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SILICON SOLAR CELL PROCESS  
DEVELOPMENT, FABRICATION AND ANALYSIS

FIRST QUARTERLY REPORT

FOR PERIOD COVERING

15 JUNE 1978 to 30 SEPTEMBER 1978

BY

H. I. YOO, P. A. ILES AND D. P. TANNER

JPL CONTRACT NO. 955089

OPTICAL COATING LABORATORY, INC.  
PHOTOELECTRONICS DIVISION  
15251 EAST DON JULIAN ROAD  
CITY OF INDUSTRY, CA 91746



"The JPL Low-Cost Silicon Solar Array Project is sponsored by the U. S. Department of Energy and forms part of the Solar Photovoltaic Conversion Program to initiate a major effort toward the development of low-cost solar arrays. This work was performed for the Jet Propulsion Laboratory, California Institute of Technology by agreement between NASA and DOE."

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## ABSTRACT

Solar cells were fabricated from unconventional silicon sheets, (Wacker "Silso" wafers and EFG ribbon, RF furnace grown), and the performances were characterized with an emphasis on statistical evaluation. A number of solar cell fabrication processes were used and conversion efficiency was measured under AMO condition at 25°C. "Silso" solar cells using standard processing showed an average efficiency of about 9.6%. Solar cells with back surface field (BSF) process showed about the same efficiency as the cells from standard process. Solar cells from grain boundary passivation process did not show any improvements in solar cell performance. These efficiency values are about 2% lower than those of the single crystalline control solar cells of about the same resistivity. A number of cells were fabricated using space technology (applying photolithographic techniques for the finer contact lines, multilayer AR coating and BSF), to see the limit of "Silso" sheets; these solar cells showed an average efficiency of 10.8%. Solar cells (2x2 cm) from corners and edges of the original "Silso" wafer (10x10 cm) showed considerably lower efficiency than those of the cells from the middle part, mainly due to the difference in grain size, and this result agrees well with the result of the minority carrier diffusion length and spectral response measurements.

EFG solar cells (area area about 506 cm<sup>2</sup>) were fabricated using standard and BSF processes. Average efficiency of the standard and BSF solar cells were around 7.8% and 8.5%, respectively, indicating about

\*All efficiencies quotes in this report refer to AMO conditions.



3% lower efficiency than those of the single crystalline control cells. This is about 1% lower efficiency than that of the "Silso" solar cells, due to lower curve fill factor and open circuit voltage, and was suspected to be due to shunting caused by silicon carbided particles from die material. Minority carrier diffusion length stayed about the same in both sheets, showing about 40-60  $\mu\text{m}$  range.

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## I. INTRODUCTION

The objective of this program is to investigate, develop and utilize technologies appropriate and necessary for improving the efficiency of solar cells made from various unconventional silicon sheets. During this quarterly reporting period; work has progressed in fabrication and characterization of solar cells from Wacker "Silso" wafers and EFG ribbons from Mobil Tyco. Silicon blanks (2x2 cm) were prepared from "Silso" wafers and fabricated using a standard process typical of those used currently in the silicon solar cell industry, a back surface field (BSF) process and other process modification attempting to achieve grain boundary passivation. About 1" x 1" solar cells were fabricated from EFG ribbons using standard and back surface field process.

Performance parameters, including open circuit voltage, short circuit current, curve fill factor, conversion efficiency, spectral response, dark I-V characteristics, and minority carrier diffusion length, were characterized and the results were compared to the properties of cells made from the conventional single crystalline silicon, and processed with the sheet samples. Statistical evaluation was emphasized; the results indicated that cell performance depends strongly on the grain size (for "Silso") and the foreign inclusions, such as SiC, etc. in the EFG ribbons.



## II. TECHNICAL DISCUSSION

### A. Wacker "Silso" Solar Cells

#### 1.0 Preparation and Description of Blanks

Wacker wafers were sliced into 2x2 cm silicon blanks using an O.D. diamond saw. The wafers and the location of the blanks in each wafer were identified with letters and numerals, respectively. Figure 1 shows how these blanks were prepared from a "Silso" wafer (in this case wafer A). Identification of each blank on a wafer is very important since the cell blanks have different grain size depending on the location of the blanks on the original wafers (10x10 cm). Edges of the wafer showed smaller grain size than the middle since nucleation starts at edges during solidification of molten silicon. Grains were mm size in the middle and were less than mm in area close to edges.

The blanks were chemically polished in planar etch (2:15:5 = HF:HNO<sub>3</sub>:CH<sub>3</sub>COOH) for about 10 minutes, which removed about 1.5 mils of silicon from each face of the blanks. Four point probe measurement indicated that resistivities were in the range of 5-11 ohm-cm with p-type conductivity (four point probe measurement of polycrystalline material might introduce error in bulk resistivity reading due to the potential drop at the grain boundaries).

Surface photovoltage measurement for these "Silso" blanks indicated minority carrier diffusion lengths in the range of

40 to 80  $\mu\text{m}$  (measurement used a light beam size of around 3-4 mm in diameter). Single crystalline control blanks were prepared in the same way with the measured resistivity range 1-3 ohm-cm and minority carrier diffusion length between 100-200  $\mu\text{m}$ .

|      |      |      |      |  |
|------|------|------|------|--|
| A-1  | A-2  | A-3  | A-4  |  |
| A-5  | A-6  | A-7  | A-8  |  |
| A-9  | A-10 | A-11 | A-12 |  |
| A-13 | A-14 | A-15 | A-16 |  |
|      |      |      |      |  |

↓  
2-4 mm Edge Trim  
↑

#### Classification of Blanks

Corner: A-1

Edge: A-2, A-3, A-4, A-5, A-9,  
and A-13

Middle: A-6, A-7, A-8, A-10,  
A-11, A-12, A-14, A-15,  
and A-16

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FIGURE 1

Preparation and Classification of Silicon Blanks  
(2x2 cm) From a Wacker "Silso" Wafer (A Wafer, 10x10 cm)

## 2.0 Fabrication of Solar Cells

Cells were made from the prepared blanks, along with control cells using Czochralski silicon. The rationale for the control cells is given in the following section.

### 2.1 Control Cell Rationale

For evaluation of a wide range of silicon, use is made of control cells, made from silicon previously shown to yield good cells. Even with a well established sequence of processes, the use of these control cells can serve as a useful check that the processing has been satisfactorily completed. These control slices (along with the test samples) are previously scribed with an individual code, and can be identified when the cells is completed.

If the silicon under evaluation does not lead to any chance of contamination of furnace tubes etc., a set of control slices added at the slice preparation stage and processed along with the group to be evaluated can show that the processing has proceeded to plan (the control cell properties are known from earlier tests) and it can be verified that in the run under study, that this baseline performance has been obtained. The use of control cells effectively provides a evaluation of the integrated effect of all the process steps on the cell performance.

Should any deviation have occurred in the process steps it is convenient to determine the step(s) leading to deviation by analysis of the differences in the control cell performance.

If any cross-influence is suspected from the test silicon (e.g. contamination from high concentration of impurities), then the control cell performance can indicate this contamination. Usually such contamination is most likely to occur during the high temperature processes (especially diffusion and annealing) and in this case, use of a second group of control slices can bracket the step at which contamination occurred. This second group of control slices is formed from a similar well-behaved ingot, and is additionally diffused in a separate furnace. Should this group of cells perform well, whereas the original group showed poorer performance this indicates that the test silicon is indeed a source of contamination.

To check if the furnace itself has been contaminated, use of another group of undiffused control slices can be processed alone, to see if the output is decreased on exposure to the suspect tube.

Clearly if some of the later steps are suspected to be the cause of reduced output, additional groups of control slices, processed in acceptable equipment

up to the suspect steps, can serve to indicate degradation caused by the suspect step. [In many cases, the primary control group can serve this function.]

In addition to indication of suspect step(s), the control cells also provide quantitative estimates of the amount of degradation. Analysis of the photovoltaic parameters can show the extent of degradation in the key cell properties, e.g. decreased  $V_{oc}$  can show possible shunting or other PN junction deterioration, decreased  $I_{sc}$  can show reduced diffusion length in the silicon, or perhaps problems in the diffusion conditions or the AR coating.

The use of control cells provides a direct check of the effects of the process steps, with the information provided directly in the solar cell performance characteristics. This is often preferable to attempts to use related parameters which must still be assessed for their actual effect on cell properties. The control cells provide a constant baseline to evaluate the silicon under test, allowing direct comparison in solar cell efficiency rather than inferred comparison using cell-related physical factors.

For forms of silicon where inhomogeneity is expected (polycrystalline or ribbon silicon) the control cells can also be useful; if measurements are made of

localized small areas, comparison of the spread across the control slices and the test slices again provides a baseline indication of the degree of inhomogeneity.

In the ideal case (most usual), the control cells provide cell output as expected, and this adds confidence to any direct comparisons made on the silicon under test. In a few cases, very small deviations in control cell performance after analysis have revealed similar small deviations in the processing of the test silicon, and again necessary small adjustments were made to the process sequence (and confirmed for their effectiveness) using more control slices.

In the present work, a stock of previously acceptable silicon has been identified and retained for use as control material for the different batches of test silicon. Part of the stock has been pre-diffused for insertion with the test group and the first control group, immediately after these groups have been diffused. These are called second control group and identified in electrical data sheets of control cells in Appendices III and IV.

## 2.2 Standard Process

The first group of test samples is subjected to a "standard process", (which will be described in this section) to allow uniform evaluation of all the different sheet forms.

After applying a diffusion mask on the back surface, the silicon blanks, both Wacker (63 pieces) and the controls (10 pieces) were loaded in a furnace, with 12" temperature zone at  $875^{\circ}\pm 1^{\circ}\text{C}$  and oxidation was carried out in dry oxygen atmosphere for five minutes. Following the oxidation step, (in the same furnace) slices were diffused for 20 minutes by passing  $\text{POCl}_3$ -saturated oxygen gas and dry nitrogen gas (carrier gas) over the blanks. Finally the boat loaded with these diffused blanks was slowly pulled out of the furnace (within 10 minutes manually). After removing the glassy-layers formed during the diffusion process, sheet resistance was measured from selected samples; values of 30-60 ohm/square for Wacker silicon and 22-25 ohm/square for single crystalline controls were measured.

Front and back contacts were applied by successive evaporation of Ti, Pd and Ag in a vacuum chamber (pressure around  $10^{-6}$  Torr) using resistively heated coils as sources. Front contacts were applied by evaporation of metals through a metal shadow mask which had grid finger density of four lines per centimeter. About 90% active area of the solar cells was obtained after evaporation. The thickness of the evaporated front metals was  $1000\text{\AA}$  for Ti,  $250\text{\AA}$  for Pd and  $4-6\text{ }\mu\text{m}$  for Ag, while the thickness of Ag in the back contact was around  $2-3\text{ }\mu\text{m}$ . To



minimize peeling of metal contacts during preliminary measurement of solar cell parameters (measurement without anti-reflective coating) a post metallization heat treatment was carried out at 400°C for 10 minutes in hydrogen atmosphere.

An anti-reflective coating was applied on the finished solar cells by evaporation of silicon monoxide in a vacuum chamber pressure maintained at around  $10^{-6}$  Torr. The thickness of the evaporated  $\text{SiO}_x$  layer was around 750Å with stoichiometric factor  $x$  close to one. Finally the solar cells with anti-reflective coating were sintered again at 500°C for five minutes in hydrogen atmosphere. A block diagram of this process is given in Figure 2.

Final mechanical yield of the finished cells was around 94%. Table 1 shows the number and cause of the broken cells during process; the number of initial starting blanks was 64.

The control cells from this initial standard process showed lower open circuit voltage and higher series resistance than expected. This was suspected to be due to high contact resistance at the back metal-silicon interface. Thus, back contacts were applied first (before front contacts) and sintered in  $\text{H}_2$  atmosphere for 10-15 minutes at 600°C. Then front contacts were

FIGURE 2

SOLAR CELL STANDARD PROCESS

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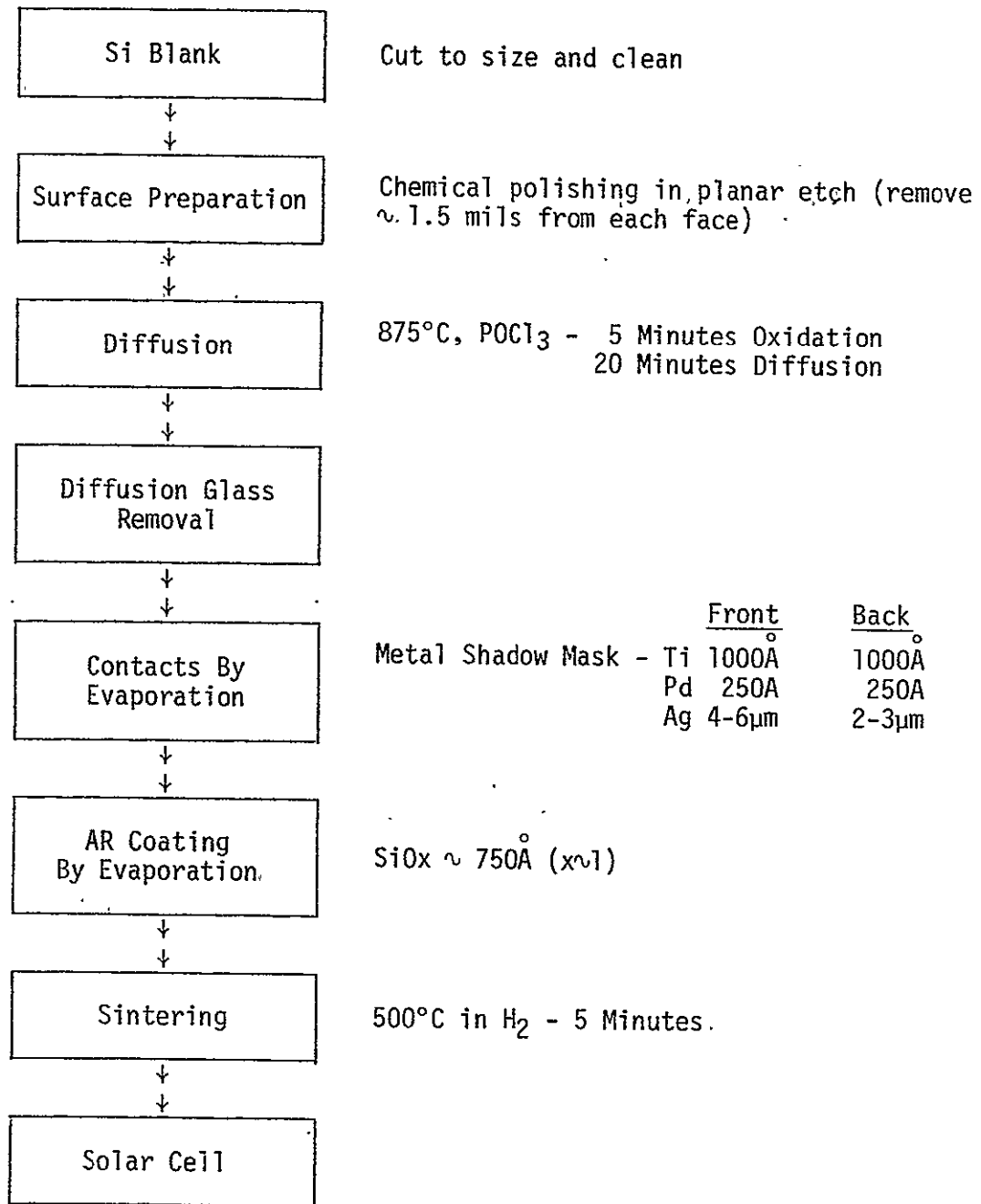


TABLE 1

| NUMBER OF<br>BROKEN CELLS | CAUSE                                                                        |
|---------------------------|------------------------------------------------------------------------------|
| 1                         | Dropped While Demounting 2x2 cm<br>Blanks                                    |
| 2                         | Corner Chipped While Clamping<br>Metal Shadow Mask In Evaporation<br>Process |
| 1                         | Shattered in Post-Metallization<br>Heat Treatment in a Furnace               |

Mechanical Failure of "Silso" Solar Cells  
in the Process of Fabrication (Standard Process)

applied and the standard process followed thereafter, the 400°C heating step was retained to minimize front contact peeling during pre-coating measurements.

NOTE: This modified process sequence (using the 600°C sintering of the back contact was used from this stage in the contract and became the "standard process".

### 2.3 Back Surface Field (BSF) Process

Back surface field was provided by evaporation of a thin Al layer followed by screen printing of Al paste, and an alloying step at an elevated temperature (~800°C). This process step was added after removal of diffused oxides in the standard process. Back and front contacts (Ti, Pd and Ag) were evaporated after the alloying step.

Two "Silso" wafers were processed in this way; the sheet resistance of the diffused layers was measured to be 27-31 ohm/square for the controls and 26-28 ohm/square for the "Silso" wafers. One cell was broken in the metallization process and two cells were damaged in electrical testing, resulting in an overall mechanical yield of around 90% (twenty-eight starting blanks).

### 2.4 Grain Boundary Passivation Process

Tests were made to try and increase the carrier collection efficiency in polycrystalline silicon by

means of a heavily doped region near (or in) the grain boundaries (1). Phosphorus dopant is preferentially introduced into the grain boundaries of p-type material by a low temperature diffusion process. A subsequent high temperature diffusion forms a heavily doped skin which covers the surface of each grain. The resulting junction around each grain surface collects electrons which might otherwise recombine at the undoped grain boundaries. This grain boundary doping (passivation) scheme offers possibility of an increase of conversion efficiency in polycrystalline silicon solar cells especially if the grain structure is columnar.

An experiment was performed in an effort to improve the conversion efficiency using this method. An N-type, (phosphorus-dopant) source (Emulsitone) was spun on 2x2 cm wafers. After drying on a hot plate, those wafers were loaded in a furnace and heated at 600°C for about 24 hours in N<sub>2</sub> atmosphere. After removing glass layers on the spin-on side of the wafers, standard process was used to complete the cells.

One "Silso" wafer was fabricated using this process with no breakage (mechanical yield of 100%). Sheet resistance of the diffused layers of both control and "Silso" wafers were in the range of 23-28 ohm/square and 28-30 ohm/square, respectively.

The next section summarizes the results obtained using the standard process, BSF, and attempted grain boundary passivation.

### 3.0 Solar Cell Performance and Characterization

#### 3.1 Characteristics Under Illumination

Parameters of the finished solar cells were measured under AMO conditions\* (135 mW/cm<sup>2</sup>, tungsten-xenon lamps with red and blue filters) before and after applying anti-reflective coating. The measurement block temperature was 25°C and the input light intensity was calibrated using a standard balloon-flown solar cell.

##### Standard Solar Cells

The detailed parameter of the individual control cells and Wacker "Silso" cells are given in Appendix III, electrical data sheets. Four (4) "Silso" wafers (A, B, C and D) were processed and their average values, standard deviation and ranges are summarized in Table 2. Slightly different performance from wafer to wafer is noticed from the summary table. To see the dependence of the parameters on the location of the cells on each "Silso" wafer, mainly due to the difference in grain structure, solar cells were classified as corner cells, edge cells, and middle cells depending on the location (see Figure 1; 1 corner cell, 6 edge cells, and 9 middle cells were obtained from each wafer). From data obtained from four Wacker wafers (standard process) dependence of cell parameters on location is

\*Detailed description of OCLI AMO Solar Simulator is given in Appendix II.

TABLE 2

Summary of Parameters of Solar Cells  
Fabricated From Four Wacker "Silso" Wafers (A, B, C & D); Standard Process\*

| WAFERS                         |                    | CONTROL               | A                        | B                    | C                    | D                      |
|--------------------------------|--------------------|-----------------------|--------------------------|----------------------|----------------------|------------------------|
| $V_{oc}$ (mV)                  | AVERAGE            | 552<br>(545)          | 532<br>(526)             | 528<br>(523)         | 541<br>(533)         | 541<br>(533)           |
|                                | STANDARD DEVIATION | 4.2<br>(4.7)          | 5.5<br>(7.2)             | 6.7<br>(8.3)         | 5.2<br>(4.3)         | 8.4<br>(6.8)           |
|                                | RANGE              | 544-557<br>(539-553)  | 524-543<br>(512-537)     | 513-537<br>(496-532) | 534-549<br>(529-541) | 532-555<br>(524-546)   |
| $J_{sc}$ (mA/cm <sup>2</sup> ) | AVERAGE            | 33.3<br>(25.6)        | 30.8<br>(22.7)           | 31<br>(23.2)         | 31<br>(23.6)         | 31<br>(24.0)           |
|                                | STANDARD DEVIATION | 1.3<br>(0.7)          | 0.7<br>(0.4)             | 0.6<br>(0.6)         | 0.9<br>(0.5)         | 0.8<br>(0.3)           |
|                                | RANGE              | 30.5-34.5<br>(25-27)  | 29.3-31.8<br>(21.8-23.3) | 29.8-31.8<br>(22-24) | 29-32<br>(22.8-24.3) | 30-32.5<br>(23.5-24.5) |
| CFF (%)                        | AVERAGE            | 73<br>(73)            | 65<br>(66)               | 67<br>(67)           | 69<br>(69)           | 68<br>(68)             |
|                                | STANDARD DEVIATION | 1.3<br>(1.1)          | 2.4<br>(3.3)             | 2.6<br>(3.6)         | 1.8<br>(1.8)         | 3.2<br>(2.0)           |
|                                | RANGE              | 70-74<br>(71-74)      | 61-68<br>(60-70)         | 61-70<br>(58-71)     | 66-71<br>(66-72)     | 65-76<br>(65-72)       |
| $\eta$ (%)                     | AVERAGE            | 9.9<br>(7.5)          | 7.9<br>(5.9)             | 8.0<br>(6.0)         | 8.6<br>(6.4)         | 8.5<br>(6.6)           |
|                                | STANDARD DEVIATION | 0.6<br>(0.2)          | 0.4<br>(0.4)             | 0.4<br>(0.2)         | 0.4<br>(0.3)         | 0.6<br>(0.5)           |
|                                | RANGE              | 8.7-10.3<br>(7.3-7.8) | 7.1-8.6<br>(5.2-6.4)     | 7.4-8.7<br>(4.9-6.5) | 8.1-9.2<br>(6.1-6.9) | 7.8-9.6<br>(6.1-7.1)   |

NOTE: 1. Measured under AMO condition at 25°C.

2. Cells (2x2cm) with SiO anti-reflective (AR) coating, parenthesis numbers are for the parameter before AR coating.

\*Later (Table 4) results are given for the modified standard process.



summarized in Table 3. As expected, due to smaller grain size at the corners and edges of Wacker wafer, solar cell efficiency clearly increases in order corner-edge-middle. All four Wacker wafers contained visible inclusions near the middle of the wafer, showing fine grain structures surrounding the inclusions and consequently producing poor solar cell performance compared with the rest of the wafer area; i.e. see cells A-10 and D-11 in Appendix III. Figure 3 shows a microscopic photograph of these inclusions which might have introduced from the container used for casting of Wacker silicon. An average conversion efficiency for the whole Wacker wafer can be estimated by considering the total area of corner cells ( $16 \text{ cm}^2$ ), edge cells ( $48 \text{ cm}^2$ ) and middle cells ( $36 \text{ cm}^2$ ). An average efficiency of around 8.1% (AM0) was obtained from the four Wacker wafers. In this case, the area occupied by the inclusion was not considered. However, the average efficiency will be lower than the above value if the area of poor performance were considered.

The initial standard process showed lower open circuit voltage and higher series resistance than expected. This was suspected to be due to a Schottky barrier formed at the back metal-silicon interface. A modified standard process (addition of a heat treatment step after back contact evaporation as described above)

TABLE 3

Dependence of Solar Cell Parameters on the Locating of a 2x2cm Blank  
Prepared From a Wacker "Silso" Wafer; Standard Process

|                                |                    | CORNER    | EDGE    | MIDDLE    |
|--------------------------------|--------------------|-----------|---------|-----------|
| $V_{oc}$ (mV)                  | AVERAGE            | 532       | 532     | 538       |
|                                | STANDARD DEVIATION | 4.2       | 7.4     | 9.3       |
|                                | RANGE              | 528~538   | 513~545 | 520~555   |
| $J_{sc}$ (mA/cm <sup>2</sup> ) | AVERAGE            | 29.8      | 30.8    | 31.5      |
|                                | STANDARD DEVIATION | 0.7       | 0.6     | 0.5       |
|                                | RANGE              | 29.3~30.8 | 29.8~32 | 30.5~32.5 |
| CFF (%)                        | AVERAGE            | 66        | 67      | 68        |
|                                | STANDARD DEVIATION | 3.6       | 1.8     | 3.2       |
|                                | RANGE              | 62~71     | 65~69   | 61~76     |
| $\eta$ (%)                     | AVERAGE            | 7.7       | 8.1     | 8.5       |
|                                | STANDARD DEVIATION | 0.5       | 0.3     | 0.5       |
|                                | RANGE              | 7.1~8.2   | 7.4~8.7 | 7.3~9.6   |

NOTE: Cells (2x2cm) with SiO<sub>2</sub> AR coating measured under AMO condition  
at 25°C.



FIGURE 3

A Microscopic Photograph of Inclusions  
in Wacker Wafer (200X Magnification)

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significantly improved the characteristics under illumination for both "Silso" cells and controls; average conversion efficiency increased from 8.1% to 9.6% for "Silso" cells and from 9.9% to 11.2% for control cells. Electric data sheets are in Appendix III and Table 4 summarizes parameters of these cells. Open circuit voltage of control cells showed greater improvement than those using Wacker silicon (compare  $V_{oc}$  in Table 4 and Table 2). The dependence of the parameters on the location of the cells on each "Silso" wafer was also obtained in Table 5, showing similar results with Table 3.

#### BSF Wacker Silicon Solar Cells

Back surface field solar cells showed an average efficiency of about 9.5%, about the same efficiency as the standard solar cells (modified); slightly improved short circuit current was offset by the decrease in open circuit voltage. However, efficiencies of the controls increased to 12.1% (about 1% conversion efficiency increase over the modified standard process cells) by improvement in both short circuit current and open circuit voltage. Individual cell parameters are listed in Appendix III and statistics are summarized in Table 6. In an effort to see the upper limit of efficiency of the Wacker sheets, fine contact lines (active area of the cell is around 93%) and multilayer

TABLE 4

Summary of Parameters of Solar Cells  
Fabricated From a Wacker "Silso" Wafer (J); Modified Standard Process

|                    | $V_{oc}$<br>(mV)     | $J_{sc}$<br>(mA/cm <sup>2</sup> ) | CFF<br>(%)       | $\eta$<br>(%)         |
|--------------------|----------------------|-----------------------------------|------------------|-----------------------|
| AVERAGE            | 558<br>(549)         | 30.5<br>(22.2)                    | 77<br>(77)       | 9.6<br>(6.9)          |
| STANDARD DEVIATION | 6.1<br>(7.4)         | 0.8<br>(0.6)                      | 1.3<br>(2.0)     | 0.5<br>(0.4)          |
| RANGE              | 549-565<br>(539-555) | 29.3-31.5<br>(21.3-23)            | 73-79<br>(72-79) | 8.8-10.2<br>(6.3-7.3) |

## Control Cells

|                    | $V_{oc}$<br>(mV)     | $J_{sc}$<br>(mA/cm <sup>2</sup> ) | CFF<br>(%)       | $\eta$<br>(%)          |
|--------------------|----------------------|-----------------------------------|------------------|------------------------|
| AVERAGE            | 593<br>(586)         | 32.9<br>(24)                      | 78<br>(78)       | 11.2<br>(8.2)          |
| STANDARD DEVIATION | N.A.                 | N.A.                              | N.A.             | N.A.                   |
| RANGE              | 591-595<br>(584-588) | 32.8-33<br>(23.8-24.3)            | 77-79<br>(76-80) | 11.1-11.3<br>(8.0-8.2) |

- NOTE: 1. Measurement under AMO condition at 25°C.  
2. Cells (2x2cm) with SiO<sub>2</sub> AR coating, parenthesis numbers are for the parameters before AR coating.

TABLE 5

Dependence of Solar Cell Parameters on the Location of a 2x2cm Blank  
Prepared From a Wacker "Silso" Wafer (I); Modified Standard Process

|                                |                    | CORNER* | EDGE      | MIDDLE    |
|--------------------------------|--------------------|---------|-----------|-----------|
| $V_{oc}$ (mV)                  | AVERAGE            | N.A.    | 551       | 563       |
|                                | STANDARD DEVIATION | N.A.    | 1.8       | 1.5       |
|                                | RANGE              | N.A.    | 549~554   | 561~565   |
| $J_{sc}$ (mA/cm <sup>2</sup> ) | AVERAGE            | N.A.    | 29.6      | 31        |
|                                | STANDARD DEVIATION | N.A.    | 0.2       | 0.2       |
|                                | RANGE              | N.A.    | 29.3~29.8 | 30.8~31.5 |
| CFF (%)                        | AVERAGE            | N.A.    | 76        | 78        |
|                                | STANDARD DEVIATION | N.A.    | 1.5       | 0.7       |
|                                | RANGE              | N.A.    | 73~77     | 76~79     |
| $\eta$ (%)                     | AVERAGE            | N.A.    | 9.2       | 10.0      |
|                                | STANDARD DEVIATION | N.A.    | 0.2       | 0.2       |
|                                | RANGE              | N.A.    | 8.8~9.4   | 9.8~10.2  |

NOTE: Cells (2x2cm) with SiO<sub>2</sub> AR coating measured under AMO condition  
at 25°C.

\*Cell broken, could not evaluate.

TABLE 6

Summary of Parameters of Solar Cells Fabricated From Wacker  
"Silso" Wafers (E & F); Back Surface Field (BSF) Process

|                    | $V_{oc}$<br>(mV)     | $J_{sc}$<br>(mA/cm <sup>2</sup> ) | CFF<br>(%)       | $\eta$<br>(%)         |
|--------------------|----------------------|-----------------------------------|------------------|-----------------------|
| AVERAGE            | 545<br>(536)         | 31.5<br>(22.6)                    | 75<br>(74)       | 9.5<br>(6.6)          |
| STANDARD DEVIATION | 8.4<br>(8.3)         | 0.9<br>(0.7)                      | 1.8<br>(2.7)     | 0.5<br>(0.4)          |
| RANGE              | 528-557<br>(518-547) | 29.5-33<br>(21.3-23.8)            | 71-79<br>(66-77) | 8.2-10.2<br>(5.7-7.2) |

## Control Cells

|         | $V_{oc}$<br>(mV)     | $J_{sc}$<br>(mA/cm <sup>2</sup> ) | CFF<br>(%)       | $\eta$<br>(%)          |
|---------|----------------------|-----------------------------------|------------------|------------------------|
| AVERAGE | 602<br>(593)         | 35.5<br>(25.8)                    | 77<br>(75)       | 12.1<br>(8.6)          |
| RANGE   | 601-602<br>(591-593) | 35.3-35.8<br>(25.8-26)            | 75-78<br>(72-78) | 12.0-12.3<br>(8.2-8.9) |

## Cells With Fine Contact Line and MLAR Coating

|         | $V_{oc}$<br>(mV) | $J_{sc}$<br>(mA/cm <sup>2</sup> ) | CFF<br>(%) | $\eta$<br>(%) |
|---------|------------------|-----------------------------------|------------|---------------|
| AVERAGE | 556              | 34.2                              | 77         | 10.7          |
| RANGE   | 550-561          | 33.6-34.8                         | 75-78      | 10.6-10.8     |

- NOTE: 1. Measured under AMO condition at 25°C.  
2. Cells (2x2cm) with SiO<sub>2</sub> AR coating, parenthesis numbers are for the parameters before AR coating.

anti-reflective coating were applied to three of the BSF cells, resulting in an average conversion efficiency of 10.7%. Results are summarized in a bottom table of table 6. Positional dependence of BSF cell performance is given in Table 7 with the similar results with the solar cells from the other processes.

#### Grain Boundary Passivated Solar Cells

Solar cells from the grain boundary passivation process showed very close performance characteristics with the cells from the standard process, indicating no improvement was achieved by using this process modification. Electrical data sheets and summary tables are given in Appendix III and Table 8, respectively.

### 3.2 Dark I-V Characteristics

Dark I-V characteristics (forward and reverse) were obtained from the selected solar cells. The plot was made by point-by-point measurement using digital multi-meters. Room temperature plots of the dark I-V curves for solar cells from various processes are given in Figures 4 through 7. Sometimes dark diode currents of a solar cell can be expressed in a simple way,

$$I_D = I_0 \left( \exp \frac{qV}{AkT} - 1 \right)$$

This could be the case at high forward bias condition ( $V > 0.4$  volts) in which diffusion component dominates



TABLE 7

Dependence of Solar Cell Parameters on the Location of a 2x2cm Blank  
Prepared From Wacker "Silso" Wafers (E & F): BSF Process

|                                |                    | CORNER    | EDGE      | MIDDLE   |
|--------------------------------|--------------------|-----------|-----------|----------|
| $V_{oc}$ (mV)                  | AVERAGE            | 531       | 540       | 552      |
|                                | STANDARD DEVIATION | N.A.      | 2.6       | 4.2      |
|                                | RANGE              | 528~533   | 534~541   | 547~557  |
| $J_{sc}$ (mA/cm <sup>2</sup> ) | AVERAGE            | 29.6      | 31.0      | 32.0     |
|                                | STANDARD DEVIATION | N.A.      | 0.4       | 0.5      |
|                                | RANGE              | 29.5~29.8 | 30.5~31.8 | 31.3~33  |
| CFF (%)                        | AVERAGE            | 72        | 75        | 75       |
|                                | STANDARD DEVIATION | N.A.      | 1.2       | 1.6      |
|                                | RANGE              | 71~72     | 74~77     | 73~79    |
| $\eta$ (%)                     | AVERAGE            | 8.4       | 9.4       | 9.9      |
|                                | STANDARD DEVIATION | N.A.      | 0.2       | 0.3      |
|                                | RANGE              | 8.2~8.5   | 8.9~9.6   | 9.4~10.2 |

NOTE: Cells (2x2cm) with SiO<sub>2</sub> AR coating measured under AMO condition  
at 25°C.

TABLE 8

Summary of Parameters of Solar Cells Fabricated From a  
Wacker "Silso" Wafer (I); Grain Boundary Passivated Process

|                    | $V_{oc}$<br>(mV)     | $J_{sc}$<br>(mA/cm <sup>2</sup> ) | CFF<br>(%)       | $\eta$<br>(%)         |
|--------------------|----------------------|-----------------------------------|------------------|-----------------------|
| AVERAGE            | 554<br>(543)         | 30<br>(22)                        | 76<br>(75)       | 9.4<br>(6.6)          |
| STANDARD DEVIATION | 9.0<br>(9.0)         | 5.3<br>(1.0)                      | 0.5<br>(3.2)     | 0.6<br>(0.5)          |
| RANGE              | 536-565<br>(524-552) | 27.5-31.5<br>(20-23)              | 76-77<br>(65-78) | 8.2-10.1<br>(5.8-7.2) |

Control Cells

|                    | $V_{oc}$<br>(mV)     | $J_{sc}$<br>(mA/cm <sup>2</sup> ) | CFF<br>(%)       | $\eta$<br>(%)          |
|--------------------|----------------------|-----------------------------------|------------------|------------------------|
| AVERAGE            | 592<br>(582)         | 32.8<br>(24.2)                    | 78<br>(76)       | 11.2<br>(7.9)          |
| STANDARD DEVIATION | N.A.                 | N.A.                              | N.A.             | N.A.                   |
| RANGE              | 590-593<br>(580-585) | 32.5-33.3<br>(24-24.3)            | 77-79<br>(74-79) | 10.9-11.6<br>(7.6-8.3) |

- NOTE: 1. Measured under AMO condition at 25°C.  
2. Cells (2x2cm) with SiO AR coating, parenthesis numbers are from the parameters before AR coating.



FIGURE 4

Dark I-V Characteristics of Wacker Solar Cells  
(2x2cm, Standard Process) at R.T.

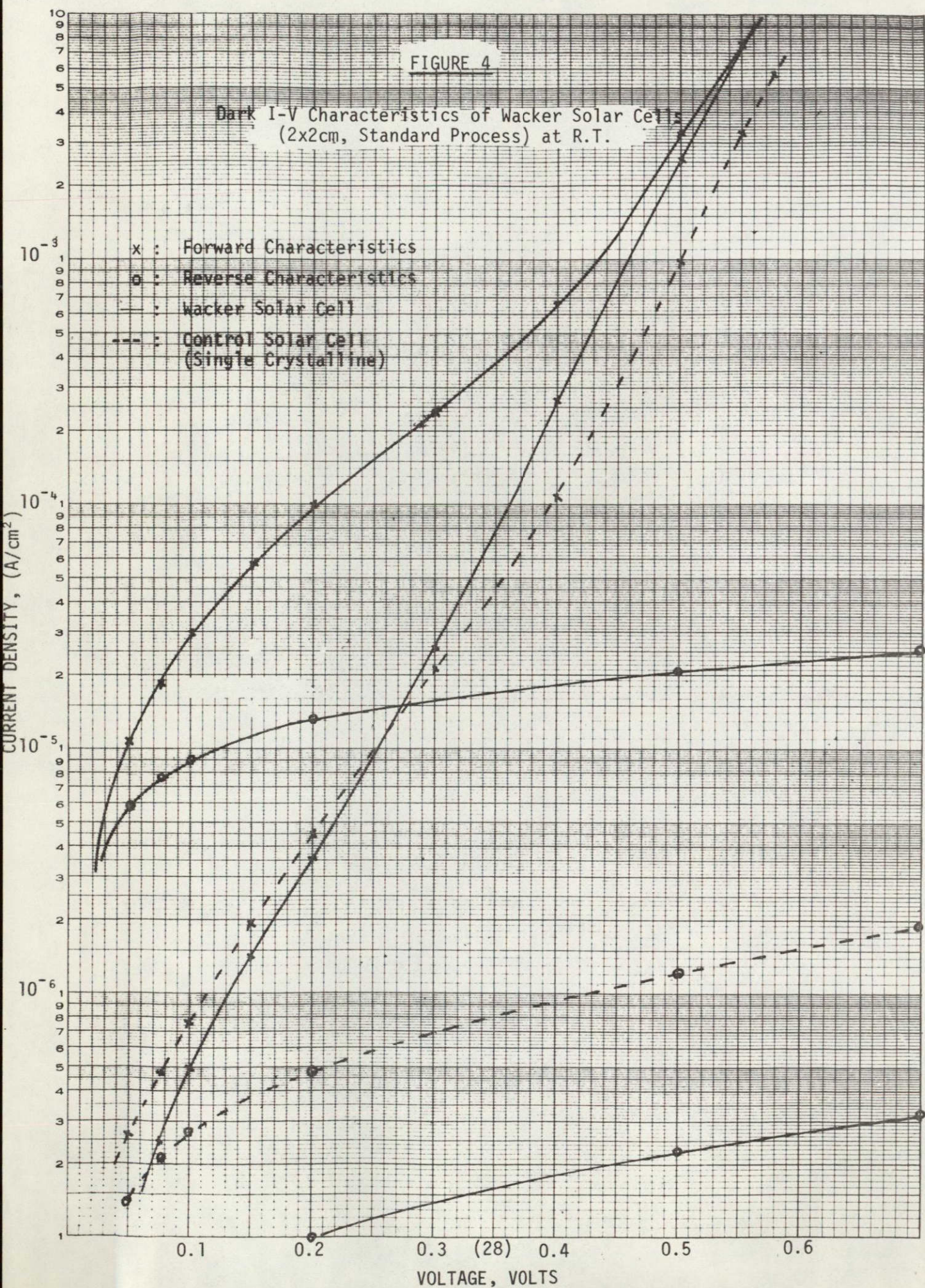




FIGURE 5

Dark I-V Characteristics of Wacker Solar Cells  
(2x2cm, Modified Standard Process) at R.T.

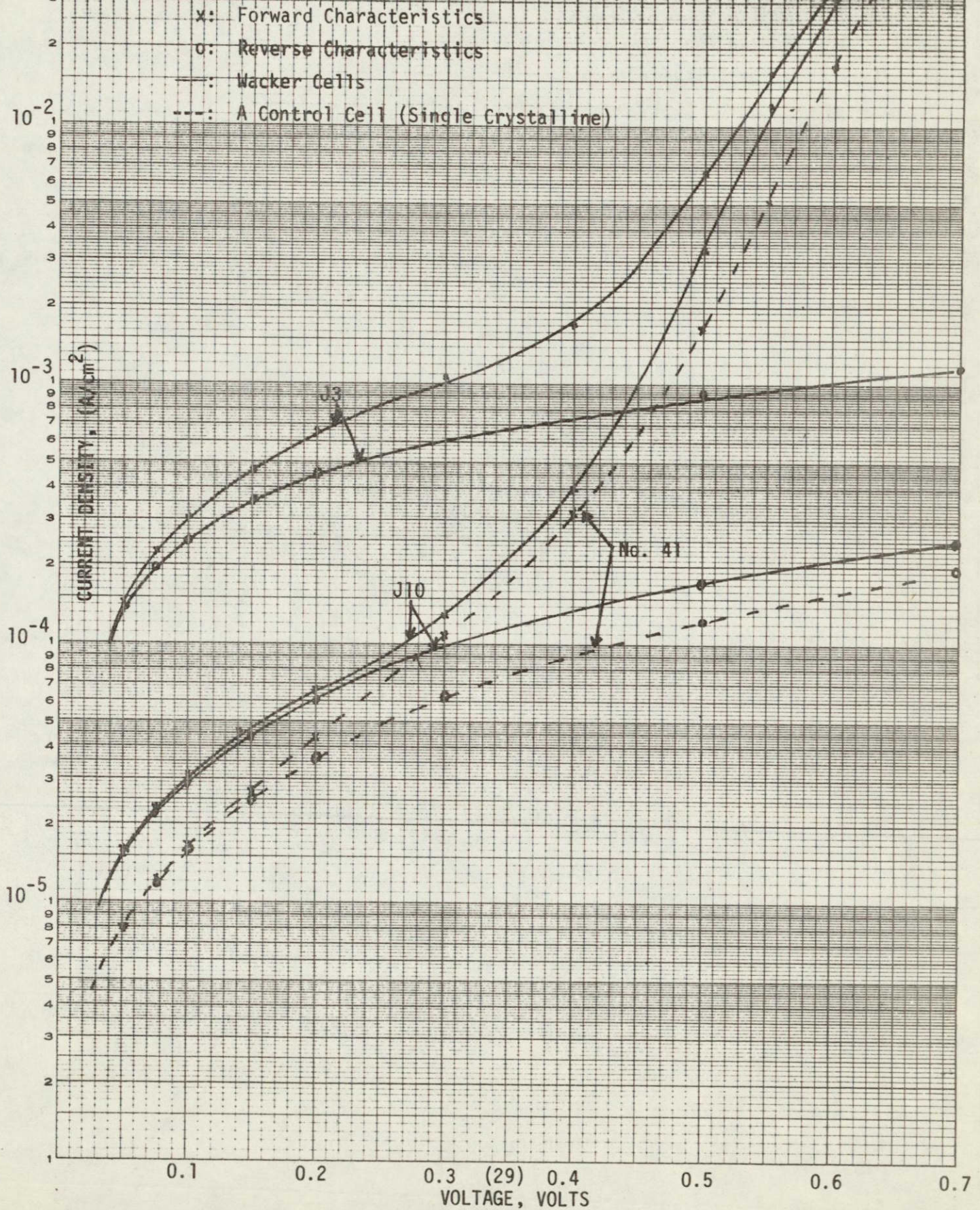




FIGURE 6

Dark I-V Characteristics of Wacker Solar Cells  
(2x2cm, BSF Process) at R.T.

- x: Forward Characteristics
- o: Reverse Characteristics
- : Wacker Cells
- : A Control Cell (Single Crystalline)

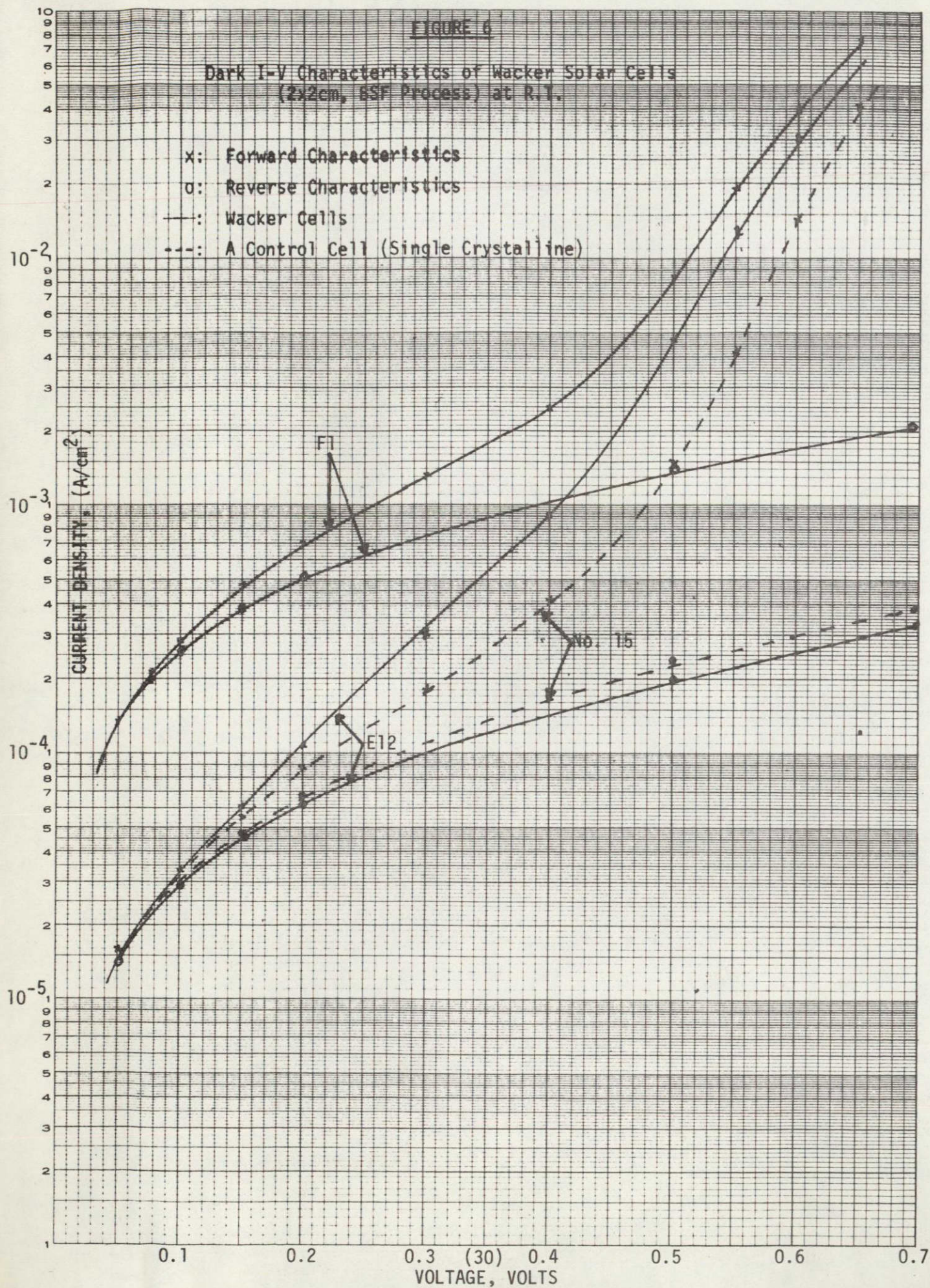
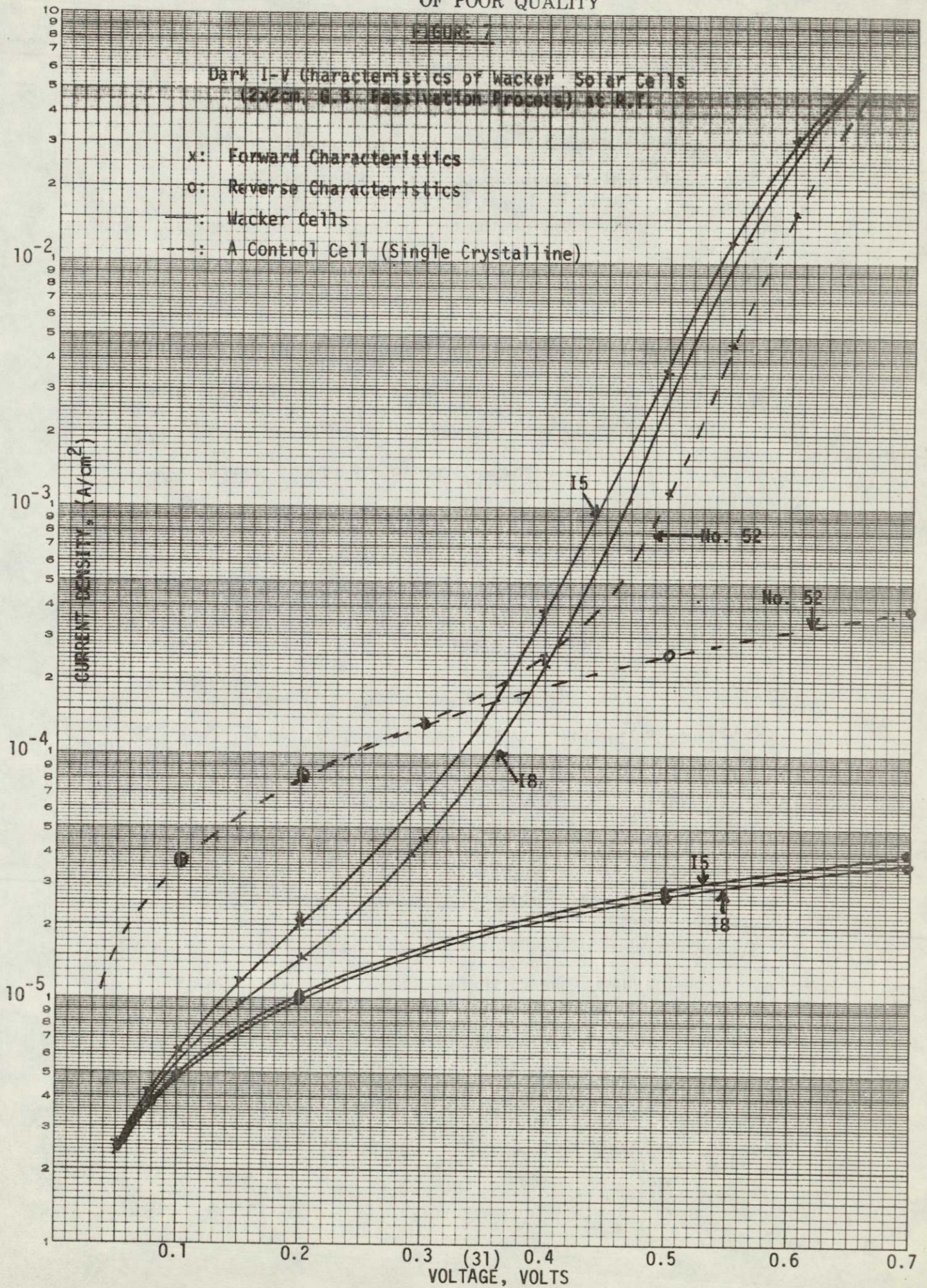




FIGURE 7

Dark I-V Characteristics of Wacker Solar Cells  
(2x2cm, G.B. Passivation Process) at R.T.





diode current. In this case "A" factor in the equation shows deviation from ideal diode characteristics, i.e. it indicates the degree of influence from the space charge recombination and shunt component of the current. Calculated "A" values from the curves ranged from 1.4 to 2.2, indicating significant deviation from the ideal diode case in which the "A" factor is unity.  $I_0$  was also obtained from the plots. A relatively wide range of  $I_0$  was observed, from  $10^{-6}$  A/cm<sup>2</sup> to  $10^{-9}$  A/cm<sup>2</sup>; solar cells with small grain structure, such as corner cells and edge cells, showed larger values. This indicates that low open circuit voltage of the cells with small grain size is due to the large value of  $I_0$ .

### 3.3 Spectral Response

Absolute spectral response (A/W) was measured using a filter wheel which is a combination of a set of narrow bandwidth filters and a light source (tungsten lamp operated at color temperature of 2800°C). Spectral response of the solar cells was obtained by reading the current (short circuit) of the cells (to be measured) at known wavelengths and by calibrating this current to the current of a cell of known spectral response (standard cell of known spectral response). The active area of the solar cells was included in the calculation. Figures 8 through 11 show spectral response of Wacker cells and typical

FIGURE 9

Spectral Response of Wacker Solar Cells  
(Modified Standard Process)

**OCLI** OPTICAL COATING  
LABORATORY, INC.

15251 E. DON JULIAN ROAD  
CITY OF INDUSTRY, CA 91746  
TELEPHONE (213) 968-6581

ABSOLUTE SPECTRAL  
RESPONSE

SAMPLE IDENTIFICATION

$\Delta$  : Control #41

O : Wacker J-15

X : " J-2

DATE: 8/23/78

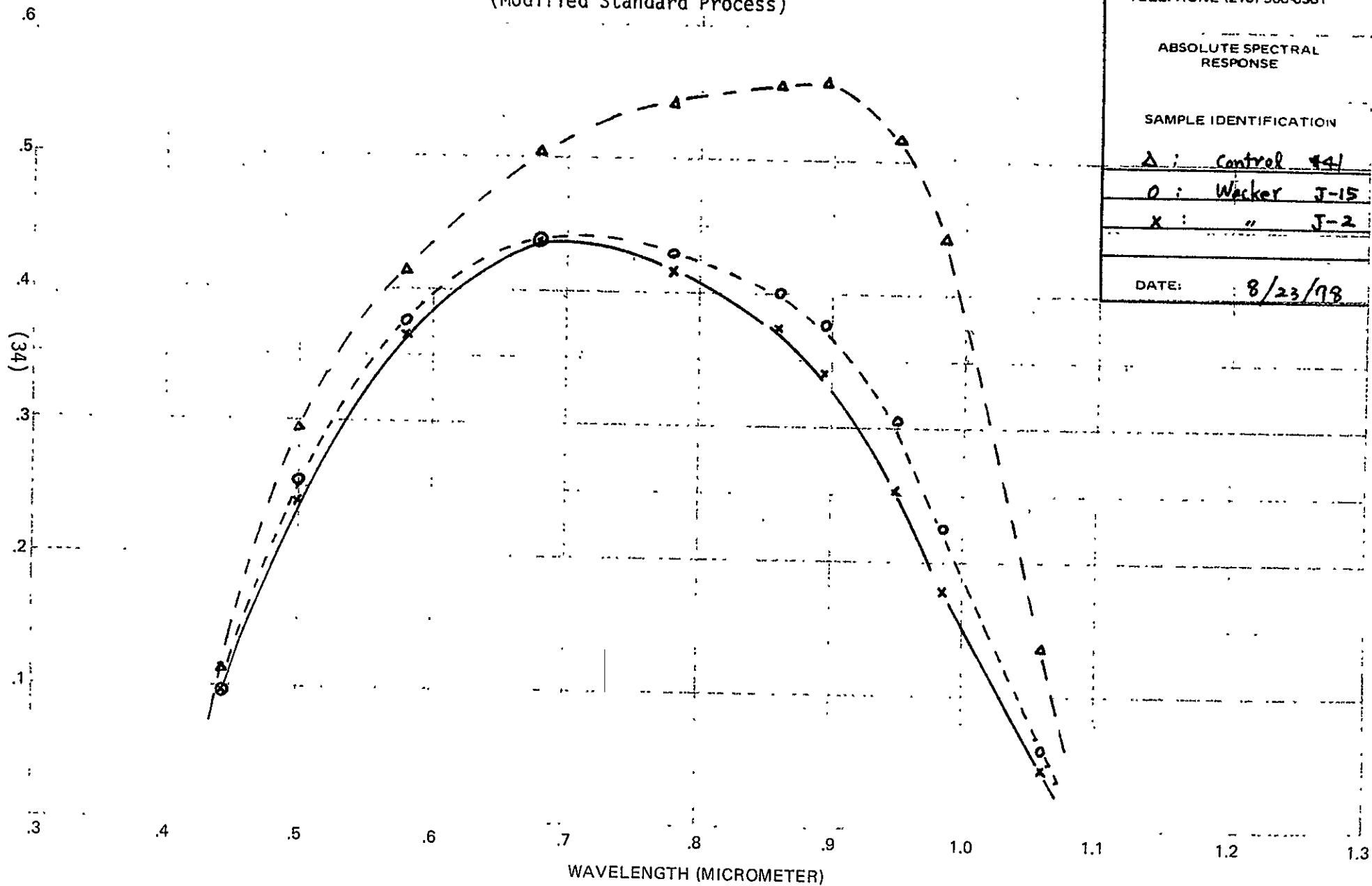




FIGURE 10

Spectral Response of Wacker Solar Cells  
(BSF Process)

**OCLI** OPTICAL COATING  
LABORATORY, INC.

15251 E. DON JULIAN ROAD  
CITY OF INDUSTRY, CA 91746  
TELEPHONE (213) 968-6581

ABSOLUTE SPECTRAL  
RESPONSE

SAMPLE IDENTIFICATION

X : (control) #13

O : E7

□ : E1

△ : E2

DATE: 7/31/98

SPECTRAL RESPONSE (A/W)

(35)

WAVELENGTH (MICROMETER)

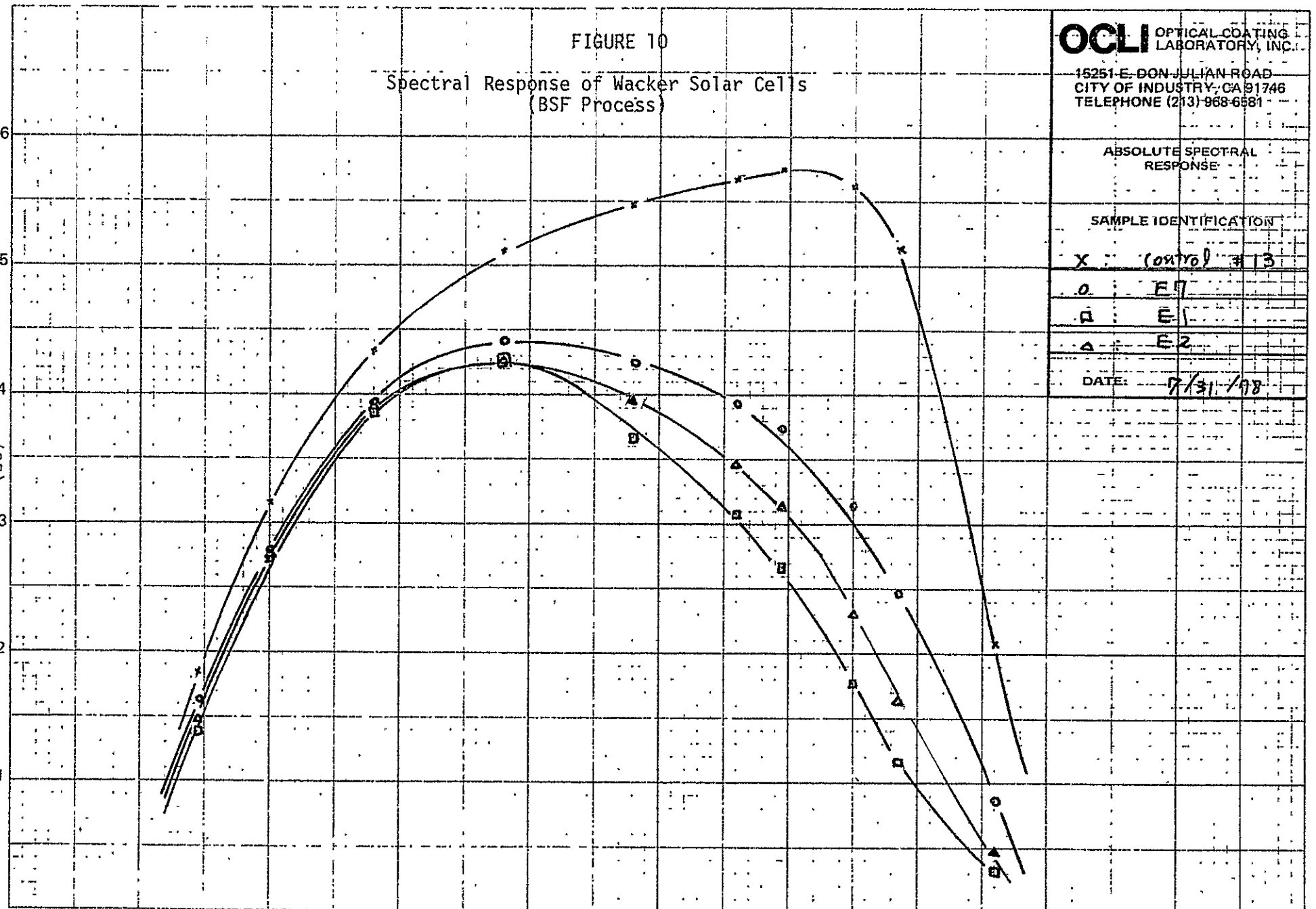


FIGURE 11

Spectral Response of Wacker Solar Cells  
(G.B. Passivation Process)

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LABORATORY, INC.

15251 E. DON JULIAN ROAD  
CITY OF INDUSTRY, CA 91746  
TELEPHONE (213) 988-6581

ABSOLUTE SPECTRAL  
RESPONSE

SAMPLE IDENTIFICATION

$\Delta$  : # 51 control

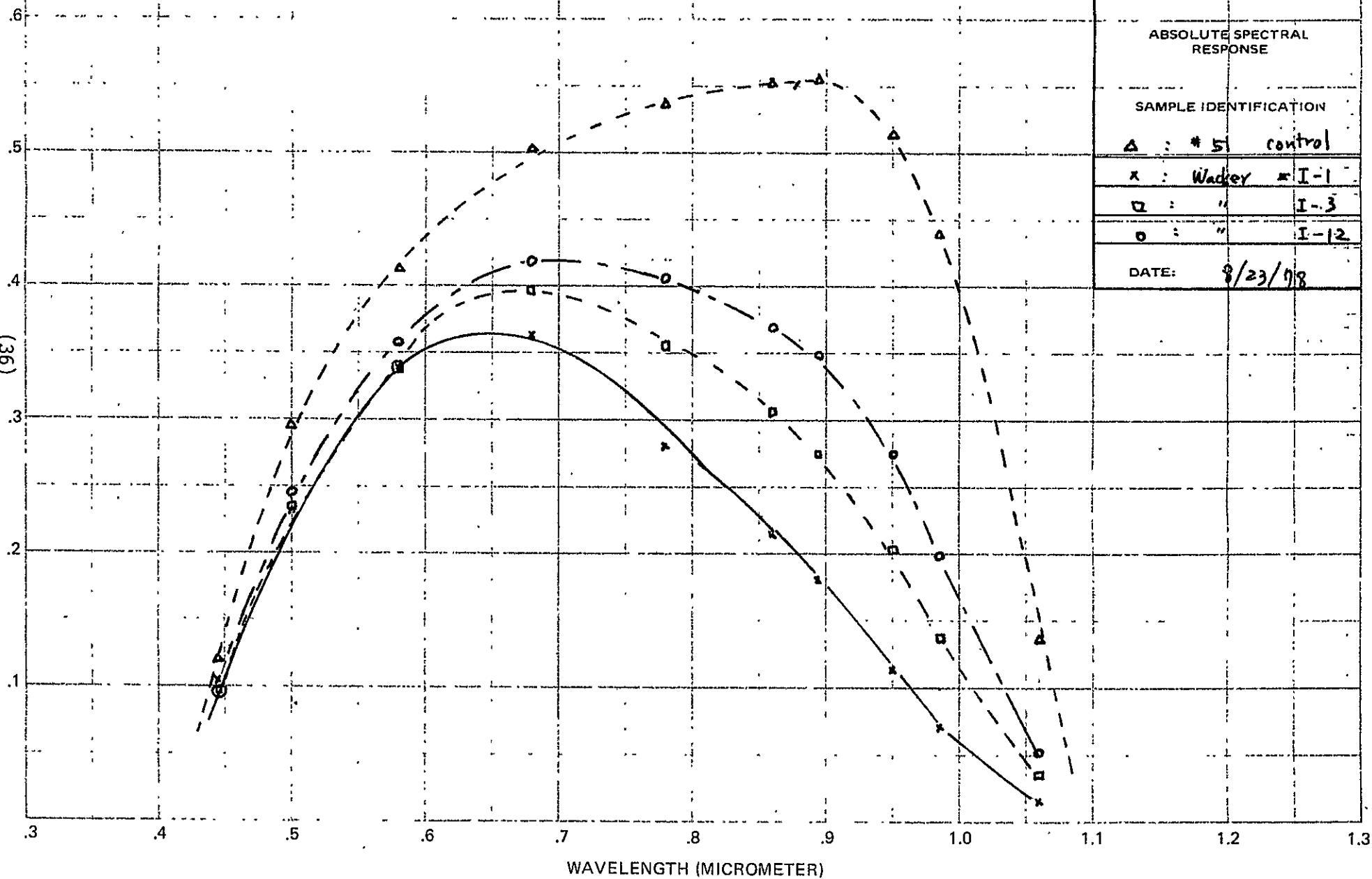
x : Wacker # I-1

$\square$  : " I-3

o : " I-12

DATE: 8/23/78

SPECTRAL RESPONSE (A/W)  
(36)



control cells of different process modification. Cells made from Wacker wafers indicated lower spectral response than single crystalline control cells at longer wavelengths ( $>0.6 \mu\text{m}$ ), mainly due to smaller minority carrier diffusion length caused by grain boundary effects. The Wacker cells with lower spectral response were located in the edge (small grain size) while Wacker cells with higher response were located in the middle (large grain size) of the Wacker wafers, confirming the effect of grain size on spectral response of solar cells. The spectral response variations also agreed with the cell performance variations. However, no significant difference in spectral response was noticed from Wacker cells taken through the process variations tried (BSF, GB passivation).

### 3.4 Minority Carrier Diffusion Length

Minority carrier diffusion length (D.L.) was measured using the surface photovoltage (SPV) method on both bulk "Silso" wafers and diffused wafers. The exposed filtered beam size was about 2-3 mm in diameter and the results are summarized in Table 9. Generally middle blanks showed higher D.L., showing D.L. in some spots as close to those of single crystalline silicon. No significant change in D.L. before and just after the diffusion step were observed. Diffusion length measurement was also carried out using a short circuit current method

TABLE 9

Minority Carrier Diffusion Length  
Measurement on Bulk Wacker Wafers

|                    | CORNER & EDGE    | MIDDLE             |
|--------------------|------------------|--------------------|
| AVERAGE            | 43<br>(35)       | 75<br>(88)         |
| STANDARD DEVIATION | 5<br>(5)         | 15<br>(19)         |
| RANGE              | 40-55<br>(30-40) | 60-130<br>(55-120) |

- NOTE: 1) Parenthesis numbers for the diffused wafers without contacts.
- 2) Measurement by SPV method with a light beam size ~2-3 mm diameter.
- 3) Unit;  $\mu\text{m}$ .

(2) for the finished solar cells. The whole area of a solar cell was illuminated by light source through a filter wheel and the effective minority carrier diffusion length of a solar cell was obtained from light intensity values at selected wavelengths. Wavelengths used for this measurement were 0.78, 0.86, 0.895 and 0.95  $\mu\text{m}$ . The wavelength dependence of reflection and absorption in anti-reflective coating layer was not considered for simplicity (generally, a straight line plot could be achieved). Table 10 summarizes the diffusion length values of solar cells made from four Wacker wafers (A, B, C and D) and Table 11 indicates the dependence of diffusion length on location of each cell in a wafer, such as corners, edges and middle. Diffusion length of solar cells (2x2 cm) ranged from 30-65  $\mu\text{m}$ , showing lower diffusion length for the cells fabricated from either corners or edges of a wafer. Diffusion length measurement using small beam size ( $\sim 3\text{-}4$  mm beam diameter) indicated that significant variation in the values are observed even within a single solar cell (2x2 cm). These are well illustrated in Figure 12, again indicating smaller diffusion length at spots close to edge due to small grain structure.

Diffusion length measurement was performed on areas of the wafer containing inclusions (as in A-10 and D-11 solar cells). Diffusion length values were about the

TABLE 10

Minority Carrier Diffusion Length of Solar Cells (2x2cm)  
Fabricated From Four Wacker Wafers (A, B, C and D)

| WAFERS               |                    | CONTROL | A     | B     | C     | D     |
|----------------------|--------------------|---------|-------|-------|-------|-------|
| Le ( $\mu\text{m}$ ) | AVERAGE            | 130     | 47    | 46    | 52    | 51    |
|                      | STANDARD DEVIATION | N.A.    | 7.7   | 11.7  | 10    | 9.5   |
|                      | RANGE              | 130-140 | 33-56 | 33-61 | 35-65 | 31-60 |

TABLE 11

Dependence of Diffusion Length of Solar Cells on the  
Location of a 2x2 cm Blank Prepared From a Wacker Wafer

| LOCATION             |                    | CORNER | EDGE  | MIDDLE |
|----------------------|--------------------|--------|-------|--------|
| Le ( $\mu\text{m}$ ) | AVERAGE            | 33     | 44    | 56     |
|                      | STANDARD DEVIATION | 1.6    | 5.4   | 5.4    |
|                      | RANGE              | 31-35  | 34-51 | 49-65  |

- NOTE: 1) Measurement by  $I_{sc}$  method.  
2) Illuminated whole area of 2x2cm cells.  
3) Unit;  $\mu\text{m}$ .



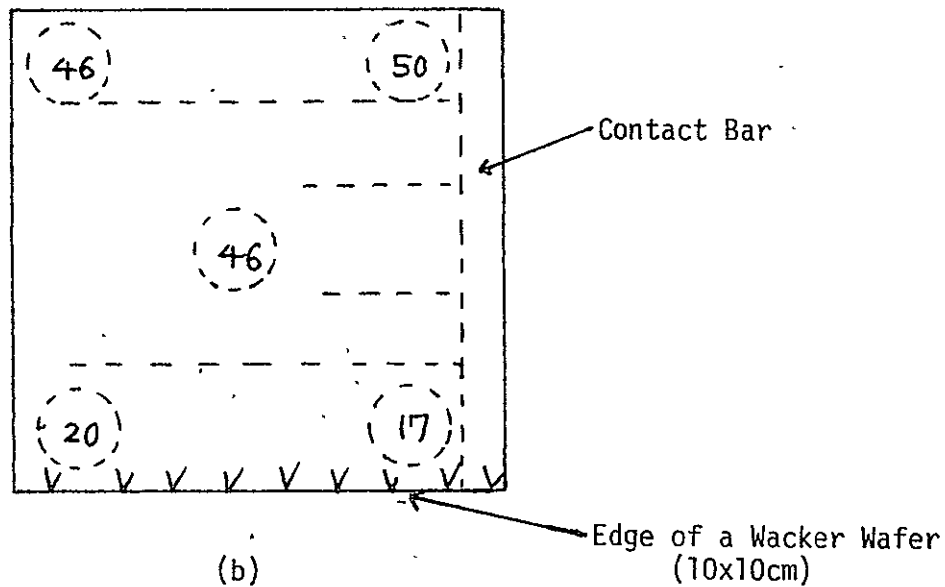
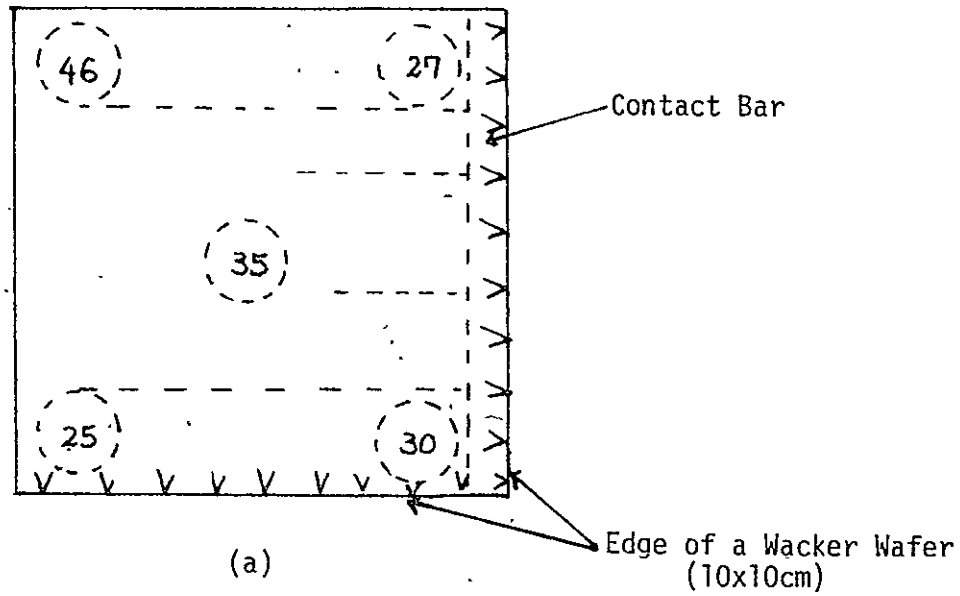
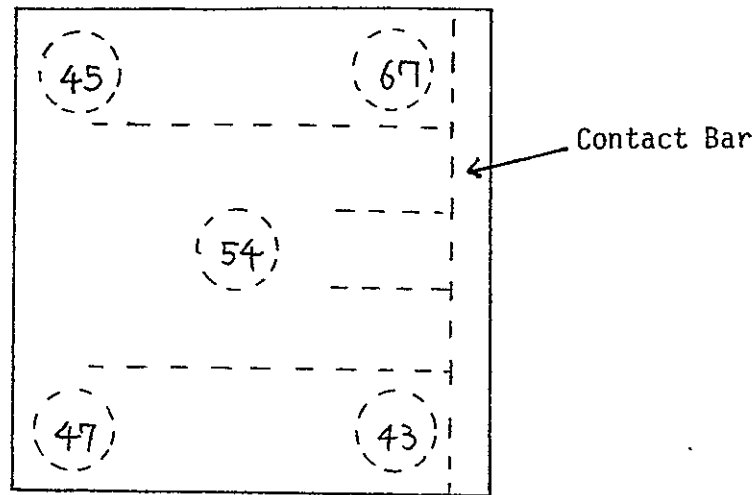


FIGURE 12

Minority Carrier Diffusion Length ( $\mu\text{m}$ ) Variation  
Within a Wacker Solar Cell (2x2cm), Measured by  $I_{SC}$  Method  
With an illuminated Beam Size of  $\sim 3\text{-}4\text{mm}$  Diameter

- a) A Corner Solar Cell (A1)
- b) A Edge Solar Cell (A3)



(c)

FIGURE 12

Minority Carrier Diffusion Length ( $\mu\text{m}$ ) Variation  
 Within a Wacker Solar Cell (2x2cm), Measured by  $I_{SC}$  Method  
 With an Illuminated Beam Size of  $\sim 3\text{-}4\text{mm}$  Diameter

c) A Middle Solar Cell (A11)

same as the rest of the cell area. This indicated that the poor performance of these cells are not due to the small grain structure, but due to shunting caused by those inclusions.

## B. EFG Ribbon Solar Cells

### 1.0 Preparation and Description on Blanks

The EFG ribbons delivered were of the R.F. furnace grown type with visible surface undulations and inclusions from the die materials. The ribbon was about one inch wide and was sliced into approximately 1x1 inch blanks. Thickness was measured (by micrometer), at several locations of each blank, indicating around 13 mils at the edges and 10 mils in the middle. To obtain detailed information on the surface profile of the ribbons, a Dektak (Sloan) was used to scan thickness across the width of the ribbons. Figure 13 shows a typical profile of a ribbon surface, indicating significant variation in thickness across the ribbon width.

NOTE: In the worst case, thickness could be around 6 mils or less at certain localized areas, indicating problems of handling in the process of cell fabrication.

Since most of the blanks showed warpage, a bow gauge (Brown & Sharp) was used to show the degree of warpage (this may not be the proper way to check the warpage of such blanks). From 15 samples of 1" x 1" blanks bows were averaged to be around 2.0 mils with the range of 0.4-3.0 mils.

Resistivity measurement by four point probe ranged between 0.8-2.8 ohm-cm with p-type conductivity. This might not necessarily indicate accurate bulk resistivity because of thickness variations and possible grain boundary effects.

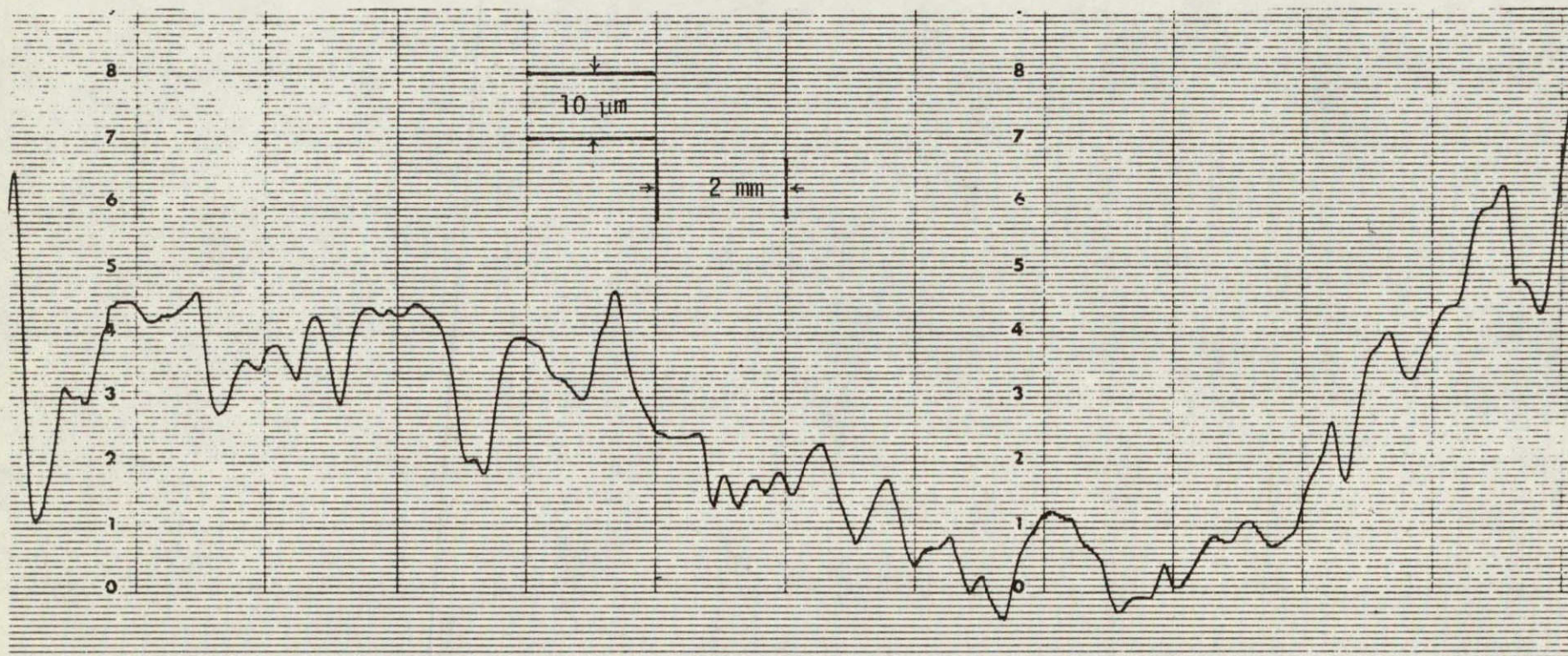


FIGURE 13

A Typical Surface Profile Across the Width of a EFG Ribbon  
(Ribbon Width ~1") by Dektak (Sloan)



SPV measurement of minority carrier diffusion length from a number of measurements with the beam size of 3-4 mm in diameter indicated values between 30-70  $\mu\text{m}$ .

Initial cleaning of the blanks was done by organic solvent in ultrasonic cleaner, to remove most of the contaminants from wafer handling. However, a hazy color on the surface was difficult to eliminate without removing some silicon. Following efforts were made to remove hazy surface features.

1. Dip in HF.
2. Boil in hot D.I. water followed by HF dip (since haze was suspected to be a thin  $\text{SiO}$  layer).
3. Clean in  $\text{H}_2\text{SO}_4$ ;  $\text{H}_2\text{O} = 1:1$
4. Standard RCA Clean
  - Solution 1 -  $\text{NH}_4\text{OH}$ ;  $\text{H}_2\text{O}_2$ ;  $\text{H}_2\text{O} = 1:1:5$
  - Solution 2 -  $\text{HCL}$ ;  $\text{H}_2\text{O}_2$ ;  $\text{H}_2\text{O} = 1:1:5$

None of the above procedure succeeded in removing the haze. Thus, the standard wafer cleaning procedure was chosen to be the initial organic solvent cleaning procedure which will remove all the surface contamination from wafer handling.

breakage are listed in Table 12. An analysis indicated that the most of the breakage are closely related with the non-flat features of the ribbons and possibly to residual stress in the blanks. This is considered to be a significantly low yield compared with either the single crystalline or "Silso" cells.

## 2.2 Back Surface Field Process

The same BSF process, described in Section A.2.3, was used for EFG sheets with the modification of front contact formation by photolithographic techniques as described in the previous section (B.2.1).

Finished EFG solar cells showed a mechanical yield of about 54%; again 13 cells out of 28 starting sheets were broken in this process. Detailed cause of the breakage are given in Table 13, and again are attributed to the properties of the starting ribbon.



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TABLE 12

Mechanical Failure of EFG Solar Cells  
in the Process of Fabrication; Standard Process

| NUMBER OF<br>BROKEN CELLS | CAUSE                                                    |
|---------------------------|----------------------------------------------------------|
| 3                         | TEST<br>Diamond Scribing 1<br>Back Contact 2             |
| 2                         | FRONT CONTACT<br>Photoresist Spin 1<br>Develop & Rinse 1 |
| 1                         | BACK CONTACT                                             |
| 2                         | EDGE TRIMMING OR CUTTING USING DICING SAW                |
| 2                         | ELECTRICAL TEST                                          |

Starting: 22 Wafers

TABLE 13

Mechanical Failure of EFG Solar Cells  
in the Process of Fabrication; BSF Process

| NUMBER OF<br>BROKEN CELLS | CAUSE                                                                                                                              |
|---------------------------|------------------------------------------------------------------------------------------------------------------------------------|
| 1                         | INITIAL CLEANUP PROCESS                                                                                                            |
| 4                         | BSF PROCESS<br>Al Screen Printing 1<br>Al Alloy (Al Penetration) 1<br>Al Scrubbing (Residual) 1<br>Acid Clean (Remove Excess Al) 1 |
| 2                         | FRONT CONTACT, PHOTORESIST EXPOSURE                                                                                                |
| 4                         | ELECTRICAL TEST                                                                                                                    |
| 1                         | EDGE TRIMMING                                                                                                                      |
| 1                         | PROCESS MISTAKE                                                                                                                    |

Starting: 28 Wafers

### 3.0 Solar Cell Performance and Characterization

#### 3.1 Characteristics Under Illumination

Solar cell parameters, such as  $I_{sc}$ ,  $V_{oc}$ , CFF and  $\eta$ , were measured under AMO solar simulation at 25°C. Electrical data sheets in Appendix IV give detailed information on individual cells and Table 14 and Table 15 summarize the results for cells of two process types, standard process and BSF process, respectively. BSF solar cells showed improved efficiency compared with standard solar cells, 8.5% versus 7.8%, with the overall increase in  $I_{sc}$ ,  $V_{oc}$ , and CFF.

Conversion efficiency of EFG solar cells was less than those of "Silso" solar cells and also less than recently reported results with EFG ribbon, mainly due to lower  $V_{oc}$  and CFF. This was suspected to be due to shunting by SiC (die material), which can be detected visually on the surface of the ribbon in many cases. Thus, a number of experiments were done to eliminate the effect of those particles by isolating and dicing off the area possessing the inclusions. In one case open circuit voltage increased from 525 (mV) to 545 (mV) while curve fill factor improved from 58% to 66% after removal of some inclusions. A typical inclusion, which is presumed to have originated from die material, is shown in Figure 14 (from Cell No. 13). However, improvement in either  $V_{oc}$  or CFF was not always obtained after the

TABLE 14

Summary of Parameters of Solar cells  
Fabricated From EFG Ribbons; Standard Process

|                    | $V_{oc}$<br>(mV)     | $J_{sc}$<br>(mA/cm <sup>2</sup> ) | CFF<br>(%)       | $\eta$<br>(%)        |
|--------------------|----------------------|-----------------------------------|------------------|----------------------|
| AVERAGE            | 540<br>(529)         | 28.8<br>(21.4)                    | 67.8<br>(64.8)   | 7.8<br>(5.5)         |
| STANDARD DEVIATION | 12.5<br>(14.4)       | 1.2<br>(1.4)                      | 8.9<br>(11.6)    | 1.3<br>(1.2)         |
| RANGE              | 517-556<br>(496-549) | 26.3-30.2<br>(18.8-22.9)          | 52-79<br>(43-80) | 5.8-9.6<br>(3.5-7.1) |

Control Cells

|                    | $V_{oc}$<br>(mV) | $J_{sc}$<br>(mA/cm <sup>2</sup> ) | CFF<br>(%)       | $\eta$<br>(%)        |
|--------------------|------------------|-----------------------------------|------------------|----------------------|
| AVERAGE            | 596<br>(589)     | 33.65<br>(24.3)                   | 79<br>(78)       | 11.8<br>(8.3)        |
| STANDARD DEVIATION | 0<br>(0)         | 0.1<br>(0.1)                      | 1.1<br>(1.8)     | 0.2<br>(0.2)         |
| RANGE              | 596<br>(589)     | 33.5-33.8<br>(24.3-24.5)          | 78-80<br>(76-80) | 11.6-12<br>(8.0-8.5) |

- NOTE: 1. Measured under AMO condition at 25°C.  
2. Cells (~5-6cm<sup>2</sup> in area) with SiO<sub>2</sub> AR coating, parenthesis numbers are for the parameters before AR coating.

TABLE 15

Summary of Parameters of Solar Cells  
Fabricated From EFG Ribbon; BSF process

|                    | $V_{oc}$<br>(mV)     | $J_{sc}$<br>(mA/cm <sup>2</sup> ) | CFF<br>(%)       | $\eta$<br>(%)         |
|--------------------|----------------------|-----------------------------------|------------------|-----------------------|
| AVERAGE            | 549<br>(538)         | 29.4<br>(22.4)                    | 71<br>(70)       | 8.5<br>(6.2)          |
| STANDARD DEVIATION | 14<br>(17.5)         | 1.3<br>(1.2)                      | 7.4<br>(7.5)     | 1.1<br>(0.9)          |
| RANGE              | 533-572<br>(506-565) | 26-31.2<br>(19.9-24.3)            | 55-78<br>(51-77) | 6.5-10.3<br>(4.4-7.8) |

Selected EFG Cells With MLAR Coating

|         | $V_{oc}$<br>(mV) | $J_{sc}$<br>(mA/cm <sup>2</sup> ) | CFF<br>(%) | $\eta$<br>(%) |
|---------|------------------|-----------------------------------|------------|---------------|
| AVERAGE | 572<br>(562)     | 32.3<br>(24.2)                    | 78<br>(76) | 10.6<br>(7.7) |

Control Cells

|         | $V_{oc}$<br>(mV) | $J_{sc}$<br>(mA/cm <sup>2</sup> ) | CFF<br>(%) | $\eta$<br>(%) |
|---------|------------------|-----------------------------------|------------|---------------|
| AVERAGE | 603<br>(597)     | 33.9<br>(24.8)                    | 76<br>(75) | 11.5<br>(8.2) |

- NOTE: 1. Measured under AMO condition at 25°C.  
2. Cells ( $\sim 5\text{-}6\text{cm}^2$  in area) with SiO<sub>2</sub> AR coating (middle table is for the selected EFG cells with MLAR coating), parenthesis numbers are for the parameters before AR coating.

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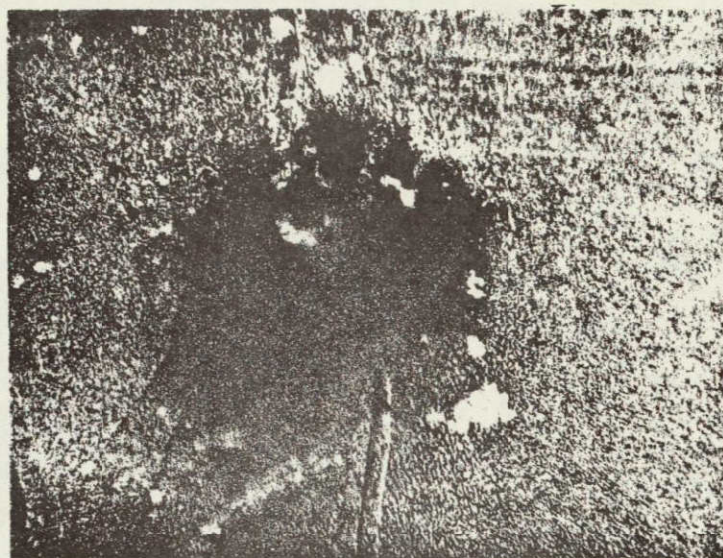


FIGURE 14

A Microscopic Photograph of a Typical Surface Inclusion  
in EFG Ribbon (50x Magnification)



removal of specific surface inclusions. This indicated that either there are microscopic particles that cannot be detected by eye or it may depend on the way that the particle is embedded in silicon matrix. For example, a particle might not cause any shunting problem if the particle is completely isolated by the coverage of a thin silicon layer all over the surface of the particle.

Selected solar cells from BSF process were coated with MLAR coating (instead of SiO<sub>2</sub> AR coating) to show the improvement of the performance. The results are given in the middle table of the Table 15. Although an average efficiency of about 10.6% was obtained, improvement in short circuit current after MLAR coating was only about 33%. (Generally close to 50% current gain after MLAR coating was achieved in single crystalline solar cell case.) This reduced coating gain could be the result of the haze remaining on the starting blanks. The figures quoted for highest efficiency can be characterized as "preliminary", because of limited tests, and small sample size.

Limited solar cells (Cell Nos. 1 through 4) were fabricated from the ribbons of chemically etched surface to check the performance difference between cells with and without etching step (the ribbons were chemically etched in planar solution for about two minutes, which



will remove about 10  $\mu\text{m}$  of silicon from each side of a ribbon). No significant difference in performance were observed (refer to data sheets in Appendix IV for detailed information). However, these solar cells showed slightly lower short current density than the solar cells without chemical etching. Reasons for this difference have not been identified yet.

### 3.2 Dark I-V Characteristics

Measurement techniques were described in previous Section A.3.2. Plots of the selected solar cells are given in Figure 15 for the standard process and Figure 16 for the BSF process. "A" factor and  $I_0$  in the diode equation (described in Section A.3.2) were in the range of 1.5-3 and  $10^{-7}$ - $10^{-6}$  A/cm<sup>2</sup>, respectively. These are slightly increased values compared with the "Silso" solar cells, and this result agrees with the slightly lower open circuit voltage and curve fill factor of EFG solar cells.

### 3.3 Spectral Response

Absolute spectral response (A/W) was measured using the same method described in Section A.3.3. Plots of the response are given in Figure 17 for the standard cells and in Figure 18 for the BSF cells. Spectral response of EFG cells at long wavelength ( $\lambda > 0.6 \mu\text{m}$ ) was significantly lower than those of the single crystalline control cells



FIGURE 15

Dark I-V Characteristics of EFG Solar Cells  
( $45.5\text{cm}^2$ , Standard Process) at R.T.

- : EFG Cells
- : A Control Cell (Single Crystalline)
- o: Cell No. 7
- x: Cell No. 14
- $\Delta$ : Control No. 70

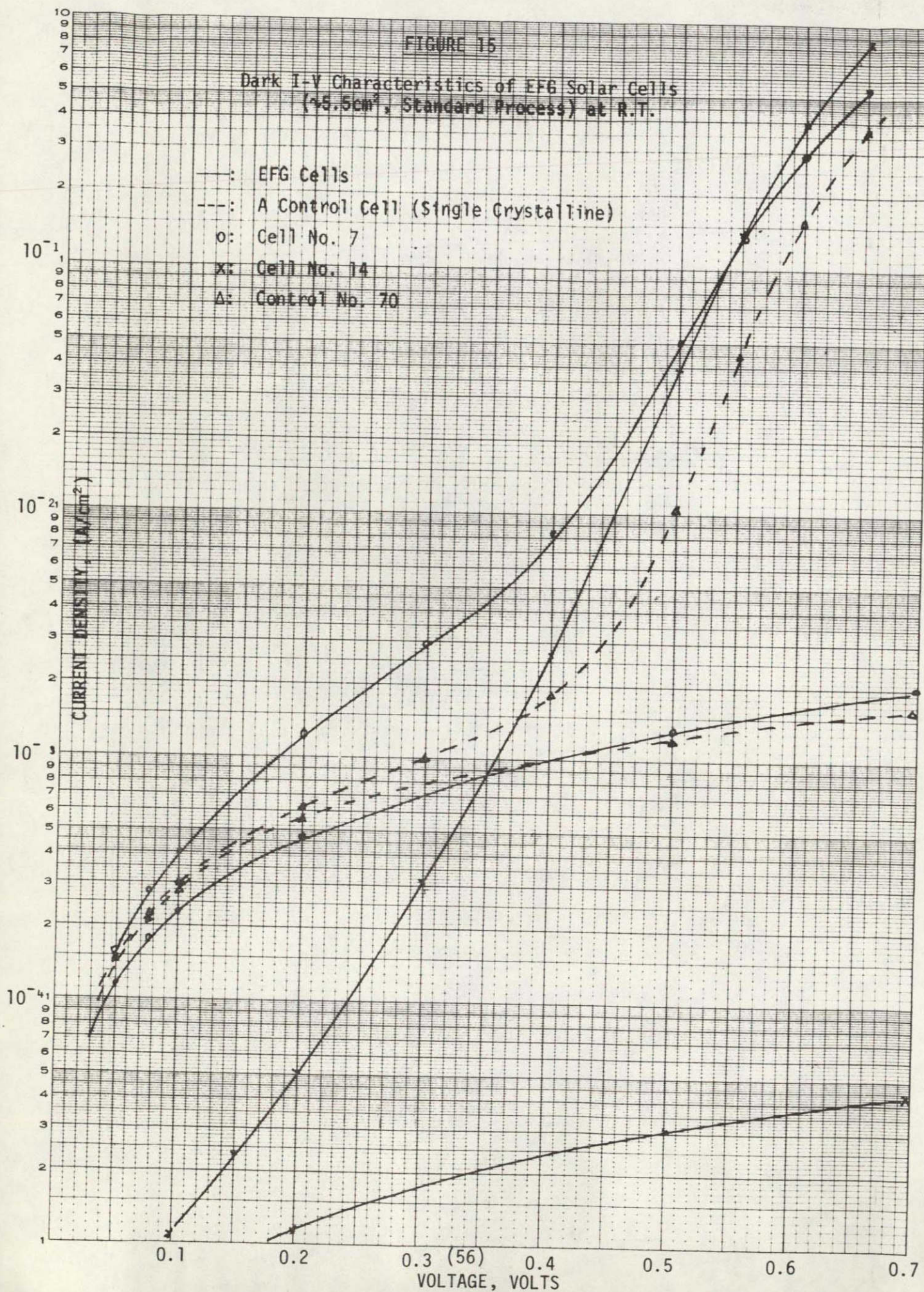




FIGURE 16

Dark I-V Characteristics of EFG Solar Cells  
( $\sim 5.5\text{cm}^2$ , BSP Process) at R.T.

x: Cell No. 50

o: Cell No. 29

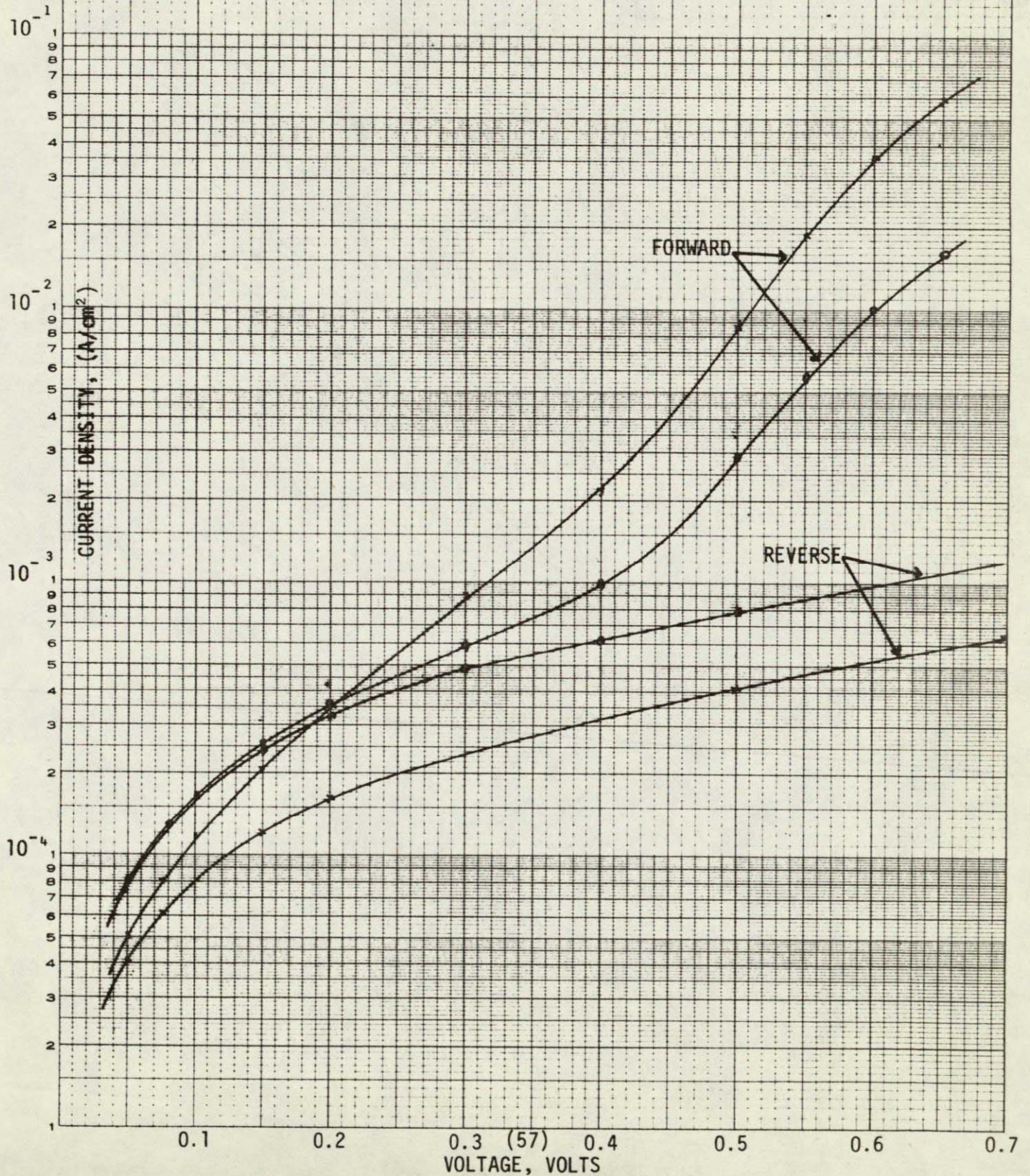




FIGURE 17

Spectral Response of EFG Solar Cells  
(Standard Process)

**OCLI** OPTICAL COATING  
LABORATORY, INC.

15251 E. DON JULIAN ROAD  
CITY OF INDUSTRY, CA 91746  
TELEPHONE (213) 968-6581

ABSOLUTE SPECTRAL  
RESPONSE

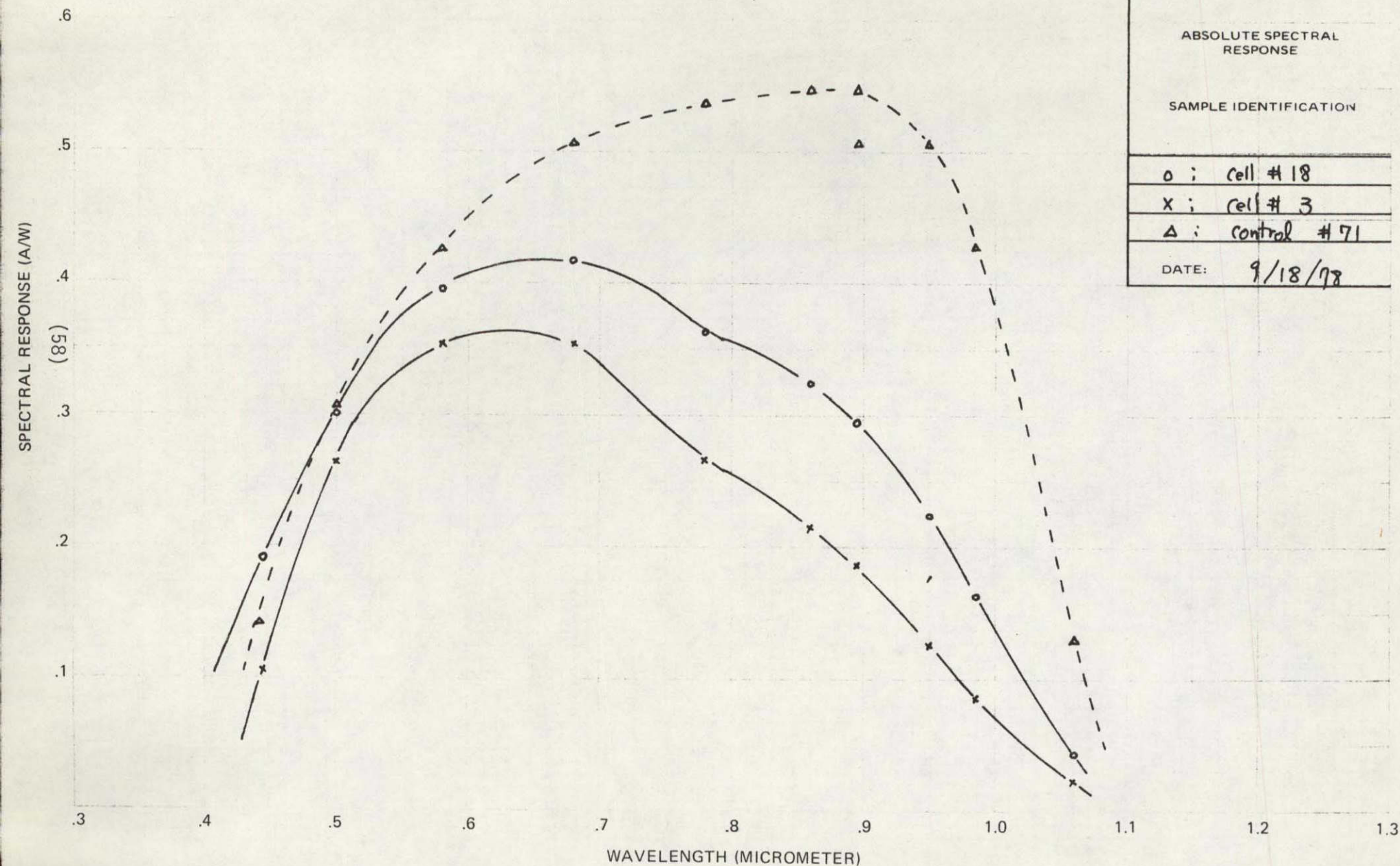
SAMPLE IDENTIFICATION

o : cell #18

x : cell #3

Δ : control #71

DATE: 9/18/78



due to crystalline defects such as grain boundary, stacking faults, dislocations and perhaps of inclusions. The slight dip at  $0.78\text{ }\mu\text{m}$  was observed for the both response figures and the origin of the dip is not known at the present time.

### 3.4 Minority Carrier Diffusion Length

Diffusion length was measured on the finished solar cells using the short circuit current method described in Section A.3.4. Table 16 summarizes the results of the EFG solar cells, from both standard and BSF process, measured under illumination of entire cell area, showing average diffusion length between 40 and  $50\text{ }\mu\text{m}$ .

Variation of diffusion length was also detected from small beam size measurement on two solar cells and Figure 19 show results of this, indicating significant variation from spot to spot; i.e. from 20 to  $50\text{ }\mu\text{m}$  in case (b). This variation in diffusion length can affect the overall carrier collection (current) obtained in the full active area of the cell.

TABLE 16

Minority Carrier Diffusion Length ( $\mu\text{m}$ ) of EFG Solar Cells

|               | AVERAGE | STANDARD<br>DEVIATION | RANGE |
|---------------|---------|-----------------------|-------|
| STANDARD CELL | 40      |                       | 38-41 |
| BSF CELLS     | 52      | 11                    | 40-65 |

NOTE: 1) Measured by  $I_{sc}$  method illuminated whole solar cell area ( $\sim 5.5\text{cm}^2$ ).

2) Samples:

Standard Cells: Nos. 7 and 18

BSF Cells: Nos. 29, 32, 40, 45, 49 and 55





### III. CONCLUSIONS AND RECOMMENDATIONS

These conclusions reached after processing of the Wacker "Silso" wafers and EFG ribbons are as follows.

#### Wacker "Silso" Wafer

- o Fabrication process for conventional single crystalline solar cell can easily be adapted to this type of sheets without causing any significant process problems, in yield, or in the need for complex (expensive) process steps, etc.
- o The average conversion efficiency of solar cells (2x2 cm) under AMO condition at 25°C was about 9.5%. The maximum achievable AMO efficiency (using optimum processing, assuming material unchanged) of a solar cell (2x2 cm) from this material is predicted to be in the range between 11% and 12%.
- o The results on this sheet measured from solar cell performance, spectral response, and diffusion length showed good qualitative correlation with the average grain size. There did not appear to be any major doping impurity influence, not unexpected since the sheets are reportedly prepared from highly pure starting silicon. A secondary impurity effect was the degradation caused by "inclusions"; these were found mostly in the large grain area (middle), showing that they were not influencing the regrowth mechanism but were probably stray particles included during the casting process.
- o The BSF process indicated no improvement of performance. this could possibly be ascribed to the relatively low diffusion length (<50  $\mu\text{m}$ ) observed in the starting and processed sheets.

- o The G.B. passivation test did not show any improvement. This does not rule out the chance of other G.B. passivation methods, but shows that there may not have been a preferential diffusion rate of phosphorus down G.B. at low temperature as required for the method used.
- o For both the BSF and the G.B. passivation process, it was noteworthy that there was also no deterioration of performance. This indicates good stability of grain behavior under fairly severe process changes.
- o Future improvements in cells made from Wacker "Silso" sheet appear to lie in the increased grain size within the sheet (especially near the edge), or another method of G.B. passivation. Elimination of inclusions by better control of casting process will improve the utilization of this silicon material.

#### EFG Ribbon

- o Warpage of the sheets and thickness variation within a sheet caused major problems in application of conventional solar cell process, especially in metallization and electrical test steps. However, with care screen printing type of metallization can possibly be applied successfully on this sheet (this is based on the experience in screen printing of Al paste in BSF process).
- o An average AMO efficiency of EFG solar cells (5-6 cm<sup>2</sup> in area) at 25°C was about 8-9%, which was a slightly lower efficiency than the "Silso" solar cells. Maximum achievable AMO efficiency of a solar cell (1" x 1" in area) from this sheet, using optimum process steps, is estimated to be around 12%.

- o The BSF process showed only slight improvement in  $I_{sc}$  and  $V_{oc}$ , probably because of the relatively low starting diffusion length and the high doping concentration ( $\sim 10^{16}$  Atoms/cm<sup>3</sup>).
- o Electrically the results were only moderately good, and this was correlated with the reduced average diffusion length and possible junction shunting problem caused by the inclusions from die material (the reduced  $V_{oc}$  and CFF were thought to be due to these inclusions). The inclusions appeared more severe on this batch of ribbons than has been observed on other ribbon samples, indicating perhaps a correctable variation in the ribbon growth techniques.
- o The localized areas of low diffusion length or low quality sheet will reduce one advantage of ribbon material, namely the ability to fabricate good single cells from relatively larger continuous areas of ribbon.

#### IV. WORK PLAN STATUS

Following unconventional silicon sheets are expected to process and evaluate during the next period.

- o RTR Ribbon
- o Dendritic Web
- o Cast Silicon by HEM

#### Additional Measurements

Equipment has been built to enable rapid measurement of dark forward log I-V plots, and one for fine light spot scanning of sample. This equipment will be used to aid in material evaluation; some samples from the Wacker and EFG groups will be included.



V. REFERENCES

- T. H. Distefano and J. J. Cuomo, "Enhancement of Carrier Lifetime in Polycrystalline Silicon", Proceeding Workshop on Low Cost Polycrystalline Silicon Solar Cells, Southern Methodist University, Texas, May, 1976.
2. E. D. Stokes and T. L. Chu, "Diffusion Lengths in Solar Cells From Short-Circuit Current Measurement", Applied Physics Letters, 30, 425, 1977.

APPENDIX I

TIME SCHEDULE

# TIME SCHEDULE

| TASK                       | MONTH |     |     |     |     |     |     |     |     |     |     |     |     |
|----------------------------|-------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
|                            | JUL   | AUG | SEP | OCT | NOV | DEC | JAN | FEB | MAR | APR | MAY | JUN | JUL |
| 1. PROCESS SHEET SAMPLES   |       |     |     |     |     |     |     |     |     |     |     |     |     |
| (a) 1/2 Samples → Cells    |       |     |     |     |     |     |     |     |     |     |     |     |     |
| (b) Analysis               |       |     |     |     |     |     |     |     |     |     |     |     |     |
| (c) Back Up Measurements   |       |     |     |     |     |     |     |     |     |     |     |     |     |
| (d) Test Alternate Process |       |     |     |     |     |     |     |     |     |     |     |     |     |
| 2. REPORTS                 |       |     |     |     |     |     |     |     |     |     |     |     |     |
| (a) Monthly                |       | ▲   | ▲   |     | Δ   | Δ   |     | Δ   | Δ   |     | Δ   | Δ   |     |
| (b) Quarterly              |       |     |     | ▲   |     |     |     |     |     | Δ   |     |     |     |
| (c) Semi-Annual            |       |     |     |     |     |     | Δ   |     |     |     |     |     |     |
| (d) Final                  |       |     |     |     |     |     |     |     |     |     |     |     | Δ   |
| 3. INTEGRATION MEETING     |       |     |     |     |     |     |     |     |     |     |     |     |     |

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## APPENDIX II

OCLI AMO SOLAR SIMULATOR

The OCLI AMO Simulator is described under three headings; the light sources and calibration, the cell holding fixtures and the readout equipment.

(a) Light Sources and Calibration

The AMO spectrum is simulated by two separate sources.

- o The blue portion of the spectrum is obtained from a xenon arc lamp with an absorption filter which attenuates the large energy spikes in the near IR region.
- o The red portion of the spectrum is due to a tungsten lamp set at 2800°K color temperature with suitable filters to blend with the blue portion of the spectrum, resulting in close approximation to the AMO spectrum. Figure 1 shows the Johnson AMO spectrum (approximates closely to the Thekaekara spectrum) and also the output of the OCLI Simulator. Also shown are the separate xenon (blue) and tungsten (red) contributions.

The two light sources do not provide collimated light, the cell test plane is placed at the plane of correct convergence; the uniformity across this plane is  $\pm 2\%$  for areas up to 8 cm<sup>2</sup>. The deviation of the centerline of each light source from perpendicular is around 11°.

In addition to allowing cell characterization under the AMO spectrum, this simulator has an added advantage for cell evaluation. By use of suitable blocking shields, either the blue or the red spectral output shown in Figure 1 can be used to illuminate the cell. Analysis of the absolute output under



these two filters can provide a rapid indication of the process control achieved on the cell. Experience has provided guidelines for "typical" readings in these two broadband regions for a variety of cells [including intentional variations in the silicon resistivity, diffusion conditions, surface finish, contact area coverage and whether or not the cell surface has an AR coating]. Thus evaluation of the blue response can indicate the performance of a given diffusion schedule with a given resistivity silicon, and can also check the effectiveness of an AR coating. The red response can also indicate whether the final bulk output is as expected, and can thus be used to assess the minority carrier diffusion length (D.L.) achieved. Although separate methods (surface or bulk photovoltage) are used for diffusion length measurement, this broadband check is most valuable to indicate the possible range of the diffusion length. For low diffusion length values, the red response decreases and crosses over the blue response for D.L.  $\sim 10 \mu\text{m}$ . Thus the red response data are most useful for scanning a larger number of samples, and can then be related to more precise D.L.-values obtained by more detailed (separate) measurements.

### Calibration

When first constructed the AMO Simulators were calibrated by a set of standard cells which were calibrated regularly on Table Mountain by measuring the solar spectrum incident there, and by adjusting for the measured absorption band in the spectrum, extrapolating to AMO readings. Since then, it has become common

practice to use balloon-flown and recovered standard cells to set the AM0 simulator intensity, and OCLI follows this practice using either OCLI-BF cells or those supplied by customers.

(b) Cell Holding Fixture

A variety of fixtures are used, depending on the size of the cell; if the cells are very fragile (thin or stressed slices) or the contacts are wraparound, a special fixture is used.

All these fixtures include a block which is controlled at pre-set temperatures by water pumped by a thermostatically controlled water bath, with feedback from a thermocouple embedded in the test block. These blocks also have vacuum hold-down facility, and contain voltage and current probes for measurement of cell electrical output.

(c) Read-Out Equipment

The simulator has a digital meter, reading selected parameter  $V_{oc}$ ,  $I_{sc}$  and the current at pre-set voltage levels. In addition, digital print out of these values plus up to three other load voltage readings are available.

Finally for development purposes, the I-V curves can be traced and from these maximum power, CFF and efficiency values can be estimated.

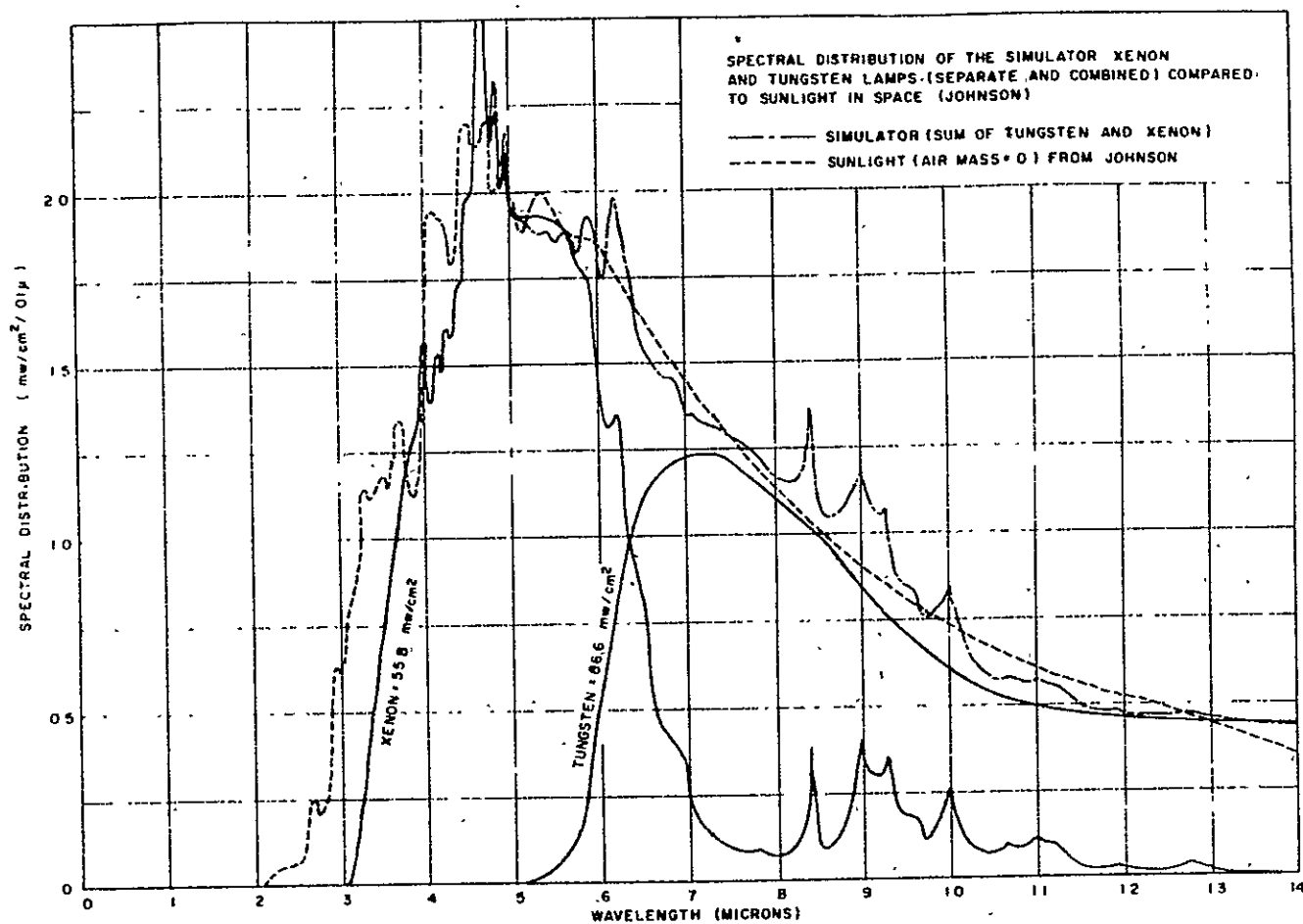


FIGURE 1

Spectral Distribution of the Simulator Xenon and Tungsten Lamps (Separate and Combined) Compared to Sunlight in Space (Johnson)

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### APPENDIX III

ELECTRICAL DATA SHEETS FOR "SILSO" SOLAR CELL

# SOLAR CELL ELECTRICAL DATA

CELL DESCRIPTION: Solar Cells (2x2 cm) from Wacker Wafers (A, B, C, D), standard Process  
 TEST CONDITION: NO A.R. Coating,  $\approx 90\%$  active Area.  
 TEMPERATURE: AMO 25°C DATE: 6/26/78

| NO. | V <sub>OC</sub> | I <sub>SC</sub> | I <sub>SCB</sub> | I <sub>SCR</sub> | I <sub>Max</sub> | V <sub>Max</sub> | P <sub>Max</sub> | CFF  | $\eta$ |
|-----|-----------------|-----------------|------------------|------------------|------------------|------------------|------------------|------|--------|
|     | mV              | mA              | mA               | mA               | mA               | mV               | mW               | %    | %      |
| A1  | 523             | 87              | 37               | 50               | 80               | 375              | 30               | 60.1 | 5.6    |
| A3  | 526             | 91              | 37               | 53               | 84               | 385              | 32.3             | 67.6 | 6.0    |
| A4  | 530             | 90              | 37               | 53               | 83               | 390              | 32.4             | 67.9 | 6.0    |
| A6  | 512             | 91              | 38               | 53               | 74               | 382              | 28.3             | 60.7 | 5.2    |
| A7  | 537             | 92              | 38               | 54               | 85               | 400              | 34.0             | 68.8 | 6.3    |
| A8  | 524             | 92              | 37               | 54               | 78               | 388              | 30.3             | 62.8 | 5.6    |
| A9  | 528             | 90              | 37               | 53               | 82               | 388              | 31.8             | 67.0 | 5.9    |
| A10 | 456             | 89              | 37               | 52               | 60               | 290              | 17.4             | 42.9 | 3.2    |
| A11 | 532             | 93              | 38               | 55               | 86               | 400              | 34.4             | 69.5 | 6.4    |
| A13 | 526             | 90              | 37               | 52               | 82               | 381              | 31.2             | 66.0 | 5.8    |
| A14 | 532             | 91              | 37               | 54               | 82               | 405              | 33.2             | 68.6 | 6.2    |
| A15 | 528             | 93              | 37               | 55               | 82               | 406              | 33.3             | 67.8 | 6.2    |
| A16 | 514             | 90              | 37               | 52               | 75               | 390              | 29.3             | 63.2 | 5.4    |
| B1  | 525             | 88              | 37               | 50               | 80               | 385              | 30.8             | 66.7 | 5.7    |
| B2  | 523             | 91              | 37               | 53               | 83               | 380              | 31.5             | 66.3 | 5.8    |
| B3  | 496             | 92              | 37               | 54               | 70               | 375              | 26.3             | 57.5 | 4.9    |
| B4  | 528             | 92              | 37               | 54               | 84               | 395              | 33.2             | 68.3 | 6.1    |

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# SOLAR CELL ELECTRICAL DATA

CELL DESCRIPTION: Solar Cells (2x2 cm) from Wacker Wafers (A, B, C, D), Standard Process  
NO A.R. coating,  $\approx 90\%$  active area  
 TEST CONDITION: AMO  
 TEMPERATURE: 25°C DATE: 6/26/78

| NO. | V <sub>OC</sub> | I <sub>SC</sub> | I <sub>SCB</sub> | I <sub>SCR</sub> | I <sub>Max</sub> | V <sub>Max</sub> | P <sub>Max</sub> | CFF  | $\eta$ |
|-----|-----------------|-----------------|------------------|------------------|------------------|------------------|------------------|------|--------|
|     | mV              | mA              | mA               | mA               | mA               | mV               | mW               | %    | %      |
| B5  | 523             | 89              | 37               | 52               | 81               | 395              | 32.0             | 68.7 | 5.9    |
| B6  | 531             | 92              | 37               | 55               | 85               | 406              | 34.5             | 70.6 | 6.4    |
| B7  | 532             | 93              | 37               | 56               | 85               | 408              | 34.7             | 70.1 | 6.4    |
| B9  | 519             | 92              | 38               | 54               | 85               | 388              | 33.0             | 69.1 | 6.1    |
| B10 | 526             | 96              | 39               | 56               | 89               | 395              | 35.2             | 69.6 | 6.5    |
| B11 | 522             | 95              | 39               | 55               | 80               | 375              | 30.0             | 60.5 | 5.6    |
| B12 | 523             | 96              | 39               | 57               | 88               | 390              | 34.3             | 68.4 | 6.4    |
| B13 | 521             | 92              | 38               | 53               | 84               | 378              | 31.8             | 66.2 | 5.9    |
| B14 | 522             | 94              | 39               | 55               | 88               | 380              | 33.4             | 68.2 | 6.2    |
| B15 | 527             | 95              | 39               | 56               | 87               | 392              | 34.1             | 68.8 | 6.3    |
| B16 | 526             | 94              | 39               | 55               | 86               | 387              | 33.3             | 67.3 | 6.2    |
| C1  | 529             | 91              | 39               | 52               | 82               | 400              | 32.8             | 68.1 | 6.1    |
| C2  | 529             | 93              | 39               | 54               | 84               | 400              | 33.6             | 68.3 | 6.2    |
| C3  | 534             | 94              | 39               | 55               | 84               | 395              | 33.2             | 66.1 | 6.1    |
| C4  | 533             | 93              | 39               | 54               | 85               | 400              | 34.0             | 68.6 | 6.3    |
| C5  | 528             | 92              | 38               | 53               | 85               | 395              | 33.6             | 69.1 | 6.2    |
| C7  | 541             | 97              | 40               | 57               | 89               | 420              | 37.4             | 71.1 | 6.9    |



# SOLAR CELL ELECTRICAL DATA

CELL DESCRIPTION: Solar cells (2x2 cm) from Wacker Waters (A,B,C,D), Standard Process  
No. A.R. coating, ~90% active area  
 TEST CONDITION: AMO  
 TEMPERATURE: 25°C DATE: 6/26/78

| NO. | V <sub>OC</sub> | I <sub>SC</sub> | I <sub>SCB</sub> | I <sub>SCR</sub> | I <sub>Max</sub> | V <sub>Max</sub> | P <sub>Max</sub> | CFF  | η   |
|-----|-----------------|-----------------|------------------|------------------|------------------|------------------|------------------|------|-----|
|     | mV              | mA              | mA               | mA               | mA               | mV               | mW               | %    | %   |
| C8  | 534             | 95              | 39               | 56               | 86               | 410              | 35.3             | 69.5 | 6.5 |
| C9  | 527             | 95              | 39               | 55               | 87               | 395              | 34.4             | 68.6 | 6.4 |
| C10 | 539             | 97              | 40               | 57               | 90               | 417              | 37.5             | 71.8 | 6.9 |
| C14 | 534             | 95              | 39               | 56               | 87               | 395              | 34.4             | 67.7 | 6.4 |
| C15 | 534             | 96              | 39               | 56               | 86               | 390              | 33.5             | 65.4 | 6.2 |
| C16 | 531             | 94              | 39               | 55               | 85               | 405              | 34.4             | 69.0 | 6.4 |
| D1  | 528             | 94              | 41               | 53               | 86               | 385              | 33.1             | 66.7 | 6.1 |
| D2  | 528             | 96              | 41               | 54               | 88               | 390              | 34.3             | 67.7 | 6.4 |
| D3  | 529             | 96              | 41               | 55               | 87               | 395              | 34.4             | 67.7 | 6.4 |
| D4  | 529             | 94              | 41               | 53               | 86               | 390              | 33.5             | 67.4 | 6.2 |
| D5  | 529             | 96              | 41               | 54               | 83               | 400              | 33.2             | 65.4 | 6.1 |
| D6  | 545             | 97              | 41               | 55               | 90               | 420              | 37.8             | 71.5 | 7.0 |
| D8  | 535             | 97              | 41               | 56               | 89               | 410              | 36.5             | 70.3 | 6.8 |
| D9  | 524             | 96              | 41               | 55               | 87               | 390              | 33.9             | 67.4 | 6.3 |
| D10 | 537             | 98              | 41               | 56               | 90               | 402              | 36.2             | 68.7 | 6.7 |
| D11 | 455             | 94              | 40               | 53               | 61               | 290              | 17.7             | 41.4 | 3.3 |
| D14 | 534             | 97              | 41               | 55               | 88               | 397              | 34.9             | 67.4 | 6.5 |

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### SOLAR CELL ELECTRICAL DATA

CELL DESCRIPTION: Solar cells (2x2 cm) from Wacker Wafers (A, B, C, D), standard process.

TEST CONDITION:

TEMPERATURE:

No. A.R. Coating

$\approx 90\%$

active area

AMO

25°C

DATE:

6 / 26 / 78

[illegible]

# SOLAR CELL ELECTRICAL DATA

CELL DESCRIPTION: Wacker Solar cells (2x2 cm) standard Process  
SiO<sub>2</sub> A.R. coating ≈ 90 % active area  
 TEST CONDITION: AMO  
 TEMPERATURE: 25°C DATE: 6/27/78

| NO. | V <sub>OC</sub> | I <sub>SC</sub> | I <sub>SCB</sub> | I <sub>SCR</sub> | I <sub>Max</sub> | V <sub>Max</sub> | P <sub>Max</sub> | CFF  | n   |
|-----|-----------------|-----------------|------------------|------------------|------------------|------------------|------------------|------|-----|
|     | mV              | mA              | mA               | mA               | mA               | mV               | mW               | %    | %   |
| A1  | 528             | 117             | 47               | 70               | 105              | 365              | 38.3             | 62.2 | 7.1 |
| A3  | 529             | 124             | 52               | 72               | 113              | 380              | 42.9             | 65.7 | 8.0 |
| A4  | 533             | 123             | 51               | 72               | 113              | 380              | 42.9             | 65.7 | 8.0 |
| A6  | 526             | 124             | 52               | 72               | 103              | 385              | 39.7             | 60.9 | 7.4 |
| A7  | 543             | 125             | 52               | 73               | 116              | 400              | 46.4             | 68.1 | 8.6 |
| A8  | 530             | 126             | 53               | 73               | 108              | 390              | 42.1             | 63.3 | 7.8 |
| A9  | 531             | 122             | 50               | 72               | 111              | 385              | 42.7             | 66   | 7.9 |
| A10 | 476             | 119             | 47               | 71               | 82               | 315              | 25.8             | 45.6 | 4.8 |
| A11 | 535             | 124             | 49               | 75               | 114              | 395              | 45.0             | 67.9 | 8.3 |
| A13 | 527             | 119             | 48               | 71               | 108              | 380              | 41.0             | 65.3 | 7.6 |
| A14 | 538             | 126             | 52               | 74               | 114              | 395              | 45.0             | 67.9 | 8.3 |
| A15 | 534             | 127             | 52               | 75               | 114              | 395              | 45.0             | 67.9 | 8.3 |
| A16 | 524             | 124             | 53               | 71               | 107              | 390              | 41.7             | 64.2 | 7.7 |
| B1  | 531             | 119             | 48               | 70               | 107              | 380              | 40.7             | 64.4 | 7.5 |
| B2  | 526             | 124             | 51               | 73               | 114              | 390              | 42.2             | 64.9 | 7.8 |
| B3  | 513             | 125             | 53               | 72               | 105              | 380              | 39.9             | 62.2 | 7.4 |
| B4  | 536             | 122             | 48               | 74               | 112              | 395              | 44.2             | 67.5 | 8.2 |

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# SOLAR CELL ELECTRICAL DATA

CELL DESCRIPTION: Wacker Solar Cells (2x2 cm) standard process  
SiO<sub>2</sub> A.R. Coating, a 90 (%) active area  
 TEST CONDITION: AM0  
 TEMPERATURE: 25°C DATE: 6/27/98

| NO. | V <sub>OC</sub> | I <sub>SC</sub> | I <sub>SCB</sub> | I <sub>SCR</sub> | I <sub>Max</sub> | V <sub>Max</sub> | P <sub>Max</sub> | CFF  | η   |
|-----|-----------------|-----------------|------------------|------------------|------------------|------------------|------------------|------|-----|
|     | mV              | mA              | mA               | mA               | mA               | mV               | mW               | %    | %   |
| B5  | 528             | 120             | 48               | 72               | 110              | 390              | 42.9             | 67.4 | 7.9 |
| B6  | 537             | 123             | 49               | 74               | 113              | 405              | 45.8             | 69.2 | 8.5 |
| B7  | 535             | 126             | 50               | 76               | 116              | 405              | 47.0             | 69.7 | 8.7 |
| B9  | 528             | 122             | 48               | 74               | 112              | 395              | 44.2             | 68.8 | 8.2 |
| B10 | 530             | 124             | 47               | 77               | 113              | 400              | 45.2             | 68.9 | 8.4 |
| B11 | 529             | 124             | 50               | 74               | 105              | 380              | 39.9             | 61.1 | 7.4 |
| B12 | 520             | 127             | 51               | 76               | 113              | 390              | 44.1             | 66.7 | 8.2 |
| B13 | 520             | 124             | 52               | 72               | 113              | 370              | 41.8             | 64.8 | 7.7 |
| B14 | 521             | 124             | 48               | 76               | 115              | 385              | 44.3             | 68.5 | 8.2 |
| B15 | 531             | 127             | 51               | 76               | 117              | 390              | 45.6             | 67.5 | 8.5 |
| B16 | 531             | 123             | 49               | 74               | 112              | 390              | 43.7             | 66.8 | 8.1 |
| C1  | 538             | 116             | 46               | 70               | 112              | 395              | 44.2             | 70.6 | 8.2 |
| C2  | 537             | 120             | 47               | 73               | 112              | 400              | 44.8             | 69.3 | 8.3 |
| C3  | 545             | 123             | 48               | 75               | 112              | 400              | 44.8             | 67.1 | 8.3 |
| C4  | 536             | 124             | 50               | 74               | 106              | 410              | 43.5             | 65.7 | 8.1 |
| C5  | 535             | 121             | 48               | 73               | 112              | 395              | 44.2             | 68.3 | 8.2 |
| C6  | 547             | 128             | 51               | 77               | 118              | 420              | 49.6             | 70.9 | 9.2 |

# SOLAR CELL ELECTRICAL DATA

CELL DESCRIPTION: Wacker Solar Cells (2x2 cm) standard Process  
S<sub>2</sub>O A.R Coating, ≈ 90 (%) active area  
 TEST CONDITION: AM 0  
 TEMPERATURE: 25°C DATE: 6/27/78

| NO. | V <sub>OC</sub> | I <sub>SC</sub> | I <sub>SCB</sub> | I <sub>SCR</sub> | I <sub>Max</sub> | V <sub>Max</sub> | P <sub>Max</sub> | CFF  | η   |
|-----|-----------------|-----------------|------------------|------------------|------------------|------------------|------------------|------|-----|
|     | mV              | mA              | mA               | mA               | mA               | mV               | mW               | %    | %   |
| C8  | 544             | 128             | 54               | 74               | 117              | 415              | 48.6             | 69.6 | 9.0 |
| C9  | 534             | 128             | 53               | 75               | 117              | 400              | 46.8             | 68.5 | 8.7 |
| C10 | 549             | 128             | 49               | 78               | 118              | 420              | 49.6             | 70.9 | 9.2 |
| C14 | 538             | 126             | 50               | 76               | 114              | 395              | 45.0             | 66.3 | 8.3 |
| C15 | 546             | 125             | 48               | 77               | 115              | 400              | 46.0             | 67.4 | 8.5 |
| C16 | 542             | 124             | 49               | 75               | 115              | 405              | 46.6             | 69.1 | 8.6 |
| D1  | 533             | 123             | 51               | 71               | 110              | 390              | 42.9             | 65.7 | 7.9 |
| D2  | 532             | 125             | 53               | 73               | 115              | 390              | 44.9             | 67.3 | 8.3 |
| D3  | 534             | 120             | 46               | 74               | 109              | 385              | 42.0             | 65.3 | 7.8 |
| D4  | 534             | 120             | 47               | 72               | 109              | 385              | 42.0             | 65.4 | 7.8 |
| D5  | 544             | 124             | 50               | 74               | 113              | 410              | 46.3             | 68.7 | 8.6 |
| D6  | 555             | 125             | 50               | 75               | 117              | 430              | 50.3             | 72.5 | 9.3 |
| D8  | 546             | 124             | 48               | 75               | 113              | 420              | 47.5             | 70.4 | 8.8 |
| D9  | 532             | 126             | 51               | 75               | 114              | 395              | 45.0             | 67.0 | 8.3 |
| D10 | 544             | 130             | 53               | 76               | 119              | 410              | 48.8             | 69.1 | 9.0 |
| D11 | 493             | 117             | 44               | 72               | 80               | 330              | 26.4             | 45.9 | 4.9 |
| D14 | 542             | 122             | 47               | 75               | 110              | 405              | 44.6             | 67.5 | 8.3 |

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## SOLAR CELL ELECTRICAL DATA

CELL DESCRIPTION: Wacker Solar Cells (2x2 in) Standard Process  
SiO<sub>2</sub> A.R coating ≈ 90 (%) active area  
 TEST CONDITION: AMO  
 TEMPERATURE: 25°C DATE: 6/27/78

[illegible]



# SOLAR CELL ELECTRICAL DATA

CELL DESCRIPTION: Control solar cells (2x2 cm) Wacker Standard Process (Wafer A, B, C, D)  
 TEST CONDITION: No A.R coating, ± 90 % active area  
 TEMPERATURE: AM0  
25°C DATE: 6/26/78

| NO. | V <sub>OC</sub> | I <sub>SC</sub> | I <sub>SCB</sub> | I <sub>SCR</sub> | I <sub>Max</sub> | V <sub>Max</sub> | P <sub>Max</sub> | CFF  | η   |
|-----|-----------------|-----------------|------------------|------------------|------------------|------------------|------------------|------|-----|
|     | mV              | mA              | mA               | mA               | mA               | mV               | mW               | %    | %   |
| 1   | 553             | 100             | 40               | 60               | 92               | 435              | 40               | 72.4 | 7.4 |
| 2   | 544             | 101             | 40               | 61               | 93               | 428              | 39.8             | 72.4 | 7.4 |
| 3   | 552             | 100             | 40               | 61               | 89               | 440              | 39.2             | 70.9 | 7.3 |
| 4   | 548             | 101             | 40               | 61               | 93               | 425              | 39.5             | 71.4 | 7.3 |
| 5   | 539             | 101             | 40               | 62               | 94               | 427              | 40.1             | 73.7 | 7.4 |
| 6   | 542             | 101             | 39               | 61               | 94               | 425              | 40.              | 73.0 | 7.4 |
| 7   | 544             | 105             | 42               | 63               | 98               | 430              | 42.1             | 73.8 | 7.8 |
| 8   | 540             | 105             | 42               | 63               | 98               | 426              | 41.7             | 73.6 | 7.7 |
| 9   | 543             | 102             | 41               | 61               | 94               | 427              | 40.1             | 72.5 | 7.4 |
| 10  | 544             | 108             | 44               | 65               | 98               | 425              | 41.7             | 70.9 | 7.7 |
|     |                 |                 |                  |                  |                  |                  |                  |      |     |
|     |                 |                 |                  |                  |                  |                  |                  |      |     |
|     |                 |                 |                  |                  |                  |                  |                  |      |     |
|     |                 |                 |                  |                  |                  |                  |                  |      |     |
|     |                 |                 |                  |                  |                  |                  |                  |      |     |
|     |                 |                 |                  |                  |                  |                  |                  |      |     |
|     |                 |                 |                  |                  |                  |                  |                  |      |     |
|     |                 |                 |                  |                  |                  |                  |                  |      |     |
|     |                 |                 |                  |                  |                  |                  |                  |      |     |
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## SOLAR CELL ELECTRICAL DATA

|                   |                               |                         |
|-------------------|-------------------------------|-------------------------|
| CELL DESCRIPTION: | Control Solar cells (2x2 cm)  | Wacker standard process |
| TEST CONDITION:   | SiO <sub>2</sub> A.R. coating | ~90 % active area       |
| TEMPERATURE:      | AM0<br>25 °C                  | DATE: 6/27/78           |

[illegible]

# SOLAR CELL ELECTRICAL DATA

CELL DESCRIPTION: Solar cells (2x2 cm) from Wacker wafer (J), Standard Process (Modified)  
No A.R coating,  $\approx 90\%$  active area  
 TEST CONDITION: AMO  
 TEMPERATURE: 25 °C DATE: 8/18/78

| NO. | V <sub>OC</sub> | I <sub>SC</sub> | I <sub>SCB</sub> | I <sub>SCR</sub> | I <sub>Max</sub> | V <sub>Max</sub> | P <sub>Max</sub> | CFF  | $\eta$ |
|-----|-----------------|-----------------|------------------|------------------|------------------|------------------|------------------|------|--------|
|     | mV              | mA              | mA               | mA               | mA               | mV               | mW               | %    | %      |
| J2  | 539             | 85              |                  |                  | 78               | 445              | 34.7             | 75.8 | 6.4    |
| J3  | 540             | 87              |                  |                  | 76               | 445              | 33.8             | 72.0 | 6.3    |
| J5  | 540             | 87              |                  |                  | 80               | 450              | 36.0             | 76.6 | 6.7    |
| J7  | 555             | 92              |                  |                  | 83               | 460              | 38.2             | 74.8 | 7.1    |
| J8  | 553             | 89              |                  |                  | 83               | 465              | 38.6             | 78.4 | 7.1    |
| J9  | 543             | 87              |                  |                  | 80               | 450              | 36.0             | 76.2 | 6.7    |
| J10 | 558             | 91              |                  |                  | 84               | 470              | 39.5             | 77.8 | 7.3    |
| J11 | 555             | 90              |                  |                  | 85               | 465              | 39.5             | 79.1 | 7.3    |
| J13 | 545             | 87              |                  |                  | 81               | 451              | 36.5             | 77.1 | 6.8    |
| J14 | 555             | 91              |                  |                  | 85               | 465              | 39.5             | 78.3 | 7.3    |
| J15 | 555             | 91              |                  |                  | 85               | 465              | 39.5             | 78.3 | 7.3    |
|     |                 |                 |                  |                  |                  |                  |                  |      |        |
|     |                 |                 |                  |                  |                  |                  |                  |      |        |
|     |                 |                 |                  |                  |                  |                  |                  |      |        |
|     |                 |                 |                  |                  |                  |                  |                  |      |        |
|     |                 |                 |                  |                  |                  |                  |                  |      |        |
|     |                 |                 |                  |                  |                  |                  |                  |      |        |
|     |                 |                 |                  |                  |                  |                  |                  |      |        |
|     |                 |                 |                  |                  |                  |                  |                  |      |        |

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### SOLAR CELL ELECTRICAL DATA

CELL DESCRIPTION: Solar cell, (2x2 cm) from Wacker wafer (J) Standard Process (modified)  
TEST CONDITION:  $\text{SiO}_2$  A.R coating,  $\approx 90\%$  active area  
TEMPERATURE: AMO  
 $25^\circ\text{C}$  DATE: 8/21/78

TEST CONDITION:

TEMPERATURE:

DATE: 8/21/78

[illegible]

# SOLAR CELL ELECTRICAL DATA

CELL DESCRIPTION: Control Solar cells (2x2 cm) Wacker (J) standard process (Modified)  
S<sub>2</sub>O<sub>2</sub> A.R. coating, ± 90 % active area  
 TEST CONDITION: AM0  
 TEMPERATURE: 25 °C DATE: 8/21/78

| NO. | V <sub>OC</sub>                              | I <sub>SC</sub> | I <sub>SCB</sub>                                     | I <sub>SCR</sub> | I <sub>Max</sub> | V <sub>Max</sub> | P <sub>Max</sub> | CFF    | η     |
|-----|----------------------------------------------|-----------------|------------------------------------------------------|------------------|------------------|------------------|------------------|--------|-------|
|     | mV                                           | mA              | mA                                                   | mA               | mA               | mV               | mW               | %      | %     |
| 41  | 595                                          | 131             | 48                                                   | 83               | 122              | 496              | 60.5             | 77.8   | 11.2  |
|     | (588)                                        | (95)            |                                                      |                  | (88)             | (505)            | (44.4)           | (79.6) | (8.2) |
| 42  | 593                                          | 132             | 49                                                   | 84               | 122              | 496              | 60.5             | 77.5   | 11.2  |
|     | (586)                                        | (96)            |                                                      |                  | (88)             | (505)            | (44.4)           | (79.0) | (8.2) |
| 43  | 591                                          | 132             | 50                                                   | 82               | 120              | 500              | 60.              | 76.9   | 11.1  |
|     | (584)                                        | (97)            |                                                      |                  | (87)             | (495)            | (43.1)           | (76.0) | (8.0) |
| 44  | 593                                          | 131             | 50                                                   | 81               | 121              | 506              | 61.2             | 78.6   | 11.3  |
|     | (586)                                        | (96)            |                                                      |                  | (88)             | (505)            | (44.4)           | (79)   | (8.2) |
|     |                                              |                 | Following cell # 46, 47, 48 are second control group |                  |                  |                  |                  |        |       |
| 46  | 600                                          | 131             | 49                                                   | 82               | 123              | 511              | 62.9             | 79.9   | 11.6  |
|     | (592)                                        | (95)            |                                                      |                  | (89)             | (505)            | (45.0)           | (79.9) | (8.3) |
| 47  | 597                                          | 133             | 49                                                   | 84               | 124              | 510              | 63.2             | 79.8   | 11.7  |
|     | (590)                                        | (97)            |                                                      |                  | (90)             | (505)            | (45.5)           | (79.4) | (8.4) |
| 48  | 596                                          | 132             | 49                                                   | 84               | 123              | 510              | 62.7             | 79.7   | 11.6  |
|     | (589)                                        | (97)            |                                                      |                  | (87)             | (505)            | (43.9)           | (76.9) | (8.1) |
| ※   | Parenthesis Numbers for before A.R. coating. |                 |                                                      |                  |                  |                  |                  |        |       |

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# SOLAR CELL ELECTRICAL DATA

CELL DESCRIPTION: Solar cells (2x2 cm) from Wacker Wafer (E, F), BSF process  
 TEST CONDITION: No A.R coating, ± 90 % active area  
 TEMPERATURE: AM0  
25°C DATE: 7/26/78

| NO. | V <sub>OC</sub> | I <sub>SC</sub> | I <sub>SCB</sub> | I <sub>SCR</sub> | I <sub>Max</sub> | V <sub>Max</sub> | P <sub>Max</sub> | CFF  | η   |
|-----|-----------------|-----------------|------------------|------------------|------------------|------------------|------------------|------|-----|
|     | mV              | mA              | mA               | mA               | mA               | mV               | mW               | %    | %   |
| E1  | 521             | 85              |                  |                  | 75               | 422              | 31.7             | 71.5 | 5.9 |
| E2  | 530             | 87              |                  |                  | 79               | 435              | 34.4             | 74.5 | 6.4 |
| E4  | 530             | 89              |                  |                  | 82               | 440              | 36.1             | 76.5 | 6.7 |
| E5  | 531             | 88              |                  |                  | 78               | 440              | 34.3             | 73.4 | 6.4 |
| E6  | 543             | 93              |                  |                  | 83               | 455              | 37.8             | 74.8 | 7.0 |
| E7  | 543             | 95              |                  |                  | 85               | 455              | 38.7             | 75.0 | 7.2 |
| E8  | 536             | 92              |                  |                  | 78               | 440              | 34.3             | 69.6 | 6.4 |
| E11 | 542             | 91              |                  |                  | 82               | 450              | 36.9             | 74.8 | 6.8 |
| E12 | 547             | 94              |                  |                  | 84               | 455              | 38.2             | 74.3 | 7.1 |
| E13 | 525             | 87              |                  |                  | 75               | 435              | 32.6             | 71.4 | 6.0 |
| E14 | 542             | 92              |                  |                  | 85               | 450              | 38.3             | 76.7 | 7.1 |
| E15 | 545             | 93              |                  |                  | 85               | 456              | 38.8             | 76.5 | 7.2 |
| F1  | 518             | 85              |                  |                  | 72               | 425              | 30.6             | 69.5 | 5.7 |
| F2  | 530             | 89              |                  |                  | 79               | 445              | 35.2             | 74.5 | 6.5 |
| F3  | 530             | 89              |                  |                  | 79               | 440              | 34.8             | 73.7 | 6.4 |
| F5  | 527             | 88              |                  |                  | 79               | 445              | 35.2             | 75.8 | 6.5 |
| F6  | 536             | 92              |                  |                  | 80               | 447              | 35.8             | 72.5 | 6.6 |



### SOLAR CELL ELECTRICAL DATA

CELL DESCRIPTION: Solar cells (2x2 cm) from Wacker Wafer (E, F), BSF process

TEST CONDITION NO A.R Coating,  $\approx 90\%$  active area

TEST CONDITION: AMO  
TEMPERATURE: 25°C

DATE: 7/26/78

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# SOLAR CELL ELECTRICAL DATA

CELL DESCRIPTION: Solar cells (2x2cm) from Wacker Wafer (E, F), BSF process

TEST CONDITION:  $\text{SiO}_2$  A.R coating,  $\approx 90\%$  active area

TEMPERATURE: AMO  
25°C

DATE: 7/27/78

| NO. | V <sub>OC</sub> | I <sub>SC</sub> | I <sub>SCB</sub> | I <sub>SCR</sub> | I <sub>Max</sub> | V <sub>Max</sub> | P <sub>Max</sub> | CFF  | $\eta$ |
|-----|-----------------|-----------------|------------------|------------------|------------------|------------------|------------------|------|--------|
|     | mV              | mA              | mA               | mA               | mA               | mV               | mW               | %    | %      |
| E1  | 533             | 119             | 51               | 68               | 105              | 432              | 45.9             | 72.4 | 8.5    |
| E2  | 541             | 123             | 51               | 71               | 111              | 450              | 50               | 75.1 | 9.3    |
| E4  | 540             | 125             | 52               | 72               | 115              | 445              | 51.2             | 75.9 | 9.5    |
| E5  | 541             | 124             | 52               | 71               | 111              | 446              | 49.5             | 73.8 | 9.2    |
| E6  | 553             | 129             | 53               | 75               | 118              | 455              | 53.7             | 75.3 | 9.9    |
| E7  | 555             | 132             | 53               | 78               | 122              | 452              | 55.1             | 75.2 | 10.2   |
| E8  | 548             | 128             | 52               | 75               | 114              | 447              | 51.0             | 72.7 | 9.4    |
| E11 | 552             | 126             | 52               | 74               | 115              | 453              | 52.1             | 74.9 | 9.7    |
| E12 | 557             | 131             | 53               | 78               | 120              | 458              | 55.0             | 75.4 | 10.2   |
| E13 | 534             | 123             | 52               | 71               | 110              | 440              | 48.2             | 73.4 | 8.9    |
| E14 | 543             | 128             | 52               | 76               | 118              | 450              | 53.1             | 76.4 | 9.8    |
| E15 | 555             | 129             | 52               | 77               | 120              | 460              | 55.2             | 77.1 | 10.2   |
|     |                 |                 |                  |                  |                  |                  |                  |      |        |
| F1  | 528             | 118             | 51               | 67               | 103              | 427              | 44               | 70.6 | 8.2    |
| F2  | 541             | 124             | 52               | 72               | 114              | 445              | 50.7             | 75.6 | 9.4    |
| F3  | 541             | 125             | 52               | 73               | 115              | 450              | 51.8             | 76.6 | 9.6    |
| F5  | 537             | 122             | 51               | 71               | 112              | 450              | 50.4             | 76.9 | 9.3    |
| F6  | 547             | 128             | 52               | 75               | 116              | 450              | 52.2             | 74.6 | 9.7    |

### SOLAR CELL ELECTRICAL DATA

CELL DESCRIPTION: Solar cells (2x2 cm) from Wacker Wafer (E, F) BSF Process  
TEST CONDITION: SiO<sub>2</sub> A.R. coating, ≈ 90 % active area  
TEMPERATURE: AMO 25°C DATE: 7/27/78

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### SOLAR CELL ELECTRICAL DATA

CELL DESCRIPTION: Solar cells ( $\approx 2 \times 2 \text{ cm}$ ) from Wacker wafers (E, F), BSF process  
TEST CONDITION: MLAR coating, Fine contact line  $\approx 93\%$  active area  
TEMPERATURE: AMO  
25°C

[illegible]

# SOLAR CELL ELECTRICAL DATA

CELL DESCRIPTION: Control Solar cells (2x2 cm), Wacker (E, F) BSF process  
SiO<sub>2</sub> A.R. coating, ≈ 90 % active area  
 TEST CONDITION: AM1.0  
 TEMPERATURE: 25°C DATE: 7/27/78

| NO.                                                 | V <sub>OC</sub>                                    | I <sub>SC</sub> | I <sub>SCB</sub> | I <sub>SCR</sub> | I <sub>Max</sub> | V <sub>Max</sub> | P <sub>Max</sub> | CFF    | η     |
|-----------------------------------------------------|----------------------------------------------------|-----------------|------------------|------------------|------------------|------------------|------------------|--------|-------|
|                                                     | mV                                                 | mA              | mA               | mA               | mA               | mV               | mW               | %      | %     |
| 11                                                  | 602                                                | 142             | 55               | 87               | 132              | 503              | 66.4             | 77.8   | 12.3  |
|                                                     | (593)                                              | (104)           |                  |                  | (96)             | (500)            | (48.0)           | (77.8) | (8.9) |
| 12                                                  | 602                                                | 141             | 56               | 86               | 130              | 500              | 65.0             | 76.6   | 12.0  |
|                                                     | (593)                                              | (103)           |                  |                  | (92)             | (505)            | (46.5)           | (76.1) | (8.6) |
| 13                                                  | 601                                                | 143             | 56               | 87               | 131              | 495              | 64.8             | 75.4   | 12.0  |
|                                                     | (591)                                              | (103)           |                  |                  | (88)             | (500)            | (44.0)           | (72.3) | (8.2) |
| Following cell # 15 and 17 are second control group |                                                    |                 |                  |                  |                  |                  |                  |        |       |
| 15                                                  | 603                                                | 137             | 53               | 84               | 129              | 500              | 64.5             | 78.1   | 11.9  |
|                                                     | (594)                                              | (99)            |                  |                  | (89)             | (500)            | (44.5)           | (75.7) | (8.2) |
| 17                                                  | 599                                                | 139             | 53               | 87               | 131              | 500              | 65.5             | 78.7   | 12.1  |
|                                                     | (592)                                              | (99)            |                  |                  | (90)             | (505)            | (45.5)           | (77.5) | (8.4) |
| *                                                   | Parenthesis numbers for <u>before</u> A.R. coating |                 |                  |                  |                  |                  |                  |        |       |
|                                                     |                                                    |                 |                  |                  |                  |                  |                  |        |       |
|                                                     |                                                    |                 |                  |                  |                  |                  |                  |        |       |

### SOLAR CELL ELECTRICAL DATA

CELL DESCRIPTION: Solar cells (2x2cm) from Wacker Wafer (I), Grain Boundary (G.B) passivation proc  
TEST CONDITION: NO. AR coating,  $\approx 90\%$  active area.

TEST CONDITION:

TEMPERATURE:

AMO

25 °C

DATE: 8/18/78

[illegible]



# SOLAR CELL ELECTRICAL DATA

CELL DESCRIPTION: Solar cells (2x2 cm) from Wacker wafer (I), Grain Boundary (G.B) Passivation Process.  
SiO<sub>2</sub> A.R coating, ~ 90 % active area  
 TEST CONDITION: AMO  
 TEMPERATURE: 25°C DATE: 8/21/78

| NO.  | V <sub>OC</sub> | I <sub>SC</sub> | I <sub>SCB</sub> | I <sub>SCR</sub> | I <sub>Max</sub> | V <sub>Max</sub> | P <sub>Max</sub> | CFF  | η    |
|------|-----------------|-----------------|------------------|------------------|------------------|------------------|------------------|------|------|
|      | mV              | mA              | mA               | mA               | mA               | mV               | mW               | %    | %    |
| I 1  | 536             | 110             | 46               | 62               | 101              | 440              | 44.4             | 75.7 | 8.2  |
| I 2  | 549             | 117             | 47               | 69               | 110              | 450              | 49.5             | 77.1 | 9.2  |
| I 3  | 548             | 114             | 46               | 68               | 106              | 450              | 47.7             | 76.2 | 8.8  |
| I 4  | 548             | 116             | 47               | 69               | 109              | 450              | 49.1             | 76.9 | 9.1  |
| I 5  | 550             | 117             | 48               | 69               | 109              | 450              | 49.1             | 76.1 | 9.1  |
| I 6  | 558             | 121             | 47               | 74               | 111              | 460              | 51.1             | 75.5 | 9.5  |
| I 7  | 562             | 126             | 50               | 76               | 118              | 460              | 54.3             | 76.8 | 10.1 |
| I 8  | 561             | 125             | 51               | 73               | 117              | 460              | 53.8             | 77.1 | 10.0 |
| I 11 | 546             | 123             | 49               | 74               | 104              | 430              | 44.7             | 66.5 | 8.3  |
| I 12 | 565             | 125             | 49               | 76               | 116              | 465              | 53.9             | 76.4 | 10.0 |
| I 13 | 544             | 114             | 45               | 69               | 107              | 445              | 47.6             | 76.6 | 8.8  |
| I 14 | 558             | 122             | 47               | 74               | 114              | 455              | 51.9             | 76.4 | 9.6  |
| I 15 | 564             | 124             | 49               | 75               | 115              | 460              | 52.9             | 75.6 | 9.8  |
| I 16 | 562             | 126             | 51               | 74               | 116              | 465              | 53.9             | 76.4 | 10.0 |
|      |                 |                 |                  |                  |                  |                  |                  |      |      |
|      |                 |                 |                  |                  |                  |                  |                  |      |      |
|      |                 |                 |                  |                  |                  |                  |                  |      |      |
|      |                 |                 |                  |                  |                  |                  |                  |      |      |

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### SOLAR CELL ELECTRICAL DATA

CELL DESCRIPTION: Control solar cells (2x2 cm) Wacker (I) G.B. passivation Process.  
TEST CONDITION: SiO<sub>2</sub> A.R coating, ~ 90 % active area  
TEMPERATURE: AMO 25°C DATE: 8/12/93

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APPENDIX IV

ELECTRICAL DATA SHEETS FOR EFG SOLAR CELLS

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|                   |                       |                    |
|-------------------|-----------------------|--------------------|
| CELL DESCRIPTION: | Cells from EFG Ribbon | standard Process   |
| TEST CONDITION:   | No A.R coating        | ≈ 88 % Active area |
| TEMPERATURE:      | AMO<br>25°C           | DATE: 9/6/02       |

[illegible]

### SOLAR CELL ELECTRICAL DATA

CELL DESCRIPTION: Cells from EFG Ribbon, Standard Process  
TEST CONDITION: SiO<sub>2</sub> A.R. coating,  $\approx 88\%$  active area  
TEMPERATURE: AMO 25°C DATE: 9/8/78

[illegible]

# SOLAR CELL ELECTRICAL DATA

CELL DESCRIPTION: Control Solar Cells (2x2 cm) EFG Ribbon Standard Process  
SiO<sub>2</sub> A.R. coating, 2 90 % active area.  
 TEST CONDITION: AM 0  
 TEMPERATURE: 25°C DATE: 9/8/78

| NO. | V <sub>OC</sub><br>mV | I <sub>SC</sub><br>mA | I <sub>SCB</sub><br>mA | I <sub>SCR</sub><br>mA | I <sub>Max</sub><br>mA | V <sub>Max</sub><br>mV | P <sub>Max</sub><br>mW | CFF<br>%     | η<br>%        |
|-----|-----------------------|-----------------------|------------------------|------------------------|------------------------|------------------------|------------------------|--------------|---------------|
| 70  | 596<br>(589)          | 134<br>(97)           | 52<br>(36)             | 82<br>(61)             | 126<br>(91)            | 515<br>(505)           | 64.8<br>(46.0)         | 81<br>(80)   | 12<br>(8.5)   |
| 71  | 596<br>(589)          | 135<br>(98)           | 53<br>(37)             | 83<br>(61)             | 127<br>(90)            | 500<br>(495)           | 63.5<br>(44.6)         | 79<br>(77.2) | 11.8<br>(8.3) |
| 72  | 596<br>(589)          | 134<br>(97)           | 53<br>(36)             | 81<br>(61)             | 128<br>(91)            | 500<br>(500)           | 64.0<br>(45.5)         | 80<br>(79.6) | 11.9<br>(8.4) |
| 73  | 596<br>(589)          | 134<br>(97)           | 52<br>(36)             | 82<br>(61)             | 124<br>(88)            | 505<br>(498)           | 62.6<br>(43.8)         | 78<br>(76.7) | 11.6<br>(8.1) |
| 74  | 596<br>(589)          | 134<br>(97)           | 53<br>(36)             | 81<br>(61)             | 125<br>(88)            | 500<br>(493)           | 62.5<br>(43.4)         | 79<br>(75.9) | 11.6<br>(8.0) |
| 76  | 597<br>(590)          | 134<br>(97)           | 54<br>(36)             | 81<br>(61)             | 125<br>(89)            | 505<br>(500)           | 63.1<br>(44.5)         | 78<br>(77.8) | 11.7<br>(8.2) |
| 77  | 597<br>(590)          | 137<br>(99)           | 54<br>(37)             | 84<br>(62)             | 130<br>(93)            | 510<br>(502)           | 66.3<br>(46.7)         | 80<br>(79.9) | 12.3<br>(8.6) |
| 78  | 598<br>(591)          | 137<br>(98)           | 53<br>(36)             | 84<br>(61)             | 129<br>(91)            | 510<br>(507)           | 65.8<br>(46.1)         | 80<br>(79.7) | 12.2<br>(8.5) |
| 79  | 597<br>(588)          | 136<br>(97)           | 53<br>(36)             | 83<br>(61)             | 129<br>(91)            | 510<br>(507)           | 65.8<br>(46.1)         | 81<br>(80.9) | 12.2<br>(8.5) |

cell # 76, 78, 77 and 79 are second central group

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# SOLAR CELL ELECTRICAL DATA

CELL DESCRIPTION: Cells from EFG Ribbon BSF process  
NO A.R coating , ~ 88 % active area  
 TEST CONDITION: AMO  
 TEMPERATURE: 25°C DATE: 9/26/78

| NO. | V <sub>OC</sub> | I <sub>SC</sub> | I <sub>SCB</sub> | I <sub>SCR</sub> | I <sub>Max</sub> | V <sub>Max</sub> | P <sub>Max</sub> | CFF | $\eta$ | AREA            |
|-----|-----------------|-----------------|------------------|------------------|------------------|------------------|------------------|-----|--------|-----------------|
|     | mV              | mA              | mA               | mA               | mA               | mV               | mW               | %   | %      | cm <sup>2</sup> |
| 26  | 547             | 125             | 53               | 71               | 94               | 450              | 42.3             | 62  | 5.8    | 5.42            |
| 28  | 564             | 133             | 56               | 76               | 121              | 470              | 56.9             | 76  | 7.6    | 5.55            |
| 29  | 565             | 134             | 56               | 77               | 122              | 475              | 58.0             | 77  | 7.8    | 5.56            |
| 31  | 547             | 125             | 53               | 72               | 112              | 455              | 51.0             | 74  | 6.8    | 5.58            |
| 32  | 538             | 120             | 51               | 68               | 103              | 435              | 44.8             | 69  | 6.1    | 5.42            |
| 33  | 506             | 115             | 42               | 65               | 87               | 345              | 30.0             | 51  | 4.4    | 5.07            |
| 36  | 529             | 127             | 54               | 71               | 88               | 410              | 36.1             | 54  | 4.8    | 5.62            |
| 38  | 532             | 116             | 50               | 64               | 104              | 435              | 45.2             | 73  | 6.1    | 5.49            |
| 40  | 515             | 111             | 47               | 62               | 92               | 415              | 38.2             | 67  | 5.4    | 5.28            |
| 41  | 555             | 128             | 54               | 72               | 109              | 460              | 50.1             | 71  | 6.2    | 6.01            |
| 43  | 529             | 106             | 44               | 61               | 96               | 440              | 42.2             | 75  | 6.5    | 4.80            |
| 44  | 555             | 122             | 53               | 68               | 103              | 465              | 47.9             | 71  | 6.6    | 5.35            |
| 45  | 529             | 121             | 51               | 69               | 107              | 435              | 46.6             | 73  | 6.3    | 5.52            |
| 46  | 526             | 122             | 52               | 70               | 112              | 435              | 48.7             | 76  | 6.7    | 5.37            |
| 49  | 524             | 112             | 47               | 65               | 100              | 430              | 43.0             | 73  | 5.7    | 5.62            |
| 50  | 524             | 116             | 49               | 66               | 100              | 420              | 42.0             | 69  | 5.9    | 5.29            |
| 55  | 558             | 134             | 56               | 77               | 119              | 470              | 55.9             | 74  | 7.5    | 5.52            |



### SOLAR CELL ELECTRICAL DATA

CELL DESCRIPTION: Cells from EFG Ribbon, BSF Process  
TEST CONDITION: SiO<sub>2</sub> A.R coating, ≈ 88 % active area  
TEMPERATURE: AMO  
25°C DATE: 9/27/78

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### SOLAR CELL ELECTRICAL DATA

CELL DESCRIPTION: Cells from EFG Ribbon, BSF process  
TEST CONDITION: MLAR coating,  $\approx$  88 active area -  
TEMPERATURE: AMO  
25°C DATE: 9/27/78

TEST CONDITION: MLAR coating,  $\approx 88$  active area -  
 TEMPERATURE: AMO  
 25°C DATE: 9/27/78

DATE: 9/27/78

[illegible]

### SOLAR CELL ELECTRICAL DATA

|                   |                             |               |             |
|-------------------|-----------------------------|---------------|-------------|
| CELL DESCRIPTION: | Control Solar cell (2x2 cm) | FFG Ribbon    | BSF process |
| TEST CONDITION:   | AM0                         | ~ 90 %        | active area |
| TEMPERATURE:      | 25 °C                       | DATE: 9/27/17 |             |

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## APPENDIX V

### ABBREVIATIONS

### ABBREVIATIONS

|             |                                                                               |
|-------------|-------------------------------------------------------------------------------|
| $V_{OC}$ :  | Open Circuit Voltage                                                          |
| $I_{SC}$ :  | Short Circuit Current                                                         |
| $J_{SC}$ :  | Short Circuit Current Density                                                 |
| $I_{SCR}$ : | Short Circuit Current (Red Response) at Wavelength Above<br>$\sim 0.6 \mu m$  |
| $I_{SCB}$ : | Short Circuit Current (Blue Response) at Wavelength Below<br>$\sim 0.6 \mu m$ |
| CFF:        | Curve Fill Factor                                                             |
| $\eta$ :    | Solar Cell Conversion Efficiency                                              |
| $L_e$ :     | Minority Carrier Diffusion Length                                             |
| $I_{MAX}$ : | Current at Maximum Power Point                                                |
| $V_{MAX}$ : | Voltage at Maximum Power Point                                                |
| $P_{MAX}$ : | Maximum Power Point                                                           |
| BSF:        | Back Surface Field                                                            |
| MLAR:       | Multi-Layer Anti-Reflective                                                   |
| D.L.:       | Minority Carrier Diffusion Length                                             |