

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION



SPACE SHUTTLE

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DATA MANagement services

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SPACE DIVISION

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RESULTS OF HEAT TRANSFER TESTS

OF AN 0.0175-SCALE SPACE SHUTTLE

VEHICLE MODEL 22 OTS IN THE NASA-AMES

3.5-FOOT HYPERSONIC WIND TUNNEL (IH3)

VOLUME II

By

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Prepared under NASA Contract Number NAS9-13247

By

Data Management Services Chrysler Corporation Space Division New Orleans, La. 70189

for

Engineering Analysis Division

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Johnson Space Center National Aeronautics and Space Administration Houston, Texas

WIND TUNNEL TEST SPECIFICS:

Test Number:	ARC 3.5-178
NASA Series Number:	IH3
Model Number:	22 OTS
Test Dates:	October 31 to November 9, 1973

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Concurrence:

RESULTS OF HEAT TRANSFER TESTS OF AN 0.0175-SCALE SPACE SHUTTLE VEHICLE MODEL 22 OTS IN THE NASA-AMES 3.5-FOOT HYPERSONIC WIND TUNNEL (IH3)

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ABSTRACT

Heat-transfer data for the 0.0175-scale Space Shuttle Vehicle 3 are presented in this data report. Interference heating effects were investigated by a model build-up technique of Orbiter alone, tank alone, second, and first stage configurations.

The test program was conducted in the NASA-Ames 3.5-Foot Hypersonic Wind Tunnel at Mach 5.3 for nominal free-stream Reynolds number per foot values of 1.5 x 10^6 and 5.0 x 10^6 .

This report is presented in four volumes. The contents of the volumes are as follows:

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INTRODUCTION

The experimental investigation documented in this report was performed to obtain aerodynamic heat-transfer rate data on the space shuttle vehicle 3 first and second stage configurations. A component build-up of orbiter alone, tank alone, orbiter plus tank, and fully mated launch configuration was utilized to investigate component interference effects.

The test program was conducted in the NASA-Ames 3.5-Foot Hypersonic Wind Tunnel at Mach 5.3 and nominal free-stream Reynolds number per foot values of 1.5×10^6 and 5.0×10^6 . The model angles of attack were 0°, -3° , -5° and 20° (SRB alone) and angles of yaw were 0° and -5° .

NOMENCLATURE

Symbol	Plot Symbol	Definition
b		thickness of model skin
В		span length
C		specific heat of model skin material or OMS crease
с		chord length
c _o , c _l , c ₂		constants in curve fit for C over model wall temperature range
с _р		specific heat of air stream (perfect gas value)
CHAN	CHAN	recording-system channel
Haw	HAW	adiabatic wall enthalpy
Ht	нт	free-stream total enthalpy
	НО	average of free-stream total enthalpy values of all tunnel runs incorporated into an aero dataset
Hw	HW	enthalpy based on model wall temperature for given T/C location
h	Н	heat-transfer coefficient at model wall for given T/C location
href	HREF	stagnation-point heat-transfer coefficient for reference sphere
h/href	H/HREF	ratio of model heat-transfer coefficient to heat-transfer coefficient of reference sphere for H _{aw} /H _t = X.XXX
	HI/HU	interference to undisturbed heat transfer coefficient ratio
IML		inner module line
L	Length	model reference length

NOMENCLATURE (Continued)

Symbol	Plot Symbol	Definition
M _{co} ,	MACH	free-stream Mach number
, ^P t	PT	free-stream total pressure
	PO .	average of free-stream total pressure values of all tunnel runs incorporated into an aero dataset
ġ	Q	heat-transfer rate at model wall for given T/C location
q _s	QS	stagnation-point heat-transfer rate for reference sphere at initial time
R _s	RS	reference sphere radius at model scale equivalent to 0.305 m (1 ft) for full-scale vehicle
Re_{∞}/ft		free-stream Reynolds number per foot
	RN/L	average of free-stream Reynolds number values (per foot) of all tunnel runs incorporated into an aero dataset
Re _∞ ,L		free-stream Reynolds number based on model reference length, L
	S	assumed chordwise location (for Clusters Band C) - see Figure 2
St	ST	Stanton number based on free-stream flow conditions and the model heat-transfer coefficient for H _{aw} /H _t = X.XXX
T		temperature
Tt	TT	free-stream total temperature
	то	average of free-stream total temperature values of all tunnel runs incorporated into an aero dataset



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NOMENCLATURE (Continued)

Symbol	Symbol	Definition
Tw	τw	model wall temperature for given T/C location
т/с	T/C	thermocouple
t		time
ti	TIME	initial time (before model insertion into flow) extrapolated from f(T _W) vs time
u,V		velocity
W		density of model skin material
x		axial distance measured from nose
	X/C	chordwise location, fraction of local chord
	X/L	longitudinal location, fraction of body length
Y		spanwise distance from centerline
	2Y/B	spanwise location, fraction of semi-span
Z		water plane distance
	Z/BV	spanwise location on vertical tail, fraction of exposed span
Θ		tank radial position measured clockwise looking forward, O degrees at bottom centerline
α	ALPHA	angle of attack, degrees
β	BETA	angle of sideslip, degrees
μ		viscosity of air
ρ		density of air
ф		Orbiter radial position measured clockwise looking forward. O degrees at bottom centerline

NOMENCLATURE (Concluded)

Sumbol	Plot	
Symbol	Symbol	Definition
ψ		SRB radial position measured clockwise looking forward. O degrees at bottom centerline
SUBSCRIPTS	<u>5</u>	
aw		adiabatic wall
i		initial value before model insertion into tunnel flow
0		Orbiter
PG		perfect gas (calorically and thermally perfect gas)
S		reference sphere
S		SRB
t		free-stream total condition
т		tank
V		vertical tail
w		wall
ω		free-stream

REMARKS

Tunnel blockage was suspected during the first stage (mated) $\alpha = -5^{\circ}$ runs, but could not be confirmed due to inconclusive shadowgraph data. Therefore, additional data were taken at $\alpha = -3^{\circ}$. Both $\alpha = -3^{\circ}$ and -5° data are presented in this report; however, the $\alpha = -5^{\circ}$ data are question-able.

Near the end of the test program the number of test runs used to obtain a complete mapping of the mated-vehicle heating rates was reduced from seven to five to conserve test time. The data acquisition capacity is 75 thermocouple channels per run. This reduced the number of recorded thermocouples from 525 to 375 for these runs (runs with T/C hook-up numbers 12 and 13).

A post-test analysis and dimensional check of the model were performed on the orbiter to investigate suspected incorrect data from wing leading edge clusters B and C. As a result of this investigation, the thermocouple locations and skin thicknesses presented in Table IV and figure 2a were found to be incorrect for clusters B and C. Figure 2b presents the correct locations and thicknesses. The data presented in the plots and tabulated listings reflect the pretest locations and skin thicknesses and should be scaled accordingly. Data reports for other tests of this model are also in error due to the clusters on the wing leading edge. These test data should be corrected for the test data publications of tests OH4B, IH2O, and OH6.

CONFIGURATIONS INVESTIGATED

The 22-OTS model is a 0.0175-scale replica of the vehicle three configuration Rockwell International Space Shuttle orbiter, tank, and solid rocket boosters. The model is a thin-skin thermocouple model instrumented with 527 30-gauge iron-constantan thermocouples. The structural areas of the model were constructed of 15-5PH stainless steel with instrumented areas of 15-5PH and 17-7PH stainless steel.

Provisions have been made to test elevon deflections of -40°, 0°, +5, and +10°; body flap deflections of 0° and +10°; and rudder flare of 0° and 40°. For this ascent test, all control surfaces were tested at 0° deflection.

The configurations tested are described below with the component definitions given in table III.

Symbol

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ORB	$B_{17} C_7 M_4 F_5 W_{103} E_{22} V_7 R_5$	Orbiter
ET	T ₁₀	external tank
SRB	s ₈	solid rocket booster
0TS	$B_{17} C_7 M_4 F_5 W_{103} E_{22} V_7 R_5 T_{10} S_8$	mated vehicle
TRIPS		.050" steel spheres spot welded to .005" shim stock band 1/4 inch wide. Center- line displacement between

trips was 3 diameters

TEST FACILITY DESCRIPTION

The NASA-Ames 3.5-Foot Hypersonic Wind Tunnel is a closed-circuit, blowdown-type tunnel capable of operating at nominal Mach numbers of 5, 7, and 10 at pressures to 1800 psia and temperatures to 3400°R for run times to four minutes. The major components of the facility include a gas storage system where the test gas is stored at 3000 psi, a storage heater filled with aluminum-oxide pebbles capable of heating the test gas to 3400°R, axisymmetric contoured nozzles with exit diameters of 42 inches for generating the desired Mach number, and a 900,000 ft³ vacuum storage system which operates to pressures of 0.3 psia. The test section itself is an open-jet type enclosed within a chamber approximately 12-feet in diameter and 40-feet in length, arranged transversally to the flow direction.

A model support system is provided that can pitch models through an angle-of-attack range of -20 to +20 degrees, in a vertical plane, about a fixed point of rotation on the tunnel centerline. This rotation point is adjustable from 1 to 5 feet from the nozzle exit plane. The model normally is out of the test stream (strut centerline 37-inches from tunnel centerline) until the tunnel test conditions are established after which it is inserted. Insertion time is adjustable to as little as 1/2 second and models may be inserted at any strut angle.

A high-speed, analog-to-digital data acquistion system is used to record test data on magnetic tape. The present system is equipped to measure and record the outputs from 80 transducers in addition to 20 channels of tunnel parameters.

TEST PROCEDURES

The data acquisition capability was 75 recorded thermocouples per run. Since there were 525 T/C's selected for mated launch-configuration testing, seven runs were necessary for a complete mated heating distribution. Cannon plugs with 15 thermocouples for full data acquisition capability were used at the model. A five plug junction (connector) box was constructed to mate the model plugs to the facility's 150°F reference box terminal posts. Most model changes were, therefore, simple plug changes between runs.

Due to the complexity of the mated configuration sting arrangement, oil-flow visualization techniques were employed to confirm that there were no sting-interference effects.

Shadowgraphs were taken for each run. Sting-effect shadowgraphs were also obtained for selected runs.

DATA REDUCTION

All test data were reduced at the NASA/Ames Research Center using the data reduction techniques outlined below. The thermocouple data were reduced using the one-dimensional, thin-wall equation:

$$\dot{q} = WCb \frac{dT_W}{dt} = h (H_{aw} - H_w) \equiv hH_t \left(\frac{H_{aw}}{H_t} - \frac{H_w}{H_t}\right)$$
 (1)

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which neglects heat-conduction losses.

Assuming that W and h are constant and

 $C = C_0 + C_1 T_W + C_2 T_W^2 \text{ for } T_W \text{ ranges}$ (2)

the integration of equation (1) for $t = t_i$ to t and $T_w = T_{w_i}$ to T_w yields the linear equation:

$$f(T_w) = - \ln \left(\frac{T_{aw}' - T_w}{T_{aw}' - T_{w_i}} \right) - \left[\frac{C_1}{C'aw} + \frac{C_2}{C'aw} \left(T_{aw}' + \frac{T_w + T_{w_i}}{2} \right) \right]$$
$$(T_w - T_{w_i}) = \frac{hc_p}{WC'aw} (t - t_i)$$
(3)

where it is defined that:

$$T'_{aw} \equiv \frac{H_{aw}}{c_p} = \frac{H_{aw}}{H_t} \quad \frac{H_t}{c_p} \ge (T_{aw})_{PG}$$
(4)

 $C'_{aw} \equiv C_0 + C_1 T'_{aw} + C_2 T'_{aw} 2$ (5)

\$ specific heat at adiabatic wall temperature

The form of Eq (3) is $f(T_W) = mt + b$ where m is the slope and b is the intercept for a straight line if heat-conduction errors are negligible. Thus, deviations from a straight line can indicate heat-conduction effects.

DATA REDUCTION (Continued)

The slope, m, of $f(T_w)$ vs t from Eq (3) is computed by a leastsquares, straight-line fit over a finite time interval (approx. 1 sec.) beginning when the model reaches uniform tunnel flow. The value of the heat-transfer coefficient, h, is then determined from:

$$h = \frac{WC_{awb}}{c_{p}} m$$
 (6)

Using this value of h, the heat-transfer rate is evaluated at the initial time, t_i, when the model is isothermal at the initial wall enthalpy, H_{w_i}

$$\dot{q} = \dot{q}_{i} = h (H_{aw} - H_{w_{i}}) \equiv hH_{t} \left(\frac{H_{aw}}{H_{t}} - \frac{H_{wi}}{H_{t}}\right)$$
 (7)

where H_{aw}/H_t is the same value used to evaluate h. The resultant value of \dot{q} is independent of the value of H_{aw}/H_t used for both the h and \dot{q} evaluations.

The reference sphere heating is also evaluated at the initial wall enthalpy by the method of Fay and Riddell (ref. 2):

$$\dot{q}_{s} = h_{ref} \left(H_{t} - H_{w_{i}}\right) \equiv h_{s} H_{t} \left(1.0 - \frac{H_{w_{i}}}{H_{t}}\right)$$
(8)

The model-to-sphere ratio of heat-transfer coefficients is then determined from Eqs. (7) and (8) as

$$\frac{h}{h_{ref}} = \frac{\dot{q}_i}{\dot{q}_s} \left[\frac{1.0 - {}^{H_W} i^{/H} t}{H_{aw}/H_t - H_W i^{/H} t} \right]$$
(9)

DATA REDUCTION (Concluded)

where \dot{q}_i is constant for all values of $H_{aw}/H_t.$

To determine h/h_{ref} for various values of H_{aw}/H_t , the particular value of H_{aw}/H_t is substituted into Eq. (9).

The Stanton number is defined as

$$St = \frac{h}{\rho u} = \frac{\dot{q_i}}{\rho u(H_{aw} - H_{w_i})}$$
(10)

where for free-stream conditions, $\rho u = \rho_{\infty} V_{\infty}$.

The calculations of the model heating, reference sphere heating, and Reynolds number included the corrections of NACA report 1135 (ref. 3) for calorically imperfect thermally perfect air. Keyes' equation for viscosity (see ref. 4) was also used for the sphere heating and Reynolds number computations:

$$\mu = \frac{0.0232 \times 10^{-6} T^{0.5}}{1 + \frac{220}{T} \times 10^{-9/T}}$$
(11)

where the units for T and μ are °R and 1b-sec/ft, respectively.

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TABLE I.

EST : IH3 (ARC 3.	5 #178) NO	MINAL	DATE: 11/9/73
	TEST O	ONDITIONS	
MACH NUMBER	REYNOLDSNUMBER (perft)	TOTAL PRESSURE (pounds/sq. inch)	STAGNATION TEMPERATU (degrees Rankine)
5.2	$1 = 10^{6}$	100	1.000
5.3	$\frac{1.5 \times 10}{5.0 \times 10^6}$	120	1300
	3.U_X_10	405	1300
			,
	<u> </u>		
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BALANCE UTILIZED: _	No	ne	
	CAPACITY:	ACCURACY:	
NE			OLEMANCE.
SF			<u></u>
AF			
Рм			
RM			
YM			····
COMMENTS: Thermoc	ouple Test		
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TABLE II.

	F				_		_	т	EST	RUN	NU	мве	RS					·			T	92			٦
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TABLE III. - COMPONENT DIMENSIONAL DATA

MODEL COMPONENT: BODY - B17

GENERAL DESCRIPTION: Fuselage, 3 configuration, lightweight orbiter per

Rockwell lines drawing No. VL70-000139

MODEL SCALE: 0.0175

DRAWING NO.: VL70-000139

DIMENSIONS:

MENSIONS:	FULL SCALE	MODEL SCALE
Length - In.	1290.3	22.58025
Max. width - In.	267.6	4.6830
Max.depth - In.	244.5	4.27875
Fineness Ratio	4.82175	4.82175
Area - ft ²		
Max. Cross-sectional	386.67	0.11842
Planform		
Wetted		
Base		

TABLE III. - COMPONENT DIMENSIONAL DATA - Continued. MODEL COMPONENT: <u>CANOPY - C7</u> GENERAL DESCRIPTION: <u>Configuration 3 per Rockwell Lines VL70-000139</u>

Insufficient information to complete dimensional data at this time.

MODEL COMPONENT: ELEVON- E22

GENERAL DESCRIPTION: 3 configuration per W103 Rockwell Lines Drawing

VL70-000139 data for (1) of (2) sides.

SCALE MODEL: 0.0175

DRAWING NUMBER: VL70-000139

DIMENSIONS:

TENSICIS:	FULL SCALE	MODEL SCALE
Area - ft ²	205.52	0.06294
Span (equivalent) - In.	353.34	6.18345
Inb'd equivalent chord	114.78	2.00865
Outb'd equivalent chord	55.00	0.96250
Ratio movable surface chord/ total surface chord		
At inb'd equiv. chord	.208	.208
At outb'd equiv. chord	.400	.400
Sweep-back angles, degrees		
Leading edge	0.00	0.00
Trailing edge	- 10.24	- 10.24
Hingeline	0.00	0.00
Area Moment (Normal to hingeline) - ft ³ (Product of Area Moment)	1548.07	0.00829

MODEL COMPONENT: BODY FLAP - F5

MODEL SCALE: 0.0175

GENERAL DESCRIPTION: <u>3 Configuration per Rockwell Lines VL70-000139</u>

DRAWING NUMBER: VL70-000139 DIMENSIONS: TULL SCALE MODEL SCALE Length - In. 84.70 1.48225 267.6 4.6830 Max. width - In. Max. Depth Fineness Ratio Area - ft^2 Max Cross-sectional Planform **142.5195** 0.04365 Wetted Base <u>38.0958</u> 0.01167

FULL SCALE MODEL SCALE

MODEL COMPONENT: OMS POD - M4

GENERAL DESCRIPTION: Orbital maneuvering system pods located on the orbiter

aft fuselage.

MODEL SCALE: 0.0175

DRAWING NUMBER: VL70-000139

DIMENSIONS:

Length - In.		6.0550
Max. Width - In.	108.0	1.890
Max. Depth - In.	113.0	
Fineness Ratio		
Area - ft ²		
Max cross sectional		
Planform		
Wetted	••••	
Base		
C of OMS Pod		
WP = 463.9 In. FS; WP 400 + 63.9 = 463.9		
BP = 80.0 In. FS		
LENGTH: 1214.0 to 1560.0 = 346.0 In. FS		

NOTE: M₄ is identical to M₃ of 2A configuration, except intersection to body.

a construction of the second s

MODEL COMPONENT: RUDDER - R5

GENERAL DESCRIPTION: 2A, 3 and 3A configuration per Rockwell Lines Drawing

VL70-000095

MODEL SCALE: 0.0175

DRAWING NUMBER: VL70-000139, VL70-000095

DIMENSIONS:	FULL SCALE	MODEL SCALE
Area - ft ²	106.38	0.03258
Span (equivalent) - in.	201.0	3.5175
Inb'd equivalent chord	91.585	1.60274
Outb'd equivalent chord	50.833	0.88958
Ratio movable surface chord/ total surface chord		
At inb'd equiv. chord	0.400	0.400
At outb'd equiv. chord	0.400	0.400
Sweep-back angles, degrees		
Leading edge		
Trailing edge	26.25	_26.25
Hingeline	34.83	
Area Moment (normal to hingeline) - ft ³ Product of area and mean chord	526.13	0.00282

MODEL COMPONENT: BOOSTER SOLID ROCKET MOTOR - S8		
GENERAL DESCRIPTION: Booster solid rocket, 3 configur	ation, body	of
revolution, data for (1) of (2) sides per Rockwell Lin	es drawing	
VL77-000036 and VL72-000088		
MODEL SCALE: 0.0175		
DRAWING NUMBER: VL72-000088, VL77-000036		
DIMENSIONS:	FULL SCALE	MODEL SCALE
Length (Includes nozzle) - In.	1741.0	30.468
Max. Width (Tank dia.) - In.	142.0	2.485
Max. Depth (Aft shroud) - In.	205.0	3.588
Fineness Ratio	8.49268	8.49268
Area - ft ²		
Max. Cross-sectional	229.21	4.011
Planform		
Wetted		
Base		
WP of BSRM Centerline (Z_{T}) - In.	400.0	7.00
FS of BSRM Nose (X_T) - In.	200.0	3.50
TABLE III. - COMPONENT DIMENSIONAL DATA - Continued. MODEL COMPONENT: EXTERNAL TANK - TLO GENERAL DESCRIPTION: External Oxygen-hydrogen tank, 3 configuration, per Rockwell Lines drawing VL78-000041 and VL72-000088

MODEL SCALE: 0.0175

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DRAWING NUMBER: VL72-000088, VL78-000041

DIMENSIONS:	FULL SCALE	MODEL SCALE
Length - In. (Nose @ $X_{T} = 309$)		32.63750
Max. width (Dia) - In.	324	5.670
Max. depth		
Fineness Ratio	5.75617	5.75617
Area - ft ²	•	
Max. Cross-Sectional	<u> </u>	0.17534
Planform		
Wetted		
Base		
WP of Tank Centerline (X_m) In.	400.0	7.00

TABLE III. - COMPONENT DIMENSIONAL DATA - Continued.

MODEL COMPONENT: VERTICAL, V7 (Lightweight Or	biter Configuration))
GENERAL DESCRIPTION: Centerline vertical tail	, double-wedge airfo	oil with
rounded leading edge.		
NOTR: Same as V but with months into it		
and as vy but with manipulator housing	removed.	
MODEL SCALE: 0.0175		
DRAWING NUMBER: VL70-000139, VL70-000095		
DIMENSIONS:		
TOTAL DATA	FOLL SCALE	MODEL SCALE
Area (Theo) - r^{+2}	•	
Planform	425.92	0.13044
Span (Theo) - Th		
Aspect ratio		5.52510
Rate of taper		1.675
Taper ratio		0.507
Sweep-back angles, degrees	0.404	0.404
Leading edge		• _
Trailing edge	45.000	45.000
0.25 Element line		26.249
	41.130	41.130
Chords:		
Root (Theo) WP	268 50	1. (- 0
Tip (Theo) WP	200.50	4.69875
MAC	100.47	1.89822
Fus. Sta. of .25 MAC	1462 50	
W.P. of .25 MAC	635 522	- 22.01125
B.L. of .25 MAC	0.00	0.00
Airfoil section:		
Leading wedge anble - deg.	10.000	10,000
Trailing wedge angle - deg.	14.920	14.920
Leading edge radius	2.0	0.0350
W		
vold area - Fr-	13.17	0.00403
Elanketed area	0.00	0.00

JDEL COMPONENT: WING-W 105		
ENERAL DESCRIPTION: Configuration 3 Orbiter per	Lines VL70-0001	39.
NOTE: Same planform as W87, except dihedral at	TE	
	- ·	
Second Contraction Contracti		
FST NO.	DWG. NOVI	70-000139
DIMENSIONS:	FULL-SCALE	MODEL SCALE
Area (Theo.) Ft^2	2600.00	0 82281
Planform	026.60	16.39190
Span (lheo lh.	2,265	2.265
Rate of Taper	1.177	1.177
Taper Ratio	0.200	0.200
Dihedral Angle, degrees (@ TE of Elevon)	3.500	3.000
Incidence Angle, degrees	+3,000	+3.000
Sween Back Angles, degrees		
Leading Edge	45.000	45.000
Trailing Edge	<u>-10.24</u>	-10.24
0.25 Element Line	35.209	<u></u>
Chords: Reat (Theo) B P O O	689.24	12.06170
Tip. (Theo) $B_{-}P_{-}$	137.85	2.41238
MAC	474.81	<u>8.30918</u>
Fus. Sta. of .25 MAC	<u>_1136.89</u>	<u>19.09520</u> 5.2360
W.P. of .25 MAC	182.13	3,18728
B.L. OT .23 MAG		
EXPOSED DATA	1752.29	0.53664
Span. (Theo) In. BP108	720.68	12.61190
Aspect Ratio	2.058	2.058
Taper Ratio	0.2451	0.2421
Chords	562.40	9.8420
Tin 1.00 b	137.85	2.41238
	393 03	6 87802
MAC Even Sta of 25 MAC	1185.31	20.74292
W_P_{a} of 25 MAC	300.20	5.25350
B.L. of .25 MAC	251.76	2.51580
Airfoil Section (Rockwell Mod NASA)		
XXXX-64	0.10	0.10
ROOT D =		0.12
Tip <u>b</u> =	0.12	U.12
2	_	
Data for (1) of (2) Sides		
Leading Lage Lutt 2 Planform Area Ft2	120.33	0.03685
Leading Edge Intersects Fus M. L. 0 Sta	560.0	9.800
Leading Edge Intersects Wing @ Sta	1035.0	18.11250

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		FULL	SCALE		MODEL	SCALE				
T/C	X	x _o	У	2	x NOSE	y	z	ø	SKIN	REMARKS
	1								NESS	
1	0	238.00	0		0	0		0	.034	BOTTOM Q
2	.005	244.45	· ·		.113			4	.035	
3	.010	250. 90			.226				.035	
4	.020	263.81			.452				.032	
5	.030	276.71			.677				.033	
6	.040	289.61	·		.903				.034	· · · · · · · · · · · · · · · · · · ·
7	.050	302.52			1.129				.033	
8	.060	315.42			1.355				.032	
9	.070	328.32			1.581				.034	
10	•080	341.22			1.806				.035	
11	•090	354.13			2.032				.035	۲.
12	.100	367.03			2.258				.034	BOTTOM Q
13										OPEN
14	.120	392.84			2.710				.035	BOTTOM 6
15	.130	405.74			2.935				.035	Å
16	.140	418.64			3.161		-		.035	
17	.150	431.54			3.387				.034	
18	.160	444.45			3.613				.035	
19	.170	457.35			3.839				.035	
20	.180	470.25			4.064				.035	
21	.190	483.16			4.290				.035	
22	.200	496.06			4.516				.031	
23	.225	528.32			5.081				.031	
24	.250	560.58			5.645				.033	
25	.275	592.83			6.210				.033	
26	.300	625.09			6.774				.032	
27	.325	657.35			7.339				.033	
28	.350	689.60			7.903				.020	
29	.375	721.86			8.468				.028	
30	.400	754.12			9.032				.033	
31	.425	786.38	Ť	¥	9.597	¥	*	Y	.035	▼
32	•450	818.64	0		10.161	0		0	.034	BOTTOM Q

Table IV.Orbiter T/C LocationsModel 22- OTS

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Table IV (Cont'd) Orbiter

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1		FULL	SCALE		MODEI	SCALE	1	1	1		l
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NO.		_					Ì		THICK		}
33	.475	850.89	0		10.726	0			020	BOTTOM R	4
34	.500	883.15			11.290			Ť	.030	Lorion 4	-
35	.525	915.41		1	11.855	<u>†</u> †		╁╂─	.030	1	1
36	.550	947.66		+-+	12.419	╉┈╄╾	+	++-	.052	 	┨
37	.575	979.92		+ +	12.984	╏┼	┼╌┼─	╂┼╌	079		1
38	.600	1012.18			13.548	╂╌┼──	┼╌┼─	++-	021		1
39	.625	1044.44		+	14.113	╉╾┾╼	┢╶┥╾	╁┾╴	020	<u> </u>	1
40	.650	1076.70		++	14.677		┼╌┼╌	++-	020		1
41	.675	1108.95		+-+	15.242	╋╍┾╍	┼╌┼╌	╂╂╍	1095		1
42	.700	1141.21		+	15.806	++-	┼╌┼─	\square	035		-
43	.725	1173.47			16.371	+-+	++-	++	.05F		1
44	.750	1205.72		+	16.935	┼╌┼──	++-	╂┠──	.035		{
45	.775	1237.98			17.500	++-	+ + -	+	.055		{
46	.800	1270.24		+	18.064	╂╼┾╾╴	┼╌╀╌		1050		1
47	.825	1302.50		<u> </u>	18.624	┨╼╁╌╴	┼╌┼─	╏╎	035		ł
48	.850	1334.76			19.193	+-+-	 ,		033		ł
49	.875	1367.01			19.758	+	┼-┼		033		1
50	•900	1399.27		<u>+ +</u>	20.322	╂╼╂╼	┼╌┼╌	$\left\{ \right\}$	0211		1
51	.925	1431.53		1 1	20.887	╂╾╂╌╴	<u> </u>	<u> </u>	035		1
52	•950	1463.78		1-1	21.451	<u> </u>			AZ7	¥ ·····	1
53	.975	1496.04		1 1	22.016		+	<u> </u>	032	BOTTOM Q	1
54	1.000	1528.3			22.580		1		029	x=1.008@\$ =10%	.033
55	1.013	1541.56			22.812	<u>+</u>	<u>}</u>	┠╋╌┥	032	10 ONLY	
56	1.025	1560.56			23.145			$\left[\begin{array}{c} \\ \end{array} \right]$.032		1
57	1.038	1574.30			23.385				032	8 DE 10 ONLY	1
58	1.050	1592.82			23.709	<u> </u>	╏──┼──	0	.030	Br	037
59	.010	250.90			.226	<u>}</u> }	<u> </u>	180	.035	TOP C	in a
60	.025	270.26			.565	<u>+</u>	<u>├</u> ──- <u>├</u> ──		250		
61	.050	302.52		<u> </u>	1.129		<u> </u>		,033 025	<u>_</u>	
62	.075	334.77			1.694		<u>├</u>	╏╌┼╌┥	555	·····	
63	.160	367.03	¥.	V	2.258	V	¥-		037		
64	.125	399.29	0		2.823	0		180	031	TOP Q	

Table IV (Cont'd) Orbiter

		FULL	SCALE		MODE	L SCALF	6			
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65	.150	431.54	1 0		3.387			1200	14255	mon a
66	.160	444.49	5	4	3.613				026	
67	.170	457.35	5		3.839				031	
68	.180	470.25	5		4.064		┽╌┠╌	╂╂─	031	
69	.200	496.06	5		4.516		┿╋	╉┼─┐	033	
70	.250	560.58			5.645	+-+-	╶┼──┼──	╏┼╴┤	030	
71	.300	625.09		T	6.774	-11-	+	╆┿╾┧	<u> </u>	
72	.400	754.12			9.032		┼╌┼╌	$\uparrow \uparrow \uparrow$	030	
73	•500	883.15			11.290		+-+-	$\uparrow \uparrow \uparrow$	030	· · · · · · · · · · · · · · · · · · ·
74	.600	1012.18			13.548	+ +-	╪╌╂╾╴		03/	
75	.700	1141.21	•	Y	15.806		+-+	╎╷╎	032	
76	.800	1270.24	0		18.064	0		180	. 030	TOP @
77	ļ		29.60	478.00	WINDOW #1	0.518	8.365		035	TOP LEFT
78	ļ. <u>.</u>		12.80	478.00	WINDOW #1	0.224	8.365		.035	TOP RIGHT
79			21.20	464.97	Å	0.371	8.137		.033	CENTER
80	ļ	ļ	34.40	452.00	+	0.602	7.910		.035	BOTTOM LEFT
81			6.00	452.00	WINDOW #1	0.105	7.910		.034	BOTTOM RIGHT
82	ļ		43.20	478.00	WINDOW #2	0.756	8.365		.035	TOP LEFT
83	 	 	34.80	478.00	WINDOW #2	0.609	8.365	-	035	TOP RIGHT
84	 		44.80	464.97		0.784	8.137		035	CENTER
85			59.20	452.00	Y	1.036	7.910	Y.	035	BOTTOM LEFT
86			40.40	452.00	WINDOW #2	0.707	7.910	,	035	BOTTOM RIGHT
87			62.40	464.97	WINDOW #3	1.092	8.137	140	032	CENTER
88	.100	367.03	20.00		2.258	0.350		10	035	FUSELACE BOTTOM
89	.150	431.54	24.00		3.387	0.420		10	035	
90	•050	302.52	25.00	-	1.129	0.438		14/-	<u>333</u>	
91	.200	496.06	25.00		4.516	0.438		1.5,	031	
92	• 300	625,09	25.00		6.774	0.438		12.	033	
93	.200	496.06	50.00		4.516	0.875		24 .	034	
94	. 300	754 10	50.00		6.774	0.875		23	036	
95 06	.400	/54.12	50.00		9.032	0.875	T	er and	026	*
70	. 500	003.15	50.00		11.290	0.875	·· 2	1.5	076 FI	USELACE BOTTOM

	T	FUI	L SCALE			MODEL SO	CALE		SKIN	
T/C NO.	X L	×o	У	z	x FROM NOSE	У	Z	ø	THICK- NESS	REMARKS
97	.600	1012.18	50.00		13.548	0.875		21.5	.021	FUSELAGE SIDE
98	.700	1141.21	50.00		15.806	0.875			.033	
99	.800	1270.24	50.00		18.064	0.875		1	.033	
100	.900	1399.27	50.00		20.322	0.875		21.5	.034	FUSELAGE SIDE
101	1.000	1528.30	100.00		22.580	1.75		39	.03/	BODY FLAP 0 = .03
102	1.050	1592.82	100.00		23.704	1.75		39	.028	BODY FLAP
103	.100	367.03	39.20		2.258	0.686		20	.033	FUSELAGE SIDE
104	.150	431.54	40.80		3.387	0.714		20	.03/	A
105	.050	302.52		303.60	1.129		5.313	22	.031	C.C.L. TANGENT
106	.100	367.03	52.00		2.258	0.910		24.5	,03.3	
107	.150	431.54	62.00		3.387	1.085		25.5	.031	†
108	.200	496.06	65.60	287.20	4.516	1.148	5.026	31.5	.035	C.C.L. TANGENT
109	.300	625.09	74.46		6.774	1.303		34	.033	
110	.200	496.06	75.60	292.00	4.516	1.323	5.110	35	.030	``````````````````````````````````````
111	.150	431.54	79.20	304.80	3.387	1.386	5.334	40	.030	
112	.200	496.06	85.20	298.80	4.516	1.491	5.229	40	.034	
113	.300	625.09	91.43		6.774	1.600		40 ′	.026	
114	.300	625.09	102.86		6.774	1.800		45	.023	
115	.050	302.52		325.60	1.129		5.698	35	.030	M.H.B. TANGENT
116	.100	367.03		317.60	2.258		5.558	39	.030	M.H.B. TANGENT
117	.150	431.54	83.60	314.4	3.387	1.463	5.502	45.	.030	M.H.B. TANGENT
118	.200	496.06		320.00	4.516		5.600	51	.030	
119	.300	625.09		330.00	6.774		5.775	57.	5.02/	
120	.300	625.09		340.00	6.774		5.950	61	.027	•
121	.076	336.51		350.00	1.724		6.125	5	.030	RCS CENTER
122	.300	625.09		350.00	6.774		6.125	5 65	.026	
123	.800	1270.24		350.00	18.064		6.12	5 65	,017	
124	.900	1399.27		350.00	20.322		6.12	5 65	.033	3
125	.975	1496.04		350.00	22.016		6.12	5 68	.034	<u> </u>
126	.975	1496.04	I	300.00	22.016		5.25	52.	5.032	
127	.050	302.52	· · · · · · · · · · · · · · · · · · ·	342.40	1.129	T	5.99	2?	5.030	TANGENT (UPPER)

Table IV (Cont'd) Orbiter

			FULL	SCALE	<u>+</u>	MODEL	SCALE				
	NO.	Ê	×o	7	2	x NOSE	У	2].	SKIN	REMARKS
		+					ļ			NESS	ĸ
	128	.200	496.06		360.00	4.516		6 30	K7	5 0 7/	FIRELOR
	129		625.09		360.00	6.774		6.30	$\frac{1}{2}$	1020	RUSELAGE SIDE
	130	.600	1012.18	-	375.14	13.548		6 56	5 77	000-	
	<u> </u>	.05	0 302.52		376.40	1.129		6.50		.05/	
	132	1.10	0 367.03		410.00	2.258		7 17		0.000	45 TANGENT
	133	.200	496.06		410.00	4.516		7 1 9 6		5 57	
	134	.300	625.09		430.00	6.774		1.4/3	170.	1.028	
	135	.400	754.12		430.00	9,032		1.525		.634	FUSELAGE SIDE
l	136	.500	883.15		430.00	11 290	{	-	110	,033	UPPER BODY
	137	.600	1012.18		430.00	13 549			┼╀	.032	
	138	.700	1141.21		430 00	15.900			╞╌╂	.032	
ŀ	139	.800	1270.24		430.00	19.000		· V		.032	
ŀ	L40	.900	1399.27		370.00	18.064	f	7.525		.032	
þ	41	.300	625.09		179 90	20.322	6	5.475	 	.033	
þ	42	.400	754.12	· · ·	4/8.80	6.774		3.379	135	.03/	· · · · · · · · · · · · · · · · · · ·
հ	.43	.500	883.15	+		9.032			135	.030	
հ	44	.600	1012.18			11.290			135	1.033	
h	45	.700	1141,21			13.548			135	.033	
h	46	.600	1012 18		1150	15.806			135	<i>\$</i> 32	
1	47	.600	1012 18		40.0	13.548		•788	113	.032	
1	48	.750	1205.73			13.548	7	.70	112	.032	
1	49	.750	1502.73		50.00	15.806	7	.875	116	.032	<u> </u>
1	50	.400	754 12		90.00	15.806		.575	149	.:34	UPPER BODT
1	51	. 500	992 15			9.032			59.5	.03/	WING UPPER CREASE
1	52	.600	1012.10			11.290			63	.012	4
1	53	700	1141 21	+		13.548			55.5	.030	
14		900	1200 27			15.806			64	.030	•
			1333.71		32.0	20.322				.034	WING UPPER CREASE

Table IV (Cont'd) Orbiter

Table IV (Continued) Orbiter

T/C	2у	x	FULL S	CALE	MOJEL S	CALE	SKIN	REMARKS
NO.	b	ĉ	×o	У	×o	У	THICK- NESS	NETHINKS
155	.250	.025	640.650	117.085	7.043	2.049	.031	WING BOTTOM
156		.153	754.120	▲	9.030		.035	SURFACE
157		.299	883.150		11.288		.028	A
158		.444	1012.180		13.545		.023	
159		•590	1141.200		15.802		-034	
160	V	.736	1270.230	. ↓	18.060	•	.034	· · · · ·
161	•250	.900	1415.900	117.085	20.613	2.049	.034	
162	.301		754.000		9.030		.023	JOWN
163	•348		883.000		11.288		.028	DOWN
164	•400	.025	1002.063	187.336	13.364	3.278	.035	
165		.100	1039.750	•	14.031		. 034	
166		.200	1090.000		14.900		. 034	
167		.302	1141.210		15.802		.035	
168		•559	1270.230		18.060		.032	
169	•	.700	1341.250	•	19 .307	•	.032	
170	.400	.900	1441.750	187.336	21.065	3.278	.032	ELEVON
171	.500		1067.470	234.170	14.516	4.098	.033	DOWN
172		.025	1077.913		_14.696_	•	.035	
173		.177	1141.210		15.802		.030	
174		.300	1192.450		16.706		.03/	
175		.487	1270.230		18.060		.034	
176		.600	1317.428		18.895		.034	
177		•700	1359.028		19.618	★	.033	
178	•	•900	1442.350	234.170	21.075	4.098	.033	ELEVON
179	.600	.100	1152.000	281.004	15.995	4.918	.033	
180		.200	1188.00		16.625		.03/	
181		.300	1224.000		17.255		.026	
182		.428	1270.230	ļ	18.064		.026	Y
183	↓	.600	1332.000	•	19.145	•	.027	WING BOTTOM
184	•600	.700	1368.000	281.004	19.775	4.918	.024	SURFACE

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"*

Table IV (Continued) Orbiter

T/C	2y	x	FULL	SCALE	MODEL	SCALE	SKIN	
NÓ.	b	c	×o	У	× (FROM)	У	THICK- NESS	REMARKS
185	.600	.800	1404.000	281.004	20.404	4.918	.035	WING BOTTOM
186	•600	•850	1422.000	‡	20.720		.033	ELEVON
187	.600	.90	1440.000	281.004	21.034		.034	
188	.750	↓ .	1186.5	351.255	16.599	6.147	.035	L.E. ROLLED
189		.025	1193.428	≜	16.720	•	.035	DOWN 30°
190		.100	1214.228		17.084		.032	
191		.303	1270.230		18.064		-032	
192		.500	1325.028		19.023	,	.032	
193		.700	1380.400		19.992		.027	
194		.800	1408.100		20.476	•	.03/	
195	•	.850	1422.000	•	20.719		.035	
196	•750	.900	1435.800	351.255	20.962	6.147	.035	
197	•850	.100	1255.200	398.089	17.801	6.967	.03/	1
198	.850	.300	1299.600	398.089	18 .5 78	6.967	. 034	
199	.850	.500	1344.000	398.089	19.355	6.967	- 032	
200	.900	.60	1373.028	421.506	19.863	7.376	.024	
201	.900	.30	1314.743	421.506	18.846	7.376	.030	
202	•950			444.857		7.785	.035	L.E. ROLLED
203		.050	1295.925		18.514		.035	
204		100	1303.828		18.652		.035	
205		.300	1335-543		19.207		.024	
206	┇ ╋╌╌┽╶┥	500	1367-257		19.762		.022	
207		• 7 00	1398.950		20.316	•	- 035	
208	•950	•900	1430.650	•	20.870	7.785	. 030	
209	•966	0.00	1307.000	452.416	18.708	7.917	.032	L.E.
210	.993	0.00	1398,950	464.914	20.316	8.136	• 03/	L.E.
211	.600			281.004		4.918	.035	CLUSTER B
212				_			.035	
213	•					•	.035	Ý
214	•600			281.004		.4.918	.035	SURF OF

	1							· · · · · · · · · · · · · · · · · · ·
TIC	24	x	FULL	SCALE	, MODEL	SCALE	SKIN	
NO.	Б	ē	×	*	FROM	у	THICK-	REMARKS
			0	•	^ (NOSE)		NESS	
215	.600			281.154		4.918	. 035	CLUSTER B
216	.600			281.144		4.918	. 035	
217	.600			281.004		4.918	.035	
218	.850			398.029		6.967	.020	CLUSTER C
219				•			. 020	
220						·	.020	
221		• .					.020	
222							. 020	
223				•		•	. 020	
224	.850			398.089		6.967	.020	•
225	.400	.050	1015.114	187.336	13.599	3.278	. 025	WING TOP SUBFACE
226		.200	1090.428		14.918		· 024	
227	•	.600	1291.171	\checkmark			. 633	
228	.400	.950	1466.875	187.336		3.278	.03/	ELEVON
229	.600	.050	1134.886	281.004	15.696	4,918	.032	
230	.600	.200	1188.657		16.637		.031	•
231	.600	.600	1332.028		19.146		.03/	
232		.800	1404.000		20.404		.032	ELEVON
233		.900	1440.000	•	21.034	•	.034	
234	.600	.950	1458.000	281.004	21.349	4.918	.033	•
235	.800	.050	1223.057	374.672	17.239	6.557	.033	
236		.200	1260.257	•	17.889	▲	.033	
237		.600	1359.514		19.627		.032	
238		.800	1408.780		20.488		.030	ELEVON
239		.900	1433.690	•	20.924	•	.030	ELEVON
240	.800	.950	1446.145	374.672	21.192	6.557	.030	ELEVON 🔻

Table IV (Continued) Orbiter

No. L x ₀ y z x(ROM NOSE) y z ϕ THICK- NESS REMARK 241 .829 1307 18.715 .026 BOTTOM CRE OF ONS 242 .900 1399.27 20.318 .035 BOTTOM CRE OF ONS 243 .975 1496.04 22.011 .036 .037 BOTTOM CRE OF ONS 244 1.000 1528.3 22.575 .034/ BOTTOM OF R 245 1.014 1547.0 22.902 .035 BOTTOM OF R 246 .780 124.5 95.0 474.0 18.173 1.976 8.295 122.8 .037 A 248 .829 1307 124.5 474.0 18.173 1.976 8.295 19.1 .035 DOTTOM OF R 248 .829 1307 124.5 474.0 18.173 1.976 8.295 102.8 .037 A 249 .862 1350 132.6 4 19.460 2.320 8.295 117.5 .028 DOT DOT 2.55	T/C	X	FL.	JLL S	CALE	M	ODEL SC	ALE		SKIN	1
241 $.829$ 1307 18.715 $.026$ BOTTOM CRE OF ONS242.900 1399.27 20.318 $.035^{-}$ BOTTOM CRE OF ONS243.975 1496.04 22.011 $.030^{-}$ $.035^{-}$ BOTTOM CRE OF ONS244 1.000 1528.3 22.575 $.034^{-}$ BOTTOM OF R245 1.014 1547.0 22.902 $.035^{-}$ BOTTOM OF R246.780 1245 95.0 474.0 17.608 1.662 8.295 123.6 $.034^{-}$ 247.805 1276 112.9 474.0 18.173 1.976 8.295 123.6 $.03^{-}$ 248.829 1307 124.5 474.0 18.715 2.179 8.295 120.8 $.03^{-}$ 249.862 1350 132.6 19.460 2.320 8.295 117.5 $.032^{-}$ 250.963 14.80 142.5 21.740 2.494 8.295 117.5 $.033^{-}$ 251 1.000 $152^{-}.3$ 142.5 22.575 2.494 8.295 117.5 $.032^{-}$ 251 1.000 $152^{-}.3$ 142.5 22.575 2.494 8.295 117.5 $.032^{-}$ 253.805 1276 105.5 488 18.173 1.846 8.540 129.5 $.032^{-}$ 254.829 1307 117.0 498.7 18.715 2.048 8.727 130.0 $.038^{-}$ 254.8	NÓ.		×o	У	Z	×(FROM NOSE) у	Z	\$	THICK- NESS	REMARKS
242.900 1399.2^{-1} 20.318.935BOTTOM CER243.975 1496.01 22.011.935BOTTOM CER244 1.000 1528.3 22.575.932BOTTOM OF R245 1.014 1547.0 22.902.935BOTTOM OF R246.780 1245 95.0 474.0 17.608 1.662 8.295 127.4 .935247.805 1276 112.9 474.0 18.173 1.976 8.295 123.6 .937248.829 1307 124.5 474.0 18.715 2.179 8.295 120.8 .637249.862 1350 132.6 19.460 2.320 8.295 117.5 .028250.963 148.0 142.5 21.740 2.494 8.295 117.5 .033251 1.000 152^{-3} 142.5 22.575 2.494 8.295 117.5 .033252 1.014 $154.7.0$ 474.0 22.902 8.295 $.033$.033253.805 1276 105.5 488 18.173 1.846 8.540 129.5 .032254.829 1307 117.0 498.7 18.715 2.048 8.727 130.0 $.028$ 254.829 1307 117.6 95.0 22.902 8.750 $.033$ 255.862 1350 126.5 506 19.460 2.214 8.855 130.0 $.028$	241	. 829	1307			18.715				.026	BOTTOM CREASE
243. 975 1496.04 22.011 $.030$ BOTTOM CH2. OF ONE 244 1.000 1528.3 22.575 $.034'$ BOTTOM OF R 245 1.014 1547.0 22.902 $.035'$ BOTTOM OF R 246 .780 1245 95.0 4.74.0 17.608 1.662 8.295 127.5 $.035'$ BOTTOM OF R 244 .805 1276 112.9 474.0 18.173 1.976 8.295 123.6 $.03'$ $.03'$ 248 .829 1307 124.5 474.0 18.173 1.976 8.295 123.6 $.03'$ $.03'$ $.03'$ 249 .862 1350 1.22.6 $.9474.0$ 18.173 1.976 8.295 120.8 $.03'$ $.03'$ 250 .963 14.80 1.42.5 22.757 2.494 8.295 117.5 .02.8 251 1.004 15.7.0 4.74.0 22.902 8.295 $.033'$.033' .033' .033' .033' .033' .033' .033' .033' .033'	242	.900	1399.2	1	ļ	20.318			1	.035	BOTTOM CPEASE
244 1.000 1528.3 22.575 .034/ BOTTOM OF R 245 1.014 1547.0 22.902 .035 BOTTOM OF R 246 .780 1245 95.0 4.74.0 17.608 1.662 8.295 127.9 .035 BOTTOM OF R 247 .805 1276 112.9 474.0 18.173 1.976 8.295 123.6 .037 A 248 .829 1307 124.5 474.0 18.173 1.976 8.295 120.8 .037 A 249 .862 1350 132.6 19.460 2.320 8.295 119.1 .035 A 250 .963 1480 142.5 21.740 2.494 8.295 117.5 .028 A 251 1.000 157°.3 142.5 22.575 2.494 8.295 117.5 .032 A 253 .805 1276 105.5 488 18.173 1.846 8.540 129.5 .032 A 254 .829 1307 117.0 498.7<	243	.975	1496.0	4		22.011				. 030	BOTTOM CREASE
245 1.014 1547.0 22.902 $.035$ BOTTOM OF R 246 .780 1245 95.0 474.0 17.608 1.662 8.295 127.9 .032 0MS PODS 247 .805 1276 112.9 474.0 18.173 1.976 8.295 123.6 .03/ $.03/$ 248 .829 1307 124.5 474.0 18.715 2.179 8.295 123.6 .03/ $.03/$ 249 .862 1350 132.6 19.460 2.320 8.295 119.1 .035 .035 250 .963 14.80 142.5 21.740 2.494 8.295 117.5 .028 251 1.000 152°.3 142.5 22.575 2.494 8.295 117.5 .032 253 .805 1276 105.5 488 18.173 1.846 8.540 129.5 .032 254 .829 1307 117.0 498.7 18.715 2.048 8.727 130.0 .032 255 .862 <	244	1.000	1528.3			22.575				.034	BOTTOM OF RCS
246 .780 1245 95.0 474.0 17.608 1.662 8.295 127. .032 ONS PODS 247 .805 1276 112.9 474.0 18.173 1.976 8.295 123.8 .03/ 4 248 .829 1307 124.5 474.0 18.715 2.179 8.295 120.8 .63/ 1 249 .862 1350 132.6 19.460 2.320 8.295 119.1 .035 1 250 .963 14.80 142.5 21.740 2.494 8.295 117.5 .028 1 251 1.000 152°.3 142.5 22.575 2.494 8.295 117.5 .033 252 1.014 154.7.0 474.0 22.902 8.295 .033 1 254 .829 1307 117.0 498.7 18.173 1.846 8.540 129.5 .032 254 .829 1307 117.0 498.7 18.715 2.048 8.727 130.0 .028	245	1.014	1547.0			22.902			1	.035	BOTTOM OF RCS
247 .805 1276 112.9 474.0 18.173 1.976 8.295 123.8 $03/$ 248 .829 1307 124.5 474.0 18.715 2.179 8.295 120.8 $03/$ 249 .862 1350 132.6 19.460 2.320 8.295 119.1 $035'$ 250 .963 1480 142.5 21.740 2.494 8.295 117.5 028 251 1.000 152°.3 142.5 22.575 2.494 8.295 117.5 033 252 1.014 154.7.0 4.74.0 22.902 8.295 $.033$ 253 .805 1276 105.5 4.88 18.173 1.846 8.540 129.5 $.032$ 254 .829 1307 117.0 4.98.7 18.715 2.048 8.727 130.0 $.033$ 255 .862 1350 126.5 506 19.460 2.214 8.855 130.0 $.028$ 257 1.000 1528.3 500 22.575	246	.780	1245	95.0	474.0	17.608	1.662	8.295	127.9	. 032	OMS PODS
248 829 1307 124.5 474.0 18.715 2.179 8.295 120.8 $.63/$ 249 $.862$ 1350 132.6 19.460 2.320 8.295 119.1 $.035$ 250 $.963$ 1480 142.5 21.740 2.494 8.295 117.5 $.028$ 251 1.000 152° .3 142.5 22.575 2.494 8.295 117.5 $.033$ 252 1.014 1547.0 474.0 22.902 8.295 $.033$ 253 $.805$ 1276 105.5 488 18.173 1.846 8.540 129.5 $.032$ 254 $.829$ 1307 117.0 498.7 18.715 2.048 8.727 130.0 $.033$ 255 $.862$ 1350 126.5 506 19.460 2.214 8.855 130.0 $.028$ 256 $.963$ 1480 134.5 513 21.740 2.354 8.978 130.0 $.028$ 257 1.000 1528.3 500 22.902 8.750 $.032$ 258 1.014 1547.0 500 22.902 8.750 $.032$ 259 $.805$ 1276 95.0 494.3 18.173 1.662 8.942 139.0 $.034$ 259 $.805$ 1276 95.0 521.0 19.460 1.662 9.118 142.1 $.037$ 260 $.829$ 1307 95.0 530.0 21.740 1.662 <th>247</th> <th>.805</th> <th>1276</th> <th>112.9</th> <th>474.0</th> <th>18.173</th> <th>1.976</th> <th>8.295</th> <th>123.8</th> <th>.03/</th> <th></th>	247	.805	1276	112.9	474.0	18.173	1.976	8.295	123.8	.03/	
249.8621350132.619.4602.3208.295119.1 $.035$ 250.96314.80142.521.7402.4948.295117.5 $.028$ 2511.000152°.3142.522.5752.4948.295117.5 $.033$ 2521.0141547.0474.022.9028.295 $.033$ 253.8051276105.548818.1731.8468.540129.5 $.032$ 254.8291307117.0498.718.7152.0488.727130.0 -033 255.8621350126.550619.4602.2148.855130.0 $.037$ 256.9631480134.551321.7402.3548.978130.0 $.028$ 2571.0001528.350022.5758.750 $.032$ 2581.0141547.050022.9028.750 $.032$ 259.805127695.0494.318.1731.6628.942139.0 $.034$ 260.829130795.0511.018.7151.6628.942139.0 $.034$ 261.862135095.0521.019.4601.6629.118142.1 $.037$ 262.963148095.0530.021.7401.6629.275144.0 $.027$ 263.862135065517.519.4601.1389.056151.2 $.037$ <tr<< th=""><th>248</th><th>.829</th><th>1307</th><th>124.5</th><th>474.0</th><th>18.715</th><th>2.179</th><th>8.295</th><th>120.8</th><th>.631</th><th></th></tr<<>	248	.829	1307	124.5	474.0	18.715	2.179	8.295	120.8	.631	
250 .96314.80142.5 21.740 2.494 8.295 117.5 . 028 251 1.000 $152^{\circ}.3$ 142.5 22.575 2.494 8.295 117.5 . 033 252 1.014 1547.0 474.0 22.902 8.295 . 033 253 805 1276 105.5 488 18.173 1.846 8.540 129.5 . 032 254 829 1307 117.0 498.7 18.715 2.048 8.727 130.0 . 033 255 862 1350 126.5 506 19.460 2.214 8.855 130.0 . 033 256 .963 1480 134.5 513 21.740 2.354 8.978 130.0 . 028 257 1.000 1528.3 500 22.575 8.750 . 032 258 1.014 1547.0 500 22.902 8.750 . 032 259 $.805$ 1276 95.0 494.3 18.173 1.662 8.942 139.0 . 034 260 $.829$ 1307 95.0 511.0 18.715 1.662 8.942 139.0 . 034 261 $.862$ 1350 95.0 521.0 19.460 1.662 9.275 144.0 . 0277 263 $.862$ 1350 65 517.5 19.460 1.138 9.056 151.2 $.037$ 264 $.963$ 14.90 65 527.0	249	.862	1350	132.6		19.460	2.320	8.295	119.1	.035	
251 1.000 $152^{\circ} \cdot 3$ 142.5 \checkmark 22.575 2.494 8.295 117.5 $.033$ 252 1.014 1547.0 474.0 22.902 8.295 $.033$ 253 $.805$ 1276 105.5 488 18.173 1.846 8.540 129.5 $.032$ 254 $.829$ 1307 117.0 498.7 18.715 2.048 8.727 130.0 -033 255 $.862$ 1350 126.5 506 19.460 2.214 8.855 130.0 -034 256 $.963$ 1480 134.5 513 21.740 2.354 8.978 130.0 $.028$ 257 1.000 1528.3 500 22.575 8.750 $.032$ 258 1.014 1547.0 500 22.902 8.750 $.032$ 259 $.805$ 1276 95.0 494.3 18.173 1.662 8.650 135.0 $.034$ 260 $.829$ 1307 95.0 511.0 18.715 1.662 8.942 139.0 $.034$ 261 $.862$ 1350 95.0 521.0 19.460 1.662 9.118 142.1 $.037$ 262 $.963$ 1.480 95.0 530.0 21.740 1.662 9.275 144.0 $.027$ 263 $.862$ 1350 65 517.5 19.460 1.138 9.056 151.2 $.037$ 264 $.963$ 1	250	.963	1480	142.5		21.740	2.494	8.295	117.5	. 028	
252 1.014 1547.0 474.0 22.902 8.295 $.033$ 253 $.805$ 1276 105.5 488 18.173 1.846 8.540 129.5 $.032$ 254 $.829$ 1307 117.0 498.7 18.715 2.048 8.727 130.0 -033 255 $.862$ 1350 126.5 506 19.460 2.214 8.855 130.0 -033 256 $.963$ 1480 134.5 513 21.740 2.354 8.978 130.0 $.028$ 257 1.000 1528.3 500 22.575 8.750 $.033$ $.028$ 259 $.805$ 1276 95.0 494.3 18.173 1.662 8.650 135.0 $.032$ 259 $.805$ 1276 95.0 511.0 18.715 1.662 8.942 139.0 $.034$ 260 $.829$ 1307 95.0 511.0 18.715 1.662 8.942 139.0 $.034$ 261 $.862$ 1350 95.0 521.0 19.460 1.662 9.118 142.1 $.03/$ 262 $.963$ 1480 95.0 530.0 21.740 1.662 9.275 144.0 $.0277$ 263 $.862$ 1350 65 517.5 19.460 1.138 9.056 151.2 $.03/$ 264 $.963$ 1490 65 527.0 21.740 1.138 9.222 153 $.0$	251	1.000	1529.3	142.5	•	22.575	2.494	8.295	117.5	.033	
253.805 1276 105.5 488 18.173 1.846 8.540 129.5 . 032 254 .829 1307 117.0 498.7 18.715 2.048 8.727 130.0 -033 255 .862 1350 126.5 506 19.460 2.214 8.855 130.0 . 037 256 .963 1480 134.5 513 21.740 2.354 8.978 130.0 . 028 257 1.000 1528.3 500 22.575 8.750 . 037 258 1.014 1547.0 500 22.902 8.750 . 032 259 .805 1276 95.0 494.3 18.173 1.662 8.650 135.0 . 034 260 .829 1307 95.0 511.0 18.715 1.662 8.942 139.0 . 034 261 .862 1350 95.0 521.0 19.460 1.662 9.118 142.1 . 031 262 .963 1480 95.0 530.0 21.740 1.662 9.275 144.0 . 027 263 .862 1350 65 517.5 19.460 1.138 9.056 151.2 . 037 264 .963 $14P0$ 65 527.0 21.740 1.138 9.222 153 . 026 $0M5$	252	1.014	1547.0	ļ	474.0	22.902		8.295		.033	
254.8291307117.0498.718.7152.0488.727130.0 -033 255 .8621350126.550619.4602.2148.855130.0 $-03/$ 256 .9631480134.551321.7402.3548.978130.0 -028 257 1.0001528.350022.5758.750 $.03/$ 258 1.0141547.050022.9028.750 $.032$ 259 .805127695.0494.318.1731.6628.650135.0 $.032$ 260 .829130795.0511.018.7151.6628.942139.0 $.034$ 261 .862135095.0521.019.4601.6629.118142.1 $.03/$ 262 .963148095.0530.021.7401.6629.275144.0 $.027$ 263 .862135065517.519.4601.1389.056151.2 $.03/$ 264 .963149065527.021.7401.1389.222153 $.026$ OMS PODS	253	.805	1276	105.5	488	18.173	1.846	8.540	129.5	.032	
255.8621350126.550619.4602.2148.855130.0 $.03/$ 256 .9631480134.551321.7402.3548.978130.0 $.028$ 257 1.0001528.350022.5758.750 $.03/$ 258 1.0141547.050022.9028.750 $.032$ 259 .805127695.0494.318.1731.6628.650135.0 $.032$ 260 .829130795.0511.018.7151.6628.942139.0 $.034$ 261 .862135095.0521.019.4601.6629.118142.1 $.03/$ 262 .963148095.0530.021.7401.6629.275144.0 $.027$ 263 .862135065517.519.4601.1389.056151.2 $.03/$ 264 .96314.9065527.021.7401.1389.222153 $.026$ 0MS	254	.829	1307	117.0	498.7	18.715	2.048	8.727	130.0	-033	
256.9631480134.551321.7402.3548.978130.0.028 257 1.0001528.350022.5758.750.03/ 258 1.0141547.050022.9028.750.03Z 259 .805127695.0494.318.1731.6628.650135.0.03Z 260 .829130795.0511.018.7151.6628.942139.0.034 261 .862135095.0521.019.4601.6629.118142.1.03/ 262 .963148095.0530.021.7401.6629.275144.0.027 263 .862135065517.519.4601.1389.056151.2.03/ 264 .96314.9065527.021.7401.1389.222153.0260MS	255	.862	1350	126.5	506	19.460	2.214	8.855	130.0	.03/	
257 1.000 1528.3 500 22.575 8.750 $.03/$ 258 1.014 1547.0 500 22.902 8.750 $.032$ 259 $.805$ 1276 95.0 494.3 18.173 1.662 8.650 135.0 $.032$ 260 $.829$ 1307 95.0 511.0 18.715 1.662 8.942 139.0 $.034$ 261 $.862$ 1350 95.0 521.0 19.460 1.662 9.118 142.1 $.03/$ 262 $.963$ 1480 95.0 530.0 21.740 1.662 9.275 144.0 $.027$ 263 $.862$ 1350 65 517.5 19.460 1.138 9.056 151.2 $.03/$ 264 $.963$ 1490 65 527.0 21.740 1.138 9.222 153 $.026$ $0MS$ POIDS	256	.963	1480	134.5	513	21.740	2.354	8.978	130.0	.028	
258 1.014 1547.0 500 22.902 8.750 $.032$ 259 $.805$ 1276 95.0 494.3 18.173 1.662 8.650 135.0 $.032$ 260 $.829$ 1307 95.0 511.0 18.715 1.662 8.942 139.0 $.034$ 261 $.862$ 1350 95.0 521.0 19.460 1.662 9.118 142.1 $.031$ 262 $.963$ 1480 95.0 530.0 21.740 1.662 9.275 144.0 $.027$ 263 $.862$ 1350 65 517.5 19.460 1.138 9.056 151.2 $.031$ 264 $.963$ $14P0$ 65 527.0 21.740 1.138 9.222 153 $.026$ OMS PODS	257	1.000	1528.3		500	22.575		8.750		. 03/	
259 .805 1276 95.0 494.3 18.173 1.662 8.650 135.0 $.033$ 260 .829 1307 95.0 511.0 18.715 1.662 8.942 139.0 $.034$ 261 .862 1350 95.0 521.0 19.460 1.662 9.118 142.1 $.031$ 262 .963 1480 95.0 530.0 21.740 1.662 9.275 144.0 $.027$ 263 .862 1350 65 517.5 19.460 1.138 9.056 151.2 $.031$ 264 .963 $14P0$ 65 527.0 21.740 1.138 9.222 153 $.026$ $0MS$ PODS	258	1.014	1547.0		500 -	22.902	·· · _	8.750		.032	
260 829 1307 95.0 511.0 18.715 1.662 8.942 139.0 $.034$ 261 862 1350 95.0 521.0 19.460 1.662 9.118 142.1 $.034$ 262 $.963$ 1480 95.0 530.0 21.740 1.662 9.275 144.0 $.027$ 263 $.862$ 1350 65 517.5 19.460 1.138 9.056 151.2 $.03/$ 264 $.963$ $14P0$ 65 527.0 21.740 1.138 9.222 153 $.026$ OMS PODS	259	.805	1276	95.0	494.3	18.173	1,662	8.650	135.0	- 033	
261 .862 1350 95.0 521.0 19.460 1.662 9.118 142.1 .03/ 262 .963 1480 95.0 530.0 21.740 1.662 9.275 144.0 .027 263 .862 1350 65 517.5 19.460 1.138 9.056 151.2 .03/ 264 .963 1490 65 527.0 21.740 1.138 9.222 153 .026 OMS PODS	260	.829	1307	95.0	511.0	18.715	1.662	8.942	139.0	. 034	
262.963 1480 95.0 530.0 21.740 1.662 9.275 144.0 $.027$ 263 .862 1350 65 517.5 19.460 1.138 9.056 151.2 $.03/$ 264 .963 1490 65 527.0 21.740 1.138 9.222 153 $.026$ $0M5$ POD5	261	.862	1350	95.0	521.0	19.460	1.662	9.118	142.1	.03/	
263.862 1350 65 517.5 19.460 1.138 9.056 151.2 .03/ 264.963 14P0 65 527.0 21.740 1.138 9.222 153 .026 OMS POIDS	262	.963	1480	95.0	5 <u>30.0</u>	21.740	1.662	9.275	144.0	.027	
264.963 14PO 65 527.0 21.740 1.138 9.222 153 .026 ONS PODS	263	.862	1350	65	517.5	19.460	1.138	9.056	151.2	.031	*
	264	.963	140	65	527.0	21.740	1.138	9.222	153	.026	OMS PODS

Table IV (Continued)

Table IV (CONCLUDED) · Orbiter

			FULL S	CALE	MODEL	SCALE			
T/C NO.	Z bv	× c	×o	Z	× (FROM)	z	SKIN THICKNESS	REMARKS	
265	.159	.100	1353.00	550.20	19.513	9.628	, 030	VERTICAL TAIL	
266		.300	1,01.51	550.20	20.361	9.628	.030	A	
267	<u> </u>	.700	1498.66	550.20	22.062	9.628	. 028		
268	.299	0.00		594.40		0.402	- 033	L.E.	
269		.100	1394.94	▲	20.246		. 03/		
270		.300	1439.00		21.018		.03/		
271		.500	1483.06		21.789		.03/		
272	•	.700	1527.11	•	22.559	•	.022		
273	.2 99	.900	1571.17	594.40	23.330	10.402	. 022		
274	•532	0.00		667.96		11.689	.034	L.E.	
275		.100	1538.31		22.755	•	.03/		
276		.300	1574.94		23,396		.032		
277		.500	1611.57		35.034		.032		
278	•	.700	1648.14	•	24.677	¥	.023	1	
279	.532	.900	1684.77	667.96	25.318	11.689	.026		
280	.765	0.00		741.53		12,977	.034	L.E.	
281	.765	.100	1461.00		21.403		.03/		
282		.300	1490.14		21.912		.03/		
283		.500	1519.29		22.423		-030		
. 284		.700	1548.43	•	22.933	¥	.024		
285	.765	.900	1577.57	741.53	23.442	12.977	.024		
286	.905	0.00		785.73		13.750	.033	L.E.	
287	.905	.100	1576.49	785.73	23.424	13.750	.030	▼	
288	.905	.500	1625.86	785.73	24.288	13.750	.030	VERTICAL TAIL	

T/C	x FROM E	XIT PLANE	φ _n CLOCKWISE LOOKING FORWARD		
NO.	F.S.	M.S.	SKIN	0° BOTTOM (
301	5"	0.088	. 031	0°	
302			.03/	25 ⁰	
303	·		. 03/	45 ⁰	
304			.031	65 ⁰	
305			.03/	90 ⁰	
306			.03/	135 ⁰	
307	Ţ		.03/	315 ⁰	
308	10"	0.175	.03/	00	
309			. 031	25 ⁰	
310			.03/	45 ⁰	
311			.03/	65 ⁰	
312			.03/	90 ⁰	
313	15"	0.263	.03/	00	
314			.03/	45 ⁰	
315			.031	90 ⁰	
316	25"	. 0.438	. 031	00	
317			.03/	45 ⁰	
318			-03/	65 ⁰	
319			.031	90 ⁰	
320	45"	0.788	.03/	45 ⁰	
321			.032	BASE PLATE	
322			.034		
323			.03/		
324			.032	V -	

TableVOrbiterLeftMainNOzzleT/CLocationsModel22-0TS



			Mode	1 22-015		
T/C NO.	x _ş FS	× * * * * * * * * * * * * * * * * * * *	x L	*	SKIN THICKNESS	REMARKS
701	200.000	0.000	0.000	90 ⁰	.022	NOSE
702	241.900	0.733	0.025	900	.03/	
03	283.800	1.467	0.050	90 ⁰	.03/	
04	367.600	2.933	0.100	900	.033	Y
05	870.400	11.732	0.400	90 ⁰	.029	-
06	1373.200	20.531	0.700	90 ⁰	.030	
07	1507.280	22.877	0.780	90 ⁰	.030	
08	1540.800	23.464	0.800	90 ⁰	.029	
09	1708.400	26.397	0.900	90 ⁰	.03/	
10	1758.680	27.277	0.930	90 ⁰	.034	
11	1859.240	29.037	0,990	90 ⁰	.036	
12	1373.200	20.531	0.700	135 ⁰	.030	
13	1708.400	26.397	0.900	135 ^Q	.030	
14	1758.680	27.277	0.930	135 ⁰	.034	
15	1859.240	29.037	0.990	135 ⁰	.035	
16	283.800	1.467	0.050	180 ⁰	.032	
17	367.600	2.933	0.100	180 ⁰	.034	
18	535.200	5.866	0.200	180 ⁰	.030	

180⁰

180[°]

180⁰

2100

210⁰

0.400

0.500

0.600

0.650

0.700

0.750

0.780

0.800

0.850

0.900

0.930

0.960

0.990

0.904

0.918

.030

.029

.030

.030

.029

.029

.030

.028

.028

.0 28

.032

.034

.034

.028

.030

SKIRT

SKIRT

SKIRT

SEPARATION

NOZZLES

Table VI Solid Rocket Booster T/C Locations

*MEASURED FROM NOSE

719

720

721

722

723

724

725

726

727

728

729

730

731

732

733

870.400

1038.000

1205.600

1289.400

1373.200

1457.000

1507.280

1540.800

1624.600

1708.400

1758.680

1808.960

1859.240

1715.000

1738.000

11.732

14.665

17.598

19.065

20.531

21.998

22.877

23.464

24.931

26.397

27.277

28.157

29.037

26.514

26.984

T/C NO.	×s FS	× * ms	× L	¥	SKIN	REMARKS
734	1750.000	27,130	0.925	2100	AZZ	SEPARATION
735	1792,200	27,864	0.950	210	.032	NOZZLES
736	1825,720	28 450	0.970	210	.033	15-5PH
737	1750 300	27 120	0.025	~ 010	.032	
738	1775 440	27.130	0.925	≈215°	,032	
739	1909 060	27.570	0.940	≈215°	.032	
740	1808.960	28.157	0.960	~ 215	.033	•
740	325.700	2.200	0.0/5	225	.035	
741	367.600	2.933	0.100	2250	.034	
742	451.400	4.400	0.150	2250	.032	
743	535.200	5.866	0.200	2250	.0 30	
/44	702.800	8.799	0.300	225 ⁰	.028	
/45	870.400	11.732	0.400	225 ⁰	.0 30	
746	1038.000	14.665	0.500	225 ⁰	.0 30	
747	1205.600	17.598	0.600	225 ⁰	.030	
748	1373.200	20.531	0.700	225 ⁰	.030	
749	1507.280	22.877	0.780	225 ⁰	.030	
750	1540.800	23.464	0.800	225 ⁰	.029	
751	1624.600	24.931	0.850	225 ⁰	.029	
752	1708.400	26.397	0.900	225 ⁰	.027	
753	1758.680	27.277	0.930	225 ⁰	.031	SKIRT
754	1808.960	28.157	0.960	225 ⁰	.032	1
755	1859.240	29.037	0.990	225 ⁰	.032	
756	1758.68	27.277	0.930	240 ⁰	,030	······
757	1808.960	28.157	0.960	240 ⁰	031	
758	1859.240	29.037	0.990	240 ⁰	.032	
759	702.800	8.799	0.300	247.5 ⁰	.028	
760	870,400	11.732	0.400	247.5 ⁰	.030	
761	1038,000	14.665	0.500	247.5 ⁰	.030	
762	1205.600	17.598	0.600	247.5 ⁰	,030	
763	1289.400	19.065	0.650	247.50	0.21	
764	1373.200	20.531	0.700	247.5 ⁰	,030	
765	1457.000	21.998	0.750	247.5 ⁰	,031	
766	392.741	3.373	0.115	260 ⁰	1037_	

Table VI (Continued) (Solid Rocket Booster)

*MEASURED FROM NOSE

47 ' .

		SOLIG KOCK		CEL		
T/C NO.	×s FS	* × m s	× L	*	SKIN THICKNESS	REMARKS
767	203.816	0.067	0.002	270 ⁰	.035	ON 45° RAY
768	241.900	0.733	0.025	270 ⁰	.033	- FROM NOSE - Radius
769	283.800	1.467	0.050	270 ⁰	,033	
770	325.700	2.200	0.075	270 ⁰	.036	
777	367.600	2.933	0.100	270 ⁰	.036	
772	384.360	3.226	0.110	270 ⁰	.036	
773	417.880	3.813	0.130	270 ⁰	.032	·
774	451.400	4.400	0.150	270 ⁰	.032	
775	535.200	5.866	0.200	270 ⁰	.030	•
776	619.000	7.333	0.250	270 ⁰	.030	
777	702.800	8 [.] .799	0.300	270 ⁰	.028	
778	870.400	11.732	0.400	270 ⁰	.029	
779	1038.000	14.665	0.500	270 ⁰	.030	
780	1205.600	17.598	0.600	270 ⁰	.03/	
781	1289.400	19.065	0.650	270 ⁰	-03/	
782	1373.200	20.531	0.700	270 ⁰	.030	
783	1457.000	21.998	0.750	270 ⁰	.030	
7.84	1507.280	22.877	0.780	270 ⁰	.030	
785	1540.800	23.464	0.800	270 ⁰	. 030	
786	1624.600	24.931	0.850	270 ⁰	.030	
787	1708.400	26.397	0.900	270 ⁰	.027	
788	1758.680	27.277	0.930	270 ⁰	-029	SKIRT
789	1808.960	28.157	0.960	270 ⁰	.032	
790	1859.240	29.037	0.990	270 ⁰	.032	*
791	702.800	8.799	0.300	315 ⁰	.029	
792	1038.000	14.665	0.500	315 ⁰	,030	
793	1373.000	20.531	0.700	315 ⁰	.029	
794	1507.280	22.877	0.780	315 ⁰	. 028	
795	1540.800	23.464	0.800	315 ⁰	.028	
796	1708.400	26.397	0.900	315 ⁰	.028	
797	1758.680	27.277	0.930	315 ⁰	.030	
798	1859.240	29.037	0 990	315 ⁰	.032	

Table VI (Concluded)Solid Rocket Booster)

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*MEASURED FROM NOSE

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TIC		1				
NO.	× _T FS	×	× L	θ	SKIN THICKNESS	REMARKS
501	383.60	1.306	.040	0 ⁰	.03/	NOCR
502	458.20	2.6110	.080		.034	NOSE
503	588.75	4.896	.150		.035	NOSE
504	1055.00	13.055	.400		.035	
505	1428.00	19.582	.600	·	.034	†
506	1801.00	26 .110	.800	00	.035	
507	1055. 00	13.055	.400	45 ⁰	.035	
508	1241. 50	16.319	.500		.035	
509	1428.00	19.582	.600	<u>† </u>	.034	
510	1614.50	22.846	.700	+-+	.034	
511	1801.00	26.110	.800	<u>†</u> - ↓	.035	
512	1987.5	29.374	.900	45°		
513	868.5	9.791	- 300	67 5 ⁰	-	
514	961.75	11.423	. 350	1		
515	1055.00	13.055	400	† † –	035	
516	1241.50	16,319	500	╉┯╍┠┈╌		
517	1428.00	19.582	600		.034	
518	1521.25	21,214	650	++		
519	1614.50	22 846	700	}		
520	1707.75	22.040	750	┢╶╴╺┟╶╼┥	1.034	
521	1801.00	24.478	.750		.035	
522	1987.5	20.110	.800		†	
523	682.00		.900	67.5		
524	775 25	0.328	- 200	90		
525	821 88	0.075	.250	╞──╄──┧		
526	868 50	0.3/5	.275	┝──┼──╁		
527	915.12	9.791	.300	┝──┟──╎	 	
528	961 75	10.607	.325	┝━━┼━━╂		
529	1055 00	11.423	.350		.035	
530	1148 05	13.055	.400	┝━╺┈┟╴╌╸╉	.034	
531	1148.25	14.687	.450		.035	
532	1241.5	16.319	.500		.034	
522	1334.75	17.951	.550	V	.035	
222	1428.00	19.582	.600	an ^o	.03/	

Table VII External Tank Locations

*MEASURED FROM NUUSE

Table VII(Continued) (External Tank)

T/C NO.	× _T FS	× * * * * * * * * * * * * * * * * * * *	× L	θ	SKIN THICKNESS	REMARKS
534	1521.25	21.214	.650	90 ⁰	.034	
535	1614.50	22.846	.700	A	.034	
536	1707.75	24.478	.750		.035	
537	1801.00	26.110	.800		.035	
538	1894.25	27.742	.850	*	.034	· · · · · · · · · · · · · · · · · · ·
539	1987.50	29.374	.900	90 ⁰		
540	821.88	8.975	.275	112.5°	.035	
541	368.50	9.791	.300	4	4	
542	915.12	10.607	.325	L		
543	961.75	11.423	.350	ļ_ ļ		
544	1055.00	13.055	.400		T	
545	1148.25	14.687	.450	ļ	.035	
546	1241.50	16.319	.500	ļļ.	.034	
547	1334.75	17.951	.550		.035	
548	1428.00	19.582	.600		.034	
549	1521.25	21.214	.650		.034	
550	1614.50	22.846	.700		.034	
551	1707.75	24.478	.750		.035	
552	1801.00	26.110	.800			
553	· 1894.25	27.742	.850	V	+	L
554	1987.50	29.374	.900	112.50	.035	
555	1847.62	26.926	.825	123 ⁰	.034	
556	1894.25	27.742	.850		.035	
557	1940.88	28.558	.875		.034	
558	1987.50	29.374	.900		.035	
559	2034.12	30.190	.925	1	.035	
560	2099.40	31.332	.960	123 ⁰	.034	
561	915.12	10.607	.325	135 ⁰	.035	ļ
562	961.75	11.423	.350			1
563	1008.38	12.239	.375			
564	1055.00	13.055	.400		T	
565	1148.25	14.687	.450		.035	
566	1241.50	16.319	.500		.034	
567	1334.75	17.951	.550		.035	
568	1428.00	19.582	.600	•	.034	
569	1521.25	21.214	.650	135°	.034	1
	1		1	1	1	

*MEASURED FROM NUSE

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Table VII (Continued) (External Tank) -

T/C NO.	x _T FS	× ms	× L	θ	SKIN THICKNESS	REMARKS
570	1614.50	22.846	.700	135 [°]	.035	
571	170 7.7 5	24.478	.750	4	.034	
572	1801.00	26.110	.800		.035	
573	1894.25	27.742	.850		.034	
574	1987.50	29.374	.900	1	.035	
575	2052.78	30,576	.935	135 ⁰		
576	1055.00	13.055	.400	151	.035	
577	1101.62	13.871	.425	157	4	
<u>578</u>	1148.25	14.687	.450		•	
579	1194.88	15.503	.475		.035	
580	1241.50	16.319	.500		.034	
581	1334.75	17.951	.550		.035	
582	1428.00	19.582	.600		.034	
583	1521.25	21.214	.650		.034	
584	1614.50	22.846	.700		.035	
585	1707.75	24.478	.750		.035	
586	1801.00	26.110	.800		.035	
587	1894.25	27.742	.850	1	.034	
588	1987.50	29.374	.900	157	.034	
589	1101.62	13.871	.425	161	.035	
590	1241.50	16.319	.500	16 5°	.034	
591	1614.50	22.846	.700	165°	.035	
592	1987.50	29.374	.900	165°	.034	
593	1055.00	13.055	.400	16 5°	- 035	
594	309.00	0.000	0.000	180	.033	NOSE
595	318.32	0.163	.005	Å	.033	
596	327.65	0.326	.010		.034	
597	383.60	1.306	.040	*	.033	-
598	458.20	2.611	080	180 ⁰	.035	Y

*MEASURED FROM NOSE

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T/C NO.	× _T FS	* * ms	× L	θ	SKIN THICKNESS	REMARKS
599	588.75	4.896	.150	180 ⁰	.035	
600	682.00	6.528	.200		.034	
601	775.25	8.159	.250		.035	
602	868.50	9.791	.300			
603·	961.75	11. 423	.350			
604	1008.38	12.239	.375		.035	
605	1055.00	13.055	.400		.034	
606	1101.62	13.871	.425		4	
607	1148.25	14.687	.450			
608	1194.88	15,503	. 475		1	
609	1241.50	16.319	.500		.034	
610	1288.12	17.135	.525		.035	
611	1334.75	17.951	.550		.035	
612	1381.38	18.767	.575		.034	
613	1428.00	19.582	.600		A	
614	1474.62	20.398	.625			
615	1521.25	21.214	.650			
616	1567.88	22.030	.675		1	
617	1614.50	22.846	.700		.034	
618	1707.75	24.478	.750		.035	
619	1801.00	26.110	.800		.035	
620	1894.25	27.742	.850		.035	
621	1987.5	29.374	.900		.034	
622	2056.50	30.581	.937	1	.034	
623	2127.38	31.822	.975	180 [°]	.034	
624	458.20	2.611	.080	194°	.035	
625	587.75	4.896	.150	196°	.035	
626	868.50	9.791	. 300	196°	.035	

Table VII (CONTINUED (External Tank)

*MEASURED FROM NOSE

52 _.

	(External Tank)							
T/C NO.	x _T FS	× ms	× L	θ	SKIN THICKNESS	REMARKS		
627	1241.50	16.319	.500	196°	.034			
628	1614.50	22.846	.700	196°	.034			
629	1987.50	29.374	.900	197°	-034			
630	588.75	4.896	.150	208°	.033			
631	1055.00	13.055	.400	<u>+</u>	.034			
632	1428.00	19.582	.600	11-	-035	·		
633	1801.00	26.110	.800	++	.035			
634	2056.50	30.581		208	.035			
635	1055.00	13.055	.400	216°	.034			
636	1241.50	16.319	.500	216°	.034	•		
637	1614.50	22.846	.700	216°	.034			
<u>638</u>	933.78	10.934	.335	222.5°	.036			
639	1055.00	13.055	.400	2290	.034			
640	1428.00	19.582	.600	229°	.035			
641	1801.00	26.110	.800	229°	.035			
		<u> </u>						

Table VII (Concluded)

*MEASURED FROM NOSE

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Thermocouple No.	Channe 1	Thermocouple No.	Channe 1	Thermocouple No.	Channe1
1	1	48	26	Q1	51
2	2	50	27	92	57
3	3	52	28	03	52
4	4	54	29	93 04	53
6	5	56	30	95	54 EE
8	6	58	31	95	55 E C
10	7	59	32	97	50
12	8	60	33	98	57
14	9	61	34	99	50
16	10	62	35	100	59 60
18	11	63	36	101	61
20	12	64	37	102	62
22	13	65	38	104	63
24	14	66	39	105	64
26	15	67	40	111	65
28	16	68	41	115	66
30	17	69	42	116	67
32	18	71	43	134	68
34	19	72	44	135	69
36	20	74	45	150	70
38	21	79	46	155	70
40	22	84	47	156	77
42	23	87	48	157	73
44	24	88	49	158	73
46	25	90	50	159	75

Thermocouple Schedule No. X2

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$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Thermocouple No.	Channe 1	Thermocouple No.	Channe1	Thermocouple No.	Channe1
1612 188 27 215 52 162 3 189 28 216 53 163 4 190 29 218 54 164 5 191 30 219 55 165 6 192 31 220 56 166 7 193 32 221 57 167 8 196 33 222 58 168 9 197 34 229 59 169 10 198 35 230 60 170 11 199 36 232 61 171 12 200 37 234 62 172 13 201 38 246 63 173 14 202 39 247 64 174 15 203 40 274 65 175 16 204 41 275 66 176 17 205 42 276 67 177 18 206 43 277 68 178 19 207 44 278 69 179 20 208 45 279 70 180 21 209 46 280 71 181 22 210 47 281 72 182 23 211 48 282 73 183 24 212 49 283 74 <	160	1	187	26	214	51
1623 189 28 216 53 163 4 190 29 218 54 164 5 191 30 219 55 165 6 192 31 220 56 166 7 193 32 221 57 167 8 196 33 222 58 168 9 197 34 229 59 169 10 198 35 230 60 170 11 199 36 232 61 171 12 200 37 234 62 172 13 201 38 246 63 173 14 202 39 247 64 174 15 203 40 274 65 175 16 204 41 275 66 176 17 205 42 276 67 177 18 206 43 277 68 178 19 207 44 278 69 179 20 208 45 279 70 180 21 209 46 280 71 181 22 210 47 281 72 183 24 212 49 283 74 184 25 213 50 284 75	161	2	188	27	215	52
1634 190 29 218 54 164 5 191 30 219 55 165 6 192 31 220 56 166 7 193 32 221 57 167 8 196 33 222 58 168 9 197 34 229 59 169 10 198 35 230 60 170 11 199 36 232 61 171 12 200 37 234 62 172 13 201 38 246 63 173 14 202 39 247 64 174 15 203 40 274 65 175 16 204 41 275 66 176 17 205 42 276 67 177 18 206 433 277 68 178 19 207 44 278 69 179 20 208 45 279 70 180 21 209 46 280 71 181 22 210 47 281 72 183 24 212 49 283 74 184 25 213 50 284 75	162	3	189	28	216	53
16451913021955 165 61923122056 166 71933222157 167 81963322258 168 91973422959 169 101983523060 170 111993623261 171 122003723462 172 132013824663 173 142023924764 174 152034027465 175 162044127566 176 172054227667 177 182064327768 178 192074427869 179 202084527970 180 212094628071 181 222104728172 183 242124928374 184 252135028475	163	4	190	29	218	54
165 6 192 31 220 56 166 7 193 32 221 57 167 8 196 33 222 58 168 9 197 34 229 59 169 10 198 35 230 60 170 11 199 36 232 61 171 12 200 37 234 62 172 13 201 38 246 63 173 14 202 39 247 64 174 15 203 40 274 65 175 16 204 41 275 66 176 17 205 42 276 67 177 18 206 43 277 68 178 19 207 44 278 69 179 20 208 45 279 70 180 21 209 46 280 71 181 22 210 47 281 72 182 23 211 48 282 73 183 24 212 49 283 74 184 25 213 50 284 75	164	5	191	30	219	55
1667 193 32 221 57 167 8 196 333 222 58 168 9 197 34 229 59 169 10 198 35 230 60 170 11 199 36 232 61 171 12 200 37 234 62 172 13 201 38 246 63 173 14 202 39 247 64 174 15 203 40 274 65 175 16 204 41 275 66 176 17 205 42 276 67 177 18 206 43 277 68 178 19 207 44 278 69 179 20 208 45 279 70 180 21 209 46 280 71 181 22 210 47 281 72 182 23 211 48 282 73 183 24 212 49 283 74 184 25 213 50 284 75	165	6	192	31	220	56
1678 196 33 222 58 168 9 197 34 229 59 169 10 198 35 230 60 170 11 199 36 232 61 171 12 200 37 234 62 172 13 201 38 246 63 173 14 202 39 247 64 174 15 203 40 274 65 175 16 204 41 275 66 176 17 205 42 276 67 177 18 206 43 277 68 178 19 207 44 278 69 179 20 208 45 279 70 180 21 209 46 280 71 181 22 210 47 281 72 182 23 211 48 282 73 183 24 212 49 283 74 184 25 213 50 284 75	166	7	193	32	221	57
1689 197 34 229 59 169 10 198 35 230 60 170 11 199 36 232 61 171 12 200 37 234 62 172 13 201 38 246 63 173 14 202 39 247 64 174 15 203 40 274 65 175 16 204 41 275 66 176 17 205 42 276 67 177 18 206 43 277 68 178 19 207 44 278 69 179 20 208 45 279 70 180 21 209 46 280 71 181 22 210 47 281 72 182 23 211 48 282 73 183 24 212 49 283 74 184 25 213 50 284 75	167	8	196	33	222	58
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	168	9	197	34	229	59
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	169	10	198	35	2 30	60
	170	11	199	36	232	61
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	171	12	200	37	234	62
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	172	13	201	38	246	63
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	173	14	202	39	247	64
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	174	15	203	40	274	65
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	175	16	204	41	275	66
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	176	17	205	42	276	67
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	177	18	206	43	277	68
179202084527970180212094628071181222104728172182232114828273183242124928374184252135028475	178	19	207	44	278	69
180212094628071181222104728172182232114828273183242124928374184252135028475	179	20	208	45	279	70
181222104728172182232114828273183242124928374184252135028475	180	21	209	46	280	71
182232114828273183242124928374184252135028475	181	22	210	47	281	72
183242124928374184252135028475	182	23	211	48	282	73
184 25 213 50 284 75	183	24	212	49	283	74
	184	25	213	50	284	75

Thermocouple No.	Channe l	Thermocouple No.	Channe1	Thermocouple No.	Channel
5	1	57	26	119	51
7	2	70	27	120	52
9	3	73	28	121	53
11	4	75	29	122	54
15	5	76	30	123	55
17	6	77	31	124	56
19	7	78	32	125	57
21	8	80	33	126	58
23	9	81	34	127	59
25	10	82	35	128	60
27	11	83	36	129	61
29	12	85	37	130	62
31	13	86	38	131	63
33	14	89	39	1 32	64
35	15	103	40	133	65
37	16	106	41	136	66
39	17	107	42	137	67
41	18	108	43	138	68
43	19	109	44	1 39	6 9
45	20	110	45	140	70
47	21	112	46	141	71
49	22	113	47	142	72
51	23	114	48	143	73
53	24	117	49	144	74
55	25	118	50	145	75

Thermocouple No.	Channe1	Thermocouple No.	Channe 1	Thermocouple No.	Channe1
146	1	239	26	266	51
147	2	240	27	267	52
148	3	241	28	268	53
149	4	242	29	269	54
151	5	243	30	270	55
152	6	244	31	271	56
153	7	245	32	272	57
154	8	248	33	273	58
185	9	2 49	34	286	59
186	10	250	35	287	60
194	11	251	36	501	61
195	12	252	37	502	62
217	13	253	38	503	63
223	14	254	39	504	64
224	15	255	40	505	65
225	16	256	41	506	66
226	17	257	42	507	67
227	18	258	43	508	68
228	19	259	44	509	69
231	20	260	45	510	70
233	21	261	46	511	71
235	22	262	47	512	72
236	23	263	48	513	73
237	24	264	49	514	73
238	25	265	50	515	75

Thermocouple No.	Channe1	Thermocouple No.	Channe1	Thermocouple No.	Channel
516	1	541	26	566	51
517	2	542	27	567	52
518	3	542	28	560	53
519	4	.540	29	500	54
520	5	545	30	509	55
521	6	546	31	570	56
522	7	540	32	571	57
523	8	548	33	572	58
524	9	540	34	575	59
525	10	550	35	575	60
526	11	550	36	576	61
527	12	552	37	570	62
528	13	553	38	578	63
529	14	554	39	570	64
530	15	555	40	580	65
531	16	556	41	581	66
532	17	557	42	582	67
533	18	558	43	582	68
534	19	559	44	584	69
535	20	560	45	585	70
536	21	561	46	586	· 71
537	22	562	47	587	72
5 3 8	23	563	48	588	72
53 9	24	564	49	589	74
540	25	565	50	590	75

501	1 2	616	26		
591	2		20	752	51
592	-	617	27	750	52
593	3	618	28	792	52
594	4	619	29	636	54
595	5	620	30	637	55
596	6	621	31	638	56
597	7	622	32	639	57
59 8	8	623	33	640	58
599	9	624	34	641	59
600	10	625	35	Open	60
601	11	626	36	701	61
602	12	627	37	702	62
603	13	628	38	703	63
604	14	629	39	704	64
605	15	630	40	705	65
606	16	631	41	708	66
607	17	632	42	709	67
608	18	633	43	710	68
609	19	634	44	711	69
610	20	635	45	714	70
611	21	706	46	715	70 71
612	22	707	47	716	71
613	23	713	48	717	72
614	24	744	49	718	74
615	25	749	50	719	75



Thermoc ouple No.	Channe1	Thermocouple No.	Channe 1	Thermocouple No.	Channe]
720	1	753	26	784	51
721	2	754	27	785	52
722	3	755	28	787	53
723	4	756	29	788	54
724	5	757	30	789	55
725	6	758	31	790	56
726	7	760	32	791	57
728	8	762	33	793	58
729	9	766	34	797	59
730	10	767	35	798	60
731	11	768	36	712	61
732	12	769	37	727	62
733	13	770	38	746	63
734	14	771	39	748	64
735	15	772	40	750	65
736	16	773	41	751	66
737	17	774	42	761	67
738	18	775	43	763	68
739	19	776	44	764	6 9
740	20	777	45	765	70
741	21	778	46	780	71
742	22	779	47	786	72
743	23	781	48	794	73
745	24	782	49	795	74
747	25	783	50	796	75

Thermocouple Schedule No. X8

Thermocouple No.	Channe 1	Thermocouple No.	Channe 1	Thermocouple No.	Channe1
501 502 503 504 505 506 507 508 509 510 511 512 513 514 515 516 517 518 519 520 521 522 523 524 525	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25	526 527 528 529 530 531 532 533 534 535 536 537 538 539 540 541 542 543 544 545 544 545 546 547 548 549	26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49	551 552 553 554 555 556 557 558 559 560 561 562 563 564 565 566 567 568 569 569 570 571 572 573 574	51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 67 70 71 72 73 74
	~~	000	50	575	75

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Thermocouple No.	Channel	Thermocouple No.	Channe1	Thermocouple No.	Channel :
576	1	601	26	626	51
577	2	602	27	627	52 +
578	3	603	28	628	53 ⁱ
579	4	604	29	629	54
580	5	605	30	630	55
581	6	606	31	631	56
582	7	607	32	632	57
583	8	608	33	633	58
584	9	609	34	634	59
585	10	610	35	635	60
586	11	611	36	636	61
587	12	612	37	637	62
588	13	613	38	638	63 ·
589	14	614	39	639	64
590	15	615	40	640	65
591	16	616	41	641	66
592	17	617	42	0pen	67
593	18	618	43	Open	68
594	19	619	44	Open	6 9
595	20	620	45	0pen	70
596	21	621	46	Onen	71
597	22	622	47	O pen	72
598	23	623	48	Öpen	73
599	24	624	49	Open	74
600	25	625	50	Open	75

Thermocouple No.	Channe l	Thermocouple No.	Channe1	Thermocouple No.	Channe1
701	1	731	26	768	51
702	2	732	27	760	52
703	3	733	28	703	53
704	4	734	29	770	54
705	5	735	30	772	55
708	6	736	31	773	56
709	7	737	32	77/	57
710	8	738	33	775	58
711	9	739	34	776	59
714	10	740	35	777	60
715	11	741	36	778	61
716	12	742	37	779	62
717	13	743	38	781	63
718	14	745	39	782	64
719	15	74 7	40	783	65
720	16	753	41	784	66
721	17	754	42	785	67
/22	18	75 5	43	78 7	68
/23	19	756	44	788	69
/24	20	757	45	789	70
725	21	758	46	7 9 0	71
/26	22	760	47	791	72
/28	23	76 2	48	793	73
/29	24	766	49	79 <u>.</u> 7	74
/ 30	25	767	50	798	75

Thermocouple No.	Channel	Thermocouple No.	Channe1	Thermocouple No.	Channe1
37 39 41 43 45 47 49	1 2 3 4 5 6 7	106 107 108 109 110 129 130	26 27 28 29 30 31 32	521 522 523 524 525 526 527	51 52 53 54 55 56 57
51 53 Open Open 70 73 75	8 9 10 11 12 13 14	131 132 133 136 137 138 139	33 34 35 36 37 38 39	528 529 530 531 532 533 534	58 59 60 61 62 63 64
76 77 78 80 81 82 83	15 16 17 18 19 20 21	140 141 142 143 144 145	40 41 42 43 44 45 46	535 536 537 538 539 540	65 66 67 68 6 9 70
85 86 89 103	22 23 24 25	516 517 518 519 520	40 47 48 49 50	541 542 543 544 545	72 73 74 75

Thermocouple Schedule No. X12

Thermocouple No.	Channe1	Thermocouple No.	Channe1	Thermocouple No.	Channe1
146	1	239	26	266	51
147	2	240	27	200	51
148	3	241	28	20/	52
149	4	242	29	268	53
151	5	242	30	269	54
152	6	243	31	270	55
153	7	244	32	271	50
154	8	245	33	272	57
185	9	240	34	2/3	58
186	10	249	35	286	59
194	11	251	36	287	60
195	12	252	37	/01	61
217	13	252	38	702	62
223	14	255	30	703	63
224	15	204	40	704	64
225	16	200	40	705	65
226	17	200	41	708	66
227	18	257	42	709	67
228	19	200	43	710	68
231	20	209	44 AE	711	69
233	21	200	45	714	70
235	22	201	40	715	71
236	23	202	47	716	. 72
237	24	203	48	717	73
238	24	204	49	718	74
200	20	265	50	719	75

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Thermocouple No.	Channe1	Thermocouple No.	Channe1	Thermocouple No.	Channe1
546 547 548 549 550 551 552 553 554 555 556 557 558 559 560 576 577 578 579 580 581 582 583 584	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	586 587 588 589 590 591 592 593 594 595 596 597 598 599 600 601 602 603 604 605 606 607 608 609	26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49	611 612 613 614 615 616 617 618 619 620 621 622 623 624 625 626 627 628 629 630 631 632 633 634	51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74
585	25	610	50	635	75

Run #	$\frac{\text{Re}_{\infty}/\text{ft}}{\text{x } 10^6}$	PT (psi)	TT (°R)	HT (BTU/1b _m)
3 5 7	1.4909 1.4111	165.58 141.88	1581.2 1487.5	390.90 366.19
8 9	1.3945	120.04	1348.1 1327.2	329.90 324.51
10 11	1.4702	122.81	1322.1	323.19 319.30
12 13	4.7266	405.72	1298.8	317.22 329.94
14 15	4.9672 4.9723	403.68 405.35	1302.8	318.23 318.89
16 17	4.9533 5.0060	406.35 405.69	1310.5 1300.5	320.21 317.64
18 19 20	5.0979 1.4998	404.88 122.63	1284.1 1307.7	313.43 319.50
20 21 22	1.5374 1.5232 1.4696	121.33 122.04	1278.9 1291.2	312.11 315.26
23 24	1.6062	119.90	1320.8 1234.9 1289 3	322.87 300.85 314.76
25 26	1.5757 4.9504	119.48 405.67	1247.1	303.98 319.98
27 28 20	4.9770 4.9574	406.03 405.59	1305.9 1308.3	319.04 319.64
30	4.9770 5.0055 5.0063	406.32 406.22	1306.5 1301.6	319.19 317.93
32 33	5.0389 5.0961	406.71 405.17	1297.2	318.01 316.80
34 35	4.9856 5.0750	405.20 405.72	1302.8	318.24 314.80
36 37 29	5.0306 5.1486	406.14 401.85	1297.4 1270.1	316.85 309.85
39 40	5.0550 5.0452 1.6365	406.03 406.22 130.40	1293.2 1295.2 1286.8	315.78 316.28 314.12

TABLE IX. RUN NUMBER/TUNNEL CONDITION SUMMARY
TABLE IX. (Concluded)

Run #	Re _∞ /ft <u>x 10</u> 6	PT (psi)	TT (°R)	HT (BTU/15m)
42	1.5224	122.73	1296.2	316.55
43	1.5160	123.06	1301.8	317.99
44	5.1123	406.40	1284.8	313.62
45	5.0361	406.22	1296.7	316.66
46	5.0028	405.88	1301.4	317.87
47	5.3924	404.93	1239.5	302.03
48	1.5328	123.06	1292.8	315.67
49	1.5263	122.69	1293.9	315.94
50	1.4308	118.69	1319.7	322.57
51	1.4952	121.64	1303.6	318.44
52	5.0533	405.46	1292.4	315.56
53	5.0265	406.40	1298.6	317.15
54	5.1372	405.09	1278.3	311.95
55	4.9871	402.92	1298.0	317.00
56	1.5132	121.59	1293.6	315.86
57	1.5033	121.59	1298.9	317.23
58	5.0864	405.30	1286.8	314.12
59	5.0929	405.30	1285.7	313.85
60	5.0577	405.30	1291.3	315.29
61	5.0730	405.64	1289.6	314.84
62	1.5553	137.52	1373.4	336.46
63	1.5070	123.06	1306.7	319.24
64	1.5093	122.73	1303.3	318.37
65	5.0737	406.22	1290.6	315.10
66	5.1122	406.32	1284.7	313.59
68	1.4966	120.98	1298.4	317.12
69	5.2179	406.16	1268.0	309. 30
70	4.9056	407.29	1320.4	322.76
71	5.0011	406.76	1303.5	318.40
72	4.9871	403.86	1299.9	317.49
73	5.0038	405.88	1301.2	317.83
74	5.0508	406.74	1295.3	316.32
76	5.0175	406.92	1301.1	317.80
77	5.0556	410.46	1302.0	318.02
78	5.0607	406.58	1293.4	315.83
79	4.9699	406.92	1308.9	319.81

INSTRUMENTATION LOCATION SYSTEM

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Figure 1. - Concluded.



a. Assumed Plotted Wing Leading-Edge Clusters B & C T/C Locations, (Used for Plotted and Tabulated Data Presentations)

Figure 2. - Model instrumentation.



Figure 2. - Continued.



Figure 2. - Continued.

Figure 2. - Continued.

d. External Tank T/C Locations (Locations Around Plumbing Lines) Top View

TOP VIEW



EXTERNAL TANK THERMOCOUPLE LOCATIONS (LOCATIONS AROUND PLUMBING ONLY) MODEL 22-OTS





Figure 3. - Model photographs.

a. Mated Launch Configuration Installation



Figure 3. - Continued.



c. Mated Configuration Boundary Layer Trips

Figure 3. - Continued.



Figure 3. - Concluded.

d. SRB Boundary Layer Trips

DATA FIGURES

SRB DATA EXTERNAL TANK DATA (SEE VOLUME I) ORBITER DATA (SEE VOLUME III)

DATA SET SYMBCL (REISI4) (REISI4)

CONFIGURATION DESCRIPTION ARC 3.5-178 H4 598 ARC 3.5-178 H4 598 ARC 3.5-178 H4 598 ARC 3.5-178 H4 598













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COVFIGURATION RESCRIPTION C 3.5-178 1H3 ST8 C 3.5-178 1H3 ST8 C 3.5-178 1H3 ST8 C 3.5-178 1H3 ST8 ARC 3.5-178 | ARC 3.5-178 | ARC 3.5-178 | DATA SET SYNBCL (REIS14) (REIS14) (REIS14)

BOOSTER BOOSTER BOOSTER BOOSTER 888 888













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CONFIGURATION DESCRIPTION ARC 3.5-178 H43 578 ARC 3.5-178 H43 578 ARC 3.5-178 H43 578 ARC 3.5-178 H43 578

























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SYMBIL CONFIGURATION DESCRIPTION ALPHA RETA RALL Rec 3.5-178 H13 SRB SQLID B005TER .000 .000 1.500 ARC 3.5-178 H13 SRB SQLID B005TER .000 .000 1.500 ARC 3.5-178 H13 SRB SQLID B005TER .000 .000 1.500

DATA SET 9 (REIS14) (AEIS14) (BEIS14) (BEIS14)

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TITTT 683 360 PAGE 320 280 ---- 888 885 ----120 160 200 240 RADIAL LOCATION . PHI . DEGREES FIG. 7 SOLID ROCKET BOOSTER - SRB ALONE (UNDISTURBED) H = 5.300 ×/L = .500 ×1 8000 8000 MAN 8000 ф SOLID BOOSTER SOLID BOOSTER SOLID BOOSTER CONFIGURATION DESCRIPTION ARC 3.5-178 [H3 548 ARC 3.5-178 [H3 548 ARC 3.5-178 [H3 548 ARC 3.5-178 [H3 548 80 **4** DATA SET SYMBL (REISI4) (AEISI4) (BEISI4) E -010-.1001 <u>.</u> MACH LOCAL TO STAGNATION HEAT TRANSFER COEFFICIENT RATIO . H/HREF



CONFIGURATION DESCRIPTION ARC 3.5-178 1H3 S78 ARC 3.5-178 1H3 S78 ARC 3.5-178 1H3 S78 ARC 3.5-178 1H3 S78 CMIA SET SYMBIL (REISI4) (AEISI4) (BEISI4)

1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000

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COVFIGURATION DESCRIPTION ARC 3.5-178 1H3 SR8 ARC 3.5-178 1H3 SR8 ARC 3.5-178 1H3 SR8 ARC 3.5-178 1H3 SR8 INTA SET SYNBIL (REISI4) (REISI4) (REISI4)

SOLID BOOSTER SOLID BOOSTER SOLID BOOSTER SOLID BOOSTER

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320 280 0 θÐ 120 160 200 240 RADIAL LOCATION . PHI . DEGREES FIG. 7 SOLID ROCKET BOOSTER - SRB ALONE (UNDISTURBED) 1111 ¢¢ Œ 80. 40 1001 -01C MACH LOCAL TO STAGNATION HEAT TRANSFER COEFFICIENT RATIO . HUHREF

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CONFIGURATION DESCRIPTION ARC 3.5-178 1H3 578 ARC 3.5-178 1H3 578 ARC 3.5-178 1H3 578 ARC 3.5-178 1H3 578 DATA SET SYNBOL (REISIS) (REISIS)

MH 8000 BCCSTER BCCSTER BCCSTER BCCSTER **8**888



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COVFIGURATION DESCRIPTION ARC 3.5-178 1H3 SR8 ARC 3.5-178 1H3 SR8 ARC 3.5-178 1H3 SR8

1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000

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CONFIGURATION D ARC 3.5-178 1H3 S ARC 3.5-178 1H3 S ARC 3.5-178 1H3 S DATA SET SYNBUL (REISIS) (REISIS)















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FIG. 7 SOLID ROCKET BOOSTER - SRB ALONE (UNDISTURBED) + = 5.300 ×/L = .800

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1.4 733 LONGITUDINAL LOCATION . X/L . FRACTION OF BODY LENGTH PAGE ----8855 8855 ساب براسیدار 0E K1X 0000 0000 FIG. 7 SOLID ROCKET BOOSTER - SRB ALONE (UNDISTURBED) ¥ 8888 SQL ID BOOSTER SQL ID BOOSTER SQL ID BOOSTER ողոտրա ատեսովուս = 180.000 CONFIGURATION DESCRIPTION ARC 3.5-178 1H3 SR8 (TRIPS) 0EF The second s سسما Iнд 5 1 • 00 լադուդուդ 5.300 .10 II LOCAL TO STAGNATION HEAT TRANSFER COEFFICIENT RATIO . HVHREF

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4 735 E PAGE LONGITUDINAL LOCATION . X/L . FRACTION OF BODY LENGTH -PO HAVHT 1.000 1.000 1.000 1.000 1.000 • QUE OF NR ----SRB ALONE (UNDISTURBED) ¥1 8000 8000 Transformer 1 ¥ 888 ռոյությունությունությունություն SOLID BOOSTER SOLID BOOSTER SOLID BOOSTER SOLID BOOSTER ROCKET BOOSTER -= 225.000 ¢⊕-COVFIGURATION DESCRIPTION ARC 3.5-178 H43 588 (TRIPS) 1 •000 բաղուղուղուղուղուղ IHd - 2 FIG. 7 SOLID 5.300 0 + + DATA SET SYNBUL (REIS17) (REIS17) (REIS17) (REIS17) .10 11 MACH LOCAL TO STAGNATION HEAT TRANSFER COEFFICIENT RATIO . H/HREF











HVH 1.000 850 850 850 Å ----×138 8000 8000 ¥ 8888 SQLID BOOSTER SQLID BOOSTER SQLID BOOSTER COVEIGURATION DESCRIPTION ARC 3.5-178 H43 SAB (TRIPS) ARC 3.5-178 H43 SAB (TRIPS) ARC 3.5-178 H43 SAB (TRIPS) ARC 3.5-178 H43 SAB (TRIPS)

DATA SET SYNBO. (REISI7) (REISI7)















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360 320 1H/WHH 00001 00080 նունունունունունունուն 280 N STER - SRB ALONE (UNDISTURBED) ×1 8000 8000 ամամամանուն սահասկաս E FIG. 7 SOLID ROCKET BOOSTER -E .130 E 1 •00 բաղողողողողող 80 4 CALL SET SWARL (REISI7) (REISI7) (REISI7) .10 ŝ o, LOCAL TO STAGNATION HEAT TRANSFER COEFFICIENT RATIO . HVHREF

M 888 SOLID BOOSTER SOLID BOOSTER SOLID BOOSTER SOLID BOOSTER CONFIGURATION DESCRIPTION ARC 3.5-178 IH3 SR8 (TRIPS) ARC 3.5-178 IH3 SR8 (TRIPS) ARC 3.5-178 IH3 SR8 (TRIPS) ARC 3.5-178 IH3 SR8 (TRIPS)

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×1 8000 8000 AF 8886 SOLID BOOSTER SOLID BOOSTER SOLID BOOSTER SOLID BOOSTER I DESCRIPTION SRB (TRIPS) SRB (TRIPS) SRB (TRIPS)





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4 771 1111 Ē LONGI TUDINAL LOCATION . X/L . FRACTION OF BODY LENGTH PAGE Ē Ē 14/44 1.000 1.000 850 00 55550 5000 5000 5000 5000 ×1 80000 FIG. 7 SOLID ROCKET BOOSTER - SRB ALONE (UNDISTURBED) ¥⁴ 8888 SOLID BOOSTER SOLID BOOSTER SOLID BOOSTER ակավագեսվակախակոսիստ -.2 _____0__.2 Ð = 225,000 ØE CONFIGURATION DESCRIPTION ARC 3.5-178 [H3 548 (1R1PS) ARC 3.5-178 [H3 548 (TR1PS) ARC 3.5-178 [H3 548 (TR1PS) ARC 3.5-178 [H3 548 (TR1PS) IHd 5.300 1 • O() քողոու - 4 - 4 DATA SET SYMBCL (REISI8) (REISI8) (BEISI8) • 1<u>c</u> MACH = LOCAL TO STAGNATION HEAT TRANSFER COEFFICIENT RATIO . H/HREF

















1 779 360 PAGE լույսու Ê 320 THE HAVHT 1.000 9000 9000 9000 9000 RADIAL LOCATION • PHI • DEGREES 2000 2000 2000 2000 ᢒ⊟ FIG. 7 SOLID ROCKET BOOSTER - SRB ALONE (UNDISTURBED) H = 5.300 ×/L = .025 ×1 8000 8000 AL 40000 . . SOL ID BOOSYER SOL ID BOOSYER SOL ID BOOSYER SOL ID BOOSYER 1 • 00) բակավոտիակակակականունուն CESCRIPTION SRB (TRIPS) SRB (TRIPS) SRB (TRIPS) SRB (TRIPS) -fh CONFIGURATION D ARC 3.5-178 1H3 5 ARC 3.5-178 1H3 5 ARC 3.5-178 1H3 5 ARC 3.5-178 1H3 5 80. ne pres mint .10 0. MACH =

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COVFIGURATION DESCRIPTION ARC 3.5-178 1H3 S48 (TRIPS) ARC 3.5-178 1H3 S48 (TRIPS) ARC 3.5-178 1H3 S48 (TRIPS) ARC 3.5-178 1H3 S48 (TRIPS)

DATA SET ((REIS18) (AEIS18) (BEIS18)

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FIG. 7 SOLID ROCKET BOOSTER - SRB ALONE (UNDISTURBED)

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4 1111111 803 ŧ PAGE LONGITUDINAL LOCATION . X/L . FRACTION OF BODY LENGTH ② 印 TH AN 1 Q 84 5.000 5.000 ողոութո FIG. 7 SOLID ROCKET BOOSTER - SRB ALONE (UNDISTURBED) H = 5.300 PHI = 90.000 ×1 8088 ահահա ¥888 8888 հարարություն TITTI SOL 10 BOOSTER SOL 10 BOOSTER SOL 10 BOOSTER SOL 10 BOOSTER E - muluu COVFIGURATION DESCRIPTION ARC 3.5-178 1H3 SR8 ARC 3.5-178 1H3 SR8 ARC 3.5-178 1H3 SR8 ARC 3.5-178 1H3 SR8 لسياسيهم سلسشسليسا - .2 1 • 000 pmmm Ē. MACH LOCAL TO STAGNATION HEAT TRANSFER COEFFICIENT RATIO . HVHREF









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3 815 F 360 111 PAGE 320 1H/WH 00001 0000 0000 280 ورون 8000 8000 8000 റ 120 160 200 240 RADIAL LOCATION • PHI • DEGREES FIG. 7 SOLID ROCKET BOOSTER - SRB ALONE (UNDISTURBED) ×1 8000 8000 E Ē Ē A 888 888 888 888 888 888 حصاب ساد ساد سار سمار سمار سمار معارد مواد بيدار ديم SOLID BOOSTER SOLID BOOSTER SOLID BOOSTER .025 CONFIGURATION DESCRIPTION ARC 3.5-178 H3 548 ARC 3.5-178 H3 548 ARC 3.5-178 H3 548 ARC 3.5-178 H3 548 п A b Ð بمقاددها بمباريس ليسما 18 ХL 5.300 **. 4** 1.0C mm 10. RATA SET SYNBO-(REISI6) (REISI6) (BEISI6) .1C 11 MACH LOCAL TO STAGNATION HEAT TRANSFER COEFFICIENT RATIO . H/HREF




































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4 841 ۰. LONGITUDINAL LOCATION . X/L . FRACTION OF BODY LENGTH PAGE HV/HT 1.000 1.000 1.000 1.000 1.000 1.000 1.000 COCOT. FIG. 8 SOLID ROCKET BOOSTER - INTEGRATED VEHICLE (INTERFERENCE ¥ ----<u>s</u>to 040 ×1 8888 ¥ 888 3-1 BOOSTER BOOSTER BOOSTER BOOSTER 200 = 180.000 DESCRIPTION S+1+0 S+1+0 CONFIGURATION D ARC 3.5-178 1H3 0 ARC 3.5-178 1H3 0 ARC 3.5-178 1H3 0 ARC 3.5-178 1H3 0 Iнд - 5 5.300 .001 DATA SET SYNBOL (REISOI) (REISOI) (REISOI) 010 .10<u>C</u> 11 MACH FOCAL TO STAGNATION HEAT TRANSFER COEFFICIENT RATIO . HVHREF















TITTE 849 360 3 PAGE 320 111 FIG. 8 SOLID ROCKET BOOSTER - INTEGRATED VEHICLE (INTERFERENCE) NN -----×1 8888 8888 ¥8888 BOOSTER BOOSTER BOOSTER BOOSTER 200 .002 COVFIGURATION DESCRIPTION ARC 3.5-178 1H3 0+1+5 ARC 3.5-178 1H3 0+1+5 ARC 3.5-178 1H3 0+1+5 11 XL 5.300 1111 INTA SET SYMBO (REISOL) (REISOL) (BEISOL) .010 1001 H MACH LOCAL TO STAGNATION HEAT TRANSFER COEFFICIENT RATIO . H/HREF



851 360 PAGE 320 Ξ FIG. 8 SOLID ROCKET BOOSTER - INTEGRATED VEHICLE (INTERFERENCE) HVHI 90001 90001 RADIAL LOCATION . PHI . DEGREES ----8885 8885 ×1 8888 ¥ 888 1 BOOSTER BOOSTER BOOSTER **888** .050 ł COVE IGURATION DESCRIPTION CC 3.5-178 H43 0+1+5 CC 3.5-178 H43 0+1+5 CC 3.5-178 H43 0+1+5 CC 3.5-178 H43 0+1+5 11 80. X ARC 3.5-178 1 ARC 3.5-178 1 ARC 3.5-178 1 1111 5,300 **4**0 1 DATA SET SYNBUL .010 .100 8 ŝ MACH = FOCAL TO STAGNATION HEAT TRANSFER COEFFICIENT RATIO . H/HREF









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4 881 LONGITUDINAL LOCATION . X/L . FRACTION OF BODY LENGTH PAGE FIG. 8 SOLID ROCKET BOOSTER - INTEGRATED VEHICLE (INTERFERENCE) **O** 030 ×1 8000 8000 ¥ 8888 BOOSTER BOOSTER BOOSTER BOOSTER **8**888 = 270.000 400000 CONFIGURATION DESCRIPTION ARC 3.5-178 1H3 0+1+5 ARC 3.5-178 1H3 0+1+5 ARC 3.5-178 1H3 0+1+5 Ιнд 5 5.300 .001 fund INTA SET SYNBO (REISO2) (REISO2) (REISO2) .100 .010 II MACH LOCAL TO STAGNATION HEAT TRANSFER COEFFICIENT RATIO . H/HREF





















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1.000 <mark>բարողություրություրություրություրություրություրություրություն է հերանություն է հերանություն է հերանություն է հե</mark> 3 895 360 PAGE 320 FIG. 8 SOLID ROCKET BOOSTER - INTEGRATED VEHICLE (INTERFERENCE) 1 بساساس<u>،</u> 280 8000 8000 8000 8000 120 160 200 240 RADIAL LOCATION • PHI • DEGREES ×1 8.889 8.889 **ত**্র Э ł 20 M 8999 Ì -----Ì $\|$ I SQL ID BOOSTER SQL ID BOOSTER SQL ID BOOSTER .400 I ł CONFIGURATION DESCRIPTION ARC 3.5-178 1H3 0+1+5 ARC 3.5-178 1H3 0+1+5 ARC 3.5-178 1H3 0+1+5 Ţ 11 80 ХL 5.300 1111 . 4 Ē DATA SET SYNBO. (REISO2) (REISO2) (REISO2) 1001 .01C 20 II MACH LOCAL TO STAGNATION HEAT TRANSFER COFFFICIENT RATIO . H/HREF








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FIG. 8 SOLID ROCKET BOOSTER - INTEGRATED VEHICLE (INTERFERENCE) - 11 ХL 5.300

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COVFIGURATION DESCRIPTION ARC 3.5-178 H3 0+1+5 ARC 3.5-178 H3 0+1+5 ARC 3.5-178 H3 0+1+5





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inn i A 360 1111 իստիստիսոսիսոս 320 1.000 1.000 1.000 1.000 1.000 FIG. 8 SOLID ROCKET BOOSTER - INTEGRATED VEHICLE (INTERFERENCE) 1.20 1.60 200 240 280 RADIAL LOCATION . PHI . DEGREES ¥ ----Я T V 138 ł Ì H 8888 T ł BOOSTER BOOSTER BOOSTER BOOSTER -11 ||8888 9998 9998 11 COVEIGURATION DESCRIPTION ARC 3.5-178 H43 0+1+5 (TRIFS) ARC 3.5-178 H43 0+1+5 (TRIFS) ARC 3.5-178 H43 0+1+5 (TRIFS) 111 1 Ì Ø, 80. 40 E 010 .10C 8 FOCAL TO STAGNATION HEAT TRANSFER COEFFICIENT RATIO . H/HREF

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1.000) ըստություններին երեններին անտեսերություններին ուսերություններին անտեսերություններին անտեսերություններին 933 ĺ 360 PAGE 320 1.000 1.000 1.000 1.000 1.000 1.000 FIG. 8 SOLID ROCKET BOOSTER - INTEGRATED VEHICLE (INTERFERENCE) 280 Å ----RADIAL LOCATION . PHI . DEGREES × 8000 ¥ 8888 L. SOLID BOOSTER SOLID BOOSTER SOLID BOOSTER SOLID BOOSTER .650 ì 1 DESCRIPTION 0+T+S (TRIPS) 0+T+S (TRIPS) 0+T+S (TRIPS) Ħ COVFIGURATION D ARC 3.5-178 1H3 0 ARC 3.5-178 1H3 0 ARC 3.5-178 1H3 0 ARC 3.5-178 1H3 0 80. ХL 5.300 40 mi 100. .10C 0 U 11 MACH LOCAL TO STAGNATION HEAT TRANSFER COEFFICIENT RATIO . HAHREF




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1 360 PAGE 320 HAVHT 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 FIG. 8 SOLID ROCKET BOOSTER - INTEGRATED VEHICLE (INTERFERENCE) 280 5000 5000 5000 5000 120 160 200 240 RADIAL LOCATION . PHI . DEGREES 3 ×130 0000 0000 ¥ 8888 SOL ID BOOSTER SOL ID BOOSTER SOL ID BOOSTER SOL ID BOOSTER .780 CONFIGURATION DESCRIPTION ARC 3.5-178 H43 0+1+5 (TRIPS) ARC 3.5-178 H43 0+1+5 (TRIPS) ARC 3.5-178 H43 0+1+5 (TRIPS) . 11 80. X 5.300 4 .100 .010 0. MACH = LOCAL TO STAGNATION HEAT TRANSFER COEFFICIENT RATIO . H/HREF







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COVFIGURATION DESCRIPTION ARC 3.5-178 H43 0+1+5 ARC 3.5-178 H43 0+1+5 ARC 3.5-178 H43 0+1+5

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IIIII 395 360 PAGE 320 FIG. 8: SOLID ROCKET BOOSTER - INTEGRATED VEHICLE (INTERFERENCE) 120 160 200 240 280 RADIAL LOCATION . PHI . DEGREES Ì œ 861A 5-5-000 5-0000 5-0000 5-0000 ¥8888 **SQL 10 BOOSTER SQL 10 BOOSTER SQL 10 BOOSTER** .130 CONFIGURATION DESCRIPTION ARC 3.5-178 1H3 0+1+5 ARC 3.5-178 1H3 0+1+5 ARC 3.5-178 1H3 0+1+5 11 T 80. х۲ 5,300 6 .100 -010-.00 łł MACH LOCAL TO STAGNATION HEAT TRANSFER COEFFICIENT RATIO . HARREF

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E PAGE 1003 360 320 11/1/11 000.1 0008.0 FIG. 8 SOLID ROCKET BOOSTER - INTEGRATED VEHICLE (INTERFERENCE) . 120 160 200 240 280 RADIAL LOCATION . PHI . DEGREES 50000 50000 50000 1111 5.000 5.000 5.000 5.000 22 ¥ 8888 SQL 10 BOOSTER SQL 10 BOOSTER SQL 10 BOOSTER SQL 10 BOOSTER .650 CONFIGURATION DESCRIPTION ARC 3.5-178 1H3 0+1+5 ARC 3.5-178 1H3 0+1+5 ARC 3.5-178 1H3 0+1+5 ARC 3.5-178 1H3 0+1+5 II 80 ХГ 5.300 1 L L **4**. 1001. .010 8. lł MACH LOCAL TO STAGNATION HEAT TRANSFER COEFFICIENT RATIO . HARREF

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4 1019 PAGE LONGITUDINAL LOCATION , X/L , FRACTION OF BODY LENGTH QCI O FIG. 8 SOLID ROCKET BOOSTER - INTEGRATED VEHICLE (INTERFERENCE) ×1 8888 8888 SOLID BOOSTER SOLID BOOSTER SOLID BOOSTER SOLID BOOSTER = 240.000 CONFIGURATION DESCRIPTION ARC 3.5-178 1H3 0+1+5 ARC 3.5-178 1H3 0+1+5 ARC 3.5-178 1H3 0+1+5 يسابيت ايشرا يسابين HH 2 5.300 ₫4. .1001 100. 01Ú 11 MACH LOCAL TO STAGNATION HEAT TRANSFER COEFFICIENT RATIO . HVHREF







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COVFIGURATION DESCRIPTION ARC 3.5-178 1H3 0+1+5 ARC 3.5-178 1H3 0+1+5 ARC 3.5-178 1H3 0+1+5

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FIG. 8 SOLID ROCKET BOOSTER - INTEGRATED VEHICLE (INTERFERENCE) .780 11 ХL 5.300

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4 ٠. 1059 E \sim PAGE FIG. 9 SOLID ROCKET BOOSTER - INTERFERENCE TO UNDISTURFED RATIO H = 5.300 PHI = 270 000 E Î ПП TH 200000 08 TI 11 1 TTT 7 20000 20000 20000 20000 TT T TT \prod × 8888 ТГ ¥ 8888 Π Π Ш BOOSTER BOOSTER BOOSTER BOOSTER BOOSTER Ì 2222 C C (TRIPS) (TRIPS) DESCRIPTION **I**₫Ų S+1+0 S+1+0 S+1+0 1111 111111111 포포포포 CONFIGURATION and and ARC 3.5-178 ARC 3.5-178 ARC 3.5-178 ARC 3.5-178 11 **WALLER** Π 1 Ţ 1.000 .100 .01C 00 (EEIS14) (EEIS15) (EEIS17) (EEIS17) DATA SET ANTERFERENCE TO UNDISTURBED HEAT TRANSFER COEFFICIENT RATIO **UHNIH** ٠





CONFIGURATION DESCRIPTION		MPHA	BETA	æ
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PAGE 1067 Π Π 360 Т 320 INTERFERENCE TO UNDISTURBED RATIO 280 |||Ð œ 120 160 200 240 RADIAL LOCATION . PHI . DEGREES ×8888 ¥ 88888 BOOSTER BOOSTER BOOSTER BOOSTER BOOSTER **8**8888 FIG. 9 SOLID ROCKET BOOSTER -.110 (TRIPS) (TRIPS) 0+1+5 0+1+5 0+1+5 0+1+5 0+1+5 0+1+5 (TRIPS H CONFIGURATION D CONFIGURATION D CC 3.5-178 1H3 0 80. ХL 5.300 **8**8888 2 ¥ C⊡≫ 10.000 1.000 .100 .010 . 0 ISI4) ISI5) ISI8) ISI8) 251 Титектекенсе то инотатиявер немт транистер соегетствит ратто . **NH/IH**















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