A POSTPROCESSOR SYSTEM FOR THE DATA REDUCTION AND POST ANALYSIS OF NASTRAN RESULTS

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SUMMARY

A post-processor system for the data reduction and post analysis of NASTRAN results is described. NASTRAN analysis results are scanned to determine maximum and minimum displacements, forces and stresses. Allowables and margins of safety are computed, and in the case of multiple loading conditions, envelopes for displacements, forces, stresses and margins of safety are also produced for specified element sets. Graphical plots of the reduced or the regular NASTRAN results may be obtained superimposed either on a developed fuselage strip or on a projection of any specified part of the finite element model. The use of the data reduction, post analysis and graphical plotting capabilities provide the analyst with a fast and convenient tool for the study of NASTRAN analysis results and their presentation for project documentation.

INTRODUCTION

The high computational speed and large storage capacity of modern computers have enabled the analysis of large and complex structures subjected to multiple loadings and various boundary conditions. As a consequence, the structural engineer is bound to devote a substantial portion of his time in scanning and interpreting a large amount of output data, a process which is time consuming, error prone and hence inefficient. The way to alleviate this problem is to automate, wherever possible, the scanning and interpretation of the results, and to give the analyst the option to reduce the amount of computer output according to his engineering requirements. For further efficiency, this should be done in conjunction with graphical display of the reduced finite element analysis results. Additional help for the analyst can be obtained through the automation of certain standard post analysis procedures such as the computations of allowable stresses and margins of safety for the structural elements used in the finite element analysis.

The need for these capabilities has been felt for some time and as a result a large number of post-processors have been developed. However, most of these satellite programs are generally limited in scope, usually serving one particular purpose only, such as plotting (reference 1), or scanning (reference 2). At Israel Aircraft Industries an attempt has been made to integrate data reduction, post analysis, and graphic visualization into one package which has been especially devised to be engineering oriented.

This paper describes two interrelated software modules for the post processing, post analysis and graphical presentation of NASTRAN analysis results. Emphasis is put on the fact, that both modules are easy to apply, demanding a minimum of information from the user, yet leaving him with enough options to answer his design oriented requirements. The first of the two modules, NASDAT (reference 3) performs the post-processing and post analysis of the NASTRAN results; the second module, GRAS, plots any of the regular or reduced results in a graphical form.

DESCRIPTION OF MAIN MODULES

Description Of The NASDAT Module

The execution of the NASDAT module, illustrated in figure 1, may be subdivided into three main phases.

- a) In phase one, regular NASTRAN output data blocks are sorted and stored in a compact form on a disk file for subsequent use. This file may be saved after termination of NASDAT execution. Thus, a restart file, which contains all necessary I/O information of the NASTRAN analysis, is created to be used in phases 2 and 3.
- b) In phase two, the packed and sorted NASTRAN output is scanned, and efficient data reduction performed in accordance with the user's requirements.
- c) Finally, in phase three, post analysis of results including computations of allowables and margins of safety are performed.

NASDAT may be run either in conjunction with NASTRAN as a single job, or as a separate run following a NASTRAN analysis for which the necessary output data blocks have been saved. NASDAT may be restarted as many times as required.

NASDAT Capabilities

Presently, using NASDAT capabilities, the user may obtain:

- * Maxima and minima values
- * Envelopes of displacements, forces, stresses and/or margins of safety
- * Output in preferred sequence and format
- * Computations of allowables and margins of safety

The following is a brief description of the different options mentioned above:

a) Maximum and Minimum Values

The user may define a given set of elements and/or gridpoints from which the program will single out and identify those elements and grid points bearing extreme values of

force, stress and displacement; the magnitude of these extrema is also produced. In addition, it is possible to specify the upper and lower bounds beyond which the search for maximum and minimum values is to begin.

b) Envelopes of Displacements, Forces, Stresses and Margins of Safety

When analyzing several loading cases or checking various boundary condition configurations, the user has the option of obtaining envelopes of displacements, forces, stresses and margins of safety for a specified set of grid points and elements.

c) Output In A Preferred Sequence And Format

In some cases the user may require the results in a certain region of interest to be printed out separately in a specified sequence. In addition, if upper and lower bounds on the output values are also defined, then only those elements of the set with results above these bounds are printed.

d) Computations Of Allowables And Margins Of Safety

The margins of safety of any Rod, Shear Panel or Membrane element can be computed using allowables either defined by the user or automatically computed by the program. For the latter option the user may either define the section properties via manual input or allow the program to retrieve the geometrical and mechanical properties of these sections from tables generated in the NASTRAN analysis.

The NASDAT Input

In order to generate the main input for NASDAT the following DMAP statements for static analysis, must be included into the Executive Control Deck of the NASTRAN deck:

- 1. ALTER 121
- 2. OUTPUT2 CASECC, EST, MPT, GPL,/C,N,-1/C,N,11/C,N,UTAPE \$
- 3. OUTPUT2 OUGV1, OQG1, OEF1, OES1, /C, N, 0/C, N, 11 \$
- 4. ENDALTER

Statement 2 saves the necessary geometrical and mechanical properties of the structure on NASTRAN Fortran file UT1 and Statement 3 saves all the analysis results.

As can be noted, the main input to NASDAT comes from the above mentioned data blocks stored on file. However, additional input is required to specify the user's request for data reduction, post analysis and graphical presentation of results. This is prepared in a form similar to the NASTRAN input (reference 4). The NASDAT data deck consists therefore of an Executive Control Deck, a Case Control Deck and a Bulk Data Deck. The Executive Control Deck contains that information required by NASDAT to decide if the NASTRAN output files are to be sorted and/or checkpointed for restart purposes.

The Case Control Deck consists only of SET cards needed to define the element and grid sets referred to in the Bulk Data Deck, and TITLE cards which produce output labels for the preferred sequence option.

The Bulk Data Deck contains the main information required for the data reduction and post analysis. The format and order of input is similar to that of NASTRAN, i.e. data is input in 8 column fields with freedom to arrange the input cards in any sequence. Facsimiles of input cards for the data reduction and definition of lower and upper bounds are shown for Bar and Shear elements in figures 2, 3 and 4 respectively. Facsimiles of input cards for the automatic computation of margins of safety for Rod and Shear elements are shown in figures 5 and 6 respectively.

Description Of The GRAS Module

This is the off-line graphical postprocessing module, which is used to display graphically either the reduced results produced by NASDAT or the regular NASTRAN output. Input for the GRAS module is generated by NASDAT.

At present, GRAS is run in a batch mode environment and uses a Calcomp drum plotter. The plotting capabilities can take one of the following forms:

a) Developed Fuselage Strip

Using this option, a segment of the fuselage of an aircraft is developed into a flat strip upon which the values of the reduced or regular results are plotted.

b) Bulkhead Plots

Using this option graphical displays of bending moments, bending stresses and transverse shear forces in Bar elements may be obtained.

c) Projection Plots

The user may obtain a graphical display of the projection of any specified part of the structure on any one of the three principal planes. The stress values are then plotted on this projection. Figure 7 shows stresses in Rods plotted on a projected view of an aircraft delta wing in the XY plane.

NUMERICAL APPLICATIONS

The NASDAT and GRAS modules were first utilized in the data reduction and post analysis of the results obtained from the NASTRAN analysis of the IAI Westwind 1124 aft fuselage (reference 5). The structure was idealized using Shear Panels to represent the skins, Rod elements to represent the stringers and Bar elements offset from the skins to represent the bulkheads. The complete mathematical model, shown in figure 8, consisted of 460 BAR elements, 1670 ROD elements, 1030 SHEAR elements and 1250 GRID points representing a total of 3650 unconstrained degrees of freedom. The structure was subjected to 18 loading conditions. Because of the size of the structure a substructuring technique (reference 6) was employed, subdividing the aft-fuselage into 5 substructures.

Based on engineering considerations related to the structural configuration and loading conditions the analyst has asked for (presented here as an example) information relative to extreme values of average shear stresses, data relative to critical regions affected by shear buckling of skin panels, and margins of safety of Rodelements. In order to get the full picture of the internal load distribution in a bulkhead of interest, the preferred sequence option has been used to output results in this region. In addition, graphical capabilities have also been employed to display moments, shear stresses and axial stresses. Finally, a plot to represent the envelope of shear stresses has been required.

A listing of the complete input required to perform this type of data reduction and post analysis for substructure 1 (figure 9), is given in figure 10. Based on the user's request, the following data was obtained:

- (i) Twenty extreme absolute values for average stresses in Shear Panels and axial stresses in Rod elements (figure 11).
- (ii) Buckling stresses, diagonal tension factors and related margins of safety for Shear Panels located in the left hand side of the fuselage structure.

Since the actual skin panels between **bulk**heads were represented in the idealization as a mesh of NASTRAN Shear Panels, it should be noted that the aspect ratio (a/b) referred to the *actual* skin panels and not to the dimensions of an idealized element. Therefore, in this case, the user had to input the aspect ratio manually. The critical stresses, diagonal tension factors and margins of safety, shown in figure 12 were computed using criteria defined in references 7 and 8.

(iii) Euler buckling stresses, ultimate tensile stresses and related margins of safety for Rod elements located in the left hand side of the fuselage structure.

In this case the necessary geometric material and cross section properties of the rod elements were retrieved from the NASTRAN tables using the automatic procedure (via the FLAG=2 option). Computer output is shown in figure 13.

Note that this output is presented for illustration only. Usually, the user will request

с. Э only a print-out for those elements having negative margins of safety.

- (iv) A table of the internal load distribution for a bulkhead as requested via the preferred sequence option. Computer output is shown in figure 14.
- (v) Graphical display needed for project documentation including (a) plot of bending stresses for a bulkhead as shown in figure 15; (b) presentation of envelopes for maximum and minimum shear stresses as shown in figure 16 and 17 respectively, (c) presentation of stresses in Rod elements and Shear Fanels as shown in figures 18 and 19 respectively.

Since the original height of the Calcomp plots was 29 inches (73.6 cm) only a part of the plot (the left hand side) is presented.

The total amount of computer output for the complete NASTRAN finite element analysis consisted of about 5000 pages. Scanning, hand reduction, post analysis and drawing of results would have required several man months of engineering work. In contrast, meaningful engineering-oriented output and data reduction as presented above could be accomplished in the span of a few days.

CURRENT DEVELOPMENTS

Current developments of NASDAT include the expansion of the options which deal with computations of the allowables. These will incorporate bending elements as well as stiffened panels.

The NASDAT/GRAS modules are presently converted to operate in a time-sharing mode using low cost graphic display terminals, and together with NASTRAN will be included as modules in Israel Aircraft Industries' ISSAS, (Interfaced Software System for Sizing and Analysis of aircraft Structures) (reference 9).

CONCLUSION

Scanning of analysis results and computations of allowables and margins of safety, which are especially error prone and time consuming, may be performed with the aid of NASDAT and results graphically displayed by GRAS in an automated fashion, thus freeing the analyst to devote a larger portion of his time to engineering decision-making based upon results which are obtained in an organized form.

The use of the presented data reduction, post analysis and graphical plotting capabilities provide the analyst with an efficient and convenient tool for the study of NASTRAN analysis results and their presentation for project documentation.

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Bulk Dat	a Card	۳ļ	<u>AR</u> Data	reducti	on for CB	iAR elem	ents			N MI NMAX
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minimum or maximum extreme stress or	es required (Integer > 0 or blank)	nput for the plot modules	generate	do not generate (Default)
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- The element set identification number must be defined in the Case Control Deck (SET SID =) to be used by NASDAT
- In order to reduce the NASTRAN output for CBAR elements the user has the option to define the following output components to be output or plotted.

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FIGURE 2: NASDAT BULK DATA CARD BAR

	force an	nd stres.	s value	s of CB,	ÁR elem	ents.		AS	Extreme value of axial stress (Real > 0.0 (BARMAX); Real < 0.0 (BARMIN))
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			Content	S				"PREFSEQ" the values large	en the values are considered as criteria to output r than those defined on the BARMIN or BARMAX card.
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BARMIN BARMIN

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Format and Example

-1000. -2500.

Field

Type SID

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+BCD IN0+

FIGURE 3: NASDAT BULK DATA CARD BARMIN

Extreme value of moment in plane 1 at end -A- and

MIA; MIB

M2A; M2B

number (Integer > 0)

-B- (Real ≥ 0.0 (BARMAX); Real ≤ 0.0 (BARMIN))

Extreme value of moment in plane 2 at end -A- and

-B- (Real > 0.0 (BARMAX): Real < 0.0 (BARMIN))

Extreme value of transverse shear in plane 1 and

SF1; SF2

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plane 2 (Real > 0.0 (BARMAX); Real < (BARMIN))

(Real ≥ 0.0 (BARMAX), Real ≤ 0.0 (BARMIN))

Extreme value of torsional moment

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(Real ≥ 0.0 (BARMAX); Real ≤ 0.0.(BARMIN))

Extreme value of axial force

AF

Negative (BARMIN) or positive (BARMAX) bounds for

BARMIN: BARWAX

Bulk Data Cards

Description:

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reduction
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SHEAR
Card
Data
Bulk

HEAR elements

Defines the option and element set for which data reduction is requested.

Description:

Format and Example

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80	SMAX	3000
7	NIWS	
9	NO I L ON	MI NMAX
ъ	SSID	
4	SUBCASE	4
3	X	
2	SID	18
1	SHEAR	SHEAR

Alternate Form

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SMAX		
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NOITION	ENVEL	
SSID	21	
SUBCASE		
X		
SID	ALL	
SHEAR	SHEAR	

Element set identification number (Integer > 0) Contents

Field SID

SUBCASE	Single Subcase identification number for which data
	reduction is requested (lnteger > 0 or blank)
SSID	Subcase set identification number (Integer > 0 or
	blank).
OPTIØN	Data reduction option ; one of the BCD values
	"ENVEL", "MINMAX", "MS" or PREFSEQ"
	"ENVEL" - Stress envelope

maximum (positive) values per subcase Scan for minimum (negative) or ı "XAMNIM"

- Computes margin of safety , "NU"
- "PREFSEQ" Set output in preferred sequence

SMIN: SMAX	Define the negative (SMIN) and positive (SMAX)
	boundary values for the average shear stresses
	Output consists of negative values or positive
	values larger than those defined by SMIN or SMAX
	(Real ≥ 0.0 (SMAX); Real ≤ 0.0 (SMIN)).
NMI NMA X	Number of minimum and maximum extreme stress values required (Integer > 0 or blank)

The element set identification number must be defined in the Case Control Deck (SET SID =....) to be used by NASDAT. 1.

YES - Generate; NØ - do not generate (Default)

Remarks:

ΡLØT

Generate input for the plot modules,

critical stress for the shear panels defined in the element set. If OPTION = "MS" then the entry for SMAX is considered to be the 5.

FIGURE 4: NASDAT BULK DATA CARD SHEAR

Bulk Data Card		<u>ALRØD</u> margin:	Comput: s of saf	ations c fety for	of Allow r Rod el	ables a ements.	ınd relat	eq		FLAG	Flag to specify th follows: 4 5	e nature of fields 4-6 as 6
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Г		Length	of rod	elemen	t (Real	> 0.0 <	or blank	; see		Kemarks		
		below)								1. The elem	ent set identification nu ••••1 Pack (set SID -	umber must be defined in the) +∩ he wed hy NASDAT
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		or bla	ank; see	below)						R may ha	ve one of the following v	values
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		elemer	lt (Real	, 0.0,	see re	mark 2)				Bo	undary Condition	R
FTU		Ultim€	ate stre	ss for	rod ele	ment ma	terial			Simple	- Simple	1.0
		(Real	< 0.0)						*	fixed	- fixed	2.0
										fixed	- free	0.5
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FIGURE 5: NASDAT BULK DATA CARD ALROD

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·	toe	evaluate	their mar	gins of	safety.			1.	The element set identification number must be defined in the Case Control Deck (SET SID =) to be used by NASDAT
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	3	4	ا و	-	"	6	10		supported on four sides.

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Field

Contents

Element set identification number (Integer > 0)	Aspect ratio of shear panel (Real > 0.0 or blank;	see below)	Thickness of shear panel (Real > 0.0 or blank;	see below)	Young's modulus (Real > 0.0 or blank; see below)	Poisson's ratio (Real > 0.0 or blank; see below)	Radius of curvature of portion of skin under
SID	A/B		Т		ш	NN	R

ł

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9	NN	
5	в	
4	т	
8	A/B	
	FLAG=1	Flag=2

Flag to specify the nature of fields 3-6 as follows:

FLAG

investigation (Real > 0.0 or blank)

to perform computations for the allowables If FLAG=1 Then the user defines the values required of the shear panels.

If FLAG=2 Then the program takes the data from the

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appropriate NASTRAN tables.

FIGURE 6: NASDAT BULK DATA CARD ALSHEAR



FIGURE 7: ROD STRESSES DISPLAYED ON A PROJECTED VIEW OF A DELTA WING







KESTWIND-SUBSTRUCTURE 1

UNDEFORMED SHIPPE

FIGURE 9: FINITE ELEMENT MODEL OF WESTWIND 1124 AFT FUSELAGE (SUBSTRUCTURE 1)

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NASDAT EXECUTIVE CONTROL DECK ECHO

ID POST, PROCESSOR Sort YES CHKPNT YES CEND

NASDAT CASE CONTROL DECK ECHO

SET 1=1121 TMRU 1162 ExCEPT 1143.1144.1151.1152.1160.1170.1174.1175. 1179 TMRU 1184.1199 TMRU 1206.1495.1557 SET 2=1143.1144.1151.1152.1160.1168.1169.1172.1173.1176.1177.1176. 1287.1501.1507.1521.1527.1541.1545.1549 SET 3=1165.1166.1167.1185 TMRU 1190 SET 4=1191 TMRU 1198.1553 SET 5=3115. TMRU 3118.3181.3182.3189.3190.3199 TMRU 3212 ExCEPT 3205.3206. 3557.3561 SET 7=3120 SET 7=3120 SET 9=3121.3122.3129.3130.3166.3167.3171.3172.3176.3177.3187.3188.3195. 3196.3549.3553.3557.3561 SET 9=3123 TMRU 3128.3135.3136.3164.3168.3169.3491.3545 SET 10=3138.3146.3191 TMRU 3194 SET 11=3139 TMRU 3151 EXCEPT 3145.3146.3503.3517.3523.3529.3539 SET 12=3154.3162 SET 14=3152 TMRU 3152.3127.3178 TMRU 3180 SET 14=3153 TMRU 3162.3173 TMRU 3175.3178 TMRU 3180 SET 15=3183 TMRU 3162. SET 25=2 TMRU 11 SET 25=2 TMRU 11 SET 25=2 TMRU 11 SET 21=57 TFRU 84 BE61N BULK

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1	ALROD	1	0.132					5	
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5	ALSHEAR	5	6.0	0.04	10.5E+6	0.3		1	2
6	ALSHEAR	6	3.8	0.04	10.5E+6	0.3		1	5
i	ALSHEAR	7	3.4	0.04	10.5E+6	0.3		1	5
Â	AL SHEAR	8	3.0	0.04	10.5E+6	0.3		1	5
ä	AL SHEAR	9	2.0	0.04	10.5E+6	0.3		1	- 5
10	AL SHEAR	10	1.5	0.04	10.5E+6	0.3		1	5
11	ALCHEAD	ii	1.0	0.04	10.5E+6	0.3		1	- 5
	ALCHEAD	12	1.0	0.04	10.5E+6	6.3		1	5
12		12	5.0	0.04	10.5F+6	0.3		1	5
13	ALDREAK	1.5	3.0	A A72	10.55+6	0.3		1	5
14	ALSHEAR	14	2.2	4 472	10 SEA6	0.3		ī	Ś
15	ALSHEAR	15	1.07	V.V/C	14.35.0			-	YES
16	BAR	21	12010	7			1	20	
17	ROD	ALL	2	- 4		HINNAA		34	
i a	ROD	ALL	2	- 4		PREFSED	•	24	
19	RODMIN	1	-	40000.					
20	SHEAR	≜ L.		4		MINMAX		ZQ	
21	CHEAD	ALI		4		PREFSED			YES
21	SHEAD	ANI			25	ENVEL			YES
22	SHEAK	ACC							
23	LNDDAIA								

NASDAT SORTED BULK DATA ECHO

FIGURE 10: TYPICAL INPUT DATA DECK FOR NASDAT

THE FOLLOWING LIST PRESENTS THE EXTREME STRESSES IN & SHEAR ELEMENTS FOR SUBCASE 4 20 EXTREME VALUES ARE REQUESTED - 10 VALUES ARE FOUND TO BE POSITIVE: 10 ARE NEGATIVE

ELEMENT	AVG	ELEMENT	AV6
10.	STRESS	ED.	STRESS
3151	1.1645E+04	3150	1+0372E+04
3196	1+0367E+04	3158	1+0170E+04
3149	9+9385E+03	3195	9.8036E+03
3194	9.5829E+03	3193	8.9942E+03
3166	8.9071E+03	3188	8.5570E+03

MININUM (NEGATIVE) STRESSES

ELEMENT	AVG	ELEMENT	AVG
ID.	STRESS	SD.	STRESS
3049	-9.4084E+03	3066	-8.4594E+03
3073	-7.7787E+03	3048	-7.6788F+03
3040	-7.6418E+03	3060	-7.4885E+03
3056	-7.3720E+03	3032	-7.3580E+03
3036	-7.3221E+03	3047	-7.3046E+03

THE FOLLOWING LIST PRESENTS THE EXTREME AXIAL STRESSES IN C R O D ELEMENTS FOR S U B C A S E 4 20 EXTREME VALUES ARE REQUEST - 20 VALUES ARE FOUND TO BE POSITIVE, -0 ARE NEGATIVE

*********	**********	**********
MAXIMUM	(POSITIVE)	STRESSES
********	*********	*********

ELEMENT	AXIAL	ELEMENT	AXIAL
ID.	STRESS	SD.	STRESS
1139	4.9660E+04	1097	4-8070F+04
1138	4.7072E+04	1089	4-6432E+04
1113	4.6383E+04	1090	4+6018F+04
1121	4.5952E+04	1129	4-5700E+04
1091	4.5455E+04	1114	4-5029E+04
1122	4.4157E+04	1134	4-4011E+04
1115	4.3012E+04	1123	4-2808E+04
1105	4.2489E+04	1133	4-1843E+04
1102	4.1757E+04	1140	4-1635F+04
1124	4.0831E+04	1135	4.0641E+04

FIGURE 11: MAXIMUM AND MINIMUM STRESSES IN SHEAR PANELS AND ROD ELEMENTS

C S H E A R ELEMENTS AVERAGE STRESSES, CRITICAL STRESSES, DIAGONAL TENSION FACTOR AND MARGINS OF SAFETY FOR

	MARBIN OF	SAFETY	2.925+00	9°19E+01	4•21E+00	4.965+01	2.295-02	-5.206-01	1.765-02	8.65E-01	-7.88E-01	-6.95E-01	-2.37E-01	-6.95E-01	-7.42E-01	6.27E-01	=3.86E-01	-5.16E-01		-1.28E-01	1.76E+00	3.47E-01	-2.67E-02	+7.71E-01	-2.77E-01	-8.445-01	Z.11E-01	2.63E+00	-1.995-01	5.3/E-01		2.905.00	-3-22F-01	6.57E+00	3.776-01	4.26E-01	-1.47E-01	1.82E-01		1.145+00	1.156+00	3.64E-01	5.39E-01	3.02E+00] • 44E + 00	1.72E+00	1.1361.1		1.445+01	1.44E-01	5.58E+00	2.345+01
	DIAG TENSION	FACTOR	•	•	•	••	ن د •	1.586-01	•	••	3.256-01	2.52E-01	5.87E-02	2.52E-01	2.86E-01	••••••	1.06E-01	1.56E-01	3.766-01	2.97E-02	•	•0	5.88E-03	3.106-01	7.03E-02	3.83E-01	••	0.	3.356+01	0.	3.456-01		4.415-02			•••	3.45E-02	0.				•	•0	•••	•	•	U. 1 ARF_A1		0.	•••	•	•
	CRITICAL	SHEAR	4°3666E.4	5 6291E+03	6.4194E+03	7.2341E+03	1.4812E+03	1.9281E+03	2.2000E+03	2.4660E+03	1.6646E+03	2.5285E+03	1.3094E+03	1.7017E+03	1.8854E+03	6.6482E+03	1.3393E+03	1.6689E+03	1.8306E+03	6.3880E+03	6.6386E+03	7.2018E+03	7.6366E+03	1.5050E+03	5.9979E+03	1.4760E+03	6.0835E+03	7.7225E+03	1.4862E+03	6.0558E+03	1.39346+03	0.1905505 7 53705403	2.4221E+01	9.94145+03	1.12286+04	1.2426E+04	2.7978E+03	3.5283E+03	50+30+/6°5	4.40965403	5.3989E+03	6.1649E+03	6.9528E+03	5.0460E+03	6.2245E+03	7.0616E+03	7.928/E+03	C. / 36405 +03	8-4831E+03	7.7675E+03	1.3665E+04	7.67456+03
	AVG	SHEAR	1.1210E+03	2.9340E+03	1.2330E+03	1.4300E+02	1.4480E+03	4.0130E+03	2.1620E+03	1.3220E+03	7.8540E+03	8.2780E+03	1.7160E+03	5.5710E+03	7.3070E+03	4.0860E+03	2.1820E+03	3.4470E+03	1.1283E+04	7.3250E+03	2.4040E+03	5.3450E+03	7.8460E+03	6.5700E+03	8.2960E+03	9.4530E+03	5.0240E+03	2.1260E+03	7.4120E+03	3.9410E+03	7.2890E+03	2.1480E+03	1.60£VETUJ	1.31405+03	.8.1530E+03	8.7110E+03	3.2800E+03	2.9860E+03	9.8770E+03	1.00795-04	2.5120F+03	4.5200E+03	4.5190E+03	1.2560E+03	2.5510E+03	2.5990E+03	2.8870E+03	5.3540E+03	5.500E+02	6.7890E+03	2.0770E+03	3.1500E+02
ŝ	ELEMENT	10.	3114	3116	3118	3120	3122	3124	3126	3128	3130	3136	3138	3140	3142	3144	3146	3148	3150	3152	3155	3157	3159	3162	3164	3166	3168	3170	3172	3174	3176	3178		2010	JIRG	3186	3190	3192	961E	0616	1200	3202	3204	3206	3208	3210	3212	1945		3539	3549	3557
SUBCASE	MARGIN OF	SAFETY	1.77E-00	9.35E-01	4.28E+00	4.98E+01	-4.83E-01	-5.15E-01	2.49E-02	8.95E-01	-5.495-01	-6.92E-01	-7.585-01	-6.925-01	-7.40E-01	-7.19E-01	-7.92F-01	-5,137-01	-8-365-01	-8.506-01	-1.806-02	4.01F+00	-3.20F-01	-7.19F-03	2.47E-01	3.12E-01	-7.765-01	2.07E-01	-8.38E-01	5,45E-01	3.296+00	-7.185-01	9.57E-01	-300°-01	9.5/C+U1 0 60F-01	4-37F-01	-9.83E-02	1.91E-01	-5.926-01	-5.956-01	1 155-01	1.13CTUU 7.60F=01	5.625-01	3.43E+00	1.485+00	1.746+00	1.76E+00	1.996+00	-0.202-01	4.03E-01	-1.526-01	9.396-01
	DIAG TENSION	FACTOR	•••	•	•0	•0•	1.42E-01	1.56E-01			1.716-01	2.50E-01	2.985-01	2.516-01	2.856-01	2-695-01	3.28F=01	1.55F=01	745-01	3.91F=01	3.94F-03		0.35F=A2	1.57F=03			3.14E-01	.0	3.75E-01	0.	•••	2.68E-01	0.	1.05-01	•	•	2.256-02	•0	1.92E-01	1.946-01	•	•	•			•••	••	0.	2.11E-01	0.075-UJ	3.586-02	•
	CRITICAL	SHEAR	3.9474E+03	5.3184E+03	6.0665E+03	6.8070E+03	1.4025E+03	1.8252E+03	2.0805E+03	2.3294F+03	1.67025+03	2.4047F+03	1,19656+03	1.6320F+0.3	1.8100E+03	1.46565+03	1 20005403	1 60045403		1 4900F+03	6 5035F+03			7 87405403	5.8301F+03	7./1586+03	1.5500E+03	6.31346+03	1.4167E+03	5.8343E+03	7.3807E+03	1.4702E+03	6.0505E+03	2°2984E+03	9.4659E+03	1 10325404	2.6419E+03	3.3554E+03	3.7871E+03	4.1762E+03	4.0430E+04	5.1000E+03	2.53675+03	4.7247E+03	5.88A6E+03	6.6842E+03	7.4749E+03	7.9805E+03	2.7835E+03	3.3362E+03 B.1301E+03	8.0738E+03	4.8658E+03
	AVG	SHEAR	1.4250E+03	2.74906+03	1.1490E+03	1.3400E+02	2.7150E+03	3.7670E+03	2.0300E+03	1.2290F+A1	1.7220F+03	7.8000F+03	4 03505+03	E 3060E+03	5.9690F+03	7 0006403	1+UUUUC-03	0.1930C-03		1. 27005.04	1.0000 001		1.30205-13	1.07405 404	4 47605403		6.9300E+03	5.2300E+03	8.7190E+03	3.77706+03	1.7200E+03	5.2160E+03	3.0910E+03	5.21905+03	1.0000E+02	0.4100E+03	2.9300E+03	2.8180E+03	9.2710E+03	1.0305E+04	2.2870E+03	2.3770E+03	4.2000-00 4.10505-00	** 18305 403	2.3770F+03	2.4400E+03	2.7040E+03	2.6730E+03	7.4480E+03	3.4310E+03 E 0.30E+03	0.60305-03	2. 5A90F+03
	ELENENT	- ID-	ETTE	3115	3117	3119	3121	3123	3125	1010	0010				1415	2410				2115			1150	9110		2102	3167	3169	3171	3173	3175	3177	3179	3161	3183	CB15	1010	3191	3193	3195	3197	3199	1025	2005	2020	3209	3211	3485	3497	3517	3064	

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AVERAGE STRESSES, BUCKLING STRESSES, DIAGONAL TENSION FACTORS AND MARGINS OF SAFETY FOR SHEAR PANELS

FIGURE 12:

ELEMENTS CONROD CRITICAL STRESSES AND SAFETY MARGINS FOR CROD AND

SUBCASE 4

MARGIN OF Safetv	241C11 4 27F-01	5.436-01	6.99E-01	8.71E-01	6.67E-01	6.48E-01	4.31E-01	1.01E+00	3 . 38E-01	5.13E-01	1.77E+00	2.80E+00	1.18E+00	9.43E-01	1.45E+00	5.97E+00	2.57E+00	3.15E+00	3.13E+00	9.50E+00	4.25E+01	2.12E+02	3.72E+03	6.27E+01	5.99E+02	3.91E+01	6.78E+02	2.07E+01	1.78E+01	8,50E+01	7.01E+01	9.94E+01	1.80E+01	5.06E+01	6.38E+01	8.35E+01	1.60E+01	4.45E+01	5.47E+01	7.08E+01	2-77F+04	1 COFADO	7.316+00	1.52E+03	1.205+02	1.08E+02	
CRITICAL	514533	6.3000E+04	6.3000E+04	6.3000E+04	6.3000E+04	6.3000E+04	6.3000E+04	6.3000E+04	6.3000E+04	6.3000E+04	6.3000E+04	6.3000E+04	6.3000E+04	6.3000E+04	6.3000E+04	6.3000E+04	6.3000E+04	6.3000E+04	6.3000E+04	6-3000E+04	6-3000E+04	1.2104E+06	6.3428E+06	5.1895E+05	1.3746E+06	5.1644E+05	1.3686E+06	5.3919E+05	5.3949E+05	1.4180E+06	1.6280E+06	1.6277E+06	6.0624E+05	1.3578E+06	1.5587E+06	1.5587E+06	5.4082E+05	1.2464E+06	1.4309E+06	1.4308E+06	6.3117E+06	6.300F+04	6.3000E+04	2.1482E+06	2-1254F+06	I.9475E+06	
AXIAL	217550 4.41575404	4.0831E+04	3-7087E+04	3.3674E+04	3.7796E+04	3.8220E+04	4.4011E+04	3.1402E+04	4.7072E+04	4.1635E+04	2+2714E+04	1.6578E+04	2.8888E+04	3.2423E+04	2.5675E+04	9.0450E+03	1.7667E+04	1.5191E+04	1.5263E+04	5.9990E+03	1-4490E+03	-5.6720E+03	-1.7060E+03	-8.1460E+03	-2.2900E+03	-1.2869E+04	-2.0160E+03	-2.4851E+04	-2.8673E+04	-1.6496E+04	-2.2884E+04	-1.6220E+04	-3.1848E+04	-2.6296E+04	-2.4067E+04	-1.8456E+04	-3.1835E+04	-2.7402E+04	-2.5667E+04	-1.9922E+04	-2.2800E+02	2.52336+04	7.5840E+03	-1.4130E+03	+1.7532E+04	-1.7866E+04	
EL CHENT	1122	1124	1126	1128	1130	1132	1134	1136	1138	1140	1142	114	1146	1148	1150	1152	1154	1156	1158	1160	1165	1167	1169	1111	1173	1175	1177	1179	1183	1185	1187	1189	1911	1193	1195	1197	1199	1201	1203	1205	1287	1495	1507	1527	1549	1557	
MARGIN OF Saffty	3.71F-A1	4.72E-01	6.19E-01	7.83E-01	3.79E-01	8.95E-01	5.06E-01	5.50E-01	4.85E-01	2.69E-01	9.29E-01	2.75E+00	1.01E+00	l.14E+00	1.02E+00	2.62E+00	3.13E+00	4.35E+00	2.08E+00	6.68E+00	1.36E+02	1.27E+02	2.02E+02	6.39E+01	2.40E+02	3.04E+01	2.26E+02	2.65E+04	2.35E+01	1.895+01	6.81E+01	7.85E+01	1.37E+02	2.12E+01	5.19E+01	7.18E+01	1.01E+02	1.69E+01	4.48E+01	6.24E+01	8.00E+01	1.036+00	2.63E+00	8.04E+00	6.15E+02	1.56E+02	
CRITICAL	5.3000Fe04	6.3000E+04	6.3000E+04	6.3000E+04	6.3000E+04	6.3000E+04	6.3000E+04	6.3000E+04	6.3000E+04	6.3000E+04	6.3000E+04	6.3000E+04	6+3000E+04	6.3000E+04	6.3000E+04	6.3000E+04	6+3000E+04	6.3000E+04	6.3000E+04	6.3000E+04	6.3000E+04	4.1505E+05	1.3806E+06	5.4371E+05	1.4781E+06	5.4106E+05	1.4717E+06	6+2843E+06	5.14536+05	5.1427E+05	1.4180E+06	1.6280E+06	1.6277E+06	5.5245E+05	1.3578E+06	1.5587E+06	1.5587E+06	5.1463E+05	1.2464E+06	1+4309E+06	1.4308E+06	6-3000E+04	6+3000E+04	6+3000E+04	2.1384E+06	2.1694E+06	
AXIAL Stdfss	4 - 5952F + 04	4.2808E+04	3.8921E+04	3.5340E+04	4.5700E+04	3,3243E+04	4 .1 843E+04	4.0641E+04	4.24245+04	4.9660E+04	3.2667E+04	1.6800E+04	3.1339E+04	2.9498E+04	3.1210E+04	1.7413E+04	1.5262E+04	1.1765E+04	2.0445E+04	8.2030E+03	4.6000E+02	-3.2450E+03	-6.7860E+03	-8.3780E+03	-6.1430E+03	-1.7244E+04	-6.4970E+03	-2.3700E+02	-2.1027E+04	-2.5788E+04	-2.0531E+04	-2.0475E+04	-1.1795E+04	-2.4863E+ 0 4	-2.5676E+04	-2.1399E+04	-1.5254E+04	-2.8743E+04	-2.7234E+04	-2.2585E+04	-1.7654E+04	3.0985E+04	1.73395+04	6.9690E+03	-3.4710E+03	-1.3834E+04	
ELENENT	1211	1123	1125	1127	1129	1131	1133	1135	1137	1139	1141	1143	1145	1147	1149	1151	1153	1155	1157	1159	1162	1166	1168	1170	1172	1174	1176	1178	1180	1184	1186	1188	1190	1192	1194	1196	1198	1200	1202	1204	1206	1489	1501	1521	1541	1553	

FIGURE 13: AXIAL STRESSES, EULER/ULTIMATE STRESSES AND MARGINS OF SAFETY FOR ROD ELEMENTS F444E AT STATIO 1 340 - SUASTRUCTURE 1 -

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SUBCASE 4 *

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	CBAR		۲) (۲) اب	-	I (F) [K	AXIAL FORCE I	AXIAL STRESS 1	Slómax (a) I	SIGMAA(B)	SIGMIN(A) I	SIGMIN(B)
			1 1 1 1 1 1 1	-]					
				-	1 1 1 1 1 1 1 1 1 1			Z-907E+03 1	1.7245+03 I	2.848E+03 I	1.5726+02 I
	- 0 - 1	• •••	C					1.824E403 1	6.364F+02 I	3,340E+03 I	-3.020E+03 I
	e d r u		7 10EFE 100			2 20 20 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	5.6546+0 2	1.785E+03 1	-2,302E+03 I	2.875E+03 I	-4.861E+03 I
	r 4			-				7.977E+01 1	-3.523E+03 I	/.455E+02 I	-5.204E+03 I
		-4 1-	0,3355,403 1 6335,403	-		1 - 24 - 25 - 25 - 1	2.404E+02 1	2.447E+03 I	-2.654E+03 I	1.50+3+66+03 I	-6.279E+02 I
		ן 	1 0000 0000 000 2 0000 000	• -	1 20+3/50-4	+ 034E+02 I	6.125E+02 1	1.161E+03 1	1.649E+02]	1.170E+03 1	-1.032E+02 I
-	36	- i	8.8705+02	• —		-5.255E+02 I	-7.205E+02 I	2.545E+02 I	-1.4445.403 I	1.761E+02 I	-1.854F.+U.3 I
- ►	1 1 1	• •	A.122F+12	• •] 00+3124.1-	-2.432E+32 I	-3.092E+02 I	3.798E+02 I	-8.402E+U2 I	I.1255+03 I	-1.415E+03 I
	r ur Division	 	1.480F+03	•		-1.449E+02 I	-2.004E+02 I	1.210E+03 1	-1.143E+03 I	L.695E+03 I	-1.534E+03 I
•	99	• `•	1.603E+93			2.945E+01 I	2.527E+01 I	1.728E+03 I	-1.006E+03 I	2.775E+0.3 I	-].040E+03 I
	5	ו 	1.353F+03	-		7.376E+02 I	1.120E+0 4 1	3.519E+03 I	-7.507E+U2	4.512E+03 I	-1.525E+03 I
4	- 00 - 10	1	2.60hE+03		1256+02	-4.449E+01 I	-d.764E+01 1	1.031E+04 I	-4.515E+03 I	L.345E+03 1	-3.570E+03 I
	6 4 4	• •-	2-840E+02		1	-7.594E+02 I	-1.497E+0 4 1	-1.015E+0.3 1	-2.630E+03 I	7.069E+02 I	-6.675E+03 I
4	0		1.565F+03		-707E+03	-4.930E+02 I	-9.712E+0? I	1.687E+03 1	-7.216E+0.3 I	1.428E+03 I	-/./83E+03]
			1.681E+03		1.450E+UJ	-5.211E+02 1	-1.027E+0 • I	I.829E+03 I	-/.736E+03 I	1.407E+03 I	-7.683E+03 I
4 1-			3165+0		+-715E+ùč 1	-4.812E+02 I	-1.735E+0 + I	4.996E+02 I	-0.988F+03 I		-3.018E+03 I
-	- F		1.1915+0	•		-/.370E+01 I	-4.6595+01 1	I .976E+0.4 I	-4.744F+03 I	8.484E+03 I	-3.490F.+03 I
4 1-	74	1	1.6345+0		- 155E+UJ	7.460E+02 I	1.132E+07 1	4.029E+03 1	-1.126E+03 I	J.180E+03 I	-4.036F+02 I
	1 1 1	• •	2.052E+0	•	-1.176E+0.3 1	7.338E+01 I	6.296E+01 I	2.241E+03 I	-1.256F+03 I	1.312E+03 I	-6.433E+02 I
4 ⊢	75	ا ب .	9.744E+05	-	-1.1296+02	I.633E+02 I	2.183E+0~ I	I.147E+03 I	-4.350E+02 I	3.259E+02 I	1.425E+02
		•	0 - 34E + 05		16+E+01	1.179E+02 I	1.513E+02 I	j.158E+02 I	2.536E+01 I	4.130E+02 I	-8.357E+02 I
-	- 1				1516+42	-5.500F+02 I	-7.541E+02 1	-2.455E+02	-1.113E+03 I	-0.644E+01 I	-1.650E+03 I
- +	- 1			• •		-7.510F+02 [-1-1405+0 1	->,15¤E+02 I	-1.941E+03 I	-5.257E+02 I	-1.428E+03 I
-, ,		+				1 20+3285 I	- 4-00 4E+02	1.240E+03 I	-2.328E+03 I	0-832E+02 I	-1.224E+03 I
-		- •		 -		5-27F+02 I	1.285E+03 1	Z.002E+03 I	-3.958E+02 I	0.343E+03 I	-8.666E+02 I
		P					2.3836+03 1	5.538E+03 I	1.041E+03 I	541E+03 1	1.039E+03 I
-	V C œ	• •	- / • · · · · · · · · · · · · · · · · · ·				2.546F+02	5.383E+0.3 1	1.338E+03 I	4.610E+03 I	1.067E+03 I
-	5 8	•	- / • 104E • 01	 		1 230F+03 1		4.645E+03 I	1.460E+03 I	2.642E+03 I	2,330E+03 I
M	44			- V							

•.

FIGURE 14: INTERNAL LOAD DISTRIBUTION IN A BULKHEAD



STRESSES IN BAR ELEMENTS BULKHEAD AT STATION = 340.00



2866.	9114. 2786. 10.	3115 8788 10	9118. 8962. 18.	9906. 10.	8455. 10.	3007. 10.	· 1221:	7299
231:	3143:	3488:	3123: 11	8125: 1813:	9128- 7075- 10-	34 <u>17:</u>	: UR:	
18.	3130.				1	3135. 11359. 10.	91 96. 12052. 19.	3487 0922 10
3128: 6272: 18.	1825.		5140.	?191:	5142. 8851.	3143. 7340. 10.	3144. 4262. LO.	3503 8795 10
3137. Gidi. 10.	3136. 2652. 10.	3139 5900:	\$\$ <u>71</u> . 5.	-10.	3150,	3151. 12700.	9152 7375: 5.	3517 5159 10
3145. BC43.	3148. 2182. 5.	5147. 5905. 5.	3148. 3446. 5.	3148. 10952. 10.	10.	3158	3160.	3523 2356 10
10.	3154.	3155. 2405. 5.	9156. 1966. 7.	3157. 5346. 5.	5158. 10941. 10.	6305.	10.	<u> </u>
	1.	9183. 12104.	3184. 15874. 10.	3165. 11307. 10.				3520
	1956.	3168.	3158:	3170: 2199:				353
3166. 10972. 10.	9187. 6929. 5.	5024.		3175: 1014:				354
3171.	3172. 7412. 5.	9179. 3777. 5.	3942.	3180.				354
·/₽	3177	3178. 3823. 9.	3178. 4014. 9.	1980. B. 3165.	3188. 8155. 5.	3167. 8234. 5.	3188. 6711. 5. 3198.	355
3178. 7280. 5.	5.	3183. 442: 6.	3184. 685. 2.	5418. 5. 3193. 9271.	3194. 9676. 5	3195. 10305. 5.	5204. V520. Si	122
3101 5335 1	3572: 5.	3191. 3643. 10.	3192. 3061. 10. 32209.	2201:	9202: 4518: 5: 9210: 2599:	23 gi	2000.	<u> </u>
3109. 2959.	3100. 2013.	3189 2985; 8, 5207.	3173. 8. 3208. 3043. 8.	209. 2491.: 3.:	3.			
3197:	5.	2046: 4.	1					

WESTWIND SUBSTRUCTURE 1 ENVELOPE FOR MAXIMUM SHEAR STRESS IN PANELS

FIGURE 16: POSITIVE SHEAR STRESSES ENVELOPE DISPLAYED ON A DEVELOPED STRIP OF THE FUSELAGE

3113. -2960.	3114. -2446. 8.	3115. -7980. 9.	3116 -8518. 9.	-7802.	3118. -0339. 9.	-2890.	-3085. 9.	-505
9121. -3250.	3122 -2758. 8.	3123. -6895. 9.	3124. -6817. 9.	3125. -5830. 8.	3126. -6380. 8.	5127. -5207.	3128. -5137. 9.	5481 -622 8.
J.	3130.					3135. -0075. 9.	5138. -8567. 1.	349 -54
-4773. 9.	8.		3140,	3141 -4774,	9142. -5006.	3143. -4588. 7.	9146. -2601. 7.	350
3137. -5853. 0.	9136. -1998. 9.	-2824.	-2965.		3150.	3151. -8941.	3152. -4030. 7.	351
3145. -4977.	3148. -1303. 2	3147. -1800. 2.	3148. -1983. 2.	-6416.	-6697.	3159.	3150. -5482.	352
	3154 -3725.	3155. -1438. 2.	9158. -1714. 6.	3157. -2890. 2.	3158. -8312. -7.	-5231.		-
	2. 3162. -15148.	3163. -10024. 9.	3164. -12061. 9.	3165. -9046. 8.				35: -21
	3167.	3168. -2807. 2.	9189. -2923, 2.	9170. -1303. 2.				35
3166, -5858. 8.		3173	3174. -2207. 2.	\$175. -1092. 2.				35
3171. -4790. 2.	3172. - 4054. 2.		2129	3180. -1234. 10.			3146.	35
31.75.	3177. -2748. 2.	3178, -3036, 10,	3184	3165 -3071. 2.	3188. -4554. 2.	9187. -4665. 2. 9185.	2. 3198 -6003. 2.	35
-4194.	9182. -2088. -2,	3163. -97. 2.	-1314. 5. 3192.	3193. -5160. 2.	3194 -5519. 2. 3202.	-3876. 2. -2019. -2019. 2.	-2183. -2183. -2183. -1313.	
9161 - 3140. 2.	3100. -2099. 2.	3191. -1942. 7.	-2038. 3200. -2184. -2	5201 -2172. 2. 5700	-2306, 2, -218, -1148, 5,	-1229. 5:	3.0	
3189 -1753, 2.	9108. -1120. 2.	-2027. 7. -1994.	5200. -2122. 0.	-10/0. 5.				
			_					

WESTWIND SUBSTRUCTURE 1 ENVELOPE FOR MINIMUM SHEAR STRESS IN PANELS

FIGURE 17: NEGATIVE SHEAR STRESSES ENVELOPE DISPLAYED ON A DEVELOPED STRIP OF THE FUSELAGE



WESTWIND SUBSTRUCTURE A SUBCASE 4 -UPGUST CONDITION CONFIG. 5-STRESSES IN ROD ELEMENTS

FIGURE 18: ROD STRESSES DISPLAYED ON A DEVELOPED STRIP OF THE FUSELAGE

3114. 807.	2115 1760:	? 1 38:	3117.	3118. 224.	2110.	2120. U.	2201:
ł ł ??:	3133:	3124: 3118:	? \$ 35:	7489:	₹ <u>1</u> 27:	7188:	E384:
1139:	+			L	1435:	7335 :	134 2:
	3128.	\$140. 5017:	2323:	3148:	2142 5565	3177:	2583:
1481:	4//6.		2149.	?1 59 2.	1184.	3155 :	1547:
31 %5 :	3827:	3152:	8039.	3158.	3158:	718R:	21178;
1222:	2376:	21 21 3.	2323:	10178.			
1163:	8383:	3184. 7604.:	8198:				1989:
1117.	2419:	3178:	2178:				DB:
113.	2172-	HZ:	₹17 ₹ :				35%:
1173:		8129-	74 1 9:			24.89;	-186 i.
3177:	1138:	31.04.	1385:	3111:	3687: 2195-	?6 58 7.	
ILBE:	118:	-1179.	HR:	31893; 7202:	Kill:	3997:: 3513:	-1022.
3182:	3151:	2799:	379%: 7882:	4000. 7840:	Ifth:		
1118:	2007. 5207. 1888.	3831 :					
3587.							
	JUY: IIII: IIII: III:	JJJY: PHE: HITT: JJJZ: HITT: JJJZ: HITT: JJJZ: HITT: JJJZ: HITT: JJJZ: HITT: JJJZ: HITT: HITT: HIT	JJJ?: 1716: JHE: HIT: JHE: JHE: HIT: JHE: JHE: HIE: JHE: JHE: JHE: JHE: JHE: JHE: JHE: JHE: JHE: JHE: <t< td=""><td>1011: 1012: 1014: 3017: 1123: 1023: 1173: 1036: 1123: 1017: 1017: 1017: 1123: 1017: 1017: 1017: 1121: 1017: 1017: 1017: 1121: 1017: 1017: 1017: 1111: 1017: 1017: 1017: 1112: 1017: 1017: 1017: 1112: 1017: 1017: 1017: 1112: 1017: 1017: 1017: 1112: 1017: 1017: 1017: 1113: 1017: 1017: 1017: 1112: 1018: 1017: 1017: 1113: 1017: 1017: 1017: 1113: 1017: 1017: 1017: 1113: 1017: 1017: 1017: 1113: 1017: 1017: 1017: 1114: 1017: 1017: 1017: 1113: 1017: 1017: 1017: 11141: 1017: 1017:</td><td>LLAY: PLAE: PLAE: PLAE: PLAE: PLAE: PLAE: LLAE: JLAE: JLAE: JLAE: PLAE: PLAE: PLAE: JLAE: JLAE: JLAE: JLAE: PLAE: PLAE: PLAE: JLAE: JLAE: JLAE: JLAE: JLAE: PLAE: PLAE: JLAE: JLAE: JLAE: JLAE: JLAE: PLAE: PLAE: JLAE: JLAE: JLAE: JLAE: JLAE: PLAE: PLAE: JLAE: JLAE: JLAE: JLAE: PLAE: PLAE: PLAE: PLAE: JLAE: JLAE: JLAE: JLAE: PLAE: PLAE: PLAE: PLAE: JLAE: JLAE: JLAE: JLAE: PLAE: PLAE: PLAE:</td><td>101* 1011:</td><td>1331: 1342: 1341: 2341: 2342: 2344: 2344: 2344: 1117: 1342: 1173: 1345: 1442: 1113: 1143: 1143: 1143: 1328: </td></t<>	1011: 1012: 1014: 3017: 1123: 1023: 1173: 1036: 1123: 1017: 1017: 1017: 1123: 1017: 1017: 1017: 1121: 1017: 1017: 1017: 1121: 1017: 1017: 1017: 1111: 1017: 1017: 1017: 1112: 1017: 1017: 1017: 1112: 1017: 1017: 1017: 1112: 1017: 1017: 1017: 1112: 1017: 1017: 1017: 1113: 1017: 1017: 1017: 1112: 1018: 1017: 1017: 1113: 1017: 1017: 1017: 1113: 1017: 1017: 1017: 1113: 1017: 1017: 1017: 1113: 1017: 1017: 1017: 1114: 1017: 1017: 1017: 1113: 1017: 1017: 1017: 11141: 1017: 1017:	LLAY: PLAE: PLAE: PLAE: PLAE: PLAE: PLAE: LLAE: JLAE: JLAE: JLAE: PLAE: PLAE: PLAE: JLAE: JLAE: JLAE: JLAE: PLAE: PLAE: PLAE: JLAE: JLAE: JLAE: JLAE: JLAE: PLAE: PLAE: JLAE: JLAE: JLAE: JLAE: JLAE: PLAE: PLAE: JLAE: JLAE: JLAE: JLAE: JLAE: PLAE: PLAE: JLAE: JLAE: JLAE: JLAE: PLAE: PLAE: PLAE: PLAE: JLAE: JLAE: JLAE: JLAE: PLAE: PLAE: PLAE: PLAE: JLAE: JLAE: JLAE: JLAE: PLAE: PLAE: PLAE:	101* 1011:	1331: 1342: 1341: 2341: 2342: 2344: 2344: 2344: 1117: 1342: 1173: 1345: 1442: 1113: 1143: 1143: 1143: 1328:

WESTWIND SUBSTRUCTURE 1 SUBCASE 4 - UPGUST CONDITION CONFIG. 5-SHEAR STRESS IN PANELS

FIGURE 19: SHEAR STRESSES DISPLAYED ON A DEVELOPED STRIP OF THE FUSELAGE