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APPENDIX A

NUMERICAL SIMULATION OF THE WORLD OCEAN CIRCULATION

by

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Abstract

A multi-level model, based on the primitive equations, is developed for simulating the temperature and velocity fields produced in the world ocean by differential heating and surface wind stress. The model ocean has constant depth, free slip at the lower boundary, and neglects momentum advection; so that there is no energy exchange between the barotropic and baroclinic components of the motion, although the former influences the latter through temperature advection.

The ocean model was designed to be coupled to the UCLA atmospheric general circulation model, for the study of the dynamics of climate and climate changes. But here, the model is tested by prescribing the observed seasonally varying surface wind stress and the incident solar radiation, the surface air temperature and humidity, cloudiness and the surface wind speed, which, together with the predicted ocean surface temperature, determine the surface flux of radiant energy, sensible heat and latent heat. From an initial state, in which the temperature as a function of depth and latitude is given, the integration is carried forward over several decades of simulated time, which is longer than the adjustment time scale for the upper levels of the model. In this test, the model successfully simulates most of the large scale features of the world ocean circulation, including a good simulation of the ocean surface temperature.

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NUMERICAL SIMULATION OF  
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## Introduction

### Governing equations

With momentum advection neglected, and with the Boussinesq approximation for the density and incompressibility, the governing equations are

$$\frac{\partial \mathbf{v}}{\partial t} = - \frac{1}{\rho_0} \nabla p - 2\boldsymbol{\Omega} \times \mathbf{v} + \mathbf{F} , \quad (1)$$

$$\frac{\partial p}{\partial z} = - g \rho , \quad (2)$$

$$\rho = \rho_0 (1 - \alpha |T - T_0|) , \quad (3)$$

$$\frac{\partial T}{\partial t} + \nabla \cdot (T \mathbf{v}) + \frac{\partial}{\partial z} (T w) = \frac{Q}{C} , \quad (4)$$

and

$$\nabla \cdot \mathbf{v} + \frac{\partial w}{\partial z} = 0 , \quad (5)$$

where  $\mathbb{V}$  is horizontal velocity,  $w$  is vertical velocity,  $p$  is pressure,  $\rho$  is density and  $\rho_0$  is a constant,  $T$  is temperature and  $T_0$  is a constant,  $\Omega$  is the earth's rotation vector,  $g$  is the acceleration of gravity,  $\alpha$  is the coefficient of thermal expansion, and  $c$  is the specific heat of sea water.  $z$  is the positive upward vertical coordinate and  $t$  is time.  $\mathbb{F}$  is the horizontal frictional force per unit mass and  $Q$  is the rate of heating per unit mass, which are taken as

$$\mathbb{F} = A_M \nabla^2 \mathbb{V} + K \frac{\partial^2 \mathbb{V}}{\partial z^2}, \quad (6)$$

and

$$Q = c A_H \nabla^2 T + \frac{cK}{\delta} \frac{\partial^2 T}{\partial z^2}, \quad (7)$$

where  $A_M$  is the coefficient of horizontal eddy viscosity,  $A_H$  is the coefficient of horizontal eddy heat diffusion, and  $K$  is the coefficient of both the vertical eddy viscosity and the vertical eddy heat diffusion. The coefficient  $\delta$  (in 7) is defined as

$$\delta \begin{cases} = 1 \\ = 0 \end{cases} \quad \text{when } \frac{\partial T}{\partial z} \begin{cases} \geq 0 \\ < 0 \end{cases},$$

as a parameterization of strong vertical mixing that restores a neutral stratification whenever a vertically unstable stratification develops.

The boundary conditions at the ocean bottom ( $z = H$ ) are

$$w = 0, \quad (8)$$

$$\frac{\partial \mathbb{V}}{\partial z} = 0, \quad (9)$$

and

$$\frac{\partial T}{\partial z} = 0, \quad (10)$$

so that there is no vertical motion, no momentum transfer and no heat transfer across the lower boundary.

The boundary conditions at the ocean surface ( $z = 0$ ) are

$$w = 0, \quad (11)$$

$$\frac{\partial \psi}{\partial z} = \frac{\tau_s}{\rho_o K}, \quad (12)$$

and

$$\frac{\partial T}{\partial z} = \frac{Q_s}{c K \rho}, \quad (13)$$

where  $\tau_s$  is the vector wind stress and  $Q_s$  is the downward heat flux at the ocean surface. Setting  $w = 0$  at the ocean surface filters out external gravity waves and allows the use of a long computational time step.

The boundary conditions at the lateral walls are zero normal velocity and zero tangential velocity, and zero heat transfer through the walls.

### Computational procedure

The assumption of no momentum advection, constant depth, and free slip at the lower boundary, decouples the barotropic component of the velocity (the vertical mean of the horizontal velocity) from the baroclinic component of the velocity (the deviation of the horizontal velocity from its vertical mean). The former is governed entirely by the wind stress curl and is independent of the heating, while the latter is governed by both the stress and the heating. There is no energy exchange between the two components, although the barotropic

component affects the baroclinic component through the horizontal temperature advection (Eq. 4).

The barotropic component of the velocity is obtained by taking the curl of the vertical integral of Eq. 1, or

$$\frac{\partial M}{\partial t} = -\frac{1}{\rho_0} \nabla^2 P - 2\Omega \times M + \frac{\tau_s}{\rho_0} + A_M \nabla^2 M, \quad (14)$$

where

$$M = \int_{-H}^0 \Psi dz \quad \text{and} \quad P = \int_{-H}^0 p dz,$$

and

$$\frac{\partial}{\partial t} \nabla^2 \Phi = -f \frac{\partial \Phi}{\partial \lambda} + \frac{1}{\rho_0} \mathbf{k} \cdot \nabla \times \tau_s + A_M \nabla^2 \Phi, \quad (15)$$

where  $\mathbf{k} \times \nabla \Phi = M$  defines the stream function  $\Phi$  of the vertically integrated velocity  $M$ ,  $f = 2\Omega \sin \phi$  is the coriolis parameter,  $\lambda$  is longitude and  $\phi$  is latitude,  $\mathbf{k}$  is unit vertical vector, and  $a$  is the Earth's radius. This vorticity equation, for the barotropic component of the velocity, is solved as an initial-value boundary-value problem in the way which is described below.

The baroclinic component of the velocity is obtained by substituting for  $\Psi = \bar{\Psi} + \Psi'$  and  $\nabla p = \bar{\nabla p} + (\nabla p)'$  in Eq. 1, where the bar denotes the vertical mean from  $z = -H$  to  $z = 0$ , and the prime denotes the deviation from the vertical mean. Then, subtracting the vertical mean of Eq. 1, we obtain

$$\frac{\partial \Psi'}{\partial t} = -\frac{1}{\rho_0} (\nabla p)' - 2\Omega \times \Psi' + A_M \nabla^2 \Psi' + \left( K \frac{\partial^2 \Psi'}{\partial z^2} - \frac{\tau_s}{\rho_0 H} \right), \quad (16)$$

which is the prediction equation for the baroclinic component of the velocity,

The temperature is obtained from Eq. 4.

$(\nabla p)'$  is found by taking the horizontal gradient of Eq. 2,  $\partial(\nabla p)/\partial z = -g\nabla\rho$ , integrating over the entire depth of the ocean from an arbitrary value of  $\nabla p$  at  $z = -H$ , and subtracting the vertical mean,  $\overline{\nabla p}$ . This insures that the vertical mean of  $(\nabla p)'$  is identically zero.

The vertical velocity  $w$  is calculated by Eq. 5.

#### Grid structure, domain, and finite difference scheme

The finite difference calculations are made using spherical coordinates and the same grid structure that was used by Haney (1971a). As shown in Figure 1, the  $T$ ,  $p$ ,  $\Phi$ , and  $w$  points are located at the coast lines. The  $\overline{V}$  and  $V'$  points match the distribution of the horizontal velocity points of the UCLA atmospheric general circulation model, and therefore include points on the equator. In the atmospheric model the horizontal grid size is  $4^\circ$  in latitude and  $5^\circ$  in longitude; but in the ocean model the zonal grid size is reduced to  $2.5^\circ$  in longitude to obtain a somewhat better resolution of the western boundary currents.

The model ocean is divided into five layers, which lie between 0, 70, 380, 960, 2020 and 4000 m in depth, and the horizontal velocities and temperatures are predicted for each layer. To calculate the vertical eddy diffusions of momentum and heat, these velocities and temperatures are attributed to the 20, 120, 640, 1280 and 2760 m depths. The vertical velocities are calculated at the interfaces of the five layers.

The horizontal domain extends from  $66^\circ\text{S}$  to  $74^\circ\text{N}$ , which excludes the Arctic Ocean. The northern boundary follows the edge of the continental shelf of the composite landmass of North and South America, Europe, Africa and Asia.

The southern boundary approximately follows the edge of the continental shelf of Antarctica. New Zealand, and Australia combined with New Guinea, are retained as islands.

The finite differencing scheme is the same as the one used by Haney (1971a), except that his nine point specification of the vorticity of the barotropic velocity component, which was almost the same as a  $45^\circ$  rotated five point scheme, is here replaced by the usual nearest five point scheme. This prevents a computationally false two grid point noise from being produced by the irregular lateral boundaries and irregular wind stress.

The time integration is carried forward by the leap-frog scheme, with the Euler-backward scheme applied every five time steps.

#### Prescribed parameters

The prescribed constant parameters are given in Table I.

Table I. Prescribed Constants

$g = 980 \text{ cm/sec}^2$	$T_o = 0^\circ\text{C}$
$\Omega = 7.29 \times 10^{-5} \text{ sec}^{-1}$	$H = 4 \times 10^5 \text{ cm}$
$R = 6.37 \times 10^8 \text{ cm}$	$A_M = 10^9 \text{ cm}^2/\text{sec}$
$c = 0.93 \text{ cal/cm/deg}$	$A_H = 2.5 \times 10^7 \text{ cm}^2/\text{sec}$
$\alpha = 2.5 \times 10^{-4} \text{ deg}^{-1}$	$K = 1 \text{ cm}^2/\text{sec}$
$\rho_o = 1 \text{ gm/cm}^3$	$\Delta t = 40 \text{ min, 8 hours}$

40 minutes is the time step for the integration of the vorticity equation for the barotropic velocity component, and 8 hours is the time step for the integration of the primitive equations for the baroclinic velocity component.

When the oceanic model will be coupled to the atmospheric general circulation model, the surface wind stress will be determined by the atmospheric model. But, here, for the purpose of testing the oceanic model, the surface wind stress is taken as the observed seasonally varying stress given by Hellerman (1967, 1968). Hellerman's values of the mean wind stress for the four seasons of the year (Dec-Jan-Feb; Mar-Apr-May; June-July-Aug; Sept-Oct-Nov) are subjectively interpolated and extrapolated to cover the domain of the oceanic model. A 1-2-1 zonal filter is used to remove some of the two grid interval noise in Hellerman's tabulations. Then, at each grid point, the four seasonal values of  $\bar{\tau}_s$  are used to calculate the annual mean and the amplitude and phase of the first annual harmonic of the stress; and from these parameters the surface wind stress is prescribed as a time varying function of the model year.

$Q_s$ , the net downward heat flux at the ocean surface, has four components,

$$Q_s = Q_I - (Q_B + Q_F + Q_L), \quad (17)$$

where  $Q_I$  is the net downward flux of solar radiation,  $Q_B$  is the net upward flux of infrared radiation,  $Q_F$  is the net upward flux of sensible heat, and  $Q_L$  is the net upward flux of latent heat.

When the oceanic model will be coupled to the atmospheric general circulation model, the net fluxes of solar and infrared radiation at the ocean surface will depend on the atmospheric state parameters in the fairly complex way given by Katayama (1973). In the present test of the ocean model, however, we use the relatively simple formulations, given by Angstrom (1922) for the solar radiation flux,

$$Q_I = Q_{I_0} (1 - 0.7 \frac{C}{8})(1 - A_s), \quad (18)$$



and by Brunt (1952) for the infrared radiation flux,

$$Q_B = \sigma T_s^4 \times 0.985 [0.39 - 0.05 e^{\frac{1}{e}}] \times [1 - 0.6 (C/8)^2] \quad (19)$$

Where  $Q_{I_0}$  is the direct plus indirect solar radiation reaching the ground through a cloudless atmosphere,  $C$  is the number of octants of the sky covered by clouds,  $A_s$  is the albedo of the ocean surface,  $\sigma$  is the Stefan-Boltzman constant; and  $e$  is the vapor pressure of the air (in mb) at 10 m above the ocean surface.

The annual mean and the amplitude and phase of the first annual harmonic of  $Q_{I_0}$  are obtained from the Smithsonian Meteorological Tables (1966, tables 133 and 136), with an atmospheric transmission coefficient of 0.7. The albedo of the ocean surface is taken as 0.07.

The annual mean and the amplitude and phase of the first annual harmonic of the number of octants of the sky covered by clouds,  $C$ , are calculated from the charts in the cloud atlas of Miller (1971).

The annual mean and the amplitude and phase of the first annual harmonic of the atmospheric vapor pressure,  $e$ , are calculated from tabulations of the surface air dewpoint temperature in the atlases of Taljaard et. al. (1969) and Crutcher and Meserve (1970).

These time varying parameters are used, in Eqs. 18 and 19, to prescribe the net flux of solar radiation and to calculate the net flux of infrared radiation at the ocean surface.

For the sensible and latent heat fluxes, the formulations for the test calculations are nearly the same as those that will be used with the combined atmospheric and oceanic models,

$$Q_F = \rho_A C_D C_P |V_A| (T_s - T_A), \quad (20)$$

and

$$Q_L = \rho_A C_D L |V_A| (q_s^* - q_A), \quad (21)$$

where  $\rho_A$  is the surface air density,  $C_D (= 1.23 \times 10^{-3})$  is the surface drag coefficient,  $C_p$  is the specific heat of air,  $|V_A|$  is the surface air speed,  $L$  is the latent heat of evaporation,  $q_s^*$  is the saturation water vapor mixing ratio at the ocean surface temperature, and  $q_A$  is the water vapor mixing ratio of the surface air.

The annual means and the phases and amplitudes of the first annual harmonics of  $T_A$  and  $q_A$  are calculated from tabulations of the surface air temperature and the surface air dewpoint temperature in the atlases of Taljaard et. al. (1969) and Crutcher and Meserve (1970). The annual mean and the phase and amplitude of the first annual harmonic of the surface (scalar) wind speed are calculated from data in the atlas of MacDonald (1934, charts 27 through 30).

#### The simulated barotropic circulation

#### The simulated baroclinic circulation

The simulated surface heat flux

Summary and conclusions

Acknowledgments

References

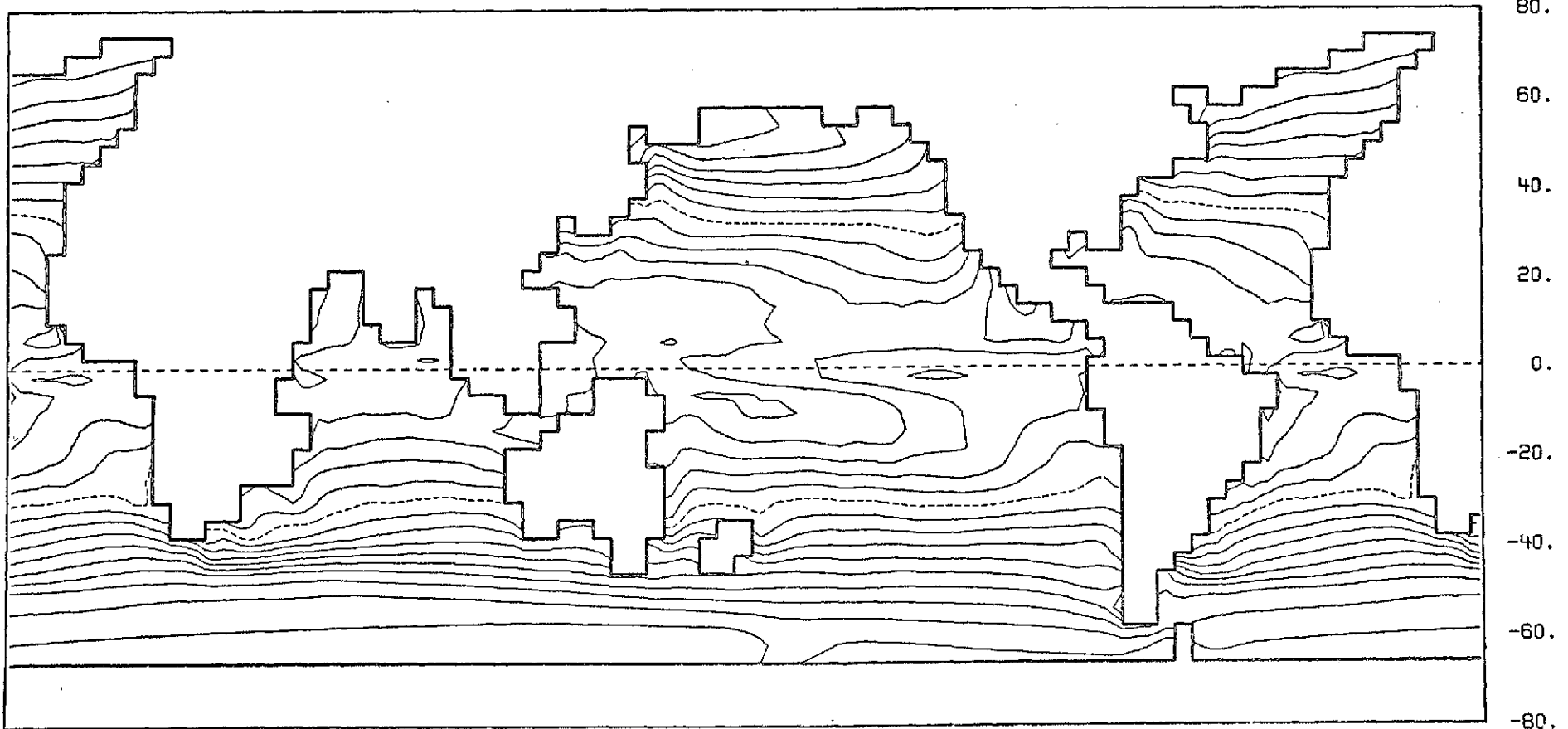
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DAY = 8773.7

TEMPERATURE AT LEVEL 1 (DEG CENT)

CONTOUR INTERVAL = 2.0 (SOLID LINES)

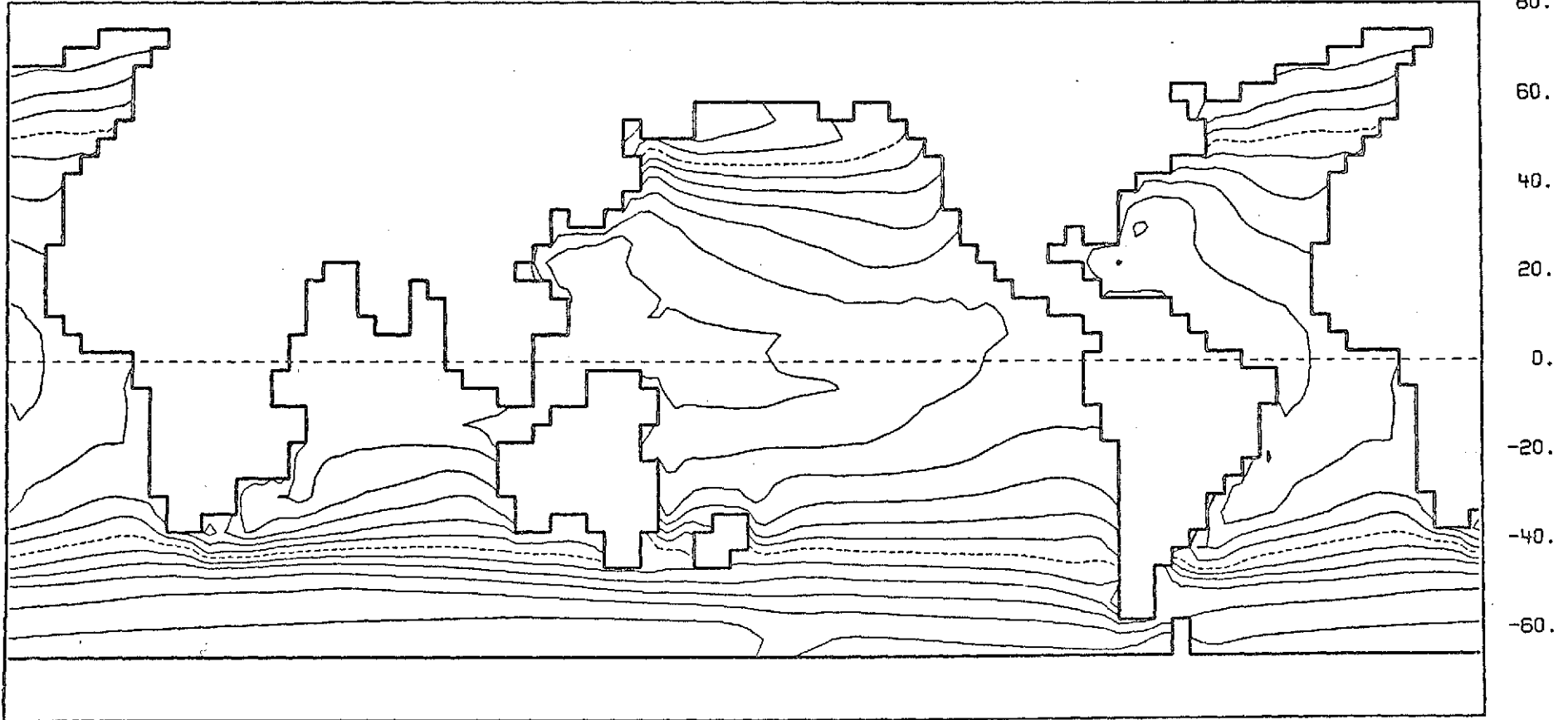
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TEMPERATURE AT LEVEL 2 (DEG CENT)  
CONTOUR INTERVAL = 2.0

DASHED LINE = 12.0



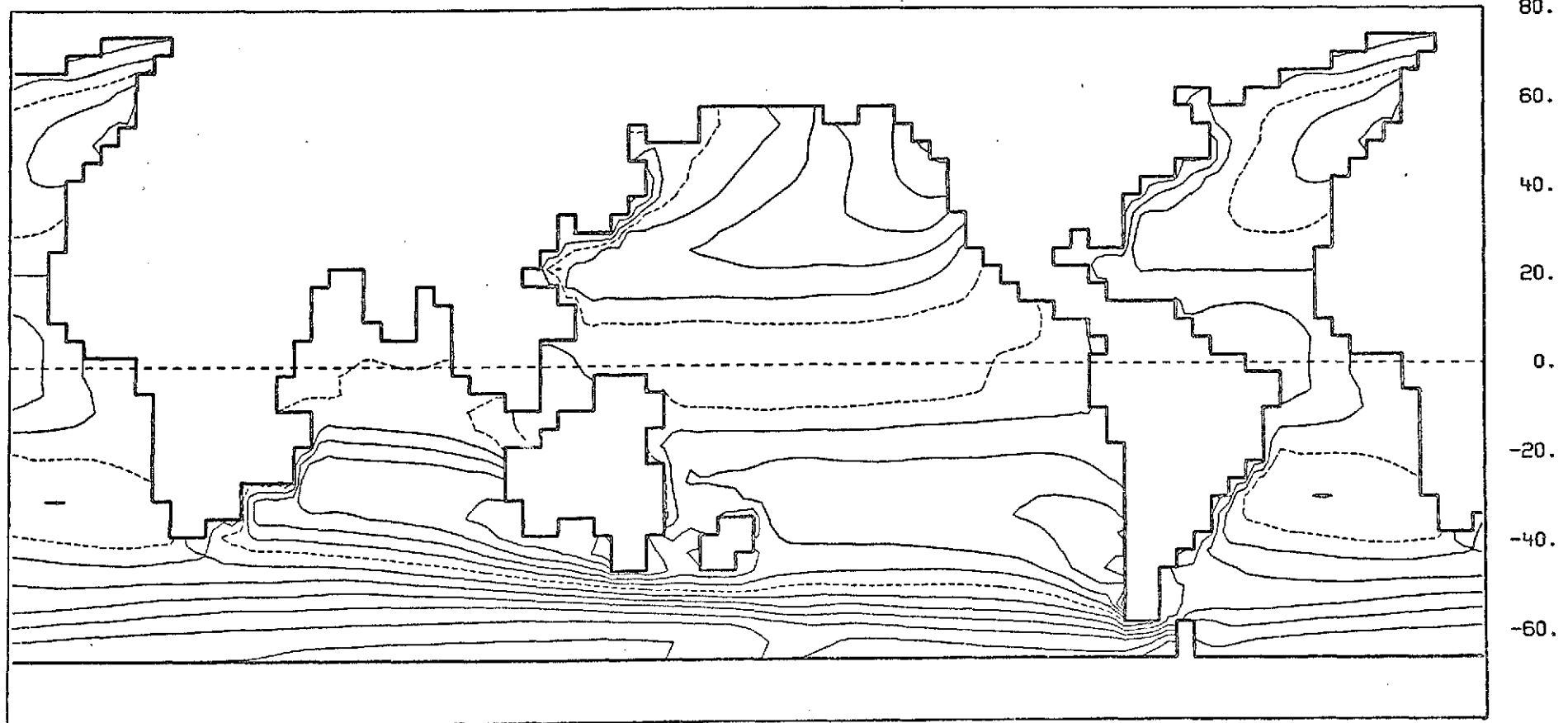
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DAY = 8773.7

TEMPERATURE AT LEVEL 3 (DEG CENT)

CONTOUR INTERVAL = 1.0

DASHED LINE = 7.0

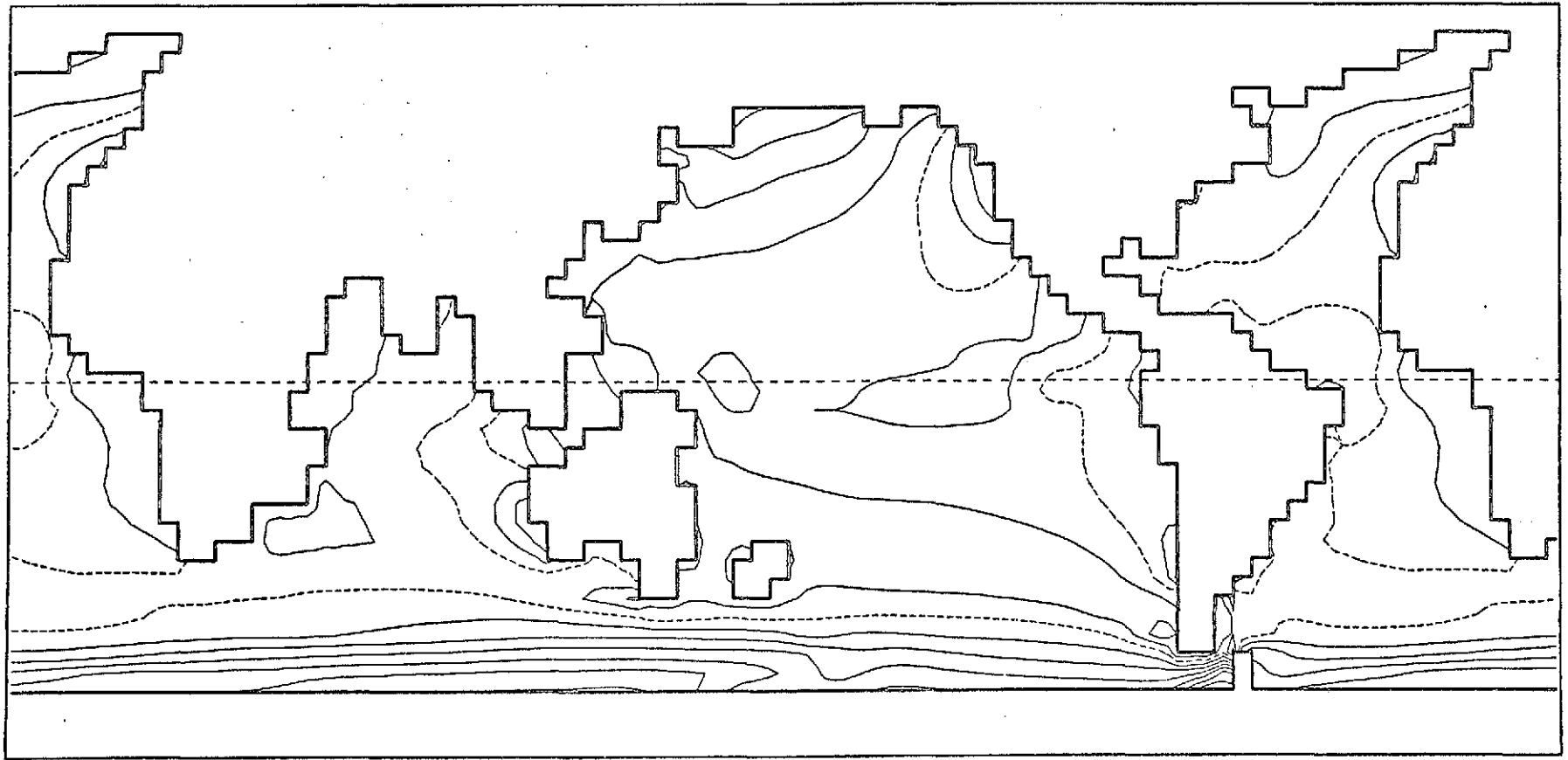


14  
+

EXPERIMENT S1  
DAY = 8773.7

TEMPERATURE AT LEVEL 4 (DEG CENT)  
CONTOUR INTERVAL = 0.5 (SOLID LINES)

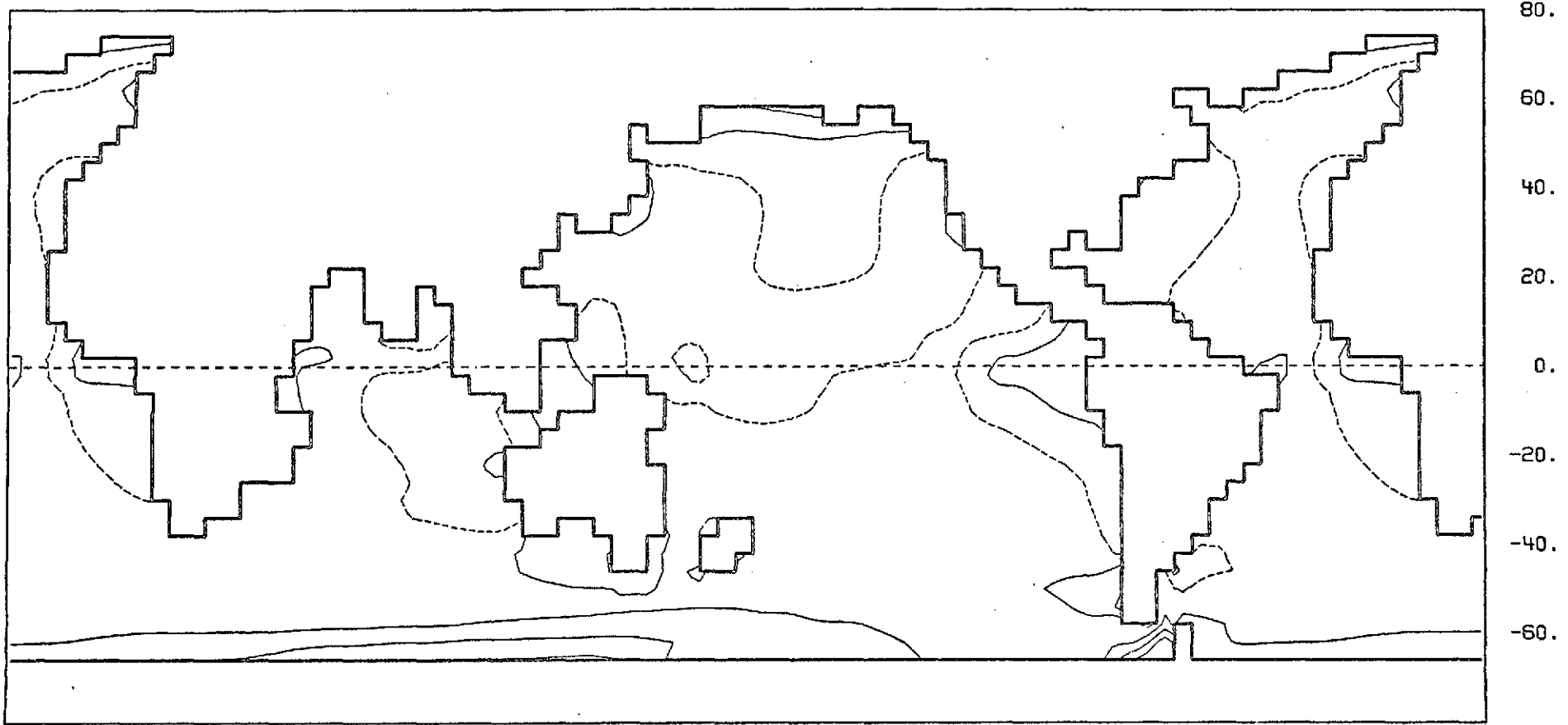
DASHED LINE = 3.5



EXPERIMENT S1  
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TEMPERATURE AT LEVEL 5 (DEG CENT)  
CONTOUR INTERVAL = 0.5 (SOLID LINES)

DASHED LINE = 2.0



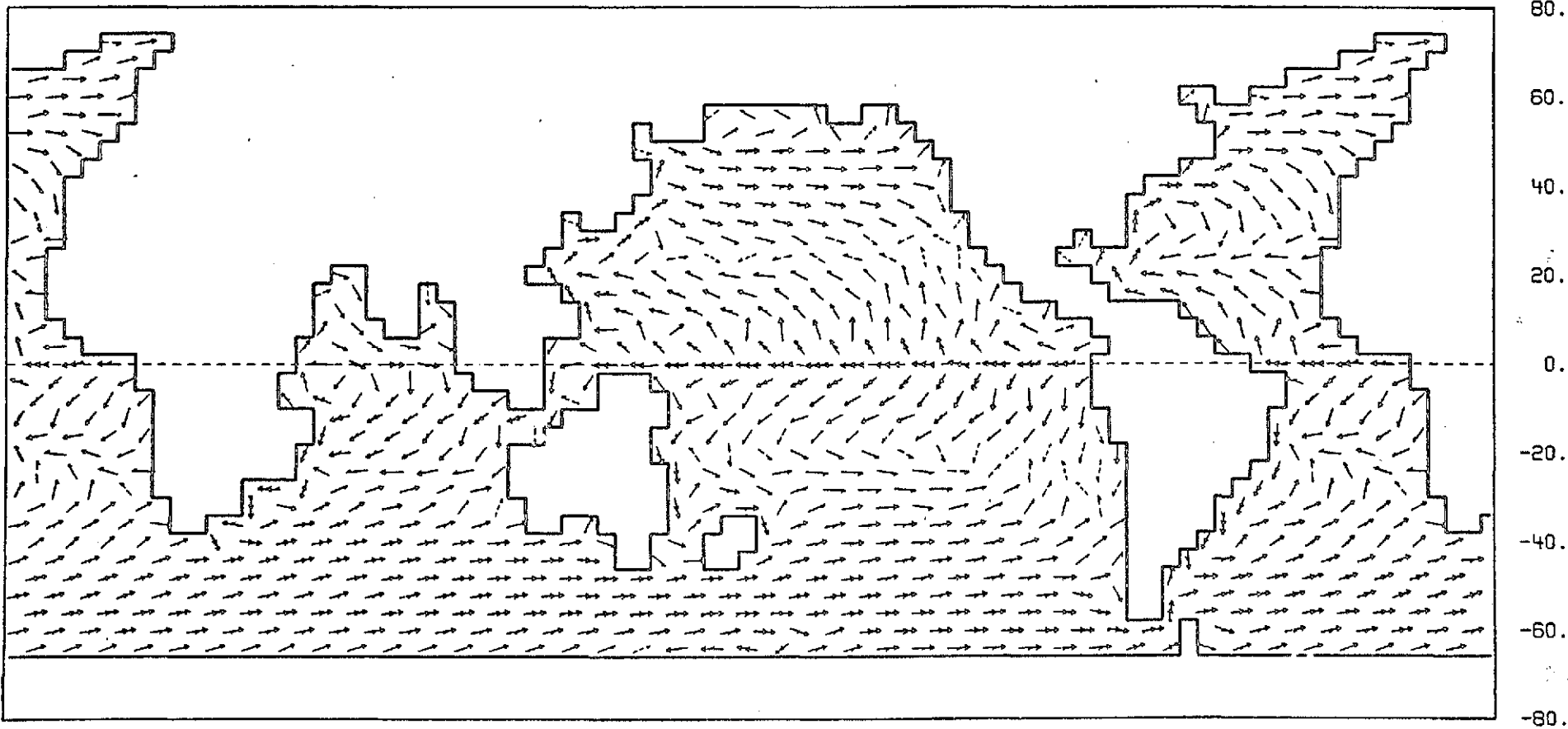


EXPERIMENT S1

DAY = 8773.7

HORIZONTAL VELOCITY AT LEVEL 1 (CM/SEC)

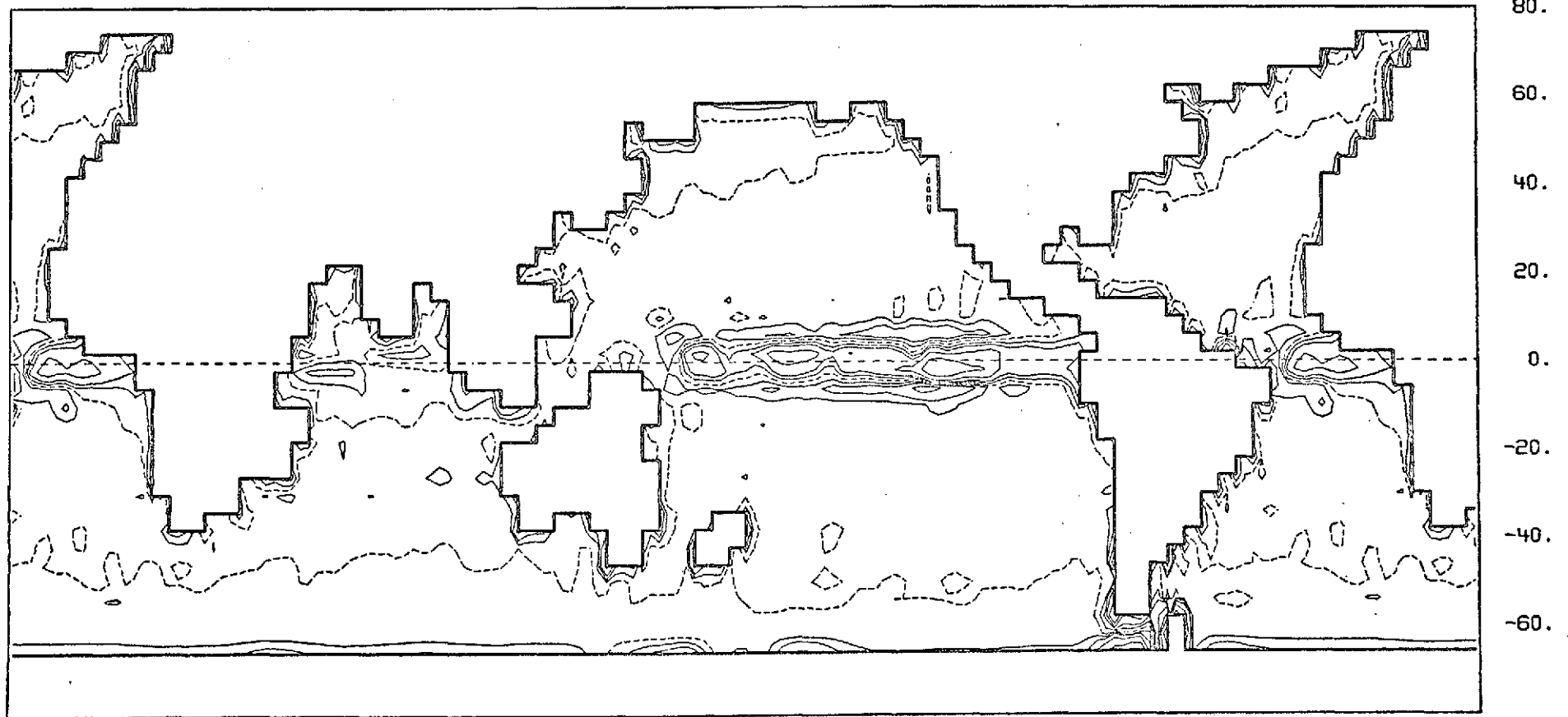
0.0 → 0.6 → 1.2 → 2.5 → 4.9 → 9.8 → 19.6 → 39.2 → 78.4



EXPERIMENT S1  
DAY = .8773.7

VERTICAL VELOCITY AT LEVEL 1.5 (CM/DAY)  
CONTOUR LINES 0, 25, 50, 100, 200, 400, 800

DASHED LINE = 0.0

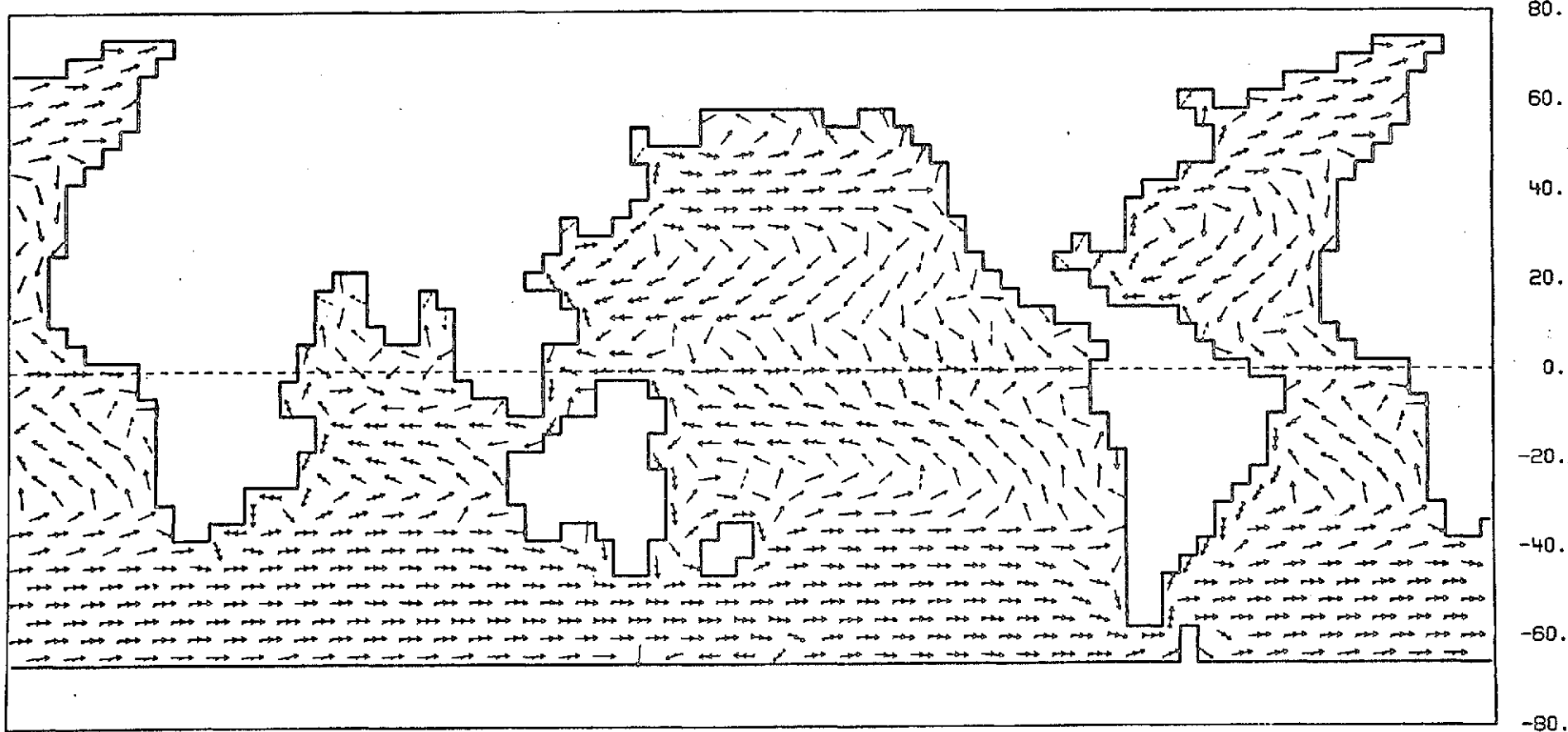


EXPERIMENT S1

DAY = 8773.7

HORIZONTAL VELOCITY AT LEVEL 2 (CM/SEC)

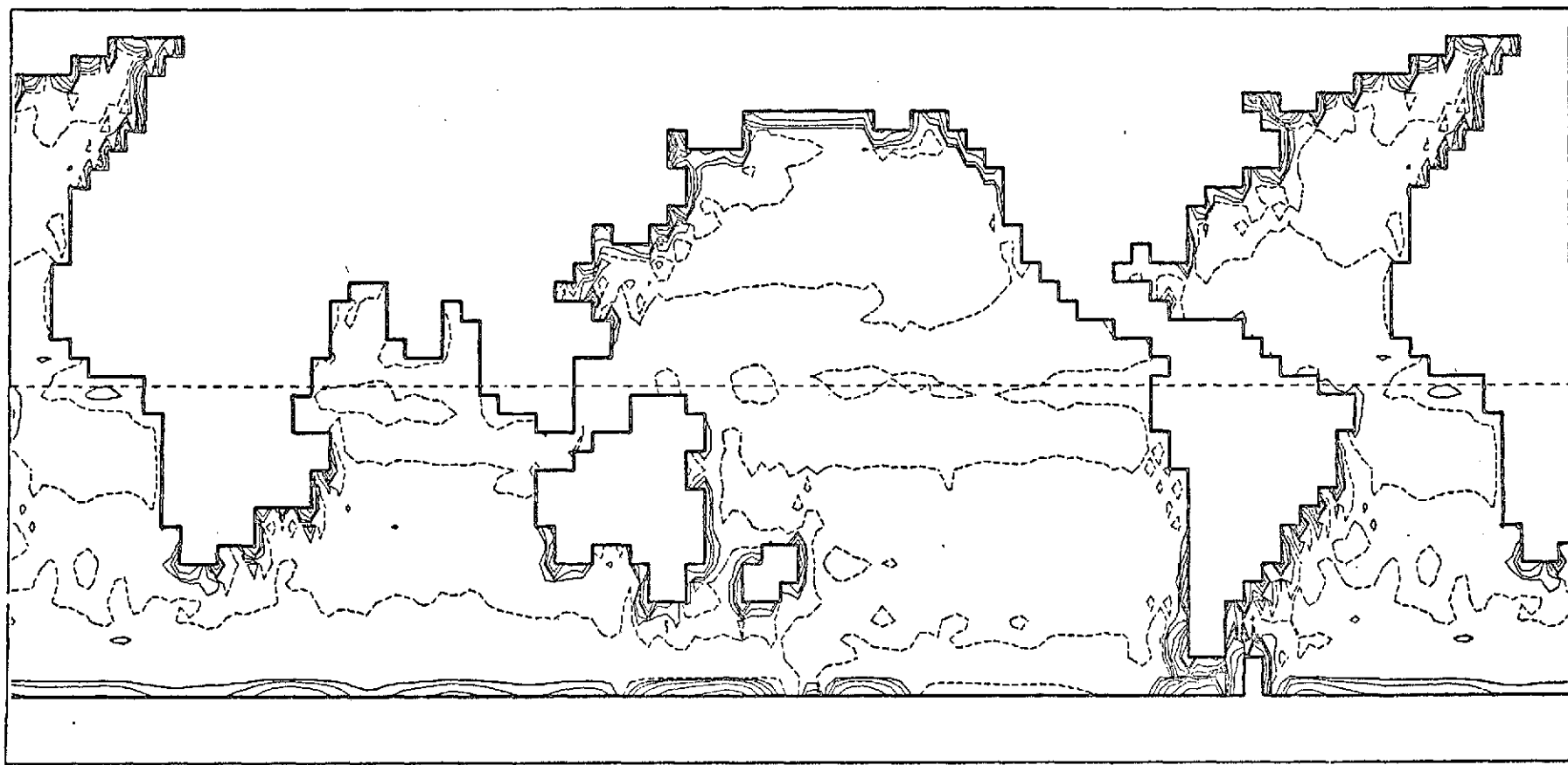
0.0 → 0.2 → 0.5 → 1.0 → 2.0 → 3.9 → 7.9 → 15.8 → 31.6



EXPERIMENT S1  
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VERTICAL VELOCITY AT LEVEL 2.5 (CM/DAY)  
CONTOUR LINES 0, 25, 50, 100, 200, 400, 800

DASHED LINE = 0.0

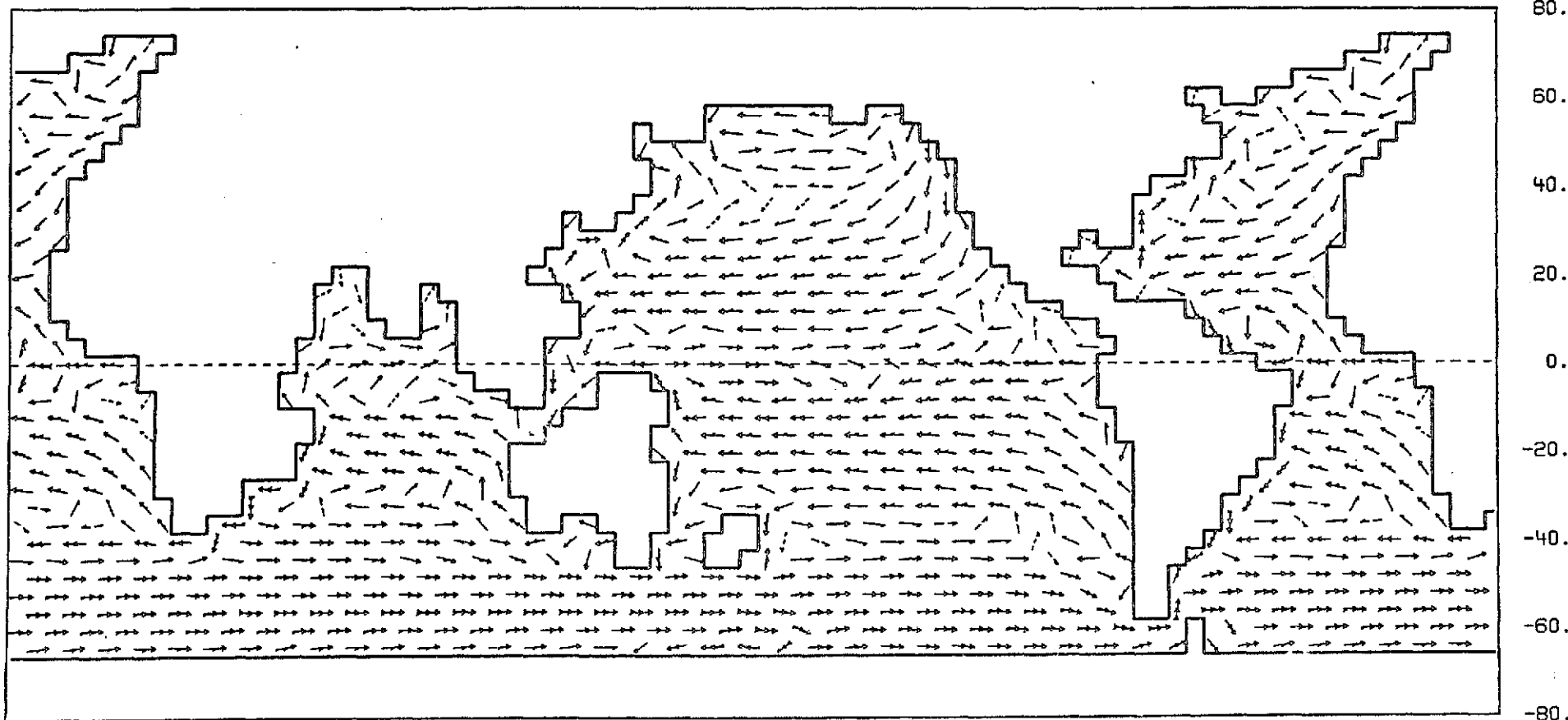


EXPERIMENT S1

DAY = 8773.7

HORIZONTAL VELOCITY AT LEVEL 3 (CM/SEC)

0.0 → 0.2 → 0.4 → 0.7 → 1.4 → 2.9 → 5.8 → 11.6 → 23.2

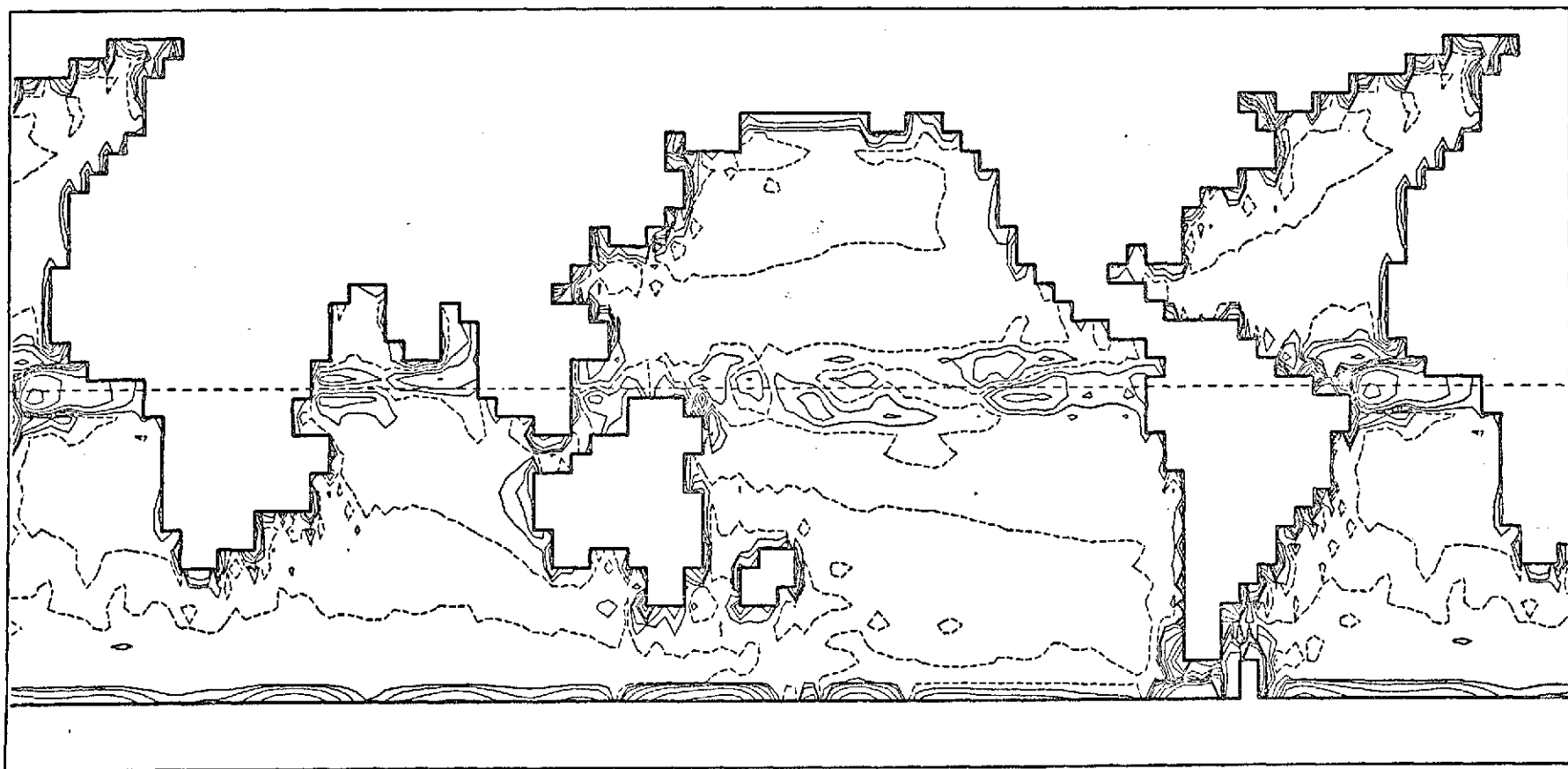


21

EXPERIMENT S1  
DAY = 8773.7

VERTICAL VELOCITY AT LEVEL 3.5 (CM/DAY)  
CONTOUR LINES 0, 25, 50, 100, 200, 400, 800

DASHED LINE = 0.0



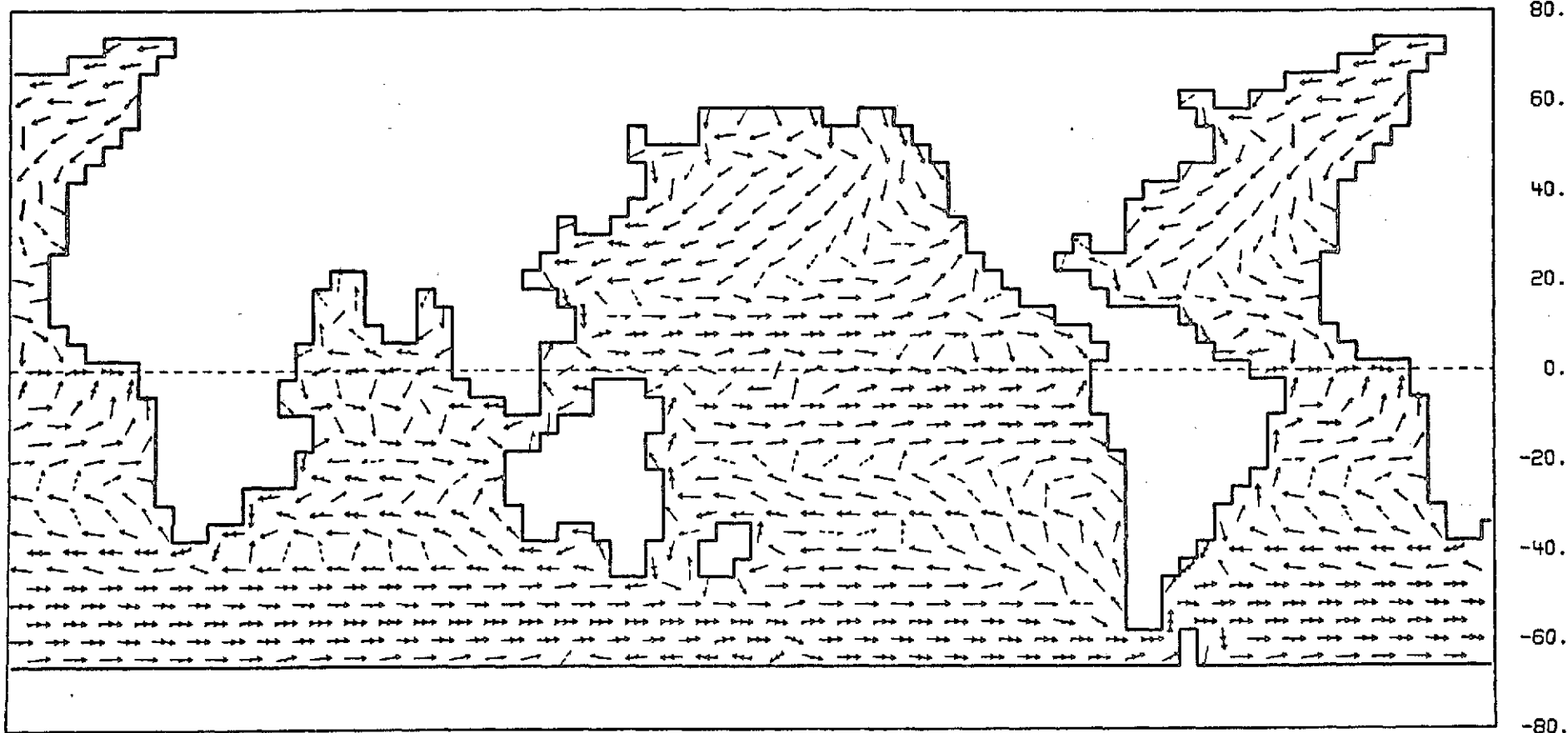
80.  
60.  
40.  
20.  
0.  
-20.  
-40.  
-60.

EXPERIMENT S1

DAY = 8773.7

HORIZONTAL VELOCITY AT LEVEL 4 (CM/SEC)

0.0 → 0.1 → 0.3 → 0.6 → 1.2 → 2.4 → 4.8 → 9.5 → 19.1



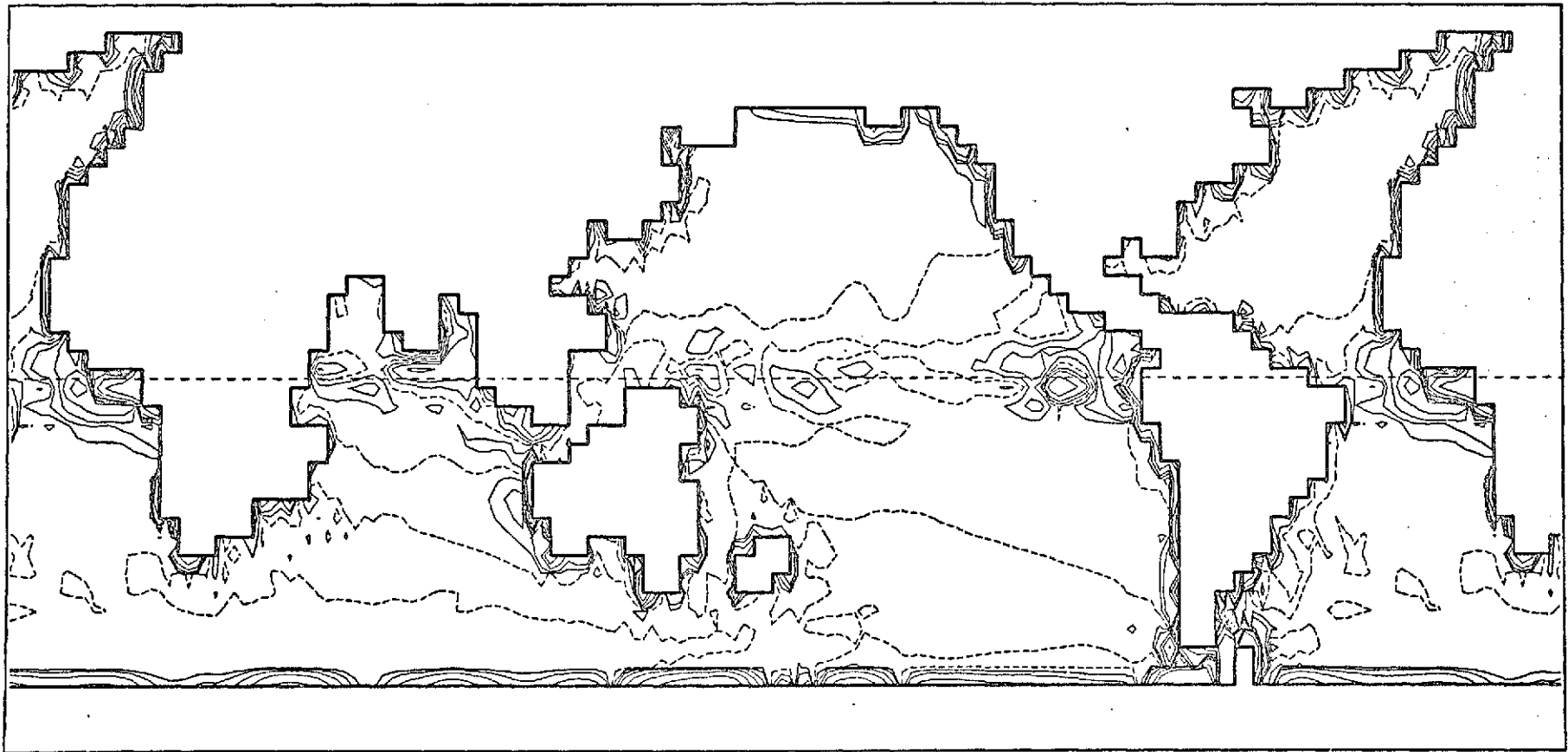
EXPERIMENT S1

VERTICAL VELOCITY AT LEVEL 4.5 (CM/DAY)

DAY = 8773.7

CONTOUR LINES 0, 25, 50, 100, 200, 400, 800

DASHED LINE = 0.0



+

24

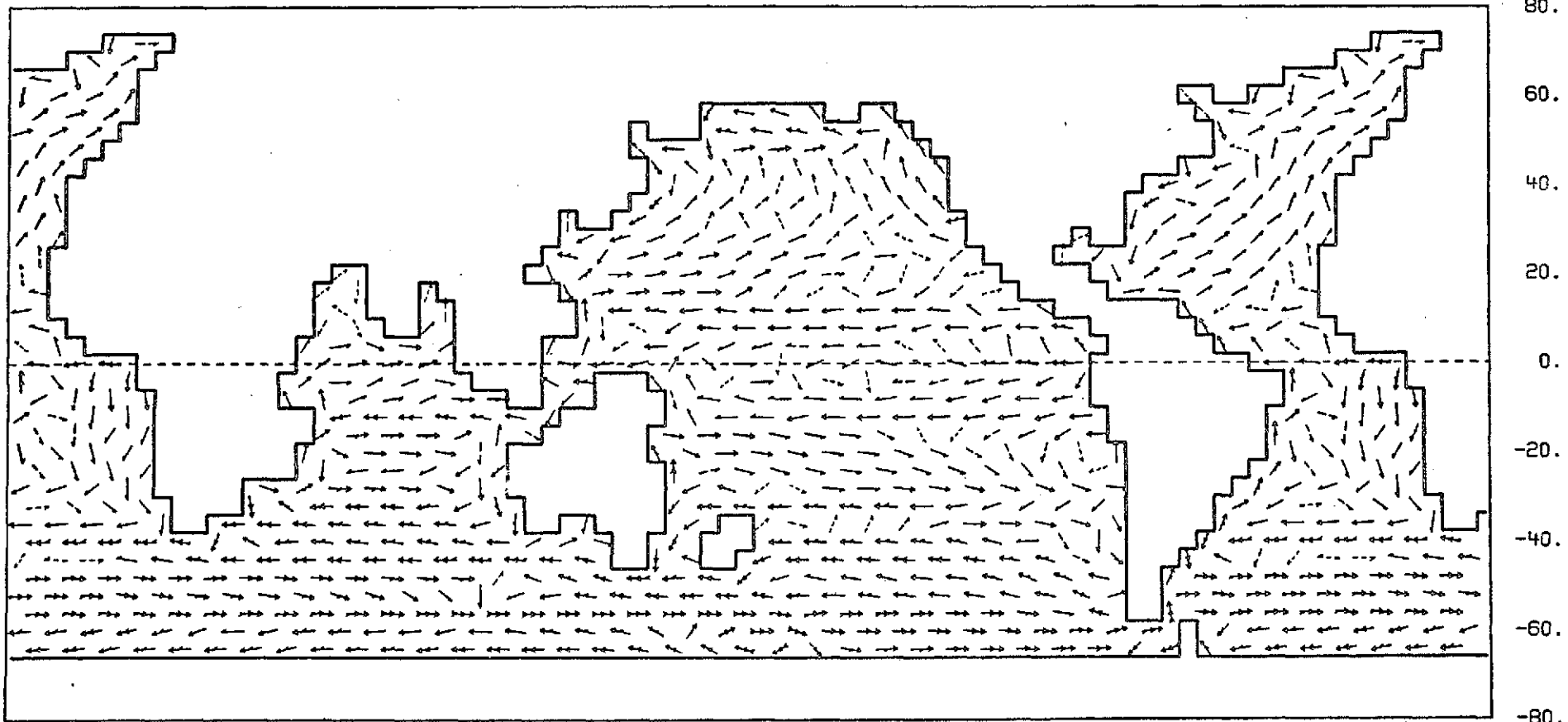


EXPERIMENT S1

DAY = 8773.7

HORIZONTAL VELOCITY AT LEVEL 5 (CM/SEC)

0.0 → 0.1 → 0.2 → 0.4 → 0.8 → 1.6 → 3.3 → 6.6 → 13.1



15

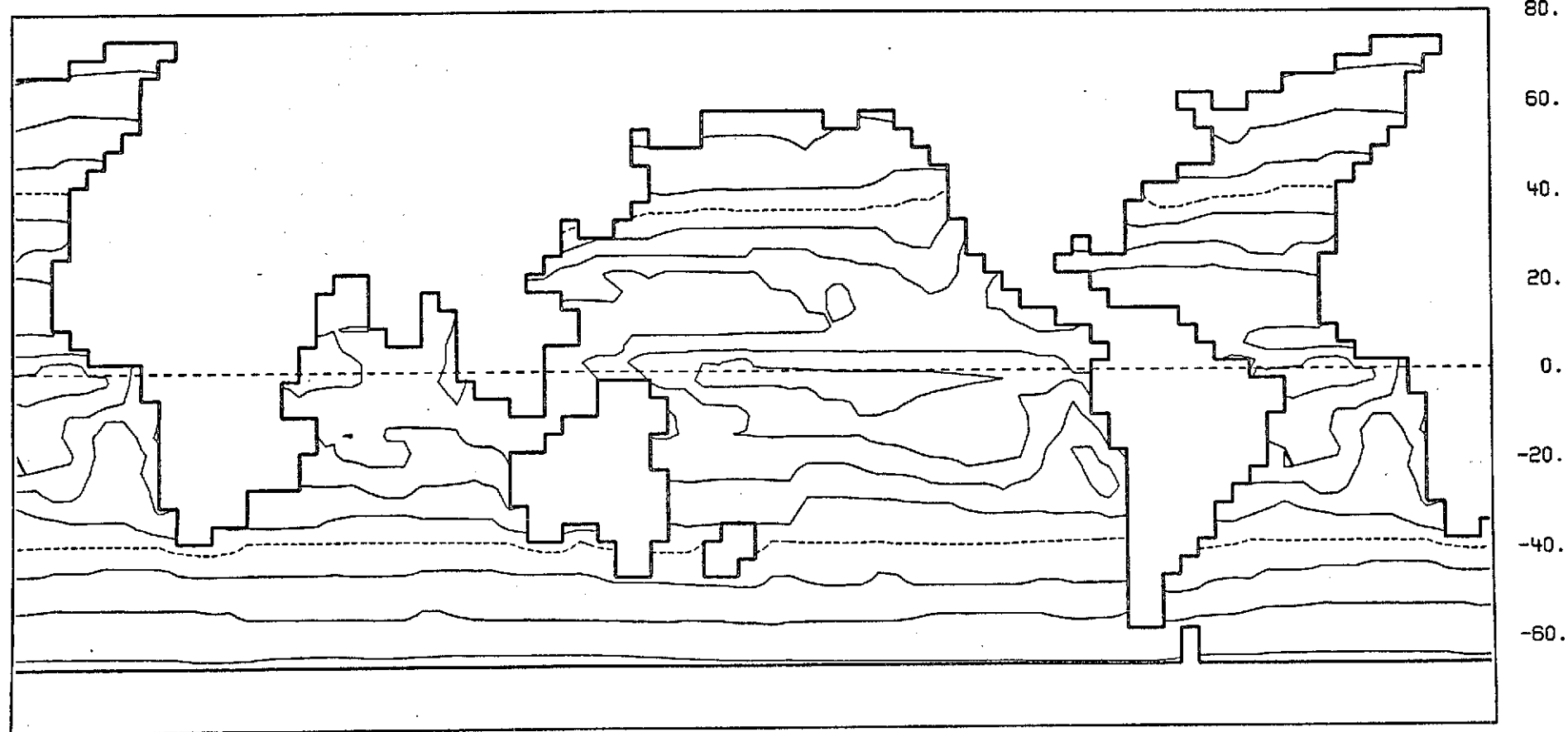
EXPERIMENT S1

DAY = 8773.7

SURFACE RADIATION FLUX (CAL/CM\*\*2/DAY)

CONTOUR INTERVAL = 60.0

DASHED LINE = 180.0

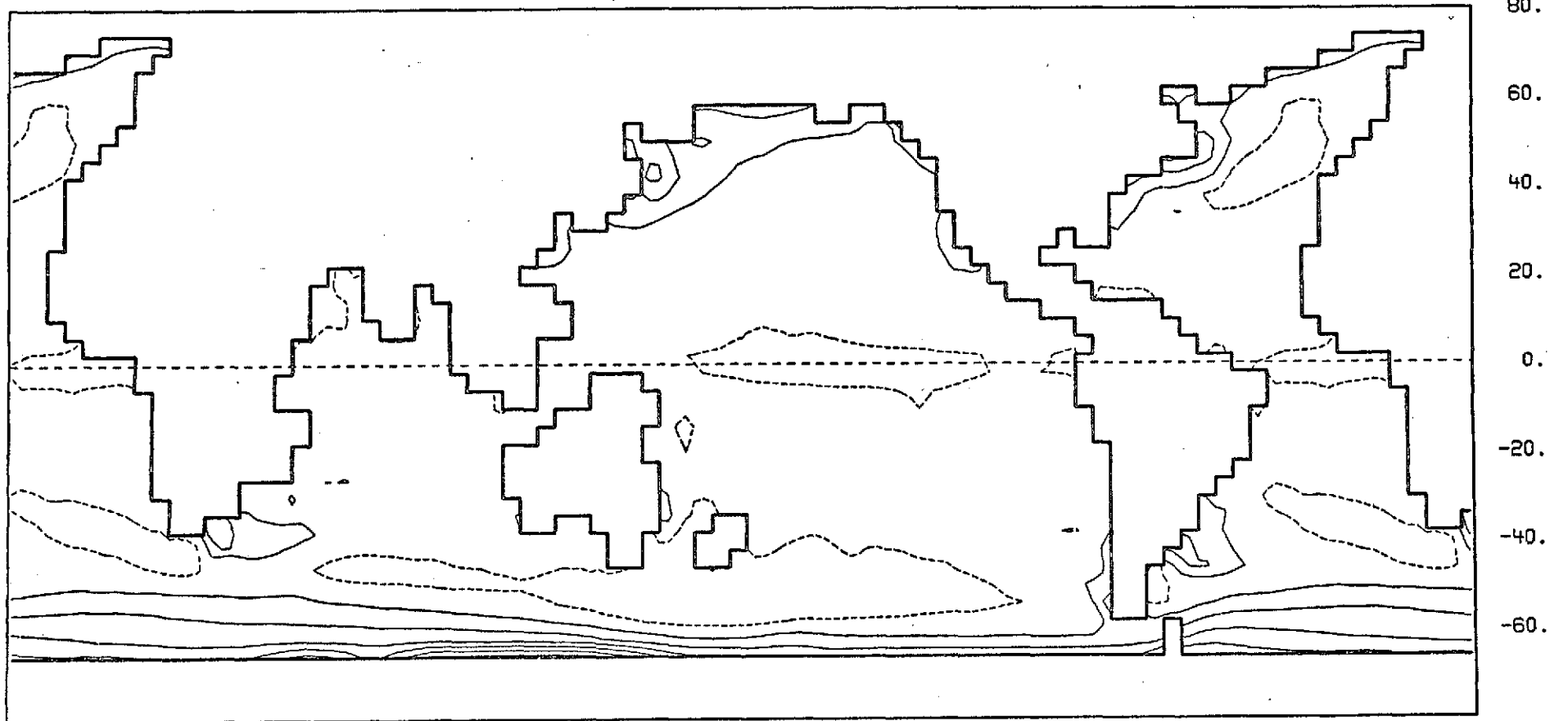


26

EXPERIMENT S1  
DAY = 8773.7

SURFACE SENSIBLE HEAT FLUX (CAL/CM\*\*2/DAY)  
CONTOUR INTERVAL = 60.0

DASHED LINE = 0.0



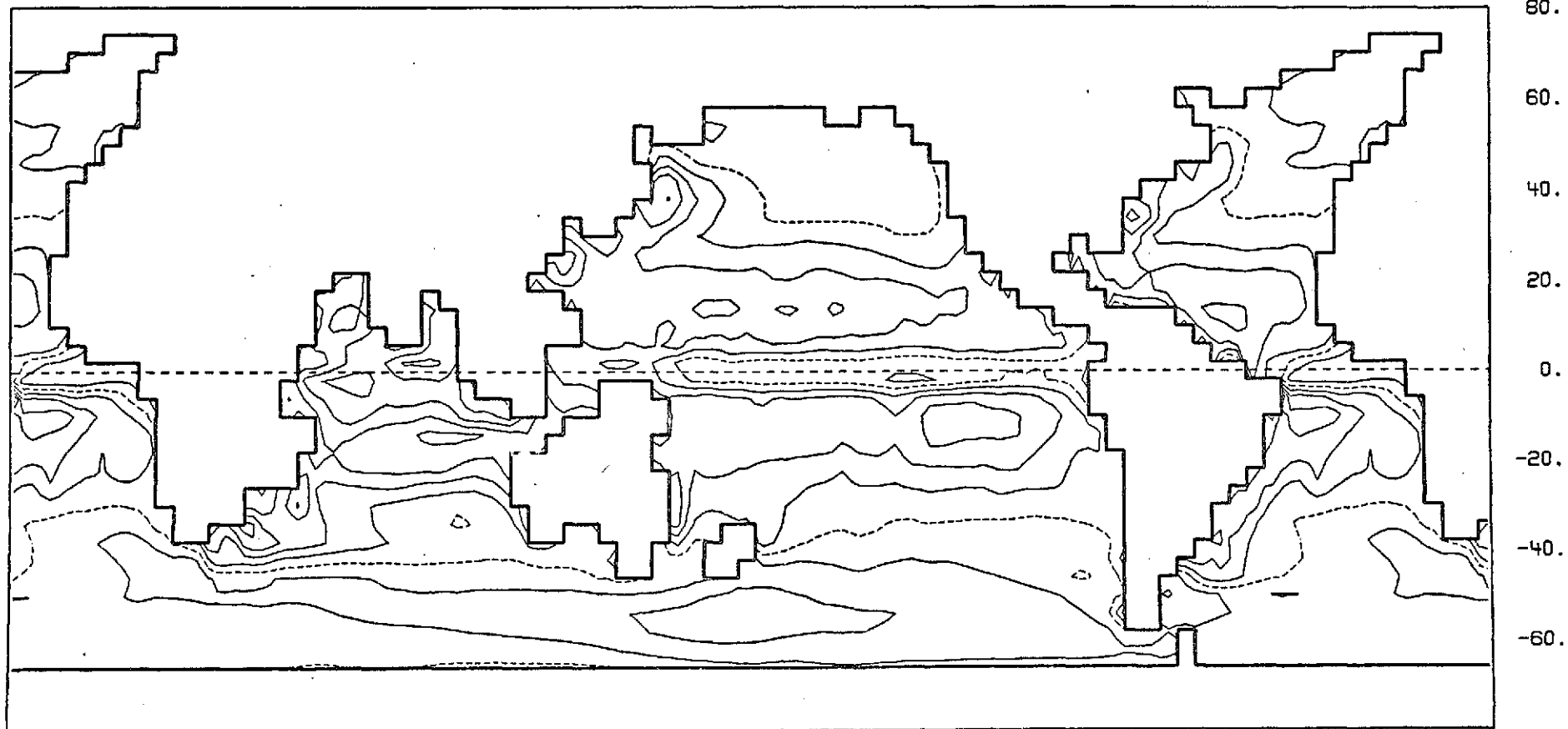
EXPERIMENT S1

SURFACE LATENT HEAT FLUX (CAL/CM\*\*2/DAY)

DAY = 8773.7

CONTOUR INTERVAL = 60.0

DASHED LINE = 180.0



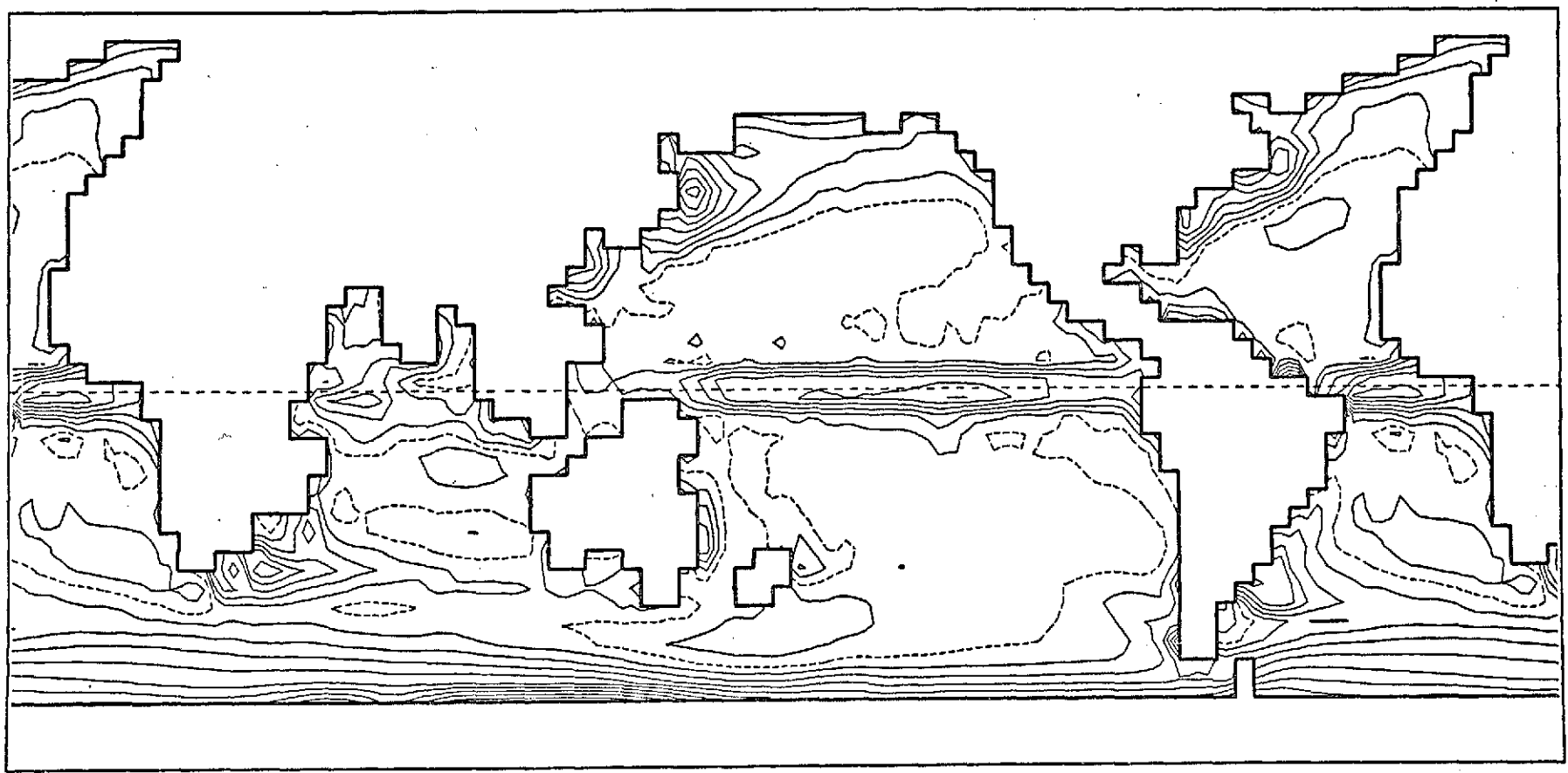
80.  
60.  
40.  
20.  
0.  
-20.  
-40.  
-60.

28

EXPERIMENT S1  
DAY = 8773.7

TOTAL SURFACE HEAT FLUX (CAL/CM\*\*2/DAY)  
CONTOUR INTERVAL = 60.0

DASHED LINE = 0.0

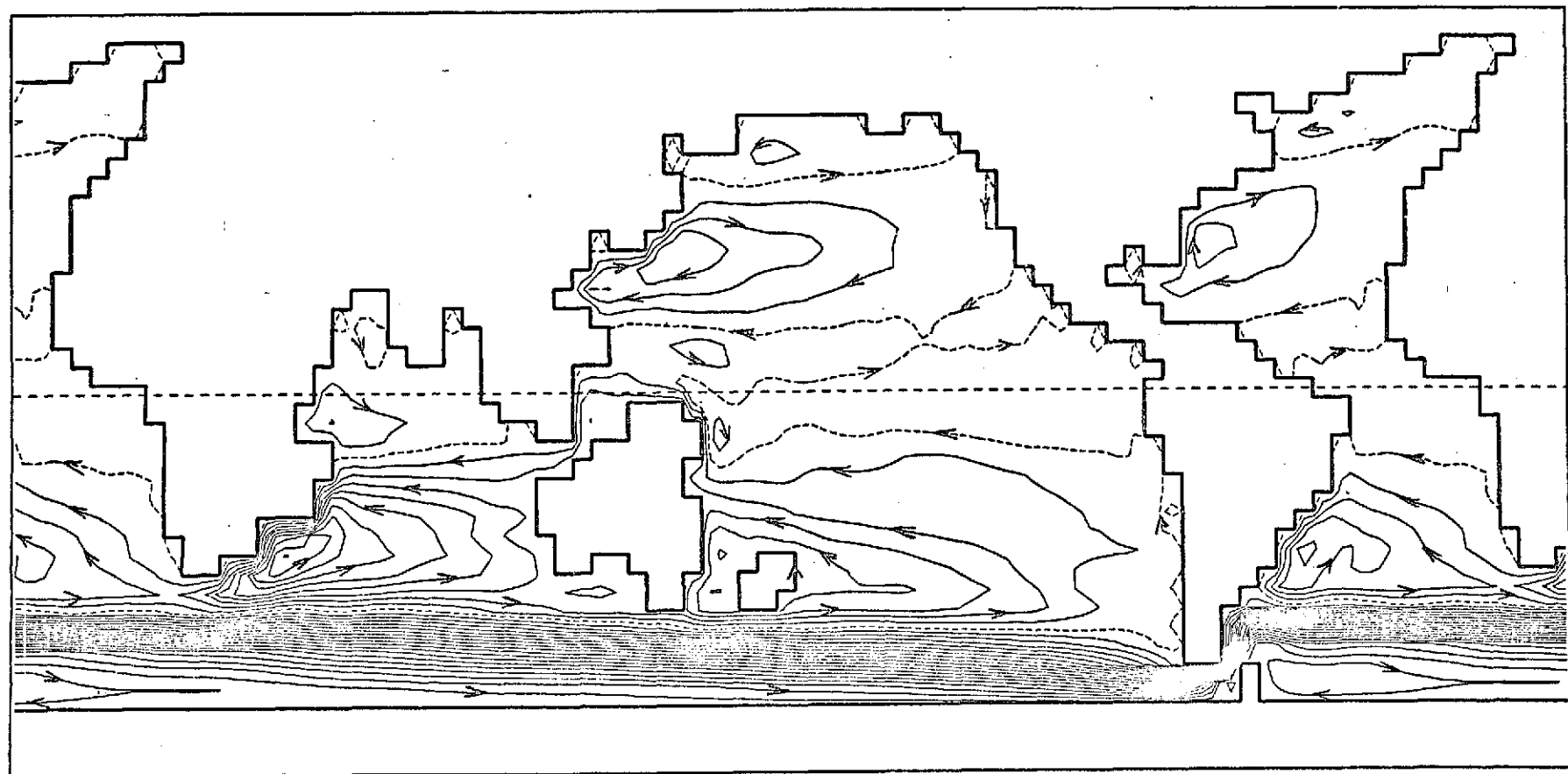


80.  
60.  
40.  
20.  
0.  
-20.  
-40.  
-60.

EXPERIMENT S1  
DAY = 0.0

STREAM LINES OF HORIZONTAL TRANSPORT (10\*\*12 CM\*\*3/SEC)  
CONTOUR INTERVAL = 10.0

DASHED LINE = 0.0



80.  
60.  
40.  
20.  
0.  
-20.  
-40.  
-60.

BAROTROPIC CIRCULATION IN A MULTI-CONNECTED GLOBAL OCEAN

MPP=0 IF THE FOUR NEAREST SURROUNDING POINTS ARE WATER POINTS,  
 =1 IF ONE OF THE FOUR NEAREST SURROUNDING POINTS IS ON THE  
 COAST OF THE MAIN LANDMASS (AFRICA, EUROPE, ASIA),  
 =3 INSIDE THE ANTARCTICA,  
 =30 ON THE COAST OF THE ANTARCTICA,  
 =4 INSIDE AUSTRALIA,  
 =40 ON THE COAST OF AUSTRALIA,  
 =5 INSIDE NEWZEALAND,  
 =50 ON THE COAST OF NEWZEALAND.

MULTIPLY THE STREAM FUNCTION VALUES BY R\*H (R=EARTH'S  
 RADIUS, H=OCEAN DEPTH) TO GET THE STREAM FUNCTION VALUES  
 FOR THE VOLUME TRANSPORT (INTEGRAL OF THE HORIZONTAL VELOCITY  
 OVER THE WHOLE DEPTH.

MQQ=1 FOR THE WATER POINTS,  
 =2 FOR THE MAIN LAND MASS,  
 =3 FOR THE ANTARCTICA,  
 =4 FOR AUSTRALIA,  
 =5 FOR NEWZEALAND.

THE SUBROUTINE HAJIME SPECIFY THE SHAPE OF THE OCEAN (MPP AND  
 MQQ), THE WIND STRESS TO COMPUTE ITS CURL AND OTHER CONSTANTS  
 AS WELL AS THE INITIAL FIELD OF THE STREAM FUNCTION.

THE SUBROUTINE RESID GIVES THE CHANGE OF THE SUM OF THE  
 RESIDUALS (RES) AT EACH SEPARATE LAND MASS WHICH TAKES PLACE  
 BY THE UNIT INCREASE OF THE STREAM FUNCTION AT EACH SEAPARATE  
 LAND MASS POINT, JUST AS IN CASE OF THE BLCK RELAXATION.

F AND G DENOTE THE STREAM FUNCTION AT TIME STEP N+1, N,  
 RESPECTIVELY, XU, XV, U, AND V THE BAROTROPIC COMPONENTS AT TIME  
 STEPS N+1, N, RESPECTIVELY.

WIND STRESS CURL=-TW/(2.0\*Y\*X(J))/R\*H

X, XM, Y=GRID SIZE

AH=COEFFICIENT OF EDDY VISCOSITY

DT IS THE TIME STEP.

H IS THE OCEAN DEPTH. CD IS THE TIME (DAY).

E IS THE WORKING SPACE FOR RELAXATION.

JM DENOTES THE EASTERNMOST POINTS TO BE SWEPT. (EX. 146)

JM DENOTES THE NORTHERNMOST PONTs TO BE SWEPT.

THE BACKWARD DIFFERENCING SCHEME IN TIME APPLIES EVERY MAT  
 TIME STEPS. MATS CONTROLS THE SWITCHING FROM THE LEAP-FROG TO  
 BACKWARD OF FROM THE BACKWARD TO LEAP-FROG SCHEMES.

PRINTING IS DONE EVERY NPRINT TIME STEPS.

WRINTING IN MAGNETIC TAPE IS DONE EVERY NTAPE TIME STEPS.

WHEN (IN) EQUALS ONE, THE IMAG-TH RECORD IN THE MAGNETIC TAPE  
 IS PICKED UP, AND THE INTEGRATION GOES ON UNTIL NN=NNEND.

REL=RELAXATION ACCURACY

WIND STRESS CURL=-TW (I, J) \*H (DEPTH)/(2.0\*Y\*X (J) \*RAD) RAD=  
 RADIUS OF THE EARTH)

IND(1)=30 ANTARCTIC COAST

IND(2)=40 AUSTRALIA COAST

IND(3)=50 NEWZEALAND COAST

INDIN(1)=3 ANTARCTIC INLAND

INDIN(2)=4 AUSTRALIA INLAND

INDIN(3)=5 NEWZEALAND INLAND

FIGURE 1 EXPLAINS THE MEANING OF LX1, LX2, LY1 AND LY2.

X=LX1	---	***	-----	X=LX2
Y=LY2		***		Y=LY2
		***		
		***		

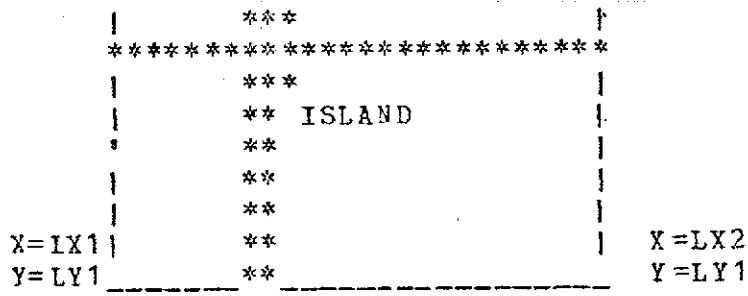


FIG. 1

L, KA, KB SPECIFY THE STREAM FUNCTION POINTS TO BE SWEEPED AND OTHER LAND POINTS TO BE SKIPPED. FIGURE 2 EXPLAINS THEIR MEANINGS.

\* POINT TO BE SWEEPED

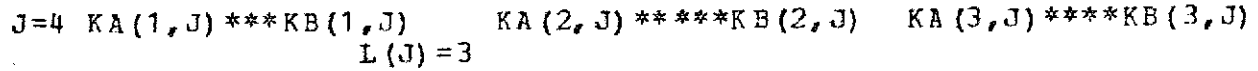


FIG. 2

THE COMPUTATION STOPS IF THE ENERGY EXCEEDS A CERTAIN VALUE, OR IF THE NUMBER OF ITERATION IN RELAXATION EXCEEDS A CERTAIN VALUE. THESE VALUES ARE SPECIFIED IN THE PROGRAM. THEY SHOULD BE CHANGED IF NECESSARY. THE COEFFICIENT OF THE OVER-RELAXATION IS GIVEN AT THE BEGINNING.

```
COMMON AH,DT,Y,H,REL, XM(39),FJU(39),X(39),F(147,39),E(147,39),  
1U(147,39),V(147,39),G(147,39),XU(147,39),XV(147,39),TW(147,39),CD,  
2BET(39),Y4,CCY,AR,ARY,RES(3), DDT,  
3MAT,L(39),LV(39),LA(10,37),LB(10,37),KA(10,37),KB(10,37),MATS,  
4MPP(147,39),MQQ(147,39),INDIN(3),IND(3),NRES(3),  
5LX1(3),LX2(3),LY1(3),LY2(3),IM,JM,IMP1,JMP1,IMM1  
SOR=1.775  
SOR=1.875  
SOR=1.825  
SOR=1.85  
SOR1=SOR-1.0  
1000 READ(5,1000) IN  
1000 FORMAT(I5)  
IF(IN.EQ.1) GO TO 1001  
CALL HAJIME  
CALL RESID  
CD=0.0  
NN=0  
MAG=0  
GO TO 5555  
1001 CONTINUE  
1001 READ(5,1000) IMAG  
IF(IMAG.EQ.1) GO TO 77  
DO 7 J=2,IMAG  
1001 READ(10)  
7 CONTINUE  
7 READ(10) XU,XV,F,G,U,V,TW,MPP,MQQ,L,KA,KB,LV,LA,LB,AH,DT,MAT,  
1Y,REL,XM,FJU,X,BET,LX1,LX2,LY1,LY2,IND,INDIN,NN,NEND,RES,  
2NRES,ARY,AR,Y4,E,CCY,MATS,CD,IM,JM,IMP1,JMP1,IMM1,MAG  
5555 CONTINUE  
AH=1.0E9  
AH=3.0E8  
AR=AH/6.37E8/6.37E8  
ARY=AR/Y  
IMAG=NN=1
```



```

NN=0.0
READ(5,5) NEND,MAT,NPRINT,NTAPE,DT,REL
5 FORMAT(4I5,2F15.7)
WRITE(6,6) IMAG,NEND,DT,REL,AH,MAT,NTAPE,NPRINT
6 FORMAT(1H,16HTIME STEP FROM I5,2X,3H TO I5,2X,3HD T=E15.7,2X,4HREL
1=E15.7,2X,3H A H=E15.7,2X,4H MAT=I3/1H,5HTAPE=I4,5X,6H PRINT=I4)
20 DAY=DT/0.864E5
MQQ(49,5)=1
MQQ(50,5)=1
MQQ(49,3)=3
MQQ(50,3)=3
39 NN=NN+1
CD=CD+DAY
NNN=(NN/MAT)*MAT
IF(NNN.EQ.NN) GO TO 25
MATS=0
DDT=DT
DO 1 J=3,JM
DO 2 I=1,IMP1
R=G(I,J)
G(I,J)=F(I,J)
F(I,J)=R
2 CONTINUE
1 CONTINUE
GO TO 26
25 MATS=1
DDT=DT*0.5
DO 42 J=3,JM
DO 43 I=1,IMP1
U(I,J)=XU(I,J)
V(I,J)=XV(I,J)
G(I,J)=F(I,J)
43 CONTINUE
42 CONTINUE
26 CONTINUE
DO 30 J=3,JM
JP1=J+1
JM1=J-1
JM2=J-2
XMJ=XM(J)
XM1=XM(JM1)
C1=Y/XMJ
S1=Y/XM1
CB=X(JP1)/Y
CS=X(J)/Y
B=X(JM1)/Y
BETJ=BET(J)*CCY
LJ=L(J)
DO 31 LL=1,LJ
II=KA(LL,J)
MM=KB(LL,J)
DO 310 I=II,MM
IP1=I+1
IM1=I-1
IM2=I-2
UIJ=U(I,J)
VIJ=V(I,J)
UP1J=U(IP1,J)
UM1J=U(IM1,J)
UIP1=U(I,JP1)
UM1P1=U(IM1,JP1)
UIM1=U(I,JM1)
UM1M1=U(IM1,JM1)
UPI1M1=U(IP1,JM1)
UIM2=U(I,JM2)
VIM2=V(I,JM2)

```

```

UM2J=U(IM2,J)
VM2J=V(IM2,J)
UM1M2=U(IM1,JM2)
VM1M2=V(IM1,JM2)
UM2M1=U(IM2,JM1)
VM2M1=V(IM2,JM1)
VP1J=V(IP1,J)
VM1J=V(IM1,J)
VIP1=V(I,JP1)
VIM1=V(I,JM1)
VM1P1=V(IM1,JP1)
VM1M1=V(IM1,JM1)
VP1M1=V(IP1,JM1)
MP=MPP(I,J)
IF(MP.EQ.0) GO TO 304
IF(MP.EQ.30) GO TO 304
IF(MP.EQ.50) GO TO 304
IF(MQQ(IP1,J).NE.2) GO TO 27
UP1J=-UIJ
VP1J=-VIJ
27 IF(MQQ(I,JP1).NE.2) GO TO 271
UIP1=-UIJ
VIP1=-VIJ
271 IF(MQQ(IM1,JP1).NE.2) GO TO 272
UM1P1=-UM1J
VM1P1=-VM1J
272 IF(MQQ(IM2,J).NE.2) GO TO 28
UM2J=-UM1J
VM2J=-VM1J
28 IF(MQQ(IM2,JM1).NE.2) GO TO 29
UM2M1=-UM1M1
VM2M1=-VM1M1
29 IF(MQQ(IM1,JM2).NE.2) GO TO 291
UM1M2=-UM1M1
VM1M2=-VM1M1
291 IF(MQQ(I,JM2).NE.2) GO TO 292
UIM2=-UIM1
VIM2=-VIM1
292 IF(MQQ(IP1,JM1).NE.2) GO TO 303
UP1M1=-UIM1
VP1M1=-VIM1
303 CONTINUE
304 DF=-BET J *(XV(I,J)+XV(IM1,J)+XV(IM1,JM1)+XV(I,JM1))*0.25
SS=(C1*(UM1J+UIJ-UM2J-UP1J)-(UIP1-UIJ+UM1P1-UM1J)*CB+2.0*CS*
1(UIJ-UIM1+UM1J-UM1M1)+S1*(UP1M1+UM2M1-UIM1-UM1M1)-(UIM1-UIM2+UM1M1
2-UM1M2)*B)*ARY+TW(I,J)+DF
DF=CS*(VIJ-VIM1-VM1J+VM1M1)
SS=AR/XMJ*(C1*(-3.0*(VIJ-VIM1J)+VP1J-VM2J)-DF
1+(VIP1-VIJ-VM1P1+VM1J)*CB)+AR/XM1*(S1*(3.0*(VM1M1-VIM1)+VP1M1
2-VM2M1)+(VM1M1-VM1M2-VIM1+VIM2)*B+DF)+SS
4 E(I,J)=-SS*DDT
310 CONTINUE
31 CONTINUE
E(2,J)=E(IM,J)
E(IMP1,J)=E(3,J)
30 CONTINUE
IP=0
37 IP=IP+1
C****ISLANDS
MAR=0
C*****ANTARCTICA
C*****NEWZEALAND
C*****AUSTRALIA
DO 5021 K=1,3
RESK=RES(K)
MP=IND(K)

```

```

MPMP=INDLN(N)
II=LX1(K)
IG=LX2(K)
IM2=LY1(K)
JM2=LY2(K)
R=0.0
DO 5016 J=IM2,JM2
DO 5015 I=II,IG
IF(MPP(I,J).NE.MP) GO TO 5015
R=R+E(I,J)
5015 CONTINUE
5016 CONTINUE
IF(ABS(R).LE.REL) GO TO 5021
DF=-R/RESK
MAR=MAR+1
IF(K.EQ.1) IM2=2
DO 5022 J=IM2,JM2
JP1=J+1
JM1=J-1
CS=Y/X(J)
CB=2.0*(CS+1.0/CS)
SS=X(JP1)/Y
C1=X(JM1)/Y
DO 5023 I=II,IG
MPPIJ=MPP(I,J)
MMMM=(MPPIJ-MP)*(MPPIJ-MPMP)
IF(MMMM.NE.0) GO TO 5023
F(I,J)=F(I,J)+DF
IM1=I-1
IP1=I+1
CCC=DF*CS
E(I,JP1)=E(I,JP1)+SS*DF
E(I,JM1)=E(I,JM1)+C1*DF
E(IP1,J)=E(IP1,J)+CCC
E(IM1,J)=E(IM1,J)+CCC
E(I,J)=E(I,J)-CB*DF
5023 CONTINUE
5022 CONTINUE
IF(K.EQ.2) GO TO 5021
IF(K.EQ.1) GO TO 5024
DO 5026 J=8,12
E(2,J)=E(IM,J)
5026 CONTINUE
GO TO 5021
5024 CONTINUE
E(IMP1,5)=E(3,5)
E(2,5)=E(IM,5)
CCC=DF*Y/X(4)
E(3,4)=E(3,4)+CCC
E(IM,4)=E(IM,4)+CCC
E(IMP1,4)=E(3,4)
E(2,4)=E(IM,4)
5021 CONTINUE
C*****NEWZEALAND
C*****ANTARCTICA
DO 32 J=4,JM
JM1=J-1
JP1=J+1
XJ=X(J)
CS=Y/XJ
SS=X(JP1)/Y
C1=X(JM1)/Y
CB=2.0*(CS+XJ/Y)
LJ=L(J)
DO 33 LL=1,LJ
TT=KA(LL,J)

```

```

IM=AB(LL,J)
DO 330 I=II,MM
IF(MPP(I,J).GE.3) GO TO 330
R=E(I,J)
IF (ABS(R).LE.REL) GO TO 330
MAR=MAR+1
DF=R/CB*SOR
E(J,J)=-R*SOR1
F(I,J)=F(I,J)+DF
IP1=I+1
CCC=DF*CS
E(IP1,J)=E(IP1,J)+CCC
IM1=I-1
E(IM1,J)=E(IM1,J)+CCC
E(I,JP1)=E(I,JP1)+SS*DF
E(I,JM1)=E(I,JM1)+C1*DF
IF(I.NE.3) GO TO 331
E(IMP1,JP1)=E(3,JP1)
E(IMP1,JM1)=E(3,JM1)
E(IMP1,J)=E(3,J)
E(IM,J)=E(2,J)
GO TO 330

```

```

331 IF(I.NE.IM) GO TO 332
E(2,J)=E(IM,J)
E(2,JP1)=E(IM,JP1)
E(2,JM1)=E(IM,JM1)
E(3,J)=E(IMP1,J)
GO TO 330

```

```

332 IF(I.NE.4) GO TO 333
E(IMP1,J)=E(3,J)
GO TO 330

```

```

333 IF(I.NE.IMM1) GO TO 330
E(2,J)=E(IM,J)

```

```

330 CONTINUE
33 CONTINUE
32 CONTINUE

```

```

IF(MAR.EQ.0) GO TO 36
IF(IP.GT.1000) GO TO 1112
IF(IP.NE.1) GO TO 37
WRITE(6,38) IP,MAR

```

```

38 FORMAT(1H ,7X,6HKAISU=I5,5X,12HTEN NO KAZU=I5)
GO TO 37

```

```

36 EN=0.0
WRITE(6,38) IP,MAR
DO 70 J=3,JM
F(1,J)=F(IMM1,J)
F(2,J)=F(IM,J)
F(IMP1,J)=F(3,J)

```

```

70 CONTINUE
DO 23 J=3,JM
JM1=J-1
JP1=J+1
XMJ=XM(J)*2.0
DF=XMJ*Y4
LVJ=LV(J)
DO 24 LJ=1,LVJ
II=LA(LJ,J)
IG=IB(LJ,J)
DO 244 I=II,IG
IP1=I+1
U(I,J)=XU(I,J)
V(I,J)=XV(I,J)
XU(I,J)=

```

```

1 (F(I,J)+F(IP1,J)-F(I,JP1)-F(IP1,JP1))/CCY

```

```

XV(I,J)=

```

```

1 (F(IP1,J)+F(IP1,JP1)-F(I,J)-F(I,JP1))/XMJ

```

```

EN=EN+DF*(XU(1,J)+*2+XV(1,J)+*2)
244 CONTINUE
* 24 CONTINUE
XU(IMP1,J)=XU(3,J)
XV(IMP1,J)=XV(3,J)
U(IMP1,J)=U(3,J)
V(IMP1,J)=V(3,J)
XU(2,J)=XU(IM,J)
XV(2,J)=XV(IM,J)
XU(1,J)=XU(IMM1,J)
XV(1,J)=XV(IMM1,J)
U(2,J)=U(IM,J)
V(2,J)=V(IM,J)
U(1,J)=U(IMM1,J)
V(1,J)=V(IMM1,J)
23 CONTINUE
WRITE(6,34) NN,CD,EN,F(1,3)
34 FORMAT(1H ,5HSTEP=I5,5X,5HTIME=E15.7,5X,7HENERGY=E15.7,5X,4HACC=F7
1.4)
IF(EN.GT.5.0E1) GO TO 1111
IF(NN.GE.NEND) GO TO 88
IF(MATS.NE.0) GO TO 10
IF(NN.NE.((NN/NTAPE)*NTAPE)) GO TO 9
MAG=MAG+1
WRITE(10) XU,XV,F,G,U,V,TW,MPP,MOQ,L,KA,KB,LV,LA,LB,AH,DT,MAT,
1Y,REL,XM,PJU,X,BET,LX1,LX2,LY1,LY2,IND,INDIN,NN,NEND,RES,
2NRES,ARY,AR,Y4,E,CCY,MATS,CD,IM,JM,IMP1,JMP1,IMM1,MAG
WRITE(6,8) MAG
9 IF(NN.EQ.((NN/NPRINT)*NPRINT)) GO TO 88
10 ENN=EN
IF(MATS.EQ.0) GO TO 39
MATS=MATS+1
IF(MATS.EQ.3) GO TO 46
DO 44 J=3,JM
DO 45 I=1,IMP1
F(I,J)=G(I,J)
U(I,J)=XU(I,J)
V(I,J)=XV(I,J)
45 CONTINUE
44 CONTINUE
GO TO 26
46 DO 47 J=3,JM
DO 48 I=1,IMP1
R=F(I,J)
F(I,J)=G(I,J)
G(I,J)=R
48 CONTINUE
47 CONTINUE
DO 49 J=3,JM
JP1=J+1
XMJ=XM(J)*2.0
LVJ=LV(J)
DO 55 LJ=1,LVJ
II=LA(LJ,J)
IG=LB(LJ,J)
DO 550 I=II,IG
IP1=I+1
U(I,J)=
1 (F(I,J)+F(IP1,J)-F(I,JP1)-F(IP1,JP1))/CCY
V(I,J)=
1 (F(IP1,J)+F(IP1,JP1)-F(I,J)-F(I,JP1))/XMJ
550 CONTINUE
55 CONTINUE
U(1,J)=U(IMM1,J)
V(1,J)=V(IMM1,J)
U(2,J)=U(IM,J)

```

```

V(2,J)=V(1H,J)
U(IMP1,J)=U(3,J)
V(IMP1,J)=V(3,J)
49 CONTINUE
MATS=0
NN=NN+1
DDT=DT
NNT=NNT+1
CD=CD+DAY
GO TO 39
88 K=1
MP=-1
613 MP=MP+1
MM=K-MP
IG=18*MP+3
IF(MM.EQ.0) GO TO 614
II=IG+17
GO TO 615
614 II=38
615 WRITE(6,701)
701 FORMAT(1H0,15HSTREAM FUNCTION)
DO 702 J=1,IMP1
WRITE(6,703) J,(F(J,I),I=IG,II)
703 FORMAT(1H ,I3,1X,18F7.4)
702 CONTINUE
IF(MM.NE.0) GO TO 613
IF(NN.LT.NEND) GO TO 10
MAG=MAG+1
WRITE(10) XU,XV,F,G,U,V,TW,MPP,MOQ,L,KA,KB,LV,LA,LE,AH,DT,MAT,
1Y,REL,XM,FJU,X,BET,LX1,LX2,LY1,LY2,IND,INDIN,NN,NEND,RES,
2NRES,ARY,AR,Y4,E,CCY,MATS,CD,IM,JM,IMP1,JMP1,IMM1,MAG
WRITE(6,8) MAG
8 FORMAT(1H0,32HNO. OF RECORDS IN MAGNETIC TAPE=I3)
GO TO 1111
1112 WRITE(6,38) IP,MAR
1111 STOP
END
SUBROUTINE RESID
RETURN
END
SUBROUTINE HAJIME
RETURN
END
SUBROUTINE RESID
COMMON AH,DT,Y,H,REL,XM(39),FJU(39),X(39),F(147,39),E(147,39),
1U(147,39),V(147,39),G(147,39),XU(147,39),XV(147,39),TW(147,39),CD,
2BET(39),Y4,CCY,AR,ARY,RES(3),DDT,
3MAT,L(39),LV(39),LA(10,37),LB(10,37),KA(10,37),KB(10,37),MATS,
4MPP(147,39),MOQ(147,39),INDIN(3),IND(3),NRES(3),
5LX1(3),LX2(3),LY1(3),LY2(3),IM,JM,IMP1,JMP1,IMM1
DO 1 K=1,3
DO 8 J=1,JMP1
DO 9 I=1,IMP1
E(I,J)=0.0
9 CONTINUE
CONTINUE
S=0.0
I1=LX1(K)
I2=LX2(K)
J1=LY1(K)
J2=LY2(K)
MIN=IND(K)
MININ=INDIN(K)
NUM=0
IF(K.EQ.1) J1=2
DO 3 J=J1,J2

```

```

JM1=J-1
JP1=J+1
CS=Y/X(J)
C1=X(JM1)/Y
SS=X(JP1)/Y
CB=-2.0*(CS+1.0/CS)
DO 4 I=I1,I2
MP=MPP(I,J)
MMM=(MP-MIN)*(MP-MININ)
IF(MMM.NE.0) GO TO 4
IP1=I+1
IM1=I-1
NUM=NUM+1
E(I,J)=E(I,J)+CB
E(IP1,J)=E(IP1,J)+CS
E(IM1,J)=E(IM1,J)+CS
E(I,JP1)=E(I,JP1)+SS
E(I,JM1)=E(I,JM1)+C1
4 CONTINUE
3 CONTINUE
IF(K.GE.2) GO TO 10
J1=3
DO 11 J=3,3
CS=Y/X(J)
E(3,J)=E(3,J)+CS
E(IM,J)=E(IM,J)+CS
11 CONTINUE
10 CONTINUE
DO 5 J=J1,J2
DO 6 I=I1,I2
IF(MPP(I,J).EQ.MIN) S=S+E(I,J)
6 CONTINUE
5 CONTINUE
NRES(K)=NUM
RES(K)=S
WRITE(6,7) K,NUM,S
7 FORMAT(1H ,2HK=I2,2X,12HGRID POINTS=I3,2X,4HRES=E15.7)
1 CONTINUE
DO 16 J=1,18
DO 17 I=1,IMP1
IF(MQQ(I,J).EQ.1) GO TO 17
MP=MPP(I,J)
IF(MP.EQ.2) GO TO 17
IF(MP.EQ.((MP/3)*3)) GO TO 18
IF(MP.EQ.((MP/4)*4)) GO TO 19
MQQ(I,J)=5
GO TO 17
18 MQQ(I,J)=3
GO TO 17
19 MQQ(I,J)=4
17 CONTINUE
16 CONTINUE
WRITE(6,15) (I,I=1,38)
15 FORMAT(1H ,4X,38I3)
DO 12 I=1,IMP1
WRITE(6,14) I,(MPP(I,J),J=1,38)
WRITE(6,13) I,(MQQ(I,J),J=1,38)
12 CONTINUE
13 FORMAT(1H ,I3,3X,38I3)
14 FORMAT(1H ,I3,2X,38I3)
RETURN
END
SUBROUTINE HAJIME

```

DATA:

IM, JM, IMH, JMH

OCEAN SHAPE (SUBROUTINE SHAPE 1)  
X,DX,DY (DX AND DY ARE THE GRID SIZES IN LONGITUDE AND  
LATITUDE (DEGREES), RESPECTIVELY. Y IS THE LATITUDE  
CORRESPONDING TO J=0).

AH,H, REL,DT,MAT

IT: IT=1 WIND STRESS IS READ TO COMPUTE THE WIND STRESS CURL.  
IT=2 WIND STRESS CURL IS GIVEN FROM CARDS, A MAGNETIC  
TAPE, OR THE SUBROUTINE CURL.

COMMON AH,DT,Y,H,REL,XM(39),FJU(39),X(39),F(147,39),E(147,39),  
1U(147,39),V(147,39),G(147,39),XU(147,39),XV(147,39),TW(147,39),CD,  
2BET(39),Y4,CCY,AR,ARY,RES(3), DDT,  
3MAT,L(39),LV(39),LA(10,37),LB(10,37),KA(10,37),KB(10,37),MATS,  
4MPP(147,39),MQQ(147,39),INDIN(3),IND(3),NRES(3),  
5LX1(3),LX2(3),LY1(3),LY2(3),IM,JM,IMP1,JMP1,IMM1  
DIMENSION L1(9),WE(147,39),WN(147,39),C(39)  
EQUIVALENCE (U(1),WE(1)), (V(1),WN(1))  
READ(5,40) IM,JM,IMH,JMH

40 FORMAT(4I5)  
IMP1=IM+1  
IMM1=IM-1  
JMP1=JM+1

CALL SHAPE1  
CALL SHAPE 1  
DO 548 J=1,MM  
DO 549 I=1,IMP1  
F(I,J)=0.0  
G(I,J)=0.0  
U(I,J)=0.0  
V(I,J)=0.0  
XU(I,J)=0.0  
XV(I,J)=0.0

549 CONTINUE  
548 CONTINUE

READ(5,18) Y,DX,DY  
18 FORMAT(3F10.0)  
P=3.1415926/180.0  
DX=DX\*P  
MM=JM+2  
DO 100 I=1,MM  
AR=(Y+DY\*FLOAT(I))\*P  
F1=COS(AR)  
X(I)=DX\*F1  
C(I)=F1  
BET(I)=F1\*X(I)\*14.58E-5

100 CONTINUE  
Y=DY\*P  
CD=14.58/(DX\*Y)  
DO 9997 J=1,JMP1  
XM(J)=(X(J)+X(J+1))/2.0  
FJU(J)=CD\*(X(J)-X(J+1))

9997 CONTINUE  
READ(5,16) AH,H,REL,DT,MAT

16 FORMAT(4E15.7,I5)  
WRITE(6,17) AH,H,REL  
17 FORMAT(1H,15HEDDY VISCOSITY=E15.7,10X,6HDEPTH=E15.7,10X,  
11SHRELAX ACCURACY=E15.7)

READ(5,10) IT  
10 FORMAT(I5)  
GO TO (1,2), IT

1 CONTINUE  
CALL WIND  
CALL WIND  
P=0.01/4.0E5  
DO 540 J=JMH,JMP1  
XMJ=XM(J)

C  
C  
C  
C  
C  
C  
C  
C  
C  
C

C

C



```

JM1=J-1
XM1=XM(JM1)
DO 541 I=IMH, IM
IM1=I-1
TW(I, J) = (XMJ* (-WE(I, J) -WE(IM1, J)) +XM1*(WE(I, JM1) +WE(IM1, JM1))
1      + Y*(WN(I, J) +WN(I, JM1) -WN(IM1, J) -WN(IM1, JM1))) *P
41 CONTINUE
TW(1, J) =TW(IMM1, J)
TW(2, J) =TW(IM, J)
TW(IMP1, J) =TW(IMH, J)
540 CONTINUE
GO TO 3
2 CONTINUE
C CALL CURL
CALL CURL
READ(5, 6004) (TW(I, J), I=3, IM)
6004 FORMAT(5E15.7)
TW(IMP1, J) =TW(3, J)
TW(2, J) =TW(IM, J)
TW(1, J) =TW(IMM1, J)
3 CONTINUE
C INITIAL GUESS
DO 4000 J=4, JM
CJ=1.0/(C(J)*Y*14.58E-5)/4.0
LJ=L(J)
DO 360 LL=1, LJ
II=KA(LL, J)
IG=KB(LL, J)
MP=II+IG
362 DO 361 I=II, IG
MM=MP-I
K=MM+1
P=F(K, J) - (TW(MM, J) +TW(K, J)) *CJ
P(MM, J) =P
361 CONTINUE
IF(II.NE.3) GO TO 360
F(IMP1, J) =F(3, J)
360 CONTINUE
F(1, J) =F(IMM1, J)
F(2, J) =F(IM, J)
4000 CONTINUE
C INITIAL GUESS
CCC=2.0*Y
DO 4049 J=3, JM
JP1=J+1
LJ=LV(J)
DO 4058 LL=1, LJ
II=LA(LL, J)
IG=LB(LL, J)
DO 4053 I=II, IG
IP1=I+1
P=(F(I, J) +F(IP1, J) -F(I, JP1) -F(IP1, JP1))/CCC
U(I, J) =P
XU(I, J) =P
P=(F(IP1, J) +F(IP1, JP1) -F(I, J) -F(I, JP1))/XMJ
V(I, J) =P
XV(I, J) =P
53 CONTINUE
4058 CONTINUE
XU(IMP1, J) =XU(3, J)
XV(IMP1, J) =XV(3, J)
XU(2, J) =XU(IM, J)
XV(2, J) =XV(IM, J)
XU(1, J) =XU(IMM1, J)
XV(1, J) =XV(IMM1, J)
U(IMP1, J) =U(3, J)

```

V (IMP1, J) = V (3, J)

U (2, J) = U (IM, J)

V (2, J) = V (IM, J)

U (1, J) = U (IMM1, J)

V (1, J) = V (IMM1, J)

4049 CONTINUE

AR=AH/6.37E8/6.37E8

ARY=AR/Y

CCY=2.0\*Y

Y4=Y\*0.25

RETURN

END

SUBROUTINE SHAPE1

SUBROUTINE TO BE USED FOR THE BAROTROPIC PART OF THE WORLD OCEAN CIRCULATION WHEN THE SHAPE OF THE OCEAN IS CHANGED.

DATA: LV, LA AND LB FOR MQQ.

MM, M1(K), M2(K) AND M3(K) FOR MPP.

LV, LA AND LB ARE THE SAME AS THOSE USED FOR THE SUBROUTINE SHAPE 2 (BAROCLINIC PART), BUT THE DATA FOR MPP ARE DIFFERENT FROM THOSE USED FOR THE SHAPE2.

LX1, LX2, LY1, LY2 WHICH SPECIFY THE AREAS INCLUDING THE SEPARATE ISLANDS.

COMMON AH, DT, Y, H, REL, XM(39), FJU(39), X(39), F(147,39), E(147,39), 1U(147,39), V(147,39), G(147,39), XU(147,39), XV(147,39), TW(147,39), CD, 2BET(39), Y4, CCY, AR, ARY, RES(3), DDT, 3MAT, L(39), LV(39), LA(10,37), LB(10,37), KA(10,37), KB(10,37), MATS, 4MPP(147,39), MQQ(147,39), INDIN(3), IND(3), NRES(3), 5LX1(3), LX2(3), LY1(3), LY2(3), IM, JM, IMP1, JMP1, IMM1

IMM1=IM-1

IMP1=IM+1

JMM1=JM-1

JMP1=JM+1

JMH=3

IMH=3

DO 30 J=1, JM

DO 31 I=1, IMP1

MQQ(I, J)=2

31 CONTINUE

30 CONTINUE

DO 32 J=3, JMM1

READ(5, 33) M

33 FORMAT(I2)

READ(5, 34) (LA(I, J), LB(I, J), I=1, M)

34 FORMAT(7(2I4, 2X))

DO 35 I=1, M

II=LA(I, J)

IG=LB(I, J)

DO 36 N=II, IG

MQQ(N, J)=1

36 CONTINUE

35 CONTINUE

LV(J)=M

MQQ(1, J)=MQQ(IMM1, J)

MQQ(2, J)=MQQ(IM, J)

MQQ(IMP1, J)=MQQ(3, J)

32 CONTINUE

DO 3006 J=3, 38

READ(5, 3007) MM

3007 FORMAT(I2)

READ(5, 3008) (M1(K), M2(K), M3(K), K=1, MM)

3008 FORMAT(8(2I4, I2))

DO 3009 K=1, MM

K5=M1(K)

K6=M2(K)

K7=M3(K)

DO 3010 I=K5, K6

```

MPP1(I,J)=K7
3010 CONTINUE
3009 CONTINUE
3006 CONTINUE
DO 3011 J=3,38
READ(5,3007) MM
L1(J)=MM
READ(5,3012) (KA1(LL,J),KB1(LL,J),LL=1,MM)
3012 FORMAT(16I5)
3011 CONTINUE
DO 6003 J=1,JMP1
MPP1(1,J)=MPP1(IMM1,J)
MPP1(2,J)=MPP1(IM,J)
MPP1(IMP1,J)=MPP1(3,J)
6003 CONTINUE
DO 6004 J=3,JM
JP1=J+1
JM1=J-1
DO 6005 I=3,IM
IF(MPP1(I,J).GT.1) GO TO 6005
IF(MPP1(I-1,J).EQ.2) GO TO 6005
IF(MPP1(I,JP1).EQ.2) GO TO 6005
IF(MPP1(I,JM1).EQ.2) GO TO 6005
IF(MPP1(I+1,J).EQ.2) GO TO 6005
MPP1(I,J)=0
6005 CONTINUE
MPP1(IMP1,J)=MPP1(3,J)
MPP1(2,J)=MPP1(IM,J)
MPP1(1,J)=MPP1(IMM1,J)
6004 CONTINUE
WRITE(6,6016) (J,J=3,38)
6016 FORMAT(1H,5X,38I3/)
DO 6012 I=1,IMP1
WRITE(6,6014) I,(MPP1(I,J),J=3,38)
WRITE(6,6015) (MQQ(I,J),J=3,38)
6012 CONTINUE
6014 FORMAT(1H,I3,2X,38I3)
6015 FORMAT(1H,6X,38I3)
READ(5,2) (LX1(K),LX2(K),LY1(K),LY2(K),K=1,3)
2 FORMAT(4I5)
RETURN
END
SUBROUTINE WIND
COMMON AH,DT,Y,H,REL,XM(39),FJU(39),X(39),F(147,39),E(147,39),
1U(147,39),V(147,39),G(147,39),XU(147,39),XV(147,39),TW(147,39),CD,
2BET(39),Y4,CCY,AR,ARY,RES(3),DDT,
3MAT,L(39),LV(39),LA(10,37),LB(10,37),KA(10,37),KB(10,37),MATS,
4MPP(147,39),MQQ(147,39),INDIN(3),IND(3),NRES(3),
5LX1(3),LX2(3),LY1(3),LY2(3),IM,JM,IMP1,JMP1,IMM1
DIMENSION WE(147,7),WN(147,7)
RETURN
END
SUBROUTINE CURL
RETURN
END

```

BAROTROPIC CIRCULATION IN A MULTI-CONNECTED GLOBAL OCEAN

MPP=0 IF THE FOUR NEAREST SURROUNDING POINTS ARE WATER POINTS,  
 =1 IF ONE OF THE FOUR NEAREST SURROUNDING POINTS IS ON THE  
 COAST OF THE MAIN LANDMASS (AFRICA, EUROPE, ASIA),  
 =3 INSIDE THE ANTARCTICA,  
 =30 ON THE COAST OF THE ANTARCTICA,  
 =4 INSIDE AUSTRALIA,  
 =40 ON THE COAST OF AUSTRALIA,  
 =5 INSIDE NEWZEALAND,  
 =50 ON THE COAST OF NEWZEALAND.

MULTIPLY THE STREAM FUNCTION VALUES BY R\*H (R=EARTH'S  
 RADIUS, H=OCEAN DEPTH) TO GET THE STREAM FUNCTION VALUES  
 FOR THE VOLUME TRANSPORT (INTEGRAL OF THE HORIZONTAL VELOCITY  
 OVER THE WHOLE DEPTH.

MQQ=1 FOR THE WATER POINTS,  
 =2 FOR THE MAIN LAND MASS,  
 =3 FOR THE ANTARCTICA,  
 =4 FOR AUSTRALIA,  
 =5 FOR NEWZEALAND.

THE SUBROUTINE HAJIME SPECIFY THE SHAPE OF THE OCEAN (MPP AND  
 MQQ), THE WIND STRESS TO COMPUTE ITS CURL AND OTHER CONSTANTS  
 AS WELL AS THE INITIAL FIELD OF THE STREAM FUNCTION.

THE SUBROUTINE RESID GIVES THE CHANGE OF THE SUM OF THE  
 RESIDUALS (RES) AT EACH SEPARATE LAND MASS WHICH TAKES PLACE  
 BY THE UNIT INCREASE OF THE STREAM FUNCTION AT EACH SEPARATE  
 LAND MASS POINT, JUST AS IN CASE OF THE BLOCK RELAXATION.

F AND G DENOTE THE STREAM FUNCTION AT TIME STEP N+1, N,  
 RESPECTIVELY, XU, XV, U, AND V THE BAROTROPIC COMPONENTS AT TIME  
 STEPS N+1, N, RESPECTIVELY.

WIND STRESS CURL=-TW/(2.0\*Y\*X(J))/R\*H

X, XM, Y=GRID SIZE

AH=COEFFICIENT OF EDDY VISCOSITY

DT IS THE TIME STEP.

H IS THE OCEAN DEPTH. CD IS THE TIME (DAY).

E IS THE WORKING SPACE FOR RELAXATION.

IM DENOTES THE EASTERNMOST POINTS TO BE SWEEPED. (EX. 146)

JM DENOTES THE NORTHERNMOST POINTS TO BE SWEEPED.

THE BACKWARD DIFFERENCING SCHEME IN TIME APPLIES EVERY MAT  
 TIME STEPS. MATS CONTROLS THE SWITCHING FROM THE LEAP-FROG TO  
 BACKWARD OF FROM THE BACKWARD TO LEAP-FROG SCHEMES.

PRINTING IS DONE EVERY NPRINT TIME STEPS.

WRITING IN MAGNETIC TAPE IS DONE EVERY NTAPE TIME STEPS.

WHEN (IN) EQUALS ONE, THE IMAG-TH RECORD IN THE MAGNETIC TAPE  
 IS PICKED UP, AND THE INTEGRATION GOES ON UNTIL NN=NEND.

REL=RELAXATION ACCURACY

WIND STRESS CURL=-TW(I, J)\*H (DEPTH)/(2.0\*Y\*X(J)\*RAD) RAD=  
 RADIUS OF THE EARTH)

IND(1)=30 ANTARCTIC COAST

IND(2)=40 AUSTRALIA COAST

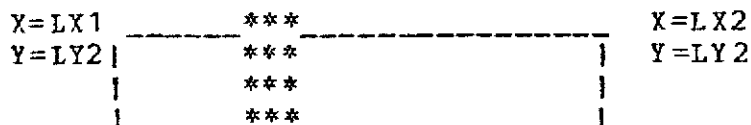
IND(3)=50 NEWZEALAND COAST

INDIN(1)=3 ANTARCTIC INLAND

INDIN(2)=4 AUSTRALIA INLAND

INDIN(3)=5 NEWZEALAND INLAND

FIGURE 1 EXPLAINS THE MEANING OF LX1, LX2, IY1 AND LY2.



```

*****
|      ***      |
|      ** ISLAND |
|      **      |
|      **      |
|      **      |
|      **      |
X=LX1 |      **      | X=LX2
Y=LY1 |      **      | Y=LY1
-----

```

FIG. 1

L, KA, KB SPECIFY THE STREAM FUNCTION POINTS TO BE SWEEPED AND OTHER LAND POINTS TO BE SKIPPED. FIGURE 2 EXPLAINS THEIR MEANINGS.

\* POINT TO BE SWEEPED

```

J=4 KA (1, J) *** KB (1, J)   KA (2, J) *** KB (2, J)   KA (3, J) *** KB (3, J)
                      L (J) =3

```

FIG. 2

THE COMPUTATION STOPS IF THE ENERGY EXCEEDS A CERTAIN VALUE, OR IF THE NUMBER OF ITERATION IN RELAXATION EXCEEDS A CERTAIN VALUE. THESE VALUES ARE SPECIFIED IN THE PROGRAM. THEY SHOULD BE CHANGED IF NECESSARY. THE COEFFICIENT OF THE OVER-RELAXATION IS GIVEN AT THE BEGINNING.

```

COMMON AH,DT,Y,H,REL,XM(39),FJU(39),X(39),F(147,39),E(147,39),
1U(147,39),V(147,39),G(147,39),XU(147,39),XV(147,39),TW(147,39),CD,
2BET(39),Y4,CCY,AR,ARY,RES(3),DDT,
3MAT,L(39),LV(39),LA(10,37),LB(10,37),KA(10,37),KB(10,37),MATS,
4MPP(147,39),MQQ(147,39),INDIN(3),IND(3),NRES(3),
5LX1(3),LX2(3),LY1(3),LY2(3),IM,JM,IMP1,JMP1,IMM1
SOR=1.775
SOR=1.875
SOR=1.825
SOR=1.85
SOR1=SOR-1.0
1000 READ(5,1000) IN
      FORMAT(I5)
      IF(IN.EQ.1) GO TO 1001
      CALL HAJIME
      CALL RESID
      CD=0.0
      NN=0
      MAG=0
      GO TO 5555
1001 CONTINUE
      READ(5,1000) IMAG
      IF(IMAG.EQ.1) GO TO 77
      DO 7 J=2,IMAG
      READ(10)
7 CONTINUE
77 READ(10) XU,XV,F,G,U,V,TW,MPP,MQQ,L,KA,KB,LV,LA,LB,AH,DT,MAT,
1Y,REL,XM,FJU,X,BET,LX1,LX2,LY1,LY2,IND,INDIN,NN,NEND,RES,
2NRES,ARY,AR,Y4,E,CCY,MATS,CD,IM,JM,IMP1,JMP1,IMM1,MAG
5555 CONTINUE
      AH=1.0E9
      AH=3.0E8
      AR=AH/6.37E8/6.37E8
      ARY=AR/Y
      IMAG=NN+1

```

```

NN=0.0
READ(5,5) NEND,MAT,NPRINT,NTAPE,DT,REL
5 FORMAT(4I5,2E15.7)
WRITE(6,6) IMAG,NEND,DT,REL,AH,MAT,NTAPE,NPRINT
6 FORMAT(1H,16HTIME STEP FROM I5,2X,3HTO I5,2X,3HDT=E15.7,2X,4HREL
1=E15.7,2X,3HAH=E15.7,2X,4HMAT=I3/1H,5HTAPE=I4,5X,6HPRINT=I4)
20 DAY=DT/0.864E5
MQQ(49,5)=1
MQQ(50,5)=1
MQQ(49,3)=3
MQQ(50,3)=3
39 NN=NN+1
CD=CD+DAY
NNN=(NN/MAT)*MAT
IF(NNN.EQ.NN) GO TO 25
MATS=0
DDT=DT
DO 1 J=3,JM
DO 2 I=1,IMP1
R=G(I,J)
G(I,J)=F(I,J)
F(I,J)=R
2 CONTINUE
1 CONTINUE
GO TO 26
25 MATS=1
DDT=DT*0.5
DO 42 J=3,JM
DO 43 I=1,IMP1
U(I,J)=XU(I,J)
V(I,J)=XV(I,J)
G(I,J)=F(I,J)
43 CONTINUE
42 CONTINUE
26 CONTINUE
DO 30 J=3,JM
JP1=J+1
JM1=J-1
JM2=J-2
XMJ=XM(J)
XM1=XM(JM1)
C1=Y/XMJ
S1=Y/XM1
CB=X(JP1)/Y
CS=X(J)/Y
B=X(JM1)/Y
BETJ=BET(J)*CCY
LJ=L(J)
DO 31 LL=1,LJ
II=KA(LL,J)
MM=KB(LL,J)
DO 310 I=II,MM
IP1=I+1
IM1=I-1
IM2=I-2
UIJ=U(I,J)
VIJ=V(I,J)
UP1J=U(IP1,J)
UM1J=U(IM1,J)
UIP1=U(I,JP1)
UM1P1=U(IM1,JP1)
UIM1=U(I,JM1)
UM1M1=U(IM1,JM1)
UPIM1=U(IP1,JM1)
UIM2=U(I,JM2)
VIM2=V(I,JM2)

```

```

UM2J=U(IM2,J)
VM2J=V(IM2,J)
UM1M2=U(IM1,JM2)
VM1M2=V(IM1,JM2)
UM2M1=U(IM2,JM1)
VM2M1=V(IM2,JM1)
VP1J=V(IP1,J)
VM1J=V(IM1,J)
VIP1=V(I,JP1)
VIM1=V(I,JM1)
VM1P1=V(IM1,JP1)
VM1M1=V(IM1,JM1)
VP1M1=V(IP1,JM1)
MP=MPE(I,J)
IF(MP.EQ.0) GO TO 304
IF(MP.EQ.30) GO TO 304
IF(MP.EQ.50) GO TO 304
IF(MQQ(IP1,J).NE.2) GO TO 27
UP1J=-UIJ
VP1J=-VIJ
27 IF(MQQ(I,JP1).NE.2) GO TO 271
UIP1=-UIJ
VIP1=-VIJ
271 IF(MQQ(IM1,JP1).NE.2) GO TO 272
UM1P1=-UM1J
VM1P1=-VM1J
272 IF(MQQ(IM2,J).NE.2) GO TO 28
UM2J=-UM1J
VM2J=-VM1J
28 IF(MQQ(IM2,JM1).NE.2) GO TO 29
UM2M1=-UM1M1
VM2M1=-VM1M1
29 IF(MQQ(IM1,JM2).NE.2) GO TO 291
UM1M2=-UM1M1
VM1M2=-VM1M1
291 IF(MQQ(I,JM2).NE.2) GO TO 292
UIM2=-UIM1
VIM2=-VIM1
292 IF(MQQ(IP1,JM1).NE.2) GO TO 303
UP1M1=-UIM1
VP1M1=-VIM1
303 CONTINUE
304 DF=-BET J *(XV(I,J)+XV(IM1,J)+XV(IM1,JM1)+XV(I,JM1))*0.25
SS=(C1*(UM1J+UIJ-UM2J-UP1J)-(UIP1-UIJ+UM1P1-UM1J)*CB+2.0*CS*
1(UIJ-UIM1+UM1J-UM1M1)+S1*(UP1M1+UM2M1-UIM1-UM1M1)-(UIM1-UIM2+UM1M1
2-UM1M2)*B)*ARY+TW(I,J)+DF
DF=CS*(VIJ-VIM1-VM1J+VM1M1)
SS= AR/XMJ*(C1*(-3.0*(VIJ-VM1J)+VP1J-VM2J)-DF
1+(VIP1-VIJ-VM1P1+VM1J)*CB)+AR/XM1*(S1*(3.0*(VM1M1-VIM1)+VP1M1
2-VM2M1)+(VM1M1-VM1M2-VIM1+VIM2)*B+DF)+SS
4 E(I,J)=-SS*DDT
310 CONTINUE
31 CONTINUE
E(2,J)=E(IM,J)
E(IMP1,J)=E(3,J)
30 CONTINUE
IP=0
37 IP=IP+1
C***ISLANDS
MAR=0
C*****ANTARCTICA
C*****NEWZEALAND
C*****AUSTRALIA
DO 5021 K=1,3
RESK=RES(K)
MP=IND(K)

```

```

MPP=INDL(I,K)
II=LX1(K)
IG=LX2(K)
IM2=LY1(K)
JM2=LY2(K)
R=0.0
DO 5016 J=IM2,JM2
DO 5015 I=II,IG
IF(MPP(I,J).NE.MP) GO TO 5015
R=R+E(I,J)
5015 CONTINUE
5016 CONTINUE
IF(ABS(R).LE.REL) GO TO 5021
DF=-R/RESK
MAR=MAR+1
IF(K.EQ.1) IM2=2
DO 5022 J=IM2,JM2
JP1=J+1
JM1=J-1
CS=Y/X(J)
CB=2.0*(CS+1.0/CS)
SS=X(JP1)/Y
C1=X(JM1)/Y
DO 5023 I=II,IG
MPPIJ=MPP(I,J)
MMMM=(MPPIJ-MP)*(MPPIJ-MPMP)
IF(MMMM.NE.0) GO TO 5023
F(I,J)=F(I,J)+DF
IM1=I-1
IP1=I+1
CCC=DF*CS
E(I,JP1)=E(I,JP1)+SS*DF
E(I,JM1)=E(I,JM1)+C1*DF
E(IP1,J)=E(IP1,J)+CCC
E(IM1,J)=E(IM1,J)+CCC
E(I,J)=E(I,J)-CB*DF
5023 CONTINUE
5022 CONTINUE
IF(K.EQ.2) GO TO 5021
IF(K.EQ.1) GO TO 5024
DO 5026 J=8,12
E(2,J)=E(IM,J)
5026 CONTINUE
GO TO 5021
5024 CONTINUE
E(IMP1,5)=E(3,5)
E(2,5)=E(IM,5)
CCC=DF*Y/X(4)
E(3,4)=E(3,4)+CCC
E(IM,4)=E(IM,4)+CCC
E(IMP1,4)=E(3,4)
E(2,4)=E(IM,4)
5021 CONTINUE
C*****NEWZEALAND
C*****ANTARCTICA
DO 32 J=4,JM
JM1=J-1
JP1=J+1
XJ=X(J)
CS=Y/XJ
SS=X(JP1)/Y
C1=X(JM1)/Y
CB=2.0*(CS+XJ/Y)
LJ=L(J)
DO 33 LL=1,LJ
II=KA(LL,J)

```



```

MM=RB(LL,J)
DO 330 I=II,MM
IP(MPP(I,J).GE.3) GO TO 330
R=E(I,J)
IF(ABS(R).LE.REL) GO TO 330
MAR=MAR+1
DF=R/CB*SOR
E(I,J)=-R*SOR1
F(I,J)=F(I,J)+DF
IP1=I+1
CCC=DF*CS
E(IP1,J)=E(IP1,J)+CCC
IM1=I-1
E(IM1,J)=E(IM1,J)+CCC
E(I,JP1)=E(I,JP1)+SS*DF
E(I,JM1)=E(I,JM1)+C1*DF
IF(I.NE.3) GO TO 331
E(IMP1,JP1)=E(3,JP1)
E(IMP1,JM1)=E(3,JM1)
E(IMP1,J)=E(3,J)
E(IM,J)=E(2,J)
GO TO 330
331 IF(I.NE.IM) GO TO 332
E(2,J)=E(IM,J)
E(2,JP1)=E(IM,JP1)
E(2,JM1)=E(IM,JM1)
E(3,J)=E(IMP1,J)
GO TO 330
332 IF(I.NE.4) GO TO 333
E(IMP1,J)=E(3,J)
GO TO 330
333 IF(I.NE.IMM1) GO TO 330
E(2,J)=E(IM,J)
330 CONTINUE
33 CONTINUE
32 CONTINUE
IF(MAR.EQ.0) GO TO 36
IF(IP.GT.1000) GO TO 1112
IF(IP.NE.1) GO TO 37
WRITE(6,38) IP,MAR
38 FORMAT(1H ,7X,6HKAISU=I5,5X,12HTEN NO. KAZU=I5)
GO TO 37
36 EN=0.0
WRITE(6,38) IP,MAR
DO 70 J=3,JM
F(1,J)=F(IMM1,J)
F(2,J)=F(IM,J)
F(IMP1,J)=F(3,J)
70 CONTINUE
DO 23 J=3,JM
JM1=J-1
JP1=J+1
XMJ=XM(J)*2.0
DF=XMJ*Y4
LVJ=LV(J)
DO 24 LJ=1,LVJ
II=LA(LJ,J)
IG=LB(LJ,J)
DO 244 I=II,IG
IP1=I+1
U(I,J)=XU(I,J)
V(I,J)=XV(I,J)
XU(I,J)=
1 (F(I,J)+F(IP1,J)-F(I,JP1)-F(IP1,JP1))/CCY
XV(I,J)=
1 (F(IP1,J)+F(IP1,JP1)-F(I,J)-F(I,JP1))/XMJ

```

```

EN= EN+DZ (AU (1,J) **2+XV (1,J) **2)
244 CONTINUE
24 CONTINUE
XU (IMP1,J)=XU (3,J)
XV (IMP1,J)=XV (3,J)
U (IMP1,J)=U (3,J)
V (IMP1,J)=V (3,J)
XU (2,J)=XU (IM,J)
XV (2,J)=XV (IM,J)
XU (1,J)=XU (IMM1,J)
XV (1,J)=XV (IMM1,J)
U (2,J)=U (IM,J)
V (2,J)=V (IM,J)
U (1,J)=U (IMM1,J)
V (1,J)=V (IMM1,J)
23 CONTINUE
WRITE (6,34) NN,CD,EN,F (1,3)
34 FORMAT (1H ,5HSTEP=I5,5X,5HTIME=E15.7,5X,7HENERGY=E15.7,5X,4HACC=F7
1.4)
IF (EN.GT.5.0E1) GO TO 1111
IF (NN.GE.NEND) GO TO 88
IF (MATS.NE.0) GO TO 10
IF (NN.NE. ((NN/NTAPE)*NTAPE)) GO TO 9
MAG=MAG+1
WRITE (10) XU,XV,F,G,U,V,IW,MPP,MOQ,L,KA,KB,LV,LA,LB,AH,DT,MAT,
1Y,REL,XM,FJU,X,BET,LX1,LX2,LY1,LY2,IND,INDIN,NN,NEND,RES,
2NRES,ARY,AR,Y4,E,CCY,MATS,CD,IM,JM,IMP1,JMP1,IMM1,MAG
WRITE (6,8) MAG
9 IF (NN.EQ. ((NN/NPRINT)*NPRINT)) GO TO 88
10 ENN=EN
IF (MATS.EQ.0) GO TO 39
MATS=MATS+1
IF (MATS.EQ.3) GO TO 46
DO 44 J=3,JM
DO 45 I=1,IMP1
F (I,J)=G (I,J)
U (I,J)=XU (I,J)
V (I,J)=XV (I,J)
45 CONTINUE
44 CONTINUE
GO TO 26
46 DO 47 J=3,JM
DO 48 I=1,IMP1
R=F (I,J)
F (I,J)=G (I,J)
G (I,J)=R
48 CONTINUE
47 CONTINUE
DO 49 J=3,JM
JP1=J+1
XMJ=XM (J) *2.0
LVJ=LV (J)
DO 55 LJ=1,LVJ
II=LA (LJ,J)
IG=LB (LJ,J)
DO 550 I=II,IG
IP1=I+1
U (I,J)=
1 (F (I,J)+F (IP1,J)-F (I,JP1)-F (IP1,JP1))/CCY
V (I,J)=
1 (F (IP1,J)+F (IP1,JP1)-F (I,J)-F (I,JP1))/XMJ
550 CONTINUE
55 CONTINUE
U (1,J)=U (IMM1,J)
V (1,J)=V (IMM1,J)
U (2,J)=U (IM,J)

```

```

V(2,J)=-V(LU,J)
U(IMP1,J)=U(3,J)
V(IMP1,J)=V(3,J)
49 CONTINUE
MATS=0
NN=NN+1
DDT=DT
NNT=NNT+1
CE=CD+DAY
GO TO 39
88 K=1
MP=-1
613 MP=MP+1
MM=K-MP
IG=18*MP+3
IF(MM.EQ.0) GO TO 614
II=IG+17
GO TO 615
614 II=38
615 WRITE(6,701)
701 FORMAT(1H0,15HSTREAM FUNCTION)
DO 702 J=1,IMP1
WRITE(6,703) J,(F(J,I),I=IG,II)
703 FORMAT(1H ,I3,1X,18F7.4)
702 CONTINUE
IF(MM.NE.0) GO TO 613
IF(NN.LT.NEND) GO TO 10
MAG=MAG+1
WRITE(10) XU,XV,F,G,U,V,TW,MPP,MOQ,L,KA,KB,LV,LA,LB,AH,DT,MAT,
1Y,REL,XM,FJU,X,BET,LX1,LX2,LY1,LY2,IND,INDIN,NN,NEND,RES,
2NRES,ARY,AR,Y4,E,CCY,MATS,CD,IM,JM,IMP1,JMP1,IMM1,MAG
WRITE(6,8) MAG
8 FORMAT(1H0,32HNO. OF RECORDS IN MAGNETIC TAPE=I3)
GO TO 1111
1112 WRITE(6,38) IP,MAR
1111 STOP
END
SUBROUTINE RESID
RETURN
END
SUBROUTINE HAJIME
RETURN
END
SUBROUTINE RESID
COMMON AH,DT,Y,H,REL,XM(39),FJU(39),X(39),F(147,39),E(147,39),
1U(147,39),V(147,39),G(147,39),XU(147,39),XV(147,39),TW(147,39),CD,
2BET(39),Y4,CCY,AR,ARY,RES(3),DDT,
3MAT,L(39),LV(39),LA(10,37),LB(10,37),KA(10,37),KB(10,37),MATS,
4MPP(147,39),MOQ(147,39),INDIN(3),IND(3),NRES(3),
5LX1(3),LX2(3),LY1(3),LY2(3),IM,JM,IMP1,JMP1,IMM1
DO 1 K=1,3
DO 8 J=1,JMP1
DO 9 I=1,IMP1
E(I,J)=0.0
9 CONTINUE
8 CONTINUE
S=0.0
I1=LX1(K)
I2=LX2(K)
J1=LY1(K)
J2=LY2(K)
MIN=IND(K)
MININ=INDIN(K)
NUM=0
IF(K.EQ.1) J1=2
DO 3 J=J1,J2

```

```

JM1=J-1
JP1=J+1
CS=Y/X(J)
C1=X(JM1)/Y
SS=X(JP1)/Y
CB=-2.0*(CS+1.0/CS)
DO 4 I=I1,I2
MP=MPP(I,J)
MMM=(MP-MIN)*(ME-MININ)
IF(MMM.NE.0) GO TO 4
IP1=I+1
IM1=I-1
NUM=NUM+1
E(I,J)=E(I,J)+CB
E(IP1,J)=E(IP1,J)+CS
E(IM1,J)=E(IM1,J)+CS
E(I,JP1)=E(I,JP1)+SS
E(I,JM1)=E(I,JM1)+C1
4 CONTINUE
3 CONTINUE
IF(K.GE.2) GO TO 10
J1=3
DO 11 J=3,3
CS=Y/X(J)
E(3,J)=E(3,J)+CS
E(IM,J)=E(IM,J)+CS
11 CONTINUE
10 CONTINUE
DO 5 J=J1,J2
DO 6 I=I1,I2
IF(MPP(I,J).EQ.MIN) S=S+E(I,J)
6 CONTINUE
5 CONTINUE
NRES(K)=NUM
RES(K)=S
WRITE(6,7) K,NUM,S
7 FORMAT(1H ,2HK=I2,2X,12HGRID POINTS=I3,2X,4HRES=E15.7)
1 CONTINUE
DO 16 J=1,18
DO 17 I=1,IMP1
IF(MQQ(I,J).EQ.1) GO TO 17
MP=MPP(I,J)
IF(MP.EQ.2) GO TO 17
IF(MP.EQ.((MP/3)*3)) GO TO 18
IF(MP.EQ.((MP/4)*4)) GO TO 19
MQQ(I,J)=5
GO TO 17
18 MQQ(I,J)=3
GO TO 17
19 MQQ(I,J)=4
17 CONTINUE
16 CONTINUE
WRITE(6,15) (I,I=1,38)
15 FORMAT(1H ,4X,38I3)
DO 12 I=1,IMP1
WRITE(6,14) I,(MPP(I,J),J=1,38)
WRITE(6,13) I,(MQQ(I,J),J=1,38)
12 CONTINUE
13 FORMAT(1H ,I3,3X,38I3)
14 FORMAT(1H ,I3,2X,38I3)
RETURN
END
SUBROUTINE HAJIME

```

DATA:

IM, JM, IMH, JMH

OCEAN SHAPE (SUBROUTINE SHAPE 1)  
X,DX,DY (DX AND DY ARE THE GRID SIZES IN LONGITUDE AND  
LATITUDE (DEGREES), RESPECTIVELY. Y IS THE LATITUDE  
CORRESPONDING TO J=0).

AH,H, REL,DT,MAT

IT: IT=1 WIND STRESS IS READ TO COMPUTE THE WIND STRESS CURL.  
IT=2 WIND STRESS CURL IS GIVEN FROM CARDS, A MAGNETIC  
TAPE, OR THE SUBROUTINE CURL.

COMMON AH,DT,Y,H,REL,XM(39),FJU(39),X(39),F(147,39),E(147,39),  
1U(147,39),V(147,39),G(147,39),XU(147,39),XV(147,39),TW(147,39),CD,  
2BET(39),Y4,CCY,AR,ARY,RES(3),DDT,  
3MAT,L(39),LV(39),LA(10,37),LB(10,37),KA(10,37),KB(10,37),MATS,  
4MPP(147,39),MQQ(147,39),INDIN(3),IND(3),NRES(3),  
5LX1(3),LX2(3),LY1(3),LY2(3),IM,JM,IMP1,JMP1,IMM1  
DIMENSION L1(9),WE(147,39),WN(147,39),C(39)  
EQUIVALENCE (U(1),WE(1)), (V(1),WN(1))  
READ(5,40) IM,JM,IMH,JMH

40 FORMAT(4I5)  
IMP1=IM+1  
IMM1=IM-1  
JMP1=JM+1

CALL SHAPE1  
CALL SHAPE 1  
DO 548 J=1,MM  
DO 549 I=1,IMP1  
F(I,J)=0.0  
G(I,J)=0.0  
U(I,J)=0.0  
V(I,J)=0.0  
XU(I,J)=0.0  
XV(I,J)=0.0

549 CONTINUE  
548 CONTINUE

READ(5,18) Y,DX,DY  
18 FORMAT(3F10.0)  
P=3.1415926/180.0  
DX=DX\*P  
MM=JM+2  
DO 100 I=1,MM  
AR=(Y+DY\*FLOAT(I))\*P  
F1=CCS(AR)  
X(I)=DX\*F1  
C(I)=F1  
BET(I)=F1\*X(I)\*14.58E-5

100 CONTINUE  
Y=DY\*P  
CD=14.58/(DX\*Y)  
DO 9997 J=1,JMP1  
XM(J)=(X(J)+X(J+1))/2.0  
FJU(J)=CD\*(X(J)-X(J+1))

9997 CONTINUE  
READ(5,16) AH,H,REL,DT,MAT

16 FORMAT(4E15.7,I5)  
WRITE(6,17) AH,H,REL  
17 FORMAT(1H,15HEDDY VISCOSITY=E15.7,10X,6HDEPTH=E15.7,10X,  
115HRELAX ACCURACY=E15.7)

READ(5,10) IT  
10 FORMAT(I5)  
GO TO (1,2), IT

1 CONTINUE  
CALL WIND  
CALL WIND  
P=0.01/4.0E5  
DO 540 J=JMH,JMP1  
XMJ=XM(J)

```

JM1=JM(JM1)
XM1=XM(JM1)
DO 541 I=IMH, IM
IM1=I-1
TW(I, J) = (XMJ* (-WE(I, J) - WE(IM1, J)) + XM1*(WE(I, JM1) + WE(IM1, JM1)))
1 + Y*(WN(I, J) + WN(I, JM1) - WN(IM1, J) - WN(IM1, JM1)) * P
541 CONTINUE
TW(1, J) = TW(IMM1, J)
TW(2, J) = TW(IM, J)
TW(IMP1, J) = TW(IMH, J)
540 CONTINUE
GO TO 3
2 CONTINUE
C CALL CURL
CALL CURL
READ(5, 6004) (TW(I, J), I=3, IM)
6004 FORMAT(5E15.7)
TW(IMP1, J) = TW(3, J)
TW(2, J) = TW(IM, J)
TW(1, J) = TW(IMM1, J)
3 CONTINUE
C INITIAL GUESS
DO 4000 J=4, JM
CJ=1.0/(C(J)*Y*14.58E-5)/4.0
LJ=L(J)
DO 360 LL=1, LJ
II=KA(LL, J)
IG=KB(LL, J)
MP=II+IG
362 DO 361 I=II, IG
MM=MP-I
K=MM+1
P=F(K, J) - (TW(MM, J) + TW(K, J)) * CJ
F(MM, J) = P
361 CONTINUE
IF(II.NE.3) GO TO 360
F(IMP1, J) = F(3, J)
360 CONTINUE
F(1, J) = F(IMM1, J)
F(2, J) = F(IM, J)
4000 CONTINUE
C INITIAL GUESS
CCC=2.0*Y
DO 4049 J=3, JM
JP1=J+1
LJ=LV(J)
DO 4058 LL=1, LJ
II=LA(LL, J)
IG=LB(LL, J)
DO 4053 I=II, IG
IP1=I+1
P=(F(I, J) + F(IP1, J) - F(I, JP1) - F(IP1, JP1))/CCC
U(I, J) = P
XU(I, J) = P
P=(F(IP1, J) + F(IP1, JP1) - F(I, J) - F(I, JP1))/XMJ
V(I, J) = P
XV(I, J) = P
53 CONTINUE
58 CONTINUE
XU(IMP1, J) = XU(3, J)
XV(IMP1, J) = XV(3, J)
XU(2, J) = XU(IM, J)
XV(2, J) = XV(IM, J)
XU(1, J) = XU(IMM1, J)
XV(1, J) = XV(IMM1, J)
U(IMP1, J) = U(3, J)

```

```

V (IMP1,J)=V (3,J)
U (2,J)=U (IM,J)
V (2,J)=V (IM,J)
U (1,J)=U (IMM1,J)
V (1,J)=V (IMM1,J)

```

```

#049 CONTINUE
AR=AH/6.37E8/6.37E8
ARY=AR/Y
CCY=2.0*Y
Y4=Y*0.25
RETURN
END
SUBROUTINE SHAPE1

```

SUBROUTINE TO BE USED FOR THE BAROTROPIC PART OF THE WORLD OCEAN CIRCULATION WHEN THE SHAPE OF THE OCEAN IS CHANGED.

DATA: LV, LA AND LB FOR MQQ.  
MM, M1(K), M2(K) AND M3(K) FOR MPP.  
LV, LA AND LB ARE THE SAME AS THOSE USED FOR THE SUBROUTINE SHAPE 2 (BAROCLINIC PART), BUT THE DATA FOR MPP ARE DIFFERENT FROM THOSE USED FOR THE SHAPE2.  
LX1, LX2, LY1, LY2 WHICH SPECIFY THE AREAS INCLUDING THE SEPARATE ISLANDS.

```

COMMON AH,DT,Y,H,REL,XM(39),FJU(39),X(39),F(147,39),E(147,39),
1U(147,39),V(147,39),G(147,39),XU(147,39),XV(147,39),TW(147,39),CD,
2BET(39),Y4,CCY,AR,ARY,RES(3),DDT,
3MAT,L(39),LV(39),LA(10,37),LB(10,37),KA(10,37),KB(10,37),MATS,
4MPP(147,39),MQQ(147,39),INDIN(3),IND(3),NRES(3),
5LX1(3),LX2(3),LY1(3),LY2(3),IM,JM,IMP1,JMP1,IMM1

```

```

IMM1=IM-1
IMP1=IM+1
JMM1=JM-1
JMP1=JM+1
JMH=3
IMH=3
DO 30 J=1,JM
DO 31 I=1,IMP1
MQQ(I,J)=2

```

```
31 CONTINUE
```

```
30 CONTINUE
DO 32 J=3,JMM1
READ(5,33) M

```

```
33 FORMAT(I2)
READ(5,34) (LA(I,J),LB(I,J),I=1,M)

```

```
34 FORMAT(7(2I4,2X))
DO 35 I=1,M
II=LA(I,J)
IG=LB(I,J)
DO 36 N=II,IG
MQQ(N,J)=1

```

```
36 CONTINUE
```

```
35 CONTINUE
LV(J)=M
MQQ(1,J)=MQQ(IMM1,J)
MQQ(2,J)=MQQ(IM,J)
MQQ(IMP1,J)=MQQ(3,J)

```

```
32 CONTINUE
DO 3006 J=3,38
READ(5,3007) MM

```

```
3007 FORMAT(I2)
READ(5,3008) (M1(K),M2(K),M3(K),K=1,MM)

```

```
3008 FORMAT(8(2I4,I2))
DO 3009 K=1,MM
K5=M1(K)
K6=M2(K)
K7=M3(K)
DO 3010 I=K5,K6

```

```

MPP1(I,J)=K7
3010 CONTINUE
3009 CONTINUE
3006 CONTINUE
DO 3011 J=3,38
READ(5,3007) MM
L1(J)=MM
READ(5,3012) (KA1(LL,J),KB1(LL,J),LL=1,MM)
3012 FORMAT(16I5)
3011 CONTINUE
DO 6003 J=1,JMP1
MPP1(1,J)=MPP1(IMM1,J)
MPP1(2,J)=MPP1(IM,J)
MPP1(IMP1,J)=MPP1(3,J)
6003 CONTINUE
DO 6004 J=3,JM
JP1=J+1
JM1=J-1
DO 6005 I=3,IM
IF(MPP1(I,J).GT.1) GO TO 6005
IF(MPP1(I-1,J).EQ.2) GO TO 6005
IF(MPP1(I,JP1).EQ.2) GO TO 6005
IF(MPP1(I,JM1).EQ.2) GO TO 6005
IF(MPP1(I+1,J).EQ.2) GO TO 6005
MPP1(I,J)=0
6005 CONTINUE
MPP1(IMP1,J)=MPP1(3,J)
MPP1(2,J)=MPP1(IM,J)
MPP1(1,J)=MPP1(IMM1,J)
6004 CONTINUE
WRITE(6,6016) (J,J=3,38)
6016 FORMAT(1H,5X,38I3/)
DO 6012 I=1,IMP1
WRITE(6,6014) I,(MPP1(I,J),J=3,38)
WRITE(6,6015) (MQQ(I,J),J=3,38)
6012 CONTINUE
6014 FORMAT(1H,I3,2X,38I3)
6015 FORMAT(1H,6X,38I3)
READ(5,2) (LX1(K),LX2(K),LY1(K),LY2(K),K=1,3)
2 FORMAT(4I5)
RETURN
END
SUBROUTINE WIND
COMMON AH,DT,Y,H,REL,XM(39),FJU(39),X(39),F(147,39),E(147,39),
1U(147,39),V(147,39),G(147,39),XU(147,39),XV(147,39),TW(147,39),CD,
2BET(39),Y4,CCY,AR,ARY,RES(3),DDT,
3MAT,L(39),LV(39),LA(10,37),LB(10,37),KA(10,37),KB(10,37),MATS,
4MPP(147,39),MQQ(147,39),INDIN(3),IND(3),NRES(3),
5LX1(3),LX2(3),LY1(3),LY2(3),IM,JM,IMP1,JMP1,IMM1
DIMENSION WE(147,7),WN(147,7)
RETURN
END
SUBROUTINE CURL
RETURN
END

```



MPP

MPP=1 IF THE FOUR NEAREST SURROUNDING POINTS ARE WATER-POINT,  
=2 ON THE LAND (EXCLUDING THE COAST LINE).  
FOR THE COAST-POINTS, REFER TO FIG.1.

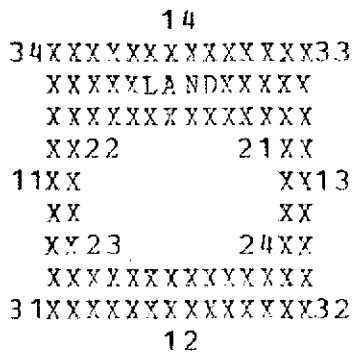


FIG. 1

MQQ

MQQ=1 IF THE FOUR NEAREST SURROUNDING POINTS ARE WATER-POINT,  
=2 ON THE LAND.  
IN OTHER CASES, REFER TO FIG.2.

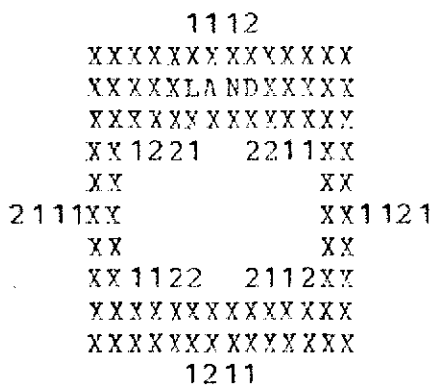


FIG. 2

COMMON T(147,39,5), TT(147,39,5), SP(147,39), AT(5), HH(147,39,5),  
 1VV(147,39,5), U(147,39,5), V(147,39,5), W(147,39,5), UB(147,39),  
 2VB(147,39), WE(147,39), WN(147,39), Q(39), YJA(38), XHT(38), XHS(38),  
 3 XMY(38), Z(5), X(39), XM(39), FH(39), FJU(39), ZZ(6), H, AZ, AH, DT, AL,  
 4GAM, Y, YY, R, RR, HH, H2, AZHH, R2, AHY, AHRP, AH2, BB, BE2, AAA, BBB, DDT, A1, UV,  
 5UUU, VVV, RRH, AQ, GAM2, AL2, BUN, EY, AN, AMRR, GAMGAM, AJAL, BAN, KMP1,  
 6HPP(147,39), MQQ(147,39), IM, JM, KM, IMM1, JMM1, FMM1, IMP1, JMP1, MAT,  
 7 NK, NNNN, IMH, JMH, MATS, L(39), KA(10,39), KB(10,39), LV(39), NEND,  
 8LA(10,39), LB(10,39), NN, TE(147,46), UN(147,39), TD(147,46), RN(147,39)  
 \*, CL(147,39)

DIMENSION UHEAD(39), THEAD(39)  
 DIMENSION QE(147,39), QH(147,39), QSH(147,39)  
 COMMON /TEMP/ QF, QH, QSH, ZQE, ZQH, ZSH, ZRN  
 DIMENSION ZQE(39), ZQH(39)  
 LOGICAL STOP  
 REAL KK  
 DIMENSION ZRN(39), ZSH(39)  
 DIMENSION ZT(39,5), ZW(39,5), UZ(39,5), VZ(39,5)  
 EQUIVALENCE(ZT(1), UZ(1)), (ZW(1), VZ(1)), (ZT(1), W(1)), (ZW(1), W(196))  
 DIMENSION ICTL(7), RCTL(2), FIELD(18)  
 DATA ICTL/1,6,9,1,18,7,2/  
 DATA RCTL /0.001,60./

FORMAT(1), 30X, (EXPERIMENT ST CALCULATED RADIATION)  
UHEAD(1) = -72.  
THEAD(1) = -74.  
DO 88 I=2,39  
UHEAD(I) = UHEAD(1) + 4.\*(I-1)  
THEAD(I) = THEAD(1) + 4.\*(I-1)  
CONTINUE

58

NNNN=0  
READ(5,9) KT  
READ(5,9) IN  
9 FORMAT(I5)  
IF(IN.EQ.0) GO TO 11  
17 RRAD(KT,FND=92)  
\* TT, UU, VV, T, U, V, AT, SP, W, UB, VB, X, XM, O, PU, FJU, DT, AZ, AH, WE,  
1WN, BAN, AL, GAM, Y, YY, R, RR, HH, H2, AZHH, BUN, R2, AHY, AHPE, AH2, PB, PB2,  
2AAA, BBB, DDT, A1, UV, UUU, VVV, RRH, A0, GAN2, AL2, RV, ANRP, GANGAM, ALAL,  
3H, Z, ZZ, AM, XJA, XHT, XHS, XMY, CD,  
4MPP, MQQ, KA, KB, L, LA, LB, LV, MATS, NEND, NK, NNNN, MAT, IM, JM, KM, IMH, IMY1,  
5IMP1, KMP1, KMM1, JMM1, JMP1, NN, JMH, MAG, TE, TD, RN  
6, QF, QH, QSH, CL, UN  
GO TO 17  
92 BACK SPACE KT  
IF(MAG.LI.34) GO TO 94  
REWIND KT  
KT = KT + 1  
MAG=0  
94 CONTINUE  
73 READ(10,END=74) UR, VB  
GO TO 73  
74 REWIND 10  
DO 2222 I=1,145  
WRITE(6,7000) I, (UN(I,J), J=3,20)  
2222 CONTINUE  
DO 4444 I=1,145  
WRITE(6,7000) I, (UN(I,J), J=21,38)  
4444 CONTINUE  
WRITE(6,890) (THEAD(J), J=3,20)  
DO 7040 I=1,147  
WRITE(6,7000) I, (TE(I,J), J=3,20)  
7040 CONTINUE  
WRITE(6,890) (THEAD(J), J=21,38)  
DO 7034 I=1,147  
WRITE(6,7000) I, (TE(I,J), J=21,38)  
7034 CONTINUE  
CL(1,3)=6.00  
CL(2,3)=6.00  
CL(145,3)=6.00  
CL(146,3) = 6.  
CL(147,3) = 6.  
DO 3333 I=1,145  
WRITE(6,7000) I, (CL(I,J), J=3,20)  
3333 CONTINUE  
DO 5555 I=1,145  
WRITE(6,7000) I, (CL(I,J), J=21,38)  
5555 CONTINUE  
FA=400000.  
DO 311 I=1,147  
WE(I,3)=1.16\*FA  
WE(I,4)=1.72\*FA  
WE(I,5)=1.83\*FA  
WE(I,6)=1.90\*FA  
WE(I,7)=1.83\*FA  
WE(I,8)=1.50\*FA  
WE(I,9)=1.10\*FA  
WE(I,10)=0.72\*FA

89

WE(I,11)=-0.50\*FA  
WE(I,12)=-0.07\*FA  
WE(I,13)=-0.30\*FA  
WE(I,14)=-0.52\*FA  
WE(I,15)=-0.60\*FA  
WE(I,16)=-0.60\*FA  
WE(I,17)=-0.52\*FA  
WE(I,18)=-0.38\*FA  
WE(I,19)=-0.30\*FA  
WE(I,20)=-0.24\*FA  
WE(I,21)=-0.26\*FA  
WE(I,22)=-0.38\*FA  
WE(I,23)=-0.50\*FA  
WE(I,24)=-0.53\*FA  
WE(I,25)=-0.40\*FA  
WE(I,26)=-0.14\*FA  
WE(I,27)=0.10\*FA  
WE(I,28)=0.42\*FA  
WE(I,29)=0.61\*FA  
WE(I,30)=0.74\*FA  
WE(I,31)=0.78\*FA  
WE(I,32)=0.63\*FA  
WE(I,33)=0.48\*FA  
WE(I,34)=0.14\*FA  
WE(I,35)=+0.01\*FA  
WE(I,36)=-0.04\*FA  
WE(I,37)=-0.13\*FA

311 CONTINUE

AH=2.5E7

AHY=AH\*Y

AHRR=AH/RR

AH2=AH/(YY\*RR)

AL=0.25E-3

ALAL=AL\*2.0

AL2=AL/2.0

AZ=1.0

AZHH=AZ/HH

GAMGAM=25.0\*H/(AZ\*0.864E5)

WRITE(6,7777)

WRITE(6,9005)

9005 FORMAT(1H0,21HBAROTROPIC COMPONENTS/)

WRITE(6,9110)

9110 FORMAT(1X,'UB')

WRITE(6,9004) (J,J=3,21)

9004 FORMAT(1H0,4X,19(2X,J2,2X)/)

DO 9000 I=1,147

WRITE(6,9001) I,(UB(I,J),J=3,21),I

9000 CONTINUE

WRITE(6,7777)

WRITE(6,9004) (J,J=20,38)

DO 9002 I=1,147

WRITE(6,9001) I,(UB(I,J),J=20,38),I

9002 CONTINUE

WRITE(6,7777)

WRITE(6,9200)

9200 FORMAT(1X,'VB')

WRITE(6,9004) (J,J=3,21)

DO 9006 I=1,147

WRITE(6,9001) I,(VB(I,J),J=3,21),I

9006 CONTINUE

WRITE(6,7777)

WRITE(6,9004) (J,J=20,38)

DO 9007 I=1,147

WRITE(6,9001) I,(VB(I,J),J=20,38),I

9007 CONTINUE

9001 FORMAT(1H ,I3,1X,19F6.2,1X,I3)

```

WRITE(6,9100) (Q(J),J=3,38)
9100 FORMAT(1H0,18F6.2/1H,18F6.2/)
IF(NK.NE.3) GO TO 492
GO TO 5
11 CONTINUE
NN=0
CD=0.0
NK=3
MAG=0
CALL FRFP
CALL FRFPA
CALL GEOST
5 READ(5,3) MATS, NEND, NPRINT, NTAPE, DT
3 FORMAT(4I5,E15.7)
WRITE(6,6) NPRINT,NTAPE
6 FORMAT(' NPRINT = ',I5,' NTAPE = ',I5)
WRITE(6,8) KT, MAG, CD
8 FORMAT(' KT = ',I2,' MAG = ',I2,' CD = ',F7.1)
DTD=DT/0.864E5
K=NN+1
NEND=NEND+K
WRITE(6,4) K, NEND, MATS, DT,AZ,AM,AH
4 FORMAT(' ',TIME STEP FROM ',I5,3X,' TO ',I5,5X,'MATS=',I3,5X,
X 'DT=',4E15.7/)
IF(DT.LT.10.) STOP 100
DDT=DT*2.0
DO 111 J=JMH,JMM1
XJ=FJU(J)*DDT
XJA(J)=XJ*AAA
XHT(J)=1.0/(1.0+XJA(J)**2)
XHS(J)=XJ*BBB
XMY(J)=Y*XM(J)
111 CONTINUE
IF(NN.GT.0) GO TO 251
CALL CONTI
MAT=2
WRITE(2) TT
REWIND 2
WRITE(3) U,V
REWIND 3
DDT=DT
GO TO 253
-251 NN=NN+1
CD=CD+DTD
NNN=(NN/MATS)*MATS
IF(NNN.NE.NN) GO TO 250
MAT=1
WRITE(6,2)
2 FORMAT(1H,5HBEGIN)
250 CONTINUE
253 CALL THERME
CALL EQA
CALL CONTI
WRITE(6,7013) UUU,VVV,UV,NN,CD
7013 FORMAT(1H,7HEENERGY=3(E15.7,3X),5HSTEP=I5,2X,4HDAY=F10.2)
IF(MAT.NE.0) GO TO 7019
CALL WTO(STOP)
IF(STOP) NEND=10
IF(NN.GE.NEND) GO TO 7015
IF(((NN/NTAPE)*NTAPE).NE.NN) GO TO 7025
IF(NN.EQ.0) GO TO 7019
7015 MAG = MAG+1
WTM = 0.0
GQSH = 0.0
GQE=0.0
GQH = 0.0

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```

GRN = 0.
DO 2001 J=3,38
DXYP = X(J) * Y
CLAT = ABS(DXYP)
KF=0.
ZQH(J) = 0.
ZQF(J) = 0.0
ZZZ=0.
ZRN(J) = 0.
DO 2002 I=3,146
IF (MPP(I,J).GT.1.AND.MPP(I,J).LE.5) GO TO 9011
UM=UN(I,J)*51.48
TEIJ=TE(I,J)
TIJ= T(I,J,1)
TW=TD(I,J)+273.15
123 TS=T(I,J,1)+273.15
PCB=1013.25*0.1
ESS=10.0**(8.4051-2353.0/TS)
ESD=10.0**(8.4051-2353.0/TW)
QS=0.622*ESS/(PCB-ESS)
QA=0.622*ESD/(PCB-ESD)
IF ((TIJ-TEIJ)+0.609* TS*(QS-QA)).LT.0.0) GO TO 334
332 CU=0.033
CO=1.23*0.001
GO TO 133
334 CU=0.018
CO=0.41*0.001
133 QH(I,J)=-1.2*0.001*.24*CO*UM*(TIJ-TEIJ)*0.864E5
QE(I,J)=-1.2*0.001*CO*595.*UM*(QS-QA)*0.864E5
RN(I,J)=RN(I,J)*0.864E5
QSH(I,J)=RN(I,J)+QH(I,J)+QE(I,J)
GQSH = GQSH+QSH(I,J)*CLAT
GQE = GQE + QE(I,J)*CLAT
GQH = GQH + QH(I,J)*CLAT
GRN = GRN + RN(I,J) * CLAT
WTM = WTM+CLAT
KK=KK+1.
ZZZ = QSH(I,J) + ZZZ
ZQH(J) = QH(I,J) + ZQH(J)
ZQF(J) = QE(I,J) + ZQF(J)
ZRN(J) = RN(I,J) + ZRN(J)
GO TO 2002
9011 QSH(I,J) = 0.
QE(I,J)=0.
QH(I,J)=0.
2002 CONTINUE
KK = 1./KK
ZSH(J) = ZZZ*KK
ZQF(J) = ZQF(J) *KK
ZQH(J) = ZQH(J)*KK
ZRN(J) = ZRN(J) * KK
2001 CONTINUE
WTM = 1./WTM
GQSH = GQSH*WTM
GQE = GQE*WTM
GQH = GQH*WTM
GRN = GRN*WTM
WRITE(KT)
* TT, UU, VV, T, U, V, AT, SP, W, UB, VR, X, XM, Q, PU, FJU, DT, AZ, AH, WE,
1WN, BAN, AL, GAM, Y, YY, R, RP, HH, H2, AZHH, BUN, R2, AHY, AHPE, AH2, EB, B52,
2AAA, BBB, DDT, A1, UV, UUU, VVV, RRH, AC, GAM2, AL2, RY, AMRR, GAMGAM, ALAI,
3H, Z, ZZ, AM, XJA, XHT, XHS, XMY, CD,
4MPP, HQQ, KA, KB, L, LA, LB, LV, MATS, NEND, NK, NNNN, MAT, IM, JM, KM, IMH, IMM1,
5IMP1, KMP1, KMM1, JMM1, JMP1, NN, JMH, MAG, TE, TD, RN
*, QF, QH, QSH, CL, UN
ENDDFILE KT

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BACKSPACE RE
WRITE(6,1) MAG
1 FORMAT(1H ,35HNUMBER OF RECOPIES IN MAGNETIC TAPE=I2)
IF(NN.GE.NEND) GO TO 7014
IF(MAG.GE.34) GO TO 93
7025 IF(UV.GT.1.0E26) GO TO 7014
IF(((NN/NPRINT)*NPRINT).NE.NN) GO TO 7019
14 WRITE(6,7020) NN,CD
7020 FORMAT(1H ,11HTIME(STEP)=I8,5X,10HTIME(DAY)=E15.7)
DO 300 K=1,5
KK=0.
DO 301 J=3,38
UZSUM=0.
VZSUM=0.
DO 303 I=3,146
IF(MQQ(I,J).LE.5.AND.MQQ(I,J).NE.1) GO TO 303
KK=KK+1.
UZSUM=UZSUM+U(I,J,K)
VZSUM=VZSUM+V(I,J,K)
303 CONTINUE
IF(KK.LT.1.)GO TO 300
UZ(J,K)=UZSUM/KK
VZ(J,K)=VZSUM/KK
301 CONTINUE
300 CONTINUE
DO 7009 K=1,KM
WRITE(6,7777)
WRITE(6,7010) K, CD
7010 FORMAT(1X,'UU AT K = ',I1,' DAY ',F7.1)
WRITE(6,890) (UHEAD(J),J=3,20)
DO 7011 I=IMH,IM
WRITE(6,7012) I,(UU(I,J,K),J=3,20)
7012 FORMAT(1H ,I3,1X,18F7.2)
7011 CONTINUE
WRITE(6,7778) (UZ(J,K),J=3,20)
WRITE(6,7777)
WRITE(6,7010) K,CD
WRITE(6,890) (UHEAD(J),J=21,38)
DO 7022 I=IMH,IM
WRITE(6,7012) I,(UU(I,J,K),J=21,38)
7022 CONTINUE
WRITE(6,7778) (UZ(J,K),J=21,38)
7009 CONTINUE
DO 7070 K=1,KM
WRITE(6,7777)
WRITE(6,7053) K,CD
WRITE(6,890) (UHEAD(J),J=3,20)
7053 FORMAT(1X,'VV AT K = ',I1,' DAY ',F7.1)
DO 7021 I=IMH,IM
WRITE(6,7012) I,(VV(I,J,K),J=3,20)
7021 CONTINUE
WRITE(6,7778) (VZ(J,K),J=3,20)
890 FORMAT(/5X,18F7.2/)
WRITE(6,7777)
WRITE(6,7053) K,CD
WRITE(6,890) (UHEAD(J),J=21,38)
DO 7023 I=IMH,IM
WRITE(6,7012) I,(VV(I,J,K),J=21,38)
7023 CONTINUE
WRITE(6,7778) (VZ(J,K),J=21,38)
7070 CONTINUE
DO 200 K=1,KM
DO 201 J=3,38
KK=0.
WZSUM=0.
TZSUM=0.

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DO 203 I=3,146
IF (MPP(I,J).GT.1.AND. MPP(J,J).LE.5) GO TO 203
KK=KK+1.
WZSUM=WZSUM+W(I,J,K)
TZSUM=TZSUM+TT(I,J,K)
203 CONTINUE
IF (KK.I.T.1.) GO TO 200
ZW(J,K)=WZSUM/KK
ZI(J,K)=TZSUM/KK
201 CONTINUE
200 CONTINUE
DO 7005 K=1,KM
WRITE(6,7777)
WRITE(6,7006) K
7006 FORMAT(1H,17HTEMPERATURE AT K=I1)
WRITE(6,890) (THEAD(J),J=3,20)
DO 7050 I=IMH,IM
WRITE(6,7000) I,(TT(I,J,K),J=3,20)
7050 CONTINUE
WRITE(6,7778) (ZI(J,K),J=3,20)
WRITE(6,7777)
WRITE(6,7006) K
WRITE(6,890) (THEAD(J),J=21,38)
DO 7051 I=IMH,IM
WRITE(6,7000) I,(TT(I,J,K),J=21,38)
7051 CONTINUE
WRITE(6,7778) (ZI(J,K),J=21,38)
7005 CONTINUE
DO 7002 K=2,KM
FK = K-.5
WRITE(6,7777)
WRITE(6,7001) FK,CD
7001 FORMAT(1X,'VERTICAL VELOCITY AT K = ',F4.1,' DAY ',F7.1)
WRITE(6,890) (THEAD(J),J=3,20)
DO 7003 I=IMH,IM
WRITE(6,7000) I,(W(I,J,K),J=3,20)
7000 FORMAT(1H,I3,1X,18F7.2)
7003 CONTINUE
WRITE(6,7778) (ZW(J,K),J=3,20)
WRITE(6,7777)
WRITE(6,7001) FK,CD
WRITE(6,890) (THEAD(J),J=21,38)
DO 7024 I=IMH,IM
WRITE(6,7000) I,(W(I,J,K),J=21,38)
7024 CONTINUE
WRITE(6,7778) (ZW(J,K),J=21,38)
7778 FORMAT(/30X,'ZONAL MEANS'//5X,18F7.2)
7002 CONTINUE
IF (UV.GT.1.0E26) STOP 792
WRITE(6,7777)
WRITE(6,9016) CD
9016 FORMAT(1X,'SURFACE HEAT FLUX(CAL PER DAY) DAY = ',F7.1/)
WRITE(6,9020) GQSH
9020 FORMAT(' GLOBAL MEAN = ',F10.3)
CALL PRINT(QSH,ZSH,THEAD,ICTL,RCTL)
WRITE(6,7777)
WRITE(6,9017)
9017 FORMAT(' LATENT HEAT FLUX')
WRITE(6,9020) GQE
CALL PRINT(QE,ZQE,THEAD,ICTL,RCTL)
WRITE(6,7777)
WRITE(6,9018)
9018 FORMAT(' SENSIBLE HEAT FLUX')
WRITE(6,9020) GQH
CALL PRINT(QH,ZQH,THEAD,ICTL,RCTL)
WRITE(6,7777)

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WRITE(6,9023)
9023  FORMAT(' SURFACE RADIATION FLUX (CAL/CM**2/DAY) ')
WRITE(6,9020) GRN
CALL PRINT(PN,ZRN,THEAD,ICTL,RCTL)
IF(NN.GE.NPND) GO TO 2501
7019  CONTINUE
IF(MAT.EQ.0) GO TO 251
MAT=MAT+1
IF(MAT.LT.8) GO TO 7017
DDT=DT*2.0
GO TO 251
7017  DDT=DT
IF(MAT.EQ.3) GO TO 20
IF(MAT.EQ.4) NK=3
IF(MAT.EQ.5) GO TO 21
IF(MAT.EQ.6) NK=3
GO TO 250
20  NK=1
MAT=7
NK=3
GO TO 22
21  NK=2
22  NN=NN+1
CD=CD+DDT
GO TO 250
2501  CONTINUE
DO 3005 J=3,37
LJ =LV(J)
DO 3005 M1=1,LJ
II = LA(M1,J)
99  FORMAT('0',4X,19F6.1/)
IG = LB(M1,J)
DO 3005 I=II,IG
UU(I,J,1) = UU(I,J,1)*Z(1)+UU(I,J,2)*Z(2)+UU(I,J,3)*Z(3)
X + UU(I,J,4)*Z(4) + UU(I,J,5)*Z(5)
VV(I,J,1) = VV(I,J,1)*Z(1)+VV(I,J,2)*Z(2)+VV(I,J,3)*Z(3)
X + VV(I,J,4)*Z(4) + VV(I,J,5)*Z(5)
3005  CONTINUE
3004  FORMAT(' ',I3,1X,19F6.3,1X,I3)
WRITE(6,7777)
WRITE(6,3001)
3001  FORMAT(' UHBAR '/')
WRITE(6,89) (UHEAD(J),J=3,21)
DO 3006 I=3,146
3006  WRITE(6,3004) I,(UU(I,J,1),J=3,21),I
WRITE(6,89) (UHEAD(J),J=20,38)
DO 3007 I=3,146
3007  WRITE(6,3004) I,(UU(I,J,1),J=20,38),I
WRITE(6,7777)
WRITE(6,3002)
3002  FORMAT(' VVBAR '/')
WRITE(6,89) (VHEAD(J),J=3,21)
DO 3008 I=3,146
3008  WRITE(6,3004) I,(VV(I,J,1),J=3,21),I
WRITE(6,89) (VHEAD(J),J=20,38)
DO 3009 I=3,146
3009  WRITE(6,3004) I,(VV(I,J,1),J=20,38),I
92  STOP
93  REWIND KT
KT=KT+1
MAG = 0
GO TO 7015
END
SUBROUTINE PRINT(PI,ZSP,THEAD,ICTL,RCTL)
DIMENSION THEAD(39)
DIMENSION FIELD(18),ZSP(39),PI(147,39),ICTL(7),RCTI(2)

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7011 FORMAT('I',30X,'EXPERIMENT 50')
7012 FORMAT(' ',I3,1X,18F7.2)
890  FORMAT(/5X,18F7.2/)
7778  FORMAT(/30X,'ZONAL MEANS'//5X,18F7.2)
      WRITE(6,890) (THEAD(J),J=3,20)
      CALL SHADE (ICTL,RCTL,0.)
      DO 9013 I=3,146
      DO 701 J=3,20
      J1 = J-2
701  FIELD(J1) = FI(I,J)
      CALL SHADE(0,0.,FIELD(1))
      WRITE(6,7012) I,FIELD
9013  CONTINUE
      WRITE(6,7778) (ZSP(J),J=3,20)
      WRITE(6,7777)
      WRITE(6,890) (THEAD(J),J=21,38)
      CALL SHADE (ICTL,RCTL,0.)
      DO 9015 I=3,146
      DO 702  J=21,38
      J1 = J-20
702  FIELD(J1) = FI(I,J)
      CALL SHADE(0,0.,FIELD(1))
      WRITE(6,7012) I,FIELD
9015  CONTINUE
      WRITE(6,7778) (ZSP(J),J=21,38)
      RETURN
      END
      SUBROUTINE ADJUST
      COMMON T(147,39,5),TT(147,39,5),SP(147,39),AT(5),UU(147,39,5),
1VV(147,39,5),U(147,39,5),V(147,39,5),W(147,39,5),UB(147,39),
2VB(147,39),WB(147,39),WN(147,39),Q(39),XJA(38),XBT(38),XHS(38),
3 XMY(38),Z(5),X(39),XM(39),FU(39),FJU(39),ZZ(6),H,AZ,AH,DT,AL,
4GAM,Y,YY,R,RR,HH,H2,AZHH,R2,AHY,AHPR,AH2,BB,BB2,AAA,BBB,DDT,A1,UV,
5UUU,VVV,RRH,AQ,GAM2,AL2,BON,RY,AM,AMR,GAMGAM,AJAL,BAN,KMP1,
6MPP(147,39),MQQ(147,39),TM,JM,KM,IMM1,JMM1,KMM1,IMP1,JMP1,MAT,
7 NK,NNNN,IMH,JMH,MATS,L(39),KA(10,39),KB(10,39),LV(39),NEND,
8LA(10,39),LB(10,39),NN,TE(147,46),UN(147,39),TD(147,46),RN(147,39)
*,CL(147,39)
      MR=0
41  KP1=1
      MAR=0
40  IF(KP1.EQ.KM) GO TO 50
      K=KP1
      KP1=K+1
      B=(AT(K)-AT(KP1))/(ABS(AT(K)))
      IF(R.GE.-5.0E-6) GO TO 40
      DZ1=Z(K)
      DZ2 = Z(KP1)
      AVT=(AT(KP1)*DZ2+AT(K)*DZ1)/(DZ2+DZ1)
      AT(KP1)=AVT
      AT(K)=AVT
      MAR=1
      GO TO 40
50  IF(MAR.EQ.0) GO TO 51
      MR=MR+1
      IF(MR.LT.1000) GO TO 41
      WRITE(6,1) (AT(J),I=1,KM)
1  FORMAT(1H ,23H TOO MANY OPER IN ADJUST,5E15.7)
51  RETURN
      END
      SUBROUTINE EQA
      COMMON T(147,39,5),TT(147,39,5),SP(147,39),AT(5),UU(147,39,5),
1VV(147,39,5),U(147,39,5),V(147,39,5),W(147,39,5),UB(147,39),
2VB(147,39),WB(147,39),WN(147,39),Q(39),XJA(38),XBT(38),XPS(38),
3 XMY(38),Z(5),X(39),XM(39),FU(39),FJU(39),ZZ(6),H,AZ,AH,DT,AL,
4GAM,Y,YY,R,RR,HH,H2,AZHH,R2,AHY,AHPR,AH2,BB,BB2,AAA,BBB,DDT,A1,UV,

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5 DUU, VVV, RRR, AQ, GANZ, ALZ, DUN, R1, AN, AMR, GANAD, ALAL, BAW, RRR1,  
 6MPP (147, 39), MOO (147, 39), JM, JM, KM, IMM1, JMM1, KMM1, IMP1, JMP1, NAT,  
 7 NK, NNNN, IMH, JMH, MATS, L (39), KA (10, 39), KB (10, 39), LV (39), HEND,  
 8LA (10, 39), LB (10, 39), NN, TE (147, 46), ON (147, 39), TD (147, 46), PN (147, 39)  
 \*, CL (147, 39)

DIMENSION SEN (147, 39, 5)  
 EQUIVALENCE (W(1), SEN(1))  
 COMMON/TEMP/TFN(146, 38, 5)  
 DO 3000 J=JMH, JMM1  
 JP1=J+1  
 JM1=J-1  
 XMJ=XM(J)  
 XMJ1=XM(JM1)  
 XJ=X(J)  
 XJP1=X(JP1)  
 XJ1=X(JM1)  
 AD=A1\*XJ/XMJ\*0.3  
 AC=A1\*XJP1/XMJ\*0.3  
 AB=AMRR/(XMJ\*XMJ)\*0.3  
 RXMJ=R\*XMJ  
 LJ=LV(J)  
 DO 4002 M1=1, LJ  
 II=LA(M1, J)  
 IG=LB(M1, J)  
 DO 3001 I=II, IG  
 MQ=MQQ(I, J)  
 IP1=I+1  
 IM1=I-1

C\*\*\*\*\*COMPUTAITON OF PRESSURE

GO TO (1, 2, 3), NK  
 3 CONTINUE  
 SPO=SP(I, J) - SP(IP1, JP1)  
 SP1=SP(IP1, J) - SP(I, JP1)  
 PYBIJ=SP1-SPO  
 PYBIJ=-SP1-SPO  
 GO TO 4  
 1 PXBIJ=(SP(IP1, JP1) - SP(T, JP1)) \* 2.0  
 PYBIJ=(SP(IP1, JP1) - SP(TP1, J)) \* 2.0  
 GO TO 4  
 2 PXBIJ=(SP(IP1, J) - SP(I, J)) \* 2.0  
 PYBIJ=(SP(I, JP1) - SP(I, J)) \* 2.0  
 4 CONTINUE

C\*\*\*\*\*COMPUTATION OF PRESSURE

WEIJ=WR(I, J)  
 WNIJ=WN(I, J)  
 DO 3002 K=1, KM  
 KP1=K+1  
 ZK=Z(K)  
 ZZ1=ZZ(KP1)  
 KM1=K-1  
 ZZK=ZZ(K)  
 5555 HS=V(I, J, K)  
 HT=U(I, J, K)  
 UM1J=U(IM1, J, K)  
 VM1J=V(IM1, J, K)  
 UP1J=U(IP1, J, K)  
 VP1J=V(IP1, J, K)  
 UIP1=U(I, JP1, K)  
 VIP1=V(I, JP1, K)  
 UIM1=U(I, JM1, K)  
 VIM1=V(I, JM1, K)  
 5556 UIJ=HT  
 VIJ=HS  
 AX=AZHH/ZK  
 IF(K.EQ.1) GO TO 3003  
 DUZ=(U(T, J, KM1) - HT) / ZK

```

DVZ=(V(I,J,KP1)-HS)/ZK
IF(K.NE.KM) GO TO 3004
DUZP1=0.0
DVZP1=0.0
GO TO 3009
3003 DUZ=WELJ
DVZ=WNIJ
3004 DUZP1=(HT-U(T,J,KP1))/ZK1
DVZP1=(HS-V(T,J,KP1))/ZK1
3009 HT=AX*(DUZ-DUZP1-WELJ*ZK)
HS=AX*(DVZ-DVZP1-WNIJ*ZK)
IF(MQ.EQ.1) GO TO 3008
IF(MQ.EQ.1211) GO TO 1211
IF(MQ.EQ.1112) GO TO 1112
IF(MQ.EQ.1121) GO TO 1121
IF(MQ.EQ.2211) GO TO 2211
IF(MQ.EQ.2112) GO TO 2112
IF(MQ.EQ.1221) GO TO 1221
IF(MQ.EQ.1122) GO TO 1122
IF(MQ.EQ.2121) GO TO 2121
IF(MQ.EQ.1212) GO TO 1212
IF(MQ.EQ.2221) GO TO 2221
IF(MQ.EQ.2212) GO TO 2212
IF(MQ.EQ.1222) GO TO 1222
IF(MQ.EQ.2122) GO TO 2122
2111 UP1J=-UIJ
VP1J=-VIJ
GO TO 3008
1211 UIP1=-UIJ
VIP1=-VIJ
GO TO 3008
1121 UM1J=-UIJ
VM1J=-VIJ
GO TO 3008
1112 VIM1=-VIJ
UIM1=-UIJ
GO TO 3008
2221 UP1J=-UIJ
VP1J=-VIJ
UIP1=-UIJ
VIP1=-VIJ
UM1J=-UIJ
VM1J=-VIJ
GO TO 3008
2212 UP1J=-UIJ
VP1J=-VIJ
VIP1=-VIJ
UIP1=-UIJ
UIM1=-UIJ
VIM1=-VIJ
GO TO 3008
1222 UIP1=-UIJ
VIP1=-VIJ
UM1J=-UIJ
VM1J=-VIJ
UIM1=-UIJ
VIM1=-VIJ
GO TO 3008
2122 UP1J=-UIJ
VP1J=-VIJ
UM1J=-UIJ
VM1J=-VIJ
UIM1=-UIJ
VIM1=-VIJ
GO TO 3008
2211 UP1J=-UIJ

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```

VP1J=-VIJ
UIP1=-UIJ
VIP1=-VIJ
GO TO 3008
2121 UP1J=-UIJ
VP1J=-VIJ
UM1J=-UIJ
VM1J=-VIJ
GO TO 3008
2112 UP1J=-UIJ
VP1J=-VIJ
UIM1=-UIJ
VIM1=-VIJ
GO TO 3008
1221 UIP1=-UIJ
VIP1=-VIJ
UM1J=-UIJ
VM1J=-VIJ
GO TO 3008
1212 UIP1=-UIJ
VIP1=-VIJ
UIM1=-UIJ
VIM1=-VIJ
GO TO 3008
1122 UM1J=-UIJ
VM1J=-VIJ
UIM1=-UIJ
VIM1=-VIJ
3008 HT=HT+AB*(UP1J+UM1J-2.0*UIJ)+AC*(UIP1-UIJ)-AD*(UIJ-UIM1)
HS=HS+AB*(VP1J+VM1J-2.0*VIJ)+AC*(VIP1-VIJ)-AD*(VIJ-VIM1)
IF(K.NE.1) GO TO 4000
PA=0.0
PB=0.0
GO TO 4001
4000 GO TO (5,6,7),NK
5 PA=PA+ZK*ALAL*(T(I,JP1,K)+T(I,JP1,KM1)-T(IP1,JP1,K)-T(IP1,JP1,K
1M1))
PB=PB+ZK*ALAL*(T(IP1,J,K)+T(IP1,J,KM1)-T(IP1,JP1,K)-T(IP1,JP1,KM
1))
GO TO 4001
6 PA=PA+ZK*ALAL*(T(I,J,K)+T(I,J,KM1)-T(IP1,J,K)-T(IP1,J,KM1))
PB=PB+ZK*ALAL*(T(I,J,K)+T(I,J,KM1)-T(I,JP1,K)-T(I,JP1,KM1))
GO TO 4001
7 CONTINUE
P1=T(I,JP1,K)+T(I,JP1,KM1)-T(IP1,J,K)-T(IP1,J,KM1)
P2=T(I,J,K)+T(I,J,KM1)-T(IP1,JP1,K)-T(IP1,JP1,KM1)
PA=PA+Z K * AL*(P1+P2)
PB=PB+Z K * AL*(P2-P1)
4001 TEN(I,J,K)=((-PA*AQ+PXBIJ)/R X MJ +HT)*DDT
SEN(I,J,K)=((-PB*AQ+PYBIJ)/R Y +HS)*DDT
3002 CONTINUE
3001 CONTINUE
4002 CONTINUE
3000 CONTINUE
UUU=0.0
VVV=0.0
IF(MAT.EQ.0) GO TO 3010
IF(MAT.EQ.((MAT/2)*2)) GO TO 3012
IF(MAT.EQ.1) GO TO 3013
C MAT=3,5,7
3011 READ(3) U,V
REWIND 3
DO 3106 J=JMH,JMM1
XJ1=XJA(J)/2.0
HT=1.0/(1.0+XJ1**2)
HS=YHS(J)/2.0

```

```

LJ=LV (J)
DO 4005 M1=1, LJ
II=IA (M1, J)
IG=LB (M1, J)
DO 3107 I=II, IG
DO 3108 K=1, KM
VL=XMJN*Z (K)
AIJ=U (I, J, K)
BIJ=V (I, J, K)
AUZ=AIJ+TEN (I, J, K) +HS*BIJ
AVZ=BIJ+SEN (I, J, K) -HS*AIJ
P1=(AUZ+XJ1*AVZ) *HT
P2=(AVZ-XJ1*AUZ) *HT
UU (I, J, K) =P1
VV (I, J, K) =P2
UUU=UUU+P1*P1*VL
VVV=VVV+P2*P2*VL

```

3108 CONTINUE  
3107 CONTINUE  
4005 CONTINUE  
3106 CONTINUE

```

10 DO 8 K=1, KM
DO 12 J=JMH, JMM1
UU (2, J, K) =UU (IM, J, K)
VV (2, J, K) =VV (IM, J, K)
UU (IMP1, J, K) =UU (3, J, K)
VV (IMP1, J, K) =VV (3, J, K)

```

12 CONTINUE  
8 CONTINUE

```

READ (2) T
REWIND 2
IF (MAT.EQ.7) GO TO 3120
WRITE (3) UU, VV
REWIND 3
DO 3999 K=1, KM
DO 3998 J=JMH, JMM1
DO 3997 I=1, IMP1
U (I, J, K) =UU (I, J, K)
V (I, J, K) =VV (I, J, K)

```

3997 CONTINUE  
3998 CONTINUE  
3999 CONTINUE  
GO TO 11

C  
3013 DO 3100 J=JMH, JMM1

```

LJ=LV (J)
XJ1=XJA (J)
HT=XHT (J)
HS=XHS (J)
XMJN=XMY (J)
DO 4003 M1=1, LJ
II=IA (M1, J)
IG=LB (M1, J)
DO 3101 I=II, IG
DO 3102 K=1, KM
VL=XMJN*Z (K)
AIJ=U (I, J, K)
BIJ=V (I, J, K)
AUZ=AIJ +TEN (I, J, K) +HS*BIJ
AVZ=BIJ+SEN (I, J, K) -HS*AIJ
AIJ=(AUZ+XJ1*AVZ) *HT
BIJ=(AVZ-XJ1*AUZ) *HT
UU (I, J, K) =AIJ
VV (I, J, K) =BIJ
UUU=UUU+ATJ*AIJ*VL

```

VVV=VVV+BIJ\*VI.  
 3102 CONTINUE  
 3101 CONTINUE  
 4003 CONTINUE  
 3100 CONTINUE  
 GO TO 10  
 MAT=2,4,6

12 DO 3103 J=JMH,JMM1  
 XJ1=XJA(J)/2.0  
 HT=1.0/(1.0+XJ1\*XJ1)  
 HS=XHS(J)/2.0  
 LJ=LV(J)  
 XMJN=XMY(J)  
 DO 4004 M1=1,LJ  
 II=LA(M1,J)  
 IG=LB(M1,J)  
 DO 3104 I=II,IG  
 DO 3105 K=1,KM  
 VL=XMJN\*Z(K)  
 AIJ=U(I,J,K)  
 BIJ=V(I,J,K)  
 AUZ=AIJ+TEN(I,J,K)+HS\*BIJ  
 AVZ=BIJ+SEN(I,J,K)-HS\*AIJ  
 P1=(AUZ+XJ1\*AVZ)\*HT  
 P2=(AVZ-XJ1\*AUZ)\*HT  
 U(I,J,K)=P1  
 UU(I,J,K)=P1  
 V(I,J,K)=P2  
 VV(I,J,K)=P2  
 UUU=UUU+P1\*P1\*VL  
 VVV=VVV+P2\*P2\*VI.

3105 CONTINUE  
 3104 CONTINUE  
 4004 CONTINUE  
 3103 CONTINUE  
 DO 3113 K=1,KM  
 DO 3114 J=JMH,JM  
 DO 3115 I=2,IMP1  
 T(I,J,K)=TT(I,J,K)  
 3115 CONTINUE  
 3114 CONTINUE  
 3113 CONTINUE  
 GO TO 3120

C MAT=0  
 3010 DO 3109 J=JMH,JMM1  
 XJ1=XJA(J)  
 HT=XHT(J)  
 HS=XHS(J)  
 XMJN=XMY(J)  
 LJ=LV(J)  
 DO 4006 M1=1,LJ  
 II=LA(M1,J)  
 IG=LB(M1,J)  
 DO 3110 I=II,IG  
 DO 3111 K=1,KM  
 VL=Z(K)\*XMJN  
 AIJ=U(I,J,K)  
 BIJ=V(I,J,K)  
 U(I,J,K)=UU(I,J,K)  
 V(I,J,K)=VV(I,J,K)  
 AUZ=AIJ+TEN(I,J,K)+HS\*BIJ  
 AVZ=BIJ+SEN(I,J,K)-HS\*AIJ  
 P1=(AUZ+XJ1\*AVZ)\*HT  
 P2=(AVZ-XJ1\*AUZ)\*HT  
 UU(I,J,K)=P1  
 VV(I,J,K)=P2

UUU=UUU+P1+P1\*VL  
VVV=VVV+P2\*P2\*VL

711

3111 CONTINUE

3110 CONTINUE

4006 CONTINUE

3109 CONTINUE

4020 CONTINUE

DO 4007 K=1, KM  
DO 4008 J=JMH, JMM1  
U(2, J, K) = U(IM, J, K)  
V(2, J, K) = V(IM, J, K)  
UU(2, J, K) = UU(IM, J, K)  
VV(2, J, K) = VV(IM, J, K)  
U(IMP1, J, K) = U(3, J, K)  
V(IMP1, J, K) = V(3, J, K)  
UU(IMP1, J, K) = UU(3, J, K)  
VV(IMP1, J, K) = VV(3, J, K)

4008 CONTINUE

4007 CONTINUE

11 UUU=UUU\*ERH

VVV=VVV\*RRH

UV=UUU+VVV

RETURN

END

SUBROUTINE CONTI

COMMON T(147, 39, 5), TT(147, 39, 5), SP(147, 39), AT(5), HU(147, 39, 5),  
1VV(147, 39, 5), U(147, 39, 5), V(147, 39, 5), W(147, 39, 5), UB(147, 39),  
2VB(147, 39), WE(147, 39), WN(147, 39), Q(39), XJA(38), XHT(38), XHS(38),  
3 XMY(38), Z(5), X(39), XM(39), FU(39), FJU(39), ZZ(6), H, AZ, AH, DT, AL,  
4GAM, Y, YY, R, RR, HH, H2, AZHH, R2, AHY, AHPR, AH2, BS, BE2, AAA, BBE, DDT, A1, UV,  
5UUU, VVV, RRH, AQ, GAM2, AL2, BUN, RY, AM, AMRR, GANGAM, ALAL, BAN, KMP1,  
6MPP(147, 39), MOQ(147, 39), IM, JM, KM, IMM1, JMM1, KMM1, IMP1, JMP1, MAT,  
7 NK, NNN, IMH, JMH, MATS, L(39), KA(10, 39), KB(10, 39), LV(39), NEND,  
8LA(10, 39), LB(10, 39), NN, TF(147, 46), UN(147, 39), TD(147, 46), PN(147, 39)  
\*, CL(147, 39)

DIMENSION WWW(10)

5 DO 1000 J=3, JM

XJ=X(J)

JM1=J-1

XMJ=XM(J)

XM1=XM(JM1)

WT=1.0/(XJ\*Y)

B=XMJ\*WT

CCC=XM1\*WT

LJ=L(J)

DO 1 M1=1, LJ

II=KA(M1, J)

IG=KB(M1, J)

DO 1001 I=II, IG

MP=MPP(I, J)

IM1=I-1

IF(MP.EQ.1) GO TO 1200

1999 IF(MP.EQ.11) GO TO 1011

IF(MP.EQ.12) GO TO 1012

IF(MP.EQ.13) GO TO 1013

IF(MP.EQ.14) GO TO 1014

IF(MP.EQ.21) GO TO 1021

IF(MP.EQ.22) GO TO 1022

IF(MP.EQ.23) GO TO 1023

IF(MP.EQ.24) GO TO 1024

IF(MP.EQ.31) GO TO 1031

IF(MP.EQ.32) GO TO 1032

IF(MP.EQ.34) GO TO 1034

1033 DO 1113 K=1, KMM1

WWW(K) = ((UU(I, J, K) + UU(I, JM1, K) - UU(IM1, J, K)) / XJ

1 + (VV(I, J, K) + VV(IM1, J, K)) \* B - VV(I, JM1, K) \* CCC) \* BAN \* Z(K)

```

1113 CONTINUE
GO TO 1998
1200 DO 1003 K=1,KMM1
WWW(K)=((UU(I,J,K)+UU(IM1,J,K)-UU(IM1,J,K)-UU(JM1,JM1,K))/XJ
1+(VV(I,J,K)+VV(IM1,J,K))*B-(VV(I,JM1,K)+VV(IM1,JM1,K))*CCC)/2.0
2)*Z(K)
1003 CONTINUE
GO TO 1998
1011 DO 1004 K=1,KMM1
WWW(K)=(-(UU(IM1,J,K)+UU(IM1,JM1,K))/XJ+VV(IM1,J,K)*B
1-VV(IM1,JM1,K)*CCC)*Z(K)
1004 CONTINUE
GO TO 1998
1012 DO 1005 K=1,KMM1
WWW(K)=((UU(I,JM1,K)-UU(IM1,JM1,K))/XJ-
1(VV(I,JM1,K)+VV(IM1,JM1,K))*CCC)*Z(K)
1005 CONTINUE
GO TO 1998
1013 DO 1006 K=1,KMM1
WWW(K)=((UU(I,J,K)+UU(I,JM1,K))/XJ+VV(I,J,K)*B-VV(I,JM1,K)*CCC)*
1Z(K)
1006 CONTINUE
GO TO 1998
1014 DO 1007 K=1,KMM1
WWW(K)=((UU(I,J,K)-UU(IM1,J,K))/XJ+(VV(I,J,K)+VV(IM1,J,K))*B)*Z(K)
1007 CONTINUE
GO TO 1998
1021 DO 1008 K=1,KMM1
WWW(K)=(-UU(IM1,JM1,K)/XJ-VV(IM1,JM1,K)*CCC)*2.0*Z(K)
1008 CONTINUE
GO TO 1998
1022 DO 1009 K=1,KMM1
WWW(K)=(UU(I,JM1,K)/XJ-VV(I,JM1,K)*CCC)*2.0*Z(K)
1009 CONTINUE
GO TO 1998
1023 DO 1109 K=1,KMM1
WWW(K)=2.0*Z(K)*(UU(I,J,K)/XJ+VV(I,J,K)*B)
1109 CONTINUE
GO TO 1998
1024 DO 1110 K=1,KMM1
WWW(K)=2.0*Z(K)*(-UU(IM1,J,K)/XJ+VV(IM1,J,K)*B)
1110 CONTINUE
GO TO 1998
1031 DO 1111 K=1,KMM1
WWW(K)=((UU(I,JM1,K)-UU(IM1,J,K)-UU(IM1,JM1,K))/XJ+VV(JM1,J,K)*B
1-(VV(I,JM1,K)+VV(IM1,JM1,K))*CCC)*BAN*Z(K)
1111 CONTINUE
GO TO 1998
1032 DO 1112 K=1,KMM1
WWW(K)=((UU(I,J,K)+UU(I,JM1,K)-UU(IM1,JM1,K))/XJ
1-(VV(IM1,JM1,K)+VV(I,JM1,K))*CCC+VV(I,J,K)*B)*BAN*Z(K)
1112 CONTINUE
GO TO 1998
1034 DO 1114 K=1,KMM1
WWW(K)=((UU(I,J,K)-UU(IM1,JM1,K)-UU(IM1,J,K))/XJ
1+(VV(I,J,K)+VV(IM1,J,K))*B-VV(IM1,JM1,K)*CCC)*BAN*Z(K)
1114 CONTINUE
1998 WT=0.0
DO 1997 K=1,KMM1
W1=WT+WWW(K)
W(I,J,K+1)=W1
WT=W1
1997 CONTINUE
1001 CONTINUE
1 CONTINUE
1000 CONTINUE

```



END

SUBROUTINE THERME

```

COMMON T(147,39,5), TT(147,39,5), SP(147,39), AT(5), HU(147,39,5),
1VV(147,39,5), U(147,39,5), V(147,39,5), W(147,39,5), UE(147,39),
2VB(147,39), WE(147,39), WN(147,39), Q(39), XJA(38), XHT(38), XHS(38),
3 XMY(38), Z(5), X(39), XM(39), FU(39), FJU(39), ZZ(6), H, AZ, AH, DT, AL,
4GAM, Y, YY, R, RP, HH, H2, AZHH, R2, AHY, AHPE, AH2, BB, BB2, AAA, BBB, DDT, A1, UV,
5HUU, VVV, RRR, AQ, GAM2, AL2, RUM, RY, AM, AMPE, GANGAM, ALAL, BAN, KMP1,
6MPP(147,39), HQQ(147,39), JM, JM, KM, IMM1, JMM1, KMM1, IMP1, JMP1, MAT,
7 NK, NNN, IMB, JMH, MATS, L(39), KA(10,39), KB(10,39), LV(39), NEND,
8LA(10,39), LB(10,39), NN, TE(147,46), UN(147,39), TD(147,46), RN(147,39)
*, CL(147,39)

```

COMMON/TEMP/TFN(147,39,5)

HG=H\*490.0

IF(MAT.NE.8) GO TO 6

MAT=0

WRITE(6,234) NN

234 FORMAT(1H,3HEND,4X,5HTIME=I6)

6 CONTINUE

SBC=8.3E-11\*0.01666

DO 20 J=JM, JM

JM1=J-1

QJ=Q(J)

XJ=X(J)

JP1=J+1

AA=1.0/(R2\*XJ)

AA2=AA/2.0

XJ1=X(JM1)

XMJ=X(J)

XMJ1=XM(JM1)

BB2=XMJ\*AA2/Y

AH22=AH2\*XMJ/XJ

BB1=BB2\*2.0

CC2=XMJ1\*AA2/Y

CC=CC2\*2.0

AHM=AH Y/XJ

AH1=AHFR/(XJ\*XJ)

AH3=AH2\*XMJ1/X J

LJ=L(J)

DO 4011 M1=1, LJ

II=KA(M1, J)

IG=KB(M1, J)

DO 21 I=II, IG

UM=UN(I, J)\*51.48

TEIJ=TE(I, J)

CLN=CL(I, J)\*0.125

MP=MPP(I, J)

RSN=QJ\*(1.-0.7\*CLN)

C\*\*\*\*\*COMPUTATION OF PRESSURE\*\*\*\*\*

PZ=0.0

PZ1=0.0

DO 4018 K=1, KMM1

KP1=K+1

PZ=PZ-ZZ(KP1)\*AL2\*(TT(I, J, K)+TT(I, J, KP1))

PZ1=PZ1+PZ\*Z(KP1)

4018 CONTINUE

SP(I, J)=PZ1\*HG

IP1=I+1

IM1=I-1

UBJ=UB(I, J)

UBM1J=UB(IM1, J)

UBIM1=UB(I, JM1)

VBIJ=VB(I, J)

VBM1J=VB(IM1, J)

VBIM1=VB(I, JM1)

```

UBM1M1=UB(IM1, JM1, KM1)
VBM1M1=VB(IM1, JM1)
TA=TE(I, J)+273.15
TW=TD(I, J)+273.15
123 TS=T(I, J, 1)+273.15
PCB=1013.25*0.1
ESS=10.0**(8.4051-2353.0/TS)
ESD=10.0**(8.4051-2353.0/TW)
RLN=SBC*TS**4*0.985*(0.39-0.05*SQRT(ESD*10.))*(1.-0.6*CLN**2)
RNS=RSN-RLN
RN(I, J)=RNS
QS=0.622*ESS/(PCB-ESS)
QA=0.622*ESD/(PCB-ESD)
DO 22 K=1, KM
KP1=K+1
ZZ1=ZZ(KP1)
ZZK=ZZ(K)
ZK=Z(K)

```

```

C VERTICAL DIFFUSION(HT, HS) AND VERTICAL ADVECTION(WT, WS)
WIJ=W(I, J, K)
CC1=1.0/(R2*ZK)
KM1=K-1
TTP1J=TT(IP1, J, K)
TTM1J=TT(IM1, J, K)
TTIP1=TT(I, JP1, K)
TTIM1=TT(I, JM1, K)
TTIJ=TT(I, J, K)
TIJ=T(I, J, K)
IF(K.EQ.1.AND.((TIJ-TI1J)+0.609*TS*(QS-QA)).GE.0.0) GO TO 333
IF(K.EQ.1) GO TO 334
TXIJ=(T(I, J, KM1)-TIJ)/ZZK
WT=(TTIJ+TT(I, J, KM1))*WIJ
IF(K.NE.KM) GO TO 2003
TYIJ=C.0
PK=0.0
PK1=0.0
GO TO 2004

```

```

333 CH=0.033
CO=1.23*0.001
GO TO 133

```

```

334 CU=0.018
CO=0.41*0.001
133 QH=1.2*0.001*0.24*CO*UM*(TIJ-TI1J)
QE=1.2*0.001*CO*595.*UM*(QS-QA)
TXIJ=(RNS-QH-QE)*H/AZ
WT=0.0

```

```

2003 TYIJ=(TIJ-T(I, J, KP1))/ZZ1
WIJP=W(I, J, KP1)
PK=(TTIJ+TT(I, J, KP1))*WIJP

```

```

2004 HS=AZHH/ZK
WT=(WT-PK)*CC1
HT=HS*(TXIJ-TYIJ)
C HORIZONTAL DIFFUSION(HT, HS) AND HORIZONTAL ADVECTION(WT, WS)

```

```

TXIJ=(T(IP1, J, K)-TIJ)*AH1
TXM1J=(TIJ-T(IM1, J, K))*AH1
TYIJ=(T(I, JP1, K)-TIJ)*AH2
TYIM1=(TIJ-T(I, JM1, K))*AH3
VIJ=VV(I, J, K)+VBIJ
VM1J=VV(IM1, J, K)+VBM1J
VIM1=VV(I, JM1, K)+VBIM1
VM1M1=VV(IM1, JM1, K)+VEM1M1
UIJ=UU(I, J, K)+UBIJ
UM1J=UU(IM1, J, K)+UBM1J
UIM1=UU(I, JM1, K)+UBIM1
UM1M1=UU(IM1, JM1, K)+UBM1M1
IF(MP.EQ.1) GO TO 2001

```

IF(MP.EQ.11) GO TO 2011  
 IF(MP.EQ.12) GO TO 2012  
 IF(MP.EQ.13) GO TO 2013  
 IF(MP.EQ.14) GO TO 2014  
 IF(MP.EQ.21) GO TO 2021  
 IF(MP.EQ.23) GO TO 2023  
 IF(MP.EQ.24) GO TO 2024  
 IF(MP.EQ.31) GO TO 2031  
 IF(MP.EQ.32) GO TO 2032  
 IF(MP.EQ.34) GO TO 2034  
 IF(MP.EQ.22) GO TO 2022

2033 F=UIJ+UIM1  
 G=(VIJ+VM1J)\*BB2  
 FF=VIM1\*CC2  
 WT=WT+((TTIJ+TTP1J)\*F - (TTIJ+TTM1J)\*UM1J)\*AA2+  
 1(TTIJ+TTIP1)\*G - (TTIJ+TTIM1)\*FF ) \*BUN  
 HT=HT+(TXIJ+TYIJ-(TXM1J+TYIM1)/2.0)\*BUN  
 GO TO 2005

2001 F=UIJ+UIM1  
 G=(VIJ+VM1J)\*BB2  
 FF=UM1J+UM1M1  
 GG=(VIM1+VM1M1)\*CC2  
 WT=WT+((TTIJ+TTP1J)\*F - (TTIJ+TTM1J)\*FF ) \*AA2  
 1+(TTIJ+TTIP1)\*G - (TTIJ+TTIM1)\*GG  
 HT=TXIJ-TXM1J+TYIJ-TYIM1+HT  
 GO TO 2005

2011 F=(UM1M1+UM1J)\*AA  
 G=VM1J\*BB1  
 FF=VM1M1\*CC  
 WT=WT-(TTIJ+TTM1J)\*F + (TTIJ+TTIP1)\*G  
 1-(TTIJ+TTIM1)\*FF  
 HT=-TXM1J\*2.0+TYIJ-TYIM1+HT  
 GO TO 2005

2012 F=(VIM1+VM1M1)\*CC  
 WT=WT+((TTIJ+TTP1J)\*UIM1-(TTIJ+TTM1J)\*UM1M1)\*AA  
 1-(TTIJ+TTIM1)\*F  
 HT=TXIJ-TXM1J-TYIM1\*2.0+HT  
 GO TO 2005

2013 F=(UIJ+UIM1)\*AA  
 G=VIJ\*BB1  
 FF=VIM1\*CC  
 WT=WT+(TTIJ+TTP1J)\*F + (TTIJ+TTIP1)\*G  
 1-(TTIJ+TTIM1)\*FF  
 HT=TXIJ\*2.0+TYIJ-TYIM1+HT  
 GO TO 2005

2014 F=(VIJ+VM1J)\*BB1  
 WT=WT+((TTIJ+TTP1J)\*UIJ-(TTIJ+TTM1J)\*UM1J)\*AA  
 1+(TTIJ+TTIP1)\*F  
 HT=TXIJ-TXM1J+TYIJ\*2.0+HT  
 GO TO 2005

2021 F=UM1M1\*AA  
 G=VM1M1\*CC  
 WT=WT-(TTIJ+TTM1J)\*F \*2.0-(TTIJ+TTIM1)\*G \*2.0  
 HT=HT-(TXM1J+TYIM1)\*2.0  
 GO TO 2005

2022 F=UIM1\*AA  
 G=VIM1\*CC  
 WT=WT+((TTIJ+TTP1J)\*F - (TTIJ+TTIM1)\*G ) \*2.0  
 HT=(TXIJ-TYIM1)\*2.0+HT  
 GO TO 2005

2023 F=UIJ\*AA  
 G=VIJ\*BB1  
 WT=WT+((TTIJ+TTP1J)\*F + (TTIJ+TTIP1)\*G ) \*2.0  
 HT=(TXIJ+TYIJ)\*2.0+HT  
 GO TO 2005

2024 F=UM1J\*AA

```

G=VT+LJ
WT=WT-((TTIJ+TTM1J)*F-(TTIJ+TTIP1)*G)*2.0
HT=(TYIJ-TXM1J)*2.0+HT
GO TO 2005
2031 F=UM1M1+UM1J
G=VM1J*BB2
PF=(VIM1+VM1M1)*CC2
WT=WT+(((TTIJ+TTP1J)*UIM1-(TTIJ+TTM1J)*F) *AA2+
1 (TTIJ+TTIP1)*G - (TTIJ+TTIM1)*FF ) *BUN
HT=((TXIJ+TYIJ)/2.0-TXM1J-TYIM1)*BUN+HT
GO TO 2005
2032 F=UIM1+UIJ
G=VIJ*BB2
FF=(VIM1+VM1M1)*CC2
WT=WT+(((TTIJ+TTP1J)*F-(TTIJ+TTM1J)*UM1M1) *AA2+
1 (TTIJ+TTIP1)*G - (TTIJ+TTIM1)*FF ) *BUN
HT=((TYIJ-TXM1J)/2.0+TXIJ-TYIM1)*BUN+HT
GO TO 2005
2034 G=(VIJ+VM1J)*BB2
F=VM1M1*CC2
FF=UM1J+UM1M1
WT=WT+(((TTIJ+TTP1J)*UIJ-(TTIJ+TTM1J)*FF) *AA2+
1 (TTIJ+TTIP1)*G - (TTIJ+TTIM1)*F ) *BUN
HT=((TXIJ-TYIM1)/2.0-TXM1J+TYIJ)*BUN+HT
2005 TEN(I,J,K)=DDI*(HT-WT/0.93)
22 CONTINUE
21 CONTINUE
4011 CONTINUE
20 CONTINUE
IF(MAT.EQ.0) GO TO 2036
IF(MAT.EQ.((MAT/2)*2)) GO TO 2037
IF(MAT.EQ.1) GO TO 2038
MAT=3,5,7
2035 READ(2) TT
REWIND 2
DO 38 J=JMH,JM
LJ=L(J)
DO 4014 M1=1,LJ
II=KA(M1,J)
IG=KB(M1,J)
DO 39 I=II,IG
DO 40 K=1,KM
AT(K)=TT(I,J,K)+TEN(I,J,K)
40 CONTINUE
CALL ADJUST
DO 41 K=1,KM
TT(I,J,K)=AT(K)
41 CONTINUE
39 CONTINUE
4014 CONTINUE
38 CONTINUE
IF(MAT.EQ.7) GO TO 2500
9 DO 2 K=1,KM
DO 3 J=JMH,JM
TT(IME1,J,K)=TT(3,J,K)
TT(2,J,K)=TT(IM,J,K)
T(2,J,K)=T(IM,J,K)
T(IMP1,J,K)=T(3,J,K)
3 CONTINUE
2 CONTINUE
WRITE(2) TT
REWIND 2
GO TO 10
MAT=1
2038 DO 30 J=JMH,JM
LJ=L(J)

```

```

DO 4012 M1=1, LJ
II=KA(M1, J)
IG=KB(M1, J)
DO 31 I=II, IG
DO 32 K=1, KM
AT(K)=T(I, J, K)+TEN(I, J, K)
32 CONTINUE
CALL ADJUST
DO 33 K=1, KM
T(I, J, K)=TT(I, J, K)
TT(I, J, K)=AT(K)
33 CONTINUE
31 CONTINUE
4012 CONTINUE
30 CONTINUE
GO TO 9

```

```

C MAT=2, 4, 6
2037 DO 34 J=JMH, JM
LJ=L(J)
DO 4013 M1=1, LJ
II=KA(M1, J)
IG=KB(M1, J)
DO 35 I=II, IG
DO 36 K=1, KM
AT(K)=T(I, J, K)+TEN(I, J, K)
36 CONTINUE
CALL ADJUST
DO 37 K=1, KM
TT(I, J, K)=AT(K)
37 CONTINUE
35 CONTINUE
4013 CONTINUE
34 CONTINUE
GO TO 2500

```

```

C MAT=0
2036 DO 42 J=JMH, JM
LJ=L(J)
DO 4015 M1=1, LJ
II=KA(M1, J)
IG=KB(M1, J)
DO 43 I=II, IG
DO 44 K=1, KM
AT(K)=T(I, J, K)+TEN(I, J, K)
44 CONTINUE
CALL ADJUST
DO 45 K=1, KM
T(I, J, K)=TT(I, J, K)
TT(I, J, K)=AT(K)
45 CONTINUE
43 CONTINUE
4015 CONTINUE
42 CONTINUE
2500 CONTINUE
DO 4016 K=1, KM
DO 4017 J=JMH, JM
T(2, J, K)=T(IM, J, K)
TT(2, J, K)=TT(IM, J, K)
T(IMP1, J, K)=T(3, J, K)
TT(IMP1, J, K)=TT(3, J, K)
4017 CONTINUE
4016 CONTINUE
10 DO 4019 J=JMH, JM
SP(IMP1, J)=SP(3, J)
4019 CONTINUE
RETURN
END

```

```

SUBROUTINE PREP,
RETURN
END
SUBROUTINE GEOST
RETURN
END
SUBROUTINE PREPA
RETURN
END
SUBROUTINE SHADE (ICTL, RCTL, BVAL)

```

78/

```

REAL RCTL (2), BVAL (44), ALIN (132), BLIN (132)
INTEGER ICTL (8)
LOGICAL*1 BLANK, ' ', LP, '(', '/', QM, ' ', ' ', RP, ' ', ' '
LOGICAL*1 PRSTLN, DATAL, NSHADE, COND, CLIN (137), CTBL (20)

```

```

C *****
C CALL SHADE (ICTL, RCTL, RFIELD) *
C *****
C ICTL (1) ... CALL CODE *
C =0 -NORMAL INTRA-FIELD CALL *
C (ONLY RFIELD IS USED, ICTL (2) THRU ICTL (8) AND *
C RCTL ARE IGNORED) *
C =1 -BEGINNING-OF-FIELD CALL *
C (ONLY ICTL AND RCTL PARAMETERS ARE USED, RFIELD *
C IS IGNORED) *
C ICTL (2) ... OUTPUT TAPE NUMBER *
C ICTL (3) ... LEFT (SHADE) MARGIN *
C ICTL (4) ... NUMBER OF SHADING LINES *
C ICTL (5) ... NUMBER OF FIELDS *
C ICTL (6) ... FIELD WIDTH *
C ICTL (7) ... DOES THE CALLING PROGRAM PRINT INTERSPERSED DATA *
C =1 -NO *
C =2 -YES *
C ICTL (8) ... IGNORED *
C ..... *
C RCTL (1) ... CYCLE POINT *
C RCTL (2) ... SHADE INTERVAL *
C ..... *
C RFIELD ... ONE DIMENSIONAL VECTOR WITH NUMERIC INFORMATION *
C TO BE SHADED *
C *****
IF (ICTL (1) .NE. 0) GO TO 1000
XL= (BVAL (1) -CP) /SINT
M2=LM
IF (COND) GO TO 3100
BLIN (LM) = (XL -ALIN (LM)) /VDIVS
3021 DO 3029 K=LP, NE, ISKP
M1=M2+1
M2=M2+IFW
XR= ((BVAL (K) -CP) /SINT -XL) /FW
DO 3029 J=M1, M2
XL=XL+XR
3029 BLIN (J) = (YL -ALIN (J)) /VDIVS
3051 DO 3059 L=1, NSL
3041 DO 3049 K=LM, MR
ALIN (K) =ALIN (K) +BLIN (K)
TBLC=AMOD (ALIN (K), TLEN) +1.
IF (TBLC .LT. 1.) TBLC=TBLC+TLEN
IT=TBLC
3049 CLIN (K+2) =CTBL (IT)
3059 WRITE (NTP, CLIN)
IF (.NOT. DATAL) RETURN
3061 DO 3069 K=LM, MR
3069 ALIN (K) =ALIN (K) +BLIN (K)
RETURN

```

```

00000100
00000120
00000140
00000160
00000180
00000200
00000220
00000240
00000260
00000280
00000300
00000320
00000340
00000360
00000380
00000400
00000420
00000440
00000460
00000480
00000500
00000520
00000540
00000560
00000580
00000600
00000620
00000640
00000660
00000680
00000700
00000720
00000740
00000760
00000780
00000800
00000820
00000840
00000860
00000880
00000900
00000920
00000940
00000960
00000980
00001000
00001020
00001040
00001060
00001080
00001100
00001120
00001140
00001160
00001180
00001200
00001220

```

```

3100 IF (NSHADE) GO TO 2000
COND=.FALSE.
ALIN(LM)=XL
3121 DO 3129 K=LF,NF,ISKP
N1=M2+1
M2=M2+IFW
XR=((BVAL(K)-CP)/SINT-XL)/FW
DO 3129 J=N1,M2
XL=XL+XR
3129 ALIN(J)=XL
IF (DATA) RETURN
3141 DO 3149 K=LM,MR
TBLC=AMOD(ALIN(K),TLEN)+1.
IF (TBLC.LT.1.) TBLC=TBLC+TLEN
IT=TBLC
3149 CLIN(K+2)=CTBL(IT)
WRITE(NTP,CLIN)
RETURN
2000 IF (FRSTLN) GO TO 2030
2011 DO 2019 L=1,NSL
2019 WRITE(NTP,CLIN)
2030 FRSTLN=.FALSE.
RETURN
C*****
1000 CONTINUE
ISKP=ICTL(1)
LF=ISKP+1
NTP=ICTL(2)
LM=ICTL(3)
NSL=ICTL(4)
NF=ICTL(5)
IFW=ICTL(6)
DATA=ICTL(7).NE.1
VDIVS=NSL
IF (DATA) VDIVS=VDIVS+1.
IF (LM.LT.2) LM=2
IF (IFW.LT.2) IFW=2
FW=IFW
NS=(NF-1)/ISKP+1
MR=LM+(NS-1)*IFW
IF (MR.LE.LL) GO TO 1011
NF=(LL-LM)/IFW*ISKP+1
NS=(NF-1)/ISKP+1
MR=LM+(NS-1)*IFW
1011 CP=RCTL(1)
SINT=RCTL(2)
FRSTLN=.TRUE.
COND=.TRUE.
NSHADE=SINT.EQ.0.
IF (.NOT.NSHADE) GO TO 1021
SINT=1.
CP=0.
MR=1
LM=1
1021 DO 1029 I=1,LM
1029 CLIN(I+2)=BLANK
CLIN(1)=LP
CLIN(2)=QM
CLIN(MR+3)=QM
CLIN(MR+4)=RP
RETURN
DATA LL/132/
DATA TLEN/20.0/, CTBL/1H0,1H ,1H1,1H ,1H2,1H ,1H3,1H ,1H4,1H
*, 1H5,1H ,1H6,1H ,1H7,1H ,1H8,1H ,1H9,1H /
END

```

(79)

```

0.001240
00001260
00001280
00001300
00001320
00001340
00001360
00001380
00001400
00001420
00001440
00001460
00001480
00001500
00001520
00001540
00001560
00001580
00001600
00001620
00001640
00001660
1680
00001700
00001720
00001740
00001760
00001780
00001800
00001820
00001840
00001860
00001880
00001900
00001920
00001940
00001960
00001980
0002000
0002020
0002040
0002060
0002080
0002100
0002120
0002140
0002160
0002180
0002200
0002220
0002240
0002260
0002280
0002300
0002320
0002340
0002360
0002380
0002400
0002420
0002440
0002460
0002480
0002500
0002520

```

SUBROUTINE PREP

DATA: IM, JM, KM, IMH, JMH  
 OCEAN SHAPE (SUBROUTINE SHAPE2)  
 H, Z (I)  
 AZ, AM, AH  
 WE, WN (GIVEN FROM CARDS, OR A TAPE OR THE SUBROUTINE WIND)  
 Q (J) (HEATING FUNCTION, REFERENCE ATMOSPHERIC TEMPERATURE)  
 AT (K) (INITIAL TEMPERATURE)  
 UB, VB (GIVEN FROM CARDS, OR A MAGNETIC TAPE, OR THE SUBROUTINE  
 BARO)  
 BB, AAA, BBB (AAA: GRID SIZE IN LATITUDE, BBB: GRID SIZE IN  
 LONGITUDE. BOTH IN DEGREES. BB IS THE LATITUDE CORRESPOND-  
 ING TO J=0.)

```

COMMON P (147, 39, 5), TT (147, 39, 5), SP (147, 39), AT (5), UD (147, 39, 5),
1VV (147, 39, 5), U (147, 39, 5), V (147, 39, 5), W (147, 39, 5), UB (147, 39),
2VB (147, 39), WE (147, 39), WN (147, 39), Q (39), XJA (38), XHT (38), XHS (38),
3 XNY (38), Z (5), X (39), XM (39), FU (39), FJU (39), ZZ (6), H, AZ, AH, DT, AL,
4GAM, Y, YY, R, RR, HH, H2, AZHH, R2, AHY, AHR, AH2, BB, BE2, AAA, BBB, DDT, A1, UV,
5DUU, VVV, FRH, AQ, GAM2, AL2, BUN, RY, AM, AMR, GAMGAM, AIAL, BAN, KMP1,
6MPP (147, 39), MOQ (147, 39), IM, JM, KM, IMM1, JMM1, KMM1, IMP1, JMP1, MAT,
7 NK, NNN, IMH, JMH, MATS, L (39), KA (10, 39), KB (10, 39), LV (39), NEND,
8LA (10, 39), LF (10, 39)
  READ (5, 80) IM, JM, KM, IMH, JMH
80 FORMAT (5I5)
  JMP1=JM+1
  JMM1=JM-1
  IMP1=IM+1
  IMM1=IM-1
  KMM1=KM-1
  CALL SHAPE2
  CALL SHAPE2
  DO 47 K=1, KM
  DO 48 J=1, JMP1
  DO 49 I=1, IMP1
  UD (I, J, K) = 0.0
  VV (I, J, K) = 0.0
  W (I, J, K) = 0.0
  U (I, J, K) = 0.0
  V (I, J, K) = 0.0
  TT (I, J, K) = 0.0
  T (I, J, K) = 0.0
49 CONTINUE
48 CONTINUE
47 CONTINUE
  READ (5, 81) H, (Z (I), I=1, KM)
81 FORMAT (E15.7, 5F10.2)
  WRITE (6, 13) (Z (I), I=1, KM)
13 FORMAT (1H, 19HDEPTHS FOR T, U, V=5F10.5)
  KMP1=KM+1
  ZZ (1) = -2.0*Z (1)
  DO 82 I=2, KM
  ZZ (I) = Z (I-1) - Z (I)
82 CONTINUE
  ZZ (KMP1) = 2.0* (1.0+Z (KM))
  DO 83 I=1, KM
  Z (I) = (ZZ (I) + ZZ (I+1)) / 2.0
83 CONTINUE
  WRITE (6, 33) H, (Z (I), I=1, KM)
33 FORMAT (1H, 2HH=E15.7, 2X, 2HZ=6E15.7)
  WRITE (6, 21) (ZZ (I), I=1, KMP1)
21 FORMAT (1H, 3HZZ=7E15.7)

```



```

34 READ(5,84) AZ,AA,AB
4567 DO 4568 J=1,39
DO 4569 I=1,IMP1
WE(I,J)=0.0
WN(I,J)=0.0
4569 CONTINUE
4568 CONTINUE
CALL WIND
CALL WIND
AL=H/AZ
DO 2000 J=1,IMP1
DO 2001 I=1,IMP1
WE(I,J)=WE(I,J)*AL
MP=MPP(I,J)
IF(MP.LE.1) GO TO 2003
IF(MP.GT.5) GO TO 2003
DO 2002 K=1,KM
T(I,J,K)=0.0
TT(I,J,K)=0.0
W(I,J,K)=444.444
2002 CONTINUE
2003 IF(MQQ(I,J).NE.2) GO TO 2001
DO 2004 K=1,KM
U(I,J,K)=333.333
UU(I,J,K)=333.333
VV(I,J,K)=444.444
V(I,J,K)=-444.444
2004 CONTINUE
2001 CONTINUE
2000 CONTINUE
READ(5,5) (Q(J),J=JMH,JM)
5 FORMAT(12F5.0)
DO 5094 J=3,38
READ(5,5095) (AT(K),K=1,KM)
5095 FORMAT(5F10.2)
LJ=L(J)
DO 5096 LL=1,LJ
IM1=KA(LL,J)
IP1=KB(LL,J)
DO 97 I=IM1,IP1
DO 98 K=1,KM
T(I,J,K)=AT(K)
TT(I,J,K)=AT(K)
98 CONTINUE
97 CONTINUE
5096 CONTINUE
5094 CONTINUE
DO 200 J=3,38
DO 201 K=1,KM
T(IMP1,J,K)=T(3,J,K)
TT(IMP1,J,K)=TT(3,J,K)
T(2,J,K)=T(IM,J,K)
TT(2,J,K)=TT(IM,J,K)
201 CONTINUE
200 CONTINUE
CALL BARO
CALL BARO
AL=COEFFICIENT OF THERMAL EXPANSION
3 AL=0.2E-3
ALAL=AL*2.0
HEAT FLUX ACROSS THE SEA SURFACE IS SPECIFIED AS 70.0*(Q(J)-
TT(I,J,1)) CAL/DAY
GAMGAM=H*70.0/(AZ*0.864E5)
R=6.37E8
READ(5,1) BB,AAA,BBB

```

```

1 FORMAT(3F10.0)
HR=3.1415926/180.0
RY=AAA*HH
Y=HH*EBB
DO 10 I=1, JMP1
A1=(BB+BBB*FLOAT(I))*HH
X(I)=RY*COS(A1)
10 CONTINUE
CD=14.58E-5/(Y*RY)
DO 9997 J=1,38
XM(J)=(X(J)+X(J+1))/2.0
FJU(J)=CD*(X(J)-X(J+1))
9997 CONTINUE

```

AAA AND BBB ARE WEIGHTS IN THE IMPLICIT SCHEME FOR THE INERTIA OSCILLATION

```

AAA=0.6
BBB=0.4
RR=R*R
RRH=RR*H
AL2=AL/2.0
HH=H*H
AZHH=AZ/HH
R2=R*2.0
AHY=AH*Y
AQ=245.0*H
BB=YY*RR
A1=AM/BB
AHRH=AH/RR
BUN=4.0/3.0
BAN=2.0/3.0
AMRR=AM/RR
AH2=AH/BB
RY=R*Y
BB=1.0/(Y*R)
BB2=BB/2.0
RETURN
END

```

SUBROUTINE BARO

```

RETURN
END

```

SUBROUTINE WIND

```

RETURN
END

```

SUBROUTINE SHAPE2

```

COMMON T(147,39,5),TT(147,39,5),SP(147,39),AT(5),UU(147,39,5),
1VV(147,39,5),U(147,39,5),V(147,39,5),W(147,39,5),UB(147,39),
2VB(147,39),WE(147,39),WN(147,39),Q(39),XJA(38),XHT(38),XHS(38),
3 XMY(38),Z(5),X(39),XM(39),FU(39),FJU(39),ZZ(6),H,AZ,AH,DT,AL,
4GAM,Y,YY,R,RR,HH,H2,AZHH,R2,AHY,AHRH,AH2,BB,BB2,AAA,BBB,DDT,A1,UV,
5UUU,VVV,RRH,AQ,GAM2,AL2,BUN,RY,AM,AMRR,GAMGAM,ALAL,BAN,KMP1,
6MPP(147,39),MQQ(147,39),IM,JM,KM,IMM1,JMM1,KMM1,IMP1,JMP1,MAT,
7 NK,NNNN,IMH,JMH,MATS,L(39),KA(10,39),KB(10,39),LV(39),NEND,
8LA(10,39),LB(10,39),NN

```

SUBROUTINE TO BE USED WHEN THE OCEAN SHAPE IS CHANGED.

MPP

MPP=1 IF THE FOUR NEAREST SURROUNDING POINTS ARE WATER-POINT,  
=2 ON THE LAND (EXCLUDING THE COAST LINE).  
FOR THE COAST-POINTS, REFER TO FIG.1.

```

14
34XXXXXXXXXXXXXXXXXX33
XXXXXXLANDXXXXXX
XXXXXXXXXXXXXXXXXX
XX?? ?1XX

```

```

1111 1111
XX      XX
XX23    24XX
XXXXXXXXXXXXXXXXXX
31XXXXXXXXXXXXXXXXXX32
12

```

FIG. 1

MQQ

MQQ=1 IF THE FOUR NEAREST SURROUNDING POINTS ARE WATER-POINT,  
 =2 ON THE LAND.  
 IN OTHER CASES, REFER TO FIG.2.

```

1112
XXXXXXXXXXXXXXXXXX
XXXXXXLANDXXXXXX
XXXXXXXXXXXXXXXXXX
XX1221  2211XX
XX      XX
2111XX  XX1121
XX      XX
XX1122  2112XX
XXXXXXXXXXXXXXXXXX
XXXXXXXXXXXXXXXXXX
1211

```

FIG. 2

BAROCLINIC PART ONLY. LV (J), LA (I, J), AND LB (I, J) SHOULD BE READ FROM DATA CARDS. THEN, L (J), KA (I, J), KB (I, J), MQQ (I, J) AND MPP (I, J) ARE DETERMINED IN THIS SUBROUTINE. THE DATA LV, LA AND LB USED HERE ARE IDENTICAL TO THE DATA LV, LA AND LB TO BE USED FOR THE BAROTROPIC PART, BUT IT IS NOT THE CASE WITH L, KA AND KB. L, KA AND KB ARE DIFFERENT FROM EACH OTHER IN BOTH PARTS.

```

IMM1=IM-1
IMP1=IM+1
JMM1=JM-1
JMP1=JM+1
JMH=3
IMH=3
DO 30 J=1, JM
DO 31 I=1, IMP1
MQQ (I, J) = 2
31 CONTINUE
30 CONTINUE
DO 32 J=3, JMM1
READ (5, 33) M
33 FORMAT (I2)
READ (5, 34) (LA (I, J), LB (I, J), I=1, M)
34 FORMAT (7 (2I4, 2X))
DO 35 I=1, M
II=LA (I, J)
IG=LB (I, J)
DO 36 N=II, IG
MQQ (N, J) = 1
36 CONTINUE
35 CONTINUE
LV (J) = M
MQQ (1, J) = MQQ (IMM1, J)
MQQ (2, J) = MQQ (IM, J)
MQQ (IMP1, J) = MQQ (3, J)
32 CONTINUE
DO 1 J=2, JM

```

```

JM1=J-1
DO 2 I=3, IM
IM1=I-1
IF(MQQ(I, J).EQ.1) GO TO 3
IF(MQQ(IM1, J).EQ.1) GO TO 3
  IF(MQQ(IM1, JM1).EQ.1) GO TO 3
IF(MQQ(I, JM1).EQ.1) GO TO 3
MPP(I, J)=2
GO TO 2
3 MPP(I, J)=1
2 CONTINUE
MPP(1, J)=MPP(IMM1, J)
MPP(2, J)=MPP(IM, J)
MPP(IM1, J)=MPP(3, J)
1 CONTINUE
DO 4 J=3, JMM1
MM=LV(J)
WRITE(6, 9) J, LV(J), (LA(I, J), LB(I, J), I=1, MM)
9 FORMAT(1H, 20I5)
4 CONTINUE
DO 11 I=3, IM
WRITE(6, 12) I, (MPP(I, J), J=3, JM)
WRITE(6, 13) (MQQ(I, J), J=3, JM)
12 FORMAT(1H, I3, 2X, 38I3)
13 FORMAT(1H, 6X, 38I3)
11 CONTINUE
DO 18 J=3, JM
MM=0
MP=MPP(3, J)
IF(MP.EQ.2) GO TO 70
II=3
MM=MM+1
70 DO 50 I=4, IMM1
MPPIJ=MPP(I, J)
IF(MPPIJ.EQ.MP) GO TO 60
GO TO (16, 200), MPPIJ
16 II=I
MM=MM+1
GO TO 60
200 KA(MM, J)=II
KB(MM, J)=I-1
60 MP=MPPIJ
50 CONTINUE
IF(MPP(IM, J).EQ.2) GO TO 80
KA(MM, J)=II
KB(MM, J)=IM
80 L(J)=MM
WRITE(6, 9) J, L(J), (KA(I, J), KB(I, J), I=1, MM)
18 CONTINUE
DO 8004 J=JMH, JM
JP1=J+1
JM1=J-1
DO 8005 I=IMH, IM
IF(MPP(I, J).EQ.2) GO TO 8005
IP1=I+1
IM1=I-1
K=0
IF(MQQ(I, J).EQ.2) K=K+1000
IF(MQQ(IM1, J).EQ.2) K=K+100
IF(MQQ(IM1, JM1).EQ.2) K=K+10
IF(MQQ(I, JM1).EQ.2) K=K+1
IF(K.EQ.0) GO TO 8005
IF(K.EQ.11) GO TO 42
IF(K.EQ.1100) GO TO 1100
IF(K.EQ.110) GO TO 110
IF(K.EQ.1001) GO TO 1001

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IF(K.EQ.1110) GO TO 1110
IF(K.EQ.1101) GO TO 1101
IF(K.EQ.111) GO TO 111
IF(K.EQ.1011) GO TO 1011
IF(K.EQ.10) GO TO 40
IF(K.EQ.1) GO TO 41
IF(K.EQ.1000) GO TO 1000
IF(K.EQ.100) GO TO 100
100 MPP(I,J)=32
GO TO 8005
1000 MPP(I,J)=31
GO TO 8005
41 MPP(I,J)=34
GO TO 8005
40 MPP(I,J)=33
GO TO 8005
1011 MPP(I,J)=24
GO TO 8005
111 MPP(I,J)=23
GO TO 8005
1101 MPP(I,J)=21
GO TO 8005
1110 MPP(I,J)=22
GO TO 8005
1001 MPP(I,J)=11
GO TO 8005
110 MPP(I,J)=13
GO TO 8005
1100 MPP(I,J)=12
8005 CONTINUE
8004 CONTINUE
DO 7501 J=2,JMM1
JP1=J+1
JM1=J-1
DO 7500 I=2,IM
IF(MQQ(I,J).EQ.2) GO TO 7500
IP1=I+1
IM1=I-1
K=1111
IF(MQQ(IP1,J).EQ.2) K=1000+K
IF(MQQ(I,JP1).EQ.2) K=K+100
IF(MQQ(IM1,J).EQ.2) K=K+10
IF(MQQ(I,JM1).EQ.2) K=K+1
IF(K.EQ.1111) K=1
MQQ(I,J)=K
7500 CONTINUE
MPP(1,J)=MPP(IMM1,J)
MQQ(1,J)=MQQ(IMM1,J)
MPP(IMP1,J)=MPP(3,J)
MQQ(IMP1,J)=MQQ(3,J)
MPP(2,J)=MPP(IM,J)
MQQ(2,J)=MQQ(IM,J)
7501 CONTINUE
MPP(1,JM)=MPP(IMM1,JM)
MPP(2,JM)=MPP(IM,JM)
MPP(IMP1,JM)=MPP(3,JM)
DO 9000 I=1,IMP1
WRITE(6,12) I,(MPP(I,J),J=3,JM)
WRITE(6,13) (MQQ(I,J),J=3,JM)
9000 CONTINUE
RETURN
END
```

SUBROUTINE GEOST

```

COMMON T(147,39,5),TT(147,39,5),SP(147,39),AT(5),UU(147,39,5),
1VV(147,39,5),U(147,39,5),V(147,39,5),W(147,39,5),UB(147,39),
2VB(147,39),WE(147,39),WN(147,39),Q(39),XJA(38),XHT(38),XHS(38),
3 XMY(38),Z(5),X(39),XM(39),FU(39),FJU(39),ZZ(6),H,AZ,AH,DT,AL,
4GAM,Y,YY,R,RR,HH,H2,AZHH,R2,AHY,AHRR,AH2,BB,BE2,AAA,BBB,DDT,A1,UV,
5UUU,VVV,RRH,AQ,GAM2,AL2,BUN,RY,AM,AMRR,GAMGAM,ALAL,BAN,KMP1,
6MPP(147,39),MQQ(147,39),IM,JM,KM,IMM1,JMM1,KMM1,IMP1,JMP1,MAT,
7 NK,NNNN,IMH,JMH,MATS,L(39),KA(10,39),KB(10,39),LV(39),NEND,
8LA(10,39),LB(10,39),NN

```

HG=H\*490.0

JJ=0

DO 20 J=JMH,JM

LJ=L(J)

DO 4011 M1=1,LJ

II=KA(M1,J)

IG=KB(M1,J)

DO 21 I=II,IG

PZ=0.0

PZ1=0.0

DO 4018 K=1,KMM1

KP1=K+1

PZ=PZ-ZZ(KP1)\*AL2\*(TI(I,J,K)+TT(I,J,KP1))

PZ1=PZ1+PZ\*Z(KP1)

4018 CONTINUE

SP(I,J)=PZ1\*HG

21 CONTINUE

4011 CONTINUE

20 CONTINUE

DO 4019 J=JMH,JM

SP(IMP1,J)=SP(3,J)

4019 CONTINUE

DO 3000 J=JMH,JMM1

FJUJ=FJU(J)

IF(ABS(FJUJ).LE.1.0E-7) GO TO 3

JP1=J+1

RXMJ=R\*XM(J)

R1=RXMJ\*FJUJ

RX=RY\*FJUJ

GO TO 4

3 JJ=J

GO TO 3000

4 LJ=LV(J)

DO 4002 M1=1,LJ

II=LA(M1,J)

IG=LB(M1,J)

DO 3001 I=II,IG

IP1=I+1

SPO=SP(I,J)-SP(IP1,JP1)

SP1=SP(IP1,J)-SP(I,JP1)

PXBIJ=SP1-SPO

PYBIJ=-SP1-SPO

DO 3002 K=1,KM

ZZK=ZZ(K)

KM1=K-1

IF(K.NE.1) GO TO 4000

PA=0.0

PB=0.0

GO TO 4001

4000 CONTINUE

P1=T(I,JP1,K)+T(I,JP1,KM1)-T(IP1,J,K)-T(IP1,J,KM1)

P2=T(I,J,K)+T(I,J,KM1)-T(IP1,JP1,K)-T(IP1,JP1,KM1)

PA=P1\*ZZK\*AL2(P1,P2)

```

PB=PB+ZK*AL*(P2-P1)
4001 CONTINUE
PV=(PA*AQ-PXBIJ)/R1
PU=(-PB*AQ+PYBIJ)/RX
U(I,J,K)=PU
UU(I,J,K)=PU
V(I,J,K)=PV
VV(I,J,K)=PV

```

```

3002 CONTINUE
3001 CONTINUE
4002 CONTINUE
3000 CONTINUE
IF(JJ.EQ.0) GO TO 7
JM1=JJ-1
JP1=JJ+1
DO 5 I=IMH,IM
IF(MQQ(I,JJ).EQ.2) GO TO 5
DO 6 K=1,KM
PA=UU(I,JM1,K)
PB=UU(I,JP1,K)
PU=VV(I,JM1,K)
PV=VV(I,JP1,K)
IF(PA.GT.200.0) PA=0.0
IF(PB.GT.200.0) PB=0.0
IF(PU.GT.200.0) PU=0.0
IF(PV.GT.200.0) PV=0.0
AU=(PA+PB)/2.0
AV=(PU+PV)/2.0
UU(I,JJ,K)=AU
U(I,JJ,K)=AU
VV(I,JJ,K)=AV
V(I,JJ,K)=AV

```

```

6 CONTINUE
5 CONTINUE
7 DO 4007 K=1,KM
DO 4008 J=JMH,JMM1
U(2,J,K)=U(IM,J,K)
V(2,J,K)=V(IM,J,K)
UU(2,J,K)=UU(IM,J,K)
VV(2,J,K)=VV(IM,J,K)
U(IMP1,J,K)=U(3,J,K)
V(IMP1,J,K)=V(3,J,K)
UU(IMP1,J,K)=UU(3,J,K)
VV(IMP1,J,K)=VV(3,J,K)

```

```

4008 CONTINUE
4007 CONTINUE
CALL CONTI
DO 7002 K=2,KM
WRITE(6,7001) K
7001 FORMAT(1H ,23HVERTICAL VELOCITY AT K=I1)
DO 7003 I=IMH,IM
WRITE(6,7000) I,(W(I,J,K),J=3,20)
7000 FORMAT(1H ,I3,1X,18F7.2)
7003 CONTINUE
DO 7024 I=IMH,IM
WRITE(6,7000) I,(W(I,J,K),J=21,38)
7024 CONTINUE
02 CONTINUE
DO 7009 K=1,KM
WRITE(6,7010) K
7010 FORMAT(1H ,7HU AT K=I1)
DO 7011 I=IMH,IM
WRITE(6,7012) I,(UU(I,J,K),J=3,20)
7012 FORMAT(1H ,I3,2X,18F5.0)
7011 CONTINUE
DO 7022 I=IMH,IM

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WRITE(6,7012) I, (UU(I,J,K), J=21,38)
7022 CONTINUE
DO 7021 I=IMH,IM
WRITE(6,7012) I, (VV(I,J,K), J=3,20)
7021 CONTINUE
DO 7023 I=IMH,IM
WRITE(6,7012) I, (VV(I,J,K), J=21,38)
7023 CONTINUE
7009 CONTINUE
RETURN
END
```