

NASA CR-72694
PW-3772



**SINGLE-STAGE EVALUATION OF HIGHLY-LOADED
HIGH-MACH-NUMBER COMPRESSOR STAGES
II. DATA AND PERFORMANCE
MULTIPLE-CIRCULAR-ARC ROTOR**

by
D. H. Sulam, M. J. Keenan, and J. T. Flynn

**Pratt & Whitney Aircraft Division
United Aircraft Corporation**

prepared for
National Aeronautics and Space Administration

**NASA Lewis Research Center
Contract NAS3-10482
L. Reid, Program Manager
Fluid Systems Components Division**



FACILITY FORM 602

(ACCESSION NUMBER)	(THRU)
0231	1
(PAGES)	(CODE)
14	01
(NASA CR OR TMX OR AD NUMBER)	(CATEGORY)

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FOREWORD

The work described herein was done under NASA Contract NAS-3-10482 by Pratt & Whitney Aircraft Division of United Aircraft Corporation, East Hartford, Connecticut. Mr. L. Reid, NASA - Lewis Research Center, Fluid System Components Division, was Project Manager.

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ABSTRACT

Data and Performance Report, Single Stage Evaluation of Highly-Loaded-High-Mach- Number Compressor Stages, Multiple Circular Arc Rotor

Tests were conducted on a 0.5 hub/tip ratio single-stage compressor designed to produce a pressure ratio of 1.936 at an efficiency of 84.2 percent with a rotor-tip speed of 1600 feet per second and a flow rate of 187.1 pounds per second. Design pressure ratio was obtained at design speed with an efficiency of 84.5 percent and a flow of 181.3 pounds per second. For tests with radial inlet-flow distortion, the peak stage efficiency obtained at design speed was 78.4 at a pressure ratio of 1.774 and flow of 177.2 pounds per second. The peak stage efficiency with circumferentially-distorted inlet flow was 77.7 percent at a flow of 173.1 pounds per second and a pressure ratio of 1.747.

1. SUMMARY

A compressor stage with a rotor tip speed of 1600 ft/sec, supersonic relative rotor-inlet Mach numbers over nearly the entire span, and a diffusion factor of 0.5 at 10% span from the tip was tested with uniform inlet flow and with radially and circumferentially-distorted inlet flow. Design stator inlet Mach numbers were subsonic, with a maximum value of 0.89 occurring at the hub where the diffusion factor was 0.6. Both the rotor and stator blades had multiple-circular-arc airfoil sections with the chord held constant from root to tip. The stage was designed without inlet guide vanes and the stator exit flow was axial.

Over-all performance at design speed with uniform inlet flow for near-design and near-surge aerodynamic conditions are compared with design values in the following table.

<u>Parameter</u>	<u>Design Value</u>	<u>Near-Design Data Point</u>	<u>Near-Stall Data Point</u>
Corrected Weight Flow, lb/sec	187.1	180.4	173.7
Rotor Pressure Ratio	2.000	2.010	2.037
Rotor Efficiency, Percent	88.7	89.0	86.7
Stage Pressure Ratio	1.936	1.946	1.959
Stage Efficiency, Percent	84.2	84.5	81.4

Over-all stage performance characteristics at design speed for uniform inlet flow and for radially and circumferentially distorted inlet flow are shown in the following table.

<u>Parameter</u>	<u>Uniform Inlet Flow</u>	<u>Radially-Distorted Inlet Flow</u>	<u>Circumferentially Distorted Inlet Flow</u>
Flow range, lb/sec $\frac{W\sqrt{\theta}}{\delta \max}$ $\frac{W\sqrt{\theta}}{\delta \min}$	184.3 - 171.0	179.6 - 176.0	178.2 - 157.5
Maximum stage pressure ratio	1.959	1.814	1.780
Maximum stage efficiency, percent	84.5	78.4	77.7
<u>Pmax - Pmin</u> Pmax	0	0.16 (outer 0.4 of span)	0.2 (90° arc)

Rotor incidence angles were more positive than design values across the entire span as a result of the inability to attain design flow. Rotor deviations, diffusion factors, and losses were close to design estimates. Stator blade incidence angle, loss, diffusion factor, and deviation were also in general agreement with design values.

Static pressure patterns relative to rotor blade tips show regions of supersonic expansion and compression and shock locations. The shock was usually detached from the blade, oblique to the direction of the mean flow, and tended to move upstream as the rotor pressure ratio was increased.

Measured levels of continuous stress due to centrifugal and untwist loads agreed with the design prediction. Vibratory stresses with uniform inlet flow did not exceed 5,000 psi except at stall, where the blade vibratory stresses were approximately 20,000 psi. Indications of blade resonance with two excitations per revolution limited test speeds to 105 percent of design. With radially and circumferentially distorted inlet flows, minimum flow was limited by a 15,000 psi vibratory stress boundary. Rotating stall patterns were present at the blade tip and midspan during the surge cycle with uniform and distorted inlet flow.

II. INTRODUCTION

Design of the single-stage compressor was based on the technology generated by two previous programs:

- (1) High-tip-speed, highly-loaded rotors were tested under Contract NAS3-7617, and the results were reported in CR-54623 (Reference 1). Rotor efficiencies exceeding 0.88 were demonstrated, with a tip speed of 1400 feet per second and D factors greater than 0.5 over the entire span.
- (2) Transonic highly-loaded stators were tested under Contract NAS3-7614, and the results were reported in References 2, 3, and 4. Moderate stator losses were measured with high subsonic Mach numbers and with D factors greater than 0.5.

Multiple-circular-arc airfoil sections were selected for the rotor and the stator in order to obtain low losses at high Mach numbers. Blade elements were designed for efficient alignment of supersonic flow to the suction surfaces in the entrance region. Blade design also included a stream-tube analysis to obtain the desired values of critical area ratio (a/a^*) in channels between blades.

In addition to the multiple-circular-arc rotor, a slotted rotor and a tandem rotor were designed in order to evaluate advanced concepts. The slotted rotor was designed to reduce over-all blade shock losses. It provides an oblique shock, caused by the slot discharge flow, which lowers the Mach number upstream of the normal shock and decreases normal shock losses. The combination of an oblique shock and a normal shock results in a greater efficiency than a strong normal shock. The tandem rotor was designed with a supersonic forward blade and a subsonic rear blade so that the shock impinges on the forward blade and is isolated from the subsonic suction surface by a stream of high-energy air. Design details of the three rotors and the stator are given in Reference 5.

The purpose of this program is to extend the scope of available design information. Experimental evaluations include over-all performance with uniform inlet flow and with radial and circumferential distortions, and blade-element performance with uniform and radially-distorted inlet flow.

This report presents the test results for the multiple-circular-arc rotor and stator.

III. APPARATUS AND PROCEDURES

A. Test Facility

The test program was carried out in a sea-level compressor test facility (Figure 1). The stand is equipped with a gas-turbine-drive engine which uses a 2.1:1 gearbox to provide optimum speed-range capability.

Air enters through a calibrated nozzle for flow measurements. A 72-foot straight section of 42-inch-diameter pipe runs from the nozzle to a 90-inch-diameter inlet plenum. Wire-mesh screen and an "egg-crate" structure, located midway through the plenum, provide a uniform pressure profile to the compressor.

The compressor airflow is exhausted into a toroidal collector and then into a 6-foot-diameter discharge stack, which contains a six-foot-diameter valve to provide back-pressure, or throttling, for the test compressor. Two smaller valves in the by-pass lines, one 24-inch and one 12-inch, provide vernier control of back-pressure.

Inlet distortion patterns are generated by screens of varied porosity which are attached to the 1 x 1-inch-mesh support screen. Twelve struts, thirty-three inches upstream of the rotor leading edge, are used to support the radial and circumferential screens for distortion tests. The method of attaching the distortion screens is shown in Figures 2 and 3. The distortion-screen support is removed for uniform-inlet testing as shown in Figure 4. Strain-gage and static-pressure instrumentation is routed through the nonrotating nose fairing. Ten struts, fourteen inches upstream of the rotor leading edge, support the forward bearing and strain-gage slip-ring assembly. Eight struts, eleven inches downstream of the stator trailing edge, support the rear bearing.

B. Test Compressor

Design of the stage flowpath was guided by the aerodynamic objectives outlined in detail in the design report (Reference 5). The rotor inlet flow per unit of annulus area was set at 42 lb/sec/ft². The test compressor (Figure 5) is a single-stage, axial-flow design with no inlet guide vanes, thirty rotor blades and forty-four stator blades, each of constant chord length.

The stator-blade leading edge is 1.2 inches behind the rotor trailing edge at the hub. Running tip-clearance was 0.050 inch at 100 percent of design speed. Rotor and stator designs are summarized as follows; complete descriptions are given in Reference 5.

Rotor

The rotor was designed to operate at a tip speed of 1600 ft/sec with a constant spanwise pressure ratio of 2.0 and an over-all adiabatic efficiency of 88.7 percent. The thirty multiple-circular-arc blades have a constant 4.4-inch chord, an aspect ratio of 1.663 and a hub-to-tip ratio at the rotor inlet of 0.5. Relative Mach numbers at the rotor inlet are 1.6 at the blade tip and are supersonic over nearly the entire span. Photographs of the rotor

blade and the blade disk assembly are shown in Figures 6 and 7. A summary of the rotor blade metal angles for 9 streamlines passing through 5, 10, 15, 30, 50, 70, 85, 90 and 95 percent span of the rotor blade trailing-edge passage height from the hub is given in Table 1.

TABLE 1

Rotor Design Parameters
Stations 8 and 9

<u>% Span</u>	<u>Dia - 1</u>	<u>Dia - 2</u>	<u>β^*_8</u>	<u>β^*_9</u>	<u>β^*_{9ss}</u>	<u>β^*_{sh}</u>	<u>σ</u>
5(hub)	17.47	19.77	48.97	1.87	55.40	45.74	2.276
10	18.47	20.41	49.59	9.63	56.02	46.76	2.173
15	19.47	21.05	50.44	16.51	56.59	47.76	2.080
30	22.31	22.96	53.77	29.73	57.87	50.53	1.855
50	25.79	25.52	56.40	42.30	59.30	54.68	1.638
70	28.95	28.08	59.08	50.53	61.07	59.17	1.476
85	31.29	29.99	61.63	54.11	62.96	63.01	1.379
90	31.88	30.63	62.53	55.10	63.65	64.18	1.355
95(tip)	32.50	31.27	63.21	55.84	64.14	64.96	1.332

NOTE: Symbol definitions appear in Appendix 2.

Stator

The 44 multiple-circular-arc stator blades have a constant chord of 3.0 inches and an aspect ratio of 1.721. Photographs of the stator blade and the stator assembly are shown in Figures 8 and 9. Stator inlet Mach numbers are subsonic with a maximum value of 0.89 occurring at the hub, where the diffusion factor is 0.6. Design incidence to the stator suction surface was set at zero degrees. Stator exit flow is axial. A summary of the stator blade metal angles for 9 streamlines passing through 5, 10, 15, 30, 50, 70, 85, 90 and 95 percent of the rotor-blade trailing-edge passage height from the hub is given in Table 2.

TABLE 2

Stator Design Parameters
Stations 10 and 11

<u>% Span</u>	<u>Dia-1</u>	<u>Dia-2</u>	<u>β^*_{10}</u>	<u>β^*_{11}</u>	<u>β^*_{10ss}</u>	<u>β^*_{sh}</u>	<u>Solidity</u>
5 (hub)	20.41	21.49	43.23	-12.41	46.15	38.47	2.010
10	21.01	21.96	42.27	-11.44	45.21	36.62	1.959

TABLE 2 (CONT'D)

Stator Design Parameters
Stations 10 and 11

<u>% Span</u>	<u>Dia-1</u>	<u>Dia-2</u>	<u>β^* 10</u>	<u>β^* 11</u>	<u>β^* 10ss</u>	<u>β^* sh</u>	<u>Solidity</u>
15	21.59	22.43	41.42	-10.89	44.36	34.94	1.911
30	23.31	23.90	39.44	-11.22	42.44	31.18	1.781
50	25.60	25.89	37.60	-12.04	40.72	28.01	1.632
70	27.82	27.90	36.45	-13.48	39.68	26.38	1.508
85	29.41	29.38	36.12	-15.91	39.44	26.82	1.430
90	29.91	29.86	36.15	-17.40	39.48	27.36	1.477
95 (tip)	30.38	30.29	36.33	-19.69	39.69	28.40	1.387

C. Instrumentation and Calibration

Airflow was measured within 1 percent, using a flow nozzle designed to ISA specification (Reference 6). Compressor speed was measured with an electromagnetic pickup that counts the number of gear teeth passing in an interval of time and converts the count into revolutions per minute. Measurement accuracy is better than 0.2 percent of indicated speed between 4,000 rpm and 13,000 rpm.

All temperatures were measured using chromel-alumel Type K thermocouples and recorded in millivolts by the automatic data-acquisition system. Temperature elements were calibrated over their full operating-temperature range for Mach-number and total-pressure effects. The thermocouple leads were calibrated for each temperature element. Overall RMS temperature accuracy was estimated to be $\pm 1.0^\circ\text{F}$.

Disk probes were calibrated for Mach number as a function of indicated static-to-total pressure ratio, with pitch angle as a parameter. Total-pressure recovery and yaw-angle deviation were calibrated as functions of Mach number and pitch angle. The measurement accuracy of the air-angle probe was within 1.0 degree.

All pressures from probes, fixed rakes, and static taps were measured with transducers and recorded in millivolts by the automatic data-acquisition system. The accuracy of the pressure readings was ± 0.2 percent of the full-scale value.

Ten quartz-crystal, high frequency-response pressure transducers were installed in the case over the rotor tip to measure instantaneous static-pressure fluctuations. Ten wall static-pressure taps were installed over the rotor-blade tip in axial locations corresponding to the pressure transducers to measure the average static-pressure level.

Three proximity detectors, circumferentially positioned an integral number of blade gaps from the pressure transducers, generated an electrical pulse for each blade passing. Signals from both the pressure transducers and the proximity detectors were recorded by a multi-channel tape recorder on the same time reference.

Figure 10 shows the rotor-blade tip-shock pressure instrumentation in relation to the blades. Photographs of typical instrumentation are shown on Figure 11. The axial and circumferential positions of the instrumentation are shown in Figures 12 and 13.

Pressure measured by the fixed radial total-pressure rakes at the rotor leading edge (Station 7 in Figure 12) were in place only during the distortion testing. Instrumentation for measuring over-all and blade-element performance data is listed in Table 3.

TABLE 3

Performance and Blade Element Instrumentation

All measurements recorded by automatic data acquisition system unless noted otherwise.

<u>Instrument</u> <u>Plane Location</u>	<u>Parameter</u>	<u>Type and Quantity</u>
Station 0 plenum chamber	P	6 pressure taps on plenum wall (2 read on manometers)
	T	6 bare-wire thermocouples (2 read on self-balancing precision potentiometers)
Station 1.1 bellmouth instrumentation ring	$\Delta P = P-p$	6 pitot-static probes at mid-channel and evenly spaced about the instrument ring. ΔP water and acetylene tetrabromide manometers. (After initial check point the bellmouth pitot-static probes were removed.)

TABLE 3 (CONT'D)

<u>Instrument Plane Location</u>	<u>Parameter</u>	<u>Type and Quantity</u>
	p	4 O.D. wall static taps
Station 5.1 inlet duct		
5.2	p	2 O.D. and 2 I.D. wall static taps, 180 degrees apart
6.1		
6.2		
7.1		
Station 7 rotor inlet (within 1/2 chord)	P, p, β	2 disk traverse probes, 9 radial positions
	p	4 O.D. and 4 I.D. wall static taps
	P	2 fixed rakes, 180° apart, each with sensors at nine radial positions
Station 8.5 rotor shroud	p	10 rapid response pressure transducers mounted in axial line over rotor tip. Recorded on magnetic tape.
	p,	10 O.D. wall static taps in axial line over rotor tip
	Blade Passing	Three proximity detectors positioned apart from the pressure transducers and in a line at the rotor-blade tip-chord angle. Recorded on magnetic tape.
Station 10 stator leading edge	p	4 O.D. and 4 I.D. wall static taps equally spaced and located on extension of mid-channel lines
	p	4 O.D. and 4 I.D. wall static taps spaced across one vane gap

TABLE 3 (CONT'D)

<u>Instrument</u> <u>Plane Location</u>	<u>Parameter</u>	<u>Type and Quantity</u>
	P	2 sets of impact tubes at 9 radial locations
Station 12 stator exit	P	2 circumferential wake rakes (15-element) traversable to each of nine radial locations. Each wake rake spans at least one vane gap at O. D.
Station 12 stator exit	T	7 fixed radial rakes, each with temperature sensors at 9 radial positions. 6 probes spaced circumferentially to obtain readings evenly distributed across a vane gap. The 7th rake is a duplicate mid-gap rake, and spaced 180 degrees from the other mid-gap rake.
	P, p, β	2 disk traverse probes, 9 radial positions. Probes spaced 180 degrees apart. One traverse mechanism capable of tangential probing across a vane gap
	p	4 O. D. and 4 I. D. wall static taps
	p	4 O. D. and 4 I. D. wall static taps spaced across vane gap
Station 13.1 rig exit	P	1 fixed five-element radial rake

Note: The nine radial positions of each axial station are defined by the intersection of the axial station and the design streamlines which pass through 5, 10, 15, 30, 50, 70, 85, 90, and 95 percent of the passage height at the rotor trailing edge.

Table 4 shows the parameters that were continuously recorded during excursions into stall to detect and evaluate rotating stall. Three rapid-response pressure transducers, located at the rotor exit at 25, 50, and 85 percent of blade height from the hub and at unequal circumferential locations, were used to record pressure pulses continuously on a multi-channel tape recorder when operating near or within the stall region.

TABLE 4
Stall Transient Instrumentation

<u>Instrument Plane Location</u>	<u>Parameter</u>	<u>Type and Quantity</u>
Inlet orifice	p	1 static tap downstream of inlet orifice
Station 7 rotor inlet	p	1 O.D. wall static tap
Station 9 rotor exit	P frequency	3 rapid-response pressure transducers at unequal circumferential spacing. Sensors located at 25, 50 and 85% of blade height from hub
	p	1 O.D. wall static tap
Station 10 stator leading edge	P	3 impact tubes at 5, 50, and 95% of passage height from hub
Station 12 stator exit	p	1 O.D. wall static tap
Station 13.1 rig discharge	P	1 element of fixed radial rake
gearbox	N	impulse pick-up

Critical stationary and rotating parts were instrumented with strain gages to determine the levels of continuous stress due to centrifugal and blade untwist loads and vibratory stress over the operating range of the compressor.

D. Test Procedure

1. Shakedown Test

Before taking performance data, shakedown tests were conducted to establish the mechanical integrity of the compressor and to locate critical stress boundaries which might limit the operating range over which the tests could be conducted.

Accelerations were made to 50, 70, 90, 100, and 115 percent of design speed, with open discharge throttle and uniform inlet flow. Continuous and vibratory stresses of the rotor and stator were recorded. A rotor blade resonance with two excitations per revolution was detected at 12,600 RPM, and maximum speed for performance testing was set at 105 percent of design speed in order to avoid it. Continuous stress due to centrifugal and untwist loads was slightly lower than predicted and did not limit test speeds.

Stress and rotating-stall surveys were made with uniform, radially-distorted, and circumferentially-distorted inlet flow. Vibratory stresses were recorded simultaneously with transient readings of the parameters shown in Table 4 in order to correlate blade stress with stall. In all surveys, vibratory stress at stall increased with speed and closely approached the maximum allowable transient stress at design-speed. Stress boundaries for steady-state operation were defined with radially and circumferentially distorted flows. Rotor blade vibratory stress increased as the compressor was throttled, which prevented steady-state operation near stall. The range of operation was severely limited by high stresses with radial distortion, making it necessary to increase screen porosity. A satisfactory operating range was obtained by reducing the distortion parameter ($P_{\max} - P_{\min} / P_{\max}$) from 0.20 to 0.16. Beyond the boundary for steady-state operation, only transient data were recorded.

Rotating stall was detected by measuring pressure fluctuations with rapid-response transducers at 25, 50, and 85 percent of passage height. Continuous recordings were made as the throttle was closed until the compressor stalled and as the throttle was opened to recover from stall. Several surge pulses were recorded before the throttle could be opened enough to get the compressor out of stall.

Five over-all and blade-element performance data points, over a range of flows between wide-open throttle and stall at design speed, were taken during the shakedown test. A disk probe was traversed tangentially across a stator-blade gap at the stator exit to measure total pressure, static pressure and flow angle at each of nine radial positions for each of the five performance points. Gapwise distributions of static pressure and air angle, determined by tangential traversing, were compared to mid-gap values measured by a radial traverse probe. Averaged circumferential values were close to mid-gap values, and remaining tests were made without tangential traversing. Simultaneous immersion of all traverse probes was possible without causing data inaccuracies due to probe blockage effects.

2. Uniform-Inlet-Flow Performance Test

Six performance points, ranging in flow from open-throttle to near-surge, were obtained at 50, 70, 90, 100, and 105 percent of design speed, and stall flows were measured at 50, 70,

90, and 100 percent of design speed. The periodic static pressure fluctuations over the rotor tip were recorded at three points at 70 percent speed, four points at 90 percent speed, five points at 100 percent speed, and three points at 105 percent speed, ranging in flow from choke to near-stall. These data were obtained to show the static-pressure-field relative to the rotor blade tip, indicating shock position and strength.

3. Distorted-Inlet-Flow Performance Test

The rotatable distortion-screen support was added to the flow path 33 inches upstream of the rotor leading edge. Open-throttle, part-throttle, and near-stall performance points at 70, 90, and 100 percent of design speed, with the distortion support but with no distortion screens attached, showed that the support screen did not affect uniform inlet performance. A radial screen covering one-fifth of the inlet area (Figure 2) was required to create a radial-distortion pattern covering two-fifths of the rotor inlet area. A 20-degree, full-span screen (Figure 3) was required to produce a 90-degree circumferential pattern with a distortion parameter of 0.20 at the rotor inlet, with the throttle wide-open at 100 percent of design speed.

Performance data with both radial and circumferential inlet-flow distortion were taken at 70, 90, and 100 percent of design speed, with the discharge throttle at three positions (wide-open, part-throttle, and near-surge), except where high stresses prevented taking near-stall data points. Each circumferential-distortion data point was taken with the screen in six different positions with respect to the compressor instrumentation.

E. Calculation Procedure

Data reduction was accomplished in three steps:

1. Raw data were converted from electrical values to engineering units and thermocouple-wire corrections were applied.
2. Aerodynamic corrections and averaging techniques were used to obtain radial distributions of circumferentially-mass-flow-averaged pressures, temperatures, and angles
3. Blade-element data were calculated for uniform and radial distortion tests, using a flow-field calculation procedure.

Aerodynamic corrections and averaging techniques were:

1. Total-pressure probes located in supersonic flow were corrected for shock losses. Total pressures from the two wake rakes were circumferentially mass-flow-averaged at each radial position, using a constant static pressure obtained by a linear interpolation between wall static pressures. Free-stream values of total pressure downstream of the stator (peak wake rake values) were selected at each radial position. A wake blockage factor was also calculated at each radial location, as defined in Appendix 1, and used in a flow-field calculation program to improve the accuracy

of the static pressure and velocity calculations at the stator exit. Free-stream and circumferentially mass-flow-averaged pressures and wake blockage factors were each arithmetically averaged from the two rakes at each radial location to be used in the flow-field calculation.

2. Temperature probes were corrected for Mach number recovery, including the pressure-level effect. Six radial rakes were approximately equally-spaced about the annulus at the stator exit, and located at different circumferential positions relative to a stator gap. A circumferential mass-flow average was calculated at each radial position and used in the flow-field calculation. Circumferential wake-rake total-pressure distributions were used for the circumferential mass-flow-averaging of the stator exit temperatures.
3. Over-all performance calculations were based on the inlet plenum pressure as a reference for uniform inlet flow, and on an arithmetical average of radially mass-averaged pressures from the two radial rakes at the rotor inlet for radially-distorted inlet flow. The reference pressure for circumferentially-distorted inlet flow was the arithmetical average of twelve radially-mass-averaged pressures obtained from the two radial rakes at the rotor inlet for each of the six screen positions. The relationship between plenum and rotor inlet total pressure was correlated as a function of corrected flow (Figure 14). Calculations of corrected flow, pressure ratio, and efficiency were based on pertinent reference stage inlet pressures. All averaging techniques were the same for both uniform and radially-distorted inlet flow. For circumferential distortion tests, a different technique for stator-exit pressure and temperature averaging was used. Radially mass-flow-averaged values of pressure from the two wake rakes at each screen position were arithmetically averaged. This pressure was used for over-all pressure ratio and efficiency calculations. Data from each of the six individual temperature rakes were radially mass-averaged for each screen position, and the 36 resulting values were arithmetically averaged. This temperature was used for overall efficiency calculations. Circumferential distributions of static and total pressure (Appendix 5) are ratioed to the inlet plenum.
4. Velocity vectors were calculated from disk probe traverse data for nine radial locations at the instrumentation planes upstream of the rotor and downstream of the stator. Measurements at each probe position were used to determine corrected total pressure and calculated static pressure, Mach number, and air angle. Calibrations of individual probes were used to correct the raw data. Each probe was first calibrated for Mach number under controlled wind-tunnel conditions, and test Mach number was then determined from the ratio of measured static to measured total pressure. Total pressure and yaw angle corrections were made by using calibrations versus Mach number. Static pressure was calculated by using the corrected total pressure and the calibrated Mach number. An arithmetical average of the two stator-exit-probe-angle readings for each radial position was used in the flow-field calculation.

Blade-element performance for uniform-inlet and radial-inlet-distortion test points was calculated by a flow-field analysis computer program. All parameters were corrected to standard-day conditions. The inputs were:

Compressor Inlet	1) corrected weight flow 2) corrected rotor speed
Rotor Inlet Instrument Plane	1) total pressure versus radius 2) blockage factor versus radius (to account for estimated wall boundary layers)
Stator Inlet	1) total pressure versus radius 2) blockage factor versus radius (to account for estimated wall boundary layers)
Stator Exit Instrument Plane	1) total temperature versus radius 2) total pressure versus radius 3) blockage factor versus radius (to account for stator wake blockage and wall boundary angle) 4) absolute air angle versus radius

All pressures and temperatures are expressed as ratios to mass-averaged values at the rotor inlet.

All static-pressure distributions and air angles behind the rotor were calculated by assuming axisymmetric flow and consideration of mass-flow continuity, radial equilibrium, and energy equations. Curvature, enthalpy, and entropy gradient terms were used in the equilibrium calculations. Blade-element performance parameters at the blade edges were calculated by translating the measured data from the instrument plane along streamlines which passed through the rotor trailing edge at 5, 10, 15, 30, 50, 70, 85, 90, and 95 percent of the passage height. Blade-element parameters were calculated at airfoil sections lying on conical surfaces defined by the intersections of these streamlines and the blade edges. Pertinent performance parameters are defined in Appendix 3.

Static pressure contours over the rotor blade tips were obtained by using continuously-recorded pressure fluctuations, which were measured by high-frequency-response transducers. Ten transducers were distributed axially over the blade tip (Figure 10), and ten wall static pressure taps were located at the same axial positions to measure average static pressure. Records of fluctuating pressures versus time indicated that the transducers were not in agreement in terms of known blade location, and the signals were oriented by positioning the pressure drop caused by the passing of the suction surface in relation to the actual position of the blade. A computer program converted electrical signals from the transducers to pressure fluctuations for one blade-passing time period, with each transducer referenced to the same point in time. The program then added average pressure to the pressure fluctuations at each axial position. The full range of pressure variation for a given point was broken into ten

equal increments and a code number assigned for each increment of pressure range (see page 100 for the static pressure code), e.g., a code of 5 means that the pressure in the region lies in the range of 5 to 6 psia. Regions of constant pressure were outlined by displaying the code numbers relative to the blade tips across two blade gaps.

IV. RESULTS AND DISCUSSION

The results of the multiple-circular-arc rotor test were discussed under the headings of shakedown tests, uniform-inlet-flow performance, distorted-inlet-flow performance, and rotor-blade-tip static pressure contours.

Shakedown test results include stress and rotating stall data for uniform and distorted inlet flows and an evaluation of traversing methods. Over-all performance of the rotor and stage are presented for uniform and distorted inlet flows in terms of pressure ratio and efficiency versus corrected weight flow ($W\sqrt{\theta}/\delta$) with corrected speed ($N/\sqrt{\theta}$) as a parameter. Rotor and stator blade-element performance curves are presented for uniform-inlet-flow and for radially-distorted-inlet-flow tests. Loss coefficient, diffusion factor, and deviation are presented as functions of incidence at radial locations on streamlines passing through 5, 10, 15, 30, 50, 70, 85, 90, and 95 percent of the rotor-blade exit passage height from the hub. For circumferentially-distorted-inlet-flow tests, circumferential distributions of pressure, velocity, and air angle are included to describe the extent of distortion on the rotor inlet and stator exit.

Rapid-response static-pressure data over the rotor blade tips are presented as contours outlining regions of constant static pressure and are shown with respect to the rotor-tip blade gap. The blade-tip shock was located by the instantaneous pressure rise in the blade passage.

A. Shakedown Tests

Continuous stresses due to centrifugal and untwist loads were measured near blade root leading and trailing edges and were slightly lower than design predictions. Using the design prediction of stress distribution, the maximum blade stress was 60,000 psi on the pressure surface at 10 percent span from the hub. Predicted stress at this location was 61,000 psi.

Vibratory stress with uniform inlet flow was not high except at stall, but a resonance with two excitations per revolution appeared at 12,600 RPM, which is 109 percent of design speed when corrected for 100° F ambient temperatures. This resonance limited performance testing to 105 percent of design speed. During stall at design speed, the blade tip vibratory stresses were approximately 20,000 psi. The mode of this tip vibration was shown in laboratory tests with stress-coated blades (Figure 15). Since stall stress levels increased rapidly with speed, a stall point was not run at 105 percent of design speed.

The maximum allowable vibratory stress of 15,000 psi for steady-state operation limited the range of operation with radially and circumferentially distorted inlet flows. Stress boundaries for radially-distorted inlet flow are discussed in Section IVC1, Radially-Distorted Inlet Flow, Overall Performance. Stress boundaries for circumferentially-distorted inlet flow will be found in Section IVD1, Circumferentially-Distorted Inlet Flow, Over-all Performance. With both types of distortion, the maximum stress during stall was 23,000 psi at design speed and was increasing rapidly with increasing speed.

Stall surveys with rapid-response instrumentation showed that stalls were abrupt, originating near the tip and progressing to mid-span and the root. An oscillograph trace at 90 percent speed with uniform inlet flow (Figure 16) shows the general pattern for all stalls. All stalls appeared as surge cycles with a frequency of approximately 3 cps, each cycle consisting of a surge pulse lasting approximately 0.17 seconds and a stall recovery lasting approximately 0.14 seconds. At the start of each surge pulse, pressure fluctuations with a period of about one rotor revolution occurred at the tip and mid-span, indicating the presence of rotating stall cells (Figure 17). Pressure dropped sharply after this initial phase and then rose toward the pre-stall level. The stall-recovery portion of the cycle began with a strong pressure rise, followed by a gradual pressure reduction. Similar stall patterns were observed with radially and circumferentially distorted inlet flows.

Tangential traverses of stator exit total pressure, static pressure, and air angle were taken at five points with uniform-inlet flow design speed. Circumferential distributions across a stator blade gap for open-throttle, part-throttle, and near-stall settings at 10, 50, and 90 percent span from the hub are presented in Figures 18, 19, and 20. Variations of air angle and static pressure across the stator gap are small except when the discharge throttle is wide open. Total pressure distributions from the tangentially-traversed disk probe and from the two radially-traversed wake rakes are compared in Figure 21 at the near-stall throttle setting.

Stator exit total pressure, static pressure, and air angle versus percent span for the near-stall point at design speed are shown in Figure 22. Mass-averaged total pressures across a stator gap, calculated from the tangentially-traversed disk probe and from the wake-rake measurements, were in good agreement. Static-pressure and air-angle measurements from a radially-traversed disk probe in the center of the stator-blade gap were compared to the mass-averaged static pressure and average air angle, calculated from the tangentially-traversed probe. Since these results also showed good agreement, it was concluded that tangential traverse would have almost no effect on over-all and blade-element performance parameters.

B. Uniform-Inlet-Flow

1. Overall Performance

Over-all performance of the rotor only and the stage is presented in Figures 23 and 24. Tabulated results are presented in Appendix 3. The stall line was established by extrapolating the characteristic speed lines to measured stall airflows, shown as slashed symbols. Stalled operation above 100 percent of design speed was avoided because of high rotor-blade tip stresses. A maximum stage efficiency of 84.5 percent (Figure 24) at a pressure ratio of 1.946 and a corrected weight flow of 180.4 lb/sec was achieved at design speed, compared with a design stage efficiency of 84.2 at a pressure ratio of 1.936 and a corrected weight flow of 187.1 lb/sec. The rotor efficiency for the same data point (Figure 23) was 89.0 percent for a pressure ratio of 2.01, compared with a design rotor efficiency of 88.7 percent and pressure ratio of 2.00. The inability to achieve design flow was probably caused by local choking at the rotor blade root, as suggested by the high losses in this region with the discharge throttle wide open.

Maximum rotor and stage efficiencies, as shown by Figures 23 and 24 are essentially constant over the range of compressor operation between 50 and 100 percent of design speed but decrease 3 percent at 105 percent of design speed. Although a stall point was not obtained at 105 percent speed because of stress limitations, the peak efficiency performance point was identified. The abrupt decrease in peak efficiency above design speed was the result of increased rotor-blade losses from 50 percent span to the blade tip. Stator losses at 105 percent of design speed are no higher than at design speed. The fact that rotor efficiency at part speed did not rise significantly above the level obtained at design speed may be attributed to a rotor design characteristic: Channel areas between blades were designed to decelerate high Mach-number flow; and the converging channels between blades, optimized for design speed, were too small at part speed, forcing the rotor to operate at high incidence angles.

2. Blade - Element Data

Blade-element performance for a data point at design speed and near design pressure ratio agreed closely with design values. Figure 25 shows the rotor and stage adiabatic efficiency versus percent span from the hub, compared to the design. Total-pressure-loss coefficient, diffusion factor, incidence, and deviation are presented versus percent span from the hub for the rotor and stator in Figures 26 and 27. Blade-element performance parameters were calculated at stations corresponding to the actual leading and trailing edge of the blades (Stations 8 and 9 of Figure 12). Rotor and stator blade-element plots for the entire uniform-inlet performance test are presented in Figures 28 and 29, with data tabulated in Appendix 3.

Rotor incidence at design speed (Figure 26) was more positive than designed over the entire span because of the inability to attain design flow. Incidence at part speed was generally higher than at design speed because critical area ratios in channels between blades were sized for design relative Mach numbers, and they result in a lack of flow capacity at part speed. Maximum rotor diffusion factors were equal to, or exceeded, design values over nearly the entire span except at the blade hub, where they were lower than design. Rotor diffusion factor increased with increasing speed but levelled off at 100 and 105 percent of design speed. A maximum diffusion factor of almost 0.6 was achieved at 30 percent span from the hub, as compared to the design value of 0.55 at this span. Rotor deviations were greater than design, particularly at the blade tip, where a maximum difference of 5 degrees occurred. Minimum rotor losses (Figure 28) were equal to, or less than, design predictions, except at 105 percent of design speed. Stator deviations were in general agreement with design except at the end walls, and the diffusion factor exceeded design values except at 5 percent span. Stator losses and incidence agreed reasonably well with design values.

Loss coefficients at the rotor hub (Figure 26) were unrealistically low, and in some cases were slightly negative, while stator loss coefficients at corresponding spanwise locations (Figure 27) were greater than expected. The distribution of losses between the rotor and stator depends on rotor trailing-edge total pressure, which is used in the calculation of both loss coefficients (Appendix 1). In the data-reduction procedure used for these tests, the stator inlet total pressure is equal to the peak total pressure as measured by the stator trailing-edge wake rake at equivalent percentages of span. The gapwise distributions of total pressure at the stator exit for various percents of span (Figure 21) show that, at 10 percent span, the peak pressure occurs near the stator blade suction surface. The peak wake rake total pressure at this percent

of span may not be an accurate approximation of the average total pressure at the stator inlet. Because of the tendency of the low-pressure rotor wake flow to migrate toward the stator pressure surface (Reference 7), the peak value of total pressure downstream of the stator may be above the level of the average stator inlet pressure.

Peak wake-rake readings were used because they generally produce more reasonable blade-element data than either the stator leading-edge traverse probes (which strongly affect rotor operation due to their blockage) or stator leading-edge impact tubes, whose recovery varies with stator incidence and which are difficult to maintain in good working order. The stator trailing-edge wake-rake impact tubes operate with a much smaller air-angle variation than those at the stator leading edge.

An alternate method for evaluating rotor exit pressure was also investigated. Plots of pressure and temperature across the stator gap reveal that areas of high total pressure are also areas of high total temperature, so that the local efficiency does not exceed 1.0. The gapwise distribution of total pressure ratio, total temperature ratio, and local adiabatic efficiency at the stator exit at 15 percent span for the maximum efficiency point at design speed (Figure 30), shows that the free-stream region of the efficiency plot appears to give a direct measure of rotor efficiency at a spanwise location. Using this efficiency with the corresponding spanwise-mass-averaged temperature rise to calculate rotor exit total pressure profiles provides a more reasonable distribution of losses between the rotor and the stator. Figures 26 and 27 show spanwise distributions of rotor and stator blade-element performance for the two methods of determining rotor exit total pressure. The free-stream-efficiency method eliminates the problem of unrealistic efficiency and loss near the hub without affecting the other spanwise locations. Rotor deviations and stator incidences changed significantly when calculated with the free-stream-efficiency method.

Blade-element data for design-speed performance points are presented in Figure 28 and 29 for both methods of data reduction. Blade-element performance of the rotor and stator for the alternate method is tabulated in Tables 10.7 to 10.12 in Appendix 3.

3. Distortion Support Screen Effects

Open-throttle, part-throttle, and near-stall performance points were taken at 70, 90, and 100 percent of design speed with the distortion-screen support but without distortion screens. Since performance was not affected by the support screen (Figures 31 and 32), the uniform-inlet-flow performance provides a valid basis for determining effects of inlet-flow distortion.

C. Radially-Distorted Inlet Flow

A radial-distortion pattern which covered two-fifths of the rotor inlet area provided a distortion parameter of 0.16 with the discharge throttle wide open at 100 percent of design speed. Figure 33 shows the total pressure and meridional velocity at the rotor inlet versus percent span with radially-distorted inlet flow for wide-open and near-stall throttle conditions at 100 percent of design speed.

1. Over-all Performance

Over-all rotor and stage performance with radially-distorted inlet flow is presented in Figures 31 and 32. A 15,000 psi vibratory stress boundary prevented steady-state operation at a near-stall throttle setting at 70 and 90 percent of design speed. The stall line with radially-distorted inlet flow was lower than with uniform-inlet-flow. Maximum stage efficiency at design speed of 78.4 percent occurred at a pressure ratio of 1.774 and a corrected weight flow of 177.2 lb/sec, which was 6 percent lower than the maximum stage efficiency with uniform inlet flow. Maximum corrected weight flow at design speed was 4.5 lb/sec. lower than with uniform inlet flow.

2. Blade-Element Data

Rotor and stator blade-element performance for radially-distorted inlet tests is shown in Figures 34 and 35. Blade-element performance with radially-distorted inlet flow is compared with uniform inlet flow at 10, 50 and 90 percent span from the hub for the rotor and stator. The rotor-blade tip, with radially-distorted inlet flow, operated at increased positive incidence due to low axial velocity in the distorted region. The levels of loss, diffusion factor, and deviation at the rotor blade tip for design speed were essentially unaffected by the distortion. Rotor mid-span and root incidences were negative and losses increased. Stator-blade-tip incidences were slightly more positive than with uniform inlet flow and became negative at the root. Tabulations of the blade-element and over-all performance data for radially-distorted inlet flow are presented in Appendix 4.

D. Circumferentially-Distorted-Inlet-Flow

A circumferential distortion parameter of 0.20 covering a 90-degree arc was achieved at the rotor inlet with the throttle wide open at design speed using a 120-degree full span screen.

1. Over-all Performance

Over-all performance with circumferential inlet distortion is compared with uniform-inlet-flow performance in Figure 36. The maximum stage efficiency at design speed obtained with circumferentially-distorted inlet flow was 77.7 percent at a corrected weight flow of 173.1 lb/sec and a pressure ratio of 1.747. Flow range with circumferential distortion was higher than with radial distortion. This greater flow range gave a higher stall line even though stall pressure ratio was lower than with radial distortion. Stall flow at 100 percent of design speed occurred 15 lb/sec lower than with uniform inlet flow, but with an accompanying decrease in pressure ratio. Stall at 70 and 90 percent speed occurred at approximately the same flow as with uniform inlet flow, with a smaller decrease in pressure ratio than at design speed. High vibratory rotor-blade-tip stresses limited the range of steady-state operation at 90 and 100 percent of design speed. Because of the limited operating range, only two performance points were taken at 90 percent speed. Tabulations of circumferential distributions and over-all stage performance are presented in Appendix 5.

2. Circumferential Distributions of Velocity Vector Parameters

Rotor inlet circumferential distributions of total pressure, absolute and relative flow angle, absolute velocity, meridional velocity, and absolute Mach number are shown in Figures 37, 38, and 39 at 10, 50 and 90 percent span from the hub. Measurements from radially-traversed disk probes at the rotor inlet at twelve locations relative to the distortion screen were used to construct these plots. Stator discharge circumferential patterns, measured by disk probes at stator mid-gap, are shown in Figures 40, 41, and 42. Circumferential distributions of static pressure at the rotor inlet on both the inner case and outer case are presented in Figures 43 and 44.

E. Rotor Blade Tip Static Pressure Contours

Static pressures over rotor blade tips were measured by ten high-frequency-response pressure transducers. Data were obtained over a range of compressor operating conditions at 70, 90, 100, and 105 percent of design speed with uniform inlet flow. Figure 45 shows four typical oscillograph traces of static pressure versus time. At the rotor leading edge, the static pressure rise caused by the shock occurs near the pressure surface and moves toward the suction surface at measurement locations downstream of the leading edge.

Shock position with respect to the blade tip is shown in Figures 46 through 60 as a series of points, each representing the location where the instantaneous static pressure rise was observed on the oscillograph traces. Contours outlining static pressure regions over the rotor blade tip are shown in Figures 49 through 54 and 58 through 60. A rotor performance characteristic and the axial distribution of wall static pressure over the blade tip are also included in the figures. Figures 49 through 52 show the rotor tip static pressure contours over a range of flows for 90 percent of design speed. Both expansion and compression fields are indicated by the contours ahead of the passage shock. The expansion (Figure 49) along the suction surface during flow alignment is followed by a compression field ahead of the passage shock. This precompression results from the blade shape at the entrance region, which was designed for precompression to reduce the passage shock loss. The static pressure rise in this shock is about equal to the rise in the precompression region. With open throttle, shocks are nearly attached and are oblique. As back pressure is increased, the shocks become stronger and farther detached. Normal shocks were never seen, even at near-stall operating points.

These data are considered qualitative due to the difficulties in obtaining highly accurate quantitative measurements of pressure fluctuations. In view of the inherent inaccuracies, no attempt was made to construct fields of relative Mach numbers or to calculate shock strengths.

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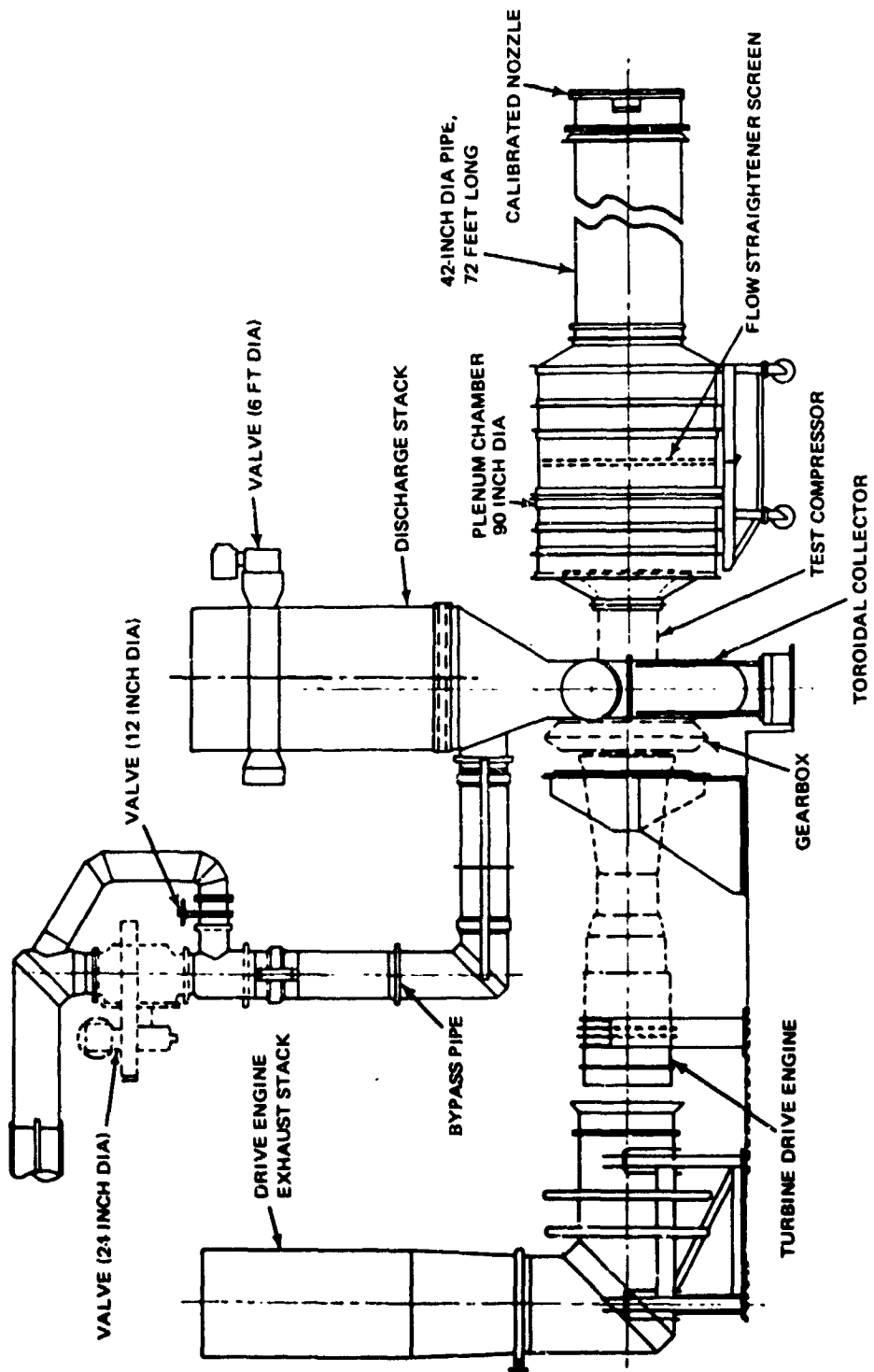


Figure 1 Schematic of Compressor Test Facility



Figure 2 Radial Distortion Screen



Figure 3 Circumferential Distortion Screen



Figure 4 Compressor Inlet Configuration for Undistorted Testing

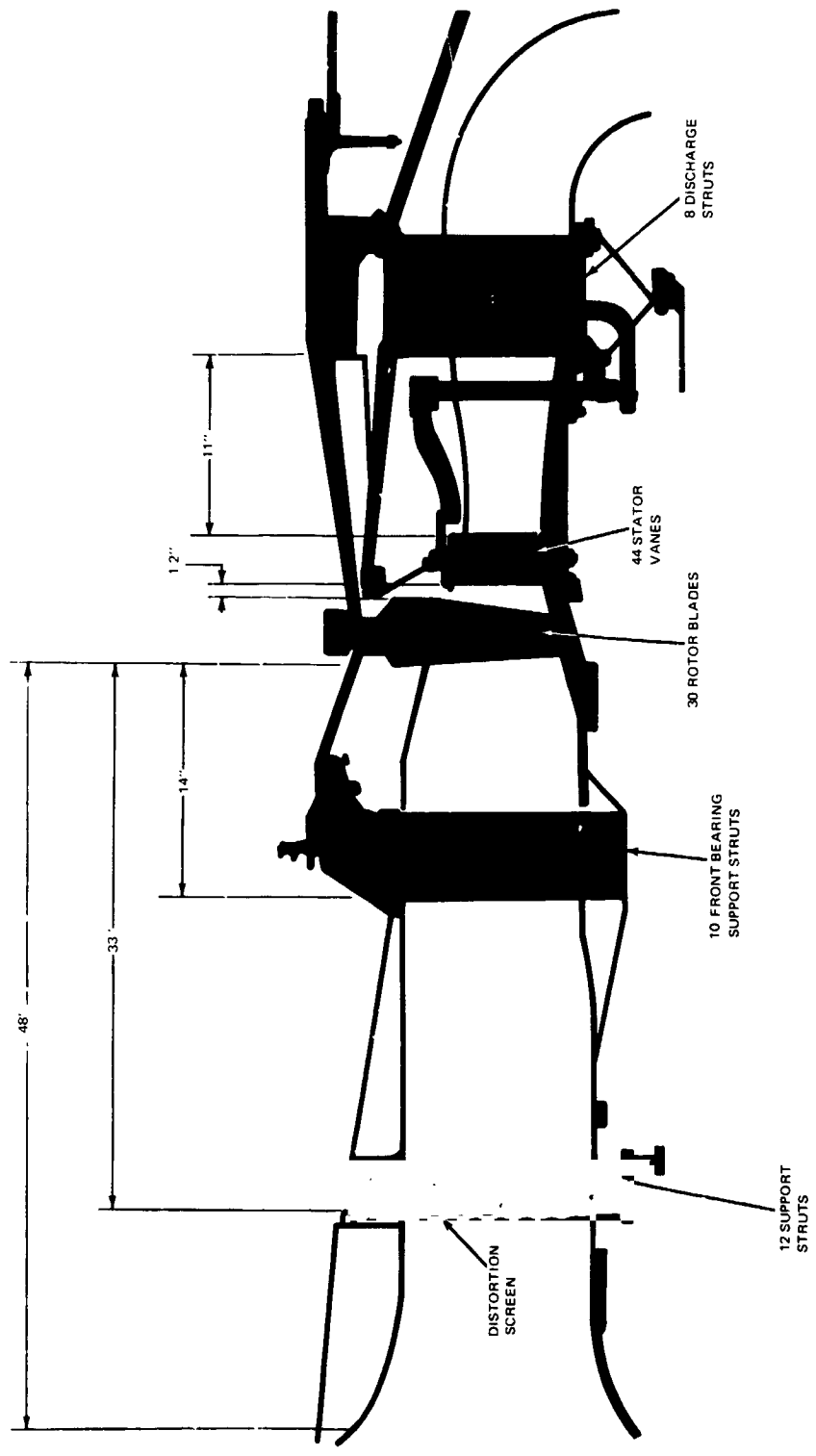


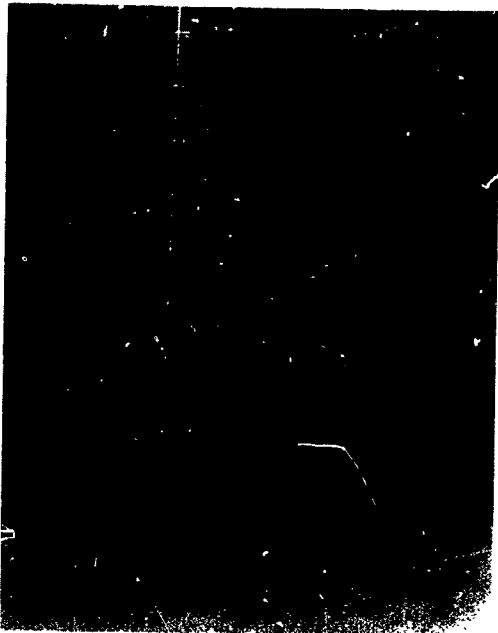
Figure 5 Cross-Section of Test Compressor



Convex Surface



Concave Surface

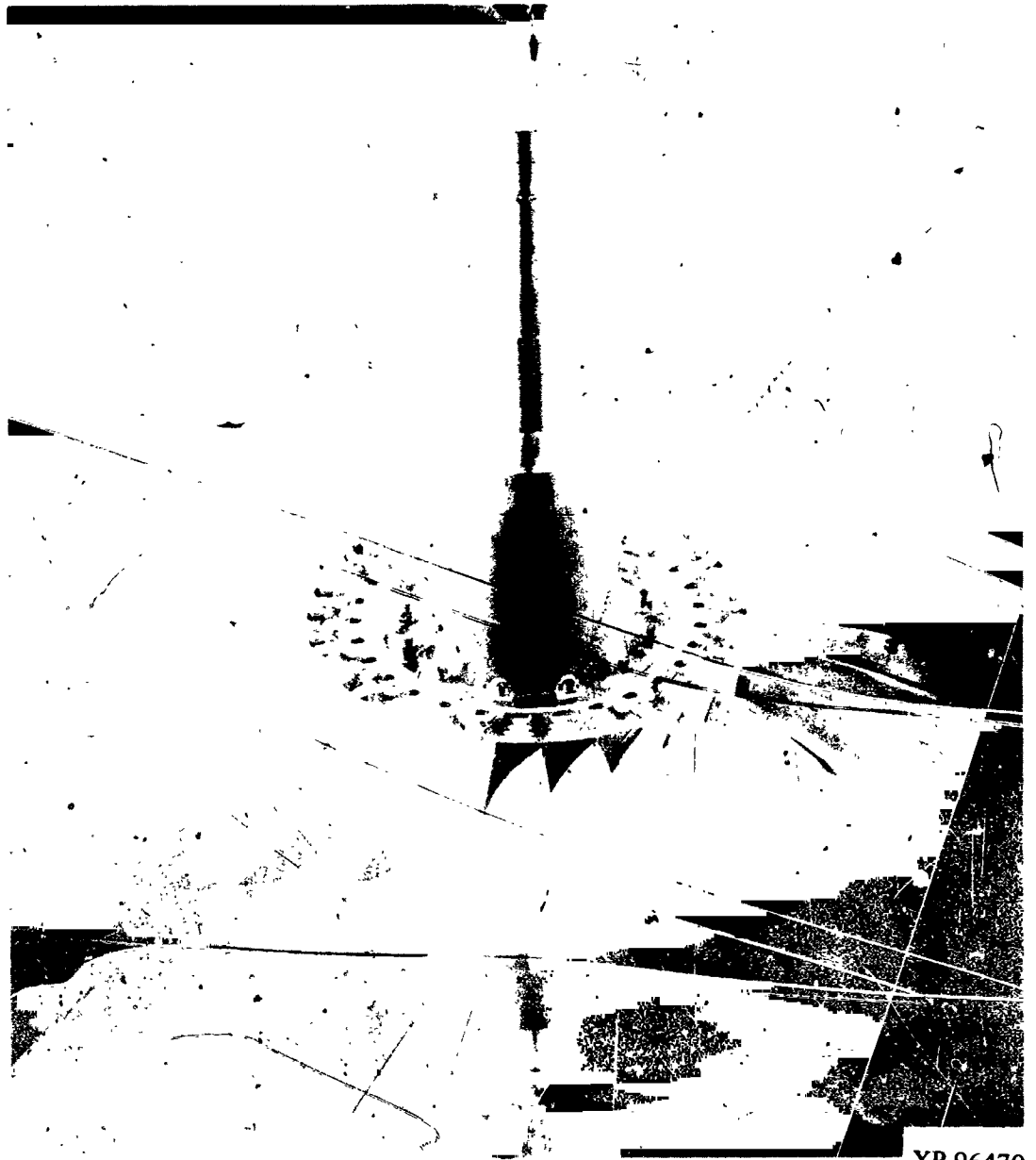


Leading Edge



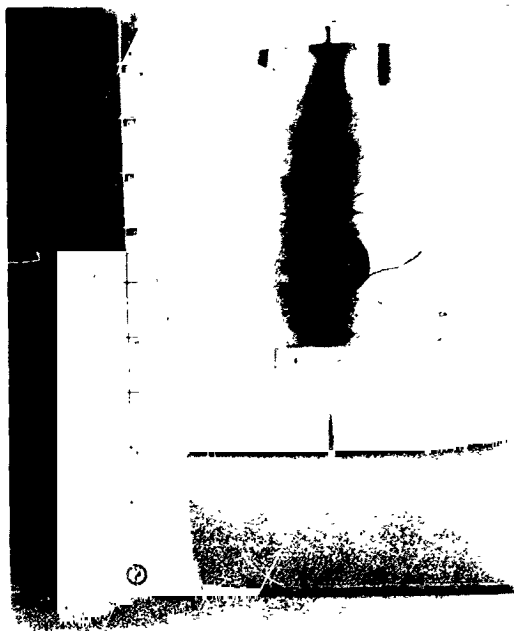
Trailing Edge

Figure 6 Multiple-Circular-Arc Rotor Blade

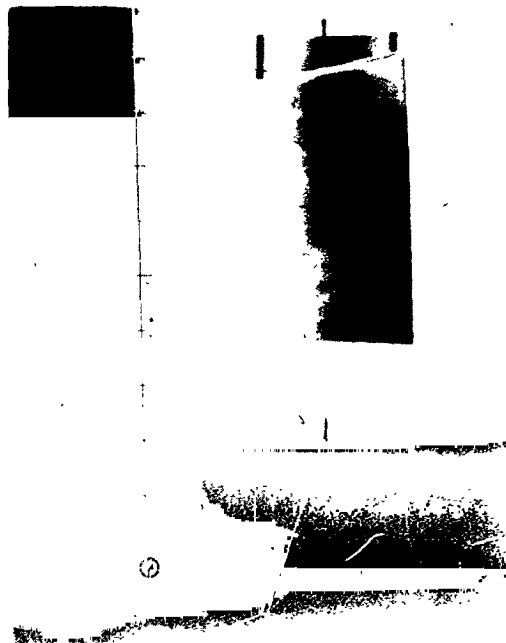


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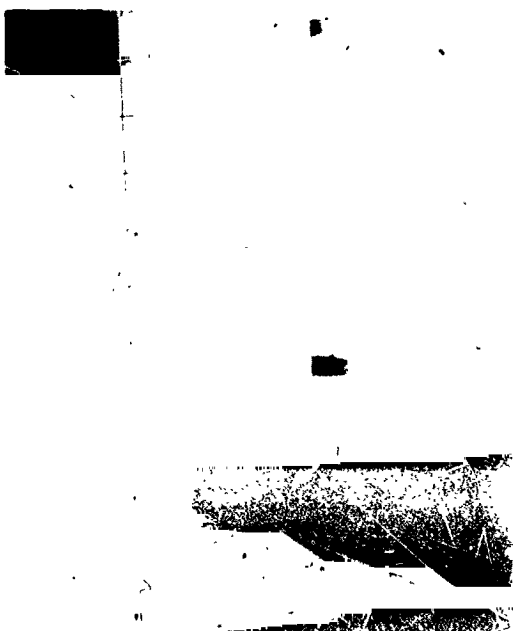
Figure 7 Assembled MCA Rotor



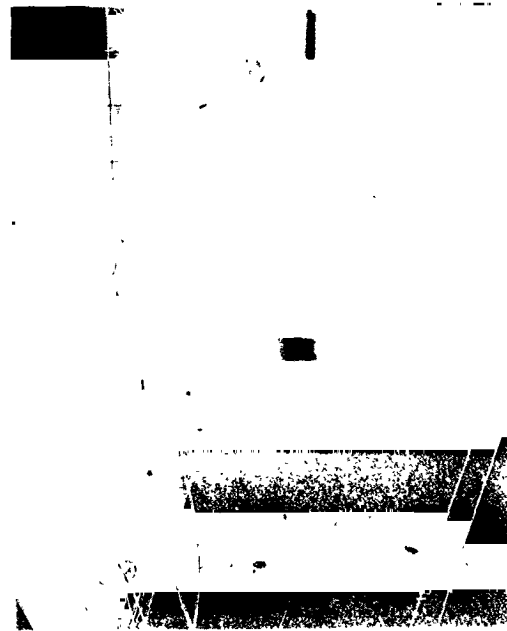
Convex Surface



Concave Surface



Leading Edge



Trailing Edge

Figure 8 Multiple Circular-Arc Stator Blade

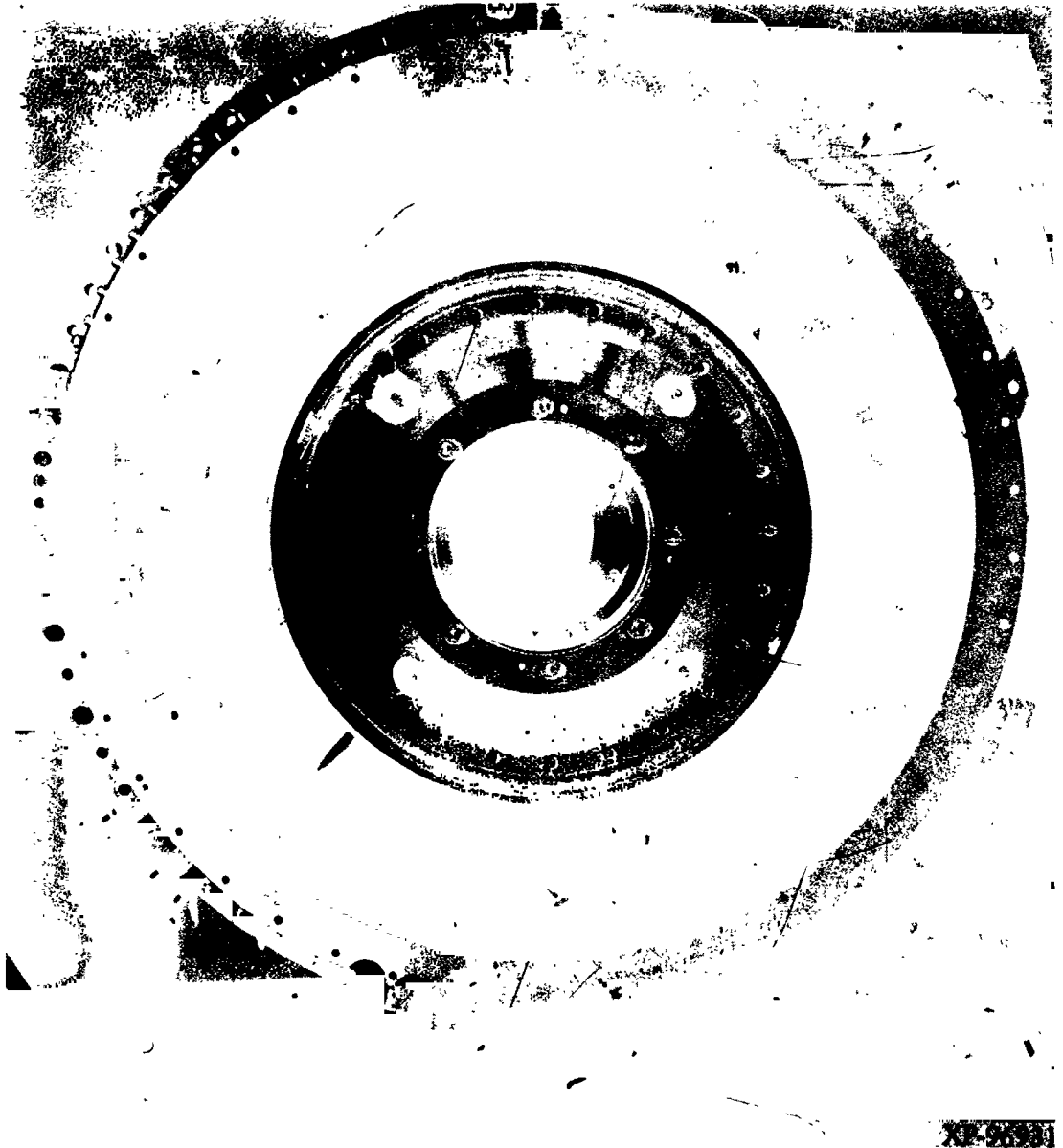


Figure 9 Assembled MCA Stator

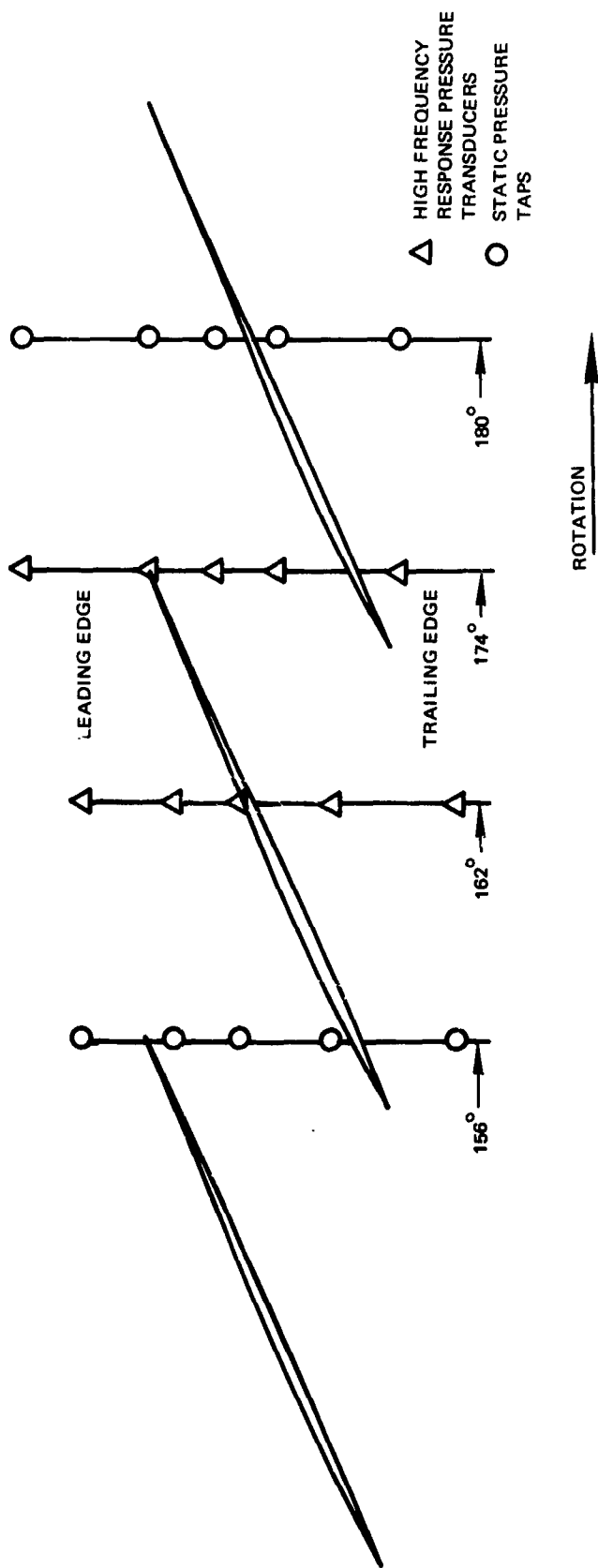
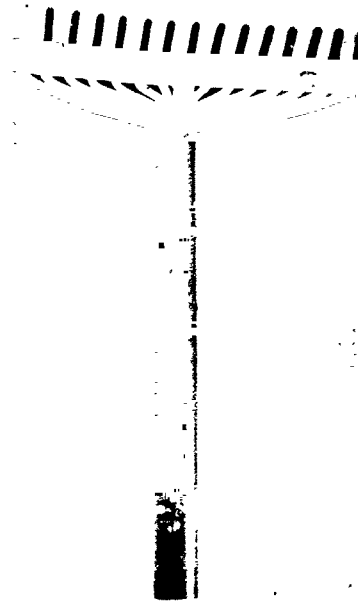


Figure 10 Rotor Blade Tip Shroud Instrumentation



XP-99889

Radial Temperature Rake



XPN-1815

Traversable Total Pressure Wake Rake



XP-99886

Total Pressure Rake



XP-99893

Traversable Disk Probe

Figure 11 Typical Instrumentation

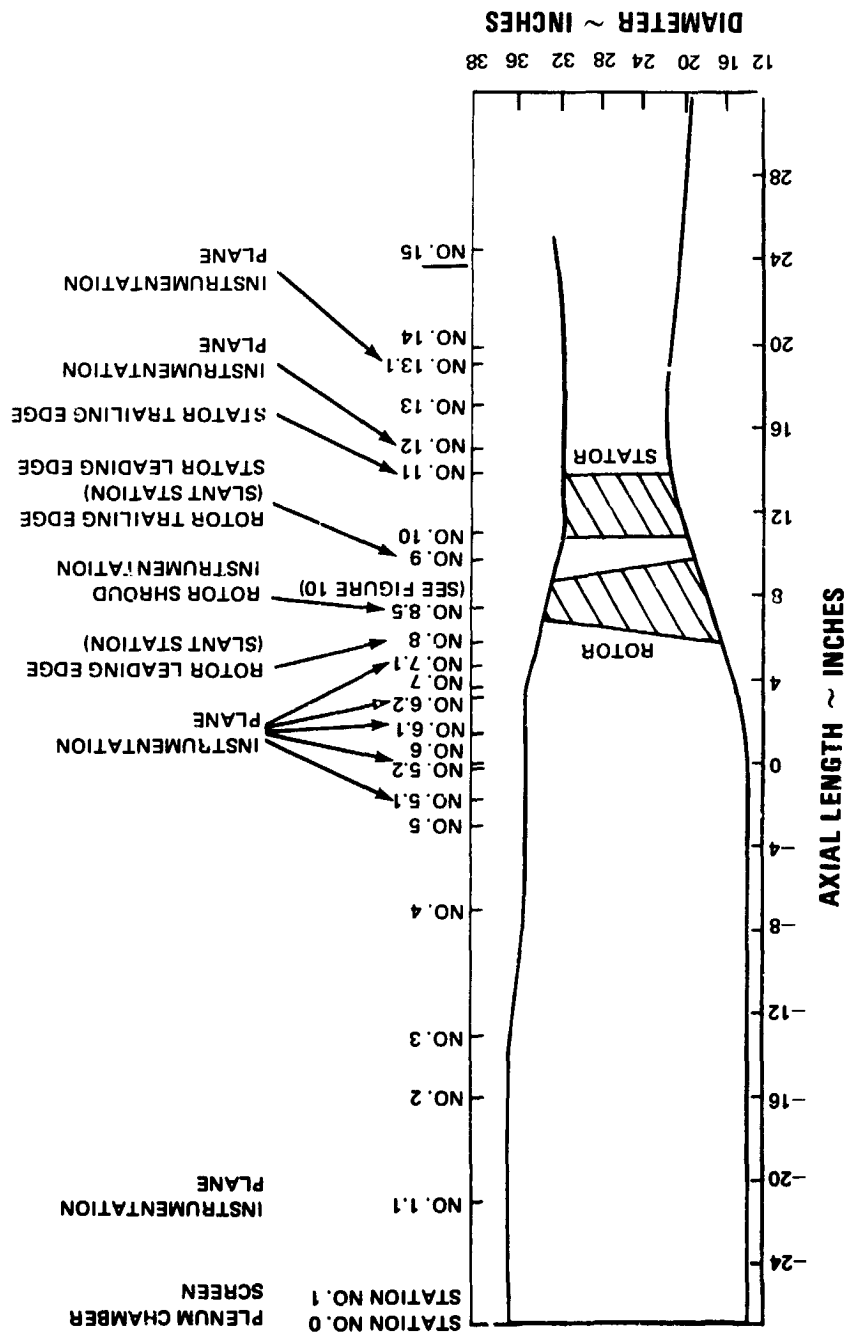


Figure 12 Axial Station Number Designation and Location of Instrumentation

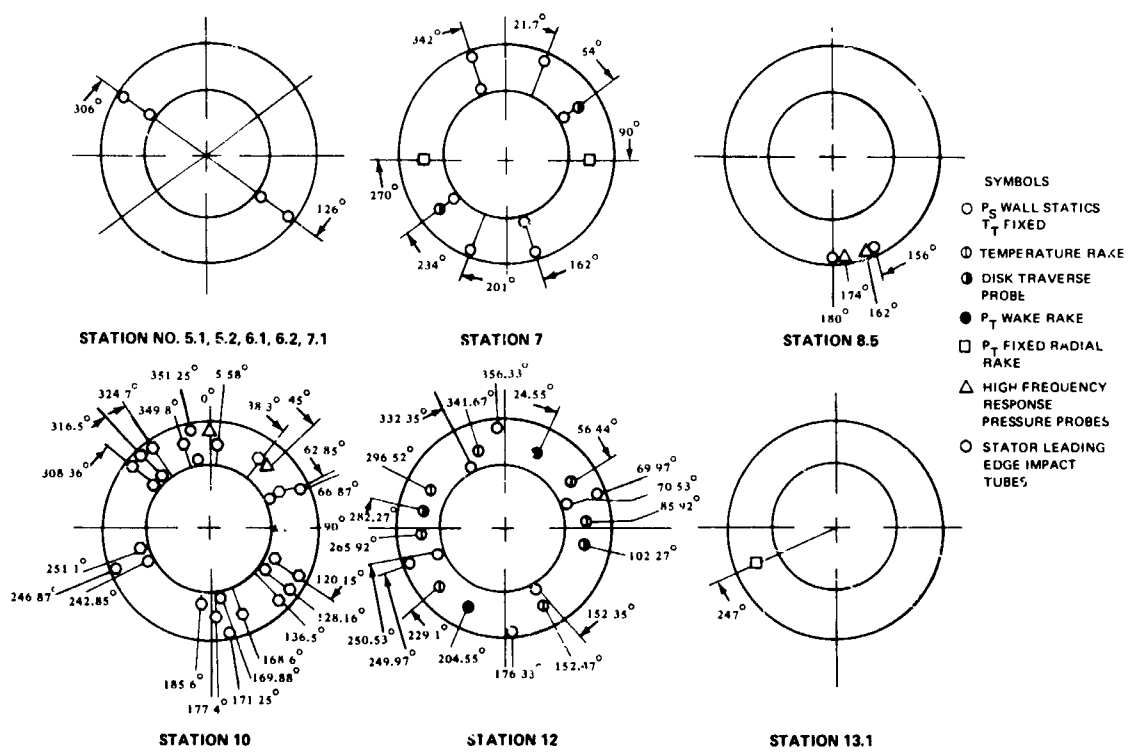


Figure 13 Circumferential Location of Instrumentation, Viewed from Rear

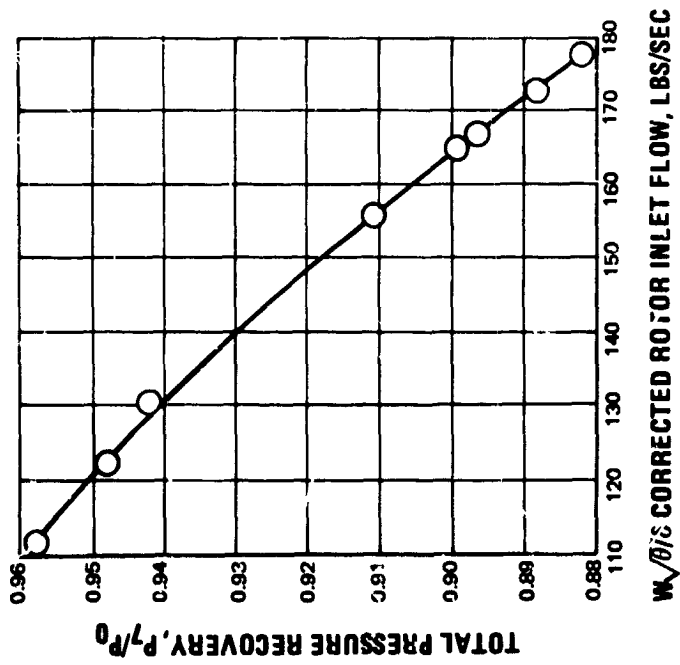


Figure 14 Circumferential Screen Pressure Recovery

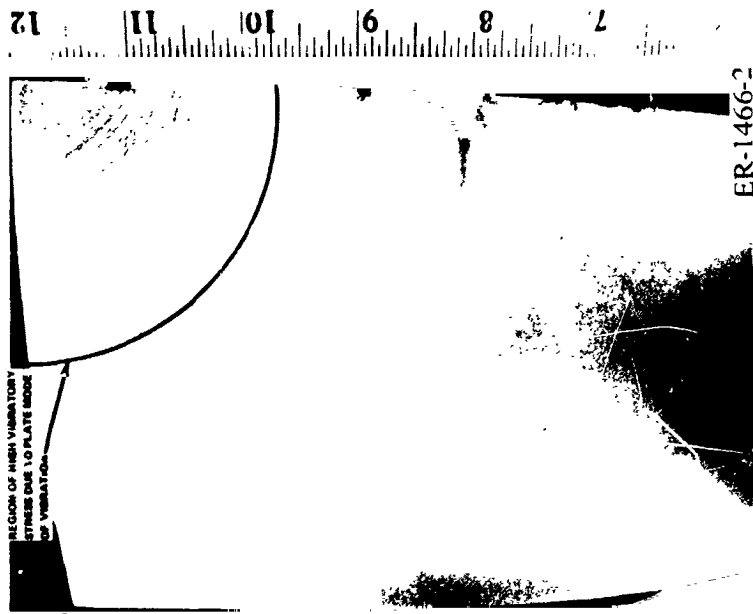


Figure 15 Plate Mode Vibration at Rotor Tip

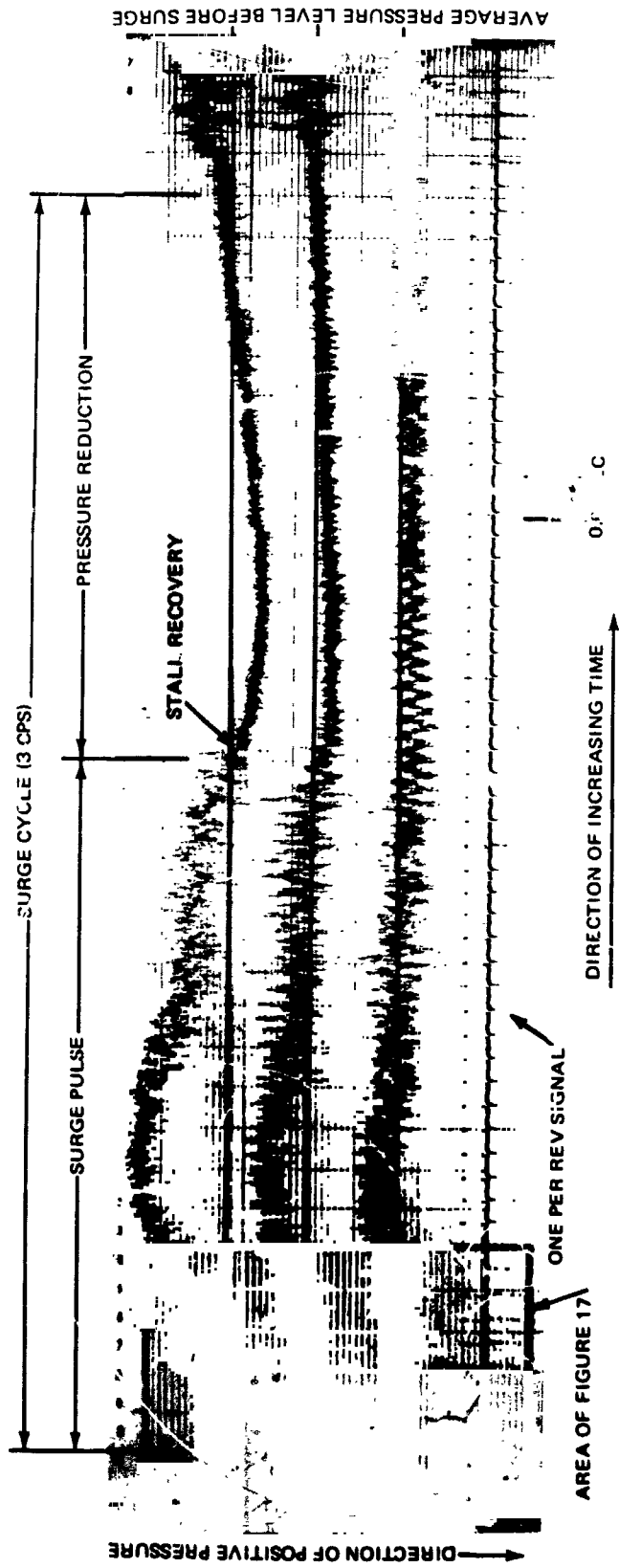


Figure 16 Oscillograph Trace of Typical Surge Cycle

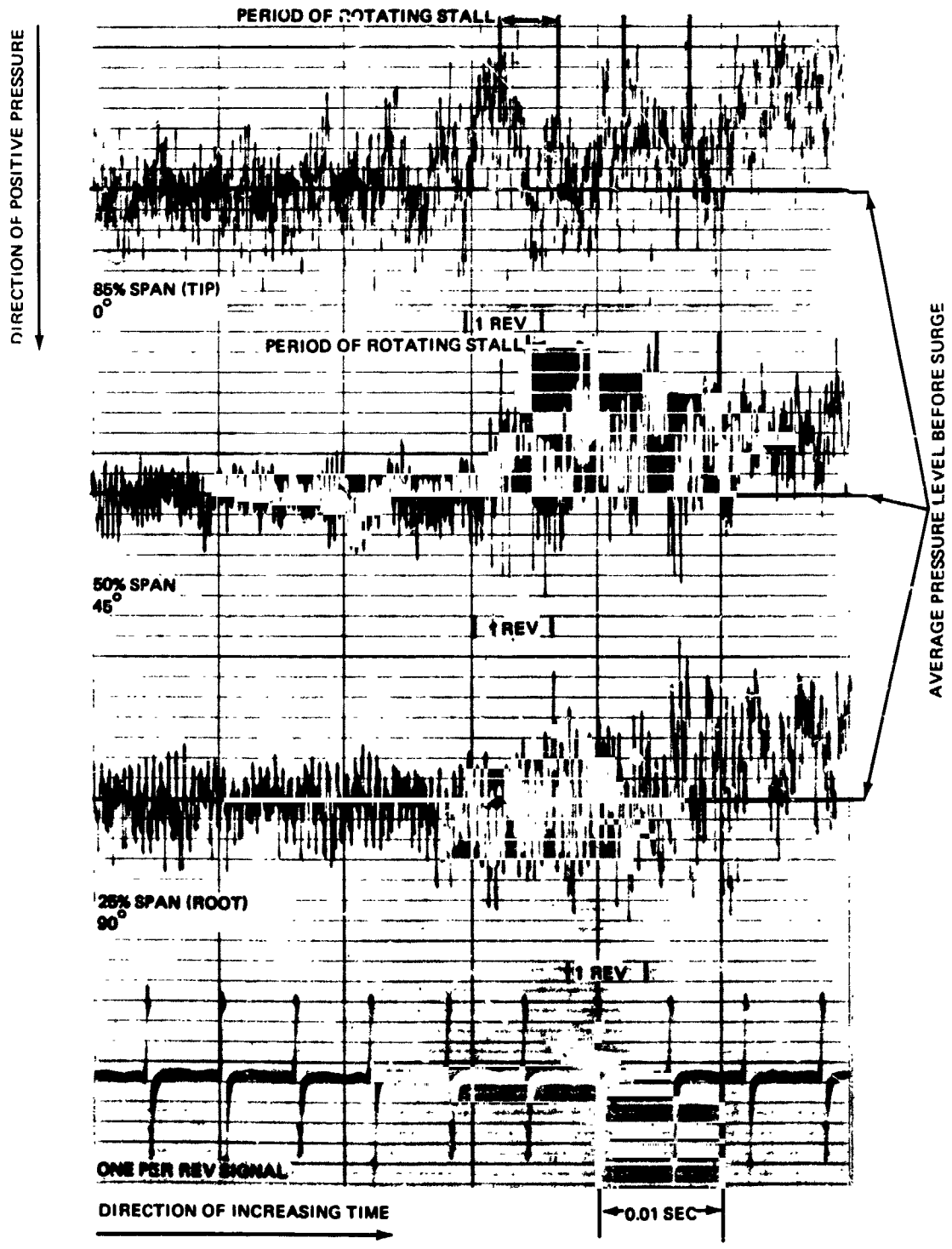


Figure 17 Oscillograph Trace of Typical Rotating Stall Pattern

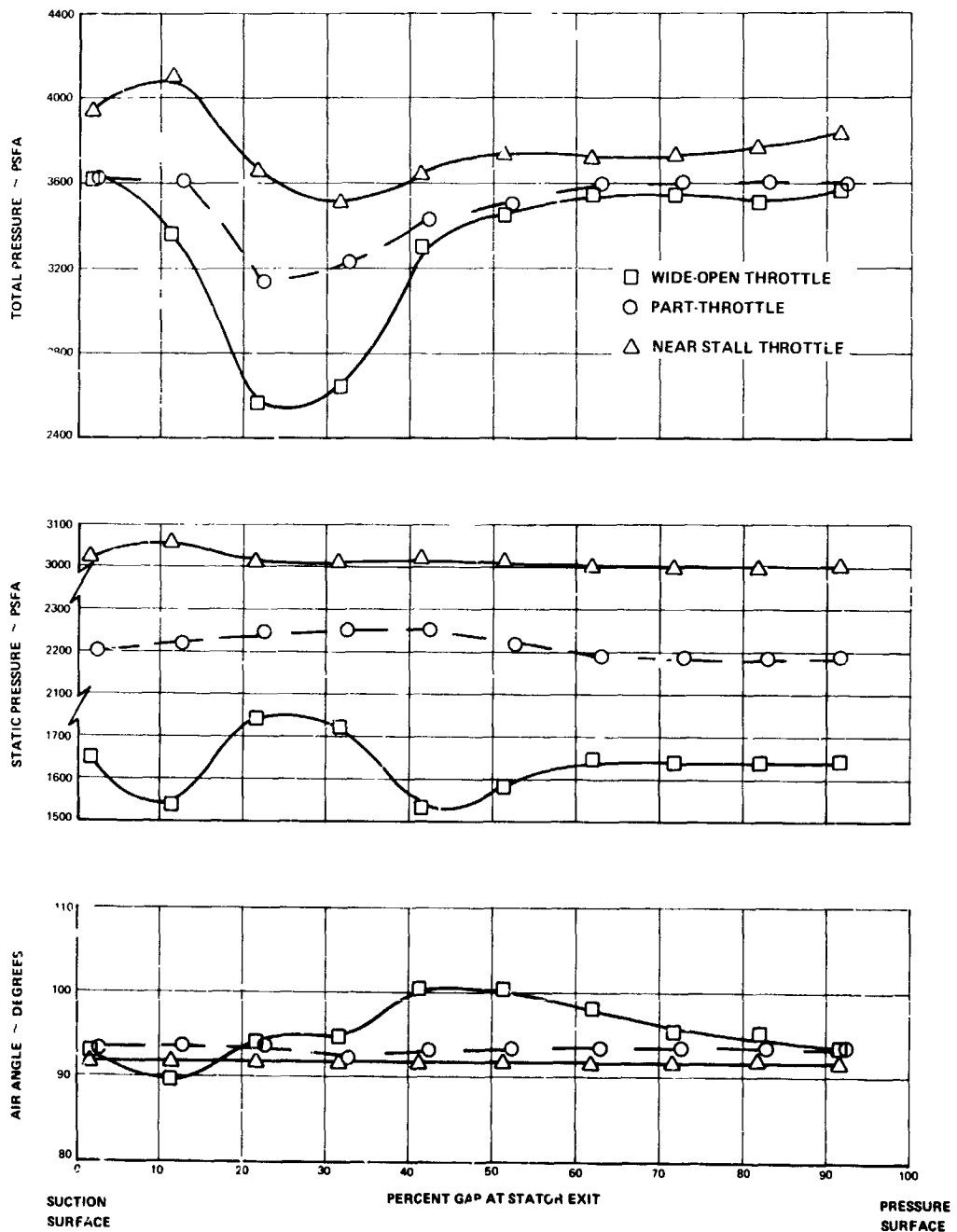


Figure 18 Circumferential Variation in Stator Exit Total Pressure, Static Pressure, and Air Angle from Tangential Traverses at Station 12, 100% Design Speed, 10% Span

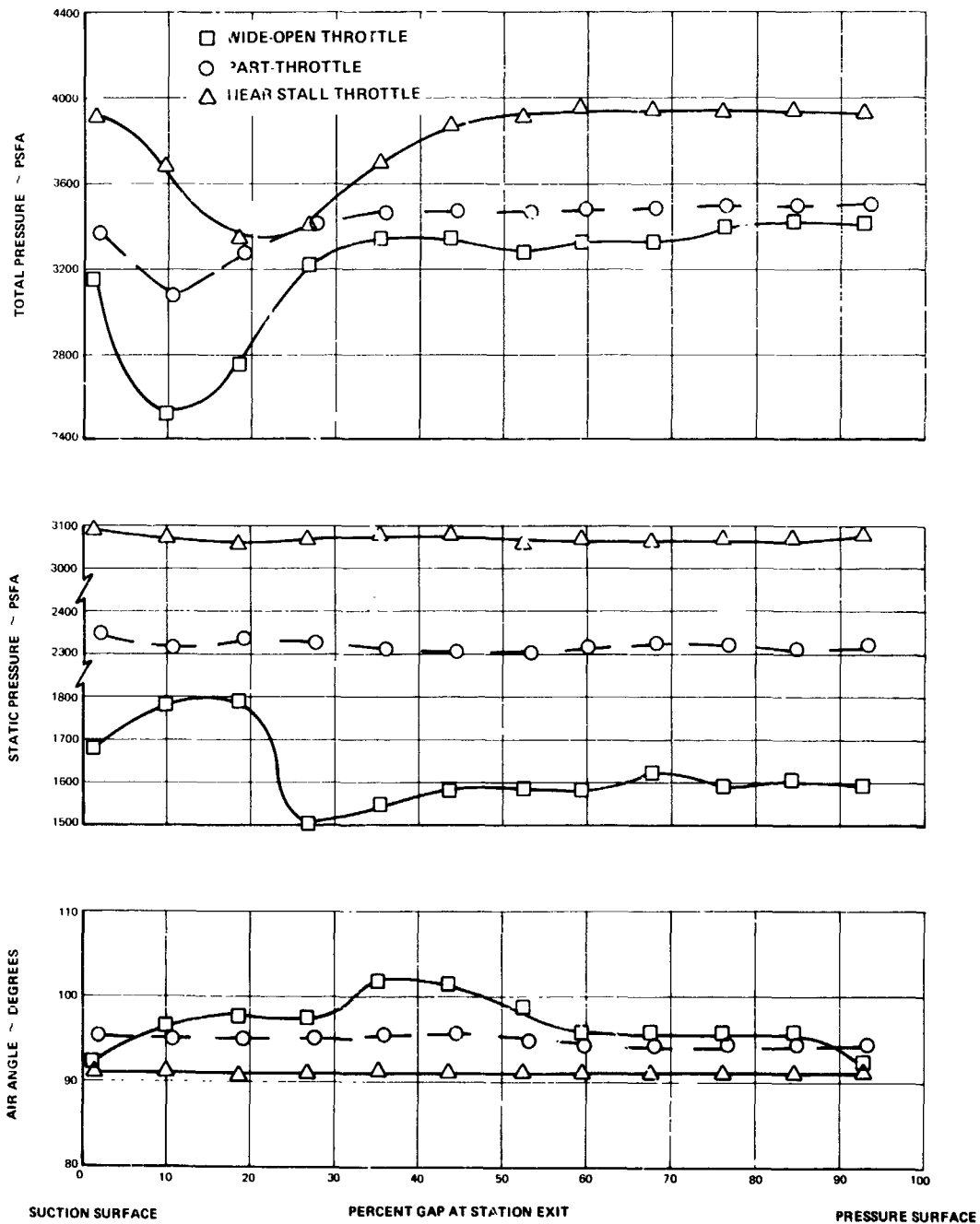


Figure 19 Circumferential Variation in Stator Exit Total Pressure, Static Pressure and Air Angle from Tangential Traverses at Station 12, 100% Design Speed, 50% Span

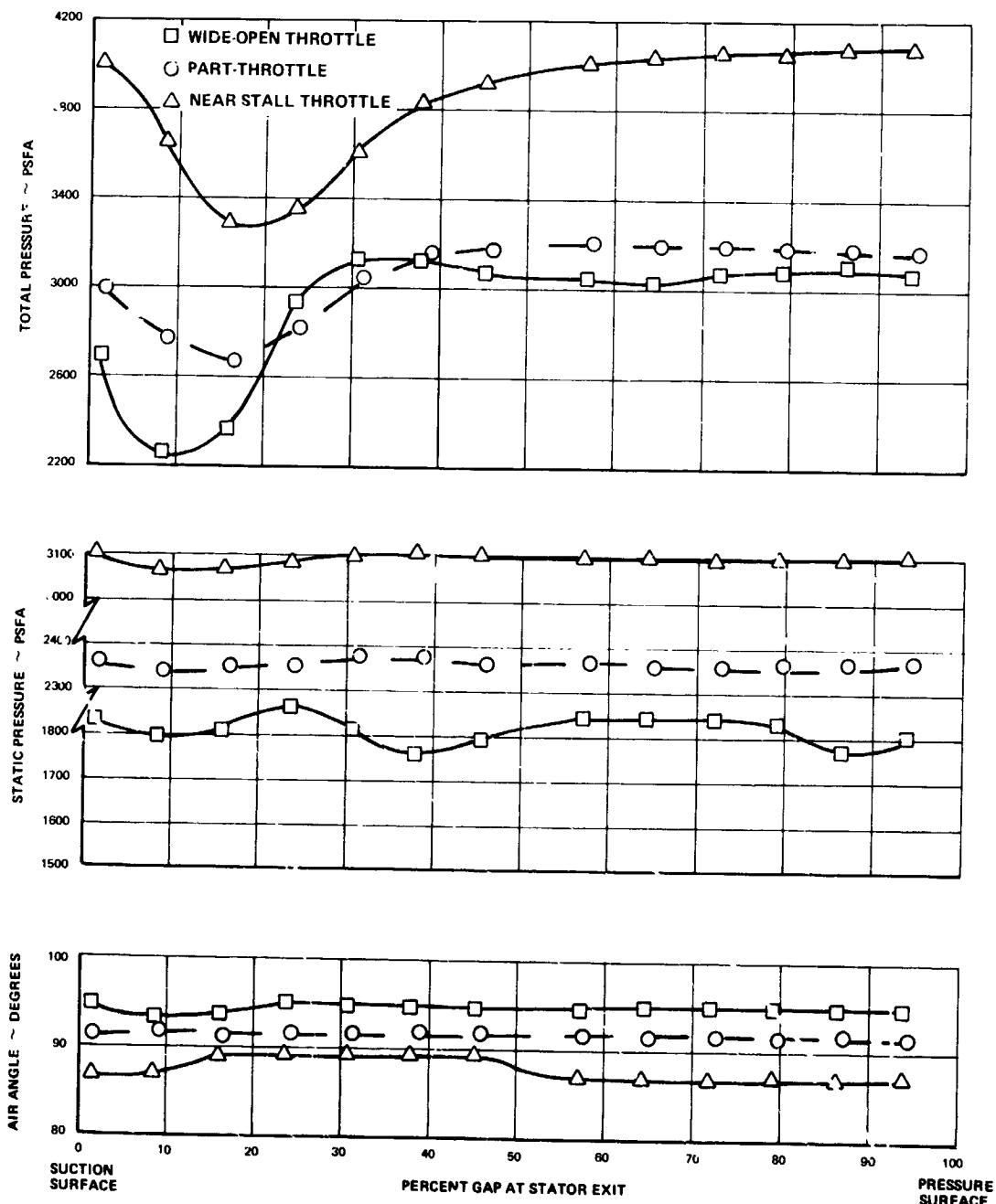


Figure 20 Circumferential Variation in Stator Exit Total Pressure, Static Pressure, and Air Angle from Tangential Traverses at Station 12, 100% Design Speed, 90% Span

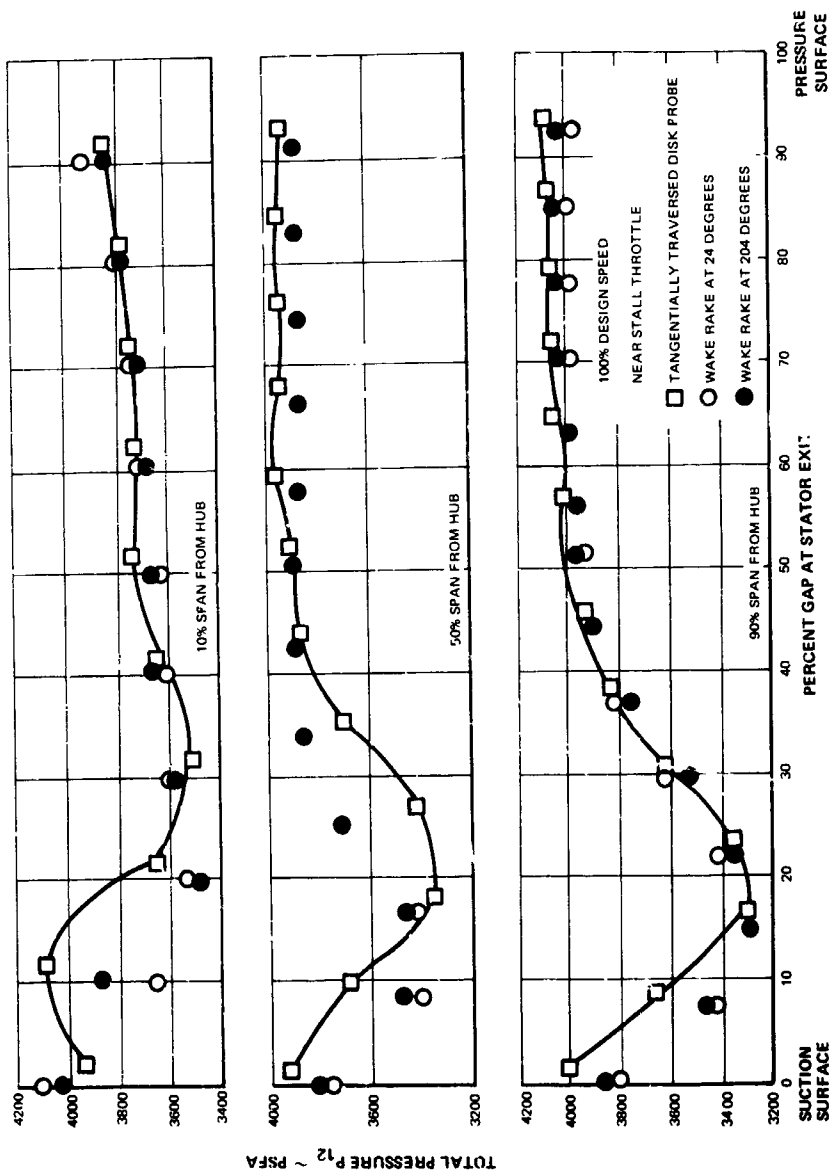


Figure 21 Comparison of Circumferential Variation in Stator Exit Total Pressure from Tangential and Wake Rake Traverses at Station 12, 100% Design Speed, 10%, 50%, and 90% Spans

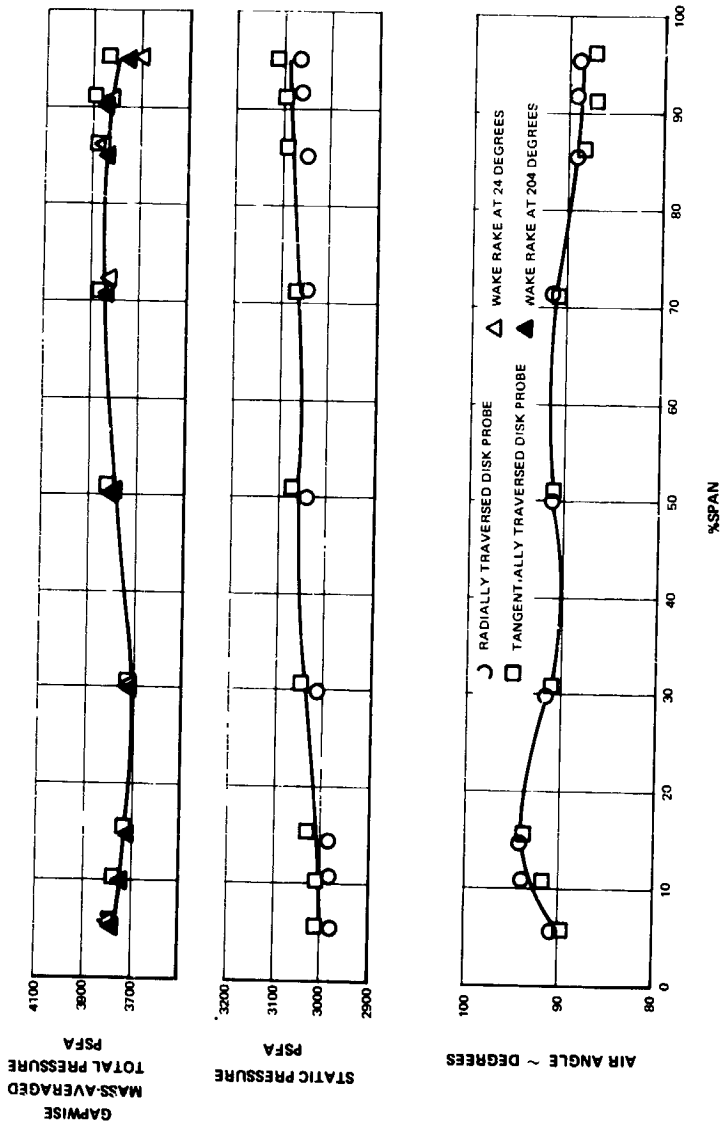


Figure 22 Comparison of Spanwise Variations in Total Pressure, Static Pressure, and Air Angle from a Tangentially Traversed Disk Probe, a Radially Traversed Disk Probe, and a Total Pressure Wake Rake, 100% Design Speed.

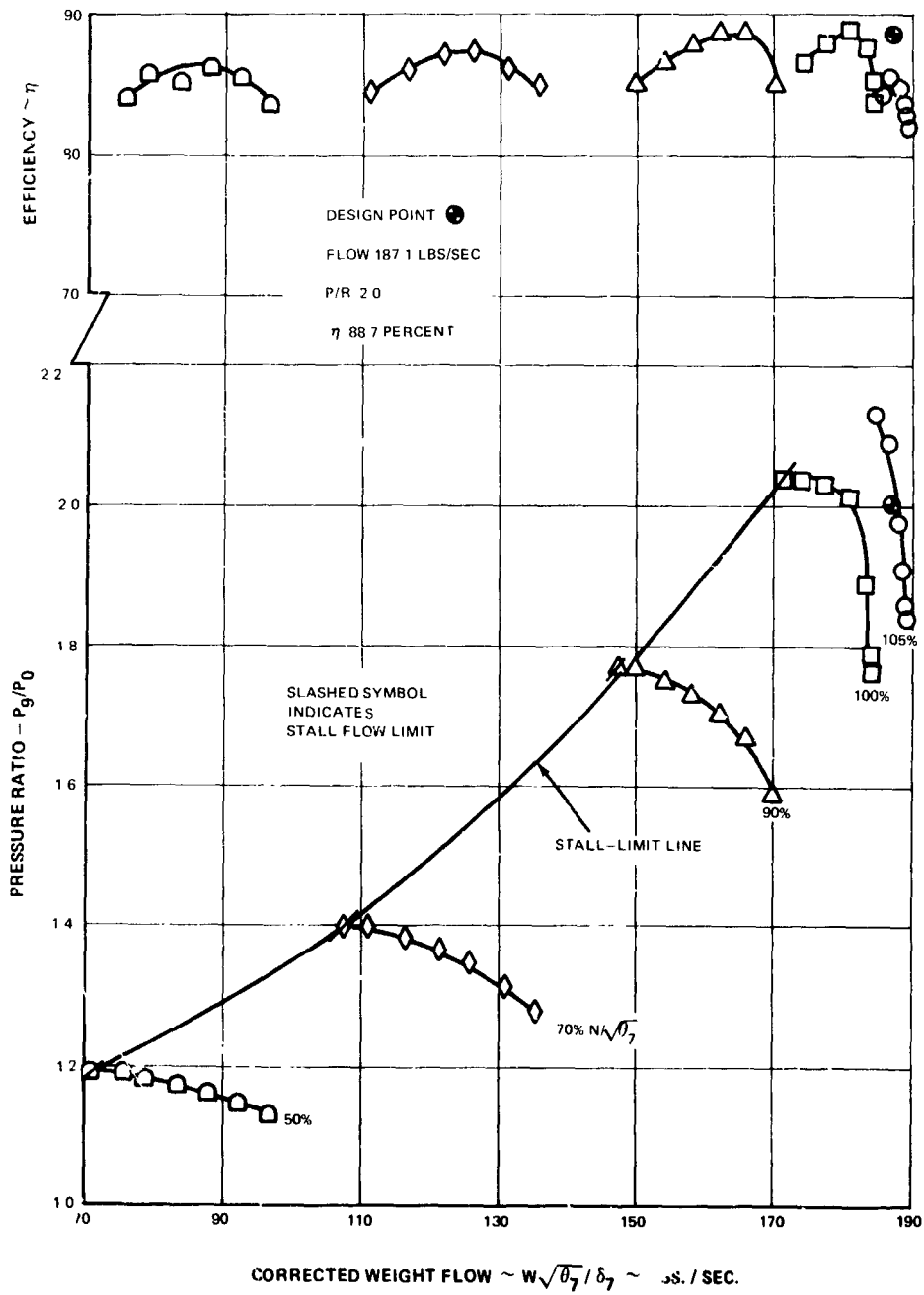


Figure 23 Rotor Over-all Performance with Uniform Inlet Flow

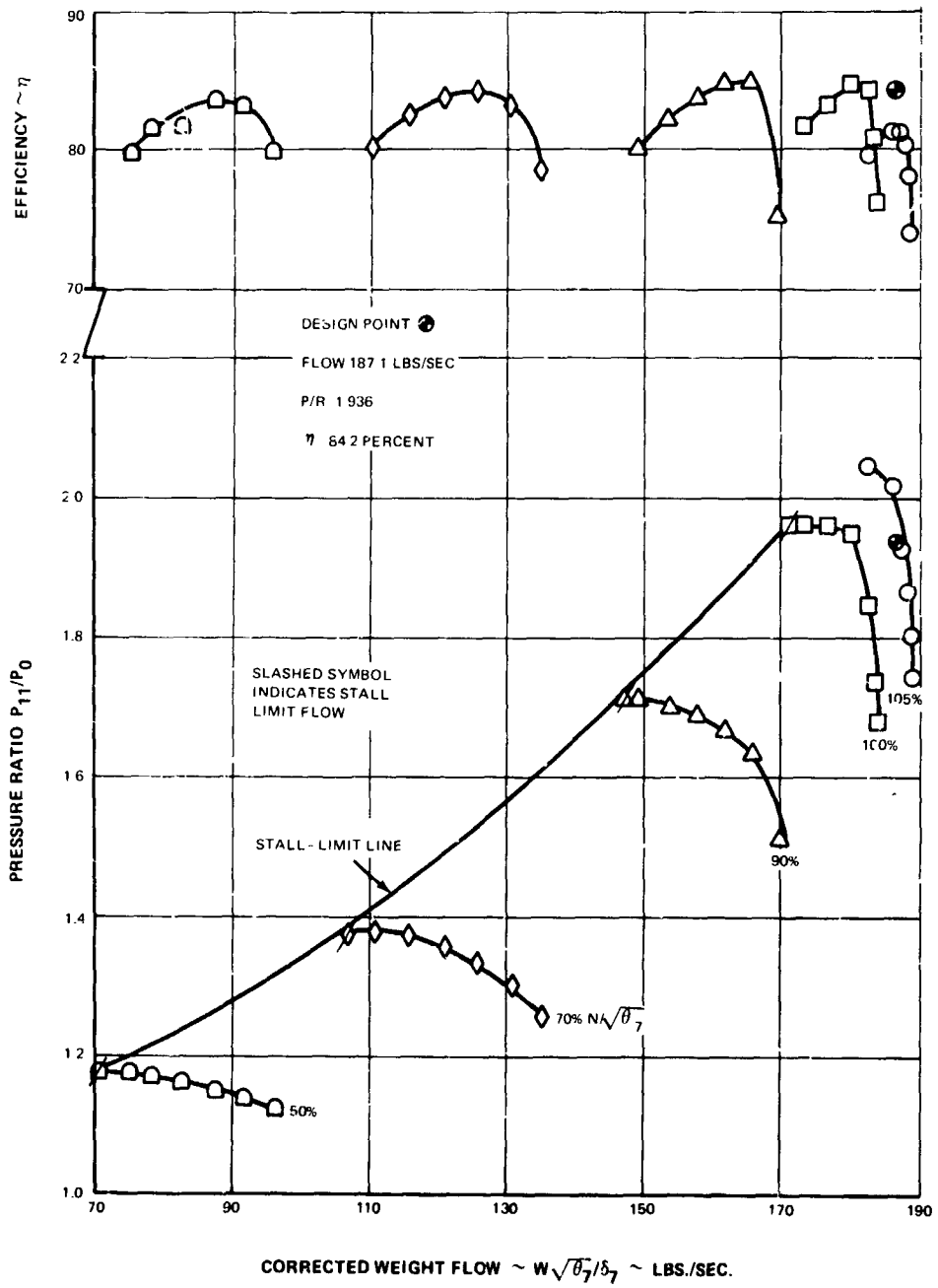


Figure 24 Stage Over-all Performance with Uniform Inlet Flow

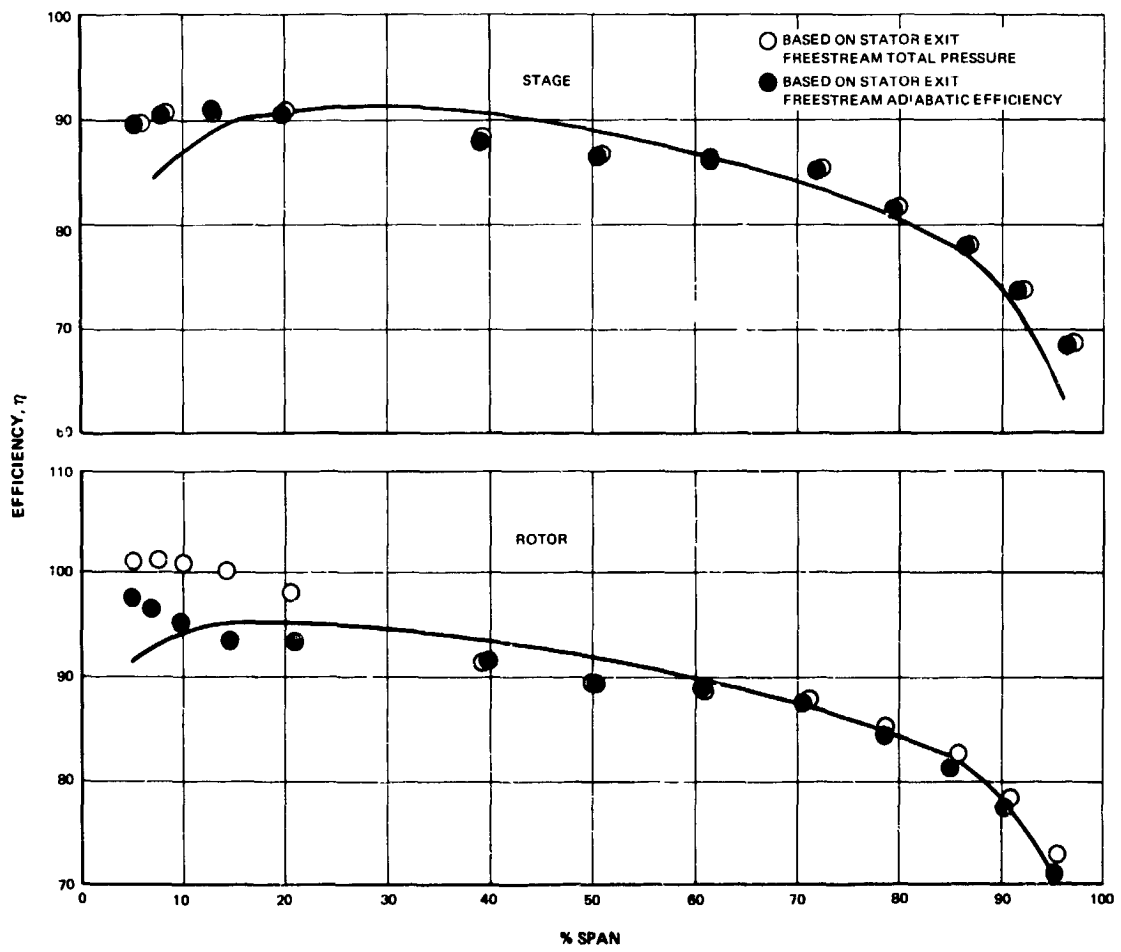


Figure 25 Rotor and Stage Spanwise Efficiency

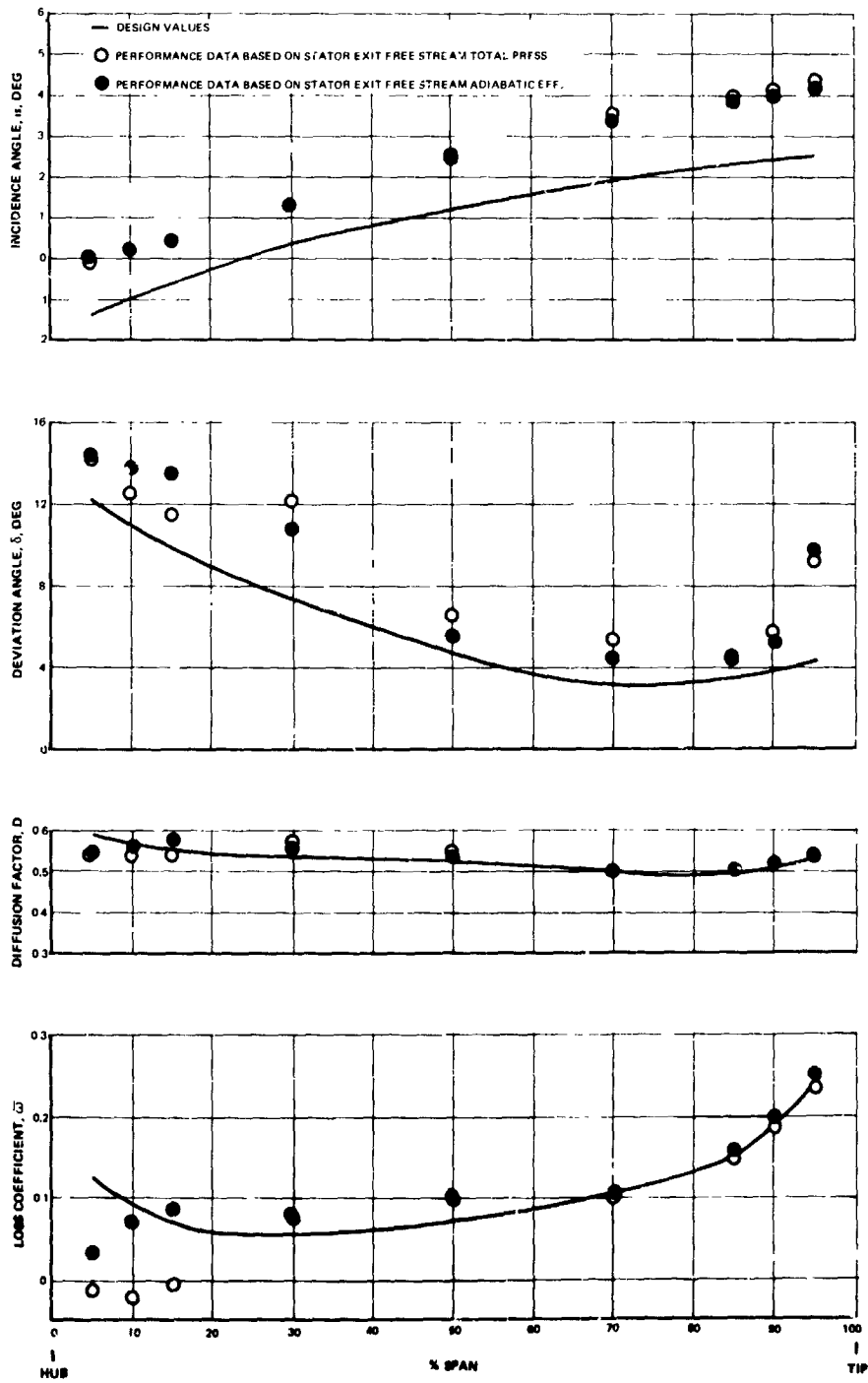


Figure 26 Comparison of Spanwise Rotor Blade Element Performance

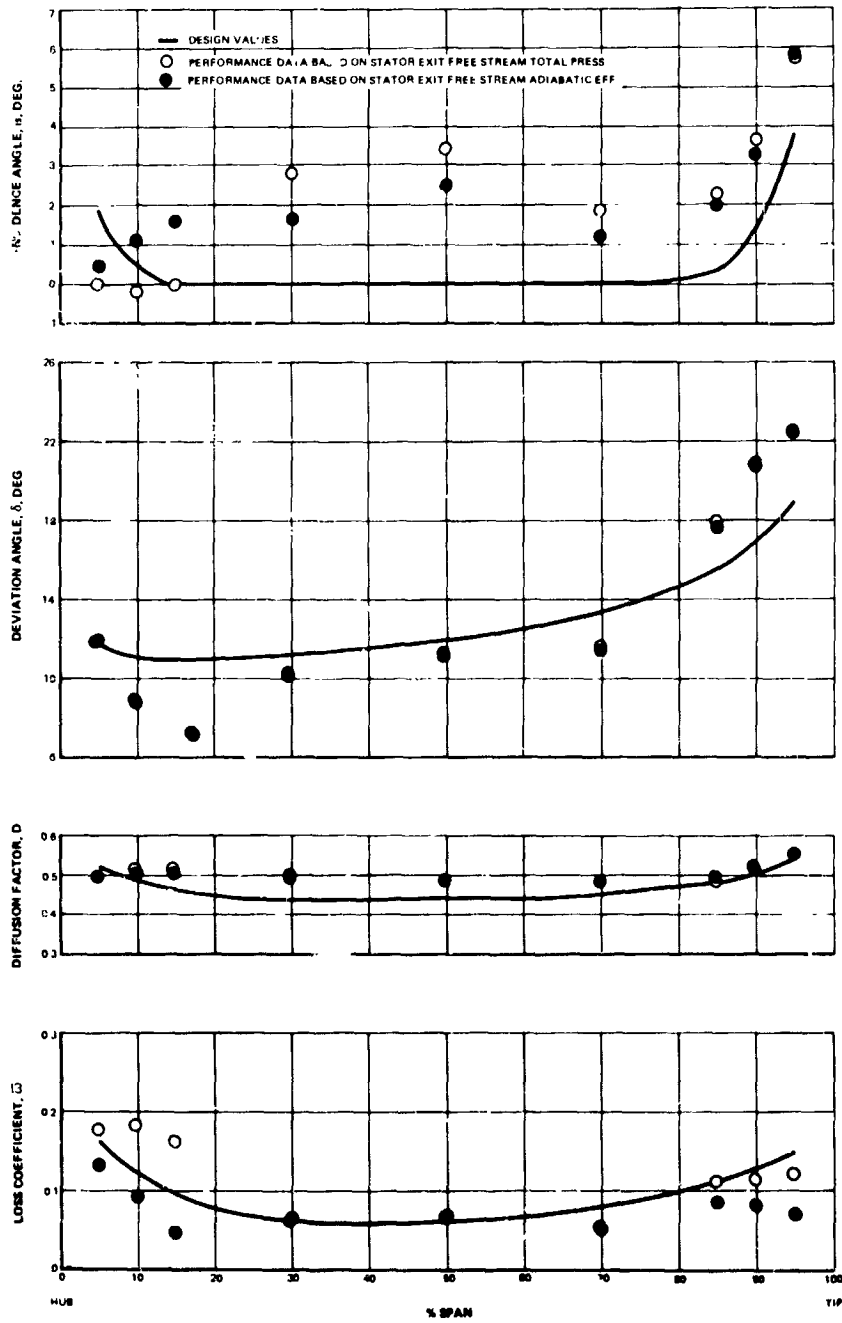


Figure 27 Comparison of Spanwise Stator Blade Element Performance

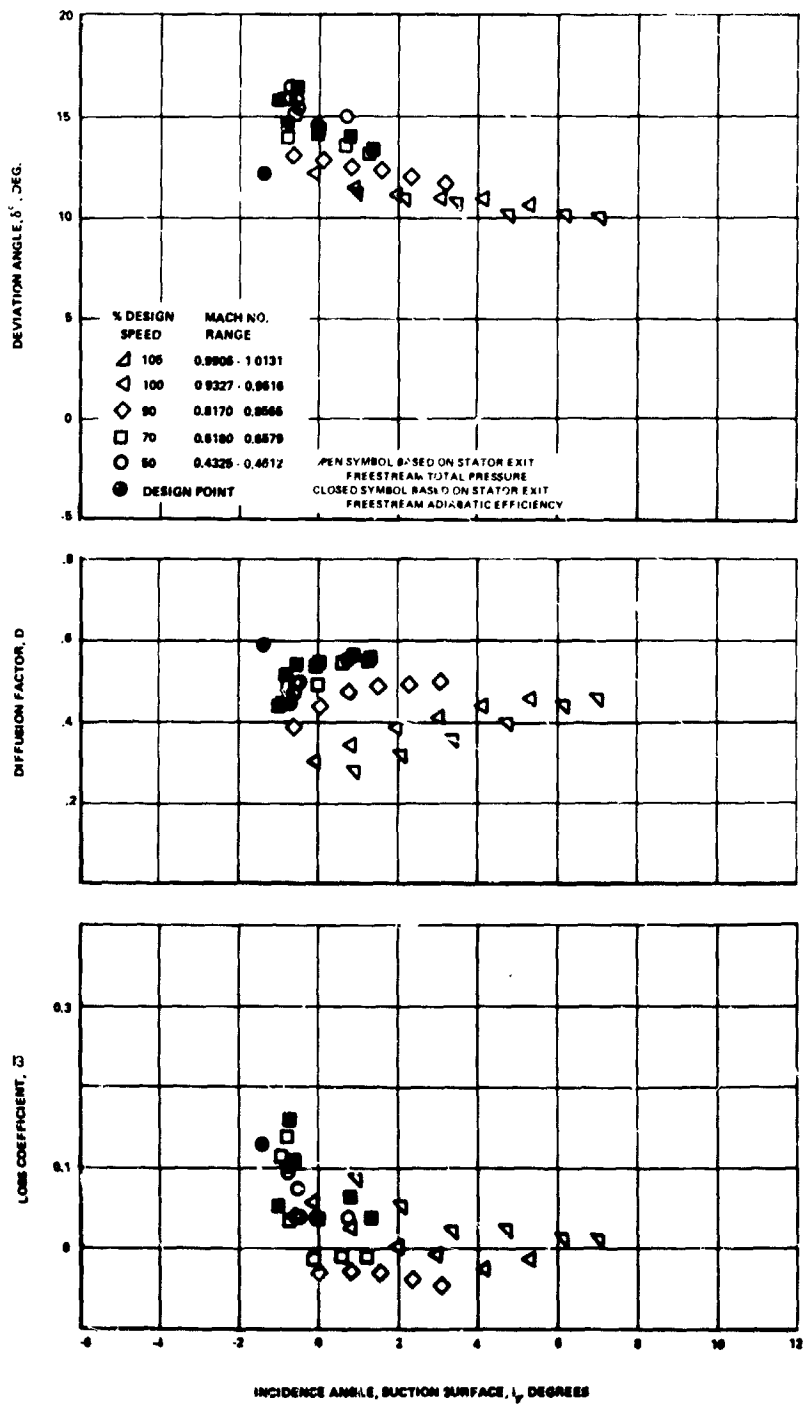


Figure 28a Rotor Blade Element Performance with Uniform Inlet Flow, 5% Span

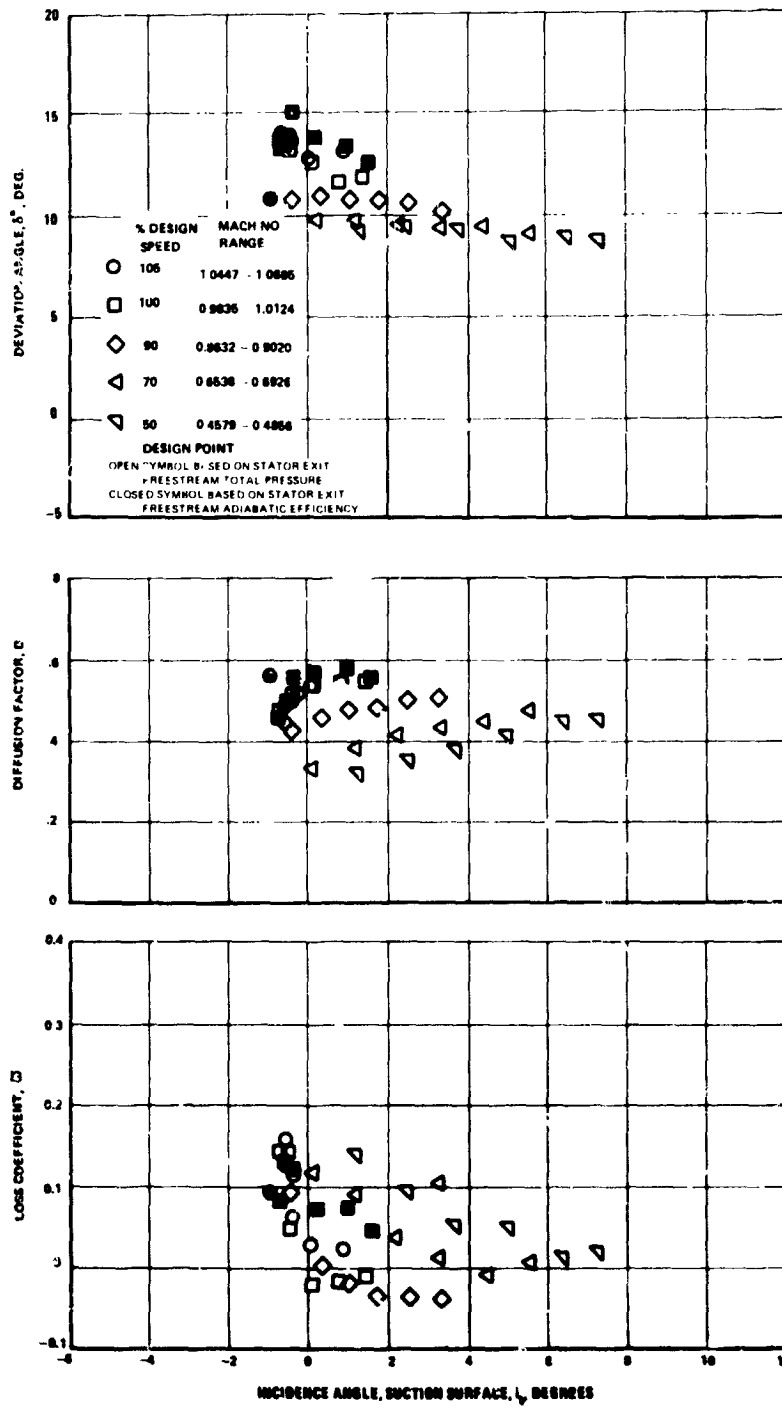


Figure 28b Rotor Blade Element Performance with Uniform Inlet Flow, 10% Span

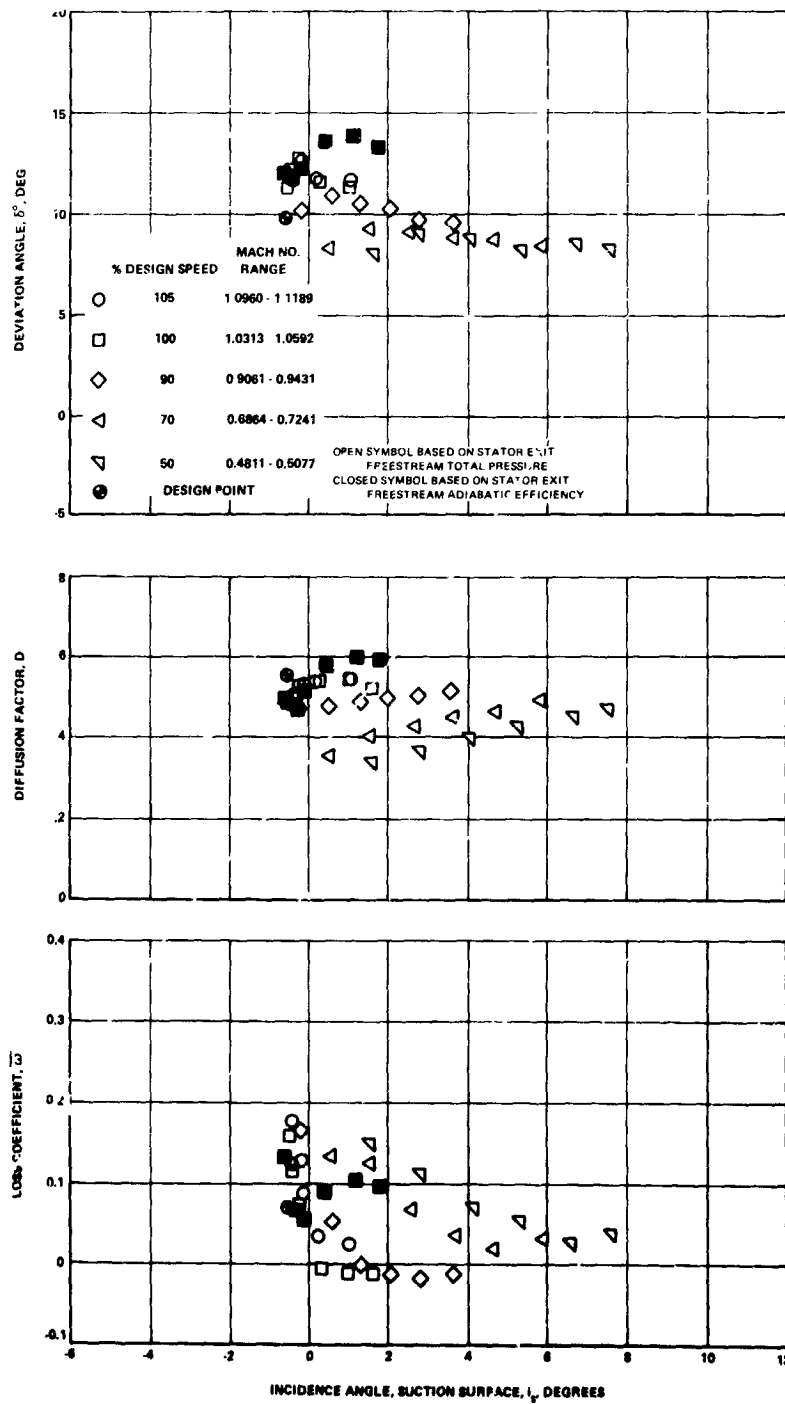


Figure 28c Rotor Blade Element: Performance with Uniform Inlet Flow, 15% Span

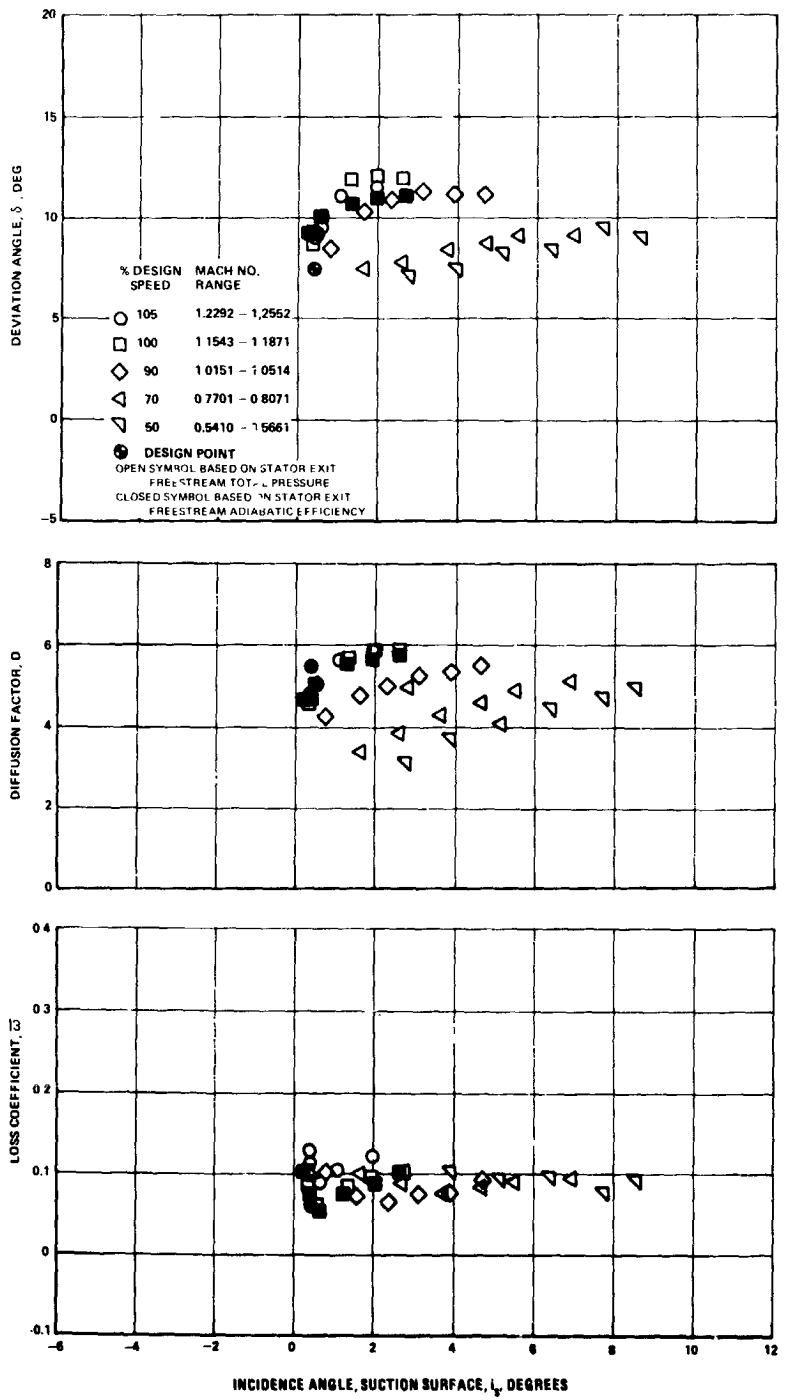


Figure 28 d Rotor Blade Element Performance with Uniform Inlet Flow, 30% Span

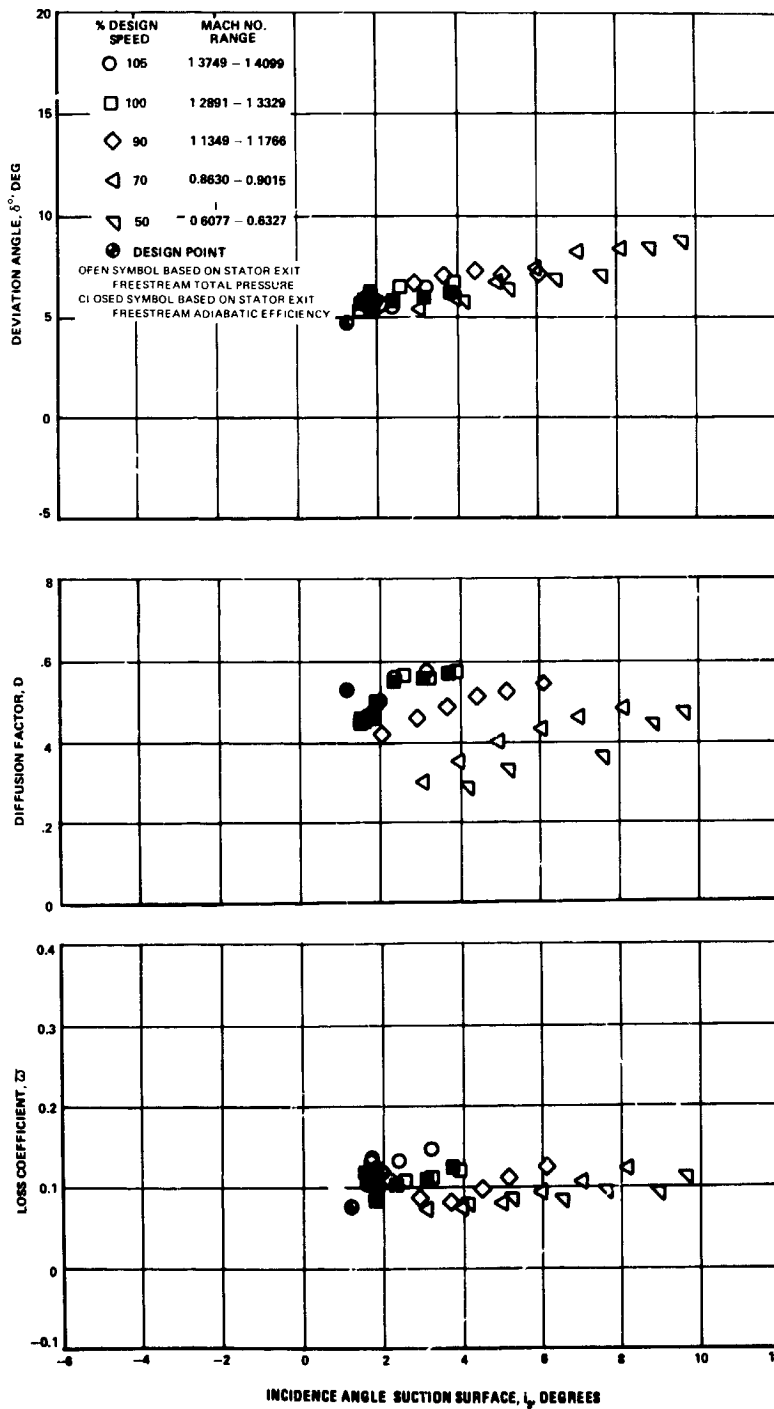


Figure 28 e Rotor Blade Element Performance with Uniform Inlet Flow, 50% Span

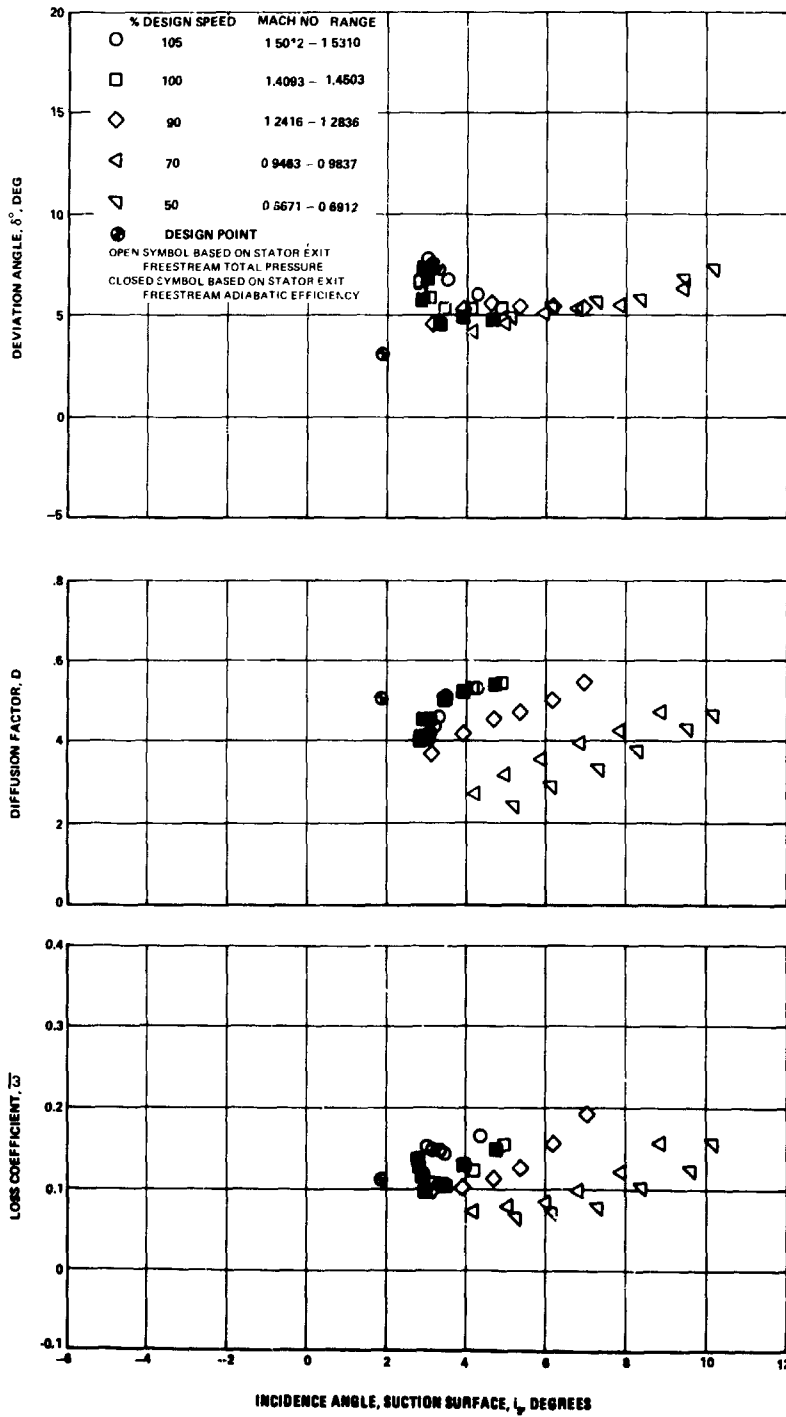


Figure 28 f Rotor Blade Element Performance with Uniform Inlet Flow, 70% Span

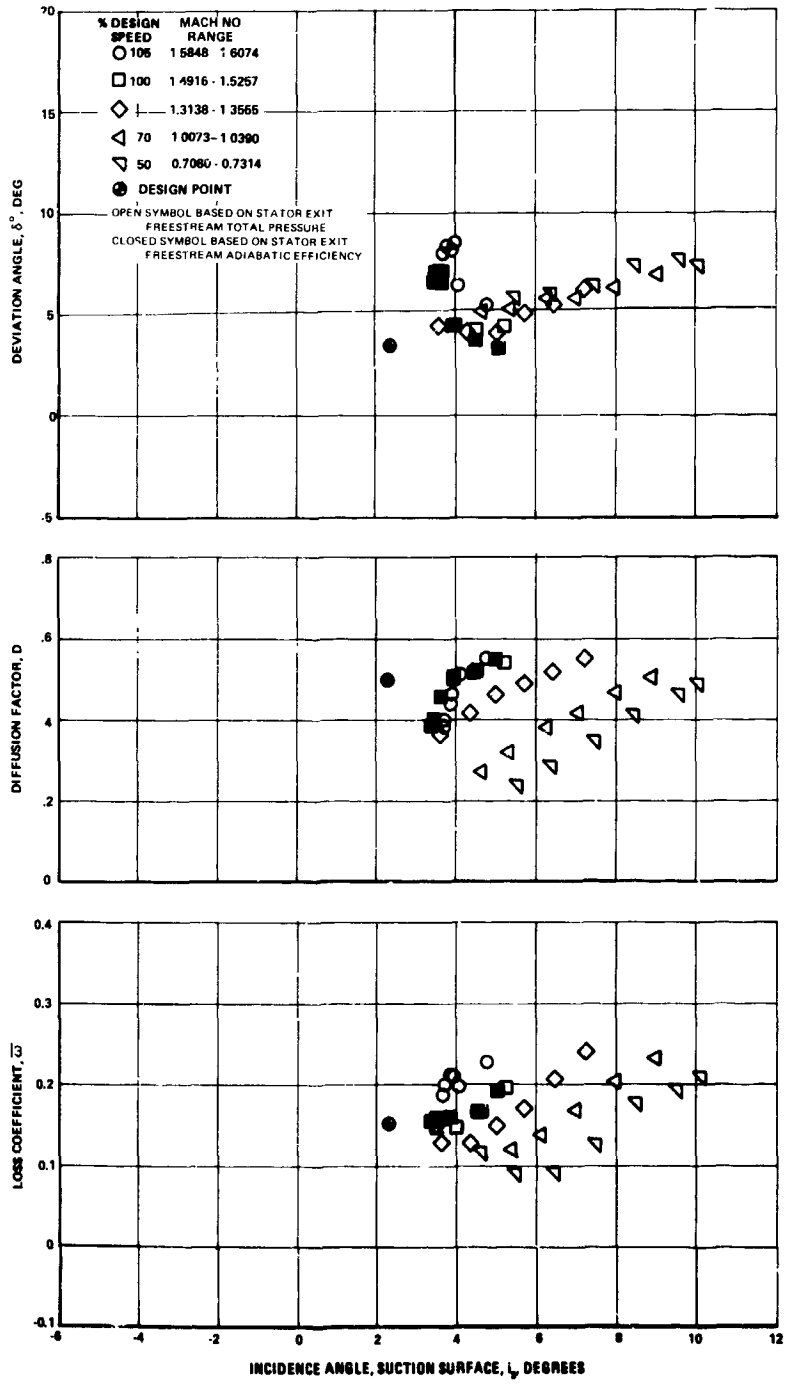


Figure 28 g Rotor Blade Element Performance with Uniform Inlet Flow, 85% Span

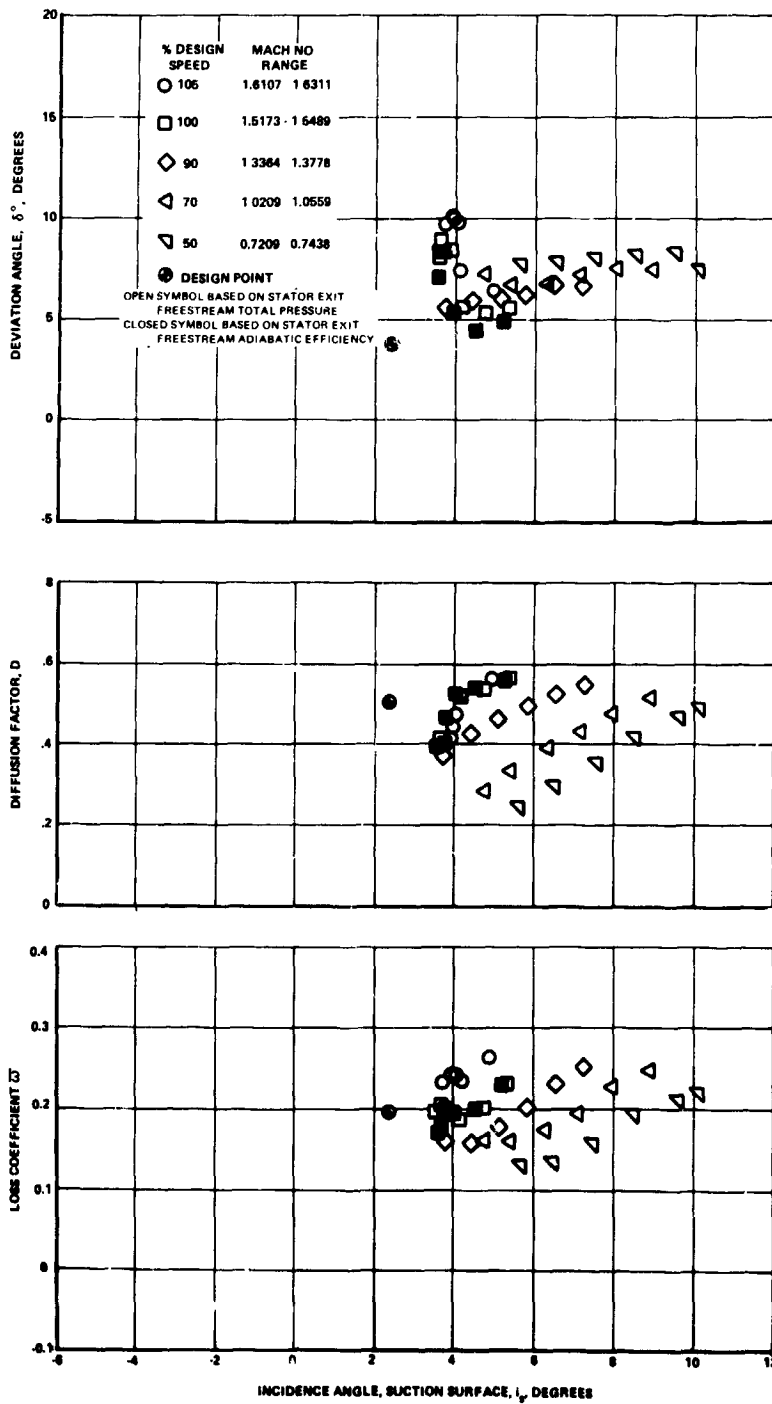


Figure 28 h Rotor Blade Element Performance with Uniform Inlet Flow, 90% Span

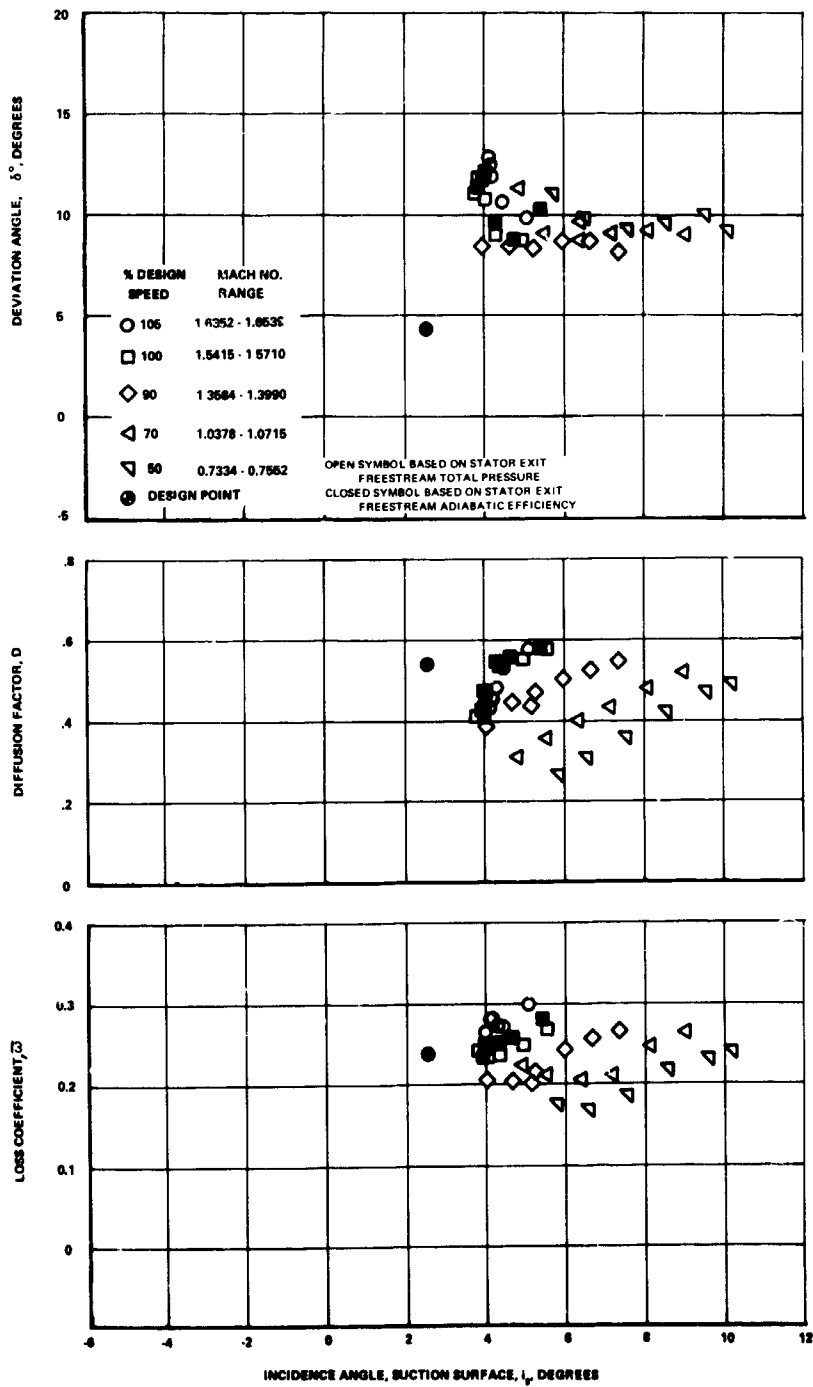


Figure 28 i Rotor Blade Element Performance with Uniform Inlet Flow, 95% Span

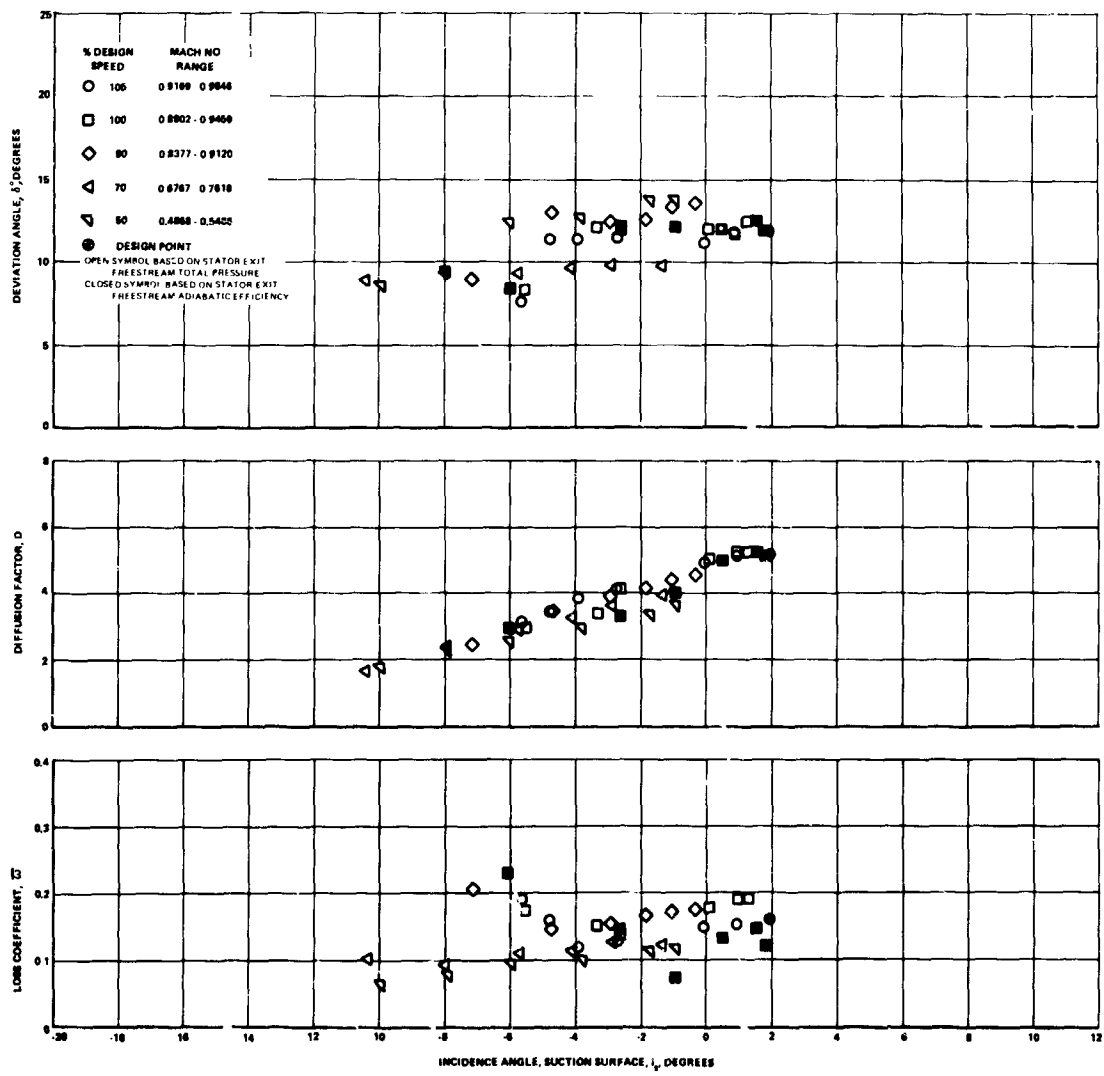


Figure 29 a Stator Blade Element Performance with Uniform Inlet Flow, 5% Span

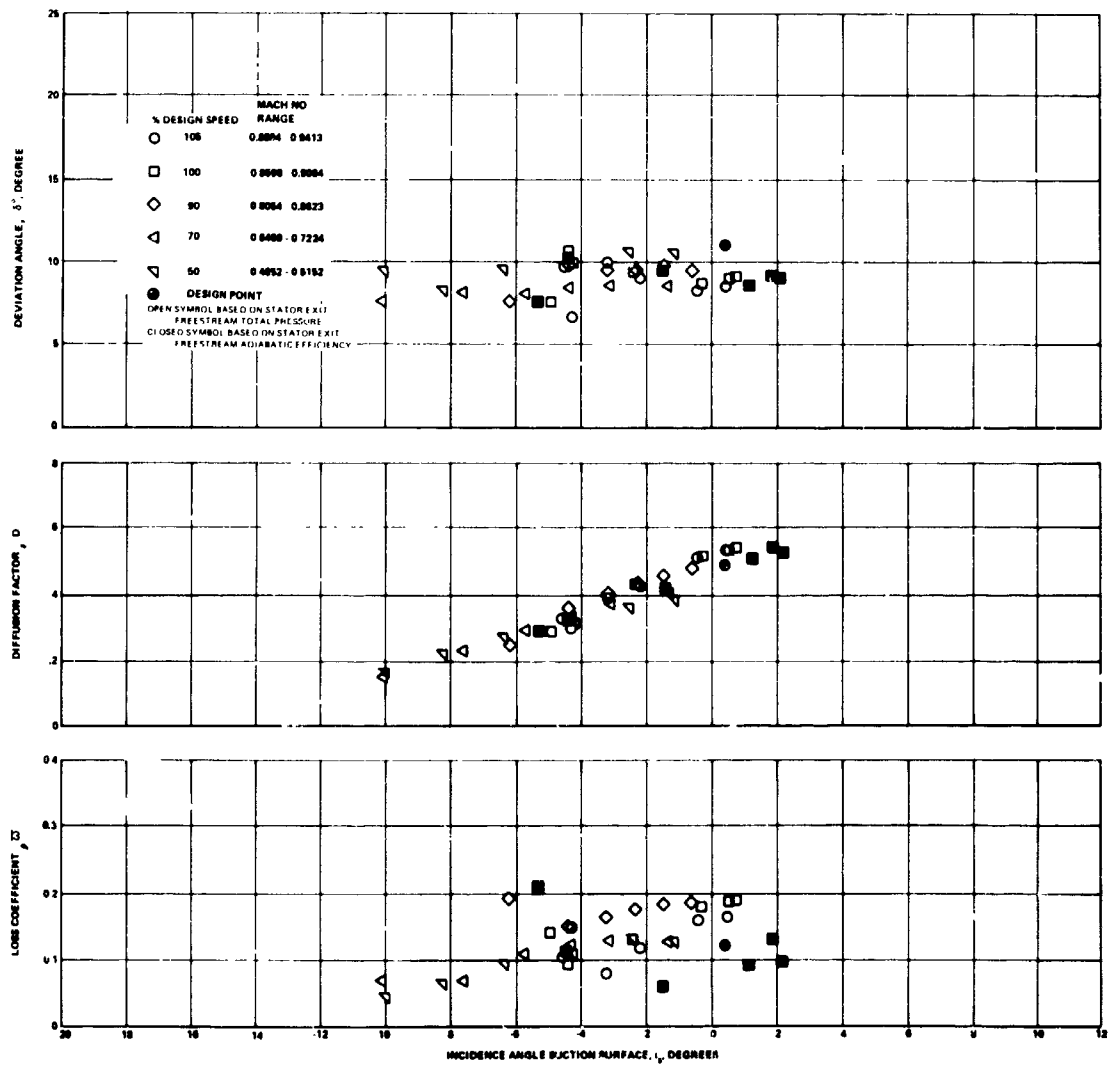


Figure 29b Stator Blade Element Performance with Uniform Inlet Flow, 10% Span

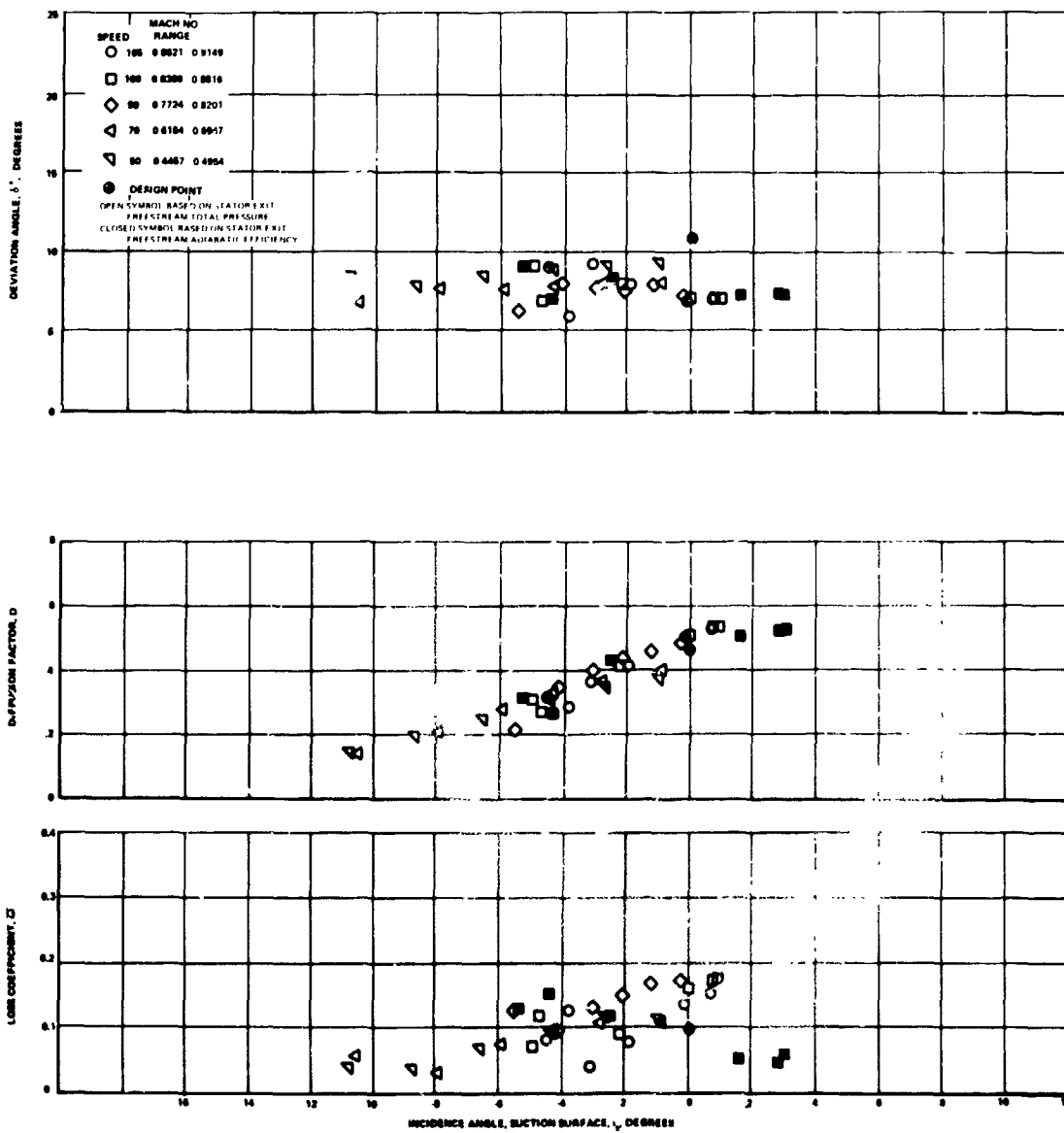


Figure 29c Stator Blade Element Performance with Uniform Inlet Flow, 15% Span

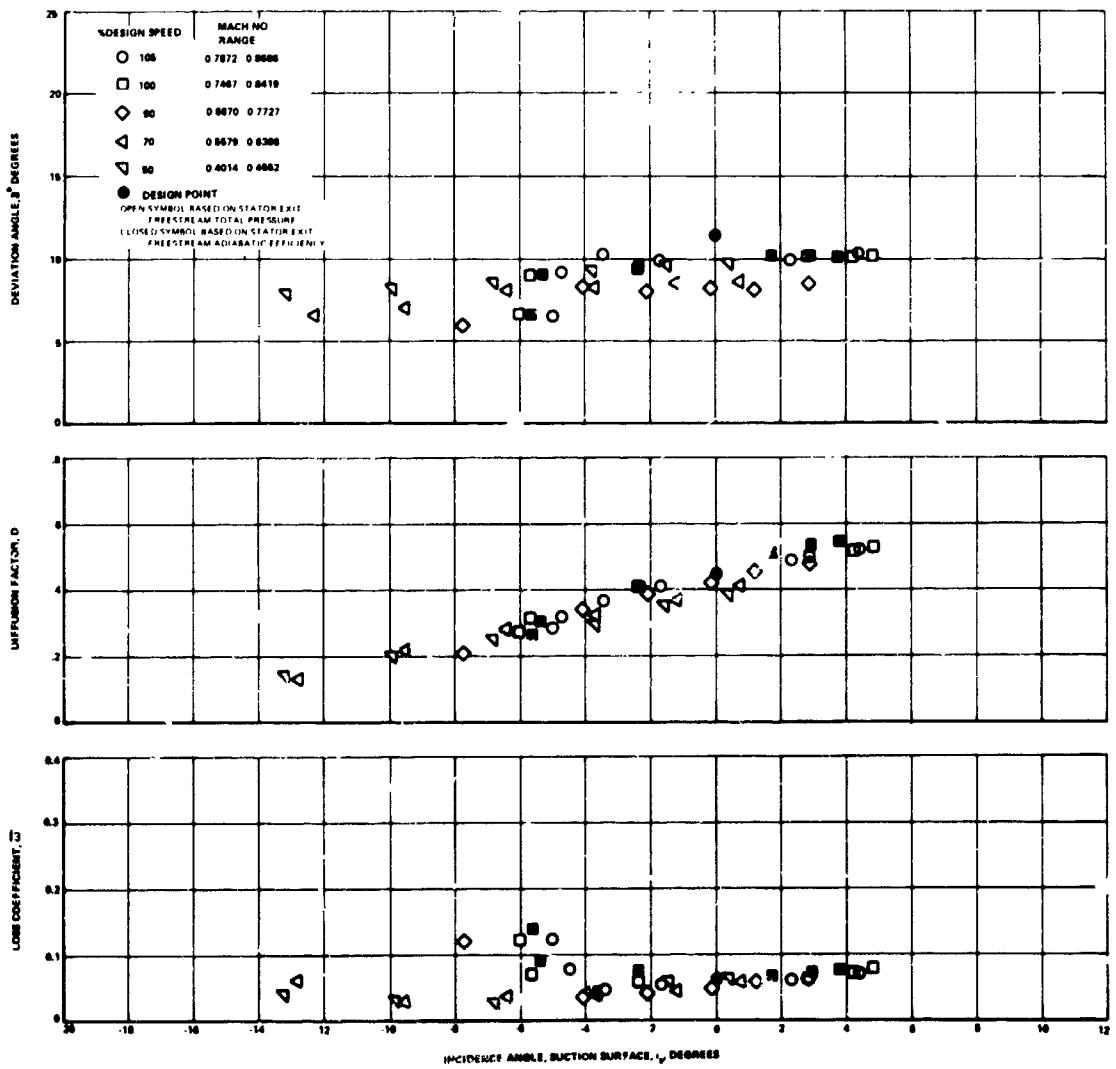


Figure 29 d Stator Blade Element Performance with Uniform Inlet Flow, 30% Span

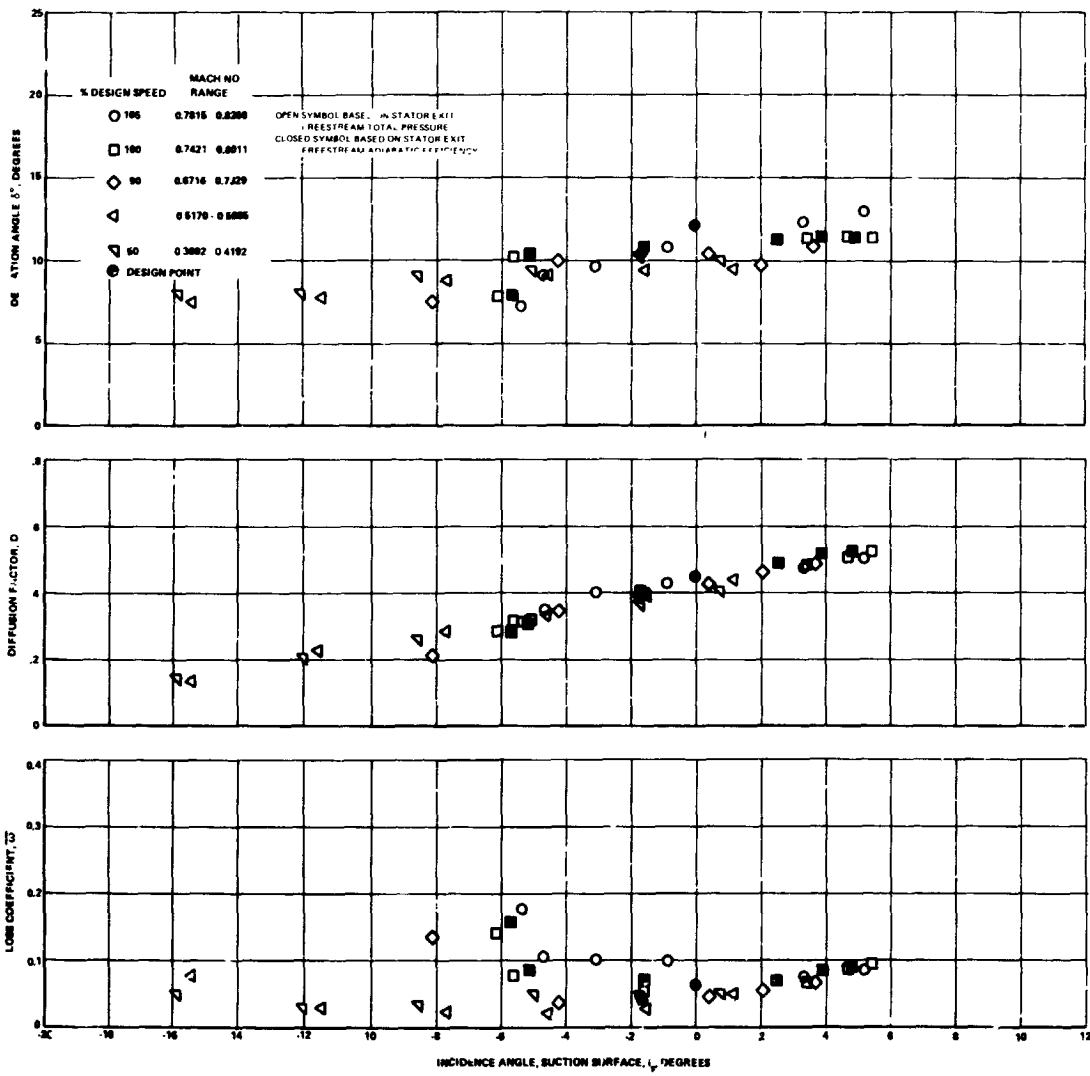


Figure 29 e Stator Blade Element Performance with Uniform Inlet Flow, 50% Span

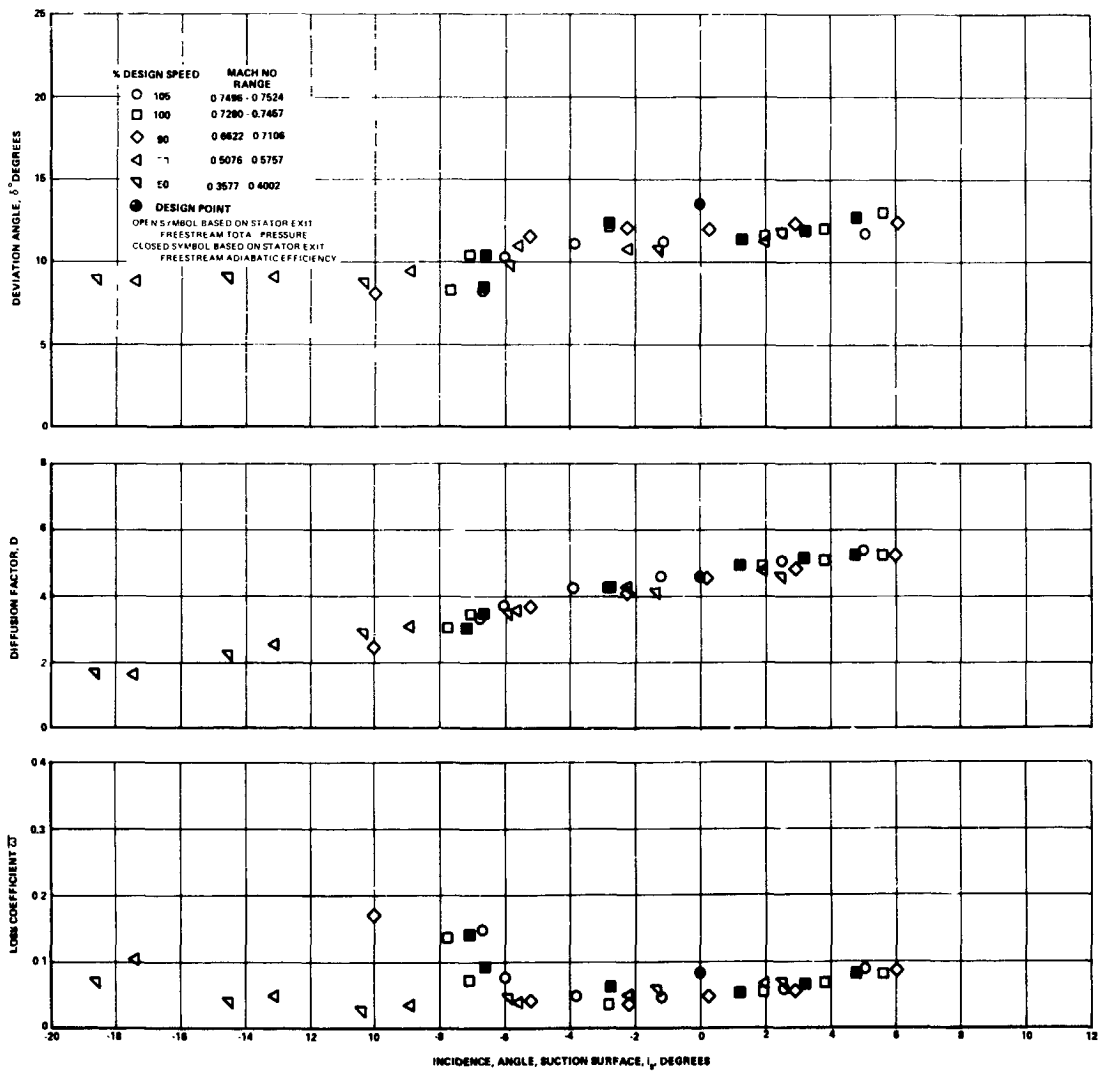


Figure 29 f Stator Blade Element Performance with Uniform Inlet Flow, 70% Span

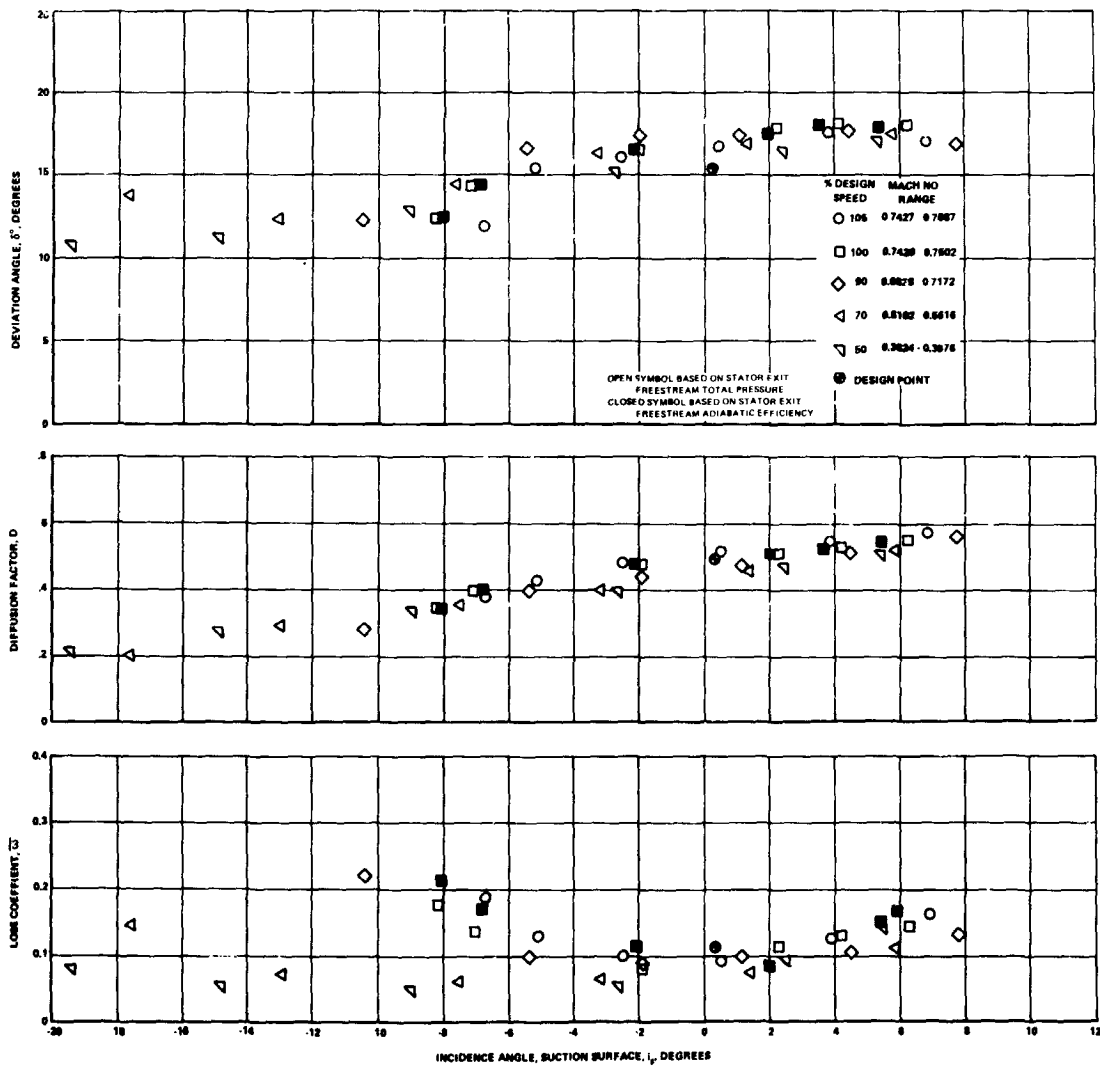


Figure 29 g Stator Blade Element Performance with Uniform Inlet Flow, 85% Span

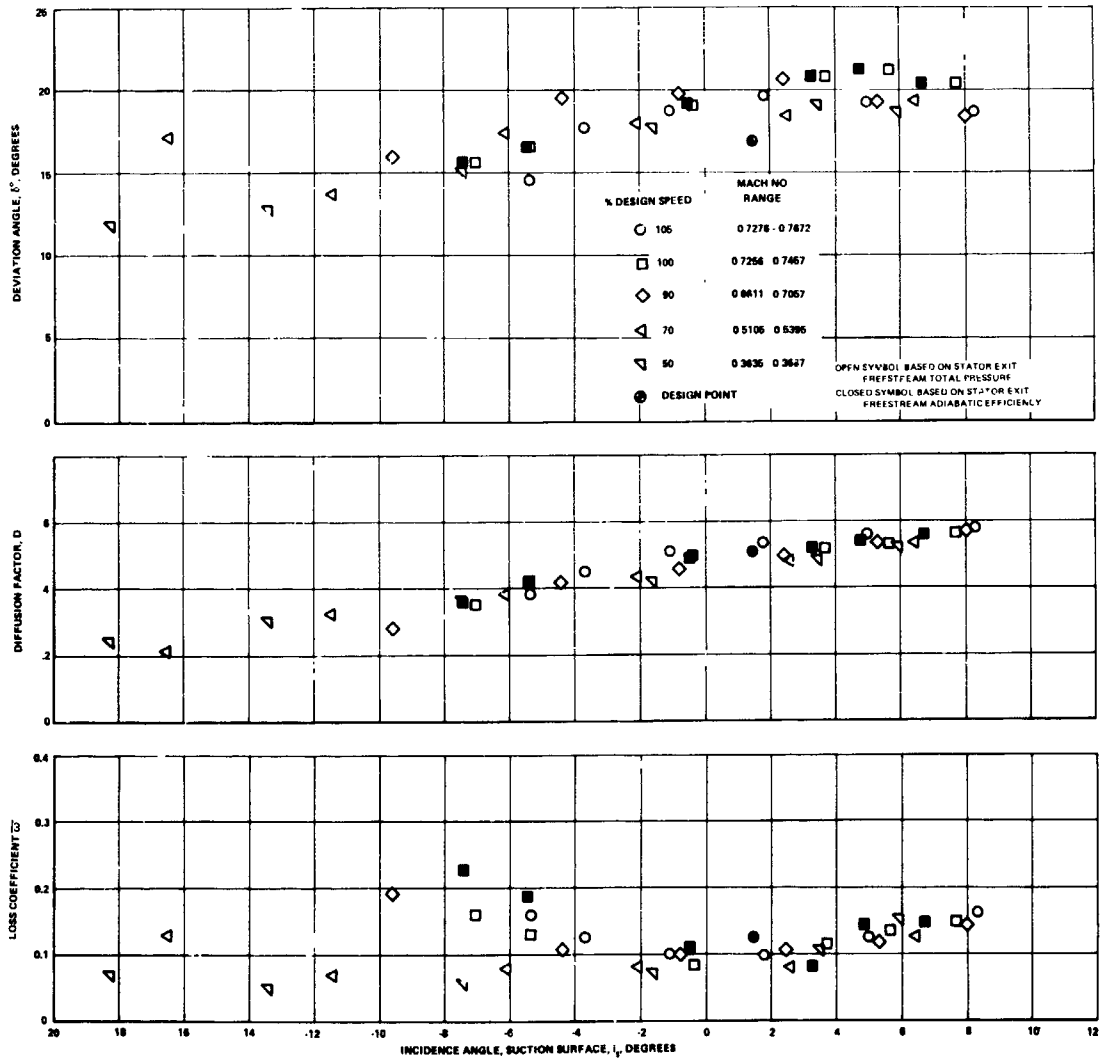


Figure 29 h Stator Blade Element Performance with Uniform Inlet Flow, 90% Span

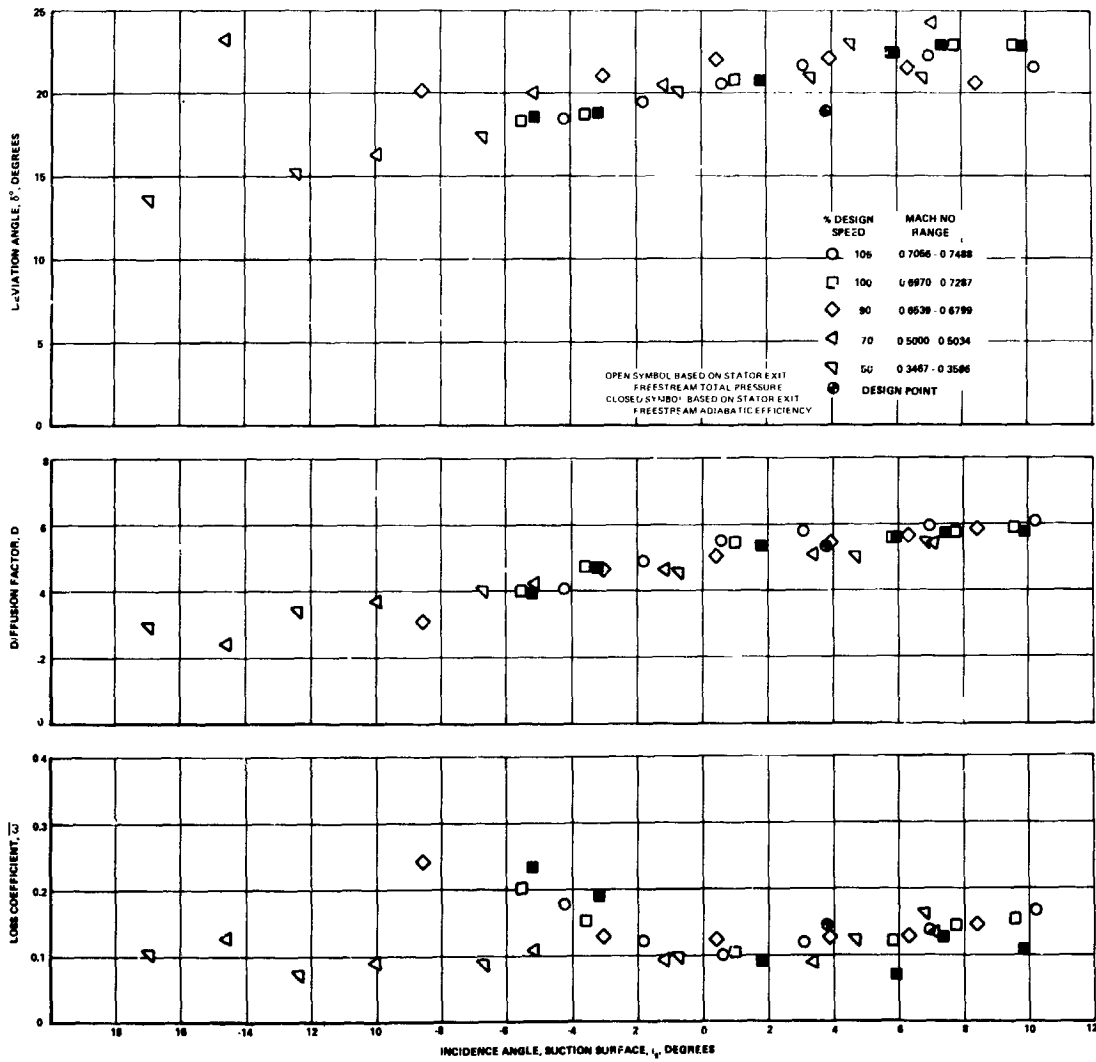


Figure 29 i Stator Blade Element Performance with Uniform Inlet Flow, 95% Span

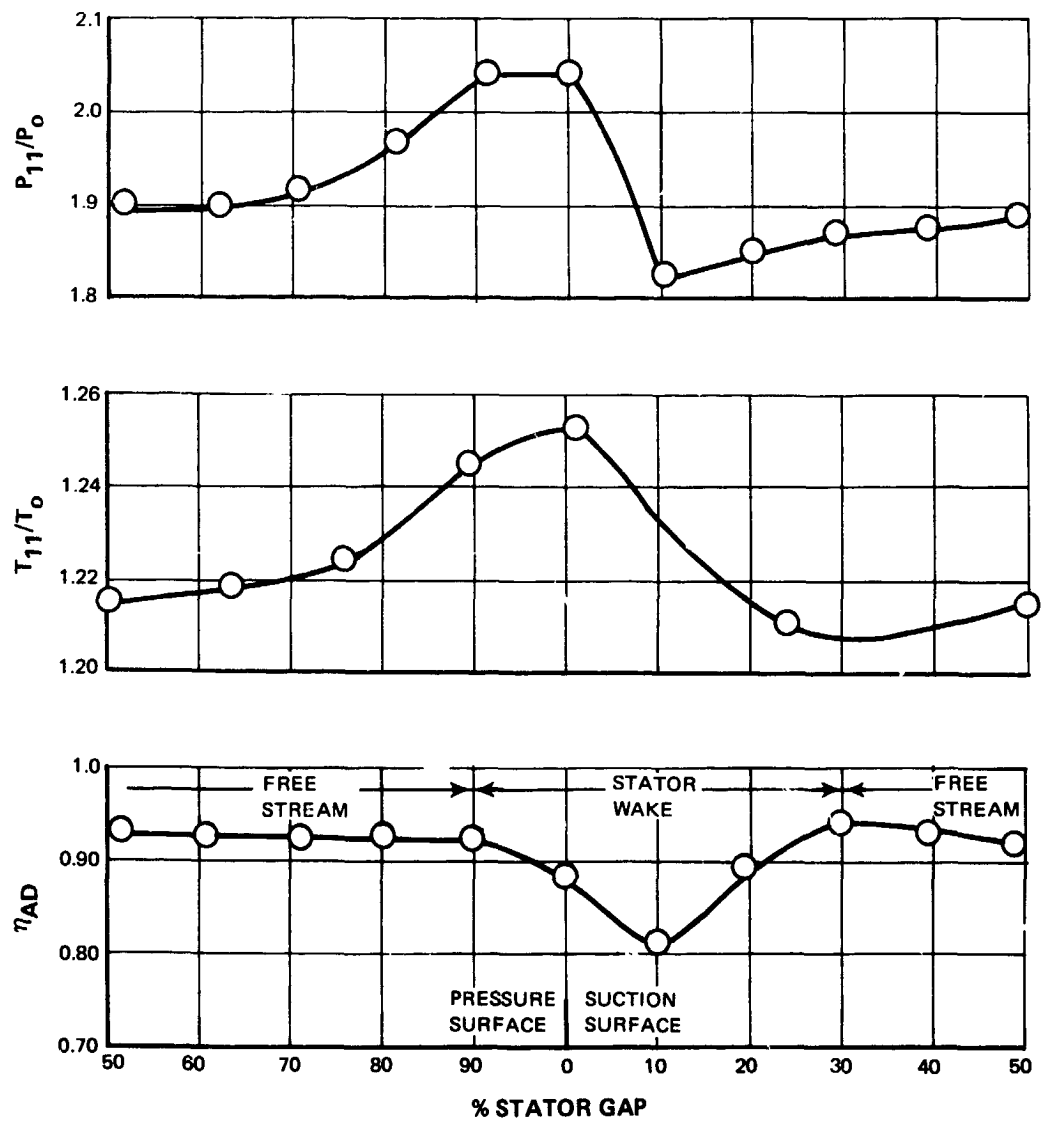


Figure 30 Pressure Ratio, Temperature Ratio, and Adiabatic Efficiency vs. Stator Exit Gapwise Location at 15% Span, Near Design Data Point

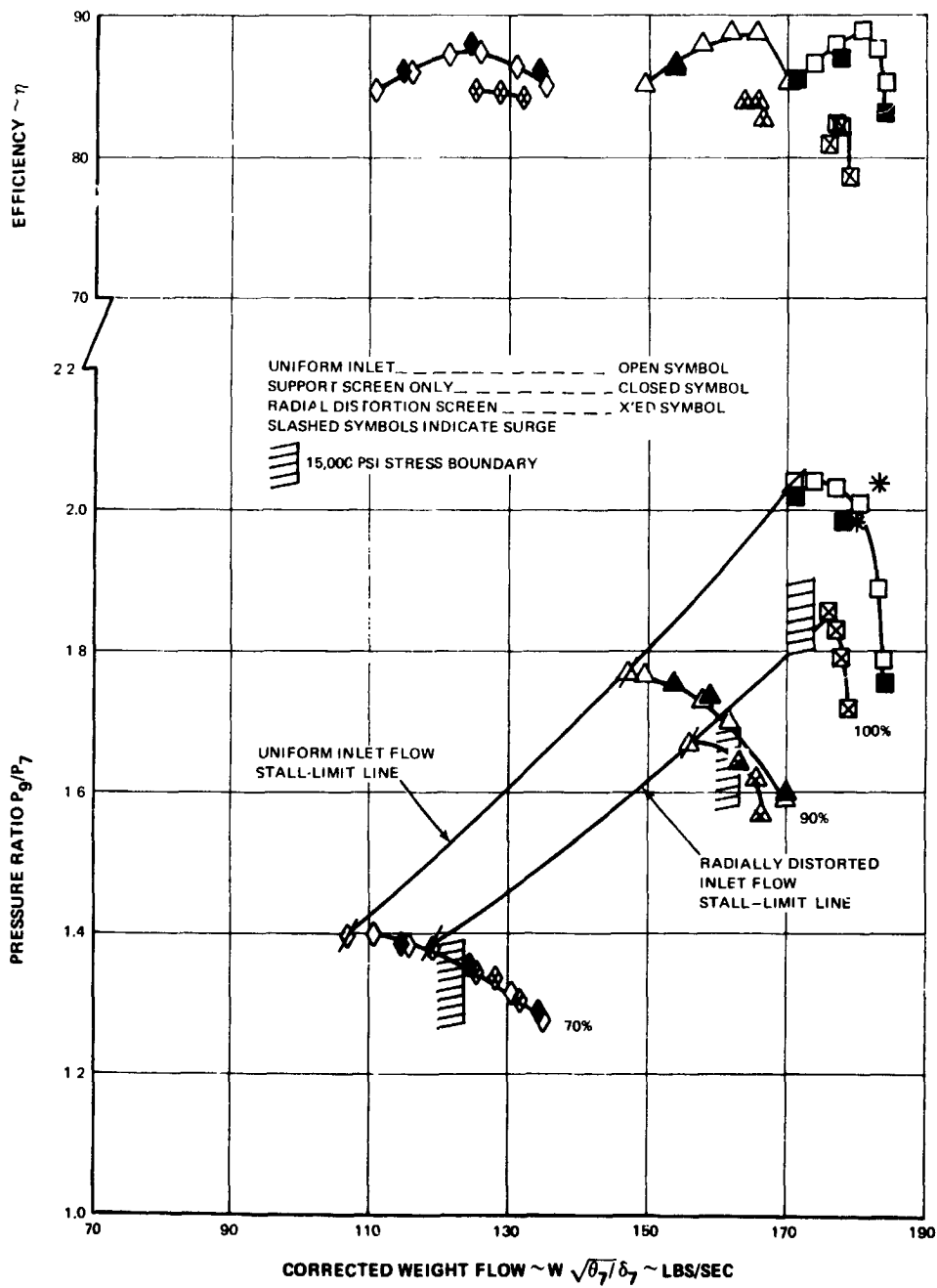


Figure 31 Comparison of Rotor Over-all Performance with the Distortion Screen Support, Radially Distorted Inlet Flow and Uniform Inlet Flow

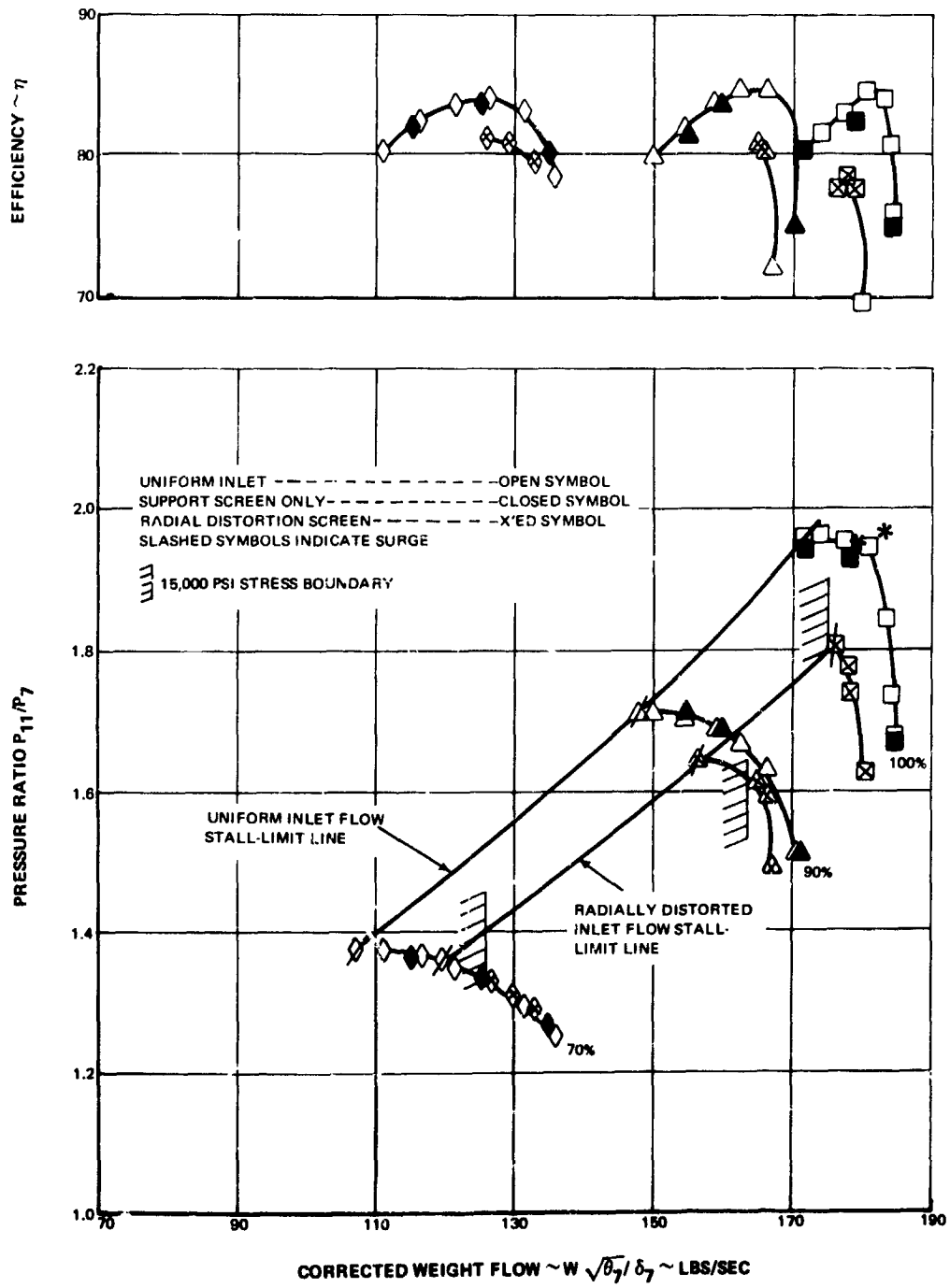


Figure 32 Comparison of Stage Over-all Performance with the Distortion Screen Support, Radially Distorted Inlet Flow and Uniform Inlet Flow

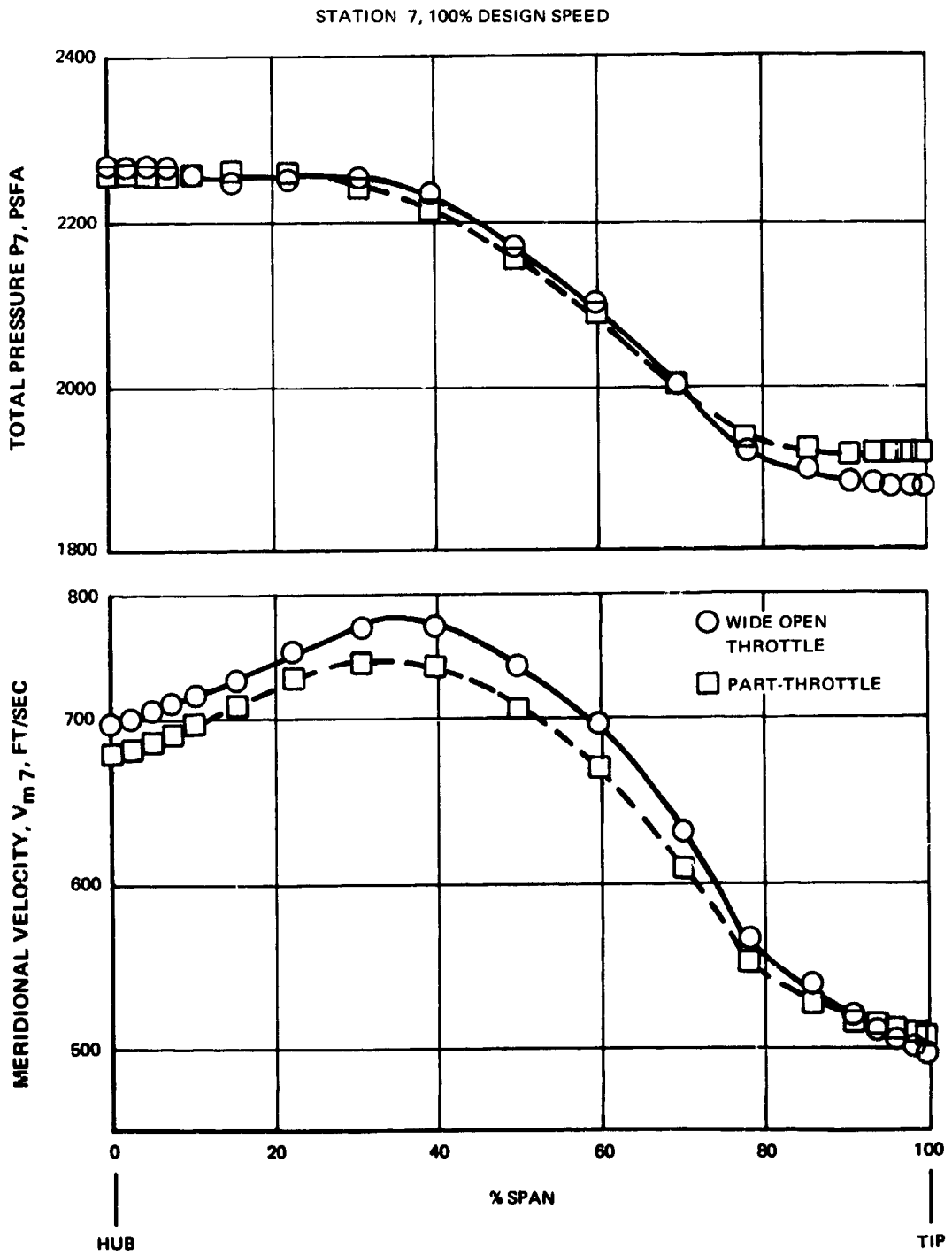


Figure 33 Spanwise Variation in Rotor Inlet Total Pressure and Meridional Velocity with Radially Distorted Inlet Flow

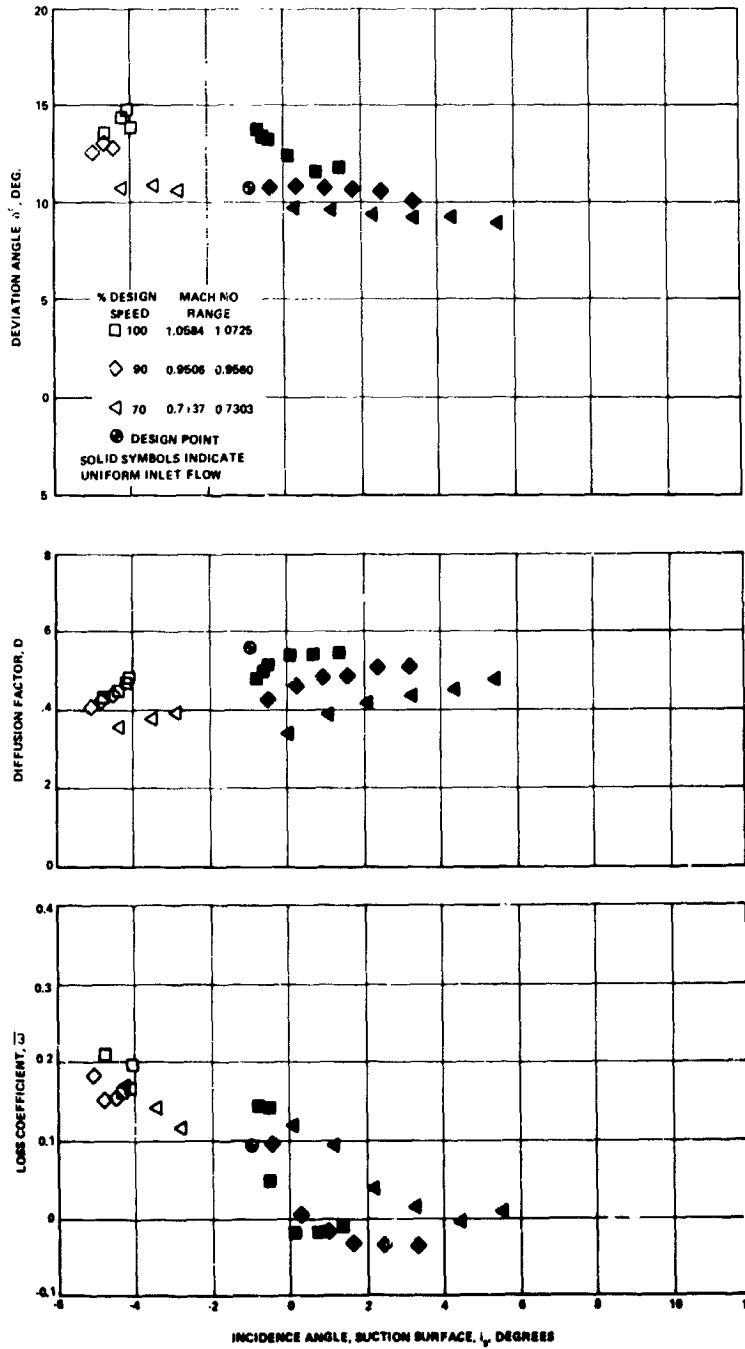


Figure 34 a Rotor Blade Element Performance with Radially Distorted Inlet Flow, 10% Span

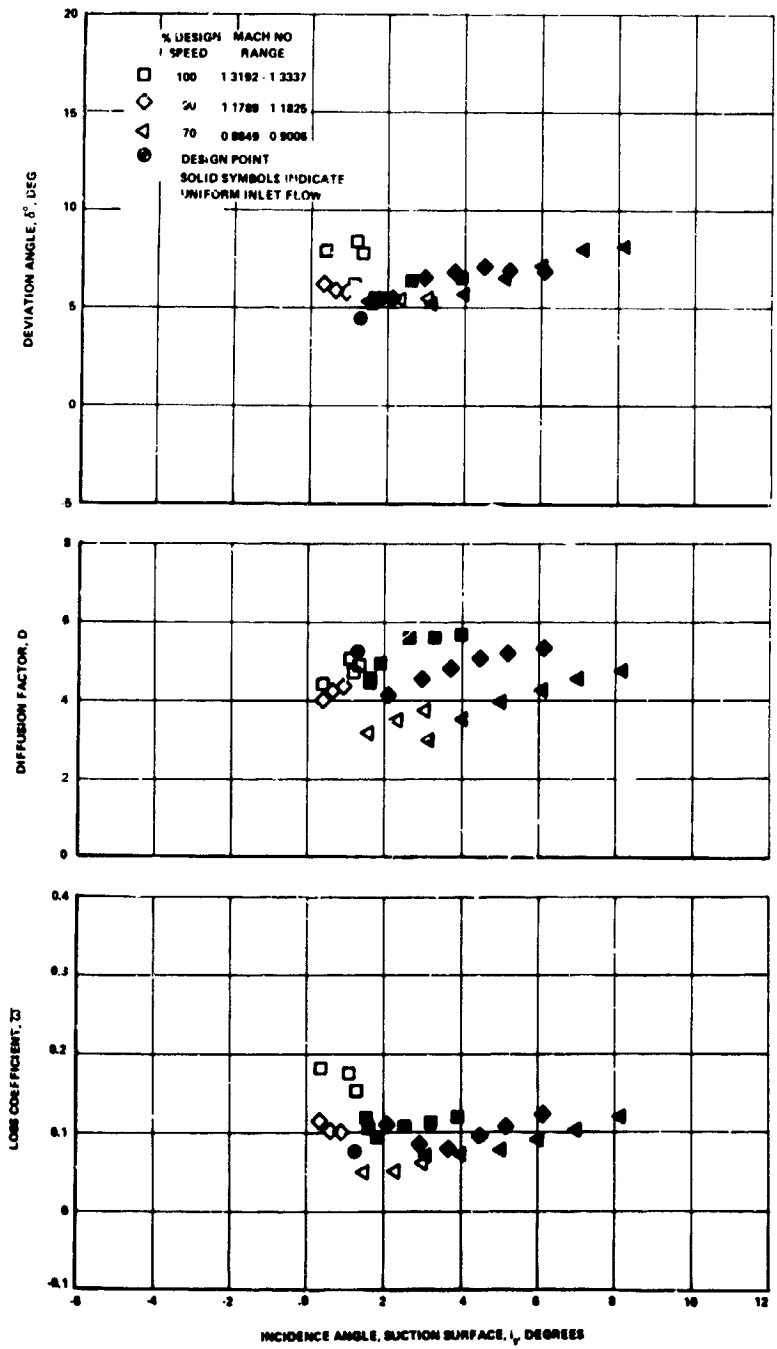


Figure 34 b Rotor Blade Element Performance with Radially Distorted Inlet Flow, 50% Span

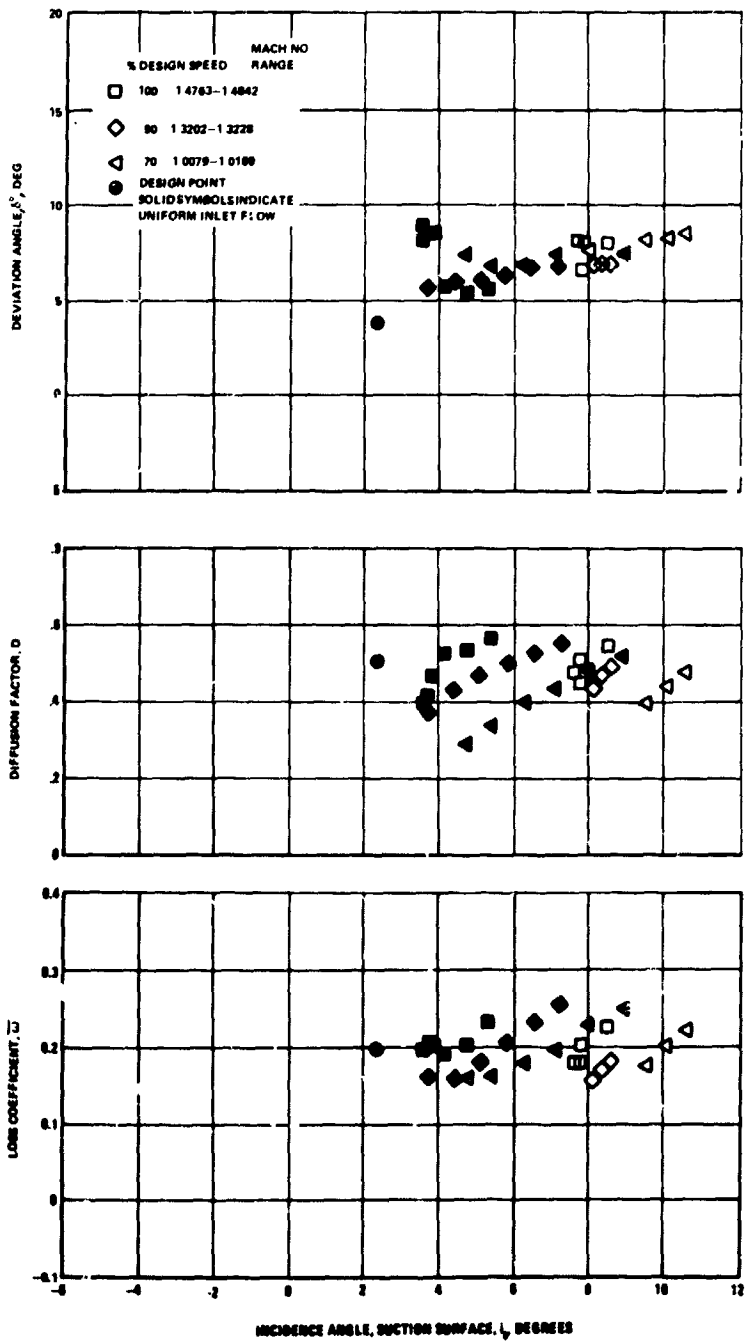


Figure 34 c Rotor Blade Element Performance with Radially Distorted Inlet Flow, 90% Span

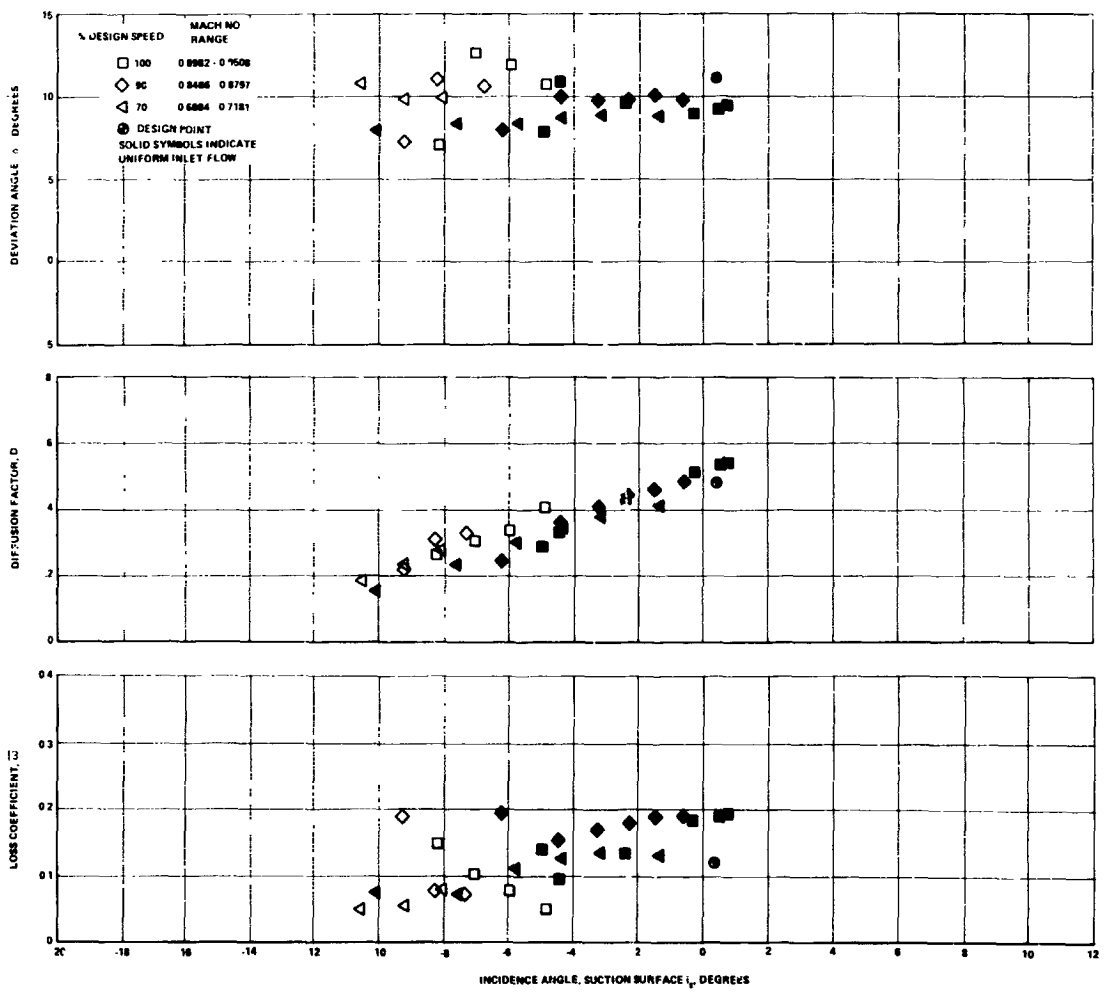


Figure 35 a Stator Blade Element Performance with Radially Distorted Inlet Flow, 10% Span

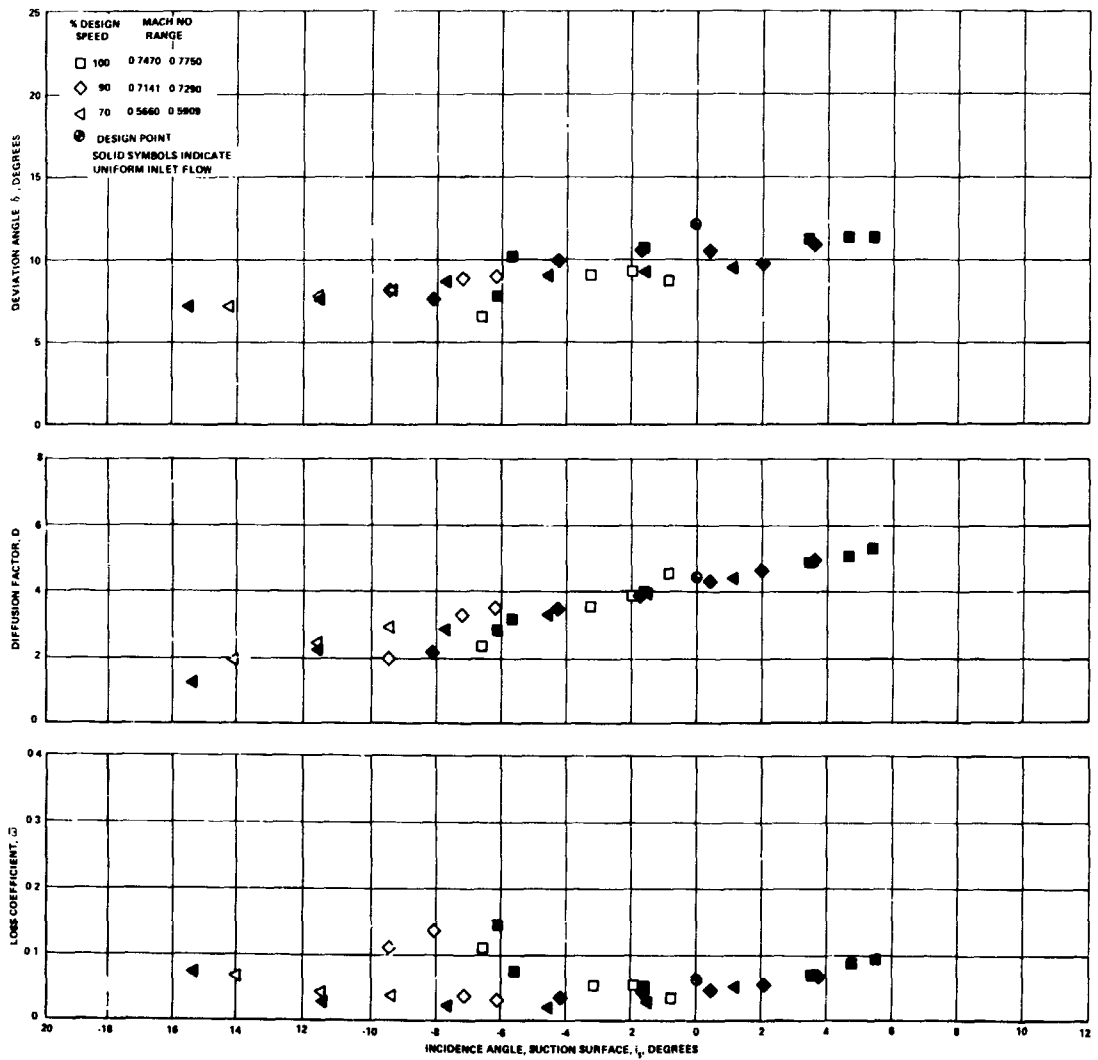


Figure 35 b Stator Blade Element Performance with Radially Distorted Inlet Flow, 50% Span

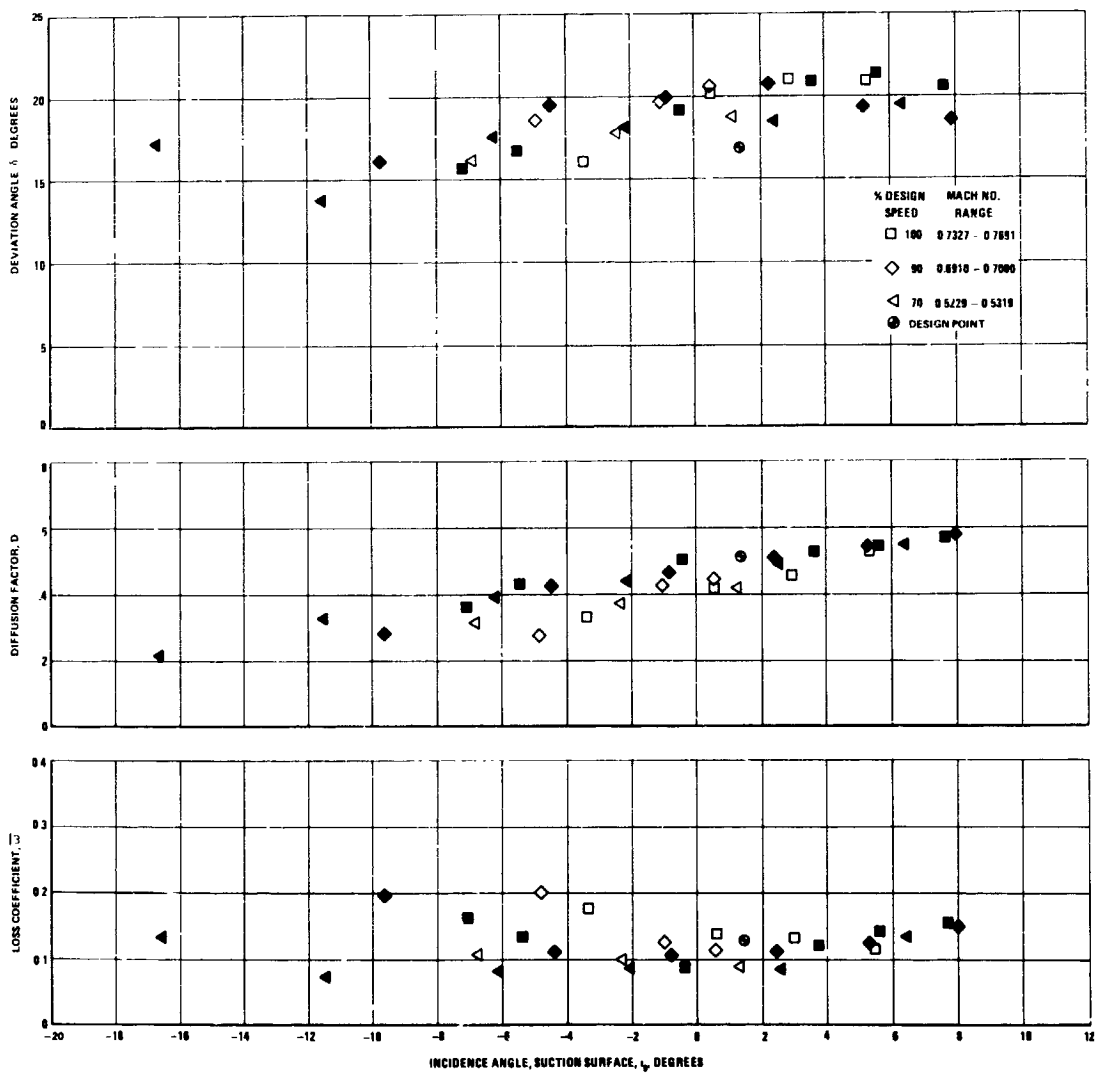


Figure 35c Stator Blade Element Performance with Radially Distorted Inlet Flow, 90% Span

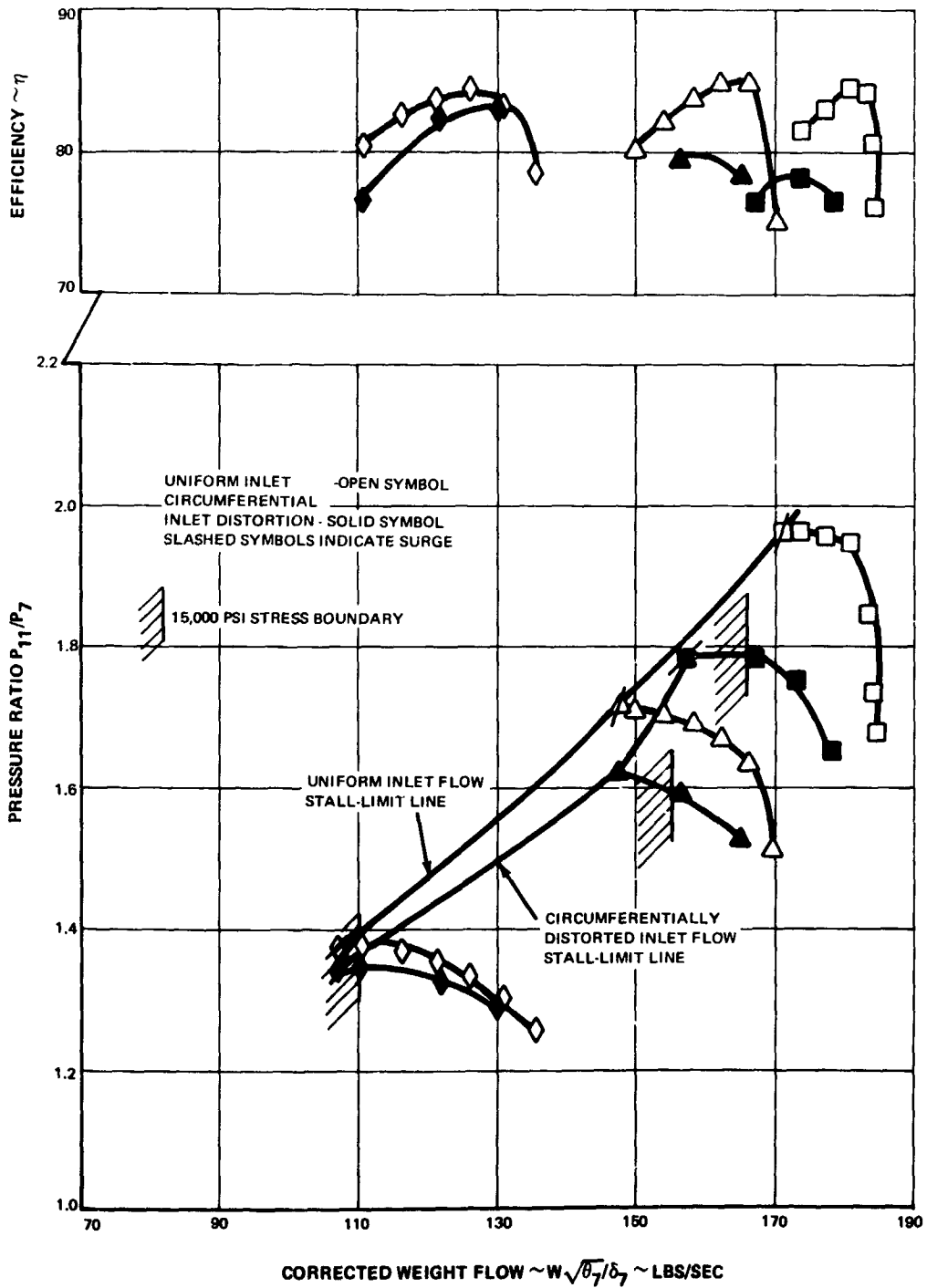


Figure 36 Comparison of Stage Over-all Performance With Circumferentially Distorted Inlet Flow and Uniform Inlet Flow

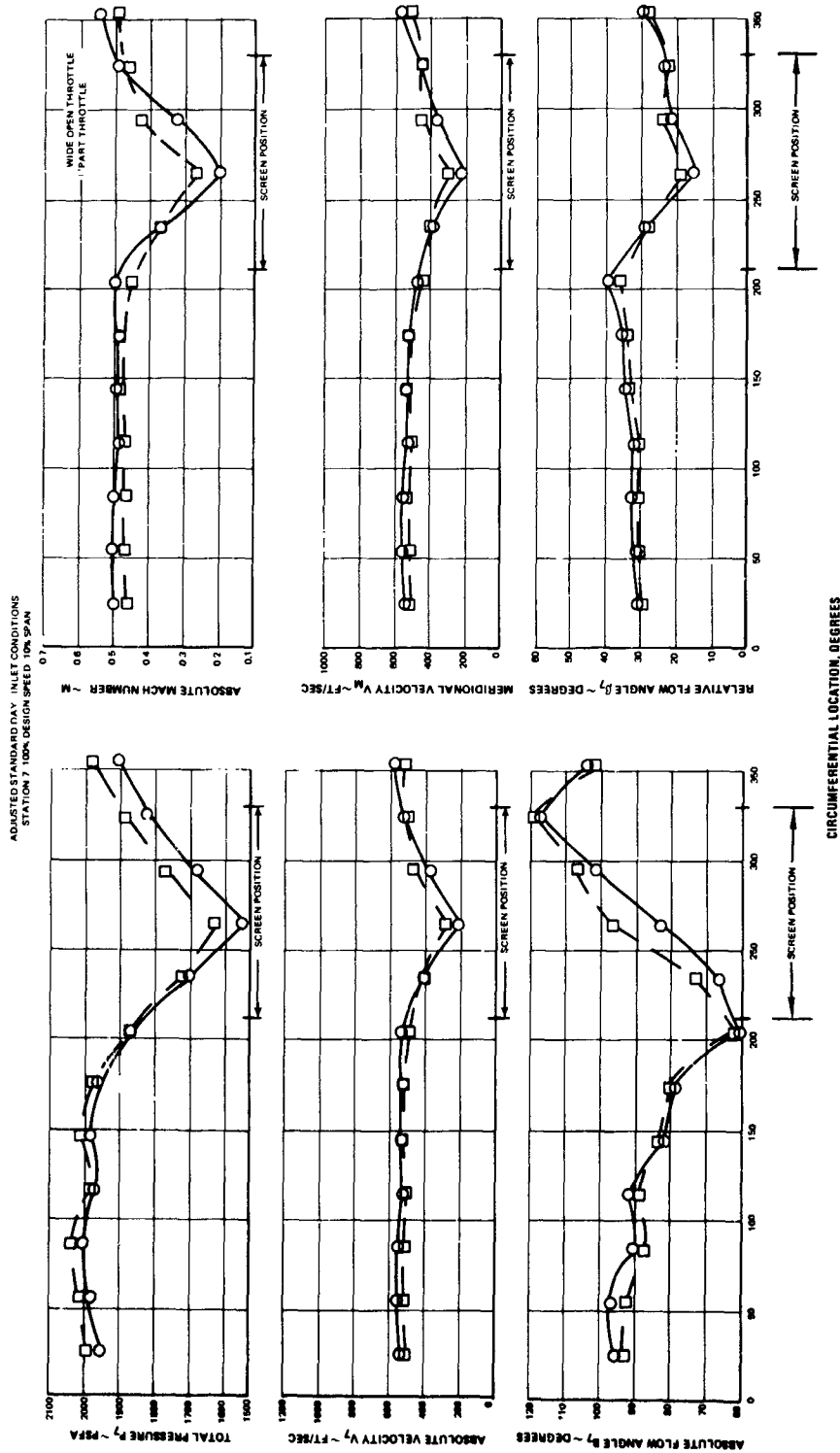


Figure 37 Circumferential Distributions of Rotor Inlet Total Pressure, Absolute Velocity, Meridional Velocity, Absolute Mach Number, and Absolute and Relative Flow Angle, 10% Span

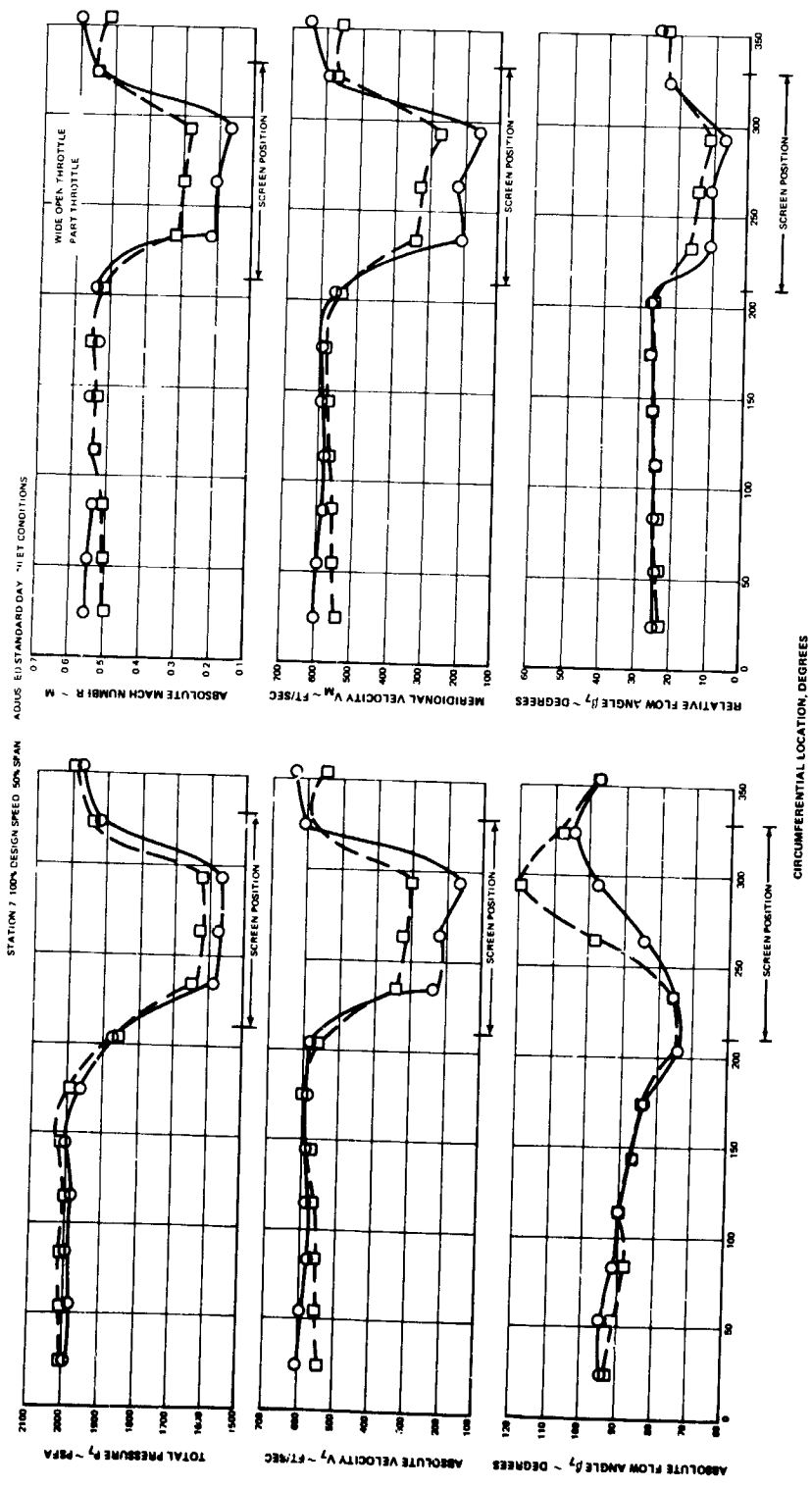


Figure 38 Circumferential Distributions of Rotor Inlet Total Pressure, Absolute Velocity, Meridional Velocity, Absolute Mach Number, and Absolute and Relative Flow Angle, 50% Span

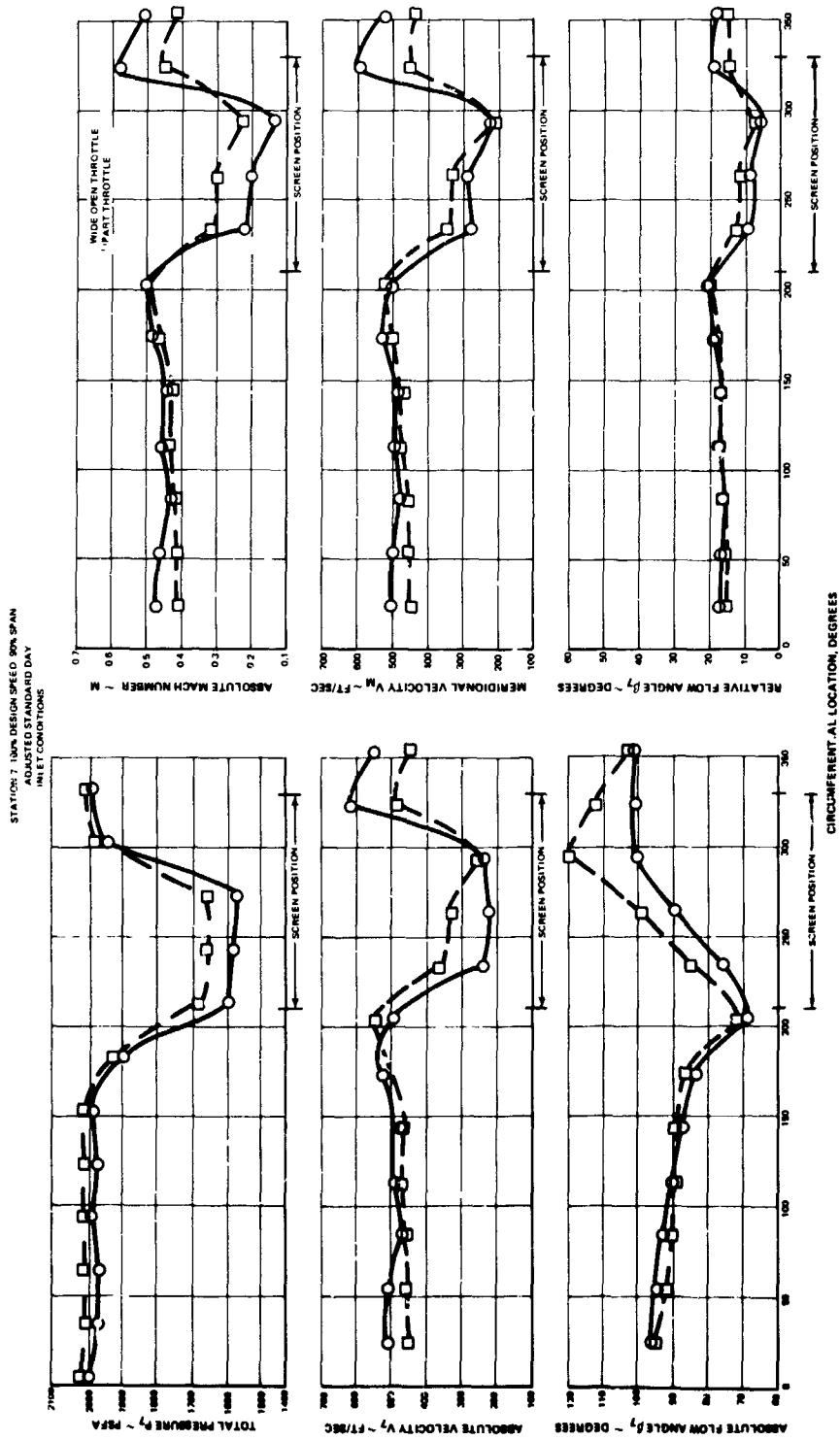


Figure 39 Circumferential Distributions of Rotor Inlet Total Pressure, Absolute Velocity, Meridional Velocity, Absolute Mach Number, and Absolute and Relative Flow Angle, 90% Span

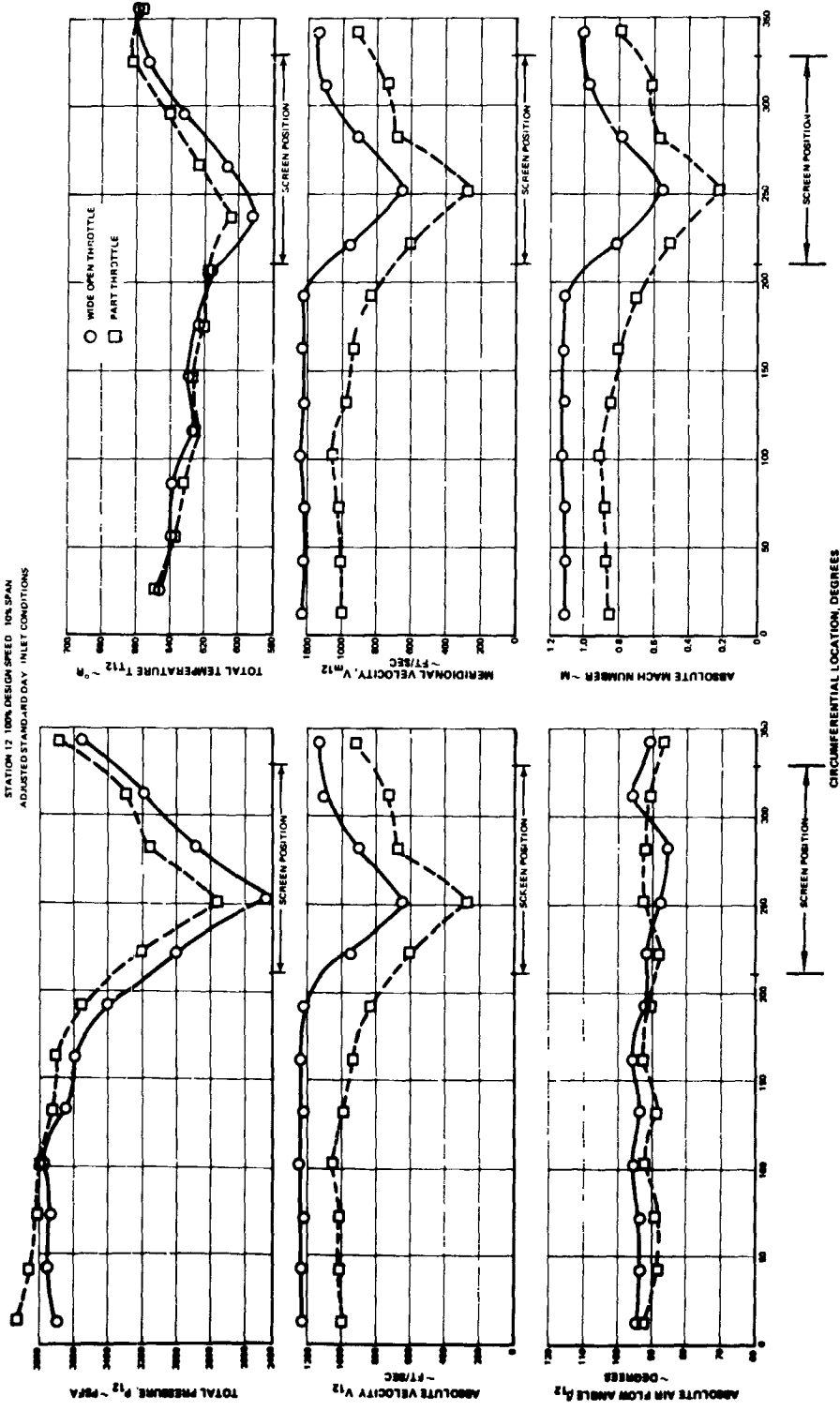


Figure 40 Circumferential Distribution of Stator Discharge Total Pressure, Total Temperature, Absolute Velocity, Meridional Velocity, Absolute Mach Number, and Absolute Air Flow Angle, 10% Span

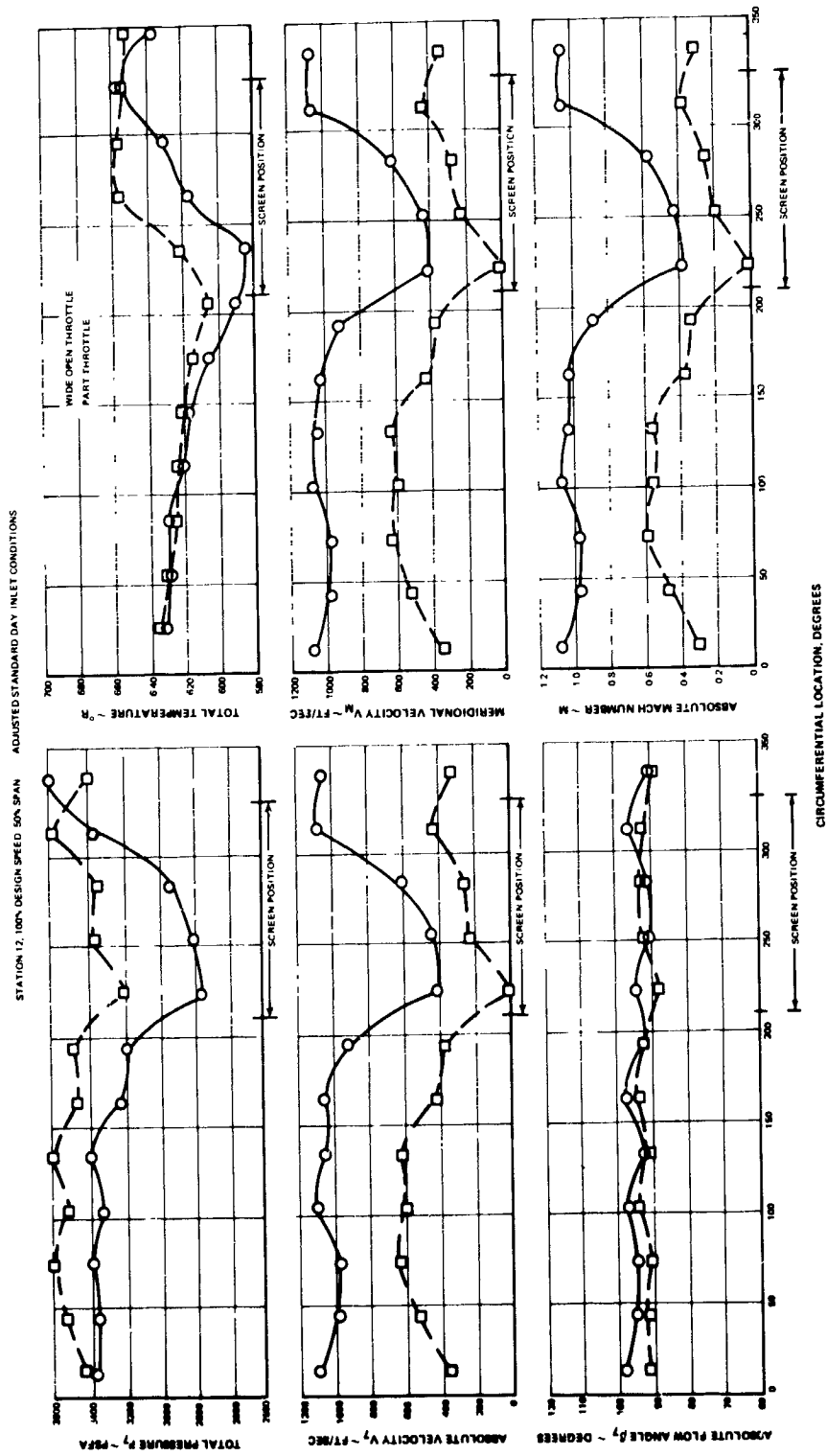


Figure 41 Circumferential Distribution of Stator Discharge Total Pressure, Total Temperature, Absolute Velocity, Meridional Velocity, Absolute Mach Number and Absolute Air Flow Angle, 50% Span

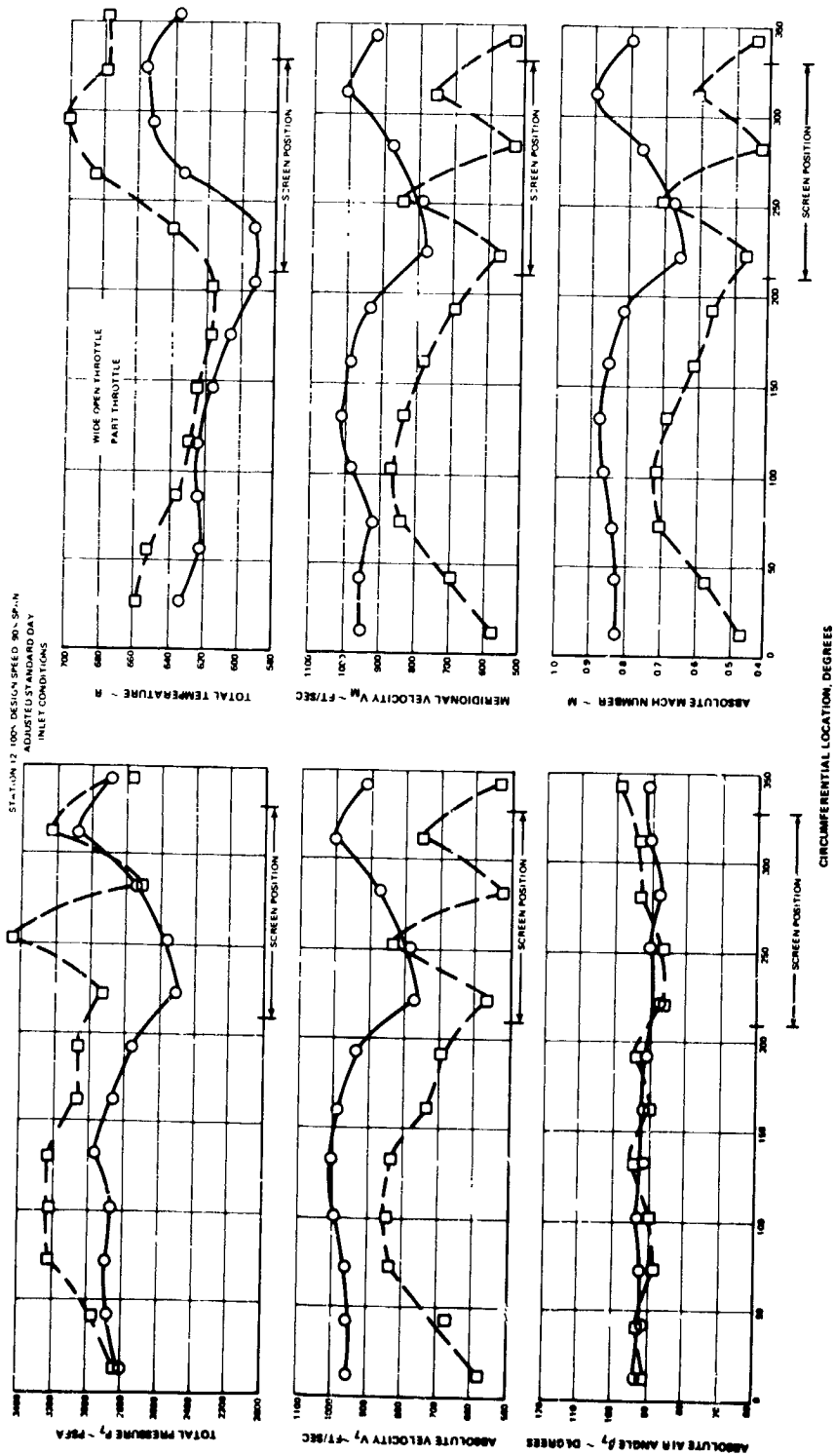


Figure 42 Circumferential Distribution of Stator Discharge Total Pressure, Total Temperature, Absolute Velocity, Meridional Velocity, Absolute Mach Number, and Absolute Air Flow Angle, 90% Span

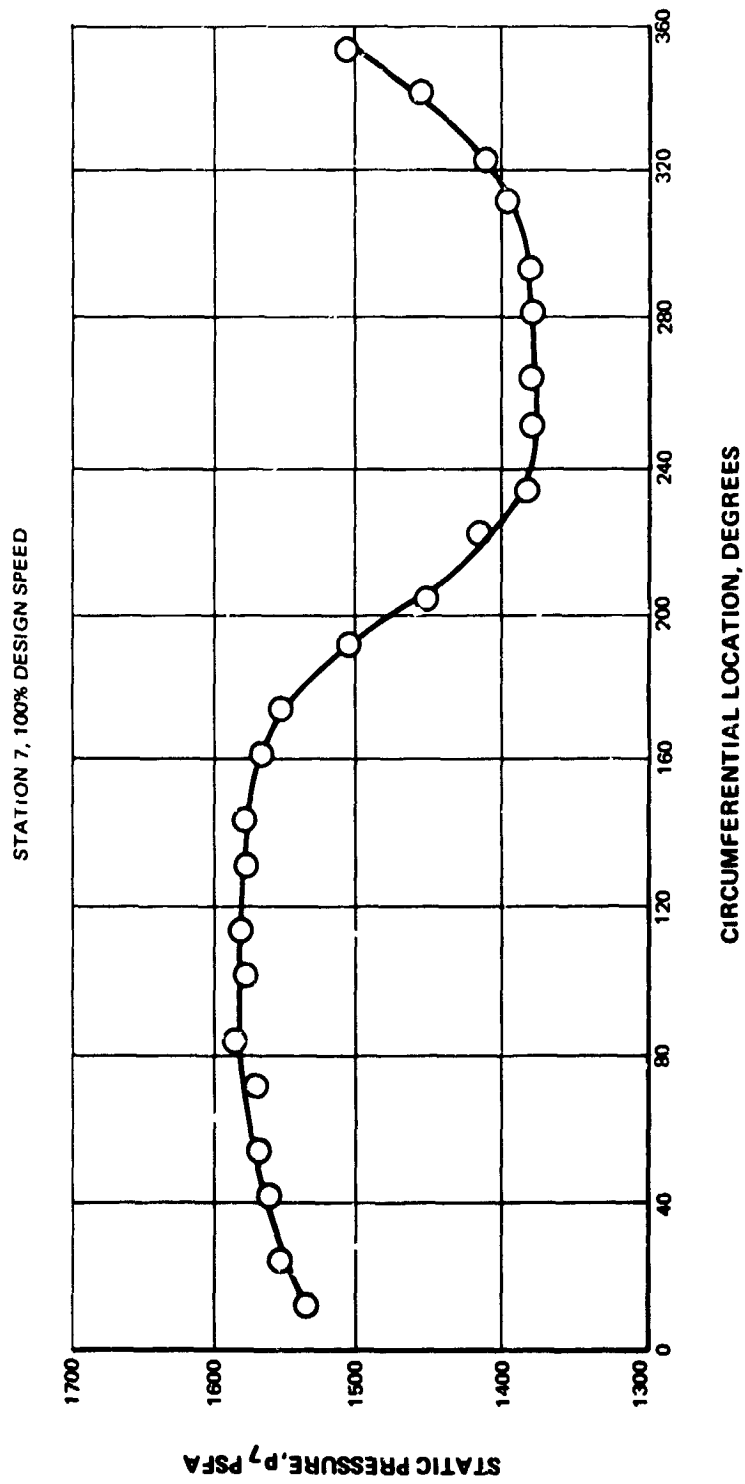


Figure 43 Circumferential Distribution of Rotor Inlet Hub Static Pressure

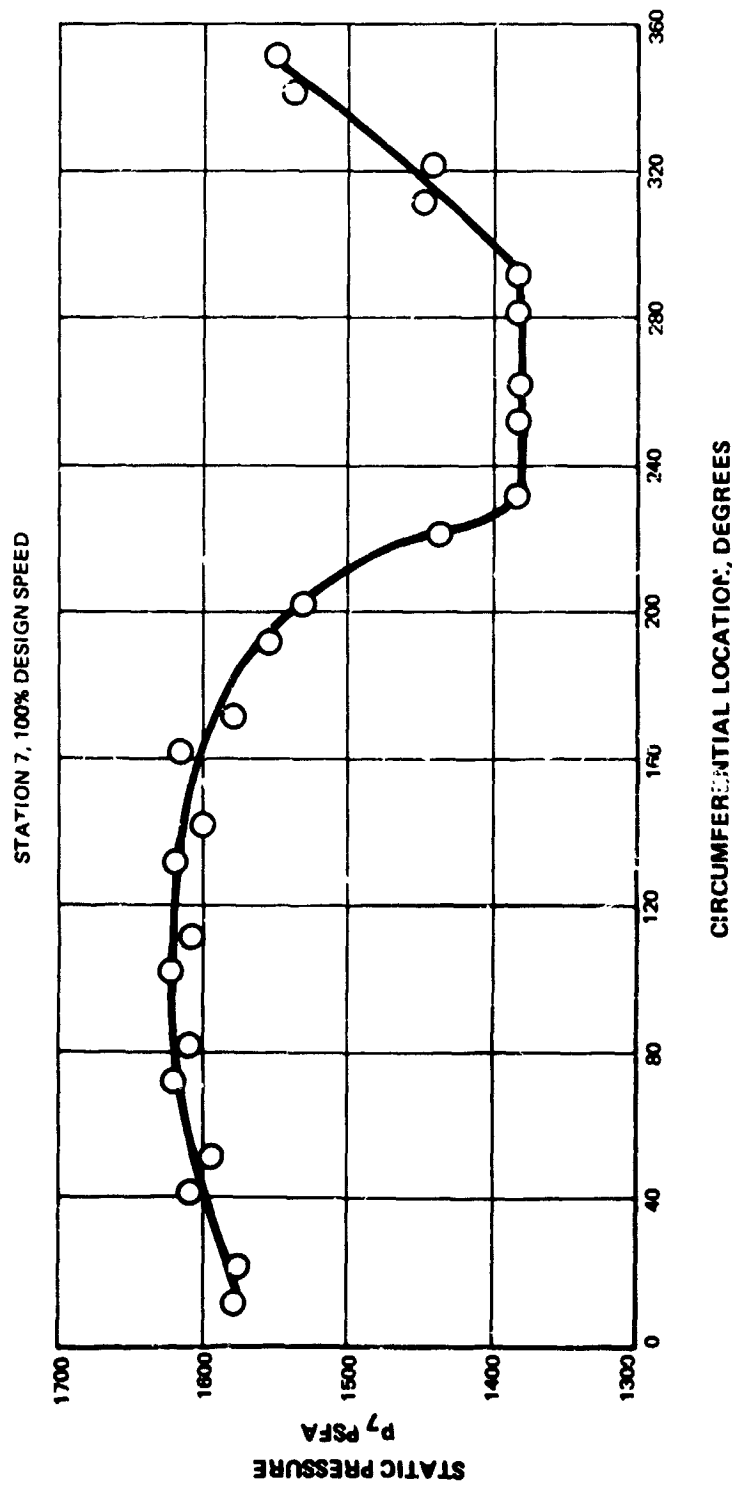


Figure 44 Circumferential Distribution of Rotor inlet Tip Static Pressure

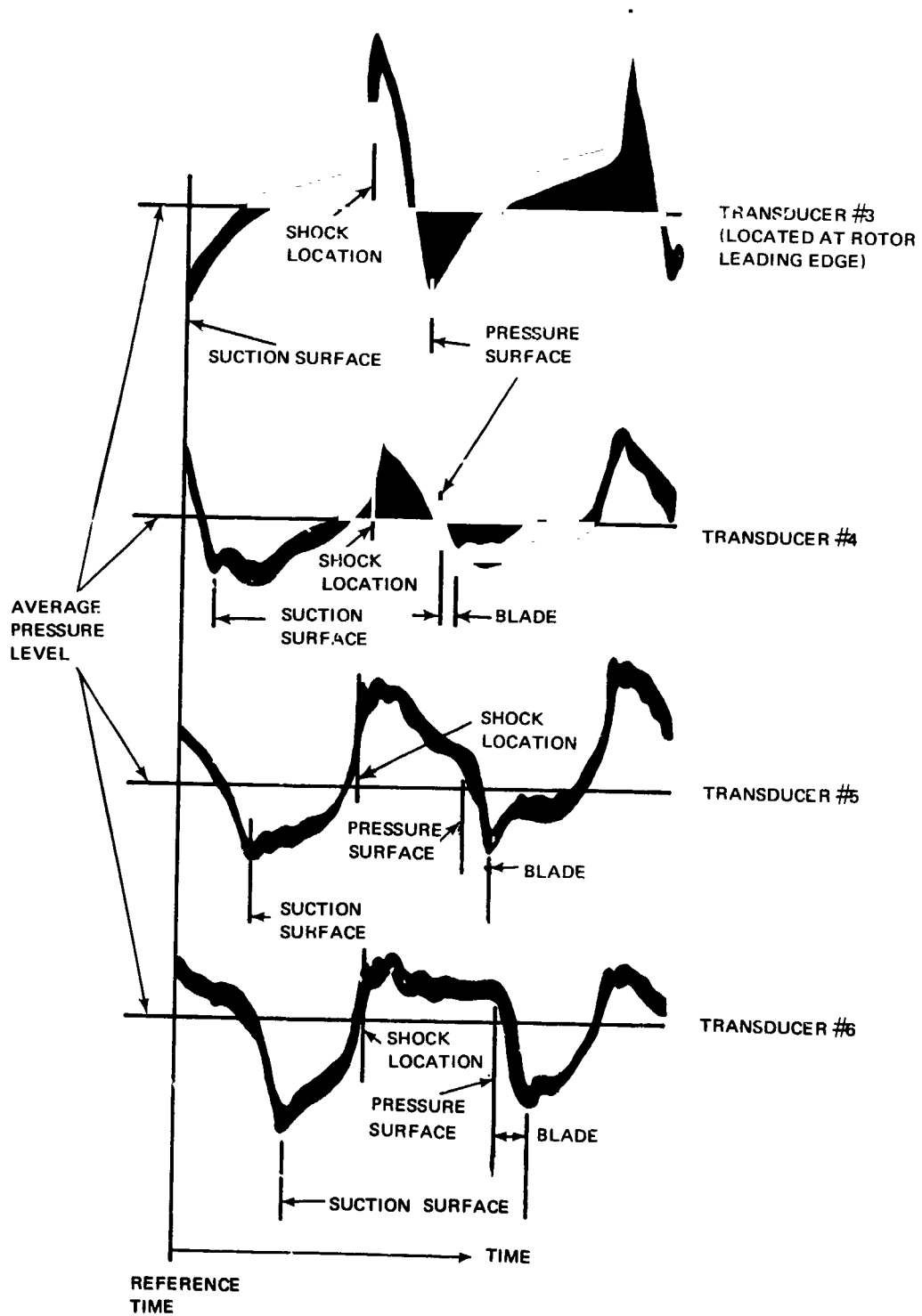
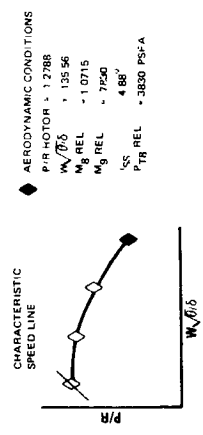
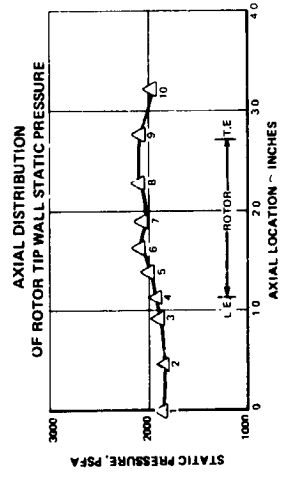
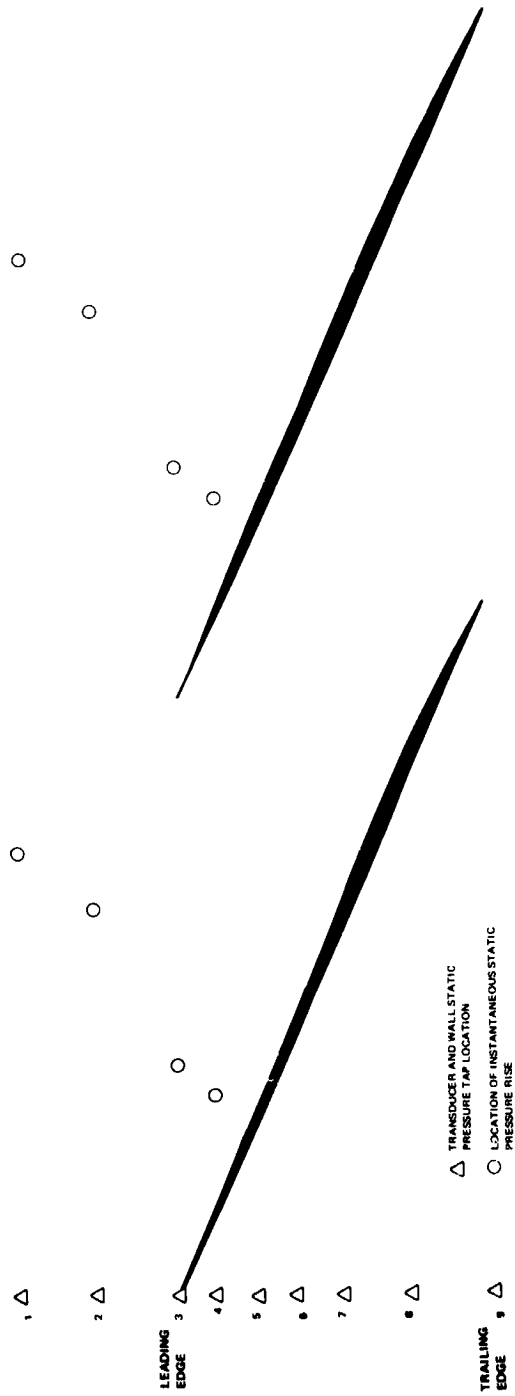


Figure 45 Typical Oscillograph Traces Showing Presence of Shock over Blade Tip

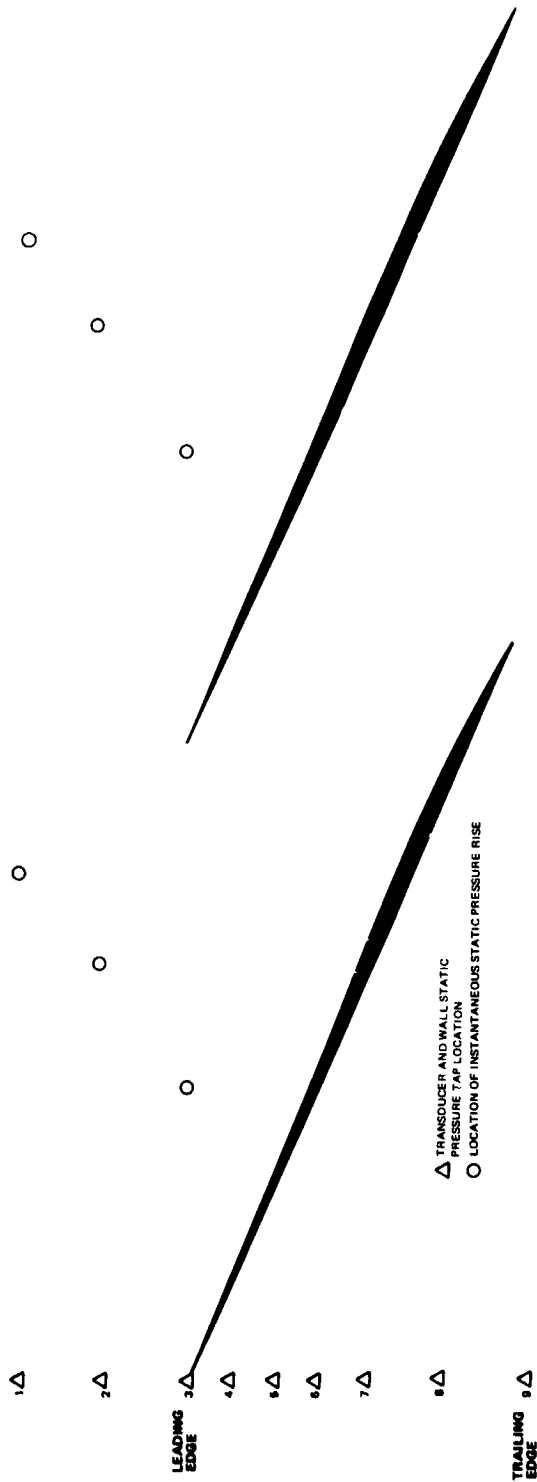
70% SPEED



AERODYNAMIC CONDITIONS
 P/R MOTOR = 1.2788
 $W_{\infty}/\beta_0 = 135.56$
 $M_{\infty} REL = 1.0715$
 $M_{\infty} REL = 7250$
 $N_{\infty} = 4.88'$
 $P_{TR} REL = 3850 \text{ PSF-A}$

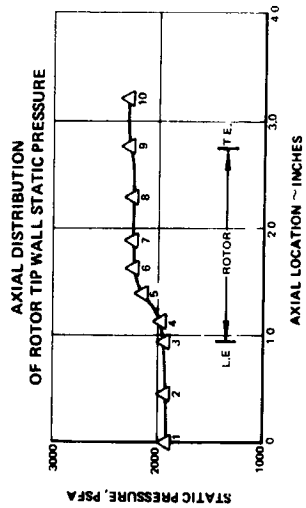
Figure 46 Rotor Blade Tip Shock Location, $\frac{W_{\infty}\theta}{\delta} = 135.56$

70% SPEED

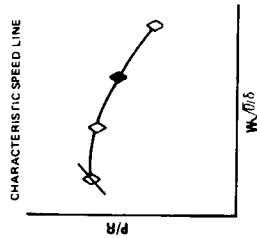


△ TRANSDUCER AND WALL STATIC PRESSURE TAP LOCATION
○ LOCATION OF INSTANTANEOUS STATIC PRESSURE RISE

10 △
TRAILING EDGE



AXIAL DISTRIBUTION OF ROTOR TIP WALL STATIC PRESSURE



◆ AERODYNAMIC CONDITIONS
P/B ROTOR = 1.445
W_r/δ = 126.24
M₈ REL = 1.0569
M₉ REL = 0.7071
ISS = 6.37
P_{r,B} REL = 3.384 PSFA

Figure 47 Rotor Blade Tip Shock Location, $\frac{W_r \sqrt{\theta}}{\delta} = 126.24$

70% SPEED

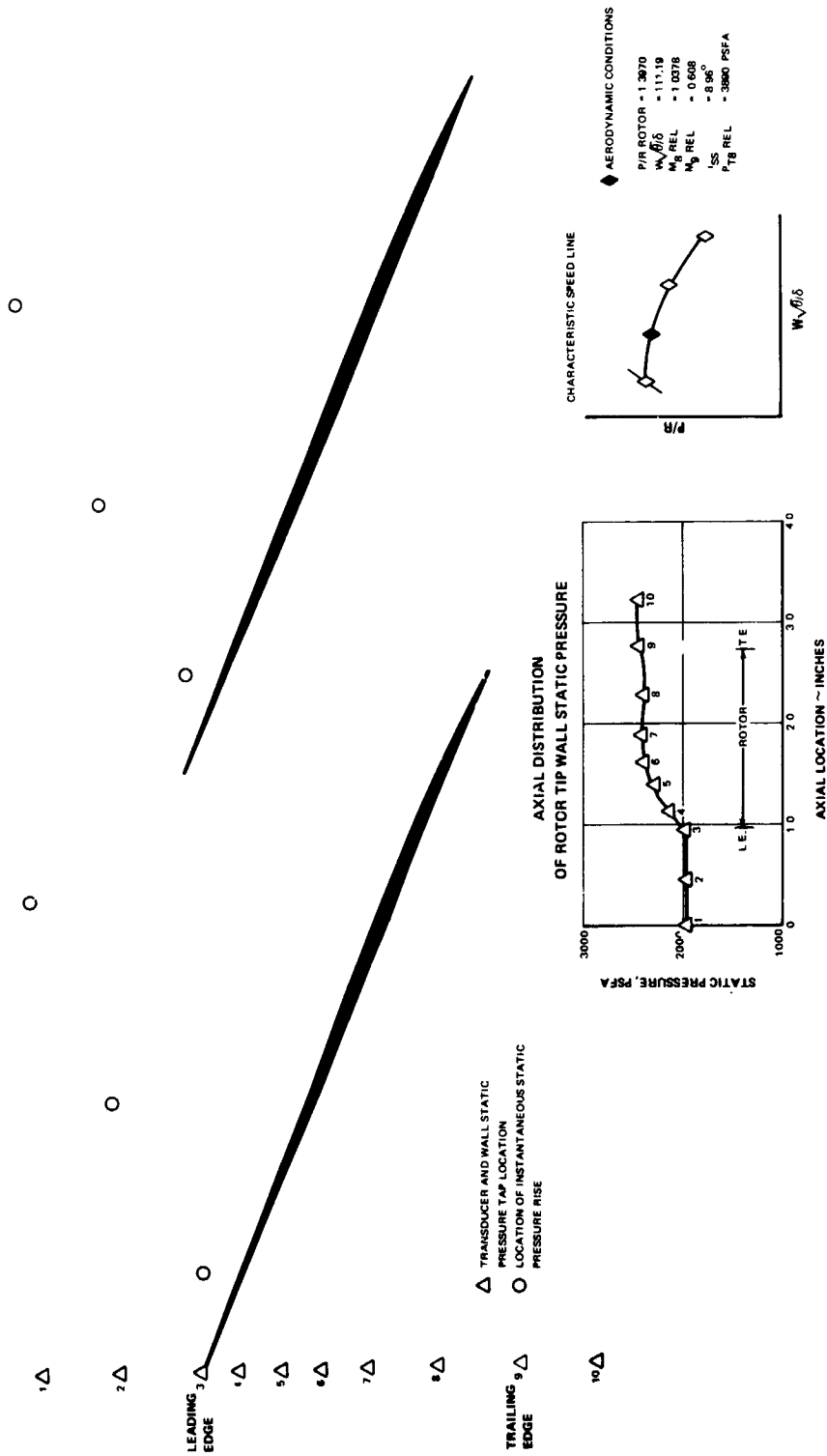


Figure 48 Rotor Blade Tip Shock Location, $\frac{W/V_{TIP}}{\delta} = 111.19$

90% SPEED

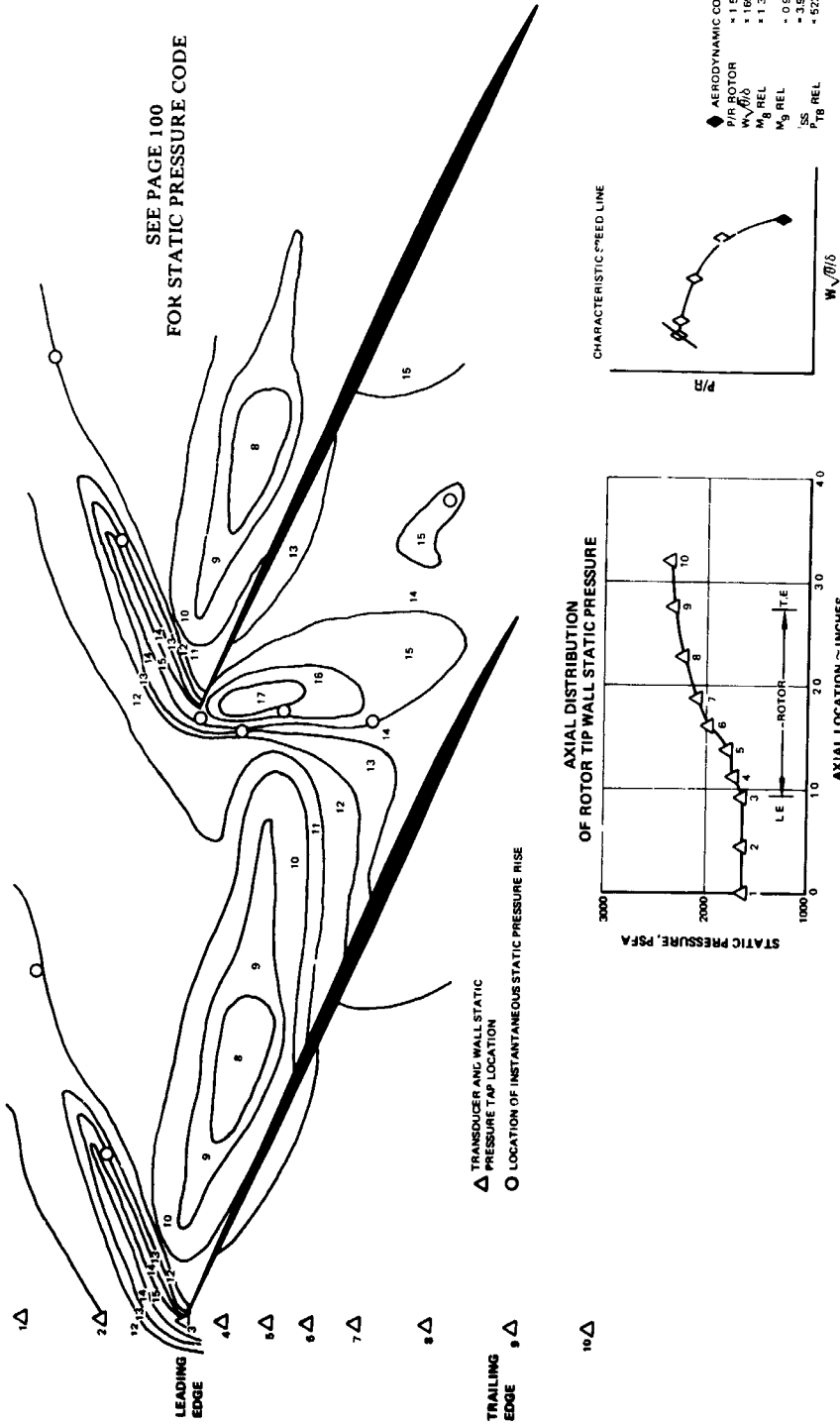


Figure 49 Rotor Blade Tip Static Pressure Contours, $\frac{W_{\infty} \sqrt{\theta}}{\delta} = 169.95$

90% SPEED

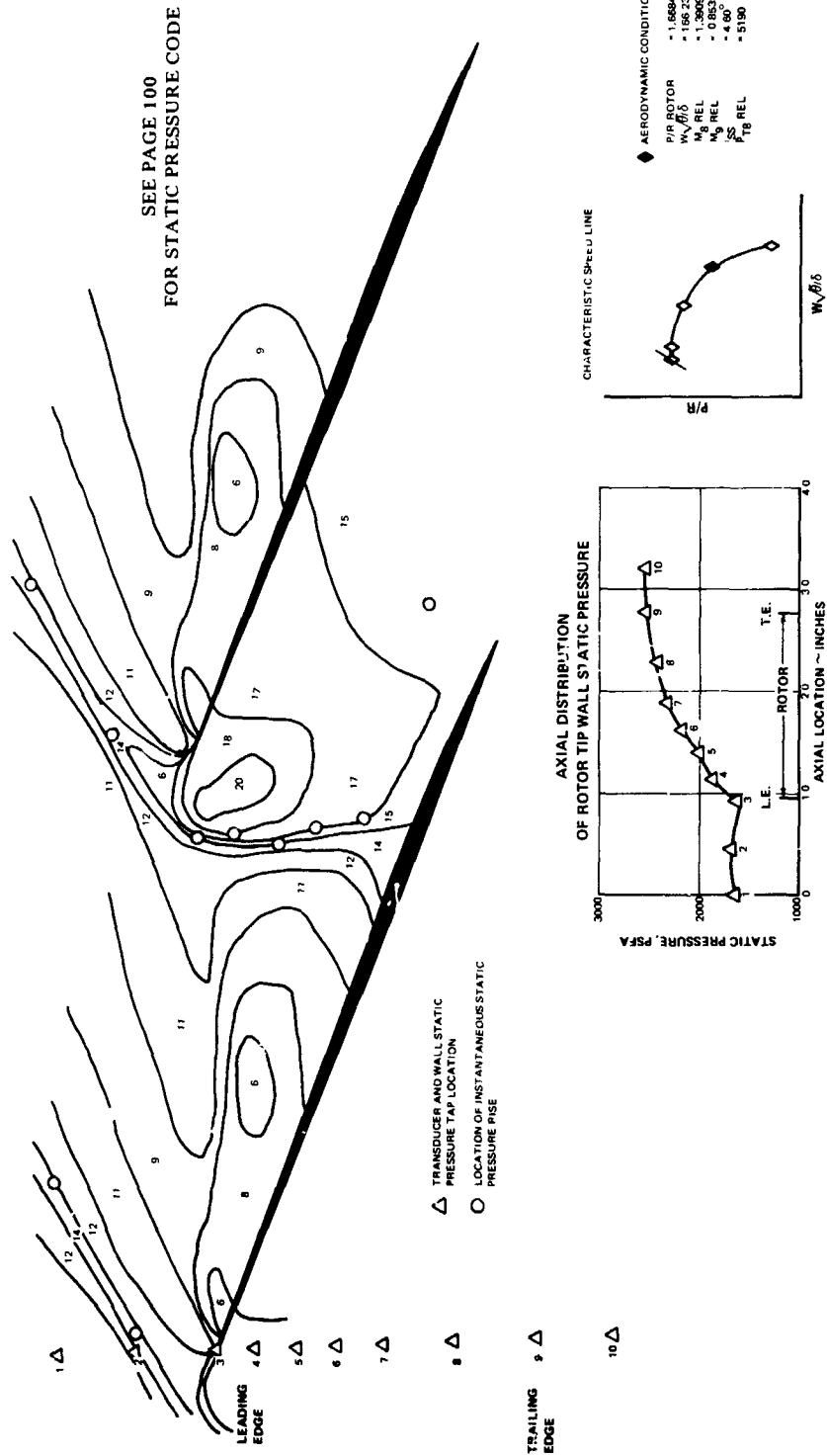


Figure 50 Rotor Blade Tip Static Pressure Contours, $\frac{W_{tip}\theta}{\delta} = 166.23$

90% SPEED

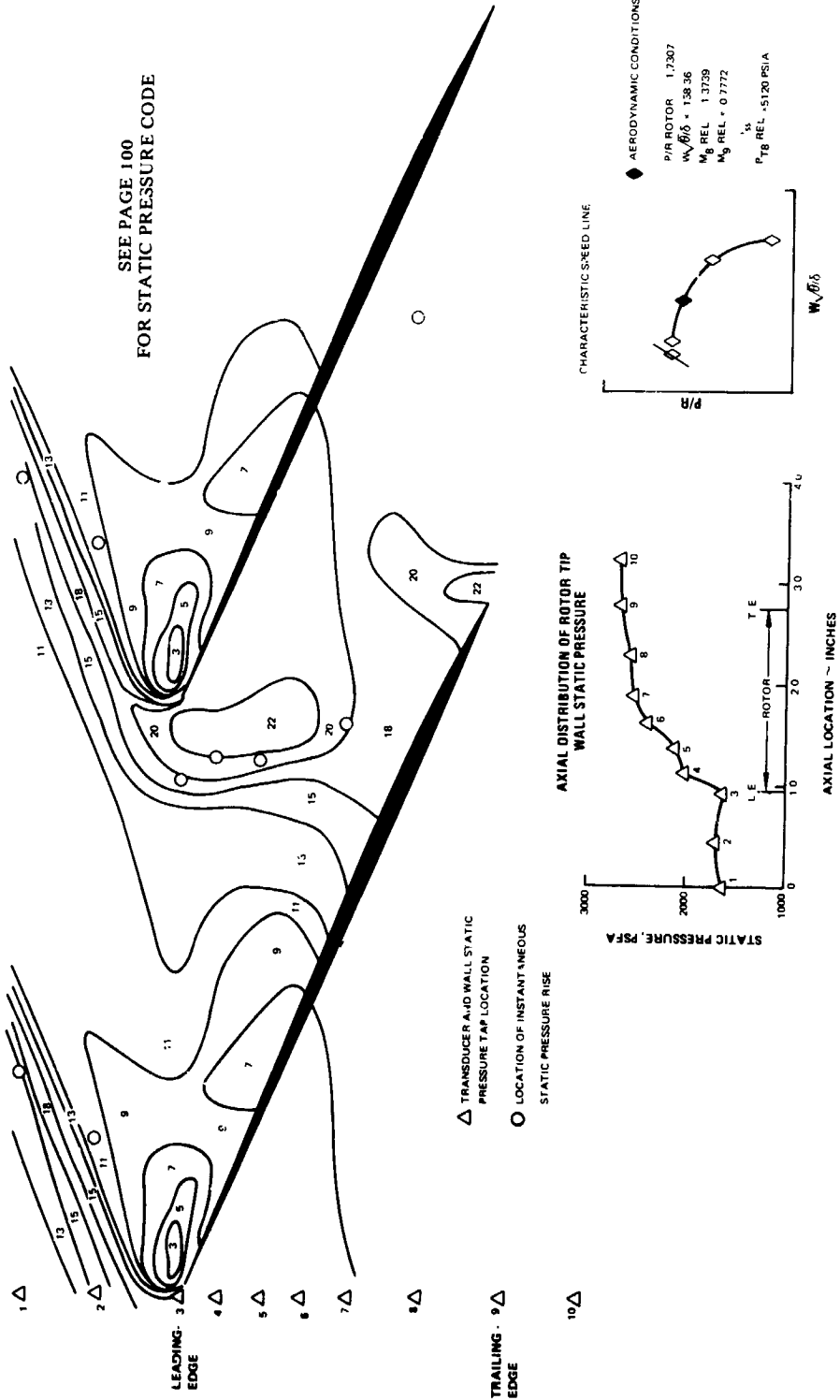
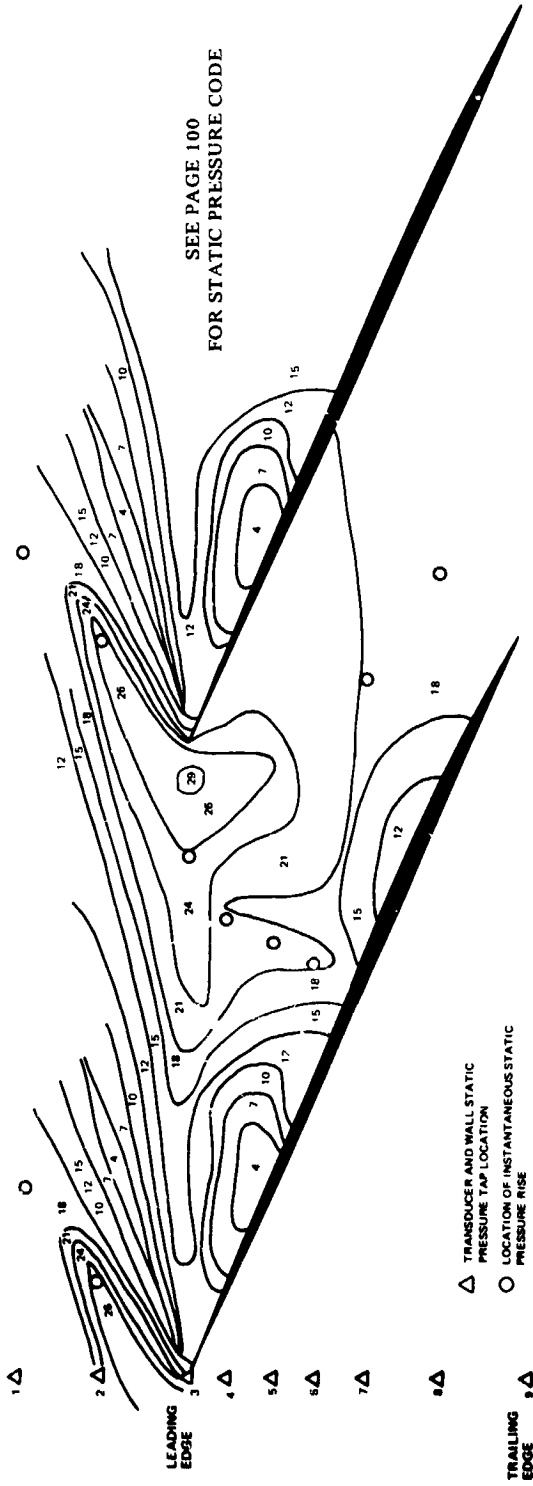


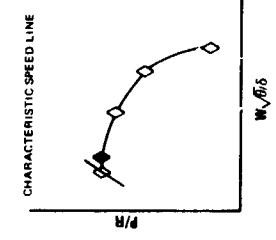
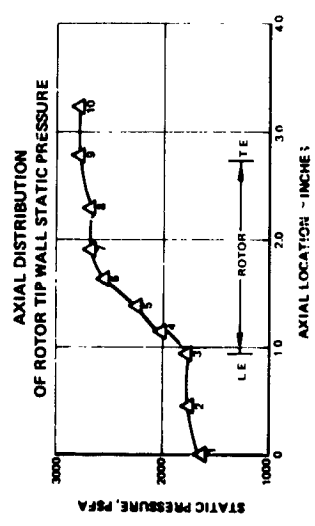
Figure 51 Rotor Blade Tip Static Pressure Contours, $\frac{W\sqrt{\sigma}}{\delta} = 158.36$

90% SPEED



SEE PAGE 100
FOR STATIC PRESSURE CODE

- △ TRANSDUCER AND WALL STATIC PRESSURE TAP LOCATION
- LOCATION OF INSTANTANEOUS STATIC PRESSURE RISE



◆ AERODYNAMIC CONDITIONS
P/R ROTOR = 1.7564
W_r / U_∞ = 1.4974
M₀ R₀ = 1.3584
M₀ REL = 0.7331
Ψ₀ = 7.34°
P/TB REL = 5280. PSFA

Figure 52 Rotor Blade Tip Static Pressure Contours, $\frac{W_r \sqrt{\theta}}{\delta} = 149.74$

100% SPEED

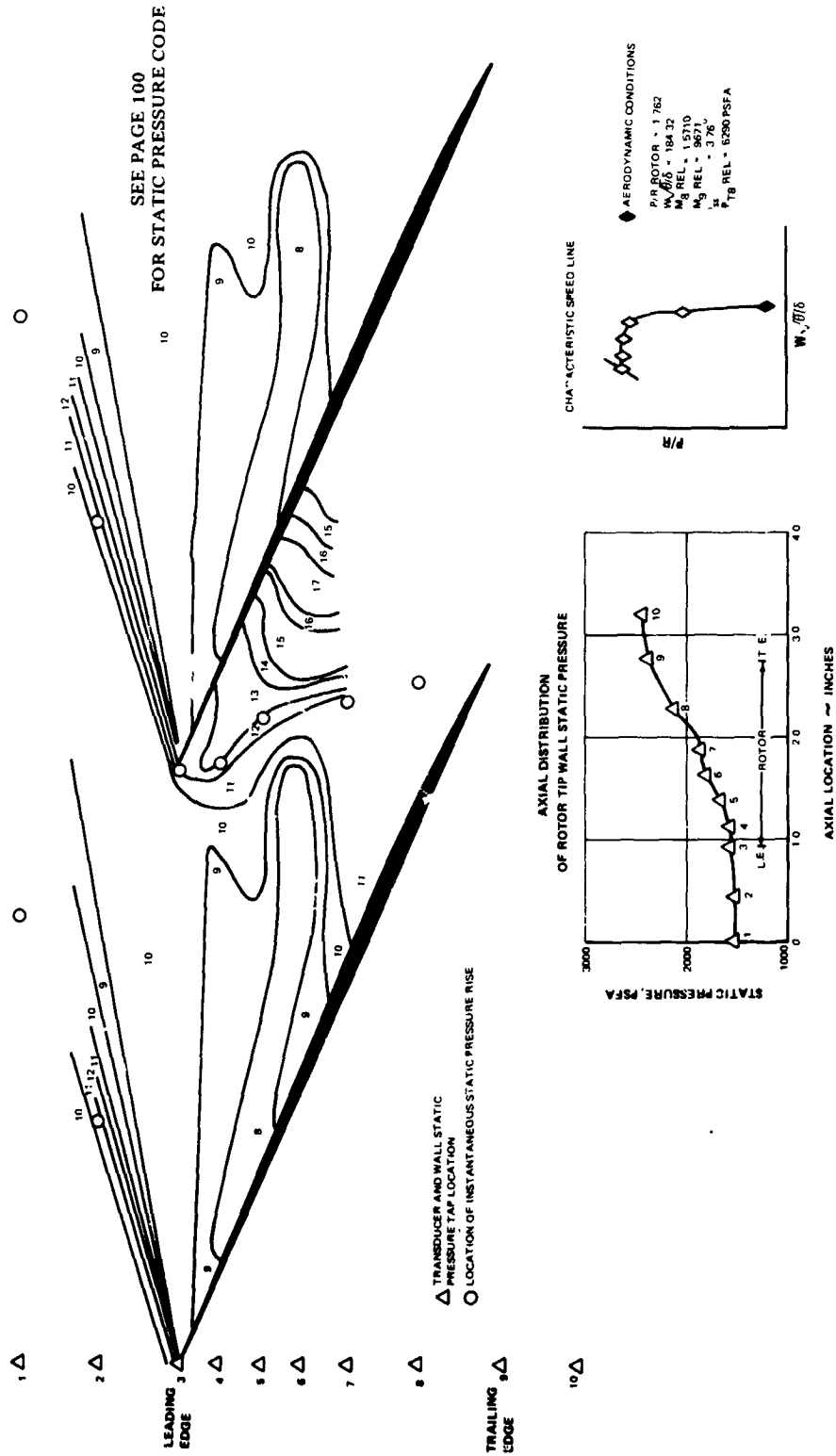


Figure 53 Rotor Blade Tip Static Pressure Contours, $\frac{W_{tip}\theta}{\delta} = 184.32$

100% SPEED

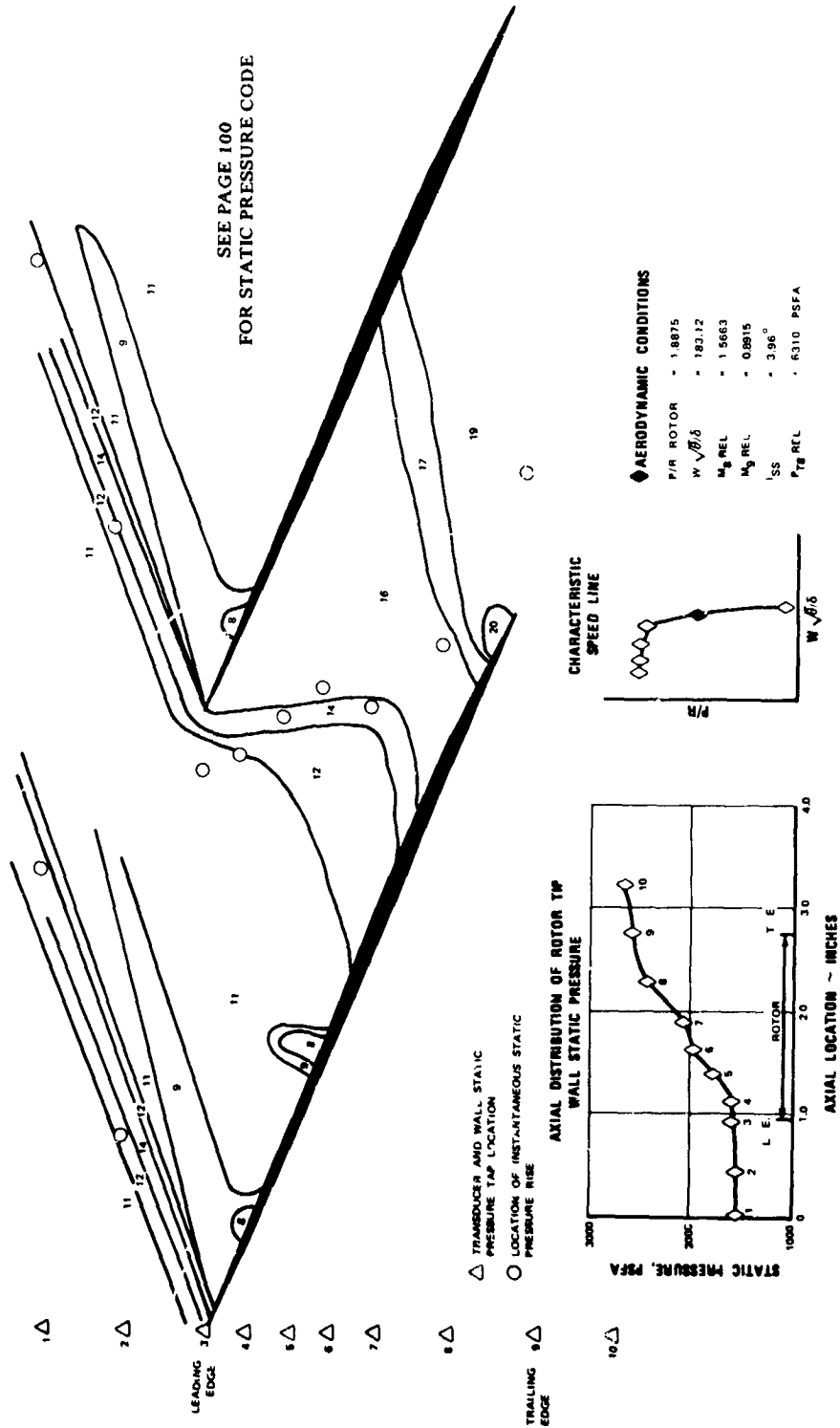


Figure 54 Rotor Blade Tip Static Pressure Contours, $\frac{W\sqrt{\theta}}{\delta} = 183.12$

100% SPEED

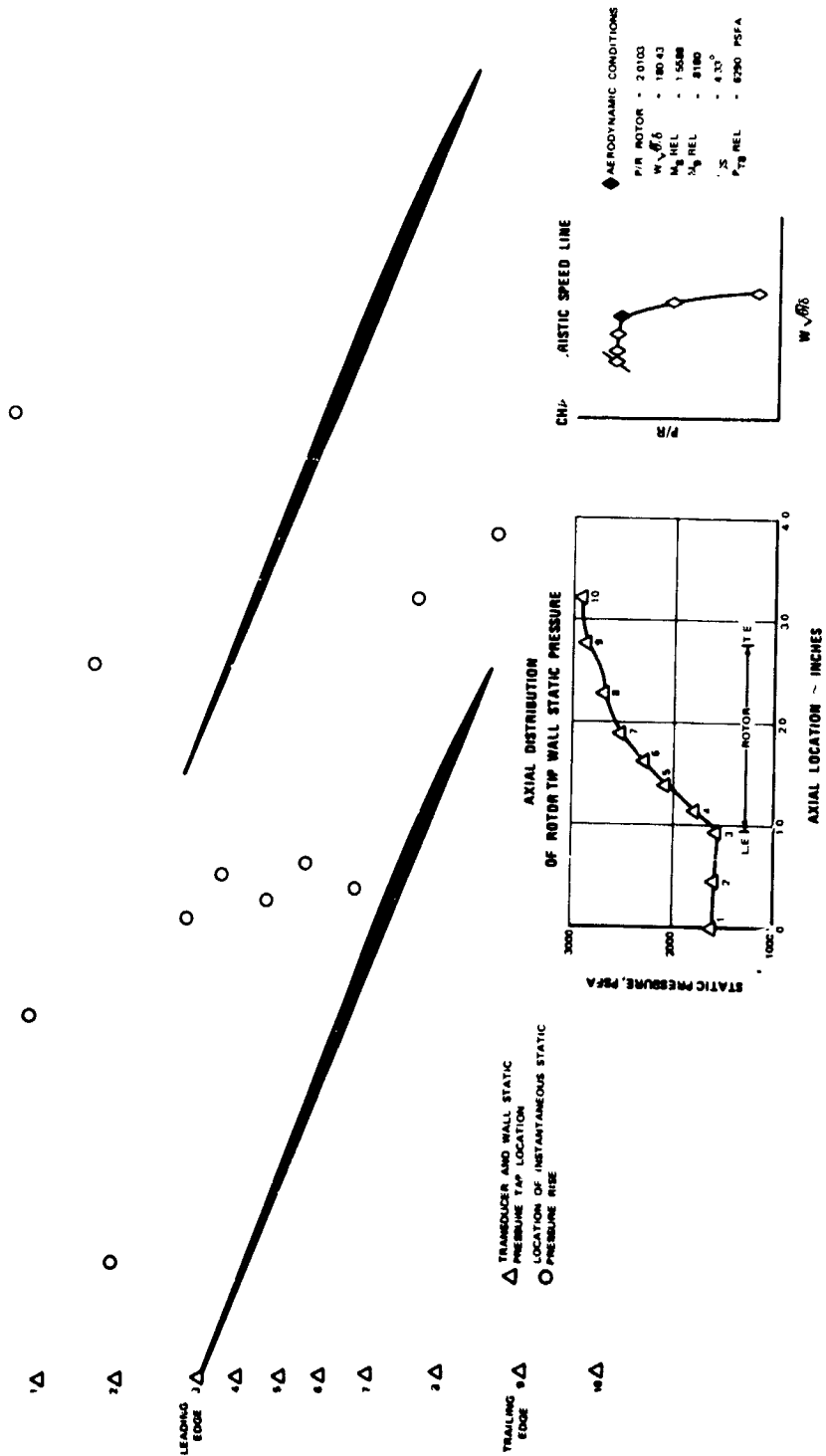


Figure 55 Rotor Blade Tip Shock Location, $\frac{W\sqrt{\rho}}{\delta} = 180.43$

100% SPEED

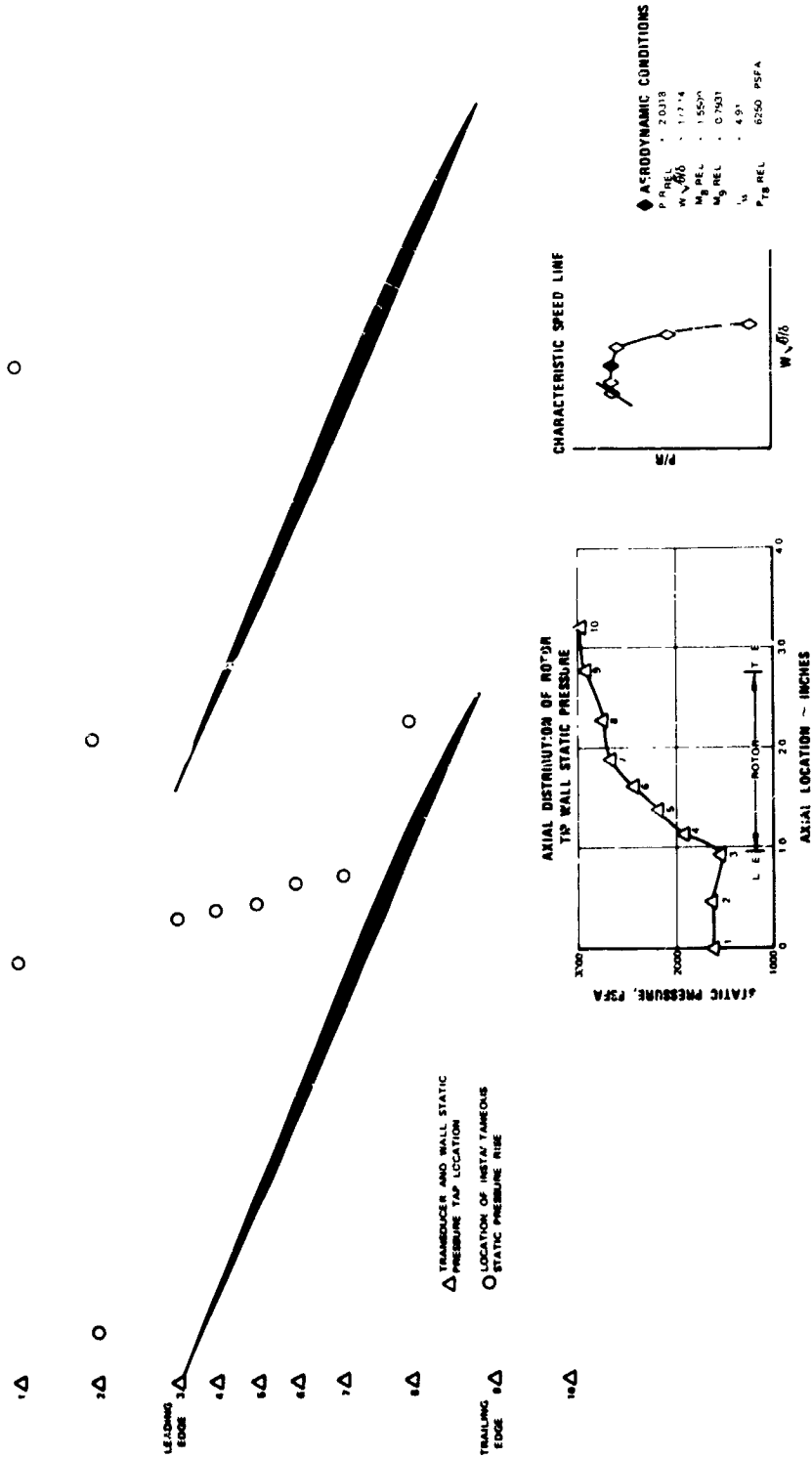


Figure 56 Rotor Blade Tip Shock Location, $\frac{W_{tip}}{\delta} = 177.14$

100% SPEED

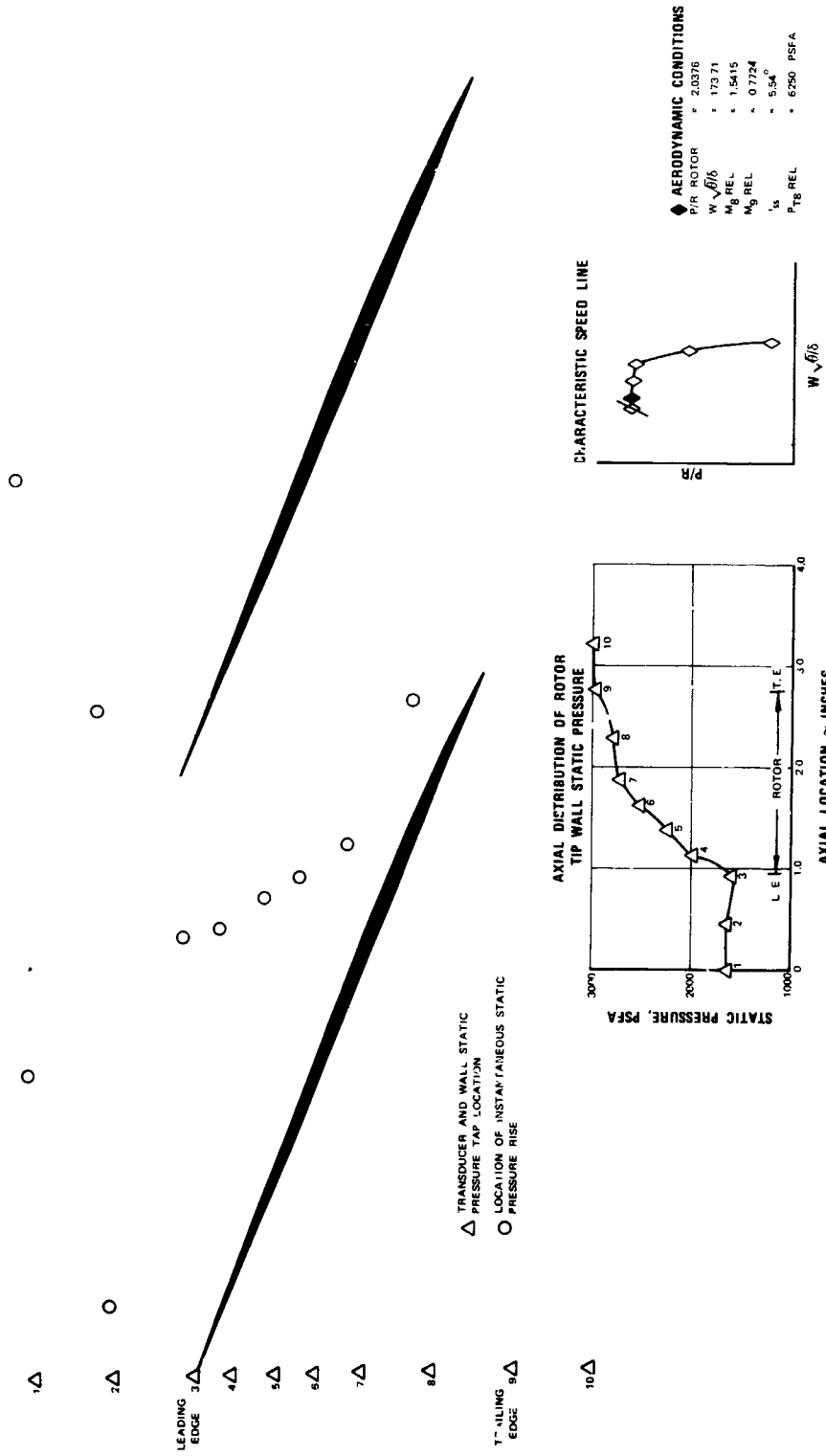


Figure 57 Rotor Blade Tip Shock Location, $\frac{W \sqrt{\theta}}{\delta} = 173.71$

105% SPEED

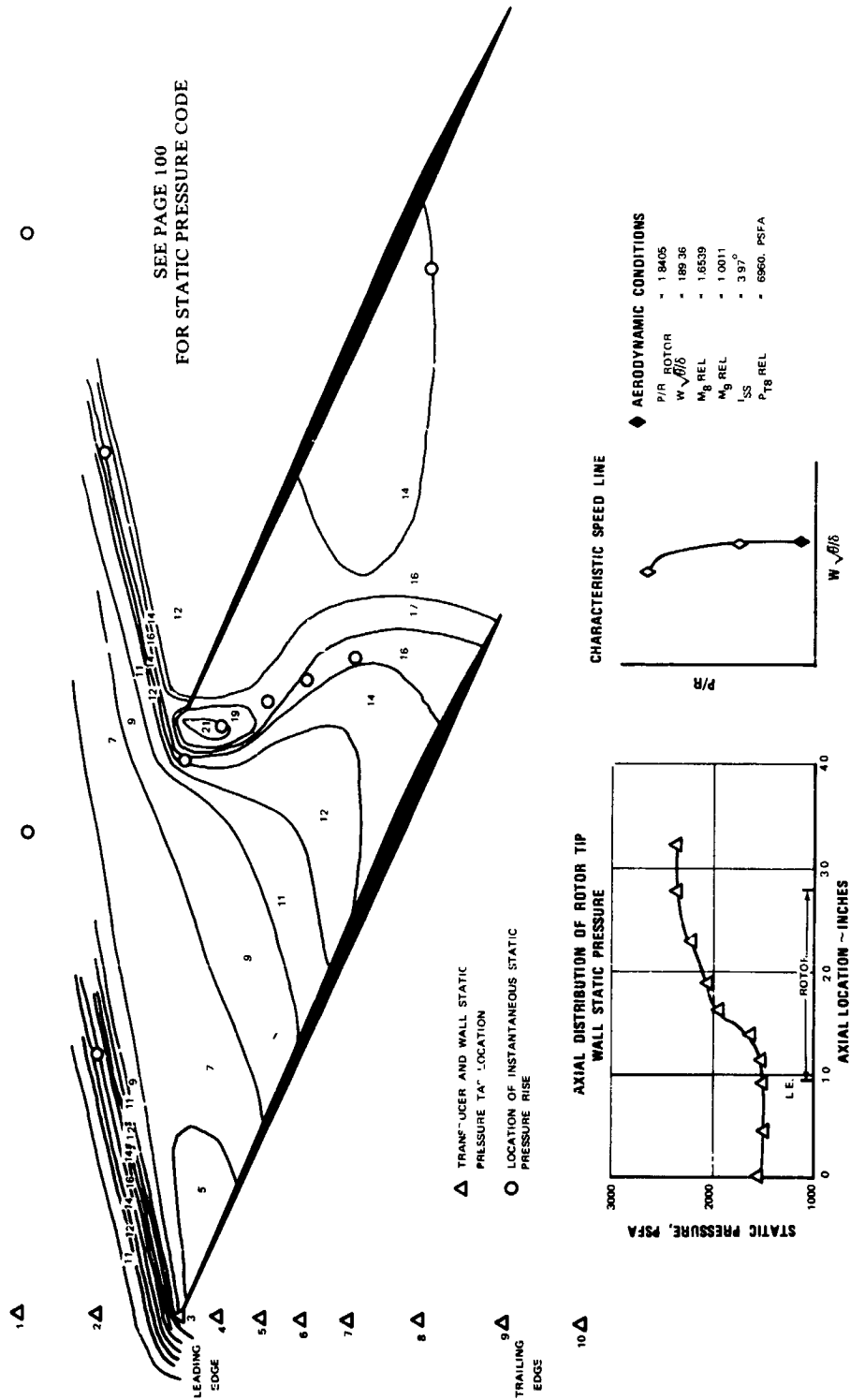


Figure 58 Rotor Blade Tip Static Pressure Contours, $\frac{W_{\infty} \beta}{\delta} = 189.36$

105% SPEED

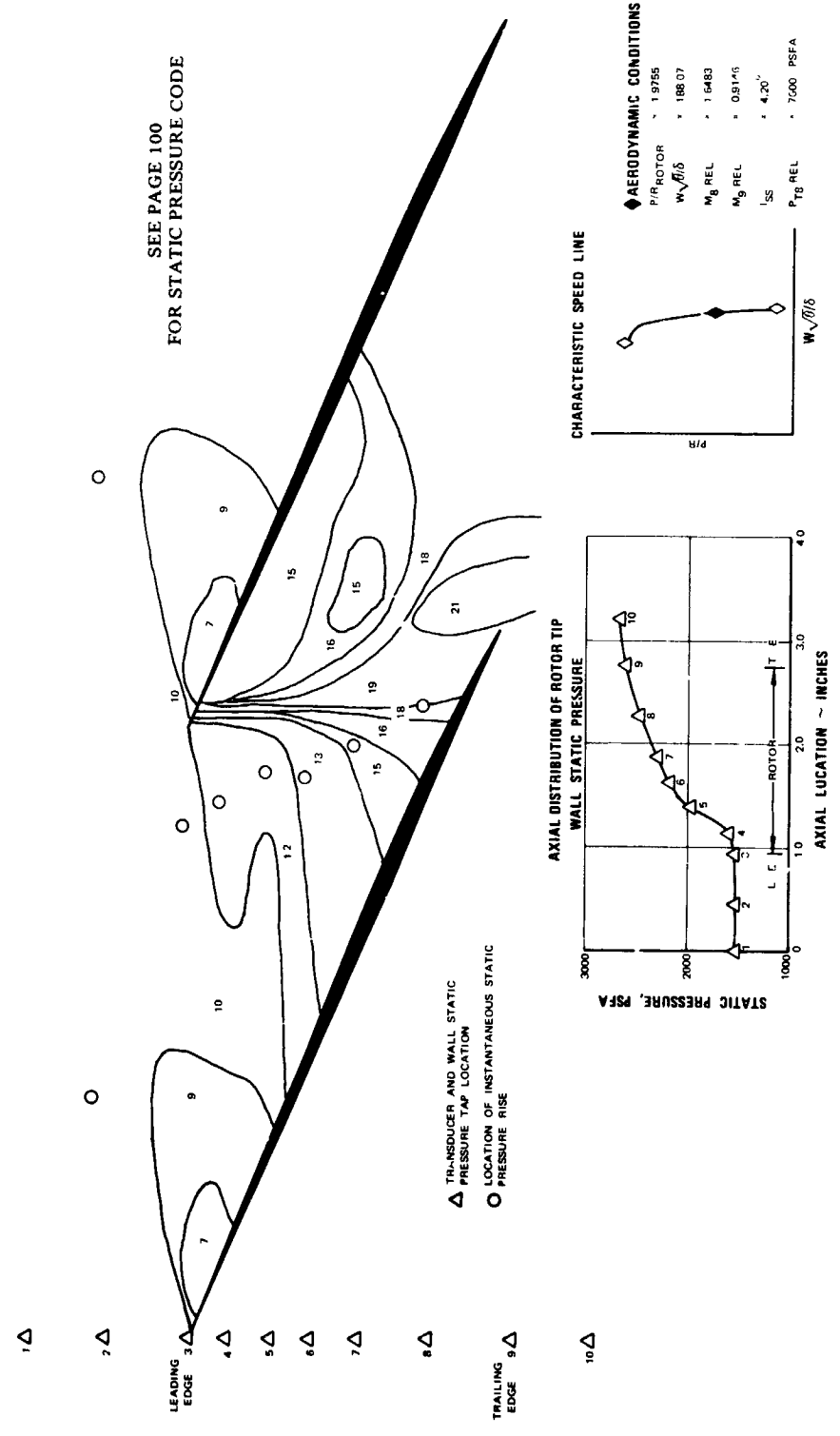


Figure 59 Rotor Blade Tip Static Pressure Contours, $\frac{W\sqrt{\theta}}{\delta} = 188.07$

105% SPEED

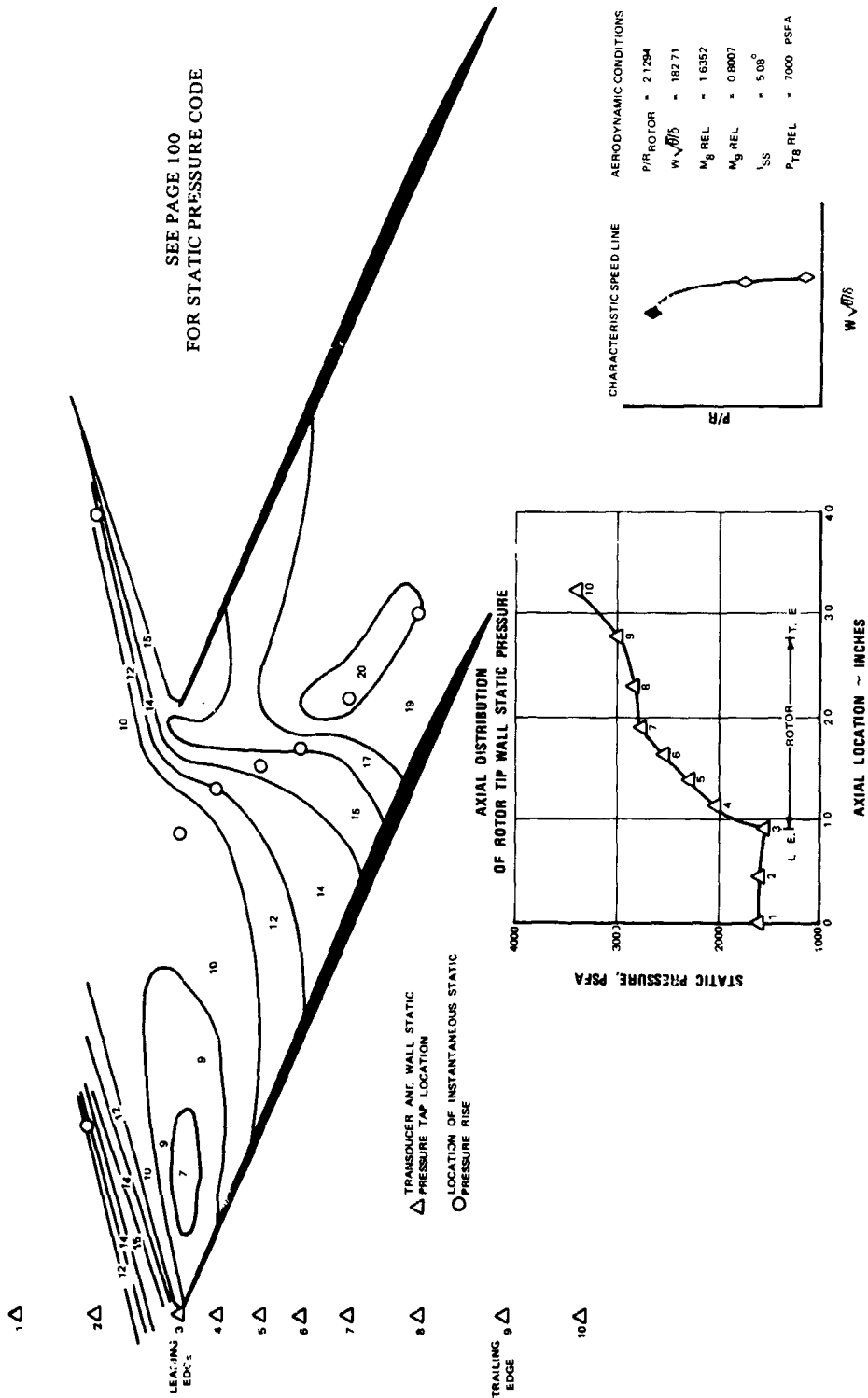


Figure 60 Rotor Blade Tip Static Pressure Contours, $\frac{W\sqrt{\theta}}{\delta} = 182.71$

TABLE 19

ROTOR BLADE TIP STATIC PRESSURE CODE

<u>SYMBOL</u>	<u>ABSOLUTE PRESSURE RANGE (PSIA)</u>	<u>AVERAGE PRESSURE (PSFA)</u>
0	0 - 1	72
1	1 - 2	216
2	2 - 3	360
3	3 - 4	504
4	4 - 5	648
5	5 - 6	792
6	6 - 7	936
7	7 - 8	1080
8	8 - 9	1224
9	9 - 10	1368
10	10 - 11	1512
11	11 - 12	1656
12	12 - 13	1800
13	13 - 14	1944
14	14 - 15	2088
15	15 - 16	2232
16	16 - 17	2376
17	17 - 18	2520
18	18 - 19	2664
19	19 - 20	2808
20	20 - 21	2952
21	21 - 22	3096
22	22 - 23	3240
23	23 - 24	3384
24	24 - 25	3528
25	25 - 26	3672
26	26 - 27	3816
27	27 - 28	3960
28	28 - 29	4104
29	29 - 30	4248
30	30 - 31	4392

APPENDIX 1

Performance Parameters

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APPENDIX 1

Performance Parameters

- a) Relative total temperature

$$T'_8 = t_8 \left[1 + \frac{\gamma - 1}{2} (M'_8)^2 \right] \quad (\text{rotor in})$$

$$T'_9 = T'_8 + \left[\frac{(\omega r_8)^2 - (\omega r_9)^2}{\frac{2\gamma}{\gamma - 1} Rg_c} \right] \quad (\text{rotor out})$$

- b) Incidence angle based on mean camber line

$$i_m = \beta'_8 - \beta'^*_8 \quad (\text{rotor})$$

$$i_m = \beta_{10} - \beta^*_{10} \quad (\text{stator})$$

- c) Deviation

$$\delta^\circ = \beta'_9 - \beta'^*_9 \quad (\text{rotor})$$

$$\delta^\circ = \beta_{11} - \beta^*_{11} \quad (\text{stator})$$

- d) Diffusion factor

$$D = 1 - \frac{V'_9}{V'_8} + \frac{r_9 V_{\theta 9} - r_8 V_{\theta 8}}{(r_8 + r_9) \sigma V'_8} \quad (\text{rotor})$$

$$D = 1 - \frac{V_{11}}{V_{10}} + \frac{r_{10} V_{\theta 10} - r_{11} V_{\theta 11}}{(r_{10} + r_{11}) \sigma V_{10}} \quad (\text{stator})$$

- e) Loss coefficient

$$\varepsilon = \frac{P'_8 \left[\frac{T'_9}{T'_8} \right]^{\frac{\gamma}{\gamma - 1}} - P'_9}{P'_8 - P_8} \quad (\text{rotor})$$

$$\varepsilon = \frac{P_{10} - P_{11}}{P_{10} - P_{10}} \quad (\text{stator})$$

f) Loss parameter

$$\frac{\bar{\omega} \cos \beta' 9}{2 \sigma} \quad (\text{rotor})$$

$$\frac{\bar{\omega} \cos \beta 11}{2} \quad (\text{stator})$$

g) Polytropic efficiency

$$1) \eta_p = \frac{\frac{\gamma-1}{\gamma} \ln \left[\frac{P_9}{P_7} \right]}{\ln \left[\frac{T_9}{T_0} \right]} \quad (\text{rotor})$$

$$2) \eta_p = \frac{\frac{\gamma-1}{\gamma} \ln \left[\frac{P_{11}}{P_{10}} \right]}{\ln \left[\frac{t_{11}}{t_{10}} \right]} \quad (\text{stator})$$

h) Adiabatic efficiency

$$\eta_{ad} = \frac{\left[\frac{P_9}{P_7} \right]^{\frac{\gamma-1}{\gamma}} - 1}{\left[\frac{T_{12}}{T_0} \right]^{-1} - 1} \quad (\text{rotor})$$

$$\eta_{ad} = \frac{\left[\frac{P_{12}}{P_7} \right]^{\frac{\gamma-1}{\gamma}} - 1}{\left[\frac{T_{12}}{T_0} \right]^{-1} - 1} \quad (\text{stage})$$

i) Wake blockage factor

$$\bar{K} = \frac{\sum_n \rho AV}{n} / \rho AV_{avg}$$

APPENDIX 2

Symbols

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APPENDIX 2

Symbols

- A - area, ft²
- A_{an} - annulus area, ft²
- A_f - frontal area, ft²
- c - chord length, in
- D - diffusion factor
- g_c - conversion factor, 32.17 lb_mft/lb sec²
- i_m - incidence angle, angle between inlet air direction and line tangent to blade mean camber line at leading edge, degrees (labelled INCM, Table 5)
- i_s - incidence angle, angle between inlet air direction and line tangent to blade suction surface at leading edge, degrees (labelled INCS, Table 5)
- M - Mach number
- MR - mass average in radial directions (Tables 15 and 16)
- N - rotor speed, rpm ($N/\sqrt{\theta}$ labelled NCOR, Table 5)
- P - total pressure, psfa
- p - static pressure, psfa
- r - radius, ft
- R - gas constant for air, ft lb/lb_m °R
- S - blade spacing, in
- T - total temperature, °R
- t - static temperature, °R
- t/c - thickness-to-chord ratio

- U - rotor speed, ft/sec
- V - air velocity, ft/sec
- V_m - meridional velocity ($V_r^2 + V_z^2$)^{1/2} ft/sec (labelled VM, Table 5)
- W - weight flow, lbs/sec
- β - absolute air angle, $\cot^{-1}(V_m/V_\theta)$, degrees (labelled B, Table 5)
- β' - rotating air angle, $\cot^{-1}(V_m/V_\theta')$, degrees (labelled B', Table 5)
- γ - ratio of specific heats for air, 1.4
- Δβ - air turning angle, degrees
- Δβ* - camber angle, degrees
- δ - ratio of inlet total pressure to standard pressure of 2116.22 lbs/ft²
- δ° - deviation angle, angle between exit air direction and tangent to blade mean camber line at trailing edge, degrees
- ε - angle between tangent to streamline projected on meridional plane and axial direction, degrees
- η - efficiency, %
- θ - ratio of inlet total temperature to standard temperature of 518.6°R
- ρ - mass density, lbs-sec²/ft⁴
- σ - solidity, ratio of chord to spacing
- Ω - total pressure loss coefficient (labelled OMEGA - B, Table 5)
- ω - angular velocity of rotor, radians/sec

Superscripts:

- ' - relative to moving blades
- * - designates blade metal angle

Subscripts:

- ad - adiabatic
- F - polytropic or profile
- r - radial direction
- m - meridional direction (in z-r plane)
- sh - shock
- ss - suction surface
- z - axial direction
- θ - tangential direction (labelled O, Table 5)
- 0 - plenum chamber
- 7 - instrument plane upstream of rotor
- 8 - station at rotor leading edge
- 9 - station at rotor trailing edge
- 10 - station at stator leading edge
- 11 - station at stator trailing edge
- 12 - instrument plane downstream of stator

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APPENDIX 3

**Blade-Element and Overall Performance with
Uniform Inlet Flow**

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TABLE 5
Identification of Blade-Element and Overall Performance Table Headings

ROTOR

1	DIA-1	IN	V-1	VM-1	VO-1	B-1	B'-1	V'-1	VO'-1	U-1	U'-1
5	IN	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC
10	2I8	V8	Vm8	Vθ8	Vθ9	β8	β9	V'8	V'9	θ8	U8
15											
20											
30											
40											
50											
60											
70											
80											
90											

1	INCS	INCM	DEV	TURN	CAMBER	OMEGA-B	D-FAC	OMEGA-B	LOSS-P	LOSS-P	PO2/	PO2/	EFF-P	EFF-AD	EFF-P	M-1	M-2	M'-1	M'-2
5	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	TOTAL	PROFILE	TOTAL	TOTAL	TOTAL	STATIC	STATIC	STATIC	STATIC
10	i _{s8}	i _{m8}	δ ₉	Δβ	Δβ*	ω _{sh}	D	ω	$\frac{\bar{\omega} \cos \beta'_9}{2\sigma}$	$\frac{P_9}{P_8}$	η _p	η _{ad}	η _{ps}	M ₈	M ₉	M' ₈	M' ₉	M' ₈	M' ₉
15																			
20																			
30																			
40																			
50																			
60																			
70																			
80																			
90																			

TO/TO PO/PO EFF-AD EFF-P
INLET INLET INLET

$\frac{T_9}{T_0}$ $\frac{P_9}{P_0}$ η_{ad} η_p

STATOR

1	DIA-1	IN	V-1	VM-1	VO-1	B-1	B'-1	V'-1	VO'-1	U-1	U'-1
5	IN	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC
10	2I10	V10	Vm10	Vθ10	Vθ11	β10	β11	V'10	V'11	θ10	U10
15											
20											
30											
40											
50											
60											
70											
80											
90											

1	INCS	INCM	DEV	TURN	CAMBER	OMEGA-B	D-FAC	OMEGA-B	LOSS-P	LOSS-P	PO2/	PO2/	EFF-P	EFF-AD	EFF-P	M-1	M-2	M'-1	M'-2
5	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	TOTAL	PROFILE	TOTAL	TOTAL	TOTAL	STATIC	STATIC	STATIC	STATIC
10	i _{s10}	i _{m10}	δ ₁₁	Δβ	Δβ*	ω _{sh}	D	ω	$\frac{\bar{\omega} \cos \beta'_{11}}{2\sigma}$	$\frac{P_{11}}{P_{10}}$	η _p	η _{ad}	η _{ps}	M ₁₀	M ₁₁	M' ₁₀	M' ₁₁	M' ₁₀	M' ₁₁
15																			
20																			
30																			
40																			
50																			
60																			
70																			
80																			
90																			

TO/TO PO/PO EFF-AD EFF-P
INLET INLET INLET

$\frac{T_{11}}{T_0}$ $\frac{P_{11}}{P_0}$ η_{ad} η_p

STAGE PARAMETERS

1	INCORR	WCORR	TO/TO	PO/PO	EFF-AD	EFF-P
5	RPM	LBM/SEC	INLET	INLET	INLET	INLET
10	$\frac{N}{\sqrt{\theta}}$	$\frac{W\sqrt{\theta}}{\delta}$	$\frac{T_{11}}{T_0}$	$\frac{P_{11}}{P_0}$	η _{ad}	η _p
15						
20						
30						
40						
50						
60						
70						
80						
90						

TABLE 6
Blade-Element and Overall Performance - Design Data

ROTOR

Table with columns for span, dia, in, v, ft/sec, v-1, v-2, vm-1, vm-2, u-1, u-2, b-1, b-2, b-1-1, b-1-2, v-1-1, v-1-2, v-2-1, v-2-2, u-1-1, u-1-2, u-2-1, u-2-2, m-1, m-2, m-1-1, m-1-2, m-2-1, m-2-2. Includes sub-sections for camber, omega, and loss profile.

STATOR

Table with columns for span, dia, in, v, ft/sec, v-1, v-2, vm-1, vm-2, u-1, u-2, b-1, b-2, b-1-1, b-1-2, v-1-1, v-1-2, v-2-1, v-2-2, u-1-1, u-1-2, u-2-1, u-2-2, m-1, m-2, m-1-1, m-1-2, m-2-1, m-2-2. Includes sub-sections for camber, omega, and loss profile.

TABLE 7.2
Blade-Element and Overall Performance with Uniform Inlet
50% of Design Speed

ROTOR

%SPAN	DIA-1 IN	DIA-2 IN	V-1 FT/SEC	V-2 FT/SEC	VM-1 FT/SEC	VM-2 FT/SEC	VO-1 FT/SEC	VO-2 FT/SEC	B-1 DEGREE	B-2 DEGREE	B1-1 DEGREE	B1-2 DEGREE	V1-1 FT/SEC	V1-2 FT/SEC	VO-1 FT/SEC	VO-2 FT/SEC	U-1 FT/SEC	U-2 FT/SEC
5	17.467	19.769	269.2	268.4	269.2	419.6	0	385.3	0.0	42.41	57.55	12.86	501.6	430.4	423.3	494.8	423.3	479.1
10	18.467	20.408	274.8	274.3	274.3	400.6	0	355.6	0.0	41.58	58.45	13.15	525.2	424.5	417.5	487.5	487.5	494.6
15	19.467	21.047	279.7	279.7	279.7	385.7	0	325.9	0.0	40.75	59.34	23.48	548.5	427.9	411.8	471.8	471.8	510.1
30	22.314	22.964	289.4	289.4	289.4	368.7	0	273.1	0.0	36.50	61.84	31.49	613.4	465.6	450.8	483.5	483.5	556.3
50	25.791	25.520	292.8	292.8	292.8	350.7	0	220.6	0.0	32.15	64.90	46.56	650.2	530.6	520.0	537.9	537.9	618.5
70	28.954	28.076	287.8	287.8	287.8	337.6	0	171.5	0.0	28.57	67.74	55.85	756.4	600.4	591.7	606.9	606.9	680.4
85	31.295	29.993	279.2	279.2	279.2	317.2	0	171.5	0.0	28.47	69.79	60.25	808.2	639.3	636.4	654.9	654.9	726.9
90	31.883	30.630	276.6	276.6	276.6	290.1	0	175.5	0.0	31.19	70.30	62.90	820.7	636.6	636.6	654.9	654.9	742.3
95	32.499	31.271	274.3	274.3	274.3	259.8	0	176.0	0.0	34.12	70.80	65.94	834.0	637.2	637.2	654.9	654.9	757.9

%SPAN	INCS DEGREE	INCM DEGREE	DEV DEGREE	TURIN DEGREE	CAMBER DEGREE	OMEGA-B DEGREE	D-FAC DEGREE	LOSS-P DEGREE	LOSS-P TOTAL	LOSS-P PROFILE	P02/ POL	EFF-P TOTAL	EFF-P TOTAL	EFF-P TOTAL	M-1 DEGREE	M-2 DEGREE	M-1 DEGREE	M-2 DEGREE
5	2.17	6.60	10.99	44.69	47.12	0.000	3.202	0.947	0.117	0.117	1.2134	0.649	0.638	0.626	2.432	5.072	4.549	3.861
10	2.50	6.84	9.51	39.32	39.99	0.000	3.552	0.962	0.209	0.209	1.1957	0.299	0.280	0.280	2.489	4.773	4.794	3.762
15	2.86	6.62	8.95	33.85	34.03	0.000	3.682	1.108	0.240	0.240	1.1794	0.702	0.949	0.862	2.533	4.495	5.016	3.808
30	4.01	7.95	7.76	24.35	24.18	0.000	3.626	0.989	0.211	0.211	1.1595	0.883	0.857	0.8120	2.614	4.079	5.599	4.138
50	5.35	7.97	6.31	16.34	14.68	0.000	3.281	0.818	0.165	0.165	1.1398	0.722	0.696	0.6165	2.638	3.681	6.244	4.714
70	6.24	6.64	5.34	11.85	9.14	0.000	2.889	0.608	0.134	0.134	1.1252	0.873	0.846	0.8105	2.591	3.408	6.852	5.333
85	6.43	6.13	9.54	8.61	0.000	2.844	0.644	0.448	0.170	0.170	1.1244	0.861	0.824	0.7334	2.510	3.201	7.364	5.670
90	6.47	7.55	7.78	7.41	7.64	0.000	3.014	0.363	0.229	0.229	1.1030	0.958	0.910	0.8482	2.493	3.002	7.730	5.631
95	6.59	7.50	10.08	4.86	7.45	0.000	3.136	0.1693	0.259	0.259	1.0952	0.6193	0.6137	0.5884	2.472	2.773	7.508	5.631

To/To P0/P0 EFF-AD EFF-P
INLET INLET INLET INLET

1.0458 1.1441 85.60 85.96

STATOR

%SPAN	DIA-1 IN	DIA-2 IN	V-1 FT/SEC	V-2 FT/SEC	VM-1 FT/SEC	VM-2 FT/SEC	VO-1 FT/SEC	VO-2 FT/SEC	B-1 DEGREE	B-2 DEGREE	B1-1 DEGREE	B1-2 DEGREE	V1-1 FT/SEC	V1-2 FT/SEC	VO-1 FT/SEC	VO-2 FT/SEC	U-1 FT/SEC	U-2 FT/SEC
5	20.409	21.489	602.8	564.1	474.8	563.3	371.3	29.4	38.03	2.99	14.56	44.32	490.6	787.4	123.3	550.2	494.6	520.8
10	21.008	21.924	570.1	539.1	453.6	538.4	345.3	29.0	37.27	3.08	19.86	46.19	482.7	777.7	133.8	501.2	509.1	532.4
15	21.589	22.432	540.5	519.8	437.5	519.1	317.4	27.9	35.95	3.08	25.17	47.76	483.9	772.2	205.8	511.6	523.2	543.6
30	23.314	23.902	496.3	479.5	417.3	478.6	268.6	26.0	32.75	3.11	35.34	51.65	512.3	771.9	296.4	605.3	565.0	579.3
50	25.601	25.893	456.0	440.1	399.7	438.9	219.5	32.9	28.76	4.29	45.05	56.39	565.4	793.1	401.0	690.4	620.4	627.5
70	27.813	27.982	434.5	408.1	383.4	406.8	185.2	31.8	25.22	4.47	51.20	60.11	627.4	816.6	489.0	748.2	674.2	676.2
85	29.408	29.382	424.5	380.8	366.3	379.7	175.9	29.6	24.48	4.46	54.26	62.89	661.4	833.3	536.8	741.7	712.7	712.1
90	29.914	29.856	410.4	361.1	368.8	360.0	180.1	28.1	26.03	4.40	55.91	64.41	650.0	833.4	544.9	751.6	725.0	733.6
95	30.382	30.293	395.3	334.8	351.3	333.8	181.3	26.0	27.29	4.46	57.67	66.29	656.9	830.2	555.0	760.2	736.3	734.1

%SPAN	INCS DEGREE	INCM DEGREE	DEV DEGREE	TURIN DEGREE	CAMBER DEGREE	OMEGA-B DEGREE	D-FAC DEGREE	LOSS-P DEGREE	LOSS-P TOTAL	LOSS-P PROFILE	P02/ POL	EFF-P TOTAL	EFF-P TOTAL	EFF-P TOTAL	M-1 DEGREE	M-2 DEGREE	M-1 DEGREE	M-2 DEGREE
5	7.85	4.93	9.42	41.01	55.96	0.000	2.258	0.618	0.203	0.203	0.9853	0.000	0.000	0.463	5.310	4.339	7.024	6.939
10	8.20	5.26	8.37	40.35	53.87	0.000	2.187	0.643	0.164	0.164	0.9896	0.000	0.000	0.496	4.986	4.303	6.939	6.883
15	8.65	5.71	7.93	39.83	52.51	0.000	2.077	0.308	0.086	0.086	0.9951	0.000	0.000	0.526	4.772	4.834	6.883	6.873
30	9.89	6.88	8.11	35.86	54.60	0.000	1.988	0.308	0.086	0.086	0.9961	0.000	0.000	0.570	4.368	4.270	6.883	6.873
50	12.11	8.97	7.76	33.85	49.60	0.000	2.036	0.232	0.093	0.093	0.9971	0.000	0.000	0.610	4.086	4.317	6.883	6.873
70	14.89	11.24	9.03	29.63	43.98	0.000	2.221	0.130	0.130	0.130	0.9961	0.000	0.000	0.6921	3.867	3.630	6.883	6.873
85	14.79	11.47	11.44	28.94	51.99	0.000	2.271	0.562	0.196	0.196	0.9947	0.000	0.000	0.781	3.768	3.582	6.883	6.873
90	13.38	10.05	12.94	30.49	53.54	0.000	3.006	0.524	0.186	0.186	0.9954	0.000	0.000	0.742	3.641	3.520	6.883	6.873
95	12.41	9.04	15.23	31.75	56.01	0.000	3.424	0.745	0.268	0.268	0.9939	0.000	0.000	0.7506	3.511	3.262	6.883	6.873

NCOR-1 WCOR-1 To/To P0/P0 EFF-AD EFF-P
INLET INLET INLET INLET
RPM LBW/SEC
5554 92.28 1.0458 1.1396 83.66 83.40 20.74

TABLE 7.4
Blade-Element and Overall Performance with Uniform Inlet
50% of Design Speed

ROTOR

Table with columns: %SPAN, DIA-1 IN, DIA-2 IN, V-1 FT/SEC, V-2 FT/SEC, VM-1 FT/SEC, VM-2 FT/SEC, VO-1 FT/SEC, VO-2 FT/SEC, B-1 DEGREE, B-2 DEGREE, B-1-2 DEGREE, V1-1 FT/SEC, V1-2 FT/SEC, V1-1-2 FT/SEC, U1 FT/SEC, U2 FT/SEC, M1, M2, M1-1, M2-1, M1-2. Rows 6-95.

TO/TO PO/PO EFF-AD EFF-P
INLET-INLET INLET INLET
1.0539 1.1702 85.31 85.66

STATOR

Table with columns: %SPAN, DIA-1 IN, DIA-2 IN, V-1 FT/SEC, V-2 FT/SEC, VM-1 FT/SEC, VM-2 FT/SEC, VO-1 FT/SEC, VO-2 FT/SEC, B-1 DEGREE, B-2 DEGREE, B-1-2 DEGREE, V1-1 FT/SEC, V1-2 FT/SEC, V1-1-2 FT/SEC, U1 FT/SEC, U2 FT/SEC, M1, M2, M1-1, M2-1, M1-2. Rows 5-95.

MCOR-1 MCOR-1 YU/TO PO/PO EFF-AD EFF-P WC/A-1
INLET INLET INLET INLET INLET
RPM LHM/SEC 5543 83.24 1.0539 1.1628 81.79 82.20 18.71

TABLE 7.5
Blade-Element and Overall Performance with Uniform Inlet
50% of Design Speed

ROTOR

%SPAN	DIA-1 IN	DIA-2 IN	V-1 FT/SEC	V-2 FT/SEC	VM-1 FT/SEC	VM-2 FT/SEC	VO-1 FT/SEC	VO-2 FT/SEC	B-1 DEGREE	B-2 DEGREE	B-1-1 DEGREE	B-1-2 DEGREE	V1-1 FT/SEC	V1-2 FT/SEC	V0-1-1 FT/SEC	V0-1-2 FT/SEC	U-1 FT/SEC	U-2 FT/SEC	TOTAL PROFILE										
																			PO2/ IDIAL	EFF-AD STATIC	LOSS-P	OMEGA-B							
5	17.467	19.769	228.7	535.7	226.7	553.2	0	49.8	0.0	48.76	61.57	12.05	480.5	361.2	-422.5	-75.4	422.5	478.2	0.028	0.028	1.2317	0.923	0.920	0.9808	0.264	0.4760	0.358	0.329	
10	18.467	20.498	233.5	513.4	233.5	349.0	0	37.5	0.0	47.10	62.40	18.53	504.1	368.6	-448.9	-117.1	448.9	493.7	0.028	0.028	1.2317	0.923	0.916	0.914	0.9812	0.213	0.455	0.460	0.373
15	19.467	21.047	237.7	483.0	237.7	340.6	0	34.5	0.0	45.73	63.22	25.09	527.5	376.7	-470.9	-159.6	470.9	509.1	0.044	0.044	1.2110	0.953	0.949	0.9703	0.2151	0.430	0.483	0.332	
20	22.34	22.964	245.3	431.9	245.3	368.7	0	34.4	0.0	44.73	65.56	39.26	592.9	397.2	-539.8	-251.5	539.8	555.5	0.074	0.074	1.1869	0.920	0.921	0.8868	0.2211	0.3822	0.543	0.355	
30	25.791	25.520	246.3	392.5	246.3	288.8	0	28.5	0.0	42.61	68.45	59.54	670.8	455.3	-623.9	-351.6	623.9	617.3	0.177	0.177	1.1726	0.867	0.869	0.849	0.2213	0.3467	0.6099	0.4021	
40	28.564	28.076	246.6	372.6	246.6	273.7	0	26.0	0.0	42.26	71.04	78.06	709.6	509.8	-700.4	-428.7	700.4	679.2	0.222	0.222	1.1661	0.854	0.854	0.813	0.2159	0.3284	0.6699	0.4493	
50	31.295	29.993	232.8	361.9	232.8	245.3	0	27.2	0.0	47.32	72.91	61.90	732.0	520.9	-757.0	-459.9	757.0	725.5	0.334	0.334	1.1533	0.818	0.818	0.7124	0.2075	0.3144	0.7255	0.4615	
60	31.883	30.630	230.7	358.6	230.7	235.3	0	27.0	0.0	48.90	73.35	63.40	693.0	528.5	-771.2	-470.7	771.2	780.9	0.359	0.359	1.1591	0.6606	0.6531	0.6261	0.2058	0.3038	0.7355	0.4847	
86	32.499	31.271	228.7	347.0	228.7	216.0	0	271.6	0.0	51.50	73.78	65.98	618.7	550.8	-786.1	-484.9	786.1	756.4	0.451	0.451	1.1551	0.6066	0.6066	0.5951	0.2051	0.2851	0.7451	0.5753	

STATOR

%SPAN	DIA-1 IN	DIA-2 IN	V-1 FT/SEC	V-2 FT/SEC	VM-1 FT/SEC	VM-2 FT/SEC	VO-1 FT/SEC	VO-2 FT/SEC	B-1 DEGREE	B-2 DEGREE	B-1-1 DEGREE	B-1-2 DEGREE	V1-1 FT/SEC	V1-2 FT/SEC	V0-1-1 FT/SEC	V0-1-2 FT/SEC	U-1 FT/SEC	U-2 FT/SEC	TOTAL PROFILE										
																			PO2/ IDIAL	EFF-AD STATIC	LOSS-P	OMEGA-B							
5	20.409	21.489	557.4	461.7	598.1	461.7	390.2	10.5	44.43	1.30	14.58	47.82	411.3	687.4	-103.5	-59.3	493.7	519.8	0.5	0.5	1.170	0.923	0.920	0.9808	0.264	0.4760	0.358	0.329	
10	21.988	21.961	535.1	437.9	390.6	437.9	365.0	8.6	41.85	-1.67	20.04	50.86	410.2	653.8	-142.0	-54.8	493.7	531.2	0.5	0.5	1.170	0.923	0.916	0.914	0.9812	0.213	0.455	0.460	0.373
15	22.432	22.432	510.2	420.3	360	420.1	340.5	-12.3	41.85	-1.67	37.55	52.87	421.7	636.1	-161.8	-54.8	493.7	542.6	0.5	0.5	1.170	0.923	0.949	0.9703	0.2151	0.430	0.483	0.332	
20	23.314	23.92	456.6	384.8	344.6	384.8	299.3	-11.2	40.96	-1.67	47.25	56.87	435.1	703.9	-204.6	-59.6	568.7	578.2	0.5	0.5	1.170	0.923	0.921	0.8868	0.2211	0.3822	0.543	0.355	
30	25.681	25.885	420.9	351.6	327.1	351.4	264.9	-11.4	39.00	-1.80	61.13	61.13	462.5	728.3	-254.4	-69.3	618.3	626.3	0.5	0.5	1.170	0.923	0.921	0.8868	0.2211	0.3822	0.543	0.355	
40	27.811	27.811	404.1	300.5	318.2	330.1	253.3	-15.6	38.38	-2.70	52.68	64.45	537.3	765.4	-319.5	-70.7	618.3	674.9	0.5	0.5	1.170	0.923	0.921	0.8868	0.2211	0.3822	0.543	0.355	
50	29.914	29.382	406.6	314.5	342.2	314.5	272.0	5.9	41.99	1.75	55.48	66.06	553.8	776.3	-346.2	-71.2	618.3	722.2	0.5	0.5	1.170	0.923	0.921	0.8868	0.2211	0.3822	0.543	0.355	
60	30.382	30.293	389.3	294.4	285.6	293.9	279.8	17.5	43.40	3.40	56.38	66.68	535.8	773.3	-355.2	-75.3	618.3	732.6	0.5	0.5	1.170	0.923	0.921	0.8868	0.2211	0.3822	0.543	0.355	

NCOR-1 WCOR-1 TC/TO PO/PO EFF-AD EFF-P WC/A-1
 TMEFF TMEFF TMEFF TMEFF TMEFF TMEFF LBM/SEC
 RPM LHM/SEC % % %
 5544 78.40 1.0569 1.1721 81.67 82.13 17.62

TABLE 7.6
Blade-Element and Overall Performance with Uniform Inlet
50% of Design Speed

ROTOR

SPAN IN	DIA-1 IN	DIA-2 IN	V-1 FT/SEC	V-2 FT/SEC	VM-1 FT/SEC	VM-2 FT/SEC	V0-1 FT/SEC	V0-2 FT/SEC	B-1 DEGREE	B-2 DEGREE	B1-1 DEGREE	B1-2 DEGREE	V1-1 FT/SEC	V1-2 FT/SEC	V0-1 FT/SEC	V0-2 FT/SEC	U-1 FT/SEC	U-2 FT/SEC
5	7.467	19.769	220.4	533.5	220.8	347.0	0	405.2	0	49.42	62.44	11.96	477.1	354.8	-422.9	-73.5	422.9	478.7
10	18.467	20.408	225.4	511.3	225.4	340.5	0	391.4	0	48.23	63.25	18.31	500.7	359.1	-447.1	-112.7	447.1	494.1
15	19.467	21.047	229.4	486.4	229.4	329.9	0	357.4	0	47.28	64.05	24.75	524.2	363.9	-471.4	-152.2	471.4	509.6
30	22.314	22.964	236.4	432.6	236.4	297.3	0	314.2	0	46.58	66.36	32.03	540.3	368.8	-540.3	-241.8	540.3	556.0
50	25.791	25.520	236.9	391.7	236.9	276.1	0	277.8	0	45.17	69.22	50.88	667.9	438.4	-624.5	-340.1	624.5	617.9
70	28.958	28.078	231.1	372.5	231.1	257.1	0	263.5	0	46.55	71.75	57.92	735.2	484.2	-701.1	-410.3	701.1	675.8
86	31.295	29.993	224.0	371.5	224.0	238.6	0	249.5	0	50.02	73.53	61.62	790.2	502.0	-757.7	-441.7	757.7	726.2
90	31.883	30.630	222.1	370.2	222.1	233.4	0	247.4	0	50.92	73.95	62.81	803.3	510.7	-772.0	-454.3	772.0	741.6
96	32.499	31.271	220.1	360.0	220.1	216.2	0	287.8	0	53.08	74.37	65.26	817.1	516.8	-786.9	-469.4	786.9	757.2

SPAN	INCS	INCM	DEV	TURN	CAMBER	OMEGA-B	D-FAC	OMEGA-E	LOSS-P	PO2	EFF-AD	EFF-P	M-1	M-2	M-1	M-2	M-1	M-2
5	7.05	13.48	10.09	50.48	47.12	0.000	4.545	0.026	0.026	1.2336	0.930	0.928	1.992	0.4730	0.4325	0.3151	0.3151	
10	7.29	13.61	8.68	44.94	39.99	0.000	4.659	0.218	0.048	1.2247	0.962	0.958	2.040	0.4537	0.4279	0.3186	0.3186	
15	7.59	13.75	8.14	39.30	34.03	0.000	4.761	0.361	0.043	1.2134	0.9732	0.9724	2.076	0.4312	0.4111	0.3226	0.3226	
30	8.60	12.47	9.27	27.33	24.13	0.000	4.958	0.909	0.190	1.1913	0.9168	0.9146	1.868	0.2131	0.3455	0.5410	0.3393	
50	9.71	12.30	8.68	18.34	14.70	0.000	4.698	1.126	0.217	1.1768	0.8673	0.8640	1.877	0.2127	0.3455	0.6077	0.3667	
70	10.28	11.07	7.46	13.83	9.20	0.000	4.855	1.250	0.240	1.1718	0.7924	0.7874	1.754	0.2074	0.3277	0.6674	0.4859	
86	10.19	11.44	7.51	11.91	8.02	0.000	4.923	1.201	0.362	1.1747	0.7163	0.7095	1.652	0.2018	0.3254	0.7080	0.4400	
90	10.12	11.21	7.62	11.14	7.63	0.000	4.935	1.234	0.376	1.1757	0.6988	0.6916	1.622	0.2022	0.3241	0.7209	0.4471	
96	10.16	11.08	9.39	9.11	7.44	0.000	4.972	1.202	0.377	1.1727	0.6732	0.6655	1.604	0.2018	0.3148	0.7334	0.4519	

T0/T0 PO/PO EFF-AD EFF-P
INLET INLET INLET INLET
1.0596 1.1872 84.32 84.72

STATOR

SPAN IN	DIA-1 IN	DIA-2 IN	V-1 FT/SEC	V-2 FT/SEC	VM-1 FT/SEC	VM-2 FT/SEC	V0-1 FT/SEC	V0-2 FT/SEC	B-1 DEGREE	B-2 DEGREE	B1-1 DEGREE	B1-2 DEGREE	V1-1 FT/SEC	V1-2 FT/SEC	V0-1 FT/SEC	V0-2 FT/SEC	U-1 FT/SEC	U-2 FT/SEC
5	20.409	21.489	553.1	444.3	369.7	444.2	392.5	10.6	45.20	1.36	14.63	48.93	402.7	676.1	-101.7	-509.8	474.2	520.3
10	21.008	21.961	530.8	422.5	360.2	422.4	370.4	-5.7	44.24	-1.79	19.98	51.83	404.9	683.7	-138.2	-537.4	508.7	543.1
15	21.589	22.432	506.5	405.1	367.7	405.0	348.2	-10.8	43.43	-1.53	25.33	53.83	407.5	686.3	-174.5	-554.0	522.7	543.1
30	23.314	23.902	455.1	369.7	333.7	369.6	309.4	-10.3	42.83	-1.59	37.34	57.88	420.5	695.5	-255.1	-589.0	564.5	578.7
50	25.801	25.693	418.3	335.6	313.0	336.4	277.0	-12.0	41.51	-2.05	47.57	62.23	464.5	722.2	-342.9	-639.0	619.9	626.9
70	27.818	27.902	415.6	316.5	300.5	316.3	272.4	-9.3	42.83	-1.74	53.18	65.22	501.0	754.7	-400.8	-685.2	673.6	675.6
86	29.408	29.382	412.6	304.5	292.4	304.4	291.1	6.9	44.87	1.29	55.22	66.63	512.5	767.5	-421.0	-704.6	712.1	711.4
90	29.914	29.855	413.2	301.1	290.0	301.0	295.2	6.8	45.50	1.29	55.95	67.20	518.0	776.8	-429.1	-716.1	724.3	722.9
96	30.382	30.293	408.7	291.5	281.3	291.4	296.5	6.6	46.51	1.30	57.36	68.15	521.5	783.1	-439.1	-726.9	735.6	733.5

SPAN	INCS	INCM	DEV	TURN	CAMBER	OMEGA-B	D-FAC	OMEGA-E	LOSS-P	PO2	EFF-AD	EFF-P	M-1	M-2	M-1	M-2	M-1	M-2
5	-89	2.03	13.7	43.84	55.90	0.000	3.637	11.80	0.291	0.294	0.919	0.000	0.000	0.000	4.868	3.920	3.570	5.965
10	-1.13	1.81	10.66	45.03	53.87	0.000	3.810	12.95	0.330	0.310	0.987	0.000	0.000	0.000	4.652	3.726	3.603	6.030
15	-95	1.99	9.44	44.96	52.51	0.000	3.821	11.42	0.299	0.299	0.952	0.000	0.000	0.000	4.457	3.572	3.623	6.051
30	.41	3.41	9.63	44.83	50.67	0.000	3.823	9.67	0.184	0.184	0.930	0.000	0.000	0.000	4.256	3.256	3.735	6.125
50	.82	3.95	9.93	43.55	49.61	0.000	4.055	8.78	0.146	0.146	0.957	0.000	0.000	0.000	4.068	2.960	4.108	6.351
70	2.56	5.74	11.75	43.97	49.92	0.000	4.406	6.65	0.065	0.065	0.941	0.000	0.000	0.000	3.577	2.775	4.415	6.619
86	5.45	4.76	17.22	43.58	52.01	0.000	5.029	4.04	0.484	0.484	0.880	0.000	0.000	0.000	3.624	2.59	4.501	6.703
90	5.97	9.29	14.89	44.21	53.54	0.000	5.203	3.38	0.546	0.546	0.866	0.000	0.000	0.000	3.631	2.927	4.547	6.777
96	6.81	10.18	20.97	45.21	56.80	0.000	5.529	1.69	0.594	0.594	0.863	0.000	0.000	0.000	3.586	2.540	4.568	6.824

RCOR-1 #CGM-1 T0/T0 PO/PC EFF-AD EFF-P *C/A-1
INLET INLET INLET INLET INLET
RPM LBM/SEC LBM/SEC
5549 75.64 1.0596 1.1754 79.74 80.22 16.99

TABLE 8.1
Blade-Element and Overall Performance with Uniform Inlet
70% of Design Speed

ROTOR:

%SPAN	DIA-1 IN.	DIA-2 IN.	V-1 FL/SEC	V-2 FL/SEC	VM-1 FL/SEC	VM-2 FL/SEC	V0-1 FL/SEC	V0-2 FL/SEC	B-1 DEGREE	B-2 DEGREE	B1-1 DEGREE	B1-2 DEGREE	V1-1 FL/SEC	V1-2 FL/SEC	V01-1 FL/SEC	V01-2 FL/SEC	U-1 FL/SEC	U-2 FL/SEC
5	17.467	19.769	410.6	799.3	410.6	801.2	515.4	.00	40.27	55.24	14.10	720.3	628.9	591.8	153.2	591.8	669.8	
10	16.467	20.408	419.8	757.6	419.8	839.6	481.4	.00	40.04	56.14	14.38	753.5	615.3	625.7	204.0	625.7	691.4	
15	15.467	21.047	427.9	721.5	427.9	878.0	453.0	.00	38.88	57.02	14.66	786.2	619.4	659.6	412.3	659.6	713.1	
30	22.314	22.984	444.8	653.0	444.8	907.6	440.4	.00	34.05	59.53	17.26	877.2	680.7	756.0	412.3	756.0	778.0	
50	25.791	25.520	451.9	599.4	451.9	937.2	429.4	.00	28.97	62.65	17.79	983.8	777.9	873.5	412.3	873.5	864.6	
70	28.954	28.074	443.7	552.4	443.7	966.8	424.4	.00	24.24	65.44	18.48	1074.1	868.5	981.0	412.3	981.0	981.0	
85	31.295	29.993	428.7	521.2	428.7	996.4	420.4	.00	26.26	67.98	19.25	1183.7	914.4	1060.3	412.3	1060.3	1016.2	
90	31.883	30.630	424.3	483.1	424.3	1026.0	423.4	.00	23.44	68.55	19.28	1180.6	911.2	1080.2	412.3	1080.2	1037.8	
96	32.449	31.271	420.9	448.6	420.9	1055.6	423.4	.00	23.44	69.08	19.28	1178.6	896.4	1101.1	412.3	1101.1	1057.5	

%SPAN	INCS	INCM	DEV	TURN	CAMBER	OMEGA-R	LOSS-P	PO2	EFF-P	EFF-AD	EFF-F	M-1	M-2	M1-1	M1-2	M2-1	M2-2
5	-14	6.29	12.23	41.14	47.12	0.000	.2942	.0554	.0118	1.4264	.9632	.9613	.6935	.3739	.7124	.6579	.5608
10	-18	6.53	9.75	36.76	39.99	0.000	.3397	.1164	.0253	1.3893	.9146	.9105	.8039	.3034	.6731	.6226	.5466
15	-15	6.32	8.29	32.21	34.03	0.000	.3559	.1321	.0280	1.3599	.8906	.8857	.7835	.3010	.6398	.6241	.5492
30	1.68	5.53	7.54	22.27	24.14	0.000	.3379	.0982	.0211	1.3120	.8844	.8825	.6058	.5783	.8071	.9015	.6888
50	3.12	5.74	5.31	15.08	14.68	0.000	.2988	.0674	.0140	1.2753	.8940	.8903	.4112	.5307	.9015	.9015	.6888
70	4.23	6.02	4.17	11.00	9.15	0.000	.2684	.0430	.0139	1.2424	.8607	.8654	.4023	.4936	.9837	.9837	.7485
85	4.63	5.86	5.16	8.73	8.04	0.055	.2717	.1152	.0203	1.2110	.7544	.7477	.7081	.3898	.4596	1.0390	.8063
90	4.75	5.80	7.22	6.27	7.69	0.063	.2864	.2619	.0266	1.1854	.6739	.6453	.6224	.3853	.4244	1.0559	.8004
96	4.88	5.78	11.36	1.90	7.48	0.074	.3123	.2640	.0314	1.1480	.4863	.4655	.5313	.3823	.3656	1.0715	.7830

TO/TO PO/PO EFF-AD EFF-P
INLET INLET INLET INLET

1.0856 1.2788 85.09 84.63

STATOR

%SPAN	DIA-1 IN.	DIA-2 IN.	V-1 FL/SEC	V-2 FL/SEC	VM-1 FL/SEC	VM-2 FL/SEC	V0-1 FL/SEC	V0-2 FL/SEC	B-1 DEGREE	B-2 DEGREE	B1-1 DEGREE	B1-2 DEGREE	V1-1 FL/SEC	V1-2 FL/SEC	V01-1 FL/SEC	V01-2 FL/SEC	U-1 FL/SEC	U-2 FL/SEC
5	20.409	21.669	860.8	853.2	700.3	851.6	500.4	-53.3	35.55	-3.58	15.26	42.54	725.9	1155.7	-191.0	-781.4	691.5	728.1
10	21.008	21.961	820.0	826.9	694.4	825.2	473.7	-53.3	35.28	-3.70	19.58	44.03	710.8	1147.6	-238.1	-797.3	711.8	744.1
15	21.589	22.432	785.5	801.1	649.7	795.1	441.4	-56.3	34.18	-4.03	24.04	45.61	712.0	1142.5	-290.0	-816.3	731.4	760.0
30	23.314	23.902	720.9	740.1	624.5	737.7	359.9	-59.5	29.94	-4.61	34.51	49.58	758.7	1140.3	-430.0	-869.3	789.9	809.8
50	25.601	25.893	673.2	687.7	607.4	694.5	289.2	-54.6	25.44	-4.80	43.54	53.85	839.2	1157.0	-578.2	-931.9	867.4	877.3
70	27.818	28.902	646.4	639.2	587.2	637.8	245.4	-52.5	22.29	-4.70	49.39	57.45	837.6	1183.8	-687.4	-987.9	942.5	945.3
85	29.408	29.382	631.9	591.8	586.6	591.8	203.6	-20.3	21.84	-1.95	52.39	59.79	961.2	1175.4	-761.4	-1013.7	946.4	995.1
90	29.916	29.856	608.6	564.1	560.5	564.1	151.3	-4	22.94	-1.01	54.18	60.88	957.7	1158.6	-776.5	-1012.0	1013.5	1011.1
96	30.382	30.293	565.7	506.9	512.2	505.6	96.6	31.7	25.11	3.59	57.02	63.04	940.9	1115.9	-789.3	-904.6	1029.4	1026.3

%SPAN	INCS	INCM	DEV	TURN	CAMBER	OMEGA-R	LOSS-P	PO2	EFF-P	EFF-AD	EFF-F	M-1	M-2	M1-1	M1-2	M2-1	M2-2	
5	-10.34	-7.41	8.63	39.13	55.90	0.000	.1654	.1000	.0337	1.3577	.9661	.9600	.0000	-3.7234	.7618	.7663	.6489	1.0380
10	-10.05	-7.12	7.75	38.97	53.87	0.000	.1527	.0940	.0346	1.3407	.9581	.9550	.0000	2.4967	.7254	.7417	.6387	1.0292
15	-10.46	-7.53	6.97	38.21	52.49	0.000	.1434	.0860	.0350	1.3246	.9483	.9400	.0000	1.6041	.6547	.7177	.6396	1.0235
30	-12.79	-9.78	6.61	34.55	50.68	0.000	.1352	.0627	.0376	.9848	.9400	.9400	.0000	1.6241	.6388	.6520	.6230	1.0200
50	-15.40	-12.26	7.49	29.99	49.80	0.000	.1342	.0772	.0236	.9833	.9833	.9833	.0000	2.1856	.5985	.6146	.7534	1.0340
70	-17.40	-14.16	8.78	27.00	49.92	0.000	.1636	.1046	.0346	.9788	.9788	.9788	.0000	-3.4432	.5757	.5703	.8223	1.0557
85	-17.54	-14.23	13.94	23.79	52.01	0.000	.2048	.1446	.0505	.9720	.9720	.9720	.0000	-0.0432	.5616	.5250	.4559	1.0427
90	-16.52	-13.19	17.39	22.95	53.57	0.000	.2120	.1318	.0469	.9762	.9762	.9762	.0000	.0000	.5395	.4987	.8498	1.0243
96	-14.61	-11.24	23.26	21.53	56.04	0.000	.2371	.1597	.0575	.9750	.9750	.9750	.0000	.2601	.5000	.4455	.8308	.9809

NCOR-1 NCOR-1 TO/TO PO/PO EFF-AD EFF-P WC/A-1
INLET INLET INLET INLET INLET INLET
RPM LBW/SEC
7765 135.56 1.0856 1.2554 78.50 79.16 30.46

TABLE 8.2
Blade-Element and Overall Performance with Uniform Inlet
70% of Design Speed

ROTOR

SPAN IN	DIA-1 IN	DIA-2 IN	V-1 FT/SEC	V-2 FT/SEC	VH-1 FT/SEC	VH-2 FT/SEC	VO-1 FT/SEC	VO-2 FT/SEC	B-1 DEGREE	B-2 DEGREE	B-1 DEGREE	B-2 DEGREE	B-1 DEGREE	B-2 DEGREE	B-1 DEGREE	B-2 DEGREE	V-1 FT/SEC	V-2 FT/SEC	VO-1 FT/SEC	VO-2 FT/SEC	U-1 FT/SEC	U-2 FT/SEC	
5	17.837	19.769	384.7	787.4	384.7	500.5	.0	332.0	.00	42.30	56.27	13.29	710.8	586.5	-591.1	-137.1	591.1	689.1					
10	18.467	20.408	403.4	840.1	403.4	547.0	.0	498.5	.00	42.34	57.16	19.38	743.9	580.4	-625.0	-192.2	625.0	690.7					
15	19.487	21.487	411.0	898.1	411.0	521.1	.0	461.0	.00	37.53	50.04	25.74	658.0	578.3	-650.8	-251.3	650.8	712.3					
20	22.314	22.964	426.9	936.8	426.9	506.8	.0	385.8	.00	31.28	60.52	37.64	667.5	640.7	-755.2	-391.4	755.2	777.2					
30	29.791	25.520	433.7	983.5	433.7	468.4	.0	318.9	.00	33.13	63.57	48.08	674.7	735.0	-872.9	-544.8	872.9	863.7					
40	40.934	28.076	425.8	942.8	425.8	469.5	.0	276.5	.00	30.59	66.46	55.12	668.8	821.3	-979.9	-673.7	979.9	930.2					
50	51.293	29.993	413.4	913.4	413.4	440.9	.0	266.8	.00	31.19	68.67	59.89	654.9	888.8	-1039.1	-768.3	1039.1	1013.1					
60	61.003	30.630	409.5	891.1	409.5	407.1	.0	274.6	.00	34.02	69.22	61.89	615.4	868.0	-1079.0	-762.0	1079.0	1036.6					
70	70.899	31.271	406.0	855.2	406.0	359.4	.0	279.3	.00	37.86	69.74	65.23	617.4	857.9	-1099.9	-775.0	1099.9	1058.3					
80																							
90																							
95																							

SPAN	INCS DEGREE	INCX DEGREE	DEV DEGREE	TURN DEGREE	CAMBER DEGREE	OMEGA-B	D-FAC	OMEGA-B	LOSS-P TOTAL	OMEGA-B	LOSS-P PROFILE	PO2/ PO1	EFF-AD TOTAL	EFF-P	M-1	M-2	M-1	M-2
5	1.20	7.32	11.42	42.90	47.12	.0000	.3354	.0237	.0051	.0051	1.44518	.9883	.9837	.9594	.3590	.7000	.6888	.3303
10	1.20	7.55	9.75	37.78	39.99	.0000	.3616	.0907	.0197	1.4099	.9363	.9332	.9332	.8655	.3661	.6555	.8434	.5140
15	1.55	7.34	9.21	32.30	34.03	.0000	.4035	.1221	.0264	1.3723	.9027	.8962	.8230	.3751	.6140	.7145	.5109	
20	2.46	6.62	7.92	22.88	24.19	.0000	.3830	.0899	.0192	1.3375	.9057	.9006	.8551	.3486	.5616	.7484	.5650	
30	4.02	6.65	5.81	15.30	14.67	.0000	.3482	.0729	.0149	1.3048	.8974	.8934	.8640	.3442	.5140	.8908	.6447	
40	5.91	6.51	5.37	11.35	9.12	.0000	.3177	.0775	.0150	1.2783	.8668	.8622	.8562	.3474	.4793	.8736	.7224	
50	5.31	6.56	5.37	9.16	8.01	.0065	.3192	.1123	.0216	1.2577	.8668	.8622	.8562	.3474	.4793	.8736	.7224	
60	5.47	6.46	6.77	7.33	7.64	.0072	.3373	.1628	.0263	1.2414	.7853	.6973	.6731	.3718	.4287	1.0471	.7542	
70	5.53	6.44	9.30	4.51	7.45	.0069	.3559	.2084	.0328	1.2197	.6257	.6150	.6082	.3685	.3957	1.0633	.7458	

STATOR

SPAN IN	DIA-1 IN	DIA-2 IN	V-1 FT/SEC	V-2 FT/SEC	VH-1 FT/SEC	VH-2 FT/SEC	VO-1 FT/SEC	VO-2 FT/SEC	B-1 DEGREE	B-2 DEGREE	B-1 DEGREE	B-2 DEGREE	B-1 DEGREE	B-2 DEGREE	B-1 DEGREE	B-2 DEGREE	V-1 FT/SEC	V-2 FT/SEC	VO-1 FT/SEC	VO-2 FT/SEC	U-1 FT/SEC	U-2 FT/SEC
5	20.408	21.961	839.3	736.6	682.5	724.4	515.3	840.4	-11.7	37.87	14.83	48.87	6.33	1050.0	-175.4	-769.0	690.7	727.3				
10	21.509	22.432	750.1	712.7	600.7	711.5	489.1	40.6	36.77	3.27	25.06	48.35	683.9	1070.6	-281.5	-789.8	730.7	759.2				
15	23.314	23.902	695.2	662.3	582.3	660.6	379.6	48.4	33.09	4.19	35.07	52.38	712.3	1002.9	-409.4	-857.3	780.0	808.9				
20	25.601	25.893	648.5	616.5	565.4	614.6	317.6	47.7	29.32	4.44	34.44	56.36	788.2	1109.5	-548.8	-924.8	866.4	876.3				
30	27.618	27.902	624.2	576.7	558.3	575.0	279.1	44.0	26.57	4.37	49.87	59.81	866.3	1143.5	-662.3	-966.3	941.5	944.3				
40	29.408	29.382	614.6	541.7	550.7	540.7	272.8	32.5	26.34	3.44	32.69	62.23	908.4	1140.6	-722.5	-1026.9	1043.7	1048.7				
50	29.914	29.856	500.9	519.2	530.7	518.5	262.0	-31.0	27.99	-3.44	54.00	63.54	902.9	1163.3	-730.4	-1061.4	1114.8	1124.8				
60	30.382	30.293	579.0	482.8	503.5	482.0	287.8	-28.4	29.75	-3.57	55.79	65.42	895.4	1158.6	-740.5	-1053.6	1022.7	1031.2				

SPAN	INCS DEGREE	INCX DEGREE	DEV DEGREE	TURN DEGREE	CAMBER DEGREE	OMEGA-B	D-FAC	OMEGA-B	LOSS-P TOTAL	OMEGA-B	LOSS-P PROFILE	PO2/ PO1	EFF-AD TOTAL	EFF-P	M-1	M-2	M-1	M-2
5	-7.92	-5.00	9.32	40.17	55.90	.0000	.2388	.0969	.0241	.0241	.9497	.9697	.0000	.0000	.7382	.6865	.6083	.9673
10	-7.58	-4.64	8.28	40.82	53.88	.0000	.2336	.0716	.0183	.0383	.9747	.9747	.0000	.0000	.6272	.6904	.6552	.9546
15	-7.89	-4.95	7.74	40.04	52.50	.0000	.2197	.0307	.0050	.0863	.9921	.9921	.0000	.0000	.8486	.8603	.6312	.9482
20	-8.55	-6.54	7.03	37.28	50.68	.0000	.2144	.0328	.0092	.0992	.9925	.9925	.0000	.0000	.7690	.8127	.5659	.9376
30	-11.48	-9.34	7.41	33.76	49.60	.0000	.2212	.0334	.0102	.1020	.9933	.9933	.0000	.0000	.7248	.8448	.7032	.9874
40	-13.09	-9.85	9.11	30.94	48.90	.0000	.2475	.0462	.0163	.0862	.9904	.9904	.0000	.0000	.6933	.8524	.5086	.7690
50	-12.95	-9.64	12.46	29.80	52.01	.0000	.2943	.0715	.0247	.0471	.9871	.9871	.0000	.0000	.7011	.8424	.8756	.8025
60	-11.45	-8.12	13.98	31.41	53.55	.0000	.3212	.0704	.0250	.0470	.9878	.9878	.0000	.0000	.7456	.8532	.8532	.7950
70	-9.98	-6.62	16.32	33.12	56.02	.0000	.3643	.0908	.0327	.0327	.9853	.9853	.0000	.0000	.7344	.8205	.8205	.7461

MCOR-1 MCOR-1
INLET INLET
RPM 7756 131.14 1.0934 1.2497 83.28 83.69
LBM/SEC 50FT 29.53

TABLE 8.6
Blade-Element and Overall Performance with Uniform Inlet
70% of Design Speed

ROTOR

%SPAN	IN	DIR-1	DIR-2	V-1	V-2	VM-1	VM-2	B-1		B-2		P-1	P-2	V-1-1	V-1-2	V-2-1	V-2-2	U-1	U-2
								FT/SEC	DEGREE	FT/SEC	DEGREE								
5	17.467	19.769	331.9	744.4	331.9	498.0	0	542.1	0.00	49.03	60.71	12.44	678.5	499.4	-591.7	-107.6	591.7	669.7	669.7
10	18.467	20.498	339.2	712.8	339.2	473.9	0	530.5	0.00	48.11	61.53	15.66	711.6	502.8	-625.6	-160.7	625.6	691.3	691.3
15	18.467	21.047	345.5	677.9	345.5	457.9	0	500.0	0.00	47.52	63.35	20.94	744.5	505.7	-659.5	-213.0	659.5	713.0	713.0
30	22.314	22.964	356.3	605.2	356.3	411.3	0	443.9	0.00	47.18	64.72	30.99	835.9	530.6	-755.0	-334.0	755.9	777.9	777.9
50	27.991	25.380	358.6	553.0	358.6	388.0	0	387.0	0.00	46.88	67.68	40.45	944.5	805.9	-873.7	-487.5	873.7	868.5	868.5
70	23.954	28.076	350.3	534.2	350.3	370.6	0	394.5	0.00	46.06	67.04	56.80	1041.5	677.1	-980.4	-566.6	980.8	951.1	951.1
85	31.295	29.993	339.0	529.1	339.0	332.5	0	411.6	0.00	51.08	72.27	61.18	1113.0	689.8	-1060.1	-604.4	1067.1	1016.0	1016.0
90	31.883	30.630	335.9	525.7	335.9	322.3	0	415.2	0.00	52.18	72.72	62.62	1121.1	700.9	-1080.1	-622.4	1080.1	1037.6	1037.6
96	32.499	31.271	333.0	511.5	333.0	300.2	0	414.2	0.00	54.07	73.17	65.05	1150.2	711.8	-1100.9	-645.1	1100.9	1059.3	1059.3

%SPAN	IN	DIR-1	DIR-2	VM-1	VM-2	B-1	B-2	P-1	P-2	TOTAL PROFILE		STAT	TOTAL	V-1-1	V-1-2	V-2-1	V-2-2	U-1	U-2
										LOSS-P	LOSS-B								
6	9.38	11.75	10.56	48.27	47.12	0.000	0.000	0.566	-0.043	1.4949	1.0068	1.0072	1.0169	0.3010	0.3010	0.5562	0.5562	0.6180	0.4906
10	5.87	11.90	9.03	42.89	39.99	0.000	0.000	0.736	0.060	1.4739	0.9956	0.9954	0.9918	0.3087	0.3087	0.5271	0.5271	0.6538	0.4424
15	5.89	11.56	8.34	37.41	34.03	0.009	0.009	0.885	0.330	1.4483	0.9771	0.9759	0.9586	0.3185	0.3185	0.5952	0.5952	0.6864	0.4480
30	6.95	10.54	7.25	25.73	24.14	0.000	0.000	1.047	0.947	1.4015	0.9177	0.9137	0.8790	0.3284	0.3284	0.5285	0.5285	0.7701	0.4683
50	8.16	10.76	6.25	17.80	14.99	0.000	0.000	1.193	1.193	1.3749	0.8705	0.8645	0.8108	0.3248	0.3248	0.4804	0.4804	0.6330	0.5288
70	8.88	10.67	6.35	13.54	9.19	0.000	0.000	1.562	0.289	1.3704	0.8022	0.7641	0.7064	0.3162	0.3162	0.4621	0.4621	0.5453	0.5453
85	8.92	10.17	7.08	11.08	8.03	0.143	0.143	2.325	0.406	1.3732	0.7191	0.7064	0.6503	0.3064	0.3064	0.4541	0.4541	0.6033	0.5970
90	8.89	9.97	7.51	10.10	7.64	0.149	0.149	2.485	0.422	1.3739	0.7004	0.6868	0.6409	0.3039	0.3039	0.4502	0.4502	0.6003	0.6003
96	8.96	9.97	8.13	7.44	0.159	0.159	2.643	0.419	0.392	1.3675	0.6783	0.6639	0.6223	0.3011	0.3011	0.4371	0.4371	0.6078	0.6080

TO-TO TO-TO
INLET INLET

1.1186 1.3970 84.54 95.25

STATOR

%SPAN	IN	DIR-1	DIR-2	VM-1	VM-2	B-1	B-2	P-1	P-2	TOTAL PROFILE		STAT	TOTAL	V-1-1	V-1-2	V-2-1	V-2-2	U-1	U-2
										LOSS-P	LOSS-B								
5	20.409	21.499	773.7	604.3	549.7	504.2	544.4	-28.0	44.72	-2.166	14.97	51.37	569.0	967.4	-146.0	-746.0	691.4	726.0	726.0
10	21.008	21.961	742.2	575.3	533.9	574.6	515.5	-27.9	43.99	-2.778	20.17	53.33	569.3	962.3	-196.1	-771.9	711.7	744.0	744.0
15	21.589	22.432	708.2	551.0	513.9	550.3	487.3	-26.8	43.47	-2.780	25.40	55.03	569.5	960.2	-244.1	-786.8	731.5	759.9	759.9
30	23.314	23.902	639.1	503.2	466.1	503.4	437.2	-23.8	43.16	-2.71	37.05	58.87	568.1	973.9	-352.6	-833.5	789.8	809.7	809.7
50	25.601	25.895	602.8	480.0	421.2	497.9	395.9	-20.9	41.90	-2.50	46.86	62.89	585.8	1008.8	-471.4	-848.0	867.5	877.2	877.2
70	27.818	27.902	581.1	443.9	435.7	443.5	399.4	-16.7	41.76	-2.15	51.78	65.25	704.3	1059.2	-553.3	-941.9	942.4	945.2	945.2
85	29.409	29.382	591.6	431.6	415.8	431.4	420.9	12.4	45.34	1.65	54.15	66.30	707.9	1073.5	-575.4	-942.9	996.2	995.3	995.3
90	29.914	29.856	592.2	424.4	411.3	424.1	426.1	14.5	46.02	1.96	55.00	66.95	717.0	1083.4	-587.3	-996.9	1013.4	1011.4	1011.4
96	30.382	30.293	585.1	411.5	400.4	426.4	434.8	13.4	46.81	4.72	56.40	67.55	723.5	1073.8	-602.6	-942.4	1029.2	1026.2	1026.2

%SPAN	IN	DIR-1	DIR-2	VM-1	VM-2	B-1	B-2	P-1	P-2	TOTAL PROFILE		STAT	TOTAL	V-1-1	V-1-2	V-2-1	V-2-2	U-1	U-2
										LOSS-P	LOSS-B								
6	1.33	1.60	9.75	47.34	55.90	0.000	0.000	0.979	1.246	0.309	0.9665	0.000	0.000	0.7282	0.7282	0.6767	0.6767	0.5008	0.4911
10	-1.28	1.65	8.67	46.77	53.87	0.000	0.000	1.300	0.831	0.331	0.9674	0.000	0.000	0.7408	0.7408	0.6459	0.6459	0.5020	0.5058
15	-0.86	2.08	8.22	46.27	52.51	0.000	0.000	1.408	0.486	0.291	0.9743	0.000	0.000	0.7110	0.7110	0.6184	0.6184	0.5017	0.5033
30	0.74	3.74	8.51	45.07	50.57	0.000	0.000	4.117	0.561	0.163	0.9889	0.000	0.000	0.8651	0.8651	0.5579	0.5579	0.5141	0.5141
50	1.21	4.33	7.88	44.50	49.21	0.000	0.000	4.582	0.931	0.156	0.9915	0.000	0.000	0.8807	0.8807	0.5170	0.5170	0.5640	0.5640
70	2.02	5.25	11.33	43.91	49.21	0.000	0.000	4.687	1.214	0.214	0.9896	0.000	0.000	0.8702	0.8702	0.5074	0.5074	0.6118	0.6118
85	5.89	9.19	17.55	43.70	52.02	0.000	0.000	4.187	1.687	0.380	0.9823	0.000	0.000	0.7961	0.7961	0.5102	0.5102	0.6799	0.6799
90	6.45	9.78	19.35	44.05	53.55	0.000	0.000	4.265	1.265	0.449	0.9794	0.000	0.000	0.7685	0.7685	0.5105	0.5105	0.6609	0.6609
96	7.12	10.45	24.41	42.10	56.71	0.000	0.000	4.391	1.391	0.495	0.9786	0.000	0.000	0.7577	0.7577	0.5034	0.5034	0.6211	0.6211

NEOR-1 TOR-1 TOR-1 TOR-1 TOR-1 TOR-1 TOR-1 TOR-1 TOR-1 TOR-1

INLET INLET INLET INLET INLET INLET INLET INLET INLET INLET

4PM LBM/SEC 7764 11.19 1.1186 1.3753 80.39 81.25

MC/AT LBN/SEC 24.99

TABLE 9.2

Blade-Element and Overall Performance with Uniform Inlet
90% of Design Speed

ROTOR

%SPAN	DIA-1 IN	DIA-2 IN	V-1 FI/SEC	V-2 FI/SEC	VM-1 FI/SEC	VM-2 FI/SEC	VO-1 FI/SEC	VO-2 FI/SEC	B-1 DEGREE	B-2 DEGREE	B1-1 DEGREE	B1-2 DEGREE	V1-1 FT/SEC	V1-2 FT/SEC	V0-1 FT/SEC	V0-2 FT/SEC	U-1 FT/SEC	U-2 FT/SEC	EFF-P				
																			PO1	PO2	EFF-AD	EFF-P	
INCS																			TOTAL				
DEGREE		INCH		TURN		CAMBER		OMEGA-B		D-FAC		OMEGA-B		LOSS-P		LOSS-P		TOTAL		EFF-P			
5	17.467	19.769	523.5	655.0	523.5	663.2	0.0	687.1	0.0	46.02	55.47	14.70	923.5	685.7	-760.8	-174.0	760.8	861.9	6012	8373	4942	7965	5971
10	18.467	20.408	536.5	612.0	536.5	640.1	0.0	649.7	0.0	45.43	56.30	20.51	966.9	683.7	-804.4	-239.3	804.4	889.9	6012	8373	4942	7965	5971
15	19.467	21.047	548.1	852.6	548.1	598.7	0.0	606.9	0.0	45.38	57.12	27.33	1009.7	674.7	-847.9	-309.9	847.9	916.8	6012	8373	4942	7965	5971
30	22.314	22.964	572.1	769.9	572.1	560.6	0.0	527.5	0.0	43.25	59.52	40.10	1127.8	733.7	-972.0	-472.7	972.0	1000.3	6012	8373	4942	7965	5971
50	25.791	25.076	583.5	728.7	583.5	547.8	0.0	480.5	0.0	41.82	62.85	49.03	1265.9	835.8	-1123.4	-631.1	1123.4	1111.6	6012	8373	4942	7965	5971
70	28.954	28.076	576.2	687.9	576.2	522.9	0.0	439.0	0.0	39.68	63.49	55.25	1384.6	946.1	-1261.2	-783.9	1261.2	1222.9	6012	8373	4942	7965	5971
85	31.295	29.963	559.3	675.7	559.3	517.2	0.0	434.8	0.0	40.05	67.69	59.31	1473.4	1013.8	-1363.1	-871.7	1363.1	1306.8	6012	8373	4942	7965	5971
90	31.883	30.630	553.8	661.5	553.8	491.9	0.0	442.0	0.0	41.95	68.26	61.13	1495.1	1018.8	-1388.8	-892.2	1388.8	1324.2	6012	8373	4942	7965	5971
95	32.499	31.271	548.2	627.1	548.2	438.8	0.0	448.1	0.0	45.60	68.83	64.36	1518.0	1013.9	-1415.6	-914.0	1415.6	1362.1	6012	8373	4942	7965	5971

STATOR

%SPAN	DIA-1 IN	DIA-2 IN	V-1 FI/SEC	V-2 FI/SEC	VM-1 FI/SEC	VM-2 FI/SEC	VO-1 FI/SEC	VO-2 FI/SEC	B-1 DEGREE	B-2 DEGREE	B1-1 DEGREE	B1-2 DEGREE	V1-1 FT/SEC	V1-2 FT/SEC	V0-1 FT/SEC	V0-2 FT/SEC	U-1 FT/SEC	U-2 FT/SEC	EFF-P				
																			PO1	PO2	EFF-AD	EFF-P	
INCS																			TOTAL				
DEGREE		INCH		TURN		CAMBER		OMEGA-B		D-FAC		OMEGA-B		LOSS-P		LOSS-P		TOTAL		EFF-P			
5	20.409	21.809	1009.6	818.1	759.1	818.1	665.6	1.2	41.25	50	16.40	48.63	791.3	1237.8	-223.4	-928.8	889.0	936.0	6012	8373	4942	7965	5971
10	21.008	21.961	968.2	779.7	734.4	779.7	630.9	-21.2	40.67	-1.58	21.16	51.44	778.7	1250.7	-284.1	-977.8	915.1	956.6	6012	8373	4942	7965	5971
15	21.589	22.532	912.4	750.5	694.9	749.7	591.3	-35.6	40.39	-2.72	26.66	53.49	778.1	1260.1	-349.1	-1012.7	940.4	977.1	6012	8373	4942	7965	5971
30	23.314	23.902	837.4	707.9	656.7	707.0	519.0	-36.4	38.35	-2.95	37.03	56.73	823.2	1288.9	-495.9	-1071.5	1012.5	1041.1	6012	8373	4942	7965	5971
50	25.601	25.893	805.9	682.1	648.0	681.6	479.1	-25.8	36.47	-2.17	44.45	59.42	908.1	1340.1	-636.0	-1153.7	1112.5	1127.8	6012	8373	4942	7965	5971
70	27.818	27.902	784.7	658.7	627.5	658.3	443.4	-22.2	34.40	-1.94	49.88	62.14	1004.7	1399.9	-768.5	-1237.6	1211.7	1215.4	6012	8373	4942	7965	5971
85	29.908	29.382	795.7	633.4	660.0	633.3	444.5	9.0	33.86	1.82	51.72	63.51	1065.4	1419.8	-848.4	-1277.6	1303.0	1300.5	6012	8373	4942	7965	5971
90	29.914	29.856	792.0	617.8	648.5	617.4	454.6	22.8	35.03	2.12	52.61	64.21	1067.9	1419.0	-848.4	-1277.6	1303.0	1300.5	6012	8373	4942	7965	5971
95	30.382	30.293	773.5	578.8	620.6	578.7	461.7	13.7	36.65	1.35	54.24	66.10	1061.9	1428.3	-861.7	-1305.8	1323.4	1319.5	6012	8373	4942	7965	5971

TO/TO PO/PO EFF-AD EFF-P
INLET INLET INLET INLET
1.1771 1.6684 88.84 89.64

NCOR-1 MCR-1 TO/TO PO/PO EFF-AD EFF-P
INLET INLET INLET INLET
9983 166.23 1.1771 1.6332 84.87 85.90

TABLE 9.4
Blade-Element and Overall Performance with Uniform Inlet
90% of Design Speed

ROTOR

Table with columns: %SPAN, IN, DIA-1, DIA-2, V-1, V-2, VM-1, VM-2, VO-1, VO-2, B-1, B-2, B1-1, B1-2, V1-1, V1-2, V01-1, V01-2, U-1, U-2. Rows 5-95.

Table with columns: %SPAN, INCH, DEV, TURN, CAMBER, OMEGA-B, D-FAC, OMEGA-B, LOSS-P, PO2, EFF-P, EFF-AD, EFF-P, M-1, M-2, M1-1, M1-2. Rows 5-95.

10/10 INLET PO/PO
1.1927 1.7307 87.96 88.87

STATOR

Table with columns: %SPAN, IN, DIA-1, DIA-2, V-1, V-2, VM-1, VM-2, VO-1, VO-2, B-1, B-2, B1-1, B1-2, V1-1, V1-2, V01-1, V01-2, U-1, U-2. Rows 5-95.

Table with columns: %SPAN, INCH, DEV, TURN, CAMBER, OMEGA-B, D-FAC, OMEGA-B, LOSS-P, PO2, EFF-P, EFF-AD, EFF-P, M-1, M-2, M1-1, M1-2. Rows 5-95.

NCOR-1 WCOR-1 TO/TO PO/PO EFF-AD EFF-P WC/A-1
INLET INLET INLET INLET LBM/SEC LBM/SEC
9978 158.36 1.1927 1.6882 83.66 84.84 35.59

TABLE 9.5
Blade-Element and Overall Performance with Uniform Inlet
90% of Design Speed

ROTOR

%SPAN	DIA-1	DIA-2	V-1	V-2	VM-1	VM-2	VO-1	VO-2	B-1	B-2	B1-1	B1-2	V1-1	V1-2	VO1-1	VO1-2	U-1	U-2	
	IN	IN	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE	DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	
5	17.467	19.769	480.9	934.7	480.9	934.7	0	710.8	0.0	49.50	57.70	13.89	899.9	625.4	-760.7	-150.2	760.7	480.9	
10	18.467	20.499	492.5	959.9	492.5	959.9	0	670.4	0.0	48.22	56.52	19.95	943.0	638.2	-804.2	-217.7	804.2	492.5	
15	19.467	21.087	502.9	985.1	502.9	985.1	0	630.4	0.0	47.28	55.32	26.17	985.7	649.4	-847.8	-286.2	847.8	502.9	
20	22.314	22.564	522.4	754.7	522.4	754.7	0	562.7	0.0	46.20	61.74	40.96	1103.3	667.0	-971.8	-374.4	971.8	1000.1	
30	25.791	23.920	527.7	728.3	527.7	728.3	0	533.9	0.0	47.15	64.83	49.35	1241.8	761.0	-1123.2	-577.5	1123.2	1111.9	
40	28.534	24.076	517.2	703.8	517.2	703.8	0	513.3	0.0	47.63	67.70	56.03	1182.9	848.1	-1258.9	-703.4	1258.9	1242.7	
50	31.295	24.993	500.8	700.5	500.8	700.5	0	537.0	0.0	50.05	69.82	59.68	1452.0	891.1	-1382.7	-785.2	1382.7	1305.2	
60	31.883	30.630	496.8	688.4	496.8	688.4	0	540.1	0.0	51.68	70.34	61.73	1474.4	901.3	-1382.5	-793.8	1382.5	1333.9	
70	32.499	31.271	491.4	665.6	491.4	665.6	0	540.1	0.0	51.68	70.34	61.73	1474.4	901.3	-1382.5	-793.8	1382.5	1333.9	
85																			
90																			
95																			

INCS INCH DEV TURN CAMBER OMEGA-B D-FAC OMEGA-B LOSS-P LOSS-P PO2/ EFF-P EFF-AD EFF-P M1 M2 M1-1 M1-2

%SPAN	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE
5	2.30	8.73	12.02	43.81	47.12	0.000	0.893	-0.860	-0.098	1.8497	1.0223	1.0223	1.0450	4.398	81.87	82.87	34.51	
10	2.52	8.96	10.32	38.57	39.99	0.000	0.952	-0.895	-0.085	1.8699	1.0211	1.0230	1.0386	4.822	78.24	87.06	35.46	
15	2.81	8.61	9.64	33.16	34.03	0.000	0.909	-0.828	-0.045	1.8263	1.0116	1.0127	1.0195	4.824	74.41	81.32	36.31	
20	3.91	7.85	11.23	20.77	24.17	0.241	0.549	-0.155	0.105	1.7323	0.9357	0.9304	0.9184	4.793	64.78	70.28	37.23	
30	5.27	7.90	7.88	15.48	14.67	0.28	0.174	0.093	0.217	1.7248	0.8933	0.8866	0.8727	4.831	62.08	68.44	38.44	
40	6.23	8.42	5.88	11.86	9.41	0.528	0.546	0.544	0.272	1.7204	0.8355	0.824	0.819	4.731	53.99	58.00	40.62	
50	6.46	7.72	5.53	10.14	7.98	0.772	0.574	0.297	0.360	1.7344	0.7747	0.7607	0.7428	4.850	50.62	53.23	42.57	
60	6.50	7.59	6.00	8.61	7.62	0.824	0.521	0.297	0.403	1.7272	0.7505	0.7305	0.7185	4.836	47.59	48.84	43.14	
70	6.64	7.55	8.82	6.16	0.962	0.5267	0.2559	0.411	0.2676	1.7091	0.7216	0.6999	0.6929	4.482	35.29	36.82	45.54	

TO/TO PO/PO EFF-AD EFF-P INLET INLET INLET INLET

1.1996 1.149 86.69 67.70

STATOR

%SPAN	DIA-1	DIA-2	V-1	V-2	VM-1	VM-2	VO-1	VO-2	B-1	B-2	B1-1	B1-2	V1-1	V1-2	VO1-1	VO1-2	U-1	U-2
	IN	IN	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE	DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC
5	20.409	21.489	973.3	748.1	687.9	738.1	680.5	11.4	45.02	93	16.23	52.55	716.5	1104.4	200.3	-924.4	888.8	935.8
10	21.008	21.961	973.1	675.3	676.1	675.0	651.7	17.9	43.94	-1.54	21.27	55.28	723.9	1183.5	283.2	-974.3	914.9	950.4
15	21.569	22.432	988.7	649.0	655.9	648.2	614.3	31.7	43.13	-2.80	26.42	57.27	733.8	1199.8	325.8	-1048.0	942.2	976.9
20	23.314	23.982	802.9	601.8	569.8	600.9	554.3	33.3	43.66	-3.17	38.41	60.77	741.8	1239.8	481.0	-1042.2	1013.0	1044.9
30	25.601	25.893	784.7	592.9	576.0	592.4	532.9	24.3	42.77	-2.35	45.28	62.78	81.0	1239.3	582.4	-1151.9	1114.9	1127.6
40	27.818	27.902	776.0	581.8	570.8	574.7	525.7	11.5	42.65	-1.91	50.23	64.63	83.2	1357.6	689.7	-1228.7	1211.5	1215.1
50	29.408	29.382	790.7	578.3	568.9	574.9	549.1	19.1	43.98	1.51	52.13	65.52	92.5	1385.0	731.6	-1290.5	1280.7	1279.6
60	29.914	29.886	786.4	558.2	557.6	557.9	534.5	18.8	44.84	1.91	53.31	66.48	93.2	1397.8	748.3	-1281.7	1302.8	1304.2
70	30.382	30.293	774.3	534.4	534.2	536.0	17.5	45.99	1.88	54.93	67.69	93.62	1407.1	766.2	-1301.8	1323.1	1313.3	

INCS INCH DEV TURN CAMBER OMEGA-B D-FAC OMEGA-B LOSS-P LOSS-P PO2/ EFF-P EFF-AD EFF-P M1 M2 M1-1 M1-2

%SPAN	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE
5	-1.02	1.90	13.34	44.18	55.91	0.000	0.400	0.157	0.437	0.9335	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
10	-1.45	1.49	9.90	45.48	53.88	0.000	0.456	0.150	0.475	0.9335	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
15	-1.20	1.75	8.15	45.92	52.43	0.000	0.462	0.164	0.445	0.9445	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
20	2.05	4.21	8.05	46.83	50.67	0.000	0.4536	0.167	0.467	0.9336	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
30	2.94	6.17	12.31	43.78	49.87	0.000	0.4794	0.168	0.458	0.9356	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
40	4.53	7.84	17.79	42.08	51.98	0.000	0.5001	0.163	0.394	0.9738	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
50	5.28	8.60	19.32	42.93	53.56	0.000	0.5326	0.178	0.418	0.9700	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
60	6.29	9.66	21.57	44.12	56.01	0.000	0.5613	0.195	0.470	0.9678	0.000	0.000	0.000	0.000	0.000	0.000	0.000	

WCOR-1 WCOR-1 TO/TO PO/PO EFF-AD EFF-P INLET INLET INLET INLET

1.1996 1.1996 1.7012 82.04 83.34 34.65

TABLE 9.6
Blade-Element and Overall Performance with Uniform Inlet
90% of Design Speed

ROTOR

%SPAN	DIA-1		DIA-2		V-1		V-2		VM-1		VM-2		VO-1		VO-2		B-1		B-2		B1-1		B1-2		V1-1		V1-2		V0-1		V0-2		U-1		U-2			
	IN	IN	IN	IN	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC			
5	17.467	19.769	465.4	934.8	465.4	600.3	0	719.5	0	50.04	58.55	13.56	892.0	617.5	-761.0	-144.7	761.0	861.3	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	
10	18.467	20.408	476.6	898.5	476.6	591.0	0	676.7	0	48.56	59.36	19.75	935.1	628.4	-804.5	-212.4	804.5	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	
15	19.467	21.047	486.5	856.7	486.5	548.4	0	637.1	0	37.17	48.56	14.56	892.0	617.5	-761.0	-144.7	761.0	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1
30	22.314	22.964	504.6	754.2	504.6	487.4	0	575.6	0	24.00	34.12	34.03	800.0	510.1	-800.0	-34.03	800.0	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1
50	25.791	25.520	508.2	733.8	508.2	484.9	0	550.8	0	20.00	28.50	28.50	700.0	484.9	-700.0	-28.50	700.0	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1
70	29.924	29.076	496.7	716.0	496.7	453.2	0	544.7	0	15.00	22.00	22.00	600.0	453.2	-600.0	-22.00	600.0	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1
85	31.295	29.993	460.9	706.0	460.9	423.2	0	566.6	0	10.00	18.00	18.00	500.0	423.2	-500.0	-18.00	500.0	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1
90	31.683	30.650	476.5	696.6	476.5	406.7	0	566.6	0	5.00	12.00	12.00	400.0	406.7	-400.0	-12.00	400.0	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1
95	32.499	31.271	472.1	683.3	472.1	384.7	0	564.7	0	0.00	8.00	8.00	300.0	384.7	-300.0	-8.00	300.0	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1	809.1

TO/TO PO/PO EFF-AD EFF-P
INLET INLET INLET INLET
1.2071 1.7664 85.18 86.31

STATOR

%SPAN	DIA-1		DIA-2		V-1		V-2		VM-1		VM-2		VO-1		VO-2		B-1		B-2		B1-1		B1-2		V1-1		V1-2		V0-1		V0-2		U-1		U-2						
	IN	IN	IN	IN	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC					
5	20.409	21.489	969.3	687.3	687.3	687.3	687.3	687.3	687.3	687.3	687.3	687.3	687.3	687.3	687.3	687.3	14.8	45.73	1.23	1.23	16.04	53.29	704.3	704.3	704.3	704.3	704.3	704.3	704.3	704.3	704.3	704.3	704.3	704.3	704.3	704.3	704.3	704.3			
10	21.008	21.961	933.7	654.1	654.1	654.1	654.1	654.1	654.1	654.1	654.1	654.1	654.1	654.1	654.1	18.8	44.74	1.63	1.63	21.25	56.23	711.9	711.9	711.9	711.9	711.9	711.9	711.9	711.9	711.9	711.9	711.9	711.9	711.9	711.9	711.9	711.9	711.9	711.9		
15	21.599	22.432	893.0	624.1	624.1	624.1	624.1	624.1	624.1	624.1	624.1	624.1	624.1	624.1	624.1	21.5	44.05	2.02	2.02	26.47	58.45	717.6	717.6	717.6	717.6	717.6	717.6	717.6	717.6	717.6	717.6	717.6	717.6	717.6	717.6	717.6	717.6	717.6	717.6	717.6	
30	23.314	23.902	797.6	576.5	576.5	576.5	576.5	576.5	576.5	576.5	576.5	576.5	576.5	576.5	576.5	27.4	45.31	3.45	3.45	36.62	63.29	796.1	796.1	796.1	796.1	796.1	796.1	796.1	796.1	796.1	796.1	796.1	796.1	796.1	796.1	796.1	796.1	796.1	796.1	796.1	
50	25.601	25.893	705.0	573.9	573.9	573.9	573.9	573.9	573.9	573.9	573.9	573.9	573.9	573.9	573.9	34.2	44.47	4.85	4.85	45.25	63.29	849.0	849.0	849.0	849.0	849.0	849.0	849.0	849.0	849.0	849.0	849.0	849.0	849.0	849.0	849.0	849.0	849.0	849.0	849.0	
70	27.818	27.702	785.3	564.9	564.9	564.9	564.9	564.9	564.9	564.9	564.9	564.9	564.9	564.9	564.9	41.0	45.05	6.25	6.25	54.25	65.28	897.0	897.0	897.0	897.0	897.0	897.0	897.0	897.0	897.0	897.0	897.0	897.0	897.0	897.0	897.0	897.0	897.0	897.0	897.0	
85	29.408	29.382	789.1	552.1	552.1	552.1	552.1	552.1	552.1	552.1	552.1	552.1	552.1	552.1	552.1	47.8	47.22	7.65	7.65	63.29	66.51	883.3	883.3	883.3	883.3	883.3	883.3	883.3	883.3	883.3	883.3	883.3	883.3	883.3	883.3	883.3	883.3	883.3	883.3	883.3	883.3
90	29.914	29.856	788.4	544.3	544.3	544.3	544.3	544.3	544.3	544.3	544.3	544.3	544.3	544.3	544.3	51.8	47.51	9.05	9.05	71.61	67.14	897.0	897.0	897.0	897.0	897.0	897.0	897.0	897.0	897.0	897.0	897.0	897.0	897.0	897.0	897.0	897.0	897.0	897.0	897.0	
95	30.382	30.293	781.6	531.7	531.7	531.7	531.7	531.7	531.7	531.7	531.7	531.7	531.7	531.7	531.7	56.3	48.07	10.45	10.45	79.62	67.92	907.5	907.5	907.5	907.5	907.5	907.5	907.5	907.5	907.5	907.5	907.5	907.5	907.5	907.5	907.5	907.5	907.5	907.5	907.5	

INCOR-1 WCOR-1 10/TC PO/PO EFF-AD EFF-P WC/A-1
INLET INLET INLET INLET INLET
RPM LBM/SEC X X X X X
9985 149.74 1.2071 1.7123 80.14 81.59 33.65

TABLE 10.2
Blade-Element and Overall Performance with Uniform Inlet

100% of Design Speed

ROTOR

%SPAN	DIA-1 IN	DIA-2 IN	V-1 FI/SEC	V-2 FI/SEC	VM-1 FI/SEC	VM-2 FI/SEC	V0-1 FI/SEC	V0-2 FI/SEC	B-1 DEGREE	B-2 DEGREE	R-1 DEGREE	R-2 DEGREE	V1-1 FT/SEC	V1-2 FT/SEC	V01-1 FT/SEC	V01-2 FT/SEC	U-1 FT/SEC	U-2 FT/SEC
5	17.467	19.769	601.1	1024.9	601.1	683.9	0	703.3	0.0	48.14	54.58	15.79	1037.3	710.8	843.3	193.4	843.3	966.7
10	18.467	20.408	616.5	967.3	616.5	661.8	0	705.9	0.0	46.82	55.40	23.08	1085.7	719.7	893.7	282.3	893.7	987.7
15	19.467	21.047	631.2	931.3	631.2	636.9	0	656.9	0.0	44.85	56.16	28.70	1134.0	753.0	942.1	361.7	942.1	1018.6
30	22.314	22.964	666.1	877.8	666.1	650.9	0	582.2	0.0	41.55	58.33	38.83	1268.8	843.8	1079.9	519.2	1079.9	1143.1
50	25.791	25.520	685.5	825.7	685.5	637.2	0	531.5	0.0	39.83	61.22	47.80	1424.2	949.7	1248.2	703.2	1248.2	1333.1
70	28.954	28.076	673.4	774.8	673.4	581.1	0	471.1	0.0	38.44	64.33	57.05	1554.7	1074.2	1401.3	801.5	1401.3	1358.8
85	31.295	29.993	648.1	724.5	648.1	556.6	0	444.5	0.0	36.63	67.44	64.00	1670.8	1195.8	1507.0	874.9	1507.0	1331.5
90	31.883	30.630	640.9	676.5	640.9	532.3	0	428.8	0.0	42.07	67.44	64.00	1670.8	1195.8	1507.0	874.9	1507.0	1331.5
95	32.499	31.271	635.3	629.8	635.3	530.3	0	459.8	0.0	46.90	68.00	67.78	1696.3	1138.1	1572.8	903.6	1572.8	1513.4

%SPAN	INCS	INCH	DEV	TURN	CAMBER	OMEGA-F	D-FAC	OMEGA-B	LOSS-P	LOSS-B	PO2	EFF-P	EFF-B	EFF-AD	EFF-P	M=1	M=2	M1=1	M1=2
5	-0.82	5.61	13.92	38.79	47.12	0.000	0.864	1.139	0.296	1.943	0.133	0.111	0.638	0.554	0.893	0.955	0.955	0.955	0.955
10	-0.63	5.78	13.46	32.32	39.99	0.141	0.940	1.142	0.303	1.890	0.107	0.884	0.803	0.571	0.833	1.007	1.007	1.007	1.007
15	-0.81	5.54	12.19	27.48	34.03	0.168	0.805	1.159	0.244	1.861	0.160	0.906	0.832	0.561	0.804	1.052	1.052	1.052	1.052
30	1.40	4.40	9.11	19.50	24.20	0.408	0.303	0.859	0.176	1.842	0.242	0.916	0.979	0.622	0.752	1.161	1.161	1.161	1.161
50	1.66	4.30	5.52	13.42	14.66	0.768	0.463	1.038	0.213	1.811	0.893	0.879	0.874	0.630	0.707	1.324	1.324	1.324	1.324
70	5.91	4.70	6.53	7.28	9.12	1.097	0.069	1.171	0.215	1.719	0.510	0.831	0.829	0.630	0.707	1.324	1.324	1.324	1.324
85	3.47	4.70	6.96	5.76	8.02	1.321	0.970	1.511	0.264	1.697	0.797	0.782	0.782	0.615	0.615	1.528	1.528	1.528	1.528
90	3.63	4.69	8.91	3.44	7.66	1.394	1.120	2.006	0.324	1.652	0.738	0.738	0.738	0.593	0.593	1.549	1.549	1.549	1.549
95	3.80	4.70	11.94	0.22	7.47	1.498	1.238	2.493	0.311	1.605	0.670	0.648	0.648	0.582	0.582	1.570	1.570	1.570	1.570

TO/TO PO/PO EFF-AD EFF-P
INLET INLET INLET INLET
1.2106 1.7803 85.37 86.50

STATOR

%SPAN	DIA-1 IN	DIA-2 IN	V-1 FI/SEC	V-2 FI/SEC	VM-1 FI/SEC	VM-2 FI/SEC	V0-1 FI/SEC	V0-2 FI/SEC	B-1 DEGREE	B-2 DEGREE	R-1 DEGREE	R-2 DEGREE	V1-1 FT/SEC	V1-2 FT/SEC	V01-1 FT/SEC	V01-2 FT/SEC	U-1 FT/SEC	U-2 FT/SEC
5	20.409	21.489	1891.9	897.3	803.5	897.3	739.4	-0.2	42.62	-0.40	17.17	49.38	841.0	1378.3	248.3	1046.2	967.7	1040.0
10	21.008	21.961	1838.7	877.3	807.7	877.3	739.4	-16.5	41.26	-1.08	23.01	50.90	848.4	1390.9	331.6	1079.3	1016.7	1042.6
15	21.589	22.432	1805.8	862.1	795.8	861.6	640.2	-27.1	39.53	-1.80	27.53	52.24	875.1	1407.4	404.6	1112.7	1044.8	1045.8
30	23.314	23.902	958.5	828.8	767.8	828.1	573.4	-33.7	36.75	-2.33	35.84	55.17	947.6	1450.3	554.9	1190.5	1180.3	1156.8
50	25.601	25.893	920.0	799.6	752.2	799.1	529.6	-25.3	35.14	-1.82	43.30	57.98	1034.4	1507.5	709.4	1278.4	1259.0	1233.1
70	27.818	27.902	855.6	728.6	720.4	727.5	461.5	-40.2	32.65	-3.16	50.84	62.38	1181.0	1569.5	884.7	1390.6	1366.3	1350.3
85	29.408	29.362	851.0	679.6	720.2	679.4	453.5	-17.0	32.20	-1.42	53.40	64.72	1208.0	1591.3	969.6	1438.9	1423.2	1422.0
90	29.914	29.856	831.0	648.5	689.4	648.3	463.5	-8.7	33.95	-1.77	54.98	65.96	1201.4	1591.8	963.8	1453.6	1447.7	1444.9
95	30.382	30.293	802.9	597.7	648.6	597.6	473.3	-10.6	36.12	-1.01	56.96	67.97	1189.5	1593.0	997.1	1476.6	1470.4	1464.1

%SPAN	INCS	INCM	DEV	TURN	CAMBER	OMEGA-F	D-FAC	OMEGA-B	LOSS-P	LOSS-B	PO2	EFF-P	EFF-B	EFF-AD	EFF-P	M=1	M=2	M1=1	M1=2
5	-3.31	-3.39	12.02	43.02	55.90	0.036	3.837	1.546	0.384	0.312	0.000	0.000	0.646	0.419	0.646	0.419	0.646	0.419	
10	-4.41	-4.48	10.37	42.55	53.88	0.000	3.842	0.945	0.241	0.241	0.000	0.000	0.769	0.872	0.769	0.872	0.769	0.872	
15	-4.95	-5.00	9.14	41.53	52.44	0.000	3.135	0.694	0.181	0.181	0.000	0.000	0.818	0.830	0.818	0.830	0.818	0.830	
30	-5.71	-5.70	8.69	39.08	50.68	0.000	3.111	0.720	0.202	0.202	0.000	0.000	0.900	0.900	0.900	0.900	0.900	0.900	
50	-5.39	-5.42	10.22	36.96	49.60	0.000	3.147	0.748	0.229	0.229	0.000	0.000	0.945	0.945	0.945	0.945	0.945	0.945	
70	-7.05	-7.02	10.33	35.81	49.91	0.000	3.425	0.715	0.236	0.236	0.000	0.000	0.948	0.948	0.948	0.948	0.948	0.948	
85	-5.40	-5.47	14.47	33.62	52.30	0.000	3.448	0.671	0.241	0.241	0.000	0.000	0.956	0.956	0.956	0.956	0.956	0.956	
90	-5.40	-5.40	16.63	34.72	53.56	0.000	4.421	0.666	0.266	0.266	0.000	0.000	0.962	0.962	0.962	0.962	0.962	0.962	
95	-3.61	-3.61	18.68	37.15	56.33	0.000	4.752	0.548	0.266	0.266	0.000	0.000	0.975	0.975	0.975	0.975	0.975	0.975	

NCOR-1 NCOR-1 TO/TO PO/PO EFF-AD EFF-P WC/A-1
RPM LBM/SEC INLET INLET INLET INLET LBM/SEC
11092 183.99 1.2106 1.7320 80.63 82.06 41.35

TABLE 10.4
Blade-Element and Overall Performance with Uniform Inlet
100% of Design Speed

ROTOR

%SPAN	IN	DIA-1 IN	DIA-2 IN	V-1 FT/SEC	V-2 FT/SEC	VM-1 FT/SEC	VM-2 FT/SEC	VO-1 FT/SEC	VO-2 FT/SEC	B-1 DEGREE	B-2 DEGREE	B*1 DEGREE	B*2 DEGREE	V1-1 FT/SEC	V1-2 FT/SEC	V01-1 FT/SEC	V01-2 FT/SEC	U-1 FT/SEC	U-2 FT/SEC
5	17.467	19.769	584.0	999.1	584.0	520.1	0.0	776.2	0.0	50.97	50.35	15.99	1077.3	654.5	-843.1	-180.4	845.1	956.5	
10	18.467	20.468	599.4	963.5	599.4	525.2	0.0	733.1	0.0	49.54	50.15	28.13	1075.9	675.0	-893.5	-254.3	893.5	987.4	
15	19.467	21.047	613.5	923.1	613.5	500.3	0.0	693.4	0.0	48.70	50.92	41.80	1154.1	690.9	-941.9	-324.9	941.9	1014.3	
30	22.314	22.964	642.6	828.0	642.6	530.3	0.0	636.7	0.0	50.21	50.21	41.80	1256.4	711.6	-1079.7	-474.4	1079.7	1111.1	
50	25.781	25.520	657.6	819.0	657.6	539.5	0.0	616.9	0.0	48.83	52.21	41.80	1410.6	820.3	-1247.9	-749.9	1247.9	1234.4	
70	28.948	28.078	651.6	760.2	651.6	524.0	0.0	589.8	0.0	46.81	65.05	55.91	1545.1	933.4	-1404.9	-749.9	1404.9	1354.4	
85	31.883	29.993	631.3	707.2	631.3	523.0	0.0	568.0	0.0	47.78	67.97	58.65	1640.5	1016.7	-1514.2	-685.4	1514.2	1451.2	
90	31.883	30.630	624.3	774.7	624.3	494.1	0.0	596.6	0.0	50.38	67.97	58.65	1640.5	1016.7	-1514.2	-685.4	1514.2	1451.2	
95	32.899	31.271	617.6	738.6	617.6	423.9	0.0	604.8	0.0	54.97	68.56	58.98	1689.4	1002.3	-1724.4	-908.2	1572.4	1513.0	

%SPAN	INCM	DEV DEGREE	TURN DEGREE	CAMBER DEGREE	OMEGA-B D-FAC	OMEGA-B D-FAC	LOSS-P PO2/	LOSS-P FILE	TOTAL POL	EFF-AD TOTAL	EFF-AD STATIC	M-1	M-2	M*-1	M*-2		
																INLET	INLET
5	7.06	6.37	14.12	39.36	47.12	0.000	5.991	-0.0159	-0.0034	2.1235	1.0065	1.0073	1.0119	5.585	8.620	9.081	5.647
10	12	6.54	12.52	34.01	39.99	0.000	5.372	-0.0202	-0.0043	2.0930	1.0100	1.0111	1.0159	5.548	8.292	9.087	5.609
15	13.35	6.28	11.55	28.86	34.03	0.201	5.394	-0.0283	-0.018	2.0492	1.0033	1.0037	1.0052	5.688	7.921	1.0402	5.928
30	1.30	5.32	12.06	17.44	24.17	0.022	5.721	0.0799	0.0161	1.9528	0.9343	0.9277	0.9231	5.961	7.024	1.1693	6.032
50	2.56	5.25	6.51	13.34	14.60	0.740	5.613	0.1020	0.045	1.9049	0.9058	0.8968	0.8971	6.102	6.807	1.3059	6.693
70	3.54	5.40	5.32	9.14	9.48	1.103	5.057	0.1495	0.075	1.9957	0.8911	0.8953	0.8949	6.518	6.518	1.4274	7.064
85	3.97	5.25	4.45	6.72	7.93	1.327	5.064	0.2278	0.032	2.0359	0.8455	0.8291	0.8348	6.569	6.516	1.5396	8.415
90	4.11	5.21	5.69	7.13	7.60	1.400	5.204	0.337	0.090	2.0255	0.8073	0.7871	0.7942	5.746	6.32	1.5350	8.840
95	4.33	5.25	9.08	3.58	7.42	1.505	5.985	0.371	0.135	1.9836	0.7600	0.7356	0.7532	5.713	6.024	1.5548	8.180

TO/TO PO/PO EFF-AD EFF-P

INLET INLET INLET INLET

1.2478 2.0103 89.00 90.04

STATOR

%SPAN	IN	DIA-2 IN	V-1 FT/SEC	V-2 FT/SEC	VM-1 FT/SEC	VM-2 FT/SEC	VO-1 FT/SEC	VO-2 FT/SEC	B-1 DEGREE	B-2 DEGREE	B*1 DEGREE	B*2 DEGREE	V1-1 FT/SEC	V1-2 FT/SEC	V01-1 FT/SEC	V01-2 FT/SEC	U-1 FT/SEC	U-2 FT/SEC
5	20.409	21.489	1040.6	704.4	719.5	704.4	751.8	514	46.26	-4.44	18.13	56.02	757.2	1260.4	-235.7	-1045.1	987.5	1039.7
10	21.008	21.961	1006.1	676.1	711.0	675.3	711.9	503.6	45.03	-2.60	23.19	58.29	775.6	1285.1	-304.9	-1093.1	1016.5	1062.0
15	21.389	22.432	987.8	654.3	692.6	653.0	675.9	401.3	44.30	-3.52	28.82	59.88	784.9	1301.4	-368.6	-1125.6	1044.6	1085.4
30	23.314	23.902	883.6	626.2	621.7	626.1	627.8	111.3	45.28	-1.04	38.61	61.80	798.0	1325.1	-500.2	-1167.6	1128.0	1156.5
50	25.601	25.893	884.9	651.4	651.4	651.4	615.7	91.3	44.09	-1.82	44.42	62.70	890.0	1420.3	-625.0	-1262.1	1258.0	1321.8
70	27.818	27.902	866.7	645.5	649.8	645.1	574.4	221.0	41.51	-1.96	49.93	64.82	1008.2	1516.2	-771.6	-1372.1	1346.0	1350.0
85	29.408	29.382	897.5	648.9	649.9	648.5	576.9	221.8	41.70	2.01	50.96	65.13	1063.5	1541.8	-826.0	-1498.9	1422.9	1421.6
90	29.914	29.856	894.7	637.9	651.2	646.7	613.5	371.6	43.29	3.39	52.01	65.65	1058.0	1544.3	-833.8	-1406.9	1447.4	1444.6
95	30.382	30.293	873.3	601.7	612.1	601.0	622.9	294.9	45.50	2.84	54.15	65.65	1045.1	1556.6	-847.1	-1435.9	1470.0	1465.7

%SPAN	INCM	DEV DEGREE	TURN DEGREE	CAMBER DEGREE	OMEGA-B D-FAC	OMEGA-B D-FAC	LOSS-P PO2/	LOSS-P FILE	TOTAL POL	EFF-AD TOTAL	EFF-AD STATIC	M-1	M-2	M*-1	M*-2			
																INLET	INLET	INLET
5	0.08	3.00	11.97	40.70	55.91	0.000	4.994	-1.788	0.445	3.445	0.265	0.000	0.000	7.437	8.031	5.865	6.575	1.0484
10	-0.31	2.62	8.85	47.64	53.48	0.000	5.126	-1.828	0.466	3.266	0.287	0.000	0.000	7.453	8.022	5.631	6.723	1.0704
15	0.00	2.95	7.33	47.83	52.34	0.000	5.192	-1.824	0.424	3.424	0.444	0.000	0.000	7.545	5.444	5.444	6.677	1.0487
30	2.83	5.82	10.18	46.32	50.67	0.000	4.920	-0.639	0.179	3.179	0.900	0.000	0.000	6.943	7.510	5.200	6.603	1.1004
50	3.44	6.57	11.20	44.91	49.55	0.000	4.791	-0.661	0.203	3.203	0.924	0.000	0.000	8.832	7.499	5.382	7.512	1.1714
70	1.92	5.15	11.49	43.47	49.83	0.000	4.831	-0.527	0.174	3.174	0.944	0.000	0.000	9.014	7.315	5.322	8.487	1.2512
85	2.29	5.61	17.91	39.69	51.98	0.000	5.006	-1.114	0.389	3.389	0.652	0.000	0.000	8.125	7.511	5.299	8.064	1.2502
90	3.70	7.03	20.85	39.91	53.61	0.000	5.160	-1.158	0.411	3.411	0.411	0.000	0.000	8.148	7.461	5.179	8.624	1.2519
95	5.77	9.14	22.53	42.66	56.01	0.000	5.562	-1.251	0.443	3.443	0.443	0.000	0.000	8.062	7.241	4.813	8.444	1.2514

MCOR-1 MCOR-1 TO/TO PO/PO EFF-AD EFF-P
INLET INLET INLET INLET INLET
110.89, 180.43 1.2478 1.9464 84.48 85.67
RPM LBM/SEC INLET INLET INLET
SOFT 40.55

TABLE 10.5

Blade-Element and Overall Performance with Uniform Inlet
100% of Design Speed

ROTOR

%SPAN	DIA-1		DIA-2		V-1		V-2		VM-1		VM-2		VO-1		VO-2		B-1		B-2		R1-1		R1-2		V1-1		V1-2		V01-1		V01-2		U-1		U-2						
	IN	OUT	IN	OUT	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE					
5	17.467	19.769	576.2	1002.1	570.2	620.9	.0	786.6	.00	31.72	56.01	15.36	1020.0	843.9	-843.7	-170.3	843.7	987.2	843.7	987.2	843.7	987.2	843.7	987.2	843.7	987.2	843.7	987.2	843.7	987.2	843.7	987.2	843.7	987.2	843.7	987.2	843.7	987.2			
10	18.467	20.408	584.9	964.5	584.9	616.4	.0	741.9	.00	50.28	56.81	21.77	1068.5	663.9	-663.1	-249.2	663.9	988.1	663.9	988.1	663.9	988.1	663.9	988.1	663.9	988.1	663.9	988.1	663.9	988.1	663.9	988.1	663.9	988.1	663.9	988.1	663.9	988.1	663.9	988.1	
15	19.467	21.047	598.5	925.7	598.5	603.9	.0	701.6	.00	49.28	57.58	27.73	1111.5	682.6	-682.5	-317.4	682.6	982.5	682.6	982.5	682.6	982.5	682.6	982.5	682.6	982.5	682.6	982.5	682.6	982.5	682.6	982.5	682.6	982.5	682.6	982.5	682.6	982.5	682.6	982.5	
30	23.314	23.944	625.8	828.3	625.8	515.6	.0	647.6	.00	51.51	59.92	31.94	1248.6	693.4	-693.4	-108.0	693.4	1080.4	693.4	1080.4	693.4	1080.4	693.4	1080.4	693.4	1080.4	693.4	1080.4	693.4	1080.4	693.4	1080.4	693.4	1080.4	693.4	1080.4	693.4	1080.4	693.4	1080.4	693.4
50	28.921	28.076	634.5	785.6	634.5	519.2	.0	592.6	.00	48.63	65.71	55.98	1538.0	924.6	-924.6	-101.9	924.6	1401.9	924.6	1401.9	924.6	1401.9	924.6	1401.9	924.6	1401.9	924.6	1401.9	924.6	1401.9	924.6	1401.9	924.6	1401.9	924.6	1401.9	924.6	1401.9	924.6	1401.9	924.6
70	31.283	29.993	613.0	799.7	613.0	419.3	.0	608.9	.00	49.59	67.27	58.82	1634.8	988.2	-988.2	-83.2	988.2	1452.2	988.2	1452.2	988.2	1452.2	988.2	1452.2	988.2	1452.2	988.2	1452.2	988.2	1452.2	988.2	1452.2	988.2	1452.2	988.2	1452.2	988.2	1452.2	988.2	1452.2	988.2
90	31.883	30.630	606.2	789.2	606.2	419.3	.0	623.6	.00	52.21	68.56	60.84	1658.3	986.2	-986.2	-134.3	986.2	1452.2	986.2	1452.2	986.2	1452.2	986.2	1452.2	986.2	1452.2	986.2	1452.2	986.2	1452.2	986.2	1452.2	986.2	1452.2	986.2	1452.2	986.2	1452.2	986.2	1452.2	986.2
96	32.499	31.271	599.6	756.3	599.6	413.8	.0	631.8	.00	56.65	69.13	64.77	1663.9	975.8	-975.8	-1573.5	975.8	1573.5	975.8	1573.5	975.8	1573.5	975.8	1573.5	975.8	1573.5	975.8	1573.5	975.8	1573.5	975.8	1573.5	975.8	1573.5	975.8	1573.5	975.8	1573.5	975.8	1573.5	

TO/TO PO/PO EFF-AD EFF-P
INLET INLET INLET INLET

1.2547 2.0310 88.03 89.16

STATOR

%SPAN	DIA-1		DIA-2		V-1		V-2		VM-1		VM-2		VO-1		VO-2		B-1		B-2		R1-1		R1-2		V1-1		V1-2		V01-1		V01-2		U-1		U-2						
	IN	OUT	IN	OUT	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE					
5	20.409	21.489	1039.8	887.1	707.6	687.1	761.9	-7.2	47.12	-2.39	17.73	56.74	782.9	1252.8	-1087.6	988.1	1030.4	23.02	38.88	759.0	1274.0	226.8	1090.6	1017.1	1083.3	37.69	50.51	77.7	1372.3	384.2	1174.6	105.3	1097.3	37.69	50.51	77.7	1372.3	384.2	1174.6	105.3	1097.3
10	21.008	21.961	1003.4	858.6	698.4	698.2	720.4	-27.3	45.88	-3.46	23.02	58.88	829.0	1274.0	-226.8	1090.6	1017.1	23.02	38.88	759.0	1274.0	226.8	1090.6	1017.1	1083.3	37.69	50.51	77.7	1372.3	384.2	1174.6	105.3	1097.3	37.69	50.51	77.7	1372.3	384.2	1174.6	105.3	1097.3
15	21.509	22.332	948.3	837.1	653.5	656.4	659.2	-38.5	45.08	-1.24	34.04	62.61	874.1	1318.2	-384.2	1174.6	105.3	34.04	62.61	874.1	1318.2	-384.2	1174.6	105.3	1097.3	37.69	50.51	77.7	1372.3	384.2	1174.6	105.3	1097.3	37.69	50.51	77.7	1372.3	384.2	1174.6	105.3	1097.3
30	23.314	23.944	899.0	806.5	603.5	606.4	639.2	-13.2	46.88	-1.24	34.04	62.61	874.1	1318.2	-384.2	1174.6	105.3	34.04	62.61	874.1	1318.2	-384.2	1174.6	105.3	1097.3	37.69	50.51	77.7	1372.3	384.2	1174.6	105.3	1097.3	37.69	50.51	77.7	1372.3	384.2	1174.6	105.3	1097.3
50	25.601	25.993	880.3	828.4	618.5	628.3	626.4	-6.9	45.37	-1.24	34.04	62.61	874.1	1318.2	-384.2	1174.6	105.3	45.37	48.74	63.51	1408.5	-613.1	1260.6	1239.5	1293.7	48.74	63.51	78.9	1408.5	-613.1	1260.6	1239.5	1293.7	48.74	63.51	78.9	1408.5	-613.1	1260.6	1239.5	1293.7
70	27.818	27.922	867.4	833.3	630.4	633.4	635.8	-17.6	43.39	-1.24	34.04	62.61	874.1	1318.2	-384.2	1174.6	105.3	48.74	63.51	78.9	1408.5	-613.1	1260.6	1239.5	1293.7	48.74	63.51	78.9	1408.5	-613.1	1260.6	1239.5	1293.7	48.74	63.51	78.9	1408.5	-613.1	1260.6	1239.5	1293.7
85	28.408	29.382	803.8	844.3	634.1	633.4	623.7	25.5	43.84	-1.24	34.04	62.61	874.1	1318.2	-384.2	1174.6	105.3	51.81	65.70	1086.7	1240.7	-806.8	1404.2	1444.4	1445.9	65.70	1086.7	1240.7	-806.8	1404.2	1444.4	1445.9	65.70	1086.7	1240.7	-806.8	1404.2	1444.4	1445.9		
90	29.914	29.856	803.5	834.9	634.9	633.9	641.4	41.3	45.29	3.73	51.81	65.70	1086.7	1240.7	-806.8	1404.2	1444.4	51.81	65.70	1086.7	1240.7	-806.8	1404.2	1444.4	1445.9	65.70	1086.7	1240.7	-806.8	1404.2	1444.4	1445.9	65.70	1086.7	1240.7	-806.8	1404.2	1444.4	1445.9		
96	30.362	30.493	883.0	801.4	596.9	600.5	650.6	33.9	47.46	3.23	51.81	65.70	1086.7	1240.7	-806.8	1404.2	1444.4	51.81	65.70	1086.7	1240.7	-806.8	1404.2	1444.4	1445.9	65.70	1086.7	1240.7	-806.8	1404.2	1444.4	1445.9	65.70	1086.7	1240.7	-806.8	1404.2	1444.4	1445.9		

NCOR-1 WCOR-1 TO/TO PO/PO EFF-AD EFF-P WC/A-1
INLET INLET INLET INLET INLET INLET
RPM LBM/SEC % % % % %
11096 177.14 1.2547 1.9586 83.01 84.54 39.81

TABLE 10.6
Blade-Element and Overall Performance with Uniform Inlet
100% of Design Speed

ROTOR

%SPAN	DIA-1 IN	DIA-2 IN	V-1 FT/SEC	V-2 FT/SEC	VH-1 FT/SEC	VH-2 FT/SEC	VO-1 FT/SEC	VO-2 FT/SEC	B-1 DEGREE	B-2 DEGREE	B-1 DEGREE	B-2 DEGREE	V-1 FT/SEC	V-2 FT/SEC	VH-1 FT/SEC	VH-2 FT/SEC	VO-1 FT/SEC	VO-2 FT/SEC	U-1 FT/SEC	U-2 FT/SEC
6	17.467	19.769	571.9	1804.5	571.9	571.9	0.0	790.6	0.0	31.84	59.82	15.02	1087.6	821.9	895.6	146.8	895.6	895.6	895.6	927.8
10	18.467	20.408	571.9	1804.5	571.9	571.9	0.0	748.1	0.0	50.83	59.82	15.02	1087.6	821.9	895.6	146.8	895.6	895.6	895.6	927.8
15	19.467	21.049	571.9	1804.5	571.9	571.9	0.0	705.6	0.0	50.83	59.82	15.02	1087.6	821.9	895.6	146.8	895.6	895.6	895.6	927.8
30	22.514	22.924	610.2	2111.5	610.2	610.2	0.0	639.9	0.0	50.61	63.56	49.02	1394.4	795.4	1248.5	600.5	1248.5	1248.5	1248.5	1399.2
50	25.791	25.820	610.2	2111.5	610.2	610.2	0.0	610.1	0.0	50.36	66.41	55.96	1529.5	903.7	1401.7	749.1	1401.7	1401.7	1401.7	1599.2
85	31.885	31.993	610.2	2111.5	610.2	610.2	0.0	610.1	0.0	50.36	66.41	55.96	1529.5	903.7	1401.7	749.1	1401.7	1401.7	1401.7	1599.2
90	31.885	30.630	586.1	1785.9	586.1	586.1	0.0	645.5	0.0	54.21	69.20	60.93	1651.0	958.0	1543.4	837.3	1543.4	1543.4	1543.4	1482.8
95	32.499	31.271	580.1	1767.8	580.1	580.1	0.0	642.0	0.0	58.12	69.76	64.80	1676.8	952.6	1573.3	861.9	1573.3	1573.3	1573.3	1513.8

%SPAN	INCS DEGREE	INCH DEGREE	DEV DEGREE	TURN CAMBER	OMEGA-A DEGREE	OMEGA-B DEGREE	D-FAC	OMEGA-B TOTAL	LOSS-P TOTAL	LOSS-P PROFILE	POZ	EFF-P TOTAL	EFF-P TOTAL	EFF-P TOTAL	M-1	M-2	M-1	M-2	M-1	M-2
5	1.21	7.61	13.16	51.59	47.12	0.000	5485	-0.021	-0.026	2.1475	1.0093	1.0093	0.067	5125	8655	9327	8655	9327	8655	9327
10	1.40	7.81	11.81	35.98	39.00	0.000	5468	-0.034	-0.034	2.1143	1.0091	1.0091	0.123	5277	8313	9638	8313	9638	8313	9638
15	1.65	7.52	10.81	30.86	34.03	0.231	5426	-0.135	-0.029	2.0773	1.0065	1.0072	1.009	5407	7876	1.0313	5407	7876	1.0313	5407
30	2.84	6.63	12.04	18.77	24.18	0.449	5910	0.0991	-0.199	0.108	1.9667	0.923	0.913	5644	7022	1.1743	5644	7022	1.1743	5644
50	3.94	6.61	6.68	14.54	14.61	0.806	5678	0.243	0.091	2.0171	0.8926	0.813	0.8763	5738	6844	1.2891	5738	6844	1.2891	5738
70	4.91	6.76	5.40	10.43	9.07	1.130	5421	0.286	0.073	2.0238	0.8535	0.862	0.832	5856	6577	1.4093	5856	6577	1.4093	5856
85	5.26	6.53	4.37	10.09	7.95	1.353	5074	0.370	0.118	2.0776	0.8088	0.881	0.782	5483	6429	1.4916	5483	6429	1.4916	5483
90	5.36	6.45	3.79	6.27	7.61	1.427	5611	0.232	0.046	0.185	2.0702	0.760	0.751	5409	6497	1.5173	5409	6497	1.5173	5409
95	5.54	6.45	6.91	4.96	7.42	1.533	5751	0.2691	0.0450	0.187	2.0431	0.7402	0.733	5393	6226	1.5415	5393	6226	1.5415	5393

INLET PROFILE

INLET PROFILE EFF-P
1.2598 2.0376 86.69 87.95

STATOR

%SPAN	DIA-1 IN	DIA-2 IN	V-1 FT/SEC	V-2 FT/SEC	VH-1 FT/SEC	VH-2 FT/SEC	VO-1 FT/SEC	VO-2 FT/SEC	B-1 DEGREE	B-2 DEGREE	B-1 DEGREE	B-2 DEGREE	V-1 FT/SEC	V-2 FT/SEC	VH-1 FT/SEC	VH-2 FT/SEC	VO-1 FT/SEC	VO-2 FT/SEC	U-1 FT/SEC	U-2 FT/SEC
6	20.409	21.989	1040.0	681.6	703.7	681.6	785.8	-2.2	47.42	-0.1	17.52	56.77	738.0	1243.8	822.2	1098.5	968.0	1098.5	968.0	1098.5
10	21.008	21.961	1063.0	684.1	694.8	683.5	784.5	-25.4	46.26	-2.25	22.82	59.01	754.0	1269.8	822.2	1098.5	1017.0	1098.5	1017.0	1063.0
15	21.589	22.432	948.3	633.0	681.9	681.9	687.5	-38.9	45.24	-3.52	27.68	60.67	770.4	1290.2	857.6	1124.8	1045.1	1290.2	1045.1	1085.9
30	23.214	23.902	877.9	597.7	595.6	597.6	684.9	-1.07	47.28	-1.07	39.06	62.91	767.4	1312.3	887.7	1168.8	1125.6	1312.3	1125.6	1157.1
50	25.601	25.893	878.8	616.4	608.8	616.3	633.7	-7.5	46.15	-7.4	44.84	63.96	856.8	1403.9	805.6	1261.4	1239.3	1403.9	1239.3	1253.5
70	27.818	27.982	869.1	623.2	612.4	623.2	616.8	-4.2	45.21	-5.37	50.00	65.33	952.7	1493.2	723.9	1358.9	1346.7	1493.2	1346.7	1399.7
85	29.914	29.856	901.8	623.1	610.8	622.2	659.4	33.1	47.37	3.05	52.11	66.22	998.4	1543.3	754.7	1412.2	1448.1	1543.3	1448.1	1448.3
90	30.382	30.293	885.8	597.4	577.9	596.5	671.4	32.6	49.28	3.13	54.14	67.41	986.4	1553.0	759.4	1433.9	1470.8	1553.0	1470.8	1468.5

%SPAN	INCS DEGREE	INCH DEGREE	DEV DEGREE	TURN CAMBER	OMEGA-A DEGREE	OMEGA-B DEGREE	D-FAC	OMEGA-B TOTAL	LOSS-P TOTAL	LOSS-P PROFILE	POZ	EFF-P TOTAL	EFF-P TOTAL	EFF-P TOTAL	M-1	M-2	M-1	M-2	M-1	M-2
6	1.28	8.20	12.40	47.44	53.91	0.000	5231	1.909	0.073	0.073	0.9221	0.000	0.000	7456	6902	6902	6902	6902	6902	6902
10	1.76	3.69	7.20	46.44	53.88	0.000	5351	1.806	0.046	0.046	0.9261	0.000	0.000	7456	6902	6902	6902	6902	6902	6902
15	1.95	3.89	7.34	48.76	52.34	0.000	5391	1.785	0.061	0.061	0.9353	0.000	0.000	7456	6902	6902	6902	6902	6902	6902
30	4.82	7.81	10.14	46.35	50.67	0.000	5264	0.0792	0.217	0.217	0.9713	0.000	0.000	8658	7467	4939	6409	1.0644	6409	1.0644
50	5.45	8.58	11.28	46.88	49.56	0.000	5211	0.2268	0.288	0.288	0.9713	0.000	0.000	8593	7421	5063	7208	1.1931	7208	1.1931
70	5.58	8.80	12.88	46.77	49.85	0.000	5202	0.2740	0.258	0.258	0.9769	0.000	0.000	8742	7280	5091	7945	1.2199	7945	1.2199
85	6.27	9.58	18.10	43.51	51.99	0.000	5116	0.426	0.098	0.098	0.9659	0.000	0.000	7800	7502	5112	8299	1.2400	8299	1.2400
90	7.68	11.01	20.53	44.32	53.63	0.000	5577	0.478	0.524	0.524	0.9545	0.000	0.000	7780	7457	5008	8286	1.2402	8286	1.2402
95	9.55	12.92	22.82	46.15	56.02	0.000	5961	0.556	0.556	0.556	0.9542	0.000	0.000	7636	7287	4773	8091	1.2408	8091	1.2408

NGOR-1 TO/TO PO/PO EFF-P
INLET INLET INLET
W/A-1
LBM/SEC
SOFT

11095 173.71 1.2598 1.9589 81.40 83.08 39.04

TABLE 10.9
Blade Element and Overall Performance with Uniform Inlet, Alternate Method
100% of Design Speed

ROTOR

%SPAN	IN	DIA-2	DIA-1	IN	V-1	V-2	VM-1	VM-2	V0-1	V0-2	B-1		B-2		B'-1		B'-2		R1-1	R1-2	V1-1	V1-2	V0'-1	V0'-2	U-1	U-2	
											FT/SEC	DEGREE	LOSS-P	DEGREE	LOSS-P	DEGREE	PO2/	PO1/									DEGREE
5	17.467	19.769	595.7	975.9	595.7	621.4	.0	752.5	.0	50.05	54.02	18.16	1033.9	654.1	-845.0	-203.9	845.0	956.4									
10	18.467	20.408	610.6	932.0	610.8	598.5	.0	714.4	.0	50.05	55.64	24.51	1082.2	657.8	-893.4	-272.9	893.4	987.1									
15	19.467	21.047	625.4	922.4	625.4	631.0	.0	672.9	.0	46.84	56.41	28.68	1130.5	719.4	-941.4	-345.4	941.4	1014.2									
30	22.314	22.964	660.8	857.5	660.8	610.7	.0	601.9	.0	44.58	58.53	39.80	1265.7	795.2	-1079.5	-509.1	1079.5	1111.0									
50	25.791	25.520	681.0	834.4	681.0	605.2	.0	574.4	.0	43.50	61.37	47.46	1421.5	895.9	-1247.7	-660.2	1247.7	1234.6									
70	28.954	28.076	670.5	762.8	670.3	567.9	.0	509.2	.0	41.88	64.43	56.21	1552.9	1021.5	-1400.8	-849.0	1400.8	1354.6									
85	31.295	29.993	644.9	731.2	644.9	528.5	.0	505.2	.0	43.72	66.93	60.81	1645.7	1083.5	-1514.0	-945.8	1514.0	1451.0									
90	31.883	30.630	637.5	707.3	637.5	483.4	.0	516.0	.0	46.90	67.54	63.42	1669.0	1080.4	-1542.5	-965.9	1542.5	1511.8									
95	32.499	31.271	631.7	656.2	631.7	400.3	.0	519.9	.0	52.80	68.11	68.04	1694.4	1070.6	-1572.3	-992.9	1572.3	1512.0									
INCS																											
DEGREE																											
INCM																											
DEV																											
TURN																											
CAMBER																											
OMEGA-B																											
D-FAC																											
OMEGA-B																											
LOSS-P																											
TOTAL																											
PROFILE																											
PO2/																											
PO1/																											
DEGREE																											
DEGREE																											
EFF-P																											
EFF-AD																											
EFF-P																											
TOTAL																											
STATIC																											
M-1																											
M-2																											
M'-1																											
M'-2																											
U-1																											
U-2																											

TO/TO PO/PO EFF-AD EFF-P
INLET INLET INLET INLET
1.2264 1.8926 88.23 89.23

STATOR

%SPAN	IN	DIA-1	DIA-2	IN	V-1	V-2	VM-1	VM-2	V0-1	V0-2	B-1		B-2		B1-1		B1-2		V1-1	V1-2	V0'-1	V0'-2	U-1	U-2			
											FT/SEC	DEGREE	LOSS-P	DEGREE	LOSS-P	DEGREE	PO2/	PO1/							DEGREE	DEGREE	FT/SEC
5	20.409	21.489	1029.7	794.6	727.4	794.6	727.4	794.6	728.9	-6.5	45.06	19.56	52.78	772.0	1313.6	-258.5	-1046.1	987.4	1039.6								
15	21.008	21.961	989.5	762.7	705.7	749.0	740.2	655.6	-25.1	44.51	-1.90	24.57	54.97	1328.3	322.7	-1087.6	1016.3	1062.4									
30	23.314	23.942	923.0	722.2	707.1	721.8	721.8	593.2	-34.6	41.96	-2.67	28.06	56.53	826.4	1342.4	-386.4	-1119.8	1044.4	1085.2								
50	25.601	25.893	908.3	727.3	705.2	727.1	727.1	572.5	-16.1	39.99	-1.94	37.08	58.56	886.6	1384.0	-534.7	-1180.8	1127.9	1154.3								
70	27.818	27.912	851.0	674.8	687.3	674.8	674.8	514.1	-16.7	36.80	-1.41	50.43	63.73	1079.0	1524.0	-831.7	-1366.5	1345.8	1349.9								
85	29.408	29.382	851.0	628.1	677.2	628.1	628.1	515.3	7.8	37.27	1.66	54.63	66.96	1126.9	1550.5	-918.8	-1426.8	1447.2	1444.4								
90	29.914	29.856	839.6	606.9	652.4	606.9	606.9	528.4	17.6	39.02	1.66	54.63	66.96	1126.9	1550.5	-918.8	-1426.8	1447.2	1444.4								
95	30.382	30.293	806.0	566.3	602.8	566.3	566.3	535.1	10.1	41.59	1.02	57.18	68.74	1112.3	1561.7	-934.8	-1455.5	1469.8	1465.5								
INCS																											
DEGREE																											
INCM																											
DEV																											
TURN																											
CAMBER																											
OMEGA-B																											
D-FAC																											
OMEGA-B																											
LOSS-P																											
TOTAL																											
PROFILE																											
PO2/																											
PO1/																											
DEGREE																											
DEGREE																											
EFF-P																											
EFF-AD																											
EFF-P																											
TOTAL																											
STATIC																											
M-1																											
M-2																											
M'-1																											
M'-2																											
U-1																											
U-2																											
NCORR																											
WCORR																											
TO/TO																											
PO/PO																											
EFF-AD																											
EFF-P																											
INLET																											
INLET																											
INLET																											
LBM/SEC																											
RPM																											
LBM/SEC																											
SOFT																											
11088. 183.12 1.2264 1.8441 84.32 85.30 41.15																											

TABLE 10.10
Blade-Efficient and Overall Performance with Uniform Inlet, Alternate Method
100% of Design Speed

ROTOR

SPAN IN	DIA-1	DIA-2	V-1	V-2	V-1	V-2	V0-1	V0-2	R-1	R-2	B1-1	B1-2	V1-1	V1-2	V0-1	V0-2	U-1	U-2
%	IN	IN	FEET	FEET	FEET/SEC	FEET/SEC	FEET/SEC	FEET/SEC	DEGREE	DEGREE	DEGREE	DEGREE	FEET/SEC	FEET/SEC	FEET/SEC	FEET/SEC	FT/SEC	FT/SEC
5	17.467	19.769	581.9	964.1	541.9	521.1	0	776.2	0	51.34	55.45	15.18	1026.1	646.7	845.1	180.3	805.1	956.5
10	18.467	20.408	596.6	939.2	546.6	527.5	0	732.8	0	51.28	56.27	23.43	1074.4	640.5	893.5	254.6	887.5	987.4
15	19.467	21.147	610.0	918.0	550.6	530.6	0	695.6	0	51.75	57.07	30.06	1122.2	648.0	941.3	324.9	941.9	1019.3
20	22.314	22.964	641.0	844.9	641.0	587.2	0	639.1	0	48.74	59.30	44.51	1255.6	732.9	1070.6	476.0	1070.6	1111.1
30	25.791	25.520	561.7	533.1	661.7	560.2	0	616.6	0	47.75	62.06	47.81	1412.4	834.3	1247.0	618.1	1247.0	1234.4
40	28.954	28.978	566.8	492.0	656.8	580.9	0	588.9	0	46.03	64.88	55.87	1547.2	962.7	1440.0	748.9	1440.0	1354.4
50	31.295	29.993	634.7	790.4	634.7	531.9	0	588.9	0	47.71	67.26	58.46	1641.8	1016.7	1514.2	866.5	1514.2	1451.2
60	31.883	30.630	627.3	780.7	627.3	500.8	0	598.9	0	50.10	67.87	60.44	1665.3	1015.2	1542.6	883.1	1542.6	1482.0
70	32.499	31.271	620.8	410.4	0	605.3	0	55.87	0	55.87	68.46	65.67	1690.5	996.2	1572.4	907.7	1572.4	1513.0

SPAN IN	INCM	DEV	TURN	CAMBER	OMEGA-B	D-FAC	OMEGA-B	LOSS-P	LOSS-P	PO2/	EFF-P	EFF-P	EFF-P	EFF-P	EFF-P	EFF-P	M-1	M-1	M-1	M-1
%	IN	IN	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	TOTAL	PROFILE	POL	TOTAL	TOTAL	STATIC	STATIC	STATIC	STATIC				
5	6.47	13.27	39.27	44.83	0.131	54.61	0.359	0.076	0.048	2.0803	0.790	0.767	0.9673	0.5365	0.570	0.473	0.576	0.576	0.576	0.576
10	6.55	13.79	32.83	43.55	0.161	56.88	0.702	0.148	0.14	2.0122	0.9566	0.920	0.9384	0.5514	0.656	0.664	0.664	0.664	0.664	0.664
15	4.8	6.45	13.95	27.01	34.14	0.204	57.68	0.872	0.191	0.139	1.9600	0.908	0.9348	0.5230	0.564	0.621	0.621	0.621	0.621	0.621
30	1.30	5.37	10.77	18.80	24.19	0.422	55.85	0.785	0.153	0.066	1.9556	0.9385	0.9323	0.5230	0.564	0.621	0.621	0.621	0.621	0.621
50	2.40	5.11	4.45	14.26	14.61	0.777	54.19	0.992	0.203	0.045	2.0039	0.9082	0.8987	0.6140	0.702	0.702	0.702	0.702	0.702	0.702
70	3.48	5.23	4.48	9.81	9.05	1.101	50.04	1.050	0.204	0.042	1.9951	0.904	0.8701	0.6140	0.702	0.702	0.702	0.702	0.702	0.702
85	5.86	5.13	4.28	8.80	7.95	1.325	50.70	1.586	0.301	0.053	2.0193	0.8336	0.8222	0.589	0.653	0.653	0.653	0.653	0.653	0.653
90	4.02	5.11	5.29	7.43	7.61	1.398	52.03	1.973	0.359	0.099	2.0120	0.7970	0.7758	0.589	0.653	0.653	0.653	0.653	0.653	0.653
95	4.24	5.15	9.80	2.79	7.44	1.503	54.25	2.502	0.387	0.156	1.9917	0.7415	0.7159	0.589	0.653	0.653	0.653	0.653	0.653	0.653

STATOR

SPAN IN	DIA-1	DIA-2	V-1	V-2	V-1	V-2	V0-1	V0-2	R-1	R-2	B1-1	B1-2	V1-1	V1-2	V0-1	V0-2	U-1	U-2
%	IN	IN	FEET	FEET	FEET/SEC	FEET/SEC	FEET/SEC	FEET/SEC	DEGREE	DEGREE	DEGREE	DEGREE	FEET/SEC	FEET/SEC	FEET/SEC	FEET/SEC	FT/SEC	FT/SEC
5	20.409	21.489	1035.3	698.7	711.7	698.7	751.9	-5.9	46.57	-2.70	18.31	56.25	749.7	1257.6	-235.6	1045.6	987.5	1030.7
10	21.808	21.961	583.2	670.6	678.4	669.8	711.7	-31.5	46.37	-2.70	24.19	58.52	743.8	1283.0	-304.7	1094.0	1016.5	1062.6
15	21.589	22.432	939.5	649.2	652.3	647.9	676.2	-40.0	46.03	-3.53	29.44	60.07	749.3	1298.6	-368.4	1125.4	1046.6	1085.4
30	23.314	23.302	903.0	623.4	646.4	623.3	626.3	-12.1	44.09	-1.11	37.82	61.92	818.3	1324.4	-501.8	1168.6	1124.0	1156.5
50	25.601	25.193	899.3	651.7	655.5	651.7	615.7	-9.0	43.21	-1.79	43.54	62.69	904.3	1420.2	-622.0	1261.8	1234.7	1252.8
70	27.814	27.302	879.4	646.6	665.8	646.6	574.5	-22.8	40.79	-2.02	48.20	64.79	1019.0	1517.3	-771.5	1372.8	1345.9	1350.0
85	29.408	29.382	901.9	649.3	675.6	649.0	597.5	19.6	41.49	1.73	50.70	65.16	1066.6	1544.9	-825.4	1402.0	1422.9	1421.6
90	29.914	29.956	901.0	642.8	658.9	641.6	614.5	38.5	43.01	3.44	51.65	65.47	1062.0	1545.5	-832.8	1406.0	1447.4	1444.6
95	30.382	30.293	969.7	602.8	606.7	602.1	623.2	30.3	45.77	2.88	54.38	67.24	1041.8	1556.6	-846.8	1435.4	1470.0	1465.7

SPAN	JEGEE	INCM	DEV	TURN	CAMBER	OMEGA-R	D-FAC	OMEGA-B	LOSS-P	LOSS-P	PO2/	EFF-P	EFF-P	EFF-P	EFF-P	EFF-P	M-1	M-1	M-1	M-1
%	IN	IN	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	TOTAL	PROFILE	POL	TOTAL	TOTAL	STATIC	STATIC	STATIC				
5	3.50	3.43	11.93	47.06	55.90	0.049	50.25	0.132	0.330	0.318	0.9459	0.000	0.000	0.813	0.866	0.5814	0.6476	1.0465	1.0465	1.0465
10	1.18	4.12	8.74	49.08	53.88	0.062	50.70	0.901	0.230	0.214	0.9662	0.000	0.000	0.879	0.874	0.5583	0.6420	1.0681	1.0681	1.0681
15	1.59	4.53	7.32	49.56	52.34	0.076	50.50	0.487	0.127	0.107	0.9830	0.000	0.000	0.927	0.907	0.5404	0.6482	1.0899	1.0899	1.0899
30	1.67	4.67	10.11	45.20	50.67	0.105	50.91	0.661	0.156	0.156	0.9786	0.000	0.000	0.888	0.888	0.5385	0.7016	1.0906	1.0906	1.0906
50	2.54	5.67	11.22	44.00	49.54	0.129	48.70	0.698	0.214	0.214	0.9777	0.000	0.000	0.887	0.887	0.5385	0.7631	1.1734	1.1734	1.1734
70	1.19	4.42	11.42	42.81	49.85	0.139	48.85	0.500	0.156	0.156	0.9846	0.000	0.000	0.905	0.905	0.5385	0.8592	1.2512	1.2512	1.2512
85	2.04	5.36	17.63	39.76	52.00	0.158	50.91	0.840	0.293	0.293	0.9735	0.000	0.000	0.856	0.856	0.5385	0.8933	1.2618	1.2618	1.2618
90	3.27	6.60	20.89	19.57	53.62	0.192	51.80	0.823	0.292	0.292	0.9743	0.000	0.000	0.879	0.879	0.5221	0.8777	1.2553	1.2553	1.2553
95	5.93	9.30	22.57	12.89	56.03	0.247	55.31	0.685	0.247	0.247	0.9900	0.000	0.000	0.8951	0.8951	0.5221	0.8624	1.2555	1.2555	1.2555

NCORR W/CORR TO/PO EFF-AD EFF-P WCI/A1
INLET INLET INLET INLET INLET INLET INLET
NPM LBW/SEC % % SOFT
11089. 18J.44 1.2478 1.9468 84.51 85.90 40.55

TABLE 10.11
Blade-Element and Overall Performance with Uniform Inlet, Alternate Method
100% of Design Speed

ROTOR

XSPAN	DIA-1	DIA-2	V-1	V-2	V-1	V-2	VM-1	VM-2	VM-1	VM-2	R-1	R-2	B1-1	B1-2	V1-1	V1-2	VO1-1	VO1-2	U-1	U-2
5	17.467	19.769	566.0	989.7	565.0	598.9	.0	786.6	.0	52.71	56.20	15.89	10.17	6	622.8	845.7	-170.5	845.7	957.2	957.2
10	18.467	20.409	580.1	942.8	544.1	581.6	.0	742.0	.0	51.91	57.82	22.94	10.65	8	631.7	874.1	-246.1	894.1	944.1	944.1
15	19.467	21.47	592.9	887.2	522.9	542.7	.0	701.7	.0	52.27	57.82	30.29	11.3	5	629.0	902.5	-317.3	982.5	1019.0	1019.0
30	22.314	22.964	622.5	843.9	622.5	542.7	.0	646.2	.0	49.98	60.05	40.62	12.46	9	715.1	1080.4	-445.6	1040.4	1111.8	1111.8
50	25.791	25.520	642.2	829.2	642.2	541.7	.0	626.4	.0	49.15	62.78	42.34	14.4	2	815.3	1248.7	-609.2	1248.7	1355.6	1355.6
70	28.954	28.176	630.7	791.9	630.7	528.0	.0	580.5	.0	48.10	55.51	44.0	15.48	5	834.3	1401.9	-769.4	1401.9	1500.3	1500.3
85	31.295	29.993	619.2	807.0	619.2	529.5	.0	609.0	.0	48.99	57.87	46.36	16.36	9	895.7	1515.2	-843.2	1515.2	1632.2	1632.2
90	31.583	30.330	612.2	800.8	612.2	501.6	.0	624.2	.0	51.21	68.37	59.71	16.60	6	994.7	1543.7	-858.9	1543.7	1683.0	1683.0
95	32.499	31.271	605.6	786.5	605.6	415.7	.0	632.0	.0	56.67	68.95	64.76	16.86	0	975.2	1573.5	-882.1	1573.5	1514.0	1514.0

STATOR

XSPAN	I-ACS	INCM	DEV	TURN	CAMER	OMEGA-B	D-FAC	OMEGA-B	LOSS-P	PO2	EFF-P	EFF-AD	EFF-P	M-1	V-2	M-1	M-1	M-1	M-1
5	.79	7.22	14.22	40.31	44.83	.0150	.5683	.0645	.0136	.0104	2.0767	.9645	.9607	.9439	.5210	.8503	.9376	.5356	.5356
10	.97	7.41	13.29	34.09	43.56	.0181	.5755	.0724	.0153	.0167	1.9624	.9564	.9517	.9357	.5355	.8080	.9861	.5414	.5414
15	1.23	7.22	13.78	27.54	39.14	.0222	.5925	.1026	.0213	.0231	.9252	.9321	.9252	.9107	.5757	.7568	1.0387	.5365	.5365
30	2.04	6.13	10.92	19.43	24.23	.0439	.5681	.0862	.0176	.0287	1.9665	.9310	.9240	.9181	.5752	.7155	1.1513	.6064	.6064
50	3.11	5.83	5.99	14.45	14.62	.0793	.5548	.1099	.0223	.0263	2.0128	.9006	.8903	.8888	.5944	.6955	1.2943	.6847	.6847
70	3.94	5.86	4.68	10.92	9.04	.1144	.5312	.1245	.0230	.0232	2.0154	.8748	.8619	.8654	.5921	.6609	1.4199	.7784	.7784
85	4.38	5.66	3.66	9.90	7.92	.1359	.5237	.1657	.0320	.0265	2.0714	.8328	.8147	.8170	.5750	.6660	1.5041	.8217	.8217
90	4.51	5.61	4.55	8.66	7.60	.1441	.5370	.2023	.0377	.0319	2.0710	.7997	.7781	.7824	.5666	.6568	1.5301	.8154	.8154
95	4.73	5.64	8.88	4.19	7.43	.1517	.5596	.2539	.0406	.0166	2.0160	.7480	.7220	.7359	.5594	.6151	1.5541	.7930	.7930

STATOR

XSPAN	DIA-1	DIA-2	V-1	V-2	VM-1	VM-2	VM-1	VM-2	R-1	R-2	B1-1	B1-2	V1-1	V1-2	VO1-1	VO1-2	U-1	U-2
5	20.409	21.489	1026.0	680.0	687.1	580.0	761.9	-7.1	47.96	-6.0	18.22	57.01	723.4	1248.9	-226.2	1047.7	988.1	1040.4
10	21.006	21.961	982.2	651.7	667.4	651.1	720.6	-27.0	47.19	-2.39	23.96	59.15	730.5	1270.1	-296.5	1090.3	1017.1	1083.3
15	21.589	22.432	931.0	630.6	631.4	629.4	684.1	-46.0	47.29	-3.46	29.76	60.75	727.6	1288.4	-361.2	1124.1	1045.5	1086.1
30	23.314	23.902	894.9	603.4	629.5	637.0	-13.1	45.39	-1.24	38.04	62.73	798.0	1316.7	-491.8	1170.3	1128.8	1157.3	
50	25.601	25.393	891.2	629.5	634.6	629.5	695.7	-7.0	44.60	-6.4	44.04	63.47	882.9	1409.1	-613.8	1260.6	1258.5	1257.3
70	27.818	27.902	875.7	636.6	642.0	636.6	593.5	-17.7	43.55	-1.60	49.48	65.06	988.3	1509.4	-751.3	1366.7	1346.9	1350.9
85	29.408	29.382	913.5	649.5	667.9	647.9	623.2	25.6	43.02	2.26	50.16	65.12	1042.7	1539.9	-807.7	1397.0	1423.8	1422.6
90	29.914	29.556	916.8	639.8	655.0	638.4	641.4	41.9	44.40	3.76	50.93	65.54	1039.4	1542.0	-807.0	1403.6	1448.3	1445.5
95	30.382	30.293	887.6	605.9	603.6	605.0	650.7	34.2	47.15	3.23	53.65	67.11	1018.4	1555.0	-820.3	1432.5	1471.0	1466.7

STATOR

XSPAN	I-ACS	INCM	DEV	TURN	CAMER	OMEGA-B	D-FAC	OMEGA-B	LOSS-P	PO2	EFF-P	EFF-AD	EFF-P	M-1	V-2	M-1	M-1	M-1
5	1.82	4.75	11.81	44.56	55.90	.0073	.5189	.1211	.0301	.0283	.9515	.0000	.8334	.8768	.5641	.6247	1.0360	1.0360
10	2.14	5.07	9.06	49.59	53.88	.0090	.5268	.0999	.0255	.0234	.9626	.0000	.8718	.8327	.5410	.6273	1.0543	1.0543
15	2.85	5.79	7.39	50.75	52.35	.0107	.5231	.0400	.0105	.0077	.9863	.0000	.9390	.7938	.5234	.6284	1.0604	1.0604
30	2.97	5.97	9.98	46.63	50.67	.0146	.5273	.0731	.0205	.0164	.9766	.0000	.8825	.7632	.4993	.6826	1.0805	1.0805
50	3.92	7.06	11.38	45.23	49.54	.0253	.5100	.0824	.0252	.0175	.9741	.0000	.8664	.7501	.5182	.7458	1.1600	1.1600
70	3.24	6.47	11.85	44.45	49.84	.0227	.5044	.0604	.0200	.0125	.9817	.0000	.8952	.7370	.5226	.8227	1.2389	1.2389
85	3.60	6.92	18.16	40.75	51.99	.0236	.5189	.0439	.0356	.0359	.9599	.0000	.9000	.7623	.5270	.8700	1.2515	1.2515
90	4.78	8.11	21.23	40.64	53.62	.0276	.5347	.0402	.0497	.0399	.9553	.0000	.9000	.7858	.5169	.8645	1.2458	1.2458
95	7.35	10.71	22.92	43.92	56.02	.0347	.5683	.1253	.0451	.0326	.9625	.0000	.8067	.7341	.4863	.8400	1.2480	1.2480

NCORR TO/TO PO/PO EFF-AD EFF-P WC1/A1
INLET INLET INLET INLET INLET
RPM LBW/SEC % %
11096. 177.14 1.2547 1.9586 83.02 84.55. 39.81

TABLE 11.1
Blade-Element and Overall Performance with Uniform Inlet
105% of Design Speed

ROTOR

%SPAN	DIA-1 IN	DIA-2 IN	V-1	V-2	VN-1	VN-2	V0-1	V0-2	B-1	B-2	B1-1	B1-2	V1-1	V1-2	V01-1	V01-2	U-1	U-2
	IN	IN	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC
5	17.467	19.769	630.3	1062.9	630.3	744.4	0	756.0	0	45.55	54.65	18.36	1089.5	784.3	-888.7	-247.0	888.7	1005.8
10	18.467	20.468	647.6	1013.6	647.6	790.7	0	732.5	0	46.27	55.42	23.58	1141.1	764.8	-939.6	-305.8	939.6	1038.3
15	19.167	21.067	663.5	980.0	663.5	830.8	0	707.4	0	46.20	56.18	28.15	1192.1	769.9	-990.4	-363.4	990.4	1078.0
30	22.3.4	22.964	700.5	921.8	700.5	890.8	0	621.4	0	42.38	56.32	38.74	1334.0	873.7	-1135.3	-547.0	1135.3	1168.4
50	26.954	26.976	783.8	846.2	783.8	966.2	0	561.2	0	40.11	61.23	47.84	1497.0	894.8	-1121.2	-737.2	1121.2	1298.4
85	31.295	29.993	675.7	723.4	675.7	858.7	0	461.7	0	39.68	67.61	64.79	1734.4	1201.3	-1592.2	-1064.3	1592.2	1526.0
90	31.883	30.630	648.3	696.3	648.3	818.7	0	469.5	0	42.50	67.61	64.79	1734.4	1203.7	-1622.1	-1088.9	1622.1	1553.4
95	32.499	31.271	662.3	658.1	662.3	856.5	0	471.3	0	45.92	68.17	67.62	1781.2	1209.2	-1653.5	-1119.7	1653.5	1591.0

%SPAN	INCS	INCH	DEV	TURN	CAMBER	OMEGA-B	D-FAC	OMEGA-B	LOSS-P	LOSS-P	POZ/	POZ/	EFF-AD	EFF-P	M-1	M-2	M1-1	M1-2
			DEGREE	DEGREE	DEGREE	DEGREE		DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE
5	-75	5.68	16.49	36.29	47.12	0155	0426	1007	0210	0177	2.0372	9405	0382	0994	5850	9232	1.0131	6812
10	-50	5.79	13.95	31.84	39.99	0211	0048	1595	0336	0291	1.9464	0877	0872	0877	6038	8741	1.0685	6595
15	-38	5.49	11.64	28.03	34.03	0288	5023	1769	0375	0313	1.9499	0768	0845	0315	6196	8413	1.1189	6609
30	42	4.40	9.03	19.59	24.21	0592	4723	1892	0272	0186	1.9177	0803	0775	0660	6555	7886	1.2552	7474
50	3.07	4.34	5.58	13.39	14.67	1042	4494	1354	0277	0060	1.8428	0606	0477	0482	6730	7401	1.4059	8448
70	5.07	4.78	7.79	8.20	9.16	1435	7065	1545	0275	0017	1.7423	0670	0211	0211	6645	6392	1.5310	9401
85	3.79	4.87	8.25	4.62	8.03	1691	4000	1691	0320	0037	1.7065	0488	0292	0292	6290	6065	1.6074	10071
90	3.79	4.87	8.25	4.62	8.03	1691	4000	1691	0320	0037	1.7065	0488	0292	0292	6290	6065	1.6074	10071
95	3.79	4.87	11.98	4.35	7.46	1888	4185	2660	0377	0110	1.6353	0515	0266	0266	6151	5432	1.6539	1.0011

TO/TO PO/PO EFF-AD EFF-P
INLET INLET INLET INLET
1.2310 1.0495 82.07 83.53

STATOR

%SPAN	DIA-1 IN	DIA-2 IN	V-1	V-2	VN-1	VN-2	V0-1	V0-2	B-1	B-2	B1-1	B1-2	V1-1	V1-2	V01-1	V01-2	U-1	U-2
	IN	IN	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC
5	20.409	21.449	1135.3	982.4	865.3	979.0	735.0	-82.2	40.34	-4.80	19.32	50.21	917.0	1529.8	-303.4	-1173.5	1038.4	1093.3
10	21.008	21.961	1099.3	963.1	825.0	959.8	711.6	-79.5	40.78	-4.73	23.42	51.27	899.2	1534.2	-357.3	-1196.8	1066.8	1117.3
15	21.589	22.432	1058.6	947.3	803.2	948.1	689.6	-78.5	40.65	-4.73	26.96	52.26	901.5	1542.5	-408.8	-1219.8	1098.4	1141.3
30	23.314	23.902	1008.6	911.8	799.1	908.7	612.0	-75.0	37.44	-4.72	35.67	54.85	984.3	1578.9	-574.1	-1291.0	1186.2	1216.1
50	25.601	25.893	965.9	857.1	787.4	854.0	559.4	-72.8	35.39	-4.68	43.31	58.83	1083.3	1631.8	-743.1	-1390.2	1302.8	1317.4
70	27.408	27.902	878.8	774.8	737.3	788.4	478.0	-71.7	35.95	-5.33	51.61	62.74	1192.6	1677.7	-937.4	-1491.3	1415.3	1419.8
85	29.408	29.382	871.4	726.9	733.1	725.2	471.0	-69.5	34.72	-3.91	54.43	64.85	1260.4	1706.2	-1025.2	-1544.4	1496.2	1494.9
90	29.914	29.855	857.4	715.4	709.7	714.5	461.1	-64.9	34.14	-2.79	55.71	65.31	1259.8	1710.3	-1040.9	-1553.9	1528.0	1519.8
95	30.382	30.293	835.2	675.3	679.8	675.1	445.2	-64.1	35.52	-1.20	57.34	66.54	1259.7	1695.6	-1060.6	-1555.4	1543.8	1541.2

%SPAN	INCS	INCH	DEV	TURN	CAMBER	OMEGA-B	D-FAC	OMEGA-B	LOSS-P	LOSS-P	POZ/	POZ/	EFF-AD	EFF-P	M-1	M-2	M1-1	M1-2
			DEGREE	DEGREE	DEGREE	DEGREE		DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE
5	-5.03	-2.70	7.61	45.14	55.90	0000	3100	1916	0475	0375	9098	0000	0000	4462	9486	8429	8002	1.3126
10	-4.89	-2.35	6.71	45.51	53.67	0000	2980	1480	0377	0477	9347	0000	0000	5024	9413	8244	7628	1.3133
15	-3.82	-1.87	6.19	45.40	52.43	0000	2920	1265	0330	0330	9467	0000	0000	5335	9149	8097	7877	1.3185
30	-5.06	-2.06	6.51	42.16	50.68	0000	2839	1231	0345	0345	9519	0000	0000	4787	8686	7791	8583	1.3590
50	-5.34	-2.21	7.17	40.26	49.61	0000	2812	1165	0339	0339	9535	0000	0000	3495	8286	7271	8358	1.3844
85	-6.73	-3.49	8.16	38.28	49.92	0000	2807	1490	0492	0492	9535	0000	0000	4616	7524	6524	7824	1.4192
90	-5.41	-2.08	14.61	36.92	53.37	0000	3797	1503	0506	0506	9528	0000	0000	5634	7276	6096	1.0744	1.4308
95	-4.24	-1.88	18.44	36.72	56.03	0000	4074	1709	0649	0649	9493	0000	0000	5607	7056	5601	1.0423	1.4063

MCOR-1 MCOR-1 TO/TO PC/PO EFF-AD EFF-P
INLET INLET INLET INLET
11660 189.36 1.2310 1.7391 73.82 75.78
W/A
LBM/SEC
RPM
SGFT
42.55

TABLE 11.3
Blade-Element and Overall Performance with Uniform Inlet
105% of Design Speed

ROTOR

%SPAN	DIA-1		V-1		V-2		VM-1		VM-2		VO-1		VO-2		B-1		B-2		B1-1		B1-2		V1-1		V1-2		V01-1		V01-2		U-1		U-2			
	IN	IN	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE		
5	17.467	19.769	625.4	1053.2	625.4	700.3	0	766.6	0	48.32	54.84	17.31	1046.0	733.5	-887.9	-218.3	867.9	1004.9																		
10	18.467	20.408	642.5	1008.4	642.5	676.1	0	748.6	0	47.89	55.61	17.31	1137.5	738.0	-958.7	-289.3	934.7	1037.4																		
15	19.467	21.047	658.4	958.9	658.4	645.8	0	748.7	0	47.45	56.36	29.17	1188.6	740.5	-989.5	-361.1	984.5	1069.8																		
30	22.314	22.964	694.3	899.7	694.3	621.2	0	641.1	0	45.44	58.53	39.78	1328.9	822.0	-1134.2	-526.2	1134.2	1167.3																		
50	25.781	25.520	712.4	884.0	712.4	633.9	0	616.1	0	44.18	61.30	47.00	1492.1	931.4	-1315.0	-681.1	1311.0	1297.2																		
7	28.284	28.024	694.3	774.7	694.3	557.5	0	538.0	0	43.28	64.74	57.50	1627.3	1042.7	-1471.8	-884.5	1591.6	1324.6																		
85	31.295	29.993	668.2	780.0	668.2	505.8	0	540.0	0	46.89	67.27	62.81	1624.6	1107.0	-1590.8	-984.5	1591.6	1324.6																		
90	31.883	30.630	659.2	721.3	659.2	469.8	0	547.3	0	49.37	67.86	65.05	1749.6	1113.7	-1620.6	-1009.7	1620.6	1537.0																		
95	32.499	31.271	653.8	695.1	653.8	422.0	0	552.3	0	49.62	68.41	67.86	1776.6	1119.6	-1682.0	-1037.2	1652.0	1580.5																		

TO/TO PO/PO EFF-AD EFF-P
INLET INLET INLET INLET

1.2523 1.9755 84.98 86.36

STATOR

%SPAN	DIA-1		V-1		V-2		VM-1		VM-2		VO-1		VO-2		B-1		B-2		B1-1		B1-2		V1-1		V1-2		V01-1		V01-2		U-1		U-2			
	IN	IN	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE		
5	20.409	21.469	1110.4	835.1	807.7	835.0	761.9	-14.2	43.33	42.89	-2.28	23.55	55.03	854.0	1401.2	-341.0	-1148.1	1067.9	1116.3																	
10	21.008	21.961	1068.0	803.7	782.5	803.0	726.9	-31.6	42.89	42.89	-2.72	28.36	56.53	856.8	1411.5	-406.5	-1177.3	1097.4	1140.2																	
15	21.589	22.432	1021.5	779.3	752.4	778.4	690.8	-37.1	42.55	42.55	-3.37	37.01	58.60	919.2	1444.4	-453.5	-1232.9	1185.1	1215.0																	
30	23.314	23.902	968.0	752.6	733.6	752.4	651.6	-16.8	40.72	40.72	-4.31	42.98	60.94	1008.1	1525.1	-687.3	-1333.0	1301.3	1316.2																	
50	25.601	25.893	959.0	740.7	736.6	740.5	614.1	-18.8	39.81	39.81	-5.31	51.90	65.85	1107.3	1588.8	-871.4	-1445.1	1414.0	1416.3																	
70	27.818	27.922	872.4	680.6	683.8	660.1	592.6	-28.8	38.47	38.47	-6.31	55.04	67.67	1152.0	1603.8	-984.1	-1483.5	1494.8	1493.5																	
85	29.408	29.382	859.7	609.4	609.4	660.0	550.7	10.0	39.84	39.84	-2.30	56.30	68.57	1133.7	1605.1	-959.8	-1494.0	1520.6	1517.6																	
90	29.914	29.856	851.1	587.0	640.1	586.5	560.8	23.6	41.22	41.22	-2.03	57.83	70.13	1152.7	1616.6	-975.7	-1520.4	1544.3	1539.8																	
95	30.382	30.293	836.7	549.8	613.8	549.5	568.6	19.4	42.81	42.81	-2.03	57.83	70.13	1152.7	1616.6	-975.7	-1520.4	1544.3	1539.8																	

TO/TO PO/PO EFF-AD EFF-P
INLET INLET INLET INLET

1.2523 1.9212 81.17 82.82

MCOR-1

%SPAN	DIA-1		V-1		V-2		VM-1		VM-2		VO-1		VO-2		B-1		B-2		B1-1		B1-2		V1-1		V1-2		V01-1		V01-2		U-1		U-2			
	IN	IN	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE		
5	11650.	13807	1.2523	1.9212	81.17	82.82																														

MCOR-1

%SPAN	DIA-1		V-1		V-2		VM-1		VM-2		VO-1		VO-2		B-1		B-2		B1-1		B1-2		V1-1		V1-2		V01-1		V01-2		U-1		U-2		
	IN	IN	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	FI/SEC	DEGREE	
5	11650.	13807	1.2523	1.9212	81.17	82.82																													

TABLE 11.4
Blade-Element and Overall Performance with Uniform Inlet
105% of Design Speed

ROTOR

%SPAN	DIA-1 IN	DIA-2 IN	V-1 FI/SEC	V-2 FI/SEC	VM-1 VM-2 FI/SEC	VO-1 VO-2 FI/SEC	B-1 B-2 LOSS-P	PO2/PO1	EFF-AD	EFF-P	M-1 M-2	U-1 U-2 FT/SEC		
5	17.467	19.769	626.4	1058.8	626.4	720.3	0.00	47.13	54.81	17.67	107.9	756.0	880.3	1085.8
10	18.467	20.408	643.5	1007.2	643.5	684.4	0.00	47.20	55.58	23.59	118.5	756.0	880.3	1085.8
15	19.467	21.047	659.3	962.1	659.3	659.0	0.00	46.76	56.34	29.23	118.5	756.0	880.3	1085.8
20	20.467	21.686	675.1	917.0	675.1	634.7	0.00	46.32	57.10	34.97	118.5	756.0	880.3	1085.8
30	22.314	23.982	696.3	811.5	696.3	658.1	0.00	43.06	60.36	39.19	131.4	863.5	1011.7	1277.9
50	25.781	28.520	715.8	672.8	715.8	647.3	0.00	42.12	61.37	47.69	131.4	863.5	1011.7	1277.9
70	28.954	28.076	698.5	671.1	698.5	576.6	0.00	40.59	64.62	57.96	146.8	951.4	1127.9	1427.9
85	31.295	29.993	669.8	731.1	669.8	527.9	0.00	41.78	67.47	62.63	176.8	1127.9	1427.9	1427.9
90	31.883	30.636	682.5	708.5	682.5	485.2	0.00	40.62	67.47	68.90	176.8	1127.9	1427.9	1427.9
95	32.499	31.271	657.1	668.5	657.1	422.2	0.00	39.83	68.32	68.30	176.8	1127.9	1427.9	1427.9

%SPAN	INCS	INCM	DEV	TURN	CAMBER	OMEGA-B	D-FAC	OMEGA-B	LOSS-P	PO2	EFF-AD	EFF-P	M-1 M-2	U-1 U-2 FT/SEC	
5	-0.59	5.84	15.80	37.14	47.12	0.158	4.710	0.729	0.153	2.115	0.975	0.504	0.811	916.7	1010.3
10	-0.43	5.94	13.96	31.99	39.99	0.142	5.003	1.142	0.241	2.032	0.978	0.504	0.598	866.9	1065.7
15	-0.22	5.04	12.72	27.10	34.03	0.219	5.116	1.256	0.272	1.985	0.979	0.504	0.528	824.8	1118.4
30	0.57	4.54	9.48	19.28	24.20	0.592	4.911	1.043	0.218	1.967	0.974	0.504	0.891	777.5	1253.2
50	1.89	4.49	5.43	13.69	14.67	1.040	4.741	1.253	0.253	1.964	0.978	0.504	0.672	738.5	1407.7
70	3.25	5.41	7.50	6.65	9.17	1.433	4.355	1.454	0.268	1.824	0.974	0.504	0.545	688.5	1529.1
85	3.97	5.03	10.03	2.69	7.70	1.771	4.885	2.062	0.343	1.751	0.971	0.504	0.225	617.9	1653.4
90	4.12	5.01	12.68	-1.8	7.48	1.886	4.593	2.218	0.367	1.751	0.971	0.504	0.139	587.7	1728.6
95										0.127	1.716	0.971	0.635	548.6	1851.4

To/To PO/PO EFF-AD EFF-P
INLET INLET INLET INLET

1.2420 1.0985 03.71 87.13

STATOR

%SPAN	DIA-1 IN	DIA-2 IN	V-1 FI/SEC	V-2 FI/SEC	VM-1 VM-2 FI/SEC	VO-1 VO-2 FI/SEC	B-1 B-2 LOSS-P	PO2/PO1	EFF-AD	EFF-P	M-1 M-2	U-1 U-2 FT/SEC		
5	20.409	21.489	1123.0	877.0	834.3	876.9	751.6	-15.2	42.01	18.94	51.61	143.0	286.3	1107.9
10	21.008	21.961	1074.9	851.9	799.6	851.7	718.1	-20.7	41.92	23.66	53.18	142.2	350.3	1157.5
15	21.589	22.432	1032.7	832.0	774.3	831.7	683.3	-22.5	41.42	28.15	54.43	140.2	414.7	1203.4
30	23.314	23.982	986.9	799.7	766.9	799.6	621.2	-13.9	39.00	36.33	56.95	146.7	564.5	1229.5
50	25.801	25.893	955.7	758.6	756.9	757.9	583.5	-8.8	37.62	43.47	60.67	148.2	718.5	1259.6
70	27.818	27.982	872.7	682.9	707.8	682.2	510.4	-2.8	35.79	51.94	68.78	148.3	914.4	1308.8
85	29.408	29.382	860.2	626.8	688.6	626.8	435.4	3.5	36.81	54.91	67.20	148.3	914.4	1308.8
90	29.914	29.856	847.5	601.8	664.9	600.8	525.5	19.5	38.33	56.21	68.22	149.2	914.4	1308.8
95	30.382	30.293	824.3	561.8	628.4	553.5	403.3	40.33	40.33	58.15	69.88	149.2	914.4	1308.8

%SPAN	INCS	INCM	DEV	TURN	CAMBER	OMEGA-B	D-FAC	OMEGA-B	LOSS-P	PO2	EFF-AD	EFF-P	M-1 M-2	U-1 U-2 FT/SEC
5	-3.89	-0.97	11.42	43.01	55.90	0.000	3.887	12.14	0.302	0.949	0.000	0.000	0.7711	793.1
10	-3.21	-2.8	10.06	43.31	53.88	0.000	3.759	0.754	0.203	0.949	0.000	0.000	0.820	718.0
15	-3.11	-1.6	9.83	42.97	52.47	0.000	3.699	0.878	0.132	0.943	0.000	0.000	0.884	647.1
30	-3.14	-0.3	10.23	40.00	50.68	0.000	3.662	0.989	0.134	0.920	0.000	0.000	0.834	587.7
50	-3.06	0.7	9.56	40.10	49.61	0.000	4.027	1.003	0.076	0.944	0.000	0.000	0.791	511.6
70	-3.38	0.82	11.04	38.25	49.93	0.000	4.222	1.000	0.166	0.947	0.000	0.000	0.880	441.8
85	-2.19	0.82	16.22	36.48	52.01	0.000	4.794	0.986	0.345	0.979	0.000	0.000	0.810	374.2
90	-1.09	2.24	18.79	36.94	53.58	0.000	5.54	1.004	0.357	0.913	0.000	0.000	0.798	314.9
95		3.98	20.63	39.58	56.05	0.000	5.862	1.026	0.370	0.922	0.000	0.000	0.675	254.1

MCOR-1 MCOR-1 To/To PO/PO EFF-AD EFF-P MC/A-1
INLET INLET INLET INLET INLET INLET
RPM LGM/SEC % % %
11656 188.53 1.2420 1.0621 80.25 81.69 42.37

APPENDIX 4

Blade-Element and Overall Performance with Radial Inlet Distortion

TABLE 12.1 Blade-Element and Overall Performance with Radial Inlet Distortion 70% of Design Speed

ROTOR

Table with columns: %SPAN, DIA-1, DIA-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, B-1, B-2, V1-1, V1-2, V01-1, V01-2, U-1, U-2. Includes rotor inlet and exit flow parameters.

STATOR

Table with columns: %SPAN, DIA-1, DIA-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, B-1, B-2, V1-1, V1-2, V01-1, V01-2, U-1, U-2. Includes stator inlet and exit flow parameters.

TABLE 12.2
Blade-Element and Overall Performance with Radial Inlet Distortion
70% of Design Speed

ROTOR

%SPAN	DIA-1 IN	DIA-2 IN	V-1 FT/SEC	V-2 FT/SEC	VM-1 FT/SEC	VM-2 FT/SEC	VO-1 FT/SEC	VO-2 FT/SEC	B-1 DEGREE	B-2 DEGREE	B1-1 DEGREE	B1-2 DEGREE	V1-1 FT/SEC	V1-2 FT/SEC	V01-1 FT/SEC	V01-2 FT/SEC	U-1 FT/SEC	U-2 FT/SEC
5	17.467	19.769	472.9	778.7	472.9	778.7	0	518.5	0.00	40.76	51.39	15.35	75A.0	611.7	592.3	161.9	592.3	670.4
10	18.467	20.408	479.5	744.0	479.5	569.8	0	499.4	0.00	40.12	52.55	20.49	788.8	607.8	626.2	212.6	626.2	692.4
15	19.467	21.047	487.1	712.2	487.1	554.7	0	466.8	0.00	38.82	53.57	25.67	820.5	616.4	660.2	265.1	660.2	713.4
30	22.314	22.964	496.5	649.9	496.5	536.5	0	356.8	0.00	38.34	54.71	37.86	905.2	677.1	756.7	312.0	756.7	778.8
50	25.791	25.520	457.6	590.1	457.6	497.5	0	317.3	0.00	36.53	62.36	47.74	987.4	740.8	874.6	348.2	874.6	865.4
70	28.954	28.074	361.5	530.3	361.5	473.6	0	316.6	0.00	36.33	69.77	55.82	1085.7	767.9	961.9	363.3	961.9	952.1
85	31.295	29.993	318.8	513.7	318.8	371.8	0	354.4	0.00	43.64	73.28	60.70	1108.1	760.1	1061.3	662.8	1061.3	1017.1
90	31.883	30.630	311.9	494.4	311.9	336.6	0	360.1	0.00	46.80	73.91	63.49	1125.3	758.7	1081.2	678.7	1081.2	1038.7
96	32.449	31.271	302.7	465.7	302.7	285.0	0	360.4	0.00	50.69	74.64	67.15	1142.9	759.7	1102.1	700.1	1102.1	1060.5

%SPAN	INCX	INCM	DEV	TURN	CAMBER	OMEGA-B	D-FAC	OMEGA-B	LOSS-P	LOSS-P	PO2	EFF-AD	EFF-P	TOTAL	TOTAL	STATIC	M-1	M-2	M1-1	M1-2
5	-4.02	2.51	13.48	36.04	47.12	0.000	3.493	1.181	0.250	0.250	1.3937	91.32	90.90	8153	8314	6932	.6919	.5445		
10	-3.49	2.94	10.89	32.06	39.99	0.000	3.760	1.407	0.303	0.303	1.3696	88.60	88.08	7909	8060	6605	.7209	.5395		
15	-3.07	2.99	9.12	27.89	34.03	0.000	3.843	1.419	0.307	0.307	1.3458	87.15	86.59	7898	8047	6314	.7490	.5463		
30	-1.85	2.69	7.42	19.25	24.29	0.000	3.623	0.911	0.194	0.194	1.3182	89.10	88.67	8506	8657	6506	.8221	.5993		
50	2.30	5.13	5.46	14.62	14.66	0.000	3.472	0.537	0.110	0.110	1.3134	92.23	91.92	9006	9227	5202	.8919	.6530		
70	7.66	9.60	4.96	14.16	8.95	0.000	3.681	0.721	0.138	0.138	1.3593	89.94	89.70	8632	8703	6423	.8423	.6709		
85	9.83	11.12	6.34	12.57	7.81	0.176	4.278	1.691	0.301	0.270	1.3434	77.01	76.03	7114	7218	4442	.8442	.6571		
90	10.06	11.17	8.27	19.42	7.52	0.185	4.417	2.025	0.334	0.304	1.3395	72.70	71.56	6685	6828	4260	1.0119	.8536		
96	10.41	11.33	11.21	17.49	7.37	0.215	4.515	2.298	0.356	0.304	1.3213	68.79	67.54	6352	6538	3999	1.0288	.8524		

TO/T0 PO/P0 EFF-AD EFF-P
INLET INLET INLET INLET
1.0094 1.3259 84.42 85.95

STATOR

%SPAN	DIA-1 IN	DIA-2 IN	V-1 FT/SEC	V-2 FT/SEC	VM-1 FT/SEC	VM-2 FT/SEC	VO-1 FT/SEC	VO-2 FT/SEC	B-1 DEGREE	B-2 DEGREE	B1-1 DEGREE	B1-2 DEGREE	V1-1 FT/SEC	V1-2 FT/SEC	V01-1 FT/SEC	V01-2 FT/SEC	U-1 FT/SEC	U-2 FT/SEC
5	20.409	21.489	824.8	747.2	661.7	747.2	492.5	4.6	36.66	.35	16.79	44.10	681.1	1040.5	199.6	724.1	692.1	788.7
10	21.008	21.961	791.5	723.4	639.5	733.0	486.3	-20.2	36.09	-1.62	21.05	46.51	685.4	1032.8	246.1	765.0	712.4	784.7
15	21.599	22.432	760.6	703.4	623.2	649.4	435.9	-36.7	34.96	-3.02	25.40	48.74	590.3	1060.9	296.2	797.5	732.1	760.7
30	23.314	23.902	701.3	647.4	600.6	645.4	351.8	-50.6	31.05	-4.49	35.44	53.15	739.6	1076.4	428.8	861.2	790.6	810.6
50	25.601	25.893	649.1	597.1	567.0	595.4	315.8	-45.1	29.12	-4.33	44.23	57.17	791.9	1098.6	552.4	923.1	868.2	878.1
70	27.818	27.902	614.7	552.9	525.5	582.3	338.0	-23.7	31.19	-2.85	49.98	60.34	816.9	1139.2	645.3	967.8	943.4	966.2
85	29.408	29.382	611.4	524.4	494.6	524.4	350.5	2	36.01	.02	52.21	62.21	874.1	1125.9	637.8	996.2	997.3	996.4
90	29.914	29.856	603.7	509.3	478.8	509.3	377.6	3.8	37.52	.42	53.50	63.21	944.8	1130.0	646.9	1006.7	1014.4	1012.5
96	30.382	30.293	585.0	487.3	452.4	487.3	370.9	3.8	39.34	.45	55.54	64.54	997.1	1133.5	659.4	1023.5	1030.3	1027.3

%SPAN	INCX	INCM	DEV	TURN	CAMBER	OMEGA-B	D-FAC	OMEGA-B	LOSS-P	LOSS-P	PO2	EFF-AD	EFF-P	TOTAL	TOTAL	STATIC	M-1	M-2	M1-1	M1-2
5	-9.50	-6.58	12.76	36.31	55.89	0.000	2.374	-0.754	-0.189	-0.189	97.71	0.000	6587	7326	6626	.6176	.9227			
10	-9.23	-6.30	9.83	37.71	53.86	0.000	2.397	-0.559	-0.143	-0.143	98.91	0.000	7854	8690	6409	.6115	.9328			
15	-9.63	-6.69	7.99	37.98	52.50	0.000	2.391	-0.403	-0.105	-0.105	98.93	0.000	8303	9070	6218	.6020	.9395			
30	-11.46	-8.46	6.74	35.34	50.67	0.000	2.403	-0.418	-0.113	-0.113	99.07	0.000	7894	8624	5729	.6095	.9525			
50	-11.59	-8.46	7.71	33.44	49.61	0.000	2.496	-0.418	-0.128	-0.128	99.14	0.000	7623	8356	5267	.7020	.9691			
70	-8.71	-5.48	11.05	33.63	49.95	0.000	2.845	-0.447	-0.148	-0.148	99.19	0.000	6575	7411	4840	.7193	.9771			
85	-3.59	-2.23	15.92	35.99	52.05	0.000	3.479	-0.899	-0.311	-0.311	98.83	0.000	4226	5336	4540	.7038	.9747			
90	-2.29	1.04	17.82	37.10	53.59	0.000	3.703	-0.965	-0.343	-0.343	98.53	0.000	3726	4874	4395	.7014	.9751			
96	-1.42	2.94	20.14	38.69	56.04	0.000	3.937	-0.911	-0.329	-0.329	98.53	0.000	3000	4148	4191	.6923	.9750			

NCORR WCORR TO/T0 PC/P0 EFF-AD EFF-P W1/A1
INLET INLET INLET INLET LBM/SEC
KPM LBM/SEC
7772 128.99 1.0394 1.3113 80.99 82.62 28.99

TABLE 13.1
Blade-Element and Overall Performance with Radial Inlet Distortion
90% of Design Speed

ROTOR

SPAN	DIA-1 IN	DIA-2 IN	V-1 FT/SEC	V-2 FT/SEC	VM-1 FT/SEC	VM-2 FT/SEC	VW-1 FT/SEC	VW-2 FT/SEC	VO-1 FT/SEC	VO-2 FT/SEC	B-1 DEGREE	B-2 DEGREE	B1-1 DEGREE	B1-2 DEGREE	V1-1 FT/SEC	V1-2 FT/SEC	V1-1 FT/SEC	V1-2 FT/SEC	U-1 FT/SEC	U-2 FT/SEC
5	17.467	19.769	641.6	943.4	641.6	690.4	0	642.8	0	42.55	49.82	17.46	994.5	723.9	-759.9	-417.2	759.3	860.1		
10	18.467	20.408	649.7	925.3	649.7	703.6	0	570.9	0	40.50	51.03	22.18	1033.3	760.0	-803.4	-286.9	803.4	887.9		
15	19.467	21.047	660.1	902.7	660.1	593.0	0	549.4	0	39.50	48.92	25.93	1073.6	771.2	-846.9	-337.2	846.9	915.7		
30	22.314	22.964	678.1	824.1	678.1	661.4	0	491.6	0	36.61	55.01	37.45	1184.7	834.5	-970.8	-507.4	970.8	996.1		
50	25.791	25.520	634.8	739.5	634.8	599.4	0	433.2	0	35.86	60.48	40.45	1289.5	904.8	-1132.0	-677.1	1132.0	1110.3		
70	28.954	28.176	520.4	688.5	520.4	541.4	0	425.3	0	38.16	67.54	55.78	1353.4	982.9	-1359.6	-786.1	1359.6	1224.3		
85	31.883	30.930	481.9	668.7	481.9	498.7	0	445.3	0	41.76	71.28	59.88	1437.8	993.9	-1361.5	-859.8	1361.5	1306.9		
90	32.499	31.271	442.5	602.4	442.5	388.6	0	460.3	0	44.82	71.96	62.21	1423.8	991.8	-1367.1	-877.0	1367.1	1332.6		
95							0	460.3	0	49.82	72.62	65.65	1481.5	980.5	-1413.9	-900.2	1413.9	1360.5		

TO/TO PC/PC EFF-AD EFF-P
INLET INLET INLET
1.1683 1.5707 81.76 83.71

STATOR

SPAN	DIA-1 IN	DIA-2 IN	V-1 FT/SEC	V-2 FT/SEC	VM-1 FT/SEC	VM-2 FT/SEC	VW-1 FT/SEC	VW-2 FT/SEC	VO-1 FT/SEC	VO-2 FT/SEC	B-1 DEGREE	B-2 DEGREE	B1-1 DEGREE	B1-2 DEGREE	V1-1 FT/SEC	V1-2 FT/SEC	V1-1 FT/SEC	V1-2 FT/SEC	U-1 FT/SEC	U-2 FT/SEC	
																					INCS DEGREE
5	20.409	21.489	1009.6	931.9	1009.6	994.3	994.4	633.2	671.9	38.11	4.18	18.43	47.17	837.3	1367.2	-284.7	-1002.8	867.9	934.9		
10	21.008	21.961	992.1	926.0	992.1	929.4	929.4	583.9	694.3	36.03	-4.27	22.37	47.79	867.5	1363.9	-330.1	-1084.7	916.0	955.4		
15	21.589	22.432	971.2	927.6	971.2	924.7	924.7	564.1	737.7	35.30	-4.56	25.36	48.62	875.5	1398.9	-375.2	-1049.6	939.2	975.9		
30	23.314	23.902	900.5	877.8	900.5	874.6	874.6	484.8	744.1	32.36	-4.94	34.86	51.86	925.9	1416.4	-529.5	-1113.9	1014.3	1039.9		
50	25.601	25.993	830.6	815.5	830.6	815.5	815.5	431.0	647.7	31.26	-3.64	43.86	55.44	985.3	1434.4	-682.8	-1181.2	1113.8	1126.5		
70	27.818	27.902	803.7	772.8	803.7	771.6	771.6	427.3	524.7	32.11	-3.16	48.99	58.45	1037.5	1474.6	-783.0	-1256.6	1210.2	1213.9		
85	29.408	29.362	813.6	751.8	813.6	751.7	751.7	452.5	447.7	33.78	-3.6	50.73	59.63	1068.2	1487.0	-856.9	-1283.0	1279.4	1278.3		
90	29.914	29.856	811.3	750.3	811.3	750.1	750.1	465.4	455.4	35.01	1.46	51.33	59.70	1068.0	1486.8	-859.1	-1283.7	1301.4	1296.9		
95	30.382	30.293	789.1	712.0	789.1	712.0	712.0	473.7	473.7	37.23	1.79	53.87	61.22	1052.6	1478.2	-848.0	-1295.6	1321.8	1317.9		

TO/TO PC/PC EFF-AD EFF-P
INLET INLET INLET
1.1683 1.5707 81.76 83.71

TABLE 13.2

Blade-Element and Overall Performance with Radial Inlet Distortion
90% of Design Speed

ROTOR

%SPAN	IN	DIA-1		DIA-2		V-1		V-2		VM-1		VM-2		VO-1		VO-2		B-1		B-2		B1-1		B1-2		V1-1		V1-2		V01-1		V01-2		U-1		U-2					
		IN	IN	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC			
5	17.467	19.769	636.3	936.3	636.3	936.3	636.3	936.3	636.3	936.3	636.3	936.3	636.3	936.3	636.3	936.3	636.3	936.3	636.3	936.3	636.3	936.3	636.3	936.3	636.3	936.3	636.3	936.3	636.3	936.3	636.3	936.3	636.3	936.3	636.3	936.3	636.3	936.3	636.3	936.3	
10	16.467	20.408	684.5	912.2	684.5	912.2	684.5	912.2	684.5	912.2	684.5	912.2	684.5	912.2	684.5	912.2	684.5	912.2	684.5	912.2	684.5	912.2	684.5	912.2	684.5	912.2	684.5	912.2	684.5	912.2	684.5	912.2	684.5	912.2	684.5	912.2	684.5	912.2	684.5	912.2	684.5
15	19.467	21.047	684.5	885.7	684.5	885.7	684.5	885.7	684.5	885.7	684.5	885.7	684.5	885.7	684.5	885.7	684.5	885.7	684.5	885.7	684.5	885.7	684.5	885.7	684.5	885.7	684.5	885.7	684.5	885.7	684.5	885.7	684.5	885.7	684.5	885.7	684.5	885.7	684.5	885.7	684.5
30	22.314	22.954	674.1	813.6	674.1	813.6	674.1	813.6	674.1	813.6	674.1	813.6	674.1	813.6	674.1	813.6	674.1	813.6	674.1	813.6	674.1	813.6	674.1	813.6	674.1	813.6	674.1	813.6	674.1	813.6	674.1	813.6	674.1	813.6	674.1	813.6	674.1	813.6	674.1	813.6	674.1
50	25.791	25.520	629.9	742.7	629.9	742.7	629.9	742.7	629.9	742.7	629.9	742.7	629.9	742.7	629.9	742.7	629.9	742.7	629.9	742.7	629.9	742.7	629.9	742.7	629.9	742.7	629.9	742.7	629.9	742.7	629.9	742.7	629.9	742.7	629.9	742.7	629.9	742.7	629.9	742.7	629.9
70	28.954	28.076	549.9	692.5	549.9	692.5	549.9	692.5	549.9	692.5	549.9	692.5	549.9	692.5	549.9	692.5	549.9	692.5	549.9	692.5	549.9	692.5	549.9	692.5	549.9	692.5	549.9	692.5	549.9	692.5	549.9	692.5	549.9	692.5	549.9	692.5	549.9	692.5	549.9	692.5	
85	31.295	29.993	455.7	641.1	455.7	641.1	455.7	641.1	455.7	641.1	455.7	641.1	455.7	641.1	455.7	641.1	455.7	641.1	455.7	641.1	455.7	641.1	455.7	641.1	455.7	641.1	455.7	641.1	455.7	641.1	455.7	641.1	455.7	641.1	455.7	641.1	455.7	641.1	455.7	641.1	
90	31.883	30.630	485.5	644.8	485.5	644.8	485.5	644.8	485.5	644.8	485.5	644.8	485.5	644.8	485.5	644.8	485.5	644.8	485.5	644.8	485.5	644.8	485.5	644.8	485.5	644.8	485.5	644.8	485.5	644.8	485.5	644.8	485.5	644.8	485.5	644.8	485.5	644.8	485.5	644.8	
95	32.499	31.271	436.2	617.9	436.2	617.9	436.2	617.9	436.2	617.9	436.2	617.9	436.2	617.9	436.2	617.9	436.2	617.9	436.2	617.9	436.2	617.9	436.2	617.9	436.2	617.9	436.2	617.9	436.2	617.9	436.2	617.9	436.2	617.9	436.2	617.9	436.2	617.9	436.2	617.9	

TO/TO PO/PO EFF-AD EFF-P
INLET INLET INLET INLET
1.1759 1.6208 83.95 85.76

STATOR

%SPAN	IN	DIA-1		DIA-2		V-1		V-2		VM-1		VM-2		VO-1		VO-2		B-1		B-2		B1-1		B1-2		V1-1		V1-2		V01-1		V01-2		U-1		U-2			
		IN	IN	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	DEGREE	FT/SEC	
5	23.409	21.489	696.5	642.1	779.3	841.9	621.0	14.8	38.55	1.01	19.01	47.52	524.3	1248.4	-684.5	-921.8	889.6	936.6	636.3	936.3	636.3	936.3	636.3	936.3	636.3	936.3	636.3	936.3	636.3	936.3	636.3	936.3	636.3	936.3	636.3	936.3	636.3	936.3	
10	21.008	21.961	973.7	825.1	775.8	825.0	588.2	-7.9	37.16	-0.56	22.87	49.47	842.5	1269.8	-327.5	-965.1	915.7	977.2	761.3	861.7	861.7	861.7	861.7	861.7	861.7	861.7	861.7	861.7	861.7	861.7	861.7	861.7	861.7	861.7	861.7	861.7	861.7	861.7	861.7
15	21.589	22.932	948.1	869.1	765.7	869.7	559.1	-25.1	35.13	-1.78	26.50	51.11	856.0	1288.4	-381.9	-1002.4	941.0	977.2	804.9	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5
30	23.314	23.902	882.0	759.4	733.3	758.0	490.1	-46.9	33.76	-3.55	35.63	55.15	903.0	1326.8	-526.0	-1088.8	1016.2	1041.8	804.9	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5
50	25.601	25.693	823.5	736.1	685.0	705.0	453.9	-59.1	33.50	-3.17	43.97	56.87	953.6	1364.8	-662.0	-1167.7	1115.9	1126.6	804.9	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5
70	27.818	27.902	793.6	668.6	648.9	669.1	456.8	-25.6	35.15	-2.19	49.35	61.72	996.0	1410.0	-755.7	-1241.7	1216.2	1216.2	804.9	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	
85	29.008	29.382	807.6	651.4	641.4	651.2	490.8	16.2	37.42	1.42	50.97	62.75	1018.4	1428.3	-781.0	-1264.5	1281.8	1281.8	804.9	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	
90	29.214	29.950	807.6	641.9	629.4	641.4	506.6	25.1	36.85	2.24	51.72	63.32	1015.8	1428.3	-797.2	-1276.3	1303.9	1303.9	804.9	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5		
95	30.362	30.693	776.9	608.2	580.6	603.7	516.4	23.9	41.66	2.26	54.30	65.03	994.8	1430.2	-807.8	-1296.5	1324.3	1324.3	804.9	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5	889.5		

INCORR W/CORR TO/TO PO/PO EFF-AD EFF-P W1/W1
INLET INLET INLET INLET INLET INLET LBM/SEC
RPM LBM/SEC
9989 165.76 1.1757 1.5893 50.40 82.39 37.25

TABLE 14.2
Blade-Element and Overall Performance with Radial Inlet Distortion

ROTOR

100% of Design Speed

SPAN IN	DIA-1		DIA-2		V-1		V-2		VM-1		VM-2		U-1		U-2		V1-1		V1-2		V01-1		V01-2		U-1		U-2		
	DEGREE	IN	DEGREE	IN	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC
5	-4.45	1.89	16.58	32.45	47.12	0.056	4.884	2.252	0.499	0.457	1.8258	85.17	83.67	7.801	6.402	0.8715	1.0145	6.322	8.456	1.0561	6.501	8.517	1.0995	6.802	7.787	1.2205	7.507	8.464	9.98.0
10	-4.00	2.43	13.78	28.70	39.99	0.095	4.861	1.964	0.444	0.394	1.8138	85.00	84.79	8.103	6.496	0.8456	1.0561	6.501	8.517	1.0995	6.802	7.787	1.2205	7.507	8.464	9.98.0	8.464	9.98.0	
15	-3.52	2.50	10.83	25.73	34.03	0.149	4.743	1.606	0.392	0.310	1.8214	87.62	86.56	8.6618	6.618	0.8618	1.0618	6.618	8.618	1.0618	6.618	7.618	1.2618	7.467	8.467	9.98.0	8.467	9.98.0	
30	-2.37	1.75	7.45	18.63	24.28	0.385	4.763	1.479	0.317	0.245	1.8007	86.42	85.28	8.858	6.697	0.858	1.0697	6.697	8.697	1.0697	6.697	7.697	1.2697	7.467	8.467	9.98.0	8.467	9.98.0	
50	1.07	3.89	6.22	12.57	14.65	0.727	5.047	1.737	0.351	0.207	1.8132	82.54	81.03	8.145	6.511	0.8145	1.0651	6.511	8.511	1.0651	6.511	7.511	1.2651	7.467	8.467	9.98.0	8.467	9.98.0	
70	5.77	7.72	6.00	11.80	8.95	1.163	4.979	1.395	0.269	0.077	1.9488	85.78	84.38	8.394	6.526	0.8394	1.0652	6.526	8.526	1.0652	6.526	7.526	1.2652	7.467	8.467	9.98.0	8.467	9.98.0	
85	8.11	9.41	6.01	11.27	7.80	1.450	5.216	1.807	0.323	0.070	2.0384	82.11	80.21	8.021	6.521	0.8021	1.0652	6.521	8.521	1.0652	6.521	7.521	1.2652	7.467	8.467	9.98.0	8.467	9.98.0	
90	8.44	9.55	8.01	12.07	7.52	1.527	5.416	1.924	0.319	0.068	2.0325	78.27	75.94	8.525	6.525	0.8025	1.0652	6.525	8.525	1.0652	6.525	7.525	1.2652	7.467	8.467	9.98.0	8.467	9.98.0	
95	8.71	9.63	11.89	5.12	7.38	1.640	5.568	2.023	0.372	0.141	1.9989	74.49	71.88	8.714	6.507	0.8007	1.0652	6.507	8.507	1.0652	6.507	7.507	1.2652	7.467	8.467	9.98.0	8.467	9.98.0	

TO/TO P/U/P0 EFF-AD EFF-P
-INLET -INLET -INLET I-LIFT
1.2387 1.8550 80.80 83.02

STATOR

SPAN IN	DIA-1		DIA-2		V-1		V-2		VM-1		VM-2		U-1		U-2		V1-1		V1-2		V01-1		V01-2		U-1		U-2	
	DEGREE	IN	DEGREE	IN	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC
5	-4.37	-1.45	11.52	42.72	55.89	0.0000	4.146	0.718	0.178	0.9694	0.0000	0.0000	8.792	7.049	0.7049	1.0537	7.049	9.049	1.0537	7.049	8.049	1.2537	7.989	10.41.3	10.41.3	10.41.3	10.41.3	
10	-4.84	-1.91	10.58	41.56	53.87	0.0000	4.088	0.569	0.145	0.9145	0.0000	0.0000	8.747	7.019	0.7019	1.0537	7.019	9.019	1.0537	7.019	8.019	1.2537	7.989	10.41.3	10.41.3	10.41.3	10.41.3	
15	-5.15	-2.21	9.97	40.28	52.46	0.0000	4.068	0.330	0.165	0.8747	0.0000	0.0000	8.747	7.019	0.7019	1.0537	7.019	9.019	1.0537	7.019	8.019	1.2537	7.989	10.41.3	10.41.3	10.41.3	10.41.3	
30	-4.61	-1.61	8.77	40.20	50.67	0.0000	4.108	0.500	0.140	0.9814	0.0000	0.0000	8.747	7.019	0.7019	1.0537	7.019	9.019	1.0537	7.019	8.019	1.2537	7.989	10.41.3	10.41.3	10.41.3	10.41.3	
50	-8.5	2.28	8.78	43.12	49.61	0.0000	4.515	0.565	0.112	0.9883	0.0000	0.0000	8.747	7.019	0.7019	1.0537	7.019	9.019	1.0537	7.019	8.019	1.2537	7.989	10.41.3	10.41.3	10.41.3	10.41.3	
70	1.18	4.72	12.49	42.20	49.94	0.0000	4.848	0.611	0.093	0.9818	0.0000	0.0000	8.747	7.019	0.7019	1.0537	7.019	9.019	1.0537	7.019	8.019	1.2537	7.989	10.41.3	10.41.3	10.41.3	10.41.3	
85	3.78	7.09	10.28	40.99	52.04	0.0000	5.131	1.120	0.046	0.9626	0.0000	0.0000	8.747	7.019	0.7019	1.0537	7.019	9.019	1.0537	7.019	8.019	1.2537	7.989	10.41.3	10.41.3	10.41.3	10.41.3	
90	5.41	8.74	20.84	41.86	53.59	0.0000	5.235	1.145	0.042	0.9424	0.0000	0.0000	8.747	7.019	0.7019	1.0537	7.019	9.019	1.0537	7.019	8.019	1.2537	7.989	10.41.3	10.41.3	10.41.3	10.41.3	
95	8.05	11.41	23.16	44.43	56.05	0.0000	5.614	1.261	0.056	0.9456	0.0000	0.0000	8.747	7.019	0.7019	1.0537	7.019	9.019	1.0537	7.019	8.019	1.2537	7.989	10.41.3	10.41.3	10.41.3	10.41.3	

NCORR WCCR TO/TO PC/P0 EFF-AD EFF-P M1/M1
INLET INLET INLET INLET INLET
RPM LBM/SEC M X SGFT
11106 176.26 1.2387 1.8140 77.61 80.04 39.61

APPENDIX 5

**Circumferential Inlet Distortion,
Distribution and Overall Performance**

PRECEDING PAGE BLANK NOT FILMED.

TABLE 15.1
Rotor Inlet Circumferential Distributions
Disk Probe Station 7, 70% of Design Speed, $\frac{W\sqrt{\theta}}{\delta} = 129.8$

Circumferential Position	54°					114°					174°				
	P ₇ /P ₀	90-β ₇	M	V	V _m	P ₇ /P ₀	90-β ₇	M	V	V _m	P ₇ /P ₀	90-β ₇	M	V	V _m
5 (hub)	.975	30.75	.321	355	352	.968	30.00	.291	322	322	.966	34.40	.291	322	322
10	.973	30.35	.335	370	368	.970	30.02	.313	346	346	.977	34.46	.313	346	346
15	.973	30.18	.351	387	385	.972	30.18	.334	369	369	.977	33.75	.334	369	369
30	.970	27.49	.366	403	402	.972	27.85	.357	394	394	.965	29.55	.352	388	383
50	.976	24.60	.380	418	417	.976	24.35	.366	403	403	.971	25.78	.370	408	405
70	.973	20.75	.355	392	391	.975	20.70	.346	382	382	.972	22.10	.359	396	394
85	.967	17.50	.321	354	353	.972	17.70	.317	350	350	.969	19.15	.335	370	368
90	.962	15.81	.299	331	329	.968	16.20	.299	330	330	.966	17.75	.318	352	350
95 (tip)	.954	13.35	.262	291	286	.954	13.12	.250	277	276	.952	14.61	.268	297	297
MR	.971		.350	386	384	.972		.338	373	373	.968		.346	382	379

Circumferential Position	204°					264°					324°				
	P ₇ /P ₀	90-β ₇	M	V	V _m	P ₇ /P ₀	90-β ₇	M	V	V _m	P ₇ /P ₀	90-β ₇	M	V	V _m
5 (hub)	.952	42.20	.346	382	333	.863	21.88	.200	222	222	.951	27.70	.200	222	222
10	.947	39.78	.349	385	335	.861	21.20	.206	229	229	.952	28.45	.206	229	229
15	.936	36.18	.338	373	325	.859	20.90	.215	239	239	.948	28.00	.215	239	239
30	.924	28.40	.323	357	337	.860	26.35	.237	263	263	.956	27.40	.237	263	263
50	.914	22.65	.307	340	322	.860	17.12	.241	268	267	.965	24.90	.241	268	267
70	.915	19.28	.301	333	309	.860	14.50	.232	258	258	.969	21.80	.232	258	258
85	.918	17.30	.297	329	302	.862	12.85	.223	248	248	.966	19.12	.223	248	248
90	.921	16.90	.299	330	300	.862	12.30	.219	244	244	.961	17.50	.219	244	244
95 (tip)	.916	14.63	.270	299	266	.861	11.20	.207	230	229	.936	12.62	.207	230	229
MR	.922		.312	345	318	.861		.228	253	253	.960		.228	253	253

- 1) Inlet plenum conditions: P₀ = 2012 psf, T₀ = 534 °R
- 2) V_m calculation is based on standard-day inlet plenum conditions
- 3) Circumferential reference position is TDC looking forward
- 4) Relative position of circumferential distortion screen is 210° - 330°
- 5) β₇ = tan⁻¹ [tan β₇/cos ε]

TABLE 15.2
Rotor Inlet Circumferential Distributions
Disk Probe Station 7, 70% of Design Speed, $\frac{W\sqrt{\theta}}{\delta} = 122.1$

Circumferential Position	24°				54°				84°				114°										
	P ₇ /P ₀	90-β ² /γ	90-β ² /γ	V _m	I ₇ /P ₀	90-β ² /γ	90-β ² /γ	M	V	V _m	P ₇ /P ₀	90-β ² /γ	90-β ² /γ	M	V	V _m	P ₇ /P ₀	90-β ² /γ	90-β ² /γ	M	V	V _m	
5 (hub)	.971	29.48	94.6	320	353	352	361	362	361	362	361	362	361	362	361	362	361	362	361	362	361	362	361
10	.971	29.48	94.6	320	353	352	361	362	361	362	361	362	361	362	361	362	361	362	361	362	361	362	361
15	.972	28.70	94.8	328	362	361	362	361	362	361	362	361	362	361	362	361	362	361	362	361	362	361	362
30	.977	27.12	93.6	357	394	393	394	393	394	393	394	393	394	393	394	393	394	393	394	393	394	393	394
50	.975	23.20	93.9	355	391	390	392	391	390	391	390	391	390	391	390	391	390	391	390	391	390	391	390
70	.976	19.80	94.0	338	373	372	373	372	373	372	373	372	373	372	373	372	373	372	373	372	373	372	373
85	.975	16.70	98.6	314	347	344	345	344	345	344	345	344	345	344	345	344	345	344	345	344	345	344	345
90	.974	15.60	102.5	304	336	328	328	329	328	329	328	329	328	329	328	329	328	329	328	329	328	329	328
95 (tip)	.974	13.50	107.8	286	317	301	301	302	301	302	301	302	301	302	301	302	301	302	301	302	301	302	301
MR	.975	95.8	335	370	368																		

Circumferential Position	144°				174°				204°				234°										
	P ₇ /P ₀	90-β ² /γ	90-β ² /γ	V _m	I ₇ /P ₀	90-β ² /γ	90-β ² /γ	M	V	V _m	P ₇ /P ₀	90-β ² /γ	90-β ² /γ	M	V	V _m	P ₇ /P ₀	90-β ² /γ	90-β ² /γ	M	V	V _m	
5 (hub)	.974	32.85	82.3	300	332	329	332	331	332	331	332	331	332	331	332	331	332	331	332	331	332	331	332
10	.976	31.70	83.7	312	345	343	344	343	344	343	344	343	344	343	344	343	344	343	344	343	344	343	344
15	.974	30.40	83.8	316	349	347	348	347	348	347	348	347	348	347	348	347	348	347	348	347	348	347	348
30	.978	27.60	85.8	339	374	373	374	373	374	373	374	373	374	373	374	373	374	373	374	373	374	373	374
50	.977	23.70	86.1	342	377	376	377	376	377	376	377	376	377	376	377	376	377	376	377	376	377	376	377
70	.975	20.10	86.3	326	360	360	361	360	361	360	361	360	361	360	361	360	361	360	361	360	361	360	361
85	.974	16.90	91.2	303	335	335	336	335	336	335	336	335	336	335	336	335	336	335	336	335	336	335	336
90	.972	16.00	91.2	294	325	325	326	325	326	325	326	325	326	325	326	325	326	325	326	325	326	325	326
95 (tip)	.971	14.05	98.1	272	302	299	299	300	299	300	299	300	299	300	299	300	299	300	299	300	299	300	299
MR	.975	87.2	322	356	356																		

Circumferential Position	294°				324°				354°														
	P ₇ /P ₀	90-β ² /γ	90-β ² /γ	V _m	I ₇ /P ₀	90-β ² /γ	90-β ² /γ	M	V	V _m	P ₇ /P ₀	90-β ² /γ	90-β ² /γ	M	V	V _m	P ₇ /P ₀	90-β ² /γ	90-β ² /γ	M	V	V _m	
5 (hub)	.974	22.00	88.7	200	222	222	222	222	222	222	222	222	222	222	222	222	222	222	222	222	222	222	222
10	.873	20.65	88.7	200	222	222	222	222	222	222	222	222	222	222	222	222	222	222	222	222	222	222	222
30	.872	19.65	88.7	201	223	223	223	223	223	223	223	223	223	223	223	223	223	223	223	223	223	223	223
50	.871	18.20	87.1	216	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240
70	.870	15.28	89.5	217	241	241	241	241	241	241	241	241	241	241	241	241	241	241	241	241	241	241	241
85	.871	12.90	89.0	207	230	230	230	230	230	230	230	230	230	230	230	230	230	230	230	230	230	230	230
90	.875	11.88	89.6	207	230	230	230	230	230	230	230	230	230	230	230	230	230	230	230	230	230	230	230
95 (tip)	.878	11.42	90.7	205	228	228	228	228	228	228	228	228	228	228	228	228	228	228	228	228	228	228	228
MR	.876	10.70	94.4	200	222	222	222	222	222	222	222	222	222	222	222	222	222	222	222	222	222	222	222
	.872	89.4	209	232	232																		

1) Inlet plenum conditions: P₀ = 2020 psf, T₀ = 525.2 °R
 2) V_m calculation is based on standard-day inlet plenum conditions
 3) Circumferential reference position is IDC looking forward
 4) Relative position of circumferential distortion screen is 210° - 330°
 5) β₇° = tan⁻¹ [tan β₇/cos ε]

TABLE 15.3
Rotor Inlet Circumferential Distributions
Disk Probe Station 7, 70% of Design Speed, $W\sqrt{\theta} / \delta = 111.0$

Circumferential Position	54°				114°				174°			
	P_7/P_0	$90-\beta_7$	M	V_m	P_7/P_0	$90-\beta_7$	M	V_m	P_7/P_0	$90-\beta_7$	M	V_m
5 (hub)	.981	27.10	.263	291	.975	27.60	.258	286	.975	30.60	.269	298
10	.983	27.10	.281	311	.976	26.90	.269	299	.979	30.65	.293	325
15	.981	26.60	.291	323	.977	26.80	.284	314	.979	30.00	.304	336
30	.979	23.80	.302	334	.979	25.00	.313	346	.975	26.05	.310	343
50	.982	20.90	.309	342	.982	21.90	.320	354	.980	23.00	.328	363
70	.981	17.10	.282	313	.981	18.45	.303	335	.981	19.65	.318	351
85	.976	14.25	.255	283	.978	15.55	.276	305	.978	16.80	.292	324
90	.973	13.08	.241	267	.974	14.30	.260	289	.975	15.90	.279	309
95 (tip)	.964	10.75	.206	229	.961	11.50	.217	241	.963	12.75	.235	261
MR	.979		.284	315	.978		.295	327	.977		.306	338

Circumferential Position	204°				264°				324°			
	P_7/P_0	$90-\beta_7$	M	V_m	P_7/P_0	$90-\beta_7$	M	V_m	P_7/P_0	$90-\beta_7$	M	V_m
5 (hub)	.955	32.60	.271	300	.902	20.90	.200	222	.967	23.85	.297	328
10	.959	31.15	.293	324	.898	19.65	.200	222	.969	24.70	.317	351
15	.954	30.60	.294	325	.896	18.70	.206	229	.968	24.15	.323	356
30	.935	23.40	.267	296	.897	16.60	.206	229	.966	23.00	.345	381
50	.933	19.40	.265	293	.898	14.50	.208	232	.974	20.35	.352	388
70	.931	16.20	.254	282	.898	12.10	.200	222	.979	17.00	.327	361
85	.931	14.50	.248	275	.898	11.25	.200	222	.974	13.70	.286	317
90	.935	14.50	.255	283	.899	11.00	.200	222	.966	11.70	.257	285
95 (tip)	.934	13.10	.239	266	.899	10.50	.200	222	.945	8.65	.200	222
MR	.937		.264	292	.898		.203	225	.971		.323	357

- 1) Inlet plenum conditions: $P_0 = 2037$ psf, $T_0 = 529.3$ °R
- 2) V_m calculation is based on standard-day inlet plenum conditions
- 3) Circumferential reference position is TDC looking forward
- 4) Relative position of circumferential distortion screen is $210^\circ - 330^\circ$
- 5) $\beta_7^\circ = \tan^{-1} [\tan \beta_7 / \cos \epsilon]$

TABLE 15.5

Rotor Inlet Circumferential Distributions

Disk Probe Station 7, 90% of Design Speed, $\frac{W\sqrt{\theta}}{\delta} = 156.2$

Circumferential Position

% Span	24°				54°				84°				114°					
	P _r /P ₀	90-β ¹ /γ	90-β ² /γ	M	V	V _m	P _r /P ₀	90-β ¹ /γ	90-β ² /γ	M	V	V _m	P _r /P ₀	90-β ¹ /γ	90-β ² /γ	M	V	V _m
5 (hub)	.944	31.40	93.7	.112	452	451	.954	31.80	94.3	.422	463	451	.961	34.10	88.0	.429	470	470
10	.947	31.20	92.9	.434	476	475	.952	31.20	94.0	.438	480	479	.961	33.00	88.8	.444	487	487
15	.952	30.60	92.9	.450	493	492	.954	30.70	93.2	.455	498	497	.959	31.70	88.9	.450	493	493
30	.960	28.60	92.4	.480	524	523	.950	27.70	93.4	.471	515	514	.957	28.35	89.0	.466	509	509
50	.957	24.18	92.6	.473	517	516	.957	24.60	92.3	.484	528	528	.957	24.63	89.3	.471	515	515
70	.952	20.07	95.5	.449	492	489	.953	20.60	93.6	.456	499	498	.956	20.70	91.6	.450	493	493
85	.955	17.28	96.7	.418	469	465	.949	17.70	93.4	.419	460	459	.954	17.50	92.5	.411	451	451
90	.956	16.33	97.6	.405	445	441	.948	17.20	93.5	.402	442	441	.954	16.65	92.5	.399	438	438
95 (tip)	.950	14.48	98.8	.386	403	398	.939	14.50	94.2	.355	391	390	.953	14.90	93.6	.365	402	402
MR	.954		94.3	.448	491	489	.952		93.3	.451	493	492	.957		90.4	.445	487	487
5 (hub)	.956	35.45	82.6	.425	466	463	.950	36.30	78.4	.423	464	454	.905	39.20	60.7	.414	455	397
10	.957	34.00	84.0	.440	482	479	.947	34.64	79.9	.434	476	468	.897	36.18	60.5	.411	452	394
15	.952	32.60	84.0	.445	487	484	.946	33.40	80.1	.446	489	482	.884	32.80	65.5	.403	442	402
30	.960	25.70	85.6	.477	520	519	.938	29.20	82.7	.457	500	495	.890	29.30	74.7	.438	490	463
50	.961	25.35	86.8	.479	523	522	.956	26.30	85.5	.493	538	536	.895	25.20	77.2	.451	493	481
70	.958	21.55	87.6	.460	503	502	.953	22.30	86.4	.472	516	515	.896	22.35	75.2	.453	495	479
85	.959	18.52	88.2	.427	469	469	.950	19.30	85.9	.440	482	481	.911	20.50	74.0	.454	497	477
90	.958	17.43	88.3	.410	450	450	.949	18.16	85.9	.424	465	464	.915	15.70	72.7	.446	488	468
95 (tip)	.958	16.10	88.3	.386	425	424	.937	15.64	85.5	.389	406	405	.900	17.08	69.3	.397	436	408
MR	.959		86.5	.453	496	495	.949		84.2	.457	499	497	.897		73.1	.439	481	460
5 (hub)	.793	19.00	93.8	.226	251	251	.843	24.0	109.9	.363	400	376	.905	23.38	119.3	.423	464	405
13	.792	18.70	93.8	.239	265	264	.835	24.0	104.5	.384	401	388	.898	23.60	115.7	.425	466	420
15	.789	18.80	93.7	.254	282	281	.827	22.3	104.7	.350	386	373	.898	24.95	110.5	.444	486	455
30	.791	18.50	93.3	.294	325	325	.792	15.9	105.4	.275	305	294	.918	25.35	106.5	.501	546	523
50	.791	15.75	95.1	.297	328	327	.786	11.88	115.4	.262	291	283	.927	22.10	106.9	.503	547	524
70	.784	12.20	98.0	.264	293	289	.781	9.02	119.9	.234	260	258	.933	18.83	108.5	.480	524	497
85	.785	10.33	106.1	.243	270	266	.782	7.64	119.8	.212	236	205	.941	16.45	105.6	.451	493	465
90	.785	10.23	98.6	.246	273	270	.781	7.13	119.8	.202	225	195	.934	14.95	111.4	.422	463	431
95 (tip)	.781	8.36	103.9	.211	234	227	.780	6.16	119.7	.177	197	171	.899	10.50	119.7	.321	355	308
MR	.788		96.6	.269	298	296	.797		112.7	.279	309	285	.923		109.4	.469	512	433
5 (hub)	.793	19.00	93.8	.226	251	251	.843	24.0	109.9	.363	400	376	.905	23.38	119.3	.423	464	405
13	.792	18.70	93.8	.239	265	264	.835	24.0	104.5	.384	401	388	.898	23.60	115.7	.425	466	420
15	.789	18.80	93.7	.254	282	281	.827	22.3	104.7	.350	386	373	.898	24.95	110.5	.444	486	455
30	.791	18.50	93.3	.294	325	325	.792	15.9	105.4	.275	305	294	.918	25.35	106.5	.501	546	523
50	.791	15.75	95.1	.297	328	327	.786	11.88	115.4	.262	291	283	.927	22.10	106.9	.503	547	524
70	.784	12.20	98.0	.264	293	289	.781	9.02	119.9	.234	260	258	.933	18.83	108.5	.480	524	497
85	.785	10.33	106.1	.243	270	266	.782	7.64	119.8	.212	236	205	.941	16.45	105.6	.451	493	465
90	.785	10.23	98.6	.246	273	270	.781	7.13	119.8	.202	225	195	.934	14.95	111.4	.422	463	431
95 (tip)	.781	8.36	103.9	.211	234	227	.780	6.16	119.7	.177	197	171	.899	10.50	119.7	.321	355	308
MR	.788		96.6	.269	298	296	.797		112.7	.279	309	285	.923		109.4	.469	512	433

- 1) Inlet plenum conditions P₀ = 1977 psf, T₀ = 536.1 R
- 2) V_m calculations is based on standard-day inlet conditions
- 3) Circumferential reference position is TDC locking forward
- 4) Relative position of circumferential distortion screen is 210°-330°
- 5) β_r° = tan⁻¹ [tan β_r / cos ε]

TABLE 15.6

Rotor Inlet Circumferential Distributions

Disk Probe Station 7, 100% of Design Speed, $W\sqrt{\theta} = 178.2$

Circumferential Position	24°			54°			114°								
	P _r /P ₀	M	V	P _r /P ₀	M	V	P _r /P ₀	M	V						
5 (hub)	.926	.90-β ^h	96.2	.930	90-β ^h	97.6	.946	89.5	89.5	.919	90-β ^h	91.2	.447	489	489
10	.922	20.80	95.9	.934	31.25	96.7	.946	32.78	80.5	.928	31.70	90.7	.480	524	524
15	.924	30.40	95.3	.937	34.23	96.1	.948	32.00	80.6	.933	31.26	90.7	.502	547	547
30	.933	28.10	95.2	.932	29.60	95.7	.941	28.40	90.7	.935	27.70	90.6	.532	577	577
50	.941	24.75	94.5	.940	24.52	94.8	.944	24.60	90.9	.939	24.70	90.9	.535	581	581
70	.939	22.35	95.3	.938	21.07	94.4	.942	20.90	91.0	.938	21.27	90.5	.513	558	558
85	.940	18.00	96.6	.936	18.18	94.4	.936	17.55	92.3	.939	18.32	90.3	.472	517	517
90	.942	17.12	96.9	.932	16.98	94.6	.930	16.18	92.4	.937	17.14	90.6	.452	495	495
95 (tip)	.942	15.80	97.8	.919	15.28	96.8	.920	14.38	94.1	.922	15.11	92.0	.407	447	447
MR	.936		95.5	.935		96.3	.941		91.2	.935		90.8	.503	548	548

			144°			204°			234°						
			P _r /P ₀	M <td>V <td>P_r/P₀</td><td>M <td>V <td>P_r/P₀</td><td>M <td>V <td>P_r/P₀</td><td>M <td>V </td></td></td></td></td></td></td>	V <td>P_r/P₀</td> <td>M <td>V <td>P_r/P₀</td><td>M <td>V <td>P_r/P₀</td><td>M <td>V </td></td></td></td></td></td>	P _r /P ₀	M <td>V <td>P_r/P₀</td><td>M <td>V <td>P_r/P₀</td><td>M <td>V </td></td></td></td></td>	V <td>P_r/P₀</td> <td>M <td>V <td>P_r/P₀</td><td>M <td>V </td></td></td></td>	P _r /P ₀	M <td>V <td>P_r/P₀</td><td>M <td>V </td></td></td>	V <td>P_r/P₀</td> <td>M <td>V </td></td>	P _r /P ₀	M <td>V </td>	V	
5 (hub)	.937	36.50	80.3	.928	36.23	78.4	.880	42.50	60.7	.815	35.05	63.0	.417	458	408
10	.936	34.65	81.7	.925	35.35	78.5	.876	39.70	60.5	.792	28.78	66.6	.370	408	374
15	.925	32.57	83.1	.926	34.60	79.5	.857	35.40	62.3	.777	24.08	67.6	.331	366	338
30	.940	29.75	85.3	.919	30.47	80.8	.868	30.80	74.0	.741	13.55	65.5	.227	252	229
50	.945	25.65	86.3	.929	26.10	83.7	.884	26.95	74.4	.737	10.23	59.9	.213	237	205
70	.937	21.45	87.2	.936	22.70	84.9	.904	22.10	70.9	.728	6.48	64.1	.154	171	154
85	.934	18.42	86.6	.940	19.90	84.4	.890	20.05	68.6	.736	8.51	74.9	.209	232	224
90	.929	16.98	87.0	.938	18.77	83.8	.890	14.60	63.4	.740	8.79	75.9	.221	246	238
95 (tip)	.914	15.00	86.8	.914	15.95	83.6	.838			.740	8.66	75.9	.223	248	241
MR	.936		85.7	.928		82.7	.881			.762		66.8	.264	293	269

			284°			324°			354°						
			P _r /P ₀	M <td>V <td>P_r/P₀</td><td>M <td>V <td>P_r/P₀</td><td>M <td>V <td>P_r/P₀</td><td>M <td>V </td></td></td></td></td></td></td>	V <td>P_r/P₀</td> <td>M <td>V <td>P_r/P₀</td><td>M <td>V <td>P_r/P₀</td><td>M <td>V </td></td></td></td></td></td>	P _r /P ₀	M <td>V <td>P_r/P₀</td><td>M <td>V <td>P_r/P₀</td><td>M <td>V </td></td></td></td></td>	V <td>P_r/P₀</td> <td>M <td>V <td>P_r/P₀</td><td>M <td>V </td></td></td></td>	P _r /P ₀	M <td>V <td>P_r/P₀</td><td>M <td>V </td></td></td>	V <td>P_r/P₀</td> <td>M <td>V </td></td>	P _r /P ₀	M <td>V </td>	V	
5 (hub)	.719	16.18	80.5	.794	23.57	106.3	.867	24.20	119.3	.913	29.44	106.4	.513	558	535
10	.717	12.10	83.3	.780	21.72	101.7	.857	23.58	117.5	.922	29.90	104.1	.542	589	571
15	.719	14.25	83.3	.765	28.82	99.6	.857	24.10	111.7	.919	29.58	102.6	.550	596	582
30	.719	12.10	83.2	.736	11.79	99.8	.823	25.00	105.5	.933	28.70	99.2	.586	633	635
50	.728	10.15	85.1	.725	6.91	98.5	.804	22.60	104.9	.935	25.45	97.5	.596	643	637
70	.727	8.93	85.3	.720	4.06	102.5	.913	20.55	105.0	.934	21.50	98.7	.563	610	603
85	.730	8.15	87.2	.722	4.12	100.2	.912	19.30	106.0	.936	18.54	100.4	.521	567	557
90	.731	7.92	89.2	.725	5.29	100.1	.912	18.50	106.6	.935	17.46	101.1	.503	548	538
95 (tip)	.724	7.52	85.5	.725	5.06	102.7	.870	15.08	111.3	.929	15.28	105.4	.460	504	486
MR	.725		85.7	.744		100.9	.895			.931		100.1	.539	605	596

1) Inlet plenum conditions P₀ = 1946 rbf, T₀ = 538.5 °R
 2) Vm calculation is based on standard day inlet plenum conditions
 3) Circumferential reference position is TDC looking forward
 4) Relative position of circumferential distortion screen is 210° - 330°
 5) β₇ = tan⁻¹ [tanβ₇/cos ε]

TABLE 15.7
Rotor Inlet Circumferential Distributions
Disk Probe Station 7, 100% of Design Speed, $W\sqrt{\theta} = 173.1$

Circumferential Position	24°				54°				84°				114°					
	P_7/P_0	$90-\beta_7$	M	V/V_m	P_7/P_0	$90-\beta_7$	M	V/V_m	P_7/P_0	$90-\beta_7$	M	V/V_m	P_7/P_0	$90-\beta_7$	M	V/V_m		
Span																		
5 (hub)	.926	31.70	94.5	.472	516	514	.935	31.45	96.0	.478	520	517	.946	33.80	88.9	.480	524	523
10	.925	30.65	94.2	.468	533	531	.938	30.95	95.6	.495	540	537	.948	32.58	89.8	.500	545	545
15	.927	30.20	94.3	.504	549	547	.940	30.78	94.8	.519	564	562	.947	31.78	89.9	.509	554	554
20	.941	30.30	93.7	.546	592	591	.933	27.65	94.6	.534	580	578	.943	28.30	90.0	.524	569	569
30	.943	24.70	93.0	.648	594	593	.943	24.48	94.0	.545	591	590	.946	24.60	90.1	.530	575	575
40	.944	20.80	94.6	.520	566	564	.940	20.80	94.0	.516	561	560	.945	20.86	90.9	.507	552	552
65	.943	17.07	95.6	.481	525	522	.940	17.90	93.8	.474	517	516	.943	17.80	91.4	.462	505	505
90	.946	17.03	95.9	.468	511	508	.937	16.85	93.7	.453	496	495	.939	16.60	91.7	.442	484	484
95 (tip)	.945	15.50	97.6	.436	478	474	.918	14.60	95.5	.401	441	439	.930	14.58	95.0	.401	440	439
MR	.940		94.4	.515	560	558	.938		94.4	.509	555	553	.944		90.7	.500	545	545
5 (hub)	.940	35.60	81.7	.475	519	513	.923	36.45	77.2	.469	513	500	.890	40.90	60.7	.484	528	461
10	.937	33.55	83.3	.465	529	526	.927	35.38	75.4	.493	538	528	.872	37.95	60.5	.480	524	458
15	.925	31.30	84.6	.475	519	516	.926	34.20	80.2	.509	554	546	.855	34.10	63.8	.463	507	455
30	.947	29.45	86.2	.531	577	575	.926	30.98	81.9	.524	570	564	.866	30.60	74.8	.512	558	538
50	.947	25.35	86.4	.531	579	578	.934	26.40	84.7	.547	593	591	.976	26.50	75.3	.527	573	554
70	.940	21.18	87.7	.504	549	548	.938	22.55	86.1	.534	580	579	.884	23.70	74.4	.536	582	560
85	.937	18.22	87.0	.463	506	505	.940	19.65	85.2	.498	543	541	.900	21.65	72.2	.532	578	550
90	.937	17.00	87.2	.443	485	485	.946	18.68	85.0	.483	528	526	.900	20.75	70.8	.518	563	532
95 (tip)	.927	15.22	88.1	.406	446	445	.917	16.00	84.9	.421	461	460	.870	16.90	67.2	.438	480	443
MR	.940		86.3	.498	543	542	.931		83.7	.515	560	557	.878		71.9	.512	558	530
5 (hub)	.736	16.16	92.6	.216	253	233	.602	24.20	108.2	.400	440	418	.873	23.70	119.3	.485	529	461
10	.736	15.43	92.9	.215	237	236	.784	21.95	103.9	.358	394	383	.865	23.80	116.0	.484	528	474
15	.736	15.11	91.9	.216	243	242	.773	19.70	103.0	.326	361	351	.864	25.35	110.0	.500	545	512
30	.736	13.08	92.4	.222	247	247	.741	12.47	106.5	.236	262	251	.899	25.93	105.5	.568	615	593
50	.735	10.92	93.7	.221	246	246	.737	9.94	108.8	.222	247	234	.911	22.95	105.2	.578	622	601
70	.734	9.26	95.0	.215	239	233	.733	8.90	111.7	.211	235	218	.928	20.48	105.8	.575	621	598
85	.742	9.54	95.0	.241	268	267	.734	7.64	110.5	.213	237	221	.929	17.85	106.5	.534	579	556
90	.744	9.54	95.2	.247	274	273	.734	7.40	110.5	.212	236	221	.920	16.50	107.1	.501	546	522
95 (tip)	.738	8.43	100.3	.229	254	250	.734	7.70	113.2	.212	235	216	.879	12.75	112.9	.407	447	412
MR	.737		94.2	.224	249	248	.749		108.4	.265	294	278	.906		107.3	.544	591	564

- 1) Inlet plenum conditions: $P_0 = 195$ psf, $T_0 = 536.8$ R
- 2) V_m calculation is based on standard-day inlet plenum conditions
- 3) Circumferential reference position is IDC looking forward
- 4) Relative position of circumferential distortion screen is $210^\circ - 330^\circ$
- 5) $\beta_7 = \tan^{-1} (\tan \beta_7 / \cos \epsilon)$

TABLE 15. 8
Rotor Inlet Circumferential Distributions
Disk Probe Station 7, 100% of Design Speed, $W\sqrt{\theta} = 167.2$

Circumferential Position	24°				54°				84°				114°					
	P ₇ /P ₀	90-β ² /γ	M	V	P ₇ /P ₀	90-β ² /γ	M	V	P ₇ /P ₀	90-β ² /γ	M	V	P ₇ /P ₀	90-β ² /γ	M	V		
5 (hub)	.933	30.45	92.2	.440	482	481	.946	31.00	93.0	.449	492	491	.951	31.68	96.5	.460	503	502
10	.936	29.60	93.4	.461	504	503	.946	30.45	92.9	.468	512	511	.952	30.95	87.7	.477	520	520
15	.940	29.20	93.5	.476	520	519	.948	30.00	92.4	.487	531	530	.953	30.65	87.8	.489	533	533
30	.951	27.25	92.4	.512	557	557	.959	26.60	92.4	.496	541	540	.949	27.90	87.9	.506	551	550
50	.947	22.80	92.7	.498	543	542	.948	24.40	91.9	.507	553	552	.962	24.20	88.1	.511	556	556
70	.947	19.00	93.4	.463	506	505	.945	19.60	91.9	.474	518	517	.949	20.38	89.1	.487	531	531
85	.949	16.18	95.1	.422	463	461	.941	16.80	91.6	.433	475	475	.947	17.28	89.9	.443	485	485
90	.950	15.05	95.4	.410	450	447	.939	15.75	91.8	.415	456	456	.943	15.85	91.3	.420	461	460
95 (tip)	.947	13.40	98.2	.373	411	407	.929	13.60	92.5	.365	402	402	.939	14.38	92.7	.390	429	428
MR	.947		93.7	.469	512	511	.943	92.1	.472	516	516	.949	88.8	.481	525	525		

Circumferential Position	144°				174°				204°				234°					
	P ₇ /P ₀	90-β ² /γ	M	V	P ₇ /P ₀	90-β ² /γ	M	V	P ₇ /P ₀	90-β ² /γ	M	V	P ₇ /P ₀	90-β ² /γ	M	V		
5 (hub)	.945	35.18	81.5	.469	513	507	.935	36.20	78.4	.470	513	503	.879	38.45	60.7	.455	499	434
10	.944	33.20	82.7	.484	528	524	.933	34.55	79.9	.482	526	517	.870	35.65	61.7	.453	496	437
15	.945	31.65	84.0	.478	522	519	.934	33.38	81.0	.497	541	535	.857	32.40	66.3	.444	486	445
30	.948	29.00	85.7	.519	564	563	.927	29.45	82.7	.514	559	555	.868	29.65	75.6	.495	540	523
70	.953	25.60	85.9	.530	576	575	.948	26.40	86.4	.550	597	595	.871	25.65	76.5	.510	556	540
70	.948	21.10	87.2	.502	547	546	.945	22.40	85.3	.524	570	563	.875	23.25	75.9	.503	548	532
85	.942	16.78	87.6	.436	478	478	.944	18.18	85.5	.490	514	512	.894	30.58	73.3	.504	549	526
90	.942	15.00	87.7	.398	438	438	.922	15.55	84.9	.409	449	447	.883	17.03	69.2	.440	482	451
95 (tip)	.933		86.0	.494	539	537	.939		84.2	.509	554	551	.976			.491	535	512

Circumferential Position	264°				294°				324°				354°					
	P ₇ /P ₀	90-β ² /γ	M	V	P ₇ /P ₀	90-β ² /γ	M	V	P ₇ /P ₀	90-β ² /γ	M	V	P ₇ /P ₀	90-β ² /γ	M	V		
5 (tip)	.761	13.82	97.9	.258	286	283	.836	24.42	111.2	.426	467	456	.882	23.30	119.3	.470	513	448
10	.756	16.63	97.3	.270	299	297	.827	24.38	105.4	.426	467	448	.886	22.70	118.2	.473	517	455
15	.754	18.38	97.4	.283	314	311	.814	23.22	105.0	.410	450	435	.882	23.70	112.0	.480	524	483
30	.757	16.53	97.5	.287	329	326	.768	15.20	109.4	.395	319	286	.904	24.73	107.2	.547	594	517
50	.757	14.03	97.4	.296	323	325	.757	10.70	119.9	.280	310	266	.917	21.40	107.8	.545	592	563
70	.751	11.42	101.2	.278	308	302	.760	8.76	119.9	.253	281	244	.941	18.80	108.3	.532	578	548
85	.759	11.65	98.1	.302	334	331	.761	7.64	119.8	.236	282	237	.941	16.00	109.6	.487	531	500
90	.761	11.25	97.6	.299	331	328	.760	7.09	119.8	.223	248	215	.928	14.20	112.3	.448	490	453
95 (hub)	.762	10.03	98.8	.274	303	300	.759	6.50	119.7	.209	233	202	.881	9.65	119.7	.324	358	311
MR	.757		98.3	.289	320	316	.778		114.5	.317	350	319	.916		110.0	.512	557	523

1) Inlet plenum conditions: P₀ = 1964 psf, T₀ = 539.5 R
 2) V_m calculation is based on standard-day inlet plenum conditions
 3) Circumferential reference position is TDC looking forward
 4) Relative position of circumferential distortion screen is 210° - 330°
 5) β γ = tan⁻¹ |tanβ/cos ε|

TABLE 16.1

Stator Discharge Circumferential Distributions

Disk Probe Station 12, 70% of Design Speed, $W\sqrt{\theta} = 129.8$

Circumferential Position	12°				42°				72°				102°			
	P_{12}/P_0	$90-\beta_{12}^\circ$	M	V	P_{12}/P_0	$90-\beta_{12}^\circ$	M	V	P_{12}/P_0	$90-\beta_{12}^\circ$	M	V	P_{12}/P_0	$90-\beta_{12}^\circ$	M	V
5 (hub)	1.437	91.6	.860	948	1.414	87.3	.841	928	1.397	87.6	.811	898	1.393	92.1	.818	907
10	1.381	94.2	.804	891	1.387	90.0	.807	893	1.372	90.1	.787	872	1.362	94.0	.782	869
15	1.350	94.7	.772	857	1.371	90.8	.782	877	1.360	90.9	.775	859	1.344	94.8	.760	845
30	1.299	94.7	.714	793	1.309	93.2	.786	815	1.304	93.8	.721	801	1.280	94.9	.694	773
50	1.280	92.9	.684	761	1.280	93.4	.699	775	1.265	93.8	.673	749	1.245	95.0	.649	725
70	1.244	93.7	.644	719	1.241	94.2	.652	726	1.230	93.9	.633	708	1.213	93.3	.614	685
85	1.226	93.1	.622	698	1.223	94.3	.635	709	1.215	95.5	.612	687	1.194	94.5	.589	662
90	1.211	92.6	.600	676	1.209	95.4	.609	684	1.199	95.6	.590	665	1.187	94.5	.574	648
95 (tip)	1.172	92.6	.544	616	1.178	100.8	.560	633	1.175	100.4	.547	620	1.156	94.6	.524	593
MR	1.284	93.5	.685	775	1.285	93.3	.705	784	1.275	93.6	.685	764	1.258	94.3	.669	748

Circumferential Position	132°				162°				192°				222°			
	P_{12}/P_0	$90-\beta_{12}^\circ$	M	V	P_{12}/P_0	$90-\beta_{12}^\circ$	M	V	P_{12}/P_0	$90-\beta_{12}^\circ$	M	V	P_{12}/P_0	$90-\beta_{12}^\circ$	M	V
5 (hub)	1.387	88.5	.790	878	1.379	91.6	.746	835	1.322	89.0	.698	787	1.209	87.6	.546	625
10	1.346	91.0	.756	841	1.337	93.0	.707	793	1.287	91.3	.664	750	1.184	89.8	.518	594
15	1.338	91.2	.748	832	1.320	94.0	.688	771	1.279	91.4	.656	740	1.179	91.2	.508	582
30	1.269	94.1	.697	777	1.276	94.8	.636	714	1.236	92.8	.603	680	1.155	92.4	.468	534
50	1.249	94.8	.646	722	1.234	94.8	.588	662	1.212	93.9	.571	644	1.149	92.4	.452	514
70	1.213	94.4	.607	681	1.197	94.9	.543	612	1.159	96.2	.505	572	1.133	92.3	.423	482
85	1.199	96.0	.587	661	1.180	95.9	.520	589	1.150	96.3	.486	553	1.124	90.5	.406	464
90	1.184	96.1	.565	639	1.164	95.9	.497	565	1.139	96.2	.465	531	1.117	90.5	.382	449
95 (tip)	1.101	100.3	.526	598	1.138	95.7	.444	507	1.131	96.2	.448	513	1.103	90.5	.358	412
MR	1.259	94.2	.660	739	1.246	94.6	.604	680	1.211	93.9	.572	647	1.149	91.4	.455	519

Circumferential Position	252°				282°				312°				342°			
	P_{12}/P_0	$90-\beta_{12}^\circ$	M	V	P_{12}/P_0	$90-\beta_{12}^\circ$	M	V	P_{12}/P_0	$90-\beta_{12}^\circ$	M	V	P_{12}/P_0	$90-\beta_{12}^\circ$	M	V
5 (hub)	1.136	87.8	.474	546	1.177	87.8	.557	638	1.315	90.4	.741	829	1.397	87.6	.837	924
10	1.150	86.7	.492	565	1.203	87.7	.582	663	1.308	92.3	.729	815	1.368	89.1	.827	912
15	1.171	88.4	.514	587	1.205	89.5	.581	661	1.315	92.8	.731	814	1.370	90.0	.807	891
30	1.177	92.4	.516	586	1.202	90.9	.571	646	1.312	93.2	.714	794	1.333	91.5	.761	841
50	1.170	92.4	.500	568	1.194	92.4	.555	626	1.293	93.7	.685	762	1.290	92.8	.712	790
70	1.170	90.5	.497	564	1.177	92.4	.530	599	1.275	91.1	.663	739	1.255	94.6	.671	746
85	1.165	90.5	.484	551	1.166	90.8	.514	583	1.259	91.8	.643	719	1.240	93.4	.652	728
90	1.166	90.4	.479	546	1.160	90.8	.500	569	1.238	92.6	.616	693	1.211	93.5	.615	691
95 (tip)	1.155	90.3	.452	517	1.156	90.8	.487	556	1.178	95.2	.439	611	1.193	96.2	.582	656
MR	1.187	90.8	.496	565	1.185	91.1	.545	618	1.284	92.6	.681	760	1.295	92.5	.720	799

- 1) Inlet plenum conditions $P_0 = 2012$ psf, $T_0 = 534$ °R
- 2) V_m calculation is based on standard-day inlet plenum conditions
- 3) Circumferential reference position is TDC looking forward
- 4) Relative position of circumferential distortion screen is $210^\circ-330^\circ$
- 5) $\beta_{12}^\circ = \tan^{-1} [\tan \beta_{12} / \cos \epsilon]$

TABLE 16.2

Stator Discharge Circumferential Distributions

Disk Probe Station 12, 70% of Design Speed, $\frac{W\sqrt{\theta}}{\delta} = 122.1$

Circumferential Position	12°			42°			72°			102°		
	P_{12}/P_0	V	V_m	P_{12}/P_0	V	V_m	P_{12}/P_0	V	V_m	P_{12}/P_0	V	V_m
5 (hub)	1.450	.727	818	1.418	.716	805	1.409	.702	791	1.415	.710	799
10	1.404	.687	775	1.393	.687	774	1.382	.681	767	1.377	.676	756
15	1.376	.658	744	1.378	.677	762	1.370	.672	756	1.362	.670	735
30	1.342	.621	701	1.389	.682	712	1.386	.680	710	1.384	.678	688
50	1.310	.583	660	1.310	.597	674	1.303	.593	670	1.293	.590	644
70	1.270	.545	611	1.269	.553	625	1.260	.543	617	1.250	.542	597
85	1.257	.523	600	1.260	.538	614	1.256	.532	607	1.245	.524	585
90	1.245	.504	581	1.241	.515	591	1.241	.520	596	1.233	.518	572
95 (tip)	1.235	.478	551	1.230	.488	573	1.231	.490	575	1.209	.485	523
MR	1.317	.593	672	1.312	.603	682	1.306	.597	677	1.298	.581	658

Circumferential Position	132°			162°			192°			222°		
	P_{12}/P_0	V	V_m	P_{12}/P_0	V	V_m	P_{12}/P_0	V	V_m	P_{12}/P_0	V	V_m
5 (hub)	1.403	.687	775	1.395	.665	753	1.355	.612	698	1.228	.438	506
10	1.375	.663	748	1.359	.627	711	1.323	.576	658	1.240	.451	521
15	1.363	.653	736	1.344	.611	682	1.313	.567	647	1.233	.438	506
30	1.327	.610	690	1.311	.570	647	1.290	.536	611	1.218	.405	470
50	1.299	.579	656	1.290	.533	606	1.257	.489	560	1.213	.395	454
70	1.253	.523	596	1.241	.482	551	1.234	.454	522	1.214	.395	454
85	1.249	.517	592	1.239	.479	550	1.242	.462	534	1.212	.388	449
90	1.242	.505	581	1.233	.465	536	1.231	.448	519	1.208	.383	444
95 (tip)	1.231	.491	567	1.214	.430	497	1.219	.431	501	1.196	.360	418
MR	1.300	.580	659	1.287	.543	618	1.269	.506	590	1.216	.403	465

Circumferential Position	232°			282°			312°			342°		
	P_{12}/P_0	V	V_m	P_{12}/P_0	V	V_m	P_{12}/P_0	V	V_m	P_{12}/P_0	V	V_m
5 (hub)	1.145	.317	370	1.187	.403	469	1.305	.588	671	1.410	.706	794
10	1.159	.343	399	1.211	.433	501	1.301	.583	664	1.394	.687	772
15	1.194	.405	467	1.221	.448	516	1.304	.580	659	1.378	.671	755
30	1.223	.439	504	1.243	.473	542	1.336	.595	673	1.326	.613	690
50	1.228	.442	506	1.254	.481	550	1.317	.568	645	1.278	.559	634
70	1.244	.457	523	1.249	.470	538	1.288	.538	613	1.251	.523	596
85	1.244	.450	518	1.232	.446	514	1.275	.521	597	1.225	.495	568
90	1.247	.453	522	1.224	.433	501	1.275	.514	590	1.220	.485	558
95 (tip)	1.244	.446	515	1.221	.426	494	1.268	.500	575	1.220	.478	551
MR	1.227	.437	502	1.237	.460	528	1.303	.559	636	1.295	.581	659

1) Inlet plenum conditions $P_0 = 2020$ psf, $T_0 = 525.2$ R

2) V_m calculation is based on standard-day inlet plenum conditions

3) Circumferential reference position is TDC looking forward

4) Relative position of circumferential distortion screen is 210° - 330°

5) $\beta^*_{12} = \tan^{-1} [\tan \beta_{12} / \cos \epsilon]$

TABLE 16.3
Stator Discharge Circumferential Distributions
Disk Probe Station 12, 70% of Design Speed, $W\sqrt{\theta} = 111.0$

Circumferential Position	12°				42°				72°				102°				
	P_{12}/P_0	V	V_m	M	P_{12}/P_0	V	V_m	M	P_{12}/P_0	V	V_m	M	P_{12}/P_0	V	V_m	M	
5 (hub)	1.460	739	739	.650	1.423	715	715	.629	1.418	715	715	.628	1.416	714	714	.641	728
10	1.421	689	689	.613	1.405	694	694	.610	1.398	697	697	.613	1.383	697	697	.610	694
15	1.399	674	673	.591	1.390	682	682	.600	1.383	682	682	.600	1.370	682	682	.593	674
30	1.341	604	603	.528	1.346	621	620	.544	1.355	620	620	.562	1.343	639	639	.559	636
50	1.303	545	544	.474	1.302	561	560	.490	1.306	560	560	.506	1.304	578	578	.512	586
70	1.264	487	486	.419	1.274	514	513	.446	1.293	514	514	.484	1.296	556	556	.508	574
85	1.242	452	452	.386	1.248	480	480	.413	1.270	480	480	.447	1.278	519	519	.469	545
90	1.239	440	440	.374	1.239	463	463	.397	1.263	463	463	.438	1.273	510	510	.467	544
95 (tip)	1.235	426	426	.363	1.235	456	456	.390	1.264	456	456	.443	1.268	517	517	.468	522
MR	1.321	576	576	.500	1.316	584	583	.509	1.324	603	603	.526	1.322	603	603	.533	610
132°																	
5 (hub)	1.414	717	717	.630	1.409	703	703	.617	1.373	703	703	.565	1.204	649	649	.322	376
10	1.368	689	689	.606	1.372	661	661	.579	1.353	661	661	.544	1.263	624	624	.411	476
15	1.371	674	674	.592	1.359	640	640	.561	1.342	640	640	.533	1.267	612	612	.411	476
30	1.347	635	634	.557	1.329	600	599	.526	1.314	600	599	.496	1.265	569	569	.404	466
50	1.303	580	578	.506	1.301	559	555	.487	1.293	555	555	.464	1.254	533	533	.382	441
70	1.306	580	580	.504	1.294	547	546	.474	1.285	546	546	.445	1.261	514	514	.385	446
85	1.294	566	565	.489	1.287	536	536	.462	1.264	536	536	.441	1.261	514	514	.386	450
90	1.284	549	548	.471	1.283	524	524	.451	1.275	524	524	.427	1.254	499	499	.374	437
95 (tip)	1.281	545	545	.468	1.271	504	504	.433	1.267	504	504	.421	1.243	493	493	.355	415
MR	1.326	611	610	.532	1.317	583	583	.508	1.305	583	583	.478	1.257	552	552	.386	448
192°																	
5 (hub)	1.414	717	717	.630	1.409	703	703	.617	1.373	703	703	.565	1.204	649	649	.322	376
10	1.368	689	689	.606	1.372	661	661	.579	1.353	661	661	.544	1.263	624	624	.411	476
15	1.371	674	674	.592	1.359	640	640	.561	1.342	640	640	.533	1.267	612	612	.411	476
30	1.347	635	634	.557	1.329	600	599	.526	1.314	600	599	.496	1.265	569	569	.404	466
50	1.303	580	578	.506	1.301	559	555	.487	1.293	555	555	.464	1.254	533	533	.382	441
70	1.306	580	580	.504	1.294	547	546	.474	1.285	546	546	.445	1.261	514	514	.385	446
85	1.294	566	565	.489	1.287	536	536	.462	1.264	536	536	.441	1.261	514	514	.386	450
90	1.284	549	548	.471	1.283	524	524	.451	1.275	524	524	.427	1.254	499	499	.374	437
95 (tip)	1.281	545	545	.468	1.271	504	504	.433	1.267	504	504	.421	1.243	493	493	.355	415
MR	1.326	611	610	.532	1.317	583	583	.508	1.305	583	583	.478	1.257	552	552	.386	448
252°																	
5 (hub)	1.222	409	408	.350	1.209	407	407	.349	1.324	407	407	.522	1.422	600	600	.625	711
10	1.250	455	454	.392	1.237	454	454	.391	1.325	454	454	.523	1.407	600	600	.609	692
15	1.266	484	484	.418	1.250	471	473	.408	1.327	473	473	.520	1.385	595	595	.589	671
30	1.269	483	483	.419	1.271	495	495	.430	1.357	495	495	.435	1.326	611	611	.519	593
50	1.279	492	492	.427	1.295	520	520	.452	1.346	520	520	.458	1.291	591	591	.469	538
70	1.291	511	510	.442	1.298	549	549	.471	1.308	549	549	.470	1.245	541	541	.399	463
85	1.283	495	495	.425	1.260	474	472	.406	1.297	472	472	.454	1.221	529	529	.361	422
90	1.278	482	482	.413	1.264	477	477	.411	1.295	477	477	.438	1.213	522	522	.345	404
95 (tip)	1.270	470	470	.402	1.267	470	477	.410	1.290	477	477	.431	1.209	503	503	.340	399
MR	1.375	611	610	.532	1.368	583	583	.508	1.326	583	583	.478	1.257	552	552	.386	448
342°																	
5 (hub)	1.222	409	408	.350	1.209	407	407	.349	1.324	407	407	.522	1.422	600	600	.625	711
10	1.250	455	454	.392	1.237	454	454	.391	1.325	454	454	.523	1.407	600	600	.609	692
15	1.266	484	484	.418	1.250	471	473	.408	1.327	473	473	.520	1.385	595	595	.589	671
30	1.269	483	483	.419	1.271	495	495	.430	1.357	495	495	.435	1.326	611	611	.519	593
50	1.279	492	492	.427	1.295	520	520	.452	1.346	520	520	.458	1.291	591	591	.469	538
70	1.291	511	510	.442	1.298	549	549	.471	1.308	549	549	.470	1.245	541	541	.399	463
85	1.283	495	495	.425	1.260	474	472	.406	1.297	472	472	.454	1.221	529	529	.361	422
90	1.278	482	482	.413	1.264	477	477	.411	1.295	477	477	.438	1.213	522	522	.345	404
95 (tip)	1.270	470	470	.402	1.267	470	477	.410	1.290	477	477	.431	1.209	503	503	.340	399
MR	1.375	611	610	.532	1.368	583	583	.508	1.326	583	583	.478	1.257	552	552	.386	448

- 1) Inlet plenum conditions $P_0 = 2037$ psf, $T_0 = 529.3$ °R
- 2) V_m calculation is based on standard-day inlet plenum conditions
- 3) Circumferential reference position is TDC looking forward
- 4) Relative position of circumferential distortion is $210^\circ\text{-}330^\circ$
- 5) $\beta_{*12} = \tan^{-1} [\tan \beta_{12} / \cos \epsilon]$

TABLE 16.4
 Stator Discharge Circumferential Distributions
 Disk Probe Station 12, 90% of Design Speed, $\frac{W\sqrt{\theta}}{\delta} = 164.8$

Circumferential Position	42°				72°				132°			
	P_{12}/P_0	$90-\beta_{12}^\circ$	M	V_m	P_{12}/P_0	$90-\beta_{12}^\circ$	M	V_m	P_{12}/P_0	$90-\beta_{12}^\circ$	M	V_m
5 (hub)	1.481	93.8	.903	1022	1.520	95.6	.986	1089	1.499	95.4	1.073	1110
10	1.570	93.4	1.054	1161	1.547	95.2	1.036	1134	1.524	94.4	1.047	1148
15	1.638	92.8	1.105	1203	1.622	93.9	1.106	1197	1.581	93.6	1.100	1195
30	1.563	92.7	1.027	1124	1.575	93.1	1.036	1123	1.538	91.9	1.030	1125
50	1.556	91.3	.995	1091	1.540	91.8	.989	1082	1.486	91.9	.960	1060
70	1.494	91.3	.938	1035	1.492	92.1	.956	1050	1.443	92.6	.905	1006
85	1.476	91.3	.898	1000	1.468	92.7	.919	1020	1.444	92.4	.894	1000
90	1.459	90.2	.873	979	1.449	91.3	.879	983	1.439	91.2	.874	982
95 (tip)	1.426	94.8	.807	917	1.404	96.1	.807	908	1.390	96.9	.796	907
MR	1.527	92.1	.968	1070	1.523	93.0	.980	1077	1.485	92.9	.959	1062

Circumferential Position	192°				282°				342°			
	P_{12}/P_0	$90-\beta_{12}^\circ$	M	V_m	P_{12}/P_0	$90-\beta_{12}^\circ$	M	V_m	P_{12}/P_0	$90-\beta_{12}^\circ$	M	V_m
5 (hub)	1.358	89.4	.819	940	1.136	88.0	.548	648	1.489	92.3	.895	1012
10	1.371	88.0	.843	961	1.204	86.1	.619	726	1.547	91.3	.990	1100
15	1.467	80.1	.904	1017	1.290	88.1	.696	807	1.608	91.3	1.067	1168
30	1.420	91.4	.862	969	1.305	90.5	.713	817	1.602	91.5	1.014	1112
50	1.359	91.8	.799	905	1.296	93.6	.693	793	1.587	90.6	.968	1067
70	1.314	94.0	.739	843	1.297	91.6	.685	786	1.512	90.6	.901	1002
85	1.319	92.5	.737	844	1.318	87.9	.694	798	1.489	91.3	.878	985
90	1.302	93.9	.706	814	1.330	87.8	.691	796	1.438	90.7	.832	943
95 (tip)	1.271	98.9	.656	762	1.327	90.6	.668	774	1.398	96.0	.768	880
MR	1.361	92.4	.795	904	1.296	90.6	.687	791	1.541	91.4	.942	1046

1) Inlet plenum conditions $P_0 = 1968$ psf, $T_0 = 536.2$
 2) V_m calculation is based on standard-day inlet conditions
 3) Circumferential reference position is TDC looking forward
 4) Relative position of circumferential distortion screen is $210^\circ-330^\circ$
 5) $\beta_{12} = \tan^{-1} [\tan \beta_{12} / \cos \epsilon]$

TABLE 16.5
Stator Discharge Circumferential Distributions
Disk Probe Station 12, 90% of Design Speed, $W\sqrt{\theta} = 156.2$

Circumferential Position	42°				72°				132°				
	P_{12}/P_0	$90-\beta_{12}$	M	V	P_{12}/P_0	$90-\beta_{12}$	M	V	P_{12}/P_0	$90-\beta_{12}$	M	V	V_{in}
% Span													
5 (hub)	1.431	89.5	.714	830	1.451	89.2	.732	847	1.484	89.4	.732	846	846
10	1.576	86.1	.824	940	1.534	86.5	.802	915	1.519	87.3	.767	881	880
15	1.655	89.7	.873	989	1.628	89.8	.856	968	1.617	88.8	.830	943	943
30	1.600	90.0	.840	950	1.583	89.9	.834	941	1.570	91.0	.791	901	901
50	1.543	89.7	.777	885	1.555	89.7	.787	895	1.523	91.4	.745	855	855
70	1.482	93.1	.715	824	1.483	92.9	.720	829	1.466	93.7	.690	801	800
85	1.489	91.3	.715	830	1.499	90.7	.725	840	1.486	92.0	.699	817	816
90	1.464	91.7	.687	803	1.487	91.3	.707	824	1.478	92.1	.687	808	807
95 (tip)	1.440	91.9	.662	778	1.442	94.0	.664	780	1.430	94.0	.644	762	761
MR	1.532	90.7	.769	882	1.531	90.8	.770	882	1.516	91.6	.739	853	853

Circumferential Position	192°				282°				342°				
	P_{12}/P_0	$90-\beta_{12}$	M	V	P_{12}/P_0	$90-\beta_{12}$	M	V	P_{12}/P_0	$90-\beta_{12}$	M	V	V_{in}
5 (hub)	1.430	90.2	.620	730	1.269	89.6	.437	523	1.446	89.6	.688	803	803
10	1.480	90.1	.652	764	1.307	89.6	.479	570	1.529	88.1	.752	867	866
15	1.536	90.6	.696	808	1.332	90.7	.507	600	1.592	88.6	.794	909	909
30	1.494	93.1	.658	763	1.382	89.4	.551	644	1.596	88.6	.793	901	901
50	1.475	93.2	.638	740	1.398	92.6	.558	653	1.523	91.5	.727	833	833
70	1.440	94.9	.596	700	1.412	92.6	.575	674	1.418	95.0	.635	739	736
85	1.438	91.9	.591	699	1.407	92.6	.568	670	1.345	91.3	.568	669	669
90	1.439	91.9	.604	715	1.352	92.7	.512	608	1.317	89.2	.537	638	638
95 (tip)	1.429	92.0	.590	701	1.319	89.8	.468	559	1.298	89.3	.513	611	611
MR	1.469	92.7	.630	737	1.378	91.5	.544	640	1.484	90.8	.702	811	811

- 1) Inlet plenum conditions $P_0 = 1977$ psf, $T_0 = 536.1$ R
- 2) V_m calculations is based on standard-day inlet conditions
- 3) Circumferential reference position is TDC looking forward
- 4) Relative position of circumferential distortion screen is $210^\circ-330^\circ$
- 5) $\beta_{12} = \tan^{-1} [\tan \beta_{12} / \cos \epsilon]$

TABLE 16.6

Stator Discharge Circumferential Distributions

Disk Probe Station 12, 100% of Design Speed, $\frac{W\sqrt{\theta}}{\delta} = 178.2$

Circumferential Position	12°			42°			72°			102°		
	P_{12}/P_0	$90-\beta$	V_m	P_{12}/P_0	$90-\beta$	V_m	P_{12}/P_0	$90-\beta$	V_m	P_{12}/P_0	$90-\beta$	V_m
5 (mid)	1.738	94.9	1.118	1.648	93.6	1.037	1.720	94.4	1.101	1.838	95.7	1.147
10	1.739	94.9	1.118	1.775	93.5	1.108	1.762	93.6	1.112	1.779	95.8	1.133
15	1.740	96.1	1.109	1.779	93.0	1.106	1.760	93.7	1.106	1.735	97.6	1.116
20	1.744	94.1	1.109	1.750	92.1	1.071	1.718	92.2	1.061	1.643	95.6	1.100
30	1.588	98.2	1.041	1.587	94.6	0.978	1.600	94.6	0.982	1.564	97.1	1.032
40	1.492	94.7	0.935	1.532	92.3	0.909	1.532	93.2	0.925	1.491	97.2	0.958
50	1.451	93.3	0.868	1.500	92.6	0.871	1.510	92.0	0.892	1.472	94.8	0.898
60	1.418	93.4	0.829	1.461	91.4	0.832	1.462	92.5	0.839	1.453	93.6	0.868
70	1.386	90.5	0.765	1.437	94.9	0.785	1.430	95.8	0.787	1.420	91.0	0.788
80	1.597	95.0	1.011	1.613	93.1	0.976	1.608	93.5	0.985	1.585	96.0	1.018
MR												
5	1.698	94.6	1.102	1.755	95.7	1.137	1.575	93.7	1.050	1.444	91.7	0.858
10	1.719	93.6	1.109	1.687	95.8	1.123	1.593	92.2	1.102	1.394	91.8	0.819
15	1.708	94.0	1.099	1.661	96.9	1.112	1.566	93.3	1.043	1.364	93.7	0.782
20	1.666	92.5	1.050	1.599	96.9	1.096	1.529	91.9	1.011	1.302	94.6	0.720
30	1.609	92.6	1.010	1.519	97.0	1.002	1.481	92.5	0.939	1.274	94.3	0.688
40	1.519	93.1	0.941	1.455	97.1	0.897	1.416	91.4	0.871	1.248	94.2	0.660
50	1.522	93.1	0.900	1.455	94.0	0.881	1.414	90.5	0.851	1.243	91.0	0.646
60	1.503	91.9	0.878	1.448	92.8	0.859	1.397	91.1	0.817	1.262	88.4	0.656
70	1.464	95.7	0.818	1.394	90.6	0.771	1.368	96.5	0.759	1.244	88.4	0.610
80	1.595	93.2	0.955	1.540	95.9	0.994	1.475	92.3	0.936	1.295	93.0	0.708
MR												
5	1.120	89.0	0.563	1.268	86.9	0.732	1.465	94.8	1.001	1.631	91.2	0.952
10	1.110	87.8	0.546	1.332	85.8	0.772	1.484	96.2	0.975	1.673	91.2	1.004
15	1.154	87.7	0.589	1.361	86.3	0.797	1.509	96.2	1.024	1.702	91.2	1.025
20	1.272	90.3	0.696	1.367	89.8	0.793	1.561	96.1	1.030	1.797	90.6	1.054
30	1.285	90.4	0.705	1.364	91.0	0.779	1.581	96.1	1.024	1.713	93.1	1.016
40	1.288	90.3	0.692	1.372	88.6	0.768	1.607	94.9	1.022	1.570	93.1	0.984
50	1.266	90.3	0.681	1.369	87.1	0.755	1.586	92.8	0.979	1.534	90.6	0.864
60	1.295	90.3	0.676	1.368	87.2	0.754	1.555	91.1	0.896	1.455	91.3	0.795
70	1.264	90.2	0.628	1.367	91.8	0.715	1.477	91.5	0.797	1.414	96.2	0.741
80	1.259	90.0	0.673	1.362	89.0	0.770	1.560	94.9	0.936	1.646	91.7	0.957
MR												

1) Inlet plenum conditions $P_0 = 1946$ psf, $T_0 = 538.5$ °R

2) V_m calculation is based on standard-day inlet plenum conditions

3) Circumferential reference position is TDC looking forward

4) Relative position of circumferential distortion screen is 210°-330°

5) $\beta^*_{12} = \tan^{-1} [\tan \beta_{12} / \cos \epsilon]$

TABLE 16.7
Stator Discharge Circumferential Distributions
Disk Probe Station 12, 100% of Design Speed, $W\sqrt{\theta} = 173.1$

Circumferential Position	12°				42°				72°				102°				
	P_{12}/P_0	$90-\beta_{12}$	M	V	P_{12}/P_0	$90-\beta_{12}$	M	V	P_{12}/P_0	$90-\beta_{12}$	M	V	P_{12}/P_0	$90-\beta_{12}$	M	V	
5 (hub)	1.627	92.9	1.065	1197	1196	1.624	91.3	.893	1028	1028	1.651	90.6	.872	1003	1003	1.832	94.3
10	1.815	96.6	1.008	1142	1138	1.736	91.2	1.024	1154	1153	1.779	90.3	1.007	1131	1131	1.787	94.3
15	1.813	94.9	.967	1119	1115	1.751	91.2	1.032	1162	1161	1.783	90.3	1.013	1136	1136	1.774	96.9
30	1.779	92.6	.943	1070	1069	1.756	89.8	1.008	1130	1130	1.733	90.3	.922	1043	1043	1.661	94.7
50	1.644	94.7	.823	952	949	1.650	91.4	.891	1017	1017	1.642	90.9	.844	968	968	1.623	94.2
70	1.611	94.4	.769	898	896	1.579	91.9	.819	943	943	1.566	94.1	.765	888	888	1.545	95.7
85	1.598	91.4	.753	890	890	1.559	91.4	.793	925	925	1.558	91.6	.762	888	888	1.549	92.7
90	1.570	91.0	.723	861	861	1.524	92.3	.758	894	893	1.527	92.5	.724	851	850	1.523	92.4
95 (tip)	1.524	89.4	.693	817	817	1.468	94.4	.721	857	855	1.483	94.9	.683	809	806	1.463	91.9
MR	1.639	93.3	.861	985	993	1.641	91.4	.892	1022	1022	1.639	91.7	.846	972	972	1.635	94.4

Circumferential Position	132°				162°				192°				222°				
	P_{12}/P_0	$90-\beta_{12}$	M	V	P_{12}/P_0	$90-\beta_{12}$	M	V	P_{12}/P_0	$90-\beta_{12}$	M	V	P_{12}/P_0	$90-\beta_{12}$	M	V	
5 (hub)	1.642	89.0	.840	972	972	1.777	91.8	.971	1107	1107	1.558	90.4	.692	823	823	1.476	86.0
10	1.753	88.7	.925	1056	1055	1.730	92.0	.900	1034	1033	1.643	89.1	.747	880	879	1.474	88.0
15	1.761	90.3	.917	1046	1046	1.709	93.4	.871	1004	1002	1.630	90.8	.735	866	866	1.464	90.7
30	1.702	90.6	.862	968	968	1.641	96.4	.798	923	919	1.591	93.2	.700	822	821	1.431	90.8
50	1.649	90.4	.803	931	931	1.570	94.5	.735	859	856	1.582	93.3	.680	802	801	1.415	90.8
70	1.556	94.4	.725	862	850	1.508	94.0	.683	803	801	1.503	93.6	.615	733	731	1.408	90.9
85	1.556	93.0	.720	855	853	1.507	92.0	.674	800	799	1.491	93.9	.588	708	706	1.389	90.8
90	1.532	93.4	.696	833	832	1.489	92.0	.653	778	778	1.475	93.7	.578	701	699	1.389	90.8
95 (tip)	1.492	93.8	.661	796	795	1.430	91.9	.602	722	722	1.447	93.9	.560	681	679	1.379	90.7
MR	1.629	91.7	.797	928	928	1.590	93.6	.764	892	890	1.549	92.9	.660	784	783	1.422	90.5

Circumferential Position	252°				312°				342°								
	P_{12}/P_0	$90-\beta_{12}$	M	V	P_{12}/P_0	$90-\beta_{12}$	M	V	P_{12}/P_0	$90-\beta_{12}$	M	V	P_{12}/P_0	$90-\beta_{12}$	M	V	
5 (hub)	1.211	90.8	.227	279	279	1.404	90.2	.679	698	698	1.453	87.7	.639	761	760	1.609	89.1
10	1.200	91.5	.208	255	255	1.448	90.1	.618	738	738	1.447	90.1	.639	758	758	1.638	88.7
15	1.215	91.5	.246	304	304	1.461	91.4	.624	744	744	1.496	92.6	.669	790	789	1.728	88.8
30	1.312	92.2	.407	490	490	1.513	91.2	.655	771	771	1.585	93.0	.720	843	841	1.754	88.8
50	1.495	90.7	.602	713	713	1.553	92.9	.676	795	794	1.699	90.1	.697	822	822	1.646	91.3
70	1.591	90.8	.678	795	795	1.562	93.8	.704	826	824	1.587	90.1	.681	791	791	1.591	90.4
85	1.633	87.9	.706	829	829	1.522	92.5	.662	787	786	1.546	90.0	.646	777	777	1.491	90.4
90	1.641	87.6	.703	829	828	1.391	89.9	.550	664	664	1.537	90.0	.646	777	777	1.467	86.3
95 (tip)	1.634	87.7	.688	812	812	1.393	89.9	.545	661	661	1.533	89.9	.634	764	764	1.459	86.4
MR	1.516	90.1	.617	731	731	1.515	92.1	.655	776	775	1.559	91.3	.688	814	814	1.624	90.3

- 1) Inlet plenum conditions $P_0 = 1955$ psf, $T_0 = 536.8$ R
- 2) V_m calculation is based on standard-day inlet plenum conditions
- 3) Circumferential reference position is TDC looking forward
- 4) Relative position of circumferential distortion screen is $210^\circ\text{-}330^\circ$
- 5) $\beta_{12} = \tan^{-1} [\tan \beta_{12} / \cos \epsilon]$

TABLE 16.8
Stator Discharge Circumferential Distributions
Disk Probe Station 12, 100% of Design Speed, $\frac{W\sqrt{\theta}}{\delta} = 167.2$

Circumferential Position	12°			42°			72°			102°		
	$\frac{P_{12}}{P_0}$	$\frac{V_m}{V}$	$\frac{M}{M}$	$\frac{P_{12}}{P_0}$	$\frac{V_m}{V}$	$\frac{M}{M}$	$\frac{P_{12}}{P_0}$	$\frac{V_m}{V}$	$\frac{M}{M}$	$\frac{P_{12}}{P_0}$	$\frac{V_m}{V}$	$\frac{M}{M}$
5 (hub)	1.591	1006	.865	1.768	1006	.832	1.701	969	.823	956	.995	1131
10	1.873	996	.857	1.832	1007	.871	1.806	1007	.881	1012	.915	1050
15	1.861	980	.844	1.831	1008	.872	1.807	1008	.884	1014	.887	1020
30	1.795	903	.774	1.797	903	.825	1.770	89.8	.844	970	.772	897
50	1.631	91.1	.653	1.681	775	.736	1.710	90.5	.788	915	.743	873
70	1.594	91.1	.554	1.593	669	.659	1.654	88.4	.718	865	.728	866
85	1.440	91.2	.499	1.425	612	.609	1.634	89.7	.701	838	.710	849
90	1.420	91.1	.470	1.491	579	.574	1.619	88.7	.685	822	.662	796
95 (tip)	1.412	91.0	.448	1.469	553	.552	1.601	88.7	.685	822	.662	796
MIR	1.668	91.7	.698	1.679	828	.743	1.703	90.0	.786	918	.661	934

Circumferential Position	132°			162°			192°			222°		
	$\frac{P_{12}}{P_0}$	$\frac{V_m}{V}$	$\frac{M}{M}$	$\frac{P_{12}}{P_0}$	$\frac{V_m}{V}$	$\frac{M}{M}$	$\frac{P_{12}}{P_0}$	$\frac{V_m}{V}$	$\frac{M}{M}$	$\frac{P_{12}}{P_0}$	$\frac{V_m}{V}$	$\frac{M}{M}$
5 (hub)	1.673	930	.796	1.792	929	.837	1.825	89.7	.678	809	.452	551
10	1.757	978	.894	1.751	978	.799	1.874	90.7	.701	832	.503	609
15	1.747	93.8	.839	1.730	972	.765	1.859	90.8	.696	825	.531	640
30	1.728	90.0	.813	1.685	943	.734	1.836	92.6	.667	790	.516	619
50	1.711	90.8	.777	1.638	908	.686	1.845	92.6	.664	786	.502	604
70	1.644	82.2	.727	1.570	862	.632	1.873	92.9	.606	728	.475	580
85	1.639	82.7	.710	1.589	853	.619	1.846	93.0	.575	699	.475	580
90	1.617	83.0	.689	1.546	834	.603	1.843	93.1	.568	694	.461	567
95 (tip)	1.573	81.7	.667	1.492	811	.587	1.818	93.1	.553	676	.444	546
MIR	1.683	90.9	.766	1.639	902	.698	1.607	92.3	.640	765	.497	602

Circumferential Position	282°			312°			342°					
	$\frac{P_{12}}{P_0}$	$\frac{V_m}{V}$	$\frac{M}{M}$	$\frac{P_{12}}{P_0}$	$\frac{V_m}{V}$	$\frac{M}{M}$	$\frac{P_{12}}{P_0}$	$\frac{V_m}{V}$	$\frac{M}{M}$			
5 (hub)	1.277	249	.202	1.423	249	.516	1.530	708	.591	709	.724	855
10	1.272	268	.216	1.473	267	.559	1.541	726	.608	726	.780	913
15	1.289	315	.257	1.480	315	.563	1.587	765	.644	766	.788	919
30	1.379	484	.400	1.623	483	.684	1.681	817	.693	817	.756	861
50	1.576	91.7	.598	1.568	712	.612	1.698	814	.688	814	.641	760
70	1.685	91.1	.681	1.600	95.8	.648	1.700	806	.676	807	.490	594
85	1.733	91.2	.700	1.495	835	.679	1.639	770	.634	770	.457	560
90	1.734	87.1	.702	1.351	838	.628	1.618	751	.615	751	.435	529
95 (tip)	1.728	85.9	.693	1.329	827	.604	1.612	732	.599	732	.422	522
MIR	1.603	90.9	.617	1.523	737	.569	1.656	789	.661	789	.650	774

- 1) Inlet plenum conditions $P_0 = 1964$ psf, $T_0 = 539.5$ °R
- 2) V_m calculation is based on standard-day inlet plenum conditions
- 3) Circumferential reference position is TDC looking forward
- 4) Relative position of circumferential distortion screen is $210^\circ - 330^\circ$
- 5) $\beta_{12}^\circ = \tan^{-1} [\tan \beta_{12} / \cos \epsilon]$

TABLE 17.1
Stator Discharge Circumferential Distributions
Temperature Rakes 70% Speed

Inlet Plenum Conditions: $P_0 = 2020$ psf $T_0 = 525.2$ °R	Circumferential Position											
	28°	56°	84°	112°	140°	168°	196°	224°	252°	280°	308°	336°
$\frac{W\sqrt{\theta}}{\delta} = 129.8$	$\frac{T_{12}}{T_0}$	$\frac{T_{12}}{T_0}$	$\frac{T_{12}}{T_0}$	$\frac{T_{12}}{T_0}$	$\frac{T_{12}}{T_0}$	$\frac{T_{12}}{T_0}$	$\frac{T_{12}}{T_0}$	$\frac{T_{12}}{T_0}$	$\frac{T_{12}}{T_0}$	$\frac{T_{12}}{T_0}$	$\frac{T_{12}}{T_0}$	$\frac{T_{12}}{T_0}$
5 (amb)	1.1307	1.1199	1.1173	1.1106	1.1138	1.1027	1.0938	1.0868	1.1011	1.1230	1.1416	1.1392
10	1.1203	1.1094	1.1079	1.1009	1.1048	1.0915	1.0848	1.0796	1.0974	1.1161	1.1294	1.1238
15	1.1129	1.1044	1.1027	1.0973	1.0978	1.0864	1.0769	1.0735	1.1108	1.1108	1.1203	1.1114
30	1.0963	1.0930	1.0923	1.0888	1.0873	1.0794	1.0643	1.0735	1.0945	1.1092	1.1164	1.1029
50	1.0864	1.0838	1.0816	1.0804	1.0805	1.0749	1.0571	1.0791	1.0985	1.1102	1.1079	1.0941
70	1.0817	1.0767	1.0752	1.0732	1.0747	1.0682	1.0524	1.0842	1.0984	1.1134	1.1090	1.0887
85	1.0840	1.0789	1.0777	1.0742	1.0772	1.0680	1.0554	1.0865	1.1102	1.1237	1.1222	1.0910
90	1.0850	1.0825	1.0818	1.0779	1.0800	1.0698	1.0586	1.0881	1.1147	1.1251	1.1260	1.0948
95 (top)	1.0906	1.0847	1.0837	1.0811	1.0833	1.0735	1.0615	1.0909	1.1179	1.1277	1.1347	1.0970
MR	1.0950	1.0893	1.0877	1.0842	1.0853	1.0770	1.0632	1.0912	1.1149	1.1149	1.1179	1.1001

Inlet Plenum Conditions: $P_0 = 2012$ psf $T_0 = 534$ °R

$$\frac{W\sqrt{\theta}}{\delta} = 122.1$$

5	1.1285	1.1191	1.1181	1.1137	1.1159	1.1075	1.1006	1.0914	1.1023	1.1191	1.1406	1.1429
10	1.1182	1.1095	1.1101	1.1057	1.1071	1.1003	1.0922	1.0851	1.0989	1.1137	1.1320	1.1299
15	1.1136	1.1046	1.1043	1.1014	1.1038	1.0948	1.0863	1.0846	1.0979	1.1106	1.1259	1.1188
30	1.1009	1.0971	1.0967	1.0935	1.0938	1.0903	1.0787	1.0864	1.0991	1.1139	1.1235	1.1090
50	1.0961	1.0903	1.0921	1.0904	1.0888	1.0845	1.0737	1.0828	1.0885	1.1210	1.1227	1.1042
70	1.0938	1.0879	1.0872	1.0876	1.0854	1.0836	1.0711	1.0806	1.1194	1.1329	1.1366	1.1093
85	1.1045	1.0946	1.0927	1.0925	1.0896	1.0873	1.0767	1.1074	1.1289	1.1454	1.1584	1.1290
90	1.1099	1.1002	1.0979	1.0982	1.0934	1.0923	1.0827	1.1117	1.1348	1.1493	1.1634	1.1282
95	1.1142	1.1035	1.1016	1.1024	1.0993	1.0977	1.0882	1.1140	1.1386	1.1539	1.1695	1.1342
MR	1.1041	1.0970	1.0967	1.0949	1.0934	1.0899	1.0797	1.0953	1.1119	1.1285	1.1355	1.1158

Inlet Plenum Conditions: $P_0 = 2020$ psf $T_0 = 525.2$ °R

$$\frac{W\sqrt{\theta}}{\delta} = 111.0$$

5	1.1322	1.1219	1.1219	1.1142	1.1155	1.1085	1.1053	1.0975	1.1043	1.1297	1.1414	1.1423
10	1.1237	1.1146	1.1120	1.1074	1.1091	1.1026	1.0988	1.0905	1.1022	1.1227	1.1330	1.1314
15	1.1177	1.1086	1.1066	1.1029	1.1034	1.0985	1.0913	1.0884	1.1012	1.1198	1.1254	1.1192
30	1.1046	1.1037	1.1009	1.0988	1.0986	1.0952	1.0860	1.0952	1.1053	1.1193	1.1230	1.1147
50	1.1037	1.0981	1.0957	1.0958	1.0942	1.0911	1.0827	1.1010	1.1145	1.1306	1.1252	1.1164
70	1.1117	1.1097	1.1025	1.0960	1.0943	1.0932	1.0826	1.1111	1.1241	1.1399	1.1375	1.1256
85	1.1239	1.1230	1.1152	1.1086	1.1018	1.1038	1.0918	1.1190	1.1371	1.1525	1.1558	1.1366
90	1.1305	1.1285	1.1180	1.1124	1.1071	1.1080	1.0974	1.1225	1.1426	1.1578	1.1639	1.1406
95	1.1387	1.1327	1.1242	1.1165	1.1104	1.1116	1.1026	1.1262	1.1457	1.1634	1.1716	1.1445
MR	1.1149	1.1105	1.1060	1.1025	1.1003	1.0979	1.0892	1.1037	1.1178	1.1341	1.1364	1.1252

Inlet Plenum Conditions: $P_0 = 2037$ psf $T_0 = 529.3$ °R

TABLE 17.2
Stator Discharge Circumferential Distributions
Temperature Rakes 90% Speed

% Span	Circumferential Position											
	26°	56°	8°	116°	146°	176°	206°	236°	266°	296°	326°	356°
$\frac{W\sqrt{\theta}}{\delta} = 164.8 \frac{T_{12}}{T_0}$	$\frac{T_{12}}{T_0}$	$\frac{T_{12}}{T_0}$	$\frac{T_{12}}{T_0}$	$\frac{T_{12}}{T_0}$	$\frac{T_{12}}{T_0}$	$\frac{T_{12}}{T_0}$	$\frac{T_{12}}{T_0}$	$\frac{T_{12}}{T_0}$	$\frac{T_{12}}{T_0}$	$\frac{T_{12}}{T_0}$	$\frac{T_{12}}{T_0}$	$\frac{T_{12}}{T_0}$
5	1.2162	1.2011	1.1971	1.1780	1.1861	1.1745	1.1579	1.1366	1.1551	1.1823	1.2227	1.2362
10	1.2013	1.1886	1.1842	1.1677	1.1749	1.1711	1.1467	1.1177	1.1487	1.1783	1.2098	1.2195
15	1.1904	1.1822	1.1785	1.1640	1.1618	1.1565	1.1360	1.1103	1.1565	1.1744	1.2044	1.2058
30	1.1780	1.1718	1.1650	1.1563	1.1496	1.1379	1.1127	1.1018	1.1563	1.1719	1.2101	1.1971
50	1.1799	1.1661	1.1589	1.1517	1.1465	1.1350	1.1020	1.1083	1.1652	1.1716	1.2167	1.1939
70	1.1655	1.1559	1.1539	1.1486	1.1457	1.1338	1.1004	1.1139	1.1705	1.1838	1.2163	1.1729
85	1.1716	1.1534	1.1581	1.1531	1.1482	1.1341	1.1038	1.1152	1.1927	1.1995	1.2308	1.1766
90	1.1810	1.1614	1.1673	1.1598	1.1531	1.1370	1.1100	1.1166	1.2027	1.2094	1.2432	1.1845
95	1.1865	1.1682	1.1731	1.1656	1.1616	1.1427	1.1161	1.1187	1.2115	1.2205	1.2584	1.1903
	1.1803	1.1683	1.1655	1.1568	1.1531	1.1415	1.1134	1.1122	1.1695	1.1831	1.2200	1.1923

Inlet Plenum Conditions: $P_0 = 1968$ psf $T_0 = 536.2$ °R

$$\frac{W\sqrt{\theta}}{\delta} = 156.2$$

5	1.2065	1.1959	1.1906	1.1818	1.1859	1.1739	1.1650	1.1450	1.1626	1.1818	1.2264	1.2274
10	1.1991	1.1864	1.1812	1.1690	1.1767	1.1651	1.1582	1.1362	1.1624	1.1769	1.2173	1.2153
15	1.1907	1.1764	1.1732	1.1627	1.1654	1.1552	1.1484	1.1319	1.1660	1.1758	1.2088	1.2050
30	1.1802	1.1679	1.1601	1.1580	1.1527	1.1438	1.1344	1.1380	1.1815	1.1803	1.2052	1.1914
50	1.1748	1.1610	1.1585	1.1544	1.1500	1.1460	1.1287	1.1521	1.1992	1.1994	1.2114	1.1847
70	1.1752	1.1619	1.1580	1.1563	1.1523	1.1459	1.1295	1.1674	1.2162	1.2249	1.2216	1.1980
85	1.2011	1.1636	1.1624	1.1600	1.1561	1.1479	1.1365	1.1753	1.2372	1.2565	1.2427	1.2257
90	1.2092	1.1729	1.1702	1.1686	1.1620	1.1540	1.1430	1.1775	1.2407	1.2672	1.2543	1.2333
95	1.2238	1.1798	1.1766	1.1747	1.1710	1.1609	1.1487	1.1814	1.2468	1.2729	1.2694	1.2447
	1.1877	1.1693	1.1651	1.1610	1.1582	1.1505	1.1381	1.1538	1.2005	1.2107	1.2222	1.2047

Inlet Plenum Conditions: $P_0 = 1977$ psf $T_0 = 536.1$ °R

TABLE 17.3
Stator Discharge Circumferential Distributions
Temperature Rakes 100% Speed

$\frac{W\sqrt{\theta}}{\delta} = 178.2$	Circumferential Position											
	26°	56°	86°	116°	146°	176°	206°	236°	266°	296°	326°	356°
	T_{12}/T_0	T_{12}/T_0	T_{12}/T_0	T_{12}/T_0	T_{12}/T_0	T_{12}/T_0	T_{12}/T_0	T_{12}/T_0	T_{12}/T_0	T_{12}/T_0	T_{12}/T_0	T_{12}/T_0
5	1.2557	1.2439	1.2432	1.2181	1.2216	1.2070	1.1989	1.1621	1.1827	1.2198	1.2694	1.2781
10	1.2463	1.2325	1.2346	1.2071	1.2138	1.1985	1.1915	1.1436	1.1746	1.2163	1.2571	1.2649
15	1.2380	1.2245	1.2272	1.2013	1.2042	1.1893	1.1799	1.1347	1.1750	1.2142	1.2535	1.2539
30	1.2373	1.2166	1.2143	1.1952	1.1968	1.1845	1.1493	1.1193	1.1849	1.2098	1.2624	1.2535
50	1.2195	1.2105	1.2110	1.1959	1.1887	1.1692	1.1347	1.1268	1.1895	1.2156	1.2664	1.2232
70	1.2060	1.1890	1.1941	1.1812	1.1766	1.1629	1.1307	1.1364	1.1966	1.2284	1.2589	1.2044
85	1.2107	1.1894	1.1996	1.1926	1.1836	1.1641	1.1370	1.1425	1.2177	1.2395	1.2551	1.2160
90	1.2248	1.1996	1.2084	1.2017	1.1896	1.1696	1.1475	1.1449	1.2242	1.2511	1.2651	1.2244
95	1.2362	1.2074	1.2168	1.2086	1.1974	1.1799	1.1597	1.1476	1.2304	1.2615	1.2812	1.2310
MR	1.2253	1.2087	1.2120	1.1962	1.1903	1.1735	1.1493	1.1346	1.1945	1.2241	1.2625	1.2324

Inlet Plenum Conditions: $P_0 = 1946$ psf $T_0 = 538.5$ °R

$$\frac{W\sqrt{\theta}}{\delta} = 173.1$$

5	1.2545	1.2352	1.2368	1.2216	1.2262	1.2094	1.1976	1.1651	1.1912	1.2289	1.2736	1.2785
10	1.2434	1.2323	1.2336	1.2187	1.2207	1.2028	1.1896	1.1613	1.1882	1.2198	1.2674	1.2678
15	1.2303	1.2218	1.2220	1.2069	1.2090	1.1945	1.1819	1.1589	1.1874	1.2140	1.2606	1.2562
30	1.2281	1.2124	1.2090	1.1970	1.1907	1.1782	1.1603	1.1646	1.2087	1.2180	1.2651	1.2467
50	1.2293	1.2164	1.2128	1.2020	1.1938	1.1821	1.1528	1.1844	1.2429	1.2368	1.2752	1.2337
70	1.2044	1.1957	1.1927	1.1837	1.1802	1.1764	1.1515	1.2032	1.2776	1.2807	1.2945	1.2351
85	1.2064	1.1978	1.2044	1.1960	1.1936	1.1796	1.1615	1.2127	1.2903	1.3146	1.3247	1.2758
90	1.2185	1.2089	1.2144	1.2073	1.2007	1.1865	1.1714	1.2145	1.2952	1.3268	1.3391	1.2961
95	1.2254	1.2201	1.2231	1.2157	1.2083	1.1970	1.1807	1.2173	1.3068	1.3360	1.3546	1.3159
	1.2236	1.2124	1.2116	1.2004	1.1957	1.1856	1.1643	1.1945	1.2414	1.2538	1.2883	1.2555

Inlet Plenum Conditions: $P_0 = 1955$ psf $T_0 = 536.8$ °R

$$\frac{W\sqrt{\theta}}{\delta} = 167.2$$

5	1.2576	1.2379	1.2285	1.2178	1.2206	1.2095	1.2020	1.1720	1.2047	1.2423	1.2889	1.2829
10	1.2512	1.2309	1.2179	1.2034	1.2122	1.2041	1.1950	1.1707	1.2039	1.2365	1.2771	1.2718
15	1.2456	1.2223	1.2070	1.1949	1.2021	1.1865	1.1882	1.1705	1.241	1.2336	1.2685	1.2626
30	1.2391	1.2173	1.2044	1.1960	1.1917	1.1827	1.1709	1.1766	1.2230	1.2346	1.2604	1.2513
50	1.2260	1.2127	1.2047	1.2007	1.1994	1.1879	1.1695	1.1979	1.2630	1.2631	1.2595	1.2526
70	1.2366	1.2203	1.2015	1.1952	1.1896	1.1847	1.1666	1.2216	1.2904	1.3024	1.2704	1.2701
85	1.2596	1.2480	1.2163	1.2048	1.1983	1.1867	1.1796	1.2339	1.3105	1.3354	1.2950	1.2981
90	1.2707	1.2614	1.2255	1.2160	1.2060	1.1954	1.1895	1.2371	1.3161	1.3449	1.3052	1.3103
95	1.2656	1.2762	1.2347	1.2251	1.2159	1.2053	1.1994	1.2408	1.3279	1.3510	1.3223	1.3212
	1.2442	1.2272	1.2101	1.219	1.1982	1.1905	1.1779	1.1989	1.2573	1.2761	1.2750	1.2716

Inlet Plenum Conditions: $P_0 = 1964$ psf $T_0 = 539.5$ °R

TABLE 18

Stage Overall Performance for Inlet Circumferential Distortion

<u>% of Design Speed</u>	<u>$W\sqrt{\theta}/\delta$</u>	<u>P_{12}/P_8</u>	<u>η</u>	<u>T_{12}/T_O</u>
70	129.8	1.292	82.4	1.092
	122.1	1.320	82.2	1.101
	111.0	1.341	76.4	1.114
90	164.8	1.522	78.1	1.163
	156.2	1.594	79.3	1.180
100	178.2	1.647	76.3	1.201
	173.1	1.747	77.7	1.223
	167.2	1.781	76.5	1.235