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# A SIMULATION MODEL FOR WIND ENERGY STORAGE SYSTEMS

Volume II: Operation Manual

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BOEING COMPUTER SERVICES COMPANY

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16. Abstract The effort developed a comprehensive computer program for the modeling of wind energy/storage systems utilizing any combination of five types of storage (pumped hydro, battery, thermal, flywheel and pneumatic). An acronym for the program is SIMWEST (Simulation Model for Wind Energy Storage). The level of detail of SIMWEST is consistent with a role of evaluating the economic feasibility as well as the general performance of wind energy systems.  The software package consists of two basic programs and a library of system, environmental, and load components. The first program is a precompiler which generates computer models (in Fortran) of complex wind source/storage/application systems, from user specifications using the respective library components. The second program provides the techno-economic system analysis with the respective I/O, the integration of system dynamics, and the iteration for conveyance of variables. This SIMWEST program, as described, runs on the UNIVAC 1100 series computers.  This technical report contains three volumes. Volume I gives a brief overview of the SIMWEST program and describes the two NASA defined simulation studies. Volume II, the SIMWEST operation manual, describes the usage of the SIMWEST program, the design of the library components, and a number of simple example simulations intended to familiarize the user with the program's operation. Volume II also contains a listing of each SIMWEST library subroutine. Volume III, the SIMWEST program description contains program descriptions, flow charts and program listings for the SIMWEST Model Generation Program, the Simulation program, the File Maintenance program and the Printer Plotter program. Volume III generally would not be required by SIMWEST user.			
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FOREWARD

This report presents results of work conducted by Boeing Computer Services Company under NASA Contract NAS3-20385, "Wind Energy Storage Model Development." This program was conducted under the sponsorship of the Advanced Physical Methods Branch, Office of Conservation, ERDA, under the direction of Dr. G. C. Chang, and was administered by the NASA-Lewis Research Center Thermal and Mechanical Storage Section with Mr. L. H. Gordon as Project Manager. This report is in three volumes.

- I. Technical Report
- II. Operation Manual
- III. Program Descriptions

The Boeing Program Manager for this work was R. W. Edsinger, and A. W. Warren was the principal investigator.

For completeness, the summary sections 1.1 and 1.2 of Volume I have been repeated in the Operation Manual, Volume II.

## 1.0 INTRODUCTION

Energy storage systems for the utilization of Intermittent power sources have received increased study over the past few years. However, the type and degree of storage required for optimal utilization of wind energy and the total costs and utility of the resulting wind turbine/generator/storage system have not been thoroughly analyzed. The purpose of the SIMWEST (Simulation Model for Wind Energy Storage) program described in this document is to provide a tool for performing this needed analysis. It is a tool to aid in the design of an optimal wind energy system for a given application and to allow the resulting system to be evaluated and verified through realistic simulation.

SIMWEST consists of a library of system components and a precompiler program which allows these components to be put together in building block form. The present library contains components for five types of energy storage systems. They are pumped hydro, battery, thermal, flywheel, and pneumatic. The SIMWEST program, as described here runs on the UNIVAC 1100 series of computers.

Other computer programs exist for the simulation of wind systems and various forms of energy storage. However SIMWEST is the only program capable of simulating total wind systems containing any one or combination of the above types of storage and at the same time having the flexibility and depth required to perform thorough and meaningful parameter studies.

### 1.1 GENERAL APPROACH

The structure and much of the software for the SIMWEST program is based on a computer program called EASY, which was previously developed by Boeing Computer Services, Inc. (BCS). SIMWEST consists of two basic programs, and a library of system, environmental, and load components. The first program, the Model Generation Program, is a precompiler which generates computer models (in FORTRAN) of complex wind energy generator/storage/application systems, from user specifications using SIMWEST library components. The second program exercises the resulting computer model to perform cost and potential utilization

tion analysis. It handles input, output, integration of system dynamics, and iterates to obtain convergence of variables involved in implicit loops. The combination of these two programs provides a powerful tool for analyzing alternate storage system designs.

Figure 1-1 shows the general organization of the SIMWEST program. In addition to the two programs described above, there is a third which performs file maintenance. It is used to incorporate user supplied data for new subsystem models. Although the program is shown to be made up of a number of subprograms, it can be executed as a single batch program by supplying the model description control cards and the control cards describing the desired analysis to be performed and the desired tabular and/or plotted output.

## 1.2 SIMWEST LIBRARY

### 1.2.1 Overview

The SIMWEST library is listed in Table 1-1. It is made up of five types of components: physical, environmental, load, logical, and utility.

Physical components encompass such things as motors, generators, transmissions, flywheels, etc. These components model actual physical hardware which might be used in a wind energy system. The selection of the particular SIMWEST library set of physical components was based on the requirement that it be capable of modeling five types of energy storage systems mentioned previously: thermal, flywheel, battery, pumped hydro and pneumatic.

The degree of detail in the component models is based upon two design criteria. First, all models should contain sufficient detail to simulate all physical characteristics and constraints having significant impact on the systems overall cost effectiveness. Second, the models should be designed to minimize computer time and required user specification. It is assumed that a typical SIMWEST simulation might cover a time span of one year. Thus

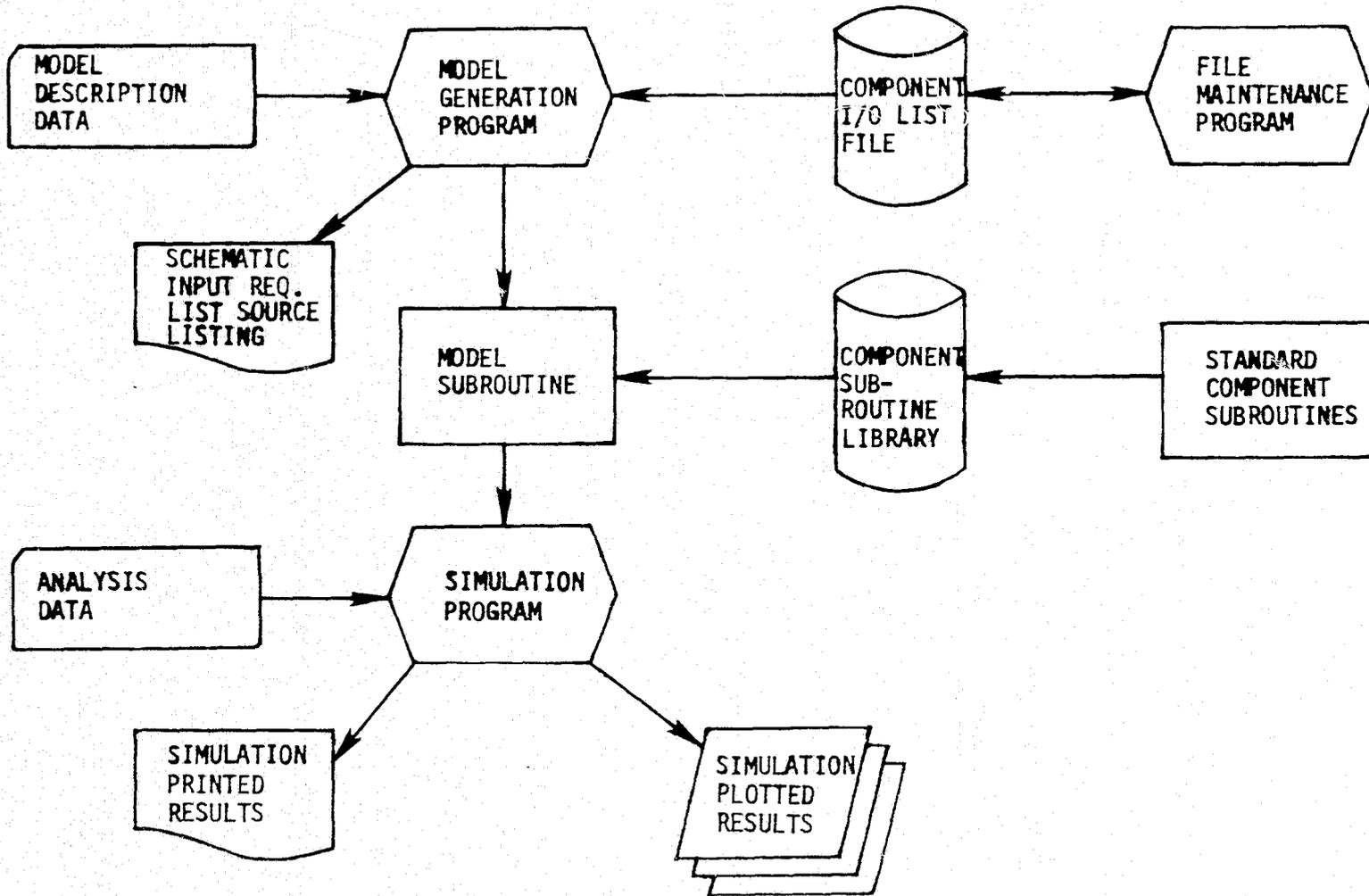


FIGURE 1-1 SIMWEST PROGRAM ORGANIZATION

TABLE 1-1 SIMWEST LIBRARY COMPONENTS

<u>PHYSICAL</u>		<u>ENVIRONMENTAL</u>	
WIND TURBINE	WT	WIND	WD
TURBINE/GENERATOR	WP	AMBIENT TEMP	TP
AC INDUCTION GEN.	GE		
FIXED RATIO TRANSMISSION	GR	<u>LOAD</u>	
RECTIFIER	RE	ELECTRICAL LOAD	LO
BATTERY	BA	THERMAL LOAD	TL
INVERTER	IV		
ADMITTANCE	AD	<u>LOGIC</u>	
COMPRESSOR (PNEUMATIC)	CO	POWER DIVIDER	PD
ADIABATIC HEAT EXCHANGER (INPUT CYCLE)		POWER ACCUMULATOR	PA
ADIABATIC HEAT EXCHANGER (OUTPUT CYCLE)	HX	PRIORITY INTERRUPT SWITCH	PI SW, SX, SY, SZ
PNEUMATIC STORAGE VESSEL	HY		
BURNER	CS	<u>UTILITY</u>	
TURBINE (PNEUMATIC)	BN	COST MONITOR	CM
INDUCTION MOTOR	TU	SATURATION	SA
VARIABLE RATIO TRANSMISSION	MO	RANDOM NUMBER GENERATOR	RN
FLYWHEEL/CLUTCH	TR	TEST FUNCTIONS	AF
PUMP (HYDRO)	FL	TABLE LOOKUP	FU, FV
TURBINE (HYDRO)	PU	TRANSFER FUNCTION	IT, LA, LL, TF
HYDRO STORAGE	HT	ARITHMETIC ELEMENT	MA, MB, MC
THERMAL STORAGE	HS	HISTOGRAM	HG
UTILITY	TS	TAPE READ	TA
	UT	TIME CONVERSION	TI

from a computer run time and economic impact point of view a simulation step size of between 15 minutes and one hour seemed reasonable.

As a result of the above two design criteria many physical components, such as the electrical components, were modeled mainly in terms of power flow and steady state response. This lack of detail is consistent with the 15 minute time step and with the concept that the important transients are on the time scale of demand curves or weather patterns, i.e. an hour or more, rather than on the time scale of electric motor transients of a few seconds. If short electric transients were to be modeled, much detail would need to be added to the component models which would greatly increase the user's task of specifying the model. Further, the simulation time step would have to be reduced to a fraction of a second so the model would not only be much larger but computer runs would be much costlier.

Environmental components are those which simulate environmental conditions. In the present SIMWEST library these conditions are wind speed and ambient temperature. These variables are generally used as inputs to physical components. Environmental component output can either be computed from measurement data provided by the user on a data tape, or from randomly generated data, based on user furnished profiles.

The load components in the SIMWEST library are used to simulate various types of power demand. They also monitor how well the system meets the simulated demand and compute the value of the energy delivered by the wind energy system to the load. Like the environmental components these components may be computed from actual measurement data or from randomly generated data based on user furnished load profiles.

The library's logical components are the power dividers, power accumulators, switches and priority interrupts. Although physical hardware could generally be built to serve the function of the logical components, they are not meant to represent any particular piece of existing hardware. Instead, they are

Idealized components that allow the user the flexibility of modeling the wide variety of control logic which a wind energy storage system would require. In practice, the control function might be performed by a control room operator using a predefined control strategy or by use of a minicomputer.

Finally, the utility components include such things as the tape read, the histogram and the cost monitor. These components serve only to help the user run the simulation and analyze its results.

### 1.2.2 Storage Subsystems

Figures 1-2 through 1-6 give example configurations of the five types of storage subsystems which can be modeled with the present SIMWEST library. For illustrative purposes the number of variables shown passed between components is limited. A description of the variables being passed is given in Table 1-2.

A total wind energy system will generally be made up of elements from a number of different subsystems (see Figure 1-8). In addition, the SIMWEST program can be used for models which include networks of storage subsystems of the same type or a network of wind generators.

### 1.2.3 Logic Components

The capability for modeling complex system control logic is provided by the power divider, power accumulator and priority interrupt components. Both the divider and accumulator operate on a priority basis. The priority interrupt is used by other system components to change the priority setting of the divider and accumulator.

The power divider has one input power port and four output power ports (not all output ports need be used for a given simulation). The divider also has

TABLE 1-2 PARTIAL LIST OF COMPONENT INPUTS AND OUTPUTS

SYMBOLS

P	POWER
RE	POWER REQUEST
MP	MAXIMUM POWER
RS	ROTOR SPEED
T	TEMPERATURE
TA	AMBIENT TEMPERATURE
M	MASS FLOW RATE
H	RESERVOIR HEIGHT
LD	THERMAL LOAD DELIVERED
W	WIND VELOCITY
GR	GEAR RATIO
EF	EFFICIENCY
INT	INTERRUPT FLAG
TSO	MINIMUM AIR TEMPERATURE
PR	PRESSURE
PS	PRIORITY SEQUENCE
WY	WEEK OF YEAR
DW	DAY OF WEEK
TD	TIME OF DAY
SP	SURPLUS POWER
VAR	FILE READ VARIABLE

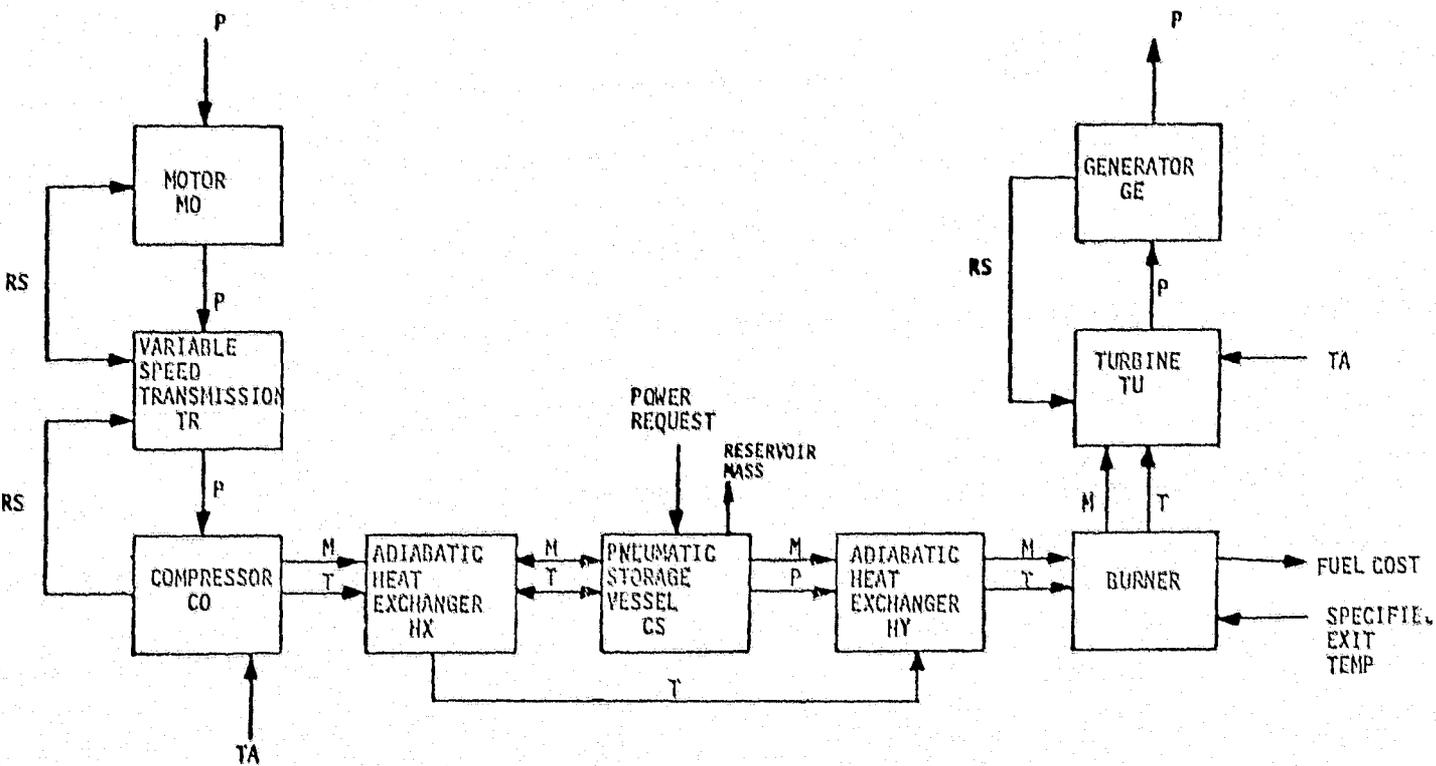


FIGURE 1-2 PNEUMATIC STORAGE SUBSYSTEM

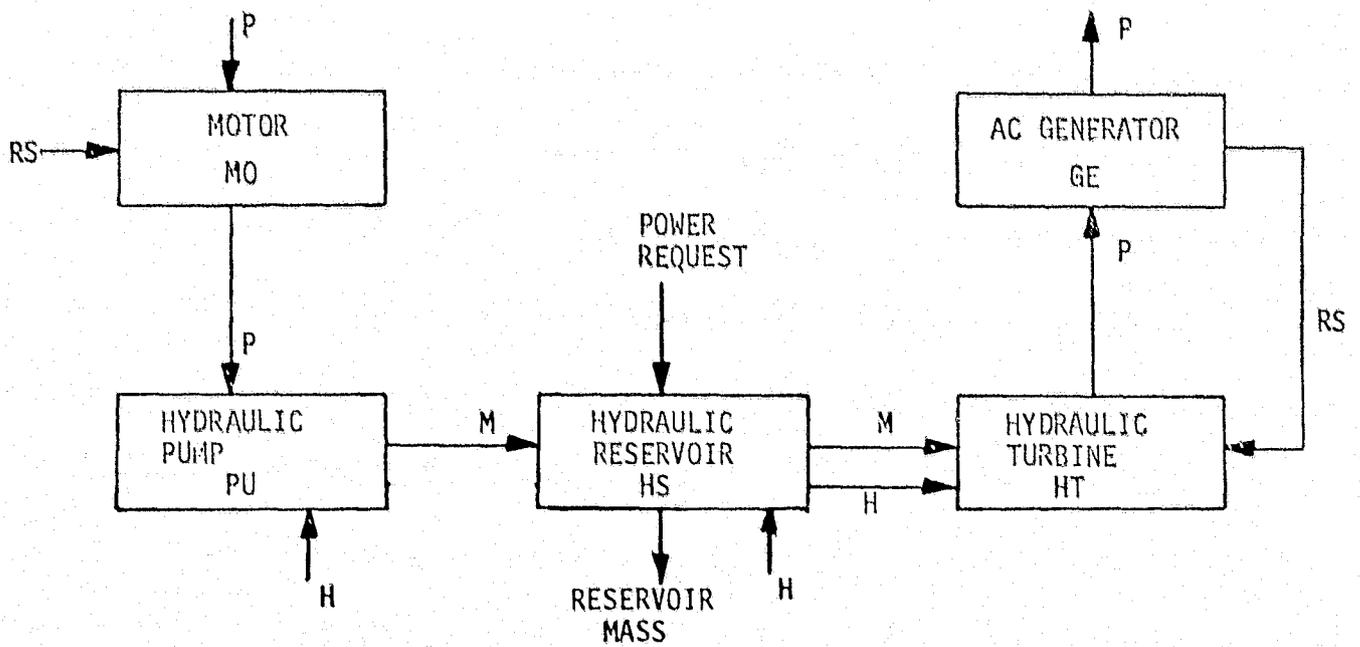


FIGURE 1-3 PUMPED HYDRO STORAGE SUBSYSTEM

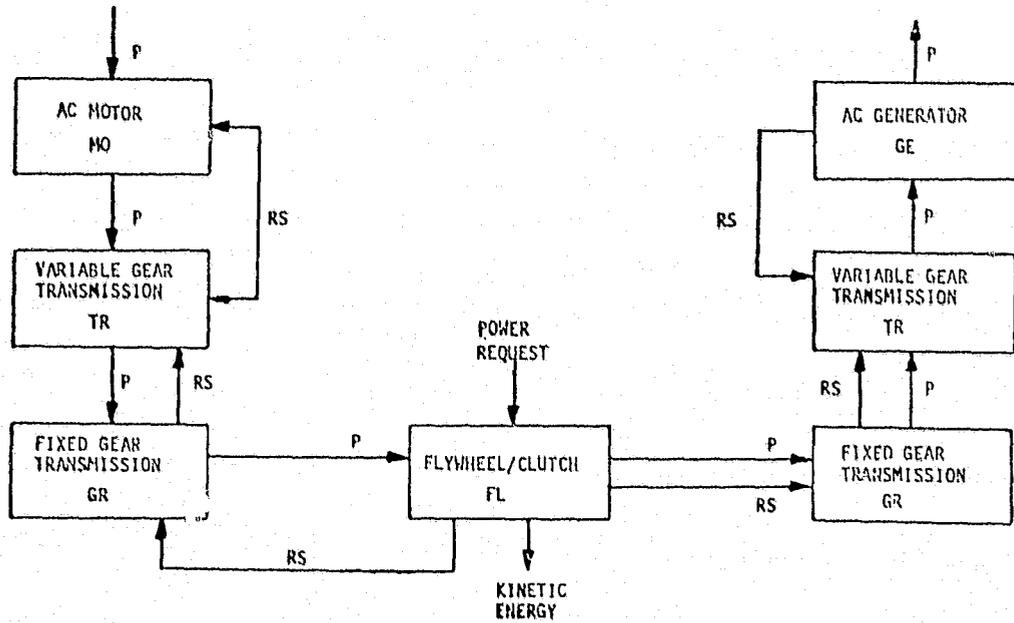


FIGURE 1-4 FLYWHEEL STORAGE

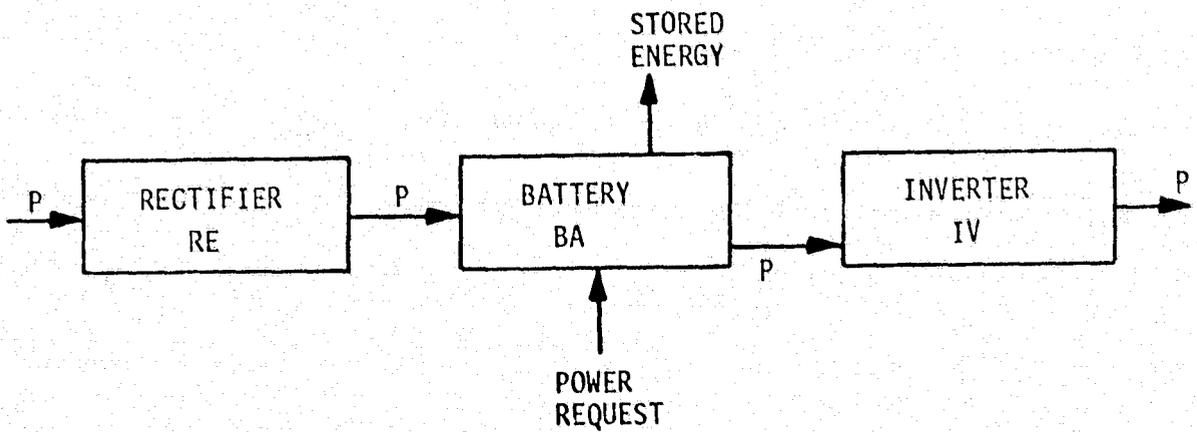
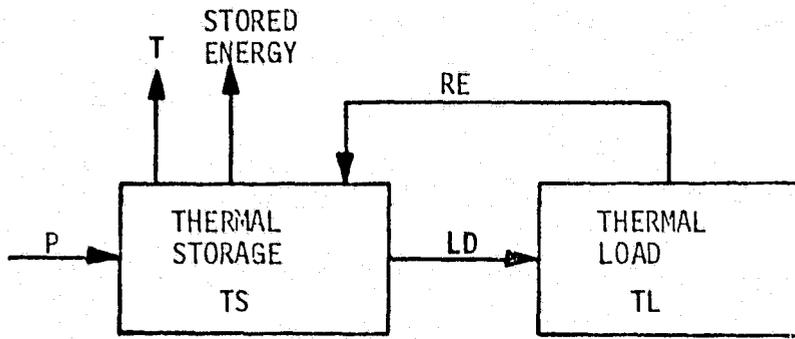


FIGURE 1-5 BATTERY STORAGE



LD = LOAD DELIVERED

FIGURE 1-6 THERMAL STORAGE

an input request associated with each of its output power ports. These power requests generally come from a component with which the output power port is directly or indirectly connected. The user specifies priorities of either 0,1,2,3, or 4 to be associated with each of the output ports. If the input power to the power divider exceeds that requested of the port with highest priority (priority 1) then the excess power goes to the port with the next lower priority. This process continues until either all power is distributed or all requests of non-zero priority ports are met. A port with zero (0) priority will never receive power. Such ports are included so that the port may be connected to a component but transmit power only in critical situations, say, when a battery has been in discharge state for a critical amount of time. In these situations, the connected component would have to change the zero priority setting of the power divider by use of a priority interrupt.

Two or more ports may be assigned the same priority in which case the user may specify weights to be associated with each port. Then if there is not enough power available to satisfy all requests of equal priority the power is divided between them in proportion to the user specified weights.

The power accumulator is similar to the divider except that instead of distributing power from a single input port between four output ports, it accumulates power from four input ports and sends it out through a single output port. The power accumulator also accepts output power requests from the component connected to its single output power port and it outputs requests for each of its input ports in order to service the output power request.

In addition to the actual power delivered to each input port, the power accumulator also accepts information as to the maximum power that can be delivered to that port. These values are used by the accumulator to determine how to distribute its power request between its four input ports. If the input power request exceeds the maximum deliverable power for the port of highest priority, then the remainder is shifted to the port with the next lower priority. This process continues until either the power request has been completely distributed between the highest priority input ports or all input

ports have requests equal to their maximum deliverable power. An example illustrative of the use of power dividers and power accumulators is given in Figure 1-7.

Here the wind turbine distributes power first to satisfy the request from load 1. If there is power left over, it then tries to satisfy the request from the battery. Finally, if the battery is full or if its charging rate is met, then the excess power goes to the flywheel. The battery is connected to the wind turbine and also has a priority zero connection to the utility. Thus, if the battery remains in a discharge state for more than a specified amount of time, it can change the utility priority (from 0 to 1) to receive the needed power.

Also in Figure 1-7, we see that load 2 prefers to draw power from the flywheel before turning to the battery. This configuration tends to keep the flywheel as discharged as possible, using it primarily as a means to absorb large influxes of power.

Figure 1-7 is a rather simple configuration used for illustrative purposes. A more complex configuration is shown in Figure 1-8.

#### 1.2.4 SIMWEST Output

There are three basic forms of SIMWEST output to facilitate the analysis of wind energy storage systems; line printer plots, histograms of system variables and time sequenced output of variable values. To enhance the usefulness of these outputs each SIMWEST library component is associated with a number of output variables. Prior to simulating a given system the user specifies which of these variables he wants plotted. For plotted output he may select to have the independent variable be the plot time or any of the other variables. For example he may want to plot the energy of pneumatic storage as a function of time and/or as a function of storage versus temperature. If the user wants a time sequenced listing of all variable values

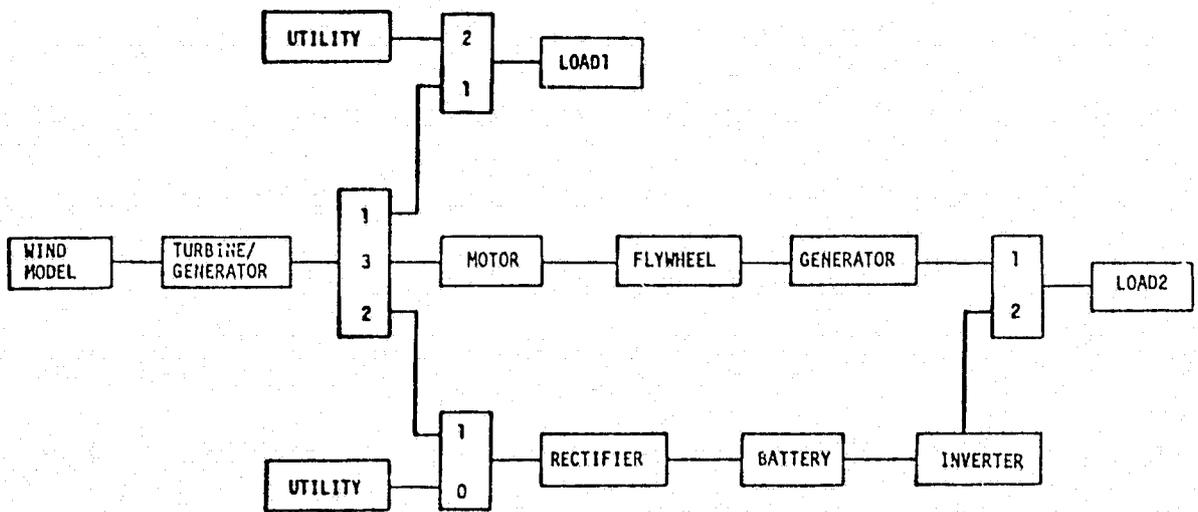


FIGURE 1-7 EXAMPLE OF POWER DIVIDER & ACCUMULATOR USE

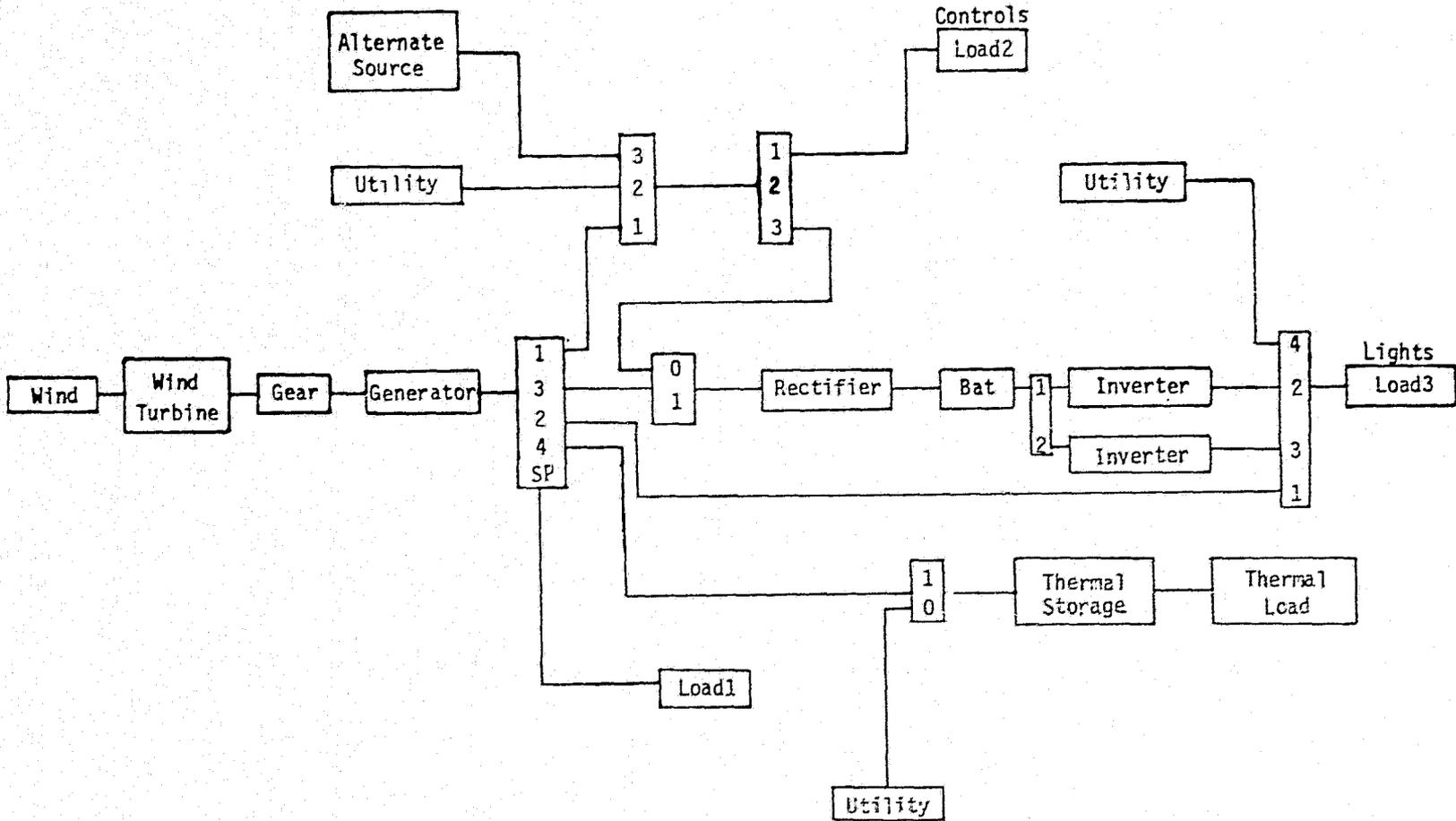


FIGURE 1-8 PLUMBROOK CONFIGURATION FOR PARAMETER STUDY

he just specifies the time step between printouts. The listing of all variables has proven to be a useful tool in understanding the performance of the storage system under consideration and a valuable aid in validating the system design.

## 2.0 MODEL GENERATION

The Model Generation program design is based on the assumption that the system analyst will begin by constructing a schematic diagram of the system he wishes to analyze. This schematic will be comprised primarily of standard SIMWEST library components. Standard library components include wind turbine, wind models, AC induction motors, inverters, rectifiers, etc. If a particular system cannot be modeled with existing standard components, the analyst may construct the model by including appropriate FORTRAN statements in his system description.

All interconnections between standard components are accomplished by the Model Generation program. The analyst merely specifies each standard component in the schematic diagram and all of the components that provide inputs to that component. The Model Generation program then generates names and the proper interconnections between the specified components. This is accomplished by matching the input quantities required by each standard component to the output quantities of the specified input components.

After processing the complete system model description, the Model Generation program generates a schematic diagram of the model showing the interconnections between standard components and the quantities such as power, pressure, temperature, mass flow rates, etc., that pass through each interconnection. This schematic is produced on the lineprinter to provide a rapid graphic check on the program's interpretation of the model description.

In addition, the program produces a list of input data that will be required by each component to complete the model description. Both the scalar parameters and tabular data required for the analysis are included in this list. The program assumes that any quantity not supplied by another component will be supplied as a fixed parameter by the analyst. Thus requests for non-parameter items in the input data list will reveal any connection that was omitted from the system model description.

## 2.1 MODEL DESCRIPTION

The Model Generation program is a precompiler program which accepts model description instructions and from these instructions generates a FORTRAN model of a system. These instructions, referred to as "program commands," are made up of one or more words. In addition, the system model description contains numeric values, standard component names, and standard input and output quantity names.

The Model Generation commands may be best introduced with a simple example of their use to describe a wind turbine system. Figure 2.1-1 shows an analyst's schematic of a wind turbine model that has been constructed using standard components on a SIMWEST schematic form. The standard component names used in this sample are:

- WD - Wind Model
- WT - Wind Turbine
- TI - Time Conversion
- HG - Histogram Generator
- GR - Fixed Ratio Transmission
- LO - Electrical Load
- GE - AC Induction Generator

The SIMWEST description of this model would be as follows:

### Example 2.1

```
LIST STANDARD COMPONENTS
MODEL DESCRIPTION      WIND TURBINE TEST CASE
LOCATION=15      TI
LOCATION=11      WD      INPUTS=TI
LOCATION=31      WT      INPUTS=WD
```

SIMWEST SCHEMATIC FORM

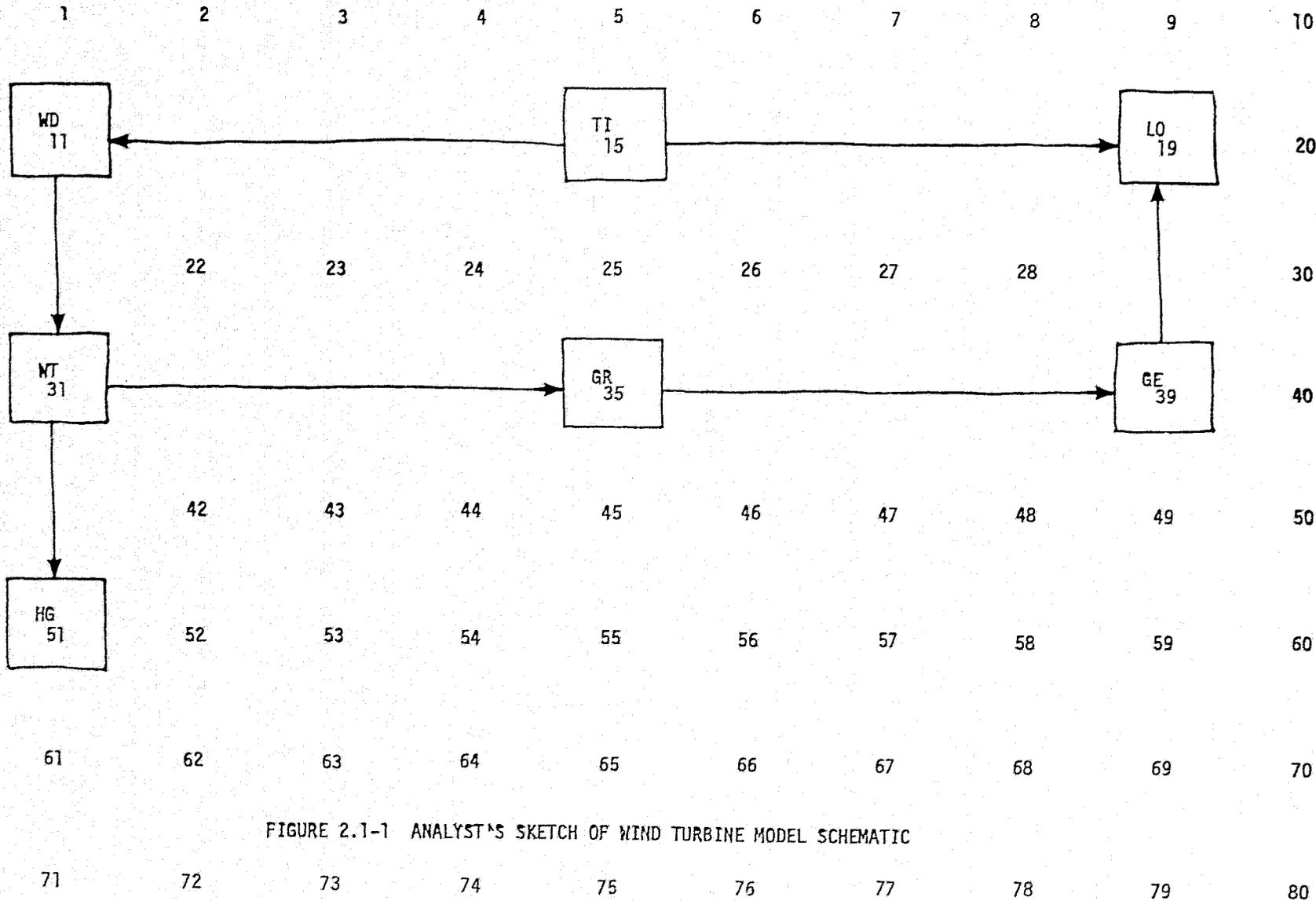


FIGURE 2.1-1 ANALYST'S SKETCH OF WIND TURBINE MODEL SCHEMATIC

Example 2.1 (Cont.)

```
LOCATION=35      GR      INPUTS=WT
LOCATION=51      HG      INPUTS=WT(P =FIN)
LOCATION=39      GE      INPUTS=GR
LOCATION=19      LO      INPUTS=GE, TI
END OF MODEL
PRINT
```

The model description consists of a statement as to the location of each component in the schematic and a list of all components that provide inputs to that component. The location of the component in the schematic is used for a line printer drawn schematic of the model, such as shown in Figure 2.1-2. In the line printer schematic the input and output quantities such as powers (P2 WT, P2 GE, P2 GR) are shown on the various connecting lines.

2.1.1 Phrases and Delimiters

The system model description is interpreted by the Model Generation program as a series of "phrases", which can appear in a free field format in any position on a data card. Phrases must be separated by any one of the delimiter symbols shown in Table 2.1-1.

Table 2.1-1

Model Generation Program Language Delimiters

= equal sign  
, comma  
( left parenthesis  
) right parenthesis  
three or more blanks



### 2.1.2. Command Phrases

The Model Generation command phrases are described in this section in a logical sequence similar to that in which they appear in system model descriptions.

#### MODEL DESCRIPTION

The MODEL DESCRIPTION command phrase indicates the start of a new system model. This phrase may be followed, (on the same card), by a title of up to 60 characters. This title will be used to identify various program output schematics, lists and program listings. In Example 2.1, the title was "Wind Turbine Test Case."

#### LOCATION

The LOCATION command phrase indicates the start of the description of a new component in the system model. This command must be followed by a numeric value phrase that specifies the location of the new component on the model schematic. Thus in the example of Figure 2.1-1, the location number of the wind model WD was 11 and the wind turbine WT was 31, etc. To be a valid component location, the last two digits of this number must comprise a number between 1 and 80. The hundreds column is used to specify additional pages as needed for the schematic. Thus the numbers:

1, 13, 51, 80

would be valid location numbers for components on the first page, (PAGE 0), of a system schematic. These same locations on the second page of the schematic, (PAGE 1), would be:

101, 113, 151, 180

The location number phrase is followed by the name of the component at that location. Component names are discussed in Section 2.2.

A LOCATION statement should be given only once for each component. That is, once a LOCATION statement is started for a component the complete description of all inputs to that component should be given.

### INPUTS

The INPUTS command phrase indicates that the following phrases contain the names of the components that provide inputs to the component at the specified location. Thus in the example of Figure 2.1-1, the electric load at location 19 which receives inputs from generator GE and the time source TI was described as:

```
LOCATION=19      LO      INPUTS=GE,TI
```

In this example the command phrase INPUTS is followed by two component names. As many component names as are necessary to specify the inputs to a particular system component may be included in each component description.

For some system components there are multiple input and/or output ports. For example, a power divider has four input power ports. When specifying the connections between such components, it is advisable to specify which ports are to be connected. This is done by adding the port numbers to be connected after the name of the input component. Thus, the wind turbine to transmission connection could have been more explicitly described as:

```
LOCATION=35      GR      INPUTS=WT(2,1)
```

This says that port 2 of the wind turbine (WT) drives port 1 of the transmission (GR). Any quantities which have no port numbers are considered "universal ports" for input connections. Thus, the GR input of GR is connected

up to GR WT, and the RS input of WT is connected up to RSIGR by the above command. If the port designations are omitted, as they were in example 2.1., the connections will be made to the first available input port starting with the minimum port number. Once a connection has been made to an input port, those input quantities that are connected are unavailable for further connections. An exception is made when the physical quantities of both input and output are specified. This method of specifying connections is described in the following paragraphs.

For certain components, such as control elements, the inputs to the component can be any physical quantity in the model. For these components, the input component names must be supplemented by the name of the particular output quantity that is to provide the input.

As an example, consider a component that represents a linear first order lag transfer function. If the transfer function component's input, FIN, was to be the rotor speed of the wind turbine WT in example 2.1, then the statement:

```
LOCATION=53      LA      INPUTS=WT(RS=FIN)
```

would indicate to the program that of the outputs of the wind turbine, the output rotor speed, RS, was to be used as the input, FIN, to the transfer function, LA.

To summarize, there are three levels of connection specification:

1. Default (only component names are specified)

Connections are made between all unconnected inputs and outputs for the first ports for which a match of physical quantity names occurs.

## 2. Ports Specified

Connections are made between matching physical quantities for all unconnected inputs and outputs of the specified ports.

## 3. Physical Quantities Specified

Connections are made between only those quantities specified. Previous connections can be over-ridden, providing the three character physical quantity name of the previously connected variable is used. For example, the phrase

```
LOCATION=19      LO      INPUTS=GE,GE(P,2=MP2),TI
```

will replace the input parameter MP1LO by MP26E and then override the connection MP2GE and substitute P2 GE as the LO input.

END OF MODEL

The END OF MODEL command phrase indicates that model description has been completed and that the Model Generation program should proceed with the generation of the model subroutines.

PRINT

The PRINT command phrase causes the program to: (1) draw a schematic of the system model, as shown in Figure 2.1-2; (2) print a list of input requirements for the model; and (3) print a source listing of the FORTRAN subroutines that were generated for the model. The Model Generation program then terminates.

PUNCH

The PUNCH command phrase has the same effect as the PRINT command, but in addition a FORTRAN source deck of the system model is produced.

## FORTRAN STATEMENTS

The FORTRAN STATEMENTS command phrase allows the system analyst to supplement the library components with FORTRAN statements. Using this feature, the analyst can introduce his own program logic, DO loops, etc., as necessary to model any system feature not obtainable with standard library components.

One of the common uses of the FORTRAN STATEMENTS command is to input large tables into the model. Two function subprograms TBLU1 and TBLU2 are provided for this use. They perform linear interpolation from one and two dimension tables, respectively. TBLU1 is in general called in the form

$$F = \text{TBLU1}(X, \text{TAB}(4), \text{TAB}(4+N), I, \pm N),$$

where F is the interpolated value at the desired point X, TAB is a one dimension table with dimension N, TAB(4) is the independent variable and TAB(4+N) is the dependent variable list, I = 0 for equal spaced data, I = 1 for unequal spaced data, and the dimension N is specified as the last variable if linear extrapolation is desired, and -N is specified if truncation is desired outside the table limits. Similarly, TBLU2 is in general called using the form

$$F = \text{TBLU2}(X, Y, \text{TAB}(4+M), \text{TAB}(4), \text{TAB}(4+M+N), IX, IY, \pm N, \pm M, N, M),$$

where X and Y are the values of the primary and secondary independent variables, N and M are the dimensions of the primary and secondary variable arrays, IX and IY are indicators for equal spaced or unequal spaced data as above, and the sign convention on N and M is positive for extrapolation, negative for truncation.

The FORTRAN STATEMENTS command would normally be used only when some portion of the system cannot be modeled with library components. Then using this feature of the program, the analyst must perform many of the detail connections

and naming of variables, that are normally accomplished by the Model Generation program. In return for these added tasks, the analyst gains a great deal of additional freedom and flexibility in forming details of his system model. Non-executable code such as common blocks must precede the first component definition and executable code should come after a component has been defined for the iteration logic to work properly.

ADD STATES  
ADD VARIABLES  
ADD PARAMETERS  
ADD TABLES

The ADD commands may be used in conjunction with the FORTRAN STATEMENTS to add states, variables, parameters, and tables that occur within the FORTRAN statements, to the system model. Quantities that are not specified by one of these commands cannot be accessed or manipulated by the Analysis Program.

Before discussing these commands, a few definitions of terms are in order.

States:

States are those quantities in the system model that are described by first order differential equations. The state variables are the result of integrating the set of first order differential equations that comprise the dynamic system model. The number of states equals the order of the system model. The states are dynamic, time varying quantities during most simulation studies. The initial values, (initial conditions), of the states must be input as part of the system model description.

**Variables:**

Variables are all other dynamic time varying quantities in the system model that are not states. In general, variables are related to states by algebraic relationships.

**Parameters:**

Parameters are constant scalar quantities in the system model. Parameters can be manipulated by the analyst to alter the system model. All parameter values\* should be input as part of the system model description.

**Tables:**

Tables are constant nonscalar quantities in the system model. Tables are used to represent algebraic functional relationships with one or two independent variables. All table values must be input as part of the system model description.

The format for the ADD commands is that the command is followed by one or more phrases that contain the names of the states, variables, parameters, or tables. In addition to each table name, a number, specifying the amount of storage to be allocated for that table must be given. This number is positive if the table is two dimensional and negative if one dimensional, with absolute value determined by the formula:

$$N = 3 + I + J + D$$

N = the total storage required by the table,  
in words.

---

\* For certain components, default values are provided for some parameters.

I = the number of data points in the primary independent variable table.

J = the number of data points in the secondary independent variable table. (J=0 if there is only one independent variable.)

D = the number of data points in the dependent variable table. (D=1 if there is only one independent variable. D=I\*J if there are two independent variables.)

The following example illustrates the use of FORTRAN STATEMENTS in the parameter study model:

Example 2.2

```
MODEL DESCRIPTION      PARAMETER STUDY
.
.
.
ADD TABLES = WIND,802
LOCATION = 41  TI
FORTRAN STATEMENTS
C      READ WIND VELOCITY DATA
      WIND = TBLU2(TD TI ,DY TI ,WIND(35),WIND(4),
1 WIND(59),0,0,24,-31,24,31)
LOCATION = 71  WD  INPUTS = TI
.
.
.
```

In this model, Fortran is used to input wind velocity data. The wind table, denoted WIND, consists of up to 31 days of hourly wind speeds. Hence, as described previously, the total storage required is  $3+24+31+24*31=802$ . The Fortran is inserted after time of day and day of the year are computed in T1. In this case,  $N=24$ ,  $M=31$ , the data is equal spaced, and extrapolation is used to provide velocity data over each 24 hour period. The variable WVIWD is the name at the wind input to WD generated by the precompiler. Fortran insertion in the model ends when the LOCATION=71 ... command is read and a call to the subroutine WD is then generated.

#### LIST STANDARD COMPONENTS

The LIST STANDARD COMPONENTS command phrase causes the program to print a list of all standard components. For each standard component, lists of inputs, outputs, and tables for that component are provided. For each input, the physical quantity name and port number is given. For each output, the physical quantity name, port number, and the letter S, if the quantity is a state is given. For each table, the table name, the number of independent variables and the maximum amount of storage allowed is provided. This command is usually given as the first command of a model description and will result in a list of all standard component information as the first output from the Model Generation program.

#### 2.2 NAMING CONVENTION

All standard components are given names consisting of two characters, the first of which is alphabetical. Thus we have WT for wind turbine, GE for generator, WD for wind model, etc. Where multiple components of the same type are required, the second character is used to distinguish between the different models of the same basic component type. A specific component in a model can be distinguished from other components of the same type by adding one

more character to the standard component name. This character is usually numeric but can also be alphabetical or blank. Thus a given model can contain up to 37 different components of the same standard component type. For example, a model with ten different wind turbines might have these components designated as:

WT1,WT2,WT3,.....,WT8,WT9,WTA

### 2.2.1 Variable, Parameter, and Table Naming Conventions

All of the input, output, and tabular quantities required by each component in a system model must have unique FORTRAN names. These quantities are given names consisting of up to three characters that describe the physical quantity they represent.

Since a single component may have several inputs or outputs of the same physical quantity, the program adds the port number to the second or third character of the physical quantity name to prevent such a duplication.

The physical quantities that are outputs of a given component are identified by adding the three character name of that component to the three character name of the physical quantity. In this way, unique six character FORTRAN names are generated for all output quantities of the system model components.

Input quantities to a component that are driven by another component carry the names of the component that drives them. Any inputs that are not driven by other model components are assumed to be parameters and are assigned the name of the component for which they are an input.

If a component should require tabular data as an input, unique table names are generated just as scalar input quantity names by adding the component

name to the table name. A pictorial representation of the character assignment in component, variable, and table names is given in Figure 2.2-1.

## 2.3 MODEL SCHEMATIC

The Model Generation program produces a schematic diagram of the system being modeled. This schematic is crude but is inexpensive and does not have the flow time delays associated with more elaborate plotting methods. Its purpose is to provide a means of rapidly locating errors in the model description.

In order to construct a schematic diagram in an efficient manner with a reasonable size program, it was necessary to establish some simple rules for symbol generation, component connection paths, and labeling. If these rules are kept in mind when laying-out a schematic for the system, the SIMWEST produced schematic will match that developed by the analyst. If the rules are violated by the analyst's schematic, the SIMWEST schematic should still be correct, but may contain some unusual component connection paths and some labeling information may be overwritten.

### 2.3.1 Standard Schematic Form

The SIMWEST schematic diagrams are produced on a standard 11" by 14" line-printer page with 80 component locations per page. A standard form containing only the location numbers can be obtained by executing the Model Generation program with the single program command, PRINT. This form can then be reproduced and the copies used as forms for drawing system model schematics.

### 2.3.2 Input Quantity Labeling

The names of the physical quantities that are input to one component from another component are listed adjacent to the downstream component symbol.

INPUT/OUTPUT OR TABLE NAMES

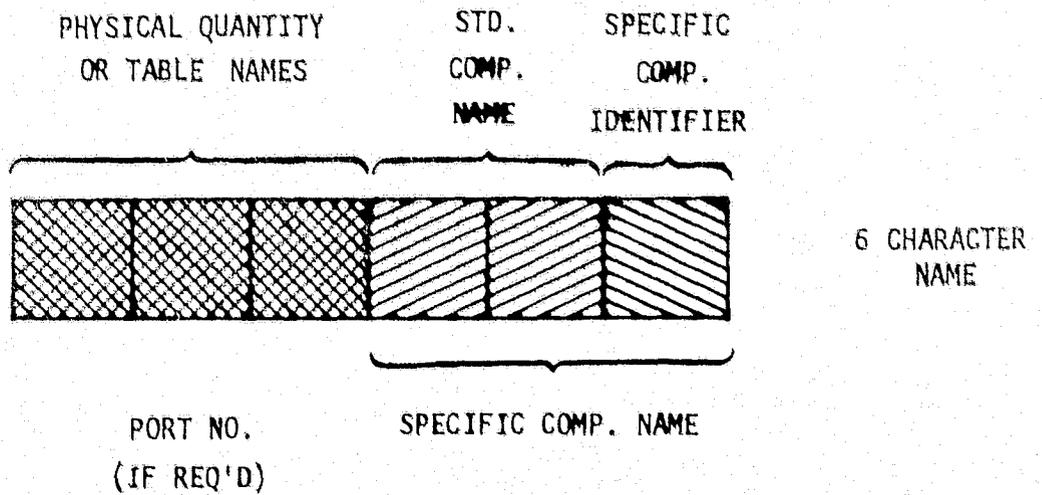


FIGURE 2.2-1 CHARACTER ASSIGNMENT INPUT/OUTPUT OR TABLE NAME

These labels are placed near the connecting line that joins the two components. Since these names are composed of the physical quantity name and the name of the component that generates the information, the source of the input is evident from the name itself. Parameter and tabular inputs to a component are not shown on the schematic. These constant inputs are described in the Input Requirements List.

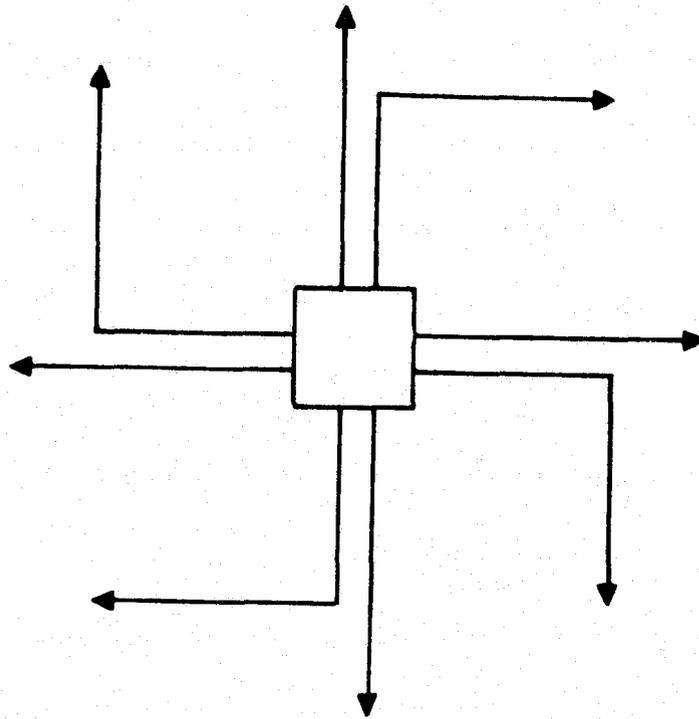
### 2.3.3 Component Connection Paths

In order to keep the core requirements and run time of the SIMWEST schematic drawing subroutine small, it was necessary to limit the types of connecting paths between components to a few basic routes. These paths are shown in Figure 2.3-1. Connections between components on the same horizontal or vertical line are straightforward. However, connections between components that do not share a horizontal or vertical line require at least a two segment path. These paths have been arbitrarily chosen to follow a clockwise route. It is therefore advisable that components that are on diagonal locations be placed in a clockwise sequence. If counter-clockwise flow between components is necessary, it can be accommodated by placing the components on the same horizontal or vertical lines.

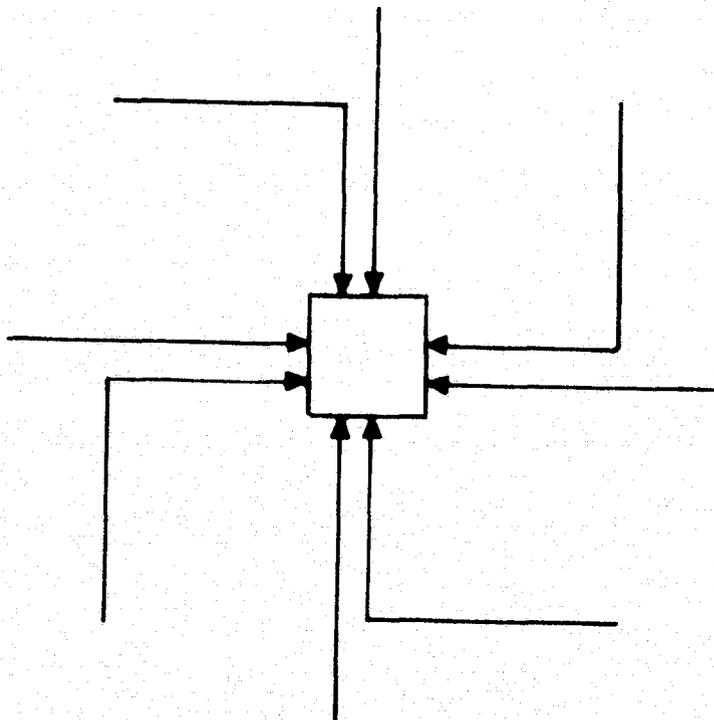
The SIMWEST schematic drawing subroutine makes no attempt to go around components that get in the way of a connection path. Such components are "run-over" by the connecting line.

### 2.3.4 Additional Pages

The SIMWEST schematic diagram may be broken down into as many pages as are necessary. No attempt is made to draw connecting paths between components located on different pages. It is therefore advisable to minimize the number of connecting paths between pages. This can usually be done by grouping



POSSIBLE OUTPUT PATHS



POSSIBLE INPUT PATHS

FIGURE 2.3-1 COMPONENT CONNECTION PATHS

components with many interconnections on the same page and placing page boundaries between such groups of components.

### 2.3.5 Guidelines for Schematic Layout

The following guidelines may help in creating schematic layouts that can be duplicated by the SIMWEST program.

1. Try to place connected components on the same horizontal or vertical line.
2. Avoid placing components on adjacent location points.
3. Place diagonal components so that flow is clockwise.
4. Group components to minimize flow paths between pages.

### 2.4 WARNING MESSAGES

One or more of the following warning messages will occur if the program is unable to interpret a portion of the model description or encounters problems in assembling the system model. These messages will be preceded by: \*\*\*WARNING \*\*\* or \*\*\*NOTICE \*\*\*. The symbols xxx and zzz are used to indicate phrases from the model description that are included as part of the warning message. The following messages are listed in alphabetical order:

1. CAN'T IDENTIFY xxx AS A STANDARD COMPONENT

xxx will contain the first two characters of the phrase which cannot be identified as a command or standard component. This message will often follow other warning messages as the program makes successive attempts to interpret the given phrase.

2. CAN'T IDENTIFY xxx AS A VALID INPUT COMPONENT TO zzz

The component xxx cannot be found in the list of components for the current system model.

3. CAN'T LOCATE xxx AS AN INPUT COMPONENT TO LOCATION n

This message indicates that the component xxx, which provides inputs to location n in the schematic, has not been assigned a location number. Check for a missing LOCATION statement or misspelling of the component name.

4. COMPONENT xxx DEFINITION WASN'T COMPLETED BEFORE STARTING THE DEFINITION OF COMPONENT zzz

The command INPUTS was not given between the component names xxx and zzz. Check for proper spelling of INPUTS and a valid delimiter after the phrase xxx.

5. COMPONENT xxx HAS ALREADY BEEN DEFINED

The component xxx was defined in a previous LOCATION statement.

6. LOCATION NO. xxx FOR COMPONENT zzz HAS LAST TWO DIGITS OUTSIDE THE ALLOWABLE RANGE 1 TO 80. NO SYMBOL WILL BE PLACED IN SCHEMATIC FOR THIS COMPONENT

This message will occur at the end of the model description for a component zzz which has an invalid location number. The system model may still be valid but the schematic will not contain this component.

7. NO xxx OUTPUTS MATCH UNSATISFIED zzz INPUTS

Check that it was intended to drive component zzz with component xxx or that the inputs to zzz have been previously satisfied by other component connections.

8. TABLE NAME xxx MUST BE FOLLOWED BY A NUMERIC DIMENSION RATHER THAN zzz

When using the ADD TABLES command, it is necessary to provide the maximum amount of storage to be allocated for the table as well as the table name. This storage value must be a numeric quantity.

9. xxx IS NOT A VALID INPUT QUANTITY OR PORT DESIGNATION FOR COMPONENT zzz

The phrase xxx cannot be located as one of the input quantities or input ports of the component zzz. No connections will occur. Check the list of standard components for the proper spelling or port designations for this component.

10. xxx IS NOT A VALID LOCATION NUMBER

The LOCATION command must be followed by a numeric location number.

11. xxx IS NOT A VALID PORT DESIGNATION FOR INPUT COMPONENT zzz. ERRONEOUS CONNECTIONS MAY OCCUR.

The phrase xxx cannot be located as a valid input port for the component zzz. Connections will be attempted using the upstream output port that was identified.

## 2.5 MODEL GENERATION LIMITATIONS

Certain limitations exist in the Model Generation program due to array dimensions within the program. For most applications these limits should not be encountered. However, if they should be encountered they can usually be extended at the expense of larger core requirements to execute the program. The following table describes these limitations:

<u>Limitation Description</u>	<u>Maximum Value</u>
Standard components in library	150
Components per model	200
Inputs per any standard component	50
Outputs per any standard component	50
Tables per any standard component	15
Tables per model	100
Table dimension (words)	960

### 3.0 SIMULATION PROGRAM

Once a model has been generated as described in Section 2, the user must describe the simulation he wishes to perform. This involves specifying the various parameters detailing the model components and setting the models initial conditions. It involves defining input data tables and the type and quantities of printed output, both tabular and plotted. The user must also specify the number of iterations he wishes to perform at each time step and the maximum number of component diagnostics. This section describes in detail the commands for specifying the simulation and gives some example output.

#### 3.1 MODEL INPUT DATA

A dynamic system model requires that the values of numerous model parameters, tables and initial conditions, be provided to complete the model description. Sections 3.1.1, 3.1.2 and 3.2 describe the methods used to specify parameter values, tables, and initial conditions.

##### 3.1.1 Scalar Data

###### PARAMETER VALUES (Default values = .99999)

This program command allows the numeric values of parameters to be loaded into the system model. The PARAMETER VALUES command is followed by one or more parameter names followed by a numeric value. Each name and its value are separated by one of the standard delimiter symbols. This command is used to specify the values of all system model parameters at the beginning of an analysis. It may also be used at any point between analyses to modify the value of one or more model parameters. A default value of .99999 is provided by the Model Generation program for all parameters not so specified.

### Example 3.1-1

PARAMETER VALUES = CYCLES = 6.01, TO TI = 0, EC WP = .2,  
CR CM = 15, LE CM = 30, MDEHS = 4.E5, .....

#### 3.1.2 Tabular Data

If tabular data is required by the system model, it should be loaded before any of the simulation commands described in Section 3.4 are issued. Tables may be modified between analyses by loading new values. The tables required by a SIMWEST generated model are specified in the Input Requirements List. These tables may have either one or two independent variables. All data items are in a free field format with each item separated by one of the standard delimiters: comma [,], equal sign =[,], left or right parenthesis ( ) , or three or more consecutive blank spaces. The data items required for each table are placed on cards as follows:

Card 1	TABLE	table name	NX	NZ
Card 2*	Z	table values		
Card 3*	X	table values		
Card 4*	Y	table values		

where: Table Name - The six character table name generated by the Model Generation program.

NX - The number of points in the primary independent variable table.

NZ\*\* - The number of points in the secondary independent variable table.

Z table \*\* - Table of NZ secondary independent variable values.

X table - Table of NX independent table values.

Y table - 1 or NZ tables of NX dependent variable values.

\* As many cards as required may be used. Each table must start with a new card and NZ, NX, and NX\*NZ points must be given per table.

\*\* These items are omitted for tables with one independent variable.

A copy of all tabular input data is printed as it is interpreted from data cards. The following example shows the data cards for a one and a two independent variable table.

Example 3.1-2

```

Card 1    TABLE, TABONE,    10
Card 2    1, 2, 3, 4, 5, 6, 7, 8, 9, 10
Card 3    11, 12, 13, 14, 15, 16, 17, 18, 19, 110
Card 4    TABLE, TABTWO, 5, 4
Card 5    10.3, 20.4, 30.5, 40.6
Card 6    1, 2, 3, 4, 5
Card 7    11, 12, 13, 14, 15
Card 8    21, 22, 23, 24, 25
Card 9    31, 32, 33, 34, 35
Card 10   41, 42, 43, 44, 45
  
```

The printout of these tables would be:

```

                TABLE TABONE
    PRIMARY INDEPENDENT VARIABLE TABLE
1.000  2.000  3.000  4.000  5.000  6.000  7.000  8.000  9.000  10.00
    DEPENDENT VARIABLE TABLE
11.00  12.00  13.00  14.00  15.00  16.00  17.00  18.00  19.00  110.00
                TABLE TABTWO
    SECONDARY INDEPENDENT VARIABLE TABLE
10.30      20.40      30.50      40.60
    PRIMARY INDEPENDENT VARIABLE TABLE
1.000      2.000      3.000      4.000      5.000
    DEPENDENT VARIABLE TABLE
11.00      12.00      13.00      14.00      15.00
21.00      22.00      23.00      24.00      25.00
31.00      32.00      33.00      34.00      35.00
41.00      42.00      43.00      44.00      45.00
  
```

### 3.2 INITIAL CONDITION AND INTEGRATION CONTROLS

INITIAL CONDITIONS (Default value = 0)  
INT CONTROLS (Default value = 1.0)

These program commands may be used to specify initial condition values and the integrator status, (either active (=1) or frozen (=0)). Default values of 0. for initial conditions and 1 for integration controls are furnished by the simulation program. However, it is strongly recommended that values appropriate to the particular system model be furnished for the initial conditions.

Each of these commands is followed by phrases of the form of a state name followed by a numeric value.

Example 3.2-1:

INITIAL CONDITIONS = MA HS = 1.6E6, E TS = 600, VDELO = 0, ....  
INT CONTROLS = MA HS = 0, E TS = 1, VDELO = 1, .....

ALL STATES (Default Condition)  
NO STATES

These program commands may be used to activate or freeze all system integrators. These commands are normally used together with the INT CONTROLS command to specify the desired integrator configuration.

### 3.3 INITIAL CONDITION STORAGE COMMANDS

XIC-X  
XIC-XIC1  
XIC-XIC2  
XIC-XIC3  
XIC1-XIC  
XIC2-XIC  
XIC3-XIC

These program commands are used to transfer data from the current state vector, X, to the initial condition vector, XIC, and between the XIC vector and three auxiliary initial condition vectors XIC1, XIC2, XIC3.

Example 3.3-1

XIC1-XIC, XIC-X, XIC2-XIC

The three program commands shown above would take the current operating point (initial condition vector) and store it in vector XIC1; then transfer the current state, X, into XIC; and then store that value of XIC in XIC2.

### 3.4 SIMULATION COMMANDS

SIMULATE

This program command initiates simulation operation. Associated with this command are the program values:

		<u>Default Values:</u>
TINC	= time increment, hours	0.1
TMAX	= duration of the simulation run hours	1.0
OUTRATE	= output rate	1
PRATE	= print rate	1
PRINT CONTROL	= print control variable	0

These program commands specify the integration time increment, duration of simulation run, the simulation output rate, the printing rate, and the quantity of printing, at each point in time. These quantities should be specified before the first issuance of the SIMULATE command.

The Time increment, TINC, provides the integrator time step size, in hours, for the integrator. TINC also provides the report interval for which data will be available for printing or plotting. The default value for TINC is 0.1.

The duration of a simulation calculation in hours, is specified by the TMAX parameter. The default value of TMAX is 1.

The output rate parameter, OUTRATE, determines the sampling rate at which simulation data is added to plots. Thus, if OUTRATE is set equal to 10, data will be plotted every 10th time increment, TINC. The default value of OUTRATE is 1. OUTRATE should only be set to positive integer values.

The number of data samples plotted for a simulation analysis is thus given by:

$$\text{No. of Plotted Samples} = \frac{\text{TMAX}}{\text{TINC} \times \text{OUTRATE}} + 1$$

For most simulation operation, the plotted output specified by the DISPLAY commands is the primary output and no line printer output is used. However, for diagnosing problems in a simulation, the line printer options provided by the PRINT CONTROL parameter allow large amounts of detailed information about the simulated system to be obtained.

The value of the PRINT CONTROL parameter controls the quantity of data printed at each print report interval as shown in Table 3.4-1. Options 1 through 4 give "snap-shots" of all states, rates, variables, and parameters of the system model at a particular point in time. Option 5 provides tabular lists

of up to 10 specified quantities.\* The default value for PRINT CONTROL is 0.

TABLE 3.4-1

PRINT CONTROL	Print Control Values Resultant Lineprinter Output.
0	None (Default Condition)
1	All states, rates, and time
2	All states, rates, variables, and time
3	All states, rates, variables, and parameters at time = 0
4	All states, rates, variables, and parameters
5	Time and the quantities specified via PRINT VARIABLES command.

The PRATE parameter determines the sampling rate at which the simulation data specified by the PRINT CONTROL parameter is presented on the line-printer. Thus, if PRATE is set equal to 5, data will be printed on the line printer every 5th time it is added to the output plots. The rate of output to the lineprinter can never be greater than that to the plots. The default value of PRATE is 1. PRATE should only be set to positive integer values.

The number of data samples printed for a simulation analysis is thus given by:

$$\text{No. of Printed Samples} = \frac{\text{TMAX}}{\text{TINC} * \text{OUTRATE} * \text{PRATE}} + 1$$

\*See the PRINT VARIABLES command description below.

Example 3.4-1:

```
PRINT CONTROL = 2, TINC = .01, TMAX = 10.,  
OUTRATE = 10, PRATE = 10, SIMULATE
```

In the example, the simulation would run for 10 hours. Plotted output would occur every .1 hour, (10\* .01), and printed output would occur every 1. hour (10\* 10\* .01).

#### PRINT VARIABLES

This program command allows up to ten variables to be specified for printing under option 5 of the PRINT CONTROL. This command is followed by from one to ten state, rate, or variable names separated by delimiters. This command wipes out all previously stored PRINT VARIABLES names.

Example 3.4-2:

```
PRINT VARIABLES = MA HS, E TS, VDELO
```

#### 3.5 PLOT DESIGNATION COMMANDS

```
DISPLAY1  
DISPLAY2  
DISPLAY3  
DISPLAY4  
DISPLAY5  
DISPLAY6
```

These program commands may be used to define the quantities to be displayed by lineprinter plots for simulation calculations. These commands must be issued before the simulation analysis is requested. From one to five plots may be specified per display. Each plot is specified by stating the dependent variable and the independent variable separated by the letters VS. If

desired, the independent and dependent axis scale ranges can also be specified. The independent scale range is specified by the word XRANGE followed by the minimum and maximum values for this scale. The dependent scale similarly is specified by the word YRANGE. If scale ranges are not specified, values will be used that span the given data.

### SI MANUAL SCALES

#### SI AUTO SCALES (Default Condition)

The SI MANUAL SCALES command allows the plotted output requested by the DISPLAY commands to be plotted on manual scales specified by the YRANGE and XRANGE commands. The SI AUTO SCALES command can be used to return plotting to the automatic scaling mode. Auto scales are selected so that they span each plotted quantity. The auto scale option is the default used until manual scales are requested. The PRINTER PLOTS command is also required to obtain plots.

Example 3.5-1:

```
SI MANUAL SCALES, PRINTER PLOTS
DISPLAY1
W2WD, VS, TIME, YRANGE = 10,40
P1 PD, VS, TIME, YRANGE = 0,1000
P2 PD, VS, TIME, YRANGE = 0,1000
DISPLAY2
P2 IV, VS, TIME
RE2BA, VS, TIME
RE1LO, VS, TIME
DISPLAY3
P1 PD, VS, P2 PD, YRANGE = 0,1000, XRANGE = 0,1000
```

## TITLE

The TITLE command allows a title to be placed on all plotted output. Up to 74 characters may follow the delimiter that follows the TITLE command. The TITLE command may be changed before each analysis. Once defined, the title remains in effect until a new title is entered.

Example 3.5-2:

```
TITLE = BATTERY TEST MODEL
```

### 3.6 ITERATION AND DIAGNOSTIC CONTROL

There are three built-in parameters in any SIMWEST model : CYCLES, DLINES and RESET. These parameters are specified similar to component parameters using the PARAMETER VALUES command.

CYCLES controls the number of iterations through the model to obtain steady state. If  $CYCLES \leq 0$ , then only one pass is made through the model. If CYCLES is a positive integer then the number of iterations through the model is equal to  $CYCLES + 1$ . If cycles is positive, but not an integer, then the number of iterations is equal to the smallest integer value exceeding cycles. A maximum of 20 iterations are permitted per time step. Most of the simple models of Section 8 require between four and six iterations per time step to attain steady state. A complex model with cascaded logic components may require more.

The task of finding the correct value for CYCLES is facilitated by the program printing at each time step all variables which have a greater than 5% change in value in the last iteration.

Since output statistics are only updated the last iteration, many of the variables printed indicating nonconvergence are just statistics, and as such should be ignored.

DLINES controls the amount of convergence related printout to be controlled as well as the amount of diagnostic printout put out by the library components. If DLINES >0 then the total number of diagnostic printouts is no greater than DLINES. Figure 3.6 shows a typical section of diagnostic printout using DLINES >0. If DLINES <0 then only library component diagnostics are printed with no greater than - DLINES of output. Typically, DLINES = 100 is sufficient to catch most simulation errors per run.

PC3PA	NONCONVERGENCE.	OLD VALUE=	4.209	NEW VALUE=	6.109
SR UT	NONCONVERGENCE.	OLD VALUE=	177.720	NEW VALUE=	264.359
PC3PA	NONCONVERGENCE.	OLD VALUE=	6.109	NEW VALUE=	7.054
SR UT	NONCONVERGENCE.	OLD VALUE=	264.359	NEW VALUE=	312.718
FLYWHEEL KINETIC ENERGY		39.875 FALLS BELOW MINIMUM REQUIREMENT			40.000
FLYWHEEL CLUTCH LOSS		1.217 EXCEEDS DELIVERABLE POWER			.400
SP MO	NONCONVERGENCE.	OLD VALUE=	553.569	NEW VALUE=	601.994
SPCFL	NONCONVERGENCE.	OLD VALUE=	543.583	NEW VALUE=	590.798
PC3PA	NONCONVERGENCE.	OLD VALUE=	7.054	NEW VALUE=	8.152
SR UT	NONCONVERGENCE.	OLD VALUE=	312.718	NEW VALUE=	370.217

FIGURE 3.6 TYPICAL DIAGNOSTIC OUTPUT

RESET controls the initialization value for the random number generators if several simulations are run back to back. If RESET >0 (Default) then the same random numbers are used for each simulation. If RESET ≤ 0 then the random numbers at the start of each simulation are obtained from the last value at the end of the previous simulation.

### 3.7 DEFINE COMMANDS

- DEFINE STATES
- DEFINE RATES
- DEFINE PARAMETERS
- DEFINE VARIABLES

These program commands may be used to define the alphanumeric names that will be used to refer to states, rates, parameters, and variables. All system models formed by the Model Generation program have model related names generated for all states, variables, and parameters in the model. State variable derivatives, (Rates), are generated as R1, R2,... for all models. R1, R2, ... refer to the rates of the first, second,... states respectively. If it is desired to replace these machine generated names with other names, the DEFINE command may be used to substitute any eight character name of the analyst's choosing. These names are associated with the corresponding numeric quantities located in the labeled commons /CX/, /CXDOT/, /CP/, and /CV/. The appropriate location for each quantity is printed out along with the quantity name prior to each simulation. Each of these commands is followed by phrases containing the location numeric followed by an alphanumeric name with one to eight characters the first of which must be alphabetic.

Example 3.7:

```
DEFINE STATES
1 = PRESSURE, 2 = STROKE, 5 = VELOCITY, 7 = ANGLE

DEFINE PARAMETERS
5 = MASS, 35 = DCT AREA

DEFINE VARIABLES, 1 = T OUTLET, 2 = LIQ H2O
```

Note that the program commands, numeric values and alphanumeric names must be separated by delimiters which are: comma [, ], equals [=], left parentheses [(], right parenthesis [)], or three or more consecutive spaces.

### 3.8 EXAMPLE OUTPUT

Figure 3.8 shows a sample of the output print format generated using PRINT CONTROL = 3. This sample is taken from the Wind Turbine and File Read run

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DATE 072677

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TIME # .0000		STATES	
1 VDELU # .00000			
RATES			
1 MI # 5.0009			

VARIABLES																																																			
1 TI # .00000	2 TO TI # .00000	3 TH TI # .00000	4 DW TI # 1.0000	5 OY TI # 1.0000	6 NY TI # 1.0000	7 MY TI # 1.0000	8 VANTAW # 18.477	9 N TAW # 446.00	10 TO TAW # .00000	11 M TAW # .25000	12 MVZWD # 18.477	13 MV WD # 18.477	14 AV WD # 20.354	15 M WD # 58.846	16 IIMWD # -1.0000	17 P2 WT # 241.84	18 TO WT # 72080.	19 CO WT # .12500	20 GR WT # 76.391	21 MAPWT # 795.36	22 MT WT # 72080.	23 MPUWT # 241.84	24 SP WT # 30.230	25 P2 GR # 229.65	26 IO GR # 895.98	27 PL GH # 12.184	28 EF2GR # .94961	29 MP2GR # .10000*11	30 HS1GR # 23.651	31 SAMHG # 1.0000	32 AV HG # 241.84	33 SD HG # 58485.	34 P2 GE # 217.43	35 EE GE # .97710	36 KS GE # 1805.2	37 PL GE # 12.224	38 EF2GE # .89906	39 MP2GE # 750.00	40 MPNGE # .28991	41 SP GE # 27.179	42 VANTAL # 572.02	43 N TAL # 446.00	44 TO TAL # .00000	45 H TAL # .25000	46 KE1LU # 636.24	47 LOZLU # 572.02	48 SRELU # 71.502	49 SDELU # 27.179	50 PC LO # 38.011	51 TIMLU # 1.0000	52 CN LU # -1.9575

PARAMETERS																																																						
1 TO TI # .00000	2 NSTTAW # .00000	3 ITFTAW # 1.0000	4 VO WT # 21.000	5 VR WT # 28.350	6 RSGWT # 1800.0	7 BR WT # 80.000	8 EC WT # 1.5000	9 AD WT # .23000-02	10 LAMWT # 9.4000	11 CPWT # .41000	12 CP WT # .99999	13 CC WT # 16000.	14 CH WT # 2000.0	15 EF1GR # .99999	16 MP1GR # .10000*11	17 CC GH # 1000.0	18 CM GH # 200.00	19 F1 HG # .00000	20 F2 HG # .00000	21 F3 HG # .00000	22 F4 HG # 1.0000	23 F5 HG # .00000	24 F6 HG # .00000	25 F7 HG # .00000	26 F8 HG # .00000	27 F9 HG # .00000	28 F10HG # .00000	29 F11HG # .00000	30 F12HG # .00000	31 F13HG # .00000	32 F14HG # .00000	33 F15HG # .00000	34 F16HG # .00000	35 PA HG # 57.857	36 FUPHG # 1000.0	37 FLHG # 50.000	38 KAPGE # 750.00	39 KSYGE # 1800.0	40 RASGE # .10000-01	41 UA GE # .20000	42 SR GE # .50000-02	43 VU GE # 400.00	44 CC GE # 1000.0	45 CM GE # 200.00	46 NSTTAL # .00000	47 ITFTAL # 2.0000	48 NC LO # .57400-02	49 CT LO # 4.0000	50 MN LO # .00000	51 STDLU # 8.0000	52 VE LU # .25000-01	53 CYCLES # 2.0100	54 DLINES # .99999	55 RESET # .99999

TIME # 12.00		STATES	
1 VDELU # 97.264			
RATES			
1 MI # .63123			

VARIABLES																																																			
1 TI # 12.000	2 TO TI # 12.000	3 TH TI # 12.000	4 DW TI # 1.0000	5 DY TI # 1.0000	6 NY TI # 1.0000	7 MY TI # 1.0000	8 VANTAW # 13.444	9 N TAW # 446.00	10 TO TAW # .00000	11 M TAW # .25000	12 MVZWD # 13.444	13 MV WD # 39.006	14 AV WD # 20.354	15 M WD # 58.846	16 IIMWD # -1.0000	17 P2 WT # 36.664	18 TO WT # 10956.	19 CO WT # 12.125	20 GR WT # 76.391	21 MAPWT # 795.36	22 MT WT # .23555*06	23 MPUWT # 795.36	24 SP WT # 4861.1	25 P2 GR # 35.198	26 IO GR # 157.67	27 PL GH # 1.4660	28 EF2GR # .95999	29 MP2GR # .10000*11	30 HS1GR # 23.572	31 SAMHG # 17.000	32 AV HG # 38889.	33 SD HG # .24279*08	34 P2 GE # 27.445	35 EE GE # .97710	36 KS GE # 4800.7	37 PL GE # 7.7533	38 EF2GE # .74853	39 MP2GE # 750.00	40 MPNGE # .43304	41 SP GE # 4256.0	42 VANTAL # 1024.2	43 N TAL # 446.00	44 TO TAL # .00000	45 H TAL # .25000	46 KE1LU # 1002.0	47 LOZLU # 1024.2	48 SRELU # 8481.5	49 SDELU # 4256.0	50 PC LO # 50.180	51 TIMLU # 1.0000	52 CN LU # -1.9575

TIME # 24.00		STATES	
1 VDELU # 239.65			

FIGURE 3.8 SAMPLE PRINTER OUTPUT

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described in Section 8.1, which is a very simple model. At each print time the output quantities are indexed by number and component name as they occur in the model. For example, first all the variables for component TI are printed, then all variables for component TAW, etc. The parameter values at time = 0 show both the input values and the default parameters. After T = 0 only the states, rates, and output variables are printed. Since all the model connection variables and output variables are printed, this mode is especially valuable for program debugging and analysis at a fixed time. The printer plots, samples of which are shown in Section 8, are useful for monitoring the time behavior of critical parameters such as energy in storage and percent of load delivered by storage.

## 4.0 JOB CONTROL PROCEDURES

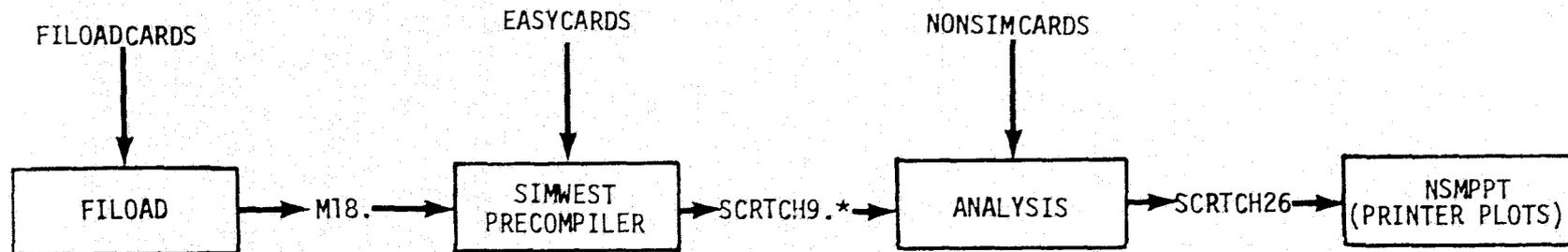
In this section, we describe job control procedures for running and maintaining the SIMWEST programs. For the convenience of the user, a number of procedure files have been set up which simplify the user control cards required. In Section 4.1, we describe the control cards for executing the model generation and analysis programs. Section 4.2 describes the procedures to maintain the programs and update the component library.

### 4.1 MODEL GENERATION AND ANALYSIS EXECUTION

Figure 4.1-1 shows an overview of the program structure to execute a simulation run. The program FILOAD is only executed when the component library is updated, and is thus described in the next section. The user input data for the model generation program is put on a file called EASYCARDS. A procedure file called XQTEASY is then used to generate the model Fortran and compile this model. Similarly, the user input data for the analysis program is put on a file called NONSIMCARDS, and a file called XQTANALYSIS maps the relocatable elements into absolute file elements, and executes both the simulation and printer plot programs.

A job control stream to execute these programs in a batch environment is given by:

```
@RUN ...
@DELETE,C EASYCARDS.
@ASG,UP EASYCARDS.
@DATA,IL EASYCARDS.
.
.
.
INPUT DATA DECK
FOR MODEL
.
.
.
@END
@ASG,A XQTEASY.
```



\*SCRTCH9 IS FORTRAN SOURCE CODE OUTPUT

FIGURE 4.1-1 SIMWEST PROGRAM EXECUTION STRUCTURE

```

@ADD,PL XQTEASY.
@DELETE,C NONSIMCARDS.
@ASG,UP NONSIMCARDS.
@DATA,IL NONSIMCARDS.
.
.
.
INPUT DATA DECK
FOR ANALYSIS
.
.
.
@END
@ASG,A XQTANALYSIS.
@ADD,PL XQTANALYSIS.
@FIN

```

The job control procedures XQTEASY and XQTANALYSIS are shown in Figures 4.1-2 and 4.1-3. If a user is creating data inputs from a terminal, then it may be somewhat simpler to create new job control procedures similar to XQTEASY and XQTANALYSIS, but substituting his data input file names for EASYCARDS and NONSIMCARDS, respectively. If the same model is used for a series of runs, then only the analysis program is required for execution. However, it is safer and also relatively inexpensive to execute both programs when using the above job stream. Whenever the file read component is desired, the user must either substitute his file for F1 or F2, or add the following job cards to XQTANALYSIS:

```

@ASG,A MYFILE.
@USE M, MYFILE.

```

where MYFILE is the user time history file and M is a unit number between 13 and 18. (See 7.38 for a discussion of the tape/file read component.)

#### 4.2 PROGRAM MAINTENANCE AND LIBRARY UPDATES

Whenever the component library is updated, the user must compile the Fortran code and run the FILOAD program to furnish the model generation program com-

```

@HDG SIMWEST MODEL GENERATION
@ASG,AX MGABS.
@ASG,A M18.
@USE 18,M18.
@ASG,T M7.
@USE 7,M7.
@ASG,T SCRTCH8.
@USE 8,SCRTCH8.
@DELETE,C SCRTCH9.
@ASG,UP SCRTCH9.
@USE 9,SCRTCH9.
@ASG,T SCRTCH10.
@USE 10,SCRTCH10.
@ASG,T SCRTCH11.
@USE 11,SCRTCH11.
@ASG,T SCRTCH12.
@USE 12,SCRTCH12.
@ASG,A EASYCARDS.
@USE 5,EASYCARDS.
@XQT MGABS.EASY
@ASG,AX ASRO.
@ASG,AX ASSI.
@ADD,PL 9.
@FREE 18.,7.,8.,9.,10.,11.,12.

```

FIGURE 4.1-2 XQTEASY JOB CONTROL FILE

```

@HDG SIMWEST ANALYSIS
@ASG,AX MAPANALYSIS.
@ADD,PL MAPANALYSIS.
@ASG,AX ASABS.
@ASG,AX F1.
@USE 11,F1.
@ASG,AX F2.
@USE 12,F2.
@ASG,T SCRTCH25.
@USE 25,SCRTCH25.
@DELETE,C SCRTCH26.
@ASG,UP SCRTCH26.
@USE 26,SCRTCH26.
@ASG,AX NONSIMCARDS.
@USE 5,NONSIMCARDS.
@XQT ASABS.NONSIM
@XQT ASABS.NSMPPT
@FREE 11.,12.,25.,26.

```

FIGURE 4.1-3 XQTANALYSIS JOB CONTROL FILE

ponent input and output name lists. A job control stream to compile a new component denoted DC and add it to the component library is given by:

```
@ASG,T SOURCE.  
@DATA,IL SOURCE.  
@FOR,IS COSI.DC,CORO.DC  
.  
.  
.  
USER FORTRAN SUBROUTINE DC  
.  
.  
.  
@END  
@ASG,A COSI.  
@ASG,A CORO.  
@ADD,PL SOURCE.  
@ASG,A CMPLCO.  
@ED,U CMPLCO.  
ADD SOURCE.  
EXIT
```

If an old component is to be updated, then one can edit the source code on CMPLCO and recompile entirely, or copy the edited subroutine including the @FOR,IS control card onto a new file and recompile. A job stream to execute the FILOAD program is given by:

```
@DELETE,C FILOADCARDS.  
@ASG,UP FILOADCARDS.  
@DATA,IL FILOADCARDS.  
.  
.  
.  
USER INPUT DATA  
FOR FILOAD  
.  
.  
.  
@END  
@ASG,A XQTFILOAD.  
@ADD,PL XQTFILOAD.
```

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```
@ASG,AX FSRO.  
@PREP FSRO.  
@ASG,AX MAPFSSI.  
@ASG,AX FILOAD4.  
@MAP,I MAPFSSI.FILOAD,FILOAD4.  
  IN FSRO.FILOAD  
  LIB FSRO.  
END
```

FIGURE 4.2-2 MAPFILOAD PROCEDURE FILE

```
@ASG,AX MGRO.  
@PREP MGRO.  
@ASG,AX MAPMGSI.  
@ASG,AX MGABS.  
@ASG,AX FSRO.  
@PREP FSRO.  
@MAP,I MAPMGSI.EASY,MGABS.EASY  
  IN MGRO.EASY  
  LIB FSRO.,MGRO.,FSRO.  
END
```

FIGURE 4.2-3 MAPEASY PROCEDURE FILE

```
@ASG,AX FSRO.  
@ASG,AX ASRO.  
@ASG,AX CORO.  
@PREP CORO.  
@PREP FSRO.  
@PREP ASRO.  
@ASG,AX MAPASSI.  
@ASG,AX ASABS.  
@MAP,I MAPASSI.NONSIM,ASABS.NONSIM  
  IN ASRO.NONSIM  
  IN ASRO.BLOCKDA  
  IN ASRO.MODEL  
  LIB FSRO.,ASRO.,FSRO.,CORO.  
END
```

FIGURE 4.2-4 MAPANALYSIS PROCEDURE FILE

```
@ASG,AX FSRO.  
@ASG,AX ASRO.  
@PREP FSRO.  
@PREP ASRO.  
@ASG,AX MAPASSI.  
@ASG,AX ASABS.  
@MAP,I MAPASSI.NSMPPT,ASABS.NSMPPT  
  IN ASRO.NSMPPT  
  LIB FSRO.,ASRO.,FSRO.  
END
```

FIGURE 4.2-5 MAPNSMPPT PROCEDURE FILE

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4. CAN'T IDENTIFY xxx VALUE WILL BE IGNORED.

This will result in not setting the quantity intended by xxx to its new value. Check for spelling of xxx or for missing delimiters.

5. CAN'T INTERPRET xxx

The phrase xxx cannot be recognized as a valid program command, program name, or program value. Check spelling of xxx or for missing delimiters.

6. nnn EXCEEDS THE ALLOWABLE INDEX RANGE FOR xxx THIS QUANTITY WILL NOT BE DEFINED

The number nnn was outside the allowable range of states, rates, variables, or parameters. Therefore, the name xxx cannot be assigned as a name for the nnnth state, rate, variable or parameter.

7. NON-ALPHA NAME ON THIS CARD --- xxx. WILL IGNORE THIS CARD.

The table inputs routine expected an alphanumeric table name but encountered a numeric value on the data card printed. Check the sequence and number of tabular data cards to assure that they match those required by the model's tables and table input formats. See Section 3.1.2 for correct formats.

8. NON-NUMERIC DATA ON THIS CARD --- xxx. WILL READ NEXT TABLE

The table input routine expected a numeric value but encountered an alphanumeric name on the data card printed. Check that the sequence and number of tabular data cards matches the model's tables and table input formats. See Section 3.1.2 for correct formats.

9. nnn PRIMARY and xxx SECONDARY INDEPENDENT VARIABLE POINTS EXCEEDS THE zzz WORD STORAGE LIMIT FOR THE FOLLOWING TABLE. SOME DATA WILL BE LOST.

The maximum amount of data allowed for each table is given in the Input Requirements List produced by the Model Generation program. Check that given data falls within this limit or for data card errors.

## 5.2 DIAGNOSTIC MESSAGES FOR LIBRARY COMPONENTS

A diagnostic message associated to a component is printed when a variable gets out of bounds during analysis. Adjustment of component parameters may be necessary.

In component alphabetical order, these diagnostic messages are:

AD: INPUT POWER xxxx TOO HIGH RELATIVE TO ADMITTANCE xxxx AND RATED VOLTAGE  
xxx  
ADMITTANCE POWER LOSS xxxx EXCEEDS INPUT POWER xxxx

BA: POWER REQUEST xxxx EXCEEDS BATTERY CAPABILITY. CHECK VC, VO, AND RT.

BN: BN INLET AIR MASS FLOW RATE xxxx GREATER THAN MAXIMUM ALLOWABLE xxxx

CO: MAX ITERATIONS FOR COMPRESSOR EFFICIENCY. NP, XNP, RS = xxxx, xxxx,  
xxxx

CS: CS STORAGE TEMPERATURE xxxx GREATER THAN ALLOWABLE xxxx  
CS MASS OF AIR IN STORAGE xxxx BELOW MINIMUM ALLOWABLE xxxx  
CS MASS OF AIR IN STORAGE xxxx EXCEEDS MAXIMUM ALLOWABLE xxxx

FL: FLYWHEEL POWER LOSS xxxx EXCEEDS CHARGING POWER xxxx  
FLYWHEEL LOSS xxxx EXCEEDS DISCHARGING POWER xxxx  
FLYWHEEL CLUTCH LOSS xxxx EXCEEDS MAXIMUM INPUT POWER xxxx  
FLYWHEEL CLUTCH LOSS xxxx EXCEEDS DELIVERABLE POWER xxxx

FLYWHEEL KINETIC ENERGY xxxx EXCEEDS CAPACITY xxxx  
FLYWHEEL KINETIC ENERGY xxxx FALLS BELOW MINIMUM REQUIREMENT xxxx

GE: GENERATOR OUTPUT EXCEEDS RATED POWER

HS: HS INLET MASS FLOW RATE xxxx OR OUTLET MASS FLOW RATE xxxx IS GREATER  
THAN MAXIMUM xxxx

HS RESERVOIR VOLUME xxxx EXCEEDED MAXIMUM ALLOWABLE xxxx

HS RESERVOIR VOLUME xxxx DROPPED BELOW MINIMUM xxxx

HT: HT TURBINE CHARACTERISTIC PARAMETER OUT OF RANGE

HT INLET MASS FLOW RATE xxxx GREATER THAN MAXIMUM DESIGN VALUE

HX: HX EXIT TEMPERATURE xxxx GREATER THAN MAXIMUM ALLOWABLE xxxx

IV: IV POWER LOSS xxxx EXCEEDS INPUT POWER xxxx CHECK RATED DC VOLTAGE VDC

MB: WARNING-DIVISOR IN MB EQUALS 0., HAS BEEN SET = 1.

MO: MOTOR INPUT POWER xxxx .GT. RATED INPUT POWER xxxx

MOTOR SLIP xxxx EXCEEDS RATED POWER SLIP xxxx

STATOR RESISTANCE xxxx OR DAMPING xxxx TOO HIGH FOR MOTOR

RE: RE POWER LOSS xxxx EXCEEDS INPUT POWER xxxx

RE, AC INPUT POWER xxxx TOO LARGE IN RELATION TO TRANSFORMER REACTANCE  
xxxx AND RATED AC VOLTAGE xxxx

TA: FILE DATA OUT OF RANGE. INITIAL VALUE = xxxx ON UNIT xx

TIME POINT PAST TABLE RANGE. LAST VALUE = xxxx ON UNIT xx

READ ERROR OR END OF FILE ON UNIT xx

TR: TRANSMISSION POWER LOSS xxxx EXCEEDS INPUT xxxx

TRANSMISSION POWER LOSS xxxx EXCEEDS MAXIMUM INPUT POWER

TS: TS WORKING FLUID FLOW RATE xxxx GREATER THAN MAXIMUM ALLOWED xxxx

TS INPUT POWER xxxx GREATER THAN MAXIMUM ALLOWED CHARGE RATE xxxx

TS STORAGE TEMPERATURE xxxx OUTSIDE MINIMUM xxxx OR MAXIMUM xxxx

TU: TURBINE BACK PRESSURE xxxx GREATER THAN STORAGE VESSEL PRESSURE xxxx

## 6.0 CREATION OF NEW LIBRARY COMPONENTS

The addition of new standard components to the SIMWEST library involves two steps. The first is the design of the component. This design must conform to certain design conventions if the new component is to be compatible with existing components. Section 6.1 discusses these design conventions and the addition of the component subroutine to the SIMWEST library. The second step involves the addition of the new component's input and output description to the SIMWEST file M18. File M18 is used by the precompiler to generate subroutine calling sequences for the library components. Section 6.2 discusses the use of the FILOAD program to accomplish this task.

### 6.1 LIBRARY COMPONENT CODING

#### 6.1.1 Component Call Sequence

The items in the component subroutine call sequence must be arranged in the following order:

1. Tables
2. Output Quantities
3. Input Quantities

Tables or inputs may not be present in the subroutine call sequence. However those items that are present must follow the sequence given above.

Dummy argument names for the call sequence quantities that are used within each subroutine should be chosen to match the physical quantity names placed in the input, output, and table name lists. Exceptions to this policy may be made when integer names (names starting with I through N) must be avoided or when additional letters will clarify the name.

The subroutine name must contain only two characters and must not duplicate the name of an existing standard component.

## Tables

The table arrays must be dimensioned within the component subroutine. They must be dimensioned with only one subscript; e.g. DIMENSION TABLE (1). When table data is passed to the component subroutine, the first word in the array contains the name of the table. The second word contains the number of values given for the primary independent variable. The third word contains the number of values given for the secondary independent variable. Both of these numbers are stored as REAL quantities and must be converted to INTEGER before they can be used as a subscript. This can be done by a statement such as:

```
NX = TABLE (2) - number of primary independent variables
NZ = TABLE (3) - number of secondary independent variables
```

If there is a secondary independent variable, the secondary independent variable array will begin with the fourth word in the array. Thus if this array is designated as  $z(1), z(2), \dots$ , then:

```
z(1) = TABLE (4)
z(2) = TABLE (5)
z(3) = TABLE (6)
.      .
.      .
.      .
```

The primary independent variable array begins with word  $NZ + 4$ . Thus if this array is designated as  $X(1), X(2), \dots$ , then:

```
X(1) = TABLE (NZ + 4)
X(2) = TABLE (NZ + 5)
.      .
.      .
.      .
```

The dependent variable array begins with word  $NX + 4$  if there is no secondary independent variable. Thus if this array is designated as  $Y(1), Y(2), \dots$ , then:

$$Y(1) = \text{TABLE } (NX + 4)$$

$$Y(2) = \text{TABLE } (NX + 5)$$

•       •  
•       •  
•       •

If there is a secondary independent variable array and this array was designated  $Y(I, J)$ , with  $1 \leq I \leq NX$  and  $1 \leq J \leq NZ$ , then  $Y(I, J)$  would be related to the table array as:

$$Y(I, J) = \text{TABLE}(NX + NZ + 3 + I + (J - 1) * NX)$$

Normally the individual elements in the table are not used directly but are passed to a table look-up routine. In this case the starting address of the X, Y, and Z tables would be referred to as:

$$Z(1) = \text{TABLE } (4) \quad \text{secondary independent variable table}$$

$$X(1) = \text{TABLE } (NZ + 4) \quad \text{primary independent variable table}$$

$$Y(1, 1) = \text{TABLE } (NX + NZ + 4) \quad \text{dependent variable table}$$

If more than one table is used by a component subroutine, the table names must appear in the same sequence in the table name list stored in M18 file as in the subroutine call sequence.

Example 6.1: Given a component, HA, that requires the tables TPH and TPC as an inputs. The call sequence of this subroutine would appear as:

SUBROUTINE HA(TPH, TPC, ...)

### Output Quantities

The term "output quantity" refers to information that is calculated and then "output" by a particular component subroutine. This is not to be confused with the "outlet quantities" of the component. The outlet quantities are associated with a particular component port as a result of assigning a positive direction of power or information flow through the component. Some outlet quantities may be calculated by the component subroutine and thus become output quantities of that component. While other outlet quantities may be furnished to the component subroutine and thus become input quantities to that subroutine.

The output quantities should be grouped together by port. That is, all outlet, (port two quantities), then all inlet, (port one quantities), etc. If a component has multiple outlet ports, the output quantities associated with each outlet port should be grouped together and listed before any inlet port output quantities.

Certain output quantities may be internal to the component and not associated with any port. In other cases the same output quantity may be associated with several ports. In such cases, no port designation is assigned to the output quantity. Such quantities are referred to as "universal port" quantities. As such, they are allowed to connect to any other similar physical quantity regardless of the input quantities port number. This is not the case for quantities with specified port numbers. Once a connection has been made between an input and output quantity with given port numbers, only connections of matching physical quantities with those port numbers occur. Manual override of this provision can be made by specifying particular physical quantity connections.

Three quantities are required for each state variable output. The first is the state variable, the second is the state variable derivative, (rate),

and the third is an integer quantity, the integrator control variable.

Example: Given a component, HA, with the following outputs:

Physical Quantity	Port No.	
T	3	} Outlet Ports
T	4	
P	1 (State Variable)	} Inlet Ports
P	2 (State Variable)	

The call sequence arguments for these outputs would be:

```
SUBROUTINE HA(TPH,TPC,T3,T4,P1,P1DOT,IP1,P2,P2DOT,IP2,...
```

### Input Quantities

The term "input quantity" refers to information that is provided to a particular component subroutine. This is not to be confused with the "inlet quantities" of the component. The inlet quantities are associated with a particular component port as a result of assigning a positive direction of power or information, through the component. Some inlet quantities may be calculated by the component subroutine and thus become output quantities of that component, while other inlet quantities may be furnished to the component subroutine and thus become input quantities to that subroutine.

The input quantities should be grouped together by port. That is, all inlet, (port one quantities), then all outlet, (port two quantities), etc. Port designations for two port components which have the same physical quantity on both inlet and outlet will be: port 1 for upstream or inlet port and port 2 for downstream or outlet port. It is important that the inlet port quantities be listed before any outlet port quantities. If a component has multiple inlet ports, the input quantities associated with each inlet port should be grouped together and listed before any outlet port quantities.

Certain input quantities may be internal to the component and not associated with any port. In other cases the same input quantity may be associated with several ports. In such cases, no port designation is assigned to the input quantity. Such quantities are referred to as "universal port" quantities. As such, they are allowed to connect to any other similar physical quantity regardless of the output quantities port number. This is not the case for quantities with specified port numbers. Once a connection has been made between an input and output quantity with given port numbers, only connections of matching physical quantities with those port numbers occur. Manual override of this provision can be made by specifying particular physical quantity connections.

Example: Given the component HA described in the above example, with the following inputs:

Physical Quantity	Port No.	
T	1	} Inlet Ports
T	2	
P	3	} Outlet Ports
P	4	
AKH		(universal port quantity)

The call sequence for these inputs would follow the output arguments, giving the complete call sequence:

```
SUBROUTINE HA(TPH,TPC,T3,T4,P1,P1DOT,IP1,P2,P2DOT,IP2,T1,T2,P3,P4,AKH)
```

The call sequence for standard component subroutines should follow the order shown in Table 6.1-1.

### 6.1.2 Additions and Modifications to Component Library

Section 4.2 describes the job control procedures to add a new component to the component library, compile the source code that describes the new component and add the relocatable binaries to the component library CORO.

TABLE 6.1-1

COMPONENT SUBROUTINE  
CALL SEQUENCE ORDER

1. Tables
2. Output Quantities
  - 2.1 All Outlet Port Quantities\*
  - 2.2 All Inlet Port Quantities\* (feedback variables)
  - 2.3 All Other Output Quantities
3. Input Quantities
  - 3.1 All Inlet Port Quantities\*
  - 3.2 All Outlet Port Quantities\* (feedback variables)
  - 3.3 All Other Input Quantities

\* Group quantities with the same port number together. If multiple inlet or outlet ports exist, arrange port quantities in order of increasing port numbers.

### 5.1.3 Coding Conventions

There are several coding rules which apply to any component coded. First of all, the calling sequence must be ordered so that it agrees with that constructed from the Fiload program. Hence the calling sequence begins with table arrays, is followed by output variables, and then by input parameters. State variables require three sequential parameters in the calling sequence: the state variable, the state derivative, and an integer valued integration control. With the exception of the latter, all parameters in the calling sequence are real valued. In general one cannot use any local variables or arrays to store information from call to call since there may be several components in the model which call a given subroutine. In other words, local variables can only be used for scratch calculations, unless the computed information is based on COMMON block inputs.

Most of the coding conventions and techniques used are illustrated in Figures 6.1-1 and 6.1-2. Figure 6.1-1 shows the code for the simple power curve component WP. Following the call sequence are a number of comment cards including the component purpose and calling sequence. The table PW is treated as a single dimension Fortran array. Power output is obtained from the table interpolation subroutine TBLU1. (Use of the table interpolation routines TBLU1 and TBLU2 is explained in Section 2.1). The rest of the code shows the conventions used to compute output statistics and add costs for the cost summary. IMPL is an integer variable which indicates the iteration control status:

IMPL = 0 the first time in a simulation that the model (EQMO) is called  
= 1 if more iterations and hence subroutine calls are expected at a given time step  
>1 the final iteration through the model.

Hence when IMPL = 0, subroutine variables are initialized, default values are assigned, etc. The statistics are only updated at the final iteration

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```

00100 1* CWP
00101 2* SUBROUTINE WP ( PW,BI,PO,AMI,AMP,SP,CO,VO,WV0,WV1,WV,CCI,CMI,EC)
00101 3* C
00101 4* C PURPOSE MODEL THE WIND TURBINE AND GENERATOR USING A POWER CURVE
00101 5* C
00101 6* C WRITTEN BY A.W. WARREN VERSION 1, MARCH 3 1977
00101 7* C
00101 8* C CALL SEQUENCE
00101 9* C TABLES
00101 10* C PW = WIND GENERATION POWER IN KW VERSUS WIND VELOCITY IN MPH
00101 11* C
00101 12* C OUTPUTS
00101 13* C BI = OUTPUT BUS CURRENT, AMPS
00101 14* C PO = POWER OUTPUT, KW
00101 15* C AMI = MAX. OBSERVED CURRENT, AMPS
00101 16* C AMP = MAX. OBSERVED POWER, KW
00101 17* C SP = TOTAL OUTPUT ENERGY, KWH
00101 18* C CO = OPERATING COST, $
00101 19* C
00101 20* C INPUTS
00101 21* C VO = RATED BUS VOLTAGE, VOLTS
00101 22* C WV0 = POWER CUTIN VELOCITY, MPH
00101 23* C WV1 = POWER CUTOOUT VELOCITY, MPH
00101 24* C WV = WIND VELOCITY, MPH
00101 25* C CCI = CAPITOL COST / YEAR, $
00101 26* C CMI = MAINTENANCE COST / YEAR, $
00101 27* C EC = CONTROL ENERGY RATE, $/HR
00101 28* C
00103 29* DIMENSION PW(1)
00104 30* COMMON / CIMPL / IMPL
00105 31* COMMON/COST/ CC,CM,COP /CTIME/ TIME /CSIMUL/ DUM(6),TINC,TMAX
00105 32* C
00105 33* C POWER OUTPUT CALCULATIONS
00105 34* C
00106 35* PO = 0.
00107 36* IF(WV.LT.WV0 .OR. WV.GT.WV1) GO TO 10
00111 37* N = PW(2)
00112 38* PO = TBLU1(WV,PW(4),PW(4+N),1,-N)
00113 39* 10 BI = PO*1000/VO
00113 40* C STATISTICS
00113 41* C
00114 42* IF(IMPL.GT.0) GO TO 20
00116 43* CO = 0.
00117 44* AMI = 0.
00120 45* AMP = 0.
00121 46* SP = 0.
00122 47* TMAX1=TMAX*.99999
00123 48* 20 IF(IMPL.LE.1) RETURN
00125 49* AMI = AMAX1(AMI,BI)
00126 50* AMP = AMAX1(AMP,PO)
00127 51* SP = SP + PO*.5*TINC
00130 52* CO = CO + EC*.5*TINC
00130 53* C COST SUMMATION
00131 54* IF( TIME.LT.TMAX1) RETURN
00133 55* CC = CC + CCI
00134 56* CM = CM + CMI
00135 57* COP = COP + .CO
00136 58* RETURN
00137 59* END
END FOR

```

FIGURE 6.1-1 SAMPLE COMPONENT CODE

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```

00100 10 CGE
00101 20 SUBROUTINE GE(P2,EE,RS,PL,EF2,PM2,PMN,SP,P1,RAP,RSY,RAS,DA,SR,VO,
00101 30 1,EF1,PM1,CCI,CMI)
00101 40 C
00101 50 PURPOSE MODLL AC INDUCTION GENERATOR
00101 60 C
00101 70 METHOD MECHANICAL AND ELECTRICAL EFFICIENCIES ARE USED TO COMPUTE
00101 80 OUTPUT POWER. ROTOR SPEED IS COMPUTED ASSUMING POWER IS
00101 90 PROPORTIONAL TO SLIP.
00101 100 C
00101 110 WRITTEN BY A.M. HARNEN
00101 120 C
00101 130 VERSION 1, MARCH 16 1977
00101 140 C
00101 150 CALL SEQUENCE
00101 160 C
00101 170 OUTPUTS
00101 180 P2 = OUTPUT POWER, KW
00101 190 EE = ELECTRICAL EFFICIENCY
00101 200 RS = ROTOR SPEED, RPM
00101 210 PL = POWER LOSS, KW
00101 220 EF2 = OUTPUT PRODUCT EFFICIENCY
00101 230 PM2 = MAXIMUM OUTPUT POWER, KW
00101 240 PMN = MAX. (OBSERVED) OUTPUT POWER / RATED POWER
00101 250 SP = TOTAL OUTPUT ENERGY, KWH
00101 260 C
00101 270 INPUTS
00101 280 P1 = INPUT POWER, KW
00101 290 RAP = RATED OUTPUT POWER, KW
00101 300 RSY = SYNCHRONOUS ROTOR SPEED, RPMN
00101 310 RAS = RATED POWER SLIP (DEFAULT = .05)
00101 320 DA = MECHANICAL DAMPING, JOULE-SEC
00101 330 SR = STATOR RESISTANCE, OHMS
00101 340 VO = RATED BUS VOLTAGE, VOLTS
00101 350 EF1 = INPUT PRODUCT EFFICIENCY
00101 360 PM1 = MAXIMUM INPUT POWER, KW
00101 370 CCI = CAPITAL COST/YEAR, $
00101 380 CMI = MAINTENANCE COST/YEAR, $
00101 390 C
00101 400 COMMON /CIMPL/ IMPL,ICNT /CTIME/ TIME
00101 410 COMMON /COST/ CC,CM,CO,CV /CSIMUL/ DUM(6),TINC,THAX
00101 420 C
00101 430 INITIALIZATION
00101 440 IF( IMPL.GT.0) GO TO 10
00101 450 EFF = 1.
00101 460 TMAX1 = TMAX, .99999
00101 470 IF(RSY.EQ. .99999) RSY = 1400.
00101 480 IF(RAS.EQ. .99999) RAS = .05
00101 490 IF(DA.EQ. .99999) DA = 0.
00101 500 IF(SR.EQ. .99999) SR = 6.0/RAP
00101 510 IF(VO.EQ. .99999) VO = 400.
00101 520 IF(PM1.EQ. .99999) PM1 = 1.E10
00101 530 PMN = 0.0
00101 540 SP = 0.0
00101 550 RATI = RAP*1000./VO
00101 560 EE = RAP/(RAP + SR*.001*RATI**2)
00101 570 C
00101 580 COMPUTE ROTOR SPEED AND OUTPUT POWER
00101 590 C
00101 600 10 IF( P1.GT. 0.) GO TO 20
00101 610 P2 = 0.0
00101 620 PL = 0.0
00101 630 RS = RSY
00101 640 GO TO 30
00101 650 C
00101 660 20 A = RAP/(EE+RAS)
00101 670 B = RSY/( 1 + RSY**2*DA**1.0966E-5)
00101 680 RS = B*(A + P1)
00101 690 P2 = RAP*(RS/RSY - 1.)/RAS
00101 700 IF (P2.GT.,RAP,AND.,IMPL.EQ.,2) WRITE(6,100)
00101 710 100 FORMAT(1H0, 40X,37HGENERATOR OUTPUT EXCEEDS RATED POWER /)
00101 720 C
00101 730 IF(P2.GT.,RAP,AND.,IMPL.EQ.,2)ICNT=ICNT+1
00101 740 PL = P1 - P2
00101 750 EFF = P2/P1
00101 760 30 EF2 = EF1*EFF
00101 770 PM2 = AMINI(RAP, PM1*EFF)
00101 780 C
00101 790 STATISTICS
00101 800 IF(IMPL.LE.1) RETURN
00101 810 PMN = AMAXI(PMN, P2/RAP)
00101 820 SP = SP + P2*.5*TINC
00101 830 C
00101 840 COST SUMMATION
00101 850 IF( TIME.LT.,TMAX1) RETURN
00101 860 CC = CC + CCI
00101 870 CM = CM + CMI
00101 880 C
00101 890 RETURN
00101 900 END
END FOR

```

FIGURE 6.1-2 SAMPLE COMPONENT CODE

when the model has presumably attained steady state values. Finally, the costs are added up when the simulation has reached the maximum time point. Capital costs, maintenance costs, and operating costs are stored in the first three locations of common block COST.

Figure 6.1-2 shows the code for the generator component GE. The program automatically assigns default parameters = .99999. Hence, when IMPL = 0 component dependent default values are assigned whenever the .99999 default is assumed. The code near Format statement 100 shows a typical diagnostic printout. The diagnostic is only printed if IMPL = 2 since we need only diagnose errors at the final iteration. Note that a counter ICNT is updated each time a diagnostic is printed. It is stored in the second location of common block CIMPL and is monitored to see if diagnostic print lines exceeds DLINES. If so, IMPL is set to 3 the final iteration, so that no further diagnostics are printed. The last convention observed here concerns the use of the maximum power and product efficiency variables denoted PM1, EF1, PM2, EF2. These variables are used to communicate information to the logic components PD and PA. The efficiency variable EFF is defined as the ratio of output power to input power except when P1 = 0. In this case the old EFF value is used, but in any case EFF = 0 must be avoided since this would communicate a zero efficiency to a logic device which would then generate an infinite request. It is seen that EF2 and PM2 represent the joint efficiency and maximum power at the output port as a consequence of the rated generator power and computed input/output efficiency.

Storage devices have in addition to the above, certain conventions to communicate with the logic components. An input parameter RE1 for port 1 request is used to initiate power discharge from storage. An output variable RE2 for port 2 request is used to communicate a maximum charge rate request and is usually computed by

$$RE2 = \text{MIN} (MP1, RAP) / EF1$$

where MP1 and EF1 are the input maximum power and input product efficiency,

and RAP denotes the maximum storage charging rate. A priority interrupt INT should also be defined so that  $INT = 1$ , when storage is empty or at a minimum,  $INT = 0$ . If no interrupt is required, and  $INT = -1$ , at full storage capacity. The state of storage is normally a state variable so that the code computes the state derivative at each time point and lets the Integrator update the state at each time point.

## 6.2 FILOAD PROGRAM

In addition to placing the subroutine representing the new standard component in the component library, descriptions of the inputs, outputs, and tables required by the new component must be added to the permanent file, M18. These lists are used by the Model Generation program to direct the connection of component inputs and outputs. The program FILOAD is provided to perform any of the following tasks:

1. Add new input, output, or table name lists.
2. Replace existing input, output or table name lists.
3. Remove all name lists for specified components.
4. Dump contents of M18 file onto Tape 9 in input format.

### 6.2.1 FILOAD Program Commands

The FILOAD program will recognize the following commands.

#### LIST STANDARD COMPONENTS

The LIST COMPONENTS command causes the program to print the input, output, and table lists for all components modified or added to the M18 file. If this command is not given the program will merely give a message stating the name of the new components being added to the file.

#### PURGE

The PURGE command can be used to remove a component from the M18 file. The PURGE command is followed by the names of the components to be purged. The command and the component names must be separated by one of the standard delimiters; i.e. [ ] three or more blanks, [,] comma, [=] equal sign, [()] left or right parentheses.

Example 6.3: PURGE = CM, TB, OB

This command would remove all lists for the CM, TB, and OB components from the name list file.

#### SYMBOL

The SYMBOL command may be used to designate the type of symbol that is to appear for each standard component in the lineprinter drawn model schematic diagram. The SYMBOL command is followed by the names of the components each followed by a symbol number. The symbol numbers and their associated symbols are shown in Figure 6.2-1. The SYMBOL command, component names, and symbol numbers are separated by standard delimiters.

Example: SYMBOL, CO = 100, SH = 200, TU = 300, OC = 400

If a symbol number is not specified for a component the default symbol of a square box will be used.

#### DUMP FILE

The DUMP FILE command causes the FILOAD program to dump the contents of the M18 file onto DUMPF9, in the input format of the FILOAD program. Thus for each standard component, a list of inputs, outputs, and tables will be produced. This data will be preceded by the command NEW FILE described below. This file may be edited to modify the input, output or tables description of any existing standard component or to derive a new standard component

STANDARD SCHEMATIC SYMBOLS

4	5	6	7	8
14	<pre> ** *  * *   * *    * * CO  * * 15  * *   * *    * *   * ** </pre> <p>SYMBOL = 100</p>	16	<pre> 00000000 0       0 0  OC   0 0  17   0 0       0 00000000 </pre> <p>SYMBOL = 400</p>	18
24	25	26	27	28
34	<pre> ***** *       * *  SH   * * 35   * *       * ***** </pre> <p>SYMBOL = 200</p>	36	<pre> ***** *       * *  ME   * * 37   * *       * ***** </pre> <p>SYMBOL = ANY OTHER NUMBER</p>	38
44	45	46	47	48
54	<pre> ** *  * *   * *    * * TU  * * 55  * *   * *    * *   * ** </pre> <p>SYMBOL = 300</p>	56	57	58
64	65	66	67	68

FIGURE 6.2-1 LIST OF STANDARD COMPONENT SYMBOLS

description from an existing one. The results of such an editing would then serve as input data to a subsequent run of the FILOAD program. Unless it is intended to purge the M18 file and start anew, the NEW FILE command at the beginning of DUMPF9 should be removed before the subsequent run of the FILOAD program.

#### NEW FILE

The NEW FILE command instructs the FILOAD program to construct a new M18 file. This command must occur as the first card in a set of data describing a completely new M18 file. Any previous components that may have existed on the M18 file are purged by this command. It is therefore only used when installing a complete new M18 file.

#### FILE NAME

This command is used to load the file name to be associated with the M18 file. The current M18 file name is WINDENERGY. This command is used as:

FILE NAME = WINDENERGY

#### 6.2.2 Input Name Lists

Input name lists are identified by the letters INPT following the component name. Thus, the input name list for a component DC would be introduced with the phrase, DCINPT. This must be followed by a phrase that contains the number of names in the input name list.

The input names are contained on the following data cards, 8 names per card. The names must be left adjusted in fields, 10 characters wide. The names are placed in Columns 1 through 3 of each field. Column 9 of each field can be used to indicate a port number which can be attached to the name to distinguish it from other quantities of the same name that occur with the given

component. Thus, to indicate that temperature, T, is an input to port 1, the input name list would be:

Column:	1	2	3	4	5	6	7	8	9	10
Item:	T									1

This quantity would then be referred to as T1.

Example 6.4:

```
SWINPT = 3
IN.....1.IN.....2.CNT
```

(The dots are used here to indicate blank spaces and would not be included in an actual data card).

These two data cards would indicate that the component SW had 3 input quantity names. A quantity IN appears at port 1, and is to be referred to as IN1. A quantity IN appears at port 2, and is to be referred to as IN2. A third input quantity CNT has no port designation. Note that if a port number is to be attached to a quantity name, that name should contain no more than 2 characters.

The sequence of names in the input name list must match the sequence of input arguments in the component call sequence.

### 6.2.3 Output Name Lists

Output name lists are identified by the letters OUTP following the component name. Thus, the output name list for a component DC would be introduced with the phrase, DCOUTP. This must be followed by a phrase that contains the number of names in the output name list.

The output names are contained on the following data cards, 8 names per card. The names must be left adjusted in fields 10 characters wide. The names are placed in Columns 1 through 3 of each field. Column 9 of each field can be used to introduce a port number which can be attached to the name to distinguish it from other quantities of the same name that occur with the given component. If the output quantity is a state variable, this must be indicated by placing S in Column 10 of the field. Thus, if power P is a state variable output quantity at port 2, the output name list would be:

Column:	1	2	3	4	5	6	7	8	9	10
Item:	P								2	S

This quantity would then be referred to as P2.

Example 6.5:

```
TZOUTP = 3
X.....1SX.....2SOUT
```

(The dots are used here to indicate blank spaces, and would not be included on an actual data card).

These two data cards would indicate that the component TZ had 3 output quantity names. A quantity X appears at port 1. This is a state variable, and will be referred to as X1. A quantity X is also a state variable that appears at port 2. It will be referred to as X2. The quantity OUT is an output variable, not a state variable, and does not have a port number associated with it. Note, that if a port number is to be attached to a quantity name that name should contain no more than 2 characters. These two characters plus the port number will reach the maximum number of 3 characters in a quantity name.

The sequence of names in the output name list must match the sequence of output arguments in the component call sequence. However, whereas three argu-

ments are provided for each state in the subroutine call sequence, only one name is included in the output name list.

#### 6.2.4 Table Name Lists

Table name lists are identified by the letters TABS, following the component name. Thus, the table name list for a component CM would be introduced with the phrase CMTABS. This must be followed by a phrase containing the number of names in the table name list. The table names are contained in the following cards, one table name per card. The name is located in the first 3 columns of the card. It must be accompanied by the maximum dimension that is to be provided for this table. This number must be given in columns 4 through 10 and should have a decimal point given. For single independent variable tables this number must be negative. For tables with two independent variables, this number must be positive.

Example:

```
CMTABS = 3
TAM      53.
TAB      43.
TCM     -27.
```

These four data cards would indicate that the component CM had 3 tables. The first two tables TAM and TAB have two independent variables each, as indicated by the positive dimension numbers. The table TCM has only one independent variable, as indicated by the negative dimension number. 53, 43, and 27 words of storage are to be provided for tables TAM, TAB, and TCM respectively. The maximum storage is related to the maximum number of primary, NX, and secondary, NZ, independent variables by:

$MAX = 3 + NX + NZ + NX * NZ$  for tables with two independent variables

$MAX = 3 + 2 * NX$  for tables with one independent variable

## 7.0 LIBRARY COMPONENT DESCRIPTIONS

This section describes the mathematical algorithms and input/output structure of the SIMWEST library components. Each component writeup contains a brief textual description of the algorithms, a mathematical expression summarizing its function, a list of input and output variables, and a description of the calculation sequence and logic used in the model. A figure is provided which shows the nominal input and output connections, and the state variables of each component.

There are a number of features and conventions in the component descriptions which require some elaboration. These are briefly summarized below.

### 7a. INPUT/OUTPUT NAME LISTS

A potentially confusing factor is the way port numbers on input parameters and output variables are designated. On the model generation input cards the name of the physical quantity and the port number is separated by a comma. For example, the power variable with port designation 1 is denoted P,1. In defining input to the simulation program, this same variable would be denoted P1. To emphasize the distinction between the physical quantities and port numbers, they are listed separately in the name lists of the component writeups. For example, P 1 in the name list denotes the power variable (or parameter) with port designation 1 even though in other parts of the text it may simply be denoted P1.

Another convention in the name lists is that the alphabetic symbol 'O' is shown as  $\emptyset$  to distinguish this symbol from a zero. Elsewhere in the text symbols such as  $V\emptyset$  may be referred to as  $V0$ .

## 7b. INPUT PARAMETER SPECIFICATION

All input parameters are associated with default values. Many of the parameters have default values denoted in the parameter description by the letter D. For example in the Battery component the default value for terminal resistance, RT, is D = .001 ohms. All input parameters for which a default value is not so specified has a default value of .99999. Default values are intended to enable users to put models together quickly by specifying a minimum of input data. Users need only specify detailed parameter values for those components of current interest. One must be careful using this approach since the operating characteristics and efficiency of a 10kw rated device may for example be quite different than for a 100kw device.

Any user specified input parameter can be driven by one or two dimension table lookups using the FU and FV components. This enables the user to build more detailed models using time or other output variables to drive the tables. For example, if one needs to specify cost of peak load generation to the utility component as a function of peak load request, then one adds FU as an input to UT and specifies load request as an input connection to FU. The desired function table is then input to FU.

It may be noted that not all of the components have maintenance or operating cost inputs. Thus, whenever these costs are important, one can aggregate such costs and input lumped costs to the model. For example, the maintenance cost of the hydro storage system may include maintenance costs for the pump and turbine.

## 7c. COMPONENT LOGIC

In constructing SIMWEST components, we have adopted several conventions to aid communication with the logic components. All physical components distributing power are given two input parameters EF and MP (port 1) and two output

variables EF and MP (port 2). The output EF is the product efficiency of all components in the distribution subsystem up to and including the given component, and MP is the maximum power deliverable at the output of the component. Each storage component has in addition a power request input denoted RE (port 1), a power request output denoted RE (port 2), and a priority interrupt flag denoted INT.

Figure 7.0 shows the logic and physical variable connections for power flow in and out of a hydro reservoir. Power flows from the power divider to the pump at a rate not to exceed the request RE from HS. The HS request is computed by dividing the input maximum power by the input (or pump) efficiency EF. Hence, the maximum power flowing to HS cannot exceed  $RE * EF = MP$ . Similarly, the input request to HS is computed by the PA component so as not to exceed the maximum input power MP divided by EF (turbine efficiency). Hence, the power that flows to PA cannot exceed  $RE * EF =$  input maximum power.

When the hydro reservoir is empty, the interrupt flag is turned on and the priority sequence is changed to 1 so that the reservoir is given access to power flowing into the divider.

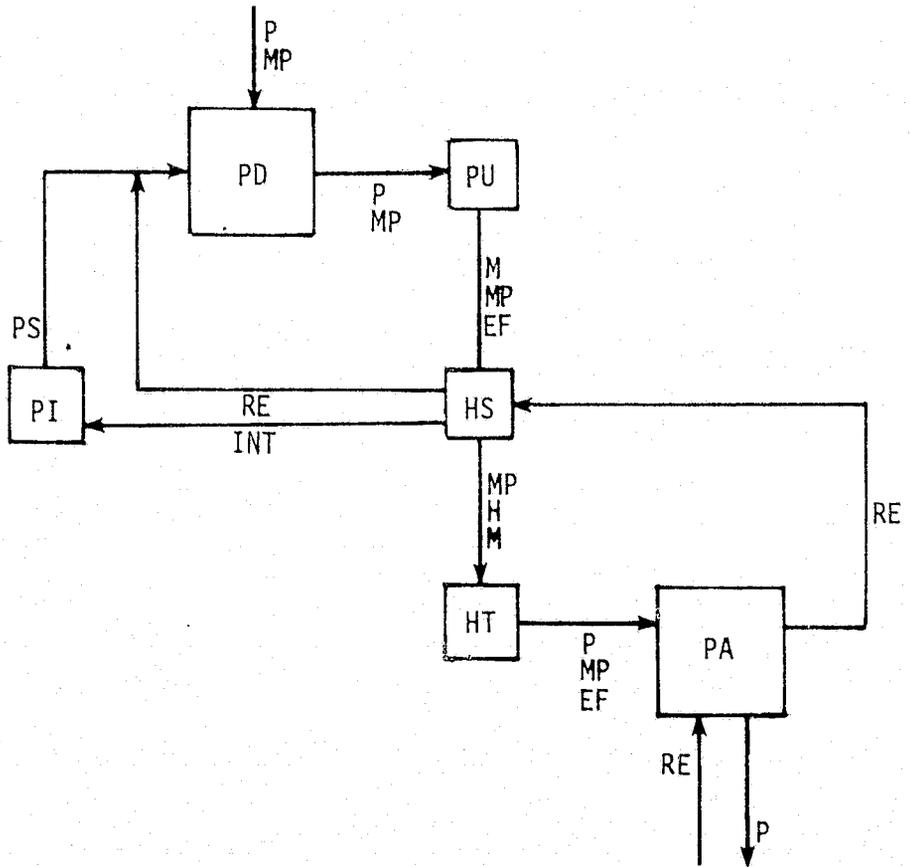
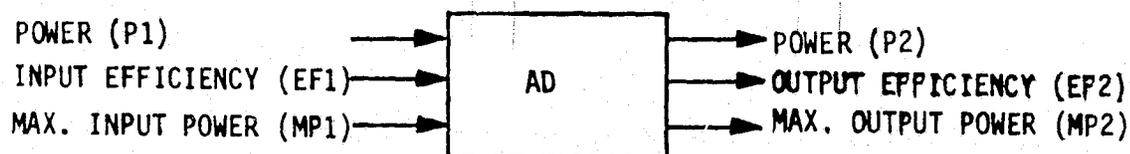


FIGURE 7.0 SAMPLE CONNECTIONS FOR LOGIC COMPONENTS

## 7.1 ADMITTANCE



The admittance model can be used to model transmission lines, transformers, capacitors or impedance power flows. A primary assumption is that the reactive parameters dominate the real parameters so that power transfer angle is solely based on reactive values, and power losses are based on the real admittance parameters and on power angle. The equation for power loss is based upon the following model:

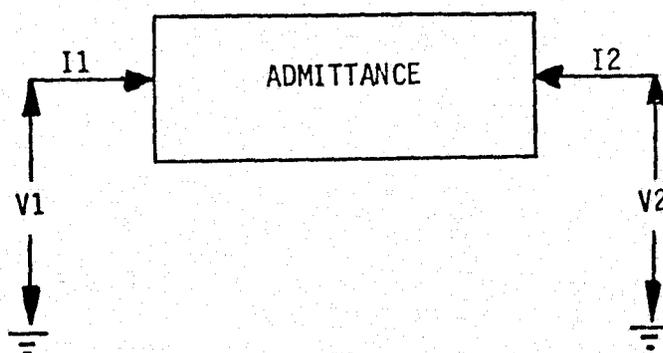


FIGURE 7.1 ADMITTANCE NETWORK MODEL

$$\begin{pmatrix} I_1 \\ I_2 \end{pmatrix} = \begin{pmatrix} G_1 + jB_1 & G_M + jB_M \\ G_M + jB_M & G_2 + jB_2 \end{pmatrix} \begin{pmatrix} V_1 \\ V_2 \end{pmatrix}$$

Where the reactive parameters  $B_1$  and  $B_2$  do not enter into the power loss calculations.

## Inputs

<u>Parameter/Port</u>	<u>Description</u>	<u>Units</u>
G1,GM,G2	Real admittance parameters *	mho
BM	Reactive admittance parameter * ( $\neq 0$ )	mho
V0	Rated voltage magnitude	volts
P            1	Input power	kw
EF            1	Input product efficiency	-
MP            1	Maximum input power	kw
CC	Capital cost/year	\$

## Outputs

<u>Variable/Port</u>	<u>Description</u>	<u>Units</u>
P            2	Output power	kw
PL	Power loss	kw
PA	Power angle	deg
EF            2	Output product efficiency	-
MP            2	Maximum output power	kw

\* - See next page for User Input to Model Transmission lines, Transformers and Impedances.

Transmission Line Input:

$$G1 = G2 = g * \ell$$

$$GM = -g * \ell$$

$$BM = 1 / (\omega * L * \ell)$$

where  $g$  = line conductance per unit length

$\ell$  = length of line

$\omega$  = frequency in radians/sec =  $120 \pi$

$L$  = line inductance per unit length

Transformer Input:

$$G1 = G2 = GM = 0$$

$$BM = 1 / X * h$$

where  $X$  = reactance in ohms

$h$  = turns ratio

(No power loss modeled with a transformer)

Impedance Input: (Includes capacitors and inductors)

$$G1 = G2 = -GM = R / (R^2 + X^2)$$

$$BM = X / (R^2 + X^2)$$

where  $R$  = resistance in ohms

$X$  = reactance in ohms

$$= \begin{pmatrix} \omega L & \text{for an inductance } L \\ -\frac{1}{\omega C} & \text{for a capacitance } C \end{pmatrix}$$

Calculation Sequence

If  $P_1 \leq 0$   $P_2 = PL = PA = 0$  and Return

1) Compute power angle

If  $P_1 * 1000 > BM * V_0^2$ ,  $\cos \theta = 0$  and write DIAGNOSTIC

$$\theta = -\sin^{-1}(P_1 * 1000 / BM * V_0^2)$$

$$PA = \theta * 180 / \pi$$

$$\cos \theta = \sqrt{1 - (P_1 * 1000 / BM * V_0^2)^2}$$

2) Compute power loss and output power

$$PL = V_0^2 * (G_1 + G_2 + 2 * GM * \cos \theta) / 1000$$

$$P_2 = P_1 - PL$$

$$EFF = P_2 / P_1$$

If  $P_2 > 0$  go to 3)

write DIAGNOSTIC

$$EFF = 1.$$

3) Efficiency and maximum output power

$$EF_2 = EF_1 * EFF$$

$$MP_2 = \min(MP_1, |BM| * V_0^2 / 1000) * EFF$$

4) Compute costs

SUBROUTINE AD ENTRY POINT 000212

STORAGE USED CODE(1) 000264; DATA(3) 000072; BLANK COMMON(2) 000000

## COMMON BLOCKS

```

0003 C IMPL 000002
0004 C TIME 000001
0005 C SIMUL 000010
0006 C COST 000001

```

## EXTERNAL REFERENCES (BLOCK, NAME)

```

0007 NWDUS
0010 NI02S
0011 ASIN
0012 SQPT
0013 NERR3S

```

## STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

```

0001 000017 10L      0001 000060 100L      0000 000006 108F      0001 000076 200L      0001 000140 300L
0000 000027 308F      0001 000162 400L      0006 R 000000 CCI      0005 000000 DUM      0000 R 000005 EFF
0003 I 000001 ICNT      0003 I 000000 IMPL      0000 000054 INJPS      0000 R 000001 RR      0000 R 000003 RPC
0000 R 000002 RR2      0000 R 000004 THETA      0004 R 000000 TIME      0005 R 000007 THAX      0000 R 000000 THAX1

```

```

00100 1* CAD
00101 2* SUBROUTINE AD(P2,PL,PA,EF2,MP2, G1,GM,G2,BM,VO,P1,EF1,HP1,CC)
00101 3* C
00101 4* C PURPOSE MODEL OF TRANSMISSION LINES,TRANSFORMERS,
00101 5* C CAPACITORS, OR IMPEDANCE POWER LOSS
00101 6* C
00101 7* C METHOD OUTPUT POWER AND POWER LOSS COMPUTED FROM
00101 8* C INPUT POWER
00101 9* C
00101 10* C WRITTEN BY Y.K.CHAN VERSION 1, JULY,1977
00101 11* C
00101 12* C CALL SEQUENCE
00101 13* C OUTPUTS
00101 14* C P2 -OUTPUT POWER,KW
00101 15* C PL -POWER LOSS,KW
00101 16* C PA -POWER ANGLE,DEG
00101 17* C EF2 -OUTPUT PRODUCT EFFICIENCY
00101 18* C MP2 -MAXIMUM OUTPUT POWER,KW
00101 19* C INPUTS
00101 20* C G1,GM,G2 -REAL ADMITTANCE PARAMETERS,MHO
00101 21* C PM -REACTIVE ADMITTANCE PARAMETERS (.NE.O.),MHO

```

AD

```

00101 22* C VO -RATED VOLTAGE MAGNITUDE,VOLTS C00000
00101 23* C P1 -INPUT POWER,KW C00000
00101 24* C EF1 -INPUT PRODUCT EFFICIENCY 000000
00101 25* C MP1 -MAXIMUM INPUT POWER,KW 000000
00101 26* C CC -CAPITAL COST/YEAR,$ 000000
00101 27* C C 000000
00103 28* COMMON /CIMPL/IMPL,ICNT/CTIME/TIME/CSIMUL/DUM(7),TMAX C00000
00103 29* X /COST/CCI C00000
00104 30* REAL MP2,MP1 000000
00104 31* C 000000
00105 32* P2=0. C00000
00106 33* 000000
00106 34* TPAX1=TMAX*.99999 000000
00107 35* IF(P1.GT.C.)GO TO 10 000003
00111 36* P2=0. 000006
00112 37* PL=C. 000007
00113 38* PA=C. 000010
00114 39* MP2=MP1 000011
00115 40* EF2=EF1 000013
00116 41* 60 TO 400 000015
00116 42* C 000015
00116 43* C COMPUTE POWER ANGLE 000015
00116 44* C 000015
00117 45* 10 RP=P1*1000./(BM*VO*VO) 000017
00120 46* RR2=RP*RR 000025
00121 47* IF(RR2.LE.1.)GO TO 100 000027
00123 48* PA=-90. 000032
00124 49* RFC=0. 000034
00125 50* IF(IMPL.EQ.2)WRITE(6,108)P1,BM,VO 000035
00133 51* 108 FORMAT(1HC,13H INPUT POWER ,F12.3,33H TOO HIGH RELATIVE TO ADMITTA 000050
00133 52* XNCE ,F12.3,19H AND RATED VOLTAGE ,F12.3) 000050
00134 53* IF(IMPL.EQ.2)ICNT=ICNT+1 000050
00136 54* GO TO 200 000056
00137 55* 100 THETA=-ASIN(RR) 000060
00140 56* PA=THETA*180./3.14159 000063
00141 57* RRC=SQRT(1.-RR2) 000066
00141 58* C 000066
00141 59* C COMPUTE POWER LOSS AND OUTPUT POWER 000066
00141 60* C 000066
00142 61* 200 PL=VO*VO*(G1+G2+2.*GH*RRC)/1000. 000076
00143 62* P2=P1-PL 000110
00144 63* EFF= P2/P1 000112
00145 64* IF(P2.GE.0.)GO TO 300 000114
00147 65* P2=0. 000117
00150 66* EFF=1. 000120
00151 67* IF(IMPL.NE.2)GO TO 300 000122
00153 68* WRITE(6,308)PL,P1 000125
00157 69* 308 FORMAT(1HC,24H ADMITTANCE POWER LOSS ,F12.3,21H EXCEEDS INPUT POWE 000134
00157 70* XR ,F12.3) 000134
00160 71* ICNT=ICNT+1 000134
00160 72* C 000134
00161 73* 300 EF2=EF1 000140
00162 74* IF(P2.GT.0.)EF2=EF1*EFF 000141
00164 75* MP2=AMIN1(MP1,ABS(BM)*VO*VO/1000.)*EFF 000147
00164 76* C 000147
00165 77* 400 IF(IMPL.LE.3)RETURN 000162
00167 78* IF(TIME.LT.TMAX1)RETURN 000170

```

00171  
00171  
00172  
00173

79\*  
80\*  
81\*  
82\*

C

CCI=CCI\*CC

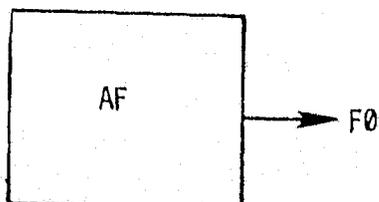
RETURN

END

000177  
000177  
000202  
000263

**AD**

## 7.2 TEST FUNCTION GENERATOR



### Inputs

#### Parameter/Port

C0D

Description  
Specifies which analytic function is calculated. (See equations below for use of these inputs)

C1

C2

C3

C4

C5

### Outputs

#### Variable/Port

F0

Output variable

### Calculation Sequence

- C0D = 1  $F0 = C1 + C2 * \sin(C3 * T + C4)$   
 2  $F0 = C1 + C2 * \cos(C3 * T + C4)$   
 3  $F0 = C1 + \exp(-C5 * T) * \sin(C3 * T + C4)$   
 4  $F0 = C1 + \exp(-C5 * T) * \cos(C3 * T + C4)$   
 5  $F0 = C1 + C2 * T$   
 6  $F0 = C1 + C2 * \exp(-C3 * T)$

where: T = TIME

SUBROUTINE AF ENTRY POINT 000143

STORAGE USED CODE(1) 000166; DATA(0) 000014; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CTIME 000001

EXTERNAL REFERENCES (BLOCK, NAME)

0004 NERR2\$  
 0005 SIN  
 0006 COS  
 0007 EXP  
 0010 NERR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000022	10L	0001	00013A	100L	0001	000035	20L	0001	000050	30L	0001	000073	40L
0001	000116	50L	0001	000123	60L	0000	000001	INJP\$	0000	I	000000	NEODE	0003	R 000000 TIME

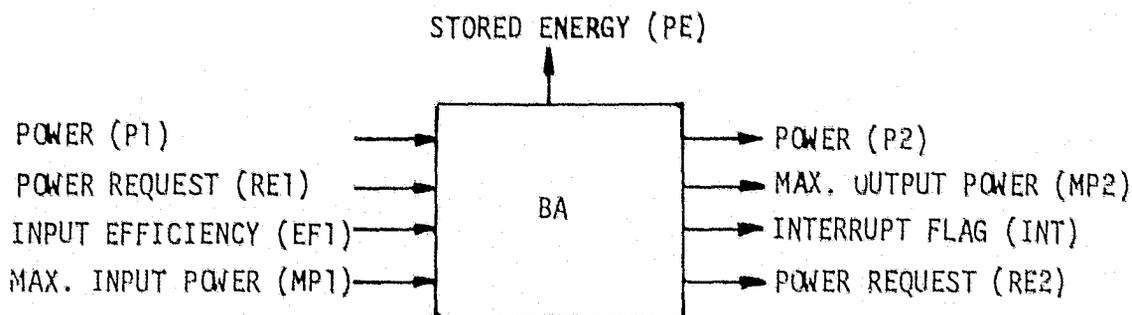
```

00100      1*      CAF
00101      2*      SUBROUTINE AF(FO,COD,C1,C2,C3,C4,C5)
00101      3*      C
00101      4*      C PURPOSE - TO SIMULATE ANALYTICAL FUNCTIONS
00101      5*      C
00101      6*      C
00101      7*      C METHOD - SEE CODING
00101      8*      C
00101      9*      C
00101     10*      C WRITTEN BY - ADAM LLOYD LATEST REVISION FEB 76
00101     11*      C
00101     12*      C
00101     13*      C LIMITATIONS - NONE
00101     14*      C
00101     15*      C
00101     16*      C INPUT/OUTPUT LIST
00101     17*      C
00101     18*      C
00101     19*      C FO OUTPUT VARIABLE ANY OUTPUT VAR
00101     20*      C COD CODE IDENTIFYING ANALYTICAL FUNCTION --- INPUT PARAM
00101     21*      C CODE= F00
00101     22*      C 1 C1+C2*SIN(C3*TIME+C4)
00101     23*      C 2 C1+C2*COS(C3*TIME+C4)
00101     24*      C 3 C1+C2*EXP(-C5*TIME)*SIN(C3*TIME+C4)
00101     25*      C 4 C1+C2*EXP(-C5*TIME)*COS(C3*TIME+C4)
00101     26*      C 5 C1+C2*TIME
00101     27*      C 6 C1+C2*EXP(-C5*TIME)
    
```

**AF**

00101	27*	C	C1	CONSTANT INPUTS FOR ABOVE EQNS	---	INPUT	PARAM	000000
00101	28*	C	C2	CONSTANT INPUTS FOR ABOVE EQNS	---	INPUT	PARAM	000000
00101	29*	C	C3	CONSTANT INPUTS FOR ABOVE EQNS	---	INPUT	PARAM	000000
00101	30*	C	C4	CONSTANT INPUTS FOR ABOVE EQNS	---	INPUT	PARAM	000000
00101	31*	C	C5	CONSTANT INPUTS FOR ABOVE EQNS	---	INPUT	PARAM	000000
00103	32*			COMMON/CTIME/TIME				000000
00104	33*			NCODE=000				000000
00105	34*			GO TO (10,20,30,40,50,60),NCODE				000006
00106	35*	10		F0=C1*C2*SIN(C3*TIME+C4)				000022
00107	36*			GO TO 100				000033
00110	37*	20		F0=C1*C2*COS(C3*TIME+C4)				000035
00111	38*			GO TO 100				000046
00112	39*	30		F0=C1*C2*EXP(-C5*TIME)*SIN(C3*TIME+C4)				000050
00113	40*			GO TO 100				000071
00114	41*	40		F0=C1*C2*EXP(-C5*TIME)*COS(C3*TIME+C4)				000073
00115	42*			GO TO 100				000114
00116	43*	50		F0=C1*C2*TIME				000116
00117	44*			GO TO 100				000121
00120	45*	60		F0=C1*C2*EXP(-C5*TIME)				000123
00121	46*	100		RETURN				000134
00122	47*			END				000165

## 7.3 BATTERY



The battery model is based on the circuit diagram shown below. Current flow is determined by the output power request minus input power. Battery leakage is proportional to stored energy. Priority interrupt logic is activated when a minimum or maximum capacity level is attained.

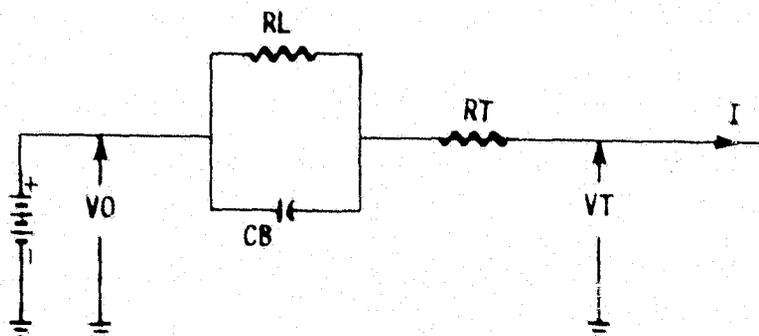


FIGURE 7.3 BATTERY CIRCUIT DIAGRAM

### Basic Equations

The output power P2, stored energy PE, terminal current I, and capacitor voltage VC is computed using the following equations:

$$P2 = RE1$$

$$PE = (VC^2 + 2 * V0 * VC) * CB / 7.2 * 10^6$$

$$(P2 - P1) * 1000 = (V0 + VC) I - I^2 * RT$$

$$PE = -(I + VC / RL) (VC + V0) / 1000$$

## Inputs

<u>Parameter/Port</u>	<u>Description</u>	<u>Units</u>
P 1	Input power	kw
V0	Internal voltage	volts
RT	Terminal resistance (D = 0.001)	ohms
CB <sup>1</sup>	Battery capacitance (D = 2.88x10 <sup>8</sup> )	farads
RL <sup>1</sup>	Leakage resistance (D = 0.05)	ohms
RAP	Rated input power	kw
EF 1	Input product efficiency	-
MP 1	Maximum input power	kw
E1	Maximum energy storage	kwh
RE 1	Power request	kw
EDE	Energy deadband for priority resequencing	kwh
DT	Down time for priority resequencing	h
CC	Capital cost/year	\$
CM	Maintenance cost/year	\$

## Outputs

<u>Variable/Port</u>	<u>Description</u>	<u>Units</u>
P 2	Output power (=RE1)	kw
PE	Stored energy (state of charge)	kwh
I	Terminal current (+=out, -=in)	amps
VC	Capacitor voltage	volts
VT	Terminal voltage	volts
PL	Power loss	kw
T0	Time when battery was discharged	h
MP 2	Maximum output power	kw
INT	Priority interrupt flag	-
RE 2	Maximum charging rate request	kw

D - Default values supplied

1 - Battery leakage time constant in hours = CB\*RL/3600

## Statistics

<u>Variable/Port</u>	<u>Description</u>	<u>Units</u>
MPE	Maximum stored energy	kwh
SPC	Sum of charging energy	kwh
SPD	Sum of discharging energy	kwh

## Calculation Sequence

- 1) Compute VC

$$VC = \sqrt{7.2 \times 10^6 * PE / CB + V0^2} - V0$$

- 2) Solve for terminal current I

If  $(P2 - P1) * 1000 \geq (VC + V0)^2 / 4 * RT$ , GO TO 2'

$$I = \frac{(VC + V0) - \sqrt{(VC + V0)^2 - 4 * RT * (P2 - P1) * 1000}}{2 * RT}$$

Go to 3)

- 2')  $I = (VC + V0) / 2 * RT$  and write DIAGNOSTIC

- 3) Compute VT

$$VT = VC + V0 - I * RT$$

- 4) Potential energy balance and power loss

$$PE = -(1 + VC / RL) (VC + V0) / 1000.$$

$$PL = (I^2 * RT + VC^2 / RL) / 1000.$$

- 5) Maximum charging and discharging rates

$$RE2 = \text{MIN}(MP1, RAP, (E1 - PE) / TINC) / EF1$$

$$MP2 = \text{MIN}(RAP, (VC + V0)^2 / (4000 * RT), (PE - EDE) / TINC)$$

where TINC = integration step size

Calculation Sequence Cont.

## 6) Priority interrupt logic

If  $PE \leq EDE$  and  $T0 = 10^6$ ,  $T0 = TIME$

If  $PE \leq EDE$  and  $TIME - T0 \geq DT$ ,  $INT = 1$  and go to 7)

$T0 = 10^6$

If  $PE > 2 \times EDE$  and  $INT = 1$ ,  $INT = 0$

If  $PE \geq E1$ ,  $INT = -1$

If  $PE < E1 - EDE$  and  $INT = -1$ ,  $INT = 0$

## 7) Compute Statistics and Costs

SUBROUTINE BA ENTRY POINT 000372

STORAGE USED CODE(1) 000537; DATA(0) 000105; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CIMPL 000002  
 0004 CTIME 000001  
 0005 CSIMUL 000010  
 0006 COST 000002

EXTERNAL REFERENCES (BLOCK, NAME)

0007 SQRT  
 0010 DSORT  
 0011 NWDUS  
 0012 NI025  
 0013 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000036 100L	0001 000111 200L	0000 000015 208F	0001 000136 300L	0001 000316 400L
0001 000274 401L	0001 000314 403L	0000 D 000000 AA	0000 R 000010 AP1	0000 R 000011 AP2
0000 D 000002 B	0000 D 000004 B2	0000 R 000012 C	0006 R 000000 CCI	0006 R 000001 CMI
0005 R 000000 DUM	0000 R 000013 ED2	0003 I 000001 ICNT	0003 I 000000 IMPL	0000 000053 INJPS
0004 R 000000 TIME	0000 R 000006 TINCI	0005 R 000007 TMAX	0000 R 000007 TMAX1	0000 R 000014 WAIT

00100	1*	CBA		000000
00101	2*		SUBROUTINE BA(P2,PE,PED,IPE,I,VC,VT,PL,TO,MP2,INT,RE2,MPE,SPC,SPD,	000000
00101	3*	1	P1,VO,RT,CB,RL,RAP,CF1,MP1,E1,RE1,EDE,DT,CC,CM)	000000
00101	4*	C		000000
00101	5*	C	PURPOSE BATTERY MODEL	000000
00101	6*	C		000000
00101	7*	C	METHOD COMPUTE STORED ENERGY AND POWER OUTPUT AS	000000
00101	8*	C	FUNCTIONS OF POWER INPUT AND POWER REQUEST.	000000
00101	9*	C	A RESISTOR/CAPACITOR NETWORK IS USED TO	000000
00101	10*	C	MODEL BATTERY STORAGE.	000000
00101	11*	C		000000
00101	12*	C	WRITTEN BY Y.K.CHAN	000000
00101	13*	C	VERSION 1, JUNE 3,1977	000000
00101	14*	C	CALL SEQUENCE	000000
00101	15*	C	OUTPUTS	000000
00101	16*	C	P2 -OUTPUT POWER, KW	000000
00101	17*	C	PE -STORED ENERGY (STATE),KWH	000000
00101	18*	C	PED -STORED ENERGY DERIVATIVE	000000
00101	19*	C	IPE -INTEGRATOR CONTROL	000000
00101	20*	C	I -TERMINAL CURRENT (+=OUT, -=IN), AMPS	000000

BA

```

00101 21* C VC -CAPACITOR VOLTAGE, VOLTS 000000
00101 22* C VT -TERMINAL VOLTAGE, VOLTS 000000
00101 23* C PL -POWER LOSS, KW 000000
00101 24* C TO TIME WHEN BATTERY WAS DISCHARGED, HR 000000
00101 25* C MP2 -MAXIMUM OUTPUT POWER, KW 000000
00101 26* C INT -PRIORITY INTERRUPT FLAG 000000
00101 27* C RE2 -MAXIMUM CHARGING RATE REQUEST, KW 000000
00101 28* C STATISTICS 000000
00101 29* C SPC -SUM OF CHARGING ENERGY, KWH 000000
00101 30* C MPE -MAXIMUM STORED ENERGY, KWH 000000
00101 31* C SPD -SUM OF DISCHARGING ENERGY, KWH 000000
00101 32* C INPUTS 000000
00101 33* C P1 -INPUT POWER, KW 000000
00101 34* C V0 -INTERNAL VOLTAGE, VOLTS 000000
00101 35* C PT -TERMINAL RESISTANCE, OHMS 000000
00101 36* C CB -BATTERY CAPACITANCE, FARADS 000000
00101 37* C RL -LEAKAGE RESISTANCE, OHMS 000000
00101 38* C RAP -RATED INPUT POWER, KW 000000
00101 39* C EF1 -INPUT PRODUCT EFFICIENCY 000000
00101 40* C MP1 -MAXIMUM INPUT POWER, KW 000000
00101 41* C E1 -MAXIMUM ENERGY STORAGE, KWH 000000
00101 42* C RE1 -POWER REQUEST, KW 000000
00101 43* C EDE -ENERGY DEADBAND FOR PRIORITY RESEQUENCING, KWH 000000
00101 44* C DT -DOWNTIME FOR PRIORITY RESEQUENCING, HR 000000
00101 45* C CC -CAPITAL COST/YEAR, $ 000000
00101 46* C CM -MAINTENANCE COST/YEAR, $ 000000
00101 47* C
00103 48* COMMON /CIMPL/IMPL,ICNT/CTIME/TIME/CSIMUL/DUM(7),TMAX/COST/CCI,CHI 000000
00104 49* REAL I,MP2,MPE,MP1,INT 000000
00105 50* DOUBLE PRECISION AA,B,RZ 000000
00106 51* TINCI=DUM(7)*.5 000000
00106 52* C 000000
00107 53* IF(IMPL.GT.0) GO TO 100 000002
00111 54* IF(IRT.EQ..99999)RT=.001 000005
00113 55* IF(CB.EQ..99999)CB=2.88E8 000012
00115 56* IF(PL.EQ..99999)RL=.05 000017
00117 57* T0=1000000. 000024
00120 58* INT=0 000026
00121 59* TMAX1=TMAX*.99999 000027
00122 60* 000032
00122 61* MPE=0. 000032
00123 62* SPC=0. 000033
00124 63* SPD=0. 000034
00124 64* C 000034
00124 65* C CAPACITOR VOLTAGE 000034
00124 66* C 000034
00125 67* 100 VC=SQRT((7.2E6)*PE/CB + V0**2) -V0 000036
00125 68* C 000036
00125 69* C TERMINAL CURRENT 000036
00125 70* C 000036
00126 71* P2=RE1 000051
00127 72* AA=(P2-P1)*4000.*RT 000053
00130 73* B=VC+V0 000062
00131 74* R2=B*R 000066
00132 75* IF(AA.GT.82) GO TO 200 000070
00134 76* I= B-DSORT(B2-AA) 000073
00135 77* I=I/(2.*RT) 000103

```

```

00136 78*      GO TO 300
00136 79*      C
00137 80*      200 I=B/(2.*RT)
00140 81*      IF(IMPL.EQ.2)WRITE(6,208)P2
00144 82*      208 FORMAT(1H0,15H POWER REQUEST ,F12.3,50H EXCEEDS BATTERY CAPABILITY
00144 83*      1. CHECK VC,VO, AND RT. )
00145 84*      IF (IMPL.EQ.2)ICNT=ICNT+1
00145 85*      C
00145 86*      C          TERMINAL VOLTAGE
00145 87*      C
00147 88*      300 VT=VC+VO-I*RT
00147 89*      C
00147 90*      C          POTENTIAL ENERGY BALANCE AND ENERGY LOSS
00147 91*      C
00150 92*      IF(IPE.NE.0)PED=(-I-VC/RL)*(VC+VO)/1000.
00152 93*      PL=(I*I*RT+VC+VC/RL)/1000.
00152 94*      C
00152 95*      C          MAXIMUM CHARGING AND DISCHARGING RATES
00152 96*      C
00153 97*      AP1= AMAX1(0.,(E1-PE)/DUM(7))
00154 98*      RE2=AMIN1(MPI,RAP,AP1)
00155 99*      RE2=RE2/EF1
00156 100*     AP2= AMAX1(0.,(PE-EDE)/DUM(7))
00157 101*     MP2=AMIN1(RAP,B2/(4000.*RT),AP2)
00157 102*     C
00157 103*     C          PRIORITY INTERRUPT
00157 104*     C
00160 105*     C=E1-EDE
00161 106*     ED2=EDE+EDE
00162 107*     IF(PE.GT.EDF)GO TO 401
00164 108*     IF(TO.GT.999999.)TO=TIME
00166 109*     WAIT=TIME-TO
00167 110*     IF (WAIT.GT.DT)INT=1
00171 111*     GO TO 400
00172 112*     401 TO=1000000
00173 113*     IF(PE.LE.ED2)GO TO 400
00175 114*     IF(PE.GT.E1)GO TO 403
00177 115*     IF(PE.GT.C)GO TO 400
00201 116*     INT=0
00202 117*     GO TO 400
00203 118*     403 INT=-1
00204 119*     400 CONTINUE
00204 120*     C
00205 121*     IF(IMPL.LE.1)RETURN
00205 122*     C
00205 123*     C          STATISTICS
00205 124*     C
00207 125*     MPE=AMAX1(MPE,PE)
00210 126*     SPC=SPC+TINC1*P1
00211 127*     SPD=SPD+TINC1*P2
00211 128*     C
00212 129*     IF(TIME.LT.TMAX1)RETURN
00214 130*     CCI=CCI+CC
00215 131*     CHI=CHI+CH
00215 132*     C
00216 133*     RETURN
00217 134*     END

```

```

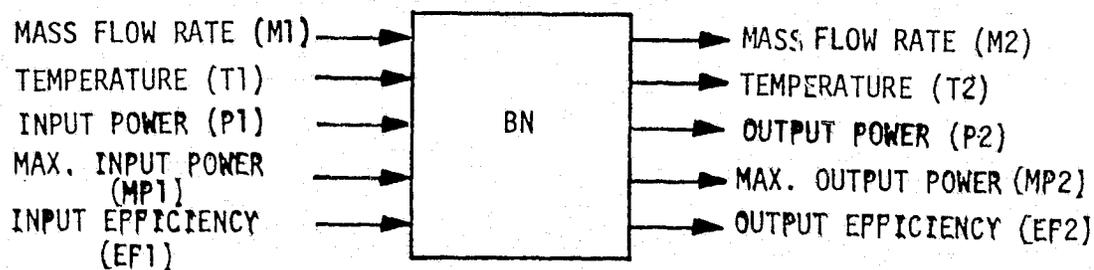
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## 7.4 BURNER



The burner model computes the amount of fuel required to be burned in the inlet airstream to raise the air temperature from the given inlet temperature to the specified outlet temperature. The fuel mass flow rate when integrated over time allows calculation of the cost of burner fuel.

### Basic Equation

The mass of fuel consumed,  $F$ , is computed from the equation:

$$\dot{F} = \frac{M1 * CP * (T2 - T1)}{NU * HF}$$

Inputs

<u>Parameter/Port</u>		<u>Description</u>	<u>Units</u>
M	1	Inlet air mass flow rate	lb/h
CP		Air heat capacity (D = $72 \times 10^{-6}$ )	kwh/lb-°F
T	1	Inlet air temperature	°F
T	3	Outlet air temperature (specified)	°F
NU		Combustor efficiency (D = 0.98)	-
HF		Fuel heating value (D = 5.56)	kwh/lb
CF		Specific fuel cost (D = 0.094)	\$/lb
FDM		Maximum allowable fuel mass flow rate (D=17800)	lb/h
CB		Burner cost coefficient (D = 1.683)	\$/lb/h
LE		Burner life expectancy	years
MDM		Maximum allowable air mass flow rate (D=27000)	lb/h
EF	1	Input product efficiency	-
MP	1	Maximum input power	kw
P	1	Input power	kw

Outputs

<u>Variable/Port</u>			
F		Fuel mass consumed (state)	lb
EF	2	Output product efficiency	-
MP	2	Maximum output power	kw
T	2	Outlet air temperature	°F
FD		Fuel mass flow rate	lb/h
CC0		Burner capital cost/year	\$
C0		Fuel cost	\$
M	2	Outlet mass flow rate (= M1)	lb/h
P	2	Output power	kw

Statistics

FDU		Maximum fuel mass flow rate	lb/h
-----	--	-----------------------------	------

D - Default values supplied

The calculation sequence and default values are based on a burner sized using first principles to maintain the outlet temperature at 600°F assuming an inlet temperature of 120°F and a mass flowrate of  $2.7 \times 10^4$  lb/h. These conditions represent the extreme conditions expected and should satisfy all burner requirements. No. 6 fuel oil is assumed to be the fuel type. Cost and heating values were obtained from References 1 and 2. Cost estimates for the burner were estimated from the results of Reference 1.

## Calculation Sequence

### 1) Capital Cost

$$CC0 = CB * MDM / LE$$

### 2) Maximum air mass flow rate allowed

If  $M1 = 0$  set  $EFF = 1$ ,  $MP2 = MP1$  and go to 3)

$$M1M = \min \left\{ \frac{NU * HF * FDM}{CP * (T3 - T1)}, MDM \right\}$$

If  $T1 > T3$ ,  $M1M = MDM$

### 3) Efficiency and maximum discharge power

$$EFF = 1 + M1 * CP * (T2 - T1) / P1 \quad (\text{if } P1 > 0)$$

$$EF2 = EF1 * EFF$$

$$MP2 = \min \{ MP1 * EFF, P1 * M1M / M1 \} \quad (\text{if } M1 > 0)$$

$$P2 = P1 * EFF$$

- 
1. "Preliminary Feasibility Evaluation of Compressed Air Storage Power Systems," United Technologies AER 74-00242, December 1976.
  2. Steam, Its Generation and Use, Babcock and Wilcox, New York, NY, 1972.

Calculation Sequence Cont.

4) Fuel mass flow rate

$$\dot{F} = \frac{M1 * CP * (T2 - T1)}{NU * HF}$$

$$T2 = \text{MAX}(T1, T3)$$

If  $M1 > M1M$  write DIAGNOSTIC

5) Compute Statics and Costs

$$C0 = CF * F$$

SUBROUTINE BN ENTRY POINT 000270

STORAGE USED CODE(1) 000411; DATA(0) 000052; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CIMPL 000002  
 0004 CTIME 000001  
 0005 CSIMUL 000010  
 0006 COST 000003

EXTERNAL REFERENCES (BLOCK, NAME)

0007 NW0US  
 0010 NIO2\$  
 0011 NERR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000056	100L	0001	000237	1000L	0000	000003	1010F	0001	000121	200L	0001	000107	300L				
0006	R	000000	CCI	0006	000001	CHI	0006	R	000002	COP	0005	000000	DUM	0000	R	000002	EFF	
0003	I	000001	ICNT	0003	I	000000	IMPL	0000	000034	INJP\$	0000	R	000000	MIM	0004	R	000000	TIME
0005	R	000007	TMAX	0000	R	000001	TMAX1											

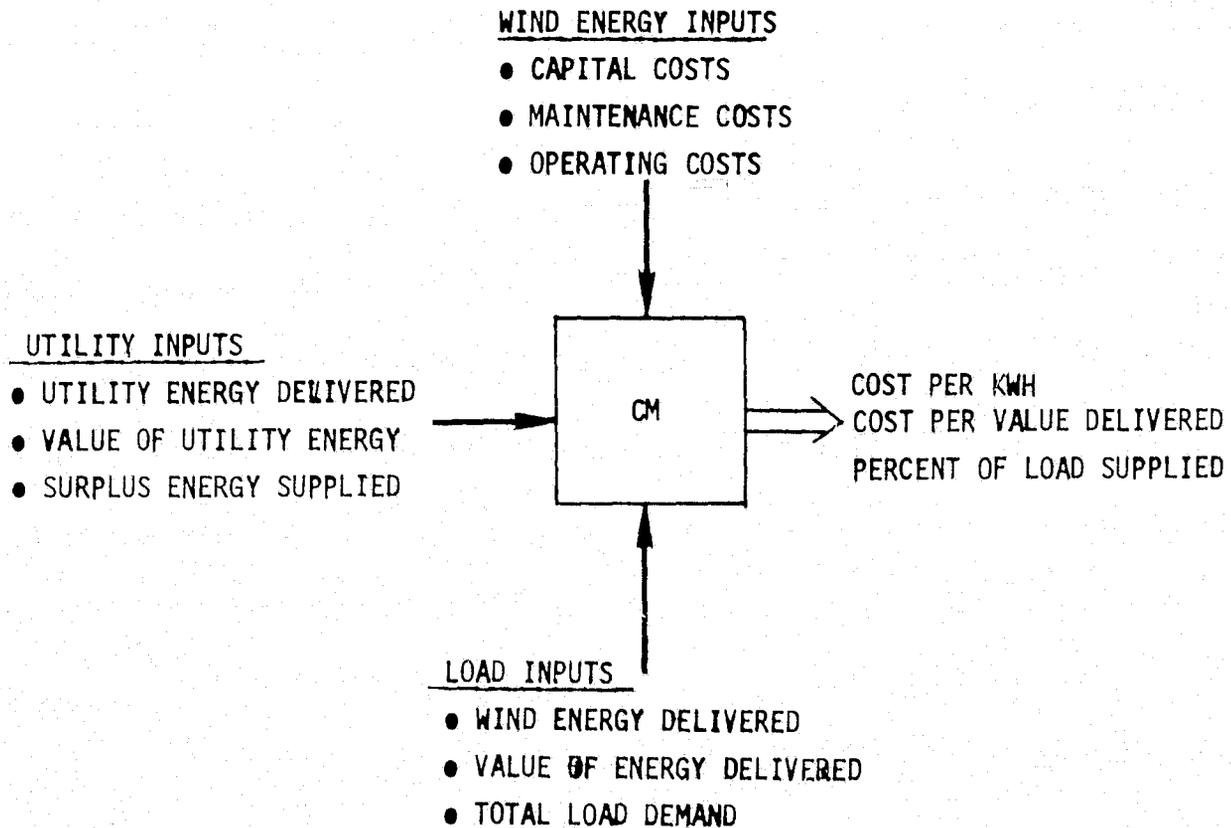
00100	1*	CBN																000000
00101	2*		SUBROUTINE BN(F,DF,IF,EF2,MP2,T3,FD,CC,CO,M2,P2,FDU,M1,CP,T1,T2															000000
00101	3*		1															000000
00101	4*	C																000000
00101	5*	C	PURPOSE	COMPUTE FUEL REQUIRED TO RAISE THE AIRSTREAM														000000
00101	6*	C																000000
00101	7*	C		TEMPERATURE A GIVEN INCREMENT.														000000
00101	8*	C																000000
00101	9*	C	METHOD	INTEGRATE THE FUEL MASS FLOW RATE OVER TIME														000000
00101	10*	C																000000
00101	11*	C	WRITTEN BY F.O. MAHONY					VERSION 1, MARCH 22 1977										000000
00101	12*	C																000000
00101	13*	C	CALL SEQUENCE															000000
00101	14*	C																000000
00101	15*	C	OUTPUTS															000000
00101	16*	C	F	- FUEL MASS CONSUMED SINCE TIME=0 (STATE), LB														000000
00101	17*	C	DF	- FUEL MASS DERIVATIVE														000000
00101	18*	C	IF	- STATUS INDICATOR														000000
00101	19*	C	EF2	- OUTPUT PRODUCT EFFICIENCY														000000
00101	20*	C	MP2	- MAXIMUM OUTPUT POWER, KW														000000
00101	21*	C	T3	- OUTLET AIR TEMPERATURE, DEG F														000000
00101	22*	C	FD	- FUEL MASS FLOW RATE, LB/HR														000000
00101	23*	C	CC	- BURNER CAPITAL COST/YEAR, \$														000000

BN

00101	24*	C	C0 - FUEL COST, \$	000000
00101	25*	C	M2 - OUTLET MASS FLOW RATE, LB/HR	000000
00101	26*	C	P2 - OUTPUT POWER, KW	000000
00101	27*	C	FDU - OBSERVED MAXIMUM FUEL MASS FLOW RATE, LB/HR	000000
00101	28*	C		000000
00101	29*	C	INPUTS	000000
00101	30*	C	M1 - INLET AIR MASS FLOW RATE, LB/HR	000000
00101	31*	C	CP - AIR HEAT CAPACITY, KWH/LB-DEG F	000000
00101	32*	C	T1 - INLET AIR TEMPERATURE, DEG F	000000
00101	33*	C	T2 - OUTLET AIR TEMPERATURE, DEG F	000000
00101	34*	C	NU - COMBUSTER EFFICIENCY	000000
00101	35*	C	HF - FUEL HEATING VALUE, KWH/LB-DEG F	000000
00101	36*	C	CF - SPECIFIC FUEL COST	000000
00101	37*	C	FDH - MAXIMUM ALLOWABLE FUEL MASS FLOW RATE, LB/HR	000000
00101	38*	C	CB - BURNER COST COEFFICIENT	000000
00101	39*	C	LE - BURNER LIFE EXPECTANCY, YEARS	000000
00101	40*	C	MDH - MAXIMUM ALLOWABLE AIR MASS FLOW RATE, LB/HR	000000
00101	41*	C	EF1 - INPUT PRODUCT EFFICIENCY	000000
00101	42*	C	MP1 - MAXIMUM INPUT POWER, KW	000000
00101	43*	C	P1 - INPUT POWER, KW	000000
00101	44*	C		000000
00103	45*		COMMON/CIMPL/IMPL,ICNT /CTIME/TIME /CSIMUL/DUM(7),TMAX	000000
00104	46*		COMMON/COST/CCI,CHI,COP	000000
00105	47*		REAL MP2,M2,M1,NU,LE,MDH,MP1,M1M	000000
00105	48*	C		000000
00106	49*		IF(IMPL.GT.0) GO TO 100	000000
00110	50*		TMAX1 =TMAX*.999999	000002
00111	51*		IF(CP .EQ. .999999) CP = 72.0E-6	000005
00113	52*		IF(NU .EQ. .999999) NU = 0.98	000012
00115	53*		IF(HF .EQ. .999999) HF = 5.56	000017
00117	54*		IF(CF .EQ. .999999) CF = 0.094	000024
00121	55*		IF(FDH.EQ. .999999) FDH=1.78E+4	000031
00123	56*		IF(CB .EQ. .999999) CB =1.683	000036
00125	57*		IF(MDH.EQ. .999999) MDH=2.7E+4	000043
00125	58*	C		000054
00127	59*		FDU = 0.0	000050
00130	60*		CC =CR*MDH/LE	000051
00131	61*	100	EFF=1.0	000056
00132	62*		IF(M1.EQ.0.0)GO TO 200	000057
00134	63*		M1M=MDH	000061
00135	64*		IF(T1.GT.T2) GO TO 200	000063
00135	65*	C		000063
00135	66*	C	MAXIMUM ALLOWABLE AIR FLOW RATE	000063
00135	67*	C		000063
00137	68*		M1M=AMIN1(NU*HF*FDH/CP/(T2-T1),MDH)	000067
00137	69*	C		000067
00140	70*		IF(M1.GT.M1M) GO TO 1000	000103
00142	71*	300	CONTINUE	000107
00142	72*	C		000107
00142	73*	C	EFFICIENCY AND MAXIMUM DISCHARGE POWER	000107
00143	74*		IF(P1.EQ.0.0)GO TO 200	000107
00143	75*	C		000107
00143	76*	C		000107
00145	77*		EFF = 1.0+M1*CP*(T2-T1)/P1	000110
00145	78*	C		000110
00146	79*	200	EF2 = EF1*EFF	000121
00147	80*		MP2=MP1	000123

00150	81*		IF(M1.GT.0.) HP2=AMIN1(MP1*EFF,P1*M1M/M1)	000125
00152	82*		P2=P1*EFF	000142
00152	83*	C		000142
00152	84*	C	FUEL FLOW RATE	000142
00152	85*	C		000142
00153	86*		IF(IF.NE.0) DF= M1*CP*(T2-T1)/NU/HF	000145
00155	87*		IF(T1.GT.T2) DF=0.0	000157
00157	88*		FD=DF	000164
00157	89*	C		000164
00157	90*	C	COSTS	000164
00160	91*		CO = CF*F	000166
00161	92*		T3= AMAX1(T1,T2)	000171
00162	93*		M2=M1	000177
00162	94*	C		000177
00162	95*	C	STATISTICS	000177
00163	96*		IF(IMPL.LE.1) RETURN	000201
00163	97*	C		000201
00165	98*		FDU = AMAX1(FD,FDU)	000210
00165	99*	C		000210
00166	100*		IF(TIME.LT.TMAX1) RETURN	000216
00170	101*		CCI= CCI + CC	000225
00171	102*		COP= COP + CO	000230
00172	103*		RETURN	000233
00172	104*	C		000233
00173	105*		1000 IF(IMPL.EQ.2)WRITE(6,1010) M1,M1M	000237
00200	106*		1010 FORMAT(1H0,28HBN INLET AIR MASS FLOW RATE ,F12.3,	000250
00200	107*		1 36H GREATER THAN MAXIMUM ALLOWABLE ,F12.3)	000250
00201	108*		IF(IMPL.EQ.2)ICNT=ICNT+1	000250
00203	109*		GO TO 300	000256
00204	110*		END	000410

## 7.5 COST MONITOR<sup>1</sup>



This component sums the capital, operating and maintenance costs of all system components. The total yearly cost TC is then computed using a fixed charge rate factor which represents depreciation, cost of money, insurance and taxes.

<sup>1</sup> This component must be placed last in the model generation input file, i.e., just prior to the END OF MODEL command.

The total wind energy delivered to the loads plus surplus energy is then summed and yearly energy delivered TED computed. Cost of operation in mills is then given by

$$\text{Wind system cost/kwh} = \text{TC} * 1000./\text{TED}$$

Similarly, the value of energy delivered to the loads is summed minus the utility energy value and including the value of surplus energy, and factored to give yearly energy value delivered VED. Energy value in mills is given by

$$\text{Load value/kwh} = \text{VED} * 1000./\text{TED}.$$

Cost per value delivered is the ratio of the above two equations.

In addition to the above cost calculations, percent of total load supplied by wind storage PCW, percent of load supplied by utilities PCU and, percent of wind energy surplus to the utilities PCS is computed. The total cost in mills to meet the load is then given by

$$\text{Load cost/kwh} = (\text{wind system cost/kwh} * \text{PCW} + \text{utility cost/kwh} * \text{PCU})/100.,$$

where

$$\text{Utility cost/kwh} = \text{value of utility energy} * 1000./\text{utility energy delivered}.$$

## Inputs

<u>Parameter/Port</u>	<u>Description</u>	<u>Units</u>
CR	Capital charge rate	%/year
LE	System life expectancy	years

## Common Block Inputs

CC	Total yearly capital costs	\$
CM	Total yearly maintenance costs	\$
CO	Operating and fuel costs over TMAX	\$
TMAX	Simulation time interval	hr
VDE	Value of energy delivered (including surplus)	\$
TDE	Wind energy delivered (including surplus)	kwh
TLD	Total load demand	kwh
UTV	Value of utility energy	\$
UTD	Utility energy delivered	kwh
SPD	Surplus wind energy supplied	kwh

## Outputs <sup>1</sup>

Total yearly costs (TC)	\$
Yearly energy delivered (TED)	kwh
Cost of energy per kwh	mills
Yearly value delivered (VED)	\$
Cost per value delivered	-
Percent of load supplied by	
Wind Storage (PCW)	-
Utility (PCU)	-
Surplus energy load factor (PCS)	-
Total load cost per kwh	mills

<sup>1</sup> Printout only occurs when simulation is completed. Thus no output variable symbol is required.

SUBROUTINE CM ENTRY POINT 000213

STORAGE USED CODE(1) 000226; DATA(0) 000330; BLANK COMMON(2) 000000

## COMMON BLOCKS

```

0003 COST 000011
0004 CIMPL 000001
0005 CTIME 000001
0006 CSIMUL 000010

```

## EXTERNAL REFERENCES (BLOCK, NAME)

```

0007 NWIND$
0010 NIO2$
0011 NEPR3$

```

## STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

```

0001 000020 100L      0000 000016 200F      0000 000034 300F      0000 000105 400F      0000 000210 500F
0003 R 000000 CC      0000 R 000003 CCY      0003 R 000001 CMA      0003 R 000002 CO      0000 R 000002 COY
0000 R 000015 CPKWH    0000 R 000011 CPV      0006 000000 DUM      0000 R 000005 EDE      0004 I 000000 IMPL
0000 000313 INJPS      0000 I 000006 IVDE      0000 I 000001 LLE      0000 R 000012 PCD      0000 R 000014 PCS
0000 R 000013 PCU      0003 R 000010 SPD      0003 R 000004 TDE      0005 R 000000 TIME      0003 R 000005 TLD
0006 R 000007 TMAX      0000 R 000000 TMAX1      0000 R 000004 TOY      0000 R 000007 TOYN      0003 R 000007 UTD
0003 R 000006 UTV      0003 R 000003 VDE      0000 R 000010 VDEN

```

```

00100 1* COST 000000
00101 2* SUBROUTINE CM(DUMM,FCR,LE) 000000
00101 3* C 000000
00101 4* C PURPOSE SUMMARIZE WIND ENERGE STORAGE COSTS AND LEVELIZED 000000
00101 5* C ENERGY COSTS PER KWH. 000000
00101 6* C 000000
00101 7* C WRITTEN BY A.W. WARREN VERSION 1, MAY 1977 000000
00101 8* C 000000
00101 9* C INPUT PARAMETERS 000000
00101 10* C 000000
00101 11* C FCR - FIXED CHARGE RATE FACTOR INCLUDING DEPRECIATION, 000000
00101 12* C MONEY COST, INSURANCE, AND TAXES, PER YEAR 000000
00101 13* C LE - SYSTEM LIFE EXPECTANCY , YEARS 000000
00101 14* C TMAX - SIMULATION TIME, HR 000000
00101 15* C CC - TOTAL YEARLY CAPITAL COSTS, $ 000000
00101 16* C CM - TOTAL YEARLY MAINTENANCE COSTS, $ 000000
00101 17* C CO - TOTAL OPERATING AND FUEL COSTS OVER TMAX, $ 000000
00101 18* C CDE - VALUE OF ENERGY DELIVERED OVER TMAX, $ 000000
00101 19* C TDE - TOTAL ENERGY DELIVERED OVER TMAX, KWH 000000
00101 20* C TLD - TOTAL LOAD DEMAND OVER TMAX, KWH 000000

```

CM

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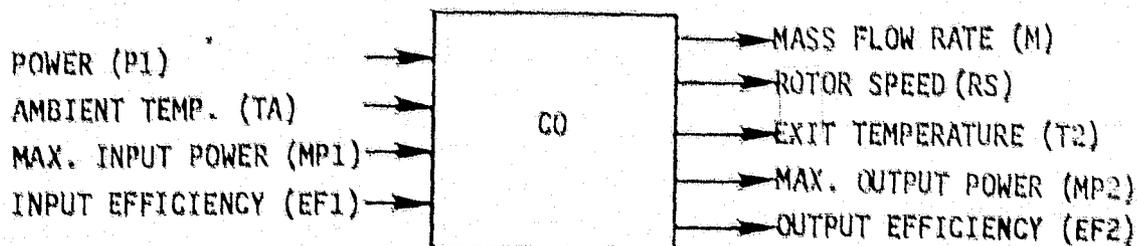
00101 21* C          UTV - VALUE OF UTILITY ENERGY SUPPLIED LESS SURPLUS VALUE, $      000000
00101 22* C          UTD - TOTAL UTILITY ENERGY DELIVERED, KWH                      000000
00101 23* C          SPD - TOTAL SURPLUS ENERGY SUPPLIED TO UTILITY, $            000000
00101 24* C
00103 25*          COMMON /COST/ CC, CMA, CO, VDE, TDE, TLD, UTV, UTD, SPD          000000
00104 26*          COMMON /CIMPL/IM-L /CTIME/ TIME /CSIMUL/ DUM(7), TMAX          000000
00105 27*          REAL LE
00105 28* C          INITIALIZATION
00105 29* C
00106 30*          IF (IMPL.GT.0) GO TO 100
00110 31*          DUM=0.0
00111 32*          CC = 0.
00112 33*          CMA = 0.
00113 34*          CO = 0.
00114 35*          VDE = 0.
00115 36*          TDE = 0.
00116 37*          TLD = 0.
00117 38*          UTV = 0.
00120 39*          UTD = 0.
00121 40*          SPD = 0.
00122 41*          TMAX1 = TMAX*.99999
00122 42* C
00123 43* 100 IF (TIME.LT.TMAX1) RETURN
00125 44*          IF (IMPL.LE.1) RETURN
00125 45* C
00125 46* C          COST SUMMARY OUTPUT
00125 47* C
00127 48*          LLE = LE
00130 49*          WRITE(6,200) LLE
00133 50* 200 FORMAT(1H1,35X,33H WIND ENERGY STORAGE COST SUMMARY // 1H ,40X,I2,
00133 51*          1 17H YEAR LIFE CYCLE )
00133 52* C
00134 53*          COY = CO*8760./TMAX
00135 54*          CCY = CC*LE*FCR*.01
00136 55*          TOY = COY + CMA + CCY
00137 56*          WRITE(6,300) CCY, CMA, COY, TOY
00145 57* 300 FORMAT(//// 30X,22HD YEARLY SYSTEM COSTS / 1H+,29X,1H+ / 1H-,42X,
00145 58*          1 12HCAPITAL COST,12X,F8.0,2H $ / 1H ,42X, 17H(INCLUDING FIXED ,
00145 59*          2 8HCARGES) / 1HD,42X,16HFIXED 0 + H COST, 8X,F8.0,2H $ / 1HD ,
00145 60*          3 42X,21HOPERATING + FUEL COST, 3X,F8.0,2H $ / 1HD,42X,5HTOTAL,
00145 61*          4 19X,F8.0,2H $ )
00145 62* C
00146 63*          EDE = TDE * 8760./TMAX
00147 64*          IVDE = VDE * 8760./TMAX
00150 65*          TOYN = TOY*1000./ EDE
00151 66*          VDEN = VDE*1000./ TDE
00152 67*          CPV = TOYN / VDEN
00152 68* C
00153 69*          WRITE(6,400) EDE, TOYN, IVDE, VDEN, CPV
00162 70* 400 FORMAT(//// 30X,26HD ENERGY DELIVERED / 1H+,29X,1H+ / 1H-,
00162 71*          1 42X,16HENERGY DELIVERED, 7X,F9.0,4H KWH / 1HD,33X,50(1H*) /
00162 72*          1 1H ,33X,1H*,42X,1H* /
00162 73*          2 1H ,33X,1H*, 8X,19HENERGY COST PER KWH, 7X,F6.1,9H PILLS * /
00162 74*          2 1H ,33X,1H*,42X,1H* / 1H ,
00162 75*          3 33X,10(15H****) / 1HD,42X,25HVALUE OF ENERGY DELIVERED,17,
00162 76*          4 2H $ / 1H ,42X,22H(IVALUE OF FUEL SAVED) / 1HD,42X,20HENERGY VALUE
00162 77*          5 PER KWH, 6X,F6.1,6H PILLS / 1HD,42X,24HCOST PER VALUE DELIVERED,

```



CC162	78*	6 ZX,F6.2}	CC0144
CC162	79*	C	CC0144
CC163	81*	PCD= (TDE-SPD)*100./TLD	CC0144
CC164	81*	PCU= UTD*100./TLD	CC0150
CC165	82*	PCS= SPD*100./TLD	CC0154
CC166	83*	CPKWH= (TOYH*(TDE-SPD) + UTV*1000.)/TLD	CC0160
CC167	84*	WRITE(6,500)PCD ,PCU,PCS,CPKWH	CC0167
CC175	85*	500 FORMAT(//// 30X,31H0 LOAD FACTOR / 1H+,29X,	CC0200
CC175	86*	1 1H+ / 1H-,42X,	CC0200
CC175	87*	1 26HPERCENT OF LOAD SUPPLIED , F6.1, 2H / 1H ,42X,22HBY TOTAL WIN	CC0200
CC175	88*	2ND SYSTEM / 1H0,42X,24HPERCENT OF LOAD SUPPLIED,2X,F6.1 /	CC0200
CC175	89*	2 1H ,41X,11H BY UTILITY /	CC0200
CC175	90*	3 1H0,42X,26HPERCENT OF WIND ENERGY , F6.1 /	CC0200
CC175	91*	3 1H ,42X,9HSURPLUSED /	CC0200
CC175	92*	4 1H0,42X,23HCOST TO MEET LOAD , 3X,F6.1,6H MILLS/	CC0200
CC175	93*	5 1H ,42X,27H(WIND + UTILITY) / 1H1	CC0200
CC175	94*	C	CC0200
CC176	95*	RETURN	CC0200
CC177	96*	END	CC0225

## 7.6 COMPRESSOR (PNEUMATIC)



The compressor model represents the off-design performance of a typical axial flow compressor. The compressor is assumed designed for a specified set of design operating conditions and performance requirements. The mass flow rate is assumed directly proportional to angular velocity and independent of the pressure ratio across the compressor. This is expected to hold for  $\pm 15\%$  of the design mass flow rate. The polytropic efficiency of the compressor is assumed to be a weak function of the angular velocity. Initial calculations are made with the design polytropic efficiency, and refinements made after the off-design parameters are calculated.

### Basic Equations

The expression for the angular velocity is

$$RS = P1 * \frac{RSD}{MD} \frac{EFF}{CP * (TA + 460) * [(PR2/PA)^{A*NP} - 1]}$$

where:

$$EFF = ((PR2/PA)^{A*NP} - 1) / ((PR2/PA)^A - 1)$$

$$A = (GAM - 1) / GAM * NP$$

Inputs

<u>Parameter/Port</u>		<u>Description</u>	<u>Units</u>
P	1	Input power	kw
RSD		Design angular velocity (D = 3600)	rpm
MD		Design mass flow rate (D = 3000)	lb/h
CP		Heat capacity of air (D = $7.2 \times 10^{-5}$ )	kwh/lb <sup>o</sup> F
TA		Inlet air temperature (ambient) (D = 70)	°F
PR	2	Exit pressure (D = 147)	psi
PA		Inlet pressure (ambient) (D = 14.7)	psi
GAM		Heat capacity ratio (D = 1.4)	-
EF	1	Input product efficiency	-
MP	1	Maximum input power	kw
NPD		Design polytropic efficiency (D = 0.88)	-
PID		Design inlet pressure (ambient) (D = 14.7)	psi
P00		Design outlet pressure (D = 147)	psi
TID		Design inlet air temp (ambient) (D = 70)	°F
CK		Compressor capacity cost coefficient <sup>1</sup> (D = 1.0)	-
F0		Compressor exponent for cost calculations (D = 0.75)	-

Outputs

<u>Variable/Port</u>			
NP		Polytropic efficiency	-
EF	2	Output product efficiency	-
MP	2	Maximum output power	kw
T0		Torque	ft-lb
M		Mass flow rate	lb/h
T	2	Exit temperature	°F
RS		Angular velocity	rpm
CC0		Cost of compressor/year	\$

<sup>1</sup> CK = capital cost (known unit)/(design point mass flow rate)<sup>F0</sup> \*  
LN (outlet/inlet pressure ratio)\*(life expectancy of unit)

D - Default values supplied

<u>Statistics</u>	<u>Description</u>	<u>Units</u>
MT	Maximum temperature	°F
MF	Maximum mass flow rate	lb/h

The calculation sequence and the default values are based on the assumption of an axial flow compressor, nominally rated at 125kw, and a pressure ratio of 10. The equations used relate first order effects among the various physical quantities and were derived from first principles originally to support the research work of Reference 1. Cost scaling was also developed in that reference based on cost estimates obtained from turbomachinery manufacturers.

#### Calculation Sequence

##### 1) Costs (First pass only)

$$CCO = CK * (MD) * F0 * LN \left( \frac{P0D}{PID} \right)$$

If  $P1 > 0$  go to 2)

$$A = (GAM - 1) / (GAM * NPD)$$

$$RAT = (P0D / PID) * A$$

$$EFF = 1, RS = 0, \text{ go to 3)}$$

- 
1. "Closed Cycle High Temperature Central Receiver Concept for Solar Electric Power," BEC/EPRI RP 377-1, June 1976.

Calculation Sequence Cont.

## 2) Angular velocity iteration

$$A = (GAM-1)/(GAM*NP) \quad (\text{Initially } NP = NPD)$$

$$RAT = (PR2/PA)**A$$

$$EFF = (RAT**NP-1)/(RAT-1)$$

$$\frac{RS}{RSD} = \frac{P1}{MD \cdot CP \cdot (TA+460)} \cdot \frac{EFF}{(RAT-1)}$$

Polytropic efficiency

$$NP = 1 - (1 - NPD) \cdot \left[ 2.0 - \left( \frac{PID \cdot (TA+460) \cdot RSD}{PA \cdot (TID+460) \cdot RS} \right)^{0.2} \right]$$

Iterate until NP and RS are consistent

(If iteration doesn't converge, then write DIAGNOSTIC and exit)

## 3) Mass flow rate

$$M = MD \cdot RS / RSD$$

## 4) Exit temperature

$$T2 = (TA+460) \cdot RAT - 460$$

## 5) Torque

If  $P1 \leq 0$ , set  $T0 = 0$  and go to 6)

$$T0 = P1 \cdot 737.6 / (RS \cdot 2\pi / 60)$$

## 6) Efficiency and maximum power

$$EF2 = EF1 \cdot EFF$$

$$MP2 = \text{MIN}(MP1 \cdot EFF, 1.5 \cdot MD \cdot CP \cdot (T2 - TA))$$

## 7) Compute Statistics and Costs

SUBROUTINE CO ENTRY POINT 000420

STORAGE USED CODE(1) 000613; DATA(0) 000066; BLANK COMMON(2) 000000

## COMMON BLOCKS

```

0003 CIMPL 000001
0004 CTIME 000001
0005 CSTMUL 000010
0006 COST 000001

```

## EXTERNAL REFERENCES (BLOCK, NAME)

```

0007 XPRR
0010 ALOG
0011 NWDUS
0012 N102S
0013 NSTOPS
0014 NERR3S

```

## STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

```

0001 000136 100L 0001 000375 1000L 0000 000010 101CF 0001 000166 200L 0001 000271 300L
0001 000315 400L 0000 R 000005 A 0006 R 000000 CC1 0005 000000 DUM 0000 R 000003 EFF
0003 I 000000 IMPL 0000 000052 INJPS 0000 I 000002 ISP 0000 R 000000 PI 0000 R 000004 RAT
0000 R 000006 RSNO 0004 R 000000 TIME 0005 R 000007 THAX 0000 R 000001 THAX1 0000 R 000007 XNP

```

```

00100 1* CCO 000000
00101 2* SUBROUTINE COINP,EF2,MP2,TO,M,T2,RS,CC,MT,MF,P1,RSD,MD,CP,TA,PR2, 000000
00101 3* I PR1,GAM,EF1,MP1,NPD,PID,POD,TID,CK,FO) 000000
00101 4* C 000000
00101 5* C PURPOSE PERFORMANCE MODEL OF AXIAL FLOW COMPRESSOR 000000
00101 6* C 000000
00101 7* C METHOD COMPRESSOR IS SIZED FROM INPUT OPERATING REQUIREMENTS. 000000
00101 8* C 000000
00101 9* C MASS FLOW IS ASSUMED PROPORTIONAL TO ANGULAR VELOCITY 000000
00101 10* C 000000
00101 11* C AND INDEPENDENT OF PRESSURE RATIO. 000000
00101 12* C 000000
00101 13* C WRITTEN BY F.O. MAHONY VERSION 1, MARCH 22 1977 000000
00101 14* C 000000
00101 15* C CALL SEQUENCE 000000
00101 16* C OUTPUTS 000000
00101 17* C NP - POLYTROPIC EFFICIENCY 000000
00101 18* C EF2 - OUTPUT PRODUCT EFFICIENCY 000000
00101 19* C MP2 - MAXIMUM OUTPUT POWER, KW 000000
00101 20* C TO - TORQUE, FT-LB 000000

```

ORIGINAL PAGE IS  
OF POOR QUALITY

GO



```

00152 78* C AND ANGULAR VELOCITY 000136
00152 79* C 000136
00153 80* C ISP = 0 000136
00153 81* C 000136
00154 82* C EFF=1.0 000136
00155 83* C IF(P1.GT.0.0)60 TO 200 000140
00155 84* C 000140
00157 85* C RAT= (POD/PID)**{(GAM-1.0)/(GAM+NP)} 000143
00160 86* C TO =0.0 000160
00161 87* C RS=0.0 000161
00162 88* C NP=NP0 000162
00163 89* C GO TO 300 000164
00163 90* C 000164
00164 91* C 200 A = (GAM-1.0)/(GAM+NP) 000166
00165 92* C RAT= (PR2/PPI)**A 000173
00166 93* C EFF=(RAT**NP - 1.)/(RAT - 1.) 000203
00166 94* C 000203
00167 95* C RSNO = EFF*P1/ND*1.0/CP/(TA+460.0)/(RAT-1.0) 000214
00167 96* C 000214
00170 97* C XNP = NP 000224
00170 98* C 000224
00171 99* C NP = 1.0-(1.0-NP)*(2.0-(PID/PRI*(TA+460.0)/(TID+460.0)/RSNO) 000226
00171 100* C 1 **0.2) 000226
00171 101* C 000226
00172 102* C IF(ISP.GT.10) GO TO 1000 000250
00172 103* C 000250
00174 104* C ISP = ISP+1 000254
00174 105* C 000254
00175 106* C IF(ABS((NP-XNP)/NP).GT.0.001) GO TO 200 000257
00177 107* C RS= RSD*RSNO 000265
00177 108* C 000265
00177 109* C MASS FLOW RATE 000265
00177 110* C 000265
00200 111* C 300 M = MD*RS/RSD 000271
00200 112* C 000271
00200 113* C EXIT TEMPERATURE 000271
00200 114* C 000271
00201 115* C T2 = (TA+460.0)*RAT-460.0 000274
00202 116* C IF(P1.LE.0.0)60 TO 400 000301
00202 117* C 000301
00202 118* C TORQUE 000301
00202 119* C 000301
00204 120* C TO = P1*737.6/(RS*2.0*PI/60.0) 000304
00204 121* C 000304
00204 122* C EFFICIENCY AND MAXIMUM POWER 000304
00204 123* C 000304
00204 124* C 000304
00204 125* C 000304
00205 126* C 400 EF2 = EF1*EFF 000315
00205 127* C 000315
00206 128* C MP2 = AMIN1(MP1*EFF,1.5*MD*CP*(T2-TA)) 000317
00206 129* C STATISTICS AND COST SUMMATION 000317
00206 130* C 000317
00207 131* C IF (IMPL.LE.1) RETURN 000334
00211 132* C MT = AMAX1(MT, T2) 000343
00212 133* C MF = AMAX1(MF, M) 000351
00213 134* C IF(TIME.LT.TMAX1) RETURN 000357

```

```

00215 135*      CCI = CCI + CC
00215 136*      C
00216 137*      RETURN
00216 138*      C
00217 139*      1000 WRITE (6,1010) NP,XNP,RS
00224 140*      1010 FORMAT (1H0,40HMAX ITERATIONS FOR COMPRESSOR EFFICIENCY,
00224 141*      1      15H - NP,XNP,RS = ,3F12.6)
00225 142*      STOP
00226 143*      END

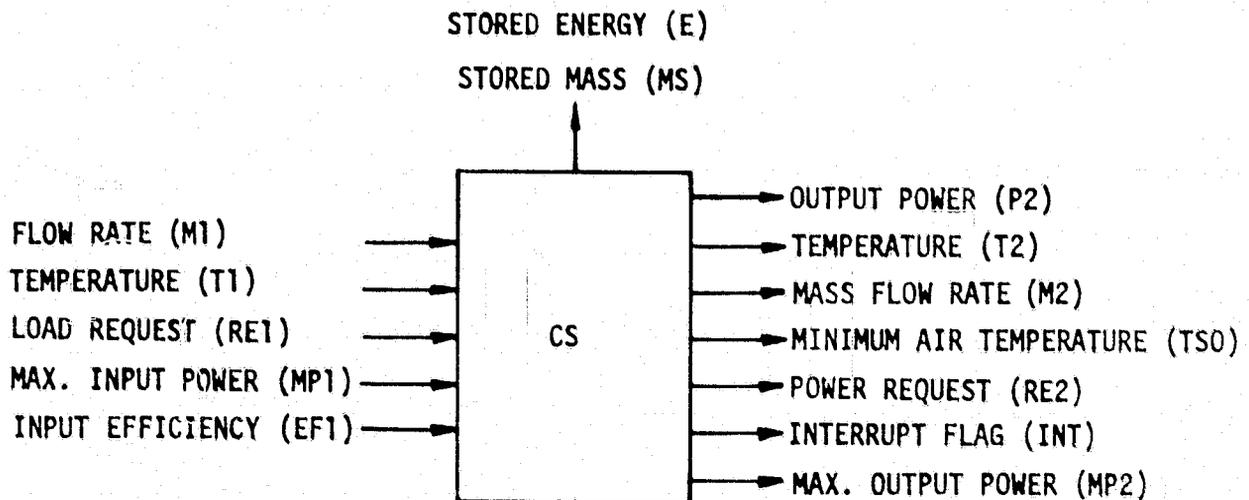
```

```

000366
000366
000371
000371
000375
000404
000404
000404
000404
000612

```

## 7.7 PNEUMATIC STORAGE VESSEL (CONSTANT PRESSURE)



The pneumatic storage vessel is based on a constant pressure underground cavern design as represented in Figure 7.7. A surface pressure-compensation pond via a water shaft is assumed to maintain the vessel pressure at a constant value. This model is assumed to be used in conjunction with a heat exchanger. The energy is calculated as a function of the stored gas mass, the inlet/storage air temperature, and a leakage function proportional to the stored energy.

### Basic Equation

The rate of energy storage is computed from the equation

$$\dot{E} = M_1 * CP * (T_1 - T_0) - NU * E, \text{ charging}$$

$$\dot{E} = -M_2 * CP * (T_2 - T_0) - NU * E, \text{ discharging}$$

where  $M_1$  = mass flow rate during charge

$M_2$  = mass flow rate during discharge

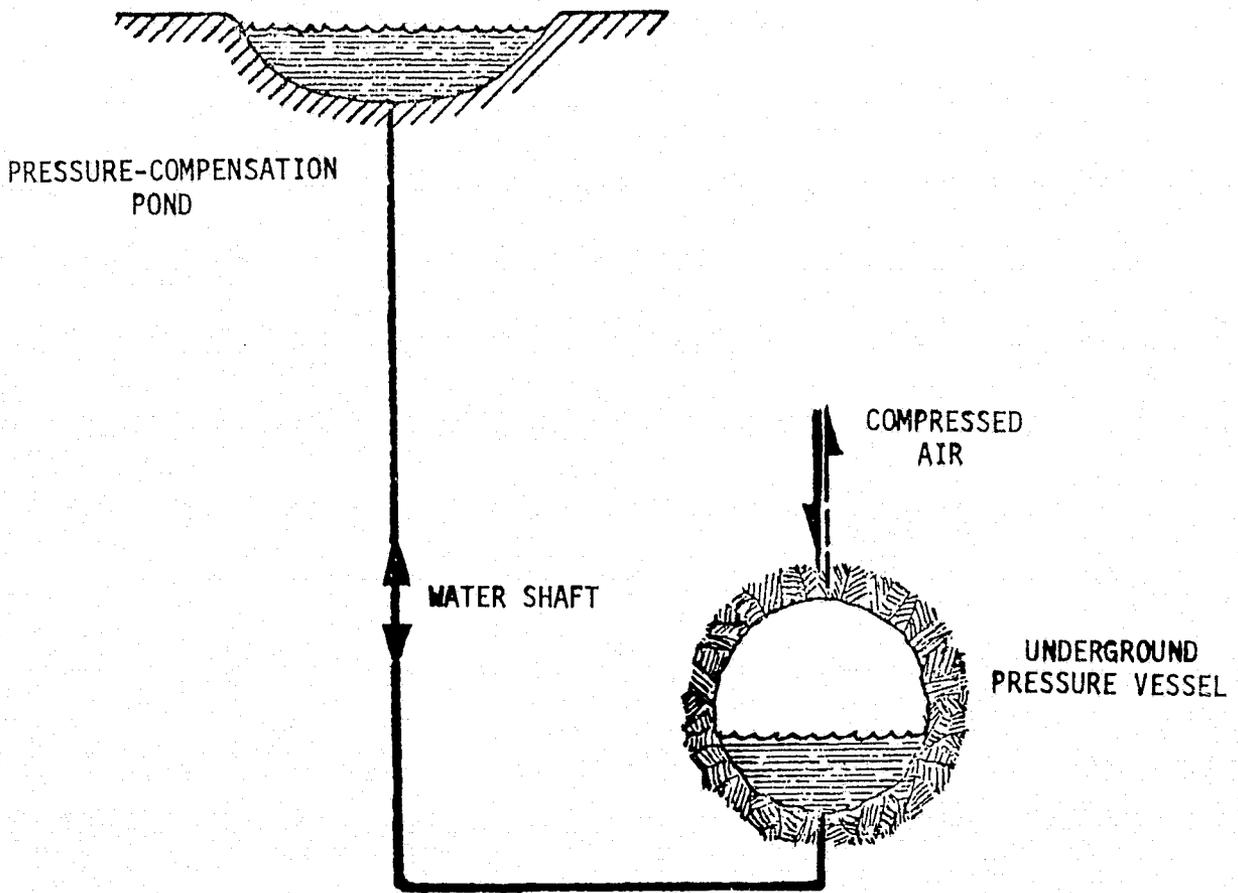


FIGURE 7.7 CONSTANT PRESSURE AIR STORAGE

## Inputs

<u>Parameter/Port</u>	<u>Description</u>	<u>Units</u>
M 1	Inlet air mass flow rate	lb/h
CP	Air heat capacity (D = $7.2 \times 10^{-5}$ )	kwh/lb <sup>o</sup> F
T 1	Inlet air temperature	oF
T0	Minimum air temperature (D = 60)	oF
NU	Leakage coefficient (D = 0.0008)	h <sup>-1</sup>
R	Gas constant (D = $2.009 \times 10^{-5}$ )	kwh/lb
VM	Maximum storage capacity (D = $1.2 \times 10^6$ )	ft <sup>3</sup>
PR 1	Vessel pressure (D = 147)	psi
LE	Life expectancy of vessel	years
CV	Vessel capacity cost (D = 0.22)	\$/ft <sup>3</sup>
RE 1	Load request	kw
EF 1	Input product efficiency	-
MP 1	Input maximum power	kw
MDE	Mass threshold for priority resequencing	lb
MD	Maximum charge or discharge mass flow rate	lb
TM	Maximum allowable air temperature (D = 120)	oF
TEM	Maximum allowable inlet temperature	oF
CM	Maintenance cost/year	\$

## Outputs

<u>Variable/Port</u>	<u>Description</u>	<u>Units</u>
E	Stored energy (state)	kwh
M 2	Outlet mass flowrate	lb/hr
T 2	Storage temperature	oF
V	Storage volume	ft <sup>3</sup>
CC0	Cost of vessel/year	\$
MS	Mass of air in storage (state)	lb
MP 2	Maximum output power	kw
RE 2	Maximum charging rate	kw
INT	Interrupt priority flag	-
TS0	Minimum air temperature (=T0)	oF

D - Default values supplied

Outputs Cont.

Variable/Port

PR	2	Vessel pressure (=PR1)	psi
P	2	Output power (discharge)	kw
MDM		Maximum allowable mass flow rate (=MD)	

Statistics

EU		Maximum stored energy	kwh
VU		Maximum storage volume	ft <sup>3</sup>

The pneumatic storage vessel calculation sequence and default values assume a 10atm cavern approximately 340 ft. below ground and sized for storage of 120kw for 24 hours. A maximum cavern wall temperature of 120°F is assumed. Cost estimates for the vessel were estimated from the results of Reference 1, with cost scaling by .05 to account for plant size differences.

- 
1. "Preliminary Feasibility Evaluation of Compressed Air Storage Power Systems," United Technologies AER 74-00242, December 1976.

## Calculation Sequence

TINC = integration step size, hr

C1 = conversion constant =  $5.43 \times 10^{-5}$

$\frac{\text{kwh/ft}^3}{\text{psi}}$

1) Vessel Cost

$$CC0 = CV * VM / LE$$

2) Storage temperature

$$T2 = \frac{E}{CP * MS} + T0$$

3) Storage volume

$$V = MS * \frac{R * (T2 + 460)}{PR1 * C1}$$

4) Maximum Mass and charging rate

$$MSM = VM * \frac{(PR1 * C1)}{R * (T2 + 460)}$$

$$MD1 = \text{MIN}(MDM, (MSM - MS) / TINC)$$

$$RE2 = \min \left\{ MP1, MD1 * CP * (TEM - T0) \right\} / EF1$$

5) Mass flow out (discharge mode)

$$M2 = \frac{RE1}{CP * (T2 - T0)}$$

$$P2 = RE1$$

6) Maximum discharge rate

$$MD = \text{MIN}(MDM, (MS - MDE) / TINC)$$

$$MP2 = CP * (T2 - T0) * MD$$

Calculation Sequence Cont.

7) Stored energy rate

$$\dot{E} = CP*(T1-T0)*M1 - NU*E - RE1$$

8) Stored mass rate

$$\dot{MS} = M1 - M2$$

9) Priority interrupt

If  $MS \leq MDE$ ,  $INT = 1$ If  $MS > 2*MDE$  and  $INT = 1$ ,  $INT = 0$ If  $MS \geq MSM$ ,  $INT = -1$ If  $MS < MSM - MDE$  and  $INT = -1$ ,  $INT = 0$ If  $T2 > TM$  write diagnostic and set  $INT = -1$ If  $MS < MDE$  or  $MS > MSM$  write diagnostic

10) Compute Statistics and Costs



00101	24*	C	T2 - STORAGE TEMPERATURE, DEG F	00000C
00101	25*	C	V - STORAGE VOLUME, FT**3	000000
00101	26*	C	CC - COST OF VESSEL/YEAP, \$	000000
00101	27*	C	MP2 - MAXIMUM OUTPUT POWER, KW	000000
00101	28*	C	RE2 - MAXIMUM CHARGING RATE, KW	000000
00101	29*	C	INT - INTERRUPT PRIORITY FLAG	000000
00101	30*	C	TSD - MINIMUM AIR TEMPERATURE, DEG F	000000
00101	31*	C	PR2 - VESSEL PRESSURE, PSI	000000
00101	32*	C	P - OUTPUT POWER (DISCHARGE), KW	000000
00101	33*	C	MDM - MAXIMUM ALLOWABLE MASS FLOW RATE, LB/HR	000000
00101	34*	C	EU - MAXIMUM STORED ENERGY, KWH	000000
00101	35*	C	VU - MAXIMUM STORAGE VOLUME, FT**3	000000
00101	36*	C		000000
00101	37*	C	INPUTS	000000
00101	38*	C	M1 - INLET AIR MASS FLOW RATE, LB/HR	000000
00101	39*	C	CP - AIR HEAT CAPACITY, KWH/LB-DEG F	000000
00101	40*	C	T - INLET AIR TEMPERATURE, DEG F	000000
00101	41*	C	TO - MINIMUM AIR TEMPERATURE, DEG F	000000
00101	42*	C	R - GAS CONSTANT, KWH/LB-DEG R	000000
00101	43*	C	VM - MAXIMUM STORAGE CAPACITY, FT**3	000000
00101	44*	C	PR1 - VESSEL PRESSURE, PSI	000000
00101	45*	C	LE - LIFE EXPECTANCY OF VESSEL, YEARS	000000
00101	46*	C	NU - LEAKAGE COEFFICIENT, 1/HR	000000
00101	47*	C	CV - VESSEL CAPACITY COST, \$/FT**3	000000
00101	48*	C	RE1 - LOAD REQUEST, KW	000000
00101	49*	C	EF1 - INPUT PRODUCT EFFICIENCY	000000
00101	50*	C	MP1 - INPUT MAXIMUM POWER, KW	000000
00101	51*	C	MDE - RESERVOIR THRESHOLD MASS FOR PRIORITY	000000
00101	52*	C	RESEQUENCING, LB	000000
00101	53*	C	MD - MAXIMUM CHARGE / DISCHARGE MASS FLOW RATE, LB/HR	000000
00101	54*	C	TM - MAXIMUM ALLOWABLE STORAGE TEMPERATURE, DEG F	000000
00101	55*	C	TEM - MAXIMUM ALLOWABLE INLET TEMPERATURE, DEG F	000000
00101	56*	C	CM - MAINTENANCE COST / YEAR, \$	000000
00101	57*	C		000000
00101	58*	C		000000
00103	59*		COMMON /CIMPL/IMPL,ICNT/CTIME/ TIME /CSIMUL/DUM(7),TMAX	000000
00104	60*		COMMON /COST/ CCI,CMI	000000
00105	61*		REAL NU,MS,MP2,INT,MDM,M1,LE,MP1,MDE,MD,M2,MSH,MD1	000000
00105	62*	C		000000
00105	63*	C		000000
00106	64*		IF(IMPL.GT.0) GO TO 100	000000
00106	65*	C		000000
00110	66*		IF(CP.EQ..99999) CP = 72.0E-6	000002
00112	67*		IF(TM.EQ..99999) TM= 120.0	000007
00114	68*		IF(TO.EQ..99999) TO = 60.0	000014
00116	69*		IF(NU.EQ..99999) NU = 0.0008	000021
00120	70*		IF(R.EQ..99999) R = 2.009E-5	000026
00122	71*		IF(VM.EQ..99999) VM = 1.2E+6	000033
00124	72*		IF(PR1.EQ..99999) PR1 = 147.0	000040
00126	73*		IF(CV.EQ..99999) CV = 0.22	000045
00130	74*		RE1=0.0	000052
00130	75*	C		000052
00131	76*		TMAX1 = TMAX*0.99999	000053
00132	77*		TSD=TO	000056
00132	78*	C		000056
00133	79*		CC = CV*VM/LE	000060
00134	80*		C1 = 5.43E-5	000064

```

00134 81* C
00135 82* INT = 0.
00136 83* PR2=PR1
00137 84* EU= 0.
00140 85* VU= 0.
00141 86* 1CD CONTINUE
00141 87* C
00141 88* C
00141 89* C
00141 90* C
00141 91* C
00142 92* T2 = E/CP/MS+T0
00142 93* C
00142 94* C
00142 95* C
00143 96* V = MS*R*(T2+460.0)/PR1/C1
00143 97* C
00143 98* C
00143 99* C
00144 100* MSM = VM*PR1*C1/R/(T2+460.0)
00145 101* MDM=MD
00146 102* MD1= AMIN1(MDM,AMAX1(0.,(MSM-MS)/DUM(7)))
00147 103* RE2 = AMIN1(MP1,MD1*CP*(TEM-T0))/EF1
00147 104* C
00147 105* C
00147 106* C
00150 107* M2 = RE1/CP/(T2-T0)
00151 108* P = RE1
00151 109* C
00151 110* C
00151 111* C
00152 112* MDM= AMIN1(MDM,AMAX1(0.,(MS-MDE)/DUM(7)))
00153 113* MP2 = CP*(T2-T0)*MDM
00153 114* C
00153 115* C
00153 116* C
00154 117* IF(IE.NE.0) DE=CP*(T-T0)*M1 - NU*E -RE1
00154 118* C
00154 119* C
00154 120* C
00156 121* IF(IMS.NE.0) DMS=M1-M2
00156 122* C
00156 123* C
00160 124* IF(IMS.LE. MDE) INT=1.
00162 125* IF(IMS.GT. 2.*MDE .AND. INT.EQ.1.) INT=0.
00164 126* IF(IMS.GE.MSM) INT = -1.
00166 127* IF(IMS.LT. MSM-MDE .AND. INT.EQ.-1.) INT=0.
00170 128* IF(T2.GT. TM) INT= -1.
00170 129* C
00172 130* IF(IMPL.LE.1) RETURN
00174 131* IF(IMPL.GT.2)GO TO 200
00176 132* IF(T2.LT.TM) GO TO 10
00200 133* WRITE(6,1000) T2,TM
00204 134* ICNT=ICNT+1
00205 135* 10 IF(IMS.GT.MDE) GO TO 20
00207 136* WRITE(6,1010)MS,MDE
00213 137* ICNT=ICNT+1

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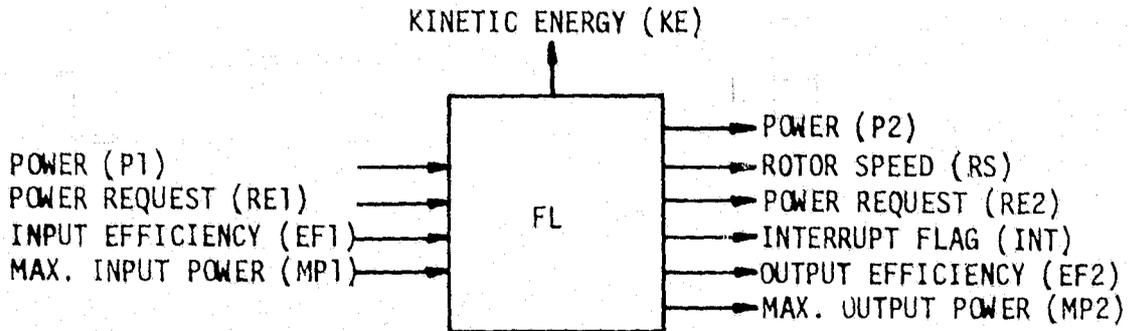
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00214	138*	20	IF(MS.LT.MSM) GO TO 200	000344
00216	139*		WRITE(6,1020) MS,MSH	000347
00222	140*		ICNT=ICNT+1	000356
00222	141*	C		000356
00222	142*	C	STATISTICS	000356
00222	143*	C		000356
00223	144*	200	EU = AMAX1(EU,E)	000362
00224	145*		VU = AMAX1(VU,V)	000367
00224	146*	C		000367
00225	147*		IF(TIME.LT.TMAX1) RETURN	000375
00227	148*		CCI = CCI+CC	000404
00230	149*		CHI=CHI+CH	000407
00230	150*	C		000407
00231	151*		RETURN	000412
00232	152*	1000	FORMAT(1H0,23HCS STORAGE TEMPERATURE,F12.3,18HGREATER THAN ALLOW,	000636
00232	153*		1 5HABLE , F12.3)	000636
00233	154*	1010	FORMAT(1H0,25HCS MASS OF AIR IN STORAGE,F12.3,	000636
00233	155*		1 26H BELOW MINIMUM ALLOWABLE,F12.3)	000636
00234	156*	1020	FORMAT(1H0,25HCS MASS OF AIR IN STORAGE,F12.3,	000636
00234	157*		1 28H EXCEEDS MAXIMUM ALLOWABLE,F12.3)	000636
00235	158*		END	000636

7.8 FLYWHEEL/CLUTCH



The flywheel model is a first order differential equation for kinetic energy which is driven by input power when charging and by a load request when discharging. Power losses include clutch losses versus shaft speed and torque, windage losses, and friction losses due to bearing and seals. Shaft speed is determined analytically from kinetic energy. Priority interrupt logic is activated if minimum or maximum capacity levels are reached.

Basic Equations

$$KE = k * \omega^2$$

$$\dot{KE} = P_{IN} - P_{OUT} - C_1 * \omega - C_2 * \omega^{2.8},$$

where  $k, C_1, C_2$  are flywheel constants

$\omega$  = rotor speed in rad/sec

$P_{IN}$  = input power - clutch losses

$P_{OUT}$  = output load request

<u>Tables</u>	<u>Description</u>	<u>Units</u>
CL0	Clutch losses versus rotor speed (rpm) and torque (ft-lb), when engaged (Table dimension = 90)	kw
CL1	Clutch losses versus rotor speed (rpm) when disengaged (Table dimension = 17)	kw

### Inputs

#### Parameter/Port

PR		Pressure in vacuum housing	psi
HM		Moment of inertia <sup>1</sup>	slug-ft <sup>2</sup>
RF		Radius of flywheel	ft
SR		Shaft radius	ft
WT		Flywheel weight	lb
KF		Coefficient of friction	-
ZE		Width of flywheel at tip	ft
C2		Windage loss coefficient (analytic default)	-
P	1	Input power	kw
EF	1	Input product efficiency	-
MP	1	Input maximum charging rate	kw
RAP		Rated power, charge or discharge	kw
RE	1	Discharge load request	kw
E0		Minimum allowable storage capacity	kwh
E1		Maximum allowable storage capacity	kwh
EDE		Energy deadband for priority resequencing	kwh
CM		Maintenance cost/year	\$
CC		Capital cost/year	\$

### Outputs

#### Variable/Port

RS		Rotor speed	rpm
KE		Kinetic energy (state)	kwh

<sup>1</sup> Includes physical drive system.

## Outputs Cont.

<u>Variable/Port</u>	<u>Description</u>	<u>Units</u>
T0	Input torque (charging)	ft-lb
T1	Output torque (discharging)	ft-lb
P 2	Output power	kw
PL0	Clutch losses (charging)	kw
PL1	Clutch losses (discharging)	kw
EF 2	Output efficiency	-
MP 2	Maximum output power	kw
INT	Priority Interrupt flag	-
RE 2	Maximum charging power request	kw

## Statistics

ME	Maximum stored energy	kwh
MPC	Maximum charge rate	kw
MPD	Maximum discharge rate	kw
SPC	Sum of charging energy	kwh
SPD	Sum of discharging energy	kwh

## Calculation Sequence

1) Compute flywheel constants

$$k = \frac{1}{2} * HW * 3.76616 * 10^{-7}$$

$$C_1 = KF * WT * SR * 1.3558 * 10^{-3}$$

$$C_2 = C_o * PR^{0.8} * RF^{4.6} * (1 + 2.3 * ZE / RF) \quad (\text{DEFAULT})$$

$$C_o = 1.0946 * 10^{-7}$$

If  $KE < E0$  or  $KE > E1$  write diagnostic

2) Compute rotor speed

$$\omega = \sqrt{KE/k}$$

$$RS = \omega * (60 / 2\pi)$$

$$P_{IN} = 0$$

3) Compute power losses and net power when charging

If  $P1 = 0$ , set  $T0 = PL0 = P_{IN} = 0$  and go to 4)

$$T0 = P1 * 737.6 / \omega$$

$$PL0 = CL0(RS, T0)$$

$$P_{IN} = P1 - PL0$$

If  $P_{IN} < 0$ , write diagnostic

4) Compute power losses and output power when discharging

If  $RE1 = 0$ , set  $T1 = PL1 = P2 = P_{OUT} = 0$  and go to 5)

$$T1 = RE1 * 737.6 / \omega$$

$$PL1 = CL0(RS, -T1)$$

## Calculation Sequence

4) Cont.

$$P_2 = RE_1 - PL_1$$

$$P_{OUT} = RE_1$$

If  $P_2 < 0$ , set  $P_2 = 0$ . and write diagnostic

5) Compute power losses when disengaged

If  $P_1 > 0$  or  $RE_1 > 0$ , go to 6)

$$P_{OUT} = CL_1(RS)$$

6) Flywheel kinetic energy rate

$$\dot{KE} = P_{IN} - P_{OUT} - C_1 * \omega - C_2 * \omega^{2.8}$$

7) Maximum Input (charging power)

$$TM = MP_1 * 737.6 / \omega$$

$$MP_0 = MP_1 - CL_0(RS, TM)$$

If  $MP_0 \leq 0$ , write diagnostic and go to 8)

$$EF_0 = EF_1 * MP_0 / MP_1$$

$$RE_2 = \text{MIN}(MP_0, RAP), (EI - KE) / TINC / EF_0$$

8) Output efficiency and maximum power

$$RAP_1 = \text{MIN}(RAP, (KE - E_0) / TINC), TINC = \text{integration step}$$

$$TM = RAP_1 * 737.6 / \omega$$

$$MP_2 = RAP_1 - CL_0(RS, -TM)$$

Calculation Sequence

8) Cont.

If  $MP2 < 0$  write diagnostic

$$EF2 = MP2/RAP1$$

If  $RE1 > 0$ ,  $EF2 = P2/RE1$

9) Priority interrupt logic

If  $KE \leq E0$  ,  $INT = 1$

If  $KE > E0 + EDE$  and  $INT=1$ ,  $INT=0$

If  $KE \geq E1$  ,  $INT = -1$

If  $KE < E1 - EDE$  and  $INT= -1$ ,  $INT=0$

10) Compute Statistics and Costs

SUBROUTINE FL ENTRY POINT 001125

STORAGE USED CODE(1) 001333; DATA(0) 000231; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CIMPL 000002
0004 CTIME 000001
0005 CSIMUL 000010
0006 COST 000002

EXTERNAL REFERENCES (BLOCK, NAME)

0007 TBLU2
0010 TBLU1
0011 XPRR
0012 NWDUS
0013 NI025
0014 SQRT
0015 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000060 10L 0000 000042 108F 0000 000026 109F 0001 000147 20L 0001 000315 200L
0000 000060 208F 0001 000412 300L 0000 000074 308F 0001 000440 400L 0001 000544 500L
0000 000110 508F 0001 000574 600L 0001 000705 700L 0000 000125 708F 0000 R 000005 AK
0000 R 000022 APC 0006 R 000000 CCI 0006 R 000001 CHI 0000 R 000006 C1 0005 R 000000 DUM
0000 R 000025 ECO 0000 R 000024 EC1 0000 R 000021 EFO 0003 I 000001 ICNT 0003 I 000000 IMPL
0000 S00166 INJPS 0000 I 000012 MN4 0000 R 000001 MPA 0000 R 000002 MPB 0006 R 000000 MPO
0000 I 000011 M4 0000 I 000013 MNR5 0000 I 000014 MNR54 0000 I 000007 NNRS 0000 I 000013 NNT
0000 R 000015 OMEGA 0000 R 000016 PIN 0000 R 000017 POUT 0000 R 000023 RAPT 0010 R 000000 TRLU1
0007 R 000000 TPLU2 0004 R 000000 TIME 0000 R 000003 TINC 0000 R 000020 TH 0005 R 000007 THAX
0000 R 000004 TMAX1

00100 1\* CFL
00101 2\* SUBROUTINE FL(CLO,CL1,RS,KE,KED,IKE,TO,T1,P2,PL0,PL1,EF2,MP2,INT,
00101 3\* 1 REZ,ME,MPC,MPD,SPC,SPD, PR,HM,RF,SR,WT,KF,ZE,C2,P1,EF1,MP1,RAP
00101 4\* 2 ,RE1,E0,F1,EDE,CM,CC)
00101 5\* C
00101 6\* C PURPOSE MODEL OF FLYWHEEL CAPABLE OF ABSORBING POWER
00101 7\* C AND OF DELIVERING POWER ON REQUEST
00101 8\* C
00101 9\* C METHOD OUTPUT POWER AND KINETIC ENERGY COMPUTED FROM
00103 10\* C
00103 11\* C POWER REQUEST AND INPUT POWER
00103 12\* C
00103 13\*

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00114 71* C
00115 72* MF=0.
00116 73* RE1=0.
00117 74* MPC=0.
00120 75* MPD=C.
00121 76* SPC=D.
00122 77* SPD=0.
00123 78* 10 CONTINUE
00124 79* AK=.5*HM*3.76616E-7
00125 80* C1=KF*WT*SR*1.3558E-3
00126 81* IF((KE.GT.E0).AND.(KE.LT.E1)).OR.(IMPL.NE.2)GO TO 20
00130 82* IF(KE.LE.E0)WRITE(6,108)KE,E0
00135 83* IF(KE.GE.E1)WRITE(6,109)KE,E1
00142 84* 109 FORMAT(1H0,26H FLYWHEEL KINETIC ENERGY ,F12.3,
00142 85* X 18H EXCEEDS CAPACITY ,F12.3)
00143 86* 108 FORMAT(1H0,24H FLYWHEEL KINETIC ENERGY,F12.3,
00143 87* X 33H FALLS BELOW MINIMUM REQUIREMENT ,F12.3)
00144 88* ICNT=ICNT+1
00145 89* 20 CONTINUE
00146 90* NNRS=CL0(2)
00147 91* NNT=CL0(3)
00150 92* M4=NNT*4
00151 93* MN4=M4*NNRS
00152 94* MNRS=CL1(2)
00153 95* NNNRS4=NNNRS*4
00154 96* T0=0.
00155 97* T1=0.
00156 98* P2=0.
00157 99* PLO=0.
00160 100* PL1=0.
00161 101* RE2=0.
00161 102* C
00161 103* C COMPUTE ROTOR SPEED
00161 104* C
00162 105* 100 OMEGA=1.E-6
00163 106* IF(KE.GT.C.)OMEGA=SQRT(KE/AK)
00165 107* RS= OMEGA*30./3.14159
00166 108* PIN=0.
00166 109* C
00166 110* C COMPUTE POWER LOSSES AND NET POWER WHEN CHARGING
00166 111* C
00167 112* IF(P1.EQ.0.)GO TO 200
00171 113* T0=P1*737.6/OMEGA
00172 114* PLO=TPLU2(RS,T0,CL0(M4),CL0(4),CL0(MN4),1,1,-NNRS,-NNT,MNRS,NNT)
00173 115* PIN=P1-PLO
00174 116* POUT=0.
00174 117* C
00175 118* IF(PIN.GE.0.)GO TO 200
00177 119* IF(IMPL.NE.2)GO TO 200
00201 120* WRITE(6,208)PLO,P1
00205 121* 208 FORMAT(1H0,21H FLYWHEEL POWER LOSS ,F12.3,
00205 122* X24H EXCEEDS CHARGING POWER ,F12.3)
00206 123* ICNT=ICNT+1
00206 124* C
00206 125* C COMPUTE POWER LOSSES AND OUTPUT POWER WHEN DISCHARGING
00206 126* C
00207 127* 200 IF(RE1.EQ.0.)GO TO 300

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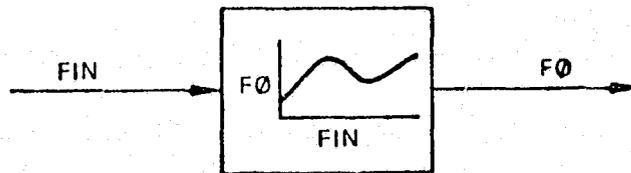
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00277	185*			000715
00277	186*	C	PRIORITY INTERRUPT	000715
00277	187*	C		000715
00301	188*		EC1=E1-EDE	000734
00302	189*		ECO=E0+EDE	000737
00303	190*		IF((KE.GT.ECO).AND.(INT.EQ.1.))INT=0.	000742
00305	191*		IF((KE.LT.EC1).AND.(INT.EQ.-1.))INT=0.	000760
00307	192*			000776
00307	193*		IF(KE.LE.E0)INT=1.	000776
00311	194*		IF(KE.GT.E1)INT=-1.	001004
00313	195*		IF((KE.GT.ECO).AND.(KE.LT.EC1))INT=0.	001012
00315	196*		IF(IMPL.LE.1)RETURN	001031
00315	197*	C		001031
00315	198*	C	STATISTICS	001031
00315	199*	C		001031
00317	200*		ME=AMAX1(ME,KE)	001040
00320	201*		MPC=AMAX1(MPC,KED)	001046
00321	202*		MPD=AMAX1(MPD,-KED)	001054
00322	203*		SPC=SPC+TINC*P1	001062
00323	204*		SPD=SPD+TINC*P2	001066
00323	205*	C		001066
00324	206*		IF(TIME.LT.TMAX1)RETURN	001072
00326	207*		CCI=CCI+CC	001101
00327	208*		CHI=CHI+CH	001104
00327	209*	C		001104
00330	210*			001107
00330	211*		RETURN	001107
00331	212*		END	001332

## 7.9 ONE DIMENSION TABLE LOOKUP



### Tables

FTA

Tabular values of function

### Description

### Inputs

#### Parameter/Port

FIN

Input quantity

AN

$ABS(AN) \leq 0.5$  for equispaced interpolation  
( $AN < 0$  prevents extrapolation)

### Outputs

#### Variable/Port

F0

Output quantity

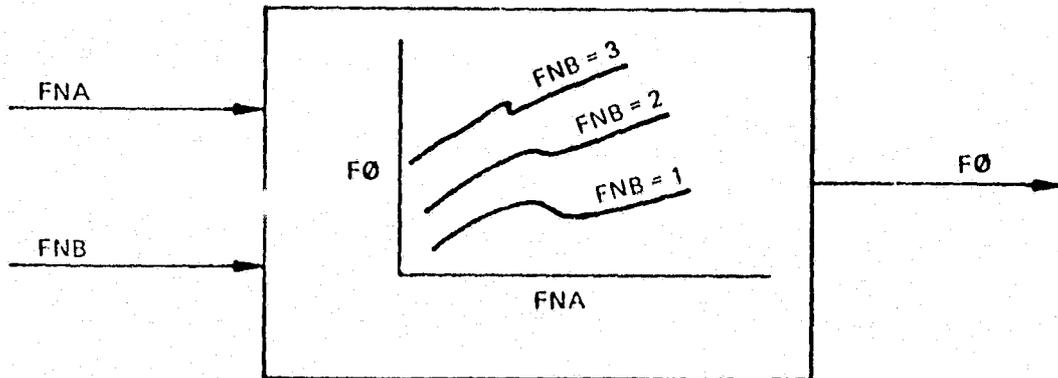
### Calculation Sequence

$$F0 = FTA(FIN)$$

NOTE: A maximum of 18 points is allowed in the table.



## 7.10 TWO DIMENSION TABLE LOOKUP



### Tables

FTA

Description  
Table of functional relationships (maximum number of table values = 144)

### Inputs

#### Parameter/Port

FNA	Input quantity (primary)
FNB	Input quantity (secondary)
AN	$ABS(AN) \leq 0.5$ for equal spaced FNA data*
BN	$ABS(BN) \leq 0.5$ for equal spaced FNB data*

### Outputs

#### Variable/Port

F0	Output quantity
----	-----------------

### Calculation Sequence

$$F0 = FTA(FNA, FNB)$$

\* A negative value for AN or BN prevents extrapolation beyond the table boundaries.

SUBROUTINE FV ENTRY POINT 000161

STORAGE USED CODE(1) 000204; DATA(0) 000036; BLANK COMMON(2) 000060

EXTERNAL REFERENCES (BLOCK, NAME)

0003 TBLU2  
0004 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0000	CG0012	INJPS	0000	I	000006	NAN	0000	I	000007	N8N	0000	I	000000	N1	0000	I	000001	N2	
0000	I	000002	N3	0000	I	000003	N4	0000	I	000004	N5	0000	I	000005	N6	0003	R	000000	TBLU2

```

00100      1*      CFV
00101      2*      SUBROUTINE FV(FTA,FO,FNA,FNB,AN,BN)
00101      3*      C
00101      4*      C PURPOSE - TO CALCULATE OUTPUT FO AS AN ARBITRARY FUNCTION OF INPUT
00101      5*      C VARIABLES FNA AND FNB. INPUT TABLE FTA IS USED GIVING
00101      6*      C FC=F(FNA,FNB)
00101      7*      C
00101      8*      C METHOD - TWO DIMENSIONAL TABLE LOOKUP
00101      9*      C
00101     10*      C
00101     11*      C LIMITATIONS - MAX ALLOWABLE SIZE OF TABULAR ARRAY IS 12X12.
00101     12*      C
00101     13*      C
00101     14*      C WRITTEN BY - GEORGE DULEBA LATEST REVISION MAY 76
00101     15*      C
00101     16*      C
00101     17*      C INPUT/OUTPUT LIST
00101     18*      C
00101     19*      C FTA TABULAR INPUT --- INPUT TABLE
00101     20*      C FO OUTPUT ANY OUTPUT VAR
00101     21*      C FNA INPUT A ANY INPUT VAR
00101     22*      C FNB INPUT B ANY INPUT VAR
00101     23*      C AN SET ABS(AN) .GT. 0.5 FOR UNEQUAL SPACED FNA DATA- INPUT PARM
00101     24*      C A NEGATIVE VALUE INDICATES THAT THE NEAREST END
00101     25*      C POINT IS TO BE USED UPON EXTRAPOLATION.
00101     26*      C BN SET ABS(BN) .GT. 0.5 FOR UNEQUAL SPACED FNB DATA- INPUT PARM
00101     27*      C A NEGATIVE VALUE INDICATES THAT THE NEAREST END
00101     28*      C POINT IS TO BE USED UPON EXTRAPOLATION.
00101     29*      C
00103     30*      DIMENSION FTA(1)
00104     31*      N1=FTA(3)+4
00105     32*      N2=FTA(2)+FTA(3)+4
00106     33*      N3=FTA(2)

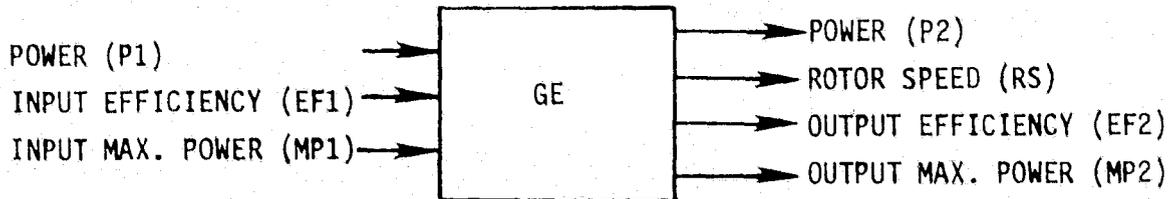
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00107	34*	N4=FTA(3)	000035
00110	35*	N5= SIGN(FTA(2),AN)	000044
00111	36*	N6= SIGN(FTA(3),BN)	000056
00112	37*	NAN=1	000070
00113	38*	IF (ABS(AN).LE.D.5) NAN=0	000072
00115	39*	NPN=1	000077
00116	40*	IF (ABS(BN).LE.D.5) NBN=0	000101
00120	41*	F0=TBLU2(FNA,FNB,FTA(N1),FTA(N2),FTA(N3),NAN,NBN,N5,N6,N3,N4)	000114
00121	42*	RETURN	000142
00122	43*	END	000203

7.11 AC INDUCTION GENERATOR



The induction generator produces electrical power proportional to rotor slip, i.e. difference between rotor speed and synchronous speed. This relationship is used to compute rotor speed given input power and the generator parameters. Two power losses are modeled: a constant multiplicative term due to resistive heating and an additive term due to mechanical friction. Default parameters are based on a conventional squirrel-cage induction motor/generator machine. This component can also be used as a synchronous generator with  $RAS \leq .01$ .

Basic Equations

Output power P2 and rotor speed RS are computed from the following equations:

$$P2 = EE * (P1 - C * RS^2)$$

$$\frac{P2}{RAP} = \frac{(RS/RSY - 1)}{RAS} \quad (\text{Power is proportional to slip})$$

where EE = electrical efficiency

C = constant of conversion

Inputs

<u>Parameter/Port</u>		<u>Description</u>	<u>Units</u>
P	1	Input power	kw
RAP		Rated output power	kw
RSY		Synchronous rotor speed (D = 1800)	rpm
RAS		Rated power slip (D = 0.05)	-
DA		Mechanical damping (D = 0.0)	joule-sec
SR		Internal stator resistance (D = 0.4/RAP)	ohms
V0		Rated bus voltage (D = 400)	volts
EF	1	Input product efficiency	-
MP	1	Maximum input discharge rate (D = $1 \times 10^8$ )	kw
CC		Capital cost/year	\$
CM		Maintenance cost/year	\$

Outputs

<u>Variable/Port</u>			
P	2	Output power	kw
EL		Electrical efficiency	-
RS		Rotor speed	rpm
PL		Power loss	kw
EF	2	Output product efficiency	-
MP	2	Maximum output discharge rate	kw

Statistics

MPN		Maximum output power/rated power	kw
SP		Total output energy	kwh

D - Default values supplied.

## Calculation Sequence

- 1) First pass only

$$EFF = 1$$

$$I_{RAT} = RAP * 1000 / V_0$$

$$EE = \frac{RAP}{RAP + SR * I_{RAT}^2 / 1000}$$

- 2) If  $P_1 = 0$  set  $P_2 = 0$ ,  $RS = RSY$  and go to 4)

Compute rotor speed  $\omega$  in rad/sec using

$$\frac{EE(P_1 * 1000 - \omega^2 * DA)}{RAP * 1000} = \frac{(\omega / \omega_0 - 1)}{RAS}$$

with  $\omega_0 = RSY * (2\pi / 60)$

- 3) Compute  $RS$  and output power

$$RS = \omega * (60 / 2\pi)$$

$$P_2 = RAP * (RS / RSY - 1) / RAS$$

$$P_2 > RAP \quad \Rightarrow \quad \text{DIAGNOSTIC}$$

$$EFF = P_2 / P_1$$

- 4) Compute loss, efficiency terms

$$PL = P_1 - P_2$$

$$EF_2 = EF_1 * EFF$$

- 5) Compute maximum output rate

$$MP_2 = \text{MIN}(RAP, MP_1 * EFF)$$

- 6) Compute Statistics and Costs

SUBROUTINE GE ENTRY POINT 000253

STORAGE USED CODE(1) 000363; DATA(0) 000043; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CIMPL 000002
0004 CTIME 000001
0005 COST 000004
0006 CSIMUL 000010

EXTERNAL REFERENCES (BLOCK, NAME)

0007 NWDUS
0010 NI02\$
0011 NERR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000064 10L 0000 000005 100F 0001 000074 20L 0001 000172 30L 0000 R 000003 A
0000 R 000004 B 0005 R 000000 CC 0005 P 000001 CM 0005 000003 CV 0005 000002 CO
0006 000000 DUM 0000 R 000000 EFF 0003 I 000001 ICNT 0003 I 000000 IMPL 0000 000032 INJPS
0000 R 000002 RATI 0004 R 000000 TIME 0006 R 000006 TINC 0006 R 000007 THAX 0000 R 000001 THAX1

00100 1\* C6E
00101 2\* SUBROUTINE GE(P2,EE,RS,PL,EF2,PM2,PMN,SP,P1,RAP,RSY,RAS,DA,SR,VO,
00101 3\* 1 EF1,PM1,CCI,CMI)
00101 4\* C
00101 5\* C PURPOSE MODEL AC INDUCTION GENERATOR
00101 6\* C
00101 7\* C METHOD MECHANICAL AND ELECTRICAL EFFICIENCIES ARE USED TO COMPUTE
00101 8\* C OUTPUT POWER. ROTOR SPEED IS COMPUTED ASSUMING POWER IS
00101 9\* C PROPORTIONAL TO SLIP.
00101 10\* C
00101 11\* C WRITTEN BY A.W. WARREN VERSION 1, MARCH 16 1977
00101 12\* C
00101 13\* C CALL SEQUENCE
00101 14\* C OUTPUTS
00101 15\* C P2 - OUTPUT POWER, KW
00101 16\* C EE - ELECTRICAL EFFICIENCY
00101 17\* C RS - ROTOR SPEED, RPM
00101 18\* C PL - POWER LOSS, KW
00101 19\* C EF2 - OUTPUT PRODUCT EFFICIENCY
00101 20\* C PM2 - MAXIMUM OUTPUT POWER, KW
00101 21\* C PMN - MAX. OBSERVED OUTPUT POWER / RATED POWER
00101 22\* C SP - TOTAL OUTPUT ENERGY, KWH
00101 23\* C

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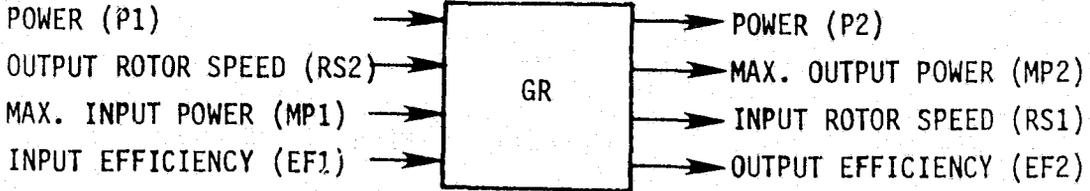


00160	81*	C	
00161	82*		
00163	83*		
00164	84*		
00164	85*	C	
00165	86*		
00166	87*		

COST SUMMATION  
IF( TIME.LT.TMAX1) RETURN  
CC = CC + CCI  
CM = CM + CMI  
RETURN  
END

000221  
000226  
000235  
000240  
000240  
000243  
000243  
000362

## 7.12 FIXED RATIO TRANSMISSION



This component models a fixed gear ratio transmission. Power losses are modeled by a table lookup depending on input power. Rotor input speed is used as a feedback variable.

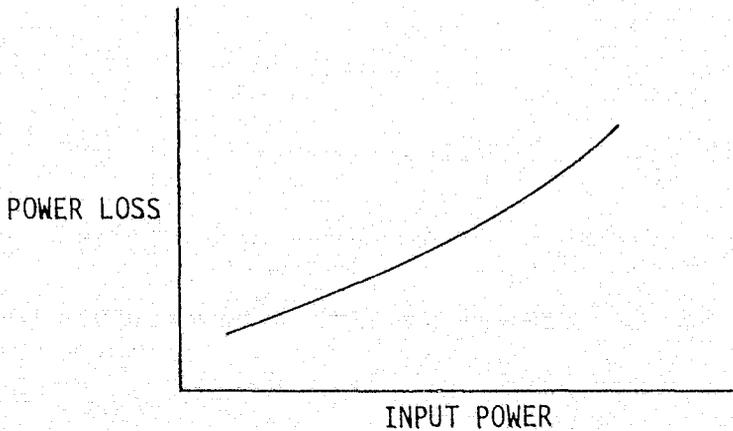


FIGURE 7.12: FIXED GEAR POWER LOSS

<u>Tables</u>	<u>Description</u>	<u>Units</u>
PL0	Power loss versus input power	kw

Inputs

<u>Parameter/Port</u>			
GR		Gear ratio	-
RS	2	Output rotor speed	rpm
P	1	Input power	kw
EF	1	Input product efficiency	-
MP	1	Maximum input power (Default = $1 \times 10^8$ )	kw
CC		Capital cost/year	\$
CM		Maintenance cost/year	\$

Outputs

<u>Variable/Port</u>			
P	2	Output power	kw
T0		Output torque	ft-lb
PL		Power loss	kw
EF	2	Output product efficiency	-
MP	2	Maximum output power	kw
RS	1	Input rotor speed	rpm

## Calculation Sequence

1)  $MP2 = MP1 - PL\phi(MP1)$  (First Pass Only)

If  $P1 \leq 0$ , set  $PL = P2 = 0$  and go to 2)

$$PL = PL\phi(P1)$$

$$P2 = P1 - PL$$

$$RS1 = RS2/GR$$

$$EF2 = EF1 * P2/P1$$

2)  $T\phi = P2 * 737.6 / (RS2 * 2 \pi / 60)$

3) Compute Costs

SUBROUTINE GR ENTRY POINT D00157

STORAGE USED CODE(1) 000237; DATA(0) 000023; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CIMPL 000001  
 0004 CTIME 000001  
 0005 COST 000004  
 0006 CSIMUL 000010

EXTERNAL REFERENCES (BLOCK, NAME)

0007 TBLU1  
 0010 NEPR3

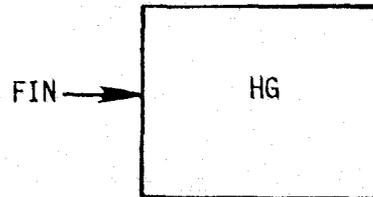
STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	C00057	I0L	0001	000113	Z0L	0005	R	000000	CC	0005	R	000001	CM	0005	C00002	C0	
0005	000003	CV	0006	000000	DUM	0003	I	000000	IMPL	0000		000007	INJPS	0000	I	000000	NP
0007	R	C00000	TBLU1	0004	R	000000	TIME	0006	R	000007	TMAX	0000	R	000001	TMAX1		

00100	1*	CGR															000000	
00101	2*	C	SUBROUTINE GR(PLO,P2,TO,PL,EF2,PH2,RS1,GRA,RS2,P1,EF1,PH1,CCI,CHI)														000000	
00101	3*	C															000000	
00101	4*	C	PURPOSE	MODEL A FIXED GEAR RATIO TRANSMISSION												000000		
00101	5*	C															000000	
00101	6*	C	METHOD	POWER LOSSES ARE INPUT AS A FUNCTION OF INPUT POWER P1.												000000		
00101	7*	C															000000	
00101	8*	C	WRITTEN BY	A.W. WARREN								VERSION	1, MARCH 16 1977				000000	
00101	9*	C															000000	
00101	10*	C	CALL SEQUENCE															000000
00101	11*	C	TABLES															000000
00101	12*	C		PLO - POWER LOSS IN KW VERSUS INPUT POWER IN KW												000000		
00101	13*	C															000000	
00101	14*	C	OUTPUTS															000000
00101	15*	C		P2 - OUTPUT POWER, KW												000000		
00101	16*	C		TO - OUTPUT TORQUE, FT-LB												000000		
00101	17*	C		PL - POWER LOSS, KW												000000		
00101	18*	C		EF2 - OUTPUT PRODUCT EFFICIENCY												000000		
00101	19*	C		PH2 - MAXIMUM OUTPUT POWER, KW												000000		
00101	20*	C		RS1 - INPUT ROTOR SPEED, RPM												000000		
00101	21*	C															000000	
00101	22*	C	INPUTS															000000
00101	23*	C		GRA - GEAR RATIO												000000		
00101	24*	C		RS2 - OUTPUT ROTOR SPEED, RPM												000000		
00101	25*	C		P1 - INPUT POWER, KW												000000		

00101	26*	C	EF1 - INPUT PRODUCT EFFICIENCY	000000
00101	27*	C	PM1 - MAXIMUM INPUT POWER, KW	000000
00101	28*	C	CCI - CAPITAL COST / YEAR, \$	000000
00101	29*	C	CM1 - MAINTENANCE COST / YEAR, \$	000000
00101	30*	C		000000
00103	31*		DIMENSION PLO(1)	000000
00104	32*		COMMON /CIMPL/IMPL /CTIME/ TIME	000000
00105	33*		COMMON /COST/CC,CM,CO,CV /CSIMUL/ DUH(7),TMAX	000000
00105	34*	C		000000
00105	35*	C	INITIALIZATION	000000
00105	36*	C		000000
00106	37*		NP = PLO(2)	000000
00107	38*		IF( IMPL.GT.0) GO TO 10	000007
00111	39*		EF2= 1.	000012
00112	40*		TMAX1 = .999999*TMAX	000014
00113	41*		RS2=1.	000021
00114	42*		IF(PM1.EQ. .999999) PM1=1.E10	000023
00116	43*		PM2 = PM1	000030
00117	44*		IF(PM1.LE. PLO(3+NP) ) PM2 = PM1-TBLU1(PM1,PLO(4),PLO(4+NP),1,-NP)	000032
00117	45*	C		000032
00117	46*	C	POWER LOSS AND ROTOR SPEED CALUCATIONS	000032
00121	47*		10 PL=0.	000057
00122	48*		P2=0.	000057
00123	49*		IF(P1 .EQ. 0.) GO TO 20	000060
00125	50*		PL = TBLU1(P1,PLO(4),PLO(4+NP),1,-NP)	000062
00126	51*		P2 = P1 - PL	000102
00127	52*		EF2 = EF1*P2/ P1	000104
00130	53*		RS1 = RS2/6PA	000107
00131	54*		20 IF(RS2 .GT. 0.) TO = P2*7043./RS2	000113
00131	55*	C		000113
00131	56*	C	COST SUMMATION	000113
00133	57*		IF(IMPL.LE.1) RETURN	000121
00135	58*		IF(TIME.LE.TMAX1) RETURN	000130
00137	59*		CC = CC + CCI	000137
00140	60*		CM = CM + CM1	000142
00141	61*		RETURN	000145
00142	62*		END	000236

## 7.13 HISTOGRAM



The input quantity is monitored during a SIMULATE analysis. When time reaches TMAX a plotted histogram is produced with 16 intervals that span the range from FLO to FUP.

### Inputs

<u>Variable/Port</u>	<u>Description</u>
FIN	Input quantity to be monitored
FUP	Upper limit for histogram
FLO	Lower limit for histogram
F1,...F16 <sup>1</sup>	Array containing histogram data
FA <sup>1</sup>	Measurement interval

### Outputs

<u>Variable/Port</u>	<u>Description</u>
AV	Mean value (running sum during simulation)
SD	Standard deviation (running sum squared)
SAM	Number of samples

<sup>1</sup> These quantities do not require data input values.

SUBROUTINE HG ENTRY POINT 000430

STORAGE USED CODE(1) 000506; DATA(0) 000166; BLANK COMMON(2) 012174

COMMON BLOCKS

0003 CTIME 000001
0004 CSIMUL 000010
0005 COVRLY 000004
0006 CIMPL 000001

EXTERNAL REFERENCES (BLOCK, NAME)

0007 SORT
0010 NWDUS
0011 NI035
0012 NI025
0013 NI015
0014 HERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000023 100L 0000 000052 100CF 0000 000056 1100F 0001 000012 120G 0000 000062 1200F
0000 000067 1300F 0001 000034 134G 0000 000073 140CF 0001 000111 154G 0001 000154 166G
0001 000175 177G 0001 000203 205G 0001 000211 213G 0001 000216 220G 0001 000223 225G
0001 000224 230G 0001 000234 236G 0001 000257 241G 0001 000272 246G 0001 000306 255G
0001 000314 262G 0001 000053 300L 0001 000364 303G 0001 000364 305G 0000 00047 900F
0000 R 000010 AX1 0000 R 000030 BLANK 0005 000003 CPUSEC 0004 000000 DUM 0005 000000 DUMM
0000 R 000036 FAX 0002 R 000000 GRAPH 0000 R 000032 HORIZ 0000 R 000041 HX 0000 I 000034 I
0000 I 000043 IC 0006 I 000000 IMPL 0000 000135 INJPS 0000 I 000037 ISAMP 0000 I 000042 J
0000 I 000044 JI 0000 I 000045 J2 0000 I 000046 J3 0000 I 000035 L 0000 R 000033 POINT
0000 R 000000 TD1 0003 R 000000 TIME 0004 R 000007 TMAX 0000 R 000031 VERT 0000 R 000040 XMAX

00100 1\* CHG
00101 2\* SUBROUTINE HG(SAMP,AV,SD,F1,F2,F3,F4,F5,F6,F7,F8,F9,F10,F11,
00101 3\* 1 F12,F13,F14,F15,F16,FA,FIN,FUP,FLO )
00101 4\* C VERSION 2. REVISED MARCH 1977
00101 5\* C PURPOSE - DEVELOP A RUNNING HISTOGRAM OF AN INPUT SEQUENCE
00101 6\* C CALL SEQUENCE
00101 7\* C SAMP- OUTPUT NUMBER OF SAMPLES
00101 8\* C AV - OUTPUT AVERAGE (RUNNING SUM)
00101 9\* C SD - OUTPUT STANDARD DEVIATION (RUNNING SUM SQUARED)
00101 10\* C F1-F16 - ARRAY WITH NUMBER OF OCCURENCES IN EACH INTERVAL
00101 11\* C FA - OUTPUT CONTAINING MEASUREMENT INTERVAL
00101 12\* C FUP - INPUT SPECIFYING UPPER MEASUREMENT LIMIT
00101 13\* C FLO - INPUT SPECIFYING LOWER MEASUREMENT LIMIT
00101 14\* C FIN - INPUT MEASUREMENT

HG

```

00103 15*      DIMENSION F1(16),TD1(8),AX1(16)
00104 16*      DIMENSION GRAPH(114,46)
00105 17*      COMMON GRAPH
00106 18*      COMMON/CTIME/TIME/CSIMUL/DUM(7),TMAX
00107 19*      COMMON/COVRLY/DUM(3),CPUSEC /CIMPL/IMPL
00110 20*      DATA BLANK,VERT,HORIZ,POINT/1H ,1H1,1H-,1H*/
00115 21*      IF(IMPL.GT.0) GO TO 100
00117 22*      DO 50 I=1,16
00122 23*          50 F1(I)=0.
00124 24*          FA=(FUP-FLO)/14.
00125 25*          SD=0.
00126 26*          AV =0.0
00127 27*          SAMP=0.0
00130 28*          100 CONTINUE
00131 29*          IF(IMPL.LT.2) RETURN
00133 30*          DO 200 I=1,16
00136 31*              L=I
00137 32*              FAX=FLO+(I-1)*FA
00140 33*              IF(FIN.LE.FAX) GO TO 300
00142 34*          200 CONTINUE
00144 35*          300 F1(L)=F1(L)+1.
00145 36*              SAMP=SAMP+1.
00146 37*              AV=AV+FIN
00147 38*              SD=SD+FIN*FIN
00150 39*              IF(TIME.LT.TMAX*.99999)RETURN
00152 40*              SAMP=0.
00153 41*              DO 350 I=1,16
00156 42*          350 SAMP=SAMP+F1(I)
00160 43*              ISAMP=SAMP
00161 44*              ISAMP=MAX(1,ISAMP)
00162 45*              AV=AV/ISAMP
00163 46*              SD=SD/ISAMP-AV*AV)
00164 47*              XMAX=F1(1)
00165 48*              DO 360 I=1,16
00170 49*          360 IF(F1(I).GE.XMAX) XMAX=F1(I)
00173 50*              IF(XMAX.EQ.0.) XMAX=10.
00175 51*              HX=XMAX/44.
00176 52*              DO 370 I=1,46
00201 53*              GRAPH(I,1)=VERT
00202 54*          370 GRAPH(114,I)=VERT
00204 55*              DO 380 I=2,113
00207 56*              GRAPH(I,1)=HORIZ
00210 57*          380 GRAPH(I,46)=HORIZ
00212 58*              DO 400 I=5,103,14
00215 59*          400 GRAPH(I,46)=VERT
00217 60*              DO 450 I=8,106,7
00222 61*          450 GRAPH(I,1)=VERT
00224 62*              DO 500 I=2,45
00227 63*              DO 500 J=2,113
00232 64*          500 GRAPH(J,I)=BLANK
00235 65*              DO 600 IC=1,16
00240 66*              J=IFIX(45.5-F1(IC)/HX)
00241 67*              DO 600 J1=1,7
00244 68*              J2=(IC-1)*7+J1+1
00245 69*              DO 600 J3=J,45
00250 70*
00250 71*          600 GRAPH(J2,J3)=POINT

```

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00254 72*      DO 700 I=1,16
00257 73*
00257 74*      700 AX1(I)=F1(I)/ISAMP
00261 75*      DO 800 I=1,8
00264 76*
00264 77*      800 TD1(I)=FLO+(I-1)*2.*FA-FA/2.
00266 78*
00266 79*      WRITE(6,900)((GRAPH(I,I),I=1,114)
00271 80*      900 FORMAT(11H1,9X,114A1/)
00272 81*      WRITE(6,1000)(AX1(I),I=1,16)
00275 82*      1000 FORMAT(1H+,9X,1H1,16F7.5,1H1/)
00276 83*      WRITE(6,1100)
00300 84*      1100 FORMAT(1H+,9X,1H1,112X,1H1/)
00301 85*      WRITE(6,1200)((GRAPH(I,J),I=1,114),J=2,46)
00312 86*      1200 FORMAT(1H+,9X,114A1/45(10X,114A1/))
00313 87*      WRITE(6,1300)(TD1(I),I=1,8)
00316 88*      1300 FORMAT(1H+,9X,8(F13.5,1X)/)
00317 89*      WRITE(6,1400) ISAMP,AV,SD
00324 90*      1400 FORMAT(1H+,10X,14HHISTOGRAM FOR ,I7,8H SAMPLES,
00324 91*      19H MEAN= ,F13.5,18H STANDARD DEV.= ,F13.5/)
00325 92*      RETURN
00326 93*      END

```

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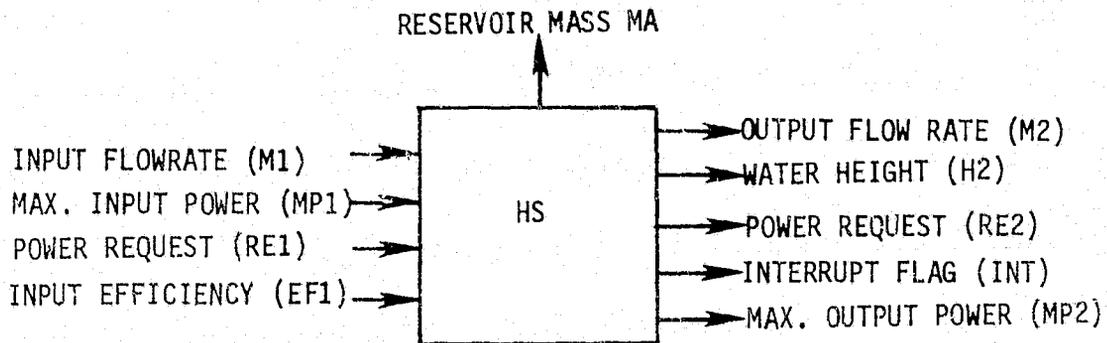
000306
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## 7.14 HYDRO STORAGE VESSEL



The hydro storage vessel is modeled as an above ground reservoir with a large and constant surface area. The change in reservoir height between maximum and minimum levels is assumed small in comparison to the height of the water above the turbine. Hence, reservoir height is assumed constant. The reservoir has specified evaporation and leakage rates. Average input flow gained by rainfall is also specified. Energy storage is calculated based on the potential energy of the water in the reservoir relative to the turbine inlet.

### Basic Equation

$$MA = M1 - M2 - NE*AS - NL + MDR*AS/14052$$

## Inputs

<u>Parameter/Port</u>	<u>Description</u>	<u>Units</u>
M 1	Input water mass flow rate	gal/h
NE	Evaporation coefficient (D = 0.03)	gal/ft <sup>2</sup> -h
AS	Reservoir surface area	ft <sup>2</sup>
NL	Leakage coefficient (D = 8.0)	gal/h
MDR	Rainfall rate	inches/year
MDM	Maximum allowable mass flow rate (D = 4X10 <sup>5</sup> )	gal/h
MM	Maximum allowable reservoir capacity (D=5X10 <sup>6</sup> )	gal
MØ	Minimum allowable reservoir capacity	gal
H 1	Reservoir height above turbine	ft
MDE	Reservoir deadband for priority resequence	gal
RE 1	Power request (discharge)	kw
CR	Reservoir cost coefficient (D = 0.025)	\$/gal
EF 1	Input product efficiency	-
MP 1	Maximum input charging rate	kw
LE	Reservoir life expectancy	years
CM	Maintenance cost/year	\$

## Outputs

<u>Variable/Port</u>	<u>Description</u>	<u>Units</u>
M 2	Outlet water mass flow rate	gal/hr
E	Energy stored	kwh
H 2	Reservoir height above turbine (=H1)	ft
MA	Reservoir mass (state)	gal
CCØ	Reservoir cost/year	\$
MP 2	Maximum discharge rate allowable	kw
INT	Priority interrupt flag	-
RE 2	Maximum charging rate request	kw

D - Default values supplied

<u>Statistics</u>	<u>Description</u>	<u>Units</u>
MDU	Maximum mass flow rate	gal/hr
MU	Maximum reservoir mass	gal
ML	Minimum reservoir mass	gal

The calculation sequence and default values assume a pond sized for 120kw storage for 24 hours ( $5 \times 10^6$  gallons of water 200 ft. above turbine inlet). The evaporation coefficient NE assures the pond drops  $\frac{1}{2}$ " in height per 10 hours. To obtain a more accurate value for this parameter requires knowledge of local conditions. The leakage coefficient NL is based on the assumption of a loss of 0.1% of the maximum reservoir capacity in the rated storage time of 24 hours. The reservoir cost estimates are based on the compensation reservoir given in Reference 1.

- 
1. "Preliminary Feasibility Evaluation of Compressed Air Storage Power Systems," United Technologies AER 74-00242, December 1976.

## Calculation Sequence

$$C1 = \text{conversion constant} = 0.377 \times 10^{-6} \frac{\text{kw-h}}{\text{ft-lb}}$$

$$C2 = \text{conversion constant} = 8.3398 \text{ lb/gal}$$

$$A = C1 * C2 * H1$$

### 1) Reservoir cost

$$CC = CR * WM / LE$$

### 2) Volume of water discharged

$$M2 = RE1 / A$$

### 3) Reservoir water volume

$$MA = M1 - M2 - NE * AS - NL + (MDR * AS / 14052.)$$

### 4) Energy stored

$$E = A * M$$

### 5) Checks

$$M1 > MDM \text{ or } M2 > MDM \Rightarrow \text{DIAGNOSTIC}$$

$$M > WM, \Rightarrow \text{DIAGNOSTIC}$$

$$M < M0 \Rightarrow \text{DIAGNOSTIC}$$

### 6) Priority interrupt

$$\text{If } M \leq M0, \text{ INT} = 1$$

$$\text{If } M > M0 + MDE \text{ and } \text{INT} = 1, \text{ INT} = 0$$

$$\text{If } M \geq WM, \text{ INT} = -1$$

$$\text{If } M < WM - DME \text{ and } \text{INT} = -1, \text{ INT} = 0$$

Calculation Sequence Cont.

7) Maximum charging rate request

$$MD1 = \text{MIN} (MDM, (MM-M)/TINC)$$

$$RE2 = \text{MIN} (MP1, MD1 * A) / EF1$$

Maximum discharge rate

$$MP2 = A * \text{MIN} (MDM, (M-M\emptyset) / TINC)$$

where TINC = integration step size in hrs

8) Compute Statistics and Costs

SUBROUTINE HS ENTRY POINT 000405

STORAGE USED CODE(1) 000551; DATA(0) 000117; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 C1MPL 000002  
 0004 CTIME 000001  
 0005 CSIMUL 000010  
 0006 COST 000002

EXTERNAL REFERENCES (BLOCK, NAME)

0007 HWDUS  
 0010 N1023  
 0011 NERR33

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000055	100L	0000	000005	1010F	0000	000030	1020F	0000	000045	1030F	0001	000144	200L					
0001	000171	300L	0001	000215	400L	0000	R	000004	A	0006	R	000000	CCI	0006	R	000001	CMI		
0000	R	000003	C1	0005	R	000000	DUM	0003	I	000001	ICNT	0003	I	000000	IMPL	0000	000076	INJPS	
0000	R	000001	MDM1	0000	R	000000	MD1	0004	R	000000	TIME	0005	R	000007	THAX	0000	R	000002	THAX1

00100	1*	CHS		000000
00101	2*		SUBROUTINE HS(M,DM,IM,M2,E,H2,CC,MP2,INT,RE2,MDU,MU,ML,M1,NE	000000
00101	3*		1 ,AS,NL,MDR,MDM,MM,MO,H1,MDE,RE1,CR,EF1,MP1,LE,CH)	000000
00101	4*	C		000000
00101	5*	C	PURPOSE PERFORMANCE OF A LARGE RESERVOIR AS AN ENERGY STORAGE	000000
00101	6*	C		000000
00101	7*	C	DEVICE.	000000
00101	8*	C		000000
00101	9*	C	METHOD ENERGY IN STORAGE IS CALCULATED FROM THE POTENTIAL	000000
00101	10*	C		000000
00101	11*	C	BETWEEN THE RESERVOIR AND THE TURBINE INLET.	000000
00101	12*	C		000000
00101	13*	C	WRITTEN BY F. O. MAHONY VERSION 1, MARCH 30 1977	000000
00101	14*	C		000000
00101	15*	C	CALL SEQUENCE	000000
00101	16*	C	OUTPUTS	000000
00101	17*	C	M - RESERVOIR MASS (STATE VARIABLE), GAL	000000
00101	18*	C	DM - RESERVOIR MASS FLOWRATE, GAL/HR	000000
00101	19*	C	IM - STATUS INDICATOR	000000
00101	20*	C	M2 - OUTLET WATER MASS FLOW RATE, GAL/HR	000000
00101	21*	C	E - ENERGY STORED, KWH	000000
00101	22*	C	H2 - RESERVOIR HEIGHT ABOVE TURBINE (=H1), FT	000000
00101	23*	C	CC - RESERVOIR COST/YEAR, \$	000000

HS

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00101 24* C MP2 - MAXIMUM DISCHARGE RATE ALLOWABLE, KW 000000
00101 25* C INT - PRIORITY INTERRUPT FLAG 000000
00101 26* C REZ - MAXIMUM CHARGING RATE REQUEST, KW 000000
00101 27* C MDU - MAXIMUM MASS FLOW RATE, GAL/HR 000000
00101 28* C MU - MAXIMUM RESERVOIR MASS, GAL 000000
00101 29* C ML - MINIMUM RESERVOIR MASS, GAL 000000
00101 30* C
00101 31* C INPUTS 000000
00101 32* C M1 - INPUT WATER MASS FLOW RATE, GAL/HR 000000
00101 33* C NE - EVAPORATION COEFFICIENT, GAL/FT**2-HR 000000
00101 34* C AS - RESERVOIR SURFACE AREA, FT**2 000000
00101 35* C NL - LEAKAGE COEFFICIENT 000000
00101 36* C MDR - RAINFALL RATE, INCHES/YEAR 000000
00101 37* C MDH - MAXIMUM ALLOWABLE MASS FLOW RATE, GAL/HR 000000
00101 38* C MH - MAXIMUM ALLOWABLE RESERVOIR CAPACITY, GAL 000000
00101 39* C MO - MINIMUM ALLOWABLE RESERVOIR CAPACITY, GAL 000000
00101 40* C H1 - RESERVOIR HEIGHT ABOVE TURBINE, FT 000000
00101 41* C MDE - RESERVOIR DEADBAND FOR PRIORITY RESEQUENCE, GAL 000000
00101 42* C RE1 - POWER REQUEST (DISCHARGE), KW 000000
00101 43* C CR - RESERVOIR COST COEFFICIENT 000000
00101 44* C EFi - INPUT PRODUCT EFFICIENCY 000000
00101 45* C MP1 - MAXIMUM INPUT CHARGING RATE, KW 000000
00101 46* C LE - RESFRVOIR LIFE EXPECTANCY, YEARS 000000
00101 47* C CM - MAINTENANCE COST/YEAR, $ 000000
00101 48* C
00103 49* C COMMON/CIMPL/INPL,ICNT/CTIME/TIME/CSINHUL/DUM(7),TMAX 000000
00104 50* C COMMON/COST/CCI,CM1 000000
00105 51* C REAL M2,MP2,MDU,MU,ML,M1,NE,NL,MDR,MDH,MH,MO,MDE,MP1,LE,INT,M 000000
00106 52* C REAL MD1,MDH1 000000
00106 53* C 000000
00107 54* C IF(IMPL.GT.0)GO TO 100 000000
00107 55* C 000000
00111 56* C RF1=0.0 000002
00112 57* C H2=H1 000003
00113 58* C TMAX1=TMAX*0.99999 000005
00114 59* C C1 = 3.1441E-6 000010
00114 60* C 000010
00115 61* C INT=0.0 000012
00116 62* C MDU=0.0 000013
00117 63* C MU =0.0 000014
00120 64* C ML =1.0E10 000015
00121 65* C IF(NE .EQ. .99999)NE =0.03 000017
00123 66* C IF(NL .EQ. .99999)NL =8.0 000024
00125 67* C IF(MDH.EQ. .99999)MDH=4.0E5 000031
00127 68* C IF(MH .EQ. .99999)MH =5.0E6 000036
00131 69* C IF(CR .EQ. .99999)CR =0.025 000043
00131 70* C 000043
00131 71* C 000043
00131 72* C RESERVOIR COST 000043
00131 73* C 000043
00133 74* C CC =CR*MH/LE 000050
00133 75* C 000050
00133 76* C VOLUME OF WATER DISCHARGED 000050
00133 77* C 000050
00134 78* C 100 A=C1*H1 000055
00135 79* C M2 =RE1/A 000057
00135 80* C 000057

```

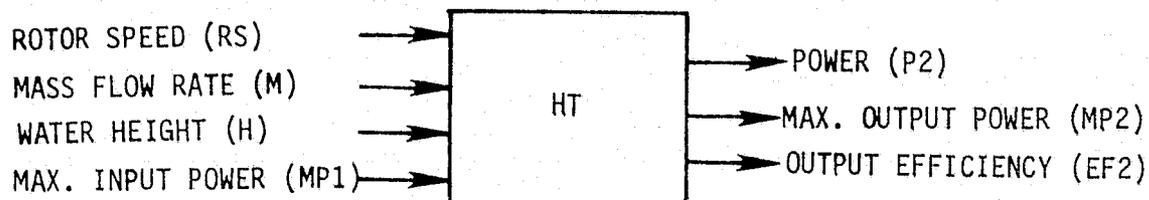
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**H S**



00223	138*	2	26H	IS GREATER THAN MAXIMUM,F12.3)	000550
00224	139*	1020	FORMAT(1H0,19HHS	RESERVOIR VOLUME,F12.3,	000550
00224	140*	1	30H	EXCEEDED MAXIMUM ALLOWABLE,F12.3)	000550
00225	141*	1030	FORMAT(1H0,19HHS	RESERVOIR VOLUME,F12.3,	000550
00225	142*	1	24H	DROPED BELOW MINIMUM,F12.3)	000550
00225	143*	C			000550
00226	144*		END		000550

## 7.15 HYDRAULIC TURBINE



The hydraulic turbine model is based on a constant speed design and is typical of a reaction/Francis type turbine. The turbine is assumed to be designed to a specified operating point and output power.

For off design performance the pump efficiency is assumed to be functionally related to the first power of the mass flow rate. The equations are assumed to be valid over a specified range of values for the turbine parameter.

### Basic Equations

$$P = \text{EFF} * M * C1 * C2 * H$$

$$\text{EFF} = 1 - (1 - \text{EFD}) * MD / M$$

where C1, C2 are conversion constants.

## Inputs

<u>Parameter/Port</u>	<u>Description</u>	<u>Units</u>
M	Inlet mass flow rate	gal/h
H	Height of reservoir above turbine inlet	ft
EFD	Design pt. turbine efficiency (D = 0.90)	-
MD	Design pt. mass flow rate (D = $2 \times 10^5$ )	gal/h
MM	Maximum mass flow rate (D = $3 \times 10^5$ )	gal/h
EF	1 Input product efficiency	-
MP	1 Input maximum discharge rate	kw
CK	Turbine capacity cost coefficient <sup>1</sup> (D = 0.011)	-
F0	Turbine exponent for cost calculations (D = 0.5)	-
RS	Angular velocity	rpm
X	Turbine head exponent for cost calculations (D = 0.25)	-

## Outputs

### Variable/Port

CC0	Turbine cost/year	\$
EFF	Turbine efficiency	-
P	2 Output power	kw
EF	2 Output product efficiency	-
MP	2 Output maximum discharge rate	kw
CP	Turbine characteristic parameter	-

## Statistics

CPU	Maximum CP	-
CPL	Minimum CP	-
PU	Maximum output power	kw

D - Default values

<sup>1</sup>CK = Capital cost (known unit) / ((MD \* 481.2) \*\* F0 \* H \*\* X \* life expectancy)

The calculation sequence and default values assume a constant speed reaction type hydraulic turbine nominally rated for 120kw and located 200 ft. below the reservoir. The equations relating the various physical parameters are assumed to be valid for the indicated range of the characteristic turbine parameter, CP. The equations and cost estimates are based on the data given in Reference 1, and the cost estimates on data from Reference 2.

## Calculation Sequence

$$C1 = 0.377 \times 10^{-6} \frac{\text{kwh}}{\text{ft-lb}}$$

$$C2 = 8.3398 \text{ lb/gal}$$

$$A = C1 * C2 * H$$

### 1) Costs

$$CC0 = CK * (MD * 481.2) * F0 * H * X$$

### 2) Efficiency

If  $M \leq 0$  set  $EFF = 1$  and go to 3)

$$EFF = 1 - (1 - EFD) * MD / M$$

$$EFF = \text{MAX}(EFF, 0.6)$$

- 
1. L. Marks and T. Baumeister, "Mechanical Engineers Handbook", McGraw Hill, N.Y., 1958, Section 9, p. 207.
  2. Carson and Fogleman, "Comparison of Methods for Converting Existing Power Plants to Pumped Storage Facilities", International Engineering Company, Inc., 1974.

Calculation Sequence Cont.

- 3) Output Power

$$P2 = EFF * A * M$$

- 4) Product Efficiency

$$EF2 = EF1 * EFF$$

$$EFM = MM - (1 - EFD) * MD$$

- 5) Maximum Discharge Rate

$$MP2 = \text{Min} \{ MP1 * EFD, EFM * A \}$$

- 6) Turbine Characteristic Parameter

(If  $P2 \leq 0$  go to 7)

$$CP = RS * \text{SQRT} (P2 * 0.746) / H^{**1.25}$$

If  $CP > 100$  write DIAGNOSTIC

If  $M > MM$  write DIAGNOSTIC

- 7) Compute Statistics and Costs

SUBROUTINE HT ENTRY POINT 000305

STORAGE USED CODE(1) 000430; DATA(1) 000075; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 SIMPL 000002  
 0004 CTIME 000001  
 0005 CSIMUL 000010  
 0006 COST 000001

EXTERNAL REFERENCES (BLOCK, NAME)

0007 XPRR  
 0010 SQRT  
 0011 NWD05  
 0012 NI025  
 0013 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000073	100L	0000	000003	1010F	0000	000016	1020F	0001	000205	200L	0001	000231	300L				
0001	000113	400L	0006	R	000000	CCI	0000	R	000001	CI	0005	000000	DUM	0000	R	000002	EFM	
0003	I	000001	ICNT	0003	I	000000	IMPL	0000	000057	INJPS	0004	R	000000	TIME	0005	R	000007	TMAX
0000	R	000000	TMAX1															

00100	1*	CHT		000000
00101	2*		SUBROUTINE HT(C,C,EFF,P,EF2,MP2,CP,CPU,CPL,PU,H,H,EPD,MD,HH	000000
00101	3*		1	000000
00101	4*	C	,EF1,MP1,CK,FO,RS,X)	000000
00101	5*	C	PURPOSE PERFORMANCE OF A HYDRAULIC TURBINE	000000
00101	6*	C		000000
00101	7*	C	METHOD OFF DESIGN PERFORMANCE IS ASSUMED PROPORTIONAL TO	000000
00101	8*	C		000000
00101	9*	C	MASS FLOW RATE	000000
00101	10*	C		000000
00101	11*	C	WRITTEN BY F. O. MAHONY	000000
00101	12*	C	VERSION 1, MARCH 30 1977	000000
00101	13*	C	CALL SEQUENCE	000000
00101	14*	C	OUTPUTS	000000
00101	15*	C	CC - TURBINE COST/YEAR, S	000000
00101	16*	C	EFF - TURBINE EFFICIENCY	000000
00101	17*	C	P - OUTPUT POWER, KW	000000
00101	18*	C	EF2 - OUTPUT PRODUCT EFFICIENCY	000000
00101	19*	C	MP2 - OUTPUT MAXIMUM DISCHARGE RATE, KW	000000
00101	20*	C	CP - TURBINE CHARACTERISTIC PARAMETER	000000
00101	21*	C	CPU - MAXIMUM CP	000000

HT

```

00101 22* C CPL - MINIMUM CP 000000
00101 23* C PU - MAXIMUM OUTPUT POWER, KW 000000
00101 24* C 000000
00101 25* C INPUTS 000000
00101 26* C M - INLET MASS FLOW RATE, GAL/HR 000000
00101 27* C H - HEIGHT OF RESERVOIR ABOVE TURBINE INLET, FT 000000
00101 28* C EFD - DESIGN POINT TURBINE EFFICIENCY 000000
00101 29* C MD - DESIGN POINT MASS FLOW RATE, GAL/HR 000000
00101 30* C MM - MAXIMUM MASS FLOW RATE, GAL/HR 000000
00101 31* C EF1 - INPUT PRODUCT EFFICIENCY 000000
00101 32* C MP1 - INPUT MAXIMUM DISCHARGE RATE 000000
00101 33* C CK - TURBINE CAPACITY COST COEFFICIENT 000000
00101 34* C FO - TURBINE EXPONENT FOR COST CALCULATIONS 000000
00101 35* C RS - ANGULAR VELOCITY, RPM 000000
00101 36* C X - TURBINE HEAD EXPONENT FOR COST CALCULATIONS 000000
00101 37* C 000000
00103 38* C COMMON/CIHPL/IMPL,ICNT/CTIME/TIME /CSIMUL/DUM(7),TMAX /COST/ CCI 000000
00104 39* C REA' MP2,M,MD,MM,MP1 000000
00104 40* C 000000
00105 41* C IF(IMPL.GT.0)GO TO 100 000000
00105 42* C 000000
00107 43* C TMAX1=TMAX*0.99999 000002
00110 44* C RS =3600.0 000005
00110 45* C 000005
00111 46* C IF(EFD.EQ. .99999)EFD=0.9 000007
00113 47* C IF(MD .EQ. .99999)MD =2.0E5 000014
00115 48* C IF(MM .EQ. .99999)MM =3.0E5 000021
00117 49* C IF(CK .EQ. .99999)CK =0.011 000026
00121 50* C IF(FO .EQ. .99999)FO =0.5 000033
00123 51* C IF(X .EQ. .99999)X =0.25 000040
00123 52* C 000040
00125 53* C CPL=1.0E10 000045
00126 54* C CPU=0.0 000047
00127 55* C PU =0.0 000050
00127 56* C 000050
00130 57* C C1 = 3.1441E-6 000051
00131 58* C CC =CK*(MD*481.2)**FO*M**X 000053
00131 59* C 000053
00131 60* C EFFICIENCY 000053
00132 61* C 100 EFF =1.0 000073
00132 62* C 000073
00133 63* C IF(M.LE.0.0)GO TO 400 000074
00133 64* C 000074
00135 65* C EFF=1.0-(1.0-EFD)*MD/M 000077
00136 66* C IF(EFF.LT.0.6) EFF=0.6 000104
00136 67* C 000104
00136 68* C OUTPUT POWER 000104
00136 69* C 000104
00140 70* C *00 P =EFF*M*M*C1 000113
00140 71* C 000113
00140 72* C PRODUCT EFFICIENCY 000113
00140 73* C 000113
00141 74* C EF2=EF1*EFF 000117
00141 75* C 000117
00141 76* C MAXIMUM DISCHARGE RATE 000117
00141 77* C 000117
00142 78* C EFM =MM*.9999-(1.0-EFD)*MD 000122

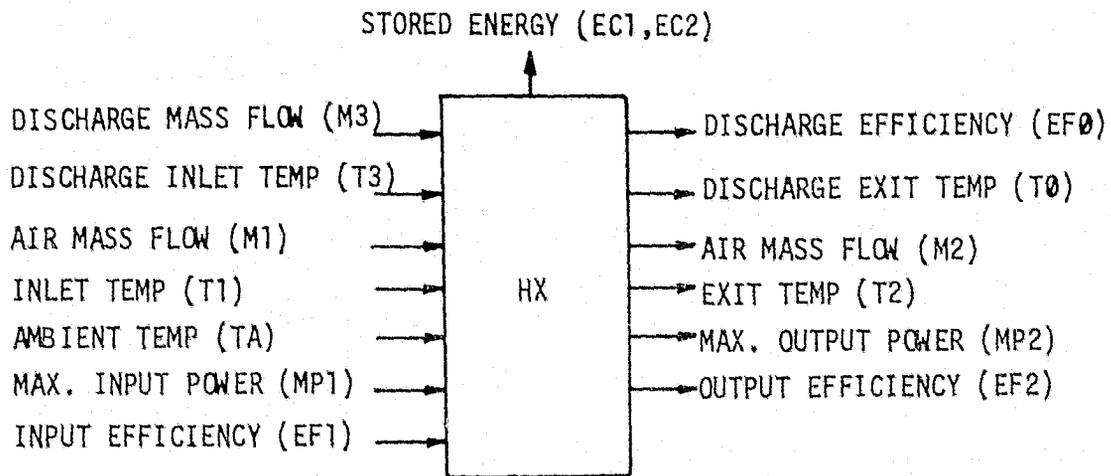
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00142	79*	C				000122
00143	80*		MP2=AMIN1(MP1+EFD,EFH*H+C1)			000131
00143	81*	C				000131
00143	82*	C		TURBINE CHARACTERISTIC PARAMETER		000131
00143	83*	C				000131
00144	84*		IF(P .LE. 0.0) GO TO 300			000142
00146	85*		CP =RS*SQRT(P*0.746)/H**1.25			000144
00146	86*	C				000144
00147	87*		IF(CP.LT.100.0)GO TO 200			000162
00147	88*	C				000162
00151	89*		IF(IMPL.EQ.2)WRITE(6,1010)CP			000165
00155	90*		IF(IMPL.EQ.2) ICNT=ICNT+1			000176
00155	91*	C				000176
00157	92*		200 IF(M.LT.MM)GO TO 300			000205
00157	93*	C				000205
00161	94*		IF(IMPL.EQ.2)WRITE(6,1020)M,MM			000210
00166	95*		IF(IMPL.EQ.2) ICNT=ICNT+1			000222
00166	96*	C				000222
00170	97*		300 IF(IMPL.LE.1)RETURN			000231
00170	98*	C				000231
00170	99*	C		STATISTICS		000231
00170	100*	C				000231
00172	101*		CPU=AMAX1(CPU,CP)			000237
00173	102*		CPL=AMIN1(CPL,CP)			000245
00174	103*		PU =AMAX1(PU ,P )			000253
00174	104*	C				000253
00175	105*		IF(TIME.LT.TMAX1)RETURN			000261
00175	106*	C				000261
00175	107*	C		COST		000261
00175	108*	C				000261
00177	109*		CCI=CCI+CC			000270
00177	110*	C				000270
00200	111*		RETURN			000273
00200	112*	C				000273
00201	113*		1010 FORMAT(1H0,48HHT TURBINE CHARACTERISTIC PARAMETER OUT OF RANGE			000427
00201	114*		1 F12.3)			000427
00202	115*		1020 FORMAT(1H0,23HHT INLET MASS FLOW RATE,F12.3			000427
00202	116*		1 ,37H GREATER THAN MAXIMUM DESIGN VALUE,F12.3)			000427
00202	117*	C				000427
00203	118*		END			000427

HT

## 7.16 ADIABATIC HEAT EXCHANGER



The purpose of the adiabatic heat exchanger is to recover a portion of the heat of compression from the high pressure, high temperature air exiting from the compressor. Figure 7.16-1 shows an adiabatic heat exchanger used in an underground, constant pressure compressed air energy storage system. The adiabatic heat exchanger operates in a manner similar to the high temperature thermal energy storage systems currently conceived for solar thermal power plants<sup>1</sup>. In the storage charging mode, high pressure, high temperature air enters the top of the heat exchanger and deposits a portion of its thermal energy in the storage media as either sensible heat or latent heat of fusion. The exiting high pressure air is stored in an appropriate vessel, e.g., underground cavern. In the discharge cycle (HY), high pressure, low temperature air enters the bottom of the heat exchanger, recovers thermal energy from the storage media and exits to the turbine.

The adiabatic heat exchanger model is based on a two cell storage model. Given the stored energy in both cells, a linear temperature profile is computed

<sup>1</sup> BEC/EPRI RP 788-1, "Advanced Thermal Energy Storage Systems," November 1976.

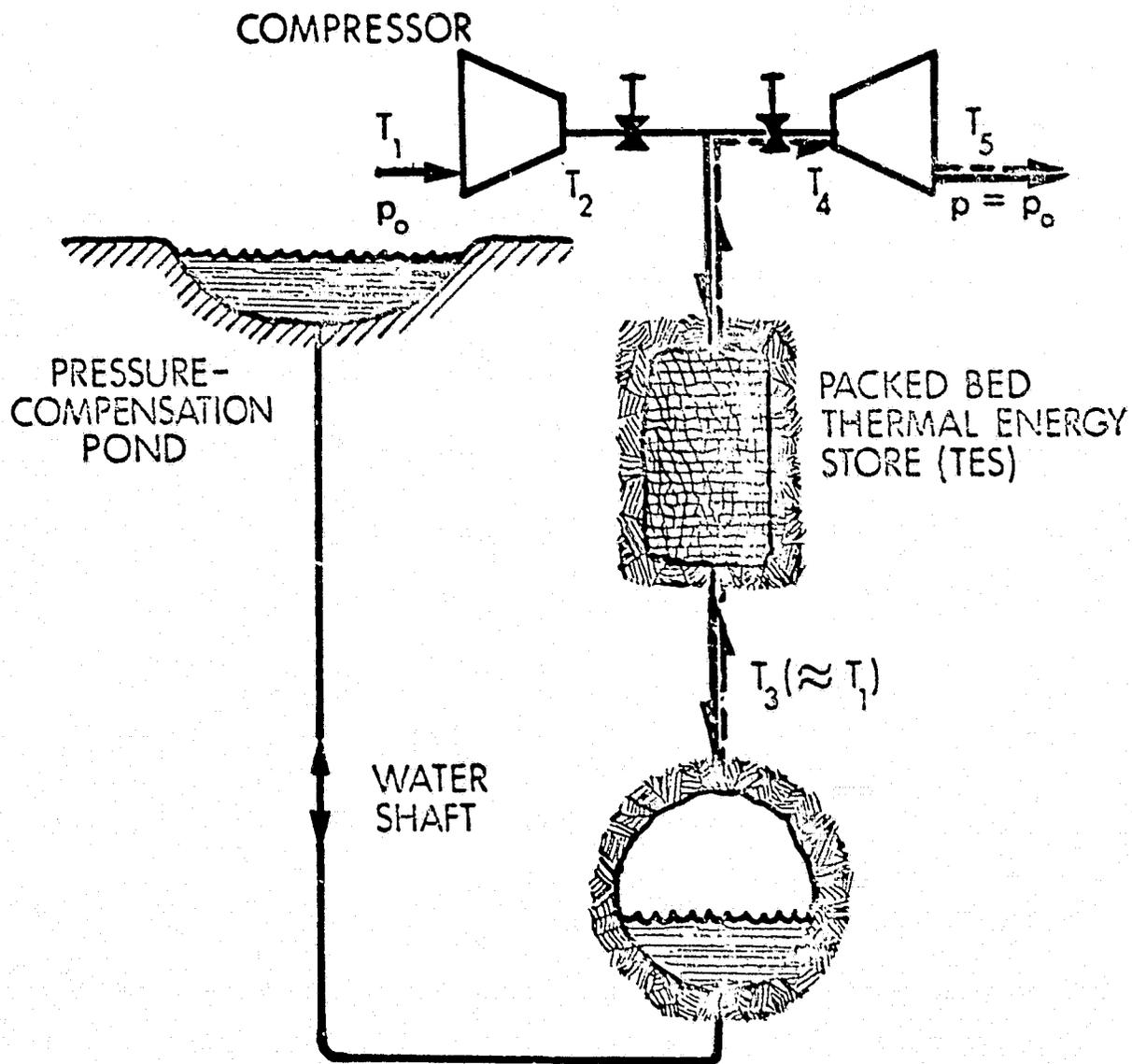


FIGURE 7.16-1 KOUTZ-GLENDENNING ADIABATIC COMPRESSED AIR STORAGE SCHEME (SINGLE-STAGE HEAT-OF-COMPRESSION STORAGE)

for the media mass. Based on a given inlet mass flow rate, the convective film coefficient, unit thermal conductance, and heat exchanger exit temperature are calculated.

The rate of energy deposited (or withdrawn) is calculated and integrated to yield the stored energy state. For a phase change media, the temperature profile is approximated in the following way: Average cell temperatures TS1 and TS2 are determined from the enthalpy diagram (Figure 7.16-2) using average cell entropy EC1/MA and EC2/MA, respectively. Then a linear temperature profile is constructed as shown in Figure 7.16-3.

### Basic Equations

$$\dot{EC}_1 = PX - PY - NU * EC_1 - BE * (EC_1 - EC_2)$$

$$\dot{EC}_2 = (P_2 - PX) - (P_0 - PY) - NU * EC_2 + BE * (EC_1 - EC_2)$$

where

EC1, EC2 = storage power in cells 1 and 2, respectively

PX = charging power in cell 1

PY = discharging power in cell 1

P2 - PX = charging power in cell 2

P0 - PY = discharging power in cell 2

NU = storage media leakage constant

BE = storage media mixing constant

# HX

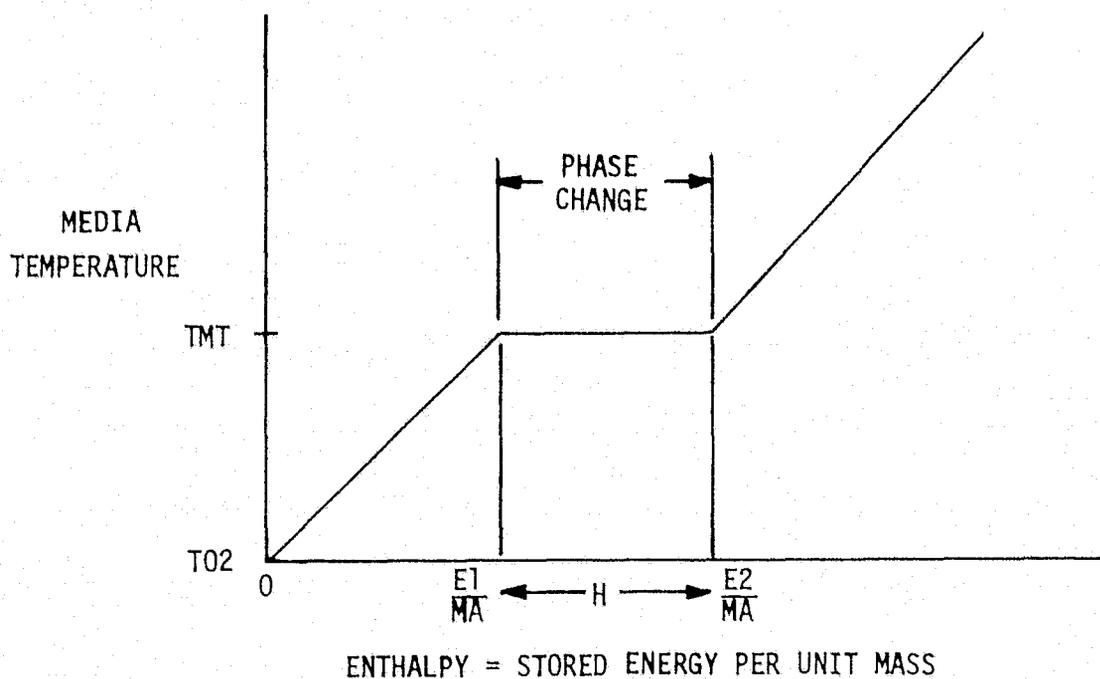


FIGURE 7.16-2: ENTHALPY-TEMPERATURE DIAGRAM FOR HX

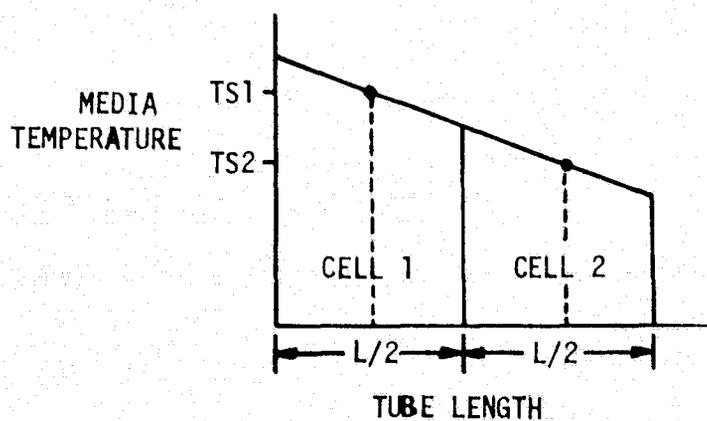


FIGURE 7.16-3: STORAGE TEMPERATURE VERSUS TUBE LENGTH

## Inputs

<u>Parameter/Port</u>	<u>Description</u>	<u>Units</u>
NU	Storage energy loss coefficient (D = 0.002)	(h) <sup>-1</sup>
ST	Rated storage time <sup>1</sup>	h
BE	Storage energy mixing coefficient (D = 0.0)	h <sup>-1</sup>
T01	Minimum allowable storage temperature (D = 60)	°F
DTD	Media temperature swing <sup>1</sup> (D = 400)	°F
PD	Rated storage thermal power	kw
TEM	Maximum allowable exit temperature (D = 240)	°F
XD	Design point fraction of molten media mass (D = 0.8)	-
EF	1 Input product efficiency	-
MP	1 Maximum input charging rate	kw
CP1	Storage media heat capacity (D = 2.93X10 <sup>-4</sup> )	kwh/lb °F
H	Storage media heat of fusion <sup>2</sup> (D = 0.0219)	kwh/lb
TMT	Storage media melt temperature <sup>2</sup> (D = 147)	°F
CPF	Air heat capacity (D = 7.6X10 <sup>-5</sup> )	kwh/lb °F
KF	Air thermal conductivity (D = 1.03X10 <sup>-4</sup> )	kw/ft °F
MU	Air viscosity (D = 0.055)	lb/ft-h
NT	Number of tubes (D = 200)	-
D	Tube diameter (D = 0.03)	ft
L	Tube length (D = 4)	ft
DEL	Tube half spacing (D = 0.085)	ft
K	Storage media thermal conductivity (D = 0.0078)	kw/ft-°F
T	1 Inlet air temperature	°F
M	1 Inlet mass flow rate	lb/h
CM	Storage device yearly maintenance cost (D = 0.6)	\$/kw
CSA	Storage device capacity cost (D = 50)	\$/kw
CSB	Storage device energy cost (D = 15.6)	\$/kwh
LE	Unit life expectancy	years

D - Default values specified

1 - Design point conditions

2 - Used for phase change media, H = 0 for sensible heat

## Inputs

<u>Parameter/Port</u>		<u>Description</u>	<u>Units</u>
M	3	Discharge cycle mass flow rate from storage	lb/hr
T	3	Discharge cycle temperature from storage	$^{\circ}\text{F}$
TA		Ambient temperature	$^{\circ}\text{F}$
TS0		Storage vessel minimum temperature	$^{\circ}\text{F}$

## Outputs

<u>Variable/Port</u>		<u>Description</u>	<u>Units</u>
EC1		Stored energy (state) for cell 1 (hot side)	kwh
EC2		Stored energy (state) for cell 2 (cold side)	kwh
M	2	Outlet mass flow rate (-ML)	lb/hr
MP	2	Maximum discharge rate	kw
TS1, TS2		Average temperatures for cells 1 and 2	$^{\circ}\text{F}$
T	2	Air exit temperature	$^{\circ}\text{F}$
WA		Required storage media mass	lb
CC0		Storage device capital cost/year	\$
HF		Convective heat transfer coefficient	$\text{kwh}/\text{ft}^2 - ^{\circ}\text{F}$
U		Unit thermal conductance	$\text{kwh}/\text{ft}^2 - ^{\circ}\text{F}$
P	2	Charge rate into heat exchanger	kw
E1, E2		Energy stored at start and end of melt	kwh
PM		Maximum allowable charge rate	kw
EF	2	Output product efficiency	-
RT		Thermal resistance	$^{\circ}\text{F}/\text{kw}$
P0		Discharge power taken from heat exchanger	kw
T0		Discharge cycle output temperature	$^{\circ}\text{F}$
EF0		Discharge cycle efficiency	-

## Statistics

TSU		Maximum storage temperature	$^{\circ}\text{F}$
TSL		Minimum storage temperature	$^{\circ}\text{F}$
ME		Maximum stored energy	kwh
MT		Maximum exit temperature	$^{\circ}\text{F}$

The default values assume use of paraffin wax as the phase change storage medium. (In reality, paraffin wax may not be applicable to temperatures as high as 600°F. The selection of a phase change medium involves careful consideration of a number of factors [see Reference 1]). The heat exchanger geometric parameters, i.e., tube number, diameter, etc., and heat exchanger cost estimates are based on the baseline phase change storage device developed in Reference 1, but scaled down to reflect expected mass flow rates and required media mass. Although these data were developed for a different application (50 MWe, 6 hour storage, average temperature = 786°C), they can be considered representative until detail design data is available.

---

1. "Advanced Thermal Energy Storage," BEC/EPRI RP 788-1, July 1976.

## Calculation Sequence

### 1) Initial Calculations

$$MA = \frac{PD * ST * 0.5}{XD * H + CP1 * DTD}$$

$$CC0 = (CSA + CSB * ST) * PD / LE$$

$$E1 = MA * CP1 * (TMT - T01)$$

$$E2 = MA * [H + CP1 * (TMT - T01)]$$

$$T3 = TS0 = TA$$

$$A = (D * DEL + DEL ** 2) / 5.$$

$$RB(1) = D/2, RB(i+1) = \text{SQRT}(RB(i)**2 + A) \quad i=1,5$$

$$RN(1) = \text{SQRT}((RB(i+1)**2 + RB(i)**2) / 2)$$

$$RT = \frac{D}{2 * k} \sum_{i=1}^4 \text{LN} \left( \frac{RN(i+1)}{RN(i)} \right)$$

### 2) Storage Temperature (see Figure 7.16-2)

$$TS = \begin{cases} T01 + \frac{E}{MA * CP1} & \text{if } E < E_1 \\ TMT & \text{if } E_1 \leq E \leq E_2 \\ T01 + \frac{\left( \frac{E}{MA} - H \right)}{CP1} & \text{if } E > E_2 \end{cases}$$

where  $TS = TS1$  and  $E = E1$  for storage cell 1 and similarly for cell 2.

### 3) HX Exit Temperature Calculations

$$M2 = M1$$

$$P2 = 0$$

$$PX = 0$$

3) Cont.

$$T2 = TS2 - (TS1 - TS2)/2$$

$$\Delta T = TS1 - TS2$$

If  $M_L = 0$ , GO TO 7)

4) Convective Heat Transfer Coefficient<sup>1</sup>

$$HF = \frac{KF}{D} \left[ 0.0215 * \left( \frac{M1}{NT} * \frac{4}{MU * PI * D} \right)^{0.8} * \left( \frac{CPF * MU}{KF} \right)^{0.6} \right]$$

5) Thermal Conductance

$$U = \left\{ \frac{1}{HF} + RT \right\}^{-1}$$

$$UA = U * PI * D * L * NT / (CPF * M1 * 2)$$

6) Exit Temperature and Charge Rate (See Equation A2. in Appendix)

$$TX = T1 - \Delta T - (1. - EXP(-UA)) * (T1 - TS1 - \Delta T/2 - \Delta T/UA)$$

$$T2 = TX - \Delta T - (1. - EXP(-UA)) * (TX - (TS1 + TS2)/2 - \Delta T/UA)$$

$$P2 = M1 * CPF * (T1 - T2)$$

$$PX = M1 * CPF * (T1 - TX)$$

7) HY Exit Temperature Calculations

$$T0 = TS1 + \Delta T/2$$

$$P0 = 0.$$

$$PY = 0.$$

If  $M3 = 0$  GO TO 11)

<sup>1</sup> Kays, W. M., Convective Heat and Mass Transfer, McGraw Hill, N.Y., 1966, p. 173.

8) Convective Heat Transfer Coefficient

$$HF\theta = \frac{KF}{D} \left( .0215 * \left( \frac{M3}{NT} * \frac{4}{MU * PI * D} \right)^{0.8} * \left( \frac{CPF * MU}{KF} \right)^{0.6} \right)$$

9) Thermal Conductance

$$U\theta = \left( \frac{1}{HF\theta} + RT \right)^{-1}$$

$$UA = U\theta * PI * D * L * NT / (CPF * M3 * 2)$$

10) Exit Temperature and Discharge Rate (See Equation A3. in Appendix)

$$TY = T3 + \Delta T - (1. - EXP(-UA)) * (T3 - TS2 + \Delta T / 2 + \Delta T / UA)$$

$$T\theta = TY + \Delta T - (1. - EXP(-UA)) * (TY - (TS1 + TS2) / 2 + \Delta T / UA)$$

$$P\theta = M3 * CPF * (T\theta - T3)$$

$$PY = M3 * CPF * (T\theta - TY)$$

11) Energy Deposited

$$\dot{EC}1 = PX - NU * EC1 - PY - BE * (EC1 - EC2)$$

$$\dot{EC}2 = (P2 - PX) - NU * EC2 - (P\theta - PY) + BE * (EC1 - EC2)$$

If  $T2 \geq TEM$ , WRITE DIAGNOSTIC

12) Maximum Allowable Mass Flow Rate

$$MDM = PD / (CPF * \theta TD)$$

13) Maximum Allowable Charge Rate

$$PM = MDM * CPF * (T1 - TA)$$

## 14) Charging and Discharging Efficiency

$$EFF = 1$$

$$\text{If } T2 > TS0 \quad EFF = \frac{T2 - TS0}{T1 - TA}$$

$$EF0 = 1$$

$$\text{If } T3 > TS0 \quad EF0 = \frac{T0 - TA}{T3 - TS0}$$

$$MP2 = \text{MIN} (MP1, PM) * EFF$$

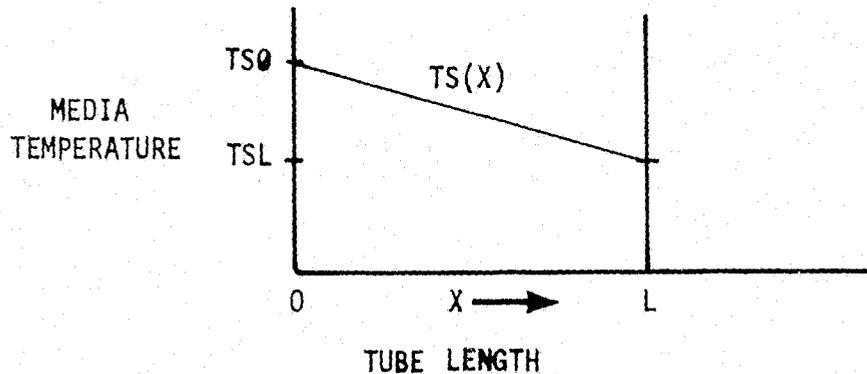
$$EF2 = EF1 * EFF$$

## 15) Compute Statistics and Cost Summation

Appendix: Temperature Equations for a Media with Constant Gradient

Assumptions

1) Constant Gradient Media Temperature:



2) Working Fluid Differential Equation:

$$A1. \quad \frac{\partial T_f}{\partial X} = \frac{UA}{L} (TS - T_f) \quad 0 < x < L$$

Main Results: Exit temperature in the charging and discharging cycles are given by

$$A2. \quad T_f(L) = T_f(0) + \Delta TS - (1 - \exp(-UA)) * \left( T_f(0) - TS0 + \frac{\Delta TS}{UA} \right)$$

$$A3. \quad T_f(0) = T_f(L) - \Delta TS - (1 - \exp(-UA)) * \left( T_f(L) - TSL - \frac{\Delta TS}{US} \right)$$

where  $\Delta TS = TSL - TS0$ .

Proof: Multiplying A1. by  $\exp(UA \cdot X/L)$  and recombining terms yields:

$$A4. \quad \frac{\partial}{\partial X} \left( \exp(UA \cdot X/L) * T_f \right) = \frac{UA}{L} * \exp(UA \cdot X/L) * TS(X).$$

Integrating A4. and substituting  $TS(X) = TS0 + \frac{\Delta TS}{L} * X$  yields

$$\begin{aligned}
 \text{A5. } T_f(X) &= \exp(-UA*X/L)*T_f(0) + \frac{UA}{L} \int_0^X \exp(-UA(x-y)/L)*TS(y)dy \\
 &= \exp(-UA*X/L)T_f(0) + (1-\exp(-UA*X/L))*(TS_0 - \Delta TS/UA) \\
 &\quad + \frac{\Delta TS}{L} * X
 \end{aligned}$$

Recombining terms in A5. and letting  $X=L$  yields A2. Equation A3. follows from A2. by symmetry, i.e., substitute in A2:

$T_f(0)$  for  $T_f(L)$

$T_f(L)$  for  $T_f(0)$

$TSL$  for  $TS_0$

$TS_0$  for  $TSL$ .

SUBROUTINE HX ENTRY POINT 001065

STORAGE USED CODE(1) 001517; DATA(0) 000143; BLANK COMMON(2) 000000

## COMMON BLOCKS

```

0003 C IMPL 000002
0004 C TIME 000001
0005 C SIMUL 000010
0006 C COST 000002

```

## EXTERNAL REFERENCES (BLOCK, NAME)

```

0007 SQR1
0010 ALOG
0011 XPRR
0012 EXP
0013 NWDUS
0014 NIO2%
0015 NERR3%

```

## STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

```

0001 000301 100L      0000 000034 1010F      0001 000514 200L      0001 000236 205G      0001 000264 214G
0001 000637 300L      0001 000714 500L      0000 R 000016 A      0006 R 000000 CCI      0006 R 000001 CMI
0000 R 000020 DELT      0005 000000 DUM      0000 R 000033 EFF      0000 R 000030 HFO      0000 I 000017 I
0003 I 000001 ICNT      0003 I 000000 IMPL      0000 000107 INJPS      0000 R 000000 HDM      0000 R 000014 PI
0000 R 000023 PX        0000 R 000027 PY        0000 R 000001 RB      0000 R 000007 RN      0000 R 000025 TEMP
0004 R 000000 TIME      0005 R 000007 TMAX      0000 R 000015 TMAX1      0000 R 000022 TSC      0000 R 000021 TSH
0000 R 000026 TX        0000 R 000032 TY        0000 R 000024 UA      0000 R 000031 UO

```

```

00100      1*      CHX
00101      2*
00101      3*      SUBROUTINE HX(IE1,DE1,IE1,EC2,DE2,IE2,M2,MP2,TS1,TS2,T2,MA,
00101      4*      1CC,HF,U,P,E1,E2,PH,EF2,PO,TO,EFO,R,TSU,TSL,ME,MT,NU,ST,BE,T01,OTD
00101      5*      2      ,PD,TEM,XD,EF1,MP1,CP1,H,TMT,CPF,KF,HU,NT,D,L,DEL,K,T1
00101      6*      3      ,M1,CM,CSA,CSB,LE,M3,T3,TA,TSO)
00101      7*      C
00101      8*      C      PURPOSE PERFORMANCE OF ADIABATIC HEAT EXCHANGER DURING CHARGE
00101      9*      C
00101      10*      C      CYCLE
00101      11*      C      METHOD HEAT STORAGE MEDIA ASSUMED TO CONTAIN NO TEMPERATURE
00101      12*      C
00101      13*      C      GRADIENTS. ENERGY DEPOSITED IS A FUNCTION OF TEMPERATURE
00101      14*      C
00101      15*      C      AND THERMAL CONDUCTANCE
00101      16*      C

```

```

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HX





```

00202 131* C COMPUTE THERMAL RESISTANCE OF MEDIA 000221
00202 132* C 000221
00203 133* C RB(1)=0/2.0 000230
00203 134* C 000230
00204 135* C DO 20 I=1,5 000236
00207 136* C RB(I+1)=SQRT(RB(I)**2+A) 000236
00210 137* C 20 RN(I)=SQRT((RB(I+1)**2+RB(I)**2)/2.0) 000245
00210 138* C 000245
00212 139* C R=0.0 000260
00212 140* C 000260
00213 141* C DO 30 I=1,4 000264
00216 142* C 30 R=R+ALOG(RN(I+1)/RN(I)) 000264
00216 143* C 000264
00220 144* C R=R*0/2.0/G/K 000274
00220 145* C 000274
00222 146* C STORAGE TEMPERATURES 000274
00220 147* C 000274
00221 148* C 100 TS1=T*1 000301
00221 149* C 000301
00222 150* C IF(EC1.LT.E1) TS1= T01+ EC1/(MA*CP1) 000302
00224 151* C IF(EC1.GT.E2) TS1= T01+ (EC1/MA - H)/CP1 000315
00226 152* C TS2=T*2 000327
00227 153* C IF(EC2.LT.E1) TS2= T01+ EC2/(MA*CP1) 000331
00231 154* C IF(EC2.GT.E2) TS2= T01+ (EC2/MA - H)/CP1 000341
00231 155* C 000341
00233 156* C DELT= TS1 - TS2 000353
00234 157* C TSH= TS1+ .5*DELT 000356
00235 158* C TSC= TS2 - .5*DELT 000362
00235 159* C 000362
00236 160* C T2= TSC 000365
00237 161* C M2=M1 000366
00240 162* C P =0.0 000370
00241 163* C PX=0.0 000371
00242 164* C U=1.0/R 000372
00242 165* C 000372
00243 166* C IF(M1.LT.0.001)60 TO 200 000375
00243 167* C 000375
00243 168* C CONVECTIVE HEAT TRANSFER COEFFICIENT 000375
00243 169* C 000375
00245 170* C HF =KF/D*(0.0215*(M1/NT+4.0/MU/PI/D)**0.8+(CPF*MU/KF)**0.6) 000400
00245 171* C 000400
00245 172* C UNIT THERMAL CONDUCTANCE 000400
00245 173* C 000400
00246 174* C U = 1.0/(1.0/HF+R) 000432
00247 175* C UA= U*PI*D*L*NT/(M1*CPF*2.) 000440
00250 176* C TEMP= DELT/UA 000452
00251 177* C UA= 1. - EXP(-UA) 000455
00251 178* C 000455
00251 179* C EXIT TEMPERATURE 000455
00251 180* C 000455
00252 181* C TX= T1 - DELT - UA*(T1-TSH-TEMP) 000463
00253 182* C T2= TX- DELT - UA*(TX-(TS1+TS2)*.5-TEMP) 000473
00253 183* C 000473
00253 184* C CHARGE RATE 000473
00253 185* C 000473
00254 186* C P =M1*CPF*(T1-T2) 000504
00255 187* C PX = M1*CPF*(T1-TX) 000507

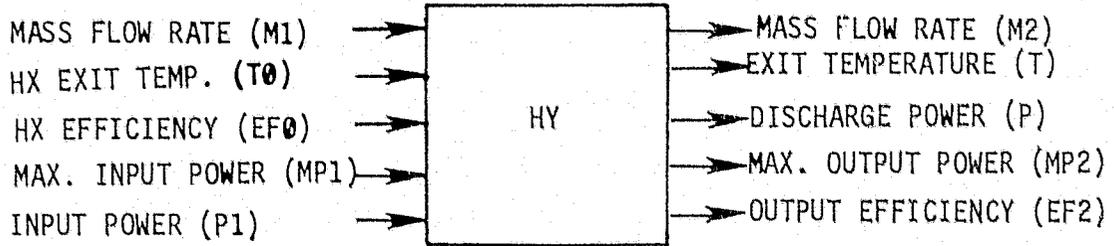
```

HX



00322	245*	C			000763
00322	246*	C		STATISTICS	000763
00322	247*	C			000763
00323	248*			IF(I*PL+LE-1)RETURN	000766
00323	249*	C			000766
00325	250*			TSU =AMAX1(TSU,TS1)	000775
00326	251*			TSL =AMIN1(TSL,TS2)	001003
00327	252*			TE = AMAX1(TE, EC1+EC2)	001011
00330	253*			MT =AMAX1(MT ,T2)	001020
00330	254*	C			001020
00331	255*			IF(TIME.LT.TMAX)RETURN	001026
00331	256*	C			001026
00333	257*			CCI =CCI+CC	001035
00334	258*			CPI=CPI+CK	001040
00335	259*			CM= CM/PP	001043
00335	260*	C			001043
00336	261*			RETURN	001046
00336	262*	C			001046
00337	263*			1010 FORMAT(1H0,22HX EXIT TEMPERATURE ,F12.3	001516
00337	264*			1 +35H GREATER THAN MAXIMUM ALLOWABLE ,F12.3)	001516
00337	265*	C			001516
00340	266*			END	001516

## 7.17 ADIABATIC HEAT EXCHANGER - DISCHARGING CYCLE



HY is the discharge cycle complement to HX. All the calculations to obtain the exit temperature and heat exchange power deposited or withdrawn are done in HX. The results are then passed to HY for summary.

## Inputs

<u>Parameter/Port</u>	<u>Description</u>	<u>Units</u>
M 1	Air mass flow rate from storage	lb/hr
T0	Exit temperature from HX	°F
P 1	Discharge power from storage	kw
EF0	Discharge cycle efficiency from HX	-
MP 1	Maximum power from storage	kw

## Outputs

<u>Variable/Port</u>	<u>Description</u>	<u>Units</u>
M 2	Exit air mass flow rate (=M1)	lb/hr
T	Exit temperature (=T0)	°F
P 2	Discharge power	kw
MP 2	Maximum discharge power	kw
EF 2	Output product efficiency	-

## Statistics

TL	Minimum exit temperature	°F
TU	Maximum exit temperature	°F
SP	Total energy discharged	kwh

## Calculation Sequence

1)  $M2 = M1$

$T = T0$

$MP2 = MP1 * EF0$

$EF2 = EF0$

$P2 = P1 * EF0$

2) Compute Statistics

SUBROUTINE HY ENTRY POINT 000064

STORAGE USED CODE(1) 000135; DATA(0) 000017; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CIMPL 000001  
0004 CSIMUL 000007

EXTERNAL REFERENCES (BLOCK, NAME)

0005 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000007 100L 0004 000000 DUM 0003 I 000000 IMPL 0000 000002 INJPS 0004 R 000006 TINC

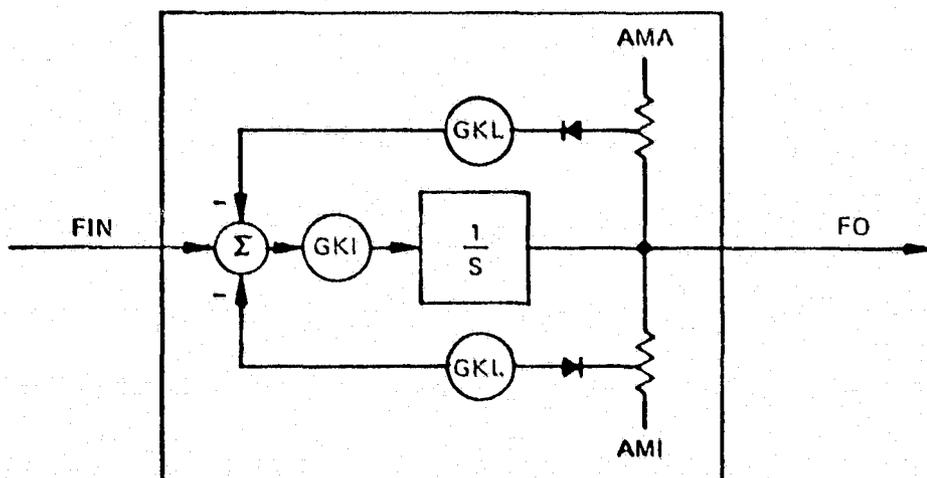
00100	1*	CHY		000000
00101	2*		SUBROUTINE HY(M2,T,P2,MP2,EF2,TL,TU,SP,M1,TO,P1,EFO,MP1)	000000
00101	3*	C		000000
00101	4*	C	PURPOSE PERFORMANCE OF ADIABATIC HEAT EXCHANGER DURING DISCHARGE	000000
00101	5*	C		000000
00101	6*	C	CYCLE	000000
00101	7*	C		000000
00101	8*	C	METHOD COMPUTE EXIT CONDITIONS USING HEAT EXCHANGER STATE	000000
00101	9*	C		000000
00101	10*	C	DETERMINED IN HX	000000
00101	11*	C		000000
00101	12*	C	WRITEN BY F. O. MAHONY VERSION 1, MARCH 27 1977	000000
00101	13*	C		000000
00101	14*	C	CALL SEQUENCE	000000
00101	15*	C	OUTPUTS	000000
00101	16*	C	M2 - EXIT AIR MASS FLOW RATE (=M1), LB/HR	000000
00101	17*	C	T - EXIT TEMPERATURE (=TO), DEG F	000000
00101	18*	C	P2 - TOTAL DISCHARGE POWER, KW	000000
00101	19*	C	MP2 - MAXIMUM DISCHARGE POWER, KW	000000
00101	20*	C	EF2 - OUTPUT PRODUCT EFFICIENCY	000000
00101	21*	C		000000
00101	22*	C	STATISTICS	000000
00101	23*	C	TL - MINIMUM EXIT TEMPERATURE, DEG F	000000
00101	24*	C	TU - MAXIMUM EXIT TEMPERATURE, DEG F	000000
00101	25*	C	SP - TOTAL ENERGY DISCHARGED, KWH	000000
00101	26*	C		000000
00101	27*	C	INPUTS	000000
00101	28*	C	M1 - AIR MASS FLOW RATE FROM STORAGE, LB/HR	000000
00101	29*	C	TO - EXIT TEMPERATURE FROM HX, DEG F	000000
00101	30*	C	P1 - DISCHARGE POWER FROM STORAGE, KW	000000

HY

CO101	31*	C	EFO - DISCHARGE CYCLE EFFICIENCY	000000
CO101	32*	C	MPI - MAXIMUM POWER FROM STORAGE, KW	000000
CO101	33*	C		000000
CO103	34*		COMMON /CIMPL/IMPL /CSIMUL/DUM(6),TINC	000000
CO103	35*	C		000000
CO104	36*		RFAL M2,MP2,M1,MPI	000000
CO104	37*	C		000000
CO105	38*		IF(IMPL.GT.0)GO TO 100	000000
CO105	39*	C		000000
CO107	40*		TU =0.0	000002
CO110	41*		SP =0.0	000003
CO110	42*	C		000003
CO111	43*		TL =1.0E10	000004
CO112	44*	100	M2 =M1	000007
CO113	45*		T =T0	000010
CO114	46*		P2 =P1*EFO	000012
CO115	47*		MP2=MP1*EFO	000015
CO116	48*		EF2=EFO	000020
CO116	49*	C		000020
CO117	50*		IF(IMPL.LE.1)RETURN	000022
CO117	51*	C		000022
CO121	52*		TL =AMIN1(TL ,T )	000031
CO122	53*		TU =AMAX1(TU ,T )	000037
CO122	54*	C		000037
CO123	55*		SP =SP +P2*TINC/2.0	000045
CO123	56*	C		000045
CO124	57*		RETURN	000052
CO125	58*		END	000134

HY

## 7.18 INTEGRATOR WITH SATURATION



### Inputs

<u>Parameter/Port</u>	<u>Description</u>
FIN	Input
GKI	Integration gain
GKL	Saturation limiter gain
AMA	Upper limit of output (Default = $10^{36}$ )
AMI	Lower limit of output (Default = $-10^{36}$ )

### Outputs

<u>Variable/Port</u>	<u>Description</u>
F0	Output (state)

### Calculation Sequence

- $F0 = GKI * [ FIN - GKL * (F0 - AMA) ]$  if  $F0 > AMA$
- $F0 = GKI * FIN$  if  $AMI \leq F0 \leq AMA$
- $F0 = GKI * [ FIN - GKL * (F0 - AMI) ]$  if  $F0 < AMI$

SUBROUTINE IT ENTRY POINT 000051

STORAGE USED CODE(1) 000067; DATA(0) 000007; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 NEPR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0000 R 000000 EPS 0000 000003 INJPS

```

00100 1* CIT 000000
00101 2* SUBROUTINE IT(FO,FODOT,IFO,FIN,GKI,GKL,AMA,AHI) 000000
00101 3* C VERSION 2. REVISED OCT 8 1976 000000
00101 4* C 000000
00101 5* C PURPOSE - SIMULATION OF AN INTEGRATOR WITH SATURATION 000000
00101 6* C 000000
00101 7* C 000000
00101 8* C METHOD - SEE CODING 000000
00101 9* C 000000
00101 10* C 000000
00101 11* C LIMITATIONS - EXCESSIVELY HIGH VALUES OF GKL MAY RESULT IN POOR 000000
00101 12* C STEADY STATE CONVERGENCE 000000
00101 13* C 000000
00101 14* C 000000
00101 15* C WRITTEN BY - ADAM LLOYD LATEST REVISION - NOV 75 000000
00101 16* C 000000
00101 17* C 000000
00101 18* C INPUT/OUTPUT LIST 000000
00101 19* C 000000
00101 20* C FO INTEGRATOR OUTPUT ANY OUTPUT STATE 000000
00101 21* C FODOT OUTPUT DERIVATIVE ANY OUTPUT DERIV 000000
00101 22* C IFO INTEGRATOR CONTROL --- PROGRAM VAR 000000
00101 23* C FIN FUNCTION INPUT ANY INPUT VAR 000000
00101 24* C GKI INTEGRATOR GAIN ANY INPUT PARAM 000000
00101 25* C GKL DERIVATIVE LIMITER GAIN ANY INPUT PARAM 000000
00101 26* C AMA UPPER LIMIT OF OUTPUT ANY INPUT PARAM 000000
00101 27* C WHERE DERIV. LIMITER STARTS 000000
00101 28* C AHI LOWER LIMIT OF OUTPUT ANY INPUT PARAM 000000
00101 29* C WHERE DERIV. LIMITER STARTS 000000
00103 30* EPS=FTN 000000
00103 31* C --- PROVIDE DEFAULTS THAT ELLIMINATE SATURATION 000000
00104 32* IF(AMA.EQ..999999)AMA=1.E36 000001
00106 33* IF(AHI.EQ..999999)AHI=-1.E36 000006
00110 34* IF(FO.GT.AMA)EPS = FIN - GKL*(FO-AMA) 000013
00112 35* IF(FO.LT.AHI)EPS = FIN - GKL*(FO-AHI) 000024

```

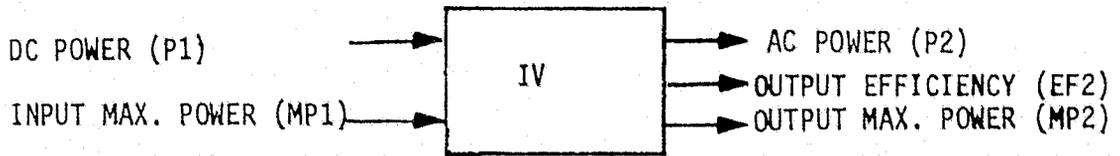


00114 36\*  
00116 37\*  
00117 38\*

IF(IFO.NE.O)F000T=GKI\*EPS  
RETURN  
END

000035  
000042  
000066

## 7.19 DC-AC INVERTER



This component models a solid state inverter/transformer. Power losses due to resistive heating and contact potential loss are modeled. A step-up transformer may also be needed to boost output voltage up to that of the bus. Default parameter values are based on rated power = 200 kw.

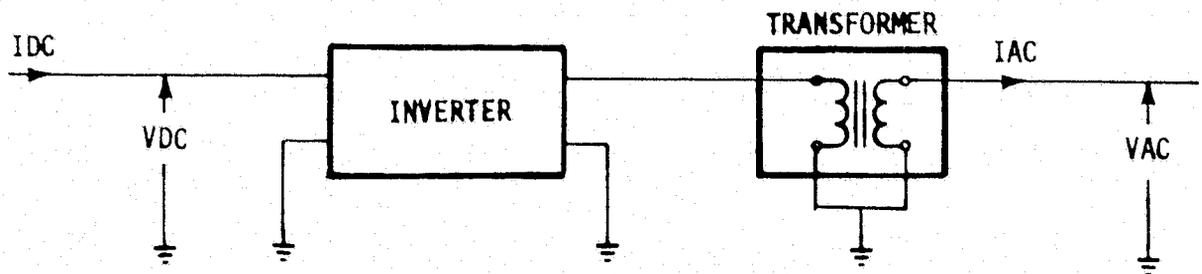


FIGURE 7.19 INVERTER FUNCTIONAL DIAGRAM

## Inputs

<u>Parameter/Port</u>	<u>Description</u>	<u>Units</u>
P 1	DC Input power	kw
RT	Transformer resistance (D = 0)	ohms
VDC	Rated DC voltage (D = 100)	volts
DI	Inverter contact potential (D = 0)	volts
RI	Inverter resistance (D = 0.005)	ohms
RAP	Rated input power	kw
EF 1	Input product efficiency	-
MP 1	Maximum input power	kw
CC	Inverter cost/year	\$

## Outputs

<u>Variable/Port</u>	<u>Description</u>	<u>Units</u>
P 2	AC output power	kw
IDC	DC Input current	amps
PL	Power loss	kw
EF 2	Output product efficiency	-
MP 2	Maximum output power	kw

D - Default values supplied.

Calculation Sequence

If  $P_1 \leq 0$ ,  $P_2 = IDC = PL = 0$ ,  $EFF = 1$  and go to 3)

- 1) Input and output current

$$IDC = P_1 * 1000 / VDC$$

$$IAC = \sqrt{6} * IDC / \pi$$

- 2) Power loss and output power

$$PL = (IDC * (DI + RI * IDC) + \sqrt{3} * RT * IAC^2) / 1000$$

$$P_2 = P_1 - PL$$

$$EFF = P_2 / P_1$$

$$P_2 \leq 0 \quad \Rightarrow \quad \text{Diagnostic, } EFF = 1$$

- 3) Efficiency and maximum power

$$EF_2 = EF_1 * EFF$$

$$MP_2 = \text{MIN}(MP_1, RAP) * EFF$$

- 4) Compute Costs



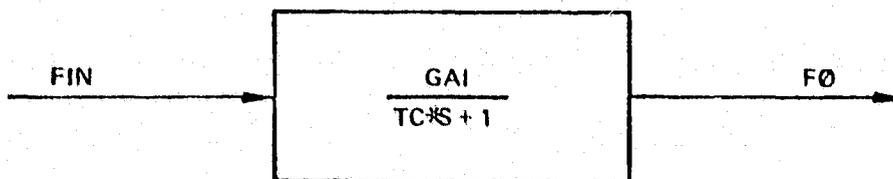
```

GO101 24* C RAP -RATED OUTPUT POWER, KW 000000
GO101 25* C EF1 -INPUT PRODUCT EFFICIENCY 000000
GO101 26* C MPI -MAXIMUM INPUT POWER, KW 000000
GO101 27* C CC -INVERTER COST/YEAR 000000
GO101 28* C 000000
GO103 29* COMMON /CIMPL/IMPL,ICNT/CTIME/TIME/CSIMUL/DUM(7),TMAX/COST/CCI 000000
GO104 30* REAL IDC,MP2,MPI,IAC 000000
GO105 31* DATA PI/3.14159/ 000000
GO105 32* C 000000
GO107 33* IF(IMPL.GT.0) GO TO 100 000000
GO111 34* IF(RT.EQ..99999)RT=0. 000002
GO113 35* IF(VDC.EQ..99999)VDC=100. 000006
GO115 36* IF(DI.EQ..99999)DI=0. 000013
GO117 37* IF(RI.EQ..99999)RI=.005 000017
GO121 38* TMAX1=TMAX*.99999 000024
GO121 39* C 000024
GO121 40* C COMPUTE INPUT AND OUTPUT CURRENT 000024
GO121 41* C 000024
GO122 42* 100 IF(P1.GT.0.)GO TO 200 000030
GO124 43* P2=0. 000032
GO125 44* IDC=0. 000033
GO126 45* PL=0. 000034
GO127 46* EFF2=EFF1 000035
GO130 47* MP2=AMIN1(MPI,RAP) 000037
GO131 48* GO TO 400 000045
GO132 49* 200 IDC=P1*1000./VDC 000047
GO133 50* IAC=SQRT(6.)*IDC/PI 000052
GO133 51* C 000052
GO133 52* C POWER LOSS AND OUTPUT POWER 000052
GO133 53* C 000052
GO134 54* PL=(IDC*(DI+RI+IDC)+SQRT(3.)*RT*IAC*IAC)/1000. 000060
GO135 55* P2=P1-PL 000075
GO136 56* EFF=P2/P1 000077
GO136 57* C 000077
GO136 58* C EFFICIENCY AND MAXIMUM POWER 000077
GO136 59* C 000077
GO137 60* EF2=EF1*EFF 000101
GO140 61* MP2=AMIN1(MPI,RAP) 000103
GO141 62* MP2=MP2*EFF 000111
GO142 63* IF(P2.GT.0.)GO TO 400 000114
GO142 64* C 000114
GO144 65* EF2=EF1 000117
GO145 66* MP2=AMIN1(MPI,RAP) 000121
GO146 67* IF(IMPL.EQ.2)WRITE(6,208)PL,P1 000123
GO153 68* 208 FORMAT(1H0,14HIV POWER LOSS ,F12.3,21H EXCEEDS INPUT POWER ,F12.3, 000135
GO153 69* 128H CHECK RATED DC VOLTAGE VDC ) 000135
GO154 70* IF(IMPL.EQ.2)ICNT=ICNT+1 000135
GO156 71* P2=0. 000143
GO156 72* C 000143
GO157 73* 400 IF(IMPL.LE.1)RETURN 000145
GO161 74* IF(TIME.LT.TMAX1)RETURN 000153
GO163 75* CCI=CCI+CC 000162
GO164 76* RETURN 000165
GO165 77* END 000260

```

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## 7.20 FIRST ORDER LAG



### Inputs

<u>Parameter/Port</u>	<u>Description</u>
FIN	Input quantity
GAI	Gain
TC	Time constant <sup>1</sup> (hours)
F0	Output variable (state)

### Calculation Sequence

$$\dot{F0} = (GAI * FIN - F0) / TC$$

NOTE: d.c. gain = GAI; time constant = TC

infinite frequency gain = 0

pole location =  $\frac{1}{TC}$  rad/sec.

---

<sup>1</sup> If TC = 0, then F0 = FIN \* GAI

SUBROUTINE LA ENTRY POINT 000026

STORAGE USED CODE(1) 000045; DATA(0) 000010; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CIO 000003

EXTERNAL REFERENCES (BLOCK, NAME)

0004 HERR34

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000010 1DL 0003 000002 1DIAG 0000 000000 1MIPS 0003 000000 1READ 0003 000001 1WRITE

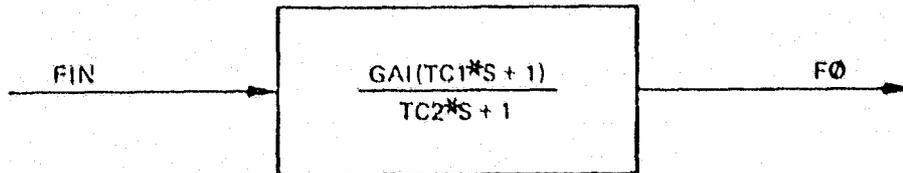
```

00100 1*   CLA
00101 2*   SUBROUTINE LA(FO,FODOT,IFO,FIN,GAI,TC)
00101 3*   C
00101 4*   C PURPOSE - TO SIMULATE FIRST ORDER LAG      FO      GAI
00101 5*   C                                     -----
00101 6*   C                                     FIN      (1.+TC*S)
00101 7*   C
00101 8*   C
00101 9*   C METHOD - SEE CODING
00101 10*  C
00101 11*  C
00101 12*  C WRITTEN BY - ADAM LLOYD          LATEST REVISION   NOV 75
00101 13*  C
00101 14*  C
00101 15*  C INPUT/OUTPUT LIST
00101 16*  C
00101 17*  C FO          TRANSFER FUNCTION OUTPUT          ANY      OUTPUT STATE
00101 18*  C FODOT      TRANSFER FUNCTION OUTPUT "  Y.    ANY      OUTPUT STATE
00101 19*  C IFO        INTEGERATOR CONTROL              ---      PROGRAM VAR
00101 20*  C FIN        TRANSFER FUNCTION INPUT          ANY      INPUT VAR
00101 21*  C GAI        TRANSFER FUNCTION GAIN          ---      INPUT PARAM
00101 22*  C TC         TIME CONSTANT                   SECS     INPUT PARAM
00103 23*  COMMON/CIO/IREAD,IWRITE,IDIAG
00104 24*  IF(TC.NE.C.) GO TO 10
00106 25*  FC= GAI*FIN
00107 26*  RETURN
00110 27*  10 IF(IFO.NE.O) FODOT=(GAI*FIN-FO)/TC
00112 28*  RETURN
00113 29*  END
    
```

RCS 40180-2

LA

## 7.21 LEAD LAG



### Inputs

<u>Parameter/Port</u>	<u>Description</u>
FIN	Input quantity
TC1	Numerator time constant (hours)
TC2	Denominator time constant (hours)
GAI	Gain

### Outputs

<u>Variable/Port</u>	<u>Description</u>
X1	Intermediate quantity (state)
F0	Output quantity (variable)

### Calculation Sequence

$$F0 = (X1 + FIN*TC1*GAI)/TC2$$

$$\dot{X1} = GAI*FIN - F0$$

NOTE: d.c. gain = GAI

$$\text{infinite gain} = \frac{GAI*TC1}{TC2}$$

$$\text{zero location} = -\frac{1}{TC1}, \text{ rad/sec}$$

$$\text{pole location} = -\frac{1}{TC2}, \text{ rad/sec}$$

SUBROUTINE LL ENTRY POINT 000022

STORAGE USED CODE(1) 000031; DATA(0) 000004; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 C10 000003

EXTERNAL REFERENCES (BLOCK, NAME)

0004 NERR3S

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0003 000002 IDIAG 0000 000000 INJPS 0003 000000 IREAD 0003 000001 IWRITE

00100	1*	CLL				000000
00101	2*		SUBROUTINE LL(X1,X1DOT,IX1,FO,FIN,TC1,TC2,GAI)			000000
00101	3*	C				000000
00101	4*	C	PURPOSE - TO SIMULATE LEAD LAG TRANSFER FUNCTION			000000
00101	5*	C				000000
00101	6*	C				000000
00101	7*	C				000000
00101	8*	C				000000
00101	9*	C				000000
00101	10*	C				000000
00101	11*	C	METHOD - SELF EXPLANATORY			000000
00101	12*	C				000000
00101	13*	C				000000
00101	14*	C	LIMITATIONS - NONE			000000
00101	15*	C				000000
00101	16*	C				000000
00101	17*	C	WRITTEN BY - ADAM LLOYD LATEST REVISION NOV 75			000000
00101	18*	C				000000
00101	19*	C				000000
00101	20*	C	INPUT/OUTPUT LIST			000000
00101	21*	C				000000
00101	22*	C	X1	STATE VARIABLE	ANY	OUTPUT STATE
00101	23*	C	X1DOT	STATE VARIABLE DERIVATIVE	ANY	OUTPUT STATE
00101	24*	C	IX1	INTEGRATOR CONTROL	---	PROGRAM VAR
00101	25*	C	FO	TRANSFER FUNCTION OUTPUT	ANY	OUTPUT VAR
00101	26*	C	FIN	TRANSFER FUNCTION INPUT	ANY	INPUT VAR
00101	27*	C	TC1	TIME CONSTANT (NUMERATOR)	SECS	INPUT PARAM
00101	28*	C	TC2	TIME CONSTANT (DENOMINATOR)	SECS	INPUT PARAM
00101	29*	C	GAI	TRANSFER FUNCTION GAIN	---	INPUT PARAM
00103	30*		COMMON/C10/IREAD,IWRITE,IDIAG			000000
00104	31*		FO=(X1*FIN*TC1*GAI)/TC2			000000



00105  
00107  
00110

32\*  
33\*  
34\*

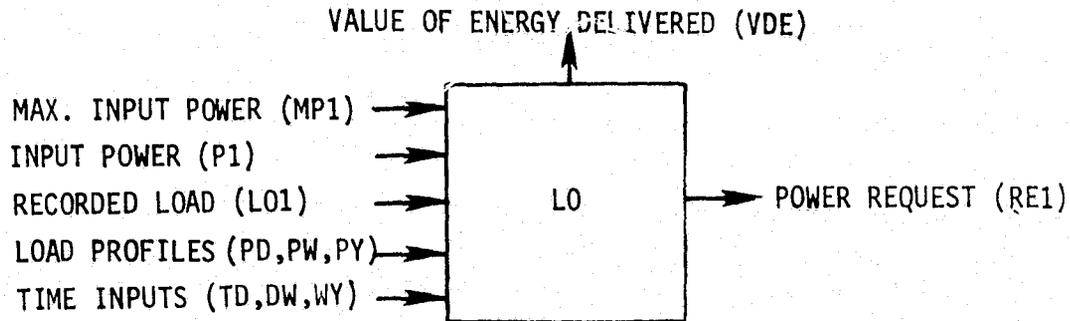
IF(IX1.NE.0)X100T= GAI\*FIN-F0  
RETURN  
END

000005  
000013  
000030

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LL

## 7.22 ELECTRICAL LOAD



This component represents electrical load either by a user-specified data file time history or by a set of random numbers with user-specified daily, weekly, and yearly average profiles and user-specified random variation. It also computes the value of the power delivered to the load by the system. This value delivered is determined from a user-specified value per kwh. This value may be input in tabular form as a function of time of day, time of year, or any other system parameter.

If the user selects to have the electrical load represented by random numbers, then the load (L02) is generated from the following equation:

### Basic Equation

$$L02 = [ PD(TD) + CN(t) ] * PW(DW) * PY(WY) * NC$$

where

PD, PW, PY are the daily, weekly, and yearly profiles, respectively, and TD, DW, WY are the time of day, day of the week, and week of the year, respectively. NC is a normalizing constant.

CN is a colored noise term with user-specified correlation time, standard deviation and mean.

<u>Tables</u>	<u>Description</u>	<u>Units</u>
PD	Daily profile (tabular with TD)	kw
PW	Weekly profile (tabular with DW)	arbitrary
PY	Yearly profile (tabular with WY)	arbitrary

### Inputs

#### Parameter/Port

P	1	Power delivered	kw
MP	1	Maximum Input Power deliverable ( $D = 1 \times 10^{10}$ )	kw
NC		Normalizing constant	
VE		Value of Electrical Energy	\$/kwh
LØ	1	Electrical load data file input	kw
TD		Time of day	-
DW		Day of week	-
WY		Week of year	-
CT		Correlation time of random noise	hr
MN,STD		Mean ( $D = 0$ ) and std. deviation of random noise	kw
EF	1	Input Power Efficiency	-

### Outputs

#### Variable/Port

RE	1	Power request	kw
VDE		Value of energy delivered (state)	\$
LØ	2	Electrical load	kw
TIM		Last time a random sample was used	hr
CN		Colored noise sample	kw

### Statistics

SRE		Total energy requested	kwh
SDE		Total energy delivered	kwh
PC		Percentage of load met	-

D - Default values supplied

## Calculation Sequence

1) Initialize CN(0) (first pass)

2) Check for data file input

    If L01 = .99999 go to 3)

    L02 = L01 and go to 5)

3) Generate colored noise CN

    If TIM = TIME go to 5)

$$A = \begin{cases} \exp(-\Delta/CT), & CT > 0, \Delta = \text{integration step size, hr} \\ 0, & CT = 0 \end{cases}$$

$$CN = A*CN+W,$$

Where W is white noise generated by RN with

$$\text{Mean} = MN * (1-A) \text{ and standard deviation} = \text{STD} * \sqrt{1-A^2}$$

4) Compute L02

$$L02 = (PD(TD) + CN) * PW(DW) * PY(WY) * NC$$

$$TIM = TIME$$

5) Power request and value delivered

$$RE = \text{MIN}(MP, L02)/EF1$$

6) Statistics

$$VDE = P1*VE$$

$$SRE = SRE + L02 * \Delta / 2$$

$$SDE = SDE + P1 * \Delta / 2$$

$$PC = 100. * SDE / SRE$$

SUBROUTINE LO ENTRY POINT 000344

STORAGE USED CODE(1) 000471; DATA(0) 000055; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CIMPL 000001  
 0004 CSIMUL 000010  
 0005 CTIME 000001  
 0006 COST 000006

EXTERNAL REFERENCES (BLOCK, NAME)

0007 RN  
 0010 TBLU1  
 0011 EXP  
 0012 SQRT  
 0013 NERR3

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000062	10L	0001	000070	100L	0001	000233	150L	0000	R	000005	A	0000	R	000000	AX			
0006	000000	CC	0006	R	000004	CDE	0006	000001	CM	0006	000002	CO	0006	R	000005	CRE			
0006	R	000003	CV	0000	R	000011	DLO	0004	000000	DUM	0003	I	000000	IMPL	0000	000022	INJPS		
0000	I	000001	ND	0000	I	000002	NW	0000	I	000003	NY	0010	R	000000	TBLU1	0005	R	000000	TIME
0004	R	000006	TINC	0004	R	000007	TMAX	0000	R	000004	TMAX1	0000	R	000010	W	0000	R	000012	WLO
0000	R	000006	WMN	0000	R	000007	WSD	0000	R	000013	YLO								

00100	1*	CLO		000002
00101	2*		SUBROUTINE LO (PD,PW,PY,VDE,DVD,IVD,RE,LO2,SRE,SDC,PC,TIMO,XN,	000002
00101	3*		1 TD,DM,WY,XNC,CT,XMN,STD,VE,LO1,PMAX,PO,EF)	000002
00101	4*	C		000002
00101	5*	C	PURPOSE GENERATE ELECTRICAL LOAD FROM DAILY, WEEKLY, YEARLY AND	000002
00101	6*	C	RANDOM PROFILE DATA AND EVALUATE PERFORMANCE STATISTICS	000002
00101	7*	C		000002
00101	8*	C	METHOD COLORED NOISE IS ADDED TO A MEAN DAILY PROFILE AND MULTIPLIED	000002
00101	9*	C	BY WEEKLY AND YEARLY WEIGHTING FCNS. POWER REQUESTED IS EITHER	000002
00101	10*	C	THE GENERATED LOAD OR THE MAX. POWER DELIVERABLE.	000002
00101	11*	C		000002
00101	12*	C	WRITTEN BY A.W.WARREN	000002
00101	13*	C	VERSION 1, MARCH 9 1977	000002
00101	14*	C	CALL SEQUENCE	000002
00101	15*	C	TABLES	000002
00101	16*	C	PD - MEAN DAILY PROFILE, KW	000002
00101	17*	C	PW - MEAN WEEKLY PROFILE, -	000002
00101	18*	C	PY - MEAN YEARLY PROFILE, -	000002
00101	19*	C		000002

00101	20*	C	OUTPUTS		000002
00101	21*	C	VDE - VALUE OF ENERGY DELIVERED (STATE), S		000002
00101	22*	C	DVD - DERIVATIVE OF VDE		000002
00101	23*	C	IVD - INDICATOR FOR VDE		000002
00101	24*	C	RE - POWER REQUEST, KW		000002
00101	25*	C	LO2 - ELECTRICAL LOAD DEMAND, KW		000002
00101	26*	C	SRE - SUM OF ENERGY DESIRED, KWH		000002
00101	27*	C	SDE - SUM OF ENERGY DELIVERED, KWH		000002
00101	28*	C	PC - CUMULATIVE PERCENT OF LOAD DELIVERED, -		000002
00101	29*	C	TIMO - LAST TIME A RANDOM SAMPLE WAS USED, HR		000002
00101	30*	C	XN - COLORED NOISE SAMPLE, KW		000002
00101	31*	C			000002
00101	32*	C	INPUTS		000002
00101	33*	C	TD - TIME OF DAY, HR		000002
00101	34*	C	DW - DAY OF WEEK (1-7)		000002
00101	35*	C	WY - WEEK OF YEAR (1-52)		000002
00101	36*	C	XNC - NORMALIZING CONSTANT, -		000002
00101	37*	C	CT - CORRELATION TIME OF RANDOM NOISE, HR		000002
00101	38*	C	XMN - MEAN OF RANDOM NOISE, KW		000002
00101	39*	C	STD - STANDARD DEVIATION OF RANDOM NOISE, KW		000002
00101	40*	C	VE - VALUE OF ELECTRICAL ENERGY, S/KWH		000002
00101	41*	C	LO1 - ELECTRICAL LOAD DATA FILE INPUT, XW		000002
00101	42*	C	PMAX - MAX. INPUT POWER DELIVERABLE, KW		000002
00101	43*	C	PO - POWER DELIVERED TO LOAD, KW		000002
00101	44*	C	EF - INPUT POWER EFFICIENCY		000002
00101	45*	C			000002
00103	46*		DIMENSION PD(1),PW(1),PY(1)		000002
00104	47*		REAL LO1,LO2		000002
00105	48*		COMMON /CIMPL/ IMPL /CSINHUL/ DUM(6),TINC,THAX/CTIME/TIME		000002
00106	49*		COMMON /COST/CC,CM,CO,CV,CDE,CRE		000002
00107	50*		DATA AX/.99999/		000002
00107	51*	C			000002
00107	52*	C	INITIALIZATION		000002
00107	53*	C			000002
00111	54*		ND = PD(2)		000002
00112	55*		NW = PW(2)		000011
00113	56*		NY = PY(2)		000020
00114	57*		IF(IMPL.GT.0) GO TO 10		000027
00116	58*		IF(XMN.EQ. .99999)XMN=0.		000032
00120	59*		THAX1 = THAX*.99999		000036
00121	60*		TIMO=-1.		000041
00122	61*		SRE =0.0		000043
00123	62*		SDE =0.0		000044
00124	63*		PC =0.0		000045
00125	64*		CALL RN(XN,AX,STD,XMN)		000046
00126	65*		IF(PMAX.EQ. .99999) PMAX = 1.E10		000054
00126	66*	C			000054
00126	67*	C	CHECK FOR DATA FILE INPUT		000054
00126	68*	C			000054
00130	69*		10 IF(LO1.EQ. .99999) GO TO 100		000062
00132	70*		LO2 = LO1		000064
00133	71*		GO TO 150		000066
00133	72*	C			000066
00133	73*	C	GENERATE COLORED NOISE SAMPLE XN		000066
00133	74*	C			000066
00134	75*		100 IF( TIMO.EQ.TIME) GO TO 150		000070
00136	76*		A=0.		000072

```

00137 77*      IF(CT.GT.G.) A = EXP(-TINC/CT)
00141 78*      WPN = XHN*(1.-A)
00142 79*      WSD = STD*SQRT(1.-A*A)
00143 80*      CALL RN(W,AX,WSD,WPN)
00144 81*      XN = XN*A + W
00144 82*      C
00144 83*      COMPUTE ELECTRICAL LOAD DEMAND
00145 84*      C
00146 85*      DLO = TBLU1(TD,PD(4),PD(ND+4),1,-ND)
00147 86*      WLO = TBLU1(DW,PW(4),PW(NW+4),1,-NW)
00148 87*      YLO = TBLU1(WY,PY(4),PY(NY+4),1,-NY)
00149 88*      LO2 = (DLO*XN)*WLO + YLO*XNC
00150 89*      TIME = TIME
00151 90*      150 RE = AMIN1(PMAX,LO2)/EF
00152 91*      C
00152 92*      PERFORMANCE STATISTICS
00153 93*      C
00154 94*      IF(IMPL.LE.1) RETURN
00155 95*      IF(IYN.NE.0) DVD = PO*VE
00156 96*      SFE = SRE + LO2*0.5*TINC
00157 97*      SDE = SDE + PO*0.5*TINC
00158 98*      IF(SRE.GT.0.) PC = 100.*SDE/SRE
00159 99*      C
00160 100*     IF(TIME.LT.TMAX) RETURN
00161 101*     CVE = CV + VDE
00162 102*     CDE = CDE + SDE - PO*0.5*TINC
00163 103*     CRE = CRE + SRE - LO2*0.5*TINC
00164 104*     RETURN
00165 105*     END

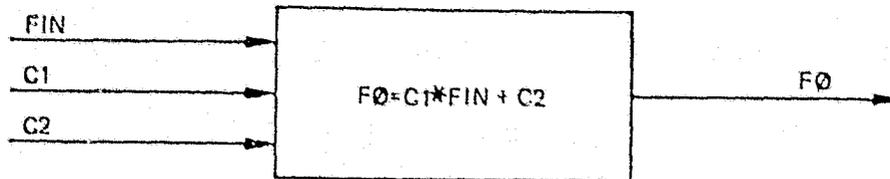
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C00073
C00116
C00122
C00133
C00141
C00141
C00141
C00145
C00164
C00203
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C00232
C00233
C00233
C00233
C00241
C00250
C00261
C00266
C00271
C00271
C00300
C00307
C00312
C00316
C00325
C00470

```

## 7.25 MULTIPLY AND ADD



### Inputs

<u>Parameter/Port</u>	<u>Description</u>
FIN	Input quantity
C1	Input quantity
C2	Input quantity

### Outputs

<u>Variable/Port</u>	<u>Description</u>
F0	Output quantity

### Calculation Sequence

$$F0 = C1 * FIN + C2$$

SUBROUTINE MA            ENTRY POINT 000012

STORAGE USED    CODE(1) 000016; DATA(0) 000004; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003    NERR35

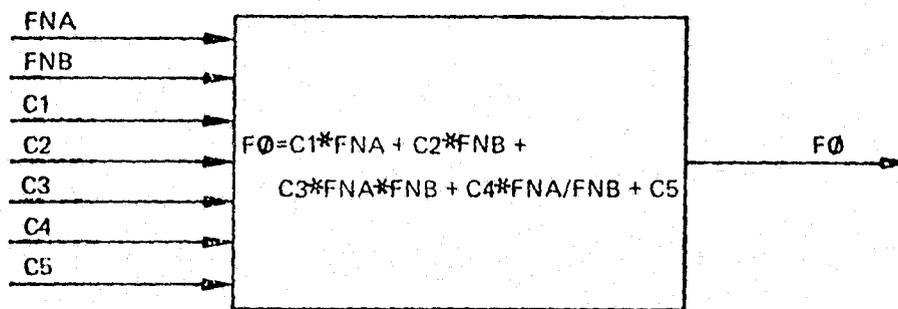
STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0000    000000 INJPS

00100	1*	CMA				000000
00101	2*		SUBROUTINE MA(F0,FIN,C1,C2)			000000
00101	3*	C				000000
00101	4*	C	PURPOSE - TO SIMULATE THE EQUATION	OUTPUT=C1*INPUT + C2		000000
00101	5*	C				000000
00101	6*	C				000000
00101	7*	C	METHOD - SEE CODING			000000
00101	8*	C				000000
00101	9*	C				000000
00101	10*	C	WRITTEN BY - ADAM LLOYD	LATEST REVISION	NOV 75	000000
00101	11*	C				000000
00101	12*	C				000000
00101	13*	C	LIMITATIONS - NONE			000000
00101	14*	C				000000
00101	15*	C				000000
00101	16*	C	INPUT/OUTPUT LIST			000000
00101	17*	C				000000
00101	18*	C	F0	OUTPUT VARIABLE	ANY	OUTPUT VAR
00101	19*	C	FIN	INPUT VARIABLE	ANY	INPUT VAR
00101	20*	C	C1	CONSTANT MULTIPLIER	---	INPUT PARAM
00101	21*	C	C2	CONSTANT ADDITION	---	INPUT PARAM
00103	22*		F0=C1*FIN + C2			000000
00104	23*		RETURN			000003
00105	24*		END			000015

**MA**

## 7.24 MULTIPLY, DIVIDE, AND ADD



### Inputs

<u>Parameter/Port</u>	<u>Description</u>
FNA	Input quantity
FNB	Input quantity
C1	Input quantity
C2	Input quantity
C3	Input quantity
C4	Input quantity
C5	Input quantity.

### Outputs

#### Variable/Port

F0	Output quantity
----	-----------------

### Calculation Sequence

$$F0 = C1 * FNA + C2 * FNB + C3 * FNA * FNB + C4 * FNA / FNB + C5$$

SUBROUTINE MB ENTRY POINT 000051

STORAGE USED CODE(1) 000064; DATA(0) 000023; BLANK COMMON(2) 000000

## COMMON BLOCKS

0003 ERMESS 000002  
0004 C10 000003

## EXTERNAL REFERENCES (BLOCK, NAME)

0005 MWDUS  
0006 MI02%  
0007 MERR3%

## STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000030 IGL 0000 000000 20F 0001 000042 30L 0004 000002 IDIAG 0003 000001 IERR  
0003 000000 IFATAL 0000 000015 INJPS 0004 000000 IREAD 0004 I 000001 IWRITE

```

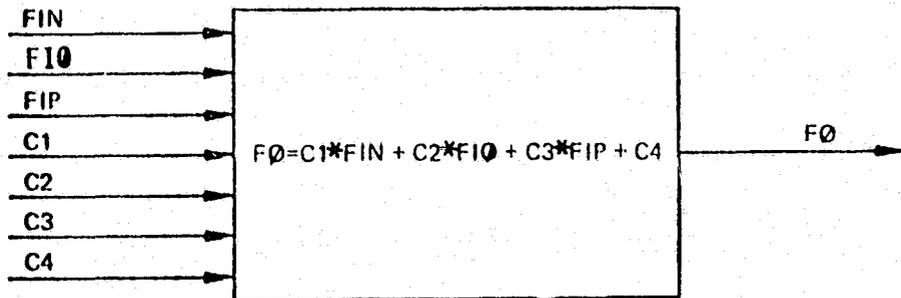
00100 1*   CMB                               000000
00101 2*   SUBROUTINE MB(F0,FNA,FNB,C1,C2,C3,C4;C5) 000000
00101 3*   C                               000000
00101 4*   C   PURPOSE - TO SIMULATE THE EQUATION  Y=C1*XA+C2*XB+C3*XA*XB+C4*XA/XB+C5 000000
00101 5*   C                               000000
00101 6*   C                               000000
00101 7*   C   WRITTEN BY - GEORGE DULEBA                LATEST REVISION  MAY 76 000000
00101 8*   C                               000000
00101 9*   C                               000000
00101 10*  C   LIMITATIONS - IF FNB=0 DURING DIVISION, FNB IS SET TO E-20. 000000
00101 11*  C   DIAGNOSTIC MESSAGE IS GIVEN.                000000
00101 12*  C                               000000
00101 13*  C                               000000
00101 14*  C   INPUT/OUTPUT LIST                          000000
00101 15*  C                               000000
00101 16*  C   F0      OUTPUT VARIABLE                    ANY      OUTPUT VAR  000000
00101 17*  C   FNA    INPUT VARIABLE A                    ANY      INPUT VAR   000000
00101 18*  C   FNB    INPUT VARIABLE B                    ANY      INPUT VA   000000
00101 19*  C   C1     MULTIPLIER 1                        ANY      INPUT VAR   000000
00101 20*  C   C2     MULTIPLIER 2                        ANY      INPUT VAR   000000
00101 21*  C   C3     MULTIPLIER 3                        ANY      INPUT VAR   000000
00101 22*  C   C4     MULTIPLIER 4                        ANY      INPUT VAR   000000
00101 23*  C   C5     ADDITIVE VARIABLE                    ANY      INPUT VAR   000000
00101 24*  C                               000000
00101 25*  C                               000000
00103 26*  COMMON/ERMESS/IFATAL,IERR                      000000
00104 27*  COMMON/C10/IREAD,IWRITE,IDIAG                  000000

```

MB

00105	28*		FO= C1*FNA + C2*FNB + C3*FNA*FNB + C5	000000
00106	29*		IF(C4.EQ.0.99999) GO TO 30	000012
00110	30*		IF(FNB.EQ.0.) GO TO 10	000015
00112	31*		FO= FO + C4*FNA/FNB	000017
00113	32*		RETURN	000024
00114	33*	10	WRITE(IWRITE,20)	000030
00116	34*	20	FORMAT(/,30X, 53HWARNING- DIVISOR IN MB EQUALS 0., HAS BEEN SET=1.	000034
00116	35*		2E-20)	000034
00117	36*		FO= FO + C4*FNA*1.E+20	000034
00120	37*	30	RETURN	000042
00121	38*		END	000063

## 7.25 MULTIPLY AND ADD



### Inputs

<u>Parameter/Port</u>	<u>Description</u>
FIN	Input quantity
FI0	Input quantity
FIP	Input quantity
C1	Input quantity
C2	Input quantity
C3	Input quantity
C4	Input quantity

### Outputs

<u>Variable/Port</u>	<u>Description</u>
F0	Output quantity

### Calculation Sequence

$$F0 = C1*FIN + C2*FI0 + C3*FIP + C4$$

SUBROUTINE MC

ENTRY POINT 000020

STORAGE USED CODE(1) 000024; DATA(0) 000004; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

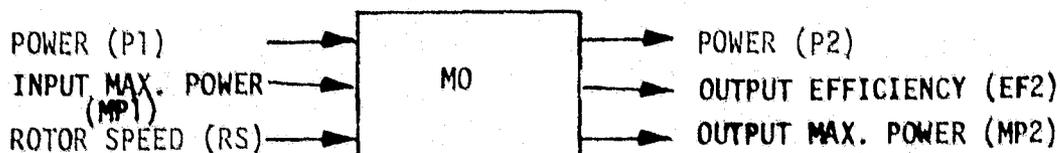
0003 HLRR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0000 000000 INJPS

00100	1*	CMC					000000
00101	2*		SUBROUTINE MC(F0,FIN,FIO,FIP,C1,C2,C3,C4)				000000
00101	3*	C					000000
00101	4*	C	PURPOSE - TO SIMULATE THE EQUATION	$F0=C1*FIN+C2*FIO+C3*FIP+C4$			000000
00101	5*	C					000000
00101	6*	C					000000
00101	7*	C	METHOD - SEE CODING				000000
00101	8*	C					000000
00101	9*	C					000000
00101	10*	C	WRITTEN BY - ADAM LLOYD	LATEST REVISION	NOV 75		000000
00101	11*	C					000000
00101	12*	C					000000
00101	13*	C	LIMITATIONS - NONE				000000
00101	14*	C					000000
00101	15*	C					000000
00101	16*	C	INPUT/OUTPUT LIST				000000
00101	17*	C					000000
00101	18*	C	F0	OUTPUT VARIABLE	ANY	OUTPUT VAR	000000
00101	19*	C	FIN	INPUT VARIABLE	ANY	INPUT VAR	000000
00101	20*	C	FIO	INPUT VARIABLE	ANY	INPUT VAR	000000
00101	21*	C	FIP	INPUT VARIABLE	ANY	INPUT VAR	000000
00101	22*	C	C1	CONSTANT MULTIPLIER	---	INPUT PARAM	000000
00101	23*	C	C2	CONSTANT MULTIPLIER	---	INPUT PARAM	000000
00101	24*	C	C3	CONSTANT MULTIPLIER	---	INPUT PARAM	000000
00101	25*	C	C4	CONSTANT ADDITION	---	INPUT PARAM	000000
00103	26*		$F0=C1*FIN+C2*FIO+C3*FIP+C4$				000000
00104	27*		RETURN				000011
00105	28*		END				000023

## 7.26 AC INDUCTION MOTOR



The induction motor produces mechanical power and torque proportional to slip speed, i.e. power and torque approach zero as the rotor approaches synchronous speed. Two power losses are modeled: a constant multiplicative term due to resistive heating and an additive term due to mechanical friction. Default parameters are based on a conventional squirrel-cage induction motor/generator machine.

### Basic Equations

$$P2 = EE * P1 + DA * RS^2 * C$$

where

$P1, P2$  = Input and output power

$EE$  = electrical efficiency

$DA$  = mechanical damping

$C$  = conversion constant

## Inputs

<u>Parameter/Port</u>		<u>Description</u>	<u>Units</u>
P	1	Input power	kw
DA		Mechanical damping (D = 0)	joule-sec
RS		Rotor speed	rpm
RSY		Synchronous rotor speed (D = 1800)	rpm
SR		Stator resistance (D = 8/RAP)	ohms
VØ		Rated input voltage (D = 400)	volts
RAP		Rated input power	kw
RAS		Rated power slip (D = 0.05)	-
EF	1	Input product efficiency	-
MP	1	Maximum input power (D = $1 \times 10^8$ )	kw
CC		Capital cost/year	\$
CM		Maintenance cost/year	\$

## Outputs

<u>Variable/Port</u>			
P	2	Output mechanical power	kw
EE		Electrical efficiency	-
TØ		Mechanical torque	ft-lb
PL		Power loss	kw
EF	2	Output product efficiency	-
MP	2	Output maximum power	kw

## Statistics

MT		Maximum torque	ft-lb
MPN		Maximum output power/rated power	-
SP		Output energy sum	kwh

D - Default values supplied.

## Calculation Sequence

- 1) Compute electrical efficiency (first pass only)

$$I_{RAT} = RAP * 1000 / V_0$$

$$EE = 1 - SR * I_{RAT}^2 / RAP * 1000$$

- 2) Diagnostics

$$P_1 > RAP \Rightarrow \text{DIAGNOSTIC}$$

$$SLIP = 1 - RS / RSY > RAS \Rightarrow \text{DIAGNOSTIC}$$

- 3) Output power and power loss

$$\omega = RS * (2\pi / 60)$$

$$P_2 = EE * P_1 - DA * \omega^2 / 1000$$

$$PL = P_1 - P_2$$

- 4) If  $P_2 > 0$  go to 5)

$$P_1 > 0 \Rightarrow \text{DIAGNOSTIC}$$

$$EF_2 = EF_1, MP_2 = \text{MIN}(MP_1, RAP)$$

Go to 7)

- 5) Compute torque

$$T_0 = P_2 * 1000 / \omega * k$$

$$k = 1.3558 \text{ joules/ft-lb}$$

Calculation Sequence Cont.

6) Efficiency and maximum output power

$$EF2 = EF1 * (P2/P1)$$

$$MP2 = \text{MIN}(MP1, \text{RAP}) * (P2/P1)$$

7) Compute Statistics and Costs

SUBROUTINE M0 ENTRY POINT 000312

STORAGE USED CODE(1) 000434; DATA(0) 000102; BLANK COMMON(2) 000000

## COMMON BLOCKS

```

0003 CIMPL 000002
0004 CTIME 000001
0005 CSTMUL 000010
0006 COST 000010

```

## EXTERNAL REFERENCES (BLOCK, NAME)

```

0007 NWDUS
0010 N102$
0011 NERR3$

```

## STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

```

000) 000062 100L 0001 000106 200L 0000 000004 208F 0001 000135 300L 0000 000017 308F
0001 000213 400L 0000 000032 408F 0001 000201 409L 0001 000235 500L 0006 R 000003 CCI
0006 R 000001 CHI 0006 000002 COP 0005 R 000000 DUM 0003 I 000001 ICNT 0003 I 000000 IMPL
0000 000066 INJPS 0000 R 000003 OMEGA 0000 R 000002 SLIP 0006 000004 TDC 0004 R 000000 TIME
0000 R 000001 TINC 0006 000005 TLD 0005 R 000007 TMAX 0000 R 000000 TMAX1 0006 000007 UTD
0006 000006 UTV 0006 000003 VDE

```

```

00100 1* CMO 000000
00101 2* SUBROUTINE M0(P2,EE,TO,PL,EF2,MP2,MT,MPN,SP, 000000
00101 3* 1 P1,DA,RS,RSY,SR,VO,RAP,RAS,EF1,MP1,CC,CM) 000000
00101 4* C 000000
00101 5* C PURPOSE AC INDUCYION MOTOR MODEL 000000
00101 6* C 000000
00101 7* C METHOD MECHANICAL POWER AND TORQUE CALCULATED 000000
00101 8* C FROM INPUT AC POWER AND ROTOR SPEED 000000
00101 9* C 000000
00101 10* C WRITTEN BY Y.K.CHAN VERSION 1, JUNE 13, 1977 000000
00101 11* C 000000
00101 12* C CALL SEQUENCE 000000
00101 13* C OUTPUTS 000000
00101 14* C P2 -OUTPUT MECHANICAL POWER,KW 000000
00101 15* C EE -ELECTRICAL EFFICIENCY 000000
00101 16* C TO -MECHANICAL TORQUE,FT-LB 000000
00101 17* C PL -POWER LOSS,KW 000000
00101 18* C EF2 -OUTPUT POWER EFFICIENCY 000000
00101 19* C MP2 -OUTPUT MAXIMUM POWER,KW 000000
00101 20* C STATISTICS 000000
00101 21* C MT -MAXIMUM TORQUE,FT-LB 000000

```

```

00101 22* C MPN -MAXIMUM OUTPUT POWER/RATED POWER 000000
00101 23* C SP-OUTPUT POWER SUM 000000
00101 24* C INPUTS CS0000
00101 25* C P1 -INPUT POWER,KW 000000
00101 26* C DA -MECHANICAL DAMPING, JOULE-SEC 000000
00101 27* C RS -ROTOR SPEED,RPM 000000
00101 28* C RSY -SYNCHRONOUS ROTOR SPEED,RPM 000000
00101 29* C SR -STATOR RESISTANCE, OHMS 000000
00101 30* C VO -RATED INPUT VOLTAGE, VOLTS 000000
00101 31* C RAP -RATED INPUT POWER, KW 000000
00101 32* C RAS -RATED PWER SLIP 000000
00101 33* C EFi -INPUT PRODUCT EFFICIENCY 000000
00101 34* C MP1 -MAXIMUM INPUT POME, KW 000000
00101 35* C CC -CAPITAL COST/YEAR,$ 000000
00101 36* C CM -MAINTENANCE COST/YEAR,$ 000000
00101 37* C 000000
00103 38* COMMON /CIMPL/IMPL, ICNT/CTIME/TIME/CSIMUL/DUM(7), TMAX 000000
00103 39* X /COST/CCI, CHI, COP, VDE, TOE, TLD, UTV, UTD 000000
00104 40* REAL MP2, MT, MPN, MP1 000000
00104 41* C 000000
00105 42* IF(IMPL.GT.0)GO TO 100 000000
00107 43* IF(DA.EQ..99999)DA=0. 000002
00111 44* IF(RSY.EQ..99999)RSY=1800. 000006
00113 45* IF(SR.EQ..99999)SP=8./RAP 000013
00115 46* IF(VO.EQ..99999)VO=400. 000021
00117 47* IF(MP1.EQ..99999)MP1=1.E8 000026
00121 48* IF(RAS.EQ..99999)RAS=.05 000033
00123 49* TMAX=TMAX*.99999 000040
00124 50* MT=C. 000043
00125 51* MPN=0. 000044
00126 52* SP=0. 000045
00127 53* TINC=DUM(7)*.5 000046
00127 54* C 000046
00127 55* C COMPUTE ELECTRICAL EFFICIENCY 000046
00127 56* C 000046
00130 57* EE=1.-SR*RAP*1000./(VO*VO) 000051
00131 58* 100 IF(P1.LE.RAP)GO TO 200 000062
00133 59* IF(IMPL.EQ.2)WRITE(6,208)P1,RAP 000065
00140 60* 208 FORMAT(1H0,18H MOTOR INPUT POWER,F12.3,23H .GT.RATED INPUT POWER . 000077
00140 61* 1 F12.3) 000077
00141 62* IF(IMPL.EQ.2)ICNT=ICNT+1 000077
00143 63* 200 SLIP=1.-(RS/RSY) 000106
00144 64* IF(SLIP.LE.PAS)GO TO 300 000111
00146 65* IF(IMPL.EQ.2)WRITE(6,308)SLIP,RAS 000114
00153 66* 308 FORMAT(1H0,11H MOTOR SLIP,F12.3,25H EXCEEDS RATED POWER SLIP, 000126
00153 67* 1 F12.3) 000126
00154 68* IF(IMPL.EQ.2)ICNT=ICNT+1 000126
00154 69* C 000126
00154 70* C COMPUTE POWER AND POWER LOSS 000126
00154 71* C 000126
00156 72* 300 OMEGA=RS*3.14159/30. 000135
00157 73* P2=EE*P1-DA*OMEGA*OMEGA/1000. 000140
00160 74* PL=P1-P2 000147
00161 75* TC=0. 000151
00162 76* IF(P2.GT.0.)GO TO 400 000152
00164 77* IF(P1.LE.0.)GO TO 400 000155
00166 78* IF(IMPL.EQ.2)WRITE(6,408)SR,DA 000160

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00173 79*      408 FORMAT(1H0,19H STATOR RESISTANCE ,F12.3,12H OR DAMPING ,
00173 80*      XF12.3,20H TOO HIGH FOR MOTOR )
00174 81*      IF(IMPL.EQ.2)ICNT=ICNT+1
      C
00174 82*      C          EFFICIENCY AND MAXIMUM OUTPUT POWER
      C
00174 83*      C
00174 84*      C
00176 85*      409 CONTINUE
00177 86*      P2=0.
00177 86*      EF2=EF1
00200 87*      MP2=AMIN1(MP1,RAP)
00201 88*      GO TO 500
00202 89*      400 EF2=EF1*P2/P1
00203 90*      MP2=AMIN1(MP1,RAP)*P2/P1
00204 91*      IF(IRS.NE.C.)TO=P2*737.6/OMEGA
00205 92*
00205 93*      C
00207 94*      500 IF(IMPL.LE.1)RETURN
00207 95*      C
00207 96*      C          STATISTICS
      C
00207 97*      C
00211 98*      MT=AMAX1(TO,MT)
00212 99*      MPN=AMAX1(P2/RAP,MPN)
00213 100*     SP=SP+P2*TINC
00213 101*     C
00214 102*     IF(TIME.LT.TMAX1)RETURN
00216 103*     CCI=CCI+CC
00217 104*     CMI=CMI+CM
00217 105*     C
00220 106*     RETURN
00221 107*     END

```

```

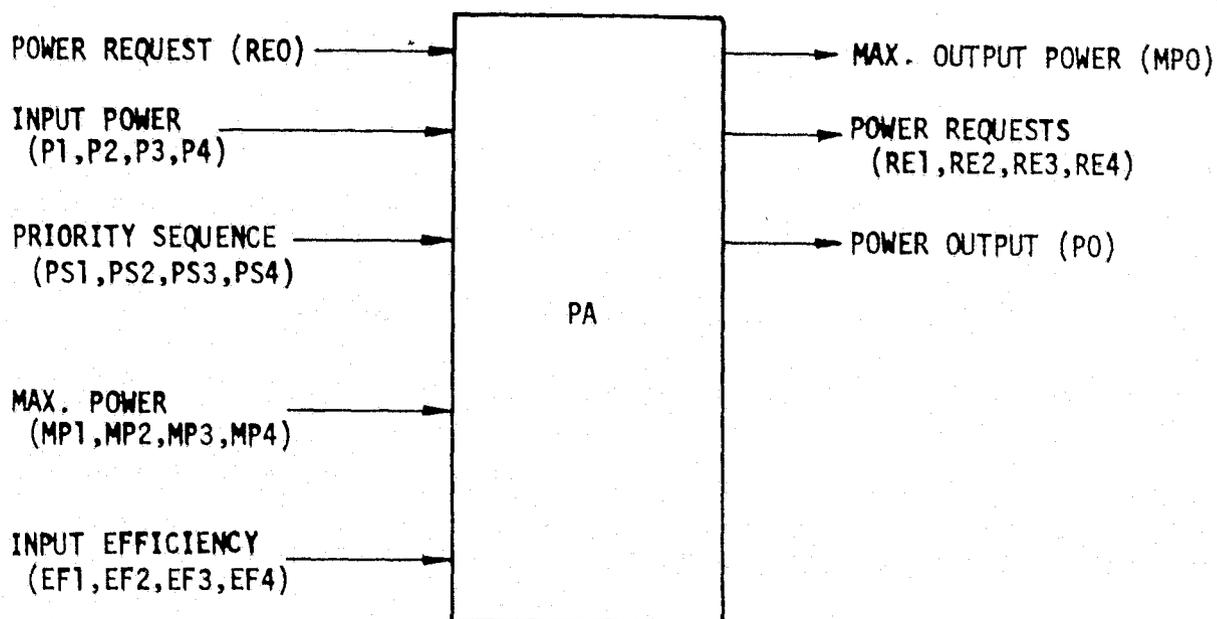
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## 7.27 POWER ACCUMULATOR



This component sums power from four input ports and allocates power requests to each port's source of power generation. If an input power request (load) exceeds the maximum power that can be delivered by the port of highest priority, then the remaining load is allocated according to weight within priority, and then allocated to the next priority ports. (See 1.2.3 for further discussion.)

## Inputs<sup>1</sup>

<u>Parameter/Port</u>	<u>Description</u>	<u>Units</u>
RE      0	Load request	kw
EF      1,2,3,4	Input efficiency from port i	-
P        1,2,3,4	Input power from port i (default = 0.)	kw
PS      1,2,3,4	Priority sequence (default=1,2,3,4)	-
F        1,2,3,4	Allocation weight (for equal priorities)	-
MP      1,2,3,4	Maximum power (default = $1 \times 10^8$ )	kw

## Outputs

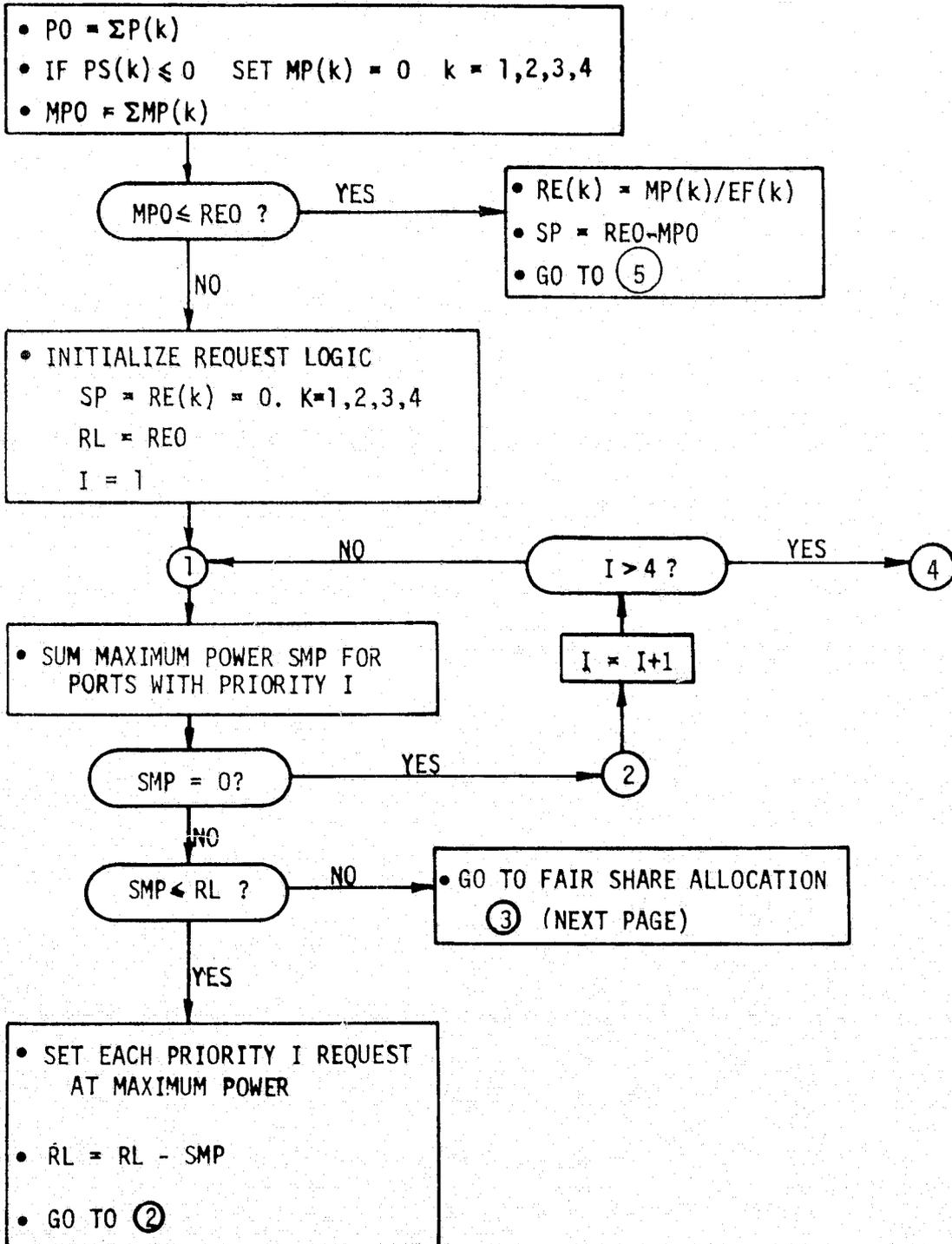
<u>Variable/Port</u>	<u>Description</u>	<u>Units</u>
MP      0	Maximum deliverable power ( $\sum MP(i)$ )	kw
RE      1,2,3,4	Power request for port i	kw
P        0	Power output	kw
SP	Supplemental power request to meet load (Power deficit) = $RE_0 - \sum MP_i$	kw

## Statistics

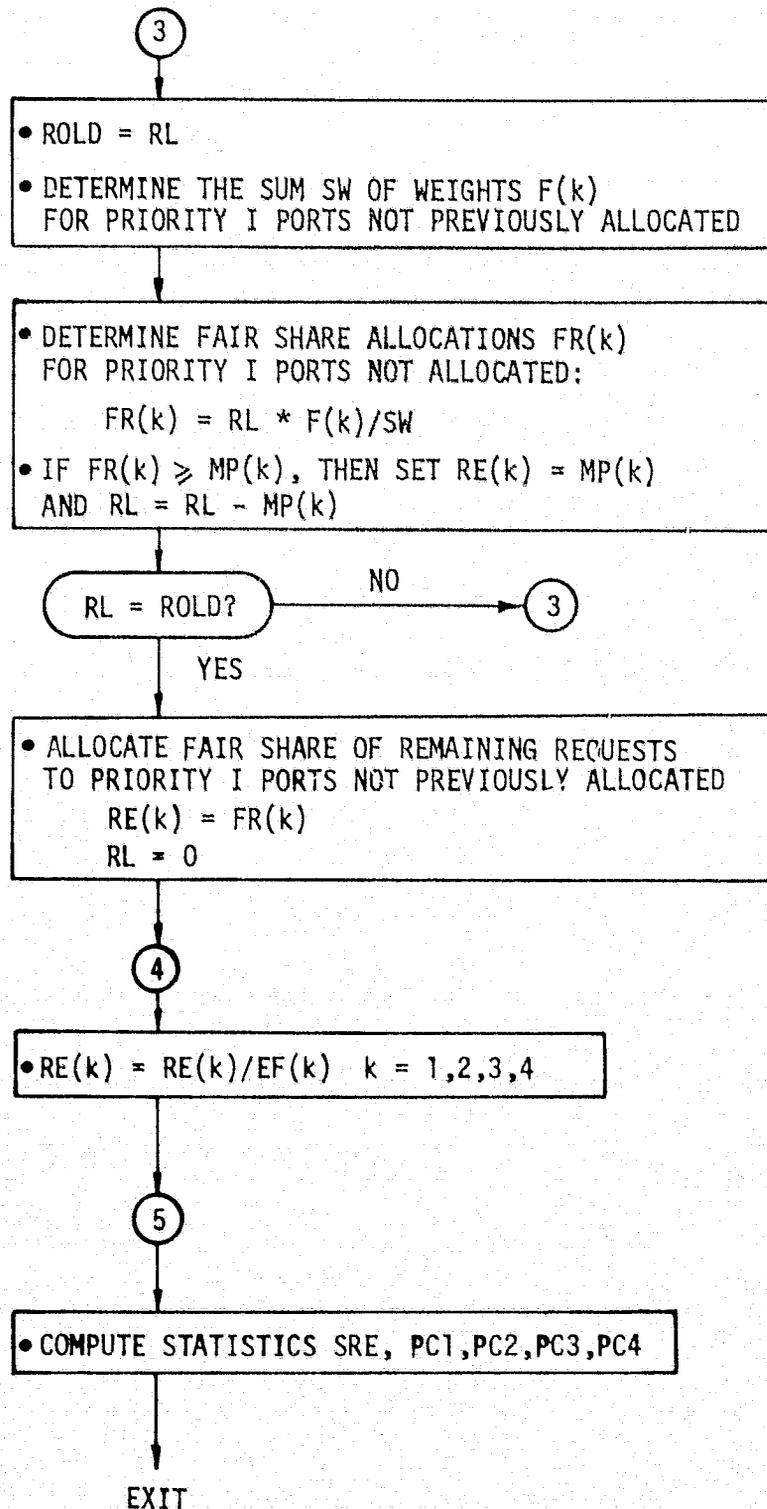
SRE	Sum of energy requested	kwh
PC      1,2,3,4	Percent of cumulative load request delivered by port i	%

<sup>1</sup> No capital costs assigned since this is an allocation component, not a physical device.

## CALCULATION LOGIC



## PA FAIR SHARE ALLOCATION



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SUBROUTINE PA ENTRY POINT 000520

STORAGE USED CODE(1) 000752; DATA(0) 000110; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CIMPL 000001  
0004 CSTMUL 000010

EXTERNAL REFERENCES (BLOCK, NAME)

0005 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000376	100CL	0001	000401	2000L	0001	000235	2346	0001	000244	2416	0001	000264	2546
0001	000306	2736	0001	000325	3056	0001	000363	3256	0001	000104	40L	0001	000301	400L
0001	000417	500L	0001	000301	600L	0001	000316	70CL	0001	000161	80L	0001	000353	800L
0001	000372	900L	0004	000000	DUM	0000	R 000030	FR	0000	R 000042	FRU	0000	I 000037	I
0003	I 000000	IMPL	0000	000055	INJPS	0000	I 000041	K	0000	R 000034	LL	0000	R 000035	(OLD
0000	R 000014	MP	0000	R 000004	PR	0000	R 000000	R	0000	R 000024	SMP	0000	R 000044	SRI
0000	R 000043	SRO	0000	R 000020	SW	0004	R 000006	TINC	0000	R 000036	TINC1	0004	C00007	TMAX
0000	R 000010	W	0000	R 000040	XI									

00100	1*	CPA												000000
00101	2*			SUBROUTINE PA(MPO,										000000
00101	3*		1	R1, R2, R3, R4,										000000
00101	4*		2	PC, SP,										000000
00101	5*		3	SR, PC1, PC2, PC3, PC4,										000000
00101	6*		4	RO,										000000
00101	7*		4	EF1, EF2, EF3, EF4,										000000
00101	8*		5	P1, P2, P3, P4,										000000
00101	9*		6	PR1, PR2, PR3, PR4,										000000
00101	10*		7	W1, W2, W3, W4,										000000
00101	11*		8	MP1, MP2, MP3, MP4)										000000
00101	12*	C												000000
00101	13*	C		PURPOSE. MODEL POWER ACCUMULATOR										000000
00101	14*	C												000000
00101	15*	C		METHOD. PRIMARY REQUEST ALLOCATION RESULTING FROM PRIORITY										000000
00101	16*	C		ASSIGNMENTS. SECONDARY REQUEST ALLOCATION RESULTING										000000
00101	17*	C		FROM WEIGHT ASSIGNMENTS.										000000
00101	18*	C		THAT IS, REQUESTS ARE ALLOCATED ACCORDING TO										000000
00101	19*	C		* PORT PRIORITY (HIGHEST PRIORITY = 1)										000000
00101	20*	C		* PORT WEIGHTS (IN CASE OF EQUAL PRIORITIES. )										000000
00101	21*	C												000000
00101	22*	C		FORMAL ARGUMENT DEFINITION.										000000
00101	23*	C		R1, ..., R4 POWER REQUESTS IN KW (OUTPUTS)										000000

PA

00101	24*	C	MP0	TOTAL MAXIMUM POWER	(OUTPUT)	000000
00101	25*	C	SP	SURPLUS REQUEST	(OUTPUT)	000000
00101	26*	C	PO	TOTAL LOAD IN KW	(OUTPUT)	000000
00101	27*	C	SR	SUM OF ENERGY REQUESTED, KWH	(OUTPUT)	000000
00101	28*	C	PC1,....,PC4	PERCENT OF CUM LOAD DELIVERED	(OUTPUT)	000000
00101	29*	C	RO	TOTAL POWER REQUESTED,KW	(INPUT)	000000
00101	30*	C	P1,...., P4	INPUT POWER IN KW	(INPUTS)	000000
00101	31*	C	PR1,...., PR4	PORT PRIORITIES	(INPUTS)	000000
00101	32*	C	W1,...., W4	PORT WEIGHTS	(INPUTS)	000000
00101	33*	C	MP1, ...., MP4	MAXIMUM POWERS	(INPUTS)	000000
00101	34*	C	EF1, ...., EF4	EFFICIENCIES	(INPUTS)	000000
00101	35*	C		COMMON STORAGE		000000
00103	36*			COMMON/ CIMPL / TMPL		000000
00104	37*			COMMON / CSIMUL / DUM(6), TINC, TMAX		000000
00105	38*			REAL MP0,MP1,MP2,MP3,MP4		000000
00105	39*	C				000000
00105	40*	C		LOCAL VARIABLES		000000
00105	41*	C				000000
00105	42*	C				000000
00105	43*	C		PK(K) IS THE POWER REQUEST AT PORT K		000000
00106	44*			REAL R(4)		000000
00106	45*	C				000000
00106	46*	C		PR(K) IS THE PRIORITY ASSIGNED TO PORT K		000000
00107	47*			REAL PR(4)		000000
00107	48*	C				000000
00107	49*	C		W(K) IS THE WEIGHT ASSIGNED TO PORT K		000000
00110	50*			REAL W(4)		000000
00110	51*	C				000000
00110	52*	C		MP(K) IS MAXIMUM POWER TO BE ALLOCATED TO PORT K		000000
00111	53*			REAL MP(4)		000000
00111	54*	C				000000
00111	55*	C		SW(I) IS THE SUM OF THE WEIGHTS ASSIGNED TO PRIORITY-I PORTS		000000
00112	56*			REAL SW(4)		000000
00112	57*	C				000000
00112	58*	C		SHP(I) IS THE SUM OF THE MAXIMUM POWER AT PRIORITY-I PORTS		000000
00113	59*			REAL SHP(4)		000000
00113	60*	C				000000
00113	61*	C		FRU IS "FAIR SHARE" UNIT FOR PRIORITY-I PORTS		000000
00113	62*	C				000000
00113	63*	C		FR(K) IS THE COMPUTED "FAIR SHARE" REQUEST FOR PORT K		000000
00114	64*			REAL FR(4)		000000
00114	65*	C				000000
00114	66*	C		LL IS THE LOAD LEFT AT EACH POINT IN THE ITERATION		000000
00115	67*			REAL LL,LOLD		000000
00115	68*	C				000000
00115	69*	C		IF IMPL IS ZERO, THEN ASSIGN DEFAULT VALUES		000000
00116	70*			IF (IMPL .GT. 0) GO TO 40		000000
00120	71*			RO = 0.0		000002
00121	72*			IF (PR1 .EQ. 0.999999) PR1 = 1.0		000003
00123	73*			IF (PR2 .EQ. 0.999999) PR2 = 2.0		000010
00125	74*			IF (PR3 .EQ. 0.999999) PR3 = 3.0		000015
00127	75*			IF (PR4 .EQ. 0.999999) PR4 = 4.0		000022
00131	76*			IF (MP1 .EQ. 0.999999) MP1 = 1.0E8		000027
00133	77*			IF (MP2 .EQ. 0.999999) MP2 = 1.0E8		000034
00135	78*			IF (MP3 .EQ. 0.999999) MP3 = 1.0E8		000041
00137	79*			IF (MP4 .EQ. 0.999999) MP4 = 1.0E8		000046
00141	80*			IF (P1 .EQ. .999999) P1=0.0		000053

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00143      81*      IF(P2 .EQ. .99999) P2=0.0
00145      82*      IF(P3 .EQ. .99999) P3= 0.0
00147      83*      IF(P4 .EQ. .99999) P4=0.0
00151      84*      SR=C.
00152      85*      PC1=0.
00153      86*      PC2=0.
00154      87*      PC3=0.
00155      88*      PC4=0.
00156      89*      TINC1= 0.5*TINC
00157      90*      NO CONTINUE
00157      91*      C
00157      92*      C      IF THE TOTAL MAXIMUM POWER IS .LE. TOTAL POWER
00157      93*      C      REQUESTED, THEN SUBMIT REQUESTS AT MAX-POWER, SET REQUEST
00157      94*      C      SURPLUS EQUAL TO THE DIFFERENCE, AND RETURN
00160      95*      PC = P1 + P2 + P3 + P4
00161      96*      IF(PR1.LE.0.0) MP1=0.
00163      97*      IF(PR2.LE.0.0) MP2=0.
00165      98*      IF(PR3.LE.0.0) MP3=0.
00167      99*      IF(PR4.LE.0.0) MP4=0.
00171     100*      MPJ = MP1 + MP2 + MP3 + MP4
00172     101*      IF (MPC .GT. R0) GO TO 80
00174     102*      R1 = MP1/EF1
00175     103*      R2 = MP2/EF2
00176     104*      R3 = MP3/EF3
00177     105*      R4 = MP4/EF4
00200     106*      SP = R0 - MPC
00201     107*      GO TO 500
00202     108*      NO CONTINUE
00202     109*      C
00202     110*      C      PROCEED WITH ALLOCATION ALGORITHM SINCE THE SUM OF
00202     111*      C      ALL MAXIMUM POWER INPUTS EXCEEDS THE TOTAL REQUEST R0
00202     112*      C
00202     113*      C      INITIALIZATION
00203     114*      LL = R0
00204     115*      R1 = 0.0
00205     116*      R2 = 0.0
00206     117*      R3 = 0.0
00207     118*      R4 = 0.0
00210     119*      SP = 0.0
00210     120*      C
00210     121*      C      IF THE TOTAL REQUEST (OR LOAD) IS ZERO, THEN RETURN
00211     122*      IF (R0 .LE. 0.0) GO TO 500
00213     123*      R(1)=R1
00214     124*      R(2)=R2
00215     125*      R(3)=R3
00216     126*      R(4)=R4
00217     127*      PP(1) = PR1
00220     128*      PR(2) = PR2
00221     129*      PR(3) = PR3
00222     130*      PR(4) = PR4
00223     131*      W(1) = W1
00224     132*      W(2) = W2
00225     133*      W(3) = W3
00226     134*      W(4) = W4
00227     135*      MP(1) = MP1
00230     136*      MP(2) = MP2
00231     137*      MP(3) = MP3
000057
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00303	195*	C	FIRST, SUBMIT FAIR SHARE REQUESTS TO PORTS FOR WHICH THE	000317
00303	196*	C	FAIR SHARE REQUEST EXCEEDS THE MAXIMUM POWER. CONSIDER ONLY	000317
00303	197*	C	PORTS TO WHICH NO REQUEST HAS BEEN SUBMITTED	000317
00304	198*		DO 800 K = 1, 4	000325
00307	199*		IF (R(K) .NE. 0.0) GO TO 800	000325
00311	200*		IF (PR(K) .NE. XI) GO TO 800	000326
00311	201*	C		000326
00311	202*	C	COMPUTE FAIR SHARE	000326
00313	203*		FR(K) = (WK) * FRU) * LL	000331
00313	204*	C		000331
00313	205*	C	IF FAIR SHARE EXCEEDS MAXIMUM POWER, THEN SUBMIT REQUEST	000331
00314	206*		IF (FR(K) .GE. MP(K)) R(K) = MP(K)	000335
00314	207*	C	- - - AND REDUCE LOAD LEFT TALLY	000335
00316	208*		IF (FR(K) .GE. MP(K)) LL = LL - MP(K)	000343
00320	209*	BCC	CONTINUE	000354
00320	210*	C		000354
00320	211*	C	IF LL .NE. LOLD, THEN LL WAS REDUCED DURING THE	000354
00320	212*	C	PROCESSING IN THE "DO 800" LOOP ABOVE. THIS CHANGES	000354
00320	213*	C	THE FAIR SHARE COMPUTATION. IT IS THEREFORE	000354
00320	214*	C	NECESSARY TO GO BACK THROUGH THE "DO 800" LOOP IN	000354
00320	215*	C	ORDER TO RECONSIDER ANY PORT WHICH MAY NOW	000354
00320	216*	C	SAISFY THE REQUIREMENT THAT FR(K) .GE. MP(K). ONLY	000354
00320	217*	C	PRIORITY-I PORTS TO WHICH NO REQUEST HAS BEEN	000354
00320	218*	C	MADE ARE ELIGIBLE FOR RECONSIDERATION	000354
00322	219*		IF (LL .LT. LOLD) GO TO 600	000354
00322	220*	C		000354
00322	221*	C	FINALLY, SUBMIT REQUESTS TO THOSE PORTS FOR WHICH THE FAIR SHARE	000354
00322	222*	C	.LT. THAN THEIR MAXIMUM POWER. CONSIDER ONLY	000354
00322	223*	C	PRIORITY-I PORTS TO WHICH NO REQUEST HAS BEEN SUBMITTED	000354
00324	224*		DO 900 K = 1, 4	000363
00327	225*		IF (R(K) .NE. 0.0) GO TO 900	000363
00331	226*		IF (PR(K) .NE. XI) GO TO 900	000364
00333	227*		R(K) = FR(K)	000367
00334	228*	9CC	CONTINUE	000373
00336	229*		LL=0.0	000373
00337	230*		GO TO 2000	000374
00337	231*	C		000374
00340	232*	1000	CONTINUE	000401
00340	233*	C		000401
00342	234*	2000	CONTINUE	000401
00342	235*	C		000401
00342	236*	C	FINALLY, ASSIGN OUTPUTS TO NON-SUBSCRIBED FORMAL PARAMETERS.	000401
00342	237*	C	ALSO, MODIFY ALL REQUESTS ACCORDING TO THE INPUT EFFICIENCIES	000401
00343	238*		R1 = R(1) / EF1	000401
00344	239*		R2 = R(2) / EF2	000403
00345	240*		R3 = R(3) / EF3	000406
00346	241*		R4 = R(4) / EF4	000411
00347	242*		SP = LL	000414
00350	243*	500	IF(1MPL.LE.1) RETURN	000417
00352	244*		SPO= SR	000425
00353	245*		SR=SR+ RD*YINC1	000427
00354	246*		IF(SR.LE.C.) RETURN	000433
00356	247*		SRO=SRO/SR	000441
00357	248*		SRI= YINC1*100./SR	000444
00360	249*		PC1= PC1*SRO + P1*SRI	000450
00361	250*		PC2= PC2*SRO + P2*SRI	000454
00362	251*		PC3= PC3*SRO + P3*SRI	000462

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PA

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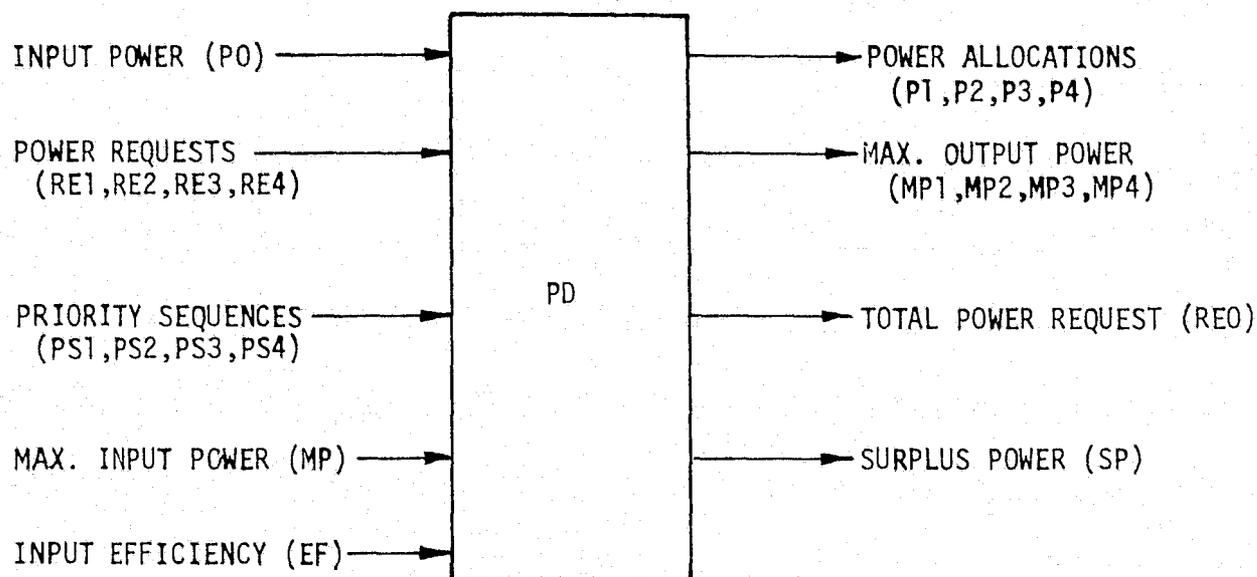
PA

000470  
000476  
000751

PC4= PC4\*SR0 + P4\*SR1  
RETURN  
END

00363 252\*  
00364 253\*  
00365 254\*

## 7.28 POWER DIVIDER



This component allocates power to four ports plus surplus based on priority, port requests, and allocation weights for equal priority ports. Each port is assigned a priority sequence from 1 to 4, and a weighting  $F_i > 0$ ,  $i=1,2,3,4$  for proportional allocation among equal priority ports. If power available exceeds the power requested for a set of ports of equal priority, then the remaining power is allocated to ports having the next highest priority. If power available is less than the power requested for ports of equal priority then power is allocated between them in proportion to their respective allocation weights.

The total power request is the sum of the port requests divided by input efficiency. The maximum power outputs  $MP_1, \dots, MP_4$  are necessary for direct connections to a power accumulator PA. These variables may be used as maximum power inputs to other components, although such connections are not required. (See 1.2.3 for further discussion.)

## Inputs<sup>1</sup>

<u>Parameter/Port</u>	<u>Description</u>	<u>Units</u>
P            0	Input power	kw
RE        1,2,3,4	Power requests of output ports	kw
PS        1,2,3,4	Priority sequence (default = 1,2,3,4)	-
F         1,2,3,4	Allocation weight (for equal priorities)	-
MP	Maximum input power (default = $1 \times 10^8$ )	kw
EF	Input efficiency	-

## Outputs

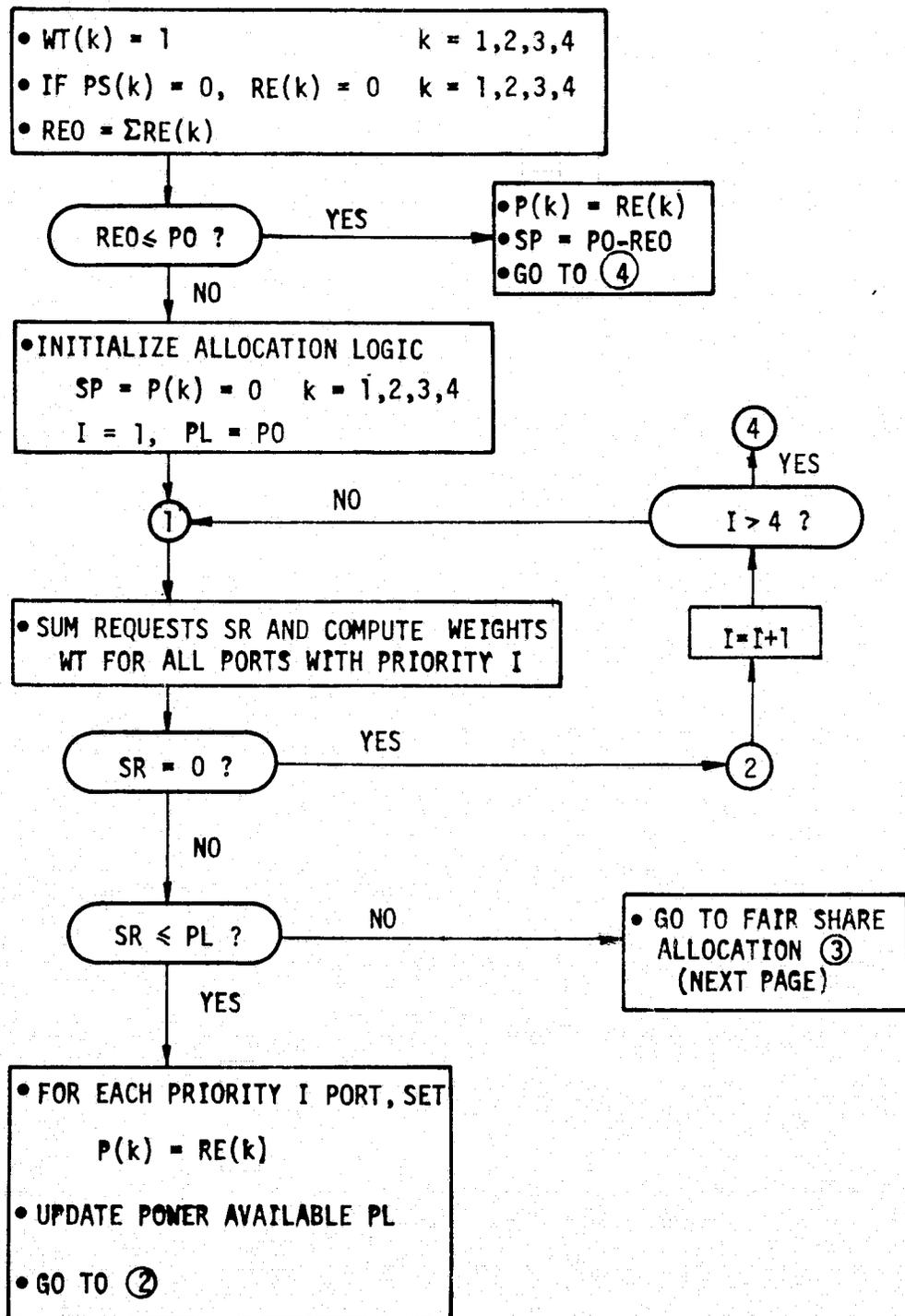
### Variable/Port

P        1,2,3,4	Output power for port i	kw
RE       0	Output power request	kw
SP	Surplus power	kw
MP       1,2,3,4	Output maximum power based on MP	kw

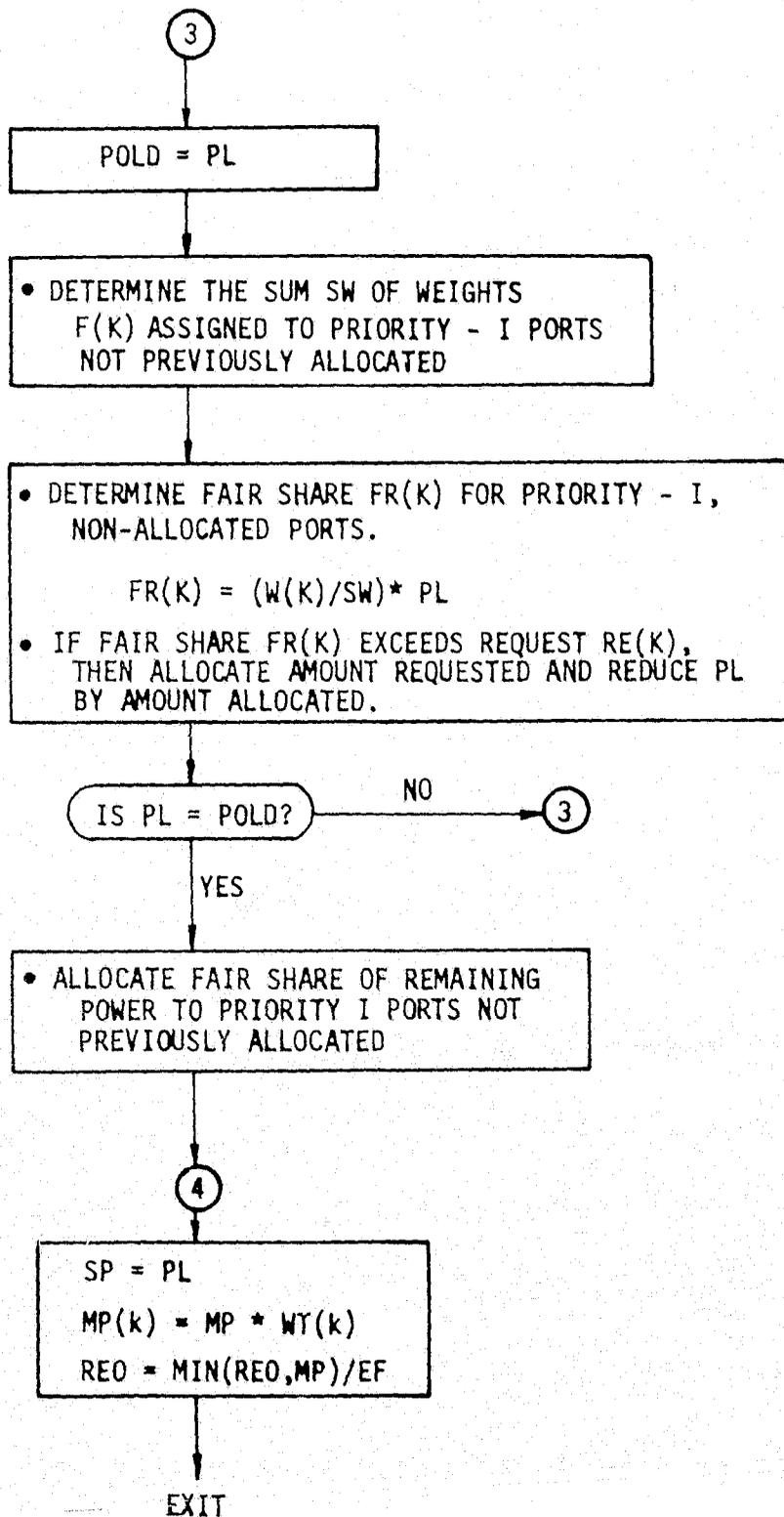
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<sup>1</sup> No capital costs assigned since this is an allocation component, not a physical device.

## CALCULATION LOGIC



## PD FAIR SHARE ALLOCATION



SUBROUTINE PD ENTRY POINT 000452

STORAGE USED CODE(1) 000642; DATA(0) 000106; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CIMPL 000001

EXTERNAL REFERENCES (BLOCK, NAME)

0004 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000371	1000L	0001	000172	216G	0001	000202	224G	0001	000263	253G	0001	000303	270G	
0001	000406	300CL	0001	000322	302G	0001	000357	322G	0001	000445	40L	0001	000276	40CL	
0001	000276	600L	0001	000313	700L	0001	000116	80L	0001	000350	800L	0001	000366	900L	
0000	R	000030	FR	0000	R	000046	FRU	0000	R	000035	FI	0000	R	000036	F2
0000	R	000040	FR	0000	I	000041	I	0000	I	000000	INPL	0000	I	000044	K
0000	R	000000	P	0000	R	000034	PL	0000	R	000045	POLD	0000	R	000010	PR
0000	R	000024	SR	0000	R	000020	SW	0000	R	000014	W	0000	R	000043	WT
												0000	R	000042	XI

```

00100      1*      CPD
00101      2*
00101      3*      1      SUBROUTINE PD(
00101      4*      2      P1, P2, P3, P4,
00101      5*      3      RO,
00101      6*      4      SP, PM1, PM2, PM3, PM4,
00101      7*      5      PO,
00101      8*      6      R1, R2, R3, R4,
00101      9*      7      PR1, PR2, PR3, PR4,
00101      10*     7      W1, W2, W3, W4, PM, EF)
00101      11*     C
00101      12*     C      PURPOSE.      MODEL POWER DIVIDER
00101      13*     C
00101      14*     C      METHOD.      PRIMARY FLOW ALLOCATION RESULTING FROM PRIORITY
00101      15*     C      ASSIGNMENTS.      SECONDARY FLOW ALLOCATION RESULTING
00101      16*     C      FROM WEIGHT ASSIGNMENTS.
00101      17*     C      THAT IS, TOTAL AVAILABLE POWER IS ALLOCATED
00101      18*     C      ACCORDING TO
00101      19*     C      * PORT REQUESTS
00101      20*     C      * PORT PRIORITY (HIGHEST PRIORITY = 1)
00101      21*     C      * PORT WEIGHTS (IN CASE OF EQUAL PRIORITIES)
00101      22*     C
00101      23*     C      ALLOCATION SCHEME.
00101      24*     C      IS SUM OF ALL REQUESTS .LT. POWER AVAILABLE PD
00101      25*     C      YES.
00101      26*     C      FULFILL EACH REQUEST

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PD



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00113 83* C
00113 84* C IF IMPL IS ZERO, THEN ASSIGN DEFAULT VALUES
00114 85* IF (IMPL .GT. 0) GO TO 40
00116 86* R1 = 0.0
00117 87* R2 = 0.0
00120 88* R3 = 0.0
00121 89* R4 = 0.0
00122 90* IF (PM.EQ. .99999) PM=1.E8
00124 91* IF (PR1 .EQ. 0.99999) PR1 = 1.0
00126 92* IF (PR2 .EQ. 0.99999) PR2 = 2.0
00130 93* IF (PR3 .EQ. 0.99999) PR3 = 3.0
00132 94* IF (PR4 .EQ. 0.99999) PR4 = 4.0
00134 95* IF (PM .EQ. .99999) PM= 1.E8
00134 96* C
00134 97* C INITIALIZATION OF F'S
00136 98* NO CONTINUE
00137 99* F1= 1.
00140 100* F2= 1.
00141 101* F3= 1.
00142 102* F4= 1.
00142 103* C
00142 104* C IF THE TOTAL POWER REQUESTED IS .LE. TOTAL POWER
00142 105* C INPUT, THEN SATISFY REQUESTS, SET POWER SURPLUS
00142 106* C EQUAL TO THE DIFFERENCE, AND RETURN
00143 107* IF (PR1.LE.0.0) R1=0.0
00145 108* IF (PR2.LE.0.0) R2=0.0
00147 109* IF (PR3.LE.0.0) R3=0.0
00151 110* IF (PR4.LE.0.0) R4=0.0
00153 111* R0 = R1 + R2 + R3 + R4
00154 112* IF (R0 .GT. PD) GO TO 80
00156 113* P1 = R1
00157 114* P2 = R2
00160 115* P3 = R3
00161 116* P4 = R4
00162 117* SP = PD - R0
00163 118* GO TO 3000
00164 119* 80 CONTINUE
00164 120* C
00164 121* C PROCEED WITH ALLOCATION ALGORITHM SINCE THE SUM OF
00164 122* C ALL REQUESTS EXCEEDS THE TOTAL AVAILABLE POWER PD
00164 123* C
00164 124* C INITIALIZATION
00165 125* PL = PD
00166 126* P1 = 0.0
00167 127* P2 = 0.0
00170 128* P3 = 0.0
00171 129* P4 = 0.0
00172 130* SP = 0.0
00172 131* C
00172 132* C IF THE TOTAL POWER IS ZERO, THEN RETURN
00173 133* IF (PD .EQ. 0.0) GO TO 3000
00175 134* P(1) = P1
00176 135* P(2) = P2
00177 136* P(3) = P3
00200 137* P(4) = P4
00201 138* R(1) = R1
00202 139* R(2) = R2

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PD

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00203 140* R(3) = R3
00204 141* R(4) = R4
00205 142* PR(1) = PR1
00206 143* PR(2) = PR2
00207 144* PR(3) = PR3
00210 145* PR(4) = PR4
00211 146* W(1) = W1
00212 147* W(2) = W2
00213 147* W(3) = W3
00214 149* W(4) = W4
00214 150* C
00214 151* C
00214 152* C ITERATE ON PRIORITY I FOR I = 1, 2, 3, 4
00214 153* C
00215 154* C DO 1000 I = 1, 4
00215 155* C
00220 156* C XI = I
00220 157* C OBTAIN SUM OF REQUESTS FROM PORTS WITH PRIORITY I
00221 158* C SR(I) = 0.0
00222 159* C WT=0.0
00223 160* C DO 100 K = 1, 4
00226 161* C IF (PR(K) .EQ. XI) SR(I) = SR(I) + R(K)
00230 162* C IF (PR(K) .EQ. XI) WT = WT + W(K)
00232 163* C 100 CONTINUE
00232 164* C
00234 165* C IF (PR1 .EQ. XI) F1 = W1/WT
00236 166* C IF (PR2 .EQ. XI) F2 = W2/WT
00240 167* C IF (PR3 .EQ. XI) F3 = W3/WT
00242 168* C IF (PR4 .EQ. XI) F4 = W4/WT
00244 169* C IF (PL.LE.0.0) GO TO 1000
00244 170* C
00244 171* C IF NO PRIORITY-I REQUESTS EXIST, THEN PROCEED WITH
00244 172* C THE NEXT HIGHER PRIORITY
00246 173* C IF (SR(I) .EQ. 0.0) GO TO 1000
00246 174* C
00246 175* C IF THE SUM OF ALL PRIORITY-I REQUESTS .GT. POWER
00246 176* C AVAILABLE, THEN GO AROUND
00250 177* C IF (SR(I) .GT. PL) GO TO 400
00250 178* C
00250 179* C THE SUM OF ALL PRIORITY-I REQUESTS .LE. POWER
00250 180* C AVAILABLE, SO FULFILL EACH PRIORITY-I REQUEST
00252 181* C DO 200 K = 1, 4
00255 182* C IF (PR(K) .EQ. XI) P(K) = R(K)
00257 183* C 200 CONTINUE
00257 184* C
00257 185* C UPDATE POWER AVAILABLE
00261 186* C PL = PL - SR(I)
00262 187* C GO TO 1000
00262 188* C
00263 189* C 400 CONTINUE
00263 190* C
00263 191* C THE SUM OF THE PRIORITY-I REQUESTS EXCEEDS THE
00263 192* C POWER AVAILABLE, SO COMPUTE AND ALLOCATE FAIR
00263 193* C SHARE TO EACH PRIORITY-I PORT
00263 194* C
00264 195* C 600 CONTINUE
00264 196* C

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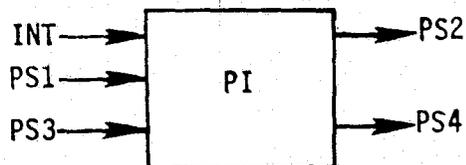
PD



```
00341 254*      P4 = P(4)
00342 255*      SP = PL
00343 256*      3000 PM1=PM*F1
00344 257*      PM2=PM*F2
00345 258*      PM3=PM*F3
00346 259*      PM4=PM*F4
00347 260*      RO= AMIN1(RO,PM)/EF
00350 261*      RETURN
00351 262*      END
```

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000401
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## 7.29 PRIORITY INTERRUPT



This component is used by the storage components to change priority of the power requests when minimum or maximum capacity is approached.

### Inputs

<u>Parameter/Port</u>	<u>Description</u>
PS 1	Input priority for PS4 output
PS 3	Input priority for PS2 output (default=PS1)
INT	Interrupt flag

### Outputs

<u>Variable/Port</u>	<u>Description</u>
PS 2	Output priority for charge cycle
PS 4	Output priority for discharge cycle

### Equations

$$\begin{aligned}
 PS2 &= PS1 && \text{if } INT=0 \\
 PS2 &= 1 && \text{if } INT > 0 \\
 PS2 &= 0 && \text{if } INT < 0 \\
 PS4 &= PS3 && \text{if } INT \leq 0 \\
 PS4 &= 0 && \text{if } INT > 0
 \end{aligned}$$

SUBROUTINE PI ENTRY POINT 000040

STORAGE USED CODE(1) 000061; DATA(0) 000010; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CIMPL 000001

EXTERNAL REFERENCES (BLOCK, NAME)

0004 NERR34

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000010 10L 0003 I 000000 IMPL 0000 000002 INJPS

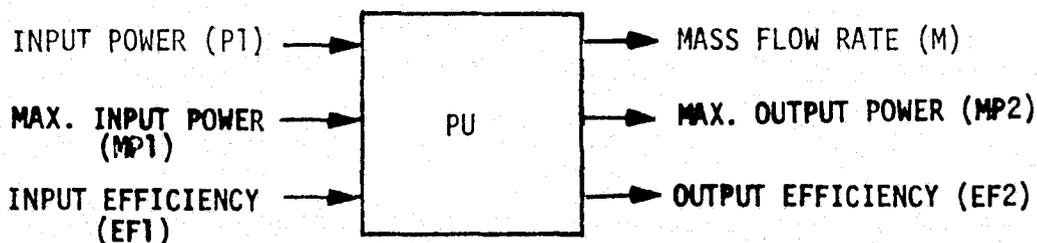
```

00100 1* CPI 000000
00101 2* SUBROUTINE PI(PS2,PS4,PS1,PS3,INT) 000000
00101 3* C 000000
00101 4* C PURPOSE CHANGE PRIORITY OF POWER ALLOCATION TO STORAGE COMPONENTS 000000
00101 5* C 000000
00101 6* C WRITTEN BY A.W.WARREN VERSION 1, APRIL 14 1977 000000
00101 7* C 000000
00101 8* C CALL SEQUENCE 000000
00101 9* C PS2 - OUTPUT PRIORITY (0 TO 4) 000000
00101 10* C PS4 - OUTPUT PRIORITY (COMPLEMENT TO PS2) 000000
00101 11* C PS1 - INPUT PRIORITY FOR PS2 000000
00101 12* C PS3 - INPUT PRIORITY FOR PS4 000000
00101 13* C INT - INTERRUPT FLAG 000000
00101 14* C 0= NO INTERRUPT 000000
00101 15* C 1= INCREASE ALLOCATION PRIORITY 000000
00101 16* C -1= DECREASE ALLOCATION PRIORITY 000000
00101 17* C 000000
00103 18* REAL INT 000000
00104 19* COMMON /CIMPL/IMPL 000000
00105 20* IF(IMPL.GT.0) GO TO 10 000000
00107 21* IF(PS3.EQ. .99999) PS3=PS1 000002
00107 22* C 000002
00111 23* 10 PS2=PS1 000010
00112 24* PS4=PS3 000011
00113 25* IF(INT.GT.0.) PS2=1. 000013
00115 26* IF(INT.LI.0.) PS2=0. 000020
00117 27* IF(INT.GT.0) PS4= 0. 000024
00121 28* RETURN 000030
00122 29* END 000060

```

PI

## 7.30 HYDRAULIC PUMP



The hydraulic pump model is based on a constant speed design. The pump is assumed to be designed to a nominal operating point and input power. For off-design performance the pump efficiency is assumed to be functionally related to the square root of the mass flow rate.

### Basic Equations

The output mass flow rate is based on the equations

$$M = P1 * EFF / (C1 * C2 * H1)$$

$$EFF = 1 - (1 - EFD) * SQRT(MD / M)$$

where C1, C2 are conversion constants

## Inputs

<u>Parameter/Port</u>		<u>Description</u>	<u>Units</u>
P	1	Input power	kw
H	1	Height of water above inlet	ft
EFD		Pump efficiency at design pt. (D = 0.90)	-
MD		Mass flow rate at design pt. (D = $2 \times 10^5$ )	gal/h
EF	1	Input product efficiency	-
MP	1	Input maximum charging rate	kw
MM		Maximum allowable mass flow rate (D = $3 \times 10^5$ )	gal/h
CK		Pump capacity cost coefficient <sup>1</sup> (D = 0.011)	
F0		Pump exponent for cost calculations (D = 0.5)	-
Y		Pumphead exponent for cost calculations (D=0.25)	-

## Outputs

<u>Variable/Port</u>			
M		Output mass flow rate	gal/h
EFF		Pump efficiency	-
CC0		Pump cost/year	\$
EF	2	Output product efficiency	-
MP	2	Maximum output power	kw

## Statistics

M2U		Maximum output mass flow rate	gal/h
-----	--	-------------------------------	-------

D - default values

<sup>1</sup>CK = capital cost (known unit)/((MD\*481.2)\*\*F0\*H1 \*\*Y \* expected life time)

The calculation sequence and default values assume a constant speed hydraulic pump nominally rated for 120KW and located 200 ft. below a reservoir. The equations relating the various physical quantities and the cost estimates are based on first principles and the data presented in Reference 1, and the cost estimates on Reference 2.

### Calculation Sequence

$$C1 = 0.377 * 10^{-6} \frac{\text{kwh}}{\text{ft-lb}}$$

$$C2 = 8.3398 \text{ lb/gal}$$

1) Costs (first pass only)

$$CC = CK * (MD * 481.2)^{F0} * H1 * Y$$

- 
1. L. Marks and T. Baumeister, "Mechanical Engineers Handbook", McGraw Hill, N.Y., 1958, Section 14, p. 19.
  2. Carson and Fogleman, "Comparison of Methods for Converting Existing Power Plants to Pumped Storage Facilities", International Engineering Company, Inc., 1974.

## Calculation Sequence Cont.

### 2) Mass flow rate and pump efficiency

If  $P_1 \leq 0$ , set  $EFF = 1$ ,  $M = 0$  and go to 3)

Solve the basic equations for  $M$  and  $EFF$  using:

$$X^3 - XA + B = 0$$

where

$$A = P_1 / (C_1 * C_2 * H_1)$$

$$B = A * (1 - EFD) * \sqrt{MD}$$

$$M = X^2$$

$$EFF = 1 - (1 - EFD) * \sqrt{MD} / X$$

### 3) Product efficiency and maximum charge rate

$$EF_2 = EF_1 * EFF$$

$$MP_2 = \min(MP_1 * EFF, MW * C_1 * C_2 * H_1)$$

### 4) Compute Statistics and Costs

SUBROUTINE PU ENTRY POINT 000216

STORAGE USED CODE(1) 000313; DATA(0) 000033; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CIMPL 000001  
 0004 CTIME 000001  
 0005 CSIMUL 000010  
 0006 COST 000001

EXTERNAL REFERENCES (BLOCK, NAME)

0007 CURIC  
 0010 XPRR  
 0011 SORT  
 0012 NERR3S

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000073	100L	0001	000142	200L	0000 R 000004	ANS	0000 R 000002	A3	0000 R 000003	A4	
0006	R	000000	CCI	0000	R	000001	C1	0005	000000	DUM	0003 I 000000	IMPL
0004	R	000000	TIME	0005	R	000007	TMAX	0000	R	000000	TMAX1	

00100	1*	CPU		000000
00101	2*		SUBROUTINE PU(M,EFF,CC,EF2,MP2,M2U,P1,H1,EFD,HD,EF1,MP1,MM	000000
00101	3*		1	000000
00101	4*	C		000000
00101	5*	C	PURPOSE PERFORMANCE OF HYDRAULIC PUMP	000000
00101	6*	C		000000
00101	7*	C	METHOD COMPUTE PUMP FLOW RATES ASSUMING CONSTANT SPEED WITH	000000
00101	8*	C		000000
00101	9*	C	EFFICIENCY A FUNCTION OF SORT(FLOW RATE)	000000
00101	10*	C		000000
00101	11*	C	WRITTEN BY F. O. MAHONY	000000
00101	12*	C	VERSION 1, MARCH 29 1977	000000
00101	13*	C	CALL SEQUENCE	000000
00101	14*	C	OUTPUTS	000000
00101	15*	C	M - OUTPUT MASS FLOW RATE, GAL/HR	000000
00101	16*	C	EFF - PUMP EFFICIENCY	000000
00101	17*	C	CC - PUMP COST/YEAR, \$	000000
00101	18*	C	EF2 - OUTPUT PRODUCT EFFICIENCY	000000
00101	19*	C	MP2 - MAXIMUM OUTPUT CHARGE RATE, KW	000000
00101	20*	C	M2U - MAXIMUM OUTPUT MASS FLOW RATE, GAL/HR	000000
00101	21*	C		000000
00101	22*	C	INPUTS	000000
			P1 - INPUT POWER, KW	000000

PU

00101	24*	C	H1 - HEIGHT OF WATER ABOVE INLET, FT	000000
00101	25*	C	EFD - PUMP EFFICIENCY AT DESIGN POINT	000000
00101	26*	C	MD - MASS FLOW RATE AT DESIGN POINT, GAL/HR	000000
00101	27*	C	EF1 - INPUT PRODUCT EFFICIENCY	000000
00101	28*	C	MP1 - INPUT MAXIMUM CHARGING RATE, KW	000000
00101	29*	C	MM - MAXIMUM ALLOWABLE MASS FLOW RATE, GAL/HR	000000
00101	30*	C	CK - PUMP CAPACITY COST COEFFICIENT	000000
00101	31*	C	FO - PUMP EXPONENT FOR COST CALCULATIONS	000000
00101	32*	C	Y - PUMP HEAD EXPONENT FOR COST CALCULATIONS	000000
00101	33*	C		000000
00103	34*		COMMON /CIMPL/IMPL /CTIME/TIME/CSIMUL/DUM(7),TMAX /COST/CCI	000000
00103	35*	C		000000
00104	36*		REAL M,MP2,M2U,MD,MP1,MM	000000
00104	37*	C		000000
00105	38*		IF (IMPL.GT.0) GO TO 100	000000
00105	39*	C		000000
00107	40*		TMAX1=TMAX*.999999	000002
00107	41*	C		000002
00110	42*		C1= 3.1441E-6	000005
00110	43*	C		000005
00111	44*		IF (EFD.EQ. .99999) EFD=0.9	000007
00113	45*		IF (MD .EQ. .99999) MD =2.0E5	000014
00115	46*		IF (MP1.EQ. .99999) MP1=1.E8	000021
00117	47*		IF (MM .EQ. .99999) MM =3.0E5	000026
00121	48*		IF (CK .EQ. .99999) CK =0.011	000033
00123	49*		IF (FO .EQ. .99999) FO =0.5	000040
00125	50*		IF (Y .EQ. .99999) Y =0.25	000045
00127	51*		CC =CK*(MD*481.2)**FO*H1**Y	000052
00127	52*	C		000052
00130	53*		M2U =C.0	000071
00131	54*	100	EFF= 1.0	000073
00132	55*		M= 0.0	000074
00133	56*		IF (PI .LE. 0.0) GO TO 200	000075
00133	57*	C		000075
00133	58*	C	SOLVE CUBIC EQUATION FOR M AND EFF	000075
00133	59*	C		000075
00135	60*		A3= -P1/(C1*H1)	000100
00136	61*		A4 =-A3*(1.0-EFD)*SQRT(MD)	000105
00136	62*	C		000105
00137	63*		CALL CUBIC(A3,A4,ANS)	000115
00140	64*		IF (ANS.LT.0.) GO TO 200	000122
00140	65*	C		000122
00142	66*		M =ANS**2	000125
00143	67*		EFF=1.0-(1.0-EFD)*SQRT(MD)/ANS	000130
00143	68*	C		000130
00143	69*	C	PRODUCT EFFICIENCY AND CHARGE RATE	000130
00143	70*	C		000130
00144	71*	200	EF2=EF1*EFF	000142
00145	72*		MP2=AMIN1(MP1*EFF,MM*H1*C1)	000144
00145	73*	C		000144
00146	74*		IF (IMPL.LE.1) RETURN	000156
00146	75*	C		000156
00146	76*	C	STATISTICS	000156
00146	77*	C		000156
00150	78*		M2U=AMAX1(M2U,M )	000165
00150	79*	C		000165
00151	80*		IF (TIME.LT.TMAX1) RETURN	000173

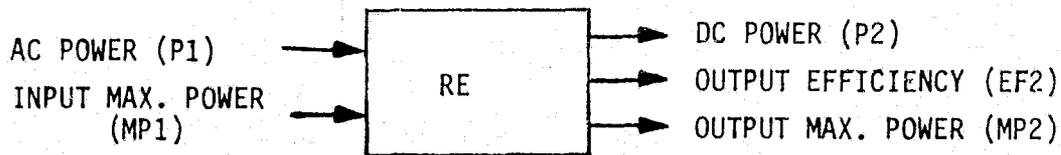
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00151	81*	C	
00153	82*		CCI=CCI*CC
00153	83*	C	
00154	84*		RETURN
00155	85*		END

000173  
000202  
000202  
000205  
000312

## 7.31 AC-DC RECTIFIER



This component models a solid-state rectifier/transformer. Power losses due to resistive heating and contact potential loss are modeled. Default parameter values determining power losses are based on 200 kw rated power.

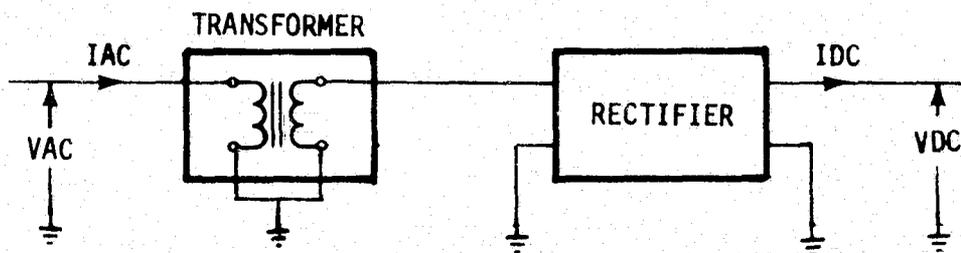


FIGURE 7.31: RECTIFIER FUNCTIONAL DIAGRAM

## Inputs

<u>Parameter/Port</u>		<u>Description</u>	<u>Units</u>
P	1	AC input power	kw
RT		Transformer resistance (D = 0)	ohms
XT		Transformer reactance (D = 0.03)	ohms
VAC		Rated AC voltage (D = 440)	volts
DR		Rectifier contact potential (D = 0)	volts
RR		Rectifier resistance (D = 0.02)	ohms
RAP		Rated input power	kw
EF	1	Input product efficiency	-
MP	1	Maximum input power (D = $1 \cdot 10^8$ )	kw
CC		Rectifier cost/year	\$

## Outputs

### Variable/Port

P	2	DC output power	kw
IAC		AC input current	amps
PL		Power loss	kw
EF	2	Output product efficiency	-
MP	2	Maximum output power	kw

D - Default values supplied.

Calculation Sequence

- 1) Compute transformer power angles

$$Y = \sin(\theta) = \sqrt{3} * X_T * P_1 * 1000 / VAC^2$$

$$ABS(Y) > 1 \Rightarrow \text{DIAGNOSTIC}$$

- 2) Input and output current

If  $P_1 \leq 0$  set  $P_2 = IAC = PL = 0.$ ,  $EFF = 1$  and go to 4)

$$IAC = VAC \sqrt{2 - 2\cos(\theta)} / (\sqrt{3} * X_T)$$

$$" = VAC \sqrt{2 - 2 * \sqrt{1 - Y^2}} / (\sqrt{3} * X_T)$$

$$IDC = \pi * IAC / \sqrt{6}$$

- 3) Power loss and output power

$$PL = (\sqrt{3} * R_T * IAC^2 + IDC * (DR + IDC * RR)) / 1000$$

$$P_2 = P_1 - PL$$

$$EFF = P_2 / P_1$$

$$P_2 \leq 0 \Rightarrow \text{DIAGNOSTIC, } EFF = 1$$

- 4) Efficiency and maximum power

$$EF_2 = EF_1 * EFF$$

$$MP_2 = \min(MP_1, RAP) * EFF$$

- 5) Compute Costs



00101	23*	C	DR -RECTIFIER CONTACT POTENTIAL, VOLTS	000000
00101	24*	C	RR -RECTIFIER RESISTANCE, OHMS	000000
00101	25*	C	RAP -RATED INPUT POWER, KW	000000
00101	26*	C	EF1 -INPUT PRODUCT EFFICIENCY	000000
00101	27*	C	MP1 -MAXIMUM INPUT POWER, KW	000000
00101	28*	C	CC -RECTIFIER COST/YEAR, \$	000000
00101	29*	C		000000
00103	30*		COMMON /CIMPL/IMPL,ICNT/CTIME/TIME/CSIMUL/DUM(7),TMAX/COST/CCI	000000
00104	31*		REAL IAC,MP2,MP1,IDC	000000
00105	32*		DATA PI/3.14159/	000000
00107	33*		DATA ROOT3/1.73205/	000000
00107	34*	C		000000
00111	35*		IF(IMPL.GT.0) GO TO 100	000000
00113	36*		IF(MP1.EQ..99999)MP1=1.E8	000002
00115	37*		IF(RT.EQ..99999) RT=0.	000007
00117	38*		IF(XT.EQ..99999) XT=.03	000013
00121	39*		IF(VAC.EQ..99999) VAC=440.	000020
00123	40*		IF(DR.EQ..99999) DR=0.	000025
00125	41*		IF(RR.EQ..99999) RR=.02	000031
00127	42*		TMAX1=TMAX*.99999	000036
00127	43*	C		000036
00127	44*	C	COMPUTE TRANSFORMER POWER ANGLES	000036
00127	45*	C		000036
00130	46*		100 Y=ROOT3*XT*PI*1000./(VAC*VAC)	000042
00131	47*		YY=Y*Y	000051
00132	48*		IF(YY.LE.1.)GO TO 200	000053
00134	49*		IF(IMPL.EQ.2)WRITE(6,108)PI,XT,VAC	000056
00142	50*		108 FORMAT(1HG,19HRE, AC INPUT POWER ,F12.3,49H TOO LARGE IN RELATION	000071
00142	51*		1TO TRANSFORMER REACTANCE ,F12.3,22H AND RATED AC VOLTAGE ,F12.3)	000071
00143	52*		IF(IMPL.EQ.2)ICNT=ICNT+1	000071
00145	53*		200 YY=AMIN(1.,YY)	000100
00145	54*	C		000100
00145	55*	C	INPUT AND OUTPUT CURRENT	000100
00145	56*	C		000100
00146	57*		IF(P1.GT.0.)GO TO 300	000105
00150	58*		P2=0.	000110
00151	59*		IAC=0.	000111
00152	60*		PL=0.	000112
00153	61*		EFF=1.	000113
00154	62*		GO TO 400	000115
00154	63*	C		000115
00155	64*		300 IAC=VAC*SQRT(2.-2.*SQRT(1.-YY))/(ROOT3*XT)	000117
00156	65*		IDC=PI*IAC/SQRT(6.)	000140
00156	66*	C		000140
00156	67*	C	POWER LOSS AND OUTPUT POWER	000140
00156	68*	C		000140
00157	69*		PL=(ROOT3*RT*IAC*IAC+IDC*(DR+IDC*RR))/1000.	000147
00160	70*		P2=P1-PL	000161
00161	71*		EFF=P2/P1	000163
00162	72*		IF(P2.GT.0.) GO TO 400	000165
00164	73*		IF(IMPL.EQ.2)WRITE(6,308)PL,P1	000170
00171	74*		308 FORMAT(1HG,14HRE POWER LOSS ,F12.3,21H EXCEEDS INPUT POWER ,F12.3)	000202
00172	75*		IF(IMPL.EQ.2)ICNT=ICNT+1	000202
00174	76*		P2=0.	000210
00175	77*		EFF=1.	000211
00175	78*	C		000211
00175	79*	C	EFFICIENCY AND MAXIMUM POWER	000211

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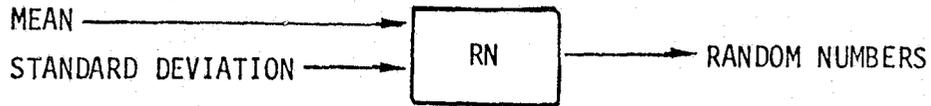
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```
00175 80* C
00176 81* *00 EF2=EF1*EFF
00177 82* MP2=AMIN1(MP1,RAP)
00200 83* MP2=MP2*EFF
00201 84* IF(IMPL.LE.1)RETURN
00203 85* IF(TIME.LT.TMAX1)RETURN
00205 86* CCI=CCI+CC
00205 87* C
00206 88* RETURN
00207 89* END
```

```
G00211
000214
000216
C00224
C00226
000235
G00244
000244
000247
000351
```

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## 7.32 RANDOM NUMBERS



This component generates an uncorrelated sequence of normally distributed random numbers with a specified mean and standard deviation.

### Inputs

#### Parameter/Port

#### Description

MN	Mean value of sequence
SIG	Standard deviation of sequence
NST <sup>1</sup>	Start parameter. (Use any odd integer greater than 1). Default supplied.

### Outputs

#### Variable/Port

F0	Random number output
----	----------------------

---

<sup>1</sup> If RESET parameter > 0 then succeeding simulations use NST to start random sequence.

200

SUBROUTINE RN ENTRY POINT 000065

STORAGE USED CODE(1) 000105; DATA(0) 000033; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CIMPL 000003

EXTERNAL REFERENCES (BLOCK, NAME)

0004 NEPR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

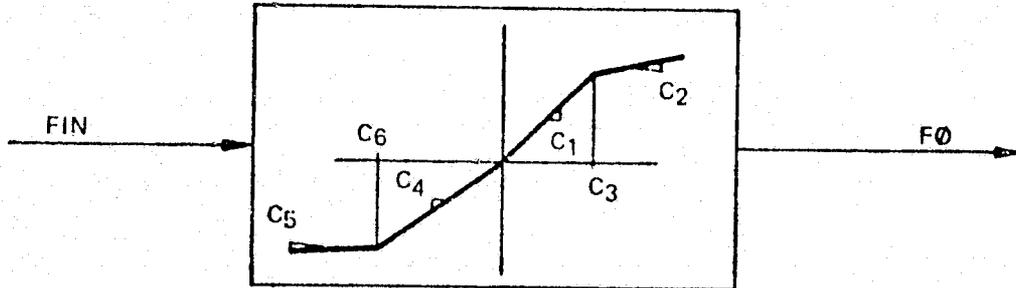
0001	000026	1236	0001	000021	5L	0000	R	000006	AXO	0000	I	000007	I	0003	000001	ICNT		
0003	I	000000	IMPL	0000	000024	INJP5	0003	I	000002	ITEST	0000	D	000004	SUM	0000	D	000000	X
0000	D	000002	Y															

00100	1*	CRN		000000
00101	2*		SUBROUTINE RN(U,AX,SIG,AMN)	000000
00101	3*	C	VERSION 2. REVISED MAY 1977	000000
00101	4*	C	PURPOSE - GENERATES A NORMALLY DISTRIBUTED RANDOM NUMBER	000000
00101	5*	C	CALL SEQUENCE	000000
00101	6*	C	U - RANDOM NUMBER OUTPUT	000000
00101	7*	C	AX- A START PARAMETER WHICH CONTROLS THE BEGINNING POINT	000000
00101	8*	C	OF THE OUTPUT SEQUENCE. AX SHOULD BE ANY ODD INTEGER	000000
00101	9*	C	GREATER THAN ONE. THE DEFAULT VALUE OF AX IS 431469.	000000
00101	10*	C	AX IS UPDATED FOR NEW CALLS TO THE SUBROUTINE.	000000
00101	11*	C	SIG- THE DESIRED STANDARD DEVIATION OF THE SEQUENCE	000000
00101	12*	C	AMN- THE DESIRED MEAN OF THE SEQUENCE	000000
00101	13*	C		000000
00101	14*	C	DESIGNED BY ROGER W. CALL	000000
00101	15*	C	COMMON /CIMPL/IMPL,ICNT,ITEST	000000
00104	16*	C	DOUBLE PRECISION X,Y,SUM	000000
00105	17*	C	DATA Y /253967.00/ AX0/D./	000000
00110	18*	C	IF(IMPL.GT.0160 TO 5	000000
00112	19*	C	IF(AX.EQ..999999) AX=431469.	000000
00114	20*	C	IF(AX0.EQ.0.) AX0= AX	000007
00116	21*	C	IF(ITEST.EQ.1) AX= AX0	000013
00120	22*	5	X =AX	000021
00121	23*	C	SUM=0.00	000022
00122	24*	C	DO 1 I=1,12	000026
00125	25*	C	X= DMOD(X*Y,16777216.00)	000026
00126	26*	1	SUM= SUM+ X/16777215.00	000036
00130	27*	C	AX= X	000043
00131	28*	C	U=(SUM*-6.C)*SIG+AMN	000045
00132	29*	C	RETURN	000054
00133	30*	C	END	000104

**RN**

BCS 40180-2

## 7.33 SATURATION FUNCTION



### Inputs

<u>Parameter/Port</u>	<u>Description</u>
FIN	Input quantity
C1	Slope $0 < FIN < C3$
C2	Slope $FIN > C3$
C3	Positive saturation intercept
C4	Slope $0 > FIN > C6$
C5	Slope $FIN < C6$
C6	Negative saturation intercept

### Outputs

<u>Variable/Port</u>	<u>Description</u>
F0	Output quantity

### Calculation Sequence

$$\begin{aligned}
 F_0 &= C_1 * C_3 + C_2 * (FIN - C_3) && \text{if } FIN > C_3 \\
 F_0 &= C_1 * FIN && \text{if } 0 < FIN < C_3 \\
 F_0 &= C_4 * FIN && \text{if } 0 > FIN > C_6 \\
 F_0 &= C_4 * C_6 + C_5 * (FIN - C_6) && \text{if } FIN < C_6
 \end{aligned}$$

SUBROUTINE SA ENTRY POINT 000051

STORAGE USED CODE(1) 000076; DATA(0) 000013; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000017 10L 0001 000042 100L 0001 000027 20L 0001 000037 30L 0000 000000 INJPS

```

00100      1*      CSA
00101      2*      SUBROUTINE SA(F0,FIN,C1,C2,C3,C4,C5,C6)
00101      3*      C
00101      4*      C PURPOSE - TO SIMULATE SATURATION
00101      5*      C
00101      6*      C
00101      7*      C METHOD - SEE CODING. C3 AND C6 ARE VALUES OF THE INPUT AT WHICH
00101      8*      C SATURATION OCCURS. C3 IS GREATER THAN C6. THE ROUTINE
00101      9*      C CAN SIMULATE A CHANGE OF SLOPE AT THE ORIGIN (C1,NE,C4)
00101     10*      C PROVIDED C6 IS LESS THAN ZERO. SIMILARLY THE SLOPES
00101     11*      C IN THE SATURATION REGION (C2 AND C5) CAN DIFFER.
00101     12*      C THE SLOPES CAN BE POSITIVE OR NEGATIVE
00101     13*      C
00101     14*      C
00101     15*      C WRITTEN BY - ADAM LLOYD LATEST REVISION - NOV 75
00101     16*      C
00101     17*      C LIMITATIONS - USE OF ZERO SLOPES (C2=0 OR C5=0) IN THE SATURATION
00101     18*      C REGION SHOULD BE AVOIDED. IT IS DESIRABLE THAT THE
00101     19*      C SLOPE RATIOS C1/C2 AND C4/C5 SHOULD NOT EXCEED 100.
00101     20*      C EXCESSIVE SLOPE RATIOS MAY RESULT IN VERY SLOW
00101     21*      C CONVERGENCE
00101     22*      C
00101     23*      C
00101     24*      C INPUT/OUTPUT LIST
00101     25*      C
00101     26*      C F0          OUTPUT VARIABLE          ANY          OUTPUT VAR
00101     27*      C FIN          INPUT VARIABLE           ANY          INPUT VAR
00101     28*      C C1          SLOPE                   ) FIRST    ANY          INPUT PARAM
00101     29*      C C2          SATURATION SLOPE         ) SLOPE    ANY          INPUT PARAM
00101     30*      C C3          SATURATION INTERCEPT ) ANY          INPUT PARAM
00101     31*      C C4          SLOPE                   ) SECOND  ANY          INPUT PARAM
00101     32*      C C5          SATURATION SLOPE         ) SLOPE    ANY          INPUT PARAM
00101     33*      C C6          SATURATION INTERCEPT ) ANY          INPUT PARAM
00101     34*      C
00103     35*      IF(FIN.GT.C3)GO TO 10

```

SA

```

00105 36*      IF(FIN.LT.C6)GO TO 20
00107 37*      IF(FIN.LT.C.160 TO 30
00111 38*      FO=C1*FIN
00112 39*      GO TO 100
00112 40*      C POSITIVE SATURATION
00113 41*      10 FO=C1*C3+C2*(FIN-C3)
00114 42*      GO TO 100
00114 43*      C NEGATIVE SATURATION
00115 44*      20 FO=C4*C6+C5*(FIN-C6)
00116 45*      GO TO 100
00116 46*      C NEGATIVE UNSATURATED
00117 47*      30 FO=C4*FIN
00120 48*      100 RETURN
00121 49*      END

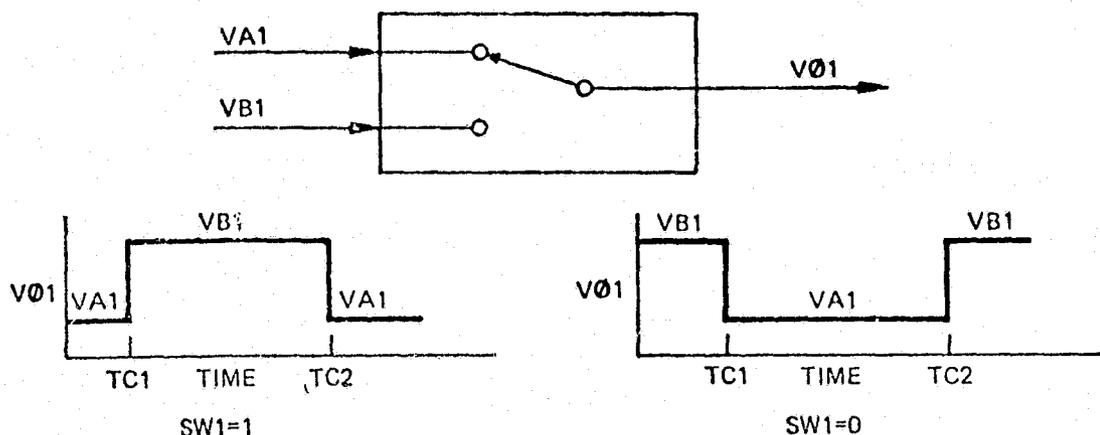
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```

000003
000007
000012
000015
000015
000017
000025
000025
000027
000035
000035
000037
000042
000075

```

## 7.34 SINGLE POLE SWITCH



THE SWITCHING OPERATION MAY BE CONTROLLED BY EITHER TIME OR THE INPUT PARAMETER SW1. THE TIME DEPENDENCE MAY BE ELIMINATED BY SETTING  $TC1 = 10^{36}$

### Inputs

<u>Parameter/Port</u>	<u>Description</u>
VA1	Input to switch
VB1	Input to switch
SW1	Switch control parameter
TC1	Time for first switching (hours)
TC2	Time for second switching (hours)

### Outputs

<u>Variable/Port</u>	
V01	Switch output

### Calculation Sequence

$$\text{If } SW1 = 0 \text{ then } V01 = \begin{pmatrix} VA1 & TC1 < TIME < TC2 \\ VB1 & \text{otherwise} \end{pmatrix}$$

$$\text{If } SW1 = 1 \text{ then } V01 = \begin{pmatrix} VB1 & TC1 < TIME < TC2 \\ VA1 & \text{otherwise} \end{pmatrix}$$

SUBROUTINE SW ENTRY POINT 000C42

STORAGE USED CODE(1) 000047; DATA(0) 000007; BLANK COMMON(2) 000000

## COMMON BLOCKS

```

0003 CTIME 000001
0004 CIO 000003

```

## EXTERNAL REFERENCES (BLOCK, NAME)

0005 NERR35

## STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

```

0004 000002 IDIAG 0000 000003 INJPS 0004 000000 IREAD 0004 000001 IWRITE 0000 R 000000 SX
0003 R 000000 TIME

```

```

00100 1* CSW 000000
00101 2* SUBROUTINE SW(V01,VA1,V01,SW1,TC1,TC2) 000000
00101 3* C 000000
00101 4* C PURPOSE - TO PROVIDE SWITCH CONTROL FOR ONE VARIABLE 000000
00101 5* C 000000
00101 6* C 000000
00101 7* C METHOD - SEE CODING 000000
00101 8* C 000000
00101 9* C 000000
00101 10* C WRITTEN BY - ADAM LLOYD LATEST REVISION NOV 75 000000
00101 11* C 000000
00101 12* C 000000
00101 13* C LIMITATIONS - NOT MORE THAN TWO SWITCHINGS AT TIMES TC1 AND TC2 000000
00101 14* C 000000
00101 15* C 000000
00101 16* C INPUT/OUTPUT LIST 000000
00101 17* C 000000
00101 18* C V01 OUTPUT VARIABLE NO 1 ANY OUTPUT VAR 000000
00101 19* C VA1 INPUT VARIABLE NO A1 ANY INPUT VAR 000000
00101 20* C V01 INPUT VARIABLE NO B1 ANY INPUT VAR 000000
00101 21* C SW1 SWITCH CONTROL INITIAL VALUE --- INPUT PARAM 000000
00101 22* C =1. V0=VR 000000
00101 23* C =0. V0=VA 000000
00101 24* C TC1 TIME FOR FIRST SWITCH SECS INPUT PARAM 000000
00101 25* C TC2 TIME FOR SECOND SWITCH SECS INPUT PARAM 000000
00101 26* C (TC2.GT.TC1) 000000
00103 27* COMMON/CTIME/TIME 000000
00104 28* COMMON/CIO/IREAD,IWRITE,IDIAG 000000
00105 29* SX=SW1 000000

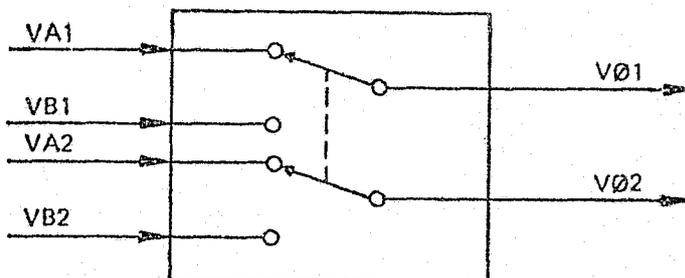
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MS

```
00106 30* IF(TIME.GT.TC1.AND.TIME.LT.TC2)SX=ABS(SW1-1.)
00110 31* V01=VA1
00111 32* IF(SX.GT.0.5)V01=VB1
00113 33* RETURN
00114 34* END
```

```
C00001
C00023
000025
000033
C00046
```

## 7.35 TWO POLE SWITCH



SEE SW FOR SWITCH CONTROL LOGIC

### Inputs

#### Parameter/Port

#### Description

VA1	Input to switch 1
VA2	Input to switch 2
VB1	Input to switch 1
VB2	Input to switch 2
SW1	Switch control parameter
TC1	Time for first switching (hours)
TC2	Time for second switching (hours)

### Outputs

#### Variable/Port

VØ1	Output from switch 1
VØ2	Output from switch 2

SUBROUTINE SX

ENTRY POINT 000052

STORAGE USED CODE(1) 000062; DATA(0) 000007; BLANK COMMON(2) 000000

## COMMON BLOCKS

0003 CTIME 000001  
 0004 CIO 000003

## EXTERNAL REFERENCES (BLOCK, NAME)

0005 NERR3

## STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0004 000002 IDIAG 0000 000003 INJPS 0004 000000 IREAD 0004 000001 IWRITE 0000 R 000000 SW  
 0003 R 000000 TIME

00100	1*	CSX						000000
00101	2*		SUBROUTINE SX(V01,V02,VA1,VA2,VB1,VR2,SW1,TC1,TC2)					000000
00101	3*	C						000000
00101	4*	C	PURPOSE - TO PROVIDE A SWITCH COMPONENT FOR TWO VARIABLES					000000
00101	5*	C						000000
00101	6*	C						000000
00101	7*	C	METHOD - SEE CODING					000000
00101	8*	C						000000
00101	9*	C						000000
00101	10*	C	WRITTEN BY - ADAM LLOYD		LATEST REVISION		NOV 75	000000
00101	11*	C						000000
00101	12*	C						000000
00101	13*	C	LIMITATIONS - NOT MORE THAN TWO SWITCHINGS AT TIMES TC1 AND TC2					000000
00101	14*	C						000000
00101	15*	C						000000
00101	16*	C	INPUT/OUTPUT LIST					000000
00101	17*	C						000000
00101	18*	C	V01	OUTPUT VARIABLE NO 1	ANY	OUTPUT	VAR	000000
00101	19*	C	V02	OUTPUT VARIABLE NO 2	ANY	OUTPUT	VAR	000000
00101	20*	C	VA1	INPUT VARIABLE NO A1	ANY	INPUT	VAR	000000
00101	21*	C	VA2	INPUT VARIABLE NO A2	ANY	INPUT	VAR	000000
00101	22*	C	VB1	INPUT VARIABLE NO B1	ANY	INPUT	VAR	000000
00101	23*	C	VB2	INPUT VARIABLE NO B2	ANY	INPUT	VAR	000000
00101	24*	C	SW1	SWITCH CONTROL INITIAL VALUE	---	INPUT	PARAM	000000
00101	25*	C		=1. V0=VB				000000
00101	26*	C		=C. V0=VA				000000
00101	27*	C	TC1	TIME FOR FIRST SWITCH	SECS	INPUT	PARAM	000000
00101	28*	C	TC2	TIME FOR SECOND SWITCH	SECS	INPUT	PARAM	000000
00101	29*	C		(TC2.GT.TC1)				000000

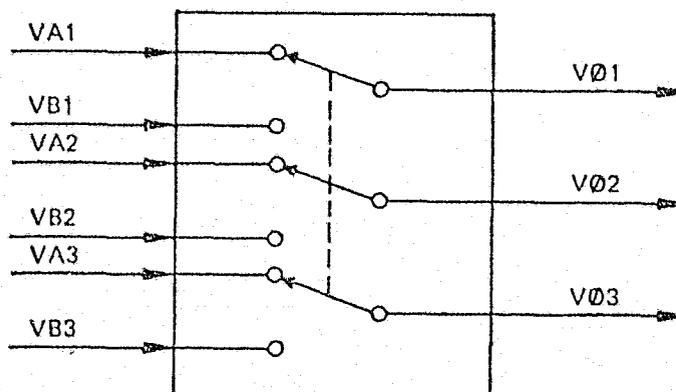
SX

```
00103 30* COMMON/CTIME/TIME
00104 31* COMMON/CIO/IREAD,IWRITE,IDIAS
00105 32* SW=SW1
00106 33* IF (TIME.GT.TC1.AND.TIME.LT.TC2)SW=ABS(SW1-1.)
00110 34* V01=VA1
00111 35* V02=VA2
00112 36* IF(SW.GT.0.5)V01=VB1
00114 37* IF(SW.GT.0.5)V02=VB2
00116 38* RETURN
00117 39* END
```

```
C00000
C00000
C00000
C00001
C00023
C00025
000027
C00035
000043
C00061
```

**SX**

## 7.36 THREE POLE SWITCH



SEE SW FOR SWITCH CONTROL LOGIC

### Inputs

#### Parameter/Port

#### Description

VA1	Input to switch 1
VA2	Input to switch 2
VA3	Input to switch 3
VB1	Input to switch 1
VB2	Input to switch 2
VB3	Input to switch 3
SW1	Switch control parameter
TC1	Time for first switching (hours)
TC2	Time for second switching (hours)

### Outputs

#### Variable/Port

VØ1	Output from switch 1
VØ2	Output from switch 2
VØ3	Output from switch 3

SUBROUTINE SY ENTRY POINT 000063

STORAGE USED CODE(1) 000077; DATA(0) 000011; BLANK COMMON(2) 000000

## COMMON BLOCKS

0003 CTIME 000001  
 0004 CIO 000003

## EXTERNAL REFERENCES (BLOCK, NAME)

0005 NERR33

## STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0004 000002 IDIAG 0000 000003 INJPS 0004 000000 IREAD 0004 000001 IWRITE 0000 R 000000 SW  
 0003 R 000000 TIME

```

00100 1* CSY
00101 2* SUBROUTINE SY(V01,V02,V03,VA1,VA2,VA3,VB1,VB2,VB3,SW1,TC1,TC2)
00101 3* C
00101 4* C PURPOSE - TO PROVIDE A SWITCH COMPONENT FOR THREE VARIABLES
00101 5* C
00101 6* C
00101 7* C METHOD - SEE CODING
00101 8* C
00101 9* C
00101 10* C WRITTEN BY - ADAM LLOYD LATEST REVISION NOV 75
00101 11* C
00101 12* C
00101 13* C LIMITATIONS - NOT MORE THAN TWO SWITCHINGS AT TIMES TC1 AND TC2
00101 14* C
00101 15* C
00101 16* C INPUT/OUTPUT LIST
00101 17* C
00101 18* C V01 OUTPUT VARIABLE NO 1 ANY OUTPUT VAR 000000
00101 19* C V02 OUTPUT VARIABLE NO 2 ANY OUTPUT VAR 000000
00101 20* C V03 OUTPUT VARIABLE NO 3 ANY OUTPUT VAR 000000
00101 21* C VA1 INPUT VARIABLE NO A1 ANY INPUT VAR 000000
00101 22* C VA2 INPUT VARIABLE NO A2 ANY INPUT VAR 000000
00101 23* C VA3 INPUT VARIABLE NO A3 ANY INPUT VAR 000000
00101 24* C VB1 INPUT VARIABLE NO B1 ANY INPUT VAR 000000
00101 25* C VB2 INPUT VARIABLE NO B2 ANY INPUT VAR 000000
00101 26* C VB3 INPUT VARIABLE NO B3 ANY INPUT VAR 000000
00101 27* C SW1 SWITCH CONTROL INITIAL VALUE --- INPUT PARAM 000000
00101 28* C =1. VG=VB 000000
00101 29* C =0. VG=VA 000000

```

SY

				SECS	INPUT	PARAM	
00101	30*	C	TC1				000000
00101	31*	C	TC2				000000
00101	32*	C					000000
00103	33*						000000
00104	34*						000000
00105	35*						000000
00106	36*						000001
00107	37*						000003
00110	38*						000005
00111	39*						000007
00113	40*						000031
00115	41*						000037
00117	42*						000045
00121	43*						000053
00122	44*						000076

```

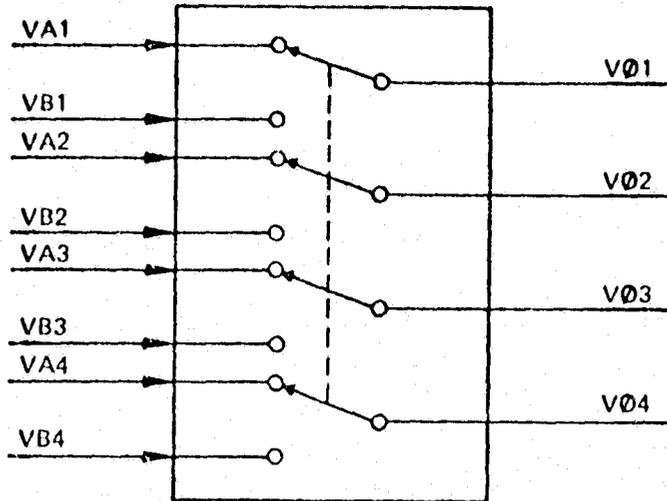
COMMON/CTIME/TIME
COMMON/CIO/IREAD,IWRITE,IDIAG
SW=SW1
V01=VA1
V02=VA2
V03=VA3
IF (TIME.GT.TC1.AND.TIME.LT.TC2)SW=ABS(SW1-1.)
IF (SW.GT.0.5)V01=VB1
IF (SW.GT.0.5)V02=VB2
IF (SW.GT.0.5)V03=VB3
RETURN
END

```

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SY

7.37 FOUR POLE SWITCH



SEE SW FOR SWITCH CONTROL LOGIC

Inputs

Parameter/Port

Description

VA1	Input to switch 1
VA2	Input to switch 2
VA3	Input to switch 3
VA4	Input to switch 4
VB1	Input to switch 1
VB2	Input to switch 2
VB3	Input to switch 3
VB4	Input to switch 4
SW1	Switch control parameter
TC1	Time for first switching (hours)
TC2	Time for second switching (hours)

Outputs

Variable/Port

V01	Output from switch 1
V02	Output from switch 2
V03	Output from switch 3
V04	Output from switch 4

SUBROUTINE SZ ENTRY POINT 000073

STORAGE USED CODE(1) 000112; DATA(0) 000011; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CTIME 000001  
0004 CIO 000003

EXTERNAL REFERENCES (BLOCK, NAME)

0005 HERR3X

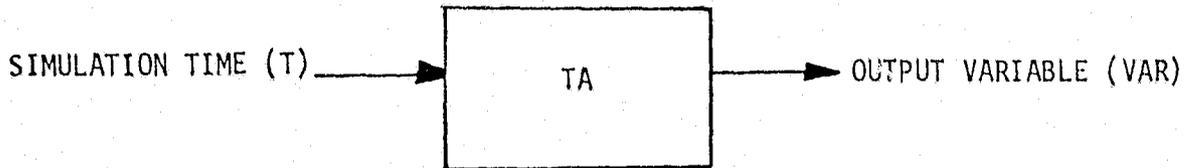
STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0004 000002 INIAG 0000 000003 INJPS 0004 000000 IREAD 0004 000001 IWRITE 0000 R 000000 SM  
0003 R 000000 TIME

00100	1*	CSZ				000000	
00101	2*		SUBROUTINE SZ (V01,V02,V03,V04,VA1,VA2,VA3,VA4,VB1,VB2,VB3,VB4,			000000	
00101	3*		1 SW1,TC1,TC2)			000000	
00101	4*	C				000000	
00101	5*	C	PURPOSE - TO PROVIDE A SWITCH COMPONENT FOR FOUR VARIABLES			000000	
00101	6*	C				000000	
00101	7*	C				000000	
00101	8*	C	METHOD - SEE CODING			000000	
00101	9*	C				000000	
00101	10*	C				000000	
00101	11*	C	WRITTEN BY - ADAM LLOYD	LATEST REVISION	NOV 75	000000	
00101	12*	C				000000	
00101	13*	C				000000	
00101	14*	C	LIMITATIONS - NOT MORE THAN TWO SWITCHINGS AT TIMES TC1 AND TC2			000000	
00101	15*	C				000000	
00101	16*	C				000000	
00101	17*	C	INPUT/OUTPUT LIST			000000	
00101	18*	C				000000	
00101	19*	C	V01	OUTPUT VARIABLE NO 1	ANY	OUTPUT VAR	000000
00101	20*	C	V02	OUTPUT VARIABLE NO 2	ANY	OUTPUT VAR	000000
00101	21*	C	V03	OUTPUT VARIABLE NO 3	ANY	OUTPUT VAR	000000
00101	22*	C	V04	OUTPUT VARIABLE NO 4	ANY	OUTPUT VAR	000000
00101	23*	C	VA1	INPUT VARIABLE NO A1	ANY	INPUT VAR	000000
00101	24*	C	VA2	INPUT VARIABLE NO A2	ANY	INPUT VAR	000000
00101	25*	C	VA3	INPUT VARIABLE NO A3	ANY	INPUT VAR	000000
00101	26*	C	VA4	INPUT VARIABLE NO A4	ANY	INPUT VAR	000000
00101	27*	C	VB1	INPUT VARIABLE NO B1	ANY	INPUT VAR	000000
00101	28*	C	VB2	INPUT VARIABLE NO B2	ANY	INPUT VAR	000000

00101	30*	C	VB4	INPUT VARIABLE NO B*	ANY	INPUT	VAR	000000
00101	31*	C	SW1	SWITCH CONTROL INITIAL VALUE	---	INPUT	PARAM	000000
00101	32*	C		=1. VO=VB				000000
00101	33*	C		=0. VO=VA				000000
00101	34*	C	TC1	TIME FOR FIRST SWITCH	SECS	INPUT	PARAM	000000
00101	35*	C	TC2	TIME FOR SECOND SWITCH	SECS	INPUT	PARAM	000000
00101	36*	C		(TC2.GT.TC1)				000000
00103	37*			COMMON/CTIME/TIME				000000
00104	38*			COMMON/CIO/IREAD, IWRITE, IDIAG				000000
00105	39*			SW=SW1				000000
00106	40*			IF(TIME.GT.TC1.AND.TIME.LT.TC2)SW=ABS(SW1-1.)				000001
00110	41*			V01=VA1				000023
00111	42*			V02=VA2				000025
00112	43*			V03=VA3				000027
00113	44*			V04=VA4				000031
00114	45*			IF(SW.GT.0.5)V01=VB1				000033
00116	46*			IF(SW.GT.0.5)V02=VB2				000041
00120	47*			IF(SW.GT.0.5)V03=VB3				000047
00122	48*			IF(SW.GT.0.5)V04=VB4				000055
00124	49*			RETURN				000063
00125	50*			END				000111

## 7.38 TAPE/FILE READ



This component reads a data file containing a single output variable time history. The file structure is specified below, and assumes equal increment data. Linear interpolation is used to obtain the output value. No more than eight TA components are allowed per model. The component TI is used to supply the time input T. The data files must be catalogued using the names F1, F2, or the JCL procedure file XQTANALYSIS modified appropriately. If tape data is used, it must be read into permanent storage files in a prior job step.

### Inputs

<u>Parameter/Port</u>	<u>Description</u>	<u>Units</u>
NST	Number of records to skip at start <sup>1</sup>	
T	Simulation time referenced to start of year	hr
ITF	Indicator function: 0 = no read J = read data into Jth array (J ≤ 8)	

<sup>1</sup> NST = (start time of simulation - start time of file) / (data increment × 446)

## Outputs

<u>Variable/Port</u>	<u>Description</u>	<u>Units</u>
VAR	Output variable at time T	
N	Length of file record	
T0	Time of first data value in current record	hr
H	Time increment between data values	hr

## Record Structure

1st record = identification header, 28 words

Nth record ( $N > 1$ ): 448 words

first word = time of first data value in hours ( $T_0$ )

second word = time increment between data values ( $H$ )

$J+2$  word = data value at time =  $T_0 + (J-1)H$

( $J=1, \dots, 446$ )

If the useful data ends in the middle of a record, then an end value = .99999 is used to signal end of information.

## Calculation Sequence

If ITF = 0 RETURN

1) Initialization. (First Pass Only)

o Read 1st record and write out identification header data and unit number. (Error exit to 6)

o Read past NST data records. Go to 4)

Calculation Sequence Cont.

2) File location incorrect; use initial value

- o If  $T \geq T_0$  GO TO 3)
  - Write diagnostic
  - VAR = A(1,J) (J=ITF)
  - Return

3) Table Interpolation for Output

- o If  $T \geq T_0 + N * H$  GO TO 4)
  - XT(1) =  $T_0$
  - XT(2) =  $T_0 + H$
  - VAR = TBLU1(T,XT,A(1,J),O,N)
  - Return

4) Read Next Data Record

If end has been encountered previously go to 5)  
 Read next record into array A(\*,J). If end encountered, set  
 N = last value. (Error exit to 6))  
 $T_0 = A(1,J)$   
 $H = A(2,J)$   
 GO TO 3)

5) End of File. Use last value.

VAR = A(N,J)  
 Write Diagnostic  
 Return

6) Read Error Encountered

Write Diagnostic and STOP

SUBROUTINE TA ENTRY POINT 000343

STORAGE USED CODE(1) 000403; DATA(1) 007132; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CIMPL 000002  
 0004 DATARD 000700

EXTERNAL REFERENCES (BLOCK, NAME)

0005 NTRAM  
 0006 TBLU1  
 0007 NWDUS  
 0010 J103%  
 0011 N102%  
 0012 NSTOP%  
 0013 NERR3%

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000321	10L	0001	000102	100L	0001	000231	1676	0000	007035	20F	0001	000135	200L	
0000	007046	30F	0001	000176	300L	0001	000262	400L	0001	000244	60L	0000	007062	80F	
0000	007076	90F	0000	R	000000	A	0000	R	006760	B	0000	I	007034	I	
0003	I	000000	IMPL	0000	I	007014	IND	0000	007121	INJPS	0000	I	007030	IUN	
0000	I	007031	L1	0000	I	007033	N	0000	I	007032	NO	0006	R	000000	TBLU1
0000	R	007026	X	0000	R	007024	XT					0004	R	000000	TEMP

00100	1*	CTAPE													000000
00101	2*		SUBROUTINE	TA(	VAR,	HOUT,	TO,	M,	NST,	T,	ITF)				000000
00101	3*	C													000000
00101	4*	C	PURPOSE			READ	TIME	HISTORY	DATA	ON	STORAGE	DEVICE			000000
00101	5*	C													000000
00101	6*	C													000000
00101	7*	C	METHOD			USE	NTRAM	SEQUENTIAL	BLOCK	READ	FROM	MASS	STORAGE		000000
00101	8*	C				INTO	CORE.	LINFAR	INTERPOLATION	IS	USED	TO	OBTAIN		000000
00101	9*	C				VALUE	AT	SPECIFIED	TIME	T.					000000
00101	10*	C													000000
00101	11*	C	WRITTEN	BY	A.W.	WARREN				JUNE	1977				000000
00101	12*	C													000000
00101	13*	C	CALL	SEQUENCE											000000
00101	14*	C				OUTPUTS									000000
00101	15*	C				VAR	-	OUTPUT	VARIABLE	AT	TIME	T			000000
00101	16*	C				HOUT	-	LENGTH	OF	DATA	BLOCK	LAST	READ		000000
00101	17*	C				TO	-	TIME	OF	FIRST	DATA	VALUE	IN	CORE,	HR
00101	18*	C				H	-	TIME	INCREMENT	BETWEEN	DATA	VALUES,	HR		000000
00101	19*	C				INPUTS									000000

TA

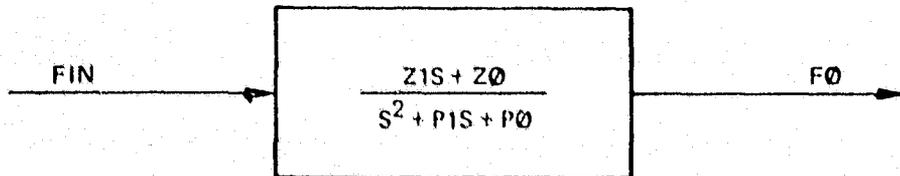


00171	77*	IF(TEMP(I+2).EQ.X)GO TO 60	000231
00173	78*	50 A(I,J)= TEMP(I+2)	000234
00175	79*	I=I+1	000240
00176	80*	60 NCUT= I-1	000244
00177	81*	IF(I.LT.447)IND(J)=0	000250
00201	82*	60 TO 200	000260
00201	83*	C	000260
00201	84*	C	000260
00201	85*	C	000260
00201	86*	C	000260
00202	87*	400 N= NCUT	000262
00203	88*	VAR=A(N,J)	000270
00204	89*	IF(IMPL.EQ.2)WRITE(6,80)VAR,IUN	000275
00211	90*	80 FORMAT(1H0,41HTIME POINT PAST TABLE RANGE. LAST VALUE= ,	000307
00211	91*	1 F12.5,9H ON UNIT,I4)	000307
00212	92*	IF(IMPL.EQ.2)ICNT=ICNT+1	000307
00214	93*	RETURN	000315
00214	94*	C	000315
00214	95*	C	000315
00214	96*	C	000315
00215	97*	10 WRITE(6,90)IUN	000321
00220	98*	90 FORMAT(1H0,33HREAD ERROR OR END OF FILE ON UNIT,I4)	000326
00221	99*	STOP	000326
00222	100*	END a SUBROUTINE TA	000402

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TA

## 7.39 SECOND ORDER TRANSFER FUNCTION



### Inputs

<u>Parameter/Port</u>	<u>Description</u>
FIN	Input quantity
Z0	Numerator coefficient
Z1	Numerator coefficient
P0	Denominator coefficient
P1	Denominator coefficient

### Outputs

<u>Variable/Port</u>	<u>Description</u>
X1	Intermediate state
F0	Output quantity (state)

### Calculation Sequence

$$\dot{X}_1 = Z_0 * FIN - P_0 * F_0$$

$$\dot{F}_0 = X_1 + Z_1 * FIN - P_1 * F_0$$

NOTE: d.c. gain =  $\frac{Z_0}{P_0}$  ; infinite frequency gain = 0.

SUBROUTINE TF ENTRY POINT 000027

STORAGE USED CODE(1) 000025; DATA(0) 000004; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 C10 000002

EXTERNAL REFERENCES (BLOCK, NAME)

0004 MLEP31

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

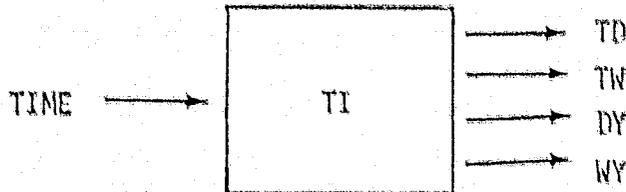
0003 000002 IDIAG 0003 000003 INJPS 0003 000000 IREAD 0003 000001 IWRITE

00100	1*	C	TF						000000
00101	2*	C		SUBROUTINE TF(XI,XIDOT,IXI,FO,FDDOT,IFG,FIW,Z0,Z1,PD,PI)					000000
00101	3*	C							000000
00101	4*	C		PURPOSE - TO SIMULATE A SECOND ORDER TRANSFER FUNCTION WITH					000000
00101	5*	C		FIRST ORDER NUMERATOR					000000
00101	6*	C							000000
00101	7*	C							000000
00101	8*	C							000000
00101	9*	C							000000
00101	10*	C							000000
00101	11*	C							000000
00101	12*	C							000000
00101	13*	C		METHOD - SELF EXPLANATORY					000000
00101	14*	C							000000
00101	15*	C							000000
00101	16*	C		LIMITATIONS - NONE					000000
00101	17*	C							000000
00101	18*	C							000000
00101	19*	C		WRITTEN BY ADAM LLOYD					000000
00101	20*	C							000000
00101	21*	C							000000
00101	22*	C		LATEST REVISION NOV 75					000000
00101	23*	C							000000
00101	24*	C		INPUT/OUTPUT LIST					000000
00101	25*	C							000000
00101	26*	C							000000
00101	27*	C							000000
00101	28*	C							000000
00101	29*	C							000000
00101	30*	C							000000
00101	31*	C							000000

TF

00101	32*	C	P0	DENOMINATOR COEFFICIENT	1/SEC2	INPUT	VAR	00000
00101	33*	C	P1	DENOMINATOR COEFFICIENT	1/SEC	INPUT	VAR	00000
00103	34*			COMMON/CIO/IREAD,IWRITE,IDIAS				00000
00104	35*			IF(I*X1.NE.0)X1DOT=Z0*FIN-P0*F0				00000
00106	36*			IF(I*F0.NE.0)F0DOT=X1+Z1*FIN-P1*F0				00007
00110	37*			RETURN				000020
00111	38*			END				000034

## 7.40 TIME CONVERSION



Converts simulation running time in hours to time referenced to start of day and start of week, and computes number of days and weeks elapsed since start of year.

### Inputs

<u>Parameter/Port</u>	<u>Description</u>	<u>Units</u>
TO	Initial time of simulation from start of year	hrs
TIME	Running time (input via common/CTIME)	hrs

### Outputs

<u>Variable/Port</u>	<u>Description</u>	<u>Units</u>
TW	Time since start of week	hrs
TD	Time since start of day	hrs
WY	Number of weeks	-
DY	Number of days	-
MY	Number of months (approx.)	-
T	Running time from start of year	hrs
DW	Day of week	-

### Calculation Sequence

$$\begin{aligned}
 T &= \text{AMOD}(TO + \text{TIME}, 8760) & TW &= \text{AMOD}(T, 168) \\
 WY &= T/168 + 1 & TD &= \text{AMOD}(T, 24) \\
 DY &= T/24 + 1 & DW &= TW/24 + 1 \\
 MY &= T/730 + 1 & &
 \end{aligned}$$

SUBROUTINE TI ENTRY POINT 000122

STORAGE USED CODE(1) 000155; DATA(0) 000031; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CTIME 000001

EXTERNAL REFERENCES (BLOCK, NAME)

0004 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0000 000013 INJPS 0000 I 000002 MY 0000 I 000000 MD 0000 I 000001 MW 0003 R 000000 TIME

```

00100 1* CTI 000000
00101 2* SUBROUTINE TI(T,TD,TW,DW,DY,WY,MY,TD) 000000
00101 3* C CCC000
00101 4* C PURPOSE CONVERT SIMULATION TIME TO DAILY, WEEKLY, MONTHLY UNITS 000000
00101 5* C 000050
00101 6* C WRITTEN BY A.W. WARREN VERSION 1, MARCH 3 1977 000000
00101 7* C 000000
00101 8* C CALL SEQUENCE 000000
00101 9* C T - SIMULATION TIME FROM START OF YEAR, HR OUTPUT VAR. 000000
00101 10* C TD - TIME OF DAY, HR OUTPUT VAR. 000000
00101 11* C TW - TIME SINCE START OF WEEK, HR OUTPUT VAR. 000000
00101 12* C DW - DAY OF WEEK OUTPUT VAR. 000000
00101 13* C DY - DAY OF YEAR OUTPUT VAR. 000000
00101 14* C WY - WEEK OF YEAR OUTPUT VAR. 000000
00101 15* C MY - MONTH OF YEAR (APPROX.) OUTPUT VAR. 000000
00101 16* C TD - SIMULATION INITIAL TIME FROM START OF YEAR, HR INPUT PARM 000000
00101 17* C 000000
00103 18* COMMON / CTIME / TIME 000000
00104 19* T = AMOD(TD + TIME, 8760.) 000000
00105 20* TD = AMOD(T, 24.) 000000
00106 21* TW = AMOD(T, 168.) 000000
00107 22* MD = TW/24.+1.001 000023
00110 23* DW = MD 000034
00111 24* ND = T/24.+1.001 000037
00112 25* DY = ND 000050
00113 26* MW = T/168.+1.001 000053
00114 27* WY = MW 000065
00115 28* MY = T/730.+1.001 000070
00116 29* AMY = MY 000102
00116 30* C 000102
00117 31* RETURN 000105

```



00120

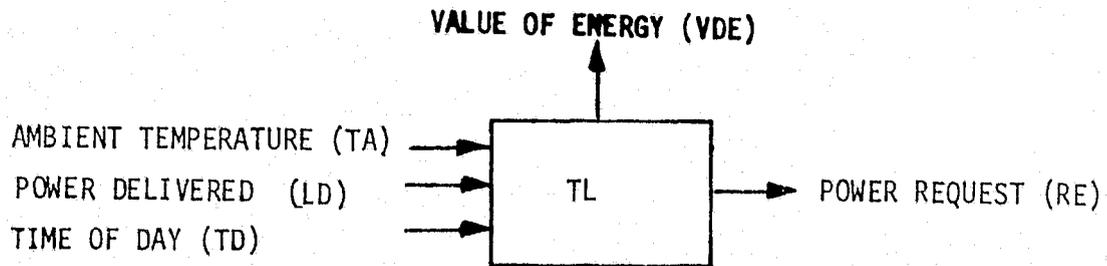
32\*

END

000154

11

## 7.41 THERMAL LOAD



Thermal load is computed as a user specified function of ambient temperature and time of day. The actual load delivered is either the load requested or the maximum discharge rate of the thermal storage chamber. The value of the thermal energy delivered and % of total load actually delivered are also computed.

### Basic Equation

$$RE = TL\theta(TA) * TWT(TD) * NC$$

where

$TL\theta$  = Thermal load versus temperature table

TWT = Daily profile weighting function

NC = Normalizing constant

<u>Tables</u>	<u>Description</u>	<u>Units</u>
TLO	Thermal load versus ambient temperature	kw
TWT	Daily profile weighting function (tabular with time of day)	

### Inputs

<u>Parameter/Port</u>		
TA	Ambient temperature	°F
LD	Power delivered	kw
TD	Time of day (0-24)	h
VE	Value of thermal energy	\$/kwh
NC	Normalizing constant	

### Outputs

<u>Variable/Port</u>		
RE	Load request	kw
VDE	Total value of energy delivered (state)	\$

### Statistics

PC	Cumulative percent of load delivered	-
SLD	Total energy delivered	kwh
SRE	Total energy requested	kwh

## Calculation Sequence

- 1) Compute load request

$$RE = TL \cdot (TA) \cdot TWT(TD) \cdot NC$$

- 2) Value of energy dynamics

$$\dot{VDE} = LD \cdot VE$$

- 3) Statistics

$$SLD = SLD + LD \cdot \Delta / 2$$

$$SRE = SRE + RE \cdot \Delta / 2$$

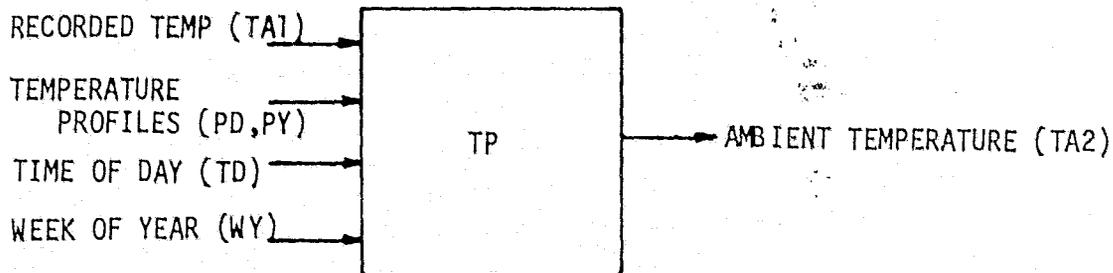
$$PC = 100. \cdot SLD / SRE$$

where  $\Delta$  = integration step size





## 7.42 AMBIENT TEMPERATURE



This component is very similar to the wind component. Ambient temperature is output either from user supplied time histories on storage files or by generating a set of random numbers with user specified random variations. If user supplied profiles are available, then the temperatures are generated from the following equation:

$$TA2 = [PD(TD) + CN(t)] * PY(WY) / MØ$$

where PD and PY are the user supplied daily and weekly profiles, TD and WY are the time of the day and week of the year, CN is a colored noise term and MØ is the average value of PY:

$$MØ = \frac{1}{J} \sum_{j=1}^J PY(j)$$

<u>Tables</u>	<u>Description</u>	<u>Units</u>
PD	Daily profile versus TD	°F
PY	Yearly profile versus WY	arbitrary

## Inputs

### Parameter/Port

TA	1	Ambient temperature data file	°F
TD		Time of day	hr
WY		Week of the year	-
CT		Correlation time of colored noise	hr
MN		Mean temperature of colored noise	°F
STD		Standard deviation of colored noise	°F

## Outputs

### Variable/Port

CN		Colored noise sample	°F
TA	2	Ambient temperature	°F
AV		Mean of daily temperature	°F
MO		Mean of yearly profile	
TIM		Last time a random sample was generated	hr

## Calculation Sequence

- 1) Initialization (first pass only)  
Compute AV, MO, and Initial CN

$$AV = MN + \frac{1}{N} \sum_{J=1}^N PD(J)$$

- 2) Check for data file input  
If TAL = .99999 go to 3)  
TA2 = TAL  
Return

- 3) Generate colored noise sample CN

If TIME = TIM RETURN

$$A = \begin{cases} \text{EXP}(-TINC/CT) & CT > 0 \\ 0. & CT = 0 \end{cases}$$

where TINC = Integration step size

$$CN = CN * A + W$$

Where W is white noise with mean =  $MN*(1-A)$  and

$$\text{standard deviation} = \text{STD} * \sqrt{1-A^2}$$

TIM = TIME

- 4) Compute Temperature

$$TA2 = (PD(TD) + CN) * PY (WY) / MO$$

SUBROUTINE TP ENTRY POINT 000265

STORAGE USED CODE(1) 000350; DATA(0) 000044; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CIMPL 000001
0004 CSIMUL 000007
0005 CTIME 000001

EXTERNAL REFERENCES (BLOCK, NAME)

0006 RN
0007 TBLU1
0010 EXP
0011 SQRT
0012 NERR3

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000121 10L 0001 000127 100L 0001 000057 1176 0001 000102 1276 0001 000247 150L
0000 R 000005 A 0000 R 000000 AX 0000 R 000011 DTP 0004 000000 DUM 0000 I 000003 I
0003 I 000000 IMPL 0000 000016 INJPS 0000 I 000004 L 0000 I 000001 ND 0000 I 000002 NY
0007 R 000000 TRLU1 0005 R 000000 TIME 0004 R 000006 TIME 0000 R 000010 W 0000 R 000006 WMN
0003 R 000007 MSD 0000 R 000012 YTP

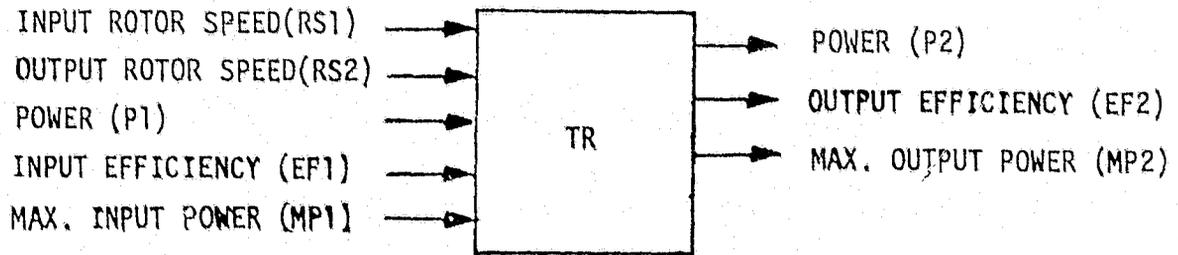
00100 1\* CTP
00101 2\* SUBROUTINE TP (PD,PY,TAO,AV,XM,TIMO,XN, TAI, TD,MY,CT,XMN,STD)
00101 3\* C
00101 4\* C PURPOSE GENERATE AMBIENT TEMPERATURE FROM DAILY, YEARLY AND RANDOM DATA
00101 5\* C
00101 6\* C METHOD COLORED NOISE WITH SPECIFIED PARMS IS ADDED TO A MEAN DAILY
00101 7\* C PROFILE AND MULTIPLIED BY A YEARLY PROFILE.
00101 8\* C
00101 9\* C WRITTEN BY A.W. WARREN VERSION 1, MARCH 7 1977
00101 10\* C
00101 11\* C CALL SEQUENCE
00101 12\* C TABLES
00101 13\* C PD - MEAN DAILY PROFILE, DEG.F
00101 14\* C PY - MEAN YEARLY PROFILE, DEG.F
00101 15\* C OUTPUTS
00101 16\* C TAO - AMBIENT TEMPERATURE OUTPUT, DEG.F
00101 17\* C AV - MEAN DAILY TEMPERATURE, DEG.F
00101 18\* C XM - MEAN YEARLY TEMPERATURE, DEG.F
00101 19\* C TIMO - LAST TIME COLORED NOISE WAS USED, HR
00101 20\* C XN - COLORED NOISE SAMPLE, DEG.F

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## 7.43 VARIABLE RATIO TRANSMISSION



This component models a transmission which couples a fixed speed rotor input (or output) to a variable speed rotor output (or input) component. Power losses are modeled as a table lookup depending on gear ratio and input power.

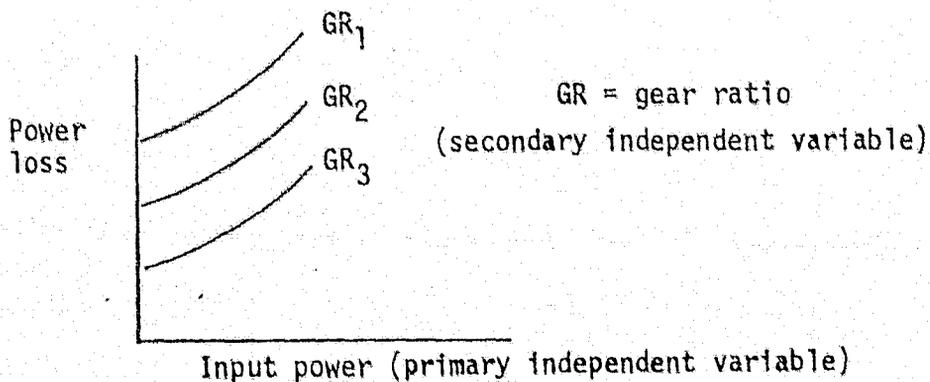


FIGURE 7.43 TRANSMISSION MODEL - LOOKUP TABLE

<u>Tables</u>	<u>Description</u>	<u>Units</u>
PLØ	Power loss versus input power and gear ratio (TABLE DIMENSION = 66)	kw

InputsParameter/Port

RS	1	Input rotor speed	rpm
RS	2	Output rotor speed	rpm
P	1	Input power	kw
EF	1	Input product efficiency	-
MP	1	Maximum input power	kw
CC		Capital cost/year	\$
CM		Maintenance cost/year	\$

OutputsVariable/Port

P	2	Output power	kw
TØ		Output torque	ft-lb
PL		Power loss	kw
EF	2	Output product efficiency	-
MP	2	Maximum power output	kw

Calculation Sequence

If  $P_1 \leq 0$  or  $RS_1 \leq 0$  set  $P_2 = T_0 = PL = 0$  and go to 4)

- 1) Determine gear ratio and power terms

$$GR = RS_2/RS_1$$

$$PL = PL_0(P_1, GR)$$

$$P_2 = P_1 - PL$$

- 2) Determine output torque

$$T_0 = P_2 * 737.6 / (RS_2 * (2 \pi / 60))$$

- 3) Efficiency and maximum power

$$EF_2 = EF_1 * (P_2 / P_1)$$

If  $P_2 \leq 0$ , set  $EF_2 = EF_1$  and write Diagnostic

$$MP_2 = MP_1 - PL_0(MP_1, GR)$$

$$MP_2 \leq 0 \quad \Rightarrow \quad \text{DIAGNOSTIC}$$

- 4) Compute Costs

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SUBROUTINE TR ENTRY POINT 000307

STORAGE USED CODE(1) 000374; DATA(0) 000075; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CIMPL 000002  
0004 CTIME 000001  
0005 CSIMUL 000010  
0006 COST 000002

EXTERNAL REFERENCES (BLOCK, NAME)

0007 TBLU2  
0010 NWDUS  
0011 NI02\$  
0012 NERR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000014	10L	0001	000245	400L	0000	000007	408F	0001	000165	409L	0000	000023	508F
0000	R	000006	AMP2	0006	R	000000	CCI	0006	R	000001	CMI	0005	000000	DUM
0003	I	000001	ICNT	0003	I	000000	IMPL	0000	I	000047	INJP\$	0000	I	000004
0000	I	000001	NNGR	0000	I	000002	NNP1	0007	R	000000	TBLU2	0004	R	000000
0000	R	000000	THAX1									0005	R	000007
														THAX

00100	1*	CTR													000003
00101	2*		SUBROUTINE TR	(P10,P2,TO,PL,EF2,MP2,RS1,RS2,P1,EF1,MP1,CC,CM)											000003
00101	3*	C													000003
00101	4*	C	PURPOSE	TRANSMISSION MODEL											000003
00101	5*	C													000003
00101	6*	C	METHOD	OUTPUT POWER AND TORQUE COMPUTED FROM											000003
00101	7*	C		INPUT AND OUTPUT ROTOR SPEEDS. POWER											000003
00101	8*	C		LOSS MODELED BY TABLE LOOKUP DEPENDING											000003
00101	9*	C		ON GEAR RATIO AND INPUT POWER											000003
00101	10*	C													000003
00101	11*	C	WRITTEN BY	Y.K.CHAN											000003
00101	12*	C		VERSION 1, JUNE 17, 1977											000003
00101	13*	C	CALL SEQUENCE												000003
00101	14*	C	TABLES												000003
00101	15*	C		P10 -POWER LOSS VERSUS INPUT POWER AND GEAR RATIO ,KW											000003
00101	16*	C	OUTPUTS												000003
00101	17*	C		P2 -OUTPUT POWER, KW											000003
00101	18*	C		TO -OUTPUT TORQUE, FT-LB											000003
00101	19*	C		PL -POWER LOSS, KW											000003
00101	20*	C		EF2 -OUTPUT PRODUCT EFFICIENCY											000003
00101	21*	C		MP2 -MAXIMUM POWER OUTPUT, KW											000003

TR

00101	22*	C	INPUTS	C00003
00101	23*	C	RS1 -INPUT ROTOR SPEED,RPM	C00003
00101	24*	C	RS2 -OUTPUT ROTOR SPEED,RPM	C00003
00101	25*	C	P1 -INPUT POWER,KW	G00003
00101	26*	C	EF1 -INPUT PRODUCT EFFICIENCY	000003
00101	27*	C	MP1 -MAXIMUM INPUT POWER,KW	C00003
00101	28*	C	CC -CAPITOL COST/YEAR,\$	G00003
00101	29*	C	CM -MAINTENANCE COST/YEAR,\$	C00003
00101	30*	C		C00003
00103	31*		COMMON/CI MPL/IMPL,ICNT/CTIME/TIME/CSIMUL/DUM(7),TMAX	G00003
00103	32*	X	/COST/CCI, CMI	000003
00104	33*		REAL MP2,MP1	C00003
00105	34*		DIMENSION PLO(1)	G00003
00105	35*	C		C00003
00106	36*		IF(IMPL.GT.0)GO TO 10	C00003
00110	37*		TMAX1=TMAX*.9999	C00006
00111	38*		RS2=RS1	C00011
00112	39*	10	CONTINUE	C00014
00113	40*		NNGR=PLO(3)	C00014
00114	41*		NNP1=PLO(2)	C00022
00115	42*		M4=NNGR*4	C00031
00116	43*		MN4=NNP1*M4	000033
00116	44*	C		C00033
00116	45*	C	COMPUTE GEAR RATIO AND POWER TERMS	C00033
00116	46*	C		000033
00117	47*		P2=0.	000035
00120	48*		T0=0.	C00036
00121	49*		PL=0.	C00037
00122	50*		EF2=EF1	000040
00123	51*		MP2=MP1	000042
00124	52*	100	IF((RS1.LE.0.).OR.(P1.LE.0.))GO TO 400	C00044
00126	53*		P2=P1	000060
00127	54*	200	IF(RS2.LE.0)GO TO 400	000062
00131	55*	300	GR=RS2/RS1	000071
00132	56*		PL=TBLU2(P1,GR,PLO(M4),PLO(4),PLO(MN4),1,1,-NNP1,-NNGR,NNP1,NNGR)	000074
00133	57*		P2=P1-PL	000124
00133	58*	C		000124
00133	59*	C	OUTPUT TORQUE	000124
00133	60*	C		000124
00134	61*		T0=P2*737.6*30./(RS2*3.14159)	C00126
00134	62*	C		G00126
00134	63*	C	EFFICIENCY AND MAXIMUM POWER	G00126
00134	64*	C		000126
00135	65*		EF2=EF1*P2/P1	C00134
00136	66*		IF(EF2.GT.0.1)GO TO 409	000140
00140	67*		EF2=EF1	C00142
00141	68*		IF(IMPL.EQ.2)WRITE(6,408)PL,P1	C00144
00146	69*	408	FORMAT(1H0,25H TRANSMISSION POWER LOSS ,F12.3,	C00156
00146	70*	X	21H EXCEEDS INPUT POWER ,F12.3)	C00156
00147	71*		IF(IMPL.EQ.2)ICNT=ICNT+1	C00156
00151	72*	409	CONTINUE	G00165
00152	73*		AMP2=TBLU2(MP1,GR,PLO(M4),PLO(4),PLO(MN4),1,1,-NNP1,-NNGR,	G00165
00152	74*		XNNP1,NNGR)	C00165
00153	75*			C0022C
00153	76*		MP2=MP1-AMP2	C0022C
00154	77*		IF(MP2.GT.0.)GO TO 400	000222
00154	78*		IF(IMPL.EQ.2)WRITE(6,508)AMP2,MP1	C00224

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```

00163 79*      508 FORMAT(1H0,25H TRANSMISSION POWER LOSS ,F12.3,
00163 80*      X 29H EXCEEDS MAXIMUM INPUT POWER ,F12.3)
00164 81*      IF(IMPL.EQ.2)ICNT=ICNT+1
00164 82*      C
00166 83*      400 IF(IMPL.LE.1)RETURN
00170 84*      IF(TIME.LT.TMAX1)RETURN
00172 85*      CCI=CCI+CC
00173 86*      CHI=CHI+CM
00173 87*      C
00174 88*      RETURN
00175 89*      END

```

```

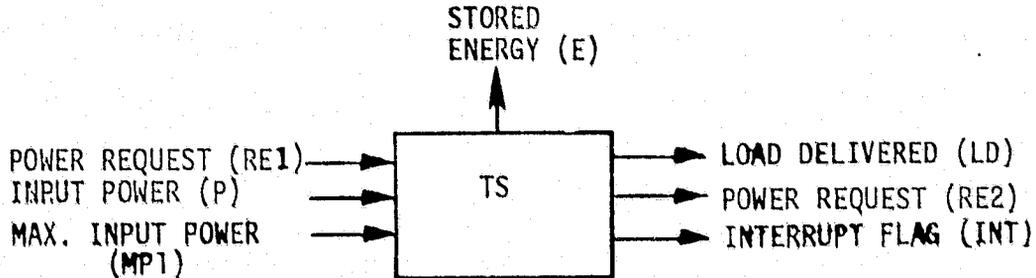
000236
000236
000236
000236
000245
000253
000262
000265
000265
000270
000373

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## 7.44 THERMAL STORAGE CHAMBER



The thermal storage chamber is modeled by a "lumped" parameter approach. The entire storage media mass is characterized by a single temperature (no temperature gradient). The storage media is either a sensible heat or a phase change media. Energy is input via electrical resistance heaters and withdrawn by a heat exchanger. Energy is deposited in the media at a rate equal to the available electrical power up to a maximum charging power. The discharge heat exchanger fluid mass flow rate is adjusted to provide the desired heat load demand. The maximum mass flow rate condition determines the maximum thermal load. The maximum energy limit represents the point where the maximum media temperature is reached.

The model initially calculates the required storage media mass to provide the rated thermal energy storage (design point). Cost calculations are also made on the design point conditions. Initial checks on charge and discharge power and initial stored energy level are made. The storage temperature is determined based on the energy level.

### Basic Equation

$$E = P - LD - NU * E$$

<u>Tables</u>		<u>Description</u>	<u>Units</u>
HT		Media temperature versus enthalpy in KWH/LB <sup>1</sup>	°F
<u>Inputs</u>			
<u>Parameter/Port</u>			
P		Input power	kw
RE	1	Demand thermal load	kw
NU		Stored energy loss coefficient (D = 0.02)	(h) <sup>-1</sup>
TS		Rated storage time <sup>2</sup>	h
V0		Rated input voltage <sup>2</sup>	V
TM1		Maximum allowable storage temperature (D = 212)	°F
T01		Minimum allowable storage temperature (D = 60)	°F
DH		Design point enthalpy	kwh/lb
PD		Rated storage thermal power <sup>2</sup>	kw
PM		Maximum charge rate (D = 2*PD)	kw
MFM		Maximum working fluid mass flow rate (D = 9000)	lb/h
TDE		Temperature deadband for priority resequence (D = 4)	°F
EF	1	Input product efficiency	-
MP	1	Maximum input charging rate (D = 1.X10 <sup>8</sup> )	kw
CP2		Working fluid heat capacity (D = 2.93X10 <sup>-4</sup> )	kwh/lb-°F
T02		Working fluid return temperature (D = 40)	°F
TM2		Maximum allowable working fluid temperature (D = 212)	°F
R		Effective heat exchanger thermal resistance (D = 3.08X10 <sup>-4</sup> )	°F/kw
CM		Storage device yearly maintenance cost (D = 0.6)	\$/kw
CSA		Storage device capacity cost (D = 50)	\$/kw
CSB		Storage device energy cost (D = 15.2)	\$/kwh
LE		Unit life expectancy	years

D - Default values specified

1 - See Figure 7.44

2 - Design point conditions

### Outputs

<u>Variable/Port</u>	<u>Description</u>	<u>Units</u>
E	Stored energy (state)	kwh
I	Input current	amps
MP 2	Maximum discharge rate allowable	kw
INT	Priority interrupt flag	-
T	Storage temperature	°F
M	Required storage media mass	lb
CCØ	Storage device capital cost/year	\$
RE 2	Maximum charging rate request	kw
MF	Working fluid mass flow rate	lb/h
LD	Power Delivered	kw

### Statistics

TSU	Maximum storage temperature	°F
TSL	Minimum storage temperature	°F
ME	Maximum stored energy	kwh
MFU	Maximum working fluid mass flow rate	lb/h

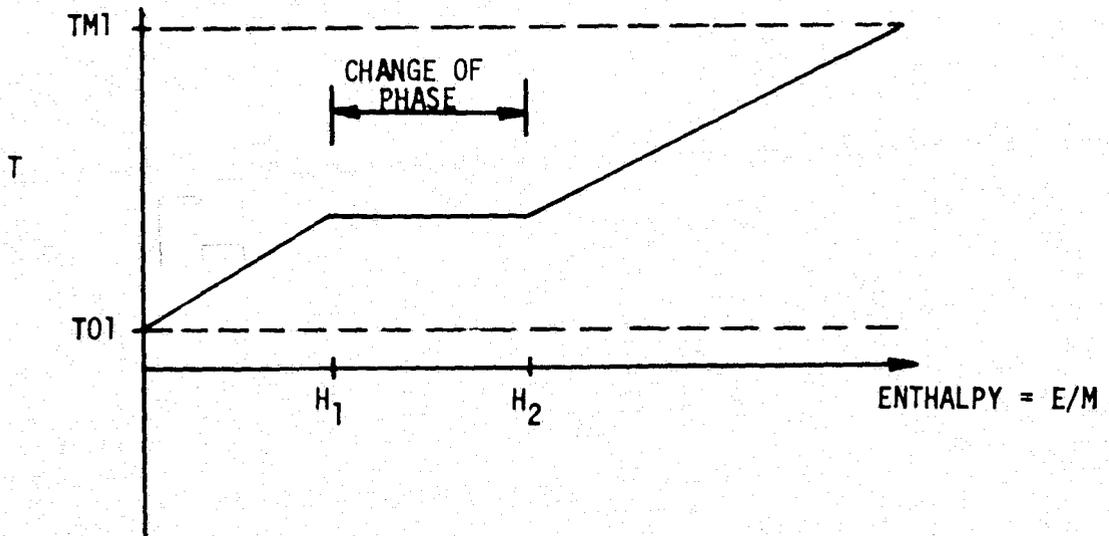


FIGURE 7.44: TEMPERATURE - ENTHALPY DIAGRAM

The calculation sequence and default values assume a thermal storage device sized to provide 10kw for 24 hours. A paraffin wax phase change storage medium is assumed. Water is assumed as the thermal transport fluid. Costs are assumed to be given by data for the phase change storage device given in Reference 1. The thermal resistance value, R, is assumed equal to that determined for the device of Reference 1. The value for the maximum charging rate, PM, reflects the acceptance of twice the design charge rate. The actual numbers which should be used will depend on specific design and performance requirements obtained from a desired application.

## Calculation Sequence

- 1) Media mass, capital cost, maintenance cost (first pass)

$$M = \frac{PD * TS}{DH}$$

$$CC = (CSA + CSB * TS) * PD / LE$$

$$CM = CM * PD$$

- 2) Storage Temperature and Working Fluid Temperature

$$T = HT(E/M)$$

$$TF = \min(TM2, \max[T02, T - RE1 * R])$$

$$E2 = M * HT^{-1}(TM1)$$

---

1. "Advanced Thermal Energy Storage," BEC/EPRI RP 789-1, July 1976.

Calculation Sequence Cont.

3) Discharge Rate and Thermal Load

$$E1 = M*HT^{-1}(T01)$$

$$MP2 = MFM*CP2*(TF-T02)$$

$$LD = \text{MIN}(RE1, MP2, (E-E1)/TINC)$$

$$MF = LD / (CP2*(TF-T02))$$

4) Diagnostic Checks

$$MF \leq MFM$$

$$P \leq PM$$

$$T01 \leq T \leq TM1$$

5) Current calculations

$$I = \frac{P*1000}{V0}$$

6) Energy dynamics

$$\dot{E} = P - LD - NU*E$$

7) Maximum Charging Rates

$$RE2 = \text{min}(PM, MP1, (E2-E)/TINC)/EF1$$

where TINC = integration step size

## Calculation Sequence Cont.

### 8) Priority resequencing

if  $T \leq T_{01}$ ,  $INT = 1$

if  $T \geq T_{01} + TDE$  and  $INT=1$ ,  $INT=0$

if  $T \geq TM_1$ ,  $INT=-1$

if  $T < TM_1 - TDE$  and  $INT=-1$ ,  $INT=0$

### 9) Compute Statistics and Costs

SUBROUTINE TS

ENTRY POINT 000612

STORAGE USED CODE(1) 001071; DATA(0) 000131; BLANK COMMON(2) 000000

## COMMON BLOCKS

```
0003 CIMPL 000002
0004 CTIME 000001
0005 CSIMUL 000010
0006 COST 000002
```

## EXTERNAL REFERENCES (BLOCK, NAME)

```
0007 TBLU1
0010 NWDUS
0011 NI02%
0012 WERR3%
```

## STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

```
0001 000144 100L      0000 000007 1010F      0000 000025 1020F      0000 000043 1030F      0001 000407 200L
0000 R 000006 A      0006 R 000000 CCI      0006 R 000001 CMI      0005 R 000000 DUM      0000 R 000003 E1
0003 I 000001 ICN      0003 I 000000 IMPL      0000 000107 INJPS      0000 I 000002 NH      0000 R 000005 PM1
0007 R 000000 TBLU1    0000 R 000004 TF      0004 R 000000 TIME      0000 R 000001 TINC      0005 R 000007 TMAX
0000 R 000000 TMAX1
```

```
00100 1* CTS 00000
00101 2* SUBROUTINE TS(HT,E,DE,IE,I,MP2,INT,T,M,CCO,RE,MF,LD 00000
00101 3* 1 ,TSU,TSL,ME,MFU,P,RE1,NU,TSO,VO,TM1,TO1,DH,PD,PH, 00000
00101 4* 2 MFH,TDE,EF1,MP1,CP2,T02,TM2,R,CM,CSA,CSB,LE) 00000
00101 5* C 00000
00101 6* C PURPOSE COMPUTE ENERGY CONTAINED IN A THERMAL STORAGE MEDIA 00000
00101 7* C 00000
00101 8* C METHOD A PHASE CHANGE OR SENSIBLE HEAT MEDIA IS MODELED AS 00000
00101 9* C 00000
00101 10* C A SINGLE TEMPERATURE MASS WITH NO GRADIENTS. 00000
00101 11* C 00000
00101 12* C WRITTEN BY F. O. MAHONY VERSION 2, JULY 1977 00000
00101 13* C 00000
00101 14* C CALL SEQUENCE 00000
00101 15* C 00000
00101 16* C TABLES 00000
00101 17* C HT - MEDIA TEMPERATURE VERSUS ENTHALPY IN KWH/LB, DEG F 00000
00101 18* C OUTPUTS 00000
00101 19* C E - STORED ENERGY (STATE VARIABLE), KWH 00000
00101 20* C DE - POWER INTO STORAGE, KW 00000
00101 21* C IE - STATUS INDICATOR 00000
```

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```

00140 79*      IF(CSA.EQ. .99999)CSA=50.0
00142 80*      IF(CSB.EQ. .99999)CSB=15.2
00144 81*      IF(MP1.EQ. .99999) MP1= 1.0E8
00144 82*      C
00146 83*      INT=0.0
00147 84*      RE1=0.0
00147 85*      C
00150 86*      TSU=0.0
00151 87*      ME =0.0
00152 88*      MFU=0.0
00153 89*      TSL=1.0E8
00154 90*      CM= CM*PD
00154 91*      C
00155 92*      M =PD*TSU/DH
00156 93*      CCO=(CSA+CSR+TSU)*PD/LE
00156 94*      C
00156 95*      COMPUTE STORAGE TEMPERATURE
00156 96*      C
00157 97*      100 NH= HT(2)
00160 98*      T= TBLU1(E/H,HT(4),HT(4+NH),1,NH)
00161 99*      E1= H*TBLU1(TM1,HT(4+NH),HT(4),1,NH)
00161 100*     C
00161 101*     C
00161 102*     WORKING FLUID TEMPERATURE
00161 103*     C
00162 104*     TF =AMIN1(TM2,AMAX1(T02,T-RE1*R))
00162 105*     C
00162 106*     MAXIMUM DISCHARGE RATE AND THERMAL LOAD
00162 107*     C
00163 108*     MP2=MFH*CP2*(TF-T02)
00164 109*     IF(INT.EQ.1)MP2=0.
00166 110*     LD =AMIN1(RE1,MP2)
00166 111*     C
00166 112*     WORKING FLUID MASS FLOW RATE
00166 113*     C
00167 114*     IF(LD.GT.0.0) MF =LD/CP2/(TF-T02)
00167 115*     C
00171 116*     IF(IMPL.LE.1)GO TO 200
00173 117*     IF(IMPL.GT.2) GO TO 200
00175 118*     PM1= PH/.9999
00175 119*     C
00176 120*     IF(MF .GT.MFH)WRITE(6,1010)MF,MFH
00203 121*     IF(P .GT.PM1 )WRITE(6,1020)P ,PM
00210 122*     IF(MF.GT.MFH .OR. P.GT.PM1)ICN=ICN+1
00212 123*     IF(T .LT.T01.OR.
00212 124*     1 T .GT.TM1)WRITE(6,1030)T,T01,TM1
00220 125*     IF(T.LT.T01 .OR. T.GT.TM1) ICN=ICN+1
00220 126*     C
00220 127*     CURRENT CALCULATION
00220 128*     C
00222 129*     200 I =P*1000.0/V0
00222 130*     C
00222 131*     ENERGY STATE
00222 132*     C
00222 133*     C
00223 134*     IF(IE.NE.0)DE=P-LD-NU*E

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**TS**

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00223 136* C
00223 137* C
00223 138* C
00225 139* A= AMAX1(E1-E,0.)/TINC
00226 140* RE =AMIN1(PM,MP1,A)/EF1
00226 141* C
00226 142* C
00226 143* C
00226 144* C
00227 145* IF(T.LE.T01)INT=1.0
00227 146* C
00231 147* IF(T.GE.(T01+TDE).AND.
00231 148* 1 INT.EQ.1.)INT=0.0
00231 149* C
00233 150* IF(T.GE.TM1)INT=-1.0
00233 151* C
00235 152* IF(T.LT.(TM1-TDE).AND.
00235 153* 1 INT.EQ.-1.)INT=0.0
00235 154* C
00237 155* IF(IMPL.LE.1)RETURN
00237 156* C
00241 157* TSU=AMAX1(TSU,T)
00242 158* TSL=AMIN1(TSL,T)
00243 159* ME =AMAX1(ME ,E )
00244 160* MFU=AMAX1(MFU,MF)
00245 161* IF(TIME.LT.TMAX1)RETURN
00245 162* C
00245 163* C
00245 164* C
00247 165* CHI=CMI+CM
00250 166* CCI=CCI+CCO
00251 167* CM = CM/PD
00251 168* C
00252 169* RETURN
00253 170* 1010 FORMAT(1H0,26HTS WORKING FLUID FLOW RATE,F12.3
00253 171* 1 ,32H GREATER THAN MAXIMUM ALLOWED,F12.3)
00254 172* 1020 FORMAT(1HC,14HTS INPUT POWER,F12.3
00254 173* 1 ,44H GREATER THAN MAXIMUM ALLOWED CHARGE RATE,F12.3)
00255 174* 1030 FORMAT(1H0, 23HTS STORAGE TEMPERATURE ,F12.3
00255 175* 1 ,20H OUTSIDE MINIMUM ,F12.3
00255 176* 2 ,15H AND MAXIMUM,F12.3)
00255 177* C
00256 178* END

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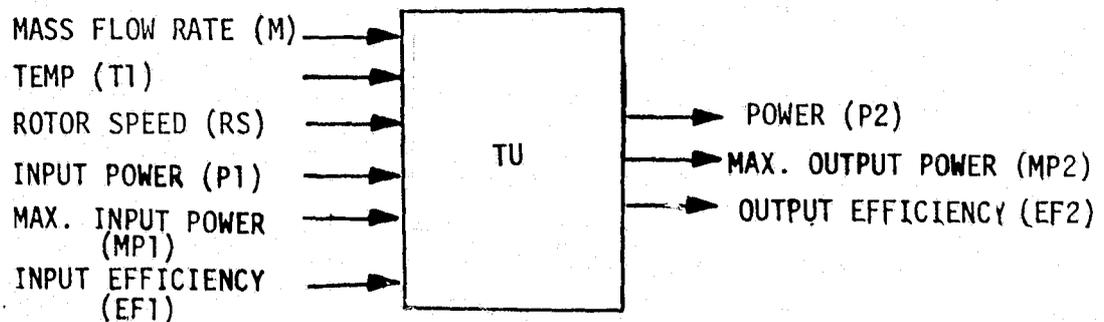
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## 7.45 TURBINE (PNEUMATIC)



The turbine model is based on a high pressure ratio, constant angular velocity design. The turbine is assumed to be designed to a set of operating conditions defined in terms of user specified parameters. The polytropic efficiency is only weakly related to angular velocity. Initial calculations are made with the design polytropic efficiency, and refinements are then computed after off-design parameters are calculated.

### Basic Equation

The equation for output power  $P_2$  is

$$P_2 = M * C_P * (T_1 - T_A)$$

Inputs

<u>Parameter/Port</u>	<u>Description</u>	<u>Units</u>
M	Inlet mass flow rate	lb/h
CP	Air heat capacity (D = $7.2 \times 10^{-5}$ )	kwh/lb/°F
T	1 Input air temperature	°F
TA	Ambient air temperature	°F
MD	Design mass flow rate (D = 4800)	lb/h
TID	Design inlet air temperature (D = 600)	°F
PID	Design inlet pressure (D = 117.6)	psi
P2D	Design exit pressure (ambient) (D = 14.7)	psi
T2D	Design exit temperature (ambient) (D = 70)	°F
PS	Storage vessel pressure	psi
RS	Angular velocity	rpm
EF	1 Input product efficiency	-
MP	1 Maximum input power	kw
P	1 Input power	kw
CK	Capacity cost coefficient <sup>1</sup> (D = 0.015)	
F0	Turbine mass flow exponent for capital cost (D = 0.75)	-
G	Turbine temperature exponent for capital cost (D = 0.5)	-
NPD	Design Polytropic Efficiency (D = 0.88)	

Outputs

<u>Variable/Port</u>	<u>Description</u>	<u>Units</u>
P	2 Output power	kw
XC0	Turbine cost/year	\$
PR	Back pressure	psi
T0	Torque	ft-lb

D - Default values supplied

<sup>1</sup> CK = Capital cost (known unit) / [(design point mass flow rate)<sup>F0\*</sup> \* LN (design point temperature + 460)<sup>G</sup> \* LN (inlet/outlet pressure ratio)\*LE], where LE = life expectancy in years.

Outputs Cont.

<u>Variable/Port</u>		<u>Description</u>	<u>Units</u>
EF	2	Output product efficiency	-
MP	2	Maximum discharge power	kw

Statistics

MOP		Maximum power observed	kw
-----	--	------------------------	----

The calculation sequence and the default values are based on the assumption of a high pressure ratio, constant angular velocity turbine, rated at 150 kw and a pressure ratio of 8. The equations used relate first order effects among the various physical quantities and were derived from first principles originally in support of the research work of Reference 1. Cost scaling was also developed in that reference based on cost estimates from turbomachinery manufacturers.

- 
1. "Closed Cycle High Temperature Control Receiver Concept for Solar Electric Power," BEC/EPRI RP377-1, June 1976.

Calculation Sequence

## 1) Costs

$$CC = CK*(MD)**F0*(TID+460)**G*LN(PID/P2D)$$

## 2) Back Pressure PR determined by

$$PR = (M/MD)*PID* \sqrt{(T1+460)/(TID+460)}$$

If PR > PS write DIAGNOSTIC

## 3) Efficiency

$$RAT = (PID/P2D)**(2/7)$$

$$EFF = (RAT-1.)/(RAT**(1/NPD)-1)$$

## 4) Power Out

$$P2 = M*CP*(T1-TA)*EFF$$

## 5) Torque

If RS = 0, set T0 = 0 and go to 6)

$$T0 = P2*(737.6)/(RS*2 \pi /60)$$

## 6) Efficiency and maximum power

$$EF2 = EF1*EFF$$

$$MP2 = \min(MP1*EFF, MD*CP*(T1-TA))$$

## 7) Compute Statistics and Costs

SUBROUTINE TU ENTRY POINT 000335

STORAGE USED CODE(1) 000471; DATA(0) 000065; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CIMPL 000002  
 0004 CTIME 000001  
 0005 CSTMUL 000010  
 0006 COST 000001

EXTERNAL REFERENCES (BLOCK, NAME)

0007 XPRR  
 0010 ALOG  
 0011 SQRT  
 0012 AWDUS  
 0013 NI02%  
 0014 WERR3%

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000137	100L	0001	000304	1000L	0000	000004	1010F	0001	000204	200L	0001	000233	300L		
0006	R	000000	CCI	0005	000000	DUM	0000	R	000003	EFF	0003	I	000001	ICNT		
0000	000047	INJPS	0000	R	000000	PI	0000	R	000002	RA7	0004	R	000000	TIME		
0000	R	000001	TMAXI										0005	R	000007	TMAX

00100	1*	CTU														000000
00101	2*		SUBROUTINE TU(P2,CC,PR,TO,EF2,MP2,MOP,M,CP,T1,TA,MD,TID,PID,P2D,													000000
00101	3*		1	T2D,PS,RS,EF1,MP1,P1,CK,F,G,NPD)												000000
00101	4*	C														000000
00101	5*	C	PURPOSE	TURBINE PERFORMANCE MODEL												000000
00101	6*	C														000000
00101	7*	C	METHOD	COMPUTE TURBINE POWER OUTPUT FROM INPUT DESIGN												000000
00101	8*	C														000000
00101	9*	C		CONDITIONS AS A FUNCTION OF INLET TEMPERATURE												000000
00101	10*	C														000000
00101	11*	C		AND MASS FLOW RATE												000000
00101	12*	C														000000
00101	13*	C	WRITTEN BY	F.O. MAHONY												000000
00101	14*	C														000000
00101	15*	C	CALL SEQUENCE													000000
00101	16*	C		OUTPUTS												000000
00101	17*	C		P2 - OUTPUT POWER, KW												000000
00101	18*	C		CC - TURBINE COST PER YEAR, \$												000000
00101	19*	C		PR - BACK PRESSURE, PSI												000000
00101	20*	C		TO - TORQUE, FT-LB												000000

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00101	21*	C	EF2 - OUTPUT PRODUCT EFFICIENCY	000000
00101	22*	C	MP2 - MAXIMUM DISCHARGE POWER, KW	000000
00101	23*	C	MOP - MAXIMUM POWER OBSERVED, KW	000000
00101	24*	C	INPUTS	000000
00101	25*	C	M - INLET MASS FLOW RATE, LB/HR	000000
00101	26*	C	CP - AIR HEAT CAPACITY, KWH/LB/DEG F	000000
00101	27*	C	T1 - INPUT AIR TEMPERATURE, DEG F	000000
00101	28*	C	TA - AMBIENT AIR TEMPERATURE, DEG F	000000
00101	29*	C	MD - DESIGN MASS FLOW RATE, LB/HR	000000
00101	30*	C	TID - DESIGN INLET AIR TEMPERATURE, DEG F	000000
00101	31*	C	PID - DESIGN INLET PRESSURE, PSI	000000
00101	32*	C	P2D - DESIGN EXIT PRESSURE (AMBIENT), PSI	000000
00101	33*	C	T2D - DESIGN EXIT TEMPERATURE (AMBIENT), PSI	000000
00101	34*	C	PS - STORAGE VESSEL PRESSURE, PSI	000000
00101	35*	C	RS - ANGULAR VELOCITY, RPM	000000
00101	36*	C	EF1 - INPUT PRODUCT EFFICIENCY	000000
00101	37*	C	MP1 - MAXIMUM INPUT POWER, KW	000000
00101	38*	C	P1 - INPUT POWER, KW	000000
00101	39*	C	CK - CAPACITY COST COEFFICIENT	000000
00101	40*	C	F - TURBINE MASS FLOW EXPONENT FOR CAPITAL COST	000000
00101	41*	C	G - TURBINE TEMPERATURE EXPONENT FOR CAPITAL COST	000000
00101	42*	C	NPD - DESIGN POLYTROPIC EFFICIENCY	000000
00101	43*	C		000000
00103	44*		COMMON /CIMPL/IMPL, ICNT/CTIME/ TIME /CSIMUL/DUM(7), THAX /COST/CCI	000000
00104	45*		REAL MP2, MOP, M, MD, MP1, NPD	000000
00105	46*		DATA PI /3.14159/	000000
00105	47*	C		000000
00107	48*		IF (IMPL.GT.0) GO TO 100	000000
00111	49*		IF (CP .EQ. .99999) CP = 72.0E-6	000002
00113	50*		IF (TA .EQ. .99999) TA = 70.0	000007
00115	51*		IF (MD .EQ. .99999) MD = 4800.	000014
00117	52*		IF (TID .EQ. .99999) TID = 600.0	000021
00121	53*		IF (PID .EQ. .99999) PID = 117.6	000026
00123	54*		IF (P2D .EQ. .99999) P2D = 14.7	000033
00125	55*		IF (T2D .EQ. .99999) T2D = 70.0	000040
00127	56*		IF (CK .EQ. .99999) CK = 0.015	000045
00131	57*		IF (F .EQ. .99999) F = 0.75	000052
00133	58*		IF (G .EQ. .99999) G = 0.5	000057
00135	59*		IF (NPD .EQ. .99999) NPD = .88	000064
00137	60*		MOP = L.	000071
00140	61*		RS = AMAX1(0.0, AMIN1(RS, 4000.))	000072
00141	62*		THAX = .99999 * THAX	000104
00142	63*		CC = CK * MD ** F * (TID + 460.0) ** 6 * ALOG(PID/P2D)	000107
00142	64*	C	DETERMINE BACK PRESSURE	000107
00142	65*	C		000107
00143	66*		100 RAT = (PID/P2D) ** .2857	000137
00144	67*		EFF = (RAT - 1.0) / (RAT ** (1./NPD) - 1.0)	000146
00145	68*		PR = M / MD * PID * SQRT((T1 + 460.0) / (TID + 460.0))	000162
00145	69*	C		000162
00146	70*		IF (PR.GT.PS) GO TO 1000	000200
00146	71*	C		000200
00146	72*	C	POWER OUTPUT	000200
00146	73*	C		000200
00146	74*	C		000200
00150	75*		200 P2 = M * CP * (T1 - TA) * EFF	000204
00151	76*		T0 = 0.	000212
00152	77*		IF (RS.EQ.0. .OR. P1.EQ. 0.) GO TO 300	000213

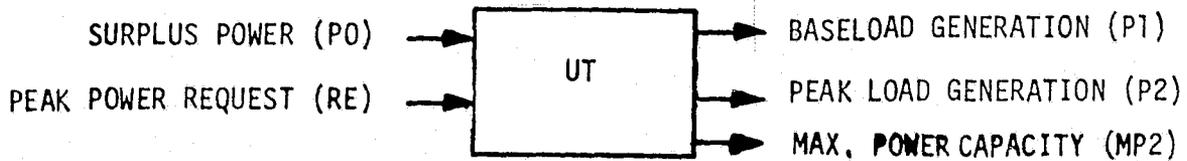
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00152	78*	C			000213
00154	79*		TORQUE		000223
00154	80*		TO = P2*737.6/(RS*2.0*PI/60.0)		000223
00154	81*	C		EFFICIENCY AND MAXIMUM POWER	000223
00154	82*	C			000223
00155	83*		300 EF2 = EF1*EFF		000233
00156	84*		MP2 = AMIN1(MP1*EFF ,MD*CP*(T1-TA))		000235
00157	85*		IF(IMPL.LE. 1) RETURN		000251
00161	86*		MOP = AMAX1(MOP,P2)		000260
00162	87*		IF(TIME.LT.TMAX1) RETURN		000266
00164	88*		CCI = CCI + CC		000275
00164	89*	C		RETURN	000275
00165	90*				000300
00165	91*	C			000300
00166	92*		1000 IF(IMPL.EQ.2)WRITE(6,1010) PR,PS		000304
00173	93*		1010 FORMAT (1H0,21HTURBINE BACK PRESSURE,F12.3,		000315
00173	94*		1 39H GREATER THAN STORAGE VESSEL PRESSURE ,F12.3)		000315
00174	95*		IF(IMPL.EQ.2)ICNT=ICNT+1		000315
00174	96*	C			000315
00176	97*		GO TO 200		000323
00176	98*	C			000323
00177	99*		END		00047C

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## 7.46 UTILITY



The utility model has two power outputs corresponding to baseload and peak generation, with corresponding generation cost inputs. A surplus power input is also provided with cost credit depending on whether baseload or peak power is reduced. Total energy cost, total output power and total peak load requests are monitored.

## Inputs

<u>Parameter/Port</u>	<u>Description</u>	<u>Units</u>
BS	Baseload generation (default = 0.)	kw
CB	Cost of baseload generation/kwh	\$
MP        1	Maximum power capacity (default = $1 \times 10^8$ )	kw
P            0	Surplus power returned to utility	kw
RE	Peak generation request	kw
CP	Cost of peak load generation/kwh	\$
CC	Capital cost/year	\$
CM	Maintenance cost/year	\$

## Outputs

<u>Variable/Port</u>	<u>Description</u>	<u>Units</u>
P            1	Baseload generation (= BS)	kw
MP           2	Maximum power capacity (= MP1)	kw
P            2	Peak load generation	kw
C0	Cost of energy used (state)	\$

## Statistics

SR	Sum of requested peak generation	kwh
SP0	Sum of output energy	kwh
SP	Sum of surplus energy	kwh
VSP	Value of surplus energy	\$

## Calculation Sequence

### 1) Power outputs

If  $BS > MP1$ , write diagnostic

$$P1 = BS, MP2 = MP1$$

$$P2 = \text{MIN} (MP1 - BS, RE)$$

### 2) Energy cost dynamics

$$C0 = BS * CB + (P2 - P0) * CX$$

$$CX = \begin{cases} CP & \text{if } P2 - P0 > 0 \\ 0 & \text{if } P2 - P0 < 0 \end{cases}$$

### 3) Statistics

$$SR = SR + RE * TINC$$

$$DEL = \begin{cases} 0 & \text{if } P2 > P0 \\ (P0 - P2) * TINC & \text{if } P0 > P2 \end{cases}$$

$$SP0 = SP0 + (P1 + P2 - P0) * TINC + DEL$$

$$SP = SP + DEL$$

$$VSP = VSP + DEL * CB$$

Where  $TINC = \text{integration step size}/2$

### 4) Compute Costs

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SUBROUTINE UT ENTRY POINT 000217

STORAGE USED CODE(1) 000341; DATA(0) 000045; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CIMPL 000002  
0004 CTIME 000001  
0005 CSIMUL 000010  
0006 COST 000011

EXTERNAL REFERENCES (BLOCK, NAME)

0007 NWDUS  
0010 NI025  
0011 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000053	100L	0001	000146	200L	0000	000004	208F	0006 R	000000	CCI.	0006 R	000001	CM1
0006	000002	COP	0000 R	000002	CX	0005 R	000000	DUM	0003 I	000001	ICNT	0003 I	000000	IMPL
0000	000023	INJP5	0006 R	000010	SPD	0006 R	000004	TDE	0000 R	000003	TERM	0004 R	000000	TIME
0000 R	000001	TINC1	0006	000005	TLD	0005 R	000007	THAX	0000 R	000000	THAX1	0006 R	000007	UTO
0006 R	000006	UTV	0006 R	000003	VDE									

00100	1*	CUT										000000
00101	2*		SUBROUTINE UT(P1,MP2,P2,CO,COD,ICO,SR,SPO,SP,VSP									000000
00101	3*		1									000000
00101	4*	C										000000
00101	5*	C	PURPOSE	MODEL OF UTILITY CAPABLE OF PRODUCING								000000
00101	6*	C		BASELOAD AND PEAKLOAD POWER, AND OF								000000
00101	7*	C		ABSORBING SURPLUS POWER								000000
00101	8*	C										000000
00101	9*	C	METHOD	COMPUTE PEAKLOAD GENERATION AND ENERGY COST								000000
00101	10*	C										000000
00101	11*	C	WRITTEN BY Y.K.CHAN	VERSION 1, JUNE 8, 1977								000000
00101	12*	C										000000
00101	13*	C	CALL SEQUENCE									000000
00101	14*	C	OUTPUT									000000
00101	15*	C	P1	-BASELOAD GENERATION,KW								000000
00101	16*	C	MP2	-MAXIMUM POWER CAPACITY,KW								000000
00101	17*	C	P2	-PEAKLOAD GENERATION,KW								000000
00101	18*	C	CO	-COST OF ENERGY USED (STATE), \$								000000
00101	19*	C	COD	-ENERGY COST RATE, \$/HR								000000
00101	20*	C	ICO	-INTEGRATOR CONTROL FOR CO								000000
00101	21*	C	STATISTICS									000000
00101	22*	C	SR	-SUM OF REQUESTED PEAK GENERATION,KW								000000

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00101 23* C SPO -SUM OF OUTPUT ENERGY, KWH 000000
00101 24* C SP -SUM OF SURPLUS ENERGY, KWH 000000
00101 25* C VSP -VALUE OF SURPLUS ENERGY, $ 000000
00101 26* C INPUTS 000000
00101 27* C BS -BASELOAD GENERATION (DEFAULT=0.),KW 000000
00101 28* C CB -COST OF BASELOAD GENERATION/KWH, $ 000000
00101 29* C MP1 -MAXIMUM POWER CAPACITY,KW 000000
00101 30* C PD -SURPLUS POWER RETURNED TO UTILITY,KW 000000
00101 31* C RE -PEAK GENERATION REQUEST, KW 000000
00101 32* C CP -COST OF PEAKLOAD GENERATION/KWH, $ 000000
00101 33* C CC -CAPITAL COST/YEAR, $ 000000
00101 34* C CM -MAINTENANCE COST/YEAR, $ 000000
00101 35* C
00103 36* C COMMON /CIMPL/IMPL,ICNT/CTIME/TIME/CSIMUL/DUM(7),TMAX
00103 37* X /COST/CCI,CHI,COP,VDE,TDE,TLO,UTV,UTD,SPD 000000
00104 38* REAL MP2,MP1 000000
00104 39* C
00105 40* IF(IMPL.GT.0)GO TO 100 000000
00107 41* IF(BS.EQ..99999)BS=0. 000000
00111 42* IF(MP1.EQ..99999)MP1=1.E8 000006
00113 43* TMAX1=TMAX*.99999 000013
00114 44* SR=0. 000016
00115 45* SP=0. 000017
00116 46* SPO=0. 000020
00117 47* VSP=0. 000021
00120 48* RE=0. 000022
00121 49* PD=0. 000023
00121 50* C
00121 51* C COMPUTE POWER OUTPUTS 000023
00121 52* C
00122 53* TINC1=DUM(7)*.5 000024
00123 54* IF(BS.LE.MP1)GO TO 100 000027
00125 55* WRITE(6,2GB)BS,MP1 000033
00131 56* 208 FORMAT(1H0,10H BASELOAD ,F12.3,32H EXCEEDS MAXIMUM POWER CAPACITY, 000042
00131 57* 1 F12.3) 000042
00132 58* IF(IMPL.EQ.2)ICNT=ICNT+1 000042
00134 59* BS=MP1 000050
00134 60* C 000050
00135 61* 100 P1=BS 000053
00136 62* MP2=MP1 000054
00137 63* P2=AHIN1(MP1-BS,RE) 000056
00137 64* C 000056
00137 65* C COMPUTE ENERGY COST 000056
00137 66* C
00140 67* CX=0. 000056
00141 68* IF(P2.GT.PD)CX=CP 000065
00143 69* IF(ICO.NE.D)COD=BS*CB+(P2-PD)*CX 000073
00145 70* IF(IMPL.LE.1)RETURN 000104
00145 71* C 000104
00145 72* C STATISTICS 000104
00145 73* C 000104
00147 74* SR=SR+RE*TINC1 000113
00150 75* SPO=SPO+(P1+P2-PD)*TINC1 000117
00151 76* IF(P2.GT.PD) GO TO 200 000125
00153 77* TERM=(PD-P2)*TINC1 000131
00154 78* SPO= SPO+TERM 000135
00155 79* SP= SP+ TERM 000137

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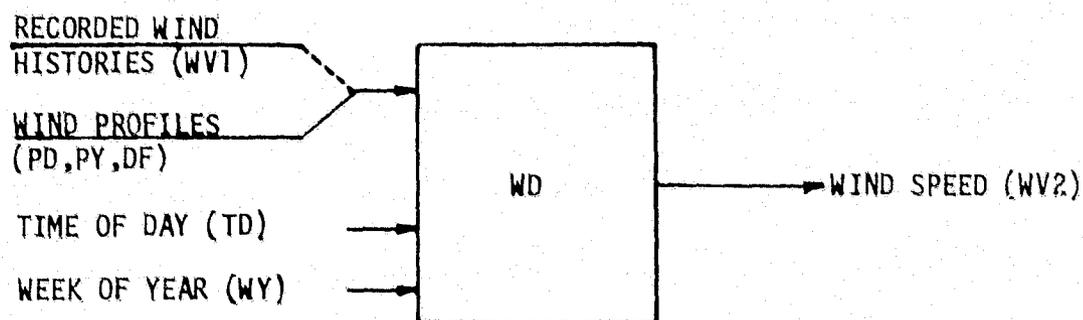
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00156      80*      VSP= VSP+ CB*TERM
00157      81*
00157      82*      C
00157      83*      200 IF (TIME.LT.TMAX)RETURN
00161      84*      CCI=CCI+CC
00162      85*      CMI=CMI+CM
00163      86*      VDE=VDE-CO+VSP
00164      87*      TDE=TDE-SPD+SP
00165      88*      UTV=UTV+CO
00166      89*      UTD=UTD+SPD
00167      90*      SPD= SPD+SP
00170      91*      RETURN
00171      92*      END
```

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000141
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000157
000162
000166
000172
000175
000200
000203
000340
```

## 7.47 WIND



This model computes wind speed either from user supplied time histories (data tape) or by generating a set of random numbers with user supplied daily and yearly average profiles and user specified random variation. If user supplied profiles are available then the wind speeds are generated from the following equation:

### Basic Equation

$$WV = [PD(TD) + N(T)] * PY(WY) / M$$

where PD is the user supplied daily mean profile  
TD is the time of the day  
PY is the user supplied yearly profile  
WY is the week of the year  
N is white noise with user specified probability distribution

$$M = \frac{1}{J} \sum_{i=1}^J PY(i)$$

# WD

<u>Tables</u>	<u>Description</u>	<u>Units</u>
PD	Daily profile versus TD (default = 0)	miles/hr
PY	Yearly profile versus WY	arbitrary
DF	Densit. function for white noise terms (tabular with speed W)	arbitrary

## Inputs

### Parameter/Port

WV	1	Wind speed data file input	miles/hr
TD		Time of day	hr
WY		Week of the year	-

## Outputs

### Variable/Port

WV	2	Wind speed	miles/hr
M		Mean of yearly profile	
TIM		Last time a random sample was generated	hr

## Statistics

MV		Maximum speed	miles/hr
AV		Average speed (expected daily wind)	miles/hr

## Calculation Sequence

- 1) Compute distribution function and mean M (first pass only)

$$F(W) = \frac{(\sum DF(V_i) : V_i \leq W)}{\sum DF(V_i)}$$

- 2) Check for data file input

If  $W1 = .99999$  go to 3)

$W2 = W1$

Go to 5)

- 3) Generate white noise input N

If  $TIME = TIM$  go to 5)

U = random noise sample, uniformly distributed [0,1]

Interpolate to find  $N = F^{-1}(U)$

$TIM = TIME$

- 4) Compute wind speed

$$W2 = [PD(TD) + N] * PY(WY) / M$$

- 5) Compute Statistics

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SUBROUTINE WD ENTRY POINT 000412

STORAGE USED CODE(1) 000473; DATA(0) 000063; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CIMPL 000001  
0004 CTIME 000001

EXTERNAL REFERENCES (BLOCK, NAME)

0005 UNIF  
0006 TBLU1  
0007 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000245	10L	0001	000253	100L	0001	000074	1226	0001	000133	1376	0001	000353	150L						
0001	000202	1556	0001	000225	1656	0001	000146	40L	0000	R	000010	A	0000	R	000005	AMN				
0000	R	000014	0000	I	000006	I	0003	I	000003	IMPL	0000	000024	INJPS	0000	I	000006	IX			
0000	I	000007	L	0000	I	000002	ND	0000	I	000001	NP	0000	I	000012	NP1	0000	I	000003	NY	
0000	R	000004	SUM	0006	R	000000	TRLU1	0004	R	000003	TIME	0000	R	000011	U	0000	R	000013	WV	
0000	R	000015	YVW																	

00100	1*	CWD																		000016
00101	2*		SUBROUTINE WD (PD,PY,WV,AMV,AV,XM,TIMO ,WVI,TD,WY)																	000016
00101	3*	C																		000016
00101	4*	C	PURPOSE	GENERATE WIND SPEED FROM DAILY, YEARLY, AND RANDOM PROFILE DATA																000016
00101	5*	C																		000016
00101	6*	C	METHOD	RANDOM NOISE WITH SPECIFIED DIST. IS ADDED TO MEAN DAILY PROFILE																000016
00101	7*	C		AND MULTIPLIED BY A YEARLY PROFILE. INITIALLY THE DENSITY TABLE																000016
00101	8*	C		WF IS CONVERTED TO A DIST. FUNCTION.																000016
00101	9*	C																		000016
00101	10*	C	WRITTEN BY A.W. WARREN																	000016
00101	11*	C																		000016
00101	12*	C	CALL SEQUENCE																	000016
00101	13*	C	TABLES																	000016
00101	14*	C		PD - MEAN DAILY WIND PROFILE, MPH																000016
00101	15*	C		PY - MEAN YEARLY WIND PROFILE																000016
00101	16*	C		WF - WIND FREQUENCY FUNCTION (NON-GUST, RANDOM COMPONENT), HR																000016
00101	17*	C																		000016
00101	18*	C	OUTPUTS																	000016
00101	19*	C		WV - WIND VELOCITY OUTPUT, MPH																000016
00101	20*	C		AMV - MAX. OBSERVED WIND SPEED, MPH																000016
00101	21*	C		AV - MEAN DAILY WIND SPEED, MPH																000016
00101	22*	C		XM - MEAN YEARLY WIND, -																000016
				TIMO - LAST TIME A RANDOM SAMPLE WAS USED, HR																000016

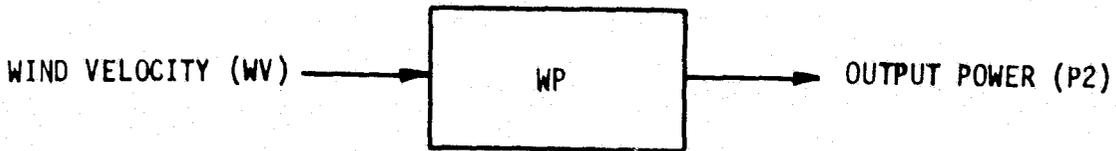
BCS 40180-2

WD



00176	81*	WVO = WVI	000247
00177	82*	GO TO 150	000251
00177	83*		000251
00177	84*	C GENERATE WHITE NOISE WITH DIST. WF	000251
00200	85*	C 100 IF( TIME.EQ.TIME) GO TO 150	000253
00202	86*	CALL UNIF(U,IX)	000255
00203	87*	NP1=NP+1	000261
00204	88*	WN = TBLU1(U,WF(4+NP),WF(3),1,-NP1)	000264
00204	89*	C	000264
00204	90*	C GENERATE WIND SPEED USING DAILY AND YEARLY PROFILES	000264
00205	91*	DWV = TBLU1(TD,PD(4),PD(4+ND),1,-ND)	000303
00206	92*	YWV = TBLU1(WY,PY(4),PY(4+NY),1,-NY)	000323
00207	93*	WV0 = (DWV + WN)* YWV / XM	000343
00210	94*	TIME=TIME	000350
00210	95*	C	000350
00210	96*	C MAX. OBSERVED WIND SPEED	000350
00211	97*	150 IF(IMPL.LE.1) RETURN	000353
00213	98*	AMPV = AMAX1(AMPV,WV0)	000361
00214	99*	RETURN	000367
00215	100*	END	000472

## 7.48 TURBINE/GENERATOR



This component uses a power curve relationship with wind velocity to model the wind turbine and generator. It may be used in place of the more detailed wind turbine-transmission-generator components where a simplified analysis is desirable, or where a nonstandard wind generator model is desired. The model may be used for either A.C. or D.C. power generation.

### Basic Equations

$$P_2 = 0 \quad \left( \begin{array}{l} WV < W_{V0} \\ WV > W_{V1} \end{array} \right)$$

$$P_2 = V^3 / 1000 \quad W_{V0} \leq WV \leq W_{V1}$$

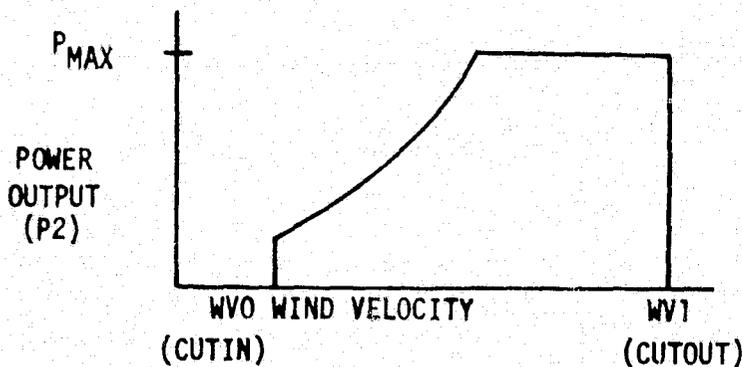


FIGURE 7.48: OUTPUT POWER VERSUS WIND VELOCITY

<u>Tables</u>	<u>Description</u>	<u>Units</u>
PW	Wind generation power versus wind velocity <sup>1</sup>	kw
<u>Inputs</u>		
<u>Parameter/Port</u>		
V	Bus voltage (Rated)	volts
WO	Power cutin velocity	mph
W1	Power cutout velocity	mph
W	Wind velocity	mph
CC	Capital cost/year	\$
CM	Maintenance cost/year	\$
EC	Control Energy Rate	\$/hr
<u>Outputs</u>		
<u>Variable/Port</u>		
I	Bus current	amps
P	2 Real power output	kw
<u>Statistics</u>		
MI	Maximum current	amps
MP0	Maximum power	kw
SP	Total output energy	kwh
C0	Total operating costs	\$

<sup>1</sup> Output power including mechanical and electrical efficiencies

## Calculation Sequence

1) Initialize statistics

2) Compute P2 and I

$$P2 = \begin{pmatrix} PW(W) & W0 \leq W \leq W1 \\ 0 & \text{otherwise} \end{pmatrix}$$

$$I = P2 * 1000 / V$$

3) Compute Statistics and Costs

SUBROUTINE WP ENTRY POINT 000153

STORAGE USED CODE(1) 000232; DATA(1) 000024; BLANK COMMON(2) 000000

## COMMON BLOCKS

```

0003 CIMPL 000001
0004 COST 000003
0005 CTIME 000001
0006 CSIMUL 000010

```

## EXTERNAL REFERENCES (BLOCK, NAME)

```

0007 TBLU1
0010 NERR35

```

## STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

```

0001 000046 10L      0001 000064 20L      0004 R 000000 CC      0004 R 000001 CM      0004 R 000002 COP
0006 000000 DUM      0003 I 000000 IMPL     0000 000006 INJPS    0000 I 000000 N      0007 R 000000 TBLU1
0005 R 000000 TIME    0006 R 000006 TINC     0006 R 000007 TMAX    0000 R 000001 TMAX1

```

```

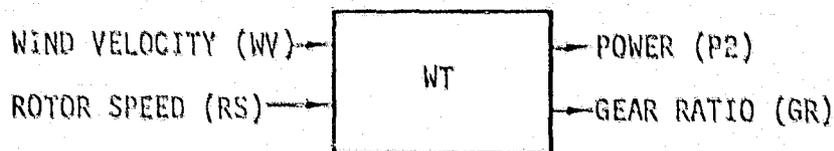
00100 1* CWP
00101 2* SUBROUTINE WP ( PW,BI,PO,AMI,AMP,SP,CO,VO,WVC,WV1,WV,CCI,CHI,EC)
00101 3* C
00101 4* C PURPOSE MODEL THE WIND TURBINE AND GENERATOR USING A POWER CURVE
00101 5* C
00101 6* C WRITTEN BY A.W. WARREN VERSION 1, MARCH 3 1977
00101 7* C
00101 8* C CALL SEQUENCE
00101 9* C TABLES
00101 10* C PW - WIND GENERATION POWER IN KW VERSUS WIND VELOCITY IN MPH
00101 11* C
00101 12* C OUTPUTS
00101 13* C BI - OUTPUT BUS CURRENT, AMPS
00101 14* C PO - POWER OUTPUT, KW
00101 15* C AMI - MAX. OBSERVED CURRENT, AMPS
00101 16* C AMP - MAX. OBSERVED POWER, KW
00101 17* C SP - TOTAL OUTPUT ENERGY, KWH
00101 18* C CO - OPERATING COST, $
00101 19* C
00101 20* C INPUTS
00101 21* C VO - RATED BUS VOLTAGE, VOLTS
00101 22* C WVO - POWER CUTIN VELOCITY, MPH
00101 23* C WV1 - POWER CUTOUT VELOCITY, MPH
00101 24* C WV - WIND VELOCITY, MPH
00101 25* C CCI - CAPITOL COST / YEAR, $

```

W/P



## 7.49 WIND TURBINE



This component models the wind turbine in terms of physical properties such as blade radius, power coefficient, and design tip speed ratio.<sup>1</sup> The step-up gear ratio is computed based on design rotor speed.

### Basic Equations

Output power is given by

$$P2 = CP * 1/2 * AD * A * (W * C)^3 * k$$

where:

CP = effective power coefficient (tabular with WV)

A =  $\pi * (BR)^2$

C = 1.4667 (mph to ft/sec. conversion)

k =  $1.3558 \times 10^{-5}$  (ft-lb to kw-sec. conversion)

<sup>1</sup> NASA CR 134937 "Design Study of Wind Turbines - 50kw to 3000 kw - For Electric Utility Applications", Kaman Aerospace Corporation, February 1976.

## Inputs

<u>Parameter/Port</u>	<u>Description</u>	<u>Units</u>
WV	Wind speed	mph
V0	Mean wind speed (yearly)	mph
VR	Rated wind speed (default = $1.35 \times V0$ )	mph
RS	Rotor speed	rpm
RSG	Generator shaft speed (design)(default = 1800)	rpm
BR	Blade radius	ft
EC	Cost to operate controls	\$/h
AD	Air density (default = 0.0023)	slugs/ft <sup>3</sup>
LAM <sup>1</sup>	Design tip speed ratio (default = 9.4)	-
CPM <sup>2</sup>	Maximum power coefficient at V0 (default = 0.4)	-
CP	Effective power coefficient (default table versus V0/W)	-
CC	Capital cost/year	\$
CM	Maintenance cost/year	\$

## Outputs

<u>Variable/Port</u>		<u>Description</u>	<u>Units</u>
P	2	Output mechanical power	kw
T0		Mechanical torque	ft-lb
C0		Total operating cost	\$
GR		Step-up gear ratio	-
RAP		Rated output power	kw

## Statistics

MT	Maximum torque	ft-lb
MP0	Maximum power	kw
SP	Total energy delivered	kwh

<sup>1</sup> LAM may be computed using the design equation:

$$LAM = \text{SQRT}(8 / (3 * \text{solidity constant} * \text{design lift coefficient}))$$

<sup>2</sup> If default CP table not used then set CPM = CP(rated wind speed)

## Calculation Sequence

- 1) First pass - Compute Gear Ratio and Rated Power

$$RS = (LAM * V_0 * C / BR) * (60 / 2\pi)$$

$$GR = RSG / RS$$

$$RAP = .5 * CP1 * AD * A * (VR * C)^3$$

where

$$CP1 = \begin{cases} CPM * F(V_0 / VR) & \text{if CP default used} \\ CPM & \text{otherwise} \end{cases}$$

- 2) Compute power coefficient CP

If  $W = 0$  set  $P2 = T_0 = 0$  and go to 4)

If CP default used, then

$$CP = CPM * F(V_0 / W)$$

where F is shown in Figure 7.49

- 3) Power and torque

$$A = \pi * BR^2$$

$$P = .5 * CP * AD * A * (WV * C)^3 \quad (C = 1.4667)$$

$$T_0 = P / (RS * 2\pi / 60)$$

$$P2 = P * k \quad (k = 1.3558 \times 10^{-3})$$

- 4) Compute Statistics and Costs

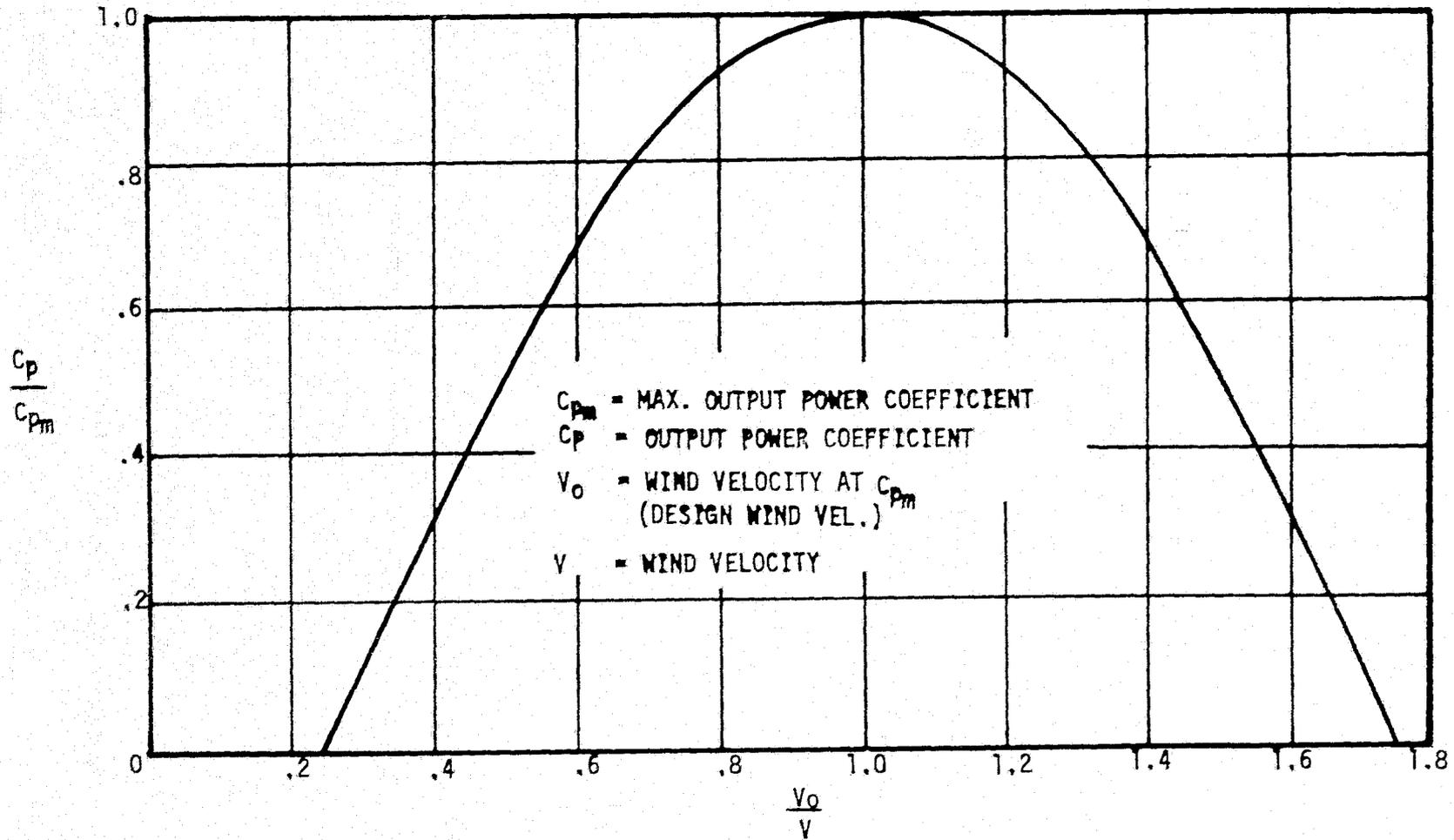


FIGURE 7.49 GENERALIZED MACHINE POWER OUTPUT PERFORMANCE

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SUBROUTINE WY ENTRY POINT 000274

STORAGE USED CODE(1) 000413; DATA(0) 000070; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 C1MPL 000001  
0004 CTIME 000001  
0005 CSIMUL 000010  
0006 COST 000003

EXTERNAL REFERENCES (BLOCK, NAME)

0007 TELUI  
0010 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000122	100L	0001	000211	200L	0000	R	000034	A	0006	R	000000	CCI	0006	R	000001	CHI		
0006	R	000002	COI	0000	R	000033	CP1	0000	R	000026	C1	0000	R	000027	C2	0005	000000	DUM	
0000	R	000000	F	0003	I	000000	IMPL	0000	000051	INJPS	0000	R	000035	P	0000	R	000030	PI	
0007	R	000000	TPUI	0004	R	000000	TIME	0005	R	000006	TINC	0000	R	000032	TINC2	0005	R	000007	TMAX
0000	R	000031	TMAX1																

00100	1*	CNT1																		000000
00101	2*		SUBROUTINE WY (P2,TO,CO,GR,RAP,MT,MPO,SP,WV,VO,VR,RS, RSG,BR,EC,																	000000
00101	3*		1	AD,LAM,CPM, CP,CC,CM)																000000
00101	4*	C																		000000
00101	5*	C	PURPOSE	MODEL WIND TURBINE POWER OUTPUT																000000
00101	6*	C																		000000
00101	7*	C	METHOD	COMPUTE POWER COEFFICIENT AND ROTOR SPEED FROM PHYSICAL																000000
00101	8*	C		DESIGN PARAMETERS. RATED POWER COEFF. IS 3/4 OF CPH.																000000
00101	9*	C																		000000
00101	10*	C	WRITTEN BY A. W. WARREN							VERSION 2, APRIL 6 1977										000000
00101	11*	C																		000000
00101	12*	C	CALL SEQUENCE																	000000
00101	13*	C	OUTPUTS																	000000
00101	14*	C		P2 - OUTPUT MECHANICAL POWER, KW																000000
00101	15*	C		TO - OUTPUT MECHANICAL TORQUE, FT-LB																000000
00101	16*	C		CO - OPERATING COST SUM, \$																000000
00101	17*	C		GR - TURBINE/GENERATOR GEAR RATIO																000000
00101	18*	C		RAP - RATED OUTPUT POWER, KW																000000
00101	19*	C		MT - MAXIMUM TORQUE STATISTIC, FT-LB																000000
00101	20*	C		MPO - MAXIMUM POWER STATISTIC, KW																000000
00101	21*	C		SP - TOTAL OUTPUT ENERGY DELIVERED, KWH																000000
00101	22*	C																		000000
00101	23*	C	INPUTS																	000000

WT

00101	24*	C	WV - WIND SPEED MPH	000000
00101	25*	C	VO - MEAN WIND SPEED (YEARLY), MPH	000000
00101	26*	C	VR - RATED WIND SPEED, MPH	000000
00101	27*	C	RS - ROTOR SPEED, RPM	000000
00101	28*	C	RSG - GENERATOR SHAFT SPEED, RPM	000000
00101	29*	C	BR - BLADE RADIUS, FT	000000
00101	30*	C	EC - CONTROL ENERGY RATE, \$/HR	000000
00101	31*	C	AD - AIR DENSITY, SLUGS/FT**3	000000
00101	32*	C	LAM - DESIGN TIP SPEED RATIO	000000
00101	33*	C	CPM - MAXIMUM POWER COEFFICIENT AT VO	000000
00101	34*	C	CP - EFFECTIVE POWER COEFFICIENT AT WV	000000
00101	35*	C	CC - CAPITAL COST PER YEAR	000000
00101	36*	C	CM - MAINTENANCE COST PER YEAR	000000
00101	37*	C		000000
00103	38*		COMMON /CINPL/IMPL /CTIME/ TIME /CSIMUL/ DUM(6),TINC,TMAX	000000
00104	39*		COMMON /COST/ CCI,CHI,COI	000000
00105	40*		REAL MT,MPO,LAM	000000
00106	41*		DIMENSION F(22)	000000
00107	42*		DATA F/.24,.4,.6,.68,.8,1.,1.2,1.31,1.4,1.6,1.74,0.,.31,.68,.8,	000000
00107	43*		1 .92,1.,.92,.8,.68,.3,0. /,C1,C2,PI/1.4667,.0013558,3.14159	000000
00107	44*	C		000000
00107	45*	C	INITIALIZATION	000000
00107	46*	C		000000
00114	47*		IF(IMPL.GT.0) GO TO 100	000000
00116	48*		TMAX1 = TMAX* .99999	000002
00117	49*		TINC2 = .5* TINC	000005
00117	50*	C		000005
00120	51*		IF( VR .EQ. .99999) VR = 1.35* VO	000010
00122	52*		IF(RSG .EQ. .99999) RSG= 1800.	000016
00124	53*		IF( AD .EQ. .99999) AD = .0023	000026
00126	54*		IF(LAM .EQ. .99999) LAM= 9.4	000033
00130	55*		IF(CPM .EQ. .99999) CPM= 0.4	000040
00130	56*	C		000040
00132	57*		RS = C1*LAM*VO/BR*(30./PI)	000045
00133	58*		GR = RSG /RS	000055
00134	59*		CP1= CPM	000060
00135	60*		IF(CP.EQ. .99999) CP1= CPM*TBLU1(VO/VR,F(1),F(12),1,-11)	000062
00137	61*		RAP= .5*CP1*AD*PI*BR*RR*(VR*C1)**3+C2	000101
00140	62*		CO = 0.0	000115
00141	63*		SP = 0.0	000116
00142	64*		MPO= 0.0	000117
00143	65*		MT = 0.0	000120
00143	66*	C		000120
00143	67*	C	POWER COEFFICIENT CALCULATION	000120
00143	68*	C		000120
00144	69*		100 P2 = 0.0	000122
00145	70*		T0 = 0.0	000122
00146	71*		IF( WV.EQ. 0.) GO TO 200	000123
00150	72*		CP1 = CP	000125
00151	73*		IF( CP1.EQ. .99999) CP1 = CPM*TBLU1(VO/WV,F(1),F(12),1,-11)	000127
00153	74*		IF(CP1.EQ. 0.) GO TO 200	000151
00153	75*	C		000151
00153	76*	C	OUTPUT POWER AND TORQUE	000151
00153	77*	C		000151
00155	78*		A = PI*BR**2	000153
00156	79*		P = .5*CP1*AD*A*(WV*C1)**3	000157
00157	80*		IF(WV.GT.VR)P= RAP/C2	000170

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WT

00161	81*		T0=P/(RS*PI/30.)		000177
00162	82*		P2 = P*C2		000205
00162	83*	C			000205
00162	84*	C		STATISTICS AND COSTS	000205
00162	85*	C			000205
00163	86*		200 IF(IMPL.LE.1) RETURN		000211
00163	87*	C			000211
00165	88*		CO = CO + EC*TINC2		000217
00166	89*		MT = AHAX1( MT,T0)		000223
00167	90*		MPO= AHAX1(MPO,P2)		000231
00170	91*		SP = SP + P2*TINC2		000237
00170	92*	C			000237
00171	93*		IF(TIME.LT.TMAX)RETURN		000243
00173	94*		CCI = CCI + CC		000252
00174	95*		CHI = CHI + CM		000255
00175	96*		COI = COI + CO		000260
00175	97*	C			000260
00176	98*		RETURN		000263
00177	99*		END		000412

## 8.0 EXAMPLES

This section gives five simple example simulations using the SIMWEST program. These examples exercise all physical components of the SIMWEST library and many of the model features such as Fortran code insertion and the file read capability. Each example contains the input data for model generation and analysis, selected printer output generated by the programs and a discussion of the results obtained. It is recommended that a user work through and understand the model connections for these examples before attempting to build more complex models such as that of Figure 1-7.

### 8.1 WIND TURBINE AND FILE READ MODEL

Figure 8.1-1 shows a simplified schematic of the wind turbine and file read model. In this example a wind turbine is used to feed power directly to a load. Wind and load time histories are read from a mass storage file and then used to drive the simulation. A histogram for power output is also included. Figure 8.1-2 shows the input data to build the model and print out some of the load file data. The order of the component definitions is such that information passes down the list, i.e. no component is defined before components in the INPUTS list. This assures that the component subroutines in the Fortran model will be called in the right order. The first Fortran statement is inserted in the model prior to the Fortran which sets up the iteration loop, while the second set of Fortran statements is within the loop and writes out the load file data from array TEMP the first pass through the model. Figure 8.1-3 shows the model schematic generated. In addition to showing the component connections, the names of the input connections are printed out. Notice that information passes not only from WT to GR but also vice-versa. The input RSIGR to WT is a feedback variable and so is the input RS GE to GR. It is the presence of the feedback variables which require several iterations to attain steady state.

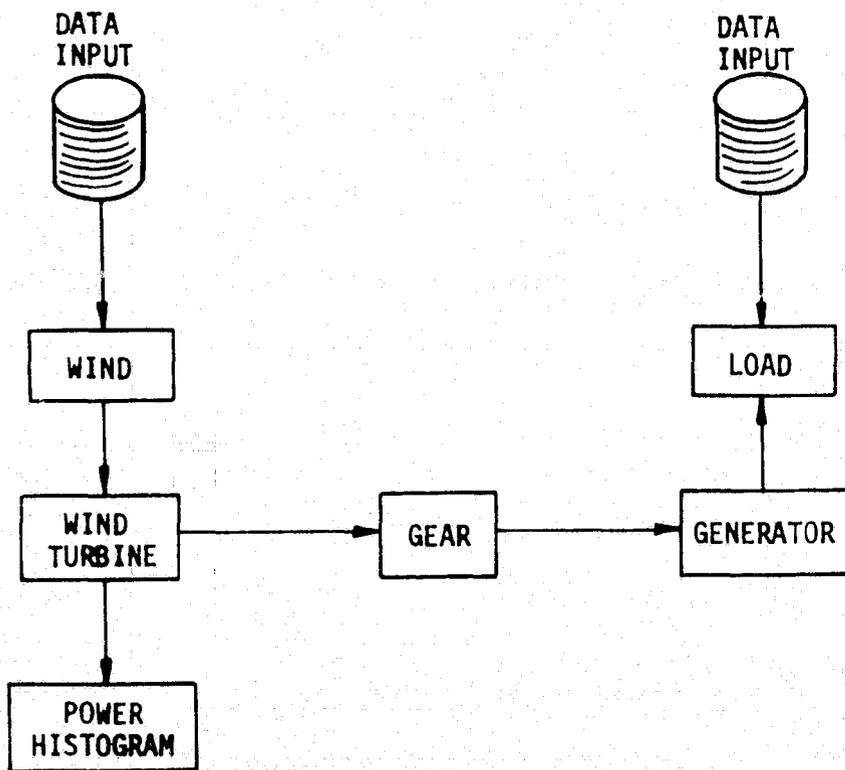


FIGURE 8.1-1: WIND TURBINE AND FILE READ EXAMPLE

```

MODEL DESCRIPTION      TAPE READ TEST
FORTRAN STATEMENTS
COMMON /DATARD/ TEMP(448)
LOCATION=15      TI
LOCATION=3       TAW      INPUTS=TI
LOCATION=11      WD      INPUTS=TI,TAW(VAR=W)
LOCATION=31      WT      INPUTS=WD
LOCATION=35      GR      INPUTS=WT
LOCATION=51      HG      INPUTS=WT(P =FIN)
LOCATION=39      GE      INPUTS=GR
LOCATION= 7      TAL     INPUTS=TI
LOCATION=19      LO     INPUTS=GE,TI,TAL(VAR=LO)
FORTRAN STATEMENTS
IF(IMPL.GT.0) GO TO 2
WRITE (6,100) (TEMP(I),I=1,448)
100 FORMAT(1H ,12F10.3)
2 CONTINUE
END OF MODEL
LIST STANDARD COMPONENTS
PRINT

```

FIGURE 8.1-2 INPUT DATA FOR FILE READ MODEL

The input data for several simulations using this model is shown in Figure 8.1-4. The component parameter values are first specified, those inputs not specified taking default values. A number of tables are then specified. The WD and LO tables are not really needed here. The wind and load file data was originally generated from an earlier run using these tables. Following the tables are the printer plot input commands, and the simulation values and print commands for a one week run. The parameter values for a second simulation which reads to the end of the file are then given. The last simulation attempts to read past the end of file.

Some of the output for the first simulation are shown in Figures 8.1-5 to 8.1-8. Figure 8.1-5 shows the output resulting from the FORTRAN STATEMENTS code. This data is formatted to output the time of the initial load value (0.0), the data increment step (0.25), and 446 load values at successive time increments. Figure 8.1-6 shows the power output histogram from the wind turbine. Almost 40% of the time the turbine reaches rated power (800 kw). Figure 8.1-7 shows a crossplot of wind turbine output versus wind velocity. The cutin velocity is about 12 mph and rated power is attained at about 28



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```
TITLE= TAPE READ TEST
PARAMETER VALUES
CYCLES=2.01, T0 TI=0, FUPHG=1000, FLOHG=50, NSTTAW=0, ITFTAW=1
UD WT=21, BR WT=80, EC WT=1, CPMWT=.41, CC WT=16000, CM WT=2000
RPSGE=.01, CC GR=1000, CM GR=200, NSTTAL=0, ITFTAL=2
RPSGE=750, RSYGE=1800, DA GE=0.2, SR GE=.005, UD GE=400, CC GE=1000, CM GE=200
N0 LO=.00574, CT LO=4, MN LO=0, STOLO=6, VE LO=.023
TABLE, PY WD=13
0., 4.33, 8.67, 13., 17.33, 21.67, 26., 30.33, 34.67, 39., 43.33, 47.67, 52.
55, 67, 68, 65, 61, 56, 51, 49, 49, 52, 56, 61, 65
TABLE, PD WD=7
0, 4, 8, 12, 16, 20, 24
0, 0, 0, 6, 6, 6, 0
TABLE, DF WD=16
0, 3, 6, 9, 12, 15, 18, 21, 24, 27, 30, 33, 36, 39, 42, 45
5, 44, 160, 380, 480, 512, 440, 376, 307, 270, 148, 76, 40, 22, 9, 3
TABLE, PLOGR =7
0, 100, 200, 300, 400, 500, 600
0, 4, 9, 18, 32, 50, 72
TABLE, PD LO=17
0, 1.5, 3, 4.5, 6, 7.5, 9, 10.5, 12
13.5, 15, 16.5, 18, 19.5, 21, 22.5, 24
45, 60, 372, 330, 450, 660, 810, 798, 804
650, 702, 699, 702, 750, 708, 570, 450
TABLE, FW LO=7
1, 2, 3, 4, 5, 6, 7
1, 1.5, .9, .9, .6, .5
TABLE, PY LO=6
0, 10, 20, 30, 40, 50
196, 194, 180, 174, 194, 226
PRINT, PLOTS, DISPLAY1
PP WD, US, TIME
PP NT, US, P2WD
PP GR, US, P2 WT
PC LO, US, TIME
PC LO, US, TIME
DISPLAY2, P2 GE, US, TIME
TIME=.25, TMAX=168., PRATE=24, PRINT CONTROL=3, INT MODE=3, OUTFRATE=2
SIMULATE
PARAMETER VALUES, T0 TI=4200, NSTTAW=38, NSTTAL=39, TMAX=220
SIMULATE
PARAMETER VALUES, NSTTAL=40,
```

FIGURE 8.1-4 INPUT DATA FOR ANALYSIS PROGRAM

mph. The load-time profile for the simulation is shown in Figure 8.1-8. Daily peaks and troughs are clearly indicated. The lower levels of the last two days reflect week-end load modeling.

TAPE READ TEST

CASE NO. 1

IDENTIFICATION HEADER FOR UNIT 11  
NO GENERATED MIND DATA

IDENTIFICATION HEADER FOR UNIT 12  
LO GENERATED LOAD DATA

000	250	512,020	576,458	541,275	542,305	504,160	490,027	458,856	465,241	471,429	461,310
472,202	469,504	484,207	478,548	457,784	462,708	428,157	417,025	435,024	424,541	477,498	477,597
524,878	529,255	580,527	574,953	655,125	684,704	751,090	774,545	849,244	842,653	919,063	906,349
976,191	971,344	1035,062	1030,417	1019,400	1025,785	1025,351	1015,678	1029,436	1016,803	1021,731	1030,062
1036,085	1020,695	1024,203	1026,614	982,779	972,742	929,110	935,981	880,347	874,323	886,260	897,320
894,753	914,397	906,599	905,685	896,960	897,141	895,837	899,829	899,173	897,042	908,923	887,126
902,818	898,822	898,457	898,273	910,522	928,584	951,416	932,214	966,968	961,958	927,407	940,644
906,296	909,801	914,014	904,625	848,249	849,443	783,334	799,167	737,316	728,981	668,681	668,212
622,550	653,111	566,890	571,379	529,372	544,840	509,411	501,604	464,107	453,340	459,528	467,007
460,501	477,917	482,686	483,800	462,589	457,579	444,235	439,874	419,515	429,792	483,195	466,143
526,520	528,161	572,035	570,269	660,377	652,042	770,330	756,319	843,668	857,838	896,782	901,220
957,964	976,595	1026,770	1039,277	1021,489	1024,710	1030,602	1024,092	1031,524	1028,826	1013,439	1024,933
1010,194	1036,326	1032,617	1025,094	991,639	974,384	937,970	924,526	874,771	866,031	886,739	888,582
910,631	899,353	897,415	907,327	909,429	902,392	897,479	895,145	901,262	885,588	900,631	888,768
897,689	893,247	886,110	907,132	909,001	926,617	950,342	937,912	958,230	960,458	963,353	935,515
929,145	918,661	895,342	903,105	849,841	844,314	785,423	780,048	725,415	734,232	684,312	683,844
620,583	621,210	527,518	515,674	487,255	479,243	454,255	434,638	413,080	415,578	421,951	409,596
425,091	425,911	429,801	427,555	417,808	404,358	389,100	388,022	376,195	378,948	417,267	427,101
469,653	461,386	516,310	539,500	592,569	600,906	670,397	672,822	764,028	771,088	805,735	828,013
812,988	858,862	932,067	940,076	917,971	932,658	923,327	932,503	929,850	921,327	920,069	942,602
917,149	934,573	925,140	924,464	878,517	881,672	830,214	842,894	801,363	796,343	790,602	795,509
808,635	804,783	818,895	811,978	807,374	814,032	812,055	807,109	803,271	810,696	812,447	801,771
806,953	818,793	799,780	808,956	826,075	820,398	835,254	839,504	854,944	865,672	850,213	837,347
822,271	837,615	832,466	814,272	757,037	770,703	702,264	691,352	654,351	653,748	608,418	607,997
566,499	567,063	522,901	523,648	498,076	490,064	449,639	451,553	411,712	436,143	423,429	408,227
420,876	436,731	431,681	429,435	413,593	408,683	405,614	402,090	378,074	386,922	421,993	438,323
474,379	466,112	508,445	528,789	594,047	596,289	680,816	677,548	750,470	775,412	807,615	820,550
868,372	872,950	942,887	935,459	925,544	915,451	925,206	921,792	913,044	913,864	912,204	922,549
915,379	911,673	926,217	919,446	883,644	883,150	834,940	841,525	791,053	794,974	805,072	799,833
801,172	794,474	811,432	814,259	824,690	812,262	807,840	811,835	801,501	806,079	804,181	800,402
814,525	820,271	800,856	819,777	827,553	837,715	861,511	838,135	850,327	864,102	858,187	844,919
838,785	823,656	812,413	809,656	756,070	757,145	709,836	711,495	659,479	661,320	609,896	615,971
571,225	562,447	518,686	512,937	481,270	488,695	448,270	450,184	410,343	406,747	403,375	418,646
416,260	429,268	417,722	425,220	421,165	413,810	392,056	388,131	376,304	385,152	429,967	427,612
472,609	473,684	513,171	521,326	592,678	592,074	679,849	682,274	761,291	758,607	818,435	812,685
863,755	874,428	935,424	940,586	939,612	929,921	920,590	930,167	914,924	918,590	923,426	908,991
923,353	916,399	928,498	927,420	878,626	885,029	827,477	834,062	804,720	796,452	809,396	801,713
796,556	789,857	809,662	803,548								

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FIGURE 8.1-5 TAPE READ FORMATTED LOAD DATA



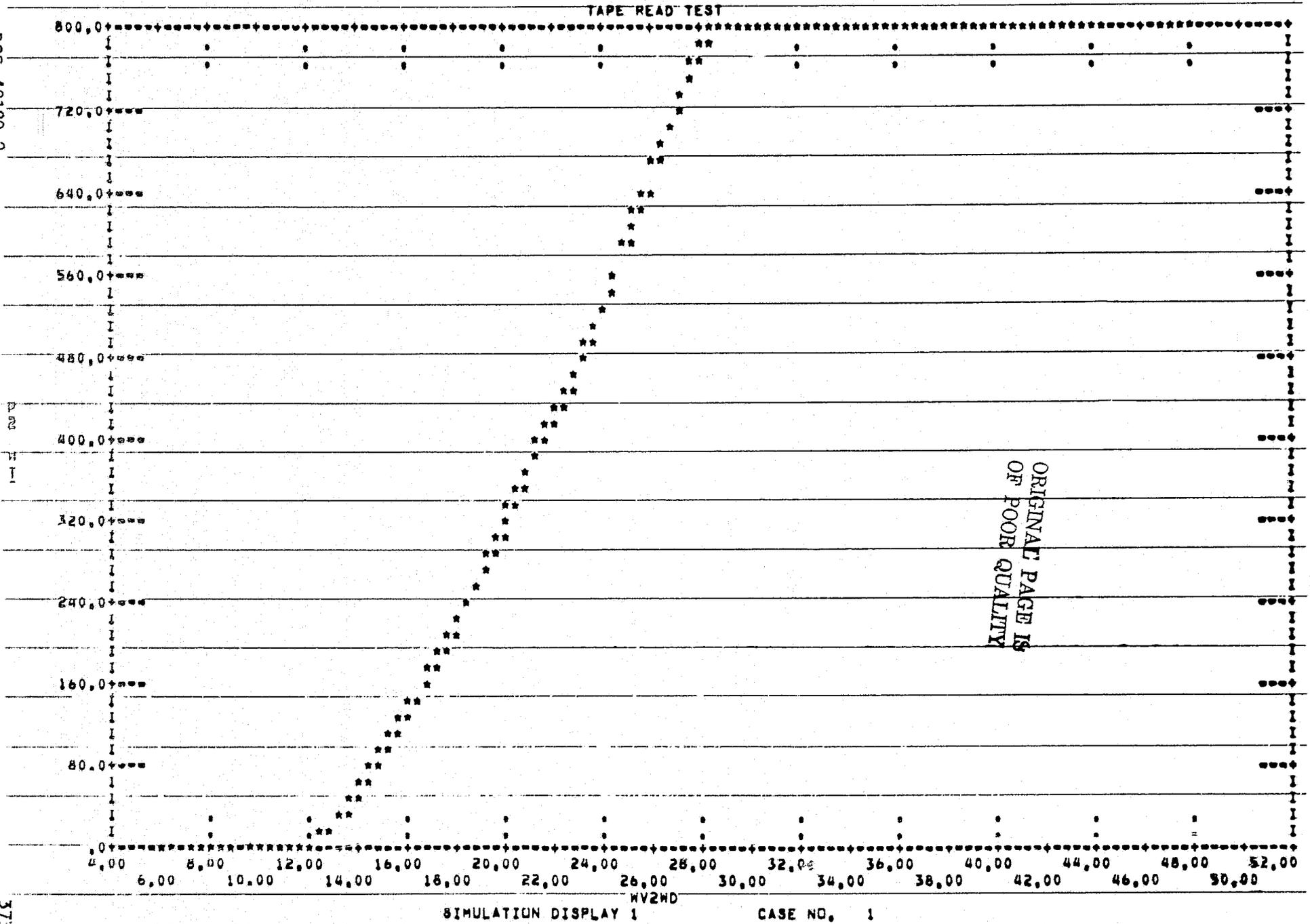


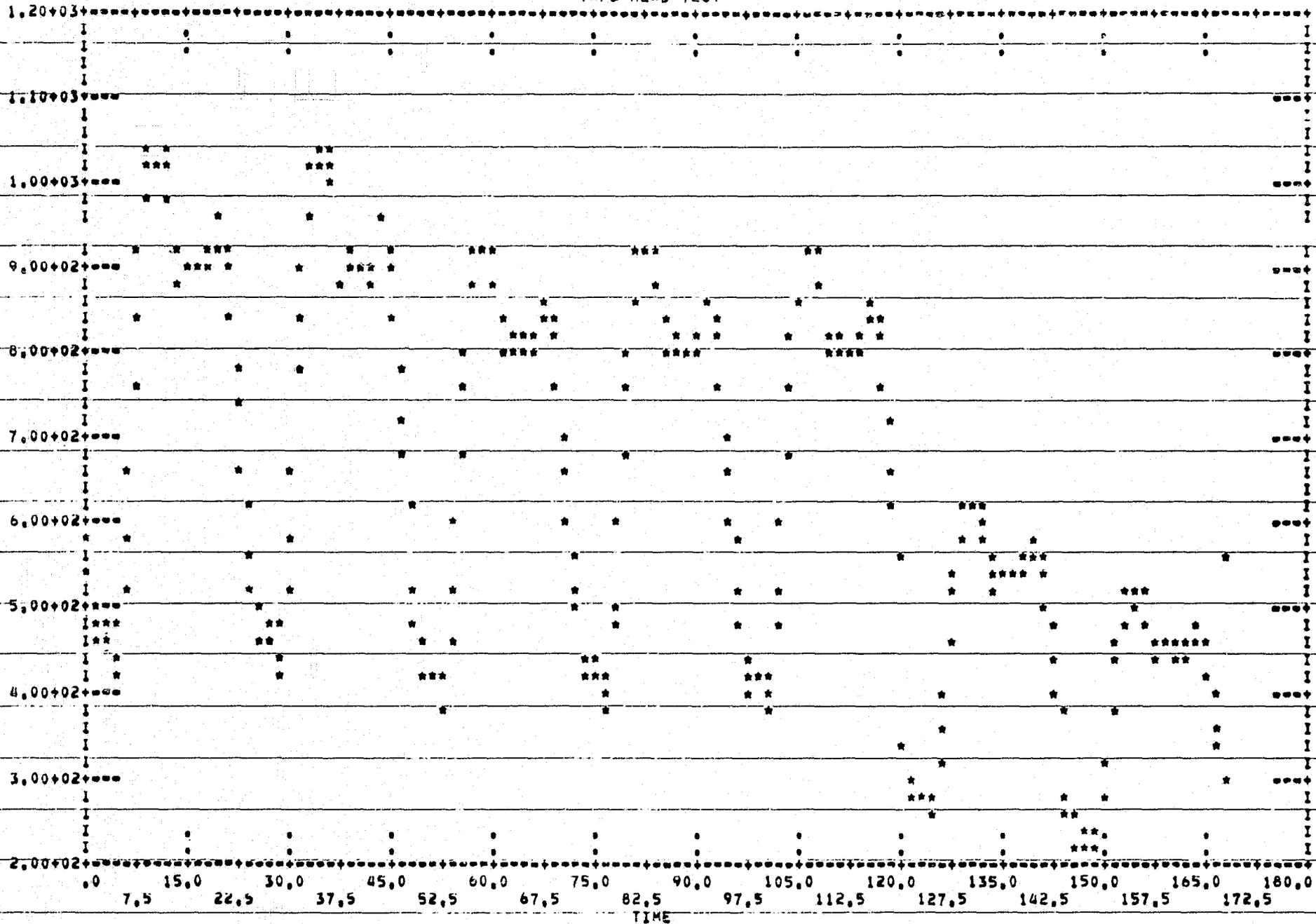
FIGURE 8.1-7 WIND POWER OUTPUT VERSUS WIND VELOCITY

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TAPE READ TEST

JAN 13

BCS 40180-2



SIMULATION DISPLAY 1

CASE NO. 1

FIGURE 8.1-8 WEEKLY LOAD PROFILE

## 8.2 BATTERY STORAGE MODEL

A simplified schematic of the battery storage model is shown in Figure 8.2-1. In this model, wind power supplemented by a utility generation source is supplied to a power divider, which delivers power to the load as a first priority, and battery storage as second priority. Similarly, if the load cannot be met from the wind or storage, then the utility is requested to supply peaking power to meet the load. This model exercises the logic components including the priority Interrupt.

Figure 8.2-2 shows the model generation input data for the model. The components are generally defined in the order of power flow shown in Figure 8.2-1. Ordering the component definition in this way is recommended to avoid convergence problems in the iteration loop. Thus, it would be somewhat better for consistency to define UT after WP rather than after LO in the model. All three types of model connections are illustrated in this example. For example, WP has the general input connection WD, MAB has the specific input connection WP (P,2 = FIN), and PD has the port to port connection PA (1,1). The port connections are especially useful for connecting up the multiport logic components PA and PD. The connection PA (1,1), for example, connects an input request of PD to PA and a power and maximum power input of PA to PD. It may be observed that the utility is connected up to the surplus port of PD. Thus the baseload power sent to MAB in effect is reduced whenever the load and battery cannot absorb all the power generated. The last component defined is the cost monitor CM, which receives cost input data from other components through a common block rather than by model connections. Figure 8.2-3 shows the model schematic generated by the program. Most of the connection inputs are shown but occasionally a model connection will be overprinted. For example, the input RE1PA to PD is not shown in 8.2-3. In cases like this it is necessary to check the Fortran model (EQMO) in order to verify the model connections.

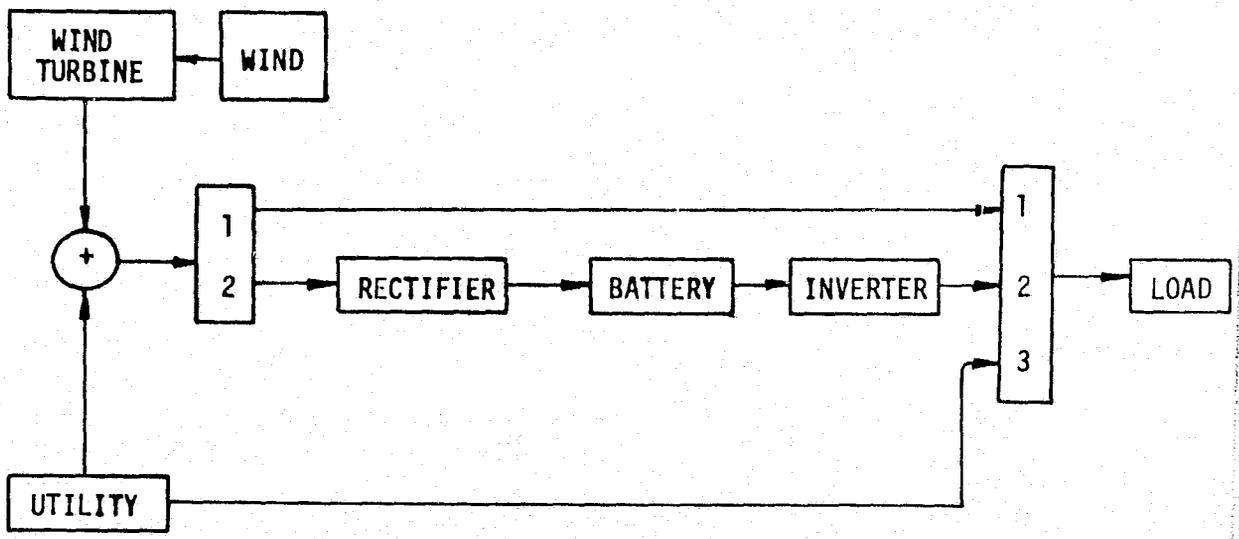


FIGURE 8.2-1: BATTERY STORAGE EXAMPLE

MODEL DESCRIPTION		BATTERY TEST CASE
LOCATION=74	TI	
LOCATION=61	WD	INPUTS=TI
LOCATION=21	WP	INPUTS=WD
LOCATION=42	MAB	INPUTS=WP (P, 2=FIN), UT(P, 1=C2)
LOCATION=33	PD	INPUTS=MAB(FO=P), MAB(FO=MP), PA(1,1), PIB(2,2), BA(RE=RE, 2)
LOCATION=15	RE	INPUTS=PD (2,1)
LOCATION=17	BA	INPUTS=RE, PA(RE, 2=RE)
LOCATION=45	PIB	INPUTS=BA
LOCATION=19	IV	INPUTS=BA
LOCATION=69	PA	INPUTS=IV(2,2), LO(1,0) PIB(4,2), UT(2,3)
LOCATION=76	LO	INPUTS=TI
LOCATION=62	UT	INPUTS=PD(SP=P, 0)
LOCATION=1	CM	
END OF MODEL		
LIST STANDARD COMPONENTS		
PRINT		

FIGURE 8.2-2 BATTERY MODEL INPUT DATA

The input data for two simulations is shown in Figure 8.2-4. In the first simulation the battery is nearly full at time = 0 and the load is chosen larger on the average than the wind and utility power supplied. In the second simulation the reverse is true, i.e. the load is less than that supplied by the wind system, and the battery storage is fairly low. Figures 8.2-5 to 8.2-8 show results from the first simulation. The cost monitor output is shown in Figure 8.2-5. The energy cost of the wind system is low because the wind profile delivers high energy winds during most of the simulation. The average wind velocity in Figure 8.2-6 is about 22 mph. Figure 8.2-7 shows the wind power output supplied directly to the load. The median power output is seen to exceed 450 kw and occasionally output reaches 800 kw or rated power. Figure 8.2-8 shows the usage of battery energy to meet the load during the week, and the increase in storage capacity during the weekends. Since the battery subsystem was limited to 180 kw maximum discharge, the utility was frequently called to meet peak load. Thus about 10% of the load was satisfied by the utility.



TITLE= BATTERY MODEL TEST  
PARAMETER VALUES  
CR CM=15.,LE CM=30.  
BS UT=20.,CB UT=.016,CP UT=.03,CC UT=1000.,CM UT=1000.  
C1 HAMB1.  
CYCLES=4.01,TO TIME=0,V WP=400,WVOWP=8,WV1WP=60,DLINES=100.  
CC WP=16000,CM WP=1200,PS1PYB=2.  
EC WP=.2  
NC LD=.005,CT LD=4,MN LD=0,STDLD=6,VE LD=.023  
RAPBA=200.,E1 BA=2000.,EDEBA=100.  
VQ BA=100  
DT BA=10.,CC BA=2000.,CM BA=100.  
RAPRE=200.,CC RE=200.,RAPIV=200.,CC IV=0.  
TABLE,PW WP=10  
8,10,12,14,16,18,20,21,53,25,30  
25,6,50,1,86,5,137,4,205,1,292.,400,6,500,782,8,800  
TABLE,PY WDM=13  
0.,4,33,8,67,13.,17,33,21,67,26.,30,33,34,67,39.,43,33,47,67,52.  
65,67,68,65,61,56,51,49,49,52,56,61,65  
TABLE,PD WDM=7  
0,4,8,12,16,20,24  
10,12,14,16,14,12,10  
TABLE,DF WDM=16  
0,1,2,3,4,5,6,7,8,9,10,11,12,13,14,15  
5,44,160,380,480,512,440,376,307,270,148,76,40,22,9,3  
TABLE,PD LD=17  
0,1,5,3,4,5,6,7,5,9,10,5,12  
13,5,15,16,5,18,19,5,21,22,5,24  
450,360,372,330,450,660,810,798,804  
690,708,699,702,750,708,570,450  
TABLE,PW LD=7  
1,2,3,4,5,6,7  
1,1,9,9,9,6,.5  
TABLE,PY LD=6  
0,10,20,30,40,52  
226,194,180,174,194,226  
INITIAL CONDITIONS,PE BA =1990.  
PRINTER PLOTS,DISPLAY1  
WV2WD,V,S,TIME  
P1 PD,V,S,TIME  
P2 PD,V,S,TIME  
PE BA,V,S,TIME  
DISPLAY2  
P2 IV,V,S,TIME  
RE2BA,V,S,TIME  
RE1LD,V,S,TIME  
TINC=.25,TMAX=336.,PRATE=8,PRINT CONTROL=3,INT MODE=3,OUTRATE=8  
SIMULATE  
PARAMETER VALUES,BS UT=0.,NC LD=.005  
E1 BA=1000.,EDEBA=200.  
CC IV=1000.  
INITIAL CONDITIONS,PE BA=250.  
SIMULATE

## WIND ENERGY STORAGE COST SUMMARY

- 30 YEAR LIFE CYCLE

## YEARLY SYSTEM COSTS

CAPITAL COST (INCLUDING FIXED CHARGES)	86400. \$
FIXED O + M COST	2300. \$
OPERATING + FUEL COST	1753. \$
TOTAL	90453. \$

## ● ENERGY DELIVERED

ENERGY DELIVERED 4682165. KWH

\*\*\*\*\*  
 \* ENERGY COST PER KWH 19.3 MILLS \*  
 \*  
 \*\*\*\*\*

VALUE OF ENERGY DELIVERED 105440. \$  
 (VALUE OF FUEL SAVED)

ENERGY VALUE PER KWH 22.5 MILLS

COST PER VALUE DELIVERED .86

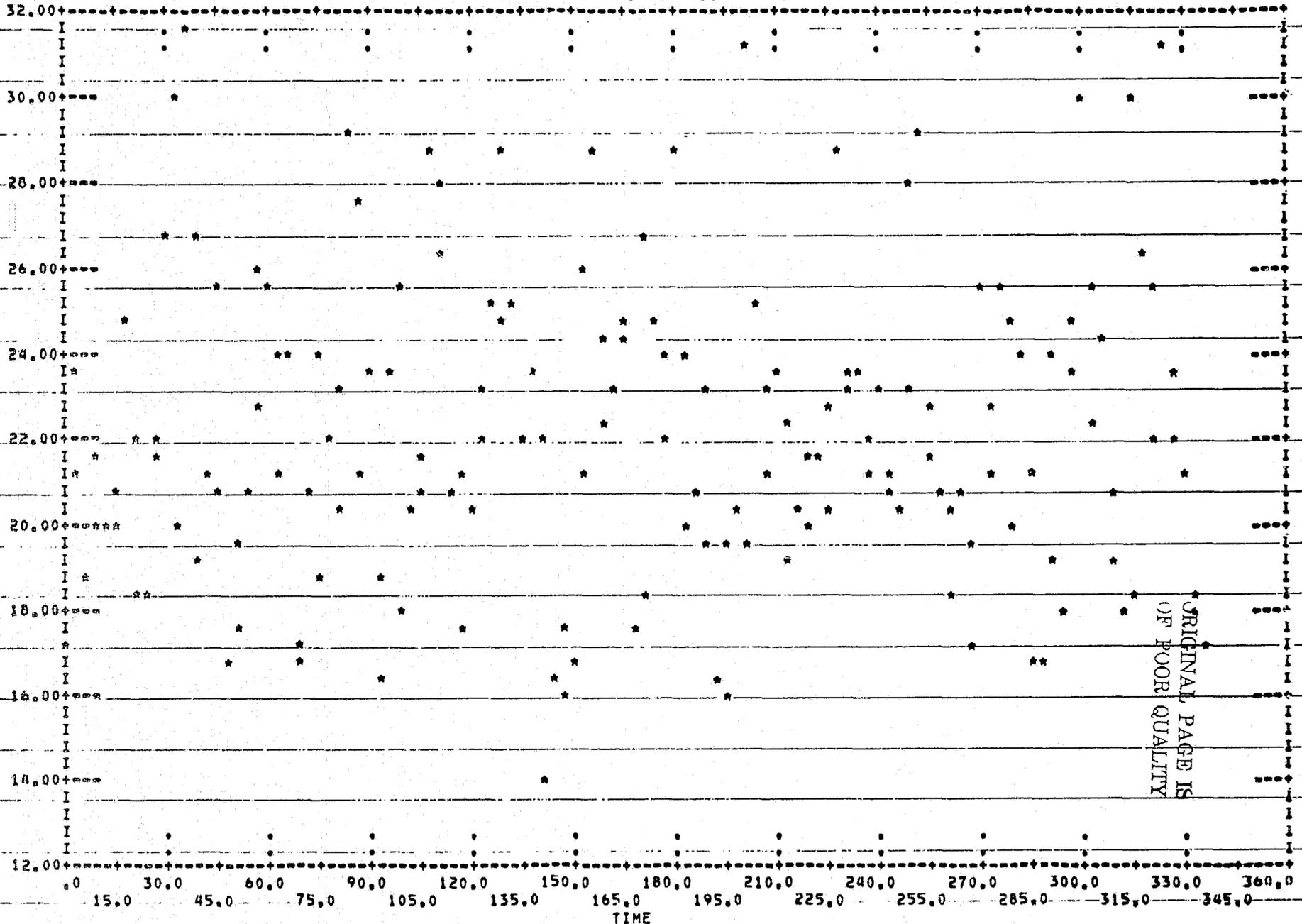
## ● LOAD FACTOR

PERCENT OF LOAD SUPPLIED 90.4  
BY TOTAL WIND SYSTEMPERCENT OF LOAD SUPPLIED 9.6  
BY UTILITYPERCENT OF WIND ENERGY 4.0  
SURPLUSEDCOST TO MEET LOAD 19.8 MILLS  
(WIND + UTILITY)ORIGINAL PAGE IS  
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BATTERY MODEL TEST

BCS 40180-2

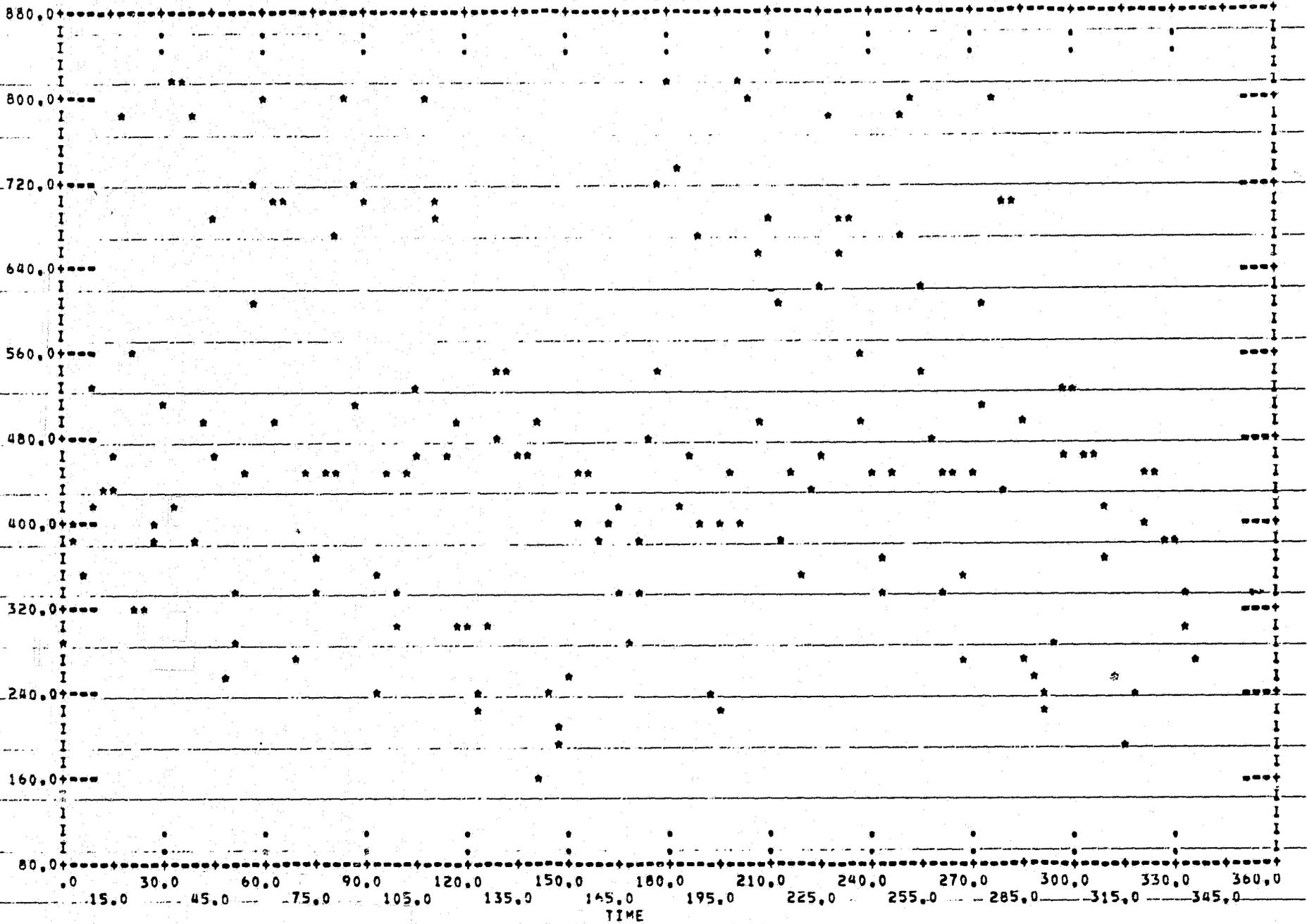
M  
V  
2  
M  
D



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FIGURE 8.2-6 WIND PROFILE FOR BATTERY SIMULATION

BATTERY MODEL TEST



SIMULATION DISPLAY 1 CASE NO. 1

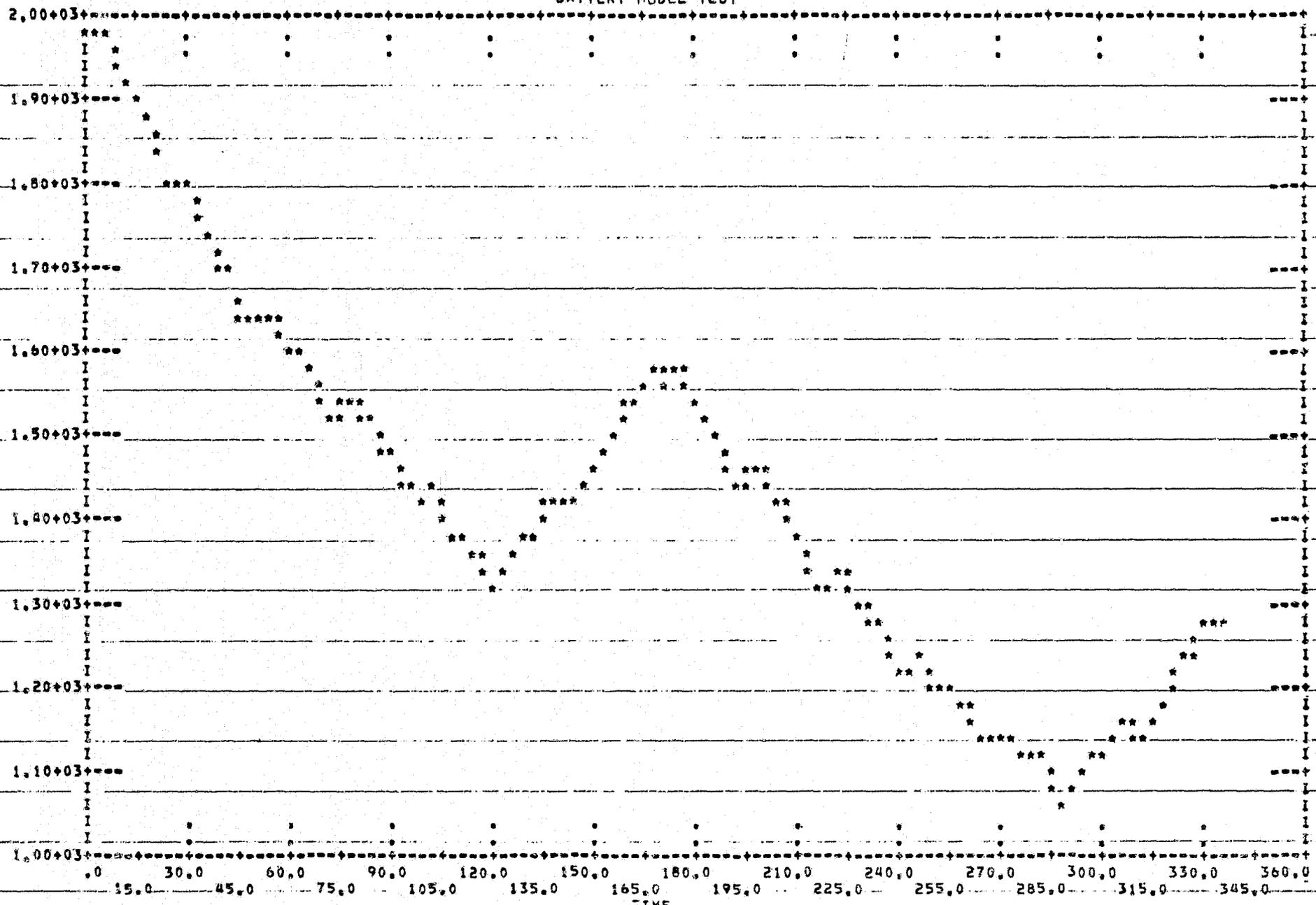
FIGURE 8.2-7 WIND POWER SUPPLIED TO LOAD

BMS 40180-2

BATTERY MODEL TEST

BDS 40180-2

P  
E  
S  
A



SIMULATION DISPLAY 1

CASE NO. 1

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FIGURE 8.2-8 BATTERY POTENTIAL ENERGY STORAGE

### 8.3 FLYWHEEL STORAGE MODEL

Figure 8.3-1 shows a simplified schematic of the flywheel storage model. This model is very similar to that of 8.2 except that flywheel storage replaces battery storage, and a power line loss is included in the model. The input data for this model is shown in Figure 8.3-2. Observe that the components are defined in the order of information flow shown in 8.3-1. The admittance component AD is used to model transmission line power losses. The model schematic is shown in Figure 8.3-3.

MODEL DESCRIPTION	FLYWHEEL TEST CASE	
LOCATION=74	TI	
LOCATION=61	WD	INPUTS=TI
LOCATION=21	WP	INPUTS=WD
LOCATION=42	MAB	INPUTS=WP(P,2=FIN),UT(P,1=C2)
LOCATION=33	PD	INPUTS=MAB(FO=P,0),MAB(FO=WP),PA(1,1),PIB(2,2) FL(RE=RE,2)
LOCATION=13	MO	INPUTS=PD(2,1)
LOCATION=4	TRI	INPUTS=MO(2,1),FL(RS=RS,2)
LOCATION=6	FL	INPUTS=TRI,PA(2,1)
LOCATION=8	TRO	INPUTS=FL,GE(RS=RS,2)
LOCATION=19	GE	INPUTS=TRO
LOCATION=45	PIB	INPUTS=FL
LOCATION=69	PA	INPUTS=GE(2,2),LO(RE,1=RE,0),PIB(4,2) UT(2,3)
LOCATION=78	AD	INPUTS=PA
LOCATION=76	LO	INPUTS=TI,AD
LOCATION=62	UT	INPUTS=PD(SP=P,0)
LOCATION=1	CM	
END OF MODEL		
LIST STANDARD COMPONENTS		
PRINT		

FIGURE 8.3-2 FLYWHEEL MODEL INPUT DATA

The simulation input data shown in Figure 8.3-4 uses the same wind and load data as Example 8.2. However, the storage component is rated at 400 kw with one hour storage, simulating a system used for temporary storage and discharge during peak power generation and load demand periods. It may be noted that the transmission power loss table is input for both TRI and TRO. Figures 8.3-5 to 8.3-7 show results from the simulation. Charging power to the

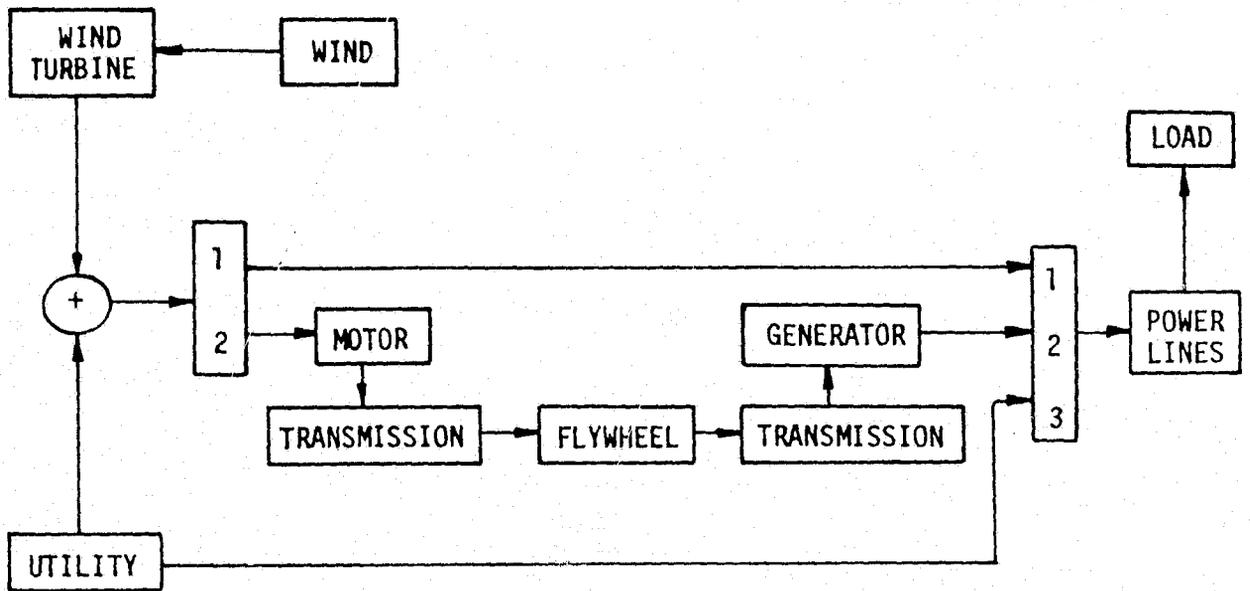
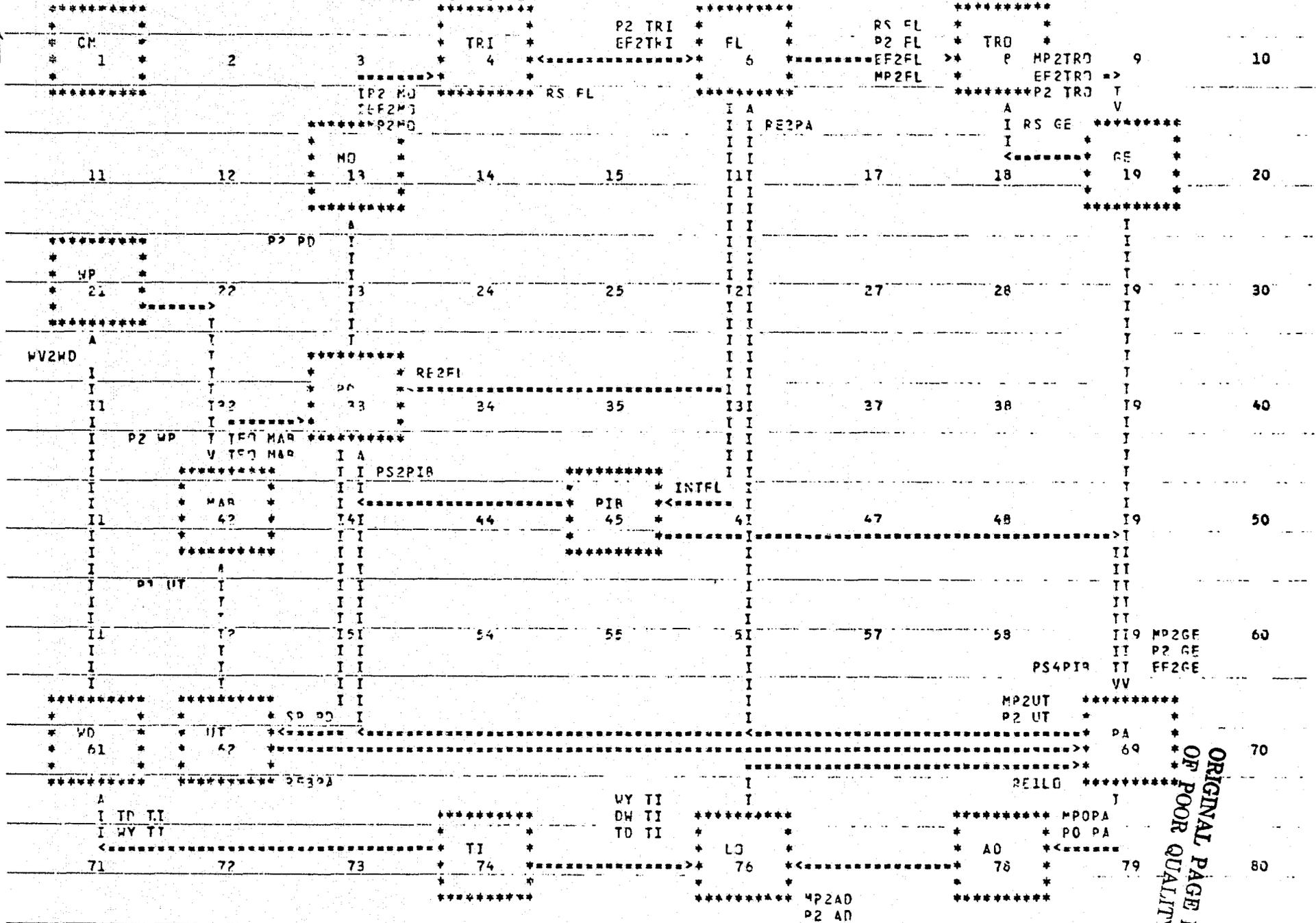


FIGURE 8.3-1: FLYWHEEL STORAGE EXAMPLE

FLYWHEEL TEST CASE



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FIGURE 8.3-3 FLYWHEEL MODEL SCHEMATIC

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flywheel in excess of that needed for the load is shown in Figure 8.3-5. Even with average load demand exceeding wind generation, the flywheel is charged at rated power fairly often. The kinetic energy stored by the flywheel over a two week period is shown in Figure 8.3-6. During the week energy is frequently withdrawn and storage is generally not much above the dead-band (80 kwh), whereas during the weekend the reverse is true. Output from the cost monitor is shown in Figure 8.3-7. The capital costs are probably low since nominal values were used for component costs. The utility supplied nearly 20% of the load in this case, since flywheel storage capacity is quite low.

```

TITLE= FLYWHEEL MODEL TEST
PARAMETER VALUES
VO AD=100,G1 AD=8,,G2 AD=8,,GM AD=8,,BM AD=200
SR GE=.008,C2 FL=3,E=8
PR FL=.02,MM FL=3372,RF FL=3.5,SR FL=.4,WT FL=24000,KF FL=1,3E=5
ZE FL=.1,RAPFL=400,ED FL=40,E1 FL=400,EDEFL=20,CM FL=800,CC FL=300
RS MD=1750,RAPMD=1000,MP1MD=1.E8,CC MD=500,CM MD=0.
RS1TRI=1750,CC TRI=500,CM TRI=0,CC TRO=500,CM TRO=0.
RARGE=1000,CC GE=1000,CM GE=100.
CR CM=15,,LE CM=30.
BS UT=20,,CB_UT=.016,CP_UT=.03,CC_UT=1000,,CM_UT=1000.
C1 MAB=1.
CYCLES=4.01,TO TI=0,V WP=400,WVOWP=8,WV1WP=60,DLINES=100.
CC WP=16000,CM WP=1200,PS1PIB=2.
EC WP=.2
NC LD=.005,CT LD=4,MN LD=0,STDLO=6,VE LO=.023
TABLE,PLOTRI=5,4
0.5,1,1.5,1.72
0.400,900,1100,1300
0.16,18,18.5,20
0.10,11,11.5,12
0.10,10,10.5,11
0.6,6.5,7,10
TABLE,PLOTRO=5,4
.5,1,1.5,1.72
0.400,900,1100,1300
0.16,18,18.5,20
0.10,11,11.5,12
0.10,10,10.5,11
0.6,6.5,7,10
TABLE,CLOFL=3,3
=1000, .0, 1000
2000,4000,7000
2.8, 7.4, 15
.9, 2.5, 5
2.6, 7.2, 15
TABLE,CL1FL=3
2000,4000,7000
.8, 2.4, 4
TABLE,PW WP=10
8,10,12,14,16,18,20,21.53,25,30
25.5,50,1,86.5,137.4,205.1,292.,400,6,500,782,8,800
TABLE,PY WD=13
0.,.4,33,8.67,13.,.17,33,21.67,26.,30,33,34.67,39.,43,33,47.67,52.
65,67,68,65,61,56,51,49,49,52,56,61,65
TABLE,PD WD=7
0,4,8,12,16,20,24
10,12,14,16,14,12,10
TABLE,DF WD=16
0,1,2,3,4,5,6,7,8,9,10,11,12,13,14,15
5,44,160,380,480,512,440,376,307,270,148,76,40,22,9,3
TABLE,PD LO=17
0,1,5,3,4,5,6,7,5,9,10,5,12
13.5,15,16.5,18,19.5,21,22.5,24
450,360,372,330,450,660,810,798,804
690,708,699,702,750,708,570,450
TABLE,PW LO=7
1,2,3,4,5,6,7
1,1,.9,.9,.9,.6,.5
TABLE,PY LO=6
0,10,20,30,40,52
226,194,180,174,194,226
INITIAL CONDITIONS, KE FL=300.
PRINTER PLOTS,DISPLAY1
WV2WD,VS,TIME
P1 PD,VS,TIME
P2 PD,VS,TIME
KE FL,VS,TIME
DISPLAY2
P2 GE,VS,TIME
RE2FL,VS,TIME
RE1LO,VS,TIME
TINC=.25,TMAX=336.,PRATE=8,PRINT CONTROL=3,INT MODE=3,OUTRATE=8
SIMULATE

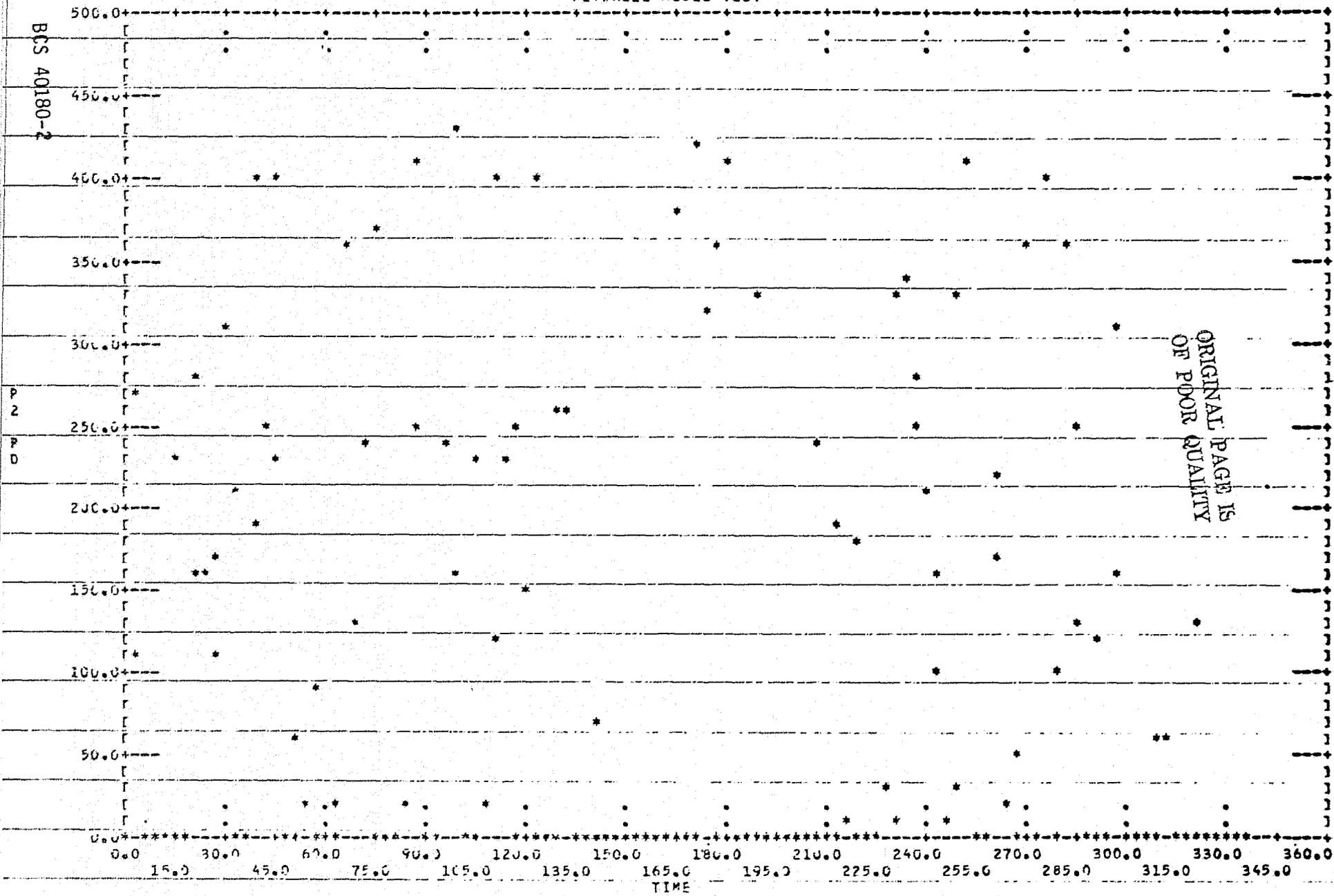
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FIGURE 0.3-4 FLYWHEEL SIMULATION DATA

FLYWHEEL MODEL TEST

BCS 40180-2



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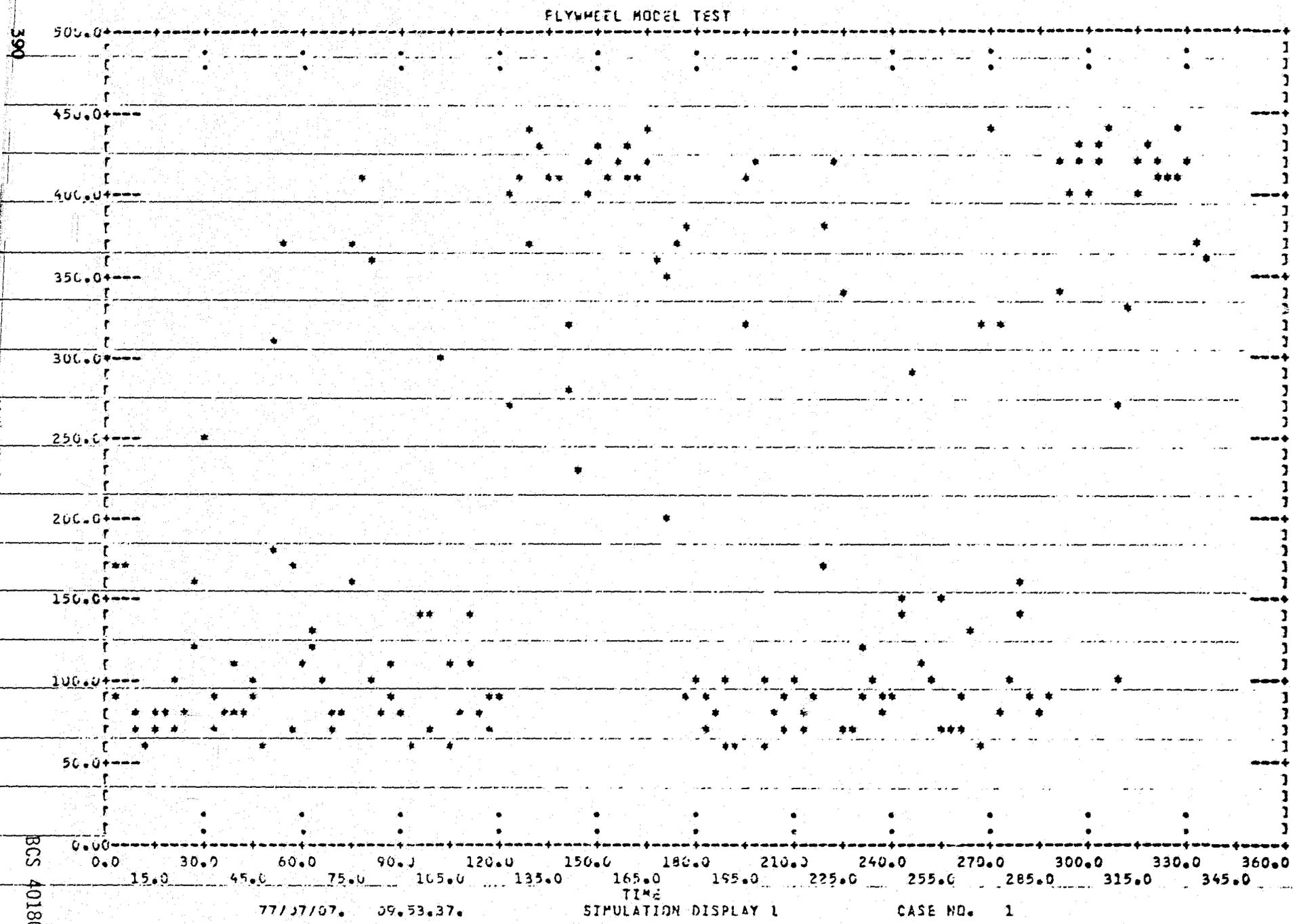
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SIMULATION DISPLAY 1

CASE NO. 1

FIGURE 8.3-5 WIND POWER SUPPLIED TO FLYWHEEL STORAGE

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BCS 40180-2

FIGURE 8.3-6 FLYWHEEL KINETIC ENERGY STORAGE

WIND ENERGY STORAGE COST SUMMARY

30 YEAR LIFE CYCLE

YEARLY SYSTEM COSTS

CAPITAL COST (INCLUDING FIXED CHARGES)	89104. \$
FIXED O + M COST	3100. \$
OPERATING + FUEL COST	1753. \$
TOTAL	93957. \$

ENERGY DELIVERED

ENERGY DELIVERED	4440974. KWH
------------------	--------------

*****	
* ENERGY COST PER KWH	21.2 MILLS *
*****	

VALUE OF ENERGY DELIVERED (VALUE OF FUEL SAVED)	95217. \$
--	-----------

ENERGY VALUE PER KWH	21.4 MILLS
----------------------	------------

COST PER VALUE DELIVERED	.99
--------------------------	-----

LOAD FACTOR

PERCENT OF LOAD SUPPLIED BY TOTAL WIND SYSTEM	61.3
--	------

PERCENT OF LOAD SUPPLIED BY UTILITY	18.7
--	------

PERCENT OF WIND ENERGY SUPPLUSED	8.3
-------------------------------------	-----

COST TO MEET LOAD (WIND + UTILITY)	22.3 MILLS
---------------------------------------	------------

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FIGURE 8.3-7 FLYWHEEL MODEL COST MONITOR OUTPUT

BCS 40180-2

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#### 8.4 HYDRO AND THERMAL STORAGE MODEL

Figure 8.4-1 shows the basic model schematic for a model with both thermal and electrical loads. Wind power is supplied first to meet the electrical load, with excess power going into hydro and thermal storage. The thermal load is driven by an ambient temperature component and electrical load energy value is supplied by a time dependent look-up table. Figure 8.4-2 shows the model input data. The components are ordered according to the flow of information in 8.4-1. Observe that the maximum power input of the power divider is connected up to the wind power output P. The model schematic is shown in Figure 8.4-3.

##### LIST STANDARD COMPONENTS

MODEL DESCRIPTION		HYDRO AND THERMAL TEST CASE
LOCATION=77	TI	
LOCATION=51	WD	INPUTS=TI
LOCATION=21	WP	INPUTS=WD
LOCATION=33	PD	INPUTS=WP, WP (P=MP), PA(1,1), PIH(2,2), HS(RE=RE, 2) INPUTS=TS(2,3), PIT(2,3)
LOCATION=13	MO	INPUTS=PD(2,1)
LOCATION=15	PU	INPUTS=MO
LOCATION=17	HS	INPUTS=PU, PA(RE, 2=RE)
LOCATION=45	PIH	INPUTS=HS
LOCATION=19	HT	INPUTS=HS
LOCATION=40	GE	INPUTS=HT
LOCATION=59	PA	INPUTS=GE(2,2), LO(1,0), PIH(4,2)
LOCATION=78	FU	INPUTS=TI (TD=FIN)
LOCATION=80	LO	INPUTS=TI, FU (FO=VE)
LOCATION=63	TS	INPUTS=TL
LOCATION=52	PIT	INPUTS=TS
LOCATION=67	TP	INPUTS=TI
LOCATION=65	TL	INPUTS=TI, TP
LOCATION= 1	CM	
END OF MODEL		
PRINT		

FIGURE 8.4-2 HYDRO AND THERMAL MODEL INPUT DATA

The input data for a two week simulation with this model is shown in Figure 8.4-4. CYCLES is equal to 6 in this model for sufficient iterations to attain steady state in the hydro storage subsystem. The hydro system has

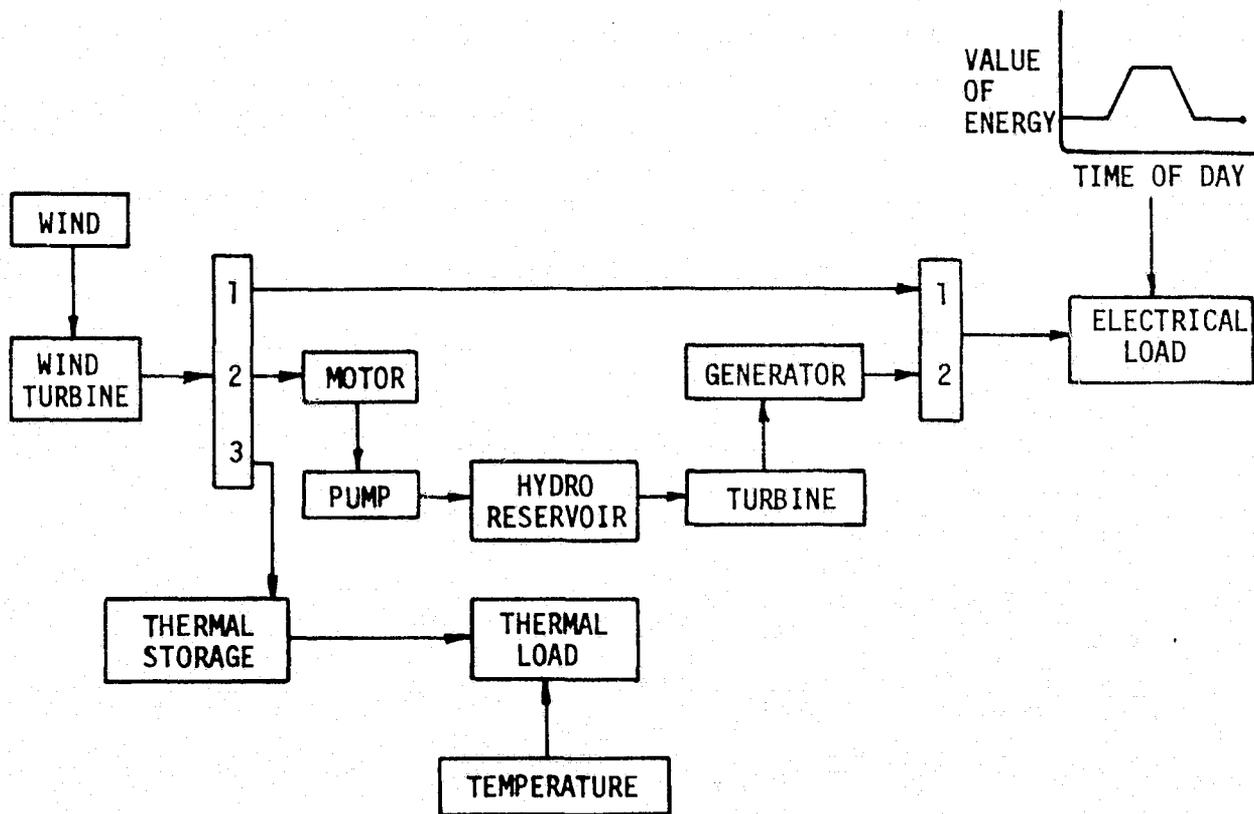


FIGURE 8.4-1: HYDRO AND THERMAL STORAGE EXAMPLE



```

PARAMETER VALUES
CYCLES=6.01,TD=TI=0,V WP=400,WVOWP=8,WV1JP=60,DLINES=100.
CC WP=15000,CM WP=1200,PS1PIH=2.,EC WP=.,2,CR CM=15,LE CM=30
41 PU=200,AS HS=3600,MDRHS=80,MO HS=80000,CM HS=1000
41 HS=200,4DEHS=400000,LE HS=30,F2 PD=.5,F3 PD=.5
RANGE=200,RSYGE=3600,SR GE=.0333,CC GE=1000,CM GE=120
VC LO=.004,CT LO=4,MN LO=0,STLO=6,AN FU=-1.
SLPIT=2.,FS TS=10,VQ TS=110,PD TS=100,LE TS=30,MF4TS=10000.
J4 TS=.01455,DETS=2,RS MO=1750,RAPMO=200,CC MO=500,CM MO=100
VE TL=.023,VC TL=40.,CT TP=12,MN TP=0,STTP=5.
TABLE,PW WP=10
3,10,12,14,16,18,20,21.53,25,30
25,6.50,1,85.5,137.4,205.1,292.,400.6,500,782.8,900
TABLE,PY WD=13
J.,4.33,8.57,13.,17.33,21.67,26.,30.33,34.67,39.,43.33,47.67,52.
55,67,69,55,51,55,51,49,49,52,55,61,65
TABLE,PD WJ=7
J.,1,8,12,16,20,24
10,12,14,16,18,12,10
TABLE,DF WJ=15
J,1,2,3,4,5,6,7,8,9,10,11,12,13,14,15
5,14,160,390,480,512,440,376,307,270,148,76,40,22,9,3
TABLE,4F TS=4
J,1879,.025131,.047371,.061072
30,147,147,204
TABLE,PD LJ=17
J,1.5,3,4.5,5,7.5,9,10.5,12
13.5,15,16.5,18,19.5,21,22.5,24
59,360,372,330,450,560,810,798,804
59,708,699,702,750,708,570,450
TABLE,PW LJ=7
1,2,3,4,5,6,7
1,1.,9.,9.,9.,6.,5
TABLE,PY LJ=6
J,10,20,30,40,52
225,134,180,174,194,226
TABLE, FTAFJ = 5
0,5,10,16,22,24
.019,.019,.029,.028,.019,.019
TABLE,TLDTL=4
J,52,60,100
4,2.,1.5,1.
TABLE,TWITL=4
0,5,18,24
.4,1.,1.,.4
TABLE,PD TP=9
J,5,6,9,12,15,18,21,24
45,45,48,55,52,54,56,48,46
TABLE,PY TP=5
0,13,25,39,52
40,50,75,65,40
INITIAL CONDITIONS, MA HS=1600000,E TS=600
PRINTER PLOTS DISPLAY1
JVPD,VS,TIME
P1 PD,VS,TIME
4--PU,VS,TIME
DISPLAY2
E HS,VS,TIME

42 HS,VS,TIME
42 HS,VS,TIME
DISPLAY3
PC LO,VS,TIME
PS PD,VS,TIME
E TS,VS,TIME
RELO,VS,TIME
DISPLAY4
LD TS,VS,TIME
PC TL,VS,TIME
TABLE TP,VS,TIME
FD FU,VS,TD TI
TINC=.50,TMAX=336.,PRATE=6,PRINT CONTROL=3,INT MODE=3,OUTRATE=4
TITLE = HYDRO AND THERMAL TEST
SIMULATE

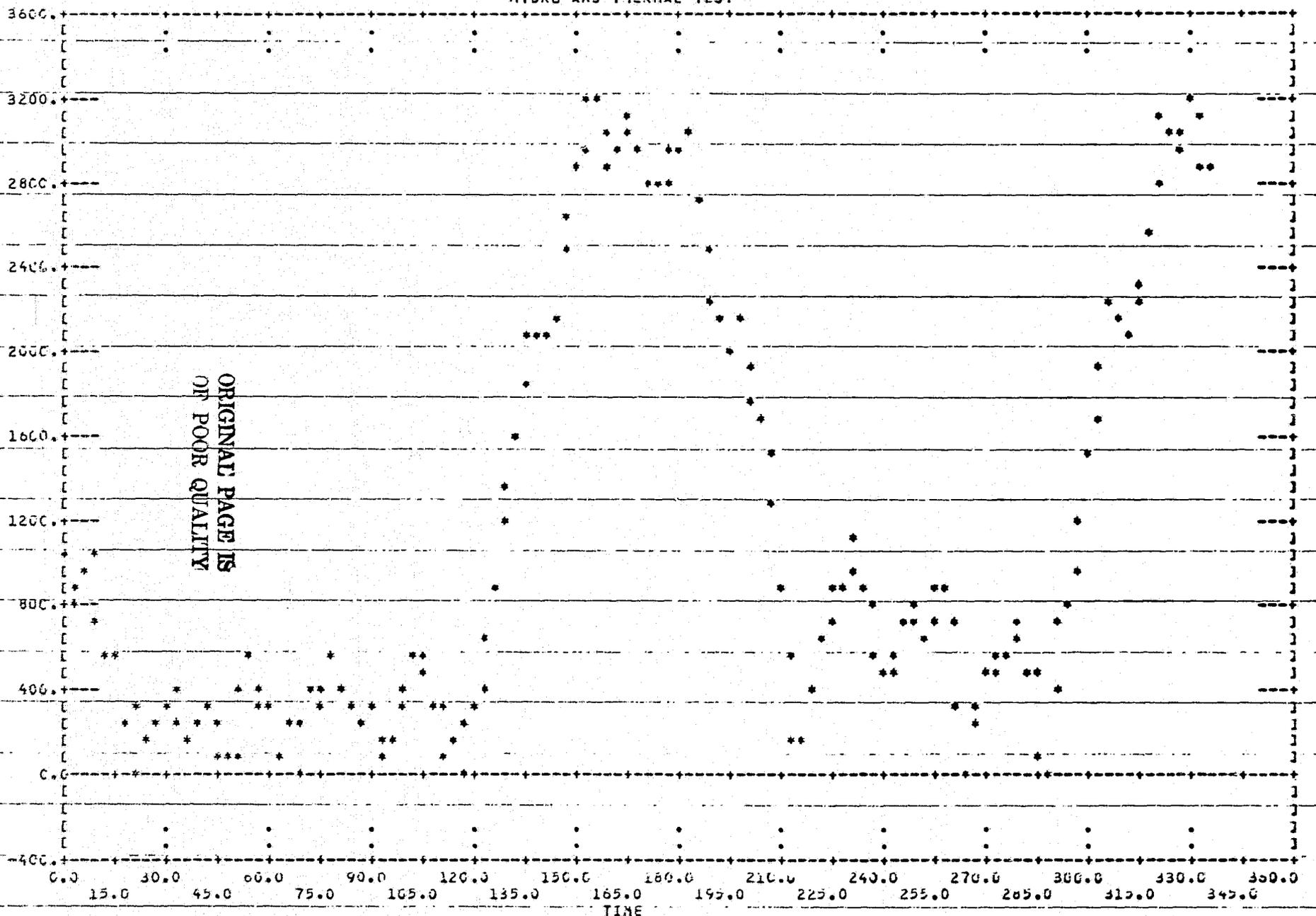
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FIGURE 8.4-4 HYDRO AND THERMAL SIMULATION DATA

much larger capacity and supplies a bigger load than the thermal system in this run. Figures 8.4-5 to 8.4-9 show results of the simulation. Hydro energy storage is shown in 8.4-5. During the week most of the wind energy goes directly to the load except at night. The reservoir builds up to capacity during the week-ends. The cumulative percent load delivered by wind and hydro storage is shown in 8.4-6, and averages about 91%. Similarly, thermal energy stored and percent thermal load delivered are shown in 8.4-7 and 8.4-8. The ambient temperature profile for a similar, one week simulation is shown in 8.4.9.

HYDRO AND THERMAL TEST



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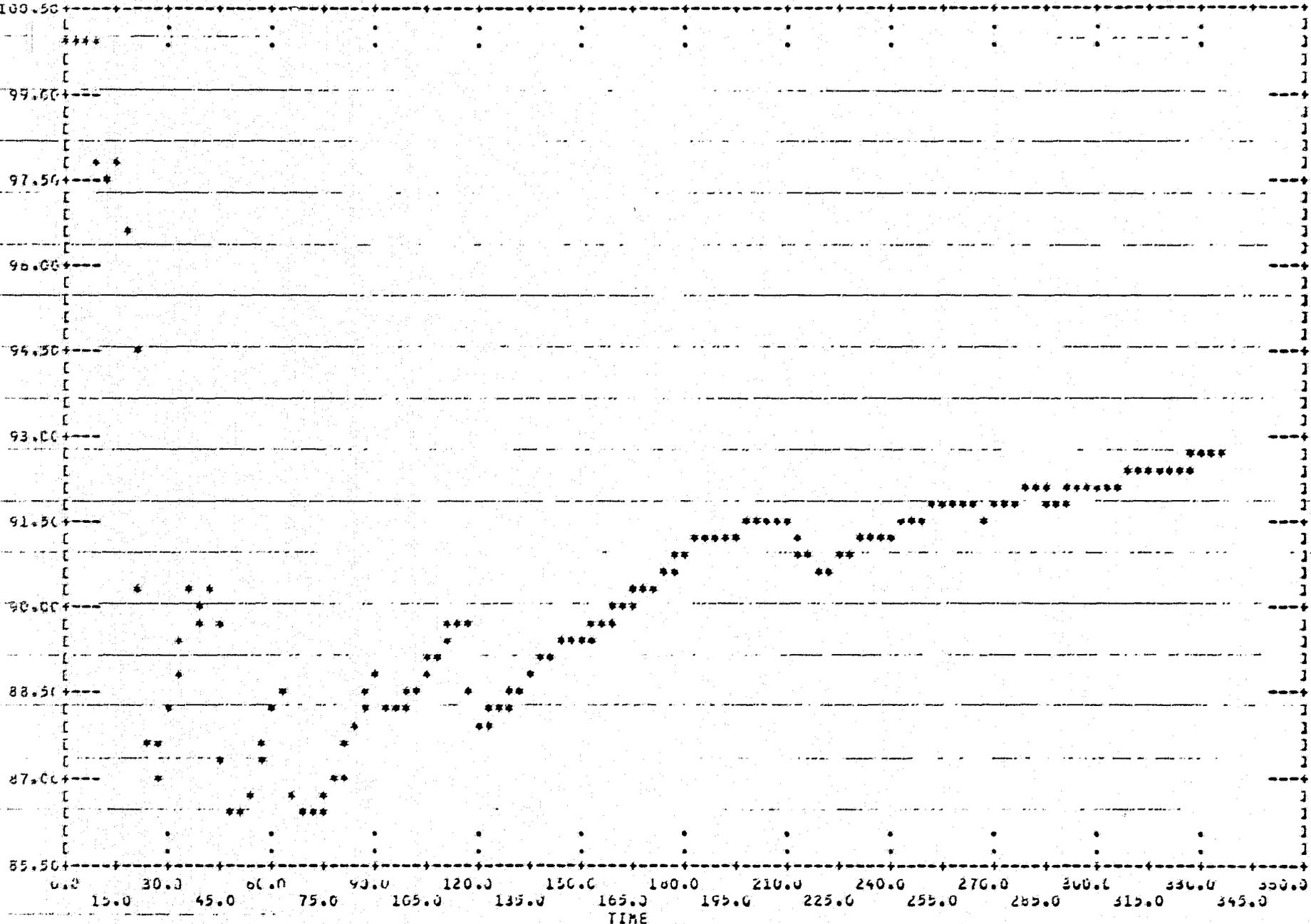
SIMULATION DISPLAY 2

CASE NO. 1

FIGURE 8.4-5 HYDRO RESERVOIR ENERGY STORAGE

HYDRO AND THERMAL TEST

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SIMULATION DISPLAY 3

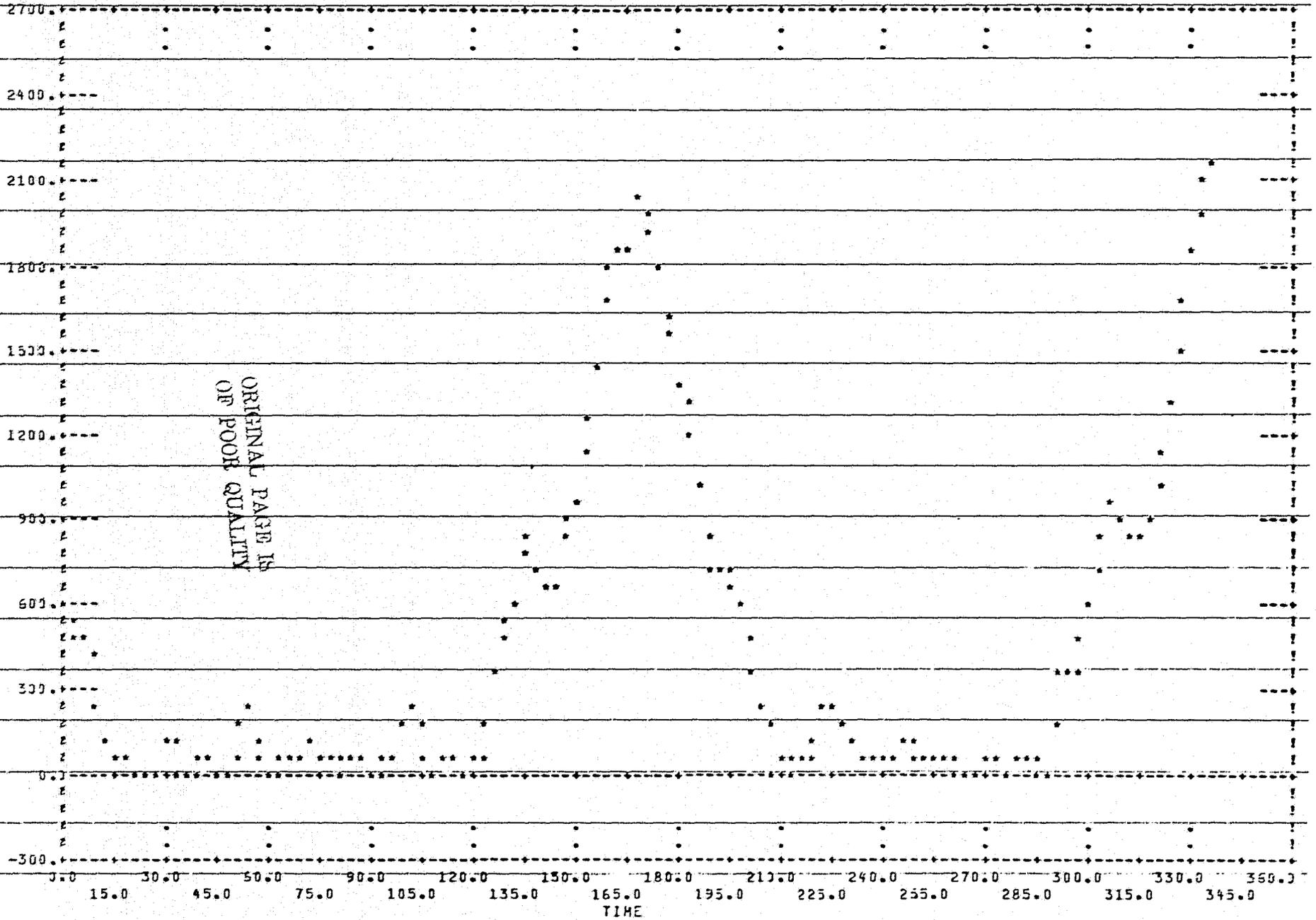
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FIGURE 8.4-6 PERCENT CUMULATIVE LOAD DELIVERED

HYDRO AND THERMAL TEST

BGS A0180-2



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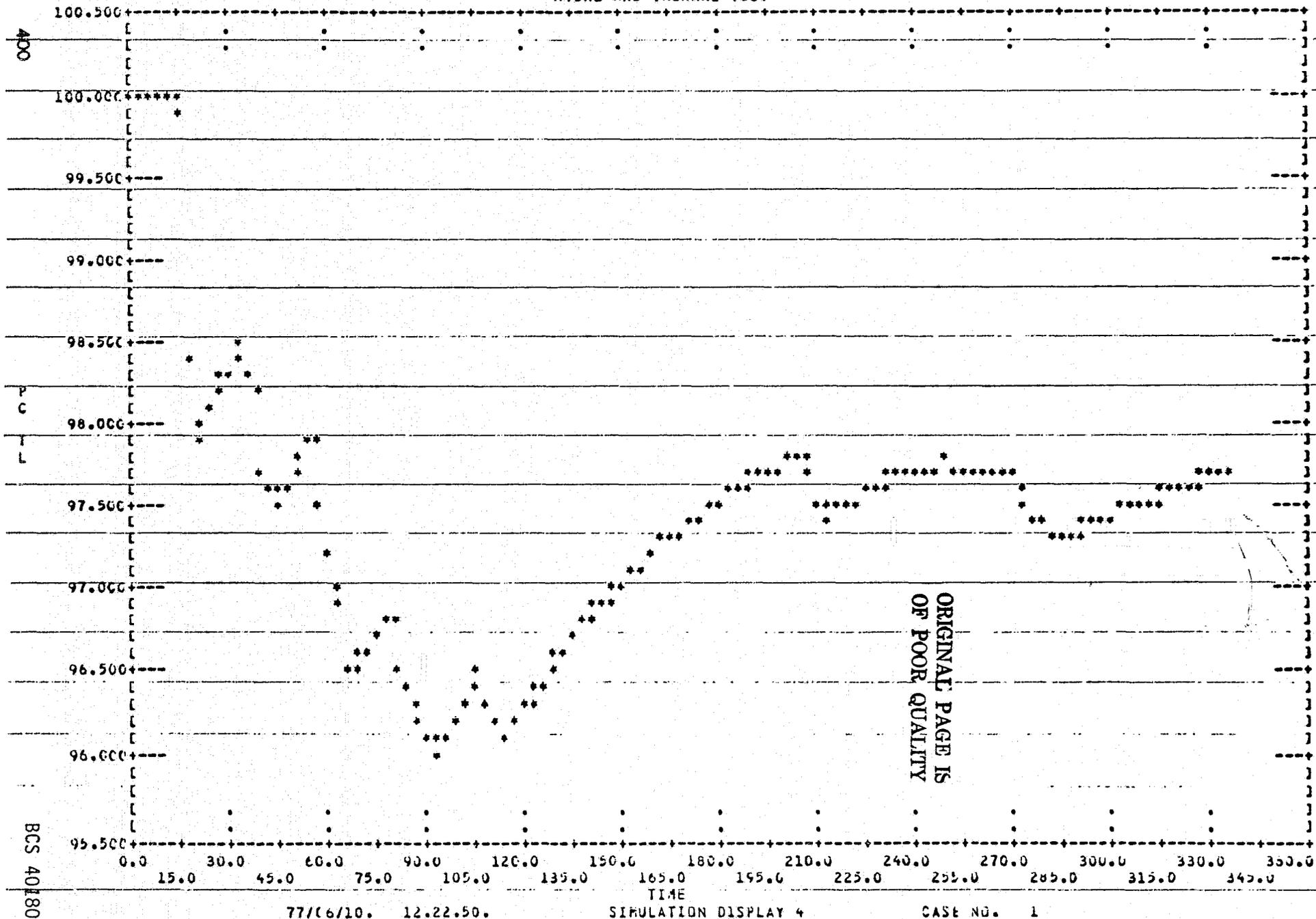
SIMULATION DISPLAY 3

CASE NO. 1

599

FIGURE 8.4-7 THERMAL ENERGY STORAGE

HYDRO AND THERMAL TEST



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SIMULATION DISPLAY 4

CASE NO. 1

FIGURE 8.4-8 PERCENT CUMULATIVE THERMAL LOAD DELIVERED

BCS 40180-2

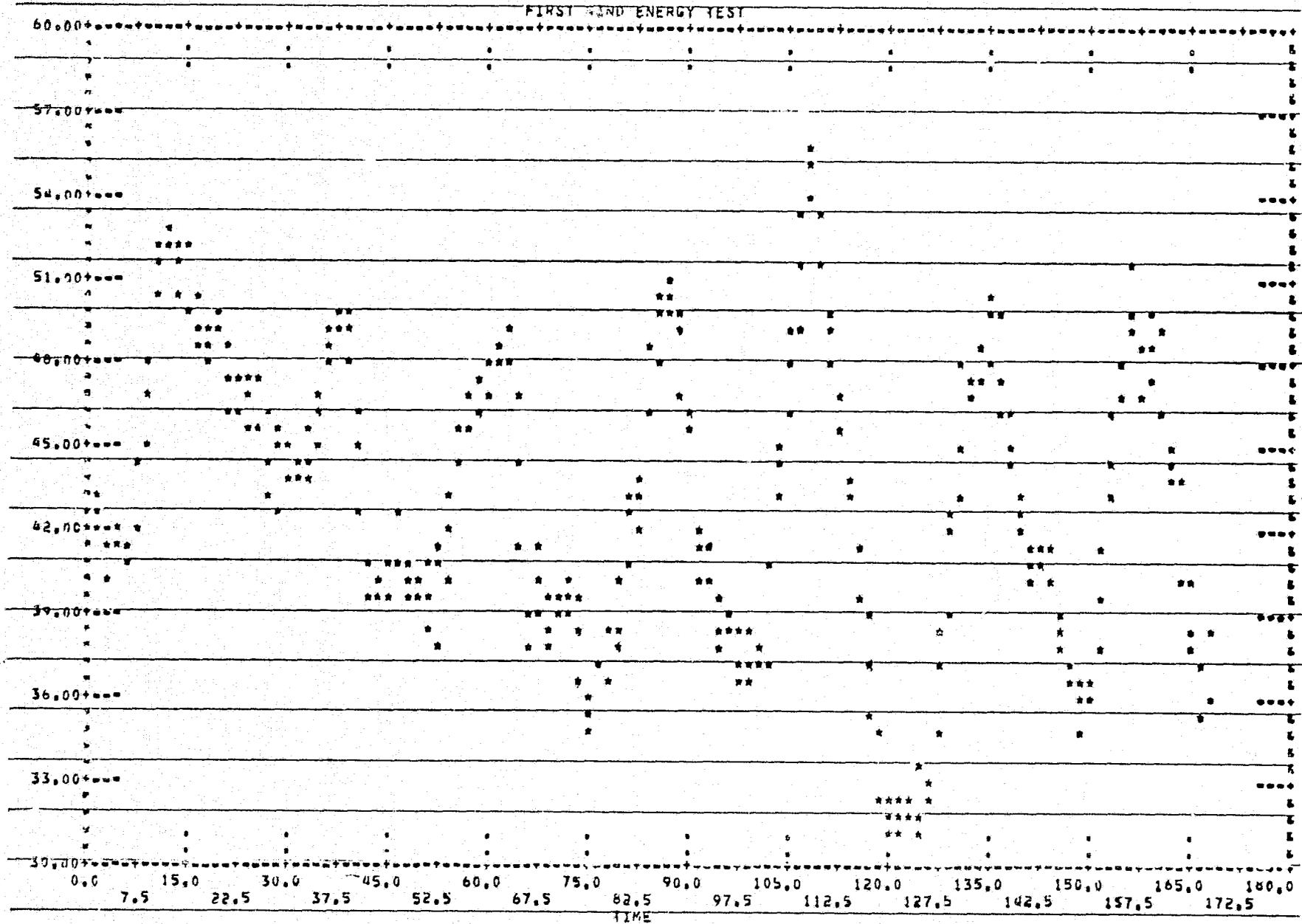


FIGURE 8.4-9 AMBIENT TEMPERATURE SIMULATION OVER ONE WEEK

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## 8.5 PNEUMATIC STORAGE MODEL

Figure 8.5-1 shows the simplified schematic for the pneumatic storage model. For simplicity the motor and generator have been omitted from the pneumatic storage subsystem. A burner is used if needed to heat the exiting air to the turbine. The heat exchanger has a phase change medium. Figure 8.5-2 shows the input data for this model.

MODEL DESCRIPTION		PNEUMATIC STORAGE TEST CASE
LOCATION= 1	TI	
LOCATION=21	WO	INPUTS=TI
LOCATION=51	WP	INPUTS=WO
LOCATION= 5	TP	INPUTS=TI
LOCATION=43	PD	INPUTS=WP, WP (P=MP), PA(1,1), PI(2,2), CS(RE=RE,2)
LOCATION=64	UT	INPUTS=PD(SP=P)
LOCATION=15	CO	INPUTS=PD(2,1), TP
LOCATION=17	HX	INPUTS=CO, TP, CS
LOCATION=47	CS	INPUTS=HX, PA(RE, 2=RE)
LOCATION=36	PI	INPUTS=CS
LOCATION=49	HY	INPUTS=CS, HX
LOCATION=59	BN	INPUTS=HY
LOCATION=80	TU	INPUTS=BN, TP, CS (PR=PS)
LOCATION=76	PA	INPUTS=TU(2,2), LO(1,0), PI(4,2), UT(2,3)
LOCATION=72	LO	INPUTS=TI
LOCATION=71	CM	
END OF MODEL		
LIST STANDARD COMPONENTS		
PRINT		

FIGURE 8.5-2 PNEUMATIC STORAGE MODEL INPUT DATA

The input data for a two week simulation is shown in 8.5-3. In order to keep the air entering the storage cavern from overheating, a fairly large leakage coefficient ( $NU = 0.01$ ) is assumed. Hence the storage cavern loses about 2/3 of its heat energy every four days. The load constant NC LO can be adjusted to balance wind energy to the load so that weekly air mass flow in and out of the cavern is balanced. The initial values for the CS and HX states were chosen on the basis of an earlier one week simulation. Figures 8.5-4 to 8.5-8 show results of this simulation. Figure 8.5-4 shows the average temperature of the heat exchanger storage medium for the 'cool' cell. The initial

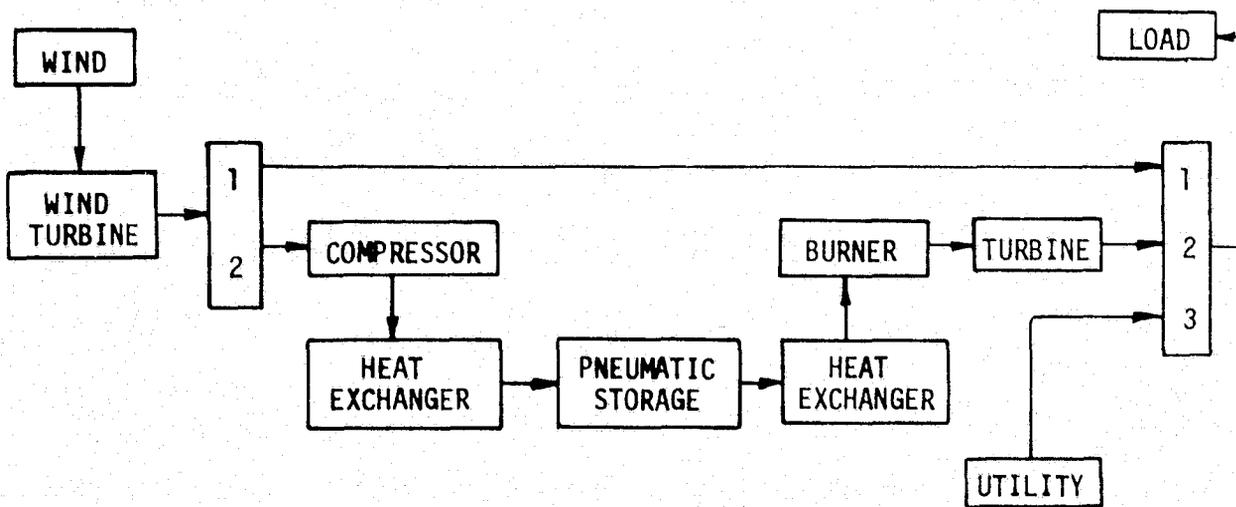


FIGURE 8.5-1: PNEUMATIC STORAGE EXAMPLE

TITLE= PNEUMATIC STORAGE TEST CASE2

PARAMETER VALUES

CYCLES=4.01, TO TIME=0, CT TP=12, MN TP=0, STDTP=5, DLINES=100  
V WP=400, WVOWP=8, WV1WP=60, CC WP=16000, CM WP=1200, PS1PI=2., EC WP=.2  
LE CS=30, MDECS=10000, TEMCS=350, NU CS=.010, TM CS=125, BE HX=.001  
MD CO=1500, T3 BN=600, LE BN=30, MDMBN=3000  
ST HX=24, LE HX=30, PD HX=150, TMTHX=250, TEMHX=350, L HX=8  
MD CS=1500, TIDTU=600, RS TU=3600, CR CM=15, LE CM=30, CM CS=400  
NC LO=.0043, CT LO=4, MN LO=0, STDLO=6, VE LO=.023  
CB UT=.019, MP1UT=1.58, CP UT=.023, CC UT=0, CM UT=0

TABLE, PW WP=10

0, 10, 12, 14, 16, 18, 20, 21, 23, 24, 30

25.6, 50.1, 86.5, 137.4, 205.1, 292., 400.6, 500., 880., 880.

TABLE, PY WD=13

0., 4.33, 8.67, 13., 17.33, 21.67, 26., 30.33, 34.67, 39., 43.33, 47.67, 52.  
65, 67, 68, 65, 61, 56, 51, 49, 49, 52, 56, 61, 65

TABLE, PD WD=7

0, 4, 8, 12, 16, 20, 24

10, 12, 14, 16, 14, 12, 10

TABLE, DF WD=16

0, 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13, 14, 15

5, 44, 160, 380, 480, 512, 440, 376, 307, 270, 148, 76, 40, 22, 9, 3

TABLE, PD TP=9

0, 3, 6, 9, 12, 15, 18, 21, 24

46, 45, 48, 55, 62, 62, 56, 48, 46

TABLE, PY TP=5

0, 13, 26, 39, 52

40, 50, 75, 65, 40

TABLE, PD LO=17

0, 1, 5, 3, 4, 5, 6, 7, 5, 9, 10, 5, 12

13, 5, 15, 16, 5, 18, 19, 5, 21, 22, 5, 24

450, 360, 372, 330, 450, 660, 810, 798, 804

690, 708, 699, 702, 750, 708, 570, 450

TABLE, PW LO=7

1, 2, 3, 4, 5, 6, 7

1, 1, .9, .9, .9, .6, .6

TABLE, PY LO=6

0, 10, 20, 30, 40, 52

226, 194, 180, 174, 194, 226

INITIAL CONDITIONS, E CS=1250, MS CS=5, E5, EC1HX=1300, EC2HX=800

PRINTER PLOTS, DISPLAY1

M CO, VS, TIME

T2 CO, VS, TIME

T2 HX, VS, TIME

TS1HX, VS, TIME

P2 UT, VS, TIME

DISPLAY2

E CS, VS, TIME

MS CS, VS, TIME

T2 CS, VS, TIME

M2 HY, VS, TIME

T HY, VS, TIME

DISPLAY3, P2 TU, VS, TIME, TS2HX, VS, TIME

TINC=.5, TMAX=336., PRATE=6, PRINT CONTROL=3, INT MODE=3, OUTFRATE=4

SIMULATE

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PNEUMATIC STORAGE TEST CASE2

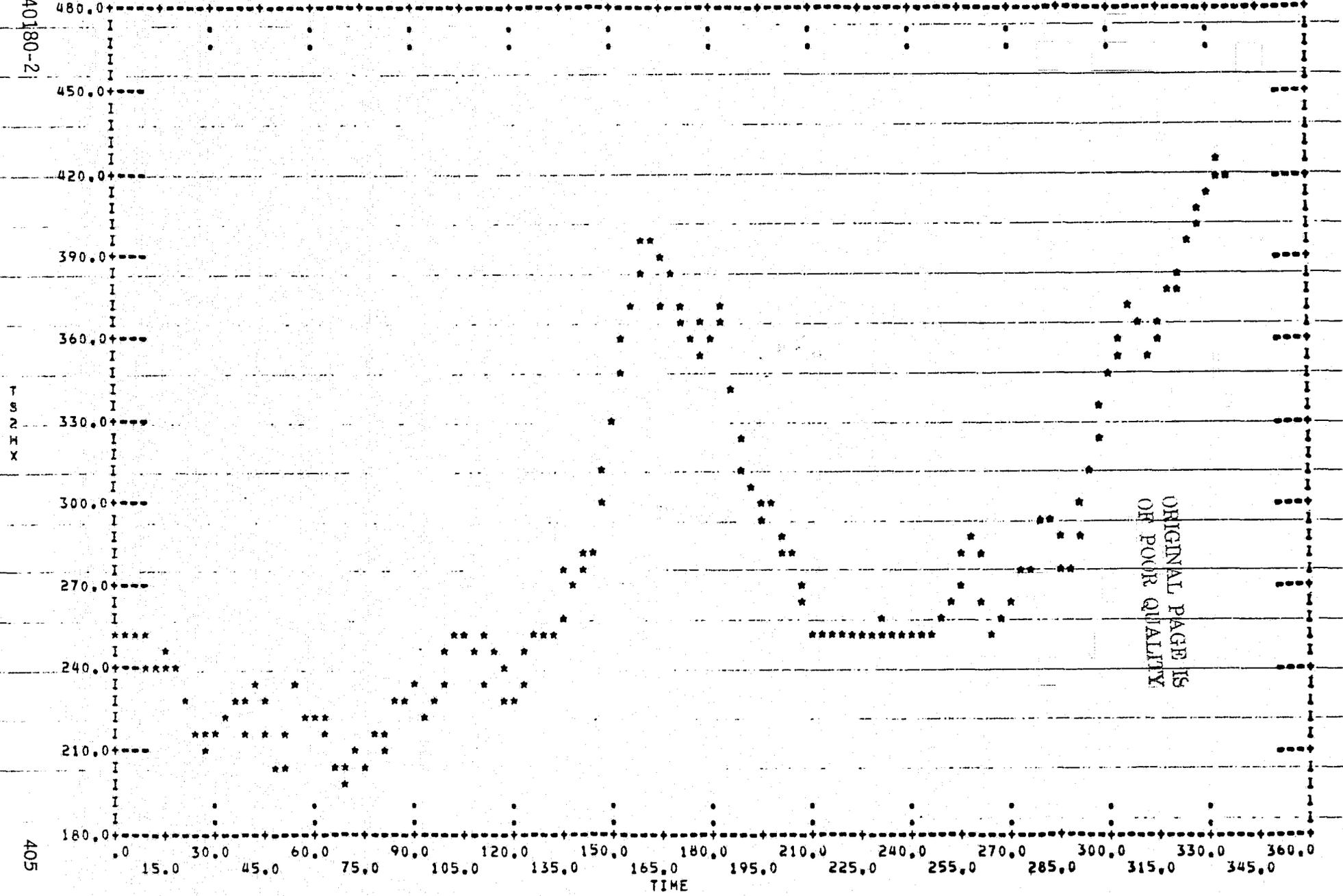


FIGURE 8.5-4 AVERAGE TEMPERATURE IN HEAT EXCHANGER CELL 2

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PNEUMATIC STORAGE TEST CASE2

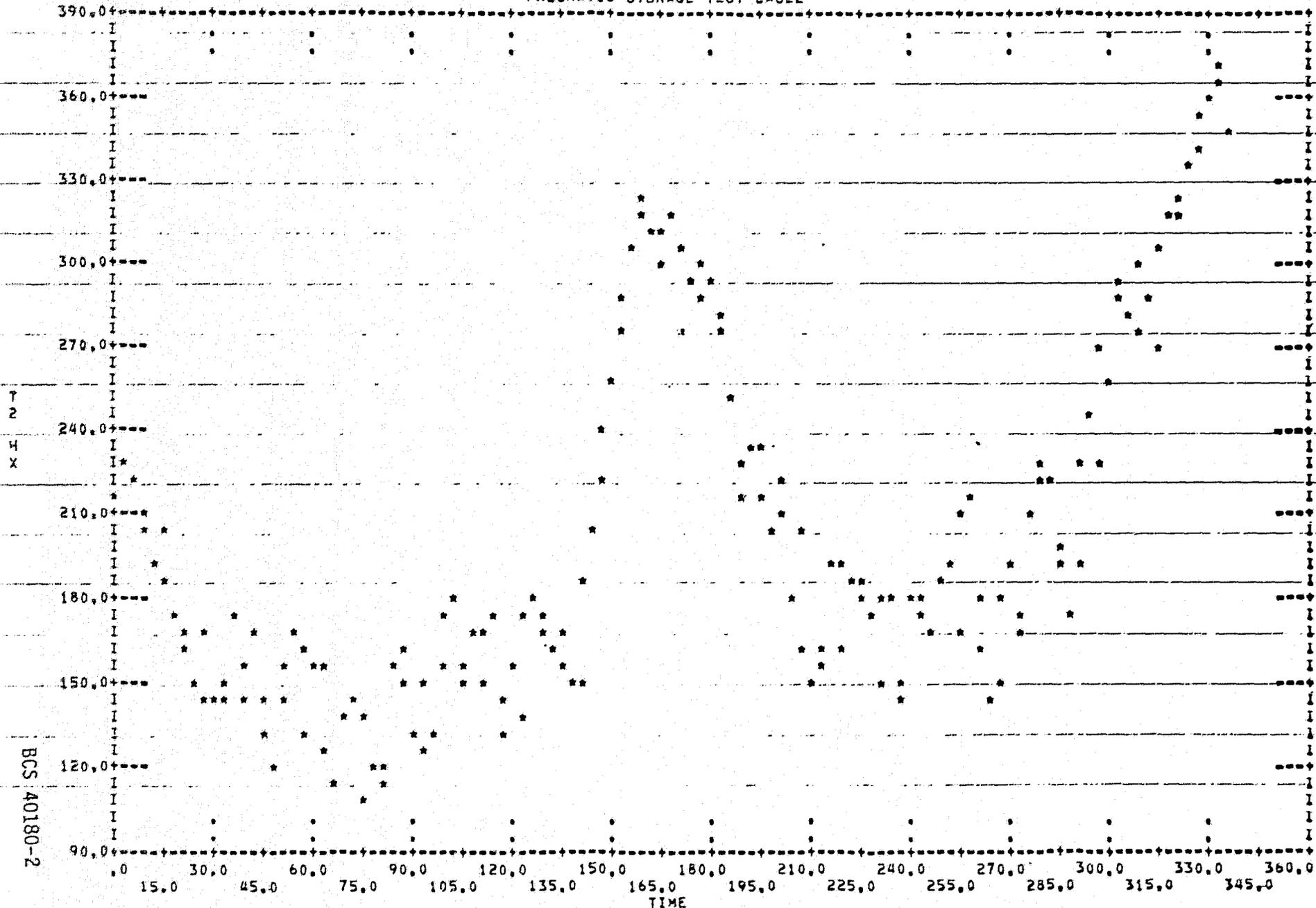
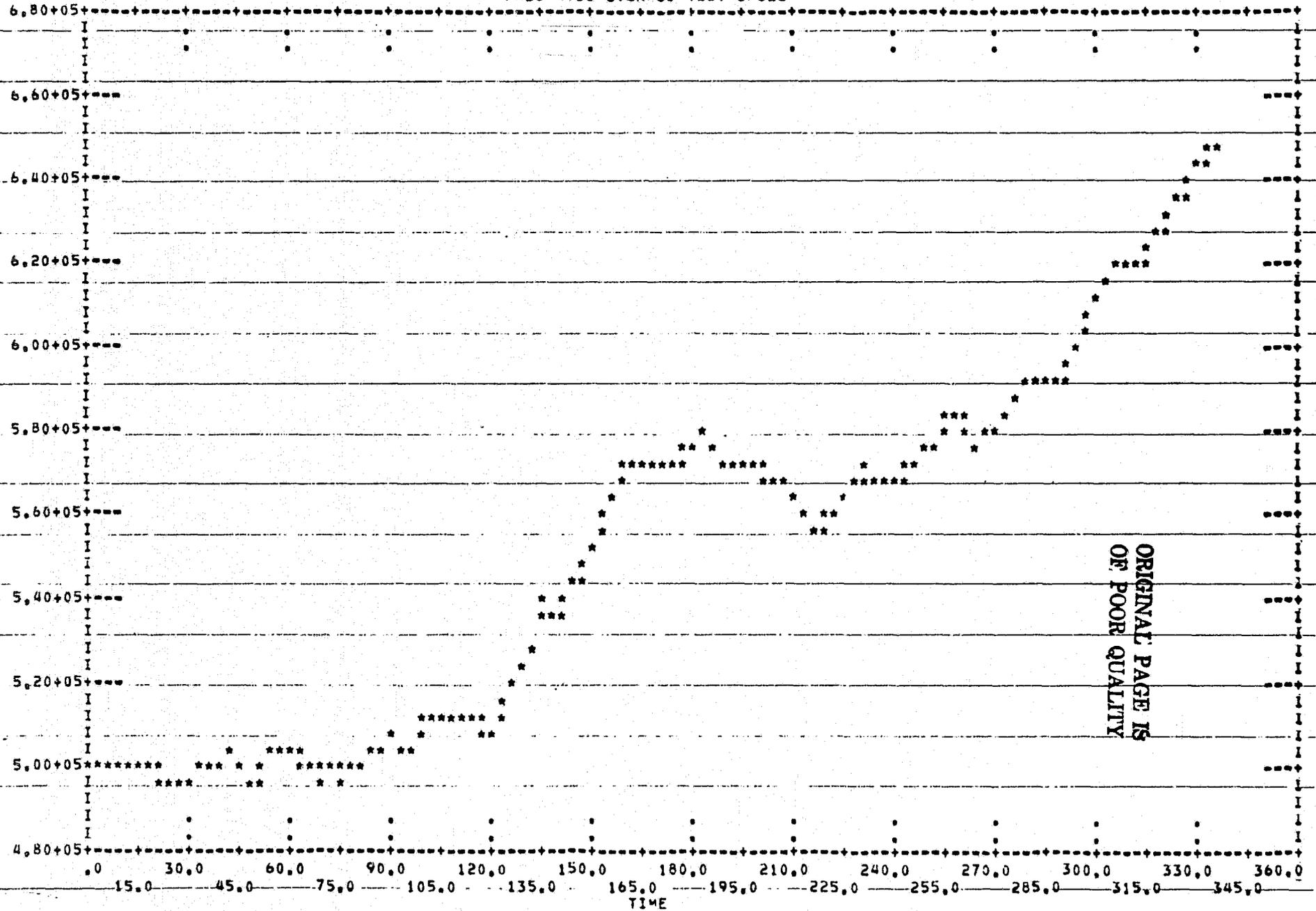


FIGURE 8.5-5 HEAT EXCHANGER OUTLET TEMPERATURE (CHARGING)

BCS 40180-2

PNEUMATIC STORAGE TEST CASE2

lbs

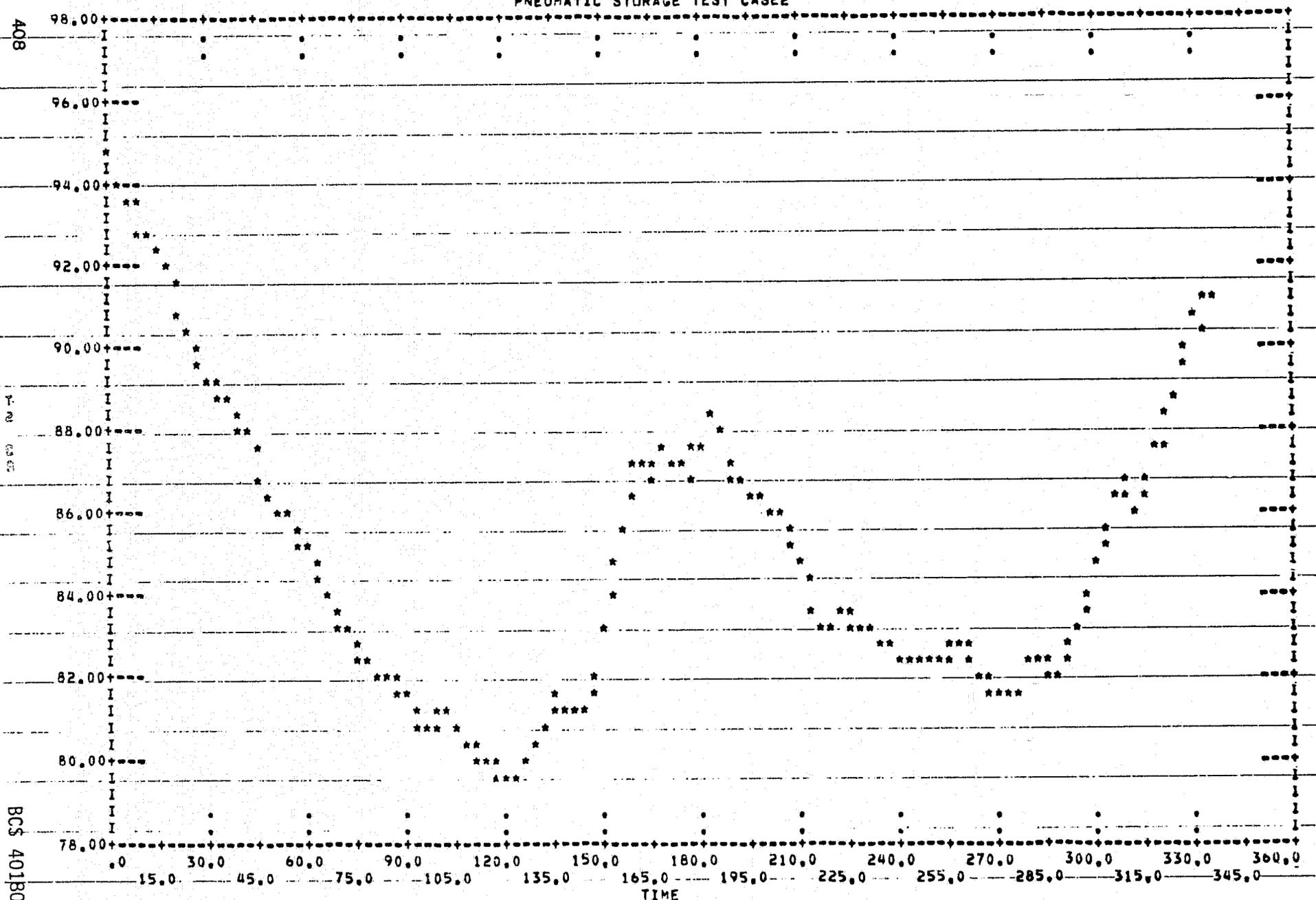


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FIGURE 8.5-6 AIR MASS IN PNEUMATIC STORAGE

PNEUMATIC STORAGE TEST CASE2



BCS 40180-2

FIGURE 8.5-7 AIR MASS TEMPERATURE IN PNEUMATIC STORAGE VESSEL

RCS 40180-2

PNEUMATIC STORAGE TEST CASE2

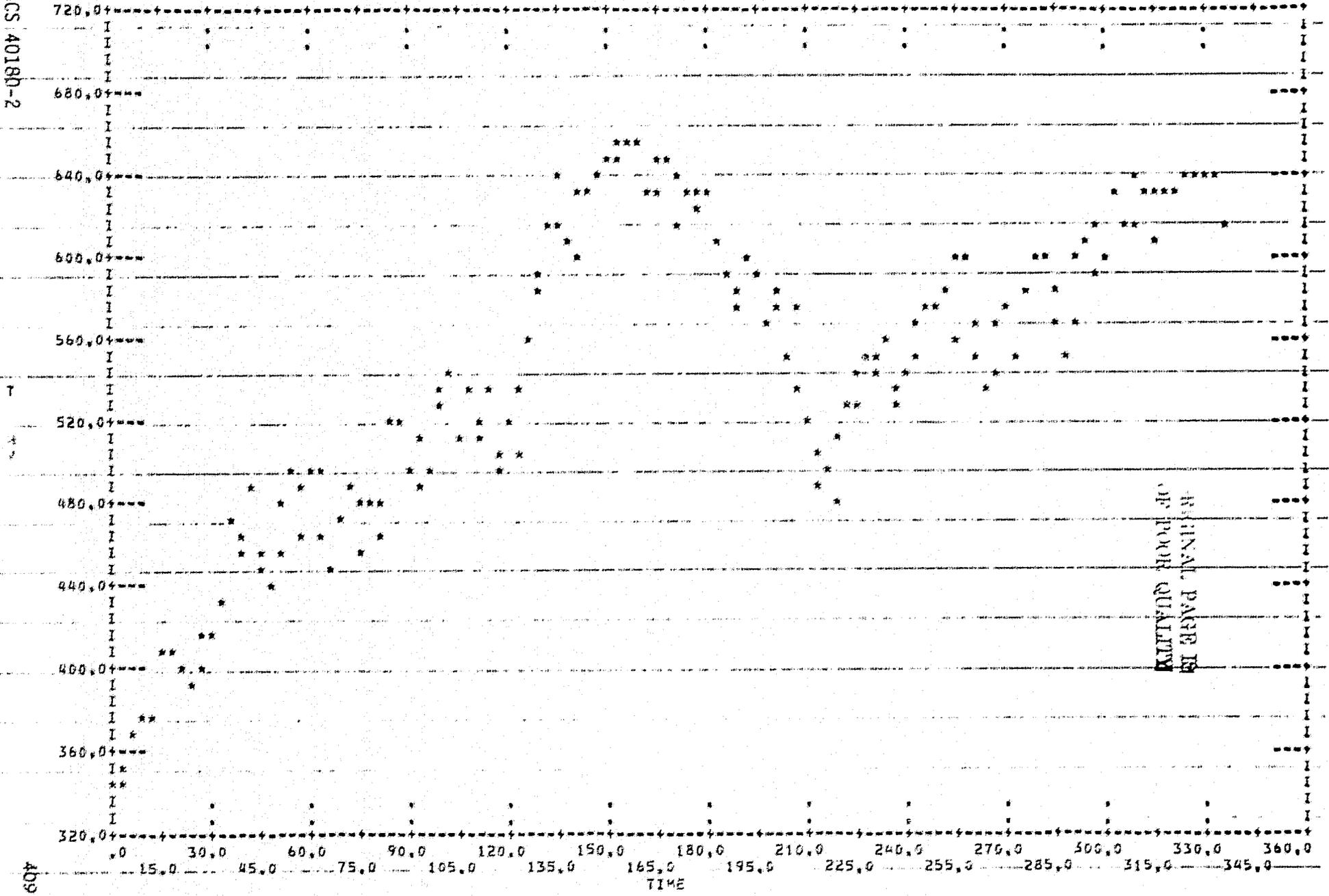


FIGURE 8.5-2 HEAT EXCHANGER OUTLET TEMPERATURE (DISCHARGING)

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temperature at the beginning of the week is a little too cool since the temperature rises to about  $400^{\circ}$  during the weekends. Phase change in this medium is indicated by the constant temperature intervals at  $250^{\circ}$ . Figure 8.5-5 shows the air temperature exiting from the heat exchanger into the cavern. During the week this temperature is generally held below  $200^{\circ}$  but may exceed  $350^{\circ}$  during the weekend. Figure 8.5-6 shows the air mass stored in the cavern. In this simulation wind power generated exceeded that of the load and thus there is a gradual buildup of air mass in the cavern. The temperature of the stored air mass is shown in Figure 8.5-7. There is about a  $10^{\circ}$  fluctuation in temperature each week in this case. The last figure, 8.5-8 shows the air temperature exiting from the heat exchanger to the burner. Neglecting the influence of the initial conditions, the average temperature is about  $550^{\circ}$  and thus a burner is probably not required for this system.

\*USGPO: 1978 - 757-139/6320 Region 5-11