

CR-128736

USER'S MANUAL

**SPACE SHUTTLE ENVIRONMENTAL
AND
THERMAL CONTROL
LIFE SUPPORT SYSTEM
COMPUTER PROGRAM**

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION
MANNED SPACECRAFT CENTER
HOUSTON, TEXAS

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ENVIRONMENTAL AND THERMAL CONTROL LIFE
SUPPORT SYSTEM COMPUTER PROGRAM (Hamilton
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**SECTION 1.0
INTRODUCTION**

1.0 INTRODUCTION

1.1 Objective

The evaluation and ultimate definition of an integrated Shuttle ETC/LSS is an evolutionary process which reflects frequent changes in both technical and program related requirements. To support the NASA, Shuttle vehicle primes and in-house IRD, Hamilton Standard has developed an ETC/LSS computer program which provides accurate and rapid responses to these changing requirements. This design optimization tool has proven invaluable, saving countless hours of hand calculations and allowing the conceptual and preliminary design study phases to proceed in a comprehensive fashion. Two key features, which have made this computer model unique and of significant benefit to both Hamilton Standard and the people it supports, are:

- a. Simplicity - ease of use/flexibility relative to schematics and requirement changes; and
- b. Subroutines - unique models representing the "true" analytical descriptions of the mechanical and chemical processes under evaluation.

Under NASA sponsorship (NAS 9-12411), this program has been expanded and upgraded to meet the design evaluation demands of the forthcoming Shuttle phases. These demands include continuation of trade-off studies to further validate selections, expansion of these studies to include new requirements, and initial performance evaluations (steady state off-design transients) required to support development.

1.1 (Continued)

The objective of this document is to define this expanded computer program and provide the user with sufficient information for running and modifying the program as desired for the NASA-MSD computer facilities.

1.2 Outline

An outline of this document is presented in Table 1-1.

TABLE 1-1

USER'S MANUAL - OUTLINE

- 1.0 INTRODUCTION
 - 1.1 Objective
 - 1.2 Outline
 - 2.0 BASIC OPTIMIZATION PROGRAM
 - 3.0 PROGRAM CHANGES
 - 3.1 Sizing Program Changes
 - 3.2 Off Design Performance
 - 3.3 Radiator/Evaporator Expendable Usage
 - 3.4 Component Weights
 - 4.0 OPERATING PROCEDURES
 - 4.1 How to Set Up Deck
 - 4.2 Program Input and Output
 - 4.3 How to Vary Program
- APPENDIX I
- Logic Flow Diagrams of
- 1. Main Program
 - 2. Condensing Heat Exchanger Subroutine
 - 3. Sensible Heat Exchanger Subroutine
 - 4. LiOH Subroutine

TABLE 1-1 (CONTINUED)

APPENDIX I (continued)

5. Contaminant Control Subroutine
6. Fan Weight Subroutine
7. Valve Weight Subroutine
8. Q_{met} Subroutine
9. Sensible Heat Exchanger Off Design Subroutine
10. Flash Evaporator Subroutine

APPENDIX II

Subroutine Descriptions

APPENDIX III

Logic Flow Diagrams

SECTION 2.0
BASIC OPTIMIZATION PROGRAM

2.0

BASIC OPTIMIZATION PROGRAM

A simplified logic diagram of the program is shown in Figure 2-1. The computer program consists of a "main line" program which does bookkeeping and a number of subroutines which calculate subsystem or component weights for the required performance. The "main line" program is "keyed" to select the desired subroutines (either condenser or solid amine for example) for the system under consideration. If other schematic arrangements are desired, it is a simple matter to change the "main line" program to select the subroutines in a different order or add other components.

There are three convergence loops in the program:

- a. Condenser air outlet temperature/heat exchanger size
- b. Interface heat exchanger outlet temperature
- c. Radiator outlet temperature

When using a condenser, the air outlet temperature is initially set 2°F above the condenser coolant inlet temperature and the heat exchanger, fan, valve, and power equivalent weight calculated. The air outlet temperature is then increased in 1°F increments until the total equivalent weight is found to increase over the previous iteration. The previous iteration is then used as the condenser weight and performance.

The interface heat exchanger water loop outlet temperature for the first iteration is set by input data. For this value, the condenser and sensible heat exchanger are

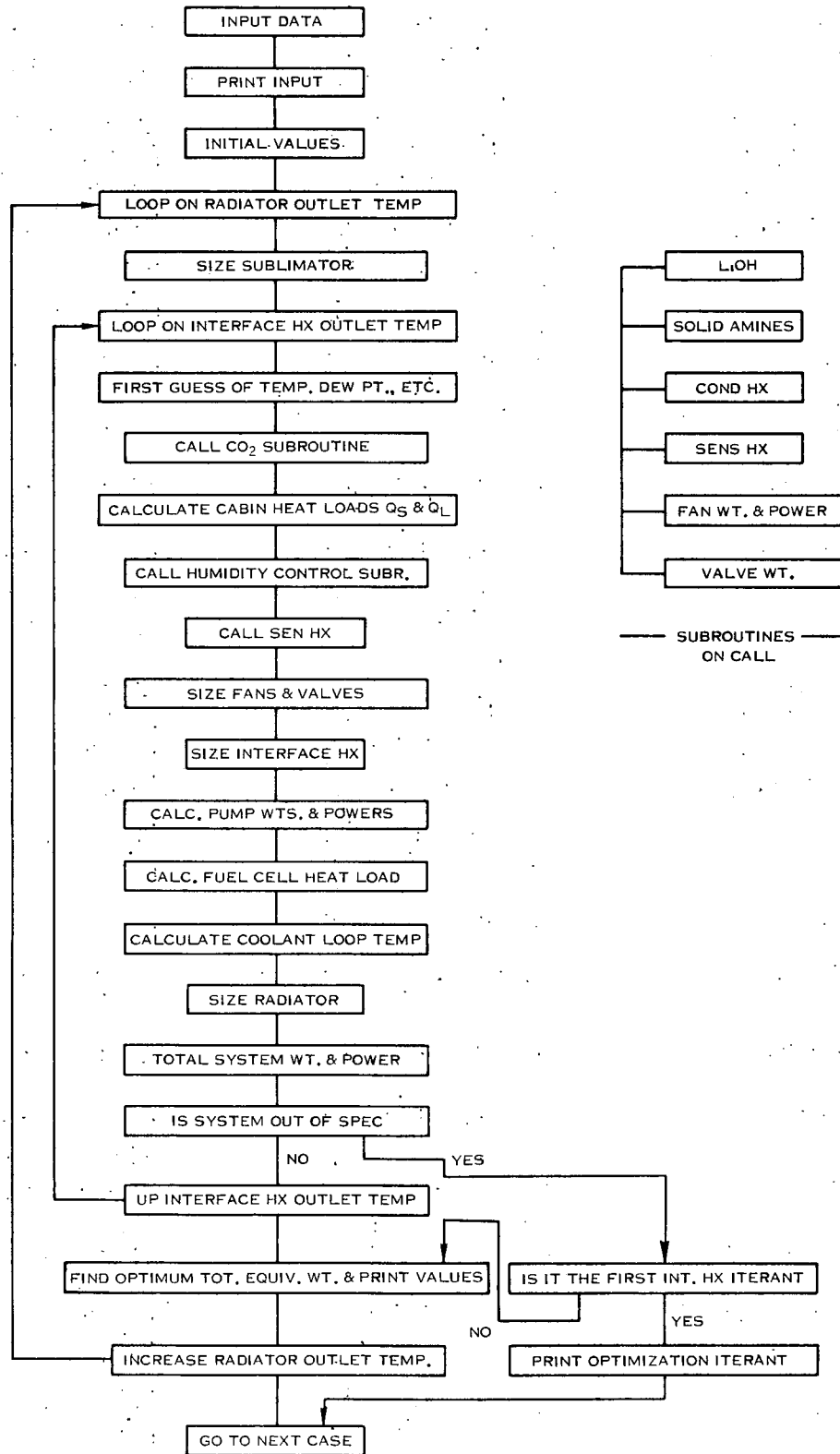


FIGURE 2-1. OPTIMIZATION COMPUTER PROGRAM LOGIC

2.0

(Continued)

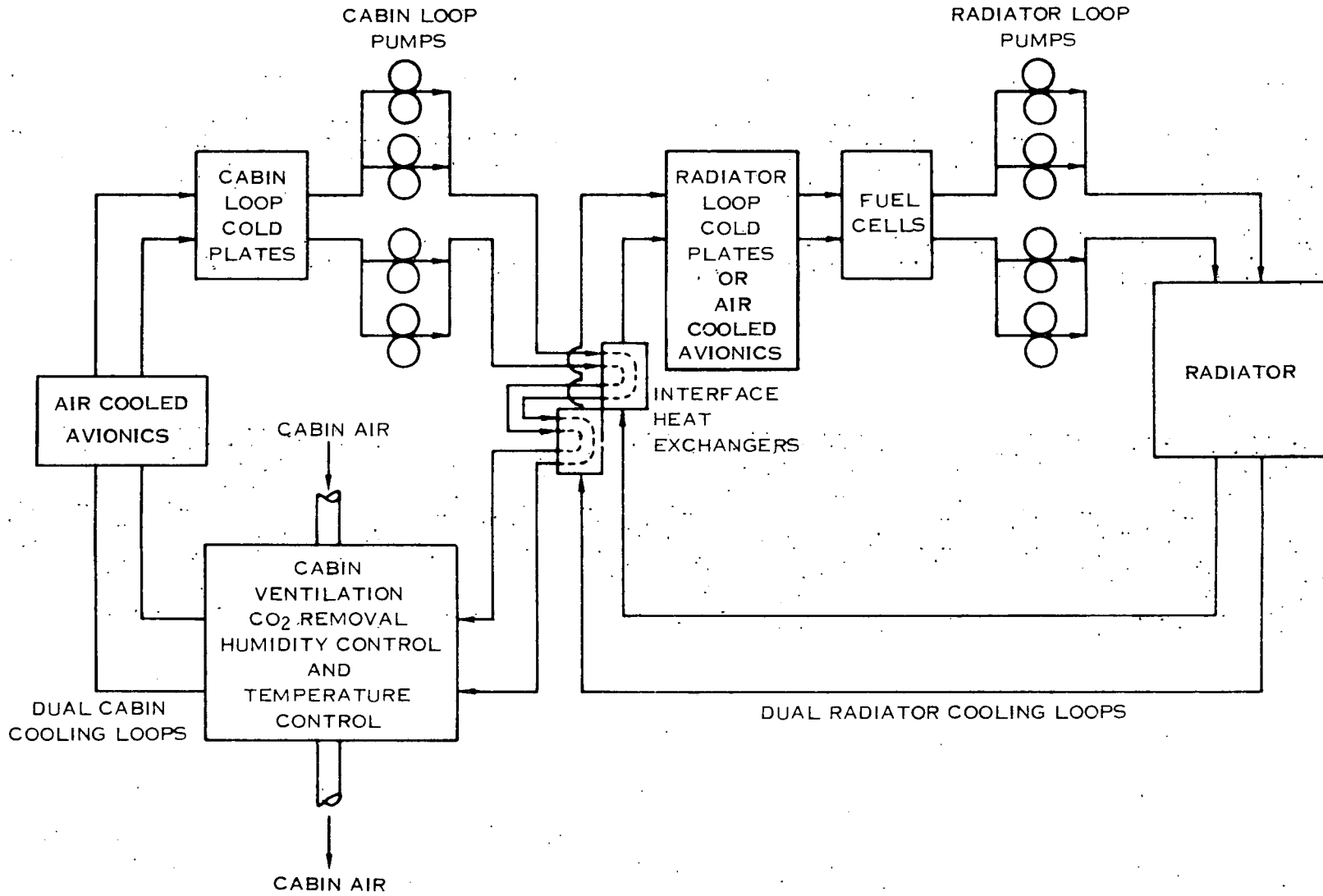
optimized and the weight of pumps, fans, radiator, and other components are calculated and summed. The interface outlet temperature is then raised in 1°F increments until either the condenser or sensible heat exchanger can no longer provide the required cooling. The minimum total equivalent weights for various interface heat exchanger outlet temperatures are then compared and the minimum value stored.

The radiator outlet temperature is then raised by an input delta and the process repeated. When the cabin heat exchanger(s) cannot provide the required cooling (even at the lowest cabin loop temperatures), the minimum total equivalent weights for each radiator outlet temperature are compared and the minimum value selected. The case with lowest total equivalent weight is then recalculated and the weights, powers, flow rates and temperatures for the optimum case printed.

A simplified schematic of the ETC/LSS used by the computer program is shown in Figure 2-2. In the box labeled "Cabin Ventilation, CO₂ Removal, Humidity Control and Temperature Control" several different combinations of CO₂ removal and humidity control concepts can be used. A typical schematic of the LiOH/Condenser Approach is shown in Figure 2-3.

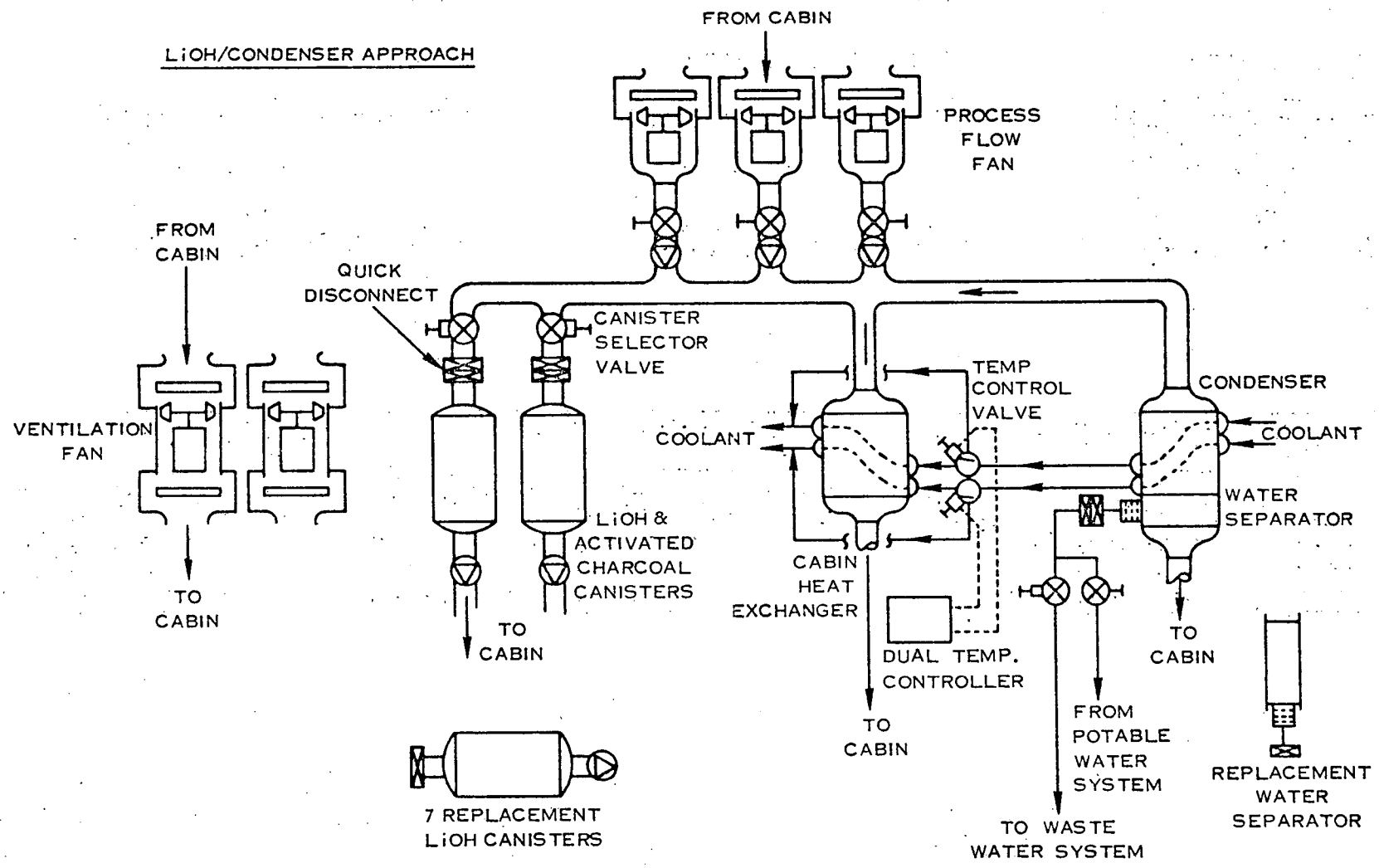
Items that can be varied when comparing optimized systems are:

- a. Cabin conditions (temperature, pressure, maximum relative humidity, etc.)



2-4

FIGURE 2-2. SYSTEM SCHEMATIC — SAMPLE CASE



2-5

FIGURE 2-3. SAMPLE CASE - VENTILATION, CO₂, HUMIDITY &

2.0 (Continued)

- b. Heat loads (metabolic sensible, metabolic latent, fuel cell, etc.)
- c. Radiator loop flow rate and properties
- d. Mission parameter (length, power penalty, etc.)
- e. Which subsystems to use (LiOH or solid amine for CO₂; condenser or solid amine for humidity control, etc.)
- f. Component data (pressure drops, fixed weights, structural weight factors, component weight factors, tables of optimization data, radiator influx, etc.)

**SECTION 3.0
PROGRAM CHANGES**

3.0

PROGRAM CHANGES

Program changes fall into four categories:

- a. Changes to the sizing program (Basic Optimization Program)
- b. Addition of "off design" performance calculations
- c. Addition of loop to calculate the amount of water or cryogenic hydrogen required to supplement the radiator around an orbit
- d. Addition of selected component weight calculations

3.1 Sizing Program Changes

Changes to the sizing program consist of additions, deletions, and a more detailed print out. The items deleted were the Desiccant, Hydrogen Depolarized Cell, and the Molecular Sieve Subroutines. As previous studies have shown these subsystems to be non-competitive, it was decided not to expand them to include "off design" performance calculations and, additionally, to delete them from the sizing program.

The additions made to the sizing program are:

- a. A loop to calculate the optimum coolant flow rate
- b. Additional components
 1. Flash Evaporator
 2. Fuel Cell Heat Exchanger
 3. GSE Heat Exchanger
 4. Separate Avionics Bay (with the capability to consider two bays in series using common hardware)
 5. Cryogenic Heat Exchanger
- c. Ability to change component parameters by input data
 1. Input fan and pump overall efficiency
 2. Input the number of fans, check valves, and pumps
- d. The radiator subroutine was changed to account for different delta temperatures between the fluid and wall at the inlet and outlet

In order to facilitate the running of the program, a convergence subroutine was added to optimize the coolant flow rate. If a flow rate is given in the input, the program will

3.1 (Continued)

use the input value as the first guess of flow rate. If the input value is zero or negative, the program will calculate a minimum coolant flow rate to be used for the first iteration. If the program does not converge with the original flow rate, the total equivalent weight is set to a large value and the flow rate is increased by an inputted factor. At the end of each radiator outlet temperature loop, the optimum total equivalent weight for that flow rate is compared to the optimum equivalent weight for the previous flow rate. If the weight is lower, the flow rate is again increased. If the weight is higher, the program goes back to recalculate the optimum condition ($W_{coolant}$, $T_{radiator\ out}$, $T_{interface\ hx\ out}$, W_{air} , etc.) and prints the optimum condition. It is also possible to run only one condition by setting an input key. The program will then use the input TRO and Wc and only optimize the heat exchangers.

The program has been changed to allow the radiator to be supplemented with:

- a. Sublimator
- b. Flash Evaporator
- c. Cryogenic Hydrogen Heat Exchanger

If the maximum radiator area is too small to handle the required heat load, the excess heat load is rejected by the supplementary heat sink using an input expendable penalty. In addition, the supplementary heat sink will be used for a period of time (input) to handle the entire heat load. This simulates the time when the radiator is not

3.1 (Continued)

exposed to space. Three supplementary heat sinks are capable of being provided-- cryogenic heat exchanger, sublimator or flash evaporator. If the cryogenic heat exchanger is desired, no additional input data is necessary except the expendable penalty. The cryogenic heat exchanger subroutine automatically calculates the heat exchanger weight and adds this value to the system total equivalent weight. If the cryogenic heat exchanger is not desired, then the component weight factors must be set to zero by input. The use of either a sublimator or flash evaporator must be selected and the necessary weight penalty factors included in the input data.

The fuel cell heat exchangers are sized to meet the input temperature requirements. The mass flow rate ($W \times C_p$) of the fuel cell loop required, based on the fuel cell heat load and temperatures, is calculated and stored in the input data block. For off-design performance, the fuel cell loop temperatures are calculated based on Freon loop temperatures, heat exchanger size, and fuel cell loop flow rate. The heat exchanger is sized as a single unit capable of rejecting the entire heat load. If some type of parallel arrangement is used, the weight penalty would be equivalent to the single unit weight.

The GSE heat exchanger is sized to reject the maximum vehicle heat load. The GSE fluid inlet temperature is considered to be 0°F and the mass flow ratio is set at 2.

With the addition of air cooled avionics on the Shuttle, a special subroutine was developed that sizes a heat exchanger with the desired number of fans to remove the

3.1 (Continued)

heat from a separate compartment. The heat exchanger air flow rate is optimized to obtain the minimum total equivalent weight of the heat exchanger and fans. An initial air outlet temperature is assumed to be 2°F higher than the coolant inlet temperature. The required air flow, fan power, and component weights are calculated. The air outlet temperature is then increased 2°F and a new total equivalent weight is calculated. This process continues until the total equivalent weight is higher than the previous iteration. The values for the previous (lightest) iteration are used for system weight.

EBAY2 is a subroutine that sizes two avionics compartments in series. The compartments have the same ECLSS equipment. The subroutine calculates the equipment size (heat exchanger and fans) required to meet performance in the second (downstream) compartment. The air temperature of first (upstream) compartment is then calculated using the equipment sized for the downstream compartment. If the desired compartment temperatures are not met, the equipment is resized to meet the temperature requirements of the first compartment. The temperature of the downstream compartment is recalculated with the larger sized equipment. The optimization of the heat exchanger/fan air flow rate is similar to that explained in the paragraph above.

The basic program has the ability to change heat exchanger characteristics by changing the weight factors. It is also possible to now change other components such as the number of fans, number of pumps, number of HS-C canisters, etc., by changes to the input data. This is useful as several of prime contractors are using different numbers of components.

3.1 (Continued)

As heat loads change, flow rates and pressure losses also change. In order to better match the expected fan and pump efficiencies, these variables were made inputs to the computer program.

Recent radiator studies have shown that the difference in temperature between the fluid and the wall will vary considerably between the inlet and outlet of the radiator. The radiator subroutine was rewritten to account for this difference. At present, there is a predicted 15°F difference between the fluid and wall at the radiator inlet and a 5°F difference at the outlet.

3.2

Off-Design Performance

The inputs required for the "off-design" performance section of the computer program are:

- a. Air volumetric flow rates
- b. Heat exchanger sizes
- c. Pump and fan powers
- d. Coolant flow rates
- e. Heat loads
- f. Desired control temperatures

All of these parameters are calculated by the sizing program and stored in the input data block. If an "off-design" performance case is run after a "sizing" case, the only inputs required are the changes to heat loads, cabin temperature or cabin pressure desired. If an "off-design" case is to be run without a "sizing" case preceding it, the above parameters must be inputted.

The program first calculates the total vehicle heat loads and then the radiator inlet temperature. The program then goes to the desired heat rejection method:

- a. Radiator/expendable (if required)
- b. Expendable heat sink only
 1. Sublimator
 2. Flash evaporator
 3. Cryogenic heat exchanger

3.2 (Continued)

If a sublimator is used, the heat sink inlet and outlet temperatures must be iterated as the temperatures are a function of the sublimator size and vehicle heat load.

In calculating the total vehicle heat load, the sensible and latent heat of the LiOH must be included. The LiOH subroutine has been expanded to also calculate the CO₂ partial pressure resulting from both a new cartridge and the level at which the cartridge would normally be changed.

Once the interface heat exchanger heat load and radiator loop inlet temperature is known, the cabin loop outlet temperature is calculated by a subroutine called HX. This subroutine calculates the hot side outlet temperature based on the heat load, heat exchanger size, coolant flow rates, and cold side inlet temperature. This subroutine is used for all of the sensible heat exchangers.

The program then enters a loop on cabin temperature. This loop is needed only if there is a sensible heat exchanger. After entering the loop the program selects the water removal subroutine--either HS-C or a condenser. The HS-C subroutine calculates the cabin water vapor partial pressure or determines the air flow required for humidity control. Based on the flow through the beds, the CO₂ partial pressure is also calculated. The program then goes to the sensible heat exchanger.

If a condenser is used, a key is set to tell the condenser subroutine if there is a sensible heat exchanger also. If there is no sensible heat exchanger, the condenser

3.2 (Continued)

subroutine CX2 calculates the air flow required through the heat exchanger to meet the required cabin temperature and the cabin dew point. If the cabin temperature cannot be met, the cabin temperature is raised in 1°F increments, until the heat exchanger can remove the heat load. As the cabin temperature is raised, a subroutine QMET calculates a new latent/sensible metabolic heat load split for the new cabin temperature.

If there is also a sensible heat exchanger, the condenser subroutine calculates the sensible load removed by the condenser and the cabin dew point.

If there is a sensible heat exchanger, the Hx subroutine calculates the air flow through the heat exchanger required to reject the remaining sensible heat load. If the heat load is negative, a message is printed that a reheater is required and the program continues. If the heat exchanger cannot remove the required heat load, the cabin temperature is increased 1°F, the metabolic latent/sensible load split recalculated, and the program returns to the water removal subroutine. If the temperature is raised 15°F and the heat exchanger still cannot meet the load, a message is printed and the case continues.

If there is a water cooled avionics bay, the compartment temperature is calculated in a manner similar to that used for the interface heat exchanger.

Temperatures into and out of the other components (pump, fuel cell heat exchanger, etc.) are calculated in a similar manner and the results printed.

3.3 Radiator/Evaporator Expendable Usage

A section has been added to the program to determine the maximum nominal and minimum evaporating rates of expendables required to supplement the radiator over an entire orbit. The program calculates steady state performance at discrete orbital positions.

The inputs required are the vehicle heat loads, coolant flow rate, radiator characteristics (α , ϵ , Area, etc.), evaporator characteristics, and the radiator influx versus orbital position. It is assumed that the influx is modified to account for radiator mass.

The program sums the vehicle heat loads, finds the radiator influx for the orbital position, and calculates radiator outlet temperature. If the temperature is higher than the required temperature, a secondary sink is used:

- a. Sublimator
- b. Flash Evaporator
- c. Cryogenic Heat Exchanger

If a sublimator is used, a convergence loop is used to find the proper load split between the radiator and sublimator.

The program prints the average rate of expendable usage as well as the radiator inlet and outlet temperatures and the rate of expendable usage for each orbital position.

Up to 30 steps may be used for each orbit.

3.4 Component Weights

The weights printed for each subsystem are a buildup of the individual component weights within the subsystem. Generalized routines are used to calculate fan weights, as a function of flow and pressure rise; valve weights, as a function of type and flow; heat exchanger weights, as a function of UA, etc. In addition, fixed weights for items such as controllers, disconnects, accumulators, etc., are added. Finally, a structural weight factor is included to account for packaging consideration. Since heat exchangers usually include mounting provisions as an integral part of their design, structural weight factors are not applied to heat exchangers as the basic weight models include these mounting provisions. Table 3-1 shows the general weight equations used for the subsystem weights. Table 3-2 shows a breakdown of the subsystems, what components are included within each subsystem, and the source of weight values - F, for fixed weight that does not change with various conditions and P, for weight values calculated by the program as a part of the optimization process. All symbols are described in Appendix I.

TABLE 3-1
WEIGHT EQUATIONS

<u>Subroutine</u>	<u>Weight Equations</u>
FEVAP	WT = (FWT(L)*CFT(L)+FXW(L))*SWT(L)
	WH2O = QR/965
LIOH	WT = (WL*FWT(J)+FXW(J)+2.*WTM)*SWT(J)
	WL = WCO2*DAY*1.145
RAD	WT = AR*SWT(J) + FXW (J)
CHX	WT = FWT(J)*UA+(FXW(J)+WTV)*SWT(J)
EBAY	WTHX= FWT(J)*UA+FXW(J)*SWT(J)
	WTFAN = (FWT(J+1)*(WTF+WTK)+FXW(J+1))*SWT(J+1)
HSC	WTS = (FWT(J)*(WBS+WTX+WTV)+FXW(J)+WVC)*SWT(J)
	WTF = (WTF+3.*WTK)*SWT(12)
	WTV = VACUUM VALVE WT.
	WTC = CONTROL VALVE WT.
	WTX = CANISTER WT.
	WUS = 83.4*RHO*DAY*WBS/CYCL
CONT	WT = [WTB*FWT(J)+WTV+FXW(J)]*SWT(J)
EBAY2	WTHX = [FWT(J)*UA+FWX(J)*SWT(J)]*2.
	WTFAN = [(FWT(J+1)*(WTF+WTK)+FXW(J+1))*SWT(J+1)]*2.
SHX	WT = FWT(J)*UA+FXW(J)+WTV*SWT(J)
PUMP WT	WT = [(WC/RHO*.0748*DP) ^{0.4} *FWT(J)+FXW(J)]*SWT(J)
INTER. HX WT	WT = CFT(J)*FWT(J)+FXW(J)

TABLE 3-1 (CONT)
WEIGHT EQUATIONS

<u>Subroutine</u>	<u>Weight Equations</u>
SUBL. WT	WT = FWT(J)*UA+FXW(J)*SWT(J) WSUB = Q/1065.*TSUB
CRYO. HX	WT = FWT(J)*CFT(J)+FXW(J)*SWT(J) WHYD = Q/1440*TCRY
F/C HX&GSEHX	WT = UA*FWT(J)+FXW(J)*SWT(J)
EXPEND WT	WT = Q*FEXP
COND FAN	WT = (FWT(J)*(WCF+WCV)+.9*WCF+FXW(J))*SWT(J)
SENS FAN	WT = (FWT(J)*(WSF+WSV)+.9*WSF+FXW(J))*SWT(J)
VENT FAN	WT = FWT(J)*WTF

All Symbols Explained in Appendix 1.

TABLE 3-2
COMPONENT AND SUBSYSTEM LISTING

<u>Subsystem Component</u>	<u>No. Required</u>	<u>Weight Source</u>
<u>Water Removal/Condenser</u>		
HX	1	P
Temperature Control Valve (If no sens. HX)	1	P
Temperature Controller (Dual)	1	F
W/S Gutter/Duct	1	F
<u>Sensible HX</u>		
HX	1	P
Temperature Control Valve (Air)	1	P
Temperature Controller (Dual)	1	F
<u>Water Separator</u>		
W/S	1	F
Air Check Valves	2	F
H ₂ O Check Valves	2	F
<u>Water Loop Pump Package</u>		
Water Pump	3	P
Check Valves	3	F
Accumulator	3	F
Filters	2	F
Valve, Shutoff, Manual	2	F
Potable H ₂ O	1	F
Chiller	1	F

C

TABLE 3-2 (CONT)
COMPONENT AND SUBSYSTEM LISTING

<u>Subsystem Component</u>	<u>No. Required</u>	<u>Weight Source</u>
Disconnects, Liquid	5	F
Disconnects, Gas	3	F
Low Pressure Sensor	2	F
Pump Switchover	1	F
<u>Interface HX</u>		
HX's	2	P
<u>Pumps Freon Loop</u>		
Water Pump	3	P
Check Valves	3	F
Accumulator	3	F
Filter	2	F
Valve, Shutoff Solenoid	2	F
Disconnects, Liquid	5	F
Disconnects, Gas	3	F
Low Pressure Sensor	2	F
Pump Switchover	1	F
<u>Water Evaporator - Sublimator</u>		
HX	2	P
Shutoff Valves, Solenoid	4	F

TABLE 3-2 (CONT)
COMPONENT AND SUBSYSTEM LISTING

<u>Subsystem/Component</u>	<u>No. Required</u>	<u>Weight Source</u>
Shutoff Valves, Manual	5	F
Pressure Regulators	3	F
<u>CO₂ Control - LiOH</u>		
Cartridges	P	P
Valves, Shutoff, Manual	2	P
<u>Ventilation Fans</u>		
Fans	2	P
Silencer/Screen	1	P
<u>Condenser Fans</u>		
Fan	3	P
Check Valve	3	P
Silencer/Screen (.9 Fan)	1	P
<u>Sensible Fans</u>		
Fan	3	P
Check Valve	3	P
Silencer/Screen (.9 Fan)	1	P
<u>Contaminate Control</u>		
Cartridge	1	P
Check Valve	1	P

TABLE 3-2 (CONT)
COMPONENT AND SUBSYSTEM LISTING

<u>Subsystem Component</u>	<u>No. Required</u>	<u>Weight Source</u>
<u>Avionics Bay - Water Cooled</u>		
HX	1	P
Fan	3	P
Check Valve	3	P
Fan Speed Sensor		
<u>Avionics Bay - Freon Cooled</u>		
HX	1	P
Fan	3	P
Valve Check	3	P
Fan Speed Sensor	3	F
<u>Fuel Cell HX</u>		
HX	3	P
<u>Cryo Hx</u>		
HX	2	P
Valve, Shutoff Solenoid	6	F
Valve, Control	3	F
Temperature Controller	2	F
<u>Water Evaporator - Flash</u>		
HX	2	P
Solenoid Shutoff Valves	4	F

TABLE 3-2 (CONT)
COMPONENT AND SUBSYSTEM LISTING

<u>Subsystem/Component</u>	<u>No. Required</u>	<u>Weight Source</u>
Manual Valves	4	F
Temperature Controllers	2	F
<u>Other</u>		
Chiller (with water pumps)	1	F
Cooler (with water pumps)	1	F
<u>GSE Cooling</u>		
HX	1	P
Disconnects	2	F
Cold Plates		
<u>HS-C Subsystem</u>		
Beds & Canisters	4	P
Valves, Cycling	4	P
Valves, Vacuum	4	F
Timer (triple)	1	F
Humidity Control Valve	1	P
Humidity Controller (Dual)	2	F
Humidity Sensor	3	F
Gas Actuator Valves	8	F
<u>Radiator</u>		
Panels	1	P
Hinge, Valves, Controls, Orifices, Etc.	1	F

3.4 (Continued)

In order to run the HS-C or the orbital transient programs, tables of input data must be stored in the computer. Tables are set up in accordance with the following format.

X ~ Name of data block where table is stored

I ~ Location of first item in table within X

X(1) ~ Table or curve number

X(I+1) ~ Degree Interpolation choice (1, 2 or 3)

X(I+2) = NX Number of X values

X(I+3) = NY Number of Y values

X(I+4) "X" Values in ascending order

X(I+4+NX) "Y" Values in ascending order

X(I+4+NX+NY) "Z" Values in the following order

Z(1, 1), Z(1, 2), Z(1, 3), ----- Z(1, NY)

Z(2, 1), Z(2, 2), Z(2, 3), ----- Z(2, NY)

Z(NX, 1), Z(NX, 2), Z(NX, 3)----- Z(NX, NY)

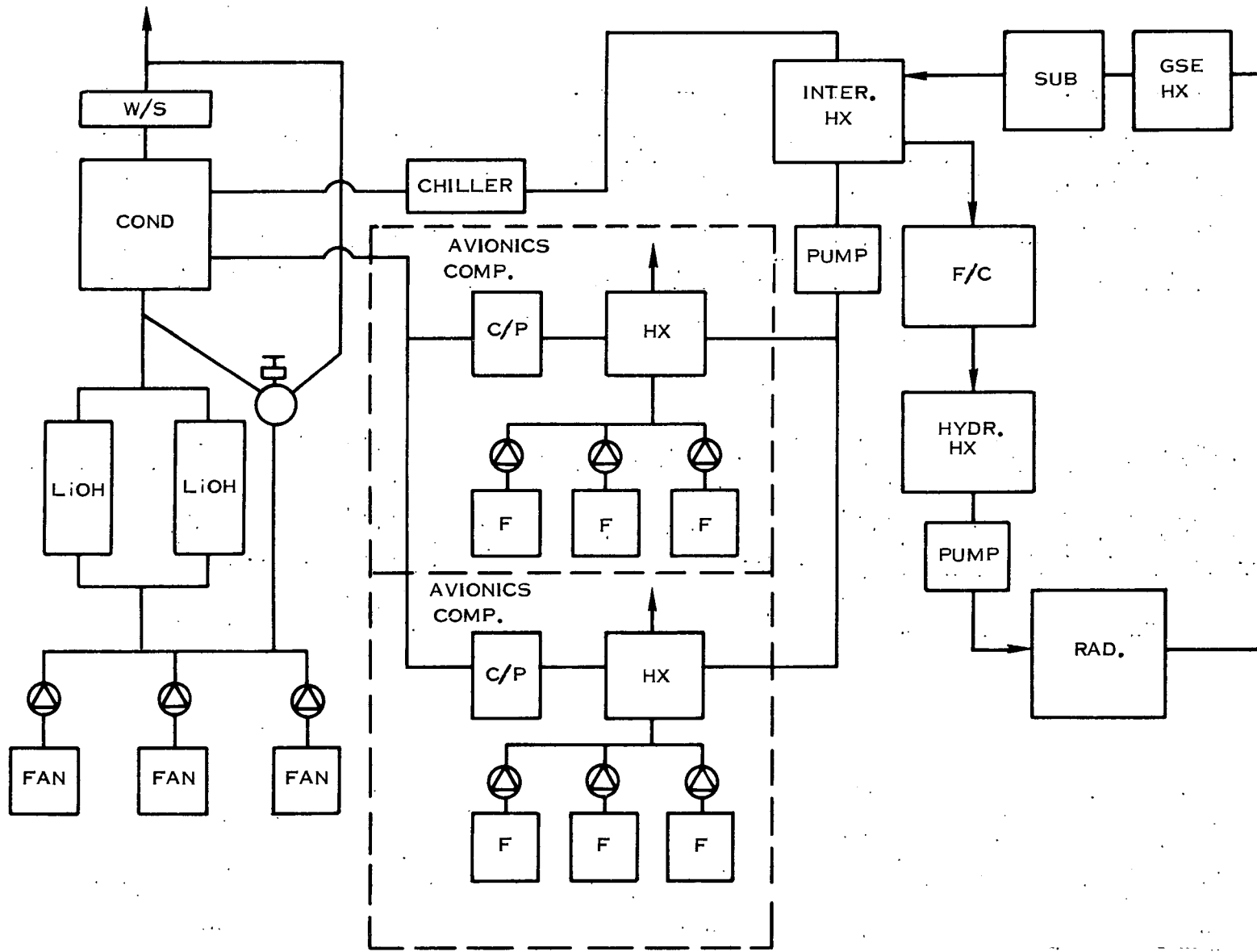
SECTION 4.0
OPERATING PROCEDURES

4.0 OPERATING PROCEDURES4.1 How To Set Up The Deck

The data cards are set up as shown in Figure 4-1. The object of source deck with the system control cards are denoted by (1). The next card (2), the first data card, is a "comment" card. This card will be printed with the case. It must not be blank. The rest of the data for the first case is denoted by (3). The last card of (3) has a "minus" in the second field. This denotes the fact that this is the last data card for a particular case. The next case consists of another comment card (4) and whatever data it is desirable to change from the previous case. This is shown as (5). Again the last card in (5) has a "minus" in the second field. A run is ended by putting a blank card (6) at the end of the last case.

All of the data cards with the exception of the "comment" card, are set up according to the format shown in Figure 4-2. A card is divided into 8 fields. The first field is one (1) digit long. In this field a number is noted telling the load routine how many pieces of input are on this card. The digit will be between 0 and 5. The second field is the location in the input data block into which the first piece of information will be loaded. This field extends from the second digit to the 12th digit. A minus sign in this field will terminate a case.

Field 3 contains the first piece of input data which is loaded into the location given in the second field. The number may be punched anywhere within the field and must contain a decimal point. Data in fields 4, 5, 6, and 7 are loaded into sequential locations in the data block. The last field, locations 73 and 80 may be used as a



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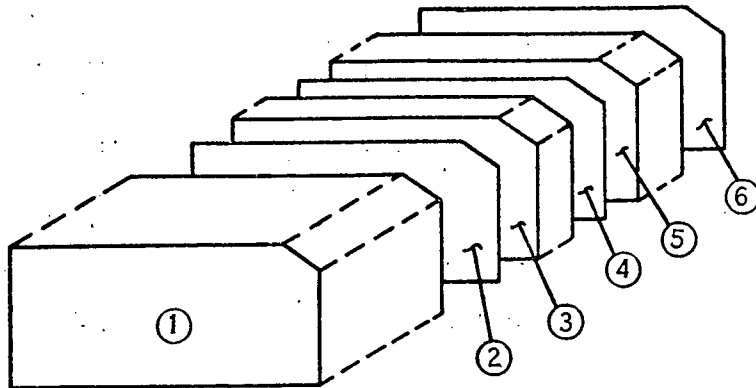


FIGURE 4-1 DECK SET UP

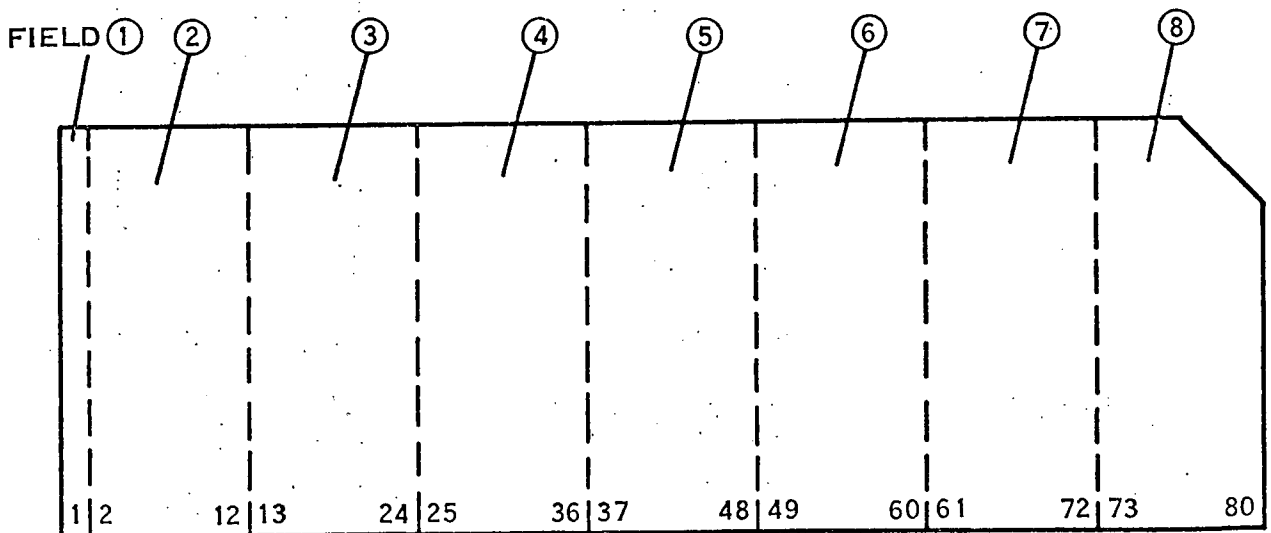


FIGURE 4-2 COMPUTER CARD SETUP

4.1 (Continued)

label. It is not examined by the computer and may contain any alpha-numeric character desired.

If a number does not appear in the second field, the data will be loaded into sequential locations from the previous piece of data input. The first data card in the case must have a location to place the data in the second field.

Definition of input data including location and units are described in the next Section 4.2. Input required for a typical case is shown in Figure 4-3. If a second case is added after the first case, the only input data that must be inputed is that desired to be changed. In the case shown in Figure 4-3, the cabin temperature is changed from 65°F to 70°F.

4.2 Program Input and Output4.2.1 Input Definition

The following information provides the input definition for operating the program. Information includes location, symbols, the printed label, description, and unit. An explanation of all symbols is presented in Appendix I. Typical printouts of the input data are shown in Figures 4-4, 4-5, and 4-6 for a sizing case, performance case, and an orbital transient case, respectively.

INPUT DATA SHEET

NAME R. Balinskas MAIL ADDRESS _____ TEL. EXT. _____
 PROGRAM NO. H247 TITLE _____ ESTIMATED COMPUTER TIME _____ SHEET 1 OF 2
 JOB NO. _____ KEYPUNCHER: 1. Do not verify title cards. COMPUTER MODEL _____
 2. Observe dotted lines only for numbers containing "E."

4-5

PROGRAM INFO		INPUT DATA										LABEL	
n	LOCATION NO.	1		2		3		4		5			
1	3	13	21	25	33	37	45	49	57	61	69	73	80
	MULSS SIZING	CASE	MAX	HEAT LOAD	TCAB	=	65						
5	1.	65.		14.5		53.3		34.		1600.			
5	6.	1.		.25		62.4		85.		13.2			
5	11.	7.		2070.		6700.		1230.		17500.			
5	16.	0.		23000.		4200.		1.		2.			
5	21.	2.		.01		24000.		2.		15.			
5	26.	15.		1.		1.		.73		1.			
5	31.	2.		0.		.16		.0013		0.			
5	36.	0.		20.		1.04		0.		0.			
5	41.	2.25		1.3		40.		60.		2.25			
5	46.	.5		459.		.24		900.		.16			
5	51.	0.		0.		0.		0.		120.			
5	56.	120.		1.3		1.3		0.		1.19			
5	61.	2.		120.		.16		0.		30.			
5	66.	0.		0.		.04		0.		2.			
5	71.	0.		0.		4.		0.		115.			
5	76.	150.		1.		.9		0.		0.			
1	100.	1.											
5	101.	.0632		.0432		0.		3.		.022			
5	106.	3.		5.22		.08		1.785		2.5			
5	111.	3.		2.		1.		4.		1.			
5	116.	.0432		3.		.052		3.		.0231			
5	121.	.011		.001		0.		.08		.0082			

SP 01T72

INPUT DATA SHEET

NAME R. Balinskas MAIL ADDRESS _____ TEL. EXT. _____

PROGRAM NO. H247 TITLE _____ ESTIMATED COMPUTER TIME _____ SHEET 2 OF 2

JOB NO. _____ KEYPUNCHER: 1. Do not verify title cards. COMPUTER MODEL _____

2. Observe dotted lines only for numbers containing "E."

PROGRAM INFO		INPUT DATA										LABEL	
n	LOCATION NO.	1		2		3		4		5			
1	3	13	21	25	33	37	45	49	57	61	69	73	80
5	126.	0.		0.		0.		0.		0.			
5	131.	18.3		10.5		12.3		45.55		0.			
5	136.	44.0		999.		22.1		0.		0.			
5	141.	0.		0.		0.		44.3		0.			
5	146.	0.		0.		0.		0.		0.			
5	151.	.8		30.		0.		0.		26.6			
5	156.	0.		0.		0.		0.		0.			
5	161.	1.25		1.25		1.25		1.25		1.0			
5	166.	1.25		1.35		1.25		1.15		1.0			
5	171.	1.25		1.25		1.25		1.15		1.15			
5	176.	1.25		1.25		1.25		1.25		1.0			
5	181.	1.0		1.25		1.0		1.25		1.25			
5	186.	1.		1.		1.		1.		1.			
5	221.	0.		0.		0.		.20		0.			
5	226.	.22		0.		0.		.6		.35			
5	231.	.35		.35		0.		0.		0.			
5	236.	0.		.35		0.		.35		.0			
0	-1.												
	MULSS SIZING CASE	TCAB = 70											
1	1.	70.											
0	-1.												

4-6

SP 01T72

MULSS SIZING CASE MAX HEAT LOAD TCAB = 65										DATE 10/11/72		TIME 18-54-57			
INPUT DATA															
65.00	TCAB	14.50	PCAB	53.30	PGAS	34.000	TRADO	1600.00	WRAD	1.00	CPCOOL	0.25	CPRAD	62.40	RHOC
85.00	RHOR	13.20	WCO2	7.00	DAYS	2070.0	OSMET	6700.0	QSENE	1230.0	QLMET	17500.0	QCP1	0.0	QCP2
23000.0	QFCELL	4200.0	QSUBL	1.0	KEY CO2	2.0	KEY H2O	2.00	DTIHX	0.010	TOLP	24000.0	TVENT	2.000	DAYEM
15.00	NO TRAD	15.00	NO TIHO	1.00	BLANK	1.00	NO QLAT	0.730	RHMAX	1.00	WC/WR	2.0000	DI RADD	0.0	EF FC
0.1600	PPFIX	0.00130	PPVAR	0.0	KEY HXS	0.0	KEY OPT	20.0000	NO WC	1.0400	FACT WC	0.0	KEY RAD	0.0	KEY CON
2.25	DP H2O	1.30	DP SHX	40.00	DP CP	60.00	DP RP	2.25	DP CO2	0.50	DP VENT	459.00	T SINK	0.24	CPA
900.00	AMAX	0.16	FEXP	0.0	QAHIN	0.0	QCPM	0.0	QE1	0.0	QE2	120.00	TE1	120.00	TE2
1.30	DPE1	1.30	DPE2	0.0	F RAD	1.19	F CO2	2.00	FN CO2	120.00	TCMAX	0.160	CCO2L	0.0	EFH2O
30.0	CYCLE	0.0	QEB2	0.0	WF/C	2.0	KEYSK	0.0	WCOCL	0.0	TIFXI	4.00	TIMECY	0.0	TIMESB
0.0	OCHIL	0.040	TOLQ	0.0	NUBERH	0.9000	EMIS	20.0	STEP	0.0	TORBIT	1.0	PERF		
115.00	TFCI	150.30	TFCO	1.0	NUBERH	0.9000	EMIS	20.0	STEP	0.0	TORBIT	1.0	PERF		
COMPONENT WEIGHT FACTORS															
COND	SENHX	W/S	PUMPC	HXINT	PUMPR	RAD	SUB	LIOH	VENT	FANC	FANS	C	HSC	CONTM	
0.0632	0.0437	0.0	3.0000	0.0220	3.0000	5.2200	0.0000	1.7850	2.5000	3.0000	2.0000	1.0000	4.0000	1.0000	
SUBSYSTEM FIXED WT															
18.30	10.50	12.30	45.55	0.0	44.00	959.00	22.10	0.0	0.0	0.0	0.0	0.0	44.30	0.0	
STRUCTURAL WT FACTORS															
1.2500	1.2500	1.2500	1.2500	1.0000	1.2500	1.3500	1.2500	1.1500	1.0000	1.2500	1.2500	1.2500	1.1500	1.1500	
COMPONENT WEIGHT FACTORS															
EBHX1	EBFAN1	FRHX2	EBFAN2	FCHX	GSEHX	CRYHX	CHILL	SUBLT	FEVAP	A	B				
0.0432	3.0000	0.0520	3.0000	0.0231	0.0110	0.0010	0.0	0.0800	0.0082	0.0	0.0				
SUBSYSTEM FIXED WT															
0.0	0.0	0.0	0.0	0.0	0.8000	30.0000	0.0	0.0	26.6000	0.0	0.0				
STRUCTURAL WT FACTORS															
1.2500	1.2500	1.2500	1.2500	1.0000	1.0000	1.2500	1.0000	1.2500	1.2500	1.0000	1.0000				

4-7

FIGURE 4-4. SIZING CASE INPUT

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PERFORMANCE												DATE 10/11/72	TIME 18-55-33		
INPUT DATA															
70.00	TCAB	14.50	PCAB	53.30	PGAS	34.000	TPADD	1600.00	WRAD	1.00	CPCOOL	0.25	CPRAD	62.40	RHOC
85.00	RHOR	13.20	MC02	7.00	DAYS	2070.0	QSMET	6700.0	QSENE	1230.0	OLMET	17500.0	QCP1	0.0	QCP2
23300.0	QFCELL	4200.0	OSURL	1.0	KEY CO2	2.0	KEY H2O	2.00	DTIHX	0.010	TOLP	24000.0	TVENT	2.000	DAYEM
15.00	NO TRAD	15.00	NO TIHO	1.00	BLANK	1.00	NO QLAT	0.730	PHMAX	1.00	WC/WR	2.0000	DT RADD	0.0	EF FC
0.1600	PPFIX	0.00130	PPVAR	0.0	KEY HXS	0.0	KEY OPT	20.0000	NO WC	1.0400	FACT WC	0.0	KEY RAD	0.0	KEY COM
2.25	DP H2O	1.30	DP SHX	40.00	DP CP	60.00	DP RP	2.25	DP CO2	0.50	DP VENT	459.00	T SINK	0.24	CPA
900.00	AMAX	0.16	FEXP	0.0	QAMIN	0.0	QCPH	0.0	QE1	0.0	QE2	120.00	TE1	120.00	TE2
1.30	DPE1	1.30	DPE2	0.0	F RAD	1.19	F CO2	2.00	FN CO2	120.00	TCMAX	0.160	CO2L	0.0	EFH2O
30.0	CYCLE	0.0	QEB2												
0.0	QCHIL	0.040	TOLQ	657.1	WF/C	2.0	KEYSK	1946.6	KCOOL	39.4	TIFXI	4.00	TIMCY	0.0	TIMESB
115.00	TFCI	150.00	TFCO	1.0	NUBFRH	0.9000	EMIS	20.0	STEP	0.0	TORBIT	2.0	PERF		
COMPONENT POWERS -WATTS															
0.0	0.0	0.0	84.54	0.0	338.53	0.0	0.0	0.0	0.0	411.60	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.000	0.000	0.000	0.000	0.000	-0.000	0.000	0.000	0.000	0.000	-0.000
COMPONENT FACTORS-UA, FFF, ETC.															
2320.04	0.0	0.0	0.20	7504.62	0.22	889.83	1352.48	0.60	0.35	0.35	0.35	0.0	0.0	0.0	0.0
0.0	0.35	0.0	0.35	3962.73	857.67	221.11	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
COMPONENT FLOW RATES-CFH															
32653.9	COND	0.0	SENF	0.0	AVFAAH	0.0	AVFANP	0.0	VENTF	3960.0	LJH				

FIGURE 4-5. PERFORMANCE CASE INPUT

H2O REQUIRED									
DATE 10/11/72 TIME 18-55-34									
INPUT DATA									
75.00 TCAR	14.50 PCAR	53.30 RGAS	34.000 TRADO	1600.00 WRAD	1.00 CPCOOL	0.25 CPRAD	62.40 RHOC		
85.00 RHOR	13.20 WCO2	7.00 DAYS	2070.0 QSMET	6700.0 QSENE	1230.0 QLMET	17500.0 QCP1	0.0 QCP2		
23000.0 QFCCELL	4200.0 QSUBL	1.0 KEY CO2	2.0 KEY H2O	2.00 DTIHX	0.010 TOLP	24000.0 TVENT	2.000 DAYEM		
15.00 ND TPAD	15.00 NO TIMD	1.00 BLANK	1.00 NO QLAT	0.730 RHMAX	1.00 WC/WR	2.0000 DT RADO	0.0 EF FC		
0.1600 PPFIX	0.00130 PPVAR	0.0 KEY HXS	0.0 KEY OPT	20.0000 NO WC	1.0400 FACT WC	0.0 KEY RAD	0.0 KEY CON		
2.25 DP H2O	1.30 DP SHX	40.00 DP CP	60.00 DP RP	2.25 DP CO2	0.50 DP VENT	459.00 T SINK	0.24 CPA		
900.00 AMAX	0.16 FFXP	0.0 OAMIN	0.0 QCPM	0.0 QE1	0.0 QE2	120.00 TE1	120.00 TE2		
1.30 DPE1	1.30 DPE2	0.0 F RAD	1.19 F CO2	2.00 FN CO2	120.00 TCMAX	0.160 CO2I	0.0 EFH2O		
30.0 CYCLE	0.0 QEB2								
0.0 QCHIL	0.040 TOLQ	657.1 WF/C	2.0 KEYSK	1946.6 WCOOL	39.4 TIFXI	4.00 TIMECY	0.0 TIMESB		
115.00 TFCT	150.00 TFCC	1.0 NURFRH	0.9000 EMIS	20.0 STEP	0.0 TORBIT	3.0 PERF			

4-9

FIGURE 4-6. ORBITAL TRANSIENT CASE INPUT

LOCATION	PROGRAM SYMBOL	PRINTED LABEL	DESCRIPTION	UNIT
1	TCAB	TCAB	Cabin Temperature	°F
2	PCAB	PCAB	Cabin Pressure	psia
3	RA	RGAS	Cabin Atmosphere Gas Constant	ft/°F
4	TROIN	TRADO	Radiator Outlet Coolant Temp. a) If value is 0 and EX in location 36 is 0, program will find initial radiator outlet temp. b) If value is >0 and EX is 0, program will use input value as initial radiator outlet temp. c) If EX is >0, program will not optimize and will use input value for radiator outlet temp.	°F
5	WCIN	WRAD	Radiator Loop Coolant Flow Rate a) If value is >0 and EX in location 36 is 0, program will use input value as initial flow rate b) If EX is >0, program will not optimize and will use input value for flow rate	lb/hr
6	CPC	CPCOOL	Coolant Loop Specific Heat	BTU/lb/°R
7	CPR	CPRAD	Radiator Loop Specific Heat	BTU/lb/°R
8	RHOC	RHOC	Coolant Loop Density	lb/ft ³
9	RHOR	RHOR	Radiator Loop Density	lb/ft ³
10	WC02	WC02	CO ₂ Generation Rate	lb/day
11	DAYN	DAYS	Normal Mission Length	days

LOCATION	PROGRAM SYMBOL	PRINTED LABEL	DESCRIPTION	UNITS
12	QSM	QSMET	Sensible Metabolic Heat Load	BTU/hr
13	QSE	QSENE	Cabin Air Heat Load (Q wall + Q elect)	BTU/hr
14	QLM	QLMET	Latent Metabolic Heat Load	BTU/hr
15	QCP1	QCP1	Coolant Loop Cold Plate Heat Load	BTU/hr
16	QCP2	QCP2	Radiator Loop Cold Plate Heat Load	BTU/hr
17	QFC	QFCELL	Fuel Cell Heat Load (Less Heat Load Due to EC/LSS Power)	BTU/hr
18	QSUBI	QSUBL	Heat Load Rejected by Flash Evaporator Sublimator Using Excess Fuel Cell Water	BTU/hr
19	M1	Key CO ₂	CO ₂ Removal Key a) 1 = LIOH b) 2 = Solid Amine (HS-C)	
20	M2	Key H ₂ O	Humidity Control Key b) 1 = Solid Amine c) 2 = Condenser	
21	DTX	DTHX	Initial Temp. Difference Between Coolant and Radiator Loops	°F
22		TOLP	Not Used	
23	TV QL	TVENT	Minimum Cabin Ventilation Flow Req.	EHH
24	DAYE	DAYEM	Emergency Contingency Period	days

LOCATION	PROGRAM SYMBOL	PRINTED LABEL	DESCRIPTION	UNITS
25	RMAX	NO TRAD	Max. Times Thru Radiator Outlet Temp Loop	
26	HXIM	NO TIHO	Max. Times Thru Interface HX Outlet Temp Loop	
27		BLANK	Not Used	
28		NO QLAT	Not Used	
29	RHMAX	RHMAX	Max Allowable Cabin Relative Humidity	Decimal fraction
30	WRAT	WC/WR	Coolant/Radiator Loop Mass Flow (WC _P Coolant/WC _P Radiator)	
31	FW1	DT RADO	Increments of Radiator Outlet Temp (TRO Increased by this value each iteration)	°F
32	FW2	EFFC	Waste Heat Factor For Fuel Cell (Q waste heat/output power)	BTU/hr/watt
33	PPF	PPFIX	Fixed Power Penalty	lb/watt
34	PPV	PPVAR	Expendable Power Penalty	lb/watt hr
35	FW5	KEY HXS	Heat Exchanger Arrangement Key a) 0 = no sensible HX b) 1 = separate sensible HX	
36	EX	KEY OPT	Optimization Key a) 0 = optimize coolant flow rate and radiator outlet temp. b) 1 = no optimization - use input coolant flow rate and radiator outlet temp.	
37	EY	NO WC	Max Times Thru Coolant Flow Rate Loop	

LOCATION	PROGRAM SYMBOL	PRINTED LABEL	DESCRIPTION	UNITS
38	DWC	FACT WC	Factor Flow Rate is Increased by Every Iteration (new flow rate/old flow rate)	
39	Not Used			
40	Not Used			
41	DP1	DP H ₂ O	ΔP Of Humidity Control Equip	In. H ₂ O
42	DP2	DP SHX	ΔP Of Sensible HX	In. H ₂ O
43	DP4	DP CP	ΔP Of Coolant Loop Pump	psi
44	DP6	DP RP	ΔP Of Radiator Loop Pump	psi
45	DP9	DP CO ₂	ΔP Of CO ₂ Removal Equip.	In. H ₂ O
46	DP10	DP VENT	ΔP Of Ventilation System	In. H ₂ O
47	TS	TSINK	Radiator Sink Temp.	°R
48	CPA	CPA	Cabin Atmosphere Specific Heat	ft/°R
49	AMAX	AMAX	Maximum Allowable Radiator Area	ft ²
50	FEXP	FEXP	Heat Rejection Expendable Weight Penalty Used to Top Radiator if Area Exceeds Max. Allowable	lb/BTU/hr
51	Not Used			
52	Not Used			
53	QE1	QE1	Air Cooled Electronic Bay in Coolant Loop Heat Load (less fan)total	BTU/hr
54	QE2	QE2	Air Cooled Electronic Bay in Radiator Loop Heat Load (less fan)	BTU/hr

LOCATION	PROGRAM SYMBOL	PRINTED LABEL	DESCRIPTION	UNITS
55	TE1	TE1	Air Cooled Electronic Bay In Coolant Loop Max. Air Temp.	°F
56	TE2	TE2	Air Cooled Electronic Bay In Radiator Loop Max. Air Temp.	°F
57	DPE1	DPE1	ΔP Of Fan In Coolant Loop Elect. Bay	in. H ₂ O
58	DPE2	DPE2	ΔP Of Fan In Radiator Loop Elect. Bay	in. H ₂ O
59	FRAD	FRAD	0. - Calculates RAD Area 1. - Uses RAD Area in 49.	
60	FCO2	FCO2	LiOH Heat Load Factor <u>Actual Production Rates</u> Ave. Production Rate	
61	FN CO2	FN CO2	No. of LiOH Cans on Line	
62	TCMAX	TCMAX	Max. Allowable Coolant Temp. Out Of Cold Plates	°F
63	CHSB	CO2L	HSC CO ₂ Loading	lbs/lb
64	Not Used			
65	CYCL	CYCL	HSC 1/2 Cycl Time	minutes
66	QEB2	QEB2	Heat load of Second EBAY in series - Cabin Loop	BTU/Hr
67	QCHIL	QCHIL	Low Temp. Chiller Heat Load	BTU/Hr
68	TOLQ	TOLQ	Tolerance on Sensible Heat Load Converg	decimal fraction
69	WFC	WFC	Fuel Cell Coolant Mass Flow Rate	BTU/Hr-°F

LOCATION	PROGRAM SYMBOL	PRINTED LABEL	DESCRIPTION	UNITS
70	RN	NR	Heat Rejection Sink 1 - RAD + SUB 2 - RAD + CRY 3 - RAD + FLASH EVAP 4 - SUB 5 - CRYO 6 - FLASH EVAP	
71	WC	WC	Calculated Optimum Flow Rate (Used for off design Performance)	
72	TZ	TIFXI	Freon Loop Control Temp (into int HX)	°F
73	TCRY	TCRY	Time Cry. HX is Used @ Full Heat Load	hrs.
74	TSUB	TSUB	Time Sublimator or Flash Evaporator is Used that H ₂ O Must be Supplied	hrs.
75	TFCI	TFCI	Temp. of Fluid Entering F/C	°F
76	TFCO	TFCO	Temp. of Fluid Leaving F/C	°F
77	FRESH	NFRESH	No. of Fresh LiOH Cart. On Line	
78	EMIS	EMIS	Radiator Emissivity	
79	STEP	STEP	No. of Steps Taken to Determine Radiator Topping Requirements	
80	TAU	TIME	Time Required for 1 Orbit	hrs.
100	PERF	PERF	1 - Sizing Program 2 - Performance Program 3 - Radiator/Evaporator Sizing	
101	FWT (1)	COND	Component Weight Factors Condenser - Weight/UA	lb/btu/hr/°F

LOCATION	PROGRAM SYMBOL	PRINTED LABEL	DESCRIPTION	UNITS
102	FWT (2)	SENHX	Sensible Heat Exchanger - Weight/UA	lb/btu/hr/°F
103	(3)	W/S	Water Separator	
104	(4)	PUMPC	Coolant Pump - No. of Pumps	
105	(5)	HXINT	Interface HX - Weight/UA	lb/btu/hr/°F
106	(6)	PUMPR	Radiator Pump - No. of Pumps	
107	(7)	RAD	Radiator - Area/WC _P (B-C)	ft ² /btu/hr/°F
108	(8)	SUB	Sublimator - Weight/UA	lb/btu/hr/°F
109	(9)	LiOH	LiOH - Packaging Factor For Canisters	
110	(10)	VENT	Ventilation Fans - No. of Fans	
111	(11)	FANC	Condenser Fan - Number	
112	(12)	FANS	Sens. HX Fan - Number	
113	(13)	MC	Molecular Sieve - Not Used	
114	(14)	HSC	Number of Canisters	lb
115	(15)	CONTM	Charcoal Canister - pkg Factor for Canister	
116	(16)	EBHXI	Coolant Loop Elect Bay HX Weight/UA	lb/btu/hr/°F
117	(17)	EBFANI	Coolant Loop Elect Bay Fan - Number of Fans	
118	(18)	EBHX2	Radiator Loop Elect Bay HX - weight/UA	lb/btu/hr/°F
119	(19)	EBFAN2	Radiator Loop Elect. Bay Fan Number of Fans	

LOCATION	PROGRAM SYMBOL	PRINTED LABEL	DESCRIPTION	UNITS
120	FWT (20)	FCHX	Fuel Cell HX	lbs/btu/hr/°F
121	(21)	GSEHX	GSE HX - Not Used	lbs/btu/hr/°F
122	(22)	CRYHX	Cryogenic H ₂ HX	lbs/btu/hr/°F
123	(23)	CHILL	Low Temp Chiller - Not Used	
124	(24)	SUBLT	Topping Sublimator	lbs/btu/hr/°R
125	(25)	FLASH	Flash Evap	lbs/btu/hr/°R
131	FXW (1)	COND	Subsystem Fixed Weight Condenser	lb
132	(2)	SENHX	Sensible Heat Exchanger*	lb
133	(3)	W/S	Water Sep *	
134	(4)	PUMPC	Coolant Loop *	lb
135	(5)	HXINT	Interface HX	lb
136	(6)	PUMPR	Radiator Loop Pump *	lb
137	(7)	RAD	Radiator - Weight of Hinge For Fold Out	lb
138	(8)	SUB	Sublimator	lb
139	(9)	LiOH	LiOH *	lb
140	(10)	VENT	Ventilation Fans - Not Used	
141	(11)	FANC	Condenser Fan	lb
142	(12)	FANS	Sensible Fan	lb
143	(13)	C	Not Used	lb
144	(14)	HSC	HSC Fixed Wt.	lb

LOCATION	PROGRAM SYMBOL	PRINTED LABEL	DESCRIPTION	UNITS
145	FXW (15)	CONTM	Charcoal Canister	lb
146	(16)	EBHX1	Coolant Loop Elect. Bay HX*	lb
147	(17)	EBFAN	Coolant Loop Elect. Bay Fan*	lb
148	(18)	EXHX2	Radiator Loop Elect. Bay HX*	lb
149	(19)	EBFAN2	Radiator Loop Elect. Bay Fan*	lb
150	(20)	FCHX	Fuel Cell HX	lb
151	(21)	GSEHX	GSE HX	lb
152	(22)	CRYHX	Cryogenic HX	lb
153	(23)	CHILL	Not Used	
154	(24)	SUBLT	Not Used	
155	(25)	FLASH	Flash Evaporator	
161	SWT (1)	COND	Structural Weight Factors Condenser Fans	
162	(2)	SEN HX	Sensible HX & Process Flow Fans	
163	(3)	WS	Water Sep *	
164	(4)	PUMPC	Coolant Loop Pump	
165	(5)	HXINT	Interface HX	
166	(6)	PUMPR	Radiator Loop Pump	lb/ft ²
167	(7)	RAD	Radiator	
168	(8)	SUB	Sublimator	

* Program Factors Fixed wt by Structure wt Factor
FXW (n) * SWT (n)

LOCATION	PROGRAM SYMBOL	PRINTED LABEL	DESCRIPTION	UNIT
169	(9)	LIOH	LiOH	
170	(10)	VENT	Ven tilation Fans	
171	(11)	FANC	Condenser Fan	
172	(12)	HSB	Sensible Fan	
173	(13)	MS	Not Used	
174	(14)	H2DP	HSC	
175	(15)	CONTM	Charcoal Canister	
176	(16)	EBHX1	Coolant Loop Elect. Bay HX	
177	(17)	EBFAN1	Coolant Loop Elect. Bay Fan	
178	(18)	EBHX2	Radiator Loop Elect. Bay HX	
179	(19)	EBFAN2	Radiator Loop Elect. Bay Fan	
180	(20)	FCHX	Fuel Cell HX's	
181	(21)	GSEHX	Not Used	
182	(22)	CRYHX	Cryogenic HX	
183	(23)	CHILL	Not Used	
184	(24)	SUBLET	Not Used	
185	(25)	FLASH	Flash Evaporator	
191-220	PW (30)	PW (30)	Power Table For All Components	
221-250	CFT (30)	CFT (30)	Component Factors (UA, η , Etc.)	
426-500	T (75)	Not Printed	Table of HSC Performance (Water Loading VS Partial Press and Air Flow/lb Bed)	

LOCATION	PROGRAM SYMBOL	PRINTED LABEL	DESCRIPTION	UNITS
351- 425	-	Not Printed	CO ₂ Bed Loading Vs Air Flow LB Bed & PCO ₂	
221	CFT (1)		Condenser UA	BTU/Hr-°F
222	(2)		Sens HX UA	BTU/Hr-°F
223	(3)		-	
224	CFT (4)		Coolant Pump EFF	
225	(5)		Inter HX UA	BTU/Hr-°F
226	(6)		Radiator Loop Pump EFF	
227	(7)		RAD Area	Ft ²
228	(8)		Sublimator UA	BTU/Hr-°F
229	(9)		LiOH Removal EFF of CO ₂	
230	(10)		Vent Fan EFF	
231	(11)		Condenser Fan EFF	
232	(12)		Sensible Fan EFF	
233	(13)		-	
234	(14)		HSC Bed Size	Lbs
235	(15)		-	
236	(16)		EBHX UA	BTU/Hr-°F
237	(17)		EBFAN EFF	
238	(18)		EBHX2 UA	BTU/Hr-°F
239	(19)		EBFAN 2FF	
240	(20)		Fuel Cell HX UA	BTU/Hr-°F

LOCATION	PROGRAM SYMBOL	PRINTED LABEL	DESCRIPTION	UNITS
241	(21)		-	
242	(22)		CRY. HX UA	BTU/Hr-°F
243	(23)		-	
244	(24)		Topping Sub UA	BTU/Hr-°F
245	(25)		Flash Evap UA	BTU/Hr-°F
251	V11		Condenser Fan Air Low Rate	CFH
252	V12		Sensible Fan Air Flow Rate	CFH
253	V9		LiOH Air Flow Rate	CFH
254	V10		Ventilation Fan Air Flow Rate	CFH
255	V17		Cabin Loop Cooled Avion. Bay Fan Flow	CFH
256	V19		Radiator Loop Cooled Avion. Bay Fan Flow	CFH
301-350			Radiator Influx vs Orbit Position	
501-517			Qmetabolic Table	

PROGRAM OUTPUT4.2.2 Program Output

The program output can be separated by the type of case that is run:

- a. Sizing
- b. Off-Design Performance
- c. Orbital Radiator/Evaporator Transient

For all cases, the input data in locations 1 - 100 (that are used) are printed. The labels are described in the table that describes the input data.

For the sizing program, the Weight factors (FWT, FXW, & SWT) are printed under the component name and in component order: from 1 to 15 and from 16 to 27. Tables of optimization results are printed in the following order:

1. Optimization of the interface heat exchanger outlet coolant temperature for each radiator outlet temperature.
2. A summary table of the optimum total equivalent weight for each radiator outlet temperature at a given flow rate.
3. A summary table of the optimum total equivalent weight for each flow rate.

Lastly, the results of the optimum condition are printed so that a flow chart can be produced.

4.2.2 (Continued)

The labels that are printed with the output data are described in the following tables:

Table 4-1	Sizing Program
Table 4-2	Off-Design Performance Program
Table 4-3	Orbital Transient Program

As with the input, all labels and symbols are explained in Appendix 1.

Typical computer output printouts are shown in Figure 4-7, 4-8, and 4-9. These outputs are for the respective inputs which are shown in Figures 4-4, 4-5, and 4-6.

OUTPUT DATA

TOTEQWT	TINHXC	TOTPW	TOTWT	1871.8 WC	TRQ
5827.0	36.0	790.4	5478.5		34.00
5744.1	37.0	808.0	5388.0		
5723.8	38.0	827.5	5359.0		
5740.4	39.0	849.3	5366.0		
5805.1	40.0	849.3	5430.7		
6182.5	41.0	827.5	5817.7		
TOTEQWT	TINHXC	TOTPW	TOTWT	1871.8 WC	36.00 TRQ
5677.2	36.0	790.4	5328.8		
5594.4	37.0	808.0	5238.2		
5574.1	38.0	827.5	5209.3		
5590.6	39.0	849.3	5216.2		
5655.4	40.0	849.3	5281.0		
6032.7	41.0	827.5	5668.0		
TOTEQWT	TINHXC	TOTPW	TOTWT	1871.8 WC	38.00 TRQ
5527.5	36.0	790.4	5179.0		
5444.7	37.0	808.0	5088.5		
5424.3	38.0	827.5	5059.5		
5440.9	39.0	849.3	5066.5		
5505.6	40.0	849.3	5131.2		
5883.0	41.0	827.5	5518.2		
TOTEQWT	TINHXC	TOTPW	TOTWT	1871.8 WC	40.00 TRQ
5377.7	36.0	790.4	5029.3		
5294.9	37.0	808.0	4938.7		
5274.6	38.0	827.5	4909.8		
5291.1	39.0	849.3	4916.8		
5355.9	40.0	849.3	4981.5		
5733.3	41.0	827.5	5368.5		
TOTEQWT	TINHXC	TOTPW	TOTWT	1871.8 WC	42.00 TRQ
5228.0	36.0	790.4	4879.6		
5145.2	37.0	808.0	4789.0		
5124.8	38.0	827.5	4760.1		
5141.4	39.0	849.3	4767.0		
5206.1	40.0	849.3	4831.8		
5583.5	41.0	827.5	5218.7		
TOTEQWT	TINHXC	TOTPW	TOTWT	1871.8 WC	44.00 TRQ
5114.2	37.0	808.5	4757.8		
5040.5	38.0	828.0	4675.5		
5037.1	39.0	849.9	4662.5		
5052.7	40.0	849.9	4718.0		
5491.5	41.0	828.0	5126.5		
OPTIMUM CONDITION			1871.8 WC		
TOTEQWT	TRQ	TINHXC	TOTPW	TOTWT	
5723.8	34.0	38.0	827.5	5359.0	
5574.1	36.0	38.0	827.5	5209.3	
5424.3	38.0	38.0	827.5	5059.5	
5274.6	40.0	38.0	827.5	4909.8	
5124.8	42.0	38.0	827.5	4760.1	
5037.1	44.0	39.0	849.9	4662.5	
TOTEQWT	TINHXC	TOTPW	TOTWT	1946.6 WC	34.00 TRQ
5883.4	36.0	790.8	5534.8		
5796.2	37.0	806.7	5440.6		
5768.9	38.0	824.3	5405.6		
5771.9	39.0	843.8	5399.9		
5807.1	40.0	865.6	5420.6		
5886.7	41.0	897.2	5494.3		
6426.0	42.0	843.8	6054.0		
TOTEQWT	TINHXC	TOTPW	TOTWT	1946.6 WC	36.00 TRQ
5727.6	36.0	790.8	5379.0		
5640.5	37.0	806.7	5284.9		
5613.2	38.0	824.3	5249.8		
5616.1	39.0	843.8	5244.2		
5646.4	40.0	865.6	5264.9		
5731.0	41.0	897.2	5338.6		
6270.2	42.0	843.8	5898.3		
TOTEQWT	TINHXC	TOTPW	TOTWT	1946.6 WC	38.00 TRQ
5571.9	36.0	790.8	5223.3		
5484.8	37.0	806.7	5129.2		
5457.4	38.0	824.3	5094.1		
5460.4	39.0	843.8	5088.4		
5490.7	40.0	865.6	5109.1		
5575.3	41.0	897.2	5182.9		
6114.5	42.0	843.8	5742.6		

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FIGURE 4-7. SIZING CASE OUTPUT (SHEET 1 OF 3)

TOTFGWT	TINHXC	TOTPW	TOTWT	1946.6 WC	40.00 TR0
5416.2	36.0	790.8	5067.6		
5329.0	37.0	806.7	4973.4		
5301.7	38.0	824.3	4938.4		
5304.7	39.0	843.8	4932.7		
5335.0	40.0	865.6	4953.4		
5419.5	41.0	890.2	5027.1		
5958.8	42.0	843.8	5586.8		
TOTFGWT	TINHXC	TOTPW	TOTWT	1946.6 WC	42.00 TR0
5260.4	36.0	790.8	4911.8		
5173.3	37.0	806.7	4817.7		
5146.0	38.0	824.3	4782.6		
5148.9	39.0	843.8	4777.0		
5179.2	40.0	865.6	4797.7		
5263.8	41.0	890.2	4871.4		
5803.0	42.0	843.8	5431.1		
TOTFGWT	TINHXC	TOTPW	TOTWT	1946.6 WC	44.00 TR0
5186.1	37.4	813.0	4827.7		
5106.7	38.4	831.3	4740.3		
5092.6	39.4	851.6	4717.2		
5123.1	40.4	874.3	4737.7		
5251.1	41.4	874.3	4865.7		
TOTFGWT	TINHXC	TOTPW	TOTWT	1946.6 WC	46.00 TR0
5116.6	39.4	851.6	4741.2		
5070.8	40.4	874.3	4685.4		
5165.7	41.4	874.3	4780.3		
TOTFGWT	TINHXC	TOTPW	TOTWT	1946.6 WC	48.00 TR0
5265.2	41.4	874.3	4879.8		
OPTIMUM CONDITION 1946.6 WC					
TOTFGWT	TR0	TINHXC	TOTPW	TOTWT	
5768.9	34.0	38.0	824.3	5405.6	
5613.2	36.0	38.0	824.3	5245.8	
5457.4	38.0	38.0	824.3	5094.1	
5301.7	40.0	38.0	824.3	4938.4	
5146.0	42.0	38.0	824.3	4782.6	
5092.6	44.0	39.4	851.6	4717.2	
5070.8	46.0	40.4	874.3	4685.4	
5265.2	48.0	41.4	874.3	4879.8	
OPTIMUM CONDITIONS SUMMARY					
TOTFGWT	WC	TR0	TINHXC	TOTPW	TOTWT
999999.0	1600.0	34.0	36.0	0.0	0.0
999998.0	1664.0	34.0	36.0	0.0	0.0
999997.0	1730.6	34.0	36.0	0.0	0.0
999996.0	1798.8	34.0	36.0	0.0	0.0
5037.1	1871.8	44.0	39.0	849.9	4662.5
5070.8	1946.6	46.0	40.4	874.3	4685.4
CONDENSER WEIGHTS 183.27 WTHX 12.28 MVALVE					
CONDENSER FAN 9.58 FANWT 1.56 WTVK					
RADIATOR SUBPOUTLINE					
610.51 TIN	503.60 TOUT	517.60 TOUTC	895.14 APADC	900.00 ARMAX	2207.44 WTRFO

FIGURE 4-7. SIZING CASE OUTPUT (SHEET 2 OF 3)

SYSTEM ITERATION WEIGHTS													
35.0	TIHX1	39.02	TIHX0	5037.13	TECWT	4662.48	TOTWT	849.91	TOTPW	65.00	TAOS	48.02	TAOC
0.1653	POPO	1871.8	WC00L	159.896	WBCO2	0.0	WDEF5	0.0	ULLPEN	895.1	ARAD	1048.19	WTEXP
0.0	ULLDES	0.0	ULLCO2	50.3	DEW PT	65.0	TAOF11	65.0	TADE12	65.0	TER1	65.0	TEB2
65.0	TADE2												
COMPONENT POWERS (WATTS)													
H2OREM	HXSENS	W/S	PUMPC	HXINIF	PUMPR	RADWT	SUBLIM	CO2REM	VENT	CONTG	FAN C	FAN A	FAN MS
221.49	0.0	15.77	69.95	165.63	78.55	2207.44	165.07	333.67	0.0	16.60	52.55	0.0	0.0
FBHX1	EBFAN1	EEHY2	EBFAN2	FCHX	CRYHX	WTH2C	WTHYD	FEVAP	GSE				
0.0	0.0	0.0	0.0	88.77	37.72	0.0	150.63	0.0	10.85				
COMPONENT FLOW RATES (CFM)													
H2OREM	SENSE	PUMPC	PUMPR	CO2REM	VENTF	EBAY1	EBAY2						
443.11	0.0	81.29	325.51	0.0	0.0	0.0	0.0						
519.9	H2OREM	66.0	CO2REM	0.0	SENHX	0.0	VENT	0.0	CONTM	585.9	FAN C	0.0	FAN A
0.0	EBAY1	0.0	EBAY2										
CABIN LOOP TEMPERATURES													
39.02	65.39	65.79	65.39	65.39	65.39	102.79	103.38						
RADIATOR LOOP TEMPERATURES													
35.02	99.38	99.38	79.38	148.53	150.91	58.00	44.00	35.02					
HEAT LOADS													
CONDHX	SENSHX	INTERHX	FUELCELL	RADIATOR	FXP HX	TOTLAT	SFNCO2	LATCO2	SENSH2DP	LATH2DP	OSINK		
12337.4	0.0	30115.0	23000.0	43475.0	6551.2	1504.9	549.8	274.9	0.0	0.0	0.0		
54226.2													
EPAY1	EBAY2	SUBLIM											
0.0	0.0	4200.0											

FIGURE 4-7. SIZING CASE OUTPUT (SHEET 3 OF 3)

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LIQH SUBROUTINE-CP2 PARTIAL PRESSURES
3.557 PMAX      2.247 PMIN      549.8 OS      274.9 OL
RADIATOR SUBROUTINE
610.29 TIN      498.97 TOUT      519.97 TOUTC      882.66 ARADC      900.00 ARMAX      2190.59 WTREQ

CRYOGENIC HX PERFORMANCE
39.36 THOTCAL      6.82 WHYD      60.34 THYDC
2295.12      2300.04      509.41      72.41      51.37      70.00

CONDENSER PERFORMANCE
70.00 TCAB      72.41 TARI      51.37 TATPC      478.2 HXCFM      53.58 TOPCAR      10718.7 QSENS      2070.0 QSMET      1504.9 QLTCT
69.99 TFANI      72.41 TFANO

FUEL CELL HX
2300.0 QFC      657.1 WFC      115.00 TF/CI      150.00 TE/CC

CABIN LOOP TEMPS
43.37      43.37      68.49      68.49      68.49      104.45      105.04

RADIATOR LOOP TEMPS
150.69      150.69      60.37      60.37      39.37      39.37      101.05      101.05      101.05      149.31

HEAT LOADS
12223.6 QCOND      0.0 QSENS      288.6 QCPUMP      30018.5 QINTX      1155.7 QRPUMP      43954.3 QRAD
0.0 QEVAP      10219.8 QPY      1504.9 QLAT
  
```

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FIGURE 4-8. PERFORMANCE CASE OUTPUT

RADIATOR/EVAPORATOR		EXPENDABLE USAGE														
54174.2 QDOT		4.1 WEVAVG				20.0 NO.STEP										
ORBIT STEP		1/16	2/17	3/18	4/19	5/20	6/21	7/22	8/23	9/24	10/25	11/26	12/27	13/28	14/29	15/30
WEVAPORANT		8.97	11.67	12.79	11.67	9.57	6.82	4.93	3.32	2.34	1.69	0.68	0.0	0.0	0.0	0.0
T RAD IN		150.69	150.69	150.69	150.69	150.69	150.69	150.69	150.69	150.69	150.69	150.69	150.69	150.69	150.69	150.69
T SINK		475.26	493.59	499.70	493.10	478.20	459.97	443.66	431.95	422.93	414.97	405.48	398.44	391.47	389.32	389.64
TEVAP OUT		39.37	39.37	39.37	39.37	39.37	39.37	39.37	39.37	39.37	39.37	39.37	39.37	39.37	39.37	39.37
OFF TABLES		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

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FIGURE 4-9. ORBITAL TRANSIENT CASE OUTPUT

TABLE 4-1. OUTPUT DATA DESCRIPTION - SIZING

<u>Label</u>	<u>Description</u>	<u>Unit</u>
TOTEQWT	Total equivalent weight	lbs
TINHXO	Water temperature leaving the interface heat exchanger	°F
TOTPW	Total ECS power (thermal control)	watts
TOTWT	Total ECS weight (thermal control)	lbs
WC	Radiator loop flow rate	lbs/hr
TRO	Radiator outlet temperature	°F
WTHX	Heat Exchanger weight	lbs
MVALVE)	Temperature Control Valve weight	lbs
WVALVE)		
WTFAN)	Fan Weight (one)	lbs
FANWT)		
WTVK)	Check valve weight	lbs
WTCK)		
QREJ	Total heat removed	BTU/hr
TCIN	Coolant loop inlet temperature	°F
TCOUT	Coolant loop outlet temperature	°F
WH20	Water usage rate	lbs/hr
WEIGHT	Flash evaporator subsystem weight	lbs
TIN	Radiator inlet temperature	°R
TOUT	Desired radiator outlet temperature	°R

TABLE 4-1. OUTPUT DATA DESCRIPTION - SIZING (CONTINUED)

<u>Label</u>	<u>Description</u>	<u>Unit</u>
TOUTC	Calculated outlet temperature	°R
ARADC	Calculated radiator area	ft ²
ARMAX	Maximum allowable radiator area	ft ²
WTREQ	Radiator weight	lbs
TIHXI	Radiator loop coolant temperature entering interface HX	°F
TIHXO	Cabin loop coolant temperature leaving interface HX	°F
TEQWT	SYSTEM total equivalent weight	lbs
TOTWT	System total weight	lbs
TOTPW	System total power	watts
TAOS	Sensible heat exchanger gas outlet temperature	°F
TAOC	Condenser gas outlet temperature	°F
PDPO	Water vapor pressure leaving the condenser	psia
WCOOL	Optimum coolant flow rate (radiator loop)	lbs/hr
WBCO ₂	Bed weight of the CO ₂ removal system total LiOH wt.	lbs
WBDES	Weight of one HSC Bed	lbs
ULLPEN	Ullage penalty for the HSC subsystem	lbs
ARAD	Calculated radiator area	ft ²
WTEXP	Weight of expendables required to supplement radiator (does not include QSUBL)	lbs

TABLE 4-1. OUTPUT DATA DESCRIPTION - SIZING (CONTINUED)

<u>Label</u>	<u>Description</u>	<u>Unit</u>
ULLDES	Ullage penalty for the HSC subroutine	lbs
ULLCO ₂	Not used	
DEWPT	Cabin dew point	°F
TAOE11	Temperature of air leaving the HX of the first (or only) water cooled avionics bay in series	°F
TAOE12	Temperature of air leaving the HX of the second water cooled avionics bay in series	°F
TEB1	Temperature of the first (or only) water cooled avionic bay in series	°F
TEB2	Temperature of the second water cooled avionics bay in series	°F
TAOE2	Temperature of the gas leaving the heat exchanger of the radiator loop cooled avionics bay	°F
H ₂ OREM	Water removal (HSC or Condenser) subsystem weight	lbs
HXSENS	Sensible HX temperature control subsystem weight	lbs
W/S	Water separator subsystem weight	lbs
PUMPC	Cabin loop pump package weight	lbs
HXINTF	Interface HX's weight	lbs
PUMPR	Radiator loop pump package weight	lbs
RADWT	Radiator weight	lbs
SUBLIM	Sublimator package weight	lbs

TABLE 4-1. OUTPUT DESCRIPTION - SIZING (CONTINUED)

<u>Label</u>	<u>Description</u>	<u>Unit</u>
CO ₂ REM	LiOH Subsystem weight	lbs
VENT	Ventilation fan package weight	lbs
CONTC	Contaminant removal weight	lbs
FAN C	Condenser fan package weight or HSC fan weight increase.	lbs
FAN A	Sensible fan package weight	lbs
FAN MS	Not used	
EBHX1	Water cooled avionics bay HX weight (total)	lbs
EBFAN1	Water cooled avionics bay HX package weight (total)	lbs
EBHX2	Radiator loop avionics bay HX weight	lbs
EBFAN2	Radiator loop avionics bay fan package weight	lbs
FCHX	Fuel cell heat exchanger package weight	lbs
CRYHX	Cryogenic HX package weight	lbs
WTH20	Weight of water required for period when radiator is inoperative	lbs
WTHYD	Weight of hydrogen required for period when radiator is inoperative	lbs
FEVAP	Flash evaporator package weight	lbs
GSE	Ground Support HX weight	lbs

TABLE 4-1. OUTPUT DESCRIPTION - SIZING (CONTINUED)

<u>Label</u>	<u>Description</u>	<u>Unit</u>
<u>COMPONENT POWERS</u>		
H2OREM	Condenser fan or HSC fan power	watts
SENSF	Sensible HX fan power	watts
PUMPC	Cabin loop pump power	watts
PUMPR	Radiator loop pump power	watts
CO2REM	Not used	
VENTF	Ventilation fan power	watts
EBAY1	Avionics bay (water cooled) fan power (total)	watts
EBAY2	Radiator loop avionics bay fan power	watts
<u>COMPONENT FLOW RATES</u>		
H2OREM	Condenser or HSC gas flow rate	CFM
CO2REM	LiOH gas flow rate	CFM
SENHX	Sensible heat exchanger gas flow rate	CFM
VENT	Ventilation fan flow rate	CFM
CONTM	Flow rate supplied by ECS fan through contaminate canister	CFM
FAN C	Condenser fan flow rate	CFM
FAN A	Sensible fan flow rate	CFM
EBAY1	Water Cooled avionics bay fan flow rate	CFM
EBAY2	Radiator loop avionics bay fan flow rate	CFM

TABLE 4-1. OUTPUT DESCRIPTION - SIZING (CONTINUED)

<u>Label</u>	<u>Description</u>	<u>Unit</u>
<u>CABIN LOOP TEMPERATURES</u>		•F
	Printed in order are:	
1st	Leaving the interface HX	
2nd	Leaving the condensing HX	
3rd	Leaving the sensible HX	
4th	Same as 3rd	
5th	Temperature entering the second avionics bay if two in series, otherwise same as 3rd	
6th	Temperature entering cold plates	
7th	Temperature leaving cold plates	
8th	Temperature leaving pump	
<u>RADIATOR LOOP TEMPERATURES</u>		•F
	Printed in order are:	
1st	Temperature entering interface HX	
2nd	Temperature leaving interface HX	
3rd	Temperature leaving avionics bay	
4th	Temperature leaving cold plates	
5th	Temperature leaving F/C HX's	
6th	Radiator inlet temperature	
7th	Radiator outlet temperature	

TABLE 4-1. OUTPUT DESCRIPTION - SIZING (CONTINUED)

<u>Label</u>	<u>Description</u>	<u>Unit</u>
8th	Temperature leaving that portion of the radiator topping HX that must pay for expendables	
9th	Temperature leaving topping heat exchanger	
<u>HEAT LOADS</u>		
CONDHX	Total heat removed by condensing HX	BTU/hr
SENSHX	Heat removed by sensible HX	BTU/hr
INTERHX	Heat transferred by the interface HX	BTU's/hr
FUELCELL	Heat removed from fuel cells	BTU's/hr
RADIATOR	Heat rejected by radiator	BTU's/hr
EXP HX	Portion of heat removed by topping HX for which expendables must be launched	BTU's/hr
TOTLATQ	Total latent heat load removed by condenser	BTU's/hr
SENSCO ₂	Sensible heat generated by LiOH	BTU's/hr
LATCO ₂	Latent heat generated by LiOH	BTU's/hr
SENSH ₂ DP	Not used	
LATH ₂ DP	Not used	
QSINK	Total heat rejected by all heat sinks	BTU/hr
EBAY1	Heat removed in cabin loop avionic bay	BTU/hr
EBAY2	Heat removed in radiator loop avionic bay	BTU/hr
SUBLIM	Heat removed with excess fuel cell H ₂ O	BTU/hr

TABLE 4-1. OUTPUT DESCRIPTION - SIZING (CONTINUED)

<u>Label</u>	<u>Description</u>	<u>Unit</u>
<u>CONDENSER WEIGHTS</u>		
WTHX	Condensing Hx weight	Lbs
MVALVE	Bypass air valve weight	Lbs
<u>SENSIBLE HX</u>		
WTHX	Sensible Hx weight	Lbs
WVALVE	Air bypass valve weight	Lbs
<u>AVIONICS BAY</u>		
WTHX	Weight of one heat exchanger	Lbs
WTFAN	Weight of one fan	Lbs
WTCK	Check valve weight	Lbs
<u>BED LOADING</u>		
1ST	Volumetric air flow per lb of HSC	cfm/lb HSC
2ND	Water vapor pressure	psia
3RD	Bed water loading	lb H ₂ O/lb HSC
4TH	Off Tables Indicator if non-zero	
Next Line Printed in Order		
1ST	Weight of HSC canisters and valves	Lbs
2ND	Weight of fans and check valves	Lbs
3RD	Total Equivalent Weight (excluding ullage)	Lbs
4TH	Weight of HSC per canister	Lbs
Next Line Printed in Order		
WTCAN	Canister weight	Lbs
WVVAL	Vacuum valve weight	Lbs
WCVAL	Humidity control valve weight	Lbs
WTFAN	Increase in fan weight	Lbs
WKVAL	Fan check valve weight	Lbs

F

TABLE 4.1. OUTPUT DESCRIPTION - SIZING (CONTINUED)

<u>Label</u>	<u>Description</u>	<u>Unit</u>
<u>DOUBLE EBAY</u>		
WTHX	Heat exchanger weight (1)	Lbs
WTFAN	Fan weight (1)	Lbs
WTKV	Fan check valve weight (1)	Lbs
<u>FLASH EVAPORATOR SIZE</u>		
QREJ	Heat rejected	BUT/hr
TCIN	Coolant circuit inlet temperature	°F
TCOUT	Coolant circuit outlet temperature	°F
WH ₂ O	Water used	Lbs
WEIGHT	F/E unit weight	Lbs
<u>RADIATOR SUBROUTINE</u>		
TIN	Coolant inlet temperature	°R
TOUT	Coolant outlet temperature	°R
TOUTC	Calculated outlet temperature	°R
ARADC	Radiator area required	Ft ²
ARMAX	Maximum available radiator area	Ft ²
WTREQ	Radiator weight	Lbs

TABLE 4-2. OUTPUT DATA DESCRIPTION OFF DESIGN PERFORMANCE CASES

<u>Label</u>	<u>Description</u>	<u>Unit</u>
<u>COMPONENT POWERS-WATTS</u>		
The data in locations 191 - 220 are printed in order		
<u>COMPONENT FACTORS - UA, EFF, Etc.</u>		
The data in locations 221 to 250 are printed in order		
<u>COMPONENT FLOW RATES -CFH</u>		
CONDF	Condenser or HSC flow rate	ft ³ /hr
SENF	Sensible HX flow rate	ft ³ /hr
AVFANH	Flow rate of cabin loop cooled avionics bay fan	ft ³ /hr
AVFANR	Flow rate of radiator loop cooled avionics bay fan	ft ³ /hr
VENTF	Ventilation fan flow rate	ft ³ /hr
LiOH	LiOH flow rate	ft ³ /hr
<u>LiOH SUBROUTINE - CO₂ PARTIAL PRESSURES</u>		
PMAX	Cabin CO ₂ Pressure level at inputted removal efficiency	mm Hg
PMIN	Cabin CO ₂ pressure level with fresh cartridge	mm Hg
QS	Sensible heat generated by LiOH	BTU/hr
QL	Latent heat generated by LiOH	BTU/hr
<u>RADIATOR SUBROUTINE</u>		
TIN	Radiator inlet temperature	°R
TOUT	Radiator outlet temperature desired	°R

**TABLE 4-2. OUTPUT DATA DESCRIPTION OFF DESIGN PERFORMANCE CASES
(CONTINUED)**

<u>Label</u>	<u>Description</u>	<u>Unit</u>
TOUTC	Calculated outlet temperature	°R
ARADC	Calculated radiator area	ft ²
ARMAX	Maximum allowable radiator area	ft ²
WTREQ	Radiator weight	lbs
<u>FLASH EVAPORATOR PERFORMANCE</u>		
QREJ	Heat rejected	BTU/hr
TCIN	Coolant loop inlet temperature	°F
TCOUT	Coolant loop outlet temperature	°F
TOMAX	Maximum coolant loop outlet temperature	°F
TOMIN	Minimum coolant loop outlet temperature	°F
WH20	Water required to supplement radiator for TSUB hours	lbs
<u>CRYOGENIC HX PERFORMANCE</u>		
THOTCAL	Calculated coolant outlet temperature	°F
WHYD	Hydrogen flow rate	lbs/hr
THYDO	Hydrogen outlet temperature	°F
<u>CONDENSER PERFORMANCE</u>		
TCAB	Cabin temperature	°F
TAIRI	Heat exchanger air inlet temperature	°F
TAIRO	Heat exchanger air outlet temperature	°F
HXC FM	Gas flow rate through HX	CFM

TABLE 4-2. OUTPUT DATA DESCRIPTION OFF DESIGN PERFORMANCE CASES
(CONTINUED)

<u>Label</u>	<u>Description</u>	<u>Unit</u>
TDPCAB	Cabin dew point	°F
QSENS	Sensible heat transferred by condenser	BTU/hr
QSMET	Crew sensible metabolic heat load	BTU/hr
QLMET	Crew latent metabolic heat load	BTU/hr

SENS HX PERFORMANCE

QSENS	Heat transferred by HX	BTU/hr
VHX	Flow rate through HX	CFM
TXAI	Heat exchanger air inlet temperature	°F
TXAO	Heat exchanger air outlet temperature	°F
TCAB	Cabin temperature	°F
QMETS	Crew sensible metabolic heat load	BTU/hr

WATER COOLED AVIONICS BAY

QHX	Rate of heat removal	BTU/hr
WCPAIR	Mass flow rate of air	BTU/hr-°F
TBAY	Compartment temperature	°F
TXO	HX air outlet temperature	°F
THXAO		
THXCO	HX coolant outlet temperature	°F

RADIATOR COOLED AVIONICS BAY
(Same as Water Cooled Avionics Bay)

TABLE 4-2. OUTPUT DATA DESCRIPTION OFF DESIGN PERFORMANCE CASES
(CONTINUED)

<u>Label</u>	<u>Description</u>	<u>Unit</u>
<u>FUEL CELL HX</u>		
QFC	Heat rejected by fuel cells	BTU/hr
WFC	Fuel cell coolant mass flow rate	BTU/hr-°F
TF/CI	Temperature entering fuel cells	°F
TF/CO	Temperature leaving fuel cells	°F
<u>CABIN LOOP TEMPERATURES</u>		
1st	Interface HX outlet temperature	°F
2nd	Chiller outlet temperature	
3rd	Condensing HX outlet temperature	
4th	Sensible HX outlet temperature	
5th	Temperature into cold plates	
6th	Temperature out of cold plates	
7th ω	Temperature into interface HX	
<u>RADIATOR LOOP TEMPERATURES</u>		
1st	Calculated temperature (around loop) into Radiator	°F
2nd	Radiator inlet temperature	
3rd	Radiator outlet temperature	
4th	Flash evaporator outlet temperature	
5th	Sublimator outlet temperature	

TABLE 4-2. OUTPUT DATA DESCRIPTION OFF DESIGN PERFORMANCE CASES
(CONTINUED)

<u>Label</u>	<u>Description</u>	<u>Unit</u>
6th	Cryogenic HX coolant outlet temperature	
7th	Interface HX outlet temperature	
8th	Avionics bay HX outlet coolant temperature	
9th	Cold plate outlet temperature	
10th	Fuel Cell HX's outlet temperature	
<u>HEAT LOADS</u>		
QCOND	Total heat transferred by condenser	BTU/hr
QSENS	Heat transferred by sensible HX	BTU/hr
QCPUMP	Cabin loop pump heat load	BTU/hr
QINTX	Heat transferred by interface HX	BTU/hr
QRPUMP	Radiator loop pump heat generated	BTU/hr
QRAD	Heat rejected by radiator	BTU/hr
QEVAP	Heat rejected by water evaporation	BTU/hr
QRY	Heat rejected by cryogenic HX	BTU/hr
QLAT	Total latent heat load	BTU/hr

TABLE 4-3. OUTPUT DATA DESCRIPTION - ORBITAL TRANSIENT

<u>Label</u>	<u>Description</u>	<u>Unit</u>
QTOT	Average vehicle heat rejection around orbit	BTU/hr
WEVAVG	Average rate of evaporant usage	lbs/hr
NO. STEPS	Number of steps taken around orbit - 310 max.	-
ORBIT STEPS	Each step around the orbit - 2 rows of 15 steps per row	-
WEVAPORANT	Instantaneous rate of evaporant usage for each orbit step	lb/hr
TRAD IN	Radiator inlet temperature for each orbit step	°F
T SINK	Radiator adiabatic sink temperature for each orbit step	°R
TEVAP OUT	Coolant temperature leaving the evaporative sink for orbit step	°F
OFF TABLES	If other than "O", reading off curve - answers may not be good	

4.3 How to Vary the Program

One of the features of the computer program is the ease with which it can be changed to other schematic configurations. To demonstrate the ease of changing schematics, an example will be presented to optimize, calculate the off-design performance, and do an orbital transient to determine the amount of water evaporated for a schematic similar to Figure 4-1.

This schematic differs from the schematic already in the program in the following areas:

1. The cold plates are in front of the avionics bay heat exchanger rather than downstream of the avionics heat exchanger.
2. There are two sets of cold plates and avionics bays operating in parallel splitting the heat load equally between them rather than one of each.
3. The LiOH is in series with the condenser instead of in parallel.

To accomplish these changes, the following must be changed in the sizing program:

- A. The heat and latent load of the LiOH are not circulated into the cabin but flow directly to the condensing heat exchanger.
- B. The fan flow is only flow rate required by the heat exchanger for maximum cabin heat loads with no parallel LiOH path.
- C. The arrangement of the cold plates and avionics bays must be changed.
- D. The weights and powers must include the extra avionics compartment.

In making these changes, two approaches may be used:

4.3 (Continued)

- a. Write the changes for the specific schematic and leave out the items that are not there.
- b. Write the changes with the ability to add or delete items such as the sensible heat exchanger the avionics bays, etc.

The first approach is the quickest but program flexibility such as the ability to make continued changes is lost. For this example, the second approach will be described and this approach is recommended to the user for all changes of this nature.

To change the fan flow rate and the placement of the LiOH heat and latent load, cards 87 through 89:

87	QSH = 0
88	QLH = 0
89	QCH = 0

are replaced with the following cards:

QSH	=	QS9 - PW9 * 3.414
QLH	=	QL9
QCH	=	0
QS9	=	0
QL9	=	0
PW9	=	0

The cold plates, even though split into two parallel groups are treated as one group.

To change the location, the following cards are changed:

Replace card 276 with:

276 242 IF (QE1) 247, 247, 248

4.3 (Continued)

with:

242 T24 = T23 + QCP1/WCPC

IF (QE1) 247, 247, 248

Replace card 305

305 249 T25 = T24P = QCP1/WCPC

with:

249 CONTINUE

The parallel avionics bays are accomplished by splitting the heat load and coolant flow rate and adding in an extra set of fans and heat exchangers to account for the weight and doubling the fan power to account for the second set of fans. This is accomplished by the following changes:

Replace cards 292 and 293

292 253 Call EBAY (QE1, TE1, T24, WCPC, RHOE1, CPA, PP, DPE1,

WEHX1, WEF1, PW (17), V17

293 293 2, T24P, TAOE1, QET1, 16

with:

253 Call E6AY (QE1/2., TE1, T24, WCPC/2., RHOE1, CPA, PP,

DPE1, WEHX1, WEF1, PW (1 27), V17, T24P, TAOE1, QET1,

16)

Replace card 353

353 2 + PW (3)

with:

4.3 (Continued)

2 + PW (3) + PW (17)

After card 424

424 4 + WT21 + WT25

Add a card

5 + WEHX1 + WEF1

For the off design performance section of the program the same type of changes must be made. To account for the change in LiOH position the following cards must be changed:

Replace card 724

724 $V1 = V11 - V9$

with:

$V1 = V11$

$QCABS = QCHBS - QS9$

Replace card 744

744 642 Call CX2 (WHC, T22, QCABS, QCABL, TCAB, QSH, QLH,

V1, PW (11), 1, KY, T23

with:

642 Call CX2 (WHC, T22, QCABS, QLM, TCAB, QS9, QL9, V1,

PW (11), 1, KY, T23

To make the total heat load correct, after card 634

634 $Q5 = QCABS + QCABL + QE1 + QCP1 + QCHIL + 3.414^*$

PW (4) + PW (17)

4.3 (Continued)

Add a card:

$$2 + PW (17) * 3.414$$

After card 636

636 $PWT = PW (11) + PW (12) + PW (3) + PW (4) + PW (6) +$
 $PW (10) + PW (17) + PW (19)$

Insert the following card

$$2 + PW (17)$$

In order to change the location of the cold plates the following cards must be changed.

Replace card 823.

823 613 IF (V17) 614, 614, 6151

with:

613 $T2C = T24 + QCP1/WHC$

IF (V17) 614, 614, 6151

and replace cards 866 and 867

866 616 $T26 = T25 + QCP1/WHC$

867 $T27 = T26 + PW (4) * 3.414/WHC$

with:

616 $T26 = T2C$

$$T27 = T25 + PW (4) * 3.414/WHC$$

For the double avionics bays the following cards must be changed:

Replace card 850

4.3 (Continued)

$$850 \quad 615 \quad Q16 = QE1 + PW (17) * 3.414$$

with:

$$615 \quad Q16 = QE1 + PW (17) * 6.828$$

Replace cards 855 to 859

855 Call HX (Q16, WE1, WHC, T24, 16 TE10)

856 C EBAY TEMPERATURE

$$857 \quad TE1I = TE1O + QE1/WE1$$

858 C COOLANT TEMPERATURE

$$859 \quad T25 + T24 + Q16/WHC$$

with:

Call HX (Q16/2., WE1, WHC/2., T2C, 16, TE10)

C EBAY TEMPERATURE

$$TE1I = TE1O + QE1/2./WE1$$

C COOLANT OUTLET TEMPERATURE

$$T25 = T2C + Q16/WHC$$

For the radiator/evaporator orbital transient, only the heat load due to the second bay fan must be corrected. This can be done by inserting a card after card 933.

After card 933

$$933 \quad QPW = (PW (11) + PW (12) + PW (17) + PW (19) + \\ PW (4) + PW (6) + PW (10) + PW (3)) * 3.414$$

Insert:

$$2 + PW (17) * 3.414$$

4.3 (Continued)

These are the changes needed to change the program to the new schematic. Following the completion of these changes, the sizing program, the off-design performance program, and the orbital transient program could be run with the new schematic.

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**APPENDIX I
DEFINITION OF SYMBOLS**

SYMBOL DESCRIPTION - MAIN PROGRAM

<u>Symbol</u>	<u>Description</u>	<u>Units</u>
LA	Key to Subroutines IF = 2, Print; IF = 1, Do Not Print	-
NPER	Same as "Perf"	-
PP	Power Penalty	Lbs/Watt
J	Counter - Index	-
NR	Same as "RN" - Heat Rejection Sink Key	-
KR	Same as "RMAX" - Max. Radiator Loop Count	-
KI	Same as "HXIM" - Max. Interface HX Loop Count	-
KS	Not Used	-
KC	Not Used	-
WEXP	Expendable Weight Penalty Required to Supplement Radiator	Lbs
WT13	Not Used	-
M1	Same as "A1" - CO ₂ Removal Key	-
M2	Same as "A2" - Humidity Control Key	-
KEYC	Same as "FW5" - HX Arrangement Key	-
QSH	Sensible Heat Upstream of Condenser	BTU/Hr
QLH	Latent Heat Upstream of Condenser	BTU/Hr
I	Convergence Key - IF = 0, Subroutines Converged	-
RHOA	Cabin Gas Density	Lbs/Ft ³
PX	Saturation Pressure @ Cabin Temperature	PSIA
PMAX	Maximum Allowable Cabin Vapor Pressure	PSIA
DAY	Total Mission Length Including Emergency	DAYS
WTCH	Contaminant Removal Weight	Lbs
VCH	Contaminant Removal Flow Rate	Ft ³ /Hr
QCH	Contaminant Removal Heat Generated	BTU/Hr
WBC	CO ₂ Removal Bed Weight (Lbs LiOH Total)	Lbs
WT9	CO ₂ Removal Subsystem Weight	Lbs
PW9	CO ₂ Removal Subsystem Power	Watts
QS9	CO ₂ Removal Subsystem Sensible Heat Generated	BTU/Hr
QL9	CO ₂ Removal Subsystem Latent Heat Generated	BTU/Hr
WUC	CO ₂ Removal Subsystem Ullage Penalty	Lbs
ND	Flow Rate Iteration Count	-
NT	Same as "EY" - Max. Times Through Flow Rate Loop	-
NQ	Flow Rate Loop Index Counter	-
WCPC	Radiator Loop Thermal Mass Flow Rate	BTU/Hr-°F
NC	Radiator Temperature Loop Count	-
TB	Adiabatic Sink Temperature - Radiator	°F

SYMBOL DESCRIPTION - MAIN PROGRAM (CONT)

<u>Symbol</u>	<u>Description</u>	<u>Units</u>
KTS	Truncated TB	°F
TBI	KTS + 2	°F
TRO	Radiator Outlet Temperature	°F
N1	Radiator Loop Index Counter	-
T1	Radiator Loop Temperature Into Interface HX	°F
QSUB	Topping Water Evaporator Heat Load	BTU/Hr
KT	Interface HX Loop Max. Index Count	-
T21	Cabin Loop Interface HX Outlet Temperature	°F
NB	Interface HX Outlet Temperature Loop Count	-
N2	Interface HX Outlet Temperature Loop Index Counter	-
PDPI	Not Used	-
PVI	Control Value of Cabin Vapor Pressure	PSIA
TDPT	Cabin Dew Point	°F
WT1	Water Removal Subsystem Weight	Lbs
V1	Water Removal Subsystem Gas Flow Rate	CFH
WBD	Water Removal Bed Weight (HSC)	Lbs
WUD	Water Removal Ullage Penalty	Lbs
WT11	Water Removal Subsystem Fan Package Weight	Lbs
QSI	Sensible Heat Removed by Water Removal Subsystem	BTU/Hr
T22	Coolant Temperature Leaving H ₂ O Removal Subsystem	°F
QLT	Total Latent Heat Load	BTU/Hr
QST	Total Cabin Sensible Heat Load	BTU/Hr
TAOC	Condenser Air Outlet Temperature	°F
VX	Same as V1	Ft ³ /Hr
QS2	Cabin Heat Load to be Removed by Sens. HX	BTU/Hr
WT2	Sens. HX Package Weight	Lbs
V2	Sens. HX Flow Rate	Ft ³ /Hr
T23	Sens. HX Outlet Coolant Temperature	°F
TAOS	Sens. HX Gas Outlet Temperature	°F
T24	Same as "T23"	°F
WT3	Water Separator Weight	Lbs
WT10	Ventilation Fan Package Weight	Lbs
WTF	Fan Weight	Lbs
WTK	Check Valve Weight	Lbs
WT12	Sensible Fan Package Weight	Lbs
PW1	Fan Power Required For Cond. HX Fan Flow Rate	Watts

SYMBOL DESCRIPTION - MAIN PROGRAM (CONT)

<u>Symbol</u>	<u>Description</u>	<u>Units</u>
PDPO	Condenser Air Outlet Dew Point Pressure.	PSIA
XX	Not Used	-
VFC	M/S Fan Flow Rate - Not Used	-
WCF	Condenser Fan Weight	Lbs
WCV	Condenser Fan Check Valve Wt.	Lbs
VT	Same as "V2"	Ft ³ /Hr
WSF	Sensible Fan Wt.	Lbs
WSV	Sensible Fan Check Valve Wt.	Lbs
T24P	Coolant Loop Temperature Entering C/P	°F
WEHX1	Cabin Loop Cooled Avionic's HX Wt. (Total)	Lbs
WEF1	Cabin Loop Cooled Avionic's Fan Package Wt. (Total)	Lbs
TAOE1	Air Temperature Leaving First Avionic's HX	°F
QET1	First Avionic's HX Load	BTU/Hr
T24PP	Coolant Temperature Leaving First Avionic's HX	°F
TEB1	Compartment Temperature 1st Avionic's Bay	°F
TEB2	Compartment Temperature 2nd Avionic's Bay	°F
TAOB2	Air Temperature Leaving 2nd Avionic's HX	°F
QEBT2	2nd Avionic's HX Load	BTU/Hr
RHOE1	Gas Density in Cabin Loop Cooled Avionic's Compt.	Lbs/Ft ³
QEB1	Heat Load to be Removed from 1st Avionic's Bay	BTU/Hr
T25	Cold Plate Outlet Coolant Temperature	°F
WT4	Pump Package Weight	Lbs
T26	Pump Outlet Temperature-Interface HX Inlet Temperature	°F
T2	Interface HX Outlet Temperature Radiator Loop	°F
WT5	Interface HX Wt.	Lbs
DTLM	HX Log-Mean Temperature Difference	°F
T2P	Temperature Leaving Radiator Loop Cooled Avionic's HX	°F
WEHX2	Radiator Loop Cooled Avionic's HX Wt.	Lbs
WEF2	Radiator Loop Cooled Avionic's Fan Package Wt.	Lbs
TAOE2	Radiator Loop Cooled Avionic's HX Air Outlet Temperature	°F
QET2	Radiator Loop Cooled Avionic's HX Heat Load	BTU/Hr
RHOE2	Gas Density in Radiator Loop Cooled Avionic's Compt.	Lbs/Ft ³
T3	Radiator Loop C/P Outlet Temperature	°F
TPW	Total ECS Power (As calculated by program)	Watts
QFCT	Total F/C Heat Load	BTU/Hr
T4	F/C Coolant Leaving Temperature	°F

SYMBOL DESCRIPTION - MAIN PROGRAM (CONT)

<u>Symbol</u>	<u>Description</u>	<u>Units</u>
WT6	Radiator Loop Pump Package Wt.	Lbs.
TRI	Radiator Inlet Temperature	°F
TI	Radiator Inlet Temperature	°R
TO	Radiator Outlet Temperature	°R
QF	Total ECS Heat Rejection	BTU/Hr
T1A	Interface HX Inlet Temperature - Calculated	°F
WT25	Flash Evaporator Subsystem Weight	Lbs
WSUB	Weight of H ₂ O Stored for Periods When No Radiator	Lbs
WT8	Sublimator Subsystem Wt.	Lbs
WHYD	Weight of H ₂ Stored for Periods When No Radiator	Lbs
WT22	Hydrogen HX Package Wt.	Lbs
EFF	Heat Exchanger Temperature Effectiveness	-
WT21	GSE HX Weight	Lbs
WT20	F/C HX Weight	Lbs
WT7	Radiator Panel Weight	Lbs.
ARAD	Required Radiator Area	Ft ²
TORAD	Calculated Radiator Leaving Temperature	°F
QEXP	Heat Load That Must Supplement Radiator	BTU/Hr
WUT	Total Ullage Penalty	Lbs
TWT	Total Fixed Weight	Lbs
TEWT	Total Equivalent Weight	Lbs
TMIN	Minimum Total Equivalent Wt. (Interface HX Loop)	Lbs
NJ	Index Counter	-
JJ	Index Counter	-
TMIN1	Minimum Total Equivalent Wt. (Radiator Temperature Loop)	Lbs
NK	Index Counter	-
JK	Index Counter	-
WQ	Float Number of Times Through Flow Rate Loop	-
J1	Index Counter	-
J2	Index Counter	-
Q1	Condenser Total Heat Load	BTU/Hr
Q2	Sensible HX Total Heat Load	BTU/Hr
Q5	Interface HX Total Heat Load	BTU/Hr
Q6	Total F/C Heat Load (Same "QFCT")	BTU/Hr
Q7	Heat Rejected by Radiator	BTU/Hr
Q8	Expendable Heat to Supplement Radiator	BTU/Hr

SYMBOL DESCRIPTION - MAIN PROGRAM (CONT)

<u>Symbol</u>	<u>Description</u>	<u>Units</u>
<u>TABLES</u>		
TRA(N)	Optimum Cond. Air Outlet Temperature for each Coolant Flow Rate	°F
TRB(N)	Optimum Cond. Air Outlet Temperature for each Radiator Outlet Temp.	°F
TEO(N)	Optimum Cond. Air Outlet Temperature for each Interface HX Outlet Temp.	°F
WEV(N)	Rate of Expendable Usage for each Orbit Step	Lbs/Hr
L(N)	Off Tables for each Orbit Step	-
TQ(N)	Total Equivalent Wt. for each T-Interface HX Out	Lbs
TXO(N)	Interface HX Outlet Temperature	°F
PT(N)	Total Power for each TXO	Watts
WTT(N)	Total Weight for each TXO	Lbs
T41(N)	F/C Outlet Temperature for each TXO	°F
TQ1(N)	Optimum TEQWT for each TRO	Lbs
TRDO(N)	Radiator Outlet Temperature	°F
TXO1(N)	Optimum TXO for each TRDO	°F
PT1(N)	Optimum PT for each TRDO	Watts
WTT1(N)	Optimum WTT for each TRDO	Lbs
T42(N)	Optimum T4 for each TRDO	°F
WC1(N)	Table of Coolant Flow Rates	Lbs/Hr
TQ2(N)	Optimum TEQWT for each Coolant Flow Rate	Lbs
TRDO1(N)	Optimum Radiator Outlet Temperature for each WC	°F
TXO2(N)	Optimum TXO for each WC	°F
PT2(N)	Total Power at Optimum TEQWT for each WC	Watts
WTT2(N)	Total Weight at Optimum TEQWT for each WC	Lbs
T43(N)	F/C Outlet Temperature @ Optimum TEQWT for each WC	°F
<u>SUBROUTINE LiOH</u>		
WL	Weight of LiOH Required for Mission	Lbs
DAY	Total Mission Length	DAYS
TN	Number of LiOH Canisters	-
IN	Truncate "TN"	-
WN	Float "IN"	-
PW	Fan Power for LiOH	Watts
DPF	Fan Pressure Rise	In-H ₂ O
QS	LiOH Sensible Heat	BTU/Hr
QL	LiOH Latent Heat	BTU/Hr
V	Volume Flow Rate Required/Available	Ft ³ /Hr

SYMBOL DESCRIPTION - MAIN PROGRAM (CONT)

<u>Symbol</u>	<u>Description</u>	<u>Units</u>
QCRY	Excess Expendable H ₂ O Used	BTU/Hr
QLAT	Latent Heat Rejected	BTU/Hr
VC	LiOH Flow Rate (V9/60)	CFM
VV	Ventilation Flow Rate (V10/60)	CFM
VE1	Same as "V17"	Ft ³ /Hr
VE2	Same as "V19"	Ft ³ /Hr
WHC	Cabin Loop Thermal Mass Flow Rate	BTU/Hr-°F
NA	Cabin Temperature Loop Index Register	-
QCABL	Total Cabin Latent Load	BTU/Hr
QCABS	Total Cabin Sensible Load	BTU/Hr
PWT	Total ECS Power	Watts
QFT	Total F/C Heat Load	BTU/Hr
QTOT	Total Heat to be Rejected	BTU/Hr
T6	Radiator Inlet Temperature	°R
N	Radiator Loop (Performance) Index Register	-
WR	Radiator Wt. (Not Used)	Lbs
WE	Not Used	-
T7	Calculated Radiator Outlet Temperature	°R-°F
T8	Sublimator Outlet Temperature (Flash Evap.)	°F
T9	GSE Outlet Temperature	°F
QR	Calculated Total Heat Rejection	BTU/Hr
Q22	Cryogenic HX Heat Rejected	BTU/Hr
Q25	Flash Evap. Heat Rejected	BTU/Hr
RHO	Dummy Variable	-
QCDS	Sensible Heat Removed by Condensing HX	BTU/Hr
KY	Key to Tell Cond. if there is a Sens. HX 0 - NO Sensible HX; 1 - Followed by Sensible HX	-
WHOT	Sensible HX Thermal Mass Flow Rate	BTU/Hr-°F
WMX	Maximum "WHOT"	BTU/Hr-°F
TAI	HX Air Inlet Temperature	°F
TAOR	HX Air Outlet Temperature	°F
TAO	Calculated HX Air Outlet Temperature	°F
QSN	New Sensible Metabolic Heat Load	BTU/Hr
KA	Off Tables If > 0 in QMET Subroutine	-
VHX	Volumetric Flow Rate Through HX	Ft ³ /Hr
QEE1	Heat to be Removed from First Cabin Loop Avionic's HX	BTU/Hr

SYMBOL DESCRIPTION - MAIN PROGRAM (CONT)

<u>Symbol</u>	<u>Description</u>	<u>Units</u>
QEE2	Heat to be Removed from Second Cabin Loop Avionic's HX	BTU/Hr
WE1	Avionics (Cabin Loop) Thermal Mass Flow Rate	BTU/Hr-°F
TEE1	1st Avionic's HX Air Inlet Temperature	°F
T25A	Coolant Loop Temperature Into Second Avionic's HX	°F
TAE2	Air Temperature Leaving 2nd Avionic's HX	°F
TEE2	2nd Avionic's HX Air Inlet Temperature	°F
TEIC	Same as "TE1"	°F
Q16	Single Avionic's HX Heat Load	BTU/Hr
TE10	Single Avionic's HX Air Outlet Temperature	°F
TE11	Single Avionic's HX Air Inlet Temperature	°F
T27	Pump Outlet Temperature (Performance)	°F
Q18	Radiator Loop Avionic's HX Load	BTU/Hr
WHX	Radiator Loop Avionic's HX Thermal Mass Flow Rate	BTU/Hr-°F
TE20	Radiator Loop Avionic's HX Air Outlet Temperature	°F
TE2B	Radiator Loop Avionic's HX Air Inlet Temperature	°F
T5	F/C Coolant Loop Outlet Temperature	°F
T6C	Calculated Radiator Inlet Temperature	°F
Q4	Cabin Loop Pump Heat Load	BTU/Hr
QLTOT	Total Latent Load	BTU/Hr
DTHEA	Degrees of Orbit for Each Step	°
TAUS	Time for Each Orbit Step	Hr
A	Orbital Position	°
WA	Average Expendable Use Rate	Lbs/Hr
NS	Orbital Transient Loop No. of Steps	-
QPW	Total ECS Power Heat Load	BTU/Hr
DT	Radiator Loop Delta T	°F
T10	Actual Interface HX Coolant Inlet Temperature	°F
FK	Radiator Ambient Heat Load	BTU/Hr-Ft ²
NN	Evaporator Loop Temperature Index Register	-
AR	Dummy Variable	-
TOR	Radiator Outlet Temperature	°R
TR	Same as "TOR"	°F
QE	Evaporator Heat Load	BTU/Hr
WT	Dummy Variable	-
TR2	Sublimator Outlet Temperature	°F

SYMBOL DESCRIPTION - MAIN PROGRAM (CONT)

<u>Symbol</u>	<u>Description</u>	<u>Units</u>
WTM	Manual Valve Weight	Lbs
WT	Total Subsystem Weight	Lbs
J	Component Number	-
PMIN	Minimum CO ₂ Partial Pressure (R = .95)	mm Hg
PMAX	CO ₂ Partial Pressure Before Cartridge is Replaced (R = CFT (9))	mm Hg
<u>SUBROUTINE CHX</u>		
PMAX	Max. Allowable Cabin H ₂ O Vapor Pressure	PSIA
TMAX	Max. Allowable Cabin Dew Point Temperature	°R/°F
WH2O	Rate of H ₂ O Removal from Cabin Atmosphere	Lbs/Hr
QL	Cabin Latent Load	BTU/Hr
QL3	Total HX Latent Load	BTU/Hr
QL2	Latent Heat Downstream of Cabin	BTU/Hr
K	IF = 0; No Sensible HX; I = 0; Sensible HX	-
L	Set to 1 If No Sensible HX, Set to 2 If Sensible HX	-
QT	Cabin Sensible and Latent Load	BTU/Hr
QS	Cabin Sensible Load	BTU/Hr
TCO	Coolant HX Outlet Temperature	°F
QC	Calculated HX Total Heat Load	BTU/Hr
WCPC	Coolant Thermal Mass Flow Rate	BTU/Hr-°F
TCI	Coolant Inlet Temperature	°F
TAO	HX Gas Outlet Temperature	°F
NT	Maximum Number of Times Through Optimization Loop	-
I	Set = 0; If Subroutine Converged	-
N	Index Register	-
V	Gas Volume Flow Rate	Ft ³ /Hr
TC	Cabin Temperature	°F
RHO	Gas Density	Lbs/Ft ³
CPA	Gas Specific Heat	BTU/Lb-°F
PXO	H ₂ O Vapor Pressure of Gas Leaving HX	PSIA
WVO	Water Flow Rate in Gas Leaving HX	Lbs/Hr
WWI	Water Flow Rate in Gas Entering HX	Lbs/Hr
TCCO	Calculated Coolant Outlet Temperature	°F
QCDDT	Minimum Total Heat Load for Humidity Control	BTU/Hr
VMIN	Minimum Volume Flow Rate for Humidity Control	Ft ³ /Hr
PPF	Fan Pressure Rise	In-H ₂ O

SYMBOL DESCRIPTION - MAIN PROGRAM (CONT)

<u>Symbol</u>	<u>Description</u>	<u>Units</u>
J	Component Number	-
PXI	Inlet Water Vapor Pressure	PSIA
TDP	Cabin Dew Point	°F
TWTS	Total Equivalent Weight-Stored	Lbs
WT	Total Weight	Lbs
PW	Total Power	Watts
WTF	Fan Weight	Lbs
TAI	HX Gas Inlet Temperature	°F
QS2	Heat Load Downstream of Cabin	BTU/Hr
QCS	Sensible Heat Removed by Condenser	BTU/Hr
PDPI	Dew Point Pressure Where Condensing Starts	PSIA
TDPI	Dew Point Temperature Where Condensing Starts	°F
TY	Coolant Temperature Where Condensing Starts	°F
QW	Heat in Wet Section of Condenser	BTU/Hr
QD	Heat in Dry Section of Condenser	BTU/Hr
TAOD	Gas Temperature Where Condensing Starts	°F
DTLM	Log-Mean-Temperature Difference	
UAD	Dry Section UA	BTU/Hr-°F
UAW	Wet Section UA	BTU/Hr-°F
WTM	Not Used	-
WTK	Check Valve Weight	Lbs
WTV	Temperature Control Bypass Valve Weight	Lbs
TWT	Total Equivalent Weight	Lbs
WTS	Total Weight Stored	Lbs
PWS	Total Power Stored	Watts
UAS	HX UA Stored	BTU/Hr-°F
TDPS	Cabin Dew Point Stored	°F
VS	Volume Flow Rate Stored	Ft ³ /Hr
PXOS	HX Outlet Dew Point Pressure	PSIA
QSS	Sensible Heat Removed - Stored	BTU/Hr
WHX	Heat Exchanger Weight	Lbs

SUBROUTINE SHX

<u>Symbol</u>	<u>Description</u>	<u>Units</u>
DTF	Fan Temp. Rise	°F
DP	Fan Pressure Rise	In-H ₂ O
RHO	Cabin Gas Density	Lbs/Ft ³
CPA	Cabin Gas Specific Heat	BTU/Lb-°F
J	Component Number	-
TAI	HX Gas Inlet Temp	°F
TCAB	Cabin Gas Temp	°F
DTM	Maximum Gas To Coolant Temp Difference	°F
TCI	Coolant Inlet Temp	°F
TAO	Gas Outlet Temp	°F
N	Index Register	-
V	Gas Volumetric Flow Rate	Ft ³ /Hr
QS	Sensible Heat Load To Be Removed From Cabin	BTU/Hr
PW	Fan Power	Watts
TCO	Coolant Outlet Temp	°F
WCPC	Coolant Thermal Mass Flow Rate	BTU/Hr-°F
DTLM	Log-Mean-Temperature Difference	°F
UA	Thermal Conductance x Area	BTU/Hr-°F
WTF	Fan Weight	Lbs
WTM	Not Used	-
WTK	Check Valve Weight	Lbs.
WTV	Temp Control Valve Weight	Lbs.
WT	Total Weight	Lbs.
TWT	Total Equivalent Weight	Lbs.
PP	Power Penalty	Lbs./Watts
TWTS	Total Equivalent Weight Stored	Lbs.
WTS	Total Weight Stored	Lbs.
PWS	Total Power Stored	Watts
UAS	Thermal Conductance x Area Stored	BTU/Hr-°F
TCOS	Coolant Outlet Temp Stored	°F
VS	Volumetric Flow Rate Stored	Ft ³ /Hr
WTX	Heat Exchanger Weight	Lbs.

SYMBOL DESCRIPTION - EBAY

DTF	Fan Temp Rise	°F
DP	Fan Pressure Rise	In-H ₂ O
RHO	Gas Density	Lbs/Ft ³
CPA	Gas Specific Heat	BTU/Lb-°F

SYMBOL DESCRIPTION - EBAY (CONT)

<u>Symbol</u>	<u>Description</u>	<u>Units</u>
LF	Component Number	-
TAI	Gas Inlet Temp	°F
TE	Compartment Temp	°F
TAO	HX Gas Outlet Temp	°F
TCI	Coolant Inlet Temp	°F
N	Index Resister	-
V	Volumetric Flow Rate	Ft ³ /Min
QE	Compartment Heat Load (Excluding Fan)	BTU/Hr
PW	Fan Power	Watts
QT	HX Total Load	BTU/Hr
TCO	Coolant Outlet Temp	°F
WCPC	Flow Stream Capacity Rate	BTU/Hr-°F
DTLM	Log-Mean-Temperature-Difference	°F
UA	Thermal Conductance x Area	BTU/Hr-°F
WTF	Fan Weight	Lbs.
WTK	Check Valve Weight	Lbs.
WTHX	Heat Exchanger Weight (Package)	Lbs.
WTFAN	Fan Package Weight	Lbs.
TWT	Total Equivalent Weight	Lbs.
PP	Power Penalty	Lbs/Watt
TWTS	Total Equivalent Weight Stored	Lbs.
WTHXS	Heat Exchanger Weight Stored (Package)	Lbs.
UAS	Thermal Conductance x Area Stored	BTU/Hr-°F
WTFS	Fan Package Weight Stored	Lbs.
PWS	Fan Power Stored	Watts
TCOS	Coolant Outlet Temp Stored	°F
QTS	HX Total Load Stored	BTU/Hr
VS	Volumetric Flow Rate Stored	Ft ³ /Min
WTX	Heat Exchanger Weight	Lbs.
<u>SUBROUTINE HSC</u>		
VB	Gas Flow Rate Per Lb of Bed	CFM/LbHSC
WH2O	Water Removed Per Cycle	Lbs/Cycle
QLAT	Latent Heat Removal Rate From Cabin	BTU/Hr
WBC	Bed Size Required For CO ₂ Control	Lbs.
WCO2	CO ₂ Generation Rate	Lbs./DAY
NC	Loop Counter	-

SUBROUTINE HSC (CONT)

<u>Symbol</u>	<u>Description</u>	<u>Units</u>
N	Index Register - Bed Sizing Loop H ₂ O	-
PVI	Cabin Water Vapor Pressure Level	PSIA
BL	Bed Water Loading	Lbs/Lb
K	Off Tables IF = O	-
V	Volumetric Flow Rate Required/Available	Ft ³ /Hr
WTV	Vacuum Valve Weight	Lbs
DP	Fan Pressure Rise	In-H ₂ O
PD	System Pressure Loss - Excluding Bed	In-H ₂ O
WTF	Fan Weight	Lbs
WTK	Check Valve Weight	Lbs
WVC	Humidity Control Valve Weight	Lbs
RHO	Gas Density	Lbs/Ft ³
DAY	Mission Length	DAYS
WTX	Canister Weight (Excluding HSC)	Lbs
L	Component Weight	Lbs
WT	System Total Weight	Lbs
WF	Fan Weight Increase	Lbs
PW	Fan Power	Watts
WB	Bed Weight	Lbs
WU	Ullage Penalty Weight	Lbs
VBM	Maximum Volumetric Flow Rate	Ft ³ /Hr
WH2OC	Calculated Amount of H ₂ O Removed Per Cycle	Lbs/Cycle
WC	Same As "WBC"	Lbs/Cycle
VC	Volumetric Flow Rate	Ft ³ /Hr
WCR	Required CO ₂ Bed Loading	Lbs/Lb
PCO ₂	First Guess of CO ₂ Cabin Partial Pressure Level	MMHG
J	CO ₂ Performance Index Register	-
BLS	Calculated CO ₂ Bed Loading	Lbs/Lb
KC	Off Tables IF φ O	-
TDP	Cabin Dew Point	°F
VCH	Dummy - Not Used	-
PWS(N)	Same As "PW" - Stored	Watts
WTS(N)	Same As "WT" - Stored	Lbs
WBS(N)	Same As "WB" - Stored	Lbs
WUS(N)	Same As "WU" - Stored	Lbs
WFS(N)	Same As "WF" - Stored	Lbs
VS(N)	Same As "V" - Stored	Ft ³ /Hr

SUBROUTINE HSC (CONT)

<u>Symbol</u>	<u>Description</u>	<u>Units</u>
WTSYS(N)	System Total Equivalent Weight	Lbs

SUBROUTINE (CONT)

V	Volumetric Flow Rate	Ft ³ /Hr
WTB	Bed Weight (Chemical)	Lbs
DAY	Mission Length	DAYS
WTV	Check Valve Weight	Lbs
WT	Total Weight	Lbs
J	Component Number	-
QSC	Heat Generated	BTU/Hr
DP	Fan Pressure Rise	In-H ₂ O

SUBROUTINE EBAY2

DTF	Fan Temp Rise	°F
DP	Fan Pressure Rise	In-H ₂ O
RHO	Gas Density	Lbs/Ft ³
CPA	Gas Specific Heat	BTU/Lb-°F
LF	Component Number	-
TAI2	Gas Inlet Temp - 2nd HX In Series	°F
TE	Compartment Temp - Design	°F
TB2	Compartment Temp - 2nd Bay	°F
TCI2	Coolant Inlet Temp - 2nd HX	°F
TCI	Coolant Inlet Temp - 1st HX	°F
QB1	Compartment Heat Load - 1st Bay	BTU/Hr
TAO2	Gas Outlet Temp - 2nd HX	°F
N	Index Register	-
V	Volumetric Flow Rate	Ft ³ /Hr
QB2	Compartment Heat Load - 2nd Bay	BTU/Hr
PW	Fan Power	Watts
QT2	2nd HX Total Heat Load	BTU/Hr
QTI	1st HX Total Heat Load	BTU/Hr
TCO1	Same As "TCI2"	°F
TCO2	Coolant Temp Leaving 2nd HX	°F
DTLM2	Log-Mean-Temp-Difference: 2nd HX	°F
UA2	Thermal Conductance x Area: 2nd HX	BTU/Hr-°F
WTF	Fan Weight	Lbs
WTK	Check Valve Weight	Lbs

SUBROUTINE EBAY2 (CONT)

<u>Symbol</u>	<u>Description</u>	<u>Units</u>
WTHX	HX Package Weight	Lbs
WTFAN	Fan Package Weight	Lbs
TWT	Total Equivalent Weight	Lbs
PP	Power Penalty	Lbs/Watt
TWTS	Total Equivalent Weight Stored	Lbs
WTHXS	HX Package Weight Stored	Lbs
WTFS	Fan Package Weight Stored	Lbs
PWS	Power - Stored	Watts
TCO1S	Coolant Temp Leaving 1st HX Stored	°F
TCO2S	Coolant Temp Leaving 2nd HX Stored	°F
UA2S	Thermal Conductance x Area Stored	BTU/Hr-°F
QT1S	Total Heat Removed 1st HX Stored	BTU/Hr
QT2S	Total Heat Removed 2nd HX Stored	BTU/Hr
VS	Volumetric Flow Rate - Stored	Ft ³ /Min
TAO1	Gas Outlet Temp - 1st HX	°F
EFF	Temp Effectiveness	-
TBI	1st Compartment Temp	°F
M	Index Register	-
TAI1	1st HX Gas Inlet Temp	°F
DTLM1	Log-Mean-Temp-Difference 1st HX	°F
UA1	Thermal Conductance x Area 1st HX	BTU/Hr-°F
UA1S	Thermal Conductance x Area 1st HX Stored	BTU/Hr-°F

SUBROUTINE FEVAP

TCO	Coolant Outlet Temp	°F
TCI	Coolant Inlet Temp	°F
Q	Heat Load Desired	BTU/Hr
WCP	Flow Stream Capacity - Rate	BTU/Hr-°F
QR	Heat Load Rejected	BTU/Hr
L	Component Number	-
WT	Subsystem Weight	Lbs
WH2O	Water Usage Rate	Lbs/Hr
TOMIN	Minimum Coolant Outlet Temp	°F
TOMAX	Maximum Coolant Outlet Temp	°F

SUBROUTINE FANWT

<u>Symbol</u>	<u>Description</u>	<u>Units</u>
CFM	Volumetric Flow Rate	FT ³ /Min
CFH	Volumetric Flow Rate	Ft ³ /Min
A	Specific Speed	-
DP	Fan Pressure Rise	In-H ₂ O
WT	Fan Weight	Lbs

SUBROUTINE CRY

THO	Coolant Outlet Temp-Assumed	°F
TIN	Coolant Inlet Temp	°F
Q	Heat Rejected	BTU/Hr
WH	Flow Stream Capacity-Rate	BTU/Hr-°F
TH2O	Hydrogen Outlet Temp	°F
N	Index Register	-
WC	Hydrogen Flow Stream Capacity-Rate	BTU/Hr-°F
NC	Component Number	-
TOC	Calculated Coolant Outlet Temp	°F
WH2	Hydrogen Flow Rate	Lbs/Hr

SUBROUTINE HX

R	Mass Flow Ratio (Cold/Hot)	-
WC	Cold Side Flow Stream Capacity-Rate	BTU/Hr-°F
WH	Hot Side Flow Stream Capacity-Rate	BTU/Hr-°F
THO	Hot Side Outlet Temp	BTU/Hr-°F
TCI	Cold Side Inlet Temp	°F
Q	Heat Rate To Be Transferred	BTU/Hr
NCOMP	Component Number	-
EFF	Temperature Effectiveness (Hot Side)	-

SUBROUTINE WTV2

N	Type of Valve 1- Manual Valve 2- Check Valve 3- Elec. Solenoid Valve 4- Gas Disconnect	-
WT	Component Weight	Lbs

SUBROUTINE WTV2 (CONT)

<u>Symbol</u>	<u>Description</u>	<u>Units</u>
V	Gas Flow Rate	Ft ³ /Hr

SUBROUTINE RAD

TY	Calculated Coolant Outlet Temp	°R
T2	Desired Coolant Outlet Temp	°R
B	Number (2.0 x 10 ⁻¹⁰)	-
TI	Wall Temp At Inlet	°R
T1	Inlet Coolant Temp	°R
ZETA	Function of TI	BTU/Hr
ALPHA	$\delta \epsilon T_s^3$	BTU/Hr
TO	Wall Temp At Outlet	BTU/Hr
BETA	$B * T_s^3$	°R
I	Index Register	-
QA	Heat Rejected Per Unit Area	BTU/Hr-Ft ³
AR	Required Radiator Area	Ft ²
WCP	Flow Stream Capacity-Rate	BTU/Hr °F
WR	Radiator Wt.	Lbs
J	Component Number	-
WE	Dummy - Not Used	-

SUBROUTINE CX2

RHO	Gas Density	Lbs/Ft ³
TC	Cabin Temp	°F
WAM	Max Gas Flow Stream Capacity-Rate-HX	BTU/Hr-°F
V	Volumetric Flow Rate - HX	Ft ³ /Hr
WF	Gas Flow Stream Capacity-Rate Through Fan	BTU/Hr-°F
V11	Fan Volumetric Flow Rate	Ft ³ /Hr
WH	Assumed HX Gas Flow Stream Capacity-Rate	BTU/Hr-°F
WH2C	Water Condensing Rate	Lbs/Hr
QL	Cabin Latent Load	BTU/Hr
QL2	Latent Load Downstream of Cabin	BTU/Hr
TAMIN	Minimum Gas Outlet Temp	°F
TCI	Coolant Inlet Temp	°F
QF	Fan Heat Load	BTU/Hr
P	Fan Power	Watts

SUBROUTINE CX2 (CONT)

<u>Symbols</u>	<u>Description</u>	<u>Units</u>
QSMAX	Maximum Sensible Heat Load	BTU/Hr
QS	Cabin Sensible Heat Load (Includes Fan)	BTU/Hr
QS2	Sensible Heat Downstream of Cabin	BTU/Hr
K	IF = 0, Single HX, 70 - Has Sensible HX Also	-
TAO	Gas Outlet Temp-Assumed	°F
TAI	Gas Inlet Temp-Assumed	°F
QSX	HX Sensible Load	BTU/Hr
TCN	New Cabin Temp	°F
QSN	New Crew Sensible Load	BTU/Hr
KL	Off Tables IF = 0	-
NP	Index Register	-
PXO	H ₂ O Vapor Pressure At HX Exit	PSIA
WWO	H ₂ O Vapor Leaving HX In Gas Stream	Lbs/Hr
PXI	Vapor Pressure of H ₂ O At HX Inlet	PSIA
TDP	Inlet Dew Point	°F
TY	Coolant Temp Where Condensing Starts	°F
QT	HX Total Load	BTU/Hr
TCO	Coolant Outlet Temp	°F
WC	Coolant Flowstream Capacity Rate	BTU/Hr-°F
QW	Heat Removed In Wet Section	BTU/Hr
QD	Heat Removed In Dry Section	BTU/Hr
TAOD	Gas Temp Where Condensing Starts	°F
DT	Log-Mean-Temp-Difference	°F
UAD	Dry Section Thermal Conductance x Area	BTU/Hr-°F
UAW	Wet Section Thermal Conductance x Area	BTU/Hr-°F
UAR	Required Thermal Conductance x Area	BTU/Hr-°F
NL	Component Number	-
I	IF = 0, Converged	-
WHX	Volumetric Flow Rate Through HX	FT ³ /Min
PXC	Cabin H ₂ O Vapor Pressure	PSIA
TDPC	Cabin Dew Point Temp.	°F

SUBROUTINE QMET

T2	New Cabin Temp	°F
Q2	New Sensible Metabolic Load	BTU/Hr
K	IF ≠ 0, Off Tables	-

SUBROUTINE QMET (CONT)

<u>Symbols</u>	<u>Description</u>	<u>Units</u>
T1	Original Cabin Temp	°F
QO	Original Metabolic Heat Rate	BTU/Hr/Min
K1	Same As "K"	-
QN	New Metabolic Heat Rate	BTU/Hr/Min
K2	Same As "K"	-
Q1	Original Cabin Heat Load-Metabolic	BTU/Hr

SENSIBLE HX SUBROUTINE - SHX

INPUTS

QS2	CABIN SENSIBLE HEAT TO BE REMOVED	BTU/HR
TCAB	CABIN TEMPERATURE	°F
T22	COOLANT INLET TEMP	°F
WCPC	COOLANT MASS FLOW	BTU/LB-°F
RHOA	CABIN GAS DENSITY	LBS/FT ³
CPA	CABIN GAS SPECIFIC HEAT	BTU/LB -°F
PP	POWER PENALTY	LBS/WATT
DP2	FAN PRESSURE RISE	IN-H ₂ O
N	COMPONENT NUMBER	—
FWT(N)	HX WEIGHT FACTOR	LBS/UA
FXW(N)	SYSTEM FIXED WEIGHT	LBS
SWT(N)	PACKAGING WEIGHT FACTOR	LBS/LB
CFT(N+10)	FAN EFFICIENCY	—

OUTPUTS

WT2	HX & FIXED WEIGHT	LBS
PW(12)	FAN POWER FOR SENS. HX FLOW	WATTS
V12	HX FLOW RATE	CFH
T23	COOLANT OUTLET TEMP	°F
TAOS	HX GAS OUTLET TEMP	°F
CFT(N)	HX UA	BTU/HR-°F
WTHX	HX WEIGHT	LBS
WVALVE	AIR BYPASS VALVE WEIGHT	LBS

SUBROUTINE EBAY 2 (QB1, QB2, TE, TCI, WCPC, RHO, CPA, PP, DP,
WTHX, WTFAN, PW, V, TCO1, TCO2, TB1, TB2,
TAO1, TAO2, QT1, QT2, LF)

INPUT

QB1	- HEAT LOAD IN FIRST SERIES BAY	BTU/HR
QB2	- HEAT LOAD IN SECOND SERIES BAY	BTU/HR
TE	- MAXIMUM COMPACTMENT TEMP	°F
TCI	- COOLANT TEMP INTO FIRST BAY	°F
WCPC	- COOLANT MASS FLOW RATE	BTU/HR-°F
RHO	- COMPARTMENT DENSITY AT TE	LBS/FT ³
CPA	- GAS SPECIFIC HEAT	BTU/LB-°F
PP	- POWER PENALTY	LBS/WATT
DP	- FAN PRESSURE RISE	IN - H ₂ O
LF	- HX COMPONENT NUMBER	-
	FAN COMPONENT NUMBER=LF+1	-
FWT(LF)	- HEAT EXCHANGER WEIGHT FACTOR	LBS/UA
FWT(LF+1)	- NUMBER OF FANS & CHECK VALVES	-
FXW(LF)	- FIXED WEIGHT ADDED TO HX	LBS
FXW(LF+1)	- FIXED WEIGHT ADDED TO FANS	LBS
SWT(LF)	- STRUCTURAL WEIGHT FACTOR-HX	LBS/LB
SWT(LF+1)	- STRUCTURAL WEIGHT FACTOR - FANS	LBS/LB
CFT(LF+1)	- OVERALL FAN EFFICIENCY	-

OUTPUT

WTHX	- TOTAL HX WT-BOTH BAYS	LBS
WTFAN	- TOTAL FAN WT-BOTH BAYS	LBS
PW	- TOTAL POWER - BOTH BAYS	WATTS
V	- FAN VOLUME FLOW RATE	CFM
TCO1	- COOLANT OUTLET TEMP-1ST BAY	°F
TCO2	- COOLANT OUTLET TEMP-2ND BAY	°F
TB1	- 1ST COMPARTMENT TEMP	°F
TB2	- 2ND COMPARTMENT TEMP	°F
TAO1	- AIR OUTLET TEMP 1ST JX	°F
TAO2	- AIR OUTLET TEMP 2ND HX	°F
QT1	- TOTAL HEAT REMOVED BY HX 1ST BAY	BTU/HR
QT2	- TOTAL HEAT REMOVED BY HX 2ND BAY	BTU/HR

SUBROUTINE RAD (T1, T2, WCP, WR, AR, WE, TY, J)

INPUTS

T1	- RADIATOR INLET TEMP.	°R
T2	- DESIRED RADIATOR OUTLET TEMP	°R
WCP	- COOLANT FLOW RATE	BTU/HR-°F
J	- COMPONENT NUMBER	-
TS	- EQUIVALENT SINK TEMP (DUE TO ENVIRONMENT)	°R
AMAX	- MAXIMUM ALLOWABLE RADIATOR SURFACE AREA	FT ²
EMIS	- RADIATOR EMISSIVITY	-
SWT (J)	- RADIATOR WEIGHT FACTOR	LBS/FT ²

OUTPUTS

TY	- RADIATOR OUTLET TEMP	°R
WR	- RADIATOR PANEL WEIGHT	LBS
AR	- RADIATOR AREA REQUIRED FOR TY	FT ²

SUBROUTINE F E VAP (Q, WCP, TCI, L, TCO, WT)

INPUTS

Q	- HEAT TO BE REJECTED	BTU/HR
WCP	- COOLANT MASS FLOW RATE	BTU/HR-°F
TCI	- COOLANT INLET TEMP	°F
L	- COMPONENT NUMBER	-
FWT(L)	- HEAT EXCHANGER WT. FACTOR	LBS/UA
FXW(L)	- SUBSYSTEM FIXED WT	LBS
SWT(L)	- STRUCTURAL WT. FACTOR	LBS
CFT(L)	- HEAT EXCHANGER UA	BTU/HR-°F
PP	- POWER PENALTY	LBS/WATT

OUTPUTS

TCO	- COOLANT OUTLET TEMP	°F
WT	- SUBSYSTEM WEIGHT	LBS
QR	- ACTUAL HEAT REJECTED	BTU/HR
WH2O	- WATER USAGE RATE	LBS/HR
TOMAX	- MAX. COOLANT OUTLET TEMP POSSIBLE	°F
TO MIN	- MIN. COOLANT OUTLET TEMP POSSIBLE	°F

SUBROUTINE QMET (Q1, T1, T2, Q2, K)

INPUTS

Q1	- METABOLIC SENSIBLE HEAT LOAD AT T1	BTU/HR
T1	- ORIGINAL CABIN TEMPERATURE	°F
T2	- NEW CABIN TEMPERATURE	°F
-	- TABLE OF QS VS TCABIN FOR ONE MAN (LOC 501)	-

OUTPUTS

Q2	- METABOLIC SENSIBLE HEAT LOAD AT T2	BTU/HR
K	- IF ≠ 0, OFF TABLES	-

SUBROUTINE CRY (Q, WH, TIN, NC, WH2)

INPUTS

Q - HEAT TO BE REJECTED	BTU/HR
WH - COOLANT MASS FLOW RATE	BTU/HR-°F
TIN - COOLANT INLET TEMP	°F
NC - COMPONENT NUMBER	-
CFT (NC) - HEAT EXCHANGER UA	BTU/HR-°F

OUTPUTS

WH2 - HYDROGEN FLOW RATE (WHYD)	LBS/HR
TOC - COOLANT OUTLET TEMP (THOTCAL)	°F
TH2O - HYDROGEN OUTLET TEMP (THYDO)	°F

SUBROUTINE EBAY (QE, TE, TCI, WCPC, RHO, CPA, PP, DP, WTHX
WTFAN, PW, V, TCO, TAO, QT, LF)

INPUTS

QE	-	COMPARTMENT HEAT LOAD	BTU/HR
TE	-	DESIRED COMPARTMENT TEMP	°F
TCI	-	INLET COOLANT TEMP TO HX	°F
WCPC	-	COOLANT MASS FLOW	BTU/HR-°F
RHO	-	COMPARTMENT GAS DENSITY	LBS/FT ³
CPA	-	GAS SPECIFIC HEAT	BTU/LB-°F
PP	-	POWER PENALTY	LBS/WATT
DP	-	FAN PRESSURE RISE	IN - H ₂ O
LF	-	COMPONENT NUMBER OF HX	-
FWT(N)	-	WEIGHT FACTOR HX	LBS/UA
FXW(N)	-	FIXED WEIGHT ADDED TO COMPONENT	LBS
SWT(N)	-	STRUCTURAL WEIGHT FACTOR	-
		(USED FOR FAN, VALVE, & FIXED WEIGHT)	

OUTPUTS

WTHX	-	HEAT EXCHANGER & FIXED WEIGHT	LBS
WTFAN	-	FANS & CHECK VALVES WEIGHT	LBS
PW	-	FAN POWER	WATTS
V	-	FAN VOLUMETRIC FLOW RATE	CFM
TCO	-	COOLANT OUTLET TEMP	°F
TAO	-	AIR OUTLET TEMP LEAVING HX	°F
QT	-	TOTAL HEAT REMOVED BY HX	BTU/HR

SUBROUTINE CX2 (WC, TCI, QS, QL, TC, QS2, QL2, V, P, NL, K, TCO, V11, I, QSX)

INPUTS

WC	- COOLANT MASS FLOW RATE	BTU/HR - °F
TCI	- COOLANT INLET TEMP	°F
QS	- TOTAL SENS. HEAT TO BE REMOVED FROM CABIN (INCLUDES FAN)	BTU/HR
QL	- LATENT HEAT TO BE REMOVED FROM CABIN	BTU/HR
TC	- CABIN TEMPERATURE	°F
QS2	- SENSIBLE HEAT DOWNSTREAM OF FAN	BTU/HR
QL2	- LATENT HEAT DOWNSTREAM OF FAN	BTU/HR
V	- HEAT EXCHANGER MAX FLOW RATE	CFH
P	- FAN POWER	WATTS
NL	- COMPONENT NUMBER	-
K	- IF 0, SINGLE HX IF 1, ALSO SENS. HX	-
V11	- FAN FLOW RATE	FT ³ /HR
TOLQ	- TOLERANCE ON HX UA CONVERGENCE	DEC. FRAC.
PCAB	- CABIN PRESSURE	PSIA
RA	- CABIN GAS CONSTANT	FT/°R
CPA	- CABIN GAS SPECIFIC HEAT	BTU/LB-°R
QSM	- METABOLIC SENSIBLE HEAT	BTU/HR

OUTPUT

TCAB	- CABIN TEMP (MAY BE RAISED IF SYSTEM NOT CAPABLE)	°F
HXCFM	- AIR FLOW THROUGH HX	CFM
TDPCAB	- CABIN DEW POINT	°F
TAIRO	- HX AIR OUTLET TEMP	°F
TCO	- COOLANT OUTLET TEMP	°F
QSX	- SENSIBLE HEAT REMOVED BY CONDENSER	BTU/HR
I	- IF 0, SUBROUTINE CONVERGED	-

**SUBROUTINE CHX (QS, QL, TC, TCI, WCPC, RHO, CPA, PMAX, DPF, TAO, J, QCS, V,
PW, WT, TCCO, PXO, I, QS2, QL2, K, TDP)**

INPUT

QS	- CABIN SENS. HEAT LOAD	BTU/HR
QL	- CABIN LATENT HEAT LOAD	BTU/HR
TC	- CABIN TEMP HEAT LOAD	°F
TCI	- COOLANT INLET TEMP	°F
WCPC	- COOLANT MASS FLOW RATE	BTU/HR-°F
RHO	- CABIN GAS DENSITY	LB / FT ³
CPA	- CABIN GAS SPECIFIC HEAT	BTU/LB-°F
PMAX	- MAXIMUM CABIN H ₂ O VAPOR PRESS.	PSIA
DPF	- FAN PRESSURE RISE	IN-H ₂ O
J	- COMPONENT NO.	-
QS2	- SENS. HEAT ADDED DOWN STREAM OF FAN	BTU/HR
QL2	- LATENT HEAT ADDED DOWN STREAM OF FAN	BTU/HR
K	- { (IF 0, NO SENS HX (IF 1, SENS HX ALSO	-
CFT(J+10)	- FAN OVERALL EFFICIENCY	-
FWT(J)	- HX WEIGHT FACTOR	LBS/UA
FXW(J)	- FIXED WEIGHT ADDED TO SUBSYSTEM	LBS
SWT(J)	- STRUCTURAL WEIGHT FACTOR	LBS/LB

OUTPUT

TAO	- HX AIR OUTLET TEMP	°F
TDP	- CABIN DEW POINT	°F
QCS	- SENSIBLE HEAT REMOVED BY COND.	BTU/HR
V	- HX AIR FLOW RATE	FT ³ /HR
PW	- POWER REQUIRED BY COND. FLOW	WATTS
WT	- HX+VALVE WEIGHT	LBS
TCCO	- COOLANT OUTLET TEMP.	°F
PXO	- HX OUTLET VAPOR PRESS.	PSIA
I	- CONVERGENCE KEY -IFO, O.K.	-
WTHX	- HX WEIGHT	LBS
MVALVE	- AIR BYPASS VALVE WEIGHT	LBS
CFT(J)	- HX UA	BTU/HR-°F

SUBROUTINE HSC (WCO2, QLAT, DAY, RHO, PVI, PD, L, WT, V, WB, WU, VCH, WF)

INPUTS

WCO2	- CO2 REMOVAL RATE	LBS/DAY
QLAT	- LATENT HEAT REMOVAL RATE	BTU/HR
DAY	- MISSION LENGTH	DAYS
RHO	- CABIN GAS DENSITY	LBS/FT ³
PVI	- REQUIRED MAX. H ₂ O VAPOR PRESS LEVEL	PSIA
PD	- SYSTEM PRESSURE LOSS EXTERNAL TO CANISTER	IN-H ₂ O
L	- COMPONENT NUMBER	-
FCO2	- RATIO OF PEAK PRODUCTION RATE TO AVG RATE	-
CO2L	- CO2 DESIGN BED LOADING	LBS/LB
CYCL	- 1/2 CYCLE TIME	MIN
TCAB	- CABIN TEMP	°F
FWT(L)	- NUMBER OF CANISTERS	-
FXW(L)	- SYSTEM FIXED WEIGHT	LBS
SWT(L)	- STRUCTURAL WEIGHT FACTOR	LBS/LB
X(426)	- TABLE H ₂ O LOADING	-
X(351)	- TABLE OF CO ₂ LOADING	-
VCH	- NOT USED	-

OUTPUTS

WT	- SUBSYSTEM WEIGHT (EXCLUDING FAN)	LBS
V	- SUBSYSTEM FLOW RATE	FT ³ /HR
WB	- HSC BED WEIGHT	LBS
WU	- ULLAGE PENALTY	LBS
WF	- FAN WEIGHT INCREASE FOR HSC	LBS
WTCAN	- EMPTY CANISTER WT	LBS
WVVAL	- VACUUM CYCLING VALVE WT	LBS
WCVAL	- CONTROL VALVE WT	LBS
WKVAL	- CHECK VALVE WT (FAN FLOW)	LBS

SUBROUTINE LIOH (J, DAY, DPF, WL, WT PW, V, QS, QL)

INPUTS

J	- COMPONENT NUMBER	-
DAY	- MISSION LENGTH	DAYS
DPF	- FAN ΔP	IN - H ₂ O
WCO2	- AVERAGE CO ₂ REMOVAL RATE	LBS/DAY
TCAB	- CABIN TEMPERATURE	°F
FCO2	- RATIO OF ACTUAL PRODUCTION RATE/AVG.	-
FNCO	- NUMBER OF CANISTERS ON LINE	-
FRESH	- NUMBER OF FRESH CANISTERS ON LINE	-
CFT (11)	- FAN EFFICIENCY	-
CFT (J)	- CO ₂ REMOVAL EFFICIENCY	-
FWT (J)	- CANISTER WEIGHT FACTOR (TOTAL WT.)	LBS/LB

OUTPUTS

WT	- SUBSYSTEM TOTAL FIXED WEIGHT	LBS
WL	- MINIMUM WT OF LIOH REQUIRED FOR MISSION	LBS
PW	- FAN POWER REQUIRED FOR LIOH	WATTS
V	- VOLUME FLOW RATE	FT ³ /HR
QS	- { (SIZING PROGRAM - SENS & FAN HEAT LOAD	BTU/HR
	{ (OFF DESIGN - SENS HEAT OF REACTION	BTU/HR
Q L	- LATENT HEAT LOAD	BTU/HR
P MAX	- CO ₂ PARTIAL PRESSURE AT 60% η REM	MM HG
P MIN	- CO ₂ PARTIAL PRESSURE AT 95% η REM	MM HG

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**APPENDIX II
SUBROUTINE DESCRIPTION**

APPENDIX IISUBROUTINE DESCRIPTIONS

Listed below is a short description of what each of the subroutines does:

- START - Reads a comment card and prints it. A blank card terminates a run.
- LOAD - Loads the input data into the proper storage locations.
- UNBAR - A table interpolation routine.
- KANDK - Calculates the vapor pressure or dew point temperature of water vapor. Given one property it will calculate the corresponding property.
- LIQH - Calculates the heat loads, flow required, and weight of LiOH required for CO₂ removal.
- CHX - Calculates the optimum volume flow required and the heat exchanger weight to remove a given sensible and latent heat load.
If a sensible heat exchanger is also used, the coolant leaving temperature will be kept at or below the cabin dew point.
- SHX - Sensible heat exchanger subroutine calculates optimum volume flow rate and heat exchanger size.
- EBAY - Calculates the optimum heat exchanger size and volume flow rate to remove an air heat load from a separate compartment. Also calculates fan weight and power.

- 2 -

APPENDIX II (CONT)SUBROUTINE DESCRIPTIONS

- EBAY2 - Does the same as EBAY for two compartments in series. Calculates which compartment controls the sizing of the equipment and uses the same equipment in each compartment.
- HSC - This routine calculates the optimum flow rate and bed size for HSC. This material absorbs both CO₂ and H₂O vapor. During the off design performance, the water vapor partial pressure and CO₂ partial pressure are calculated as well as the air flow required for humidity control.
- CONT - Calculates the contaminant canister weight and volume flow rate required for contaminant control.
- FEVAP - Calculated the subsystem weight required to remove the input heat load. For off design performance it will remove as much heat as possible up to the desired heat load.
- FANWT - Calculates fan weight as a function of volume flow rate and pressure rise.
- CRY - Calculates the cryogen flow rate required to meet the given heat load. (Off design performance only).
- HX - Calculates the hot side leaving temperature giving the flow rates, heat rejected, and the cold side inlet temperatures. Used for sensible heat transfer only.

- 3 -

APPENDIX II

SUBROUTINE DESCRIPTIONS

- WTV2 - Calculates valve weight as a function of volume flow rate for:
- a) Check valves
 - b) Solenoid valves
 - c) Manual shut off valves
 - d) Gas disconnects
- RAD - Calculated radiator area and weight required to reject a given heat load at a given inlet temperature. If the area required exceeds the maximum area available, the routine will calculate the outlet temperature that can be reached at the maximum area.
- CX2 - Calculates condenser air outlet temperature and cabin dew point for a given sensible and latent load. It also calculates the heat exchanger volume flow rate required to meet the heat load. If the heat load can not be met at maximum air flow, the cabin temperature will be raised in 1°F increments until it can be met.
- QMET - Calculates the metabolic sensible/latent heat load ratio as the cabin temperature is varied.

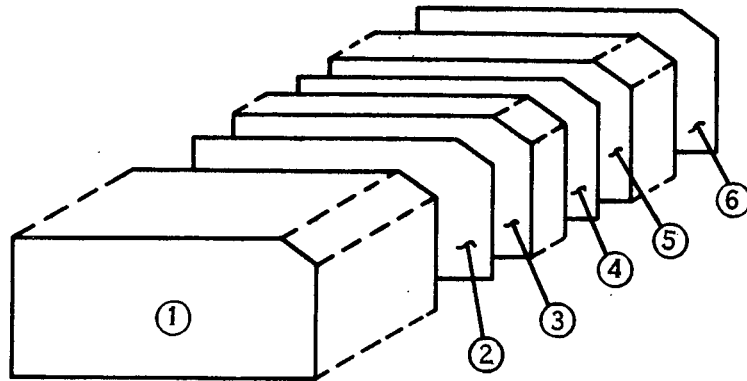


FIGURE 4-1 DECK SET UP

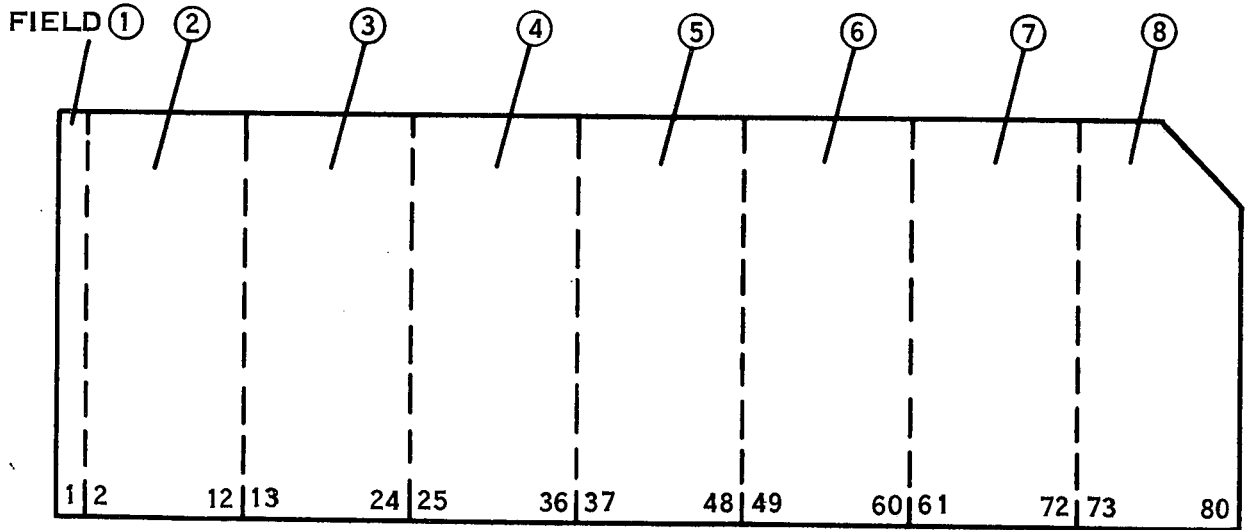
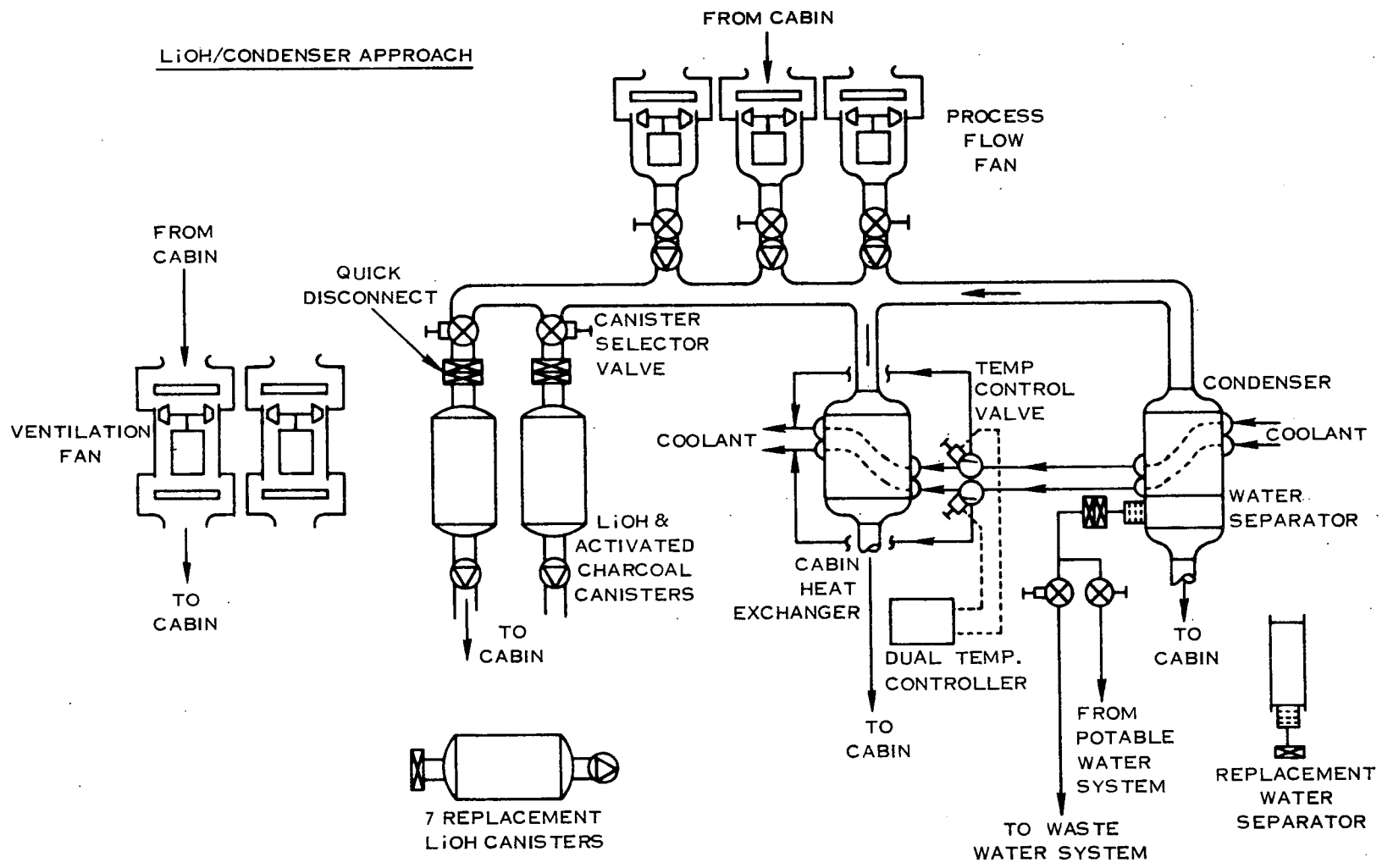


FIGURE 4-2 COMPUTER CARD SETUP



II-5/II-6

FIGURE 2-3. SAMPLE CASE - VENTILATION, CO₂, HUMIDITY &

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**APPENDIX III
LOGIC FLOW DIAGRAM**

12/12/72

AUTOFLOW CHART SET - H247B

PAGE 01

CHART TITLE - INTRODUCTORY COMMENTS

H247 SHUTTLE EC/LSS SIZING PROGRAM
LOAD DATA

CHART TITLE - PROCEDURES

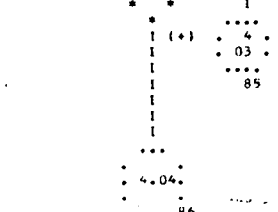
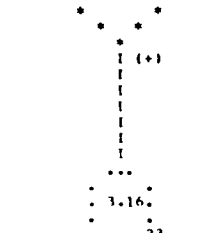
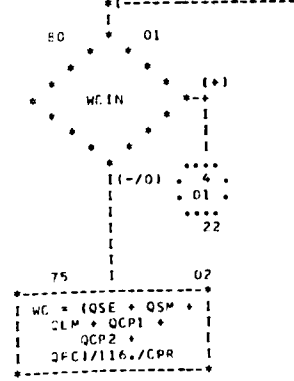
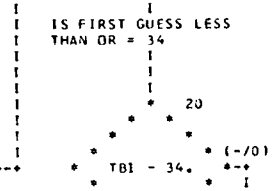
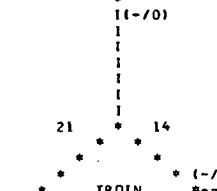
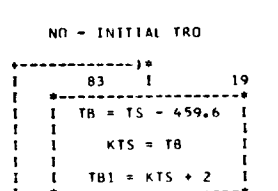
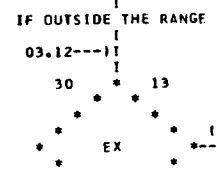
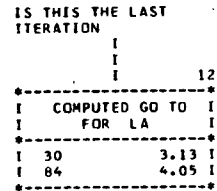
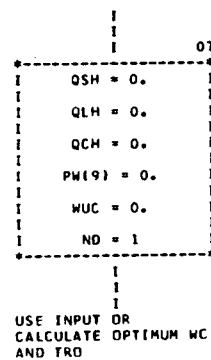
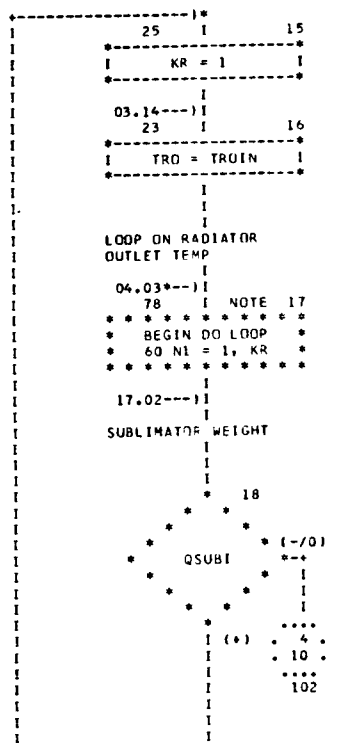
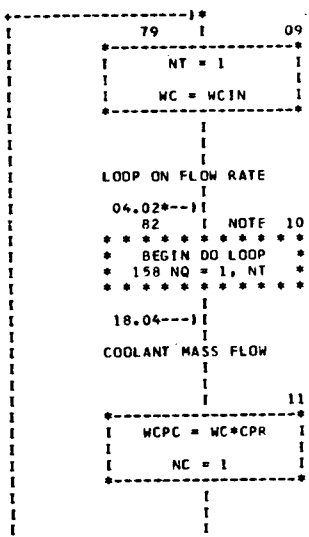
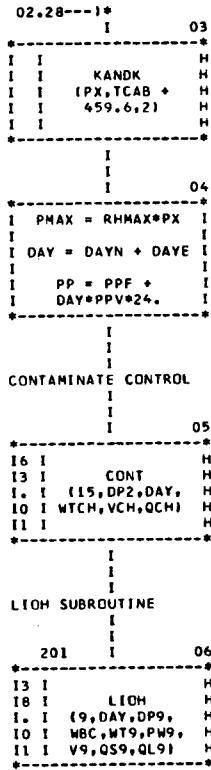


CHART TITLE - PROCEDURES

```

-----
/ 22 /
-----
03.01---) 01
|
| WC = WCIN |
|-----|
|
| 03.22---) 02
| 74 |
|-----|
| NT = EY |
|-----|
|
| ...
| 3.10.
| ... 82

```

```

NO
03.20---) 03
| 85 |
|-----|
| TR0 = 34. |
|-----|
|
| ...
| 3.17.
| ... 78

```

```

YFS
03.20---) 04
| 86 |
|-----|
| TR0 = TB1 |
|-----|
|
| ...
| 3.17.
| ... 78

```

```

THIS IS LAST
ITERATION
03.12---) 05
| 84 |
|-----|
| KR = 1 |
|-----|
|
| ...
| 3.17.
| ... 78

```

```

OUTLET TEMP
03.18---) 06
| 101 |
|-----|
| T1 = TR0 - |
| QSUB1/WCPC |
|-----|
| QSUB = QSUB1 |
|-----|

```

IS TEMP TOO LOW

```

07
* T1 - 34. * (-/0)
* * * *
* * * *
| (+) |
|-----|

```

TOO LOW

```

103 | 08
|-----|
| T1 = 34. |
|-----|
| QSUB = |
| WCPC*(TR0 - T1) |
|-----|

```

SUB WT

```

104 | 09
|-----|
| CFT(24) = |
| WCPC*ALOG1((TR0 - |
| 32.)/(T1 - 32.)) |
|-----|

```

NO QSUB

```

03.18---) 10
| 102 |
|-----|
| T1 = TR0 |
|-----|
| QSUB = 0. |
|-----|

```

CALCULATE - IS THIS
LAST ITERATION

```

105 | 11
|-----|
| COMPUTED GO TO |
| FOR LA |
|-----|
| 87 5.01 |
| 88 4.12 |
|-----|

```

IF OUTSIDE THE RANGE

LAST ITERATION

```

04.11---) 12
| 88 |
|-----|
| KT = 1 |
|-----|

```

```

|
| ...
| 5.02.
| ... 91

```



CHART TITLE - PROCEDURES

NOT LAST ITERATION

```

04.11---) *
87 I 01
[ T21 = T1 + DTX ]
[ KT = KI ]

```

```

04.12---) I
91 I 02
[ NB = 1 ]

```

LOOP ON INTERFACE
OUTLET TEMP

```

110 I NOTE 03
* * * * *
* BECIN DO LOOP *
* 50 N2 = 1, KT *
* * * * *

```

```

10.39*---) I
407 I 04
[ WPCPC = WPCPC*WRAT ]

```

FIRST GUESS OF DEW PT

```

[ PDP1 = .R*PHAX ]
[ WT13 = 0. ]

```

GO TO DESIRED CO2
SURROUTINE

```

[ COMPUTED GO TO ]
[ FOR M1 ]
210 7.01 I
301 5.07 I

```

IF OUTSIDE THE RANGE

HSB SURROUTINE

```

05.36---) I
301 I 07
[ KANDK ]
[ [PVI, T21 + ] ]
[ 459.6, 2 ] ]

```

```

[ TDPT = T21 ]

```

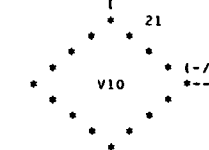
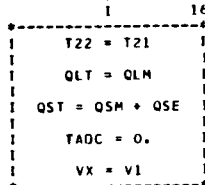
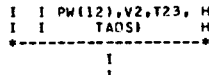
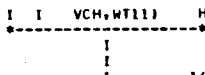
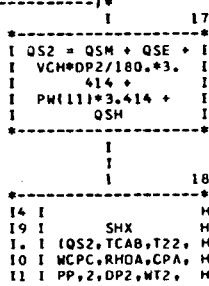
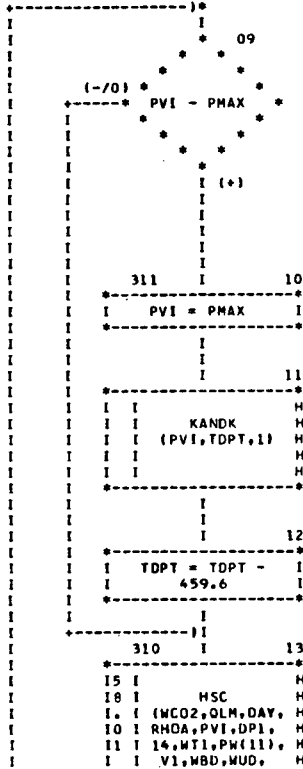


CHART TITLE - PROCEDURES

VENTILATION REQUIRED

```

07.18---)*
241 I 01
-----*
I PW(10) = I
I V10*DP10/510./ I
I CFT(10) I
-----*
I
I
I 02
-----*
17 I H
14 I FANWT H
1. I (V10,DP10,MTF) H
10 I H
11 I H
-----*

```

```

I
I
I
VENT -WT
I
I
I 03
-----*
I WT10 = I
I FWT(10)*MTF I
-----*

```

```

I
07.19---)I
550 I 04
-----*
I VX = V1 I
I
I VFC = 0. I
-----*

```

```

I
245 I 05
-----*
17 I H
14 I FANWT H
1. I (V11,DP1,MCF) H
10 I H

```

```

11 I H
-----*
I
I
I 06
-----*
18 I H
11 I MTV2 H
1. I (V11,2,WCV) H
10 I H
11 I H
-----*

```

```

I
I
I 07
-----*
I WT11 = I
I (FWT(11)*(WCF + I
I WCV) + .9*WCF + I
I FXW(11))*SWT(11) I
I
I PW(11) = I
I V11*DP1/510./CFT I
I (11) I
-----*

```

```

I
I
I 08
-----*
I COMPUTED GO TO I
I FOR LA I
-----*
I 1001 9.03 I
I 1002 9.01 I
-----*

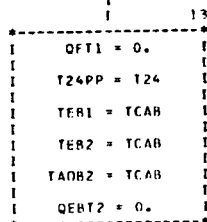
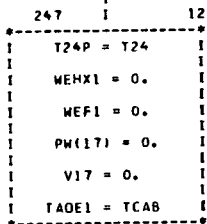
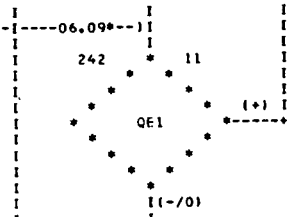
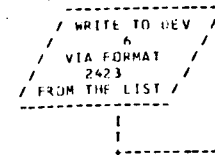
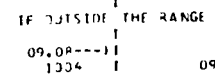
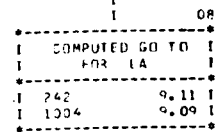
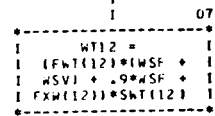
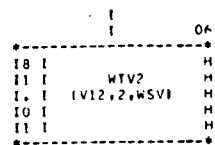
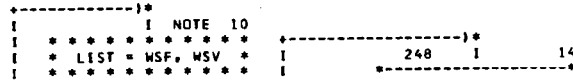
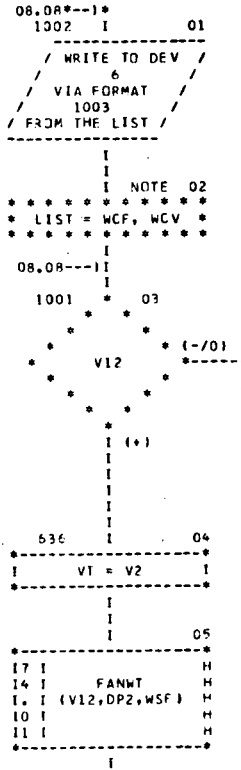
```

```

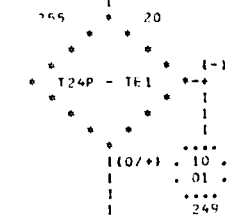
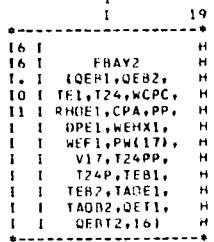
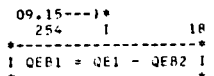
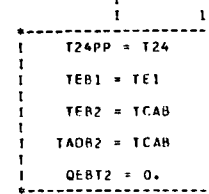
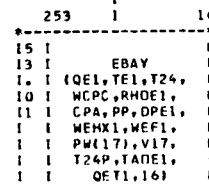
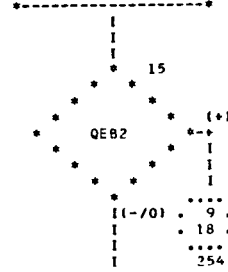
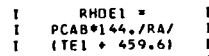
I
I
I
IF OUTSIDE THE RANGE
I
I
I /
-----*
/ 9.01

```

CHART TITLE - PROCEDURES



... 10.01
... 249



... 14.09
... 51

CHART TITLE - PROCEDURES

SIZE SUBL FOR TOTAL Q

11.20*--)*
170 I 01

CFT(8) =
WCPC*ALOG((TRI -
32.1)/(T1 - 32.1))

SUBL WT

02

WT8 =
FWT(8)*CFT(8) +
FXW(8)*SWT(8)
WT25 = 0.

WATER STORED

03

WSUB =
WCPC*(TRI -
T1)/1065.*TSUB

SIZE CRVD HX

11.22---)*
172 I 04

WHYD =
WCPC*(TRI -
T1)/(1440)*TCRY

DTLM = (TRI -
460. -
T1)/ALOG((TRI -
40.)/(T1 + 420.))

05

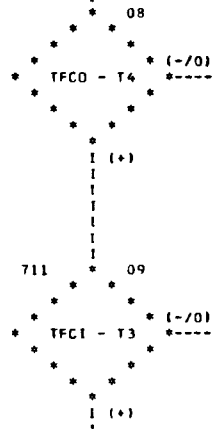
CFT(22) =
WCPC*(TRI -
T1)/DTLM
WT22 =
FWT(22)*CFT(22) +
FXW(22)*SWT(22)

SIZE GSE HX MFR=2
TC1=0

06

EFF = 1. - T1/TRI
CFT(21) =
WCPC*2.*ALOG((1. -
EFF/2.)/(1. -
EFF))
WT21 =
FWT(21)*CFT(21) +
FXW(21)*SWT(21)

SIZE F/C HX -CHECK
FLUID TEMPS



CAN NOT BUILD HX

12.08*--)*
710 I 10
WT20 = 2000.
CFT(20) = 10000.

14.09
... 51

13.01
... 712

CHART TITLE - PROCEDURES

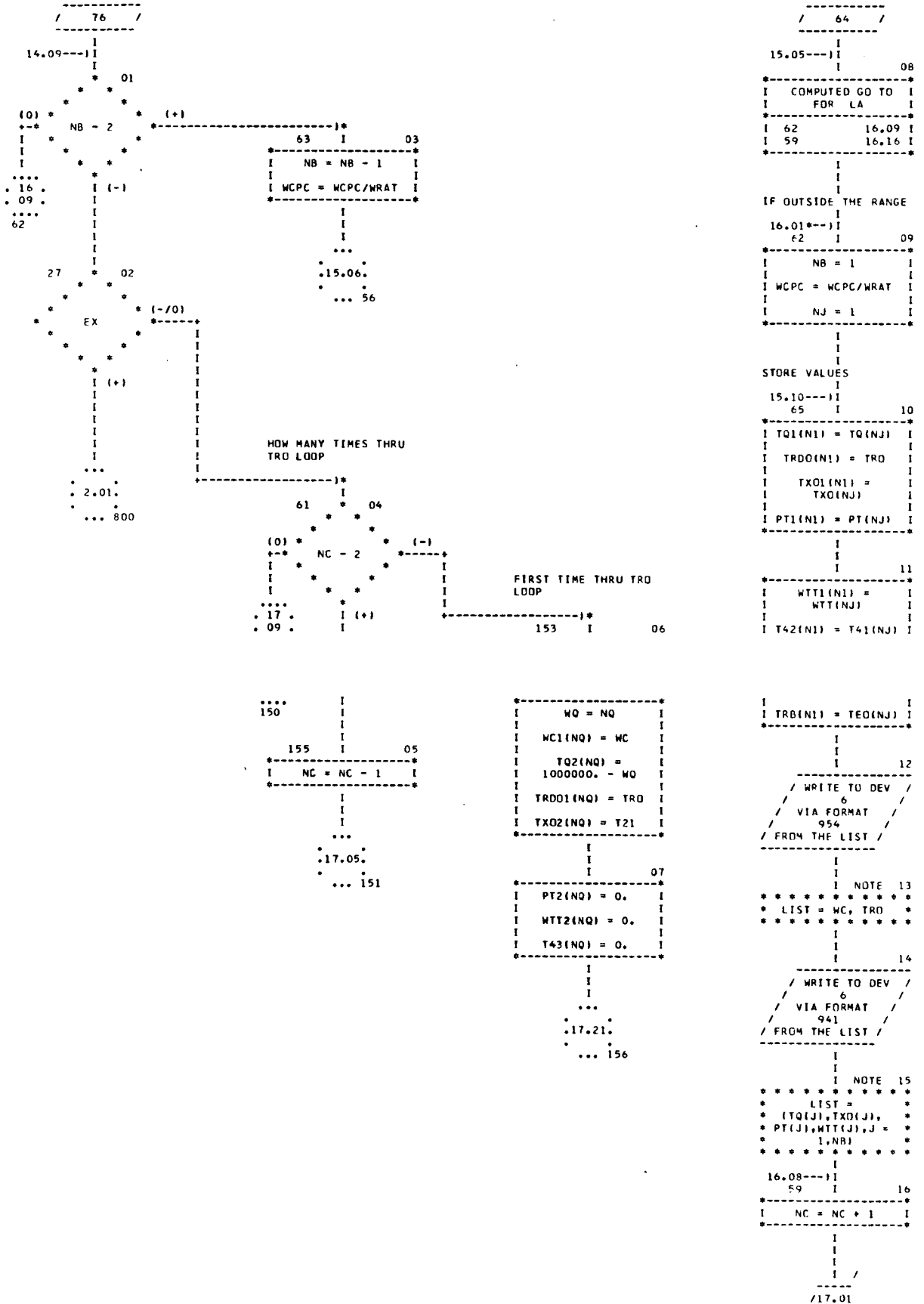


CHART TITLE - PROCEDURES

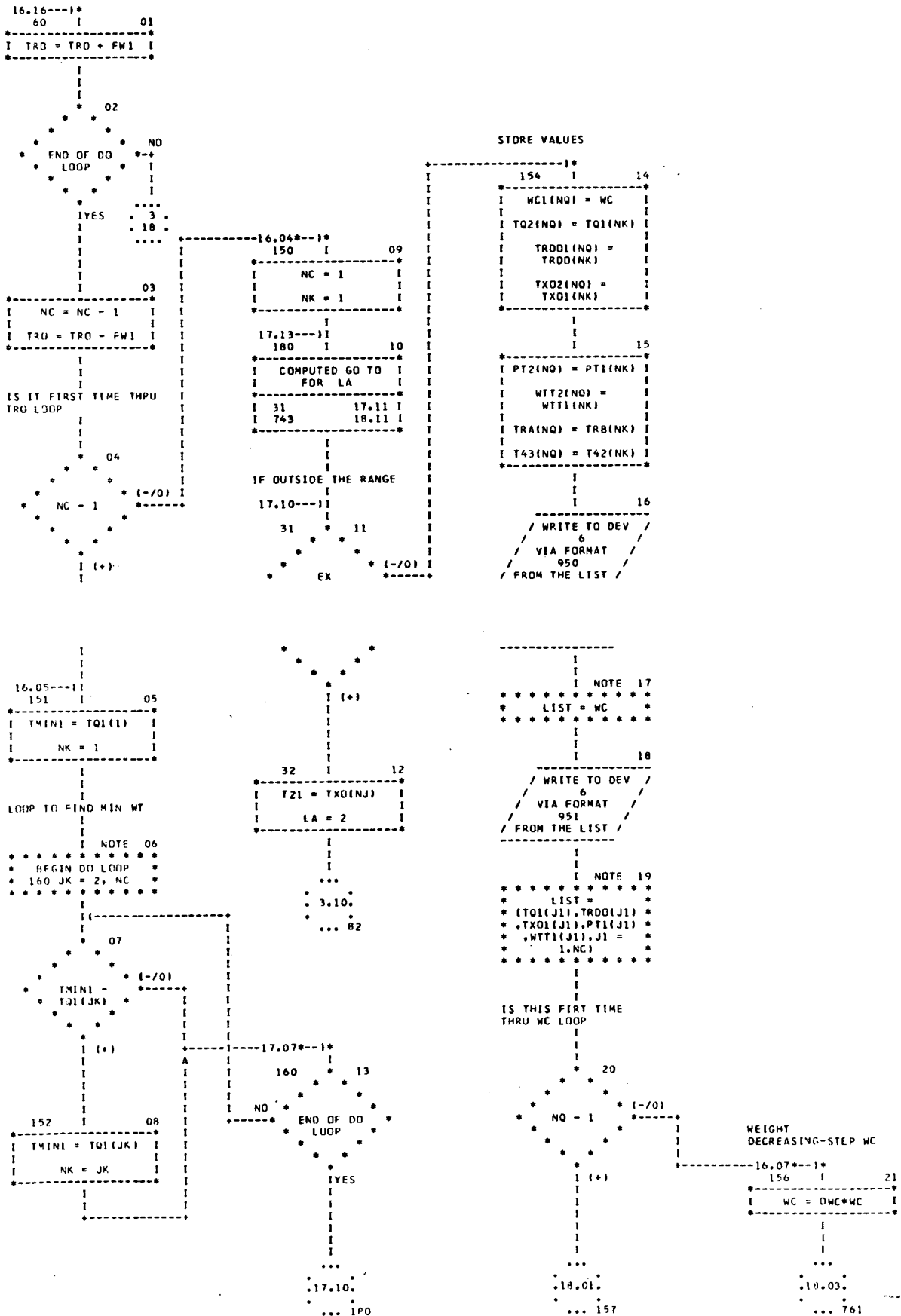


CHART TITLE - PROCEDURES

OFF DESIGN
PERFORMANCE-PRINT
POWERS

02.10---)*
801 I 01

WRITE TO DEV
6
VIA FORMAT
988
FROM THE LIST

I
I
I NOTE 02

* LIST = (X(J),J = *
* 191,205) *

I
I 03

WRITE TO DEV
6
VIA FORMAT
981
FROM THE LIST

I
I
I NOTE 04

* LIST = (X(J),J = *
* 206,220) *

I
I

PRINT COMPONENT
FACTORS

I
I 05

WRITE TO DEV
6
VIA FORMAT
976
FROM THE LIST

I
I
I NOTE 06

* LIST = (X(J),J = *
* 221,250) *

I
I

COMPONENT FLOW RATES

WRITE TO DEV
6
VIA FORMAT
977
FROM THE LIST

I
I
I NOTE 08

* LIST = V11, V12, *
* V17, V19, V10, V9 *

I
I

SFT VARIABLES

-----)*
I 10
I
I KEYC = FW5 I
I
I QSH = 0. I
I
I QLH = 0. I
I
I I = 0 I
I
I WCPC = WC*CPR I
I
I 11
I WHC = WCPC*WRAT I

I
I LA = 2 I
I TRO = TZ + 459.6 I
I
I Y1 = TZ I

LOOP ON CABIN TEMP

I
I
I NOTE 12

* BEGIN DO LOOP *
* 6123 NA = 1, 15 *

I
I 28.12---I

GET LIGH HEAT LOADS

I
I
I 13
I COMPUTED GO TO I
I FOR M1 I
I 655 21.01 I
I 656 20.14 I

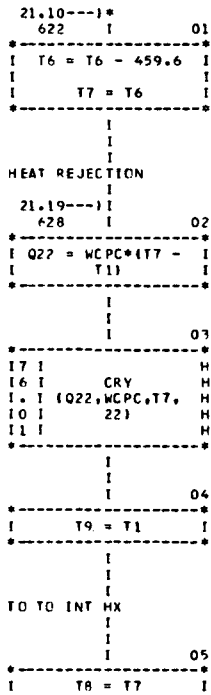
IF OUTSIDE THE RANGE

I
I
I HSC -NO LATENT LOADS
I
I 20.13---I
I 656 I 14
I QCABL = 0. I
I
I Q59 = 0. I

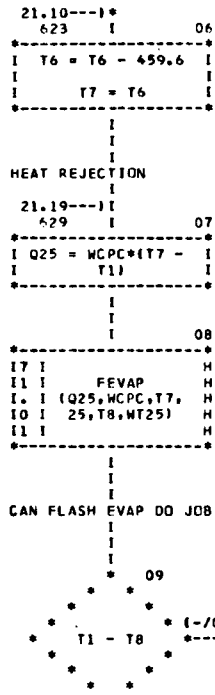
...
21.03
... 657

CHART TITLE - PROCEDURES

CRYOGENIC HX -SET
TEMPS



FLASH EVAP -SET
TEMPS



CAN MEET TEMP

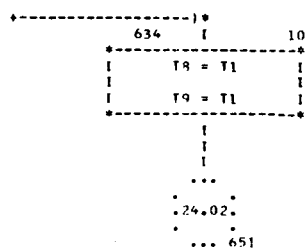
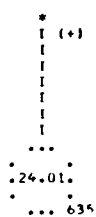
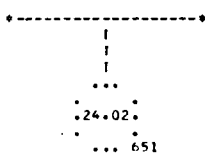


CHART TITLE - PROCEDURES

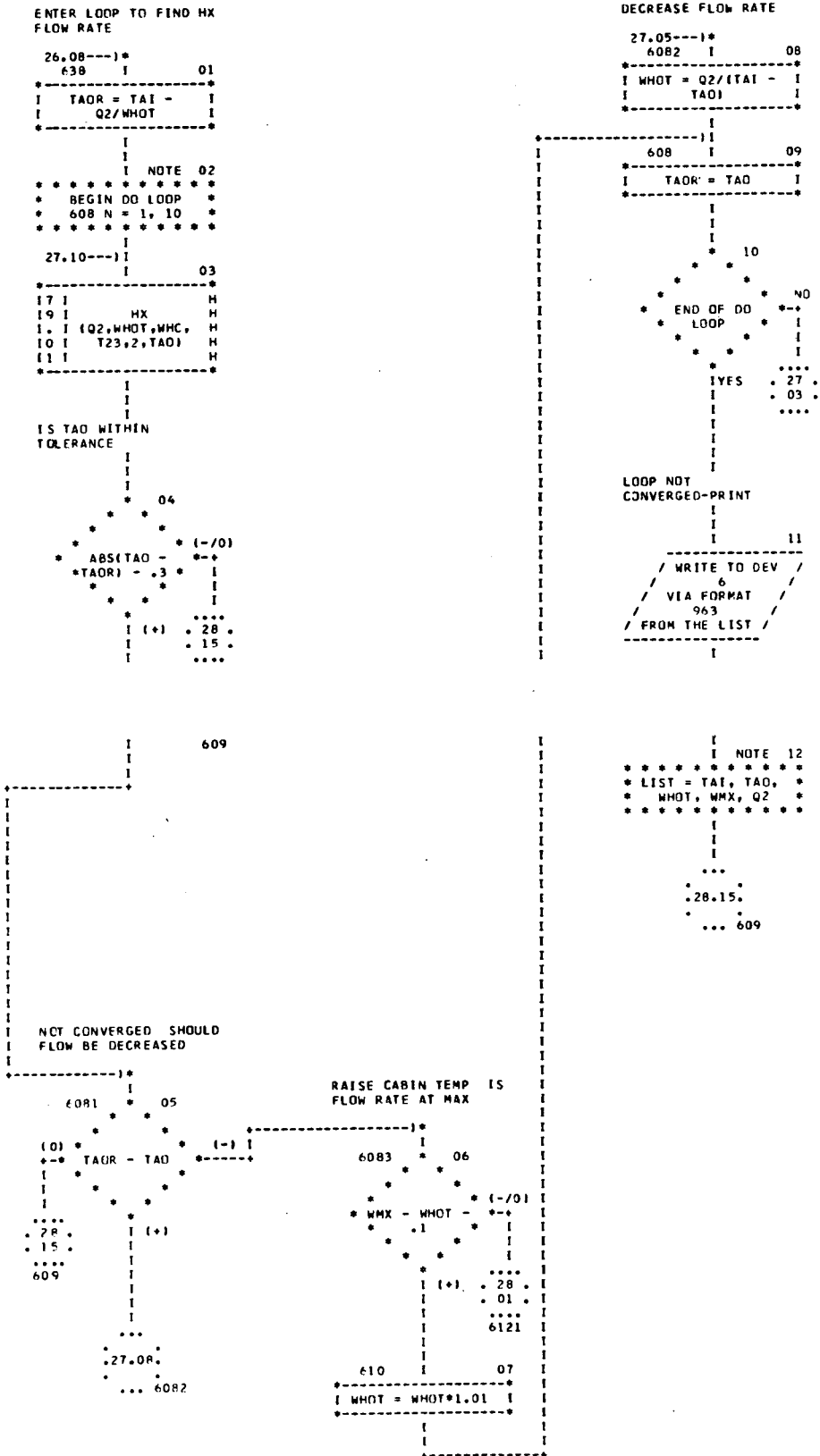


CHART TITLE - PROCEDURES

6121 RAISE CABIN TEMP
& CHANGE METABOLIC
LOADS

27.06---)*
6121 I 01

19 I QMET H
14 I QSM,TCAB, H
10 I TCAB + H
11 I 1.,QSN,KAI H

02
TCAB = TCAB + 1.

WHAT IS CO2 REMOVAL
SYSTEM

03
COMPUTED GO TO
FOR M1

6122 28.04 I
6124 28.10 I

IF OUTSIDE THE RANGE
LIQH-CONDENSER +SENS
HX
28.03---)*
6122 I 04

QCABS = QCABS +
QSN - QSM

QCABL = QCABL +
QSM - QSN

QIM = QLM + QSM -
QSN

612 05
QSM = QSN

06
END OF DD
LOOP
YES 24
NO 06

CABIN TEMP NOT
CONVERGED

08
WRITE TO DEV
6
VIA FORMAT
962
FROM THE LIST

NOTE 09
LIST = TCAB,
WHOT, Q2, QCDS,
T22, T23, QSM,
QLM

HSC SUBROUTINE

28.03---)*
6124 I 10
QLM = QLM - QSN +
QSM

6123 I 11
QSM = QSN

12
END OF DD
LOOP
YES 20
NO 13

LOOP ON CABIN
TEMP-NOT CONVERGED

13
WRITE TO DEV
6
VIA FORMAT
9621
FROM THE LIST

NOTE 14
LIST = QSM, QLM,
TCAB, QCABS

CONTINUE
27.04---)*
609 I 15

T24 = T23 +
Q2/WMC
VHX =
WHOT/CPA/PCAB/
144.*RA*(TCAB +
459.6)

SENS HX PRINT

16
WRITE TO DEV
6
VIA FORMAT
972
FROM THE LIST

NOTE 17
LIST = Q2, VHX,
TAI, TAO, TCAB,
QSM

25.06
613

CHART TITLE - PROCEDURES

DOUBLE EBAY

25.07---)*
6152 I 01

QEE1 = QE1 -
QEB2 +
PW(17)*1.707
QEE2 = QEB2 +
PW(17)*1.707
RHOE1 =
PCAB*144./RA/
(TE1 + 459.6)

02

WE1 =
V17*RHOE1*CPA

FIRST BAY

03

17 I H
19 I HX H
18 I (QEE1,WE1,WHC, H
10 I T24,16,TAE1) H
11 I H

04

TEE1 = TAE1 +
QEE1/WE1
T25A = T24 +
QEE1/WHC

05

WRITE TO DEV
6
VIA FORMAT
9641
FROM THE LIST

NOTE 06

* * * * *
* LIST = QEE1, WE1, *
* TEE1, TAE1, T25A *
* * * * *

SECOND BAY

07

17 I H
19 I HX H
18 I (QEE2,WE1,WHC, H
10 I T25A,16,TAE2) H
11 I H

08

TEE2 = TAE2 +
QEE2/WE1

COOLANT OUTLET TEMP

10

T25 = T25A +
QEE2/WHC

11

WRITE TO DEV
6
VIA FORMAT
9641
FROM THE LIST

NOTE 12

* * * * *
* LIST = QEE2, WE1, *
* TEE2, TAE2, T25 *
* * * * *

CHART TITLE - PROCEDURES

AVION BAY -HEAT LOAD

```

25.07---)*
615 I 01
I Q16 = QE1 + I
I PW(17)*3.414 I

```

MINIMUM AIR DENSITY

```

I I
I I
I I C2
I RHDE1 = I
I PCAB*144./RA/ I
I (TF1 + 459.6) I

```

MIN FLOW RATE

```

I I
I I 03
I WE1 = I
I V17*RHDE1*CPA I

```

```

I I 04
17 I H
19 I HX H
1. I (Q16,WE1,WHC, H
10 I T24,16,TE10) H
11 I H

```

EBAY TEMP

```

I I 05
I T11 = TE10 + I
I QE1/WE1 I

```

COOLANT OUTLET TEMP

```

I I 06
I T25 = T24 + I
I 216/WPC I

```

PRINT OUTPUT

```

I I 07
I WRITE TO DEV I
I VIA FORMAT I
I 964 I
I FROM THE LIST I

```

```

I I NOTE OR
I LIST = Q16, WE1, *
I T11, TE10 *

```

PUMP OUTLET TEMP
COLD PLATE OUTLET TEMP

```

I I
I I

```

BAY- HEAT LOAD HX

```

30.12---)*
618 I 14
I Q18 = QE2 + I
I PW(19)*3.414 I

```

MIN AIR DENSITY

```

I I
I I
I I 15
I RHDE2 = I
I PCAB*144./RA/ I
I (TE2 + 459.6) I

```

MIN AIR MASS FLOW

```

I I
I I 16
I WHX = I
I V19*RHDE2*CPA I

```

```

I I 17
17 I H
19 I HX H
1. I (Q18,WHX,WPCPC, H
10 I T2,18,TE20) H
11 I H

```

AIR TEMP

```

I I 18
I TE2B = TE20 + I
I QE2/WHX I

```

COOLANT TEMP

```

I I 19
I T3 = T2 + I
I Q18/WPCPC I

```

PRINT DATA

```

I I 20
I WRITE TO DEV I
I VIA FORMAT I
I 965 I
I FROM THE LIST I

```

```

I I NOTE ?1
I LIST = Q18, WHX, *
I TE2B, TE20 *

```

COLD PLATE TEMP

```

I I
I I /
I 31.01

```

```

25.08---)*
616 I 10
I T26 = T25 + I
I QCPI/WHC I
I T27 = T26 + I
I PW(4)*3.414/WHC I

```

RAD LOOP -INTER HX
OUTLET TEMP

```

I I 11
I T2 = T1 + Q5/WCPC I

```

AVIONICS BAY -RAD
LOOP

```

I I 12
I (-/0)
I V19
I (+)

```

NO BAY-SET TEMPS

```

I I 13
I T3 = T2 I

```

```

... 30.14
... 618

```

```

... 31.01
... 619

```


CHART TITLE - PROCEDURES

HSC- NO LATENT LOADS

```

31.22---)*
8052 I 01
-----)
I QLT = 0. I
-----)
I
31.24---)I
8052 I 02
-----)
I QTOT = QPH + I
I QSE + QSM + QSN + I
I QSE + QF1 + QE2 + I
I QCP1 + QCP2 + I
I QC+IL + QFC + QLT I
I DT = QTOT/WCPC I
-----)
I
I
ENTER LOOP TO GO
AROUND ORBIT
I
I NOTE 03
*****
* BEGIN DD LOOP *
* P10 N = 1, NS *
*****
I
33.10---)I
I 04
-----)
I T10 = T1 I
-----)
I
I 05
-----)
I I UNBAP H
I I (S,L,A,O.,FK, H
I I L(N)) H
I I H

```

```

-----)
I
I
SINK TEMP
I
I 06
-----)
I TS = I
I (F</(EMIS*.1714E- I
I R))**.25 I
I
I TPR(N) = TS I
-----)
I
I
INLET RAD TEMP
I
I 07
-----)
I TRAIN) = T1 + DT I
-----)
I
I
TEMP RATIOS
I
I 08
-----)
I T1 = TRAIN) + I
I 459.6 I
I
I T1 = T1 + 459.6 I
-----)
I
I
ENTER LOOP TO FIND
EVAP OUTLET TEMP
I
I

```

RADIATOR CAN NOT DO
JOB -CHANGE TEMP

```

-----)I*
811 I 13
-----)
I TR = TOR - 459.6 I
-----)
I
I
EVAPORATOR HEAT LOAD
I
I 14
-----)
I QE = WCPC*(TR - I
I T10) I
-----)
I
I
GO TO SUPPLEMENTRY
HEAT SINK
I
I 15
-----)
I COMPUTED GO TO I
I FOR NR I
-----)
I 813 32.20 I
I 812 32.16 I
I 814 32.18 I
-----)
I
I
IF OUTSIDE THE RANGE
I
I
CRYOGENIC HX
I
32.15---)I 16
812 I

```

FLASH EVAPORATOR

```

32.15---)*
814 I 18
-----)
I7 I FFVAP H
I1 I (QE,WCP,TR, H
I I (QE,WCP,TR, H
I0 I 25,TEO(N),WT) H
I1 I H
-----)
I
I
I 19
-----)
I WEV(N) = QE/965. I
-----)
I
I
...
.33.08.
... 816

```

SUBLIMATOR HEAT SINK

```

32.15---)*
813 I 20
-----)
I EFF = 1. - I
I 1./EXP(CFT(24) I
I /WCPC) I
I
I TR2 = TR - I

```

```

-----)I*
I NOTE 10
*****
* BEGIN DD LOOP *
* 815 NN = 1, 10 *
*****
I
33.03---)I
I
RAD PERFORMANCE
I
I 11
-----)
I8 I RAD H
I12 I (T1,TD,WCP, H
I I WT7,AP,WEXP, H
I2 I TOR,7) H
-----)
I
I
DID RADIATOR DO TOTAL
JOB
I
I 12
-----)
I TOR - TD - .5 (-/0) I
-----)
I
I (+) .33. I
I .07. I
I
I 819
-----)

```

```

-----)I*
17 I CRY H
16 I (QE,WCP,TR, H
I I 22,WEV(N)) H
I1 I H
-----)
I
I 17
-----)
I TEO(N) = T1 I
-----)
I
I
...
.33.08.
... 816

```

```

I EFF*(TR - 32.) I
-----)
I
I
HEAT REJECTED
I
I 21
-----)
I WEV(N) = I
I WCPC*(TR - I
I TR2)/1060. I
I
I TEO(N) = TR2 I
-----)
I
I
IS TEMP WITHIN
TOLERANCE
I
I 22
-----)
I
I
* ABS(T10 - (-/0)
* TR2) - .5 * I
I
I
I (+) .33.
I .08.
I
I 816
-----)
I
I
...
.33.01.
... 817

```

E

CHART TITLE - PROC EDURES

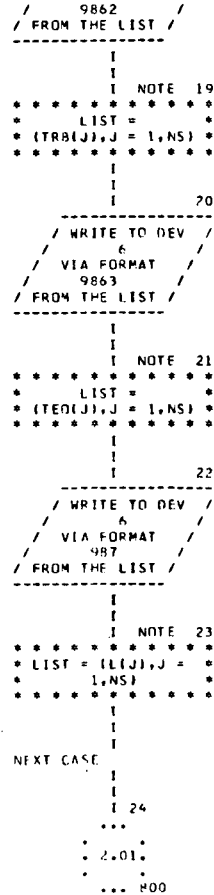
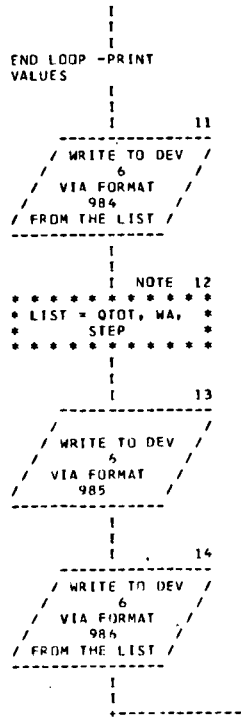
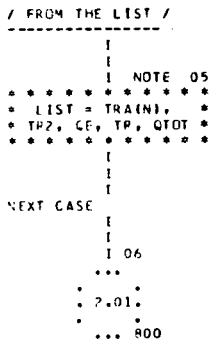
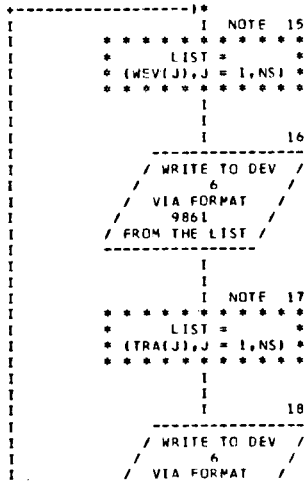
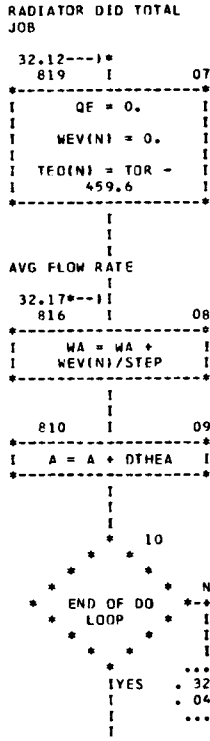
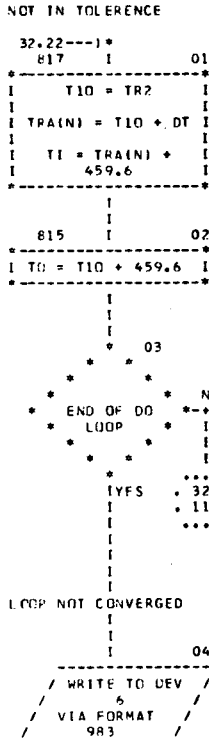


CHART TITLE - NON-PROCEDURAL STATEMENTS

```

DIMENSION S(100),T(100)
DIMENSION TRA(30),TRB(30),TED(30),WEV(30),L(30)
DIMENSION FWT(30),FXW(30),SWT(30)
DIMENSION TQ(20),TXO(20),PT(20),WTT(20)
DIMENSION T41(20),TQ1(20),TRD0(20),TXO1(20),PT1(20),WTT1(20),
T42(20),WC1(50),TQ2(50),TRD01(50),TXO2(50),PT2(50),WTT2(50),
T43(50)
,CFT(30),PW(30)
COMMON X(700),LA,NPER,PP
EQUIVALENCE
(X(101),FWT(1)),(X(131),FXW(1)),(X(161),SWT(1))
,(X(191),PW(1)),(X(221),CFT(1))
EQUIVALENCE
(X( 1),TCAB ),(X( 2),PCAB ),(X( 3),RA ),(X( 4),TROIN ),
(X( 5),WCIN ),(X( 6),CPC ),(X( 7),CPR ),(X( 8),RHOC ),
(X( 9),RHOR ),(X(10),WCO2 ),(X(11),DAYN ),(X(12),QSM ),
(X(13),QSE ),(X(14),QLM ),(X(15),QCP1 ),(X(16),QCP2 ),
(X(17),QFC ),(X(18),QSUBI ),(X(19),A1 ),(X(20),A2 ),
(X(21),DTX ),(X(22),TDLP ),(X(23),TVOL ),(X(24),DAYE ),
(X(25),RMAX ),(X(26),HXIM ),(X(27),SPLITM),(X(28),CONDM ),
(X(29),RHMAX ),(X(30),WRAT )
EQUIVALENCE
(X(31),FW1 ),(X(32),FW2 ),(X(33),PPF ),(X(34),PPV ),
(X(35),FW5 ),(X(36),EX ),(X(37),EY ),(X(38),DWC ),
(X(39),FW9 ),(X(40),FW10 ),(X(41),DPI ),(X(42),DP2 ),
(X(43),DP4 ),(X(44),DP6 ),(X(45),DP9 ),(X(46),DP10 ),
(X(47),TS ),(X(48),CPA ),(X(49),AMAX),(X(50),FEXP)
EQUIVALENCE
(X(51),QAMIN),(X(52),QCPM),(X(53),QE1 ),(X(54),QE2 ),
(X(55),TE1 ),(X(56),TE2 ),(X(57),DPE1 ),(X(58),DPE2 )
EQUIVALENCE (X(59),FRAD),(X(60),FCO2),(X(61),FNCO2),(X(62),TCMAX)
EQUIVALENCE
(S(1),X(301)),(T(1),X(401))
,(X(63),CHSB),(X(64),EM2D),(X(65),CYCL),(X(66),QEB2)
,(X(77),FRESH),(X(67),QCHIL),(X(68),TOLQ),(X(69),WFC )
,(X(70),RN ),(X(71),WC ),(X(72),T2 ),(X(73),FACT )
,(X(100),PERF ),(X(191),PW(1)),(X(221),CFT(1))
,(X(251),V11 ),(X(252),V12 ),(X(253),V9 ),(X(254),V10 )
,(X(255),V17 ),(X(256),V19 )
,(X(73),TCRY),(X(74),TSUB),(X(75),TFCL),(X(76),TFCL)
,(X(100),PERF)
,(X(78 ),FMIS ),(X(79 ),STEP ),(X(80),TAU )
2423 FORMAT(1H0'SFNSIBLE FAN ',F8.2,BH FANWT F8.2,BH WTVK )
1003 FORMAT(1H0'CONDENSER FAN ',F8.2,BH FANWT F8.2,BH WTVK )
977 FORMAT(1H0' COMPONENT FLOW RATES-CFH'/F8.1,' CONDF ',F8.1,' SENE
',F8.1,' AVFANh ',F8.1,' AVFANR ',F8.1,' VENTF ',F8.1,' LIQH ')
976 FORMAT(1H0'COMPONENT FACTORS-UA,EFF,FTC.'/1H 15F8.2/1H 15F8.2 )

```

CHART TITLE - NON-PROCEDURAL STATEMENTS

```

999   FORMAT(1HO'SUBLIMATOR LOOP NOT CONVERGED'/1H F8.1,8H QTDT F8.1,
      8H QREJ F8.2,8H TRI F8.2,8H TRD F8.2,8H TSUBO )
961   FORMAT(1HO'CONDESER PERFORMANCE NOT CONVERGED'/F8.1,' WCOOL ',
      F8.2,' TCI ',F8.1,' QCABS ',F9.1,' QCABL ',F8.2,' TCAB ',F8.1,'
      QSH ',F8.1,' QLH '/F8.1,'VAIR ',F8.2,' PMFAN ')
980   FORMAT(1HO'REHEATER REQUIRED'/ F8.1,' QSENS ',F8.2,' TCAB ',F8.1,
      ' VSENS ',F8.2,' TCIN ' )
963   FORMAT(1HO'SENS HX FLOW LOOP NOT CONVG'/F8.2,' TAI ',F8.2,' TAO
      ',F8.1,' WAIR ',F8.1,' WAIRMAX ' )
962   FORMAT(1HO'CABIN TEMP NOT CONVERGED'/F8.2,' TCAB ',F8.1,' WASEN',
      F8.1,' QSENSX ',F8.1,' QCSEN ',F8.2,' TCDI ',F8.2,' TSI '
      ,F8.1,8H QSMET F8.1,8H QLMET )
9671  FORMAT(1HO'HSC-CABIN TEMP LOOP NOT CONVERGED'/1H F8.2,8H QSM
      F8.2,8H QLM F8.2,8H TCAB F8.2,8H QCABS )
9641  FORMAT(1HO'WATER COOLED AVIONICS BAY'/1H F8.1,8H QHX F8.2,8H WC
      PAIR F8.2,8H TBAY F8.2,8H TMXAD F8.2,8H TMXCO )
964   FORMAT(1HO'WATER COOLED AVIONICS BAY'/F8.1,' QHX ',F8.1,' WCPAIR'
      ,F8.2,' TBAY ',F8.2,' TXO ')
965   FOPMAT(1HO'RADIATOR LOOP COOLED AVIONIC BAY'/
      F8.1,' QHX ',F8.1,' WCPAIR ',F8.2,' TBAY ',F8.2,' TXO ')
96A   FORMAT(1HO'FUEL CELL HX '/
      F8.1,' QFC ',F8.1,' WFC ',F8.2,' TF/CI ',F8.2,' TF/CO ')
967   FORMAT(1HO'CABIN LOOP TEMPS ')
968   FORMAT(1HO'RADIATOR LOOP TEMPS ')
971   FORMAT(1HO' HEAT LOADS '/

      F8.1,' QCOND ',F8.1,' QSENS ',F8.1,' QCPUMP ',F8.1,' QINTX ',
      F8.1,' QRPUMP ',F8.1,' QRAD '/F8.1,' QEVAP ',F8.1,' QRY ',
      F8.1,' QLAT ' )
972   FORMAT(1HO'SENS HX PERFORMANCE '/
      F8.1,8H QSENS F8.1,8H VMX F8.2,8H TXAI F8.2,8H TXAD F8.2,
      8H TCAB F8.1,8H QMETS )
901   FORMAT(20H QLAT NOT CONVERGED /1H F8.2,8H TRD F8.2,8H TIMXO
      F8.4,8H PH2OI F8.4,8H PH2OU )
902   FORMAT(20H CANNOT MEET QSENS /1H F8.2,8H TRD F8.2,8H TIMXO )
903   FORMAT(1H F8.1,8H QHXS F8.2,8H TEQWT F8.2,8H MXWT F8.2,8H WAL
      LWT F8.2,8H FANPh F8.2,8H TAOX )
904   FORMAT(26H1SYSTEM ITERATION WEIGHTS /1H F8.1,8H TIMXI F8.2,8H TIM
      XD F8.2,8H TEQWT F8.2,8H TOTWT F8.2,8H TOTPW F8.2,8H TAOS
      F8.2,8H TAOC )
905   FORMAT(114HO H2OREM HXSENS W/S PUMPC HXINTF PUMPR RADWT
      SUBLIM CO2REM VENT CONTC FAN C FAN A FAN MS )
906   FORMAT(14F8.2)
907   FORMAT(27HO COMPONENT POWERS (WATTS) /65H H2OREM SENSEF PUMPC
      PUMPR CO2REM VENTF EBAY1 EBAY2 )
908   FOPMAT(30HO COMPONENT FLOW RATES CFM /
      1H F10.1,8H H2OREM F9.1,8H CO2REM F9.1,8H SENHX F10.1,8H VENT
      F10.1,8H CONTM F10.1,8H FAN C F10.1,8H FAN A /

```

CHART TITLE - NON-PROCEDURAL STATEMENTS

```

1H F10.1,8H EBAY1 F10.1,8H EBAY2 )
909 FORMAT(1H F8.4,8H PDPO F8.1,8H WCOOL F8.3,8H WBCO2 F8.3,8H WBO
ES F8.2,8H ULLPEN F8.1,8H ARAD F8.2,8H WTEXP )
910 FORMAT(13HO INPUT DATA /
1H F8.2,8H TCAB F8.2,8H PCAB F8.2,8H RGAS F8.3,8H TRADO
F8.2,8H WRAD F8.2,8H CPCOOL F8.2,8H CPRAD F8.2,8H RHOC /
1H F8.2,8H RHOR F8.2,8H WCO2 F8.2,8H DAYS F8.1,8H QSMET
F8.1,8H QSENE F8.1,8H QLMET F8.1,9H QCP1 F8.1,8H QCP2 /
1H F8.1,8H QFCELL F8.1,8H QSUBL F8.1,8H KEY CO2F8.1,8H KEY H2O
F8.2,8H DTIMX F8.3,8H TOLP F8.1,8H TVENT F8.3,8H DAYEM /
1H F8.2,8H NO TRADF8.2,8H NO TIHOF8.2,8H BLANK FR.2,8H NO QLAT
F8.3,8H PHMAX F8.2,8H WC/WR F8.4,8H DT RADUF8.4,8H EF FC /
1H F8.4,8H PPFIX F8.5,8H PPVAR F8.2,8H KEY HXS F8.4,8H KEY OPT
F8.4,8H NO WC F8.4,8H FACT WCF8.4,8H KEY RADF8.4,8H KEY CON /
1H F8.2,8H DP H2O F8.2,8H DP SHX F8.2,8H DP CP F8.2,8H DP RP
F8.2,8H DP CO2 F8.2,8H DP VENTF8.2,8H T SINK F8.2,8H CPA /
1H F8.2,8H AMAX F8.2,8H FEXP F8.2,8H QAMIN F8.2,8H QCPM
F8.1,8H QE1 F8.1,8H QE2 F8.2,8H TE1 F8.?,8H TE2 /
1H F8.2,8H DPE1 F8.2,8H DPE2 F8.2,8H F RAD F8.2,8H F CO2
F8.2,8H FN CO2 F8.2,8H TCMAX F8.3,8H CO2L FR.3,8H EFM2O )
911 FORMAT(1H F8.1,8H ULLDES F8.1,8H ULLCO2 F8.1,8H DEW PT F8.1,8H TAO
E11 F8.1,8H TAOE12 F8.1,8H TEB1 F8.1,8H TEB2 /1H F8.1,8H TAOE2
)
912 FORMAT(1HO* EBHX1 EBFAN1 EBHX2 EBFAN2 FCHX CRYHX WTH2O
WTHYD FFEVAP GSE *)

930 FORMAT(26HO COMPONENT WEIGHT FACTORS /
122H COND SENHX W/S PUMPC HXINT PUMPR RAD SUB
L1OH VENT FANC FANS C HSC CONTM /
1H 15F8.4 )
931 FORMAT(20H SUBSYSTEM FIXED WT / 1H 15F8.2 )
932 FORMAT(23H STRUCTURAL WT FACTORS /1H 15F8.4 )
933 FORMAT(1HO* COMPONENT WEIGHT FACTORS*/' EBHX1 EBFAN1 EBHX2 EB
FAN2 FCHX GSEHX CRYHX CHILL SUBLT FFEVAP A B*
/15F8.4 )
934 FORMAT(20H SUBSYSTEM FIXED WT /1H 15F8.4)
935 FORMAT(23H STRUCTURAL WT FACTORS /1H 15F8.4)
936 FORMAT(29HO RADIATOR LOOP TEMPERATURES )
937 FORMAT(29HO CABIN LOOP TEMPERATURES )
938 FORMAT(32HO EBAY1 EBAY2 SUBLIM )
940 FORMAT(18H CASE DID NOT RUN )
941 FORMAT(1H 4F10.1)
950 FORMAT(20HO OPTIMUM CONDITION F8.1,5H WC /50H TOTEQWT TRD
TINHXO TOTPW TOTWT)
951 FORMAT(1H 5F10.1)
952 FORMAT(32H FLOW RATE LOOP DID NOT CONVRGE)
953 FORMAT(1H 6F10.1)
954 FORMAT(40HO TOTEQWT TINHXO TOTPW TOTWTF8.1,5H WC F8.2

```

CHART TITLE - NON-PROCEDURAL STATEMENTS

```

,4H TR0)
955  FORMAT(28HO OPTIMUM CONDITIONS SUMMARY/60H  TOTEQMT      WC
      TR0  TINHXO  TOTPW  TOTWT)
960  FORMAT(13HO OUTPUT DATA)
970  FORMAT(1H 11F10.1)
975  FORMAT(12HO HEAT LOADS/119H  CONDMX  SENSMX  INTERMX  FUELCEL
      L RADIATOR  EXP MX  TOTLAT  SENSCO2  LATCO2  SENSHZDP  LA
      TH2DP  QSINK  )
985  FORMAT(1H F8.1,8H CYCLE  F8.1,8H QEBZ  )
981  FORMAT(1H 15F8.3)
982  FORMAT(1H F8.2,8H QCHIL  F8.3,8H TOLQ  F8.1,8H WF/C  F8.1,8H KEY
      SK  F8.1,8H WCOOL  F8.1,8H TIFXI  F8.2,8H TIMECY  F8.2,8H TIMESB  /
      1H F8.2,8H TFCI  F8.2,8H TFCO  F8.1,8H NUBFRM  F8.4,8H EMIS
      F8.1,8H STEP  F8.2,8H TORBIT  F8.1,8H PERF  )
983  FORMAT(1HO'RADIATOR/EVAPORATOR EXPENDABLE USAGE NOT CONVERGED'/1H
      F8.1,8H TRADIN  F8.1,8H TEVAPD  F8.1,8H QEVAP  F8.1,8H TRADO
      F8.1,8H QTOT  )
984  FORMAT(1H1'RADIATOR/EVAPORATOR EXPENDABLE USAGE'/1H F8.1,8H QTOT
      F8.1,8H WEVAVG  F8.1,8H NO.STEP  )
985  FORMAT(12HO ORBIT STEP  *  1/16  2/17  3/18  4/19  5/20
      6/21  7/22  8/23  9/24  10/25  11/26  12/27  13/28  1
      4/29  15/30')
986  FORMAT(11H WEVAPORANT  15F8.2/11H  15F8.2 )
9861  FORMAT(11H T RAD IN  15F8.2/11H  15F8.2 )
9862  FORMAT(11H T SINK  15F8.2/11H  15F8.2 )

9863  FORMAT(11H TEVAP OUT  15F8.2/11H  15F8.2 )
997  FORMAT(11H OFF TABLES  1518 /11H  1518 )
989  FORMAT(1HO'COMPONENT POWERS -WATTS'/1H 15F8.2 )

```


CHART TITLE - NON-PROCEDURAL STATEMENTS

```
      DIMENSION FWT(15),FXW(15),SWT(15)
      DIMENSION
      CFT(30)
      COMMON X(700),LA,NPER,PP
      EQUIVALENCE
      (X(101),FWT(1)),(X(131),FXW(1)),(X(161),SWT(1))
      EQUIVALENCE (X(60),FCO2),(X(61),FNCO2) ,
      (X(221),CFT(1)) ,(X(100),PERF) ,(X(10),WCO2)
      ,(X(11),TCAB ) ,(X(77),FRESH)
23  FORMAT(1HOF8.1,8H NO.CAR F8.2,8H MVALVE F8.2,8H LIOHWT )
20  FORMAT(1H1 *LIOH SUBROUTINE-CO2 PARTIAL PRESSURES*/F8.3,' PMAX '
      ,F8.3,' PMIN ',F8.1,' QS ',F8.1,' QL ' )
```

CHART TITLE - INTRODUCTORY COMMENTS

COND HX SUBROUTINE

CHART TITLE - SUBROUTINE CHX(QS,QL,TC,TCI,WCPC,RHO,CPA,PMAX,DPF,TAO,J,QCS,V,PW,

```

-----
/ 76 /
-----
I
41.10---)I
I 01
I NT = 1 I
I I = 0 I
-----
I
I
ENTER OPTIMAZIATION
LOOP
I
41.11---)I
77 I NOTE 02
* * * * *
* BEGIN DO LOOP *
* 100 N = 1, NT *
* * * * *
I
46.06---)I
I 03
I COMPUTED GO TO I
I FOR L I
-----
I 21 42.04 I
I 22 43.01 I
-----
I
I
IF OUTSIDE THE RANGE
I
I
HX LOES TOTAL Q
21 VOLUME FLOW REQ
I
42.03---)I
21 I 04
-----
I V = QS/ITC - I
I TAO1/RHO/CPA I
-----
I
I

```

```

RH TOO HIGH
-----) *
I 32 I 12
I I = 1 I
-----
I
I
CABIN DFW PT.
I
-----) I
I 31 I 13
I I I H
I I I H
I I KANDK I H
I I (PX1,TDP,1) I H
I I I H
I I I H
-----
I
I
I 14
...
.43.13.
... 33

```

```

HX LUTLET WATER VAPOR
PRES
I
I 05
-----
I I KANDK H
I I (PX0,TAO + H
I I 459.6,2) H
I I H
-----
I
I
H2O LEAVING HX
I
I 06
-----
I WWC = I
I (PX0/0.595/(TAO + I
I 459.6)) * V I
-----
I
I
WATER ENTERING
I
I 07
-----
I Ww1 = WWC + WH2O I
-----
I
I
INLET VAPOR PRES
I
I 08
-----
I PX1 = I
I Ww1*0.595*(TAO + I
I 459.6)/V I
-----
I
I

```

```

-----) *
I 09
-----
I I KANDK H
I I (PX1,TDP,1) H
I I H
I I H
-----
I
I 10
-----
I PX1 = I
I Ww1*.595*TDP/V I
-----
I
I
IS RH OK
I
I 11
* * * * *
* PX1 - PMAX * (-/0)
* * * * *
I (+)
I
I

```

CHART TITLE - SUBROUTINE CHX(QS,QL,TC,TCL,WPCPC,RHO,CPA,PMAX,DPF,TAO,J,QCS,V,PM,

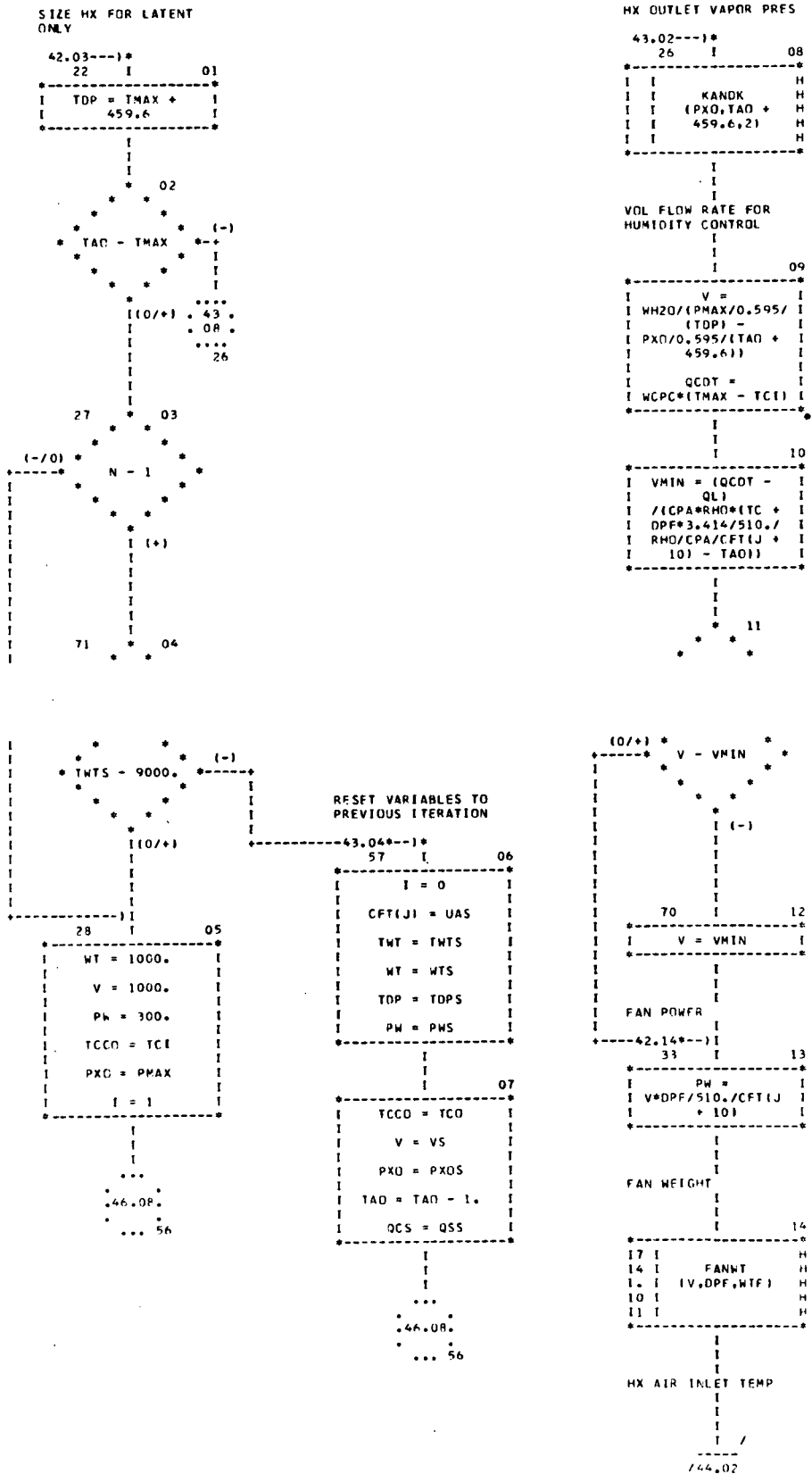
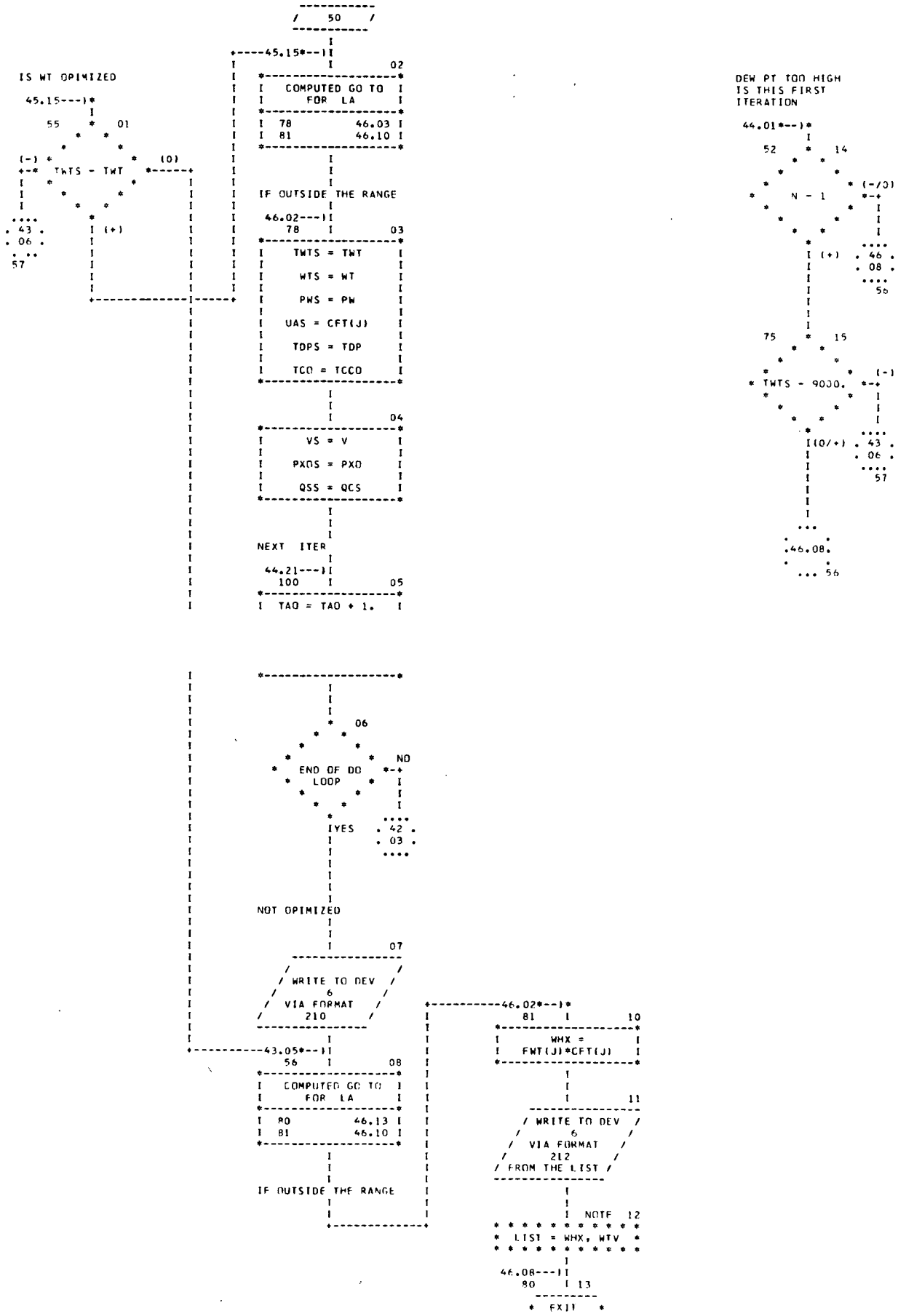


CHART TITLE - SUBROUTINE CHX(QS,QL,TC,TCI,WCPC,RHO,CPA,PMAX,DPF,TAO,J,QCS,V,PW,



F

CHART TITLE - NON-PROCEDURAL STATEMENTS

```
      DIMENSION FWT(30),FXW(30),SWT(30)
      ,CFT(30)
      COMMON X(700),LA,NPER ,PP
      EQUIVALENCE
      (X(101),FWT(1)),(X(131),FXW(1)),(X(161),SWT(1))
      ,(X(221),CFT(1))
211  FORMAT(20H REHEATER REQUIRED /1H F8.1,8H TAO   F8.1,8H VOL
      F8.1,8H QSENS   )
215  FORMAT(20H TEMPERATURE PINCH /1H F8.1,8H TAO   F8.1,8H V
      F8.1,8H QCS   )
212  FORMAT(11H0*CONDENSER WEIGHTS*,F8.2,8H WTHX   F8.2,8H MVALVE  )
210  FORMAT(29H NOT OPTIMIZED -TAO TOO LOW  )
```

CHART TITLE - INTRODUCTORY COMMENTS

DRY HX SUBROUTINE

CHART TITLE - NON-PROCEDURAL STATEMENTS

```
      DIMENSION FWT(15),FXW(15),SWT(15)
      ,CFT(30)
      COMMON X(700),LA,NPER
      EQUIVALENCE
      (X(101),FWT(1)),(X(131),FXW(1)),(X(161),SWT(1))
      ,(X(221),CFT(1))
30    FORMAT(1H0'SENSIBLE HX ',F8.2,8H WTHX  F8.2,8H MVALVE )
10    FORMAT(2H HX CANNOT BE BUILT  )
```

CHART TITLE - INTRODUCTORY COMMENTS

ELECTRONIC BAY COOLING SUBROUTINE

CHART TITLE - SUBROUTINE EBAY(QE,TE,TCI,MCPC,RND,CPA,PP,DP,WTHX,WTFAN,PM,V,TCO,

IS FIRST TIME OR TWT
DECREASING - STORE
VALUES

```

54.10*--)*
15 | | 01
|---|---|
| TWS = TWT | |
| WTHXS = WTHX | |
| UAS = UA | |
| WTFS = WTFAN | |
| WFS = WTF | |
| WKS = WTK | |
|---|---|

```

```

| | 02
|---|---|
| PMS = PW | |
| TCOS = TCO | |
| QTS = QT | |
| VS = V | |
|---|---|

```

END LOOP - STEP AIR
OUTLET TEMP

```

100 | | 03
|---|---|
| TAD = TAD + 2. | |
|---|---|

```

* 04

NOT FIRST TIME THRU
OR TWT INCREASING -
USE PREVIOUS VALUES

```

53.06*--)*
19 | | 10
|---|---|
| PM = PMS | |
| WTHX = WTHXS | |
| WTFAN = WTFS | |
| CFT(LF) = UAS | |
| TCO = TCOS | |
| QT = QTS | |
|---|---|

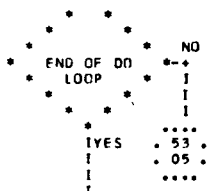
```

```

| | 11
|---|---|
| V = VS | |
| TAD = TAD - 2. | |
|---|---|

```

...
.55.05.
... 20



```

53.09*--)*
20 | | 05
|---|---|
| COMPUTED GO TO | |
| FOR LA | |
| 21 55.09 | |
| 22 55.06 | |
|---|---|

```

IF OUTSIDE THE RANGE

```

55.05*--)*
22 | | 06
|---|---|
| WTX = FWT(LF)*UAS | |
|---|---|

```

```

| | 07
|---|---|
| WRITE TO DEV | |
| VIA FORMAT | |
| FROM THE LIST | |
|---|---|

```

```

| NOTE 08
| * * * * *
| * LIST = WTX, WFS, *
| * WKS *
| * * * * *
|
| 55.05*--)*
| 21 | 09
|---|---|
| * EXIT *
|---|---|

```

CHART TITLE - NON-PROCEDURAL STATEMENTS

```
DIMENSION FWT(30),FXW(30),SMT(30)
,CFT(30)
COMMON X(700),LA,NPER
EQUIVALENCE (X(101),FWT(1)),(X(131),FXW(1)),(X(161),SMT(1))
,(X(221),CFT(1))
23  FORMAT(1H0'AVIONICS BAY ',F8.2,8H WTHX  F8.2,8H WTFAN  F8.2,8H WT
CK  )
10  FORMAT(22H HX CANNOT BE BUILT  )
```

10/12/72

AUTOFLOW CHART SET - H247B

SP 01T72
PAGE 57

CHART TITLE - INTRODUCTORY COMMENTS

HSC ROUTINE

CHART TITLE - SUBROUTINE HSC(WC02,QLAT, DAY,RHO,PVI,PD,L,MT,PN,V,WB,MU,VCH,WF)

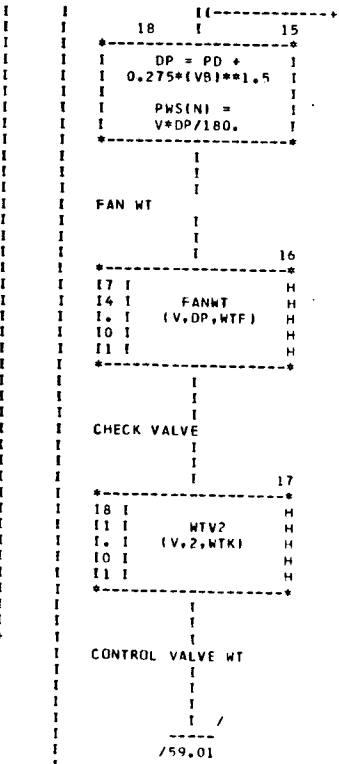
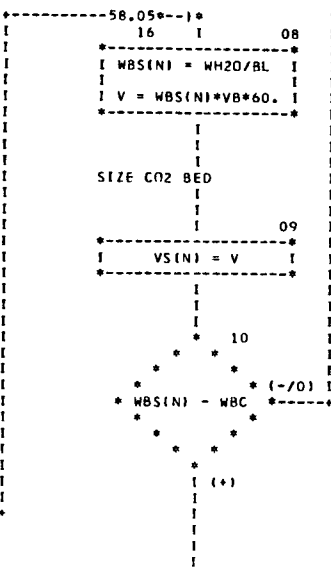
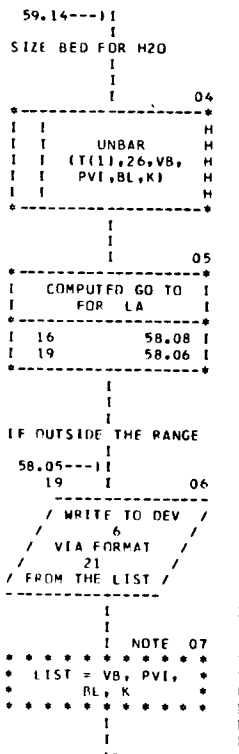
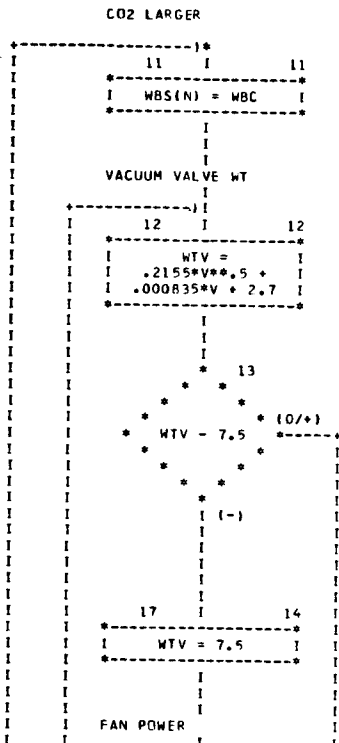
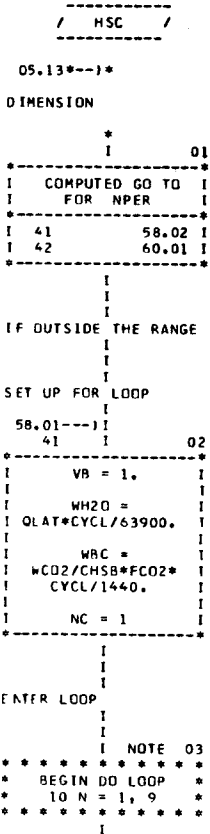


CHART TITLE - NON-PROCEDURAL STATEMENTS

```

DIMENSION FWT(30),FXW(30),SWT(30)
,PHS(10),WTS(10),WBS(10),WUS(10),WFS(10),VSI(10),WTSYS(10)
,T(100),CFT(30)
COMMON X(700),LA,NPER,PP
EQUIVALENCE
(X(101),FWT(1)),(X(131),FXW(1)),(X(161),SWT(1)),(X(63),CHSB)
,(X(64),EH20),(X(160),FCO2),(X(65),CYCL)
,(X(40),T(1)),(X(1),TCAB),(X(221),CFT(1))
21  FORMAT(14H BED LOADING 3F10.3,12 )
70  FORMAT(1H F8.2,8H WTCAN F8.2,8H WVAL F8.2,8H WCVL F8.2,8H WTF
AN F8.2,8H WKVAL )
22  FORMAT(1H 6F10.2)
101  FORMAT(1H0'HSC WATER LOOP NOT CONVERGED*/1H F8.2,8H WH20 F8.2,8H
WH20C F8.2,8H VOLF F8.4,8H PVI F6.4,8H BEDLD )
102  FORMAT(1H0'CO2 LOOP NOT CONVERGED*/1H F8.3,8H WCO2CY F8.1,8H FLOW
F8.3,8H PCO2 F8.3,8H BLOADR F8.3,8H BLOADC 13,8H OFFTAB )
103  FORMAT(1H0'HSC PERFORMANCE */1H F8.1,8H VREQ F8.1,8H VAVAIL F8.4
,8H PVI F8.2,8H IDEWPT F8.3,8H PCO2 12,12,8H OFFTAB )
20  FORMAT(19H NOT CONVERGED HSC / 2F8.2 )

```


CHART TITLE - SUBROUTINE CONT(J,DP,DAY,WT,V,QSC)

/ CONT /

03.05---)*

VOL FLOW RATE

```

      *
      I
      I 01
-----*
I V = WCD2*300. I
-----*
    
```

BED WEIGHT

```

      I
      I
      I 02
-----*
I WTB = I
I DAY*WCD2*.11R I
-----*
    
```

VALVE WEIGHT

```

      I
      I
      I 03
-----*
I8 I H
I1 I WTV2 H
I. I (V,2,WTV) H
I0 I H
I1 I H
-----*
    
```

TOTAL WT

```

      I
      I
      I 04
-----*
I WT = I
I (WTB*FMT(J) + I
I WTV + I
I FXW(J))*SWT(J) I
-----*
    
```

FAN HEAT LOAD

```

      I
      I
      I 05
-----*
I QSC = 0. I
-----*
    
```

```

      I 06
-----*
* EXIT *
-----
    
```

CHART TITLE - NON-PROCEDURAL STATEMENTS

```
DIMENSION FWT(15),FXW(15),SMT(15)
,CFT(30)
COMMON X(700),LA,NPER,PP
EQUIVALENCE
(X(101),FWT(1)),(X(131),FXW(1)),(X(161),SMT(1))
,(X(221),CFT(1)),(X(10),MCO2)
```

CHART TITLE - INTRODUCTORY COMMENTS

DOUBLE ELECTRONIC BAY COOLING SUBROUTINE

CHART TITLE - SUBROUTINE EBAY2(QB1,QB2,TE,TC1,WPCP,RHO,CPA,PP,DP,WTHX,MTFAN,PW,

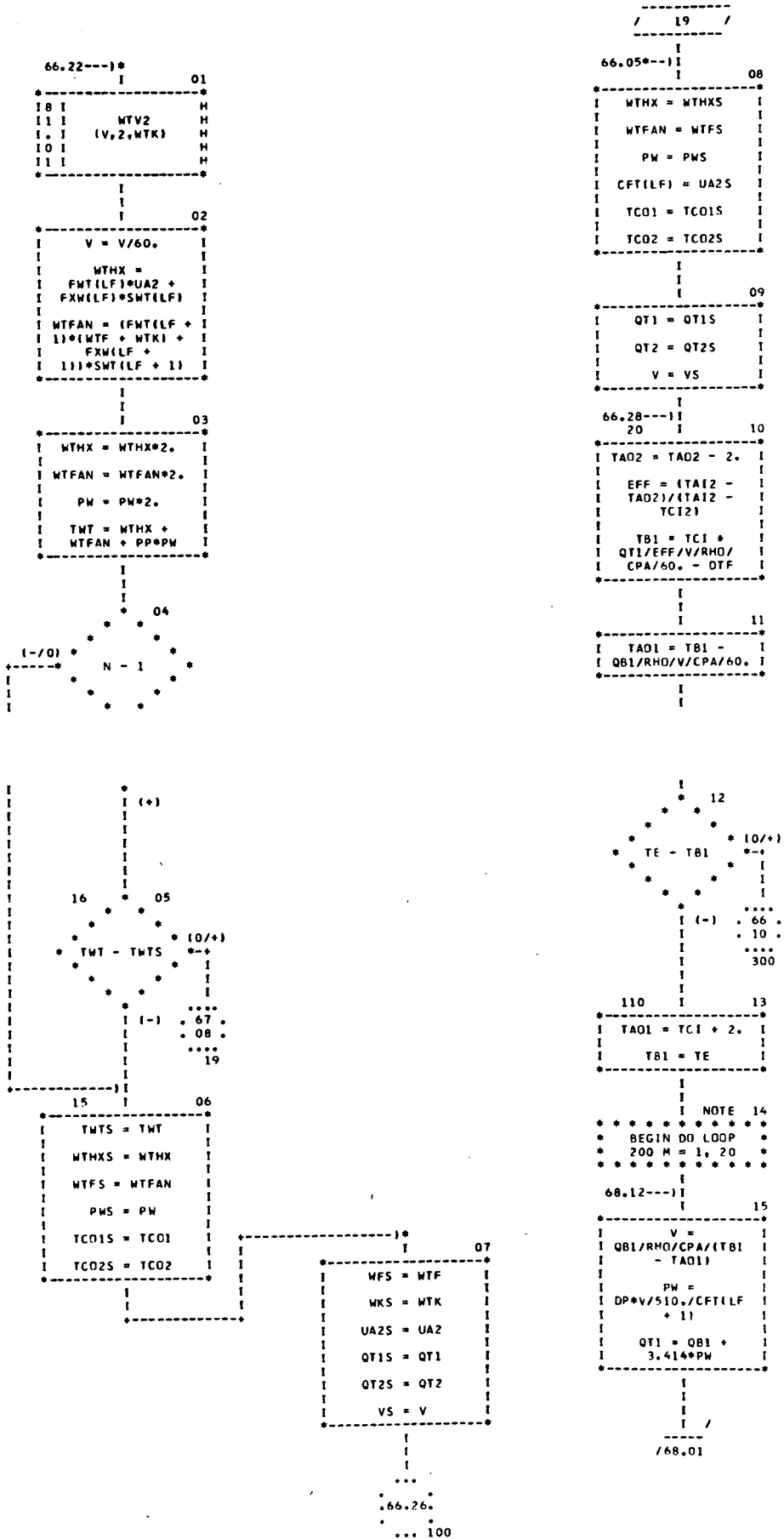


CHART TITLE - SUBROUTINE EBAY2(QB1,QB2,TE,TC1,WCPC,RHO,CPA,PP,DP,WTHX,WTFAN,PW).

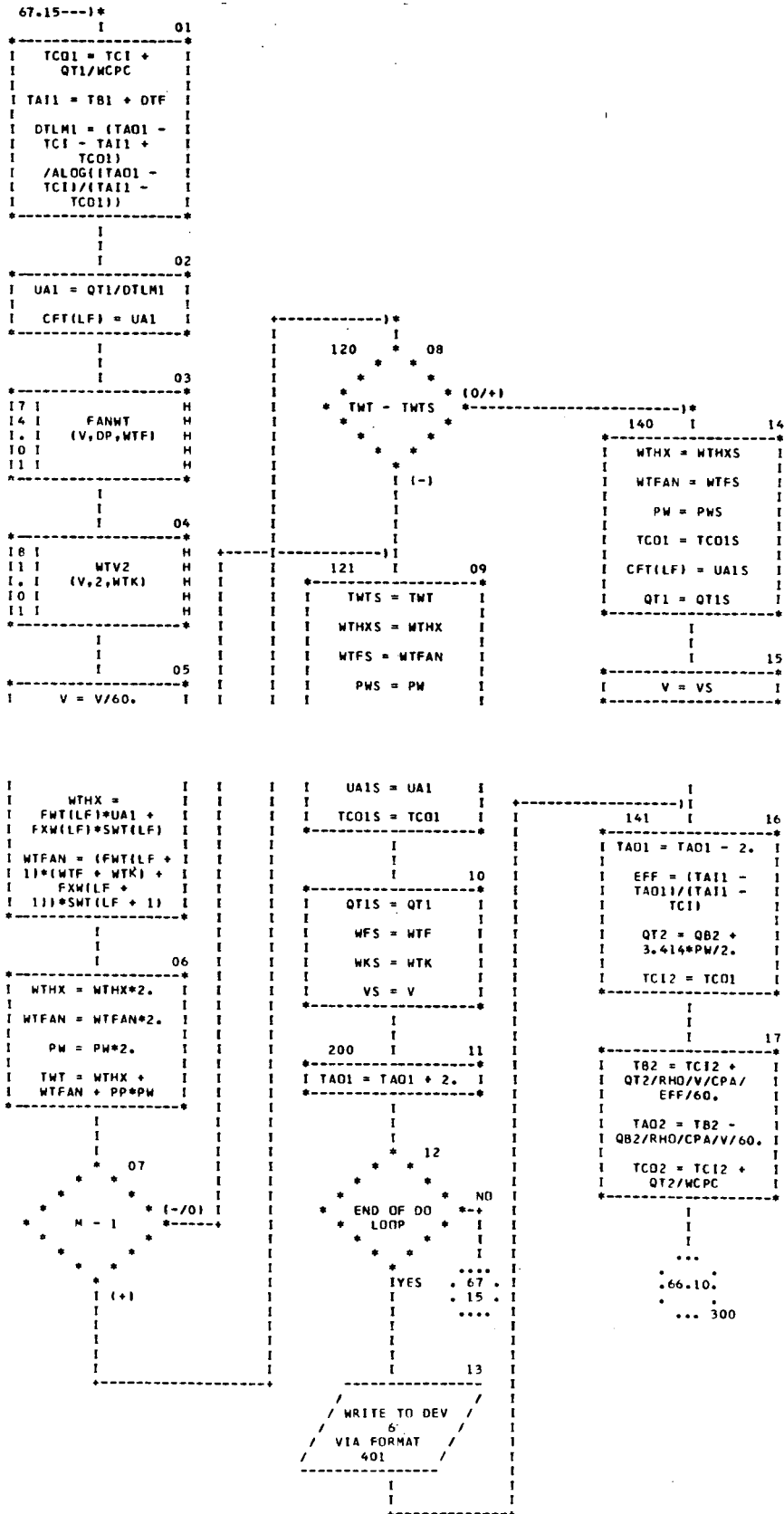


CHART TITLE - NON-PROCEDURAL STATEMENTS

```
DIMENSION FWT(30),FXW(30),SWT(30)
,CFT(30)
COMMON X(700),LA,NPER
EQUIVALENCE (X(101),FWT(1)),(X(131),FXW(1)),(X(161),SWT(1))
,(X(221),CFT(1))
403  FORMAT(1H 'DOUBLE EBAY ',F8.2,' WTHX ',F8.2,' WTFAN ',F8.2,' WTKV
' )
400  FORMAT(22H EBAY2 NOT OPTIMIZED )
401  FORMAT(22H EBAY1 NOT OPTIMIZED )
402  FORMAT(26H EBAY HX CANNOT BE BUILT )
```

CHART TITLE - INTRODUCTORY COMMENTS

FLASH EVAP SUBROUTINE

CHART TITLE - SUBROUTINE FEVAP (Q, WCP, TCI, L, TCO, WT)

LAST ITERATION-PRINT

```

71.09---)*
15 I 01
-----
WRITE TO DEV
 6
VIA FORMAT
51
FROM THE LIST
-----
I
I NOTE 02
*****
* LIST = QR, TCI, *
* TCO, WH2O, WT *
*****
I
71.09*---)I
14 I 03
-----
* EXIT *
-----

```

PERFORMANCE -MINIMUM
OUTLET TEMP

```

71.01*---)*
11 I 04
-----
I TOMIN = 30. + I
I Q/CFT(L) I
-----
I
I

```

IS TEMP TOO LOW

```

05
* TOMIN - 34. (-) *

```

TOO LOW

```

16 I 06
-----
I TOMIN = 34. I
-----

```

MAXIMUM OUTLET TEMP

```

17 I 07
-----
I TOMAX = TCI - I
I Q/WCP I
-----

```

USE LIMITING TEMP

```

08
* TOMAX - TOMIN (-/0) *

```

USE MIN TEMP

```

19 I 09
-----
I TCO = TOMIN I
-----

```

```

...
.72.10.
... 18

```

USE MAX TEMP

```

72.08---)*
18 I 10
-----
I TCO = TOMAX I
-----

```

HEAT LOAD REJECTED

```

20 I 11
-----
I QR = WCP*(TCI - I
I TCO) I
-----

```

WATER USED

```

12
-----
I WH2O = I
I QR/965.*TSUB I
-----

```

PRINT

```

13
-----
WRITE TO DEV
 6
VIA FORMAT
52
FROM THE LIST
-----

```

NOTE 14

```

*****
* LIST = QR, TCI, *
* TCO, TOMAX, *
* TOMIN, WH2O *
*****

```

RETURN

```

15
...
.72.03.
... 14

```

FORMATS

CHART TITLE - NON-PROCEDURAL STATEMENTS

DIMENSION FMT(30),FXW(30),SWT(30),CFT(30)

COMMON X(700),LA,NPER,PP

EQUIVALENCE

(X(101),FMT(1)),(X(131),FXW(1)),(X(161),SWT(1)),(X(221),CFT(1))

,(X(100),PERF),(X(74),TSUB)

51 FORMAT(1H0'FLASH EVAPORATOR SIZE '/1H F8.1,8H QREJ F8.2,8H TCIN

F8.2,8H TCOUT F8.1,8H WH2D F8.2,8H WEIGHT)

52 FORMAT(1H0'FLASH EVAPORATOR PERFORMANCE'/1H F8.1,8H QREJ F8.2,8H

TCIN F8.2,8H TCOUT F8.2,8H TOMAX F8.2,8H TOMIN F8.1,8H WH2D

)

10/12/72

AUTOFLOW CHART SET - H2470

SP 01T72
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CHART TITLE - INTRODUCTORY COMMENTS

CRYOGENIC HX SUBROUTINE

CHART TITLE - SUBROUTINE CRY(Q,WH,TIN,NC,WH2)

/ CRY /

23.03---)*

OUTLET HOT TEMP

01
I THO = TIN - Q/WH I

FIRST GUESS OF H2
FLOW RATE-OUTLET TEMP

02
I TH20 = (TIN + THO)/2. I

ENTER LOOP

NOTE 03
* BEGIN DO LOOP *
* 10 N = 1, 10 *
* * * * *

76.13---) I
FLOW RATE-MASS

04
I WC = Q/(TH20 + 420.) I

CALL HX SUB

NO -H2 OUTLET TEMP

76.06---)*
3 I 12
I TH20 = TH20 - TOC + THO I

10 * 13
* * * * *
* END OF DO LOOP *
* * * * *

YES 76
04

NOT CONVERGED

14
WRITE TO DEV
6
VIA FORMAT
50
FROM THE LIST

NOTE 15
* LIST = THO, TOC, *
* WC, Q, TIN *
* * * * *

05
I 17 I H
I 19 I HX H
I 10 I (Q,WH,WC, - H
I 11 I 420.,NC,TOC) H

IS TEMP CONVERGED

06
* ABS(THO - TOC) - 3. *
* (-/0) *
* * * * *

(+)
76.12
3

CONVERGED PRINT

2 I 07
I WH2 = WC/3.12 I

IS THIS LAST
ITERATION

08
I COMPUTED GO TO I
I FOR LA I
I 20 76.11 I
I 4 76.09 I

IF OUTSIDE THE RANGE

PRINT
76.08---) I
4 I 09

WRITE TO DEV
6
VIA FORMAT
51
FROM THE LIST

NOTE 10
* LIST = TOC, WH2, *
* TH20 *
* * * * *

76.08---) I
20 I 11
* EXIT *

10/12/72

AUTOFLOW CHART SET - H247B

CHART TITLE - NON-PROCEDURAL STATEMENTS

DIMENSION CFT(30)

COMMON X(700),LA,NPER,PP

EQUIVALENCE (X(221),CFT(1))

50 FORMAT(1H0°CRYOGENIC HX NOT CONVERGED*/1H F8.2,8H THO F8.2,8H T
HOC F8.2,8H WH2CP F8.2,8H OCRY F8.2,8H TIN)
51 FORMAT(1H0°CRYOGENIC HX PERFORMANCE*/1H F8.2,8H THDTCAL F8.2,8H WH
YD F8.2,8H THYDD)

CHART TITLE - INTRODUCTORY COMMENTS

HX OFF DESIGN PERFORMANCE -SENS HXS

10/12/72

AUTOFLOW CHART SET - M2478

CHART TITLE - SUBROUTINE MX(Q,WH,WC,TCI,NCOMP,THO)

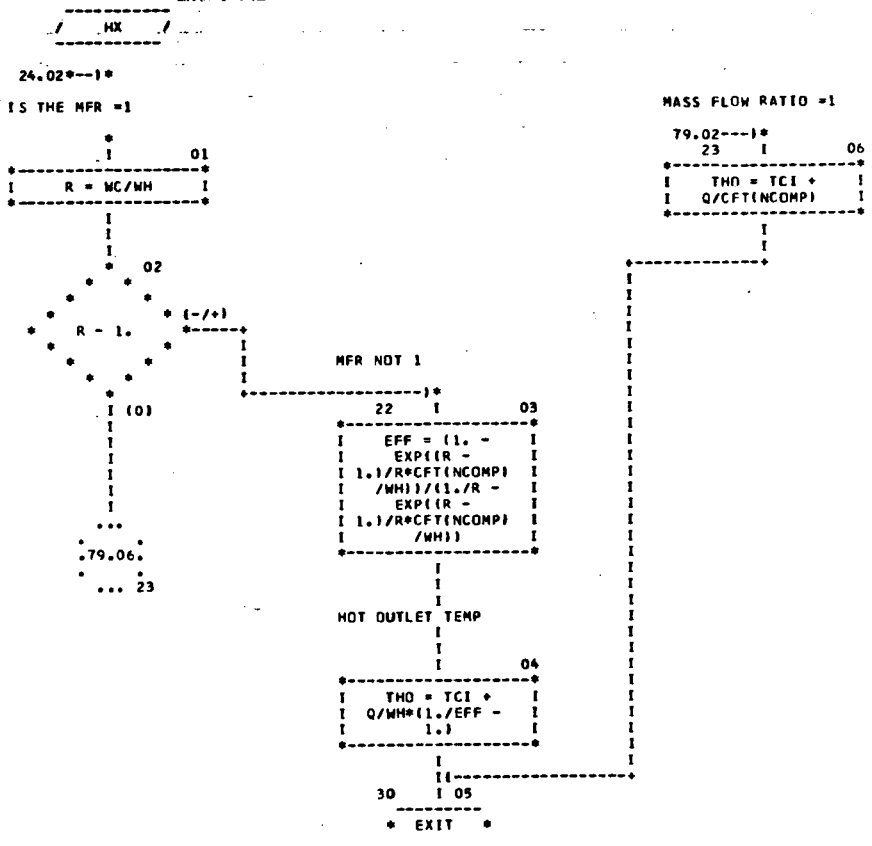


CHART TITLE - NON-PROCEDURAL STATEMENTS

DIMENSION CFT(30)
COMMON X(700),LA,NPER,PP
EQUIVALENCE (X(221),CFT(1))

CHART TITLE - SUBROUTINE RADIT1,T2,WCP,WR,AR,WE,TY,J1

OUTLET TEMP TOO HIGH

```

82.09---)*
15 | 01
| TY = TS + 6. |
|-----|
82.09---)|
16 | 02
| TO = (TY - 5.)/TS |
| BETA = B*TS**3. |
|-----|

```

ENTER LOOP TO
CALCULATE REQUIRED
AREA

```

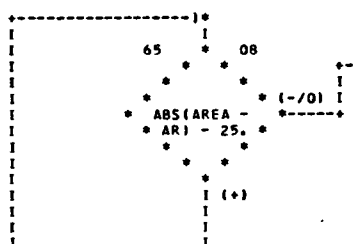
| NOTE 03
|-----|
| *****
| BEGIN DO LOOP
| 25 I = 1, 100
| *****
|-----|

```

```

83.17---)|
| Q PER UNIT AREA
|-----|
| 04
| QA = ALPHA*(T1 -
| TY)
| /((.25*ALOG((T2 +
| 1.)/(T0 - 1.)) +
| .5*ATAN(T0) -
| ZETA +
| BETA*ALOG((T1**4.
| - 1.)/(T0**4. -
| 1.)))
|-----|

```



```

| LOOP CONVERGED
| -RADIATOR WT
|-----|
| 83.08---)*
| 68 | 11
| AR = AREA
|-----|
| 11 | 12
| WR =
| AR*SMT(J)GFXW(J)
|-----|

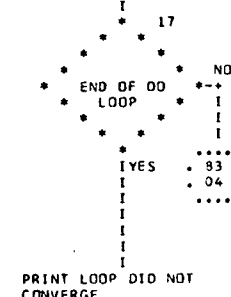
```

AREA TOO SMALL -
INCREASE HEAT LOAD

```

83.09---)*
67 | 15
| TY = TY - 1.
|-----|
83.14---)|
25 | 16
| TO = (TY - 5.)/TS
|-----|

```



```

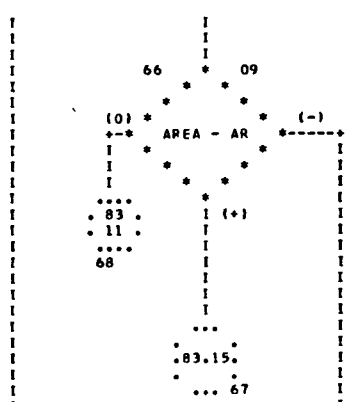
| PRINT LOOP DID NOT
| CONVERGE
|-----|
| WRITE TO DEV
| 6
| VIA FORMAT
| 50
| FROM THE LIST
|-----|
| 18

```

```

| 05
| AR = WCP*(T1 -
| TY)/QA
|-----|
| COMPARE WITH AREA
|-----|
| 06
| COMPUTED GO TO
| FOR NPER
| 63 83.07
| 64 83.10
| 64 83.10
|-----|

```



```

| IS THIS THE LAST
| ITERATION
|-----|
| 13
| LA - 1
|-----|
| 11 | 12
| WR =
| AR*SMT(J)GFXW(J)
|-----|

```

```

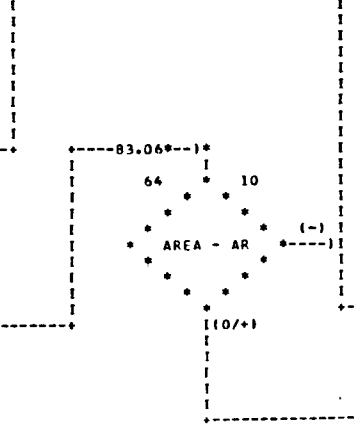
| NOTE 19
| *****
| LIST = T1, T2,
| TS, TY
| *****
|-----|

```

```

83.06---)|
63 | 07
| FRAD = 1.
|-----|
| 10/+
|-----|
| 10

```



```

83.09---)*
10 | 14
| TY = TY*.
|-----|
| 10

```

```

| PRINT-LAST
|-----|
| 12 | 20
| WRITE TO DEV
| 6
| VIA FORMAT
| 51
| FROM THE LIST
|-----|
| NOTE 21
| *****
| LIST = T1, T2,
| TY, AR, AMAX, WR
| *****
|-----|
| 82.07---)|
22 | 22
| * EXIT *
|-----|

```

CHART TITLE - NON-PROCEDURAL STATEMENTS

```
DIMENSION FWT 15(,FXW 15(,SWT 15(
,CFT(30)
COMMON X(700),LA,NPER,PP
EQUIVALENCE
(X(101),FWT(1)),(X(131),FXW(1)),(X(161),SWT(1))
, X 39(,FW9(, X 40(,FW10(, X 47(,TS(, X 49(,AMAX(, X 50(,FEXP(
, X 221(,CFT 1((, X 78(,EMIS(, X 59(,FRAD(, CFT 7(,AACT(
51 FORMAT(1H0' RADIATOR SUBROUTINE '/F8.2,' TIN ',F8.2,' TOUT ',F8.2,
' TOUTC ',F8.2,' ARADC',F8.2,' ARMAX',F8.2,' WTREQ ' )
50 FORMAT(1H0'RAD NOT CONVG'/F8.2,' TIN ',F8.2,' TOUT ',F8.2,' TSINK
',F8.2,' TOUTC ' )
```

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AUTOFLOW CHART SET - M247B

SP 01T72
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CHART TITLE - INTRODUCTORY COMMENTS

CONDENSER PERFORMANCE SUBROUTINE

CHART TITLE - SUBROUTINE CX2(MC,TCl,QS,QL,TC,QS2,QL2,V,P,NL,K,TCO,V11,I,QSX)

```

-----
/ CX2 /
-----
I 25.02---)I
I
I 01
I QM = QSM + QLM
I
I
I=0
AIR DENSITY
I
I
I 02
I RHO =
I PCAB/RA/(TC +
I 459.6)*144.
I
I WF = V11*RHO*CPA
I
I TFI = TC +
I QCAV/WF + 459.6
I
I
I 03
I RHO = RHO*(TC +
I 459.6)/TFI
I
I
MAX AIR FLOW RATE
I
I
I 04
I WAM = V*RHO*CPA
I
I WF = V11*RHO*CPA
I
I
FIRST GUESS OF HX AIR
FLOW
I

```

```

I
I 05
I WH = WAM
I
I
H2O CONDENSED
I
I
I 06
I WH2O = (QL +
I QL2)/1065.
I
I
MIN AIR OUTLET TEMP
I
I
I 07
I TMIN = TCl + 2.
I
I
FAN HEAT LOAD
I
I
I 08
I QF = P*3.414
I
I
MAX HX SENS LOAD
I

```

```

-----
I 10
I QSMAX = QS +
I QS2 + QCAV
I
I
IS THIS A SINGLE HX
SYSTEM
I
I
I 11
I K
I
I (+)
I
I
I 102
I
I
I 103
I

```

```

-----
SINGLE HX-TAI
-----
I 101 I 12
I
I TAI = TC + (QF +
I QCAV)/WF + QS2/WH
I
I
I
I
I
I

```

```

I
I
AIR OUTLET TEMP
I
I
I 13
I
I TAO = TAI -
I QSMAX/WH
I
I
SET SENS LOAD=MAX
I
I
I 14
I
I QSX = QSMAX
I
I MA = 0
I
I MB = 0
I
I
IS TAO TOO LOW
I
I
I 15
I
I TAO - TMIN (-)
I
I
I (10/+)
I
I 87
I 01
I 104
I
I
I 1041 I 16
I
I M = 0
I
I
I
I
I
I
I 86.17
I
I 87.05
I
I 102
I 103

```

```

DUAL HX ASSUME TAO
I
I 86.11---)*
I 102 I 17
I
I TAO = TCl + 5.
I
I
I
SET HX AIR FLOW
I
I
I 18
I
I WH = WAM
I
I
I
CAL HX INLET TEMP
I
I
I 19
I
I TAI = TC +
I QF/WF + QS2/WH
I
I
I
CAL SENS LOAD
I
I
I 20
I
I QSX = WH*(TAI -
I TAO)
I
I
I
CAL HX UA
I
I
I 21
I

```

...
.87.05
... 103

CHART TITLE - SUBROUTINE CX2(MC,TC1,QS,QL,TC,QS2,QL2,V,P,NL,K,TCO,V11,I,QSX)

INCREASE CABIN TEMP
CHANGES TO CX2
SUBROUTINE

```

88.07*--)*
112 I 01
-----
19 I H
14 I QMET H
1. I (QSM,TC,TC + H
10 I 1.,QSN,KL) H
11 I H
-----

```

NEW SENSIBLE LOAD

```

-----
1 QS = QS + QSN - I
1 QSM I
-----

```

NEW LATENT LOAD

```

-----
1 QL = QL + QSM - I
1 QSN I
-----

```

NEW MAX HEAT LOAD
SENSIBLE

```

-----
1 QSMAX = QSMAX + I
1 QSN - QSM I
-----

```

```

1 QSX = QSX + QSN - I
1 QSM I
1 QSN = QSN I
-----

```

NEW H2O REMOVAL

```

-----
1 WH2O = (QL + I
1 QL2)/1065. I
-----

```

UP CABIN TEMP

```

-----
1 TC = TC + 1. I
-----

```

AIR INLET TEMP

```

-----
1 TAI = TC + (QF + I
1 QCAV)/WF + I
1 QS2/WAM I
1 TAO = TAI - I
1 QSMAX/WAM I
-----

```

...
.92.15.
... 200

TWO HXS IS HX TOO
SMALL

```

90.01---)*
106 I 08
-----
(0) * UAR - CFT(NL) (-) I
-----
.89 I (+)
.11 I
250 I
-----

```

HX TOO SMALL-LOWER QS

```

-----
113 I 09
1 TAO = TCI + I
1 (TAO - I
1 TCI)*UAR/CFT(NL) I
-----

```

HX TOO LARGE -RAISE Q
IS TAO TOO LOW

```

-----
114 I 10
-----
* TAO - TAIMIN (-/0) *
-----
.89 I (+)
.11 I
250 I
-----

```

IS OUTLET TEMP TOO
LOW

```

(0/+) *
116 I 11
1 TAO = TCI + I
1 (TAO - I
1 TCI)*UAR/CFT(NL) I
-----
12
(0/+) *
1 TAO - TAIMIN *
-----
1 (-)

```

```

118 I 13
1 TAO = TAIMIN I
-----

```

```

119 I 14
1 QSX = WH*(TAI - I
1 TAO) I
-----

```

END OF LOOP

87.20*--)

```

200 I 15
-----
* END OF DO *
* END OF LOOP *
-----

```

YES
87
06
....

LOOP NOT
CONVERGED-PRINT

```

16
WRITE TO DEV
VIA FORMAT
701
FROM THE LIST
-----

```

```

I NOTE 17
* * * * *
* LIST = UAR, *
* CFT(NL), TAI, *
* TAO, WH, WAM, *
* QSX, QSM, QL *
* * * * *

```

```

SET I
-----
18
1 I = 1 I
-----

```

... 89.19.
... 300

CHART TITLE - NON-PROCEDURAL STATEMENTS

```
DIMENSION FWT(30),FXW(30),SMT(30),CFT(30)
COMMON X(700),LA,NPER,PP
EQUIVALENCE
(X(101),FWT(1)),(X(131),FXW(1)),(X(161),SMT(1)),(X(221),CFT(1))
,(X(48),TOLQ),(X(2),PCAB),(X(3),RAI),(X(48),CPA)
,(X(12),QSM),(X(14),QLM),(X(84),QCAV )
703 FORMAT(1H 6F10.2)
701 FORMAT(1H0 'CONDENSER NOT CONVERGED '/F8.1,'UAREQ ',F8.1,' UAAYAI
L ',F8.2,' TAI ',F8.2,' TAO ',F8.1,' WAIR ',F8.1,' WAMAX
',F8.1,8H QSEN /1H F8.1,8H QSMET F8.1,8H QLMET )
702 FORMAT(1H0 'CONDENSER PERFORMANCE '/ F8.2,' TCAB ',F8.2,' TAIRI
',F8.2,' TAIR0 ',F8.1,' HXCFM ',F8.2,' TDPCAB ',F8.1,' QSENS '
,F8.1,8H QSMET F8.1,8H QLTOT /F8.2,8H TFANI F8.2,8H TFANO )
```


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AUTOFLOW CHART SET - H2470

CHART TITLE - NON-PROCEDURAL STATEMENTS

COMMON X17001,LA,NPER,PP