR S		ADVANCE RATIO, MU = 0.4			
		(0.0)R			
0	.1396+05				
1-S,C	.1107+05	.1354+04	.9316+03	.1677+03	.3048+02
1-S,S	.3557+04	-.6400+03	-.3970+03	-.1929+03	-.1015+02
		(0.14)R			
0	.5301+04				
1-S,C	.4064+04	.5507+03	.2163+03	.5191+02	.5946+01
1-S,S	.1914+04	-.3368+03	-.5011+02	-.3328+02	-.4550+01
		(0.325)R			
0	.1345+04				
1-S,C	.7997+03	.2877+03	-.2287+03	-.3003+02	-.9624+01
1-S,S	.1587+04	-.2673+03	.1470+03	.8133+02	.5761+01
		(0.55)R			
0	-.9162+02				
1-S,C	-.2574+03	.3620+03	-.3902+03	-.1042+03	-.1414+02
1-S,S	.1319+04	-.2134+03	.1054+03	.1400+03	.2923+02
		(0.75)R			
0	-.3679+03				
1-S,C	-.3216+03	.3036+03	-.2611+03	-.9691+02	-.8654+01
1-S,S	.6364+03	-.9866+02	.4731-01	.1016+03	.3107+02
		(0.85)R			
0	-.2242+03				
1-S,C	-.1751+03	.1636+03	-.1286+03	-.5298+02	-.4113+01
1-S,S	.2742+03	-.4148+02	-.1353+02	.5172+02	.1756+02

N,C OR S		ADVANCE RATIO, MU = 0.5			
		(0.0)R			
0	.1434+05				
1-S,C	.1411+05	.2458+04	.1814+04	.3973+03	.3365+02
1-S,S	.4268+04	-.9499+03	-.1027+04	-.4693+03	-.6273+02
		(0.14)R			
0	.5370+04				
1-S,C	.5177+04	.9087+03	.4290+03	.1175+03	.1023+02
1-S,S	.2288+04	-.5078+03	-.1358+03	-.9276+02	-.3246+01
		(0.325)R			
0	.1233+04				
1-S,C	.1020+04	.3142+03	-.4386+03	-.7489+02	-.5660+01
1-S,S	.1925+04	-.4234+03	.3929+03	.1876+03	.4117+02
		(0.55)R			
0	-.2131+03				
1-S,C	-.3095+03	.4123+03	-.7796+03	-.2294+03	-.1850+02
1-S,S	.1709+04	-.3699+03	.3549+03	.3712+03	.5613+02
		(0.75)R			
0	-.4143+03				
1-S,C	-.3877+03	.4038+03	-.5376+03	-.2053+03	-.1675+02
1-S,S	.9039+03	-.1918+03	.9176+02	.2925+03	.3522+02
		(0.85)R			
0	-.2403+03				
1-S,C	-.2104+03	.2270+03	-.2679+03	-.1111+03	-.9092+01
1-S,S	.4089+03	-.8596+02	.1731+02	.1529+03	.1698+02

N,C OR S		ADVANCE RATIO, MU = 0.7			
		(0.0)R			
0	.1364+05				
1-S,C	.1888+05	.5107+04	.3324+04	.2167+03	-.1284+03
1-S,S	.4612+04	-.2505+04	-.3848+04	-.1937+04	-.4340+03
		(0.14)R			
0	.5486+04				
1-S,C	.7810+04	.1951+04	.9649+03	.1063+03	-.2630+01
1-S,S	.2679+04	-.1264+04	-.7910+03	-.4498+03	-.8967+01
		(0.325)R			
0	.1097+04				
1-S,C	.2026+04	.4040+03	-.6488+03	.1008+03	.8708+02
1-S,S	.2257+04	-.7630+03	.1343+04	.7387+03	.2678+03
		(0.55)R			
0	-.4401+03				
1-S,C	.7029+01	.3795+03	-.1354+04	.1878+03	.8410+02
1-S,S	.2092+04	-.5214+03	.1900+04	.1468+04	.1889+03
		(0.75)R			
0	-.4540+03				
1-S,C	-.2515+03	.4785+03	-.9509+03	.1654+03	.3135+02
1-S,S	.1190+04	-.2398+03	.1083+04	.1107+04	.1152+02
		(0.85)R			
0	-.2338+03				
1-S,C	-.1438+03	.2830+03	-.4731+03	.8904+02	.1090+02
1-S,S	.5569+03	-.1025+03	.4965+03	.5662+03	-.1523+02

N,C OR S		ADVANCE RATIO, MU = 1.0			
		(0.0)R			
0	.1578+05				
1-S,C	.2326+05	.6888+04	.2394+04	-.2750+04	-.2370+03
1-S,S	.6717+04	-.4189+04	-.6680+04	-.5403+03	.1405+04
		(0.14)R			
0	.6825+04				
1-S,C	.1081+05	.2992+04	.9993+03	-.6719+03	.2565+01
1-S,S	.3848+04	-.2424+04	-.1691+04	-.1970+03	.4817+03
		(0.325)R			
0	.1101+04				
1-S,C	.3322+04	.6718+03	.7167+02	.1413+04	.2248+03
1-S,S	.2494+04	-.1618+04	.2298+04	.1806+03	-.3819+03
		(0.55)R			
0	-.1084+04				
1-S,C	.3938+03	.1273+03	-.3100+03	.3092+04	.3091+03
1-S,S	.1676+04	-.1134+04	.3839+04	.6103+03	-.1117+04
		(0.75)R			
0	-.8535+03				
1-S,C	-.9299+02	.1874+03	-.2333+03	.2414+04	.1897+03
1-S,S	.7555+03	-.5317+03	.2417+04	.5405+03	-.9271+03
		(0.85)R			
0	-.4141+03				
1-S,C	-.6650+02	.1209+03	-.1149+03	.1239+04	.8989+02
1-S,S	.3207+03	-.2300+03	.1150+04	.2868+03	-.4832+03

N,C OR S		ADVANCE RATIO, MU = 1.4			
		(0.0)R			
0	.2208+05				
1-S,C	.2637+05	.8029+04	.1464+03	-.2258+04	.4539+04
1-S,S	.1442+05	-.2826+04	-.5136+04	.9219+04	.5841+04
		(0.14)R			
0	.1061+05				
1-S,C	.1324+05	.4109+04	.9416+03	-.4881+03	.1309+04
1-S,S	.8484+04	-.1929+04	-.9559+03	.2507+04	.1775+04
		(0.325)R			
0	.2238+04				
1-S,C	.4027+04	.1452+04	.1869+04	.1511+04	-.1690+04
1-S,S	.4668+04	-.1435+04	.2755+04	-.3462+04	-.2005+04
		(0.55)R			
0	-.1333+04				
1-S,C	.1572+03	.4274+03	.1944+04	.3086+04	-.3242+04
1-S,S	.2246+04	-.8813+03	.3905+04	-.5921+04	-.4048+04
		(0.75)R			
0	-.1121+04				
1-S,C	-.2412+03	.2071+03	.1009+04	.2301+04	-.2186+04
1-S,S	.7362+03	-.3120+03	.2217+04	-.3689+04	-.2780+04
		(0.85)R			
0	-.5404+03				
1-S,C	-.1206+03	.1047+03	.4463+03	.1158+04	-.1062+04
1-S,S	.2664+03	-.1134+03	.1009+04	-.1740+04	-.1358+04

NOTE- DIVIDE LISTED VALUES BY 1000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 6.
INFLOW RATIO TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(6) MP = 0.5
FP = 0.001 (FOR MU = 0.25,0.4,0.5)
FP = 0.000447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S		ADVANCE RATIO, MU = 0.25			
		(0,0)R			
0	.6241+05				
1-S,C	.2151+05	-.1190+04	.5789+03	.2025+01	.2864+02
1-S,S	.1141+05	.3040+03	.5090+03	.1061+03	.5677+02
		(0.14)R			
0	.2746+04				
1-S,C	.6739+03	.1110+03	-.4186+02	.1414+02	-.7395+01
1-S,S	.1179+04	-.1912+03	.2980+02	-.1613+02	-.6857+01
		(0.325)R			
0	.5348+02				
1-S,C	-.1169+04	.5000+03	-.1296+03	.1098+02	-.5166+01
1-S,S	.1300+04	-.2458+03	-.7277+02	-.1603+02	-.1693+02
		(0.55)R			
0	-.4244+03				
1-S,C	-.2201+04	.8565+03	-.1089+02	-.3179+02	.9331+01
1-S,S	.9933+03	.1560+03	-.2866+03	-.4550+01	-.1048+01
		(0.75)R			
0	-.2307+04				
1-S,C	-.1722+04	.7922+03	.2392+03	-.5175+02	-.1106+02
1-S,S	.2063+03	.3568+03	-.3585+03	-.8755+02	.2152+02
		(0.85)R			
0	-.2316+04				
1-S,C	-.8844+03	.4918+03	.2459+03	-.3674+02	-.1906+02
1-S,S	-.6690+02	.2530+03	-.2483+03	-.9899+02	.2218+02

N,C OR S		ADVANCE RATIO, MU = 0.4			
		(0,0)R			
0	.5901+05				
1-S,C	.3279+05	-.3321+04	.2166+04	-.3634+02	-.1693+01
1-S,S	.1241+05	.8096+03	.1330+04	.3659+03	.3913+03
		(0.14)R			
0	.2443+04				
1-S,C	.1043+04	.1468+03	-.1256+03	.9472+02	-.2100+02
1-S,S	.1549+04	-.4820+03	.1621+03	-.8366+02	-.6544+02
		(0.325)R			
0	-.2304+03				
1-S,C	-.1659+04	.1111+04	-.4851+03	.1186+03	.4062+02
1-S,S	.2105+04	-.7149+03	-.1183+03	-.4309+02	-.1278+03
		(0.55)R			
0	-.5647+03				
1-S,C	-.3053+04	.2182+04	-.1990+03	-.2116+03	.5164+02
1-S,S	.1916+04	.9894+02	-.1046+04	.2634+02	.1643+02
		(0.75)R			
0	-.2153+04				
1-S,C	-.2358+04	.2040+04	.6651+03	-.6199+03	-.2853+03
1-S,S	.5711+03	.5884+03	-.1622+04	-.4904+03	.1832+03
		(0.85)R			
0	-.2123+04				
1-S,C	-.1200+04	.1241+04	.7559+03	-.5433+03	-.3414+03
1-S,S	-.2561+02	.4423+03	-.1224+04	-.5748+03	.1673+03

N,C OR S		ADVANCE RATIO, MU = 0.5			
		(0,0)R			
0	.5546+05				
1-S,C	.3983+05	-.4951+04	.3603+04	-.4241+03	-.6179+02
1-S,S	.1067+05	.1424+04	.1362+04	.7796+03	.1339+04
		(0.14)R			
0	.2362+04				
1-S,C	.8893+03	.2874+03	-.2264+03	.2292+03	.1046+02
1-S,S	.1580+04	-.5075+03	.2922+03	-.8255+02	-.2010+03
		(0.325)R			
0	-.4834+03				
1-S,C	-.2189+04	.1423+04	-.7571+03	.3443+03	.1613+02
1-S,S	.2425+04	-.1124+04	.1018+03	-.2394+03	-.4505+03
		(0.55)R			
0	-.1200+04				
1-S,C	-.3003+04	.2646+04	-.3785+03	-.4556+03	-.3554+02
1-S,S	.2501+04	-.6137+03	-.1516+04	-.1658+03	.3755+02
		(0.75)R			
0	-.1789+04				
1-S,C	-.2741+04	.3265+04	.4801+03	-.1572+04	-.1042+03
1-S,S	.1227+04	.6044+03	-.3442+04	.5263+02	.8525+03
		(0.85)R			
0	-.1396+04				
1-S,C	-.1776+04	.2408+04	.5946+03	-.1416+04	-.9218+02
1-S,S	.4337+03	.7913+03	-.2938+04	.1041+03	.8335+03

N,C OR S		ADVANCE RATIO, MU = 0.7			
		(0,0)R			
0	.4605+05				
1-S,C	.4442+05	-.3083+04	.9220+04	.2628+04	.4769+04
1-S,S	.5926+04	.6155+04	.1447+04	.4334+04	.3263+04
		(0.14)R			
0	.2107+04				
1-S,C	.1910+04	-.2033+02	.9266+02	-.2003+03	-.6789+03
1-S,S	.1585+04	-.7278+03	.6949+03	-.7297+03	-.1965+03
		(0.325)R			
0	-.1799+04				
1-S,C	-.2660+04	.1045+04	-.1702+04	-.1950+03	-.1713+04
1-S,S	.2558+04	-.2201+04	.4962+03	-.1514+04	-.1282+04
		(0.55)R			
0	-.1650+04				
1-S,C	-.3337+04	.2913+04	-.2957+04	-.4703+03	.2458+03
1-S,S	.2667+04	-.2072+04	-.2556+04	.4274+03	-.4704+03
		(0.75)R			
0	-.1425+04				
1-S,C	-.1909+04	.3679+04	-.2493+04	-.3075+04	.3208+04
1-S,S	.1748+04	-.1706+04	-.5750+04	.2393+04	.3039+04
		(0.85)R			
0	-.9875+03				
1-S,C	-.7969+03	.2565+04	-.1422+04	-.3014+04	.2919+04
1-S,S	.9422+03	-.1136+04	-.4631+04	.2011+04	.3183+04

N,C OR S		ADVANCE RATIO, MU = 1.0			
		(0,0)R			
0	.4376+05				
1-S,C	.5602+05	.6528+03	.2133+05	.9555+04	.1348+05
1-S,S	.3714+04	.1280+05	-.1889+04	.6263+04	.8132+03
		(0.14)R			
0	.2607+04				
1-S,C	.3542+04	.7613+03	.9956+03	-.8043+03	-.1534+04
1-S,S	.2160+04	-.7933+03	.1222+04	-.1145+04	.2187+03
		(0.325)R			
0	-.3624+04				
1-S,C	-.4138+04	.1100+04	-.3828+04	-.2816+04	-.5703+04
1-S,S	.2826+04	-.3577+04	.1597+04	-.2679+04	.2452+03
		(0.55)R			
0	-.3476+04				
1-S,C	-.3706+04	.4071+03	-.7805+04	-.1015+04	.1298+03
1-S,S	.1148+04	-.2928+04	-.1830+04	.1384+04	-.1047+04
		(0.75)R			
0	-.1734+04				
1-S,C	-.1486+04	.3344+02	-.8157+04	.2551+03	.1067+05
1-S,S	.3810+03	-.2899+04	-.3704+04	.5739+04	-.3088+04
		(0.85)R			
0	-.7542+03				
1-S,C	-.4962+03	.1826+02	-.5168+04	.2666+03	.9457+04
1-S,S	.2867+03	-.2092+04	-.2586+04	.4587+04	-.2514+04

N,C OR S		ADVANCE RATIO, MU = 1.4			
		(0,0)R			
0	.4741+05				
1-S,C	.4803+05	-.8970+04	.1555+05	.6060+03	.4916+04
1-S,S	-.1804+03	.2045+05	-.1756+05	.3764+04	-.9055+04
		(0.14)R			
0	.4096+04				
1-S,C	.2615+04	.2918+03	.1892+04	-.8250+03	-.2452+03
1-S,S	.2940+04	-.3997+03	.1512+04	-.1277+04	.1788+04
		(0.325)R			
0	-.4413+04				
1-S,C	-.7733+04	.2901+04	-.2285+04	-.5580+03	-.2117+04
1-S,S	.3966+04	-.4643+04	.5740+04	-.2043+04	.4682+04
		(0.55)R			
0	-.2766+04				
1-S,C	-.5151+04	.1339+04	-.5992+04	.2250+04	-.4720+03
1-S,S	.4126+03	-.1089+04	.2043+04	.3514+04	-.1682+04
		(0.75)R			
0	-.1457+04				
1-S,C	-.1248+04	-.9184+03	-.5773+04	.2709+04	.2950+04
1-S,S	.8449+02	-.4103+03	.1780+04	.7222+04	-.7473+04
		(0.85)R			
0	-.8777+03				
1-S,C	-.2323+03	-.9615+03	-.3363+04	.1583+04	.2579+04
1-S,S	.3813+03	-.5326+03	.1552+04	.5031+04	-.5598+04

NOTE- DIVIDE LISTED VALUES BY 1000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 6.
INFLOW RATIO TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(H) MP = 0.5
FP = 0.0025 (FOR MU = 0.25,0.4,0.5)
FP = 0.00112(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S		ADVANCE RATIO, MU = 0.25			
		(0.0)R			
0	.4265+05				
1-S,C	.1530+05	-.4903+03	.5168+03	.6972+02	.3604+02
1-S,S	.8444+04	.1857+03	.3788+03	.3569+02	.2511+02
		(0.14)R			
0	.6351+04				
1-S,C	.1746+04	.9769+02	.2661+01	.8669+01	-.3104+01
1-S,S	.1830+04	-.1044+03	.4079+02	.3138+01	-.1817+01
		(0.325)R			
0	.5777+03				
1-S,C	-.1037+04	.4460+03	-.1341+03	-.1037+02	-.1422+02
1-S,S	.1389+04	-.2334+03	-.7611+02	-.8544+01	-.9705+01
		(0.55)R			
0	-.7527+0				
1-S,C	-.1724+04	.7182+03	-.6303+02	-.3920+02	-.5174-00
1-S,S	.1120+04	-.3118+02	-.2531+03	-.2451+02	-.2171+01
		(0.75)R			
0	-.1459+04				
1-S,C	-.1473+04	.6637+03	.6032+02	-.5240+02	.1650+02
1-S,S	.3146+03	.2281+03	-.3283+03	-.3040+02	.8224+01
		(0.85)R			
0	-.1025+04				
1-S,C	-.8514+03	.3964+03	.6117+02	-.3471+02	.1345+02
1-S,S	.3720+02	.1906+03	-.2160+03	-.1979+02	.7078+01

N,C OR S		ADVANCE RATIO, MU = 0.4			
		(0.0)R			
0	.4095+05				
1-S,C	.2330+05	-.1667+04	.1971+04	.3736+03	.1786+03
1-S,S	.9796+04	.7345+03	.1171+04	.1178+03	.2471+03
		(0.14)R			
0	.5975+04				
1-S,C	.2705+04	.1320+03	.2147+02	.7185+02	-.9511+01
1-S,S	.2396+04	-.2675+03	.1805+03	.5945+01	-.3288+02
		(0.325)R			
0	.3022+03				
1-S,C	-.1454+04	.1024+04	-.5157+03	-.2738+02	-.6358+02
1-S,S	.2229+04	-.7170+03	-.1837+03	-.3767+02	-.1131+03
		(0.55)R			
0	-.9026+03				
1-S,C	-.2416+04	.1785+04	-.3504+03	-.2830+03	-.1765+02
1-S,S	.1953+04	-.3378+03	-.9787+03	-.8913+02	.1724+02
		(0.75)R			
0	-.1401+04				
1-S,C	-.2041+04	.1746+04	.5132+02	-.4364+03	.4830+02
1-S,S	.7216+03	.2980+03	-.1404+04	-.1028+03	.1665+03
		(0.85)R			
0	-.9495+03				
1-S,C	-.1174+04	.1063+04	.1102+03	-.2975+03	.4253+02
1-S,S	.2039+03	.3070+03	-.9442+03	-.6570+02	.1313+03

N,C OR S		ADVANCE RATIO, MU = 0.5			
		(0.0)R			
0	.3940+05				
1-S,C	.2759+05	-.2121+04	.3658+04	.8881+03	.8833+03
1-S,S	.9116+04	.2047+04	.1389+04	.4951+03	.6255+03
		(0.14)R			
0	.5556+04				
1-S,C	.3179+04	.1061+03	.9588+02	.1348+03	-.9935+02
1-S,S	.2424+04	-.3153+03	.3614+03	-.5669+02	-.7490+02
		(0.325)R			
0	-.1085+03				
1-S,C	-.1740+04	.1217+04	-.9237+03	-.1172+03	-.3795+03
1-S,S	.2567+04	-.1261+04	-.6368+02	-.2257+03	-.2753+03
		(0.55)R			
0	-.1158+04				
1-S,C	-.2758+04	.2369+04	-.9413+03	-.6246+03	.3079+02
1-S,S	.2518+04	-.9925+03	-.1626+04	-.3376+02	.2807+02
		(0.75)R			
0	-.1357+04				
1-S,C	-.2223+04	.2486+04	-.4313+03	-.8948+03	.5139+03
1-S,S	.1255+04	-.1336+03	-.2627+04	.2182+03	.3822+03
		(0.85)R			
0	-.8638+03				
1-S,C	-.1254+04	.1548+04	-.1644+03	-.6014+03	.4097+03
1-S,S	.5249+03	.8609+02	-.1806+04	.1831+03	.3037+03

N,C OR S		ADVANCE RATIO, MU = 0.7			
		(0.0)R			
0	.3274+05				
1-S,C	.3313+05	.8465+03	.9546+04	.4095+04	.4080+04
1-S,S	.6880+04	.3989+04	.3137+03	-.1105+03	-.1891+04
		(0.14)R			
0	.5235+04				
1-S,C	.4898+04	.3492+03	.8880+03	.2754+03	-.3779+03
1-S,S	.2424+04	-.1936+03	.6587+03	-.2187+03	.2958+03
		(0.325)R			
0	-.1089+04				
1-S,C	-.2056+04	.8215+03	-.2202+04	-.1134+04	-.1835+04
1-S,S	.2791+04	-.2031+04	.5924+03	-.1703+03	.9713+03
		(0.55)R			
0	-.1777+04				
1-S,C	-.2971+04	.2070+04	-.3977+04	-.1742+04	.7440+02
1-S,S	.2911+04	-.2284+04	-.1948+04	.7543+03	-.4115+03
		(0.75)R			
0	-.1029+04				
1-S,C	-.1847+04	.2360+04	-.3670+04	-.1427+04	.2159+04
1-S,S	.1661+04	-.1310+04	-.3668+04	.1357+04	-.1718+04
		(0.85)R			
0	-.4772+03				
1-S,C	-.9011+03	.1466+04	-.2143+04	-.7988+03	.1659+04
1-S,S	.7789+03	-.6140+03	-.2499+04	.9189+03	-.1259+04

N,C OR S		ADVANCE RATIO, MU = 1.0			
		(0.0)R			
0	.3348+05				
1-S,C	.4178+05	.4270+04	.1662+05	.5734+04	.1664+04
1-S,S	.7349+04	.6139+04	-.4624+04	-.2867+04	-.5557+04
		(0.14)R			
0	.6208+04				
1-S,C	.7749+04	-.1386+04	.2602+04	.2191+03	-.4382+02
1-S,S	.2963+04	-.1789+03	.1637+03	-.7770+03	.9237+03
		(0.325)R			
0	-.2508+04				
1-S,C	-.2948+04	.8291+03	-.3536+04	-.2006+04	-.7778+03
1-S,S	.2726+04	-.3267+04	.2213+04	.5205+03	.3237+04
		(0.55)R			
0	-.3453+04				
1-S,C	-.3571+04	.1966+03	-.7901+04	-.1266+04	-.4335+03
1-S,S	.1718+04	-.3132+04	.1126+04	.3278+04	-.1312+04
		(0.75)R			
0	-.1694+04				
1-S,C	-.1225+04	-.3911+03	-.7563+04	.2372+03	.1594+03
1-S,S	.7723+02	-.1238+04	-.6047+03	.4143+04	-.5109+04
		(0.85)R			
0	-.7024+03				
1-S,C	-.3340+03	-.3179+03	-.4361+04	.3742+03	.1858+03
1-S,S	-.2060+03	-.4274+03	-.6239+03	.2555+04	-.3577+04

N,C OR S		ADVANCE RATIO, MU = 1.4			
		(0.0)R			
0	.4420+05				
1-S,C	.4451+05	.6782+04	.1224+05	-.1554+04	-.2936+04
1-S,S	.2014+05	.4908+04	-.1528+05	-.2165+04	.2512+03
		(0.14)R			
0	.1076+05				
1-S,C	.8774+04	.2538+04	-.3216+04	-.9858+03	.2530+03
1-S,S	.7528+04	-.2255+03	-.1583+04	-.1540+04	.9460+03
		(0.325)R			
0	-.2379+04				
1-S,C	-.6475+04	.1077+04	-.1061+04	.3205+03	.1796+04
1-S,S	.3900+04	-.2283+04	.5843+04	-.3299+03	.1081+04
		(0.55)R			
0	-.3628+04				
1-S,C	-.6522+04	-.5532+03	-.4089+04	.4945+04	.4959+03
1-S,S	.1172+04	.7372+03	.7346+04	.4901+04	-.1371+04
		(0.75)R			
0	-.1132+04				
1-S,C	-.1531+04	-.1377+04	-.4070+04	.6236+04	-.9579+03
1-S,S	-.9404+03	.3078+04	.4273+04	.6698+04	-.2716+04
		(0.85)R			
0	-.2697+03				
1-S,C	-.1523+03	-.8949+03	-.2312+04	.3737+04	-.7500+03
1-S,S	-.8148+03	.2084+04	.2003+04	.4070+04	-.1736+04

NOTE- DIVIDE LISTED VALUES BY 1000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 6.
INFLOW RATIO TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(I) MP = 0.5
FP = 0.01 (FOR MU = 0.25,0.4,0.5)
FP = 0.00447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S — ADVANCE RATIO, MU = 0.25

(0.0)R

0	.2295+05				
1-S,C	.8401+04	.3892+03	.3970+03	.5522+02	.1665+02
1-S,S	.5117+04	-.5742+02	-.7251+02	-.5545+02	-.4083+01

(0.14)R

0	.8764+04				
1-S,C	.2842+04	.2507+03	.8661+02	.2004+02	.6330+01
1-S,S	.2518+04	-.1198+03	-.4110+01	-.8309+01	.1338+01

(0.325)R

0	.2320+04				
1-S,C	.2863+02	.3073+03	-.1038+03	-.3408+01	.2063+01
1-S,S	.1732+04	-.1950+03	.1992+02	.2450+02	.6161+01

(0.55)R

0	-.471d+02				
1-S,C	-.9368+03	.4003+03	-.1572+03	-.2740+02	.1548+01
1-S,S	.1220+04	-.1328+03	-.3581+02	.3710+02	.7574+01

(0.75)R

0	-.55b0+03				
1-S,C	-.727d+03	.2853+03	-.9547+02	-.2820+02	.1257+01
1-S,S	.4904+03	-.2231+02	-.6245+02	.2454+02	.4538+01

(0.85)R

0	-.3495+03				
1-S,C	-.3708+03	.1453+03	-.4516+02	-.1578+02	.6836-00
1-S,S	.1885+03	.1238+01	-.3825+02	.1207+02	.2150+01

N,C OR S — ADVANCE RATIO, MU = 0.4

(0.0)R

0	.2291+05				
1-S,C	.1318+05	.9763+03	.1624+04	.2692+03	.3335+02
1-S,S	.6963+04	.3232+02	-.4125+03	-.4517+03	-.9147+02

(0.14)R

0	.8665+04				
1-S,C	.4487+04	.5587+03	.3397+03	.9112+02	.2984+01
1-S,S	.3570+04	-.2780+03	-.2900+02	-.8898+02	-.2304+02

(0.325)R

0	.2149+04				
1-S,C	.1194+03	.6280+03	-.4750+03	-.4788+02	-.1319+02
1-S,S	.2684+04	-.5758+03	.1292+03	.1572+03	.2886+02

(0.55)R

0	-.1822+03				
1-S,C	-.1361+04	.8827+03	-.7467+03	-.2116+03	-.4874+01
1-S,S	.2039+04	-.4619+03	-.1119+03	.2688+03	.7255+02

(0.75)R

0	-.5996+03				
1-S,C	-.1063+04	.e717+03	-.4805+03	-.2102+03	.5502+01
1-S,S	.8913+03	-.1407+03	-.2543+03	.1902+03	.6293+02

(0.85)R

0	-.3611+03				
1-S,C	-.5416+03	.3497+03	-.2332+03	-.1168+03	.4399+01
1-S,S	.3623+03	-.3849+02	-.1601+03	.9583+02	.3382+02

N,C OR S — ADVANCE RATIO, MU = 0.5

(0.0)R

0	.2278+05				
1-S,C	.1625+05	.1963+04	.3069+04	.5405+03	.4908+02
1-S,S	.7592+04	.2804+03	-.1212+04	-.1082+04	-.2809+03

(0.14)R

0	.8472+04				
1-S,C	.5530+04	.8934+03	.6773+03	.1778+03	-.3786+01
1-S,S	.3971+04	-.3537+03	-.1120+03	-.2362+03	-.3930+02

(0.325)R

0	.1854+04				
1-S,C	.1606+03	.7060+03	-.8685+03	-.9549+02	-.2477+02
1-S,S	.3154+04	-.9220+03	.4428+03	.3668+03	.1202+03

(0.55)R

0	-.4036+03				
1-S,C	-.1604+04	.1044+04	-.1507+04	-.3928+03	.2053+02
1-S,S	.2614+04	-.8497+03	.6125+02	.7422+03	.1571+03

(0.75)R

0	-.6609+03				
1-S,C	-.1229+04	.8645+03	-.1047+04	-.3831+03	.4604+02
1-S,S	.1263+04	-.3483+03	-.3152+03	.5833+03	.8942+02

(0.85)R

0	-.3755+03				
1-S,C	-.6213+03	.4623+03	-.5237+03	-.2120+03	.2892+02
1-S,S	.5588+03	-.1316+03	-.2241+03	.3046+03	.4116+02

N,C OR S — ADVANCE RATIO, MU = 0.7

(0.0)R

0	.2045+05				
1-S,C	.2141+05	.5398+04	.5796+04	-.1168+03	-.4782+03
1-S,S	.7493+04	-.1215+04	-.5665+04	-.3621+04	-.9731+03

(0.14)R

0	.8106+04				
1-S,C	.8276+04	.2169+04	.1606+04	.7425+02	-.6748+02
1-S,S	.4370+04	-.1116+04	-.1158+04	-.9037+03	-.4725+02

(0.325)R

0	.1427+04				
1-S,C	.1031+04	.7143+03	-.1397+04	.3126+03	.2694+03
1-S,S	.3655+04	-.1374+04	.1866+04	.1248+04	.5329+03

(0.55)R

0	-.7920+03				
1-S,C	-.1338+04	.8489+03	-.2899+04	.4944+03	.4352+03
1-S,S	.3255+04	-.1089+04	.2357+04	.2612+04	.3305+03

(0.75)R

0	-.6865+03				
1-S,C	-.9997+03	.8364+03	-.2110+04	.3612+03	.2991+03
1-S,S	.1771+04	-.4089+03	.1152+04	.2006+04	-.3739+02

(0.85)R

0	-.3369+03				
1-S,C	-.4831+03	.4680+03	-.1065+04	.1836+03	.1485+03
1-S,S	.8132+03	-.1471+03	.4858+03	.1032+04	-.6555+02

N,C OR S — ADVANCE RATIO, MU = 1.0

(0.0)R

0	.2220+05				
1-S,C	.2457+05	.6345+04	.3962+04	-.5258+04	-.5066+03
1-S,S	.9129+04	-.1948+04	-.1067+05	-.1801+04	.1983+04

(0.14)R

0	.9351+04				
1-S,C	.1053+05	.2858+04	.1425+04	-.137z+04	.1080+02
1-S,S	.5367+04	-.2010+04	-.2744+04	-.6800+03	.7031+03

(0.325)R

0	.1094+04				
1-S,C	.1709+04	.e456+03	-.5215+03	.2352+04	.4688+03
1-S,S	.3632+04	-.2479+04	.3449+04	.3865+03	-.6169+03

(0.55)R

0	-.1816+04				
1-S,C	-.1221+04	.3784+03	-.1555+04	.5151+04	.5916+03
1-S,S	.2296+04	-.1932+04	.5594+04	.1401+04	-.1973+04

(0.75)R

0	-.1237+04				
1-S,C	-.7931+03	.3228+03	-.1157+04	.3976+04	.3343+03
1-S,S	.8910+03	-.7262+03	.3392+04	.1220+04	-.1709+04

(0.85)R

0	-.5738+03				
1-S,C	-.3440+03	.1810+03	-.5814+03	.2033+04	.1529+03
1-S,S	.3442+03	-.2644+03	.1588+04	.6439+03	-.9015+03

N,C OR S — ADVANCE RATIO, MU = 1.4

(0.0)R

0	.2646+05				
1-S,C	.2572+05	.7742+04	.6657+03	-.5986+04	.5929+04
1-S,S	.1496+05	.9319+03	-.1076+05	.9292+04	.5735+04

(0.14)R

0	.1212+05				
1-S,C	.1148+05	.4148+04	.1386+04	-.1476+04	.1833+04
1-S,S	.9241+04	-.5631+03	-.2576+04	.2298+04	.1758+04

(0.325)R

0	.1593+04				
1-S,C	.1156+04	.1813+04	.2293+04	.3176+04	-.1934+04
1-S,S	.5632+04	-.1697+04	.4300+04	-.3909+04	-.2083+04

(0.55)R

0	-.2324+04				
1-S,C	-.2110+04	.8868+03	.2203+04	.6257+04	-.3917+04
1-S,S	.2810+04	-.1091+04	.6026+04	-.6247+04	-.4438+04

(0.75)R

0	-.1477+04				
1-S,C	-.1031+04	.4716+03	.1075+04	.4487+04	-.2672+04
1-S,S	.8106+03	-.8956+02	.3170+04	-.3768+04	-.3171+04

(0.85)R

0	-.6558+03				
1-S,C	-.3902+03	.2262+03	.4619+03	.2229+04	-.1302+04
1-S,S	.2537+03	.6146+02	.1388+04	-.1756+04	-.1570+04

NOTE- DIVIDE LISTED VALUES BY 1000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 7.
A1S CYCLIC PITCH TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(A) MP = 0.1
FP = 0.801 (FOR MU = 0.25,0.4,0.5)
FP = 0.000447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S		ADVANCE RATIO, MU = 0.25				
		(0.0)R				
0	.2146+03					
1-S,C	.5830+04	.3046+03	.5379+02	-.9929+01	.3619+02	
1-S,S	.3360+05	-.1461+03	-.4611+02	-.2398+02	-.7180+02	
		(0.14)R				
0	.7662+01					
1-S,C	.2650+03	.1882+02	.4264+01	.4825+01	-.4039+01	
1-S,S	.1545+04	-.1248+02	.4985-00	-.1560+01	.7487+01	
		(0.32)R				
0	-.6810+01					
1-S,C	.5301+01	.1110+02	.2150+01	.1020+02	-.7904+01	
1-S,S	.9115+02	-.8119+01	.5032+01	.9667-01	.1773+02	
		(0.55)R				
0	-.1092+02					
1-S,C	-.3691+01	.2322+02	-.4814+01	-.9552-00	.2668+01	
1-S,S	.1253+03	-.7183+01	.6763+01	.5365+01	-.2628-00	
		(0.75)R				
0	-.6609+01					
1-S,C	-.3239+02	.4278+02	-.1354+02	-.2517+02	.1195+02	
1-S,S	.2860+02	-.1853+02	.1006+02	.1207+02	-.2596+02	
		(0.85)R				
0	-.2430+01					
1-S,C	-.3225+02	.3664+02	-.1185+02	-.2539+02	.1006+02	
1-S,S	-.1784+02	-.1834+02	.8361+01	.1037+02	-.2500+02	

N,C OR S		ADVANCE RATIO, MU = 0.4				
		(0.0)R				
0	.1491+03					
1-S,C	.5941+04	.5060+03	.7663+02	-.1105+02	.3780+02	
1-S,S	.3382+05	-.1287+03	.3056+02	-.7582+01	-.4860+02	
		(0.14)R				
0	.2868+01					
1-S,C	.2690+03	.2617+02	.5897+01	.5716+01	-.3465+01	
1-S,S	.1557+04	-.1459+02	.4529+01	-.1470-00	.6109+01	
		(0.32)R				
0	-.1210+02					
1-S,C	.2795+01	.4730+01	.1108+01	.1201+02	-.6726+01	
1-S,S	.1001+03	-.1330+02	.1616+01	.1330+01	.1423+02	
		(0.55)R				
0	-.1914+02					
1-S,C	-.4758+01	.2215+02	-.6030+01	-.1062+01	.2974+01	
1-S,S	.1418+03	-.1310+02	-.5483+01	.6965+01	.2035+01	
		(0.75)R				
0	-.1313+02					
1-S,C	-.2786+02	.6650+02	-.5335+01	-.2934+02	.9421+01	
1-S,S	.3929+02	-.2835+02	-.8739-00	.1470+02	-.1652+02	
		(0.85)R				
0	-.6054+01					
1-S,C	-.2708+02	.6254+02	-.2154+01	-.2960+02	.7310+01	
1-S,S	-.1364+02	-.2700+02	.2630+01	.1265+02	-.1656+02	

N,C OR S		ADVANCE RATIO, MU = 0.5				
		(0.0)R				
0	.1427+03					
1-S,C	.6243+04	.6519+03	.1550+03	-.5112+02	.5644+01	
1-S,S	.3393+05	-.1837+03	.2674+03	.3623+02	.3486+02	
		(0.14)R				
0	-.5977-00					
1-S,C	.2808+03	.1877+02	.2499-00	.9806+01	.8544+00	
1-S,S	.1582+04	-.1087+02	-.2720+01	-.1849+01	-.5067+01	
		(0.32)R				
0	-.1501+02					
1-S,C	-.3694+01	-.9775+01	-.1385+02	.2138+02	.1769+01	
1-S,S	.1146+03	-.8561+01	-.3674+02	-.5997+01	-.1037+02	
		(0.55)R				
0	-.1343+02					
1-S,C	-.1299+02	.4436+02	-.1021+02	.4288+01	.3595+01	
1-S,S	.1171+03	-.2025+02	-.5431+02	.5329-00	.6361+01	
		(0.75)R				
0	-.3291+01					
1-S,C	-.2491+02	.1120+03	.1656+01	-.2738+02	.4711+01	
1-S,S	.3634+02	-.2885+02	-.5420+02	.1141+02	.3146+02	
		(0.85)R				
0	.9472-00					
1-S,C	-.2034+02	.9716+02	.4844+01	-.2849+02	.3546+01	
1-S,S	.9518-00	-.2227+02	-.3673+02	.1115+02	.2920+02	

N,C OR S		ADVANCE RATIO, MU = 0.7				
		(0.0)R				
0	.1974+03					
1-S,C	.7067+04	.1004+04	.3246+03	-.3895+01	.1381+03	
1-S,S	.3066+05	-.4932+03	.7035+03	.1038+03	.3380+03	
		(0.14)R				
0	.3379+01					
1-S,C	.4671+03	.3863+02	.9252+01	-.2630+01	-.2032+02	
1-S,S	.2120+04	-.2847+02	.1192+02	.4043-00	-.4257+02	
		(0.32)R				
0	-.2607+02					
1-S,C	-.8320+01	-.3169+02	-.4128+02	.6812+01	-.4784+02	
1-S,S	.1690+03	-.7983+01	-.1061+03	-.1526+02	-.1133+03	
		(0.55)R				
0	-.2629+02					
1-S,C	-.2361+02	.1298+02	-.5640+02	.2162+02	.2012+02	
1-S,S	.1657+03	-.1905+02	-.1955+03	-.1924+02	.1422+02	
		(0.75)R				
0	.1062+01					
1-S,C	-.3503+02	.1031+03	-.1582+02	.4287+01	.1150+03	
1-S,S	.2553+02	-.3506+02	-.2061+03	-.1528+02	.2126+03	
		(0.85)R				
0	.1058+02					
1-S,C	-.2706+02	.1581+03	.4449+01	-.5211+01	.1014+03	
1-S,S	-.3023+02	-.3018+02	-.1368+03	-.9033+01	.1945+03	

N,C OR S		ADVANCE RATIO, MU = 1.0				
		(0.0)R				
0	.6249+03					
1-S,C	.7613+04	.1140+04	.1147+04	.9610+02	.8506+03	
1-S,S	.2747+05	-.5311+03	.1381+04	.2399+03	.3321+03	
		(0.14)R				
0	.3852+02					
1-S,C	.7659+03	.1240+03	.4848+02	-.1118+02	-.1195+03	
1-S,S	.2847+04	-.6284+02	.4790+02	-.1410-00	-.3702+02	
		(0.32)R				
0	-.6609+02					
1-S,C	.2161+02	-.6278+01	-.1945+03	-.3134+02	-.3566+03	
1-S,S	.2674+03	-.5296+01	-.2572+03	-.5453+02	-.1088+03	
		(0.55)R				
0	-.7848+02					
1-S,C	-.2630+02	.9696+01	-.3511+03	.3389+01	.7875+02	
1-S,S	.1488+03	-.1041+02	-.4251+03	-.7086+02	-.6941+01	
		(0.75)R				
0	-.1573+02					
1-S,C	-.6273+02	.1460+03	-.3502+03	.3336+02	.6667+03	
1-S,S	.2572+01	-.5060+02	-.3789+03	-.6329+02	.7939+02	
		(0.85)R				
0	.8005+01					
1-S,C	-.5011+02	.1506+03	-.2196+03	.2633+02	.9609+03	
1-S,S	-.3473+02	-.7590+02	-.2253+03	-.3935+02	.6405+02	

N,C OR S		ADVANCE RATIO, MU = 1.4				
		(0.0)R				
0	.2025+04					
1-S,C	.7631+04	.5706+03	.1965+04	-.7415+01	.2067+03	
1-S,S	.2370+05	-.4289+03	.3853+03	.7979+01	-.4376+03	
		(0.14)R				
0	.2557+03					
1-S,C	.1065+04	.1461+03	.1566+03	-.2612+02	-.4443+02	
1-S,S	.3614+04	-.1184+03	.6379+02	-.5328+01	.5294+02	
		(0.32)R				
0	-.9535+02					
1-S,C	-.1502+02	.1186+03	-.3941+03	-.2801+02	-.1121+03	
1-S,S	.4293+03	-.8901+02	-.5764+02	-.2437+02	.2080+03	
		(0.55)R				
0	-.1504+03					
1-S,C	-.7848+02	.1586+03	-.7198+03	.6299+01	.2490+02	
1-S,S	.1299+03	-.8268+02	-.1204+03	.3306+01	-.9701+02	
		(0.75)R				
0	-.1147+03					
1-S,C	-.4866+02	.2227+03	-.6449+03	-.1767+01	.1416+03	
1-S,S	-.1170+02	-.1295+03	.2139+02	.7855+02	-.5041+03	
		(0.85)R				
0	-.6027+02					
1-S,C	-.2550+02	.1576+03	-.3738+03	-.6988+01	.1059+03	
1-S,S	-.3077+02	-.9719+02	.5483+02	.6682+02	-.3959+03	

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 7.
A1S CYCLIC PITCH TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(B) MP = 0.1
FP = 0.00025 (FOR MU = 0.25,0.4,0.5)
FP = 0.00112(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S — ADVANCE RATIO, MU = 0.25

(0.0)R

0	.1129+03				
1-5,C	.6027+04	.3553+03	.1899+02	-.7830+01	±.5098+01
1-5,S	.2264+05	-.2108+03	.2828+02	-.2115+02	.8274+01

(0.147)R

0	.1426+02				
1-5,C	.8799+03	.4771+02	.2354+01	±.1075+01	-.2182+01
1-5,S	.3362+04	-.3441+02	-.1798+01	-.5226+01	-.7190+01

(0.325)R

0	-.4431+01				
1-5,C	.7260+02	.1062+01	.5055-00	.8243-00	-.1918+01
1-5,S	.4213+03	-.1302+02	-.1569+02	±.4059+01	-.1379+02

(0.55)R

0	-.8964+01				
1-5,C	-.7935+01	.1778+02	.4557+01	.3659+01	.2943+01
1-5,S	.1947+03	-.1865+02	-.2613+02	±.3457-00	.3252+01

(0.75)R

0	-.8451+01				
1-5,C	-.3111+02	.9253+02	.7235+01	.5047+01	.7150+01
1-5,S	.8249+02	-.1808+02	-.2467+02	.4019+01	.2197+02

(0.85)R

0	-.5060+01				
1-5,C	-.2253+02	.2290+02	.4964+01	.3365+01	±.5206+01
1-5,S	.3274+02	-.1102+02	-.1484+02	.3313+01	.1713+02

N,C OR S — ADVANCE RATIO, MU = 0.4

(0.0)R

0	.5096+02				
1-5,C	.6105+04	.5965+03	.8653+02	±.4542+01	.6028+01
1-5,S	.2278+05	-.2376+03	.1464+03	.5120+01	.8158+01

(0.147)R

0	.1907+01				
1-5,C	.8894+03	.7653+02	.7755+01	.6096-00	-.2103+01
1-5,S	.3387+04	-.3999+02	.1011+02	±.1867+01	-.3925+01

(0.325)R

0	-.1316+02				
1-5,C	.6998+02	-.8691+01	-.9025+01	.2662+01	±.4495+01
1-5,S	.4375+03	-.1856+02	-.3040+02	±.5231+01	-.8410+01

(0.55)R

0	-.1897+02				
1-5,C	-.1049+02	.1960+02	-.7329+01	.1855+01	.4195+01
1-5,S	.2162+03	-.2905+02	-.5752+02	±.3395+01	.1779+01

(0.75)R

0	-.1545+02				
1-5,C	-.3112+02	.4757+02	-.5096-00	±.1275-00	.1208+02
1-5,S	.1005+03	-.2918+02	-.5828+02	.6158-00	.1309+02

(0.85)R

0	-.8763+01				
1-5,C	-.2203+02	.3475+02	.1034+01	±.4659-00	.8953+01
1-5,S	.4315+02	-.1796+02	-.3587+02	.1162+01	.1024+02

N,C OR S — ADVANCE RATIO, MU = 0.5

(0.0)R

0	.7139+02				
1-5,C	.6402+04	.6575+03	.3755+03	±.9577+01	.6798+02
1-5,S	.2288+05	-.3086+03	.3774+03	.4881+02	-.5274+02

(0.147)R

0	.7629-00				
1-5,C	.9320+03	.8196+02	.2283+02	.4200+01	-.8845+01
1-5,S	.3407+04	-.4870+02	.2260+02	.5325-00	.9233+01

(0.325)R

0	-.1966+02				
1-5,C	.7354+02	-.3026+01	-.7486+02	.7950+01	±.2599+02
1-5,S	.4452+03	-.1666+02	-.8213+02	±.1507+02	.2029+02

(0.55)R

0	-.1704+02				
1-5,C	-.5488+01	.6038+02	-.1088+03	±.7612+01	.8284+01
1-5,S	.2088+03	-.2978+02	-.1379+03	±.1915+02	-.7092+01

(0.75)R

0	-.4249+01				
1-5,C	-.2361+02	.1121+03	-.8835+02	±.2231+02	.5038+02
1-5,S	.8029+02	-.3334+02	-.1284+03	±.1351+02	-.3668+02

(0.85)R

0	-.9629-01				
1-5,C	-.1667+02	.7897+02	-.5014+02	±.1656+02	.3913+02
1-5,S	.2825+02	-.2122+02	-.7684+02	±.7174+01	-.2826+02

N,C OR S — ADVANCE RATIO, MU = 0.7

(0.0)R

0	.2258+03				
1-5,C	.7325+04	.8967+03	.1115+04	.7543+02	.4482+02
1-5,S	.2042+05	-.4647+03	.4977+03	.6576+02	-.1709+03

(0.147)R

0	.1755+02				
1-5,C	.1348+04	.1461+03	.9999+02	.1116+02	-.7095+01
1-5,S	.3794+04	-.9360+02	.4855+02	.1555+01	.1785+02

(0.325)R

0	-.4540+02				
1-5,C	.1557+03	.3772+01	-.2552+03	±.1773+02	-.2546+02
1-5,S	.5965+03	-.3791+02	-.1081+03	±.2261+02	.7361+02

(0.55)R

0	-.4146+02				
1-5,C	.1674+02	.6703+02	-.4271+03	±.6397+02	-.2543-00
1-5,S	.2486+03	-.6366+02	-.1950+03	±.2571+02	-.3261+02

(0.75)R

0	-.1197+02				
1-5,C	-.1117+02	.1452+03	-.3724+03	±.7940+02	.2767+02
1-5,S	.9984+02	-.6666+02	-.1793+03	±.1466+02	-.1329+03

(0.85)R

0	-.1957+01				
1-5,C	-.9593+01	.9741+02	-.2133+03	±.5026+02	.2149+02
1-5,S	.3929+02	-.4060+02	-.1045+03	±.6837+01	-.9725+02

N,C OR S — ADVANCE RATIO, MU = 1.0

(0.0)R

0	.7356+03				
1-5,C	.8020+04	.1072+04	.2169+04	.1290+03	-.8579+02
1-5,S	.1756+05	-.6044+03	-.1341+03	±.1040+03	-.3011+03

(0.147)R

0	.1250+03				
1-5,C	.1866+04	.2414+03	.2747+03	.3804+01	-.9591+01
1-5,S	.4178+04	-.1786+03	-.1390+02	±.2431+02	.1560+02

(0.325)R

0	-.8271+02				
1-5,C	.2701+03	.3739+02	-.5521+03	±.6125+02	.1139+02
1-5,S	.7933+03	-.1162+03	.5708+02	.1333+02	.1260+03

(0.55)R

0	-.1145+03				
1-5,C	.4135+02	.6128+02	-.9554+03	±.8782+02	-.1174+02
1-5,S	.2402+03	-.1460+03	.1328+03	.6887+02	-.6444+02

(0.75)R

0	-.6667+02				
1-5,C	.1036+02	.1098+03	-.7920+03	±.6469+02	-.2598+02
1-5,S	.5335+02	-.1156+03	.1333+03	.8362+02	-.2203+03

(0.85)R

0	-.3123+02				
1-5,C	.4769+01	.6910+02	-.4366+03	±.3817+02	-.2039+02
1-5,S	.9824+01	-.8315+02	.7793+02	.5112+02	-.1531+03

N,C OR S — ADVANCE RATIO, MU = 1.4

(0.0)R

0	.1775+04				
1-5,C	.7771+04	.1025+04	.1826+04	±.2212+03	±.1801+03
1-5,S	.1484+05	-.4208+03	-.1514+04	±.3612+02	.7180+02

(0.147)R

0	.4554+03				
1-5,C	.2254+04	.3299+03	.3418+03	±.5022+02	-.7939-00
1-5,S	.4552+04	-.2186+03	-.2101+03	±.2133+02	.3990+02

(0.325)R

0	-.6739+02				
1-5,C	.3207+03	.1360+03	-.4166+03	.5121+02	.6492+02
1-5,S	.1117+04	-.2223+03	.5609+03	.3053+02	.9030+01

(0.55)R

0	-.1842+03				
1-5,C	-.4370+02	.1538+03	-.7456+03	.1496+03	-.4325+02
1-5,S	.3148+03	-.1847+03	.9977+03	.1957+03	-.9855+02

(0.75)R

0	-.1202+03				
1-5,C	-.2922+02	.1295+03	-.5709+03	.1472+03	-.1187+03
1-5,S	.5050+02	-.7508+02	.7966+03	.2327+03	±.1356+03

(0.85)R

0	-.5651+02				
1-5,C	-.9210+01	.7124+02	-.3004+03	.8352+02	-.7829+02
1-5,S	.2696+01	-.2799+02	.4258+03	.1380+03	-.8249+02

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 7.
A1S CYCLIC PITCH TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(C) MP ± 0.1
FP ± 0.01 (POR MU = 0.25,0.4,0.5)
FP ± 0.00447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S		ADVANCE RATIO, MU ± 0.25			
		(0.0)R			
0	.2811+02				
1-5,C	.6036+04	.2948+03	.1837+02	±.2173+02	±.2050+02
	.1087+05	-.5111+03	-.7826+02	±.2811+02	±.2022+02
		(0.14)R			
0	.6237+01				
1-5,C	.2323+04	.1115+03	.3262+01	±.8154+01	±.7822+01
1-5,S	.4241+04	-.1260+03	-.2237+02	±.1164+02	-.8746+01
		(0.32)R			
0	-.8542+01				
1-5,C	.6920+03	.3781+02	-.7148+01	±.1911+01	-.2008+01
1-5,S	.1386+04	-.5327+02	.9084+01	±.4871+01	-.4331+01
		(0.55)R			
0	-.1618+02				
1-5,C	.1876+03	.3532+02	-.1165+02	.2687-00	.2518-00
1-5,S	.5110+03	-.3837+02	.1957+02	±.2198+01	±.2494+01
		(0.75)R			
0	-.1207+02				
1-5,C	.3828+02	.3101+02	-.8052+01	.5925-00	.7083-00
1-5,S	.1786+03	-.2422+02	.1319+02	±.5888-00	-.9347-00
		(0.85)R			
0	-.6194+01				
1-5,C	.9498+01	.1710+02	-.4026+01	.3467-00	.4293-00
1-5,S	.7057+02	-.1210+02	.6481+01	±.1596-00	±.3501-00

N,C OR S		ADVANCE RATIO, MU ± 0.4			
		(0.0)R			
0	.1006+01				
1-5,C	.6122+04	.5387+03	.8610+02	-.1431+02	-.1742+02
1-5,S	.1099+05	-.4399+03	-.1068+03	±.3296+02	-.1929+02
		(0.14)R			
0	-.9502+01				
1-5,C	.2353+04	.2004+03	.2477+02	-.4819+01	-.6488+01
1-5,S	.4297+04	-.1779+03	-.2164+02	±.1041+02	-.7330+01
		(0.32)R			
0	-.2410+02				
1-5,C	.6968+03	.8030+02	-.1056+02	-.1116+01	-.1504+01
1-5,S	.1421+04	-.7453+02	.3253+02	.2792+01	-.1867+01
		(0.55)R			
0	-.3238+02				
1-5,C	.1883+03	.5124+02	-.2455+02	±.2504+01	.4342-01
1-5,S	.5439+03	-.5323+02	.4981+02	.1016+02	.1323-00
		(0.75)R			
0	-.2192+02				
1-5,C	.4021+02	.4683+02	-.1780+02	-.3005+01	.2440-00
1-5,S	.1996+03	-.5358+02	.3151+02	.8668+01	.9211-00
		(0.85)R			
0	-.1093+02				
1-5,C	.1063+02	.2019+02	-.9000+01	±.1755+01	.1417-00
1-5,S	.8061+02	-.1678+02	.1519+02	.4615+01	.3177-00

N,C OR S		ADVANCE RATIO, MU ± 0.5			
		(0.0)R			
0	.2817+02				
1-5,C	.6439+04	.6524+03	.1776+03	-.5475+02	-.3261+02
1-5,S	.1103+05	-.5483+03	-.3323+03	-.4704+01	-.3428+02
		(0.14)R			
0	-.4398+01				
1-5,C	.2472+04	.2404+03	.4788+02	-.8767+01	-.7397+01
1-5,S	.4317+04	-.2185+03	-.6847+02	-.6267+01	-.6413+01
		(0.32)R			
0	-.2854+02				
1-5,C	.7263+03	.7830+02	-.2830+02	.1798+02	.5299+01
1-5,S	.1431+04	-.8552+02	.1086+03	-.6284+01	.7276+01
		(0.55)R			
0	-.2849+02				
1-5,C	.1963+03	.9490+02	-.5623+02	.1683+02	.2593+01
1-5,S	.5363+03	-.5731+02	.1891+03	.4447+01	.1130+01
		(0.75)R			
0	-.1243+02				
1-5,C	.4361+02	.9313+02	-.3678+02	.4513+01	-.2442+01
1-5,S	.1652+03	-.5620+02	.1344+03	.9841+01	-.5784+01
		(0.85)R			
0	-.4969+01				
1-5,C	.1250+02	.9248+02	-.1927+02	.9247+00	-.2026+01
1-5,S	.7108+02	-.1818+02	.6786+02	.6158+01	-.4127+01

N,C OR S		ADVANCE RATIO, MU ± 0.7			
		(0.0)R			
0	.1560+03				
1-5,C	.7119+04	.9551+03	.1751+03	±.8449+02	-.5379+02
1-5,S	.9330+04	-.8415+03	-.4877+03	±.2946+02	-.5669+02
		(0.14)R			
0	.3438+02				
1-5,C	.3067+04	.3952+03	.6945+02	±.1874+02	-.1245+02
1-5,S	.4103+04	-.3820+03	-.1063+03	±.9184+01	±.8823+01
		(0.32)R			
0	-.4484+02				
1-5,C	.1037+04	.1417+03	.1519+02	±.3126+02	.1096+02
1-5,S	.1539+04	-.1748+03	.1774+03	.7533+01	.1508+02
		(0.55)R			
0	-.5505+02				
1-5,C	.3129+03	.1419+03	.3755+01	±.5569+02	.6861+01
1-5,S	.5996+03	-.1178+03	.3003+03	±.3158+02	.6355+01
		(0.75)R			
0	-.2460+02				
1-5,C	.8324+02	.1276+03	.4532+01	.3910+02	-.3688+01
1-5,S	.2065+03	-.6922+02	.2028+03	.3056+02	-.9141+01
		(0.85)R			
0	-.9771+01				
1-5,C	.2850+02	.7008+02	.2835+01	.1952+02	±.3266+01
1-5,S	.8161+02	-.5364+02	.9988+02	.1674+02	±.6563+01

N,C OR S		ADVANCE RATIO, MU ± 1.0			
		(0.0)R			
0	.5579+03				
1-5,C	.7761+04	.1213+04	.1487+03	±.6965+02	±.3458+02
1-5,S	.7875+04	-.1258+04	-.6277+03	±.5109+03	.1106+03
		(0.14)R			
0	.2045+03				
1-5,C	.3774+04	.5782+03	.9915+02	±.2488+02	±.1126+02
1-5,S	.3912+04	-.6630+03	-.1538+03	.1258+03	.3427+02
		(0.32)R			
0	-.3769+02				
1-5,C	.1457+04	.2363+03	.9758+02	.3415+02	-.3693+01
1-5,S	.1640+04	-.3659+03	.2426+03	-.1816+03	-.4371+02
		(0.55)R			
0	-.1135+03				
1-5,C	.4725+03	.1664+03	.1113+03	.1141+03	-.2163+02
1-5,S	.6182+03	-.2457+03	.4277+03	±.2978+03	-.1167+03
		(0.75)R			
0	-.6603+02				
1-5,C	.1315+03	.1204+03	.7388+02	.1030+03	-.2465+02
1-5,S	.1804+03	-.1291+03	.2861+03	±.1859+03	-.9689+02
		(0.85)R			
0	-.2962+02				
1-5,C	.4654+02	.6271+02	.3643+02	.5495+02	-.1388+02
1-5,S	.6628+02	-.5955+02	.1394+03	±.8819+02	-.5856+02

N,C OR S		ADVANCE RATIO, MU ± 1.4			
		(0.0)R			
0	.1521+04				
1-5,C	.8116+04	.1335+04	.1561+03	.1140+04	.3715+03
1-5,S	.7296+04	-.1466+04	-.3244+03	.7441+03	.5304+03
		(0.14)R			
0	.7196+03				
1-5,C	.4391+04	.7509+03	.1771+03	.3199+03	.1038+03
1-5,S	.4057+04	-.9209+03	-.3579+02	.2263+03	.1591+03
		(0.32)R			
0	.1274+03				
1-5,C	.1870+04	.3953+03	.2373+03	-.3819+03	-.1588+03
1-5,S	.1869+04	-.5149+03	.2524+03	-.2239+03	-.1691+03
		(0.55)R			
0	-.1274+03				
1-5,C	.6167+03	.2569+03	.2338+03	±.6239+03	.3189+03
1-5,S	.7101+03	-.4153+03	.3908+03	±.4087+03	-.3123+03
		(0.75)R			
0	-.1001+03				
1-5,C	.1660+03	.1450+03	.1245+03	±.3651+03	±.2254+03
1-5,S	.1951+03	-.1953+03	.2510+03	±.2554+03	-.1594+03
		(0.85)R			
0	-.4823+02				
1-5,C	.5772+02	.6918+02	.5601+02	±.1676+03	-.1113+03
1-5,S	.6357+02	-.6502+02	.1203+03	±.1284+03	-.9485+03

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 7.
AIS CYCLIC PITCH TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(D) MP = 0.3
FP = 0.001 (FOR MU = 0.25,0.4,0.5)
FP = 0.000447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S — ADVANCE RATIO, MU = 0.25

(0.0)R

0	-.5566+02				
1-5,C	.3567+04	.2787+03	.7887+02	.3741+02	.3106+01
1-5,S	.3509+05	.5899+02	.1837+03	.9520+02	.7217+02

(0.14)R

0	-.3721+01				
1-5,C	.1466+03	.1397+02	-.2460+01	-.2530+01	.2236+01
1-5,S	.1015+04	-.6457+01	.3652+01	-.4672-00	-.2171+01

(0.325)R

0	-.7019+01				
1-5,C	-.6244+02	.6541+01	-.9106+01	-.4050+01	.7019+01
1-5,S	.9820+02	-.4306+02	-.1513+02	-.8646+01	-.9157+01

(0.55)R

0	-.1359+02				
1-5,C	-.1009+03	.2880+02	.6832+01	.8461+01	.6511+01
1-5,S	.1209+03	.2510+01	-.2995+02	-.3411+01	.1051+01

(0.75)R

0	-.6556+01				
1-5,C	-.7037+02	.5880+02	.2992+02	.1709+02	.7989+01
1-5,S	.5853+01	-.1115+01	-.3363+02	.5565+01	.1723+02

(0.85)R

0	-.3693-00				
1-5,C	-.4174+02	.5035+02	.2748+02	.1329+02	-.1125+02
1-5,S	-.3874+02	-.5632+01	-.2331+02	.6349+01	.1667+02

N,C OR S — ADVANCE RATIO, MU = 0.4

(0.0)R

0	-.2144+03				
1-5,C	.3697+04	.5119+03	.1998+03	.6300+02	.1639+02
1-5,S	.3503+05	.1356+03	.3710+03	.2064+03	.1460+03

(0.14)R

0	-.1426+02				
1-5,C	.1452+03	.2369+02	-.1234+01	-.1850-00	.4444+01
1-5,S	.1619+04	-.1044+02	.1035+02	-.1223+01	-.3946+01

(0.325)R

0	-.1667+02				
1-5,C	-.6435+02	.3629+01	-.2111+02	.1402+01	.9939+01
1-5,S	.1152+03	-.2038+02	-.2733+02	.1719+02	-.1664+02

(0.55)R

0	-.2524+02				
1-5,C	-.1013+03	.3332+02	-.1659+01	.1129+02	.1115+02
1-5,S	.1464+03	-.2421+01	-.6744+02	-.9760+01	.1677+01

(0.75)R

0	-.8156+01				
1-5,C	-.7935+02	.6520+02	.4626+02	.1867+02	.1023+01
1-5,S	.1651+02	-.1485+02	-.8555+02	-.7414+01	.2486+02

(0.85)R

0	.2076+01				
1-5,C	-.4276+02	.7665+02	.4818+02	.1393+02	-.3246+01
1-5,S	-.3840+02	-.1972+02	-.6199+02	-.6324+01	.2319+02

N,C OR S — ADVANCE RATIO, MU = 0.5

(0.0)R

0	-.2227+03				
1-5,C	.3949+04	.6333+03	.3951+03	.1032+03	.8120+02
1-5,S	.3504+05	.5316+02	.5491+03	.2924+03	.2776+03

(0.14)R

0	-.1726+02				
1-5,C	.1543+03	.2933+02	-.7517-00	.9831-00	-.1260+01
1-5,S	.1621+04	-.1087+02	.1668+02	-.6614-00	-.1467+02

(0.325)R

0	-.2241+02				
1-5,C	-.6714+02	-.1035+01	-.4738+02	.5762-00	-.4418+01
1-5,S	.1261+03	-.8045+01	-.4627+02	-.2267+02	.4557+02

(0.55)R

0	-.2519+02				
1-5,C	-.9905+02	.3945+02	-.4124+02	.7350+01	.1412+02
1-5,S	.1596+03	.1770+02	-.1209+03	-.2388+02	.1855+01

(0.75)R

0	.7179+01				
1-5,C	-.7248+02	.1365+03	.2437+02	.4666+01	.3417+02
1-5,S	-.5668+01	-.5083+01	-.1425+03	.4385+02	.6196+02

(0.85)R

0	.1796+02				
1-5,C	-.3703+02	.1295+03	.4127+02	-.9699+01	.2561+02
1-5,S	-.6864+02	-.1796+02	-.9840+02	-.4001+02	.6047+02

N,C OR S — ADVANCE RATIO, MU = 0.7

(0.0)R

0	.4717+03				
1-5,C	.4054+04	.3422+03	.4686+03	.1150+03	.1720+03
1-5,S	.3142+05	-.3393+03	.2723+03	.1637+03	.2011+03

(0.14)R

0	.1201+02				
1-5,C	.2374+03	.4367+02	.1809+02	-.6504+01	-.2652+02
1-5,S	.2159+04	-.5631+02	.1591+02	.2046+02	-.2272+02

(0.325)R

0	-.4290+02				
1-5,C	-.7854+02	.4749+02	-.6620+02	-.1450+02	-.6452+02
1-5,S	.1883+03	-.4110+02	-.3829+02	.5200+02	-.7244+02

(0.55)R

0	-.4271+02				
1-5,C	-.9566+02	.1147+03	-.1250+03	-.9508+01	.1761+02
1-5,S	.1619+03	-.9027+01	-.1482+03	-.5179+01	-.4739+01

(0.75)R

0	-.1354+02				
1-5,C	-.5969+02	.2120+03	-.7108+02	-.5005+02	.6416+03
1-5,S	.3735+02	-.4197+02	-.2197+03	.5228+02	.1378+03

(0.85)R

0	-.4031-00				
1-5,C	-.2896+02	.1723+03	-.2317+02	.5017+02	.1275+03
1-5,S	-.1596+02	-.4674+02	-.1618+03	.4784+02	.1334+03

N,C OR S — ADVANCE RATIO, MU = 1.0

(0.0)R

0	.5556+03				
1-5,C	.4819+04	.9446+03	.1507+04	.6266+03	.9659+03
1-5,S	.2769+05	-.2995+03	.6203+03	.4153+03	.4197+03

(0.14)R

0	.2136+02				
1-5,C	.4166+03	.1258+03	.8178+02	.2643+02	-.1065+03
1-5,S	.2894+04	-.5900+02	.7409+02	.7954+01	-.9055+01

(0.325)R

0	-.9366+02				
1-5,C	-.1212+03	.2356+02	-.2404+03	.1569+03	-.3636+03
1-5,S	.2732+03	.4223+01	-.5031+02	.7388+02	-.7081+02

(0.55)R

0	-.1064+03				
1-5,C	-.1293+03	-.9198+01	-.4648+03	.7922+02	.4854+02
1-5,S	.1443+03	.6364+02	-.2335+03	.7545+02	-.7531+02

(0.75)R

0	-.2339+02				
1-5,C	-.9425+02	.7219+02	-.4275+03	.1503+02	.6523+03
1-5,S	-.6369+01	-.4908+02	-.2693+03	.3662+02	-.1666+03

(0.85)R

0	.9314+01				
1-5,C	-.5038+02	.7674+02	-.2932+03	.2515+02	.5599+03
1-5,S	-.4066+02	-.7363+02	-.1698+03	.1444+02	-.1400+03

N,C OR S — ADVANCE RATIO, MU = 1.4

(0.0)R

0	.1415+04				
1-5,C	.3897+04	-.1136+02	.9092+03	.8393+02	.2691+03
1-5,S	.2376+05	-.1032+02	-.5361+03	.8052+01	-.2662+03

(0.14)R

0	.1404+03				
1-5,C	.3975+03	.1081+03	.1929+03	.1098+02	-.2309+02
1-5,S	.3612+04	-.1209+03	.3925+02	.2431+02	.6769+02

(0.325)R

0	-.1246+03				
1-5,C	-.2666+03	.2063+03	-.9521+02	.2413+02	.1089+03
1-5,S	.3906+03	-.1088+03	.1559+03	.3878+02	.1659+03

(0.55)R

0	-.1242+03				
1-5,C	-.2238+03	.1686+03	-.3448+03	.5310+02	-.1846+01
1-5,S	.6644+02	.9344+02	.6051+02	.1039+03	-.9076+02

(0.75)R

0	-.6956+02				
1-5,C	-.9326+02	.1050+03	-.2580+03	.1048+03	.1344+03
1-5,S	-.1292+01	.3380+02	.9619+02	.2738+03	-.3568+03

(0.85)R

0	-.3440+02				
1-5,C	-.4166+02	.5861+02	-.1228+03	.7282+02	.1091+03
1-5,S	-.3356+01	-.1486+02	.8351+02	.2056+03	-.2704+03

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 7.
A1S CYCLIC PITCH TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(E) MP ± 0.3
FP = 0.0025 (FOR MU = 0.25,0.4,0.5)
FP = 0.00112(1+MU**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S — ADVANCE RATIO, MU ± 0.25

(0.0)R

0	-.7669+02				
1-5,C	.3371+04	.2493+03	.1184+03	.2764+02	.7499+01
1-5,S	.2424+05	.8921+01	.1424+03	.6810+02	.3935+02

(0.14)R

0	-.1806+02				
1-5,C	.4551+03	.4297+02	.9021+01	.4816+01	.4944+01
1-5,S	.3601+04	-.8534+01	.1551+02	.7092+01	.4984+01

(0.325)R

0	-.1633+02				
1-5,C	-.5186+02	.2527+02	-.1788+02	.2168-00	.6167+01
1-5,S	.4523+03	-.1935+02	-.1590+02	-.6199+01	-.1872+01

(0.55)R

0	-.1568+02				
1-5,C	-.1330+03	.4902+02	-.2271+02	-.6759+01	-.2836+01
1-5,S	.1942+03	-.1072+02	-.3859+02	-.9489+01	-.4717+01

(0.75)R

0	-.7632+01				
1-5,C	-.1220+03	.5471+02	-.1531+02	.1125+02	-.1201+02
1-5,S	.6276+02	.5247+01	-.4396+02	-.7702+01	-.5207+01

(0.85)R

0	-.3125+01				
1-5,C	-.7209+02	.5471+02	-.7922+01	-.7768+01	-.9153+01
1-5,S	.1718+02	.6336+01	-.2799+02	-.4363+01	-.3282+01

N,C OR S — ADVANCE RATIO, MU ± 0.4

(0.0)R

0	-.2267+03				
1-5,C	.3435+04	.4497+03	.2817+03	.8328+02	.9422+02
1-5,S	.2412+05	.5341+02	.2910+03	.1493+03	.9063+02

(0.14)R

0	-.4562+02				
1-5,C	.4629+03	.6959+02	.1939+02	.8621+01	.3925+01
1-5,S	.3594+04	-.7431+01	.3471+02	.1589+02	.9701+01

(0.325)R

0	-.3086+02				
1-5,C	-.5330+02	.2623+02	-.4594+02	-.8594+01	-.5993+01
1-5,S	.4729+03	-.3184+02	-.2894+02	.1367+02	-.7248+01

(0.55)R

0	-.2858+02				
1-5,C	-.1310+03	.6301+02	-.5289+02	-.1586+02	.1266+01
1-5,S	.2218+03	-.2738+02	-.8663+02	-.2394+02	.1016+02

(0.75)R

0	-.1361+02				
1-5,C	-.1162+03	.7924+02	-.3047+02	.1532+02	.9880+01
1-5,S	.8317+02	-.7223+01	-.1070+03	.2204+02	-.7309+01

(0.85)R

0	-.5469+01				
1-5,C	-.6761+02	.5165+02	-.1427+02	-.9277+01	.7752+01
1-5,S	.2826+02	-.4866-00	-.6958+02	.1312+02	-.3911+01

N,C OR S — ADVANCE RATIO, MU ± 0.5

(0.0)R

0	-.2167+03				
1-5,C	.3627+04	.5151+03	.5137+03	.1294+03	.1510+03
1-5,S	.2407+05	.1947-00	.4168+03	.2192+03	.1136+03

(0.14)R

0	-.5051+02				
1-5,C	.4909+03	.7673+02	.3471+02	.1556+02	-.3834+01
1-5,S	.3593+04	-.1275+02	.4628+02	.2107+02	.1516+02

(0.325)R

0	-.4089+02				
1-5,C	-.4863+02	.3094+02	-.9064+02	-.1195+02	-.4107+02
1-5,S	.4845+03	-.2617+02	-.4864+02	.2481+02	-.5071+01

(0.55)R

0	-.2665+02				
1-5,C	-.1196+03	.9965+02	-.1226+03	-.3527+02	.7126+01
1-5,S	.2190+03	-.1801+02	-.1296+03	.3870+02	-.1821+02

(0.75)R

0	.1667+01				
1-5,C	-.1006+03	.1360+03	-.9109+02	-.4327+02	.6259+02
1-5,S	.6396+02	.1078+01	-.1540+03	-.3264+02	-.2311+02

(0.85)R

0	.6511+01				
1-5,C	-.5731+02	.9056+02	-.4963+02	.2608+02	.4925+02
1-5,S	.1327+02	.4388+01	-.9914+02	.1880+02	-.1511+02

N,C OR S — ADVANCE RATIO, MU ± 0.7

(0.0)R

0	.2365+03				
1-5,C	.3882+04	.4697+03	.7681+03	.2326+03	.1805+03
1-5,S	.2126+05	-.2713+03	.1184+03	.3031+02	-.1131+03

(0.14)R

0	.1262+02				
1-5,C	.6594+03	.9887+02	.7787+02	.1641+02	-.1841+02
1-5,S	.3969+04	-.8167+02	.3008+02	-.2539+01	.2001+02

(0.325)R

0	-.6015+02				
1-5,C	-.4197+02	.6715+02	-.1554+03	-.5998+02	-.8225+02
1-5,S	.6238+03	-.7754+02	-.1221+02	-.1199+02	.5966+02

(0.55)R

0	-.4996+02				
1-5,C	-.1191+03	.1587+03	-.2730+03	-.8530+02	.1128+02
1-5,S	.2487+03	-.7675+02	-.1263+03	.5759+01	-.3519+02

(0.75)R

0	-.9149+01				
1-5,C	-.7265+02	.1835+03	-.2454+03	-.6452+02	.1091+03
1-5,S	.8878+02	-.4113+02	-.1818+03	.2238+02	-.1209+03

(0.75)R

0	.1722+01				
1-5,C	-.3453+02	.1145+03	-.1420+03	-.3897+02	.8255+02
1-5,S	.3099+02	-.1849+02	-.1186+03	.1633+02	-.8751+02

N,C OR S — ADVANCE RATIO, MU ± 1.0

(0.0)R

0	.4911+03				
1-5,C	.4266+04	.8127+03	.1427+04	.4668+03	.1399+03
1-5,S	.1844+05	-.2464+03	-.8777+02	-.2160+02	-.1499+03

(0.14)R

0	.4957+02				
1-5,C	.9134+03	.2178+03	.2228+03	.4171+02	.8827+01
1-5,S	.4439+04	-.1103+03	.2055+02	.2496+01	.6482+02

(0.325)R

0	-.1255+03				
1-5,C	-.4073+02	.9517+02	-.2795+03	-.1313+03	-.4697+02
1-5,S	.8408+03	-.1118+03	.7941+02	.2970+02	.1358+03

(0.55)R

0	-.1304+03				
1-5,C	-.1334+03	.9739+02	-.5746+03	-.1364+03	-.4697+02
1-5,S	.2400+03	-.6651+02	.5538+02	.1086+03	-.1118+03

(0.75)R

0	-.5536+02				
1-5,C	-.3978+02	.7128+02	-.5229+03	.5904+02	-.1923+02
1-5,S	.3669+02	.3978+01	.1895+01	.1273+03	-.2537+03

(0.85)R

0	-.2050+02				
1-5,C	-.6873+01	.3797+02	-.2970+03	-.2231+02	-.6879+01
1-5,S	-.1992+01	.1315+02	-.7223+01	.7732+02	-.1999+03

N,C OR S — ADVANCE RATIO, MU ± 1.4

(0.0)R

0	.1334+04				
1-5,C	.3668+04	.2766+03	.9005+03	-.4101+02	-.9600+02
1-5,S	.1616+05	-.1747+03	-.8142+03	-.2207+03	.1346+03

(0.14)R

0	.3081+03				
1-5,C	.8893+03	.1815+03	.2296+03	-.3206+02	.1275+02
1-5,S	.4919+04	-.1631+03	-.1127+03	-.6943+02	.4405+02

(0.325)R

0	-.1066+03				
1-5,C	-.2095+03	.2300+03	-.9293+02	.1735+02	.6094+02
1-5,S	.1125+04	-.1898+03	.2536+03	.3836+02	-.9979+01

(0.55)R

0	-.1400+03				
1-5,C	-.2916+03	.2110+03	-.3152+03	.2041+03	-.3635+01
1-5,S	.2188+03	.1620+01	.3453+03	.2228+03	.9395+02

(0.75)R

0	-.4558+02				
1-5,C	-.7071+02	.9798+02	-.3068+03	.2548+03	-.5953+02
1-5,S	.3320+02	.1544+03	.2148+03	.2551+03	-.1112+03

(0.85)R

0	-.1201+02				
1-5,C	-.7167+01	.4049+02	-.1728+03	.1524+03	-.4178+02
1-5,S	-.4246+02	.1091+03	.1040+03	.1499+03	-.6576+02

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 7.
AIS CYCLIC PITCH TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(F) MP = 0.3
FP = 0.01 (FOR MU = 0.25,0.4,0.5)
FP = 0.00447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S					
ADVANCE RATIO, MU = 0.25					
		(0.0)R			
0	-.2517+02				
1-S,C	.3261+04	.2822+03	.9391+02	.2015+02	.1263+02
1-S,S	.1306+05	-.3579+02	-.2456+02	.5141+01	.9502+01
		(0.14)R			
0	-.1954+02				
1-S,C	.1195+04	.1210+03	.2621+02	.6277+01	.4017+01
1-S,S	.5213+04	-.3497+02	.1712+01	.5121+01	.4887+01
		(0.325)R			
0	-.2609+02				
1-S,C	.2295+03	.7168+02	-.1259+02	-.2786-00	.4210-00
1-S,S	.1699+04	-.3514+02	.1949+02	.8180+01	.3718+01
		(0.55)R			
0	-.2963+02				
1-S,C	-.7711+02	.6253+02	-.2611+02	-.3984-00	.1482+01
1-S,S	.6095+03	-.4318+02	.1725+02	.1007+02	.2899+01
		(0.75)R			
0	-.1848+02				
1-S,C	-.9162+02	.3521+02	-.1780+02	.7789-00	.2174+01
1-S,S	.1993+03	-.1867+02	.5511+01	.6598+01	.1318+01
		(0.85)R			
0	-.8937+01				
1-S,C	-.4944+02	.3325+02	-.8798+01	.6036-00	.1313+01
1-S,S	.7536+02	-.6234+01	.1587+01	.3256+01	.5495-00

N,C OR S					
ADVANCE RATIO, MU = 0.4					
		(0.0)R			
0	-.1148+03				
1-S,C	.3260+04	.4738+03	.2484+03	.6502+02	.3439+02
1-S,S	.1323+05	-.1243+03	-.8868+02	.6731-00	.2350+02
		(0.14)R			
0	-.6269+02				
1-S,C	.1201+04	.1973+03	.6918+02	.1990+02	.1010+02
1-S,S	.5177+04	-.6114+02	-.2129+01	.9408+01	.1135+02
		(0.325)R			
0	-.5617+02				
1-S,C	.2335+03	.1052+03	-.3695+02	-.4863+01	-.2068+01
1-S,S	.1712+04	-.8150+02	.5545+02	.2346+02	.8152+01
		(0.55)R			
0	-.5451+02				
1-S,C	-.6418+02	.1166+03	-.8171+02	-.1392+02	-.3036+01
1-S,S	.6413+03	-.5987+02	.5482+02	.3366+02	.7950+01
		(0.75)R			
0	-.3155+02				
1-S,C	-.7764+02	.9056+02	-.5993+02	-.1007+02	-.3875-00
1-S,S	.2227+03	-.1995+02	.2172+02	.2404+02	.4495+01
		(0.85)R			
0	-.1487+02				
1-S,C	-.4134+02	.4783+02	-.3046+02	-.5068+01	.1516-00
1-S,S	.8689+02	-.6303+01	.7905+01	.1222+02	.2154+01

N,C OR S					
ADVANCE RATIO, MU = 0.5					
		(0.0)R			
.0	-.1027+03				
1-S,C	.3444+04	.5693+03	.4556+03	.7449+02	.3337+02
1-S,S	.1313+05	-.1757+03	-.2366+03	-.7237+01	.1655+02
		(0.14)R			
0	-.6577+02				
1-S,C	.1258+04	.2325+03	.1210+03	.2886+02	.1221+02
1-S,S	.5150+04	-.1047+03	-.3105+02	.6243+01	.1633+02
		(0.325)R			
0	-.6631+02				
1-S,C	.2472+03	.1247+03	-.8473+02	.4323+01	.2835+01
1-S,S	.1711+04	-.9263+02	.1051+03	.3172+02	.1973+02
		(0.55)R			
0	-.5294+02				
1-S,C	-.5267+02	.1602+03	-.1785+03	-.1449+02	.1032+01
1-S,S	.6325+03	-.5862+02	.1349+03	.5652+02	.8809+01
		(0.75)R			
0	-.2150+02				
1-S,C	-.6549+02	.1347+03	-.1326+03	-.1704+02	.9355-00
1-S,S	.2084+03	-.1315+02	.7550+02	.4359+02	-.2861+01
		(0.85)R			
0	-.8198+01				
1-S,C	-.3429+02	.7264+02	-.6775+02	-.9746+01	.5473-00
1-S,S	.7810+02	-.1853+01	.3448+02	.2408+02	-.3030+01

N,C OR S					
ADVANCE RATIO, MU = 0.7					
		(0.0)R			
0	.7271+02				
1-S,C	.3965+04	.6778+03	.5876+03	.6378+02	.3363+02
1-S,S	.1160+05	-.4737+03	-.6907+03	-.1596+03	-.3845+01
		(0.14)R			
0	-.2022+02				
1-S,C	.1659+04	.3931+03	.1952+03	.3389+02	.1966+02
1-S,S	.5104+04	-.2577+03	-.1439+03	-.2499+02	.2233+02
		(0.325)R			
0	-.9468+02				
1-S,C	.4192+03	.2003+03	-.6471+02	.3427+02	.1344+02
1-S,S	.1921+04	-.1699+03	.2442+03	.9399+02	.4179+02
		(0.55)R			
0	-.9103+02				
1-S,C	.2564+02	.2176+03	-.1954+03	.5751+02	.3643+01
1-S,S	.7519+03	-.8807+02	.3628+03	.1736+03	.1972+02
		(0.75)R			
0	-.3848+02				
1-S,C	-.1868+02	.1717+03	-.1507+03	.4815+02	-.2970+01
1-S,S	.2867+03	-.1512+02	.2161+03	.1306+03	-.5872+01
		(0.85)R			
0	-.1403+02				
1-S,C	-.1013+02	.7066+02	-.7716+02	.2558+02	-.2378+01
1-S,S	.1017+03	-.3624-00	.1024+03	.6683+02	-.6279+01

N,C OR S					
ADVANCE RATIO, MU = 1.0					
		(0.0)R			
0	.3966+03				
1-S,C	.3869+04	.6750+03	.3078+03	-.2075+03	.5520+02
1-S,S	.1011+05	-.3059+03	-.1074+04	.5375+02	.1811+03
		(0.14)R			
0	.1001+03				
1-S,C	.1773+04	.4574+03	.1594+03	.4331+02	.2576+02
1-S,S	.5063+04	-.4238+03	-.2942+03	.1253+02	.6480+02
		(0.325)R			
0	-.1195+03				
1-S,C	.5061+03	.6603+03	.6108+02	.1477+03	.5215+01
1-S,S	.2065+04	-.5637+03	.3106+03	.1676+02	-.4491+02
		(0.55)R			
0	-.1652+03				
1-S,C	.5514+02	.2227+03	-.2101+02	.3386+03	-.8975+01
1-S,S	.7404+03	-.2330+03	.5298+03	-.1916+02	-.1431+03
		(0.75)R			
0	-.8059+02				
1-S,C	.8170+01	.1455+03	-.4223+02	.2754+03	-.9779+01
1-S,S	.2046+03	-.7123+02	.3272+03	-.7201+01	-.1213+03
		(0.85)R			
0	-.3408+02				
1-S,C	.5721+01	.7231+02	-.2497+02	.1431+03	-.5345+01
1-S,S	.6853+02	-.2174+02	.1545+03	-.2499+01	-.6356+02

N,C OR S					
ADVANCE RATIO, MU = 1.4					
		(0.0)R			
0	.9993+03				
1-S,C	.3456+04	.8301+03	-.1309+03	.1277+03	.8080+03
1-S,S	.9263+04	-.2552+03	-.9286+03	.8350+03	.3498+03
		(0.14)R			
0	.4041+03				
1-S,C	.1671+04	.4221+03	.7990+02	.5353+02	.1869+03
1-S,S	.5104+04	-.3691+03	-.2789+03	.2161+03	.9977+02
		(0.325)R			
0	-.4607+02				
1-S,C	.4176+03	.3320+03	.2597+03	.3538+02	-.2347+03
1-S,S	.2336+04	-.4892+03	.2566+03	-.3518+03	-.1338+03
		(0.55)R			
0	-.1820+03				
1-S,C	-.2914+02	.2773+03	.2222+03	.1087+03	-.4602+03
1-S,S	.8197+03	-.3274+03	.4139+03	-.6117+03	-.2566+03
		(0.75)R			
0	-.9461+02				
1-S,C	-.1869+02	.1513+03	.7561+02	.1081+03	-.3139+03
1-S,S	.1935+03	-.6097+02	.2267+03	-.3938+03	-.1737+03
		(0.85)R			
0	-.3983+02				
1-S,C	-.2027+01	.6969+02	.2489+02	.5881+02	-.1531+03
1-S,S	.5599+02	-.1779+02	.1008+03	-.1882+03	-.8447+02

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 9.
A1S CYCLIC PITCH TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(G) MP = 0.5
FP = 0.001 (FOR MU = 0.25,0.4,0.5)
FP = 0.000447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S		ADVANCE RATIO, MU = 0.25			
		(0.0)R			
0	.2957+03				
1-5,C	.3004+04	-.5944+02	.1351+01	-.3812+02	-.3666+02
1-5,S	.3496+05	-.1463+03	.2072+02	-.1059+02	-.1197+02
		(0.14)R			
0	.1125+02				
1-5,C	.1023+03	.1140+02	-.5681+01	-.2781+01	-.2408+01
1-5,S	.1611+04	-.2512+02	-.3121-00	-.3360+01	-.2743+01
		(0.32)R			
0	-.2347+01				
1-5,C	-.1094+03	.3332+02	-.1340+02	-.3401+01	-.1535+01
1-5,S	.8161+02	-.1813+02	-.1179+02	-.6029+01	-.5167+01
		(0.55)R			
0	-.3760+01				
1-5,C	-.1759+03	.3305+02	-.2809+01	-.2685+01	-.6535-00
1-5,S	.7834+02	.2529+02	-.3104+02	-.5921+01	-.2948+01
		(0.75)R			
0	-.1354+02				
1-5,C	-.1139+03	.9673+02	.3048+02	.3423+01	.1645+01
1-5,S	-.1960+02	.4039+02	-.3008+02	-.3816+01	.6016+01
		(0.85)R			
0	-.1344+02				
1-5,C	-.4745+02	.5078+02	.3266+02	.4668+01	.1886+01
1-5,S	-.4625+02	.2026+02	-.1796+02	-.1663+01	.7340+01

N,C OR S		ADVANCE RATIO, MU = 0.4			
		(0.0)R			
0	.1691+03				
1-5,C	.3149+04	-.1286+02	.1046+03	-.1087+02	-.2712+02
1-5,S	.3467+05	-.1174+03	.1324+03	.6959+02	.5413+02
		(0.14)R			
0	.9371-00				
1-5,C	.1061+03	.1945+02	-.6302+01	.7739-01	-.1639+01
1-5,S	.1613+04	-.3460+02	.7920+01	-.6316+01	-.6522+01
		(0.32)R			
0	-.1377+02				
1-5,C	-.1105+03	.3104+02	-.2786+02	-.2595-01	.1603+01
1-5,S	.1063+03	-.2930+02	-.1629+02	-.1267+02	-.1477+02
		(0.55)R			
0	-.1500+02				
1-5,C	-.1079+03	.3779+02	-.9771+01	-.4609+01	.4765+01
1-5,S	.1060+03	.3267+02	-.6767+02	-.7198+01	-.9185-00
		(0.75)R			
0	-.1360+02				
1-5,C	-.1056+03	.1095+03	.5082+02	.9388+01	.7948-00
1-5,S	-.6611+01	.7487+02	-.8771+02	-.1991+02	.1782+02
		(0.85)R			
0	-.9695+01				
1-5,C	-.4332+02	.8269+02	.6555+02	-.7802+01	-.1578+01
1-5,S	-.4372+02	.2443+02	-.6184+02	-.2086+02	.1724+02

N,C OR S		ADVANCE RATIO, MU = 0.5			
		(0.0)R			
0	.1455+03				
1-5,C	.3393+04	.7089+02	.2366+03	.9491+01	.9128+01
1-5,S	.3461+05	-.2438+03	.2369+03	.1851+03	.1572+03
		(0.14)R			
0	-.4393+01				
1-5,C	.1012+03	.1911+02	-.1353+02	.5293+01	-.2361+01
1-5,S	.1626+04	-.2087+02	.8469+01	-.4634+01	-.1392+02
		(0.32)R			
0	-.2360+02				
1-5,C	-.1158+03	.4619+02	-.4378+02	.6949+01	-.3510+01
1-5,S	.1196+03	-.1191+02	-.2114+02	-.2387+02	-.3723+02
		(0.55)R			
0	-.2062+02				
1-5,C	-.1390+03	.1096+03	-.6829+01	-.7906+01	.8513+01
1-5,S	.1042+03	.2701+02	-.8648+02	-.2146+02	-.2073+01
		(0.75)R			
0	-.5183+01				
1-5,C	-.9761+02	.1535+03	.6020+02	-.2896+02	.2436+02
1-5,S	-.9200-00	.7876+02	-.1502+03	-.5402+01	.5926+02
		(0.85)R			
0	.1364+01				
1-5,C	-.5331+02	.1179+03	.6183+02	-.2623+02	.2148+02
1-5,S	-.3193+02	.8962+02	-.1219+03	.1368+01	.5941+02

N,C OR S		ADVANCE RATIO, MU = 0.7			
		(0.0)R			
0	.6583+02				
1-5,C	.3820+04	.4400+03	.6438+03	.3347+03	.3774+03
1-5,S	.3148+05	-.1569+03	.3240+03	.3739+03	.4190+03
		(0.14)R			
0	-.1618+02				
1-5,C	.1782+03	.3978+02	.1048+02	-.2206+02	-.4615+02
1-5,S	.2173+04	-.4475+02	.5047+02	-.1323+02	-.1702+02
		(0.32)R			
0	-.5132+02				
1-5,C	-.1585+03	.2362+02	-.1043+03	-.5707+02	-.1133+03
1-5,S	.1856+03	-.2335+02	-.5003+01	-.7262+02	-.1103+03
		(0.55)R			
0	-.4881+02				
1-5,C	-.1518+03	.8142+02	-.1349+03	-.1086+02	.3533+02
1-5,S	.1649+03	.4067+02	-.1826+03	-.4196+02	-.4782+02
		(0.75)R			
0	.4263+01				
1-5,C	-.8026+02	.1772+03	-.2211+02	-.3326+02	.2261+03
1-5,S	.1635+02	-.6961+01	-.2777+03	.1598+02	.1695+03
		(0.85)R			
0	.1962+02				
1-5,C	-.3638+02	.1484+03	.2612+02	-.3968+02	.1980+03
1-5,S	-.3615+02	-.5206+02	-.1991+03	.2471+02	.1814+03

N,C OR S		ADVANCE RATIO, MU = 1.0			
		(0.0)R			
0	.2479+03				
1-5,C	.3691+04	.6380+03	.1042+04	.5910+03	.7846+03
1-5,S	.2757+05	-.9754+02	.1238+03	.3430+03	.3850+03
		(0.14)R			
0	-.1760+02				
1-5,C	.2515+03	.1106+03	.8387+02	-.2113+02	-.6980+02
1-5,S	.2857+04	-.7123+02	.7862+02	-.2783+01	.2441+01
		(0.32)R			
0	-.9821+02				
1-5,C	-.2097+03	.4088+02	-.1566+03	-.1522+03	-.2997+03
1-5,S	.2466+03	-.1930+02	.5422+02	-.7125+02	-.6562+02
		(0.55)R			
0	-.9756+02				
1-5,C	-.1525+03	-.2699+02	-.3533+03	-.7641+02	-.3997-00
1-5,S	.1111+03	.1123+03	-.1360+03	-.3001+02	-.8630+02
		(0.75)R			
0	-.3026+02				
1-5,C	-.5926+02	.3573+02	-.2487+03	.5622+02	.9636+03
1-5,S	.9802-00	-.1225+02	-.1969+03	.4530+02	-.1239+03
		(0.85)R			
0	-.2366+01				
1-5,C	-.2493+02	.3156+02	-.1148+03	.6455+02	.8028+03
1-5,S	-.2310+02	-.6195+02	-.1256+03	.4615+02	-.9324+02

N,C OR S		ADVANCE RATIO, MU = 1.4			
		(0.0)R			
0	.1050+04				
1-5,C	.3419+04	-.4688+03	.6935+03	-.1858+03	.5017+03
1-5,S	.2354+05	.1326+03	-.7927+03	.1315+03	-.2420+03
		(0.14)R			
0	.6156+02				
1-5,C	.2392+03	.6284+02	.1414+03	.4421+01	-.2857+02
1-5,S	.3566+04	-.1392+03	.3861+02	-.5860+02	.6465+02
		(0.32)R			
0	-.1421+03				
1-5,C	-.4073+03	.2723+03	-.6235+02	.6358+02	-.2018+03
1-5,S	.3366+03	-.1124+03	.1974+03	-.9107+02	.1401+03
		(0.55)R			
0	-.9826+02				
1-5,C	-.2293+03	.1836+03	-.2694+03	.8825+02	-.1314+01
1-5,S	-.2627+01	.1923+03	.4585+02	.1233+03	-.9104+02
		(0.75)R			
0	-.5175+02				
1-5,C	-.9447+02	.8797+02	-.1192+03	.9566+02	.3302+03
1-5,S	.2744+02	.7019+02	.7643+02	.2621+03	-.2807+03
		(0.85)R			
0	-.3192+02				
1-5,C	-.5363+02	.2785+02	-.2017+02	.6605+02	.2745+03
1-5,S	.4022+02	-.1748+02	.7587+02	.1822+03	-.2046+03

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 7.
A1S CYCLIC PITCH TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(H) MP = 0.5
FP = 0.0025 (FOR MU = 0.25,0.4,0.5)
FP = 0.0012(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S — ADVANCE RATIO, MU = 0.25

(0.0)R

0	.6518+02				
1-5,C	.2782+04	-.3699+02	.4189+02	-.1158+02	-.1979+02
1-5,S	.2420+05	-.7986+02	.4026+02	-.2649+01	-.7108+01

(0.147)R

0	.4661+01				
1-5,C	.3342+03	.4436+02	-.4709+01	-.4213+01	-.4450+01
1-5,S	.3596+04	-.5036+02	.1483+01	-.2968+01	-.2535+01

(0.325)R

0	-.9865+01				
1-5,C	-.1410+03	.5324+02	-.2069+02	-.6075+01	-.3374+01
1-5,S	.4264+03	-.5291+02	-.1603+02	-.6301+01	-.4143+01

(0.55)R

0	-.1235+02				
1-5,C	-.2291+03	.6803+02	-.1085+02	-.7039+01	-.1883+01
1-5,S	.1474+03	.2801+01	-.4048+02	-.8099+01	-.3436+01

(0.75)R

0	-.8166+01				
1-5,C	-.1832+03	.6334+02	.7002+01	-.4664+01	.6466-06
1-5,S	.1589+02	.4300+02	-.4812+02	-.6064+01	-.8892+00

(0.85)R

0	-.4161+01				
1-5,C	-.1029+03	.5019+02	.7787+01	-.2399+01	.8869+00
1-5,S	-.1160+02	.3421+02	-.3108+02	-.3323+01	-.4954+01

N,C OR S — ADVANCE RATIO, MU = 0.4

(0.0)R

0	-.9481+02				
1-5,C	.2820+04	-.1353+02	.1657+03	.4131+02	.1844+02
1-5,S	.2405+05	-.4014+02	.1448+03	.5684+02	.4099+02

(0.147)R

0	-.2535+02				
1-5,C	.3393+03	.2597+02	.1136+00	-.7256-06	-.5652+01
1-5,S	.3575+04	-.3505+02	.1777+02	.2293+01	-.1162+01

(0.325)R

0	-.2648+02				
1-5,C	-.1380+03	.7801+02	-.4607+02	-.1533+02	-.1331+02
1-5,S	.4403+03	-.5373+02	-.2456+02	-.1486+02	-.1327+02

(0.55)R

0	-.2405+02				
1-5,C	-.2141+03	.1348+03	-.2841+02	-.1862+02	.2737+01
1-5,S	.1734+03	-.1121+02	-.9332+02	-.1967+02	-.6149+01

(0.75)R

0	-.9715+01				
1-5,C	-.1613+03	.1322+03	.9295+01	-.1240+02	.2862+02
1-5,S	.3307+02	.4485+02	-.1251+03	-.1548+02	.6008+01

(0.85)R

0	-.3182+01				
1-5,C	-.8815+02	.8059+02	.1309+02	-.6381+01	.1614+02
1-5,S	-.2799+01	.3844+02	-.8294+02	-.8671+01	.6065+01

N,C OR S — ADVANCE RATIO, MU = 0.5

(0.0)R

0	-.1218+03				
1-5,C	.2949+04	.2523+02	.3055+03	.9825+02	.1119+03
1-5,S	.2396+05	-.8056+02	.2270+03	.1184+03	.9628+02

(0.147)R

0	-.3597+02				
1-5,C	.3567+03	.3093+02	.1026+02	.4780+01	-.6324+02
1-5,S	.3569+04	-.4011+02	.3073+02	.5458+01	.6018-06

(0.325)R

0	-.3817+02				
1-5,C	-.1351+03	.8393+02	-.7030+02	-.2297+02	-.4953+02
1-5,S	.4584+03	-.5139+02	-.3123+02	-.2585+02	-.2496+02

(0.55)R

0	-.2285+02				
1-5,C	-.1968+03	.1650+03	-.6536+02	-.3437+02	.1457+02
1-5,S	.1773+03	-.4875+01	-.1368+03	-.3063+02	-.1251+02

(0.75)R

0	.5869+01				
1-5,C	-.1343+03	.1763+03	-.2202+02	-.2898+02	.7728+02
1-5,S	.2420+02	.5218+02	-.1876+03	-.1965+02	.9936+01

(0.85)R

0	.9260+01				
1-5,C	-.6963+02	.1103+03	-.4990+01	-.1671+02	.6025+02
1-5,S	-.1076+02	.4313+02	-.1251+03	-.9403+01	.1049+02

N,C OR S — ADVANCE RATIO, MU = 0.7

(0.0)R

0	-.9434+02				
1-5,C	.3373+04	.3507+03	.7227+03	.4058+03	.3888+03
1-5,S	.2130+05	-.1512+03	.1879+03	.1369+03	.8615+01

(0.147)R

0	-.5945+02				
1-5,C	.5286+03	.9016+02	.7835+02	.2836+02	-.1953+02
1-5,S	.4005+04	-.5271+02	.6563+02	.1907+02	.3990+02

(0.325)R

0	-.6457+02				
1-5,C	-.1355+03	.8441+02	-.1351+03	-.1012+03	-.1496+03
1-5,S	.6359+03	-.4745+02	.1934+02	-.1260+02	.4970+02

(0.55)R

0	-.4562+02				
1-5,C	-.2006+03	.1459+03	-.2462+03	-.1316+03	-.5836+01
1-5,S	.2407+03	-.7299+01	-.1655+03	-.2149+02	-.7088+02

(0.75)R

0	.1775+02				
1-5,C	-.1063+03	.1429+03	-.2262+03	-.8548+02	.1583+03
1-5,S	.6413+02	.3696+02	-.2755+03	-.1753+02	-.1638+03

(0.85)R

0	.2173+02				
1-5,C	-.4708+02	.8522+02	-.1318+03	-.4615+02	.1237+03
1-5,S	.1331+02	.2985+02	-.1843+03	-.9780+01	-.1144+03

N,C OR S — ADVANCE RATIO, MU = 1.0

(0.0)R

0	.3607+03				
1-5,C	.3361+04	.5784+03	.8827+03	.4889+03	.2199+03
1-5,S	.1871+05	-.2782+03	-.1405+03	-.4267+02	-.1350+03

(0.147)R

0	.1136+02				
1-5,C	.6528+03	.1850+03	.1716+03	.4032+02	.1104+02
1-5,S	.4483+04	-.1149+03	.2644+02	-.1263+02	.6772+02

(0.325)R

0	-.1376+03				
1-5,C	-.1861+03	.1224+03	-.1166+03	-.1344+03	-.7098+02
1-5,S	.8062+03	-.6006+02	.9903+02	.2410+02	.1384+03

(0.55)R

0	-.1113+03				
1-5,C	-.1799+03	.6846+02	-.3560+03	-.1063+03	-.4197+02
1-5,S	.1758+03	.4989+02	.1686+02	.1243+03	-.9867+02

(0.75)R

0	-.1956+02				
1-5,C	-.1546+02	.2631+02	-.3778+03	-.1220+02	.8289+02
1-5,S	-.1192+02	.1404+03	-.7353+02	.1547+03	-.2769+03

(0.85)R

0	.2949+01				
1-5,C	.1792+02	.3995+01	-.2238+03	.7670+01	.1613+02
1-5,S	-.2786+02	.9596+02	-.5709+02	.9510+02	-.1896+03

N,C OR S — ADVANCE RATIO, MU = 1.4

(0.0)R

0	.2306+04				
1-5,C	.4254+04	.1143+04	.4980+03	.2278+02	-.1651+02
1-5,S	.1831+05	-.1033+04	-.1028+04	-.2235+03	.1559+03

(0.147)R

0	.5620+03				
1-5,C	.9215+03	.4046+03	.2210+03	-.4327+02	.1279+02
1-5,S	.5476+04	-.3021+03	-.1481+03	-.1175+03	.6437+02

(0.325)R

0	-.1153+03				
1-5,C	-.4382+03	.1927+03	.1518+03	.1422+02	.3234+02
1-5,S	.1060+04	.7266+02	.3007+03	-.2997+02	.2809+01

(0.55)R

0	-.1508+03				
1-5,C	-.4430+03	.9918+02	.2425+02	.3711+03	.9634+02
1-5,S	.4191+02	.4757+03	.3968+03	.2564+03	-.1373+03

(0.75)R

0	-.1709+02				
1-5,C	-.5826+02	.1401+02	-.7588+02	.4815+03	.8340+02
1-5,S	-.1315+03	.3310+03	.2355+03	.3568+03	-.1787+03

(0.85)R

0	.1030+02				
1-5,C	.2296+02	-.2980+01	-.5681+02	.2901+03	.4581+02
1-5,S	-.8017+02	.3100+03	.1114+03	.2174+03	-.1076+03

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 7.
A1S CYCLIC PITCH TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(I) MP ± 0.5
FP = 0.01 (FOR MU = 0.25,0.4,0.5)
FP = 0.00447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S		ADVANCE RATIO, MU ± 0.25			
		(0.0)R			
0	-.3507+02				
1-5,C	.2529+04	.9708+02	.8254+02	.4409+01	±.5822+01
1-5,S	.1359+05	-.1448+02	-.4649+02	±.1799+02	-.4147+01
		(0.14)R			
0	-.2436+02				
1-5,C	.8565+03	.6508+02	.1669+02	±.1426+01	±.3623+01
1-5,S	.5295+04	-.4621+02	-.9399+01	±.4970+01	-.2081+01
		(0.32)R			
0	-.2788+02				
1-5,C	.1773+02	.8421+02	-.2734+02	±.6885+01	-.3868+01
1-5,S	.1702+04	-.7889+02	.7668+01	.2823+01	-.1423+01
		(0.55)R			
0	-.2654+02				
1-5,C	-.2541+03	.1130+03	-.4893+02	±.9144+01	-.2917+01
1-5,S	.5765+03	-.5088+02	-.2823+01	.6599+01	-.8247-00
		(0.75)R			
0	-.1387+02				
1-5,C	-.1916+03	.8172+02	-.3189+02	±.5913+01	-.1904+01
1-5,S	.1694+03	-.5055+01	-.1120+02	.5078+01	±.1814+00
		(0.85)R			
0	-.6202+01				
1-5,C	±.9631+02	.4182+02	-.1593+02	±.2893+01	-.3277-00
1-5,S	.5897+02	.2866+01	-.7381+01	.2628+01	±.2582-01

N,C OR S		ADVANCE RATIO, MU ± 0.7			
		(0.0)R			
0	-.9737+02				
1-5,C	.2974+04	.4936+03	.6101+03	.4097+02	.3813+02
1-5,S	.1163+05	-.1456+03	-.6688+03	±.2847+03	-.4828+02
		(0.14)R			
0	-.1019+03				
1-5,C	.1140+04	.2508+03	.1972+03	.2747+02	.1928+02
1-5,S	.5116+04	-.1636+03	-.1413+03	±.6087+02	.1429+02
		(0.32)R			
0	-.1326+03				
1-5,C	.1439+03	.2163+03	-.9967+02	.3588+02	.1760+02
1-5,S	.1913+04	-.2013+03	.2147+03	.1204+03	.5506+02
		(0.55)R			
0	-.9950+02				
1-5,C	-.1290+03	.2597+03	-.2897+03	.5543+02	.1410+02
1-5,S	.7236+03	-.9710+02	.2858+03	.2296+03	.2767+02
		(0.75)R			
0	-.3170+02				
1-5,C	-.7212+02	.1848+03	-.2367+03	.4318+02	.6303+01
1-5,S	.2356+03	.1579+02	.1478+03	.1789+03	-.8353+01
		(0.85)R			
0	-.9617+01				
1-5,C	-.2904+02	.9385+02	-.1237+03	.2247+02	.2601+01
1-5,S	.8823+02	.2190+02	.6452+02	.8709+02	-.8546+01

N,C OR S		ADVANCE RATIO, MU ± 0.4			
		(0.0)R			
0	-.1755+03				
1-5,C	.2509+04	.1849+03	.2437+03	.5259+02	.1614+02
1-5,S	.1336+05	.2805+02	-.1009+03	±.4170+02	.3464+01
		(0.14)R			
0	-.8883+02				
1-5,C	.8477+03	.1096+03	.5852+02	.1261+02	.1753+01
1-5,S	.5218+04	-.5375+02	-.1126+03	±.5932+01	.2830+01
		(0.32)R			
0	-.6550+02				
1-5,C	.1962+02	.1226+03	-.6223+02	±.1453+02	±.7394+01
1-5,S	.1702+04	-.1184+03	.3514+02	.2074+02	.3727+01
		(0.55)R			
0	-.5011+02				
1-5,C	-.2330+03	.1588+03	-.1223+03	-.3039+02	-.7906+01
1-5,S	.6012+03	-.8071+02	.9871+01	.3467+02	.3967+01
		(0.75)R			
0	-.2246+02				
1-5,C	-.1681+03	.1142+03	-.9135+02	±.2380+02	±.3400+01
1-5,S	.1875+03	-.9227+01	-.1911+02	.2506+02	.2057+01
		(0.85)R			
0	-.9290+01				
1-5,C	-.8297+02	.3839+02	-.4686+02	±.1241+02	±.1319+01
1-5,S	.6801+02	.3778+01	-.1438+02	.1274+02	.9392+00

N,C OR S		ADVANCE RATIO, MU ± 1.0			
		(0.0)R			
0	-.8946+01				
1-5,C	.2654+04	.2819+03	.3113+03	±.2734+03	.5755+02
1-5,S	.9925+04	-.4419+02	-.1066+04	±.1277+03	.1147+03
		(0.14)R			
0	-.1044+03				
1-5,C	.1097+04	.2209+03	.1452+03	±.6699+02	.3378+02
1-5,S	.4904+04	-.2267+03	-.2928+03	±.3890+02	.4968+02
		(0.32)R			
0	-.1990+03				
1-5,C	.1310+03	.2504+03	.3717+01	.1509+03	.1712+02
1-5,S	.1995+04	-.3849+03	.2916+03	.3415+02	-.2613+02
		(0.55)R			
0	-.1652+03				
1-5,C	-.1041+03	.2681+03	-.1406+03	.3358+03	-.4475+01
1-5,S	.6620+03	-.2422+03	.4663+03	.7372+02	-.1277+03
		(0.75)R			
0	-.5968+02				
1-5,C	-.1917+02	.1623+03	-.1410+03	.2884+03	-.1223+02
1-5,S	.1478+03	-.2891+02	.2678+03	.5294+02	-.1206+03
		(0.85)R			
0	-.2070+02				
1-5,C	.3564+01	.7733+02	-.7663+02	.1496+03	-.7462+01
1-5,S	.3958+02	.8161+01	.1222+03	.2639+02	±.6496+02

N,C OR S		ADVANCE RATIO, MU ± 0.5			
		(0.0)R			
0	-.2068+03				
1-5,C	.2600+04	.2304+03	.4301+03	.8224+02	.3512+02
1-5,S	.1321+05	.2604+02	-.1894+03	±.7969+02	-.9049+01
		(0.14)R			
0	-.1102+03				
1-5,C	.8795+03	.1309+03	.1080+03	.2611+02	.6941+01
1-5,S	.5168+04	-.6398+02	-.2478+02	±.1220+02	.7713+01
		(0.32)R			
0	-.8414+02				
1-5,C	.3048+02	.1449+03	-.1034+03	±.1166+02	±.8681+01
1-5,S	.1696+04	-.1350+03	.6851+02	.4022+02	.1893+02
		(0.55)R			
0	-.5246+02				
1-5,C	-.2092+03	.2014+03	-.2195+03	±.4358+02	±.7857+01
1-5,S	.5951+03	-.6108+02	.4936+02	.7342+02	.8760+01
		(0.75)R			
0	-.1326+02				
1-5,C	-.1421+03	.1524+03	-.1704+03	±.4054+02	±.1391+01
1-5,S	.1765+03	.1360+01	.8797-01	.5624+02	-.3682+01
		(0.85)R			
0	-.2753+01				
1-5,C	-.6805+02	.7924+02	-.8853+02	±.2216+02	.6765-01
1-5,S	.6111+02	.1105+02	-.6294+01	.2916+02	-.3614+01

N,C OR S		ADVANCE RATIO, MU ± 1.4			
		(0.0)R			
0	-.1627+02				
1-5,C	.2001+04	-.1786+03	-.7472+02	±.9321+02	.8393+03
1-5,S	.8364+04	.3738+03	-.9432+03	.4487+03	.1803+03
		(0.14)R			
0	-.1356+03				
1-5,C	.8107+03	.3279+02	.4711+02	±.2853+02	.1824+03
1-5,S	.4645+04	-.5297+02	-.2713+03	.1138+03	.2663+02
		(0.32)R			
0	-.2366+03				
1-5,C	-.3725+02	.2345+03	.1130+03	.6771+02	-.1454+03
1-5,S	.2105+04	-.5272+03	.2599+03	±.1977+03	-.5063+02
		(0.55)R			
0	-.1657+03				
1-5,C	-.1836+03	.2774+03	-.1479+01	.1880+03	-.3308+03
1-5,S	.6740+03	-.3814+03	.3572+03	±.3467+03	-.1056+03
		(0.75)R			
0	-.3702+02				
1-5,C	-.2360+02	.1482+03	-.7678+02	.1585+03	±.2414+03
1-5,S	.1058+03	-.5247+02	.1611+03	±.2262+03	-.9758+02
		(0.85)R			
0	-.6598+01				
1-5,C	.8520+01	.8602+02	-.4990+02	.8259+02	-.1203+03
1-5,S	.1290+02	.8231+01	.6422+02	±.1087+03	-.3882+02

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 8.
FIS CYCLIC PITCH TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(A) MP = 0.1
FK = 0.001 (FOR MU = 0.25,0.4,0.5)
FK = 0.000447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S	ADVANCE RATIO, MU = 0.25			
	(0.0)R			
0 -.5795+04				
1-S,C -.3971+05	-.6645+02	.3639+02	.7151+02	.7379+02
1-S,S .5517+04	.5295+03	.1286+03	.9763+02	.8629+02
	(0.14)R			
0 -.2569+05				
1-S,C -.1615+04	.1412+01	.1825+01	.1663+01	.1009+01
1-S,S .1943+05	.5135+02	.5774+01	.5527+01	.1819+01
	(0.325)R			
0 -.1263+02				
1-S,C -.7041+02	.4870+01	.1968+01	-.2682+01	-.4374+01
1-S,S -.1263+03	.1369+02	.2959+01	.1551+01	-.3384+01
	(0.55)R			
0 .2799+02				
1-S,C -.8369+02	-.1097+02	.3792+01	-.1283+01	-.1044+01
1-S,S -.1441+03	.2630+02	.1069+02	-.1448+01	-.4706-01
	(0.75)R			
0 .2139+03				
1-S,C .1699+02	-.2870+02	.4368-00	.2745-00	.5707+01
1-S,S -.1059+03	.5960+02	.1362+02	-.5203+01	.4393+01
	(0.85)R			
0 .2197+03				
1-S,C .4831+02	-.2460+02	-.1315+01	.4803-00	.6053+01
1-S,S -.6018+02	.5420+02	.9609+01	-.4618+01	.4211+01

N,C OR S	ADVANCE RATIO, MU = 0.7			
	(0.0)R			
0 -.1052+05				
1-S,C -.7500+05	-.3076+04	-.3171+04	-.4750+03	-.8440+03
1-S,S .1052+04	.1527+04	-.3821+04	-.6102+03	-.1710+04
	(0.14)R			
0 -.9150+05				
1-S,C -.5070+04	-.2442+03	-.2394+02	.7154+02	.1395+03
1-S,S -.2564+05	.5914+03	-.9267+02	.3654+02	.2191+03
	(0.325)R			
0 -.3264+05				
1-S,C -.1951+04	-.2113+03	.5098+03	.8719+02	.3222+03
1-S,S -.7366+05	.6311+03	.5203+03	.1492+03	.6239+03
	(0.55)R			
0 .4154+05				
1-S,C .1664+05	.2337+03	.7755+03	-.1728+02	-.9387+02
1-S,S -.1639+05	.5810+03	.1175+04	.8273+02	-.2873+02
	(0.75)R			
0 .4264+05				
1-S,C .2384+05	-.7146+03	.6582+03	.2235+03	-.6775+03
1-S,S -.1159+05	.7591+03	.1528+04	-.5139+02	-.1221+04
	(0.85)R			
0 .4350+05				
1-S,C .2628+05	-.7621+03	.3901+03	.2583+03	-.6025+03
1-S,S -.4453+05	.9059+03	.1099+04	-.6845+02	-.1149+04

N,C OR S	ADVANCE RATIO, MU = 0.4			
	(0.0)R			
0 -.9396+04				
1-S,C -.4958+05	-.9984+03	-.1531+03	.1134+03	.1120+03
1-S,S .4561+04	.7913+03	-.7793+02	.1014+03	.1356+03
	(0.14)R			
0 -.4031+03				
1-S,C -.2255+04	-.1970+02	.1008+01	-.8382+01	-.3591+01
1-S,S .7720+02	.5850+02	-.8575+01	.4010+01	-.3689+01
	(0.325)R			
0 .3319+01				
1-S,C -.4737+02	.4046+02	.2408+02	.2013+02	-.1630+02
1-S,S -.3132+03	.4320+02	.1818+02	.2424+01	-.1743+02
	(0.55)R			
0 .6235+02				
1-S,C -.3309+02	.3175+02	.3052+02	.9088+01	-.1630+01
1-S,S -.3880+03	.7445+02	.9266+02	.7241-00	-.7440-00
	(0.75)R			
0 .3551+03				
1-S,C .7697+02	-.1485+03	.4980+01	.4572+02	.2844+02
1-S,S -.2506+03	.1428+03	.1268+03	.8841+01	.2867+02
	(0.85)R			
0 .3608+03				
1-S,C .8939+02	-.1393+03	-.7178+01	.4141+02	.2924+02
1-S,S -.1201+03	.1257+03	.9431+02	.9813+01	.2873+02

N,C OR S	ADVANCE RATIO, MU = 1.0			
	(0.0)R			
0 -.2736+05				
1-S,C -.1107+06	-.1565+05	-.1393+05	.2625+04	-.1059+05
1-S,S -.1178+05	.2273+04	-.1797+05	.2972+04	-.7609+04
	(0.14)R			
0 -.2264+04				
1-S,C -.1104+05	-.1203+04	-.4403+03	.3560+03	.1448+04
1-S,S -.1806+04	.4159+03	-.6080+03	.7879+02	.9365+03
	(0.325)R			
0 .1107+04				
1-S,C -.4906+03	.1265+04	.2576+04	.9512+03	.4311+04
1-S,S -.1267+04	.5490+03	.3178+04	.7527+03	.2744+04
	(0.55)R			
0 .1374+04				
1-S,C .4906+03	.1379+04	.4284+04	-.2171+03	-.1034+04
1-S,S -.1267+04	.1514+04	.5286+04	.6024+03	-.2795+03
	(0.75)R			
0 .1268+04				
1-S,C .6002+03	-.6410+03	.4180+04	-.1391+04	-.8367+04
1-S,S -.8303+03	.1910+04	.5247+04	.1741+03	-.3673+04
	(0.85)R			
0 .7372+03				
1-S,C .4451+03	-.1013+04	.2618+04	-.1118+04	-.7044+04
1-S,S -.4716+03	.1373+04	.3317+04	.2400+02	-.3042+04

N,C OR S	ADVANCE RATIO, MU = 1.4			
	(0.0)R			
0 -.6077+05				
1-S,C -.2045+06	-.2580+05	-.5458+05	-.2331+04	-.8409+04
1-S,S -.3769+05	.2459+03	-.3066+05	.5947+04	.4150+04
	(0.14)R			
0 -.8526+04				
1-S,C -.3008+05	-.3496+04	-.3557+04	.9761+03	.1380+04
1-S,S -.7031+04	.6135+03	-.2829+04	.2990+03	-.6226+03
	(0.325)R			
0 .2602+04				
1-S,C -.1294+04	.1038+04	.1171+05	.1481+04	.4161+04
1-S,S -.2986+04	.2001+04	.5202+04	.1155+04	-.2817+04
	(0.55)R			
0 .4279+04				
1-S,C .1576+04	.1769+04	.2046+05	.8717+02	-.1423+04
1-S,S -.1845+04	.4402+04	.8263+04	.1454+04	.1545+04
	(0.75)R			
0 .3394+04				
1-S,C .1660+04	-.1227+04	.1987+05	.5455+03	-.7351+04
1-S,S -.8249+03	.4866+04	.4951+04	.9639+03	.9278+04
	(0.85)R			
0 .1909+04				
1-S,C .1010+04	-.1589+04	.1207+05	.6927+03	-.5640+04
1-S,S -.3949+03	.3058+04	.2167+04	.4922+03	.7489+04

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 8.

B1S CYCLIC PITCH TRANSFER COEFFICIENTS FOR R [illegible]

(B) MP = 0.1

FP = 0.0025 (FOR MU = 0.25,0.[illegible]

FP = 0.00112(1+MU**2 (FOR MU = 0.7,1.[illegible]

N,C OR S		ADVANCE RATIO, MU = 0.25			
		(0.0)R			
0	-.3992+04				
1-S,C	-.2701+05	.2307+02	-.4594+02	.3789+02	.3333+02
1-S,S	.5988+04	.5163+03	.7201+02	.5766+02	.4301+02
		(0.14)R			
0	-.5971+03				
1-S,C	-.3992+04	.8142+01	.1161+01	.6210+01	.6741+01
1-S,S	.8228+03	.7507+02	.1202+02	.8983+01	.6701+01
		(0.325)R			
0	-.5968+02				
1-S,C	-.4564+03	.8092+01	.2007+02	.2395+01	.3853+01
1-S,S	-.4422+02	.1353+02	.7062+01	.2386+01	.1741+01
		(0.55)R			
0	.6674+02				
1-S,C	-.1706+03	-.2276+01	.3165+02	.3408+01	.8583-00
1-S,S	-.1314+03	.3497+02	.1615+02	.3141+01	.2173+01
		(0.75)R			
0	.1371+03				
1-S,C	-.5024+02	-.1319+02	.2849+02	.3277+01	-.2842+01
1-S,S	-.9847+02	.4826+02	.1941+02	.3068+01	.2050+01
		(0.85)R			
0	.9709+02				
1-S,C	-.1215+02	-.1021+02	.1685+02	.1991+01	-.2452+01
1-S,S	-.5291+02	.3228+02	.1255+02	.1878+01	.1241+01

N,C OR S		ADVANCE RATIO, MU = 0.5			
		(0.0)R			
0	-.8513+04				
1-S,C	-.4073+05	-.1542+04	-.1065+04	-.5178+02	.4479+02
1-S,S	.5116+04	.1291+04	-.2953+03	-.6945+01	.1556+03
		(0.14)R			
0	-.1256+04				
1-S,C	-.5965+04	-.1576+03	-.5787+02	-.8154+01	.7890+01
1-S,S	.5469+03	.2020+03	-.3663+02	.1205+02	-.2141+01
		(0.325)R			
0	-.5096+02				
1-S,C	-.6026+03	.9271+02	.2332+03	.1697+02	.5037+01
1-S,S	-.4101+03	.7570+02	.5309+02	.2815+02	-.3657+02
		(0.55)R			
0	.2066+03				
1-S,C	-.1432+03	-.2552+02	.3465+03	.8495+02	.9716+01
1-S,S	-.5843+03	.1657+03	.2073+03	.2510+02	.2161+02
		(0.75)R			
0	.3121+03				
1-S,C	.1247+02	-.1708+03	.2926+03	.1213+03	.1076+02
1-S,S	-.4299+03	.2016+03	.2799+03	.8337+01	.8158+02
		(0.85)R			
0	.2101+03				
1-S,C	.3076+02	-.1334+03	.1683+03	.8145+02	.6808+01
1-S,S	-.2326+03	.1309+03	.1858+03	.1841+01	.6171+02

N,C OR S		ADVANCE RATIO, MU = 0.7			
		(0.0)R			
0	-.1158+05				
1-S,C	-.5405+05	+.4611+04	-.5778+04	+.7078+03	-.[illegible]
1-S,S	.4796+04	.1972+04	-.2038+04	+.2683+03	.[illegible]
		(0.14)R			
0	-.1995+04				
1-S,C	-.9989+04	+.5957+03	-.5007+03	+.5759+02	.[illegible]
1-S,S	.9782+03	.4288+03	-.2618+03	-.1314+02	+.[illegible]
		(0.325)R			
0	.1845+03				
1-S,C	-.1228+04	.3648+03	.1368+04	.1992+03	.2817+03
1-S,S	+.6905+03	.2775+03	.3608+03	.7914+02	+.[illegible]
		(0.55)R			
0	.4804+03				
1-S,C	-.2044+03	.1126+03	.2249+04	.3986+03	+.[illegible]
1-S,S	+.5906+03	.5434+03	.9071+03	.9859+02	.1796+03
		(0.75)R			
0	.4348+03				
1-S,C	.3722+02	+.2968+03	.1945+04	.3826+03	-.2805+03
1-S,S	-.7622+03	.5836+03	.9914+03	.6483+02	.7246+03
		(0.85)R			
0	.2495+03				
1-S,C	.6543+02	-.2507+03	.1111+04	.2278+03	+.1504+03
1-S,S	-.4156+03	.3574+03	.6084+03	.3226+02	.8298+03

N,C OR S		ADVANCE RATIO, MU = 1.0			
		(0.0)R			
0	-.2053+05				
1-S,C	-.9447+05	+.1245+05	-.2656+05	+.2445+04	.3197+03
1-S,S	.4130+04	.3829+04	-.9915+03	-.8948+03	.1435+04
		(0.14)R			
0	-.4314+04				
1-S,C	-.2236+05	+.2267+04	-.3302+04	-.1638+03	-.1567+01
1-S,S	.4772+03	.1184+04	-.3675+03	-.3705+02	-.3627+03
		(0.325)R			
0	.5383+03				
1-S,C	-.3493+04	.9963+03	.6896+04	.8928+03	-.8886+02
1-S,S	-.1015+04	.9786+03	-.4576+03	.6058+02	-.9884+03
		(0.55)R			
0	.1492+04				
1-S,C	-.4607+03	.1259+04	.1184+05	.1184+04	.1544+03
1-S,S	-.1349+04	.1565+04	-.8311+03	-.2329+03	.9364+03
		(0.75)R			
0	.1089+04				
1-S,C	.1444+03	.5338+03	.9768+04	.7903+03	.3873+03
1-S,S	-.8662+03	.1423+04	-.7870+03	+.4055+03	.2239+04
		(0.85)R			
0	.5648+03				
1-S,C	.1368+03	.1941+03	.5377+04	.3998+03	.2035+03
1-S,S	-.4296+03	.8113+03	-.4936+03	-.2640+03	.1512+04

N,C OR S		ADVANCE RATIO, MU = 1.4			
		(0.0)R			
0	-.3890+05				
1-S,C	-.1060+06	-.1584+05	-.2445+05	.7285+03	.1674+04
1-S,S	.7037+04	.3452+04	-.2724+05	.1334+04	-.4230+03
		(0.14)R			
0	-.1053+05				
1-S,C	-.3179+05	-.3774+04	-.4827+04	.4379+03	+.3992+03
1-S,S	.1260+04	.2222+04	-.3846+04	.3150+03	-.4987+03
		(0.325)R			
0	.3391+03				
1-S,C	-.5462+04	.1158+04	.5741+04	.1115+03	-.9012+03
1-S,S	-.1345+04	.2926+04	-.9919+04	+.8709+03	-.3848+03
		(0.55)R			
0	.3063+04				
1-S,C	-.5433+02	.1972+04	.1031+05	-.1146+04	.1573+04
1-S,S	-.1614+04	.3125+04	-.1768+05	+.3192+04	.9614+03
		(0.75)R			
0	.2293+04				
1-S,C	.3201+03	.1041+04	.7941+04	-.1587+04	.2907+04
1-S,S	-.7466+03	.1830+04	-.1412+05	+.3456+04	.1582+04
		(0.85)R			
0	.1175+04				
1-S,C	.1566+03	.4541+03	.4188+04	-.9665+03	.1845+04
1-S,S	-.3012+03	.8678+03	-.7549+04	-.2008+04	.9887+03

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 8.
BIS CYCLIC PITCH TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(C) MP = 0.1
FP = 0.01 (FOR MU = 0.25,0.4,0.5)
FP = 0.00447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S — ADVANCE RATIO, MU = 0.25

(0.0)R

0	-.2100+04			
1-S,C	-.1367+05	.1780+03	.3613+02	.1513+02	.1075+02
1-S,S	.8272+04	.4031+03	.5709+02	.6638+01	.4311+01

(0.14)R

0	-.8342+03			
1-S,C	-.5103+04	.7445+02	.8777+01	.5827+01	.4579+01
1-S,S	.2373+04	.4559+03	.1664+02	.3330+01	.2099+01

(0.325)R

0	-.2230+03			
1-S,C	-.1644+04	.3390+02	-.8011+01	.1611+01	.2193+01
1-S,S	.8328+03	.5778+02	-.6052+01	.8950-00	.1513+01

(0.55)R

0	.3122+01			
1-S,C	-.5649+03	.2105+02	-.1419+02	-.1498-01	.1335+01
1-S,S	.1072+03	.3105+02	-.1404+02	-.1199+00	.1359+01

(0.75)R

0	.5374+02			
1-S,C	-.1819+03	.1023+02	-.9604+01	-.4079-00	.9893-00
1-S,S	-.4030+01	.1121+02	-.9754+01	-.3814-00	.7791-00

(0.85)R

0	.3300+02			
1-S,C	-.6802+02	.4560+01	-.4749+01	-.2597-00	.2480-00
1-S,S	-.9110+01	.4229+02	-.4847+01	-.2153-00	.3674-00

N,C OR S — ADVANCE RATIO, MU = 0.4

(0.0)R

0	-.3665+04			
1-S,C	-.1743+05	-.3977+02	-.5022+02	.3505+01	.1416+02
1-S,S	.6632+04	.8869+03	.2159+03	.4888+02	.7858+01

(0.14)R

0	-.1397+04			
1-S,C	-.6755+04	.1305-00	-.1837+02	.1655+01	.6209+01
1-S,S	.2441+04	.3424+03	.4944+02	.1207+02	.9581+01

(0.325)R

0	-.3636+03			
1-S,C	-.2114+04	.1918+02	-.2946+01	.3610+01	.3715+01
1-S,S	.5188+03	.1223+03	-.5107+02	-.1153+02	.4290+01

(0.55)R

0	.1534+02			
1-S,C	-.6915+03	-.2833+01	.3307+01	.9077+01	.3808+01
1-S,S	-.4727+02	.9759+02	-.7914+02	-.2292+02	-.2049+01

(0.75)R

0	.9358+02			
1-S,C	-.2097+03	-.1971+02	.3582+01	.8662+01	.2681+01
1-S,S	-.9072+02	.7639+02	-.4808+02	-.1705+02	-.5262+01

(0.85)R

0	.5788+02			
1-S,C	-.7647+02	-.1315+02	.1977+01	.4787+01	.1372+01
1-S,S	-.4865+02	.4098+02	-.2273+02	-.8730+01	-.3327+01

N,C OR S — ADVANCE RATIO, MU = 0.5

(0.0)R

0	-.4777+04			
1-S,C	-.2127+05	-.5430+03	-.7461+02	-.1038+03	.4384+02
1-S,S	.6788+04	.1364+04	.4437+03	.3146+02	.1805+01

(0.14)R

0	-.1803+04			
1-S,C	-.8227+04	-.1640+03	-.3173+02	-.1790+02	.8129+01
1-S,S	.2442+04	.5275+03	.8583+02	.1426+02	.6001+01

(0.325)R

0	-.4372+03			
1-S,C	-.2543+04	.1318+02	-.2303+02	.4277+02	-.7146+01
1-S,S	.3911+03	.1920+03	-.1358+03	.3047-00	.1094+02

(0.55)R

0	.5934+02			
1-S,C	-.7997+03	.2049+01	-.3851+02	.7156+02	.7015+01
1-S,S	-.2366+03	.1592+03	-.1856+03	-.2381+02	.9054+01

(0.75)R

0	.1432+03			
1-S,C	-.2286+03	-.3583+02	-.3421+02	.5081+02	.1619+02
1-S,S	-.2207+03	.1257+03	-.1042+03	-.2778+02	.3140+01

(0.85)R

0	.8502+02			
1-S,C	-.8015+02	-.2532+02	-.1864+02	.2566+02	.1022+02
1-S,S	-.1136+03	.6751+02	-.4755+02	-.1596+02	.1018+01

N,C OR S — ADVANCE RATIO, MU = 0.7

(0.0)R

0	-.6465+04			
1-S,C	-.2740+05	-.1978+04	-.4217+03	-.3597+03	.4645+02
1-S,S	.8153+04	.2553+04	.1262+04	.2657+03	.4605+02

(0.14)R

0	-.2659+04			
1-S,C	-.1190+05	-.7019+03	-.1759+03	-.8271+02	.1687+00
1-S,S	.3264+04	.1134+04	.2513+03	.5816+02	-.9607+01

(0.325)R

0	-.6199+03			
1-S,C	-.4131+04	-.3554+02	-.6297+02	.1044+03	-.1854+02
1-S,S	.6188+03	.5010+03	-.4800+03	-.1167+03	-.3152+02

(0.55)R

0	.1414+03			
1-S,C	-.1313+04	-.7713+01	-.5642+02	.1498+03	.2071+02
1-S,S	-.3504+03	.3887+03	-.7199+03	-.2373+03	.5125+01

(0.75)R

0	.2039+03			
1-S,C	-.3551+03	-.1044+03	-.4866+02	.8297+02	.4017+02
1-S,S	-.3503+03	.2674+03	-.4425+03	-.1837+03	.3070+02

(0.85)R

0	.1112+03			
1-S,C	-.1202+03	-.7180+02	-.2654+02	.3744+02	.2456+02
1-S,S	-.1824+03	.1369+03	-.2099+03	-.9480+02	.2005+02

N,C OR S — ADVANCE RATIO, MU = 1.0

(0.0)R

0	-.1052+05			
1-S,C	-.3967+05	-.4457+04	-.5608+03	.5953+03	.8332+02
1-S,S	.9553+04	.5480+04	.2487+04	-.8998+03	-.6776+03

(0.14)R

0	-.4012+04			
1-S,C	-.1941+05	-.1829+04	-.3942+03	.1643+03	.2521+01
1-S,S	.4247+04	.2837+04	.5351+03	-.2380+03	-.2105+03

(0.325)R

0	-.1013+04			
1-S,C	-.7654+04	-.2063+03	-.4407+03	.3264+03	-.2773+02
1-S,S	.1094+04	.1507+04	-.1114+04	.2606+03	.2090+03

(0.55)R

0	.4554+03			
1-S,C	-.2536+04	.1520+03	-.5714+03	-.8411+03	.5550+02
1-S,S	-.2022+03	.1108+04	-.1841+04	.3999+03	.3112+03

(0.75)R

0	.4009+03			
1-S,C	-.6771+03	-.2597+01	-.4037+03	.7050+03	.8705+02
1-S,S	-.2923+03	.6044+03	-.1201+04	.2238+03	.3996+03

(0.85)R

0	.2352+03			
1-S,C	-.2276+03	-.2637+02	-.2028+03	-.3691+03	.8130+02
1-S,S	-.1543+03	.3225+03	-.5803+03	.1010+03	.2048+03

N,C OR S — ADVANCE RATIO, MU = 1.4

(0.0)R

0	-.1813+05				
1-S,C	-.5163+05	-.5280+04	-.4664+03	.4946+04	-.2411+04
1-S,S	.7248+04	.6711+04	.1684+04	.4096+04	-.2865+04

(0.14)R

0	-.9021+04				
1-S,C	-.2824+05	-.2373+04	-.7459+03	-.1336+04	-.6710+03
1-S,S	.3604+04	.5280+04	.7811+02	.1181+04	-.8728+03

(0.325)R

0	-.2434+04				
1-S,C	-.1250+05	-.2390+03	-.1210+04	.1695+04	.9708+03
1-S,S	.1014+04	.3360+04	-.1577+04	.1373+04	.9832+03

(0.55)R

0	.6253+03				
1-S,C	-.4161+04	.5119+03	-.1320+04	.2576+04	.1849+04
1-S,S	-.9737+02	.2428+04	-.2401+04	.2401+04	.1721+04

(0.75)R

0	.7667+03				
1-S,C	-.1084+04	.2995+03	-.7506+03	.1416+04	.1256+04
1-S,S	-.1644+03	.1296+04	-.1549+04	.1487+04	.1121+04

(0.85)R

0	.3955+03				
1-S,C	-.3598+03	.1287+03	-.3403+03	.6324+03	.6121+03
1-S,S	-.8174+02	.5980+03	-.7445+03	.6990+03	.9372+03

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 8.

[illegible] CYCLIC PITCH TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(D) MP = 0.3

FF = 0.001 (FOR MU = 0.25,0.4,0.5)

FF = 0.000447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S	ADVANCE RATIO, MU = 0.25				
	(0.0)R				
0	[illegible]				
1-5,C	[illegible]	-.1599+03	-.2348+03	-.3598+02	-.2439+02
1-5,S	[illegible]	[illegible]	-.1805+03	-.6508+02	-.5007+02
	(0.14)R				
0	[illegible]				
1-5,C	[illegible]	-.1715+02	.5329+01	-.1384+01	.6989-00
1-5,S	[illegible]	.1593+02	-.8407+01	.4405-00	.1208+01
	(0.325)R				
0	[illegible]				
1-5,C	[illegible]	[illegible]	.3657+02	.2284+01	.1997+01
1-5,S	[illegible]	.7058+02	.1722+02	.4666+01	.6648+01
	(0.55)R				
0	[illegible]				
1-5,C	[illegible]	-.1521+03	.3310+02	.6204+01	-.1374+01
1-5,S	[illegible]	[illegible]	.7211+02	.6745+01	.2867+01
	(0.75)R				
0	[illegible]				
1-5,C	.3172+03	[illegible]	-.1299+01	.6416+01	-.2071+01
1-5,S	[illegible]	.1110+02	.1099+03	.1925+02	-.5196+01
	(0.85)R				
0	[illegible]				
1-5,C	[illegible]	-.1523+03	[illegible]	.4021+01	-.1067+01
1-5,S	[illegible]	[illegible]	[illegible]	.1861+02	-.6052+01

N,C OR S	ADVANCE RATIO, MU = 0.4				
	(0.0)R				
0	[illegible]				
1-5,C	[illegible]	[illegible]	-.1242+04	-.1036+03	.7474+02
1-5,S	[illegible]	[illegible]	-.8260+03	-.2628+03	-.1798+03
	(0.14)R				
0	[illegible]				
1-5,C	[illegible]	[illegible]	.3165+02	-.2467+02	-.1582+02
1-5,S	[illegible]	.1520+03	-.6234+02	.1041+02	.1364+02
	(0.325)R				
0	[illegible]				
1-5,C	[illegible]	-.1615+03	.2039+03	-.2326+02	-.4217+02
1-5,S	[illegible]	[illegible]	.5840+02	.1775+02	.2955+02
	(0.55)R				
0	[illegible]				
1-5,C	[illegible]	[illegible]	.1067+03	.6477+02	-.5723+01
1-5,S	[illegible]	[illegible]	.4122+03	.2403+02	-.2848+01
	(0.75)R				
0	[illegible]				
1-5,C	[illegible]	[illegible]	-.9929+01	.1851+03	.9602+02
1-5,S	[illegible]	.2411+03	.6906+03	.1488+03	-.1765+02
	(0.85)R				
0	[illegible]				
1-5,C	[illegible]	[illegible]	-.7657+02	.1639+03	.1017+03
1-5,S	[illegible]	[illegible]	.5429+03	.1564+03	-.1155+02

N,C OR S	ADVANCE RATIO, MU = 0.5				
	(0.0)R				
0	[illegible]				
1-5,C	[illegible]	[illegible]	-.2993+04	-.3480+03	-.1630+03
1-5,S	[illegible]	[illegible]	-.1286+04	-.8555+03	-.7361+03
	(0.14)R				
0	-.1272+04				
1-5,C	[illegible]	[illegible]	.5136+02	-.3825+02	.2803+02
1-5,S	[illegible]	.2569+03	-.1701+03	.8276+02	.6864+02
	(0.325)R				
0	[illegible]				
1-5,C	[illegible]	-.1953+03	.4867+03	-.4129+02	.1633+02
1-5,S	[illegible]	.6154+03	.1048+02	.1474+03	.1927+03
	(0.55)R				
0	[illegible]				
1-5,C	.1310+04	-.9952+03	.5874+03	.1663+03	-.4444+02
1-5,S	-.1564+04	.6743+03	.8624+03	.2095+02	.2925+02
	(0.75)R				
0	.1205+04				
1-5,C	.1132+04	-.1401+04	.2245+03	.5999+03	.5599+02
1-5,S	-.1013+04	.6497+03	.1621+04	.1321+03	-.3079+03
	(0.85)R				
0	.1207+04				
1-5,C	[illegible]	-.1025+04	.1155+02	.5648+03	.9269+02
1-5,S	-.3867+03	.4655+03	.1308+04	.1683+03	-.3197+03

N,C OR S	ADVANCE RATIO, MU = 0.7				
	(0.0)R				
0	-.4115+05				
1-5,C	-.8266+05	-.5372+04	-.1077+05	-.3836+04	-.4392+04
1-5,S	-.7382+04	-.2676+04	-.3889+04	-.3173+04	-.3065+04
	(0.14)R				
0	-.2116+04				
1-5,C	-.5047+04	-.2065+03	-.7217+02	.3317+03	.6281+03
1-5,S	-.1383+04	.5278+03	-.3729+03	.4080+03	.2744+03
	(0.325)R				
0	.1216+04				
1-5,C	.1273+04	.3273+02	.1854+04	.7106+03	.1587+04
1-5,S	-.2163+04	.1615+04	.2131+03	.9966+03	.1101+04
	(0.55)R				
0	.1364+04				
1-5,C	.2060+04	-.1287+04	.3112+04	.3998+03	-.2610+03
1-5,S	-.2771+04	.2245+04	.2359+04	.8803+01	.2747+03
	(0.75)R				
0	.1462+04				
1-5,C	.1508+04	-.2771+04	.2990+04	.1448+04	-.3087+04
1-5,S	-.1975+04	.2361+04	.4696+04	-.1124+04	-.2043+04
	(0.85)R				
0	.1066+04				
1-5,C	.7757+03	-.2240+04	.1891+04	.1441+04	-.2808+04
1-5,S	-.1059+04	.1627+04	.3757+04	-.9990+03	-.2076+04

N,C OR S	ADVANCE RATIO, MU = 1.0				
	(0.0)R				
0	-.6069+05				
1-5,C	-.1279+06	-.1384+05	-.3845+05	-.1612+05	-.1988+05
1-5,S	-.1638+05	-.1006+05	-.1090+05	-.8102+04	-.4708+04
	(0.14)R				
0	-.4428+04				
1-5,C	-.1153+05	-.1475+04	-.1419+04	.1425+04	.2924+04
1-5,S	-.3547+04	.7247+03	-.1303+04	.8247+03	.3093+03
	(0.325)R				
0	.3791+04				
1-5,C	.2828+04	.3540+03	.7133+04	.4819+04	.8124+04
1-5,S	-.3697+04	.3827+04	.7899+03	.2770+04	.8297+03
	(0.55)R				
0	.4511+04				
1-5,C	.3853+04	.5463+03	.1318+05	.1378+04	-.1036+04
1-5,S	-.2933+04	.5236+04	.4833+04	.4233+02	.1143+04
	(0.75)R				
0	.2690+04				
1-5,C	.2443+04	-.1130+04	.1366+05	-.1229+04	-.1477+05
1-5,S	-.1556+04	.5458+04	.7119+04	-.3379+04	.3838+04
	(0.85)R				
0	.1276+04				
1-5,C	.1207+04	-.1268+04	.8712+04	-.1069+04	-.1269+05
1-5,S	-.7928+03	.3631+04	.4975+04	-.2889+04	.3356+04

N,C OR S	ADVANCE RATIO, MU = 1.4				
	(0.0)R				
0	-.9767+05				
1-5,C	-.1365+06	.4806+04	-.4466+05	-.1354+05	-.1073+04
1-5,S	-.5976+04	-.3653+05	.2278+05	-.1315+04	.1531+05
	(0.14)R				
0	-.1060+05				
1-5,C	-.1551+05	-.8903+03	-.4928+04	.2152+04	-.7077+01
1-5,S	-.5260+04	-.4520+03	-.1972+04	.6166+03	-.2408+04
	(0.325)R				
0	.6865+04				
1-5,C	.9014+04	-.3218+04	.7348+04	.5146+04	.9520+03
1-5,S	-.6960+04	.9584+04	-.8376+04	.1354+04	-.8738+04
	(0.55)R				
0	.7468+04				
1-5,C	.8648+04	-.1631+04	.1944+05	-.1229+04	.1902+04
1-5,S	-.2560+04	.9372+04	-.5564+04	-.4721+04	.2292+04
	(0.75)R				
0	.4853+04				
1-5,C	.2758+04	.1536+04	.2125+05	-.2923+04	.2875+04
1-5,S	-.2197+03	.6165+04	-.5134+04	-.1263+05	.1833+05
	(0.85)R				
0	.2613+04				
1-5,C	.5928+03	.1588+04	.1317+05	-.1602+04	.1983+04
1-5,S	-.7494+02	.3373+04	-.3637+04	-.9557+04	.1470+05

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 8.
B1S CYCLIC PITCH TRANSFER COEFFICIENTS FOR K HINGELESS BLADE

(E) MP ± 0.3
FP ± 0.0025 (FOR MU = 0.25,0.4,0.5)
FP ± 0.00112(1+MU**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S — ADVANCE RATIO, MU ± 0.25

(0.0)R

0	-.1196E+05				
1-S,C	-.2979E+05	-.1791E+03	-.2333E+03	-.3990E+02	.2804E+02
1-S,S	.9557E+03	.1437E+03	-.7246E+02	-.3051E+02	-.2579E+02

(0.14)R

0	-.1777E+04				
1-S,C	-.4321E+04	-.3472E+02	-.1355E+02	-.4268E+01	.1508E+01
1-S,S	-.6745E+02	.5473E+02	-.1186E+02	-.3742E+01	.2851E+01

(0.325)R

0	-.1521E+03				
1-S,C	-.2921E+03	-.4311E+02	.4678E+02	.5176E+01	.2778E+01
1-S,S	-.4599E+03	.8336E+02	.7552E+01	.1913E+01	.3201E+01

(0.55)R

0	.2275E+03				
1-S,C	.1243E+03	-.1183E+03	.6369E+02	.1347E+02	.2497E+01
1-S,S	-.5088E+03	.1043E+03	.4869E+02	.4779E+01	.2965E+01

(0.75)R

0	.4249E+03				
1-S,C	.2153E+03	-.1486E+03	.4809E+02	.1590E+02	.2449E-00
1-S,S	-.2917E+03	.7662E+02	.7168E+02	.5364E+01	-.2048E+01

(0.85)R

0	.2970E+03				
1-S,C	.1445E+03	-.9705E+02	.2644E+02	.1022E+02	.3048E+01
1-S,S	-.1364E+03	.4163E+02	.4838E+02	.3399E+01	-.4588E+00

N,C OR S — ADVANCE RATIO, MU ± 0.4

(0.0)R

0	-.1884E+05				
1-S,C	-.3821E+05	-.9118E+03	-.1222E+04	-.2167E+03	-.9418E+02
1-S,S	-.1737E+04	.7364E+02	-.5136E+03	-.1333E+03	-.1639E+05

(0.14)R

0	-.2757E+04				
1-S,C	-.5429E+04	-.1608E+03	-.6244E+02	-.3123E+02	.6007E+01
1-S,S	-.7192E+03	.1375E+03	-.8392E+02	-.1587E+02	.3972E+01

(0.325)R

0	-.1503E+03				
1-S,C	-.9296E+02	-.1558E+03	.2878E+03	.2264E+02	.2569E+01
1-S,S	-.1083E+04	.2983E+03	.5392E+02	.1180E+02	.9464E+02

(0.55)R

0	.4322E+03				
1-S,C	.5465E+03	-.4437E+03	.3232E+03	.1122E+03	.8876E+02
1-S,S	-.1146E+04	.3508E+03	.3456E+03	.3276E+02	.8050E+00

(0.75)R

0	.6664E+03				
1-S,C	.5877E+03	-.5672E+03	.2895E+03	.1582E+03	.1443E+02
1-S,S	-.8450E+03	.2307E+03	.5078E+03	.3919E+02	-.5612E+02

(0.85)R

0	.9673E+03				
1-S,C	.3617E+03	-.3721E+03	.1442E+03	.1060E+03	.9557E+01
1-S,S	-.2982E+03	.1182E+03	.3438E+03	.2527E+02	-.4856E+02

N,C OR S — ADVANCE RATIO, MU ± 0.5

(0.0)R

0	-.2352E+05				
1-S,C	-.4579E+05	-.2856E+04	-.2916E+04	-.6508E+03	-.4803E+03
1-S,S	-.3545E+04	.3859E+03	-.8068E+03	-.3758E+03	-.2803E+03

(0.14)R

0	-.3356E+04				
1-S,C	-.6419E+04	-.2978E+03	-.4563E+03	-.6030E+02	.3648E+02
1-S,S	-.1181E+04	.2093E+03	-.1877E+03	-.9132E+01	.8326E+00

(0.325)R

0	-.7990E+01				
1-S,C	.9642E+02	-.1792E+03	.6594E+03	.1068E+03	.1693E+03
1-S,S	-.1586E+04	.6079E+03	.2209E+02	.6487E+02	.9452E+02

(0.55)R

0	.6804E+03				
1-S,C	.9191E+03	-.7193E+03	.8803E+03	.3509E+03	-.1353E+02
1-S,S	-.1765E+04	.7939E+03	.7017E+03	.4824E+02	.2678E+02

(0.75)R

0	.8784E+03				
1-S,C	.8983E+03	-.1013E+04	.6803E+03	.3876E+03	-.2296E+03
1-S,S	-.1101E+04	.5862E+03	.1538E+03	.2944E+02	-.6725E+02

(0.85)R

0	.5732E+03				
1-S,C	.5368E+03	-.6798E+03	.3895E+03	.2526E+03	-.1831E+03
1-S,S	-.5468E+03	.3866E+03	.7629E+03	.1379E+02	-.9388E+02

N,C OR S — ADVANCE RATIO, MU ± 0.7

(0.0)R

0	-.2970E+05				
1-S,C	-.6064E+05	-.6825E+04	-.1421E+05	-.3877E+04	-.2664E+04
1-S,S	-.5794E+04	-.9915E+03	-.3021E+03	.2299E+03	.2201E+04

(0.14)R

0	-.4936E+04				
1-S,C	-.1862E+05	-.9698E+03	-.1046E+04	-.2452E+03	.2864E+03
1-S,S	-.2044E+04	.4484E+03	-.4295E+03	.6445E+02	-.3356E+03

(0.325)R

0	.6393E+03				
1-S,C	.9972E+02	.1879E+03	.2548E+04	.1081E+04	.1204E+04
1-S,S	-.2454E+04	.1565E+04	-.3729E+03	-.3898E+02	-.1401E+04

(0.55)R

0	.1480E+04				
1-S,C	.1567E+04	-.7203E+03	.4476E+04	.1564E+04	-.2284E+02
1-S,S	-.2890E+04	.2206E+04	-.1205E+04	-.3578E+03	.8433E+03

(0.75)R

0	.1103E+04				
1-S,C	.1274E+04	-.1444E+04	.4047E+04	.1121E+04	-.1375E+04
1-S,S	-.1972E+04	.1741E+04	-.2274E+04	-.6521E+03	.2068E+04

(0.85)R

0	.5870E+03				
1-S,C	.6962E+03	-.9939E+03	.2347E+04	.6629E+03	-.1061E+04
1-S,S	-.1023E+04	.9622E+03	-.1956E+04	-.3338E+03	.1507E+00

N,C OR S — ADVANCE RATIO, MU ± 1.0

(0.0)R

0	-.4553E+05				
1-S,C	-.9575E+05	-.1721E+05	-.3292E+05	-.8879E+04	-.1456E+04
1-S,S	-.1059E+05	.4603E+04	.4899E+04	.2708E+04	.9219E+04

(0.14)R

0	-.8993E+04				
1-S,C	-.2103E+05	-.3455E+04	-.4668E+04	-.4978E+03	-.9588E+02
1-S,S	-.4106E+04	.7344E+03	-.1811E+03	.4897E+03	-.1870E+04

(0.325)R

0	.2382E+04				
1-S,C	.6678E+02	.7507E+03	.7613E+04	.2998E+04	.4592E+03
1-S,S	-.3933E+04	.4112E+04	-.2703E+04	-.9112E+03	-.2783E+03

(0.55)R

0	.4256E+04				
1-S,C	.3122E+04	.1368E+03	.1474E+05	.2615E+04	.5010E+04
1-S,S	-.3644E+04	.5079E+04	-.2638E+04	-.3152E+04	.2063E+04

(0.75)R

0	.2648E+04				
1-S,C	.1882E+04	.7977E+03	.1309E+05	.6777E+03	.9478E+03
1-S,S	-.1786E+04	.3277E+04	-.1083E+04	-.3396E+04	.5719E+04

(0.85)R

0	.1279E+04				
1-S,C	.8658E+03	.3702E+03	.7378E+04	.9186E+02	.9438E+03
1-S,S	-.7606E+03	.1634E+04	-.3924E+03	-.2169E+04	.3912E+04

N,C OR S — ADVANCE RATIO, MU ± 1.4

(0.0)R

0	-.7387E+05				
1-S,C	-.1022E+06	-.9924E+04	-.3281E+05	.2104E+03	.3809E+04
1-S,S	-.1476E+05	-.1606E+05	.2879E+05	.7482E+04	-.1451E+04

(0.14)R

0	-.1892E+05				
1-S,C	-.2559E+05	-.3188E+04	-.7233E+04	.1083E+04	-.9356E+03
1-S,S	-.7481E+04	-.4108E+03	.3856E+04	.1884E+04	-.1418E+04

(0.325)R

0	.2693E+04				
1-S,C	.4220E+04	.6939E+03	.6209E+04	.4868E+03	-.8309E+04
1-S,S	-.6956E+04	.8012E+04	-.5079E+05	.2595E+04	.9458E+03

(0.55)R

0	.6981E+04				
1-S,C	.7815E+04	.8658E+03	.1536E+05	.4686E+04	.2043E+04
1-S,S	-.4468E+04	.7074E+04	-.1665E+05	.9481E+03	.9044E+03

(0.75)R

0	.4154E+04				
1-S,C	.2927E+04	.1349E+04	.1393E+05	.6580E+04	.6798E+04
1-S,S	-.6613E+03	.2066E+04	-.1597E+05	.1016E+05	.8043E+04

(0.85)R

0	.2958E+04				
1-S,C	.2226E+03	.6303E+03	.7736E+04	.4022E+04	.3619E+04
1-S,S	.1387E+03	.4758E+03	-.6562E+04	.3889E+04	.1311E+04

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 8.
HELICOPTER PITCH TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(1) MF = 0.3
CP = 0.00 (FOR MU = 0.25,0.4,0.5)
CP = 0.00447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S

ADVANCE RATIO, MU = 0.25

(0.0)R

0	-.8765+04			
1-5,C	-.1674+05	-.1359+03	-.6070+02	-.4668+01	-.2998+01
1-5,S	.1828+04	.3573+03	.1093+03	.1507+02	-.2275+01

(0.14)R

0	-.2578+04			
1-5,C	-.6435+04	-.4312+02	-.1706+02	-.2782+01	-.1184+01
1-5,S	.4905+03	.1664+03	.2358+02	.2228+01	-.1160+01

(0.325)R

0	-.6699+03			
1-5,C	-.1899+04	-.1011+02	.1031+02	-.2344+01	-.5501-00
1-5,S	-.2613+03	.1144+03	-.2773+02	-.7036+01	-.1014+01

(0.55)R

0	.3710+02			
1-5,C	-.4818+03	-.3739+02	.2559+02	-.1131+01	-.6850-00
1-5,S	-.4527+03	.1155+03	-.3861+02	-.1132+02	-.1211+01

(0.75)R

0	.1826+03			
1-5,C	-.7396+02	-.4454+02	.2060+02	.9453-01	-.5931-00
1-5,S	.2664+03	.7617+02	-.2118+02	-.7905+01	-.8592-00

(0.85)R

0	.1125+03			
1-5,C	-.9144+01	-.2659+02	-.1061+02	.2000-00	-.3229-00
1-5,S	-.1235+03	.3802+02	-.9528+01	-.3970+01	-.4382-00

N,C OR S

ADVANCE RATIO, MU = 0.4

(0.0)R

0	-.1095+05			
1-5,C	-.2202+05	-.9226+03	-.6322+03	.1099+03	-.2716+02
1-5,S	-.4958+02	.8128+03	.4650+03	.1648+03	-.2809-00

(0.14)R

0	-.4143+04			
1-5,C	-.8366+04	-.3431+03	-.1550+03	.3830+02	-.7480+01
1-5,S	-.4745+03	.3999+03	.7792+02	.2672+02	-.2739-00

(0.325)R

0	-.1020+04			
1-5,C	-.2265+04	-.1360+03	.1434+03	.9362+01	.3430+01
1-5,S	-.1008+04	.2958+03	-.1516+03	.7256+02	-.7418+01

(0.55)R

0	.1198+03			
1-5,C	-.3500+03	-.2106+03	.2686+03	.5492+02	.6177+01
1-5,S	-.1076+04	.2708+03	-.1591+03	.1212+03	-.2648+02

(0.75)R

0	.3218+03			
1-5,C	.7895+02	-.2068+03	.1905+03	.5870+02	.3620+01
1-5,S	-.5798+03	.1571+03	-.5894+02	.8651+02	.2704+02

(0.85)R

0	.1925+03			
1-5,C	.7294+02	-.1159+03	.9592+02	.3038+02	.1671+01
1-5,S	-.2619+03	.7440+02	-.1991+02	.4378+02	.1516+02

N,C OR S

ADVANCE RATIO, MU = 0.5

(0.0)R

0	-.1396+05			
1-5,C	-.2705+05	-.2195+04	-.1558+04	.3411+03	.2669+02
1-5,S	-.1558+04	.1284+04	.1189+04	.4391+03	.3944+02

(0.14)R

0	-.5220+04			
1-5,C	-.1020+05	-.7795+03	-.3793+03	.1040+03	.1273+02
1-5,S	-.1257+04	.6538+03	.1875+03	.8709+02	-.4301+01

(0.325)R

0	-.1174+04			
1-5,C	-.2605+04	-.2193+03	.3583+03	.5248+02	.4351+01
1-5,S	-.1656+04	.5169+03	-.4140+03	.1754+03	-.3648+02

(0.55)R

0	.2603+03			
1-5,C	-.2222+03	-.3268+03	.6656+03	.1709+03	.8685+01
1-5,S	-.1707+04	.4840+03	-.4358+03	.3481+03	-.4489+02

(0.75)R

0	.4485+03			
1-5,C	.2212+03	-.3550+03	.4705+03	.1530+03	.1246+02
1-5,S	-.9563+03	.2806+03	-.1669+03	.2748+03	.2637+02

(0.85)R

0	.2582+03			
1-5,C	.1485+03	-.2041+03	.2366+03	.8278+02	.7391+01
1-5,S	-.4420+03	.1327+03	-.5833+02	.1437+03	.1237+02

N,C OR S

ADVANCE RATIO, MU = 0.7

(0.0)R

0	-.1011+05			
1-5,C	-.3300+05	-.3019+04	-.4361+04	.3600+03	.2084+03
1-5,S	-.4452+04	.4160+04	.5771+04	.2947+04	.7230+03

(0.14)R

0	-.7204+04			
1-5,C	-.1063+05	-.2559+04	-.1286+04	.1492+03	-.4679-00
1-5,S	-.2902+04	.2084+04	.1257+04	.6852+03	.3429+02

(0.325)R

0	-.1403+04			
1-5,C	-.4603+04	-.4409+03	.8482+03	.1113+03	-.1403+03
1-5,S	-.2724+04	.1256+04	-.1890+04	.1092+04	-.4140+03

(0.55)R

0	.8424+03			
1-5,C	-.6406+03	-.4038+03	.1808+04	.2615+03	-.1067+03
1-5,S	-.2840+04	.9090+03	-.2793+04	.2122+04	-.3062+03

(0.75)R

0	.6208+03			
1-5,C	.1577+03	-.3855+03	.1286+04	.2540+03	-.1630+02
1-5,S	-.1078+04	.4573+03	-.1644+04	.1575+04	-.3150+02

(0.85)R

0	.3412+03			
1-5,C	.1307+03	-.3543+03	.6425+03	.1399+03	.1981+01
1-5,S	-.7944+03	.2048+03	-.7646+03	.8015+03	.1612+02

N,C OR S

ADVANCE RATIO, MU = 1.0

(0.0)R

0	-.2811+05			
1-5,C	-.5642+05	-.1274+05	-.4066+04	.5204+04	-.1117+03
1-5,S	-.8770+04	.8629+04	.1254+05	.3780+03	-.3123+04

(0.14)R

0	-.1209+05			
1-5,C	-.2671+05	-.5452+04	-.1821+04	.1206+04	-.1638+03
1-5,S	-.5450+04	.5061+04	.3123+04	-.1410+02	-.9562+03

(0.325)R

0	-.1817+04			
1-5,C	-.9076+04	-.1160+04	-.4498+03	.2789+04	-.2702+03
1-5,S	-.4239+04	.3509+04	-.4372+04	.1592+03	.9190+03

(0.55)R

0	.2089+04			
1-5,C	-.1967+04	-.3878+03	.2755+02	.5912+04	.3040+03
1-5,S	-.3365+04	.2596+04	-.7151+04	.1109+03	.2826+04

(0.75)R

0	.1606+04			
1-5,C	-.2658+03	-.5744+03	.4046+02	.4562+04	.1785+03
1-5,S	-.1712+04	.1279+04	-.4436+04	.2561+03	.1608+04

(0.85)R

0	.7766+03			
1-5,C	-.4874+02	-.3566+03	.1672+02	.2334+04	.8368+02
1-5,S	-.7624+03	.5651+03	-.2098+04	.1578+03	.8156+03

N,C OR S

ADVANCE RATIO, MU = 1.4

(0.0)R

0	-.5207+05			
1-5,C	.7739+05	.2039+05	-.4042+03	.5275+02	-.8323+04
1-5,S	-.3053+05	.6613+04	.1124+05	.2186+05	.8373+04

(0.14)R

0	-.2512+05			
1-5,C	-.3993+05	-.9842+04	-.2256+04	.1699+03	-.2308+04
1-5,S	-.1847+05	.5042+04	.1968+04	.6150+04	-.2570+04

(0.325)R

0	-.5489+04			
1-5,C	-.1396+05	-.2482+04	-.4201+04	.1156+04	.3167+04
1-5,S	-.1099+05	.4557+04	-.6436+04	.7558+04	.2856+04

(0.55)R

0	.2979+04			
1-5,C	-.2365+04	.5784+02	-.3619+04	.3211+04	.9711+04
1-5,S	-.6021+04	.3499+04	-.9306+04	.1284+05	.4842+04

(0.75)R

0	.2593+04			
1-5,C	-.7936+02	-.2972+01	-.1668+04	.2837+04	.3708+04
1-5,S	-.2281+04	.1580+04	-.5440+04	.7824+04	.3528+04

(0.85)R

0	.1259+04			
1-5,C	.4765+02	-.4932+02	-.6723+03	.1497+04	.1977+04
1-5,S	-.8939+03	.6622+03	-.2508+04	.3655+04	.1488+04

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 8.
BIS CYCLIC PITCH TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(G) MP = 0.5
FP = 0.001 (FOR MU = 0.25,0.4,0.5)
FP = 0.000447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S — ADVANCE RATIO, MU = 0.25

		(0.0)R			
0	-.2044+05				
1-5,C	-.4473+05	.7542+03	-.2524+03	.2795+02	.2623+02
1-5,S	-.2228+04	-.1349+03	-.1809+03	-.1639+02	-.9246+01
		(0.14)R			
0	-.1244+04				
1-5,C	-.1904+04	-.2729+02	.2187+02	-.2078+01	.4349+01
1-5,S	-.4256+03	.1050+03	-.1038+02	.8202+01	.9082+01
		(0.325)R			
0	-.2208+01				
1-5,C	.4848+03	-.2165+03	.6912+02	.2267-00	.3719+01
1-5,S	-.6696+03	.1579+03	.3363+02	.9551+01	.1012+02
		(0.55)R			
0	.2198+03				
1-5,C	.9552+03	-.4183+03	.2602+02	.1714+02	-.3386-00
1-5,S	-.5892+03	-.4161+01	.1363+03	.7563+01	.3706+01
		(0.75)R			
0	.1069+04				
1-5,C	.8086+03	-.4062+03	-.8792+02	.2356+02	.1477+01
1-5,S	-.2029+03	-.1037+03	.1858+03	.3717+02	-.9650+01
		(0.85)R			
0	.1065+04				
1-5,C	.4426+03	-.2557+03	-.9900+02	.1632+02	.2686+01
1-5,S	-.2749+02	-.7875+02	.1350+03	.3931+02	-.1076+02

N,C OR S — ADVANCE RATIO, MU = 0.4

		(0.0)R			
0	-.4236+05				
1-5,C	-.5857+05	.2504+04	-.1665+04	.2799+02	.1226+03
1-5,S	-.6297+04	-.8583+03	-.9564+03	.2303+03	-.2886+03
		(0.14)R			
0	-.1736+04				
1-5,C	-.2369+04	-.7073+02	.1015+03	-.5922+02	.1063+01
1-5,S	-.1009+04	.3604+03	-.1171+03	.4776+02	.9083+02
		(0.325)R			
0	.2166+03				
1-5,C	.1186+04	-.7484+03	.3833+03	-.7354+02	-.4840+02
1-5,S	-.1559+04	.5835+03	.7496+02	.2208+02	.9042+02
		(0.55)R			
0	.4699+03				
1-5,C	.2128+04	-.1559+04	.1901+03	.1516+03	-.2852+02
1-5,S	-.1462+04	.4326+02	.7502+03	.3874+01	-.2114+02
		(0.75)R			
0	.1572+04				
1-5,C	.1765+04	-.1517+04	-.4131+03	.4421+03	.2011+03
1-5,S	-.4944+03	-.2982+03	.1221+04	.3398+03	-.1162+03
		(0.85)R			
0	.1526+04				
1-5,C	.8765+03	-.9425+03	-.4908+03	.3894+03	.2298+03
1-5,S	-.3514+02	-.2303+03	.9409+03	.3881+03	-.9771+02

N,C OR S — ADVANCE RATIO, MU = 0.5

		(0.0)R			
0	-.4949+05				
1-5,C	-.7061+05	.4635+04	-.3366+04	.3523+03	.1382+02
1-5,S	-.6791+04	-.1623+04	-.1272+04	.8802+03	-.1347+04
		(0.14)R			
0	-.2081+04				
1-5,C	-.2379+04	-.2340+03	.2058+03	-.1953+03	-.6206-00
1-5,S	-.1327+04	.4672+03	-.2687+03	.8361+02	.1863+03
		(0.325)R			
0	.4934+03				
1-5,C	.1966+04	-.1251+04	.7054+03	.2923+03	.5920-00
1-5,S	-.2254+04	.1079+04	-.9759+02	.2467+03	.4277+03
		(0.55)R			
0	.1144+04				
1-5,C	.2695+04	-.2375+04	.3865+03	.3901+03	.1389+02
1-5,S	-.2331+04	.9604+03	.1367+04	.1531+03	-.2595+02
		(0.75)R			
0	.1648+04				
1-5,C	.2479+04	-.2978+04	-.3745+03	.1342+04	.2890+02
1-5,S	-.1155+04	-.4256+03	.3113+04	.9233+02	-.9884+03
		(0.85)R			
0	.1273+04				
1-5,C	.1611+04	-.2208+04	-.4924+03	.1208+04	.2431+02
1-5,S	-.4161+03	-.6287+03	.2658+04	.1395+03	-.7735+03

N,C OR S — ADVANCE RATIO, MU = 0.7

		(0.0)R			
0	-.5761+05				
1-5,C	-.8609+05	.4928+04	-.1185+05	.3730+04	-.6534+04
1-5,S	-.3352+04	-.7727+04	-.1344+04	.5329+04	-.3443+04
		(0.14)R			
0	-.2023+04				
1-5,C	-.4000+04	.9326+02	-.1349+03	.3370+03	.9162+03
1-5,S	-.1756+04	.1036+04	-.8273+03	.9683+03	.1924+03
		(0.325)R			
0	.2306+04				
1-5,C	.3212+04	-.1382+04	.2188+04	.3878+03	.2384+04
1-5,S	-.3316+04	.3002+04	-.6627+03	.1979+04	.1437+04
		(0.55)R			
0	.2152+04				
1-5,C	.4062+04	-.3849+04	.3976+04	.5911+03	-.2585+03
1-5,S	-.3523+04	.2856+04	.3152+04	.6146+03	.5939+03
		(0.75)R			
0	.1795+04				
1-5,C	.2307+04	-.4778+04	.3585+04	.3891+04	-.4491+04
1-5,S	-.2369+04	.2404+04	.7392+04	.3348+04	-.3539+04
		(0.85)R			
0	.1214+04				
1-5,C	.1004+04	-.3302+04	.2137+04	.3841+04	-.4132+04
1-5,S	-.1296+04	.1015+04	.6016+04	.2831+04	-.3740+04

N,C OR S — ADVANCE RATIO, MU = 1.0

		(0.0)R			
0	-.7509+05				
1-5,C	-.1274+06	-.1498+04	-.3802+05	-.1919+05	.2267+05
1-5,S	-.9942+03	-.2427+05	.3320+04	.1148+05	-.4875+03
		(0.14)R			
0	-.4459+04				
1-5,C	-.9270+04	-.1085+04	-.1912+04	.1861+04	.2508+04
1-5,S	-.3361+04	.1398+04	-.2123+04	.1902+04	-.4570+03
		(0.325)R			
0	.6287+04				
1-5,C	.6865+04	-.1585+04	.6827+04	.5682+04	.9434+04
1-5,S	-.5427+04	.6884+04	-.2944+04	.4688+04	-.8725+03
		(0.55)R			
0	.6017+04				
1-5,C	.6243+04	-.9129+03	.1431+05	.1387+04	.2598+02
1-5,S	-.2877+04	.6004+04	.3162+04	.2079+04	.1741+04
		(0.75)R			
0	.2866+04				
1-5,C	.2652+04	-.4689+03	.1466+05	.7400+03	.1697+05
	-.1290+04	.5462+04	.7230+04	.9477+04	.6283+04
		(0.85)R			
0	.1175+04				
1-5,C	.9797+03	.2959+03	.9165+04	.4774+03	.1508+05
1-5,S	-.8145+03	.3757+04	.5245+04	.7624+04	.5226+04

N,C OR S — ADVANCE RATIO, MU = 1.4

		(0.0)R			
0	-.1121+06				
1-5,C	-.1348+06	.1650+05	-.3145+05	-.6924+04	-.2006+04
1-5,S	.5396+04	-.5209+05	.4264+05	.7513+04	.1984+05
		(0.14)R			
0	-.9997+04				
1-5,C	-.1035+05	-.2099+03	-.5101+04	.2574+04	-.6902+03
1-5,S	-.6425+04	.5944+03	-.2926+04	.2035+04	-.3138+04
		(0.325)R			
0	.1010+05				
1-5,C	.1652+05	-.5334+04	.3748+04	.2936+04	.1294+04
1-5,S	-.1006+05	.1231+05	-.1374+05	.4397+04	-.1018+05
		(0.55)R			
0	.6746+04				
1-5,C	.1145+05	-.2611+04	.1530+05	.5690+04	.2027+04
1-5,S	-.1709+04	.5327+04	-.6622+04	.6917+04	.1684+04
		(0.75)R			
0	.3543+04				
1-5,C	.2372+04	.3140+04	.1595+05	.6613+04	-.3134+04
1-5,S	.1007+03	.2597+04	-.4998+04	.1843+05	.1561+05
		(0.85)R			
0	.2069+04				
1-5,C	.1065+03	.3128+04	.9426+04	.3611+04	-.3389+04
1-5,S	-.4544+03	.1910+04	-.3769+04	.1365+05	.1229+05

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 8.
B1S CYCLIC PITCH TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(H) MP = 0.5
FP = 0.0025 (FOR MU = 0.25,0.4,0.5)
FP = 0.00112(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S		ADVANCE RATIO, MU = 0.25			
		(0.0)R			
0	-.1997+05				
1-S,C	-.3149+05	.3495+03	-.2595+03	+.1581+02	.5992+01
1-S,S	-.1190+04	-.9982+02	-.1105+03	.6268+01	.1013+01
		(0.14)R			
0	-.2958+04				
1-S,C	-.4405+04	-.1179+02	.1973-00	.7234-00	.5246+01
1-S,S	-.5064+03	.7316+02	-.1368+02	.2359+01	.3401+01
		(0.32)R			
0	-.2334+03				
1-S,C	.9754+02	-.1799+03	.7719+02	.1018+02	.8226+01
1-S,S	-.7517+03	.1767+03	.2881+02	.5039+01	.6411+01
		(0.55)R			
0	.3943+03				
1-S,C	.6944+03	-.3417+03	.6441+02	.2326+02	.2495+01
1-S,S	-.7205+03	.1151+03	.1482+03	.1218+02	.3369+01
		(0.75)R			
0	.7091+03				
1-S,C	.6849+03	-.3530+03	.1275+02	.2658+02	+.5565+01
1-S,S	-.3225+03	-.1916+02	.1620+03	.1276+02	+.1996+01
		(0.85)R			
0	.4928+03				
1-S,C	.4126+03	-.2187+03	-.2312+01	.1695+02	-.4985+01
1-S,S	-.1203+03	-.3798+02	.1079+03	.8138+01	-.2271+01

N,C OR S		ADVANCE RATIO, MU = 0.4			
		(0.0)R			
0	-.3014+05				
1-S,C	-.4148+05	.1255+04	-.1562+04	-.2780+03	-.6476+02
1-S,S	-.4725+04	-.7578+03	-.7888+03	-.7084+02	-.1978+03
		(0.14)R			
0	-.4366+04				
1-S,C	-.5553+04	-.5383+02	-.2290+02	-.4672+02	.7628+01
1-S,S	-.1436+04	.2019+03	-.1355+03	-.5770+01	.2354+02
		(0.32)R			
0	-.1507+03				
1-S,C	.7364+03	-.6758+03	.4196+03	.3349+02	.3176+02
1-S,S	-.1705+04	.0248+03	.1105+03	.1978+02	.8655+02
		(0.55)R			
0	.7427+03				
1-S,C	.1711+04	-.1271+04	.3519+03	.2169+03	.1296+02
1-S,S	-.1565+04	.4124+03	.7092+03	.5787+02	-.1002+02
		(0.75)R			
0	.1077+04				
1-S,C	.1509+04	-.1306+04	.7015+02	.3197+03	-.1692+02
1-S,S	-.6726+03	-.0380+02	.1045+04	.7200+02	-.1222+03
		(0.85)R			
0	.7204+03				
1-S,C	.8767+03	-.8078+03	-.1224+02	.2161+03	-.1623+02
1-S,S	-.2354+03	-.1322+03	.7066+03	.4723+02	-.9686+02

N,C OR S		ADVANCE RATIO, MU = 0.5			
		(0.0)R			
0	-.3599+05				
1-S,C	-.4969+05	.2032+04	-.3547+04	+.8756+03	-.8871+03
1-S,S	-.5795+04	-.2157+04	-.1222+04	-.5248+03	-.6311+03
		(0.14)R			
0	-.5043+04				
1-S,C	-.6476+04	-.5518+02	-.1007+03	-.1115+03	.1013+03
1-S,S	-.1901+04	.2886+03	-.3352+03	.4536+02	.5670+02
		(0.32)R			
0	.1746+03				
1-S,C	.1266+04	-.1056+04	.8939+03	.1409+03	.3816+03
1-S,S	-.2446+04	.1260+04	.3475+02	.2141+03	.2512+03
		(0.55)R			
0	.1150+04				
1-S,C	.2490+04	-.2139+04	.9678+03	.5622+03	-.2060+02
1-S,S	-.2455+04	.1078+04	.1471+04	.3814+02	.4121-00
		(0.75)R			
0	.1363+04				
1-S,C	.2063+04	-.2295+04	.5111+03	.7622+03	-.5329+03
1-S,S	-.1255+04	.2759+03	.2404+04	-.1974+03	-.3060+03
		(0.85)R			
0	.8230+03				
1-S,C	.1173+04	-.1438+04	.2238+03	.5064+03	-.4231+03
1-S,S	-.5570+03	.1229+02	.1656+04	+.1671+03	-.2476+03

N,C OR S		ADVANCE RATIO, MU = 0.7			
		(0.0)R			
0	-.4168+05				
1-S,C	-.6476+05	-.4180+03	-.1277+05	+.5570+04	-.9149+04
1-S,S	-.5149+04	-.5132+04	.3214+03	.8472+03	.3488+04
		(0.14)R			
0	-.6637+04				
1-S,C	-.1041+05	-.3225+03	-.1187+04	+.3153+03	.4890+03
1-S,S	-.2494+04	.3848+03	-.7595+03	.3535+03	-.4304+03
		(0.32)R			
0	.1457+04				
1-S,C	.2080+04	+.1067+04	.2983+04	.1626+04	.2346+04
1-S,S	-.3664+04	.2942+04	-.8474+03	.8499+02	-.1648+04
		(0.55)R			
0	.2367+04				
1-S,C	.3626+04	+.2791+04	.5478+04	.2292+04	-.3246+02
1-S,S	-.3953+04	.3347+04	.2409+04	-.1188+04	.9231+03
		(0.75)R			
0	.1398+04				
1-S,C	.2289+04	.2213+04	-.3213+04	.5115+04	.1730+04
1-S,S	-.2317+04	.1969+04	.4673+04	+.1929+04	.2647+04
		(0.85)R			
0	.6575+03				
1-S,C	.1121+04	-.2008+04	.2999+04	.9368+03	-.2076+04
1-S,S	-.1104+04	.9375+03	.3197+04	+.1286+04	.1959+04

N,C OR S		ADVANCE RATIO, MU = 1.0			
		(0.0)R			
0	-.5811+05				
1-S,C	-.9531+05	-.7717+04	-.3114+05	+.1116+05	-.1896+04
1-S,S	-.7693+04	-.1249+05	.8740+04	.4689+04	.8419+04
		(0.14)R			
0	-.1072+05				
1-S,C	-.1893+05	-.2301+04	-.4879+04	-.3401+03	-.1315+03
1-S,S	-.4270+04	.3077+03	-.2989+03	.1259+04	-.1477+04
		(0.32)R			
0	.4454+04				
1-S,C	.4136+04	-.1185+04	.6631+04	.4005+04	.7315+03
1-S,S	-.5328+04	.0582+04	-.4127+04	+.8799+03	-.4988+04
		(0.55)R			
0	.6052+04				
1-S,C	.6004+04	+.4718+03	.1486+05	.2276+04	.1115+04
1-S,S	-.3950+04	.6501+04	-.1971+04	+.5370+04	.2478+04
		(0.75)R			
0	.2950+04				
1-S,C	.2290+04	.2414+03	.1425+05	+.8268+03	.8578+03
1-S,S	-.8256+03	.2767+04	.1317+04	-.6762+04	.8093+04
		(0.85)R			
0	.1263+04				
1-S,C	.7063+03	.2483+03	.8217+04	+.9693+03	.4607+03
1-S,S	-.1444+01	.1032+04	.1284+04	+.4166+04	.5651+04

N,C OR S		ADVANCE RATIO, MU = 1.4			
		(0.0)R			
0	-.1012+06				
1-S,C	-.1192+06	-.1068+05	-.2716+05	+.2195+04	.1030+05
1-S,S	-.3528+05	-.1653+05	.3233+05	.7619+04	-.1921+04
		(0.14)R			
0	-.2503+05				
1-S,C	-.2592+05	-.4300+04	-.7497+04	.1616+04	-.6839+03
1-S,S	-.1514+05	.1777+03	.3321+04	.3103+04	-.1167+04
		(0.32)R			
0	.4761+04				
1-S,C	.1250+05	-.2518+04	.2332+04	.1444+04	-.5936+04
1-S,S	-.1063+05	.7839+04	-.1235+05	+.1053+04	-.8881+03
		(0.55)R			
0	.8231+04				
1-S,C	.1398+05	-.4227+03	.1131+05	+.8355+04	-.8355+03
1-S,S	-.4530+04	.1836+04	-.1529+05	+.1114+05	.7293+03
		(0.75)R			
0	.3049+04				
1-S,C	.3522+04	.1139+04	.1201+05	+.1238+05	.4088+04
1-S,S	.1537+04	-.4760+04	-.8722+04	-.1361+05	.1638+04
		(0.85)R			
0	.9524+03				
1-S,C	.4801+03	.0589+03	.6936+04	-.7627+04	.3022+04
1-S,S	.1692+04	-.3641+04	.4047+04	.8108+04	.1059+04

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 8.
B1S CYCLIC PITCH TRANSFER COEFFICIENTS FOR 4 HINGELESS BLADE

(I) MP = 8.5
FP = 0.01 (FOR MU = 0.25,0.4,0.5)
FP = 0.00447(1+MU**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S — ADVANCE RATIO, MU = 0.25

(0.0)R

0	-.1138+05			
1S,C	-.1781+05	-.1592+03	-.1413+03	.1558+01	.9511+01
1S,S	-.1065+03	.1265+03	.1226+03	.3974+02	.9368+01

(0.14)R

0	-.4329+04			
1S,C	-.6702+04	.6998+02	-.2728+02	.4782-01	.3143+01
1S,S	-.4010+03	.1291+03	.2611+02	.9575+01	.2265+01

(0.325)R

0	-.1113+04			
1S,C	-.1675+04	-.6877+02	.5026+02	.3535+01	.3309+01
1S,S	-.7976+03	.1893+03	-.2502+02	.9851+01	.7512-00

(0.557)R

0	.7286+02			
1S,C	-.6940+02	-.1418+03	.8475+02	.9980+01	.2325+01
1S,S	-.8260+03	.1852+03	-.1884+02	.1899+02	-.6364+00

(0.757)R

0	.3100+03			
1S,C	.2101+03	-.1317+03	.5958+02	.9558+01	.6516+00
1S,S	-.4312+03	.9437+02	.1786+01	-.1393+02	-.1022+01

(0.857)R

0	.1899+03			
1S,C	.1322+03	-.7244+02	.2991+02	.5280+01	.1604+00
1S,S	-.1917+03	.4150+02	.3708+01	-.7115+01	-.6625+00

N,C OR S — ADVANCE RATIO, MU = 0.4

(0.0)R

0	-.1764+05			
1S,C	-.2387+05	-.7999+03	-.4179+04	.1703+03	-.2201+02
1S,S	-.3246+04	.6758+02	.5002+03	.3464+03	.4757+02

(0.14)R

0	-.6718+04			
1S,C	-.8754+04	-.3839+03	-.2508+03	.5897+02	-.1267+01
1S,S	-.2003+04	.2895+03	.6507+02	.6876+02	.1246+02

(0.325)R

0	-.1605+04			
1S,C	-.1709+04	-.3603+03	.3504+03	.2774+02	.1034+02
1S,S	-.2002+04	.5572+03	-.1541+03	.1290+03	-.1841+02

(0.557)R

0	.2317+03			
1S,C	.5621+03	-.5801+03	.5867+03	.1379+03	.9187+01
1S,S	-.1766+04	.5099+03	-.2866+02	-.2219+03	.9318+02

(0.757)R

0	.5270+03			
1S,C	.6906+03	-.4884+03	.3993+03	.1398+03	-.2417+01
1S,S	-.8625+03	.2186+03	.1048+03	.1585+03	-.9917+02

(0.857)R

0	.3110+03			
1S,C	.3748+03	-.2621+03	.1983+03	.7884+02	-.2320+01
1S,S	-.3725+03	.8581+02	.7365+02	.8014+02	-.2689+02

N,C OR S — ADVANCE RATIO, MU = 0.5

(0.0)R

0	-.2199+05			
1S,C	-.2932+05	-.1905+04	-.2835+04	.4695+03	-.6944+02
1S,S	-.5225+04	-.1874+03	.1398+04	.1000+04	.2535+03

(0.14)R

0	-.8155+04			
1S,C	-.1059+05	-.8091+03	-.6353+03	.1588+03	-.4826+01
1S,S	-.3094+04	.4195+03	.1653+03	.2156+03	.1976+02

(0.325)R

0	-.1726+04			
1S,C	-.1748+04	-.5673+03	.7989+03	.7335+02	.2469+02
1S,S	-.2979+04	.1014+04	-.4904+03	-.3588+03	.2098+03

(0.557)R

0	.4927+03			
1S,C	.1082+04	-.9121+03	.1435+04	.3269+03	.2803+02
1S,S	-.2700+04	.9804+03	-.2199+03	.4784+03	-.1292+03

(0.757)R

0	.7174+03			
1S,C	.1970+04	-.8815+03	.1023+04	.3219+03	-.3417+02
1S,S	-.1392+04	.4457+03	.1659+03	-.5618+03	.6629+02

(0.857)R

0	.4039+03			
1S,C	.5628+03	-.4356+03	.5868+03	.1765+03	.8215+02
1S,S	-.6201+03	.1828+03	.1419+03	.2934+03	-.3894+02

N,C OR S — ADVANCE RATIO, MU = 0.7

(0.0)R

0	-.2662+05			
1S,C	-.4202+05	-.7672+04	-.7936+04	.3171+03	.9197+03
1S,S	-.7258+04	.2468+04	.8917+04	.5708+04	.1755+04

(0.14)R

0	-.1061+05			
1S,C	-.1688+05	-.2983+04	-.2195+04	.2194+02	.1163+03
1S,S	-.4735+04	.1956+04	.1962+04	.1418+04	.1381+03

(0.325)R

0	-.1804+04			
1S,C	-.3406+04	-.7715+03	.1963+04	-.4318+03	-.4844+03
1S,S	-.4671+04	.2194+04	-.2738+04	-.1919+04	-.8884+03

(0.557)R

0	.1188+04			
1S,C	.1149+04	-.8736+03	.4124+04	-.8333+03	-.6402+03
1S,S	-.4457+04	.1783+04	-.3766+04	-.3911+04	-.5820+03

(0.757)R

0	.1030+04			
1S,C	.1173+04	-.9638+03	.3037+04	-.6673+03	-.3659+03
1S,S	-.2475+04	.7374+03	-.2017+04	-.2950+04	.3363+02

(0.857)R

0	.5138+03			
1S,C	.5937+03	-.5537+03	.1538+04	-.3486+03	-.1684+03
1S,S	-.1142+04	.2870+03	-.8949+03	-.1508+04	.9387+02

N,C OR S — ADVANCE RATIO, MU = 1.0

(0.0)R

0	-.3994+05			
1S,C	-.5796+05	-.1194+05	-.6496+04	.9678+04	-.1206+03
1S,S	-.1314+05	.4108+04	.2086+05	.1987+04	-.3608+04

(0.14)R

0	-.1682+05			
1S,C	-.2581+05	-.5169+04	-.2497+04	.2485+04	-.3486+03
1S,S	-.8330+04	.4217+04	.5375+04	.8720+03	-.1163+04

(0.325)R

0	-.1941+04			
1S,C	-.3997+04	-.1305+04	.4906+03	-.4824+04	-.9618+03
1S,S	-.6533+04	.5223+04	-.6677+04	-.1745+03	.1216+04

(0.557)R

0	.3316+04			
1S,C	.1078+04	-.8031+03	.2112+04	-.9598+04	-.3674+03
1S,S	-.4841+04	.4167+04	-.1075+05	-.1304+04	.3324+04

(0.757)R

0	.2263+04			
1S,C	.1096+04	-.8974+03	.1636+04	.7389+04	.6253+02
1S,S	-.2184+04	.1648+04	-.6460+04	-.1235+04	.2747+04

(0.857)R

0	.1051+04			
1S,C	.5039+03	-.5215+03	.8302+03	.3775+04	-.2015-01
1S,S	-.9170+03	.6188+03	-.3014+04	.6648+03	.1431+04

N,C OR S — ADVANCE RATIO, MU = 1.4

(0.0)R

0	-.6521+05			
1S,C	-.7462+05	-.2396+05	.5322+03	.9686+04	-.1059+05
1S,S	-.3701+05	.4158+04	.2473+05	.2588+05	-.1138+05

(0.14)R

0	-.3014+05			
1S,C	-.3526+05	-.1193+05	-.3179+04	.2444+04	-.3265+04
1S,S	-.2339+05	.4373+03	.8716+04	-.6975+04	-.3431+04

(0.325)R

0	-.4434+04			
1S,C	-.7091+04	-.3787+04	-.6828+04	.5603+04	.3489+04
1S,S	-.1517+05	.3927+04	-.1056+05	.9618+04	.3844+04

(0.557)R

0	.5422+04			
1S,C	.3181+04	-.1881+04	-.6201+04	-.1199+05	.7968+04
1S,S	-.8549+04	.2876+04	-.1913+05	.1592+05	.9326+04

(0.757)R

0	.3615+04			
1S,C	.2041+04	-.7373+03	-.2612+04	-.9038+04	.4830+04
1S,S	-.3012+04	.4393+03	-.8284+04	.9647+04	.3886+04

(0.857)R

0	.1633+04			
1S,C	.6326+03	-.4108+03	-.1027+04	.4568+04	.2356+04
1S,S	-.2109+04	.3337+02	-.3701+04	.4499+04	.2431+04

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 9.
PRECONING TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(A) MP = 0.1
FP = 0.001 (FOR MU = 0.25,0.4,0.5)
FP = 0.000447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S — ADVANCE RATIO, MU = 0.25

(0.0)R

0	-.3401+05				
1-S,C	-.7564+03	-.9957+02	-.1161+03	.7420+02	-.7144+02
1-S,S	.3057+02	-.2049+03	-.1360+03	.8933+02	-.8995+02

(0.14)R

0	-.1477+04				
1-S,C	-.3706+02	-.6656+01	-.2190+01	.2149+01	-.1191+01
1-S,S	-.1115+01	-.1140+02	-.7651+01	.5716+01	-.4485-00

(0.325)R

0	.8707+02				
1-S,C	-.4469+01	-.3272+01	.9633+01	.3965+01	.4815+01
1-S,S	-.9470+01	-.5316+01	-.2357+01	.2664+01	.5455+01

(0.55)R

0	.6865+02				
1-S,C	-.2784+01	-.6719+01	.1560+02	.5963+01	.3157+01
1-S,S	-.1167+02	-.6204+01	-.6950-00	.8928-00	-.4834-00

(0.75)R

0	.1435+03				
1-S,C	-.3988+01	-.1791+02	.1143+02	.2790+01	-.4459+01
1-S,S	.4572+01	-.2665+01	.4591-00	.5943+01	-.9210+01

(0.85)R

0	.1354+03				
1-S,C	-.3905+01	-.1684+02	.5697+01	.4685-00	-.5807+01
1-S,S	.9939+01	-.5191-00	.3862-00	.5575+01	-.8749+01

N,C OR S — ADVANCE RATIO, MU = 0.4

(0.0)R

0	-.3401+05				
1-S,C	-.5592+03	-.9433+02	-.1125+03	.6287+02	-.6598+02
1-S,S	.1447+03	-.1567+03	-.1258+03	.7963+02	-.7794+02

(0.14)R

0	-.1477+04				
1-S,C	-.2863+02	-.6618+01	-.2013+01	-.2285+01	-.5471-00
1-S,S	.4319+01	-.9965+01	-.6787+01	.4948+01	-.3839-00

(0.325)R

0	.6747+02				
1-S,C	-.3298+0	-.3028+01	.1014+02	.3057+01	.5830+01
1-S,S	-.8671+01	-.5447+01	-.7594-00	-.1668+01	.5205+01

(0.55)R

0	.6909+02				
1-S,C	.1865+01	-.5327+01	.1682+02	.6949+01	.3807+01
1-S,S	-.1173+02	-.3842+01	.2257+01	.1842+01	.2734-01

(0.75)R

0	.1440+03				
1-S,C	-.1256+01	-.1686+02	.1199+02	.6327+01	-.5743+01
1-S,S	.1520+01	-.8048-00	.2632+01	.5203+01	-.6642+01

(0.85)R

0	.1359+03				
1-S,C	-.3313+01	-.1643+02	.5716+01	.3648+01	-.7405+01
1-S,S	.6740+01	.1443-00	.1830+01	.4361+01	-.6460+01

N,C OR S — ADVANCE RATIO, MU = 0.5

(0.0)R

0	-.3394+05				
1-S,C	-.5601+03	-.9259+02	-.9247+02	-.2813+02	-.4395+02
1-S,S	.1778+03	-.2212+03	-.9201+02	-.9072+02	-.1109+02

(0.14)R

0	-.1499+04				
1-S,C	-.2822+02	-.6299+01	-.2735+01	-.5854+01	-.2844+01
1-S,S	.3768+01	-.8409+01	-.5217+01	-.5689-00	-.8494+01

(0.325)R

0	.7708+02				
1-S,C	-.6558+01	-.1073+02	.4224+01	-.7457+01	-.1271+01
1-S,S	-.8132+01	.4208+01	-.5548+01	.4179+01	-.1479+02

(0.55)R

0	.1053+03				
1-S,C	-.6862+01	-.2322+02	.8559+01	.2903+01	.1200+01
1-S,S	-.3402+01	.7321+01	-.1842+02	-.9989+01	-.3897+01

(0.75)R

0	.1143+03				
1-S,C	-.3223+01	-.3161+02	.1126+02	.1906+02	.4790+01
1-S,S	.6506+01	.8692+01	-.3012+02	-.2864+02	.1696+02

(0.85)R

0	.7862+02				
1-S,C	-.1073+01	-.2407+02	.8477+01	.1798+02	.4372+01
1-S,S	.7523+01	.8315+01	-.2411+02	-.2527+02	.1803+02

N,C OR S — ADVANCE RATIO, MU = 0.7

(0.0)R

0	-.3066+05				
1-S,C	-.6309+03	-.2181+03	.4254+01	.4858+02	.9514+02
1-S,S	.1820+03	-.2945+03	-.1526+03	.9047+02	-.1193+03

(0.14)R

0	-.2003+04				
1-S,C	-.4314+02	-.9775+01	-.2708+01	.9945-00	-.2120+02
1-S,S	.1061+02	-.1975+02	-.1046+00	.6191+01	.3657+01

(0.325)R

0	.5027+02				
1-S,C	.3370+01	.1035+02	-.1117+02	.4357+01	-.4912+02
1-S,S	-.7884+01	.8223+01	-.2676+01	.3339-00	.1952+02

(0.55)R

0	.6785+02				
1-S,C	.8362+01	-.5696+01	-.4261+02	.2123+02	-.4027+01
1-S,S	-.5786+01	.2860+01	-.1355+02	.1678+02	-.1582+02

(0.75)R

0	.1417+03				
1-S,C	-.5260+01	-.4154+02	-.8036+02	.5491+02	.6773+02
1-S,S	.1850+02	.3277+02	-.2594+02	.4802+02	-.7245+02

(0.85)R

0	.1266+03				
1-S,C	-.9043+01	-.3866+02	-.6452+02	.4589+02	.6395+02
1-S,S	.2082+02	.2134+02	-.2075+02	.4178+02	-.6422+02

N,C OR S — ADVANCE RATIO, MU = 1.0

(0.0)R

0	-.2680+05				
1-S,C	-.1659+03	-.9493+02	.1633+02	.1691+02	-.5753+02
1-S,S	.1980+03	-.1078+03	-.1674+03	.3952+02	-.2170+03

(0.14)R

0	-.2656+04				
1-S,C	-.2070+02	-.3127+01	.3263+01	.2518+01	.5273+01
1-S,S	.1800+02	-.2342+02	-.9618+01	.7184+01	.2130+02

(0.325)R

0	-.2903+02				
1-S,C	.6744+01	.1346+02	-.3131+01	.3804+01	.1923+02
1-S,S	-.6198+01	.7624+01	.1554+02	.4602+01	.7284+02

(0.55)R

0	5393+02				
1-S,C	.2328+02	.9853-00	-.3803+02	-.2231+02	-.1470+02
1-S,S	-.3621+01	.2828+02	.3047+02	.2030+01	-.2135+02

(0.75)R

0	.1354+03				
1-S,C	-.2297+01	-.2541+02	-.7289+02	-.7603+02	-.6497+02
1-S,S	.1260+02	.2876+02	.4548+02	-.3525+01	-.1478+03

(0.85)R

0	.1168+03				
1-S,C	-.1100+02	-.2305+02	-.5501+02	.6295+02	-.5394+02
1-S,S	.1275+02	.1489+02	.3351+02	.3200+01	-.1236+03

N,C OR S — ADVANCE RATIO, MU = 1.4

(0.0)R

0	-.2309+05				
1-S,C	-.1166+04	-.1771+03	-.4787+03	.3577+01	-.1227+03
1-S,S	-.6052+02	-.2480+02	-.4653+03	-.1811+03	-.5266+01

(0.14)R

0	-.3360+04				
1-S,C	-.1952+03	-.3057+02	-.2258+02	-.7127-00	.1160+02
1-S,S	-.1741+02	-.4771+02	-.4925+02	-.2202+02	-.2204+02

(0.325)R

0	-.1524+03				
1-S,C	-.2553+02	-.5887+01	.9805+02	-.8271+01	.4354+02
1-S,S	-.2206+02	-.4811+02	.6198+02	.1414+02	-.3866+02

(0.55)R

0	.5501+02				
1-S,C	.4164+02	-.1986+01	.1358+03	-.2003+01	-.2357+02
1-S,S	-.1450+02	.2263+02	.1145+03	.4421+02	.3081+02

(0.75)R

0	.1227+03				
1-S,C	.3494+02	-.1069+02	.1396+03	.2467+02	-.8619+02
1-S,S	.1266+02	.1846+02	.8863+02	.6142+02	.1236+03

(0.85)R

0	.9633+02				
1-S,C	.1495+02	-.9426+01	.8946+02	.2199+02	-.6427+02
1-S,S	.1407+02	.3213+01	.4693+02	.4152+02	.9609+02

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 9.
PRECONING TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(B) MP = 0.1
FP = 0.0025 (FOR MU = 0.25,0.4,0.5)
FP = 0.00112(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S — ADVANCE RATIO, MU = 0.25

(0.0)R

0	-.2310+05				
1-S,C	-.4728+03	-.1089+03	-.1565+01	-.2770+02	-.2324+02
1-S,S	.1431+03	-.1462+03	-.7284+02	-.5093+02	-.3762+02

(0.14)R

0	-.3317+04				
1-S,C	-.7214+02	-.1520+02	-.4953+01	-.5718+01	-.6375+01
1-S,S	.1740+02	-.2201+02	-.1261+02	-.8627+01	-.6551+01

(0.325)R

0	-.1711+03				
1-S,C	-.1226+02	-.3772-00	-.1273+02	-.4398+01	-.5976+01
1-S,S	-.4802+01	-.2204+01	-.6549+01	-.4056+01	-.3110+01

(0.55)R

0	.8187+02				
1-S,C	-.4529+01	-.1118+01	-.2048+02	-.5211+01	-.2277+01
1-S,S	-.2723+01	.3480+01	-.1010+02	-.6161+01	-.3654+01

(0.75)R

0	.7669+02				
1-S,C	.1026+01	-.2665+01	-.1910+02	-.3769+01	.3049+01
1-S,S	.2808+01	.6775+01	-.9921+01	-.6051+01	-.2835+01

(0.85)R

0	.4190+02				
1-S,C	.2115+01	-.1956+01	-.1144+02	-.2052+01	.2906+01
1-S,S	.2827+01	.4773+01	-.6063+01	-.3699+01	-.1586+01

N,C OR S — ADVANCE RATIO, MU = 0.4

(0.0)R

0	-.2309+05				
1-S,C	-.3597+03	-.1042+03	.9750-00	-.1969+02	-.1516+02
1-S,S	.1575+03	-.1155+03	-.6429+02	-.4274+02	-.3114+02

(0.14)R

0	-.3316+04				
1-S,C	-.5558+02	-.1455+02	-.4410+01	-.4998+01	-.5940+01
1-S,S	.1949+02	-.1833+02	-.1122+02	-.7540+01	-.5687+01

(0.325)R

0	-.1704+03				
1-S,C	-.1056+02	-.5455-00	-.1245+02	-.5242+01	-.7152+01
1-S,S	-.4132+01	-.3222+01	-.6208+01	-.4354+01	-.3332+01

(0.55)R

0	.8290+02				
1-S,C	-.3532+01	-.1928+01	-.2071+02	-.5943+01	-.2187+01
1-S,S	-.3030+01	.3391+01	-.1011+02	-.7122+01	-.4383+01

(0.75)R

0	.7756+02				
1-S,C	.2563+01	-.3766+01	-.1977+02	-.3916+01	.4694+01
1-S,S	.1659+01	.8189+01	-.1024+02	-.7210+01	-.3713+01

(0.85)R

0	.4240+02				
1-S,C	.2698+01	-.2687+01	-.1195+02	-.2010+01	.4220+01
1-S,S	.1961+01	.5939+01	-.6315+01	-.4447+01	-.2152+01

N,C OR S — ADVANCE RATIO, MU = 0.5

(0.0)R

0	-.2308+05				
1-S,C	-.4294+03	-.1590+03	.3428+02	.7309+01	.3485+01
1-S,S	.1331+03	-.1997+03	-.1676+03	-.6868+02	-.4524+02

(0.14)R

0	-.3314+04				
1-S,C	-.6468+02	-.1931+02	-.3267+01	-.5216+01	-.7369+01
1-S,S	.1525+02	-.2100+02	-.1749+02	-.9411+01	-.6093+01

(0.325)R

0	-.1708+03				
1-S,C	-.7667+01	.6864+01	-.2232+02	-.1452+01	-.1521+02
1-S,S	-.6163+01	-.5724+01	.1505+02	-.1027+00	-.7389-00

(0.55)R

0	.7868+02				
1-S,C	.6584+01	.9293+01	-.3805+02	-.1676+02	-.7068+01
1-S,S	-.2421+01	.6680+01	.2275+02	-.1482+01	-.4873+01

(0.75)R

0	.7144+02				
1-S,C	.1526+02	.9540+01	-.3664+02	-.1065+02	.6353+01
1-S,S	.4820+01	.1413+02	.1818+02	-.3142+01	-.7785+01

(0.85)R

0	.3825+02				
1-S,C	.1098+02	.2637+01	-.2219+02	-.5334+01	.6517+01
1-S,S	.4393+01	.1009+02	.1023+02	-.2264+01	-.5352+01

N,C OR S — ADVANCE RATIO, MU = 0.7

(0.0)R

0	-.2051+05				
1-S,C	-.6961+03	-.2583+03	-.1959+03	-.3396+02	-.5676+02
1-S,S	.1503+03	-.7289+02	-.4071+03	-.1516+03	-.6219+02

(0.14)R

0	-.3715+04				
1-S,C	-.1308+03	-.3671+02	-.2131+02	-.8523+01	-.5131+01
1-S,S	.2009+02	-.2566+02	-.4765+02	-.2353+02	-.1642+02

(0.325)R

0	-.3059+03				
1-S,C	-.1520+02	.1950+02	.3083+02	-.6200+01	.5216+01
1-S,S	-.1232+02	-.2443+02	.6542+02	.1273+02	-.6521+01

(0.55)R

0	.5477+02				
1-S,C	.1402+02	.2724+02	.4193+02	-.7034+01	-.1197+02
1-S,S	-.1059+02	-.9509+01	.1182+03	.3658+02	.1439+02

(0.75)R

0	.5604+02				
1-S,C	.2501+02	.1702+02	.2885+02	-.4901+01	-.2526+02
1-S,S	-.6503-00	.1171+02	.1069+03	.4071+02	.2836+02

(0.85)R

0	.2828+02				
1-S,C	.1749+02	.8342+01	.1495+02	-.2574+01	-.1768+02
1-S,S	.1369+01	.1053+02	.6201+02	.2508+02	.1943+02

N,C OR S — ADVANCE RATIO, MU = 1.0

(0.0)R

0	-.1775+05				
1-S,C	-.7953+03	-.1995+03	-.4742+03	-.7680+02	-.5729+02
1-S,S	.1804+03	.5278+02	-.2559+03	-.1357+03	-.4852+02

(0.14)R

0	-.4136+04				
1-S,C	-.1993+03	-.5921+02	-.5789+02	-.1242+02	-.4925+01
1-S,S	.3723+02	-.9803+01	-.4152+02	-.2454+02	-.1782+02

(0.325)R

0	-.5177+03				
1-S,C	-.4821+02	.1140+02	.1186+03	.1410+02	.1236+02
1-S,S	-.5254+01	-.4119+02	.3868+02	.1176+02	-.5569+01

(0.55)R

0	.2027+02				
1-S,C	-.5011+01	.2130+02	.1851+03	.2994+02	-.2581-00
1-S,S	-.1047+02	-.2383+02	.6629+02	.4075+02	.2820+02

(0.75)R

0	.4967+02				
1-S,C	.1745+02	.1451+02	.1410+03	.2762+02	-.1363+02
1-S,S	-.5280+01	.6247+01	.5180+02	.3825+02	.4456+02

(0.85)R

0	.2536+02				
1-S,C	.1333+02	.7336+01	.7535+02	.1575+02	-.1006+02
1-S,S	-.2201+01	.8338+01	.2792+02	.2191+02	.2856+02

N,C OR S — ADVANCE RATIO, MU = 1.4

(0.0)R

0	-.1567+05				
1-S,C	-.4537+03	-.1156+03	-.2718+03	-.7028+02	-.4105+02
1-S,S	.2717+03	.1522+03	-.3266+01	-.8483+02	-.4112+02

(0.14)R

0	-.4463+04				
1-S,C	-.1712+03	-.3594+02	-.4269+02	-.1584+02	-.9604+01
1-S,S	.7906+02	.8528+01	-.1068+02	-.2128+02	-.1608+02

(0.325)R

0	-.8028+03				
1-S,C	-.9575+02	-.1310+02	.6654+02	.1247+02	.6247+01
1-S,S	.9984+01	-.5926+02	-.3087+02	.3780+01	-.3912+01

(0.55)R

0	-.4193+02				
1-S,C	-.4721+02	-.1677+02	.7647+02	.3182+02	.1678+02
1-S,S	-.8066+01	-.3102+02	-.5870+02	.7898+01	.1811+02

(0.75)R

0	.3966+02				
1-S,C	.1716-00	-.1571+02	.3538+02	.2910+02	.1547+02
1-S,S	-.8590+01	.1428+02	-.5218+02	.4071+01	.2574+02

(0.85)R

0	.2346+02				
1-S,C	.6333+01	-.8905+01	.1432+02	.1619+02	.8617+01
1-S,S	-.4793+01	.1452+02	-.2889+02	.1735+01	.1572+02

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 9.
PRECONING TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(C) MP = 0.1
FP = 0.01 (FOR MU = 0.25,0.4,0.5)
FP = 0.00447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S					
	ADVANCE RATIO, MU = 0.25				
	(0.0)R				
0	-.1202+05				
1-S,C	-.1630+02	-.6585+02	-.5624+02	-.5814+01	-.1063+02
1-S,S	.2756+03	-.1580+02	-.3957+02	-.2555+02	-.1607+02
	(0.14)R				
0	-.4516+04				
1-S,C	-.1348+02	-.2383+02	-.1724+02	-.5290+01	-.5595+01
1-S,S	.1062+03	-.1022+02	-.1372+02	-.9110+01	-.6120+01
	(0.325)R				
0	-.1161+04				
1-S,C	-.1526+02	-.3632+01	.4146+01	-.8173+01	-.4903+01
1-S,S	.3240+02	-.9432+01	-.5510-00	-.1214+01	-.1807+01
	(0.55)R				
0	-.2056+03				
1-S,C	-.8272+01	.3707+01	.1200+02	-.1030+02	-.5265+01
1-S,S	.1082+02	-.4687+01	.4809+01	.1376+01	-.7408-00
	(0.75)R				
0	-.2996+02				
1-S,C	.2375-00	.3754+01	.8708+01	-.6925+01	-.3407+01
1-S,S	.3929+01	.3679-00	.4220+01	.1236+01	-.4244-00
	(0.85)R				
0	-.8244+01				
1-S,C	.1173+01	.2027+01	.4387+01	-.3451+01	-.1682+01
1-S,S	.1641+01	.6168-00	.2238+01	.6441-00	-.2154-00

N,C OR S					
	ADVANCE RATIO, MU = 0.4				
	(0.0)R				
0	-.1202+05				
1-S,C	.5847+01	-.5390+02	-.4777+02	-.8453+01	-.1056+02
1-S,S	.2716+03	.8561+01	-.4181+02	-.2107+02	-.1360+02
	(0.14)R				
0	-.4514+04				
1-S,C	.8579+01	-.1967+02	-.1504+02	-.5443+01	-.5314+01
1-S,S	.1049+03	-.5444+01	-.1390+02	-.8370+01	-.5662+01
	(0.325)R				
0	-.1160+04				
1-S,C	-.2015+02	-.3408+01	.1951+01	-.6491+01	-.4292+01
1-S,S	.3233+02	-.1546+02	.8297-00	-.2805+01	-.2574+01
	(0.55)R				
0	-.2044+03				
1-S,C	-.1416+02	.2409+01	.6640+01	-.8030+01	-.4494+01
1-S,S	.1079+02	-.9946+01	.6853+01	-.5698-00	-.1690+01
	(0.75)R				
0	-.2897+02				
1-S,C	-.2217+01	.2626+01	.4192+01	-.5515+01	-.2907+01
1-S,S	.3729+01	-.3607-00	.5592+01	.2578-00	-.8937-00
	(0.85)R				
0	-.7713+01				
1-S,C	.2561-00	.1432+01	.1981+01	-.2774+01	-.1437+01
1-S,S	.1504+01	.1001+01	.2918+01	.2234-00	-.4147-00

N,C OR S					
	ADVANCE RATIO, MU = 0.5				
	(0.0)R				
0	-.1201+05				
1-S,C	-.7322+01	-.5873+02	-.5531+02	.1250+01	-.3495+01
1-S,S	.2828+03	.1736+02	-.6999+02	-.2037+02	-.1042+02
	(0.14)R				
0	-.4514+04				
1-S,C	-.1692+02	-.2151+02	-.1686+02	-.4159+01	-.4785+01
1-S,S	.1094+03	-.5043+01	-.2035+02	-.8901+01	-.5402+01
	(0.325)R				
0	-.1160+04				
1-S,C	-.2788+02	-.3803+01	.2718+01	-.1116+02	-.8211+01
1-S,S	.3416+02	-.1943+02	.8240+01	-.4729+01	-.4832+01
	(0.55)R				
0	-.2039+03				
1-S,C	-.1862+02	.2722+01	.6823+01	-.1496+02	-.9107+01
1-S,S	.1205+02	-.1083+02	.1996+02	-.3344+01	-.5738+01
	(0.75)R				
0	-.2879+02				
1-S,C	-.2687+01	.3047+01	.2716+01	-.1007+02	-.5307+01
1-S,S	.4519+01	.1946+01	.1473+02	-.1692+01	-.4029+01
	(0.85)R				
0	-.7637+01				
1-S,C	.4761-00	.1675+01	.1018+01	-.5008+01	-.2492+01
1-S,S	.1899+01	.2695+01	.7490+01	-.7611-00	-.2047+01

N,C OR S					
	ADVANCE RATIO, MU = 0.7				
	(0.0)R				
0	-.1060+05				
1-S,C	.7125+02	.4555+02	-.6009+02	-.7839+02	-.3656+02
1-S,S	.3952+03	.8092+02	-.3837+02	-.5394+02	-.3009+02
	(0.14)R				
0	-.4469+04				
1-S,C	.4694+01	-.2060+02	-.1986+02	-.2292+02	-.1322+02
1-S,S	.1715+03	.1345+01	-.1675+02	-.1968+02	-.1128+02
	(0.325)R				
0	-.1348+04				
1-S,C	-.4021+02	-.8510+01	.1607+01	.1478+02	.1938+01
1-S,S	.5968+02	-.3924+02	-.6138+01	.2383+01	-.3200-00
	(0.55)R				
0	-.2968+03				
1-S,C	-.3536+02	-.3352+01	.1326+01	.3100+02	.1056+02
1-S,S	.1896+02	-.3298+02	-.2461+01	.1485+02	.4024+01
	(0.75)R				
0	-.5895+02				
1-S,C	-.9644+01	-.8278-00	-.3187+01	.2168+02	.8938+01
1-S,S	.4865+01	-.8128+01	-.9830-00	.1265+02	.3158+01
	(0.85)R				
0	-.1888+02				
1-S,C	-.2185+01	-.2207-00	-.2378+01	.1077+02	.4696+01
1-S,S	.1571+01	-.1465+01	-.4205-00	.6652+01	.1601+01

N,C OR S					
	ADVANCE RATIO, MU = 1.0				
	(0.0)R				
0	-.9033+04				
1-S,C	.1737+03	-.4562+02	-.1531+03	-.1742+03	-.3406+02
1-S,S	.5951+03	.9263+02	-.9544+02	-.6781+02	-.2807+02
	(0.14)R				
0	-.4319+04				
1-S,C	.3734+02	-.2005+02	-.4493+02	-.5133+02	-.1458+02
1-S,S	.2950+03	.5157+01	-.3553+02	-.2925+02	-.1399+02
	(0.325)R				
0	-.1548+04				
1-S,C	-.5669+02	-.2048+01	.3063+02	.4619+02	-.1839+01
1-S,S	.1223+03	-.5666+02	.7871+01	-.6959-00	-.5746+01
	(0.55)R				
0	-.4224+03				
1-S,C	-.5414+02	.8801+01	.4325+02	.9012+02	.3463+01
1-S,S	.4412+02	-.4378+02	.2724+02	.1844+02	-.1571+01
	(0.75)R				
0	-.1033+03				
1-S,C	-.1278+02	.8188+01	.1874+02	.6057+02	.2774+01
1-S,S	.1219+02	-.9630+01	.1929+02	.1675+02	-.7774-02
	(0.85)R				
0	-.3576+02				
1-S,C	-.2032+01	.4331+01	.7225+01	.2949+02	.1382+01
1-S,S	.4068+01	.7194-00	.9492+01	.8853+01	.1247+00

N,C OR S					
	ADVANCE RATIO, MU = 1.4				
	(0.0)R				
0	-.7399+04				
1-S,C	.8068+03	.9065+02	-.2199+03	-.4104+02	-.9344+01
1-S,S	.9102+03	.1357+03	-.9349+02	.2729+03	.2343+02
	(0.14)R				
0	-.3990+04				
1-S,C	.3474+03	.5492+02	-.5403+02	-.1981+02	-.6940+01
1-S,S	.5067+03	.1249+02	-.3051+02	.5941+02	-.1003+01
	(0.325)R				
0	-.1664+04				
1-S,C	.2229+02	.3669+02	.7717+02	-.1395+01	-.1115+02
1-S,S	.2398+03	-.7957+02	.2201+02	-.1343+03	-.2698+02
	(0.55)R				
0	-.5525+03				
1-S,C	-.6190+02	.3127+02	.9359+02	.1245+02	-.2201+02
1-S,S	.8933+02	-.6183+02	.4083+02	-.2094+03	-.4009+02
	(0.75)R				
0	-.1535+03				
1-S,C	-.1950+02	.1905+02	.3874+02	.1139+02	-.1817+02
1-S,S	.2243+02	-.6811+01	.2425+02	-.1273+03	-.2585+02
	(0.85)R				
0	-.5490+02				
1-S,C	-.4376+01	.9194+01	.1463+02	.5977+01	-.9458+01
1-S,S	.6769+01	.1224+01	.1116+02	-.5959+02	-.1242+02

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

PRECONING TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(D) MP = 0.3
FP = 0.001 (FOR MU = 0.25,0.4,0.5)
FP = 0.000447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S		ADVANCE RATIO, MU = 0.25			
		(0.0)R			
0	-.3422+05				
1-5,C	.1154+03	.1399+03	.5570+02	.4140+02	.3040+02
1-5,S	.2856+03	.7265+02	.9492+02	.6228+02	.5540+02
		(0.14)R			
0	-.1467+04				
1-5,C	.1902+01	.1197+01	-.1350+01	-.2044+01	-.8836-00
1-5,S	.1462+02	.4587+01	.3068+01	.1616+01	-.8645-00
		(0.325)R			
0	.8362+02				
1-5,C	-.7547-00	-.1443+02	-.6894+01	-.5861+01	-.2782+01
1-5,S	.5628+01	.4397+01	-.5409+01	-.3794+01	-.6657+01
		(0.55)R			
0	.6463+02				
1-5,C	.9678+01	-.2135+02	-.4209+01	.2800-00	.9152-00
1-5,S	.7620+01	.6486+01	-.1151+02	-.7096+01	-.3469+01
		(0.75)R			
0	.1447+03				
1-5,C	.6937+01	-.1547+02	-.7729-00	.6053+01	.1909+01
1-5,S	.1457+01	.2468+01	-.1078+02	-.7421+01	.4243+01
		(0.85)R			
0	.1385+03				
1-5,C	.1891+01	-.7881+01	.1019+00	.5323+01	.9830-00
1-5,S	-.1595+01	-.8925-01	-.6458+01	-.4951+01	.5339+01

N,C OR S		ADVANCE RATIO, MU = 0.4			
		(0.0)R			
0	-.3441+05				
1-5,C	.1949+03	.3516+03	.8514+02	.6405+02	.4460+02
1-5,S	.5153+03	.1975+03	.2193+03	.1459+03	.1135+03
		(0.14)R			
0	-.1496+04				
1-5,C	.3626+01	.3824+01	-.1042+01	-.2675+01	.4946-00
1-5,S	.2640+02	.1088+02	.6297+01	.2899+01	-.1183+01
		(0.325)R			
0	.8242+02				
1-5,C	-.1064+01	-.3489+02	-.7101+01	-.7212+01	-.1344+01
1-5,S	.1137+02	.7526+01	-.1170+02	-.8574+01	-.1061+02
		(0.55)R			
0	.6287+02				
1-5,C	.1448+02	-.5211+02	.1452+01	.6428+01	.4671+01
1-5,S	.1574+02	.9921+01	-.1933+02	-.1259+02	-.4116+01
		(0.75)R			
0	.1492+03				
1-5,C	.8032+01	-.3608+02	.9559+01	.2005+02	.1048+02
1-5,S	.9936-00	-.1820+01	-.1419+02	-.1441+02	.3129+01
		(0.85)R			
0	.1442+03				
1-5,C	.2158-00	-.1730+02	.8289+01	.1707+02	.8692+01
1-5,S	-.5622+01	-.6221+01	-.7030+01	-.1059+02	.3602+01

N,C OR S		ADVANCE RATIO, MU = 0.5			
		(0.0)R			
0	-.3439+05				
1-5,C	.2490+03	.4370+03	.1496+03	.9611+02	.9989+02
1-5,S	.6026+03	.1485+03	.2525+03	.1517+03	.1459+03
		(0.14)R			
0	-.1495+04				
1-5,C	.7993+01	.7984+01	-.8069-01	-.2534+01	-.3835+01
1-5,S	.3117+02	.1255+02	.9783+01	.8422+01	-.2206+01
		(0.325)R			
0	.8326+02				
1-5,C	.3534+01	-.4248+02	-.1549+02	-.1146+02	-.1565+02
1-5,S	.1588+02	.2075+02	-.1258+02	-.1476+01	-.1422+02
		(0.55)R			
0	.6627+02				
1-5,C	.1968+02	-.7017+02	-.1725+02	-.2869+01	-.6510-00
1-5,S	.2120+02	.3272+02	-.2715+02	-.2270+02	-.8807+01
		(0.75)R			
0	.1540+03				
1-5,C	.1109+02	-.3996+02	-.1033+02	.7783+01	.2977+02
1-5,S	-.4557+01	.1552+02	-.1588+02	-.4784+02	-.9035+01
		(0.85)R			
0	.1477+03				
1-5,C	.1471+01	-.1262+02	-.4786+01	.7890+01	.3029+02
1-5,S	-.1407+02	.2650+01	-.4490+01	-.4049+02	-.8053+01

N,C OR S		ADVANCE RATIO, MU = 0.7			
		(0.0)R			
0	-.3088+05				
1-5,C	.3358+03	.4741+03	.1758+03	.1217+03	.1449+03
1-5,S	.6324+03	.4424+02	.1995+03	.1195+03	.1368+03
		(0.14)R			
0	-.2017+04				
1-5,C	.1484+02	.1841+02	.3628+01	-.3495+01	-.1037+02
1-5,S	.4668+02	.4633+01	.1595+02	.1398+02	-.8207-01
		(0.325)R			
0	.4965+02				
1-5,C	.3466+01	-.4666+02	-.2106+02	-.1885+02	-.3398+02
1-5,S	.1721+02	.2548+02	-.8025+01	.3717+01	-.1611+02
		(0.55)R			
0	.6479+02				
1-5,C	.2817+02	-.7631+02	-.3232+02	-.1172+02	-.2042-00
1-5,S	.2477+02	.5672+02	-.3044+02	-.3368+02	-.1773+02
		(0.75)R			
0	.1462+03				
1-5,C	.4228+01	-.4558+02	-.3083+02	-.1121+02	.4702+02
1-5,S	.6067+01	.2692+02	-.2014+02	-.7318+02	-.2634+02
		(0.85)R			
0	.1327+03				
1-5,C	-.9231+01	-.1760+02	-.1974+02	-.9227+01	.4310+02
1-5,S	-.3111+01	.4087+01	-.7149+01	-.5884+02	-.2152+02

N,C OR S		ADVANCE RATIO, MU = 1.0			
		(0.0)R			
0	-.2657+05				
1-5,C	-.2467+03	-.7213+02	-.3254+03	-.1393+03	-.1752+03
1-5,S	.4498+03	-.4331+02	-.2893+03	-.1983+03	-.2159+03
		(0.14)R			
0	-.2632+04				
1-5,C	-.4164+02	.1406+01	.4157+01	.4417+01	.1322+02
1-5,S	.3798+02	-.5152+02	-.2235+02	-.1508+02	.4565+01
		(0.325)R			
0	-.2096+02				
1-5,C	.6435+01	.2091+02	.7294+02	.4059+02	.6071+02
1-5,S	-.2574+02	-.4814+02	.2099+02	.1448+02	.4521+02
		(0.55)R			
0	.6083+02				
1-5,C	.6019+02	.1407+02	.5336+02	.9080+01	-.1459+02
1-5,S	-.2642+02	.3551+02	.6831+02	.4973+02	.1744+02
		(0.75)R			
0	.1226+03				
1-5,C	.1065+02	-.1403+02	.5033+01	-.6447+02	-.1482+03
1-5,S	.2129+02	.2828+02	.1120+03	.8547+02	-.1564+02
		(0.85)R			
0	.1025+03				
1-5,C	-.1404+02	-.1649+02	-.7010+01	-.6038+02	-.1286+03
1-5,S	.2786+02	.5524+01	.8278+02	.6398+02	-.1591+02

N,C OR S		ADVANCE RATIO, MU = 1.4			
		(0.0)R			
0	-.2272+05				
1-5,C	.2448+03	.2690+03	-.1239+03	-.6279+02	-.1540+01
1-5,S	.7673+03	.1076+03	-.4918+02	-.6645+02	.2121+02
		(0.14)R			
0	-.3308+04				
1-5,C	-.1798+02	.3702+02	.1986+02	.1740-00	-.7082-01
1-5,S	.1041+03	-.6610+02	-.4986+01	-.7584+01	-.6134+01
		(0.325)R			
0	-.1491+03				
1-5,C	-.4362+02	-.1955+02	.4676+02	.2009+02	-.5516+01
1-5,S	-.2280+02	-.4581+02	.1074+00	.7448+01	-.1515+02
		(0.55)R			
0	.4898+02				
1-5,C	.4626+02	-.3409+02	.1476+02	.3127+02	.7851+01
1-5,S	-.2270+02	.1170+03	.2487+02	.2662+02	.1348+02
		(0.75)R			
0	.9564+02				
1-5,C	.9825+01	.9337-00	.3703+02	.3590+02	.4345+02
1-5,S	.2648+02	.2648+02	.6889+02	.3997+02	.4753+02
		(0.85)R			
0	.7406+02				
1-5,C	-.1266+02	.1038+02	.3359+02	.2365+02	.3575+02
1-5,S	.2853+02	-.2273+02	.5335+02	.2753+02	.3632+02

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 9.
PRECONING TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(E) MP = 0.3
FP = 0.0025 (FOR MU = 0.25,0.4,0.5)
FP = 0.00112(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S		ADVANCE RATIO, MU = 0.25			
		(0.0)R			
0	-.2319+05				
1-S,C	.7516+02	.5163+02	.4125+02	.2472+02	.1510+02
1-S,S	.1543+03	.4422+02	.4111+02	.3602+02	.2782+02
		(0.14)R			
0	-.3333+04				
1-S,C	.1086+02	.6349+01	.3923+01	.2890+01	.2953+01
1-S,S	.2472+02	.6935+01	.5620+01	.3750+01	.2549+01
		(0.325)R			
0	-.1776+03				
1-S,C	.1593+01	-.2724+01	-.5342+0.	-.2271+01	.5872-00
1-S,S	.6987+01	.3042+01	-.3103-00	-.2778+01	-.2795+01
		(0.55)R			
0	.7830+02				
1-S,C	.3943+01	-.5894+01	-.1002+02	-.6049+01	-.4108+01
1-S,S	.5762+01	.7577+01	-.7102-00	-.2733+01	-.2307+01
		(0.75)R			
0	.7737+02				
1-S,C	.5555+01	-.6020+01	-.9917+01	-.7127+0.	-.7396+01
1-S,S	.3073+01	.9552+01	-.3476-00	-.8473-01	-.2080-00
		(0.85)R			
0	.4313+02				
1-S,C	.3736+01	-.3708+01	-.6056+01	-.4577+01	-.5176+01
1-S,S	.1388+01	.6252+01	-.3351-00	-.1452-00	.2871-0(

N,C OR S		ADVANCE RATIO, MU = 0.4			
		(0.0)R			
0	-.2331+05				
1-S,C	.1436+03	.1664+03	.7864+02	.4806+02	.3661+02
1-S,S	.2749+03	.1197+03	.1293+03	.9497+02	.6470+02
		(0.14)R			
0	-.3351+04				
1-S,C	.1952+02	.1706+02	.7161+01	.4665+01	.4402+01
1-S,S	.4513+02	.1859+02	.1572+02	.1022+02	.6991+01
		(0.325)R			
0	-.1809+03				
1-S,C	-.1874-00	-.1630+02	-.9604+01	-.5126+01	-.2064+01
1-S,S	.1489+02	.6086+01	-.6400+01	-.7587+01	-.5069+01
		(0.55)R			
0	.7795+02				
1-S,C	.2537+01	-.2633+02	-.1395+02	-.7430+01	-.3990+01
1-S,S	.1272+02	.1215+02	-.1138+02	-.1103+02	-.7280+01
		(0.75)R			
0	.7937+02				
1-S,C	.6108+01	-.2270+02	-.1098+02	-.5766+01	-.3792+01
1-S,S	.6665+01	.1443+02	-.9925+01	-.8314+01	-.5393+01
		(0.85)R			
0	.4480+02				
1-S,C	.4469+01	-.1319+02	-.6140+01	-.3203+01	-.2281+01
1-S,S	.2955+01	9318+01	-.5780+01	-.4552+01	-.2928+01

C OR S		ADVANCE RATIO, MU = 0.5			
		(0.0)R			
0	-.2331+05				
1-S,C	.1667+03	.1938+03	.1063+03	.6222+02	.5400+02
1-S,S	.2998+03	.1079+03	.1403+03	.1089+03	.7202+02
		(0.14)R			
0	-.3352+04				
1-S,C	.2367+02	.1964+02	.9188+01	.6125+01	.4477+01
1-S,S	.5017+02	.1812+02	.1660+02	.1135+02	.8054+01
		(0.325)R			
0	-.1813+03				
1-S,C	.3322+01	-.1784+02	-.1399+02	-.7083+01	-.6772+01
1-S,S	.1769+02	.1073+02	-.6488+01	-.8938+01	-.5066+01
		(0.55)R			
0	.7798+02				
1-S,C	.1107+02	-.2365+02	-.1956+02	-.1233+02	-.6903+01
1-S,S	.1297+02	.2398+02	-.6682+01	-.1083+02	-.7635+01
		(0.75)R			
0	.7982+02				
1-S,C	.1645+02	-.1607+02	-.1481+02	-.1146+02	-.2855+01
1-S,S	.4038+01	.2855+02	-.1837+01	-.6215+01	-.5906+01
		(0.85)R			
0	.4515+02				
1-S,C	.1117+02	-.8341+01	-.8142+01	-.6849+01	-.9511-00
1-S,S	.7864-00	.1843+02	-.1558-00	-.2891+01	-.3272+01

N,C OR S		ADVANCE RATIO, MU = 0.7			
		(0.0)R			
0	-.2062+05				
1-S,C	.1761+03	.1326+03	.7304+02	.5919+02	.4750+02
1-S,S	.2817+03	.7208+02	.6279+02	.6076+02	.2914+02
		(0.14)R			
0	-.3737+04				
1-S,C	.2432+02	.1990+02	.1033+02	.6037+01	.3138+01
1-S,S	.5613+02	.6892+01	.1283+02	.8794+01	.8434+01
		(0.325)R			
0	-.3106+03				
1-S,C	-.8381+01	-.7467+01	-.8155+01	-.1092+02	-.1048+02
1-S,S	.1499+02	-.5021+01	.3147+01	-.4483+01	.3556+01
		(0.55)R			
0	.5981+02				
1-S,C	.8150+01	-.1083+02	-.1890+02	-.1667+02	-.8080+01
1-S,S	.8124+01	.1940+02	-.1472+01	-.6978+01	-.1012+02
		(0.75)R			
0	.6703+02				
1-S,C	.2479+02	-.6550+01	-.1944+02	-.1324+02	-.5123-00
1-S,S	.1486+01	.3691+02	-.4579+01	-.5947+01	-.1989+02
		(0.85)R			
0	.3586+02				
1-S,C	.1781+02	-.3141+01	-.1173+02	-.7317+01	.1029+01
1-S,S	.1941-00	.2520+02	-.3271+01	-.2671+01	-.1309+02

N,C OR S		ADVANCE RATIO, MU = 1.0			
		(0.0)R			
0	-.1771+05				
1-S,C	.7441+02	-.8678+01	-.1024+03	-.1537+02	-.3553+02
1-S,S	.3124+03	.1062+03	-.3625+02	-.1471+02	-.1342+02
		(0.14)R			
0	-.4127+04				
1-S,C	-.1185+02	.2137+01	-.5861+01	-.4271+01	.3041-00
1-S,S	.7051+02	-.7896+01	-.2924+01	-.8919+01	-.3444+01
		(0.325)R			
0	-.5157+03				
1-S,C	-.4782+02	.9111+01	.3404+02	.1899+01	.1408+02
1-S,S	.5861-00	-.5145+0.	.9079+01	-.5424+01	.1018+01
		(0.55)R			
0	.2910+02				
1-S,C	-.4680+01	.9988+01	.2882+02	.1461+02	.3148+01
1-S,S	-.2013+02	.3652-00	.3751+01	.1752+02	.8097+01
		(0.75)R			
0	.6100+02				
1-S,C	.4066+02	.5481+01	.6390+01	.1880+02	-.9792+01
1-S,S	-.2121+02	.5221+02	-.4192+01	.2005+02	.1032+02
		(0.85)R			
0	.3283+02				
1-S,C	.3083+02	.2501+01	.2126-00	.1169+02	-.7745+01
1-S,S	-.1243+02	.3860+02	-.3697+01	.1943+02	.6371+01

N,C OR S		ADVANCE RATIO, MU = 1.4			
		(0.0)R			
0	-.1503+05				
1-S,C	.1240+03	.3245+02	-.2652+03	-.2222+02	-.7592+02
1-S,S	.4969+03	.1380+03	-.5735+02	-.3757+02	-.1133+02
		(0.14)R			
0	-.4449+04				
1-S,C	-.3524+02	.1220+02	-.2269+02	-.1076+02	-.1585+01
1-S,S	.1366+03	-.1836+02	-.7184+01	-.2239+02	-.1174+02
		(0.325)R			
0	-.7932+03				
1-S,C	-.1190+03	.4903+01	.9823+02	.2034+01	.3478+02
1-S,S	-.6958+01	-.8073+02	.9600+01	-.1335+02	-.8486+01
		(0.55)R			
0	-.1177+02				
1-S,C	-.3394+02	-.4020+01	.8438+02	.3933+02	.1894+02
1-S,S	-.6300+02	.3241+02	-.1300+02	.2728+02	.2102+02
		(0.75)R			
0	.7364+02				
1-S,C	.5939+02	-.8200+01	.1959+02	.4968+02	-.6868+01
1-S,S	-.5878+02	.1159+03	.2749+02	.4594+02	.3491+02
		(0.85)R			
0	.4328+02				
1-S,C	.4690+02	-.5236+01	.2033+01	.2977+02	-.7558+01
1-S,S	-.3262+02	.7781+02	-.1774+02	.2878+02	.2184+02

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 9.
PRECONING TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(F) MP = 0.3
FP = 0.01 (FOR MU = 0.25,0.4,0.5)
FP = 0.00447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S — ADVANCE RATIO, MU = 0.25

		(0.0)R			
0	-.1200+05				
1-5,C	.1132+03	.1190+02	.1677+02	.4344+01	.3392+01
1-5,S	.1252+03	.4955+02	.1059+02	.1066+02	.6675+01
		(0.14)R			
0	-.4511+04				
1-5,C	.2579+02	.5260+01	.4562+01	.1705+01	.1415+01
1-5,S	.4993+02	.1026+02	.4431+01	.3499+01	.2447+01
		(0.325)R			
0	-.1161+04				
1-5,C	-.2211+02	.3166+01	-.2619+01	.8002-00	.9036-00
1-5,S	.1737+02	-.1105+02	.1506+01	-.2239-00	.2947-00
		(0.55)R			
0	-.2049+03				
1-5,C	-.2352+02	.3097+01	-.5346+01	.1066+01	.1377+01
1-5,S	.4817+01	-.9374+01	-.6549-00	-.1530+01	-.8364-00
		(0.75)R			
0	-.2829+02				
1-5,C	-.6587+01	.2094+01	-.3745+01	.9469-00	.1202+01
1-5,S	-.2918-00	-.7428-00	-.1356+01	-.1151+01	-.8916-00
		(0.85)R			
0	-.7162+01				
1-5,C	-.1444+01	.1057+01	-.1872+01	.5185-00	.6531-00
1-5,S	-.6594-00	.7148-00	-.8319-00	-.5830-00	-.4970-00

N,C OR S — ADVANCE RATIO, MU = 0.4

		(0.0)R			
0	-.1206+05				
1-5,C	.1727+03	.2877+02	.3951+02	.1611+02	.1408+02
1-5,S	.1971+03	.1296+03	.2223+02	.2346+02	.1856+02
		(0.14)R			
0	-.4535+04				
1-5,C	.3919+02	.1311+02	.1163+02	.5386+01	.4562+01
1-5,S	.7943+02	.2958+02	.1177+02	.8669+01	.6940+01
		(0.325)R			
0	-.1172+04				
1-5,C	-.3280+02	.8862+01	-.4552+01	.5150-00	.4004-00
1-5,S	.2890+02	-.2298+02	.9252+01	.2874+01	.1675+01
		(0.55)R			
0	-.2096+03				
1-5,C	-.3136+02	.9695+01	-.1169+02	.2942-00	.9012-00
1-5,S	.8666+01	-.1855+02	.6894+01	.3496+01	.7895-01
		(0.75)R			
0	-.2946+02				
1-5,C	-.5191+01	.6881+01	-.8903+01	.8310-00	.1553+01
1-5,S	-.2802-00	.1013+01	.2812+01	.3409+01	-.1591-00
		(0.85)R			
0	-.7449+01				
1-5,C	.5516-00	.3522+01	-.4578+01	.5485-00	.9634-00
1-5,S	-.1050+01	.3144+01	.1086+01	.1918+01	-.9775-01

N,C OR S — ADVANCE RATIO, MU = 0.5

		(0.0)R			
0	-.1209+05				
1-5,C	.1921+03	.2796+02	.5723+02	.1228+02	.1342+02
1-5,S	.2089+03	.1766+03	.1273+02	.2938+02	.2402+02
		(0.14)R			
0	-.4547+04				
1-5,C	.3799+02	.1310+02	.1669+02	.4762+01	.4086+01
1-5,S	.8445+02	.3805+02	.1105+02	.9581+01	.8683+01
		(0.325)R			
0	-.1175+04				
1-5,C	-.4707+02	.9567+01	-.8547+01	.2468+01	.7332-00
1-5,S	.3008+02	-.3550+02	.1468+02	.1652+01	.1014+01
		(0.55)R			
0	-.2084+03				
1-5,C	-.4169+02	.1090+02	-.2335+02	.4114+01	.3699+01
1-5,S	.5634+01	-.2760+02	.1373+02	.4572+01	-.2455+01
		(0.75)R			
0	-.2705+02				
1-5,C	-.6335+01	.7801+01	-.1933+02	.3877+01	.4706+01
1-5,S	-.4246+01	.1610+01	-.6696+01	.5941+01	-.2493+01
		(0.85)R			
0	-.5991+01				
1-5,C	.1079+01	.3999+01	-.1022+02	.2148+01	.2767+01
1-5,S	-.3367+01	.4731+01	.2876+01	.3519+01	-.1369+01

N,C OR S — ADVANCE RATIO, MU = 0.7

		(0.0)R			
0	-.1067+05				
1-5,C	.1924+03	-.3141+02	-.8270+01	-.5296+02	-.7439+01
1-5,S	.2646+03	.2640+03	-.7550+02	.2331+01	.1655+02
		(0.14)R			
0	-.4505+04				
1-5,C	.1574+02	-.3178+01	.6822+01	-.1147+02	-.9786-00
1-5,S	.1164+03	.5328+02	-.1204+02	-.1863+01	.4868+01
		(0.325)R			
0	-.1366+04				
1-5,C	-.1002+03	.1877+02	.1134+02	.2168+02	.5261+01
1-5,S	.4307+02	-.7353+02	.3525+02	.1135+01	-.2180+01
		(0.55)R			
0	-.3007+03				
1-5,C	-.8224+02	.2549+02	-.7114+01	.4091+02	.1024+02
1-5,S	.3912+01	-.5744+02	.5008+02	.1889+02	-.3301+01
		(0.75)R			
0	-.5539+02				
1-5,C	-.1618+02	.1524+02	-.1678+02	.3016+02	.8018+01
1-5,S	-.9181+01	-.9896-00	.3024+02	.2170+02	-.1391+01
		(0.85)R			
0	-.1612+02				
1-5,C	-.8531-00	.7166+01	-.1043+02	.1532+02	.4157+01
1-5,S	-.6262+01	.6490+01	.1425+02	.1233+02	-.5197-00

N,C OR S — ADVANCE RATIO, MU = 1.0

		(0.0)R			
0	-.9260+04				
1-5,C	-.6114+02	-.2522+03	-.2774+03	-.2641+03	-.8225+02
1-5,S	.2953+03	.4607+03	-.1721+03	.4271+02	.4075+01
		(0.14)R			
0	-.4428+04				
1-5,C	-.1660+03	-.1005+03	-.7428+02	-.7783+02	-.2421+02
1-5,S	.1471+03	.1074+03	-.5333+02	-.1026+02	-.1207+02
		(0.325)R			
0	-.1578+04				
1-5,C	-.2709+03	-.1068+01	.6304+02	.7081+02	.1855+02
1-5,S	.5360+02	-.1282+03	.2900+02	-.5414+02	-.2794+02
		(0.55)R			
0	-.4015+03				
1-5,C	-.1955+03	.3040+02	.6723+02	.1396+03	.3096+02
1-5,S	-.6995+01	-.1099+03	.4458+02	-.5184+02	-.2638+02
		(0.75)R			
0	-.7588+02				
1-5,C	-.5095+02	.1781+02	.1635+02	.9469+02	.1751+02
1-5,S	-.2227+02	-.9917+01	.1999+02	-.2092+02	-.1162+02
		(0.85)R			
0	-.2040+02				
1-5,C	-.1167+02	.7891+01	.2738+01	.4627+02	.7919+01
1-5,S	-.1340+02	.6629+01	.7867+01	-.7883+01	-.4682+01

N,C OR S — ADVANCE RATIO, MU = 1.4

		(0.0)R			
0	-.8264+04				
1-5,C	-.3460+02	-.2577+03	-.3926+03	-.2190+03	-.7473+02
1-5,S	.1217+03	.7679+03	-.2519+03	.1822+03	-.6452+02
		(0.14)R			
0	-.4456+04				
1-5,C	-.2431+03	-.1070+03	-.9893+02	-.7301+02	-.1662+02
1-5,S	.8785+02	.2403+03	-.7148+02	.3198+02	-.2853+02
		(0.325)R			
0	-.1861+04				
1-5,C	-.4213+03	.1116+02	.1222+03	.6159+02	.3012+02
1-5,S	.5767+02	-.1346+03	.6475+02	-.9668+02	.2697+01
		(0.55)R			
0	-.5521+03				
1-5,C	-.2859+03	.5837+02	.1260+03	.1378+03	.3636+02
1-5,S	-.4758-00	-.1251+03	.7444+02	-.1250+03	.2315+02
		(0.75)R			
0	-.1119+03				
1-5,C	-.5961+02	.3744+02	.3339+02	.9711+02	.1580+02
1-5,S	-.2642+02	.4478+01	.2274+02	-.6440+02	.1888+02
		(0.85)R			
0	-.2977+02				
1-5,C	-.7942+01	.1751+02	.7309+01	.4780+02	.6192+01
1-5,S	-.1687+02	.1797+02	.6237+01	-.2799+02	.9620+01

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 9.
PRECONING TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(6) MP = 0.5
FP = 0.001 (FOR MU = 0.25,0.4,0.5)
FP = 0.000447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S		ADVANCE RATIO, MU = 0.25			
		(0.0)R			
0	-.3404+05				
1-S,C	-.2223+02	.5291+02	-.4893+01	-.4951-00	-.6478-00
1-S,S	.1936+03	.1727+01	-.3541+01	-.4417-00	-.5664-00
		(0.14)R			
0	-.1479+04				
1-S,C	-.3656+01	.8190-00	.6032-00	-.4252-01	.1874-01
1-S,S	.8785+01	-.1963+01	.1316-00	-.4383-01	.3719-01
		(0.325)R			
0	.8552+02				
1-S,C	.4721+01	-.5793+01	.1210+01	-.6417-01	.1622-01
1-S,S	.1440+01	-.6948-00	.5332-00	-.2483-01	.5417-01
		(0.55)R			
0	.6660+02				
1-S,C	.2285+02	-.9739+01	.7004-01	.4839-01	-.9649-01
1-S,S	.4761+01	.4402+01	.1201+01	.1350-00	-.7867-01
		(0.75)R			
0	.1394+03				
1-S,C	.1767+02	-.5709+01	-.7094-00	.4022-00	.1667-02
1-S,S	.5744+01	.9029-00	.2735+01	.3818-00	-.6651-01
		(0.85)R			
0	.1317+03				
1-S,C	.7329+01	-.1913+01	-.5686-00	.4079-00	.6254-01
1-S,S	.3962+01	-.1749+01	.2473+01	.3425-00	-.1600-01

N,C OR S		ADVANCE RATIO, MU = 0.4			
		(0.0)R			
0	-.3398+05				
1-S,C	-.1693+02	.1359+03	-.1235+02	.5050+01	.3298-00
1-S,S	.3449+03	-.3195+01	-.1252+02	-.6167+01	-.4063+01
		(0.14)R			
0	-.1476+04				
1-S,C	-.4870+01	.2776+01	.2246+01	-.2475-00	.4620-00
1-S,S	.1537+02	-.4771+01	.4621-00	.7680-00	.5580-00
		(0.325)R			
0	.8732+02				
1-S,C	.7802+01	-.1291+02	.4516+01	-.8344-00	.3338-00
1-S,S	.1901+01	-.5521-00	.2129+01	.1586+01	.1223+01
		(0.55)R			
0	.6780+02				
1-S,C	.3536+02	-.2239+02	.1148+01	.2881-00	-.6743-00
1-S,S	.8009+01	.1280+02	.4821+01	.5114-00	.1525-01
		(0.75)R			
0	.1362+03				
1-S,C	.2407+02	-.1366+02	-.2206+01	.2335+01	-.4866-00
1-S,S	.1074+02	.4110+01	.9836+01	.9355-01	-.1675+01
		(0.85)R			
0	.1279+03				
1-S,C	.7773+01	-.4905+01	-.2152+01	.2263+01	-.7189-01
1-S,S	.7763+01	-.3095+01	.8643+01	.1535-00	-.1615+01

N,C OR S		ADVANCE RATIO, MU = 0.5			
		(0.0)R			
0	-.3385+05				
1-S,C	-.3392+02	.1915+03	-.1498+02	.4958+01	.3026-00
1-S,S	.4364+03	-.4896+02	-.2044+02	-.1098+02	-.1288+02
		(0.14)R			
0	-.1496+04				
1-S,C	.5774+01	.1098+01	.1824+01	-.3121-00	.1733-00
1-S,S	.2042+02	.1682-00	-.4545-00	.5164-00	.1122+01
		(0.325)R			
0	.7452+02				
1-S,C	.1777+02	-.1788+02	.5141+01	-.8743-00	.1538-00
1-S,S	.2730+01	.6318+01	.2536+01	.2017+01	.3030+01
		(0.55)R			
0	.1008+03				
1-S,C	.2491+02	-.2340+02	.3808+01	.3231-00	-.6312-00
1-S,S	.7207+01	.1079+02	.8600+01	.1224+01	.2290-00
		(0.75)R			
0	.1090+03				
1-S,C	.2323+02	-.1988+02	-.5979-00	.2192+01	-.1624+01
1-S,S	.1060+02	.1244+02	.1420+02	-.8131-00	-.4694+01
		(0.85)R			
0	.7496+02				
1-S,C	.1523+02	-.1238+02	-.1785+01	.2073+01	-.1412+01
1-S,S	.8274+01	.8958+01	.1138+02	-.1190+01	-.4726+01

N,C OR S		ADVANCE RATIO, MU = 0.7			
		(0.0)R			
0	-.3130+05				
1-S,C	.1749+03	.9210+03	.3000+03	.3170+03	.1791+03
1-S,S	.7131+03	.2698+03	.3166+03	.2391+03	.2792+03
		(0.14)R			
0	-.2034+04				
1-S,C	-.1198+02	.1457+02	-.8431+01	-.2796+02	-.1551+02
1-S,S	.5560+02	.2084+02	.2599+02	.2731+02	.7408-00
		(0.325)R			
0	.6460+02				
1-S,C	-.1144+02	-.1234+03	-.5056+02	-.7764+02	-.3936+02
1-S,S	.3007+02	.2413+02	-.1360+02	-.5862+01	-.4477+02
		(0.55)R			
0	.6380+02				
1-S,C	.4893+02	-.1496+03	-.1467+02	.1485+02	.2309+02
1-S,S	.3825+02	.3738+02	-.4170+02	-.6971+02	-.3773+02
		(0.75)R			
0	.1422+03				
1-S,C	.2887+02	-.6101+02	.3912+02	.1264+03	.8956+02
1-S,S	-.3416+01	-.1166+02	-.2553+01	-.7980+02	.1879+02
		(0.85)R			
0	.1319+03				
1-S,C	.3354+01	-.1068+02	.3912+02	.1105+03	.7483+02
1-S,S	-.1755+02	-.2675+02	.1591+02	-.4930+02	.3057+02

N,C OR S		ADVANCE RATIO, MU = 1.0			
		(0.0)R			
0	-.2672+05				
1-S,C	.3176+03	.4568+03	.6903+02	.8593+02	.7430+02
1-S,S	.7983+03	.1079+03	.6615+02	.5404+01	.1145+03
		(0.14)R			
0	-.2643+04				
1-S,C	.1880-00	.3780+02	.1919+02	-.2712+01	-.3963+01
1-S,S	.7646+02	-.3495+02	.1281+02	.1271+02	-.3076+01
		(0.325)R			
0	-.1319+02				
1-S,C	-.1572+02	-.4041+02	.3128+01	-.1779+02	-.2407+02
1-S,S	-.2709+01	-.1560+02	-.6439-00	.1502+02	-.2512+02
		(0.55)R			
0	.5586+02				
1-S,C	.5037+02	-.6862+02	-.3300+02	-.1704+01	-.9655-00
1-S,S	.1326+02	.8732+02	-.4498+01	-.9908+01	-.1007+02
		(0.75)R			
0	.1023+03				
1-S,C	.8509+01	-.2020+02	-.2098+02	.1303+02	.4636+02
1-S,S	.3690+02	.9218+01	.3297+02	-.2262+02	.7681+01
		(0.85)R			
0	.8614+02				
1-S,C	-.1541+02	.3360+01	-.5982+01	.1075+02	.4182+02
1-S,S	.2939+02	-.3019+02	.3371+02	-.1557+02	.8025+01

N,C OR S		ADVANCE RATIO, MU = 1.4			
		(0.0)R			
0	-.2309+05				
1-S,C	.9376+02	-.7056+02	-.1538+02	-.1476+03	.7317+02
1-S,S	.3522+03	.4084+03	.2796+02	-.6055+02	.6650+02
		(0.14)R			
0	-.3354+04				
1-S,C	-.5809+02	.4362+01	.1729+02	.5171-00	-.6592+01
1-S,S	.3600+02	-.7360+02	-.3873+01	-.6394+01	-.1599+02
		(0.325)R			
0	-.1317+03				
1-S,C	-.4815+02	.2608+02	.4814+01	.4928+02	-.2969+02
1-S,S	-.3766+02	-.1096+03	-.3001+02	.1327+02	-.3087+02
		(0.55)R			
0	.6252+02				
1-S,C	.7309+02	.2554+02	-.3069+02	.3047+02	.3869+01
1-S,S	-.1063+02	.8690+02	-.1610+02	.1821+02	.1885+02
		(0.75)R			
0	.8127+02				
1-S,C	-.1190+02	.2542+02	.1430+02	-.2567+02	.4541+02
1-S,S	.6514+02	-.4150+02	.4987+02	-.3322+01	.3900+02
		(0.85)R			
0	.5868+02				
1-S,C	-.4205+02	.1693+02	.2427+02	-.2814+02	.3610+02
1-S,S	.5781+02	-.8088+02	.4717+02	-.7851+01	.2492+02

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 9.

PRECONING TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(H) MP = 0.5

FP = 0.0025 (FOR MU = 0.25,0.4,0.5)

FP = 0.00112(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S	ADVANCE RATIO, MU = 0.25				
			(0.0)R		
0	-.2311+05				
1-S,C	.1123+02	.1290+02	-.1779+01	-.3130-00	-.6282-02
1-S,S	.1072+03	.1023+02	-.2813-00	.6139-00	.4061-01
			(0.14)R		
0	-.3319+04				
1-S,C	-.1589-00	.1487+01	-.1578-01	-.3631-01	-.5784-01
1-S,S	.1568+02	-.8006-00	.7711-01	-.1130+00	-.3287-01
			(0.325)R		
0	-.1734+03				
1-S,C	-.1954+01	-.9106-00	.5279-00	.2747-01	-.9109-01
1-S,S	.1982+01	-.3781+01	.2075-00	-.3301-00	-.6663-01
			(0.55)R		
0	.8040+02				
1-S,C	.4723+01	-.1739+01	.5725-00	.6827-01	.3653-01
1-S,S	.1081+01	.3817-00	.2450-01	.6776-01	.1571-02
			(0.75)R		
0	.7680+02				
1-S,C	.1036+02	-.1674+01	.3078-00	.7785-01	.1696-00
1-S,S	.6710-00	.5262+01	-.2096-00	.5138-00	.8250-01
			(0.85)R		
0	.4227+02				
1-S,C	.7453+01	-.1012+01	.1368-00	.4956-01	.1300-00
1-S,S	.3506-00	.4182+01	-.1743-00	.4023-00	.6641-01

N,C OR S	ADVANCE RATIO, MU = 0.4				
			(0.0)R		
0	-.2309+05				
1-S,C	.2090+02	.3405+02	-.8069+01	.6923-00	.4365-00
1-S,S	.1807+03	.1435+02	-.4528+01	.6784-00	-.1941+01
			(0.14)R		
0	-.3315+04				
1-S,C	.6529-00	.4394+01	.3523-00	.2307-00	.2099-00
1-S,S	.2655+02	-.2686+01	.5220-01	-.3936-00	.5345-01
			(0.325)R		
0	-.1723+03				
1-S,C	-.1898+01	-.1433+01	.3249+01	.3060-00	.2548-00
1-S,S	.2803+01	-.7502+01	.1458+01	-.6924-00	.6257-00
			(0.55)R		
0	.8143+02				
1-S,C	.9189+01	-.3879+01	.3130+01	.3278-00	-.2187-01
1-S,S	.1292+01	.2909+01	.1245+01	.7122-00	.2900-00
			(0.75)R		
0	.7744+02				
1-S,C	.1787+02	-.4389+01	.1269+01	.1914-00	-.3353-00
1-S,S	.8862-00	.1397+02	.2921-00	.2024+01	-.2830-00
			(0.85)R		
0	.4260+02				
1-S,C	.1266+02	-.2785+01	.4136-00	.9087-01	-.2668-00
1-S,S	.4967-00	.1073+02	-.7585-02	.1498+01	-.2858-00

N,C OR S	ADVANCE RATIO, MU = 0.5				
			(0.0)R		
0	-.2307+05				
1-S,C	.3044+02	.5285+02	-.2122+02	-.1744+01	-.3048+01
1-S,S	.2375+03	.7096+01	-.1256+02	-.1262+01	-.6507+01
			(0.14)R		
0	-.3312+04				
1-S,C	.1721+01	.6809+01	.1937-00	.2349-00	.3496-00
1-S,S	.3436+02	-.5613+01	-.6297-00	-.1224+01	-.1848-00
			(0.325)R		
0	-.1705+03				
1-S,C	-.1501+01	-.2194+01	.7027+01	.1017+01	.1332+01
1-S,S	.2557+01	-.1011+02	.2589+01	-.1469+01	.1444+01
			(0.55)R		
0	.8313+02				
1-S,C	.1303+02	-.5796+01	.7121+01	.8545-00	-.5640-01
1-S,S	.7268-00	.6250+01	.2958+01	.1624+01	.8794-00
			(0.75)R		
0	.7840+02				
1-S,C	.2393+02	-.6473+01	.3291+01	.1963-00	-.1717+01
1-S,S	.8844+00	.2258+01	.1717+01	.4452+01	-.3245-00
			(0.85)R		
0	.4304+02				
1-S,C	.1681+02	-.4093+01	.1267+01	-.8409-02	-.1378+01
1-S,S	.6157+00	.1704+02	.8089-00	.3283+01	-.4352-00

N,C OR S	ADVANCE RATIO, MU = 0.7				
			(0.0)R		
0	-.2093+05				
1-S,C	.1903+03	.4454+03	.1690+03	.1731+03	.1432+03
1-S,S	.3663+03	.1827+03	.1730+03	.1747+03	.1198+03
			(0.14)R		
0	-.3793+04				
1-S,C	.2457+02	.5608+02	.2210+02	.1217+02	.5325+01
1-S,S	.8067+02	.3556+02	.3919+02	.3685+02	.2809+02
			(0.325)R		
0	-.3123+03				
1-S,C	-.1485+02	-.5841+02	-.2123+02	-.3890+02	-.3712+02
1-S,S	.3437+02	.1532+02	.1289+02	-.1110+01	.1438+01
			(0.55)R		
0	.7559+02				
1-S,C	-.3626+01	-.1014+03	-.4060+02	-.3801+02	-.1755+02
1-S,S	.1807+02	.3615+02	-.1426+02	-.5589+02	-.4989+02
			(0.75)R		
0	.8807+02				
1-S,C	.1362+02	-.8760+02	-.3756+02	-.1446+02	.1501+02
1-S,S	-.2357+01	.4311+02	-.3306+02	-.8291+02	-.7725+02
			(0.85)R		
0	.4930+02				
1-S,C	.1123+02	-.4997+02	-.2194+02	-.4504+01	.1473+02
1-S,S	-.4865+01	.2710+02	-.2306+02	-.5437+02	-.5105+02

N,C OR S	ADVANCE RATIO, MU = 1.0				
			(0.0)R		
0	-.1759+05				
1-S,C	.2594+03	.2210+03	-.1344+03	.2398+02	-.3483+02
1-S,S	.7065+03	.2716+02	-.3757+02	.3379+02	.7996+01
			(0.14)R		
0	-.4095+04				
1-S,C	.1958+02	.4468+02	-.2884+01	-.1030+01	.9375-00
1-S,S	.1563+03	-.2573+02	.2371+01	-.7185+01	.7873-00
			(0.325)R		
0	-.5020+03				
1-S,C	-.5965+02	-.1146+02	.5714+02	-.6074+01	.1674+02
1-S,S	-.2849+01	-.4066+02	.2053+02	-.2093+02	-.9295-00
			(0.55)R		
0	.4584+02				
1-S,C	.4768+01	-.2739+02	.5618+02	.1790+02	.1082+02
1-S,S	-.4090+02	.5092+02	.1251+02	.1371+02	.2648+01
			(0.75)R		
0	.7521+02				
1-S,C	.7040+02	-.2263+02	.2295+02	.3215+02	-.1264+01
1-S,S	-.3735+02	.1126+03	-.2504+01	.4049+02	.4903+01
			(0.85)R		
0	.4080+02				
1-S,C	.5143+02	-.1239+02	.8206+01	.2101+02	-.2627+01
1-S,S	-.2097+02	.7536+02	-.3808+01	.2783+02	.3219+01

N,C OR S	ADVANCE RATIO, MU = 1.4				
			(0.0)R		
0	-.1419+05				
1-S,C	.1005+04	.9787+03	-.3530+03	.2002+02	-.8120+02
1-S,S	.2127+04	-.4881+03	-.3033+03	-.3812+02	.7419+02
			(0.14)R		
0	-.4206+04				
1-S,C	.1647+03	.2380+03	.6284+01	-.1463+02	-.5807+01
1-S,S	.5718+03	-.1363+03	-.4913+02	-.5113+02	.7985-00
			(0.325)R		
0	-.7542+03				
1-S,C	-.1851+03	-.6294+02	.2216+03	.7417+01	.4714+02
1-S,S	-.2098+02	.6524+02	.8555+02	-.4562+02	-.3000+02
			(0.55)R		
0	-.5884+01				
1-S,C	-.8749+02	-.1192+03	.2365+03	.1566+03	.8570+02
1-S,S	-.1510+03	.3051+03	.1393+03	.8313+02	.1962+01
			(0.75)R		
0	.8078+02				
1-S,C	.7732+02	-.6810+02	.1148+03	.2023+03	.7117+02
1-S,S	-.1015+03	.3316+03	.1017+03	.1471+03	.3856+02
			(0.85)R		
0	.4812+02				
1-S,C	.6764+02	-.3111+02	.4843+02	.1219+03	.3856+02
1-S,S	-.4958+02	.1926+03	.5263+02	.9277+02	.2146+02

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS

TABLE 9.
PRECONING TRANSFER COEFFICIENTS FOR A HINGELESS BLADE

(I) MP = 0.5
FP = 0.01 (FOR MU = 0.25,0.4,0.5)
FP = 0.00447(1+MU)**2 (FOR MU = 0.7,1.0,1.4)

N,C OR S	ADVANCE RATIO, MU = 0.25				
			(0.0)R		
0	-.1199+05				
1-S,C	.1089+03	-.2783+02	-.2204+01	-.9638+01	-.9209+01
1-S,S	.1186+03	.5728+02	-.2564+01	-.2213+01	-.2101+01
			(0.14)R		
0	-.4506+04				
1-S,C	.8008+01	-.1107+02	-.5580+01	-.6129+01	-.5467+01
1-S,S	.4520+02	.5719+01	-.2298+01	-.2854+01	-.2396+01
			(0.325)R		
0	-.1157+04				
1-S,C	-.5422+02	-.2895+01	-.1077+02	-.6207+01	-.4955+01
1-S,S	.1131+02	-.2381+02	-.3481+01	-.4163+01	-.3569+01
			(0.55)R		
0	-.2016+03				
1-S,C	-.4708+02	.2353+01	-.1161+02	-.5167+01	-.3582+01
1-S,S	-.2335+01	-.1608+02	-.4290+01	-.2940+01	-.3192+01
			(0.75)R		
0	-.2665+02				
1-S,C	-.1206+02	.3553+01	-.6426+01	-.2274+01	-.1229+01
1-S,S	-.4954+01	.8354-00	-.2833+01	-.6559-00	-.1398+01
			(0.85)R		
0	-.6444+01				
1-S,C	-.2253+01	.2101+01	-.2943+01	-.9197-00	-.4030-00
1-S,S	-.2958+01	.2636+01	-.1403+01	-.8422-01	-.5589-00

N,C OR S	ADVANCE RATIO, MU = 0.4				
			(0.0)R		
0	-.1203+05				
1-S,C	.1650+03	-.4672+02	.2340+02	-.1709+01	-.1179+01
1-S,S	.1513+03	.1405+03	-.9425+01	-.6232+01	-.1677+01
			(0.14)R		
0	-.4522+04				
1-S,C	.1756+02	-.8971+01	.5296+01	-.2848-00	-.5234-00
1-S,S	.5809+02	.1875+02	-.2415-00	-.2308+01	-.3571-00
			(0.325)R		
0	-.1167+04				
1-S,C	-.6973+02	.1540+02	-.7779+01	.5380-00	.1934-00
1-S,S	.1375+02	-.4950+02	.4323+01	.1216+01	.4703-00
			(0.55)R		
0	-.2049+03				
1-S,C	-.5701+02	.2324+02	-.1656+02	.5034-00	.1589+01
1-S,S	-.7840+01	-.3389+02	.8438-01	.6451+01	.7325-00
			(0.75)R		
0	-.2510+02				
1-S,C	-.9860+01	.1470+02	-.1335+02	.1311-00	.1745+01
1-S,S	-.1178+02	.2317+01	-.3580+01	.6691+01	.4638-00
			(0.85)R		
0	-.5023+01				
1-S,C	.5487-00	.7088+01	-.7027+01	.2490-01	.9920-00
1-S,S	-.6894+01	.5955+01	-.2464+01	.3757+01	.2235-00

N,C OR S	ADVANCE RATIO, MU = 0.5				
			(0.0)R		
0	-.1224+05				
1-S,C	.1953+03	.1059+02	.9682+02	.4572+02	.3910+02
1-S,S	.1807+03	.2599+03	.3721+02	.4757+02	.4415+02
			(0.14)R		
0	-.4606+04				
1-S,C	.1805+02	.7251+01	.2463+02	.1011+02	.7680+01
1-S,S	.7320+02	.5686+02	.2108+02	.1467+02	.1421+02
			(0.325)R		
0	-.1196+04				
1-S,C	-.8490+02	.8079+01	-.2261+02	-.1170+02	-.1103+02
1-S,S	.2402+02	-.4614+02	.1791+02	.1498+01	-.1542+01
			(0.55)R		
0	-.2115+03				
1-S,C	-.6014+02	.7352+01	-.4878+02	-.1797+02	-.1355+02
1-S,S	-.3437+01	-.2296+02	.1249+02	.7913+01	-.6984+01
			(0.75)R		
0	-.2361+02				
1-S,C	-.9187-00	.3625+01	-.3809+02	-.1101+02	-.6430+01
1-S,S	-.1239+02	.1958+02	.4095+01	.1111+02	-.5105+01
			(0.85)R		
0	-.3409+01				
1-S,C	.7075+01	.1571+01	-.1982+02	-.5231+01	-.2659+01
1-S,S	-.7829+01	.1648+02	.1281+01	.6653+01	-.2566+01

N,C OR S	ADVANCE RATIO, MU = 0.7				
			(0.0)R		
0	-.1088+05				
1-S,C	.2302+03	-.7337+02	.7080+02	-.5106+01	.3450+02
1-S,S	.1733+03	.4159+03	-.4563+02	.4033+02	.5569+02
			(0.14)R		
0	-.4604+04				
1-S,C	.5468+01	-.4883+01	.3657+02	.5465+01	.1448+02
1-S,S	.8157+02	.9724+02	.9457+01	.2282+02	.2028+02
			(0.325)R		
0	-.1411+04				
1-S,C	-.1362+03	.4669+02	.1128+02	.2115+02	.4388+01
1-S,S	.3050+02	-.8155+02	.5776+02	.9946+01	.2346+01
			(0.55)R		
0	-.3164+03				
1-S,C	-.8315+02	.5576+02	-.2706+02	.3636+02	.1315+01
1-S,S	-.1181+02	-.4044+02	.6913+02	.4179+02	.2235+01
			(0.75)R		
0	-.5617+02				
1-S,C	.9974+01	.2916+02	-.3553+02	.2804+02	.6119-00
1-S,S	-.2461+02	.3390+02	.3898+02	.4499+02	.4394+01
			(0.85)R		
0	-.1508+02				
1-S,C	.1685+02	.1266+02	-.2054+02	.1450+02	.3019-00
1-S,S	-.1487+02	.2810+02	.1790+02	.2529+02	.2760+01

N,C OR S	ADVANCE RATIO, MU = 1.0				
			(0.0)R		
0	-.9619+04				
1-S,C	-.4417+01	-.4220+03	-.2311+03	-.2479+03	-.8446+02
1-S,S	-.6331+01	.7126+03	-.1410+03	.1028+03	.5838+02
			(0.14)R		
0	-.4604+04				
1-S,C	-.1913+03	-.1520+03	-.5111+02	-.7270+02	-.1787+02
1-S,S	.2400+01	.1802+03	-.2325+02	.1032+02	.3228+01
			(0.325)R		
0	-.1640+04				
1-S,C	-.3470+03	.3345+02	.6857+02	.7195+02	.3278+02
1-S,S	-.9798+01	-.1630+03	.5723+02	-.5265+02	-.3043+02
			(0.55)R		
0	-.3947+03				
1-S,C	-.2173+03	.8871+02	.5549+02	.1484+03	.4314+02
1-S,S	-.5955+02	-.1201+03	.4602+02	-.3685+02	-.2463+02
			(0.75)R		
0	-.5287+02				
1-S,C	-.2245+02	.5001+02	.2612+01	.1051+03	.2198+02
1-S,S	-.6194+02	.1855+02	.5448+01	-.6312-00	-.4789+01
			(0.85)R		
0	-.6595+01				
1-S,C	.9687+01	.2227+02	-.4924+01	.5218+02	.9493+01
1-S,S	-.3415+02	.2698+02	-.1833+01	.3912+01	-.2972-00

N,C OR S	ADVANCE RATIO, MU = 1.4				
			(0.0)R		
0	-.9244+04				
1-S,C	-.5459+03	-.9206+03	-.4563+03	-.2216+03	-.2928+03
1-S,S	-.9842+03	.1165+04	-.1531+03	-.5800+02	-.2494+03
			(0.14)R		
0	-.4958+04				
1-S,C	-.5625+03	-.4351+03	-.1671+03	-.1025+03	-.7882+02
1-S,S	-.5125+03	.3292+03	-.3537+02	-.4086+02	-.9763+02
			(0.325)R		
0	-.2008+04				
1-S,C	-.5971+03	-.8952+02	.1391+02	-.5915+01	.9452+02
1-S,S	-.2197+03	-.2732+03	.3568+02	-.5625+01	.4595+02
			(0.55)R		
0	-.4972+03				
1-S,C	-.3069+03	.3300+02	-.2961+02	.4997+02	.1271+03
1-S,S	-.1506+03	-.2475+03	-.8000+01	.7000+02	.1472+03
			(0.75)R		
0	-.3743+02				
1-S,C	-.1486+02	.1954+02	-.7677+02	.4147+02	.9834+02
1-S,S	-.1081+03	-.1459+02	-.4265+02	.7614+02	.1147+03
			(0.85)R		
0	.1070+02				
1-S,C	.2239+02	.7280+01	-.4763+02	.2111+02	.2426+02
1-S,S	-.5599+02	.1960+02	-.2717+02	.4182+02	.5816+02

NOTE- DIVIDE LISTED VALUES BY 100,000 TO OBTAIN TRANSFER COEFFICIENTS