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SINGLE-STAGE EVALUATION OF HIGHLY-LOADED HIGH-MACH-NUMBER COMPRESSOR STAGES II. DATA AND PERFORMANCE MULTIPLE-CIRCULAR-ARC ROTOR

by D. H. Sulam, M. J. Keenan, and J. T. Flynn

> Pratt & Whitney Aircraft Division United Aircraft Corporation

prepared for National Aeronautics and Space Administration

> NASA Lewis Research Center Contract NAS3-10482 L. Reid, Program Manager Fluid Systems Components Division

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FOREWORD

The work described herein was done under NASA Contract NAS-3-10482 by Pratt & Whitney Aircraft Division of United Aircraft Corporation, East Hartford, Connecticut. Mr. L. Reid, NASA - Lewis Research Center, Fluid System Components Division, was Project Manager.

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ABSTRACT

Data and Performance Report, Single Stage Evaluation of Highly-Loaded-High-Mach-Number Compresso: Stages, Multiple Circular Arc Rotor

Tests were conducted on a 0.5 hub/tip ratio single-stage compressor designed to produce a pressure ratio of 1.936 at an efficiency of 84.2 percent with a rotor-tip speed of 1600 feet per second and a flow rate of 187.1 pounds per second. Design pressure ratio was obtained at design speed with an efficiency of 84.5 percent and a flow of 181.3 pounds per second. For tests with radial inlet-flc w distortion, the peak stage efficiency obtained at design speed was 78.4 at a pressure ratio of 1.774 and flow of 177.2 pounds per second. The peak stage efficiency with circumferentially-distorted inlet flow was 77.7 percent at a flow of 173.1 pounds per second and a pressure ratio of 1.747.

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1. SUMMARY

A compressor stage with a rotor tip speed of 1600 ft/sec, supersonic relative rotor-inlet Mach numbers over nearly the entire span, and a diffusion factor of 0.5 at 10% span from the tip was tested with uniform inlet flow and with radially and circumferentially-distorted inlet flow. Design stator inlet Mach numbers were subsonic, with a maximum value of 0.89 occurring at the hub where the diffusion factor was 0.6. Both the rotor and stator blades had multiple-circular-arc airfoil sections with the chord held constant from root to tip. The stage was designed without inlet guide vanes and the stator exit flow was axial.

Over-all performance at design speed with uniform inlet flow for near-design and near-surge aerodynamic conditions are compared with design values in the following table.

Parameter	Design Value	Near-Design Data Point	Near-Stall Data Point
Corrected Weight Flow, lb/sec	187.1	180.4	173.7
Rotor Pressure Ratio	2.000	2.010	2.037
Rotor Efficiency, Percent	88.7	89.0	86.7
Stage Pressure Ratio	1.936	1.946	1.959
Stage Efficiency, Percent	84.2	84.5	81.4

Over-all stage performance characteristics at design speed for uniform inlet flow and for radially and circumferentially distorted inlet flow are shown in the following table.

Parameter	Uniform Inlet Flow	Radially-Distorted Inlet Flow	Circumferentially Distorted Inlet Flow
Flow range, lb/sec $W_{\sqrt{\theta}}$ $W_{\sqrt{\theta}}$	184.3 - 171.0	179.6 - 176.0	178.2 - 157.5
δ max δ min			
Maximum stage pressure ratio	1.959	1.814	1.780
Maximum stage efficiency, percent	84.5	78.4	77.7
Pmax - Pmin	0	0.16	0.2
Pmax		(outer 0.4 of span)	(90° arc)

Rotor incidence angles were more positive than design values across the entire span as a result of the inability to attain design flow. Rotor deviations, diffusion factors, and losses were close to design estimates. Stator blade incidence angle, loss, diffusion factor, and deviation were also in general agreement with design values.

Static pressure patterns relative to rotor blade tips show regions of supersonic expansion and compression and shock locations. The shock was usually detached from the blade, oblique to the direction of the mean flow, and tended to move upstream as the rotor pressure ratio was increased.

Measured levels of continuous stress due to centrifugal and untwist loads agreed with the design prediction. Vibratory stresses with uniform inlet flow did not exceed 5,000 psi except at stall, where the blade vibratory stresses were approximately 20,000 psi. Indications of blade resonance with two excitations per revolution limited test speeds to 105 percent of design. With radially and circumferentially, distorted inlet flows, minimum flow was limited by a 15,000 psi vibratory stress boundary. Rotating stall patterns were present at the blade tip and midspan during the surge cycle with uniform and distorted inlet flow.

II. INTRODUCTION

Design of the single-stage compressor was based on the technology generated by two previous programs:

- High-tip-speed, highly-loaded rotors were tested under Contract NAS3-7617, and the results were reported in CR-54623 (Reference 1). Rotor efficiencies exceeding 0.88 were demonstrated, with a tip speed of 1400 feet per second and D factors greater than 0.5 over the entire span.
- (2) Transonic highly-loaded stators were tested under Contract NAS3-7614, and the results were reported in References 2, 3, and 4. Moderate stator losses were measured with high subsonic Mach numbers and with D factors greater than 0.5.

Multiple-circular-arc airfoil sections were selected for the rotor and the stator in order to obtain low losses at high Mach numbers. Blade elements were designed for efficient alignment of supersonic flow to the suction surfaces in the entrance region. Blade design also included a stream-tube analysis to obtain the desired values of critical area ratio (a/a^*) in channels between blades.

In addition to the multiple-circular-arc rotor, a slotted rotor and a tandem rotor were designed in order to evaluate advanced concepts. The slotted rotor was designed to reduce over-all blade shock losses. It provides an oblique shock, caused by the slot discharge flow, which lowers the Mach number upstream of the normal shock and decreases normal shock losses. The combination of an oblique shock and a normal shock results in a greater efficiency than a strong normal shock. The tandem rotor was designed with a supersonic forward blade and a subsonic rear blade so that the shock impinges on the forward blade and is isolated from the subsonic suction surface by a stream of high-energy air. Design details of the three rotors and the stator are given in Reference 5.

The purpose of this program is to extend the scope of available design information. Experimental evaluations include over-all performance with uniform inlet flow and with radial and circumferential distortions, and blade-element performance with uniform and radially-distorted inlet flow.

This report presents the test results for the multiple-circular-arc rotor and stator.

III. APPARATUS AND PROCEDURES

A. Test Facility

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The test program was carried out in a sea-level compressor test facility (Figure 1). The stand is equipped with a gas-turbine-drive engine which uses a 2.1:1 gearbox to provide optimum speed-range capability.

Air enters through a calibrated nozzle for flow measurements. A 72-foot straight section of 42-inch-diameter pipe runs from the nozzle to a 90-inch-diameter inlet plenum. Wire-mesh screen and an "egg-crate" structure, located midway through the plenum, provide a uniform pressure profile to the compressor.

The compressor airflow is exhausted into a toroidal collector and then into a 6-foot-diameter discharge stack, which contains a six-foot-diameter valve to provide back-pressure, or throttling, for the test compressor. Two smaller valves in the by-pass lines, one 24-inch and one 12-inch, provide vernier control of back-pressure.

Inlet distortion patterns are generated by screens of varied porosity which are attached to the 1 x 1-inch-mesh support screen. Twelve struts, thirty-three inches upstream of the rotor leading edge, are used to support the radial and circumferential screens for distortion tests. The method of attaching the distortion screens is shown in Figures 2 and 3. The distortionscreen support is removed for uniform-inlet testing as shown in Figure 4. Strain-gage and static-pressure instrumentation is routed through the nonrotating nose fairing. Ten struts, fourteen inches upstream of the rotor leading edge, support the forward bearing and straingage slip-ring assembly. Eight struts, eleven inches downstream of the stator trailing edge, support the rear bearing.

B. Test Compressor

Design of the stage flowpath was guided by the aerodynamic objectives outlined in detail in the design report (Reference 5). The rotor inlet flow per unit of annulus area was set at 42 lb/sec/ft^2 . The test compressor (Figure 5) is a single-stage, axial-flow design with no inlet guide vanes, thirty rotor blades and forty-four stator blades, each of constant chord length.

The stator-blade leading edge is 1.2 inches behind the rotor trailing edge at the hub. Running tip-clearance was 0.050 inch at 100 percent of design speed. Rotor and stator designs are summarized as follows; complete descriptions are given in Reference 5.

Rotor

The rotor was designed to operate at a tip speed of 1600 ft/sec with a constant spanwise pressure ratio of 2.0 and an over-all adiabatic efficiency of 88.7 percent. The thirty multiple-circular-arc blades have a constant 4.4-inch chord, an aspect ratio of 1.663 and a hub-to-tip ratio at the rotor inlet of 0.5. Relative Mach numbers at the rotor inlet are 1.6 at the blade tip and are supersonic over nearly the entire span. Photographs of the rotor

blade and the blade disk assembly are shown in Figures 6 and 7. A summary of the rotor blade metal angles for 9 streamlines passing through 5, 10, 15, 30, 50, 70, 85, 90 and 95 percent span of the rotor blade trailing-edge passage height from the hub is given in Table 1.

TABLE 1

Rotor Design Parameters Stations 8 and 9

% Span	<u>Dia - 1</u>	<u>Dia - 2</u>	β* ₈	<u>β*</u> 9	β [*] 9ss	<u>ß*sh</u>	σ
5(hub)	17.47	19.77	48,97	1.87	55.40	45.74	2.276
10	18.47	20.41	49,59	9.63	56.02	46.76	2,173
15	19.47	21.05	50.44	16.51	56.59	47.76	2.080
30	22.31	22 96	53.77	29.73	57.87	50.53	1.855
50	25.79	25.52	56.40	42.30	59.30	54.68	1.638
70	28.95	28.08	59.08	50.53	61.07	59.17	1.476
85	31.29	29.99	61.63	54.11	62,96	63.01	1.379
90	31.88	30.63	62.53	55.10	63.65	64.18	1.355
95(tip)	32.50	31.27	63.21	55.84	64.14	64.96	1.332

NOTE: Symbol definitions appear in Appendix 2.

Stator

The 44 multiple-circular-arc stator blades have a constant chord of 3.0 inches and an aspect ratio of 1.721. Photographs of the stator blade and the stator assembly are shown in Figures 8 and 9. Stator inlet Mach numbers are subsonic with a maximum value of 0.89 occurring at the hub, where the diffusion factor is 0.6. Design incidence to the stator suction surface was set at zero degrees. Stator exit flow is axial. A summary of the stator blade metal angles for 9 streamlines passing through 5, 10, 15, 30, 50, 70, 85, 90 and 95 percent of the rotor-blade trailing-edge passage height from the hub is given in Table 2.

TABLE 2

Stator Design Parameters

Stations 10 and 11

% Span	Dia-1	Dia-2 $\beta = 10$	<u>β*11</u>	<u>β* 10ss</u>	<u>β</u> * sh	Solidity
5 (hub)	20.41	21.49 43.23	-12.41	46.15	38.47	2.010
10	21.01	21.96 42.27	-11.44	45.21	36.62	1.959

TABLE 2 (CONT'D)

Stator Design Parameters

Stations 10 and 11

% Span	Dia-1	$\underline{\text{Dia-2}} \underline{\beta * 10}$	<u>\$* 11</u>	β* 10ss	β^* sh	Solidity
15	21.59	22.43 41.42	-10.89	44.36	34.94	1.911
30	23.31	23.90 39.44	-11.22	42.44	31.18	1.781
50	25.60	25.89 37.60	-12.04	40.72	28.01	1.632
70	27.82	27.90 36.45	-13.48	39.68	26.38	1.508
85	2 9.4 1	29.38 36.12	-15.91	39.44	26.82	1.430
90	29.91	29.86 36.15	-17.40	39.48	27.36	1.407
95 (tip)	30.38	30.29 36.33	-19.69	39.69	28.40	1.387

C. Instrumentation and Calibration

Airflow was measured within 1 percent, using a flow nozzle designed to ISA specification (Reference 6). Compressor speed was measured with an electromagnetic pickup that counts the number of gear teeth passing in an interval of time and converts the count into revolutions per minute. Measurement accuracy is better than 0.2 percent of indicated speed between 4,000 rpm and 13,000 rpm.

All temperatures were measured using chromel-alumel Type K thermocouples and recorded in millivolts by the automatic data-acquisition system. Temperature elements were calibrated over their full operating-temperature range for Mach-number and total-pressure effects. The thermocouple leads were calibrated for each temperature element. Overall RMS temperature accuracy was estimated to be $\pm 1.0^{\circ}$ F.

Disk probes were calibrated for Mach number as a function of indicated static-to-total pressure ratio, with pitch angle as a parameter. Total-pressure recovery and yaw-angle deviation were calibrated as functions of Mach number and pitch angle. The measurement accuracy of the air-angle probe was within 1.0 degree.

All pressures from probes, fixed rakes, and static taps were measured with transducers and recorded in millivolts by the automatic data-acquisition system. The accuracy of the pressure readings was ± 0.2 percent of the full-scale value.

Ten quartz-crystal, high frequency-response pressure transducers were installed in the case over the rotor tip to measure instantaneous static-pressure fluctuations. Ten wall static-pressure taps were installed o' er the rotor-blade tip in axial locations corresponding to the pressure transducers to measure the average static-pressure level.

Three proximity detectors, circumferentially positioned an integral number of blade gaps from the pressure transducers, generated an electrical pulse for each blade passing. Signals from both the pressure transducers and the proximity detectors were recorded by a multichannel tape recorder on the same time reference.

Figure 10 shows the rotor-blade tip-shock pressure instrumentation in relation to the blades. Photographs of typical instrumentation are shown on Figure 11. The axial and circumferential positions of the instrumentation are shown in Figures 12 and 13.

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Pressure measured by the fixed radial total-pressure rakes at the rotor leading edge (Station 7 in Figure 12) were in place only during the distortion testing. Instrumentation for measuring over-all and blade-element performance data is listed in Table 3.

TABLE 3

Performance and Blade Element Instrumentation

All measurements recorded by automatic data acquisition system unless noted otherwise.

Instrun				
Plane Location		Parameter	Type and Quantity	
Station 0	plenum chamber	Р	6 pressure taps on plenum wall (2 read on manometers)	
		Т	6 bare-wire thermocouples (2 read on self-balancing precision potentiometers)	
Station 1.1	bellmouth			
	instrumentation ring	∆P = P-p	6 pitot-static probes at mid- channel and evenly spaced about the instrument ring. ΔP water and acetylene tetra- bromide manometers. (After initial check point the bellmouth pitot-static probes were re- moved.)	

TABLE 3 (CONT'D)			
Plane Location	Parameter	Type and Quantity	
	р	4 O.D. wall static taps	
Station 5.1 inlet duct 5.2 6.1 6.2 7.1	р	2 O.D. and 2 I.D. wall static taps, 180 degrees apart	
Station 7 rotor inlet (within 1/2 chord)	Ρ, ρ,β	2 disk traverse probes, 9 radial positions	
	р	4 O.D. and 4 I.D. wall static taps	
	Р	2 fixed rakes, 180° apart, each with sensors at nine radial positions	
Station 8.5 rotor shroud	р	10 rapid response pressure transducers mounted in axial line over rotor tip. Recorded on magnetic tape.	
	р,	10 O.D. wall static taps in axial line over rotor tip	
	Blade Passing	Three proximity detectors positioned apart from the pressure transducers and in a line at the rotor-blade tip- chord angle. Recorded on magnetic tape.	
Station 10 stator leading edge	р	4 O.D. and 4 I.D. wall static taps equally spaced and locat- ed on extension of mid- channel lines	
	p	4 O.D. and 4 I.D. wall static taps spaced across one vane gap	

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TABLE 3 (CONT'D)

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Instrument		
Plane Location	Parameter	Type and Quantity
	Р	2 sets of impact tubes at 9 radial locations
Station 12 stator exit	Р	2 circumferential wake rakes (15-element) traversable to each of nine radial locations. Each wake rake spans at least one vane gap at O.D.
Station 12 stator exit	Τ	7 fixed radial rakes, each with temperature sensors at 9 radial positions. 6 probes spaced circumferentially to obtain readings evenly dis- tributed across a vane gap. The 7th rake is a duplicate mid-gap rake, and spaced 180 degrees from the other mid-gap rake.
	Ρ, p,β	2 disk traverse probes, 9 radial positions. Probes spaced 180 degrees apart. One traverse mechanism capable of tangential probing across a vane gap
	р	4 O.D. and 4 I.D. wall static taps
	p	4 O.D. and 4 I.D. wall static taps spaced across vane gap
Station 13.1 rig exit	Р	1 fixed five-element radial rake

Note: The nine radial positions of each axial station are defined by the intersection of the axial station and the design streamlines which pass through 5, 10, 15, 30, 50, 70, 85, 90, and 95 percent of the passage height at the rotor trailing edge.

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Table 4 shows the parameters that were continuously recorded during excursions into stall to detect and evaluate rotating stall. Three rapid-response pressure transducers, located at the rotor exit at 25, 50, and 85 percent of blade height from the hub and at unequal circumferential locations, were used to record pressure pulses continuously on a multi-channel tape recorder when operating near or within the stall region.

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TABLE 4

Stall Transient Instrumentation

Instrument Plane Location	Parameter	Type and Quantity
Inlet orifice	р	l static tap downstream of inlet orifice
Station 7 rotor inlet	р	1 O.D. wall static tap
Station 9 rotor exit	P frequency	3 rapid-response pressure transducers at unequal circum- ferential spacing. Sensors located at 25, 50 and 85% of blade height from hub
	р	1 O.D. wall static tap
Station 10 stator leading edge	P	3 impact tubes at 5, 50, and 95% of passage height from hub
Station 12 stator exit	р	1 O.D. wall static tap
Station 13.1 rig discharge	Р	l element of fixed radial rake
gearbox	N	impulse pick-up

Critical stationary and rotating parts were instrumented with strain gages to determine the levels of continuous stress due to centrifugal and blade untwist loads and vibratory stress over the operating range of the compressor.

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D. Test Procedure

1. Shakedown Test

Before taking performance data, shakedown tests were conducted to establish the mechanical integrity of the compressor and to locate critical stress boundaries which might limit the operating range over which the tests could be conducted.

Accelerations were made to 50, 70, 90, 100, and 115 percent of design speed, with open discharge throttle and uniform inlet flow. Continuous and vibratory stresses of the rotor and stator were recorded. A rotor blade resonance with two excitations per revolution was detected at 12,600 RPM, and maximum speed for performance testing was set at 105 percent of design speed in order to avoid it. Continuous stress due to centrifugal and untwist loads was slightly lower than predicted and did not limit test speeds.

Stress and rotating-stall surveys were made with uniform, radially-distorted, and circumferentially-distorted inlet flow. Vibratory stresses were recorded similataneously with transient readings of the parameters shown in Table 4 in order to correlate blade stress with stall. In all surveys, vibratory stress at stall increased with speed and closely approached the maximum allowable transient stress at design-speed. Stress boundaries for steady-state operation were defined with radially and circumferentially distorted flows. Rotor blade vibratory stress increased as the compressor was throttled, which prevented steady-state operation near stall. The range of operation was severely limited by high stresses with radial distortion, making it necessary to increase screen porosity. A satisfactory operating range was obtained by reducing the distortion parameter (P_{max} - P_{min}/P_{max}) from 0.20 to 0.16. Beyond the boundary for steady-state operation, only transient data were recorded.

Rotating stall was detected by measuring pressure fluctuations with rapid-response transducers at 25, 50, and 85 percent of passage height. Continuous recordings were made as the throttle was closed until the compressor stalled and as the throttle was opened to recover from stall. Several surge pulses were recorded before the throttle could be opened enough to get the compressor out of stail.

Five over-all and blade-element performance data points, over a range of flows between wideopen throttle and stall at design speed, were taken during the shakedown test. A disk probe was traversed tangentially across a stator-blade gap at the stator exit to measure total pressure, static pressure and flow angle at each of nine radial positions for each of the five performance points. Gapwise distributions of static pressure and air angle, determined by tangential traversing, were compared to mid-gap values measured by a radial traverse probe. Averaged circumferential values were close to mid-gap values, and remaining tests were made without tangential traversing. Simultaneous immersion of all traverse probes was possible without causing data inaccuracies due to probe blockage effects.

2. Uniform-Inlet-Flow Performance Test

Six performance points, ranging in flow from open-throttle to near-surge, were obtained at 50, 70, 90, 100, and 105 percent of design speed, and stall flows were measured at 50, 70,

90, and 100 percent of design speed. The periodic static pressure fluctuations over the rotor tip were recorded at three points at 70 percert speed, four points at 90 percent speed, five points at 100 percent speed, and three points at 105 percent speed, ranging in flow from choke to near-stall. These data were obtained to show the static-pressure-field relative to the rotor blade tip, indicating shock position and strength.

3. Distorted-Inlet-Flow Performance Test

The rotatable distortion-screen support was added to the flow path 33 inches upstream of the rotor leading edge. Open-throttle, part-throttle, and near-stall performance points at 70, 90, and 100 percent of design speed, with the distortion support but with no distortion screens attached, showed that the support screen did not affect uniform inlet performance. A radial screen covering one-fifth of the inlet area (Figure 2) was required to create a radial-distortion pattern covering two-fifths of the rotor inlet area. A i 20-degree, full-span screen (Figure 3) was required to produce a 90-degree circumferential pattern with a distortion parameter of 0.20 at the rotor inlet, with the throttle wide-open at 100 percent of design speed.

Performance data with both radial and circumferential inlet-flow distortion were taken at 70, 90, and 100 percent of design speed, with the discharge throttle at three positions (wide-open, part-throttle, and near-surge), except where high stresses prevented taking near-stall data points. Each circumferential-distortion data point was taken with the screen in six different positions with respect to the compressor instrumentation.

E. Calculation Procedure

Data reduction was accomplished in three steps:

- 1. Raw data were converted from electrical values to engineering units and thermocouple-wire corrections were applied.
- 2. Aerodynamic corrections and averaging techniques were used to obtain radial distributions of circumferentially-mass-flow-averaged pressures, temperatures, and angles
- 3. Blade-element data were calculated for uniform and radial distortion tests, using a flow-field calculation procedure.

Aerodynamic corrections and averaging techniques were:

1. Total-pressure probes located in supersonic flow were corrected for shock losses. Total pressures from the two wake rakes were circumferentially mass-flow-averaged at each radial position, using a constant static pressure obtained by a linear interpolation between wall static pressures. Free-stream values of total pressure downstream of the stator (peak wake rake values) were selected at each radial position. A wake blockage factor was also calculated at each radial location, as defined in Appendix 1, and used in a flow-field calculation program to improve the accuracy

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of the static pressure and velocity calculations at the stator exit. Free-stream and circumferentially mass-flow-averaged pressures and wake blockage factors were each arithmetically averaged from the two rakes at each radial location to be used in the flow-field calculation.

- 2. Temperature probes were corrected for Mach number recovery, including the pressure-level effect. Six radial rakes were approximately equally-spaced about the annulus at the stator exit, and located at different circumferential positions relative to a stator gap. A circumferential mass-flow average was calculated at each radial position and used in the flow-field calculation. Circumferential wake-rake totalpressure distributions were used for the circumferential mass-flow-averaging of the stator exit temperatures.
- Over-all performance calculations were based on the inlet plenum pressure as a 3. reference for uniform inlet flow, and on an arithmetical average of radially massaveraged pressures from the two radial rakes at the rotor inlet for radially-distorted inlet flow. The reference pressure for circumferentially-distorted inlet flow was the arithmetical average of twelve radially-mass-averaged pressures obtained from the two radial rakes at the rotor inlet for each of the six screen positions. The relationship between plenum and rotor inlet total pressure was correlated as a function of corrected flow (Figure 14). Calculations of corrected flow, pressure ratio, and efficiency were based on pertinent reference stage inlet pressures. All averaging techniques were the same for both uniform and radially-distorted inlet flow. For circumferential distortion tests, a different technique for stator-exit pressure and temperature averaging was used. Radially mass-flow-averaged values of pressure from the two wake rakes at each screen position were arithmetically averaged. This pressure was used for over-all pressure ratio and efficiency calculations. Data from each of the six individual temperature rakes were radially mass-averaged for each screen position, and the 36 resulting values were arithmetically averaged. This temperature was used for overall efficiency calculations. Circumferential distributions of static and total pressure (Appendix 5) are ratioed to the inlet plenum.
- 4. Velocity vectors were calculated from disk probe traverse data for nine radial locations at the instrumentation planes upstream of the rotor and downstream of the stator. Measurements at each probe position were used to determine corrected total pressure and calculated static pressure, Mach number, and air angle. Calibrations of individual probes were used to correct the raw data. Each probe was first calibrated for Mach number under controlled wind-tunnel conditions, and test Mach number was then determined from the ratio of measured static to measured total pressure. Total pressure and yaw angle corrections were made by using calibrations versus Mach number. Static pressure was calculated by using the corrected total pressure and the calibrated Mach number. An arithmetical average of the two stator-exit-probe-angle readings for each radial position was used in the flow-field calculation.

Blade-element performance for uniform-inlet and radial-inlet-distortion test points was calculated by a flow-field analysis computer program. All parameters were corrected to standardday conditions. The inputs were:

Compressor Inlet	1)	corrected weight flow
	2)	corrected rotor speed
Rotor Inlet	1)	total pressure versus radius
Instrument Plane	2)	blockage factor versus radius (to account -
		for estimated wall boundary layers)
Stator Inlet	1)	total pressure versus radius
	2)	blockage factor versus radius (to account
		for estimated wall boundary layers)
Stator Exit	1)	total temperature versus radius
Instrument Plane	2)	total pressure versus radius
	3)	blockage factor versus radius (to account
		for stator wake blockage and wall boundary angle)
	4)	absolute air angle versus radius

All pressures and temperatures are expressed as ratios to mass-averaged values at the rotor inlet.

All static-pressure distributions and air angles behind the rotor were calculated by assuming axisymmetric flow and consideration of mass-flow continuity, radial equilibrium, and energy equations. Curvature, enthalpy, and entropy gradient terms were used in the equilibrium calculations. Blade-element performance parameters at the blade edges were calculated by translating the measured data from the instrument plane along streamlines which passed througn the rotor trailing edge at 5, 10, 15, 30, 50, 70, 85, 90, and 95 percent of the passage height. Blade-element parameters were calculated at airfoil sections lying on conical surfaces defined by the intersections of these streamlines and the blade edges. Pertinent performance parameters are defined in Appendix 3.

Static pressure contours over the rotor blade tips were obtained by using continuously-recorded pressure fluctuations, which were measured by high-frequency-response transducers. Ten transducers were distributed axially over the blade tip (Figure 10), and ten wall static pressure taps were located at the same axial positions to measure average static pressure. Records of fluctuating pressures versus time indicated that the transducers were not in agreement in terms of known blade location, and the signals were oriented by positioning the pressure drop caused by the passing of the suction surface in relation to the actual position of the blade. A computer program converted electrical signals from the transducers to pressure fluctuations for one blade-passing time period, with each transducer referenced to the same point in time. The program then added average pressure to the pressure fluctuations at each axial position. The full range of pressure variation for a given point was broken into ten equal increments and a code number assigned for each increment of pressure range (see page 100 for the static pressure code), e.g., a code of 5 means that the pressure in the region lies in the range of 5 to 6 psia. Regions of constant pressure were outlined by displaying the code numbers relative to the blade tips across two blade gaps.

IV. RESULTS AND DISCUSSION

The results of the multiple-circular-arc rotor test were discussed under the headings of shakedown tests, uniform-inlet-flow performance, distorted-inlet-flow performance, and rotorblade-tip static pressure contours.

Shakedown test results include stress and rotating stall data for uniform and distorted inlet flows and an evaluation of traversing methods. Over-all performance of the rotor and stage are presented for uniform and distorted inlet flows in terms of pressure ratio and efficiency versus corrected weight flow $(W\sqrt{\theta/\delta})$ with corrected speed $(N/\sqrt{\theta})$ as a parameter. Rotor and stator blade-element performance curves are presented for uniform-inlet-flow and for radially-distorted-inlet-flow tests. Loss coefficient, diffusion factor, and deviation are presented as functions of incidence at radial locations on streamlines passing through 5, 10, 15, 30, 50, 70, 85, 90, and 95 percent of the rotor-blade exit passage height from the hub. For circumferentially-distorted-inlet-flow tests, circumferential distributions of pressure, velocity, and air angle are included to describe the extent of distortion on the rotor inlet and stator exit.

Rapid-response static-pressure data over the rotor blade tips are presented as contours outlining regions of constant static pressure and are shown with respect to the rotor-tip blade gap. The blade-tip shock was located by the instantaneous pressure rise in the blade passage.

A. Shakedown Tests

Continuous stresses due to centrifugal and untwist loads were measured near blade root leading and trailing edges and were slightly lower than design predictions. Using the design prediction of stress distribution, the maximum blade stress was 60,000 psi on the pressure surface at 10 percent span from the hub. Predicted stress at this location was 61,000 psi.

Vibratory stress with uniform inlet flow was not high except at stall, but a resonance with two excitations per revolution appeared at 12,600 RPM, which is 109 percent of design speed when corrected for 100° F ambient temperatures. This resonance limited performance testing to 105 percent of design speed. During stall at design speed, the blade tip vibratory stresses were approximately 20,000 psi. The mode of this tip vibration was shown in laboratory tests with stress-coated blades (Figure 15). Since stall stress levels increased rapidly with speed, a stall point was not run at 105 percent of design speed.

The maximum allowable vibratory stress of 15,000 psi for steady-state operation limited the range of operation with radially and circumferentially distorted inlet flows. Stress boundaries for radially-distorted inlet flow are discussed in Section IVC1, Radially-Distorted Inlet Flow, Overall Performance. Stress boundaries for circumferentially-distorted inlet flow will be found in Section IVD1, Circumferentially-Distorted Inlet Flow, Over-all Performance. With both types of distortion, the maximum stress during stall was 23,000 psi at design speed and was increasing rapidly with increasing speed.

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Stall surveys with rapid-response instrumentation showed that stalls were abrupt, originating near the tip and progressing to mid-span and the root. An oscillograph trace at 90 percent speed with uniform inlet flow (Figure 16) shows the general pattern for all stalls. All stalls appeared as surge cycles with a frequency of approximately 3 cps, each cycle consisting of a surge pulse lasting approximately 0.17 seconds and a stall recovery lasting approximately 0.14 seconds. At the start of each surge pulse, pressure fluctuations with a period of about one rotor revolution occurred at the tip and mid-span, indicating the presence of rotating stall cells (Figure 17). Pressure dropped sharply after this initial phase and then rose toward the pre-stall level. The stall-recovery portion of the cycle began with a strong pressure rise, followed by a gradual pressure reduction. Similar stall patterns were observed with radially and circumferentially distorted inlet flows.

Tangential traverses of stator exit total pressure, static pressure, and air angle were taken at five points with uniform-inlet flow design speed. Circumferential distributions across a stator blade gap for open-throttle, part-throttle, and near-stall settings at 10, 50, and 90 percent span from the hub are presented in Figures 18, 19, and 20. Variations ot air angle and static pressure across the stator gap are small except when the discharge throttle is wide open. To-tal pressure distributions from the tangentailly-traversed disk probe and from the two radially-traversed wake rakes are compared in Figure 21 at the near-stall throttle setting.

Stator exit total pressure, static pressure, and air angle versus percent span for the near-stall point at design speed are shown in Figure 22. Mass-averaged total pressures across a stator gap, calculated from the tangentially-traversed disk probe and from the wake-rake measurements, were in good agreement. Static-pressure and air-angle measurements from a radially-traversed disk probe in the center of the stator-blade gap were compared to the mass-averaged static pressure and average air angle, calculated from the tangentially-traversed probe. Since these results also showed good agreement, it was concluded that tangential traverse would have almost no effect on over-all and blade-element performance parameters.

B. Uniform-Inlet-Flow

1. Overall Performance

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Over-all performance of the rotor only and the stage is presented in Figures 23 and 24. Tabulated results are presented in Appendix 3. The stall line was established by extrapolating the characteristic speed lines to measured stall airflows, shown as slashed symbols. Stalled operation above 100 percent of design speed was avoided because of high rotor-blade tip stresses. A maximum stage efficiency of 84.5 percent (Figure 24) at a pressure ratio of 1.946 and a corrected weight flow of 180.4 lb/sec was achieved at design speed, compared with a design stage efficiency of 84.2 at a pressure ratio of 1.936 and a corrected weight flow of 187.1 lb/sec. The rotor efficiency for the same data point (Figure 23) was 89.0 percent for a pressure ratio of 2.01, compared with a design rotor efficiency of 88.7 percent and pressure ratio of 2.00. The inability to achieve design flow was probably caused by local choking at the rotor blade root, as suggested by the high losses in this region with the discharge throttle wide open. Maximum rotor and stage efficiencies, as shown by Figures 23 and 24 are essentially constant over the range of compressor operation between 50 and 100 percent of design speed but decrease 3 percent at 105 percent of design speed. Although a stall point was not obtained at 105 percent speed because of stress limitations, the peak efficiency performance point was identified. The abrupt decrease in peak efficiency above design speed was the result of increased rotor-blade losses from 50 percent span to the blade tip. Stator losses at 105 percent of design speed are no higher than at design speed. The fact that rotor efficiency at part speed did not rise significantly above the level obtained at design speed may be attributed to a rotor design characteristic: Channel areas between blades were designed to decelerate high Machnumber flow; and the converging channels between blades, optimized for design speed, were too small at part speed, forcing the rotor to operate at high incidence angles.

2. Blade - Element Data

Blade-element performance for a data point at design speed and near design pressure ratio agreed closely with design values. Figure 25 shows the rotor and stage adiabatic efficiency versus percent span from the hub, compared to the design. Total-pressure-loss coefficient, diffusion factor, incidence, and deviation are presented versus percent span from the hub for the rotor and stator in Figures 26 and 27. Blade-element performance parameters were calculated at stations corresponding to the actual leading and trailing edge of the blades (Stations 8 and 9 of Figure 12). Rotor and stator blade-element plots for the entire uniform-inlet performance test are presented in Figures 28 and 29, with data tabulated in Appendix 3.

Rotor incidence at design speed (Figure 26) was more positive than designed over the entire span because of the inability to attain design flow. Incidence at part speed was generally higher than at design speed because critical area ratios in channels between blades were sized for design relative Mach numbers, and they result in a lack of flow capacity at part speed. Maximum rotor diffusion factors were equal to, or exceeded, design values over nearly the entire span except at the blade hub, where they were lower than design. Rotor diffusion factor increased with increasing speed but levelled off at 100 and 105 percent of design speed. A maximum diffusion factor of almost 0.6 was achieved at 30 percent span from the hub, as compared to the design value of 0.55 at this span. Rotor deviations were greater than design, particularly at the blade tip, where a maximum difference of 5 degrees occurred. Minimum rotor losses (Figure 28) were equal to, or less than, design predictions, except at 105 percent of design speed. Stator deviations were in general agreement with design except at the end walls, and the diffusion factor exceeded design values except at 5 percent span. Stator losses and incidence agreed reasonably well with design values.

Loss coefficients at the rotor hub (Figure 26) were unrealistically low, and in some cases were slightly negative, while stator loss coefficients at corresponding spanwise locations (Figure 27) were greater than expected. The distribution of losses between the rotor and stator depends on rotor trailing-edge total pressure, which is used in the calculation of both loss coefficients (Appendix 1). In the data-reduction procedure used for these tests, the stator inlet total pressure is equal to the peak total pressure as measured by the stator trailing-edge wake rake at equivalent percentages of span. The gapwise distributions of total pressure at the stator exit for various percents of span (Figure 21) show that, at 10 percent span, the peak pressure occurs near the stator blade suction surface. The peak wake rake total pressure at this percent

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of span may not be an accurate ..pproximation of the average total pressure at the stator inlet. Because of the tendency of the low-pressure rotor wake flow to migrate toward the stator pressure surface (Reference 7), the peak value of total pressure downstream of the stator may be above the level of the average stator inlet pressure.

Peak wake-rake readings were used because they generally produce more reasonable bladeelement data than either the stator leading-edge traverse probes (which strongly affect rotor operation due to their blockage) or stator leading-edge impact tubes, whose recovery varies with stator incidence and which are difficult to maintain in good working order. The stator trailing-edge wake-rake impact tubes operate with a much smaller air-angle variation than those at the stator leading edge.

An alternate method for evaluating rotor exit pressure was also investigated. Plots of pressure and temperature across the stator gap reveal that areas of high total pressure are also areas of high total temperature, so that the local efficiency does not exceed 1.0. The gapwise distribution of total pressure ratio, total temperature ratio, and local adiabatic efficiency at the stator exit at 15 percent span for the maximum efficiency point at design speed (Figure 30), shows that the free-stream region of the efficiency plot appears to give a direct measure of rotor efficiency at a spanwise location. Using this efficiency with the corresponding spanwisemass-averaged temperature rise to calculate rotor exit total pressure profiles provides a more reasonable distribution of losses between the rotor and the stator. Figures 26 and 27 show spanwise distributions of rotor and stator blade-element performance for the two methods of determining rotor exit total pressure. The free-stream-efficiency method eliminates the problem of unrealistic efficiency and loss near the hub without affecting the other spanwise locations. Rotor deviations and stator incidences changed significantly when calculated with the free-stream-efficiency method.

Blade-element data for design-speed performance points are presented in Figure 28 and 29 for both methods of data reduction. Blade-element performance of the rotor and stator for the alternate method is tabulated in Tables 10.7 to 10.12 in Appendix 3.

3. Distortion Support Screen Effects

Open-throttle, part-throttle, and near-stall performance points were taken at 70, 90, and 100 percent of design speed with the distortion-screen support but without distortion screens. Since performance was not affected by the support screen (Figures 31 and 32), the uniform-inlet-flow performance provides a valid basis for determining effects of inlet-flow distortion.

C. Radially-Distorted Inlet Flow

A radial-distortion pattern which covered two-fifths of the rotor inlet area provided a distortion parameter of 0.16 with the discharge throttle wide open at 100 percent of design speed. Figure 33 shows the total pressure and meridional velocity at the rotor inlet versus percent span with radially-distorted inlet flow for wide-open and near-stall throttle conditions at 100 percent of design speed.

1. Over-all Performance

Over-all rotor and stage performance with radially-distorted inlet flow is presented in Figures 31 and 32. A 15,000 psi vibratory stress boundary prevented steady-state operation at a near-stall throttle setting at 70 and 90 percent of design speed. The stall line with radially-distorted inlet flow was lower than with uniform-inlet-flow. Maximum stage efficiency at design speed of 78.4 percent occurred at a pressure ratio of 1.774 and a corrected weight flow of 177.2 lb/sec, which was 6 percent lower than the maximum stage efficiency with uniform inlet flow. Maximum corrected weight flow at design speed was 4.5 lb/sec. lower than with uniform inlet flow.

2. Blade-Element Data

Rotor and stator blade-element performance for radially-distorted inlet tests is shown in Figures 34 and 35. Blade-element performance with radially-distorted inlet flow is compared with uniform inlet flow at 10, 50 and 90 percent span from the hub for the rotor and stator. The rotor-blade tip, with radially-distorted inlet flow, operated at increased positive incidence due to low axial velocity in the distorted region. The levels of loss, diffusion factor, and deviation at the rotor blade tip for design speed were essentially unaffected by the distortion. Rotor mid-span and root incidences were negative and losses increased. Stator-blade-tip incidences were slightly more positive than with uniform inlet flow and became negative at the root. Tabulations of the blade-element and over-all performance data for radially-distorted inlet flow are presented in Appendix 4.

D. Circumferentially-Distorted-Inlet-Flow

A circumferential distortion parameter of 0.20 covering a 90-degree arc was achieved at the rotor inlet with the throttle wide open at design speed using a 120-degree full span screen.

1. Over-all Performance

Over-all performance with circumferential inlet distortion is compared with uniform-inletflow performance in Figure 36. The maximum stage efficiency at design speed obtained with circumferentially-distorted inlet flow was 77.7 percent at a corrected weight flow of 173.1 lb/sec and a pressure ratio of 1.747. Flow range with circumferential distortion was higher than with radial distortion. This greater flow range gave a higher stall line even though stall pressure ratio was lower than with radial distortion. Stall flow at 100 percent of design speed occurred 15 lb/sec lower than with uniform inlet flow, but with an accompanying decrease in pressure ratio. Stall at 70 and 90 percent speed occurred at approximately the same flow as with uniform inlet flow, with a smaller decrease in pressure ratio than at design speed. High vibratory rotor-blade-tip stresses limited the range of steady-state operation at 90 and 100 percent of design speed. Because of the limited operating range, only two performance points were taken at 90 percent speed. Tabulations of circumferential distributions and overall stage performance are presented in Appendix 5.

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2. Circumferential Distributions of Velocity Vector Parameters

Rotor inlet circumferential distributions of total pressure, absolute and relative flow angle, absolute velocity, meridional velocity, and absolute Mach number are shown in Figures 37, 38, and 39 at 10, 50 and 90 percent span from the hub. Measurements from radially-traversed disk probes at the rotor inlet at twelve locations relative to the distortion, screen were used to construct these plots. Stator discharge circumferential patterns, measured by disk probes at stator mid-gap, are shown in Figures 40, 41, and 42. Circumferential distributions of static pressure at the rotor inlet on both the inner case and outer case are presented in Figures 43 and 44.

E. Rotor Blade Tip Static Pressure Contours

Static pressures over rotor blade tips were measured by ten high-frequency-response pressure transducers. Data were obtained over a range of compressor operating conditions at 70, 90, 100, and 105 percent of design speed with uniform inlet flow. Figure 45 shows four typical oscillograph traces of static pressure versus time. At the rotor leading edge, the static pressure rise caused by the shock occurs near the pressure surface and moves toward the suction surface at measurement locations downstream of the leading edge.

Shock position with respect to the blade tip is shown in Figures 46 through 60 as a series of points, each representing the location where the instantaneous static pressure rise was observed on the oscillograph traces. Contours outlining static pressure regions over the rotor blade tip are shown in Figures 49 through 54 and 58 through 60. A rotor performance characteristic and the axial distribution of wall static pressure over the blade tip are also included in the figures. Figures 49 through 52 show the rotor tip static pressure contours over a range of flows for 90 percent of design speed. Both expansion and compression fields are indicated by the contours ahead of the passage shock. The expansion (Figure 49) along the suction surface during flow alignment is followed by a compression field ahead of the passage shock. This precompression results from the blade shape at the entrance region, which was designed for precompression to reduce the passage shock loss. The static pressure rise in this shock is about equal to the rise in the precompression region. With open throttle, shocks are nearly attached and are oblique. As back pressure is increased, the shocks become stronger and farther detached. Normal shocks were never seen, even at near-stall operating points.

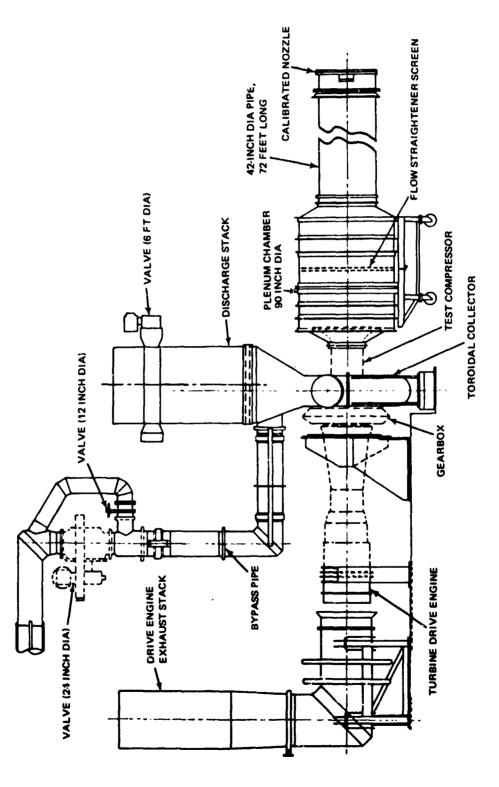
These data are considered qualitative due to the difficulties in obtaining highly accurate quantitative measurements of pressure fluctuations. In view of the inherent inaccuracies, no attempt was made to construct fields of relative Mach numbers or to calculate shock strengths.

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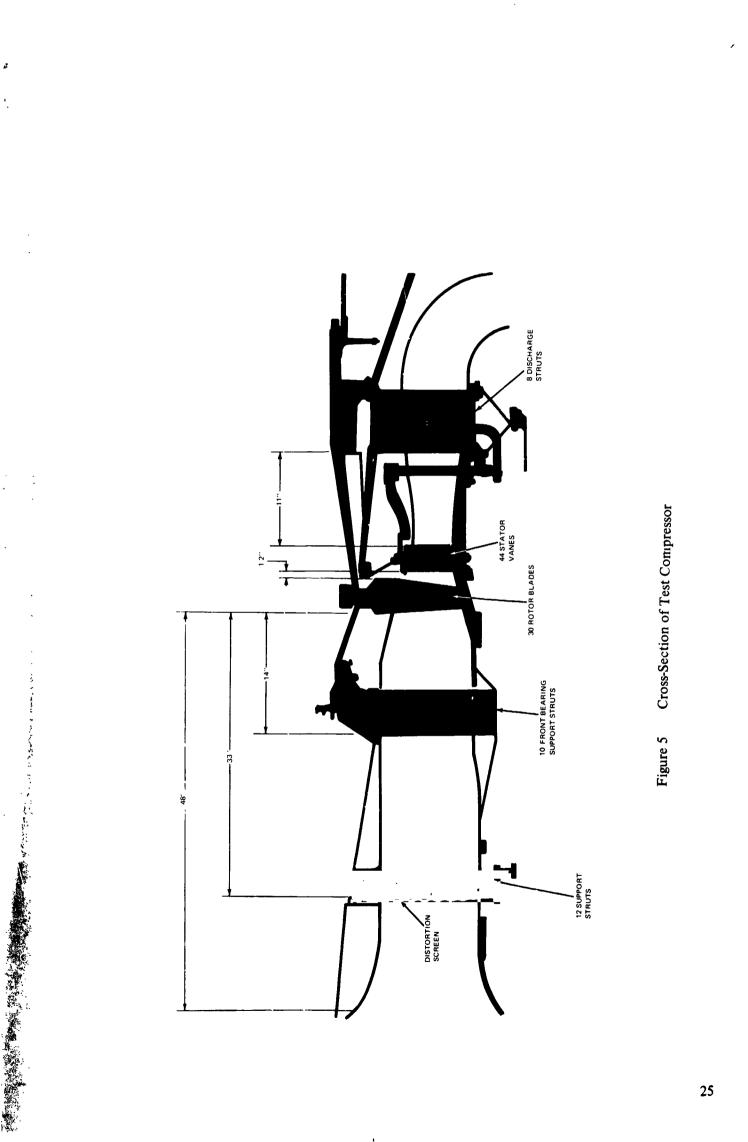
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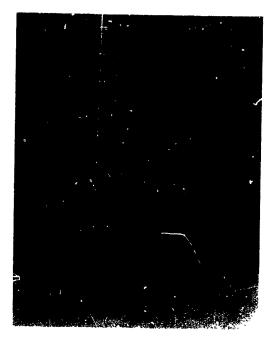
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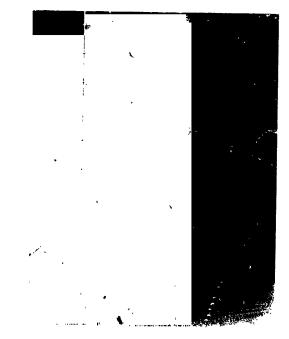
Convex Surface



Concave Surface



Leading Edge



Trailing Edge

Figure 6 Multiple-Circular-Arc Rotor Blade

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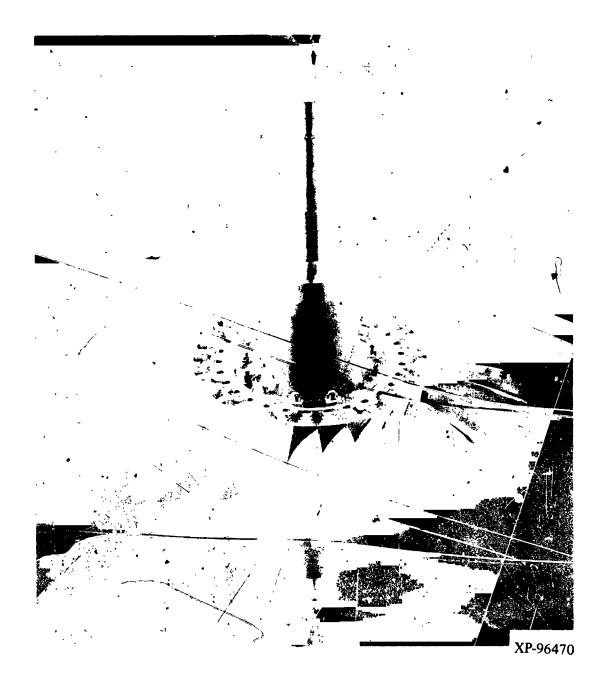


Figure 7 Assembled MCA Rotor

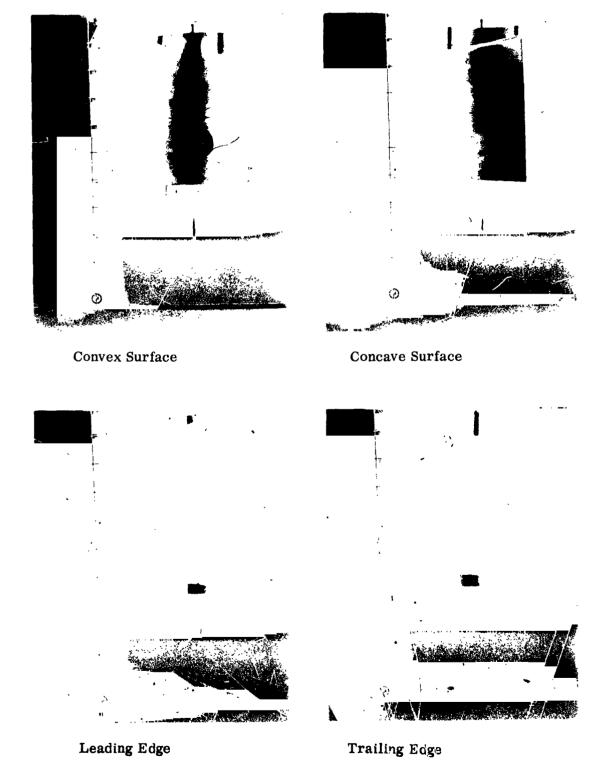
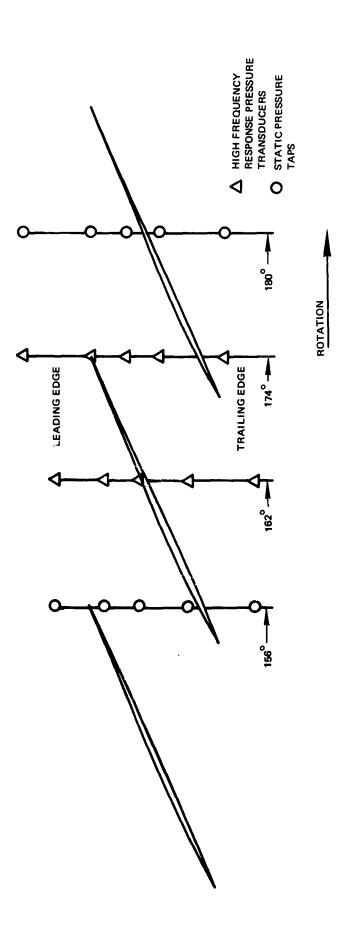


Figure 8 Multiple Circular-Arc Stator Blade

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Figure 9 Assembled MCA Stator





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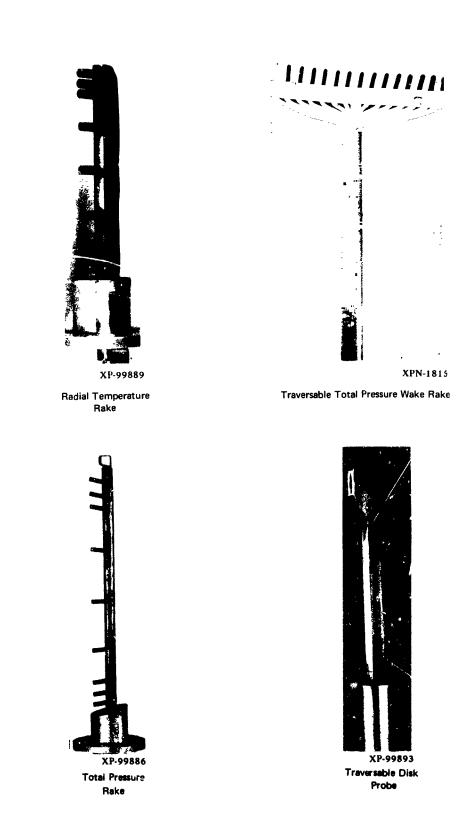
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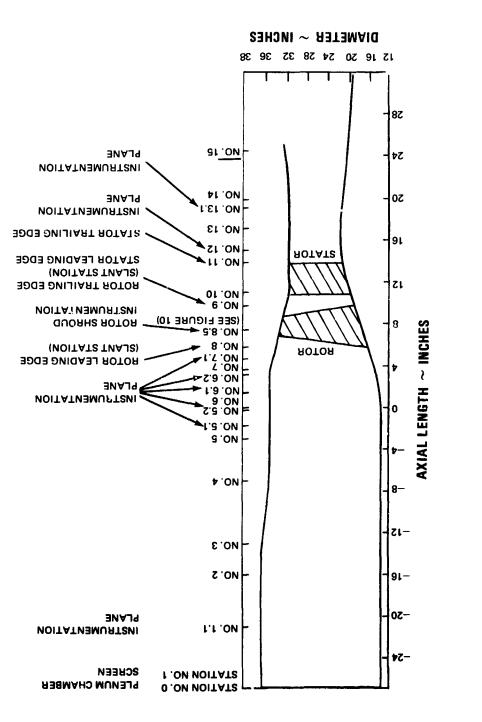
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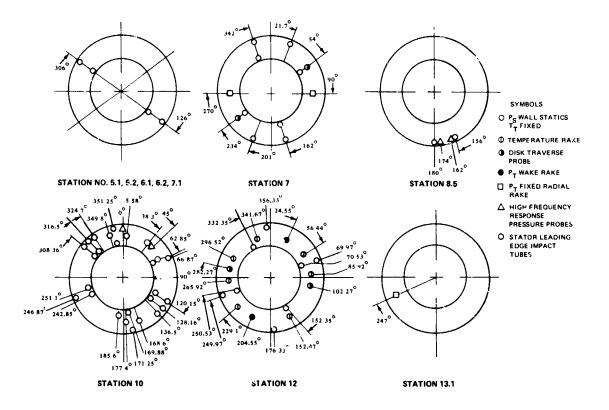
Figure 11 Typical Instrumentation





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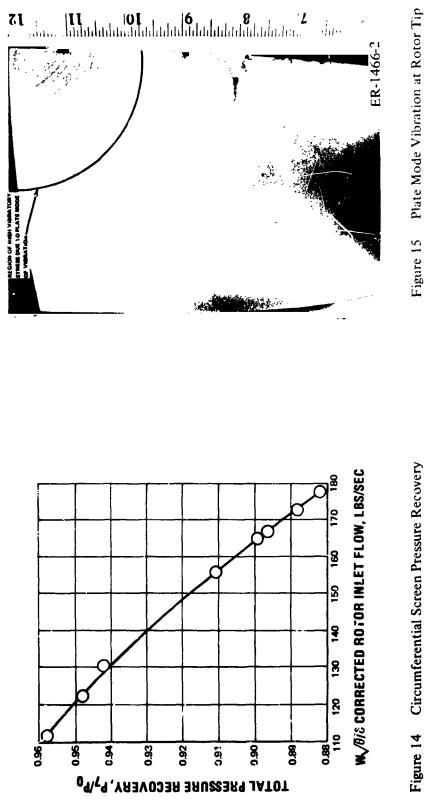
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Figure 13 Circumferential Location of Instrumentation, Viewed from Rear

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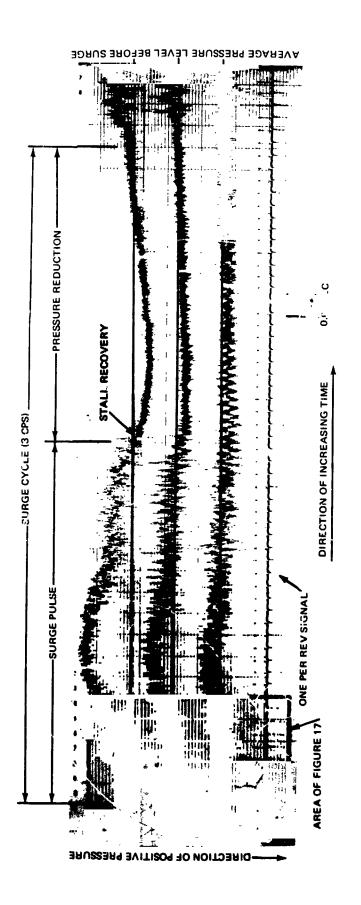
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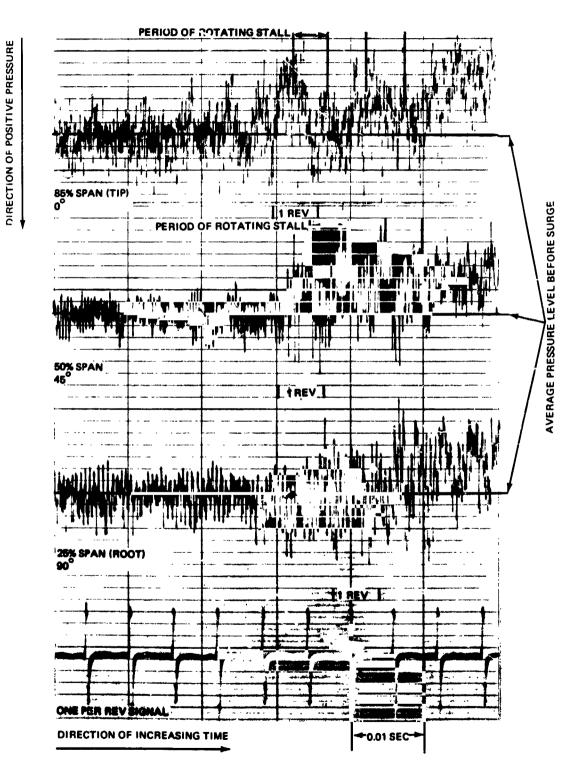
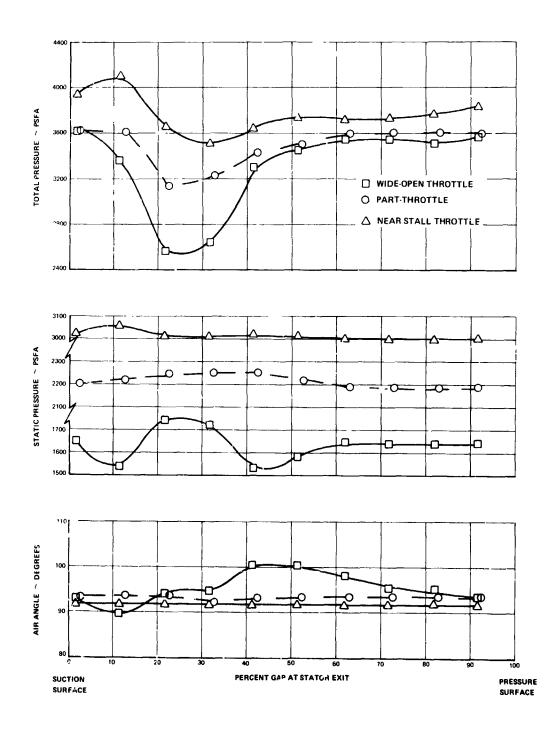


Figure 17 Oscillograph Trace of Typical Rotating Stall Pattern

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Figure 18 Circumferential Variation in Stator Exit Total Pressure, Static Pressure, and Air Angle from Tangential Traverses at Station 12, 100% Design Speed, 10% Span

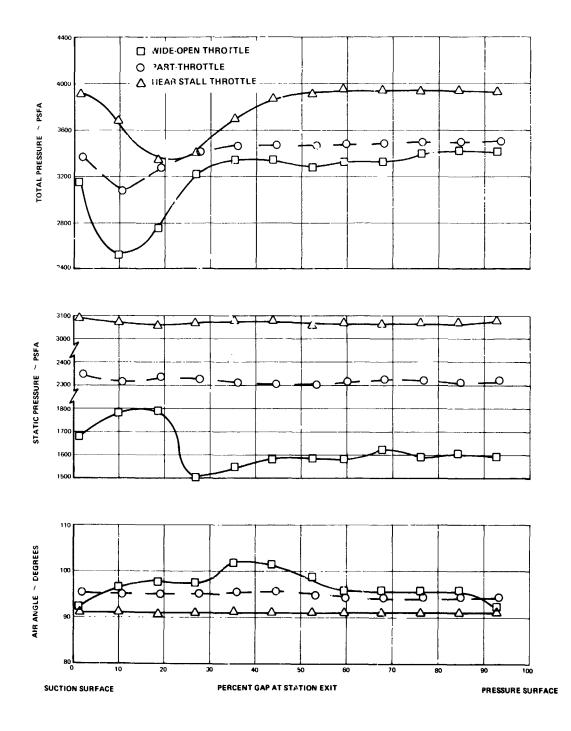


Figure 19 Circumferential Variation ir. Stator Exit Total Pressure, Static Pressure and Air Air Angle from Tangential Traverses at Station 12, 100% Design Speed, 50% Span

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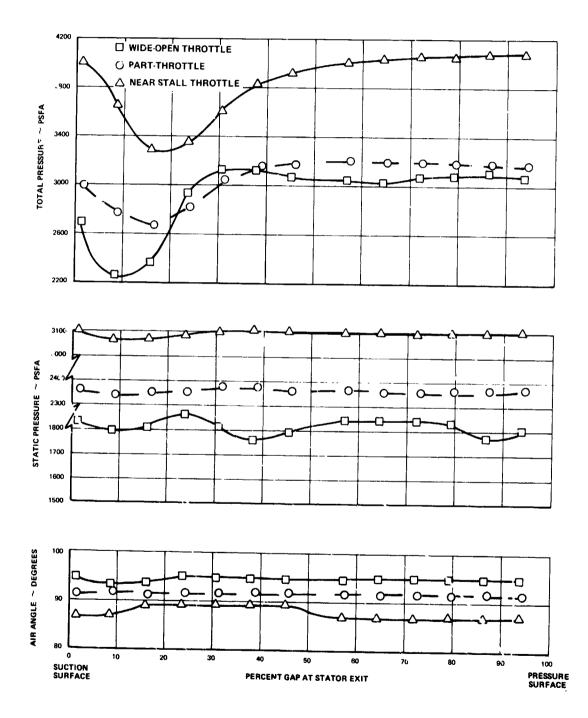
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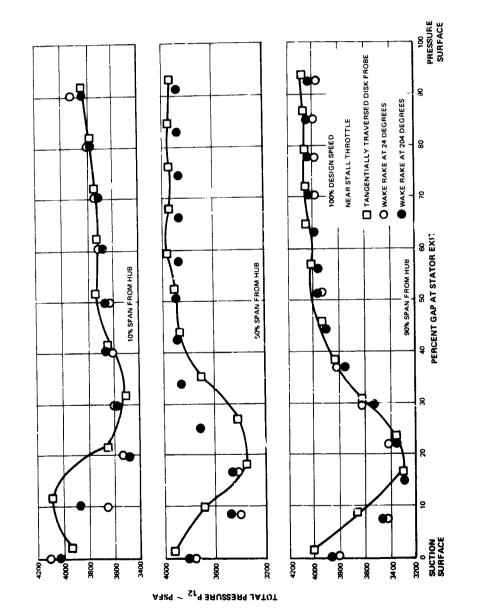
Figure 20 Circumferential Variation in Stator Exit Total Pressure, Static Pressure, and Air Air Angle from Tangential Traverses at Station 12, 100% Design Speed, 90% Span

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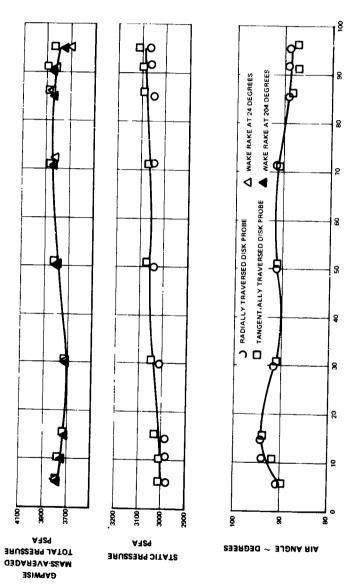
Comparison of Circumferential Variation in Stator Exit Total Pressure from Tangential and Wake Rake Traverses at Station 12, 100% Design Speed, 10%, 50%, and 90% Spans Figure 21

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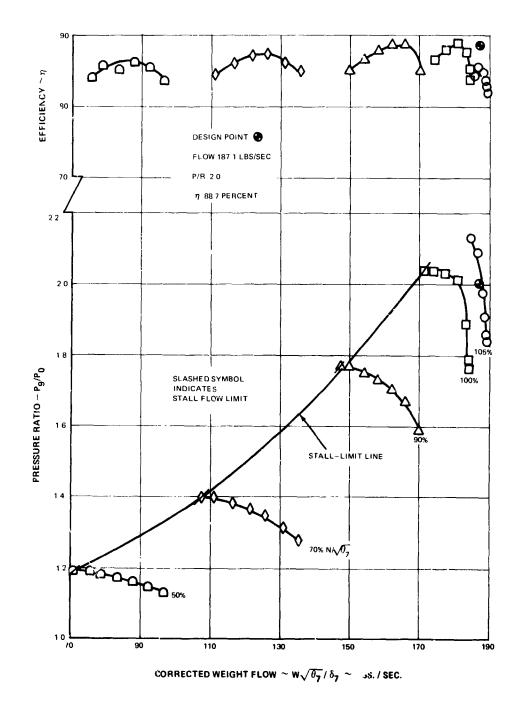
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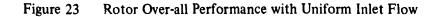
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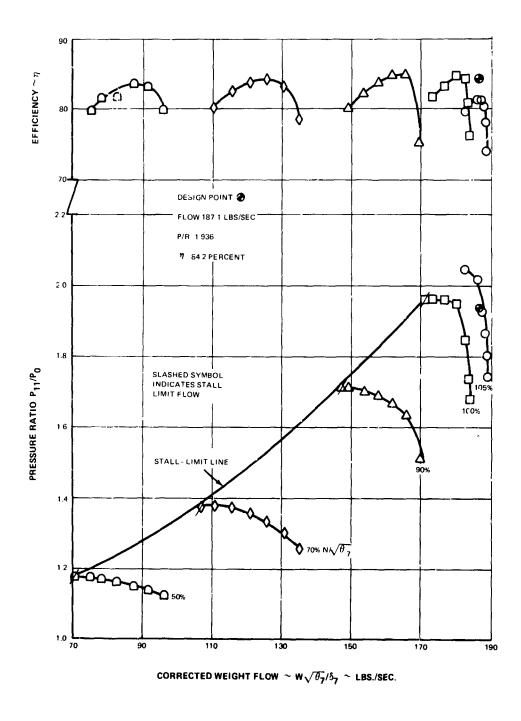
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Figure 24 Stage Over-all Performance with Uniform Inlet Flow

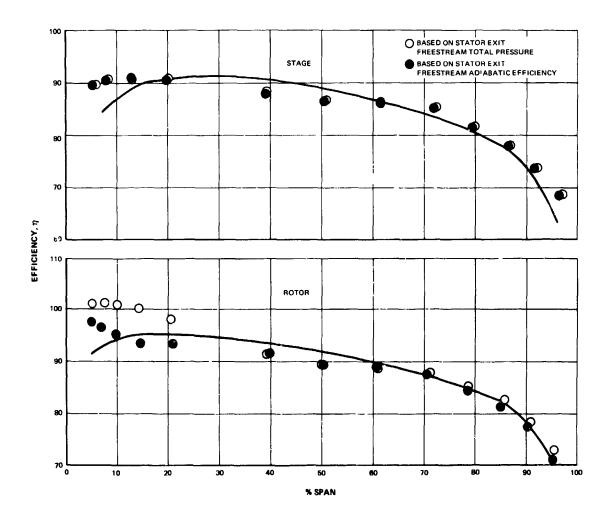


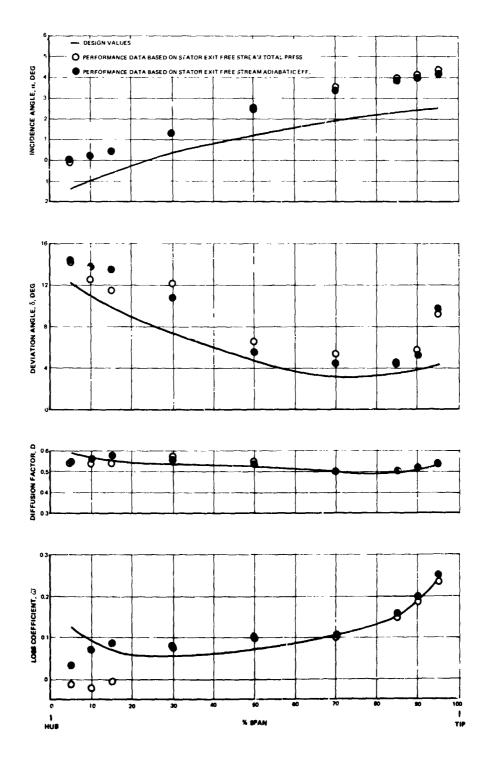
Figure 25 Rotor and Stage Spanwise Efficiency

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Figure 26 Comparison of Spanwise Rotor Blade Element Performance

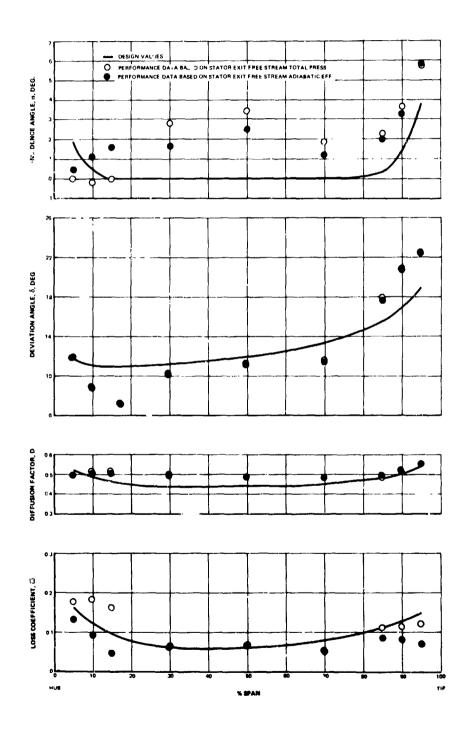


Figure 27 Comparison of Spanwise Stator Blade Element Performance

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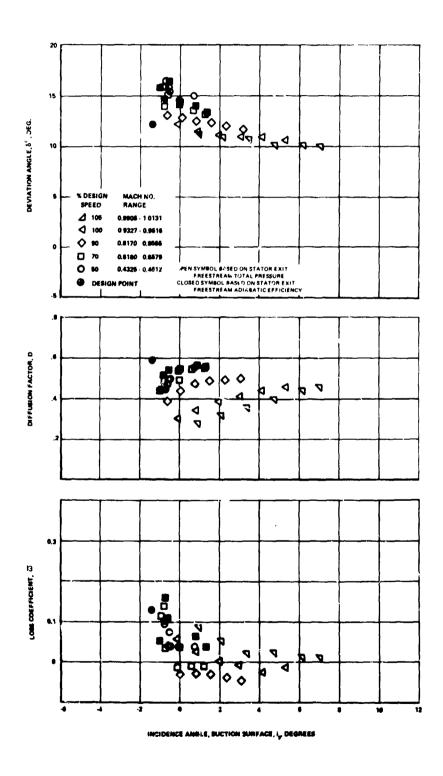
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Figure 28a Rotor Blade Element Performance with Uniform Inlet Flow, 5% Stan

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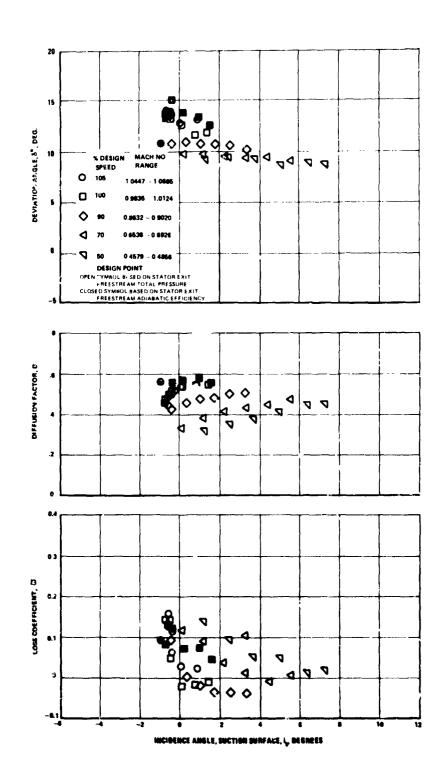
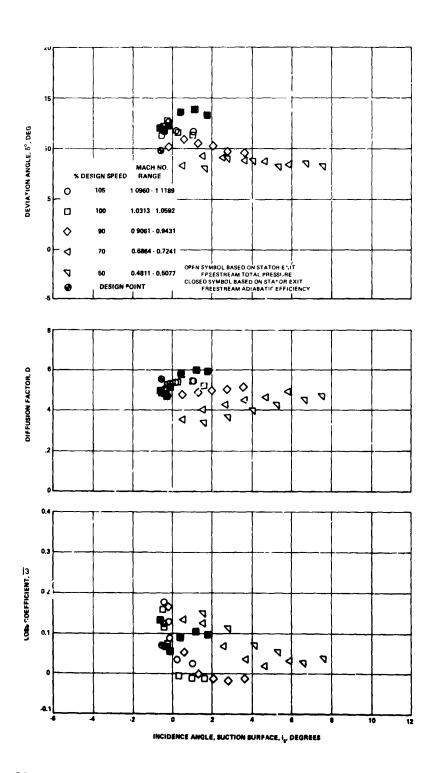


Figure 28b Rotor Blade Element Performance with Uniform Inlet Flow, 10% Span

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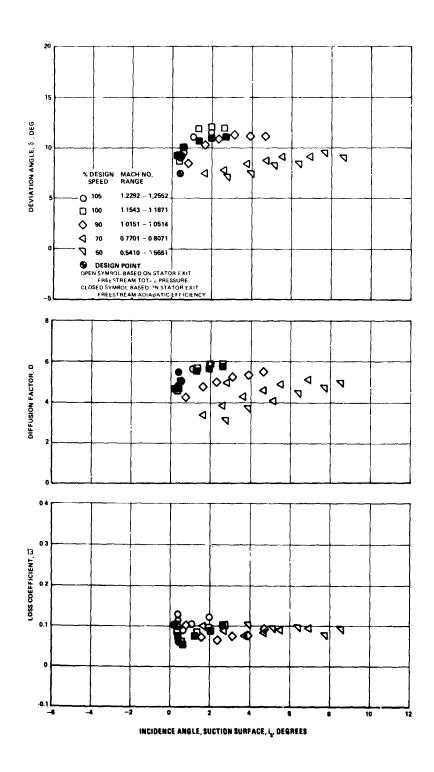


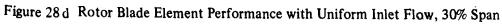
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Figure 28c Rotor Blade Elemen.: Performance with Uniform Inlet Flow, 15% Span

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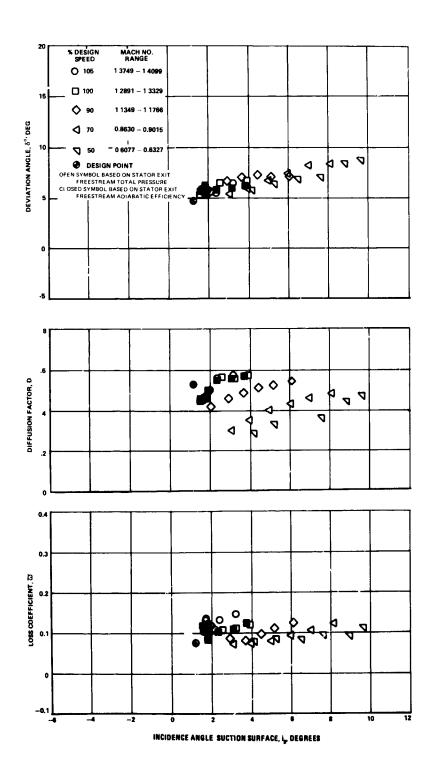
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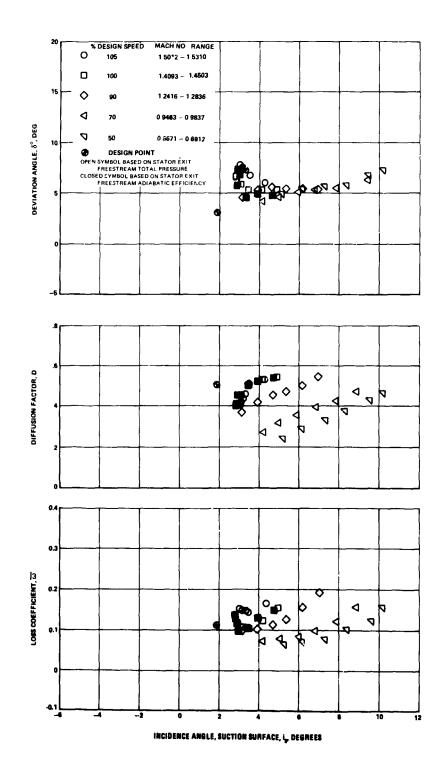
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Figure 28 e Rotor Blade Element Performance with Uniform Inlet Flow, 50% Span

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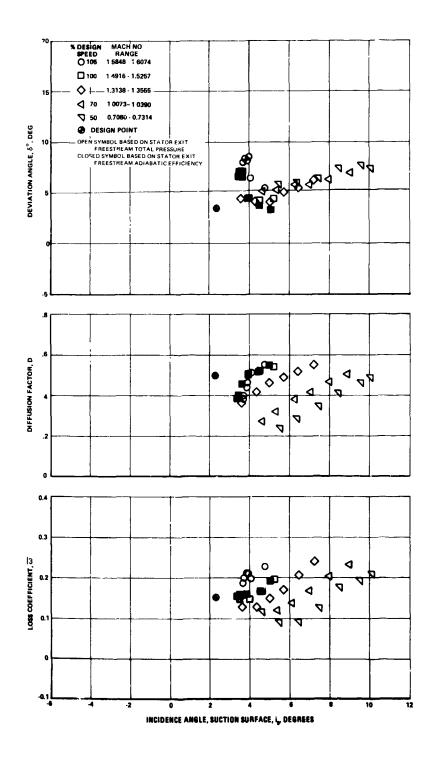
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Figure 28 g Rotor Blade Element Performance with Uniform Inlet Flow, 85% Span

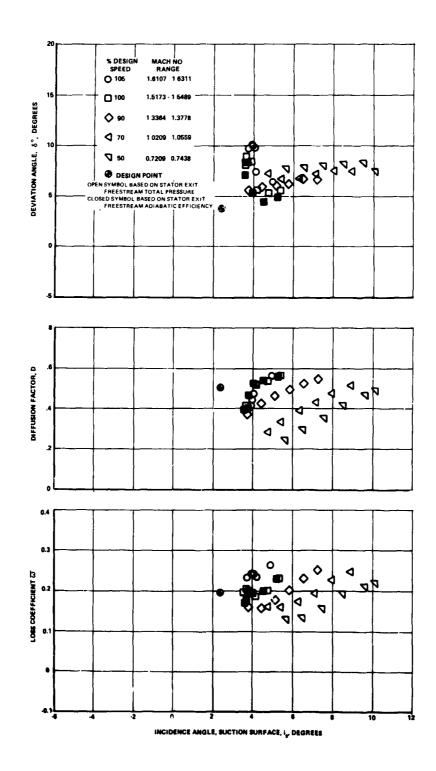
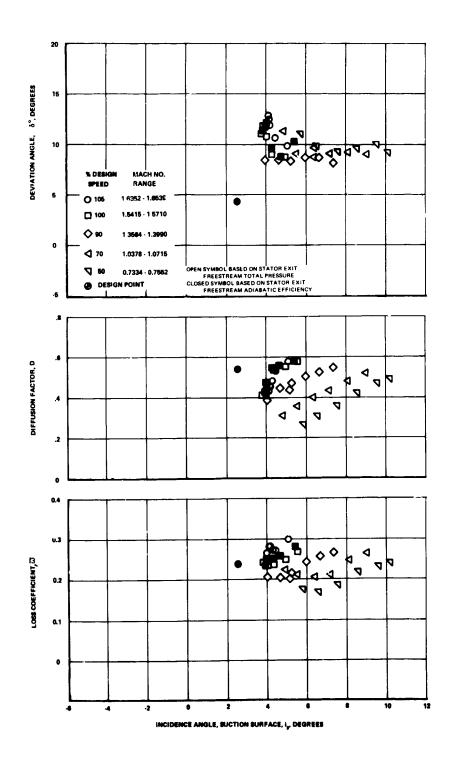


Figure 28h Rotor Blade Element Performance with Uniform Inlet Flow, 90% Span

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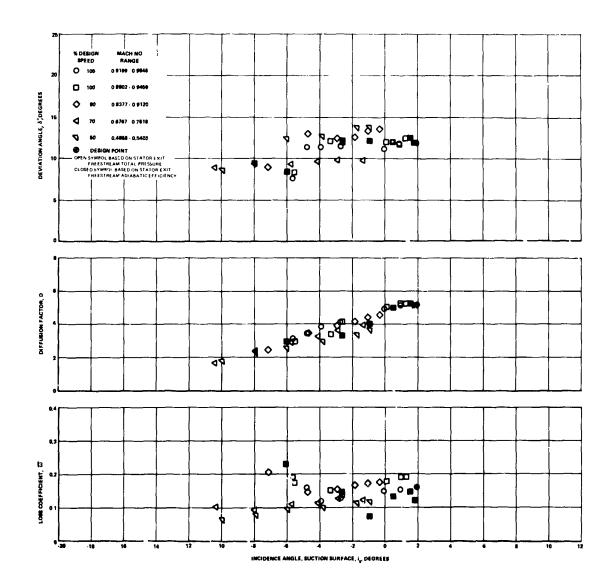
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Figure 28 i Rotor Blade Element Performance with Uniform Inlet Flow, 95% Span

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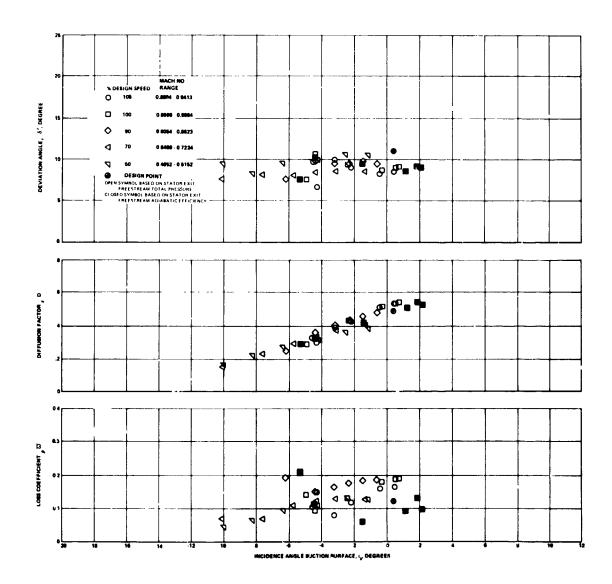
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Figure 29 a Stator Blade Element Performance with Uniform Inlet Flow, 5% Span

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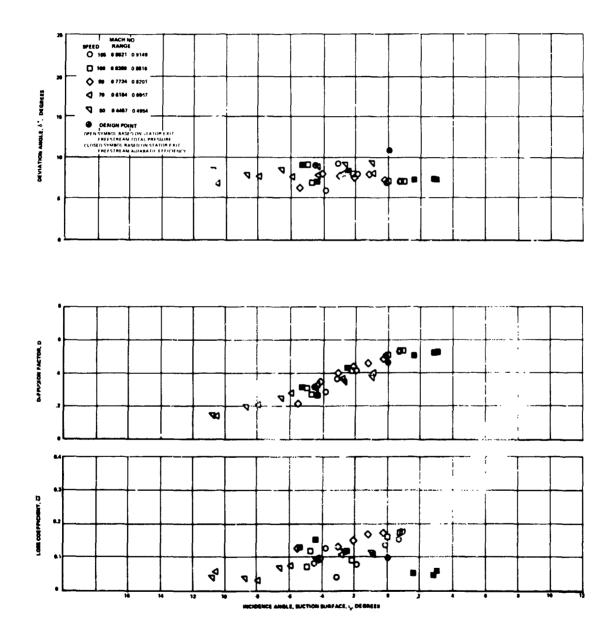
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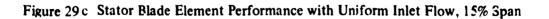
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Figure 29b Stator Blade Element Performance with Uniform Inlet Flow, 10% Span

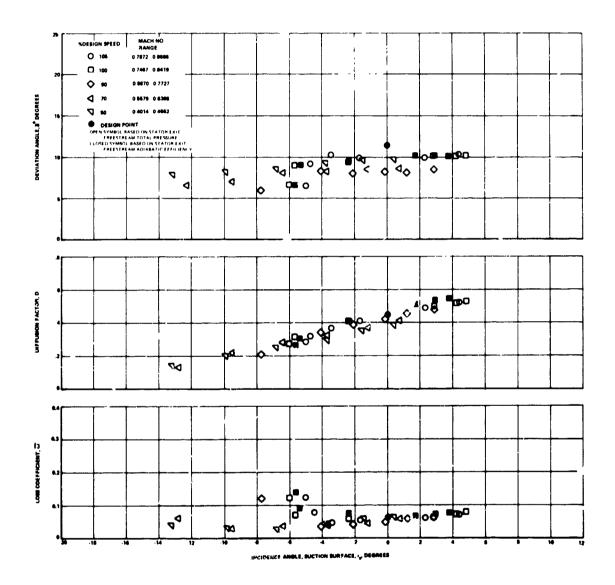


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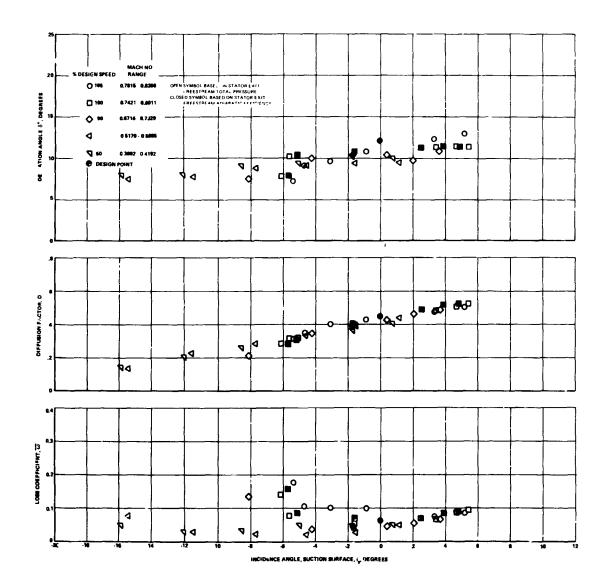
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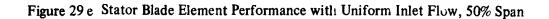
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Figure 29 d Stator Blade Element Performance with Uniform Inlet Flow, 30% Span

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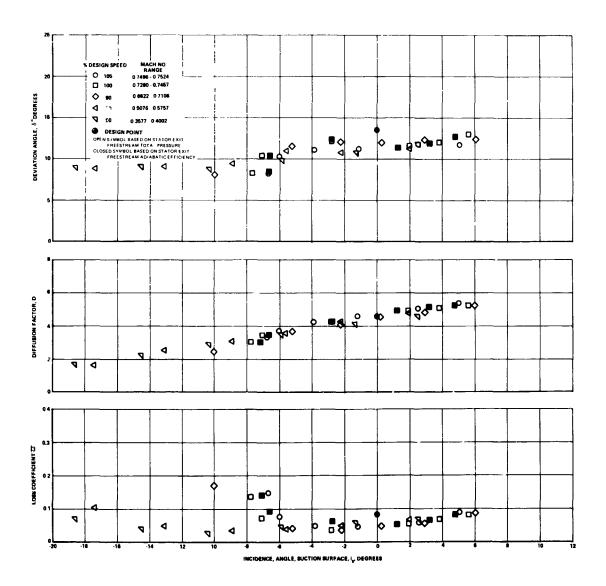
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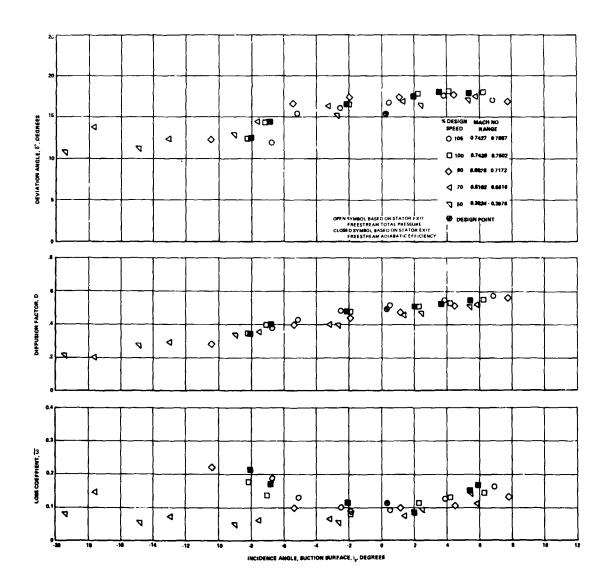
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Figure 29 f Stator Blade Element Performance with Uniform Inlet Flow, 70% Span

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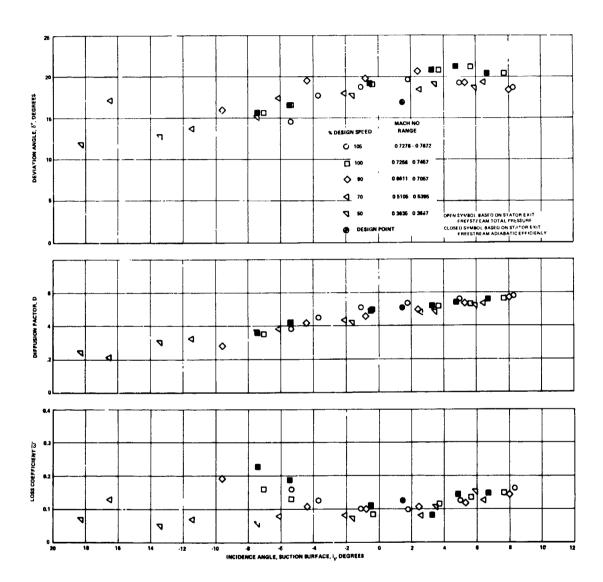
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Figure 29 g Stator Blade Element Performance with Uniform Inlet Flow, 85% Span

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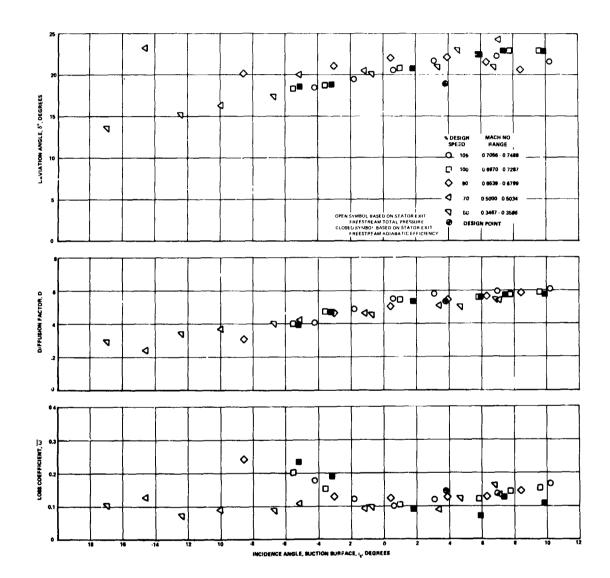
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Figure 29 h Stator Blade Element Performance with Uniform Inlet Flow, 90% Span



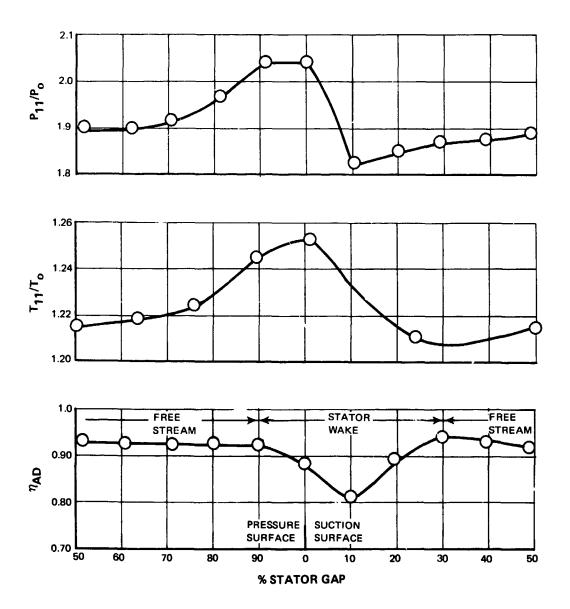
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Figure 29 i Stator Blade Element Performance with Uniform Inlet Flow, 95% Span

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Figure 30 Pressure Ratio, Temperature Ratio, and Adiabatic Efficiency vs. Stator Exit Gapwise Location at 15% Span, Near Design Data Point

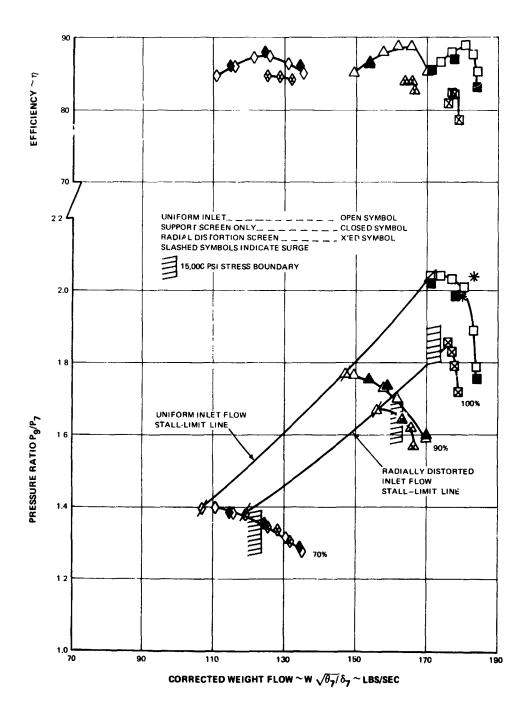
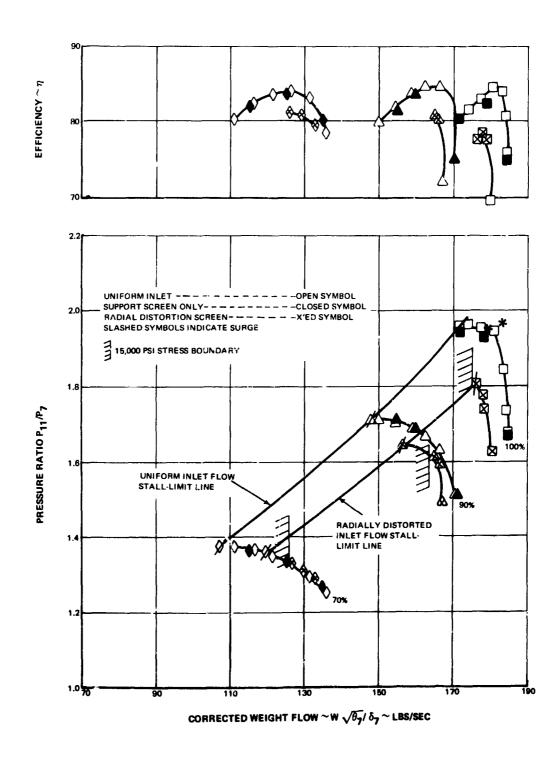


Figure 31 Comparison of Rotor Over-all Performance with the Distortion Screen Support, Radially Distorted Inlet Flow and Uniform Inlet Flow

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Figure 32 Comparison of Stage Over-all Performance with the Distortion Screen Support, Radially Distorted Inlet Flow and Uniform Inlet Flow

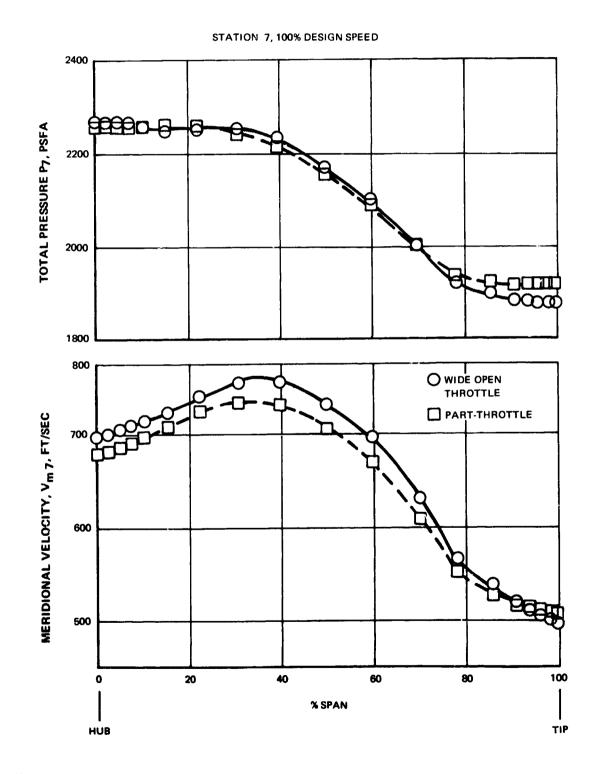


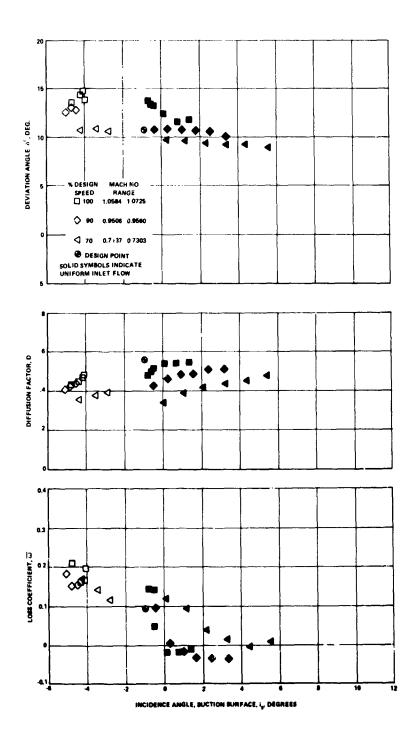
Figure 33 Spanwise Variation in Rotor Inlet Total Pressure and Meridional Velocity with Radially Distorted Inlet Flow

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Figure 34 a Rotor Blade Element Performance with Radially Distorted Inlet Flow, 10% Span

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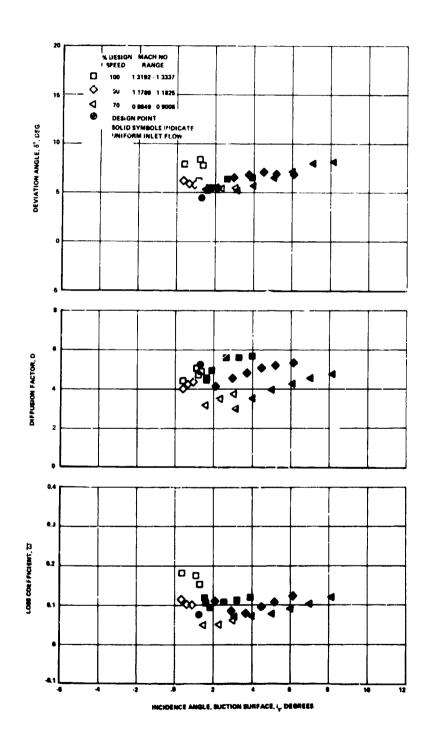
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Figure 34 b Rotor Blade Element Performance with Radially Distorted Inlet Flow, 50% Span

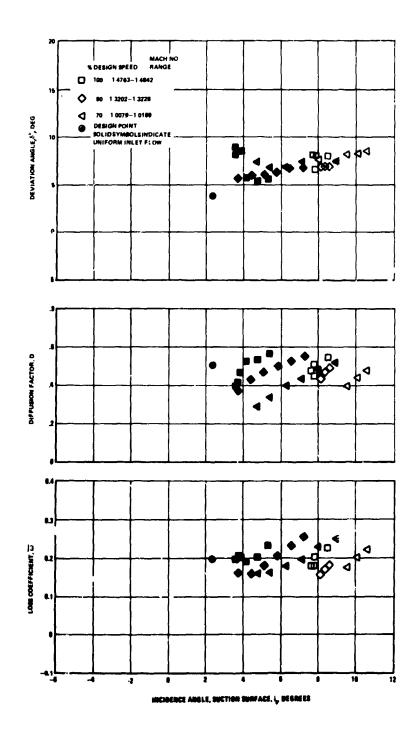
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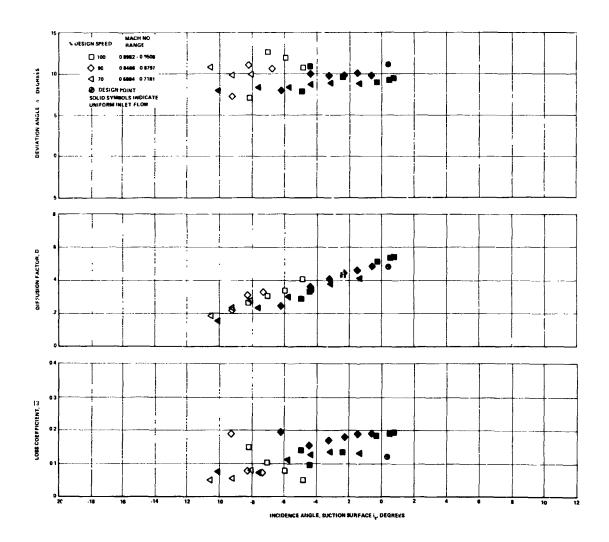


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Figure 34 c Rotor Blade Element Performance with Radially Distorted Inlet Flow, 90% Span



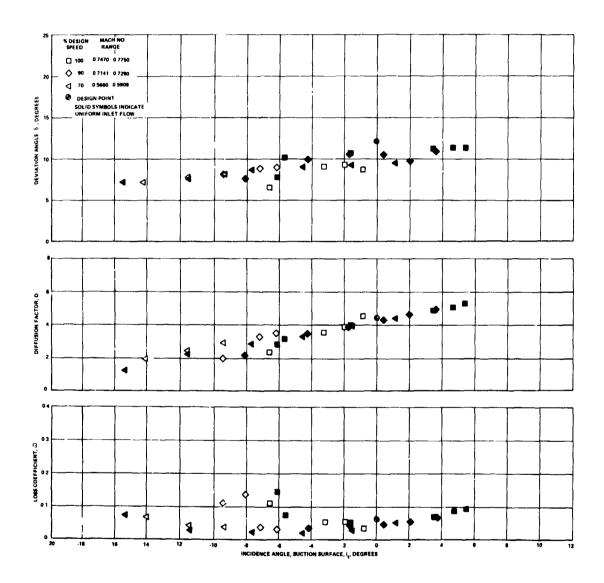
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Figure 35 a Stator Blade Element Performance with Radially Distorted Inlet Flow, 10% Span

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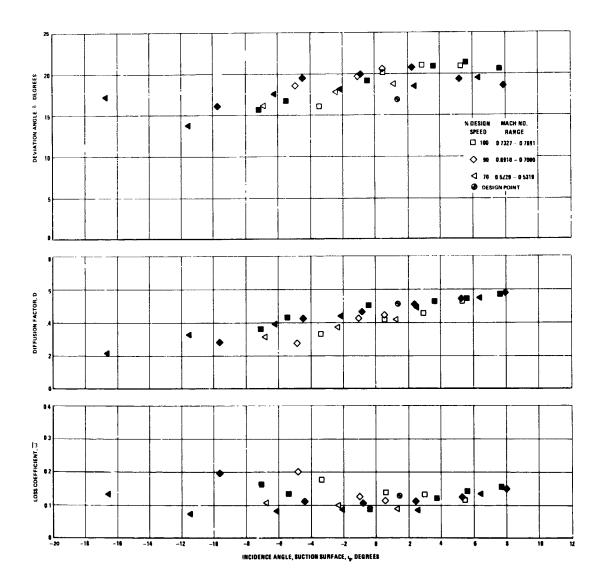
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Figure 35 b Stator Blade Element Performance with Radially Distorted Inlet Flow, 50% Span

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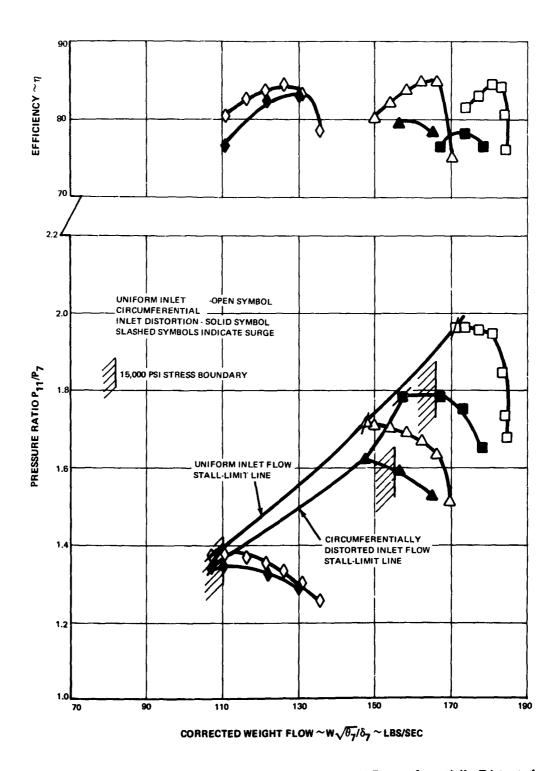
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Figure 35c Stator Blade Element Performance with Radially Distorted Inlet Flow, 90% Span

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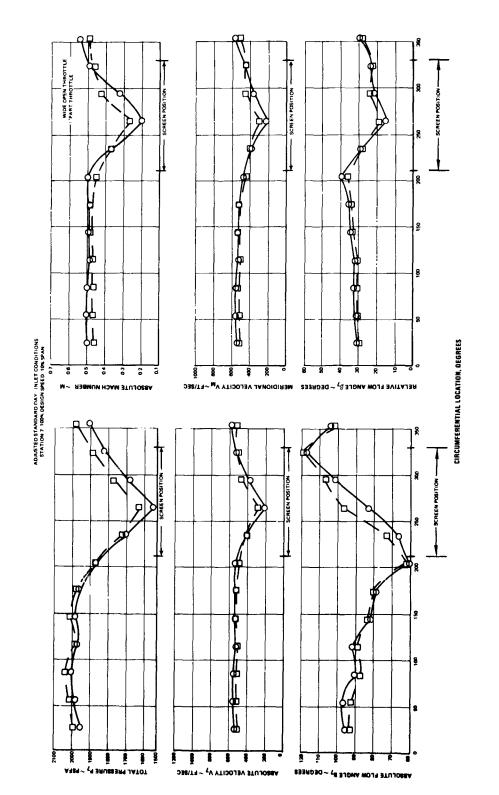


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Figure 36 Comparison of Stage Over-all Performance With Circumferentially Distorted Inlet Flow and Uniform Inlet Flow





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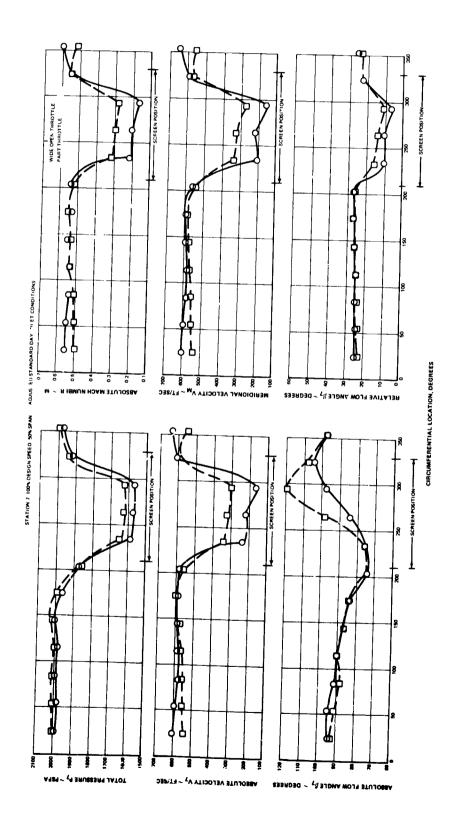
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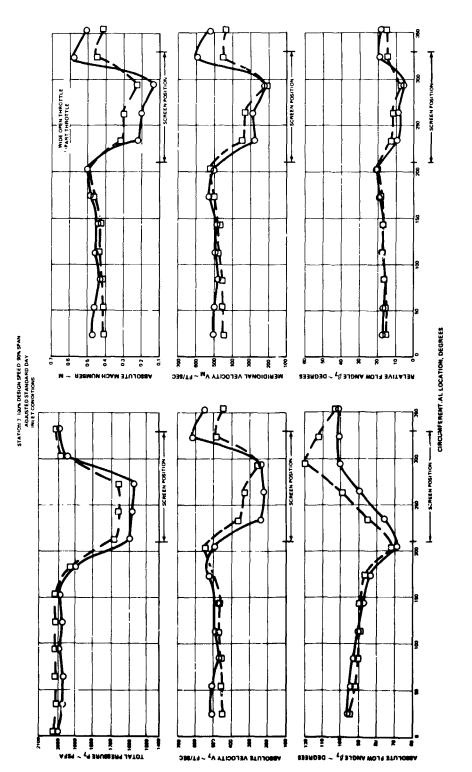


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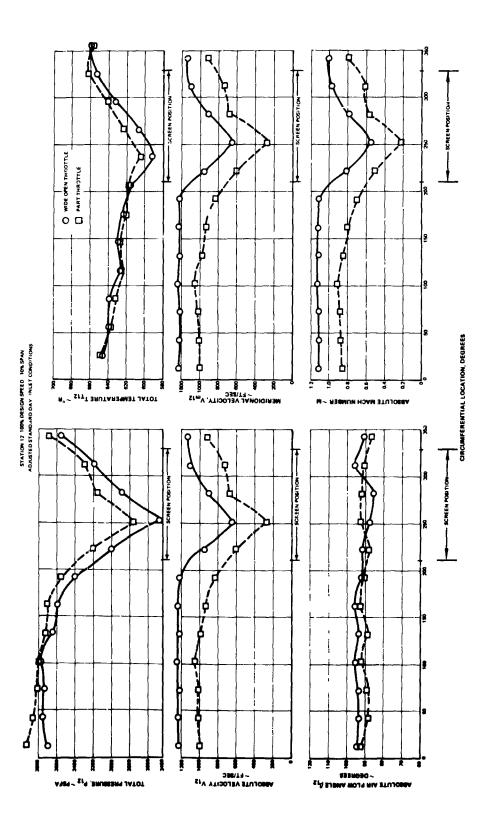
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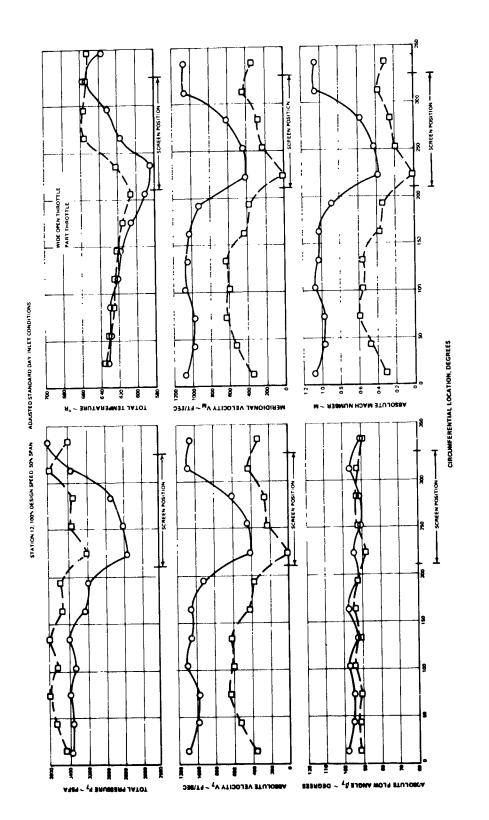


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Figure 40 Circumferential Distribution of Stator Discharge Total Pressure, Total Temperature, Absolute Velocity, Meridional Velocity, Absolute Mach Number, and Absolute Air Flow Angle, 10% Span





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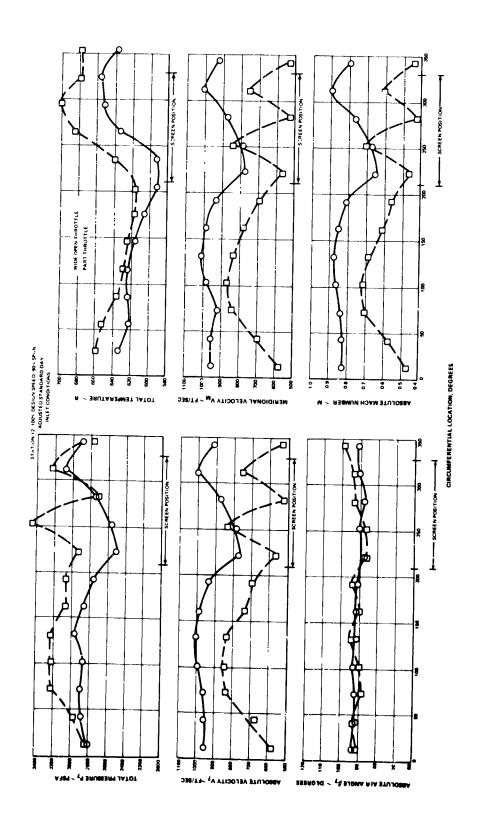
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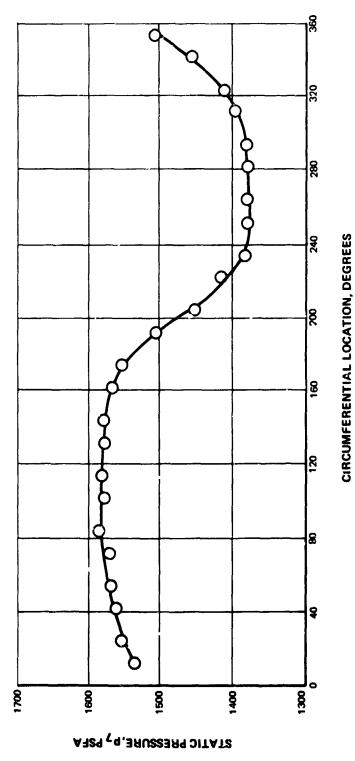
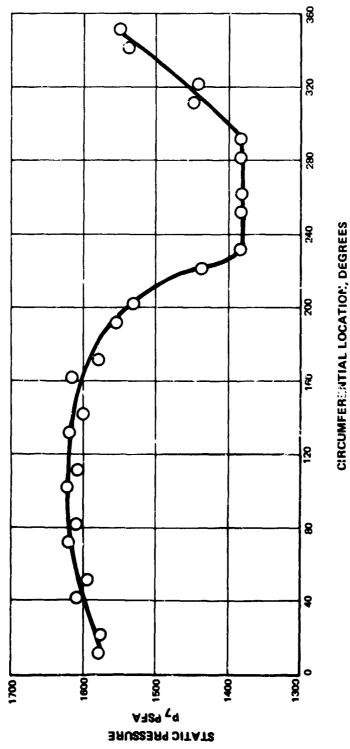


Figure 43 Circumferential Distribution of Rotor Inlet Hub Static Pressure

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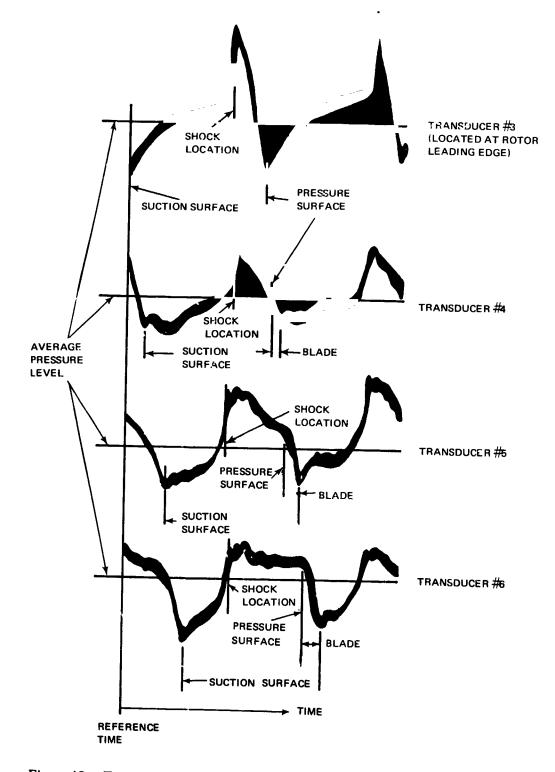


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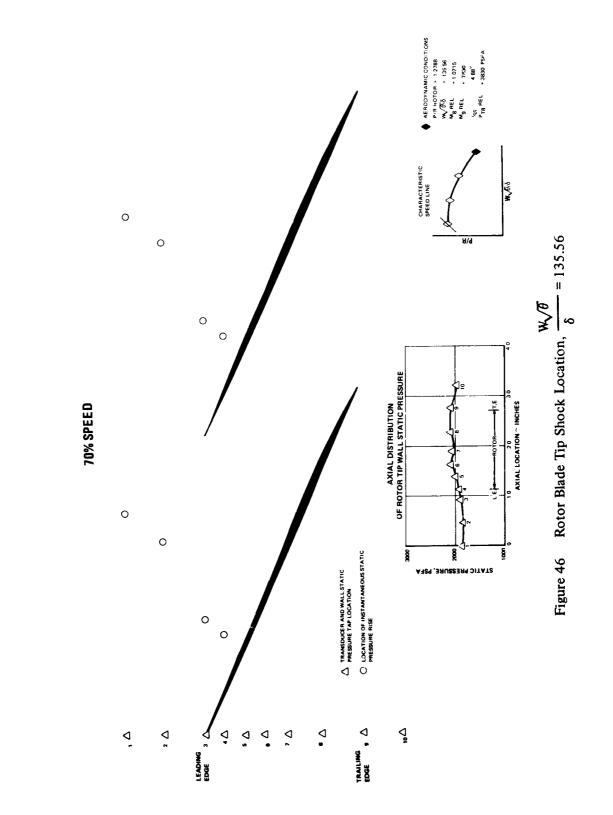
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Figure 45 Typical Oscillograph Traces Showing Presence of Shock over Blade Tip

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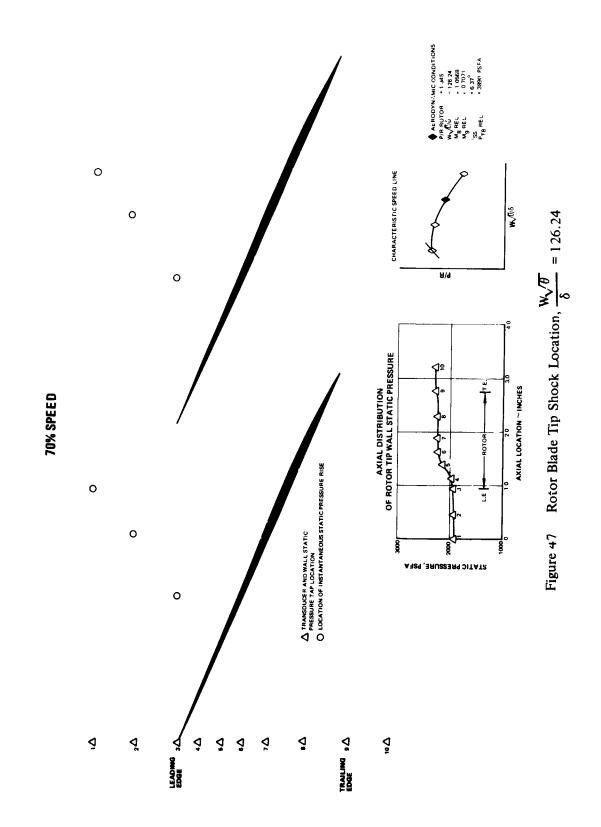


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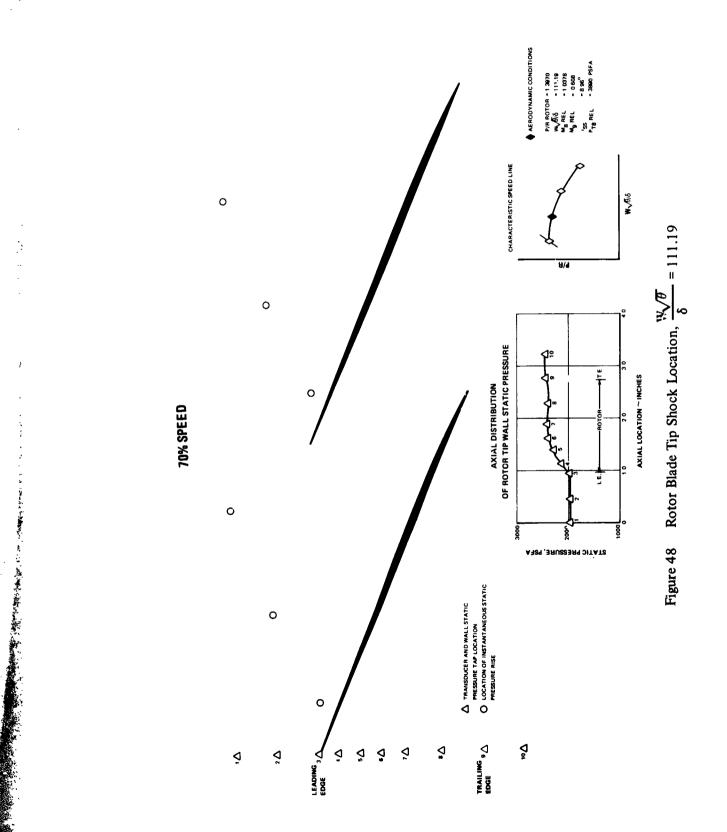
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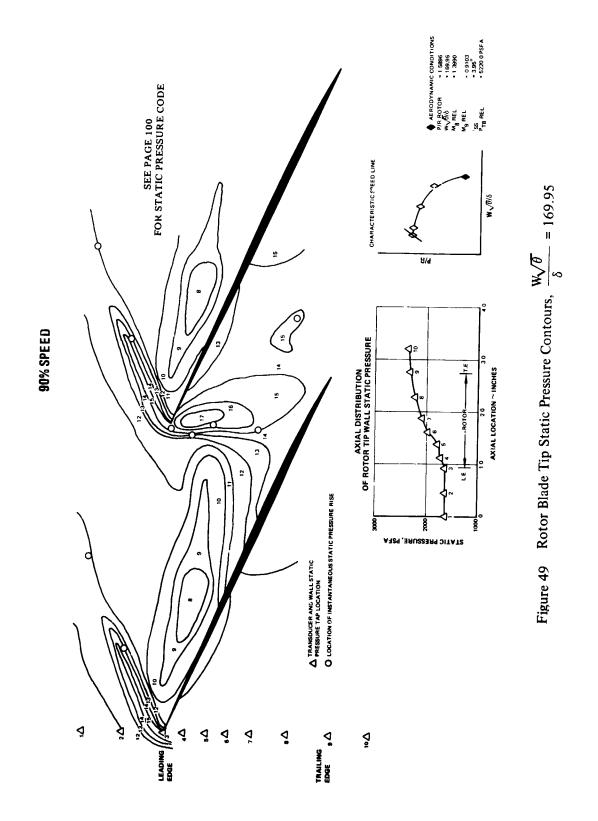


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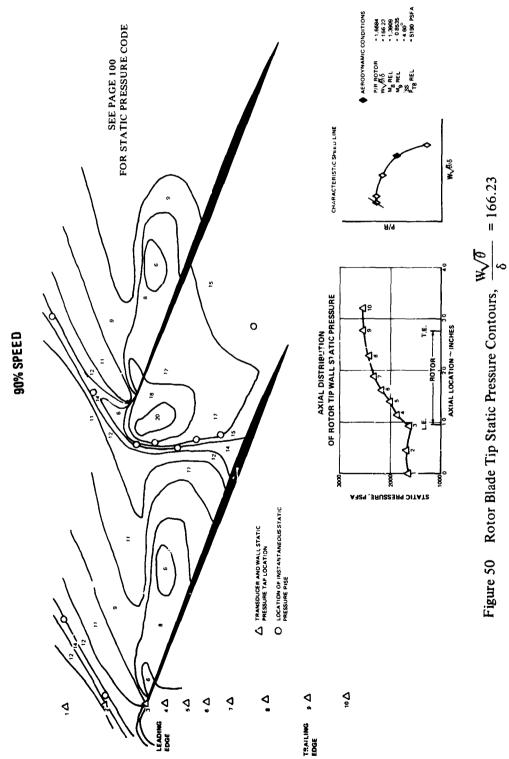
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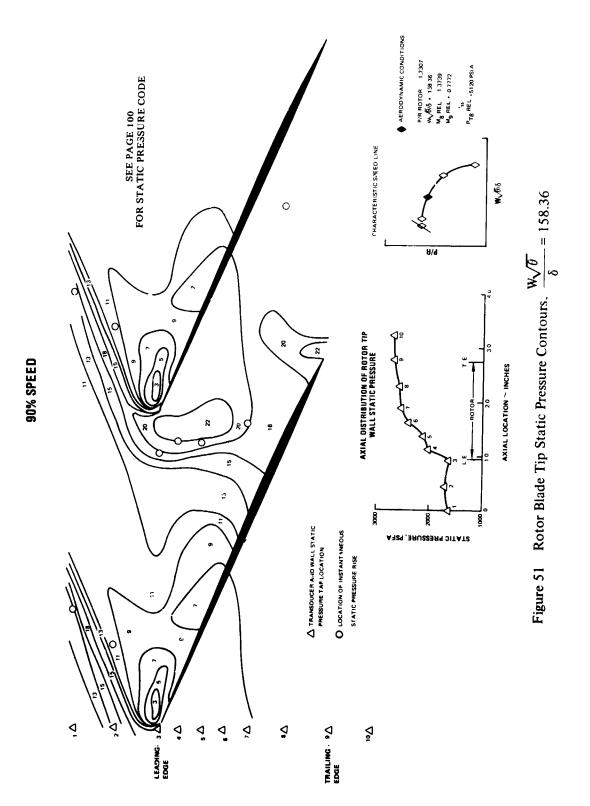
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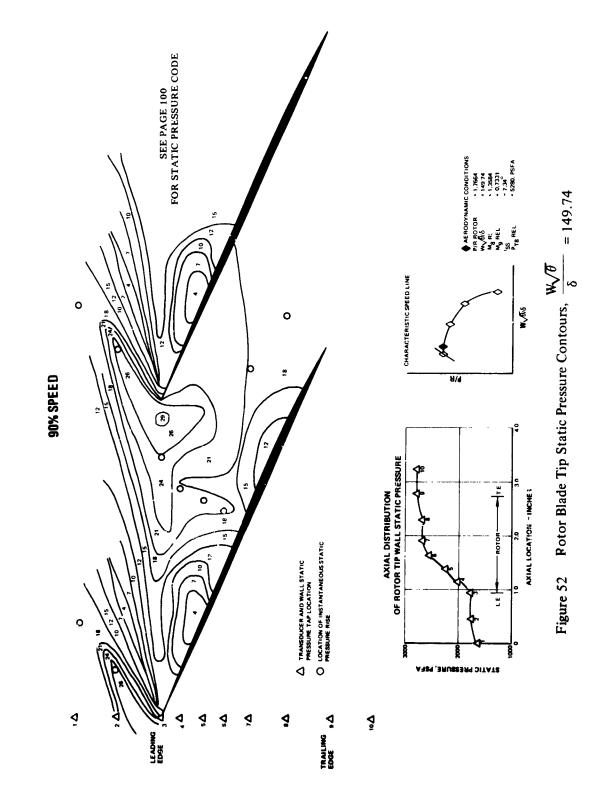
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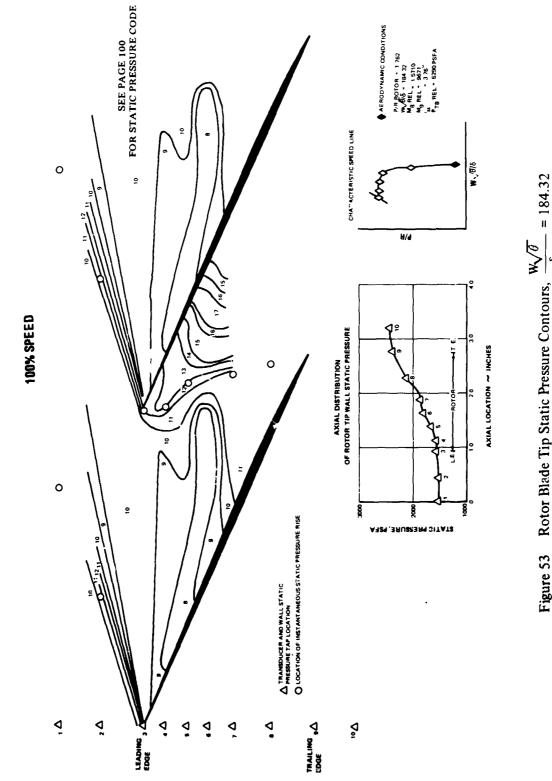


Figure 53 Rotor Blade Tip Static Pressure Contours, $\frac{W\sqrt{\theta}}{\delta} = 184.32$

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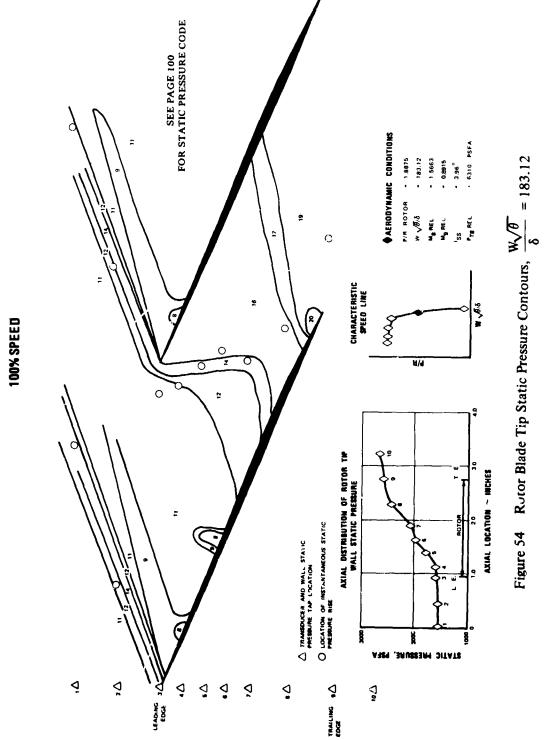
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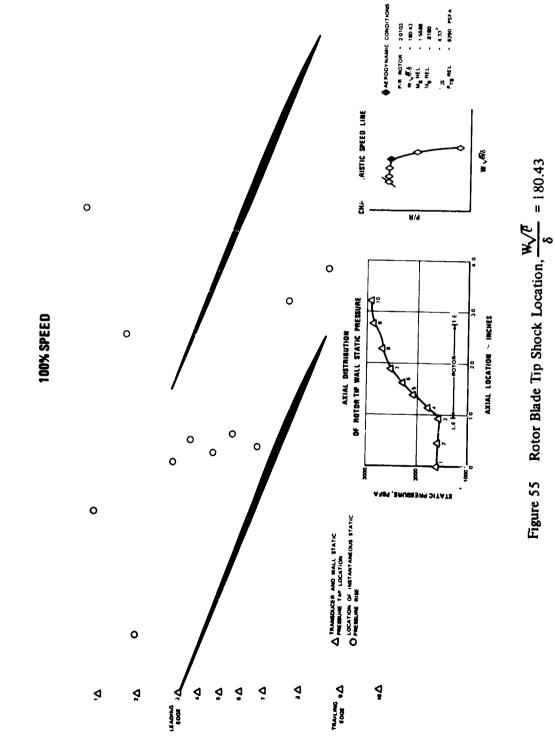
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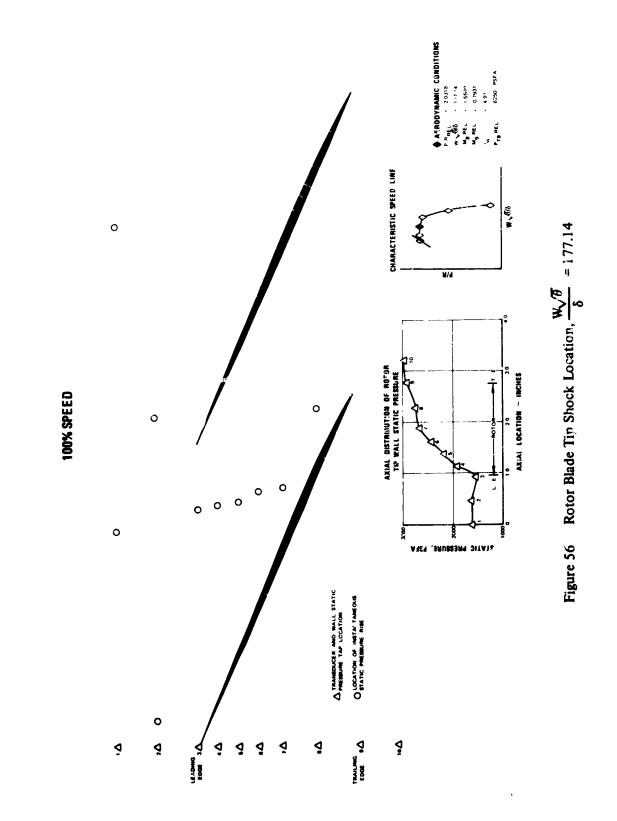
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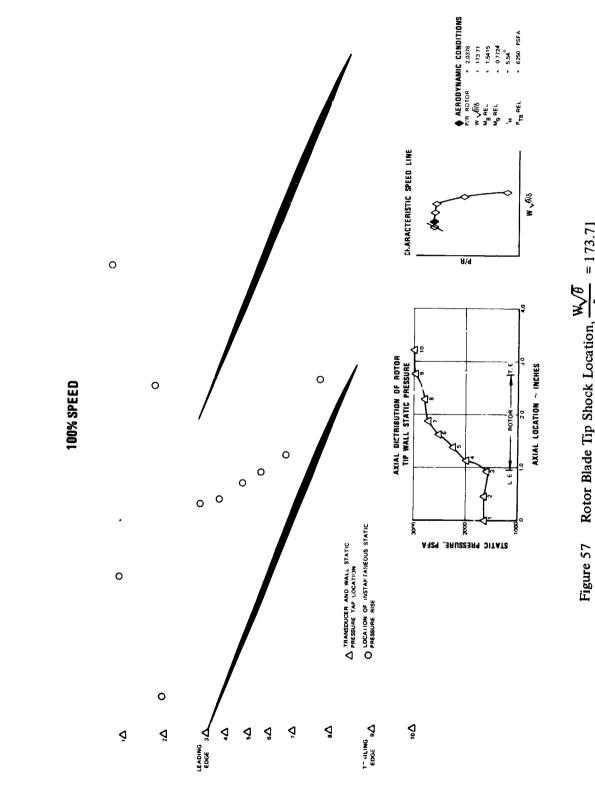
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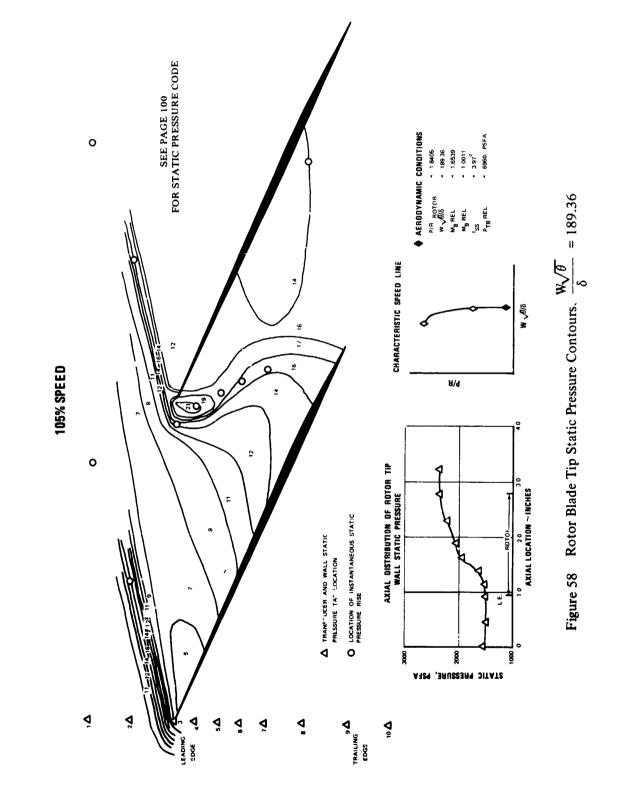
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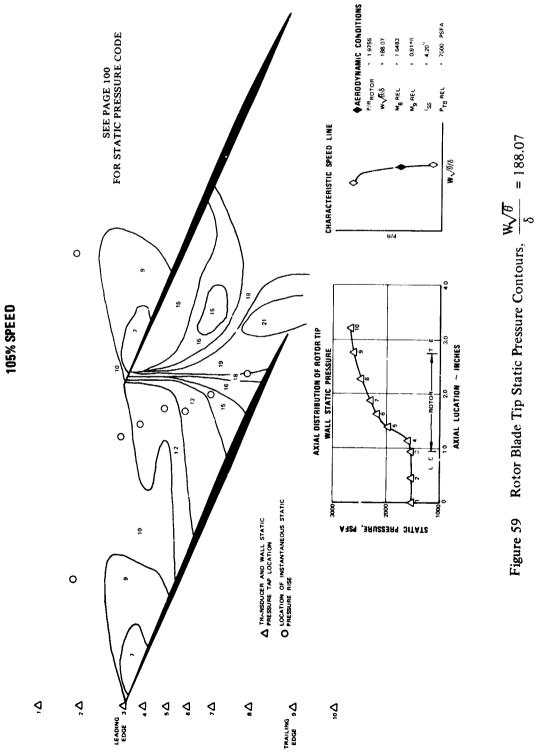
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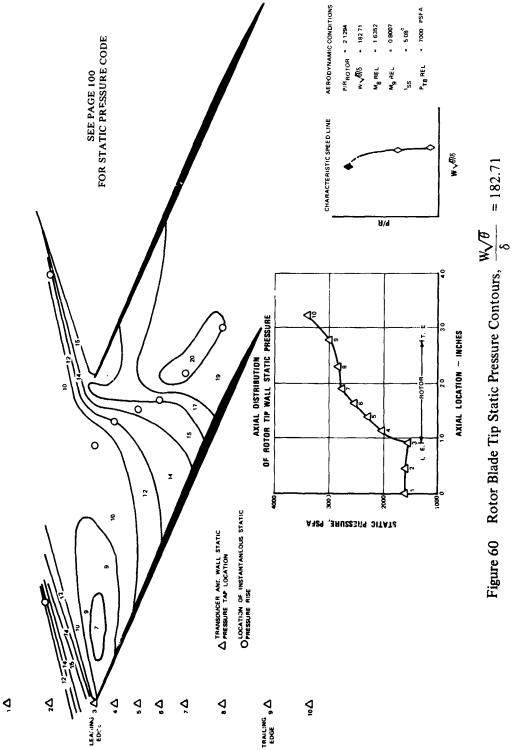
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TABLE 19

ROTOR BLADE TIP STATIC PRESSURE CODE

SYMBOL	ABSOLUTE PRESSURE RANGE (PSIA)	AVERAGE PRESSURE (PSFA)
0	0 - 1	72
1	1 · 2	216
2	2 - 3	360
3	3 - 4	504
4	4 - 5	648
5	5 - 6	792
6	6 - 7	936
7	7 - 8	1080
8	8 - 9	1224
9	9 - 10	1368
10	10 - 11	1512
11	11 - 12	1653
12	12 - 13	1800
13	13 - 14	1944
14	14 - 15	2088
15	15 - 16	2232
16	16 - 17	2376
17	17 - 18	2520
18	18 - 19	2664
19	!9 - 20	2808
20	20 - 21	2952
21	21 - 22	3096
22	22 - 23	3240
23	23 - 24	3384
24	24 - 25	3528
25	25 - 26	3672
26	26 - 27	3816
27	27 - 28	3960
28	28 - 29	4104
29	29 - 30	4248
30	30 - 31	4392

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APPENDIX 1

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Performance Parameters

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APPENDIX 1

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Performance Parameters

a) Relative total temperature

$$T'_{8} = t_{8} \left[1 + \frac{\gamma - 1}{2} (M'_{8})^{2} \right]$$
(rotor in)
$$T'_{9} = T'_{8} + \left[\frac{(\omega r_{8})^{2} - (\omega r_{9})^{2}}{\frac{2\gamma}{\gamma - 1} Rg_{c}} \right]$$
(rotor out)

b) Incidence angle based on mean camber line

$$i_{\rm m} = \beta'_8 - \beta'_8 \tag{(rotor)}$$

$$i_{\rm m} = \beta_{10} - \beta *_{10} \qquad (stator)$$

c) Deviation

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 $\boldsymbol{\delta}^{\bullet} = \boldsymbol{\beta}'_{9} - \boldsymbol{\beta}'_{9} \qquad (rotor)$

$$\delta^{\bullet} = \beta_{11} - \beta^{*}_{11} \qquad (stator)$$

d) Diffusion factor

$$D = 1 - \frac{V'_9}{V'_8} + \frac{r_9 V_{\theta 9} - r_8 V_{\theta 8}}{(r_8 + r_9) \sigma V'_8}$$
(rotor)

$$D = 1 - \frac{V_{11}}{V_{10}} + \frac{r_{10}V_{\theta 10} - r_{11}V_{\theta 11}}{(r_{10} + r_{11})\sigma V_{10}}$$
(stator)

e) Loss coefficient

$$\overline{\omega} = \frac{P'_8 \left[\frac{T'_9}{T'_8}\right] \frac{\gamma}{\gamma - 1} - P'_9}{P'_8 - P_8}$$
(rotor)

$$\overline{\omega} = \frac{P_{10} - P_{11}}{P_{10} - P_{10}}$$
 (stator)

f)

Loss parameter

$$\frac{\overline{\omega}\cos\beta'9}{2\sigma}$$
(rotor)
$$\frac{\overline{\omega}\cos\beta_{11}}{2}$$
(stator)

g) Polytropic efficiency

1)
$$\eta_{p} = \frac{\frac{\gamma - 1}{\gamma} \ln \left[\frac{P_{9}}{P_{7}}\right]}{\ln \left[\frac{T_{9}}{T_{0}}\right]}$$
 (rotor)
2) $\eta_{p} = \frac{\frac{\gamma - 1}{\gamma} \ln \left[\frac{p_{11}}{p_{10}}\right]}{\ln \left[\frac{t_{11}}{t_{10}}\right]}$ (stator)

h)

Adiabatic efficiency

 $\eta_{ad} = \frac{\begin{bmatrix} P_9 \\ P_7 \end{bmatrix}}{\begin{bmatrix} T_{12} \\ T_0 \end{bmatrix}} -1$

$$\eta_{ad} = \frac{\left[\frac{P_{12}}{P_{7}}\right] \frac{\gamma - 1}{\gamma}}{\left[\frac{T_{12}}{T_{0}}\right] - 1}$$

(stage)

(rotor)

i) Wake blockage factor

$$\vec{K} = \frac{\sum_{n}^{\infty} \rho AV}{n} / \rho AV_{avg}$$

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APPENDIX 2

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Symbols

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APPENDIX 2

Symbols

А	- area, ft ²	
A _{an}	- annulus area, ft ²	
A_{f}	- frontal area, tt^2	
с	- cherd length, in	
D	- diffusion factor	
g _c	- conversion factor, 32.17 $lb_m ft/lb sec^2$	
i _m	 incidence angle, angle between inlet air direction and line tangent to blade mean camber line at leading edge, degrees (labelled INCM Table 5) 	,
i _s	- incidence angle, angle between inlet air direction and line tangent t blade suction surface at leading edge, degrees (labelled INCS, Tab	
М	- Mach number	
MR	- mass average in radial directions (Tables 15 and 16)	
N	- rotor speed, rpm (N/ $\sqrt{\theta}$ labelled NCOR, Table 5)	
Р	- total pressure, psfa	
p	- static pressure, psfa	
r	- radius, ft	
R	- gas constant for air, ft lb/lb _{IA} °R	
S	- blade spacing, in	
Т	- total temperature, °R	
4	- static temperature, °R	
t/c	- thickness-to-chord ratio	

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U	- roto	r speed, ft/sec
v	- air v	velocity, ft/sec
Vm	- mer	idional velocity ($Vr^2 + Vz^2$), $1/2$ ft/sec (labelled VM, Table 5)
W	- weig	ht flow, lbs/sec
β	- abso	lute air angle, \cot^{-1} (Vm/V θ), degrees (labelled B, Table 5)
β'	- rota	ting air angle, \cot^{-1} (Vm/Vé), degrees (labelled B', Table 5)
γ	- ratio	o of specific heats for air, 1.4
Δβ	- air t	urning angle, degrees
Δβ*	- cam	ber angle, degrees
δ	- ratio) of inlet total pressure to standard pressure of 2116.22 lbs/ft^2
3°		ation angle, angle between exit air direction and tangent to blade n camber line at trailing edge, degrees
¢	•	e between tangent to streamline projected on meridional plane axial direction, degrees
η	- effic	ciency, %
θ	- ratio	o of inlet total temperature to standard temperature of 518.6°R
ρ	- mag	s density, lbs-sec ² /ft ⁴
σ	- soli	dity, ratio of chord to spacing
ធ	- tota	i pressure loss coefficient (labelled OMEGA - B, Table 5)
ω	- angu	ilar velocity of rotor, radians/sec
Supera	rip ts :	
t	- rela	tive to moving blades
*	- desi	gnates blade metal angle

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Subscripts:

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ad	- adiabatic
Ł	- polytropic or profile
r	- radial direction
m	- meridional direction (in z-r plane)
sh	- shock
88	- suction surface
z	- axial direction
θ	- tangential direction (labelled O, Table 5)
0	- plenum chamber
7	- instrument plane upstream of rotor
8	- station at rotor leading edge
9	- station at rotor railing edge
10	- station at stator leading edge
11	- station at stator trailing edge
12	- instrument plane downstream of stator

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APPENDIX 3

Blade-Element and Overall Performance with Uniform Inlet Flow

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0-2 -1/SE	0 ⁹	Z-1	M' 8			с-7 Г12 5	U9	21,¥	M'II		
U-1 1-1	U ₈	1¥	~M 8			1-1 E125EC	u ₈	[¥	0ľ M		
V01-2	θ_{θ}	N I	6M			V01-2	V, Ø11	X-2	M11		
28 V01-1	$v_{\theta 8}$	Ī	M_8			1-101	$v_{\theta_{10}}$	11 1 1	n ps M ₁₀ M ₁₁ M ₁₀		
eadin _t	47 6	EFF-P	۹			V2	V'11	EFF=P LATLC	1 ps		
able H v	V'8	FF-AD DTAL S	"ad			V-1 1/SEC F	V'10	FF-AD	rad		
nce T B'-2 EGREE F	β β	EFF-P E	ď			B'-2 GREE F	ß '11	EFF#P EFF#D EFF#P IgialIgialStatic	r dr		
TABLE 5 Identification of Blade-Element and Overall Performance Table Headings V-1 V-2 VN-1 VM-2 V0-1 V0-2 8-1 B-2 8-1 BV-2 VI-1 VV-2 V0-1 V0-2 U-1 U-2 TASEC FIASEC FIASEC FIASEC FIASEC DEBREE DEBREE DEBREE FIASEC FIASEC FIASEC FIASEC FIASEC FIASEC	വ്, വ	PO2/ EFF-P EFF-AD -PO1 TOTAL TOTAL	6- ⁶ -6			8 - 1 GREE DI	ß.10	P02/ 6 P01 IC		ţ	
Per 5-2 Egree D	B9		with the second	1		8-2 GREE DI	β_{11}	055-P OF LLE. I	$\frac{\cos \beta_{11}}{2\sigma} \left \begin{array}{c} P_{11} \\ P_{10} \\ P_{10} \\ (\overline{\omega} - \overline{\omega}_{sh}) \cos \beta_{11} \\ \end{array} \right $		
TABLE 5 and Overa	B 8	0055-P L 114, שני מין 16	ω cos β 9 2σ (ω-ωs			B-1 GREE.DE	β_{10}	055-P L TAL PR	<u>ω cos β11</u> 2σ (<u>ω - ω</u> sh	2 d	
TAB t and t	6θΛ	OMEGA-B D-FAC OMEGA-B LOSS-P LOSS-P Swock . Total Profile 	3 3			VO-2 ASEC DE		OMEGA-B D-FAC OMEGA-B LOSS-P 1.055-P PO2/ SHOCK TUTAL PROFILE. PO1.	13	WC/A-1 LBM/96C	$\frac{w\sqrt{\theta}}{\delta A_{an}}$
lemen vo-1 vsec F1	V _θ 8	-FAC OM	A	EFFP 14657 *	4 D	SEC FL	/010 V	FAC ON	13 Q	1	
ade-E vx-2 /sec F1		EGA-B D	$\overline{\omega}_{\mathbf{S}h}$	~	ad 1	W-2 SEC EL	Vm11 V ₀₁₀ V ₆₁₁	64 - B D.	'n	AO EFE-P	ưď ⊅p
of Bla	Vm8 Vm9	BER OM	* ©				V _{m10} V	JER OME	13 #	DU AUL FAILAMETERS WORK TO/TO PO/PO EFF-AD IMLET INLET INLET INLET BM/SEC	'n ad
ation Ec Fr/			4	PO/PO	ር ር	20 FT/S	N III III	CANE CANE	Δβ	PC/PO	$\frac{P_{11}}{P_0}$
itific; c Fr/s	V9	TURI DEGR	Δ β	TO/TO HILET	$\frac{1}{10}$		V11	TUR. DEGRE	Δβ	TO/TO	$\frac{T_{11}}{T_0}$
Ider v-1 Fryse	V ₈	DESREI	60 69			1-7 F1/SE(V10	V 3C DE ORE	°11	NUL MALET	W B
Identification DIA-1 DIA-2 V-1 V-2 IN IN F1/SEC F1/SEC F1	2 r 9	I NCH DEĢREE	im8			DIA-2	^{2r} 11	I NCM	is10 im10 S7	NCORR NCORR NCORR NCORR NCORR	XILO AIR
DIA-1	2 r 8	INCS INCM JEV TURN CAMBER -Degree degree degree degree	i ⁱ s8			DIA-1 DIA-2 V-1 V-2 VM-1 VM-2 VO-1 VO-2 B-1 B-2 B'-1 B'-2 VI-1 VI-2 VOI-1 VOI-2 U-1 U-2 14 IM FT/SEC FT/SEC FT/SEC FT/SEC FT/SEC LIGREE DEGREE DEGREE DEGREE DEGREE FT/SEC FT/SEC FT/SEC FT/SEC FT/SEC	2r10 ^{2r} 11	INCS INCM DEV TURN CAMBER 1822au - Degree Degree degree degree 10	¹ s10	1235	7
ROTOR *****	5 8 3 6 8 8	퍼	5875 88			MOINTO	x 9 3 5 8 8 8	10	x H B K # B X		

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TABLE 6

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ROTOR

Blade-Element and Overall Performance - Design Data

Nu	7.6	8.3	9.2	1.5	6.5	1.0	3.8	3.6	3.8	2- M		218	607	856	405	.7250	103	680	644	270	
ET/SEC													•	•		•		•	•	•	
FT/SEC												.9653						_			
512,13 70,15	-179.7	-256. 1	-317.0	-463.7	-638.5	-788.9	-885.9	-898.0	-884.0	N-N		. 834	. 813	.795	747	.700	.671	.659	.657	, 654	
FT/5EC	-844. I	-893.0	-945.5	-1077.8	- 1244. 7	-1:397 6	-1505.(-15:9.2	-1571 0	M-1		. 569	. 579	. 590	.621	.631	.655	. 640	. 631	.623	
FT/SEC	607.39	652.85	682.97	752.20	858, 92	966.37	1045.08	1046.70	1012.35	EFF-P											
-2 ⊎-1 8~2 è'-1 B'-2 V'-1 EC DEGRÊÊDEGREÊDEGREÊFT/SEC F	1044.7	1090.4	1136.6	1268.2	1426.8	1564.1	1655.1	1682.2	1708.1	EFF-PEFF-AD	TOIAL	.9135	.9424	.9529	. 9471	.9225	.8758	. 8260	.7850	.71533	
в'- 2 Сорен	17.22	23. 11	27.67	38. (°7	48.03	34.56	57.57	59.09	61.51	5-2-13	TOTAL	4728.	.9414	.9542	.9315	.9290	. 8548	. 8364	.7941	. 7562	
EGREED	53.91	54.49	55.94	58.20	60.74	63.33	65.49	66.21	66, 89	- 204 d	E PCI	2.0	2.0	2.0	2.0	2° 0	2.0	2.0	2.0	2.0	
B-2 SEGREFC	5.1.29	30.65	49.26	47.57	46.15	45.54	45.70	47.44	51.93	· LOS5-	PROFIL	. 0263	.0167	.0106	. 0037	-, 0009	. 0003	.0036	. 0107	.0136	
H−1 DEGRÊEC	0.	о.	θ.	÷,	۰.	۹.	٥.	0.	ο.	3 LOSS-P LOSS-P PO2/ EF	TOTAL	.0263	.0197	1410.	.0123	.0149	.0215	.0291	. 0373	.0426	
FT/SEC [06.777	732.19	762.17	647.81	597.98	572.13	567.91	385.56	629. 51	OME GA-B		.1257									
FT/SEC	0	9	0	2	0	0	3	•	c	BD-FAC		. 5936	. 5642	. 5537	. 5462	. 3252	. 5031	.4910	. 5045	. 5443	EFF-P «
VH-2 FT/SEC	580.18	600.49	604.91	542.25	574.46	561.56	554.34	537.71	493.36	OMEGA-BD-FAC	SHOCK	. 0000	.0132	.0183	. 0406	. 0773	.1083	. 1327	. 1344	.1508	0
FI/SEC	615.49	625.705	636.763	668.382	697. 536	702.305	686.769	678.618	670. 550	CAMBER	E. DEGREE S	47.17	39.99	34.03	24.17	14.60	90.6	7.93	7.60	7.42	- 9d
1 PIA-1 DIA-2 V-1 V-2	970.440	946,940	926.804	877.74I	829.215	801.681	793.611	795.003	800.046	TUPN	EEGRE	•	80	5	m	12.71		-		-	1 0 1
F1/SEC	615. 494	625.705	636.763	668.382	697.536	702.305	686.769	678.618	670.550	V DEV	8	12.20	10.75	9.80	7.50	4.60	3.10	3.42	3.80	4.40	
-DIA-I		20.408		22.964		28.076		30.630		S INCH	ň	4.65	4.72	4.70	4.46	4.03	3.70	3.45	3.40	3.32	
-110			19.467		25.791	28.954	31.295	31.883	32.499	INCS	DEGREE	-1.40	-0.96	-0.55	0.	1.22	1.89	2.29	2.37	2.50	
E SPAN	5	10	15 1	30	29 29	10	88	6	95		X SPAN	'n	01	- 22		05	20	85	06	95	

STATOR

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SPAN	DIA-1	DIA-2	SPAN IN IN FLAGE FLAGE		T-M-I	VM-2 ET/SEC F	2 VO-1 VO-2	V0-2	-2 8-1 8-2 8-1 8-2 7-1 -2 DEGREE DEGREEDEGREEDEGREET, SEC F	8-2 FGREFOR	B'-1 Gerene	8 • - 2 6 8 - 6 6 8 - 6	7,550 H		1-107 51,557	101-10 2-101-2	U-1 FT /SEC 1	U-2 e1 /Ser
													1727				-	うちてい
		21.489	1010.79		675.09	663.52	752.30	0	48.10	0	19.42	57.30 2	15.79		-237.9	-1041.2	990.2	1041.3
		21.961	992, 49		693.11	690.19	711.08	0	45.74	•	23. 57	57.03 7	57.90		-306.6	-1063.9	1017.7	1063.9
		22.432	978, 26		698.84	699.94	684.35	0	44.41	0	27.32	37.23 7	86.34		-360.9	-1066.9	1045.4	1086.9
		23.902	944.83		696.66	704.91	638.25	0	42.30	0	15, 12	58.6J F	151.70		-489.9	-1156.7	1128.2	:156.7
		25.893	916.00		694.58	694.70	597.17	0	40.69	0	42.71 (51.00 5	45.19		-641.0	-1257	1238.2	1252,7
		27.902	905.67		696.37	685.34	579.05	Ð	39.75	0	47.72 6	33.08 10	35.02		-763.7	-1349.2	1344.7	1349.2
85 23	29.408	29.382	910.45		701.25	675.22	530.71	0	39.63	a	50.19 (3.31 10	145.96		-531.0	-1421.0	1421.7	1421.0
		29.856	916.81		692.46	670.46	600.56	0	40.35	0	50.67	5. 09 IC	92.45		-844.3	-1443.6	1445.8	1443.6
95 3 (0.382	30.293	927.39		662.65	663, 86	648, 80	G	44.40	0	51,05	55.64 10	154.84		-820.7	-1465.5	1469.5	1465.5
	INCS	NONI	INCS INCM DEV TUPN		CAMBER O	MEGA-B	CAMBER OMEGA-BD-FAC OMEGA-B	EGA-B I	055-P		PU2/E	FF-P	EFF-AD	9 - 273	1 - M	M-2	1.1	M*-2
NAN D	EGREE	DEGPEE	DECREE		DEGREE S	носк			TOTAL PROFILE		POI TOTAL	OTAL	JAIOL	STATIC				
ŝ	1.95	4.82	11.80	45.10	55.91	0	. 3245		.0410		1.856	ò	0	.7366	. 473	. 330	.6185	1.0236
10	.40	3, 33	11.05	45.74	53, 88	0	. 4838	.123	.0314	.0314	1.903	0	•	. 8039	. 838	. 575	.6552	1.0571
15	0	3.0	11.00	44.41	52,35	0	.4641	. 097	.0254	. (234	1.927	c	¢	.8311	. 543	. 565	.6793	1.0799
36	0	3.1	11.25	42.50	50.6 8	0	.4410	. 065	. 1810 م	.0153	1.937	Ð	0	.8776	.812	. 369	. 7316	1. 1313
50	0	3.2	12.05	40.69	49.55	0	.4397	.061	.0187	7810.	1.960	c	0	. 8764	. 782	.578	. 8063	1. 1920
70	0	3.3	13.40	39.75	49.93	0	.4343	.080	.0265	. 0265	1.949	0	0	. 8415	. 767	. 567	.8769	1,2514
85	.31	3.62	15.43	39.63	51.96	÷	.4210	.110	. 0345	. 0335	1.931	0	0	. 7985	. 767	. 554	. 9222	1.2915
96	1.45	4.73	17.00	40.95	53.84	0	. 5013	. 12.5	.0444	. ()444	I.920	¢	ç	. 7735	. 768	. 547	.9152	1.2986
95	3.80	7.00	18.90	44, 40	56.04	0	. 5365	. 151	. 4540	.0340	1, 903	0	0	. 7521	. 769	. 505	.8746	1.2974
Z	I-707-1	1-30 2 M	10/		EF-AD E	d⊷1.	MC/A-1											
ď	Br Kdi	RPM LBM/SEC		00	85 86	ж	LBMSEC											
11,	I, 110. 0 187. I	187.1	1.247	1.936	84.2	5.6	42.04											

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TABLE 7.1

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Blade-Element and Overall Performance with Uniform Inlet

50% of Design Speed

ROTOR

	DIA-1	01Å-9	1-7		T-MV		1-07	V0-2	8-1	B2					V 1 0V			25
NYOS	1	L NI	TASEL	. M	TIJSEC 1	ш	I JSEC. 5	T/SEC D	NEGREE D	EGREE		_			_	۴ļ	_	1580
]	17-467	19.769	282.1		282.1		0	375.8	00.	40.32		-			-	~	-	478.7
2	1.8.467	20.468	280.0		298.0			350.9	00.	30.85						-		5, 46
5		24.047			0.200			322.3	00.	38.29		-			-		-	509.7
8	22.116	22.9.4			203.7			258.1	00.	33.15					-	~	-	556,1
3	55.791	25.520	107.4		107.4		9	200.7	00.	28.15						~	-	618.0
2		9-0-02					•	160.5	00	24.09						أهر	-	679.9
8	11.294	500-90 <u>-</u>	0000		0.000	i		145.4	00	23.42	68.91	59.96	A12.2	671.2 -	-	-580.9	757.8	726.3
8		10.610	280.5		289.5		-	146.0	00	25.79		-				-	-	741.7
8	32.499	32.499 31.2-1	1 287.1	296.5	287.1	258.0	; •	146.2	00	29.54					-	-	-	757,2
	INCC	1NC.		+UR1 /	- ANRER C		D-FAC 0	OMEGA-D	1.05c-P	L055-P		if and if		1000 - 1000 1000 - 1000	ĩ	H-2	H - 1	M1-2
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9	5 .92 7.16 11.22 4	7.36	11.22	43.21	47.12	0000	.2782	.0870	.0186	.0166	1.2032	.9415	5 .9399	. 5005	. 2500	.5191	.4612	1901.
2	1.27	7.61	9.21	36.38	39.99	.0000	.3246	.1428	-	1150.		.8915		Ful7.	.2610	1982	- 1 856	. 396j
2	1.64	7.41	8.09	33.49	34.03	0000	.3355	.1468		.0321		.8724		.7163	.2657	#09#.	.5077	- # 002

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2500		.2610	2467		.2746	1770		.2717	.2637		1007	2588	
-8005		.7105	7143	2012	T#7.	7801	7401+	.7354	.6950		.5420	.5064	
9399		.8667	1040	C100.	8716	1220		.8429	7584		.63/8	5075	
2		.8915	0774	17/0+	.8745	BCOT.		.8455	7618		• 6 4 2 3	5123	
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	21.008	1-9-1	586.7	582.8	7.5	582.5	340	-20	5	-2.04	19.38	43.50	ŝ	802.9	-167.9 -	-552.6		531.8
	21.589	2 · # - 2	560.	561.2	1.1	560.7	313.4	10	ħ	-2.40	24.22	45,30	<u>6</u>	797.3	- 209.0	-566.6		543.2
		3-902	513.0	517.4	6.8	516.6	253.	-29	ę,	-3.22	34.78	49.63	145	. 6. 197.9	-310.8	-607.8		578.8
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	ALL'LC	7.902	A B B T	436.5	9	435.2	161	10-	2	-4-46	50.75	56.48	660	832.5	-514.8	-709.6		675.7
2	29.408	29.3a2	135+4	4000 t	0	404.0	148.	10-	6	-4.87	54.02	61.56	ş	848.3	-563.7	-745.9	712.1	711.5
8	29.916	29.8-6	415.00	380.6	7.0	378.9	149	55-	21	-5,32	56.05	63.45	5	847.7	-574.8	-758.2		723.0
8	30.362	10.243	1900	44 341.6 35		339.7	150	36	22	73 -6.06 53.46 66.18	53.46	66.18	686		-585.3 -	3 -585.3 -769.6		733.6
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	6°-6'	-7-05	9.41	37.55	53,88	0000.	.1608	.0472	.0120	.0120	6166.	• 0000	0000	3.7505		6190.		
	-10.67	11.41	8.62	36.45	52.51	• • • • •	.1532	.0379	.0099	6600.	0#66.	.0000	0000	1.8730		2202	0001	. 1133
	-13.19	-10.18	8.00	32.79	50.68	•0000	.1460	.0439	.0123	.0123	1466.	.0000	0000	1.7932		.4628	.4916	7136
	-15,85	-12.72	7,90	29.11	49.60	•0000	.1453	.0473	.0144	****	9466.	.0000	00000	2.4373		.4236	.5399	. 7262
	-15.60	-15.15	9.04	25.62	19.94	0000	1709	.070	.0233	.0233	.9926	.0000	0000	3002		. 3900	. 5938	7439
	-19,38	-16.07	11.02	24,80	51.99	0000.	-2157	.0822	.0286	.0286	91918	.0000	0000	4036	.3876	.3617	.6225	.7568
	-16.25	-14.02	12.00	26.40	53.57	0000	2413	0110	.0251	.0251	.9936	.0000	0000	.5688		9965.	.6178	7548
8	-16,96	-13.59	13.63	28.79	56.02	0006 -	.2955	.1047	.0375	.0375	.9916	.0000	0000	.5659		4000.	.6113	.7471
	Ž	NCOR-1 NCOR-1 TO/TO F	10	TO PO/PO	PO EFF	EFF-AD EFF-P		WC/A-1										
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	. iń	5550 96.	42 1.0	419 1.1221	221 75	79.08 80.24		21.67										

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TABLE 7.2

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Blade-Element and Overall Performance with Uniform Inlet

ROTOR

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50% of Design Speed

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2-5	T/SEC	1.474		510.1	1.955	618.5	6.0.4	726.4	7.2.0	757.4	M1-2		1480.	.3782	.3808	2034.	+118.	.5333	.5670	1590.	.5631
115	r/SEC +	5.554		471.8	540.8	625+0	101.7	1.04.	772.7	787.6	1¥		6454.	424	910c.	9936.	.6264	.6855	1264	0451.	• 7508
V01-2	LISEC P		-134.0	-104-2	-283.5	-297.9	6.9.4	-204.9	566.8	-281.9	2 1		50 ⁷²	. 4773	3644.	6404.	1995.	.3408	1026.		.2773
11.07											ī	1	.2432	.2489	.2533	.2614	.2638	.2591	.2519	5463.	.2472
212	•	æ	in i	a-	¢	۵	*	n	-0	N i	5F - P	LATIC -	.6926	.8282	- 8062	·8120	•8165	6105	1334	-6482	-5884
<pre></pre>	L'SEC F1	501.6	525+2	548.5	613.4	690.2	756.4	508.2	820.7	034.0	E-AD E	LAL SI	9638	.9280	9049	.8657	.8696	6546	7824	.6910	.6137
B1-2	GREE FI	12.86	19.13	25.48	37.49	48.56	55,85	60.25	62.90	65.94									·7861		
81	EGREE DI	57.55	58.45	59.34	61.84	64.9	67.79	69.79	70.30	70.80	P02/	POL. TO	1-2134	1.1957	1-1794	1.1595	1.1398	1.1252	*****	1-1050	1 • 0 952
8 - 2	EGREE D	42.41	41.58	40.18	36.50	52.15	28.57	28.47	31.19	34.12	LOSS-P	BOFILE	•0117	•0209	.0240	•0211	616 5	10134	0110.	.0229	•0259
1- 8	EGBEED	00.	00.	00.	00.	00.	00*	00.	8.	00.	L055-P	DIAL P	.0117	.0209	.0240	•0211	• 1165	+010+	0110.	•0229	•029
Ve-2	IZSEC_D	383.3	355.6	325.9	273.1	220.6	2.5.7	171.9	175.5	176.0	MEGA-R		7 40	962	1108	986	818	708	816	1363	• <u>[</u> 693
1-07	I_ZSEC F	••	10	0.	0.	0	9	0.	0	0.	D-FAC 0		.3202	.3552	.3682	.3626	.3281	2889	.2844	-3014	.3136
VM-2	T/SEC F	419.6	400.6	385.7	368.7	350.7	3.725	317.2	290.1	259.8	ME GA-B	HOCK	0000.	0000	0000	0000-	0000	0000	0000	0000	0000-
1-MV	T/SEC	269.2	274.8	279.7	289.4	292.8	287.8	279.2	276.6	274.3	AMRER (FCDFE S	47.12	39.99	34.03	24.18	14.68	9.6	8.01	7.64	7.45
V-2	TISEC 1	568.4	535.7	505.0	458.9	4.4.4	163.7	360.9	339.1	313.8	TURN	FGREF.	44.69	39.32	33.85	24.35	16.34	11.85	9.54	7.41	4.86
T- 7	TISEC	269.2	274.8	279.7	289.4	292+8	287.8	279.2	276.6	274.3 313.	ΟFV	FGOFE	10.99	9.51	8.95	7.7	5.3		6.13	7.78	10.08
DIA-2	Z	19.769	20.408	21.047	22.964	25.520	28-076	29.993	30.630	31-271	INCH	FGREE	0.60	0.84	0.62	7.95	7.97	86	7.68	7.55	7.50
DIA-1	NI	17.467	18.467	19-467	22.314	25-791	28.954	31.295	31.033	32-499	TNCS	DECREE	2.17	2.50	2.86	10.4	5	6.24	6.43	6.47	6.59 7.50
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175-1 371-5 345-5 345-5 219-5 2219-5 180-1 180-1 181-3 181-3	→ FAC 01 → 2258 → 2258 → 2258 → 2255 → 2255 → 23424 → 22251 → 2722 → 2725 → 2727 → 2725 → 2727 → 27
СКА 232 232 232 232 232 232 232 23	ER ONEGAB D- EE SHOCK. 97 0000 2 51 0000 2 51 0000 2 60 0000 1 60 0000 2 54 0000 2 54 0000 2 54 0000 3 54 0000 3 55 0000 3 55 0000 3 55 0000 3 56 0000 3 56 0000 3 56 0000 3 57 0000 3 57 0000 3 57 0000 3 50 0000000000
VH-L LVF-L 474.8 474.8 474.8 453.6 417.5 417.5 417.5 417.5 399.7 399.7 399.7 399.7 399.7 399.7 358.5 351.5	CAMBER 01 1 55.96 1 55.96 1 55.96 5 50.60 5 50.60 6 50.60 9 55.54 9 55.54 9 55.54 0.20 0.20 0.20 0.20 0.21 0.20 0.20 0.21 0.20
V-2 564.1 564.1 5539.1 5539.1 440.1 440.1 334.8 334.8 334.8	2 2 - 00 0 0 0 0 - 0
V-1 FV-2 FILSEE F125 500.8 559 500.1 559 510.1 559 510.5 159 410.4 561 410.4 561 410.4 561 410.4 561	DEV TURN DEGREE DEGRE 9.42 41.0 8.57 49.0 8.51 49.0 9.12 5.3 8.11 35.4 8.11 35.4 8.11 35.4 9.12 5.2 12.94 28. 12.94 28. 12.94 28. 12.94 28. 12.94 28. 12.94 28. 12.94 28. 20.21 10.458 31. 02.28 1.0458 10.0458
01 A - 2 01 A - 2 0 - 2 - 4 - 4 0 - 2 - 2 0 - 2 0 0 - 2 0 0 - 2 0 0 0 0 0 0 0 0 0 0 0 0 0	7 4 6 6 6 6 9 7 6 9 7 4 5 7 4 5 7 4 5 6 7 7 6 7 7 6 7 7 7 7 7 7 7 7 7 7 7 7
A - 1 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2	1105 1105 1105 1105 1105 1105 1105 1105 1115
× × × × × × × × × × × × × ×	성 신전 m 등 뉴상 양상 중 영 유
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TABLE 7.3 Biade-Element and Overall Performance with Uniform Inlet

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	1						101			-								
ROTOR	R						0 %ne	ou% of Design Speed	ign spi	eed								
	DIA-1	014-2		V-2	VH-1	2-4-2	1-07	VL-2		8-2	_	в2	1-17	V 1-2 V				02
N SOAN	IN		T/SEC F	T/SEC F			FI/SEC F		DEGREE DE	DEGREE DE	EGREE DI	DEGREE F1		L'SEC FI	FT/SEC F	FT/SEC	T/SEC FT	FT/SFC
	17.467	19.76	256.0	557.5	256.0	398.5				44.35	μaγ.	12.68	6.464				423.5	479.5
۹ ç	18.467	20.40	261.4	528.7	261.4	384.6		362.7	00.	43.33	59.72	18.96	518.5			-132.1	447.8	8°768
2 \$	19.467	21.04		1.661	266.1	370.6	i.	100	00.	42.07	60.59	25,33	541.8		-472.0	-175.8	472.0	510.3
2 8	22.314	22.96	274.9	447.0	274.9	344.2	•	285.1	• • •	39.62	63.06	38,21	6.06.9		- 1-145-	-271.7	541.1	556.8
3 5	25.791		277.6	407-6	277.6	330.5		238.5	00.	35.80	66.06	48.96	684.2	504.1	-625.4	-380.3	423.4	618.8
82	28.954		272.6	378.5	272.6	317.7		205.4	00.	32.89	68.78	56.24	753.1	571.8 -	-702.1 -	-475.5	702+1	684.8
85	31.295	I .	264.3	356.8	264.3	292.3		204.5	00.	34.99	70.79	60.79	803.5			-522.7	754.8	727.2
8	51.083		262.0	341.3	262.0	269.8	Ċ	209.0	00.	37.77	71.26	6 3.1 9	816.2		- 113.1		775.1	742.7
8	32.499		259.8		259.8	250.4		210.3	00.	40.03	71.76	65,44	829.7	602.7 -	-788.0 -	-547.9	786.0	758.2
	71105		252	Tubu C	AMOFD 0	OMF GA-R	D.EAC O	D-EAC DME64-8 1045-0 1055-0	1 4-550	9-220	P027	FFF-P FFF-AD		و 2 ج ال		ž	N - 1	H - 2
SPAN			4	, <u>u</u>	DEGREFE A				TOTAL PE	PROFILE	-	TOTAL TO		TATIC	I		I	
		6.6		-	47.12	0000	.3581	0228		f i	1.2226	ñ	9853 9	96596	.2312	- 1961.	4467	. 3641
• 5	77.6		6.93		39.99	. 0000	3837	.0514	.0112	.0112	1.2080	.9641	.9631	.9146	-2367	.1705	9014.	.3623
2 12	1.12	•	8.78		34.03	. 0000	.3964	.0694	.0151	.0151 1	1.1930	.9447	.9432	.8864	.2409		.4960	.3650
8	5.24	9.17	8.43	24,85	24.17	0000.	.4050	.0922	• (195		1.1698	.9u21	8998.	.8422	.2482	9960.	1150.	4695.
8	6.51		6.71		14.69	.0000	.3690	.0810	.0162	.0162 3	1.1541	.8847	.8821	.8375	.2500	.3613	.6209	
2	26.1		5.74		9.15	0000-	9155.	10701	8410.		1.1413	.0596	.8567	.8165	12452	1556.	.6806	,5065
18	7.44		6.67		8.02	0000.	3440.	.1277	•022ċ		1.1318	.7584	.7537	.7049	-2384	-3152	7217	, 5292
8	7.45		8.07	8.10	7.64	.0000	3558	.1635	.0272	.0272	1.1254	.6942	.6886	.6436	.2360	.3010	1343	.5274
8	7.54		9.57		7.44	•0000	.3672	.1869	.0292		1.1202	.6492	.6430	• 6050	.2340	.2880	.7462	.3306
			10/10			EFF-AD EFF-P	Q [
				LI INEL	1													
			1.04	.0499 1.1589		86.34 86.65	65											
STATOR	JR																	
	DIA-1	DIA-2	1	V-2	L-H-J	VN-2	-v0-1			8-2 81-1	1-18	81-2 2222		2>>>>>>	1-101-1	×-+07		0-2 2-7 2-7
NY SPAN	н	N	ET/SEC F	IJSEC F	1/SEC	1/SEC F	FT/SEC F	T/SEC DI	DEGREE DI	EGREE D	EGREE D	DEGREE	I VSEC F	1/260 1		1/360	FI/SEC F	
ŝ			587.2	2 526.9	1+49.7	526.9	377.5		40.01	10.1	14-63	44.68	404.8	141.1		-521.1	6" 46#	521.0
2	21.008	3 21.961	558.3	501.7	1.004	501.4	352.2	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	39 .11	-1-16	16°61		101.1	6 251				0.220
15	51.58C	22.432	524.4	443.2	417.7	192.9	326.0	-20 • /	06.10	-2.40	23.24	~ オ・ア オ	402.4				0.020	
8	23.314	1 23.902	479.9	445.2	389.3		280.6	-21.1	35.7 ö	-2.71	36.13	53.48	452.7	747.5	-284.7	-600.6	265.4	579.6

	23.514	202	5°51 =	440.5	584.5		200.0	1-12-	0/ • 00	-2-71	30.13	01.00	1.504	0.11	-502-	0.000-		0.4710
	25.601	25,893	4.242	409.4	375.6	408.8	237.4	-21.9	32.29	-3.08	45.54	57.81	536.8	767.8	-383.3	-649.8	620.8	627.8
	27.818	27,902	1.021	382+1	36.5	380.7	207.6	-32.7	29.32	16.4-	51.64	01.77	595,5	805.0	-466.9	- 09.2	674.5	676.5
	29.408	29, 362	414.2	357.3	357.4	356.8	200.2	-18.1	30.35	-2.90	54.65	63 . 97	617.8	913.1	-503.9	-730.6	713.1	712.4
	29.914	29.856	404.8	339.8	で、うれの	039.5	2.44.5	-13.8	32.01	-2.33	56.10	65.2 9	615.4	812.1	-510.8	=737.7	725.3	723.9
8	30.382 30.203	30.203	397.8	320.5	333.0	320.3	216.7	-12.6	33.01	-2.25	57.32	66.80	617.8	812.9	-520.0	- 747.1	736.7	734.5
	INCH DEV TURN CAMBER OMEG	INCH	DEV	TURN C	AMBER (4	D-FAC	D-FAC OMEGA-B	LOSS-P	Loss-P		EFF-P (EFF-AD	EFF=Þ	1-N	0#	H'-1	м2
X SPAN	DEGREE	DEGREE D	VEGREE D	EGREE C	DEGREE S	. x		-	-OTAL P	ROFILE		OTAL	TOTAL :	STATIC				
l vo	-5.95	-3.02	12.40	40.02	55.90	0000.	.2584	1790.	.0241	.0241		.000	.0000	.5549	.5173	.4683	.4115	.6586
2	+0.0-	-3.40	9.65	00.04	53.87	.0000			.0242	0242		.0000	.0000	.6165	-	.4457	.4110	.6500
2	-6.50	-3.56	8.56	40.42	52,51	.0000			-0174	.0174		.000	.0000	.6796		.4292	1514.	.6596
8	-6.80	-3.30	8.51	38,48	50.68	0000.			.0088	.0088		.0000	.0000	.8375	-	.3950	4325	.6632
3	-8.51	-5.38	8.97	35.37	49.61	. 0060			.0103	.0103		.0000	• 0000	.8202		.3629	.4802	.6807
2	-10.29	-7.05	8,59	34.23	49.91	0000			•0102	.1102		.000	.0000	.8289		.3385	.5302	.7132
8	-8.96	-5.65	13.00	33.26	52.30	.0000			.0156	.0156		0000.	0000	.8200		.3156	.5475	7103
8	24.2-	-4.10	15.07	34.35	53.54	0000			.0200	.0200		.0000	.0000	.8152		. 2996	.5447	.7161
8	-6.68	-3.32	17.44	35.26	56.30	26 56.20 .7000			•0319 •0319	.0319	.9927	.000	0000 0	.7613		.2622	.5461	.7157
	NC	NCOR-I WCOR-1 TO/TO	R-1 T0/	To P0/00	PO EFF	EFF-AD EFF-P		WC /A-1										

LEM/SEC SQFT 19.75

TABLE 7.4 Blade-Element and Overall Performance with Uniform Inlet

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50% of Design Speed

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U-2 1/SEC	478.5		000	222	0	725	740.		н2		N N		367	224	.477			۲ •
V-1 T/SEC F	422.5	446.7		539.7	2	156.0	2.1.2	786.1	1H						- 110.	156	5 7 SY	
VO-2	-				-	ماه	~		2		1.04		7		0426.	.3137		
FT/SEC F									Ĩ		-2197	2241		2359	·2307	-2239	2218	. 17,
VI-2	(80	1D I		- 00	J		DP.	or .		TATIC				6322	-79n2	1959.	0.25	CZ. C.
VIEC F	1				_				F-AD	DIALS		140			. 8359	.7108	6754	00.0.
62 6.2 6.2 7	12.00	10.29	24 ,66	38.27	49.14 55 25	74.19	63.31	65.59				9721						
B'-1 GREE DE	60.14	00 • 1 9	61 • 84	64 -25	67•19 40-16	71.62	72.28	72 • 73	-	F		1.2152		- 10			ير ه	,
B-2 EGREE DI	46.57	45.41	90° 88	42.58	39.95	10.04	5.00	46.18	Loss-P	ROFILE	•0023				1610+	·020.	•0326	acc 0.
B-1 EGREE DI	3.	00"	00.	-00	5		9	00.	-	4		5 5						
T/467 0	398.	372.3	0.040	298.5	255.9	227.0	241.5	242.8	MEGA-B	ام ا	- B 247	614				1751	1261.	•21 //
1.00-1	Q	9	9	9	??	99	79	•	D-FAC 0		1995.	-41.87			3776	.4109	4 L 74	•4230
	376.9	366 b	356.4	324.7	312 .0		251.0	233.0	ME GA -B	HOCK	0000.	0000-	0000			0000	0000	0000-
TVK+1 T/CEC F	242.5	247.6	252.0	260.2	202.5	256.8	246.4	244.3	AMBER 0	EGREE S	47.12	39.99	34.03	2410	9.9	8	7.65	C + • 1
2 V-1 V-2 V	548.1	522.7	496.2	1.144	5.5	378-0	348.5	336.5	TURK C	FGREE C	48.14	42.7	51.19			10.35	8.97	7.14
1 - 7 1 - 7 1 - 7 1 - 7	242.5	247.6	252.0	268.2	262 2	25648 24846	246.4	244+3	DE V	LEGEE L	10.13	8.66	8.09		i i	92	6-21	9.7
014-2 5 IN	19.7	20.41	21.0	22.9	25.52	20.00	9	31.2	INCH	EGREE	11.19	11.38	11.07	01		14 6	9.53	04.0
1-410	17.467	18-467	19.467	22.314	25.791	28.254		32.499	INCS	LEREE C	4.76	5-04 11	10.0	24.0		0.47	8-45	6.52
,	7					2 8				SPAN D	6						8	
, i	d									2								

T0/T0 P0/P0 EFF-AD EFF-P -144_ET -144_ET 144_FT -744_ET 1.0559 1.1702 85.31 83.066

STATOR

Į.	••• - ?	0 r -r	a 2336 11 23 25
- 14. j			
1-1 1/5EC	20255 2025 2025 2025 2025 2025 2025 202	723	
			1 1 1 1 1 1 1 1 1 1 1 1 1 1
	-108-1 -1666 -18666 -2664 -27656 -2664 -26	A NOA	8
V2 1/5EC F	4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	788.7 788.7 791.5	EFF-P 1A11C 6447 66447 66447 68855 685555 6855555 6855555 6855555 6855555 68555555 685555555555
· · · · ·	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4		171 171 171 171 171 171 171 171 171 171
B'-2 EGREE F	86.40 81.00 81.00 80.40 80.40 80.40 80.40 80.40 80 80 80 80 80 80 80 80 80 80 80 80 80	62.99 64.94 65.92 67.28	EFF-PE 01A 11 0000 00000 00000 00000 00000 00000 0000
8'-1 EGREE DI	14+28 19+59 24+94 35+355 35+355 35+355 35+355 35+355 35+355 35+355 35+355 35+355 35+355 35+355 35+355 35+355 35+3555 35+3555 35+3555 35+3555 35+3555 35+35555 35+35555 35+355555 35+355555555	51 • 74 55 • 0 8 56 • 20 57 • 4 9	P02/ P01 II 9634 9634 9871 9952 9955 9955 9956 9956
B-2 EGREE DI	58855 1777	-1-79 	R0F1LE 80F1LE •0252 •0285 •0285 •0142 •0147 •0179
8-1 EGREE DI	42.54 41.27 40.09 58.73 8.73 8.73 8.73	33.74 36.60 39.01	LOSS-P DIAL 0252 0255 0285 0285 0129 0129 0179 0179 0179
VO-2 T/SEC D	8 2 2 5 9 7 7 5 9 7 7 5 9 7 7 7 5 9 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	21.6	#E 6A -8 - 1012 - 1012 - 1012 - 1119 - 1119
	385 6 356 8 356 8 293 8 295 8 205 8 205 8 205 8 205 8 200 8	1 -	0 - FAC 0 - 5992 - 3132 - 3132 - 3132 - 3132 - 3132 - 3927 - 4193 - 4560
<u> </u>	494 4 469 4 461 6 4 1 5 1 6 6 6 6 6 6		H 2000000000000000000000000000000000000
L L.(0.00.00.00	10 0 00	RAMBER EARES 53.607 53.607 52.61 52.651 4.9.651 4.9.651 53.555 553.555 553.601 553.601
v-2 IZSEC E	494.9 469.5 451.5 415.2	321.8 321.8 305.6	TURN CI E DEGREE J 002 42.05 003 42.05 004 42.05 20 31.55 2
V-1 1/SEC F	109 573.5 494.9 424. 101 548.0 469.5 41. 132 522.2 451.5 399. 102 469.6 415.5 366.	4180 407.5	E66E 100-07 10000000000
DIA-2 In F	40404	27.902 29.582 50.293	INCH EGREE JE - 85 - 1 - 28 - 1 - 28 - 1 - 41 - 2 - 65 - 2 - 66
1-41	20 409 21 21 589 21 23 514 23	29-408 27-90 29-408 29-36 29-914 29-85 30-382 30-29	INCS INCH DEV DEGREE DEGREE DEGREE -3.76 - 03 12.6 -4.35 -1.41 9.0 -4.35 -1.41 9.2 -4.94 -1.81 9.3 -5.62 -2.62 70 15.3 -1.59 1.74 17.7 -1.59 1.74 17.7
5 7	1	35888	20 20 20 20 20 20 20 20 20 20 20 20 20 2
-	l I		xel

WC/A-1 By/SCC LSOFT 18.71 MCOR-1 WCOR-1 YU/TO PO/20 EFF-AD EFF-P 1.4 ET 1.4 ET 1.4 ET 1.4 ET 1.4 ET 1.4 ET APH LUNYSEC 5543 83.24 1.05" J 1.1528 81.79 82.20

ROTOR

TABLE 7.5

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Blade-Element and Overall Performance with Uniform Inlet

ROTOR

50% of Design Speed

C ELVEC, ELVEL, ELVEL	$ \begin{array}{c} \mathbf{F}_{1} \left(\mathbf{F}_{1} \right) \left(\mathbf$				0		•				6 -0	1	(a		×2	1-107	V01-2	1-5	2-5
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	DIA-2 V	<u> </u>			VM-L TACTO FI	TASEC F	T/SEC F	TVSEC D	9	EGREE DI	EGREE D	- Jake	T SEC 1	T/SEC	IVSEC F	T/SEC FI	r/SEC F1	/SEC
 233.5 349.0 349.5 245.5 349.0 245.5 349.0 245.5 349.0 245.5 390.0 250.9 397.2 539.4 229.5 250.9 251.5 599.4 229.5 250.9 251.5 599.4 229.5 250.9 251.5 599.4 229.5 250.9 255.5 59.5 59.5 59.5 59.5 59.5 59.5 5	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	076 01	ŀ٩	- 20	515.7	1 100	151.2		<u>د</u>	6	48.70	61 .57	12.05	4.80.5	361.2	-422.5	-75.4	422.5	478.2
 237.7 340.6 245.5 396.7 246.5 396.7 246.5 396.7 246.5 396.7 250.4 525.6 250.5 57.6 57.5 57.5 57.5 57.5 57.5 57.5 57	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		•					2			47.10	62-44	19.55	5.4.1	368.6	-446.7	-117.1	446.7	1.56#
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$			0.000				2					20.00		176.7	-470.9	-159.6	470.9	509.1
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1.047		237.7	10001	237.1	340.0	9	0	-					107	I OF Y		5 19 . B	555.5
5 246 3 268.5 · · · · 265.7 · · · · · · · · · · · · · · · · · · ·	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	106.0		245.3	431.9	245.3	306.	••	3.4.0	~	クレ・オオ	00.00	02.00	242					
• 250.5 •00 42.26 71.04 57.24 700.5 509.6 757.0 429.5 757.0 • 220.7 250.5 •00 47.32 75.9 61.90 757.0 429.5 757.0 • 220.7 250.5 •00 47.32 53.40 050.5 505.6 771.2 • 220.7 210.5 •00 47.32 53.40 050.5 556.5 771.2 40.77 771.2 • 220.7 210.6 •0 51.50 73.55 53.40 050.6 760.7 700.7 700.7 700.7 710.2 710.7 <	$\begin{array}{c} \begin{array}{c} \begin{array}{c} \hline 0 & 0 \\ 0 &$	5.500		246.1	192.5	246 3	588°C	•	265.7	_	42.61	68.45	50.54	670-8	1.001	-9539-			
351.9 232.3 10 260.0 107.32 72.95 10.90 720.9 771.0 199.5 771.0 355.6 233.7 235.6 771.6 100 21.5 171.6 100.7 771.2 355.6 233.7 235.6 771.6 100 21.5 175.7 149.5 751.6 355.6 233.7 235.6 571.6 10.0 21.5 171.6 140.7 711.2 355.6 233.7 235.4 55.96 518.7 350.6 771.2 140.7 711.2 355.6 517.7 51.5 518.7 530.6 714.2 140.7 714.2 1700 211.6 0 51.5 731.7 992.9 996.6 140.6 140.7 166676 0 149.7 0 121.1 101.1 101.1 140.7 140.6 140.6 140.6 140.6 140.6 140.6 140.6 140.6 140.6 140.6 140.6 140.6 140.6 140.6 140.6 140.6 140.6 140.6 140.6	$\begin{array}{cccccccccccccccccccccccccccccccccccc$				172.6		275.7		250.5		42.26	Zin D ⁴	57.24	240.5	509.8	-7u0.4	-426.7	700.4	2.519
5 5.36.7 5.36.9 5.5.49 6.5.9 5.5.49 6.5.9 5.5.49 7.4.5 -470.7 771.2 6 228.7 216.0 10 271.5 .00 51.5.1 73.5.5 65.49 6.5.49 6.5.9 516.1 -40.9 760.1 771.2 6 228.7 216.0 .0 51.5.1 73.5.5 65.49 6.5.9 516.1 50.6 74.9 760.1 CAMGER SHOCK .0 1074. PROFILE POL PO21 1074. 92.6 9914 9812 2113 4555 4604 2 34.03 .0000 .4492 .0128 0028 1.2217 9929 9914 9812 2113 4555 4804 3 34.03 .0000 .4479 .0128 0028 1.2217 9929 9949 2211 .4555 4604 3 34.03 .0000 .4479 .0157 .0127 10128 1.2116 .0291 .2213 .4555 5493 5493 5493 5493 5493 5493 5493	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$						1 1 1 1 1 1 1 1		266.4		1	72.91	61.90	792.0	520.9	-757-0	-459.5	757.0	725.5
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TABLE 7.6Blade-Element and Overall Performance with Uniform Inlet 50% of Design Speed

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N N 15 15 15 15 15 15 15 15 15 15 15 15 15	DIA-1 IM 27.467 19.467 19.467 23.791 23.295 31.295 31.295 31.295	DIA-2 FM FF 7 19.769 7 20.447 7 20.447 7 20.496 7 20.966 7 25.529 9 31.271 9 31.271	V-1 220 220 220 220 220 220 220 220 220 22	2 V-1 V-2 V F175EC F175EC F17 2 220.4 511.5 2 2 225.4 486.4 2 2 236.4 432.6 2 2 236.4 432.6 2 2 236.4 432.6 2 2 236.4 331.7 2 2 235.1 371.5 2 3 222.1 300.0 2 1 220.1 300.0 2 1 20.0	77560 2259.0 2259.0 2259.0 23151 231	276-1 247-5 247-0 240-5 229-9 229-9 275-1 257-1 259-6 259-7 259-6		00+20,000 + + + 50 334+000 + + + 10 534+000 + + + - 10 534+000 + + + + + + + + + + + + + + + +	89 14 14 19000000000000000000000000000000	MB1 MB1 49 49 49 49 40 40 40 40 40 40 40 40 40 40	HER CONTROL CO	*	74 75 75 75 75 75 75 75 75 75 75 75 75 75		V01 17956	14000 14	1.556 4.2256 4.2256 4.471.4 4.471.4 7.01.4 7.01.4 7.75.0 7.75.0 7.75.0 7.75.0 7.75.0	757.2 756.2 7594.1 757.9 7126.2 731.6 731.2 731.
궻 소 전 전 전 전 전 전 전 전 월 소	INCS DE97EE 7.295 7.295 7.295 7.295 7.295 7.295 7.295 7.295 7.295 7.295 7.295 7.295 7.105 100.126 100.126 100.126 100.126 100.126 100.126 100.126 100.105 10000000000	DE DE CONCE	0.00 0.00		CLAMER CLAMER 39.99 34.03 34.03 34.03 34.03 74.07 7.02 7.02 7.02 7.02 7.02 7.05 7.05 7.05 7.05 7.05 7.05 7.05 7.05	6444 640000000000	00 + + + + + + + + + + + + + + + + + + +	046.54-6 L025-P 0.212 0049 0.2213 0049 0.231 0049 0.231 00217 1126 0217 1256 02217 1256 02217 1256 0217 1258 02217 1258 02217 1258 02217 1258 02217 1258 00217 1258 002000000000000000000000000000000000	001026 01111 001000 00100 00100 000000	LOSS-P 404111 0008 0008 00190 00190 00190 0025 00217 0025 00275 00275 00275 00275	P02/ 	0144 0 0144 0	FFFAD FOTAL 9978 9978 9978 9978 9978 9978 9978 9978 99588 995888 99588 99588 99588 99588 995888 99588 99	FFFF 			4 -1 - + + -1 - + + + + + + + + + + + + + + + + + + +	1-2 -315 -315 -3166 -3226 -3266 -3226 -3266 -3226 -3266 -327
			10	Tc/T0 P0,	PO/PU EFI	EFF-AD EFF-	đ											

INLET INLET INLET INLET INLET INLET 1.0596 1.1872 84.52 84.72

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	014-1	DIA-2	-1	۲ ۲		2442	1-07	2 - 07	8-1	8 - 2		B*-2	1-17	V2	107	V01-2		2-5
NVS X	Z	Ĩ	F1/SEC F1/S	FT/SEC	Ξ.	FT/SEC F	1235(1)	TISEC D	EGREE D	GREE	Ŧ	EGREE F	TYSEE F	TVSEC F	1/SEC F	T/SEC-F		TASEC-
uD	20+409	21.489	553.1	のまます		2.444	392.5	10.6	45,20	1.3	÷	48.93	402.7	676.1	-101-7	-509.8		520.3
	21.000	21.961	530. B	422.5		422.4	370.4	-5.7	44.24		ō	51.83	404.9	683.7	-138.2	-537.4		531.7
	21.589	22,432	506.5	405+1		435+0	348.2	-10.8	ちま ちゃ	-1.5	n,	53.83	407.5	686.3	-174.5	-554.0		543.1
	23.314	23.902	455.1	169.7		369.6	309.4	-10.3	42,83	-1.5	Ē	57.88	420.5	695.5	-255.1	-589.0		578.7
	25.601	25.693	418.5	3.5.6		336.4	277.0	-12.0	41.51	-2.0	r,	62.23	464.5	722.2	-342.9	-639.0		626.9
	27.018	27.902	0 . 2 .	316.5		- 316-3	272.9	, 6 -	42.23	1	'n	65.22	- 501:0 -	-254.34-		-68512-		-91516-
	29.408	29.382	412.6	304.5		オーオビロ	291.1	6.9	44.87	1.2	ñ	66.63	512.5	767.5	-421.0	-704.6		711.4
81	29.914 29.855	2°.855	413.8	301+1		301.0	294.2	, 8 ,	45.50	1.2	ŝ	67.20	518.0	776.8	-429.1	-716.1		722.9
	30-382	30.293	408.7	291•5	281.3	291.4	296.5 6.6	6 °	5 46,51	1.3	N.	.36 68.15 5	521.5	783.1	-439.1	-439.1 -726.9	735.6	733.5
	INCS INCH DEV TURN CI	INCM	Cev	TuRes (CANGER	OME 6A-B	C-FAC 0	MEGA-B	L055-P	LOSS-P	P02/	555-P 5	FF-AD	5 5 - P	L F	4-2	M - 1	M2
X SPAN	DEGREE	DEGREE (JEGREE L	DEGREE	DEGREE	SHOCK		-4	OTAL P	ROFILE	104	07AL - 7	OTAL 5	TATIC			1	
ھ	89	2.03	13.7-	43 . 84	55,90	.0000	.3637	.1180	• 0294	• n294	.9819	• 0000	.0000	1769.		.3920	.3570	.5965
2	-1.13	1.81	10.66	45.03	53.87	• 0000	.3010	.1205	0330	.0330	.9817	.0000	.0000	.7020		.3726	.3603	.6030
5	95	1.99	47.0	44.96	52,51	. 1000	.3821	.1142	.0299	.0299	.9852	.0000	.0000	2617.	.4457	.3572	.3623	.6051
8	14.	3.41	9.63	りま。まさ	5n.67	. 1000	. 3823	657	.0184	44TU .	.9933	.0000	. 0000	.8235	-	.3256	3735	.6125
8	.82	3.95	5.0	43.55	49.61	0000.	.4n55	.0478	.0146	.0146	.9957	.0000	.0000	.8685	-	.2960	.4108	.6351
8	2.56	2.5	11.75	#3 . 97	49.92	.0000	4506	. 06 . 5	.0230	. 1230	i all	.0000	. 0000	9168*-	_	-2775-	54442	
	5++5	P.76	17.25	43,58	52.01	0000.	5029	.1384	• 0 4 8 4	1240.	.9880	.0000	.0000	.7130		2659	.4501	.6703
8	5.97	9.29	16.00	44.21	53,54	0000.	.52 0 3	1536	•0546	• n546	•9866	.0000	.0000	•6924	•	.2027	.4547	.6777
8	6.81	10.19	20.67	45.21	56.00	1 56.00 .2000	0 .5429 .1649 .0594 .0594	.1649	•0594	• 0594	.9869	• 0000	00000 0	.6816	•	.2540	.4568	.6824
	2	NCOR-1 MC64-1 13/10	101 1-H			F-AD EFF		C/ 4-1										
	2 î	LET IN			INLET IN	LET IM		33/18										
	z iń	5549 75	IM/SEC 75.64 1.0596		-	79.74 80.22		16.99										
						•												

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ROTOR

Blade-Element and Overall Performance with Uniform Inlet TABLE 8.1

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ROTOK

70% of Design Speed

DIA-1 DIA-2 V-1 V-2 VW-1 VW-2 V0-1 V0-2 B-1 B-2 17.467 19.467 9.410.6 799.3 V10.6 609.9 ° 1656C DEGREE DEGREE 19.467 20.408 440.8 553.0 449.9 560.0 ° 1457.4 ° 00 39.05 22.314 22.909 444.8 553.0 444.8 540.9 00 35.7 ° 00 39.05 22.5179 25.520 444.8 553.0 444.8 540.9 00 35.7 ° 00 38.05 25.5791 25.552 441.7 552.4 443.7 502.9 ° 0 25.26 25.5993 428.7 521.2 425.7 447.4 ° 0 230.4 ° 00 28.7 25.993 228.779 403.1 424.3 423.9 ° 0 231.4 ° 00 28.7 25.993 228.779 403.1 424.3 423.9 ° 0 231.4 ° 00 28.7 25.993 228.779 25.21.2 425.7 447.4 ° 0 231.4 ° 00 28.7 25.993 228.7 0 231.4 ° 0 231.4 ° 0 25.6 ° 0 33.6 25.993 228.7 0 10 231.4 ° 0 231.4 ° 0 25.6 ° 0 33.6 25.959 22.993 428.7 521.2 425.7 447.4 ° 0 231.4 ° 00 28.7 25.959 22.993 428.7 521.2 425.7 447.4 ° 0 231.4 ° 00 28.7 25.959 23.993 428.7 521.2 425.7 24.14 ° 0000 33.97 ° 0554 0018 0118 25.473 41.14 47.12 0000 3397 1153 0.255 0255 1.68 5.53 7.54 22.21 34.0 0000 3397 1154 0255 0253 1.68 5.53 7.54 22.27 24.14 0000 3397 1253 0253 4.63 5.65 5.117 10.0 212 4.63 5.65 5.117 12.0000 3397 0.0554 0.2564 0.2564 0.2564 0.0000 35.7 0000 0000 0000 00000 00000 00000 00000 0000	1-2 8*-1 8*-2 V*-1 V*-> V0*-1 V**-2 U-1 U-2 2865_degree_degree_1/550 f1/560 f1/560 f1/560 f1/560	55.24 14.10 720.3 628.9 -591.8 -153.2 591.8	. 56.14 19.35 753.5 615.3 -625.7 -204.0 625.7	1 57.02 24.82 786.2 619.4 -659.6 -260.1 659.6	59.53 37.26 877.2 680.7 -756.0 -412.3 756.0	. 62.65 47.57 983.8 777.9 -873.8 -574.3 873.9		67,98 59,25 1143,7 914,4-1060.3 -785.7 106n.3	68,55 62,28 1160.6 911.2-1080.2 -806.3 1080.2	69.08 67.18 1178.8 896.4-1101.1 -826.2 1101.1	P02/	PO1 IOIAL TOTAL STATIC	1.4264 .9632 .9613	1.3893 .0146 .9105 .8039 .3834 .6731 .6926	. [.3599 .8906 .8457 .7835 .3910 .6398 .7241	[,]]20 .8884 .8A40 .8225 .4056 .5783 .6171	1.2745 . P940 . 8903 .8533 .4112 .5307 .9015	L.1.424 .8607 .86648220 .4029 .4936 .9837	1.1110 . YEA4 . 7477 . 7081 . 3898 . 4596 1.0390	1.1854 .8 339 .6453 .6224 .3853 .4244 1.0559	1.1480 . 54 . 5065 . 5313 . 3823 . 3656 1. 0715
V+2 VM-1 VM-2 759.3 4:0.6 600.4 7757.6 419.8 600.4 721.5 421.9 560.4 653.0 444.6 540.4 553.0 444.6 540.4 552.4 443.7 552.4 443.1 424.9 940.4 443.1 424.9 947.4 443.1 424.9 947.4 41.14 47.12 4000 35.21 24.19 0000 35.21 24.19 0000 35.21 24.19 0000 11.00 14.05 00000 11.00 14.05 0000 11.00 0005 11.00 14.05 0000 11.00 14.05 00000 11.00 14.05 00000 11.00 14.05 00000 11.00 14.05 00000 11.00 14.05 00000 11.00 14.05 00000 11.0	L VO-2 B-1	00	0.	00	00	00	9	00	00	00.	OMEGA-A LOSS-P	TOTAL	.0554 .0118	1161 0253	1321 .0.88	.0482 .n2'	. r67. []	10	(D. 051	1510 0277	2040 0400
DIA-1 DIA-2 V-1 17.467 19.769 410.6 19.467 20.408 410.6 19.467 20.408 419.8 22.5914 22.964 444.8 22.5914 22.964 444.8 22.991 25.596 451.7 22.459 2993 428.7 22.459 20.993 428.7 22.459 20.993 428.7 22.459 20.993 428.7 22.459 20.993 428.7 22.459 20.993 428.7 22.459 20.993 428.7 23.459 20.993 428.7 23.459 20.993 428.7 23.459 20.993 428.7 24.53 25.53 7.54 2.574 5.31 2.574 5.31 3.575 5.31 3.575 5.516 5.517 5	14-1 14-2 1550 51/560 51	4:0.6	419.8	427.9	0.111	451.9	44.2 × 7	424.7	424.5	420.9	AMBER OMEGA-R	EGREE SHOCK	47.12 .0000	39.99 .000n	34.03 .0000	24.15 .0000	14.68 .0000	9.15 .0000	8.04 .0054	1 69 .006	
	DIA-1 DIA-2 V-1 X ET/SEC FI	17.467 19.769 410.6	18.467 20.408 419.3	19.467 21.047 427.9	22.314 22.964 444.8	25.791 25.520 451.9	28.954 28.076 42.42.2	31.295 29.993 428.7	31.483 30.630 424.3	32.459 31.271 420.9	INCS INCM DEV TI	EGNEE LEGREE DEGREE DEI	14 6.29 12.23	.18 6.53 9.75	53 6.32 8.29	1.68 5.53 7.54	2.12 5.74 5.31	1.23 6.02 Lall	4.63 5.66 5.16	4.75 5.40 7.22	

T0/T0 P0/P0 EFF_AD EFF=P Imlet __Imlet. Imlet ... \$ * 1.0856 1.2788 85.09 54.65

STATOR

	1 014-2		212	1-47	ž	- U- U	Ę		R=3	8 - 1			< X	107	~-••7	Ī	2	
SPAN IN	IN	FLISEC E	LISEC E	LASEC E1	ÿ	FLASEC EL	Y	GREE DE	GREE DE	GREE DI	Ĩ	TISEC E	LISEC F	L/SEC E	TASEC E	T/SEC.E	r/SEC-	
5 20.4	09 21.48	9 860.6	853.2	700.3	5	500.4	2	35.55	-3.58	15.26		725.9	1155.7	-191.0	4.181-	691.5	728.1	
10 21.0	08 21.96	1 820.0	626.9	659.4	ŝ	473.7	ŝ	35,28	-3.70	19.58	-	710.8	1,147.6	-238.1	-797.3	711.8	744.1	
15 21.5	89 22.43	2 705.5	801.1	649.7	y,	7.1.7	56	34.18	-b.ů3	24,04		712.0	1142.5	-290.0	-616.3	731.4	760.0	
30 23.3	14 23.90	2 720.9	740.1	624.5	5	959.9	ŝ	29,94	-4.61	34.51		758.7	1149.3	0.054-	-869.3	789.9	809.8	
50 25.6	01 25.89	3 673.2	687.7	607.4	÷	289.2	ŝ	25.44	-4.50	43.54	ž	839.2	1157.0	-578.2	6.160-	867.4	877.3	
22.4	18.27.90	2 -646.0	-5.910	54742	4	**5.44 ···	ġ	72.29	-4.70	95.94	1	31916	1103.8	-697.4	-907.9	942.5	-945.3	
86 29.4	08 29,36	2 631.9	591.8	566.6	5	دي ج ،	20	21.84	-1.95	52.39	2	961.2	1175.4	-761.4-	1015.7	996.4	995.1	
90 2 9 .9	14 29.854	6 608.6	564.1	560.5	3			22.94	01	54.18	2	7.7.26	1158.6	-776.5-	1012.0	1013.5	1011.	
50° 30° 1	62 30.29	1 30.362 30.293 565.7 506.9 512.2 5	506.9	512.2	65.	د.	5	7 25.11	11 3.59 57.02 6	57.02		940.9	115.9	-789.3	14 340.9 1115.9 -789.3 -944.6 1	1029.4	6 1029.4 1026.3	
INCS	S INCH	ц С	YURN C.	AMBER ON	V TURN CAMBER OMEGALR UNDER DEFICIE	1	1. 	50	0.55. 0	P.)./	Ĩ	FFD	EFF-P		5 - 1	[¥	M2	
X.SP.AN DEGRE	E. DEGREE	DEGRI	EGREE DI	EGREE SE	HOCK		i.	14. 29	14 A A	E.L.	DIAL	DTAL S	TATIC				!	
5 -14.	1	1 8.83	39.13	55.90	.0000	.1654	1.5.5.	15.00		, ⁰ 661	.0000	-0000-	3.7234	-	.7663	6449.	1.0380	
10 -10.	05 -7.12	•	38.97	53,67	.000	.1527	.0.0.	بر د مر		1919.	.0000	.0000	2.4967	-	7417	.6347	1.0292	
15 -lu.	-14.48 -7.53	•	58.21	52.49	00000	.1434	0560		0140	りさせた 。	.0000	.0000	1.6011		.7177	.6396	1.0235	
30 -12.	79 -9.74	•	34.55	50.68	.000	.1352	.0627	.0:76	.0176	9986 .	.0000	.0000	1.6241	-	.6520	.6830	1.0200	
6 -15.	40 -12.26	~	29.99	49.64	.0000	.1342	e170.	.0236	.0236	.9833	.0000	.0000	2.1856	-	.6146	.7534	1.0340	
21- 2	4014.11	4	27.00-	49.92	- 0000-	.1630	2401	-0346 0 ·	- 0.346 -	- 97.9-	.0000	-0000-	55.44.52		.5700	8223	1.0557	
86 -17.	-17.54 -14.23	13	23.79	52.01	.0000	.2048	9451.	-0505	.0505	.9720	.0000	.0000	0432	-	.5250	.9559	1.0427	
90 -16.	52 -13.19	17	22.95	53,57	.0000	.2120	.1316	0469	.0469	.9762	.0000	.0000	.1579		.4987	.8498	1.0243	
36 -14,61	61 -11.24	23	21.53	56.04	.0000	.2371	.1597	7 .0575 .0575	.0575	.9750	.0000	-0000	0 .0000 .0000 .26n1	.5000	.4455	.8398	9 609	
	NCOR-1 P	NCOR-1 PCOR-1 T.VTO	TO POL	PO EEC.	AD CEF-	ر ع	1-4											
	INLET .IN	I .INLET . INLET	EI INFEI		INET INET.		-LBM/SEC											
	Ξ.	M/SEC			-		E T											
	7/65 1	135.56 1.000	PCC2.1 0C0	91 190	1.67 UC.		046											

8.2 TABLE

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Blade-Element and Overall Performance with Uniform Inlet

70% of Design Speed

 B-1
 B-2
 B-1
 B-2
 V'-2
 V'-1
 V'-2
 U'-1
 U'-2

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 ¥1-2 Ĩ ī VU-1 V0-2 FT/SEC FT/SEC DE 5 0 598.5 6 998.5 7 998.5 7 999.5 V-2 VM-1 VM-2 C F1/SEC F1/SEC F1/SEC F1 + 780-1 403.4 547.9 0 695-1 411-0 52.-1 -7 583-5 433.7 468.6 -8 519.4 413.4 460.5 -3 519.4 413.4 40.9 -5 491-1 409.5 401.1 -5 491-1 409.5 401.1 103.1 ROTOR

J EFF-P TO/TO PO/PO EFF-AD

1.0934 1.3118 86.33 86.85

2-+0A

1-.07

2-12

8 -2

1-18

1-07

STATOR

F1/SF 7759.2 7759.2 7759.2 7759.2 866.9 86 9675 9546 9546 9575 9676 1.0085 1.0191 1.0191 1.0191 1.0191 2-1-2 BALLAT .5943 .6376 .7032 .7698 .7698 K--1 1022.5 .7461 5409. .5908 1.56H E F1/4EC F1/3EC T1/3EC F1/4EC F1/4 13 6679 1077.0 -226.6 -794.1 7 35 6639 1070.6 -281.5 -799.8 7 36 739 1070.6 -281.5 -799.8 7 36 739.9 1070.9 -548.8 -979.8 7 36 788.2 1109.9 -548.8 -979.6 7 31 866.3 1143.5 -662.9 -968.9 7 31 866.3 1143.5 -662.9 -968.9 7 31 866.3 1143.5 -722.5 -1035.6 103 42 903.9 1163.3 -730.4 -1041.4 1 34 903.9 1163.3 -730.4 -1041.4 1 34 2 895.4 1158.6 -740.5 -1055.6 103 6865 6552 6552 6552 5559 5556 45756 45756 N-X 7382 6603 6603 65127 5528 5528 5528 5528 1 EFF-P 51411C 7 . 6778 7 . 6878 7 . 6878 7 . 7898 7 . 7898 7 . 7898 7 . 7914 7 . 7344 P02/ EFF-A EFF-AD E P01 T0TAL T1AL S 9.97 0000 0000 9921 0000 0000 9933 0000 0000 9933 0000 0000 9933 0000 0000 9953 0000 0000 9871 0000 0000 9871 0000 0000 0664EE F1 6 46.73 6 46.73 7 55.38 7 55.38 7 55.38 7 55.38 0 63.54 65-42 DEGREE D 1 2906 9 35:07 9 35:07 9 35:07 9 35:07 9 35:07 9 35:07 1 2 96 C FT/SEC DEGREE DEGREE DE 1.3 -41.7 37.87 -3.09 1.4 -00.9 35.65 -3.17 1.6 -87.7 29.32 -4.44 1.1 -44.0 28.57 -4.13 1.1 -44.0 28.57 -4.37 1.1 -44.0 28.57 -4.44 1.1 -44.0 28.57 -4.37 1.1 -14.0 28.57 -4.45 1.1 -14.0 28.57 -4.45 1.1 -14.0 28.57 -4.57 1.1 -14.0 28.57 -4.57 1.1 -14.0 28.57 1.1 -14.0 28.57 1.1 -14.0 28.57 1.1 -14.0 28.57 1.1 -14.57 1.1 -14.0 28.57 1.1 -14.57 1 P COSS 0241 OMEGA-B LOSS-P 2449-1 249-10 2122 ONEGA-B D-FAC 600.00 C F1/SEC F1/SEC F1 9 739-5 662-5 19 739-5 662-5 19 739-5 662-5 19 652-5 562-4 5 616-5 565-4 5 5 16-7 556-3 5 516-7 556-3 5 519-2 550-3 5 519-2 550-3 5 519-2 550-3 5 519-2 550-3 5 519-2 550-3 5 519-2 550-3 5 519-2 550-3 5 519-2 550-3 5 519-2 550-3 5 519-2 550-3 5 519-2 550-3 5 519-2 550-3 5 519-2 550-3 5 519-2 550-3 5 519-2 550-3 5 519-2 550-3 5 519-2 550-3 5 519-2 550-3 5 519-2 550-3 5 510-2 550-5 5 510-2 50-5 5 510-2 50-5 5 510-2 50-5 5 510-2 50-5 5 TURN CAMBER O E DEGRC DEGREE S 32 40. /7 55.90 74 40.04 52 53.88 03 37.28 50.69 55-90 53-88 30.94 29.80 31.41 33.12 750.1 648.5 614.5 500.9 579.9 7.61 9.11 12.46 13.98 15.32 DEGREE DIA-1 DIA-2 IN IN FI 20.000 21.960 21.960 22.932 23.511 25.902 25.611 25.902 25.612 25.902 27.602 6 29.901 29.902 29.001 29.902 6 29.001 29.902 6 52 3 7 7 9

KC/A-1 LBM/SEC SOFT 29 53 MCOH-1 MCOR-1 TO/TO PO/PO EFF-AD EFF-P INLET INLET INLET INLET TOLE LUM/SEC 10030 1.247 03.28 03.09

TABLE 8.3

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Blade-Element and Overall Performance with Uniform Inlet

70% of Design Speed

ROTOR

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-70/73 - 70/79 - 255-40 - 259 - 7 INLET INLET INLET INLET 1.1011 1.3450 - 87.46 - 87.98

STATOR

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*	NI	1 NI	T/SEC	CT/SEC	T/SEC	T/SEC	T/SEC F	T/SEC 0	FGREE D	EGREE D	FGREE D	CREE	-	_			-	r/SEC
	20,405	1 21.489	F15.2	715.0	622,55	714.0	526,3	-38,1	40,21	-3,05	14.85	47.01	0		c	C	_	727.9
	21.006	1 21.961	775,8	679.2	597.9	678.1	104.4	-37.3	39.58	- 3, 15	19.98	49.05	5		¥.	m		743.9
	21.565	1 22.432	735.3	653.6	574.1	6.52.6	1251	-36.3	3A.65	-3.19	25.33	50.65	•	-	c	÷.		130.4
8	23.314	23.314 23.902 672.6 6ud.1	672.6	610.1	543.3	607.1	306.5	11.92 4.45-	36.11	-3.24	1 -3.24 35.86	54.27	671.2	1039.9	193.3	-844.0	780.8	609.7
	106-52-	100.62	523-2	1.52	1.525	1.105	1041	0.00			10.51	12.10	İ۵.	~	€.	÷	L.	
	27.815	1 27.902	607.2	534.7	522.0	533.4	310.1	-37.1	30.71	-3.97	50.45	61.50	0	-	m	n	-	945,2
	29.406	1 29.362	602.0	506.0	511.4	505.9	317.5	-11.8	31,85	-1.33	53.00	63.33	*	-	÷	-		6.966
	29.914	29.856	594.5	482.4	496.5	485.4	326.5	1.1	33, 37	.16	54.12	64.33	-		*	o		4.1101
	30.302	50-293	582.7	456.8	480.0	456.8	330.5	3 . 1	34.55	.39	55.51	65.94		-	•	-		026.2
			:							1								
					CHARGER	C-ROJMO		MECK-B-	1000	1012	1204		1					
NAIS	DEGREE	DEGREE	DEGREE	DEGREF	UEGREE S	SHOCK		~		POFILE	•		v	TATIC				
	-5.61	-5.67 -2.75 9.36 4	9.36	43.27	55,9n	00001	.2913	.1096	.0272	.0272	.9675	.0001	0000.	.6078	.7157	.6295	.5676	9124.
2	-5.72	1 -2.78	A.29	5L 47	53.87	.000.	.2961	.1088		.0277	-		0000	.6553	.6755	.5973	.5631	6606.
	-5° 0£	1 -2.94	7.82	41.84	52.49	0000	.2845	.0748		.0195			0000.	.7331	.6452	.5745	.5660	640 6 .
	-4-	1 -1.42	0.00	30.45	50.68	0000	ATTC.	168		5010.			. 0000	BED9	5007	0113	EAGE.	00100

4779 4779 1089 1959 1959 1957 4677 4677 4677 53300 5534 5524 5524 8414 8414 7973 0000 9938 9966 9966 0103 0103 0070 0070 0117 0117 0214 0214 0295 0395 -6.43 -3.42 7.99 9.4.5 50.68 0000 2738 .0368 -7.60 -4.53 8.61 36.50 49.60 .0000 .2799 .0353 -8.89 -5.65 9.51 34.68 49.89 0000 .3567 .0353 -7.48 -4.17 14.58 33.17 52.00 .0000 .3569 .0519 -6.07 -2.75 17.56 33.20 53.54 .0000 .3782 .0799 -6.17 20.03 34.16 56.01 .0000 .4190 .1095 88888

MC/A-1-LBH/SEC SOFT 28.37 /

TABLE 8.4

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Blade-Element and Overall Performance with Uniform Inlet

70% of Design Speed

U-2 669.5 712.6 864.3 950.6 950.6 1015.7	137.3	24	4749				5756	6707	,6720	.67 4 8
U-1 59155 59155 659-3 755-4 755-4 755-4 755-4 755-4 755-4 755-4 755-4 755-4 7 755-4 7 755-4 7 755-4 7 755-4 7 7 755-7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	•••	•	-	•	-		-	0160	-	
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10000000000000000000000000000000000000	0.0		.3300	5955.	ロオオウ・	0000.	. 3589	.545.	.3386	.3356
74959 774959 774959 774959 774959 774959 774959 774959	783.5-	шH	-					7183		
V * -1 1/2555 694+3 727+4 727+4 755+0 855+2 855+0 10555+0 10555+0 10555+0	1142.6	FE-AD	1.0061	0066.	9118	. 4200	.8867	7522	. 7098	.6700
B - 2 12.78 12.78 12.78 12.78 255.52 255.73 40.0 255.73 255.73 255.73 255.73 255.73 255.73 255.73 255.73 255.73 255.73 255.73 255.73 255.75 255.7	62.26 05.04	LEFF-PE	1.0057	.9905	.9732	. 7230	-8914	.7020	.7209	. 0822
BL B8L 58.45 59.45 60.14 65.65 65.65		P02/	-	_	-	-		7 -		_
DE 00 4 0 4 0 4 0 4 0 4 0 4 0 4 0	45.92	LOSS-P	0025	0030	.0078	.0167	0110.	0284	0.518	.0331
B-1 66666	88	LOSS-P	0025	.0030	.0078	.0109	•0176	-0102 -0102	0110	0320
170-2 550-7 550-7 550-7 450-7 460-7 351-4	348.3	OMEGA-B	0117	.0136	•0326	.0805	-0892	1640.	1958	.2211
ET / SE - 1		D-FAC	+114.	.4317	6074.	.4577	.4273	1965.	1954.	4359
EI < C	350.0	홍권				_		00000		
VM-1 563-5 374-5 374-5 378-5 378-5 392-6 5 392-6 5 392-2 5 392-2 5 392-2 5 392-2 5 392-2 5 392-2 5 372-5 372-5 372-5 372-5 372-5 372-5 372-5 372-5 372-5 372-5 372-5 372-5 372-5 372-5 372-5 372-5 372-5 372-5 372-5 377-5 372-5 3	373.7	CANDER DEBREE		_		_	_			
5000 000 000 000 000 000 000 000 000 00	50 0 0 50 0 50 0	TUPN DE®REE	45.65	40. 29						6.36
100 100 100 100 100 100 100 100 100 100	373	DEGREE	10.91	9.38						6 0
01A-2 19-769 7 20-469 7 21-564 7 22-5564 25-550 1 25-5500 25-5500 25-5500 25-5500 25-5500 25-5500 25-5500 25-5500 25-5500 25-55000 25-55000 25-55000 25-55000 25-550000000000	31.27	INCS INCH DEV T	1 0 °	5 9.67			_		8	9 8.16
1014-1 17.467 19.467 19.467 19.467 25.731 25.731 26.536	32.49	INCS DEGREE	3.0	1	9.0 9		0	90°2	7.01	7.1
¥ S S S S S S S S S S S S S S S S S S S		2			15	3	86	5 8	8	8

T0/T0 P0/P0 EFF-AD EFF-P IME1 IMET INLET INLET * * * 1.1070 1.3057 07.11 07.66

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DIA-1

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ЧЧ Ч	727	743	759.1	609	876.	944	995.	1011.	1025.	t x			.878.		Ĭ.	. 911	18 1 6.	.9507	.9520	953	
1-1-1	691.2	711.5	731.1	789.6	867.0	942.1	995.9	1013.1	1028.9	71.¥		5416	5427	1440	.5641	.6226	.6877	.7005	.7000	.7003	
V01=2	760.6	-776-0	1.164-	+ 909-	-904-5		004	1005.3	1020.0	ĩ		1693.	.5579	5357	4962		5954.	.4135	796S.	.3755	
V04-1 V	·		•	•	-		i —			ĩ		7001	.6650	.6362	.5762	.5342	5247	.5206	.5120	.5006	
VI-2	.0	¢	~	a	¢	2	6	æ.	40	56-P	LATIC	.6689	.6884	.7226	.8739	.9226	.8710	.6292	.8100	7989	
1 - 1 - 1 1 - 2 - 1 1 - 2 - 1 1 - 2 - 1 1 - 2 1 1 1 2	ie.	æ	~	٠	2	a	0	o	2	L-AD	DTAL S	0000	0000.	.0000	.0000	.0000	.0000	.0000	.0000	.0000	
B1=2 5855 5	48.54	50.63	52.28	55.92	59.89	62.53	64.09	65.39	66.80									•0000			
81-1 F e rff D	14.87	20.06	25.31	36-32	45.86	50.74	53.15	54.50	56.05	P02/	F 109	.9672	.9674	.9759	6166 .	.9961	.9937	1686.	.9867	.9852	
B-2 Ferf D	-2.80	-2.90	-2.94	-2.97	-3.01	-2.63	9 5•	.72		Loss-P	ROFILE	.0286	.0315	.0260	.0112	.0065	.0122	.0227	, 0283	.0340	
8-1 Ferf D	16.14	41.07	40.15	38.75	36,25	34.03	36.22	37.44	38,55	Loss-P -	OTAL PI	.0286	.0315	0020.	.0112	.0068	.0122	.0227	.0288	.0340	
V0-2 T/SEC D	xi									MEPA-B	F	.1151	.1234	1660.	0017.	.0223	10367	.0648	.0811	2460.	
V0-1 1/SFC F	533.4	501.4	468.4	411.8	360.2	335.0	352.9	357.8	359.2	D-FAC O	-	.3299	.3395	.3335	.3224	.3320	.3562	.3984	.4305	.4627	
VH-2 T/SFC F	-		_		-	_				MEGA-B	H ^O CK	•0000	0000.	00000	00000	0000.	.0000	0000.	.0000	.0000	
	594.3	575.3	555.1	513.0	491.3	496.1	482.0	407.4	450.B	AMBEP C	EGREE S	55.90	53.87	52.50	50.68	49.60	49.90	52.01	53.54	50.01	
7-2 7/SEC F	672.7	637.6	612.6	568.3	525.1	504.0	481.1	460.4	437.3	TURN C	EGREE D	11.74	43°01	43.69	41.72	39.26	36.66	49 35.63	36.72	37.77	
FT/SEC FT	798.5	763.1	726.3	637.9	609•2	598.6	597.4	588.6	576.4		EGREE D	9.61	8,55	8.07	6.2 5	9.03	10.65	16.49	18.12	20.46	
1 DIA-2 F	21.489	21.961	22.432	23•9 ₀ 2	25-893	27-902	29.382	29.856	30.243	INCH	DEGREED	-1.12	-1.36	-1.32	n		-2,32	+ · · ·	1.28	2.21	
DIA-1	20.409	21-008	21.589	23-314	25.601	27.618	29.408	29.914	30.382 30.243	INCS	DEGREE D	#0°#	-4,29		-3,73		-5,55	-3,18	-2.05	-1.16	
1	20									,	Zì							8	_		

NCOR-1 WCOY-1 TO/TO PO/PO EFF-AD EFF-P WC/A-1 INLET INLET INLET INLET INLET INLET INLET INLET RPH LEWYSEC 7762 121.51 1.1070 1.3503 83.79 84.47 27.31

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ROTOR

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TABLE5Blade-Element and Overall Performance with Uniform Inlet

70% of Design Speed

ROTOR

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ĩ	2 CAL					964						8H								649.	629		6376
5	- Jack	201								1100.4			•	ASCA.					2000		1.0097	1.0275	1.0440
201	1-235/1	-115.1	170.1			485.6						и-2		0593.							.4521		4237
1-107	- Jaski	-591.5	3.55.6-			-873.4		1050.8	1070.7	1100.4		K-1		3150					0100	D D D D D	. 3245	3211	5163
2-17	- Jack	519.4	524.1	527.0		629.9		730.1-		743.5		EFF-D		0000	10101	9740	2017		10101		.6867	.6555	.6311
	+ Daski	686.3	719.5	752.3	24.7.4	951.5	0-8401	1118.7	1136.5	1155.4		FF-AD	ST ST ST ST ST ST ST ST ST ST ST ST ST S	1.0146	1.0049	9446					.7270	1500.	•6635
82	ROPER-P	12.81	10.96	25.20	30.05	50.42	10.00	60.40	62.66	65.25				1.0138	1.0046	9856	6050			0010	-7384	.7057.	.6770
B'-1	COREE 1	59,52	60.37	61.20	63.63	66.63	40°00-	71.33	71.61	72.28		P02/		1.4910	1.4688	1.4411	1.01		10001	DBCCH	1.3534	1040-1	1.3373
B-2	PORET C	47,59	46.44	45.71	45.34	43,36	00 1	46.58	48.70	50,96		LOSS-P	ROFILE	0057	0019	.0042	0185	H C C C		12200	0330	.0362	0365
₿-1	- HILL	5	00	00.	00.	0	5	00.	00.	8		LOSS-P		0057	0019	.0042	.0145	1000		22201	0159	.03A3	.0387
2-07	-1/SEC-	554 4	520.9	488.5	432.6	378.6	-2-0-0-0	380.9	384.2	343.8		MECA-R		0266	0087	.0195	-000-	1044		I/TI ·	.2011	.2265	*3#2*
1-07		ć,	٢,	с.		C •	E	<u>د</u>	۲. •			U-FAC (7154°	4464	.4612	4880	45.97			.4680	1224	.4787
2- <u>7</u> 7	1-225/1-	506.4	495.1	476.4	427.3	400.8	5	360.5	337.6	311.2		OMEGA-B	SHOCK	.0000	.0000	.0000	0000		0100	0000	.0119	.0125	44[J.
VM-1	LANSEC	34.8 .1	355.7	362.4	374.5	377.4	0.010	359.1	354.8	351 . 8		CAMBEP (PERFE	47.12	39.99	34.03	24.16	04 11		0 T • 2	8,03	7.64	7.45
<-2 -2		750.9	718.6	682.3	508.0	551.4	1.936	524.5	511.5	1,494,1		TURN	L'HANNY	46.72	41,39	36.01	24.79	16.21			10.92	9,]4	7.02
		348,1	1.000	362.4	374.5	377.4	1.010	358.1	10 " # S D	351.8		CEV		10.93	9.35	8.62	9.11	8.18			6.30	4.55	9,30
DIA-2		19,769	20.409	21.047	22.964	25.520	0.0.02	29.493	30.630	31.271		INCK		10.57	10.1	10.44	9.75	9.71			4.22	9°02	8.97
DIA-1		17.467	10.467	19.467	22,314	25.791	10.02	31.295	500-10	32.499		50%	Lawin	4.14	1 * * ·	4-24	5.85	7.09			2 Å Å	5	8. 06
K CDAN		n	2	5	8	88						2 CO 1 M		ŝ	5	9	8	8	2	8	8	2 1	\$

T0/TU P0/P0 EFF-AD FFF-P <u>1465 INEF INEF TNEF</u> * 1.1128 1.3831 86.07 A6.69

		j					7.967		610			025.9			TUX.						- AUCA		8046.	
				-				789.5				1020.9		•	8.03					D0.54	07C0*			
		<0V					0.18/-				1002-1	1102.3 -633.7-1017.4	K - 0		5526		SOLC.		1001 ·		1001		3622	
		107									-618.9	-633.7	1						•				4999	
															-			-		1			.8201	
			5	-								761.5	<u> </u>		0000	0000-	0000		0000			0000	0000	
		81-2	DFORFE	20.02						65.15	66.21	67.36		5.07 M	-0000	0000-	0000		0000	0000	0000	0000	0000.	
											54.63		P02/		9649					1				
			ж						1		1.12		TURN CAMBER OWFGA-R D-FAC OMEGA-R LOSS-P LOSS-P	a lacad	0316									
			F								42.11		LOSS-P	10741	0316									4
			t								0.0		OMEGA-P		-		•		.0277	ľ		-	-	WC/A-1 LBM/SEC SGFT 26.17
×D•			1								394.2		1 D-FAC		. 36.17	Ī	•					•	Ī	EFF-P 1NLET 83,26
			L								442.0		OMFGA-F	SINCK	Ĩ		·		0000			•	·	EFF-AD EF <u>Intet in</u> % 82.51 83
1000		1	r								436.1		CAMBER	- SOLO	55.9				14,64					P0/P0 EF INLET IN 1.3654 8
		4-2 2	È	¢	ð	ŝ	ND.	4	ľ	4	3	t	TURN		Ŧ	÷	4	Ŧ	42.00	Ŧ	ň	ž	Ŧ	6
-			1-1-SEC			2 717.2			ł			578.4	DEV	DEGREE	9.79	_		5 8.43					20°84	
		DIA-2		20.409 21.489		9 22.432						2 30.293	INCM	DEAKE DEAKE DEAKE	30° . 0£	7 		1.76	1.66	Б. 	4.73		6.74	NCOR-1 WCOR-1 T0/T0 <u>INLET INLET INLET</u> RPM LBM/SEC 7741. 116.47 1.112
	OR	DIA-1	H	20.40	21,008	21.589	23.314	25.601	219-72	29.408	29,914	30.362	INCS	LI MIL	-2.85	-9.6-	-2.75	-1.23	-1.47		1.42	8.25	3.38	Žŧ « r
	STATOR	K CBAL		ŝ	õ	5	8	8	2	8	88	ŝ			ŝ	2	5	8	8	2	8	8	\$	

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TABLE 8.6

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Blade-Element and Overall Performance with Uniform Inlet 70% of Design Speed

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	17.467]	1		- /SEC -	- 1/26/	- 735C -		1/SEC 0	EGRFE D		ECREE D		T/SEC F	u.	•		T/SEC FT	250
_		9.709	331.9	744.4	331.9	438.0	۲.	542.1	00.		60.71	12.44	679.5	œ		-177.6	591.7	669.7
	18.467 2	0.408	339.2	712.9	339.2	475.9	c	530.5	00		61.53	18,66	711.6	œ	5	-150.7	625.6	691.3
	19,467 2	740.25	345.5	677.9	345.5	457.9	c	500.0	00.		62.35	24.94	744.5	1	10	-213.0	659.5	713.0
	22.314 2	2.364	356.9	605.2	356.9	411.3	Ċ.	443.9	00.		64.72	38.99	835.9	530.6	-755.9 -	0.456-	755.9	9.777
_	2 191 2	5.520	359.6	553.1	338.6	10500	 	397.0	60.		67.68	50.48	944.5	Ь	έ.	-457.5	875.7	864.5
	23.954 2	28.076	350.3	534.2	35°.3	370.6	ſ.	394.5	00		70.34	56.80	1041.5	-	α	-556.6	980.8	951,1
	31.295 2	545.64	339.0	529.1	339.0	332.5	c	411.6	0.		72.27	61.18	1113.0	å	-	t. 119-	1067.1]	016.0
_	31,883 3	0.630	335.9	525.7	335.9	322	,	415.2	00		72.72	62,62	1.1511	å	-	-622.	1080.1 1	637,6
	32,499 3	11.271	333 n	511.5	333.0	300.2	.c.	414.2	5	54.07	73.17	65,05	1150.2	÷.	•	-645.1	1101.9 1	059,3
K SPAN	ines	INC 4	DEV	<u>1084 C</u>	LANDER C		7-74-1	M-GM-H	LOSC-P	1055=P	P027	EFE-2 F	FF-AD	<u> </u>	<u>4</u> -1	4-2	1-44	<u> </u>
	DEGREE DEGREE DEGREE	GREE D		DEGREE J	DEGREE -	A DOK	•	•	σ.	ROFILE		OTAL T	0	TATIC				
	5.3E	11.75	10.56	48.27	47.12	. NU70	.4566	0143	7031	0031	1.4949	1.0068	1.0072	1.0169	.3014	. 5562	.6180	.4406
	5.57	11,90	9.03	42,89	39.99	0000.	.4736	,0060	-	2100.	-	,9956		.9918	.3087	. 5271	.6538	セクセキ。
	5.89	11,56	8.34	37.41	34.03	e-00.	.488 5	.1330		.0072	•-4	1779.		.9585	.3145	595 2	.6964	0999.
	6,95	10.84	7. 25	25,73	24.14	.000 ·	.5104	1447		.0198	-	1116.		.8790	.3236	.5285	.7701	5197*
	910	-04-04	52.6	02 41	66.91	0000	4961	5611.	L.	0232	н	.8705	1	5158.	1426.	4082	.8430	• 524B
	8.88	10.67	5.35	13.54	61.6	0000	.472ª	.1562	-	.0299	-	.5108		.7641	.3162	.4622	.9463	.5859
	ð.92	10.17	7.09	11,08	8.13	Selc.	.511?	-325		.0381	4	1614.		.6503	.3069	. 4541	1.0733	.5970
	8,89	9,97	7.51	10.10	7.54	0149	.513°	, 2485		.0396	-	.7004		.6409	,303a	.4502	1.0209	.6003
	d.95	9.97	ю. С	8,13	7.44	0159	.5139	2043	_	5050.		.6783		.6223	.3011	1754.	1.0378	.6040

* * 1.1185 1.3970 84.54 95.25

STATOR

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		112-7			VH-HV	CTH/A	1-07	C= 11	н-1	H=5	HV-1	C= 4 E		5-10		6- + UA		C -1
N SPAN	IN		11/25/12	TT VOEL	TICEP E	1		C 1401 F	VEGOCE S	10000	10000	JEGOCE E	1,000,1	1,057 5			TICED E	1221
	-	24	2775	1 200	, , , ,	2010	1/2/1	1 110/1										1001
	20.409	21.439	773.7	6.4.3	549.7	504.2	544.4	-24.0	44.72	-2.56	14.97	51.37	569.0	967.8	-145.0	-756.0	691.4	726.0
	21.008	21.961	742.2	575.3	533.9	574.6	515.5	-27.9	43°99	-2.78	20.17	53.33	559.3	962.3	-196.1	-771.9	711.7	744.0
	21,589	22.432	708.2	551.0	513.9	550.3	487.3	-25.8	43,47	-2.79	25.40	55.03	569.5	960.2	-244.1	~786.8	731.3	759,9
8	23.314	23.402	639.1	503.3	466.1	503.4	437.2	-23.8	43.16	-2.71	37.05	58.87	765.1	973.9	-352.6	-833.5	789.8	809.7
	-25,601	268.54	592.8	0.044	2.172	5.922	6.565	-20.9	16.14	-2-50	46.86	62.89	545.8	1004.8	4.174-	-808-n	867.3	877.2
	27,818	27,902	53" 1	443.9	435.7	443.5	399.0	-16.7	41.76	-2.15	51.78	65,25	704.3	1059.2	-553.3	-951.9	4.540	945.2
	29,409	29.382	591.6	431.6	415.3	431.4	420.9	12.4	45,34	1.55	54.15	66 . 30	6°601	1073.5	-575.4	-982.9	996.2	995 J
	29,914	29,456	592.2	42.4.4	411.3	424.1	426.1	14,5	46.02	96"	55.00	66.95	717.0	1083.4	-587.3	-996.9	1013.4	1011.4
	30,382 30,293	30.293	585.1	411.5	+00+	410.1	1.26.4	33. A	46,81	4.72	56.40	67.55	723.5	1073.8	-602.6	-992.4	1029.2	1026.2
		,	1		,	I				,								
		TNCS INCH DEV			LARGER	B-VS-N	0-240	HEOU-B	1050-		1204				I-M	2-0	1-14	2-15
X SPAN	DEGREE	DEGREE DEGREE	DEGREE D	DEGAEE D	JEGREE 5	SHOCK			rotal F	PROFILE	L LOG	TOTAL 1	OTAL S	TATIC				
ŝ	-1.33	1.60	9.75	47,39	55.90	.000.	.797a	,1246	.0309	6U£0.	.9665	.0000	0000.	.7282	Ţ	.5257	.5008	.8411
₽	-1.28		8.67	46.77	53.97	00000	,408°	.1300	.0331	.0331	,9674	.0000	.0000	.7408	•	.4997	.5120	.0358
15	96		9.22	46.27	52.51	0,00.	.4086	.1113	.0291	.0291	5476.	.0000	.0000	601F.	•	4791	.5n17	8333
8:	÷2.	3.74	8.51	45,87	50.57	0000	.4117	.0581	•°163	.0163	.9889	.0000	0000	.8651	.5579	4364	.5141	.8433
81		50.0	22.44	44.51	14.64	<u>1000</u>	CBC+	1160.	9610.	95IU.	3166.	0000	• 0000	1028.	1	1465.	.5540	0119.
2	2.02	5,25	11.33	43.91	1e*6†	0000	.4702	.0547	.12I4	.0214	,9896	.0000	.0000	.87n2	-	.3815	.6118	.9105
g :	5.88	9.19	17.55	43.70	52.12	.ncjn.	.5119	.1087	.0380	.0380	.9823	.0000	0000.	.7961.	-	. 3679	.6119	.915N
8	64 . 45	9.78	19.35	44.05	53.55	. nu Jr	.5306	.1265	6440.	.0449	9794	.0000	0000	.7685	•	.3609	.6173	4126.
8	1.12	10.45	24.45	42.17	56.71	0000	.5391	1351.	. 1495	.0495	.9736	.0000	0000.	.7577	-	3494	.6711	.9115

MC/A=1 L9M/SEC 50FT 24.99 VEOR-1 *CON-1 TD/TO PD/PD EFF-AD FFF-P INLET INLET INLET INLET INLET RPM LBM/SEC X 7764 111.19 1,1186 1,3753 80,39 81,25 /

Blade-Element and Overall Performance with Uniform Inlet 90% of Design Speed

ROTOR

-1 B'-2 V'-1 V'-2 V0'-1 V0'-2 U-1 U-2 (EE DEGREE FT/SEC FT/SEC FT/SEC FT/SEC FT/SEC -75 I4.87 971.0 725.0 -760.3 -187.1 760.3 BBU-3 1.42 26.70 1017.2 687.6 -047.4 -309.1 847.4 916.2 .78 39.3 1135.8 885.9 -971.3 -488.6 971.9 996.6 .78 37.3 1135.8 885.9 -1127.7 566.5 1122.7 148.6 .78 37.3 1135.8 885.9 -1127.7 566.5 1122.7 148.6 .78 37.9 11374.5 885.9 -1127.7 566.5 1122.7 148.6 .78 37.0 1177.6 57.6 -971.3 -488.6 971.9 1100.9 .78 36.70 1017.2 687.6 -971.3 -488.6 971.9 1280.5 .78 36.70 1017.2 687.6 -971.3 -488.5 971.9 1280.5 .78 36.70 1017.2 100.9 -923.9 1280.3 1222.7 .00 55.24 1394.2 1072.9 -1250.3 -923.9 1280.5 1232.5 .01 56.70 1017.6 1075.1 -1552.7 -957.0 1350.5 1232.5 .00 60.83 1077.0 1076.3 -1397.8 -939.7 1361.8 .00 60.83 1077.0 1076.3 -1397.8 -957.0 181.0 7 1361.8 .00 60.83 1072.0 -1414.7 -967.0 181.0 7 1361.8 ×--* .8565 .9020 .9020 1.0514 1.1766 1.2355 1.35778 1.35778 1.3590 71 1 Ň 5078 5078 5193 5431 5555 5555 5555 5272 ī
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TO/TO PO/PO EFF-AD EFF-P

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Blade-Element and Overall Performance with Uniform Inlet

90% of Design Speed

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	1-17	T/SEC F	923.5	0.440		1007.0	1127.8	1265.9	TRA F			1.470.41	1518.0		DEF-AD	POTAL S		1.01774	7796.	9585	0010	1000		.0090	.8221	7705	0.00	377/8	
	5-1 H	EGREE F	14.70	50 81		21.00	40.10	0,04				61.13	64,36			INTO?		1.01/0	9479	9	0.45			e113	.8342	7040	0014		
		EGREÊ D	55.47			57.12	59.52	63.55		++•	91.05	68.26	60.83		P02/		ł	-1		••	•••	-	-	-	-	•••	7470°T		
		EGREE C	uh.n2		0 = 0 = 0	45.38	43.25			19.00	0.04	41,95	45.60		1.055-P		KOF LLF	0074	1000		2110.	-016.	.00.5	. 0075	1010	>>+>	0410.	-010°	
5		EGREE C								i	00.				0-320 I		TOTAL	- 6074	1000	4000.	0110.		.010.	.0183	0.01		- 0202	0.324	
1	0-07	FT/SEC	. 87. i		044.1	606.9	527.5			439.0	8.454	442.0	448.1		0-0200			0346	0000	****	# TOO .	/ 600.	.0836	- 0964	0.90		69CI.	.2024	
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		1-2-1		0.020	536.5	SAR.			583.5	576.2	559.3			1.0*0		DEV	NFGREE		72.21	10.88	10.81	10.37	6.70			5.13	5.98	8.46	
		DIA-2	NT NT	19.769	7 20.408			-077	25.520	28.076	29.903		020.02	51.271		INCH	DEGREF		00	6.69	6.44	5.61	5.60		00.0	5,58	5.51	5.52	
		1-VI0		17.467	18.467			-10-22	25.791	25.956	11.295.29		01.800	32.499		INCS	NF GOFF		10.		53.	1.62	0.0		2.1.2	10.4	4.41 5.51 5.98	4.60	
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TO/TO PO/PO EFF-AD EFF-P INLET INLET INLET INLET

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Blade-Element and Overall Performance with Uniform Inle 90% of Design Speed

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 5 55.24 750.2 1233.9 -341.4 -1013.7 930.8 976.5
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TABLE 9.4

Blade-Element and Overall Performance with Uniform Inlet

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	E GREE	36:95	57.79	58.60	61.01	64.07	66+92	60°69	69.63	70.16	P02/	I. B467	1.8555	1.8050	1.7077	1.7085	1.7006	1:7145	1.7062	1.6808
	EGREE C	10.01	47.51	46.59	47.00	45.66	44.91	10.93	48.83	52.40	LOSS-P ROFILE	0087	0076	0030	9600.	.0113	.0120	1810	.0224	.0247
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1	FT/SEC FT/SEC FT	1001	506.6	517.4	538.4	545.8	537.1	220-0	515.5	510.5	DEBEE	12.36	10.67	10.24	11.32	7-10	5++3	2.00	6.15	8.82
0-110		19.769	20++08	21-047	22.964	25.520	28.076	20.993	30.630	31.271	E GREE C	7.99	8.17	7.91	7.11	7.13	7.28	96.9	6.88	6.86
1-110		194-11	18-467	19-467	22.314	25.791	28-954	21.245	31-863	32.499	DEGHEE DEGREE DEGREE DE	1.56	1.79	2.07	3.14	6***	5.44	14.5	5.78	đ, 5
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Blade-Element and Ovorall Performance with Uniform Inlet

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90% of Design Speed

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TO/TO PO/PO EFF-AD EFF-P

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c196 1.0898 1.1346 1.1462 1.1525 1-0052 1-0404 6253 6555 6566 7566 7655 7860 7860 6930 6732 6602 6661 6629 F-AD E. AIA. SIALIC AIA. SIALIC 0000 7024 8 1 0000 7024 8 1 0000 8977 000 0000 8977 0000 9917 0000 9917 0000 9917 0000 1000 979 0000 177 P01 1014 1014 • 9335 • 0008 • 0008 • 9445 • 0008 • 0008 • 9455 • 0008 • 000 • 9856 • 0008 • 000 • 9738 • 0008 • 000 • 9738 • 0008 • 0008 • 9738 • 0008 • 0008 .0167 .0167 .0167 .0169 .0169 .0158 -1013 -1178 -1305 #C/A-1 - <u>L BM/SEC</u> 34.65 + 536 + 536 + 794 - 508 - 508 - 508 - 568 NCOR-1 WCOH-1 TO/TO PO/PO EFF-AD EFF-P IN.ET 14.ET 14.ET 14.ET 14.ET 14.ET RPH LBH/SEC 8 9981 154.20 1.1996 1.7012 82.04 85.34 6 25.88 000 92 52.43 000 12 49.59 000 12 49.59 000 12 49.59 000 12 96 000 12 96 000 12 56.01 000 12 56.01 000 12 56.01 000 12 56.01 000 12 56.01 000 12 56.01 000 12 56.01 000 12 56.01 000 12 56.01 000 12 56.01 000 12 56.01 000 12 56.01 000 12 56.01 000 12 56.00 12 8.05 9.68 12.51 17.79 17.79 19.32 21.57 4 9 9 9 6 9 6 9 6 9 6 **~ 12 12 13 13 13 13 14**

Blade-Element and Overall Performance with Uniform Inlet

90% of Design Speed

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STATOR

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 U-2

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C/A-1 LB/5EC 50FT 33.65 EFF-P 81.59 I WCOH-I 10/TC PO/PO EFF-AD INLET I::LET INLET INLET LBW/SEC X 149.74 1.2071 1.7123 80.14 NCOR-1

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ROTOR

TABLE 10.1

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Blade-Element and Ovcrall Performance with Uniform Inlet

ROTOR

100% of Design Speed

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V02 77/966 77 -226.7 -226.7 -322.6 -322.7 -322.6 -322.7 -10.0	N 1400 1000 1000 1000 1000 1000 1000 100
	4-1 5575 5275 62857 62857 62857 5655 5655 5655 5655 5655 5655 5655 5
7385-77855555555555555555555555555555555	EFF-P STATIC 8551 8551 8551 8573 8593 8593 8593 8593 8593 8593 8593 859
11/261	101AL 5 8776 8776 8776 8776 8619 8619 8619 8619 8619 8619 8619 861
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	E64-B D-FAC (000 000 000 000 000 000 000 0
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2 4	

TOTTO PU/PO EFF-AD EFF-P

STATOR

TABLE 10.2

1. 1.

Blade-Element and Overall Performance with Uniform Inlet

100% of Design Speed

ROTOR

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1.155C F] 🖬	*	9	2	9	-	a	40	ŝ			.0	1116.						1			
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B-2 FGREF 7	48.14	46.82	14.85	41.55	39.65	18-06	38.63	42.07	46.90			ROFILE	.0296	0273	.0205	0600.	.0054	0012	-0035	7000		T#10*
B-1 EGREE L	00	00.	00.	00.	00.	.00.	00.	00-	0			OTAL P	.0296	0303	• 02##	.0176	.0213	.0215	.0264	.0324		· · · · ·
v0-2	7-2-3	705.4	656.9	582.2	531.5	457.3	0.444	452 c 8	459.8		E GA - B	٠	.1399	.1432	.1159	.0839	.1038	1171	.1511	2006	2404	7. 17.
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VM-2 TZSEC F	683.9	661.8	660.2	656.9	637.2	584.1	556.6	502.3	5°0°5	0		HOCK	• 0000	.0141	.0188	0409	.0768	1097	.1321	.1394	1008	
VV-1	601.1	616.5	631.2	666.1	685.5	623.4	648.1	640.9	635.3			EGREE S	47.12	39.99	34 93	24.20	14.66	9.12	8.32	7.66	7.47	
V-2 FI/SEC F	1024.9	967.3	931.3	877.8	82°. /	20.08	712.5	676.5	623.8	T. 101		EGREE D	38.79	32,32	27.48	19.50	13.42	7.28	5.76	オオ・ワ		-
1-1 1/2EC	601.1	616.5	631.2	666.1	685.5	673.4	548.1	6.0+9	635.3	7.54	5	FGREE D	2 5.61 13.92 3	13.46	12.19	9.11	5.52	6.53	6 •96	8.91	11.94	
01A-2	19.769	20.405	21.047	22.964	25.520	20-076	29.993	30.630	51.271	1071		EGREE D	5.61	5.78	5° 25	04.4	4.30	4.70	4.70	4.69	4.70	•
DIA-1 DIA-2 V-1 V IN IN FIVECFIV	17.467	16.467	19.467	22.314	25.791	20.954	31.295	31.883	52.499	THE		DEALED	82	63		04.	1.65	16.3	5.47	3.63	3.80	•
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10/TO PO/PO EFF-AD EFF-P INET INLET INLET 1.2106 1.7843 85.37 86.50

STA'FOR

TYSEC TYSEC <th< th=""><th>REF DEGREF FT/SEC FT/SE</th></th<>	REF DEGREF FT/SEC FT/SE
7.17 49.43 341.6 1378.3 -246.3 1004.2 441.4 3.01 55.90 849.4 1399.9 -331.6-1079.5 1044.7 3.51 947.4 1307.5 -709.4 131.6 144.6 5.88 55.17 947.4 1307.5 -709.4 1204.6 5.88 55.17 947.4 1307.5 -709.4 1204.6 5.84 57.96 1034.4 1507.5 -709.4 1204.6 5.84 57.96 1241.0 156.5 -969.4 137.7 5.96 51.01.4 1591.5 -969.4 137.7 6.90 55.96 1201.4 1591.8 -963.6 1470.4 6.90 57.97 1201.4 1591.8 -963.6 1470.4 6.90 57.94 1201.4 1591.8 -963.6 1470.4 6.90 57.94 1201.4 1591.8 -963.6 1497.7 6.90 57.94 57.94 790.4 790.4 90.1 1000 7000 790.4 790.4 90.1 1000 7000 790.7 990.7 90.1 1000 7000 790.7 990.7 90.1 <t< th=""><th>7.17 49.34 34.0 1378.3 -246.31079.2 40.4 3.01 50.90 340.4 1309.9 -314.04.2 40.4 5.68 55.17 947.4 1807.5 -709.412976.4 1204 3.3.5 5.96 1034.4 1507.5 -709.412976.4 1204 3.3.5 96 53.1 141.0 156.5 -304.7 1197.6 136.5 0.48 65.33 1194.0 156.5 -304.7 1197.6 1376.5 0.48 65.33 1194.0 156.5 -304.7 1197.6 1375.5 0.49 65.7 91 1189.5 1591.0 -997.1 1476.6 1470.4 0.1 7014. 7114.5 1591.0 -997.1 1475.6 1470.4 0.1 7014. 7000 -0000 -7764. 3419.7 7504.4 0.1 7014. 7000 -0000 -7764. 3972.7504.7504.7000 0.000 -0000 -7764.7704.7007 -0000 0.000 -0000 -7765.752.5714.1.0.24 0.000 -0000 -7075.706.25714.10.700 0.000 -0000 -7075.7060 -5714.10.24 0.000 -0000 -7075.7064.4907</th></t<>	7.17 49.34 34.0 1378.3 -246.31079.2 40.4 3.01 50.90 340.4 1309.9 -314.04.2 40.4 5.68 55.17 947.4 1807.5 -709.412976.4 1204 3.3.5 5.96 1034.4 1507.5 -709.412976.4 1204 3.3.5 96 53.1 141.0 156.5 -304.7 1197.6 136.5 0.48 65.33 1194.0 156.5 -304.7 1197.6 1376.5 0.48 65.33 1194.0 156.5 -304.7 1197.6 1375.5 0.49 65.7 91 1189.5 1591.0 -997.1 1476.6 1470.4 0.1 7014. 7114.5 1591.0 -997.1 1475.6 1470.4 0.1 7014. 7000 -0000 -7764. 3419.7 7504.4 0.1 7014. 7000 -0000 -7764. 3972.7504.7504.7000 0.000 -0000 -7764.7704.7007 -0000 0.000 -0000 -7765.752.5714.1.0.24 0.000 -0000 -7075.706.25714.10.700 0.000 -0000 -7075.7060 -5714.10.24 0.000 -0000 -7075.7064.4907
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7596 .0000 .0000 .7072 .6800 .4960 1.0070	3596 .0000 .0000 .7072 .6800 . 4960 1.0070)
	EFF-AD EFF-P MC/A-1 INLET INLET

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TABLE 10.3 Blade-Element and Overall Performance with Uniform Inlet

ROTOR

100% of Design Speed

FT/SEC 987.3 987.3 987.3 987.3 987.3 10.12.6 11.12.6 11.234.6 11.234.6 11.234.6 11.55.3 11.55.3 11.55.1 11.55.2 11.55.2 11.55.2 15.12.4 15.12.	A 150 100 100 100 100 100 100 100 100 100
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FYV-2 FYVEC FYVEC FYVEC 703-3 703-3 703-3 703-3 703-3 894.071079-3 894.071079-3 894.071079-3 10010-3 10010-3 1000-3 1000-3 1000-3 1000-3 1000-3 1000-3 1000-3 1000-3 1000-3 1000-3 1000-3 1000-3 100-3	FFF-P 51411C 51411C 9513 9313 9319 9371 9371 9371 9371 9371 93
7 V1 7 V'-1 1034.7 1131.6 1135.6 1135.6 1135.6 1155.6 1155.6 1155.6 1668.3 1768.3 1768.3 1768.3 1768.3 1768.3 1768.3 1769.5 1769.5 1	7014-40 9451 9451 9451 9451 9450 9453 9453 9453 9453 9559 9559 9559
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60-2 60-2 60-2 60-2 60-2 60-2 60-2 50-72 50	PROFILE PROFILE 00111 00111 0000 0000 0000 0000 0000
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TVH-1 597.1 597.1 597.1 597.1 595.5 595.5 595.5 529.7	AMBER CA AMBER CA 39,99 34,03 34,03 34,03 34,03 24,18 24,18 34,030 34,030 34,0000000000
F1/55C F1/55C 6 955-5 6 955-5 6 855-5 753-3 724-0 7 670-8	
FT/SEC FT 597-1 1 623-0 660-6 668-5 668-5 658-5	M DEV TUR P 15.12 51 P 15.12
DIA-2 IN 29-769 7 29-969 4 22-964 1 25-520 5 29-993 5 29-993 5 30-690 9 31-271	
DIA-L IN IN IV-10 17-467 2 19-467 2 19-467 2 29-591 2 21-295 2 31-295 2 31-205 2 31-295 2 31-	INCS INCS
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STATOR

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	TNR 1	INLET INLET	ET INL	ET INE 265 1.8	111 INI	INLET INLET		LUM/SEC SUFT 41 15									
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TABLE 10.4

Blade-Element and Overall Performance with Uniform Inlet

ROTOR

100% of Design Speed

STATOR

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A 25 25 25 25 25 25 25 25 25 25 25 25 25	DiA-1 DIA-2 V-1 V IN FT/SEC FT/ 20.409 IN FT/SEC FT/ 21.008 21.4851 1040.4 6 21.5569 22.432 967.8 6 21.5569 22.432 967.8 6 21.5569 22.432 966.7 6 22.5101 25.903 884.9 6 27.618 27.902 866.7 6 27.618 27.902 866.7 6 27.618 27.902 866.7 6 27.613 27.803 864.7 6 27.613 27.803 864.7 6 27.614 27.855 897.3 6 29.514 29.855 897.3 6 29.514 29.855 897.3 6 20.382 30.293 873.3 6 20.393 873 873.3 6 20.394 873 873 873 873 873 873 873 873 873 873	DIA-2 IN 21,489 21,961 21,961 23,902 25,902 25,902 25,902 25,902 25,902 25,902 25,902 25,902 25,902 25,902 25,902 25,902 20,255	FTV-1 10406 10040 100000000	F V-2 F V V V V V	TX	¥7000000000000000000000000000000000000	FT.V0-1 755 711-95 612-1 612-612-612-612-612-612-612-612-612-612-	-2 VO-1 VO-2 B-1 EC FT/SEC FT/SEC DEGREE DE 5.3 7119 -5.4 °6.26 3.3 7119 -5.4 °6.26 6.1 627.8 -11.3 45.28 6.1 627.8 -11.3 45.28 6.1 627.8 -11.3 45.28 6.1 627.8 -11.3 45.28 6.1 627.9 22.6 41.51 8.5 596.9 22.6 41.51	ростана 2000-2000 2	0.010 	Image: Second	D D D D D D D D D D D D D D	777 777 777 777 777 777 777 777 777 77	F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F74 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F77 F	 V02 1045- 1045- 1045- 1045- 1045- 1262- 1262- 1265- 1406- 140- 1406- 1	74- 77- 9876 9876 9876 9876 1016 1016 1016 1016 1016 1016 1016 10	3-1 3-2 V:-1 V'-2 V0'-1 V0'-2 V-1 V-2 366E DEGREE F1/5EC F1/5EC F1/5EC F1/5EC F1/5EC 18.13 56.02 757.2 1260.4 -235.7-1045.1 987.5 1059.7 25.19 56.29 757.2 1260.4 -235.7-1045.1 987.5 1053.4 20.5 59.89 784.9 1201.4 -368.6-1125.6 1044.6 1085.4 26.5 59.89 784.9 1201.4 -368.6-1125.6 1044.6 1085.4 36.61 61.80 796.0 1201.4 -368.6-1125.6 1044.6 1085.4 36.61 61.80 796.0 1201.5 -500.2-1125.6 1044.6 1085.4 36.61 61.80 796.0 1201.5 -500.2-1125.6 1044.6 1085.4 36.61 1065.5 15441.8 *626.0-1398.9 1422.9 1424.6 36.15 1065.5 15441.8 *626.0-1398.9 1422.9 1424.6 36.15 1065.1 0144.1 -1175.5 9 1477.0 1444.6 36.15 1045.1 1556.6 -947.1 -1175.5 9 1477.0 1444.6
Ag Ag A A 2 に 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	N DEGREE DEGREE DEGREE SHOCK 08 3:00 11:97 40:77 55:91 0000 -31 2:62 8:85 47.64 53:98 0000 -31 2:62 8:85 47.64 53:98 0000 -00 2:95 7:33 47.85 52:34 0000 2:44 6:57 11:20 44.91 49:55 0000 1:92 5:61 17:91 39:69 51:98 0000 1:92 5:61 17:91 39:69 51:98 0000 1:92 5:61 17:91 39:69 51:98 0000 1:92 5:61 17:91 39:69 51:98 0000 1:92 5:61 17:91 39:69 51:98 0000 1:92 5:61 17:91 39:69 51:98 0000 1:92 5:61 17:91 39:69 51:98 0000 1:92 5:61 17:91 39:69 51:98 0000 1:92 5:61 17:91 39:69 51:98 0000 1:92 5:61 17:91 39:69 51:98 0000 1:92 5:61 17:91 39:69 51:98 0000 1:92 5:61 17:91 39:69 51:98 0000 1:92 5:61 17:91 39:69 51:98 0000 1:090 180:43 1:2478 1:9464 84:48 55.87 1:0090 180:43 1:2478 1:9464 84:48 55.87 1:0000 180:43 1:2478 1:9464 84:48 55.87 1:0000 180:43 1:2478 1:9464 85.87 1:0000 180:43 1:2478 1:9464 85.87 1:0000 180:45 1:2458 1:9464 85.87 1:0000 180:45 1:2458 1:2458 1:9464 85.87 1:0000 180:45 1:2458 1:2458 1:9464 85.87 1:0000 180:45 1:2458 1:2458 1:9464 85.87 1:0000 180:45 1:2458	INCM DEV TUR REC DEGREE DEGREE DEGREE 0.03 3.00 11.97 47 0.03 3.00 11.97 47 0.03 2.05 11.97 47 0.03 2.95 7.33 47 0.03 2.95 11.20 47 0.04 5.61 17.91 39 1.70 7.03 22.95 34 2.95 5.61 17.91 39 2.97 5.561 17.91 39 2.70 7.03 22.63 39 2.77 7.03 22.63 39 2.77 7.03 22.53 42 NCOR-1 VCOR-1 10.70 10 NCOR-1 VCOR-1 10.70 10 ILLET INLET INLET 10.72 INLET 10.43 1.24778 1.24778	DECREFE 11.97 11.97 11.945 11.20 11.20 11.20 11.445 12.53 2.	TURN F DEGREE DEGREE 55 47.64 33 47.64 47.64 47.64 47.64 47.64 47.64 47.64 47.44 49.47 49.13 55 42.69 85 39.91 55 42.66 85 39.61 1.247R 1.1 1.247R 1.1	N CANBER EE DEGREE .75 55-91 .84 55-91 .85 55-91 .85 55-91 .85 55-91 .87 49.85 .97 49.85 .97 49.85 .97 49.85 .97 49.85 .97 53.61 .97 53.61 .97 53.61 .97 53.61 .97 19.85 .91 53.61 .91 53.61 .91 53.61 .91 10.00 .91 53.61 .91 10.00 .91 10.	The second secon	0-FAC 4994 49242 5122 5122 49212 49212 4931 4931 5562 5562 5562 5562 5562	B D-FAC OMEGA-B LOSS-P LOSS-P 19 4994 1788 0445 0456 10 5128 1624 0445 0445 10 5142 1624 0446 0445 10 4920 0639 0179 0179 14791 0651 0129 0179 14831 0651 0129 0179 1274 16506 1158 0179 0179 1274 15500 1114 0589 0179 5500 1114 0589 0179 5500 11158 0411 0443 5552 1231 0443 0443 5687 40.55 1274 127	10179 10185 0042655 0042655 00179 00179 0179 0179 0179 0179 0179 0179 0179 0179 0179 0179 0179 0179 0179 0179 0179 0179 0176 0176 0176 0176 0176 0176 0176 0176 0176 0176 0176 0176 0176 0176 0176 0176 0176 0177 01779 0170	- LOSS-P PROFILE - 1445 - 1445 - 1274 - 1274 - 1274 - 1289 - 1289 - 1445 - 1285 - 1445 - 1285 - 1445 - 1285 - 1445 - 1445 - 1285 - 1445 - 1285 - 1445 - 1445 - 1285 - 1445 - 1445 - 1445 - 1445 - 1445 - 1285 - 1445 - 1445 - 1445 - 1285 - 1445 - 1445 - 1285 - 1445 - 1285 - 1445 - 1455 - 1455 - 1285 - 12855 - 12855 - 12855 - 12855 - 12855 - 12855 - 1285		EFF- 2019- 2010	EFF-P EFF-AD EFF-P TOTAL TOTAL STATIC 0000 0000 7443 0000 0000 7443 0000 0000 7443 0000 0000 7443 0000 0000 6943 1 0000 0000 9832 2 0000 0000 9148 3 0000 0000 8148 3 0000 0000 8148	512 512 512 512 512 52 52 52 52 52 52 52 52 52 52 52 52 52	 ・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・	X	

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TABLE 10.5

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Blade-Element and Overall Performance with Uniform Inlet 100% of Design Speed

ROTOR

 B'-1
 B'-2
 V'-1
 V'-2
 V0'-1
 V0'-2
 U-1

 DEGREE
 DEGREE
 FT/SEC
 FT/SEC
 FT/SEC
 FT/SEC

 B 56.01
 15.56
 105.00
 663.9
 H94.1
 989.1

 B 57.58
 27.73
 111(.5
 663.9
 H94.1
 989.1

 B 57.59
 27.73
 111(.5
 662.6
 H94.2
 982.5
 101.90

 B 59.92
 21.94
 1240.5
 663.5
 H94.1
 246.7
 113.0

 B 57.93
 27.73
 111(.5
 662.6
 H94.1
 246.7
 113.0

 B 57.99
 21.94
 124.5
 982.5
 124.7
 124.5
 123.5

 B 52.90
 491.94
 1202.6
 603.5-1508.5
 1401.9
 1239.6

 B 52.91
 55.47
 950.5
 1302.6
 900.5-1508.5
 1309.4

 B 52.90
 491.7
 1402.9
 903.5-1508.5
 1309.4

 B 52.91
 55.91
 950.6
 1401.9
 1295.6

 B 52.90
 950.6
 1503.5
 1402.9
 1309.4

 B 52.91
 55.91
 950.6
 1402.9
 1402.9

 B 52.91
 55.91
 950.6
 1402.9
 1402.9

 B 52.91
 55. 5707 5707 5707 5867 5867 6746 7752 7752 7752 8079 2-.W 5036. .9708 1.0%83 1.1609 1.5965 1.4176 1.5709 1.5267 1.5507 .8636 A'I I I ī
 OWEGA-B
 D-FAC
 OMEGA-B
 LOSS-P
 DO2/
 EFF-P
 EFF-AD
 t D 50.28 #8.63 52.21 56.63 C DE 64 C D FT/SEC FT/SEC OF FT/SEC FT/SEC FT/SEC OF FT/SEC FT/SEC FT/SEC OF FT/SEC FT/SEC FT/SEC OF FT/SEC FT/SEC FT/SEC FT/SEC FT/SEC FT/SEC OF FT/SEC 616-6 603-9 525-6 519.2 518.3 483.6 415.8 FT/SEC
 S.
 INUM
 DEV
 TURN
 CAMBER
 OME

 E
 DEGREE
 570.2 584.9 598.5 625.8 639.0 632.5 613.0 606.2 599.8 954-5 925-7 819-2 785.6 799.7 789.2 756.3 612.5 613.0 596.2 599.6 584.9 598.5 625.8 629.8 DIA-1 DIA-2 IN IN IN F 19.467 21.047 19.467 21.047 22.314 23.964 28.95, 28.076 31.293 29.993 31.883 39.650 32.499 31.271 X.SPAN

TO/TO PO/PO EFF-AD EFF-P INLET INLET INLET INLET. 1.2547 2.0318 88.03 89.15

STATOR

DEGREE FT/SEC FT 1.0582 1.0730 1.0910 1,2594 1,2547 1,2447 1,2464 99CU.1 9CH34 2-.W -5592 -6558 -6558 -7522 -7522 -5511 .8527 1-1H 5703 5472 5291 5020 5173 5197 5131 Ĩ 7491 8591 8292 7441 7292 5069 Ĩ 7923 77759 EFF-P EFF-AN EFF-P 0000 E DEGREE DEGREE FT 50 17.73 56.74 19 23.02 36.88 7 6 39.04 62.61 7 89.99 62.61 7 99.99 55.17 98 92584 0000 9259 00000 9371 0000 9774 0000 9737 0000 9737 0000 9737 0000 9737 0000 9584 0000 51.81 53.96 P02/ 00 00 00 00 00 00 CD 40 00 00 CD 40 00 1000 1 00 111 1 111 1 0263 0221 .0481 SI85 .1581 .0468 .0466 0475 OMEGA-B LOSS-P LOSS-P B#1 8-2 DEGRFE DEGREE 41.5 4 #5.29 #7.#6 0263 0448 0448 .0481 .0489 .0489 #1.5 33.9 1000. C F1/SEC F1/SEC F1/SEC 1 1 761.9 -77.2 2 720.4 -27.3 2 720.4 -27.3 2 659.2 -195.5 3 626.4 -6.9 3 625.5 -16.9 -1888 -1720 -0727 0000 641.8 650.6 .5326 INCS INCM DEV TURN CAMBER OMEGA-B D-FAC (DEGREE UEGBEE DEGREE DEGREE DEGREE SHOCK -56 3-88 11-81 475 25595 -0000 -5297 -57 3-43 9-96 49.28 53.88 0000 -5297 -7.19 9-97 47.90 50.67 0000 -5195 %.20 7.19 9-97 47.90 50.67 0000 -5158 %.70 7.63 11.38 49.69 49.69 0000 -5055 5.52 7.53 11.38 49.99 49.69 0000 -5055 5.52 7.53 11.51 41.57 51.95 00000 -5185 697-1 707-6 607-1 76 650-8 690-4 650-2 72 607-1 603-5 506-8 65 606-8 613-5 506-8 65 620-4 610-5 520-3 65 633-3 630-4 653-3 65 C F1/SC 33.9 600.5 0000. 634.9 596.9 53.62 56.01 635.3 601.4 #1.56 #4.25 20.409 21.469 1039.8 68 21.509 21.469 1039.8 68 21.509 22.492 045.3 63 23.514 25.492 045.3 63 25.601 25.893 060.3 62 27.818 27.902 067.4 63 29.408 29.382 90.2 6 63 29.302 30.293 083.0 60 21.2**2** 22.92 F1/5EC 6.99 11.11 DIA-1 UIA-2 5.66 X SPAN X SPAN **؞** Ҍ ҡ ҄ ҄ ӄ ӄ ӄ **ӄ ӄ** v ö ti Ø 3 5 8 8 8

137

VC/A-1 LBM/SEC SGFT 39.81

MCOR-1 WCOR-1 TO/TC PO/PO EFF-AD EFF-P INET IMET IMET INLET INLET RPM LBWASC 11096 177.14 1.2547 1.9586 03.01 84.54

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TABLE 10.6 Blade-Element and Overall Performance with Uniform Inlet

	F1/SEC	1:42	1812:3	2.000 2.000	9.294	1313.8	3 1 W	.5526	5095.	.385	2002 -	NOST.
	TT/SC FT	0.000	1028:2 ¥	1248.5 1	1315-0 1 1543-6 1	1573.3 1	H - 1	. 9327	5756.	1.0313	1.1440	1.2891
	V01-2		1:49:5	1.614-	-619-	-961.9	ĩ	. 8655	5158.	. 7976	.7022	6891 6577
	FT/SEC FT/SEC F	90.96 999 11	2.0001-	-1248-5	-1515-0	-1573.3	ĩ	i i				5736
	V2	64 · · · · · · · · · · · · · · · · · · ·	283:3	195	960.5	952.6	STATIC	1.0057	1.0123	1.009	5808.	.8763
	V1 1/SEC	1012.0	1246:9	1394.4 1529.5	1651.0	1676.8	EFF-AD TOTAL	5 1.0048	5 1.0081	5 1.0072	C#16. S	6915 6382
	B'-1 B'-2 EGREE DEGREE F	0.1	1:13	000	50.5	64.80	TOTAL	\$ 1.00¢	1.007	1.006	.922	8926
												2.0238
ed	8-2 DEBREE	100	5:3	50.61	54.21	58.12	PROFILE	0026	*900 ·-	0079	.0108	.0091
gn Spe	8-1 DEGREE	000				0.	LOSS-P	0026	0034	0029	.0199	0243
Desig	V0-2	798.6	398.3	630.9	632.5	65.2.0	MEGA-B	0121	0161	0135	.0991	.1511
100% of Design Speed	VO-1 FT/SEC F	•••		••	00	•	D-FAC 0	2645.	5464	5426	5910	5676 1213 0243 5421 1511 0286
10	CH-2	619-6		521.4			ONEGA-B SHOCK	0000	0000	.0231	.0449	
				620.8 612.0			CAMPER	47.12	39.90	34.03	24.18	19.61
	V-2	1889:3	830:3	821.6 792.3	809-9 795-9	767.8						10.54
	1-1-1 1/5EC 1	557-0	500.5	620.8 612.0	592.5	560.1	DEV BREF	13.16	11.81	10.81	12.04	44
	DIA-2	19.769	23:83	25-520	29.993	175.16	INCH PREE C	1.1.1	7.61	7.52	6.63	6.61 6.76
ж	DIA-1 DIA-2	17.467	12:312	25.791	51.665	32.499	DEGREE	12.1	1.40	1.65	2.04	3.94 6.61 6.68 4.91 6.76 5.40
ROTOR	N SPAN	ъğ	12 8	82	88	8	N VDV	4	Ş	5 5	8	88

		•	•	•	•	•	
	-	1.2891	-	-	-	-	
141	. 7021			662	. 649	.6224	
1040	100	5775	0.0.	5020	5409	.5543	
1.009	.908.	5949.	2459.	.7872	.7537	.7209	
1.0072	5#16.	6615	2950.	.7881	.7521	.7131	
1.0065	.9223	.8926	CCCB.	. 5055	. 7760	.7402	
2.0773	1.9687	2-0171	2.0235	2.0776	2.0702	2.0401	
0079	.0106	.0001	• 00 13	.0118	.0165	-0187	
0029	• 61 10 •	· 0243	-0236	•0370	.0416	.0430	
-		.121 ·					
.5426	.5910	5678	.5421	.5474	5611	.5751	
.0231	6740.	.0805	.1130	.1353	1427	.1533	
		14.61		1			
30.86	18.77	14.04	10.43	10.09	8.27	9 6. #	
10.81	12.04	6-68	5.40	4.37	5.79	8.91	
7.52	6.63	6-61	6.76	6.54	6.45	6+45	
1.65	2.04	10-10 10	16.4	5.26	5.36	5.54	
15	8	8	8	8	8	8	

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IRLEY PRIER FREAD FREET

1.2598 2.0376 86.69 87.95

STATOR

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J L L	1049.3	1085.9	1157-1			0.8441	1466.5	N= . H			1.0001	1.0705	1.0044	3561.1	1.2149		1.2402	1.2408
I Sec .		-		~ ~			-	H-1		9969.	.6554	.6635	.6105	.7206	7945	1.29	.5226	-60 91
C FT/SEC F	-		m .	• 6	ي ال	-		2-X		TCOC .	-5426	.5253	6664.	5905.	.5091	2116	5008.	EL.
FT/SEC F1	-2.262	357.6-1			16.2.9	111.7-1	S.	1-1	:	2069	.8598	.8308	.7467	.7421	.7280	2051	. 7457	.7287
TISEC FT		N	1000	.	N#2	10	0	ادار مراجع	ATIC	- 0664	.7456	5612.	.8538	.8543	.8742	1800	.7780	.7636
TVSEC FY	00				-					-	_	-	-		• 0000	ŧ. –		_
81-2 EGREE FT									-	1					.0000			
B-1 FREE DE		-			-1-				-		_	-	_	-	.9769	L.	~	-
B-2 GREE DE						-	-	_							.0258			
B-1 JEGREE DE			_				_	-	ā.	_				_	-0258			_
T/SEC DE		-						_	F.	Ĺ.		-	•	-	• 0780	-	_	~
T/SEC FT	-		~		-	-	-	D-FAC ON		1	~	_	-	-	.5202	2	~	
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ί. Α.Υ.	9-1-0	0.5		•		1.5		S INCH DEV TURN CAN	REE DEG		8.44 S	8.7 6 5	8.35 5	6.88 4	5.77 #	3 10 S	4.32 5	6.15 5
EC FIC	00	8.3 6	5 .			1.8 6	10 10 10	PT V	EE DEG		-20	まち.	¥ • •	•28 •	.88		-53 41	-82 41
F1/5	101	8	50			90	5	ğ	DEBRI		6 6	r 6	1 10	8 11	0 12	81 8	1 20	22
01A-2	21.90	22.43	23-90	20.02	20.02	29.85	30.29	INCH	K GREE	ì	3.6	3.5	7.8	5-5	8.8		11.0	12.9
DIA-1 DIA-2 V-1 V- IN IN F1/SEC F1/S	20.409	21.589	23.314	100-02	801-62	29-914	30-382	INCS	DEGREE	82.1	.76	5	4.82	10 * 10	5,58	6.27	7.68	9.55
-	νō								-						12			

NC/A-1 LBM/SEC SGF7 39.04 NCOR-1 MCOR-1 TO/TO PO/PO EFF-AD EFF-P INLET INLET INLET INLET INLET 1404 180/56 1 11095 173.71 1.2599 1.9589 81.40 83.08

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Blade-Element and Overall Performance with Uniform Inlet, Alternate Method 100% of Design Speed **TABLE 10.7**

RO'. OR

11-2 5565 956.8	987.9	1111-5	1358.0	1462.5	1513.6	d-14	.6570	.6565	.6419
U-1 オノムモバ A45.4	893.8	1080.0	1-101-1	1543.2	1573.0	м1			
Vr+-2 174550 F	-293.6	-526.9	-905.7	1039.4	-1r66.6	~>			
1 V'-2 VO'-1 V''-2 - FI/SEC FI/SEC FI - 753.7 - A45.4 - 227.0		1248.1	101-1	-1543.2-	-1573.0	M-1			
V2 FL/SFC 1 753-7	742.9	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1162.4	1175.5	1155.7	61610 018110	9471	.9209	.8701
9'-1 8'-2 V'-1 ' BEGREE JEGREE FI/SEC FI/ P4 54.37 17.53 1040.1 '	1136.9	1270.2	1554-7	1671.4	1696.6	EFF-P EFF+AD E Total total ct	.9657	5442.	.8971
81-2 DEGREE-1 17.53	22.90	38-83 48-00	- 57.70 60.74	62.19	67.35	EFF-P E	.9690	1646.	.9055
9•-1 DEGREE 54.37	55.17 55.97	58.24 61.22	66 - 79	67.41	68.00	P02/	1.9859	1.9365	1.8660
2 8-1 8-2 8. c.ak Gref.accref Decre 9 .00 45.44 54.	44.03 45.54	41.41 39.87	37.61	36.98	45.13	LOSS-P ROFILE	0083	.0134	.0238
9-1 DFGREE	000		000	00.	00.	LOSS-P	.0105	•0164	• 0278
Vn-1 V0-2	604.2	544.6	-453-3	1 443.2	1 446.9	NEGA-B	• 0503	.0772	1313
7 -1 -5:1,55 <u>5</u> 6-				C.•		D-FAC 1	4390	• # 26#	.4925 4645
1.18-7	696. 552.5	553. 534	568 J	548.5	445.0	MFGA-3	.0109	.0137	•0194 •0407
v.−1 FT≠556.E 3 555.8	2 621. 035.	9 569.1 4 645.6	1 649.5	4 642.C	7 635.6	CAMRER OWFGA-3 D-FAC DMEGA-B LOSS-P LOSS-P PO2/ Decree Shock	49.83	43.55	39.11
2 F1/SFC F A 1.24.3	o n	a t	tim	0	c	TURN EGREE	36.85	12.25	19.41
V-1 FI/SEC 9 605.	A 021.	4 668. 0 585.	6 073. 3 649.	0 542.	1 ەئئم	JEV JEGREE D	15-65	ດ. 	96
DIA-1 DIA-2 FN I.4 17.467 19.769	7 21.40	4 22.36	4 29-49	3 30-03	9 31.27	INCY JEGREE J	5.43		
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TO/TO PO/PY EFF+AD EFF+P -INLET INLET INLET INLET

1.2091 1.7771 85.34 86.47

 B'-1
 9'-2
 V'-1
 V'-2
 V0'-1
 V1'-2
 U-1
 U-2

 IB67EE
 DEGREE
 FT/SEC
 FT/S 1.2629 1.2619 1.2562 1.3787 1.3787 1.3787 1.3787 1.3787 1.3787 <-- 1 N .7927 .7689 1 .7927 .7611 1 .7629 .8273 1 .7523 .8988 1 .7523 .9858 1 .6271 1.0540 1 .5566 1.0290 1 .5566 1.0290 1 TTTT. 1-15 827n ì 4586 4153 8153 8760 8322 7318 7339 7339 6898 ł > EFF-AD FFF-P TOTAL STATIC 0 0000 2741 0 0000 27441 0 0000 27441 0 0000 2704 0 0000 23070 0 0000 3137 0 0000 3137 0 0000 3137 9121 9121 9412 9442 9469 9469 9469 9469 9469 9357 9351 P02/ 3-2 DEGRIE J C. FIYEE ELISEC DEGREE D. 5.5 707.1 -67.6 40.94 5.2 644.5 -62.0 40.01 5.1 575.8 -71.8 36.87 5.5 528.0 -62.0 35.03 5.5 457.6 -62.0 35.03 1.3 445.9 -47.4 31.34 1.3 445.9 -47.4 31.34 1.4 454.5 -21.2 32.04 1.9 460.2 -15.0 34.51 ī <-U/ V9-1 C-MN 1-->> <-> Y 01.4-1 31.4-2 Y-1 V Y 1N J-1 F1/SEC F1/ 21.00H /1 1054.5 9 21.00H /1 1056.5 9 21.514 23.402 959.6 5 21.514 23.402 959.6 5 21.514 23.402 959.6 5 21.514 23.402 959.6 7 23.514 23.402 95.7 1 27.914 29.156 957.1 7 29.409 29.156 957.1 7 29.409 29.256 557.1 7 29.409 29.256 557.1 7 29.409 29.256 557.1 7 20.293 910.2 5 STATOR X SPAN v ö ñ 3 3 5 8 3 3

NUCHA WLORR TO/TO PO/PO EFF-AD EFF-P WCI/AI INLET INLET INLET INLET INLET INLET LBW/SEC RPM LBW/SEC X X SOFT 11093. 144.32 1.2091 1.6762 75,99 77,67 41,42

Blade-Element and Overall Performance with Uniform Inlet, Alternate Method 100% of Design Speed **TABLE 10.8**

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ROTOR

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71X5 5375 5375 7135 7135 7135 95 7135 7135 7135 7135 7135 7135 7135 713	51711C 51711C 51711C 51711C 51717 51717 51717 51717 51717 51717 51717 51717 51717 51717 51717 51717 51717 51717 51717 51717 51717 51717 51717 517777 517777 517777 517777 517777 517777 517777 517777 517777 517777 517777 517777 517777 517777 517777 5177777 5177777 5177777 5177777777 517777777777
FT / SEC 7 1037.5 1037.5 1136.5 1136.5 1136.5 1136.5 156.5 156.5 156.7 1	101AFA 101AFA 014AFA 09007 094007 094007 09400 09204 000000 0000000000
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ГС 3 - ГС 3 - ГС 3 - 5	P02/ 1.9525 1.9525 1.9126 1.9126 1.9126 1.9128 1.9128 1.7080 1.7080 1.6804 1.6804
Гамарана Гамара Гам	PR3FILE PR3FILE 0313 0103 00066 000044 00004 0015 0015
	DIAL.P DIAL.P 0337 0359 0143 0143 01152 01152 01152 01152 01152 01252 01252 01338
11/250 7555 7555 5555 5555 5555 5555 5555 5	MECA-3 I 598 1274 1274 01225 01225 01933 1108 1400 1400
	0-FAC -5137 -5137 -5137 -5606 -4680 -4680 -46060 -42093 -42093
1 2 2 2 2 2 2 2 2 2 2 2 2 2	564-8 70112 01112 0141 0141 0147 0767 11320 11320 11320
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FT/SEC F 501.5 601.5 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	7 113559 11.651 11.5511
014-2 19.769 21.447 21.447 21.447 28.454 28.476 28.476 28.476 28.476 31.271 31.271	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
DIA-1 DIA-2 I.4 I.4 I.4.467 19.769 I.4.467 21.447 I.4.467 21.447 22.514 22.964 22.514 22.964 23.954 28.076 31.295 29.93 31.295 31.271 32.499 31.271	1
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8477 7992 7422 6613 8591 8129 7603 6935 .0000.1.7284 .0015 1.7080 .0059 1.6804 .0127 1.6201 02020 0244 0300 0338 6.94. 3.13. 1009 4093 1108 5.66 3.01 1120 507 1140 3.96 7.66 1393 408 11822 0.01 7.47 1199 4299 2902 5.83 7.02 9.35 12.16 4 4 70 4 4 6 3 7 0 4.91 5.45 5.82 5.81 ក្ខ <u>ខ</u> ខ ខ

TO/TO PO/PO EFF-AD EFF-P

x x 1.2106 1.7974 86.55 87.59

STATOR

 9-2
 B*-1
 9*-2
 V*-1
 V*-2
 V0*-1
 Vr-2
 U-1
 U-2

 1
 -u0
 17.4
 49.3
 815.0
 1379.0
 -248.5
 14.4
 1779.0
 106.5
 106.5
 106.5
 106.5

 10
 -u0
 17.4
 49.3
 811.0
 1379.0
 -248.5
 114.4
 106.7
 106.5

 10
 -u0
 23.2
 50.8
 341.0
 1391.5
 -331.4
 1172.7
 1044.8
 1065.4

 10
 -1.80
 27.21
 55.21
 884.9
 1407.0
 -404.4
 1112.7
 1044.8
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 10
 -1.80
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 -1.80
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7117 1.1745 7117 1.1745 7772 1.2056 8802 1.2056 8802 1.2056 8801 1.2835 8801 1.2835 8802 1.3314 1.00236 1.3374 41-2 I - . N 7514 7514 7514 7590 7390 5802 5429 5429 5429 ŝ 9271 8973 8973 8800 88232 8232 7555 7234 7234 7234 7234 1-1 .6494 4-113 STATIC EFF-P EFF-AD **P01** T014L 9391 0000 9501 0000 9501 0000 9501 0000 914 0000 9467 0000 9467 0000 9467 0000 P02/ TOTAL PROFILE 8 .0350 .0346 7 .0350 .0346 1 .0328 .03287 7 .0326 .03287 0 .0562 .0259 1 .0301 .0301 1 .0301 .0301 0 .0563 .0583 0 .0561 .0563 0 .0561 .0563 0 .0661 .0661 .0661 0 .0661 .0661 .0661 0 .0661 .0661 .0661 .0661 0 .0661 .0 OMEGA-3 LOSS-P LOSS-P .1408 .1136 .1247 .0910 .0855 .1670 .1864 .1889 CAMBER OMEGA-9 D-FAC .0019 .0010 .0010 .0011 .0011 SHOCK AN INCS INCM DEV TURN CAMPER ON 5 JUEGREE JEGREE JEGREE JEGREE SH 7 -2.27 -2.32 9.15 40.34 52.45 6 -0.27 -2.36 8.90 39.41 50.66 0 -0.15 -2.36 8.90 39.41 50.66 0 -0.15 -2.36 8.90 39.41 50.66 0 -0.18 -3.39 10.36.20 49.60 10.44 50.68 -3.53 14.47 33.85 51.99 5 -0.46 -2.12 18.67 37.49 55.03 5 -0.24 -212 18.67 57.49 55.03 55.90 52.45 52.45 50.68 49.60 51.99 53.56 53.03

EFF-AD EFF-P WC1/A1 Inlet inlet LBM/SEC I.4ET INLET INLET INLET INLET INLET LAMZEC 4PM L3M/SEC **% %** 50FT 11491. 133.99 1.2106 1.7325 80.67 82.10 41.35 EFF-AD NCURR WCORR TO/TO PO/PO I. M.ET INLET INLET

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TABLE 10.9Blade Element and Overall Performance with Uniform Inlet, Alternate Method100% of Design Speed

ROTOR

B1-2 V1-1 V1-2 V0-1 V1-2 U-1 U-2 18.16 17.55C FT/55C FT/55C FT/55C FT/55C 18.16 10.33.9 654.1 -845.4 943.4 97.5 24.61 10.82.6 657.8 -893.4 93.4 97.5 28.66 1130.5 719.4 -941.6 37.5 39.4 97.5 39.61 110.55.7 795.2-1079.5 591.1 1079.5 111.1.0 47.46 142.5 895.9-1247.7 -660.2 1247.7 1244.6 55.621 1552.9 1021.5-140.0.8 1359.4.5 1011.0 60.081 164.7 1083.5-5-1510.0.8 1354.5 1514.6 60.081 164.7 1083.5-5-1510.0.8 147.7 1534.6 60.081 164.9 1070.6-1572.3 1512.9 160.1.8	FFF-P M-1 W-2 W-1 W-2 TATIC W-2 W-1 W-2 W-1 9061 5549 8419 9544 554 8940 5550 8007 10025 556 9993 5795 7939 10490 619 6614 9493 7793 170490 614 680 614 680 9059 6537 7737 1.3262 759 961 801 9058 6537 7077 1.3262 759 961 80 861 8176 5594 6111 1.5233 973 973 973 973 8176 5594 5440 1.5545 895 895 895 7710 5591 5546 1.5465 895 895 895 7710 5591 55405 5545 5695 895 895	V*-1 V*-2 V0*-1 V0*-2 U-1 U-2 FTSEC FT/SEC FT/SEC FT/SEC FT/SEC 772.0 1313.6 -258.5-1046.1 987.4 1039.6 776.0 1328.3 -322.7-1087.6 1016.3 1062.4 826.4 1342.4 -388.8-1119.8 1044.4 1085.7 886.6 1384.0 -534.7-1180.8 1238.6 1055.3 970.3 146.5 -566.8.8 1236.5 1329.4 1122.3 1546.9 -907.4-1413.6 1422.7 1421.5 1112.3 1561.7 -934.8-1426.8 1447.2 1442.4 1112.3 1561.7 -934.8-1426.8 1447.2 1442.4	-2 41 42 6698 -6692 1.117 6242 -7528 1.111 6693 -7528 1.111 6697 -8337 1.225 6097 -8337 1.225 6097 -9219 1.227 7194 -9492 1.273 4632 -9376 1.275
DIA-2 V-1 V-2 VV-1 IN FT/SEC FT/SEC FT/SEC 19.769 595.7 975.9 595.7 20.0408 601.68 932.0 610.8 22.040 660.8 957.5 660.8 22.964 660.8 957.5 660.8 22.25.20 650.0 837.4 681.0 22.25.20 651.0 837.4 681.0 22.520 650.0 837.5 650.2 651.7 31.271 631.7 656.2 631.7	FEGA-B 0117 0117 0117 0117 01415 01419 01419 01419 01219 01219 012319 01319 01319 01319 01319 01319 01319 01319 01319 01319 01319 01319 01319 01319 01319 01217 01219 01217 01219 01210000000000	STATOR 1.2264 1.8926 86.23 89.23 89.23 STATOR DIA-1 DIA-2 V-1 V-2 VM-1 VM-2 V0-1 V0-2 B-2 B-1 *SPAND N N FT/5EC FT/5E FT/5E FT/5E FT/5E FT/5E </td <td>INCS INCM DEV TURN CAMBER OMEGA-B D-FAC OMEGA-B LOSS-P P02/ 1 5 - 1-55 INCM DEV TURN CAMBER OMEGA-B D-FAC OMEGA-B LOSS-P P02/ 1 5 - 1-55 I.41 9.55 45.22 55.91 0023 4015 0757 0161 0175 9705 15 -2-51 441 9.55 46.44 53.43 0031 44109 0652 0161 0175 9705 16 -2-51 441 9.55 46.44 53.43 0031 44109 0552 0196 0199 9749 16 -2-51 441 9.55 46.44 53.43 00027 44.03 0756 0216 0199 9749 20 -2.41 1.50 10.76 40.34 49.59 00027 44.04 0621 0199 9749 20 -2.61 1.50 10.76 40.34 49.59 00027 44.06 0027 0197 9705 20 -2.61 1.50 10.75 49.14 99.59 0001 4253 01395 0756 00197 9705 20 -2.61 10.65 35.55 52.03 0023 4476 1121 0392 0038 00376 9690 20 -2.83 441 12.07 38.21 49.95 0027 44.06 1022 0138 0376 9690 20 -2.83 441 12.07 38.21 49.95 0023 4476 1121 0392 0388 0376 9690 20 -2.83 441 12.07 38.55 53.03 0023 4476 1121 0392 0388 0376 9690 20 -2.83 112 16.65 35.55 52.03 0023 4476 1121 0392 0388 0376 9690 20 -2.81 10.06 37.35 53.57 0035 44915 01022 0388 0376 9690 20 -2.81 10.07 PO/PO FFF-D FVI/A1 10.05RR WCORR TO/TO PO/PO FFF-D F VC1/A1 10.06R 10.070 10.070 FMLET INLET /td>	INCS INCM DEV TURN CAMBER OMEGA-B D-FAC OMEGA-B LOSS-P P02/ 1 5 - 1-55 INCM DEV TURN CAMBER OMEGA-B D-FAC OMEGA-B LOSS-P P02/ 1 5 - 1-55 I.41 9.55 45.22 55.91 0023 4015 0757 0161 0175 9705 15 -2-51 441 9.55 46.44 53.43 0031 44109 0652 0161 0175 9705 16 -2-51 441 9.55 46.44 53.43 0031 44109 0552 0196 0199 9749 16 -2-51 441 9.55 46.44 53.43 00027 44.03 0756 0216 0199 9749 20 -2.41 1.50 10.76 40.34 49.59 00027 44.04 0621 0199 9749 20 -2.61 1.50 10.76 40.34 49.59 00027 44.06 0027 0197 9705 20 -2.61 1.50 10.75 49.14 99.59 0001 4253 01395 0756 00197 9705 20 -2.61 10.65 35.55 52.03 0023 4476 1121 0392 0038 00376 9690 20 -2.83 441 12.07 38.21 49.95 0027 44.06 1022 0138 0376 9690 20 -2.83 441 12.07 38.21 49.95 0023 4476 1121 0392 0388 0376 9690 20 -2.83 441 12.07 38.55 53.03 0023 4476 1121 0392 0388 0376 9690 20 -2.83 112 16.65 35.55 52.03 0023 4476 1121 0392 0388 0376 9690 20 -2.81 10.06 37.35 53.57 0035 44915 01022 0388 0376 9690 20 -2.81 10.07 PO/PO FFF-D FVI/A1 10.05RR WCORR TO/TO PO/PO FFF-D F VC1/A1 10.06R 10.070 10.070 FMLET INLET

Blade-Eierient and Overall Performance with Uniform Inlet, Alternate Method 100% of Design Speed **TABLE 10.10**

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ROTOR

> > >	956.5	987.4	114 3	111.1	234.8	354.4	451.2	482.0	513.0	<u>د.</u>		.5576	.5494	.5537	.6226	.7-22	.8n53	.8416	.8751	8124
U-1 57765	۰_	c	. "	ം	•	•	•	0	+	1		£740.	†96 6*	1.0411	1.1627	1.3065	1.04.17	1.5136	.5386	•5616
V01-2 51/55/ 5	° ю	ŝ	2	c	-	4	ŝ	-	1	2		. P570	.8056	.7621	.7178	.7012	.4625	.6543	.6428	• ±964
- 10'-1		693.6	c.149- (-1079.6	5-1247.0	0,0041=3	7-1514.2	2-1542.6	-1572.4	11				-	-		ŕ	-	•5809	
11-17 2-175	1 646.	4 640	548	5 732.	434	2-962	3 1016.	3 :015.	5 996.	EFF-P	SIAILC	.9673	.9384	.9230	.9282	.8987	-8834	.8228	.7849	.7364
1-17 517555							~			EFF-AD	TOTAL	.9767	+9520	.9348	.9323	.8987	1078	.8162	.7758	.7159
81-2 DFCDEE	\$					-i				EFF-P	TOTAL	.9790	.9566	8046.	.9385	-9082	1068	8336	.7970	.7415
8°-1 DEGDEE	5					1				P02/	PO1	2.0803	2-0122	1.9600	1.9556	2.0039	1.9951	2.0193	2.0120	1.9517
9-2 DEGDEF	1									LOSS-P	PROFILE	.0048								
B-1 DEGREE	00	, .0c	00	.96	.00.		00.	90.	.00	LOSS-P L	LOTAL 5	.0076	.0148	.0181	5210	.0203	4050	.0301	0359	•03 ⁸ 7
H	776.2				616.6	200	584.7		605.3	MEGA-B		.0359	1		•		1			
V0-1		e	C •		•		•	•	-	D-FAC (.5401	. •56B6.	.5768	5545	.5419	5004	.5070	.5203	.5425
517560	521.1	587.5	560.6	557.2	560.2	550-9	531.9	500-8	410.4	MEGA-B	HDCK	.0131	.0161	.0204	0422	.0777	1011	.1325	+1398	.1503
V1						I				AMHER C	щ	68.64							•	
	96 4.1	939.2	8.16 ;	944.9	833-1	0- <u>567</u>	190.4	780.7	731.4	TURN C	DEGREE	39.27	32.83	27.01	18.80	14.26	9.81	8.80	2443	2.79
v-1 ₽1,456€	581.9	596 e h	610.0	641.0	561.7		634.7	627.3	620 . f.	73C I	LIREE C	10.4	13.79	13.55	10.77	5.45	84-4	4.28	5.29	9.80
214-2	:9°7°9	20-408	2147	22-964	25.520		29.993	30.630	31.271	INCM	EGREE J	6.47	6.65	6.45	5.37	5.11	5.23	5.13	5-11	5.15
DIA-1 DIA-2	17.467	18.467	.9.467	22.314	25.791	-28-954	31.295	31.883	32.499	INCS INCH	LGREE_D	•0•	.24	.48	1. 1	2.40	35.5	3. 86	4.02	t: - 5 t
SPAN												ŝ	2	15	8	81	22	ន្ល	8	92

.9323 .8987 .8791 .8162 .7758 9385 9082 8904 8336 7970 -0745 -0992 -1586 -1586 -2502 10.77 18.80 24.19 40427 5545 5.45 14.26 14.61 4077 5419 4.28 8.80 7.95 11325 5507 5.29 7.43 7.61 1138 5670 5.29 7.43 7.64 11503 55425 5.13 5.13 5.13 5.13 5.13 5.13 838388

TO/TO PO/PO EFF-AD EFF-P INLET INLET INLET INLET \$ \$ 1.2477 1.9932 87.80 88.98

B*-1 9:-2 V*-1 V*-2 V0*-1 V*-2 U-1 ¹¹⁻² DEGREE JEGREE FL/SEC FT/SEC F [-. N ۲ ۲ ž DEGREE DE 7 -2.570 -1.11 3 -1.11 3 -1.11 3 -1.11 3 -1.11 3 -1.11 3 -1.11 3 -1.11 3 -1.11 3 -1.11 3 -1.11 3 -1.11 3 -1.13 50 3.44 54 DEGREED 9 465.57 9 465.37 465.03 444.09 444.09 441.49 441.49 45.01 45.01
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 <th STATOR DIA-1 DIA-2 V-1 V-2 V 5 20.409 21.449 1035.3 698.7 71 6 21.608 21.961 583.2 649.2 65 10 21.508 22.432 999.5 649.2 65 30 23.514 23.902 90.0 623.4 64 50 25.601 25.493 999.3 699.3 699.5 64 50 25.601 25.492 999.3 699.3 699.5 64 50 25.914 29.492 901.9 649.5 66 55 29.914 29.455 901.0 642.8 65 55 30.382 30.293 969.7 602.8 60

1.0681 0.0681 0.000581 1.1736 1.1736 1.2551 1.2551 25553 1.25553 6470 6420 6420 7016 7562 8592 8592 8624 5814 55834 55633 5176 5303 53332 53332 53332 5221 5221 5221 4863 .8866 .8374 .8374 .7697 .7697 .7535 .7535 .7535 Control C P02/ 1 201_ 11 9459 9459 9450 9777 9777 9777 9775 9775 9775 PROFILE .0318 .0214 .0107 .0155 .0155 .0155 .0238
 I.VCS
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 MEGA-B
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NCORR WCORR TO/TO PO/PJ EFF-AD EFF-P WC//AI INLET. INLET. INLET INLET INLET INLET LAW/SEC WPM LBM/SEC * * 50FT 11089. 18J.44 1.2478 1.9468 84.51 85.90 40.55

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TABLE 10.11

Blade-Element and Overall Performance with Uniform Inlet, Alternate Method 100% of Design Speed

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	DIA-1	JIA-2	;	~ - >	11/2	~~~>	1-0>	2-02	11	9-2		N - 4	>	2-2	107	21-12	5	
_	111	1.1	T/SEC 1	- 17SEC	I JEEG	11/SEC-	IJSEC E	10-935/1	EGREE DE	EGREE -D	C-33893	EGREE F	TASEC F	T/SEC.F	17SEC.1	1-335/13		
	17.467	19.769	506.0	7.996	566.0	598°	ç	746.6	00.	52.71	56.20	15.89	1017.6	622.8	-845.7	-170.5	B45.	957.2
	18.467	20409	580-1	942.6	540.1	5.81.6		742.0	00,	51.91	57+82	22.94	1065.8	631.7	-834.1	-246.1	894.	964.1
	19.467	21.47	592.9	887.2	592.9	542		7.107		52.27	57.82	30.29	1113.5	629 . n	-942.5	-337.3	942	1019.0
	22.314	22.964	622.5	843.9	622.5	542	•	646.2	00.	49,98	60.05	40.62	1246.9	715.1-	1080.4	-465.6	1080.	1111.8
		25.520	642.2	829.2	642.2	541	ç	626.4	.00	49.15	62.78	48.34	1404.2	A.5.3-	1248.7	-609.2	1248	1235.6
	959-80	9876	6.8.7	o t	9.9	- 528-	- 	5-034		01-81		-55-49.	-1540+5-	- 934-2-	0-1011	-269-9	+1041	1050 I
	31.295	100.00	619.2	507-0	619.2	529		604.0	00.	48.99	67.77	57.87	1636.9	995.7-	1515.2	-R43.2	1515.	1452.2
	31.883	30.050	612.2	200.8	612.2	501.6	-	624.2		51.21	68.37	59.71	1660.6	994.7-	1543.7	-858.9	1543.	1483.0
83	32.499 31.271	51.271	505.6	756.5	605.6	415.	ç	7 .0 632.0	2.	56.67	68.95	64.76	.n0 56.67 68.95 64.76 1686.0 975.2-1573.5 -842.1	975.2-	1573.5	-882.1	1573.	5 1514.0
X SPAN	1 405	INCM	JEV	TUPN 0	CAMJER O	OWFGA-3 D-FAC NWERA-3 LOSS-P LOSS-P	J-FAC N	VEGA-3 (-055-P	L055-P	P02/	EFF + P	EFF-AD	56-0	- -	2=2	41-1	~

۰- ۲	.5356	.5414	.5365	.5n64	.6847	*****	.8217	.8158	-79Jn	
	.9376	.9861	.0307	.1513	.2943	- 4564-	.5041	.5301	.5541	
	. P 503									
						1				
EFF-D '	9439	9367	- 2016	9181	8888.	- 9654	8170	-7824	7359	
EFF-AD EF	9607	9517	9252	9240	8903	9618	6147	7781	7220	
EFF-P EFF	9645	9564	9321 .	1310	9006	8748	8328	7997	7480 .	
25/	767	3288	9624	3665	0128	1910	1714	9710	0160	
55-P P	0104 2.	0115 2.	0167 1.	0087 1.	0063 2.	0027-2-	0065 2.	0119 2.	0166 2.	
SS-P LO	0136	0153 .	0213 .	0.176 .	0223 .	0239	0320	0377 +	0406 .	
CA-B LO	0645 .1	0724 -1	1026 .	0862 .1	- 6601	1245-4	1657 .	2023	2539 •1	0 EFF-AD EFF-P T JuleT INNET
AC NE	5683 .	5755 •1	5925 .	5681 .1	5548 .	5212	5237 .	-370 ·	5596 .	ار م
1-0 6-49	150 .	181 ·	1222 .	1439 -5	793 .		334	- TE47	517 .5	ND EFF-F
CAMAER OWFG	.83	.56 .0	.14 .0	.23 .0	. 62 .0	101	.92	60	.43 .1	EFF-2
A L	*	*	т	~	-					PO/P
JEV TURN C	07 20.	+2 62.	· 78 27	-92 I9	41 66.	.69-10	• 66 9	.55 8	•88 4	T0/T0 IN ET
INCM JE	.22 14	.41 13	. 22 13	.13 19	6. 59.	- B. U	. 66 3	.61 4	.64 8	
I 4CS IN	. 79 7	7 66.	.23 7	•04 6	.11 5	- 96-	.38 5	-51 5	.73 5	
XSPAN	n (22	2 5	35	\$ 8	: 2	38	8 8	S.	

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x x 1.2547 2.0150 86.89 88.12 STA TOR

1.1 B1-2 V1-1 V1-2 V01-1 V11-2 U-1 U1-2 BEE DEGREE F1/SEC F1/SEC F1/SEC F1/SEC F1/SEC F1/SEC B1-22 57.01 723.4 1248.9 -2266.7-11047.4 948.1 1040.4 3.06 56.17 723.6 1288.4 -361.2-1104.1 1045.3 1086.1 8.004 62.77 730.0 1316.7 -491.8-1170.3 1128.8 1157.3 4.004 65.77 730.0 1316.7 -491.8-1170.3 1128.8 1157.3 9.48 65.05 988.3 1509.4 -751.3-11548.7 1346.9 1357.9 9.48 65.02 988.3 1509.4 -751.3-11548.7 1346.9 1357.9 0.44 65.12 1042.7 1539.9 -800.7-1307.0 1423.8 1422.6 0.36 65.11 1019.4 155.0 -800.3-1187.2 1441.0 1466.7 **C-1** -- . , 2 - ; ; ł B--1 DERREE DI 9 219-25 9 219-26 9 219-26 139-04 6 49-448 6 50-16 6 50-16 6 50-16 6 53-65 67 P02/ P LOSS-P 8-2 DEGREE
 Z
 VN-1
 VN-2
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 Jn C FTXSEC E C FTXSEC E 680.0 650.0 650.6 650.6 650.4 6529.4 6529.8 656 605.9 656
 DIA-1
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1.0350 1.0350 1.0543 1.05694 1.1500 1.2389 1.2389 1.2515 1.2458 1.24580 6233 6234 6234 7453 7453 8625 8645 8645 .6247 5641 5410 5234 5182 5182 5169 5169 5169 5169 5169 8768 8327 7958 7554 7554 7554 7553 7520 7520 EFF-P EFF-AD EFF-A IDIAL TOTAL STATIC 5 0000 0000 8334 5 0000 0000 8378 6 0000 0000 93790 6 0000 0000 9864 1 0000 0000 8864 7 0000 0000 7981 5 0000 0000 7981 5 0000 0000 8067 .8718 .9390 .88664 .8955 .8952 .7931 IOIAL .9515 .9626 .9626 .9741 .9741 .9559 .9553 0285 0234 0077 0077 0175 0175 0356 0326 TOTAL B 0301 0255 0205 0205 0205 0252 0252 0443 .1211 0999 0400 0731 0731 0824 1255 1255 HDK 5189 0073 5189 00073 5289 00107 5528 0146 5223 0146 523 0253 5189 02256 5189 0226 5583 0.5833 5 11.81 44.55 55.90 7 9.06 49.59 53.88 9 7.39 50.57 52.35 6 11.38 45.53 50.67 6 11.38 44.55 49.34 7 11.85 44.45 49.34 7 11.85 49.45 51.62 1 22.92 43.92 55.02 JEGBE 4.75 5.97 5.97 5.97 5.97 6.92 6.92 8.11 I ACS IN 4 J Conter Defined 1.405 1.405 2.14 2.14 2.14 2.14 2.14 2.14 2.17 2.97 2.06 2.97 2.06 2.07 2.06 2.07 2.06 2.07 2.06 2.07 2.07 2.05 2.07 2.05 2.07 2.07 2.02 X SPAN ~ 5 ÷ 8 8 5 8 3 3

NCORR 4CORR TO/TO PO/PO EFF-AD EFF-P WCI/AI LALET INLET INLET INLET INLET INLET IBW/SEC NPM LBM/SEC % 56F 11096. 177-14 1.2547 1.9586 83.402.84.55. 39.81

TABLE 10.12 Blade-Element and Overall Performance with Uniform Inlet, Alternate Method 100% of Design Speed

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ROTOR

	1-2 1-2	957.0	987.9	1019.9	1111.7	1235.4	1359.1	1451.9	1482.4	1513.8	< »		.5446	.5543	.5387	•5966	.6743	.7579	.7979	.7870	.7625
	U-1 FT/SFC F	.0	0		A 1	÷.	ŝ	0	±.	1			.0318	.9818	1.0273	1.1469	1.2878	1.4118	1.4957	1.5216	1.5451
	VO1-2 FT/SEC F		ŝ	.	ب	∾.	-	С	α	PD -	~->		.8598	.A202	.7619	.7140	.6953	.6662	.6751	.6592	.6117
											N1		.510n	.5246	.5364	.5612	.5768	.5715	.553n	•5446	•5385
	V'-2 V0'-1 FT/SFC FT/SFC	632.6	645.9 -	631.4 -	704.4-1	R03 .9-1	912.1-1	970.1-1	963.4-1	941.7-1	FF-D	ATIC	.9666	.9629	4616.	£606.	.8763	.9397	.7889	.7516	.7071
	VI-1 ET/SEC ET	011.0	059.2	106.9	239.3	395.7	531.8	628.6	652.6	678.3	= AD E	TAL ST	.9770	.9726	.9339	.9169	.8802	.8393	.7914	.7512	.6955
	31-2 DEGREF FT										-		-	-			-	~	~	.7753	
	B-1 F	ί IO	ŝ	S	æ	ю	-	~	Q	ŝ		•••	~	•	-		~		-	2.0737	~
	B-2 B DFGREF DF6	<u> </u>													.			_		.0171 2.	-
	B-1 B FGREF DEG	-00	00	00.	00°	°00.	7 00 .	5 0 2	9 00	00-		۰								.0429	
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	VO-1 ET/SEC				•			•	Ÿ	ę	D-FAC		.5567	.5602	.5887	.5755	.5619	.5374	5424	.5587	.5820
	CH-2	610.3	596.0	547.7	533.9	533.8	520.2	521.3	480.7	380.6	MEGA-B	HOCK	.0164	.0196	.0234	·0451	.0804	.1127	.1350	•1424	.1530
	TVSEC 5	554.55	568.1	580.5	607.5	623.8	618.0	597.5	530.6	584.5	AMBER C	EGREE S	48.83	43.54	38.12	24.19	14.59	9.05	7.96	7.62	7.45
	V-2	996.8	955.7	393.1	843.0	829.0	801.8	820.7	806.9	755.4	NAL	GREE	41.50	35.46	28.61	19.95	15.05	11.00	10.98	6.99	3.46
	V-1 17257 5		-	ŝ	ŝ	60	ò	ŝ	ø	'n	DEV	EGREE D	10.16	16+40	13.54	10.96	6.03	4.61	3.32	4.04	10.31
	DIA-2 F	19.769	20.408	21.047	22.964	25.520	20.076	29.993	30.630	31.271	NUM	EGREE DI	7.78	7.94	7.71	6.72	6.49	6.56	6.35	6.30	6.31
Ţ	DIA-1 DIA-2	17.467	18.467	19.467	22.314	25.791	28.954	31.295	31.863	32.499	INCS	EGREE OL	1.35	1.55	1.80	2.67	3.80	4.71	5.09	5.22	5.41
TO TOT												X SPAN OL	ŝ	5	35	ន	3	20	æ	3	95 5.41 6.31 10.31

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-	.6117	.5385	.7071	.6955	.7237		.0431	.2843	.5820	.1530	7.45	3.46	10.31	6.31	5.41	3
1	.6592	• 5446	.7516	.7512	.7753		.0429	-2334	.5587	•1424	7.62	66.9	4.94	6.30	5.22	3
1.4	.6751	• 553n	.7889	.7914	.8119		.0375	.1928	.5424	.1350	7.96	10.98	3.32	6.35	5.09	R
1.4	.6662	.5715	.9397	.8393	.8546	0073 2.0255	.0289	.1498	.5374	.1127	9.05	11.00	4.61	6.56	4.71	2
-	.6953	.5768	.8763	.8802	4168.		.0248	.1223	.5619	.0804	14.59	15.05	6.03	6.49	3.80	3
:	.7140	.5612	£606°	.9169	.9247		.0196	.0959	.5755	.0451	24.19	19.95	10.96	6.72	2.67	ส
1	.7619	.5364	4616.	.9339	.9401		1610.	.0917	.5887	.0234	38.12	26.61	13.54	7.71	1.80	5
•	2020		1 202 1	0716.	· · · ·				2000	0670.						2

TO/TO PO/P. EFF-AD EFF-P INLET INLET INLET INLET 1.2598 2.0231 85.73 87.08

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1040.587 1040.5 1063.1			ŝ	<u>•</u> •	4 10		+ -
		1465	1.02	1.050	1 153	1.2213	1.2414
•••	1128.6 1239.3 1346.7 1423.6		.6319	.6334 .625n	.7314	.8046 .8415	.8338 .8048
	2-13-68-3 2-1361-4 2-1357.0 2-1357.0 2-1357.0		.5606	.5379 .52n6	.5073	.5118 .5142	.5037 .480n
22225551	1 - 1 - 2 - 2 - 1 - 1 - 2 - 2 - 2 - 2 -	-1-664	- 8863	.798-	.7588 .7495	.7373 .7631	.7588
V = -2 V =	1311.1 1404.4 1535.7		TATIC .7986	.8250 .9171	.8633 .8630	.8720	.7870 .8363
щ.,	784.61 784.61 968.41 962.41 1012.91 1012.91		TOTAL ST	~ ~	~ ~	~ ~	00
	65.55 10 65.52 65.55 10 65.55 10 65.55 10 65.55 10 65.55 10 65.55 10 65.55 10 65.55 10 65.55 10 75 100	<u>~</u>	01AL T01	~ ~	~ ~	00	00
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0			OTAL PROF				
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-25-2 -25-2		32.6 32.6	1483 1483	.1342	.0751	.1496	.1471
V0-1 7/5EC 724+1	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	671.6	.5254	.5353 .5276	5358	5221	5599
VM-2 T/SEC F 676.4	526.6 595.0 617.4 626.3 535.6	599.7	HOCK • 0073	0078	0176	.0324	.0539
	631.7 616.4 621.6 621.2 651.2	N m C	55.90	53.87 52.36	50.67 49.55	49.85 52.01	55.04
. u	627.7 595.1 617.5 626.3 636.1	A.A. 4	GREE 01	49.08 50.93	47.30	45.09	45.60 46.69
1.	933.8 890.9 879.2 918.2		DEGREE DE	5.20	10.14	10.10	20.53
DIA-1 N 20.409 2 21.008 2	21.589 22.432 23.314 23.902 25.601 25.893 27.818 27.902 29.408 29.342	0.362	GREE DE 1.56	1.88	9	4.88 5.38	6.75 10.08 9.89 13.25
N N N N N N N N N N N N N N N N N N N	. 8 8 5 8 5 . 9 9 9 2 8 5		LEPAN DE	6 S	88	88	8 8

	.798~	.7588	.7495	.7373	.7631	.7588	.7249	
nc70.	.9171	.8833	.8630	.8720	.7744	.7870	.8363	
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0000.	.0000	•0000	.0000	.0000	.000.	.0000	.0000	
.9489	.9809	.9762	.972g	.9761	.9521	.9537	.9687	
- 0322	.0116	.0161	.0177	-0154	.0403	.0375	.0191	
0342	.0145	.0211	.0268	.025p	,0523	。0522	.0385	
.1342	.0554	.0751	.0876	•0789	.1496	.1471	.1068	
5353	.5276	.5358	.5241	.5221	.5449	.5599	.5794	ELD ALLA
0078	.0111	•0176	.0300	.0324	.0344	\$T#0.	.0539	22 0 22
53.87	52.36	50.67	49.55	49.85	52.01	53.64	56.04	0,00 EC
49.08	50.93	47.30	46.26	45.09	42.65	45.60	46.69	0110 00
5.20	7.37	10.14	11.25	12.87	16.10	20.53	22.82	1000
4.62	5.99	6.79	7.97	0.11	6.69	10.05	13.25	
1.88	3.04	3.79	30°3		5.38	6.75	9.89	1
<u>0</u>	15	8	8	ዩ	3 5	8	53	

NCORR MCORR TO/TO PO/PO EFF-MCL/AI INLET INLET INLET INLET INLET LAW/SEC RPM LBM/SEC 11095. 173.71 1.2598 1.9589 81.41 83.09 39.04

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TABLE 11.1 TABLE 11.1 Blade-Element and Overall Performance with Uniform Inlet 105% of Design Speed

ROTOR

U-2 ETASEC	1005.8	1038.5	10/0.0	11001	10521		1526.0	1545.4	1591.6			1	.6812
1.55	5 88.7	939.6		1130	1.12.5		1592.	1622.)	1653			•	1.0131
V01-2	-247.0	-305-8	200	0	N-101+		1064.3	1088.9	1119.7	4	N I I I		9232 1.0131
VI-2 VOI-1 VOI-2 ETJEC FIJSEC FIJSEC E	-888.7	-939.6	+ 056-	1130.5	1312.2	1.0.4	1592.2	1622.1-	-1653.5-		ļ		5850
V1-2	764.3	764.8	166.9			-1111-	1201.3	1205.7-	1209.2	1		FATTO -	1668.
1-1	089.	341.	192.	-	164	ŕ	729.	754	781	:	ONEDA-B D-FAC ONEGA-B LOSS-P LOSS-P PO2/ EFF-V EFF-AD EFF-P		.9162
81-1 81-2	16.36	23.58	29-15		17.84		62.38	51.33	67.82		115	Fot a	2010 ·
81-1 54055 -1	54.65	\$5.42	20.10	26.32	61.23		67.00	67.61	66.17		P02/	104	2.0575
8-1 8-2 81. NEARE DEGOLE DEGO	45.55	46.27	16.20	80° • 34	11.04	90.45	39.68	42.50	45.92		LOSS-P		
8-1 Gerre	0		00.	00.	.00	•	.00	00	8		LOSS-P	IOTAL S	0100
V0-2	750.8	732.5	707	\$21°\$	561.2		161.7	8 6 9 E	471.3		MEGA-B	Ī	100.
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01A-2	19.769	20.408	21-047	22-964	25,520		20.001		51.27:		NNCH	Coff.	
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 1 -2283 2-, H T-. H ž Į 8255 EFF-AD EFF-P TOTAL STALLC EFF-P EFF-AL E DEGREE DEGR 014. 012. 014. 021. 0219. 0214. 0219. 0214. 0219. 0214. 0229. 0259 177752926 1777577 **;** ONE BA-B LOSS-P LOSS-P 36.05 33.67 33.75 35.75 TOTA 1625 1001 /0-1 /0-2 /SEC F1/SEC - D-FAC E 927.5 CAMBER ONE BA 1-1-2 5 INCM DEV TURN CAP E DEGREE DEGREE DEG 76 -1.00 11.39 42.33 59 -1.05 9.07 42.33 35-35 38-08 2 DI A-1 DI A-2 V-1 20.00 21.00 21.05 21.000 21.05 21.000 22.021 105 21.000 22.021 105 21.000 22.022 105 22.011 23.002 1005 22.012 23.022 65 22.012 23.022 65 22.222 20.056 622 23.012 20.293 61 20.012 20.295 61 20.012 20.012 20.012 20.012 20.012 70 20.012 20.002 1132.4 4775 1996 1996 1996 1.56 2222 7772 7772 7 **LSPAN**

NC 09-1 MC 08-1 TO/TO PO/PO EFF-AD EFF-P WC/A-1 .NLET INLET INLET ...INLET ...INLET INLET LEM/SEC RPM LBW/SEC U.2337 1.1971 ...T1.93 79.67 42.47 11644 189.00 1.2337 1.1971 ...T1.93 79.67 42.47

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Blade-Element and Overall Performance with Uniform lulet

105% of Design Speed

ROTOR

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		10	•	- 8		u c		14/1-0				1	•	1000	1.0650		0110.1	CHORO I					1.6403
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107	FT/SEC F		7.870-	000-								1-1		1	5995					1			
V1-2	FT/SEC 1	7.1.1	7.64.0	740.5				1107.0-1500.8				555-0	CTATTC	06.12	90.99	9180	1219.	.8776	A105	78.87	1980		0010.
1-17	T/SEC	1086.0	11.17		1120.0	1492.1	1.07	1726.6	1740.4	1776.6		EFF-AD	TOTAL	9730	9549	9313	9169	.8767		7146	6969		1000.
B'-2	DEGREE	17.31	71.17	50.17	10.78	47.00	×7.90	62.01	65.05	67.86		555-P	TOTAL	9766	.9593	9379	9247	. 8884	0308	7566	7210		-000-
81-1	DEGREE	54.84	55.61	56.36	58.53	61.41	68.74	67.27	67.86	66.41		P02/		2.1662				"	-			•	
8-2	DEGREE	18.32	47.89	47.45	10. F	44.18	43.98	46.89	49.37	52.62			- 0	0040						1			
	D							00.				Loss-P	TOTAL	.0082	•0136	.0186	•0186	.0246	.0273	0460.	.0379		£000.
2-0V	FT/SEC	786.6	748.1	7.8.7	641.7	616.1	538.0	540.0	547.3	552.3	•	OMEGA-B		.0393	- 0643	.0897	.0898	.1181	.1521	.2111	8542.	7 m	10.0.
1-0V	F1/SEC	•					0.	•				0-FAC		4935	.5118	.5258	.5137	.5010	. 4649	4689	.4763	0.000	
VM-2	FIJSEC	700.3	676.1	645.8	631.2	633.9	557.5	505.8	9.69.8	422.0		OMEGA-B	Б	•0158									
1-HV	F1/SEC	625.4	642.5	658.4	694.3	712.4	5-424-3	666.2	659.2	653.8		CAMBER	DESREE	47.12	39.99	34.03	24.20	14.68	9.18	8.05	7.68	7.47	
V-2	FIJSEC	1053.2	1008-4	958.9	899.7	884 • 0	774.7	7:000	721.3	695.1		TURN	DEGREE	37.53	32.44	27.19	18.75	24.48	6.85	4.47	2.81	К. Ч	
1-2	17SEC	625.4	642.5	658.4	694.3	712.4	E.#9à	666.2	659.2	653.8		DEV	DEGREE	15.44	13.54	12.65	10.06	4.75	7.45	8.73	96.6	12.03	
DIA-2	N	19.769	20.000	21-047	22-964	25.520	2A-076	29.993	30.630	31.271		INCM	DEGREE	5.87	5.97	5·•65	4.61	4 • 60	5.14	5.15	5-11	5.10	
DIA-1 DIA-2	N	17-467	10.457	19-467	22.314	25-791	28.954	31.295	31.683	32.499		INCS INCH DEV TURN C	DEGREE	56	04-1	- 19	* 9.	2.00	3.30	3.93	4.05	4.20	•
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TO/TO PO/PG EFF-AD EFF-P

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		5	T/SEC F	1037.4	1067.9	1097.4	1185.1	1301.3	1414.0	1494.8	1520.6	1544.3			1.0.47			.74.37	7597.	.8605	.9379	.9642	.96.05	.9552
		V01-2	T/SEC F	1106.3	1148.1	1177.3	1232.9	1333.0	1445.1	1483.5	1494.0	1520.4	•	N I	70.01			.6525	.6<88	.6142	.5458	.4975	.4766	8644.
		1-101	T/SEC F	-275.5-	-341.0-	-406.5-	-553-5-	-687.3-	-071.4-	-1.446-	-959.8-	-975.7-			DECY			. 0762	.8299	.6120	.7360	.7188	7083	1.4.
		V1-2	T/SEC F	1386.2	1401.2	1411.5	1444.4	1525.1	1568.5	1603.8	1605.1	1616.6												.8213
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		81	EGREE D	10.03	23-55	28.36	37.01	42.98	51.90	55.04	56.30	57.83			1010	0101		0.00.	.9798	.9652	1986.	1416.	.9723	.9671
		8-2	GREE	97	-2.28	-2.72	-1-37	-1.31	-2.31	-95	2.30	2.03			10100			-070-	.0156	.0301	.0152	.0311	0110°	02 .0000 .5600 .1198 .0432 .0432
		8-1	EGREE D	43.33	42.89	42.55	40.72	39.81	36.47	39.84	41.22	12,51			NIAL OF			1020.	•0156	1020.	.0152	.0311	-0345	• 0432
		V0-2	T/SEC D	-14.2	-31.6	-37.1	-10.0	-16.8	-26.8	10.0	23.6	10.4			1300			10/01	.0555	5860.	·0459	·0889	-0972	.1198
36		1-07	T/SEC F	761.9	726.9	690.8	631.6	614.1	542.6	550.7	560.8	568.5			A178			-202	. 087	.4280	*566	.5111	5346	.5600
2223 149/55 84.98 86.36		VM-2	L/SEC	835.0	003.0	778.4	752.4	740.5	660.1	609.2	586.5	549.5			0000			• 0000	0000.	• • • • •	.0000	0000	.0000	• 0000
155 84		L-MV	LISEC F	807.7	782.5	752.4	733.6	736.6	663.0	660.0	640.1	613.8						1	50.68	49.61	49.93	52.01	53-56	56.02
6.1 620		5-7		-	803.7	79.3	752-6	740.7	600.6	4-609	587-0	24 9.8	101			45.17			\$2.09	41.12	40.78	38.89	36.92	40.78
		1-7	4	1110-4	1068.0	1021.5	966.0	959.0	172.4	859.7	651.1	836.7	2			7			9.96	10.73	11.10	16-84	19-70	21.72
		DIA-2	í.	21-489	21.961	22 + 32	23+902	25.893	27.902	29.382	29.856	30.293			56.	-			1-30	2.25	2.09	5.63	5.12	6-46
		DIA-1		20.409 21.469	21.000	21-569	23-314	25-601	27.615	29-408	29-914	30.302	1111		-2.67	10.0-			-1.70	85	-1.16	.51	£.79	3.09 6.46 21.72
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VC/A-1 LBM/SEC 50FT 42.26 MC08-1 WC08-1 T0/T0 P0/P0 EFF-AD EFF-P IMET IMET IMET IMET IMET RPM LBM/SEC % % % 11650- :88.07 1.2523 1.9212 01.17 02.02

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Blade-Element and Overall Performance with Uniform Inlet

105% of Design Speed

ROTOR

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- UN 000	175	EFF-AD Total '	9529		9022	20 10 10	727.	699 6315
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		Ó	-4710 -5003	_				
FT/SEC 689000 659000 57795		OME GA-B SHOCK	•0158 •0213	0589	••592	.1433	•1689	177 1 866
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FT/SEC 1058-8 1058-8 1058-8 962-12 962-12 962-12 911-95 911-95 757-14	100 909 909 909	DEGREE	37 1 4 31 99	27.10	19•28		4 •55	8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9
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WC /A -1 BM /SEC 50F T 42.37 NCOR-1 WCUR-1 TO/TO PO/PO EFF-AD EFF-P INET IN ET IN ET IN ET IN ET IN ET INED 124/SEC 188.53 1.2420 1.8621 80.25 81.03

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Blade-Element and Overall Performance with Uniform Inlet 105% of Design Speed

ROTOR

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U-2 1005.1 1005.1 11297.5 11297.5 1557.8 1557.8 1559.8 1559.8	M2 .5896 .6074 .6200 .6397 .7223 .8529 .8629 .8629
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V02 -194.6 -194.7 -194.7 -194.7 -194.7 -194.6 -194.7 -194.6	M-2 98970 88655 77449 77449 665555 66555 66555 66555 66555 66555 66555 66555 66555 66555 665555 66555 665555 665555 665555 66555 66555 66555 66555 665555 665555 665555 665555 665555 665555 665555 665555 665555 6655555 665555 665555 665555 665555 665555 6655555 6655555 6655555 6655555 6655555 66555555
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FT VM 641561 641561 64470 66410 66410 66410 66410 66410 66500 665000 665000 665000 665000 665000 665000 66500000000	CAMBER DEGREE 39:99 34.03 24.013 24.013 34.03 7.998 7.9997 7.9997 7.99977 7.999777 7.99977777777
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T0/T0 P0/P0 EFF-AD EFF-P INLET INLET INLET INLET 1.2723 2.0855 85.67 87.08

STATOR

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20.409	21.489	1086.9		754.6	740.8	785.0	-16.5		-1.27	18.5 ₀	+	795.8	1337.0	-252.6-	1109.0	1037.6	1092.5	
21+008	21.961	1056.1		747.5	716.8	746.0	-38°-		-3-12	23.30	~	814.1	1359.9	-322.0-	1155.4	1068.0	1116.5	
21 • 589	22-432	1016.0	-	728.7	693.5	708.1	-45.7		-3.76	20.12	~	826.5	1374-0	-389.5-	1186.1	1097.6	1140.4	
23.314	23•902	940.3		667.9	667.8	661.9	-16.0		-1.37	38.07	~	848.6	1400.6	-523.4-	1231.1	1185.3	1215.2	
25+601	25.893	943.9	_	678.7	694.5	656.0	ດ ຄ		6 2.	43.54		937.0	1485.3	-645.6-	1312.8	1301.5	1010-1	
21.015	27-902	886.1		658-0	642.2	596-4	1.61-		P.T	51.18	÷	1049.7	1574-15	+.+I0-	やちま		0.0111	
29,408	29.382	905.9	_	659°2	625.6	621.1	18.7		1.71	52.96	•	1094.9	1602.3	-874.0-	1475.1	1495.1	1493.8	
29.914	29.656	905.6	-	645.4	619.6	635.2	20.2	_	1.87	53.92	.	1095.8	1620.8	-985.6-	1497.7	1520.8	1517.9	
30.382	30-293	885.9		607.2	582.0	645.1	26.5		2.61	55.98	•	1085.3	1621.6	-899.6-	1513.6	1544.6	1540.1	
INCS	INCM	DEV	TURN C	AMBER C	MEGA-B			-05S-P	LOSS-P	P02/	EFF-P EI	FF-AD	EFF.P	1-¥	N- 2	M - 1	M+-2	
DEGREE C	JEGREE C	PEGRES D	EGREE D	EOREE :	SHOCK		+	OTAL PI	ROFILE	-10d-	OTALT	OTAL - S	TATIC.		•	!		I
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14	2.53	8.33	48.06	53,88	.0000	5062	-	+0+0+	+0+0*	1426.	• 0000	.0000	.7859	.9000	.5945	. 7056	1.1262	
11	2.84	7.14	47.94	52.40	• 0000	5067	~	0357	.0357	.9463	.0000	.0000	7797.	.8683	.5754	.7120	1.1375	
2.31	5.31	0.85	46.11	50.67	.0000	4895		.0179	.0179	.9781	.0000	.0000	1068.	.7996	.5510	.7229	1.1552	
20.0	6.47	12.32	13.73	49.55	• 0000	4747	-	.0228	.0228	7476.	.0000	.0000	.8678	. 7953	.5691	.7895	1.2170	
2.56	5.80	11.76	43.89	19.97	: 0000		-	-0194	- #610.	-982U		-0000	-926-	0***		-1610.	1.2057	ļ
3.87	7.19	17.61	41.57	52.00	0000	5417		.0432	- 0432	.9614	.0000	.0000	.8025	.7517	.5048	•9086	1,2924	
4.99	8.32	19.27	42.68	53.55	•0000	5571	~	.0447	.0447	.9610	.0000	.0000	.8056	.7484	.4975	905	1.3007	
ó.96	10.33	22.30	44.12	56.02	0000.	5945		• 0+95	• 0495	•9593	.0000	• 0000	.7978	.7278	.4645	.8905	1.2928	
	KSPAN N <th></th> <th></th> <th>DIA-1 DIA-2 V-1 N DIA-1 DIA-2 V-1 20.409 ZH Set 7755C 7 21.008 21.961 1056.1 717.9 22.55.014 22.961 1056.1 717.9 22.5.314 22.992 9440.3 668.0 22.5.314 22.992 9440.3 668.0 22.5.314 22.992 9440.3 668.0 22.914 295.852 995.6 619.9 20.382 30.293 865.9 582.6 30.382 30.293 865.9 582.6 1NCS INCH DEV TURN C DE966E DE967E DE678E D 2.911 2.84 7.14 47.94 2.11 2.84 7.14 47.94 2.13 2.931 0.285 443.43 2.95 6 10.33 22.30 44.12 0.96 10.33 22.30 44.12</th> <th></th> <th>$\begin{array}{c} \textbf{r} \textbf{r} \textbf{r} \textbf{r} \textbf{r} \textbf{r} \textbf{r} r$</th> <th>$\begin{array}{cccccccccccccccccccccccccccccccccccc$</th>			DIA-1 DIA-2 V-1 N DIA-1 DIA-2 V-1 20.409 ZH Set 7755C 7 21.008 21.961 1056.1 717.9 22.55.014 22.961 1056.1 717.9 22.5.314 22.992 9440.3 668.0 22.5.314 22.992 9440.3 668.0 22.5.314 22.992 9440.3 668.0 22.914 295.852 995.6 619.9 20.382 30.293 865.9 582.6 30.382 30.293 865.9 582.6 1NCS INCH DEV TURN C DE966E DE967E DE678E D 2.911 2.84 7.14 47.94 2.11 2.84 7.14 47.94 2.13 2.931 0.285 443.43 2.95 6 10.33 22.30 44.12 0.96 10.33 22.30 44.12		$ \begin{array}{c} \textbf{r} \textbf{r} \textbf{r} \textbf{r} \textbf{r} \textbf{r} \textbf{r} r$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$											

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WC/A-1 LBM/5EC SGFr 41.93

NCOR-1 WCOR-1 TG/TO PO/PO EFF-AD EFF-P INLET INLET INLET INLET INLET INLET RPM LBN/SEC * * * * 11652 186.60 1.2723 2.0161 81.39 83.07

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Blade-Element and Overall Performance with Uniform Inlet

105% of Design Speed

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FT/SEC F	b. .						•		1624.0	1655.4		11		•5516	.5688	.5839	61.10		00.20	0110.	5937	.5855	5789	
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L'SEC F	1.71.6	1,22.9	73.8	0.1		0.0/11	1610.0	1717.4	1742.6	1769.6		FE-AD	OTM. S	9766	9621	9825	948		icos.	. 8233	7567	.7231	2 Auf	
E 69 - 2	16.86	22.76	28.26	41.38			56.72	59.67	61.71	65.74		EFF-P E	I TAL	9792	.9846	984	940		0//0.	.8411	.7812	.7509	. 7. 54	2011 ·
EGREE D	56+12	56.2.	57.64	50.A9		0.20	65,82	68.15	66.74	69-34			Pol J											
DEGREE C	51.17	50.32	49.14	e u		00000	49,87	52.47	54.91	59.05		Loss-P	PROFILE	TT 0.0.	10000				1,00.	•0035	+010+	7410.	22.2	~~ 10+
EGREE	00.	00-				00.	00.	60.	00	2	•	L059-P	TOIN F	12000	5 C 0 0 0			+05++	•0287	•0305	#3#U.	-0457		N
FT/SEC D	812.9	77.		1 203	0.00	664.6	626.0	660.5	676.7	50 S	C*000	OMEGA-R		19500	0000			•1206	•1420	1643	. 22.62	1201		20.24
FT/SEC 1		`	?	ş	9	°.	q	ą		•	Ð,	D-FAC		.5525	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			2985.	.5682	0424.	.5513	5645		00/01
TVH-2	640.3	5.019			0000	556.0	527.8	5n7.3	6 1 2 ° H	0		ONFEALB	1			•	-	-				5		
L-MA-L	597.7				202402	673.0	662.1	619.0			050.0	AMPED	DEGREE											
V-2 V	9.474.6				878.4	870.3	8,8,8	8.0.9	201		3.161	Triot	DFGDFF	10.05			00000	18.51	10.41	9.10	8448			3.50
V-1 F- /cFC	507			2020	654+2	673.0	662.	014			6-629	767		14 08		1.01	11./4	11 .65	6.24	6.14				
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1,5EC	1029.5	10,01			1-00-1	1.10.9	147-9	102347	1047.5	M - 1	- 1				-		. '	1098.		-
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T/SEC F	1312-1	140.0	1358.0	1383.4	1466-5	1.174.4	1014-0	1635.3	1038.5									.7601		
TYSEC F	773.3	193.0	612.9	815.0	908.3	1011.3	1044.4	1.39.1	1029.8	EFF-AD	TOTAL .	0000	0000	0000	0000	0000	.0000	0000	0000	.000
B'-2 DEGREE	57.16	59.31	60.73	62.54	63.16	66.21	66.76	67.14	68.25	EFF-P	TOTA	0000-	0000.	0000.	0000	0000.	0000-	0000	0000.	0000.
B'-1 DE GREE	19•03	23.88	28.39	38.67	57.44	50.75	21.91	52+89	55+02	P02/	POL	.9332	.933	0036	.976.	7176.	9723	4846.	.9478	6276.
8-2 DEGREE										د.	Ω,							•0557		
DE GREE	47.13	45.90	44.95	46.80	45.86	61 . 44	46.37	47.95	10.05	LOSS-P	TOTA	0.590	0419	•0462	10201	•0262	262U 0	.0557	•0576	.06.7
FT/SEC	-7.8	-33.9	-42.6	1.01-	0.01		13.5	[J.9	21.1	OMEGA-B		• 1:67	5 HQ 1 +	5141	714	855	BBB S	5691	1 623	•1085
FT/SEC	787 4	748.8	713.4	677,77	667.9	6.33.8	67549	695×0	703.8	DFAC		-5171	5309	5334	5191	5037	15345	5660	5799	•6072
FT/SEC								_		OME GA-B	SHOCK			_						
FT/SEC										CAMBER	DEGDEE	1 -	_	-			-	-		2 56.02
V-2 FT/SEC F1	111	7 684.	9 665.1	8 637°	662.	635-	637.6	635+	89	T(IRN	DFGOFF	0 47.7	6.9	1 8 1 C	10					b 48.02
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DIA-1 DIA-2	9 21.48	8 21 96	9 22 43	4 23.90	25.89	8 27 94	8 29.38	29-85	2 30 -29	NON .	NERE NERE DEGRE									2 13.59
I-VIO	20.40	21.00	21.58	23.31	25.60	57.81	29.40	9.9.6	30 - 38	INCS	DEGREE	0			4	u.			8.2	10-22
	0	5	15	8	50	2	8	ዳ	8		X SPAN	6	9	5	8	3	2	8	8	56

wc/A-1 L^BM/SEC SOFT 41.06 NCCR-1 WCOR-1 TO/TO PO/PO EFF-AD EFF-P INLET INLET INLET INLET INLET INLET RPH LBM/SEC 11674 182.71 1.2847 2.0448 79.50 81.47

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APPENDIX 4

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Blade-Element and Overall Performance with Radial Inlet Distortion

TABLE 12.1

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, . 1 Blade-Element and Overall Performance with Radial Inlet Distortion 70% of Design Speed

ROTOR

257-35 49 257-35 49 262-55-1550 262-55-1550 252-9 352 253-9 352 253-9 352 253-9 352 254-13 258-24 25
~ 5.92

DiA-1 CIA-2 STATOR

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U~2 1755	730.0	762.0	9.98.1	1029.0	. 9552	9732 0500	1.0105 1.0113 1.0081	0110.1
U-1 U-2 ET/SEC_ET/SEC		733.4		1032.0	100		7519	
V0'-2 ET/SEC	-715.3	*2 -299.6 -792.2 •2 -443.6 -864.4 •6 -572.6 -930.7	1014 3	1.8401.	4012.	6702 6131 5651	4695 4695	10 # * *
10°-1	-251.8	-572.6	-679-5-1014-3 -679-5-1014-3	-697.1-	1817.	.59093 59093	5508 5374 5319	171c.
	1083	1042	158	1166.9 LFF-P	4880 . 4880	6186 3422 2653	5914	
	712		854.0 1 854.0 1 854.0 1	EFF-PEFF-AD	80000 00000	0 0000 0 0000 0 000	00000	
3		22. 22 22. 22 22. 22			188	00000	0000	
B			22.45		1	9839	98155	
8				- పత్త	0129		0285	
			32.99	L055-p	0150		0285	
V0-2 F1/560	8 -10.		-16.2	OMEGA-B		.0662 .0679		WL/AL BM/SEC SOFT 29.70
ET 466	2 461	840 940 960 960 960	5 319.5 4 329.7	D-FAC		1073	•••	<u> </u>
		(5256 0 2256 0 215 0 th	OME GA-B	0000		0000	EFF-AD EFF-F INET INLET 79.47 81.31
VH-1 FT/SEC 1 6 686.3								PO/PO []
1-1-1		9 656.6		5				TO/TU P0/ INEET INU 1.0935 1.21
- 4 1 m -			5 586.3	DEV		1-		MCOFR T INLET II LBM/SEC 132.60 1
1 CIA-2 14-2 19 21-489	21.589 75.43	1 25.893	2 30.293	INCE DEGREE	•	الا	77	NCORR N INCT I RPM LB 7785 1
-	21.56	25-601 2 27-818 2 29-408 2	29.914	INCS	-11.02 -13.60	-14.12	-6.76	~ + ~
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TABLE 12.2

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Blade-Element and Overall Performance with Radial Inlet Distortion

ROTOR

70% of Design Speed

			1
179.4 173.4 173.4 173.4 173.4 199.5 199.5 199.5 191.7 101.7 11	1050.5 1060.5 M-2	59995 56595 56595 56655 56655	6571 6571 6524
1001-0 1000-0 10000-0 10000-0 1000-0 1000-0 1000-0 1000-0 1000-0 1000-0 1000-00	1051.2 1102.1 M*-1	6919 7209 7490 8221	-9425 -9932 1-0119 1-0288
V01-2 	-678.7 -700.1 H-2	6932 6605 6313 5753	0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44
V0 1 	-1081.2 -1102.1 M-1	1004 1004 1004 1004 1004 1004 1004 1004	2918 2918 2828 2828
V**-2 11:7 511	758.7 759.7 EFF-P		7114 • 7114 • 6685
758.0 758.0 758.0 820.5 905.2 987.4 108.1	1125.3 1142.9 EFF-AD	000000 000000 000000 000000 00000 00000 0000	7156
05049 15.35 25.67 57.49 55.67 57.45 50.70 50.70	63.49 67.15 EFF-P	9132 9132 9150 9715 9223	7270
0608*** 07088** 01.309 01.309 01.309 01.309 01.200 01.209 01.209 01.209 01.209 01.209 01.209 01.209 01.209 01.209 01.209 01.209 01.209 01.209 01.209 01.209 01.209 01.209 01.20000000000	74.64 74.64 P02/	1.3686 1.3686 1.3686 1.3458 1.3145 1.3145	1+3383 1+3383 1+3385 1+3385 1+3213
000 00 00 00 00 00 00 00 00 00 00 00 00	46.80 50.69 Loss_P	0250	0210
8841 8841 • 00 • 00 • 00 • 00 • 00 • 00 • 00	LOS LOS	0250	0138 0301 0334 0334
₩ ₩ ₩ ₩ ₩ ₩ ₩ ₩ ₩ ₩ ₩ ₩ ₩ ₩	360.1 360.4 OMEGA-B	181 1407 1419 1419 1419	1041 2025 2025
1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-	ċ		4278 4278 4417 4515
FT/SEC FT/SEC 5589.0 5560.9 55	358.6 295.0 0ME6 A -8 5M000		-0176 -0176 -0185
VH-1 VYSEC 472.9 472	ି ଟିଜୁ	47.12 39.99 34.03 24.29 14.66	7.52
17862 77867 77867 77867 54967 559081 559081 559081 559081 559081	·	4 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	12.57
1175 1775	302 DEV	13.48 9.12 7.42	6.3 6.2 8.2 11.21
014-2 19-769 20-408 21-047 22-964 22-964 22-993 22-993		888 888 888 888 888 888 888 888 888 88	
DIA-1 17.467 19.467 19.467 22.314 25.791 25.791 25.791 25.791	J2.499 J2.499 DEAREE (400400 40040 1111	9.83 10.06 10.46
x x x 0 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	96 A.SPAN	v 5 ñ 8 8 ;	5 8 8 8

TO/TO PO/PO EFF-AD EFF-P TNLET INLET INLET INLET

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128.1 128.1 128.1 128.1 128.1 1018.5 100.5 1000.5 10000000000	H - 2 9227 9528 9528 9777 9751 9751
11019-51 11019-51 11019-5 1	×
V0**2 -724+1	10000 100000 100000 100000 10000 10000 10000 10000 10000 100000
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174 10060 10060 110060 110060 110060 110060	141- 451- 451- 4525- 4555- 4555- 4555- 4555- 4555- 4555- 4555- 4555- 4555- 4555- 4555- 4555- 4555- 4555- 4555- 455- 100- 100- 100- 100- 100- 100- 100- 1
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	20128 20128 20128 20128 20128 20128 20128 20128 20128 20288 20288 20
10000000000000000000000000000000000000	L055-P T074L 10183 0143 0143 0143 0143 0148 0311 0311 0311 0312 0329
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44444444444444444444444444444444444444	TURN CAMBER CMEGA-B D-FA DEGREE JEVERE SHOCK 3 36.31 55.89 0000 23 3 7.71 53.86 0000 23 3 7.71 53.86 0000 23 4 35.54 99 52.67 0000 24 4 35.54 99.61 0000 24 5 35.99 52.05 0000 24 2 37.10 53.59 50.000 34 2 37.10 50.000 24 2 37.10 50.600 34 2 37.10 50.000 24 2 37.10 50.600 34 2 37.10 50.000 24 2 37.10 50.000 24 2 37.10 50.600 34 2 37.10 50.000 34 2 37.10 50.000 24 2 37.10 50.000 24 2 37.10 50.000 24 2 37.10 50.000 24 2 35.99 52.600 34 10.000 24 2 37.10 50.000 24 2 37.000 24 2 37.000 24 2 37.000 24 2 37.0000 24 2 37.0000 24 2
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DIA-1 DIA-2 BN -1	
DIA-1 20.409 21.5599 23.5314 23.5314 23.5314 23.5314 23.5315 2	1777
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TABLE 12.3

Blade-Element and Overall Performance with Radial Inlet Distortion

70% of Design Speed

ROTOR

4-2 ZSEC	10°4	13.2	76.1	64.7			59.6	2H	5283	5260	5297	57.04	6296		6247	62.32	62.80
U-1	••			•	11			1H		7137	_		_	T L		_	
VO1-2	•		- in	•			- 04	2-1		6559			-				-
VO'-1	•••			•	_ ا		. ^1	K=1	.4203	4265		5144.	.4095	12/2	.2822	.2735	.2640
VINZ E			~	~	ار نہ	11	7		. 8534	6339	. 6205	.8614	6468.	.8382	.6949	. 6602	.6393
L-1	750.3	812.8	897.4	980.4		1121.7	1139.2	EFF-AD	9268	.9053	.8543	.8941	9146.	1010-	. 7457	5002.	.6838
5'-2 DEGREE	14.80	25.75	37.57	17.73	80 19	63.78	66,85	EFF-P	9303	9606	. 6692	.8983	.9180	8762	.7566	.7215	.6969
91-1 DEGREE	52.07		57.44	63.05	10.36		75.16	P02/	1.4104	1.3869	1.3594	1.3283	1,3305	1.3566	1.3646	1.3564	1.3505
B-2 DEGREE	42.03	12.14	36.14	34.85	47 44	50.38	53.21	ة ت_ 1	0209	_		,		Ì		-	
DEGREE DE	ຍູ				ອີ. 		-	LOSS-P	0200					1			
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V0-1 FL/SEC		.		-	+-			B D-FAC	1.	391	•	•	•			•	•
CH-2				_]		_	OME 64	3	0010		-		ſ		Ĩ	-
VM-1					İ.			3	7 47.12		•						
V-2 CET/SEC					1			TURN	3 37.27	4 33,1	8 28.4	2 19.8	17 I5.3		7 12.6	6 10.6	1 8.3
2 V-1	191 69	107 107 107	584 493	20 443	20 349 9 20 308 6	100	162 1:		12.93	10.5	65 9.1	39 7 5	1°0 16	1	63 6. I	50 B.5	62 1 0-5
1 DIA-2	67 19.7		14 22 9	91 25.5	05 20 00	83 30 6	31.2	INTER S	33 3.10	80 J.L	39 3.	75 3.	01 5.4	2 2	33 13.4	55 11.1	92 11.1
1-410	1.7.4	101	22.3	25.7		31.8	32.4	DNI	-3.53	4.	r	;	'n	4	19.0	10.	10.
A SPAN	ωş	<u>5</u> 12	8	8	5 8	8	8		200	2	2	8	8	R	8	8	8

TC/TO PO/PO EFF-AU EFF-P

1.1044 1.3441 84.48 85.94

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1762	728.1	Ĩ	760.1	609	5	945	1.55	1011.	1080	N N	1	.899.	. 905	116	926	.9#6	151	125	1926	.957
	691.5	111.8	735	790.0	867.5	942.6	996.3	1013.6	1029.5	1-14		5979	.5928	.5967	.6346	.6753	CABA-	. 6680	.6646	.6621
V0 2	o	n	n	æ	~		0	ŝ	n	4=2		.6278	. 6059	.5859	5423	5864.	1224-	4336	4200	.4025
V0'-1	-189.8	-237.6	-289.2	-416.6		-599.5	4-609-	-618.3-	-632.8-	ī		.7230	.6884	.6597	.609.	.566.	.536.	5285	.5229	.5094
V2	n	0	ø	ው	-	æ	σ	~	s.	5°F-P	STATIC	.6807	.7455	.8366	.8584	ē. 7	.8965	.8130	.7880	. 7630
L	669.9	666.9	669.0	713.3	764.6	ZB0.0	768.9	756.8	767.9	EFF-AD	LOIAL S	•0000	00000	•0000	0000.	•0000	0000-	.0000	•0000	•0000
B'-2	45.73	48.02	50.04	54.28	56.30	1111	63.00	63,90	65.15	EFF_P [COTAL 1	.0000	0000	•000•	0000	.0000	3000	.0000	• 000C	0000.
B I										P02/	POI	.9725	.9780	5186.	12661	. 5926	9166.	.9865	9854	.9845
B-2 DEGREE	F .									LOSS-P	PROFILE	.0230	.0202	.0129	-0000 ·	.0110.	1210-	.0273	.0307	.0346
9-1 DEGREE	37.99	37.29	36.27	32,84	31.37	01,45	39,54	41.69	42,36	LOSG-P	TOTAL -	0230	0202	0129	•0 ⁰ 0	.0116	.0157	0273	0307	•0346
-2-0-5	1.1	-19.1	-32.2	0.44-	-39.9	50	7.6	11.2	11.2	MEGA-B	• •	•926	1670.	1640.			• • • TZ	.0780		.0960
V0-1	501.7	474-3	440.4	373.4	333.0	1 1 1 1 1	387.0	395.3	396.6	D-FAC		.2763	7975.	.2741	2741	2906	5349	10.01	4122	4370
VH-2	711.5	686.8	663.8	614.1	566.2	526,2	503.5	5.06#	470.2	OWE GA-B	N-OHS	.0000	.0000	.0000	.0000	.0000	0000	0000	.0000	.0000
VM-1										CAMBER (- Luij	55 . 89								
V-2	711.5	687.1	664.6	615.7	567.6	526.7	503+5	490+3	470.3	TURN	EGREE .	7 36.13	38,89	39.06	36,93	35.40	30	38,65	39.79	40.04
DIA-2 V-1 V-2 IN . FI/SEC ET/SEC E	915.2	782.8	747.5	688,4	639,8	610-B	608.0	601.6	588.7	2EV	DEGREE	:2.27	9.84	8.22	7.13	8.01	11-29	16.79	18.7n	2 5,59 21.05
DIA-2	21.489	21.961	22.432	23+902	25.893	27,962	29.382	29.856	30.293	INCM	DEGREE	-5.29	-5.47	55.51	-0.64	-6.24	19-74	3 15	12.1	5.59
DIA-1	20.409	21.008	21.589	23.314	25.601	27,818	29.408	29.914	30.332	INCS	DEGREE (-8.21	-8-00	-8.28	-9-64	-9.37	-5.35	16	1.32	2.62
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TABLE 13.1

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Blade-Element and Overall Performance with Radial Inlet Distortion

			_		_			_							_	_	•	-	_	_	_	
	U-2	860.1	887.	915.7	1.999	1110.3	1221.5	1304.9	1332.6	1360.5			128.	. 6695		1291	7847	4259			21	
	FT/SEC F	759.3	803.4	949.9	970.8	122.0	6.92S	361.5	1207.1	9.514	#1-1	-	1111	1540	5566.	4260*1	1.1625	1.2408	1.2981	1.3216		
	FT/SEC F1	~		N	*	-	-	÷	0	•	м-1		.8306	.8150	1564.	.7209	6414	5906	. 5674		50¥0	
	FT/SEC FT	759.9 -	- ***08	- 6.978	970.8 -	122.0 -	259.6 -	361.5 -	387.1 -	413.4 -	1		.5940	6019	.6118	.6317	5975	0 64 °	.4287	りまずま。	+036	
	T/SEC FT	723.9 -	760.0 -	71.2 -	134.5	1-0-00	962.9-1	1-6.966	91.4-1	1-2-040		ATIC	.7217	.7805	.7828	.8102	.8428	.8821	.8237	.7775	.7220	
	TYSEC FT													-	-	-			-	-	.7321	
	BI-2 V											AL T0T	8248	8556	8459 .	8384 .	6557	. 6968	8519 .	6086 .	7947.	
	BI-1 B GREE DEG	-	-			-	-														. 1710.1	
q	B+2 EGREE DEG												_		-						.0164 1.	
of Design Speed	1 EE DE 01						00 30				•	_	506 .0	367 .0	0.000	321 .0	232 .(151 .0	218 .0	271 .0	.0306 .0	
esign	2 2 2 5 3 1 2 5 3 1 2 5 3 1 2 2 3 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2										OWEGA-B LOSS-F	TOTA		-			-	-	-			
of De	FT/SEC DE	642	600	570	164 0	007 0	425	1000	1000	1460			_		_			_	_		202	
80%	FT/SEC	•	•				-	-	•		D-FAC		-		_	-			-		.4528	•
	VN-2	40,069	703.6	593.0	661.4	599.4	541.4	498.7	462.4	388.6	OMEGA-B	VU015	0000	1000	0000	.0116	.0305	0613	5100	.0674	.0961	
	T/SEC	641.6	649.7	660.1	678.9	8.409	520.4	461.9	451.9	442.5	MBER	GREE	47.12	39.99	34.03	24.51	14.64	8.69	7.74	7.45	7,35	
	T/SEC F	7.546	925.3	902.7	824.1	739.5	688.5	668.7	649.5	602.4	z	RE	2.36	8.85	6,12	7.57	2.02	1.76	1.38	9.74	5.97	
	FT/SEC FT/S	641 . 6	649.7	66n.1	678.9	634,8	520.4	461.94	451.9	442.5	ž	H	S.S	2.5	9.4		9	5	5	6.9	10.6	
	014-2 F	19.769	20+408	21.047	22+964	25+520	20.076	2 9 .993	50.630	11.271	Ŷ	Ĩ	•	3	3	•			š	è		
	T-VIO	17.467	16.467	19,467	22,314	25.791	28.954	31.295	31.683	32.499	INCS	EGBEE DI	-5.63	-5.05	-4.62	-3,18	.32	5.22	7.75	8.08	8,39	
ROTOR	_									5		_									88	

TO/TO PO/PC EFF-AD EFF-P INLET INLET INLET * * * 1.1663 1.5707 01.76 03.71

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Z V01-1 V01-2 C F1/SEC F1/SEC F1/SEC F - 264.7-1002.6 807.0 5 -330.2-1049.6 803.0 + -529.2-1049.6 1014.3 + -529.2-1113.9 1014.3 + -528.3-113.9 1014.3 + -528.0-1283.0 1279.4 782.0-1283.0 1279.4 126.1-1283.0 1279.4 126.1-1283.0 1279.4 126.1-1283.0 1279.4 126.1-1283.0 1279.4 126.1-1283.0 1279.4 126.1-1283.0 1329.4 126.1-1283.0 1329.4 126.1-1283.0 1329.4 126.1-1283.0 1329.4 126.1-1283.0 1329.4 126.1-1283.0 1329.4 126.1-1283.0 1329.4 126.1-1283.0 1279.4 126.1-1283.0 1279.4 126.1-128.4 -	201420200 001000000 0010000 0010000 0010000 0010000 0010000 0010000 0010000 0010000 0010000 00000 00000 00000 00000 00000 00000
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7/28-C2 929.4 929.4 929.4 9229.4 9224.5 771.5 771.5 771.5 711.7 711.7 711.7	C C C C C C C C C C C C C C C C C C C
VX-1 VX-1 VX-1 VX-1 VX-1 VX-1 VX-1 VX-1	TLRN CAMEER OVEGA-9 D FEGREE FEGREE SHOC: 42.29 55.99 0000 40.32 53.95 0000 10.37,40 51.67 0000 10.37,40 51.67 0000 10.35,20 49.95 0000 10.55 55.03 00000 10.55 55.03 0000 10.55 55.03 0000 10.55 55.03 0000 10.55 55.03 0000 10.55 55.03 0000 10.55 55.55 55.03 0000 10.55 55.03 00000 10.55 55.03 0000 10.55 55.03 0000 10.55 55.03 0000 10.55 55.00 000000 10.55 55.00 00000 10
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TABLE 13.2

Blade-Element and Overall Performance with Radial Inlet Distortion

ROTOR

90% of Design Speed

1755 861-7 861-7 861-7 861-7 861-7 861-7 1512-5 151	
U-1 77/SEC FT 761.3 804.9 972.6 1 11284.2 1264.1 1289.7 11289.7 1116.5 1	4144 4144 4144 4144 4144 4144 4144 414
7/55C F7 7/55C F7 -220.5 -220.5 -284.6 -584.6 -594.6 -555.9 1 -555.9	H-2 6236 9015 7160 1762 1762 1762 16418 5594 18 5574 1 5574 1 5574 1 5574 1 5574 1 2 5544 1 2 5544 1 2 5544 1 2 5544 1 2 5544 1 2 5554 1 2 5554 1 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
FY/SFE FY/SFE 	H - 1 - 1 - 5 - 5 - 5 - 5 - 5 - 5 - 5 - 5
77555 71715 7171777 7171777 71717777 7171777777	EFF. 7772 9405 9551 9646 8181 8181 7724
1 2 2 2 2 2 2 2 2 2 2 2 2 2	6174 Strain Stra
C 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	FT F F F F F F F F F F F F F
DEGRET [50.11 51.31 55.25 55.25 71.79 60.71 72.55 72.55 71.79	902/ 901 1.6450 1.6450 1.6596 1.65926 1.65926 1.7502 1.73002 1.7302 1.7302 1.7302 1.7302 1.7302 1.7302 1.7302 1.7302 1.73
0 4 8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Control Contro
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L	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
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66986- 66986- 7428 66986- 7428 66986- 7428 66986- 7428 66986- 7428 66986- 7428 7428 7428 7428 7428 7428 7428 7428	CAMBER 99,999 39,999 39,999 34,03 34,03 34,03 14,631 14,631 14,631 14,5311 14,5311 14,5311 14,5311 14,5311 14,5311 14,5311 14,5311 14,5311 14,5311 14,5311 14,5311 14,5311 14,5311 14,5311 14,5311 14,5311 14,5311 14,5311 14,53111 14,53111 14,53111 14,5311111111111111111111111111111111111
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T0/T0 P3/P0 EFF-AD EFF-P INLET 1.4.ET INLET INLET * * 1.4.759 1.6200 83.95 85.76

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FT47555 FT75555 FT75555 FT75555 FT75555 FT5555 -321.9 915.0 F15.0 -321.9 915.0 F15.0 -321.9 102.9 915.0 -321.9 915.0 F15.0 -324.9 -1012.9 915.0 -324.9 -1012.9 915.0 -324.9 -1012.9 915.0 -524.0 -116.1 115.9 -791.0 -1212.9 112.9 -792.0 1125.9 1212.9 -793.4 12312.9 1212.9 -794.4 -794.5 12312.9 -794.4 -794.5 1303.9 -907.8 1296.5 1324.9 -1717 21212.9 175.9 -807.8 7334 7331 -807.8 7177 60708 7334 -8455 55656 85696 85696 -6592 -55755 8416 15 -6592 -55755 8416 15

TABLE 13.3

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Blade-Element and Overall Performance with Radial Inlet Distortion

90% of Design Speed

ROTOR

-VIQ	DIA-1 DIA-2	ELISEC ELISEC	V-2	- 1 - 1	1 VM-2 V0-1 V0-2 B-1 C F1/SEC F1/SEC DEGREE DE	T/860 F	T/SEC D	B-I DEGREE D	5 8 9 8 9 8 9 8 9 8 9 8 9 8 9 8 9 8 9 8 9	8 - 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	E DEGREE	TISEC F	FT/SEC F	1. SEC	FT/SEC F		FT/SEC
17.467	19.769	4*029	936.9	630	676.0	•	651.6	ຣິ	5	50.	17.26		707.9	-761.3	-210.0	761	041.6
18.467	20.408	638.4	906.7	638	668.0	°.	613.1	00.	2	51.	22.46		723.4	-808-	-276.4	604	5.69.9
19.467	21 . 5 47	643.8	877,9	648	660.B	¢	577.9	00	:	52.	27.16		745.5	-846-5		5.5.5	917.5
22.314	22.964	668.0	809.5	668	635.3	•	501.4	.00	ġ	55	38.13		8.808	-972.5	** 667-	972.5	1000.9
25 _e 791	25.520	623.6	744.	623	578.3	ŝ	467.9	00	38.	8	48,06		1.938	124.1	-644.4	1124.1	1112.3
20.954	28-076	509.4	69643	503	51315	4	470.2	a	3	50	55.72		91210-	1261.9	-753.5	1261.9	1.22.7
31.295	200.02	449.9	687.I	034	469.0	0	562.0	5	-9	71.	59.78		-6-126	344.0	-503.2	1354.0	1307.2
51.863	30.630	439.8	673.4	439	0.404		514.3	50	¢.	72.44	62.15		920.0-	3.99.6	-820.7	1389.6	1335.0
32.499	31.271	120.0	630.4	90 W	359,6	2	517.8	8	22	73.Lo	66.95		918.4-	414.5	1-949-	1414-5	346.9
INCS	INCS INCH DEV T	JEV	- 5	RN CAMBER D	COMEGA-B	D-FAC 0	MEGA-B	L055-P	Loss	P02/	EFF-P [EFF-AD EI	EFFP	ī	Ņ	IH	N- 17
ERFE	DEGREE D	EGREE D	æ	EGBEE S	HOCK		-	OTAL P	PROFILE	Pol	DIAL	TOTAL	ILALIC				
-5.07	1, 37	15.38	n	47.12		#374	.1726	. D362	.0362	1.6652	8792	8698.	.8085		1526	9139	.6221
5.1	1.93	12.86	Ň	39.99	.00.00	1397	.1532	0325	.0325	E . 6456	.0624	.8736	62.63		7952	900 A	
80.7	2.04	10.68	Ñ	34.03	0000	1386	.1366	.0296	.0296	1.6252	.8633	.8748	8418		7647	9496.	6510
-2.67	2.49	8,51	-	24,31	.0124		.1137	.0240	.0214	1.5851	.6813	.8734	.6629		.7055	1.0567	.7050
	3-24	50° 51	-	14.65	.0318	1365	.1925	.0209		1-6101	. 6807	.8724	0000		6418	1.1789	7474
2.5	A.T.	2.26	4	8.92	2690.	455	2020-	0173	10.54	1.7009	. 8952	- 8869	.6774		.5223	1.2365	.7765
8.24	9,55	5.43	-	7.76	.0845	. 1756	.1439	.0263	.0111	1.7542	7628.	. 8266	.808.		5778	1.2965	7837
8.57	9.68	6.89	្ឋ	7.49	.0902	4 906	.1862	.0311	.0162	1.7502	6020	.7060	.7677		.5632	1.3202	116
8.87	9.8	11.01	φ	7.37	. 0 99	5086	.2236	.0329	C .5086 .2236 .0329 .0184	1.7146	7543	. 7349	.7225	.392.	.5239	1.3426	, 743e
		10,			F-AD EFF	ĥ											
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1.1800 1.6370 83.95 85.75

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								Ł					1.0723		-	-	-	-	-	-	
Ī	A VEEN	ANO. 4	9.10	0.010	1016-1	1115.6	1212.4	1281.7	1303.8	1324.2		•	.7195	.7319	7435	. 7845	.8163	2142.	. 8480	. 8465	.8241
Vr1-2	1000			1.05.8	10.07	1166.7	1226.2	1261.4	1266.2	1286.7	~->	J	.7094	.6921	.6760	6346	.5882	5505	5354	. 5262	.4926
	_	1920-	<u>م</u> ر د					<u> </u>	۰×.	Â.	Ī	•	.8756	.0466	.8233	. 7664	.7141	. 682B		.6910	.662)
										1417.0	EFF=P	TATIC	. 8063	.8560	169.	.9026	.9139	8854	7926	. 7761	.7817
		• ب ي ر											00000		0	0	0	0	0	0	0
B'-2	FGREF E	19.50	50.49	52.17	56.00	59,56	6212	63.15	63.54	65.24	_		•0000	-	_		_			_	
8'-1	FGREF C	18.5	22.62	26.71	35,86	43.92	49.28	50.88	51.62	54.11			9677	۰	•	in	æ	ŝ	o,	o	•
8=2	FGREF T	64	92	-2.07	-4-56	-3.18	89	1.72	3.19	5.24	LOSS-P	ROFILE	.020.	.0171	.0145	00300	.0097	.0167	8420.	.039'	•C395
-	JE GREE	39.24	30.14	36.96	14	34 57	36.17	39,06	40.42	42,95	L05c-P	OTAL	.0202	.0171	.0145	•0 ⁰	.0097	.0167	-03#E	#6£0*	.0395
V-2	135/14	0~~	-12.7	-28.1	9.571	-36.1	-10	19.2	35.1	33.6	MEGA-B		.0812	.4670		+926	317		. 0995	.1112	.1697
1-07	FT/SEC	631.2	596.2	563 6	493.9	465 2	471.4	509.6	525.1	533.0	D-FAC		.3261	, 3291	.3290	. 3312	.3507	.3829	.4221	.4363	.4707
VH-2	FT/SEC	820.1		7.001	733.2	654 B	648 . 8	638.6	650.1	593.5	OME GUMB	SHOCK	.0006.	000¢.	.0000	.0000	.0000	10000-	.0000	2000-	.0000
1-4-1	FI/SEC	770.1	759.9	5 . 5 HL	721.3	675.2	6.163	627.9	616.9	572.5	CAMBER	DEGREE	55,89	53,87	52.47	50.67	19.64	19.93	52.04	53,58	56.24
V-2		820+1	799.6	781.3			- !				TURN	DEGREE	38,85	39.46	39.61	37,96	37.75		3, 25	37,23	11°65
1- 7	FI/SEC F	995.7	965.2	7.729	874.2	320.0	2.292	808.7	810.2	782.2	DEV	JE GREE	12.90	10.53	12.8	7.66	8.86	12.60	17.63	20.59	22.93
DIA-2	N	21.489	21.961	22.432	23,942	25.893	21.9.2	29.382	29.856	37.293	INCH	DEGREE	-3,92	1	90°	-0.02			2.86	3.90	0 * 0
DIA-1 DIA-2	NI	20.409	21.005	21.549	23.314	25.601	27.818	29.408	\$16.63	50.362	INCS	DEFREE	5 -6.84 -3.92 12.90 36	00°		-0.12	6		0 (* *)	50.1	6C•C
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Blad - Element and Overall Performance with Radial Inlet Distortion

ROTOR

100% of Design Speed

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										1654.7									Ac.03				
81-2	DEGREE F	19.26	21.12	26.57	30.21	50.08	57.52	60.96	61.96	66.69		1111	UTAL T	8343	.8440	8778.	14141	7026	- Re16	3100			116/ •
81	DEGREE	50.14	51.12	52.31	55,06	60.39	67.22	70.95	71.65	72.31		1021	P01 1	1.7644	1.7683	1.7607	1.6806	1.6593	1 7763	1.25.17			0410-1
8-2	DEGREE	42.94	41.76		30.45	39.44	40.52	44.32	45.68	51.29	0 - U U Q -	110007	PROFILE	.0480	0421	1040	.0312	02150.	0006 1	1002	000		COTO.
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						710.2					LANDED	<u>.</u>	١						8.89				
<u>,</u> -2	FT/SEC	1023.3	1005.3	986.3	898.9	793.6	738.6	732.2	733.2	679.7	11011		DEGREE	30.87	28,19	25.74	16.85	10.31	9.70	10.00	6,4,6	5,62	30.00
t-7	51/SEC	707.5	717.1	729.3	755.8	710.2	589.4	524.0	512.9	502.8	0E u		DEGREE	17.39	13.52	10.07	8.57	7.85	6.65	6.58	6,65	10 71	
014-2	N.	19.769	20.408	21.047	22.964	25.520	28.076	29,993	30.630	31.271	NUNI		DEGREE	1.14	1.69	1.76	1.08	3.20	6.95	8.77	0.90	9.00	
DIA-1 DIA-2 V-1 V-2	3 2,	17,467	18.467	19.467	22.314	25, 791	28.954	31.295	31.883	32.499	INCS		DEGREE	-5.29	** **	うり・オー	-3.05	*0.	4.96 6.95 6.85	7.54	7.77	8.07	
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Blade-Element and Overall Performance with Radial Inlet Distortion

100% of Design Speed

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3	1.07	3.89	6.23	12.5	14.65	0727	5047		.0351		.8132	.8254	.ê103	.8145	.6511		1.3230	•7467	
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Blade-Element and Overall Performance with Radial Inlet Distortion 100% of Design Speed

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8-1	E GREE	39,83	5.0.05		36.13	37.51	37.20	38,39	39.91	42.89	1.05S-P	OTAL	0238	0900			.0109	.0167	.0268	.0448	0840.	.0489	•
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V0-1	1/SEC F	675.8	8.1.19	626-2	564.0	526.9	507.2	537.1	555.7	567.4	FAC	5	515		200	8	215	351	372	391	411	448	:
VM-2	T/SEC F	854.8	878.6	873.6	819.6	732.8	699.6	701.3	694.5	652.3	MEGA-R		0000		2020	0000-	.0000	.0000	. 9000	00000	0000	0000	
1-47	T/SEC F	810.2	819.3	819.1	772.7	686.6	668 .2	677.9	664.7	6.013) agent.		ES. AO			27.22	50.66	49,62	49,92	52.03	53.58	56.04	
V-2	11/SEC FT	88". 8	878.7	5.2.2	819.9	733.8	63919	702.1	695.4	653.1	NORT	ECDER 1		5 F F F F F F F F F F F F F F F F F F F	+1·/	50.72	37,68	40.24	38.66	35.64	37.04	10.01	2
1-7	T/SEC	1055.	1044.	1031.	956.	865.	630.	B64.	866.	833.7	7 24			3.44	++• 21	11.65	9.67	9.00	12.03	10.66	20.26	29.62	
- 4 10		21.489	21.961	22.432	23-902	25.893	27 - 902	29.382	29.856	2 30 .293	TWCM				1.1	8.7	-3.26	07	1	2.21	N N	44.4	3
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Blade-Flement and Overall Performance with Radial Inlet Distortion 100% of Design Speed

	TrySee	957.9	968.9	1019.8	1110.7	1236.6	£360.4		1464 2	1515,2			:	*999%	.6641								
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	DEGREE									14:02	. 608			1,0014	1.0121	1.6159	1.7871	1.7850	1,9065	1.9741	1.966	1.9301	, ,
	DEGREE									T0*00	9-2201				0000	.0271	.0198	.0160	-,0002	.0037	.0097	0124	
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2-0A	FT/SEC										OMF64-R		0000		101	• 1 4 2 6	ercr.	.1526	1120	,1616	4503°	2457	
1-07	FF/SEC					•				•	D-FAC		4705					4494		2267 *	5086	5236	
2-47				671.6	574.0	526.0	6.984	454.1	197		CVEGA-B	CHOCK.	9906	1000				e210.	1.1	1641	.1501	.1603	
1-MV	A A A A	700.2	114.0	133.0	684.6	528.0	520.0	514.5	510.9		CANBER (FCREE I	47.12	30.09			07442				7.51	7.55	
<	941.9	969.1	956.1	1.085	794.1	747.5	747.7	736.1	703.5		TURN	NEGREE -		G				11.10			12 B	69°†	
1-7 	999	700.2	714.9	733.0	684.6	525.0	520.0	514.5	510.9		DEV	DEGRER	18.50	14 78								11.41	
DIA+2	19.769	20.408	21.047	22.964	25.520	-26+076	29.993	30.650	31.271		NCH NCH	EGREE	1.9	2.3									
DIA-1	17.467	18.467	19, 461	22.314	25,791	28,954	31,295	31,863	32.499		INCS	DEGREE	64.4-	-4-11		10.01						10.1	
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APPENDIX 5

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Circumferential Inlet Distortion, Distribution and Overa' Performance

PR	ECEL	DIN	GF	Ά	GE	8	12,7	4N	IK	N	OT	Fl	LM	EC),							
		a B	325	373 373	383	405 394	368	350	297 370	2				370	398	410	476	455	425	395	292	435
		2	335	380	388	408 306	370	352	297	1				399	422	433	447	473	445	416	327	456
		>	. 303	.344	.352	.370	. 335	.318	.268 346					. 362	.384	730 7	445	. 431	.405	. 378	.295	.415
	174	90-97	76.2	79.6	80.5	83.8 84.7	84.5	84.8	86.8 8.89	2			<u>324</u> °	112.1	109.5	108.8	105.4	105.8	107.0	108.2	116.6	107.3
		^L ,g-06	34.40 24.46	33.75	29.55	25.78	19.15	17.75	14.61					27.70	28.45	28.00	24.90	21.80	19.12	17.50	12.62	
129.8		P_{η}/P_0	.966	.972	.965	1/6.	- 969	.966	.952 968					.951	.952	.948	. 965	696.	. 966	196.	. 936	. 960
الم الم	0	n B	322	369	394	403	350	330	276	5				222	229	239	267	258	248	244	229	253
ution d,		>	322 346	369	394	403 382	350	330	277					222	229	239	268	258	248	244	230	253
istrib 1 Spee		M	162.	.334	.357	. 366	.317	.299	250					.200	.206	.215	241	.232	.223	.219	.207	.228
1 ntial Di Design	114	90-b ₇	90.6 80.6	9.06 8.06	91.0	91.0	90.7	91.7	95.6 91 1				264	89.2	89.2	89.2	1.00	87.1	88.2	89.2	93.5	88.3
TABLE 15.1 Vircumferent 17, 70% of I		90-B'7	30.00 30.00	30.18	27.85	24.35	17.70	16.20	13. 12					21.88	21.20	20.90	17.12	14.50	12.85	12.30	11.20	
TABLE 15.1 Rotor Inlet Circumferential Distributions Probe Station 7, 70% of Design Speed, $\underline{W\sqrt{\theta}}$		P_7/P_0	.968 070	. 972	. 972	. 975 . 975	. 972	. 968	.954					. 863	. 861	. 859	860	. 860	. 862	. 862	. 861	. 861
r Inle e Stat		8	352 368	385	402	391	353	329	286 384					333	335	325	322	309	302	300	266	318
Rotor Probe		>	355 370	387	403	392	354	331	291 386					382	385	373	340	333	329	330	299	345
Disk		M	335	.351	.366	. 355	.321	.299	. 262					.346	. 349	. 338	.307	.301	.297	399.	.270	.312
	65	1 8–06	96.1 95.6	94.8	94.9	93.7	95.5	96.3	100.1 95.0				204	60.7	63.5	60.6 70.7	71.3	68.3	66.6	65.3	62.6	
		7'9-0e	30.75 30.35	30.18	27.49	20.75	17.20	15.81	13.35					42.20	39. 78	30.18 28 40	22.65	19.28	17.30	16.90	14.63	
	le.	$\frac{P_7/P_0}{P_0}$.975 .973	.973	970. 970	.973	.967	.962 296	.954 .971					.952	.947	. 938	.914	.915	.916	.921	.916	.922
	Circunfar on tial Position	% Span	5 (hub) 10	15	8 9	20	85	06	95 (tup) MR					5 (hub)	10	c1 05	20	70	85	96	95 (tip)	MR

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1) Inlet plenum conditions: $P_0 = 2012$ psf, $T_0 = 534$ °R 2) V_m calculation is based on standard-day inlet plenum conditions 3) Circumferential reference position is TDC looking forward 4) Relative position of circumferential distortion screen is $210^\circ - 330^\circ$ 5) $\beta_T^{\circ} = \tan^{-1}$ [tan $\beta_T/\cos \epsilon$]

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TABLE 15.2

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Rotor Inlet Circumferential Distributions

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Position		ed)	2						ιαi	24.						<u></u>	0			I		114		
% Spen	P7/P0	50-Br 7	90 6	×	>	₽ E	E 17/P	-	90-b' 7 91	90-P1	×	>	B	P7/P0	90-B' 7	90-B7	X	>	ц. Н	$\frac{P_7/P_0}{P_0}$	90-13" 7	² d-06	M	⊳
(prop) %	126.	29.63								6.3	305	337	335	.978	31.90	89.2	6.	342	342	368.	28.30	92.3	. 275	305
10	179.	23.48								8.2	. 317	351	640	.979	31.18	89.3	. 323	356	356	14	28.80	92.2	202.	550
28	.972	R 1 8	96.86 8.96	8 .328 6 357	807 807		3 076		28.48 26.48	95. 7 85. 7	328	202	19	778.	30.17 26 85	89.5 00 7	675 ·	363	363	518.	29.45	92.1	. 544	379
35	975	23.20									357	36	868	976	23, 33	1.06	344	380	380	.976	23.20	92.0	. 348	384
3 8	976	19.80								- 00 T	338	373	372	976	19.45	91.5	. 325	359	359	.976	19.75	91.2	331	365
38	. 575	16.70								Q. 2	299	331	329	.974	16.65	95.0	. 305	337	336	. 969	16.48	92.8	. 298	330
8	¥16.	15.60								6.5	280	310	308	₽ 7 4 .	15.50	97.1	. 294	326	323	. 962	14.95	94.1	.277	307
95 (ttp)	-974	13.50								0, 1 0, 1	236	261	257	.974	13. 78	103.0	. 279	309	301	.951	12.18	98.3	. 233	258
Alm.	0/A.		ŝ				_		,,	0	220	Š,	705	015.		92.0	975.	8	200	?		1.70	67C ·	3
		μI	.11						H)	174						204						234		
5 (Bub)	974	32.85								5 6	282		306	. 955	38. 30	60.7	. 312	345	301	606.	30.95		. 258	286
10	.976	31.70					_			4.0	316		345	. 949	35.20	60.5	.311	344	299	. 897	25.98		. 235	26
15	126.	30.40							31.75		325		355	. \$43	32.30	63.1	. 305	337	301	168.	23.40		. 225	245
8	.978	27.60								2.7	. 333		364	.945	28.73	73.7	. 330	364	350	. 877	15.60		.181	20
50	.977	23.70								5.7	353		388	.946	25.20	73.7	. 344	380	364	. 875	11.70		.166	18
Q2	.975	20.10					_			6.3	344		379	.950	21.75	72.6	. 339	374	357	-875	9.20		. 151	16
8	.974	16.90								6.9	317		350	.954	19.85	72.7	. 336	371	3.5	. 875	8.25		. 141	15
8	.972	16.00								7.5	298		329	.953	18.73	71.6	. 328	362	343	. 873	6.50		.115	
95 (tip) MR	.971 .975	14.05	98.1 87.2	1.272 2.322	5 305 7 328 7 328	2 299 6 356 356	126. 6			8.88 8.9 8.9	329	278 363	278 362	. 937 . 947	15.10	68.7 71.1	. 273	303 363	282 344	188.	5.04	68.1 68.1	181-	201
							-						-											
		রা	\$ 3						81	294						324°						354		
5 (Duch)	.874	22.00									269		284	.951	25.03	113.9	. 324	358	327	973	29.10	104.9	. 331	Ř
10	.873	20.65									257		276	.955	26.55	110.0	. 350	386	363	.971	28.47	1U2.7	. 340	è
30	.872	19.65									244		263	. 950	25.85	109.4	. 353	389	367	.968	27.70	101.6	. 342	è
50	.871	18.20									213		30	. 952	24.75	107.8	. 383	421	101	.976	27.35	98.0	. 379	Ŧ
5 2	.870	15.28									204		218	. 955	21.90	107.6	. 388	427	407	.976	23.33	98.3	.373	41
8	.871	12.90	89.0	0.207	7 230	0 230	0 .873		9.32 10	109.2	.166	185	175	. 966	19.85	107.2	. 390	429	410	.972	19.65	98.3	. 348	384
6	.875	11.88									129		135	. 964	16.97	109.4	. 359	396	374	. 972	16.30	103.9	. 321	ŝ
95 (ttp)	. 878	11.42									124		125	. 956	14.90	112.3	.328	363	335	.972	15.15	106.2	. 311	Ş
MR	.876	10.70									060		87	.932	10.60	119.7	. 252	280	2:3	126.	13.18	111.8	. 291	S
	. 879		8				-																	

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1) Inlet plenum conditions: $P_0 = 2020$ psf. $T_0 = 525.2$ °R 2) V_m calculation is based on standard-day inlet plenum conditions 3) Circumferential reference position is TDC looking forward 4) Relative position of circumferential distortion screen is $210^\circ - 330^\circ$ 5) $\beta_7^\circ = \tan^{-1}$ [tan $\beta_7/\cos \epsilon$]

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TABLE 15.3

Disk Probe Station 7, 70% of Design Speed, $W\sqrt{\theta} = 111.0$ Rotor Inlet Circumferential Distributions

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Circumferential	ial)					
Position			2			-			114						174.		
Span	$\frac{P_{7}/P_{0}}{P_{0}}$	96' ₇	2-06	W	>	> ^E	P_7/P_0	90-B ¹ 7	90-b7	W	>	, ⁸	P ₇ /P ₀	90-13 ⁴ 7	6-b ₇	M	>
5 (hub)	196.	27.10	93.0	.263	291	291	. 975	27.60	88.7	.258	286	286	.975	30.60	78.3	.269	298
16	. 983 981	27.10 96 60	8.8 8.8	.281	311	311	.976	26.90	89.3	.269	299	299	.979	30.65	80.5	.293	325
8	616. 197	23.80	32.4 92.4	.302	334	333	979 . 979 .	25.00	89.7 90.1	313	314 346	314 346	.979	30.00 26.05	6.08 6	304	336
8	.982	20.90	91.9	.309	342	341	.982	21.90	89.9	.320	354	354	.980	23.00	85.1	.328	363
70	.981	17.10	91.4	.282	313	313	.981	18.45	89.6	. 303	335	335	.981	19.65	85.6	.318	351
85	.976	14.25	92.8	.255	283	282	.978	15.55	30.8	.276	305	305	.978	16.80	85.6	.292	324
96	.973	13.08	94.1	.241	267	266	.974	14.30	92.3	.260	289	289	.975	15.60	86.4	.279	309
95 (tip)	.964	10.75	99.2	.206	229	227	. 961	11.50	96.6	.217	241	240	. 963	12.75	89.4	.235	261
MR	.979		92.6	.284	315	314	.978		90.4	.295	327	327	.977		84.3	. 306	338
			204						264						324		
5 (bub)	.955	32.60	64.9	.271	300	272	.902	20.90	96.4	.200	222	221	. 967	23.85	113.0	.297	328
10	.959	31.15	69.3	.293	324	303	. 898	19.65	96.5	.200	222	221	. 969	24.70	110.4	.317	351
15	.954	30.60	70.3	.294	325	306	. 896	18.70	96.5	.200	222	221	. 966	24, 15	109.7	323	356
8	.935	23.40	72.3	.267	296	282	897	LG RD	0.80	906	000	000	9.90	00 66	0.07	346	100

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										337	
	328	351	356	381	388	361	317	285	222	357	
	297	.317	323	. 345	.352	. 327	.286	.257	.200	. 323	
324	113.0	110.4	109.7	107.6	107.3	108.3	111 3	115.1	119.7	109.4	
	23,85	24.70	24, 15	23.00	20.35	17.00	13.70	11.70	8.65		
	.967	. 969	. 966	.968	. 974	. 979	.974	.966	.945	.971	
	221	221	221	228	231	221	222	222	220	225	
	222	222	222	229	232	222	222	222	222	226	
	.200	.200	.200	.206	.208	.200	.200	.200	.200	.203	
264*	96.4	96.5	96.5	96.0	93.3	95.7	94.9	94.9	98.1	95.4	
	20.90	19.65	18.70	16.60	14.50	12.10	1 25	11.00	10.50		ĉ
	. 902	. 898	. 896	. 897	868.	. 898	. 898	. 899	. 899	. 898	litions 1 10° - 330°
	272	303	306	38	280	266	257	263	245	276	T ₀ = 529.3 °R inlet plemum condi C looking forward rtion screen is 21
	300	324	325	236	293	282	275	283	266	292	r ₀ = 529.3 °R alet plenum co : looking forw tion screen is
	.271	.293	.294	.267	.265	.254	.248	.255	.239	.264	pef, day TD fisto
204	64.9	69.3	70.3	72.3	72.7	70.7	69.1	68.4	97. I	70.5	= 2037 standard osition i erential
	32.60	31.15	30.60	23.40	19.40	16.20	14.50	14.50	13.10		ions: Po ased on i ference p circumfi 7/cos c]
	.955	.959	.954	.935	. 933	.931	.931	. 935	.934	. 937	Inlet plenum conditions: $P_0 = 2037$ p V _m calculation is based on standard- Circumferential reference position is Relative position of circumferential d $\beta \gamma^{\bullet} = \tan^{-1}$ [tan $\beta \gamma/\cos \epsilon$]
	5 (bub)	10	15	30	8	70	85	8	96 (tip)	MR	1) Inlet plen 2) V _m calcu 3) Circumfe 4) Relative j 5) $\beta_7^{\circ} = \tan^{-1}$

TABLE 15.4

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Contraction of the local distribution of the

Disk Probe Station 7, 90% Speed, $W\sqrt{\theta} = 164.8$ Rotor Inlet Circumferential Distributions

24	1 M V W P7/Po 90-617 5	32.80 90.0 .453 496 493 .940 31.40	31.30 96.2 .460 503 500 .947 31.60	30.60 96.3 .470 513 510 .947 30.78	28.60 95.3 .595 550 548 .947 28.30	26.10 94.4 .514 559 557 .952 24.85	21.50 95.6 .490 534 532 .947 21.10	18.40 97.0 .449 491 488 .943 17.96	17.30 98.0 .435 477 472 .941 16.98	15.95 98.7 .410 450 445 .930 14.50	95.9 .482 526 523 346
54 *	0-87 M V Vm	.430 472	.460 503 3	.471 515	95.2 .497 541 539	.501 546	.472 515 S	.429 471	.411 451	. 301 398 .	f67 511
	P7/P0	. 54	. 56	. J54	1 .953	. 954	. 952	. 950	.946	.937	
ا ل ا ک	<u>-8-9</u>				29.00 91.0						91.4
	> ਸ਼				.487 531						
•	"	490	506	515	531	534	511	469	443	396	506
	P7/Po	.930	.939	.945	.950	.950	.947	.948	. 946	.932	.946
	90-1 <u>%</u> 7	31.40	31.70	31.80	29.10	25.20	21.58	18.50	17.41	14.94	
<u>114°</u>	N 4-9-06	•			90.9 .487		-	•	•		•
		~			~	~	er.		~		•

Vm 439 472 531 531 531 457 457 457 401 502 502

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	368 363 353 353 254 256 274 256 256 256 256 256 256 257		503
	425 396 378 290 289 277 278 278 278 278 278 278 312 312		524
			.480
234*	60.0 66.2 69.0 61.6 61.6 61.6 81.1 81.1 81.1 81.3 87.3	354*	106.3
	36.50 30.78 27.70 17.70 17.70 17.70 11.40 11.40 11.20 9.65		30.40
_	.827 .813 .813 .813 .805 .771 .771 .776 .768 .768 .776 .776 .776 .776 .7770 .7770	-	-934
	432 435 418 491 522 520 520 510 510 510 510 510 510 510 510 510 51		450
	496 500 544 543 543 537 537 537		516
	.453 .457 .457 .470 .470 .500 .500 .474 .474 .474 .474		.472
304	60.7 60.7 73.0 73.1 73.1 73.1 70.0 70.0 70.0	324	119.3
	42.80 336.00 28.15 28.15 28.25 30 21.00 16.69		25.30
	904 883 905 905 918 883 883 883 883		884
-	·····		
	445 445 497 511 511 529 495 495 419 507 507		422
	458 458 505 517 517 541 541 421 421 421 511		441
	417 449 474 478 478 478 478 478 454 458 438 438 438		.401
1740	76.0 79.7 88.0 88.0 89.6 7.7 88.0 88.0 89.4 88.0 89.4 89.4 80.0 80.0 80.0 80.0 80.0 80.0 80.0 80	294	107.0
	29, 60 29, 60 28, 50 24, 50 24, 50 11, 40 15, 40 15, 40		26.72
-			. 821
	473 478 478 527 526 526 444 444 397 500		255
	501 448 502 533 503 534 503 535 503 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 535 500 55 500 55 500 55 500 55 500 55 500 555		258
	438 438 485 485 485 485 485 485 485 486 486 486 486 486 486 486 486 486 486		. 232
*	81.9 82.7 82.7 83.8 85.9 87.7 87.7 87.7 87.7 87.7 87.7	264	81.1
1	38.38 38.28 39.28 39.28 39.28 39.29 39.29 39.29 39.29 39.29 39.29 39.29 39.29 39.29 39.29 39.29 39.29 39.29 39.29 39.29 39.29 39.20 30.20 30 30 30 30 30 30 30 30 30 30 30 30 30	8	20.88
	.949 .945 .935 .935 .948 .948 .948 .948 .948		. 757 .
	5 (bub) 10 15 30 55 56 70 85 85 85 85 85 MR		5 (hub)

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540 540 585 585 584 584 512 512 512 512 549 549 545 553 552 552 559 559 561 561 561 561 558 .500 .538 .546 .546 .514 .477 .477 .458 .458 103.9 102.1 99.3 99.0 99.0 101.9 101.9 101.9 30.20 30.20 29.20 25.30 21.80 117.50 15.60 936 946 946 945 945 945 945 945 465 501 532 539 614 559 569 540 569 569 569 569 569 569 521 523 615 615 636 621 532 564 477 596 596 .477 .492 .569 .569 .574 .574 .519 .519 .519 116.9 111.0 106.6 106.3 106.3 106.1 106.1 106.8 24.95 26.60 27.91 25.40 25.40 25.40 19.85 119.85 118.60 409 397 333 333 333 333 338 236 236 236 238 238 238 102.2 101.1 101.1 101.3 108.1 108.0 108.0 108.4 26.90 25.65 119.40 114.03 114.03 9.98 8.36 8.36 Inlet plenum conditions: $P_0 = 196^{\circ}$ pef, $T_0 = 536.2$ V_m calculation is based on standard-day inlet conditions .818 .805 .7772 .7757 .757 .756 .758 .756 .755 .755 277 332 332 355 355 355 355 314 355 314 325 331 279 307 334 336 336 336 337 331 84.3 .251 84.1 .277 83.3 .302 86.2 .319 86.8 .322 84.8 .233 91.2 .233 91.2 .233 91.2 .233 96.1 .300 20.20 20.90 20.90 20.90 11.70 11.70 11.70 11.70 11.70 11.30 10.30 អ្វិ 5588888 A A A A A A

Circumferential reference position is TDC looking forward

Relative position of circumferential distortion screen is 210° - 330°

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 $\beta_7^{\bullet} = \tan^{-1} [\tan \beta_7 / \cos \epsilon]$

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TABLE 15.5

Disk Probe Station 7, 90% of Design Speed, $W\sqrt{\theta}$ **Rotor Inlet Circumferential Distributions**

Circumferential	utial						с) (2	i S		2001a	: ` ;		- 15	156.2						
Position			31			•			3[21	5					114			
Span	P ₇ /P ₀	1.d-06	90-B ₇	×	>	۶.	P_{7}/P_{0}	90- ^{0, 7}	90-B7	M	>	^V B	P ₇ /P ₀	90-0° 7	90-B-	×	>	8	$\frac{P_7/P_0}{P_0}$	90-b' 7	90-B7	M	>	^v m
5 (bub)	.944	31.40			452	451	.954		94.3	. 422	463		.961	34.10	88.0	.429	470	470	.932		90.6	.375	413	413
10	.947	31.20		•	476	475	.952		94.0	.439	480		.961	33.00	88.8	ŧ	487	487	.941		90.5	.418	459	459
13	.952	30.60			493	492	.954		93.2	.455	498		. 959	31.70	88.9	.450	493	493	. 950		90.7	.449	491	491
8	.960	28.60		-	524	523	.950		93.4	.471	515		.957	28.35	89.0	.466	509	503	.952		90.8	.476	520	519
8	.957	24.16			517	516	.957		92.3	.484	528		<u>69</u> 6.	24.63	89.3	.471	515	515	. 955		90.6	.478	522	522
2	.952	20.07			492	489	.953		93.6	. 456	499		. 956	20.70	91.6	.450	* 93	453	.953		90.2	.460	503	503
85	.955	17.28		•	459	455	948		93.4	.419	460		.954	17.50	92.5	.411	451	451	.949		91.0	.421	462	462
8	.956	16.33			445	141	.948		93.5	.402	442		.954	16.65	92.5	662.	438	438	.948		91.5	. 405	445	444
95 (tip)	.950	14.48		•	403	888	.939		94.2	. 355	391		.953	14.90	93.6	. 365	402	402	.939		93.2	. 359	396	395
MB	.954		94.3		491	489	.952		93.3	.451	493		.957		90.4	445	487	487	.950		90.8	.449	491	491
						-	_											-	_					

	339 37 277 277 277 277 278 278 278 278 278 27		171
	371 353 353 353 362 303 290 293 293 293 293 293 293 293 293 293 203		100
			644
234	66.1 73.1 73.1 72.6 90.6 90.6 97.6 97.6	354°	103 7
	31.60 26.90 17.80 15.54 11.10 11.10 8.86 8.86		00 00
	. 836 . 823 . 818 . 818 . 794 . 793 . 790 . 793 . 793 . 793		040
-	3397 3394 4453 4453 4456 4473 466 466 466	-	105
	455 452 4452 4493 493 493 488 488 488		424
	.414 .411 .411 .413 .453 .453 .454 .454 .454 .454 .446		40.4
204	60.7 65.5 65.5 77.2 77.2 74.0 73.1 73.1	324	
	33. 20 32. 20 25. 20 25. 20 25. 20 17. 08 17. 08		c 2 20
	. 905 . 894 . 894 . 896 . 895 . 915 . 915 . 915 . 915 . 915 . 915		200
	4 4 5 4 4 5 4 4 5 4 4 5 4 4 5 4 4 6 8 2 5 3 8 6 4 8 1 4 8 1 4 9 5 4 9 5 5 3 8 4 9 5 4 5 4		
	4 4 4 3 3 8 6 7 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4		:
	423 457 457 457 457 457 457 457		į
174°	78. 79. 88. 88. 88. 98. 98. 5. 98. 5. 98. 5. 98. 5. 98. 5. 98. 5. 98. 5. 98. 5. 98. 5. 98. 5. 98. 5. 98. 5. 98. 5. 98. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	최	
	36. 33 33. 464 33. 564 33. 564 33. 564 15. 56 15. 5		
	9450 9450 9456 946 956 953 956 949 956 949 956 949 953 949 949 949 949 949 949 949 949 949 94		
-	<u> </u>	-	
	463 522 522 522 523 523 424 450 424 450		
	466 520 520 450 469 450 450 450 450 450 450 450 450 450 450		
	53 53 53 53 53 53 53 53 53 53 53 53 53 5		222
Ŧ	82.0 84.0 85.6 85.3 85.3 85.3 85.3 85.3 85.3	264	
	88.88 88.88 89.89 89.89 89.89 89.89 89.89 89.89 80.99 80 80 80 80 80 80 80 80 80 80 80 80 80		
	. 956 . 956 . 958 . 958 . 958 . 958 . 958 . 958		-
	5 (bab) 10 115 115 115 115 50 50 60 905 (ttp) MR		

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5 (bub)	. 793	19.00	93.8	. 226	251	251	. 843	24.0	109.9	. 363		376			119.3	.423	464	405	.949	29.80	103.7	.443	485	471
61	. 792	18.70	93.8	. 239	265	264	. 835	24.0	104.5	. 364		388			115.7	.425	466	420	.942	28.70	101.9	. 445	488	477
15	. 789	18.80	93.7	. 254	282	281	.827	22.3	104.7	. 350		373			110.5	. 444	486	455	.941	28.39	100.6	.453	496	488
8	167.	18.50	93.3	. 294	325	325	. 792	15.9	105.4	. 275		294			106.5	.501	546	523	.957	27.85	96.9	.495	540	536
23	161.	15.75	95.1	.297	328	327	. 786	11, 88	115.4	. 262		263			106.9	. 503	547	524	.952	23.35	97.2	.480	524	520
5	. 784	12.20	99.0	. 264	293	289	. 781	9.02	119.9	.234		226			108.5	.480	524	497	.952	19.50	98.2	.446	488	483
85	. 785	10.33	100.1	. 243	270	266	. 762	7.64	119.8	. 212		205			205.6	.451	493	465	. 952	16.40	100.7	.407	447	440
8	. 785	10.23	98.6	. 246	273	270	. 781	7.13	119.8	.202	225	195	3	14.95	111.4	.422	463	431	.950	15.54	100.7	. 393	432	425
95 (tip)	. 781	8.36	103.9	. 211	234	227	.780	6.16	:19.7	.177		171			119.7	. 321	355	308	. 945	13.40	103.6	. 350	386	375
MR	. 786		36.6	. 269	298	296	.797		112.7	.279		285	.923		109.4	. 469	512	483	.951		99.I	.453	495	489
1) Inlet plenum conditions $P_0 = 1977$ psf, T	lenum c	andition	s Po	= 1971	7 psf.	To =	-	¥																

1) Inter premum constitutes $r_0 = r_2 r_1 r_2 r_3$, $r_0 = c_2 r_2 r_3$, $r_1 = r_2 r_3$ 2) Vm calculations is based on standard-day inlet conditions 3) Circumferential reference position is TDC looking forward 4) Relative position of circumferential distortion screen is 210°-330° 5) $\beta \tau^{\circ} = \tan^{-1} [\tan \beta_{\tau} / \cos \epsilon]$

	Dist
TABLE 15.6	Circumferential
	Inlet
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Disk Probe Station 7, 100% of Design Speed, $W\sqrt{\theta} = 178.2$ Distributions Rotc

	м Б	6	4	2	5	1	30	2	5	~	548
									•		
	>										548
	æ	. 447	.480	. 502	. 532	. 535	. 513	.47:	.452	.407	. 503
111	-11-06	91.2	90.7	90.7	90.6	90.9	90.5	90.3	90.6	92.0	90.8
	-13, J	31.43	31.70	31.26	27.70	24.70	21.27	18.32	17.14	15.11	
	$\frac{P_7/P_0}{P_0}$.919	. 928	. 933	.935	6 26.	926.	.939	. 937	. 922	. 935
178.2	El >	533	553	565	576	579	554	500	\$ 73	430	548
	>	533	553	5 65	576	579	555	501	473	432	548
S	×	.489	508	.520	. 530	. 533	. 509	. 458	.432	. 392	. 504
: រំ រំ	90-l} 7	89.5	90.5	80°.9	90.7	90.9	91.0	92.3	92.4	94.1	91.2
γ S ³ H	L .y-06	34.18	32. 78	32.00	28.40	24.60	20.90	17.55	16.18	14.38	
þ	P_{γ}/P_{0}	.946	. 946	.948	.941	.944	.942	.936	.930	. 920	196.
	, ⁸	520	551	572	587	595	568	525	500	446	560
2	>	524	555	576	590	597	569	526	501	449	503
	×	.480	.510	. 530	. 544	. 551	.524	.482	.458	409	.517
	90- B 7	97.6	96.7	96.1	95.7	94.8	94.4	94.4	94.6	36.8	95.3
	90- ¹ , 7	31.20	31.25	34.23	29.60	24.52	21.07	18.18	16.98	15.28	
	P ₇ /P ₀	026.	9 34	.937	.932	96.	.938	.936	. 932	.919	. 935
	^N	531	543	557	294	602	570	528	514	485	565
	>	534	545	559	596	9 0	572	531	518	490	568
	×	4 90	.501	.514	. 550	. 558	.527	.487	. 474	.417	. 523
17	Ly-96	96.2	95.9	95. 3	95.2	94.5	95.3	96. 6	96.9	97.8	\$5.5
	L ₄₉ -06	32.00	20.80	30.40	28.10	24.75	22.35	18.00	17.12	15.80	
ential	od∕ [⊥] d	.926	.922	.924	.933	196	. 939	940	942	- 942	. 936
Circunferentiai Position	Span	5 (bub)	91	15	ន	R 1	8	8 3	8	(dn) ca	MR

	408 374 229 229 229 224 224 238 241 269		535
	458 408 366 237 237 237 237 237 237 237 237 237 237		558
	.417 .370 .331 .331 .227 .223 .223 .223 .223		. 513
234	63.0 66.6 67.6 65.5 74.1 74.9 75.9 66.8	354	106.4 .513
	35.05 28.78 13.55 1.2.55 6.23 8.51 8.79 8.79 8.66		29.44
	. 115 . 177 . 177 . 177 . 179 . 179 . 179 . 179 . 179 . 176 . 176 . 176 . 176 . 176 . 176 . 176 . 177 . 176 . 177 . 176 . 177 . 176 . 177 . 176 . 176		.913
	478 476 553 553 553 553 553 553 553 553 555 553 555 534		475
	503 548 503 547 503 547 514 559 514 559 514 559 550 557 566 559 548 549 548 124 548 124 558 12		. 500 545
204	60.7 60.7 74.0 74.4 70.9 68.6 70.9 70.9 70.9 70.9 70.9	324*	119.3
	42.50 38.70 38.95 38.95 28.95 28.95 28.95 28.95 14.60 14.60		24.20
	.880 .8575 .8568 .8568 .8568 .8964 .8964 .8964 .8964 .8838 .8904 .8838 .8838 .8838 .8838	-	
	492 531 548 586 584 577 545 525 555 555		396
	.463 506 .498 542 .512 557 .512 557 .513 557 .511 587 .533 579 .533 579 .484 528 .484 528 .484 528 .417 455 .515 560		.374 412
.11	76.4 79.5 80.9 83.7 83.8 82.6 82.6 82.6 82.6	<u>م</u>	106.3
	36.23 34.60 30.41 30.41 26.10 19.90 19.90 15.96 15.96		23.37
-	.915 .925 .928 .929 .929 .918 .914 .914		195
	520 537 537 535 585 585 510 483 548		219
	527 543 536 536 575 575 575 575 575 510 549 510 549 549		ដ្ឋ
	. 483 . 491 . 491 . 533 . 534 . 487 . 487 . 442 . 504		200
11	80.3 81.1 85.1 85.3 86.6 85.3 85.3 85.3 85.3	ž	80.5
	8.8.8.8.8.9.9 8.9.8.8.8.9 8.9.8.9 8.9.9 8.9 8		16.18
	935 945 945 945 945 934 934 936 936 936		617 .
	5 (mub) 10 115 30 50 50 85 85 (tip) MR		5 (hub) 10

1 3 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	-
4 .513 1 .542 6 .550 6 .550 5 .596 7 .563 4 .521	
106.4 104.1 104.1 99.2 98.7 98.7 98.7	101. 105. 100.
29.44 29.44 29.58 28.70 21.50 18.54	17.46 15.28
.913 .922 .933 .933 .934 .936	.935 .929 .931
475 474 474 487 565 588 588 598 608 608	5694 5694 5694
545 535 535 535 535 609 620 620 620	619 530 595
. 500 . 480 . 540 . 540 . 540 . 573 . 573	. 573 . 486 . 549
119.3 117.5 111.7 105.5 104.9 105.0 106.0	106.6 111.3 107.1
24.20 23.58 25.00 22.60 22.60 19.30	18.50 15.08
86 86 86 86 86 86 86 86 86 86 86 86 86 8	. 912 . 870 . 895
328 328 103 122 123 123 123 123 123 123 123 123 12	150 254 254
412 374 329 231 157 105 124	153 152 256
374 339 297 208 141 084	.137 .136 .233
106.3 101.7 99.6 99.8 98.5 102.5 100.2	100.1 102.7 100.9
23.57 21.72 28.82 28.82 6.91 6.91 4.06	
786 786 785 785 786 7780 7780	. 725 . 725 . 744 538. 5 %
និន ឆ ឆ ឆ ឆ ឆ ឆ	222 . 725 221 . 725 222 . 744 70 = 538.5
នួននួននួននួន	ពនួន 🎽
200	.200 .200 .200 .200
80.5 83.3 85.1 85.1 85.1 85.1 85.3 85.1 85.3 85.1 85.3 85.3 85.1 85.3 85.1 85.3 85.1 85.3 85.3 85.3 85.5 85.5 85.5 85.5 85.5	22 22 22 04 2 22 22 04 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
16.18 14.25 14.25 16.15 10.15 10.15 10.15	7.52 ditions
	tp) $$
5 (Auth) 15 25 26 26 26 br>26 26 26 26 26 26 26 26 26 26 26 2	NR NR 1) inlet pl

571 582 582 635 603 557 557 538 486 538

2) Vm calculation is based on 3×10^{-1} day inlet plenum conditions 3) Circumferential reference position is TDC looking forward 4) Relative position of circumfrectial distortion screen is $210^{\circ} - 330^{\circ}$ 5) $\beta T^{2} = \tan^{-1} [\tan \beta T/\cos \epsilon]$

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TABLE 15.7

Disk Probe Station 7, 100% of Design Speed, $W\sqrt{\theta} = 173$ Rotor Inlet Circum ()rential Distributions

90- ^{6,} 7 31.45 30.95 30.78 30.78 24.46 20.80 17.90 11.60 14.60	V V m v V m
94.4	560 558 . 938

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	403	385	365	253	236	247	276	257	306	3 6 7			535	550
	445	1 09	384	269	256	257	280	300	309	312				564
	.405	. 372	. 348	242	230	. 231	. 252	.270	. 278	281			.508	519
2.34	64.7	70.2	71.7	70.2	67.3	73.9	81.0	82.0	83.9	73.1		3	104.7	102.9
	33, 80	28.20	25.12	14.63	11.48	10.20	10.25	10.70	10.70				29.90	29.25
	· 804	. 789	. 780	. 743	. 739	. 739	. 746	. 753	. 756	. 755			.924	616.
-	461	456	455	538	554	560	550	532	443	530	-	•	46)	474
	528	524	507	558	573	582	578	563	8	558			529	528
	.484	480	.463	.512	. 527	. 536	. 532	.518	438	.512			. 485	. 484
.504	60.7	60.5	63.8	74.8	75.3	74.4	72.2	70.8	67.2	71.9		324	119.3	116.0
	40.90	37.95	34.10	30°.60	26.50	23.70	21.65	20.75	16.90				23.70	23, 80
	088.	. 872	. 855	. 866	. 976	. 884	900.	906.	. 870	. 878			. 873	. 865
-	500	528	546	564	591	579	1 F 5	526	6 6	557	•		418	383
	513	538	554	570	593	580	543	528	19	560			9 1	165
	.469	.493	6 0 <u>9</u> .	. 524	.547	. 534	.498	.483	.421	. 515			.400	. 358
174	77.2	+ .,	BL.2	81.9	84.7	86.1	85.2	85.0	84.9	83.7		-767	108.2	103.9
	36.45	35.38	34.20	30.98	26.40	22.55	19.65	18.68	16.00				24.20	21.95
	.923	.927	.926	.921	₩c.	.938	.940	.946	- 917	166.			. 602	. 794
-	513	526	516	575	578	548	505	485	445	542			233	236
	519	529	519	577	579	543	506	485	5	543			253	237
	.475	. 485	. 475	. 531	. 53.	504	. 463	.413	. 1 06	96¥ .			.210	. 21.3
	81.7	83.3	84.6	86.2	86.4	87.7	87.0	87.2	65.1	86.3		2	92.8	92.9
	35.60	33.55	31.30	29.4S	х. З	2:.18	18.22	17.00	15.22				16.18	15.43
	016.	726.	. 925	547	1.8.	046.	.937	286.	136.	.960			. 136	. 736
	5 (thub)	10	15	8	8	r	2	8	95 (ttp)	MR			5 (brib)	19

				-	-		551 543				
							506 5				
ŗ.			-								
- <u></u>	-								~	66	
	29.90	29.25	29.30	28.60	24.96	22.40	1.20	16.90	14.95		
	.924	919.	.917	626.	. 935	926.	.936	.937	.930	. 934	
	16)	¥14	512	593	601	598	556	522	412	564	
	529	528	545	615	622	621	579	546	447	591	
	. 485	.484	500	. 568	.576	.575	.534	. 501	.407	.544	
324	119.3	116.0	110.0	105.5	105.2	105.8	106.5	107.1	112.9	107.3	
	23.70	23.80	25.35	25.93	22.95	20.48	17.85	10.50	12.75		
	. 873	. 865	. 864	. 899	.911	.928	.929	.920	.879	. 906	
	418	383	351	251	234	218	221	221	216	278	
	9 ‡	1 59	361	262	247	235	237	236	235	294	
	.400	. 358	.326	. 236	. 222	.211	. 213	. 212	.212	. 265	
.	108.2	103.9	103.0	106.5	108.8	111.7	110.5	110.5	113.2	108.4	
	24.20	21.95	19.70	12.47	9.94	8.90	7.64	7.40	7.70		8. 8.
	. 602	. 794	. 773	. 741	. 737	. 733	. 734	734	134	. 749	= 536.
•	233	236	24.3	247	246	233	267	273	250	248	F
	253	237	243	247	246	2,39	266	274	254	249	nef
	.210	.213	. 216	223	. 221	. 215	. 241	247	. 229	. 224	= 195
के	92.6	92.9	0°16	92.4	93. 7	95.0	95.0	95.2	100.3	94.2	å
	16.18	15.43	15.11	13.08	10.32	9.26	9.54	9.54	8.43		ditions
	. 136	. 736	. 136	- 73 6	. 733	н.	SH2 .	1.744	917.	. 737	num col
	5 (brub)	2	15	8	3	20	65	8	95 (tip)	MR	1) Intet plenum conditions: $P_{\alpha} = 195$

1) House presents the standard-day inlet plenum conditions 2) V_m calculation is based on standard-day inlet plenum conditions 3) C.rcumferential reference position is TDC looking forward 4) Relative position of circumferential distortion screen is 210° - 330° 5) $\beta \gamma^{\circ} = \tan^{-1}$ (tan $\beta \gamma / \cos \epsilon$)

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									Н	TABLE	E	15, 8												
					-	17.2		r Inle	t Cir	cam	lere	entia	Rotor Inlet Circumferential Distributions	ribut	ions	ť								
Circunferential	untia.l					NALU	Frome Station 2, 100% of Lesign	s ouau	5 100	Ă	2		igis	speed, <u>W</u>	≨ ri	<u>ه</u> ۲	= 167.2	7.2						
Position			21			-	_		31			•			z	5		-						
trads 2	P ₇ /P ₀	8	8	×	>	, H	P7/P0	L .g-06	90-91	×	>	,E	P7/P0	2.4-06	90-B7	×	-		P7/Po	90-J ¹ 7	-t1-06	7	>¦	5 <
5 (bub)	.933	30.45	93.2			481	946	00.IE	93.0	.449	492	491	.951	31.68	36.5	.460		502	.926	30.78	90.1	.428	170	470
9 :	306.	8 8 8 8	93.4				346	30.45	92.9 0.1	.468	512	511	. 552	30.95 20.95	87.7 87 e	190		220	. 936	31.20 30.80	90.06 89.98	.467	511	533
18	- 351	21.25	92.4				6 26 .	3 3 3	92.4	· 196	3	3 9	.949	27.90	87.9	208		200	.946	28.30	90.1	. 524	570	570
5	796.	8.2	92.7				8 7 6.	23.40	91.9	- 307	553	352	. 952 040	24.20	88.1	.511	556	556	. 948 946	24.48 20.85	90.3	. 527	547	573
5 8		19.46	•				3. I.	19.90 16.90	91.6 91.6	133	475 475	475	2. F.	20.35 17.28	1.60 89.9	. 443		182	. 945	18.00	90.0	461	507	507
8	956.	15.05	3 6.4				626.	15.75	91.6	.415	456	456	. 943	15.85	91.3	.420		. 091	. 945 966	16.90	90.4	. 446	437	499 7 × 1
95 (tup) N/R	545 746	13.40	98.2 93.7	. 373	411 512	407 511	.929 1943	13.60	92.5 92.1	. 172	516 516	402 516	616 [.]	14.38	92.7 88.8	067 - 181 -	525 525	4 Z 8	. 943	00.11	90.2	. 1 93	538	538
												•						•						
			쾨			•			77						204			-			234			
5 (hub)	.945	35.18	81. 5		513	507	. 935	36.20	78.4	.470		203	.879	38.45	60.7	.455	498	Te	. 810	31.78	67.7	304	423	162
91	116.	33.20	82.7		528	524	.933	34.55	79.9	. 482		517	.870	35.65	61.7	.453		137	801	28.15	73.2	.377	ij.	,
15	306.	31.65	84.0		22	519	100	33.38	81.0 22 -	497		535	. 85.7	32.40	66. 3 2	. 444		145	5 61 .	8.9	74.5		5	
R 5		8 1 R 1	59.1		5	8	26		82.7	• 514 2 = 0		222	. 395	29.62	0.01 78.5	019		107	. 763	15.92	76.2	312	345	335
2 2	- -	21,10	67.2			6.6 248	346.	9 9 9 9	86.3	.524			.875	22.25	75.9	503.		232	. 760	13.50	79.2	. 303	336	330
85	.945	.8.10	8e. 8		503	502	.946	19.30	85.5	.490		532	. 894	30.58	73	504	249	526	. 768	12.63	84.5	. 312	345	343
	- 942	16. 78 25. 28	87.6		2 :	Ę	¥.	18.18	85.5	24 -		212	9 5	19.86	60 3	- 435 1 4 4 4		151	175	11.28	89.3	8	327	327
MR (up)	946.	8.41	98° 0	₿. 161 -	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5		6X6.	ce cf	8 .2	6U.	199	251	92a		73.2	161	535		. 772		78.0	. 323	357	349
			훐						.						326						2			
5 (ttp)	. 761	13.82	97.9		9.1	283	.836	24.42	111.2	426			. 892	23.30	119.3	24.		448	.937	28.55 27 70	104.8	483	520 528	503 513
9 :		16.63	5.79		83	52	. 827	2. %	106.4	428 1					112.0	84		50	. 932	27.40	102.1	8 <u>8</u>	535	523
4 A	157.		97.5			122	768	15.20	109.4	305		12			107.2	543		Lin	.947	26.76	98.0	53	579	573
3	. 757	14.03	97.4		Ş	325	. 757	10.70	119.9	. 280		999			107.8	545		63	. 965 1963	22.60	5.7. 9.00	-514	<u>8</u>	55 S
2 :	12.	11.42	101.2		8	202	1 2 2 1	6.76	119.9	. 253					108.3	- 532			H. J	15.28	101.6	420	191	452
2 2		11.2X	 		3		192	3 5	119.A	523		5 8			112.3	4 88		3 53	.942	14.3	101.6	\$	443	434
Ĩ	162	10.03		ž.	3	8	159	6.50	119.7	802	8	202			119.7	324	88	11	. 933	11.92	105.8	616.	1	370
N	. 157		8 6.3		92 X	316	. 778		114.5	.317		610	.916	-	110.0	. 512		53	942		n., , , ,	10.	50	110

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1) Inlet plenum conditions: $P_0 = 1964$ psf, $T_0 = 539.5$ R 2) V_m calculation is based on standard-day inlet plenum conditions 3) Circumferential ref-rence position is TDC looking forward 4) RekUive position of curcumferential distortion screen is $210^{\circ} - 330^{\circ}$ 5) $\beta \gamma^{\circ} = \tan^{-1} [\tan \beta \gamma / \cos \epsilon]$

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					S Disk	tator I Probe	TABLE 16.1 Stator Discharge Circumferential Distributions Disk Probe Station 12, 70% of Design Speed, $\frac{W\sqrt{\theta}}{s}$	TA ge Ci n 12,	BLE Ircur 70%	TABLE 16.1 Circumfere 12, 70% of De	1 ential I esign (Distrib Speed ,	$\frac{W}{\sqrt{8}}$		= 129.8					
Circumferential Position	ential	-1	12		_		42°	1.,				<u>8</u>					10	102°		
unds 🕷	P ₁₂ /P ₀	90- 6 12	M	>	N N	P12/P0	90-b12	M	>	^E	P12/Po	90-1 ¹ 12	M	>	,E	P12/Po	90-b12°	×		e N
5 (bucb) 10	1.437	91.6 94.2	. 860 . 804	948 891	948 889	1.414 1.387	87.3 90.0	. 841 807	928 893 277	927 893	1.397 1.372 1.360	87.6 90.1 90.9	. 811 . 787 . 775	698 872 859	897 872 859	1. 393 1. 362 1. 344	92.1 94.0 94.8	.818 .782 . 76 0		907 867 842
SI 88 [1.250	r. 7	11.	857 793 70:	791	1.309	90.0 93.2 93.4	961 . 961 .	815 775	814	1. 304	93.8 83.8	. 721	801 749	799 748	1.280 1.245	94.9 95.0	. 694 . 649		770 723
8 E 8	1. 239 1. 244 1. 226	92.9 93.7 93.1	49 19 19	10/ 10/ 869	717 717	1.223	94.2	.652	709	724	1.230	93.9 95.5	.633	708 687	707 684	1.213 1.194	93. 3 94. 5	.614 .589 .74	688 664 664	687 662 646
6(ttp) 86	1.172	62.6 92.6	99 7 5	676	675 615	1.209 1.178	95.4 100.8 93.3	. 560 560 705	684 633 784	681 621 783	1.199 1.175 1.275	95.6 100.4 93.6	.590 .547 .685	6655 620 764	662 610 762	1.156 1.258	9.96 9.95	. 524 . 669		593 746
MR	1,284	93.5	.685	115	8.4	207 -T		8	5	2					-					
		1	281				162	3.,)		-		192*	54				21	222		
5 (haib)	1.387	88.5		878	877	1.379	91.6	. 746	835	834	1.322	89.0 61.3	.698 664	787 750	787 749	1.209 1.184	87.6 89.8	.546	626 594	625 594
16	1. 346 1. 338	91.0 91.2	. 756	841 832	841 832	1.320	94.0	.688	111	170	1.279	91.4	.656	740	740	1.178	91.2	.508	582 534	582 533
83	1.269 1.249	94.1 94.8	.697 .646	777 222	775	1.234	94.8 94.8	588	662	629	1.230	03.00 03.00 03.00	.571	644 644	642	1.149	92.4	.452	515	514
e 8	1.213 1.199	94.4 96.0	.607	681 661	679 658	1,197	94.9 95.9	.543	612 589	610 586	1.150	96.3	.486	553	550	1.124	90.5 20.5	. 406	164	464
90 25 (Har)	1.184	96. 1 100 3	. 565	639	635	1.164	95.9 95.7	. 497 . 444	565 507	562 504	1.139 1.131	96.2 96.2	. 465 . 448	53 1 513	528	1.117	90.5 90.5	. 358	449	449
MR	1.259	94.2	.660	139	737	1.246	94.6	.604	680	678	1.211	93.9	,572	647	645	l.149	91.4	. 455	519	519
		মা	252			-	282	211		-		312	24		_		ωI	342°		
5 (bub) 10	1.136	87.8 86. 7	474.	546	546	1.177	87.8 87.7	.557	638 663	638 663	1.315 1.308	90.4 92.3	. 741 . 729	829 815	829 815	1. 397 1. 388	87.6 89.1	.837	924 912	923 912
1 1 1	51.1	8	514	587	587	1.205	89.5	.581	661 642	661	1.315	92.8 93.9	. 731	814 794	813 793	1.370 1.333	90.0 91.5	. 76.1	891 841	891 840
38	1.170	92.4	909. 2009.	268 268	567	1.194	92.4	.555	626	626	1.293	93.7	.685	762	192	1.290	92.8	. /12	212	749
r 2	1.170	90.5 8.5	497	1 95	564	1.177	92.4 90.8	.530	599 583	599 583	1.275 1.259	91.1 91.8	. 663 . 643	719 817	611 5	1.240	94.0 93.4	.652	728	727
81	1.166	90.4	6.	246	246	1.160	90.8	2009	569	569	1.238	92.6 05 0	.616	693 611	692 608	1.211	93.5 96.2	.615 .582	691 656	689 653
(dri) ex	1. 155 1. 167	90.3 90.8	÷	517 565	517 565	1.156	90.8 91.1	.545	500 618	518 618	1.284	92.6	.681	760	760	1.295	92.5	. 720	661	662
1) Inlet 1 2) Vm c3	1) Indet plenum conditions $P_0 = 2012 \text{ psf}$, $T_0 = 534$ "R 2) V_m calculation is based on standard-day indet plenum conditions	ditions F is based o	o = 20	= 2012 psf, T _o standard-day i	To =	= 534 °R nlet plenur	n conditic	SUS												
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Relative position of circumferential distortion screen is 210°-330° $\beta^{\circ}_{12} = \tan^{-1} \left[\tan \beta_{12} / \cos \epsilon \right]$ ~, r_{m} calculation is based on standard-day inlet plenum condit 3) Circumferential reference position is TDC looking forward 4) Relative position of circumferential distortion screen is 2105) β^{*}_{12} = tan⁻¹ / tan β . /... Ser M.

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	×	710 670 652 610 570	. 512 . 498 . 455 . 581	•	.438 .451 .451 .438 .438 .395 .395 .395	. 383 . 360 . 403 . 403	- 706 - 687 - 687 - 687 - 687 - 687 - 687 - 687 - 685 - 495 - 495 - 478 - 478 - 478 - 581
102.	90- ⁶ 12	90.2 93.2 94.1 94.2	94, 6 93, 6 95, 4 93, 8	222	85.7 88.8 90.9 91.7 91.7 88.8		88. 90.99.99.98. 91.39.95.0 89.33.95.0 89.33.33.10 89.33.33.10 89.33.33.10 89.33.33.10 89.33.33.10 89.33.33.10 89.33.33.10 89.33.33.10 89.43.10 80.45.10 80.45.10 80.10 80.45.100 80.45.10000000000000000000000000000000000
	P12/P0	1.415 1.377 1.362 1.324 1.293 1.293	1.245 1.233 1.209 1.298		1.228 1.240 1.233 1.218 1.218 1.213 1.213 1.213	1.208 1.196 1.216	1.410 1.394 1.378 1.378 1.226 1.225 1.225 1.225 1.220 1.220
$\frac{\mathrm{trions}}{\delta} = 122.1$	N R	791 767 756 756 756 708 668 668	605 594 573 675		698 656 647 647 647 558 519 534 534	519	670 664 658 658 658 642 612 597 597 597 597 597 597 597
	>	791 767 756 756 710 670 617	607 596 575 377		698 658 647 611 560 522 534	519 501 580	671 664 664 659 645 645 613 613 590 590 575 636
$\frac{w}{\delta}$	×	.702 .681 .672 .630 .593	. 532 . 520 . 597		.612 .576 .576 .536 .536 .454 .454	. 448 . 506	. 588 . 588 . 588 . 588 . 588 . 588 . 588 . 588 . 588 . 588 . 588 . 588 . 588 . 588
TABLE 16.2 Stator Discharge Circumferential Distributions sk Probe Station 12, 70% of Design Speed, $\underline{W\sqrt{6}}$	90-012	89.6 91.5 94.1 95.0	95.0 93.8 93.8		89.4 91.5 91.6 94.3 95.7 91.0	91.0 92.2 92.7	87.5 91.2 93.2 93.5 94.9 88.0 88.0 88.0
esign	P12/Po	1.409 1.382 1.382 1.370 1.336 1.303 1.260	1.256 1.241 1.231 1.306		1.355 1.323 1.313 1.290 1.257 1.234 1.242	1.219 1.269 1.269	1.305 1.305 1.304 1.336 1.336 1.336 1.336 1.288 1.288 1.268 1.268 1.268
TABLE 16.2 e Circumfere 12, 70% of I	۲ H	804 774 762 7162 672 672 625	611 589 571 681	-	753 710 691 645 549 549 549	536 496 617	469 501 542 542 550 538 514 494 501 528
ILE rcun 70%	>	805 774 762 762 674 674	614 591 573 682		753 711 647 666 551 551	536 497 618	469 501 542 550 550 538 501 494 501 528
TAB e Ci 12,	×	716 687 617 617 632 597	. 536 . 515 . 498 . 603		.665 .627 .627 .611 .533 .533 .533 .482 .482	. 465 . 430 . 543	. 403 . 433 . 448 . 448 . 473 . 473 . 481 . 470 . 446 . 446 . 426 . 426
TAB: Stator Discharge Cir Disk Probe Station 12,	90-fi ₁₂	88.5 91.6 94.4 94.5	95.1 94.3 93.5 93.5	1 E	89.5 93.9 93.9 93.9 92.6 82.6	92.5 94.1 54 54	88.9 89.4 90.7 90.7 90.7 90.7 90.7 90.7
tator D : Probe	P12/Po	1. 418 1. 393 1. 378 1. 339 1. 339 1. 269	1.260 1.241 1.230 1.312	_	1.395 1.359 1.344 1.311 1.280 1.281 1.239	1.287	1.187 1.211 1.221 1.221 1.243 1.243 1.249 1.232 1.224 1.221
S: Disk	v.m	818 774 742 742 658 658	539 551 672	-	775 747 735 688 688 654 593 593	580 565 656	370 467 504 504 505 518 518 518 518 518
	>	818 775 744 741 701 660 611	600 581 552 673		775 748 736 690 596 596	581 567 659	370 370 504 505 518 518 518 518 515 518 515
	M	.727 .687 .658 .658 .621 .583	523 504 478 593		.687 .663 .653 .610 .579 .523 .523		.317 .343 .405 .405 .439 .437 .457 .450 .456
12	90-B12	89.9 92.1 93.2 94.1 95.4	94.0 92.8 93.6	132.	89.7 91.5 93.8 94.0 95.6	94.2 94.2 93.7 252*	86.5 86.8 91.1 88.5 90.3 88.5 88.5 88.5 89.9
ent.al	P12/Po	1.450 1.404 1.376 1.342 1.310	1.257 1.245 1.235 1.317		1.403 1.375 1.363 1.327 1.327 1.253 1.253	1.242 1.231 1.300	1. 146 1. 159 1. 159 1. 128 1. 228 1. 228 1. 224 1. 224 1. 244 1. 244
Circumfer en tl Position	Span	5 (buib) 2.5 30 30 30 30 30	85 96 (ttp MR		5 (bub) 15 38 36 36 38 56 38	90 95 (tip) MR	5 (hub) 15 30 30 50 70 85 85 85 85 MR

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739 7756 644 644 535 535 523 523 523 523

799 7756 688 688 688 597 573 573 573 573

1.24

794 772 755 690 631 596 558 558 558 558 658

795 772 692 692 634 558 558 558 558 558

506 521 521 470 470 454 454 414 418 418

507 521 521 526 470 470 444 444 444 444 418 418

1) Inlet plenum conditions $P_0 = 2020 \text{ psf}$, $T_0 = 525.2 \text{ "R}$ 2) V_m calculation is based on standard-day inlet plenum conditions 3) Circumferential reference position is TDC looking for ward 4) Relative position of circumferential distortion screen is $210^{\circ}-330^{\circ}$ 5) $\beta^{\circ}_{12} = \tan^{-1}$ [tan $\beta_{12} / \cos \epsilon$]

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					01	stator]	TABLE 16.3 Stator Discharge Circuraterential Distributions	TA ge C	TABLE Circur	16.3 Diferer	3 ential	Distri	butio	S					
Circunferential Position	entia.l	-	12		Disl	k Prob	Disk Probe Station 12, 70% of Design Speed, $\frac{W\sqrt{\theta}}{\delta} = 111.0$	n 12	, 709	% of	Design	Speed	>∞ N	[0]	.111.0	0	10	102"	
K Spen	P ₁₂ /P ₀	90-Å12	×	>	, <mark>1</mark>	P ₁₂ /P ₀	90-1 ¹ 12	×	>	E A	P ₁₂ /P ₀	90-1312	۶	>	. <u></u>	P12/P0	90-t ¹ 12	×	>
5 (hub) 10	1.460 1.421	88.5 91.2	.650 .613	739 689	739 699	1.423	87.8 90.5	.629 .610	715 694 692	715 694 692	1.418 1.398	88.1 90.6	.628 .613	715 697 632	714 697 692	1.416 1.383	88.5 91.4	.641	728 694
388	1.341	91.9 92.0 93.3	.528 .474	604 545	241 53	1. 346 1. 346	92.4 93.9	- 544 - 490	621 561	560 560 560	1.355	94.4	.562	579 579 579	639 578 578	1.343	92.0 92.0 94.7	.559	636 586 586
2 2 8	1. 204 1. 242 1. 239	8.68 89.88 89.88	- 419 - 386 - 374	487 452 440	480 452 440	1.2.4 1.248 1.239	91.6 91.6	.413 .397	463 463	480 480 463	1.270	91.0 89.3	.447 .438	519 510	519 510	1. 296 1. 278 1. 273	93.4 91.0 88.5	.458 .469 .467	574 545 544
95 (tip) MR	1.235	89.8 91.7	. 363	426 576	426 576	1.235	91.6 92.2	. 509	456 584	456 583	1. 264 1. 324	89.3 92.1	. 443	517 603	517 603	1. 268 1. 322	88.4 92.1	. 448	522 611
		132	શ્ચ		-	_	162			-		192*	•				222*	ŝ	
			;					-					-		-		:		!
5 (bub) 10 15	1.414 1.386 1.371	88.9 90.9 9.06	. 606 . 606 . 592	717 689 674	717 689 674	1.409 1.372 1.359	89.1 91.6 92.5	.617 .579 .561	703 661 640	703 661 640	1. 373 1. 353 1. 342	89.7 91.2 91.2	. 565 . 544 . 533	649 624 612	649 624 612	1.204 1.263 1.267	85.0 87.8 90.6	. 322 . 411 . 411	376 476 476
8 1	1.347	92.2 05 0	. 557	635	634	1.329	93.5 94 A	.526	600 559	599 551	1.314 1.293	91.3 93.6	.496	569 534	569	1.265	90.6 41 6	.404	466
20	1.306	92.9	20.	8 28 28	280	1.294	93.1	.474	547	546	1.285	93.6	.445	515	514	1.261	91.6	. 385	446
18 9	1.294	91.7	-488 171	566 549	565 548	1.287	90.06	.462	536 524	536	1.284	91.4 91.4	.441	51 499	514 499	1.261	98.1 88 1	. 386	450
(cp) 26	1.281	91.7	.468	<u> </u>	545	1.271	89.9 89.9	. 433	504	504	1.267	91.4	421	493 493	493	1, 243	89.4	. 355	415
	1. 328	F-76	200.	110	010	10.1	P		2	-				4	-	102.1	1.00	000.	0 #
		252*	ţ.				282			-		312	۹.,		-		342	ŝı;	
5 (bub)	1.222	87.0	. 350	409	408	1.209	69.0	645.	407	407	1.324	87.2	. 522	601	600	1.422	88.2	.625	111
10	1.250 1.266	87.0 89.1	. 392	455 484	454 484	1.237 1.250	89.0 91.3	.409	454 471	454 473	1.325 1.327	91.2 93.7	. 523	600 596	600 595	1.407 1.385	90.1 91.0	. 589	692 671
89	1.269	90.3	419	483	483	1.271	90.2 60.4	.430	495 520	495 520	1.357	92.4 91 5	. 335 518	611 59%	611	1.326	93.0	.519	593
381	1.291	92.0	4	211	210	1.268	90.7	. 417	484	i ž i	1.308	94.5	470	543	15	1.245	93.0	. 399	463
88	1.278	6.16 91.9	.425	482	482	1.264	96. 8	-406 -111	180	477	1.295	87.8	.448	522 522	522	1.213	93.0	197 192	422
95 (tip) MR	1.270 1.275	91.8 90.6	. 402	470 488	470 487	1.267 1.268	96.8 91.5	.410	431 489	477 488	1.290 1.326	87.7 92.2	. 431 . 499	504 574	503 574	1.209 1.302	92.3	. 340	399 560
 Inlet pl Vm cal 	1) Inlet plenum conditions $P_0 = 2037$ psf, $T_0 = 529.3$ "R 2) Vm calculation is based on standard-day inlet plenum conditions	ditions F	o = 20	N psf	, To =	529.3 [•] F	t n conditio	SC SC											
	Circumferential reference position is TDC looking forward Relative position of circumferential distortion is 210°-330°	referenc	e posit imferen	ion is tial d	TDC	looking f ion is 21	orward •-330	l											
5) ^β •12 =	$\beta_{\bullet}_{12} = \tan^{-1} \left[\tan \beta_{12} / \cos \epsilon \right]$	a B12 /cc	s e]																

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TABLE 16.4

Stator Discharge Circumferential Distributions Disk Probe Station 12, 90% of Design Speed, $\frac{\sqrt{\theta}}{s} = 164.8$

Curcumforcential Pountion Span 5 (butb) 10 10 10 10 10 10 10 10 10 10 10 10 10	P ₁₂ /P ₀ 1.481 1.570 1.563 1.563 1.563 1.476 1.476	90-812° 93.8 92.8 91.3 91.3 90.2 91.3	42° M 1.054 1.105 1.027 1.027 1.027 1.027 .938 .838	V 1022 1161 1205 1124 1091 1035 1000 979	Vm 1019 1123 1123 1123 1034 1000 979	P ₁₂ /P ₀ 1.520 1.547 1.642 1.575 1.575 1.492 1.448	90- ^A 12° 95.6 93.1 91.8 91.8 91.3	72° M 1.036 1.036 1.105 1.036 .989 .958 .958	V 1094 1139 1197 1125 1082 1082 1050 1050 983	Vm 1134 1134 1195 1195 1089 1081 1081 1081 1050 963	P12/P0 1.524 1.528 1.538 1.486 1.444 1.444	$90 - \frac{\beta_{12}}{2}$ 95.4 91.9 91.9 92.6 91.2 92.4 91.2	132° M 1.0/3 1.047 1.100 1.030 1.030 .960 .965 .894	V 11110 11148 11195 11195 11060 10066 10006 10006
(ttp)	1.426	94.8	.807	116	913	1.404	96.1	.807	913	908 120	1.390	96.9	. 796	206
8	1.527	1.22	. 968	AV.01	1069	1.523	93.0	. 980	1077	10/15	1.485	92.9	. 559	1062

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11105 11145 11192 11059 999 982 982 982 900

28

		1011	1100	1167	1111	1067	1002	985	943	875	1046
		1012	1100	1168	1112	1667	1002	985	943	880	1046
		. 895	066.	1.067	1.014	.968	. 901	. 878	. 832	. 768	.942
		92.3	91.3	91.3	91.5	90.6	90.6	91.3	90.7	96.0	91.4
		1.489	1.547	1.608	1.602	1.587	1.512	1.489	1.438	1.398	1.541
-	······································	648	724	806	817	793	786	161	796	774	161
		649	726	807	817	795	786	798	796	774	161
000	707	.548	.619	. 696	. 713	.693	. 685	.694	.691	.668	.687
с	41	88.0	86.1	88.1	90.5	93.6	9'i6	87.9	87.8	90.6	90.6
		1.136	1.204	1.290	1.305	1.296	1.297	1.318	1.330	1.327	1.296
		940	960	1017	696	904	841	843	812	753	903
		940	9 61	1017	696	905	843	844	814	762	904
		. 819	. 843	.904	. 862	. 799	. 739	. 737	. 706	. 656	. 795
••		89.4	58.0	90.1	91.4	91.8	94.0	92.5	93.9	98.9	92.4
		1.358	1.371	1.467	1.420	1.359	1.314	1.319	1.302	1.271	1.361
		5 (hub)	10	15	8	50	20	85	96	95 (ttp)	MR

192°

1) Inlet plenum conditions $P_0 = 1968$ psf, $T_0 = 536.2$ 2) V_m calculation is based on standard-day inlet conditions 3) Circumferential reference position is TDC looking forward 4) Relative position of circumferential distortion screen is 210°-330° 5) $\beta^{-}_{12} = \tan^{-1} [\tan \beta_{12} / \cos \epsilon]$

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Stator Discharge Circumferential Distributions Disk Probe Station 12, 90% of Design Speed, $\underline{W\sqrt{\theta}}$

Circumfemential	Hal							Ì	(~	-= 156.2				
Position		•	42		-			<u>12</u>		>			132		
🔏 Span	P12/P0	90-6 ₁₂	W	>	V _m	$\frac{P_{12}/P_{0}}{P_{0}}$	90- ⁵ 12	M	>	V _m	P_{12}/P_0	90-b ₁₂	M	^	۲ ۳
(dud) 2	1.431	89.5	.714	830	830	1.451	89.2	. 732	847	847	1.484	89.4	. 732	846	846
10	1.576	86.1	.824	942	940	1.534	86.5	. 802	915	914	1.519	87.3	. 767	881	880
15	1.855	89.7	.873	986	686	1.628	89.8	. 856	968	968	1.617	88.8	. 830	943	64 3
8	1.600	90.0	. 840	950	950	1.583	89.9	.834	941	941	1.570	91.0	. 791	901	106
50	1.543	89.7	. 777	885	885	1.555	89.7	. 787	895	895	1.523	91.4	. 745	855	855
70	1.482	93.1	. 715	824	823	1.483	92.9	. 720	829	828	1.466	93.7	.690	801	800
85	1.489	91.3	. 715	830	830	1.499	90.7	. 725	840	840	1.486	92.0	. 699	817	816
06	1.464	91.7	.687	803	802	1.487	91.3	. 707	824	823	1.478	92.1	.687	808	807
95 (tip)	1.440	91.9	.662	778	778	1.442	94.0	. 664	780	778	1.430	94.0	. 644	762	192
MR	1.532	90.7	. 769	882	882	1.531	90.8	. 770	882	882	1.516	91.6	. 739	853	853
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		-1	192°				~~!	282		<u></u>			342°		
5 (bub)	1.430	90.2	.620	730	730	1.269	89.6	.437	523	523	1.446	89.6	. 688	803	803
10	1.480	90.1	.652	764	764	1.307	89.6	.479	570	570	1.529	88.1	. 752	867	866
15	1.536	90.6	. 696	808	808	1.332	90.7	.507	600	599	1.592	88.6	. 794	606	606
30	1.494	93.1	. 658	763	762	1.382	89.4	.551	644	644	1.596	88.6	. 793	901	901
50	1.475	93.2	.638	740	739	1.398	92.6	. 558	653	652	1.523	91.5	. 727	833	833
70	1.440	94.9	. 596	200	269	1.412	92.6	.575	674	673	1.418	95.0	. 635	739	736
85	1.438	91.9	. 591	669	669	1.407	92.6	.568	670	699	1.345	91.3	. 568	699	699
06	1.460	91.9	.604	715	715	1.352	92.7	.512	609	608	1.317	89.2	. 537	638	638
95 (tip)	1.439	92.0	. 590	101	101	1.319	89.8	. 468	559	559	1.298	89.3	.513	611	611
MR	1.469	92.7	.630	737	736	1.379	91.5	. 544	640	640	1.484	90.8	. 702	811	811
1) Inlet ple	1) Inlet plenum conditions P _c = 1977 psf.	MS P. = 19		T = 536.		_				-					

 V_{m} calculations is based on standard-day inlet conditions

Circumferential reference position is TDC looking forward

Relative position of circumferential distortion screen is 210*-330*

 $\beta^{\circ}12 = \tan^{-1} [\tan \beta_{12} / \cos \epsilon]$ ର ନ କ ଜ

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			> ⁸	1260	1246	1206	1138 1066	1014	986	909 1130			992	952	116	836	767	757	770	720	825		
			>	1267	1252	1211	1147	1018	066	909 1136			992	952	913	839	769 769	757	770	721	826		
		102 •	×	1.147	1.133	1.100	1.032	. 898 898	. 868	.788 1.018		, N	. 858	.819	.782	. 720	.660	.646	.656	.610	. 708		All
		21	90- ^β 12	95.7	95.8 97.6	95.6	97.1 07 2	9.16 91.8	93.6	91.0 96.0		222	91.7	91.8	93.7	94.6	94.2	91.0	88.4	88.4	93.0		342
			P ₁₂ /P ₀	1.838	1.779	1.643	1.564	1.472	1.453	1.420 1.585			1.444	1.394	1.364	1.302	1.248	1.243	1.262	1.244	1.295		
	.2	-	۴ ۲	.			<u> </u>			904 1096	-				1166		·	_				•	•
	=178.2		>	1217	1223	1165	1092	10.09	960	909 1098			1180	1223	1168	1129	1058	126	939	882	1057		
	tions $\frac{W\sqrt{\theta}}{1}$	^{72. 0}	M	1.101	1.112	1.061	. 9R2 292	. 992 1892	. 839	.787		192 •	1.050	1.102	1.043	1.011	939	. 851	. 817	.759	.936		312.
	ributi eed.	••	90-h12	94.4	93.6 29.3	92.2	94.6	93.2 92.0	92.5	95.8 93.5		¥	93.7	92.2	93.3	91.9	92.5	5.06 50.5	91.1	96.5	92.3		21
	rcumferential Distribut 100% of Design Speed,		P12/Po	1.720	1.762	1.718	1.600	1.523 1.510	1.462	1.430 1.608			1.575	1.593	1.565	1.529	1.481	1.414	1.397	1.358	1.475		
9.	rentia f Des	_	>#							906 1094	-	<u> </u>	1246	1234	1220	1195		1000	386	893	1107	,	-
Е 16	umfe) 00% o		>							909 1095					1229								
TABLE 16.6	Circ 12, 10	왕	×							.785 .976		51			1.112				. 859				.
-	Stator Discharge Circumferential Distributions Disk Probe Station 12, 100% of Design Speed, \underline{W}	4	90- ¹³ 12	53.6	93.5 93.5	92.1	9.16 81.0	92.6	91.4	94.9 93.1		162*	95.7	95.8	96.9	6.96 1	9.76	97.0	92. 8	90.6	95.9		282
	r Disc obe St	_	P12/P0	1.6¤§	1.775	1.750	1.567	1.500	1.461	1.437 1.613		1.755	1.687	1.661	1.599	1.519 1 A65	1.458	1.448	1.394	1.540			
Stator	Stato sk Pr		, <u></u>							1124					1210								-
	Dis		>							885 1128 1				-	1213		•••		•.				
		8	W	1.118	L. 118 L. 109	1.109	1.041 935		. 829	.765		132.	1.102	1.109	1.099	1.050	170.1	906	.878.	. 818	556.		252
		~1	90- ^b 12	94.9	94.9 96.1	94.1	98.2 94 7	93.3	93.4	90.5 95.0		11		93.6	94.0	82.2	36. 1 93. 1	93.1	91.9	95.7	93.2		89 87
	2	1	P12/Po	1.738	1.739	1.744	1.589	1.451	1.418	1.386 1.597			1.698	1.719	1.708	1.666	1 519	1.522	1.503	1.464	1. 596		
		Position	Kspan	5 (fmth)	10 1	8	50	85	8	55 (Ly) NG			5	92	15	8	20	: -8	96	96	MR		

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	1083 11132 11150 11167 11133 999 919 919 8159 11077
	1083 1151 1151 1151 1151 1153 1167 985 919 856 81078
342	.952 1.004 1.025 1.054 1.016 .384 .384 .384 .384 .384 .385
φļ	91.2 91.2 91.0 91.0 91.0 91.3 91.3 91.3 91.3
	1.631 1.673 1.702 1.797 1.713 1.713 1.570 1.534 1.646 1.646
-	1120 1093 1137 1136 1136 1136 1095 10095 10095 1108 820
	1124 1099 1144 1142 1137 1137 1098 1019 920 1113
312.	1.001 .975 1.024 1.024 1.024 1.022 .979 .896 .396
91 1	96.2 96.2 96.2 96.1 96.1 9.6 9.7 9.7 9.7 9.7 9.7 9.7 9.7 9.7 9.7 9.7
_	1.485 1.484 1.484 1.561 1.561 1.581 1.586 1.586 1.586 1.477 1.555 1.477
_	863 902 902 901 895 873 835 835 835 835 835 835 835
	864 904 918 918 885 873 873 873 873 873
282	.732 .772 .797 .793 .793 .779 .779 .779 .779 .775 .775 .775
8	86.9 85.8 86.3 86.3 89.6 87.1 87.1 89.6 87.1 89.6 89.6 89.6 89.6
	1. 268 1. 332 1. 361 1. 364 1. 364 1. 364 1. 368 1. 368 1. 368 1. 368
	673 651 651 651 808 808 808 816 738 738 738
	673 662 698 698 698 698 698 794 738 738 738
22	. 546 . 546 . 546 . 569 . 696 . 692 . 692 . 676 . 676 . 673
Ři	89.0 .563 673 87.8 .546 6.2 87.7 .546 6.2 90.3 .546 6.3 90.3 .695 800 90.3 .692 800 90.3 .676 734 90.3 .676 734 90.3 .676 734 90.3 .676 734 90.3 .676 734 90.3 .676 734 90.3 .676 734 90.3 .676 734
	5 1.12 15 1.11 15 1.15 50 1.15 70 1.28 85 1.28 99 99 1.28 90 1.28 90 1.28

1) Inlet plenum conditions $P_0 = 1946 \text{ pst}$, $T_0 = 538.5$ "R 2) V_{m} calculation is based on standard-day inlet plenum conditions 3) Circumferential reference position is TDC looking forward 4) Relative position of circumferential distortion screen is 210°-330° 5) $\beta^{\circ}_{12} = \tan^{-1} \left[\tan \beta_{12} \right] (\cos \epsilon)$

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		N R	1228 1156 1156	963 886 888	864 805 995		712 713	626 624 628 618	590 590 570 570 539		972 1020 1056 1053 956 831 831 831 791
		^	1231 1210 1164	965 891 890	865 905 998		712 714	654 654 628 618	594 570 639		972 972 1056 1053 956 876 878 878 878 808 808
		×	1.103 1.084 1.084	. 839 . 765 . 758	. 731 . 676 . 868		596	548 548 517	. 491 . 485 . 468 . 533	\$ 1	. 835 . 835 . 885 . 829 . 829 . 680 . 680 . 680
	102	90-9• <u>12</u>	94.3 96.9 95.9	96.2 95.7 82.7	91.9 94.4	222		9.06 8.06 9.08	90.8 90.8 90.7 90.5	342	88.88 9.19 8.69 8.67 8.63 8.63 8.63 8.63 8.63 8.63 8.63 8.63
		P12/Po	1. 832 1. 797 1. 774 1. 681	1.623 1.545 1.549	1.523 1.463 1.625		1.476 1.474 1.464	1.431 1.415 1.408	1.389 1.389 1.379 1.422		1.609 1.688 1.728 1.754 1.754 1.566 1.566 1.467 1.467
=173.1		V12	1003	896 888 888	850 806 972		823 879 86	801 108	706 699 679 783	-	760 758 841 841 840 822 777 764
	Q V	>		888 888 888 888 888 888 888	851 809 972		823 680 966	822 802 733	701 681 784		761 758 843 841 841 777 764
bution d, <u>W</u>	-22	×	.872 1.007 1.013			•.1	.692 .747 .755	. 700 . 680 . 615	. 588 . 578 . 360 . 660	• .	.639 .639 .639 .697 .697 .697 .681
Distri 1 Spee		90-fe 12	90.9 90.9 90.3	90.9 94.1 91.6	92.5 94.9 91.7	192*	90.4 89.1 ev a		93.9 93.9 92.9	315	87.7 82.6 83.0 990.1 890.0
7 ential Design		P12/P0	1.651 1.779 1.783 1.733	1.642 1.566 1.568	1.527 1.483 1.639		1.558 1.643 1.630	1.591 1.582 1.582	1. 481 1. 475 1. 447 1. 549		1. 453 1. 467 1. 589 1. 588 1. 5888 1. 5888 1. 588 1. 5888 1. 5888 1. 5888 1. 5888 1. 5888 1.
TABLE 16.7 Circumfere 12, 100% of I	-	Å	1026 1153 1161 1130	1017 943 925	893 855 1022		1107 1033	919 856 801	799 778 722 890	-	698 771 771 794 824 824 661
ABLE lircu		•	1028 1154 1162 1130	1017 943 925	894 857 1022		1004	50 00 00 00 00 00 00 00 00 00 00 00 00 0	800 778 892		698 771 771 771 787 664 661
rge C m 12	3	×	. 893 1.024 1.032 1.008	168. 618.	721 882	ŝti	178.	. 736	. 674 . 653 . 602 . 764	Sat	.579 .655 .655 .676 .676 .676 .550 .550 .550
ischa: Static	441	90-f*12	91.3 91.2 91.2 89.8	91.4 91.9 91.4	91.4 91.4	162	91.8 92.0	96.5 4.3 4.5 0.4	92.0 92.0 91.9 93.6	282	90.2 91.4 91.2 91.2 89.9 89.9 89.9
TABLE 16.7 Stator Discharge Circumferential Distributions sk Probe Station 12, 100% of Design Speed, $\underline{W \sqrt{\theta}}$		P12/Po	1.634 1.736 1.751 1.756	1.650 1.579 1.569	1. 524 1. 486 1. 641		1.777 1.730 1.709	1.570 1.570	1. 507 1. 489 1. 430 1. 590		1. 404 1. 448 1. 481 1. 513 1. 553 1. 555 1. 556 1. 586 1. 391 1. 391
St. Disk	_	H H	1136 1138 1115 1115	5 8 8 9 8 8	817 817 882	-	972 1065 1046	88 55 88	858 832 858 838 838		273 2555 2555 2555 2555 2555 2555 2555 2
-		•	1197 1142 1119 1070	56 56 58 58 58 58 58 58 58 58 58 58 58 58 58	861 995		972 1056 1046	986 988 888	855 833 796 928		273 255 713 829 829 829 829
	ă l	×	1.065 1.008 .987	. 823 . 769 . 753	. 723 689 . 861	Š 1	. 840 . 825	962 903	. 720 . 696 . 661 . 797	• .	.227 .208 .208 .602 .602 .706 .618 .602 .706
	-1	21 4 9 9	8 8 8 8	7 7 7 7 7 7 7	91.0 89.4 93.3	<u>8</u>	89.0 88.7 8.0	8 8 8 9 4 4	93.0 93.4 91.7	282	8.8.9.1.5 8.9.9.2.5 8.9.9.2.2.5 8.9.9.6 7.6.9.8 8.9.6 8.9.6 8.9.6 8.9.6 8.9.6 8.9.6 8.9.6 8.9.6 8.9.6 8.9.6 8.9.6 8.9.6 8.9.6 8.9.6 8.9.6 8.9.6 8.9.6 8.9.6 8.9.5 8.9.5 8.9.5 8.9.5 8.9.5 8.9.5 8.9.5 8.9.5 8.9.5 8.9.5 8.9.5 8.9.5 8.9.5 8.9.5 8.9.5 8.9.5 8.9.5 8.9.5 8.9.5 8.5 8.5 8.5 8.5 8.5 8.5 8.5 8.5 8.5 8
विंग्		P12/Po	1.627 1.815 1.813 1.779	1.666	1.570 1.524 1.689		1.642 1.758 1.761	1.702 1.649 1.558	1. 556 1. 552 1. 629 1. 629		1.211 1.200 1.215 1.312 1.495 1.495 1.641 1.641 1.641
Circumferential	Position.	A Space	5 (Bub) 10 15 30	83 5 83 (82 (Up) 84 (D)		5 (bub) 10 15	838	85 90 95 (tip) MR		5 (frub) 10 25 26 26 26 26 26 26 26 26 26 26 26 26 26

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1) Inlet plenum conditions $P_0 = 1955 \text{ psf}$, $T_0 = 536.8$ °R 2) Vm calculation is based on standard-day inlet plenum conditions 3) Circumferential reference position is TDC looking forward 4) Relative position of circumferential distortion screen is $210^{\circ}-330^{\circ}$ 5) $\beta^{\circ}_{12} = \tan^{-1}$ [tan β_{12} /cos ϵ]

					10	TABLE 16.8 States Discharme Circumferential Distributions	nohon	TAJ TAJ	TABLE 16.8	16. 8 Jerei	ntial I	Distril	outior	S						
				н	jisk]	Disk Probe Station 12, 100% of Design Speed,	Statio	ве сч	100%	of D	esign	Speed	$\frac{W\sqrt{\theta}}{\sqrt{\theta}}$	0	=167.2					
Circumferential Position	otial		• 21		•		4	5		-		- 1	72	0	_		102	5 1		
Span	P12/9	90-8° 12	×	>	>8	P. /P	90-fr 12	×	>	> ^{fi}	P12/P	90-6°	X	>	> ^E	P_12 /P	90-b° 12	X	>	> #
			200	2001		1 769	2 2	659	970	696	1.701	87.3	. 823	956		L. 847	92.1	.995	1131	1130
5 (000) 10	1.631		.857	966	972 975	1.832	88.3	128.	1007	1002	1.866	88.9	.881		_	1.791	92.2	.915	1050	1049
15	1.861	26.5	944	986	626	1.831	88.3	. 872	1008	1008	1.807	89.5 20.5	. 884	1014		1.781	93.9 04 1	, 887 843	1020	1018 966
8	1.795	92.3	.774	903 772	903 772	1.797	8. 8 8	. 825 736	954 861	954 861	1.710	89.5 90.5	.788		915	1.666	93.9	. 772	897	895
8	1.631	1.16	554	699	699	1.593	93.0	. 659.	182	781	1.854	92.0	.735			i.641	<u>8</u> 2.5	.743	873	872
85	1.440	91.2	663	612	612	1.525	91.5	609*	734	134	1.634	89.4 60 7	.718			1.636 1 619	8.06 8.06	.728	866 849	992 615
90 21	1.420	91.1	024.	579	579	1. 4 91 1. 469	91.6 91 ƙ	. 574	697 674	697	1.601	88.7	.685	823	_	1.561	89.8	.662	962	962
(dr) an	1.412	91.7	698	8 8	38	1.679	90.B	.743	874	874	1.703	90.0	. 786			. 692	92.7	193 .	934	933
		-	3		-		162*	*				<u>ମ</u>	192.		-		222			
- Auto	1 670	5	706	030	000	1.792	90.7	. 837	975	975	1.625	89.7	.678	608	-	1.442	87.9	.452	551	550
9	1.757	9.99 9.99	88	978	978	1.751	92.9	. 199	332	931	1.674	90.7	101.	200		1.493	88.1	203.	609	608
15	1.747	89.8	. 839	226	972	1.730	92.7	.785	516	916	1.659 1.659	8.8 8.8	. 696 667	790		1.507	88.0	.516	620	619
8 8	1.728	0.9 8	.813	5	2	1.636	93.4	686	810	808	1.545	92.6	.664	786		1.496	88.1	. 502	604	603
8 8	1.644	86.2 8	727	38	28	1.570	93.3	889.	755	754	1.573	92.9	909.	728		1.499	88.1	503	608	608
3	1.639	92.7	.710	854	853	1.559	91.1	.619	141	141	1.546	93.0 0° 1	. 575	699 607	698 693	1.469	0.88 9.78	.461	200 267	266
96	1.617	93.0	89 [.]	7 88	833 513	1.546	91.1	.603	731 679	131	1.518	93.1 93.1	. 553	929 676		1.459	87.8	444	546	546
as (dp) NUR	1. 573 1. 683	90.9	.766	28	206	1.639	86.7 86.7	.698	826	825	1.607	92.3	.640	765	—	1.493	88.0	.497	602	601
					•															
		8	252*		-		8	282		-		191	312.				38 78	.		
5 (h ub)	1.277	8.2	202	249	249	1.428	90.9	. 516	626	626	1.530	91.0	. 591	602		1.657	87.7	. 724	855	855
10	1.272	82.8	.218	268	267	1.473	92.1	. 559	672	672	1.541	91.0	. 608	726	726	1.755	87.8	.788 .788	210	516
នរ	1.289	8.8	.257	316	315	1.480	93. 4	. 563	675 604	674 894	1.681	91.2	693	817		1.738	88.6	.756	188	881
3 3	1.575	57 212	208 208 208	5 I I	212	1.568	92.8 92.8	515	726	726	1.698	92.1	.688	815		1.593	89.5 00	.641	760	760 504
20	1.685	91.1	.681	807	807	1.600	95.8	648	11.1	767	1.700	ດ. ເ	.676	801 775		394	85.7 95.7	.457	8	558
8	1.733	91.2	8 i	22 I	836 836	I. 495	e. 8	. 579	101	691	1.618	9.96 9.76	615	151		1.384	99.66	.435	536	529
S Tin	1.734	87.1 95 0	201.	8	2	1.229	0.08		476 476	476	1.612	92.7	. 599	732		1.375	99.6	.422	223	515
Ì	1.603	90°9	617	122	i &	1.523	93.5	583	704	203	1.656	91.9	.661	789		1. 591	90.3	.650	•	•••
 Inlet plenum conditions P₀ = 1964 V calculation is hased on stands 	Inlet plenum conditions P ₀ = 1964 V caleniation is hased on standa	ditions . is hased	P ₀ = 19	964 ps pdard-	f, To : day in	psf, T ₀ = 539.5 °R rd-day inlet plenum conditions	R m condi	tions												
					i		•													

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2) V_{m} calculation is based on standard day interpletum continues 3) Circumferential reference position is TDC looking forward 4) Relative position of circumferential distortion screen is 210°-330° 5) $\beta^{*}_{12} = \tan^{-1} \{ \tan \beta_{12} / \cos \epsilon \}$

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TABLE 17.1

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Stator Discharge Circumferential Distributions Temperature Rakes 70% Speed

								,	•				
10 10		Circle	prestia	Positio	g								
		5	. 93	.9 8		146*	176	206	236	266	296	326	8 8
	•	ļ	1	l			l	l					
WV = 12	: 129.8	T ₁₂ /T ₀ T ₁	۲° ۲°	T12/T6	T12/T6	T12/T0	T12/T6	$^{T_{12}/T_{0}}$	T_{12}/T_{0}	T_{12}/T_{0}	T_{12}/T_{0}	T_{12}/T_{0}	$\frac{T_{12}/T_{0}}{T_{0}}$
											ł		
	(herba	1.1307	1199	1,1173		1.1138	1.1027	1.0938	1.0868	1.101.1	1.1230	1.1416	1.1382
		1.1203	Į	1079		1.1048	1.0915	1.0848	1.0796	1.0974	1.1161	1.1294	1.1238
5 ¥		1199		1027		1.0978	1.0864	1.0758	1.0769	1.0943	1.1108	1.1203	1.1114
3 8				560V		1.0873	1.0794	1.0643	1.0735	1.0945	1.1092	1.1164	1.1029
8		10000				1 0006	0440	10671	1040.1	1 0985	1 1102	1.1079	1.0941
\$		1.0504	9530	1.0010		C000.T	24/A.T	1100-1	TEINT	7000 T			
Q2		1.0817	0787	1.0747		1.0747	1.0682	1.0524	1.0842	1.0984	1.1134	1.1090	1.880 · T
		1.0840	0779	1.0777		1.0772	1.0680	1.0554	1.0865	1.1102	1.1237	1.1222	1.0910
: \$		1.0890	0825	1.0818		1.0800	1.0698	1.0586	1.0881	1.1147	1.1251	1.1280	1.0948
3	(Mail)	1.0906	0847	1.0837		1.0833	1.0735	1.0615	1.0909	1.1179	1.1277	1.1347	1.0970
		1 0050		0077		1 0853	1 0770	1.0632	1.0819	1.1000	1.1149	1.1179	1.1001
	_	1000A-1	0000	1.001.1			A		****				
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Inlet Plenum Conditions: $P_0 = 2012 \text{ psf } T_0 = 534 \text{ °R}$

	1.1156 1.1075 1.1006 1.0914 1.1023 1.1191 1.1406 1	1.1071 1.1003 1.0922 1.0851 1.0999 1.1137 1.1320 1	1.1005 1.0348 1.0863 1.0846 1.0979 1.1106 1.1259 1	1.0938 1.0903 1.0787 1.0864 1.0991 1.1139 1.1235	1.0888 1.0845 1.0737 1.0928 1.1085 1.1210 1.1227 ¹	0876 1.0854 1.0836 1.0711 1.1006 1.1194 1.1329 1.1366 1.1093	1.0886 1.0873 1.0767 1.1074 1.1299 1.1454 1.1584 ¹	1.0934 1.0923 1.0827 1.1117 1.1348 1.1493 1.1634	1.0983 1.0977 1.0882 1.1140 1.1386 1.1539 1.1695	1.0934 1.0899 1.0797 1.0953 1.1119 1.1285 1.1355	$= 2020 \text{ psf } T_0 = 525.2 ^{\circ}\text{R}$
	1.1181 1	1.1101 1	1.1043	I. 0967	1.0921	1.C879 1.0872 1.(1.0927	1.0979 1	1.1016	1.0967	Conditions: P ₀
$\underline{W\sqrt{\theta}} = 122.1$	0 5 1.1285	1.1182	15 1.1136	30 1.1009	50 1.0961	70 1.0938	85 I.1045	90 1.1099	95 1.1142	MR 1.1041	Inlet Plenum (

 $\frac{W\sqrt{\theta}}{\delta} = 111.0$

-	1.1322	1.1219	1.1889	1.1142	1.1155	1.1095	1.1053	1.0975	1.1043	1.1287	1.1414	1.1423
01	1.1237	1.1146	1.1120	1.1074	1.1091	1.1026	1.0968	1.0895	1.1022	1.1227	1.1330	1.1314
15	1.1177	1.1096	1.1066	1.1029	1.1034	1.0985	1.0913	1.0894	1.1012	1.1188	1.1254	1.122
8	1.1046	1, 1037	1.1009	1.0988	1.0986	1.0952	1.0860	1.0952	1.1053	1.1193	1.1230	1 27
8	1.1037	1.0981	1.0957	1.0958	1.0942	1.0911	1.0827	1.1010	1.1145	1.1306	1.1252	1.1164
2	1.1117	1.1097	1.1025	1.0960	1.0943	1.0932	1.0826	1.111	1.1241	1.1399	1.1375	1.1256
38	1.1239	1.1230	1.1152	1.1086	1.1018	1.1038	1.0918	1.1190	1.1371	1.1525	1.1558	1.1366
\$	1.1305	1.1285	1.1180	1.1124	1.1071	1.1080	1.0974	1.1225	1.1426	1.1578	1.1639	1.1406
9 5	1.1387	1.1327	1.1242	1.1165	1.1104	1.1116	1.1026	1.1262	1.1457	1.1634	1.1716	1.1445
MR	1.1149	1.1105	1.1060	1.1025	1.1003	1.0979	1.0892	1.1037	1.1178	1.1341	1.1364	1.1252
Inlet	Plenum C	onditi	ons: 7	$P_0 = 20$	2037 psi	°. L	= 529.	3 °R				

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TABLE 17.2 Stator Discharge Circumferential Distributions Temperature Rakes 90% Speed

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1.2362 1.2195 1.2058 1.1971 1.1939 1.1729 1.1766 1.1845 T_{12}/T_{0} L. 1903 1.1923 356° 1.2227 1.2098 1.2044 1.2167 1.2167 1.2432 1.2584 1.2163 1.2308 r_{12}/r_{0} 1.2200 326° 1.1823 1.1719 T_{12}/T_{0} 1.1838 1.1995 1.2094 1.1744 1.1831 296° T_{12}/T_{0} 1.1551 1.1487 1.1565 1.1563 1.1563 1.1652 1.1705 1.1927 1.2027 1.2115 1.1695 266° T_{12}/T_{0} 1.1366 1.1177 1.1103 1.1083 1.1018 I.1139 1.1152 1.1187 1.1122 236° T_{12}/T_{0} 1.1579 1.1467 1.1360 1.1127 1.1020 1.1004 1.1038 1.1100 1.1161 206° T_{12}/T_0 1.1745 1.1565 1.1379 1.1350 . 341 3.370 1.1338 1.1427 176° 1.1415 1.1861 1.1749 ^T12/T₀ 1.1531 1.**1616** 1. 1483 1.1618 I.1496 1.1465 L.1457 1.1531 146° T₁₂,'T₀ 1.1598 1.1656 1.1677 1.1640 L. 1563 1.1517 L.1486 1.1531 1.1780 1.1568 116 T_{12}/T_{0} 1.1581 l.1842 L.1785 1.1650 1.1589 1.1539 1.1971 1.1731 1.1655 • Circunferential Position T_{12}/T_0 1.2011 1.1886 1.1322 1.1718 1. 1559 1. 1534 1. 1614 1. 1682 1. 1682 I.1661 26 $\frac{W\sqrt{\theta}}{\delta} = 164.8 T_{12}/T_0$ 1.2162 1.2013 1.1904 1.1780 1.1780 1.1780 1.1780 1.1655 1.1716 1.1805 1.1803 **8** % Span ŝ 2 10

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Inlet Plemm Conditions: $P_0 = 1968 \text{ psi}$ $T_0 = 536.2 \text{ R}$

1.2274 1.2153 1....5) 1.1914 1.1980 1.2257 1.2333 1.2447 1.2047 1.1847 1.2264 1.2173 1.2088 1.2052 1.2543 1.2216 1.2694 1.2222 1.2114 1.2427 1.1818 1.1769 1.1758 1.1803 1.1994 1.2249 1.2565 1.2672 1.2729 1.2372 1.2407 1.2468 1.2005 1.1626 1.1624 1.1660 1.1815 1.1992 1.2162 1.1450 1.1362 1.1319 1.1380 1.1753 1.1674 1.1521 l.1814 1.1538 1.1650 1.1582 1.1484 1.1344 1.1295 1.1287 1.1430 1.1487 1. 1459 1. 1479 1.1739 1.1651 1.1552 1.1438 1.1540 1.1609 1.1505 1.1460 1.1859 1.1553 1.1561 1.1561 1.1620 1.1710 L. 1651 1.1582 1.150 1.1818 1.1690 1.1627 1.1580 1.1563 1.1600 1.1610 1.1686 1.1544 1.1747 1.1906 1.1812 1.1732 1.1732 1.1585 1.1585 1.1580 1.1624 1.1702 1.1766 1.1651 1.1959 1.1864 1.1764 1.1764 1.1679 1.1619 1.1619 1.1636 1.1729 1.1729 L. 1693 1.1907 1.1802 1.1748 1.1752 1.2065 1.2011 1.2092 1.2238 1.1877 $\underline{W} \sqrt{\theta} = 156.2$ ŝ 2 2 8 2 2 8 8 8 8

inlet Plenum Conditions: $P_0 = 1977 \text{ psf}$ $T_0 = 536.1 \text{ }^{\circ} R$

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Stator Discharge Circumferential Distributions Cir-unferential Position Temperature Rakes 100% Speed TABLE 17.3

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C Sten		~umferential			neritariana waves 100% obeed	NAMES		pead					
		26° 36°			146	176	206	236*	265*	296°	326	356*	
$\frac{W}{\delta} = 17$	=178.2 T12/To	0 T12/To	T12/To	T12/To	T12/To	T12/To	T12/To	T12/To	T12/To	T12/To	T12/To	T12/To	
5	1.255		1.2432	1.2181	1.2216	1.2070	1.1989	1.1621	1.1827	1.2198	1.2694	1.2781	
91	1.246		1.2346	1.2011	1.2138	1.1985	1.1915	1.1436	1.1746	1.2163	1.2571	1.2649	
15	1.238		1.2272	1.2013	1.2042	1.1693	1.1799	1.1347	1.1750	1.2142	1,2535	1.2539	
8	1.237		1.2143	1.1952	1.1868	1.1695	1.1493	1.1193	1.1849	1.2098	1.2624	1.2535	
22	1.219	-	1.2110	1.1959	1.1887	1.1692	1.1347	1.1268	1.1895	1.2156	1.2664	1.2232	
20	1.206(-	1.1941	1.1812	1.1766	1.1629	1.1307	1.1364	1.1966	1.2284	1.2589	1.2044	
85	1.210		1.1996	1.1926	1.1836	1.1641	1.1370	1.1425	1.2177	1.2395	1.2551	1 2160	
8	1.224		1.2084	1.2017	1.1896	1.1696	1.1475	1.1449	1.2242	1.2511	1.2651	1. 2244	
96	1.236	-	1.2168	1.2086	1.1974	1.1799	1.1597	1.1476	1.2304	1.2615	1.2812	1.2310	
MR	1.225	3 1.2087	1.2120	1.1962	1.1903	1.1735	1.1493	1.1346	1.1945	1.2241	1.2625	1.2324	
- L-T	- 71	The second second second second second second second second second second second second second second second s			3 01	E		þ					

Inlet Plenum Conditions: $P_0 = 1946$ psf $T_0 = 538.5$ ^R

 $\frac{W\sqrt{\theta}}{\delta} = 173.1$

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10	1.2545	1.2352	1.2368	1.2216	1.2262	1.2094	1.1976	1.1651	1.1912	1.2289	1.2/76	1.2785
01	1.2434	1.2323	1.2336	1.2187	1.2207	1.2028	1.1896	1.1613	1.1882	1.2198	1.2674	1.2678
15	1.2303	1.2218	1.2220	1.2069	1.2090	1.1945	1.1819	1.1589	1.1874	1.2140	1.260€	1.2562
8	1.2281	1.2124	1.2090	1.1970	1.1907	1.1782	1.1603	1.1646	1.2087	1.2180	1.2651	1.246
8	1.2293	1.2164	1.2128	1.2620	1.1938	1.1821	1.1528	1.1844	1.2429	1.2368	1.2752	1.2336
70	1.2044	1.1957	1.1927	1.1837	1.1802	1.1764	1.1515	1.2632	1.2776	1.2807	1.2945	1.2351
85	1.2054	1.1978	1.2044	1.1960	1.1936	1, 1796	1.1615	1.2127	1.2903	1.3146	1.3247	1.2756
3 6	1.2185	1.2089	1.2144	1.2073	1.2007	1.1865	1.1714	1.2145	1.2952	1.3268	1.3391	1.2961
95	1.2254	1.2201	1.2231	1.2157	1.2083	1.1970	1.1807	1.2173	1.3068	1.3360	1.3546	1.3159
	1.2236	1.2124	1.2.16	1.2004	1.1957	1.1850	1.1643	. 1845	1.2414	1.2538	1.2883	1.2555
Inlet	Plenum	Conditi	ons:]	P ₀ = 1958	55 psf	To =	536.8°	æ				

 $\frac{W\sqrt{\theta}}{\delta} = 167.2$

1.2829	1.2718	1.2626	1.2513	1.2526	1.2701	1.2981	1.3103	1.3212	1.2716
1.2889	1.2771	1.2685	1.2604	1.2595	.2704	1.2950	1.3052	1.3223	1.2750
1.2423	1.2365	1.2336	1.2346	1.2631	1.3024	1.3354	1.3449	1.3510	1.2761
1.2047	1.2039	1.2.41	1.2230	1.2630	1.2904	1.3105	1.3161	1.3279	1.2573
1.1720	1.1707	1.1705	1.1766	1.1979	1 2216	1.2339	1.2371	1.2408	1.1989
1.2020	1.1950	1.1682	1.1709	1.1695	1.1666	1.1796	1.1895	1.1994	1779
1.2095	1.2041	1.1965	1.1827	1.1879	1.1847	1.1867	1.1954	1.2053	1.1905
1.2206	1.2122	1.2021	1.1917	1.1994	1.1896	1.1983	1.2060	1.2159	1.1992
1.2178	1.2034	1.1949	1.1960	1.2007	1.1952	1.2048	1.2160	1.2251	1.2, 19
1.2285	1.2179	1.2070	1.2044	1.2047	1.2015	1.2163	1.2255	1.2347	1.210
1.2379	1.2309	1.2223	1.2173	1.2127	1.2203	1.2480	1.2614	1.2762	1.2272
1.2576	1.2512	1.2456	1.2391	1.2260	1.2366	1.2596	1.2707	1.2656	1.2442
N	10	15	8	95	70	85	06	95	

TABLE 18

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% of Design <u>Speed</u>	<u>₩\</u> <i>θ</i> /δ	P ₁₂ /P ₈	<u>η</u>	^T ₁₂ /T _O
70	129.8	1.292	82.4	1.092
	122.1	1.320	82.2	1.101
	111.0	1.341	76.4	1.114
90	164. 8	1.522	78.1	1.163
	156.2	1.594	79.3	1.180
100	178.2	1.647	76.3	1.201
	173.1	1.747	77.7	1,223
	167.2	1.781	76.5	1.235

Stage Overall Performance for Inlet Circumferential Distortion

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