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(NASA-TM-X-62151)AERODYNAMICN72-24010CHARACTERISTICS OF A LARGE SCALE LIFT FANTRANSPORT MODEL WITH PODDED FANS FORWARDUnclassAND LIFT CRUISE FANS MOUNTED J.V. Kirk, etUnclassal (NASA)Apr. 1972132 pCSCL 01B G3/C228201

AERODYNAMIC CHARACTERISTICS OF A LARGE SCALE LIFT FAN

TRANSPORT MODEL WITH PODDED FANS FORWARD AND LIFT

CRUISE FANS MOUNTED ABOVE THE WING

Jerry V. Kirk, Stanley O. Dickinson, Leo P. Hall, and Mary G. Coffman

Ames Research Center Moffett Field, Calif. 94035



April 1972

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NOTATION

A	fan exit area, m^2 (sq ft), or wing aspect ratio
Ъ	wing span, m (ft)
с	wing chord parallel to plane of symmetry, m (ft)
T	mean aerodynamic chord, $\frac{2}{s}$ $\int_{0}^{b/2} c^2 dy$, m (ft)
CD	drag coefficient, $\frac{D}{qS}$
c	rolling-moment coefficient, $\frac{l}{qSb}$
c _L	lift coefficient, $\frac{L}{qS}$
Cm	pitching-moment coefficient, $\frac{M}{qSc}$
c _n	yawing-moment coefficient, $\frac{N}{qSb}$
с _ұ	side-force coefficient, $\frac{Y}{qS}$
D	drag, N (lb)
D _e	effective diameter of the fan, m (ft)
Df	diameter of the fan, m (ft)
i _t	horizontal-tail incidence angle, deg
l	rolling moment, m-N (ft-1b), or length, m (ft)
L	total lift on model, N (lb)
М	pitching moment, m-N (ft-1b)
N	yawing moment, m-N (ft-1b)
Po	standard atmospheric pressure, N/m^2 (1b/ft ²)
P _s	free-stream static pressure, N/m ² (lb/ft ²)

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q	free-stream dynamic pressure, N/m^2 (1b/ft ²)
RPM	corrected fan rotational speed, $\frac{fan speed}{\sqrt{\theta}}$
r	fan radius or cruise fan nacelle length,cm (in)
S	wing area, m ² (ft ²)
Т	complete ducted thrust measured along the fan axis with $\alpha = 0^{\circ}$ and $\beta_v = 0^{\circ}$, $\rho A v_j^2$, N(1b)
V	air velocity, m/sec (ft/sec)
V	free-stream air velocity, m/sec (ft/sec)
v	tail volume coefficient, $\frac{S_{tlt}}{SC}$
Y	side force, N (1b)
x	distance from fan center line or nacelle leading edge, cm (in)
α	angle of attack of the wing chord plane, deg
β	angle of sideslip, deg
β _v	lift-fan exit-louver deflection angle from the fan axis, deg
θ _v	cruise fan exit louver deflection angle from the fan axis, deg
δ	relative static pressure, $\frac{P_s}{P_o}$
٥ _f	trailing-edge flap deflection measured normal to the hinge line, deg
θ	ratio of ambient temperature to standard temperature (519°R)
ε	average downwash at the horizontal tail, deg
η	fraction of wing semispan, $\frac{2y}{b}$
μ	tip-speed ratio, $\frac{2V}{\omega D_f}$
ρ	density, Kg/m ³ (slugs/ft ³)
ω	fan rotational speed, radians/sec

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Subscripts

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- c corrected
- j fan exit

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- i induced
- s static condition
- u uncorrected
- w wing
- t tail

AERODYNAMIC CHARACTERISTICS OF A LARGE SCALE LIFT FAN TRANSPORT MODEL WITH PODDED FANS FORWARD AND LIFT CRUISE FANS MOUNTED ABOVE THE WING

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SUMMARY

The aerodynamic characteristics of a large scale V/STOL transport model powered by tip-turbine driven lift fans were investigated in the Ames Research Center's 40- by 80-foot wind tunnel. The model had four fans; the forward fans were mounted in pods forward of the wing at midsemispan. The aft fans were placed in cruise nacelles behind and above the wing. A cascade of variable camber exit louvers was placed behind each of the lift-cruise fans to turn the fan flow in the lift direction for hover and transition to wing supported flight. The wing of the model was mounted above the fuselage, had an aspect ratio of 5.8, sweepback of 35° at the quarter chord line and a taper ratio of 0.3.

Various configurations of the model were tested to explore the transition speed range. Fan performance, turning effectiveness of the variable camber exit louvers, longitudinal and lateral-directional characteristics with fan operation in crossflow are presented.

INTRODUCTION

As a continuing program, the Ames Research Center is studying lift fan V/STOL transport configurations to assure acceptable aerodynamic characteristics throughout the speed range from hover to wing supported flight.

This study was initiated to explore the use of lift-cruise fans with axes parallel to the aircraft longitudinal axis, above and behind the wing. These fans were provided with vectoring devices to give lift at zero forward speed. The forward lift fans were located in the same position as reported in reference 1. Fan performance, longitudinal and lateral-directional characteristics are shown for various model configurations throughout the transition speed range. Wall pressure distribution and inlet total pressures were measured on the left cruise fan at several tip speed ratios.

MODEL AND APPARATUS

Photographs of the model mounted in the Ames 40- by 80-foot wind tunnel are shown in figure 1. Figure 2(a) is a sketch of the model with pertinent dimensions.

Mode1

<u>Fuselage</u>.- The fuselage was slab sided with rounded corners. Overall length, height, and width in meters (feet) were 13.41(44.0), 1.98(6.5), and 1.77(5.8) respectively. The fuselage used for this investigation was the same as reported in references 1 and 2.

<u>Tail</u>.- Horizontal tail geometry and location are given in figure 2(a). The horizontal tail pivoted about the quarter chord allowing incidence angles from -10 to 20°. During tail off testing, only the horizontal tail was removed.

<u>Wing</u>.- The wing was mounted above the fuselage. Aspect ratio was 5.8, taper ratio 0.3, and sweepback at the quarter-chord line was 35°. An NACA 65-412 airfoil section was basic for the wing. Propulsion

system pods were mounted forward of and beneath the wing at mid-semispan. These pods housed the four gas generators and two front lift fans (figure 2(a)). Leading edge slats were mounted to the wing and extended full span except for the area containing the propulsion pods (n = 0.383 to 0.631). The slat chord was 15 percent of the wing chord and deflection was 20° for the entire investigation.

A 22 percent chord trailing-edge flap extended from 15.9 percent to 37.5 percent semispan (see figure 2(b)). Deflection angles of 0° and 45° were used for this study.

Propulsion System

Four modified YT58 gas generators were located in pods forward of the wing (figure 2(a)) and powered the tip turbine driven X-376 lift fans. The front podded fans were in the same position as described in reference 1. The two lift-cruise fans were installed in nacelles above and near the wing trailing edge. Nacelle exit area was intended to produce a design pressure ratio of 1.1 at zero and low forward speeds. A rack of variable camber exit louvers was mounted behind each cruise fan as shown in figure 2(c). Unless otherwise stated, the rack assembly for the louvers was at a 45° angle to the fan exhaust. The variable camber louvers (ordinates shown in figure 2(c)) were remotely actuated from 7° (thrust direction) to 82° (lift direction). Mechanical interference did not allow deflection beyond these limits.

TESTING AND PROCEDURE

Longitudinal force and moment data were obtained for an angle of attack range from 0° to 22°. Lateral-directional results were obtained for a range of sideslip angles from -18° to $+2^{\circ}$ at 0° and 8° angle of attack. The moment center for data reduction was placed at the quarter chord of the wing MAC.

At zero angle of attack, fan RPM and wind tunnel speed were varied independently. Data were obtained at several exit vane deflection angles, two flap deflections, tail on and tail off.

When angle of attack or angle of sideslip was varied, fan RPM and wind tunnel speed were held constant. When all four fans were operating, thrust-equal-drag conditions were selected at zero angle of attack by varying the front lift fan exit louvers and the lift-cruise fan cascade louver deflection angles at several tip-speed ratios. Angle of attack or angle of sideslip was then varied holding these settings constant. Angle of attack was also varied with exit louver deflection angles ±10° from the trim points to provide thrust greater than drag and thrust less than drag results.

CORRECTIONS

Force and moment data obtained without the fans operating (power off) have been corrected for the effects of wind tunnel wall interference in the following manner:

$$\alpha = \alpha_{u} + 0.488 C_{L_{u}}$$

$$C_{D} = C_{D_{u}} + 0.0085 C_{L_{u}}^{2}$$

$$C_{m} = C_{m_{u}} + 0.0203 C_{L_{u}} \text{ (tail on only)}$$

Appropriate tares have been applied to the results to account for exposed strut tips.

Reference 3 gives a set of model to wind-tunnel sizing ratios that give only small wind tunnel wall effects. The subject model, according to these restraints should produce only small wall effects, therefore no wind tunnel wall corrections have been applied to the results with the fans operating.

RESULTS

An index to the figures is given in table 1. Fan performance, both at hover and forward speed, are shown in figures 3 through 6. Figure 3 presents the hover characteristics for 4-fan operation and lift-cruise fan operation. The static turning effectiveness of the variable camber exit louvers are presented in figure 4. The relationship between tip

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speed ratio and velocity ratio are given in figure 5, while figure 6 presents the variation of fan thrust with forward speed.

Longitudinal aerodynamic characteristics at zero degrees angle of attack with fans operating are presented in figures 7 through 20. Results are shown for a representative tip speed ratio range with the forward fans operating (figure 7), all four fans operating (figures 8 through 18), and the aft lift-cruise fans operating (figures 19 and 20). Model variables included exit louver deflection angles, lift-cruise fan cascade deflection angles, wing trailing edge flap deflection, and horizontal tail off and on.

Variable angle of attack data are given in figures 21 through 30. Power off results (fans not operating) are presented in figure 21; next, results are shown with just the lift-cruise fans operating (figures 22 through 24); and finally, data with all four fans operating are presented in figures 25 through 30.

Figures 31 through 34 present lateral-directional characteristics with fans operating. Results are shown for lift-cruise fan operation (figure 31) and for all fans operating (figures 32 through 34). The exit louver and cascade angle settings were those used as trim drag points in figures 25 through 30.

Appendix A lists, in tabulated form, the inlet pressure distribution from a series of wall statics in the left cruise fan nacelle. Figure 2(c) shows the location of the static taps. Results are given for an angle of attack range from 0° to 22° at three tip speed ratios.

Inlet total pressure distributions are presented in Appendix B for the same conditions as those of Appendix A.

REFERENCES

5

- Dickinson, Stanley O.; Hall, Leo P.; and Hodder, Brent K.: Aerodynamic Characteristics of a Large-Scale V/STOL Transport Model with Tandem Lift Fans Mounted at Mid-Semispan of the Wing. NASA TN D-6234, 1971.
- Hall, Leo P.; Hickey, David H.; and Kirk, Jerry V.: Aerodynamic Characteristics of a Large Scale V/STOL Transport Model with Lift and Lift-Cruise Fans. NASA TN D-4092, 1967.
- Cook, Woodrow L.; and Hickey, David H.: Comparison of Wind Tunnel and Flight Test Aerodynamic Data in the Transition Flight Speed Range for Five V/STOL Aircraft. NASA SP-116, 1966, pp. 447-467.
- 4. Kirk, Jerry V.; Hodder, Brent K.; and Hall, Leo P.: Large Scale Wind Tunnel Investigation of a V/STOL Transport Model with Wing Mounted Lift Fans and Fuselage Mounted Lift-Cruise Engines for Propulsion. NASA TN D-4233, 1967.

INDEX OF FIGURES

1

TABLE 1

REMARKS		STATIC PERFORMANCE		TURNING EFFECTIVENESS	RELATION OF JU TO V/VJ	EFFECT OF FORWARD SPEED ON FAN THRUST	ATTACK									
δf DEG.	ic.s	4 2				•	E D F	0	45	45	0	45	0	45	0	5
ί t , DEG.	RIST	0-		t			ANG	0-	*	055	>	OFF -		0-	*	OFF
θ , , DEG.	NC T E	4	AR.	VAR.	71	7	ERO	-	-	8-	*	-1	*	2-	-	55
β ν , DEG.	HAR	0	06	06	0	0	F		-	VAR.		VAR.		AR.	-	VAR.
Π	EAN C	ł	1	1	MR.	VAR.	PATA	ÅR.		VAR.	-	ÅR.		KAR.	*	VAR.
FANS		ALL	LFT-CR	LIFT-CR	ALL	ALL	DINA	ل ا ا	*	ALL	*	ALL	*	ALL		ALL
B, DEG,		0-					DNG	0-	->	0-	-	0-		0-	-	0
ΩE.G.		0-						0-	-	0-	-	0-	->-	0-	-	0
FIGURE		3(a)	(q) E	4	Ŋ	Q		(d)(a)(T(C)(d)	(0)(0)2	B(c)(q)	(d) (D)6	9(0)	(9)01	10(c)d)	11(a)(b)

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REMARKS																
δ¢ DEG.	0	45	0	\$	0	4 13	0	45 5	0	45	0	8	40	0	45	
it, DAG.	OFF	0-		0FF: -	>	0-	₽	OFF -	~	0-	>	OFF H	0-	~	0	
θv, DEG.	55	52-		30- 20-	>	9- 9-		8-		0 N -	*	7	- ١		AR.	
BV, DEG.	¥R.	ÅR.		VAR.		VAR.	~	₹ AR		VAR.	>	ÅR.	AR.		8	
ת	VAR.	₹ ₹ ₹	-	VAR.	->-	VAR.	-	VAR.	-	₩ L	*	AR.	₹		VAR.	
EANS F	ALL	ALL		ALL	->	ALL		ALL		ALL		ALL	ALL		LFT-CR	
β, DEG.	0	0-		0-	~	0-	->-	0-		0-	~	0	0-		0	
ρEG.	0	0-		0-		0-	->-	0-		0-	~~	0	0-		0	
FIGURE	11 (C)(d)	12(a)(p)	12(c)(d)	(q)(p)	(b)(c)(c)	(a)(a)	14(c)d)	(d)(a)(2)	15(c)(q)	(a)(a)(b)	16(c)d)	(dip)/1	(ସ)(ସ)ଟା	IB(c.td)	(ano) 6!	

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CONTINUED	
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TABLE	

6, 54 REMARKS	E O LIFT-CRUISE FAN EXIT CARRIAGE ANGLE = 65°	ANGLE, OF ATTACK	O,45 POWER OFF	0	F 45	45		45				45		
, , D , D , D	8			8	ð 	5		• 0				- 0		
9 0 Deo	71 55 36	RIA	7	50	50	71,5	S. V	1				- B		
β ν, Deg.	VAR.	TH	06	8	8	8-		-5,5	13,21	0,13,23	ويع, ح	51,05,01	05,02,01	6 5, 5
ת	VAR.	ATA WI	I	34,50.7	20,34,50	.12 , .18	10.25	8	->		61.	.115	61	.245
FANS	ALL	DAL D	1	LIFT-CR	LIFTCR	UFT-CR	>	ALL			->	, ∧ ,		
a, deg.	0	D	0	0	0	0-	>	• 0-				• 0-		
DEG.	0	LONG	¥R	VAR	VAR	AAY -		₹ ₹				₹ R		
FIGURE	20 (aYb) 20(cXd) 20(eXf)		2	22	23	24 (a)	24(b)	25 (a)	25 (b)	25 (C)	(pSZ	26 (a)	<i>26</i> (b)	26(C)

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REMARKS						RISTICS				
54 Deg.	45	45	4 N	4 S		ACTE	0	\$	4S	49
it, DEG.	0	0	0	OFF		CHAR	OFF	OFF	0	0
θv, DEG.	36	20	٢	71,55	36,20		OFF	71,55	71,55	71,55
Bv, DEG.	15,25	10,20	10,28	13,20	25,28	NO1-	8	13,20	13.20	13,20
7	25	62	ĝ	61. 11.	.25.29	DIREC	25,34	.11,.19,24	11, 19, 24	
FANS	ALL	ALL	ALL	ALL		ERAL -	LFT- CK	ALL	ALL	ALL
β, DEG.	0	0	0	0		LAT	VAR.	VAR.	VAR.	VAR.
χ, DeG.	MR	VAR	ÅR	VAR			0	0	0	Ø
FIGURE	27	28	29	30			31	32	33	34

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Appendix A Cruise fan inlet statie pressure coefficients

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STATION	8	0	1	35	22	5	56	50	3.	20	
27X	DIJTER	INNER	DUITER	T NNER	DITER	IMMER	OUTER	INNER	OUTER	INNER	
• 000	-4.668		-4.790		-2.721		-2.494		-4.534		
•005	-0-150	-10.345	-0.028	-12.028	0.661	-8.733	0.694	670°6-	-0.149	-10.358	
•010	0.704	-12.360	0 • 704	-12.678	0.911	-10.236	0.934	-9.711	0.754	-10.488	
užu•	() . R5R	-13.031	6.827	-14.556	0.849	-11.676	0.934	-11-034	0.814	12.307	
• 050	0.643	-12.482	0.582	-13.554	0.160	-12.302	0.453	-11.756	0.754	-12.307	
•100	0.216	-9.857	0.216	-9.985	-0.216	-9.234	0.152	-8.929	0.453	-10.942	
• 200	-0-080	-7.415	-0.466	-7.480	-0.717	-7.185	-0.269	-4.944	-U.158	-7.564	
005.	-0.150	-6.133	-0.717	-6.102	-0.717	-5.862	-0.389	-5.621	-0.288	-6.070	
.400	-0.333	-6.133							-0.353	-6.070	
. 500	-0.333	-0.211							-0.613	-0.2AR	
• 400	-0-333	0.643	-0.279		-0.279		-2.253	-0.329	-0.548	-0.548	
· 700	-0.333	0.582	-0-341	0.849	-0-341	0.754	-0.449	-0.269	-n.4R3	-0.418	
• R00	-0.333	0.460	-0.153	0.473	-0.216	0.273	-1.452	-0°200	-0.483	-0.483	
000	-0.333	0.216	-0.153		-0.279		-0.088	-0.209	-0.223	0.037	
.950	-0-333	0-094	-0.216		-0-091		-0.0AR	512-0	-0-028	0.362	

a = n°, q = 11.85, μ = .199, RPM = 3300

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	coefficients
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Appendix	fan Unlet
	Cruise

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STATION	O	2	- - i	35	Ň	25	Ń	60	m	50	
X/7	NUTER	INNER	NITER	INNER	UUTER	à dhu I	011110	TARTR	001168	IWALFR	
000	012.4-		-5.976		-2.336		-2.184		-2.54		
500.	122.0-	-10.972	-0-393	-13.624	0.783	-9.]36	0.511	7nC - a-	HCU-U-	-9.345	
•010	0.5R0	-12.857	0.397	-13.374	200.0	-0.695	0.641	-9.372	1.5.0	-4.539	
000.	102.0	-] 4.073	U •701	900.41-	0.783	[44][-	104.0	-10.240	0.571	a99.11-	
.	0.580	-12.91R	0.580	-13.811	0.034	-12.252	0.152	-11-764	155.0	-12.127	
001.	0.033	666 • 6-	0•154	-10.049	-0-340	-0.071	BUC . 0-	2113-0-	0 <u>005</u>	-10.3RD	
002.	-0.211	-7.506	-0.527	-7.512	-0.777	-7.395	203-0-	-7.096	ad[.(-	-7.330	
005.	-0.211	-6.230	-0.777	-6.078	-0.714	-6.078	-0.627	-5.7] a	-0.222	-5.851	
• 400	-0-454	-6.230			· · ·	r ; ;			-0.287	-5. A5]	
• 500	-0.454	122.0-							147-0-	-0.158	
vuy•	-0.454	0.519	-u-215		-ñ.?7R		-1.045	-0.567	-0.352	-0.15a	
· 700	-0.454	0.519	-0-465	0.845	204-0-	0.571	-0.4 HT	-0.447	-0-352	-0.15#	
. R00	-0.454	0.337	-0.153	0.533	-0.215	0.451	-1.466	-0.447	-0-352	-0.158	
006.	-0.454	0.093	160.0-		-0.153		-0.388	-0.3RR	-0-093	0.166	
•95n	-0.332	0.033	-0.153		-0.340		-0.388	-0.028	0.166	0.489	

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α = 4°, q = 11.90, μ = .199, RPM = 3300

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Appendix A Cruise fan inlet static pressure coefficients

S Constant

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STATION	Õ	0	Ä	35	У	Ŝ	5	50	35	50	
1/2	DUTER	T NNFR	NUTER	TNNER	DUTER	IMNER	011TFR	INNER	NUTFR	I NMEP	
	-5.649		-5.374		-2.136	<u></u>	-1.436		-3.045		
• 005	-0.512	-11.330	-0.572	-15.341	0.778	-8.150	0.627	-7.352	012.0	-4.196	
010	0.516	-13.204	0.395	-14.473	0.964	-9.761	-0-74h	475.8-	1.627	145.9-	
ucu.	0.697	-14.533	0.758	-16.085	0.716	-11.125	0.686	U6U*U[-	n.627	-10.833	
U 50•	0.514	-13.204	0.637	-14.287	0.034	-12.055	150.0	-11.341	012.0	-10.833	
100	0.032	-10.121	0.153	-10.319	-0.400	620.6-	-0.246	-8.781	0.031	-9.933	
• 2 00	-0.209	-7.522	-0.462	-7.530	-0.648	-7.232	-0.564	-4.994	1-0-221	-7.167	
• 300	-0.270	-6.132	-0.710	-6.042	-0.648	-5.982	-0.683	-5.425	-0.285	-5.752	
•400	-0.512	-6.132							-0.350	-5.752	
. 500	-0-512	-0.270							-0.478	-0.157	,
• • • • •	-0.512	0.516	-0.214		-0.214		-1.338	-0.624	-0.350	-0.02a	
• 700	-0.512	0.516	-0.462	0.840	-0.400	0.508	-0.683	-0.445	-0.285	-0.028	
. 800	-0.512	0.334	-0.276	0.530	-0.214	0.567	-0.862	-U-445	-0.285	-0.028	
006.	-0.512	0.093	-0.152		060-0-		-0.385	-0.385	-0.092	0.165	
, 950	-0.270	-0.028	-0.152		-0.400		-0.385	-0.028	0.100	0.486	

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α = 8°, q = 11.97, μ = .200, RPM = 3300

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Appendix A Gruise fan Ynlet statie pressure coefficients

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STATION	Ø	0	T	35	20	5 C	х	õ	ξ.	00	
×/F	DUTER	INNER	UTFR	INNER	OUTER	INNER	OHTFR	J NNER	NUTFR	INNER	
000	-5.706		-7.354		-2.157		-].472		475.C-		
• 005	-().578	-12.604	-0.944	-16.686	0.849	-7.4] A	10,494	-7.745	0.393	-7.434	• • •
ulu•	0.440	-14.130	n.277	-15.746	0.974	-9.672	0.754	а05 - я-	0.633	-7.490	
020.	0°-704	-15-596	0.745	-17.562	0.786	-11.175	0.433	<10°01-	1.633	-10.033	
• 050	0.521	-13.581	0.704	-15.245	0.034	-12.052	ня <u>0</u> .0-	-11.275	0.092	-10.09R	
• 100	0.033	-10.345	0.216	-וּש•טוּ	-0.279	- 8-9 P3	028.0-	-8.749	-0.02R	-9.7NR	
• 200	-0.272	-7.598	-0.466	-7.668	-0.654	-7.365	-0.569	-7.005	่ 832°∪-	-7.109	
•300	-0.333	-4.255	-0.654	-6.040	-0.579	-4.042	0.630	-5.742	-0.7 AH		
40U	-0.517	-6.255							-0.353	-5.810	
• 500	-0.517	-0.272							-0.483	-0.643	
	-0.517	0.521	-0.153		-0.153	•	-0.930	-0.509	-0.353	0.167	
.700	-0.517	0.521	-0-529	0.911	-0.404	0.513	-0.430	סטר. יו-	-0.343	1.037	
. 800	-0.517	0.338	-0.216	0.661	-0.529	0.694	-0.630	-0.389	-0-353	0.167	
006.	-0.517	0.033	-0.091		-0.279		-0.449	-0.389	-0.093	0.167	
.950	-0.272	-0.028	-0-091		-0.529		-0.389	480.0-	0.147	0.492	

α = 12°, q = 11.85, μ = .199, RPM = 3300

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Appendix A Couise fan'inlet statie pressure coefficients

STATION	ð	0	1.	35	52	5	26	0	35	0	
	NUTER	INNER	NUTER	INNER	OUTER	INNER	OUTER	INNER	OUTER	INNER	
	-4.560		-R.331		-2.032		lóć•l-		066.0-		
-00F	-1.005	150.51-	-1.148	-17.425	0.786	-7.731	0.814	-7.045	0.633	-6.395	
•UU•	0.277	-14 •55R	0.155	-16.686	().974	-9.046	4 [a • 0	0. Y C • H -	1.694	-7.494	
020.	0.582	-16.023	0.704	ן הח. גו–	0.661	-10.842	0.694	134.6-	n.694	-0.642	
· 050	0.460	-13.947	0.5A2	-15.496	-0.041	108.11-	-0.078	-11.094	0.092	274.9-	
001.	0.033	-10.467	0.094	-10.842	-0.466	-9.046	-0.269	-8.428	-0.028	-9.578	
002.	-0.333	-7.720	-0.592	-7.793	-0.717	-7.305	-0-509	-6.884	-0.353	-7.109	
. 30ñ	-0.517	-6.377	-0.7P0	-4.145	-0. 529	-5.982	-0.569	-5.671	-0.353	-745	
400	-0.639	-4.377	 	;	1	•		:	-0.4]4	-5.410	
• 200	-0-439	-0.272							-1,483	£60°0-	
. knñ	-0.639	0.460	-0•153		-0.153	•	-0.544	-6.449	-1,-7 P.H	162.0	
-10U	-0-639	0.399	-Ú-524	0,844	-0, 592	0.633	-0-509	52E U-	R82.0-	0.037	-
. 400	-0.639	0.277	-0.341	n+535	-0.153	0.694	-0-389	-0-329	-0.288	0.232	
. 006 •	-0.639	-0.028	-0.153		-0.341		-0.329	-0.329	-0.028	n.232	
	-0.517	-0.089	-0.153		-0-153		-0.329	-0.028	0.102	0.427	

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· α = 16°, q = 11.85, μ = .198, RPM = 3300

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Appendix A Gruise fan'inlet statie pressure coefficients

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STATION	8	Q	Ч	35	Š	25	Ñ	60	Ē	50	
#/X	DUTER	INNER	NJTER	INNER	OUTER	INNFR	011TFR	INNER	CILLER	INNER	
UUU *	-6.316		-7.720		-1.093		-7.125		-0.269		
500*	-1.180	-12.604	-0.8R3	-17.249	160.0-	-7.480	-4 . 5 Q Q	-10.613	0.474	-5. 29n	
ulu•	0.277	-14.130	n <u>.3</u> 38	-14.748	-1.155	-4.]04	-2.73-	-2.147	2.14	-6.590	
u20*	0.521	-15.962	0.877	125.21-	-0.404	-10.411	1171-1-	-8.147	0.633	- 244	
.050	0.335	-14.069	0°309	-15.484	-0.529	-12.553	-0.569	1112.0-	-0. Î 4x	-4.344	2. 199
• 100	-0.150	-10.773	6a0 .0-	-11-300	-0.529	590°8-	-0.500	-2-24	0.2.0-	-9.513	
. 200	-0.455	-7.659	0.780-	-7.0A1	-11.780	-7.345	-0.430	-6.704	-0.548	-7.10G	
UUE .	-0.578	-6.438	-0°905	062 . 7-	-0.466	-5,922	-0.430	-4.102	-().54P	-5.810	4
400	-0-761	-6.43R		*					-0.548	-5.875	
• 500	-0.761	-0.272							-0.54R	-0.]58	
. 600	-0.761	0.338	-0.153		-0.153	• •	-0.569	-0.630	-0.4]8	0.362	
• 700	-0.761	0.33R	-0.592	0.661	-0.341	0.633	-0.329	002.0-	-0.41R	0.037	
. 800	-0.761	0.155	-0.341	0.473	-0.341	0.934	-0.088	-0.209	-0.483	1.297	
000	-0.761	-n.0R9	-0.279	1	-0.216		-0.209	-0.148	-0.093	0.102	
050.	-0.578	-0.150	-0.216		-0.153		-0.269	-0.02A	-0.158	0.362	

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. α = 20°, q = 11.85, μ = .199, RPM = 3300

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Appendix A Cruise fanvinlet statie pressure coefficients

STATION	ð	0	1:	35	22	Ň	ŭ	50	ŝ	50	
2/X	OUTER	INNER	DUTER	I WNER	UNTER	I NIME &	NITER	INWER	OUTER	I NNER	
uuu.	-4.743		-7.7RI		-3.911		-3.516		-ח. וגא		
• 005	775°()-	-14.313	-0.639	-17.93R	-1.844	-12.866	100.1-	-11.675	1.115	-4.966	
510	0.460	-14.802	0.643	-18.314	-2.220	-15.744	- 4 - 4 - 4 - 4 - 4 - 4 - 4 - 4 - 4 - 4	-10.733	1.434	-5 • 3 1 0	
u2u•	n.704	-15.596	0.888	-18.815	-1.46A	223.11-	-1.051	-9.147	1: - 754	-7.489	
050.	0.460	R()0 * 71-	0.33A	-15.871	-0.466	-11.080	-0. 00h	-10.252	-0.320	-9.343	
v01•	-0.028	-10.451	-0.211	-11-020	-0.967	-8.795	-0.509	-7.345	-1.269	-4.243	
vu2.	-0°394	-7.7Al	-0°905	-7.91H	-0.7RD	-7.1 ⁸⁵	-0 . 449	-4.744	-11.743	086-9-	
002.	-0.455	-6.194	-1.093	-6.353	-0.842	-6.53	045.0-	-6.102	-0.678	-5.745	
400	-0.700	-6.316							-0.413	+74.4-	
• 500	-0.700	-0.150							-0.613	-U.l5g	
. Änn	-0.700	0.460	-0.216		-0.216		-0.329	-0.389	-1,483	795.0	
- 700	-0-700	0.399	-0.592	0.661	-0.404	0.513	602-0-	-0.0AB	-().4 l H	-0.074	
"	-0.700	0.216	-0.592	0.473	-0.404	0 • 994	0.032	-0 . 088	-0.483	0.232	
- 006 •	-0.700	n.n33	-0.341	1	-0.341		-0.148	-0.0PR	-0.158	₩ĊU*U-	
050.	-0.517	-0,080	-0.279		-0-341		-0.148	0.032	-0.093	192.0	

 $a = 22^{\circ}$, q = 11.85, $\mu = .199$, RM = 3300

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Appendix A Cruise fanvinlet static pressure coefficients

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-1.645 900.4--3.539 0.127 -2.473 445.6-A(14.1-I NNFR -2.384 -1.406 -0.273 1.127 -0.206 1.0H3 0.216 350 918 U -3.793 -0.00 0.445 -2.888 -1. (191) -1.645 -0.324 -2.204 -0.344 -0.255 -0.428 NITER 0.815 -0.342 -0.131 -0.295 -0.255 -0.340 -0.234 -0.162 0.260 0.038 -0.3R4 202.0-0.054 -1.140 F00-2-AUNNI 260 102 0 24 0.400 -3.12 AM -4.548 -0.264 -3.901 -0.25h -3.202 -0.216 -3.327 -0.457 -3.006 -0.374 -1.828 -0.800 -1.777 -0.666 1.329 1.144 0.836 -2.291 -0.481 0.314 -0.414 0.198 -0.460 -0.1111 0.630 -0.070 OUTER 1.165 0.774 -1.464 -2.209 INNER 225 -2.345 -0.714 -7.941 0.893 002-0 OUTER 0.143 -0.328 -0.393 0.571 -0.243 -0.221 -3.284 INNER 135 -3.996 0.055 0.953 -3.056 0.640 -2.325 -0.650 -1.824 -0.778 DIJTFR 0.932 -0.446 0.243 -0.307 0.139 -0.264 0.285 -6.221 0.055 -0.243 -0.049 0.034 -0.221 -1.636 -3.390 INNFR -1.845 -0.216 8 -0.404 -0.446 -0.112 0.953 -0.530 -0.00 A 0.535 -0.02A -0.321 -0.404 -0.530 OUTER 0.828. -0.530 0.431 STATION - 700 ¥/¥ 006. 0000. 403 • 500 voo. •002 010-. 300 UUY. . ROO • • • • • 050. 100 .020 1

.. a = 0°, q = 34.64, µ = .340, RPH = 3300 ---

i i Appendix A Cruise fan vinlet statie pressure coefficients

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STATION	Ø	0	ц	35	Ś.	52 S	5	50	m	50	
	OUTER	INNER	ULTER	INNER	OUTER	INNER	DUTER	INNFR	NUTER	INNER	
UUU	624.0		-0.34l		0.676		0.914		UE7.(1		
500°	166.0	-1.Rla	106-0	-3.464	0.880	720°i-	CE4 U	-0.725	1, qT4	-0.842	
010	ч()6 ° Л	-3.524	loō°u	-3.870	0.676	-2.205	. 0.545	-1.627	602°U	-1.888	
U 2 U *	1.4.0	-3.461	0.804	-5.086	0.334	-2.910	0.5.0	114.6-	0.382	-2,905	
050.	£10°0	-4.1.99	n.18N	-4, q5g	-().434	17U°7-	195.0-	-3,595	-1.1.1	-3,604	
001.	-0.257	-3.232	-0.174	-3.486	-0.562	-3.016	-0.436	-2.754	151.0-	-3.239	er Balansida (d. 1900) - Andréan (d. 1900) - Andréa
002.	-0.361	-2.275	112.0-	-2.440	747.0-	-2.263	[7:4]	000°2-	504 °()-	-2.220	
• 300	-0.361	-1.797	-0.775	-1.864	-0.861	-1.730	-0.684	704. [-	-0.427	-1.489	
• 400	-0.528	-1 - 797	 			 ; ;			-0.449	-1.711	
UC 2	-0.52R	-0.132							-0.272	-0.139	
• 400	-0.528	0.325	-ń.178		-0.17R		1.037	540°0 <u>-</u>	-Ú.20k	101.1	
• 700	-0.382	0.284	-0.413	0.313	-9.519	0.259	-0.356	141.0-	-0.206	-0.028	
. 200	-0.27R	0.180	-0.263	0.164	-0.285	1.243	1.078	-0-151	-0.361	1.034	
006.	-0.112	0.117	-n.2R5	1	-0.285		690°0-	-0.151	-0.117	0.171	
- 052.	0.013	0.076	-0-220	;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;	-0.455		0100-	0.095	0.038	n. 259	

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, q = 34.76, µ = .340, MPH = 3300 с. Т В

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Appendix A Cruise fan'inlet static pressure coefficients

STATION	Ø	0	Ъ I	35	S.	25	2(50	3.	50	
X/F	NUTER	INNER	NUTER	INNER	DUTER	INNER	DUTER	INNFR	OUTER	INNER	
000	0.346		-0.820		0.634		1.997		0.936		
• 005	179.0	-1.757	0°6°0	-4.344	0.783	951.1-	1.57.0	-0.444	0.854	-0.738	
•010	0.930	-3.735	206-0	-4.579	0.548	-2.145	9.3A2	-1.341	0.454	-0.760	
020.	0.638	-3.54R	n.867	-5+541	0.142	-2.998	0.054	-2.347	0.177	-2.267	
• 050	0.013	-4.277	0.242	-5.390	-0.477	-3.916	-0.459	-3.455	-0.336	-3.308	
• 100	-0°266	-3.256	-0.112	-3.681	-0.648	-2.934	-0.480	-2.614	-0.254	-3.131	
002.	-0.403	-2.27R	-0.691	-2.464	-0.797	-2.203	-0.582	6ĨU"C-	-0.5]6	-2.200	
• 300	-0.466	-1.757	-0-840	-1.866	-0.755	-1.690	-0.623	-1.547	-0.516	-1.64.1-	
• 400	-0-570	-1.778	, , , , , ,						-0.516	-1.713	
. 500	- U *210	160.0-							-0.294	-0 . 139	
. 400	-0.570	0.284	-0.178	4 1 1 1 1	-0.157		0.874	n. n7 R	-0.206	0.947	
.700	-i) • 445	0.263	-0-306	0.249	-0.392	0.259	-0.234	011-0-	-0-206	-0.117	
. АОО	-0-341	0.180	-0•285	0.142	-0.199	1.141	179.0	u6u•u−	-0.383	N.R80	
UÜ6.	-0.174	0.076	-0.306		-0.434		-0.234	060.0-	-0.141	0.149	
.950	-0-174	n.055	-0-178		-0.199		-0 • 069	ر. 115	0.060	0.238	

a = 8°, q = 34.73, µ = .340, RPM = 3300

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Appendix A Gruise fan'inlet static pressure coefficients

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STATION	8	0	ı	35	5	25	Ñ	50	°	50	
A.A.A.	DUTER	INNER	MITER	INNER	OUTER	INNER	OUTER	INNER	NITER	INNER	
000	10.07		-1.176		0.763		1.020		1.020		
500*	0.973	-2.636	0.848	-5.357	0.806	-1.034	0.409	4[5.0-	0.450	-0. N2R	
010	0.931	-4.117	0.994	-5.400	0.528	-1.890	0.280	-1.077	0.239	-1.005	
·20•	0.481	-4•097	0.890	-6.106	121.0	-2.853	-0,00R	-2.145	540 . 0-	-1-583	
050.	0.013	-4.451	0.305	-5.550	-0.563	-3.902	-0.543	1941.8-	-0.522	751.5-	
001.	-0°320	-3.387	160-0-	-3.731	-0.470	216.5-	-0.563	-2.536	-0.37R	-3.092	
002-	-0.467	-2.344	-0.756	-2.511	-0.863	-2.207	-0.543	-1-960	-0.406	-2.226	
• 300	-0.487	-1.823	-0-863	-1.869	-0.649	-1.673	-0.645	-1-508	-0.606	240.1-	-
•400	-0.454	-1.802		i i					-U- 606	-1.760	
• 500	-0.454	020.0-							-0.250	-0.117	
- v0y•	-0.654	0.285	-0.157		-0.114	•	0.506	-0.028	<u>+0.5.04</u>	0.704	
• 700	-0.467	0.264	-0.521	0.271	-0.435	0.259	128.0-	020-0-	-0.184	-0-05	
. 800	-0.362	0.159	-0.285	0.164	-0.242	0.938	0.470	-0 - 070	-0.341	0.682	
006.	-0.133	0.076	-0.157	-	-0.307		-0.152	020.0-	-0.142	121.0	
.950	-0.049	0.055	-0.114		-0.499		-0-049	0.054	0•040	0.216	

---- a = 12°, q = 34.67, µ = .340, RPH = 3300

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Appendix A Cruise fam inlet static pressure coefficients

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STATION	5	0		35	Ñ	25	Ñ	60	"	50	
a/x	DUTER	INNER	NUTER	INNER	OUTER	INNER	DUTER	INNER	NUTER	INNER	
UUU *	510.0		-1.590		0.762		1.01R		7 9 9 7		
50U°	606*0	-3.132	0.763	-4.117	0.719	-0.RP3	0.464	-0.172	0.341	910°3	er de e e seger
010.	606°U	-4 -548	1.013	-6.074	0.399	-1.473	0.136	180.0-		-0.5×2	
Ú CU*	102.0	-4.402	0.930	-6.480	-0.028	-2.502	-0.131	4Ĩ6•I-	-0•163	-1.645	
, 050	0.076	-4.694	n.284	-5.797	169.0-	-3.639	-1,464	-3.164	-0.623	-2.644	
•100	-0.278	-3.465	-0•133	-3.831	-0-755	709.5-	-0.623	-2.491	-0-418	-2.843	
· 200	-0-466	-2.340	-0.819	-2.549	-0.819	-2.203	-0.623	-1.957	129-0-	-2.112	
• 300	-0.52R	66 L • 1 -	-0.883	-1.866	-0.664	-1.649	-0.464	-].506	-0.671	-1.646	
• 400	-0-674	-1-799	:						-0.649	-1.713	
• 500	-0.674	-0*U49							-0.272	-0.117	
• 600	-0.674	0.747	-0.157		-0.114		n.738	<u>100.0-</u>	-0.206	0.548	
• 700	-0.507	0.247	- 0-541	0.249	-0.306	0.213	-0.377	-0,069	-0.22 A	-0.072	
. 800	-0.403	0.159	-0.306	0.121	-0.498	0.772	0.423	-0,069	-0.383	0.526	
000.	-0•195	0.076	-0.221		-0.370		-0.316	0 <u>+0</u> +0-	-0.139	0.105	
. 950	-0.112	0.055	-0-157		-0.263		-0.234	0.013	0.03H	0.193	

a = 16°, q = 34.73, µ = .340, RPM = 3300

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Cruise fan'inlet statio pressure coefficients

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STATION	8	0	Т	35	<u>ې</u>	25	Ъ,	50	Ę,	50	
= X/F	NUTER	INNER	DUTER	INNER	OUTER	INNER	OUTEP	INNER	NITFR	JNNER	
000*	-0.776		-].647		0.674		-0.560		013.0		
5 Ú Ú Č	0.823	-3.100	n.7R1	-6.181	0.057	-0.710	-0.785	150.1-	0.033	0.413	
u[c.	0.823	-4 • 844	0.989	-5.990	-0-241	15.1-	₩₩ 8	-1.552	-1.652	-0.334	
u cu*	0.594	-4°906	0.802	-6.799	-0.667	-2.647	-().744	-]. 950	-0.662	-1-300	
U 50.	-0.049	-4.844	0.096	-6.160	-1-306	-3.052	-0.7 AL	955.4-	010-1-	-2.670	
uùt.	-0-381	-3.557	-0.361	-4.010	-1-033	-2.796	-() • 519	-2.400	-0-540	-2.78G	
uu 2•	-0.547	-2.436	048-0-	-2.404	-1.263	-2.11.4	-0.642	166°i-	-0-801	-2.127	
• 300	-0.589	-1.917	-1.029	-1.923	-0.667	-1.664	-0.703	-1.644	-1),691	-1.707	- - - - - - - - - - - - -
40U	-0.796	-1.834		1		1	1		-0.647	-1.773	
• 500	-0.776	-0.070							122.9-	-0,095	
• 400	-0.776	0.20 <u>0</u>	-ŭ.156		-0.092	1	0,033	-0.110	-0,22T	N.457	-
- 100	-0.589	0•158	-0.476	0.142	-0.390	0.217	-0.376	040.0-	122.0-	-0.073	
. 800	-0.568	0.075	-0-369	0.078	-0.454	0.687	0.319	0.0 L C	-0.382	0.457	
	-0.298	-0.028	-0.241		-0 . 199		-0.212	64U°U-	<u>cou•u-</u>	36U · U-	
.950	-0.194	-0.049	-0.177		-0.220		-0.212	-0.00R	-0.139	0.104	

a = 20°, q = 34.65, μ = .341, RPK = 3300

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Appendix A Cruise fan 'inlet statio pressure coefficients

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STATION	80	0		35	Ñ	25	8	60	1	50	
a/x	OUTER	INNER	DUTER	I NNER	OUTER	INNFR	DUTER	INNER	OUTER	I NN FR	
	-0.510		-1.619		-0-157		-0.812		1.796		
• 005	0.809	-3.838	n.788	-6.877	-0.114	-1.747	-1.410	0.095	-0.132	AUF .0	
010	0.930	-5.261	0.913	-6.169	-0.522	-2.025	240.0-	-0.544	607.0-	-0.853	
<u>u</u> zu•	n.537	-5.575	0.809	-7.006	-().527	-3.313	-1.142	-1.434	-0.565	-1.320	
•020	160.0-	-5.177	0.034	107.7-	-1.166	-3.635	-0.729	-2.111	121-1-	-2.456	
<u>uu I •</u>	-0.405	-3.670	-0-426	-4.193	-0.780	-2.001	-0.498	195.5-	-0.729	-2.964	
vuc.	-0.614	-2.49R	-1.059	-2.755	-0.RA7	-2.379	-0.523	-2.214	-0.808	112-2-	
100£	-0.656	-1.954	-1.231	-2.025	-0.801	000-2-	-0.545	-1.478	-0.741	-1.699	
.400	-0.845	-1.954							-0.674	-1.7AR	
• 500	-0.824	-0-070			· · ·				-0.385	-0.118	
· 600	-0.845	0.139	-0.222		-0.157	, , ,	-0.070	-0.173	ELC U-	205 N	
· 700	-0.656	0.118	-0-651	0.122	-0.350	0.054	-11.370	111-0-	-0-318	-0.073	
• R00	-0.594	0.013	-0.458	0.057	-0.501	0.570	0.157	-0.111	-0.452	0.395	
006.	-0.363	-0.133	-0.286		-0.372		-0.255	-0.111	-0.140	-0.118	
• 950	-0.2171	-0.154	-0.265		-0.436		-0.296	-0.193	-0.162	0.016	

a = 22°, q = 34.56, µ = .340, RPM = 3300

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Appendix A Gruise fan unlet statie pressure soefficients

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STATION	8	Q	J	35	Ň	25	Ñ	60	e	50	
a/x	CULTER	INNER	UITFR	INNER	OUTER	IMNFR	MITER	INNER	OUT FR	INNER	
000	200°1		0.723		190.0		0.915	- <u>-</u>	0.890		
• 00 5	0.497	0.023	0.8.00	-0.533	0.609	0.158	0.431	0.252	0.686	100.0-	
010.	0.412	-0.986	0.671	-1. NA4	0.317	722.0-	0.150	6LU-Ú-	n. 431	100-0-	
020.	0.153	-0-624	n.334	1.7.1-	0.025	180*0-	620°0-	0 La U-		-0 - 965	
• 150	-0.313	-1.660	-0.1a4	-2.020	-0.560	RCT.1-	0-530	-1.559	-0.258	496.0-	
	-11.494	795.1-	-0-365	-1-436	-0.533	-1.250	-0.539	cu2.1-	-0.207	-1.379	
002.	-0.494	-0.883	612 - 0-	-0 - 905	-() . R7R	-0.896	-0.615	028.0-	-0.469	-0.910	
.300	-0.494	-0.598	-0.799	-0.413	-0.692	-0.590	-0.692	-0.590	-0.469	524.0-	
. 400	-0.520	-0.598							-0.497	-0.579	
• 500	-0.520	-0.235							-0.276	-0.276	
909	-0.520	0.127	-0.188		-0.18R		-0.334	-0.02A	-1.245	425.0	
002.	-0.494	0.127	-0-427	0.104	-0.400	0.074	-11-360	021-0-	-0.276	-0.166	
. 800	-0.494	0.101	-0.400	n.025	-0.400	0.558	620.0-	-0.130	-0.442	0.302	
une.	-0.132	0.075	-0.374		-0.241		501.0-	061.0-	-0.194	0.100	
.950	-0.028	0.075	-0.241		-0.347		-0.079	-0.054	100.0-	0.100	

····· α = 0°, q = 27.93, μ = .504, RPM = 2000

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Appendix A Cruise fan Mulet statle pressure coefficients

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	80		13	5	22	5	26	0	35	0	
A/X	NUTER	INNER	OUTER	INNER	OUTER	INNER	NITFR	INNER	NUTER	I NNER	
.000	J.•()64		n.648		0.925		945 O		л . 996		
•004	0.804	0.102	0.940	-1.149	0.585	0.245	N.22R	0.535	0.5.0	0.055	
บโบ•	0.544	121.1-	0.892	-1.522	cî2.0	-0.268	-0.02	0.151	0.100	6.055	
U 2 U *	0.258	-0.730	0.544	-2.189	-0.162	680°U-	-11.144	-0.592	-0-02x	-0.084	
•050	-1:-236	-1.719	- n. 0n2	-2.349	-0.589	-]. ⁸ 15	-0.41A	-1.396	-0.413	-1.7la	
	265.0-	-1.329	-0-242	-1.602	-0-515	-1.282	-0.618	-1.104	015.0-	-1.246	
UUZ *	-()•1R	-0-835	-n.749	6 40°U-	-0.855	EC8 U-	-0.61A	-0.771	-U.499	וצדיח-	
UUE •	-0.418	-0.574	-0.855	-0-615	-0.695	-0.541	-0.669	-0.515	-0.499	-0.526	
400	-()-496	-0.548	 	1		•	;		-0.499	-0.4.26	
• 500	-0.496	-0.132							-0•194	-0+167	
. 400	-0.49Å	0.154	-0.148		-0.162		-0.336	0.049	-0.167	0.274	
• 700	-0-496	0.154	-0.428	0.078	-0.482	0.125	-0.245	-0.028	<u>-0-305</u>	-0 <u>•094</u>	
, R 00	-0.262	0.154	-0.322	0.025	-0.375	0.535	-0.080	-0°U38	-0.340	0° 304	
UU6	-0.080	0.102	-0.348	1	-0.402		-0.054	-0.028	-0.111	0.165	
. 950	-0.02	0.102	-0.215		-0.142		-0-054	0.023	0.055	0.165	

· α = 4°, q = 27.81, μ = .503, RPM = 2000 ---

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STATION	8	Q	13	5	[%]	25	5	60	3	50	
¥/¥	UITER	TINNER	NUTER	INNER	OUTER	INNER	DUTER	INNER	OUTER	INNER	
000-	1.00A		0•360		0.982		ໂ6ສ ບ		0.865		
50U°	0.853	-0.106	0.9R3	-1.624	0.477	n.344	0.150	0.610	6n()*y	0.451	
u Ĩ u •	0.568	-1.29R	136° U	-1.996	112.0	191.0-	0. 1.0-	N.274	-0.142	0.551	
1120.	n.283	₩£6°υ-	0.646	143.5-	-0.161	250-0-	44C U-	112.0-	-0.3 Nu	-0.304	
050.	-1,28R	6'98 • l -	n.075	-2.661	-0.640	-1.677	-(1.667	-1.254	-1.6 16	-0.332	
100	-0.495	475.1-	-0.236	-1.677	-0-666	401°1-	-11.667	-1-050	11	-1.104	
· 200	-0.495	-0 - RR4	65 2° 0-	-1.012	-().879	-0.820	-0.667	-0.769	-0.÷80	-u-773	
• 300	-n.445	665°u-	-0. ⁵ 06	-0.640	-0.720	-0+539	-0.667	-0.51 ¢	0a 5•u-	-0.497	
400	-0-599	-0.573	 		•				-11-580	-0.525	
. 500	-(599	-0.132							-0.166	111.0-	
	-0-59a	0.153	<u>ا ب ا م.</u>		-0.135		-0.386	<u>n.</u> n7a	-0.139	0.220	
002.	-0.599	0.153	-0.427	0.078	-0.480	0.175	742-0-	-0.013	-0.277	-0.056	
. 800	-0.313	0.101	-0.347	U*051	-0.587	0.457	-0-105	-0-U3	-0-359	0.247	
006.	-0.313	n.ñ75	-0.294		-0.135		-0.105	-0.003	-0.139	0.137	
.950	-0.054	0.049	-0.214		-0.640		-0.054	0.023	0.027	0.137	

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α = 6°, q = 27.90, μ = .503, MPM = 2000 ---

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Gruise fan'inlet static pressure coefficients Appendix A

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STATION	v	2		35	Ń	25	0	60	m	50	
X/F	NUTER	1 WER	NUTER	INNER	DUTER	INNFR	NITER	INNER	NUTER	INNER	
	0.913		n.024		0.937		0.770		617.0		
50U°	0.487	-0.342	C. 992	-2.255	0.320	0.320	-0.080 -0-	0.770	<u>'c 7 t °U-</u>	0.779	
010-	0.652	-1.571	946-0	-2.497	-0-002	-0-142	045.0-	0.441	-0.518	0.751	
ncn.	0.33R	-1.334	0•756	-3.167	-0.270	-().887	-()-44A	602-0-	-0.569	-0.056	
• • •	-0.264	240.5-	n. 155	-2.899	-0.753	-1.665	-0.477	-1.085	-0.77A	-0 <u>.084</u>	
	-0.473	-1.493	-0.159	-1.826	-0.726	-1 • 1 ×2	-0.750	020.0-	-0.515	-1.002	
002*	-0.499	-0.918	-0.RN6	-1.021	-0.780	-0°776	-1)•750	-0.498	-0.668	-0.724	
UUE •	-0.551	-0.578	-0.8P7	647°U-	6 [9 • 0-	-0.51R	-0.724	-0.465	-0.668	-0-501	
•400	-0.656	-0.578	••••••						1 22.0-	-0.50]	
• 200	-0.456	-0°081							-0.140	-0.084	
004.	-0.656	0.155	-0.136		<u>2a0-0-</u>	1	-0.441	500°U-	-0.117	0.155	
• 700	-0.454	0.155	-0.4 P4	0.106	-0.270	0.100	-0.32R	-0.003	-0.251	100-0-	:
. 200	-0.342	n.129	-0.377	0.025	-0.458	0.384	-0.131	FU7.9-	-0.342	0.194	
000.	-0.159	0.076	-0.297		-0.136		-0.260	£00°0-	-0.140	0.111	
050	<u>-0.081</u>	0.074	-0.162		-0.323	- 1	-0.080	10°03	0.055	0.139	

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a = 12°, q = 27.65, µ = .502, RPM = 2000 ...

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Appendix A Gruise fan inlet statie pressure coefficients

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STATION	8	~	13	5	22	5	26	0	35	0	
4/X	DUTER	INNER	NUTER	INNER	OUTER	INNEK	HILEN.	INNER	APT THIN	INNER	
000-	0.830		-0.237		0.933		0.632		2 4 2		
500.	11.430	-ט-גחן	0.986	-2.751	G.15R	0.479	672.0-	α[1.]	-1).874	58.3.0	
010.	n.674	-1.74K	0.9R6	-2.804	-0.135	420.0-	-0.541	1.54.1	-1-025	0.830	
u2u•	885.0	-1.494	n.778	-3 . 578	-0.482	224.0-	-11-644	501.0-	005-0-	011.0	
. 190	adl.n-	-2.1RP	0.154	-3.098	549.0-	712.1-	1-6-0-	200-[-	-11.077	640 °U	•
u u t •	-0.445	-1.564	-0.210	-1.843	CUR.0-	-1.149	-0.823	4C0.0-	-0.618	010.0-	
· 200	-u-523	£16°0-	-0.879	640 - 1-	450°U-	707.0-	10 - X 10	-0. 95	122.0-	-0.748	
UUE.	-0.575	-0-627	606°0-	-0.616	-0.616	-0.515	-0.772	-0.439	-0.721	-0.527	-
• 400	-0.479	109.0-						,	-1) • 6 03	-0-527	
• 500	-0.679	-0-054							-0.139	-0.111	
• 400	-0.679	0.1 <u>7</u> R	-0.135	1	-0.055		-0.567	820.0-	-0.111	0.082	
-100	-0.679	0.128	-0.535	0.078	-0.349	0.074	-0.336	-0.07A	-0.278	-0° 001	
. 800	-0.445	0.102	-u-245	-0.002	-0.295	0.254	-0.259	-0.028	-0.333	0.082	
une.	012.0-	0.102	-0.215		-0.295		-0.310	-0.07R	-0.139	0.055	
.950	-0.106	0.076	-0.135		-0.375		-0.105	82U°U-	-0°001	0.0R2	

 $\alpha = 16^{\circ}$, q = 27.80, $\mu = .502$, RPM = 2000 ---

Appendix A Gruise fan inlet statie pressure coefficients

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STATION		0	13	5	22	5	26	0	35	Q	
avx	NUTER	INNER	ULTER	I NNER	DUTER	INNER	OUTER	[NNFR	OUTER	I NNER	
	0.674		-u-347		30,692		556.0-		0.023		
·uu•	11 . 856	166*0-	1 46 ° U	-3.205	-()• 420	204.0	-1.233	098.C	018.1-	966°U	
010	0°200	-2.266	1.46.0	-3.072	-0. 375	CE1 . 0	-7.31-	0.744	-1.413	A60.6	
u20*	0.466	-2.110	0.776	-3.872	00 6 • ()-	512.0-	-1.592	638.0	-1.20a	0.3H7	
USU	-n . 1 84	-2.527	0-0-20	-3.312	-1.390	1.1.190	-1.336	×14.0-	-1.205	0.749	
001.	124.0-	-1.642	-0.393	-2.084	-1-096	-1.150	-1.079	507°U-	-0.746	-10-015	
• 200	-0+575	-0-945	-n.943	-1.150	-1.016	747.	10.721	-1.502)• 459	-6.445	
.U.E.	-0.453	-0.401	-1.043	-n. k96	-0. PR3	-0.515	-0.515	F (7. U-	122.0-	-0.499	
. 400	182.0-	-0.549							664.0-	-0.592	
• 500	-0.731	-0,054			<u></u>				-0.111	-0.056	
VUY	-0.731	0.076	-0.108		-0.082		-0.618	-0.054	111.0-	100.0-	
- 700	-0.731	0.076	-0.349	0.052	-0.375	0.100	-0.182	-0,054	-0.333	-0.01	
. RUN	-0.497	0.050	-0.295	-0.082	-0-269	0.177	-0.233	-0.054	-0.416	150.0	
- 500°	-0.315	0.024	-0.349		-0.242		-0.285	-0.054	-0.139	0.027	
.950	-0.211	0.024	-0.189		-0.189		-0.157	-0.028	100-0-	0.082	

----- a = 20°, q = 27.79, µ = .503, RPM = 2000

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Appendix A Appendix A Cruise fan Ynlet statle pressure coefficients

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STATION		Q	н	35	Ň	52	N I	60	(~)	50	
3/X	NUTER	TNNER	UITER	INNER	UNTER	INNER	NUTER	INNES	24 1111	άu₩×1 	
000*	0.520		062.0-		0.374		-1) . R 77		174		
500.	5.8KC	-1.452	Ú56°U	127.5-	-0.445	-0.243	-2.318	-0.444	168.1-	1.10.0	
010	0.755	-2.640	1,964	-3+833	-1.046	-11.744	- X - X -	1.441	-1.454	112.0	
0.00	13.442	-7.1]A	1.677	-4.241	-0-030	-11.645	-1.126	460.0	ウォベ・1-	0.85° C	
USO.	-0.237	-7.64	-n.ñ28	-3.726	-1.502	-1.261		-0.472	-1 • 4 0 H	000.0	
.100	-1.445	-1.831	-0.472	-2.145	7[6.]-	-1.154	-0-723	-0.74.0	-1.426	-0.073	
002.	153.0-	120.1-	-1.154	-1.150	-0.986	-1-022	-0-549	1.04.11-	-4,9 JA	-0.72a	
()()2.	-0.681	-0.681	-1.207	-0.752	-0.725	-0.723	-9.723	-0.569	-0 - 6°3	-0.556	
	-().838	-0.655	,	:		1 1 1 1 1			-0.668	-0.584	
UU 5•	-n.Al2	-0.054							46【•0-	-0.112	
100¥*	-n.al2	n <u>,</u> 05'n	-0.136		-0.j.0-	•	-(1.445	040.01	-0.167	<u>- u w</u> . u	
• 100	-0.655	<u>0</u> 50- <u>0</u>	-0.537	-0.002	-0.296	EUU • 6-	-0.4]4	-0.054	068°U-	+ CU*U-	
ບບະ •	-0.577	n•024	-0.511	-0.055	-0.511	0.126	-0.337	-0°(154	-0.445	100.0-	
000	-0.342	-0.02R	-0.377	•	-0.246		306.0-	-0 ⁺ 054	-1.167	-411.12	
. 950	-0.237	-0.054	-0.189		-0 -537		-0.1 k3	-0.040	-0-306	-0.02R	

a = 22°, q = 27.69, µ = .562, RPH = 2000

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(a) Front view.

Figure 1.- Photographs of the model in the Ames 40- by 80-Foot Wind Tunnel.



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(b) Rear view.
Figure 1.- Concluded.



(a) Model geometry.

Figure 2.- Geometric details of the model.

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Existing inlet Typical inlet-to-wing fairing

(b) Details of the leading edge slat, trailing edge flap, and forward fan inlet-to-wing fairing.

Figure 2.- Continued.



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CRUISE FAN AND EXIT CASCADE DETAILS

VARIABLE CAMBER LOUVER ORDINATES & DETAILS

(c) Aft cruise fan and exit louver geometry.

Figure 2.- Continued.



(d) Cruise nacelle pressure instrumentation.

Figure 2.- Concluded.



(a) Four fans, $\beta_v = 0^\circ$, $\theta_v = 71^\circ$.







(a) Geometric angle between the fan thrust axis and the cascade carriage = 45° .

Figure 4.-Zero forward speed turning effectiveness of the variable camber exit louver cascade behind the lift-cruise fans.





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Figure 5.- The relationship between tip-speed ratio and velocity ratio; $\alpha = 0^{\circ}$, $\beta_v = 0^{\circ}$.

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Figure 6.- The variation in fan thrust with tip-speed ratio; $\alpha = 0^{\circ}$.

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(a)  $C_L vs \mu$ ,  $\delta_f = 0^\circ$ .

Figure 7.- The effect of tip-speed ratio on longitudinal characteristics; lift fans only, tail on,  $i_t = 0^\circ$ .



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(b)  $C_D$ ,  $C_m$  vs  $\mu$ ,  $\delta_f = 0^{\circ}$ .

Figure 7.- Continued.



(c)  $C_{\rm L}$  vs  $\mu$ ,  $\delta_{\rm f}$  = 45°. Figure 7.- Continued.



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Figure 7.- Concluded.



(a)  $C_L vs \mu$ ,  $\delta_f = 45^{\circ}$ .

Figure 8.- The effect of tip-speed ratio on longitudinal characteristics; 4 fans,  $\theta_v = 82^\circ$ , tail off.



(b)  $C_D$ ,  $C_m$  vs  $\mu$ ,  $\delta_f = 45^\circ$ .

Figure 8.- Continued.



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Figure 8.- Concluded.



(a)  $C_L vs \mu$ ,  $\delta_f = 45^\circ$ .

Figure 9.- The effect of tip-speed ratio on longitudinal characteristics; 4 fans,  $\theta_v = 71^\circ$ , tail off.



(b)  $C_D$ ,  $C_m$  vs  $\mu$ ,  $\delta_f = 45^\circ$ .

Figure 9.- Continued.



(c)  $C_{\rm L}$  vs  $\mu$ ,  $\delta_{\rm f} = 0^{\circ}$ .





(d)  $C_D$ ,  $C_m$  vs  $\mu$ ,  $\delta_f = 0^\circ$ .

Figure 9.- Concluded.



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(a)  $C_{L} vs \mu, \delta_{f} = 45^{\circ}$ .

Figure 10.- The effect of tip-speed ratio on longitudinal characteristics; 4 fans,  $\theta_V = 71^\circ$ , tail on, it = 0°.



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(b)  $C_D$ ,  $C_m$  vs  $\mu$ ,  $\delta_f = 45^\circ$ .

Figure 10.- Continued.



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(c)  $C_L vs \mu$ ,  $\delta_f = 0^\circ$ .





(d)  $C_{n}$ ,  $C_{m}$  vs  $\mu$ ,  $\delta_{f} = 0^{\circ}$ .





(a)  $C_L vs \mu$ ,  $\delta_f = 45^{\circ}$ .

Figure 11.- The effect of tip-speed ratio on longitudinal characteristics; 4 fans,  $\theta_V = 55^\circ$ , tail off.



(b)  $C_{D}$ ,  $C_{m}$  vs  $\mu$ ,  $\delta_{f} = 45^{\circ}$ .

Figure 11.- Continued.


(d)  $C_{D}$ ,  $C_{m}$  vs  $\mu$ ,  $\delta_{f} = 0^{\circ}$ .

Figure 11.- Concluded.



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(a)  $C_L vs \mu$ ,  $\delta_f = 45^\circ$ .

Figure 12.- The effect of tip-speed ratio on longitudinal characteristics; 4 fans,  $\theta_v = 55^\circ$ , tail on,  $i_t = 0^\circ$ .





(c)  $C_L vs \mu$ ,  $\delta_f = 0^\circ$ .





Figure 12.- Concluded.



(a)  $C_L vs \mu$ ,  $\delta_f = 45^\circ$ .

Figure 13.- The effect of tip-speed ratio on longitudinal characteristics; 4 fans,  $\theta_V = 36^\circ$ , tail off.



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(b)  $C_D$ ,  $C_m$  vs  $\mu$ ,  $\delta_f = 45^\circ$ .

Figure 13.- Continued.



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Figure 13.- Concluded.



Figure 14.- The effect of tip-speed ratio on longitudinal characteristics; 4 fans,  $\theta_V = 36^\circ$ , tail on, it = 0°.



(b)  $C_{D}$ ,  $C_{m}$  vs  $\mu$ ,  $\delta_{f} = 45^{\circ}$ .

Figure 14.- Continued.



(c)  $C_L vs \mu$ ,  $\delta_f = 0^\circ$ .

Figure 14.- Continued.



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(d)  $C_D$ ,  $C_m$  vs  $\mu$ ,  $\delta_f = 0^\circ$ .

Figure 14.- Concluded.



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(a)  $C_L$  vs  $\mu$ ,  $\delta_f = 45^\circ$ .

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Figure 15.- The effect of tip-speed ratio on longitudinal characteristics; 4 fans,  $\theta_v = 20^\circ$ , tail off.



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Figure 15.- Continued.



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(c)  $C_L vs \mu$ ,  $\delta_f = 0^\circ$ .

Figure 15.- Continued.



(d)  $C_D$ ,  $C_m$  vs  $\mu$ ,  $\delta_f = 0^\circ$ .

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Figure 15.- Concluded.



(a)  $C_L vs \mu$ ,  $\delta_f = 45^\circ$ .

Figure 16.- The effect of tip-speed ratio on longitudinal characteristics; 4 fans,  $\theta_v = 20^\circ$ , tail on,  $i_t = 0^\circ$ .



(b)  $C_{\rm D}$ ,  $C_{\rm m}$  vs  $\mu$ ,  $\delta_{\rm f} = 45^{\circ}$ .

Figure 16.- Continued.

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(c)  $C_L vs \mu$ ,  $\delta_f = 0^\circ$ .





(d)  $C_D$ ,  $C_m$  vs  $\mu$ ,  $\delta_f = 0^\circ$ 

Figure 16.- Concluded.



(a)  $C_{L}$  vs  $\mu$ ,  $\delta_{f} = 45^{\circ}$ .

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Figure 17.- The effect of tip-speed ratio on longitudinal characteristics; 4 fans,  $\theta_v = 7^\circ$ , tail off.



(b)  $C_D$ ,  $C_m$  vs  $\mu$ ,  $\delta_f = 45^\circ$ .

Figure 17.- Concluded.



(a)  $C_{L}$  vs  $\mu$ ,  $\delta_{f} = 45^{\circ}$ .

Figure 18.- The effect of tip-speed ratio on longitudinal characteristics; 4 fans,  $\theta_v = 7^\circ$ , tail on,  $i_t = 0^\circ$ .

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(b)  $C_D$ ,  $C_m$  vs  $\mu$ ,  $\delta_f = 45^\circ$ .

Figure 18.- Continued.



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(d)  $C_D$ ,  $C_m$  vs  $\mu$ ,  $\delta_f = 0^\circ$ .

Figure 18.- Concluded.



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(a)  $C_L vs \mu$ 

Figure 19.- The effect of tip-speed ratio on longitudinal characteristics; lift-cruise fans only, tail on,  $i_t = 0^\circ$ ,  $\beta_v = 90^\circ$ ,  $\delta_f = 45^\circ$ .



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(b)  $C_D$ ,  $C_m$  vs  $\mu$ 





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(a)  $C_L vs \mu$ ,  $\theta_v = 71^\circ$ .

Figure 20.- The effect of tip-speed ratio on longitudinal characteristics; 4 fans, tail off,  $\delta_f = 0^\circ$ , lift-cruise fan exit carriage angle = 65°.



Figure 20.- Continued.



(c)  $C_L vs \mu$ ,  $\theta_v = 55^\circ$ . Figure 20.- Continued.



Figure 20.- Continued.



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(f)  $C_D$ ,  $C_m$  vs  $\mu$ ,  $\theta_v = 36^\circ$ .

Figure 20.- Concluded.



Longitudinal characteristics with power off;  $\beta_v = 90^\circ$ . lift-cruise fans windmilling,  $\theta_v = 7^\circ$ , tail on,  $i_t = 0^\circ$ . Figure 21.-


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(a)  $\theta_{\rm V} = 71^{\circ}$ , 55°.

Figure 24.- Longitudinal characteristics with lift-cruise fan operation; lift fans covered,  $\beta_V = 90^\circ$ , tail on,  $i_t = 0^\circ$ ,  $\delta_f = 45^\circ$ .

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Figure 24.- Concluded.





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Figure 25.- Continued.



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Figure 25.- Continued.

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Figure 25.- Concluded.



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Figure 26.- Longitudinal characteristics with lift and lift-cruise fan operatiou; tail on, it = 0°,  $\delta_f$  = 45°.

(a)  $\mu = .115$ 



Figure 26.- Continued.



Figure 26.- Concluded.



Figure 27.- Longitudinal characteristics with lift and lift-cruise fan operation; tail on,  $i_t = 0^\circ$ ,  $\delta_f = 45^\circ$ .



Figure 28.- Longitudinal characteristics with lift and lift-cruise fan operation; tail on,  $i_t = 0^\circ$ ,  $\delta_f = 45^\circ$ .

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Figure 32.- The effect of tip-speed ratio on lateral-directional characteristics with lift and lift-cruise fan operation, tail off,  $\delta_f = 45^\circ$ ,  $\alpha = 0^\circ$ .



Figure 33.- The effect of tip-speed ratio on lateral-directional characteristics with lift and lift-cruise fan operation; tail on, it = 0°,  $\delta_f = 45^\circ$ ,  $\alpha = 0^\circ$ .



Figure 34.- The effect of tip-speed ratio on lateral-directional characteristics with lift and lift-cruise fan operation; tail on,  $i_t = 0^\circ$ ,  $\delta_f = 45^\circ$ ,  $\alpha = 8^\circ$ .