

N 70 27068

NASA CR 86371

FINAL REPORT

PROJECT A-1167

RESEARCH IN PRECISION INTEGRATION METHODS

L. J. GALLAHER AND I. E. PERLIN

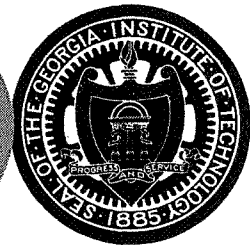
GRANT NUMBER NGR 11-002-101

1 APRIL 1969 to 31 MARCH 1970

Supported by the
NATIONAL AERONAUTICS AND SPACE ADMINISTRATION
WASHINGTON, D. C.

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Engineering Experiment Station
GEORGIA INSTITUTE OF TECHNOLOGY
Atlanta, Georgia

GEORGIA INSTITUTE OF TECHNOLOGY
Rich Electronic Computer Center
Atlanta, Georgia

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ABSTRACT

This report contains the results of comparisons and computer tests of several methods for numerically integrating systems of coupled non-linear differential equations (initial value problems). The methods tested are:

- 1) Shanks' formulas for the method of Runge and Kutta.
- 2) The Adams, Bashforth, and Moulton method.
- 3) Butcher's formulas for the method of Stetter and Gragg.
- 4) Cowell's method.

Each of these methods was programmed as a general purpose subroutine in double precision FORTRAN V for the UNIVAC 1108. The test problem on which results are given here is that of a particle in an inverse square attractive force field with an elliptic orbit of eccentricity 0.8. Single orbits were run for orders from 7 through 13 and accuracies in the range 10^{-7} to 10^{-12} . Plots are given of error versus time and versus number of function evaluations for the various methods and orders.

The results show that all of the methods perform well but the higher orders of each method are significantly faster at the higher accuracies. At corresponding orders the Butcher formulas appear to be superior.

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I. INTRODUCTION

This report gives the results of tests and comparisons for a collection of methods for numerically integrating systems of coupled non-linear differential equations.

The methods tested are :

- 1) Shanks' formulas for the method of Runge and Kutta .
- 2) The Adams, Bashforth and Moulton method .
- 3) Butcher's formulas for the method of Stetter and Gragg .
- 4) Cowell's method.

For each of these methods, general purpose subroutines were written that would handle up to 99 equations. Each method has automatic error and step size control. The multi-step methods use the Shanks subroutine for starting and for restarting to reduce step size.

Each of the methods is programmed in double precision FORTRAN V for the UNIVAC 1108.

Several test problems were used to exercise the methods. The results reported here are for an orbit of a particle in an inverse square attractive force field, with an elliptic orbit of eccentricity 0.8. Tests were run for various orders from 7 through 13 on the different methods, and plots are given of error versus the time and versus the number of function evaluations.

The results show that, while all of the methods perform well, the higher order methods are significantly faster at the higher accuracies. At corresponding orders and accuracies the Butcher formulas appear to be faster. There is a suggestion that if higher order Shanks formulas were available these would be effective at the higher accuracies.

Chapter II contains separate descriptions of each of the four integration methods together with details on the error and step size control, subroutine parameters and flow diagrams. The programs themselves are listed in Appendix A.

The coefficients for a wide range of orders for each method are listed in Appendix B.

II. INTEGRATION METHODS

A. Introduction

The four integration methods described in this chapter are as follows:

- 1) Shanks' formulas for the Runge-Kutta method.
- 2) The Adams, Bashforth and Moulton method.
- 3) Butcher's formulas for the Stetter-Gragg method.
- 4) Cowell's method.

Each of these methods is programmed in double precision (~18 decimal significant figures) in the FORTRAN V language for the UNIVAC 1108. They are written as general purpose subroutines that can handle up to 99 simultaneous ordinary differential equations. The methods are of variable order; that is, the order is specified by the user. The coefficients of the method and order to be used are supplied by the user and passed to each subroutine at the time called. Sets of these coefficients are listed in Appendix B. In practice these coefficients are read in from a machine language tape (in double precision) by the calling program.

Each of the subroutines references the external subroutine FUNCTI to obtain the derivatives for the equations being integrated. FUNCTI is of course written by the user to describe the particular problem.

A point to note is that the information about the dependent variable Y and its derivatives that is passed to and from FUNCTI, and to and from each of the subroutines, is contained in array positions 2 through $N + 1$ where N is the number of equations being integrated. The first positions in the Y vector and its derivative vector are not used by these programs.

The step size control in each method uses a parameter to indicate the expected manner that the errors accumulate and propagate. Set at 1.0 this parameter indicates that the errors are expected to be additive and all of the same sign. Setting this parameter to 0.5 indicates that the errors are expected to be random. With this parameter the subroutine tries at each step to project ahead and estimate the final error at the end of the integration and adjust the step size and error at each step accordingly.

In order to conserve storage, all the multi-step methods use some common storage allocated by the main program with the statement,

```
COMMON/COMMON/FA(35, NPI)
```

where NPI is a parameter. NPI is set to one more than the number of equations to be integrated but not greater than 100. The starting subroutine does not reference this common area.

The multistep methods all use a special Runge-Kutta-Shanks starting subroutine for getting started and for reducing step size. They also use the regular Runge-Kutta-Shanks subroutine for ending if the final step is smaller than the current step at ending. Thus, while the Runge-Kutta-Shanks subroutine could be used by itself, the others would need both the starting subroutine and the regular Runge-Kutta-Shanks in order to run.

The subroutines themselves are listed in Appendix A, together with a skeleton main program and FUNCTI subroutine.

B. The Runge-Kutta-Shanks Method

1. Introduction

The procedure described is a generalization of the Runge-Kutta method for solving a system of differential equations. It may be applied to an arbitrary system of first-order differential equations of the form

$$\vec{y}' = f(x, \vec{y})$$

with the initial conditions

$$\vec{y}(x_0) = \vec{y}_0$$

where $\vec{y}(x) = \begin{pmatrix} y_1(x) \\ \vdots \\ y_n(x) \end{pmatrix}$, $\vec{y}'(x) = \begin{pmatrix} y_1'(x) \\ \vdots \\ y_n'(x) \end{pmatrix}$,

$$\vec{f}(x, \vec{y}) = \begin{pmatrix} f_1(x, y_1, \dots, y_n) \\ \vdots \\ f_n(x, y_1, \dots, y_n) \end{pmatrix}, \quad \vec{y}_0 = \begin{pmatrix} y_{10} \\ \vdots \\ y_{n0} \end{pmatrix}.$$

2. Description of the Method

The Shanks Method is a single-step procedure for finding a numerical solution of a first-order ordinary differential equation or system of differential equations in which the derivatives of the dependent variables may be expressed explicitly as functions of the independent and dependent variables.

Consider the system of differential equation

$$\vec{y}' = \vec{f}(x, \vec{y}) .$$

Suppose the value of $\vec{y}(x)$ is known. The value $\vec{y}(x+h)$ is approximated by

$$\vec{y}(x+h) = \vec{y}(x) + h \sum_{i=1}^m \gamma_i \vec{f}_i(x, h, \vec{y}),$$

where

$$\vec{f}_1(x, h, \vec{y}) = \vec{f}(x, \vec{y}),$$

$$\vec{f}_i(x, h, \vec{y}) = \vec{f}\left(x + \alpha_i h, \vec{y} + h \sum_{j=1}^{i-1} \beta_{ij} \vec{f}_j\right), \quad i = 2, \dots, m.$$

The coefficients α_i ($i = 2, \dots, m$),

$$\beta_{ij} \quad (i = 2, \dots, m; j = 1, \dots, i-1), \text{ and } \gamma_i \quad (i = 1, \dots, m)$$

are chosen so as to make the approximation correct to some order. A special case of the Shanks formula is the fourth-order Runge-Kutta formula:

$$\alpha_2 = 1/2, \quad \alpha_3 = 1/2, \quad \alpha_4 = 1,$$

$$\beta_{21} = 1/2, \quad \beta_{31} = 0, \quad \beta_{32} = 1/2, \quad \beta_{41} = \beta_{42} = 0, \quad \beta_{43} = 1,$$

$$\gamma_1 = 1/6, \quad \gamma_2 = 1/3, \quad \gamma_3 = 1/3, \quad \gamma_4 = 1/6$$

For useful values of the various combinations of α , β , and γ , see Shanks [18].

3. The Computer Program

The subroutine was programmed for the UNIVAC 1108 computer in the FORTRAN V language. Double precision arithmetic (18 decimal digits) was used throughout except where integers are indicated.

3.1 Error Estimates and Step Size Control

In this subroutine a single set of Shanks formulas is used. Suppose

a vector $\vec{y}(x)$ is known. Then the Shanks method is applied to one step of size h (where $h = \frac{\Delta x}{c}$, Δx is the length of the interval, and c is a power of two), and to two steps of size $\frac{h}{2}$, as follows:

$$\vec{y}_p = \vec{y}(x) + h \sum_{i=1}^m \gamma_i \vec{f}_i(x, h, \vec{y}),$$

$$\vec{y}_m = \vec{y}(x) + \frac{h}{2} \sum_{i=1}^m \gamma_i \vec{f}_i(x, \frac{h}{2}, \vec{y})$$

$$\vec{y}_c = \vec{y}_m + \frac{h}{2} \sum_{i=1}^m \gamma_i \vec{f}_i(x + \frac{h}{2}, \frac{h}{2}, \vec{y}_m).$$

Both \vec{y}_p and \vec{y}_c are estimates of $\vec{y}(x+h)$. An error estimate $E_k = \frac{|y_{ck} - y_{pk}|}{f}$

(where f is an empirical factor) is calculated for each independent variable

y_k . If both $E_k > \frac{E_{ak}}{c^p}$ and $E_k > \frac{E_{rk}|y_{ck}|}{c^p}$ for any dependent variable

where E_{ak} is an absolute error estimate, E_{rk} is a relative error estimate,

and p is an input parameter, usually 1 or 1/2, then the step is rejected

and the step size is halved; otherwise the step is accepted and y_c is taken

as the vector $\vec{y}(x+h)$. If for every dependent variable, either $E_k > \frac{E_{ak}}{2^{(j+3)}c^p}$

or $E_k > \frac{E_{rk}|y_{ck}|}{2^{(j+3)}c^p}$, where j is the order, then the step size is doubled. If

the step size h is larger than the distance to the end of the interval, then that distance is taken as the step size.

3.2 Input and Output of the Subroutine

The subroutine is called as follows:

```
CALL SHANKS (N,XIV,XF,YV,IM,ORDER,CF,P,EA,ER,DXV)
```

where the parameters have the following meaning:

- N - number of dependent variables (integer);
- XIV - initial value of the independent variable;
- XF - final value of the independent variable;
- YV - array of initial values of the dependent variables;
- IM - the number of function evaluations in each application of the Shanks method (integer);
- ORDER - the order of the Shanks formulas used (integer);
- CF - the array of Shanks coefficients, starting in the first element arranged as follows: for each i, the corresponding $\alpha_i \beta_{ij}$'s, followed by α_i , with the γ_i 's at the end;
- P - an exponent (usually 1/2 or 1) used in step size control (1 assuming the errors are additive; 1/2 assuming that they are random);
- EA - an array of absolute error asked;
- ER - an array of relative error asked;
- DXV - a recommended starting step size (the actual starting step size will be $\frac{XF - XIV}{c}$, where c is the smallest power of 2 for which $\left| \frac{XF - XIV}{c} \right| \leq |DX|$).

The final values of the dependent variable are stored in YV before exiting the procedure.

All variables and arrays not designated integer are double precision.

3.3 Flow Diagram and Program Listing.

Figure 1 is the flow diagram for the Runge-Kutta-Shanks procedure.

A listing of the program is given in Appendix A.

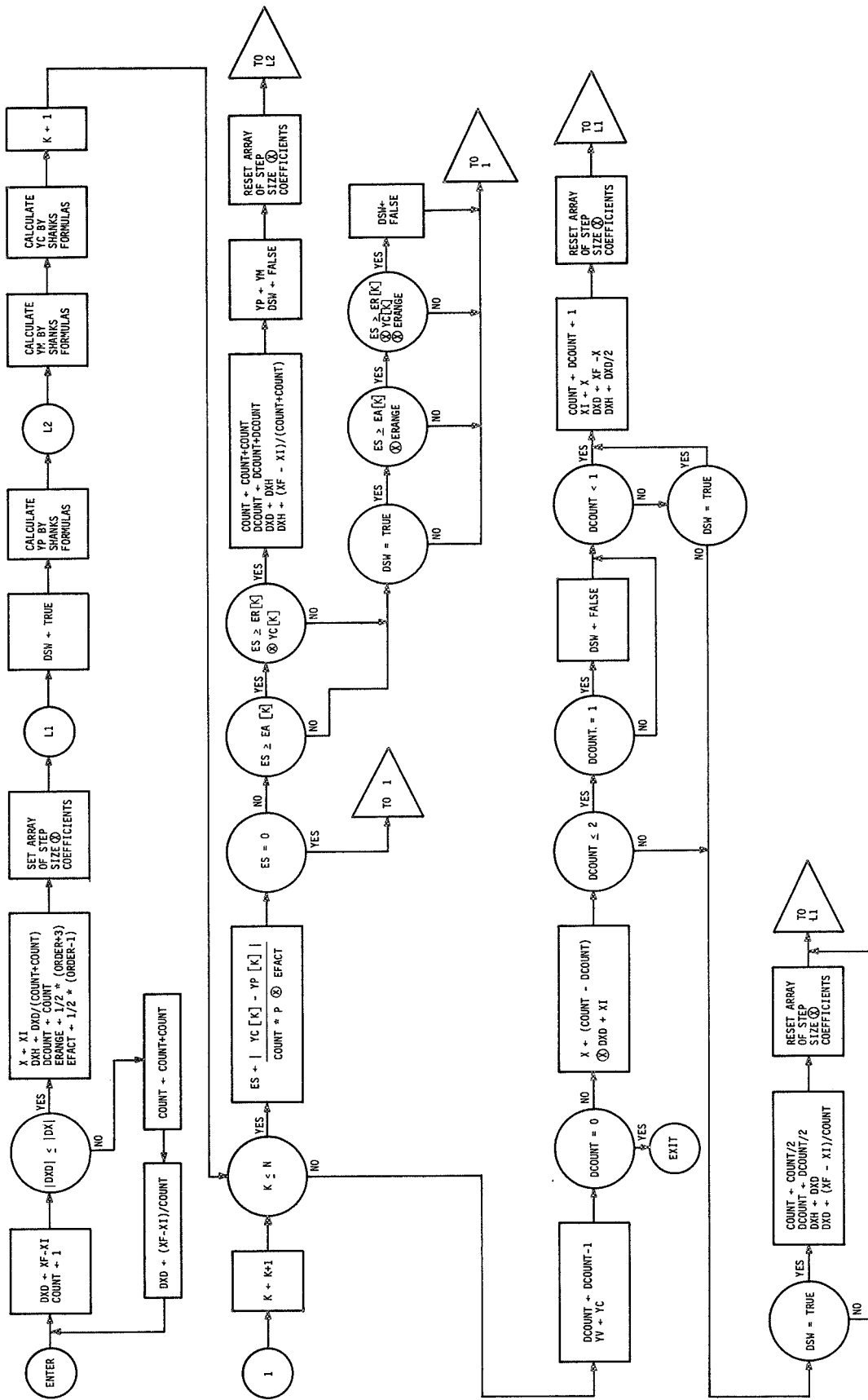


Figure 1. Flow Diagram for the Runge-Kutta-Shanks Procedure.

C. The Methods of Adams, Bashforth and Moulton

1. Description of the Method

The method investigated consists of the combination of two different versions of the method of Adams into a predictor-corrector system [5]. The use of this system to obtain numerical solutions to a set of simultaneous differential equations with given initial conditions is independent both of the number of equations in the set to be solved and of the orders of the individual equations in the set; provided, however, that each equation of order m is expressed as a set of m coupled first order equations.

In general then, one deals with the system of equations

$$\vec{y}'(x) \equiv \frac{d}{dx} \vec{y}(x) = \vec{f}(x, \vec{y}(x)), \quad (1-1)$$

where \vec{y}' , \vec{y} , and \vec{f} are vectors, each having a number of components, N , equal to $\sum_{i=1}^k m_i$, where k is the number of equations in the set to be solved, and the m_i are their individual orders.

This vector differential equation is equivalent to the integral equation

$$\vec{y}(x+h) = \vec{y}(x) + \int_x^{x+h} \vec{f}(t, \vec{y}(t)) dt. \quad (1-2)$$

At the point $x = x_q \equiv x_{q-1} + h$, this integral is approximated first by

$$\vec{y}_q(0) = \vec{y}_{q-1} + h \sum_{\mu=0}^{q-1} \beta_{q-1, q-1-\mu} \vec{f}_\mu \quad (1-3a)$$

and then repeatedly by

$$\begin{aligned} \vec{y}_q^{(\nu+1)} &= h\beta_{q,0}^* \vec{f}\left(x_q, \vec{y}^{(\nu)}(x_q)\right) + h \sum_{\mu=0}^{q-1} \beta_{q,q-\mu}^* \vec{f}_\mu + \vec{y}_{q-1} \\ &\equiv h\beta_{q,0}^* \vec{f}^{(\nu)} + \vec{C}, \quad \nu = 0, 1, 2, \dots \quad (1-3b) \end{aligned}$$

which converges toward $\vec{y}_q \equiv \vec{y}(x_q)$ as ν increases. Formula (1-3a) is called the Adams-Bashforth predictor equation, and formula (1-3b) is the Adams-Moulton corrector.

The coefficients $\beta_{q\rho}$ and $\beta_{q\rho}^*$ are derived by the equivalent of integrating Lagrangian polynomials fitted to \vec{f} , but are independent of both \vec{f} and h . The polynomial for the predictor is of degree $q-1$ passing through the q points $\vec{f}_0, \vec{f}_1, \dots, \vec{f}_{q-1}$, while that for the corrector is of degree q passing through the $q+1$ points $\vec{f}_0, \vec{f}_1, \dots, \vec{f}_q$.

An explicit formula for the $\beta_{q\rho}$ is

$$\beta_{q\rho} = (-1)^\rho \left\{ \binom{\rho}{\rho} \gamma_\rho + \binom{\rho+1}{\rho} \gamma_{\rho+1} + \dots + \binom{q}{\rho} \gamma_q \right\}, \quad \rho = 0, 1, 2, \dots, q$$

where the $\binom{\rho+i}{\rho}$ represent binomial coefficients and the γ_ρ are found by the recursion relation

$$\gamma_\rho + \frac{1}{2} \gamma_{\rho-1} + \dots + \frac{1}{\rho+1} \gamma_0 = 1, \quad \rho = 0, 1, 2, \dots,$$

and an explicit formula for the $\beta_{q\rho}^*$ is

$$\beta_{q\rho}^* = (-1)^\rho \left\{ \binom{\rho}{\rho} \gamma_\rho^* + \binom{\rho+1}{\rho} \gamma_{\rho+1}^* + \dots + \binom{q}{\rho} \gamma_q^* \right\}, \quad \rho = 0, 1, 2, \dots, q$$

where $\gamma_0^* = 1$ and $\gamma_\rho^* = \gamma_\rho - \gamma_{\rho-1}$, $\rho = 1, 2, 3, \dots$

Bounds on the errors for the two approximations are the maximums within the interval $[x_0, x_q]$ of

$$\left| \gamma_q h^{q+1} \frac{d^{q+1}}{dx} \vec{y} \right| \quad (\text{for Adams-Bashforth}) \quad (1-4a)$$

and of

$$\left| \gamma_{q+1}^* h^{q+2} \frac{d^{q+2}}{dx} \vec{y} \right| \quad (\text{for Adams-Moulton}) \quad (1-4b)$$

and M , the order of the predictor-corrector system, is assumed to approximate that of the corrector, which is $q + 1$.

2. The Computer Program

The subroutine ADAMS itself is written to be included in programs written in double precision for the UNIVAC 1108 computer. The language is FORTRAN V. There are no unusual hardware requirements, because all input and output to the procedure is under control of the including program through the formal parameter list.

2.1 Parameters

The following lists of formal parameters will be useful in describing the operation of procedure ADAMS. In the remainder of this discussion the interchange of upper and lower case letters, necessitated by approximating the notation [5] within the limited character set available to a computer, is straight-forward and will be done freely without further comment. Except for those variables designated integer, all variables are double precision. All arrays are double precision.

Formal Parameters

<u>Identifier</u>	<u>Type</u>	<u>Usage or Meaning</u>
N	Integer	The number of equations to be integrated.
XI	Double	Initial value of the independent variable.
XF	Double	Final value of the independent variable.
Y	Array	Current dependent variable vector. Contains initial values at entry and final values at exit.
P	Double	Power of C1 used in error control.
Q	Integer	Number of back \vec{f} points used in the approximating polynomials. One less than M, the order of the method.
DXV	Double	Upper bound on the initial step size.
EA	Array	Absolute error bound vector.
ER	Array	Relative error bound vector.
ADMSCF	Array	Contains the $\beta_{q\rho}$, the $\beta_{q\rho}^*$, and $1 - \gamma_{q+1}/\gamma_{q+1}^*$.
RKSFNS	Integer	Function evaluations per step for procedures START and SHANKS.
RXSRDR	Integer	Order of R.K.S. method to be used by START and SHANKS.
RKSCFF	Array	Coefficients for START and SHANKS. See the descriptions of START and SHANKS elsewhere in this report for details.

2.2 The FUNCTI Subroutine

A subroutine for calculating the vector $\vec{y}' = \vec{f}(x, \vec{y}(x))$ must be an external subroutine characterizing the set of differential equations to be solved by a program using ADAMS. This subroutine is called by ADAMS as FUNCTI and must itself have the following formal parameter list:

<u>Identifier</u>	<u>Type</u>	<u>Usage or Meaning</u>
N	Integer	Number of equations.
X	Double	Current value of the independent variable.
YV	Array	Current dependent variable vector (input).
FV	Array	f value vector (output).

2.3 Orders Available

The subroutine ADAMS is written to be completely general with regard to order, and any order may be used if the necessary coefficients are placed in the ADMSCF array. For a given order $M = q + 1$, there are $2q + 2 = 2M$ coefficients which should appear in the array beginning at position one in the following order:

$$\beta_{q-1,q-1}, \beta_{q-1,q-2}, \dots, \beta_{q-1,0}, \beta_{q,q}^*, \beta_{q,q-1}^*, \dots, \beta_{q,0}^*, \left| 1-\gamma_{q+1} / \gamma_{q+1}^* \right| .$$

2.4 Starting, Error Estimates and Step Size Control

Since the Adams methods is a multistep method it cannot start itself but must rely on a starting procedure that will supply at least $q-1$ \vec{f} points which, together with a given initial \vec{f} point and a current \vec{y} point, comprise a history upon which it can build. The starting procedure used here is the Runge-Kutta-Shanks procedure START, described elsewhere in this report. The number of function evaluations per step and the order of Runge-Kutta-Shanks method used by START may be varied at will by the user through the formal parameters of ADAMS. This will achieve optimum compatibility with the order of Adams method being used for each given set of differential equations being solved.

Initial step size is determined by the formal parameter DX. The initial trial start will be made with a step $H = \text{INTERVAL} / C1$, where C1 is set to the smallest integer power of two, such that $|H| \leq |DX|$ and $|H| \leq |\text{INTERVAL}|/Q$. This causes the procedure ADAMS to take at least one step after starting regardless of the magnitude of DX. If the procedure START cannot meet the error requirements at the initial H, it doubles C1 repeatedly until these requirements can be met.

To minimize running time without introducing errors intolerably large, the error in each component of the final \vec{Y} vector is controlled through the use of the formal parameters \vec{EA} and \vec{ER} . \vec{EA} specifies the maximum allowable absolute magnitude of the error in each component of \vec{Y} , and \vec{ER} specifies the maximum allowable relative magnitude. These two error control vectors are used in conjunction with the quantity $GR = |1 - \gamma_q / \gamma_{q+1}^*|$, which is derived from the bounds (1-4), and a parameter P, chosen from the interval $[\frac{1}{2}, 1]$ by empirical determination of the randomness of the round-off error in a particular set of differential equations. ($P = \frac{1}{2}$ corresponds to totally random error and $P = 1$ corresponds to totally additive error.) In practice γ_{q+1} has been used in GR instead of γ_q to be conservative, because the quantity being controlled is only an estimate of the true error.

The estimated error vector \vec{ERROR} is defined to be $|\vec{y}^{(c)} - \vec{y}^{(p)}|$, where $\vec{y}^{(p)}$ is the $\vec{y}_q(o)$ of (1-3a) and $\vec{y}^{(c)}$ is $\vec{y}_q^{(v_f+1)}$ in (1-3b), with v_f being the first v for which every component of

$$\vec{CHANGE} \equiv |\vec{f}_q^{(v+1)} - \vec{f}_q^{(v)}| = \left| \left(\vec{y}_q^{(v+1)} - \vec{y}_q^{(v)} \right) / h\beta_{q,o}^* \right|$$

is less than the corresponding component of either

$$\left| \frac{\vec{EA} \cdot GR}{Cl^P \cdot 2^{Q+5} \cdot h\beta_{q,o}} \right| \text{ or } \left| \frac{\vec{ER} \cdot GR}{Cl^P \cdot 2^{Q+5} \cdot h\beta_{q,o}^*} \cdot \vec{f}_q^{(v+1)} \right|$$

If any component of \vec{ERROR} is larger than the corresponding components of both

$$\left| \frac{\vec{EA} \cdot GR}{Cl^P} \right|$$

and

$$\left| \frac{\vec{ER} \cdot GR}{Cl^P} \cdot \vec{y}^{(c)} \right| ,$$

then \vec{y} is replaced by $\vec{y}^{(b)}$, the step size is halved, and $q-1$ new \vec{f} points and a new current \vec{y} are obtained from the procedure START. If it is not necessary to halve the step size, then $\vec{y}^{(c)}$ becomes the new \vec{y} . If every component of \vec{ERROR} is smaller for three consecutive steps than the corresponding components of both

$$\left| \frac{\vec{EA} \cdot GR}{Cl^P \cdot 2^{Q+5}} \right| \text{ and } \left| \frac{\vec{ER} \cdot GR}{Cl^P \cdot 2^{Q+5}} \cdot \vec{y}^{(c)} \right|$$

then if there are at least $2q-1$ back points in the FH array and there are at least two more steps of the current size necessary to reach XF, the step size is doubled before the next trial step. If it is not necessary either to halve or to double the step size, X is increased by H and a new trial step is made.

The procedure ADAMS continues as described until XF is reached unless repeated halvings and doublings of the step size bring the independent variable to within a fraction of a single step of XF. When this occurs, the fractional step is completed by the Runge-Kutta-Shanks procedure SHANKS, described elsewhere in this report. The order of Runge-Kutta-Shanks method and the number of function evaluations per step used here will be the same for a given integration as those used by the procedure START.

2.5 Flow Diagram and Program Listing

Figure 2 is the flow diagram for the method of Adams, Bashforth and Moulton. The program listing is in Appendix A.

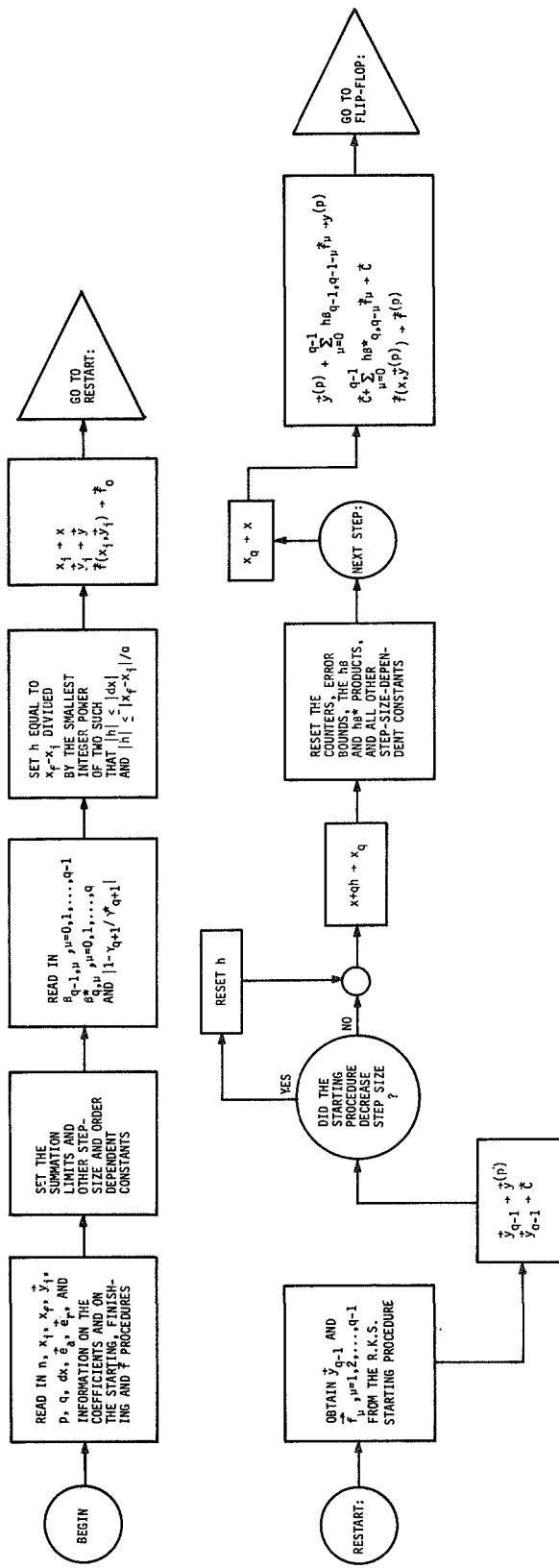


Figure 2. Flow Diagram for the Adams Method.

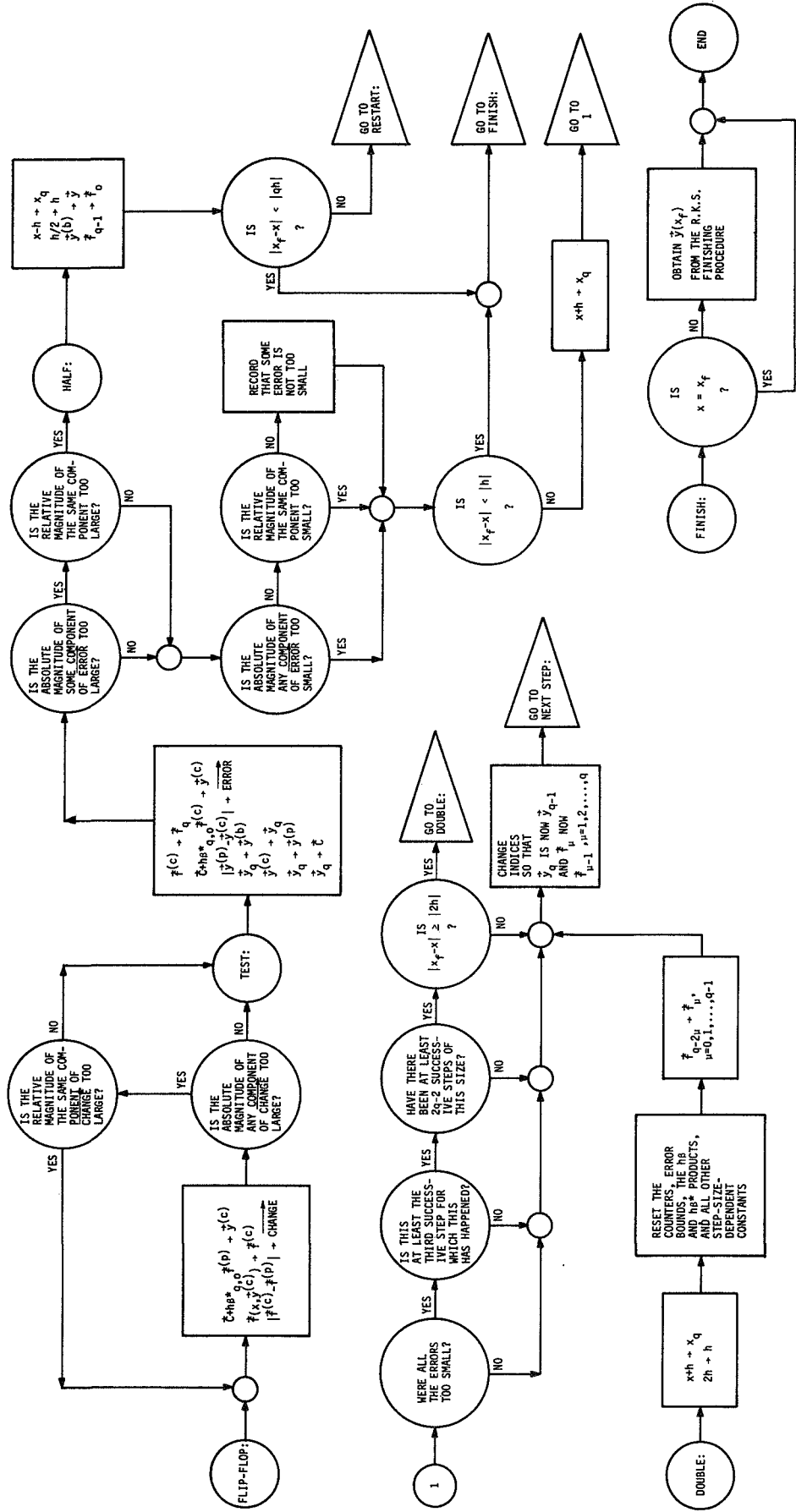


Figure 2. (Continued) Flow Diagram for the Adams Method.

D. The Method of Stetter, Gragg, and Butcher

1. Description of the Method

Following is a discussion of a method for the numerical integration of ordinary differential equations described by J. C. Butcher [13]. In his paper, Butcher presents a modification to the multistep process such that for $k \leq 7$ (where $k =$ the number of steps) processes of order $2k + 1$ are available.

A large number of possible multistep methods exist for the numerical integration of the differential equation

$$\frac{dy}{dx} = f(x,y), \quad y(x_0) = y_0 \quad (1-1)$$

Such methods are usually characterized by an integer k and a set of constants $\alpha_1, \alpha_2, \dots, \alpha_k, \beta_0, \beta_1, \dots, \beta_k$. A solution is first found for the variable y at a set of points x_1, x_2, \dots, x_{k-1} , (where $x_i = x_0 + ih$) and thereafter by the formula:

$$y_n = \alpha_1 y_{n-1} + \alpha_2 y_{n-2} + \dots + \alpha_k y_{n-k} \\ + h(\beta_0 f_n + \beta_1 f_{n-1} + \dots + \beta_k f_{n-k}) \quad (1-2)$$

for $n = k, k + 1, \dots$ where $y_i = y(x_i)$ and $f_i = f(x_i, y_i)$. Dahlquist [3] has shown that if the parameters α and β are chosen under a condition of stability, the order of a method cannot exceed $k + 1$ (if k is odd) or $k + 2$ (if k is even).

A modification to this process is presented by Butcher which consists of the addition to the right-hand side of equation (1-2) of an extra term $h \beta f_{n-\theta}$ where β and θ are additional parameters to be chosen. The modified

formula has the form:

$$y_n = \alpha_1 y_{n-1} + \alpha_2 y_{n-2} + \dots + \alpha_k y_{n-k} \\ + h (\beta f_{n-\theta} + \beta_0 f_n + \beta_1 f_{n-1} + \dots + \beta_k f_{n-k}) \quad (1-3)$$

A procedure for choosing the coefficients is presented by Butcher. The simplest stable processes are for $k = 1, 2, 3$ with $\theta = 1/2$ and for $k = 4, 5, 6$ with $\theta = 1/3$. A stable process also exists for $k = 7$ with $\theta = 13/40$.

The method for implementing the formulas is to estimate $y_{n-\theta}$ and y_n using appropriate predictor formulas, then use these predicted values to evaluate the right-hand side of equation (1-3). The forms of the predictor formulas used are:

$$y_{n-\theta} = A_1 y_{n-1} + A_2 y_{n-2} + \dots + A_k y_{n-k} \\ + h (B_1 f_{n-1} + B_2 f_{n-2} + \dots + B_k f_{n-k}) \quad (1-4)$$

$$y_n = a_1 y_{n-1} + a_2 y_{n-2} + \dots + a_k y_{n-k} \\ + h (b f_{n-\theta} + b_1 f_{n-1} + b_2 f_{n-2} + \dots + b_k f_{n-k}) \quad (1-5)$$

To use this process, $y_{n-\theta}$ is first estimated using equation (1-4). The value of the function is then determined for $y_{n-\theta}$, and these two results are used in equation (1-5) to determine a value for y_n . The value of the function is then determined for y_n and a final value is then estimated using equation (1-3).

2. The Computer Program

A double precision FORTRAN subroutine was written to implement the integration procedure described above on the UNIVAC 1108 Computer. The procedure was written to integrate a system of differential equations which have the form:

$$\frac{dy}{dx} = \vec{f}(x, \vec{y}), \quad \vec{y}(x_0) = \vec{y}_0.$$

Since the integration procedure described by Butcher is a multistep process, it must at all times have a history of back points. The process is, therefore, not self starting; it must rely on some other process to develop the first k steps. The starting procedure used in this implementation is a basic Runge-Kutta procedure as modified by E. B. Shanks and is discussed in paragraph F of this chapter. The starting procedure is called at the beginning of an integration and whenever it is necessary to reduce the step-size.

The step-size control is based on the difference between a predictor and a corrector; the control allows for halving and doubling of the step-size only. Equation (1-5) is used as the predictor (y_{np}) and equation (1-3) is considered to be the corrector (y_{nc}). An estimate of the magnitude of the error in a step is given by the absolute value of the difference in these two quantities. This is used in conjunction with a relative error term ER and an absolute error term EA in the following manner: if

$$\left| \vec{y}_{np} - \vec{y}_{nc} \right| > (\vec{EA}) \left(\frac{DX}{XF - XI} \right)^{EX}$$

and

$$\left| \vec{y}_{np} - \vec{y}_{nc} \right| > \left| (\vec{E}R) (\vec{y}_{nc}) \right| \left(\frac{DX}{XF - XI} \right)^{EX}$$

then the step is rejected and the starting procedure is entered with the previous point and a step-size equal to half the old step-size. If

$$\left| \vec{y}_{np} - \vec{y}_{nc} \right| < (\vec{E}A) \left(\frac{DX}{XF - XI} \right)^{EX} \left(\frac{1}{2^{2k+4}} \right)$$

or

$$\left| \vec{y}_{np} - \vec{y}_{nc} \right| < \left| (\vec{E}R) \left(\frac{DX}{XF - XI} \right)^{EX} (\vec{y}_{nc}) \right| \left(\frac{1}{2^{2k+4}} \right)$$

for three steps (without an intervening halving of the step-size) and if there is sufficient history of back points, then the step is accepted and the step-size is doubled. If neither the conditions for halving nor the conditions for doubling are met, then the step is accepted and the step-size remains constant. It is important to note that the above criteria must be satisfied for all corresponding components of the vector quantities before the conditions are considered to be met.

The method of ending the integration procedure is to run until the value of the independent variable plus the next step is either equal to or greater than the given final value i.e.

$$X + DX \geq XF.$$

If it is exactly equal, then the procedure takes one more step and quits.
If $X + DX > XF$, then a special ending procedure is called to take the final step. This ending procedure is also basic Runge-Kutta procedure as modified by E. B. Shanks. It is discussed in paragraph B of this chapter. The procedure call for the Butcher procedure must be as follows:

```
CALL BUTCHER (N, XI, XF, K, EA, ER, DXV, CON, EX, RKC, YIV, RKSNF, RKSODR)
```

N - the number of dependent variables (integer)

XI - the initial value of the independent variable

XF - the final value of the independent variable

K - the number of steps to be used in the Butcher method (integer)

EA - the acceptable absolute error vector contained in an array of
dimension N

ER - the acceptable relative error vector contained in an array of
dimension N

DXV - the suggested initial step-size

CON - the array row containing the Butcher constants required for the order
of the method specified

EX - the error exponent

RKC - the array containing the Runge-Kutta constants

YIV - the initial values of the dependent variable; upon exiting the Butcher
procedure, this array will contain the final values of the dependent
variables

RKSNF- the number of function evaluations in the Runge-Kutta-Shanks procedure
(integer)

RKSODR-the order of the Runge-Kutta-Shanks procedure (integer)

All variables and arrays not designated integer are double precision.

2.1 Flow Diagram and Program Listing

Figure 3 is the flow diagram for the method of Stetter, Gragg, and Butcher. A listing of the program is given in Appendix A.

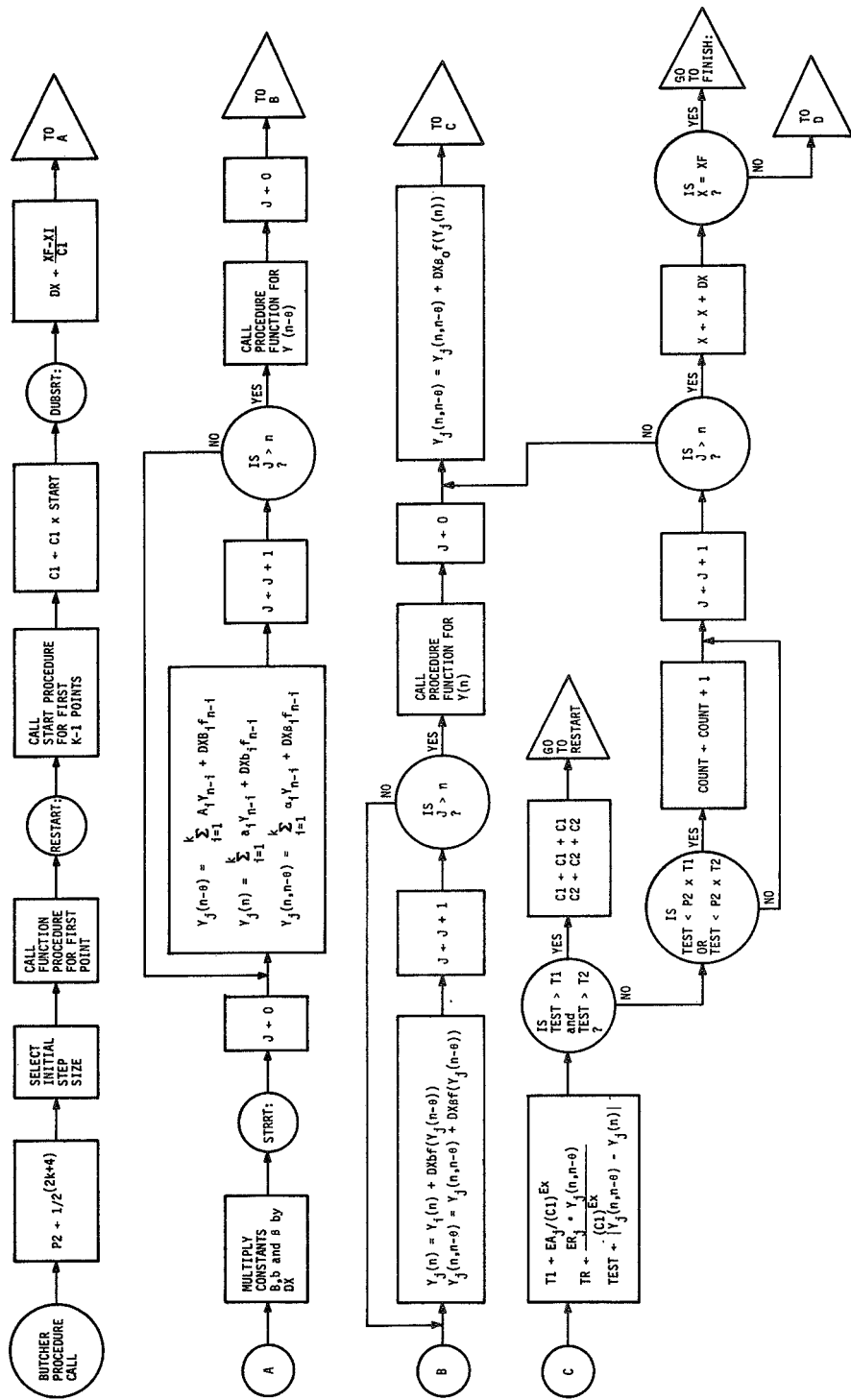


Figure 3. Flow Diagram for the Stetter-Gragg-Butcher Method.

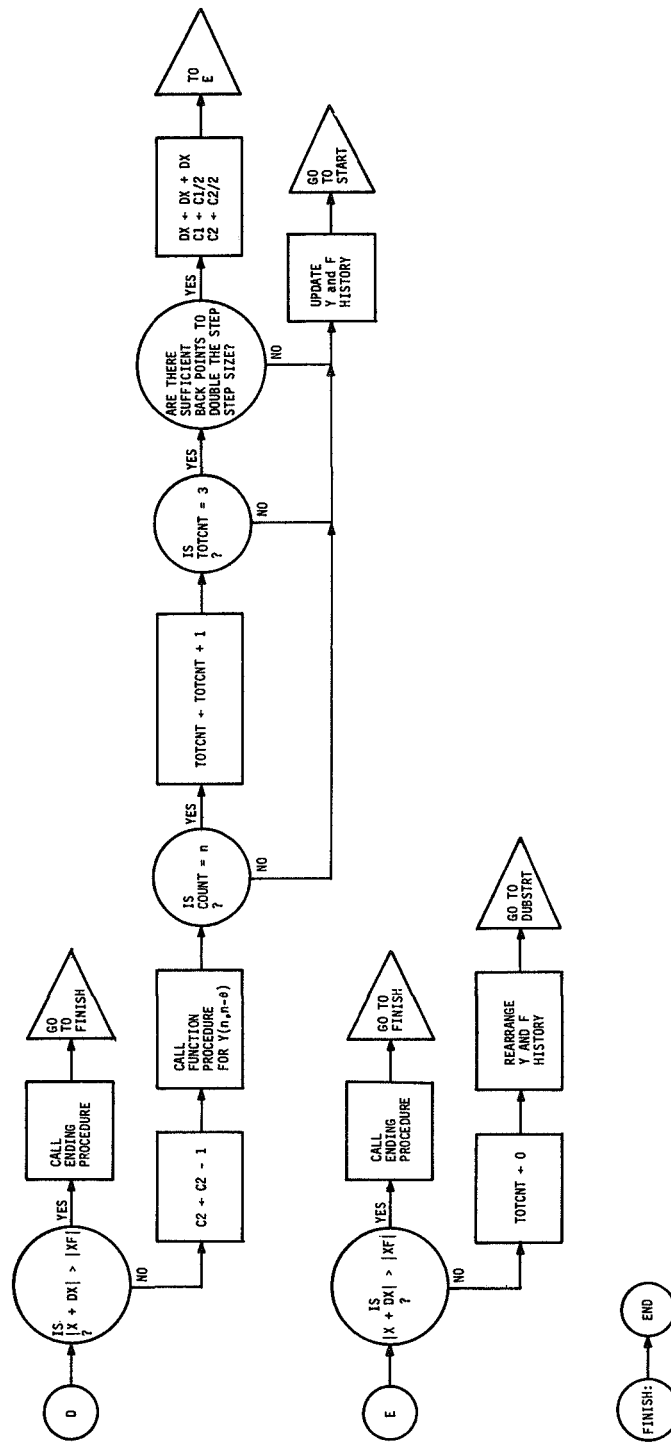


Figure 3. (Continued) Flow Diagram for the Stetter-Gragg-Butcher Method.

E. The Cowell Method

1. Description of the Method

Cowell's method as described herein is a multistep predictor-corrector method for the numerical solution of the first-order vector differential equation

$$\vec{y}'(x) = \frac{d}{dx} \vec{y}(x) = \vec{f}(x, \vec{y}(x)), \quad \vec{y}(x_0) = \vec{y}_0. \quad (1-1)$$

A complete derivation and description of Cowell's method can be found in [9] and [11]; only the essential formulas are included here.

The following notation is adopted. Let q be an even positive integer, $m = q/2$, h be the step size (assumed to be constant over some set of calculations),

$$x_n = x_0 + nh, \quad \vec{y}_n = \vec{y}(x_n), \quad \text{and} \quad \vec{f}_n = \vec{f}(x_n, \vec{y}_n).$$

The predictor formula is

$$\vec{y}_n = h \left[\overrightarrow{\delta^{-1}} f_{n-\frac{1}{2}} + \sum_{j=0}^q P_j \vec{f}_{n-1-j} \right], \quad (1-2)$$

The corrector formula is

$$\vec{y}_n = h \left[\overrightarrow{\delta^{-1}} f_{n-\frac{1}{2}} + \sum_{j=0}^q C_j \vec{f}_{n-j} \right], \quad (1-3)$$

and the mid-range formula is

$$\vec{y}_n = h \left[\overrightarrow{\delta^{-1}} f_{n-\frac{1}{2}} + \sum_{j=0}^q M_j \vec{f}_{n+m-j} \right]. \quad (1-4)$$

The predictor formula gives \vec{y}_n in terms of $\overrightarrow{\delta^{-1}f}_{n-\frac{1}{2}}$ and the function values at the previous $q+1$ points; the corrector formula gives a new value of \vec{y}_n in terms of $\overrightarrow{\delta^{-1}f}_{n-\frac{1}{2}}$, the old value of \vec{y}_n , and the function values at the previous q points; the mid-range formula gives a value of \vec{y}_n in terms of $\overrightarrow{\delta^{-1}f}_{n-\frac{1}{2}}$ and the function values at the $q+1$ consecutive points centered around x_n .

The equation

$$\overrightarrow{\delta^{-1}f}_{n-\frac{1}{2}} = \overrightarrow{\delta^{-1}f}_{n-1-\frac{1}{2}} + \vec{F}_{n-1} \quad (1-5)$$

completes the set of formulas necessary for the numerical solution of (1-1).

If it is assumed that

$$\left[\vec{f}_i \right]_{i=0}^q \quad \text{and} \quad \vec{y}_m$$

have been obtained by some starting procedure, the mid-range formula (1-4) can be applied with $n=m$ to obtain

$$\overrightarrow{\delta^{-1}f}_{m-\frac{1}{2}}.$$

Equation (1-5) can then be applied m times to obtain

$$\overrightarrow{\delta^{-1}f}_{q-\frac{1}{2}}$$

For each positive integer i

$$\overrightarrow{\delta^{-1}f}_{q+i-\frac{1}{2}}$$

can be computed from

$$\overrightarrow{\delta^{-1}f}_{q+i-1-\frac{1}{2}}$$

and \vec{f}_{q+i-1} using (1-5); \vec{y}_{q+i} can be computed using the predictor (1-2); \vec{f}_{q+i} can be computed from the predicted value; \vec{y}_{q+i} can be computed using the corrector (1-3); \vec{f}_{q+i} can be computed from the corrected value; if necessary, iteration can be resorted to, using (1-3), until the last two computed values of \vec{y}_{q+i} agree to sufficient accuracy. For any $j \geq m$ a value of \vec{y}_{q+j-m} can be obtained from the mid-range formula (1-4) and compared with the value obtained from the predictor-corrector step. If the two values of \vec{y}_{q+j-m} are in sufficient agreement, the values up through \vec{y}_{q+j} are considered acceptable; if not, \vec{y}_{q+j-m} is considered the last acceptable value and all values beyond are rejected.

Hence, the knowledge of (1-2), (1-3), (1-4), and (1-5) is sufficient to apply Cowell's method in the numerical solution of (1-1). The coefficients $\left\{ P_j \right\}_{j=0}^q$, $\left\{ C_j \right\}_{j=0}^q$, and $\left\{ M_j \right\}_{j=0}^q$ are given in [11] for $q=4, 6, 8, 10, 12, 14,$ and 16 .

2. The Computer Program

The Cowell computer program is a UNIVAC 1108 FORTRAN V double precision subroutine called as follows:

```
call Cowell (n, xi, xf, y, ea, er, p, dxv, rksfn, rksrdr, rkscff, q,
            cwillcf)
```

The parameters of the procedure are defined as follows:

- \underline{n} - the number of dependent variables in the vectors \vec{y} and \vec{f} (integers);
- \underline{xi} - x_0 , the starting value of the independent variable x ;
- \underline{xf} - the final value of the independent variable x ;
- \underline{y} - the array in which $\vec{y}_0 = \vec{y}(xi)$ is located upon entry and in which $\vec{y}(xf)$ is located upon exit;

ea - the array containing the absolute error vector;
er - the array containing the relative error vector;
p - the exponent used in step size control;
rksfn - the number of function evaluations used in the Runge-Kutta-Shanks starting and closing procedures (integer);
rksrdr - the order of the Runge-Kutta-Shanks closing procedure (integer);
rkscff - the array containing the Runge-Kutta-Shanks coefficients for the starting and closing procedures;
q - the even integer used in describing Cowell's method (integer);
cwllcf - the array containing the Cowell coefficients.

All variables not designated integer are double precision. All arrays are double precision.

The procedure performs the numerical integration of (1-1) from $x = \underline{x_i}$ to $x = \underline{x_f}$. The step size h used is always the length of the interval $\underline{x_f} - \underline{x_i}$ divided by a power of 2 in order to avoid error building in the independent variable, and two counters c1 and c2 are kept. c1 is always a positive, integral power of 2, and $h = (\underline{x_f} - \underline{x_i})/\underline{c1}$. c2 is the number of steps necessary to step from the present x to $\underline{x_f}$ using the current step size h . Initially c2 = c1; as each step is taken c2 is decremented by one and the present value of x is computed by $\underline{x} = \underline{x_f} - h \underline{c2}$. If h is halved, c1 and c2 are doubled; if h is doubled, c1 and c2 are halved. Hence, c2 need not be integral.

The error vectors \vec{ea} and \vec{er} , like \vec{y} , have n components. (Although the base of the arrays \underline{y} , ea, and er is one, the n components are placed in positions 2, 3,.. $n + 1$ of the arrays.) The procedure's error control attempts to guarantee that, in integrating from x_i to x_f , each component

of \vec{y} will not be in absolute error more than the corresponding component of \vec{ea} and will not be in relative error more than the corresponding component of \vec{er} . At each step, the procedure requires that for each i , $1 \leq i \leq n$, either the absolute error in $y [i]$ does not exceed $ea [i]/(cl^p)$ or the relative error in $y [i]$ does not exceed $er [i]/(cl^p)$.

If $p = 1$ and $\vec{er} = 0$ then the accumulated error in any component of \vec{y} should not exceed the corresponding component of \vec{ea} . If the error is assumed to accumulate randomly as the square root of the number of steps, $p = \frac{1}{2}$ and $\vec{er} = 0$ will cause the accumulated error in any component of \vec{y} to be approximately the corresponding component of \vec{ea} .

If $p = 1$ and $\vec{ea} = 0$ then the accumulated error in any component of \vec{y} should not exceed the corresponding component of \vec{er} times the largest value assumed by that component of \vec{y} during the integration. If the error is assumed to accumulate randomly as the square root of the number of steps, $p = \frac{1}{2}$ and $\vec{ea} = 0$ will cause the accumulated error in any component of \vec{y} to be approximately the corresponding component of \vec{er} times some average value assumed by that component of \vec{y} during the integration.

The subroutine FUNCTI which computes $\vec{f} = \vec{f}(x,y)$ has the following call:

call FUNCTI (n, x, yv, fv);

The parameters of the procedure FUNCTI are defined as follows:

n - the number of dependent variables in the vectors \vec{y} and \vec{f} (integer)

x - the value of the independent variable

yv - the array in which \vec{y} is stored

fv - the array in which \vec{f} is stored after computation

The procedure start is the general multistep method starting procedure described in paragraph F of this chapter. The procedure shanks is the Runge-Kutta-Shanks integration procedure described in paragraph B of this chapter. The coefficient array rkscff contains the Runge-Kutta-Shanks coefficients in the order required by the procedures start and shanks. The number of function evaluations rksfn is required by both start and shanks; the order rksrdr is required by shanks.

The array cwllcf contains the coefficients of (1-2), (1-3), and (1-4) in the order $P_0, P_1, \dots, P_q, C_0, C_1, \dots, C_q, M_0, M_1, \dots, M_q$; P_0 is in the first position of the array.

The suggested initial step size dxv is optional. The procedure first sets c1 = 2 and doubles c1 until c1 \geq q. If dxv = 0 or dxv \neq 0 and $h \leq |\underline{dx}|$ then c1 is left alone. Otherwise, c1 is doubled until $h \leq |\underline{dx}|$.

The integration now begins.

$$\vec{f}_0 = \vec{f}(x_0, \vec{y}_0)$$

is computed. The start procedure is called to obtain

$$\left[\begin{array}{c} \vec{f}_i \\ \vec{f}_i \end{array} \right]_{i=1}^q, \vec{y}_m, \vec{y}_q \text{ and } x_q.$$

c1 and c2 are adjusted if h was changed by the start procedure. c2 is decremented by q since q steps took place in the start procedure. If $c2 < m$, closing takes place. Otherwise,

$$\overrightarrow{\delta^{-1} f_{m-\frac{1}{2}}}$$

is calculated from

$$\begin{bmatrix} \vec{f}_i \end{bmatrix} \quad q \\ i=0$$

and \vec{y}_m using the mid-range formula (1-4). m applications of (1-5) yield

$$\xrightarrow{\delta^{-1}} f_{q-\frac{1}{2}}$$

and n is set equal to q .

For $1 \leq i \leq m$ the following set of steps takes place. c_2 is decremented by 1, and x_{n+i} is calculated.

$$\xrightarrow{\delta^{-1}} f_{n+i-\frac{1}{2}}$$

is calculated from

$$\xrightarrow{\delta^{-1}} f_{n+i-1-\frac{1}{2}}$$

and \vec{f}_{n+i-1} using (1-5). \vec{y}_{n+i} is calculated using the predictor (1-2), and \vec{f}_{n+i} is calculated. \vec{y}_{n+i} is next calculated using the corrector (1-3), and \vec{f}_{n+i} is again calculated. Let \vec{v} be the vector which is the absolute value of the difference between the last two calculated values of \vec{y}_{n+i} . Each component of \vec{v} is compared with the corresponding component of $\vec{ea}/(10 \cdot c_1^p)$ for absolute error and with the product of the corresponding components of $\vec{er}/(10 \cdot c_1^p)$ and the last calculated value of \vec{y}_{n+i} for relative error. If any component of \vec{v} exceeds in both the absolute and the relative error tests, the steps which calculate \vec{y}_{n+i} using the corrector (1-3), calculate \vec{f}_{n+i} from the value of \vec{y}_{n+i} , and which test the last two calculated values of \vec{y}_{n+i} are repeated. When each component of \vec{v} does not exceed in either the absolute or the relative error test, the last values of \vec{y}_{n+i} and \vec{f}_{n+i} are retained.

The mid-range formula (1-4) is now used to calculate a new value of \vec{y}_n from

$$\left[\vec{f}_{n+i} \right]_{i=m}^m$$

and

$$\overrightarrow{\delta^{-1}f_{n-\frac{1}{2}}}$$

Let \vec{v} be the vector which is the absolute value of the differences between the new value of \vec{y}_n and the previously calculated value of \vec{y}_n . If sufficient history is available for doubling the step size, i.e., $n > q + m$, each component of \vec{v} is compared with the corresponding component of $\vec{ea}/(10 \cdot c1^p \cdot 2^{q+3})$ for absolute error and with the product of the corresponding components of $\vec{er}/(10 \cdot c1^p \cdot 2^{q+3})$ and the new value of \vec{y}_n for relative error.

If each component of \vec{v} does not exceed in either the absolute or the relative error tests, the last m steps are accepted, $c1$ and $c2$ are halved, and the step size is doubled. If $c2 < m$, closing takes place. Otherwise

$$\left[\vec{f}_i \right]_{i=0}^q$$

becomes

$$\left[\vec{f}_{n-m+2i} \right]_{i=0}^q$$

\vec{y}_m becomes \vec{y}_{n-m} , \vec{y}_q becomes \vec{y}_{n+m} , x_q becomes x_{n+m} , and, as if the starting procedure had calculated these values, control returns to the step where

$$\overrightarrow{\delta^{-1}f_{m-\frac{1}{2}}}$$

is calculated using the mid-range formula (1-4).

If any component of \vec{v} exceeds in both the absolute and the relative error tests, this component and each untested component is compared with the corresponding component of $\vec{ea}/(10 \cdot c1^P)$ for absolute error and with the product of the corresponding components of $\vec{er}/(10 \cdot c1^P)$ and the new value of \vec{y}_n for relative error. If each component of \vec{v} does not exceed in either the absolute or the relative error test, the last m steps are accepted and the step size remains unchanged. If $c2 < m$, closing takes place. Otherwise, n becomes $n + m$ and control returns to the steps which calculate

$$\left[\vec{y}_{n+i} \right]_{i=1}^m \cdot$$

If any component of \vec{v} exceeds in both the absolute and the relative error tests, the last m steps are rejected, $c2$ is incremented by m , $c1$ and $c2$ are doubled, and the step size is halved. \vec{f}_0 becomes \vec{f}_n , \vec{y}_0 becomes \vec{y}_n , x_0 becomes x_n , and control is returned to the step which calls the start procedure.

If sufficient history is not available for doubling, control transfers as if the first component of \vec{v} exceeded both the first component of $\vec{ea}/(10 \cdot c1^P \cdot 2^{q+3})$ and the product of the first components of $\vec{er}/(10 \cdot c1^P \cdot 2^{q+3})$ with the first component of the new value of \vec{y}_n .

Closing takes place whenever m steps at the present step size would carry the integration beyond xf , i.e., whenever $c2 < m$. If $c2 > 0$, the Runge-Kutta-Shanks procedure is used to integrate from the present value of x to xf ; if $c2 = 0$, the present value of x is xf . In either case, the integration is now complete.

Several efficiency measures are employed in the program. First, the coefficients

$$\begin{bmatrix} P_j \\ C_j \end{bmatrix}_{j=0}^q,$$

and

$$\begin{bmatrix} M_j \end{bmatrix}_{j=0}^q$$

are multiplied by the step size h and stored as multiplied until the step size changes. Second, the vectors $\vec{e}a/(10 \cdot c1^P)$, $\vec{e}r/(10 \cdot c1^P)$, $\vec{e}a/(10 \cdot c1^P \cdot 2^{q+3})$, and $\vec{e}r/(10 \cdot c1^P \cdot 2^{q+3})$ are calculated from $\vec{e}a$ and $\vec{e}r$ and stored as calculated until the step size changes. Third, the corrector partial sum

$$h \delta^{-1} \vec{f}_{n-\frac{1}{2}} + h \sum_{j=1}^q C_j \vec{f}_j$$

is computed and stored at each step; successive applications of the corrector only require adding $h \cdot C_0 \cdot \vec{f}_n$ to obtain \vec{y}_n . Fourth, during applications of the corrector, two arrays are used to store the last two calculated values of \vec{y}_n ; a flag is used to mark the last calculated value so that the next value is placed in the unflagged array and the flag is switched. This avoids transfer from array to array as successive corrector iterates are computed. Fifth, cyclic indexing is used to avoid moving the function value history after each step or set of steps unless doubling takes place.

One unusual condition can result. If, during any step taken in computing

$$\left[\begin{array}{c} \vec{y} \\ y_{n+i} \end{array} \right]_{i=1}^m ,$$

the number of times through the corrector exceeds eight, control transfers as if the set of m steps has been completed and rejected; i.e., a step size halving was called for with a restart beginning at \vec{y}_n .

2.1 Flow Diagram and Program Listing

Figure 4 is the flow diagram for the Cowell method. The program listing is in Appendix A.

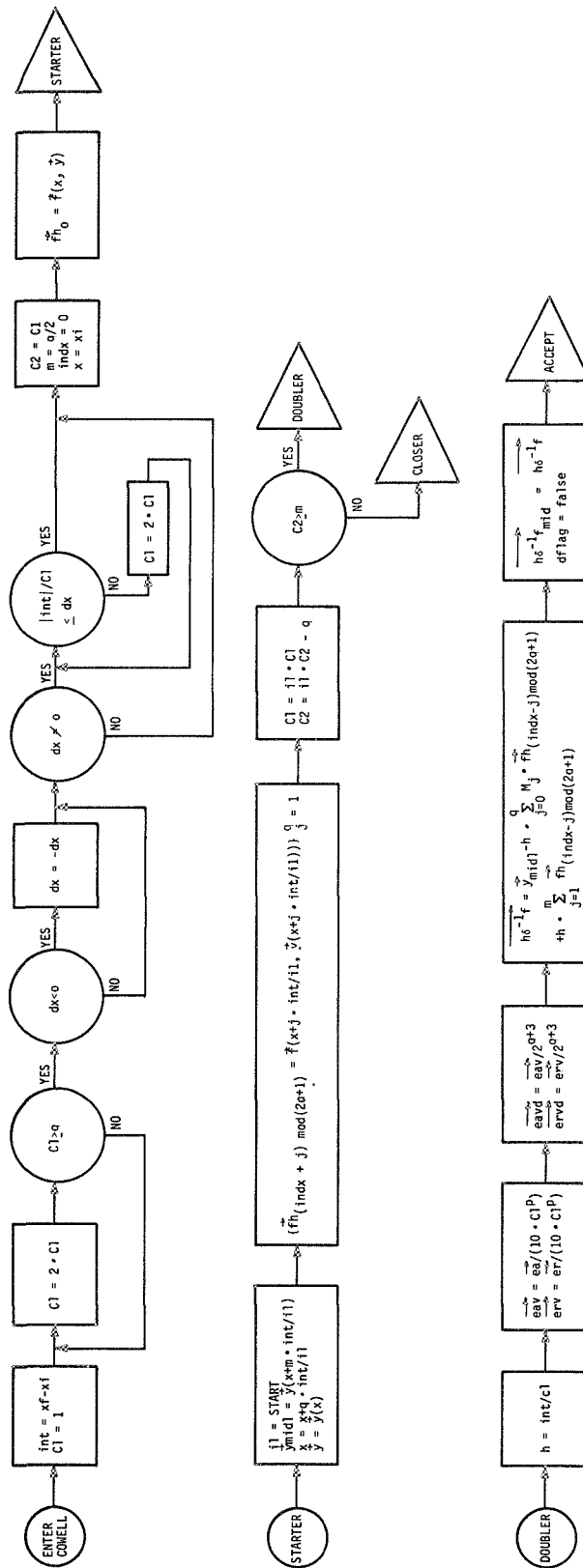


Figure 4. Flow Diagram for the Cowell Method.

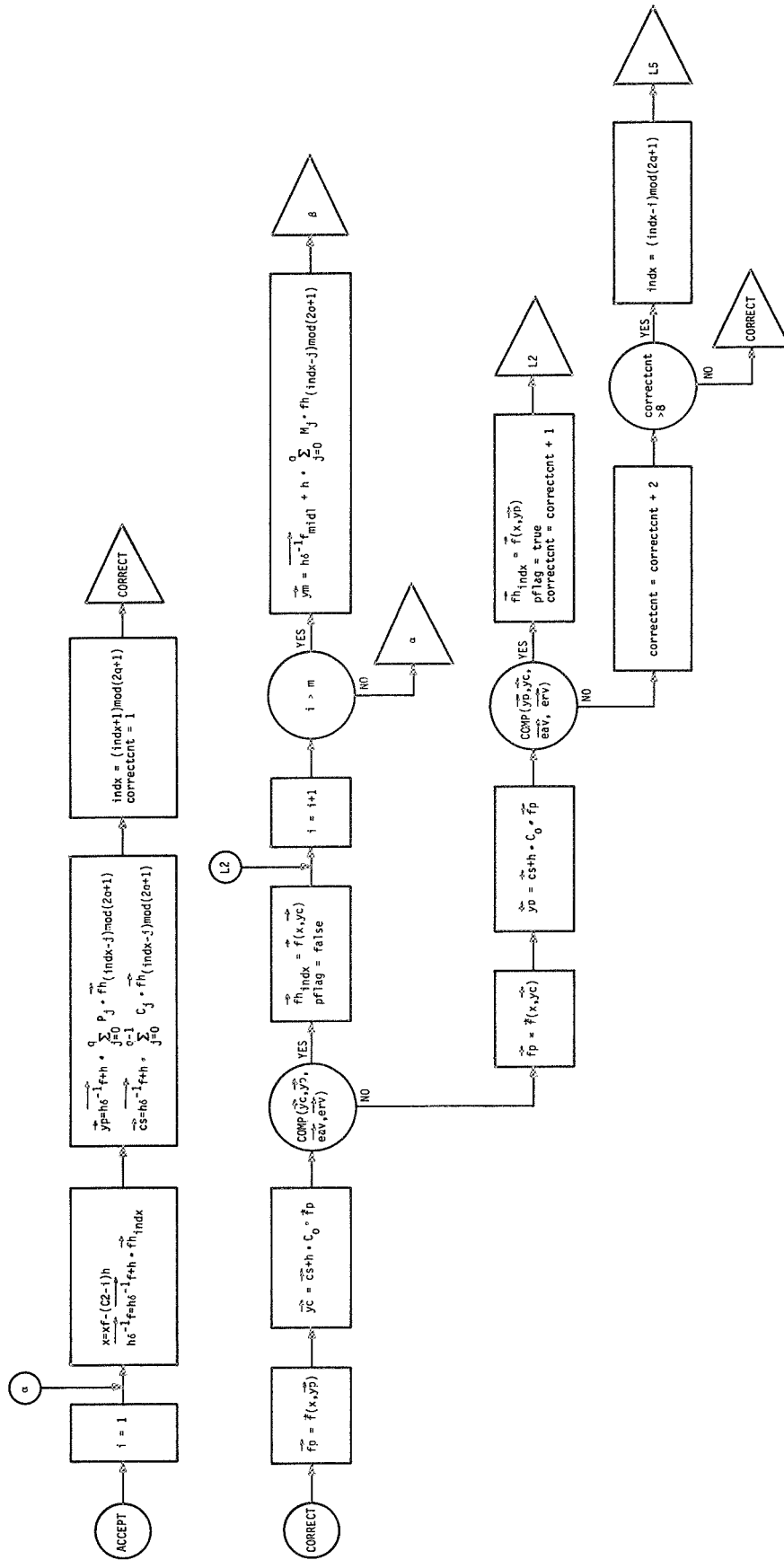


Figure 4. (Continued) Flow Diagram for the Cowell Method.

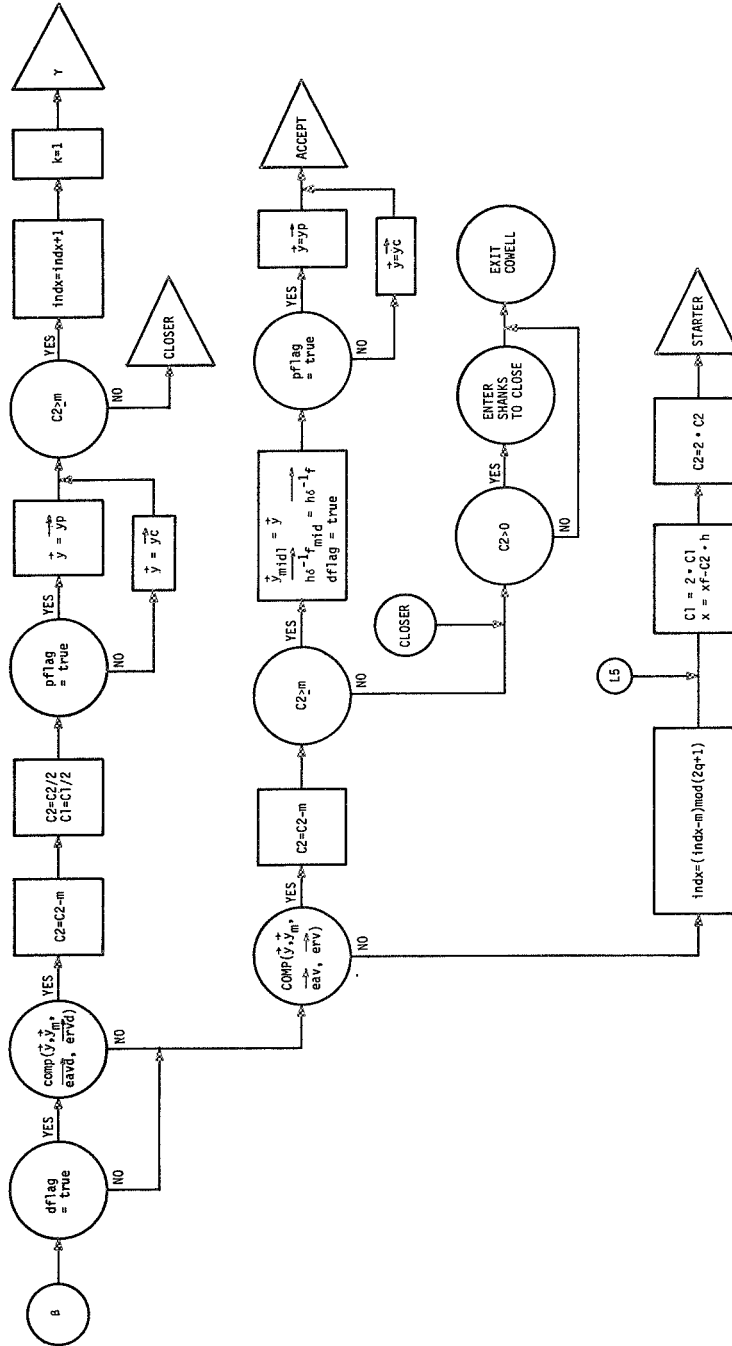


Figure 4. (Continued) Flow Diagram for the Cowell Method.

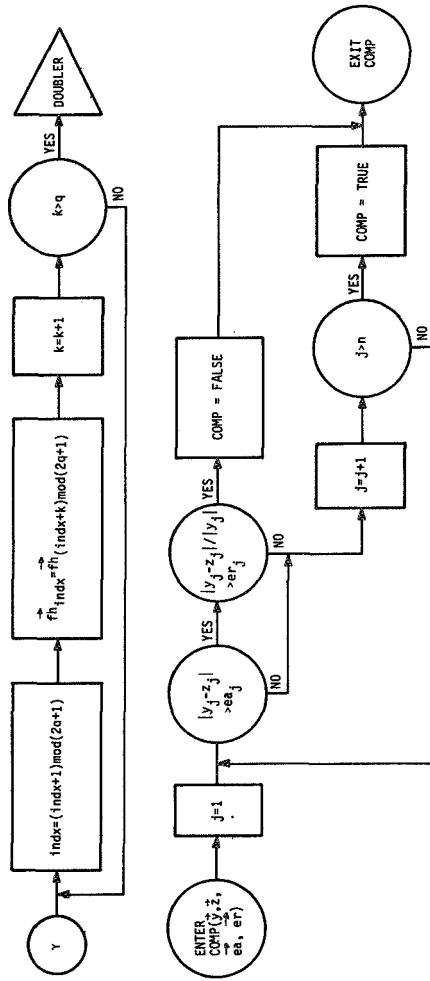


Figure 4. (Continued) Flow Diagram for the Cowell Method.

F. The General Multistep Method Starting Subroutine

1. Introduction

The general multistep method starting procedure is a UNIVAC 1108 FORTRAN V double-precision Runge-Kutta-Shanks subroutine used for obtaining starting values for the Adams, Butcher, and Cowell multistep methods.

Start is a real valued function called as follows:

```
start (n, xi, xf, icl, ea, er, m, x, yiv,  
      yh, fh, yfv, cyi, cym, pa, p,  
      fneval, rkscns)
```

2. Description of the Program

The parameters of the function are defined as follows:

- n - the number of dependent variables (integer);
- xi - the starting value of the independent variable x passed to the multistep method;
- xf - the final value of the independent variable x passed to the multistep method;
- icl - the integer counter $(xf - xi)/h$ from the multistep method (integer);
- ea - the absolute error vector passed to the multistep method;
- er - the relative error vector passed to the multistep method;
- m - the number of history points to be calculated by start (integer);
- x - the value of the independent variable at which start begins its integration;
- yiv - the array which contains on entry for Adams and Cowell the values of the dependent variables at x and which contains on exit for Cowell the values of the dependent variable at the mth point calculated by start;

yh - the array which contains on entry for Butcher in row cyi the values of the dependent variables at x and which contains on exit for Butcher the values of the dependent variables at each of the m points calculated by start;

fh - the array which contains on entry in row cyi the function values at x and which contains on exit the function values at each of the m points calculated by start;

yfv - the array which contains on exit the values of the dependent variables at the mth point calculated by start for Adams or the m/2th point calculated by start for Cowell;

cyi - the cyclic index identifying on entry the row of yh in which the values of the dependent variables at x are stored for Butcher and the row of fh in which the function values at x are stored for any method (integer);

cym - the number of rows in the arrays yh and fh (integer);

pa - the parameter which is zero for Adams, one for Cowell, two for Butcher (integer);

p - the exponent such that the absolute error at each step is not to exceed $\frac{ea}{cl^p}$ and the relative error at each step is not to exceed $\frac{er}{cl^p}$;

fneval - the number of function evaluations required by the Runge-Kutta-Shanks procedure (integer);

rkscns, - the array which contains the Runge-Kutta-Shanks coefficients in the same order as required by the procedure shanks described in section B.

The value of start on exit is two to the power of the number of halvings which took place within start (a real).

All variables and arrays not designated otherwise are double precision.

Although the base of the arrays ea, er, yiv, and yfv and of the rows of yh and fh is one, the n components are placed in position 2, . . ., $n+1$ and the first position is unused.

The procedure attempts to calculate m (if m is even and positive) or $m + 1$ (if m is odd) Runge-Kutta-Shanks steps of size $h = (x_f - x_i)/c_1$. After each even step of size h is taken, one step of size $2h$ is taken over the interval spanned by the two steps of size h . The absolute value of the differences in each dependent variable between the $2h$ -step and the second h -step is compared with the corresponding component of $\vec{ea}/(c_1/2)^P$ for absolute error and with the product of the corresponding component of $\vec{er}/(c_1/2)^P$ and the corresponding dependent variable value from the second h -step for relative error. If each component of the difference does not exceed in either the absolute or the relative error test and m steps have not yet been taken, the process of two h -steps, one $2h$ -step, and test is continued. If any component of the difference exceeds in both the absolute and the relative error tests, c_1 is doubled, h is halved, and integration begins again at x . The first step of previous size h was saved and becomes the first step of present size $2h$.

The m calculated function values from h -steps are placed in rows $(c_{y1} + 2) \bmod c_{ym+1}, (c_{yi} + 3) \bmod c_{ym+1}, \dots, (c_{yi+m+1}) \bmod c_{ym+1}$ of the array fh. For Butcher, the corresponding dependent variable values from h -steps are placed in the corresponding rows of the array yh; if m is odd, the values of the dependent variable after h -step $m + 1$ are placed in row $(c_{yi} + m + 2) \bmod c_{ym+1}$ of yh. For Adams, the dependent variable values from h -step m are placed in the array yfv. For Cowell, the dependent variable values from h -step m are placed in the array yiv and from h -step $m/2$ (m is always even for Cowell) are placed in yfv. If m is zero, no calculation takes place.

Start calls an external subroutine runkut.

2.1 Flow Diagram and Program Listing

Figure 5 is the flow diagram for the starting procedure. The program listing is in Appendix A.

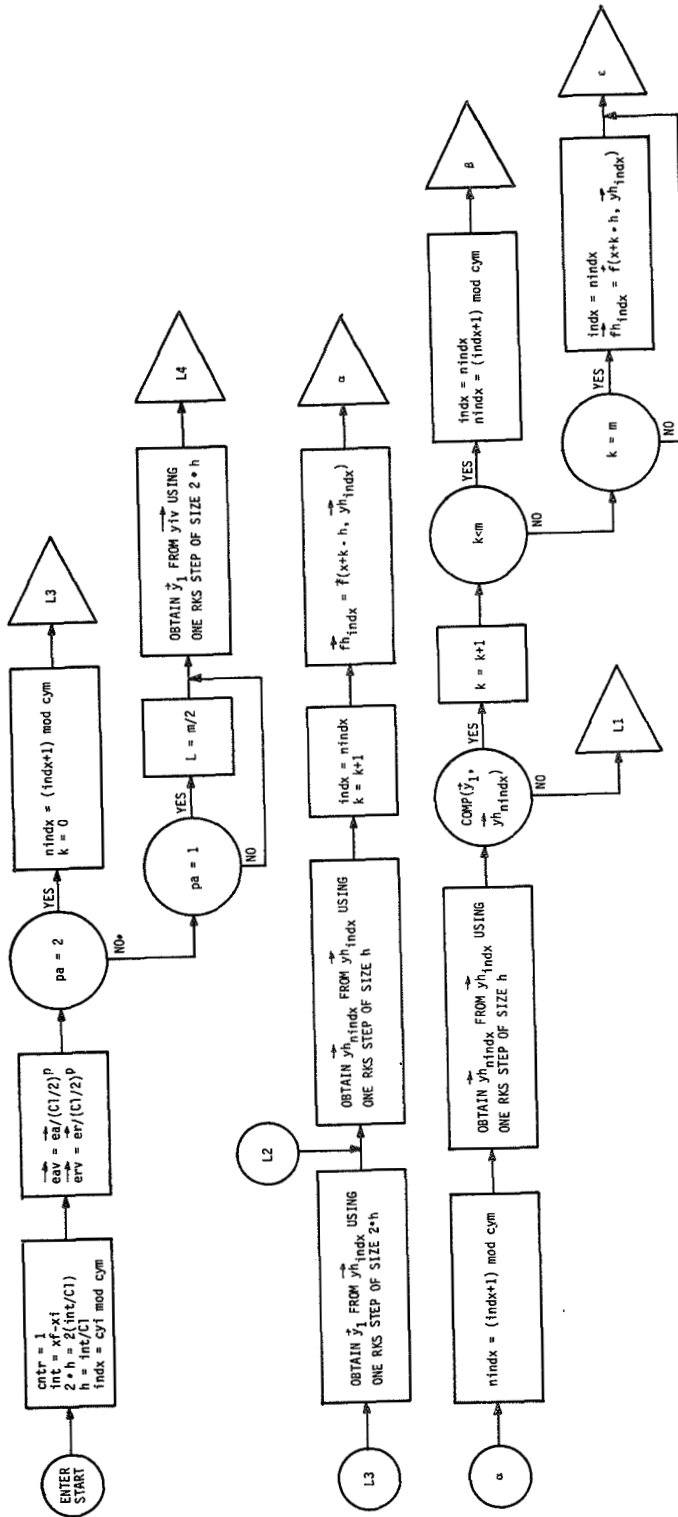


Figure 5. Flow Diagram for the General Multistep Method Starting Procedure.

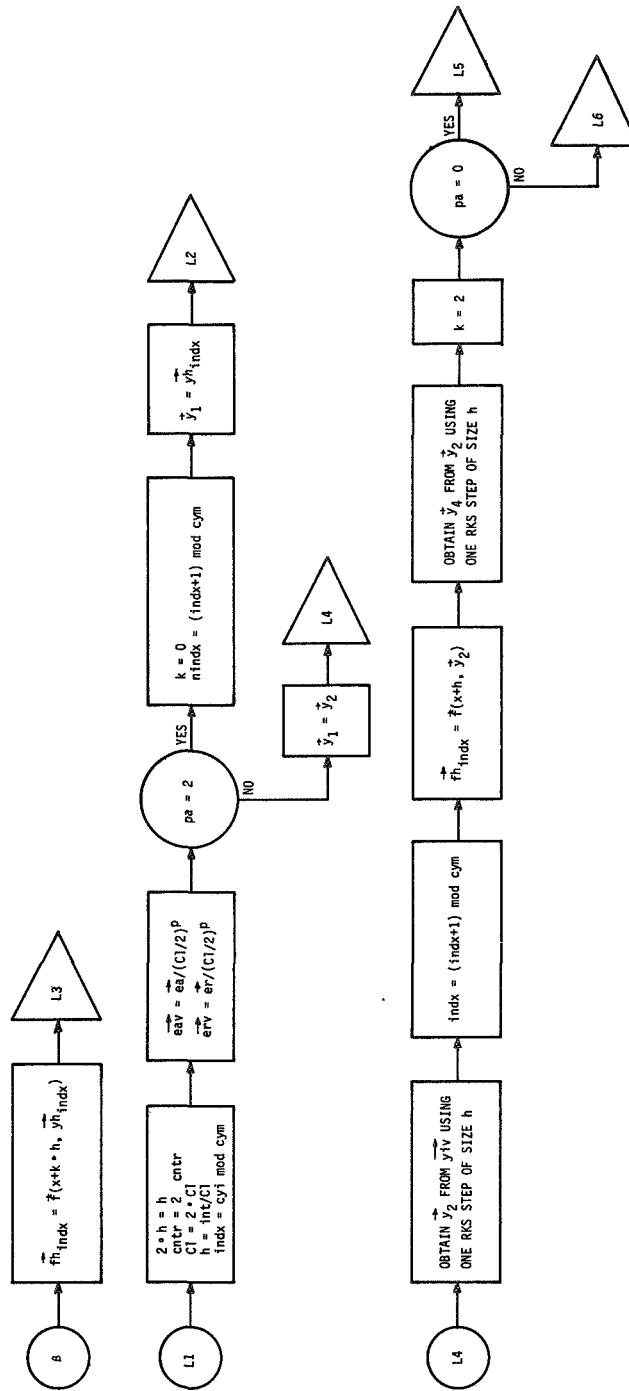


Figure 5. (Continued) Flow Diagram for the General Multistep Method Starting Procedure.

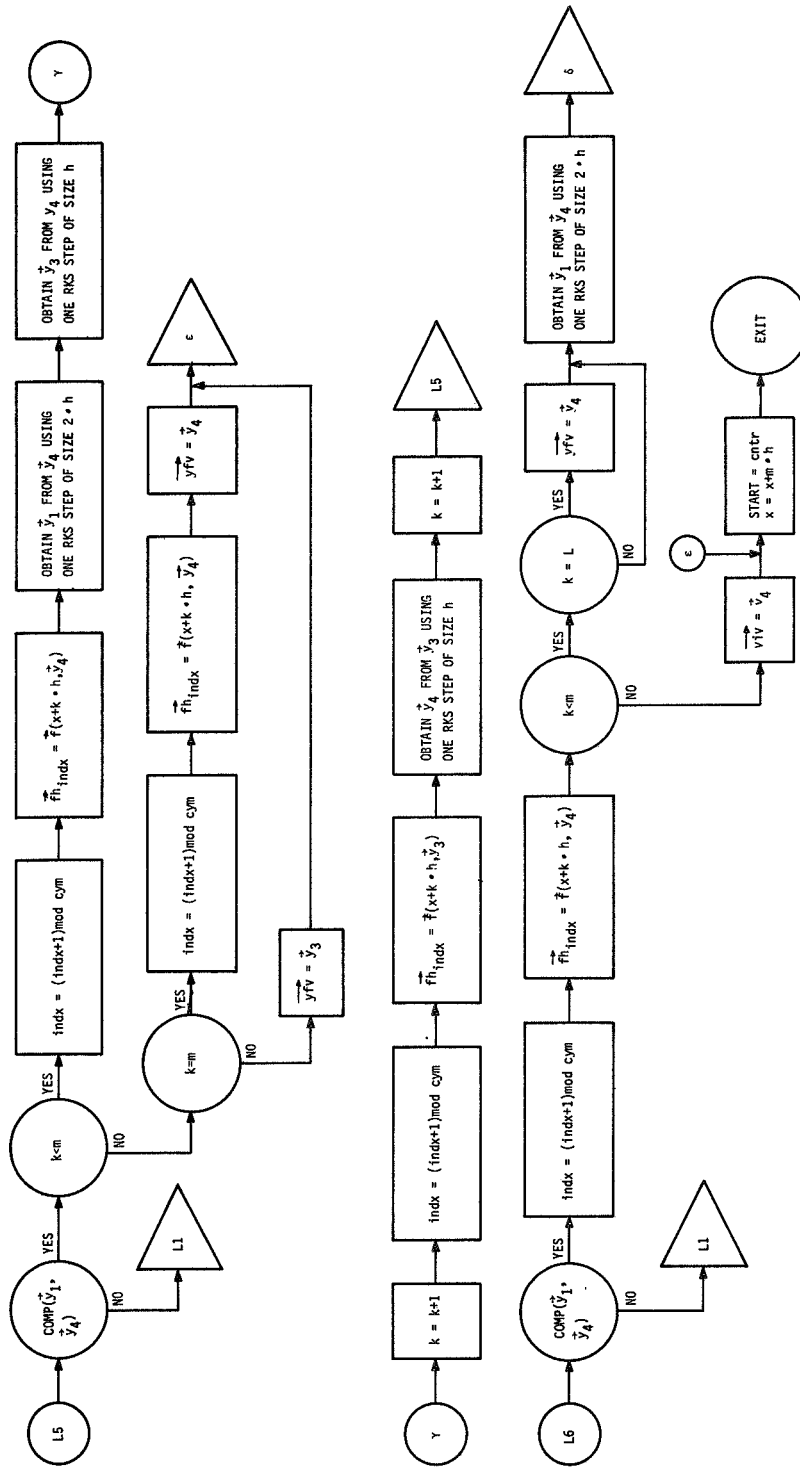


Figure 5. (Continued) Flow Diagram for the General Multistep Method Starting Procedure.

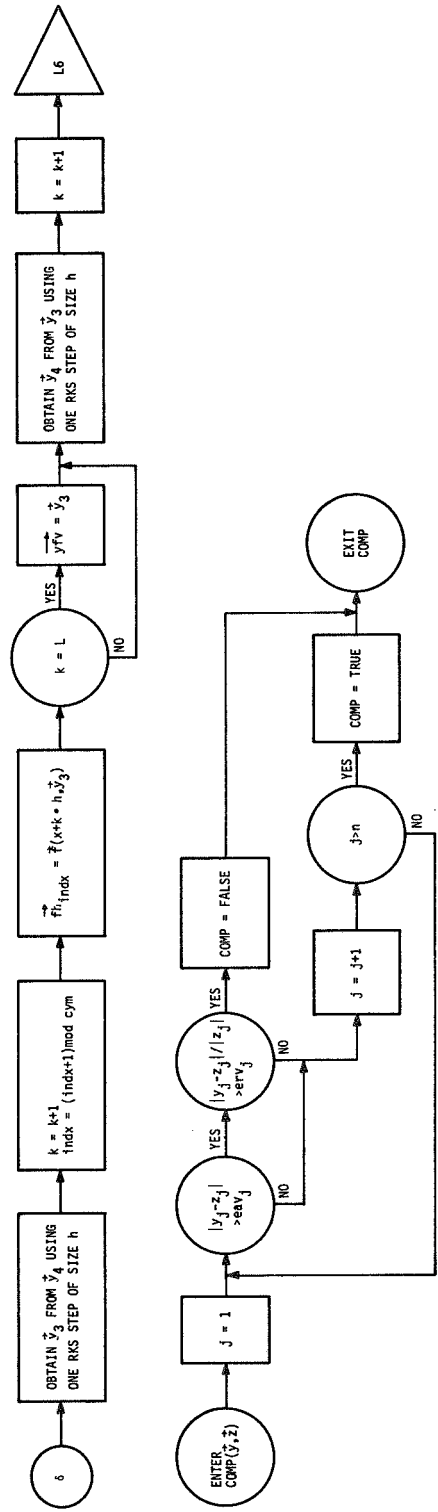


Figure 5. (Continued) Flow Diagram for the General Multistep Method Starting Procedure.

G. The Derivative Subroutine FUNCTI

A procedure for calculating the vector $\vec{y}' = \vec{f}(x, \vec{y}(x))$ must be an external subroutine characterizing the set of differential equations to be solved. This subroutine is called by each of the integration subroutines and must itself have the following formal parameter list:

<u>Identifier</u>	<u>Type</u>	<u>Usage or Meaning</u>
N	Integer	Number of equations being integrated.
X	Double	Current value of the independent variable.
YV	Double Array	Current dependent variable vector (input).
FV	Double Array	\vec{f} value vector (output).

The components of the \vec{y} vector are contained in positions 2 through $N + 1$ of YV, and the components of \vec{f} are returned in corresponding positions 2 through $N + 1$ of FV. The call on FUNCTI is as follows:

```
CALL FUNCTI (N,X,YV,FV).
```

A skeleton FUNCTI subroutine is given in the listings in Appendix A.

III. RESULTS AND CONCLUSIONS

A. The Test Problem

The results presented here are for the test problem of 2-dimensional motion in an inverse square attractive force field using x-y coordinates.

The equations are

$$\frac{dv_x}{dt} = - \frac{\partial}{\partial x} V(x,y)$$

$$\frac{dv_y}{dt} = - \frac{\partial}{\partial y} V(x,y)$$

$$\frac{dx}{dt} = v_x$$

$$\frac{dy}{dt} = v_y$$

where $V(x,y) = - (x^2 + y^2)^{-\frac{1}{2}}$

The initial conditions were chosen to give an elliptical orbit of eccentricity 0.8. In this orbit the error and step size controls will produce several step size changes as the orbit is traversed. The initial conditions are:

$$\text{at } t = 0,$$

$$x = 0.2,$$

$$y = 0,$$

$$v_x = 0,$$

$$v_y = 3.0.$$

One complete orbit was run ($t_{\text{final}} = 2\pi$) and the error taken as the square root of the sum of the squares of the differences between initial and final conditions.

The accuracy range investigated was $\sim 10^{-7}$ to $\sim 10^{-12}$. The UNIVAC 1108 maintains ~ 18 significant figures (decimal) in double precision.

B. Results

Results are presented here for test runs made with the following methods and orders:

Shanks formulas 7-7, 7-9, 8-10 and 8-12 (here the first number gives the order, the second gives the number of function evaluations per step);

Adams method orders 7, 9, 11, 13;

Cowell's method orders 7, 9, 11, 13;

Butcher's formulas orders 5, 7, 9, 11, 13.

All of the multistep methods used Shanks 8-10 for start and restart for all orders. These orders were chosen to give as close as comparison as possible across methods at corresponding orders.

Figure 6 shows what might be expected of the error behavior as a function of number of steps taken to perform a given integration. In the large step-size region (small number of steps), the truncation error dominates and decreases as N^{-n} , where N is the number of steps, and n is the order of the error. In the small step-size (large number of steps), the rounding error should dominate. If rounding errors behave like random variables, one would expect the rounding error to increase as $N^{\frac{1}{2}}$.

Figure 7 shows results of runs made with Shanks' formulas. Plotted here is error vs. number of function evaluations and error vs. computer time to complete the integration. The labelings indicate the order and number of function evaluations per step, respectively. These points lie on the truncation error part of the curve and show the advantage of the higher order methods at high accuracy requirements.

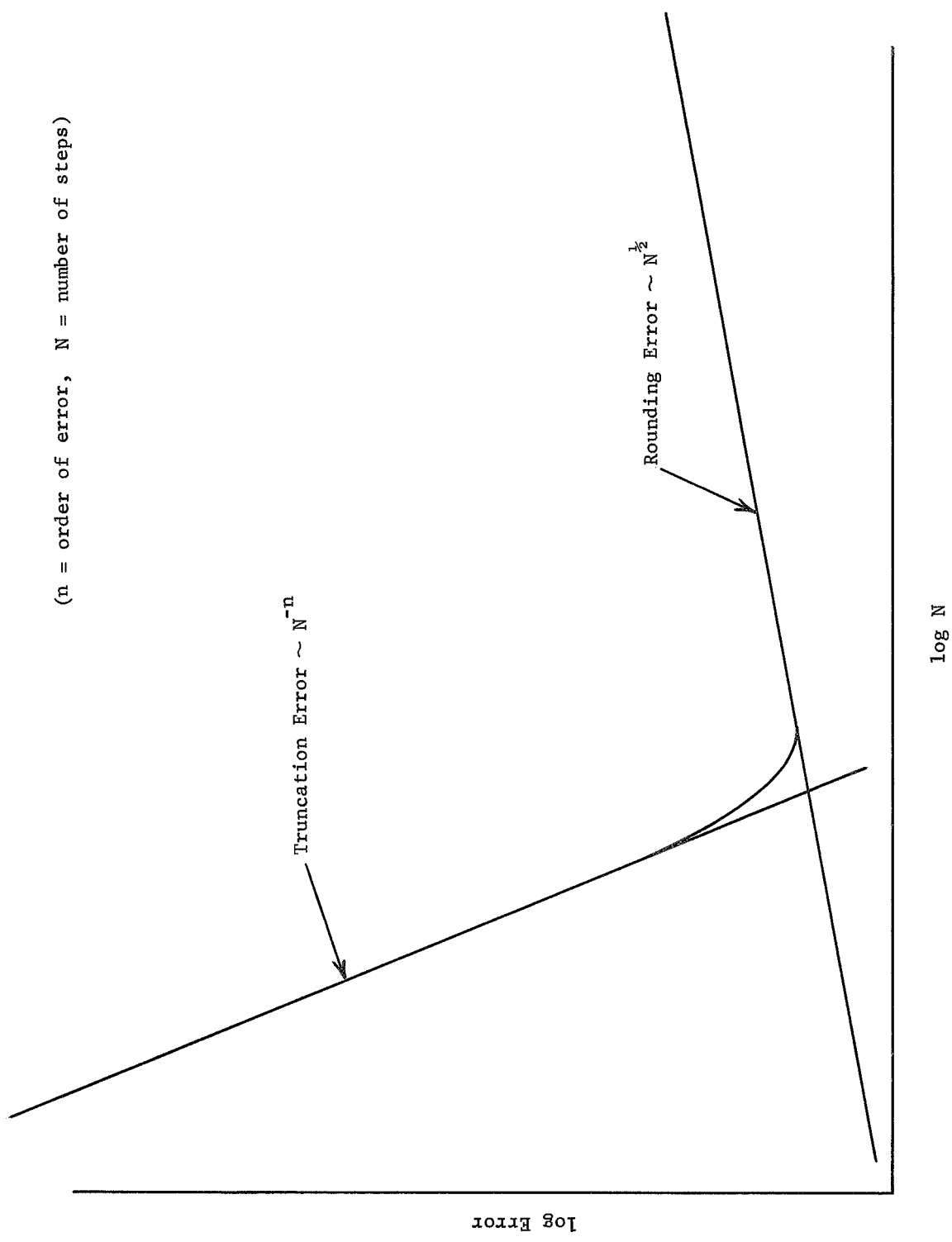


Figure 6. Expected Error Behavior in Numerical Integration of Differential Equations.

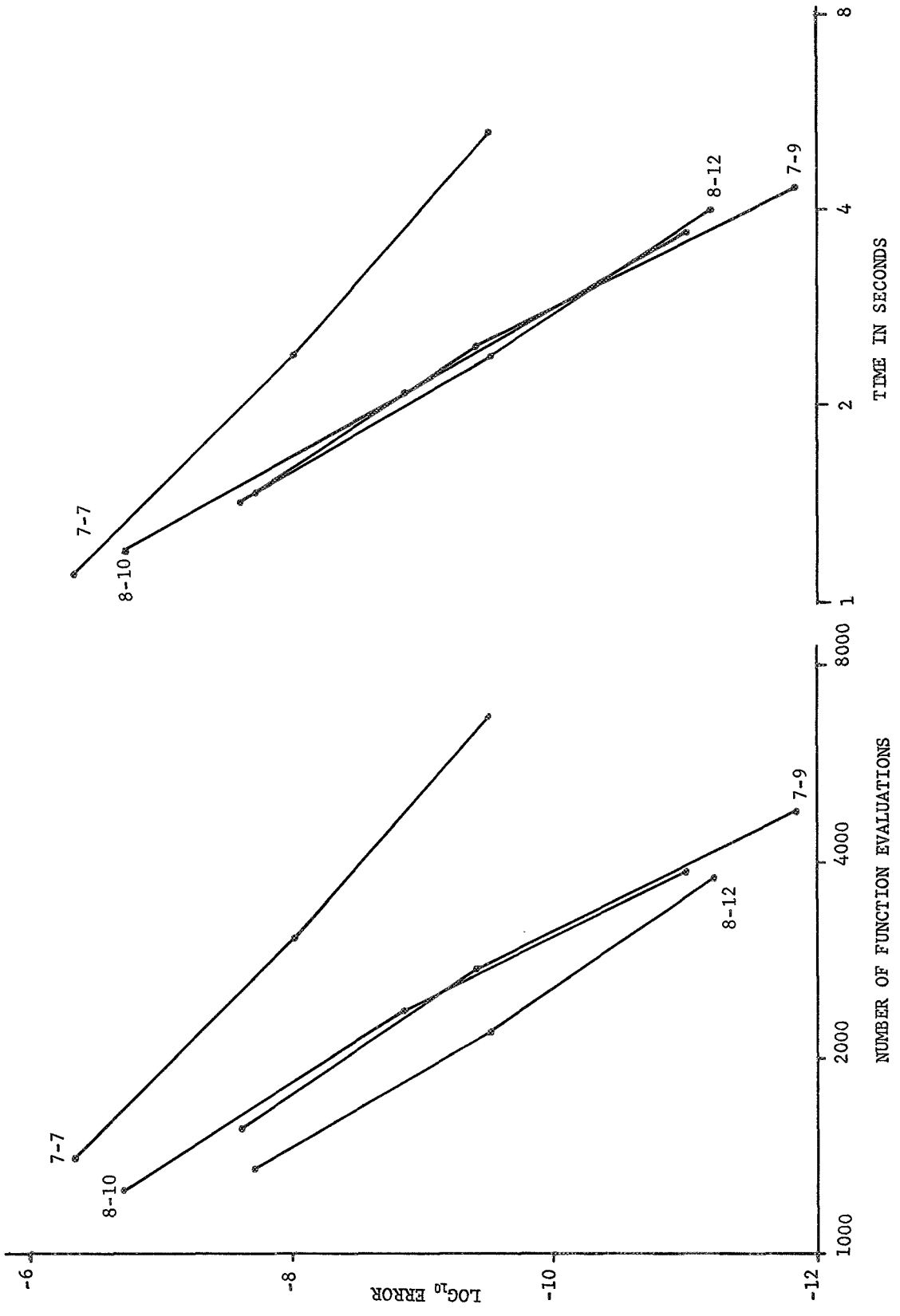


Figure 7. Error Behavior for the Runge-Kutta Formulas of Shanks.

Figure 8 shows results of runs made with Adams' method. Again the plots are of error vs. number of function evaluations and vs. time. Labels indicate order. Again this is the truncation error part of the curve, and one sees that the slopes are steeper for the higher orders.

Figure 9 shows results of runs made with Cowell's method. Both time and number of function evaluations are plotted vs. error, and the labels indicate orders. Here one sees that the region of rounding error domination is being approached or entered by the 13 order formula below errors of 10^{-12} .

Figure 10 shows runs made with Butcher's formulas. Only number of function evaluations (not time) vs. error is plotted; the labels indicate order. Here again we see that the region of rounding error is being approached at errors in the vicinity 10^{-12} .

Figure 11 is a composite plot of the four methods each of order 7. The slopes are seen to be all more or less the same. Butcher's method appears to be better than the others above 10^{-10} but enters the rounding region first.

Figure 12 is also a composite graph of different methods, all of order 13. Again Butcher's formula appears superior in the truncation region but enters the rounding region first.

Figure 13 gives a more detailed examination of Butcher's method (compare with Figure 10). Many more points were taken here, and we see considerable scatter when points are taken close together. This gives a better picture of how the rounding error region is entered by the 7th and 13th orders. The 9th and 11th orders do not exhibit rounding errors as large as those of the 7th and 13th orders.

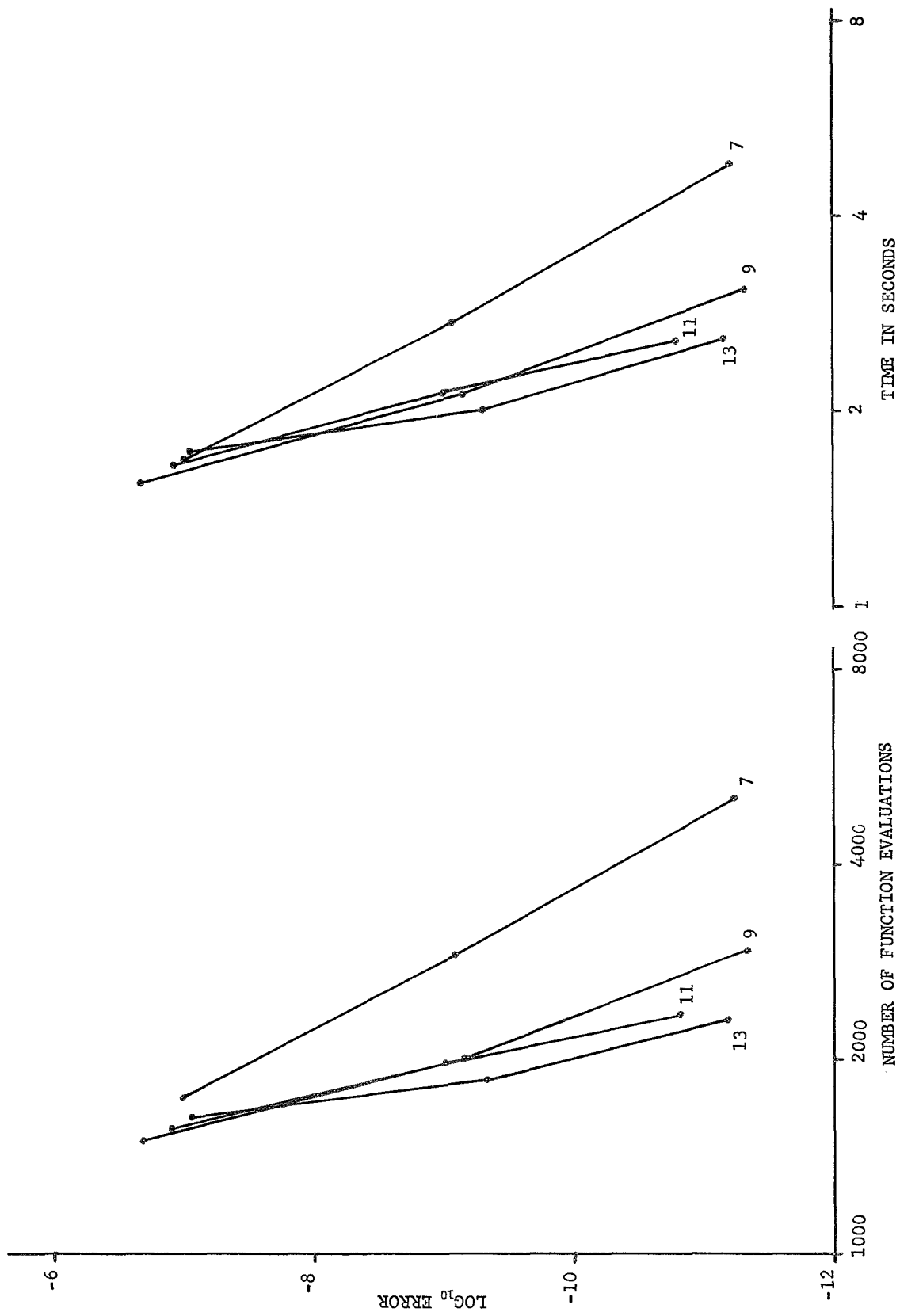


Figure 8. Error Behavior for Adams' Method.

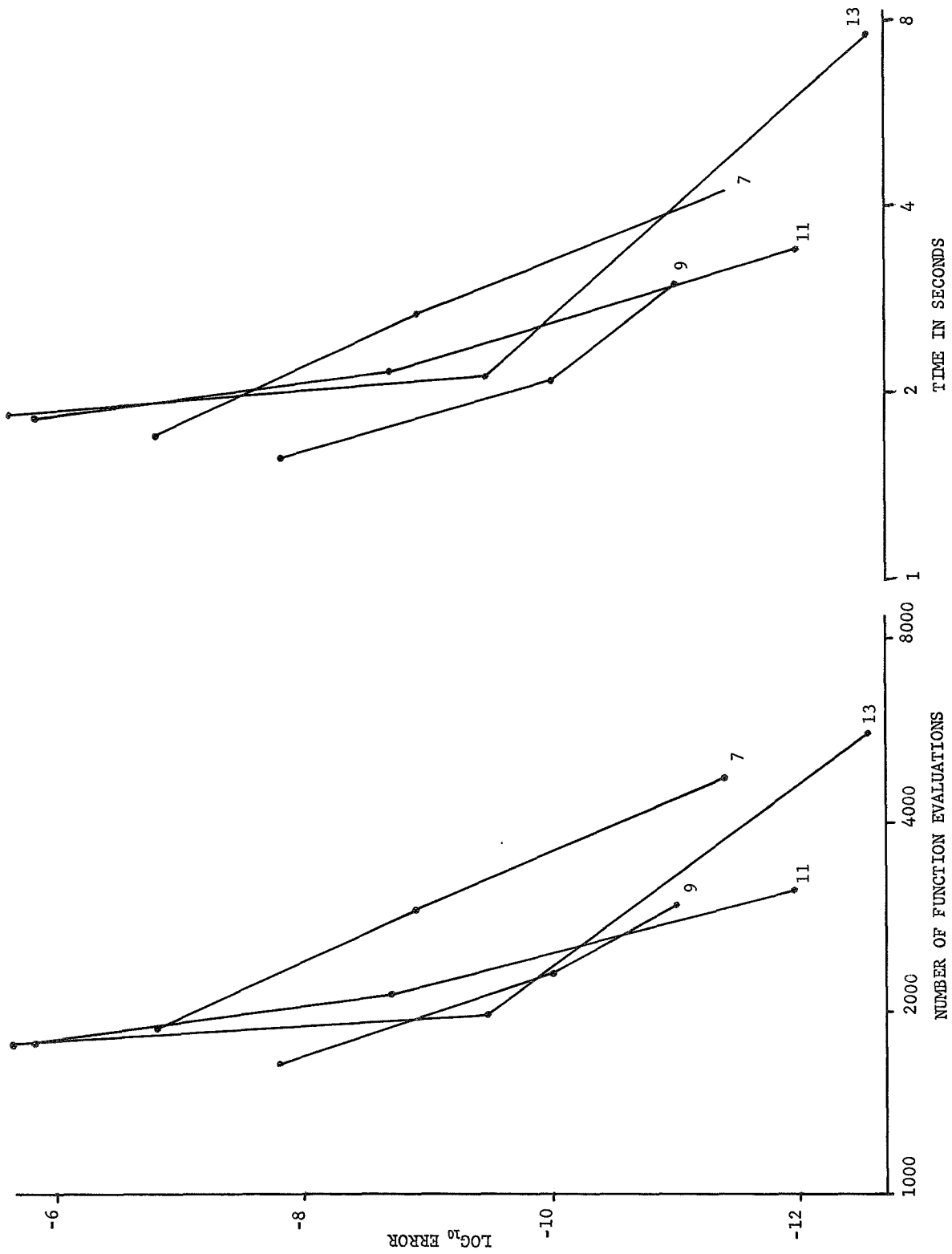


Figure 9. Error Behavior for Cowell's Method.

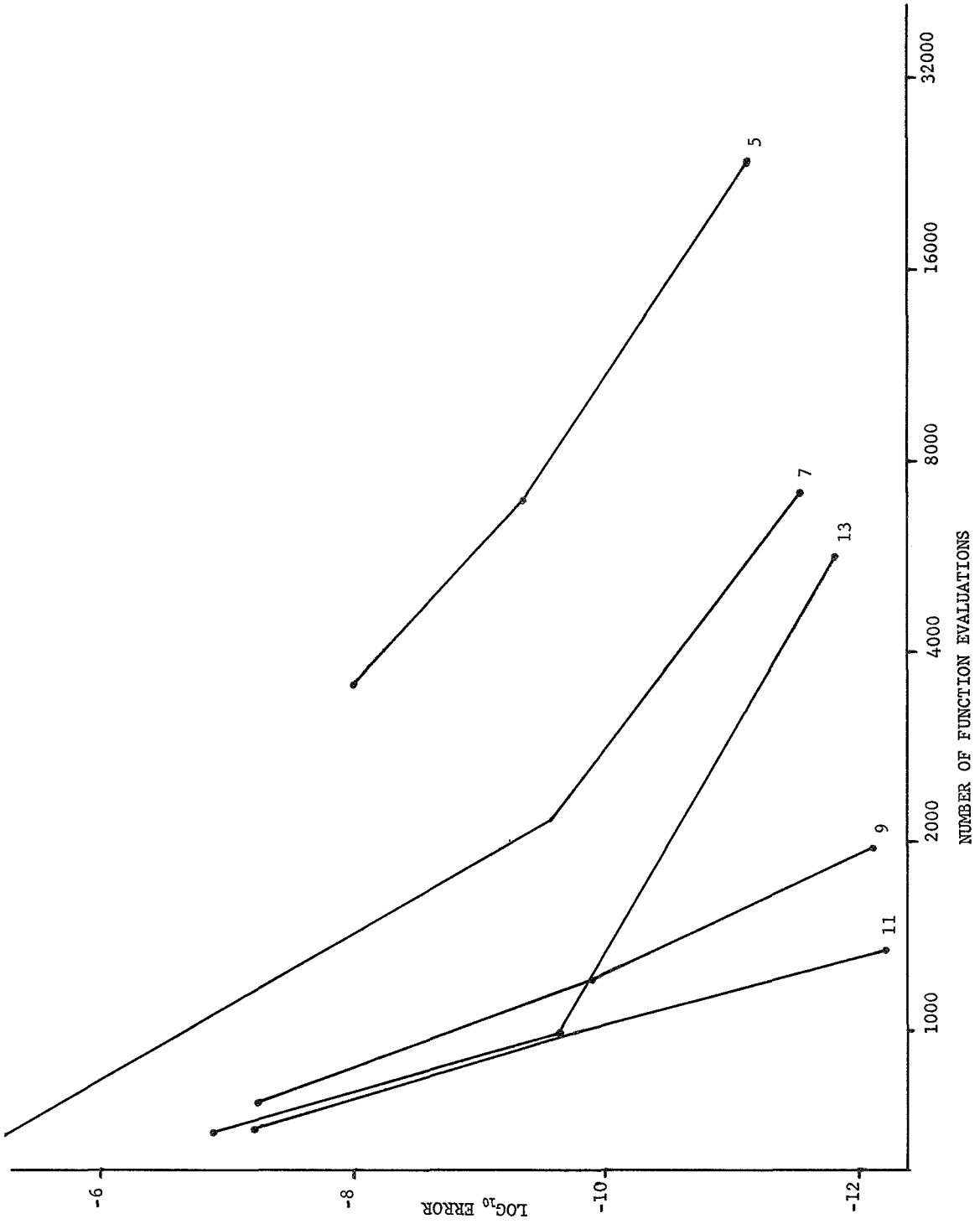


Figure 10. Error Behavior for Butcher's Formulas.

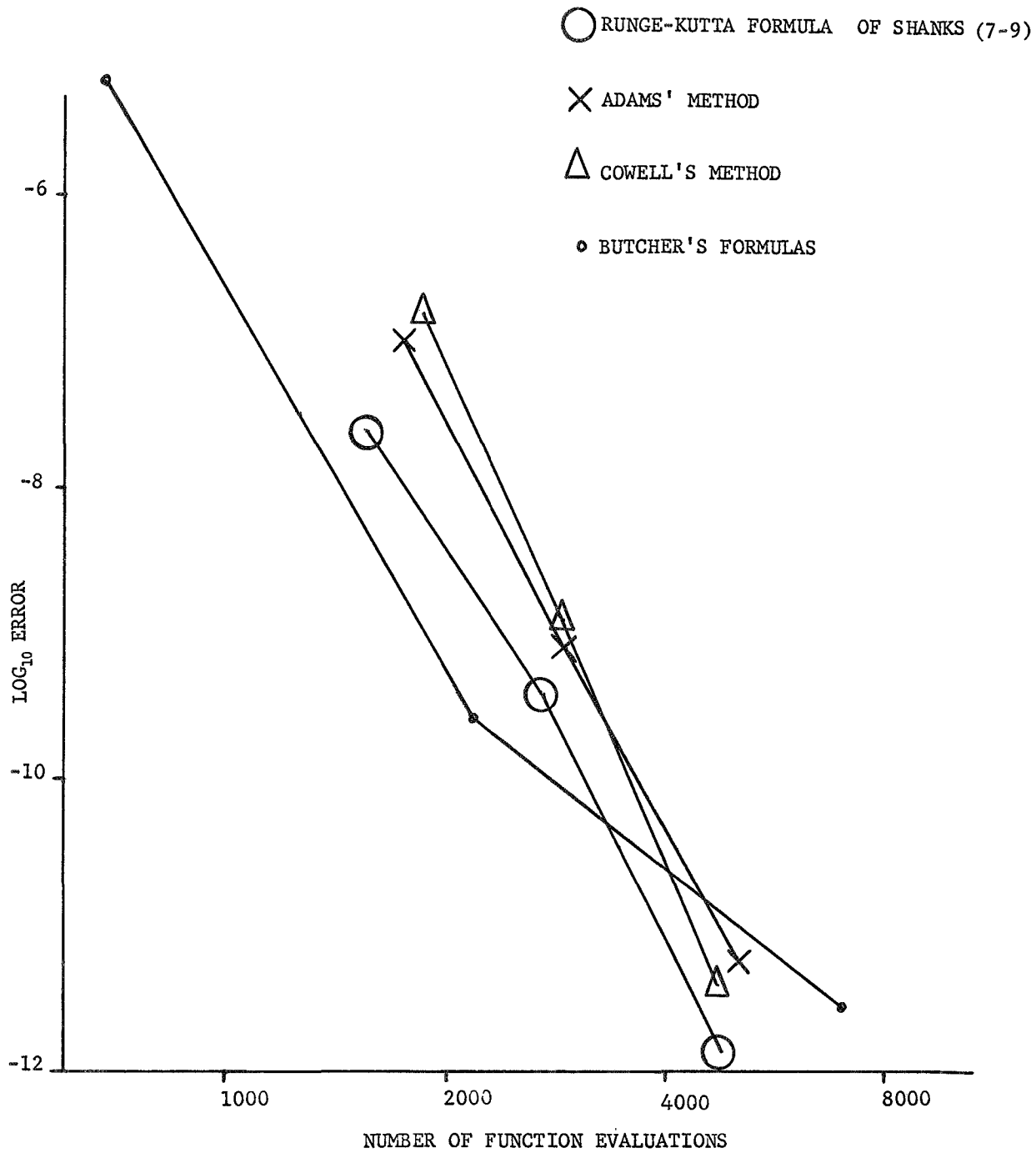


Figure 11. Error Behavior for the 7th Order Formulas.

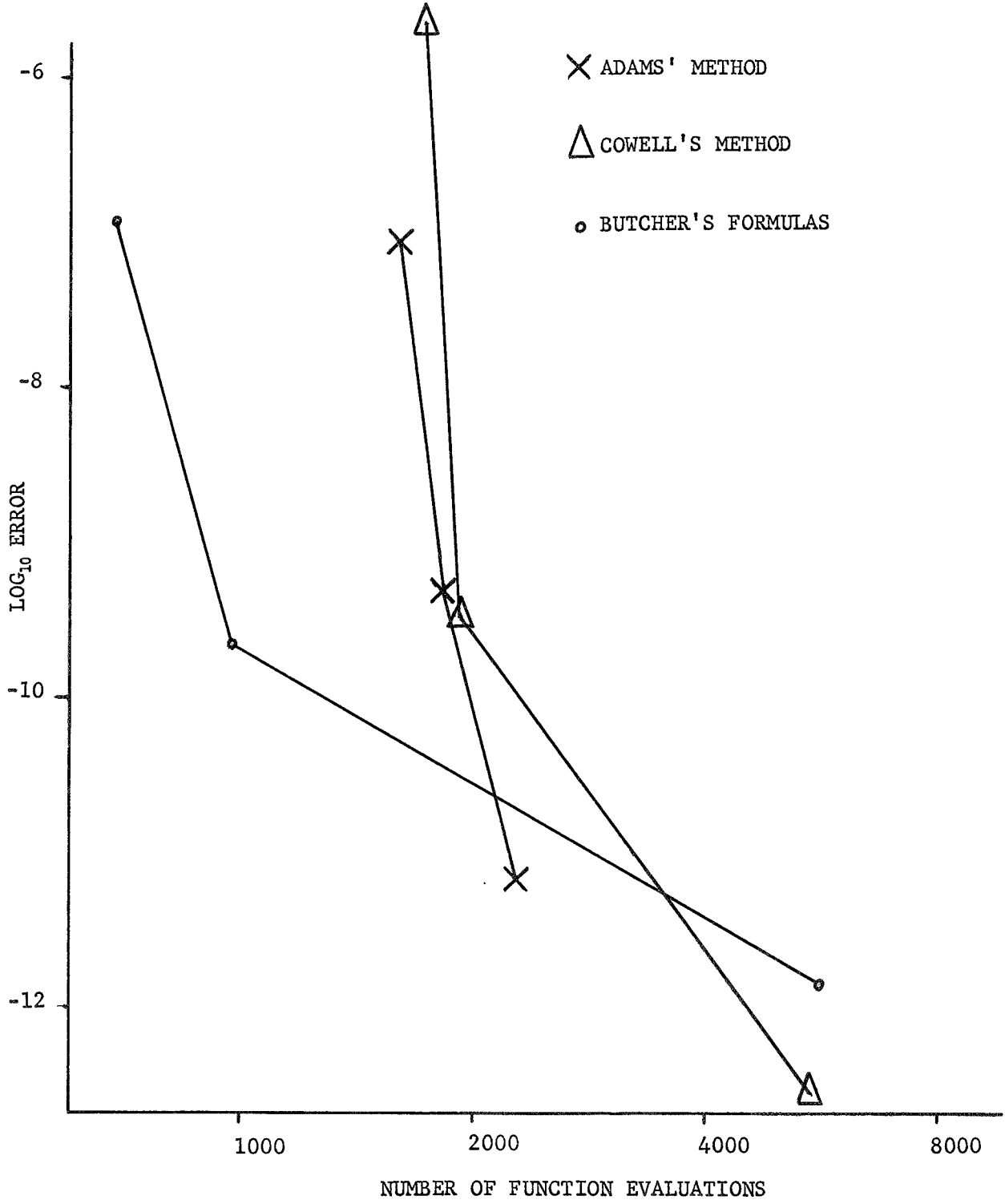


Figure 12. Error Behavior for the 13th Order Formulas.

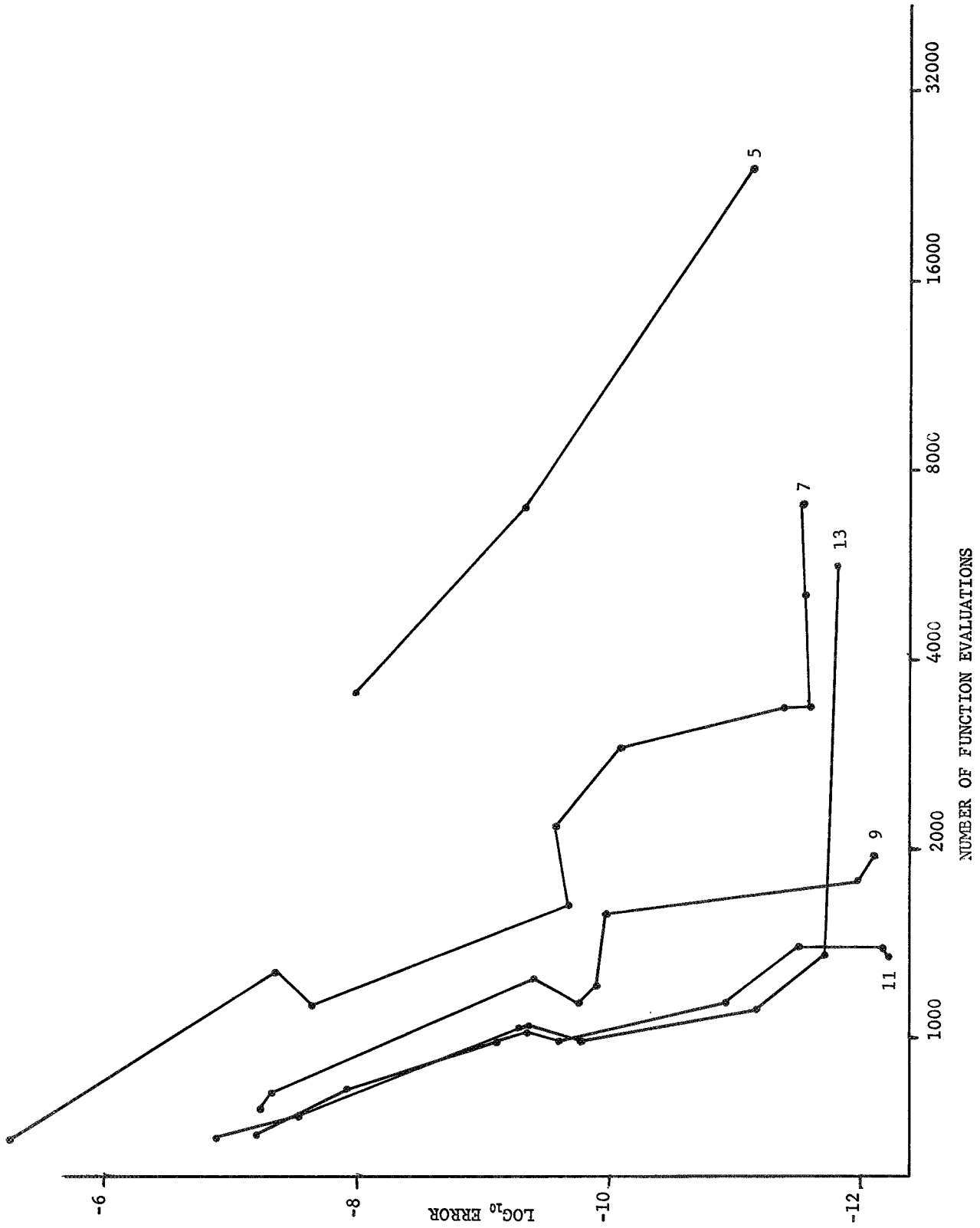


Figure 13. Detail Error Behavior for Butcher's Formulas.

C. Conclusions

From the above results one sees that all of the methods tested are fairly effective. At higher accuracies the higher order methods are more effective than the lower order methods, at least until the round off error region is reached. The region of round off error is determined primarily by the number of significant figures carried by the particular machine but is also somewhat dependent both on the method and order of the integration scheme.

For a fixed order (figure 11, 7th order; figure 12, 13th order) one sees that the Butcher formula is more effective than the others, at least until the rounding region is reached, but apparently Butcher enters the rounding error region sooner (produces larger rounding errors) than the others.

At 7th order the Shanks formula appears somewhat better than either the Cowell or Adams methods. No Shanks formulas of order higher than 8 were available at the time this work was being done, but the results here (figure 7) suggest that higher order Shanks formulas would be effective in reducing the number of function evaluations. Whether higher order Shanks formulas would take less time or not would depend on the application.

Whether number of function evaluations or computer time is more relevant in these tests depends on the application one has in mind. In the test problem used here the function evaluation time was relatively small compared to the rest of the arithmetic for any of the methods. In this case the time measurements show the additional time taken by the added complexity of the higher order methods. For example, Figure 7 shows that, while the number of function evaluations for the Shanks 8-12 formula is less than for the 7-9 or 8-10 formulas, the time taken for each is almost identical. Thus the 8-12 formula

is seen to be more advantageous only if the function evaluations are quite complex and time consuming.

One might also question whether the results for the test problem are representative of the overall behavior of these methods. The error at the end of one complete revolution might not be representative of maximum error over the orbit since error cancelling is known to take place when integrating a periodic system. The absolute error, however, is not the relevant measure here but rather the error of one method relative to another. If error cancelling takes place because of the geometric properties of the orbit, this cancelling should be the same for each method and not affect the validity of comparing the relative performance of the methods. However, one cannot rule out entirely the possibility that other type problems might show a different relative effectiveness of these methods. For example it is known that special highly stable methods out-perform those tested here when applied to very "stiff" equations [27].

D. Suggestions for Further Study

The most obvious need for further study is an examination of the performance of the subroutines for other types of problems, in particular non-orbit type problems.

Other integration formulas should be tested. In particular Shanks has now made available (private communication) a 9-16 formula and a 10-21 formula, (i.e. a 9th order formula with 16 function evaluations per step, and a 10th order with 21 function evaluations per step.) The results here suggest that at high enough accuracies these new high order Shanks formulas might be advantageous.

Gear [27] has published some highly stable methods that are reputed to be especially good when used with very "stiff" equations. Comparisons of the formulas tested here using the stiff equations and comparisons with Gear's methods should be made.

Applications of the methods studied here to the solution of other type problems (non-initial value problems) could be made. In particular these methods can be used to generate the Green's functions needed to solve differential equation problems with split boundary conditions, i.e. rendezvous type orbit problems.

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APPENDIX A
PROGRAM LISTINGS

In this appendix is listed each of the programs described in the body of the report. Also listed here are a skeleton main program and FUNCTI subroutine. The order of the listings is as follows:

1. A skeleton main program
2. The Runge-Kutta-Shanks subroutine SHANKS
3. The Adams subroutine ADAMS
4. The Stetter-Gragg-Butcher subroutine BUTCHR
5. The Cowell subroutine COWELL
6. The starting routine START
7. An auxiliary routine to START called RUNKUT
8. An auxiliary routine to START called COMP
9. A skeleton FUNCTI subroutine

```

GALLAHER-L-J*TPF$.A1167
1 C PROGRAM MAIN
2 C DEFINE FDBLE(I) = DBLE(FLOAT(I))
3 C PARAMETER NP1
4 C COMMON/NN/NN
5 C COMMON/COMMON/FA(35,NP1)
6 C DOUBLE PRECISION FA,X,Y1,Y2,XI1
7 C DIMENSION Y(100),EA(100),ER(100),ADMSCF(91),RKSCFF(91)
8 C X,Y1(100),Y2(100)
9 C DIMENSION BTCHCF(91),CWLLCF(91)
10 C DOUBLE PRECISION EA,ER,Y,ADMSCF,RKSCFF,BTCHCF,CWLLCF
11 C INTEGER A,B,C,Q,O,F
12 C END
13 C BLOCK 2

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@PRT      .SHANKS

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GALLAHER-L-J*TPFS,SHANKS
1 SUBROUTINE SHANKS(N, XIV,XF,YV,IM,ORDER,CF,P,EA,ER,DXV)
2 DOUBLE PRECISION XIV, DXV
3 INTEGER N,M,ORDER
4 DOUBLE PRECISION XI,XF,P,DX
5 DOUBLE PRECISION CF
6 DIMENSION CF(91)
7 DOUBLE PRECISION YV,EA,ER
8 DIMENSION YV(100),EA(100),ER(100)
9 INTEGER I,J,K,L,COUNT,COUNT2,II,NCF
10 INTEGER NCF1
11 INTEGER DKTK
12 DOUBLE PRECISION EFACF
13 DOUBLE PRECISION BETA,DCOUNT,DXD,DXH,DXT,EFACTR,ERANGE,ES,GAMMA,X,
14 1XM
15 LOGICAL CFSW,DSW
16 DOUBLE PRECISION CFD
17 DIMENSION CFD(180)
18 DOUBLE PRECISION FV
19 COMMON/COMMON/FV(35,1)
20 DOUBLE PRECISION TEMP9,GV,YC,YM,YP
21 DIMENSION TEMP9(100),GV(100),YC(100),YM(100),YP(100)
22 INTEGER I11
23 INTEGER STEPR,STEPS
24 DEFINE FDBLE(I) = DBLE(FLOAT(I))
25 ME IM
26 XI = XIV
27 DX = DXV
28 M = M - 1
29 STEPR = 0
30 STEPS = STEPR
31 DXT = XF - XI
32 DXD = DXT
33 IF (DXT .EQ. 0) GO TO 625
34 IF (DX .NE. 0) GO TO 628
35 DX = DXD
36 CONTINUE
37 COUNT = 1
38 IF (ABS(DX) .GE. ABS(DXD)) GO TO 630
39 COUNT = COUNT + COUNT
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01548000
01549000
01550000
01551000
01552000
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DXD = DXT / FDBLE(COUNT)
GO TO 629
630 COUNT2 = COUNT + COUNT
DXH = DXT / FDBLE(COUNT2)
DCOUNT = COUNT
EFACT = 1
I = 1
GO TO 633
634 I = I + 1
633 IF (I .LE. ORDER) GO TO 631
GO TO 632
631 EFACT = EFACT + EFACT
GO TO 634
632 ERANGE = .125 / EFACT
EFACT = 4.000 / EFACT
EFACTR = (COUNT ** P) * EFACT
DKTR = 0
NCF1 = (((M * M) + M) / 2) + M + M
NCF = NCF1 + I
CFSW = .FALSE.
I = 0
GO TO 637
638 I = I + 1
637 IF (I .LE. NCF1) GO TO 635
GO TO 636
635 CFD(I + 1) = CF(I + 1) * DXD
III2 = I + NCF
CFD(III2 + 1) = CF(I + 1) * DXH
GO TO 638
636 X = XI
XM = XI + DXH
623 DSW = .TRUE.
CALL FUNCTI(N, X, YV, GV)
IF (.NOT. CFSW) GO TO 640
L = NCF1
GO TO 639
640 L = - 1
639 I = 1
GO TO 643
644 I = I + 1
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01586000
01587000
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83 01619000
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88 01624000
89 01625000
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91 01627000
92 01628000
93 01629000
94 01630000
95 01631000
96 01632000
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119 01655000

643 IF (I, LE, M) GO TO 641
    GO TO 642
644 I11 = I - 1
    L = L + 1
    BETA = CFD(L + 1)
    K = 1
    GO TO 647
645 K = K + 1
646 IF (K, LE, N) GO TO 645
    GO TO 646
647 YP(K + 1) = (GV(K + 1) * BETA) + YV(K + 1)
    GO TO 648
648 J = 1
    GO TO 651
649 J = J + 1
650 IF (J, LE, I11) GO TO 649
    GO TO 650
651 L = L + 1
    BETA = CFD(L + 1)
    K = 1
    GO TO 655
652 K = K + 1
653 IF (K, LE, N) GO TO 653
    GO TO 654
654 YP(K + 1) = (FV(J + 1, K + 1) * BETA) + YP(K + 1)
    GO TO 656
655 GO TO 652
656 L = L + 1
    CALL FUNCTI(N, CFD(L + 1) + X, YP, TEMP9)
    I11 = 0
    GO TO 659
657 I11 = I11 + 1
658 IF (I11, LE, N) GO TO 657
    GO TO 658
659 FV(I + 1, I11 + 1) = TEMP9(I11 + 1)
    GO TO 660
660 GO TO 644
661 L = L + 1
    GAMMA = CFD(L + 1)
    K = 1

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120 GO TO 663
121 K = K + 1
122 IF (K .LE. N) GO TO 661
123 GO TO 662
124 YP(K + 1) = (GV(K + 1) * GAMMA) + YV(K + 1)
125 GO TO 664
126 I = 1
127 GO TO 667
128 I = I + 1
129 IF (I .LE. M) GO TO 665
130 GO TO 666
131 L = L + 1
132 GAMMA = CFD(L + 1)
133 K = 1
134 GO TO 671
135 K = K + 1
136 IF (K .LE. N) GO TO 669
137 GO TO 670
138 YP(K + 1) = (FV(I + 1, K + 1) * GAMMA) + YP(K + 1)
139 GO TO 672
140 GO TO 668
141 CONTINUE
142 IF (.NOT. CFSW) GO TO 674
143 L = L - 1
144 CONTINUE
145 I = 1
146 GO TO 677
147 I = I + 1
148 IF (I .LE. M) GO TO 675
149 GO TO 676
150 III = I - 1
151 L = L + 1
152 BETA = CFD(L + 1)
153 K = 1
154 GO TO 681
155 K = K + 1
156 IF (K .LE. N) GO TO 679
157 GO TO 680
158 YM(K + 1) = (GV(K + 1) * BETA) + YV(K + 1)
159 GO TO 682
  
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680 J = 1
    GO TO 685
686 J = J + 1
685 IF (J .LE. I11) GO TO 683
    GO TO 684
683 L = L + 1
    BETA = CFD(L + 1)
    K = 1
    GO TO 689
690 K = K + 1
689 IF (K .LE. N) GO TO 687
    GO TO 688
687 YM(K + 1) = (FV(J + 1, K + 1) * BETA) + YM(K + 1)
    GO TO 690
688 GO TO 686
684 L = L + 1
    CALL FUNCTI(N, CFD(L + 1) + X, YM, TEMP9)
    I11 = 0
    GO TO 693
694 I11 = I11 + 1
693 IF (I11 .LE. N) GO TO 691
    GO TO 692
691 FV(I + 1, I11 + 1) = TEMP9(I11 + 1)
    GO TO 694
692 GO TO 678
676 L = L + 1
    GAMMA = CFD(L + 1)
    K = 1
    GO TO 697
698 K = K + 1
697 IF (K .LE. N) GO TO 695
    GO TO 696
695 YM(K + 1) = (GV(K + 1) * GAMMA) + YV(K + 1)
    GO TO 698
696 I = I + 1
    GO TO 701
702 I = I + 1
701 IF (I .LE. M) GO TO 699
    GO TO 700
699 L = L + 1

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GAMMA = CFD(L + 1)
K = 1
GO TO 705
706 K = K + 1
705 IF (K .LE. N) GO TO 703
GO TO 704
703 YM(K + 1) = (FV(I + 1, K + 1) * GAMMA) + YM(K + 1)
GO TO 706
704 GO TO 702
700 CALL FUNCTI(N, XM, YM, TEMP9)
III = 0
GO TO 709
710 III = III + 1
709 IF (III .LE. N) GO TO 707
GO TO 708
707 FV(I, III + 1) = TEMP9(III + 1)
GO TO 710
708 IF (.NOT. CFSW) GO TO 712
L = -1
GO TO 711
712 L = NCF1
711 I = 1
GO TO 715
716 I = I + 1
715 IF (I .LE. M) GO TO 713
GO TO 714
713 III = I - 1
K = 1
GO TO 719
720 K = K + 1
719 IF (K .LE. N) GO TO 717
GO TO 718
717 YC(K + 1) = YM(K + 1)
GO TO 720
718 J = 0
GO TO 723
724 J = J + 1
723 IF (J .LE. III) GO TO 721
GO TO 722
721 L = L + 1

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BETA = CFD(L + 1)
K = 1
GO TO 727
728 K = K + 1
727 IF (K .LE. N) GO TO 725
GO TO 726
725 YC(K + 1) = (FV(J + 1, K + 1) * BETA) + YC(K + 1)
GO TO 728
726 GO TO 724
722 L = L + 1
CALL FUNCT1(N, CFD(L + 1) + XM, YC, TEMP9)
III = 0
GO TO 731
732 III = III + 1
731 IF (III .LE. N) GO TO 729
GO TO 730
729 FV(I + 1, III + 1) = TEMP9(III + 1)
GO TO 732
730 GO TO 716
714 K = 1
GO TO 735
736 K = K + 1
735 IF (K .LE. N) GO TO 733
GO TO 734
733 YC(K + 1) = YM(K + 1)
GO TO 736
734 I = 0
GO TO 739
740 I = I + 1
739 IF (I .LE. M) GO TO 737
GO TO 738
737 L = L + 1
GAMMA = CFD(L + 1)
K = 1
GO TO 743
744 K = K + 1
743 IF (K .LE. N) GO TO 741
GO TO 742
741 YC(K + 1) = (FV(I + 1, K + 1) * GAMMA) + YC(K + 1)
GO TO 744
  
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742 GO TO 740
738 K = 1
    GO TO 747
748 K = K + 1
747 IF (K .LE. N) GO TO 745
    GO TO 746
745 ES = ABS(YC(K + 1) - YP(K + 1)) * EFACTR
    IF (ES .EQ. 0) GO TO 750
    IF (ES .LT. EA(K + 1)) GO TO 752
    IF (ES .LT. ABS(YC(K + 1)) * ER(K + 1)) GO TO 753
    DSW = .FALSE.
    STEPR = STEPR + 1
    COUNT = COUNT2
    COUNT2 = COUNT + COUNT
    DCOUNT = DCOUNT + DCOUNT
    DXD = DXH
    DXH = DXT / FDBLE(COUNT2)
    EFACTR = (COUNT ** P) * EFACT
    IF (.NOT. CFSW) GO TO 755
    I = 0
    GO TO 758
759 I = I + 1
758 IF (I .LE. NCF1) GO TO 756
    GO TO 757
756 III3 = I + NCF
    CFD(III3 + 1) = CF(I + 1) * DXH
    GO TO 759
757 CFSW = .FALSE.
    GO TO 754
755 I = 0
    GO TO 762
763 I = I + 1
762 IF (I .LE. NCF1) GO TO 760
    GO TO 761
760 CFD(I + 1) = CF(I + 1) * DXH
    GO TO 763
761 CFSW = .TRUE.
754 XM = (((FDBLE(COUNT2 + 1)) - DCOUNT) * DXH) + XI
    K = 1
    GO TO 766

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320 K = K + 1
321 IF (K .LE. N) GO TO 764
322 GO TO 765
323 YP(K + 1) = YM(K + 1)
324 GO TO 767
325 GO TO 624
326 CONTINUE
327 CONTINUE
328 IF (.NOT. DSW) GO TO 769
329 IF (ES .LT. EA(K + 1) * ERANGE) GO TO 770
330 IF (ES .LT. (ABS(YC(K + 1)) * ER(K + 1)) * ERANGE) GO TO 771
331 DSW = .FALSE.
332 CONTINUE
333 CONTINUE
334 CONTINUE
335 CONTINUE
336 CONTINUE
337 GO TO 748
338 DCOUNT = DCOUNT - 1.000
339 STEPS = STEPS + 1
340 K = 1
341 GO TO 774
342 K = K + 1
343 IF (K .LE. N) GO TO 772
344 GO TO 773
345 YV(K + 1) = YC(K + 1)
346 GO TO 775
347 IF (DCOUNT .EQ. 0) GO TO 625
348 X = ((FDBLE(COUNT) - DCOUNT) * DXD) + XI
349 IF (DCOUNT .GE. 2) GO TO 778
350 IF (DCOUNT .NE. 1) GO TO 780
351 DSW = .FALSE.
352 CONTINUE
353 IF ((DCOUNT .GE. 1) .AND. .NOT. DSW) GO TO 782
354 IF (DCOUNT .LE. 1) GO TO 784
355 DKTR = DKTR + 1
356 CONTINUE
357 DCOUNT = 1
358 COUNT = DCOUNT + .5
359 COUNT2 = 2

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EFACTR = EFACT  
XI = X  
DXT = XF - XI  
DXD = DXT  
DXH = DXD / 2.000  
XM = XI + DXH  
CFSW = .FALSE.  
I = 0  
GO TO 787  
788 I = I + 1  
787 IF (I .LE. NCF1) GO TO 785  
GO TO 786  
785 CFD(I + 1) = CF(I + 1) * DXD  
III2 = I + NCF  
CFD(III2 + 1) = CF(I + 1) * DXH  
GO TO 788  
786 GO TO 623  
782 CONTINUE  
781 CONTINUE  
778 CONTINUE  
777 IF (.NOT. DSW) GO TO 790  
DKTR = DKTR + 1  
COUNT2 = COUNT  
COUNT = COUNT / 2  
DCOUNT = DCOUNT / 2.000  
DXH = DXD  
DXD = DXT / FDBLE(COUNT)  
EFACTR = (COUNT ** P) * EFACT  
IF (.NOT. CFSW) GO TO 792  
I = 0  
GO TO 795  
796 I = I + 1  
795 IF (I .LE. NCF1) GO TO 793  
GO TO 794  
793 CFD(I + 1) = CF(I + 1) * DXD  
GO TO 796  
794 CFSW = .FALSE.  
GO TO 791  
792 I = 0  
GO TO 799
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800 I = I + 1
799 IF (I .LE. NCF1) GO TO 797
    GO TO 798
797 III2 = I + NCF
    CFD(III2 + 1) = CF(I + 1) * DXD
    GO TO 800
798 CFSW = .TRUE.
791 CONTINUE
790 CONTINUE
789 XM = (((FDBLE(COUNT2 + 1)) - DCOUNT) * DXH) + XI
    GO TO 623
625 CONTINUE
    RETURN
    END
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@PRT

•ADAMS

GALLAHER-L-J*TPF\$.ADAMS
 1 SUBROUTINE ADAMS(N, XI, XF, Y, P, Q, DXV, EA, ER, ADMSCF, RKSFNS,

```

2 1RXSRDR, RKSCFF)
3  DOUBLE PRECISION DXV
4  COMMON/COMMON/FH(35,1)
5  DOUBLE PRECISION XI, XF, P, DX
6  INTEGER N, Q, RKSFNS, RKSRDR
7  DOUBLE PRECISION Y, EA, ER
8  DIMENSION Y(100), EA(100), ER(100)
9  DOUBLE PRECISION ADMSCF
10 DIMENSION ADMSCF(39)
11 DOUBLE PRECISION RKSCFF
12 DIMENSION RKSCFF(91)
13 INTEGER I1
14 DOUBLE PRECISION FH
15 DOUBLE PRECISION B, BS, HB, HBS
16 DIMENSION B(16), BS(16), HB(16), HBS(16)
17 DOUBLE PRECISION TEMP9, C, YP, YC, YD, FP, FC, EAU, EAL, ERU, ERL, HAL, HRL
18 DIMENSION TEMP9(100), C(100), YP(100), YC(100), YD(100), FP(100), FC(100)
19 1), EAU(100), EAL(100), ERU(100), ERL(100), HAL(100), HRL(100)
20 DOUBLE PRECISION H, X, CU, C2, GR, YCI, BSQZ, FHJI, FMUI, HBMU, MIDP, HBSMU,
21 1HBSQZ, ERROR, CHANGE, C2MQP5, INTRVL
22 INTEGER I, J, K, CL, DC, PC, MU, MULT, JZERO, QT2M1, QMINS1, QTIMS2
23 LOGICAL B600D, FLIPPED, TOSMLL
24 DEFINE FDBLE(I) = DBLE(FLOAT(I))
25 DX = DXV
26 C2MQP5 = 1.000 / (FDBLE(2 ** (Q + 5)))
27 QMINS1 = Q - 1
28 QTIMS2 = Q + Q
29 QT2M1 = QTIMS2 - 1
30 MU = 0
31 GO TO 204
32 MU = MU + 1
33 IF (MU .LE. QMINS1) GO TO 202
34 GO TO 203
35 B(MU + 1) = ADMSCF(MU + 1)
36 I1I2 = MU + Q
37 BS(MU + 1) = ADMSCF(I1I2 + 1)
38 GO TO 205
39 203 BSQZ = ADMSCF(QTIMS2 + 1)

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40 GR = ADMSCF(QTIMS2 + 2)
41 C1 = 1
42 INTRVL = XF - XI
43 H = INTRVL
44 DX = ABS(DX)
45 206 IF ((ABS(H) .LE. DX) .AND. C1 .GE. Q) GO TO 207
46 C1 = C1 + C1
47 H = INTRVL / FDBLE(C1)
48 GO TO 206
49 207 C2 = FDBLE(C1)
50 J = 0
51 JZERO = J
52 CALL FUNCTI(N, XI, Y, TEMP9)
53 II = 0
54 GO TO 210
55 211 II = II + 1
56 210 IF (II .LE. N) GO TO 208
57 GO TO 209
58 208 FH(1, II + 1) = TEMP9(II + 1)
59 GO TO 211
60 209 X = XI
61 I = 1
62 GO TO 214
63 I = I + 1
64 214 IF (I .LE. N) GO TO 212
65 GO TO 213
66 212 Y(I + 1) = Y(I + 1)
67 GO TO 215
68 213 BGOOD = .TRUE.
69 194 IF (BGOOD) GO TO 217
70 I = 1
71 GO TO 220
72 I = I + 1
73 220 IF (I .LE. N) GO TO 218
74 GO TO 219
75 218 Y(I + 1) = YD(I + 1)
76 GO TO 221
77 CONTINUE
78 217 CONTINUE
79 216 X = XF - (INTRVL * (C2 / FDBLE(C1)))
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80      MULT = START(N, XI, XF, C1, EA, ER, QMINS1, X, Y, FH, Y, J,
81      1QT2M1, O, P, RKSFNS, RKSCFF)
82      I = 1
83      GO TO 224
84      I = I + 1
85      IF (I .LE. N) GO TO 222
86      GO TO 223
87      YP(I + 1) = Y(I + 1)
88      C(I + 1) = YP(I + 1)
89      GO TO 225
90      BGOOD = .TRUE.
91      C1 = C1 * MULT
92      C2 = (C2 * FDBLE(MULT)) - FDBLE(Q)
93      J = JZERO - 1
94      IF (J .GE. 0) GO TO 227
95      J = J + QT2M1
96      CONTINUE
97      DC = 0
98      PC = Q
99      CU = (C1 ** (- P)) * GR
100     H = INTRVL / FDBLE(C1)
101     MU = 0
102     GO TO 230
103     MU = MU + 1
104     IF (MU .LE. QMINS1) GO TO 228
105     GO TO 229
106     HB(MU + 1) = B(MU + 1) * H
107     HBS(MU + 1) = BS(MU + 1) * H
108     GO TO 231
109     HBSQZ = BSQZ * H
110     I = 1
111     GO TO 234
112     I = I + 1
113     IF (I .LE. N) GO TO 232
114     GO TO 233
115     EAU(I + 1) = EA(I + 1) * CU
116     EAL(I + 1) = EAU(I + 1) * C2MQP5
117     ERU(I + 1) = ER(I + 1) * CU
118     ERL(I + 1) = ERU(I + 1) * C2MQP5
119     HAL(I + 1) = ABS(EAL(I + 1) / HBSQZ)
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120 HRL(I + 1) = ABS(ERL(I + 1) / HBSQZ)
121 GO TO 235
122 CONTINUE
123 233 CONTINUE
124 195 X = XF - (C2 * H)
125 MU = 0
126 GO TO 238
127 239 MU = MU + 1
128 238 IF (MU .LE. QMIN51) GO TO 236
129 GO TO 237
130 236 J = J + 1
131 IF (J .NE. QT2M1) GO TO 241
132 J = 0
133 241 CONTINUE
134 240 HBMU = HB(MU + 1)
135 HBSMU = HBS(MU + 1)
136 I = 1
137 GO TO 244
138 245 I = I + 1
139 244 IF (I .LE. N) GO TO 242
140 GO TO 243
141 242 FMUI = FH(J + 1, I + 1)
142 YP(I + 1) = (FMUI * HBMU) + YP(I + 1)
143 C(I + 1) = (HBSMU * FMUI) + C(I + 1)
144 GO TO 245
145 243 GO TO 239
146 237 CALL FUNCTI(N, X, YP, FP)
147 196 I = 1
148 GO TO 248
149 249 I = I + 1
150 248 IF (I .LE. N) GO TO 246
151 GO TO 247
152 246 YC(I + 1) = (FP(I + 1) * HBSQZ) + C(I + 1)
153 GO TO 249
154 247 CALL FUNCTI(N, X, YC, FC)
155 I = 1
156 GO TO 252
157 253 I = I + 1
158 252 IF (I .LE. N) GO TO 250
159 GO TO 251
250 CHANGE = ABS(FC(I + 1) - FP(I + 1))

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160 IF (CHANGE .LE. HAL(I + 1)) GO TO 255
161 IF (CHANGE .GT. ABS(HRL(I + 1) * FC(I + 1))) GO TO 197
162
163 255 CONTINUE
164 254 GO TO 253
165 251 FLIPPD = .TRUE.
166 GO TO 198
167 I = 1
168 GO TO 258
169 I = I + 1
170 258 IF (I .LE. N) GO TO 256
171 GO TO 257
172 256 YC(I + 1) = (FC(I + 1) * HBSQZ) + C(I + 1)
173 GO TO 259
174 CALL FUNCTI(N, X, YC, FP)
175 I = 1
176 GO TO 262
177 I = I + 1
178 262 IF (I .LE. N) GO TO 260
179 GO TO 261
180 260 CHANGE = ABS(FP(I + 1) - FC(I + 1))
181 IF (CHANGE .LE. HAL(I + 1)) GO TO 265
182 IF (CHANGE .GT. ABS(HRL(I + 1) * FP(I + 1))) GO TO 196
183
184 265 CONTINUE
185 264 GO TO 263
186 261 FLIPPD = .FALSE.
187 J = J + 1
188 IF (J .NE. QT2M1) GO TO 267
189 J = 0
190 267 CONTINUE
191 266 TOSMLL = .TRUE.
192 I = 1
193 GO TO 270
194 I = I + 1
195 270 IF (I .LE. N) GO TO 268
196 GO TO 269
197 268 IF (.NOT. FLIPPD) GO TO 273
198 FH(J + 1, I + 1) = FC(I + 1)
199 GO TO 272
200 FH(J + 1, I + 1) = FP(I + 1)
201 FH(J + 1, I + 1) = FH(J + 1, I + 1)

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200 YCI= FHJI * HBSQZ + C(I+I)
201 ERROR = ABS(YP(I+1) - YCI)
202 C (I+1) = YCI
203 YP(I+1) = YCI
204 IF ( .NOT. BGOOD) GO TO 275
205 YD(I + 1) = YCI
206 GO TO 274
207
208 275 Y(I + 1) = YCI
209 274 YCI = ABS(YCI)
210 IF (ERROR .LE. EAU(I + 1)) GO TO 277
211 IF (ERROR .GT. ERU(I + 1) * YCI) GO TO 200
212 CONTINUE
213 276 IF (ERROR .LE. EAL(I + 1)) GO TO 279
214 IF (ERROR .LE. ERL(I + 1) * YCI) GO TO 280
215 TOSMLL = .FALSE.
216 CONTINUE
217 280 CONTINUE
218 279 CONTINUE
219 278 GO TO 271
220 269 PC = PC + 1
221 IF ( .NOT. BGOOD) GO TO 282
222 BGOOD = .FALSE.
223 GO TO 281
224 282 BGOOD = .TRUE.
225 281 IF (C2 .LT. 1) GO TO 284
226 C2 = C2 - 1.0D0
227 GO TO 283
228 284 GO TO 201
229 283 IF ( .NOT. TOSMLL) GO TO 286
230 DC = DC + 1
231 IF (DC .LT. 3) GO TO 288
232 IF (PC .LT. QT2M1) GO TO 289
233 IF (C2 .GE. 1) GO TO 199
234 CONTINUE
235 289 CONTINUE
236 288 CONTINUE
237 287 J = JZERO
238 JZERO = J + 1
239 IF (JZERO .NE. QT2M1) GO TO 291
240 JZERO = 0
241 CONTINUE
242 291 CONTINUE
243 290 GO TO 195

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286 CONTINUE
285 DC = 0
J = JZERO
JZERO = J + 1
IF (JZERO .NE. QT2M1) GO TO 293
JZERO = 0
293 CONTINUE
292 GO TO 195
199 C1 = C1 / 2
C2 = (C2 - 1.000) / 2.000
DC = 0
PC = Q
CU = (C1 ** (- P)) * GR
H = INTRVL / FDBLE(C1)
MU = 0
GO TO 296
297 MU = MU + 1
296 IF (MU .LE. QMINS1) GO TO 294
GO TO 295
294 HB(MU + 1) = B(MU + 1) * H
HBS(MU + 1) = BS(MU + 1) * H
GO TO 297
295 HBSQZ = BSQZ * H
I = 1
GO TO 300
301 I = I + 1
300 IF (I .LE. N) GO TO 298
298 EAU(I + 1) = EAU(I + 1) * CU
EAL(I + 1) = EAU(I + 1) * C2MQP5
ERU(I + 1) = ER(I + 1) * CU
ERL(I + 1) = ERU(I + 1) * C2MQP5
HAL(I + 1) = ABS(EAL(I + 1) / HBSQZ)
HRL(I + 1) = ABS(ERL(I + 1) / HBSQZ)
GO TO 301
299 K = J
MU = 1
GO TO 304
305 MU = MU + 1
304 IF (MU .LE. QMINS1) GO TO 302

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60 TO 303
 J = J - 1
 IF (J .GE. 0) GO TO 307
 J = J + QT2M1
 307 CONTINUE
 K = K - 2
 IF (K .GE. 0) GO TO 309
 K = K + QT2M1
 309 CONTINUE
 I = I
 60 TO 312
 I = I + 1
 IF (I .LE. N) GO TO 310
 60 TO 311
 I + 1) = FH(K + 1, I + 1)
 60 TO 313
 60 TO 305
 JZERO = J
 J = JZERO - 1
 IF (J .GE. 0) GO TO 315
 J = J + QT2M1
 315 CONTINUE
 60 TO 195
 J = J - 1
 IF (J .GE. 0) GO TO 317
 J = J + QT2M1
 317 CONTINUE
 JZERO = J
 C1 = C1 + C1
 C2 = (C2 + C2) + 2.0D0
 IF (C2 .LT. Q) GO TO 201
 60 TO 194
 IF (FLIPPD) GO TO 320
 I = I
 60 TO 323
 I = I + 1
 IF (I .LE. N) GO TO 321
 60 TO 322
 FC(I + 1) = FP(I + 1)
 60 TO 324

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320 CONTINUE
321 CONTINUE
322 CONTINUE
323 CONTINUE
324 CONTINUE
325 CONTINUE
326 CONTINUE
327 CONTINUE
328 CONTINUE
329 CONTINUE
330 CONTINUE
331 CONTINUE
332 CONTINUE
333 CONTINUE
334 CONTINUE
335 CONTINUE
336 CONTINUE
337 CONTINUE
338 CONTINUE
339 CONTINUE

322 CONTINUE
320 CONTINUE
319 IF (BG00D) GO TO 326
   I = 1
   GO TO 329
330 I = I + 1
329 IF (I .LE. N) GO TO 327
   GO TO 328
327 Y(I + 1) = YD(I + 1)
   GO TO 330
328 CONTINUE
326 CONTINUE
325 X = XF - (INTRVL * (C2 / FUBLE(C1)))
   IF (C2 .EQ. 0) GO TO 332
   CALL SHANKS(N, X, XF, Y, RKSFNS, RKSRDR, RKSCFF, P, EA, ER, XF -
1)
332 CONTINUE
   RETURN
   END
C 334 BLOCK 8

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@PRT .BUTCHR


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GALLAHER-L-J*TPF$.BUTCHR
1 SUBROUTINE BUTCHR(N, XI, XF, K, EA, ER, DXV, CON, EX, RKC, YIV,
2 1RKSNF, RKSODR)
3 DOUBLE PRECISION DXV
4 COMMON/COMMON/F
5 DOUBLE PRECISION YIV,EA,ER
6 DIMENSION YIV(100),EA(100),ER(100)
7 INTEGER RKSNF,RKSODR
8 INTEGER N,K
9 DOUBLE PRECISION XI,XF,DX,EX
10 DOUBLE PRECISION RKC
11 DIMENSION RKC(91)
12 DOUBLE PRECISION CON
13 DIMENSION CON(37)
14 DOUBLE PRECISION Y,F
15 DIMENSION Y(35,1),F(35, 1)
16 DOUBLE PRECISION SC1,X
17 DOUBLE PRECISION DX2
18 DOUBLE PRECISION DX1,COA,COB,COLA,COLB,COGA,COGB,TEST,TEMPY,TEMPF,
19 1A1,A2,A3,C2
20 INTEGER I,J,CYL,INDEX,C1,M
21 INTEGER CYL3
22 DOUBLE PRECISION SUMYIP,SUMYP,SUMYC,FV1
23 DIMENSION SUMYIP(100),SUMYP(100),SUMYC(100),FV1(100)
24 DOUBLE PRECISION P2,T1,T2
25 INTEGER COUNT,TOTCNT,CYL1,CYL2,M1
26 DOUBLE PRECISION COO
27 DIMENSION COO(19)
28 INTEGER CYO
29 INTEGER COUNTR
30 INTEGER KM1,K6,K61,K62
31 DOUBLE PRECISION OMT
32 DOUBLE PRECISION INTV
33 INTEGER KM3,J2,J3,J6
34 DOUBLE PRECISION XDXT,XDX
35 DOUBLE PRECISION RE,AE
36 DIMENSION RE(100),AE(100)
37 DOUBLE PRECISION TEMP7,TEMP9
38 DIMENSION TEMP7(100),TEMP9(100)
39 INTEGER I1
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40 DEFINE FDBLE(I) = DBLE(FLOAT(I))
41 EQUIVALENCE(F(18,1), Y(1, 1))
42 DX = DXV
43 I = 1
44 GO TO 343
45 I = I + 1
46 344 IF (I .LE. N) GO TO 341
47 343 GO TO 342
48 341 Y(1, I + 1) = YIV(I + 1)
49 GO TO 344
50 342 IF ((K .NE. 1) .AND. K .NE. 2) .AND. K .NE. 3) GO TO 346
51 OMT = .5
52 GO TO 345
53 346 OMT = 2.000 / 3.000
54 345 K6 = 6 * K
55 K61 = (6 * K) + 1
56 K62 = (6 * K) + 2
57 KM1 = K - 1
58 INTV = XF - XI
59 X = XI
60 C1 = 1
61 347 IF ((C1 .GE. K + 1) .AND. ABS(INTV) / FDBLE(C1) .LE. ABS(DX)) GO
62 1TO 348
63 C1 = C1 + C1
64 GO TO 347
65 C2 = C1
66 P2 = 1.000 / (FDBLE(2 ** ((2 * K) + 4)))
67 CYL = 0
68 CYO = 0
69 TOTCNT = 0
70 II = 0
71 GO TO 351
72 II = II + 1
73 351 IF (II .LE. N) GO TO 349
74 GO TO 350
75 349 TEMP7(II + 1) = Y(1, II + 1)
76 GO TO 352
77 350 CALL FUNCTI(N, XI, TEMP7, TEMP9)
78 II = 0
79 GO TO 355

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356 II = II + 1
355 IF (II .LE. N) GO TO 353
GO TO 354
353 F(1, II + 1) = TEMP9(II + 1)
GO TO 356
354 CONTINUE
338 COUNTR = KML
I = START(N, XI, XF, C1, EA, ER, KM1, X, YIV, Y, F, YIV, CYO, 16,
12, EX, RKSNF, RKC)
C1 = C1 * I
C2 = (C2 * FDBLE(I)) - FDBLE(KM1)
CYL = CYO
340 DX = INTV / FDBLE(C1)
KM3 = 3 * KM1
J = 0
GO TO 359
360 J = J + 3
359 IF (J .LE. KM3) GO TO 357
GO TO 358
357 J2 = 2 * J
C00(J + 1) = CON(J2 + 2) * DX
C00(J + 2) = CON(J2 + 4) * DX
C00(J + 3) = CON(J2 + 6) * DX
GO TO 360
358 SC1 = 3.0D-4*(C1**EX)
IF(K.LE.3) SC1 = SC1*10
I = 1
GO TO 363
364 I = I + 1
363 IF (I .LE. N) GO TO 361
GO TO 362
361 AE(I + 1) = EA(I + 1) / SC1
RE(I + 1) = ER(I + 1) / SC1
GO TO 364
362 A1 = CON(K6 + 1) * DX
A2 = CON(K61 + 1) * DX
A3 = CON(K62 + 1) * DX
337 XDXT = X + DX * OMT
XDX = X + DX
I = 1
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120      GO TO 367
121      I = I + 1
122      IF (I .LE. N) GO TO 365
123      GO TO 366
124      SUMYC(I + 1) = 0
125      SUMYP(I + 1) = SUMYC(I + 1)
126      SUMYIP(I + 1) = SUMYP(I + 1)
127      GO TO 368
128      J = 0
129      GO TO 371
130      J = J + 1
131      IF (J .LE. KM1) GO TO 369
132      GO TO 370
133      CYL3 = MOD((KM1 - J) + CYL,16)
134      J3 = 3 * J
135      J6 = 6 * J
136      COA = CON(J6 + 1)
137      COB = COO(J3 + 1)
138      COLA = CON(J6 + 3)
139      COLB = COO(J3 + 2)
140      COGA = CON(J6 + 5)
141      COGB = COO(J3 + 3)
142      I = 1
143      GO TO 375
144      I = I + 1
145      IF (I .LE. N) GO TO 373
146      GO TO 374
147      TEMPY = Y(CYL3 + 1, I + 1)
148      TEMPF = F(CYL3 + 1, I + 1)
149      SUMYIP(I + 1) = (SUMYIP(I + 1) + COA * TEMPY) + COB * TEMPF
150      SUMYP(I + 1) = (SUMYP(I + 1) + COLA * TEMPY) + COLB * TEMPF
151      SUMYC(I + 1) = (SUMYC(I + 1) + COGA * TEMPY) + COGB * TEMPF
152      GO TO 376
153      GO TO 372
154      CALL FUNCTI(N, XDXI, SUMYIP, FV1)
155      I = 1
156      GO TO 379
157      I = I + 1
158      IF (I .LE. N) GO TO 377
159      GO TO 378
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377 TEMPF = FV1(I + 1)
SUMYP(I + 1) = SUMYP(I + 1) + A1 * TEMPF
SUMYC(I + 1) = SUMYC(I + 1) + A2 * TEMPF
GO TO 380
378 CALL FUNCTI(N, XDX, SUMYP, FV1)
CYL = MOD(CYL + 1,16)
CYO = MOD(CYL + KM1,16)
COUNT = 0
I = 1
GO TO 383
384 I = I + 1
383 IF (I .LE. N) GO TO 381
GO TO 382
381 TEMPY = SUMYC(I + 1) + A3 * FV1(I + 1)
T1 = AE(I + 1)
T2 = ABS(RE(I + 1) * TEMPY)
TEST = ABS(TEMPY - SUMYP(I + 1))
IF ((TEST .LE. T1) .OR. TEST .LE. T2) GO TO 386
C2 = C2 + C2
CYL = MOD(CYL + 15,16)
CYO = MOD(CYL + KM1,16)
IF (C2 .GE. KM1) GO TO 388
II = 0
GO TO 391
392 II = II + 1
391 IF (II .LE. N) GO TO 389
GO TO 390
389 TEMP7(II + 1) = Y(CYO + 1, II + 1)
GO TO 392
390 CALL SHANKS(N, X, XF, TEMP7, RKSNF, RKSDR, RKC, EX, EA, ER, DX)
II = 0
GO TO 395
396 II = II + 1
395 IF (II .LE. N) GO TO 393
GO TO 394
393 Y(CYO + 1, II + 1) = TEMP7(II + 1)
GO TO 396
394 GO TO 339
388 CONTINUE
387 C1 = C1 + C1
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200 GO TO 338
201 CONTINUE
202 Y(CYO + 1, I + 1) = TEMPY
203 IF ((TEST .GE. P2 * T1) .AND. TEST .GE. P2 * T2) GO TO 398
204 COUNT = COUNT + 1
205 CONTINUE
206 GO TO 384
207 C2 = C2 - 1.0D0
208 X = XF - (DX * C2)
209 IF (C2 .EQ. 0) GO TO 339
210 IF (C2 .GE. 1) GO TO 401
211 II = 0
212 GO TO 404
213 II = II + 1
214 IF (II .LE. N) GO TO 402
215 GO TO 403
216 TEMP7(II + 1) = Y(CYO + 1, II + 1)
217 GO TO 405
218 CALL SHANKS(N, X, XF, TEMP7, RKSNF, RKSDR, RKC, EX, EA, ER, DX)
219 II = 0
220 GO TO 408
221 II = II + 1
222 IF (II .LE. N) GO TO 406
223 GO TO 407
224 Y(CYO + 1, II + 1) = TEMP7(II + 1)
225 GO TO 409
226 GO TO 339
227 CONTINUE
228 II = 0
229 GO TO 412
230 II = II + 1
231 IF (II .LE. N) GO TO 410
232 GO TO 411
233 TEMP7(II + 1) = Y(CYO + 1, II + 1)
234 GO TO 413
235 CALL FUNCTI(N, X, TEMP7, TEMP9)
236 II = 0
237 GO TO 416
238 II = II + 1
239 IF (II .LE. N) GO TO 414
  
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240 GO TO 415
241 F(CY0 + 1, II + 1) = TEMP9(II + 1)
242 GO TO 417
243 IF (COUNT .NE. N) GO TO 419
244 TOTCNT = TOTCNT + 1
245 IF (TOTCNT .LT. 3) GO TO 421
246 IF (COUNTR .LT. 2 * K) GO TO 423
247 COUNTR = 0
248 C2 = C2 / 2.0D0
249 C1 = C1 / 2
250 IF (C2 .GE. 1) GO TO 425
251 II = 0
252 GO TO 428
253 II = II + 1
254 IF (II .LE. N) GO TO 426
255 GO TO 427
256 TEMP7(II + 1) = Y(CY0 + 1, II + 1)
257 GO TO 429
258 CALL SHANKS(N, X, XF, TEMP7, RKSNF, RKSDR, RKC, EA, EK, UX)
259 II = 0
260 GO TO 432
261 II = II + 1
262 IF (II .LE. N) GO TO 430
263 GO TO 431
264 Y(CY0 + 1, II + 1) = TEMP7(II + 1)
265 GO TO 433
266 GO TO 339
267 CONTINUE
268 TOTCNT = 0
269 I = 1
270 GO TO 436
271 I = I + 1
272 IF (I .LE. N) GO TO 434
273 GO TO 435
274 J = 1
275 GO TO 440
276 J = J + 1
277 IF (J .LE. KM1) GO TO 438
278 GO TO 439
279 CYL1 = MOD((CY0 + 16) - J, 16)

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280 CYL2 = MOD((CYO + 16) - (2 * J), 16)
281 Y(CYL1 + 1, I + 1) = Y(CYL2 + 1, I + 1)
282 F(CYL1 + 1, I + 1) = F(CYL2 + 1, I + 1)
283 GO TO 441
284 439 GO TO 437
285 435 GO TO 340
286 423 CONTINUE
287 422 CONTINUE
288 421 CONTINUE
289 420 CONTINUE
290 419 CONTINUE
291 418 COUNTR = COUNTR + 1
292 GO TO 337
293 339 I = 1
294 GO TO 444
295 445 I = I + 1
296 444 IF (I .LE. N) GO TO 442
297 GO TO 443
298 442 YIV(I + 1) = Y(CYO + 1, I + 1)
299 GO TO 445
300 443 CONTINUE
301 RETURN
302 END
303 C 443 BLOCK 9

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@PRT °COWELL


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GALLAHER-L-J*TPFS,COWELL
1 SUBROUTINE COWELL(N, XI, XF, Y, EA, ER, P, DXV, RKSFN, RKSRDR,
2 1RKSCFF, Q, CWLLCF)
3 DOUBLE PRECISION DXV
4 COMMON/COMMON/FH(35,1)
5 INTEGER N, RKSFN, RKSRDR, Q
6 DOUBLE PRECISION XI, XF, P, DX
7 DOUBLE PRECISION Y, EA, ER
8 DIMENSION Y(100), EA(100), ER(100)
9 DOUBLE PRECISION RKSCFF
10 DIMENSION RKSCFF(91)
11 DOUBLE PRECISION CWLLCF
12 DIMENSION CWLLCF(52)
13 INTEGER C1, M, MM1, QP1, TQP1, IND1, I1, I2, I3, I, J, K, CYI
14 INTEGER CRRCTC
15 DOUBLE PRECISION INT, C2, DFACTR, X, H, T1, T2, T3, T4, T5, T6
16 LOGICAL DFLAG, PFLAG
17 INTEGER II
18 DOUBLE PRECISION FH
19 DOUBLE PRECISION YMID1, YP, YC, YM, CS, FP, HDM1F, TEMP9, HDM1FM, EAV, ERV,
20 1EAVD, ERVD
21 DIMENSION YMID1(100), YP(100), YC(100), YM(100), CS(100), FP(100), HDM1F(100), HDM1FM(100), EAVD(100), EKVD(100)
22 1(100), TEMP9(100), HDM1FM(100), EAV(100), ERV(100), EAVD(100), ERV(100), MCOEFF
23 DOUBLE PRECISION PCOEFF, CCOEFF, MCOEFF
24 DIMENSION PCOEFF(18), CCOEFF(18), MCOEFF(18)
25 DEFINE FDBLE(I) = DBLE(FLOAT(I))
26 DX = DXV
27 INT = XF - XI
28 C1 = 1
29 C1 = C1 + C1
30 IF (C1 .LT. Q) GO TO 446
31 IF (DX .GE. 0) GO TO 459
32 DX = - DX
33 CONTINUE
34 458 IF (DX .EQ. 0) GO TO 461
35 447 IF (ABS(INT) / FDBLE(C1) .LE. DX) GO TO 463
36 C1 = C1 + C1
37 GO TO 447
38 CONTINUE
39 463 CONTINUE
462 CONTINUE
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461 CONTINUE
460 C2 = C1
    M = Q / 2
    MM1 = M - 1
    QP1 = Q + 1
    TQP1 = QP1 + Q
    DFACTR = 2 ** (Q + 3)
    INDX = 0
    X = XI
    CALL FUNCTI(N, X, Y, TEMP9)
    II = 0
    GO TO 466
467 II = II + 1
466 IF (II .LE. N) GO TO 464
    GO TO 465
464 FH(1, II + 1) = TEMP9(II + 1)
    GO TO 467
465 CONTINUE
452 I1 = START(N, XI, XF, C1, EA, ER, Q, X, Y, FH, YMID1, INDX,
1TQP1, 1, P, RKSN, RKSCFF)
    C1 = I1 * C1
    C2 = (C2 * FDBLE(I1)) - FDBLE(Q)
    INDX = MOD(INDX + Q, TQP1)
    IF (C2 .LT. M) GO TO 456
453 H = INT / FDBLE(C1)
    K = 0
    GO TO 471
472 K = K + 1
471 IF (K .LE. Q) GO TO 469
    GO TO 470
469 PCOEFF(K + 1) = CWLLCF(K + 1) * H
    I1 = K + QP1
    CCOEFF(K + 1) = CWLLCF(I1 + 1) * H
    I1I2 = I1 + QP1
    MCOEFF(K + 1) = CWLLCF(I1I2 + 1) * H
    GO TO 472
470 T1 = (C1 ** P) * 10.000
    J = 1
    GO TO 475
476 J = J + 1

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475 IF (J * LE, N) GO TO 473
    GO TO 474
473 EAV(J + 1) = EA(J + 1) / T1
    EAVD(J + 1) = EAV(J + 1) / DFACTR
    ERV(J + 1) = ER(J + 1) / T1
    ERVD(J + 1) = ERV(J + 1) / DFACTR
    GO TO 476
474 T1 = MCOEFF(1)
    J = 1
    GO TO 479
480 J = J + 1
479 IF (J * LE, N) GO TO 477
    GO TO 478
477 HDM1F(J + 1) = YMD1(J + 1) - (FH(INDX + 1, J + 1) * T1)
    GO TO 480
478 CYI = INDX + TOP1
    I3 = CYI - QP1
    K = 1
    GO TO 483
484 K = K + 1
483 IF (K * LE, M) GO TO 481
    GO TO 482
481 I1 = MOD(CYI - K, TOP1)
    I2 = MOD(I3 + K, TOP1)
    T1 = MCOEFF(K + 1) - H
    I1I2 = QP1 - K
    T2 = MCOEFF(I1I2 + 1)
    J = 1
    GO TO 487
488 J = J + 1
487 IF (J * LE, N) GO TO 485
    GO TO 486
485 HDM1F(J + 1) = (HDM1F(J + 1) - (FH(I1 + 1, J + 1) * T1)) - (FH(I2
    + 1, J + 1) * T2)
    GO TO 488
486 GO TO 484
482 J = 1
    GO TO 491
492 J = J + 1
491 IF (J * LE, N) GO TO 489
  
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120 GO TO 490
121 489 HDM1FM(J + 1) = HDM1F(J + 1)
122 GO TO 492
123 490 DFLAG = .FALSE.
124 454 I = 1
125 GO TO 495
126 496 I = I + 1
127 495 IF (I .LE. M) GO TO 493
128 GO TO 494
129 493 INDX = MOD(INDX + 1, TOP1)
130 CYI = INDX + TOP1
131 X = XF - ((C2 - FDBLE(I)) * H)
132 I1 = MOD(CYI - 1, TOP1)
133 T1 = PCOEFF(I)
134 T2 = CCoeff(2)
135 J = 1
136 GO TO 499
137 500 J = J + 1
138 499 IF (J .LE. N) GO TO 497
139 GO TO 498
140 497 T3 = FH(I1 + 1, J + 1)
141 HDM1F(J + 1) = HDM1F(J + 1) + H * T3
142 T4 = HDM1F(J + 1)
143 YP(J + 1) = T4 + T1 * T3
144 CS(J + 1) = T4 + T2 * T3
145 GO TO 500
146 498 I3 = CYI - QP1
147 K = 2
148 GO TO 503
149 504 K = K + 1
150 503 IF (K .LE. M) GO TO 501
151 GO TO 502
152 501 I1 = MOD(CYI - K, TOP1)
153 I2 = MOD(I3 + K, TOP1)
154 T1 = PCOEFF(K)
155 T2 = CCoeff(K + 1)
156 I1I3 = Q - K
157 T3 = PCOEFF(I1I3 + 1)
158 I1I3 = QP1 - K
159 T4 = CCoeff(I1I3 + 1)

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160 J = 1
161 GO TO 507
162 J = J + 1
163 IF (J .LE. N) GO TO 505
164 GO TO 506
165 T5 = FH(I1 + 1, J + 1)
166 T6 = FH(I2 + 1, J + 1)
167 YP(J + 1) = (YP(J + 1) + T1 * T5) + T3 * T6
168 CS(J + 1) = (CS(J + 1) + T2 * T5) + T4 * T6
169 GO TO 508
170 GO TO 504
171 I1 = MOD(CY1 - Q, TOP1)
172 I2 = MOD(CY1 - QP1, TOP1)
173 T1 = PCOEFF(Q)
174 T2 = CCOEFF(Q + 1)
175 T3 = PCOEFF(Q + 1)
176 J = 1
177 GO TO 511
178 J = J + 1
179 IF (J .LE. N) GO TO 509
180 GO TO 510
181 T4 = FH(I1 + 1, J + 1)
182 YP(J + 1) = (YP(J + 1) + T1 * T4) + T3 * FH(I2 + 1, J + 1)
183 CS(J + 1) = CS(J + 1) + T2 * T4
184 GO TO 512
185 T2 = CCOEFF(1)
186 CRRCTC = 1
187 CALL FUNCTI(N, X, YP, FP)
188 J = 1
189 GO TO 515
190 J = J + 1
191 IF (J .LE. N) GO TO 513
192 GO TO 514
193 YC(J + 1) = CS(J + 1) + T2 * FP(J + 1)
194 T3 = YC(J + 1)
195 T1 = ABS(T3 - YP(J + 1))
196 IF (T1 .LE. EAV(J + 1)) GO TO 518
197 IF (T1 .LE. ERV(J + 1)) * ABS(T3)) GO TO 520
198 J = J + 1
199 GO TO 523

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524 J = J + 1
523 IF (J .LE. N) GO TO 521
    GO TO 522
521 YC(J + 1) = CS(J + 1) + T2 * FP(J + 1)
    GO TO 524
522 CALL FUNCTI(N, X, YC, FP)
    J = 1
    GO TO 527
528 J = J + 1
527 IF (J .LE. N) GO TO 525
    GO TO 526
525 YP(J + 1) = CS(J + 1) + T2 * FP(J + 1)
    T3 = YP(J + 1)
    T1 = ABS(T3 - YC(J + 1))
    IF (T1 .LE. EAV(J + 1)) GO TO 530
    IF (T1 .LE. ERV(J + 1) * ABS(T3)) GO TO 532
    J = J + 1
    GO TO 535
536 J = J + 1
535 IF (J .LE. N) GO TO 533
    GO TO 534
533 YP(J + 1) = CS(J + 1) + T2 * FP(J + 1)
    GO TO 536
534 CRRCTC = CRRCTC + 2
    IF (CRRCTC .LE. 8) GO TO 538
    INDX = MOD(CYI - I, TQP1)
    GO TO 451
538 CONTINUE
537 GO TO 455
532 CONTINUE
531 CONTINUE
530 CONTINUE
529 GO TO 528
526 CALL FUNCTI(N, X, YP, TEMP9)
    II = 0
    GO TO 541
542 II = II + 1
541 IF (II .LE. N) GO TO 539
    GO TO 540
539 FH(INDX + 1, II + 1) = TEMP9(II + 1)

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GO TO 542  
540 PFLAG = .TRUE.  
CRRCTC = CRRCTC + 1  
GO TO 448  
520 CONTINUE  
519 CONTINUE  
518 CONTINUE  
517 GO TO 516  
514 CALL FUNCTI(N, X, YC, TEMP9)  
II = 0  
GO TO 545  
546 II = II + 1  
545 IF (II .LE. N) GO TO 543  
GO TO 544  
543 FH(INDX + 1, II + 1) = TEMP9(II + 1)  
GO TO 546  
544 PFLAG = .FALSE.  
448 GO TO 496  
494 I1 = MOD(CY1 - M, TQP1)  
T1 = MCOEFF(M + 1)  
J = 1  
GO TO 549  
550 J = J + 1  
549 IF (J .LE. N) GO TO 547  
GO TO 548  
547 YM(J + 1) = HDM1FM(J + 1) + T1 * FH(II + 1, J + 1)  
548 I3 = CY1 - Q  
K = 0  
GO TO 553  
554 K = K + 1  
553 IF (K .LE. MM1) GO TO 551  
GO TO 552  
551 I1 = MOD(CY1 - K, TQP1)  
I2 = MOD(I3 + K, TQP1)  
T1 = MCOEFF(K + 1)  
II12 = Q - K  
T2 = MCOEFF(II12 + 1)  
J = 1  
GO TO 557
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280 558 J = J + 1
281 557 IF (J .LE. N) GO TO 555
282 60 TO 556
283 555 YM(J + 1) = (YM(J + 1) + T1 * FH(I1 + 1, J + 1)) + T2 * FH(I2 + 1,
284 1 J + 1)
285 60 TO 558
286 556 GO TO 554
287 552 IF (.NOT. DFLAG) GO TO 560
288 J = 1
289 60 TO 563
290 J = J + 1
291 564 IF (J .LE. N) GO TO 561
292 60 TO 562
293 561 T3 = Y(J + 1)
294 T2 = ABS(T3 - YM(J + 1))
295 IF (T2 .LE. EAVD(J + 1)) GO TO 566
296 IF (T2 .LE. ERVD(J + 1) * ABS(T3)) GO TO 568
297 IF (T2 .LE. EAV(J + 1)) GO TO 570
298 IF (T2 .GT. ERV(J + 1) * ABS(T3)) GO TO 450
299 570 CONTINUE
300 569 GO TO 449
301 568 CONTINUE
302 567 CONTINUE
303 566 CONTINUE
304 565 GO TO 564
305 562 C2 = C2 - FDBLE(M)
306 C2 = C2 / 2.0D0
307 IF (.NOT. PFLAG) GO TO 573
308 J = 1
309 60 TO 576
310 J = J + 1
311 577 IF (J .LE. N) GO TO 574
312 60 TO 575
313 574 Y(J + 1) = YP(J + 1)
314 60 TO 577
315 575 GO TO 572
316 573 J = 1
317 60 TO 580
318 J = J + 1
319 580 IF (J .LE. N) GO TO 578
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320 GO TO 579
321 578 Y(J + 1) = YC(J + 1)
322 GO TO 581
323 579 CONTINUE
324 572 C1 = C1 / 2
325 IF (C2 .LE. M) GO TO 456
326 INDX = INDX + 1
327 K = 1
328 GO TO 585
329 586 K = K + 1
330 585 IF (K .LE. Q) GO TO 583
331 GO TO 584
332 583 INDX = MOD(INDX + 1, TQP1)
333 I1 = MOD(INDX + K, TQP1)
334 J = 1
335 GO TO 589
336 590 J = J + 1
337 589 IF (J .LE. N) GO TO 587
338 GO TO 588
339 587 FH(INDX + 1, J + 1) = FH(I1 + 1, J + 1)
340 GO TO 590
341 588 GO TO 586
342 584 GO TO 453
343 560 CONTINUE
344 559 J = 0
345 449 J = J + 1
346 GO TO 593
347 594 J = J + 1
348 593 IF (J .LE. N) GO TO 591
349 GO TO 592
350 591 T3 = Y(J + 1)
351 T2 = ABS(T3 - YM(J + 1))
352 IF (T2 .LE. EAV(J + 1)) GO TO 596
353 IF (T2 .LE. ERV(J + 1)) * ABS(T3)) GO TO 598
354 450 INDX = MOD(CYI - M, TQP1)
355 451 C1 = C1 + C1
356 X = XF - (C2 * H)
357 C2 = C2 + C2
358 GO TO 452
359 598 CONTINUE

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597 CONTINUE
596 CONTINUE
595 GO TO 594
592 C2 = C2 - FDBLE(M)
IF (C2 .LT. M) GO TO 600
IF (.NOT. PFLAG) GO TO 602
J = 1
GO TO 605
606 J = J + 1
605 IF (J .LE. N) GO TO 603
GO TO 604
603 YMID1(J + 1) = Y(J + 1)
Y(J + 1) = YP(J + 1)
HDM1FM(J + 1) = HDM1F(J + 1)
GO TO 606
604 GO TO 601
602 J = 1
GO TO 609
610 J = J + 1
609 IF (J .LE. N) GO TO 607
GO TO 608
607 YMID1(J + 1) = Y(J + 1)
Y(J + 1) = YC(J + 1)
HDM1FM(J + 1) = HDM1F(J + 1)
GO TO 610
608 CONTINUE
601 DFLAG = .TRUE.
GO TO 454
600 CONTINUE
599 IF (.NOT. PFLAG) GO TO 612
J = 1
GO TO 615
616 J = J + 1
615 IF (J .LE. N) GO TO 613
GO TO 614
613 Y(J + 1) = YP(J + 1)
GO TO 616
614 GO TO 611
612 J = 1
GO TO 619

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620 J = J + 1
619 IF (J .LE. N) GO TO 617
    GO TO 618
617 Y(J + 1) = YC(J + 1)
    GO TO 620
618 CONTINUE
611 CONTINUE
456 IF (C2 .LE. 0) GO TO 622
    CALL SHANKS(N, X, XF, Y, RKSFN, RKSRDR, RKSCFF, P, EA, ER, ABS(INT)
        1) / FDBLE(C1))
622 CONTINUE
621 CONTINUE
    RETURN
    END
    C 621 BLOCK 10

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@PRT *START

GALLAMER-L-J*IPF\$.START

```
1 FUNCTION START(N, XI, XF, IC1, EA, ER, M, X, YIV, YH, FH,
2 YFV, CYI, CYM, PA, P, FNEVAL, RKSCNS)
3 LOGICAL COMP
4 INTEGER N, CI, M, CYI, CYM, PA, FNEVAL
5 DOUBLE PRECISION XI, XF, X, P
6 DOUBLE PRECISION EA, ER, YIV, YFV
7 DIMENSION EA(100), ER(100), YIV(100), YFV(100)
8 DOUBLE PRECISION RKSCNS
9 DIMENSION RKSCNS(91)
10 DOUBLE PRECISION YH, FH
11 DIMENSION YH(35,100), FH(35,100)
12 INTEGER I, J, K, L, CFFCNT, FNMAX, INDX, NINDX, CNTR
13 DOUBLE PRECISION INT, H, TWOH, T1
14 DOUBLE PRECISION HC, TWOHC
15 DIMENSION HC(91), TWOHC(91)
16 DOUBLE PRECISION EAV, ERV, Y1, Y2, Y3, Y4
17 DIMENSION EAV(100), ERV(100), Y1(100), Y2(100), Y3(100), Y4(100)
18 DOUBLE PRECISION G
19 DIMENSION G(28,100)
20 DOUBLE PRECISION TEMP7, TEMP8, TEMP9
21 DIMENSION TEMP7(100), TEMP8(100), TEMP9(100)
22 INTEGER II
23 DEFINE FDBLE(I) = DBLE(FLOAT(I))
24 C1 = IC1
25 CNTR = 1
26 IF (M.EQ. 0) GO TO 49
27 CFFCNT = ((FNEVAL + 3) * FNEVAL) / 2 - 2
28 FNMAX = FNEVAL - 2
29 INT = XF - XI
30 TWOH = (INT + INT) / FDBLE(C1)
31 H = INT / FDBLE(C1)
32 I = 0
33 GO TO 52
34 I = I + 1
35 IF (I.LE. CFFCNT) GO TO 50
36 GO TO 51
37 T1 = RKSCNS(I + 1)
38 HC(I + 1) = T1 * H
39 TWOHC(I + 1) = T1 * TWOH
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40 GO TO 53
41 INDX = CYI - (CYI/CYM) * CYM
42 T1 = (FDBLE(C1) / 2.0D0) ** P
43 J = 1
44 GO TO 56
45 J = J + 1
46 IF (J .LE. N) GO TO 54
47 GO TO 55
48 EAV(J + 1) = EA(J + 1) / T1
49 ERV(J + 1) = ER(J + 1) / T1
50 GO TO 57
51 IF (PA .NE. 2) GO TO 59
52 NINDX = MOD(INDX + 1, CYM)
53 K = 0
54 GO TO 3
55 CONTINUE
56 IF (PA .NE. 1) GO TO 61
57 L = M / 2
58 CONTINUE
59 II = 0
60 GO TO 64
61 II = II + 1
62 IF (II .LE. N) GO TO 62
63 TEMP9(II + 1) = FH(INDX + 1, II + 1)
64 GO TO 65
65 CALL RUNKUT(N, X, FNMAX, TWOHC, Y1, TEMP9, G)
66 GO TO 4
67 TWOH = H
68 CNTR = CNTR + CNTR
69 C1 = C1 + C1
70 H = INT / FDBLE(C1)
71 I = 0
72 GO TO 68
73 I = I + 1
74 IF (I .LE. CFFCNT) GO TO 66
75 GO TO 67
76 TWOHC(I + 1) = HC(I + 1)
77 HC(I + 1) = RKSCNS(I + 1) * H
78 GO TO 69

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80 67 INDX = CYI - (CYI/CYM) * CYM
81 T1 = (FDBLE(C1) / 2.0D0) ** P
82 IF (PA .NE. 2) GO TO 71
83 K = 0
84 NINDX = MOD(INDX + 1,CYM)
85 J = 1
86 GO TO 74
87 J = J + 1
88 IF (J .LE. N) GO TO 72
89 GO TO 73
90 EAV(J + 1) = EA(J + 1) / T1
91 ERV(J + 1) = ER(J + 1) / T1
92 Y1(J + 1) = YH(NINDX + 1, J + 1)
93 GO TO 75
94 73 CONTINUE
95 2 II = 0
96 GO TO 78
97 II = II + 1
98 IF (II .LE. N) GO TO 76
99 GO TO 77
100 TEMP7(II + 1) = YH(INDX + 1, II + 1)
101 TEMP9(II + 1) = FH(INDX + 1, II + 1)
102 GO TO 79
103 77 CALL RUNKUT(N, (FDBLE(K) * H) + X, FNMAX, HC, TEMP7, TEMP8, TEMP9, 00125000
104 1,G)
105 II = 0
106 GO TO 82
107 II = II + 1
108 IF (II .LE. N) GO TO 80
109 GO TO 81
110 YH(NINDX + 1, II + 1) = TEMP8(II + 1)
111 GO TO 83
112 K = K + 1
113 INDX = NINDX
114 NINDX = MOD(INDX + 1,CYM)
115 II = 0
116 GO TO 86
117 II = II + 1
118 IF (II .LE. N) GO TO 84
119 GO TO 85
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120 84 TEMP7(II + 1) = YH(INDX + 1, II + 1)
121   GO TO 87
122 85 CALL FUNCTI(N, (FDBLE(K) * H) + X, TEMP7, TEMP9)
123   II = 0
124   GO TO 90
125 91 II = II + 1
126 90 IF (II .LE. N) GO TO 88
127   GO TO 89
128 88 FH(INDX + 1, II + 1) = TEMP9(II + 1)
129   GO TO 91
130 89 CALL RUNKUT(N, (FDBLE(K) * H) + X, FNMAX, HC, TEMP7, TEMP8, TEMP9,
131   1, G)
132   II = 0
133   GO TO 94
134 95 II = II + 1
135 94 IF (II .LE. N) GO TO 92
136   GO TO 93
137 92 YH(NINDX + 1, II + 1) = TEMP8(II + 1)
138   GO TO 95
139 93 IF (.NOT. COMP(N, EAV, ERV, Y1, TEMP8)) GO TO 97
140   K = K + 1
141   IF (K .GE. M) GO TO 99
142   INDX = NINDX
143   NINDX = MOD(INDX + 1, CYM)
144   II = 0
145   GO TO 102
146 103 II = II + 1
147 102 IF (II .LE. N) GO TO 100
148   GO TO 101
149 100 TEMP7(II + 1) = YH(INDX + 1, II + 1)
150   GO TO 103
151 101 CALL FUNCTI(N, (FDBLE(K) * H) + X, TEMP7, TEMP9)
152   II = 0
153   GO TO 106
154 107 II = II + 1
155 106 IF (II .LE. N) GO TO 104
156   GO TO 105
157 104 FH(INDX + 1, II + 1) = TEMP9(II + 1)
158   GO TO 107
159 105 CONTINUE
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3 II = 0
  GO TO 110
111 II = II + 1
110 IF (II .LE. N) GO TO 108
  GO TO 109
108 TEMP7(II + 1) = YH(INDX + 1, II + 1)
  TEMP9(II + 1) = FH(INDX + 1, II + 1)
  GO TO 111
109 CALL RUNKUT(N, (FDBLE(K) * H) + X, FNMAX, TWOHC, TEMP7, Y1, TEMP9,
  1 G)
  GO TO 2
99 CONTINUE
98 IF (K .NE. M) GO TO 113
  INDX = NINDX
  II = 0
  GO TO 116
117 II = II + 1
116 IF (II .LE. N) GO TO 114
  GO TO 115
114 TEMP7(II + 1) = YH(INDX + 1, II + 1)
  GO TO 117
115 CALL FUNCTI(N, (FDBLE(K) * H) + X, TEMP7, TEMP9)
  II = 0
  GO TO 120
121 II = II + 1
120 IF (II .LE. N) GO TO 118
  GO TO 119
118 FH(INDX + 1, II + 1) = TEMP9(II + 1)
  GO TO 121
119 CONTINUE
113 CONTINUE
112 GO TO 96
  97 GO TO 1
  96 GO TO 70
  71 J = 1
  GO TO 124
125 J = J + 1
124 IF (J .LE. N) GO TO 122
  GO TO 123
122 EAV(J + 1) = EA(J + 1) / T1
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200 ERV(J + 1) = ERV(J + 1) / T1
201 Y1(J + 1) = Y2(J + 1)
202 GO TO 125
203 CONTINUE
204 II = 0
205 GO TO 128
206 II = II + 1
207 IF (II .LE. N) GO TO 126
208 GO TO 127
209 TEMP9(II + 1) = FH(INDX + 1, II + 1)
210 GO TO 129
211 CALL RUNKUT(N, X, FNMAX, HC, YIV, Y2, TEMP9, G)
212 INDX = MOD(INDX + 1, CYM)
213 CALL FUNCTI(N, X + H, Y2, TEMP9)
214 II = 0
215 GO TO 132
216 II = II + 1
217 IF (II .LE. N) GO TO 130
218 GO TO 131
219 FH(INDX + 1, II + 1) = TEMP9(II + 1)
220 GO TO 133
221 CALL RUNKUT(N, X + H, FNMAX, HC, Y2, Y4, TEMP9, G)
222 K = 2
223 IF (PA .NE. 0) GO TO 135
224 IF (.NOT. COMP(N, EAV, ERV, Y1, Y4)) GO TO 137
225 IF (K .GE. M) GO TO 139
226 INDX = MOD(INDX + 1, CYM)
227 CALL FUNCTI(N, (FDBLE(K) * H) + X, Y4, TEMP9)
228 II = 0
229 GO TO 142
230 II = II + 1
231 IF (II .LE. N) GO TO 140
232 GO TO 141
233 FH(INDX + 1, II + 1) = TEMP9(II + 1)
234 GO TO 143
235 CALL RUNKUT(N, (FDBLE(K) * H) + X, FNMAX, TWOHC, Y4, Y1, TEMP9, G)
236 CALL RUNKUT(N, (FDBLE(K) * H) + X, FNMAX, HC, Y4, Y3, TEMP9, G)
237 K = K + 1
238 INDX = MOD(INDX + 1, CYM)
239 CALL FUNCTI(N, (FDBLE(K) * H) + X, Y3, TEMP9)

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270 00292000
271 00293000
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276 00298000
277 00299000
278 00300000
279 00301000

147 II = 0
146 GO TO 146
145 IF (II .LE. N) GO TO 144
144 GO TO 145
144 FH(INDX + 1, II + 1) = TEMP9(II + 1)
145 GO TO 147
145 CALL RUNKUT(N, (FDBLE(K) * H) + X, FNMAX, HC, Y3, Y4, TEMP9, G)
K = K + 1
GO TO 5
139 CONTINUE
138 IF (K .NE. M) GO TO 149
INDX = MOD(INDX + 1, CYM)
CALL FUNCTI(N, (FDBLE(K) * H) + X, Y4, TEMP9)
II = 0
GO TO 152
153 II = II + 1
152 IF (II .LE. N) GO TO 150
GO TO 151
150 FH(INDX + 1, II + 1) = TEMP9(II + 1)
GO TO 153
151 J = 1
GO TO 156
157 J = J + 1
156 IF (J .LE. N) GO TO 154
GO TO 155
154 YFV(J + 1) = Y4(J + 1)
GO TO 157
155 GO TO 148
149 J = 1
GO TO 160
161 J = J + 1
160 IF (J .LE. N) GO TO 158
GO TO 159
158 YFV(J + 1) = Y3(J + 1)
GO TO 161
159 CONTINUE
148 GO TO 136
137 GO TO 1
136 GO TO 134

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280 135 CONTINUE
281 6 IF (.NOT. COMP(N, EAV, ERV, Y1, Y4)) GO TO 163
282 INDX = MOD(INDX + 1, CYM)
283 CALL FUNCTI(N, (FDBLE(K) * H) + X, Y4, TEMP9)
284 II = 0
285 GO TO 166
286 167 II = II + 1
287 166 IF (II .LE. N) GO TO 164
288 GO TO 165
289 164 FH(INDX + 1, II + 1) = TEMP9(II + 1)
290 GO TO 167
291 165 IF (K .GE. M) GO TO 169
292 IF (K .NE. L) GO TO 171
293 J = 1
294 GO TO 174
295 J = J + 1
296 174 IF (J .LE. N) GO TO 172
297 GO TO 173
298 172 YFV(J + 1) = Y4(J + 1)
299 GO TO 175
300 173 CONTINUE
301 171 CONTINUE
302 170 II = 0
303 GO TO 178
304 179 II = II + 1
305 178 IF (II .LE. N) GO TO 176
306 GO TO 177
307 176 TEMP9(II + 1) = FH(INDX + 1, II + 1)
308 GO TO 179
309 177 CALL RUNKUT(N, (FDBLE(K) * H) + X, FNMAX, TWOHC, Y4, Y1, TEMP9, G)
310 CALL RUNKUT(N, (FDBLE(K) * H) + X, FNMAX, HC, Y4, Y3, TEMP9, G)
311 K = K + 1
312 INDX = MOD(INDX + 1, CYM)
313 CALL FUNCTI(N, (FDBLE(K) * H) + X, Y3, TEMP9)
314 II = 0
315 GO TO 182
316 183 II = II + 1
317 182 IF (II .LE. N) GO TO 180
318 GO TO 181
319 180 FH(INDX + 1, II + 1) = TEMP9(II + 1)

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GO TO 183
181 IF (K .NE. L) GO TO 185
J = 1
GO TO 188
189 J = J + 1
188 IF (J .LE. N) GO TO 186
GO TO 187
186 YFV(J + 1) = Y3(J + 1)
GO TO 189
187 CONTINUE
185 CONTINUE
184 CALL RUNKUT(N, (FDBLE(K) * H) + X, FNMAX, HC, Y3, Y4, TEMP9, G)
K = K + 1
GO TO 6
169 CONTINUE
168 J = 1
GO TO 192
193 J = J + 1
192 IF (J .LE. N) GO TO 190
GO TO 191
190 YIV(J + 1) = Y4(J + 1)
GO TO 193
191 GO TO 162
163 GO TO 1
162 CONTINUE
134 CONTINUE
70 X = (FDBLE(M) * H) + X
49 CONTINUE
48 START = CNTR
RETURN
END
C 48 BLOCK 5

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@PRT °RUNKUT

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GALLAHER=L-J*TPF$.RUNKUT
1 SUBROUTINE RUNKUT(N, X, FNMAX, COEFF, YIV, YFV, FV, G)
2 INTEGER N, FNMAX
3 DOUBLE PRECISION X
4 DOUBLE PRECISION COEFF
5 DIMENSION COEFF(91)
6 DOUBLE PRECISION YIV, YFV, FV
7 DIMENSION YIV(100), YFV(100), FV(100)
8 DOUBLE PRECISION G
9 DIMENSION G(28, 100)
10 DOUBLE PRECISION TEMP9
11 DIMENSION TEMP9(100)
12 INTEGER II
13 INTEGER I, J, K, CCNT
14 DOUBLE PRECISION TEMP
15 DEFINE FDBLE(I) = DBLE(FLOAT(I))
16 J = 0
17 I = J
18 CCNT = 0
19 TEMP = COEFF(CCNT + 1)
20 I = 0
21 GO TO 9
22 I = I + 1
23 IF (I .LE. FNMAX) GO TO 7
24 GO TO 8
25 J = 1
26 GO TO 13
27 J = J + 1
28 IF (J .LE. N) GO TO 11
29 GO TO 12
30 YFV(J + 1) = (FV(J + 1) * TEMP) + YIV(J + 1)
31 GO TO 14
32 III3 = I - 1
33 K = 0
34 GO TO 17
35 K = K + 1
36 IF (K .LE. III3) GO TO 15
37 GO TO 16
38 CCNT = CCNT + 1
39 TEMP = COEFF(CCNT + 1)
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40 J = 1
41 GO TO 21
42 J = J + 1
43 21 IF (J .LE. N) GO TO 19
44 GO TO 20
45 19 YFV(J + 1) = (G(K + 1, J + 1) * TEMP) + YFV(J + 1)
46 GO TO 22
47 20 GO TO 18
48 16 CCNT = CCNT + 1
49 TEMP = X + COEFF(CCNT + 1)
50 CALL FUNCTI(N, TEMP, YFV, TEMP9)
51 II = 0
52 GO TO 25
53 26 II = II + 1
54 25 IF (II .LE. N) GO TO 23
55 GO TO 24
56 23 G(I + 1, II + 1) = TEMP9(II + 1)
57 GO TO 26
58 24 CCNT = CCNT + 1
59 TEMP = COEFF(CCNT + 1)
60 GO TO 10
61 J = 1
62 GO TO 29
63 J = J + 1
64 30 J = J + 1
65 29 IF (J .LE. N) GO TO 27
66 GO TO 28
67 27 YFV(J + 1) = (FV(J + 1) * TEMP) + YIV(J + 1)
68 GO TO 30
69 K = 0
70 GO TO 33
71 K = K + 1
72 34 K = K + 1
73 33 IF (K .LE. FNMAX) GO TO 31
74 GO TO 32
75 31 CCNT = CCNT + 1
76 TEMP = COEFF(CCNT + 1)
77 J = 1
78 GO TO 37
79 J = J + 1
80 38 J = J + 1
81 37 IF (J .LE. N) GO TO 35
82 GO TO 36

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85  
86  
35 YFV(J + 1) = (G(K + 1, J + 1) * TEMP) + YFV(J + 1)  
36 GO TO 38  
37 GO TO 34  
32 CONTINUE  
RETURN  
END  
C 32 BLOCK 6
```

@PRT FUNCTI

```

GALLAHER-L-J*TPF$.COMP
1 LOGICAL FUNCTION COMP(N, EAV, ERV, Y, Z)
2 INTEGER N
3 DOUBLE PRECISION EAV,ERV,Y,Z
4 DIMENSION EAV(100),ERV(100),Y(100),Z(100)
5 INTEGER J
6 DOUBLE PRECISION T1
7 DEFINE FDBLE(I) = DBLE(FLOAT(I))
8 J = 1
9 GO TO 42
10 J = J + 1
11 IF (J .LE. N) GO TO 40
12 GO TO 41
13 T1 = ABS(Y(J + 1) - Z(J + 1))
14 IF (T1 .LE. EAV(J + 1)) GO TO 45
15 IF (T1 .LE. ERV(J + 1) * ABS(Z(J + 1))) GO TO 47
16 COMP = .FALSE.
17 GO TO 39
18 CONTINUE
19 CONTINUE
20 CONTINUE
21 GO TO 43
22 COMP = .TRUE.
23 CONTINUE
24 RETURN
25 END
26 C 39 BLOCK 7

```

```

00460000
00461000
00462000
00463000
00464000
00465000
00466000
00467000
00468000
00469000
00470000
00471000
00472000
00473000
00474000
00475000
00476000
00477000
00478000
00479000
00480000
00481000
00482000
00483000
00484000
00485000

```

@HGDGN X.M.66.6.3.S.PLEASE PUT STANDARD PAPER IN PR1 THANKS.


```

GALLAHER-L-J*TPFS*FUNCTI
1 SUBROUTINE FUNCTI(N, X, Y, FV)
2 DOUBLE PRECISION X
3 INTEGER N
4 DOUBLE PRECISION Y,FV
5 DIMENSION Y(100),FV(100)
6 DEFINE FDBLE(I) = DBLE(FLOAT(I))
7 COMMON/NN/NN
8 NN=NN+1
9 RETURN
10 END
11          C          BLOCK 4

```

```

00005000
00006000
00007000
00008000
00009000
00010000

00011000
00012000
00024000

```

```
@PRT          *COMP
```

APPENDIX B
LISTING OF COEFFICIENTS

This appendix lists sets of coefficients for the four methods described in this report. Given here are:

first, the Adams coefficients, β and β^* , for $q = 3$ through 18;

then come the Butcher coefficients, A , B , a , b , α and β , for $k = 1$ through 6;

then come the Cowell coefficients P , C , and M , for $m = 2$ through 8;

last are the Shanks coefficients, α , β and γ for the formulas 4-4, 5-5, 6-6, 7-7, 7-9, 8-10, and 8-12. (The γ s in each case are the last set of B 's given).

BETA (2, 2) =	5/12
BETA (2, 1) =	-4/3
BETA (2, 0) =	23/12
BETA* (3, 3) =	1/24
BETA* (3, 2) =	-5/24
BETA* (3, 1) =	19/24
BETA* (3, 0) =	3/8
Q = 2 RATIO (4) =	270/19
BETA (3, 3) =	-3/8
BETA (3, 2) =	37/24
BETA (3, 1) =	-59/24
BETA (3, 0) =	55/24
BETA* (4, 4) =	-19/720
BETA* (4, 3) =	53/360
BETA* (4, 2) =	-11/30
BETA* (4, 1) =	323/360
BETA* (4, 0) =	251/720
Q = 3 RATIO (5) =	502/27
BETA (4, 4) =	251/720
BETA (4, 3) =	-637/360
BETA (4, 2) =	109/30
BETA (4, 1) =	-1387/360
BETA (4, 0) =	1901/720
BETA* (5, 5) =	3/160
BETA* (5, 4) =	-173/1440
BETA* (5, 3) =	241/720
BETA* (5, 2) =	-133/240
BETA* (5, 1) =	1427/1440
BETA* (5, 0) =	95/288
Q = 4 RATIO (6) =	19950/863
BETA (5, 5) =	-95/288
BETA (5, 4) =	959/480
BETA (5, 3) =	-3649/720
BETA (5, 2) =	4991/720
BETA (5, 1) =	-2641/480
BETA (5, 0) =	4277/1440
BETA* (6, 6) =	-863/60480
BETA* (6, 5) =	263/2520

```

BETA* ( 6, 4) =
BETA* ( 6, 3) =
BETA* ( 6, 2) =
BETA* ( 6, 1) =
BETA* ( 6, 0) =
Q = 5 RATIO ( 7) =
  BETA ( 6, 6) =
  BETA ( 6, 5) =
  BETA ( 6, 4) =
  BETA ( 6, 3) =
  BETA ( 6, 2) =
  BETA ( 6, 1) =
  BETA ( 6, 0) =
  BETA* ( 7, 7) =
  BETA* ( 7, 6) =
  BETA* ( 7, 5) =
  BETA* ( 7, 4) =
  BETA* ( 7, 3) =
  BETA* ( 7, 2) =
  BETA* ( 7, 1) =
  BETA* ( 7, 0) =
Q = 6 RATIO ( 8) =
  BETA ( 7, 7) =
  BETA ( 7, 6) =
  BETA ( 7, 5) =
  BETA ( 7, 4) =
  BETA ( 7, 3) =
  BETA ( 7, 2) =
  BETA ( 7, 1) =
  BETA ( 7, 0) =
  BETA* ( 8, 8) =
  BETA* ( 8, 7) =
  BETA* ( 8, 6) =
  BETA* ( 8, 5) =
  BETA* ( 8, 4) =
  BETA* ( 8, 3) =
  BETA* ( 8, 2) =
  BETA* ( 8, 1) =
  BETA* ( 8, 0) =
Q = 7 RATIO ( 9) =

```

```

-6737/20160
  586/945
-15487/20160
  2713/2520
  19087/60480
  38174/1375
  19087/60480
-5603/2520
  135713/20160
-10754/945
  235183/20160
-18637/2520
  198721/60480
  275/24192
-11351/120960
  1537/4480
-88547/120960
  123133/120960
-4511/4480
  139849/120960
  5257/17280
  1103970/33953
-5257/17280
  32863/13440
-115747/13440
  2102243/120960
-296053/13440
  242653/13440
-1152169/120960
  16083/4480
-33953/3628800
  156437/1814400
-645607/1814400
  1573169/1814400
-31457/22680
  2797679/1814400
-2302297/1814400
  2233547/1814400
  1070017/3628800
  2140034/57281

```

BETA (8, 8) =	1070017/3628800
BETA (8, 7) =	-4832053/1814400
BETA (8, 6) =	19416743/1814400
BETA (8, 5) =	-45586321/1814400
BETA (8, 4) =	862303/22680
BETA (8, 3) =	-69927631/1814400
BETA (8, 2) =	47738393/1814400
BETA (8, 1) =	-21562603/1814400
BETA (8, 0) =	14097247/3628800
BETA* (9, 9) =	8183/1036800
BETA* (9, 8) =	-116687/1451520
BETA* (9, 7) =	335983/907200
BETA* (9, 6) =	-462127/453600
BETA* (9, 5) =	6755041/3628800
BETA* (9, 4) =	-8641823/3628800
BETA* (9, 3) =	200029/90720
BETA* (9, 2) =	-1408913/907200
BETA* (9, 1) =	9449717/7257600
BETA* (9, 0) =	25713/89600
Q = 8 RATIO (10) =	137461698/3250433
BETA (9, 9) =	-25713/89600
BETA (9, 8) =	20884811/7257600
BETA (9, 7) =	-2357683/181440
BETA (9, 6) =	15788639/453600
BETA (9, 5) =	-222386081/3628800
BETA (9, 4) =	269181919/3628800
BETA (9, 3) =	-28416361/453600
BETA (9, 2) =	6648317/181440
BETA (9, 1) =	-104995189/7257600
BETA (9, 0) =	4325321/1036800
BETA* (10,10) =	-3250433/479001600
BETA* (10, 9) =	9071219/119750400
BETA* (10, 8) =	-12318413/31933440
BETA* (10, 7) =	23643791/19958400
BETA* (10, 6) =	-21677723/8870400
BETA* (10, 5) =	2227571/623700
BETA* (10, 4) =	-33765029/8870400
BETA* (10, 3) =	12051709/3991680
BETA* (10, 2) =	-296725183/159667200
BETA* (10, 1) =	164046413/119750400

```

BETA* (10, 0) =
Q = 9 RATIO (11) =
BETA (10, 10) =
BETA (10, 9) =
BETA (10, 8) =
BETA (10, 7) =
BETA (10, 6) =
BETA (10, 5) =
BETA (10, 4) =
BETA (10, 3) =
BETA (10, 2) =
BETA (10, 1) =
BETA (10, 0) =
BETA* (11, 11) =
BETA* (11, 10) =
BETA* (11, 9) =
BETA* (11, 8) =
BETA* (11, 7) =
BETA* (11, 6) =
BETA* (11, 5) =
BETA* (11, 4) =
BETA* (11, 3) =
BETA* (11, 2) =
BETA* (11, 1) =
BETA* (11, 0) =
Q = 10 RATIO (12) =
BETA (11, 11) =
BETA (11, 10) =
BETA (11, 9) =
BETA (11, 8) =
BETA (11, 7) =
BETA (11, 6) =
BETA (11, 5) =
BETA (11, 4) =
BETA (11, 3) =
BETA (11, 2) =
BETA (11, 1) =
BETA (11, 0) =
BETA* (12, 12) =
BETA* (12, 11) =
26842253/95800320
53684506/1135053
26842253/95800320
52841941/17107200
2472634817/159667200
186080291/3991680
2492064913/266611200
82260679/623700
3539798831/266611200
1921376209/19958400
1572737587/31933440
2067948781/119750400
2132509567/479001600
4671/788480
68928781/958003200
384709327/958003200
87064741/63866880
501289903/159667200
91910491/17740800
1007253581/159667200
102212233/17740800
36465037/9123840
99642413/45619200
1374799219/958003200
4777223/17418240
717300033450/13695779093
4777223/17418240
30082309/9123840
17410248271/958003200
923636629/15206400
625551749/4561920
35183928883/159667200
41290273229/159667200
35689892561/159667200
15064372973/106444800
12326645437/191600640
6477936721/319334400
4527766399/958003200
13695779093/2615348736000
2724891251/39626496000

```

BETA* (12, 10) =	-30336027563/72648576000
BETA* (12, 9) =	406332786317/261534873600
BETA* (12, 8) =	-229882484333/58118860800
BETA* (12, 7) =	529394045911/72648576000
BETA* (12, 6) =	-4874320027/4864866000
BETA* (12, 5) =	84400835489/8072064000
BETA* (12, 4) =	-485500845331/58118860800
BETA* (12, 3) =	1346577425651/261534873600
BETA* (12, 2) =	-551368413119/217945728000
BETA* (12, 1) =	6595204069/4402944000
BETA* (12, 0) =	703604254357/2615348736000
Q #11 RATIO (13) =	1407208508714/24466579093
BETA (12, 12) =	703604254357/2615348736000
BETA (12, 11) =	-169639834921/48432384000
BETA (12, 10) =	4588414555201/217945728000
BETA (12, 9) =	-20232291373837/261534873600
BETA (12, 8) =	2253957198793/11623772160
BETA (12, 7) =	-2826800577631/8072064000
BETA (12, 6) =	228133014533/4864866000
BETA (12, 5) =	-34266367915049/72648576000
BETA (12, 4) =	20730767690131/58118860800
BETA (12, 3) =	-10498491598103/52306974720
BETA (12, 2) =	5963794194517/72648576000
BETA (12, 1) =	-931781102989/39626496000
BETA (12, 0) =	13064406523627/2615348736000
BETA* (13, 13) =	2224234463/475517952000
BETA* (13, 12) =	-69091417279/1046139494400
BETA* (13, 11) =	1636420501/3773952000
BETA* (13, 10) =	-4590817802567/2615348736000
BETA* (13, 9) =	5124051955567/1046139494400
BETA* (13, 8) =	-5797545653629/581188608000
BETA* (13, 7) =	1335017017153/87178291200
BETA* (13, 6) =	-7866111554491/435891456000
BETA* (13, 5) =	9575580965507/581188608000
BETA* (13, 4) =	-1748248003751/149448499200
BETA* (13, 3) =	16964495066809/2615348736000
BETA* (13, 2) =	-168235945379/58118860800
BETA* (13, 1) =	741197087471/475517952000
BETA* (13, 0) =	106364763817/402361344000
Q #12 RATIO (14) =	8296451577726/1322822840127

BETA	*	(13, 13)	#	106364763817/402361344000
BETA	*	(13, 12)	#	6460951197929/1743565824000
BETA	*	(13, 11)	#	-21029162113651/871782912000
BETA	*	(13, 10)	#	7222659159949/74724249600
BETA	*	(13, 9)	#	-10320787460413/38745907200
BETA	*	(13, 8)	#	310429955875453/581188608000
BETA	*	(13, 7)	#	-350379327127877/435891456000
BETA	*	(13, 6)	#	134046425652457/145297152000
BETA	*	(13, 5)	#	-31457535950413/38745907200
BETA	*	(13, 4)	#	570885914358161/1046139494400
BETA	*	(13, 3)	#	-3441222659093/124540416000
BETA	*	(13, 2)	#	89541175419277/871782912000
BETA	*	(13, 1)	#	-140970750679621/5230697472000
BETA	*	(13, 0)	#	905730205/172204032
BETA*	*	(14, 14)	#	-132282840127/31384184832000
BETA*	*	(14, 13)	#	124922452271/1961511552000
BETA*	*	(14, 12)	#	-14110480969927/31384184832000
BETA*	*	(14, 11)	#	137855863153/70053984000
BETA*	*	(14, 10)	#	-187504936597931/31384184832000
BETA*	*	(14, 9)	#	26159487787579/1961511552000
BETA*	*	(14, 8)	#	-236770944732449/10461394944000
BETA*	*	(14, 7)	#	38029005269/1277025750
BETA*	*	(14, 6)	#	-321201800274911/10461394944000
BETA*	*	(14, 5)	#	48869476129477/1961511552000
BETA*	*	(14, 4)	#	-71363886250691/4483454976000
BETA*	*	(14, 3)	#	3933201478249/490377888000
BETA*	*	(14, 2)	#	-102885148956217/31384184832000
BETA*	*	(14, 1)	#	3173185470929/1961511552000
BETA*	*	(14, 0)	#	1166309819657/4483454976000
Q =13 RATIO (15)				
BETA	*	(14, 14)	#	18660957114512/274523709512
BETA	*	(14, 13)	#	1166309819657/4483454976000
BETA	*	(14, 12)	#	-696561442637/178319232000
BETA	*	(14, 11)	#	859236476684231/31384184832000
BETA	*	(14, 10)	#	-58262613384023/490377888000
BETA	*	(14, 9)	#	1600835679073597/4483454976000
BETA	*	(14, 8)	#	-1544031478475483/1961511552000
BETA	*	(14, 7)	#	13760072112094753/10461394944000
BETA	*	(14, 6)	#	-2166615342637/1277025750
BETA	*	(14, 5)	#	17823675553313503/10461394944000
BETA	*	(14, 4)	#	-2614079370781733/1961511552000

BETA (14, 4) =	25298910337081429/31384184832000
BETA (14, 3) =	=25990262345039/70053984000
BETA (14, 2) =	3966421670215481/31384184832000
BETA (14, 1) =	=60007679150257/1961511552000
BETA (14, 0) =	13325653738373/2414168064000
BETA* (15, 15) =	2639651053/689762304000
BETA* (15, 14) =	=3867689367599/62768369664000
BETA* (15, 13) =	29219384284087/62768369664000
BETA* (15, 12) =	=137515713789319/62768369664000
BETA* (15, 11) =	64486158419069/8966909952000
BETA* (15, 10) =	=1096355235402331/62768369664000
BETA* (15, 9) =	679781959848881/20922789888000
BETA* (15, 8) =	=988788576755233/20922789888000
BETA* (15, 7) =	1138313909617631/20922789888000
BETA* (15, 6) =	=3129453071993581/62768369664000
BETA* (15, 5) =	2285168598349733/62768369664000
BETA* (15, 4) =	=189568380436867/8966909952000
BETA* (15, 3) =	612744541065337/62768369664000
BETA* (15, 2) =	=20999287611259/5706215424000
BETA* (15, 1) =	105145058757073/62768369664000
BETA* (15, 0) =	25221445/98402304
Q =14 RATIO (16) =	8204945906981250/111956703448001
BETA (15, 15) =	=25221445/98402304
BETA (15, 14) =	36807182273689/8966909952000
BETA (15, 13) =	=1934443196892599/62768369664000
BETA (15, 12) =	9038571752734087/62768369664000
BETA (15, 11) =	=2674355537386529/5706215424000
BETA (15, 10) =	10103478797549069/8966909952000
BETA (15, 9) =	=129930094104237331/62768369664000
BETA (15, 8) =	62029181421198881/20922789888000
BETA (15, 7) =	=70006862970773983/20922789888000
BETA (15, 6) =	62487713370967631/20922789888000
BETA (15, 5) =	=131963191940828581/62768369664000
BETA (15, 4) =	72558117072259733/62768369664000
BETA (15, 3) =	=4372481980074367/8966909952000
BETA (15, 2) =	740161300731949/4828336128000
BETA (15, 1) =	=2161567671248849/62768369664000
BETA (15, 0) =	362555126427073/62768369664000
BETA* (16, 16) =	=111956703448001/32011868528640000
BETA* (16, 15) =	956906730268873/16005934264320000

BETA*	(16, 14)	=	-171192511013729/355667428096000
BETA*	(16, 13)	=	596904922428961/246245142528000
BETA*	(16, 12)	=	-27389421430791451/3201186852864000
BETA*	(16, 11)	=	5708273541404323/25406248640000
BETA*	(16, 10)	=	-72784522563390409/16005934264320000
BETA*	(16, 9)	=	232085108601391937/3201186852864000
BETA*	(16, 8)	=	-42733352080603/463134672000
BETA*	(16, 7)	=	302240496916010687/3201186852864000
BETA*	(16, 6)	=	-1246285173964159159/16005934264320000
BETA*	(16, 5)	=	91914603656624011/1778437140480000
BETA*	(16, 4)	=	-12578861691928243/457312407552000
BETA*	(16, 3)	=	37519546987420243/3201186852864000
BETA*	(16, 2)	=	-1458231199032479/355667428096000
BETA*	(16, 1)	=	27707643610637623/16005934264320000
BETA*	(16, 0)	=	8092989203533249/32011868528640000
Q = 15	RATIO (17)	=	16185978407066498/205804074290625
BETA	(16, 16)	=	8092989203533249/32011868528640000
BETA	(16, 15)	=	-68846386581756617/16005934264320000
BETA	(16, 14)	=	942359269351333/27360571392000
BETA	(16, 13)	=	-551866398439384493/3201186852864000
BETA	(16, 12)	=	386778238886497951/640237370572800
BETA	(16, 11)	=	-2797406189209536629/1778437140480000
BETA	(16, 10)	=	7205576917796031023/2286562037760000
BETA	(16, 9)	=	-324179886697104913/65330343936000
BETA	(16, 8)	=	2879939505554213/463134672000
BETA	(16, 7)	=	-3993885936674091251/640237370572800
BETA	(16, 6)	=	80207429499737366711/16005934264320000
BETA	(16, 5)	=	-5702855818380878219/1778437140480000
BETA	(16, 4)	=	5173388005728297701/3201186852864000
BETA	(16, 3)	=	-22133884200927593/35177877504000
BETA	(16, 2)	=	2612634723678583/14227497123840
BETA	(16, 1)	=	-55994879072429317/1455084933120000
BETA	(16, 0)	=	14845854129333883/2462451425280000
BETA*	(17, 17)	=	50188465/15613165568
BETA*	(17, 16)	=	-3722582669836627/64023737057280000
BETA*	(17, 15)	=	1136320750878589/2286562037760000
BETA*	(17, 14)	=	-72974966880383/27360571392000
BETA*	(17, 13)	=	8062612208040217/800296713216000
BETA*	(17, 12)	=	-45532601008155413/1600593426432000
BETA*	(17, 11)	=	15815540301010573/25406248640000

BETA* (17,10) = -1728464634834409159/1600593426432000
 BETA* (17,9) = 964479921803293249/6402373705728000
 BETA* (17,8) = -40409465324546861/237124952064000
 BETA* (17,7) = 502364378756214437/3201186852864000
 BETA* (17,6) = -1883042979819352909/1600593426432000
 BETA* (17,5) = 63645018657622943/889218570240000
 BETA* (17,4) = -4019382738717217/114328101888000
 BETA* (17,3) = 44516885513301493/3201186852864000
 BETA* (17,2) = -146702510065339/32335220736000
 BETA* (17,1) = 114329243705491117/6402373705728000
 BETA* (17,0) = 85455477715379/342372925440000
 Q =16 RATIO (18) = 12752179117555146654/151711881512390095
 BETA (17,17) = -85455477715379/342372925440000
 BETA (17,16) = 2460247368070567/547211427840000
 BETA (17,15) = -612172313896136299/1600593426432000
 BETA (17,14) = 653581961828485643/3201186852864000
 BETA (17,13) = -454352730377247/5928123801600
 BETA (17,12) = 1719392832483362153/8002967132160000
 BETA (17,11) = -74619315086494380723/1600593426432000
 BETA (17,10) = 14237182892280945743/1778437140480000
 BETA (17,9) = -70617432699294428737/6402373705728000
 BETA (17,8) = 314640350110383511/256094948229120
 BETA (17,7) = -19726972891423175089/1778437140480000
 BETA (17,6) = 129650088885345917773/1600593426432000
 BETA (17,5) = -38023516029116089751/800296713216000
 BETA (17,4) = 65509525475265061/29640619008000
 BETA (17,3) = -511501877919758129/6402373705728000
 BETA (17,2) = 497505713064683651/228656203776000
 BETA (17,1) = -3947240465864473/92386344960000
 BETA (17,0) = 574246225956493833/9146248151040000
 BETA* (18,18) = -2334028946344463/7860144949376000
 BETA* (18,17) = 16083586213927447/283838567620608000
 BETA* (18,16) = -8727512947308437627/17030314057236480000
 BETA* (18,15) = 6216118590489229589/2128789257154560000
 BETA* (18,14) = -256626484009824989/21833735970816000
 BETA* (18,13) = 2160219719237435461/60822550204416000
 BETA* (18,12) = -23052478094030507/275839229952000
 BETA* (18,11) = 111229455689198952379/709596419051520000
 BETA* (18,10) = -2025977937601766635423/8515157028618240000
 BETA* (18,9) = 735975656988412429/2494674910728000

BETA* (18, 8) =	-170502576778289249423/567677135241216000
BETA* (18, 7) =	21409690670332474663/851515702866182400
BETA* (18, 6) =	-105083959047373621537/608225502044160000
BETA* (18, 5) =	127722520943891521/1316505415680000
BETA* (18, 4) =	-37673668595097727061/8515157028661824000
BETA* (18, 3) =	463492437836890081/28383856762060800
BETA* (18, 2) =	-5666838930556309291/1135354270482432000
BETA* (18, 1) =	78304622528683744423/4257578514309120000
BETA* (18, 0) =	12600467236042756559/51090942171709440000
BETA* (18, 0) =	25200934472085513118/281550972898020815
Q =17 RATIO (19) =	1/1
K = 1 CAP A (1) =	1/2
K = 1 CAP B (1) =	1/1
K = 1 LC A (1) =	1/1
K = 1 LC B (1) =	-1/1
K = 1 ALPHA (1) =	1/1
K = 1 BETA (1) =	1/6
K = 1 LC B	2/1
K = 1 BETA	4/6
K = 1 BETA (0) =	1/6
K = 2 CAP A (1) =	0/1
K = 2 CAP B (1) =	9/8
K = 2 LC A (1) =	28/5
K = 2 LC B (1) =	-60/15
K = 2 ALPHA (1) =	32/31
K = 2 BETA (1) =	12/93
K = 2 CAP A (2) =	1/1
K = 2 CAP B (2) =	3/8
K = 2 LC A (2) =	-23/5
K = 2 LC B (2) =	-26/15
K = 2 ALPHA (2) =	-1/31
K = 2 BETA (2) =	-1/93
K = 2 LC B	32/15
K = 2 BETA	64/93
K = 2 BETA (0) =	15/93
K = 3 CAP A (1) =	-225/128
K = 3 CAP B (1) =	225/128
K = 3 LC A (1) =	540/31
K = 3 LC B (1) =	-1395/155
K = 3 ALPHA (1) =	783/617
K = 3 BETA (1) =	-135/3085

K	=	3	CAP	A	(2)	=	200/128
K	=	3	CAP	B	(2)	=	300/128
K	=	3	LC	A	(2)	=	-297/31
K	=	3	LC	B	(2)	=	-2130/155
K	=	3	ALPHA	(2)	=	-135/617	
K	=	3	BETA	(2)	=	-495/3085	
K	=	3	CAP	A	(3)	=	153/128
K	=	3	CAP	B	(3)	=	45/128
K	=	3	LC	A	(3)	=	-212/31
K	=	3	LC	B	(3)	=	-309/155
K	=	3	ALPHA	(3)	=	-31/617	
K	=	3	BETA	(3)	=	-39/3085	
K	=	3	LC	B	(3)	=	384/155
K	=	3	BETA	(3)	=	2304/3085	
K	=	3	BETA	(0)	=	465/3085	
K	=	4	CAP	A	(1)	=	-629200/59049
K	=	4	CAP	B	(1)	=	96800/19683
K	=	4	LC	A	(1)	=	3796/61
K	=	4	LC	B	(1)	=	-75240/3355
K	=	4	ALPHA	(1)	=	2248/3943	
K	=	4	BETA	(1)	=	129360/216865	
K	=	4	CAP	A	(2)	=	-418176/59049
K	=	4	CAP	B	(2)	=	348480/19683
K	=	4	LC	A	(2)	=	2700/61
K	=	4	LC	B	(2)	=	-327096/3355
K	=	4	ALPHA	(2)	=	1080/3943	
K	=	4	BETA	(2)	=	64152/216865	
K	=	4	CAP	A	(3)	=	898425/59049
K	=	4	CAP	B	(3)	=	217800/19683
K	=	4	LC	A	(3)	=	-5204/61
K	=	4	LC	B	(3)	=	-210705/3355
K	=	4	ALPHA	(3)	=	568/3943	
K	=	4	BETA	(3)	=	14190/216865	
K	=	4	CAP	A	(4)	=	208000/59049
K	=	4	CAP	B	(4)	=	17600/19683
K	=	4	LC	A	(4)	=	-1231/61
K	=	4	LC	B	(4)	=	-17220/3355
K	=	4	ALPHA	(4)	=	47/3943	
K	=	4	BETA	(4)	=	570/216865	
K	=	4	LC	B	(4)	=	6561/3355

K = 4	BETA (0) =	118098/216865
K = 4	BETA (1) =	20130/216865
K = 5	CAP A (1) =	-9486400/531441
K = 5	CAP B (1) =	1185800/177147
K = 5	LC A (1) =	454750/4503
K = 5	LC B (1) =	-44017050/1386924
K = 5	ALPHA (1) =	230875/479327
K = 5	BETA (1) =	46719750/73816358
K = 5	CAP A (2) =	-24285184/531441
K = 5	CAP B (2) =	7589120/177147
K = 5	LC A (2) =	1181300/4503
K = 5	LC B (2) =	-328685280/1386924
K = 5	ALPHA (2) =	97000/479327
K = 5	BETA (2) =	32062800/73816358
K = 5	CAP A (3) =	12006225/531441
K = 5	CAP B (3) =	10672200/177147
K = 5	LC A (3) =	-558150/4503
K = 5	LC B (3) =	-472227525/1386924
K = 5	ALPHA (3) =	117500/479327
K = 5	BETA (3) =	13369125/73816358
K = 5	CAP A (4) =	20070400/531441
K = 5	CAP B (4) =	3449600/177147
K = 5	LC A (4) =	-965725/4503
K = 5	LC B (4) =	-153728400/1386924
K = 5	ALPHA (4) =	32375/479327
K = 5	BETA (4) =	1879500/73816358
K = 5	CAP A (5) =	2226400/531441
K = 5	CAP B (5) =	169400/177147
K = 5	LC A (5) =	-107672/4503
K = 5	LC B (5) =	-7573830/1386924
K = 5	ALPHA (5) =	1577/479327
K = 5	BETA (5) =	49170/73816358
K = 5	LC B =	2657205/1386924
K = 5	BETA =	39858075/73816358
K = 5	BETA (0) =	6934620/73816358
K = 6	CAP A (1) =	-630561008/23914845
K = 6	CAP B (1) =	13707848/1594323
K = 6	LC A (1) =	21459012/142985
K = 6	LC B (1) =	-1599082254/37433473
K = 6	ALPHA (1) =	1485084/3044563

K	=	6	BETA (1)	=	2514772260/3985332967
K	=	6	CAP A (2)	=	-3221344280/23914845
K	=	6	CAP B (2)	=	137078480/1594323
K	=	6	LC A (2)	=	110802000/142985
K	=	6	LC B (2)	=	-18173488410/37433473
K	=	6	ALPHA (2)	=	694875/3044563
K	=	6	BETA (2)	=	1660531950/3985332967
K	=	6	CAP A (3)	=	-1499295875/23914845
K	=	6	CAP B (3)	=	342696200/1594323
K	=	6	LC A (3)	=	52489000/142985
K	=	6	LC B (3)	=	-46096009575/37433473
K	=	6	ALPHA (3)	=	774000/3044563
K	=	6	BETA (3)	=	559924750/3985332967
K	=	6	CAP A (4)	=	3511928000/23914845
K	=	6	CAP B (4)	=	249233600/1594323
K	=	6	LC A (4)	=	-120483375/142985
K	=	6	LC B (4)	=	-33650498700/37433473
K	=	6	ALPHA (4)	=	121875/3044563
K	=	6	BETA (4)	=	-9906750/3985332967
K	=	6	CAP A (5)	=	1748450000/23914845
K	=	6	CAP B (5)	=	48956600/1594323
K	=	6	LC A (5)	=	-60172140/142985
K	=	6	LC B (5)	=	-6618347010/37433473
K	=	6	ALPHA (5)	=	-28812/3044563
K	=	6	BETA (5)	=	-18412020/3985332967
K	=	6	CAP A (6)	=	114738008/23914845
K	=	6	CAP B (6)	=	1612688/1594323
K	=	6	LC A (6)	=	-3951512/142985
K	=	6	LC B (6)	=	-218118054/37433473
K	=	6	ALPHA (6)	=	-2459/3044563
K	=	6	BETA (6)	=	-675290/3985332967
K	=	6	LC B	=	71744535/37433473
K	=	6	BETA	=	2152336050/3985332967
K	=	6	BETA (0)	=	374334730/3985332967
M	=	2	P (0)	=	2837/1440
M	=	2	P (1)	=	-2543/720
M	=	2	P (2)	=	17/5
M	=	2	P (3)	=	-1201/720
M	=	2	P (4)	=	95/288
M	=	2	C (0)	=	95/288

M	=	2	C	(1)	=	77/240
M	=	2	C	(2)	=	-7/30
M	=	2	C	(3)	=	73/720
M	=	2	C	(4)	=	-3/160
M	=	2	M	(0)	=	11/1440
M	=	2	M	(1)	=	-41/720
M	=	2	M	(2)	=	1/2
M	=	2	M	(3)	=	41/720
M	=	2	M	(4)	=	-11/1440
M	=	3	P	(0)	=	11603/4480
M	=	3	P	(1)	=	-104861/15120
M	=	3	P	(2)	=	1344989/120960
M	=	3	P	(3)	=	-20617/1890
M	=	3	P	(4)	=	156551/24192
M	=	3	P	(5)	=	-32371/15120
M	=	3	P	(6)	=	5257/17280
M	=	3	C	(0)	=	5257/17280
M	=	3	C	(1)	=	6961/15120
M	=	3	C	(2)	=	-66109/120960
M	=	3	C	(3)	=	33/70
M	=	3	C	(4)	=	-31523/120960
M	=	3	C	(5)	=	1247/15120
M	=	3	C	(6)	=	-275/24192
M	=	3	M	(0)	=	-191/120960
M	=	3	M	(1)	=	211/15120
M	=	3	M	(2)	=	-7843/120960
M	=	3	M	(3)	=	1/2
M	=	3	M	(4)	=	7843/120960
M	=	3	M	(5)	=	-211/15120
M	=	3	M	(6)	=	191/120960
M	=	4	P	(0)	=	3288521/1036800
M	=	4	P	(1)	=	-40987771/3628800
M	=	4	P	(2)	=	10219841/403200
M	=	4	P	(3)	=	-135352319/3628800
M	=	4	P	(4)	=	167287/4536
M	=	4	P	(5)	=	-9839609/403200
M	=	4	P	(6)	=	5393233/518400
M	=	4	P	(7)	=	-9401029/3628800
M	=	4	P	(8)	=	25713/89600
M	=	4	C	(0)	=	25713/89600

M	=	4	C	(1)	=	427487/725760
M	=	4	C	(2)	=	-3498217/3628800
M	=	4	C	(3)	=	500327/403200
M	=	4	C	(4)	=	-6467/5670
M	=	4	C	(5)	=	2616161/3628800
M	=	4	C	(6)	=	-24019/80640
M	=	4	C	(7)	=	263077/3628800
M	=	4	C	(8)	=	-8183/1036800
M	=	4	M	(0)	=	2497/7257600
M	=	4	M	(1)	=	-1469/403200
M	=	4	M	(2)	=	68119/3628800
M	=	4	M	(3)	=	-252769/3628800
M	=	4	M	(4)	=	1/2
M	=	4	M	(5)	=	252769/3628800
M	=	4	M	(6)	=	-68119/3628800
M	=	4	M	(7)	=	1469/403200
M	=	4	M	(8)	=	-2497/7257600
M	=	5	P	(0)	=	3569763199/958003200
M	=	5	P	(1)	=	-3966011741/239500800
M	=	5	P	(2)	=	1695154823/35481600
M	=	5	P	(3)	=	-1247363563/13305600
M	=	5	P	(4)	=	4144305961/31933440
M	=	5	P	(5)	=	-495967/3850
M	=	5	P	(6)	=	2087883637/22809600
M	=	5	P	(7)	=	-86656259/1900800
M	=	5	P	(8)	=	76795519/5068800
M	=	5	P	(9)	=	-144794759/47900160
M	=	5	P	(10)	=	4777223/17418240
M	=	5	C	(0)	=	4777223/17418240
M	=	5	C	(1)	=	8089801/11404800
M	=	5	C	(2)	=	-67283209/45619200
M	=	5	C	(3)	=	14380247/5702400
M	=	5	C	(4)	=	-517263181/159667200
M	=	5	C	(5)	=	76561/24948
M	=	5	C	(6)	=	-337204019/159667200
M	=	5	C	(7)	=	41021471/39916800
M	=	5	C	(8)	=	-107151937/319334400
M	=	5	C	(9)	=	15813379/239500800
M	=	5	C	(10)	=	-4671/788480
M	=	5	M	(0)	=	-14797/191600640

M	(1)	#	230371/239500800
M	(2)	#	-203257/35481600
M	(3)	#	299093/13305600
M	(4)	#	-11639731/159667200
M	(5)	#	1/2
M	(6)	#	11639731/159667200
M	(7)	#	-299093/13305600
M	(8)	#	203257/35481600
M	(9)	#	-230371/239500800
M	(10)	#	14797/191600640
P	(0)	#	733526173/172204032
P	(1)	#	-59344946587373/2615348736000
P	(2)	#	104639289835229/1307674368000
P	(3)	#	-102675619234099/523069747200
P	(4)	#	121844891963321/348713164800
P	(5)	#	-40318232897599/87178291200
P	(6)	#	31975145483/69498000
P	(7)	#	-149831214658501/435891456000
P	(8)	#	66393001798471/348713164800
P	(9)	#	-13247042672623/174356582400
P	(10)	#	491703913717/23775897600
P	(11)	#	-9000055832083/2615348736000
P	(12)	#	106364763817/402361344000
C	(0)	#	106364763817/402361344000
C	(1)	#	307515172843/373621248000
C	(2)	#	-2709005666077/1307674368000
C	(3)	#	2309296746931/523069747200
C	(4)	#	-507942835493/69742632960
C	(5)	#	4007043002299/435891456000
C	(6)	#	-2215533/250250
C	(7)	#	2816016533573/435891456000
C	(8)	#	-175102023617/49816166400
C	(9)	#	144690945961/104613949440
C	(10)	#	-486772076771/1307674368000
C	(11)	#	160495253651/2615348736000
C	(12)	#	-2224234463/475517952000
M	(0)	#	92427157/5230697472000
M	(1)	#	-132822967/523069747200
M	(2)	#	2274524387/1307674368000
M	(3)	#	-4013113421/523069747200

M	=	6	M	(4)	=	8855328071/348713164800
M	=	6	M	(5)	=	-32793164357/435891456000
M	=	6	M	(6)	=	1/2
M	=	6	M	(7)	=	32793164357/435891456000
M	=	6	M	(8)	=	-8855328071/348713164800
M	=	6	M	(9)	=	4013113421/523069747200
M	=	6	M	(10)	=	-2274524367/1307674368000
M	=	6	M	(11)	=	132822967/523069747200
M	=	6	M	(12)	=	-92427157/5230697472000
M	=	7	P	(0)	=	299786756763073/62768369664000
M	=	7	P	(1)	=	-116361307155361/3923023104000
M	=	7	P	(2)	=	2586771998343187/20922789888000
M	=	7	P	(3)	=	-356985279148297/980755776000
M	=	7	P	(4)	=	1988442368270749/2510734786560
M	=	7	P	(5)	=	-571195366208749/435891456000
M	=	7	P	(6)	=	5010047970421097/2988969984000
M	=	7	P	(7)	=	-2132356395131/1277025750
M	=	7	P	(8)	=	9030884747790859/6974263296000
M	=	7	P	(9)	=	-121630328435299/156920924160
M	=	7	P	(10)	=	2006565473520353/5706215424000
M	=	7	P	(11)	=	-3478073249303/29719872000
M	=	7	P	(12)	=	130221619246627/4828336128000
M	=	7	P	(13)	=	-2156804881129/560431872000
M	=	7	P	(14)	=	25221445/98402304
M	=	7	C	(0)	=	25221445/98402304
M	=	7	C	(1)	=	3654051145153/3923023104000
M	=	7	C	(2)	=	-172527345401401/62768369664000
M	=	7	C	(3)	=	2292797894083/326918592000
M	=	7	C	(4)	=	-886761467394133/62768369664000
M	=	7	C	(5)	=	3496017827389/156920924160
M	=	7	C	(6)	=	-192338437893109/6974263296000
M	=	7	C	(7)	=	349581097/13030875
M	=	7	C	(8)	=	-427489980816929/20922789888000
M	=	7	C	(9)	=	5256082896499/435891456000
M	=	7	C	(10)	=	-13579171932259/2510734786560
M	=	7	C	(11)	=	1748809541047/980755776000
M	=	7	C	(12)	=	-8530634387437/20922789888000
M	=	7	C	(13)	=	226717570111/3923023104000
M	=	7	C	(14)	=	-2639651053/689762304000
M	=	7	M	(0)	=	-36740617/8966909952000

M	=	7	M	(1)	=	87402869/1307674368000
M	=	7	M	(2)	=	-1306229471/2510734786560
M	=	7	M	(3)	=	2541742327/980755776000
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M	=	7	M	(5)	=	108816780203/3923023104000
M	=	7	M	(6)	=	-1610849246753/20922789888000
M	=	7	M	(7)	=	1/2
M	=	7	M	(8)	=	1610849246753/20922789888000
M	=	7	M	(9)	=	-108816780203/3923023104000
M	=	7	M	(10)	=	197301894457/20922789888000
M	=	7	M	(11)	=	-2541742327/980755776000
M	=	7	M	(12)	=	1306229471/2510734786560
M	=	7	M	(13)	=	-87402869/1307674368000
M	=	7	M	(14)	=	36740617/8966909952000
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M	=	8	P	(3)	=	-3961751682437057363/6402373705728000
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C	(5)	=	166541079499158667/3556874280960000			
C	(6)	=	-453443248829255563/6402373705728000			
C	(7)	=	20417981803080493/237124952064000			
C	(8)	=	-610091660201/7236479250			

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M	=	8		M	(16)	=	-61430943169/64023737057280000
		(4,4)		B	(1,0)	=	1/100
		(4,4)		A	(1)	=	1/100
		(4,4)		B	(2,0)	=	-4278/245
		(4,4)		B	(2,1)	=	4425/245
		(4,4)		A	(2)	=	3/5
		(4,4)		B	(3,0)	=	524746/8791
		(4,4)		B	(3,1)	=	-532125/8791
		(4,4)		B	(3,2)	=	16170/8791
		(4,4)		A	(3)	=	1/1
		(4,4)		B	(4,0)	=	-179124/70092
		(4,4)		B	(4,1)	=	200000/70092
		(4,4)		B	(4,2)	=	40425/70092
		(4,4)		B	(4,3)	=	8791/70092
		(5,5)		B	(1,0)	=	1/1000
		(5,5)		A	(1)	=	1/1000

(5,5)	B(2,0)	-447/10
(5,5)	B(2,1)	450/10
(5,5)	A(2)	3/10
(5,5)	B(3,0)	2684721/9568
(5,5)	B(3,1)	-2695500/9568
(5,5)	B(3,2)	17955/9568
(5,5)	A(3)	3/4
(5,5)	B(4,0)	-30672049/24219
(5,5)	B(4,1)	31009500/24219
(5,5)	B(4,2)	-146720/24219
(5,5)	B(4,3)	33488/24219
(5,5)	A(4)	1/1
(5,5)	B(5,0)	105/1134
(5,5)	B(5,1)	0/1134
(5,5)	B(5,2)	500/1134
(5,5)	B(5,3)	448/1134
(5,5)	B(5,4)	81/1134
(6,6)	B(1,0)	1/300
(6,6)	A(1)	1/300
(6,6)	B(2,0)	-29/5
(6,6)	B(2,1)	30/5
(6,6)	A(2)	1/5
(6,6)	B(3,0)	323/5
(6,6)	B(3,1)	-330/5
(6,6)	B(3,2)	10/5
(6,6)	A(3)	3/5
(6,6)	B(4,0)	-510104/810
(6,6)	B(4,1)	521640/810
(6,6)	B(4,2)	-12705/810
(6,6)	B(4,3)	1925/810
(6,6)	A(4)	14/15
(6,6)	B(5,0)	-417923/77
(6,6)	B(5,1)	427350/77
(6,6)	B(5,2)	-10605/77
(6,6)	B(5,3)	1309/77
(6,6)	B(5,4)	-54/77
(6,6)	A(5)	1/1
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(6,6)	B(6,2)	1225/3696

(6,6)	B(6,3)	1540/3696
(6,6)	B(6,4)	810/3696
(6,6)	B(6,5)	-77/3696
(7,7)	B(1,0)	1/192
(7,7)	A(1)	1/192
(7,7)	B(2,0)	-15/6
(7,7)	B(2,1)	16/6
(7,7)	A(2)	1/6
(7,7)	B(3,0)	4867/186
(7,7)	B(3,1)	-5072/186
(7,7)	B(3,2)	298/186
(7,7)	A(3)	1/2
(7,7)	B(4,0)	-19995/31
(7,7)	B(4,1)	20896/31
(7,7)	B(4,2)	-1025/31
(7,7)	B(4,3)	155/31
(7,7)	A(4)	1/1
(7,7)	B(5,0)	-469805/5022
(7,7)	B(5,1)	490960/5022
(7,7)	B(5,2)	-22736/5022
(7,7)	B(5,3)	5580/5022
(7,7)	B(5,4)	186/5022
(7,7)	A(5)	5/6
(7,7)	B(6,0)	914314/2604
(7,7)	B(6,1)	-955136/2604
(7,7)	B(6,2)	47983/2604
(7,7)	B(6,3)	-6510/2604
(7,7)	B(6,4)	-558/2604
(7,7)	B(6,5)	2511/2604
(7,7)	A(6)	1/1
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(7,7)	B(7,1)	0/300
(7,7)	B(7,2)	81/300
(7,7)	B(7,3)	110/300
(7,7)	B(7,4)	0/300
(7,7)	B(7,5)	81/300
(7,7)	B(7,6)	14/300
(7,9)	B(1,0)	2/9
(7,9)	A(1)	2/9
(7,9)	B(2,0)	1/12

(7,9)	B(2,1)	3/12
(7,9)	A(2)	1/3
(7,9)	B(3,0)	1/8
(7,9)	B(3,1)	0/8
(7,9)	B(3,2)	3/8
(7,9)	A(3)	1/2
(7,9)	B(4,0)	23/216
(7,9)	B(4,1)	0/216
(7,9)	B(4,2)	21/216
(7,9)	B(4,3)	=8/216
(7,9)	A(4)	1/6
(7,9)	B(5,0)	=4136/729
(7,9)	B(5,1)	0/729
(7,9)	B(5,2)	=13584/729
(7,9)	B(5,3)	5264/729
(7,9)	B(5,4)	13104/729
(7,9)	A(5)	8/9
(7,9)	B(6,0)	105131/151632
(7,9)	B(6,1)	0/151632
(7,9)	B(6,2)	302016/151632
(7,9)	B(6,3)	=107744/151632
(7,9)	B(6,4)	=284256/151632
(7,9)	B(6,5)	1701/151632
(7,9)	A(6)	1/9
(7,9)	B(7,0)	=775229/1375920
(7,9)	B(7,1)	0/1375920
(7,9)	B(7,2)	=2770950/1375920
(7,9)	B(7,3)	1735136/1375920
(7,9)	B(7,4)	2547216/1375920
(7,9)	B(7,5)	81891/1375920
(7,9)	B(7,6)	328536/1375920
(7,9)	A(7)	5/6
(7,9)	B(8,0)	23569/251888
(7,9)	B(8,1)	0/251888
(7,9)	B(8,2)	=122304/251888
(7,9)	B(8,3)	=20384/251888
(7,9)	B(8,4)	695520/251888
(7,9)	B(8,5)	=99873/251888
(7,9)	B(8,6)	=466560/251888
(7,9)	B(8,7)	241920/251888

(7,9) A(8)
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 (7,9) B(9,2)
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 (7,9) B(9,5)
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 (7,9) B(9,7)
 (7,9) B(9,8)
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 (8,10) B(3,2)
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 (8,10) B(4,2)
 (8,10) B(4,3)
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 (8,10) B(5,2)
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 (8,10) B(6,2)
 (8,10) B(6,3)
 (8,10) B(6,4)
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 (8,10) B(7,0)
 (8,10) B(7,1)
 (8,10) B(7,2)

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 0/54
 -27/54
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 8/54
 2/3
 389/4320
 0/4320
 -54/4320
 966/4320
 -624/4320
 243/4320
 1/6
 -231/20
 0/20
 81/20

(8,10)	B(7,3)	-1164/20
(8,10)	B(7,4)	656/20
(8,10)	B(7,5)	-122/20
(8,10)	B(7,6)	800/20
(8,10)	A(7)	1/1
(8,10)	B(8,0)	-127/288
(8,10)	B(8,1)	0/288
(8,10)	B(8,2)	18/288
(8,10)	B(8,3)	-678/288
(8,10)	B(8,4)	456/288
(8,10)	B(8,5)	-9/288
(8,10)	B(8,6)	576/288
(8,10)	B(8,7)	4/288
(8,10)	A(8)	5/6
(8,10)	B(9,0)	1481/820
(8,10)	B(9,1)	0/820
(8,10)	B(9,2)	-81/820
(8,10)	B(9,3)	7104/820
(8,10)	B(9,4)	-3376/820
(8,10)	B(9,5)	72/820
(8,10)	B(9,6)	-5040/820
(8,10)	B(9,7)	-60/820
(8,10)	B(9,8)	720/820
(8,10)	A(9)	1/1
(8,10)	B(10,0)	41/840
(8,10)	B(10,1)	0/840
(8,10)	B(10,2)	0/840
(8,10)	B(10,3)	27/840
(8,10)	B(10,4)	272/840
(8,10)	B(10,5)	27/840
(8,10)	B(10,6)	216/840
(8,10)	B(10,7)	0/840
(8,10)	B(10,8)	216/840
(8,10)	B(10,9)	41/840
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(8,12)	A(1)	1/9
(8,12)	B(2, 0)	1/24
(8,12)	B(2, 1)	3/24
(8,12)	A(2)	1/6
(8,12)	B(3, 0)	1/16

(8,12)	B(3, 1)	0/16
(8,12)	B(3, 2)	3/16
(8,12)	A(3)	1/4
(8,12)	B(4, 0)	29/500
(8,12)	B(4, 1)	0/500
(8,12)	B(4, 2)	33/500
(8,12)	B(4, 3)	-12/500
(8,12)	A(4)	1/10
(8,12)	B(5, 0)	33/972
(8,12)	B(5, 1)	0/972
(8,12)	B(5, 2)	0/972
(8,12)	B(5, 3)	4/972
(8,12)	B(5, 4)	125/972
(8,12)	A(5)	1/6
(8,12)	B(6, 0)	-21/36
(8,12)	B(6, 1)	0/36
(8,12)	B(6, 2)	0/36
(8,12)	B(6, 3)	76/36
(8,12)	B(6, 4)	125/36
(8,12)	B(6, 5)	-162/36
(8,12)	A(6)	1/2
(8,12)	B(7, 0)	-30/243
(8,12)	B(7, 1)	0/243
(8,12)	B(7, 2)	0/243
(8,12)	B(7, 3)	-32/243
(8,12)	B(7, 4)	125/243
(8,12)	B(7, 5)	0/243
(8,12)	B(7, 6)	99/243
(8,12)	A(7)	2/3
(8,12)	B(8, 0)	1175/324
(8,12)	B(8, 1)	0/324
(8,12)	B(8, 2)	0/324
(8,12)	B(8, 3)	-3456/324
(8,12)	B(8, 4)	-6250/324
(8,12)	B(8, 5)	8424/324
(8,12)	B(8, 6)	242/324
(8,12)	B(8, 7)	-27/324
(8,12)	A(8)	1/3
(8,12)	B(9, 0)	293/324
(8,12)	B(9, 1)	0/324

(8,12)	B(9, 2)	0/324
(8,12)	B(9, 3)	=852/324
(8,12)	B(9, 4)	=1375/324
(8,12)	B(9, 5)	1836/324
(8,12)	B(9, 6)	=118/324
(8,12)	B(9, 7)	162/324
(8,12)	B(9, 8)	324/324
(8,12)	A(9)	5/6
(8,12)	B(10, 0)	1303/1620
(8,12)	B(10, 1)	0/1620
(8,12)	B(10, 2)	0/1620
(8,12)	B(10, 3)	=4260/1620
(8,12)	B(10, 4)	=6875/1620
(8,12)	B(10, 5)	9990/1620
(8,12)	B(10, 6)	1030/1620
(8,12)	B(10, 7)	0/1620
(8,12)	B(10, 8)	0/1620
(8,12)	B(10, 9)	162/1620
(8,12)	A(10)	5/6
(8,12)	B(11, 0)	=8595/4428
(8,12)	B(11, 1)	0/4428
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(8,12)	B(11, 3)	30720/4428
(8,12)	B(11, 4)	48750/4428
(8,12)	B(11, 5)	=66096/4428
(8,12)	B(11, 6)	378/4428
(8,12)	B(11, 7)	=729/4428
(8,12)	B(11, 8)	=1944/4428
(8,12)	B(11, 9)	=1296/4428
(8,12)	B(11,10)	3240/4428
(8,12)	A(11)	1/1
(8,12)	B(12, 0)	41/840
(8,12)	B(12, 1)	0/840
(8,12)	B(12, 2)	0/840
(8,12)	B(12, 3)	0/840
(8,12)	B(12, 4)	0/840
(8,12)	B(12, 5)	216/840
(8,12)	B(12, 6)	272/840
(8,12)	B(12, 7)	27/840
(8,12)	B(12, 8)	27/840

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B(12, 9)
B(12,10)
B(12,11)

36/840
180/840
41/840