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AN ALGORITHM FOR CONTROL SYSTEM DESIGN VIA PARAMETER
OPTIMIZATION

by Prasun K. Sinha

January 1972

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VIA PARAMETER OPTIMIZATION

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PRASUN K. SINHA

B. Tech Indian Institute of Technology, Kharagpur 1969

SUBMITTED IN PARTIAL FULFILLMENT

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ABSTRACT

An algorithm for design via parameter optimization has been developed for linear-time-invariant control systems based on the model-reference adaptive control concept. A cost functional is defined to evaluate the system response relative to nominal, which involves in general the error between the system and nominal response, its derivatives and the control signals. A program for the practical implementation of this algorithm has been developed, with the computational scheme for the evaluation of the performance index based on Lyapunov's theorem for stability of Linear-Invariant-Systems.

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LIST OF PRINCIPAL NOMENCLATURE

General: Upper case letters represent matrices, lower case letters with underbars represent vectors.

SYMBOL	DEFINITION
A,B	known matrices in matrix-algebraic equation (Chapter 3)
$\underline{b}$	bus variable vector (Chapter 2)
C	known RHS matrix of matrix algebraic equation (Chapter 3)
$\underline{c}$	command variable vector
$\underline{e}$	error vector
E	three dimensional array in equations for control system representation (Chapter 2)
F_s	system differential transition matrix
F_m	model differential transition matrix
F	augmented system differential transition matrix
G	augmented system control matrix
H	three dimensional array in equations for control system representation (Chapter 2)
I	identity matrix
J	performance index
K_i	the i^{th} parameter
L_i	companion matrix (Chapter 3)
M, $\tilde{M}$, N, $\tilde{N}$, P, Q'	system matrices in describing equations (Chapter 2)

SYMBOL	DEFINITION
Q_s	system control matrix
Q_m	model control matrix
R, S, T	matrices in system describing equations (Chapter 2)
S_s	system output matrix
S_m	model output matrix
t	time
U, V	matrices in form of assumed solution for X (Chapter 3)
W_e, W_e^*, W_u	error and control signal weighting matrices
$\underline{w}$	vector of magnitudes of delta function commands
X	unknown matrix in matrix algebraic equation (Chapter 3)
$\underline{x}_s$	system state vector
$\underline{x}_m$	model state vector
$\underline{x}$	augmented system state vector
$\underline{y}_s$	system output vector
$\underline{y}_m$	model output vector

SPECIAL NOTATIONS

F^T $\equiv$ Transpose of F

$$||\underline{x}|| \equiv \sqrt{\underline{x}^T \underline{x}}$$

$$||\underline{x}||_Q^2 \equiv \underline{x}^T Q \underline{x}$$

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CHAPTER 1

Introduction

The algorithm for "design via parameter optimization" to be described in subsequent chapters is based on the model reference adaptive control concept [7]. The concept is briefly reviewed here and the problem to be examined in this study is formulated.

1.1 The Model Reference Adaptive Control Concept

These systems employ a model which represents the nominal transfer function between input and output. The model is placed in parallel configuration with the system. This arrangement is shown schematically in Fig. 1.1.

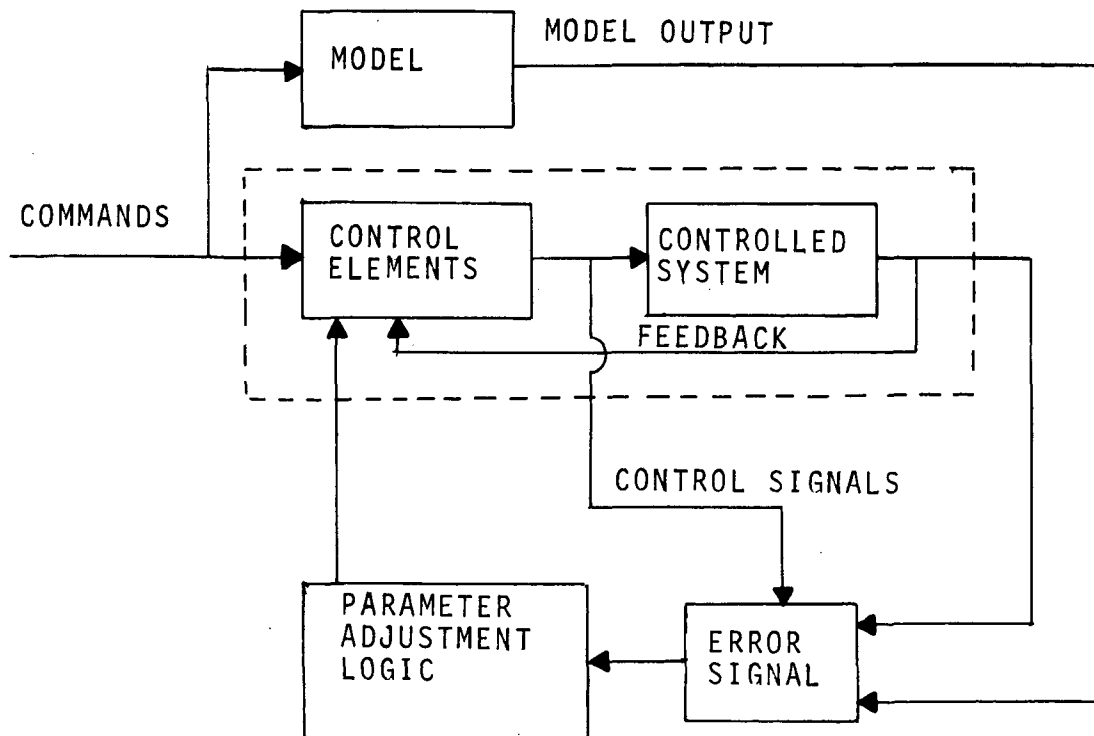


Fig. 1.1 Functional Diagram Illustrating the Model Reference Adaptive Control Concept

The same command signals are applied to both the model and system. If the system output differs from that of the model, then the control elements must be modified. The objective is to make the system response track closely that of the model by adjustment of the controller parameters (gains and time constants).

1.2 Problem Formulation and Objective

The actuating signals for controller parameter adjustment are quadratic functions of the error between the nominal and plant response and perhaps some of its derivatives. For single outputs, if y_s is the system response and y_m that of the model, then the basis for the parameter optimization design of the controller, is the minimization of the performance index

$$J = \int_0^{\infty} (e^2 + \beta \dot{e}^2) dt \quad (1.1)$$

where e is the error between model and system responses and β is a positive constant. If more than one output is involved, let $\underline{y}_s$ be the system output vector and $\underline{y}_m$ that of the model. The error is then defined by

$$\underline{e} = \underline{y}_s - \underline{y}_m \quad (1.2)$$

and the performance index could be formulated as

$$J = \int_0^{\infty} [\underline{e}^T W_e \underline{e} + \beta \dot{\underline{e}}^T W_{\dot{e}} \dot{\underline{e}}] dt \quad (1.3)$$

where W_e and $W_{\dot{e}}$ are error weighting matrices.

In some cases it may be required that restrictions be placed on the magnitude of the control signals, limiting the amount of elevator deflection for instance in affecting aircraft longitudinal control. If $\underline{u}$ represents these control signals, then the performance index to be minimized could be formulated as

$$J = \int_0^{\infty} [\underline{e}^T W_e \underline{e} + \beta \dot{\underline{e}}^T W_{\dot{e}} \dot{\underline{e}} + \underline{u}^T W_u \underline{u}] dt \quad (1.4)$$

In the following chapters an algorithm is developed which adjusts the free parameters (gains and characteristic frequencies) of fixed-configuration, linear-invariant systems to optimum values so as to make the system response track as closely as possible a specified nominal response as measured by the minimum value of a performance index given in Eqns. (1.1), (1.3), or (1.4). Further a program for the practical implementation of this algorithm which involves minimal preprocessing of the model and system configuration and other requisite data is described.

CHAPTER 2

Control System Representation and Optimization Algorithm

In this chapter the form of the equations to represent the system configuration is presented along with the motivation for such a representation. The equations for the parameter optimization algorithm are next derived and the various quantities involved therein are defined. Finally the sequence of the algorithm logic is documented.

2.1 Control System Representation:

The equations of the parameter optimization algorithm are derived for a system configuration input in the form

$$M\dot{\underline{x}}_s = N\underline{x}_s + P\underline{b} + Q'\underline{c} \quad (2.1)$$

$$\underline{b} = R\underline{x}_s + S\underline{b} + T\underline{c} + \sum_{i=1}^n (E_i \underline{x}_s + H_i \underline{b}) K_i \quad (2.2)$$

$$\underline{y}_s = S_s \underline{x}_s \quad (2.3)$$

$\underline{x}_s$ is the system state vector, $\underline{b}$ the vector of bus variables, $\underline{c}$ the commands and $\underline{y}_s$ the system output vector. M , N , P , Q' , R , S and T are system matrices. S_s is the output matrix, while E and H are three dimensional arrays relating the bus variables to the state and bus variables respectively through controller adjustable parameters K_i for $i = 1, 2, \dots, n$.

The elements of the matrices in (2.1), and (2.2), for the system representation are usually considerably easier to obtain from an actual system than a single state equation and involve less manipulation of the system configuration, particularly if the plant dynamics are specified. An example is the format for the equations of flight vehicle longitudinal dynamics [2]. As will be indicated, the representation (2.1), and (2.2) allows the system configuration to be input in a straight forward manner.

Consider the basic longitudinal flight control system of Fig. 2.1. In this instance, [2], the missile dynamics would be

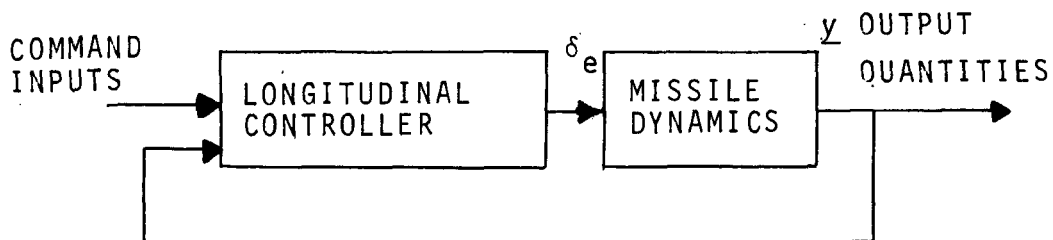


Fig. 2.1 Simplified Functional Diagram of Longitudinal Flight Control System

described by equations of the form

$$M\dot{\underline{x}} = N\underline{x} + Q\delta_e \quad (2.4 a)$$

where δ_e is the control surface (elevator) deflection. M is not an identity matrix but is a simple function of the missile aerodynamic stability derivatives. If the form

$\dot{\underline{x}} = F\underline{x} + G\underline{\delta}$ were used a large ammount of preprocessing of input data would be required.

Consider the following set of equations for the longitudinal dynamics of a jet transport in straight and level flight [2].

$$13.78'\dot{u} + 0.88'u - 0.392'\alpha + 0.74\theta = 0$$

$$1.48'u + 13.78'\dot{\alpha} + 4.46'\alpha - 13.78\dot{\theta} = -0.246\delta_e$$

$$0.552'\dot{\alpha} + 0.619'\alpha + 0.514\ddot{\theta} + 0.192\dot{\theta} = -0.710\delta_e$$

$$\dot{h} = \theta - '\alpha$$

(2.4b)

The definition of the various variables is given below. Noting the form of equation (2.4a), and the appearance of $\ddot{\theta}$ in the third equation of (2.4b), above; this requires that a new variable q be defined as $\dot{\theta} = q$. Other higher derivatives may be similarly replaced. The equations (2.4b), can now be written as

$$13.78'\dot{u} + 0.88'u - 0.392'\alpha + 0.74\theta = 0$$

$$1.48'u + 13.78'\dot{\alpha} + 4.46'\alpha - 13.78\theta = -0.246\delta_e$$

$$0.0552'\dot{\alpha} + 0.619'\alpha + 0.514\dot{q} + 0.192q = -0.710\delta_e$$

$$\dot{\theta} = q$$

$$\dot{h} = \theta - '\alpha$$

(2.4c)

The state variables for the vehicle dynamics are

'u - non dimensional perturbation in forward speed

' α - angle of attack perturbation (rads)

θ - pitch angle perturbation (rads)

q - pitch rate (rads/sec)

h - non dimensional altitude perturbation

The elevator deflection is denoted by δ_e .

If the longitudinal controller is of the form shown in Fig. 2.2a with time constant τ and α as free design parameters, two additional state variables δ_e and x_7 indicated in Fig. 2.2b, are introduced.

The actuator and lead-lag are described by the equations

$$\left. \begin{aligned} b_1 &= c_1 - K_3 \theta \\ b_2 &= -b_1 + K_1 b_1 \\ b_3 &= K_2 b_2 - K_2 x_7 \\ b_4 &= K_1 b_1 - x_7 \end{aligned} \right\} \quad (2.5a)$$

$$\left. \begin{aligned} \dot{x}_7 &= b_3 \\ \dot{x}_6 &= -\frac{x_6}{\tau_a} + \frac{b_4}{\tau_a} \end{aligned} \right\} \quad (2.5b)$$

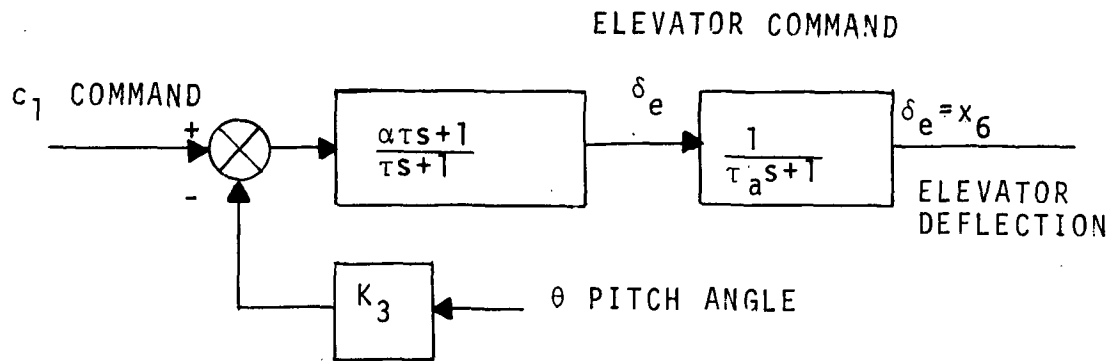
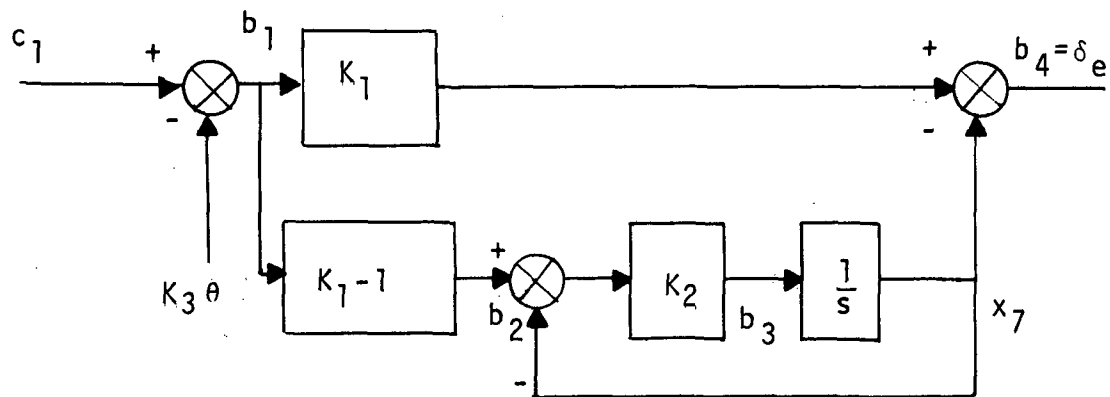


Fig. 2.2a Block Diagram of Simplified Controller



$$K_1 = \alpha; \alpha > 1 \quad K_2 = 1/\tau$$

Fig. 2.2b Block Diagram of Lead-lag Illustrating Use of Bus Variables

The equations (2.5a) are of the form (2.2), while (2.5b), together with (2.4b and c), are of the form (2.1). Therefore given the plant dynamics the form of the equations (2.1), and (2.2), makes it possible to augment the state vector to include state variables added by the controller without any redefinition of the plant variables.

From equation (2.2), it is seen that the bus variables are linear functions of the gains. This requires that E and H be at most three dimensional arrays. If a single state equation is used to describe the total system, the state variables would in general be products of the gains. This, besides involving the additional preprocessing implied in reducing (2.1), and (2.2), to a single equation would also require the definition of four and possibly five dimensional arrays to input the combinations of gains involved. This would provide considerable scope for erroneous inputting of data. Also in the representation of (2.1) and (2.2) most of the elements of each matrix would be zero. The namelist option described in Appendix A provides a convenient scheme for inputting only the non zero elements.

For the example under consideration with

$$\underline{x}_s^T = ['u' \alpha \theta q h x_6 x_7]$$

$$\underline{b}^T = [b_1 b_2 b_3 b_4]$$

The non zero elements can be written down by inspection.
For equation 2.1, these are;

1. M matrix This is a 7×7 matrix

$$M_{11} = 13.78, M_{22} = 13.78, M_{23} = -13.78, M_{32} = 0.0552$$

$$M_{33} = 0.192, M_{34} = 0.514, M_{43} = 1, M_{55} = 1, M_{66} = 1,$$

$$M_{77} = 1$$

2. N matrix (7×7)

$$N_{11} = -0.088, N_{12} = 0.392, N_{13} = -0.74$$

$$N_{21} = -1.48, N_{22} = 4.46, N_{26} = -0.246$$

$$N_{31} = -0.619, N_{36} = -0.710$$

$$N_{44} = 1$$

$$N_{52} = -1, N_{53} = 1$$

$$N_{66} = -\frac{1}{\tau_a}$$

3. P Matrix (7×4)

$$P_{64} = \frac{1}{\tau_a}, P_{73} = 1$$

4. Q matrix (7×1) is a null matrix

For equation 2.2 the non zero elements are

1. R matrix (4×7)

$$R_{47} = -1$$

2. S matrix (4×4)

$$S_{21} = -1$$

3. T matrix (4×1)

$$S_{11} = 1$$

4. E (4×7×3)

$$E_{133} = -1, E_{372} = -1$$

5. H(4×4×3)

$$H_{211} = 1, H_{322} = 1, H_{411} = 1$$

The model is represented by the equations

$$\dot{\underline{x}}_m = F_m \underline{x}_m + Q_m c \quad (2.6)$$

$$\underline{y}_m = S_m \underline{x}_m \quad (2.7)$$

The error between the model and system response is defined as

$$\underline{e} = \underline{y}_s - \underline{y}_m$$

or

$$\underline{e} = S_{s-s} \underline{x}_s + S_{m-m} \underline{x}_m \quad (2.8b)$$

The control signals whose magnitudes are to be limited are related to the system state vector by

$$\underline{u} = S_{u-s} \underline{x}_s \quad (2.9)$$

The command inputs $\underline{c}$ are taken to be impulse inputs, i.e.

$$\underline{c} = \delta(t) \underline{w} \quad (2.10)$$

where $\underline{w}$ is a constant vector with components equal to the magnitude of the input impulses at time $t = 0$, and $\delta(t)$ is the delta function.

2.2 Initial Condition Response

Substituting for $\underline{b}$ from (2.2), into (2.1), and pre-multiplying by M^{-1} , the system of equations can be written as

$$\dot{\underline{x}}_s = F_{s-s} \underline{x}_s + Q_{s-} \underline{c} \quad (2.11)$$

An augmented state vector is defined as

$$\underline{x} = \begin{bmatrix} \underline{x}_s \\ -- \\ \underline{x}_m \end{bmatrix} \quad (2.12)$$

The equations (2.11), and (2.6), for the system and model can be combined and written as

$$\dot{\underline{x}} = \underline{F}\underline{x} + \underline{G}\underline{c} \quad (2.13)$$

where the augmented system differential transition matrix

$$\underline{F} = \begin{bmatrix} \underline{F}_s & | & 0 \\ \hline 0 & | & \underline{F}_m \end{bmatrix} \quad (2.14)$$

and the augmented control matrix is

$$\underline{G} = \begin{bmatrix} \underline{Q}_s \\ -- \\ \underline{Q}_m \end{bmatrix} \quad (2.15)$$

Since the impulse response is being considered here, the solution to equation (2.13), with initial conditions $\underline{x}(0)=\underline{0}$ can be obtained by solution of

$$\dot{\underline{x}} = \underline{F}\underline{x} \quad (2.16)$$

with initial conditions

$$\underline{x}(0) = \underline{G}\underline{w} \quad (2.17)$$

2.3 Formulation of J in terms of $\underline{x}$

The performance index of equation (1.4), introduced in Chapter 1 is a measure of the error between system and nominal response, the first derivative of this error, and the magnitudes of control signals required to affect the system response. Using the definition of each of these quantities, J can be written in terms of $\underline{x}$ as follows:

From equation 2.8b, $\underline{e}$ and $\dot{\underline{e}}$ can be written as

$$\underline{e} = \begin{bmatrix} \underline{S}_s & | & \underline{S}_m \end{bmatrix} \underline{x} \quad (2.18)$$

$$\dot{\underline{e}} = \begin{bmatrix} \underline{S}_s \underline{F}_s & | & \underline{S}_m \underline{F}_m \end{bmatrix} \underline{x} \quad (2.19)$$

and from equation 2.9 $\underline{u}$ can be written as

$$\underline{u} = \begin{bmatrix} \underline{S}_u & | & 0 \end{bmatrix} \underline{x} \quad (2.20)$$

In (2.20), above and in the discussion to follow $[0]$ will be implicitly assumed to be an appropriately dimensioned

null matrix.

Substituting for $\underline{e}$, $\dot{\underline{e}}$ and $\underline{u}$ from equation (2.18), (2.19), and (2.20), into equation (1.4), leads to'

$$J = \int_0^\infty \underline{x}^T \left\{ \begin{bmatrix} S_s^T \\ -- \\ S_m^T \end{bmatrix} W_e [S_s | S_m] + \begin{bmatrix} F_s^T S_s^T \\ ---- \\ F_m^T S_m^T \end{bmatrix} \beta W_e [S_s F_s | S_m F_m] \right. \\ \left. + \begin{bmatrix} S_u^T \\ -- \\ 0 \end{bmatrix} W_u [S_u | 0] \right\} \underline{x} dt \quad (2.21)$$

For the performance index.

Defining Q as the symmetric positive-semidefinite matrix.

$$Q = \left\{ \begin{bmatrix} S_s^T \\ -- \\ S_m^T \end{bmatrix} W_e [S_s | S_m] + \begin{bmatrix} F_s^T S_s^T \\ ---- \\ F_m^T S_m^T \end{bmatrix} \beta W_e [S_s F_s | S_m F_m] \right. \\ \left. + \begin{bmatrix} S_u^T \\ -- \\ 0 \end{bmatrix} W_u [S_u | 0] \right\} \quad (2.22)$$

The expression for the performance index can be written more

compactly as

$$J = \int_0^{\infty} ||\underline{x}(t)||_Q^2 dt \quad (2.23)$$

where $\underline{x}(t)$ is the solution to equation (2.16) with initial conditions (2.17). If the F matrix in eqn. (2.16), is a "stability" matrix, that is all its eigenvalues have negative real parts, then J can be evaluated as

$$J = \underline{x}^T(0) P \underline{x}(0) ; \underline{x}(0) = G \underline{w} \quad (2.24)$$

where P is given by the solution to the matrix algebraic equation

$$F^T P + P F = -Q \quad (2.25)$$

as follows from a corollary to Lyapunov's theorem on the stability of linear invariant systems. [1,5,6]. It is noted in passing that the matrix P in equation (2.25), is symmetric. This fact leads to some computational simplification as indicated in the next chapter.

2.4 Derivation of Equations for the Parameter Adjustment Algorithm.

The control system is described by equations (2.1),

and (2.2). These are rewritten here as

$$\dot{\underline{x}}_s = M^{-1}N\underline{x}_s + M^{-1}P\underline{b} + M^{-1}Q'\underline{c} \quad (2.26)$$

$$[I-S-\sum_{i=1}^n K_i H_i]\underline{b} = R\underline{x}_s + T\underline{c} + \left(\sum_{i=1}^n K_i E_i\right)\underline{x}_s \quad (2.27)$$

define

$$\tilde{N} = \left[I-S-\sum_{i=1}^n K_i H_i \right] \quad (2.28)$$

and

$$\tilde{M} = \tilde{N}^{-1} \quad (2.29)$$

then

$$\underline{b} = \tilde{M}[R\underline{x}_s + T\underline{c} + \left(\sum_{i=1}^n K_i E_i\right)\underline{x}_s] \quad (2.30)$$

substitution into (2.26), gives

$$\dot{\underline{x}}_s = [M^{-1}N+M^{-1}P\tilde{M}R+M^{-1}P\tilde{M}\sum_{i=1}^n K_i E_i]\underline{x}_s + [M^{-1}P\tilde{M}T+M^{-1}Q']\underline{c} \quad (2.31)$$

This is of the form of equation (2.11), with F_s and Q_s defined as

$$F_s = [M^{-1}N + M^{-1}P\tilde{M}R + M^{-1}P\tilde{M}\sum_{i=1}^n K_i E_i] \quad (2.32)$$

$$Q_s = [M^{-1}\tilde{P}_{MT} + M^{-1}Q'] \quad (2.33)$$

Also required are the gradients of F_s and Q_s with respect to the i^{th} parameter K_i . Differentiating (2.32) with respect to K_i , using (2.28) and noting that

$$\frac{\partial \tilde{M}}{\partial K_i} = -\tilde{N}^{-1} \frac{\partial \tilde{N}}{\partial K_i} \tilde{N}^{-1} = -\tilde{M} \frac{\partial \tilde{N}}{\partial K_i} \tilde{M} = \tilde{M} H_i \tilde{M} \quad (2.34)$$

then

$$\frac{\partial F_s}{\partial K_i} = M^{-1} P M H_i [\tilde{M} R + \tilde{M} \sum_{i=1}^n K_i E_i] + M^{-1} P M E_i \quad (2.35)$$

Similarly

$$\frac{\partial Q_s}{\partial K_i} = M^{-1} P M H_i M T \quad (2.36)$$

The gradients of the augmented system matrices can be written down (observing that the model parameters are invariant) as

$$\frac{\partial F}{\partial K_i} = \left[\begin{array}{c|c} \frac{\partial F_s}{\partial K_i} & 0 \\ \hline 0 & 0 \end{array} \right] \quad (2.37a)$$

$$\frac{\partial G}{\partial K_i} = \left[\begin{array}{c} \frac{\partial Q_s}{\partial K_i} \\ \hline 0 \end{array} \right] \quad (2.37b)$$

The gradient of the Q matrix defined in equation (2.22)

with respect to K_i is

$$\frac{\partial Q}{\partial K_i} = \begin{bmatrix} \frac{\partial F_s^T}{\partial K_i} S_s^T \\ \hline 0 \end{bmatrix} \beta W_e [S_s F_s | S_m F_m] + \begin{bmatrix} F_s^T S_s^T \\ \hline F_m^T S_m^T \end{bmatrix} \beta W_e \left[S_s \frac{\partial F_s}{\partial K_i} \right] \begin{bmatrix} 0 \end{bmatrix} \quad (2.38a)$$

If the weighting matrix W_e , is a diagonal matrix (or symmetric) then,

$$\frac{\partial Q}{\partial K_i} = \begin{bmatrix} \left(\frac{\partial F_s}{\partial K_i} \right)^T S_s^T \\ \hline 0 \end{bmatrix} \beta W_e [S_s F_s | S_m F_m] + \left\{ \begin{bmatrix} \left(\frac{\partial F_s}{\partial K_i} \right)^T S_s^T \\ \hline 0 \end{bmatrix} \beta W_e [S_s F_s | S_m F_m] \right\}^T \quad (2.38b)$$

2.5 Parameter Adjustment Algorithm-Sequence Logic

The minimization of the performance index is carried out by first-order gradient techniques. The incremental changes in the parameter values being made so as to produce the maximum decrease in the magnitude of the performance index at any instant. This is accomplished by selecting the incremental changes proportional to the negative gradient of J at the operating point.

The incremental change of the i^{th} parameter K_i is

$$\Delta K_i = -\lambda \frac{\partial J}{\partial K_i} \quad \text{for } i = 1, 2, \dots, n \quad (2.39)$$

where λ is a positive constant. The gradient of J with respect to K_i is obtained by differentiating (2.24), with respect to K_i , that is,

$$\frac{\partial J}{\partial K_i} = \frac{\partial \underline{x}^T(0)}{\partial K_i} P \underline{x}(0) + \underline{x}(0) \frac{\partial P}{\partial K_i} \underline{x}(0) + \underline{x}^T(0) P \frac{\partial \underline{x}(0)}{\partial K_i} \quad (2.40a)$$

or since P is symmetric

$$\frac{\partial J}{\partial K_i} = \underline{x}^T(0) \frac{\partial P}{\partial K_i} \underline{x}(0) + 2 \frac{\partial \underline{x}^T(0)}{\partial K_i} P \underline{x}(0) \quad (2.40b)$$

P and $\partial P / \partial K_i$ are evaluated successively from

$$F^T P + P F^T = -Q \quad (2.41)$$

and

$$F^T \frac{\partial P}{\partial K_i} + \frac{\partial P}{\partial K_i} F = - \frac{\partial Q}{\partial K_i} - \left[\left(\frac{\partial F}{\partial K_i} \right)^T P + P \left(\frac{\partial F}{\partial K_i} \right) \right] \quad (2.42)$$

The gradient of the initial condition vector is given by

$$\frac{\partial \underline{x}(0)}{\partial K_i} = \frac{\partial G}{\partial K_i} w \quad (2.43)$$

Once $\partial P / \partial K_i$, P and $\partial \underline{x}(0) / \partial K_i$ have been evaluated $\partial J / \partial K_i$ and ΔK_i for $i = 1, 2, \dots, n$ can be evaluated from equations (2.40b), and (2.39), respectively.

In summary then: the parameter adjustment algorithm proceeds as follows:

1. A set of initial parameter values K_i , $i=1, 2, \dots, n$ is selected. Assuming the resulting system is stable [the asymptotic stability is checked using the Routh Criterion], the next step is
2. Determination of the matrices F and Q from equation (2.14), and (2.22).
3. The matrix algebraic equation (2.25), is solved for P
4. The gradients of F , Q and $\underline{x}(0)$ with respect to K_1 are obtained from equations (2.37a), (2.38a), and (2.43), respectively.
5. Using F and Q determined in step 2 and P determined in step 3, equation (2.42), is solved for $\partial P / \partial K_1$.
6. $\partial J / \partial K_1$ is evaluated from (2.40b), and ΔK_1 from (2.39).
7. Steps 4 through 6 are repeated for $i=2, 3, \dots, n$
8. The predicted change in the performance index J is then evaluated according to

$$\Delta J = -\lambda \left[\left(\frac{\partial J}{\partial K_1} \right)^2 + \left(\frac{\partial J}{\partial K_2} \right)^2 + \dots + \left(\frac{\partial J}{\partial K_n} \right)^2 \right]$$

9. The procedure from steps 2 through 8 is repeated using the revised values of the parameters until

$$\left[\left(\frac{\partial J}{\partial K_1} \right)^2 + \left(\frac{\partial J}{\partial K_2} \right)^2 + \dots + \left(\frac{\partial J}{\partial K_n} \right)^2 \right]$$

is very small.

CHAPTER 3

Program Description

In this chapter a computer program scheme for implementing the algorithm developed in the previous chapter is outlined. Fig. 3.1 presents the overall flow of the program logic while Fig. 3.2 is the flow diagram for the solution of the matrix algebraic equation $AX + XB = -C$.

3.1 The overall program

1. Input. The system configuration represented by equations 2.1, 2.2 and 2.3 and the model are input by inputting only the non-zero elements of each of the system and model matrices, the rest being automatically initialized to zeros. All data is input using the namelist option. The data input format is described in Appendix A.

2. The augmented F matrix is evaluated according to the equation (2.37), derived in Chapter 2.

3. The characteristic polynomial of the F matrix is obtained in two stages. The matrix is transformed using subroutine SMLTRN (A subroutine in the program for the solution of the matrix equation) to a block diagonal form. The transformation method used is that due to A.M. Danilevskii [3]. In the general case the process will degenerate so that the transformed matrix will consist of more than one

diagonal block.

The general form of the transformed matrix [4] is

$$\Lambda = \left[\begin{array}{ccc|ccc|ccc|ccc} L_1 & & & M_{12} & & & & & & & & \\ & \text{---} & & & M_{13} & & & & & & & \\ & & L_2 & & & & & & & & & \\ & & & \text{---} & & & & & & & & \\ & & & & L_3 & & & & & & & \\ & & & & & \text{---} & & & & & & \\ & & & & & & \ddots & & & & & \\ & & & & & & & & & & L_r & \\ & & & & & & & & & & & \text{---} \end{array} \right] \quad (3.1)$$

where the L_i 's are the companion matrices

$$L_i = \left[\begin{array}{cccccccc} 0 & 0 & \dots & \dots & \dots & 0 & a_{1i} \\ 1 & 0 & \dots & \dots & \dots & 0 & a_{2i} \\ 0 & 1 & \dots & \dots & \dots & 0 & a_{3i} \\ \dots & \dots & \dots & \dots & \dots & \dots & \dots \\ 0 & 0 & & & & 1 & a_{ki} \end{array} \right] \quad (3.2)$$

and the off diagonal blocks M_{li} are of the form

$$M_{li} = \left[\begin{array}{cccccccc} 0 & 0 & \dots & \dots & \dots & 0 & p_{1i} \\ 0 & 0 & \dots & \dots & \dots & 0 & p_{2i} \\ 0 & 0 & \dots & \dots & \dots & 0 & p_{3i} \\ \dots & \dots & \dots & \dots & \dots & \dots & \dots \\ 0 & 0 & \dots & \dots & \dots & 0 & p_{ki} \end{array} \right] \quad (3.3)$$

Due to the quasi-triangular character of Λ , its characteristic polynomial is simply the product of the characteristic polynomials of the diagonal blocks. Furthermore the characteristic polynomial is invariant under the similarity transformation. Subroutine SCAN1 identifies the characteristic polynomials of the individual blocks and forms the product to give the characteristic polynomial of the F matrix.

4. The stability of the F matrix is next checked by means of subroutine RSCHEK which is simply an implementation of the Routh criterion and works on the characteristic polynomial of the F matrix. Only asymptotic stability is checked here. The condition code ICODE = 0 indicates a stability matrix while ICODE = 1 indicates a non-stability matrix.

5. The evaluation of the G and Q matrices as well as the augmented initial condition vector proceeds according to the equation (2.15), and (2.22), respectively of the previous chapter.

6. The solution of the matrix equation

$$F^T P + P F = -Q \quad (3.4)$$

for P is a special case of the solution to

$$A X + X B = -C \quad (3.5)$$

The program flow for this stage is described in greater

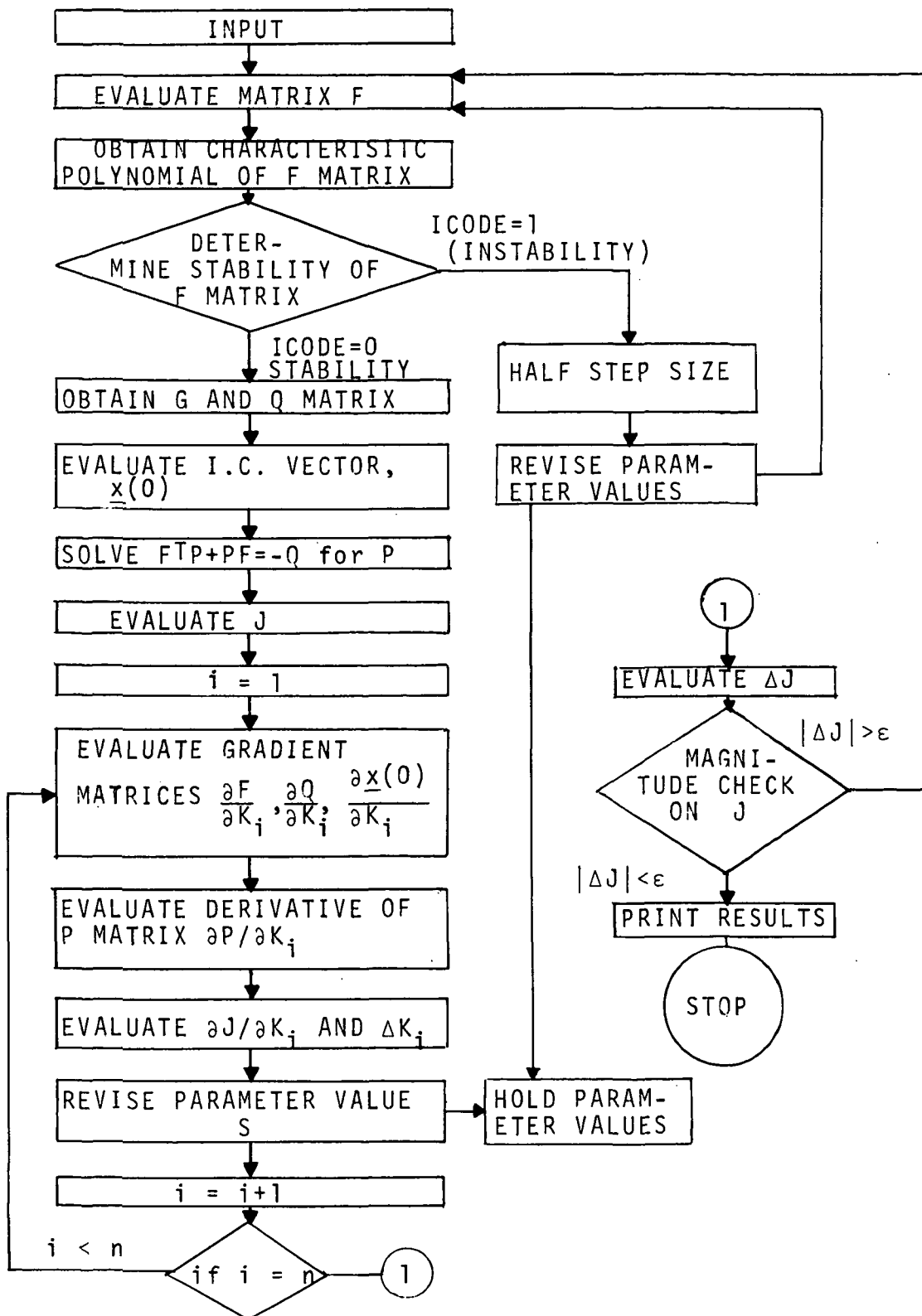


Fig. 3.1 Overall Program Flow Logic

detail in the next section. At this point the following is noted.

In order to avoid the evaluation and inversion of matrix polynomials of relatively higher degrees involving powers of matrices of relatively larger dimensions, it may be more efficient to reduce the orders of the matrix algebraic equation to be solved. This may be done by partitioning the system of equation (3.4), as indicated below.

$$\begin{bmatrix} F_s^T & | & 0 \\ \hline 0 & | & F_m^T \end{bmatrix} + \begin{bmatrix} P_{11} & | & P_{12} \\ \hline P_{21} & | & P_{22} \end{bmatrix} + \begin{bmatrix} P_{11} & | & P_{12} \\ \hline P_{21} & | & P_{22} \end{bmatrix} \begin{bmatrix} F_s & | & 0 \\ \hline 0 & | & F_m \end{bmatrix} \\
 = \begin{bmatrix} -Q_{11} & | & -Q_{12} \\ \hline -Q_{21} & | & -Q_{22} \end{bmatrix} \quad (3.5)$$

Therefore the solution to (3.4), can be obtained by solving the set of equations

$$\begin{aligned}
 F_s^T P_{11} + P_{11} F_s &= -Q_{11} \\
 F_s^T P_{12} + P_{12} F_m &= -Q_{12} \\
 F_m^T P_{21} + P_{21} F_s &= -Q_{21} \\
 F_m^T P_{22} + P_{22} F_m &= -Q_{22}
 \end{aligned} \quad (3.6)$$

Each of these equations could be solved by the same procedure. It was shown earlier that Q is a symmetric matrix. From (3.4), P is therefore symmetric. The second and third equations of (3.6), are therefore identical. If the nominal transfer function is taken to be a simple first order lag, additional simplification is possible by observing that the last equation of (3.6), becomes a scalar equation with P_{22} given by

$$P_{22} = -Q_{22}/2F_m \quad (3.7)$$

and the 2nd and 3rd equations reduce to linear algebraic equations, denoting P_{12} and Q_{12} by $\underline{P}_{12}$ and $\underline{Q}_{12}$, the solution is given by

$$\underline{P}_{12} = [F_s^T + IF_m]^{-1} \underline{Q}_{12} \quad (3.8)$$

The solution to the first equation is obtained by the method of the next section

7. The next stage is the computation of the various gradient matrices with respect to the parameters K_i , $i=1, \dots, n$ and then the gradient of the performance index. The parameter values are revised typically by about 10% of their original values, the original values being held, should the revised parameter lead to an unstable augmented

F matrix. If indeed the revised set of parameters lead to an unstable system as determined by RSCHEK in the subsequent iteration, the parameter values are revised by 50% of the old revision. The process of successive revision of parameter values with 50% reduction in step size could be terminated for maximum number of iterations exceeding say, four.

8. The change in the performance index is easily evaluated from the gradients. The magnitude of the change is used as one stopping condition. Limiting the number of iterations if this proves excessive is also used.

3.2 The solution of the equation $AX+XB = -C$.

It was indicated earlier that solution of equations of the type (3.4), is involved at each iteration of the parameter optimization algorithm. Equation (2.4), is a special case of the equation (3.5). A program for the solution of the equation (3.5) is described in the following paragraphs. The details of the algorithm on which MSOLVE is based is presented in [4]. The solution proceeds essentially as follows.

Consider the equation

$$AX + XB = -C \quad (3.9)$$

where A and B are arbitrary square matrices, of dimensions $n \times n$ and $m \times m$ respectively. C is a known $n \times n$ matrix while X is the unknown $n \times m$ matrix. The necessary and

sufficient condition that the system (3.9) possess a unique solution is that the matrices $-A$ and B not have common eigenvalues [9]. In terms of the computation procedure, violation of this condition leads to a divide check, a sentinel and indication of common eigenvalues is therefore included. For the specialized case

$$F^T P + P F = -Q \quad (3.10)$$

a unique solution exists if and only if all eigenvalues of F have negative real parts, or F is a stability matrix [1].

According to [4], a solution is assumed of the form

$$X = UV^{-1} \quad (3.11)$$

where V^{-1} is a square matrix of dimension $m \times m$ and U is rectangular of dimension $n \times m$.

Substitution into (3.9) leads to

$$AU + CV = -U\Lambda \quad (3.12)$$

where

$$\Lambda = V^{-1}BV \quad (3.13)$$

Referring to Fig. 3.2, the first step is then to obtain

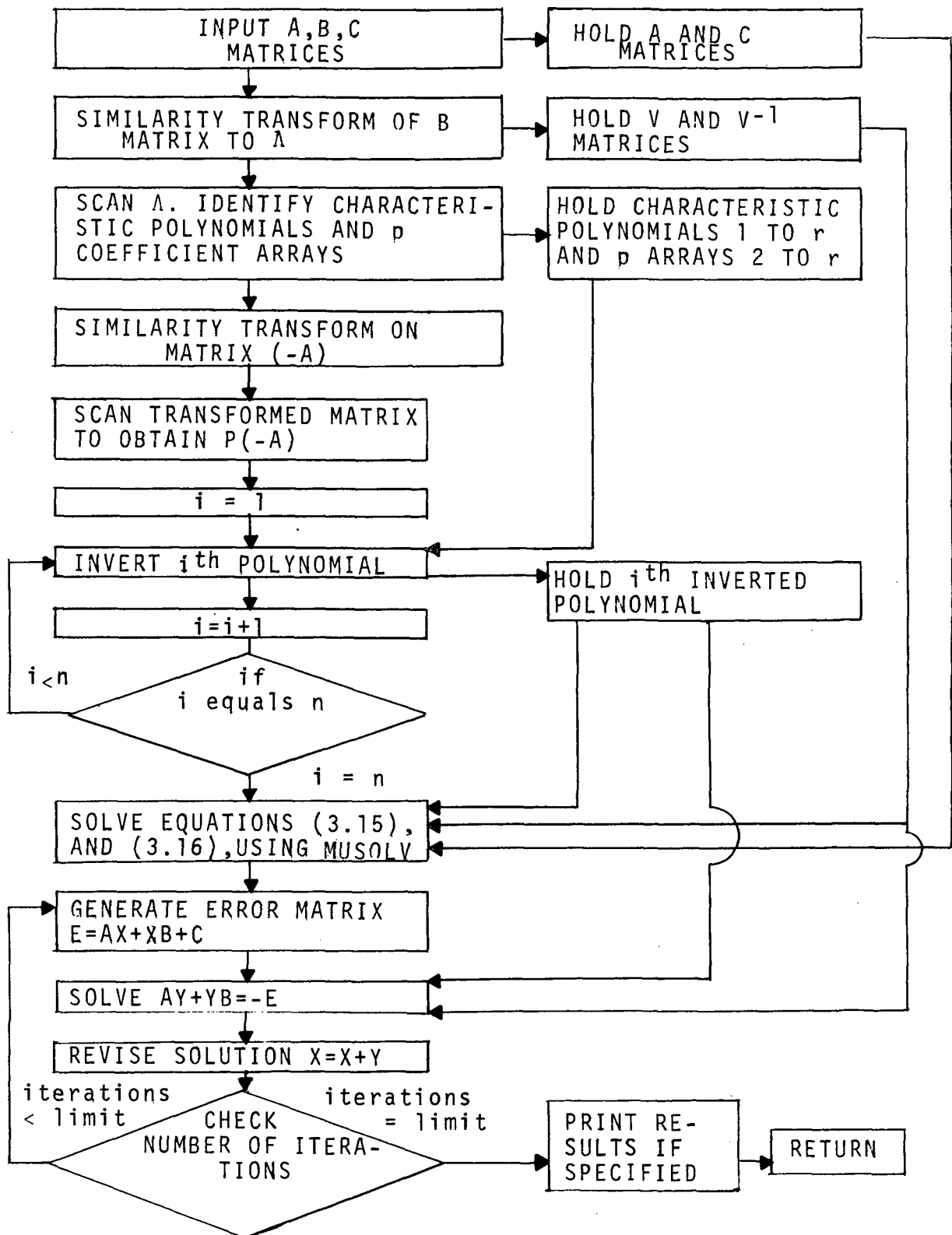


Fig. 3.2 Program Flow Logic for Solution of Matrix Algebraic Equation $AX+XB=-C$

Λ by a sequence of similarity transformations. The general form of the Λ matrix is given by equations (3.1), (3.2), and (3.3). The similarity transformation matrices V and V^{-1} are also generated by SMLTRN and held.

Writing U and CV in 3.12 as

$$U = [\underline{u}_1 | \underline{u}_2 \dots \underline{u}_m]$$

$$CV = [\underline{v}_1 | \underline{v}_2 \dots \underline{v}_m] \quad (3.14)$$

Expanding (3.12), by columns and using (3.2) and (3.3) leads to the following set of equations in terms of the columns of U .

$$A\underline{u}_1 + \underline{v}_1 = -\underline{u}_2$$

$$A\underline{u}_2 + \underline{v}_2 = -\underline{u}_3$$

$$\vdots$$

$$A\underline{u}_{k-1} + \underline{v}_{k-1} = -\underline{u}_k$$

$$A\underline{u}_k + \underline{v}_k = a_{11}\underline{u}_1 + a_{21}\underline{u}_2 + \dots + a_{k1}\underline{u}_k$$

$$A\underline{u}_{k+1} + \underline{v}_k = -\underline{u}_{k+2}$$

$$\vdots$$

$$A\underline{u}_{k+l} + \underline{v}_{k+l} = -p_{12}\underline{u}_1 - p_{22}\underline{u}_2 - \dots - p_{k2}\underline{u}_k + a_{12}\underline{u}_{k+1} + a_{22}\underline{u}_{k+2} \\ + \dots + a_{l2}\underline{u}_{k+l}$$

$$\vdots$$

$$\vdots$$

$$\begin{aligned}
& \vdots \\
& A \underline{u}_{-m-q+1} + \underline{v}_{-m-q-1} = -\underline{u}_{-m-q+2} \\
& \vdots \\
& A \underline{u}_{-m} + \underline{v}_{-m} = -p_{1r} \underline{u}_1 - p_{2r} \underline{u}_2 - \dots - p_{(m-q)r} \underline{u}_{-m-q} + a_{1r} \underline{u}_{-m-q+1} \\
& \quad + a_{2r} \underline{u}_{-m-q+2} + \dots + a_{qr} \underline{u}_{-m} \quad (3.15)
\end{aligned}$$

In the above, the dimension of the first diagonal block is k that of the 2nd ℓ and that of the r th is q . Taking $\underline{u}_1, \underline{u}_{k+1} \dots \underline{u}_{k+\ell+1} \dots \underline{u}_{-m-q+1}$ as unknowns and substituting for the other vectors of $\underline{u}$ in terms of these into k th $(k+\ell)^{th}$ and m^{th} equation of (3.15), leads to

$$\begin{aligned}
& [(-A)^k + a_{k1}(-A)^{k-1} + \dots + a_{21}(-A) + a_{11}I] \underline{u}_1 \\
& \quad = \sum_{j=1}^k \sum_{h=j+1}^{k+1} a_{h1} (-A)^{h-(j+1)} \underline{v}_j \\
& [(-A) + a_{\ell 2}(-A)^{\ell-1} + \dots + a_{22}(-A) + a_{12}I] \underline{u}_{k+1} \\
& \quad = \sum_{j=1}^{\ell} \sum_{h=j+1}^{\ell+1} a_{h2} (-A)^{h-(j+1)} \underline{v}_{j+k} + \sum_{i=1}^k p_{12} \underline{u}_i \\
& \quad \vdots \\
& \quad \vdots \\
& [(-A)^q + a_{qr}(-A)^{q-1} + \dots + a_{2r}(-A) + a_{1r}I] \underline{u}_{-m-q+1} \\
& \quad = \sum_{j=1}^q \sum_{h=j+1}^{q+1} a_{hr} (-A)^{h-(j+1)} \underline{v}_{j+m-q} + \sum_{i=1}^{m-q} p_{1r} \underline{u}_i \\
& \quad (3.16)
\end{aligned}$$

In particular if Λ is composed of a single companion block, then

$$[p_B(-A)]u_1 = \sum_{j=1}^m \sum_{h=j+1}^{m+1} a_h(-A)^{h-(j+1)} \underline{v}_j \quad (3.17)$$

The polynomials on the left hand side of the equation in (3.16), are simply the characteristic polynomials of the individual companion blocks with λ replaced by $(-A)$. The right hand side contains the elements of the last columns of each of the off diagonal M blocks. Referring to Fig. (3.2), the Λ matrix is next scanned to identify and hold the relevant arrays to be used in (3.16).

The first equation of (3.16), is next solved for $\underline{u}_1, \underline{u}_2, \underline{u}_3 \dots \underline{u}_k$ are then determined from (3.15). These in turn are used in the second equation of (3.16), to obtain $\underline{u}_{k+1}$ and so on for the r blocks.

The solution for $\underline{u}_1, \underline{u}_{k+1} \dots \underline{u}_{m-q+1}$ involves the inversion of the matrix polynomials on the left hand side of (3.16). The inversion scheme uses the characteristic polynomial of the $(-A)$ matrix, accordingly this is next evaluated as indicated in Figure (3.2). The inversion scheme is based on the following.

Given two polynomials.

$$P(x) = x^m + a_m x^{m-1} + a_{m-1} x^{m-2} + \dots + a_2 x + a_1$$

$$Q(x) = x^p + b_p x^{p-1} + b_{p-1} x^{p-2} + \dots + b_2 x + b_1 \quad (3.18)$$

which are relatively co-prime, then [4] there exist polynomials $\tilde{P}(x)$ and $\tilde{Q}(x)$, such that

$$\tilde{Q}(x)P(x) + \tilde{P}(x)Q(x) = k \quad (3.19)$$

If $P(\lambda)$ is the characteristic polynomial of matrix $(-A)$

$$\tilde{P}(-A)Q(-A) = kI \quad (3.20)$$

Therefore if $Q(-A)$ is the polynomial to be inverted,

$$Q(-A)^{-1} = \tilde{P}(-A) \quad (3.21)$$

In Fig. 3.2, MPINV is a subroutine which evaluates $\tilde{P}(-A)$ iteratively using the Euclidean Algorithm.

The required polynomials in the equation (3.16), having been evaluated, these together with the set (3.15), are solved to obtain the matrix U , from which X is obtained from (3.11).

The preliminary solution so obtained can be improved by iteration in the following manner. An error matrix E is generated as

$$E = AX + XB + C \quad (3.22)$$

The last part of the solution routine, MUSOLV, is used to solve

$$AY + YB = -E \quad (3.23)$$

The revised solution is then

$$X = X+Y$$

which can be revised again. The number of iterations required will depend on the dimensions of the A and B matrices. If for instance both are three by three square with elements of the order unity, underflows could result if the number of iterations specified exceeds say 2 or 3.

CHAPTER 4

Design Via Parameter Optimization

The preceeding chapters presented the analytical development of the parameter optimization algorithm, and outlined a program for its practical implementation.

In this chapter the basic design procedure is illustrated by means of a single input-single output system. The model used is a simple first order lag. However as indicated in Chapter 3, the scheme could be extended to include higher order models. In fact a higher order model would certainly be required if a specification envelope is to be set up around the nominal response.

4.1 System and Model Configuration Describing Equations

The closed loop systems considered in the following discussion are shown in Figs. 4.1a, and 4.2.

Referring to Fig. 4.1a, the system state variables are x_1 , x_2 and x_3 while b_1 and b_2 are bus variables. These are indicated on Fig. 4.1a. The model and system both have d.c. gains of unity for step inputs.

The equations describing the system and model are

$$\left. \begin{aligned} \dot{x}_1 &= -2x_1 + b_2 \\ \dot{x}_2 &= x_1 \\ \dot{x}_3 &= -x_3 + x_2 \end{aligned} \right\} \quad (4.1a)$$

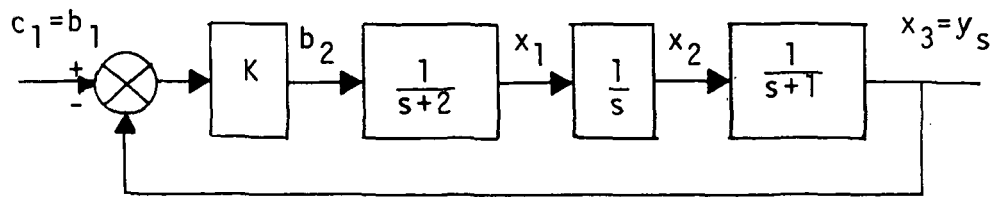


Fig. 4.1a Block Diagram of Closed Loop System with Position Feedback. K is a Free Design Parameter.

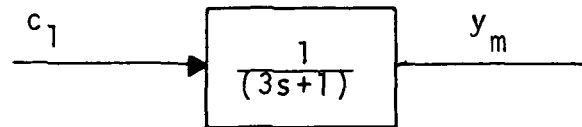


Fig. 4.1b The Nominal Transfer Function

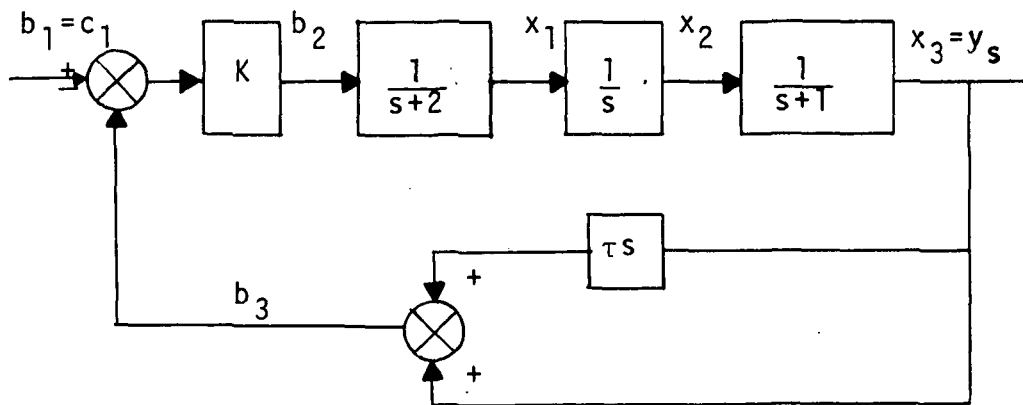


Fig. 4.2 Closed Loop System with Rate Feedback Added
 K and τ are free parameters.

$$b_1 = c_1$$

$$b_2 = Kb_1 - Kx_3 \quad (4.1b)$$

The model is described by

$$\dot{x}_m = -0.33 x_m + 0.33 c_1 \quad (4.2)$$

The system equations can be written in the form 2.1 and 2.2 as

$$\begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \dot{\underline{x}}_s = \begin{bmatrix} -2 & 0 & 0 \\ 1 & 0 & 0 \\ 0 & 1 & -1 \end{bmatrix} \underline{x}_s + \begin{bmatrix} 0 & 1 \\ 0 & 0 \\ 0 & 0 \end{bmatrix} \underline{b} + \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \underline{c} \quad (4.3a)$$

$$\underline{b} = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \underline{x}_s + \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix} \underline{b} + \begin{bmatrix} 1 \\ 0 \end{bmatrix} \underline{c} + K_1 \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} \underline{b} + K_1 \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & -1 \end{bmatrix} \underline{x}_s \quad (4.3b)$$

where

$$\underline{x}_s^T = [x_1 \ x_2 \ x_3] \quad \text{and} \quad \underline{b}^T = [b_1 \ b_2]$$

The system and model outputs are defined by

$$\underline{y}_s = [0 \ 0 \ 1] \underline{x}_s \quad (4.4a)$$

$$Y_m = -x_m \quad (4.4b)$$

No control signals are defined to be included in the cost functional. The system of equations 4.2, 4.3 and 4.4 are input using the namelist option, the input data format for which is described in Appendix A. Other input data include

1. The number of free design parameter IGAIN. IGAIN = 1 for the system of Fig. 4.1a and 2 for Fig. 4.2.
2. The dimensions of the various vectors KE = 1, KM = 1, KC = 1, KX = 3, KX1 = 4, KB = 2 for the system of Fig. 4.1a where the number of bus variables is 2 and KB = 3 for the system of Fig. 4.2.
3. The initial values of the parameter(s). PARAM(1) = 1.4 for the first system while PARAM(1) = 1, PARAM(2) = 1 for the system with rate feedback added.
4. The step size for parameter revision, STEP.
5. The error weighting matrices W1, W2 and W3 and the positive constant BETA, taken in these examples = 0.15.

For the first system the initial value of K was taken to be 1.4. The adjusted value was 0.32. The response for these two values of loop gain are shown in Fig. 4.3a. As seen from this figure, compared to the nominal, the response with position feedback alone is somewhat slow.

The next step was the addition of rate feedback as shown in the block diagram of Fig. (4.2). There are now two free parameters K and τ which allow independent adjustment of the maximum value and speed of the response. Initial parameter values were taken here to be unity for both K and τ . The values as adjusted by the program were 0.795 for K and 1.26 for τ .

Fig. 4.3b, is a plot of the closed loop system response with rate feedback. Comparison with Fig. 4.3a indicates the improvement in system response relative to nominal. A plot of the position errors for the two system is shown in Fig. 4.3c.

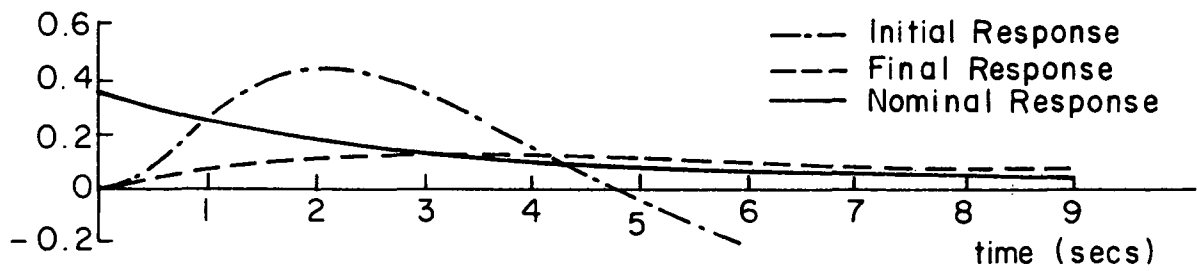


Fig. 4.3a CLOSED LOOP SYSTEM RESPONSE WITHOUT RATE FEEDBACK

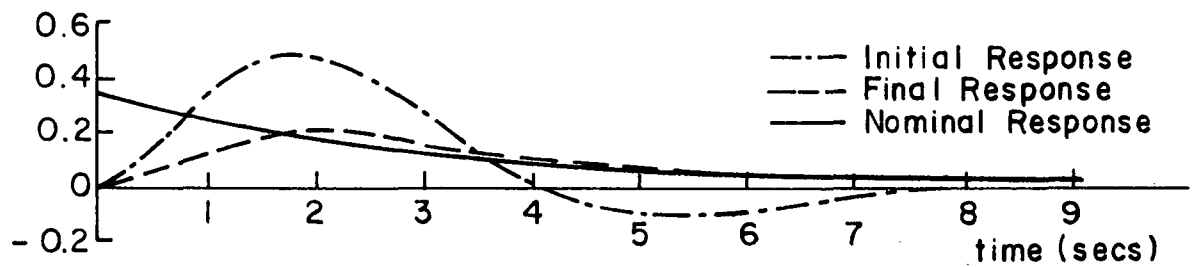


Fig. 4.3b CLOSED LOOP SYSTEM RESPONSE WITH RATE FEEDBACK

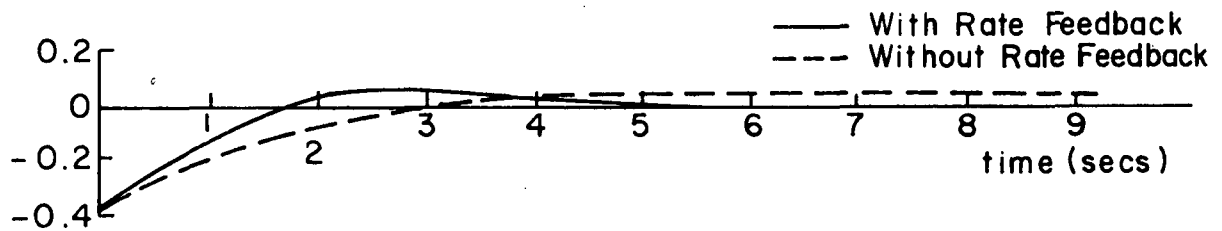


Fig. 4.3c SYSTEM RESPONSE ERROR WITH AND WITHOUT RATE FEEDBACK

CHAPTER 5

Conclusions and Recommendations

5.1 Conclusions

An algorithm for parameter optimization of linear-invariant control systems has been developed. A computer program which implements this algorithm has also been developed and illustrated by means of an example.

The performance index is evaluated using a corollary to Lyapunov's theorem on the stability of linear-invariant systems, rather than by integration of the system and model state equations and subsequent integration of the error at each stage. The aforementioned theorem makes it unnecessary at any stage to integrate the state equations. A result of this scheme was the development of a program for solution of the matrix algebraic equation $AX + XB = -C$ based on the algorithm presented in Ref. [4].

A minimal amount of preprocessing is required to input the system and model configurations as well as the other requisite data. In this context, the defining of bus variables, the form of the equations (2.1), and (2.2), and the namelist option input data format are particularly useful. The state variable selection is not restricted to phase variables. It is possible to select state variables as the outputs of the various integrators as well as physical variables directly from the plant dynamics. Variables of

the first type were a convenient selection for the illustrative example, while the equations for aircraft longitudinal dynamics for instance affords an example of the second kind.

Finally the implementation of the Routh stability criterion enables the program to indicate when the parameter revision sequence leads to unstable systems.

5.2 Recommendations

In its present form the program is restricted to the use of first order models, but as indicated in Chapter 3, the scheme could be modified to include higher order models. This would also make it possible if necessary to use a two dimensional error vector in the cost functional.

A fixed step size was used with a first order gradient method. The step size was kept small to avoid nonlinearities as well as overshooting of the minimum. However to improve the convergence rate, it would be more efficient to vary the step size in the sequence; possibly by including in the parameter revision logic the magnitude of the current parameter values.

APPENDIX A

This section describes the input data format used. All data is input using the namelist option. The necessary data cards for a specific problem are indicated below in the order in which they appear. The namelist option makes it possible to input only the non-zero elements of each matrix or vector, the rest being initialized to zeros.

The system configuration is input first. These are the system matrices of equations 2.1 and 2.2. Each list starts in column 2.

```
&INPUTM SYSM(I,J) = numeric data,&END
&INPUTN SYSN(I,J) = numeric data,&END
&INPUTP SYSP(I,J) = numeric data,&END
&INPUTQ SYSQ(I,J) = numeric data,&END
&INPUTR R(I,J)    = numeric data,&END
&INPUTS S(I,J)    = numeric data,&END
&INPUTT T(I,J)    = numeric data,&END
&INPUTH H(I,J)    = numeric data,&END
&INPUTE E(I,J,K)  = numeric data,&END
```

For the three dimensional arrays E and H in the above format, I corresponds to the bus variable on the left hand side of the equation 2.2, J to the system or bus variable on the right hand side of the equation and K to the parameter relating the two.

The model configuration or nominal transfer function is input by means of the following two lists.

```
&MODEF   FMOD(I,J) = numeric data,&END
```

```
&MODEQ   QMOD(I,J) = numeric data,&END
```

where FMOD and QMOD are the matrices F_m and Q_m respectively.

The system and model output matrices are listed as

```
&SYSOUT  SYSS(I,J) = numeric data,&END
```

```
&MODOUT  SMOD(I,J) = numeric data,&END
```

Note that in the above namelist, the output defined by SMOD is the negative of the model output.

The next three lists input the error weighting matrices W_e , $W_{\dot{e}}$, and the control signal weighting matrix W_u .

```
&WGTErr  W1(I,J) = numeric data,&END
```

```
&WGTEdT  W2(I,J) = numeric data,BETA=numeric value,&END
```

```
&WGTU    W3(I,J) = numeric data,&END
```

The dimensions of the various vectors are input according to

```
&DIMEN KE= , KE= , KM= , KX1= , KC= , KB= ,&END
```

where

KE is the dimension of the error vector ≤ 2
 KX is the dimension of the system state vector ≤ 10
 KM is the dimension of the model state vector ≤ 5
 KX1 is the dimension of the augmented system = KX+KM
 KC is the dimension of the command vector ≤ 5
 KB is the dimension of the bus vector ≤ 10

The next list is

```
&GAIN IGAIN= ,PARAM(K)= ,STEP= ,&END
```

Here IGAIN is put equal to the number of free design parameters. PARAM(K) is the initial value of the K^{th} parameter ($K=1,2,\dots,IGAIN$). STEP is the step size used for revision of the parameter values.

The matrix relating the control signals to the system state vector is SU. If any control signal is to be included in the performance index integral, the appropriate elements of the SU matrix are input as

```
&INPUTU SU(I,J) = numeric data,&END
```

If there is no penalty to be imposed on any of the control signals, then SU is a null matrix. The input list takes the form (as is the case for any null matrix)

```
&INPUTU &END.
```

The last list contains the magnitudes of the delta functions for the command variable vector, i.e.

```
&CONTRL VCOMM(J) = ,&END
```

where $J=1,2\dots KC$.

APPENDIX B

The program implementing the algorithm is listed on the following pages. The listing presents the following program packages.

1. The main program consisting of the algorithm sequence logic. The output consists of the parameter values at each iteration, the iterate number and changes in the performance index at each iteration. The program also lists the final adjusted parameter values and the corresponding system differential transition and control matrices.

2. MSOLVE: this interfaces the main program with the subroutines of the solution to the matrix algebraic equation. These subroutines are

- 2a. SMLTRN: this program implements the Danilevskii Similarity transformation

- 2b. SCAN1: identifies and stores the polynomials of the diagonal blocks of the A matrix. The characteristic polynomial is computed from these.

- 2c. SCAN2: identifies and stores the various arrays of the B matrix for use in MPINV

- 2d. MPINV: this subroutine evaluates the inverses of the various matrix polynomials using the Euclidian algorithm.

2e. MUSOLV: evaluates the matrix U and forms the product UV^{-1} to give the solution matrix X. JWRITE is set to zero if a print out of the solution and error matrices is required. Otherwise JWRITE= 1.

The other subroutines included in the listing are

3. RSCHEK: this is an implementation of the Routh stability criterion and determines asymptotic stability. The condition code ICODE = 0 indicates a stable system, while ICODE = 1 indicates instability.

4. MPDIV, MPNORM, MPMPY, MPSUB, MPMOVE: for polynomial operations and MXMULT a variable dimension matrix multiplication subroutine.

```

REAL*8 SMG(20,20),XQ(20),DELFS(10,10),DELO(20,20),DELF(20,20),
1DELFT(20,20),P(20,20),TEMP3(10,5),DELGS(10,5),DELG(20,5),DELX(20),
3U(20,20),V(20,20),VINV(20,20),A(20,20),B(20,20),XSOLN(20,20),
3RHS(20,20),QINV(5,21),QB(5,21),PB(5,21),SUM,SUM1,SIGMA,PI,DELJ,
4DELTAJ,RH1(10,10),RH12(10,5),RH21(5,10),RH22(5,5),SYSG(10,5),
5SYST(10,10),SYSF2(10,10),DELP(20,20),FINV(10,10),DELK(10),
6PARM(10),C(20,20),C1(20,20),A1(20,20),R1(20,20),PAR(10),PI
  INTEGER*4 IDENT(5),IDIMQB(5),IDIMPR(5),IDIMQI(5)
  DOUBLE PRECISION SYSM(10,10),SYSN(10,10),SYSP(10,10),SYSC(10,5),
1SYSP1(10,10),SYSN1(10,10),SYSQ1(10,5),TEMP(10,10),SI(10,10),X(11),
2SINV(10,10),R(10,10),S(10,10),T(10,5),R1(10,10),T1(10,5),XDOT(11),
3HK(10,10),EK(10,10),H(10,10,10),E(10,10,10),SYSF(10,10),
4 FMOD(5,5),FT(20,20),F(20,20),F1(20,20),F2(20,20),ARRAYF(21),
5 ROUTH1(21),ROUTH2(21),SYSS(5,10),SMOD(5,5),SFS(5,10),SFM(5,5),
6SF(5,20),SFT(20,5),SS(5,20),SST(20,5),W1(5,5),W2(5,5),W3(5,5),
7TEMP1(20,5),TEMP2(20,20),SU(5,10),SUI(5,20),SUIT(20,5),Q(20,20),
8F3(20,20),EK1(10,10),VCOMM(5),PARAM(10),QMOD(5,5),BETA,STEP
  COMMON /HOLDU,V/HOLD1/A,C/HOLD2/QINV,IDIMQI
1/HOLD3/QB,PB,IDIMQB,IDIMPB,IDENT/HOLD4/VINV,B/SECTR1/XSOLN
EQUIVALENCE (HK(1),EK(1)),(FT(1),F2(1)),(Q(1),F3(1)),
1(TEMP2(1),F1(1))
  DATA SYSM/100*0.0/,SYSN/100*0.0/,SYSP/100*0.0/,SYSQ/50*0.0/,
1R/100*0.0/,S/100*0.0/,T/50*0.0/,E/1000*0.0/,H/1000*0.0/,
2X/1.0,10*0.0/,XDOT/1.0,10*0.0/,W1/25*0.0/,W2/25*0.0/,W3/25*0.0/,
3FMOD/25*0.0/,SMOD/25*0.0/,SU/50*0.0/,SYSS/50*0.0/,PARAM/10*0.0/,
4VCOMM/5*0.0/,QMOD/25*0.0/
  NAMELIST /INPUTM/SYSM/INPUTN/SYSN/INPUTP/SYSP/INPUTQ/SYSQ/
1INPUTR/R/INPUTS/S/INPUTT/T/INPUTH/H/INPUTE/E/MODEF/FMDC/MGDEQ/
2QMOD/SYSOUT/SYSS/MODOUT/SMOD/WGTERR/W1/WGTEDT/W2,BETA/WGTU/W3/
3DIMEN/KE,KX,KM,KX1,KC,KB/GAIN/IGAIN,PARAM,STEP/CONTRL/VCOMM/
4INPUTU/SU
  READ(5, INPUTM)
  READ(5, INPUTN)
  READ(5, INPUTP)
  READ(5, INPUTQ)
  READ(5, INPUTR)

```

```

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```

READ(5, INPUTS)
READ(5, INPUTT)
READ(5, INPUTH)
READ(5, INPUTE)
READ(5, MODEF)
READ(5, MODEQ)
READ(5, SYSCUT)
READ(5, MODCUT)
READ(5, WGTERR)
READ(5, WGTEDT)
READ(5, WGTU)
READ(5, DIMEN)
READ(5, GAIN)
READ(5, INPUTU)
READ(5, CONTRL)
PI=0.0
L4=20
L2=5
L1=10
ITTR=0
ITTR1=0
ISTDP=0
CALL SIMEQ(SYSM,XDOT,KX,SINV,X,IERR)
CALL MXMULT(SINV,SYSN,SYSN1,KX,KX,KX,KX,M,N,L1,L1,L1)
CALL MXMULT(SINV,SYSP,SYSP1,KX,KX,KX,KX,M,N,L1,L1,L1)
CALL MXMULT(SINV,SYSQ,SYSQ1,KX,KX,KX,KX,M,N,L1,L1,L1)
5 DO 20 I=1,K8
DO 20 J=1,K8
IF(I.EQ.J)GO TO 10
S1(I,J)=-S(I,J)
GO TO 20
10 S1(I,J)=1.0-S(I,J)
20 CONTINUE
30 DO 40 K=1,IGAIN
DO 40 I=1,K8
DO 40 J=1,K8

```

```

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```

```

HK(I,J)=H(I,J,K)*PARAM(K)
40 SI(I,J)=SI(I,J)-HK(I,J)
CALL SIMEQ(SI,XDOT,KB,SINV,X,IERR)
CALL MXMULT(SINV,R,RI,KB,KB,KX,M,N,LI,LI,LI,LI)
DO 50 I=1,KB
DO 50 J=1,KX
50 EK(I,J)=E(I,J,1)*PARAM(I)
IF(IGAIN.EQ.1)GO TO 61
DO 60 K=2,IGAIN
DO 60 I=1,KB
DO 60 J=1,KX
60 EK(I,J)=EK(I,J)+E(I,J,K)*PARAM(K)
61 CALL MXMULT(SINV,EK,EK1,KB,KB,KX,M,N,LI,LI,LI,LI)
CALL MXMULT(SYSP1,EK1,SYSP1,KB,KB,KX,M,N,LI,LI,LI,LI)
CALL MXMULT(SYSP1,RI,TEMP,KX,KB,KB,KX,M,N,LI,LI,LI,LI)
DO 70 I=1,KX
DO 70 J=1,KX
70 SYSF(I,J)=SYSF(I,J)+TEMP(I,J)+SYSN1(I,J)
DO 100 I=1,KX
DO 100 J=1,KX1
IF(J.GT.KX)GO TO 90
F(I,J)=SYSF(I,J)
F1(I,J)=F(I,J)
GO TO 100
90 F(I,J)=0.0
F1(I,J)=0.0
100 CONTINUE
IR=KX+1
DO 120 I=IR,KX1
DO 120 J=1,KX1
IF(J.LE.KX)GO TO 110
JJ=J-KX
II=I-KX
F(I,J)=FMOD(II,JJ)
F1(I,J)=F(I,J)
GO TO 120

```

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```

GC TO 170
160 SU1(I,J)=0.0
    SU1T(J,I)=SU1(I,J)
170 CONTINUE
    CALL MXMULT(SSST,W1,TEMP1,KX1,KE,KE,M,N,L4,L2,L2,L2)
171 FORMAT(5X,D10.3)
    CALL MXMULT(TEMP1,SS,Q,KX1,KE,KE,KX1,M,N,L4,L2,L2,L4)
    CALL MXMULT(SFT,W2,TEMP1,KX1,KE,KE,M,N,L4,L2,L2,L2)
    CALL MXMULT(TEMP1,SF,TEMP2,KX1,KE,KE,KX1,M,N,L4,L2,L2,L4)
    DO 180 I=1,KX1
    DO 180 J=1,KX1
180 Q(I,J)=Q(I,J)+BETA*TEMP2(I,J)
    CALL MXMULT(SUIT,W3,TEMP1,KX1,KC,KC,M,N,L4,L2,L2,L2)
    CALL MXMULT(TEMP1,SU1,TEMP2,KX1,KC,KC,KX1,M,N,L4,L2,L2,L4)
    DO 190 I=1,KX1
    DO 190 J=1,KX1
190 Q(I,J)=Q(I,J)+TEMP2(I,J)
    DO 221 I=1,KX
    DO 221 J=1,KX
221 SYSFT(I,J)=SYSF(J,I)

      C
      C      Q MATRIX PARTITION
      C
230 DO 231 I=1,KX
    DO 231 J=1,KX
231 RH11(I,J)=Q(I,J)
    IF(ICODE.EQ.1.AND.ITTER.EQ.0)GO TO 1000
    IF(ICODE.EQ.1)GO TO 800
    ITTER1=0
    DO 238 I=1,KX
    DO 238 J=1,KX
    A1(I,J)=SYSFT(I,J)
    B1(I,J)=SYSF(I,J)
    C1(I,J)=RH11(I,J)
238 CALL MSOLVE(KX,KX,KX,A1,B1,C1,JB1,JB2)
    DO 232 I=1,KX
  
```

```

      DO 232 J=1,KX
232  P(I,J)=XSQLN(I,J)
      KX2=KX+1
      DO 233 I=1,KX
233  DO 233 J=KX2,KX1
      JJ=J-KX
      RH12(I,JJ)=Q(I,J)
      DO 234 I=1,KX
234  XDOT(I)=-RH12(I,1)
      DO 236 I=1,KX
      DO 236 J=1,KX
      IF(I.EQ.J)GO TO 235
      SYSF2(I,J)=SYSFT(I,J)
      GO TO 236
235  SYSF2(I,J)=SYSFT(I,J)+FMOD(1,1)
236  CONTINUE
      CALL SIMEQ(SYSF2,XDOT,KX,FINV,X,IERR)
      DO 237 I=1,KX
      P(I,KX1)=X(I)
237  P(KX1,I)=X(I)
      P(KX1,KX1)=-Q(KX1,KX1)/(2.0*FMOD(1,1))
      CALL MXMULT(SINV,T,T1,KB,KB,KB,KC,M,N,L1,L1,L1,L2)
      CALL MXMULT(SYSP1,T1,SYSG,KX,KB,KB,KC,M,N,L1,L1,L1,L2)
      DO 250 I=1,KX
      DO 250 J=1,KC
250  SYSG(I,J)=SYSG(I,J)+SYSQ1(I,J)
      IF(ISTOP.EQ.1)GO TO 520
      EVALUATE AUGMENTED G MATRIX
      DO 270 I=1,KX1
      DO 270 J=1,KC
      IF(I.GT.KX)GO TO 260
      SMG(I,J)=SYSG(I,J)
      GO TO 270
260  II=I-KX

```

```

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MAIN0240
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MAIN0246
MAIN0247
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MAIN0249
MAIN0250
MAIN0251
MAIN0252

270 CONTINUE
C
C
C
      EVALUATE AUGMENTED INITIAL CCNDITION VECTOR
      DO 280 I=1,KX1
      XO(I)=0.0D+00
      DO 280 J=1,KC
      XC(I)=XC(I)+SMG(I,J)*VCOMM(J)
      WRITE(6,261)(XO(I),I=1,KX1)
C
C
C
      EVALUATE PERFORMANCE INDEX
      PI1=PI
      PI=0.0D+00
      DO 300 I=1,KX1
      SIGMA=0.0D+00
      DO 290 J=1,KX1
      SIGMA=SIGMA+P(I,J)*XO(J)
      PI=PI+SIGMA*XO(I)
      WRITE(6,511)PI
      DELTAJ=PI-PI1
      WRITE(6,511)DELTAJ
C
C
C
      EVALUATION OF GRADIENT CF F MATRIX
      DO 320 I=1,KB
      DO 320 J=1,KX
      R1(I,J)=R1(I,J)+EK1(I,J)
      DELTAJ=0.0D+00
      DO 500 K=1,IGAIN
      DO 340 I=1,KB
      DO 340 J=1,KX
      SUM=0.0D+00
      DO 330 I1=1,KB
      SUM=SUM+SINV(I,I1)*H(I1,J,K)
      DO 330 I1=1,KB
      SUM=SUM+SINV(I,I1)*H(I1,J,K)

```

```

340 HK(I,J)=SUM
    CALL MXMULT(HK,RI,TEMP,KB,KB,KB,KX,M,N,L1,L1,L1)
    DO 360 I=1,KB
    DO 360 J=1,KX
    SUM=0.0D+00
    DO 350 I1=1,KB
    350 SUM=SUM+SINV(I,I1)*E(I1,J,K)
    360 TEMP(I,J)=TEMP(I,J)+SUM
    CALL MXMULT(SYSP1,TEMP,DELFS,KX,KB,KB,KX,M,N,L1,L1,L1)
    CALL MXMULT(SYSS,DELFS,SFS,KE,KX,KX,M,N,L2,L1,L1)
    DO 380 I=1,KE
    DO 380 J=1,KX1
    IF(J.GT.KX)GO TO 370
    SS(I,J)=SFS(I,J)
    SST(J,I)=SS(I,J)
    GC TO 380
    370 SS(I,J)=0.0
    SST(J,I)=SS(I,J)
    380 CONTINUE
    CALL MXMULT(SST,W2,TEMP1,KX1,KE,KE,M,N,L4,L2,L2,L2)
    CALL MXMULT(TEMP1,SF,TEMP2,KX1,KE,KE,KX1,M,N,L4,L2,L2,L4)
    DO 390 I=1,KX1
    DO 390 J=1,KX1
    390 DELQ(I,J)=BETA*(TEMP2(I,J)+TEMP2(J,I))
    C
    C
    C
    EVALUATE DELF
    DO 410 I=1,KX1
    DO 410 J=1,KX1
    IF(I.GT.KX.OR.J.GT.KX)GO TO 400
    DELF(I,J)=DELFS(I,J)
    DELFT(J,I)=DELF(I,J)
    GC TO 410
    400 DELF(I,J)=0.0
    DELFT(J,I)=0.0
    410 CONTINUE

```

```

CALL MXMULT(DELFT,P,TEMP2,KX1,KX1,KX1,M,N,L4,L4,L4,L4)
DO 420 I=1,KX1
DO 420 J=1,KX1
420 RHS(I,J)=DELQ(I,J)+TEMP2(I,J)+TEMP2(J,I)
C
C
C
      RHS MATRIX PARTITION
DO 431 I=1,KX
DO 431 J=1,KX
431 C(I,J)=RHS(I,J)
CALL MUSOLV(KX,KX,KX,KX,JB1,JB2)
DO 432 I=1,KX
DO 432 J=1,KX
432 DELP(I,J)=XSOLN(I,J)
DO 433 I=1,KX
433 RH12(I,1)=-RHS(I,KX1)
DO 445 I=1,KX
DELP(I,KX1)=0.0D+00
DO 444 J=1,KX
444 DELP(I,KX1)=DELP(I,KX1)+FINV(I,J)*RH12(J,1)
445 DELP(KX1,I)=DELP(I,KX1)
DELP(KX1,KX1)=-RHS(KX1,KX1)/(2.0*FMCD(1,1))
C
C
C
      EVALUATE DELGS MATRIX
CALL MXMULT(HK,T1,TEMP3,KB,KB,KB,KC,M,N,L1,L1,L1,L2)
CALL MXMULT(SYSP1,TEMP3,DELGS,KX,KB,KB,KC,M,N,L1,L1,L1,L2)
C
C
C
      EVALUATE AUGMENTED DELG MATRIX
DO 450 I=1,KX1
DO 450 J=1,KC
IF(I.GT.KX)GO TO 440
DELG(I,J)=DELGS(I,J)
GO TO 450
440 DELG(I,J)=0.0D+00

```

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MAIN0289
MAIN0290
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MAIN0302
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MAIN0320
MAIN0321
MAIN0322
MAIN0323
MAIN0324

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```

C      450 CONTINUE
C      EVALUATE DELX
C
C      DO 460 I=1,KX1
C      DELX(I)=0.0D+00
C      DO 460 J=1,KC
C      460 DELX(I)=DELG(I,J)*VCOMM(J)
C
C      EVALUATE DELJ
C
C      DELJ=0.0D+00
C      DO 490 I=1,KX1
C      SUM=0.0D+00
C      SUM1=0.0D+00
C      DO 490 J=1,KX1
C      SUM=SUM+DELP(I,J)*XG(J)
C      SUM1=SUM1+P(I,J)*XG(J)
C      480 SUM1=SUM1+SUM*XG(I)+2.0*SUM1*DELX(I)
C      490 DELJ=DELJ+SUM*XG(I)+2.0*SUM1*DELX(I)
C      WRITE(6,511)DELJ
C      PARAM(K)=PARAM(K)
C      DELK(K)=-STEP*DELJ
C      PARAM(K)=PARAM(K)+DELK(K)
C      PAR(K)=PARAM(K)
C      WRITE(6,511)PARAM(K)
C      DELTAJ=DELTAJ+DELJ*DELK(K)
C      500 WRITE(6,511)DELTAJ
C      511 FORMAT(5X,D10.4)
C      ITER=ITER+1
C      IF(DABS(DELTAJ).LE.1.0D-05.CR.ITER.EQ.15)GO TO 510
C      GO TO 5
C      510 ISTOP=1
C      GO TO 5
C      520 WRITE(6,530)
C      530 FORMAT('0',5X,'THE ADJUSTED PARAMETER VALUES ARE')
C      DO 540 K=1,IGAIN

```

```

540 WRITE(6,550)K,PAR(K)
550 FORMAT(20X,'K(',I1,')=',D12.4)
    WRITE(6,560)
560 FORMAT('0',5X,'THE SYSTEM DIFFERENTIAL TRANSITION MATRIX IS')
    DO 570 I=1,KX
570 WRITE(6,580)(SYSF(I,J),J=1,KX)
580 FORMAT(2X,10D12.4)
    WRITE(6,590)
590 FORMAT('0',5X,'THE SYSTEM CONTROL MATRIX IS')
    DO 600 I=1,KX
600 WRITE(6,610)(SYSG(I,J),J=1,KC)
610 FORMAT(10X,10D12.4)
    WRITE(6,620)ITITER
620 FORMAT('0',THE NUMBER OF ITERATIONS=',I3)
    GO TO 1000
800 ITITER1=ITITER1+1
    IF(ITITER1.GE.2)GO TO 520
    DO 810 K=1,IGAIN
    DELK(K)=DELK(K)/2.0
810 PARAM(K)=PARAM(K)+DELK(K)
    GO TO 5
1000 STOP
    END

```

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MAIN0361
MAIN0362
MAIN0363
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MAIN0370
MAIN0371
MAIN0372
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MAIN0375
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MAIN0379
MAIN0380
MAIN0381
MAIN0382
MAIN0383

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```

C
C
C
C
SUBROUTINE MSOLVE(MA1,MB1,MC1,NC1,A,MXB,C,JB1,JB2)
      SUBROUTINE LINK SEQUENCE FOR SOLUTION OF MATRIX EQUATION
      AX+XB=-C
      REAL*8 MXB(20,20),MXV(20,20),MXA0(20,20),MXA1(20,20),MXA2(20,20),
      1MXVIN(20,20)
      DIMENSION PB(5,21),QB(5,21),ARRAYA(21),IDIMQB(5),IDIMPB(5),
      1QINV(5,21),IDIMQI(5),IDENT(5),QIN(21),ARRAYB(21),A(20,20),C(20,20),
      2DMA(20,20),DMB(20,20),DMC(20,20),DMU(20,20),DMV(20,20),
      3DVINV(20,20),X(20,20)
      DOUBLE PRECISION ARRAYA,QB,PB,ARRAYB,QIN,QINV,DMA,DMB,DMC,DMU,
      1DMV,DVIN,CCNST,X,A,C
      COMMON /HOLD/DMU,DMV/HOLD1/DMA,DMC/HOLD2/QINV,IDIMQI/
      1HOLD3/QB,PB,IDIMQB,IDIMPB,IDENT/HOLD4/DVINV,DMB/SECTR1/X
      DO 50 I=1,MB1
      DO 50 J=1,MB1
      50 DMB(I,J)=MXB(I,J)
      DO 60 I=1,MA1
      DO 60 J=1,MA1
      60 DMA(I,J)=A(I,J)
      DO 70 I=1,MC1
      DO 70 J=1,NC1
      70 DMC(I,J)=C(I,J)
      DO 80 I=1,MA1
      DO 80 J=1,MA1
      80 MXA0(I,J)=-A(I,J)
      CALL SMLTRN(MXB,MXV,MXVIN,MB1,INDXB)
      DO 90 I=1,MB1
      DO 90 J=1,MB1
      90 DMV(I,J)=MXV(I,J)
      DO 90 I=1,MB1
      DO 90 J=1,MB1
      90 DVINV(I,J)=MXVIN(I,J)
      CALL SCAN2(MXB,MB1,JB1,JB2)
      CALL SMLTRN(MXA0,MXV,MXVIN,MA1,INDXA)
      CALL SCAN1(MXA0,ARRAYA,IDIMA,MA1)
      DO 300 LL1=1,JB1

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MSLV0001
MSLV0002
MSLV0003
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MSLV0005
MSLV0006
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MSLV0012
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MSLV0014
MSLV0015
MSLV0016
MSLV0017
MSLV0018
MSLV0019
MSLV0020
MSLV0021
MSLV0022
MSLV0023
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MSLV0026
MSLV0027
MSLV0028
MSLV0029
MSLV0030
MSLV0031
MSLV0032
MSLV0033
MSLV0034
MSLV0035
MSLV0036

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```

IDIMB=ICIMQB(LL1)
DC 100 LL2=1,IDIMB
100 ARRAYB(LL2)=QB(LL1,LL2)
CALL MPINV(QIN,IDM,ARRAYA,ICIMA,ARRAYB,IDIMB,CONST,IER)
IF(DABS(CONST).LE.1.0E-06)GO TO 350
DC 200 LL3=1,IDM
200 QINV(LL1,LL3)=QIN(LL3)
300 IDIMQI(LL1)=IDM
CALL MUSOLV(MB1,MA1,MC1,NC1,JB1,JB2)
GO TO 400
350 WRITE(6,351)
351 FORMAT('MATRICES HAVE COMMON EIGENVALUES')
400 RETURN
END

```

```

MSLV0037
MSLV0038
MSLV0039
MSLV0040
MSLV0041
MSLV0042
MSLV0043
MSLV0044
MSLV0045
MSLV0046
MSLV0047
MSLV0048
MSLV0049
MSLV0050

```



```

C      INDEX J2 INDICATES COLUMN OF MTXSIM
10    J2=J+1
C      SEARCH IN COLUMN J OF MATRXB FOR NCN ZERO ELEMENT
C      IF PIVOT ELEMENT OF MATRXB IS NCN ZERO, DISCONTINUE SEARCH
C      PROCEED TO CONSTRUCT MTXSIM, INVSIM
C      OTHERWISE SEARCH IN REMAINING ROWS FOR FIRST NON ZERO ELEMENT
C
      IF(CABS(MATRXB(J2,J)).GT.1.0D-06)GO TO 1000
      MATRXB(J2,J)=0.0D+00
      J3=J2+1
      IF(J3.EQ.(N+1))GO TO 4500
100   DO 200 I=J3,N
      IF(CABS(MATRXB(I,J)).GT.1.0D-06)GO TO 300
      MATRXB(I,J)=0.0D+00
200   CONTINUE
      J=J+1
      IF(J.EQ.N)GO TO 4500
      INDEX=INDEX+1
      GO TO 10
C
C      INTERCHANGE ROWS I AND J2 AND COLUMNS I AND J2
C
300   DO 400 J4=J,N
      ROW(J4)=MATRXB(J2,J4)
      MATRXB(J2,J4)=MATRXB(I,J4)
400   MATRXB(I,J4)=ROW(J4)
      DO 500 I1=1,N
      COLUMN(I1)=MATRXB(I1,J2)
      MATRXB(I1,J2)=MATRXB(I1,I)
500   MATRXB(I1,I)=COLUMN(I1)
C
C      CCNSTRUCT MATRIX MTX
C
      MTX(J2,J2)=0.
      MTX(I,I)=0.
      MTX(J2,I)=1.

```

SMLT0037
 SMLT0038
 SMLT0039
 SMLT0040
 SMLT0041
 SMLT0042
 SMLT0043
 SMLT0044
 SMLT0045
 SMLT0046
 SMLT0047
 SMLT0048
 SMLT0049
 SMLT0050
 SMLT0051
 SMLT0052
 SMLT0053
 SMLT0054
 SMLT0055
 SMLT0056
 SMLT0057
 SMLT0058
 SMLT0059
 SMLT0060
 SMLT0061
 SMLT0062
 SMLT0063
 SMLT0064
 SMLT0065
 SMLT0066
 SMLT0067
 SMLT0068
 SMLT0069
 SMLT0070
 SMLT0071
 SMLT0072

```

C
C
C
1000 PIVOT=MATRXB(J2,J)
DO 1100 I2=1,N
IF(I2.EQ.J2)GO TO 1050
INVSIM(I2,J2)=-MATRXB(I2,J)/PIVOT
GO TO 1100
1050 INVSIM(I2,I2)=1./PIVOT
1100 MTXSIM(I2,J2)=MATRXB(I2,J)
C      COMPUTE AUXILIARY MATRIX VECAX AND RECURSIVE MATRXB
C      CALL DMPROD(INVSIM,MATRXB,AUX,N,N,N,N,N1,N1)
C      COMPUTE RECURSIVE MATRXB
C      CALL DMPROD(AUX,MTXSIM,MATRXB,N,N,N,N,N1,N1)
C      COMPUTE RECURSIVE MATRICES: MATRXV, MTRXIN
C      CALL DMPROD(MATRXV,MTXSIM,V1,N,N,N,N,N1,N1)
C      CALL DMCOPY(V1,MATRXV,N,N,N1,N1)
C      CALL DMPROD(INVSIM,MTRXIN,VI,N,N,N,N,N1,N1)
C      CALL DMCOPY(VI,MTRXIN,N,N,N1,N1)
J=J+1
C      CHECK TO DETERMINE NEW BASIS VECTORS HAVE BEEN ESTABLISHED
IF(J.EQ.N)GO TO 4500
C      RECONVERT MTXSIM AND INVSIM TO IDENTITY MATRICES
CALL DMCOPY(MUNIT,MTXSIM,N,N,N1,N1)
CALL DMCOPY(MUNIT,INVSIM,N,N,N1,N1)
C      RETURN TO START OF PROCEDURE
GO TO 10
4500 RETURN
END
SMLT0073
SMLT0074
SMLT0075
SMLT0076
SMLT0077
SMLT0078
SMLT0079
SMLT0080
SMLT0081
SMLT0082
SMLT0083
SMLT0084
SMLT0085
SMLT0086
SMLT0087
SMLT0088
SMLT0089
SMLT0090
SMLT0091
SMLT0092
SMLT0093
SMLT0094
SMLT0095
SMLT0096
SMLT0097
SMLT0098
SMLT0099
SMLT0100
SMLT0101
SMLT0102
SMLT0103
SMLT0104
SMLT0105
SMLT0106
SMLT0107

```



```

      ID=IDENT(1)
      DO 2000 I1=1, ID
2000  ARRAYQ(1, I1)=-MATRXA(I1, ID)
      IDIM1=IDIMNQ(1)
      DO 2500 J3=1, IDIM1
2500  ARRAY1(J3)=ARRAYQ(1, J3)
      IF(J1.EQ.1) GO TO 4000
      DO 3000 K2=2, J1
      IDIMNQ(K2)=IDENT(K2)-IDENT(K2-1)+1
      INDEX=IDIMNQ(K2)-1
      ARRAYQ(K2, IDIMNQ(K2))=1.
      DO 3000 K3=1, INDEX
      K4=IDENT(K2-1)+K3
      K5=IDENT(K2)
      ARRAYQ(K2, K3)=-MATRXA(K4, K5)
3000  CONTINUE
      DO 3500 K2=2, J1
      IDIM2=IDIMNQ(K2)
      DO 3400 J3=1, IDIM2
3400  ARRAY2(J3)=ARRAYQ(K2, J3)
      CALL MPMPY(ARRAY, IDIM, ARRAY1, IDIM1, ARRAY2, IDIM2)
      CALL MPMOVE(ARRAY1, IDIM1, ARRAY, IDIM)
3500  CONTINUE
4000  RETURN
      END

```

```

SCN10037
SCN10038
SCN10039
SCN10040
SCN10041
SCN10042
SCN10043
SCN10044
SCN10045
SCN10046
SCN10047
SCN10048
SCN10049
SCN10050
SCN10051
SCN10052
SCN10053
SCN10054
SCN10055
SCN10056
SCN10057
SCN10058
SCN10059
SCN10060
SCN10061

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SCN20001
 SCN20002
 SCN20003
 SCN20004
 SCN20005
 SCN20006
 SCN20007
 SCN20008
 SCN20009
 SCN20010
 SCN20011
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 SCN20031
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 SCN20034
 SCN20035
 SCN20036

```

SUBROUTINE SCAN2(MATRXB,MN,J1,J2)
C
C      THIS SUBROUTINE IDENTIFIES AND HOLDS THE P & Q ARRAYS
C      FOR SUBSEQUENT MATRIX POLYNOMIAL INVERSION
C
      DIMENSION ARRAYP(5,21),ARRAYQ(5,21),IDIMNP(5),IDIMNQ(5),IDENT(5)
      REAL*8 MATRXB(20,20)
      DOUBLE PRECISION ARRAYP,ARRAYQ
      COMMON /HJLD3/ARRAYQ,ARRAYP,IDIMNC,IDIMNP,IDENT
C
      INITIALIZE ARPAYP,ARRAYQ
C
      DO 20 I=1,5
      DO 20 J=1,21
      ARRAYP(I,J)=0.
      20 ARRAYQ(I,J)=0.
C
      FOLLOWING SEQUENCE IDENTIFIES AND STORES RELEVANT ARRAYS
C
      J1=0
      DO 1000 K1=2,MN
      L1=K1-1
      IF(K1.EQ.MN) GO TO 500
      IF(CABS(MATRXB(K1,L1)-1.0).LE.1.0D-04)GO TO 1000
      J1=J1+1
      IDENT(J1)=K1-1
      GO TO 1000
      500 J1=J1+1
      IDENT(J1)=K1
      IF(CABS(MATRXB(K1,L1)-1.0).GE.1.0D-04)GO TO 750
      GO TO 1000
      750 J1=J1+1
      IDENT(J1)=K1
      IDENT(J1-1)=K1-1
      1000 CONTINUE
      IDIMNQ(1)=IDENT(1)+1

```

SCN20037
SCN20038
SCN20039
SCN20040
SCN20041
SCN20042
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SCN20044
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SCN20063
SCN20064
SCN20065
SCN20066

```

      ARRAYQ(1,IDIMNQ(1))=1.
      IC=IDENT(1)
      DO 2000 I1=1,ID
2000  ARRAYQ(1,I1)=-MATRXB(I1,ID)
      IF(J1.EQ.1)GO TO 6000
      IDIMNP(1)=IDIMNQ(1)
      IC1=IDENT(2)
      DO 3000 K2=2,J1
      IDIMNQ(K2)=IDENT(K2)-IDENT(K2-1)+1
      INDEX=ICIMNQ(K2)-1
      ARRAYQ(K2,IDIMNQ(K2))=1.
      DO 3000 K3=1,INDEX
      K4=IDENT(K2-1)+K3
      K5=IDENT(K2)
3000  ARRAYQ(K2,K3)=-MATRXB(K4,K5)
      DO 4000 I2=1,ID
4000  ARRAYP(1,I2)=MATRXB(I2,ID1)
      J2=J1-1
      IF(J2.EQ.1)GO TO 7000
      DO 5000 K6=2,J2
      IDIMNP(K6)=IDIMNP(K6-1)+IDIMNQ(K6)-1
      INDEX1=IDIMNP(K6)-1
      K8=IDENT(K6+1)
      DO 5000 K7=1,INDEX1
5000  ARRAYP(K6,K7)=MATRXB(K7,K8)
      GO TO 7000
6000  J2=0
      ICQ=IDIMNQ(1)
7000  RETURN
      END

```

```

C
C
C
C
SUBROUTINE MPINV(QINV, IDIMQ1, ARRAYA, IDIMA, ARRAYB, IDIMB, CONST, IER)
C
C      MATRIX POLYNOMIAL INVERSION SCHEME BASED ON THE
C      EUCLIDIAN ALGORITHM
C
      DIMENSION ARRAYA(20), ARRAYB(20), ARRAY1(20), ARAYB1(20), AUXIL(20),
1 ARRAYR(20), ARAYP1(20), ARAYP2(20), ARAYP3(20), QINV(20), Q1(20),
2 Q3(20), ARAYR1(20), ARAYP4(20), Q2(20), ARAYQ1(20), ARAYQ2(20),
3 ARAYQ3(20), ARAYQ4(20)
      DOUBLE PRECISION ARRAYA, ARRAYB, ARRAY1, ARAYB1, ARAYP4, ARRAYR, AUXIL,
1 ARAYP1, ARAYP2, ARAYP3, ARAYQ1, ARAYQ2, ARAYQ3, QINV, CONST, Q1, Q2, Q3,
2 ARAYR1, ARAYQ4
C
C      INITIALIZE ALL ARRAY HOLDS
C
      DO 10 I=1, 20
        ARAY1(I)=0.
        ARAYB1(I)=0.
        ARRAYR(I)=0.
        ARAYP1(I)=0.
        ARAYP2(I)=0.
        ARAYP3(I)=0.
10      ARAYP4(I)=0.
        IDIMP1=1
        ARAYP1(I)=1.
C
C      CHECK DEGREES OF POLYNOMIALS
C
        IF(IDIMB.LT.IDIMA)GO TO 110
        CALL MPMOVE(ARAY1, IDIM1, ARRAYA, IDIMA)
        CALL MPMOVE(ARAYB1, IDIMB1, ARRAYB, IDIMB)
        CALL MPDIV(Q1, IDIMQ1, ARAYB1, IDIMB1, ARAY1, IDIM1, IER)
        IF(IER.EQ.1)GO TO 200
        ICCUNT=1
        CALL MPMOVE(ARRAYR, IDIMR, ARAYB1, IDIMB1)
        IF(ICIMB1.EQ.1)GO TO 70
        ICCUNT=ICCUNT+1

```

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MPNV0001
MPNV0002
MPNV0003
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MPNV0030
MPNV0031
MPNV0032
MPNV0033
MPNV0034
MPNV0035
MPNV0036

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```

CALL MPDIV(Q2,IDIMQ2,ARAY1,IDIM1,ARRAYR,IDIMR,IER)
IF(IER.EQ.1)GO TO 200
IDIMP2=IDIMQ2
DO 55 J=1,IDIMP2
  ARAY2(J)=-Q2(J)
  IF(ICIM1.EQ.1)GO TO 80
  CALL MPMOVE(ARAY1,IDIMR1,ARAY1,ICIM1)
  ICOUNT=ICOUNT+1
  CALL MPDIV(Q3,IDIMQ3,ARRAYR,IDIMR,ARAY1,IDIMR1,IER)
  IF(IER.EQ.1)GO TO 200
  CALL MPMY(ARAY4,IDIMP4,Q3,IDIMQ3,ARAY2,IDIMP2)
  CALL MPSUB(ARAY3,IDIMP3,ARAY1,IDIMP1,ARAY4,IDIMP4)
  IF(IDIMR.EQ.1)GO TO 100
  CALL MPMOVE(ARAY1,IDIMP1,ARAY2,IDIMP2)
  CALL MPMOVE(ARAY2,IDIMP2,ARAY3,IDIMP3)
  CALL MPMOVE(AUXIL,IDIMU,ARRAYR,IDIMR)
  CALL MPMOVE(ARRAYR,IDIMR,ARAY1,IDIMR1)
  CALL MPMOVE(ARAY1,IDIMR1,AUXIL,IDIMU)
GO TO 60
C REMAINDER POLYNOMIAL IS CONSTANT
70 CONST=ARAY1(1)
IF(CABS(CONST).LE.1.0E-06)GO TO 200
QINV(1)=1./CONST
IDIMQ1=1
GO TO 200
80 CONST=ARAY1(1)
IF(CABS(CONST).LE.1.0E-06)GO TO 200
DO 90 I1=1,IDIMP2
  QINV(I1)=ARAY2(I1)/CONST
  IDIMQ1=IDIMP2
GO TO 200
100 CONST=ARRAYR(1)
IF(CABS(CONST).LE.1.0E-06)GO TO 200
DO 95 I2=1,IDIMP3
  QINV(I2)=ARAY3(I2)/CONST
  IDIMQ1=IDIMP3

```

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MPNV0037
MPNV0038
MPNV0039
MPNV0040
MPNV0041
MPNV0042
MPNV0043
MPNV0044
MPNV0045
MPNV0046
MPNV0047
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MPNV0049
MPNV0050
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MPNV0061
MPNV0062
MPNV0063
MPNV0064
MPNV0065
MPNV0066
MPNV0067
MPNV0068
MPNV0069
MPNV0070
MPNV0071
MPNV0072

```

```

C
GO TO 200
INITIALIZE ARRAYS
110 DO 215 I=1,20
  ARRAY1(I)=0.
  ARRAYB1(I)=0.
  ARRAYR(I)=0.
  ARRAYQ1(I)=0.
  ARRAYQ2(I)=0.
  ARRAYQ3(I)=0.
115 ARRAYQ3(I)=0.
  CALL MPMOVE(ARRAY1, IDIM1, ARRAYB, ICIMB)
  CALL MPMOVE(ARRAYB1, IDIMB1, ARRAYA, ICIMA)
  CALL MPDIV(C1, IDIMQ1, ARRAYB1, IDIMB1, ARRAY1, IDIM1, IER)
  IF(IDIMB1.EQ.1)GO TO 120
  DO 116 J=1, IDIMQ1
    116 ARRAYQ1(J)=-Q1(J)
    IDQ1=IDIMQ1
    CALL MPDIV(Q2, IDIMQ2, ARRAY1, IDIM1, ARRAYB1, IDIMB1, IER)
    CALL MPMPY(ARRAYQ2, IDQ2, Q2, IDIMQ2, C1, IDIMQ1)
    ARRAYQ2(1)=ARRAYQ2(1)+1.
    IF(IDIM1.EQ.1)GO TO 130
    CALL MPMOVE(ARRAYR, IDIMR, ARRAYB1, IDIMB1)
    CALL MPMOVE(ARRAYR1, IDIMR1, ARRAY1, ICIMA1)
117 CALL MPDIV(Q3, IDIMQ3, ARRAYR, IDIMR, ARRAYR1, IDIMR1, IER)
    CALL MPMPY(ARRAYQ4, IDQ4, Q3, IDIMQ3, ARRAYQ2, IDQ2)
    CALL MPMPY(ARRAYQ3, IDQ3, ARRAYQ1, IDQ1, ARRAYQ4, IDQ4)
    CALL MPMPY(AUX1L, IDIMU, ARRAYC3, IDQ3, ARRAYB, IDIMB)
    IF(IDIMR.EQ.1)GO TO 140
    CALL MPMOVE(ARRAYQ1, IDQ1, ARRAYQ2, IDQ2)
    CALL MPMOVE(ARRAYQ2, IDQ2, ARRAYQ3, IDQ3)
    CALL MPMOVE(AUX1L, IDIMU, ARRAYR, IDIMR)
    CALL MPMOVE(ARRAYK, IDIMR, ARRAYR1, IDIMR1)
    CALL MPMOVE(ARRAYR1, IDIMR1, AUX1L, IDIMU)
    GO TO 117
120 CONST=ARRAYB1(1)
  IF(DABS(CONST).LE.1.0E-06)GO TO 200
  IDIMQ1=IDIMQ1

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MPNV0073
MPNV0074
MPNV0075
MPNV0076
MPNV0077
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MPNV0080
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MPNV0096
MPNV0097
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MPNV0099
MPNV0100
MPNV0101
MPNV0102
MPNV0103
MPNV0104
MPNV0105
MPNV0106
MPNV0107
MPNV0108

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```

      DO 125 J=1, IDIMQ1
125  QINV(J)=-01(J)/CONST
      GO TO 200
130  CCNST=ARRAYA1(1)
      IF (CABS(CONST)).LE.1.0E-06)GO TO 200
      IDIMQ1=IDQ2
      DO 135 J=1, IDIMQ1
135  QINV(J)=ARRAYQ2(J)/CONST
      GO TO 200
140  CCNST=ARRAYR(1)
      IF (CABS(CONST)).LE.1.0E-06)GO TO 200
      IDIMQ1=IDQ3
      DO 145 J=1, IDIMQ1
145  QINV(J)=ARRAYQ3(J)/CCNST
200  RETURN
      END

```

```

MPNV0109
MPNV0110
MPNV0111
MPNV0112
MPNV0113
MPNV0114
MPNV0115
MPNV0116
MPNV0117
MPNV0118
MPNV0119
MPNV0120
MPNV0121
MPNV0122
MPNV0123
MPNV0124

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```

SUBROUTINE MUSOLV(MB1,MA1,MC1,NC1,MB1,JB1,JB2)
  DIMENSION V1(20,20),V2(20),VSUM(20),V3(20),U(20,20),C(20,20),
  1A(20,20),U1(20),IDIMQ1(5),QINV(5,21),V(20,20),QB(5,21),PB(5,21),
  2IDENT(5),IDIMQB(5),IDIMPB(5),E(20,20),VINV(20,20),Y(20,20),
  3R(20,20),AX(20,20),XB(20,20),AXXB(20,20),X(20,20)
  DOUBLE PRECISION U,V1,V2,V3,VSUM,A,U1,QINV,PB,QB,V,VINV,AX,XB,R,E,
  1Y,AXXB,X,C
  COMMON /HOLD/U,V/HOLD1/A,C/HOLD2/CINV,IDIMQ1
  1/HCLD3/QB,PE,IDIMQB,IDIMPB,IDENT/HCLD4/VINV,B/SECTR1/X
  ICOUNT=0
  JWRITE=0
  V1=C*V
  CALL DMULT(C,V,V1,MC1,NC1,MB1,MM,NN)
  INITIALIZE VSUM
  5 DO 10 I1=1,MA1
  10 VSUM(I1)=0.
  FIRST PASS SOLVE FOR U1,U2,.....UIDENT(1)
  I11=IDENT(1)
  I15=I11+1
  DO 40 I12=1,I11
  DO 20 I13=1,MA1
  20 V2(I13)=V1(I13,I12)
  I14=I12+1
  30 DO 35 I13=1,MA1
  35 VSUM(I13)=VSUM(I13)+QB(1,I14)*V2(I13)
  I14=I14+1
  IF(I14.GT.I15)GO TO 40
  V2(I13)=(-A)*V2(I13)
  CALL AVMULT(A,MA1,V2)
  GC TO 30
  40 CONTINUE
  C
  U1(L1)=(-A)*U(L1,L2-1)
  DO 41 L1=1,MA1
  41 U(L1,1)=QINV(L1,1)*VSUM(L1)
  INDXQ1=IDIMQ1(1)
  DO 43 L2=2,INDXQ1

```

```

USLV0001
USLV0002
USLV0003
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USLV0029
USLV0030
USLV0031
USLV0032
USLV0033
USLV0034
USLV0035
USLV0036

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```

      CALL AVMULT(A,MA1,VSUM)
      DO 42 L1=1,MA1
42  U(L1,1)=U(L1,1)+QINV(1,L2)*VSUM(L1)
43  CONTINUE
      DO 70 L2=2,II1
      DO 60 L1=1,MA1
60  U(L1)=U(L1,L2-1)
      CALL AVMULT(A,MA1,U1)
      DO 65 L1=1,MA1
65  U(L1,L2)=U1(L2)-V1(L1,L2-1)
70  CONTINUE
      IF(JB1.EQ.1.AND.ICOUNT.EQ.0)GO TO 300
      IF(JB1.EQ.1.AND.ICOUNT.GT.0)GO TO 400
      SOLVE FOR REMAINING VECTORS OF U
      DO 200 JJ=2,JB1
      JJ0=JJ-1
      JJ2=IDENT(JJ)
      JJ1=IDENT(JJ-1)+1
      RE INITIALIZE VSUM
      DO 80 JJ3=1,MA1
80  VSUM(JJ3)=0.
      JJ4=IDENT(JJ-1)
      DO 90 JJ5=1,JJ4
      DO 90 JJ3=1,MA1
      V3(JJ3)=PB(JJ0,JJ5)*U(JJ3,JJ5)
90  VSUM(JJ3)=VSUM(JJ3)+V3(JJ3)
      JJ6=0
      DO 130 JJ7=JJ1,JJ2
      JJ6=JJ6+1
      DO 100 JJ3=1,MA1
100  V2(JJ3)=V1(JJ3,JJ7)
      JJ8=JJ6+1
110  DO 120 JJ3=1,MA1
120  VSUM(JJ3)=VSUM(JJ3)+QB(JJ,JJ8)*V2(JJ3)
      JJ8=JJ8+1
      IF(JJ8.GT.(JJ2-JJ1+2))GO TO 130

```

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USLV0037
USLV0038
USLV0039
USLV0040
USLV0041
USLV0042
USLV0043
USLV0044
USLV0045
USLV0046
USLV0047
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USLV0049
USLV0050
USLV0051
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USLV0053
USLV0054
USLV0055
USLV0056
USLV0057
USLV0058
USLV0059
USLV0060
USLV0061
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USLV0063
USLV0064
USLV0065
USLV0066
USLV0067
USLV0068
USLV0069
USLV0070
USLV0071
USLV0072

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```

C      V2(JJ3)=(-A)*V2(JJ3)
      CALL AVMULT(A,MA1,V2)
      GO TO 110
130 CONTINUE
C      SOLVE FOR U(JJ1)
      DO 140 L1=1,MA1
140 U(L1,JJ1)=QINV(JJ,1)*VSUM(L1)
      INDXQI=IDIMQI(JJ)
      DO 160 L2=2,INDXQI
      CALL AVMULT(A,MA1,VSUM)
      DO 150 L1=1,MA1
150 U(L1,JJ1)=U(L1,JJ1)+QINV(JJ,L2)*VSUM(L1)
160 CONTINUE
      IF(JJ1.EQ.JJ2)GO TO 200
      JJ9=JJ1+1
      DO 190 L2=JJ9,JJ2
      DO 170 L1=1,MA1
170 U1(L1)=U(L1,L2-1)
      CALL AVMULT(A,MA1,U1)
      DO 180 L1=1,MA1
180 U(L1,L2)=U1(L1)-V1(L1,L2-1)
190 CONTINUE
200 CONTINUE
      IF(ICOUNT.GT.0)GO TO 400
300 CALL DMULT(U,VINV,X,MA1,MB1,MB1,MM,NN)
      CALL DMULT(A,X,AX,MA1,MA1,MA1,MB1,MM,NN)
      CALL DMULT(X,B,XB,MA1,MA1,MB1,MB1,MM,NN)
      DO 340 I=1,MA1
      DO 340 J=1,MB1
340 AXB(I,J)=AX(I,J)+XB(I,J)
      DO 350 I=1,MA1
      DO 350 J=1,MB1
350 E(I,J)=AXB(I,J)+C(I,J)
      DO 330 I=1,MA1
330 WRITE(6,600)(E(I,J),J=1,MB1)
      ICCUNT=ICOUNT+1

```

```

CALL DMULT(E,V,V1,MAL,MB1,M21,MB1,MM,NN)
GO TO 5
400 CALL DMULT(U,VINV,Y,MAL,MB1,MB1,MB1,MM,NN)
CALL DMULT(A,Y,AX,MAL,MAL,MAL,MB1,MM,NN)
CALL DMULT(Y,B,XB,MAL,MB1,MB1,MB1,MM,NN)
DO 450 I=1,MAL
DO 450 J=1,MB1
X(I,J)=X(I,J)+Y(I,J)
AXXB(I,J)=AX(I,J)+XB(I,J)
450 E(I,J)=AXXB(I,J)+E(I,J)
IF(ICOUNT.EQ.2)GO TO 500
ICOUNT=ICOUNT+1
CALL DMULT(E,V,V1,MAL,MB1,MB1,MM,NN)
GO TO 5
500 JWRITE=JWRITE+1
IF(JWRITE.EQ.2)GO TO 700
WRITE(6,550)
550 FORMAT(5X,'THE SOLUTION MATRIX X IS')
DO 560 I=1,MAL
560 WRITE(6,600)(X(I,J),J=1,MB1)
WRITE(6,650)
650 FORMAT(5X,'THE ERROR MATRIX EMATRIX=AX+XB+C IS')
DO 670 I=1,MAL
670 WRITE(6,600)(E(I,J),J=1,MB1)
600 FORMAT(10D15.5)
700 RETURN
END
USLV0109
USLV0110
USLV0111
USLV0112
USLV0113
USLV0114
USLV0115
USLV0116
USLV0117
USLV0118
USLV0119
USLV0120
USLV0121
USLV0122
USLV0123
USLV0124
USLV0125
USLV0126
USLV0127
USLV0128
USLV0129
USLV0130
USLV0131
USLV0132
USLV0133
USLV0134
USLV0135

```

```

SUBROUTINE AVMULT(AA,MAA,V4)
DIMENSION AA(20,20),V4(20),V5(20)
DOUBLE PRECISION AA,V4,V5,SSUM
DO 50 I=1,MAA
SSUM=0.
DO 45 J=1,MAA
45 SSUM=SSUM+(-AA(I,J))*V4(J)
50 V5(I)=SSUM
DO 55 K=1,MAA
55 V4(K)=V5(K)
RETURN
END

```

```

AVMT0001
AVMT0002
AVMT0003
AVMT0004
AVMT0005
AVMT0006
AVMT0007
AVMT0008
AVMT0009
AVMT0010
AVMT0011
AVMT0012

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```

C      SUBROUTINE RSCHEK(ARRAY,IDIM,ROUTH1,IDIMR1,ROUTH2,IDIMR2,ICODE)
C
C      THIS SUBROUTINE CHECKS FOR SYSTEM ASYMPTOTIC
C      STABILITY USING THE ROUTH CRITERION
C
C      CONDITION CODES
C      1)ICODE=0 INDICATES ASYMPTOTIC STABILITY
C      2)ICODE=1 INDICATES ASYMPTOTIC INSTABILITY
C
C      DIMENSION ARRAY(21),ROUTH1(21),ROUTH2(21),Q(21),AUXIL(21)
C      DOUBLE PRECISION ARRAY,ROUTH1,ROUTH2,Q,AUXIL
C      IR=IDIM
C      3 IF(ARRAY(IR).LE.0.0)GO TO 40
C      IR=IR-1
C      IF(IR.EQ.0)GO TO 4
C      GO TO 3
C
C      FORM INITIAL ARRAYS
C
C      4 IDIMR1=IDIM
C      IDIMR2=IDIM-1
C      IR1=IDIMR1
C      IR2=IDIMR2
C      5 IR3=IR1-1
C      IR4=IR2-1
C      ROUTH1(IR1)=ARRAY(IR1)
C      IF(IR1.EQ.1)GO TO 10
C      ROUTH1(IR3)=0.
C      ROUTH2(IR2)=ARRAY(IR2)
C      IF(IR2.EQ.1)GO TO 10
C      ROUTH2(IR4)=0.
C      IR1=IR1-2
C      IR2=IR2-2
C      GO TO 5
C      10 CALL MPDIV(Q,IDIMQ,ROUTH1,IDIMR1,ROUTH2,IDIMR2)

```

```

RSCK0001
RSCK0002
RSCK0003
RSCK0004
RSCK0005
RSCK0006
RSCK0007
RSCK0008
RSCK0009
RSCK0010
RSCK0011
RSCK0012
RSCK0013
RSCK0014
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RSCK0034
RSCK0035
RSCK0036

```

RSCK0037
 RSCK0038
 RSCK0039
 RSCK0040
 RSCK0041
 RSCK0042
 RSCK0043
 RSCK0044
 RSCK0045
 RSCK0046
 RSCK0047
 RSCK0048
 RSCK0049
 RSCK0050
 RSCK0051
 RSCK0052

```

IF(IDIMR1.EQ.1.AND.ROUTH1(1).GT.0.0)GO TO 50
IF(IDIMR1.EQ.1.AND.ROUTH1(1).LE.0.0)GO TO 40
IR5=IDIMR1
20 IF(ROUTH1(IR5).LE.0.0)GO TO 40
IR5=IR5-2
IF(IR5.EQ.0.OR.IR5.EQ.-1)GO TO 30
GO TO 20
30 CALL MPMOVE(AUXIL,IDIMU,ROUTH1,IDIMR1)
CALL MPMOVE(ROUTH1,IDIMR1,ROUTH2,IDIMR2)
CALL MPMOVE(ROUTH2,IDIMR2,AUXIL,IDIMU)
GO TO 10
40 ICODE=1
GO TO 60
50 ICODE=0
60 RETURN
END
  
```

```

SUBROUTINE MPDIV(P, IDIMP, X, IDIMX, Y, IDIMY, IER)
  DIMENSION P(1), X(1), Y(1)
  DOUBLE PRECISION P, X, Y, TOL
  TOL=1.0D-06
  CALL MPNORM(Y, IDIMY, TOL)
  IF (IDIMY) 50, 50, 10
  10 IDIMP=IDIMX-IDIMY+1
    IF (IDIMP) 20, 30, 60
  20 IDIMP=0
  30 IER=0
  40 RETURN
  50 IER=1
    GO TO 40
  60 IDIMX=IDIMY-1
    I=IDIMP
  70 II=I+IDIMX
    P(I)=X(II)/Y(IDIMY)
    DO 80 K=1, IDIMX
      J=K-1+I
      X(J)=X(J)-P(I)*Y(K)
  80 CONTINUE
    I=I-1
    IF (I) 90, 90, 70
  90 CALL MPNORM(X, IDIMX, TOL)
    GO TO 30
  END

```

```

MPDV00001
MPDV00002
MPDV00003
MPDV00004
MPDV00005
MPDV00006
MPDV00007
MPDV00008
MPDV00009
MPDV00010
MPDV00011
MPDV00012
MPDV00013
MPDV00014
MPDV00015
MPDV00016
MPDV00017
MPDV00018
MPDV00019
MPDV00020
MPDV00021
MPDV00022
MPDV00023
MPDV00024
MPDV00025
MPDV00026

```

```

SUBROUTINE MPNORM(X,IDIMX,EPS)
  DIMENSION X(1)
  DOUBLE PRECISION X,EPS
  1 IF(IDIMX)4,4,2
  2 IF(DABS(X(IDIMX))-EPS)3,3,4
  3 IDIMX=IDIMX-1
  GO TO 1
  4 RETURN
  END

```

```

MPNM0001
MPNM0002
MPNM0003
MPNM0004
MPNM0005
MPNM0006
MPNM0007
MPNM0008
MPNM0009

```

```

SUBROUTINE MPMY(Z, IDIMZ, X, IDIMX, Y, IDIMY)
  DIMENSION Z(1), X(1), Y(1)
  DOUBLE PRECISION Z, X, Y
  IF(IDIMX*IDIMY)10,10,20
10 IDIMZ=0
   GO TO 50
20 IDIMZ=IDIMX+IDIMY-1
   DO 30 I=1, IDIMZ
30 Z(I)=0.
     DO 40 I=1, IDIMX
       DO 40 J=1, IDIMY
         K=I+J-1
40 Z(K)=X(I)*Y(J)+Z(K)
50 RETURN
   END

```

```

MPMY0001
MPMY0002
MPMY0003
MPMY0004
MPMY0005
MPMY0006
MPMY0007
MPMY0008
MPMY0009
MPMY0010
MPMY0011
MPMY0012
MPMY0013
MPMY0014
MPMY0015

```

```

SUBROUTINE MPMOVE(Y, IDIMY, X, IDIMX)
  DIMENSION X(1), Y(1)
  DOUBLE PRECISION X, Y
  IDIMY=IDIMX
  IF (IDIMX) 30, 30, 10
  10 DO 20 I=1, IDIMX
    20 Y(I)=X(I)
  30 RETURN
    END

```

```

MPMV0001
MPMV0002
MPMV0003
MPMV0004
MPMV0005
MPMV0006
MPMV0007
MPMV0008
MPMV0009

```

```

SUBROUTINE MPSUB(Z, IDIMZ, X, IDIMX, Y, IDIMY)
  DIMENSION Z(1), X(1), Y(1)
  DOUBLE PRECISION Z, X, Y
  TEST DIMENSIONS OF SUMMANDS
  NDIM=IDIMX
  IF(IDIMX-IDIMY)10,20,20
10 NDIM=IDIMY
20 IF(NDIM)90,50,30
30 DO 90 I=1,NDIM
  IF(I-IDIMX)40,40,60
40 IF(I-IDIMY)50,50,70
50 Z(I)=X(I)-Y(I)
  GO TO 80
60 Z(I)=-Y(I)
  GO TO 80
70 Z(I)=X(I)
80 CONTINUE
90 IDIMZ=NDIM
  RETURN
  END

```

C

MPSB0001
 MPSB0002
 MPSB0003
 MPSB0004
 MPSB0005
 MPSB0006
 MPSB0007
 MPSB0008
 MPSB0009
 MPSB0010
 MPSB0011
 MPSB0012
 MPSB0013
 MPSB0014
 MPSB0015
 MPSB0016
 MPSB0017
 MPSB0018
 MPSB0019
 MPSB0020

```

SUBROUTINE MXMULT(A,B,C,MA,NA,MB,NB,MC,NC,I1,J1,I2,J2)
DOUBLE PRECISION A(I1,J1),B(I2,J2),C(I1,J2)
MC=MA
NC=NB
DO 10 I=1,MA
DO 10 J=1,NB
C(I,J)=0.0D+00
DO 10 K=1,MB
10 C(I,J)=C(I,J)+A(I,K)*B(K,J)
RETURN
END

```

```

MXMT0001
MXMT0002
MXMT0003
MXMT0004
MXMT0005
MXMT0006
MXMT0007
MXMT0008
MXMT0009
MXMT0010
MXMT0011

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