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SONIC-BOOM MEASUREMENTS FOR SR-71 AIRCRAFT OPERATING AT MACH NUMBERS TO 3.0 AND ALTITUDES TO 24 384 METERS

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16. Abstract

Sonic-boom pressure signatures produced by the SR-71 aircraft at altitudes from 10 668 to 24 384 meters and Mach numbers 1.35 to 3.0 were obtained as an adjunct to the Edwards Air Force Base Phase I and II Sonic Boom Evaluation Program relating to structural and subjective response which was conducted in 1966-1967 time period. Approximately 2000 sonic-boom signatures from 33 flights of the SR-71 vehicle and two flights of the F-12 vehicle were recorded. In this report measured ground-pressure signatures for both on-track and lateral measuring station locations are presented and the statistical variations of the overpressure, positive impulse, wave duration, and shock-wave rise time are illustrated.

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SUMMARY

Sonic-boom pressure signatures produced by the SR-71 aircraft at altitudes from 10 668 to about 24 400 meters and Mach numbers of 1.35 to 3.0 were obtained as an adjunct to the Edwards Air Force Base Phase I and II Sonic Boom Evaluation Program relating to structural and subjective response which was conducted in 1966-1967 time period. Approximately 2000 sonic-boom signatures from 33 flights of the SR-71 vehicle and two flights of the F-12 vehicle were recorded. In this report measured ground-pressure signatures for both on-track and lateral measuring station locations are presented and the statistical variations of the overpressure, positive impulse, wave duration, and shock-wave rise time are illustrated. No unusual phenomena, regarding overpressure variation with altitude and lateral distance or the variability of sonic-boom signature waveforms due to atmospheric nonuniformities in the lower layers, were encountered for the high-altitude and high-Mach-number range of these tests. The experimental results fit generally into the established patterns of other available sonic-boom flight data from F-104, B-58, and B-70 aircraft and also correlate very well with current prediction methods utilizing existing theory.

INTRODUCTION

Extensive experimental and theoretical test programs have led to a general understanding of the sonic-boom phenomena associated with supersonic flight. (See, for example, refs. 1 to 5.) Previously reported flight test data (refs. 6 to 10) have covered the altitude range of from about 15 to 22 000 meters and Mach-number range of near 1.0 to 3.0; however, the bulk of the data applies to the moderate and lower ranges of both Mach number and altitude. Results obtained in flight test programs involving the SR-71 aircraft (refs. 3 and 11) serve to expand the matrix of experimental data with particular emphasis on very high Mach numbers and altitudes.

The SR-71 data reported herein cover an altitude range from 10 668 to 24 384 meters and Mach-number range from 1.35 to 3.0. The data, some of which have been presented in reference 3, were obtained as an adjunct to the Edwards Air Force Base Phase I and II Sonic Boom Evaluation Program relating to structural and subjective response which was

conducted in 1966-1967 time period (ref. 10). Approximately 2000 sonic-boom signatures from 33 flights of the SR-71 vehicle and two flights of the F-12 vehicle were recorded.

Representative ground-pressure signature traces for both on-track and lateral measuring-station locations are illustrated and for all signatures measured on-track the statistical variations of the overpressure, positive impulse, wave duration, and shock-wave rise time are tabulated. These data are useful for evaluating the effects of altitude and Mach number on the sonic-boom ground-exposure patterns and for assessing the suitability of available theories regarding generation and the propagation of shock waves at high altitudes.

SYMBOLS

I_o	impulse of positive phase of sonic-boom ground-pressure signature, newton-seconds/meter^2
M	Mach number
Δp_o	maximum pressure rise across bow shock wave measured at ground level, newtons/meter^2
Δt_o	time duration of positive phase of sonic-boom ground-pressure signature, seconds
ΔT	total time duration of sonic-boom ground-pressure signature, seconds
τ	rise time of sonic-boom pressure signature (defined as time from onset of bow shock wave to its positive maximum value of overpressure), seconds
$\tau_{1/2}$	rise time of sonic-boom pressure signature (defined as time from onset of bow shock wave to one-half its positive maximum value of overpressure), seconds

Subscripts:

calc	calculated
meas	measured

APPARATUS AND METHODS

Test Conditions

All of the flight missions of table I (listed in order of increasing flight altitude) were made in the vicinity of Edwards Air Force Base, California. The area in which the measurements were taken has an altitude of from 700 to 1100 meters above sea level and is generally flat with only sparse vegetation. Figure 1 is a schematic diagram showing the test area, arrangement of facilities, deployment of sonic-boom measurement stations, and microphone arrangements. Also shown in the inserts on the figure are details of the

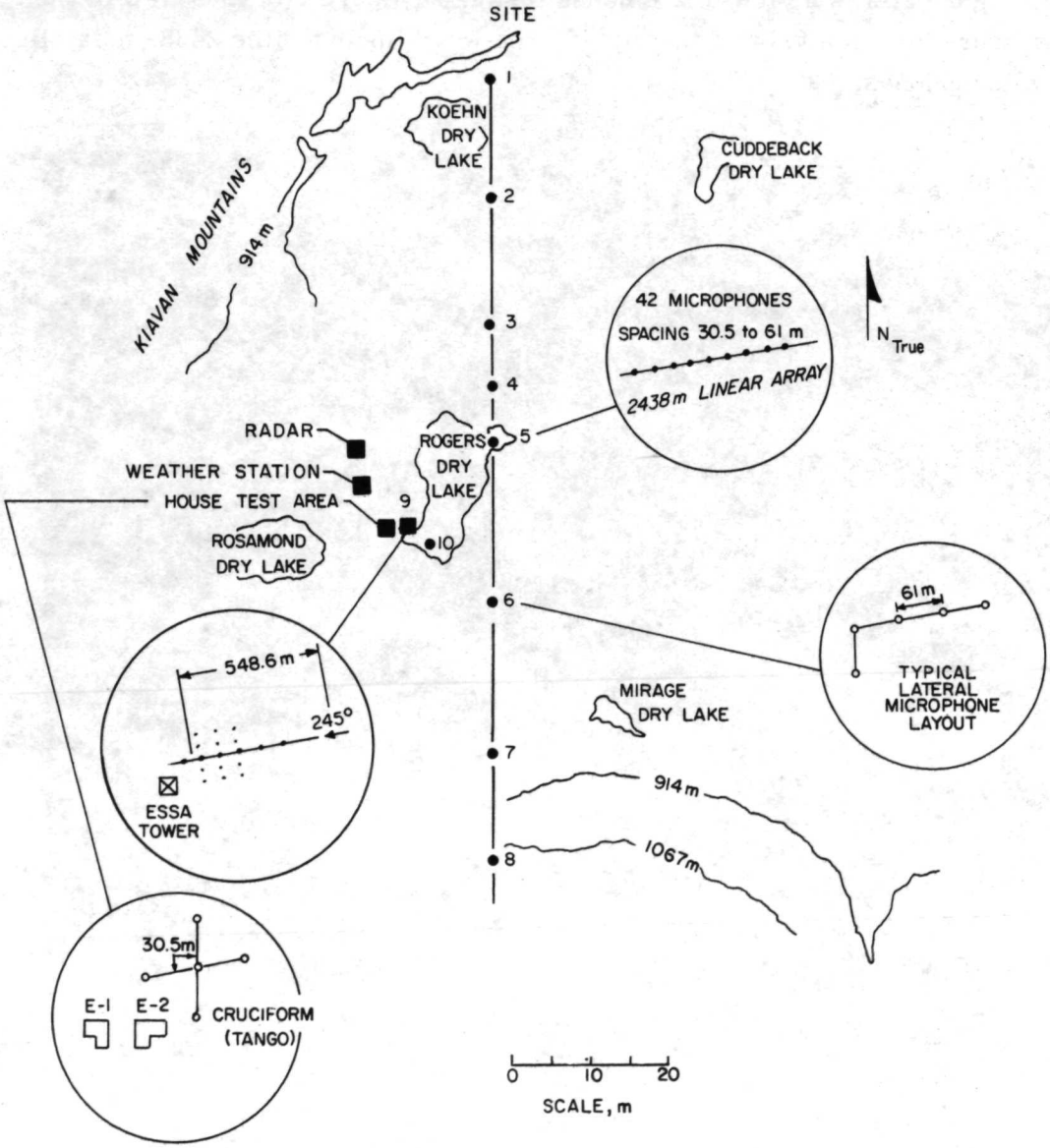
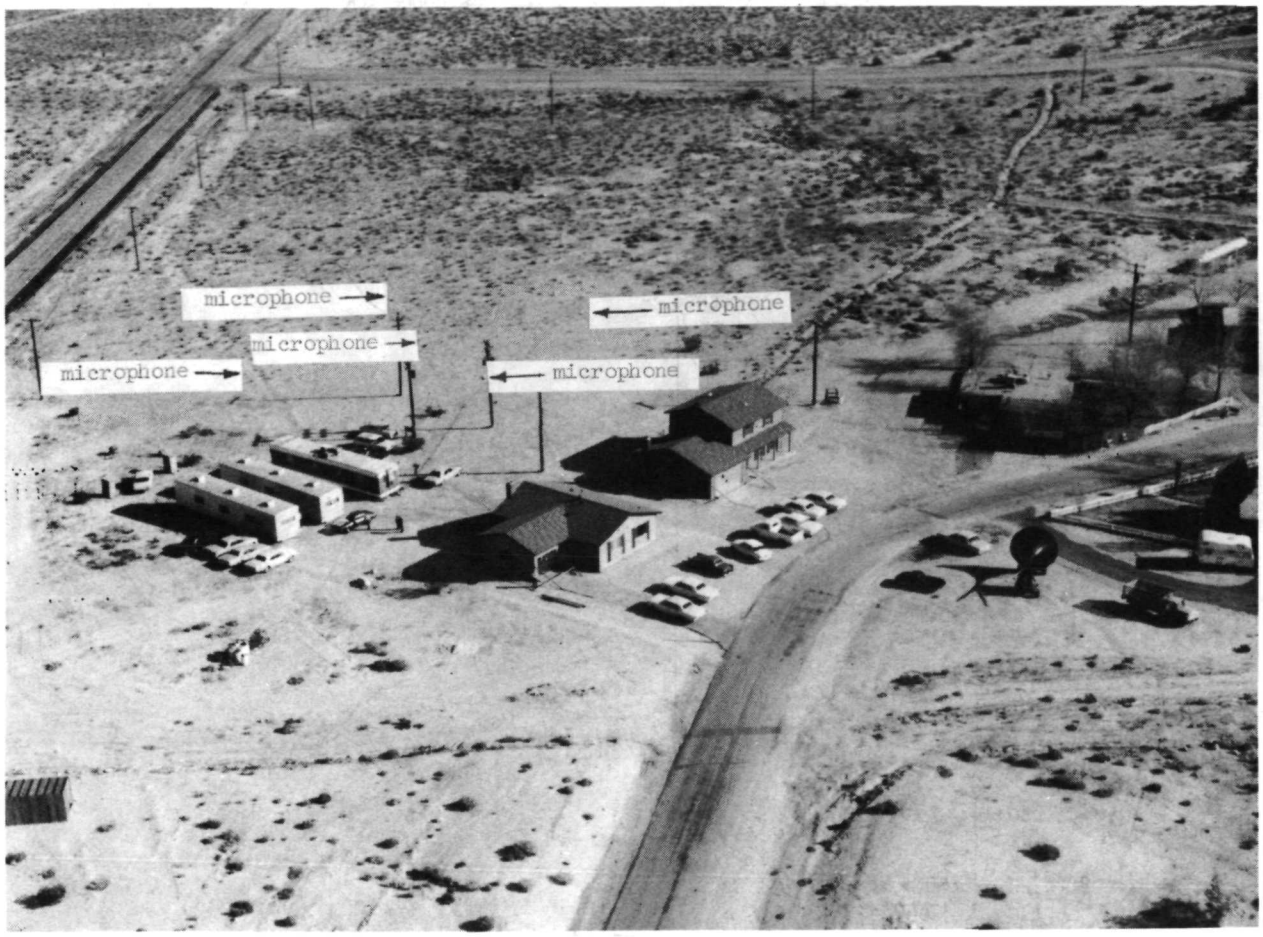


Figure 1.- Schematic diagram showing test area, arrangement of facilities, deployment of sonic-boom measurement stations, and microphone arrangements.

microphone arrangements at the various measurement site locations. It should be noted that the test layout shown in figure 1 was used for the Edwards Phase I and Phase II XB-70 sonic-boom test program reported in reference 10. The approximately 60 microphones deployed for these studies were arranged in particular arrays (see ref. 10 for detail layout) which depended on the type of flights scheduled for any given day. Because the data of the present studies were obtained on a noninterference basis, different microphone deployments existed for the different flights listed in table I.

Photographs of the primary sonic-boom measuring stations indicating the type of terrain in which the microphones were deployed are shown in the aerial photographs of figure 2. Figure 2(a) is a view of the house test area, figure 2(b) is a view of the site-9 area, and figure 2(c) is a view of the site-5 area which included the 2438-meter linear array of microphones.



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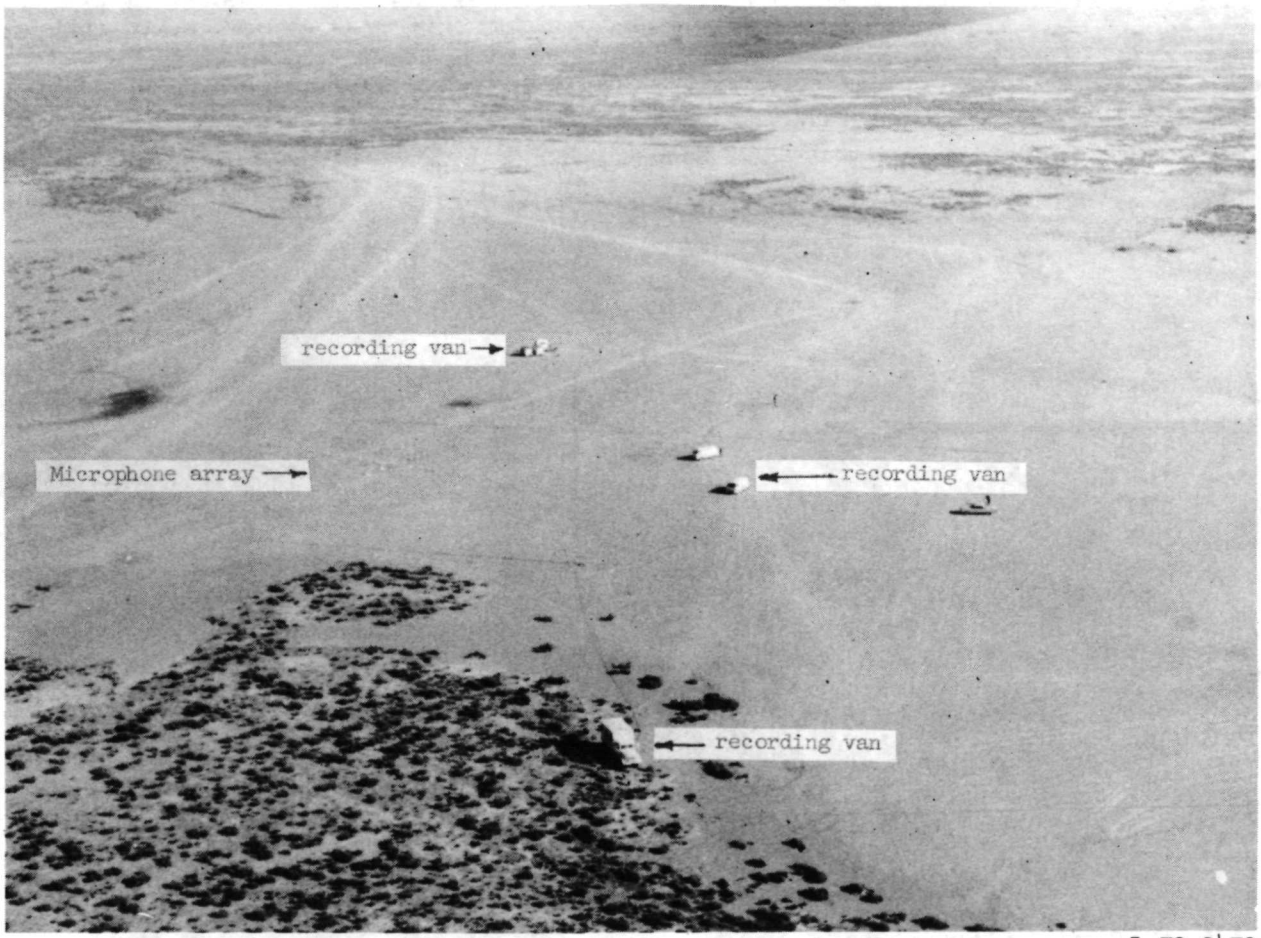
(a) House test area - Tango or Cruciform (view looking east).

Figure 2.- Aerial photographs of sonic-boom measurement stations used during tests.



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(b) Site-9 area (view looking northeast).

Figure 2.- Continued.

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(c) Site-5 area (view looking south).

Figure 2.- Concluded.

Test Airplane

A photograph of an aircraft of the type used in these tests is shown in figure 3. As indicated in table I, data were obtained primarily from flights of the SR-71 vehicle although some data are presented for the F-12 which is of the same general type. The SR-71 has a wing span of about 16.7 meters and a length of about 32.6 meters. The aircraft operated out of the Edwards and Palmdale, California, areas under USAF direction.

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Figure 3.- Photograph of airplane type used during tests.

Aircraft Positioning

The basic SR-71 missions included overflights of the Edwards test area. The Edwards Air Force Base radar control did not directly control the position of these aircraft for the sonic-boom missions; however, they did supply tracking information. The tracking information consisted of plots of plan position, altitude, and heading, at 1-second intervals within a 46-kilometer radius of the Rogers Dry Lake area. Altitude, ground speed, heading, and calculated Mach number are shown in table I and are based on information obtained from these radar plots.

The ground tracks for the flights listed in table I are shown in figure 4. Unless noted, steady, level flight conditions were maintained at least 45 kilometers prior to

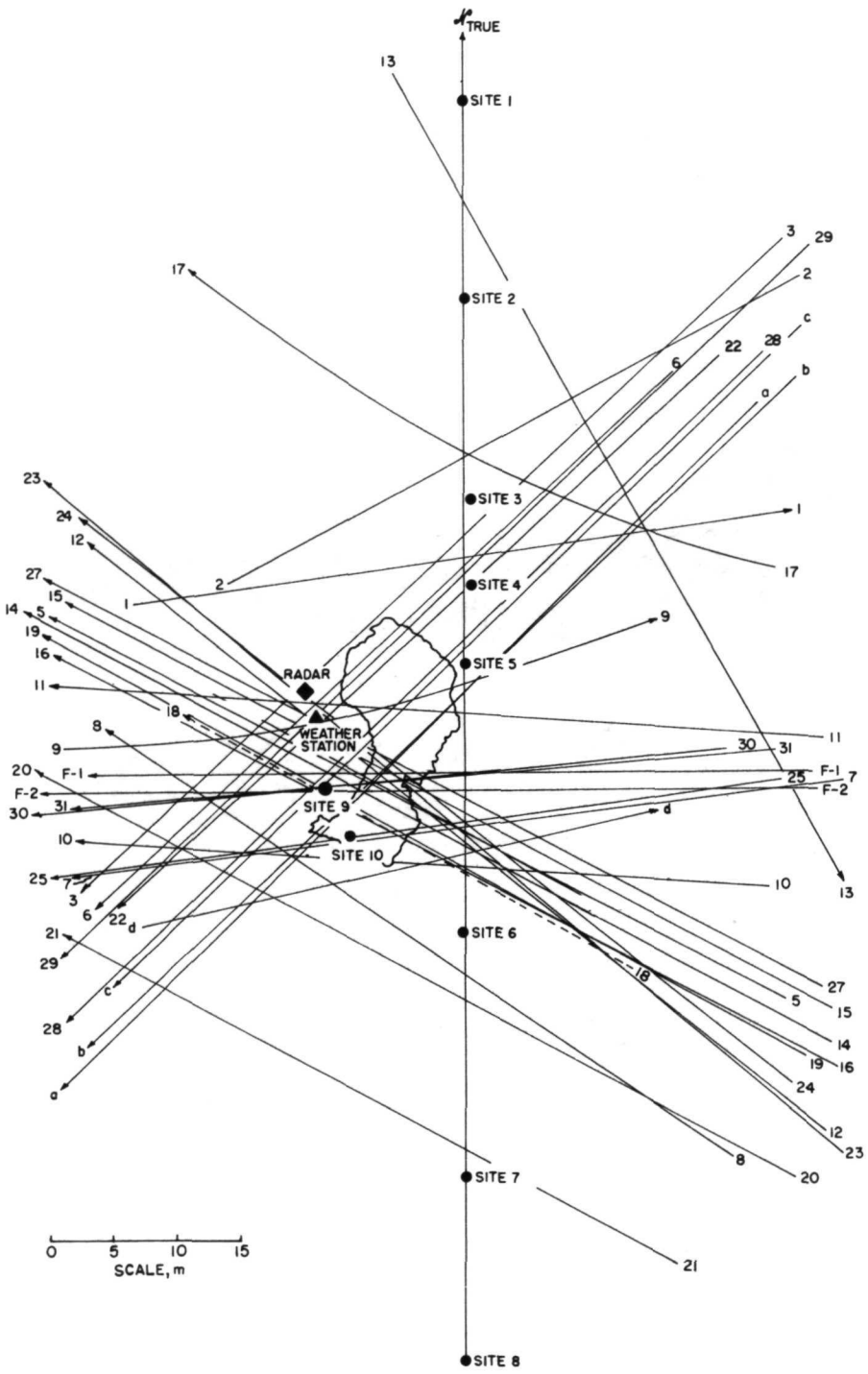


Figure 4.- Schematic diagram showing airplane ground tracks and headings for all missions along with location of sonic-boom measuring sites, radar, and weather stations. (Dotted line is estimated track.)

entering and 45 kilometers after leaving the measurement area. Also shown on the figure are the designated mission numbers, as well as locations of the sonic-boom measuring sites, the radar, and the weather station. In order to synchronize the tracking data and the data from the ground measuring stations, a 1000-Hz tone was superimposed on the data records and radar plots at the time the aircraft passed over, or was abreast of, the site-9 location.

Atmospheric Soundings

Rawinsonde observations for the present paper were obtained from the Edwards Air Force Base weather facility (see figs. 1 and 4) which was located approximately 7 kilometers from the house test area during the Edwards Phase I and Phase II sonic-boom studies. These soundings (which were launched primarily for the test program of ref. 10) were usually scheduled such that two per day were taken at approximately 1630 and 2200 GMT. Tabulations of the measured values of atmospheric pressure and temperature, the calculated values of speed of sound and wind velocity, and wind-direction values (from the sounding taken closest to the time of flight) are given in table II at approximately 610-meter intervals.

Pressure Instrumentation

The main components of the systems used for measuring sonic-boom ground pressures are described in detail in reference 1 and are the same as used in previous programs. Each channel of the measuring system used in the experiments consisted of a specially modified microphone, tuning unit, dc amplifier, oscillograph recorder, and magnetic tape recorder. The usable frequency range was from 0.02 to 10 000 Hz, and this range applies to all the data presented herein. The microphones have a dynamic range from about 70 to 150 dB and have a usable response time of 20 seconds. The entire sound measurement system was calibrated in the field by means of conventional discrete frequency calibrators. Prior to field installation, a frequency-response calibration was made for all microphone systems.

For ease of setup and consistency of measurements with this equipment, which was also used in other tests in the same time period, each microphone was shock-mounted 0.15 meter above ground level with the sensitive element parallel to the reflecting surface. Previous measurements (ref. 9) indicate that this type of mounting arrangement results in only very small differences in waveform compared to those obtained in the ground plane. Wind screens consisting of two layers of cheesecloth were employed to minimize effects of surface winds on the microphone readings and also to provide shade from the sun and protection from blowing sand particles.

RESULTS AND DISCUSSION

Waveform Variations

An indication of the waveform category is given in the diagrams of figure 5. Tracings of sample sonic-boom pressure-time histories measured along the ground track are presented in figure 6. These signatures represent the range of waveshape observed during these studies, and they are noted to vary from a normal N-wave to a peaked wave and to a rounded wave. These types of variation are similar to those observed for the F-104, B-58, and XB-70 (ref. 12). The signatures of figure 6 are also used to define the quantities of overpressure Δp_o, positive impulse I_o, rise times τ and $\tau_{1/2}$, positive time duration Δt_o, and total time duration ΔT. The values of these parameters are listed in table III in ascending order of mission numbers along with the location of the measurement station in range and direction (north or south) from the flight track. The mission-number designation was established during the work of reference 6. With a few exceptions complete signature data are given for those measurements within about 5.6 kilometers of the ground track.

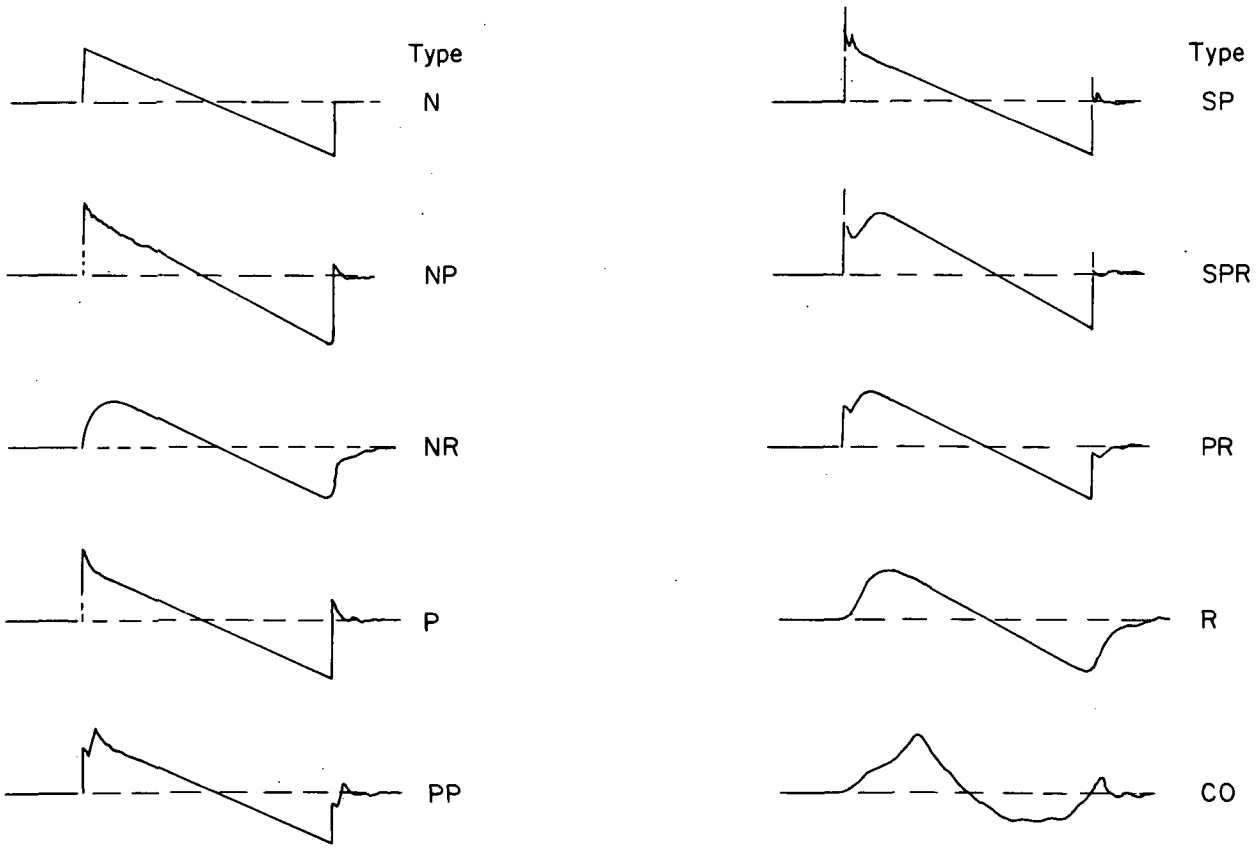


Figure 5.- Diagrams of waveforms which represent the various categories of sonic-boom signatures measured.

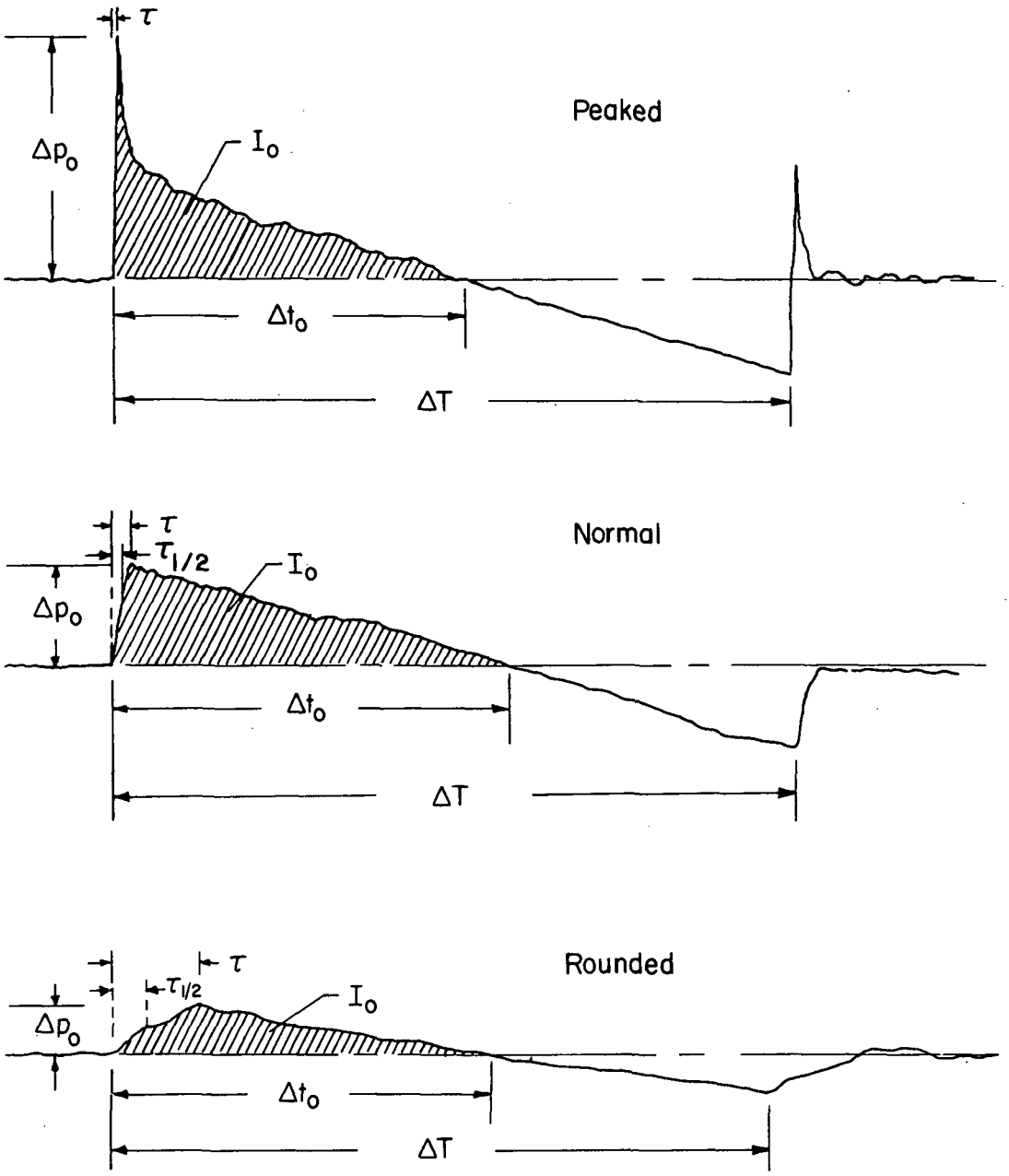


Figure 6.- Tracings of measured sonic-boom pressure-time histories along ground track showing some waveform shapes and signature definitions.

Ground-Track Measurements

Figure 7 includes tracings of sonic-boom pressure signatures measured along the ground track of the airplane at four altitudes varying from 10 668 to 24 384 meters and Mach numbers from 1.4 to 3.0, respectively. The waveforms presented are of the N-wave type. These waveforms are similar in nature to those obtained from other aircraft of similar size (ref. 10). In general, it can be seen that the peak-pressure values decrease and the time durations of the wave increase as the altitude of the aircraft is increased.

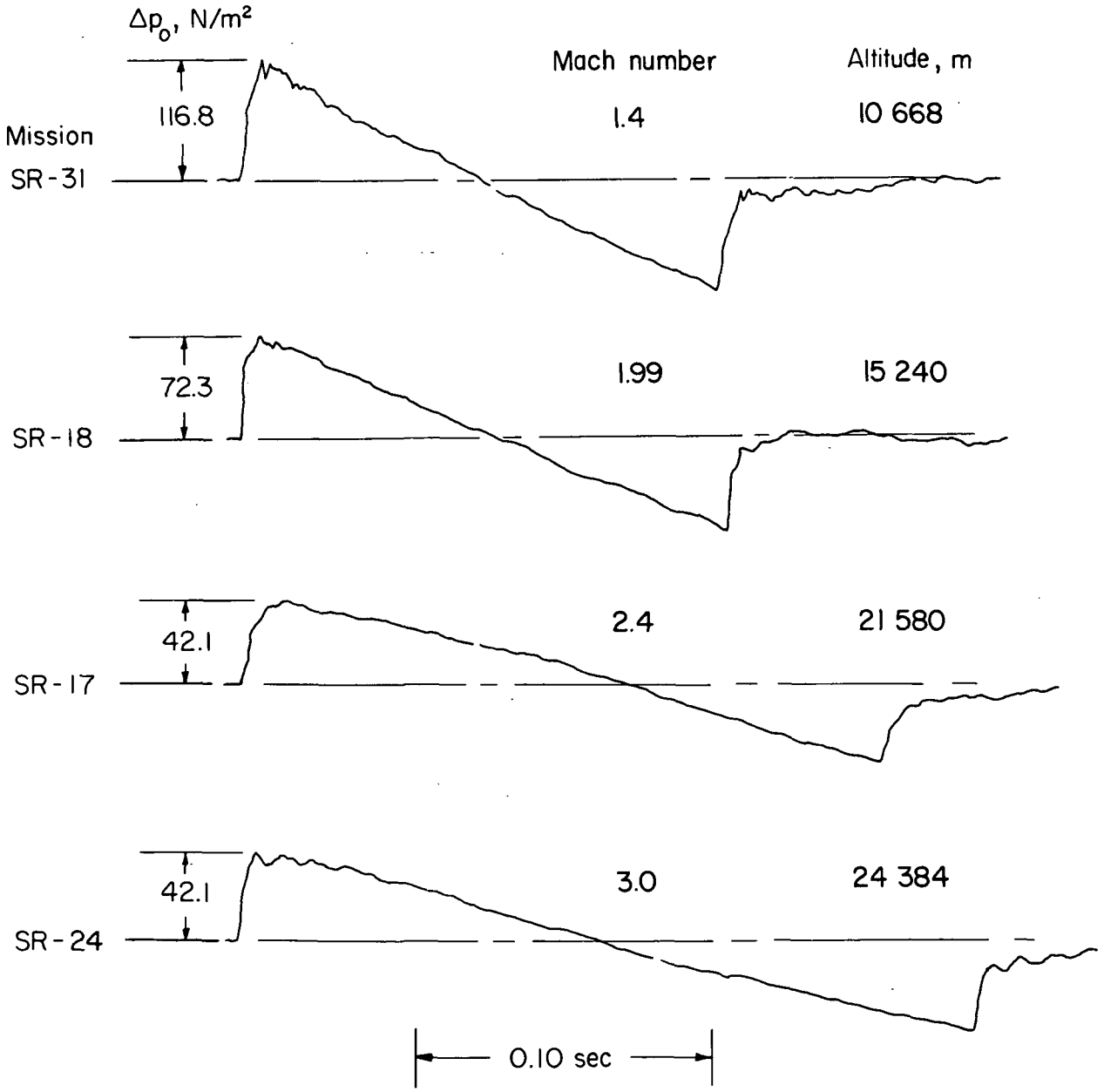


Figure 7.- Tracings of sonic-boom pressure signatures measured within 5.5 km of the track for airplane at various altitudes. (Mach number ranges from 1.40 to 3.0.)

A comparison of measured and calculated sonic-boom pressure signatures corresponding to three of the four cases shown in figure 7 is presented in figure 8. Calculations are based on the currently available methods of references 13 and 14 for the Mach number, altitude, and gross-weight conditions corresponding to the flight data. It will be noted that good agreement exists between measured and predicted signatures relative to shock locations, overpressure values, and signature duration for all three signatures measured at altitudes of 10 668, 15 240, and 24 384 meters and for Mach numbers of 1.4, 1.99, and 3.0, respectively.

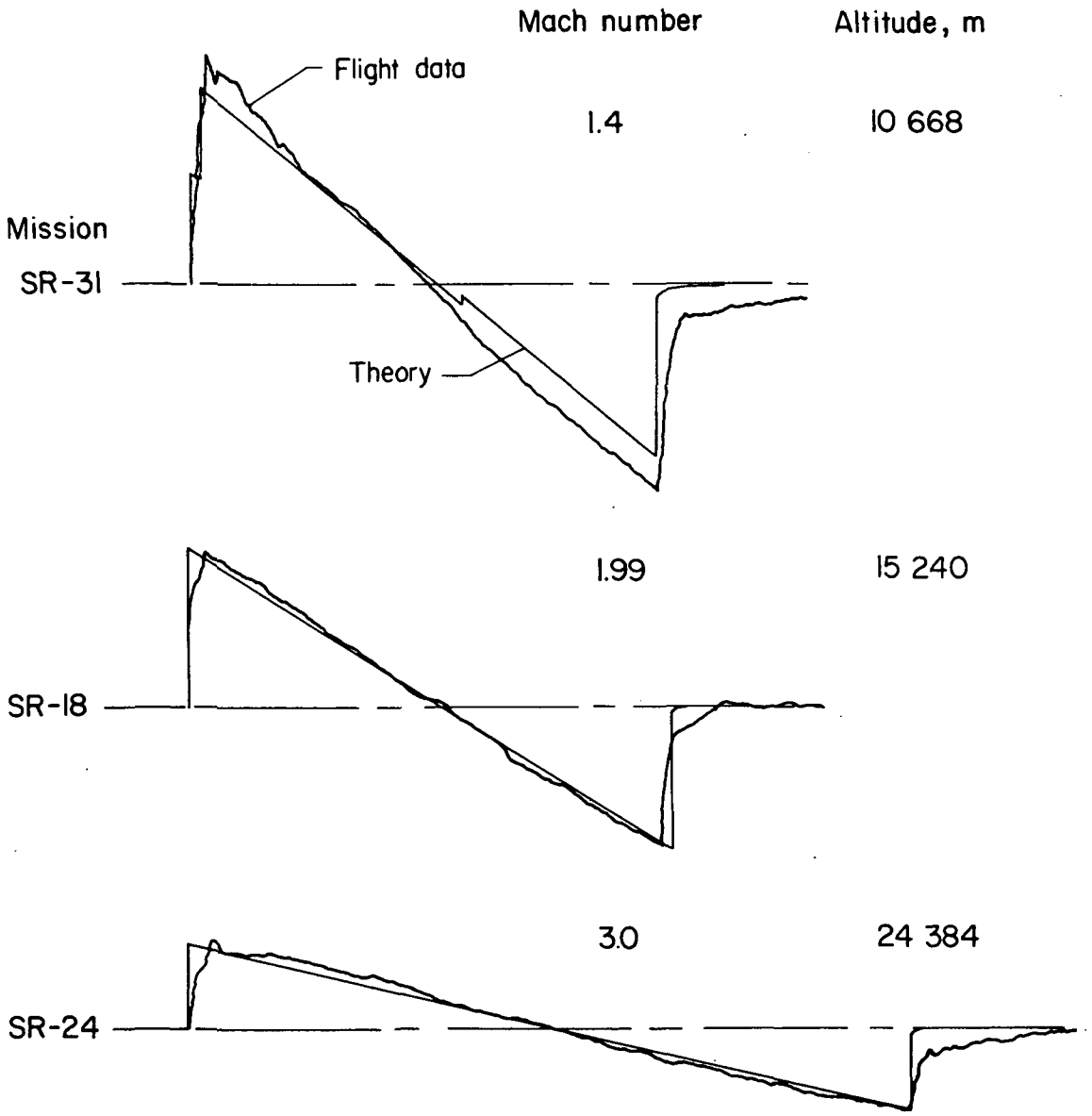


Figure 8.- Tracings of measured and calculated sonic-boom pressure signatures at various altitudes. (Mach number ranges from 1.40 to 3.0.)

The bow-wave peak overpressures obtained from signatures of the type shown in figure 7 are presented in figure 9 as a function of airplane altitude for steady level flight. The data of figure 9 represent results of 28 flights for a total of 928 data samples of measurements at distances within 5.5 kilometers of the aircraft ground track and cover a range of Mach numbers from 1.35 to 3.0. Each symbol represents an individual mission, the blocked-in symbols represent the average of the measurements obtained on 20 to 64 microphones and the open symbols the average of the measurements obtained from 3 to 5 microphones. The circle symbols represent data from flights made during the November 1966 to January 1967 time period for which atmospheric conditions were observed to be somewhat more quiescent than those during the six flights of the June 1966 time period as represented by the diamond symbols.

Calculated values of bow-wave overpressure as a function of altitude corresponding to the SR-71 experimental data points are given in figure 9. The calculated band shown by the solid lines represents the overpressure variation for the gross-weight and Mach-number variations of the aircraft during the experiments. Also shown on the figure by the shaded band are the ranges of bow overpressures for the B-58 aircraft (see fig. 16 of ref. 13 and fig. 30 of ref. 6) which is about the same size and weight as the SR-71.

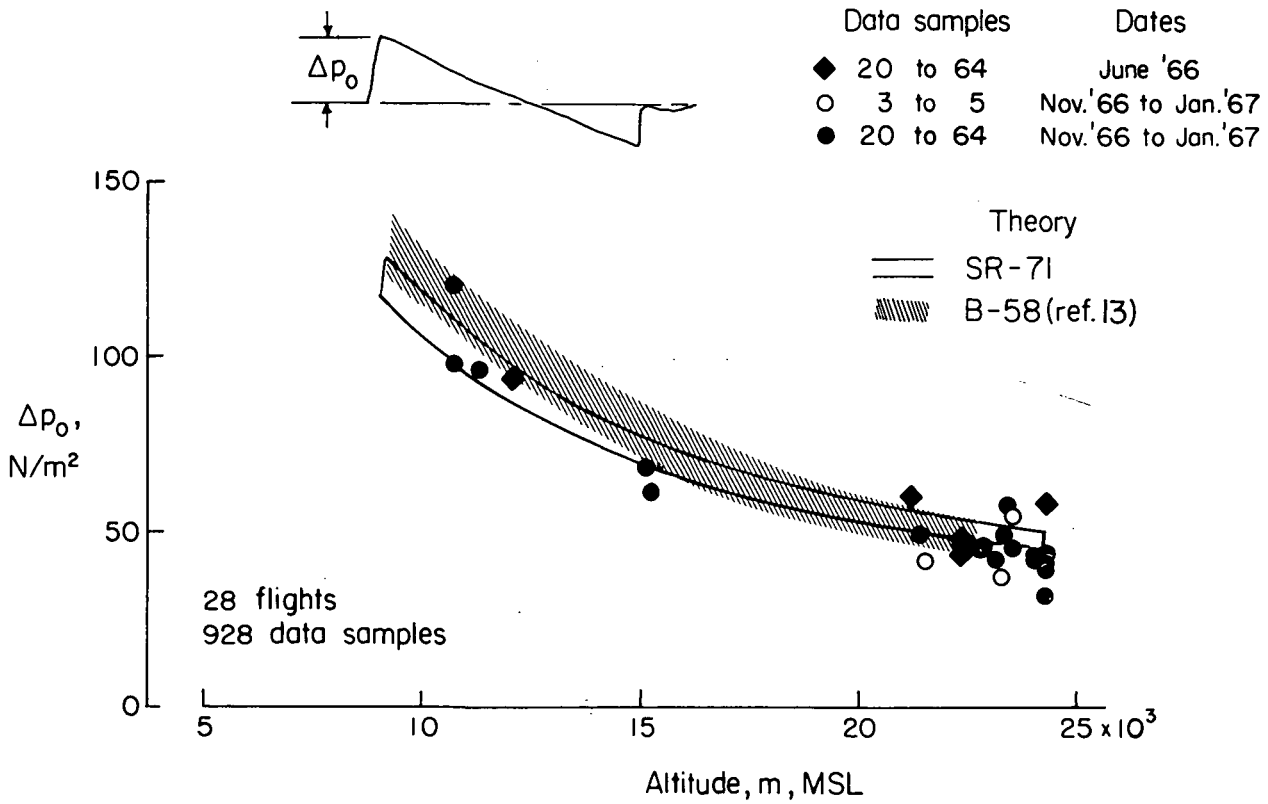


Figure 9.- Measured peak overpressures within 5.5 km of ground track as a function of altitude for airplanes in steady level flight. Data are presented for a range of Mach numbers from 1.35 to 3.0.

It can be seen from figure 9 that the SR-71 measurements are in good agreement with the calculated values and are in general agreement with the measurements and calculations for the B-58 aircraft operating in the same altitude range but at lower Mach numbers. The similarity of the two curves indicates that Mach number has little influence on the overpressure. In addition, the experimental data suggest that no unusual phenomena were observed for the high-altitude flight and high-Mach-number conditions of these tests.

Lateral Spread Measurements

Tracings of sonic-boom signatures at various lateral distances out to about 50 kilometers from the ground track for flights at an altitude of about 22 860 meters and a Mach number of about 3.0 are given in figure 10. Here again, as in figure 7, the pressure

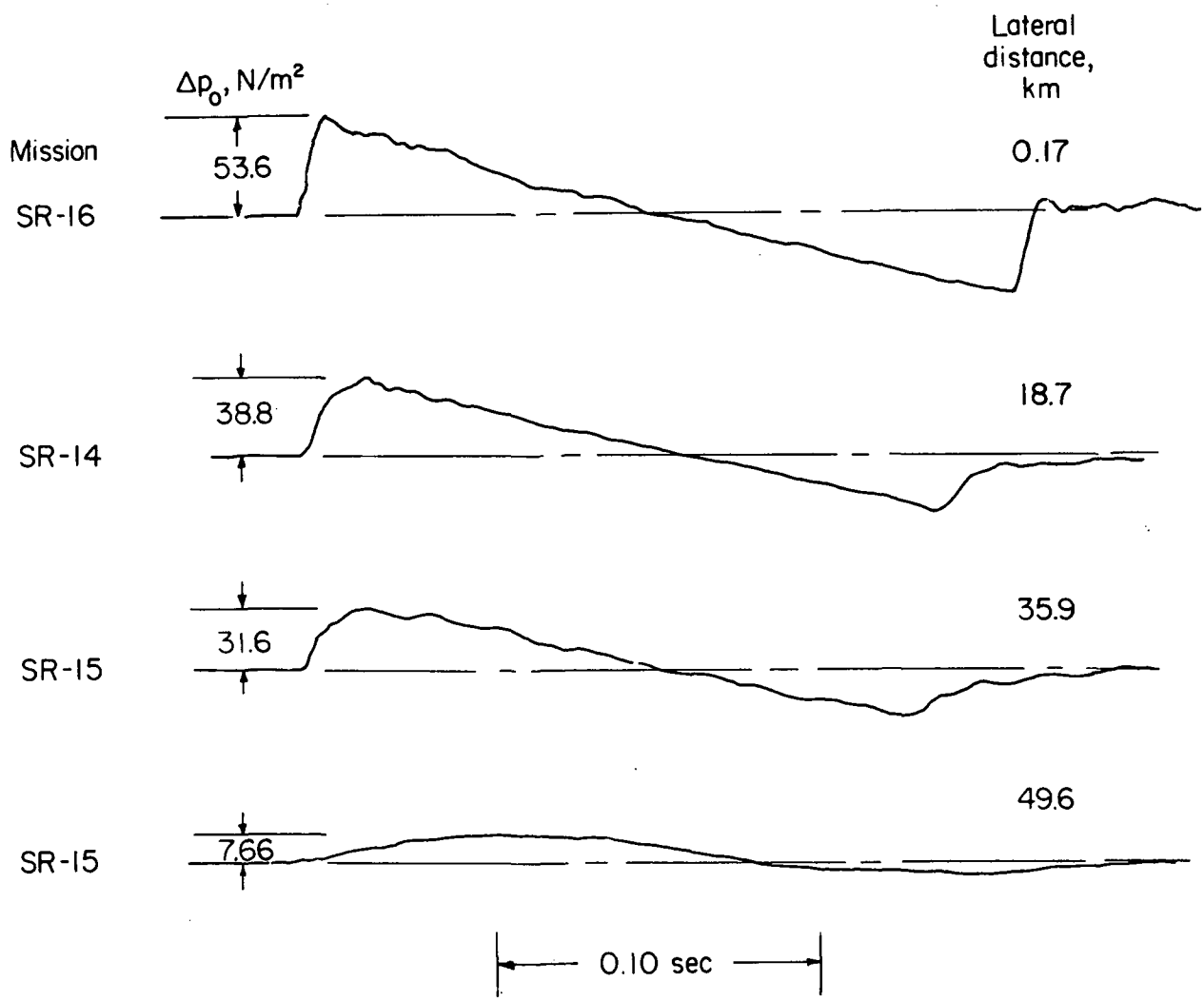


Figure 10.- Tracings of sonic-boom ground-pressure signatures at various lateral distances from the ground track for the airplane at an altitude of about 22 860 meters and a Mach number of about 3.0.

signatures are seen to have the gross features of N-waves except for extreme lateral distances. The rise times of the signatures of figure 10 become longer and the overpressures decrease as the lateral distance from the flight track increases. These findings are similar to those obtained on other aircraft. (See refs. 6 and 9.)

Overpressure data from signatures of the type shown in figure 10 and included in table III are plotted in figure 11 as a function of lateral distance from the flight track for

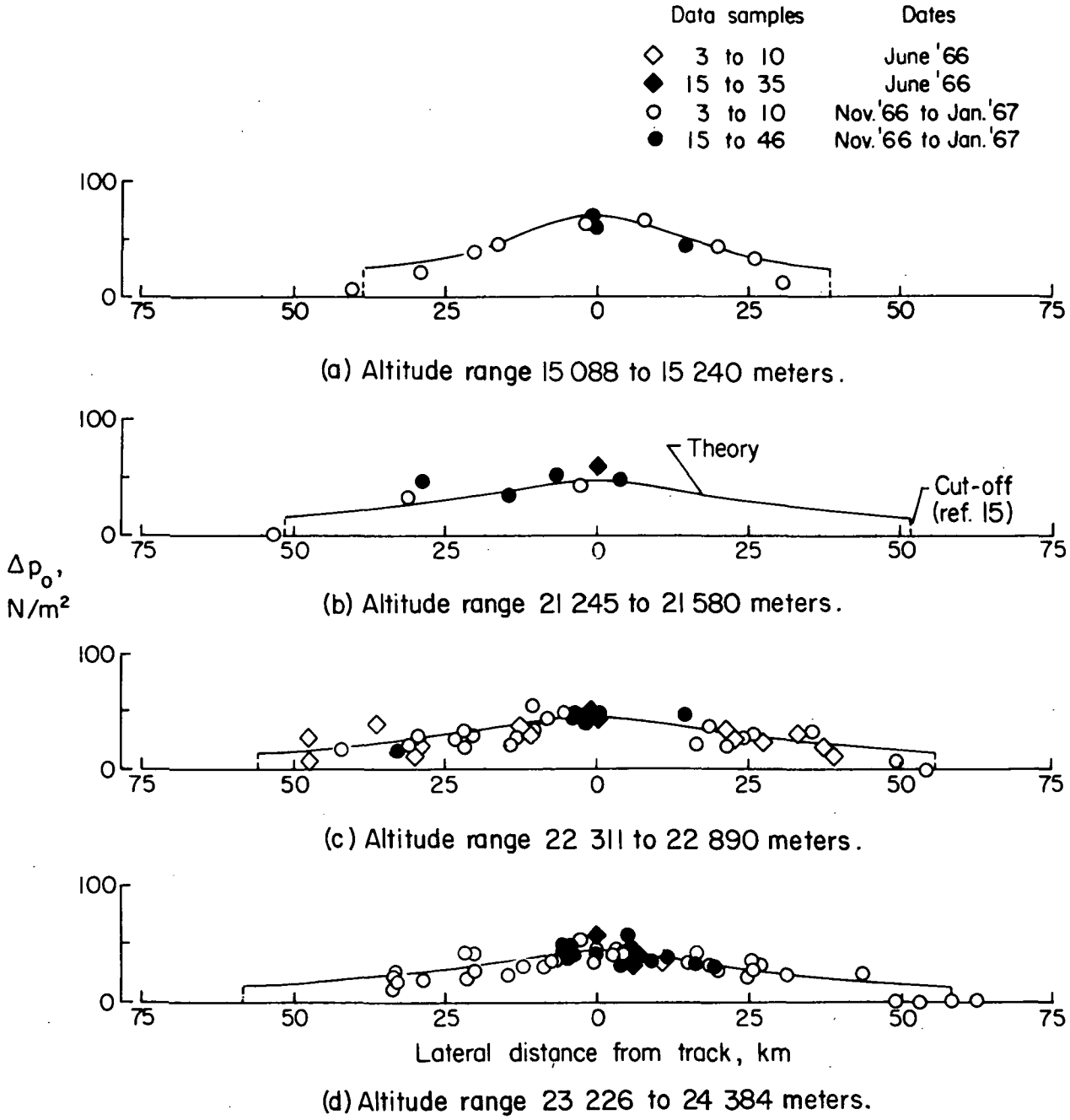


Figure 11.- Sonic-boom overpressures as a function of lateral distance for various altitude ranges. (Mach number ranges from 1.92 to 3.0.)

four altitude ranges. Symbol codes similar to those of figure 9 have been used wherein each symbol represents the average of a number of measurements for each mission. The solid curves shown in figure 11 are the predicted overpressure variations. The dashed vertical lines are estimates of the lateral extent of the pressure patterns based on atmospheric refraction (ref. 15). The overpressures are seen generally to be a maximum along the ground track and decrease with increasing lateral distance. The prediction of the lateral cut-off point appears to correlate well with the data for the Mach-number and altitude ranges of these tests.

Statistical Variation

The data of table III have been analyzed to determine the statistical variations of peak overpressures Δp_o, positive impulse values I_o, time durations Δt_o and ΔT, and rise times τ and $\tau_{1/2}$. The data are presented in the form of histograms and a probability plot in figures 12 to 16 for all flights in the altitude range from 21 336 to 24 384 meters and for measurements made within 5.5 kilometers of the aircraft ground track. Similar information relative to the same aircraft and altitude and Mach-number range is contained in reference 11 for measurements obtained at offset distances 8 kilometers away from the aircraft ground track.

Peak overpressure.- Figure 12 contains a histogram showing the variation of the measured ground pressures. The results shown are for 22 flights from which 704 data samples were obtained. The overpressure interval was taken as 2.4 N/m^2. It can be seen that the largest number of events is associated with overpressure values of the order of 43 N/m^2. Values ranged from about 26.3 N/m^2 to about 96 N/m^2 and one extreme value of about 125 N/m^2 was encountered.

The results of the histogram of overpressure variation of figure 12 are shown in figure 13 as the probability of equaling or exceeding the ratio of the measured overpressure to the nominal calculated value in a standard atmosphere. A straight line has been faired through the data points. For this type of presentation, if the logarithm of the data fit a straight line the overpressure would follow a normal distribution. The slope of the line is an indication of the variability. The results indicate that 50 percent of the occurrences can be expected to equal or exceed the calculated (nominal) value and that one boom out of 1000 will exceed the nominal value by a factor of 2 or greater.

Positive impulse.- A presentation similar to that of figure 12 is shown in figure 14 for the positive impulse values. An examination of the histogram of figure 14 indicates that the variability in the impulse is generally less than for the associated overpressures of figure 12, and this result is consistent with the findings of other similar studies (refs. 1, 2, 10, and 12).

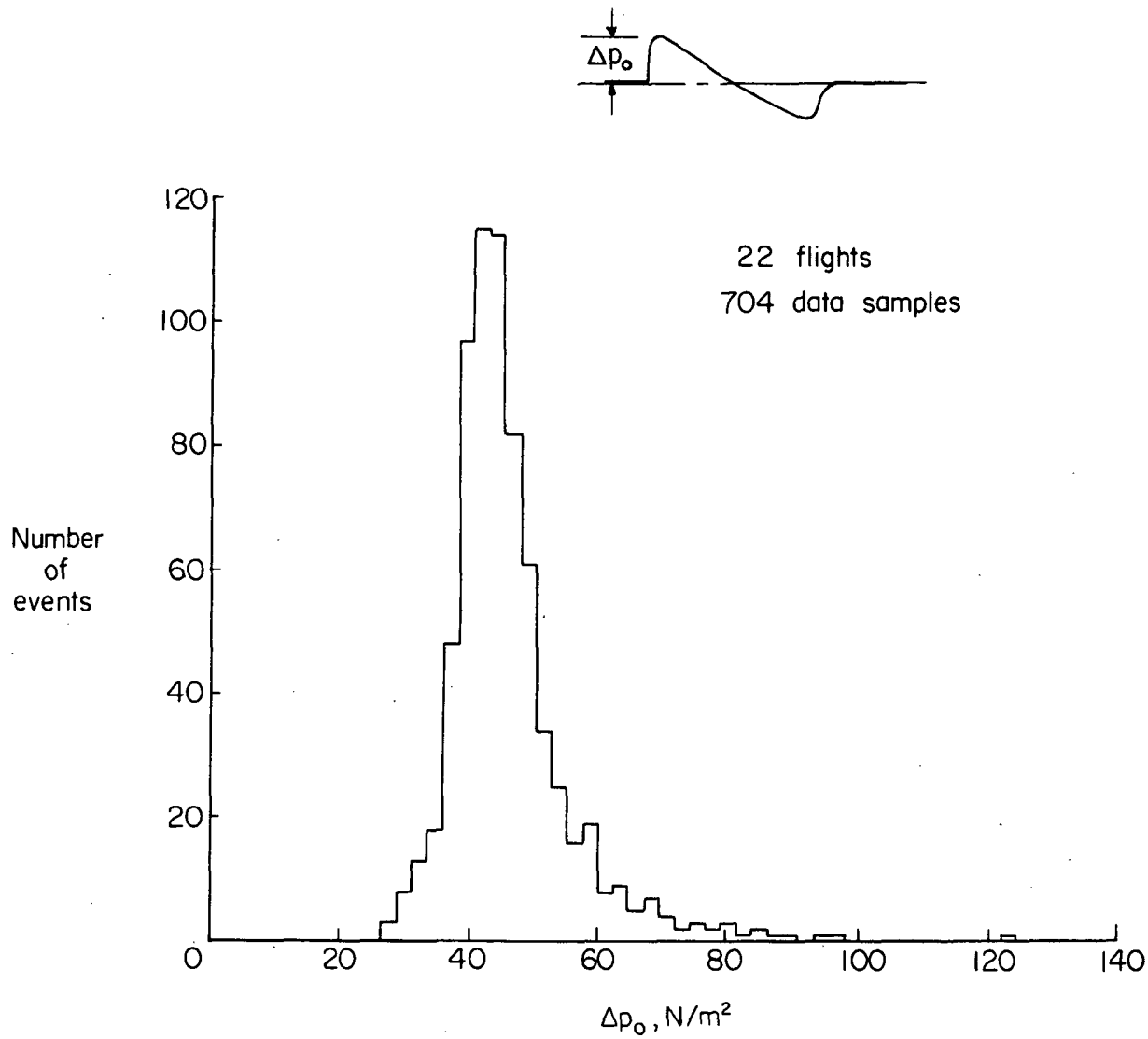


Figure 12.- Histogram showing variability of peak bow-wave overpressure of sonic-boom signatures for an altitude range from 21 336 to 24 384 meters. Data are for measurements within 5.5 km of ground track.

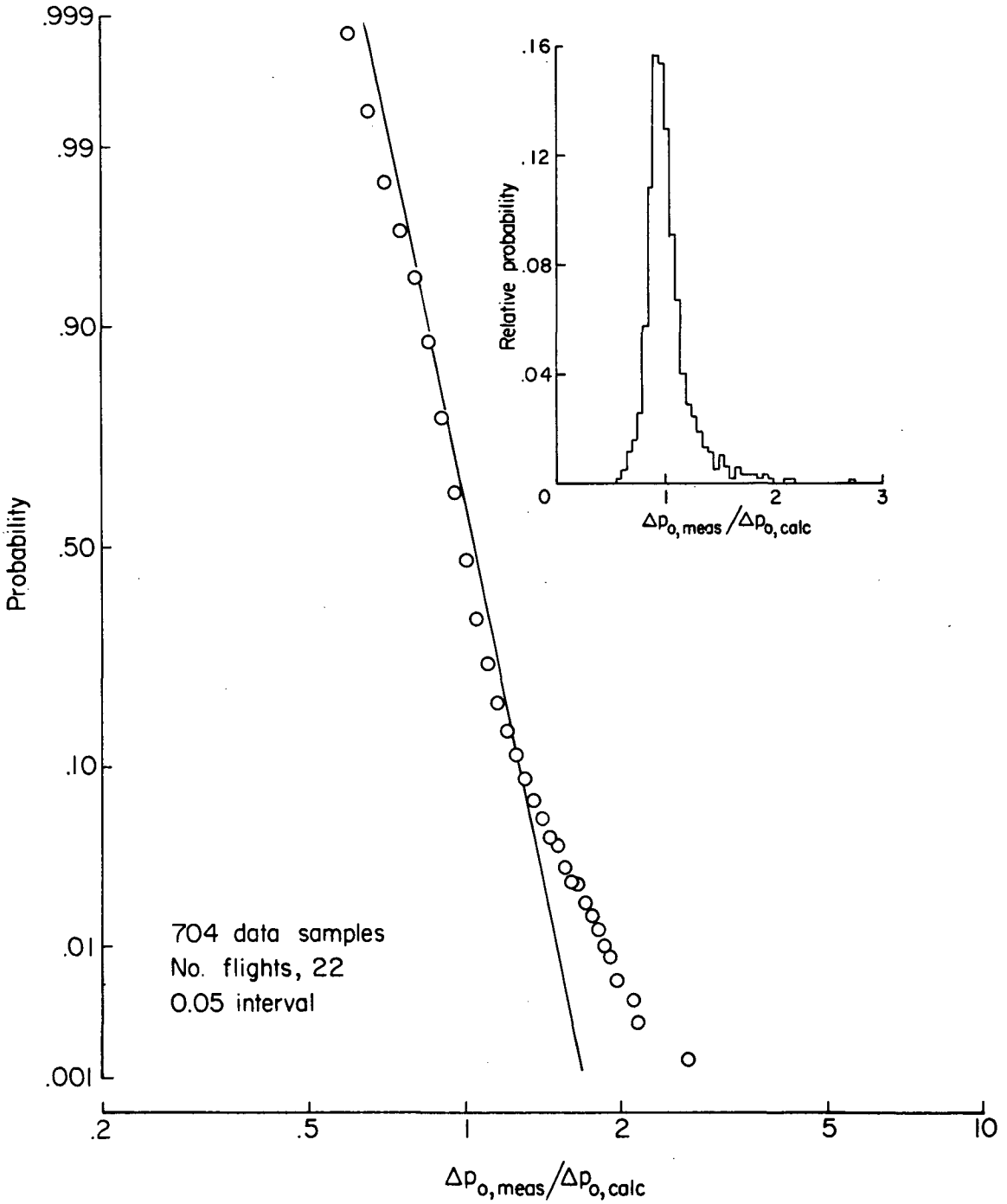


Figure 13.- Probability of exceeding given values of the ratios of measured to calculated ground overpressures for the SR-71 airplane during measurements in the Edwards area. Data are presented for an altitude range from 21 336 to 24 384 meters on measurements within 5.5 km of ground track.

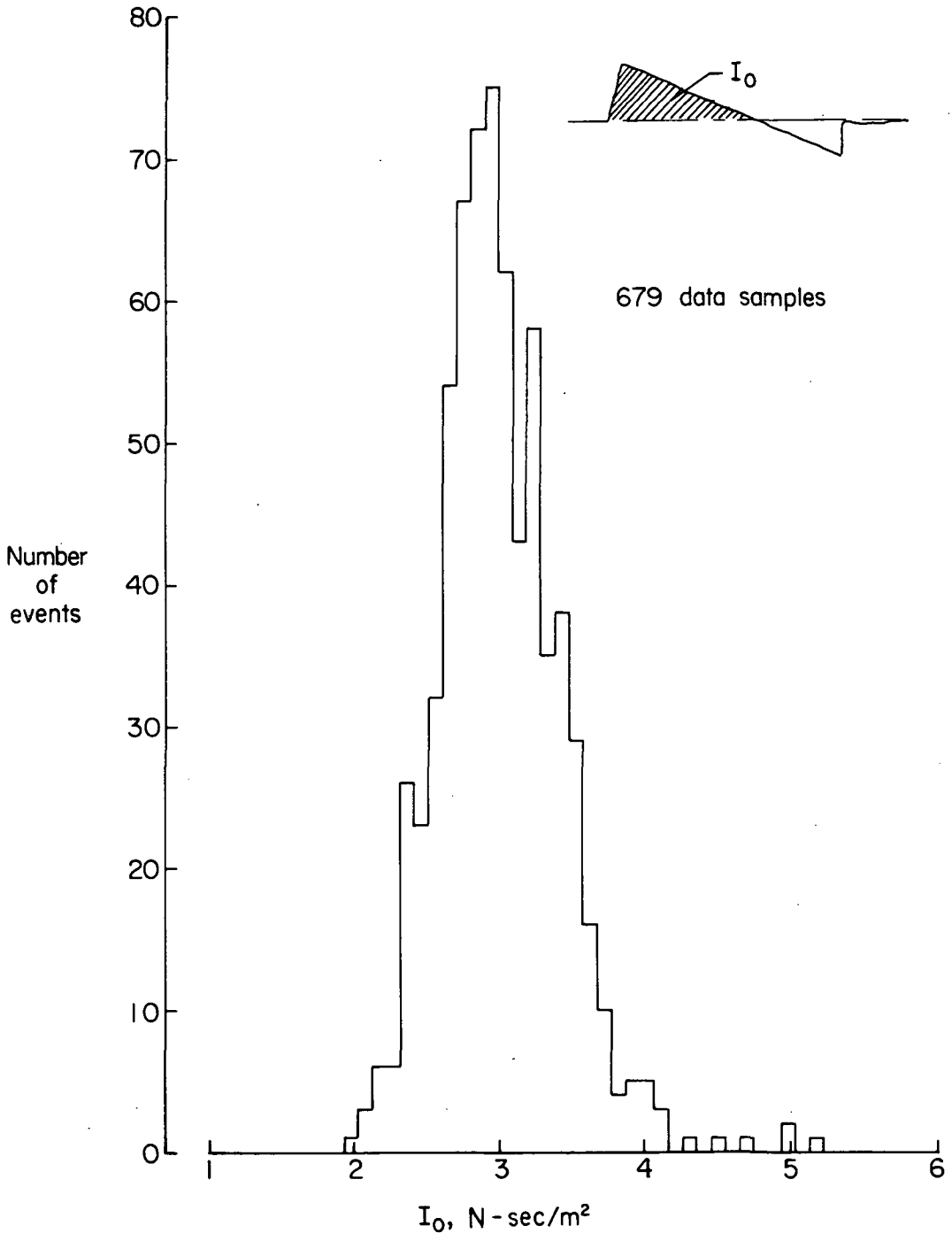
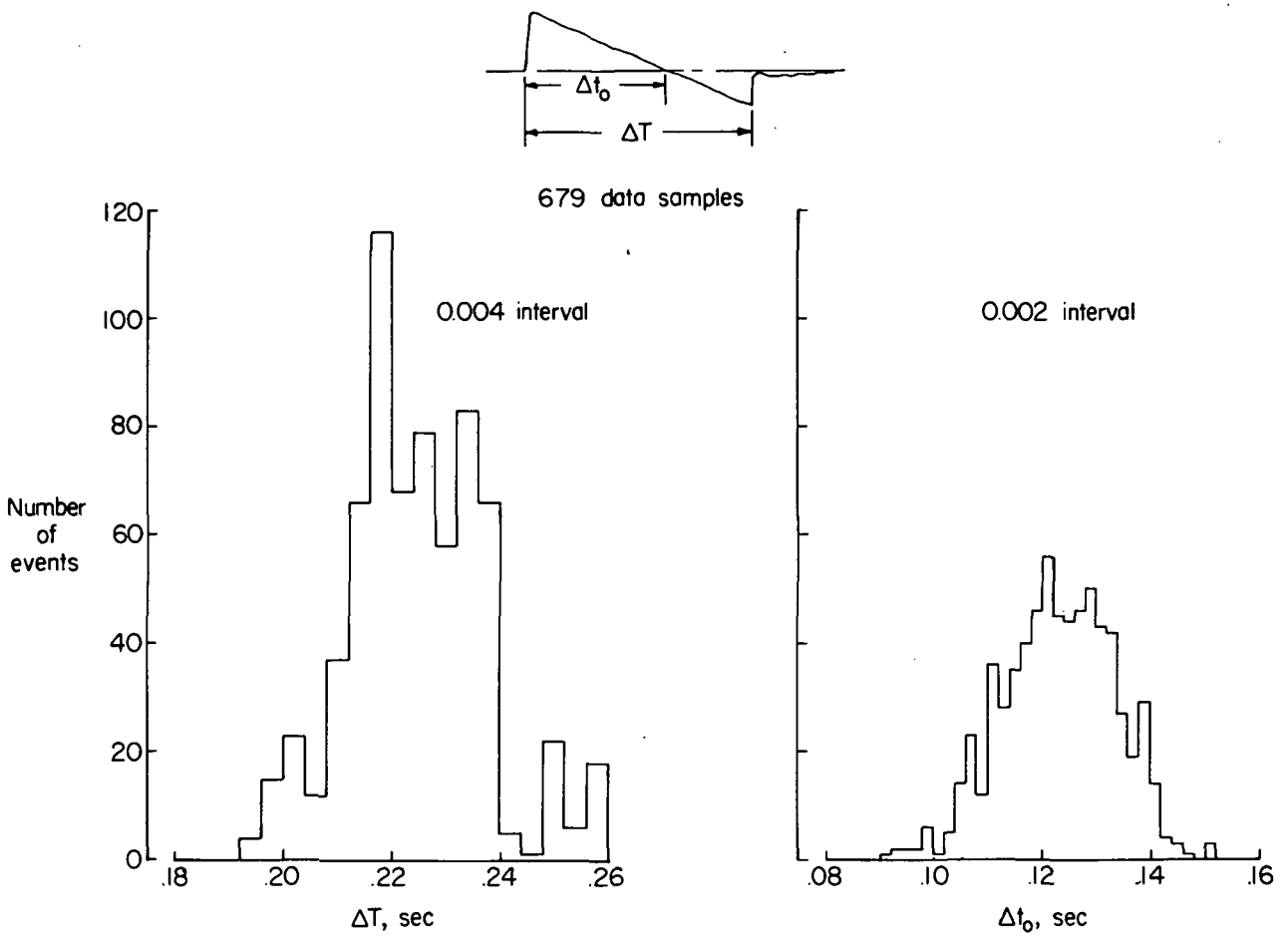


Figure 14.- Histogram showing variability of positive impulse of sonic-boom signatures for an altitude range from 21 336 to 24 384 meters. Data are for measurements within 5.5 km of ground track.

Signature durations.- Figures 15(a) and 15(b) are histograms showing the variability of the total time durations ΔT and the positive time durations Δt_o, respectively, of the sonic-boom signatures. It can be noted that variations of the order of 25 percent exist and these are consistent with similar data shown for the B-58 in reference 10. Variations of the positive time durations and the overpressures can both cause variations in the impulse; however, inspection of figures 12, 14, and 15 suggests that the overpressure variation is the dominant factor.



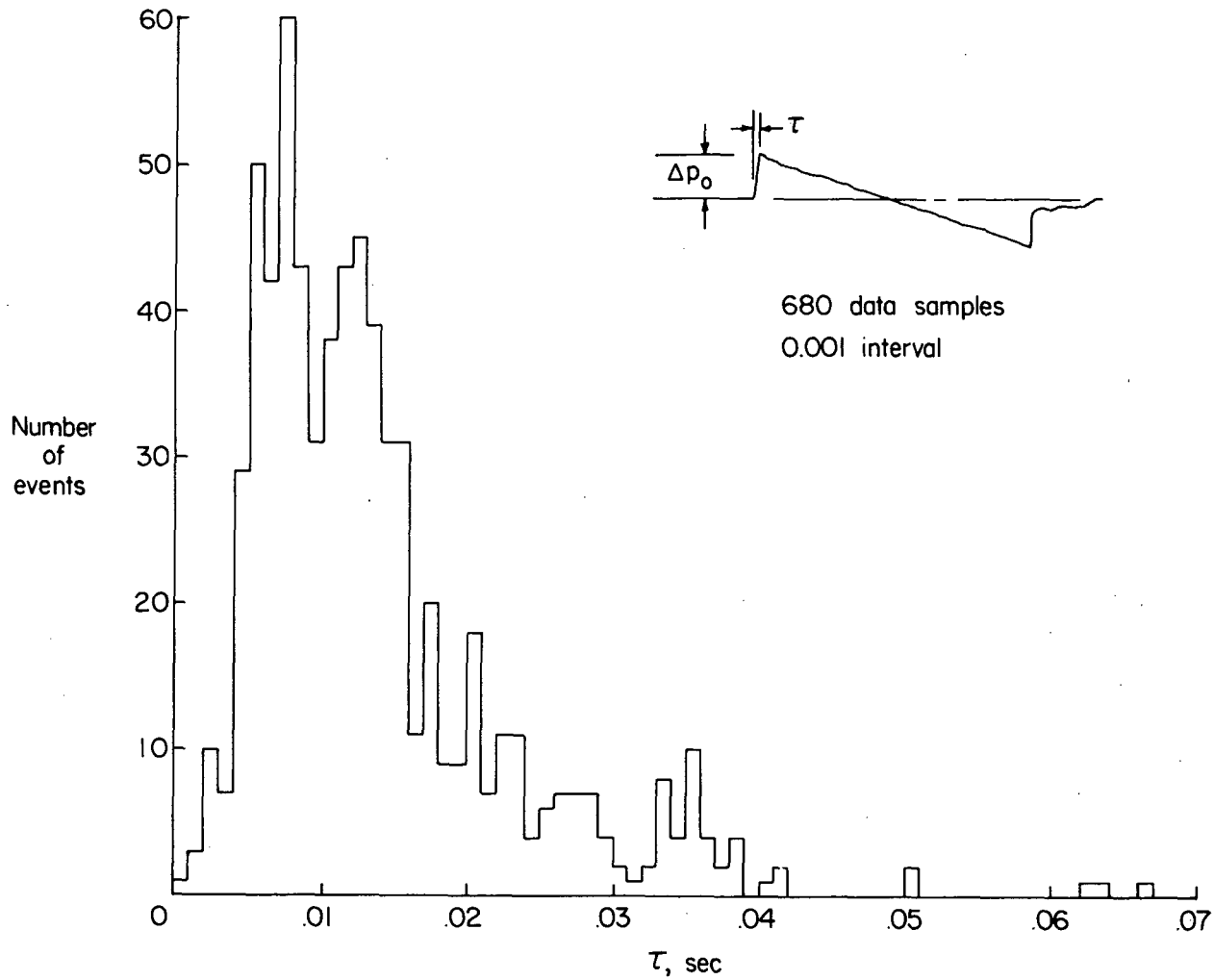
(a) Total time duration.

(b) Positive time duration.

Figure 15.- Histograms showing variability of the time durations of sonic-boom signatures for an altitude range from 21 336 to 24 384 meters. Data are for measurements within 5.5 km of ground track.

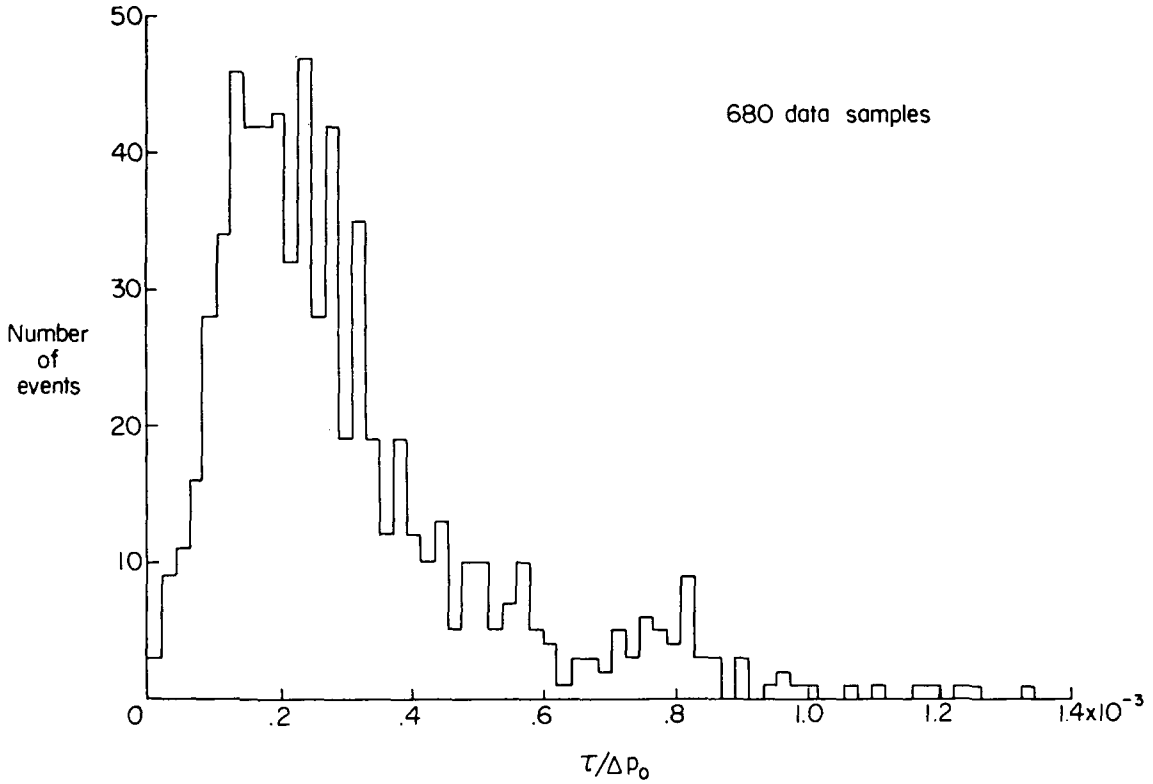
Rise time.- The data of figure 16 relate to the rise times of the waves as defined in the inset sketch of figure 16(a). For all types of waves diagrammed in figures 5 and 6, the rise time is defined as the time from the onset of bow-shock overpressure to the time of the maximum overpressure value and $\tau_{1/2}$ is the rise time to half amplitude.

Rise-time data are plotted in histogram form for the absolute values of rise times, rise time per unit overpressure, and rise time to half amplitude in figures 16(a), 16(b), and 16(c), respectively. It is shown in figure 16(a) that absolute rise-time values range from near zero to as large as about 0.065 second with the highest occurrence at about 0.009 second. Considerably smaller values of $\tau_{1/2}$ (rise time to half amplitude) are observed since the waveforms generally tend to exhibit rapid rise times at the onset of the bow shock with signature variations occurring thereafter. This can be illustrated by comparing the distributions of figures 16(b) and 16(c). Normally, longer rise times are associated with rounded waveforms and much shorter rise times are associated with peaked waveforms (ref. 16).

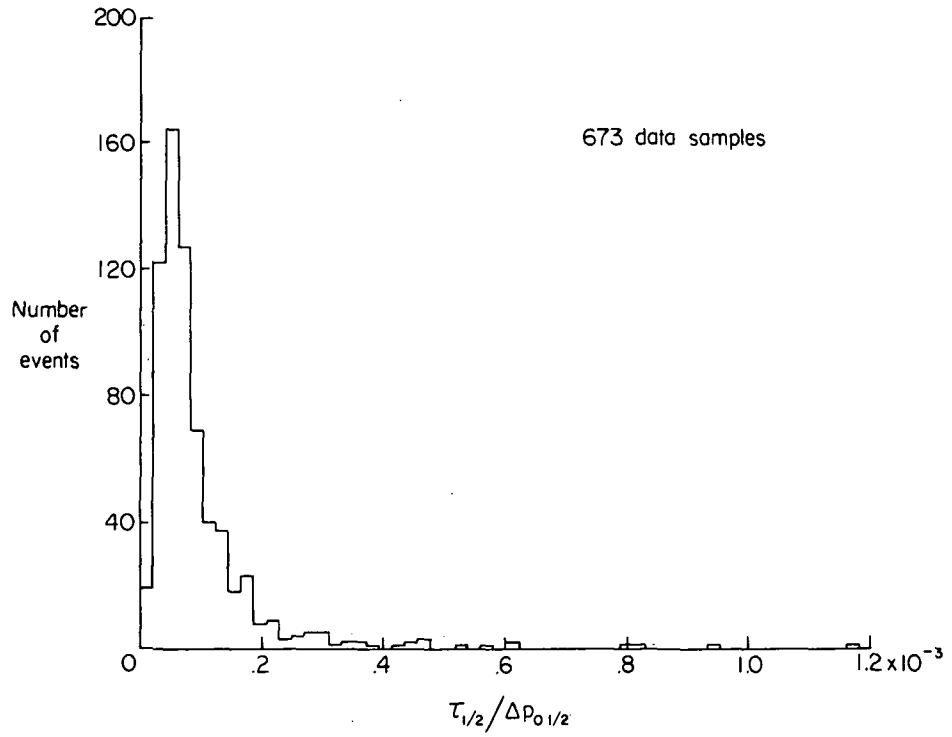


(a) Rise time τ to maximum amplitude.

Figure 16.- Histogram showing variations of bow-wave rise time to peak value of overpressure as measured from flights within 5.5 km of ground track for the altitude range from about 21 336 to 24 384 meters.



(b) Rise time per unit overpressure.

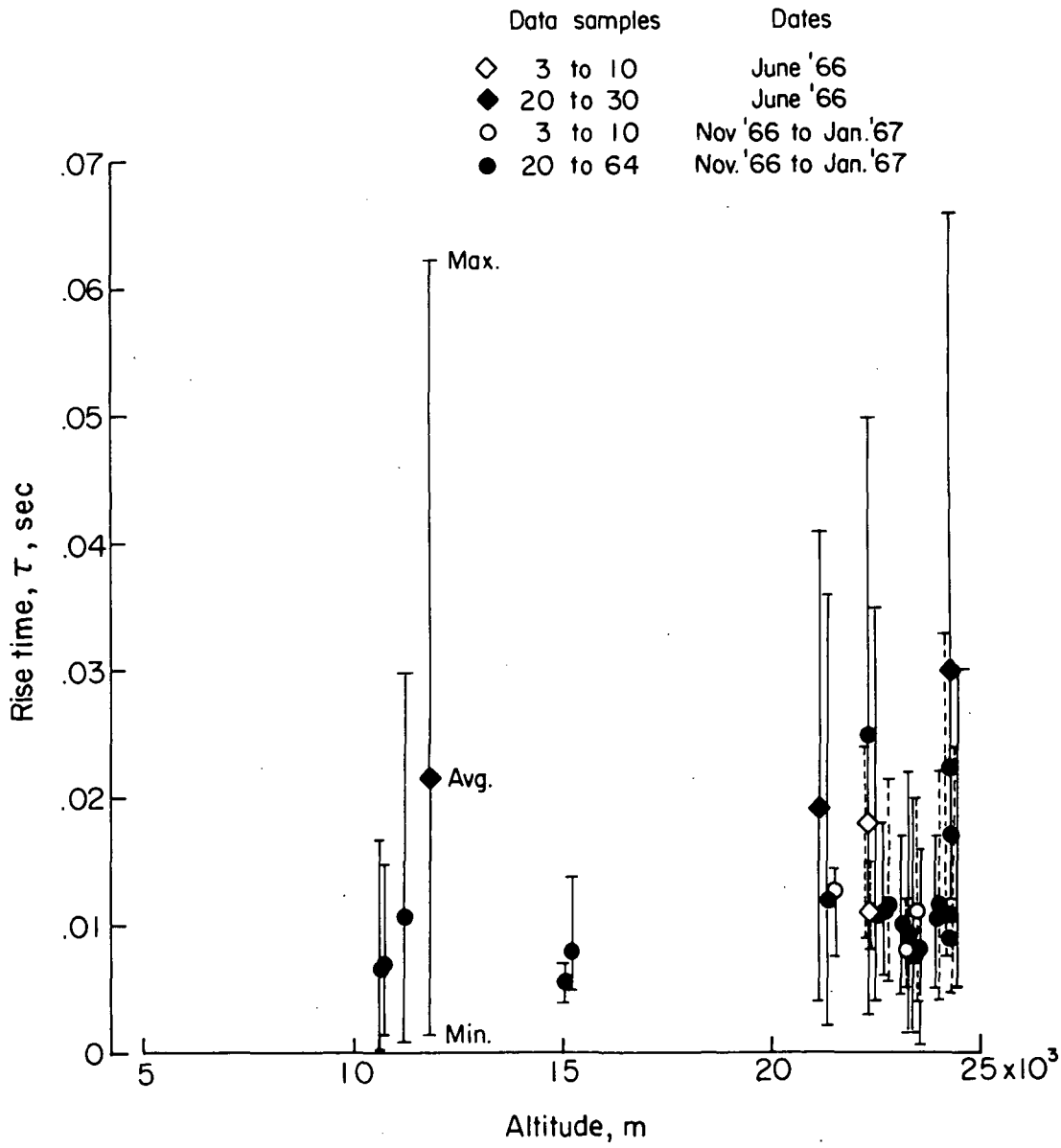


(c) Rise time to half amplitude.

Figure 16.- Concluded.

Variation of Rise Time and Altitude

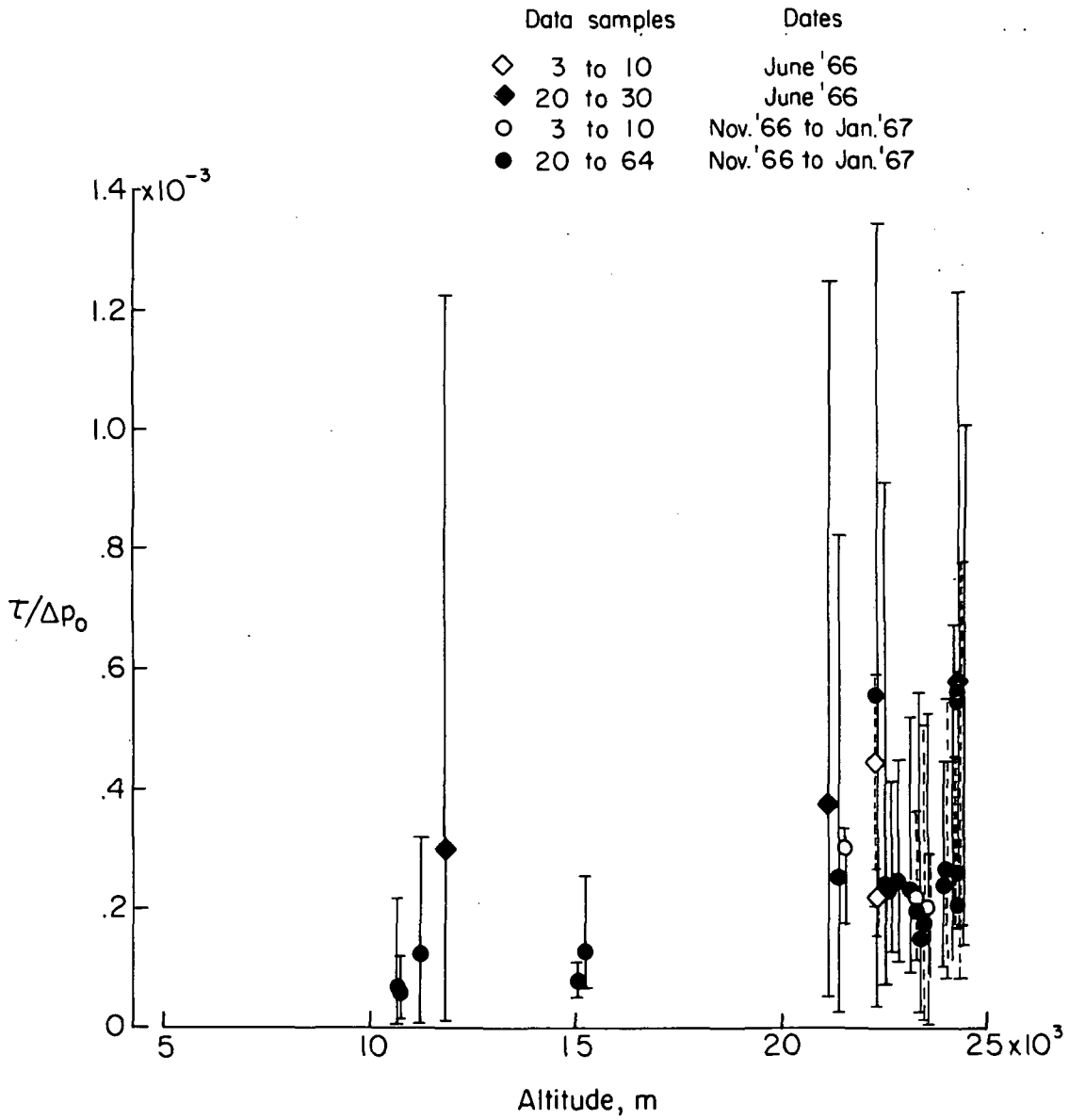
Since the rise time of the wave is a significant factor in the subjective response to sonic booms an evaluation of this parameter was made for the range of flight conditions encountered. These data are presented in figure 17 in terms of the variation of the bow-wave rise times as a function of altitude for measurements made within 5.5 kilometers of the ground track. The data symbols represent the average values of the measurements



(a) Rise time τ to maximum amplitude.

Figure 17.- Variation of bow-wave rise time to peak value of overpressure as measured from flights within 5.5 km of ground track as a function of altitude. Data symbols represent average values for each flight along with maximum and minimum values observed.

and the vertical lines indicate the extreme spread of the data observed for each particular flight. Shown in figure 17(a) are the absolute values of rise time to maximum amplitude and in figure 17(b) the rise time per unit overpressure. It can be seen from the figures that there is considerable scatter, but, in general, the rise times increase as the altitude of the aircraft increases. These results are similar to those obtained for other aircraft (see fig. 17 of ref. 7 and fig. 5 of ref. 16). There is, therefore, the suggestion that the increased altitude results generally in longer rise times.



(b) Rise time τ per unit overpressure.

Figure 17.- Concluded.

CONCLUDING REMARKS

Sonic-boom measurements have been obtained from 35 flights of the SR-71 and F-12 aircraft at altitudes from 10 620 to about 24 400 meters and Mach numbers 1.35 to 3.0, respectively. No unusual phenomena regarding overpressure variations with altitude and lateral distance or the variability of sonic-boom signature waveform due to atmospheric nonuniformities in the lower atmosphere were encountered for the high-altitude and high-Mach-number range of these tests. The experimental results fit generally into the established patterns of other available sonic-boom flight data from F-104, B-58, and XB-70 aircraft and also correlate very well with current prediction methods utilizing existing theory.

Langley Research Center,
National Aeronautics and Space Administration,
Hampton, Va. June 30, 1972.

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TABLE I.- SUMMARY OF AIRPLANE OPERATING CONDITIONS

Date	Mission number (a)	Time when aircraft was overhead or abreast of Tango, GMT	Altitude, m (from MSL)	Mach number	True heading, deg	Site 9 distance from flight track, km	Ground speed, m/sec	Remarks
1-17-67	SR-30	1950:07	10 668	1.4	265.0	0.20 S	381	
1-17-67	SR-31	2000:27	10 668	1.4	265.5	0.20 S	381	
12-1-66	SR-9	1953:52	11 217	1.35	84.0	5.00 S	418	Climb acceleration with chase aircraft
6-9-66	SR-a	2148:48	11 887	1.90	226.0	2.78 N	518	Slight descent and deceleration
11-3-66	SR-1	1956:08	12 192	1.53	82.3	16.48 S	482	Slight climb and acceleration
1-10-67	SR-28	2028:11	15 088	1.92	226.7	0.46 S	524	
12-13-66	SR-18	2203:00	15 240	1.99	300.0	0	518	No radar – pilot report only
11-3-66	SR-2	2030:16	19 861	2.12	242.0	17.96 S	610	
6-13-66	SR-b	2059:50	21 245	2.55	227.0	2.31 N	768	
12-1-66	SR-11	2042:27	21 443	2.50	273.6	6.85 S	732	
12-13-66	SR-17	2050:30	21 580	2.40	284.0	29.08 S	695	Aircraft in slight turn
12-8-66	SR-13	2032:27	22 311	2.94	151.0	32.97 N	866	
6-23-66	SR-F-2	1712:24	22 342	3.00	93.5	0.24 N	917	
12-8-66	SR-12	1847:09	22 357	2.94	308.2	3.89 S	869	
6-23-66	SR-F-1	1655:23	22 372	3.00	275.0	1.19 S	911	
12-12-66	SR-15	2334:29	22 586	3.00	298.0	3.89 S	872	
12-13-66	SR-16	2019:22	22 769	3.00	298.0	0.17 N	872	
12-9-66	SR-14	2148:14	22 890	3.00	298.2	1.67 S	884	
12-16-66	SR-19	2027:09	23 226	3.00	299.0	0.35 S	876	
12-16-66	SR-20	2216:27	23 317	2.95	298.0	9.26 N	860	
1-13-67	SR-29	2124:31	23 363	3.00	227.6	4.35 S	893	
12-1-66	SR-10	2025:17	23 500	3.00	274.0	5.19 N	887	
11-30-66	SR-8	2039:23	23 591	3.00	304.0	5.37 N	887	
11-28-66	SR-5	2311:01	23 591	3.00	298.0	2.44 S	887	
11-17-66	SR-3	2055:30	23 985	3.00	228.0	21.67 S	884	
12-19-66	SR-22	2040:51	24 049	3.00	228.2	3.70 S	884	
11-29-66	SR-6	2028:34	24 067	3.00	227.5	5.09 S	884	
12-16-66	SR-21	2406:08	24 277	3.00	298.0	19.63 N	872	
6-13-66	SR-c	2243:57	24 384	3.00	227.0	0	902	
6-22-66	SR-d	1954:45	24 384	3.00	78.0	7.41 N	900	
11-29-66	SR-7	2254:06	24 384	3.00	263.0	4.44 N	884	
12-20-66	SR-23	2138:01	24 384	2.93	309.5	4.67 S	884	
12-21-66	SR-24	1844:11	24 384	3.00	308.0	5.09 S	881	
12-21-66	SR-25	2103:29	24 384	3.00	262.5	4.07 N	882	
1-6-67	SR-27	2103:36	24 384	3.00	298.0	4.82 S	867	

[a]The SR-71 aircraft was used for missions designated SR and the F-12 was used for missions designated SR-F.

TABLE II.- SUMMARY OF WEATHER DATA

(a) Atmospheric pressure

Altitude, m	Atmospheric pressure, millibars, for following times –																					
	6-9-66 1645 GMT	6-13-66 2030 GMT	6-22-66 1530 GMT	6-23-66 1925 GMT	11-3-66 1755 GMT	11-17-66 1805 GMT	11-28-66 1905 GMT	11-29-66 2131 GMT	11-30-66 1700 GMT	12-1-66 2035 GMT	12-8-66 1937 GMT	12-9-66 1730 GMT	12-12-66 1740 GMT	12-13-66 1830 GMT	12-16-66 1630 GMT	12-19-66 1748 GMT	12-20-66 1649 GMT	12-21-66 1705 GMT	1-4-67 2000 GMT	1-6-67 1820 GMT	1-10-67 1115 GMT	1-13-67 1748 GMT	1-17-67 1143 GMT
732	927	933	928	924	932	935	936	937	938	930	933	941	941	939	942	939	933	931	939	942	946	937	938
1 219	875	883	876	873	880	882	882	883	885	878	879	885	887	884	887	884	879	877	884	886	891	881	883
1 829	815	824	815	813	819	820	821	821	823	816	816	822	824	822	824	822	816	815	821	822	828	818	821
2 438	758	768	759	756	761	761	763	764	764	758	757	762	766	764	765	763	758	756	762	762	769	759	761
3 048	704	715	706	703	707	707	709	709	710	704	702	708	711	709	710	709	704	700	708	706	713	704	706
3 658	653	665	655	653	656	655	658	658	659	653	651	655	659	657	658	657	652	649	656	655	662	652	655
4 267	604	617	608	606	608	606	610	610	611	606	603	607	610	609	610	609	604	600	609	606	613	603	606
4 877	559	572	564	562	562	561	565	564	567	561	557	561	564	564	564	563	559	554	563	560	568	557	560
5 486	516	530	522	520	520	518	523	522	524	519	515	519	521	520	521	520	516	511	520	517	525	514	517
6 096	476	490	483	481	479	478	483	482	484	479	475	478	481	480	481	481	476	471	480	476	485	474	476
6 706	440	452	446	444	442	441	446	445	447	442	439	440	442	442	444	443	439	433	442	439	439	437	439
7 315	405	417	412	409	406	406	411	410	412	407	404	406	407	407	408	408	404	398	407	404	413	402	403
7 925	372	384	380	377	373	373	379	377	379	374	371	373	373	374	375	375	371	365	375	372	380	370	369
8 534	342	353	350	347	343	342	348	346	348	343	341	343	342	343	345	345	341	334	344	340	349	340	338
9 144	314	324	322	319	314	313	319	317	319	314	313	314	313	314	316	316	313	306	316	311	320	312	309
9 754	287	297	295	292	286	286	292	290	292	287	286	287	285	287	288	289	286	280	289	284	293	285	282
10 363	262	271	271	267	261	261	267	265	266	262	261	262	260	261	263	264	261	255	264	259	267	260	257
10 972	239	248	248	244	237	238	244	242	243	238	238	239	236	238	239	241	238	233	240	236	244	237	233
11 582	218	226	226	223	216	217	222	220	221	217	217	218	214	216	217	219	217	212	219	214	222	215	212
12 192	197	205	206	203	197	197	202	200	200	197	197	198	194	196	197	200	197	192	199	193	201	194	192
12 802	180	186	187	184	179	179	183	181	182	178	179	179	176	177	179	181	179	175	180	176	183	176	175
13 411	164	169	170	167	163	163	166	164	165	161	162	162	159	160	161	165	162	159	163	159	166	159	159
14 021	149	153	154	152	148	148	150	149	149	147	147	147	145	145	146	149	147	145	148	145	150	144	144
14 630	135	139	140	137	134	134	136	135	135	133	133	133	131	131	132	135	133	131	134	132	136	130	131
15 240	123	126	126	124	122	122	123	122	122	120	121	121	119	119	120	122	121	119	121	120	123	118	118
15 850	112	114	114	113	110	111	111	111	111	108	109	109	108	108	108	110	109	108	110	109	111	107	107
16 459	102	103	103	102	100	100	---	100	100	---	99	98	98	98	98	99	98	98	99	---	101	96	97
17 069	92	94	94	92	90	---	---	90	90	---	90	89	88	89	89	90	89	88	89	---	90	87	88
17 678	83	85	85	83	82	---	---	81	81	---	81	80	80	80	80	81	80	80	80	---	82	79	79
18 288	76	77	77	76	74	---	---	74	74	---	74	72	72	72	73	73	72	72	73	---	74	71	72
18 898	69	70	70	68	67	---	---	67	67	---	67	66	66	66	66	66	65	66	66	---	67	65	65
19 507	62	64	64	62	61	---	---	60	60	---	61	59	59	59	59	60	59	59	60	---	60	58	59
20 117	57	57	58	56	55	---	---	55	55	---	55	54	54	54	54	54	54	54	54	---	54	53	54
20 726	52	52	53	51	50	---	---	49	50	---	50	49	49	49	49	49	48	49	49	---	49	48	48
21 336	47	48	48	47	45	---	---	45	45	---	46	44	44	45	45	45	44	44	45	---	45	44	44
21 946	43	44	44	43	41	---	---	41	41	---	42	40	40	40	40	40	40	40	41	---	41	40	40
22 555	39	39	40	39	37	---	---	37	37	---	38	36	36	36	36	36	36	36	37	---	37	36	36
23 164	35	36	36	35	34	---	---	34	34	---	34	33	33	33	33	33	33	33	34	---	34	33	33
23 774	32	33	33	32	31	---	---	31	31	---	32	---	30	30	30	30	30	30	31	---	31	30	30
24 384	29	30	30	29	28	---	---	28	28	---	29	---	27	27	27	27	27	27	28	---	28	27	27
24 994	27	27	27	27	26	---	---	25	25	---	26	---	25	25	25	25	24	25	25	---	25	24	25

TABLE II.- SUMMARY OF WEATHER DATA – Continued

(b) *Temperature*

Altitude, m	Temperature, °C, for following times –																					
	6-9-66 1645 GMT	6-13-66 2030 GMT	6-22-66 1530 GMT	6-23-66 1925 GMT	11-3-66 1755 GMT	11-17-66 1805 GMT	11-28-66 1905 GMT	11-29-66 2131 GMT	11-30-66 1700 GMT	12-1-66 2035 GMT	12-8-66 1937 GMT	12-9-66 1730 GMT	12-12-66 1740 GMT	12-13-66 1830 GMT	12-16-66 1630 GMT	12-19-66 1748 GMT	12-20-66 1649 GMT	12-21-66 1705 GMT	1-4-67 2000 GMT	1-6-67 1820 GMT	1-10-67 1115 GMT	1-13-67 1748 GMT	1-17-67 1143 GMT
732	24.2	36.3	20.2	29.1	19.1	18.4	17.1	18.9	9.8	20.5	12.2	5.0	6.7	7.2	4.7	8.9	4.7	10.0	9.1	7.4	-2.9	8.1	5.9
1219	19.1	29.8	16.7	20.8	18.4	12.5	12.4	12.0	13.2	14.4	7.0	5.6	9.3	9.7	8.9	10.7	9.4	9.8	7.6	2.9	9.1	7.9	9.2
1829	15.1	24.6	15.8	16.8	14.5	8.1	12.6	13.9	11.0	9.7	2.7	4.2	9.8	12.6	6.0	8.4	11.2	6.3	8.3	.9	8.1	4.2	5.2
2438	11.1	18.7	13.8	12.3	10.0	7.2	9.2	10.4	8.1	8.5	5.9	6.8	9.0	8.3	8.0	9.8	6.9	2.0	6.9	1.0	6.9	1.9	2.8
3048	4.9	12.7	11.0	9.6	5.2	2.8	7.5	5.9	8.9	6.1	3.1	2.2	5.2	3.9	3.9	6.0	3.4	-2.3	4.8	1.5	4.6	-1.9	2.0
3658	-1.2	7.7	5.9	5.9	.8	-1.3	3.5	1.2	5.9	2.6	-1.0	-2.6	.1	-.6	.2	.1	-.8	-4.8	1.9	-2.4	1.6	-4.5	-2.2
4267	-6.0	2.5	2.3	2.2	-3.9	-6.4	-1.3	-1.5	2.0	-.2	-6.1	-6.8	-5.1	-2.6	-5.2	-5.5	-5.1	-9.4	-3.3	-7.4	-1.8	-7.6	-6.5
4877	-9.5	-.8	-.8	-.6	-7.6	-8.1	-4.1	-5.0	-3.2	-3.8	-9.4	-9.6	-10.0	-11.1	-9.0	-7.4	-9.5	-13.5	-9.5	-11.2	-5.3	-11.5	-11.0
5486	-13.2	-5.1	-3.9	-5.9	-12.4	-11.7	-8.4	-8.5	-7.9	-8.6	-11.5	-13.5	-14.8	-12.9	-10.4	-11.6	-13.7	-17.8	-12.2	-15.0	-9.5	-14.5	-15.8
6096	-15.8	-9.7	-8.2	-10.9	-16.3	-16.5	-12.3	-13.4	-12.7	-13.4	-16.2	-17.9	-19.2	-16.5	-14.9	-15.1	-17.6	-22.3	-15.5	-17.3	-12.8	-18.8	-20.6
6706	-18.4	-14.3	-11.6	-14.4	-21.2	-19.5	-16.6	-18.3	-18.4	-18.2	-20.1	-19.8	-24.4	-20.7	-19.0	-19.5	-21.9	-26.9	-18.2	-21.2	-16.7	-21.7	-25.7
7315	-22.0	-19.1	-15.6	-17.8	-25.7	-25.2	-19.9	-22.3	-22.1	-23.2	-22.6	-23.1	-29.3	-25.5	-24.1	-23.3	-25.6	-32.0	-21.9	-25.7	-22.1	-22.7	-31.1
7925	-26.2	-23.9	-18.8	-22.1	-31.0	-30.9	-24.1	-27.3	-26.4	-30.3	-27.5	-28.1	-33.4	-30.8	-29.5	-27.7	-27.4	-35.8	-26.4	-31.3	-26.6	-23.7	-36.4
8534	-30.3	-28.8	-23.8	-26.9	-36.3	-35.5	-34.1	-32.4	-32.0	-38.7	-31.7	-33.5	-38.5	-35.5	-34.8	-32.9	-31.0	-37.3	-32.1	-36.9	-31.3	-26.1	-41.7
9144	-35.5	-33.9	-28.8	-31.9	-41.8	-40.2	-35.5	-37.5	-37.3	-41.1	-36.7	-38.7	-43.7	-40.6	-40.3	-37.8	-35.2	-40.3	-37.2	-42.4	-36.3	-39.2	-44.7
9754	-40.8	-38.8	-33.9	-36.7	-46.8	-44.2	-37.2	-42.4	-42.7	-43.5	-41.6	-42.3	-49.1	-46.1	-45.5	-41.6	-40.5	-42.9	-42.2	-47.9	-41.5	-47.9	-48.9
10363	-46.3	-43.2	-37.7	-41.4	-51.6	-47.3	-42.5	-47.4	-48.1	-48.5	-45.1	-45.5	-54.6	-51.9	-50.5	-45.3	-46.2	-47.5	-46.8	-53.5	-46.8	-52.6	-53.3
10973	-51.6	-47.8	-43.2	-45.9	-50.6	-50.8	-48.2	-51.5	-53.0	-53.7	-49.9	-50.8	-59.7	-57.2	-55.4	-49.9	-51.7	-50.1	-51.2	-58.2	-52.0	-57.3	-57.5
11582	-55.7	-52.8	-48.1	-50.3	-52.1	-54.4	-53.7	-55.7	-56.8	-59.1	-54.7	-56.2	-61.3	-62.2	-58.9	-52.7	-53.8	-53.4	-56.1	-61.5	-55.3	-61.9	-57.9
12192	-54.2	-56.5	-52.2	-55.4	-54.6	-56.6	-58.1	-59.9	-59.5	-61.4	-55.2	-61.2	-61.3	-64.6	-62.5	-55.1	-57.6	-55.1	-59.9	-63.0	-58.4	-66.5	-56.9
12802	-52.5	-60.2	-55.9	-58.4	-56.6	-57.5	-61.5	-60.3	-62.2	-63.8	-60.4	-63.3	-61.4	-67.6	-67.4	-58.5	-58.6	-55.8	-60.9	-58.9	-60.3	-67.0	-57.2
13411	-54.4	-60.1	-59.7	-60.9	-56.9	-56.2	-65.0	-59.4	-61.9	-60.8	-64.8	-62.7	-61.5	-64.3	-65.6	-61.3	-61.3	-57.2	-61.1	-58.4	-61.5	-65.8	-59.3
14021	-56.2	-62.0	-63.5	-62.4	-58.9	-58.6	-66.8	-62.0	-62.4	-62.7	-65.9	-62.7	-61.7	-62.6	-67.2	-64.8	-64.7	-58.9	-64.2	-55.7	-65.1	-67.8	-62.0
14630	-57.9	-62.3	-66.7	-63.8	-60.1	-59.5	-68.2	-64.7	-65.6	-65.8	-64.0	-64.9	-62.3	-62.5	-65.2	-68.1	-68.5	-61.5	-66.2	-58.6	-66.1	-63.2	-62.7
15240	-58.5	-60.9	-64.8	-66.2	-62.1	-59.6	-70.0	-67.0	-68.7	-68.9	-61.2	-67.7	-62.9	-63.3	-66.0	-67.7	-69.0	-64.0	-68.8	-56.1	-67.2	-66.1	-63.6
15850	-58.8	-62.3	-65.2	-66.8	-62.8	-61.1	-73.6	-69.2	-69.5	-69.5	-61.3	-70.1	-63.5	-62.2	-65.8	-70.6	-72.9	-63.3	-70.4	-56.5	-68.3	-66.6	-64.5
16459	-59.0	-63.7	-65.1	-66.8	-65.2	-67.1	----	-69.4	-70.4	----	-64.6	-72.4	-64.1	-65.9	-64.6	-72.8	-74.1	-64.9	-70.7	----	-71.2	-65.0	-65.6
17069	-59.3	-64.0	-62.8	-65.6	-65.1	----	----	-71.9	-69.8	----	-63.9	-70.7	-65.5	-65.7	-65.3	-71.7	-69.4	-65.6	-71.1	----	-71.6	-67.1	-66.2
17678	-59.6	-62.0	-61.6	-63.2	-64.3	----	----	-68.5	-67.2	----	-64.7	-68.4	-68.0	-65.1	-66.8	-69.4	-68.0	-65.2	-67.9	----	-71.8	-67.5	-65.6
18288	-59.8	-61.4	-60.9	-63.0	-64.8	----	----	-67.8	-64.6	----	-62.3	-68.0	-64.4	-64.5	-66.0	-68.5	-67.3	-64.9	-66.9	----	-72.0	-66.9	-65.7
18898	-59.5	-60.3	-58.2	-58.8	-64.7	----	----	-63.3	-64.1	----	-59.8	-66.8	-63.6	-63.4	-64.2	-67.7	-67.0	-61.5	-65.9	----	-71.5	-64.6	-63.4
19507	-56.5	-58.0	-57.0	-58.4	-63.7	----	----	-65.4	-65.3	----	-56.6	-65.6	-62.8	-62.3	-63.4	-66.9	-65.3	-63.5	-64.9	----	-70.0	-63.9	-64.6
20117	-56.2	-58.4	-55.9	-57.1	-61.8	----	----	-64.0	-65.0	----	-55.6	-63.5	-62.0	-61.4	-63.4	-65.5	-63.7	-62.6	-60.4	----	-65.4	-62.8	-61.4
20726	-55.9	-56.3	-54.7	-55.7	-59.2	----	----	-62.7	-63.6	----	-53.8	-61.4	-61.3	-61.3	-62.3	-62.4	-64.9	-61.7	-59.7	----	-60.8	-60.8	-59.7
21336	-55.6	-55.2	-51.6	-55.4	-60.1	----	----	-61.4	-61.1	----	-52.1	-60.1	-60.5	-61.3	-61.8	-63.2	-65.1	-60.8	-57.9	----	-59.4	-58.8	-58.6
21946	-55.3	-54.9	-52.3	-55.7	-57.7	----	----	-60.1	-58.6	----	-50.5	-56.6	-59.7	-61.2	-60.7	-62.3	-64.0	-59.9	-55.9	----	-58.4	-61.0	-57.9
22595	-55.0	-54.6	-51.2	-53.6	-55.1	----	----	-59.6	-56.2	----	-49.4	-54.8	-59.0	-60.1	-61.1	-61.2	-62.9	-59.0	-56.2	----	-60.1	-59.6	-57.3
23165	-54.7	-53.2	-50.1	-51.6	-53.7	----	----	-57.1	-55.5	----	-48.3	-55.7	-58.2	-58.9	-60.0	-60.1	-60.9	-58.1	-55.4	----	-58.2	-57.4	-56.4
23774	-52.2	-50.8	-49.0	-50.1	-53.4	----	----	-56.2	-55.3	----	-47.1	----	-57.4	-57.7	-58.9	-58.8	-58.9	-58.4	-54.4	----	-56.3	-57.0	-55.5
24384	-49.6	-50.2	-49.0	-49.6	-53.0	----	----	-55.7	-53.5	----	-46.0	----	-56.7	-56.9	-59.3	-57.9	-57.0	-58.7	-53.5	----	-54.5	-58.5	-54.7
24994	-46.9	-47.5	-47.2	-49.2	-50.1	----	----	-55.1	-51.8	----	-45.4	----	-55.9	-57.5	-57.9	-57.8	-58.0	-57.3	-52.5	----	-53.5	-55.0	-54.2

TABLE II.- SUMMARY OF WEATHER DATA – Continued

(c) Speed of sound

Altitude, m	Speed of sound, m/sec, for following times –																					
	6-9-66 1645 GMT	6-13-66 2030 GMT	6-22-66 1530 GMT	6-23-66 1925 GMT	11-3-66 1755 GMT	11-17-66 1805 GMT	11-28-66 1905 GMT	11-29-66 2131 GMT	11-30-66 1700 GMT	12-1-66 2035 GMT	12-8-66 1937 GMT	12-9-66 1730 GMT	12-12-66 1740 GMT	12-13-66 1830 GMT	12-16-66 1630 GMT	12-19-66 1748 GMT	12-20-66 1649 GMT	12-21-66 1705 GMT	1-4-67 2000 GMT	1-6-67 1820 GMT	1-10-67 1115 GMT	1-13-67 1748 GMT	1-17-67 1143 GMT
732	346	353	344	349	343	343	342	343	338	344	339	335	336	336	334	337	335	338	337	336	330	336	335
1 219	343	349	341	344	343	340	339	339	340	340	336	335	337	337	337	338	337	337	336	333	337	336	337
1 829	341	346	341	341	340	336	340	340	338	337	333	334	337	339	335	336	338	335	336	332	336	334	335
2 438	338	343	340	339	337	336	337	338	336	336	335	336	337	336	336	337	336	333	336	332	336	333	333
3 048	335	339	338	337	335	333	336	335	337	335	333	333	335	334	334	335	333	330	334	332	334	330	333
3 658	331	336	335	335	332	330	334	332	335	333	331	330	331	331	332	331	331	328	332	330	332	329	330
4 267	328	333	333	333	329	327	331	330	333	331	328	327	328	330	328	328	328	326	329	327	330	327	327
4 877	326	331	331	331	327	326	329	328	329	329	326	326	325	325	326	327	326	323	326	325	328	324	325
5 486	323	329	329	328	324	324	326	326	326	326	324	323	322	323	325	324	323	320	324	322	326	322	322
6 096	322	326	326	325	321	321	324	323	323	323	321	320	319	321	322	322	320	318	322	321	323	320	319
6 706	320	322	324	322	318	319	321	320	320	320	319	319	316	319	319	319	318	315	320	318	321	318	315
7 315	318	319	322	320	315	316	319	318	318	317	317	317	313	315	316	317	315	311	318	315	318	317	312
7 925	315	316	320	318	312	312	316	314	315	312	314	314	310	312	313	314	314	309	315	312	315	317	308
8 534	312	313	317	315	308	309	310	311	311	307	312	310	307	309	309	311	312	308	311	308	312	315	305
9 144	309	310	313	312	305	306	309	308	308	305	308	307	304	306	306	308	309	306	308	304	308	307	303
9 754	305	307	310	308	301	303	308	304	304	304	305	304	300	302	302	305	306	304	305	301	305	301	300
10 363	302	304	308	305	298	301	304	301	301	301	303	302	296	298	299	303	302	301	301	297	301	298	297
10 972	298	301	304	302	299	299	301	298	297	297	300	299	293	294	296	299	298	299	299	294	298	294	294
11 582	296	297	301	299	298	296	297	296	295	293	296	295	292	291	294	297	297	297	295	292	296	291	294
12 192	297	295	298	296	296	295	294	293	293	292	296	292	292	290	291	296	294	296	293	290	294	288	295
12 802	298	293	295	294	295	294	292	292	291	290	292	290	292	287	287	294	294	296	292	294	292	288	294
13 411	297	293	293	292	295	295	289	293	291	292	289	291	292	290	289	292	292	294	292	294	292	289	293
14 021	295	291	290	291	293	294	288	291	291	291	289	291	291	291	288	289	289	294	290	296	289	287	291
14 630	294	291	288	290	293	293	287	290	289	289	290	289	291	291	289	287	287	292	288	294	288	290	291
15 240	294	292	289	288	291	293	286	288	287	287	292	287	291	290	288	287	287	290	287	295	288	288	290
15 850	294	291	289	288	291	292	283	286	286	286	292	286	290	291	289	285	284	290	285	295	287	288	290
16 459	293	290	289	288	289	288	---	286	285	---	290	284	290	289	290	---	---	289	---	---	---	289	289
17 069	293	290	291	289	289	---	---	284	286	---	290	285	289	289	289	285	286	289	285	---	285	288	288
17 678	293	291	291	290	290	---	---	287	288	---	289	287	287	289	288	286	287	289	287	---	284	287	289
18 288	293	292	292	290	289	---	---	287	290	---	291	287	290	290	289	287	288	289	288	---	284	288	289
18 898	293	293	294	294	290	---	---	290	290	---	293	289	290	290	290	287	288	292	289	---	285	290	290
19 507	295	294	295	294	290	---	---	289	289	---	295	290	291	291	290	288	289	290	289	---	286	290	290
20 117	295	294	295	295	291	---	---	290	289	---	296	292	291	292	290	289	290	291	292	---	289	291	292
20 726	295	295	296	296	293	---	---	291	290	---	297	293	292	292	291	291	289	291	293	---	292	292	293
21 336	296	296	298	296	293	---	---	292	292	---	298	295	293	292	291	290	289	292	294	---	293	294	294
21 946	296	296	298	296	294	---	---	293	294	---	299	296	293	292	292	291	290	293	295	---	294	292	294
22 555	296	296	299	297	296	---	---	293	295	---	300	296	293	293	292	292	291	293	295	---	293	293	294
23 164	296	297	299	298	297	---	---	295	296	---	301	294	294	294	293	293	292	294	296	---	294	294	295
23 774	298	299	300	299	297	---	---	295	296	---	301	---	294	294	293	294	294	294	297	---	295	295	296
24 384	300	299	300	300	297	---	---	296	297	---	302	---	295	295	293	294	295	294	297	---	297	294	296
24 994	301	301	301	300	299	---	---	296	298	---	303	---	295	294	294	294	294	294	298	---	297	296	297

TABLE II.- SUMMARY OF WEATHER DATA – Continued

(d) Wind speed

Altitude, m	Wind speed, knots, for following times –																					
	6-9-66 1645 GMT	6-13-66 2030 GMT	6-22-66 1530 GMT	6-23-66 1925 GMT	11-3-66 1755 GMT	11-17-66 1805 GMT	11-28-66 1905 GMT	11-29-66 2131 GMT	11-30-66 1700 GMT	12-1-66 2035 GMT	12-8-66 1937 GMT	12-9-66 1730 GMT	12-12-66 1740 GMT	12-13-66 1830 GMT	12-16-66 1630 GMT	12-19-66 1748 GMT	12-20-66 1649 GMT	12-21-66 1705 GMT	1-4-67 2000 GMT	1-6-67 1820 GMT	1-10-67 1115 GMT	1-13-67 1748 GMT	1-17-67 1143 GMT
732	5.0	6.0	18.0	20.0	2.0	12.0	6.0	3.0	0	13.0	10.0	2.0	2.0	3.0	2.0	4.0	2.0	3.0	2.0	5.0	3.0	4.0	4.0
1 219	6.3	8.6	19.6	27.7	8.4	16.2	10.3	5.6	8.4	19.8	7.8	10.1	5.8	1.8	2.7	6.5	1.1	12.9	3.0	10.3	9.7	4.1	0
1 829	6.5	12.5	15.2	16.4	7.4	15.9	31.0	16.8	13.8	19.6	15.9	12.0	12.6	13.3	9.0	9.9	5.0	9.5	10.2	17.6	15.8	14.3	0
2 438	1.7	16.2	20.5	20.7	4.6	16.6	40.9	20.6	9.9	22.5	29.9	8.3	5.5	16.0	7.4	11.4	10.5	4.8	9.2	27.1	14.9	18.1	0
3 048	4.9	16.7	20.9	17.6	4.5	22.3	42.4	24.3	8.1	31.8	42.9	21.8	2.8	15.7	5.6	12.7	10.8	2.4	10.0	32.4	7.3	9.4	0
3 658	7.2	7.8	21.9	17.3	6.6	22.6	41.2	27.5	9.2	37.4	44.3	28.2	7.0	12.8	10.0	12.4	14.0	6.1	15.2	35.2	7.7	17.5	0
4 267	9.2	5.2	27.3	31.6	11.7	21.6	39.7	25.2	11.5	42.3	48.8	31.3	11.3	16.9	14.1	10.7	14.3	10.8	25.1	33.2	12.9	17.3	12.6
4 877	16.7	8.4	35.1	31.1	15.2	29.2	42.1	28.7	13.1	38.7	61.7	35.0	5.6	18.9	15.3	13.3	10.4	13.1	27.8	28.8	14.4	26.2	16.1
5 486	24.5	3.5	41.8	27.1	14.7	39.0	44.1	30.3	16.1	39.9	70.3	43.1	6.9	17.8	5.6	18.9	15.7	14.2	27.6	37.2	16.2	39.4	20.9
6 096	24.7	3.9	47.3	38.2	19.8	45.2	44.0	29.5	18.3	43.4	72.6	55.2	15.5	19.3	3.1	23.2	25.5	21.1	30.3	57.5	23.0	46.7	25.4
6 706	23.1	5.0	59.6	42.4	22.2	48.1	45.9	33.7	20.0	45.8	76.1	59.0	24.9	18.8	5.7	24.2	24.8	27.1	30.1	64.0	28.0	48.7	27.8
7 315	26.2	7.3	66.3	42.6	25.5	49.9	49.0	38.3	22.6	48.2	79.2	58.1	22.9	16.7	10.5	23.7	22.7	35.0	29.8	66.9	33.9	49.0	30.1
7 925	29.5	9.2	69.0	41.3	29.4	52.2	49.1	41.5	25.1	50.8	83.8	54.1	23.5	15.0	16.7	23.3	21.3	42.3	30.4	67.7	39.0	49.7	33.0
8 534	29.7	10.4	65.4	40.4	31.6	58.0	65.4	42.6	27.6	50.8	99.3	57.9	22.4	16.0	21.9	22.4	15.7	47.4	32.0	66.7	41.0	49.9	36.5
9 144	27.1	10.3	73.7	42.1	32.7	65.8	75.6	45.3	29.4	51.1	101.1	69.5	29.1	18.6	26.2	24.8	16.1	48.2	33.3	65.9	41.2	47.5	39.9
9 754	25.0	9.6	95.4	45.2	34.1	72.4	86.8	48.4	30.3	54.9	88.9	79.0	30.9	21.6	30.2	26.8	20.4	46.1	37.6	65.0	41.5	43.9	43.9
10 363	24.7	9.7	113.3	49.5	36.0	76.2	85.4	51.5	30.8	60.3	90.5	85.9	34.4	22.6	34.6	28.8	24.9	43.7	43.7	66.2	44.3	42.5	48.8
10 973	27.3	10.7	101.8	53.2	42.4	81.1	81.9	55.5	30.3	64.0	115.9	87.8	37.8	25.4	37.0	25.9	25.6	45.8	49.3	68.8	52.0	45.7	54.7
11 582	35.4	12.0	74.3	53.7	46.5	90.5	83.9	58.3	30.1	60.7	125.9	90.1	40.8	29.7	36.1	21.6	26.1	54.2	50.1	73.8	53.0	48.6	57.0
12 192	42.3	11.6	50.8	53.2	43.9	95.7	83.9	65.0	31.2	63.4	114.9	89.5	42.4	32.1	32.7	19.7	27.3	61.9	48.1	78.5	52.2	49.1	56.0
12 802	44.3	8.7	47.9	54.0	36.7	106.4	75.9	69.9	33.9	68.5	97.0	83.3	42.5	32.2	31.1	17.8	32.6	63.9	49.3	81.7	47.3	58.8	51.1
13 411	41.2	8.6	53.0	63.5	34.5	116.8	66.0	69.6	36.8	76.1	119.8	72.7	45.9	31.5	31.3	16.3	37.1	60.8	53.3	78.7	46.8	48.0	49.8
14 021	38.6	12.0	58.0	67.7	35.0	114.5	60.3	68.7	39.3	73.0	138.6	61.7	43.8	30.2	30.2	10.2	37.9	54.7	57.2	72.7	41.2	46.3	49.0
14 630	34.6	13.3	66.1	70.3	41.3	110.8	56.1	60.5	41.1	66.5	139.8	55.5	45.3	28.5	26.6	11.7	34.4	49.1	56.9	63.1	35.8	42.2	48.2
15 240	30.8	12.8	70.2	43.9	33.2	98.1	---	55.7	41.7	60.9	114.4	54.4	43.3	27.1	22.0	14.6	30.6	43.8	54.0	50.1	26.6	36.8	46.4
15 850	26.6	11.3	69.2	29.3	26.9	78.0	0	45.9	41.2	0	85.4	54.6	40.3	25.7	18.3	12.3	26.7	37.8	49.3	0	25.8	32.0	44.4
16 459	21.9	9.7	64.4	18.0	22.8	0	---	35.9	38.5	---	53.6	54.3	36.9	25.9	15.4	11.5	24.4	31.7	44.8	---	21.5	26.8	40.5
17 069	15.7	7.4	54.6	17.4	23.7	----	---	28.8	32.6	---	25.3	49.2	32.5	22.9	10.5	9.3	21.1	26.8	40.9	---	23.8	22.1	36.3
17 678	6.8	4.7	36.1	14.6	21.4	----	---	26.7	26.2	---	15.4	37.4	28.7	19.7	9.5	6.1	17.1	21.1	37.0	---	23.3	18.4	31.9
18 288	1.6	4.7	24.2	9.5	19.0	----	---	23.5	17.4	---	22.6	28.4	84.8	14.6	7.1	4.2	13.7	15.9	31.9	---	20.6	17.0	27.7
18 898	4.8	6.0	7.5	6.0	15.8	----	---	19.4	12.4	---	14.9	28.5	18.7	12.4	5.7	3.7	9.6	10.6	25.3	---	21.1	14.6	23.3
19 507	4.5	8.2	6.7	0	13.3	----	---	13.7	7.5	---	24.8	30.2	16.0	12.4	5.0	3.1	5.6	5.5	17.9	---	19.3	12.2	20.7
20 117	4.2	11.7	25.1	0	14.1	----	---	8.0	8.6	---	31.0	22.2	14.1	13.7	5.6	5.3	4.7	3.1	11.0	---	20.9	13.3	18.7
20 726	5.0	15.5	34.5	0	12.7	----	---	7.9	12.5	---	35.5	20.2	11.9	14.8	8.5	6.2	4.7	4.5	6.2	---	23.3	14.0	17.3
21 336	5.0	17.7	18.5	0	10.1	----	---	9.9	13.3	---	37.3	10.4	9.8	14.9	9.9	8.1	7.2	5.4	2.9	---	24.6	15.2	18.7
21 946	7.6	19.0	7.4	0	5.7	----	---	10.8	14.0	---	31.5	9.0	5.0	14.7	8.0	8.7	11.1	5.1	4.7	---	24.7	16.1	20.5
22 595	14.0	18.9	5.6	0	3.5	----	---	11.5	13.5	---	19.7	0	11.8	13.5	7.9	9.6	14.9	6.7	9.1	---	25.0	16.3	21.3
23 165	18.8	19.8	27.9	0	1.9	----	---	11.8	15.7	---	13.7	0	12.4	12.8	9.7	11.0	14.6	8.2	14.9	---	25.3	16.9	21.6
23 774	18.9	21.2	37.2	0	.7	----	---	14.0	16.1	---	13.9	---	16.6	11.9	14.2	12.1	11.8	8.6	21.4	---	31.3	17.9	22.2
24 384	19.2	22.8	44.2	0	4.5	----	---	14.2	17.5	---	19.1	---	24.0	11.6	20.0	10.9	8.3	8.3	26.7	---	37.8	19.9	22.1
24 994	15.5	25.0	40.9	0	8.3	----	---	18.6	20.8	---	27.7	---	18.3	16.2	25.1	9.5	5.4	9.0	30.2	---	43.0	23.0	19.2

TABLE II.- SUMMARY OF WEATHER DATA – Concluded

(e) Wind direction

Altitude, m	Wind direction, degrees from true North, for following times –																					
	6-9-66 1645 GMT	6-13-66 2030 GMT	6-22-66 1530 GMT	6-23-66 1925 GMT	11-3-66 1755 GMT	11-17-66 1805 GMT	11-28-66 1905 GMT	11-29-66 2131 GMT	11-30-66 1700 GMT	12-1-66 2035 GMT	12-8-66 1937 GMT	12-9-66 1730 GMT	12-12-66 1740 GMT	12-13-66 1830 GMT	12-16-66 1630 GMT	12-19-66 1748 GMT	12-20-66 1649 GMT	12-21-66 1705 GMT	1-4-67 2000 GMT	1-6-67 1820 GMT	1-10-67 1115 GMT	1-13-67 1748 GMT	1-17-67 1143 GMT
732	270.0	50.0	250.0	270.0	90.0	210.0	180.0	90.9	50.0	210.0	260.0	130.0	120.0	210.0	180.0	190.0	240.0	100.0	90.9	10.0	270.0	210.0	10.0
1 219	294.5	81.5	276.6	266.9	240.2	252.8	219.7	326.3	64.9	259.1	298.8	70.5	47.9	191.2	27.0	66.8	36.1	27.2	90.9	52.3	52.8	8.1	0
1 829	279.2	92.4	321.5	277.4	187.2	266.6	215.6	333.1	96.1	272.8	342.8	107.2	46.8	245.8	86.7	69.0	251.3	20.9	118.6	52.6	67.3	39.5	0
2 438	23.7	96.4	319.3	283.1	208.8	258.6	218.6	329.4	129.9	264.9	332.9	250.0	87.5	240.0	129.0	110.3	243.5	12.0	180.6	34.4	89.2	38.7	0
3 048	73.9	109.3	311.1	271.4	203.0	252.3	221.7	312.3	230.1	254.9	331.1	279.5	95.1	241.3	150.6	116.1	187.6	345.6	238.1	16.8	76.8	351.4	0
3 658	49.0	134.5	294.1	260.4	141.6	232.0	228.3	293.3	249.3	256.8	330.2	275.3	278.1	242.8	174.2	93.0	179.6	239.3	241.8	8.5	5.1	335.8	0
4 267	10.2	132.9	271.5	261.6	159.3	232.8	232.6	291.8	253.9	256.5	327.5	281.4	276.9	242.4	189.6	102.1	204.0	234.2	247.4	358.3	5.4	337.1	297.9
4 877	347.8	82.6	271.7	250.0	168.1	252.5	238.2	296.1	252.0	252.0	327.7	282.9	258.6	213.3	189.9	117.4	216.0	232.6	252.0	335.2	354.4	343.1	310.1
5 486	337.9	127.7	268.5	250.6	172.6	253.2	236.2	293.7	243.4	250.7	322.3	285.0	299.4	218.1	170.3	110.0	236.4	248.5	257.5	309.8	4.0	356.6	301.3
6 096	329.4	166.0	278.3	259.5	185.6	244.2	227.6	297.2	251.8	246.1	314.7	283.0	292.6	248.0	200.4	108.1	230.1	236.7	260.4	298.9	5.1	357.2	298.4
6 706	331.2	132.5	279.7	260.6	187.5	238.5	225.6	297.2	245.6	246.9	313.3	283.7	282.9	248.1	183.3	102.2	220.8	231.9	264.2	296.6	1.2	354.4	298.3
7 315	330.2	134.8	276.1	261.6	192.1	236.1	227.9	301.0	241.3	248.6	311.1	284.8	273.6	241.3	170.2	96.4	192.2	230.0	268.5	293.5	354.8	351.2	298.8
7 925	326.6	131.9	270.9	264.0	197.2	237.8	231.5	294.7	240.6	251.3	309.5	284.5	269.8	239.8	172.5	92.5	175.0	231.6	273.4	290.1	351.1	347.0	300.3
8 534	321.0	126.0	268.5	265.5	202.0	241.2	230.5	292.5	243.6	253.8	311.2	282.1	263.2	251.7	182.3	93.8	199.1	236.7	275.0	286.5	350.8	342.3	300.0
9 144	314.0	122.6	270.7	265.8	203.4	244.3	227.0	283.5	245.5	258.1	311.8	280.7	264.0	268.2	197.1	87.5	243.0	241.4	271.3	282.7	351.2	340.2	295.5
9 754	307.9	129.3	274.9	264.5	204.5	245.2	224.8	285.4	248.3	258.7	310.6	279.4	259.7	274.0	211.3	72.4	266.2	246.0	265.5	276.8	347.0	342.4	290.7
10 363	305.4	134.1	277.3	262.6	208.6	245.1	222.3	282.2	249.2	257.6	316.6	278.9	262.6	276.1	222.7	57.9	275.3	247.9	260.3	274.3	339.7	348.3	289.9
10 973	311.9	130.9	278.5	260.9	219.0	242.9	222.8	276.1	254.9	256.2	312.7	278.6	270.4	272.9	231.2	39.0	272.9	248.1	255.2	275.2	336.7	353.7	291.0
11 582	324.6	126.7	279.1	259.6	228.2	241.3	226.2	268.6	261.6	256.6	313.5	279.4	274.1	273.5	237.2	15.2	256.6	246.0	254.7	278.8	337.1	254.8	291.7
12 192	329.7	130.3	278.7	258.6	231.9	240.3	228.3	264.8	267.8	258.0	306.9	279.3	276.9	271.8	238.8	40.4	236.3	244.3	257.6	281.4	344.1	350.5	291.0
12 802	330.9	156.4	277.6	258.1	235.8	243.4	230.6	263.6	270.0	255.6	307.5	278.8	273.8	271.4	234.4	53.5	227.0	245.6	263.1	283.4	253.4	344.2	291.5
13 411	326.1	204.1	277.1	257.8	231.7	245.2	233.1	263.3	272.2	254.8	304.6	282.2	269.7	274.1	230.5	60.0	222.5	249.5	266.9	285.2	1.1	342.0	289.3
14 021	325.5	234.6	276.2	258.6	241.2	245.9	237.1	264.1	273.5	254.1	300.6	287.3	265.3	282.0	228.9	10.0	226.2	253.9	269.0	287.7	5.9	344.3	287.4
14 630	324.7	245.6	276.1	258.8	238.5	246.3	243.9	265.6	272.6	256.0	300.6	290.5	259.4	290.2	230.8	338.5	226.7	255.9	269.3	289.1	9.5	345.7	287.0
15 240	325.8	255.9	276.0	256.2	255.6	245.1	285.3	269.5	269.9	257.4	300.1	290.2	257.2	295.9	235.1	324.0	231.1	256.0	266.2	291.4	20.7	341.9	287.4
15 850	325.6	255.6	275.7	246.7	267.9	243.0	0	273.6	269.0	0	302.7	288.9	258.0	295.2	243.1	323.1	223.6	255.7	265.4	0	17.2	335.0	288.4
16 459	323.3	239.2	275.1	235.2	282.6	0	----	280.3	271.0	----	303.1	291.3	261.2	293.6	261.6	333.2	219.6	256.5	264.8	----	21.0	331.8	293.1
17 069	322.3	232.1	272.1	238.1	276.3	----	----	272.7	269.2	----	256.4	292.5	266.2	292.4	282.0	7.4	216.9	259.3	267.5	----	15.5	328.2	301.2
17 678	335.7	246.4	269.9	244.1	285.9	----	----	266.8	268.9	----	180.6	294.7	270.5	291.9	292.0	52.1	218.8	259.7	267.6	----	19.9	326.0	308.1
18 288	33.4	322.5	267.4	221.6	299.5	----	----	264.0	266.7	----	182.6	296.1	272.6	286.8	301.3	90.4	227.4	266.5	266.5	----	29.3	322.5	314.6
18 898	79.3	26.1	231.0	228.5	316.0	----	----	276.3	283.7	----	231.2	296.5	275.0	274.5	294.1	109.2	241.6	280.0	266.9	----	29.9	336.7	327.4
19 507	71.2	68.7	139.8	0	334.1	----	----	305.9	317.9	----	277.1	296.0	278.3	267.1	302.1	100.4	276.5	322.5	270.5	----	41.4	349.1	340.3
20 117	72.5	91.4	101.7	0	3.4	----	----	339.4	.7	----	291.6	295.3	289.7	271.9	331.1	79.9	318.4	47.3	280.4	----	46.0	3.3	345.6
20 726	89.9	93.1	101.7	0	24.2	----	----	7.3	31.6	----	295.9	287.0	296.5	283.9	347.2	64.8	359.7	136.2	307.5	----	50.2	8.0	353.2
21 336	100.2	96.8	105.0	0	29.8	----	----	34.6	44.6	----	294.5	249.4	294.5	293.9	343.6	69.4	48.3	142.7	359.0	----	54.9	17.9	13.7
21 946	102.0	94.5	98.9	0	20.8	----	----	55.1	65.5	----	295.6	252.7	291.1	302.7	336.4	58.1	79.1	111.6	38.1	----	55.6	34.8	33.3
22 595	106.5	99.9	84.4	0	5.1	----	----	83.4	71.7	----	283.0	0	280.6	301.5	291.6	51.1	91.0	80.0	45.6	----	53.3	53.0	33.6
23 165	105.9	100.4	91.1	0	336.3	----	----	91.2	75.5	----	239.8	0	281.7	294.7	290.3	53.2	97.7	65.2	41.7	----	50.2	58,0	25.8
23 774	93.0	99.0	92.7	0	277.2	----	----	79.8	71.8	----	212.2	----	281.5	284.7	292.6	52.8	104.0	66.4	41.5	----	53.0	55.1	17.8
24 384	90.9	99.8	92.7	0	224.8	----	----	62.1	78.8	----	222.0	----	275.2	273.0	290.1	62.7	87.6	69.6	46.4	----	57.4	53.9	15.1
24 994	84.6	101.1	91.0	0	216.7	----	----	70.6	78.3	----	249.5	----	268.2	260.2	287.5	73.8	41.3	63.1	51.7	----	60.5	57.5	13.6

TABLE III.- SUMMARY OF SONIC-BOOM DATA FOR SR-71 MISSIONS FLOWN AT EDWARDS AIR FORCE BASE

Date	Mission number	Site	Site distance from flight track, km	Station number	Micro-phone	Δp_o, N/m^2	ΔT, sec	Δt_o, sec	I_o, $N\text{-}sec/m^2$	τ, sec	$\tau_{1/2}$, sec	Type signature (fig. 5)
11-3-66	SR-1	9	16.5 S	V-4	1	65.11	----	----	---	0.030	-----	CO
					2	67.99	----	----	---	.033	-----	CO
					3	67.51	----	----	---	.033	-----	CO
					4	68.47	----	----	---	.035	-----	CO
					5	71.82	----	----	---	.035	-----	CO
				FRC	1	52.67	----	----	---	0.025	-----	CO
					2	63.20	----	----	---	.027	-----	CO
					3	65.12	----	----	---	.031	-----	CO
					4	66.55	----	----	---	.030	-----	CO
					5	56.50	----	----	---	.025	-----	CO
					6	66.07	----	----	---	.035	-----	CO
					7	65.11	----	----	---	.030	-----	CO
					8	66.55	----	----	---	.030	-----	CO
					9	70.38	----	----	---	.028	-----	CO
					10	68.95	----	----	---	.027	-----	CO
					11	69.43	----	----	---	.030	-----	CO
					12	64.64	----	----	---	.030	-----	CO
				Tango	1	87.14	----	----	---	0.047	-----	CO
					2	83.31	----	----	---	.055	-----	CO
					3	88.58	----	----	---	.055	-----	CO
					4	85.23	----	----	---	.046	-----	CO
					5	87.62	----	----	---	.045	-----	CO
					6	85.23	----	----	---	-----	-----	CO
	SR-2	9	18.0 S	V-4	1	41.66	0.194	----	---	0.0130	-----	NR
					2	43.57	.195	----	---	.0135	-----	NR
					3	41.66	.194	----	---	.0160	-----	NR
					4	43.09	.194	----	---	.0175	-----	NR
					5	44.53	.193	----	---	.0105	-----	NP
				FRC	1	63.68	.195	----	---	0.0055	-----	P
					2	48.84	.195	----	---	.0075	-----	NR
					3	42.61	.195	----	---	.0105	-----	NR
					4	40.70	.195	----	---	.0135	-----	NR
					5	33.99	.196	----	---	.0140	-----	NP
					6	47.88	.196	----	---	.0070	-----	P
					7	65.60	.196	----	---	.0060	-----	P
					8	47.88	.196	----	---	.0080	-----	NP
					9	50.75	.195	----	---	.0105	-----	NR
					10	56.02	.195	----	---	.0140	-----	NR
					11	41.18	.195	----	---	.0140	-----	NR
					12	45.01	.195	----	---	.0080	-----	NP
				Tango	1	94.80	.194	----	---	0.0250	-----	--
					2	94.32	.193	----	---	.0150	-----	PR
					3	101.03	.194	----	---	.0100	-----	NP
					4	95.76	.195	----	---	.0155	-----	--
					5	97.68	.194	----	---	.0165	-----	--
					6	39.74	----	----	---	-----	-----	--
11-17-66	SR-3	9	7.4 S	V-1	1	40.22	0.235	----	---	0.0240	-----	NR
					2	40.22	.235	----	---	.0120	-----	NR
					3	40.22	.234	----	---	.0110	-----	NR
		7	37.4 S	V-3	1	28.73	0.215	----	---	0.0200	-----	NR
					2	28.73	.216	----	---	.0095	-----	NR
					3	28.25	.216	----	---	.0055	-----	PP
					4	33.04	.215	----	---	.0045	-----	NP
					5	26.81	.215	----	---	.0145	-----	NR
		9	7.4 S	V-4	1	40.22	.233	----	---	0.0220	-----	NR
					2	49.32	.232	----	---	.0270	-----	NR
					3	40.22	.232	----	---	.0200	-----	NR
					4	41.66	.232	----	---	.0150	-----	NR
					5	42.61	.232	----	---	.0170	-----	NR
		6	22.8 S	V-5	1	52.67	.238	----	---	0.0040	-----	NP
					2	42.61	.237	----	---	.0050	-----	NP
					3	38.78	.236	----	---	.0130	-----	NR
					4	40.22	.236	----	---	.0160	-----	NR
					5	44.53	.235	----	---	.0040	-----	NP
		9	7.4 S	V-6	1	39.26	.236	----	---	0.0050	-----	NR
					2	49.80	.237	----	---	.0105		SP
					3	50.75	.237	----	---	.0060	-----	NP

TABLE III.- SUMMARY OF SONIC-BOOM DATA FOR SR-71 MISSIONS FLOWN AT EDWARDS AIR FORCE BASE – Continued

Date	Mission number	Site	Site distance from flight track, km	Station number	Micro-phone	Δp_o, N/m^2	ΔT, sec	Δt_o, sec	I_o, $N\text{-}sec/m^2$	τ, sec	$\tau_{1/2}$, sec	Type signature (fig. 5)
11-17-66	SR-3	9	7.4 S	Tango	1	46.44	0.236	----	---	0.0165	-----	R
					2	45.97	.236	----	---	.0055	-----	NR
					3	49.32	.236	----	---	.0020	-----	NP
					4	47.88	.236	----	---	.0070	-----	NR
					5	46.92	.236	----	---	.0140	-----	R
					6	22.98	----	----	---	-----	-----	--
				FRC	1	42.13	0.227	----	---	0.0085	-----	NP
					2	35.91	.227	----	---	.0150	-----	NR
					3	35.91	.228	----	---	.0170	-----	NR
					4	38.30	.228	----	---	.0250	-----	NR
					5	38.30	.228	----	---	.0240	-----	NR
					6	34.47	.228	----	---	.0145	-----	NR
					7	38.78	.227	----	---	.0210	-----	NR
					8	34.95	.227	----	---	.0240	-----	NR
					9	35.91	.228	----	---	.0240	-----	NR
					10	39.26	.228	----	---	.0240	-----	NR
					11	36.39	.228	----	---	.0200	-----	NR
					12	36.39	.227	----	---	.0140	-----	NR
		3	7.4 S	LAC	25	42.61	.235	----	---	0.0120	-----	NR
					26	42.61	.235	----	---	.0170	-----	NR
					27	54.10	.234	----	---	.0160	-----	NR
					28	50.75	.234	----	---	.0120	-----	NR
					29	40.70	.233	----	---	.0180	-----	NR
					30	44.05	.235	----	---	.0260	-----	NR
					31	----	----	----	---	-----	-----	--
					32	41.18	.234	----	---	.0120	-----	NR
					33	39.74	.234	----	---	.0230	-----	NR
					34	40.70	.234	----	---	.0120	-----	NR
					35	41.66	.234	----	---	.0130	-----	NR
					36	43.09	.233	----	---	.0160	-----	NR
					37	37.35	.233	----	---	.0205	-----	NR
					38	36.39	.234	----	---	.0120	-----	NR
					39	41.18	.232	----	---	.0040	-----	NP
					40	39.26	.233	----	---	.0055	-----	NP
					41	39.26	.234	----	---	.0230	-----	NR
					42	38.30	.234	----	---	.0220	-----	NR
11-28-66	SR-5	5	11.9 N	V-1	1	44.53	0.226	----	---	0.0150	-----	NR
					2	43.09	.226	----	---	.0140	-----	NR
					3	45.96	.226	----	---	.0050	-----	NP
					4	47.40	.227	----	---	.0035	-----	NP
				V-2	1	46.92	0.224	----	---	0.0160	-----	R
					2	44.53	.224	----	---	.0200	-----	R
					3	39.74	.224	----	---	.0320	-----	R
					4	----	----	----	---	-----	-----	--
				V-3	1	40.70	0.226	----	---	0.0070	-----	NR
					2	48.36	.227	----	---	.0075	-----	NR
					3	48.84	.226	----	---	.0075	-----	NR
					4	42.13	.226	----	---	.0070	-----	NR
					5	41.18	.226	----	---	.0145	-----	R
				V-4	1	38.30	0.223	----	---	.0200	-----	NR
					2	39.26	.223	----	---	.0210	-----	PR
					3	39.26	.222	----	---	.0110	-----	NR
					4	42.61	.222	----	---	.0110	-----	NR
					5	39.26	.222	----	---	.0050	-----	NP
				V-5	1	39.74	.222	----	---	.0150	-----	R
					2	39.26	.223	----	---	.0145	-----	R
					3	40.22	.222	----	---	.0060	-----	NP
					4	41.18	.222	----	---	.0045	-----	NP
					5	24.90	.222	----	---	.0070	-----	NR
				V-6	1	33.52	.223	----	---	.0240	-----	R
					2	33.03	.223	----	---	.0240	-----	R
					3	39.26	.224	----	---	.0210	-----	R

TABLE III.- SUMMARY OF SONIC-BOOM DATA FOR SR-71 MISSIONS FLOWN AT EDWARDS AIR FORCE BASE – Continued

Date	Mission number	Site	Site distance from flight track, km	Station number	Micro-phone	Δp_o, N/m^2	ΔT, sec	Δt_o, sec	I_o, $N\text{-}sec/m^2$	τ, sec	$\tau_{1/2}$, sec	Type signature (fig. 5)
11-28-66	SR-5	9	2.4 S	Tango	1	56.50	0.223	0.1290	3.69	0.0140	0.0017	NR
					2	54.10	.233	.1185	3.41	.0160	.001	NR
					3	55.06	.233	.1230	3.79	.0005	.0005	PR
					4	57.94	.233	.1225	3.52	.0130	.001	PR
					5	52.67	.233	.1235	3.39	.0125	.0005	NR
					6	27.77	----	-----	---	-----	------	--
		5	11.9 N	FRC	1	40.22	0.219	-----	---	0.0130	------	R
					2	42.61	.218	-----	---	.0150	------	R
					3	37.83	.219	-----	---	.0160	------	R
					4	41.18	.219	-----	---	.0180	------	R
					5	38.30	.218	-----	---	.0170	------	R
					6	34.47	.219	-----	---	.0190	------	R
					7	37.35	.219	-----	---	.0200	------	R
					8	45.01	.219	-----	---	.0220	------	R
					9	38.30	.219	-----	---	.0200	------	R
					10	41.18	.219	-----	---	.0180	------	R
					11	38.78	.219	-----	---	.0170	------	R
					12	35.91	.219	-----	---	.0200	------	R
					13	41.18	.224	-----	---	.0280	------	NR
					14	39.26	.225	-----	---	.0270	------	NR
					15	40.22	.225	-----	---	.0080	------	NP
					16	37.83	.225	-----	---	.0050	------	NP
11-29-66	SR-6	9	5.1 S	V-1	1	38.78	0.236	0.1290	2.83	0.0120	0.0025	NR
					2	38.78	.236	.1390	2.99	.0110	.002	NR
					3	37.35	.236	.1310	2.92	.0080	.0005	NR
					4	37.35	.235	.1350	3.04	.0150	.0022	NR
				V-4	1	40.22	0.237	0.1320	3.05	0.0115	0.002	NR
					2	42.13	.237	.1310	3.17	.0120	.0025	NR
					3	45.49	.236	.1340	3.36	.0120	.003	NR
					4	44.53	.236	.1305	3.05	.0150	.0015	NR
					5	43.57	.236	.1290	3.23	.0140	.001	NR
				V-6	1	45.01	0.239	0.1315	2.94	0.0120	0.001	NP
					2	44.05	.239	.1223	2.59	.0070	.001	NP
					3	43.57	.240	.1305	2.84	.0080	.002	NP
				Tango	1	45.97	0.234	0.1380	3.33	0.0055	0.0015	NP
					2	44.53	.234	.1295	3.26	.0050	.001	NP
					3	45.49	.234	.1395	3.34	.0140	.001	NR
					4	47.88	.235	.1140	2.79	.0060	.001	NP
					5	44.53	.235	.1335	3.21	.0040	.002	NP
					6	22.98	----	-----	---	-----	------	--
				FRC	1	40.70	0.229	0.1365	3.14	0.0050	0.001	NP
					2	39.26	.230	.1335	2.78	.0070	.001	NP
					3	38.30	.229	.1345	2.83	.0090	.002	NR
					4	41.66	.229	.1330	3.08	.0120	.00225	NR
					5	41.66	.230	.1329	2.93	.0110	.002	NR
					6	36.87	.229	.1285	2.49	.0050	.00075	NP
					7	39.26	.230	.1325	2.84	.0070	.001	NP
					8	37.83	.230	.1324	2.75	.0090	.001	NR
					9	40.70	.230	.1210	2.63	.0090	.001	NR
					10	43.09	.230	.1330	3.02	.0100	.0015	NR
					11	40.22	.229	.1295	2.85	.0115	.002	NR
					12	36.87	.229	.1305	2.61	.0110	.0025	NR
				LAC	32	40.22	0.238	0.1330	3.21	0.0100	0.0015	NR
					33	39.74	.238	.1390	3.22	.0220	.0015	NR
					34	43.09	.238	.1340	3.42	.0170	.002	NR
					35	42.61	.238	.1340	3.20	.0210	.002	NR
					36	43.09	.238	.1400	3.65	.0170	.00225	NR
					37	45.96	.238	.1330	3.29	.0170	.0015	NR
					38	38.30	.238	.1410	3.32	.0130	.001	NR
					39	46.44	.238	.1400	3.61	.0180	.0015	NR
					40	51.71	.239	.1320	3.72	.0140	.002	NR
					41	53.15	.239	.1330	4.08	.0140	.0015	NR
					42	45.01	.238	.1380	3.52	.0130	.002	NR

TABLE III.- SUMMARY OF SONIC-BOOM DATA FOR SR-71 MISSIONS FLOWN AT EDWARDS AIR FORCE BASE – Continued

Date	Mission number	Site	Site distance from flight track, km	Station number	Micro-phone	Δp_o, N/m^2	ΔT, sec	Δt_o, sec	I_o, $N\text{-}sec/m^2$	τ, sec	$\tau_{1/2}$, sec	Type signature (fig. 5)
11-29-66	SR-7	9	4.4 N	V-1	1	47.40	0.229	0.1200	2.46	0.0120	0.0005	NR
					2	35.43	.230	.1250	2.42	.0240	.0005	NR
					3	38.78	.229	.1220	2.64	.0045	.0005	NR
					4	40.70	.230	.1300	2.76	.0060	.00225	PR
				V-4	1	38.78	0.231	0.1360	2.94	0.0110	0.001	NR
					2	40.22	.231	.1240	2.99	.0120	.0005	NR
					3	38.78	.231	.1290	3.19	.0110	.0005	NR
					4	41.18	.230	.1255	2.75	.0050	.0005	NR
					5	43.57	.230	.1280	3.17	.0060	.001	NR
				V-6	1	40.70	0.233	0.1315	2.81	0.0130	0.0005	PR
					2	40.22	.234	.1287	2.85	.0080	.0015	NR
					3	46.44	.234	.1265	2.90	.0070	.00175	NP
				Tango	1	39.74	0.226	0.1280	2.79	0.0070	0.0015	NP
					2	39.74	.227	.1245	2.83	.0150	.0005	NR
					3	37.35	.227	.1314	2.95	.0060	.001	NP
					4	40.70	.227	.1085	2.20	.0140	.0005	NR
					5	40.22	.227	.1284	2.67	.0150	.0025	NR
					6	18.19	----	-----	---	-----	------	--
				FRC	1	43.57	0.224	0.1265	2.89	0.0050	0.001	NP
					2	43.09	.224	.1285	2.94	.0110	.002	NR
					3	41.18	.224	.1250	2.87	.0190	.001	NR
					4	43.09	.224	.1250	3.08	.0090	.00075	NR
					5	43.57	.224	.1240	3.02	.0100	.001	PR
					6	47.40	.224	.1215	2.79	.0065	.001	NP
					7	49.80	.225	.1285	3.02	.0070	.0015	NP
					8	41.18	.224	.1290	2.83	.0130	.001	PR
					9	41.66	.224	.1170	2.64	.0090	.001	PR
					10	41.66	.225	.1250	2.95	.0175	.001	PR
					11	40.70	.224	.1265	2.82	.0120	.001	PR
					12	37.35	.224	.1255	2.68	.0080	.001	PR
				LAC	32	42.61	0.231	0.1240	2.98	0.0140	0.0015	NR
					33	44.05	.232	.1325	3.19	.0090	.0015	NR
					34	45.01	.231	.1285	3.23	.0130	.00175	NR
					35	46.44	.231	.1280	3.16	.0060	.001	NR
					36	39.74	.232	.1280	3.00	.0200	.00075	NR
					37	42.13	.232	.1305	3.18	.0080	.001	NR
					38	39.26	.231	.1440	2.98	.0130	.0015	NR
					39	47.88	.231	.1320	3.22	.0070	.001	NR
					40	43.09	.231	.1260	3.31	.0100	.0015	NR
					41	47.88	.231	.1290	3.61	.0180	.0015	NR
					42	42.13	.232	.1285	3.12	.0080	.0015	NR
11-30-66	SR-8	9	5.4 N	V-1	1	45.49	0.222	0.1185	2.73	0.0050	0.001	NP
					2	35.91	.222	.1185	2.35	.0050	.00125	NP
					3	47.88	.222	.1120	2.60	.0055	.00125	NP
					4	47.88	.222	.1190	3.02	.0050	.001	NP
		4	25.9 N	V-2	1	33.52	0.198	-----	---	0.0060	------	NR
					2	34.95	.198	-----	---	.0060	------	NR
					3	36.39	.199	-----	---	.0050	------	NR
					4	37.35	.198	-----	---	.0055	------	NR
		9	5.4 N	V-4	1	43.57	.223	0.1200	2.65	0.0050	0.00125	NP
					2	44.05	.223	.1160	2.49	.0050	.0015	NP
					3	36.87	.223	.1165	2.38	.0050	.0015	NP
					4	44.53	.223	.1180	2.72	.0055	.0015	NP
					5	48.36	.223	.1165	2.74	.0040	.001	NP
		6	2.6 N	V-5	1	45.01	0.227	0.1270	2.81	0.0045	0.001	NP
					2	36.39	.227	.1285	2.82	.0150	.0015	NR
					3	38.30	.228	.1275	2.82	.0140	.002	NR
					4	45.01	.227	.1290	2.77	.0055	.0005	NP
					5	37.35	.226	.1255	2.77	.0200	.0005	NR
		9	5.4 N	V-6	1	50.27	0.221	0.1110	2.63	0.0050	0.001	NR
					2	46.44	.220	.1090	2.56	.0110	.0005	NR
					3	43.57	.220	.1239	2.86	.0190	.003	NR
				Tango	1	50.75	0.224	0.1160	3.03	0.0075	0.001	NR
					2	49.32	.223	.1050	2.78	.0050	.001	NR
					3	48.84	.223	.1160	2.94	.0150	.0015	NR
					4	51.71	.223	.0920	2.32	.0080	.00175	NR
					5	50.27	.223	.1114	2.84	.0120	.001	NR
					6	24.42	----	-----	---	-----	------	--

TABLE III.- SUMMARY OF SONIC-BOOM DATA FOR SR-71 MISSIONS FLOWN AT EDWARDS AIR FORCE BASE – Continued

Date	Mission number	Site	Site distance from flight track, km	Station number	Micro-phone	Δp_o, N/m^2	ΔT, sec	Δt_o, sec	I_o, $N\text{-}sec/m^2$	τ, sec	$\tau_{1/2}$, sec	Type signature (fig. 5)
11-30-66	SR-8	9	5.4 N	FRC	1	40.70	0.216	0.1170	2.72	0.0075	0.0005	NR
					2	42.13	.215	.1230	2.72	.0070	.001	NR
					3	42.13	.216	.1160	2.56	.0070	.001	NR
					4	45.01	.215	.1170	2.71	.0060	.0005	NP
					5	45.49	.216	.1170	2.70	.0055	.001	NP
					6	35.43	.216	.1210	2.42	.0085	.001	NR
					7	39.26	.216	.1200	2.63	.0060	.0015	NP
					8	42.13	.215	.1245	2.87	.0060	.001	NP
					9	40.22	.216	.1115	2.39	.0060	.001	NP
					10	44.05	.216	.1160	2.59	.0055	.0015	NP
					11	45.01	.216	.1155	2.66	.0060	.00125	NP
					12	48.84	.215	.1130	2.10	.0055	.001	NP
		3	31.7 N	FRC	13	21.55	0.186	-----	---	0.0150	------	NR
					14	23.94	.184	-----	---	.0145	------	NR
					15	26.33	.185	-----	---	.0090	------	NR
					16	23.46	.184	-----	---	.0080	------	NR
		9	5.4 N	LAC	32	49.32	0.226	0.1235	2.92	0.0040	0.001	NR
					33	46.92	.226	.1220	2.93	.0050	.001	NR
					34	50.75	.226	.1195	3.04	.0070	.001	NR
					35	46.92	.227	.1175	2.88	.0040	.001	NR
					36	45.01	.225	.1245	2.94	.0100	.00125	NR
					37	46.44	.226	.1180	2.76	.0070	.0005	NR
					38	46.44	.226	.1210	2.91	.0120	.00075	NR
					39	44.05	.226	.1235	2.85	.0120	.001	NR
					40	48.84	.226	.1285	3.36	.0080	.001	NR
					41	43.09	.226	.1250	2.92	.0110	.0015	NR
					42	45.01	.225	.1305	2.94	.0100	.001	NR
12-1-66	SR-9	5	1.4 N	V-2	1	123.53	----	-----	---	0.0060	0.001	NP
					2	115.39	----	-----	---	.0090	.002	NP
					3	116.35	----	-----	---	.0070	.0015	NP
					4	113.00	----	-----	---	.0070	.002	NP
				V-3	1	123.05	0.158	0.1135	5.86	0.0075	0.0005	NR
					2	149.39	.159	.1125	5.79	.0015	.0005	NP
					3	126.40	.159	.1135	5.86	.0070	.001	NR
					4	110.12	.159	.1075	5.48	.0110	.0015	R
					5	109.65	.159	.1095	5.59	.0105	.002	R
				V-4	1	101.98	0.160	0.1045	5.38	0.0060	0.00175	NR
					2	98.63	.159	.0927	5.00	.0045	.0005	NR
					3	124.97	.159	.0937	5.17	.001	.0005	SP
					4	82.35	.159	.0956	4.99	.0120	.001	NR
					5	85.71	.159	.0946	5.18	.0070	.001	PR
				V-5	1	97.68	0.160	0.0975	5.73	0.0300	0.0005	NR
					2	103.42	.160	.0950	5.71	.0070	.0005	PR
					3	108.69	.160	.0960	5.92	.0050	.0015	N
					4	122.57	.159	.0920	5.81	.0105	.001	NR
					5	140.78	.160	.0895	5.99	.0040	.0005	N
				V-6	1	118.74	0.162	0.0950	5.46	0.0050	0.0015	NP
					2	127.36	.162	.0830	4.58	.0060	.0025	NP
					3	106.77	.162	.0940	5.34	.0090	.002	NR
		9	5.0 S	Tango	1	85.71	0.162	0.1125	4.60	0.0250	0.001	CO
					2	87.14	.162	.1035	4.22	.0270	.0025	CO
					3	86.18	.162	.0998	4.28	.0240	.0025	CO
					4	79.48	.163	.0835	3.58	.0235	.003	CO
					5	86.18	.163	.0895	3.89	.0250	.003	CO
					6	67.99	----	-----	---	-----	------	--
		5	1.4 N	FRC	1	105.33	0.159	0.0965	5.12	0.0040	0.001	NN
					2	101.51	.159	.1040	6.23	.0065	.0015	NR
					3	101.03	.158	.1030	5.64	.0160	.0015	NR
					4	102.46	.158	.1001	5.60	.0180	.001	NR
					5	98.63	.159	.0995	5.31	.0190	.002	NR
					6	107.25	.158	.1005	6.04	.0160	.0025	NR
					7	89.54	.158	.1100	5.18	.0120	.0025	NR
					8	105.82	.158	.1085	6.14	.0110	.003	NR
					9	85.71	.159	.0995	4.53	.0100	.003	NR
					10	95.28	.159	.0955	5.14	.0095	.003	NR
					11	90.49	.159	.0980	4.64	.0070	.002	NR
					12	90.01	.159	.1000	4.61	.0050	.0005	NR
					13	122.57	.165	.1090	5.63	.0050	.001	NP
					14	103.42	.165	.1004	4.52	.0030	.0005	NP
					15	134.54	.164	.0993	5.19	.0050	.0005	NP
					16	181.47	.166	.1004	5.16	.0010	.0005	P

TABLE III.- SUMMARY OF SONIC-BOOM DATA FOR SR-71 MISSIONS FLOWN AT EDWARDS AIR FORCE BASE – Continued

Date	Mission number	Site	Site distance from flight track, km	Station number	Micro-phone	Δp_o, N/m^2	ΔT, sec	Δt_o, sec	I_o, $N\text{-}sec/m^2$	τ, sec	$\tau_{1/2}$, sec	Type signature (fig. 5)
12-1-66	SR-9	9	5.0 S	LAC	25	80.44	0.168	0.1070	4.27	0.0060	0.001	NR
					26	99.59	.167	.1095	4.64	.0030	.001	P
					27	72.78	.168	.1115	4.41	.0150	.002	NR
					28	87.14	.168	.1110	4.55	.0080	.0025	NR
					29	99.11	.168	.1065	4.76	.0060	.002	NP
					30	74.69	.168	.1055	4.21	.0130	.0015	NR
					31	-----	----	-----	---	-----	------	--
					32	71.34	.164	.1025	4.10	.0140	.0015	NR
					33	68.47	.164	.1077	4.39	.0020	.001	--
					34	77.09	.164	.0992	4.19	.0050	.0015	NP
					35	71.82	.164	.0920	4.04	.0210	.001	NR
					36	67.51	.165	.0952	3.94	.0100	.002	NR
					37	74.69	.165	.0973	4.16	.0050	.002	NP
					38	71.34	.164	.0994	4.26	.0200	.0015	NR
					39	70.38	.165	.1014	4.20	.0100	.0015	NR
					40	98.63	.164	.1035	4.82	.0075	.0025	NP
					41	105.82	.164	.0941	4.27	.001	.0005	SP
					42	67.03	.164	.1004	4.32	.0130	.001	NR
	SR-10	5	16.1 N	V-1	1	36.39	0.213	-----	---	0.0190	------	R
					2	35.91	.213	-----	---	.0110	------	R
					3	37.35	.213	-----	---	.0090	------	R
					4	35.43	.214	-----	---	.0070	------	NR
				V-2	1	31.12	0.216	-----	---	0.0100	------	NR
					2	33.04	.216	-----	---	.0150	------	NR
					3	32.56	.216	-----	---	.0150	------	NR
					4	41.18	.216	-----	---	.0035	------	NP
				V-3	1	39.74	0.212	-----	---	0.0095	------	NR
					2	31.60	.213	-----	---	.0170	------	R
					3	31.12	.213	-----	---	.0140	------	R
					4	30.16	.212	-----	---	.0150	------	R
					5	32.08	.212	-----	---	.0020	------	NP
				V-4	1	27.29	0.209	-----	---	0.0340	------	R
					2	27.77	.210	-----	---	.0330	------	R
					3	23.46	.210	-----	---	.0210	------	R
					4	27.29	.209	-----	---	.0085	------	PR
					5	27.29	.209	-----	---	.0350	------	R
				V-5	1	33.52	0.210	-----	---	0.0230	------	R
					2	34.95	.210	-----	---	.0190	------	R
					3	40.22	.210	-----	---	.0090	------	NR
					4	35.43	.208	-----	---	.0070	------	NR
					5	38.78	.208	-----	---	.0100	------	NR
				V-6	1	31.12	0.212	-----	---	0.0045	------	PR
					2	29.21	.212	-----	---	.0060	------	NR
					3	33.99	.212	-----	---	.0170	------	R
		9	5.2 N	Tango	1	42.13	0.224	0.1425	3.36	0.0090	0.001	NR
					2	42.13	.224	.1305	3.04	.0200	.001	NR
					3	41.18	.224	.1385	3.16	.0075	.0015	NR
					4	39.26	.224	.1160	2.48	.0150	.0025	NR
					5	38.78	.224	.1385	3.04	.0200	.0025	NR
					6	19.15	----	-----	---	-----	------	--
		5	16.1 N	FRC	1	34.95	≈0.207	-----	---	0.0160	------	--
					2	39.26	≈.207	-----	---	.0160	------	--
					3	34.47	≈.207	-----	---	.0150	------	--
					4	30.64	≈.207	-----	---	.0200	------	--
					5	37.35	≈.207	-----	---	.0250	------	--
					6	32.56	≈.207	-----	---	.0210	------	--
					7	43.57	≈.207	-----	---	.0230	------	--
					8	35.91	≈.207	-----	---	.0090	------	--
					9	33.52	≈.207	-----	---	.0280	------	--
					10	31.60	≈.207	-----	---	.0080	------	--
					11	27.29	≈.207	-----	---	.0080	------	--
					12	29.21	≈.207	-----	---	.0100	------	--
					13	----	----	-----	---	-----	------	--
					14	34.95	.213	-----	---	.0030	------	NP
					15	32.56	.214	-----	---	.0050	------	PR
					16	39.74	.216	-----	---	.0220	------	PR

TABLE III.- SUMMARY OF SONIC-BOOM DATA FOR SR-71 MISSIONS FLOWN AT EDWARDS AIR FORCE BASE – Continued

Date	Mission number	Site	Site distance from flight track, km	Station number	Micro-phone	Δp_o, N/m^2	ΔT, sec	Δt_o, sec	I_o, $N\text{-}sec/m^2$	τ, sec	$\tau_{1/2}$, sec	Type signature (fig. 5)
12-1-66	SR-10	9	5.2 N	LAC	25	59.37	0.232	0.1205	2.66	0.0070	0.001	NP
					26	55.06	.232	.1260	3.24	.0070	.001	NP
					27	65.12	.232	.1165	3.16	.0020	.001	NP
					28	63.68	.232	.1205	3.04	.0055	.001	NP
					29	53.63	.233	.1165	2.99	.0050	.0015	NP
					30	70.38	.234	.1250	3.50	.0065	.001	NP
					31	-----	----	-----	---	-----	------	--
					32	58.41	.227	.1230	3.23	.0090	.001	NR
					33	52.19	.226	.1200	3.31	.0070	.00075	NP
					34	122.09	.228	.1205	3.55	.0015	.001	P
					35	73.73	.227	.1170	3.46	.0015	.00075	NP
					36	66.55	.226	.1170	3.00	.0030	.001	NP
					37	68.95	.227	.1160	3.09	.0025	.001	NP
					38	63.68	.228	.1180	3.19	.0040	.00125	NP
					39	57.94	.228	.1175	3.23	.0070	.001	NR
					40	56.98	.228	.1160	3.32	.0070	.001	NR
					41	52.19	.227	.1165	3.15	.0090	.001	NR
					42	51.23	.227	.1160	2.99	.0100	.001	NR
	SR-11	5	4.0 N	V-1	1	49.31	0.222	0.1210	2.99	0.0140	0.003	R
					2	49.79	.222	.1220	3.09	.0070	.002	NR
					3	49.96	.221	.1195	2.86	.0150	.0015	R
					4	41.66	.221	.1260	3.04	.0180	.002	R
				V-2	1	40.70	0.223	0.1195	2.78	0.0150	0.0025	R
					2	47.88	.224	.1205	2.86	.0090	.002	NR
					3	53.15	.223	.1215	2.83	.0075	.0025	NP
					4	56.50	.223	.1270	2.94	.0035	.001	NP
				V-3	1	43.57	0.220	0.1215	2.72	0.0170	0.00125	NR
					2	40.22	.218	.1240	2.92	.0080	.0015	NR
					3	41.66	.219	.1260	2.67	.0150	.001	NR
					4	44.53	.220	.1220	2.67	.0080	.0015	PR
					5	50.75	.220	.1230	2.88	.0065	.0025	NR
				V-4	1	47.40	0.219	0.1320	2.86	0.0150	0.003	R
					2	46.44	.219	.1241	2.98	.0180	.0015	--
					3	44.05	.220	.1300	2.98	.0095	.002	NR
					4	43.09	.220	.1211	2.93	.0025	.001	NP
					5	42.61	.220	.1141	2.88	.0080	.001	NR
				V-5	1	46.92	0.222	0.1140	3.30	0.0100	0.00125	NR
					2	45.01	.222	.1190	2.94	.0290	.003	R
					3	43.57	.223	.1220	2.95	.0320	.0035	R
					4	42.61	.222	.1180	2.83	.0260	.0035	R
					5	46.44	.222	.1215	3.35	.0270	.003	R
				V-6	1	56.50	0.225	0.1170	3.43	0.0100	0.001	NR
					2	57.94	.226	.1070	3.18	.0120	.0025	NR
					3	69.90	.225	.1120	3.19	.001	.00075	SP
		9	6.9 S	Tango	1	68.95	0.220	0.1100	3.44	0.0050	0.001	NP
					2	63.68	.221	.1061	3.24	.0065	.001	NP
					3	62.72	.221	.1110	3.22	.0050	.001	NP
					4	64.16	.221	-----	---	.0050	.0015	NP
					5	59.37	.221	.1110	3.35	.0050	.001	NP
					6	25.38	----	-----	---	-----	------	--
		5	4.0 N	FRC	1	54.10	≈0.219	0.1065	3.38	0.0060	0.0005	NR
					2	61.77	≈.219	.1345	3.30	.0050	.0035	NP
					3	50.75	≈.219	.1055	2.68	.0140	.0045	--
					4	48.36	≈.219	.1160	3.02	.0180	.002	R
					5	51.71	≈.219	.1180	3.16	.0200	.004	--
					6	46.44	≈.219	.1045	2.47	.0125	.0025	--
					7	51.71	≈.219	.0990	2.92	.0140	.001	R
					8	60.33	≈.219	.0945	3.04	.0025	.001	NP
					9	54.10	≈.219	.0920	2.48	.0040	.00125	NP
					10	49.32	≈.219	.0960	2.47	.0190	.0003	--
					11	43.57	≈.219	.1040	2.54	.0360	.0015	--
					12	38.78	≈.219	.1125	2.59	.0200	.0025	NR
					13	39.74	.225	.1167	2.90	.0160	.0015	NR
					14	39.26	.224	.1173	2.69	.0080	.002	NR
					15	46.92	.224	.1189	3.04	.0040	.001	NP
					16	45.49	.224	.1200	3.29	.0100	.0015	NR

TABLE III.- SUMMARY OF SONIC-BOOM DATA FOR SR-71 MISSIONS FLOWN AT EDWARDS AIR FORCE BASE – Continued

Date	Mission number	Site	Site distance from flight track, km	Station number	Micro-phone	Δp_o, N/m^2	ΔT, sec	Δt_o, sec	I_o, $N\text{-}sec/m^2$	τ, sec	$\tau_{1/2}$, sec	Type signature (fig. 5)
12-1-66	SR-11	9	6.9 S	LAC	25	42.61	0.226	0.1260	3.22	0.0090	0.001	NR
					26	43.09	.224	.1360	3.34	.0150	.002	NR
					27	42.61	.225	.1340	3.39	.0220	.0015	NR
					28	41.18	.225	.1265	3.24	.0190	.002	NR
					29	43.09	.226	.1260	3.32	.0130	.001	NR
					30	45.01	.225	.1240	3.17	.0040	.0015	NP
					31	----	----	-----	---	-----	------	--
					32	59.37	.220	.1220	3.38	.0080	.002	NR
					33	48.84	.220	.1200	3.07	.0070	.001	NR
					34	70.38	.219	.1190	3.13	.0020	.0015	NP
					35	48.84	.220	.1160	2.95	.0070	.0015	NR
					36	49.80	.220	.1215	3.18	.0020	.0015	NP
					37	59.37	.220	.1188	2.92	.0025	.00125	NP
					38	47.40	.220	.1200	3.37	.0240	.001	NR
					39	46.92	.220	.1152	3.30	.0040	.0015	NR
					40	45.96	.220	.1194	3.34	.0160	.0015	NR
					41	46.44	.220	.1209	3.23	.0080	.0015	NR
					42	46.44	.219	.1199	3.22	.0100	.0015	NR
12-8-66	SR-12	9	3.9 S	V-1	1	44.04	0.212	0.1225	3.21	0.0340	0.0025	R
					2	46.92	.213	.1220	3.38	.0350	.0025	R
					3	44.53	.213	.1240	3.39	.0350	.003	R
					4	49.96	.214	.1205	3.37	.0350	.004	R
		4	16.5 N	V-2	1	22.50	----	-----	---	0.0180	------	CO
					2	21.55	----	-----	---	.0180	------	CO
					3	22.98	----	-----	---	.0200	------	CO
					4	21.55	----	-----	---	.0180	------	CO
		7	9.8 S	V-3	1	28.25	----	-----	---	0.0800	------	CO
					2	26.33	----	-----	---	.0860	------	CO
					3	23.94	----	-----	---	.0840	------	CO
					4	24.42	----	-----	---	.0870	------	CO
					5	30.16	----	-----	---	.0750	------	CO
		9	3.9 S	V-4	1	42.13	0.216	0.1225	3.03	0.0350	0.003	NR
					2	42.13	.216	.1225	2.98	.0350	.0035	NR
					3	41.66	.216	.1230	3.21	.0340	.0035	NR
					4	43.09	.215	.1245	3.20	.0350	.004	NR
					5	44.53	.214	.1185	3.21	.0330	.004	NR
		6	5.5 S	V-5	1	55.54	0.214	0.1205	2.96	0.0050	0.0005	NP
					2	49.32	.214	.1210	2.83	.0065	.001	NP
					3	40.70	.213	.1220	2.77	.0070	.001	NR
					4	45.49	.211	.1210	2.84	.0060	.0005	NR
					5	57.94	.214	.1205	2.82	.0050	.001	NP
		9	3.9 S	V-6	1	60.33	0.216	0.1070	3.16	0.0130	0.005	NR
					2	56.50	.216	.0954	2.80	.0135	.003	NR
					3	73.74	.217	.1060	3.01	.0030	.0005	NP
				Tango	1	50.75	0.207	0.1020	3.05	0.0230	0.002	R
					2	46.92	.206	.1069	2.86	.0260	.003	R
					3	47.40	.207	.1064	2.87	.0230	.0025	R
					4	52.67	.208	.0980	2.69	.0150	.0015	R
					5	49.32	.208	.1060	3.02	.0250	.003	R
					6	21.07	----	-----	---	-----	------	--
				FRC	1	41.18	0.210	0.1275	3.41	0.0370	0.003	NR
					2	44.05	.210	.1215	3.28	.0350	.002	NR
					3	42.13	.210	.1200	3.31	.0340	.002	NR
					4	42.61	.210	.1265	3.45	.0330	.002	NR
					5	43.57	.210	.1210	3.30	.0330	.0025	NR
					6	39.26	.210	.1150	2.97	.0360	.00225	NR
					7	39.74	.210	.1185	3.15	.0380	.002	NR
					8	39.26	.210	.1170	2.82	.0330	.003	NR
					9	39.74	.210	.1190	2.97	.0330	.0035	NR
					10	39.74	.211	.1230	3.08	.0340	.0025	NR
					11	39.74	.210	.1130	2.61	.0335	.0025	NR
					12	40.70	.210	.1220	2.91	.0330	.0025	NR
		3	21.6 N	FRC	13	20.59	≈0.170	-----	---	0.0540	------	--
					14	18.19	≈.170	-----	---	.0570	------	--
					15	19.63	≈.170	-----	---	.0590	------	--
					16	18.67	≈.170	-----	---	.0610	------	--

TABLE III.- SUMMARY OF SONIC-BOOM DATA FOR SR-71 MISSIONS FLOWN AT EDWARDS AIR FORCE BASE – Continued

Date	Mission number	Site	Site distance from flight track, km	Station number	Micro-phone	Δp_o, N/m^2	ΔT, sec	Δt_o, sec	I_o, $N\text{-}sec/m^2$	τ, sec	$\tau_{1/2}$, sec	Type signature (fig. 5)
12-8-66	SR-12	9	3.9 S	LAC	25	36.87	0.217	0.1110	2.74	0.0500	0.002	NR
					26	47.88	.218	.1164	3.50	.0410	.002	PR
					27	47.88	.219	.1197	3.35	.0370	.0025	NR
					28	49.80	.220	.1241	3.48	.0360	.004	NR
					29	54.10	.219	.1208	3.68	.0250	.004	NR
					30	53.15	.218	.1175	3.55	.0230	.0035	NR
					31	37.35	.220	.1130	2.34	.0180	.004	NR
					32	52.19	.219	.1100	2.73	.0220	.0055	NR
					33	64.16	.218	.1177	3.44	.0140	.0025	NR
					34	52.67	.218	.1166	3.32	.0210	.003	NR
					35	62.24	.219	.1188	3.53	.0150	.004	NR
					36	61.29	.218	.1155	3.39	.0100	.0035	NR
					37	45.01	.220	.1210	2.85	.0200	.0045	NR
					38	42.13	.218	.1166	2.38	.0140	.0045	NR
					39	65.60	.218	.1116	2.83	.0070	.0025	NP
					40	47.88	.218	.1133	2.52	.0130	.0045	NR
					41	59.37	.219	.1122	2.87	.0110	.003	NR
					42	----	----	-----	---	-----	-----	--
	SR-13	9	32.97 S	V-1	1	17.71	----	-----	---	0.0100	-----	NR
					2	15.80	----	-----	---	.0090	-----	NR
					3	16.76	----	-----	---	.0110	-----	NR
					4	20.11	----	-----	---	.0150	-----	NR
		4	14.3 S	V-2	1	23.94	0.200	-----	---	0.0190	-----	NR
					2	22.02	.200	-----	---	.0135	-----	NR
					3	21.55	.200	-----	---	.0150	-----	NR
					4	20.11	.200	-----	---	.0230	-----	R
		7	37.9 S	V-3	1	22.50	0.206	-----	---	0.0110	-----	NR
					2	21.55	.206	-----	---	.0150	-----	NR
					3	19.15	.208	-----	---	.0230	-----	R
					4	19.15	.206	-----	---	.0150	-----	NR
					5	22.98	.207	-----	---	.0120	-----	NR
		9	32.97 S	V-4	1	15.80	0.196	-----	---	0.0100	-----	NR
					2	16.76	.196	-----	---	.0110	-----	NR
					3	16.28	.196	-----	---	.0100	-----	NR
					4	16.28	.194	-----	---	.0120	-----	NR
					5	15.80	.194	-----	---	.0135	-----	NR
		6	28.5 S	V-5	1	22.50	0.195	-----	---	0.0380	-----	CO
					2	21.55	.195	-----	---	.0350	-----	CO
					3	21.07	.195	-----	---	.0370	-----	CO
					4	21.07	.195	-----	---	.0420	-----	CO
					5	21.07	.195	-----	---	.0380	-----	CO
		9	32.97 S	V-6	1	16.28	0.195	-----	---	0.0240	-----	R
					2	18.19	.195	-----	---	.0200	-----	R
					3	21.55	.195	-----	---	.0090	-----	R
				Tango	1	19.15	0.190	-----	---	0.0200	-----	R
					2	20.11	.190	-----	---	.0100	-----	R
					3	17.72	.190	-----	---	.0100	-----	R
					4	21.07	.190	-----	---	.0210	-----	R
					5	19.63	.190	-----	---	.0100	-----	R
					6	9.10	----	-----	---	-----	-----	--
				FRC	1	17.72	0.191	-----	---	0.0170	-----	NR
					2	17.72	.191	-----	---	.0120	-----	NR
					3	17.24	.191	-----	---	.0110	-----	NR
					4	17.24	.191	-----	---	.0100	-----	NR
					5	17.24	.191	-----	---	.0100	-----	NR
					6	15.80	.191	-----	---	.0250	-----	NR
					7	16.28	.191	-----	---	.0120	-----	NR
					8	16.76	.191	-----	---	.0120	-----	NR
					9	15.80	.191	-----	---	.0120	-----	NR
					10	15.32	.191	-----	---	.0110	-----	NR
					11	15.32	.191	-----	---	.0100	-----	NR
					12	15.32	.191	-----	---	.0100	-----	NR
		3	10.9 S	FRC	13	50.75	0.215	-----	---	0.0070	-----	NP
					14	52.67	.216	-----	---	.0105	-----	NP
					15	62.72	.216	-----	---	.0070	-----	NP
					16	59.85	.216	-----	---	.0070	-----	NP

TABLE III.- SUMMARY OF SONIC-BOOM DATA FOR SR-71 MISSIONS FLOWN AT EDWARDS AIR FORCE BASE – Continued

Date	Mission number	Site	Site distance from flight track, km	Station number	Micro-phone	Δp_o, N/m^2	ΔT, sec	Δt_o, sec	I_o, $N\text{-sec}/m^2$	τ, sec	$\tau_{1/2}$, sec	Type signature (fig. 5)
12-8-66	SR-13	9	32.97 S	LAC	25	17.24	0.195	-----	---	0.0220	------	R
					26	17.24	.192	-----	---	.0360	------	R
					27	16.76	.198	-----	---	.0140	------	R
					28	16.28	.195	-----	---	.0210	------	R
					29	16.76	.194	-----	---	.0210	------	R
					30	18.67	.189	-----	---	.0230	------	R
					31	15.32	.192	-----	---	.0220	------	R
					32	17.24	.202	-----	---	.0220	------	R
					33	19.15	.200	-----	---	.0340	------	R
					34	17.24	.199	-----	---	.0230	------	R
					35	19.15	.196	-----	---	.0220	------	R
					36	19.63	.199	-----	---	.0260	------	R
					37	*13.89*	*.198*	-----	---	*.0320*	------	R
					38	10.53	.195	-----	---	.0330	------	R
					39	17.72	.200	-----	---	.0320	------	R
					40	13.41	.196	-----	---	.0400	------	R
					41	15.80	.200	-----	---	.0260	------	R
					42	----	----	-----	---	-----	------	--
12-9-66	SR-14	9	1.67 S	V-1	1	46.92	0.222	0.1220	3.13	0.0110	0.002	NR
					2	51.71	.223	.1199	3.50	.0110	.002	NR
					3	*48.36*	*.224*	*.1215*	*3.40*	*.0130*	*.002*	NR
					4	48.84	.222	.1215	3.48	.0170	.002	NR
		4	18.7 N	V-2	1	38.78	0.199	-----	---	0.0170	------	NR
					2	39.74	.199	-----	---	.0130	------	NR
					3	34.47	.198	-----	---	.0210	------	NR
					4	37.35	.200	-----	---	.0195	------	NR
		7	23.2 S	V-3	1	19.63	0.190	-----	---	0.0170	------	NR
					2	20.11	.191	-----	---	.0130	------	NR
					3	19.63	.194	-----	---	.0130	------	NR
					4	20.11	.191	-----	---	.0170	------	NR
					5	18.67	.192	-----	---	.0330	------	R
		9	1.67 S	V-4	1	44.53	0.226	0.1225	3.12	0.0120	0.0015	NR
					2	44.53	.226	.1220	2.94	.0115	.002	NR
					3	41.66	.225	.1210	2.91	.0120	.0015	NR
					4	41.18	.225	.1215	2.84	.0140	.0025	NR
					5	39.74	.225	.1195	2.89	.0150	.002	NR
		10	3.52 S	V-5	1	48.36	0.217	0.1190	2.93	0.0060	0.0015	NP
					2	49.32	.218	.1200	2.88	.0055	.001	NP
					3	44.53	.216	.1210	2.85	.0100	.001	NR
					4	40.70	.217	.1160	2.72	.0130	.0015	NR
					5	46.92	.217	.1180	2.80	.0090	.0015	NR
		9	1.67 S	V-6	1	41.66	0.216	.1280	2.83	0.0100	0.00175	NR
					2	41.18	.216	.1190	2.60	.0090	.00175	NR
					3	*41.66*	*.217*	*.1285*	*2.82*	*.0125*	*.0015*	*NR*
				Tango	1	52.19	0.216	0.1190	3.44	0.0130	0.00125	NR
					2	47.88	.216	.1170	3.28	.0070	.001	NR
					3	47.40	.216	.1250	3.40	.0215	.0015	NR
					4	53.63	.217	.1085	2.92	.0155	.0025	NR
					5	47.88	.218	.1195	3.35	.0190	.0015	NR
					6	25.86	----	-----	---	-----	------	--
				FRC	1	47.40	0.216	0.1205	2.87	0.0075	0.0015	NR
					2	45.96	.217	.1225	3.11	.0080	.001	NR
					3	43.57	.216	.1215	2.95	.0100	.0015	NR
					4	46.44	.216	.1200	3.15	.0100	.002	NR
					5	45.01	.216	.1190	3.03	.0110	.00175	NR
					6	40.22	.218	.1200	2.65	.0090	.0015	NR
					7	41.66	.218	.1230	3.01	.0100	.002	NR
					8	45.01	.218	.1250	3.36	.0105	.002	NR
					9	42.61	.218	.1110	2.64	.0100	.00175	NR
					10	*45.01*	*.218*	*.1230*	*3.05*	*.0110*	*.002*	*NR*
					11	43.09	.218	.1230	2.80	.0110	.002	NR
					12	42.13	.218	.1210	2.71	.0120	.002	NR
		3	24.6 N	FRC	13	25.86	0.198	-----	---	0.0250	------	NR
					14	26.33	.197	-----	---	.0310	------	NR
					15	29.69	.195	-----	---	.0145	------	NR
					16	28.25	.196	-----	---	.0160	------	NR

TABLE III.- SUMMARY OF SONIC-BOOM DATA FOR SR-71 MISSIONS FLOWN AT EDWARDS AIR FORCE BASE – Continued

Date	Mission number	Site	Site distance from flight track, km	Station number	Micro-phone	Δp_o, N/m^2	ΔT, sec	Δt_o, sec	I_o, $N\text{-sec}/m^2$	τ, sec	$\tau_{1/2}$, sec	Type signature (fig. 5)
12-12-66	SR-15	1	49.6 N	V-1	1	9.10	----	-----	---	-----	------	CO
					2	7.66	----	-----	---	-----	------	CO
					3	7.18	----	-----	---	-----	------	CO
					4	----	----	-----	---	-----	------	--
		2	35.9 N	V-2	1	31.60	0.192	-----	---	0.0190	------	R
					2	34.47	.192	-----	---	.0180	------	R
					3	31.60	.192	-----	---	.0160	------	R
					4	34.95	.191	-----	---	.0220	------	R
		7	25.8 S	V-3	1	25.86	0.198	-----	---	0.0280	------	R
					2	28.73	.198	-----	---	.0240	------	R
					3	32.60	.198	-----	---	.0230	------	R
					4	26.33	.199	-----	---	.0260	------	NR
					5	25.85	.198	-----	---	.0180	------	NR
		9	3.9 S	V-4	1	42.13	0.210	0.1110	2.38	0.0110	0.0015	NR
					2	42.13	.210	.1110	2.24	.0155	.001	NR
					3	44.53	.210	.1110	1.94	.0140	.0015	NR
					4	42.61	.210	.1065	2.71	.0135	.001	NR
					5	45.97	.211	.1070	2.59	.0140	.001	NR
		6	8.3 S	V-5	1	45.97	0.222	-----	---	0.0250	------	NR
					2	40.70	.222	-----	---	.0075	------	NR
					3	49.80	.222	-----	---	.0055	------	NR
					4	47.88	.220	-----	---	.0075	------	NR
					5	41.18	.222	-----	---	.0245	------	NR
		8	29.4 S	V-6	1	31.12	0.199	-----	---	0.0180	------	NR
					2	31.60	.197	-----	---	.0260	------	R
					3	27.77	.195	-----	---	.0140	------	R
		9	3.9 S	Tango	1	40.22	0.210	0.1155	2.54	0.0055	0.0015	NP
					2	41.18	.210	.1095	2.43	.0065	.001	NP
					3	38.30	.210	.1105	2.41	.0065	.001	NP
					4	38.30	.210	.1020	2.29	.0060	.0015	NP
					5	38.30	.210	.1119	2.60	.0060	.00125	NP
					6	20.59	----	-----	---	-----	------	--
				FRC	1	43.09	0.208	0.1200	2.97	0.0060	0.001	NP
					2	43.57	.207	.1185	2.34	.0050	.002	NP
					3	42.13	.208	.1140	2.54	.0090	.002	NR
					4	43.09	.208	.1130	2.60	.0120	.001	NR
					5	44.05	.208	.1110	2.50	.0130	.0015	NR
					6	38.78	.207	.1150	2.44	.0080	.0015	NR
					7	42.13	.206	.1170	2.52	.0100	.0015	NR
					8	43.57	.207	.1160	2.81	.0140	.001	NR
					9	44.05	.206	.1085	2.39	.0110	.002	NR
					10	44.53	.207	.1110	2.58	.0120	.0015	NR
					11	41.66	.206	.1090	2.31	.0100	.001	NR
					12	41.66	.206	.1110	2.37	.0090	.001	NR
		3	22.0 N	FRC	13	38.30	0.199	-----	---	0.0150	------	NR
					14	33.52	.197	-----	---	.0140	------	NR
					15	31.12	.198	-----	---	.0100	------	NR
					16	31.60	.197	-----	---	.0090	------	NR
		9	3.9 S	LAC	25	38.30	0.218	0.1250	2.62	0.0350	0.00125	NR
					26	51.23	.219	.1140	2.71	.0050	.001	NR
					27	42.61	.217	.1140	2.65	.0100	.00125	NR
					28	51.23	.217	.1092	2.69	.0170	.001	NR
					29	51.71	.217	.1158	2.64	.0130	.001	NR
					30	50.75	.219	.1200	2.71	.0090	.00125	NR
					31	----	----	-----	---	-----	------	--
					32	51.71	.211	.1120	2.68	.0050	.0015	NR
					33	48.84	.211	.1140	2.71	.0080	.001	NR
					34	----	----	-----	---	-----	------	--
					35	51.71	.210	.1099	2.70	.0070	.0015	NR
					36	45.96	.211	.1090	2.68	.0110	.001	NR
					37	52.19	.211	.1080	2.77	.0080	.0015	NR
					38	45.96	.211	.1080	2.37	.0050	.0015	NR
					39	42.61	.211	.1165	2.61	.0230	.001	NR
					40	54.58	.212	.1140	2.75	.0040	.0015	NP
					41	45.96	.211	.1140	2.72	.0040	.0015	NP
					42	46.92	.212	.1130	2.71	.0250	.0015	NR
12-13-66	SR-16	10	1.76 S	V-1	1	44.53	0.224	0.1245	3.57	0.0060	0.001	NR
					2	45.01	.225	.1270	3.69	.0065	.00125	NR
					3	39.26	.224	.1250	3.27	.0060	.001	NR
					4	43.09	.224	.1310	3.55	.0180	.0025	R
		5	14.4 N	V-2	1	----	----	-----	---	-----	------	--
					2	----	----	-----	---	-----	------	--
					3	----	----	-----	---	-----	------	--
					4	----	----	-----	---	-----	------	--

TABLE III.- SUMMARY OF SONIC-BOOM DATA FOR SR-71 MISSIONS FLOWN AT EDWARDS AIR FORCE BASE – Continued

Date	Mission number	Site	Site distance from flight track, km	Station number	Micro-phone	Δp_o, N/m^2	ΔT, sec	Δt_o, sec	I_o, N-sec/m^2	τ, sec	$\tau_{1/2}$, sec	Type signature (fig. 5)
12-13-66	SR-16	3	26.3 N	V-3	1	29.69	0.201	-----	---	0.0050	-----	NR
					2	29.21	.202	-----	---	.0090	-----	NR
					3	31.12	.202	-----	---	.0100	-----	NR
					4	28.25	.203	-----	---	.0080	-----	NR
					5	30.16	.203	-----	---	.0085	-----	NR
		9	0.17 N	V-4	1	46.44	0.224	0.1195	2.91	0.0085	0.002	NR
					2	44.05	.224	.1195	2.88	.0110	.0015	R
					3	44.05	.224	.1200	2.94	.0120	.0015	R
					4	42.61	.224	.1245	2.77	.0140	.0025	R
					5	38.30	.224	.1200	2.58	.0150	.0015	R
		5	14.4 N	V-5	1	46.44	0.224	-----	---	0.0050	-----	NP
					2	45.01	.224	-----	---	.0050	-----	NP
					3	45.01	.224	-----	---	.0055	-----	NP
					4	56.50	.224	-----	---	.0070	-----	NP
					5	39.74	.224	-----	---	.0065	-----	N
		7	21.3 S	V-6	1	35.91	0.200	-----	---	0.0230	-----	R
					2	35.91	.200	-----	---	.0230	-----	R
					3	36.87	.201	-----	---	.0195	-----	R
		9	0.17 N	Tango	1	53.15	0.222	0.1150	2.96	0.0085	0.0015	NR
					2	53.63	.222	.1140	2.76	.0080	.0025	NR
					3	50.75	.222	.1219	2.94	.0080	.002	NR
					4	52.67	.224	.1050	2.68	.0090	.0025	NR
					5	54.10	.224	.1145	2.94	.0070	.0025	NR
					6	55.54	----	-----	---	-----	-----	--
		5	14.4 N	FRC	1	35.43	0.203	-----	---	0.0250	-----	R
					2	38.30	.203	-----	---	.0230	-----	R
					3	39.26	.203	-----	---	.0195	-----	R
					4	39.74	.203	-----	---	.0175	-----	R
					5	44.53	.203	-----	---	.0150	-----	R
					6	44.53	.203	-----	---	.0140	-----	R
					7	45.01	.203	-----	---	.0120	-----	R
					8	47.88	.203	-----	---	.0140	-----	R
					9	48.84	.203	-----	---	.0130	-----	R
					10	52.67	.203	-----	---	.0090	-----	R
					11	57.46	.203	-----	---	.0050	-----	NP
					12	58.89	.204	-----	---	.0015	-----	NP
					13	55.06	.210	-----	---	.0080	-----	NR
					14	52.67	.211	-----	---	.0110	-----	NR
					15	45.01	.210	-----	---	.0130	-----	R
					16	44.53	.208	-----	---	.0180	-----	R
		9	0.17 N	LAC	25	37.35	0.234	0.1230	2.25	0.0120	0.0015	NR
					26	46.92	.235	.1280	3.36	.0130	.002	NR
					27	45.49	.234	.1270	2.92	.0110	.0015	NR
					28	43.09	.234	.1455	3.50	.0150	.001	NR
					29	41.66	.234	.1200	2.32	.0110	.002	NR
					30	47.88	.233	.1385	3.95	.0140	.0015	NR
	SR-17	10	31.3 S	V-1	1	29.68	0.228	-----	---	0.0180	-----	CO
					2	32.08	.228	-----	---	.0190	-----	CO
					3	32.56	.228	-----	---	.0190	-----	CO
					4	32.56	.228	-----	---	.0200	-----	CO
		3	2.78 S	V-3	1	42.61	0.216	0.1230	2.96	0.0075	0.0015	NR
					2	43.57	.216	.1294	3.15	.0145	.0015	R
					3	42.13	.217	.1250	3.08	.0140	.0015	R
					4	40.22	.217	.1270	2.98	.0135	.0015	R
					5	41.66	.216	.1295	2.96	.0140	.0015	R
		9	29.1 S	V-4	1	46.44	≈0.224	-----	---	0.0070	-----	CO
					2	47.40	≈.224	-----	---	.0090	-----	CO
					3	46.92	≈.224	-----	---	.0080	-----	CO
					4	45.96	≈.224	-----	---	.0090	-----	CO
					5	43.09	≈.224	-----	---	.0065	-----	CO
		5	14.8 S	V-5	1	29.69	----	-----	---	0.0390	-----	CO
					2	30.16	----	-----	---	.0360	-----	CO
					3	29.69	----	-----	---	.0355	-----	CO
					4	31.60	----	-----	---	.0350	-----	CO
					5	28.73	----	-----	---	.0370	-----	CO
		7	54.6 S	V-6	1 2 3	Slight Rumble						
		9	29.1 S	Tango	1	38.30	0.225	-----	---	0.0100	-----	NR
					2	38.30	.224	-----	---	.0105	-----	NR
					3	38.30	.224	-----	---	.0100	-----	NR
					4	38.30	.224	-----	---	.0090	-----	NR
					5	39.26	.224	-----	---	.0100	-----	NR
					6	41.66	----	-----	---	-----	-----	--

TABLE III.- SUMMARY OF SONIC-BOOM DATA FOR SR-71 MISSIONS FLOWN AT EDWARDS AIR FORCE BASE - Continued

Date	Mission number	Site	Site distance from flight track, km	Station number	Microphone	Δp_o, N/m^2	ΔT, sec	Δt_o, sec	I_o, $N\text{-sec}/m^2$	τ, sec	$\tau_{1/2}$, sec	Type signature (fig. 5)
12-13-66	SR-17	5	14.8 S	FRC	1	32.08	0.217	-----	---	0.0150	------	R
					2	33.04	.217	-----	---	.0120	------	R
					3	32.08	.217	-----	---	.0110	------	R
					4	32.08	.217	-----	---	.0090	------	R
					5	33.52	.217	-----	---	.0080	------	R
					6	32.08	.217	-----	---	.0090	------	R
					7	32.08	.218	-----	---	.0080	------	R
					8	32.56	.217	-----	---	.0100	------	R
					9	33.04	.217	-----	---	.0080	------	R
					10	32.08	.217	-----	---	.0090	------	R
					11	34.47	.218	-----	---	.0110	------	R
					12	35.43	.217	-----	---	.0150	------	R
					13	41.66	.224	-----	---	.0190	------	R
					14	40.70	.225	-----	---	.0220	------	R
					15	37.83	.223	-----	---	.0270	------	R
					16	36.39	.224	-----	---	.0230	------	R
		9	29.1 S	LAC	25	43.09	≈.229	-----	---	0.0085	------	CO
					26	52.19	≈.229	-----	---	.0090	------	CO
					27	49.32	≈.229	-----	---	.0080	------	CO
					28	48.84	≈.229	-----	---	.0075	------	CO
					29	45.97	≈.229	-----	---	.0090	------	CO
					30	50.27	≈.229	-----	---	.0090	------	CO
	SR-18	10	2.04 S	V-1	1	65.60	0.175	0.0955	3.67	0.0090	0.00075	NR
					2	65.60	.176	.0990	3.84	.0090	.0005	NR
					3	63.68	.176	.0980	3.74	.0080	.001	NR
					4	55.06	.176	.0960	3.10	.0065	.001	NR
		5	14.4 N	V-2	1	----	----	-----	---	-----	------	--
					2	----	----	-----	---	-----	------	--
					3	----	----	-----	---	-----	------	--
					4	----	----	-----	---	-----	------	--
		3	26.3 N	V-3	1	32.56	----	-----	---	0.0250	------	CO
					2	33.52	----	-----	---	.0215	------	CO
					3	33.99	----	-----	---	.0200	------	CO
					4	33.52	----	-----	---	.0205	------	CO
					5	33.99	----	-----	---	.0200	------	CO
		9	0	V-4	1	58.42	0.166	0.0915	2.84	0.0120	0.00125	NR
					2	54.58	.166	.0930	3.03	.0105	.001	NR
					3	53.15	.166	.0935	3.17	.0100	.0005	NR
					4	56.50	.166	.0900	2.91	.0060	.001	NR
					5	54.58	.166	.0890	2.76	.0060	.0005	NR
		5	14.4 N	V-5	1	64.63	0.161	-----	---	0.0085	------	NR
					2	60.81	.160	-----	---	.0145	------	NR
					3	50.27	.160	-----	---	.0300	------	NR
					4	57.46	.160	-----	---	.0075	------	NR
					5	59.37	.160	-----	---	.0080	------	NR
		7	21.3 S	V-6	1	39.74	0.169	-----	---	0.0040	------	NP
					2	39.26	.169	-----	---	.0045	------	NP
					3	41.18	.169	-----	---	.0040	------	NP
		9	0	Tango	1	71.82	0.163	0.0860	3.18	0.0060	0.001	NP
					2	70.86	.164	.0821	2.93	.0065	.001	NP
					3	69.91	.164	.0860	2.96	.0060	.001	NP
					4	70.86	.164	.0800	3.01	.0065	.001	NP
					5	72.30	.164	.0850	3.21	.0050	.0001	NP
					6	69.91	----	-----	---	-----	------	--
		5	14.4 N	FRC	1	32.08	0.151	-----	---	0.0250	------	R
					2	31.60	.151	-----	---	.0260	------	R
					3	33.99	.152	-----	---	.0290	------	R
					4	33.52	.152	-----	---	.0270	------	R
					5	33.52	.152	-----	---	.0290	------	R
					6	31.12	.151	-----	---	.0180	------	R
					7	32.08	.152	-----	---	.0180	------	R
					8	32.56	.152	-----	---	.0190	------	R
					9	34.47	.153	-----	---	.0070	------	NR
					10	35.43	.154	-----	---	.0070	------	NR
					11	38.30	.154	-----	---	.0070	------	NR
					12	39.26	.154	-----	---	.0060	------	NR
					13	46.92	.156	-----	---	.0040	------	NR
					14	59.85	.155	-----	---	.0010	------	NP
					15	51.71	.156	-----	---	.0130	------	NR
					16	63.68	.155	-----	---	.0140	------	R
		9	0	LAC	25	59.85	0.169	0.0950	3.05	0.0130	0.001	NR
					26	61.29	.169	.0944	3.39	.0060	.0005	NR
					27	57.46	.168	.0939	3.15	.0050	.00075	NR
					28	57.94	.169	.0933	3.03	.0050	.001	NR
					29	55.06	.168	.0928	2.92	.0140	.001	NR
					30	57.46	.168	.0916	3.07	.0065	.0005	NR

TABLE III.- SUMMARY OF SONIC-BOOM DATA FOR SR-71 MISSIONS FLOWN AT EDWARDS AIR FORCE BASE – Continued

Date	Mission number	Site	Site distance from flight track, km	Station number	Micro-phone	Δp_o, N/m^2	ΔT, sec	Δt_o, sec	I_o, $N\text{-}sec/m^2$	τ, sec	$\tau_{1/2}$, sec	Type signature (fig. 5)
12-16-66	SR-19	7	21.3 S	V-3	1	24.90	0.211	-----	---	0.0130	------	NR
					2	24.42	.211	-----	---	.0200	------	NR
					3	22.98	.211	-----	---	.0120	------	NR
					4	23.94	.210	-----	---	.0110	------	NR
					5	24.90	.210	-----	---	.0200	------	NR
		9	0.35 S	V-4	1	41.18	0.229	0.1235	2.94	0.0120	0.00125	NR
					2	42.13	.230	.1274	3.08	.0125	.0015	NR
					3	40.22	.229	.1195	2.82	.0115	.00125	NR
					4	40.70	.229	.1260	2.87	.0130	.001	NR
					5	40.70	.229	.1225	2.80	.0080	.001	NR
				Tango	1	45.01	0.228	0.1265	2.75	0.0045	0.0005	NP
					2	41.66	.227	.1180	2.60	.0060	.0002	NR
					3	43.57	.227	.1240	2.74	.0060	.0005	NR
					4	46.44	.228	.1100	2.55	.0045	.00075	NP
					5	44.05	.228	.1205	2.75	.0065	.0005	NR
					6	22.50	----	-----	---	-----	------	--
				FRC	1	37.35	0.216	0.1210	2.67	0.0070	0.00015	NR
					2	33.99	.216	.1201	2.34	.0070	.0015	NR
					3	32.56	.217	.1247	2.37	.0170	.00125	NR
					4	37.83	.217	.1289	2.78	.0140	.0015	NR
					5	35.91	.216	.1284	2.52	.0070	.0015	NR
					6	34.47	.216	.1266	2.43	.0080	.001	NR
					7	35.43	.216	.1260	2.48	.0120	.001	NR
					8	37.83	.216	.1227	2.73	.0120	.00125	NR
					9	----	----	-----	---	-----	------	--
					10	39.74	.217	.1264	2.87	.0130	.0015	NR
					11	35.43	.217	.1246	2.56	.0150	.0015	NR
					12	33.99	.216	.1237	2.48	.0120	.0015	NR
		3	25.9 N	FRC	13	25.38	0.210	-----	---	0.0130	------	NR
					14	----	----	-----	---	-----	------	--
					15	30.16	.210	-----	---	.0065	------	NP
					16	29.21	.209	-----	---	.0060	------	NP
		9	0.35 S	LAC	25	45.01	0.237	0.1300	3.52	0.0085	0.0015	NR
					26	41.66	.238	.1265	3.19	.0070	.001	NR
					27	43.09	.238	.1270	3.10	.0075	.00125	NR
					28	39.26	.237	.1360	3.07	.0070	.0015	NR
					29	42.13	.238	.1310	3.16	.0080	.001	NR
					30	41.18	.237	.1315	3.14	.0070	.001	NR
					31	45.01	.238	.1305	2.97	.0070	.001	NR
					32	45.96	.236	.1260	3.31	.0070	.0015	NR
					33	45.96	.236	.1271	3.28	.0110	.001	NR
					34	43.09	.236	.1271	3.13	.0150	.0005	NR
					35	46.44	.236	.1249	3.22	.0120	.001	NR
					36	52.19	.236	.1290	3.69	.0105	.00075	NR
					37	46.92	.236	.1288	3.39	.0100	.00125	NR
					38	47.40	.237	.1385	4.01	.0150	.001	NR
					39	44.53	.236	.1275	3.16	.0100	.001	NR
					40	48.84	.237	.1295	3.48	.0120	.00125	NR
					41	48.36	.236	.1265	3.38	.0115	.001	NR
					42	55.06	.236	.1225	3.53	.0080	.0015	NR
	SR-20	7	13 S	V-3	1	43.57	0.223	-----	---	0.0050	0.001	NP
					2	36.87	.223	-----	---	.0065	.001	NR
					3	32.56	.223	-----	---	.0120	.0015	NR
					4	33.99	.223	-----	---	.0065	.001	NR
					5	36.39	.222	-----	---	.0100	.001	NR
		9	9.26 N	V-4	1	38.30	.0.219	-----	---	0.0110	------	NR
					2	36.87	.219	-----	---	.0115	------	NR
					3	36.87	.219	-----	---	.0110	------	NR
					4	35.91	.220	-----	---	.0140	------	NR
					5	29.69	.219	-----	---	.0080	------	NR
				Tango	1	39.74	0.220	-----	---	0.0060	------	NR
					2	38.30	.219	-----	---	.0150	------	NR
					3	40.22	.219	-----	---	.0070	------	NR
					4	43.09	.220	-----	---	.0130	------	NR
					5	40.70	.220	-----	---	.0050	------	NR
					6	21.55	----	-----	---	-----	------	--
				FRC	1	35.91	0.217	-----	---	0.0100	------	NR
					2	31.12	.217	-----	---	.0160	------	NR
					3	28.73	.217	-----	---	.0075	------	NR
					4	33.04	.217	-----	---	.0150	------	NR
					5	31.60	.217	-----	---	.0120	------	NR
					6	29.69	.218	-----	---	.0220	------	NR
					7	31.60	.216	-----	---	.0115	------	NR
					8	32.08	.218	-----	---	.0140	------	NR
					9	----	----	-----	---	-----	------	--
					10	34.47	.218	-----	---	.0140	------	NR
					11	32.08	.217	-----	---	.0120	------	NR
					12	31.12	.217	-----	---	.0120	------	NR

TABLE III.- SUMMARY OF SONIC-BOOM DATA FOR SR-71 MISSIONS FLOWN AT EDWARDS AIR FORCE BASE – Continued

Date	Mission number	Site	Site distance from flight track, km	Station number	Micro-phone	Δp_o, N/m^2	ΔT, sec	Δt_o, sec	I_o, $N\text{-}sec/m^2$	τ, sec	$\tau_{1/2}$, sec	Type signature (fig. 5)
12-16-66	SR-20	9	9.26 N	LAC	25	34.95	0.222	-----	---	0.0110	------	NR
					26	*37.83*	.222	-----	---	*.0110*	------	*NR*
					27	41.18	.222	-----	---	.0090	------	NR
					28	35.43	.222	-----	---	.0100	------	NR
					29	33.04	.223	-----	---	.0140	------	NR
					30	32.04	.223	-----	---	.0100	------	NR
					31	40.22	.223	-----	---	.0095	------	NR
					32	41.18	.224	-----	---	.0075	------	NR
					33	38.30	.224	-----	---	.0110	------	NR
					34	35.43	.224	-----	---	.0100	------	NR
					35	39.74	.224	-----	---	.0105	------	NR
					36	40.22	.224	-----	---	.0060	------	NR
					37	40.22	.224	-----	---	.0050	------	NR
					38	37.83	.223	-----	---	.0100	------	NR
					39	36.87	.223	-----	---	.0100	------	NR
					40	38.30	.224	-----	---	.0080	------	NR
					41	40.22	.223	-----	---	.0070	------	NR
					42	44.53	.223	-----	---	.0050	------	NR
	SR-21	7	2.2 N	V-3	1	44.53	0.234	-----	---	0.0110	------	NR
					2	41.66	.234	-----	---	.0120	------	NR
					3	44.53	.236	-----	---	.0060	------	NP
					4	45.96	.234	-----	---	.0080	------	NR
					5	44.05	.234	-----	---	.0100	------	NR
		9	19.6 N	V-4	1	33.52	0.220	-----	---	0.0100	------	NR
					2	32.56	.219	-----	---	.0100	------	NR
					3	32.56	.219	-----	---	.0060	------	NR
					4	32.08	.219	-----	---	.0060	------	NR
					5	30.64	.220	-----	---	.0060	------	NR
				Tango	1	25.38	0.220	-----	---	0.0060	------	NR
					2	24.42	.220	-----	---	.0065	------	NR
					3	25.86	.220	-----	---	.0060	------	NR
					4	25.38	.220	-----	---	.0070	------	NR
					5	24.90	.220	-----	---	.0055	------	NR
					6	13.41	----	-----	---	-----	------	--
				FRC	*1*	*31.12*	*0.218*	-----	---	*0.0085*	------	*NR*
					2	27.29	.218	-----	---	.0120	------	NR
					3	27.29	.218	-----	---	.0120	------	NR
					4	30.16	.218	-----	---	.0120	------	NR
					5	29.68	.218	-----	---	.0080	------	NR
					6	25.86	.218	-----	---	.0090	------	NR
					7	26.81	.218	-----	---	.0100	------	NR
					8	27.77	.218	-----	---	.0075	------	NR
					9	29.69	.219	-----	---	.0070	------	NR
					10	31.60	.219	-----	---	.0070	------	NR
					11	29.21	.219	-----	---	.0100	------	NR
					12	28.73	.219	-----	---	.0120	------	NR
		3	45.6 N	FRC	13	18.67	≈0.219	-----	---	0.0130	------	NR
					14	16.76	≈.219	-----	---	.0150	------	NR
					15	17.24	≈.219	-----	---	.0180	------	NR
					16	18.19	≈.219	-----	---	.0165	------	NR
		9	19.6 N	LAC	25	29.21	0.227	-----	---	0.0055	------	NR
					26	34.47	.228	-----	---	.0060	------	NR
					27	34.95	.228	-----	---	.0090	------	NR
					28	30.64	.228	-----	---	.0070	------	NR
					29	31.12	.228	-----	---	.0070	------	NR
					30	31.60	.228	-----	---	.0050	------	NR
					31	32.56	.229	-----	---	.0030	------	NR
					32	33.52	.221	-----	---	.0100	------	NR
					33	34.95	.220	-----	---	.0110	------	NR
					34	36.39	.221	-----	---	.0090	------	NR
					35	34.47	.220	-----	---	.0070	------	NR
					36	35.43	.220	-----	---	.0070	------	NR
					37	34.95	.221	-----	---	.0060	------	NR
					38	38.30	.221	-----	---	.0100	------	NR
					39	33.52	.221	-----	---	.0085	------	NR
					40	35.43	.221	-----	---	.0080	------	NR
					41	33.99	.220	-----	---	.0075	------	NR
					42	35.43	.220	-----	---	.0060	------	NR
12-19-66	SR-22	9	3.7 S	V-1	1	44.53	0.234	0.1260	3.41	0.0110	0.0015	NR
					2	48.84	.234	.1265	3.46	.0080	.0015	NR
					3	47.40	.234	.1235	3.46	.0080	.0015	NR
					4	36.87	.234	.1235	2.70	.0150	.002	NR
		4	0	V-2	1	46.92	0.232	0.1265	3.55	0.0075	0.00125	NR
					2	46.92	.233	.1260	3.38	.0080	.0015	NR
					3	47.40	.232	.1265	3.61	.0090	.0015	NR
					4	47.40	.233	.1199	3.20	.0050	.001	NP

TABLE III.- SUMMARY OF SONIC-BOOM DATA FOR SR-71 MISSIONS FLOWN AT EDWARDS AIR FORCE BASE – Continued

Date	Mission number	Site	Site distance from flight track, km	Station number	Micro-phone	Δp_o, N/m^2	ΔT, sec	Δt_o, sec	I_o, $N\text{-sec}/m^2$	τ, sec	$\tau_{1/2}$, sec	Type signature (fig. 5)
12-19-66	SR-22	7	35.2 S	V-3	1	21.55	0.217	-----	---	0.0270	------	R
					2	20.59	.217	-----	---	.0230	------	R
					3	21.07	.217	-----	---	.0170	------	R
					4	21.07	.217	-----	---	.0240	------	R
					5	21.07	.217	-----	---	.0250	------	R
		9	3.7 S	V-4	1	41.66	0.234	0.1355	3.01	0.0080	0.001	NR
					2	40.70	.234	.1285	2.99	.0130	.0015	NR
					3	38.78	.234	.1350	2.99	.0070	.00125	NR
					4	38.78	.234	.1305	2.93	.0080	.0015	NR
					5	42.13	.234	.1390	3.28	.0080	.002	NR
		6	20.1 S	V-5	1	24.90	0.221	-----	---	0.0280	------	NR
					2	27.29	.221	-----	---	.0250	------	NR
					3	26.81	.222	-----	---	.0180	------	NR
					4	28.25	.221	-----	---	.0150	------	NR
					5	26.81	.221	-----	---	.0270	------	NR
		9	3.7 S	V-6	1	41.66	0.236	0.1335	3.16	0.0125	0.0015	NR
					2	43.09	.236	.1280	2.89	.0130	.002	NR
					3	42.61	.236	.1370	3.23	.0070	.001	NP
				Tango	1	48.36	0.234	0.1300	3.25	0.0050	0.001	NP
					2	44.53	.234	.1220	2.97	.0140	.001	NR
					3	46.44	.234	.1310	3.17	.0130	.001	NR
					4	48.36	.234	.1125	2.86	.0070	.0015	NP
					5	46.92	.234	.1234	3.05	.0120	.001	NR
					6	24.42	----	-----	---	-----	------	--
				FRC	1	45.00	0.231	0.1290	3.15	0.0075	0.002	NR
					2	49.32	.232	.1415	3.93	.0080	.0015	NR
					3	40.22	.231	.1285	2.76	.0100	.0025	NR
					4	41.18	.232	.1255	2.78	.0100	.002	NR
					5	42.13	.231	.1310	3.01	.0100	.002	NR
					6	39.26	.232	.1330	2.83	.0130	.002	NR
					7	43.57	.231	.1342	3.19	.0125	.0015	NR
					8	----	----	-----	---	-----	------	--
					9	39.26	.231	.1248	2.52	.0075	.0015	NR
					10	40.22	.232	.1312	2.86	.0070	.002	NR
					11	40.70	.231	.1283	2.73	.0110	.0015	NR
					12	39.74	.231	.1293	2.64	.0120	.002	NR
				LAC	25	40.70	0.235	0.1350	3.05	0.0130	0.0015	NR
					26	44.05	.235	.1322	3.13	.0120	.0015	NR
					27	48.84	.235	.1322	3.51	.0090	.0015	NR
					28	44.05	.234	.1289	3.11	.0070	.0015	NR
					29	46.92	.235	.1328	3.48	.0090	.0015	NR
					30	46.92	.235	.1300	3.30	.0130	.001	NR
					31	46.44	.235	.1333	3.50	.0130	.0015	NR
					32	42.13	.236	.1370	3.43	.0080	.0015	NR
					33	41.66	.237	.1338	3.18	.0160	.0015	NR
					34	45.01	.236	.1283	3.16	.0130	.002	NR
					35	41.18	.236	.1288	3.44	.0110	.00125	NR
					36	----	----	-----	---	-----	------	--
					37	37.83	.237	.1365	3.14	.0110	.00125	NR
					38	43.09	.236	.1283	3.26	.0080	.001	NR
					39	42.13	.236	.1272	3.01	.0140	.0015	NR
					40	38.78	.236	.1239	2.81	.0170	.00175	NR
					41	37.83	.237	.1316	2.84	.0170	.0015	NR
					42	43.57	.235	.1332	3.32	.0070	.0015	NR
12-20-66	SR-23	1	44.4 N	V-1	1	26.81	----	-----	---	0.0100	------	CO
					2	28.73	----	-----	---	.0110	------	CO
					3	25.38	----	-----	---	.0165	------	CO
					4	----	----	-----	---	-----	------	--
		2	32.6 N	V-2	1	25.38	0.226	-----	---	0.0420	------	NR
					2	26.33	.226	-----	---	.0430	------	NR
					3	23.94	.226	-----	---	.0440	------	NR
					4	24.42	.226	-----	---	.0420	------	NR
		7	20.4 S	V-3	1	33.99	0.230	-----	---	0.0180	------	NR
					2	38.30	.227	-----	---	.0100	------	NR
					3	42.61	.226	-----	---	.0090	------	NR
					4	36.39	.230	-----	---	.0095	------	NR
					5	30.64	.225	-----	---	.0100	------	NR
		9	4.67 S	V-4	1	37.35	0.238	0.1350	2.69	0.0220	0.004	NR
					2	37.83	.239	.1350	2.87	.0200	.0035	NR
					3	36.39	.239	.1335	2.64	.0205	.0035	NR
					4	36.39	.239	.1410	2.79	.0220	.0035	NR
					5	40.22	.239	.1415	2.90	.0200	.0035	NR
		6	6.30 S	V-5	1	37.83	0.236	0.1380	2.90	0.0185	0.0025	NR
					2	38.30	.236	.1390	2.74	.0170	.003	NR
					3	38.30	.236	.1340	2.83	.0190	.003	NR
					4	43.57	.236	.1190	2.70	.0075	.003	NP
					5	37.35	.236	.1309	2.64	.0130	.002	NR

TABLE III.- SUMMARY OF SONIC-BOOM DATA FOR SR-71 MISSIONS FLOWN AT EDWARDS AIR FORCE BASE – Continued

Date	Mission number	Site	Site distance from flight track, km	Station number	Micro-phone	Δp_o, N/m^2	ΔT, sec	Δt_o, sec	I_o, $N\text{-sec}/m^2$	τ, sec	$\tau_{1/2}$, sec	Type signature (fig. 5)
12-20-66	SR-23	8	31.5 S	V-6	1	14.84	0.235	-----	---	0.0520	------	CO
					2	15.32	.235	-----	---	.0530	------	CO
					3	16.28	.235	-----	---	.0515	------	CO
		9	4.67 S	Tango	1	35.43	0.237	0.1371	3.05	0.0270	0.003	NR
					2	35.91	.237	.1440	2.91	.0240	.0025	NR
					3	35.43	.237	.1215	2.80	.0230	.0025	NR
					4	36.39	.236	.1328	2.75	.0155	.002	NR
					5	36.39	.236	.1430	3.00	.0255	.002	NR
					6	17.24	----	-----	---	-----	------	--
				FRC	1	42.13	0.234	-----	2.90	0.0330	0.0065	NR
					2	45.49	.234	-----	3.50	.0320	.006	NR
					3	39.26	.234	-----	2.94	.0280	.0055	NR
					4	42.61	.234	-----	3.02	.0280	.006	NR
					5	40.22	.234	-----	2.91	.0270	.006	NR
					6	40.22	.234	-----	2.92	.0230	.0045	NR
					7	41.18	.234	-----	2.89	.0235	.0045	NR
					8	----	----	-----	---	-----	------	--
					9	38.78	0.234	-----	2.81	.0220	.0045	NR
					10	42.61	.235	-----	3.21	.0235	.0055	NR
					11	39.26	.234	-----	2.90	.0205	.005	NR
					12	36.39	.234	-----	2.70	.0210	.005	NR
12-21-66	SR-24	9	5.09 S	V-1	1	47.40	0.251	0.1385	3.59	0.0100	0.001	NR
					2	46.92	.251	.1370	3.50	.0130	.00075	NR
					3	45.97	.250	.1380	3.52	.0065	.001	NR
					4	38.30	.250	.1355	2.68	.0070	.0015	NR
		4	15.2 N	V-2	1	37.35	0.244	-----	---	0.0140	------	NR
					2	34.95	.243	-----	---	.0160	------	NR
					3	36.39	.243	-----	---	.0180	------	NR
					4	33.52	.243	-----	---	.0140	------	NR
		7	22 S	V-3	1	27.77	0.240	-----	---	0.0190	------	NR
					2	28.73	.242	-----	---	.0070	------	NR
					3	28.73	.241	-----	---	.0060	------	NR
					4	27.77	.240	-----	---	.0140	------	NR
					5	28.73	.241	-----	---	.0160	------	NR
		9	5.09 S	V-4	1	41.66	0.254	0.1385	3.13	0.0110	0.0005	NR
					2	42.13	.254	.1340	3.14	.0110	.0005	NR
					3	42.61	.254	.1370	3.07	.0035	.00075	NR
					4	41.18	.254	.1330	3.11	.0050	.001	NR
					5	40.22	.254	.1350	3.17	.0090	.001	NR
		6	6.85 S	V-5	1	39.26	0.241	0.1395	2.98	0.0130	0.001	NR
					2	37.83	.242	.1365	2.78	.0135	.0015	NR
					3	38.30	.242	.1325	2.94	.0175	.0015	NR
					4	39.74	.242	.1290	2.74	.0065	.0005	NP
					5	33.52	.241	.1380	2.52	.0115	.001	NR
		9	5.09 S	V-6	1	41.66	0.251	0.1400	3.28	0.0050	0.0005	NP
					2	43.09	.252	.1350	2.85	.0120	.00075	PP
					3	43.57	.252	.1515	3.41	.0050	.00075	NP
				Tango	1	39.26	0.251	0.1388	3.32	0.0130	0.0005	NR
					2	40.22	.251	.1303	3.12	.0060	.0005	NR
					3	44.05	.251	.1353	3.14	.0070	.001	NR
					4	42.13	.251	.1240	3.01	.0050	.0005	NR
					5	42.13	.250	.1305	3.25	.0040	.0005	NP
					6	21.55	----	-----	---	-----	------	--
				FRC	1	38.30	0.248	0.1375	2.73	0.0075	0.001	NR
					2	35.91	.248	.1370	2.77	.0070	.00075	NR
					3	36.39	.248	.1355	2.73	.0090	.0005	NR
					4	43.09	.248	.1415	3.38	.0105	.0005	NR
					5	40.22	.248	.1345	3.04	.0110	.0005	NR
					6	39.26	.248	.1395	2.98	.0100	.00125	NR
					7	39.74	.248	.1330	2.86	.0075	.001	NR
					8	36.39	.248	.1315	2.70	.0070	.001	NR
					9	38.30	.248	.1255	2.55	.0090	.00075	NR
					10	43.09	.248	.1385	3.21	.0120	.00075	NR
					11	37.83	.248	.1295	2.77	.0110	.0005	NR
					12	37.35	.248	.1285	2.72	.0120	.0005	NR
		3	20.6 N	FRC	13	30.16	0.242	-----	---	0.0210	------	NR
					14	31.12	.242	-----	---	.0130	------	NR
					15	30.64	.242	-----	---	.0150	------	NR
					16	30.64	.242	-----	---	.0260	------	NR

TABLE III.- SUMMARY OF SONIC-BOOM DATA FOR SR-71 MISSIONS FLOWN AT EDWARDS AIR FORCE BASE – Continued

Date	Mission number	Site	Site distance from flight track, km	Station number	Micro-phone	Δp_o, N/m^2	ΔT, sec	Δt_o, sec	I_o, $N\text{-}sec/m^2$	τ, sec	$\tau_{1/2}$, sec	Type signature (fig. 5)
12-21-66	SR-24	9	5.09 S	LAC	25	45.49	0.258	0.1400	3.73	0.0060	0.001	NR
					26	43.57	.257	.1367	3.33	.0120	.0015	NR
					27	50.75	.258	.1351	4.00	.0050	.0005	NR
					28	44.05	.258	.1356	3.27	.0090	.001	NR
					29	55.54	.258	.1362	4.23	.0100	.0005	NR
					30	41.66	.258	.1323	3.18	.0060	.0005	NR
					31	48.36	.258	.1400	3.46	.0100	.001	NR
					32	44.05	.258	.1325	3.24	.0090	.001	NR
					33	40.22	.257	.1336	3.13	.0130	.001	NR
					34	46.44	.257	.1391	3.54	.0115	.0005	NR
					35	43.57	.258	.1380	3.41	.0050	.0005	NR
					36	43.09	.258	.1430	3.45	.0060	.001	NR
					37	47.88	.257	.1325	3.60	.0100	.00075	NR
					38	43.57	.258	.1415	3.55	.0060	.00075	NR
					39	45.96	.258	.1380	3.53	.0060	.001	NR
					40	49.80	.256	.1358	3.91	.0070	.001	NR
					41	48.84	.258	.1468	3.85	.0100	.001	NR
					42	51.23	.258	.1413	3.94	.0110	.001	NR
	SR-25	4	18.7 N	V-2	1	35.91	0.228	-----	---	0.0060	------	NP
					2	34.95	.229	-----	---	.0035	------	NP
					3	37.34	.230	-----	---	.0075	------	NP
					4	33.04	.228	-----	---	.0120	------	NR
		7	27.8 S	V-3	1	23.94	0.226	-----	---	0.0275	------	R
					2	22.98	.229	-----	---	.0300	------	R
					3	25.86	.229	-----	---	.0470	------	R
					4	25.38	.230	-----	---	.0190	------	R
					5	24.90	.226	-----	---	.0260	------	R
		9	4.07 N	V-4	1	30.64	0.236	0.1380	2.64	0.0300	0.0015	NR
					2	31.60	.236	.1375	2.64	.0300	.0015	NR
					3	32.56	.236	.1345	2.60	.0110	.002	NR
					4	32.08	.236	.1350	2.56	.0280	.002	NR
					5	31.12	.237	.1320	2.49	.0260	.001	NR
		6	8.52 S	V-5	1	----	----	-----	---	-----	------	--
					2	----	----	-----	---	-----	------	--
					3	33.04	0.236	-----	---	0.0055	------	NP
					4	32.56	.234	-----	---	.0200	------	NR
					5	26.33	.235	-----	---	.0055	------	NR
		9	4.07 N	V-6	1	29.69	0.234	0.1380	2.59	0.0140	0.0025	NR
					2	29.69	.234	.1320	2.34	.0170	.0025	NR
					3	29.21	.234	.1435	2.62	.0160	.0025	NR
				Tango	1	39.26	0.232	0.1310	2.81	0.0060	0.001	NR
					2	40.70	.232	.1250	2.46	.0075	.0015	NR
					3	39.26	.232	.1335	2.57	.0070	.0015	NR
					4	36.87	.232	.1190	2.38	.0050	.001	NR
					5	42.61	.232	.1250	2.51	.0070	.0025	NR
					6	21.07	----	-----	---	-----	------	--
				FRC	1	32.08	0.231	0.1295	2.31	0.0080	0.001	NR
					2	29.21	.231	.1314	2.19	.0170	.0015	NR
					3	30.64	.231	.1370	2.40	.0200	.002	NR
					4	33.04	.232	.1380	2.69	.0180	.002	NR
					5	31.12	.231	.1300	2.47	.0175	.002	NR
					6	31.60	.231	.1300	2.34	.0160	.0015	NR
					7	28.25	.231	.1315	2.15	.0140	.0015	NR
					8	29.69	.231	.1325	2.08	.0150	.002	NR
					9	26.33	.231	.1265	2.18	.0140	.002	NR
					10	33.52	.231	.1355	2.66	.0280	.0025	NR
					11	28.73	.231	.1305	2.24	.0290	.002	NR
					12	28.73	.231	.1305	2.14	.0285	.0015	NR
		3	25.5 N	FRC	13	25.38	0.224	-----	---	0.0190	------	NR
					14	22.98	.223	-----	---	.0200	------	PR
					15	23.94	.224	-----	---	.0080	------	NR
					16	22.50	.224	-----	---	.0140	------	NR
1-6-67	SR-27	5	9.63 N	V-1	1	37.82	0.226	-----	---	0.0125	------	NR
					2	37.35	.228	-----	---	.0135	------	NR
					3	33.52	.227	-----	---	.0100	------	NR
					4	33.52	.228	-----	---	.0200	------	NR
				V-2	1	35.43	0.228	-----	---	0.0100	------	NR
					2	39.26	.228	-----	---	.0045	------	NN
					3	36.39	.228	-----	---	.0060	------	NN
					4	37.35	.228	-----	---	.0200	------	R
				V-3	1	35.91	0.234	-----	---	0.0100	------	NR
					2	46.92	.235	-----	---	.0035	------	NP
					3	35.43	.234	-----	---	.0230	------	R
					4	35.91	.234	-----	---	.0160	------	NR
					5	50.27	.235	-----	---	.0055	------	P

TABLE III.- SUMMARY OF SONIC-BOOM DATA FOR SR-71 MISSIONS FLOWN AT EDWARDS AIR FORCE BASE – Continued

Date	Mission number	Site	Site distance from flight track, km	Station number	Micro-phone	Δp_o, N/m^2	ΔT, sec	Δt_o, sec	I_o, $N\text{-sec}/m^2$	τ, sec	$\tau_{1/2}$, sec	Type signature (fig. 5)
1-6-67	SR-27	5	9.63 N	V-4	1	39.26	0.235	-----	---	0.0210	------	NR
					2	36.87	.235	-----	---	.0240	------	NR
					3	33.04	.236	-----	---	.0380	------	NR
					4	33.04	.235	-----	---	.0065	------	NP
					5	31.12	.236	-----	---	.0105	------	NR
				V-5	1	35.43	0.232	-----	---	0.0190	------	NR
					2	35.91	.232	-----	---	.0160	------	NR
					3	33.99	.232	-----	---	.0190	------	NR
					4	34.95	.233	-----	---	.0140	------	NR
					5	29.21	.232	-----	---	.0270	------	NR
				V-6	1	36.87	0.233	-----	---	0.0290	------	R
					2	37.35	.231	-----	---	.0180	------	R
					3	45.01	.231	-----	---	.0100	------	NR
				FRC	1	41.66	0.228	-----	---	0.0120	------	NR
					2	39.74	.228	-----	---	.0130	------	NR
					3	36.87	.227	-----	---	.0050	------	NP
					4	38.30	.228	-----	---	.0200	------	PR
					5	31.60	.227	-----	---	.0240	------	NR
					6	32.08	.228	-----	---	.0260	------	NR
					7	31.12	.226	-----	---	.0080	------	NR
					8	41.18	.227	-----	---	.0100	------	NR
					9	37.35	.226	-----	---	.0130	------	NR
					10	44.53	.226	-----	---	.0160	------	NR
					11	33.04	.226	-----	---	.0215	------	NR
					12	32.08	.227	-----	---	.0230	------	NR
					13	36.87	.232	-----	---	.0290	------	NR
					14	39.74	.234	-----	---	.0070	------	NR
					15	42.13	.233	-----	---	.0200	------	NR
					16	45.48	.232	-----	---	.0170	------	NR
1-10-67	SR-28	1	30.9 N	V-1	1	13.88	0.166	-----	---	0.0220	------	R
					2	13.41	.166	-----	---	.0230	------	R
					3	13.41	.166	-----	---	.0240	------	R
					4	----	----	-----	---	-----	------	--
		2	19.8 N	V-2	1	48.84	0.160	-----	---	0.0050	------	NP
					2	40.70	.160	-----	---	.0070	------	NP
					3	43.09	.160	-----	---	.0095	------	NP
					4	41.66	.160	-----	---	.0075	------	NP
		7	31.5 S	V-3	1	25.38	0.161	-----	---	0.0260	------	R
					2	23.94	.162	-----	---	.0275	------	R
					3	26.33	.161	-----	---	.0090	------	NR
					4	24.42	.162	-----	---	.0310	------	R
					5	23.46	.160	-----	---	.0110	------	NR
		9	0.46 S	V-4	1	----	----	-----	---	-----	------	--
					2	76.13	0.171	0.0910	3.60	0.0040	0.0003	NP
					3	75.65	.172	.0890	3.36	.0040	.0003	NP
					4	75.65	.172	.0895	3.74	.0045	.0005	NP
					5	77.09	.172	.0880	3.50	.0055	.0005	NP
		6	16.6 S	V-5	1	45.01	0.155	-----	---	0.0050	------	NP
					2	47.40	.155	-----	---	.0050	------	NP
					3	50.75	.154	-----	---	.0040	------	NP
					4	44.53	.154	-----	---	.0055	------	NP
					5	42.61	.154	-----	---	.0120	------	NR
		8	42.6 S	V-6	1	12.45	0.164	-----	---	0.0350	------	CO
					2	11.97	.164	-----	---	.0250	------	CO
					3	12.45	.165	-----	---	.0230	------	CO
		9	0.46 S	Tango	1	63.20	0.167	0.0980	3.38	0.0050	0.00075	NR
					2	59.85	.168	.0935	3.31	.0055	.0005	NR
					3	62.24	.168	.0975	3.29	.0055	.0005	NR
					4	68.47	.168	.0860	3.13	.0050	.00025	NP
					5	59.37	.168	.0928	3.44	.0060	.0003	NR
					6	29.69	----	-----	---	-----	------	--
				FRC	1	63.68	0.167	0.0890	3.17	0.0060	0.0002	NP
					2	77.57	.168	.0965	4.38	.0070	.0005	NP
					3	67.99	.168	.0900	3.28	.0070	.0003	NP
					4	73.26	.168	.0905	3.72	.0055	.0005	NP
					5	66.55	.168	.0885	3.21	.0055	.0003	NP
					6	63.20	.168	.0875	2.93	.0070	.0005	NP
					7	67.03	.168	.0880	3.23	.0055	.0005	NP
					8	66.55	.168	.0910	3.29	.0070	.0003	NP
					9	70.86	.168	.0845	3.13	.0065	.0003	NP
					10	74.21	.168	.0860	3.41	.0050	.0005	NP
					11	----	----	-----	---	-----	------	--
					12	65.12	.168	.0905	3.15	.0045	.0005	NP
		3	7.78 N	FRC	13	66.55	0.165	-----	---	0.0050	0.0050	NP
					14	64.16	.164	-----	---	.0050	------	NP
					15	62.24	.164	-----	---	.0060	------	NP
					16	68.95	.164	-----	---	.0050	------	NP

TABLE III.- SUMMARY OF SONIC-BOOM DATA FOR SR-71 MISSIONS FLOWN AT EDWARDS AIR FORCE BASE – Continued

Date	Mission number	Site	Site distance from flight track, km	Station number	Micro-phone	Δp_o, N/m^2	ΔT, sec	Δt_o, sec	I_o, $N\text{-sec}/m^2$	τ, sec	$\tau_{1/2}$, sec	Type signature (fig. 5)
1-13-67	SR-29	1	27.6 N	V-1	1	34.47	0.202	-----	---	0.0245	------	PR
					2	33.04	.201	-----	---	.0230	------	NR
					3	33.52	.203	-----	---	.0210	------	PR
					4	-----	----	-----	---	-----	------	--
		2	16.3 N	V-2	1	45.97	0.196	-----	---	0.0040	------	NP
					2	33.52	.196	-----	---	.0075	------	NR
					3	34.47	.197	-----	---	.0170	------	NR
					4	51.23	.196	-----	---	.0020	------	P
		7	35.2 S	V-3	1	20.59	0.195	-----	---	0.0260	------	R
					2	20.59	.196	-----	---	.0190	------	R
					3	21.07	.196	-----	---	.0055	------	--
					4	22.50	.196	-----	---	.0295	------	R
					5	-----	----	-----	---	-----	------	--
		9	4.35 S	V-4	1	45.01	0.222	0.1120	2.96	0.0200	0.0005	NR
					2	44.05	.222	.1120	2.94	.0190	.0005	NR
					3	45.01	.221	.1136	2.88	.0040	.0005	NR
					4	45.97	.221	.1125	2.87	.0040	.0005	NR
					5	48.84	.221	.1104	2.81	.0055	.0005	NR
		6	20.6 S	V-5	1	44.53	0.219	-----	---	0.0160	------	NR
					2	44.53	.219	-----	---	.0095	------	NR
					3	40.70	.219	-----	---	.0150	------	NR
					4	39.26	.218	-----	---	.0140	------	NR
					5	39.26	.218	-----	---	.0085	------	NR
		9	4.35 S	Tango	1	68.47	0.216	0.1020	3.01	0.0045	0.00075	PP
					2	66.55	.217	.0970	2.90	.0045	.00025	NP
					3	69.90	.216	.1040	3.09	.0040	.00025	PP
					4	79.48	.216	.0910	2.80	.0040	.0001	AP
					5	75.65	.217	.1045	3.12	.0035	.0001	AP
					6	45.01	----	-----	---	-----	------	--
				FRC	1	44.05	0.214	0.1110	2.77	0.0170	0.001	NR
					2	41.18	.214	.1130	2.64	.0070	.001	NR
					3	*41.66*	*.214*	*.1067*	*2.62*	*.0080*	*.0005*	*NR*
					4	43.09	.214	.1043	2.64	.0130	.0005	NR
					5	40.22	.215	.1029	2.41	.0200	.0005	NR
					6	39.74	.214	.1072	2.27	.0140	.001	NR
					7	41.66	.213	.1140	2.59	.0170	.001	NR
					8	39.74	.213	.1072	2.41	.0160	.001	NR
					9	39.74	.213	.1040	2.35	.0055	.0005	NR
					10	47.88	.214	.1120	3.08	.0210	.0005	NR
					11	40.70	.214	.1075	2.62	.0160	.0005	NR
					12	39.26	.214	.1115	2.62	.0220	.0005	NR
		3	4.26 N	FRC	13	43.57	0.214	0.1220	2.78	0.0080	0.0025	NR
					14	41.18	.215	.1198	2.68	.0125	.002	NR
					15	41.66	.215	.1140	2.52	.0055	.001	NP
					16	45.49	.214	.1155	2.71	.0060	.001	NP
		9	4.35 S	LAC	25	45.49	0.220	0.1155	2.92	0.0150	0.001	NR
					26	55.54	.220	.1130	3.51	.0140	.001	NR
					27	46.44	.220	.1135	3.06	.0090	.001	NR
					28	47.88	.219	.1110	2.94	.0040	.001	NR
					29	49.80	.220	.1170	3.34	.0160	.001	NR
					30	48.36	.220	.1100	3.06	.0110	.001	NR
					31	46.44	.218	.1190	2.78	.0100	.001	NR
					32	49.32	.216	.1060	3.03	.0020	.00075	NP
					33	----	----	-----	---	-----	------	--
					34	50.27	.216	.1105	3.02	.0020	.001	NP
					35	49.80	.215	.1120	3.21	.0020	.00075	NP
					36	45.97	.215	.1125	3.03	.0040	.001	NP
					37	57.94	.216	.1100	3.24	.0040	.001	NP
					38	53.63	.216	.1130	3.44	.0015	.0005	NP
					39	61.77	.216	.1120	3.83	.0030	.001	NP
					40	57.46	.216	.1120	3.36	.0045	.001	NP
					41	53.15	.216	.1115	2.97	.0040	.001	NP
					42	59.37	.216	.1140	3.11	.0035	.001	NP
1-17-67	SR-30	9	0.20 S	V-4	1	98.63	0.164	0.0820	4.14	0.0010	0.0005	NP
					2	95.76	.164	.0820	3.96	.0005	.001	NP
					3	85.71	.164	.0835	3.92	.0050	.00075	NP
					4	92.89	.164	.0845	4.16	.0020	.001	NP
					5	78.52	.164	.0875	4.04	.0060	.001	NP
				Tango	1	115.87	0.163	0.0850	4.74	0.0010	0.0005	PP
					2	139.81	.163	.0845	4.45	.0010	.001	P
					3	121.14	.163	.0835	4.72	.0050	.001	NP
					4	121.14	.163	.0775	4.35	.0050	.00125	NP
					5	124.01	.163	.0845	4.75	.0030	.001	NP
					6	-----	----	-----	---	-----	------	--

TABLE III.- SUMMARY OF SONIC-BOOM DATA FOR SR-71 MISSIONS FLOWN AT EDWARDS AIR FORCE BASE – *Continued*

Date	Mission number	Site	Site distance from flight track, km	Station number	Micro-phone	Δp_o, N/m^2	ΔT, sec	Δt_o, sec	I_o, $N\text{-sec}/m^2$	τ, sec	$\tau_{1/2}$, sec	Type signature (fig. 5)
1-17-67	SR-30	9	0.20 S	FRC	1	96.72	0.162	0.0815	3.73	0.0050	0.0015	NP
					2	95.76	.162	.0854	3.92	.0070	.0005	NP
					3	90.97	.162	.0810	3.77	.0070	.001	NR
					4	102.94	.162	.0884	4.71	.0055	.0005	NR
					5	85.71	.162	.0815	3.93	.0065	.0005	NR
					6	79.96	.162	.0825	3.84	.0120	.001	NR
					7	77.57	.162	.0840	3.73	.0170	.0015	NR
					8	72.78	.162	.0820	3.18	.0130	.0005	NR
					9	117.79	.162	.0790	3.85	.0005	.001	SP
					10	99.11	.162	.0909	5.00	.0055	.001	PR
					11	91.93	.162	.0820	4.14	.0070	.0005	PR
					12	93.37	.163	.0855	4.26	.0090	.001	PR
				LAC	25	95.28	0.168	0.0900	4.76	0.0140	0.0015	NR
					26	94.32	.169	.0917	5.12	.0150	.002	NR
					27	85.71	.169	.0906	4.72	.0170	.002	NR
					28	87.62	.169	.0917	4.85	.0120	.0015	NR
					29	103.90	.169	.0894	5.05	.0130	.001	NR
					30	106.77	.165	.0906	5.28	.0120	.0015	NR
					31	98.63	.164	.0972	4.92	.0090	.00125	NR
					32	89.54	.164	.0875	4.39	.0040	.0015	NP
					33	91.93	.164	.0891	4.32	.0090	.001	PP
					34	99.59	.164	.0853	4.50	.0040	.00075	NP
					35	95.28	.163	.0864	4.28	.0060	.001	NR
					36	95.76	.163	.0864	4.63	.0010	.001	NP
					37	95.28	.165	.0891	4.53	.0010	.001	NP
					38	121.62	.163	.0875	4.46	.0015	.00075	NP
					39	118.26	.164	.0897	4.66	.0010	.0005	NP
					40	148.43	.163	.0831	5.16	.0005	.0005	SP
					41	100.55	.164	.0864	4.18	.0030	.0005	NP
					42	88.58	.164	.0946	4.29	.0055	.0005	NP
	SR-31	9	0.20 S	FRC	1	100.07	0.160	0.0860	4.32	0.0025	0.001	NP
					2	124.01	.161	.0855	4.22	.0005	.0005	SP
					3	113.96	.161	.0835	4.46	.0050	.001	NR
					4	133.11	.161	.0875	5.41	.0060	.0015	NR
					5	111.56	.162	.0850	4.48	.0070	.001	NR
					6	115.39	.161	.0826	4.48	.0060	.0005	PP
					7	117.79	.160	.0815	4.25	.0015	.001	NP
					8	101.98	.160	.0844	3.68	.0070	.001	NP
					9	128.32	.160	.0825	4.50	.0060	.001	NP
					10	140.29	.160	.0923	5.77	.0055	.001	NP
					11	122.57	.161	.0874	4.61	.0070	.00125	NP
					12	114.91	.161	.0859	4.67	.0070	.00125	NR
				LAC	25	139.33	0.167	0.0860	5.38	0.0030	0.00075	NP
					26	150.82	.166	.0860	5.71	.0030	.001	NP
					27	140.29	.166	.0870	5.39	.0030	.001	NP
					28	155.13	.166	.0850	5.42	.001	.001	SP
					29	146.03	.165	.0885	5.60	.0055	.00125	NR
					30	150.82	.165	.0860	6.01	.0080	.001	NR
					31	112.04	.166	.0920	5.86	.0070	.0005	NR
					32	124.97	.162	.0850	5.21	.0060	.001	NR
					33	117.79	.162	.0860	5.00	.0100	.00075	NR
					34	119.70	.162	.0860	4.95	.0110	.0015	NR
					35	114.91	.162	.0875	4.83	.0100	.001	PR
					36	125.45	.162	.0875	5.44	.0100	.0005	NR
					37	112.52	.162	.0850	4.84	.0080	.0005	PR
					38	113.48	.162	.0895	6.10	.0080	.001	PR
					39	119.70	.162	.0885	5.18	.0150	.0015	PR
					40	138.37	.163	.0890	6.06	.0110	.001	NR
					41	110.12	.162	.0880	5.01	.0100	.00075	NR
					42	96.72	.162	.0850	5.02	.0020	.0005	NP
				V-4	1	126.40	0.164	0.0885	5.53	0.0055	0.00125	NR
					2	118.74	.164	.0880	4.63	.0055	.0015	NR
					3	111.56	.163	.0875	4.73	.0055	.0015	NR
					4	116.35	.163	.0885	5.08	.0090	.00125	NR
					5	104.38	.163	.0845	4.84	.0080	.0005	NR
				Tango	1	119.22	0.162	0.0900	5.29	0.0060	0.0005	NR
					2	114.43	.163	.0910	5.12	.0115	.001	NR
					3	126.40	.163	.0930	5.37	.0055	.001	NP
					4	116.83	.163	.0815	4.82	.0065	.00125	NP
					5	114.91	.163	.0880	5.22	.0105	.001	NR
					6	57.46	-----	------	---	-----	------	--
6-9-66	SR-a	5	1.07 N	V-1	1	44.53	0.193	0.1150	2.51	0.0340	0.006	CO
					2	73.74	.194	.1120	3.16	.0240	.008	CO
					3	76.61	.193	.1170	2.95	.0125	.007	CO
				V-2	1	81.40	≈0.197	0.0910	4.09	0.0060	0.003	CO
					2	81.40	≈.197	.1040	3.88	.0100	.001	CO
					3	60.81	≈.197	.1005	3.72	.0085	.0055	CO

TABLE III.- SUMMARY OF SONIC-BOOM DATA FOR SR-71 MISSIONS FLOWN AT EDWARDS AIR FORCE BASE – Continued

Date	Mission number	Site	Site distance from flight track, km	Station number	Micro-phone	Δp_o, N/m^2	ΔT, sec	Δt_o, sec	I_o, $N\text{-}sec/m^2$	τ, sec	$\tau_{1/2}$, sec	Type signature (fig. 5)
6-9-66	SR-a	5	1.07 N	V-3	1	98.63	0.197	0.1060	3.29	0.0250	0.0125	CO
					2	76.61	.197	.1075	3.39	.0340	.0085	CO
					3	54.58	.197	.1160	3.14	.0430	.0045	CO
				V-5	1	76.13	0.201	-----	---	0.0510	-----	CO
					2	50.75	.201	-----	---	.0625	-----	CO
					3	63.68	.201	-----	---	.0325	-----	CO
					4	109.65	.201	-----	---	.0185	-----	CO
					5	-----	----	-----	---	-----	-----	--
				V-6	1	135.98	0.196	0.0875	3.05	0.0080	0.003	CO
					2	129.28	.196	.1000	3.11	.0140	.010	CO
					3	90.01	.196	.0960	3.18	.0210	.002	CO
				V-7	1	96.72	0.197	0.0960	3.71	0.0300	0.008	CO
					2	107.73	.197	.0800	3.72	.0330	.016	CO
					3	100.55	.197	.0850	3.42	.0220	.011	CO
		9	2.78 N	Tango	404	88.10	0.186	0.1110	4.98	0.0080	0.003	--
					406	95.76	.185	.1180	5.35	.0090	.0035	--
					410	127.36	.185	.1120	5.21	.0015	.001	NP
					411	119.22	.185	.1100	5.88	.0070	.002	NP
					412	115.39	.185	.1110	5.35	.0035	.002	NP
					408	54.58	----	-----	---	-----	-----	--
		5	1.07 N	FRC	1	71.34	----	-----	---	-----	-----	--
					2	76.61	----	-----	---	-----	-----	--
					3	89.54	----	-----	---	-----	-----	--
					4	75.65	----	-----	---	-----	-----	--
					5	98.15	----	-----	---	-----	-----	--
					6	70.38	----	-----	---	-----	-----	--
					7	67.03	----	-----	---	-----	-----	--
					8	62.24	----	-----	---	-----	-----	--
					9	63.20	----	-----	---	-----	-----	--
					10	75.65	----	-----	---	-----	-----	--
					11	80.92	----	-----	---	-----	-----	--
					12	78.52	----	-----	---	-----	-----	--
					13	65.60	----	-----	---	-----	-----	--
					14	50.27	----	-----	---	-----	-----	--
					15	43.09	----	-----	---	-----	-----	--
					16	46.44	----	-----	---	-----	-----	--
6-13-66	SR-b	9	2.31 N	V-1	1	57.94	0.200	0.1240	3.53	0.0175	0.004	NR
					2	57.94	.199	.1145	3.24	.0060	.0025	--
					3	45.97	.200	.1035	2.71	.0060	.003	--
				V-2	1	62.72	0.201	0.1175	3.38	0.0200	0.012	CO
					2	61.29	.201	.1290	3.75	.0195	.0105	CO
					3	74.21	.201	.1275	4.89	.0270	.0115	CO
				V-3	1	67.99	0.201	0.1180	3.67	0.0260	0.010	CO
					2	42.61	.201	.1130	2.56	.0365	.0115	NR
					3	56.98	.201	.1180	3.58	.0110	.0065	PR
					4	81.40	.201	.1250	3.89	.0040	.0035	NP
					5	56.50	.201	.1240	3.46	.0160	.004	NR
				V-5	1	79.48	0.199	0.1050	3.52	0.0110	0.008	NP
					2	67.03	.198	.0985	3.55	.0160	.0075	NR
					3	62.24	.198	.0990	3.27	.0225	.0035	NR
					4	----	----	-----	---	-----	-----	--
					5	39.74	.199	.1180	2.54	.0315	.009	NR
				V-6	1	50.27	0.201	0.1175	2.88	0.0220	0.0075	NR
					2	51.23	.201	.1155	2.69	.0225	.0035	NR
					3	83.79	.201	.1230	4.91	.0230	.008	NR
				V-7	1	50.75	≈0.214	0.1090	3.25	0.0200	0.0015	CO
					2	59.37	≈.214	.1045	2.73	.0260	.004	CO
					3	49.32	≈.214	.1130	2.15	.0290	.0045	CO
				V-8	1	37.82	0.199	0.1310	2.74	0.0270	0.003	R
					2	38.30	.200	.1300	3.05	.0290	.005	R
					3	47.88	.200	.1320	3.82	.0350	.0045	R
				Tango	404	55.06	0.200	0.1150	2.55	0.0105	0.005	--
					406	67.99	.204	.1090	2.62	.0130	.0045	--
					410	53.63	.200	.1270	2.64	.0255	.010	NR
					411	84.75	.201	.0980	2.46	.0110	.003	--
					412	61.76	.204	.1175	2.73	.0120	.005	NP
					408	37.35	----	-----	---	-----	-----	--
	SR-c	9	0	V-1	1	57.94	0.214	0.1190	2.84	0.0120	0.007	CO
					2	68.95	.216	.1080	3.27	.0270	.007	CO
					3	88.58	.212	.1015	3.17	.0150	.008	CO
				V-2	1	45.01	0.215	0.1360	3.59	0.0500	0.004	CO
					2	50.27	.215	.1360	3.69	.0620	.0055	CO
					3	53.63	.215	.1315	4.60	.0260	.004	CO

TABLE III.- SUMMARY OF SONIC-BOOM DATA FOR SR-71 MISSIONS FLOWN AT EDWARDS AIR FORCE BASE – Continued

Date	Mission number	Site	Site distance from flight track, km	Station number	Micro-phone	Δp_o, N/m^2	ΔT, sec	Δt_o, sec	I_o, $N\text{-}sec/m^2$	τ, sec	$\tau_{1/2}$, sec	Type signature (fig. 5)
6-13-66	SR-c	9	0	V-3	1	46.44	0.216	0.1275	3.79	0.0150	0.0045	CO
					2	80.44	.216	.1075	4.05	.0630	.006	CO
					3	86.66	.216	.0985	3.59	.0355	.012	CO
					4	96.24	.216	.1040	3.70	.0260	.0065	CO
					5	93.84	.216	.1150	3.86	.0280	.020	CO
				V-5	1	70.86	0.212	0.1240	3.18	0.0120	0.004	CO
					2	77.09	.212	.1270	3.27	.0190	.0125	CO
					3	43.57	.212	.1235	2.83	.0170	.005	CO
					4	----	----	-----	---	-----	------	--
					5	----	----	-----	---	-----	------	--
				V-6	1	56.02	≈0.214	0.1180	2.96	0.0660	0.0055	CO
					2	35.43	≈.214	.1320	2.64	.0380	.008	CO
					3	55.06	≈.214	.1380	4.03	.0400	.013	CO
				V-7	1	50.75	0.214	0.1300	3.08	0.0200	0.012	CO
					2	59.37	.214	.1230	2.95	.0260	.017	CO
					3	49.32	.214	.1110	2.22	.0290	.015	CO
				V-8	1	55.54	0.214	0.1175	2.49	0.0220	0.013	CO
					2	77.09	.214	.1120	2.74	.0170	.0135	CO
					3	48.84	.214	.1245	2.83	.0380	.015	CO
				Tango	404	34.95	0.216	0.1290	2.43	0.0215	0.014	CO
					406	31.60	.216	.1305	2.45	.0385	.015	CO
					410	43.57	.214	.1260	2.39	.0200	.008	CO
					411	33.99	.216	.1260	2.38	.0280	.020	CO
					412	33.99	.214	.1325	2.57	.0210	.014	CO
					408	----	----	-----	---	-----	------	--
6-22-66	SR-d	1	58.4 N	V-1	1	34.95	0.206	-----	---	0.0370	------	R
					2	38.30	.206	-----	---	.0200	------	R
					3	31.12	.206	-----	---	.0170	------	R
		9	7.41 N	V-3	1	37.82	0.227	-----	---	0.0230	------	R
					2	33.52	.226	-----	---	.0135	------	R
					3	31.60	.227	-----	---	.0140	------	R
					4	33.04	.227	-----	---	.0150	------	R
					5	33.04	.227	-----	---	.0165	------	R
				V-5	1	33.04	0.227	-----	---	0.0265	------	PR
					2	39.26	.226	-----	---	.0130	------	NR
					3	30.64	.227	-----	---	.0320	------	R
					4	----	----	-----	---	-----	------	--
					5	32.08	.227	-----	---	.0145	------	NR
				V-6	1	31.12	0.220	-----	---	0.0110	------	NR
					2	31.60	.220	-----	---	.0140	------	NR
					3	23.46	.221	-----	---	.0160	------	NR
				V-8	1	33.99	0.187	-----	---	0.0080	------	NR
					2	33.04	.188	-----	---	.0095	------	NR
					3	30.64	.188	-----	---	.0090	------	NR
				Tango	404	55.06	0.230	-----	---	0.0040	------	NP
					406	55.54	.231	-----	---	.0200	------	NR
					410	53.15	.231	-----	---	.0140	------	NR
					411	50.27	.232	-----	---	.0220	------	NR
					412	62.24	.231	-----	---	.0130	------	NR
					408	32.08	----	-----	---	-----	------	--
			6.43 N	FRC	1	28.72	----	-----	---	-----	------	--
					2	33.52	----	-----	---	-----	------	--
					3	33.99	----	-----	---	-----	------	--
					4	28.72	----	-----	---	-----	------	--
					5	34.95	----	-----	---	-----	------	--
					6	33.04	----	-----	---	-----	------	--
					7	32.56	----	-----	---	-----	------	--
					8	30.16	----	-----	---	-----	------	--
					9	31.12	----	-----	---	-----	------	--
					10	30.64	----	-----	---	-----	------	--
					11	34.95	----	-----	---	-----	------	--
					12	37.35	----	-----	---	-----	------	--
					13	31.60	----	-----	---	-----	------	--
					14	31.60	----	-----	---	-----	------	--
					15	29.21	----	-----	---	-----	------	--
					16	26.81	----	-----	---	-----	------	--
6-23-66	SR-F-1	2	37.8 N	V-2	1	19.63	----	-----	---	0.0530	------	CO
					2	18.19	----	-----	---	.0620	------	CO
					3	21.07	----	-----	---	.0620	------	CO
		3	21.7 N	V-3	1	31.12	0.190	-----	---	0.0200	------	NR
					2	39.26	.190	-----	---	.0155	------	NR
					3	31.60	.190	-----	---	.0100	------	NR
					4	----	----	-----	---	-----	------	--
					5	----	----	-----	---	-----	------	--
		9	1.19 S	V-5	1	50.27	0.199	0.1075	2.75	0.0135	0.0025	NR
					2	45.01	.198	.1140	2.84	.0120	.003	NR
					3	48.84	.198	.1055	2.58	.0080	.00225	NR
					4	----	----	-----	---	-----	------	--
					5	47.88	.198	.1070	2.83	.0110	.001	NR

TABLE III.- SUMMARY OF SONIC-BOOM DATA FOR SR-71 MISSIONS FLOWN AT EDWARDS AIR FORCE BASE – Concluded

Date	Mission number	Site	Site distance from flight track, km	Station number	Micro-phone	Δp_o, N/m^2	ΔT, sec	Δt_o, sec	I_o, $N\text{-}sec/m^2$	τ, sec	$\tau_{1/2}$, sec	Type signature (fig. 5)
6-23-66	SR-F-1	6	12.6 S	V-6	1	41.18	0.203	-----	---	0.0140	-----	NR
					2	32.08	.202	-----	---	.0155	-----	NR
					3	38.30	.202	-----	---	.0170	-----	NR
		7	30.4 S	V-7	1	22.50	0.194	-----	---	0.0340	-----	CO
					2	21.07	.196	-----	---	.0320	-----	CO
					3	19.63	.193	-----	---	.0340	-----	CO
		8	44.5 S	V-8	1	45.97	----	-----	---	0.0250	-----	CO
					2	38.30	----	-----	---	.0290	-----	CO
					3	32.08	----	-----	---	.0420	-----	CO
		9	1.19 S	Tango	404	50.75	0.200	0.1060	2.85	0.0080	0.003	NR
					406	46.44	.200	.1100	2.87	.0095	.004	NR
					410	57.94	.200	.1100	3.00	.0150	.002	--
					411	44.53	.200	.1100	2.73	.0080	.003	NR
					412	53.15	.200	.1110	3.19	.0125	.004	NR
					408	26.33	----	-----	---	-----	-----	--
				FRC	1	45.49	----	-----	---	-----	-----	--
					2	44.53	----	-----	---	-----	-----	--
					3	43.09	----	-----	---	-----	-----	--
					4	47.88	----	-----	---	-----	-----	--
					5	49.32	----	-----	---	-----	-----	--
					6	56.50	----	-----	---	-----	-----	--
					7	44.53	----	-----	---	-----	-----	--
					8	43.09	----	-----	---	-----	-----	--
					9	49.32	----	-----	---	-----	-----	--
					10	49.32	----	-----	---	-----	-----	--
					11	46.92	----	-----	---	-----	-----	--
					12	50.27	----	-----	---	-----	-----	--
					13	26.81	----	-----	---	-----	-----	--
					14	22.50	----	-----	---	-----	-----	--
					15	22.02	----	-----	---	-----	-----	--
					16	25.86	----	-----	---	-----	-----	--
	SR-F-2	2	39.2 N	V-2	1	12.45	----	-----	---	0.0480	-----	CO
					2	10.05	----	-----	---	.0250	-----	CO
					3	10.05	----	-----	---	.0310	-----	CO
		3	23.1 N	V-3	1	25.38	0.150	-----	---	0.0150	-----	--
					2	26.33	.171	-----	---	.0100	-----	CO
					3	26.33	.177	-----	---	.0160	-----	CO
					4	----	----	-----	---	-----	-----	--
					5	----	----	-----	---	-----	-----	--
		9	24 N	V-5	1	39.26	0.192	0.1105	2.53	0.0230	0.003	R
					2	43.09	.192	.1070	2.57	.0150	.004	R
					3	45.97	.192	.1075	2.68	.0175	.003	R
					4	----	----	-----	---	-----	-----	--
					5	43.09	.193	.1145	2.60	.0090	.0035	R
		6	11.2 S	V-6	1	30.16	0.181	-----	---	0.0065	-----	NP
					2	30.16	.182	-----	---	.0150	-----	NR
					3	34.95	.182	-----	---	.0180	-----	NR
		7	30.4 S	V-7	1	21.55	0.174	-----	---	0.0225	-----	R
					2	18.67	.173	-----	---	.0220	-----	R
					3	24.42	.173	-----	---	.0230	-----	R
		8	44.5 S	V-8	1	11.97	0.145	-----	---	0.0250	-----	R
					2	10.53	.145	-----	---	.0285	-----	R
					3	10.05	.145	-----	---	.0360	-----	R
		9	0.24 N	Tango	404	40.70	0.197	0.1100	2.33	0.0145	0.003	NR
					406	41.18	.198	.1110	2.37	.0230	.0035	NR
					410	40.22	.197	.1200	2.37	.0240	.0035	NR
					411	37.82	.197	.1050	2.09	.0150	.002	NR
					412	35.43	.197	.1105	2.39	.0200	.003	NR
					408	20.59	----	-----	---	-----	-----	--
				FRC	1	38.30	----	-----	---	-----	-----	--
					2	43.57	----	-----	---	-----	-----	--
					3	40.70	----	-----	---	-----	-----	--
					4	39.74	----	-----	---	-----	-----	--
					5	37.35	----	-----	---	-----	-----	--
					6	53.15	----	-----	---	-----	-----	--
					7	53.62	----	-----	---	-----	-----	--
					8	49.80	----	-----	---	-----	-----	--
					9	44.05	----	-----	---	-----	-----	--
					10	40.70	----	-----	---	-----	-----	--
					11	41.66	----	-----	---	-----	-----	--
					12	52.67	----	-----	---	-----	-----	--
					13	31.12	----	-----	---	-----	-----	--
					14	27.29	----	-----	---	-----	-----	--
					15	34.47	----	-----	---	-----	-----	--
					16	30.64	----	-----	---	-----	-----	--

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