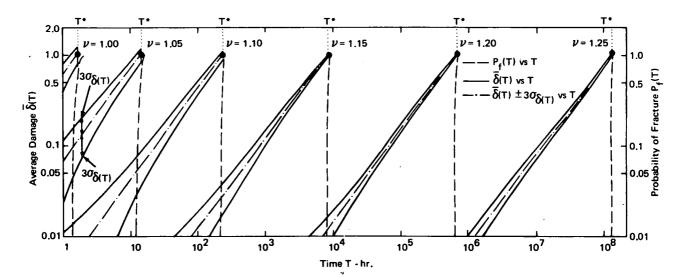
NASA TECH BRIEF

NASA Pasadena Office



NASA Tech Briefs announce new technology derived from the U.S. space program. They are issued to encourage commercial application. Tech Briefs are available on a subscription basis from the National Technical Information Service, Springfield, Virginia 22151. Requests for individual copies or questions relating to the Tech Brief program may be directed to the Technology Utilization Office, NASA, Code KT, Washington, D.C. 20546.

Probability of Stress-Corrosion Fracture Under Random Loading



Probability of Structural Fracture as a Function of Time and Average Damage as a Function of Time

Pressure vessels (such as rocket-propellant storage tanks, fuel and water tanks, undersea pressure vessels, and submerged structures) occasionally fail at relatively-low stress levels, after being subjected to sustained loading much below the critical level. Such failures often result from stress-corrosion crack propagation.

A mathematical method has been developed for evaluating the probability of stress-corrosion fracture under random loadings. The formulation is based on a cumulative-damage hypothesis and experimentally-determined stress-corrosion characteristics. Under both stationary and nonstationary random loadings, the mean value and the variance of the cumulative damage are obtained. The probability of stress-corrosion fracture is then evaluated, using the principle of maximum entropy. It is found that, under stationary random loadings, the standard deviation of the cumulative damage increases in proportion to the square root of time, while the coefficient of variation (dispersion)

decreases in inverse proportion to the square root of time.

The solutions are based on a linear structure, which is related to the excitation g(t) as follows:

$$\dot{Y}(t)+2\zeta\omega_0Y(t)+\omega_0^2Y(t)=g(t)$$

where ζ and ω_0 are, respectively, the damping coefficient and the natural frequency of the structure and Y(t) is the displacement response, assuming that the cumulative damage is essentially due to stress corrosion.

The probability of fracture then can be computed as a function of time, T, as shown in the figure. It is observed that T^* , the average time to failure, increases rapidly with respect to the increasing safety factor, ν . Additional information presented in the figure is the average damage, $\bar{\delta}(T)$, as a function of time, and $\bar{\delta}(T) \pm 3\sigma_{\bar{\delta}(T)}$, as a function of time, where $\sigma_{\bar{\delta}(T)}$ is the standard deviation.

(continued overleaf)

Note:

Requests for further information may be directed to:

Technology Utilization Officer

NASA Pasadena Office 4800 Oak Grove Drive

Pasadena, California 91103

Reference: TSP73-10453

Patent status:

NASA has decided not to apply for a patent.

Source: Jann-Nan Yang of

Caltech/JPL

under contract to NASA Pasadena Office

(NPO-13113)