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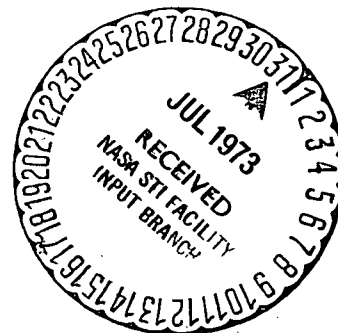
MONOPROPELLANT HYDRAZINE RESISTOJET

FLIGHT APPLICATION DESIGN TASK SUMMARY REPORT

**TRW SYSTEMS GROUP
ONE SPACE PARK
REDONDO BEACH, CALIFORNIA 90278**

MARCH 1973

**Prepared for
GODDARD SPACE FLIGHT CENTER
GREENBELT, MARYLAND 20771**



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Prepared by Charles K. Murch Approved by Dennis Asato
Charles K. Murch Dennis Asato

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FOREWORD

This is the sixth and final Task Summary Report submitted under Contract NAS5-11477, "Design, Development, and Testing of Engineering Model Nominal 20-Millipound Thrust Monopropellant Hydrazine Resistojet." The program originated in the Auxiliary Propulsion Branch of the NASA/Goddard Space Flight Center. Mr. Dennis Asato is the Technical Officer for NASA/GSFC. Mr. Charles K. Murch is the Project Manager for TRW Systems Group.

TABLE OF CONTENTS

	<u>Page</u>
1.0 INTRODUCTION AND SUMMARY	1
2.0 RECOMMENDATIONS FOR FLIGHT DESIGN.	2
2.1 General Configuration for a Flight Application. . .	2
2.2 Potential Improvements to the Basic Design.	4
3.0 DRAWINGS	7
4.0 CONCLUSIONS.	18
5.0 REFERENCES	19

1.0 INTRODUCTION AND SUMMARY

The "Design, Development, and Testing of an Engineering Model Nominal 20-Millipound Thrust Monopropellant Hydrazine Resistojet Program" is directed toward the advanced development of an Electrothermal Hydrazine Thruster (EHT). The EHT decomposes hydrazine thermally and expands the decomposition products through a nozzle to provide the impulse necessary to fulfill spacecraft propulsive requirements. The thruster is capable of operation at pulse widths from 0.050 second to steady state and delivers specific impulse values up to about 230 seconds depending on the duty cycle. The program is comprised of six tasks including analyses, the generation of specifications and other documentation, design, fabrication and test, data correlation, and recommendations for the design of flight units. The first five tasks are summarized in references 1 through 7; this document includes drawings and specific recommendations for flight.

The Engineering Model EHT described in Reference 4 is considered to be flight worthy except for minor design concessions to facilitate testing. This thruster successfully demonstrated 300,000 cycles and 30 hours of steady state operation. The demonstrated lifetime and performance are considered adequate for many flight applications. During the course of the Engineering Model tests, however, areas of potential improvement to the design were noted. These are discussed in Section 2.0 of this report. Section 3.0 includes component and assembly drawings for the EHT.

2.0 RECOMMENDATIONS FOR FLIGHT DESIGN

The overall configuration of the Engineering Model EHT is shown in the cut-away drawing in Figure 1. The thermal, mechanical and electrical interfaces, in general, are compatible with an existing GSFC spacecraft (ATS-F) propulsion subsystem. The Engineering Model tests to which the EHT was subjected are believed to be more severe than the performance portion of the qualification tests required for that spacecraft. On the basis of these tests, the Engineering Model design is believed capable of flight qualification for many applications with a minimum of redesign effort. The next section of this report discusses those minor changes necessary for a flight application. Subsequent sections discuss improvements of a more general nature which are believed to be applicable to all small hydrazine thrusters — both electrothermal and catalytic.

2.1 General Configuration for a Flight Application

As indicated earlier, the overall configuration is compatible with an existing propulsion subsystem. A few minor design concessions were included in the Engineering Model design for ease of test and disassembly.

A chamber pressure tap was included for test purposes. Most flight applications would not require a pressure tap; this is reflected in the nozzle drawings in the next section. As an alternative, flight units could be fabricated and acceptance tested with a chamber pressure tap which could then be crimped, cut off, and welded shut prior to flight.

The outer canister of the EM-EHT (Engineering Model EHT) is a three-piece unit which retains the insulation package. For a flight application, the canister should be more structurally sound. This could be accomplished by spot welding after acceptance test. As an alternative, the outer canister could be manufactured as a one-piece cup which would be welded or bolted to the bracket after the acceptance test.

Finally, the heater lead wires should be provided with a strain-relief device. This could be accomplished with a standard electrical receptacle brazed to the outer canister or with an arrangement similar to that used on the valve as shown in Figure 1.

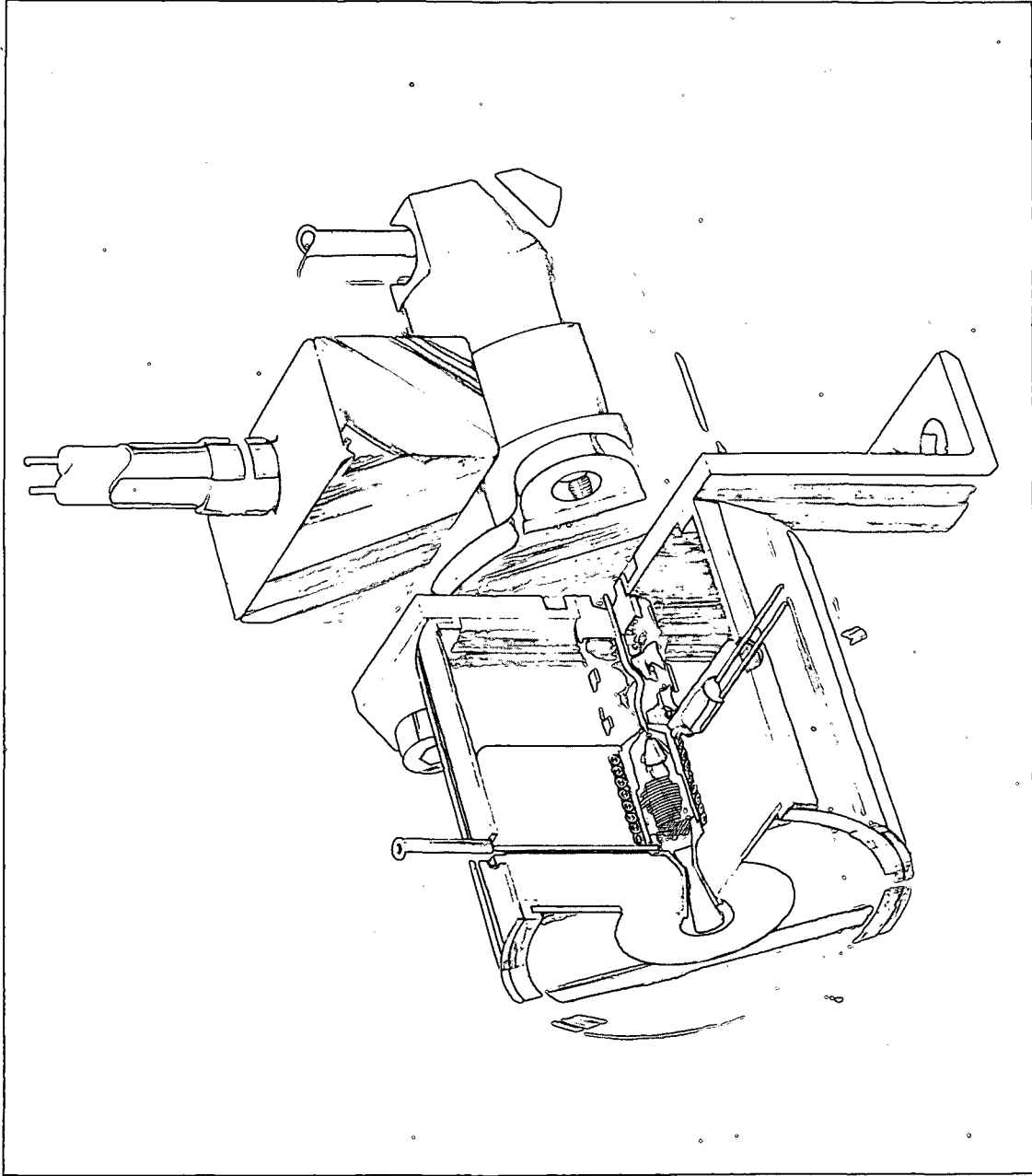


Figure 1. Cutaway Drawing of Engineering Model EHT

2.2 Potential Improvements to the Basic Design

During the course of the Engineering Model tests three areas of potential improvement were noted. These relate to heater manufacturability, thruster materials, and thruster injector design. None of these are unique to the electrothermal hydrazine thruster; all have been encountered previously by TRW and other investigators working with small catalytic thrusters.

Heater Element Manufacturability. The heater element design used on the Engineering Model EHT is the same as that used for catalyst bed and line heaters on several flight systems. The reliability of this type of heater has been demonstrated by a cumulative total of tens of thousands of hours of failure-free operation in space and real-time ground testing of about 2000 hours at 1800°F on a number of individual units.

The heater units are differentially swaged by the manufacturers in a number of "standard" diameters, each of which requires special tooling. Should a requirement exist for a specific diameter for which no tooling exists, the manufacturer would embark on a small development program. The initial result is likely to be sub-standard. This was the case with one lot of heaters procured for the EHT program. Until the time of fabrication of the last three EM thrusters, a standard configuration heater was used. No failures were encountered in more than two years of development testing with perhaps 20 different thrusters.

Twelve special-order heaters were procured for the EM thrusters. These units were purchased with a specific resistance, diameter, and maximum length. All were examined by X-ray testing and found to be of questionable quality. One of the units experienced a failure in the lead section.

For a flight program, a new heater element configuration must be treated as any other unqualified component, and not accepted on the basis of similarity to a proven design. This implies vendor surveillance, qualification and screening tests, and a component acceptance test.

Thruster Materials. Small hydrazine thrusters, both catalytic and electrothermal, use small diameter injector tubes. These tubes are typically in the size range of 0.005 to 0.015 inch. Larger hydrazine thrusters

have relied on stainless steel and super alloy materials, notably Haynes 25 (also called L-605), for injector materials. For these applications, the relatively slow nitriding rate of Haynes 25 has been adequate. For thrusters smaller than about 0.5 pound thrust, however, even a small amount of nitriding in the injector has proven detrimental for long life missions. While the material strength may not be degraded significantly, a small nitride layer may change the effective injector diameter to a significant degree. This results in an increased pressure drop and decreased thrust. This phenomenon was observed in the EM EHT and is reported in Reference 4.

Noble metals, notably platinum-10 percent iridium, have been found to be much more nitride-resistant to hydrazine than the super alloys. A development model EHT with a Pt-10Ir injector was cycled 10^6 times. Post test inspection showed no evidence of nitriding or materials degradation of the injector. For long-life missions, the use of noble-metal injectors should be investigated further.

Injector Design. The injectors of most small hydrazine thrusters have a large length-to-diameter ratio to provide a pressure drop sufficient to prevent chamber pressure oscillations from influencing the supply pressure. The injector also supports a very large temperature gradient since it is attached at one end to the control valve at ambient temperature and the thrust chamber at the other end. Under steady state conditions the thrust chamber may reach 1700°F. These two factors combined result in the injector being a very efficient heat exchanger. Heat from the injector is transferred into the incoming propellant immediately upstream of the chamber. If the heat transfer rate is too high, the incoming propellant will be vaporized. This results in a large pressure drop and a reduced flow rate. This phenomenon is most severe for short pulses following a steady state run which heats the chamber to a high temperature.

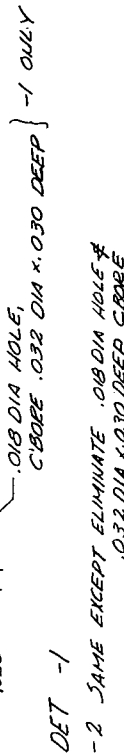
Performance and pulse shape of the Engineering Model EHT would be improved if the injector tube diameter were larger — the maximum diameter being dictated by factors such as injector exit velocity, "tail off" time due to dribble volume, and decoupling of chamber pressure oscillations from the supply pressure. The increased instantaneous flow rate at the time the valve is opened would result in faster chamber pressure rise times, and a reduced possibility of vaporization in the injector under high chamber

temperature conditions. Since the reduced injector pressure drop would result in higher chamber pressures, the thrust would be increased proportionally at any given inlet pressure. This increased thrust could then be decreased by reducing the nozzle throat diameter.

3.0 DRAWINGS

A complete set of Electrothermal Hydrazine Thruster Drawings is included in this section. The Engineering Model is identified as X410572-2. The unit is comprised of the following components.

(1) Nozzle-EHT	X409237-1
(1) Body, Thruster-EHT	X409235-1
(1) Standoff-EHT	X410562-2
(1) Tube, Barrier-EHT	X409236-1
(1) Bracket, Thruster MTG, EHT	X410560-1
(1) Seal, Tube-EHT	X410563-1
(2) End Plate-EHT	X410561-1
(1) Shield-EHT	X410559-2
(1) Tube, Injector	X409240-14
(1) Sleeve, Injector	X409240-13
(60) Screen	X409240-7
(1) Screen	X409240-8
(1) Tube, Pressure Tap	X409240-4
(1) Sleeve	X409240-5
(1) Valve	Parker, 5701060-104
(1) O-Ring	Parker, 2-12
(1) Heater	Am.Std. BXA04-FB-AM
(1) Insulation Package	X410572, WRP-X
(3) Bolt	#10-32UNF 3BTHRD



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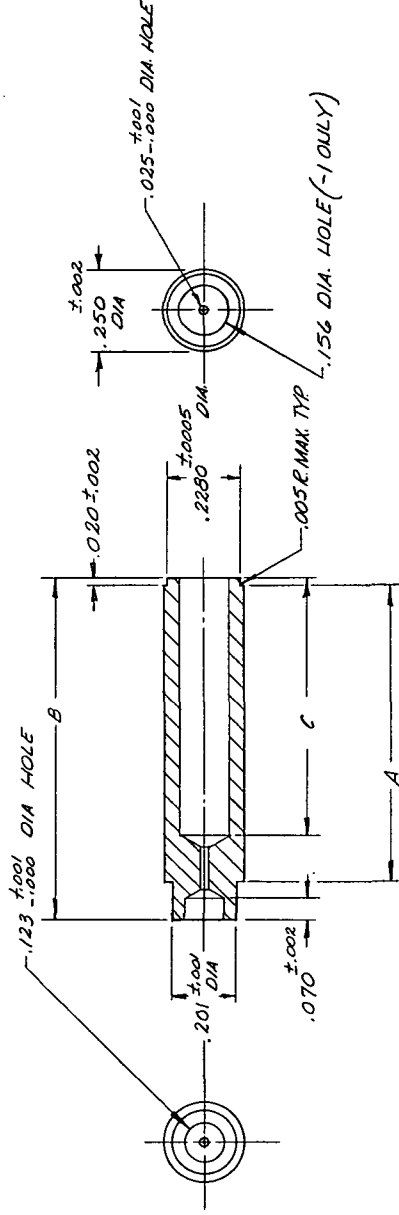


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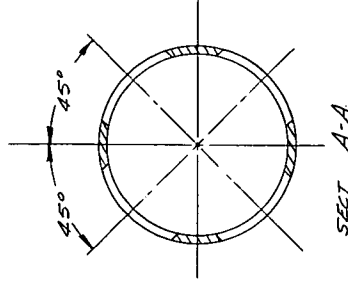
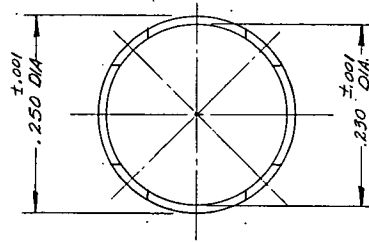
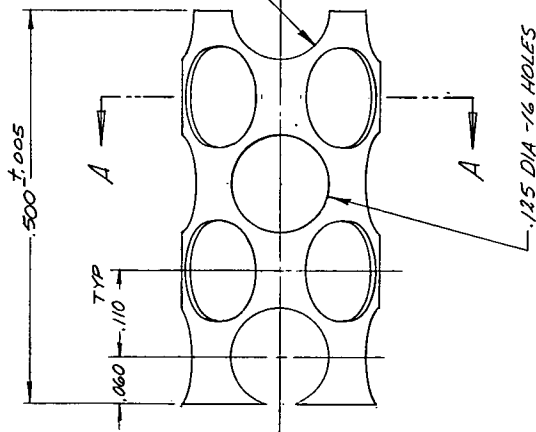
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98X ± .005		APPROVALS						
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1. IDENTIFICATION MARKING PER PR 12-6-0900
TYPE _____ CLASS _____

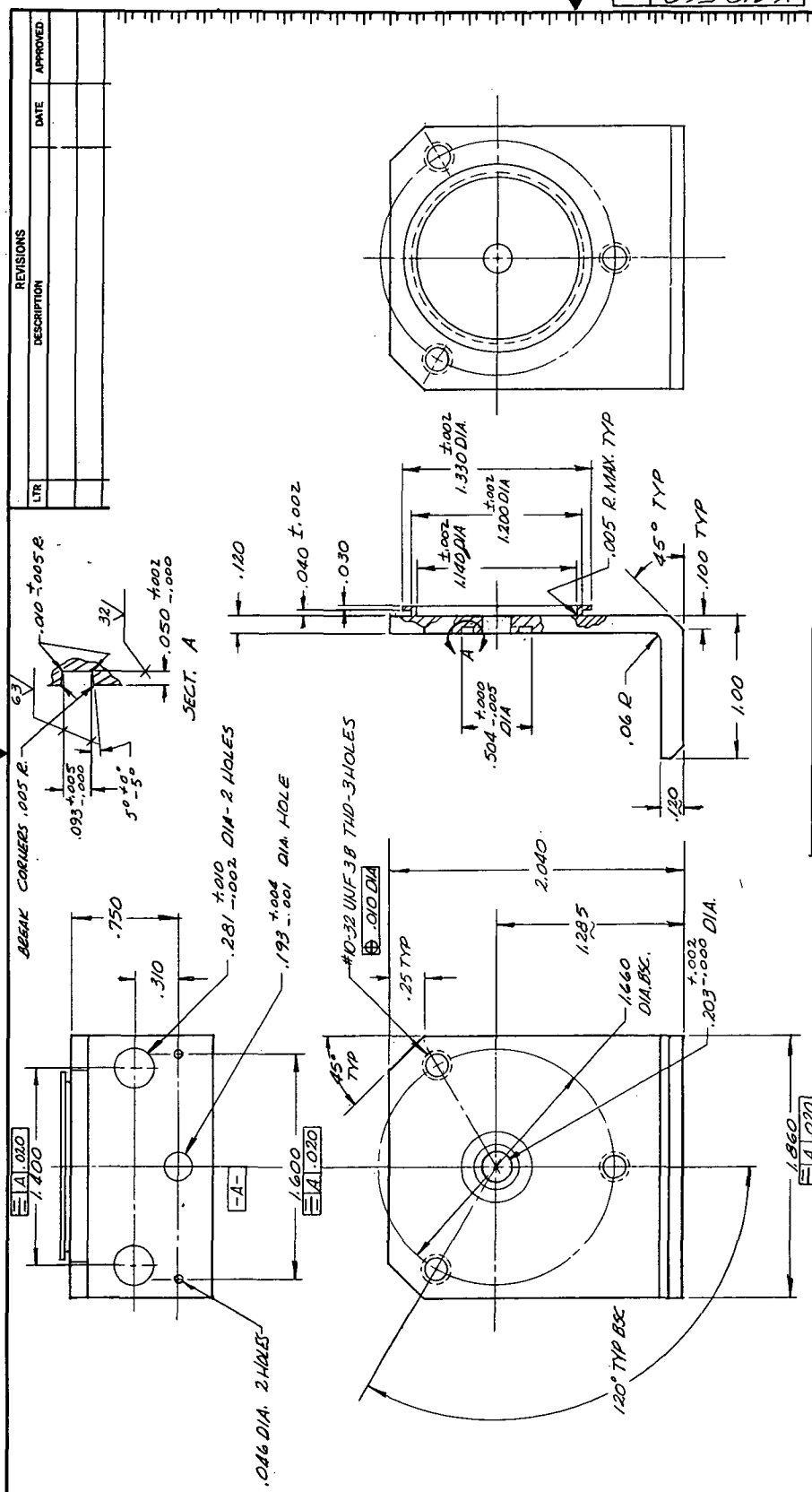
PART NUMBER _____

NOTES: UNLESS OTHERWISE SPECIFIED

BY DETACHMENT CLEARPRINT 88

SYMBOL 100 REV. 1000

SHEET

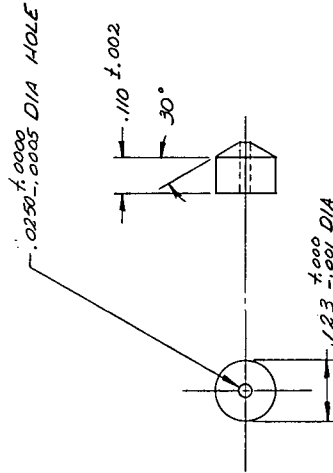


NOTES: UNLESS OTHERWISE SPECIFIED

1. IDENT. MARKING PER PR 12-6-0900

[illegible]

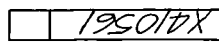
REVISIONS		
LTR	DESCRIPTION	DATE



NOTES: UNLESS OTHERWISE SPECIFIED
1. IDENT MACHINE PER DE 12-6-0900

QTY READ PER ASSY		CORE IDENT NO.	PART OR IDENTIFYING NO.	-1 SEAL	TEFLOU 800	MIL P 19463	DES DES	REV
UNLESS OTHERWISE SPECIFIED		PARTS LIST		THE FOLLOWING EOS HAVE BEEN ATTACHED TO THIS PRINT		TRW ONE SPACE PARK • REDONDO BEACH, CALIFORNIA SEAL, TUBE - EHT		
1. DO NOT SCALE DRAWING. 2. INTERPRET PER MIL-STD-100. 3. DIMENSIONS ARE IN INCHES. 1/25 4. SURFACE TEXTURE SHALL BE 125 5. REMOVE BURRS AND SHARP EDGES. 6. DIMENSIONS SHOWN ARE PLATING OR CONVERSION COATING. 7. PARENT METRIC DATA IS FOR REFERENCE ONLY.		TOLERANCES ON ALL HOLE DIAMETERS UNDER .2500 +.0005 .2500 THRU .7500 +.001 .7500 THRU 1.0000 +.0015 1.0000 THRU 1.2500 +.002 1.2500 THRU 2.0000 +.003 OVER 2.0000 +.005 ON DECIMAL DIMENSIONS MACHINED ±.001 CAST ±.005 FURNISHED ±.01 CHAMFERS ±.5°		CONTRACT NO. DRAWN BY: MARGARET CHECKED: 1/1/73 STRUCTURES MATERIAL PROCESS ENGINEER: M. H. H. 3/24/73 SUPERVISOR: J. H. H. 3/24/73 PROJECT		SIZE CODE IDENT NO. C 11982 SCALE: NONE		
FINISH HEAT TREAT		OTHER APPROVALS		SHEET		EXTENSION SHEET NO.		

X410563

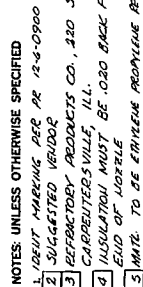


NOTES: UNLESS OTHERWISE SPECIFIED
1. IDENT MARKING PER PD 12-6-0900

QTY		REQD PER ASSY	UNLESS OTHERWISE SPECIFIED		TOLERANCES		CONTRACT NO.		THE FOLLOWING EOS HAVE BEEN ATTACHED TO THIS PRINT		ITEM NO.	
CODE	IDENT NO.	PART OR IDENTIFYING NO.	NOMENCLATURE OR DESCRIPTION	MATERIAL	SPCC	REF DES						
PARTS LIST												
			1. DO NOT SCALE DRAWING.	ON ALL HOLE DIAMETERS		DRAWN BY WINCESOU 3/4/92						
			2. HOLE SIZE FRACTIONAL.	± .001								
			3. DIMENSIONS IN INCHES.	± .005								
			4. SURFACE TEXTURE SHALL BE .25	351 THRU 350								
			5. REMOVE BURRS AND SHARP EDGES.	241 THRU 135								
			6. DIMENSIONS APPLY BEFORE PLATING.	135 THRU 250								
			7. PARENTHETICAL DATA IS FOR REFERENCE ONLY.	251 THRU 250								
				ON DECIMAL DIMENSIONS		ON ANGULAR DIMENSIONS		ENGINEER				
				± .001		± .005		SUPERVISOR				
				± .002		± .010		PROJECT				
				± .005		± .020		OTHER APPROVALS				
				± .010		± .050						
				± .020		± .100						
				± .050		± .200						
				± .100		± .500						
				± .200		± 1.000						
				± .500		± 2.000						
				± 1.000		± 5.000						
				± 2.000		± 10.000						
				± 5.000		± 25.000						
				± 10.000		± 50.000						
				± 25.000		± 125.000						
				± 50.000		± 250.000						
				± 125.000		± 625.000						
				± 250.000		± 1250.000						
				± 625.000		± 3125.000						
				± 1250.000		± 6250.000						
				± 3125.000		± 15625.000						
				± 6250.000		± 31250.000						
				± 15625.000		± 78125.000						
				± 31250.000		± 156250.000						
				± 78125.000		± 390625.000						
				± 156250.000		± 781250.000						
				± 390625.000		± 1953125.000						
				± 781250.000		± 3906250.000						
				± 1953125.000		± 9765625.000						
				± 3906250.000		± 19531250.000						
				± 9765625.000		± 48828125.000						
				± 19531250.000		± 97656250.000						
				± 48828125.000		± 244140625.000						
				± 97656250.000		± 488281250.000						
				± 244140625.000		± 1220703125.000						
				± 488281250.000		± 2441406250.000						
				± 1220703125.000		± 6103515625.000						
				± 2441406250.000		± 12207031250.000						
				± 6103515625.000		± 30517578125.000						
				± 12207031250.000		± 61035156250.000						
				± 30517578125.000		± 152587890625.000						
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				± 152587890625.000		± 762939453125.000						
				± 305175781250.00								

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5 MATL. TO BE ETHYLENE PROPYLENE RESIN (PARKER #E515-8 COMPOUND)

4.0 CONCLUSIONS

On the basis of the results of the Engineering Model tests, the thruster is capable of rapid flight qualification to performance and lifetime requirements applicable to a large class of spacecraft. Only minor modifications are required to the configuration of the Engineering Model EHT.

5.0 REFERENCES

1. Monopropellant Hydrazine Resistojet, Analysis Task Summary Report, TRW Document 20266-6006-R0-00, November 1971.
2. Monopropellant Hydrazine Resistojet, Preliminary Design Task Summary Report, TRW Document 20266-6009-R0-00, February 1972.
3. Monopropellant Hydrazine Resistojet, Model Specification Task Summary Report, TRW Document 20266-6010-R0-00, February 1972.
4. Monopropellant Hydrazine Resistojet, Engineering Model Fabrication and Test Task Summary Report, TRW Document 20266-6024-R0-00, March 1973.
5. Monopropellant Hydrazine Resistojet, Data Correlation Task Summary Report, TRW Document 20266-6025-R0-00, March 1973.
6. Murch, Charles K. and Charles R. Hunter, Electrothermal Hydrazine Thruster Development, AIAA Paper No. 72-451, April 1972.
7. Callens, R. A. and Charles K. Murch, Electrothermal Hydrazine Thruster Analyses and Performance Evaluation, AIAA Paper No. 72-1152, November 1972.