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A THEORETICAL STUDY OF A LAMINAR
DIFFUSION FLAME

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I. ABSTRACT

Theoretical models of an axisymmetric laminar diffusion flame are discussed, with an emphasis on the behavior of such flames at increasing pressures. The flame-sheet or Burke-Schumann model (in terms of Bessel functions) and various boundary-layer numerical solutions are presented and their results compared with experimental data. The most promising theoretical model combines the numerical flow field solution of the Patankar-Spalding computer code with the Pratt-Wormeck chemical reaction subroutine. The flame shapes for pressures of 1, 5, 10, 20, and 50 atmospheres have been computed and agree remarkably well with experimental data. There is a noticeable shape change with pressure, believed to be a result of buoyancy effects. The chemical concentration profiles do not exhibit much dependence on pressure, a reflection of the fact that only one chemical mechanism was utilized at all pressures.

II. INTRODUCTION

The problem of pollutant formation in turbine combustors is currently receiving a great deal of warranted attention, especially the pollution associated with aircraft turbine engines in and around airports. Of the various pollutants discharged from these engines, two of the most harmful are nitric oxide and nitrogen dioxide, commonly referred to as NO_x . Since actual combustors may operate at pressures up to 30 atm, it is of special interest to consider the effect of pressure on the formation of NO_x during the combustion process, which has been done experimentally by Miller and Maahs [1] at NASA-Langley.

In their experimental investigation, an intentionally simplified combustion system--a laminar diffusion flame--was chosen to model the actual combustion process. The diffusion, or non-premixed, flame was selected over the premixed flame because it is an experimentally simpler system and because larger NO_x concentrations are expected with the diffusion flame. The laminar flow regime was selected in order to eliminate fluid flow effects as much as possible so as to concentrate on chemical effects.

The structure of laminar diffusion flames has been the subject of investigation for a great many years. The first analytical study of diffusion flames was made by Burke and Schumann [2] in 1928. They introduced the assumption that the zone of combustion might be approximated as a surface, i.e. infinitely thin. It would then follow that the associated reaction rates would be infinite. Burke and Schumann were concerned with a cylindrical laminar fuel jet discharging into an air stream moving with the same velocity as the fuel; they proceeded to calculate the flame shape for various initial conditions. The same assumption has been utilized to predict the length of both laminar and

turbulent open flames. (Hotte1 and Hawthorne [3], Wohl, Gasley, and Knapp [4], Barr [5]).

Zeldovich [6] was among the first to consider the structure of a reaction zone of finite thickness and hence the effects of finite reaction rates. Similar studies have been done by Spalding [7] with an emphasis on the phenomenon of extinction. Linan [8] has also studied the effects of finite chemical reaction rates by means of a boundary-layer-type solution, while many have applied perturbation techniques to the problem (Fendell [9], Kasso y and Williams [10], Chung, Fendell, and Holt [11]).

The computer simulation and prediction of chemically reacting flows, an extremely difficult problem because one must describe the interaction of many reacting chemical species with fluctuating temperature and velocity fields, is nevertheless a method of solution that is being used to a greater and greater degree as computer software/hardware facilities become more advanced.

There exist at present two well-defined bodies of literature on the numerical (computer) solution to chemically reacting flows: 1) fluid flow with infinite-rate chemistry (chemical equilibrium), and 2) finite-rate chemically reacting flow without mixing or with infinite-rate mixing. Examples of such works are those by Patankar and Spalding [12] and Pratt [13], respectively. Pratt and Wormeck [14] have then attempted to combine aspects of both bodies of literature to achieve a scheme that could model the phenomena of a diffusion flame-a laminar finite-rate chemically reacting flow field.

It is the purpose of this study to construct an analytical model of the laminar diffusion flame described by Miller and Maahs [1] and to compare experimental and theoretical results concerning the effects of high pressure on flame shape, temperature distribution and NO_x formulation.

Sections III and IV describe the physical system and experimental results, Section V introduces the governing equations and Section VI describes various theoretical models and associated results.

III. DESCRIPTION OF THE PHYSICAL SYSTEM

For purposes of completeness a summarized description of the physical system employed at NASA-Langley is included. For a more detailed description, Reference [1] should be consulted.

A diagram of the burner and collection system is shown in Figure 1. Methane gas issues from a cylindrical tube into a concentric cylindrical tube through which air is flowing. The fuel tube has an inside diameter of 3.06 mm and the air tube has an inside diameter of 20.5 mm. Fuel and air flow rates are held constant at 41.8 standard cm^3/min (sccm) and 2450 sccm, respectively.

In order to obtain a flat velocity profile in the fuel and air streams as they exit from their respective ducts, porous disks of sintered stainless steel were installed near the duct exits. Ignition is accomplished by means of an electrical hot-wire igniter. During operation the igniter is positioned 10 to 20 mm above the burner; once ignition is attained the igniter is removed from the flow.

The combustion products exit from the top of the quartz chimney and are swept into a total-sample collector by the nitrogen pressurizing gas. The nitrogen flow rate is kept low enough so as not to excessively dilute the gases to be analyzed. The products are analyzed by a continuous infrared CO_2 monitor and a chemiluminescent NO-NO_x analyzer.

The measurement of flame temperature is the most difficult and most uncertain of any measurements made. The method of two-color pyrometry was employed (with the carbon in the flame as the radiant emitter) to determine a spatial average temperature near the hottest point in the flame.

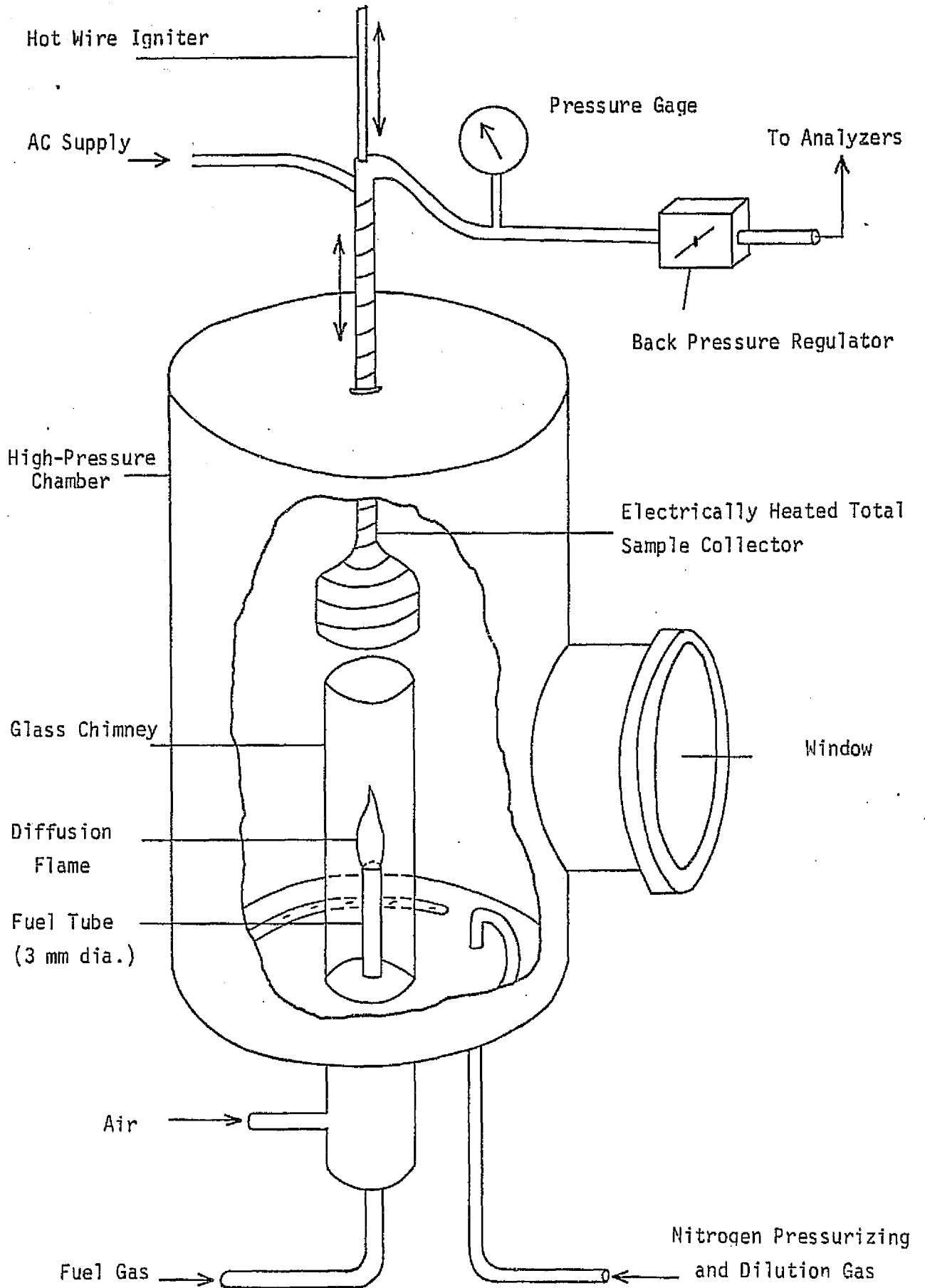


Figure 1 - Schematic diagram of burner and collection system

IV. EXPERIMENTAL RESULTS

A. Flame Shape

A definite change in the shape of the diffusion flame occurred as pressure was increased from 1 to 50 atm. This is shown in Figure 2, taken from Reference [1]. At 1 atm the sides of the flame bow outward, but this decreased as the pressure was increased above 1 atm. At about 10 atm the flame exhibited a slight concavity and the diameter decreased considerably. A further decrease in flame diameter occurred as the pressure increased, the maximum change associated with a pressure of approximately 20 atm.

An increase in the amount of carbon accompanied the change of flame shape and at pressures higher than 20 atm only minor changes occurred.

The height of the flame did not change drastically with pressure, as illustrated in Figure 3. The flames were typically 10 mm in height.

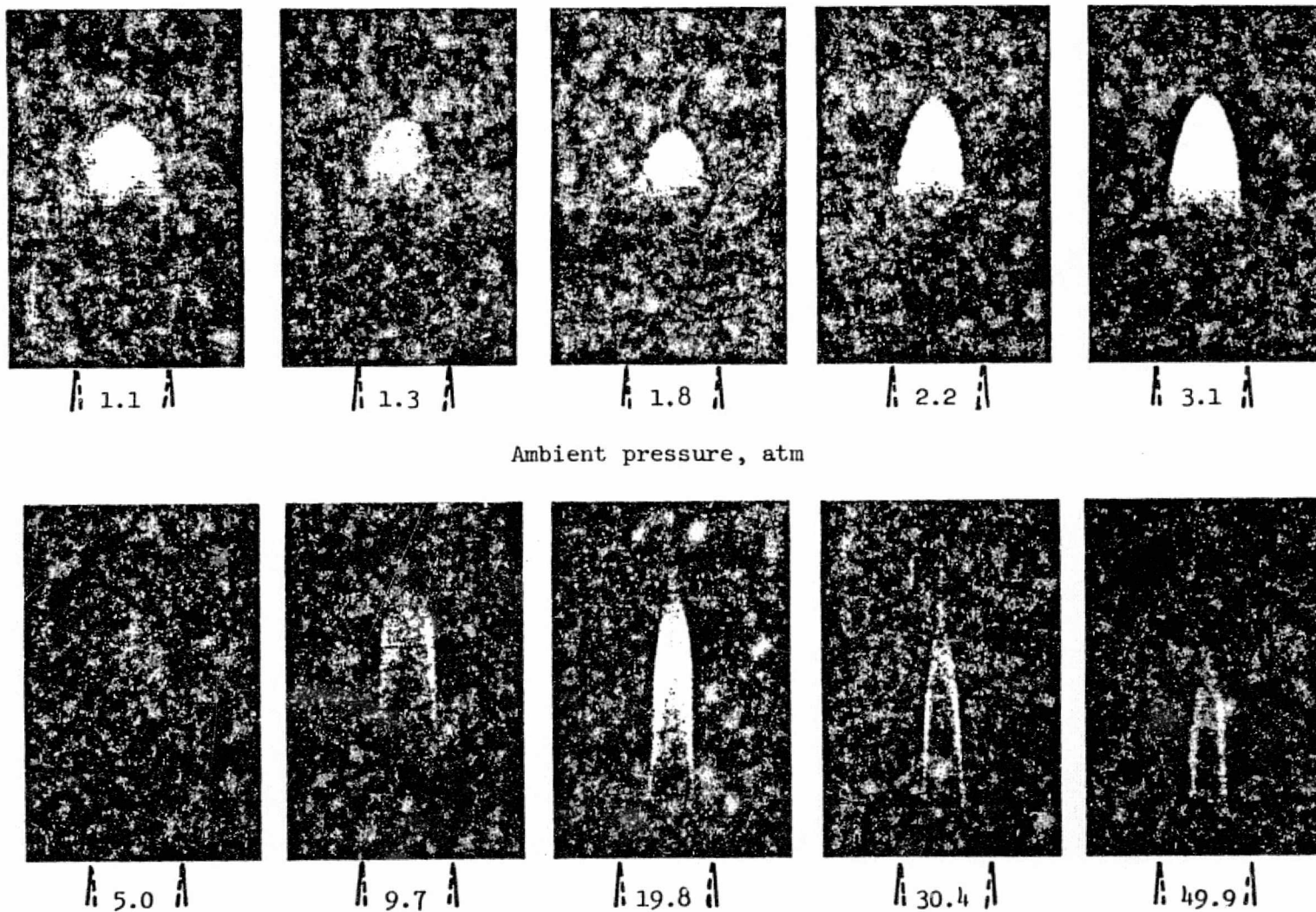
B. Nitrogen Oxide

The molar emission index of NO_x , I_m , is defined as the number of moles of NO and NO_2 produced per mole of fuel burned. Figure 4 shows that this quantity increases rapidly as pressure increases, reaching a maximum at about 9 atm. Above this pressure the molar emission index decreases slowly and continuously until it returns to roughly its original value.

C. Flame Temperature

A plot of the optically-measured peak temperature as a function of pressure is shown in Figure 5, with data limits shown by vertical lines. There is a steady decrease of peak temperature with pressure.

1 mm



L-77-167

Figure 2 - Photographs of methane-air diffusion flames for various ambient pressures.
Methane flow rate, 41.8 sccm; air flow rate, 2450 sccm; burner diameter, 3.06 mm. See Ref. 1.

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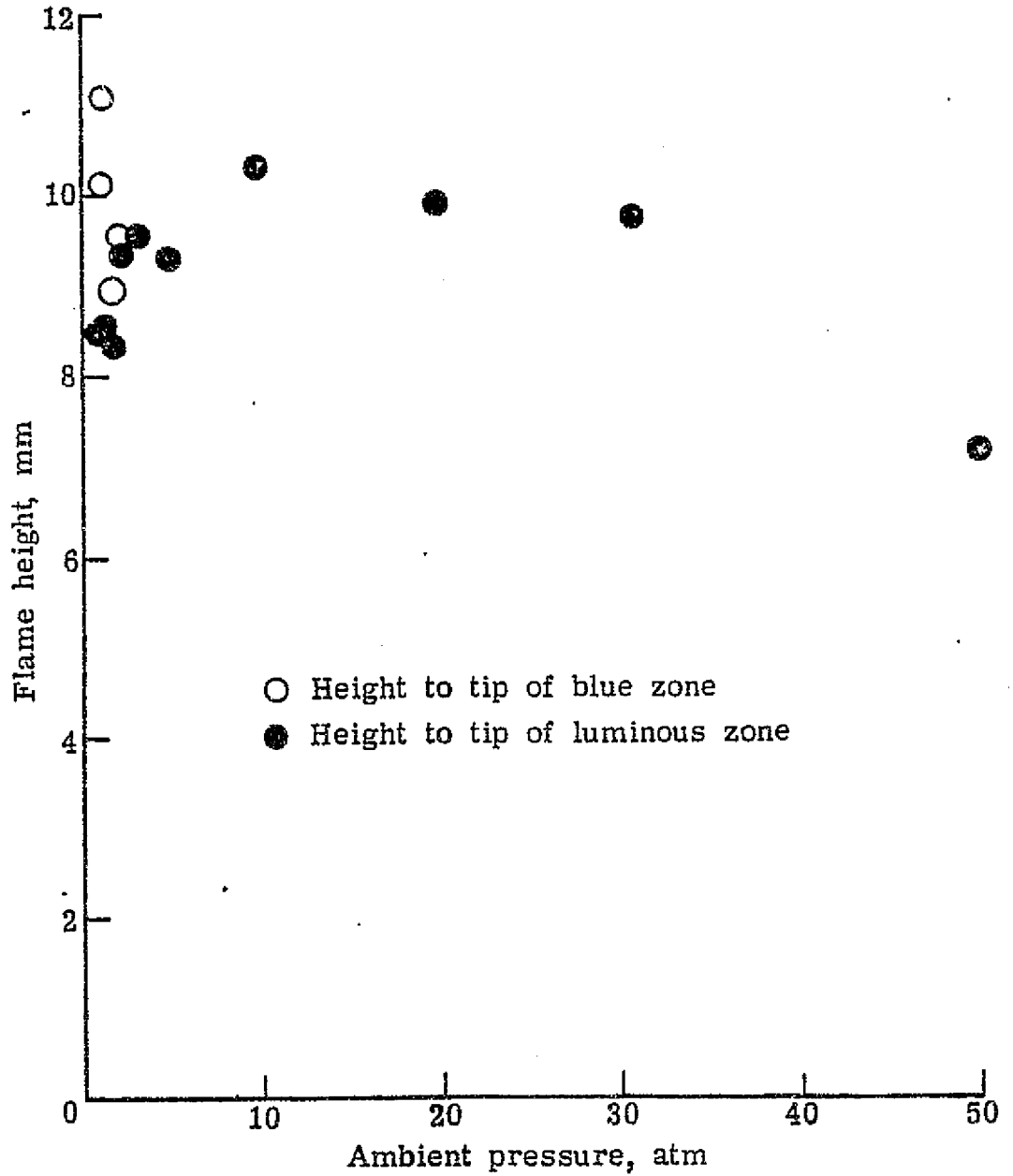
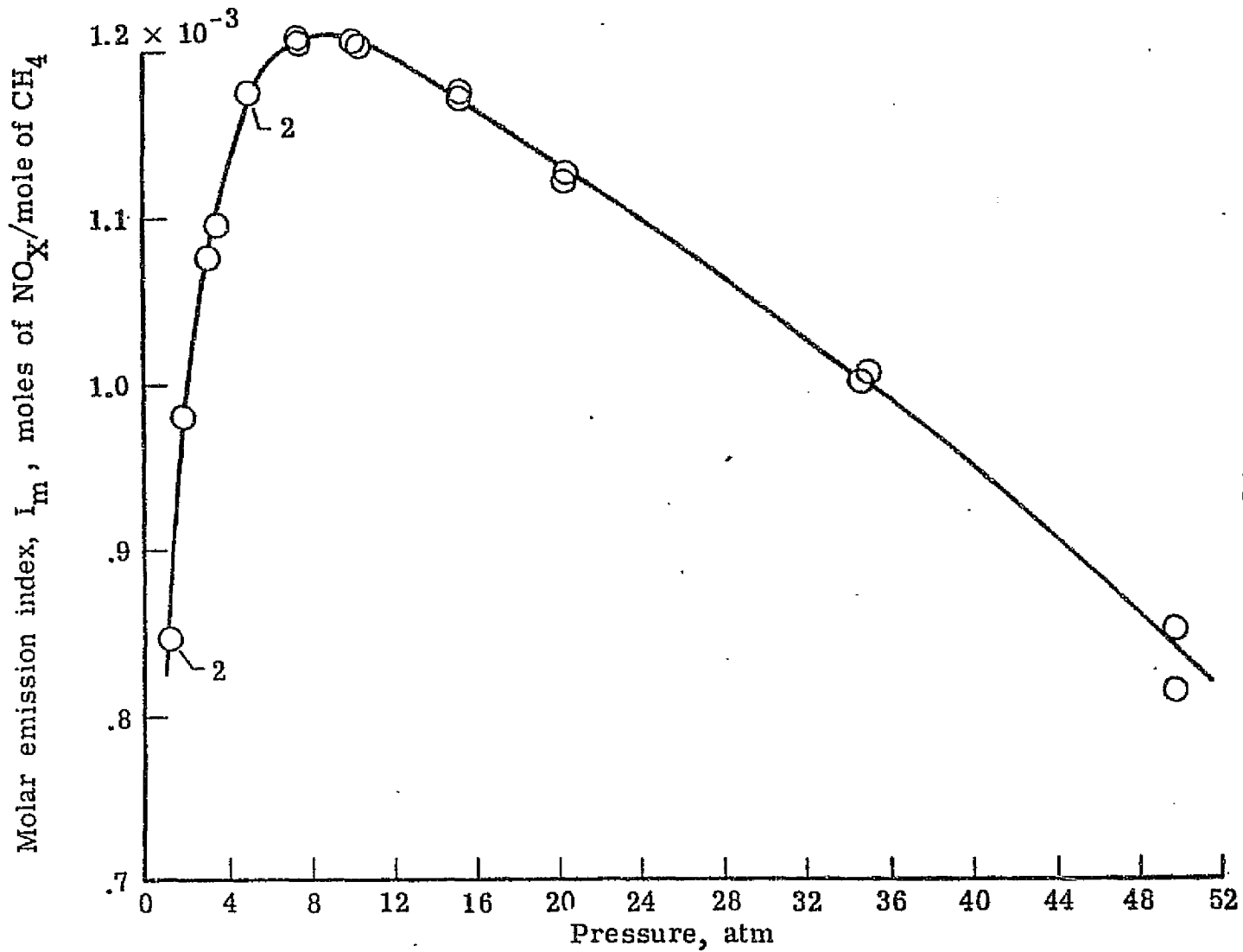


Figure 3 - Flame height as function of pressure. See Ref. 1



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Figure 4 - Molar emission index of NO_x as function of pressure. See Ref. 1

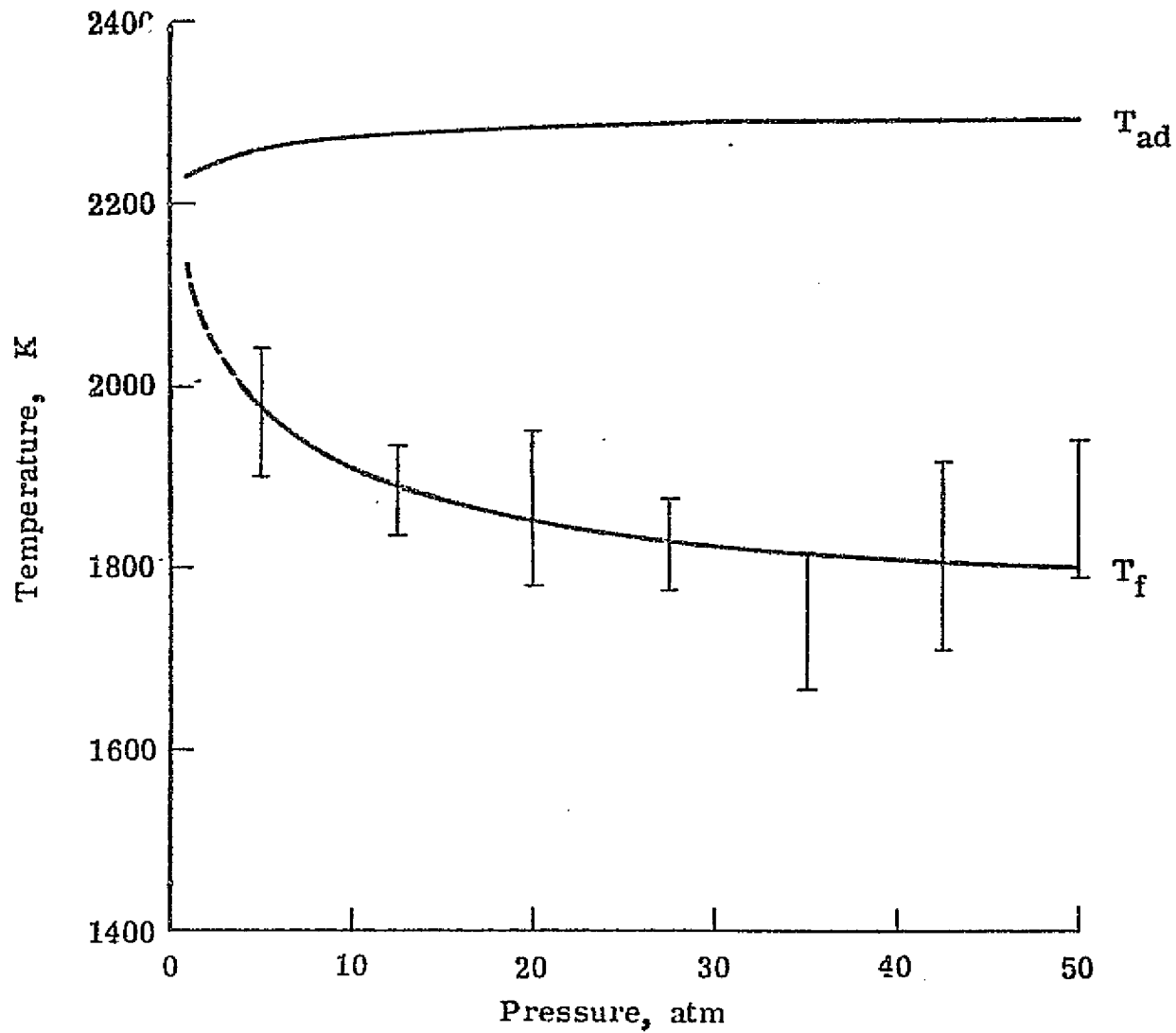


Figure 5 - Flame temperature as function of pressure.
 Dashed line indicates extrapolation. See Ref. 1

V. GOVERNING DIFFERENTIAL EQUATIONS

The equations of motion reflecting the conservation of mass, momentum, energy, and mass of each component for a chemically reacting gas mixture are:

Conservation of Mass

$$\frac{\partial \rho}{\partial t} + \text{div } \rho \bar{V} = 0$$

where ρ = density \bar{V} = velocity vector

Newton's Second Law

$$\rho \frac{D\bar{V}}{Dt} = -\nabla p + \text{div } \tau$$

where $\frac{D}{Dt}$ = substantial derivative = $\frac{\partial}{\partial t} + \bar{V} \cdot \nabla$

p = pressure

τ = viscous stress tensor

Conservation of Energy

$$\rho \frac{Dh}{Dt} = \frac{Dp}{Dt} + \tau : \epsilon - \text{div } \bar{q}$$

where

h = enthalpy

ϵ = rate of strain tensor

\bar{q} = heat flux vector

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Species Conservation

$$\rho \frac{Dm_i}{Dt} = -\text{div } \bar{J}_i + R_i$$

where

m_i = mass fraction of species i = $\frac{\rho_i}{\rho}$

\bar{J}_i = mass flux vector

R_i = rate of creation of species i by chemical reactions

In order to close the system the following constitutive relationships and equations of state are introduced:

$$\tau = 2\mu\epsilon + \lambda \operatorname{div} \bar{V} \Pi$$

where $\mu + \lambda$ are the 1st and 2nd coefficient of viscosity and

Π is the unit tensor

$$\epsilon = 1/2(\nabla \bar{V} + \nabla \bar{V}^T)$$

$$\bar{J}_i = \rho \sum_j \tilde{D}_{ij} \nabla m_j$$

where \bar{J}_i is the mass flux vector and \tilde{D}_{ij} 's are the diffusion coefficients

$$\bar{q} = -k\nabla T + \sum h_i \bar{J}_i \quad \bar{q} \text{ is the heat flux vector} \quad T = \text{temperature}$$

k = coefficients of conductivity.

$$p = \rho RT \sum_i \frac{m_i}{W_i} \quad h = \sum h_i m_i \quad h_i = h_i + \int_{T_0}^T C_{p_i} dT$$

where W_i = molecular weight of species i .

The above equations are non-linear second order partial differential equations. The two main types of solutions are analytical and numerical.

Analytical methods are those that express the solution as algebraic formulae, power series, etc. Methodologies such as separation of variables, series expansions, and coordinate transformations are employed to obtain such solutions. These types of solutions are usually limited to linear or linearized differential equations.

Numerical methods are those that express the solution in the form of numbers related to the particular circumstances of the flow. The differential equations are transformed to algebraic "finite-difference" equations and the values of all dependent variables are calculated at the nodes of a grid covering the domain of interest.

The flow to be considered is in general governed by nonlinear equations with the rate of chemical production term (R_i) being highly complex. Simplifying assumptions may be made and various solutions obtained. A discussion of these solutions and associated assumptions follows in Section VI.

VI. THEORETICAL ANALYSES

A. Burke - Schumann Analytical Solution

If the following assumptions are made:

1. steady cylindrical flow
2. inviscid flow
3. negligible pressure and thermal diffusion
4. Ficks Diffusion Law
5. single step chemical reaction of fuel and oxidant \rightarrow product
6. parallel and equal gas velocities
7. constant mass flux
8. axial diffusion \lll radial diffusion
9. entire chemical reaction occurs at the flame surface

then the governing equations may be combined into a single linear partial differential equation with appropriate boundary conditions. The solution is in terms of Bessel functions and a flame shape may be predicted from the analysis. Reference [15] presents a more detailed discussion of this solution.

The predicted flame shape agrees fairly well with the experimental evidence, although the predicted flame height at 1 atm (3.6 cm) is greater than the experimental. Furthermore, the Burke-Schumann model predicts absolutely no change of shape with pressure, hence it is evident that a more refined theoretical analysis is necessary.

B. Edelman - Fortune - Weilerstein Numerical Solution

The effects of inertia, viscosity, diffusion, gravity, and combustion on an axisymmetric laminar diffusion flame have been investigated via a boundary layer type formulation by Edelman, Fortune, and Weilerstein [16]. First a von Mises transformation is made in going from axisymmetric physical coordinates (x, r) , where x is the axial distance and r the

radial distance, to (x, ψ) coordinates. The stream function ψ is defined

by

$$\int_{\psi_a}^{\psi_b} \psi d\psi = \int_{r_a}^{r_p} \rho u r dr$$

The governing equations are then non-dimensionalized by means of an empirical normalization parameter.

"It is customary practice to do this (non-dimensionalization) by normalizing the variables directly in terms of the boundary conditions. However . . . the resulting dimensionless groups do not truly characterize the process and that is due to the large variation in flow properties throughout the domain of interest. Accordingly, the current approach involves the introduction of a set of characteristic quantities which are based upon some state within the flow that more accurately reflects the flame structure."
[16]

The equations are then solved numerically by means of an explicit finite difference formulation.

The Burke-Schumann combustion model, or "flame sheet assumption", is that all the heat is released on the surface where the fuel-air ratio is stoichiometric. A more accurate combustion description is offered in this model in terms of a basic equilibrium theory for the combustion in either the fuel-lean or fuel-rich regime.

For a pressure of one atmosphere this program predicted a flame height of .8 cm and a flame shape that agrees remarkably well with experimental data. However, the results for pressures greater than one atmosphere could not be substantiated either qualitatively or quantitatively by experimental data. This was due to the fact that the analysis in Ref. [16] utilizes a normalization parameter obtained experimentally at one atmosphere of pressure. This does not affect the original work since the problem considered was buoyancy effects of diffusion flames, all at one atmosphere. The analysis, limited as it is to a pressure of one atmosphere, does not therefore lend itself to the problem at hand.

C. Patankar-Spalding Numerical Solution

Patankar and Spalding [12] likewise utilize a boundary layer formulation and a von Mises coordinate transformation so as to put the conservation equations in the general form

$$\frac{\partial \phi}{\partial x} + (a + b\omega) \frac{\partial \phi}{\partial \omega} = \frac{\partial}{\partial \omega} \left(\frac{c \partial \phi}{\partial \omega} \right) + d$$

where

x and ω are the two independent coordinates

a and b are arbitrary functions of x

c and d are arbitrary functions of any dependent and independent variables

ϕ stands for any one of a set of variables, each possessing its own differential equation, e.g., fluid velocity, stagnation enthalpy, mass fraction, etc.

These differential equations are transformed into finite difference equations and solved by means of the tri-diagonal matrix algorithm (TDMA).

The chemistry incorporated into this numerical scheme is a very simple fuel-oxidant-product equilibrium model where the rate of generation of fuel by chemical reaction, R_{f_u} , is assumed to obey an "Arrhenius-type" relation.

For the case of negligible chemical reactions this program produces acceptable results in that the diffusional nature of the axial flow of fuel and air is well represented by means of velocity and concentration profiles. With the inclusion of limited equilibrium chemistry a flame shape can be obtained that agrees qualitatively with that obtained experimentally.

The theoretical flame height at one atmosphere is 8 cm as opposed to an experimental height of .8 cm however. Since the chemistry of the flow field under consideration is of prime importance, the very simple chemistry incorporated into this

model does indeed limit its ability to accurately describe the flame under investigation.

D. Patankar-Spalding and Pratt-Wormeck Numerical Solution

As stated previously, the hydrodynamic aspects of Spalding's code are well-developed and offer a valid model of the diffusional nature of the flow. A more realistic chemical model is provided by Pratt and Wormeck [14] in their subroutine for the calculation of chemically complex equilibrium or non-equilibrium stationary states.

The scheme employed by Pratt and Wormeck in their determination of chemical equilibrium states at prescribed temperature and pressure is essentially the same utilized by Gordon and McBride [17]: Gibbs function minimization.

A similar procedure is employed for the case of non-equilibrium (kinetic) stationary states. A chemical-kinetic source term is included which takes into account the effects of forward and reverse reaction rates, and reaction contact indices.

A combination of the hydrodynamic code of Spalding and the chemical package of Pratt and Wormeck results in a computer code that is capable of producing a numerical solution to the hydrodynamic equations of motion while taking into account the effects of complex chemical reaction. This combination computer code was applied to the problem at hand for the two cases of equilibrium and kinetic chemistry. It was found that the kinetic solution proved much too costly in computer time (IBM 370) to even consider, so the following results are limited to the case of equilibrium chemistry.

The thermochemical data were taken from Gordon and McBride [17]. A reaction mechanism consisting of 19 species and 34 reactions was utilized, as given in the actual computer listing found in the Appendix. A

cross-stream grid of 21 grid points was used. The results were found to be fairly sensitive to the input value for the temperature at the base of the burner. Since the computer solution is for a steady flow, the actual ignition phase is not considered, but a temperature is chosen that hopefully represents the physical situation after a steady state has been achieved. All the results discussed are for a base temperature of 1000°K.

Figure 6 demonstrates the change in theoretical flame height with pressure. As can be seen from a comparison of Figures 6 and 3, this agrees very well with the data obtained experimentally. The average computed flame height was 8.6 mm, as compared to the value of 10 mm for the empirical case.

Figures 7 and 8 demonstrate the theoretical flame shapes for pressures of one and five atmospheres of pressure and ten, twenty, and fifty atmospheres, respectively. The flame position at a particular height above the burner was assumed to be at the point of maximum temperature for that height.

As can be seen from a comparison of these Figures (7 and 8) with the actual flame shapes obtained (Figure 2), there is a remarkable agreement between the mathematical model and the empirical data. At one atmosphere the computed flame is fairly bulbous in nature, the sides of the flame bowing outward away from the burner. As pressure is increased the outward bowing of the sides of the flame decreases, and at 10 atmospheres there is almost no bowing at all. At 20 and 50 atmospheres the flame exhibits a concave appearance, which agrees extremely well with experimental results.

This shape change is believed to be a direct result of buoyancy effects. As the pressure increases, the difference between the densities

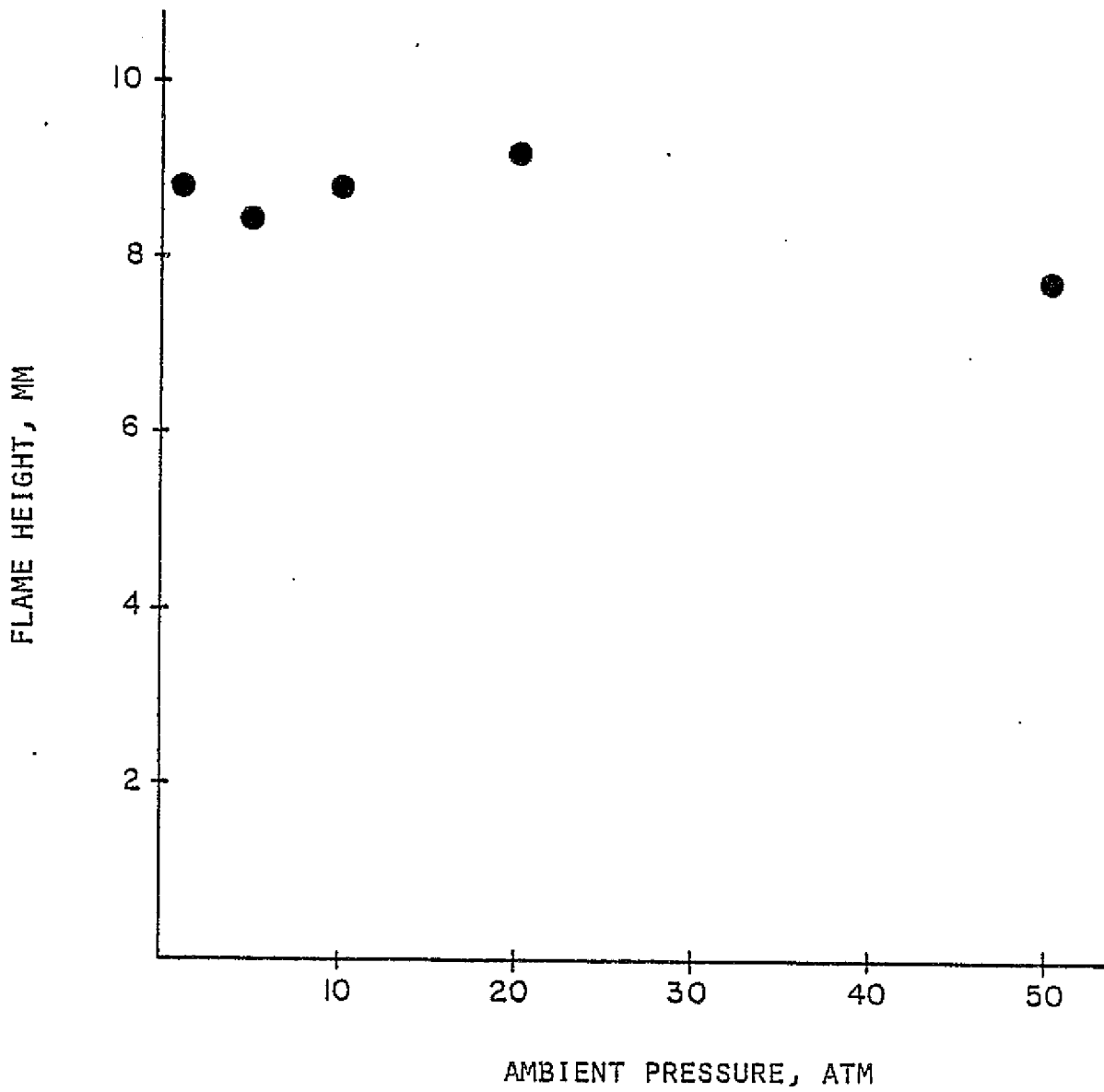
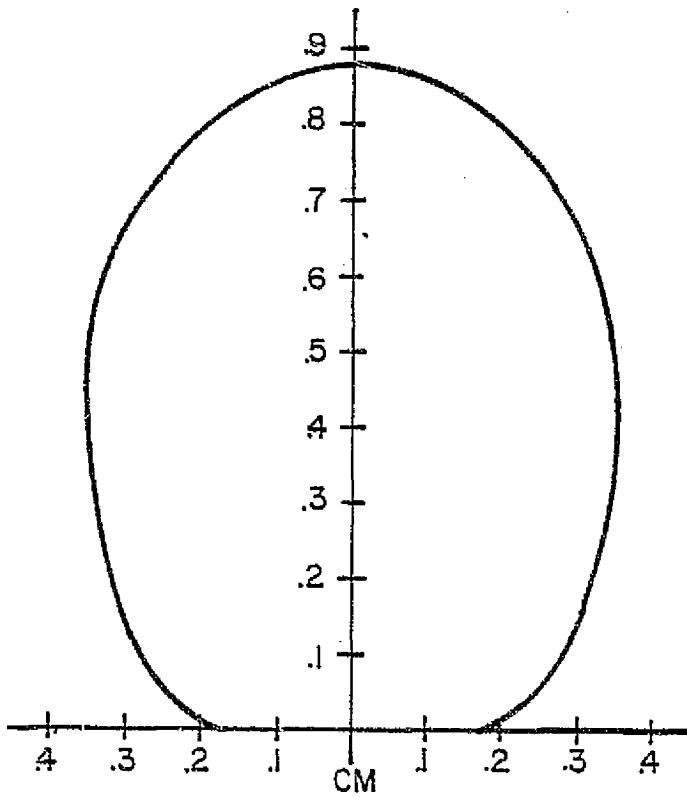


FIGURE 6 - THEORETICAL FLAME HEIGHT AS A FUNCTION OF PRESSURE



PRESSURE = 1 ATM

PRESSURE = 5 ATM

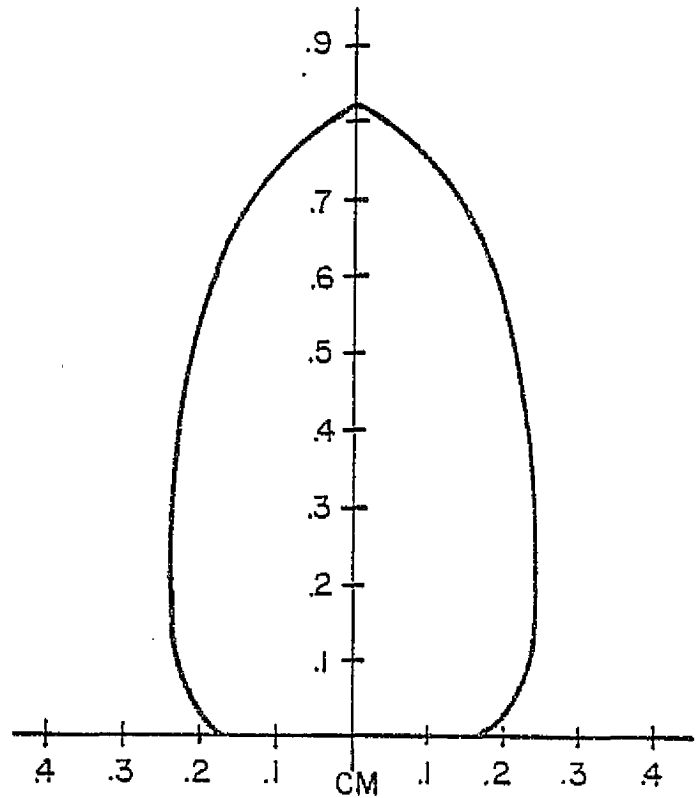


FIGURE 7 - THEORETICAL FLAME SHAPES

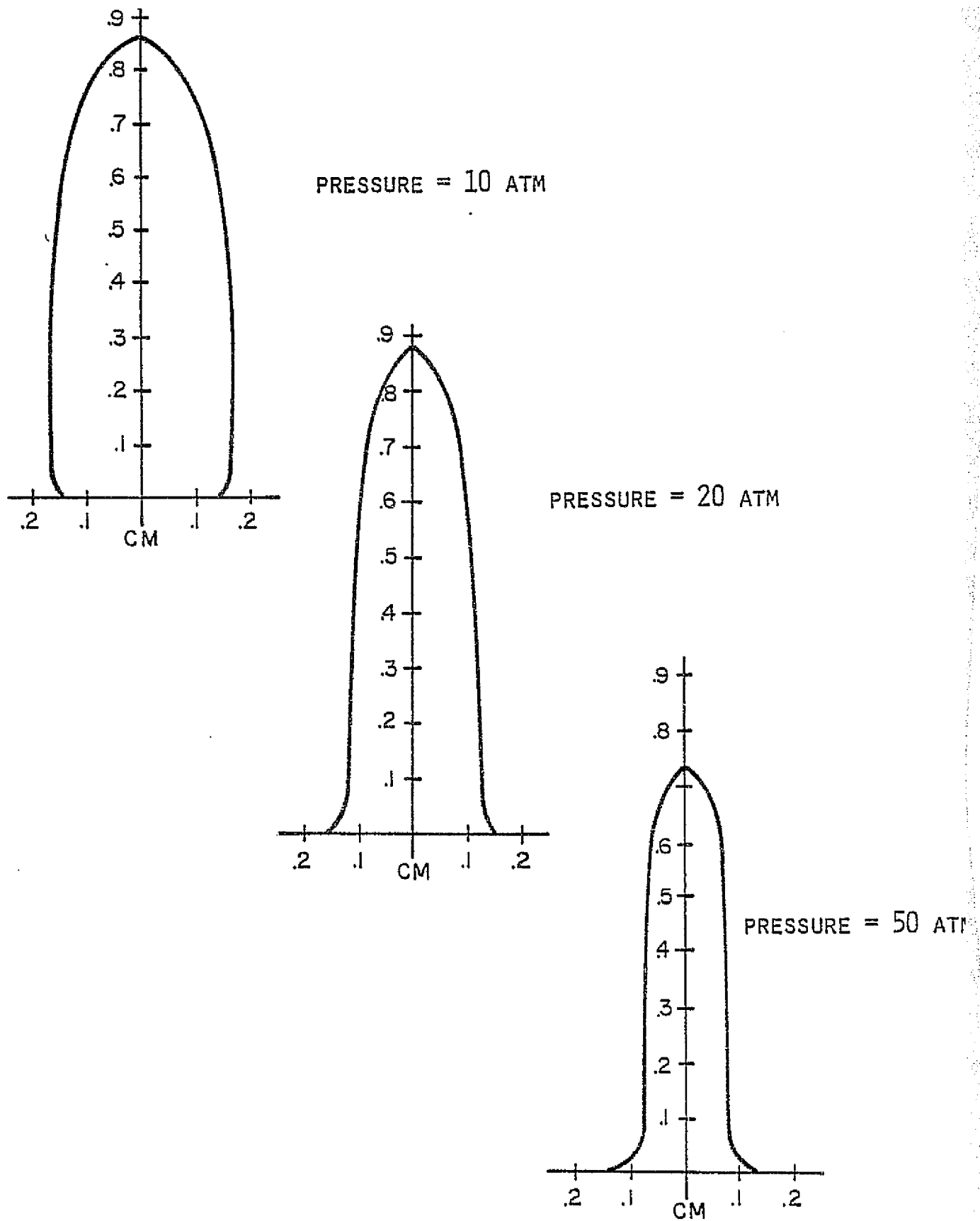


FIGURE 8 - THEORETICAL FLAME SHAPES

of methane and air become much more pronounced, hence the behavior of the two now very different gases under the action of gravity, i.e., buoyancy, affects the resulting flow field. In addition, the problem at hand is one of fairly low velocities. As the pressure is increased these velocities become even smaller and the fluid flow more sensitive to buoyancy effects. Prior to the inclusion of buoyancy effects in the computer program, all flames exhibited a somewhat bulbous shape similar to that found at one atmosphere.

Figure 9 is a plot of approximate maximum flame temperature as a function of pressure. Since these values are fairly sensitive to the input temperature at the base of the burner, it is difficult to make any general statement concerning this data except to say that in comparison with Figure 5, the computed flame temperature behaves in qualitatively the same manner as the adiabatic flame temperature shown there.

Figures 10-15 demonstrate various species mass fractions as a function of the radial distance outward from the center of the burner. Figure 10 is for a pressure of 1 atmosphere at a position of .15 cm above the inlet. Figures 11-15 are for a position of 0.5 cm above the burner, toward the top of the flame, and for pressures of 1, 5, 10, 20, and 50 atmospheres respectively.

At a vertical distance of .15 cm above the burner there still exists some unburned fuel close to the axis of the burner. The maximum NO_x concentration occurs closer to the flame position, as does the maximum concentration of CO_2 .

At a vertical distance of .5 cm above the burner, there is no CH_4 present and once again the maximum NO_x production occurs near the flame

front. There is essentially no change in the relative magnitude of this maximum concentration with pressure, only a change in where it occurs. This of course corresponds to the change of flame position with pressure.

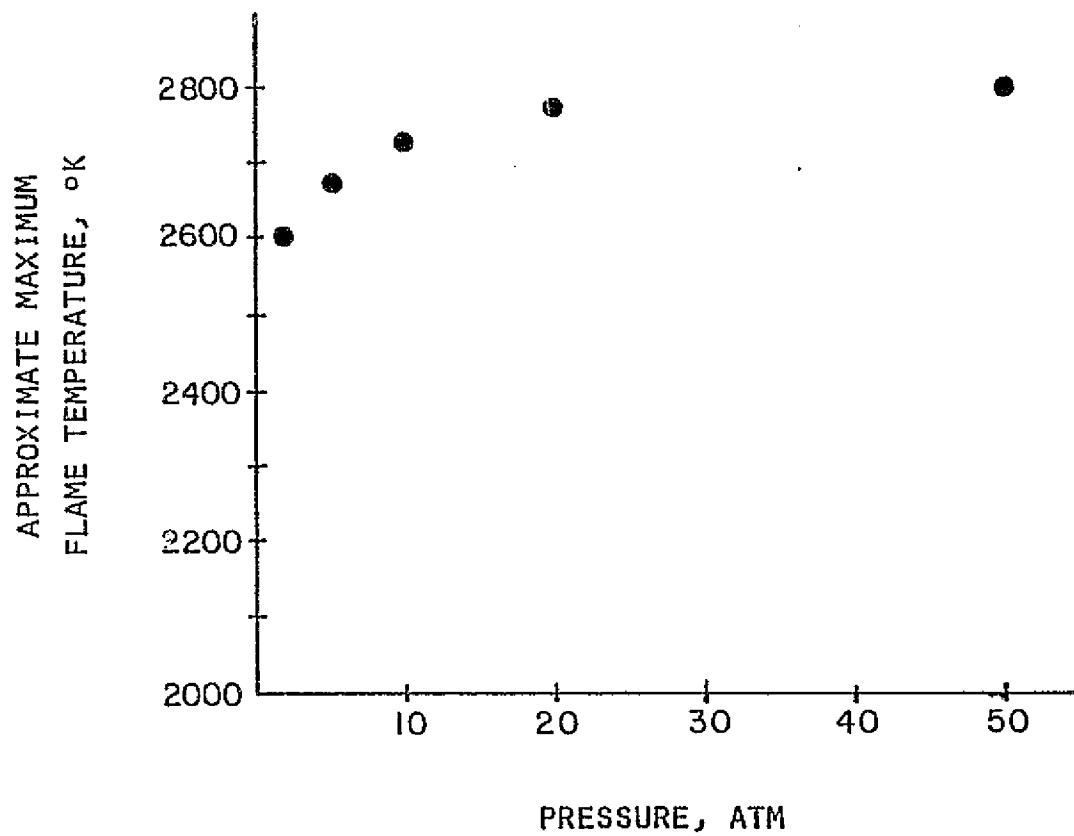


FIGURE 9 - MAXIMUM FLAME TEMPERATURE AS A FUNCTION OF PRESSURE

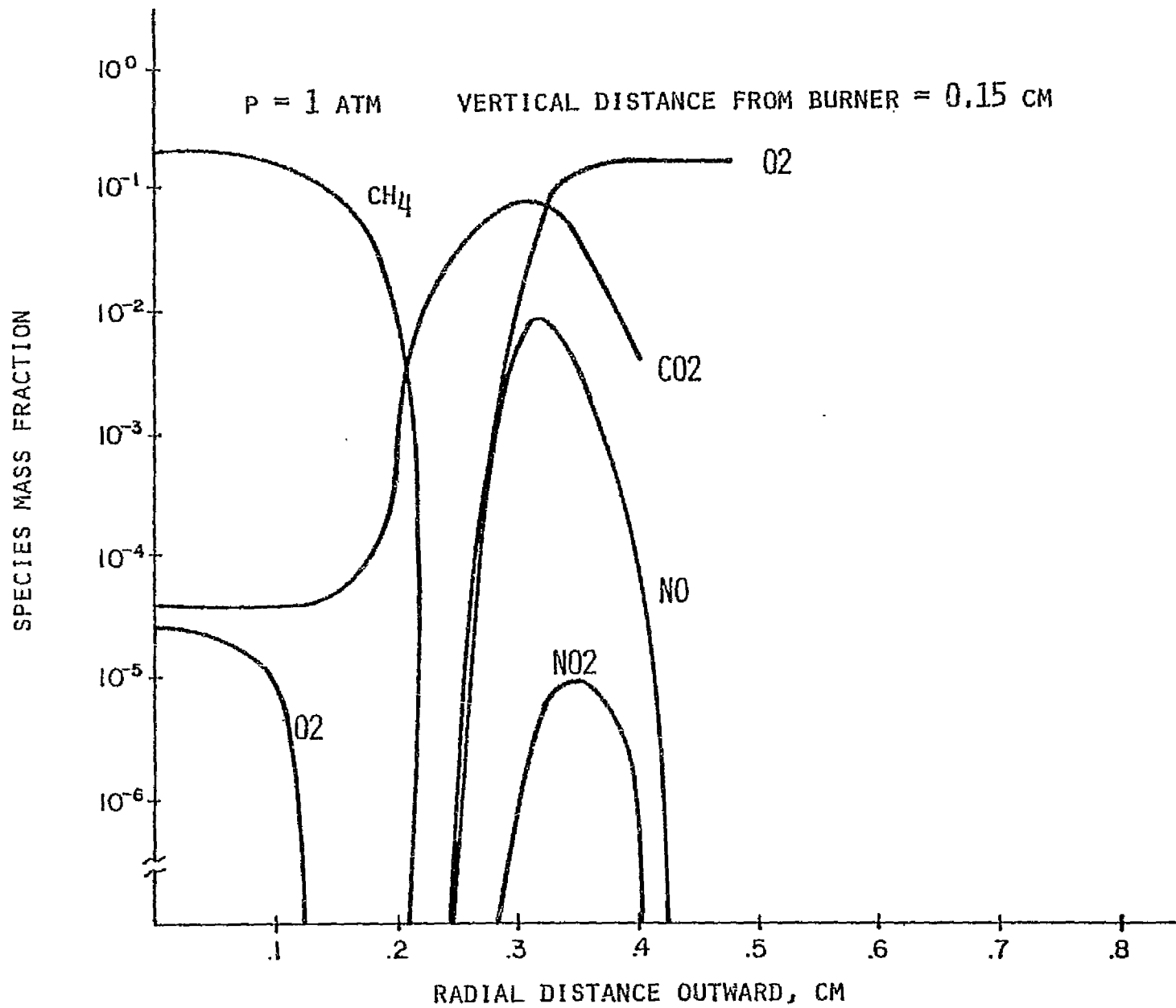


FIGURE 10 - SPECIES MASS FRACTION AS FUNCTION OF PRESSURE

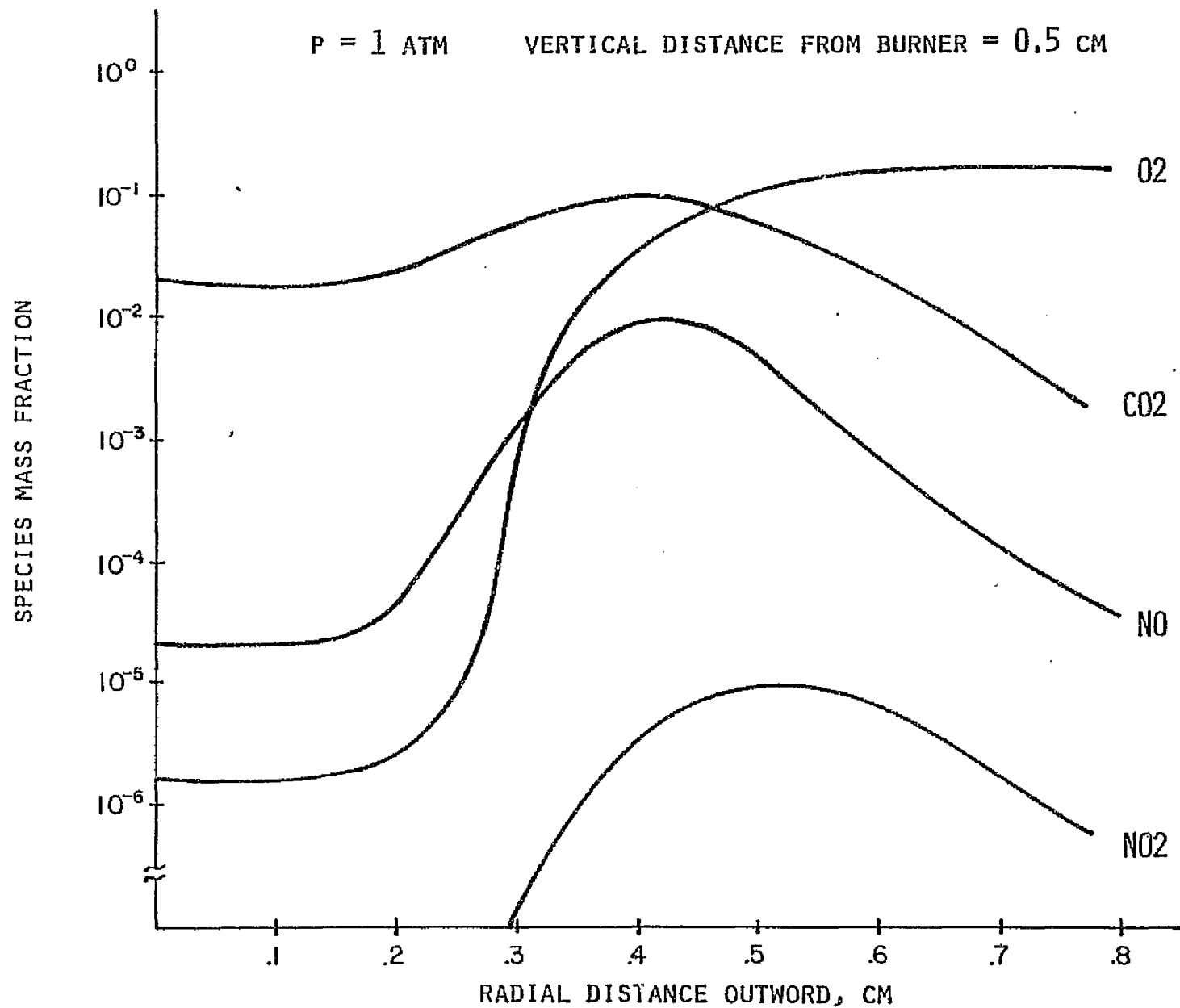


FIGURE 11 - SPECIES MASS FRACTION AS FUNCTION OF PRESSURE

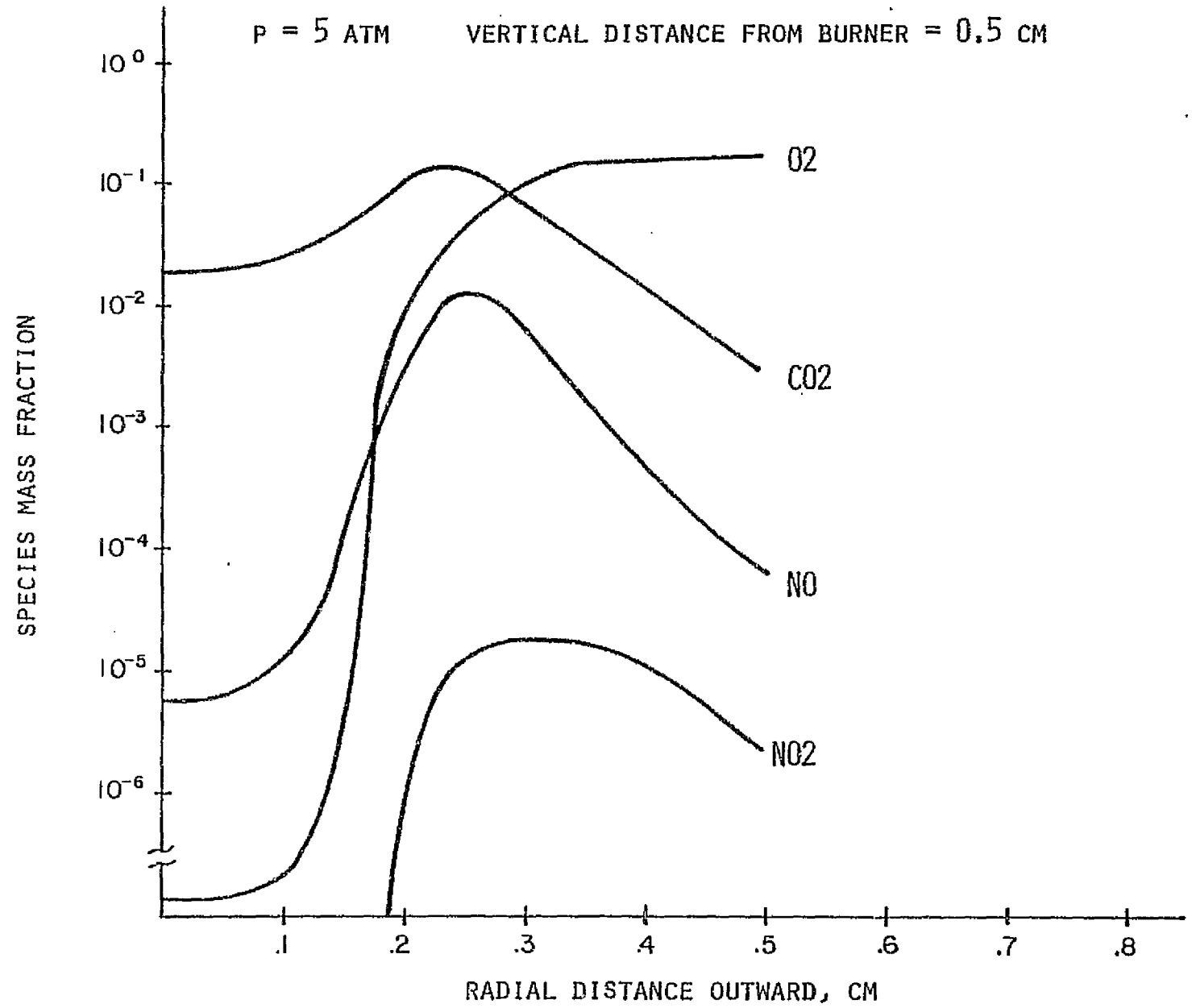


FIGURE 12 - SPECIES MASS FRACTION AS FUNCTION OF PRESSURE

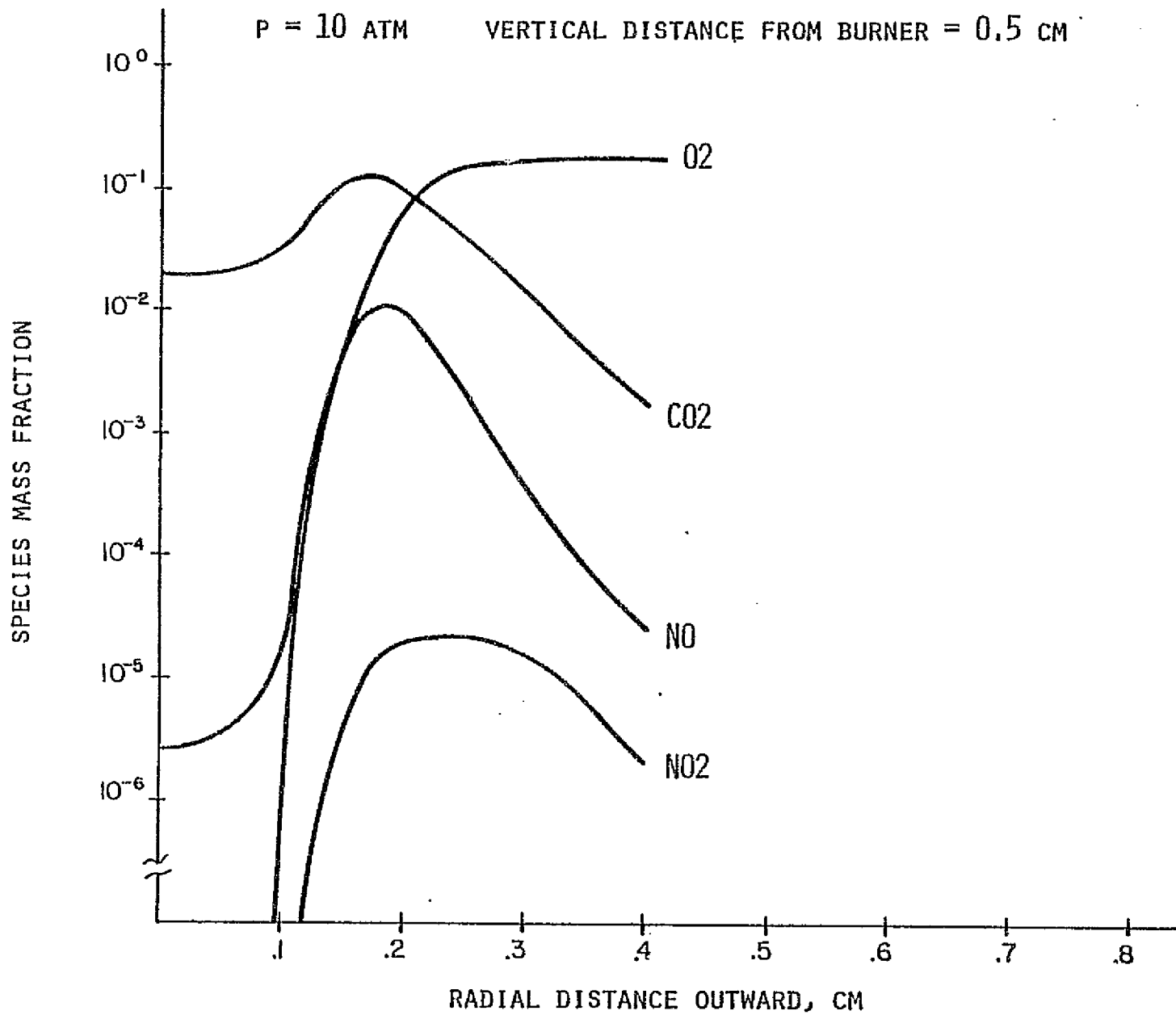


FIGURE 13 - SPECIES MASS FRACTION AS FUNCTION OF PRESSURE

P = 20 ATM

VERTICAL DISTANCE FROM BURNER = 0.5 CM

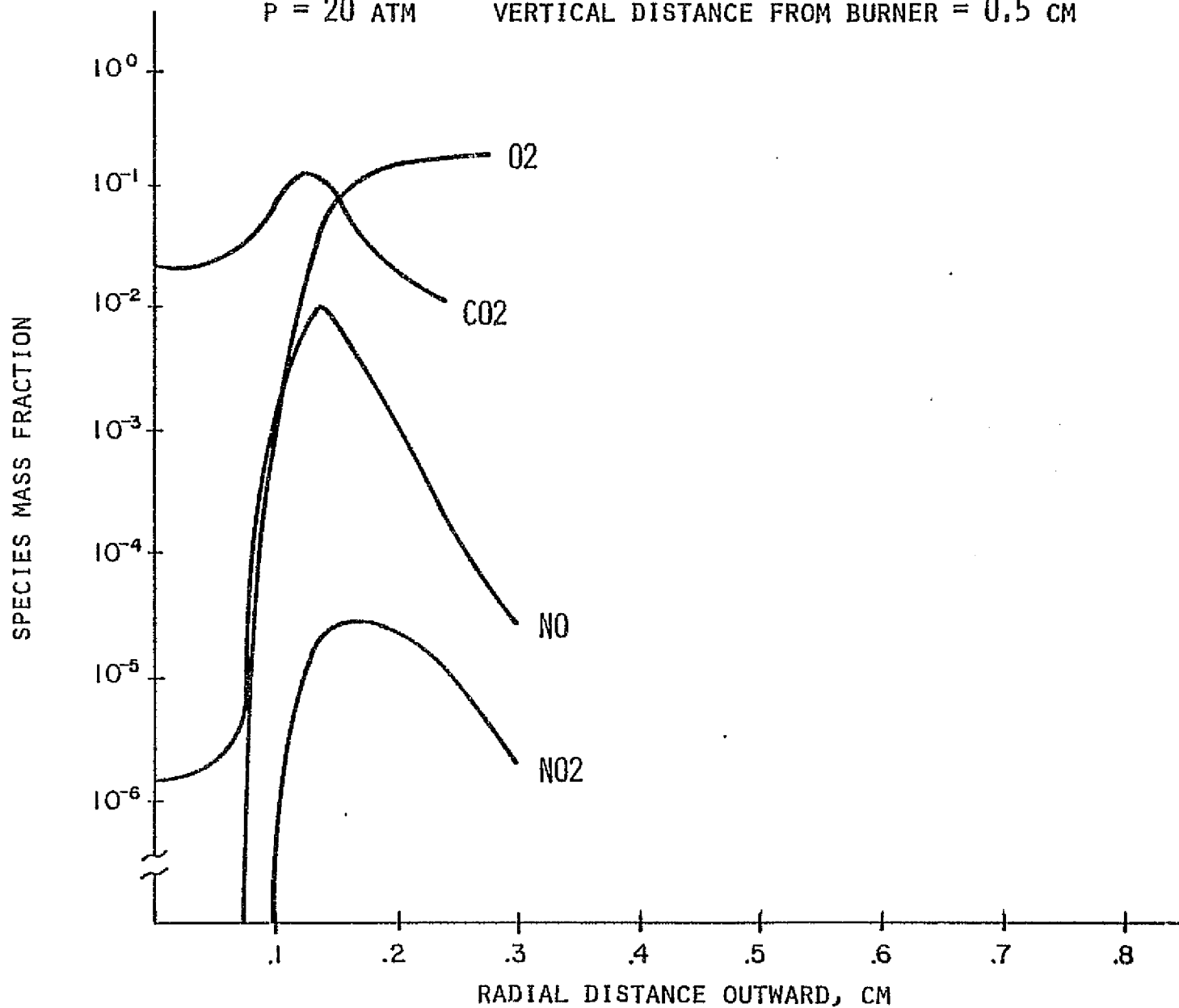


FIGURE 14 - SPECIES MASS FRACTION AS FUNCTION OF PRESSURE

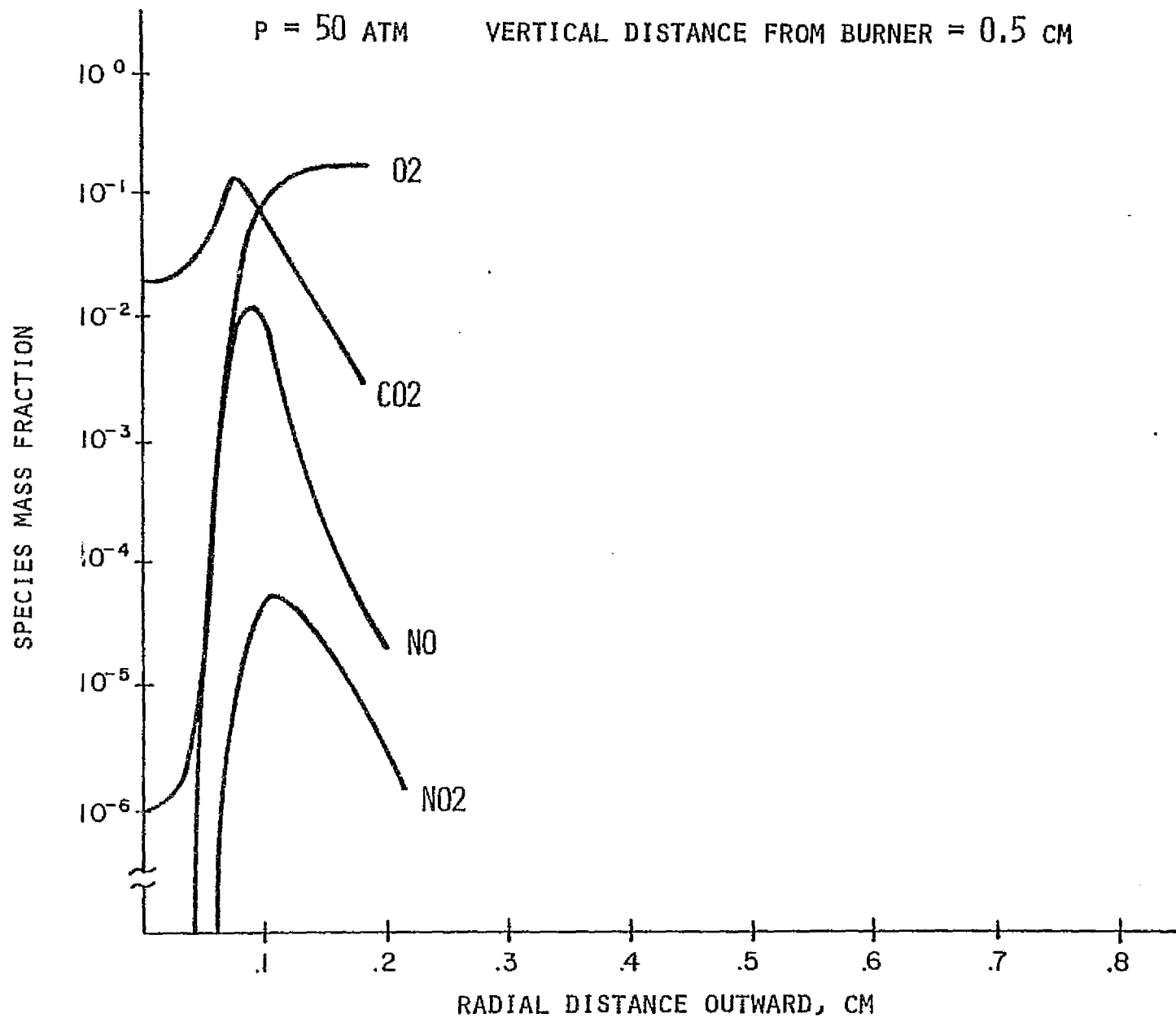


FIGURE 15 - SPECIES MASS FRACTION AS FUNCTION OF PRESSURE

VII. CONCLUSIONS

In order to reflect the physical system under consideration to an acceptable degree, the governing differential equations must be solved numerically. The algorithm utilized by the Patankar-Spalding computer code produces a solution that represents the hydrodynamic nature of the flow field extremely well. It has been found, however, that refinements must be made to the chemical reaction portion of the code in order to produce meaningful results. These refinements take the form of the Pratt-Wormeck chemical subroutine which has been incorporated into the Patankar-Spalding computer code.

The flame shapes for pressures of 1, 5, 10, 20, and 50 atm have been computed and agree remarkably well with experimental data. There is a noticeable shape change that occurs with increasing pressure and believed to be a result of buoyancy effects, which become increasingly important at higher pressures.

The species concentrations computed for the flow regime at hand seem to reflect the chemical aspect of combustion fairly well. The concentration profiles do not reflect much dependence on pressure, however, except in so far as position is concerned. Since the chemical mechanism incorporated into the program did not vary with pressure this is a somewhat expected result. It would be of considerable interest to change the input chemical mechanism with pressure and to note any resulting changes in the general shape of the concentration profiles.

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APPENDIX

Computer Listing and Sample Output

ISN 0060
ISN 0061

NT=NF+1
NE=NF+2

CHAPTER ***** MATERIAL CONSTANTS *****
S.I. UNITS

C SPECIES MOLECULAR WEIGHT ARE STORED IN SMW(K) N=1,NS
GASCON=KGAS
HMIX=29.
GAMMA=1.0
VISMIX=1.0-0

ISN 0062
ISN 0063
ISN 0064
ISN 0065

C C C
-----MODEL=1=LAMINAR, =2=TURBULENT.
-----INERT=1=INERT FLUID, OTHERWISE INERT=2
MODEL=1
INERT=2

ISN 0066
ISN 0067

ISN 0068
ISN 0069
ISN 0070
ISN 0071
ISN 0072
ISN 0073
ISN 0075
ISN 0076
ISN 0077
ISN 0078
ISN 0079
ISN 0080

C
PL=.7
PLEF=.80
DU 4 J=1,NF
PR(IJ)=PL
PR(FI,1)=PLEF
IF (MODEL.EQ.1) PRF(J,1)=PR(IJ)
+ CONTINUE
M=.7
AK=.435
ALMG=.09
FK=.033
UFAC=.01

CHAPTER ***** INITIAL CONDITIONS *****

ISN 0081
ISN 0082
ISN 0083
ISN 0084
ISN 0085
ISN 0086
ISN 0087
ISN 0088
ISN 0089
ISN 0090
ISN 0091
ISN 0092
ISN 0093
ISN 0094
ISN 0095
ISN 0096
ISN 0097
ISN 0098
ISN 0099
ISN 0100
ISN 0101
ISN 0102
ISN 0103
ISN 0104
ISN 0105

TKA=2000.
TKB=2000.
TKC=500.
TKD=500.
TWALL=500.
TKC=2000.
TND=2000.
TWALL=2000.
RA=0.
KB=0.
PRESS=20.00
TKA=1000.
TKB=1000.
TKC=1000.
TKD=1000.
TWALL=1000.
PRESS=1.00
KC=.100E-2
KD=.820E-2
KU=.100E-1
PI=3.141592054
AFLW=2400.
FFLW=41.8
FARL=F1+(IKC*100.)**2
AREA=PI*(IKD*100.)**2+FAREA

GEN00212
GEN00214
GEN00216
GEN00218
GEN00220
GEN00222
GEN00224
GEN00226
GEN00228
GEN00230
GEN00232
GEN00234
GEN00236
GEN00238
GEN00240
GEN00242
GEN00244
GEN00246
GEN00248
GEN00250
GEN00252
GEN00254
GEN00256
GEN00258
GEN00260
GEN00262
GEN00264
GEN00266
GEN00268
GEN00270
GEN00272
GEN00274
GEN00276
GEN00278
GEN00280

GEN00282
GEN00284
GEN00286

GEN00288
GEN00290
GEN00292
GEN00294
GEN00296
GEN00298
GEN00300
GEN00302

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1SN 0106 UB=FFLW*(TKB/273.1+(1.E5/PRESS)*(1./FAREA)
1SN 0107 UC=APLW*(TAC/273.1+(1.E5/PRESS)*(1./FAREA)
1SN 0108 UB=UB/0.000.
1SN 0109 UC=UC/0.000.
1SN 0110 UA=UB
1SN 0111 UC=UC
1SN 0112 KB=KC
1SN 0113 PA=PRESS
1SN 0114 UPLDX=0.
1SN 0115 K(A)=KC
1SN 0116 KUUT=RU
C ESTABLISH PROPERTIES OF FUEL STREAM
1SN 0117 TR=TKA
1SN 0118 CALL CKEAU.
1SN 0119 UC 551 K=1,NS
C133 IUCU USED TO IDENTIFY C4, THE FUEL
1SN 0120 IF (SZ(K).GT.0.) IUCU=K
1SN 0121 IF (SZ(K).LT.1INY) SZ(K)=1INY
1SN 0122 FA(K)=SZ(K)
1SN 0123 FB(K)=SZ(K)
1SN 0124 551 CONTINUE
C44 AKKCON USED TO SAVE INLET STREAM FUEL MOLE NUMBER
1SN 0127 SZFUEL=SZ(IUCU)
1SN 0128 FAINF)=HS0L0
1SN 0129 FBINF)=HS000
1SN 0130 FAINT)=TK
1SN 0131 FBINT)=TK
1SN 0132 FA(NE)=100000.
1SN 0133 FB(NE)=100000.
1SN 0134 KUA=RHUP
1SN 0135 KUB=RHUP
C ESTABLISH PROPERTIES OF AIR STREAM
1SN 0136 TR=TKD
1SN 0137 CALL CKERC
1SN 0138 UC 552 K=1,NS
1SN 0139 IF (SZ(K).LT.1INY) SZ(K)=1INY
1SN 0140 FC(K)=SZ(K)
1SN 0141 FD(K)=SZ(K)
1SN 0142 552 CONTINUE
1SN 0143 FCINF)=HS000
1SN 0144 FDINF)=HS000
1SN 0145 FCINT)=TK
1SN 0146 FDINT)=TK
1SN 0147 FC(NE)=0.
1SN 0148 FD(NE)=0.
1SN 0149 KUC=RHUP
1SN 0150 KUD=RHUP
1SN 0151 FLUA=RUA*UA*.5*(KB**2
1SN 0152 FLUB=RUB*UB*.5*(KB**2-KB**2)
1SN 0153 FLUC=RUC*UC*.5*(KB**2-KC**2)
1SN 0154
C
1SN 0155 UMDIV=FLUB/(FLUB+FLUC)
C ----- SEQUENCE TO PUT CELL BOUNDARY AT UMDIV.
1SN 0156 IF (UMDIV.EQ.0. OR UMDIV.EQ.1.) GO TO 55
1SN 0158 UC 55 I=3,NP

```

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GENC0304
GENC0306
GENC0308
GENC0310
GENC0312
GENC0314
GENC0316
GENC0318
GENC0320
GENC0322
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GENC0326
GENC0328
GENC0330
GENC0332
GENC0334
GENC0336
GENC0338
GENC0340
GENC0342
GENC0344
GENC0346
GENC0348
GENC0350
GENC0352
GENC0354
GENC0356
GENC0358
GENC0360
GENC0362
GENC0364
GENC0366
GENC0368
GENC0370
GENC0372
GENC0374
GENC0376
GENC0378
GENC0380
GENC0382
GENC0384
GENC0386
GENC0388
GENC0390
GENC0392
GENC0394
GENC0396
GENC0398
GENC0400
GENC0402
GENC0404
GENC0406
GENC0408
GENC0410
GENC0412

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ISN 0209          IFIN=1                                GEN00524
ISN 0210          GU TO 1011                             GEN00526
C                                                         GEN00528
ISN 0211          15 XU=XU+LX                             GEN00530
C               ----- FURTHER ADJUSTMENTS TO DX ARE MADE IN CHAPTERS 8 AND 9. GEN00532
C               ----- ADJUST LONGITUDINAL CONDITIONS ----- GEN00534
C               CHAPTER 8A BOUNDARY CONDITIONS          GEN00536
C               CHAPTER 8A BOUNDARY CONDITIONS          GEN00538
ISN 0212          IF (ISTEP-1AX) 8000,80,84              GEN00540
ISN 0213          8000 IF (ISTEP-1END) 8002,83,84        GEN00542
C               ----- WALL -----                   GEN00544
C               8002 KIN=1                                GEN00546
ISN 0214          U(1)=0.                                GEN00548
ISN 0215          IF (ISTEP.EQ.0) TAUI=0.                GEN00550
ISN 0216          EWALL=.5.                              GEN00552
ISN 0217          DO 81 J=1,NP                           GEN00554
ISN 0218          INDE(J)=2                               GEN00556
ISN 0219          81 ADEL(J)=0.                           GEN00558
ISN 0220          KMI=0.                                  GEN00560
ISN 0221          GU TO 84                                GEN00562
ISN 0222          -----FREE -----                   GEN00564
ISN 0223          82 KIN=2                                GEN00566
ISN 0224          TAUI=0.                                 GEN00568
ISN 0225          U(1)=0.                                 GEN00570
ISN 0226          KU(1)=KMU(1)+U(1)                      GEN00572
ISN 0227          DO 83 K=1,NE                            GEN00574
ISN 0228          83 F(K,1)=FAIK)                         GEN00576
ISN 0229          831 CONTINUE                           GEN00578
ISN 0230          GU TO 84                                GEN00580
ISN 0231          ----- ADJUSTMENT WHEN PIPE AXIS IS REACHED. ----- GEN00582
C               80 KIN=3                                  GEN00584
ISN 0232          KMI=0.                                  GEN00586
ISN 0233          K(1)=0.                                 GEN00588
ISN 0234          PS(1)=0.                                GEN00590
ISN 0235          TAUI=0.                                 GEN00592
ISN 0236          ----- E BOUNDARY -----             GEN00594
ISN 0237          84 IF (ISTEP-1OUT) 8004,83,85          GEN00596
C               ----- WALL -----                   GEN00600
ISN 0238          8004 KEX=1                               GEN00602
ISN 0239          J(NP3)=0.                               GEN00604
ISN 0240          KME=0.                                  GEN00606
ISN 0241          IF (ISTEP.EQ.0) TAUE=0.                GEN00608
ISN 0242          EWALL=.5.                              GEN00610
ISN 0243          DO 82 J=1,NP                           GEN00612
ISN 0244          INDE(J)=2                               GEN00614
ISN 0245          82 ADEL(J)=0.                           GEN00616
ISN 0246          INDE(1)=1                               GEN00618
ISN 0247          FIN(1,NP3)=1WALL                       GEN00620
ISN 0248          TK=1WALL                                GEN00622
ISN 0249          INCLPS=1                                GEN00624
ISN 0250          MSCUM=0.                                GEN00626
ISN 0251          CALL HCLPS                               GEN00628
ISN 0252          DO 82 K=1,NE                            GEN00630
ISN 0253          MSCUM=MSCUM+F(K,NP3)+F(0,K)            GEN00632
ISN 0254

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ISN 0255      821 CONTINUE
ISN 0256      MSUB0=MSUM+RGAS*TK
ISN 0257      FINH,NP3)=MSUB0
ISN 0258      GO TO 86
C --- FREE
ISN 0259      85 KEX=Z
ISN 0260      TAUE=C.
ISN 0261      U(NP3)=UU
ISN 0262      RU(NP3)=RHU(NP3)+U(NP3)
ISN 0263      UU 851 K=1,NE
ISN 0264      F(K,NP3)=FU(K)
ISN 0265      851 CONTINUE
ISN 0266      RHU(NP3)=RDU
C CHAPTER 88 DUCT GEOMETRY
ISN 0267      88 IF (ISTEP.EQ.1001) GO TO 89
ISN 0268      IF (ISTEP.GT.8) GO TO 87
ISN 0271      RCU1=RU
ISN 0272      ADUU=(R(NP3)**2-R(1)**2)*.5
ISN 0273      87 YDUCT=RCU1-R(1)
ISN 0274      ADUU=ADUU
ISN 0275      AIN=R(1)**2+.5*DFLUAT(1)/KIN)
ISN 0276      IF (ISTEP.EQ.1END) ADUU=.5*RCU1**2
ISN 0277      AFLU=R(NP3)**2+.5-AIN
ISN 0278      AEX=AFLU-ADUU
ISN 0280      AEXU=AEX/AFLU
ISN 0281      IF(XD.EQ.XEND.OR.XL.EQ.XOUT.OR.XD.EQ.XOLAST.OR.IAX.EQ.1STEP+1)
1          GO TO 88
          IF(DABS(AEXU).GT.AEXULM) UX=UX*AEXULM/DABS(AEXU)
          XD=XD+UX
ISN 0283      88 RCU1=RCU1+IAN*UX
ISN 0284      ADUU=RCU1**2+.5-AIN
ISN 0285      UA=AFAL*(ADUU-AFLU)
C
C CHAPTER 89 SUBSONIC PRESSURE GRADIENT
ISN 0289      89 UBAR=C.
ISN 0290      DO 820 I=2,NP1
ISN 0291      820 UBAR=UBAR+(U(I)+U(I+1))*UMD(I)
ISN 0292      UBAR=.5*UBAR
ISN 0293      IF(KIN.EQ.2) UBAR=(UBAR-UA)*PE1/PSIE+UA
C SUBSONIC FLOW
ISN 0295      803 IF (ISTEP=1001) 822,823,900
ISN 0296      823 DPODX=C.
ISN 0297      GO TO 824
C UNFINISHED SUBSONIC FLOW
ISN 0298      822 FLU101=PSIE-PSI1*FLUAT(1)/KIN)
ISN 0299      DYNMED=UBAR*FLU101/AFLU
ISN 0300      DPODX=(DYNMED+UA/UX-IAU1*K(1)-IAUE*K(NP3)+Z.*RME*UBAR)/ADUU
ISN 0301      824 DP=DPDX+UA
ISN 0302      DO 825 I=1,NP3
ISN 0303      825 DPDX(I)=DPDX
C TESTS
ISN 0304      IF(1TEST) 802,801,802
ISN 0305      802 LAB=1
ISN 0306      WRITE(C,I) LAB,UBAR,DYNMED,UX,UA,DPODX,AEXU,RMI

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GENC0634
GENC0636
GENC0638
GENC0640
GENC0642
GENC0644
GENC0646
GENC0648
GENC0650
GENC0652
GENC0654
GENC0656
GENC0658
GENC0660
GENC0662
GENC0664
GENC0666
GENC0668
GENC0670
GENC0672
GENC0674
GENC0676
GENC0678
GENC0680
GENC0682
GENC0684
GENC0686
GENC0688
GENC0690
GENC0692
GENC0694
GENC0696
GENC0698
GENC0700
GENC0702
GENC0704
GENC0706
GENC0708
GENC0710
GENC0712
GENC0714
GENC0716
GENC0718
GENC0720
GENC0722
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GENC0732
GENC0734
GENC0736
GENC0738
GENC0740
GENC0742

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1 5H KEX=,12,4H UX=, D11.3,6H PSII=,D11.3,6H PSIE=,D11.3/
 2 5H KMI=,D11.3,5H KME=,D11.3,5H PEI=,D11.3)

GEN00958
 GEN00960
 GEN00962
 GEN00964
 GEN00966
 GEN00968
 GEN00970
 GEN00972
 GEN00974
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 GEN00992
 GEN00994
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 GEN01000
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 GEN01038
 GEN01040
 GEN01042
 GEN01044
 GEN01046
 GEN01048
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 GEN01052
 GEN01054
 GEN01056
 GEN01058
 GEN01060
 GEN01062
 GEN01064
 GEN01066

ISN 0401
 ISN 0402
 ISN 0403
 ISN 0404
 ISN 0405
 ISN 0406
 ISN 0407
 ISN 0408
 ISN 0409
 ISN 0410
 ISN 0411

 ISN 0412
 ISN 0413
 ISN 0414
 ISN 0415
 ISN 0416
 ISN 0417
 ISN 0418
 ISN 0419
 ISN 0420
 ISN 0421

 ISN 0422
 ISN 0423

 ISN 0424
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 ISN 0431
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 ISN 0439
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 ISN 0444
 ISN 0445

 ISN 0446
 ISN 0447
 ISN 0448

```

C
C
      UBAR=0.
      DO 1020 J=1,NF
1020  FLUX(J)=0.
      DO 1021 I=2,NP1
      UBAR=UBAR+UMD(I)*UG(I)+U(I+1)
      DO 1021 J=1,NF
1021  FLUX(J)=FLUX(J)+UMD(I)*(F(J,I)+F(J,I+1))
      UBAR=.5*UBAR
      UFLUX=PEI*UBAR
      DO 1022 J=1,NF
1022  FLUX(J)=.5*PEI*FLUX(J)
C
      UREF=UBAR
      RUKCF=PEI/.5/(K(I,1)+K(INP3))/Y(INP3)
      DO 1023 J=1,NF
      UFI(J)=FLUX(J)/PEI-F(J,I)
1023  DFE(J)=DFE(J)+F(J,I)-F(J,NP3)
      UFLUX=UFLUX-PEI*U(INP3)+U(I)*PSII
      DO 1041 K=1,NF
      FLUX(K)=FLUX(K)-PSIE*FU(K)+FA(K)*PSII
1041  CONTINUE
      PRESSD=PRESS/PRESS1-1.
C
      WRITE(6,1031) XU,UFLUX,PRESSD,AEXD,(FLUX(J),J=1,NF)
1031  FORMAT(4H XU=, D11.3,7H UFLUX=,D11.3,8H PRESSD=,D11.3,
      1 6H AEXD=,D11.3,9H FLUX(J)= /10D12.3/10D12.3/10D12.3/)
C
      IF(KIN.NE.1) GO TO 1024
      LAUD=LAU/UREF/RUKCF
      DO 1025 J=1,NF
1025  AJID(J)=AJID(J)/RUKCF/DFE(J)
      WRITE(6,1029) KIN,LAUD,(AJID(J),J=1,NF)
1029  FORMAT(5H KIN=,12,7H LAUD=,2PD11.3,9H AJID(J)=,/3(10D12.3/))
1024  IF (KEX.NE.1) GO TO 1026
      LAUED=LAU/UREF/RUKCF
      DO 1027 J=1,NF
1027  AJED(J)=AJE(J)/RUKCF/DFE(J)
      WRITE(6,1028) KEX,LAUED,(AJED(J),J=1,NF)
1028  FORMAT(5H KEX=,12,7H LAUED=,2PD11.3,9H AJED(J)=,/3(10D12.3/))
1026  CONTINUE
CHAPTER 100
      IF (IPRINT.EQ.1) GO TO 110
      LAB=9
      DIV=1.
      DO 1095 I=2,NP3
1095  UUI(I)=Y(I)/DIV
      WRITE(6,100) LAB,K(I),(UUI(I),I=2,NP2),Y(NP3)
C
      LAB=10
      SUB=C.
      DIV=1.
    
```

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ISN 0449      DU 1094 I=2,NP3
ISN 0450      1094 OUT(I)=(U(I)-SUB)/DIV
ISN 0451      IF (NLEVEL.NE.1)
ISN 0452      1WRITE(10,100) LAB,U(I),1OUT(I),I=2,NP2),U(NP2)
ISN 0453      NY=1
C
ISN 0454      WRITE (10,997) (ASUB(K,1),ASUB(K,2),K=1,NS),1OUT(J),J=1,10)
ISN 0455      997 FORMAL (LHO,OA,44MMASS FRACTIONS,ENTHALPY,TEMP,F/A EQUIV RATIO,
1 42MCELL LOADING EMV (KG/M 3-3), CELL RES TIME/BNO STA. ,
2 12(2A+,2X)/6X,12(2A+,2X)/)
ISN 0456      DU 999 I=1,NP3
ISN 0457      DU 300 J=1,NS
ISN 0458      OUT(J)=F(I,1)*SMW(J)
C
ISN 0459      SUPPRESS PRINTOUT OF MASS FRAC.LE.1.0-10
ISN 0460      IF (OUT(J).LT.1.0-10) OUT(J)=0.
ISN 0461      300 CONTINUE
ISN 0462      IF (1STEP.EQ.0) GO TO 301
ISN 0463      IF (1.EQ.1.UR.1.EQ.NP3) GO TO 301
ISN 0464      OUT(NF)=L(1)/S U(3,1)
ISN 0465      OUT(NI)=FOUT(I)/OUT(NF)
ISN 0466      IF (.NOT.LREAL1) GO TO 302
ISN 0467      IF (.EQVIL) OUT(NF)=0.
ISN 0468      IF (.LEQVIL) OUT(NI)=1000000.
ISN 0469      GO TO 302
ISN 0470      301 CONTINUE
ISN 0471      OUT(NF)=0.
ISN 0472      OUT(NI)=0.
ISN 0473      302 CONTINUE
ISN 0474      WRITE (10,998) 1,(OUT(K),K=1,NS),1F(K,1),K=NH,NE),OUT (NF),OUT (NI)
ISN 0475      998 FORMAL (1H ,10,1P12D10.2/6X,1P12D10.2/6X,1P12D10.2)
ISN 0476      999 CONTINUE
ISN 0477      CHAPTER 11 11 11 11 11 11 11 11 11 11 11 11 END OF MAIN LOOP
ISN 0478      110 IF(1STEP.GE.LASTEP.UR.XU.GE.XULAST.UR.1FIN.NE.0) GO TO 111
C
ISN 0479      -----STRIDE3-----STRIDE3-----STRIDE3-----STRIDE3
ISN 0480      CALL STRIDE(3)
ISN 0481      IF(1FIN) 1011,00,111
C
C
C ----- TERMINATION
ISN 0482      111 WRITE(10,112) 1STEP,LASTEP,XU,XULAST,1FIN
ISN 0483      112 FORMAL(120H TERMINATED WITH 1STEP=,10,8H LASTEP=,10,
1 4H XU=,2P11.3,8H XULAST=,011.3,6H 1FIN=,13)
C
ISN 0484      120 CONTINUE
ISN 0485      STOP
ISN 0486      100 FORMAL(11H ,10, 11D11.3/19X,11D11.3))
ISN 0487      101 FORMAL(11H ,18,11111)
ISN 0488      END
GEN01072
GEN01074
GEN01076
GEN01078
GEN01080
GEN01082
GEN01084
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GEN01166

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*OPTIONS IN EFFECT#NAME(MAIN) NOOPTIMIZE LINECOUNT(57) SIZE(MAX) AUTODECLINE)

*OPTIONS IN EFFECT*SOURCE EBDIC NOLIST NOCHECK OBJECT NUMAP NOFORMAT NOJUSTM NOXREF NOALC NUANSF TERM FL)

STATISTICS SOURCE STATEMENTS = 491, PROGRAM SIZE = 10176, SUBPROGRAM NAME = MAIN

STATISTICS NO DIAGNOSTICS GENERATED

REQUESTED OPTIONS:

OPTIONS IN EFFECT: NAME(MAIN) NOOPTIMIZE LIRECOUNT(57) SIZE(MAX) AUTOUBL(NONE) SOURCE EBCDIC NULIST NUDECK OBJECT NOMAP NOFORMAT NOGOSTMT NOXREF NUALL NUANSF TERM FLA

ISN 0002 SUBROUTINE AUX GENC1150
ISN 0003 IMPLICIT REAL*8 (A-H,U-Z) GENC1152
ISN 0004 DIMENSION ASUB(20,3) GENC1154
ISN 0005 COMMON/CUMA/A(43),AJE(22),AJ1(22),B(43),C(43),CSALFA,D(43),DPDX(43) GENC1156
1) DA,EMU(43),F(22,43),IAA,IEND,IFIN,INDE(22),IND1(22),IOUT,IUUMY, GENC1158
2) ISTEP,IIES1,IUKAP,JS,JSH,JY,KEX,KIN,KRAD,N,ND2,NF,NOVEL,NP1, GENC1160
3) NP2,NP3,UM(43),UMU(43),P(43),PE1,PK(22),PREF(22,43),PSIE,PSI1,K146 GENC1162
43),KMU(43),RME,RM1,KU(43),SU(5,43),TAUC,IAU1,U(43),XU,XU,SU(5,43), GENC1164
5) Y(43),YE,Y1 GENC1166
ISN 0006 COMMON/CUMG/AK,ALMG,ANKOUN,EWALL,FR,M,HFU,INERT,MASSTR,NDUMY, GENC1168
1 MODEL,UXDFU,PREEAF,PRESS,UBAR,UFAC GENC1170
C/----- SUBROUTINE FOR PROGRAM GENMIX 4A GENC1172
ISN 0007 DIMENSION YEDGE(8),US(43) GENC1174
ISN 0008 EQUIVALENCE (UPDX(1),US(1)) GENC1176
C GENC1178
C C C C C GENC1180
C C C C C GENC1182
C C C C C GENC1184
C C C C C GENC1186
C C C C C GENC1188
ISN 0009 IF(MODEL.EQ.1) GO TO 200 GENC1190
ISN 0011 UMAX=0. GENC1192
ISN 0012 UMIN=0. GENC1194
ISN 0013 DO 1 I=1,NP3 GENC1196
ISN 0014 UMAX=UMAX+(UMAX,U(1)) GENC1198
ISN 0015 1 JMIN=UMIN+(UMIN,U(1)) GENC1200
ISN 0016 UUMAX=UMAX-UMIN GENC1202
ISN 0017 DUDYMN=FR*UUMAX/Y(NP3) GENC1204
ISN 0018 DO 10 I=2,NP1 GENC1206
ISN 0019 S U(1,I)=(U(1+1)-U(1))/(Y(1+1)-Y(1)) GENC1208
ISN 0020 IF(DABS(S U(1,I))-DUDYMN) 111,111,112 GENC1210
ISN 0021 111 S U(2,I)=0. GENC1212
ISN 0022 GO TO 10 GENC1214
ISN 0023 112 S U(2,I)=1. GENC1216
ISN 0024 10 CONTINUE GENC1218
ISN 0025 IF(KIN.EQ.1) S U(2,2)=1. GENC1220
ISN 0027 IF(KEY.EQ.1) S U(2,NP1)=1. GENC1222
ISN 0029 S U(2,I)=0. GENC1224
C ----- TEST 7 GENC1226
ISN 0030 IF(IIES1) 17,16,17 GENC1228
ISN 0031 17 LAB=11 GENC1230
ISN 0032 WRITE(10,100) LAB,DUDYMN,FR,AK,ALMG,UBAR GENC1232
ISN 0033 LAB=12 GENC1234
ISN 0034 WRITE(10,100) LAB,(S U(1,2),I=1,NP3) GENC1236
ISN 0035 LAB=13 GENC1238
ISN 0036 WRITE(10,100) LAB,(S U(2,I),I=1,NP3) GENC1240
ISN 0037 10 CONTINUE GENC1242
C ----- GENC1244
ISN 0038 K=1 GENC1246
ISN 0039 DO 13 L=1,6 GENC1248


```

ISN 0040      13 YEDGE(L)=Y(NP3)
ISN 0041      DO 11 I=2,NP1
ISN 0042      IF(S U(2,I)-S U(2,I-1)) 110,11,110
ISN 0043      110 YEDGE(N)=Y(I)
ISN 0044      K=K+1
ISN 0045      IF(K.GE.6) GO TO 14
ISN 0047      11 CONTINUE
ISN 0048      14 EL12=(YEDGE(2)-YEDGE(1))*ALMG
ISN 0049      EL34=(YEDGE(4)-YEDGE(3))*ALMG
ISN 0050      EL56=(YEDGE(6)-YEDGE(5))*ALMG
ISN 0051      EL23=.5*(EL12+EL34)
ISN 0052      EL45=.5*(EL34+EL56)

```

GEN01250
GEN01252
GEN01254
GEN01256
GEN01258
GEN01260
GEN01262
GEN01264
GEN01266
GEN01268
GEN01270
GEN01272

----- TEST 8

```

ISN 0053      IF(11EST) 19,18,19
ISN 0054      19 LAB=14
ISN 0055      WRITE(6,100) LAB
ISN 0056      LAB=15
ISN 0057      WRITE(6,100) LAB,EL12,EL23,EL34,EL45,EL56
ISN 0058      LAB=16
ISN 0059      WRITE(6,100) LAB,(YEDGE(I),I=1,6)
ISN 0060      18 CONTINUE

```

GEN01274
GEN01276
GEN01278
GEN01280
GEN01282
GEN01284
GEN01286
GEN01288
GEN01290
GEN01292

```

ISN 0061      DO 12 I=2,NP1
ISN 0062      IF(Y(I)-YEDGE(I)) 120,121,121
ISN 0063      121 IF(Y(I)-YEDGE(2)) 122,123,123
ISN 0064      123 IF(Y(I)-YEDGE(3)) 124,125,125
ISN 0065      125 IF(Y(I)-YEDGE(4)) 126,127,127
ISN 0066      127 IF(Y(I)-YEDGE(5)) 128,129,129
ISN 0067      120 S U(3,I)=0.
ISN 0068      GO TO 130
ISN 0069      122 S U(3,I)=EL12
ISN 0070      GO TO 130
ISN 0071      124 S U(3,I)=EL23
ISN 0072      GO TO 130
ISN 0073      126 S U(3,I)=EL34
ISN 0074      GO TO 130
ISN 0075      128 S U(3,I)=EL45
ISN 0076      GO TO 130
ISN 0077      129 S U(3,I)=EL56

```

GEN01294
GEN01296
GEN01298
GEN01300
GEN01302
GEN01304
GEN01306
GEN01308
GEN01310
GEN01312
GEN01314
GEN01316
GEN01318
GEN01320
GEN01322
GEN01324
GEN01326

----- UPPER LIMITS TO MIXING LENGTH

```

ISN 0078      130 S U(3,I)=DMIN(15 U(3,I),.5*UDMAX/(UABS(S U(1,I))+1.0-30))
ISN 0079      IF(KIN-1) 131,132,131
ISN 0080      132 S U(3,I)=DMIN(15 U(3,I),AK*.5*(Y(I)+Y(I+1)))
ISN 0081      131 IF(KEX-1) 12,135,12
ISN 0082      135 S U(3,I)=DMIN(15 U(3,I),AK*(Y(NP3)-.5*(Y(I)+Y(I+1))))
ISN 0083      12 CONTINUE

```

GEN01328
GEN01330
GEN01332
GEN01334
GEN01336
GEN01338
GEN01340
GEN01342

----- TEST 9

```

ISN 0084      IF(11EST) 109,108,109
ISN 0085      109 LAB=17
ISN 0086      WRITE(6,100) LAB
ISN 0087      LAB=18
ISN 0088      WRITE(6,100) LAB,(S U(3,I),I=1,NP3)
ISN 0089      108 CONTINUE

```

GEN01344
GEN01346
GEN01348
GEN01350
GEN01352
GEN01354
GEN01356

----- VISCOSITIES

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C ----- LAMINAR VISCOSITIES FOR CELL BOUNDARIES
ISN 0090 200 DO 23 I=2,NP1
ISN 0091 23 EMU(I)=.5*(EMU(I)+EMU(I+1))
ISN 0092 IF(MODEL.EQ.1) GO TO 29

C ----- TURBULENT CONTRIBUTION
ISN 0094 DO 20 I=2,NP1
ISN 0095 DUDYL=DABS(S U(I,1)*S U(3,1))
ISN 0096 UDMIN=UFAC*.5*(U(I)+U(I+1))
ISN 0097 DUDYL=DMAX1(DUDYL,UDMIN)
ISN 0098 RHM=.5*(RHO(I)+RHO(I+1))
ISN 0099 CMU=NHM*S U(3,1)*DUDYL

C ----- IN THIS VERSION, THE TURBULENT AND LAMINAR CONTRIBUTIONS
C ARE SIMPLY ADDED. AN ALTERNATIVE WOULD BE TO INTRODUCE
C THE VAN DRIEST DAMPING FUNCTION.
ISN 0100 CMU(I)=EMU(I)+CMU
ISN 0101 CONTINUE

C ----- TEST 10
ISN 0102 IF(ITE=1) 202,201,202
ISN 0103 LAB=19
ISN 0104 WRITE(10,100) LAB
ISN 0105 LAB=20
ISN 0106 WRITE(10,100) LAB,(EMU(I),I=1,NP1)
ISN 0107 LAB=21
ISN 0108 WRITE(10,100) LAB,(S U(I,1),I=1,NP1)
ISN 0109 201 CONTINUE

C ----- MODIFICATION OF EMU ARRAY
ISN 0110 29 DO 24 I=2,NP1
ISN 0111 24 EM U(I)=EMU(I)/(Y(I+1)-Y(I))
ISN 0112 IF(KKAD.EQ.0) GO TO 25
ISN 0114 DO 26 I=2,NP1
ISN 0115 26 EM U(I)=EM U(I)+.5*(K(I)+K(I+1))
ISN 0116 25 IF (1STEP) 28,28,300
INITIAL PKEF S.
ISN 0117 26 DO 27 J=1,NF
ISN 0118 DO 27 I=1,NP3
ISN 0119 27 PKEF(J,I)=PKEF(J,I)
S S S S S S SOURCES
C VELOCITY U
ISN 0120 300 DO 307 I=2,NP2
ISN 0121 307 S U(3,I)=PEI*(UM(I+1)-UM(I-1))/RHO(I)/U(I)
ISN 0122 GO TO (310,312,312), KIN
ISN 0123 310 S U(3,2)=(K(1)+.5*(K(2)+K(3)))*YI
ISN 0124 GO TO 313
ISN 0125 312 S U(3,2)=PEI*UM(3)/RHO(3)/U(3)
ISN 0126 313 GO TO (314,315,315), KEX
ISN 0127 314 S U(3,NP2)=(K(NP3)+.5*(K(NP1)+K(NP2)))*YE
ISN 0128 GO TO 316
ISN 0129 315 S U(3,NP2)=PEI*(1.-UM(NP1))/RHO(NP1)/U(NP1)
ISN 0130 316 CONTINUE
ISN 0131 DO 308 I=2,NP2
ISN 0132 308 US(I)=UPUR(I)+SU(3,I)
ISN 0133 IF (INF.EQ.0) RETURN
ISN 0135 RETURN
ISN 0136 100 FORMAT(11M,10, 11D11.5/19X,11D11.5)
ISN 0137 END

```

GEN01360
GEN01362
GEN01364
GEN01366
GEN01368
GEN01370
GEN01372
GEN01374
GEN01376
GEN01378
GEN01380
GEN01382
GEN01384
GEN01386
GEN01388
GEN01390
GEN01392
GEN01394
GEN01396
GEN01398
GEN01400
GEN01402
GEN01404
GEN01406
GEN01408
GEN01410
GEN01412
GEN01414
GEN01416
GEN01418
GEN01420
GEN01422
GEN01424
GEN01426
GEN01428
GEN01430
GEN01432
GEN01434
GEN01436
GEN01438
GEN01440
GEN01442
GEN01444
GEN01446
GEN01448
GEN01450
GEN01452
GEN01454
GEN01456
GEN01458
GEN01460
GEN01462
GEN01464
GEN01466
GEN01468

REQUESTED OPTIONS:

OPTIONS IN EFFECT: NAME(MAIN) NOOPTIMIZE LINECOUNT(57) SIZE(MAX) AUTOUBL(NONE) SOURCE EBCDIC NOLIST NODECK OBJECT NUMAP NUFORMAT NUGUSIMI NUXREF NUALLC NUANSF TERM FLA

```

ISN 0002      SUBROUTINE SIRIDE1(SW)                                GENU1470
ISN 0003      IMPLICIT REAL*8 (A-H,O-Z)                          GENU1472
ISN 0004      LOGICAL LADIAB,LEQUIL,LKREAL,LDEBUB,LBORN          GENU1474
ISN 0005      DIMENSION ASUB(20,3)                                GENU1476
ISN 0006      COMMON                                              GENU1478
                1/LCHEM1/LPSUM,FQ,PPLN,RGAS,KGASIN,SMINV,IKINV,ILN,LCUNVB,LNRG  GENU1480
                1/CINDEX/IDCU,IDCU2,IUM2,IUM2U,IUN2,IUU2,IMCPS,ILC,ILM,IMAT,ITEK,  GENU1482
                2      JJ,N1,N2,N3,NA,NGLUB,NGLUBP,NLM,NW,NSM          GENU1484
                2/LPARAM/ASUB,N1,NE,EMV,EN,HSUBD,INDEBUB,NS,PA,QU,U1,U2,U3,U4,RHUP,  GENU1486
                2      SM,S1(20),S2(20),IK,LADIAB,LDEBUB,LEQUIL,LKREAL  GENU1488
ISN 0007      COMMON/UMM/A(43),AJE(22),AJI(22),B(43),C(43),CSALFA,U(43),DPOX(43)  GENU1490
                1),DX,EMU(43),F(22,43),IAX,IEND,IFIN,INDE(22),INDI(22),IUU1,UDUMY,  GENU1492
                2  ISTEP,IIEE1,IUKAP,JS,JSW,JV,JY,KEA,KIN,KFAU,N,NJ2,NF,NOVEL,NP1,  GENU1494
                3  NP2,NP3,UM(43),UMU(43),P(43),PE1,PREF(22,43),PSIC,PS11,KI(43)  GENU1496
                43),KMU(43),KME,KM1,KU(43),SD(5,43),IAUC,IAU1,U(43),XU,XU,SD(5,43),  GENU1498
                5  Y(43),YC,YI                                          GENU1500
ISN 0008      COMMON/CMB/AK,ALMG,ARKLUN,EWALL,FR,M,HFU,INERT,MASTR,NDUMY,      GENU1502
                1  MODEL,UAUFU,PKEEXP,PRESS,UBAK,UFAL                    GENU1504
C/----- SUBROUTINE FOR PROGRAM GENMIX 4A                          GENU1506
C/ THIS SUBROUTINE PERFORMS THE SAME OPERATIONS AS THE ONE IN GENMIX4A  GENU1508
C BUT MORE ECONOMICALLY. THE A,B,C ARRAYS ARE ONE-DIMENSIONAL. SOME  GENU1510
C OFTEN USED FUNCTIONS OF UM ARE STORED, AND A D ARRAY SAVES          GENU1512
C UNNECESSARY ARITHMETIC IN THE IUMA OPERATION.                       GENU1514
C-----
ISN 0009      DIMENSION AZ(22),ANP2(22),B2(22),BNP2(22),C2(22),CNP2(22),D2(22),  GENU1516
                1  UNP2(22),AHLPI(43),BUM(3(43),FUIFE(22),FUIFI(22),GE(22),G1(22),  GENU1520
                2  PBUM(43),PGUM(43),THLPI(43),ITPF(22)                GENU1522
ISN 0010      DIMENSION BOM(43),UMPUM(43),US(43)                  GENU1524
ISN 0011      DIMENSION ISAVE(43),CF(22,43)                        GENU1526
ISN 0012      DATA SMALL/1.0-0/,IINY/1.0-20/                       GENU1528
C                                                                GENU1530
ISN 0013      EQUIVALENCE (DPOX(1),US(1))                          GENU1532
ISN 0014      EQUIVALENCE (ARKLUN,SZFUEL)                            GENU1534
ISN 0015      GO TO (1000,2000,3000,4000), ISW                      GENU1536
C                                                                GENU1538
C*****SIRIDE1*****
ISN 0016      1000 IF(1STEP) 1003,1003,1100                          GENU1540
ISN 0017      1003 UM1=.5*UM(3)                                       GENU1542
ISN 0018      UME=.5*(1.-UM(NP1))                                       GENU1544
ISN 0019      DO 1002 I=2,NP2                                           GENU1548
ISN 0020      BUM(I)=UM(I+1)-UM(I-1)                                       GENU1550
ISN 0021      BUM(3(1))=3.*BOM(I)                                       GENU1552
ISN 0022      UMPUM(1)=UM(1)+UM(1+1)                                       GENU1554
ISN 0023      1002 UMU(1)=UM(1+1)-UM(1)                                       GENU1556
ISN 0024      UMB(1)=BUM(2)                                             GENU1558
ISN 0025      BPE=1.                                                    GENU1560
ISN 0026      BPI=1.                                                    GENU1562
ISN 0027      Y(1)=0.                                                  GENU1564
ISN 0028      IF(ARAU.EQ.1) GO TO 1100                                       GENU1566
ISN 0030      DO 1001 I=1,NP3                                           GENU1568

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ISN 0031      1001 R(1)=1.                                GENC1570
ISN 0032      R25=1.                                    GENC1572
ISN 0033      RN15=1.                                   GENC1574
ISN 0034      IF(1TEST.NE.0) WRITE(6,9010) (R(I),I=1,NP3),R25,RN15 GENC1576
----- CALCULATION OF RHO*U *S. ----- GENC1578
ISN 0036      1100 DO 1101 I=1,NP3                    GENC1580
ISN 0037      IF(RHO(I).GT.0.) GO TO 1101              GENC1582
ISN 0038      WRITE(6,1106) RHO(I),I,RHO(I)          GENC1584
ISN 0040      1108 FORMAT(50H ***** NEGATIVE OR ZERO RHO(I)=,2P011.3,6H AT I=, GENC1586
      1 15,0A,ZIMSET TO ABS OF RHO(I)=,D11.3,17H ***** STRIDE1) GENC1588
ISN 0041      RHO(I)=DABS(RHO(I))                    GENC1590
ISN 0042      1101 RUI(I)=RHO(I)*U(I)                GENC1592
ISN 0043      RUS=RUI(3)                             GENC1594
ISN 0044      RUI1=RUI(NP1)                          GENC1596
ISN 0045      DO 1102 I=2,NP1                       GENC1598
ISN 0046      1102 RUI(I)=.5*(RUI(I)+RUI(I+1))        GENC1600
ISN 0047      IF(1TEST.NE.0) WRITE(6,9010) (RUI(I),I=1,NP3),RUI1,RUS,PE1 GENC1602
----- CALCULATION OF Y *S AND R *S ----- GENC1604
C ----- Y *S FOR PLANE GEOMETRY ----- GENC1606
ISN 0049      Y1=PE1+UM1/(DPI+RU(2))                GENC1608
ISN 0050      Y(1)=Y1+PE1*UM(3)/(RU(2)+RUS)         GENC1610
ISN 0051      Y(2)=2.*Y1-Y(3)                       GENC1612
ISN 0052      DO 1103 I=4,NP1                       GENC1614
ISN 0053      1103 Y(I)=Y(I-1)+PE1*UM(I)/(RU(I-1))   GENC1616
ISN 0054      YN15=Y(NP1)+PE1*UM(NP1)/(RU(NP1)+RUI1) GENC1618
ISN 0055      YE=PE1+UM6/(BPE*RU(NP1))             GENC1620
ISN 0056      Y(NP3)=YN15+YE                        GENC1622
ISN 0057      Y(NP2)=2.*YN15-Y(NP1)                 GENC1624
ISN 0058      IF(KRAD.EQ.0) RETURN                  GENC1626
C ----- Y *S AND R *S FOR AXISYMMETRICAL GEOMETRY ----- GENC1628
ISN 0060      1106 IF(CSALFA.EQ.0.) GO TO 1110        GENC1630
C ----- CSALFA NE ZERO ----- GENC1632
ISN 0062      LUSDZ=.5*CSALFA                        GENC1634
ISN 0063      IF(R(1).NE.0.) GO TO 1105              GENC1636
C ----- R(1)=0. ----- GENC1638
ISN 0065      DO 1106 I=2,NP3                        GENC1640
ISN 0066      Y(I)=DSQR(DABS(Y(I)/LUSDZ))            GENC1642
ISN 0067      1106 R(I)=Y(I)*CSALFA                  GENC1644
ISN 0068      YI=DSQR(DABS(YI/LUSDZ))               GENC1646
ISN 0069      YN15=DSQR(DABS(YN15/LUSDZ))           GENC1648
ISN 0070      GO TO 1107                             GENC1650
C ----- R(1) NE 0. ----- GENC1652
ISN 0071      1105 R1D2=.5*R(1)                      GENC1654
ISN 0072      R1D2SQ=R1D2*R1D2                      GENC1656
ISN 0073      DO 1104 I=2,NP3                       GENC1658
ISN 0074      Y(I)=Y(I)/(R1D2+DSQR(DABS(R1D2SQ+LUSDZ*Y(I)))) GENC1660
ISN 0075      1104 R(I)=R(I)+Y(I)*CSALFA            GENC1662
ISN 0076      YI=YI/(R1D2+DSQR(DABS(R1D2SQ+LUSDZ*YI))) GENC1664
ISN 0077      YN15=YN15/(R1D2+DSQR(DABS(R1D2SQ+LUSDZ*YN15))) GENC1666
ISN 0078      1107 R25=R(1)+YI*CSALFA                GENC1668
ISN 0079      RN15=R(1)+YN15*CSALFA                 GENC1670
ISN 0080      YE=Y(NP3)-YN15                        GENC1672
ISN 0081      RETURN                                  GENC1674
C ----- CSALFA EQ ZERO ----- GENC1676
ISN 0082      1110 DO 1111 I=2,NP3                    GENC1678

```

ISN 0083
ISN 0084
ISN 0085
ISN 0086
ISN 0087
ISN 0088
ISN 0089
ISN 0090

```
Y(1)=Y(1)/K(1)
1111 R(1)=K(1)
YI=YI/K(1)
YNI5=YNI5/K(1)
K25=K(1)
RNI5=R(1)
Y2=Y(INP5)-YNI5
RETURN
```

GEN01680
GEN01682
GEN01684
GEN01686
GEN01688
GEN01690
GEN01692
GEN01694

C*****STRIDE 2*****
C-----PRELIMINARIES FOR COEFFICIENTS

ISN 0091
ISN 0092
ISN 0093
ISN 0094
ISN 0095
ISN 0096
ISN 0097
ISN 0098
ISN 0099
ISN 0100
ISN 0101
ISN 0102
ISN 0103
ISN 0104
ISN 0105

```
2000 PX=PE1/UX
PDB=.125+PX
PDB4=PDB+PDB
G=KMI-KML
AKMI=UABS(KMI)
AKME=UABS(KME)
GD4=.25*G
PG=PX+G
PDB6=.125+PG
PDB4=PDB6+PDB6
KMI02=.5*KMI
DL 2004 I=2,NP2
PDOM(1)=PA+DOM(1)
2004 PDOM(1)=PDB4+DOM(1)
P4UMP=PDB4*DOM(2)
```

GEN01696
GEN01698
GEN01700
GEN01702
GEN01704
GEN01706
GEN01708
GEN01710
GEN01712
GEN01714
GEN01716
GEN01718
GEN01720
GEN01722
GEN01724
GEN01726
GEN01728

C-----GRID POINT 2
C-----TAU1, BPI, TI

ISN 0106
ISN 0108
ISN 0109
ISN 0110
ISN 0111
ISN 0113

```
IF (IN.NE.1) GO TO 2001
CALL WFC(1,BPI,TI,TAU1)
GO TO 2002
2001 I1=0.
IF (KRAU.EQ.0) BPI=.55553+.06667*KU(1)/KU(2)
IF (KRAU.NE.1) BPI=(K(1)*(5.*KU(1)+KU(2))+3.*K25*
1 (KU(1)+KU(2)))/6./(K(1)+K25)/KU(2)
```

GEN01730
GEN01732
GEN01734
GEN01736
GEN01738
GEN01740
GEN01742
GEN01744
GEN01746

C-----BOUNDARY COEFFICIENTS FOR VELOCITY

ISN 0115
ISN 0116
ISN 0117
ISN 0118
ISN 0119
ISN 0120
ISN 0121
ISN 0122
ISN 0123
ISN 0124

```
2002 HLP=RMI02-GD4+PUMPOM(2)
ANLP=UABS(HLP)
IHLP=HLP+HLP
THLPT(2)=IHLP
IP=EM U(2)
IIP=IP+ANLP+UABS(IP-ANLP)
A(2)=IIP-IHLP-I1-PDOM(2)
B(2)=2.*I1+KMI+AKMI
C(2)=P4UMP*(5.*U(2)+U(3))-US(2)
D(2)=A(2)+B(2)+PDOM(2)
```

GEN01748
GEN01750
GEN01752
GEN01754
GEN01756
GEN01758
GEN01760
GEN01762
GEN01764
GEN01766
GEN01768

C-----BOUNDARY COEFFICIENTS FOR F'S

ISN 0125
ISN 0127
ISN 0128
ISN 0129
ISN 0130
ISN 0132
ISN 0133
ISN 0135
ISN 0136

```
IF (NF.EQ.0) GO TO 2304
DO 2300 J=1,NF
TPF2=TP/PRCF(J,2)
IIPF(J)=IIPF2+ANLP+UABS(IIPF2-ANLP)
IF (KIN.NE.1) GO TO 2301
CALL WFC(J,1,FDIFI(J),IF,G1(J))
IF (INDI(J).EQ.2) GO TO 2303
A(1,J)=G1(J)+IF(J,1)-.5*(IF(J,2)+IF(J,3))-FDIFI(J)
GO TO 2302
```

GEN01770
GEN01772
GEN01774
GEN01776
GEN01778
GEN01780
GEN01782
GEN01784
GEN01786
GEN01788

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ISN 0137      2301  TIF=0.
ISN 0138      FDIFF(J)=0.
ISN 0139      2302  A2(J)=11PF(J)-IMLP-11F-PGUM(2)
ISN 0140      B2(J)=2.+11F+KMI+AKM1
ISN 0141      U2(J)=A2(J)+B2(J)+PBUM(2)
ISN 0142      I=-11F+FDIFF(J)
ISN 0143      GU TO 2303
ISN 0144      2303  A2(J)=11PF(J)-IMLP-PGUM(2)
ISN 0145      B2(J)=0.
ISN 0146      U2(J)=A2(J)+PBUM(2)
ISN 0147      T=KMI*F(J,1)+AJ1(J)*R(1)
ISN 0148      2305  T1=3.+F(J,2)+F(J,3)
ISN 0149      2306  L2(J)=P+LMP*T1+2.*T
-----
C ----- GRID POINT NP2
C ----- TALE, DPE, TNP3
ISN 0150      2307  IF(KEX.NE.1) GU TO 2005
ISN 0151      CALL WFLU,NP3,DPE,INP3,IAU=)
ISN 0152      GU TO 2310
ISN 0153      2005  INP3=0.
ISN 0154      IF(KKAL.EQ.0) DPE=.55555+.66667*RU(INP3)/RU(NP1)
ISN 0155      IF(KKAL.EQ.1) DPE=(R(INP3)+15.*RU(INP3)+RU(NP1))+3.*KN15*
ISN 0156      1 (RU(INP3)+RU(NP1))/6./ (R(INP3)+KN15)/RU(NP1)
C ----- BOUNDARY COEFFICIENTS FOR VELOCITY
ISN 0159      2310  HLM=KMI*U2-GU4*UMPUM(NP1)
ISN 0160      AHLM=UABS(HLM)
ISN 0161      THLM=HLM+HLM
ISN 0162      (M=EM U(NP1)
ISN 0163      ITM=(M+AHLM+UABS(M-AHLM)
ISN 0164      P4UMM=P4+PBUM(NP2)
ISN 0165      A(NP2)=2.+TNP3-KME+ARME
ISN 0166      B(NP2)=ITM+HLM-TNP3-PGUM(NP1)
ISN 0167      C(NP2)=P4UMM*15.*U(NP2)+U(NP1))-US(NP2)
ISN 0168      D(NP2)=A(NP2)+B(NP2)+PBUM(NP2)
C ----- BOUNDARY COEFFICIENTS FOR F'S
ISN 0169      GU 2320 J=1,NF
ISN 0170      TMF=TM/PKEF(J,NP1)
ISN 0171      TTMF=TMF+AHLM+UABS(TMF-AHLM)
ISN 0172      IF(KEX.NE.1) GU TO 2311
ISN 0173      CALL WFLU,NP3,FUIFE(J),TNP3F,GE(J)
ISN 0174      IF(INDX(J).EQ.2) GU TO 2313
ISN 0175      AJE(J)=GE(J)+15.* (F(J,NP2)+F(J,NP1))+FUIFE(J)-F(J,NP3)
ISN 0176      GU TO 2312
ISN 0177      2311  TNP3F=0.
ISN 0178      FUIFE(J)=0.
ISN 0179      2312  ANP2(J)=2.+TNP3F-KME+ARME
ISN 0180      BNP2(J)=TTMF+HLM-TNP3F-PGUM(NP1)
ISN 0181      UNP2(J)=ANP2(J)+BNP2(J)+PBUM(NP2)
ISN 0182      T=-TNP3F+FUIFE(J)
ISN 0183      GU TO 2315
ISN 0184      2313  ANP2(J)=0.
ISN 0185      BNP2(J)=TTMF+HLM-PGUM(NP1)
ISN 0186      UNP2(J)=BNP2(J)+PBUM(NP2)
ISN 0187      T=-KME+F(J,NP3)-AJE(J)+K(INP3)
ISN 0188      2315  T1=3.+F(J,NP2)+F(J,NP1)
ISN 0189      2320  UNP2(J)=P4UMM*T1+2.*T
ISN 0190
ISN 0191

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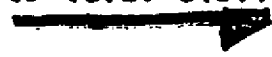
```

RETURN
C*****STRIDE3*****
3000 DO 3005 I=3,NP1
      THLM=THLP
      HLP=RNID2-GD4+UMPUM(I)
      THLP=HLP+HLP
      THLPT(I)=THLP
      AHLPT(I)=AHLPT(I)
      ITP=ITP
      ITP=ITP+AHLPT+DABS(ITP-AHLPT)
      A(I)=ITP-THLP-PGUM(I)
      B(I)=ITP+THLM-PGUM(I-1)
      C(I)=PL4+(EUMI3(I)+U(I)+UMD(I)+U(I+1)+OMD(I-1)+U(I-1))-US(I)
      U(I)=A(I)+B(I)+PBUM(I)
3005 CONTINUE
      GO TO (3021,3020), NUVEL
3020 IF (I.EQ.3) 3900,3905,3900
3900 WRITE(6,3901) (A(I),I=2,NP2)
      WRITE(6,3902) (B(I),I=2,NP2)
      WRITE(6,3903) (C(I),I=2,NP2)
      WRITE(6,3904) (U(I),I=2,NP2)
3901 FURMA(17H A(I),1P11D11.3/(7X,11D11.3))
3902 FURMA(17H B(I),1P11D11.3/(7X,11D11.3))
3903 FURMA(17H C(I),1P11D11.3/(7X,11D11.3))
3904 FURMA(17H U(I),1P11D11.3/(7X,11D11.3))
3905 CONTINUE
C-----
      IF (KIN.EQ.2.AND.RU(1).NE.0.) U(1)=U(1)-UPDX(1)*DX/RU(1)
      IF (KEX.EQ.2.AND.RU(NP3).NE.0.) U(NP3)=U(NP3)-UPDX(NP3)*DX/RU(NP3)
C----- SOLVE FOR DOWNSTREAM U 'S -----
      B(2)=(B(2)+U(1)+C(2))/D(2)
      A(2)=A(2)/D(2)
      DO 3048 I=3,NP2
      T=U(1)-B(1)*A(I-1)
      A(I)=A(I)/T
3048 B(I)=(B(I)+B(I-1)+C(I))/T
      DO 3050 IDASH=2,NP2
      I=N+4-IDASH
      U(I)=A(I)*U(I+1)+B(I)
C----- TEST FOR NEGATIVE U'S -----
      C/1UTKAP=0,NO ACTION/ .GT.0,SET TO 1.0-30/ .GT.1,IFIN=-1/ .GT.2,1TEST=1/
      IF (1UTKAP.EQ.0.OR.1.EQ.2.OR.1.EQ.NP2) GO TO 3050
      IF (U(1)) 3046,3040,3050
3046 J=1STEP+1
      WRITE(6,3047) U(1),J
3047 FURMA(25H ***** U (LE ZERU) =,2PD10.3,6H AT I=,I3,
      1 8H, 1STEP=,I0,34H, SET U TO 1.0-30 ***** STRIDE3)
      U(1)=1.0-30
      IF IN=-1UTKAP/2
      1TEST=1UTKAP/3
3050 CONTINUE
C-----
      IF (KIN.EQ.3) U(1)=.5*(U(2)+U(3))

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ISN 0244      IF (KX.EQ.3) U(NP3) = .5*(U(NP1)+U(NP2))
ISN 0246      3021 IF (I.LES1) 3011,3013,3011
ISN 0247      3011 WRITE(6,3012) (U(I),I=1,NP3)
ISN 0248      3012 FORMAT(3H 0 ,6X,1P11D11.5/(9X,11D11.5))
-----
ISN 0249      3013 IF (NF) 3000,3000,3014
ISN 0250      3014 CONTINUE
ISN 0251      DO 324 J=1,NF
-----
ISN 0252      U(2)=U2(J)
ISN 0253      A(2)=A2(J)/D(2)
ISN 0254      B(2)=B2(J)/D(2)
ISN 0255      C(FJ,2)=C2(J)/U(2)
ISN 0256      D(NP2)=DNP2(J)
ISN 0257      A(NP2)=ANP2(J)/D(NP2)
ISN 0258      B(NP2)=BNP2(J)/D(NP2)
ISN 0259      C(FJ,NP2)=CNP2(J)/D(NP2)
ISN 0260      DO 3002 I=3,NF1
ISN 0261      TIME=TIME(J)
ISN 0262      IPR=EM U(I)/PKR F(J,I)
ISN 0263      ITP(J)=IPR+ANLP(I)+DABS(IPR-ANLP(I))
ISN 0264      A(I)=ITP(J)-IMLP(I)-PGUM(I)
ISN 0265      B(I)=ITM+IMLP(I-1)-PGUM(I-1)
ISN 0266      C(I)=PL4+(BDM)3(I)*F(J,I)+UMD(I)*F(J,I+1)+UMD(I-1)*F(J,I-1)
ISN 0267      D(I)=A(I)+B(I)+PBUM(I)
ISN 0268      A(I)=A(I)/D(I)
ISN 0269      B(I)=B(I)/D(I)
ISN 0270      C(FJ,I)=C(I)/D(I)
ISN 0271      3002 CONTINUE
ISN 0272      IF (I.LES1) 3906,3907,3906
ISN 0273      3906 WRITE(6,3901) (A(I),I=2,NP2)
ISN 0274      WRITE(6,3902) (B(I),I=2,NP2)
ISN 0275      WRITE(6,3903) (C(FJ,I),I=2,NP2)
ISN 0276      WRITE(6,3904) (D(I),I=2,NP2)
ISN 0277      3907 CONTINUE
ISN 0278      324 CONTINUE
-----
ISN 0279      LC1=0
ISN 0280      DO 61 I=2,NP2
ISN 0281      ISAVE(I)=F(IN1,I)
ISN 0282      61 CONTINUE
ISN 0283      62 CONTINUE
ISN 0284      DO 300 I=2,NP2
ISN 0285      EMV=D(I)/S D(3,I)
ISN 0286      DO 305 J=1,NS
ISN 0287      ITM=A(I)*F(J,I+1)+B(I)*F(J,I-1)+C(FJ,I)
ISN 0288      IF (ITM.LI.IINY) ITM=IINY
ISN 0289      S(I)=ITM
ISN 0290      S2(I)=F(J,I)
ISN 0291      C INSURE MDL ESTIMATE BY S2(K).G1.SMALL (SEE DATA STATEMENT)
ISN 0292      IF (S2(I).LT(.1D-10) S2(I)=SMALL
ISN 0294      305 CONTINUE
ISN 0294      C PREVENT FUEL CONCENTRATION FROM EXCEEDING INLET VALUE
ISN 0294      C IDCU USED TO IDENTIFY CUS THE FUEL

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C AKRCON USED TO SAVE INLET STREAM FUEL MOLE NUMBER
ISN 0295 IF (S1(1000).GT.S2FUEL) S1(1000)=S2FUEL
ISN 0297 HSUB0=A(1)+F(INF,1+1)+B(1)*F(INF,I-1)+C(FINF,1)
ISN 0298 IK=FINI,1)
C ESTABLISH CONTACT INDEXES FOR FORWARD AND REVERSE REACTION, IF DESI
C CALL X1X2
IF (IK.LT.1.500.) LREACT=.FALSE.
ISN 0299 CALL LREK
ISN 0301 IF (LBUKN) LREACT=.TRUE.
ISN 0302 DO 306 J=1,NS
ISN 0304 F(J,I)=S2(I)
ISN 0305 306 CONTINUE
ISN 0306 F(INF,I)=HSUB0
ISN 0307 FINI,I)=IK
ISN 0308 FINE,I)=EK
ISN 0309 KRC(I)=KRCF
ISN 0310 300 CONTINUE
ISN 0311 C TEST FOR CONVERGENCE OF THERMOCHEMICAL FIELD
ISN 0312 IQUIT=0
ISN 0313 DO 114 I=1,NP2
ISN 0314 TEST=ABS(S1(SAVE(I))-FINI,I))
ISN 0315 IF (TEST.GT.1.) IQUIT=1
ISN 0317 ISAVE(I)=FINI,I)
ISN 0318 114 CONTINUE
ISN 0319 IF (IQUIT.EQ.0) GO TO 115
ISN 0321 ICI=ICI+1
ISN 0322 IF (ICI.LT.20) GO TO 62
ISN 0324 WRITE (6,915) ISTEP,(FINI,K),K=1,NP3)
ISN 0325 915 FORMAT (1H0,20X,50H NO CONVERGENCE OF THERMOCHEMICAL FIELD...TEMPS
ISN 0326 115 CONTINUE
C----- ADJUST F(J,1) AND F(J,NP3) -----
ISN 0327 DO 321 J=1,NE
ISN 0328 GO TO (3210,3220,3230),KIN
ISN 0329 3210 IF (INDEX(J).EQ.2) F(J,1)=F0IF1(J)+.5*(F(J,2)+F(J,3))+AJ1(J)/G1(J)
ISN 0331 GO TO 3220
ISN 0332 3230 F(J,1)=.5*(F(J,2)+F(J,3))
ISN 0333 3220 GO TO (3310,3320,3330),KEX
ISN 0334 3310 IF (INDEX(J).EQ.2) F(J,NP3)=F0IF1(J)+.5*(F(J,NP2)+
F(J,NP1))-AJE(J)/GE1(J)
GO TO 3320
ISN 0336 3330 F(J,NP3)=.5*(F(J,NP1)+F(J,NP2))
ISN 0337 3320 IF (TEST) 3322,3321,3322
ISN 0338 3322 WRITE (6,3325) J,(F(J,I),I=1,NP3)
ISN 0339 3325 FORMAT (6H F, J=,13,1P11D11.3/(9X,11D11.3))
ISN 0341 3321 CONTINUE
C-----
ISN 0342 3060 XU=XU
ISN 0343 PS1I=PS1I-KM1*UX
ISN 0344 PS1E=PS1E-KME*UX
ISN 0345 PEI=PS1E-PS1I
ISN 0346 ISTEP=ISTEP+1
ISN 0347 RETURN
C*****+*****+*****+*****+*****+*****+*****+*****+*****+*****+*****
ISN 0348 4000 CONTINUE

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LEVEL 2.2 (SEPT 76)

STRIDE

OS/360 FORTRAN H EXTENDED

DATE 78.199/10.30.18

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ISN 0349 NDZ=N/2
ISN 0350 NP1=N+1
ISN 0351 NP2=N+2
ISN 0352 NP3=N+3
ISN 0353 UM(1)=0.
ISN 0354 UM(NP3)=1.
ISN 0355 ISTEP=0
ISN 0356 IEND=10000
ISN 0357 IAX=10000
ISN 0358 IOUT=10000
ISN 0359 XU=1.0-30
ISN 0360 UX=1.0-30
ISN 0361 IFIN=0
ISN 0362 KIN=1
ISN 0363 KEX=1
ISN 0364 LBURN=.TRUE.
ISN 0365 IF (.NOT. LREAL) LBURN=.FALSE.
ISN 0367 RETURN
ISN 0368 GO TO FORMATTIN , (PIID11.3)
ISN 0369 END

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*OPTIONS IN EFFECT*NAME(MAIN) NOOPTIMIZE LINECOUNT(157) SIZE(MAX) AUTOUBL(NONE)

*OPTIONS IN EFFECT*SOURCE EBCDIC NOLIST NODECK OBJECT NUMAP NOFORMAT NUGOSIMI NOXREF NOALC NOANSF TERM FLAG

STATISTICS SOURCE STATEMENTS = 368, PROGRAM SIZE = 26408, SUBPROGRAM NAME =STRIDE

STATISTICS NO DIAGNOSTICS GENERATED

***** END OF COMPILATION *****

292K BYTES OF CORE NOT USED

REQUESTED OPTIONS:

OPTIONS IN EFFECT: NAME(MAIN) NOOPTIMIZE LINECOUNT(57) SIZE(MAX) AUTOUBL(NONE) SOURCE EBCDIC NDLIST NUDECK OBJECT NUMAP NDFORMAT NUGUSTH NDXREF NUALL NUANSF TERM FLA

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ISN 0002      SUBROUTINE WF(J, I, U01, U02, U03)
ISN 0003      IMPLICIT REAL*8 (A-H, O-Z)
ISN 0004      DIMENSION ASUB(20,3)
ISN 0005      COMMON/LUMA/A(43),AJE(22),AJI(22),B(43),C(43),CSALFA,U(43),OPUX(43)
1) UX,EMU(43),F(22,43),IAX,IEND,IPIN,INDE(22),INDI(22),IDUT,IDUMY,
2) STEP,IECT,ITRAP,JS,JSW,JV,JY,KEX,KIN,KKAD,N,ND2,NF,NOVEL,NP1,
3) NP2,NP3,UM(43),UMD(43),P(43),PEI,PR(22),PRF(22,43),PSIE,PSII,R1,
43),RHU(43),RME,RMI,KU(43),SD(5,43),TAUE,TAUI,U(43),XU,XU,SD(5,43),
5) Y(43),YE,YI
ISN 0006      COMMON/CLME /AK,ALMG,AKKLN,EWALL,FR,H,HFU,INERT,MASSTR,NDUMY,
1) MODEL,DADFO,PKEEXP,PKESS,UBAR,UFAL
C
C      EFFECTS OF PRESSURE GRADIENT AND MASS TRANSFER ARE INCLUDED
C      EFFECTS OF RADIUS VARIATION ARE NEGLECTED
C      FOR VELOCITY,      U01=BP,      U02=I,      U03=TAU
C      FOR F'S,          U01=FDIF, U02=T,      U03=G
C
ISN 0007      DATA SHALF/.04/, UPLAS1/.9/
ISN 0008      INT=1/11
ISN 0009      I2=11-1+2*INT
ISN 0010      I3=11-2+4*INT
ISN 0011      I25=I3-INT
ISN 0012      IF(IJ) 100,100,200
C ----- VELOCITY
ISN 0013      100 UKEF=.5*(U(12)+U(13))
ISN 0014      RKUKEF=.5*(RHU(11)+.25*(RHU(12)+RHU(13)))
ISN 0015      RUKEF=RKUKEF*UKEF
ISN 0016      RKEF=.5*(K(12)+K(13))
ISN 0017      VKEF=EMU(11)
ISN 0018      YKEF=YI+(YE-YI)*UM(11)
ISN 0019      KE=UKEF*RKUKEF+YKEF/VKEF
ISN 0020      RKUKEF=RKEF*RUKEF
ISN 0021      AM=(RMI-(RME+RMI)*UM(11))/RKUKEF
ISN 0022      EF=YREF*OPUX(11)/RUKEF/UKEF
ISN 0023      IF(MODEL.EQ.1) GO TO 110
ISN 0025      IF(KE.LT.132.25) GO TO 110
C ----- EXTENDED LOG LAW
ISN 0027      ER=KE*EWALL
ISN 0028      N11=0
ISN 0029      101 SHALF1=SHALF
ISN 0030      S=SHALF**2
ISN 0031      SLUC=S+AM+EF
ISN 0032      IF(SLUC.GT.0.) GO TO 104
ISN 0034      SLUC=1.0-30
ISN 0035      SHALF=DSQRT(DABS(AM+EF))
ISN 0036      104 BEE=DSQRT(SLUC)/AK
ISN 0037      ARG=ER*(SHALF*(AM/11.+BEE)+.5*EF)/SHALF
ISN 0038      IF(ARG.GT.11.5*EWALL) GO TO 106
ISN 0040      GO TO 110
ISN 0041      106 SHALF=AK/DLOG(ARG)

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ISN 0042      IF(DABS(SHALF-SHALF1).LT..0001.UR.N11.61.10) GO TO 102
ISN 0044      NIT=NIT+1
ISN 0045      GO TO 101
ISN 0046      102 S=SHALF**2
ISN 0047      SAV=.5*(SHALF**2+SLUC)
ISN 0048      UO11=1./(1.+BLE)
ISN 0049      EM U(125)=.25*(HUKET*KRER*DABS(U(13)-U(12))+(AK/UO11)**2
ISN 0050      GO TO 103

```

C ----- LAMINAR FLOW

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ISN 0051      110 AMKE=AM*KE
ISN 0052      FRE=EF*RE
ISN 0053      IF(DABS(AMKE).LT..01) GO TO 111
ISN 0055      AMKE=UMAX1(-0.01,UMIN1(0.01,AMKE))
ISN 0056      EXPMKE=UCXP(AMKE)
ISN 0057      STUKE=EXPAMKE-1.-AMKE
ISN 0058      AMKESQ=AMKE*AMKE
ISN 0059      SKE=AMKE*(1.-STUKE*FRE/AMKESQ)/(EXPAMKE-1.)
ISN 0060      UO11=SKE*STUKE/AMKESQ+FRE*(1-STUKE-.5*AMKESQ)/(AMKESQ*AMKE)
ISN 0061      GO TO 112
ISN 0062      111 SKE=(2.-FRE*(1.+AMKE/0.)))/(2.+AMKE)
ISN 0063      UO11=SKE*(1.+AMKE/0.)+FRE*(1.10057+AMKE/24.)
ISN 0064      112 IF(SKE.GT.1.0-30) GO TO 113
ISN 0066      SKE=1.0-30
ISN 0067      UO11=.53333
ISN 0068      113 S=SKE/KE
ISN 0069      EM U(125)=VREF*KRER/DABS(Y(13)-Y(12))
ISN 0070      103 UO12=S*PKUKET
ISN 0071      UO13=UO12*UKER/K(11)

```

C ----- UNDER-RELAX OUT1.

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ISN 0072      UO11=.1*UO11+.9*BPLAST
ISN 0073      BPLAST=UO11
ISN 0074      RETURN

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C ----- STAGNATION ENTHALPY, FUEL, UX-FU/UXDFU

```

ISN 0075      200 I=(RE.LT.132.25) GO TO 210
ISN 0077      IF(MODEL.EQ.1) GO TO 210
ISN 0079      PKKAT=PK(IJ)/PREF(IJ,125)
ISN 0080      PJAY=Y.*(PKKAT-1.)/PKKAT**25
ISN 0081      S=SAV/PREF(IJ,125)/(1.+UMAX1(-9.9999D-1,PJAY*DSQR(DABS(SAV))))
ISN 0082      UO11=0.
ISN 0083      IF(J.EQ.1) UO11=(H-1.)*.5*UKER**2
ISN 0085      UO12=S*PKUKET
ISN 0086      UO13=UO12/K(11)
ISN 0087      RETURN
ISN 0088      210 IF(DABS(AMKE).LT..01) GO TO 211
ISN 0090      S=AM/(1+EXP(PK(IJ)*AMKE)-1.)
ISN 0091      GO TO 212
ISN 0092      211 S=1./PK(IJ)/KE/(1.+0.5*PK(IJ)+AMKE)
ISN 0093      212 UO11=0.
ISN 0094      IF(J.EQ.1) UO11=(PK(IJ)-1.)*.5*UKER**2
ISN 0096      UO12=S*PKUKET
ISN 0097      UO13=UO12/K(11)
ISN 0098      RETURN
ISN 0099      END

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GEN02472
GEN02474

REQUESTED OPTIONS:

OPTIONS IN EFFECT: NAME(MAIN) NOOPTIMIZE LINECOUNT(57) SIZE(MAX) NOUDBL(NONE) SOURCE EBCDIC NOELIST NODECK OBJECT NUMAP NOFORMAT NOGUSTMT NOXREF NOALL NOANSF TERM FLAI

ISN 0002 SUBROUTINE CREK GEN02476
ISN 0003 IMPLICIT REAL*8 (A-H,O-Z) GEN02478
ISN 0004 DIMENSION ASUB(20,3) GEN02480
ISN 0005 LOGICAL LADIAB,LCUNVG,LDEBUG,LEQUIL,LNRG,LREACT GEN02482
ISN 0006 COMMON GEN02484
1/LCHEM/CP2UM,FW,PPLN,KGAS,KGASIN,SMINV,TKINV,ILN,LCUNVG,LNRG GEN02488
1/LEQUIL/AL(7,20),ALUM(3,7),BU(7),PI(7) GEN02490
1/CINDEX/IDCU,IDCU2,IDM2,IDM20,IDN2,IDQ2,IMCPS,ILL,ILM,IMAT,ITER, GEN02492
2 JJ,NI,NE,NS,NA,NGLOB,NGLOBP,NLM,NQ,NSM GEN02494
1/LPARAM/ASUB,NT,NE,EMV,EK,MSUB0,NDEBUG,NS,PA,Q0,Q1,Q2,Q3,Q4,KMCP, GEN02496
2 SM,S1(20),S2(20),TK,LADIAB,LDEBUG,LEQUIL,LREACT GEN02500
1/USPEC/MD(20),SU(20),SMW(20),SSAVE(20),Z(7,2,20) GEN02502
C ***** GEN02504
C THIS SUBROUTINE IS THE MAIN EQUILIBRIUM AND KINETIC SOLUTION ROUTINE. GEN02506
C THE CALLING PROGRAM MUST SUPPLY ALL THE VARIABLES EXCEPT KMCP AND SM GEN02508
C THROUGH THE LABELLED COMMON BLOCK LPARAM IN SI UNITS. BOTH EQUIL GEN02510
C SOLUTIONS (LEQUIL=F) -- BY MINIMIZATION OF THE GIBBS FUNCTION -- GEN02512
C AND KINETIC (LEQUIL=F) SOLUTIONS ARE CALCULATED BY A NEWTON-RAPHSON GEN02514
C TECHNIQUE. CREK ALSO CONTROLS THE LOGIC FOR PROBLEM CELLS. GEN02516
C REFERENCE CREK (WASHINGTON STATE UNIVERSITY) MARCH 1976 GEN02518
C ***** GEN02520
ISN 0007 DATA FACTOR/D.07,SMALL/1.00-6/ GEN02522
C ***** GEN02524
C ***NORMAL SOLUTION*** GEN02526
C DETERMINE EQUIVALENCE RATIO AND IF OUTSIDE INTERVAL (0.1,10) ASSUME GEN02528
C NO REACTION AND RETURN ADIABATIC NON-REACTED MIXTURE PROPERTIES: GEN02530
C SAVE GIVEN ESTIMATES OR PROGRAM GENERATED ESTIMATES IF TK IS SMALL GEN02532
C IF SOLUTION IS SUCCESSFUL, RETURN TO CALLING ROUTINE; OTHERWISE, GEN02534
C ENTER PROBLEM CELL LOGIC BELOW GEN02536
C ***** GEN02538
ISN 0008 Q0=0. GEN02540
ISN 0009 Q1=0.300-30 GEN02542
ISN 0010 Q2=-1.190-6 GEN02544
ISN 0011 Q3=2.510-1 GEN02546
ISN 0012 Q4=2.510-1 GEN02548
ISN 0013 CALL ERATIO GEN02550
ISN 0014 IF (.NOT.LDEBUG) GO TO 30 GEN02552
ISN 0015 WRITE(6,10) LREACT,LEQUIL,LADIAB,EMV,EK,MSUB0,Q0,Q1,Q2,Q3,Q4,PA,TK GEN02554
ISN 0017 10 FORMAT(1X,5L3,1P10D12.3) GEN02556
ISN 0018 IF (NDEBUG.EQ.1) GO TO 30 GEN02558
ISN 0020 WRITE(6,20) (S1(I),I=1,NS) GEN02560
ISN 0021 WRITE(6,20) (S2(I),I=1,NS) GEN02562
ISN 0022 20 FORMAT(11X,1P10D12.3) GEN02564
ISN 0023 30 IF (.NOT.LREACT) GO TO 410 GEN02566

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ISN 0054
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 ISN 0098
 ISN 0099
 ISN 0100

```

GO TO 500
C
C-----COMPLETE COMBUSTION ESTIMATE
C
C-----IF NO CARBON IN FUEL, SKIP TO GARBAGE ESTIMATES.
130 IF (11C.EQ.0) GO TO 176
    X=C.0
    Y=C.0
    DU 132 I=1,NS
    S2(1)=SMALL
    X=X+AL(11C,1)*S1(1)
    Y=Y+AL(11H,1)*S1(1)
132 CONTINUE
    S2(1UN2)=S1(1UN2)
C
    ER1=(4.0*X+Y)/(2.0*X+Y)
    ER2=2.0*Y/(2.0*X)
    IF (ER.LE.1.0) GO TO 133
    IF (ER.L1.ER1) GO TO 134
    IF (ER.L1.ER2) GO TO 135
C-----ER.GT.ER2 ---- ALL C AND H IN CO, H2 AND UNBURNED C4HY
    S2(1DCO)=2.0*(X+Y/4.0)
    S2(1DH2)=Y*(1.0+Y/(4.0*X))
C-----MULE NUMBER FOR C4HY SHOULD BE (ER-2*(1+Y/(4*X)))
    GO TO 136
C-----FUEL-LEAN COMBUSTION ---- ONLY CO2 AND H2O FORMED
133 S2(1DCO2)=X*ER
    S2(1DH2O)=(1.-ER)*(X+Y/4.)
    S2(1DH2O)=Y*ER/2.
    GO TO 136
C-----SLIGHTLY FUEL-RICH ---- CO,CO2, AND H2O PRESENT
134 S2(1DCO)=2.+(X+Y/4.)*(ER-1.)
    S2(1DCO2)=Y*(1.-ER)/2.+X*(2.-ER)
    S2(1DH2O)=Y*ER/2.
    GO TO 136
C-----FUEL-RICH ---- CO,H2, AND H2O PRESENT
135 S2(1DCO)=ER*X
    S2(1DH2)=Y+(ER-1.0)/2.0*X*(ER-2.0)
    S2(1DH2O)=Y/2.+X*(2.-ER)
C
136 SM=C.0
    DU 137 I=1,NS
137 SM=SM+S2(1)
    IK=1500.0
    IKINV=C.00000000U-4
    INCP5=1
    XLU=IK
    DU 139 K=1,10
    CALL HCP5
    HSUM=C.0
    DU 13E I=1,NS
13E HSUM=HSUM+nU(1)*S2(1)
    IK=IK+11.0*(HSUBC+KGASIN*IKINV-HSUM)/CPSUM)
    IKINV=1.0/IK
    
```

GEN02686
 GEN02688
 GEN02690
 GEN02692
 GEN02694
 GEN02696
 GEN02698
 GEN02700
 GEN02702
 GEN02704
 GEN02706
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 GEN02794

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ISN 0101
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 ISN 0103
 ISN 0105
 ISN 0106
 ISN 0107
 ISN 0108
 ISN 0109
 ISN 0111
 ISN 0112
 ISN 0114
 ISN 0116
 ISN 0118
 ISN 0119

```

XHI=DABS(TR-XLU)
XLU=TR
IF (XHI.LT.1.0) GO TO 141
139 CONTINUE
WRITE(6,140) K,XHI
140 FORMAT(1H0,1GX,42MIXTURE TEMPERATURE FAILED TO CONVERGE IN
,12,11M ITERATIONS,5X,17HTEMP DIFFERENCE =,2PD12.3/)
141 CONTINUE

C
IF (LDEBUG) WRITE(6,142) (S2(K),K=1,NS),SM,TK
142 FORMAT(1/5X,28HCOMPLETE COMBUSTION ESTIMATE/1P11D10.2/1P11D10.2/)
IF (MODE.EQ.1) ASSIGN 900 TO NEXTJK
IF (MODE.EQ.2) ASSIGN 300 TO NEXTJK
IF (MODE.GE.3) ASSIGN 200 TO NEXTJK
ASSIGN 170 TO NEXTNG
GO TO 500
    
```

GEN02796
 GEN02798
 GEN02800
 GEN02802
 GEN02804
 GEN02806
 GEN02808
 GEN02810
 GEN02812
 GEN02814
 GEN02816
 GEN02818
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 GEN02822
 GEN02824
 GEN02826
 GEN02828
 GEN02830

C-----GARBAGE ESTIMATES (GARDEN AND MURKID)

ISN 0120
 ISN 0121
 ISN 0122
 ISN 0123
 ISN 0124
 ISN 0125
 ISN 0127
 ISN 0129
 ISN 0131
 ISN 0132

```

170 TR=3800.0
SM=0.1/DFLOAT(NS)
DO 171 I=1,NS
171 S2(I)=SM
SM=0.1
IF (MODE.EQ.1) ASSIGN 900 TO NEXTJK
IF (MODE.EQ.2) ASSIGN 300 TO NEXTJK
IF (MODE.GE.3) ASSIGN 200 TO NEXTJK
ASSIGN 600 TO NEXTNG
GO TO 500
    
```

GEN02832
 GEN02834
 GEN02836
 GEN02838
 GEN02840
 GEN02842
 GEN02844
 GEN02846
 GEN02848
 GEN02850
 GEN02852
 GEN02854
 GEN02856

C*** CHAPTER 2 ** ** **
 C*** CHAPTER 2 ** ** **

C ***KINETIC***
 C SECTION FOR KINETIC SOLUTION FROM ADIABATIC EQUILIBRIUM ESTIMATES
 C (MODE 3 AND 4 ONLY)

C-----NEAR-EQUILIBRIUM SOLUTION (KINETIC WITH EMV=1.00-3 KG/CM M-SEC)

ISN 0133
 ISN 0134
 ISN 0135
 ISN 0136
 ISN 0137
 ISN 0138
 ISN 0140
 ISN 0141
 ISN 0142
 ISN 0143

```

200 LEQUIL=.FALSE.
IX=0
EMV=1.00
XLU=EMV
C-----INCREASE MINJK SPECIES FROM EQUILIBRIUM ESTIMATES
DO 201 I=1,NS
IF (S2(I).LT.SMALL) S2(I)=SMALL
201 CONTINUE
ASSIGN 250 TO NEXTJK
ASSIGN 210 TO NEXTNG
GO TO 500
    
```

GEN02858
 GEN02860
 GEN02862
 GEN02864
 GEN02866
 GEN02868
 GEN02870
 GEN02872
 GEN02874
 GEN02876
 GEN02878
 GEN02882
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 GEN02886
 GEN02888
 GEN02890
 GEN02892
 GEN02894
 GEN02896
 GEN02898

C-----FAILURE ON NEAR-EQUIL WITH EMV=XLU, DECREASE EMV BY AN ORDER OF
 C-----MAGNITUDE AND ATTEMPT AGAIN, ITERATING THIS WAY UP TO 12 TIMES

GEN02902
 GEN02904


```

C
ISN 0144 210 EMV=EMV*0.1
ISN 0145 XLU=EMV
ISN 0146 IX=IX+1
ISN 0147 IF (IX.EQ.12) GO TO 610
ISN 0149 IK=ISAVE
ISN 0150 DO 211 I=1,NS
ISN 0151 211 S2(I)=SSAVE(I)
ISN 0152 ASSIGN 230 TO NEXTIK
ISN 0153 ASSIGN 210 TO NEXTNG
ISN 0154 GO TO 500

C
C
C-----HAVE NEAR-EQUIL SOLUTION, SO FIRST TRY DIRECTLY TO OBTAIN
C-----REQUIRED SOLUTION AT GIVEN EMV
C-----HAVE NEAR-EQUIL SOLUTION, SO FIRST TRY DIRECTLY TO OBTAIN
C-----REQUIRED SOLUTION AT GIVEN EMV

ISN 0155 230 EMV=EMVSAV
ISN 0156 IF (MODE.EQ.3) ASSIGN 900 TO NEXTIK
ISN 0158 IF (MODE.EQ.4) ASSIGN 300 TO NEXTIK
ISN 0160 ASSIGN 250 TO NEXTNG
ISN 0161 GO TO 500

C
C
C ***UPPER BRANCH MARCHING***
C HAVE A KINETIC SOLUTION BUT AT EMV .LT. EMVSAV. START AT
C KNOWN SOLUTION AND INCREASE EMV BY FACTOR TO MOVE TOWARDS
C A SOLN THERE, IF SUCCESSFUL, REPEAT UNTIL EMVSAV IS REACHED, IF
C NOT SUCCESSFUL START HALF INTERVAL SEARCHING DESCRIBED BELOW
C

ISN 0162 250 EMV=EMV*1.01
ISN 0163 IF (EMV.GT.EMVSAV) EMV=EMVSAV
ISN 0165 XH1=EMV
ISN 0166 IX=0
ISN 0167 IK=ISAVE
ISN 0168 DO 251 I=1,NS
ISN 0169 251 S2(I)=SSAVE(I)
ISN 0170 ASSIGN 250 TO NEXTIK
ISN 0171 IF (EMV.GE.EMVSAV.AND.MODE.EQ.3) ASSIGN 900 TO NEXTIK
ISN 0173 IF (EMV.GE.EMVSAV.AND.MODE.EQ.4) ASSIGN 300 TO NEXTIK
ISN 0175 ASSIGN 270 TO NEXTNG
ISN 0176 GO TO 500

C
C
C ***HALF-INTERVAL SEARCHING***
C HAVE SOLUTION AT XLU BUT NOT AT XH1, HENCE START INTERVAL
C SEARCHING BY SETTING EMV TO THE LOGARITHMIC AVERAGE
C IF ITERATING MORE THAN TEN TIMES, TERMINATE.
C

ISN 0177 270 IX=IX+1
ISN 0178 IK=ISAVE
ISN 0179 DO 271 I=1,NS
ISN 0180 271 S2(I)=SSAVE(I)
ISN 0181 IF (IX.GT.10) GO TO 620
ISN 0183 EMV=DSQR((XLU*XH1))
ISN 0184 XH1=EMV
    
```

GEN02906
 GEN02908
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 GEN02988
 GEN02990
 GEN02992
 GEN02994
 GEN02996
 GEN02998
 GEN03000
 GEN03002
 GEN03004
 GEN03006
 GEN03008
 GEN03010
 GEN03012
 GEN03014

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ISN 0185
ISN 0186
ISN 0187

ASSIGN 250 TO NEXTOK
ASSIGN 270 TO NEXTING
GO TO 500

GEN03016
GEN03018
GEN03020

C
C*** *** *** *** *** *** *** *** CHAPTER 3 *** ***
C*** *** *** *** *** *** *** *** CHAPTER 3 *** ***

GEN03022
GEN03024
GEN03026

C
C ***NON-ADIABATIC***
C SECTION FOR NON-ADIABATIC SOLUTIONS FROM ADIABATIC ESTIMATES
C (MODE 2 AND 4 ONLY)
C TRY DIRECTLY TO OBTAIN NON-ADIABATIC SOLUTION! IF NOT SUCCESSFUL,
C START HALF-INTERVAL SCALING FROM THE ADIABATIC SOLUTION BY
C DEFINING A SCALING FACTOR FQ (0.0-1.0) TO MULTIPLY THE NON-ADIABATIC
C TERM (Q) IN THE ENERGY EQUATION IN SPECE.

GEN03028
GEN03030
GEN03032
GEN03034
GEN03036
GEN03038
GEN03040
GEN03042

ISN 0188
ISN 0189
ISN 0190
ISN 0191
ISN 0192
ISN 0193
ISN 0194
ISN 0195

300 LADIAS=.FALSE.
XLU=0.0
XMI=1.0
FQ=1.0
IX=0
310 ASSIGN 320 TO NEXTOK
ASSIGN 330 TO NEXTING
GO TO 500

GEN03044
GEN03046
GEN03048
GEN03050
GEN03052
GEN03054
GEN03056
GEN03058
GEN03060

ISN 0196
ISN 0198
ISN 0199
ISN 0200
ISN 0201
ISN 0202

320 IF (FQ.EQ.1.0) GO TO 500
XLU=FQ
FQ=1.0
XMI=1.0
IX=0
GO TO 310

GEN03062
GEN03064
GEN03066
GEN03068
GEN03070
GEN03072
GEN03074

ISN 0203
ISN 0204
ISN 0206
ISN 0207
ISN 0208
ISN 0209
ISN 0210
ISN 0211

330 IX=IX+1
IF (IX.GT.10) GO TO 340
IK=ISAVE
DO 331 I=1,NS
331 S2(I)=SSAVE(I)
FQ=0.5*(XLU+XMI)
XMI=FQ
GO TO 310

GEN03076
GEN03078
GEN03080
GEN03082
GEN03084
GEN03086
GEN03088
GEN03090
GEN03092

ISN 0212
ISN 0213
ISN 0214

340 CONTINUE
FQ=1.
GO TO 330

GEN03094
GEN03096
GEN03098
GEN03100
GEN03102

C
C**** **** **** **** **** **** CHAPTER 4 ****
C**** **** **** **** **** **** CHAPTER 4 ****

***GEN03104
***GEN03106

C
C ***FAILURE EXIT***
C FAILED EQUIL OR KINETIC SOLN OR EQUIV RATIO OUTSIDE (0.1,10)
C RETURN ADIABATIC, NON-REACTED MIXTURE PROPERTIES

GEN03108
GEN03110
GEN03112
GEN03114
GEN03116

ISN 0215
ISN 0216
ISN 0217
ISN 0218

400 SM=0.0
DO 401 I=1,NS
S2(I)=S1(I)
SM=SM+S2(I)

GEN03118
GEN03120
GEN03122
GEN03124

```

ISN 0219      401 CONTINUE
ISN 0220      TR=1000.0
ISN 0221      ALU=IK
ISN 0222      INLPS=1
ISN 0223      TRINV=1.00-3
ISN 0224      DL 403 I=1,1L
ISN 0225      CALL HLPS
ISN 0226      MSUM=0.0
ISN 0227      DU 402 K=1,NS
ISN 0228      MSUM=MSUM+RU(K)*SZ(K)
ISN 0229      402 CONTINUE
ISN 0230      TR=IK*(1.0+(MSUBC*RGASIN*TRINV-MSUM)/LPSUM)
ISN 0231      TRINV=1.0/TR
ISN 0232      XHI=UABS(IK-ALU)
ISN 0233      XLU=IK
ISN 0234      IF (XHI.LT.1.0) GO TO 404
ISN 0235      403 CONTINUE
ISN 0236      WRITE(C,14C) I,XHI
ISN 0237      404 CONTINUE
ISN 0238      RPLP=PA/(RGAS*IK*SM)
ISN 0239      GO TO 500
ISN 0240

```

GEN03126
GEN03128
GEN03130
GEN03132
GEN03134
GEN03136
GEN03138
GEN03140
GEN03142
GEN03144
GEN03146
GEN03148
GEN03150
GEN03152
GEN03154
GEN03156
GEN03158
GEN03160
GEN03162
GEN03164
GEN03166
GEN03168

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C
C*****      *****      *****      *****      *****      CHAPTER 3      *****
C*****      *****      *****      *****      *****      CHAPTER 3      *****
C

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GEN03170
GEN03172

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C
C ***PROBLEM CELL CALL TO SPECE***
C TAKE THE ESTIMATES GENERATED IN CHAPTERS 1,2 AND ATTEMPT A SOLUTION
C WITH FULL EQUATIONS. IF SUCCESSFUL, UPDATE THE SAVE ANSWERS WITH THE
C SOLUTION AND RETURN TO STATEMENT NUMBER NEXTOK. IF NOT, THE ACTION
C DEPENDS ON WHETHER AN EQUILIB OR KINETIC SOLN IS SOUGHT. FAILED
C EQUIL SOLN, RETURN TO STATEMENT NUMBER NEXING, WHILE FAILURE IN A
C KINETIC SOLN WILL BE FOLLOWED BY AN ATTEMPT WITH LNKG=F --- RT=0.0
C AND SAME ESTIMATES. SETTING RT=0.0 IMPLIES THAT A CHANGE IN TEMP
C FIELD HAS NO EFFECT ON SPECIES DISTRIBUTION FOR THAT PARTICULAR
C ITERATION, BUT DOES ALLOW THE SPECIES CHANGES TO INFLUENCE THE TEMP
C CHANGE --- PARTIAL DECOUPLING OF THE ENERGY EQUATION. IF SUCCESSFUL
C WITH LNKG=F, REPEAT WITH LNKG=I (FULL EQUATIONS) IF STILL NO GOOD,
C RETURN TO STATEMENT NUMBER NEXING.
C

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GEN03174
GEN03176
GEN03178
GEN03180
GEN03182
GEN03184
GEN03186
GEN03188
GEN03190
GEN03192
GEN03194
GEN03196
GEN03198

```

ISN 0241      500 CALL SPECE
ISN 0242      IF (LUNVG) GO TO 540
C SOLUTION FAILED TRY RT=0.0
ISN 0244      IF (LNKG) GO TO 520
ISN 0245      LNKG=.TRUE.
ISN 0247      510 GO TO NEXING, (100,130,170,210,250,270,330,600)
ISN 0248      520 IF (LEQUIL) GO TO 510
ISN 0250      530 LNKG=.FALSE.
ISN 0251      GO TO 500
C HAVE SOLN BUT WITHOUT RT TERMS, SEND THIS
C SOLN AS ESTIMATES WITH RT CALCULATION
ISN 0252      540 IF (LNKG) GO TO 550
ISN 0254      LNKG=.TRUE.
ISN 0255      GO TO 500

```

GEN03200
GEN03202
GEN03204
GEN03206
GEN03208
GEN03210
GEN03212
GEN03214
GEN03216
GEN03218
GEN03220
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GEN03228
GEN03230
GEN03232

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C-----SOLUTION IS SUCCESSFUL, UPDATE SAVE ANSWERS AND CONTINUE.

```

GEN03234

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C
ISN 0256      550 TSAVE=TK
ISN 0257      DU 560 I=1,N3
ISN 0258      560 SSAVE(I)=S2(I)
C
ISN 0259      GO TO NEXLOC, (200,230,250,300,320,400)
C
C*****      *****      *****      *****      CHAPTER 6      *****
C*****      *****      *****      *****      CHAPTER 6      *****
C
C ***ERROR MESSAGES***
C
ISN 0260      600 WRITE(I0,601)
ISN 0261      601 FORMAT(1H0,10X,3(4H****),30H FAILURE TO FIND EQUIL SOLN...,
                A24HAVG INLET PRPS RETURNED/)
ISN 0262      GO TO 650
ISN 0263      610 WRITE(I0,611)
ISN 0264      611 FORMAT(1H0,10X,3(4H****),35H FAILURE TO FIND NEAR-EQUIL SOLN...,
                A24HAVG INLET PRPS RETURNED/)
ISN 0265      GO TO 650
ISN 0266      620 WRITE(I0,621)
ISN 0267      621 FORMAT(1H0,10X,3(4H****),37H FAILURE TO OBTAIN KINETIC SOLN AFTER,
                A40H IN INTERVAL HALVING...AVG INLET PRPS RETURNED/)
ISN 0268      GO TO 650
ISN 0269      630 WRITE(I0,631)
ISN 0270      631 FORMAT(1H0,10X,3(4H****),29H NON-ADIABATIC SOLN FAILED...,
                A14HADIAB SOLN RETURNED/)
ISN 0271      GO TO 670
C
C-----RESTORE FAILED PROBLEM MODE PRIOR TO RETURN
C
ISN 0272      650 IF (MODE.EQ.2) LAADIAB=.FALSE.
ISN 0274      IF (MODE.EQ.3) LEQUIL=.FALSE.
ISN 0276      IF (MODE.EQ.4) LAADIAB=.FALSE.
ISN 0278      GO TO 400
C
C-----FAILED NON-ADIABATIC SOLUTION...RETURN ADIABATIC
C-----EQUIL OR KINETIC SOLUTION
C
ISN 0279      670 IK=ISAVE
ISN 0280      SM=0.0
ISN 0281      DU 671 I=1,N3
ISN 0282      S2(I)=SSAVE(I)
ISN 0283      671 SM=SM+S2(I)
C
ISN 0284      900 RMUP=PA/(RGAS*IK*SM)
ISN 0285      RETURN
ISN 0286      END
    
```

GEN03236
 GEN03238
 GEN03240
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 GEN03250
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 GEN03324
 GEN03326
 GEN03328
 GEN03330

NUMBER LEVEL FORTRAN H EXTENDED ERROR MESSAGES
 IFÉ3071 4(W) NAME FACTUR THE DATA STATEMENT CONTAINS A VARIABLE THAT IS NOT REFERENCED.
 *OPTIONS IN EFFECT: NAME (HAIN) NOOPTIMIZE LINECOUNT (571) SIZE (MAX) AUTODBL (NONE)

REQUESTED OPTIONS:

OPTIONS IN EFFECT: NAME(MAIN) NOOPTIMIZE LINECOUNT(57) SIZE(MAX) AUTODBL(NONE) SOURCE EBCDIC NOLIST NUDECK OBJECT NCMAP NCFORMAT NUGUSIMI NOXREF NUCALL NUANSF ITERM FLAL

```

ISN 0002      SUBROUTINE CPEXO
ISN 0003      IMPLICIT REAL*8 (A-H,O-Z)
C
ISN 0004      LOGICAL LADJAB,LCUNVB,LUDEBUG,LEQUIL,LMLLES,LNRG,LREACT,LSI
ISN 0005      DIMENSION ASUB(20,3)
ISN 0006      DIMENSION ATUM(7),DATA(12),AT(4)
ISN 0007      DIMENSION U(4)
C
ISN 0008      COMMON
1/LCHEM1/CPSUM,PG,PPLN,KGAS,KGASIN,SMINV,ININV,ILN,LCUNVB,LNRG
1/LEQUIL/AL(7,20),ATUM(3,7),D(17),P(17)
1/CINDEX/ICCU,ICCU2,ICM2,ICM2U,ICN2,ICU2,ICUPS,ICC,ILN,IMAT,ITER,
  JU,NI,NZ,NS,NA,NGLOB,NGLOBP,NLP,NO,NSM
1/LMAKI/MSUM,X(22),Y(22)
1/CPAKM/ACOB,NI,NE,EMV,EN,MSJCB,NDEBUB,NS,PA,QU,UI,UZ,US,UY,KNUP,
  SM,S(120),S2(20),TR,LADJAB,LUDEBUG,LEQUIL,LREACT
1/LREACT/BA(30),BA2(30),I(4,30),MUR(30),TAC(130),TAC2(30),
  TEN(30),TEN2(30),X(130),X2(30)
ISN 0009      COMMON /CSPECF/
1  H(20),SG(20),SMH(20),SSAVE(20),Z(7,2,20)
ISN 0010      DATA ACU/4MCU /,ACU2/4MCU2 /,AM2/4MH2 /,AM20/4MH20 /,
1  AMCH/4MECH/,AM2/4MH2 /,AO2/4HO2 /,BLANK/4H /,ELEM/4MELEM/,
2  GLOB/4MGLOB/,KEAL/4HKEAL/,KEVE/4HKEVE/,THER/4HTHER/,THRU/4HM
3  UGS/4MUGS /,LUMM/4MLUMM/,GAZ/1MG/,MOL/1MM/,BLNK/2H /,
4  CAKE/2ML /,MYDR/2MM /
ISN 0011      DATA NSTRM /0/,TENLN/2.3020/,XMAX/.001/,XMIN/.0003/
C
C *****
C THIS SUBROUTINE IS THE INITIALIZING ROUTINE. THE FIRST CALL READS
C (1) ELEMENT DATA DECK, (2) THERMU DATA DECK, AND (3) MECHANISM DATA
C DECK. EACH SUBSEQUENT CALL READS ONE REACTANTS DATA DECK...NO LIMIT
C ON NUMBER OF CALLS...ONE FOR EACH DIFFERENT REACTANT STREAM
C PRESSURE AND TEMPERATURE OF EACH REACTANT STREAM MUST BE SUPPLIED BY
C CALLING PROGRAM IN PA AND TK, RESPECTIVELY
C ON RETURN, CALLING PROGRAM MUST STATE MOLE NUMBERS S2(I), PRESSURE,
C TEMPERATURE, ENTHALPY AND DENSITY AT APPROPRIATE INLET GRID NODE
ISN 0012      10 READ (5,20) (DATA(I),I=1,12)
ISN 0013      20 FORMAT (12A4)
ISN 0014      WRITE (6,30) (DATA(I),I=1,12)
ISN 0015      30 FORMAT (10H,2X,12A4)
ISN 0016      IF (DATA(1).EQ.BLANK) GO TO 10
ISN 0018      IF (DATA(1).LQ.ELEM) GO TO 100
ISN 0020      IF (DATA(1).EQ.THER)GO TO 200
ISN 0022      IF (DATA(1).EQ.AMCH) GO TO 300
ISN 0024      IF (DATA(1).EQ.REACT) GO TO 400
ISN 0026      GO TO 10
C
C
C
C *****ELEMENTS*****

```

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```

C READ ELEMENT DATA FROM CARDS
C ATUM(1,K)=SYMBOL, ATUM(2,K)=ATOMIC WT ATOM(3,K)=VALENCE
100 RGAS=8314.4
    RGASIN=1./RGAS
    ILCU=0
    ILCU2=0
    IUFZ=0
    IUN2U=0
    IUN2=C
    ILL2=0
    ILL=0
    ILH=0
    LADIAL=.TRUE.
    LDEBUG=.TRUE.
    LDEBUC=.FALSE.
    NLEBUC=0
    LENCIL=.TRUE.
    LREACT=.TRUE.
    LSI=.TRUE.
    LARG=.TRUE.
    RW=1.
    NLM=1
110 READ (1,120) ATUM(NLM),(ATUM(K,NLM),K=2,3)
120 FURMA(1A2,1X,2F10.0)
    IF (ATUM(NLM) .EQ. BLANK) GO TO 140
    WRITE(6,130) ATUM(NLM),(ATUM(K,NLM),K=2,3)
130 FURMA(11X,A2,3X,2F10.0/)
    IF (ATUM(NLM) .EQ. CARB) ILC=NLM
    IF (ATUM(NLM) .EQ. HYDR) ILH=NLM
    NLM=NLM+1
    GO TO 110
C
140 CONTINUE
    NLM=NLM-1
    N1=NLM+1
    N2=NLM+2
    N3=NLM+3
    GO TO 10
C
C** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** **
C** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** **
C ***THERMU***
C READ THERMODYNAMIC DATA CARDS
200 NS=1
201 READ(5,210) (DATA(1),I=1,3),DT1,DT2,(AT(J),B(J),J=1,4),PHAZ,
    I1,I2,NCU
210 FURMA(13A4,0X,2A3,4(A2,F3.0),A1,2F10.3,115)
    IF (DATA(1) .EQ. BLANK) GO TO 200
    WRITE(6,211) (DATA(1),I=1,3),DT1,DT2,(AT(J),B(J),J=1,4),PHAZ,
    I1,I2,NCU
211 FURMA(110X,3A4,0X,2A3,2X,4(A2,2X,F3.0),2X,A1,2X,2F10.3,115)
    IF (PHAZ.NE.GAZ) WRITE(6,212) (DATA(1),I=1,3),PHAZ
212 FURMA(11F0,10A,2GHWARNING...DATA FOR SPECIES,2X,3A4,3X,

```

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GEN03432
GEN03434
GEN03436
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GEN03500
GEN03502
GEN03504
GEN03506
GEN03508
GEN03510
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GEN03528
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GEN03534
GEN03536
GEN03538
GEN03540

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ALHNDI GAS BU,2X,A1//
C-----READ Z WITH FIRST AND SECOND SUBSCRIPTS REVERSED
ISN 0075 READ(5,213) (Z(J,1,NS),J=1,2),NLU
ISN 0076 215 FORMAT(5D15.6,15)
ISN 0077 WRITE(6,214) (Z(J,1,NS),J=1,2),NLU
ISN 0078 214 FORMAT(10X,5D15.6,15)
ISN 0079 READ(5,213) (Z(J,1,NS),J=6,7),(Z(K,2,NS),K=1,3),NLU
ISN 0080 WRITE(6,214) (Z(J,1,NS),J=6,7),(Z(K,2,NS),K=1,3),NLU
ISN 0081 READ(5,215) (Z(J,2,NS),J=4,7),NLU
ISN 0082 215 FORMAT(4D15.6,120)
ISN 0083 WRITE(6,216) (Z(J,2,NS),J=4,7),NLU
ISN 0084 216 FORMAT(10X,4D15.6,120//)
C-----ESTABLISH AILM SILICHIUMETRY...AL(L,N) = (KG-ATOMS ELEMENT L
C-----PER KG-MOLECULE OF SPECIES N)
C
ISN 0085 DO 220 L=1,NLM
ISN 0086 220 AL(L,NS)=0.0
C
ISN 0087 SUM=0.0
ISN 0088 DO 240 K=1,4
ISN 0089 IF (BIN).EQ.0.01 GO TO 240
ISN 0091 DO 250 L=1,NLM
ISN 0092 IF (ATOM(L).NE.A(K)) GO TO 250
ISN 0094 AL(L,NS)=AL(L,NS)+B(K)
C
C-----ESTABLISH MOLECULAR WEIGHT OF SPECIES
C
ISN 0095 SUM=SUM+ATOM(2,L)*B(K)
ISN 0096 230 CONTINUE
ISN 0097 240 CONTINUE
ISN 0098 SMW(NS)=SUM
ISN 0099 SZ(NS)=1.00-0
C
C-----STORE MULLERITH NAME OF SPECIES
C
ISN 0100 DO 250 I=1,3
ISN 0101 250 ASUB(NS,I)=DATA(I)
C
C-----STORE INDEX NUMBER OF SPECIES
C
ISN 0102 IF (ASUB(NS,1).EQ.ALU) IUCU=NS
ISN 0104 IF (ASUB(NS,1).EQ.ALU2) IUCU2=NS
ISN 0106 IF (ASUB(NS,2).EQ.AH2) IUM2=NS
ISN 0108 IF (ASUB(NS,1).EQ.AH2U) IUM2U=NS
ISN 0110 IF (ASUB(NS,1).EQ.AN2) IUN2=NS
ISN 0112 IF (ASUB(NS,1).EQ.AU2) IUU2=NS
C
ISN 0114 NS=NS+1
ISN 0115 GO TO 201
C
ISN 0116 260 NS=NS-1
ISN 0117 NSM=NS+1
ISN 0118 NU=NS+2
ISN 0119 NA=NS+3
ISN 0120 GO TO 10

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GEN03542
GEN03544
GEN03546
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GEN03638
GEN03640
GEN03642
GEN03644
GEN03646
GEN03648
GEN03650

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C
C***   ***   ***   ***   ***   ***   ***   ***   CHAPTER 3   ***   ***
C***   ***   **.   ***   ***   ***   ***   ***   CHAPTER 3   ***   ***
C
C   ***MECHANISM***
C   READ MECHANISM/RATE DATA CARDS
C   THE VARIABLE DT1 (COLUMN 75/76) IS USED AS A FLAG:
C   CGS   ---- CGS UNITS, RATE CONSTANTS IN GM-MOLES, CM, SEC
C           AND EAL IN (KCAL/GM-MOLE)
C   COMM  ---- COMMENT CARD, FIRST 48 CHARACTERS PRINTED OUT
C   REVE  ---- REVERSE RATE DATA, IN SAME UNITS AS FORWARD DATA
C   GLOB  ---- GLOBAL RATE EXPRESSION DATA IN SI UNITS
C   OTHERWISE THE SI UNITS (KG-MOLES, M, SEC) ARE ASSUMED
C   DT1 AND DT2 (COL 75/80) CAN HAVE ANYTHING (COMMENTS) IF ABOVE FOUR
C   WORDS ARE NOT REQUIRED
C   TACT IS ACTIVATION TEMPERATURE, = EACT/GASLN, DEG K

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GEN03652
GEN03654
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GEN03760

ISN 0121
ISN 0122

ISN 0123
ISN 0124
ISN 0125

ISN 0127
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ISN 0130
ISN 0131

ISN 0132
ISN 0134
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ISN 0136
ISN 0137
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ISN 0139

ISN 0140
ISN 0141
ISN 0143
ISN 0144
ISN 0145
ISN 0147

ISN 0148
ISN 0149

ISN 0151
ISN 0152
ISN 0153
ISN 0155

ISN 0157

```

C   300 JJ=1
C       NGLUB=0
C
C   310 READ(10,311) (DATA(I),I=1,12),BX(JJ),TEN(JJ),TACT(JJ),DT1,DT2
C   311 FORMAT(12A4,3F8.3,2A4)
C       IF (DATA(1).EQ.0LANK.AND.DT1.NE.COMM) GO TO 300
C-----CHECK FOR COMMENT CARD
C       IF (DT1.NE.COMM) GO TO 313
C       WRITE(6,312) (DATA(I),I=1,12)
C   312 FORMAT(1H0,5X,3H***,12A4,3H***)
C       GO TO 310
C-----CHECK FOR REVERSE RATE DATA...ORDER OF CARDS MUST BE CORRECT
C-----UNITS OF REVERSE DATA ASSUMED SAME AS FORWARD DATA
C   313 IF (DT1.NE.REVE) GO TO 315
C       J=JJ-1
C       BX2(J)=BX(JJ)
C       TEN2(J)=TEN(JJ)
C       TACT2(J)=TACT(JJ)
C       WRITE(6,314) BAZ(J),TEN2(J),TACT2(J),DT1,DT2
C   314 FORMAT(14X,1MREVERSE RATE DATA,28X,3F15.3,2A4)
C-----CONVERT BAZ FOR INTERNAL CALCULATIONS
C       BX2(J)=BX2(J)*TENLN
C       IF (LS1) GO TO 310
C       BX2(J)=BX2(J)-TENLN*3.0
C       TACT2(J)=TACT2(J)*1000.0/1.987
C       IF (MODK(J).EQ.2) BAZ(J)=BAZ(J)-TENLN*3.0
C       GO TO 310
C-----CHECK FOR UNITS
C   315 LSI=.TRUE.
C       IF (DT1.EQ.CGS) LSI=.FALSE.
C
C       WRITE(6,316) JJ,(DATA(I),I=1,12),BX(JJ),TEN(JJ),TACT(JJ),DT1,DT2
C   316 FORMAT(1H0,5X,15,4H,12A4,3F15.3,5X,2A4)
C       IF (.NOT. LSI) TACT(JJ)=TACT(JJ)*1000./1.987
C       IF (DT1.EQ.GLOB) NGLUB=NGLUB+1
C-----CONVERT BX FOR INTERNAL CALCULATIONS
C       BX(JJ)=BX(JJ)*TENLN
C

```


C-----I(I,J) IS THE INDEX NUMBER OF THE I-TH DISTINCT SPECIES IN
 C-----REACTION J ... I=1,4 AS NO DISTINCT THIRD BODIES ARE CONSIDERED

ISN 0158
 ISN 0159
 ISN 0160
 ISN 0161
 ISN 0162
 ISN 0163
 ISN 0165
 ISN 0167
 ISN 0168
 ISN 0169
 ISN 0170
 ISN 0171
 ISN 0173
 ISN 0175
 ISN 0176
 ISN 0177
 ISN 0178
 ISN 0180
 ISN 0181
 ISN 0182
 ISN 0183
 ISN 0185
 ISN 0186
 ISN 0187

```

C      DO 320 I=1,4
C      ID(I,JJ)=0
C
C      NU=1
C      DO 325 N=1,0
C      K=N*2-1
C      IF (DATA(K).EQ.BLANK) GO TO 325
C      IF (DATA(K).NE.THIRD) GO TO 321
C      DATA(K)=BLANK
C      GO TO 325
321 CONTINUE
C      DO 322 I=1,NS
C      IF (DATA(K).NE.ASUB(I,1)) GO TO 322
C      IF (DATA(K+1).NE.ASUB(I,2)) GO TO 322
C      I=1
C      GO TO 325
322 CONTINUE
323 IF (K.GT.0) GO TO 324
C      I(IIND,JJ)=1
C      NU=NU+1
C      GO TO 325
324 IF (NU.EQ.2) NU=3
C      I(IIND,JJ)=11
C      NU=NU+1
325 CONTINUE
    
```

C-----STORE THE TYPE OF REACTION...THREE TYPES

```

MUDK 1 ... A + B ----> L + U
MUDK 2 ... AB + M ----> A + B + M
MUDK 3 ... A + B + M ----> AB + M
    
```

ISN 0188
 ISN 0189
 ISN 0191

```

MUDK(JJ)=1
IF (ID(2,JJ).EQ.0) MUDK(JJ)=2
IF (ID(4,JJ).EQ.0) MUDK(JJ)=3
    
```

C-----THE FOLLOWING SECTION, UP TO STATEMENT 355 INCLUSIVE, MAY BE
 C-----ELIMINATED IF REVERSE (AS WELL AS FORWARD) RATE DATA IS SUPPLIED
 C-----FOR ** ALL ** REACTIONS.

C-----CALCULATES REVERSE RATE CONSTANTS FROM EQUILIBRIUM CONSTANTS
 C-----AND FORWARD RATE CONSTANTS FOR FIFTEEN POINTS
 C-----OVER THE TEMPERATURE RANGE 1000 TO 3000 DEG K

ISN 0193
 ISN 0194
 ISN 0195
 ISN 0196
 ISN 0198
 ISN 0199
 ISN 0200
 ISN 0201

```

BAZ(JJ)=0.
TENZ(JJ)=0.
IACI2(JJ)=0.
IF (D(11).EQ.GLUB) GO TO 355
DX=(XMAX-XMIN)/14.0
SUMX=0.0
SUMY=0.0
INLPS=2
    
```

GEN03762
 GEN03764
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 GEN03770
 GEN03772
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 GEN03864
 GEN03866
 GEN03868
 GEN03870

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ISN 0202      DU 351 N=1,15
ISN 0203      X(N)=XMIN+DX*DFLOAT(N-1)
ISN 0204      SUMX=SUMX+X(N)
ISN 0205      IKINV=X(N)
ISN 0206      IK=1.0/IKINV
ISN 0207      TLN=DLG(IK)
ISN 0208      CALL HCLPS
ISN 0209      SUM1=0.0
ISN 0210      DU 350 ND=1,4
ISN 0211      K=10*(ND, JJ)
ISN 0212      IF (K.EQ.0) GO TO 350
ISN 0214      GF=H0(K)-S0(K)
ISN 0215      IF (ND.LT.3) SUM1=SUM1+GF
ISN 0217      IF (ND.GE.3) SUM1=SUM1-GF
ISN 0219      350 CONTINUE
ISN 0220      IM1=0.0
ISN 0221      IF (10*(2, JJ).EQ.0) IM1=TLN-2.50034
ISN 0223      IF (10*(4, JJ).EQ.0) IM1=2.50034-TLN
ISN 0225      Y(N)=(IM1-SUM1+TEN(JJ)*TLN-TACT(JJ)*IKINV+BX1(JJ)
ISN 0226      SUMY=SUMY+Y(N)
ISN 0227      351 CONTINUE
ISN 0228      XBAR=SUMX/15.0
ISN 0229      YBAR=SUMY/15.0
ISN 0230      SUMX=0.0
ISN 0231      SUM1=0.0
ISN 0232      SUMY=0.0
ISN 0233      DU 352 N=1,15
ISN 0234      SUMX=SUMX+Y(N)*(X(N)-XBAR)
ISN 0235      SUM1=SUM1+(X(N)-XBAR)**2
ISN 0236      SUMY=SUMY+(Y(N)-YBAR)**2
ISN 0237      352 CONTINUE
ISN 0238      TEN2(JJ)=0.0
ISN 0239      TACT2(JJ)=-SUMX/SUM1
ISN 0240      BX2(JJ)=(YBAR+TACT2(JJ)*XBAR)/TENLN
ISN 0241      SUMX=0.0
ISN 0242      DU 353 N=1,15
ISN 0243      SUMX=SUMX+(Y(N)+TACT2(JJ)*X(N)-TENLN*BAX2(JJ))**2
ISN 0244      353 CONTINUE
ISN 0245      SUMY=DSQRT(1.0-SUMX/SUMY)
ISN 0246      SUMA=DSQRT(SUMX/14.0)
ISN 0247      DTHLC =TACT2(JJ)
ISN 0248      IF (.NOT.LS1) DTHLC =TACT2(JJ)*1.987*.001
ISN 0250      WRITE (6,354) BX2(JJ),TEN2(JJ),DTHLC ,SUMA,SUMY
ISN 0251      354 FORMAT (CX,51H CALCULATED REVERSE RATE DATA, STD DEV AND CURR CUEFGEN03872
      1 = ,3F15.3,4X,2P2010.3)
      C-----CONVERT BX2 FOR INTERNAL CALCULATIONS
      BX2(JJ)=BX2(JJ)*TENLN
      C
      355 JJ=JJ+1
      C-----CONVERT ALL RATE DATA TO SI UNITS
      IF (LS1) GO TO 310
      J=JJ-1
      BX1(J)=BX1(J)-TENLN*.5
      BX2(J)=BX2(J)-TENLN*.5
      IF (MOD(J).EQ.2) BX2(J)=BX2(J)-TENLN*.5
      GEN03874
      GEN03876
      GEN03878
      GEN03880
      GEN03882
      GEN03884
      GEN03886
      GEN03888
      GEN03890
      GEN03892
      GEN03894
      GEN03896
      GEN03898
      GEN03900
      GEN03902
      GEN03904
      GEN03906
      GEN03908
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      GEN03912
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      GEN03962
      GEN03964
      GEN03966
      GEN03968
      GEN03970
      GEN03972
      GEN03974
      GEN03976
      GEN03978
      GEN03980
  
```

ISN 0261
ISN 0263

```
IF (MODK(J).EQ.3) BX(J)=BX(J)-TENLN*3.0  
GO TO 310
```

ISN 0264
ISN 0265

```
C  
356 JJ=JJ-1  
NGLLBP=NGLLBP+1
```

ISN 0266
ISN 0267
ISN 0268
ISN 0269
ISN 0270
ISN 0272
ISN 0273
ISN 0274
ISN 0276
ISN 0278
ISN 0280
ISN 0281
ISN 0282
ISN 0283
ISN 0284
ISN 0285
ISN 0287
ISN 0289
ISN 0290
ISN 0291
ISN 0292

```
C  
C-----PRINT OUT ARRAY OF STOICHIOMETRIC COEFFICIENTS  
C  
DO 372 J=1, JJ  
DO 370 N=1, 0  
K=N*2-1  
L=N  
IF (N.GT.3) L=N-1  
DATA(N)=BLANK  
DATA(K+1)=BLANK  
IF (N.EQ.3) GO TO 370  
IF (N.EQ.6) GO TO 370  
IF (ID(L,J).EQ.0) GO TO 370  
IDLJ=1+(L,J)  
DATA(N)=ASUB(IDLJ,1)  
KPLUS1=K+1  
DATA(KPLUS1)=ASUB(IDLJ,2)  
370 CONTINUE  
IF (ID(2,J).EQ.0) DATA(5)=THIRU  
IF (ID(4,J).EQ.0) DATA(5)=THIRU  
DATA(11)=DATA(5)  
WRITE(6,371) J,(DATA(K),K=1,12)  
371 FORMAT(5X,15,1H,,5X,6A4,+H---,6X,6A4/)  
372 CONTINUE
```

ISN 0293
ISN 0294

```
C  
C-----PRINT OUT ALL RATE DATA IN SI UNITS
```

```
C  
WRITE(6,380)  
380 FORMAT(//1H0,40X,29H KINETIC RATE DATA IN SI UNITS/  
1H0,6X,1H0,6X,+HMODK,12X,2H10,19X,2H6X,10X,5H1EN,9X,4H1ACT,  
613X,3H6X2,9X,4H1EN2,9X,5H1ACT2/)  
DO 382 J=1, JJ  
IM1=BX1(J)/TENLN  
IM2=BX2(J)/TENLN  
WRITE(6,381) J,MODK(J),(ID(I,J),I=1,4),IM1,TEN(J),TACT(J),  
1IM2,TEN2(J),TACT2(J)  
382 CONTINUE  
381 FORMAT(15X,12,1H,,18,2X,+15,2(5X,3F13.3))
```

ISN 0301
ISN 0302
ISN 0303
ISN 0304

```
C  
C-----SET CONTACT INDEXES TO UNITY  
C  
DO 390 J=1, JJ  
X1(J)=1.0  
X2(J)=1.0  
390 CONTINUE
```

ISN 0305

```
C  
RETURN
```

```
C  
C****      ****      ****      ****      ****      ****      CHAPTER 4      ****  
C****      ****      ****      ****      ****      ****      CHAPTER 4      ****  
C
```

GEN03982
GEN03984
GEN03986
GEN03988
GEN03990
GEN03992
GEN03994
GEN03996
GEN03998
GEN04000
GEN04002
GEN04004
GEN04006
GEN04008
GEN04010
GEN04012
GEN04014
GEN04016
GEN04018
GEN04020
GEN04022
GEN04024
GEN04026
GEN04028
GEN04030
GEN04032
GEN04034
GEN04036
GEN04038
GEN04040
GEN04042
GEN04044
GEN04046
GEN04048
GEN04050
GEN04052
GEN04054
GEN04056
GEN04058
GEN04060
GEN04062
GEN04064
GEN04066
GEN04068
GEN04070
GEN04072
GEN04074
GEN04076
GEN04078
GEN04080
GEN04082
GEN04084
GEN04086
GEN04088
GEN04090

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```

C ***REACTANTS***
C READ REACTANTS DATA CARDS FOR EACH INLET STREAM
C
ISN 0300 400 NSTRM=NSTRM+1
ISN 0307 LMOLES=.FALSE.
C-----SCRUB SPECIES MOLE NUMBER ARRAY
ISN 0308 DO 405 I=1,NS
ISN 0309 405 S2(I)=0.0
ISN 0310 SUM1=0.0
C
ISN 0311 410 READ(5,411) (A(I),B(I),I=1,4),(DATA(I),I=1,2),PELWT,MLE,PHAZ
ISN 0312 411 FURMA(14,(A2,F7.3),Z4,1X,F7.3,A1,9X,A1)
ISN 0313 IF (A(1).EQ.BLNK) GO TO 450
ISN 0315 WRITE(6,412) (A(I),B(I),I=1,4),(DATA(I),I=1,2),PELWT,MLE,
PHAZ,NSTRM
ISN 0316 412 FURMA(1X,(Z4,A2,F7.3),Z4,Z4,2X,F7.3,Z4,A1,Z4,A1,Z4,15)
ISN 0317 IF (MLE.EQ.MUL) LMOLES=.TRUE.
C
C-----ESTABLISH MOLE NUMBERS (KG-MOL 1/KGM MIXTURE) IN INLET STREAM
C
ISN 0319 INRV=.0/IK
ISN 0320 DO 430 I=1,NS
C-----SCREEN FOR SPECIES NAME
ISN 0321 IF (DATA(1).NE.ASUB(1,1)) GO TO 430
ISN 0325 IF (DATA(2).NE.ASUB(1,2)) GO TO 430
ISN 0325 DO 420 L=1,NLM
C-----SCREEN FOR ATOMIC COMPOSITION
ISN 0326 DO 420 K=1,4
ISN 0327 IF (ATOM(L).NE.A(K)) GO TO 420
ISN 0329 IF (AL(L,1).NE.B(K)) GO TO 430
ISN 0331 420 CONTINUE
C-----IF PELWT IS RELATIVE MASS, CONVERT TO RELATIVE MOLE NUMBERS
ISN 0332 AMLE=PELWT/SMW(1)
ISN 0333 IF (LMOLES) AMLE=PELWT
ISN 0335 S2(I)=S2(I)+AMLE
ISN 0336 SUM1=SUM1+AMLE*SMW(1)
ISN 0337 GO TO 410
ISN 0338 430 CONTINUE
C
ISN 0339 WRITE(6,440)
ISN 0340 440 FURMA(11H,10X,45H REACTANT ABOVE NOT FOUND IN THERMO LIBRARY /)
ISN 0341 GO TO 410
C
ISN 0342 450 CONTINUE
C
C-----ESTABLISH MIXTURE ENTHALPY
C
ISN 0343 HMCPS=1
ISN 0344 CALL HMCPS
C
ISN 0345 WRITE(6,460) NSTRM
ISN 0346 460 FURMA(11H,19H*** REACTANT STREAM,13,4H ***/
A1H,5X,1H,1,4X,7H SPECIES,1+X,16H MOLECULAR WEIGHT,5X,
61Z MOLE NUMBERS,8X,1+H MASS FRACTIONS/32X,17H (KG MOLE 1)/(KG 1),
C+X,17H (KG MOLE 1)/(KG X),5X,13H (KG 1)/(KG X)/)

```

GENC4092
GENC4094
GENC4096
GENC4098
GENC4100
GENC4102
GENC4104
GENC4106
GENC4108
GENC4110
GENC4112
GENC4114
GENC4116
GENC4118
GENC4120
GENC4122
GENC4124
GENC4126
GENC4128
GENC4130
GENC4132
GENC4134
GENC4136
GENC4138
GENC4140
GENC4142
GENC4144
GENC4146
GENC4148
GENC4150
GENC4152
GENC4154
GENC4156
GENC4158
GENC4160
GENC4162
GENC4164
GENC4166
GENC4168
GENC4170
GENC4172
GENC4174
GENC4176
GENC4178
GENC4180
GENC4182
GENC4184
GENC4186
GENC4188
GENC4190
GENC4192
GENC4194
GENC4196
GENC4198
GENC4200

ISN 0347
ISN 0348
ISN 0349
ISN 0350

HSUM=0.0
SM=0.0
DU 480 I=1,NS
S2(I)=S2(I)/SUM1
C-----S2(I) IN MOLE NUMBERS, KG-MOLES 1/KG MIXTURE

GEN04202
GEN04204
GEN04206
GEN04208
GEN04210

ISN 0351
ISN 0352
ISN 0353
ISN 0354
ISN 0355
ISN 0356

HSUM=HSUM+H0(I)*S2(I)
SM=SM+S2(I)
DTHLD=S2(I)*SMW(I)
WRITE(6,470) I,(ASUB(I,J),J=1,3),SMW(I),S2(I),DTHLD
470 FORMAT(1X,12,1H.,4X,3A+,2P3D20.3)
480 CONTINUE

GEN04212
GEN04214
GEN04216
GEN04218
GEN04220
GEN04222

ISN 0357

C-----HSUB0 IN JOULES/KG REACTANT MIXTURE
HSUB0=HSUM*RGAS*TK

GEN04224
GEN04226

ISN 0358

C-----RHO P IS MASS DENSITY, KG/CM M
RHO P=PA/(RGAS*TK*SM)

GEN04228
GEN04230

ISN 0359
ISN 0360
ISN 0361

SMINV=1.0/SM
WRITE(6,490) IK,HSUB0,PA,RHO P,SMINV
490 FORMAT(1H//12X,10HTEMPERATURE =,2P12.5,5X,5HMOLES K/
12X,10HENTHALPY =,3X,2P12.5,5X,9HMOLES/KG/
12X,10HPRESSURE =,3X,2P12.5,5X,6H/M**2/
12X,9HDENSITY =,4X,2P12.3,3X,7HKG/M**3/
12X,10HMEAN MOL WT =,2P12.3,3X,9HKG/KGMOLE//)

GEN04232
GEN04234
GEN04236
GEN04238
GEN04240
GEN04242
GEN04244
GEN04246
GEN04248

C-----ON RETURN, CALLING PROGRAM MUST STORE MOLE NUMBERS S2(I),
C-----PRESSURE, TEMPERATURE, ENTHALPY AND DENSITY AT APPROPRIATE INLET
C-----INLET GRID NODE

GEN04250
GEN04252
GEN04254

ISN 0362
ISN 0363

RETURN
END

GEN04256
GEN04258
GEN04260

*OPTIONS IN EFFECT*NAME(MAIN) NOOPTIMIZE LINECOUNT(157) SIZE(MAX) AUTODBL(NONE)
*OPTIONS IN EFFECT*SOURCE EBCDIC NOLIST NUDECK OBJECT NUMAP NUFORMAT NUGUSTMT NOXREF NUALC NUANSF TERM FLA
STATISTICS SOURCE STATEMENTS = 362, PROGRAM SIZE = 10620, SUBPROGRAM NAME = CREKO
STATISTICS NO DIAGNOSTICS GENERATED
***** END OF COMPILATION ***** 308K BYTES OF CORE NOT USED

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ISN 0024
ISN 0025
ISN 0026
ISN 0027
ISN 0028

ETA=1.0
ETA0=ETA
NDEC=C
NRLX=0
DO 300 ITER=1,ITMAX

GEN04362
GEN04364
GEN04366
GEN04368
GEN04370
GEN04372

ISN 0029
ISN 0030

CALL CALL
IF (IMAT.EQ.NN) GO TO 300

GEN04374
GEN04376
GEN04378
GEN04380

C
C

C** CHAPTER 2 ** ** **
C** ** ** ** **

GEN04382
GEN04384
GEN04386
GEN04388

C ***CONSTRUCT CORRECTIONS FOR EQUILIBRIUM SPECIES***
C CHECK FOR SINGULAR MATRIX (LLUNVG SET TO TRUE AT END OF CALL)
IF (.NOT.LLUNVG) GO TO 200
LLUNVG=.FALSE.
RETURN

GEN04390
GEN04392
GEN04394
GEN04396
GEN04398
GEN04400

ISN 0030
ISN 0031
ISN 0032
ISN 0033
ISN 0034
ISN 0035
ISN 0036
ISN 0037
ISN 0038
ISN 0039
ISN 0040
ISN 0041
ISN 0042
ISN 0043
ISN 0044
ISN 0045

200 DO 210 L=1,NLM
210 P(L)=X(L)
X(NSM)=X(N1)
X(N2)=X(N2)
DO 230 I=1,NS
X(I)=HO(I)*X(N2)-(HO(I)-SO(I)+Y(I)+PPLN-Y(NSM))+X(NSM)
DO 220 L=1,NLM
X(L)=X(L)+AL(L,1)*P(L)
220 CONTINUE
230 CONTINUE

GEN04402
GEN04404
GEN04406
GEN04408
GEN04410
GEN04412
GEN04414
GEN04416
GEN04418
GEN04420
GEN04422

C*** ** ** ** CHAPTER 3 *** ***
C*** ** ** ** CHAPTER 3 *** ***

GEN04424
GEN04426
GEN04428

C ***CALCULATE UNDERRELAXATION PARAMETER ETA***
C UNDERRELAXATION TESTS ARE DIFFERENT FOR MAJOR AND MINOR SPECIES WITH
C ETA = MIN(ETA1,ETA2,1) WHERE
C MAJOR SPECIES --- S2(I)/SM ~ 1.00-B
C MINOR SPECIES --- S2(I)/SM 1.00-B
C AND ONLY POSITIVE CORRECTION CHANGES FOR MOLE NUMBERS ARE MONITORED
C ETA1 = MAJOR SPECIES CONTROL
C ETA2 = MINOR SPECIES CONTROL

GEN04430
GEN04432
GEN04434
GEN04436
GEN04438
GEN04440
GEN04442
GEN04444
GEN04446
GEN04448
GEN04450
GEN04452

ISN 0046
ISN 0047
ISN 0048
ISN 0049
ISN 0050
ISN 0051
ISN 0052
ISN 0053
ISN 0054
ISN 0055

300 ETA0=ETA
ETA=1.0
ETA1=1.0
SUM=DABS(X(NSM))
IM1=DABS(X(N2))
IF (IM1.GT.SUM) SUM=IM1
DO 320 I=1,NS
IF (X(I).LE.0.0) GO TO 320
IF (S2(I)*SMINV.LE.1.00-B) GO TO 310

GEN04454
GEN04456
GEN04458
GEN04460
GEN04462
GEN04464
GEN04466
GEN04468
GEN04470

C-----MAJOR SPECIES
IF (X(I).GT.SUM) SUM=X(I)
GO TO 320

ISN 0056
ISN 0060

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C-----MINOR SPECIES
ISN 0061 310 TS11=UABS((Y(NSM)-Y(11)-9.2103404)/(X(1)-X(NSM)))
ISN 0062 IF (TS11.LI.EIA1) EIA1=TS11
ISN 0064 320 CONTINUE
ISN 0065 IF (SUM.GI.2.C) EIA=2.0/SUM
ISN 0067 IF (ETA1.LI.ETA) ETA=EIA1

C
C ***CONVERGENCE MONITORING***
C AFTER TEN SUCCESSIVE UNDERRELAXED ITERATIONS, IN WHICH ETA DOES NOT
C INCREASE BY TWICE OR MORE, OR AFTER SIX ITERATIONS IN WHICH ETA
C DECREASES, DIVERGENCE IS ASSUMED AND THE SOLUTION TERMINATED
C
C LNKG=.TRUE. ---- FULL EQUATIONS
ISN 0069 IF (ETA.EU.1.0) NKLX=-1
ISN 0071 IF ((ETA/ETAO).GE.2.0) NKLX=-1
ISN 0073 NKLX=NKLX+1
ISN 0074 IF (NKLX.GI.10) GO TO 900
ISN 0076 IF (ETA.LI.ETAO) NDEC=NDEC+1
ISN 0078 IF (.NOT.LNKG) NDEC=1
ISN 0080 IF (NDEC.GI.6) GO TO 900

C
C****      ****      ****      ****      ****      ****      CHAPTER 4      ****
C****      ****      ****      ****      ****      ****      CHAPTER 4      ****
C
C APPLY CORRECTIONS TO ESTIMATES
C
ISN 0082 DO 420 I=1,NS
ISN 0083 Y(I)=Y(I)+ETA*X(I)
ISN 0084 IF (Y(I).LT.TNY) GO TO 410
ISN 0086 S2(I)=DEXP(Y(I))
ISN 0087 GO TO 420

C
ISN 0088 410 Y(I)=TNY
ISN 0089 S2(I)=TINY
C-----INSURE CONVERGENCE TEST PASSED WHENEVER Y(I)=TNY
ISN 0090 X(I)=0.0
ISN 0091 +20 CONTINUE
ISN 0092 Y(NSM)=Y(NSM)+ETA*X(NSM)
ISN 0093 SM=DEXP(Y(NSM))
ISN 0094 SMINV=1.0/SM
ISN 0095 Y(INQ)=Y(INQ)+ETA*X(INQ)
ISN 0096 ILN=Y(INQ)
ISN 0097 IK=DEXP(ILN)
ISN 0098 TRINV=1.0/IK

C
ISN 0099 IF (.NOT.LDEBUG) GO TO 500
ISN 0101 IF (NDEBUG.GE.3) WRITE(6,430) ITER,ETA,LREACT,LEQUIL,LADIAB,
1 LNRG,MSUBO,SM,EMV,IK
ISN 0103 IF (NDEBUG.GE.4) WRITE(6,440) (I,ASUB(I,1),S1(I),S2(I),Y(I),
1 X(I),M0(I),S0(I),I=1,NS)
ISN 0105 430 FORMAT(2X,13,2PD12.5,4L8,2P4D12.5)
ISN 0106 440 FORMAT(20X,7MSPECIES,4X,2MS11),7X,2MS211),7X,4MY11),8X,
1 A+NA11),8X,2MH011),7X,2MS011)/(16X,12,3X,A4,2X,2P0U12.5))
C

```

GENO4472
GENO4474
GENO4476
GENO4478
GENO4480
GENO4482
GENO4484
GENO4486
GENO4488
GENO4490
GENO4492
GENO4494
GENO4496
GENO4498
GENO4500
GENO4502
GENO4504
GENO4506
GENO4508
GENO4510
GENO4512
GENO4514
GENO4516
GENO4518
GENO4520
GENO4522
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GENO4544
GENO4546
GENO4548
GENO4550
GENO4552
GENO4554
GENO4556
GENO4558
GENO4560
GENO4562
GENO4564
GENO4566
GENO4568
GENO4570
GENO4572
GENO4574
GENO4576
GENO4578
GENO4580


```

C*****      *****      *****      *****      *****      CHAPTER 5      *****      *GEN04582
C*****      *****      *****      *****      *****      CHAPTER 5      *****      *GEN04584
C
C
C      CONVERGENCE CHECK...ALL MULE NUMBER CORRECTIONS MUST BE .LT. 1.0 PCI
C
ISN 0107      200 IF (ELA.LT.1.0) GO TO 250
ISN 0109      DU 210 I=1,N3
ISN 0110      IF (UABS(X(I)).GT.0.10) GO TO 250
ISN 0112      510 CONTINUE
ISN 0113      LCUNVG=.TRUE.
ISN 0114      MSUBU=MSUM*RGAS*TR
ISN 0115      RETURN
C
ISN 0116      250 CONTINUE
C
C
ISN 0117      RETURN
C
C*****      *****      *****      *****      *****      CHAPTER 6      *****      *GEN04618
C*****      *****      *****      *****      *****      CHAPTER 6      *****      *GEN04620
C
ISN 0118      ENTRY ERATIO
C
C      CALCULATES FUEL/AIR EQUIV RATIO, GIVEN MULE NUMBERS IN SI ARRAY,
C      USING POSITIVE AND NEGATIVE OXIDATION STATES (VALENCES)
C
ISN 0119      VP=0.0
ISN 0120      VM=0.0
ISN 0121      DU 610 I=1,N3
ISN 0122      IF (SI(I).LE.TINY) GO TO 610
ISN 0124      DU 600 L=1,NLM
ISN 0125      IF (AL(L,1).EQ.0.) GO TO 600
ISN 0127      IF (ATUM(3,L).GT.0.0) VP=VP+AL(L,1)*ATUM(3,L)*SI(I)
ISN 0129      IF (ATUM(3,L).LT.0.0) VM=VM+AL(L,1)*ATUM(3,L)*SI(I)
ISN 0131      600 CONTINUE
ISN 0132      610 CONTINUE
C
ISN 0133      VM=-VM
ISN 0134      IF (VM.LT.TINY) GO TO 620
ISN 0136      IF (VP.LT.TINY) GO TO 630
ISN 0138      ER=VP/VM
ISN 0139      RETURN
C
ISN 0140      620 ER=1000000.0
ISN 0141      RETURN
C
ISN 0142      630 ER=0.0
C
ISN 0143      900 RETURN
ISN 0144      END

```

*GEN04582
*GEN04584
GEN04586
GEN04588
GEN04590
GEN04592
GEN04594
GEN04596
GEN04598
GEN04600
GEN04602
GEN04604
GEN04606
GEN04608
GEN04610
GEN04612
GEN04614
GEN04616
*GEN04618
*GEN04620
GEN04622
GEN04624
GEN04626
GEN04628
GEN04630
GEN04632
GEN04634
GEN04636
GEN04638
GEN04640
GEN04642
GEN04644
GEN04646
GEN04648
GEN04650
GEN04652
GEN04654
GEN04656
GEN04658
GEN04660
GEN04662
GEN04664
GEN04666
GEN04668
GEN04670
GEN04672
GEN04674
GEN04676
GEN04678
GEN04680

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REQUESTED OPTIONS:

OPTIONS IN EFFECT: NAME(MAIN) NOOPTIMIZE LINECOUNT(57) SIZE(MAX) AUTODOBL(NONE) SOURCE EBCDIC NDLIST NODLCK OBJECT NOMAP NOFORMAT NUGUSTM1 NOXREF NOALC NUANSF TERM FL

```

ISN 0002      SUBROUTINE CALL                                GEN04682
ISN 0003      IMPLICIT REAL*8 (A-H,U-Z)                      GEN04684
C                                                     GEN04686
ISN 0004      LOGICAL LADIAB,LCUNVG,LDEBUC,LEQUIL,LKREACT,LNRG GEN04688
ISN 0005      DIMENSION ASUB(20,3)                            GEN04690
C                                                     GEN04692
C THE FOLLOWING DOUBLE PRECISION REQUIRED ONLY FOR IBM MACHINES GEN04694
C DOUBLE PRECISION A,DIMI                                     GEN04696
C                                                     GEN04698
ISN 0006      COMMON                                          GEN04700
1/CHEM1/CPSON,F0,PPLN,KGAS,KGASIN,SMINV,TKINV,ILN,LCUNVG,LNRG GEN04702
1/LEQUIL/AL1(7,20),ALUM1(3,7),E0(7),P1(7)                    GEN04704
1/LINDEX/IDCU,IDCU2,IDNZ,IDNZ0,IDNZ,IDU2,INCP5,ILC,ILN,IMAT,ITER, GEN04706
2      JJ,N1,N2,N3,NA,INCLUB,INGLUB,NLM,NV,NCM                GEN04708
1/LMATN1/HSUM,X1(22),Y1(22)                                    GEN04710
1/CPANON/ASUB,IN,NE,EMV,CK,HSUBC,INDEBUC,NS,PA,UC,U1,U2,U3,Q4,KMUP, GEN04712
2      SM,S1(20),S2(20),IA,LADIAB,LDEBUC,LEQUIL,LKREACT    GEN04714
1/LKREACT/DX1(30),DX2(30),ID1(4,30),MDUR(30),IAC1(30),IAC12(30), GEN04716
2      TEN(30),TEN2(30),X1(30),X2(30)                        GEN04718
C COMMON /LSPECE/                                             GEN04720
1      HC(20),SG(20),SMW(20),SSAVE(20),Z(1,2,20)            GEN04722
C                                                     GEN04724
C*****
C THIS SUBROUTINE CONSTRUCTS THE NEWTON-RAPHSON DERIVATIVE MATRIX FOR GEN04726
C BLM KINETIC AND EQUILIBRIUM SOLUTIONS AND SOLVES IT BY PIVOTAL GEN04728
C GAUSSIAN REDUCTION. WHENEVER TEMP IS LESS THAN 1500K, THE REVERSE GEN04730
C RATE IS CALCULATED FROM THE FORWARD RATE AND EQUILIBRIUM CONSTANT. GEN04732
C PROVISION IS MADE FOR GLOBAL REACTIONS GEN04734
C REFERENCE CREK (WASHINGTON STATE UNIVERSITY) MARCH 1976 GEN04736
C*****
ISN 0008      DIMENSION A(22,23)                               GEN04740
C                                                     GEN04742
ISN 0009      DATA B16/46.051/                                GEN04744
C                                                     GEN04746
ISN 0010      DO 10 I=1,NV                                      GEN04748
ISN 0011      DO 10 K=1,NA                                       GEN04750
ISN 0012      10 A(I,K)=0.0                                         GEN04752
C                                                     GEN04754
ISN 0013      IHCP5=1                                             GEN04756
ISN 0014      IF (LEQUIL) IHCP5=2                                   GEN04758
ISN 0016      IF (TK.LT.1500.0) IHCP5=2                           GEN04760
ISN 0018      CALL HCPS                                           GEN04762
ISN 0019      HIN=HSUBC+KGASIN+TKINV                               GEN04764
ISN 0020      W=0.                                                 GEN04766
ISN 0021      WLRV=0.                                              GEN04768
ISN 0022      IF (LADIAB) GO TO 20                                  GEN04770
C-----C AND CURV ARE NON-DIMENSIONAL                          GEN04772
1      IM1=F0/(EMV*KGAS)                                           GEN04774
ISN 0024      W=(11*W+TK+Q3)+(K+Q2)+(K+Q1+Q0+TKINV)+IM1          GEN04776
ISN 0025      W=11*W+TK+Q3)+(K+Q2)+(K+Q1+Q0+TKINV)+IM1          GEN04778

```

ISN 0026
ISN 0027

ISN 0028

ISN 0030
ISN 0031
ISN 0032

```
QDKV=(((+.Q4*IK+.3.*Q3)*IK+2.*Q2)*IK+Q1)*TM1
20 CONTINUE

IF (LEQUIL) GO TO 300

RHSM=PA+RBASIN*IKINV
RHOP=RHSM*SMINV
RMSQ=RHOP**2
```

C

C* * * * * CHAPTER 1 * * * * *
C* * * * * CHAPTER 1 * * * * *

C

C ***GLOBAL REACTION***
C GLOBAL RATE EQUATIONS FOR HYDROCARBON PYROLYSIS...
C GLOBAL RATE EXPRESSION DUE TO EDELMAN OF GASL
C CXMY + (X/Z) DZ ----- X LU + (Y/Z) MZ

ISN 0033
ISN 0035
ISN 0037
ISN 0038
ISN 0039
ISN 0040
ISN 0041
ISN 0042
ISN 0043
ISN 0044
ISN 0045
ISN 0046
ISN 0048

```
IF (NGLOB.EQ.0) GO TO 110
IF (TR.LI.DOO.) GO TO 110
DO 100 J=1,NGLOB
I=1001,J)
K=1002
M=1000
N=10M2
XC=AL(ILL,1)
YM=AL(ILM,1)
TK1=TAL(I,J)+TKINV
TM2=TK1-BX(I,J)+10.815*PPLN)
IF (DABS(TM2).GT.BIG) GO TO 100
KI=DEXP(-IM2)
```

C

C-----PROVISION FOR CONTACT INDEX

ISN 0049
ISN 0050
ISN 0051
ISN 0052
ISN 0053
ISN 0054
ISN 0055
ISN 0056
ISN 0057
ISN 0058
ISN 0059

```
KI=XI(J)*KI
KI=(0.0009*TK-0.5)*KI+(RHOP*S2(K))*DSQRT(RHOP*S2(1))
TM1=KI*0.5
A(I,I)=A(I,I)+TM1
A(I,K)=A(I,K)+KI
A(K,I)=A(K,I)+KI*XC*0.25
A(K,K)=A(K,K)+TM1*XC
A(M,I)=A(M,I)-TM1*XC
A(M,K)=A(M,K)-KI*XC
A(N,I)=A(N,I)-KI*YM*0.25
A(N,K)=A(N,K)-TM1*YM
```

C

C-----A(IANY,M)=A(IANY,N)=0 BECAUSE NO REVERSE REACTION ASSUMED

ISN 0060
ISN 0061
ISN 0062
ISN 0063
ISN 0064
ISN 0065
ISN 0066
ISN 0067
ISN 0068
ISN 0069
ISN 0071

```
RN=KI*1.5
A(I,NSM)=A(I,NSM)-KN
A(K,NSM)=A(K,NSM)-RN*XC*0.5
A(M,NSM)=A(M,NSM)+KN*XC
A(N,NSM)=A(N,NSM)+RN*YM*0.5
A(I,NA)=A(I,NA)-KI
A(K,NA)=A(K,NA)-KI*XC*0.5
A(M,NA)=A(M,NA)+KI*XC
A(N,NA)=A(N,NA)+KI*YM*0.5
IF (.NOT.LNK6) GO TO 100
KI=KI*(IKI+1.0/11.0-0.55*IKINV)-1.5)
```

GEN04782
GEN04784
GEN04786
GEN04788
GEN04790
GEN04792
GEN04794
GEN04796
GEN04798
GEN04800
GEN04802
GEN04804
GEN04806
GEN04808
GEN04810
GEN04812
GEN04814
GEN04816
GEN04818
GEN04820
GEN04822
GEN04824
GEN04826
GEN04828
GEN04830
GEN04832
GEN04834
GEN04836
GEN04838
GEN04840
GEN04842
GEN04844
GEN04846
GEN04848
GEN04850
GEN04852
GEN04854
GEN04856
GEN04858
GEN04860
GEN04862
GEN04864
GEN04866
GEN04868
GEN04870
GEN04872
GEN04874
GEN04876
GEN04878
GEN04880
GEN04882
GEN04884
GEN04886
GEN04888
GEN04890

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ISN 0072
 ISN 0073
 ISN 0074
 ISN 0075
 ISN 0076
 ISN 0077

A(I,NQ)=A(I,NQ)+KI
 A(K,NQ)=A(K,NQ)+KI+XC*0.5
 A(H,NQ)=A(H,NQ)-KI+XL
 A(L,NQ)=A(L,NQ)-KI+YH*0.5
 100 CONTINUE
 110 CONTINUE

GEN04892
 GEN04894
 GEN04896
 GEN04898
 GEN04900
 GEN04902

ISN 0078

C

DU 270 J=NGLUBP,JJ

GEN04904
 GEN04906
 GEN04908

C

C** ** * ** * ** ** ** ** ** ** ** ** ** ** ** ** * CHAPTER 2 ** ** **
 C** ** * ** * ** ** ** * ** * ** * CHAPTER 2 ** ** **

GEN04910
 GEN04912
 GEN04914

C

C

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C

REACTION RATES
 CALCULATE FORWARD AND REVERSE RATES R1 AND R2
 THREE TYPES OF REACTIONS

MODE 1 ... A + B ----> C + D
 MODE 2 ... AB + M ----> A + I + M
 MODE 3 ... A + B + M ----> AI + M

ISN 0079
 ISN 0080
 ISN 0081
 ISN 0082
 ISN 0083

I=ID(1,J)
 N=ID(2,J)
 M=ID(3,J)
 R=ID(4,J)
 MODE=MODE(I)

GEN04920
 GEN04922
 GEN04924
 GEN04926
 GEN04928
 GEN04930

ISN 0084
 ISN 0085
 ISN 0086
 ISN 0087
 ISN 0088
 ISN 0089

K1=0.0
 K2=0.0
 TM1=0.0
 TM2=0.0
 RN=0.0
 RI=0.0

GEN04932
 GEN04934
 GEN04936
 GEN04938
 GEN04940
 GEN04942
 GEN04944

ISN 0090
 ISN 0091
 ISN 0092
 ISN 0094
 ISN 0096

TK1=IAC(I)*IKINV
 TM2=TK1-BX(J)
 IF (TEN(J).NE.0.) TM2=TM2-TEN(J)*TLN
 IF (DABS(TM2).GT.0.16) GO TO 205
 RI=DEXP(-TM2)

GEN04946
 GEN04948
 GEN04950
 GEN04952
 GEN04954
 GEN04956
 GEN04958

C-----PROVISION FOR CONTACT INDEX

ISN 0097
 ISN 0098
 ISN 0099
 ISN 0100
 ISN 0101
 ISN 0103

KI=RI*KI(I)
 IF (MODE=2) Z00,Z01,Z02
 Z00 KI=KI+S2(I)*KMSQ+S2(K)
 RN=KI+2.0
 IF (LNKG) KI=KI*(TEN(J)+TK1-2.0)
 GO TO 205

GEN04960
 GEN04962
 GEN04964
 GEN04966
 GEN04968
 GEN04970
 GEN04972

ISN 0104
 ISN 0105
 ISN 0106
 ISN 0108

Z01 KI=KI+KMSM*KHOP*S2(I)
 RN=KI
 IF (LNKG) KI=KI*(TEN(J)+TK1-2.0)
 GO TO 205

GEN04974
 GEN04976
 GEN04978
 GEN04980
 GEN04982
 GEN04984
 GEN04986

ISN 0109
 ISN 0110
 ISN 0111

Z02 KI=KI+KMSM+S2(I)*KMSQ+S2(K)
 RN=KI+2.0
 IF (LNKG) KI=KI*(TEN(J)+TK1-2.0)

GEN04988
 GEN04990
 GEN04992
 GEN04994
 GEN04996
 GEN04998
 GEN05000

```

C
ISN 0113      205 TM1=R1
C
C
C-----CALCULATE REVERSE RATE CONST FROM FWD RATE CONST AND EQUIL CONST
C-----WHENEVER TEMP IS LESS THAN 1500 K
C
ISN 0114      IF (TK.GT.1500.0) GO TO 220
C
ISN 0116      HH=H0(I)-HGIM)
ISN 0117      SS=S0(I)-SGIM)
ISN 0118      IF (MODE-2) 210,211,212
C
ISN 0119      210 HH=HH+H0(K)-HG(K)
ISN 0120      SS=SS+S0(K)-SG(K)
ISN 0121      BXX=BX(J)+SS
ISN 0122      TK2=TK1+HH
ISN 0123      TN2=TEN(J)
ISN 0124      GO TO 230
C
ISN 0125      211 HH=HH-HU(IN)
ISN 0126      SS=SS-SU(IN)
C-----2.500304 IS E-LOG OF GAS CONST 0.00206 M**3-ATM/KGMOL-DEG K.
ISN 0127      BXX=BX(J)+SS-2.500304
ISN 0128      TK2=TK1+HH
ISN 0129      TN2=TEN(J)+1.0
ISN 0130      GO TO 230
C
ISN 0131      212 HH=HH+H0(K)
ISN 0132      SS=SS+S0(K)
ISN 0133      BXX=BX(J)+SS+2.500304
ISN 0134      TK2=TK1+HH
ISN 0135      TN2=TEN(J)-1.0
ISN 0136      GO TO 230
C
ISN 0137      220 BXX=BX2(J)
ISN 0138      TK2=TK12(J)*TKINV
ISN 0139      TN2=TN2(J)
C
ISN 0140      230 TM2=TK2-BXX
ISN 0141      IF (TN2.NE.0.) TM2=TM2-TN2*ILM
ISN 0143      IF (UABS(TM2).GT.0.16) GO TO 250
ISN 0145      R2=DEXP(-TM2)
C-----MULTIPLY HOMOGENEOUS RATE CONSTANT BY CONTACT INDEX
ISN 0146      R2=R2*X2(I)
C
ISN 0147      IF (MODE-2) 240,241,242
C
ISN 0148      240 R2=R2+S2(M)*RHSM+S2(N)
ISN 0149      RN=RN-R2+2.0
ISN 0150      IF (LNKG) KF=K1-R2*(TN2+TK2-2.0)
ISN 0152      GO TO 250
C
ISN 0153      241 R2=R2*RHSM*S2(M)*RHSM+S2(N)
ISN 0154      RN=RN-R2+2.0

```

GEN05002
GEN05004
GEN05006
GEN05008
GEN05010
GEN05012
GEN05014
GEN05016
GEN05018
GEN05020
GEN05022
GEN05024
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GEN05028
GEN05030
GEN05032
GEN05034
GEN05036
GEN05038
GEN05040
GEN05042
GEN05044
GEN05046
GEN05048
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GEN05052
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GEN05066
GEN05068
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GEN05072
GEN05074
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GEN05078
GEN05080
GEN05082
GEN05084
GEN05086
GEN05088
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GEN05092
GEN05094
GEN05096
GEN05098
GEN05100
GEN05102
GEN05104
GEN05106
GEN05108
GEN05110

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ISN 0203      A(I,NA)=A(I,NA)+EMV*(S1(I)-S2I)
ISN 0204      A(NSM,I)=S2I
ISN 0205      A(NSM,NA)=A(NSM,NA)-S2I
ISN 0206      A(INQ,I)=H0(I)*S2I
ISN 0207      HSUM=HSUM+A(INQ,I)
ISN 0208      280 CONTINUE
C
ISN 0209      A(NSM,NSM)=-SM
C-----A(NSM,NU) AND A(NU,NSM) ARE EQUAL TO ZERO.
ISN 0210      A(NSM,NA)=A(NSM,NA)+SM
ISN 0211      A(INQ,NU)=CPSCM+QDKV
ISN 0212      A(INQ,NA)=HIN-Q-HSUM
C
ISN 0213      IMAT=NU
ISN 0214      GO TO 400
C
C***      ***      ***      ***      ***      ***      ***      ***      CHAPTER 3      ***      ***
C***      ***      ***      ***      ***      ***      ***      ***      CHAPTER 3      ***      ***
C
C      **EQUILIBRIUM**
C      DERIVATIVE AND FUNCTION MATRIX FOR EQUILIBRIUM SOLUTION
C
ISN 0215      300 DO I=1,NLM
ISN 0216      310 B0(I)=0.0
C
ISN 0217      HSUM=0.0
ISN 0218      SUM=0.0
ISN 0219      DO 340 I=1,NS
ISN 0220      SUM=SUM+S2(I)
ISN 0221      IM1=H0(I)*S2(I)
ISN 0222      HSUM=HSUM+IM1
ISN 0223      IM2=(H0(I)-S0(I)+Y(I)-Y(NSM)+PPLN)*S2(I)
ISN 0224      A(N1,N3)=A(N1,N3)+IM2
ISN 0225      A(N2,N2)=A(N2,N2)+H0(I)*IM1
ISN 0226      A(N2,N3)=A(N2,N3)+H0(I)*IM2
C
ISN 0227      DO 330 L=1,NLM
ISN 0228      IF (AL(L,I).EQ.0.0) GO TO 330
ISN 0230      IM3=AL(L,I)*S2(I)
C-----CROSS-DERIVATIVES OF ELEMENT EQUATIONS, D FILE/D PI(K)
ISN 0231      DO 320 K=L,NLM
ISN 0232      IF (AL(K,I).EQ.0.0) GO TO 320
ISN 0234      A(L,K)=A(L,K)+AL(K,I)*IM3
ISN 0235      320 CONTINUE
C-----DERIVATIVES OF L-ELEMENT EQN W.R.T. LN SM AND LN T
ISN 0236      A(L,N1)=A(L,N1)+IM3
ISN 0237      A(L,N2)=A(L,N2)+AL(L,I)*IM1
C-----NEGATIVE OF L-ELEMENT EQN, FILE
ISN 0238      A(L,N3)=A(L,N3)+AL(L,I)*IM2
ISN 0239      B0(L)=B0(L)+AL(L,I)*S1(I)
ISN 0240      330 CONTINUE
ISN 0241      340 CONTINUE
C
ISN 0242      A(N1,N1)=SUM-SM
ISN 0243      A(N1,N3)=A(N1,N3)-(SUM-SM)

```

GEN05222
GEN05224
GEN05226
GEN05228
GEN05230
GEN05232
GEN05234
GEN05236
GEN05238
GEN05240
GEN05242
GEN05244
GEN05246
GEN05250
GEN05252
GEN05254
GEN05256
GEN05258
GEN05260
GEN05262
GEN05264
GEN05266
GEN05270
GEN05272
GEN05274
GEN05276
GEN05278
GEN05280
GEN05282
GEN05284
GEN05286
GEN05288
GEN05290
GEN05292
GEN05294
GEN05296
GEN05298
GEN05300
GEN05302
GEN05304
GEN05306
GEN05308
GEN05310
GEN05312
GEN05314
GEN05316
GEN05318
GEN05320
GEN05322
GEN05324
GEN05326
GEN05328
GEN05330

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ISN 0244
ISN 0245
ISN 0246

A(N1,N2)=HSUM
A(N2,N2)=A(N2,N2)+CPSUM+QURV
A(N2,N3)=A(N2,N3)+HIN-HSUM-Q

GEN05332
GEN05334
GEN05336

ISN 0247
ISN 0248
ISN 0249

C
C-----NEGATIVE OF L-ELEMENT QUAS. F(L)
DO 350 L=1,NLM
A(L,N3)=A(L,N3)+B0(L)-A(L,N1)
350 CONTINUE

GEN05338
GEN05340
GEN05342
GEN05344
GEN05346

ISN 0250
ISN 0251
ISN 0252
ISN 0253

C
C-----STORE SYMMETRIC ELEMENTS OF MATRIX
C
DO 360 I=1,N2
DO 360 J=1,N2
A(I,J)=A(I,J)
360 CONTINUE

GEN05348
GEN05350
GEN05352
GEN05354
GEN05356
GEN05358
GEN05360

ISN 0254
ISN 0255
ISN 0256
ISN 0258
ISN 0259
ISN 0260

C
C-----INTERCHANGE SM-LON WITH ELEMENT ROW L WITH LARGEST A(L,N1) TO
C-----AVOID POTENTIAL ZERO IN DIAGONAL ELEMENT A(N1,N1)
C
IM1=0.
DO 370 L=1,NLM
IF (A(L,N1).LT.IM1) GO TO 370
IM1=A(L,N1)
LL=L
370 CONTINUE

GEN05362
GEN05364
GEN05366
GEN05368
GEN05370
GEN05372
GEN05374
GEN05376
GEN05378
GEN05380

ISN 0261
ISN 0262
ISN 0263
ISN 0264
ISN 0265
ISN 0266

C
DO 380 J=1,N3
IM1=A(N1,J)
A(N1,J)=A(LL,J)
A(LL,J)=IM1
380 CONTINUE
IM1=N2

GEN05382
GEN05384
GEN05386
GEN05388
GEN05390
GEN05392
GEN05394
GEN05396

C
C**** **** **** **** **** **** CHAPTER 4 ****
C**** **** **** **** **** **** CHAPTER 4 ****

**GEN05398
**GEN05400

ISN 0267

C
C ***MATRIX SOLUTION***
C SOLVE FOR CORRECTIONS BY STANDARD PIVOTAL GAUSSIAN ELIMINATION

GEN05402
GEN05404
GEN05406

ISN 0268
ISN 0270
ISN 0272
ISN 0273
ISN 0274
ISN 0275
ISN 0276
ISN 0277
ISN 0278
ISN 0279
ISN 0280

C
400 KMAT=IM1+1
C-----OPTIONAL OUTPUT OF INTERMEDIATE VALUES FOR DEBUGGING
IF (I.NU).LEDEBUG) GO TO 410
IF (INDEBUG.LT.5) GO TO 410
WRITE(C,401)
401 FURMA(1M0,10X,30ELEMENTS A(I,K) OF CORRECTION MATRIX/)
DO 403 K=1,IM1
WRITE(C,402) (A(K,I),I=1,KMAT)
402 FURMA(1X,1P16D8.0)
403 CONTINUE
410 CONTINUE
DO 450 NN=1,IM1
IF (A(NN,NN).EQ.0.0) GO TO 500

GEN05410
GEN05412
GEN05414
GEN05416
GEN05418
GEN05420
GEN05422
GEN05424
GEN05426
GEN05428
GEN05430
GEN05432
GEN05434

ISN 0282
ISN 0283

C-----CHANGE 1.000 TO 1.0 FOR NON-IBM MACHINES NOT REQUIRING DOUBLE PRE
D1M1=1./A(NN,NN)
K=NN+1

GEN05436
GEN05438
GEN05440


```

ISN 0284      DO 420 J=K,KMAT
ISN 0285      A(NN,J)=A(NN,J)*DIM1
ISN 0286      420 CONTINUE
ISN 0287      IF (K.EQ.KMAT) GO TO 430
ISN 0288      DO 440 I=K,IMAT
ISN 0289      IF (A(I,NN).EQ.0.0) GO TO 440
ISN 0292      DO 450 J=K,KMAT
ISN 0293      A(I,J)=A(I,J)-A(I,NN)*A(NN,J)
ISN 0294      430 CONTINUE
ISN 0295      440 CONTINUE
ISN 0296      450 CONTINUE

```

C
C-----BACK SOLVE FOR CORRECTION VECTOR
C

```

ISN 0297      K=IMAT
ISN 0298      460 J=K+1
ISN 0299      USUM=0.
ISN 0300      X(K)=0.0
ISN 0301      IF (IMAT.LI.J) GO TO 480
ISN 0303      DO 470 I=J,IMAT
ISN 0304      USUM=USUM+A(I,J)*X(I)
ISN 0305      470 CONTINUE
ISN 0306      480 CONTINUE
ISN 0307      X(K)=A(K,KMAT)-USUM
ISN 0308      K=K-1
ISN 0309      IF (K.NE.0) GO TO 460

```

ISN 0311

RETURN

C
C***** ***** ***** ***** ***** CHAPTER 5 *****
C***** ***** ***** ***** ***** CHAPTER 5 *****

C
C ***SINGULAR MATRIX***
C

```

ISN 0312      500 WRITE(6,501)
ISN 0313      501 FORMAT(1MC,1CX,31(4H****),16HSINGULAR MATRIX/)
ISN 0314      C-----SET LCONV=.TRUE. TO NULLIFY SPECF OF SINGULAR MATRIX
ISN 0315      LCONV=.TRUE.
ISN 0316      RETURN
ISN 0316      END

```

GEN05442
GEN05444
GEN05446
GEN05448
GEN05450
GEN05452
GEN05454
GEN05456
GEN05458
GEN05460
GEN05462
GEN05464
GEN05466
GEN05468
GEN05470
GEN05472
GEN05474
GEN05476
GEN05478
GEN05480
GEN05482
GEN05484
GEN05486
GEN05488
GEN05490
GEN05492
GEN05494
GEN05496
GEN05498
*GEN05500
*GEN05502
GEN05504
GEN05506
GEN05508
GEN05510
GEN05512
GEN05514
GEN05516
GEN05518
GEN05520

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*OPTIONS IN EFFECT*NAME(MAIN) NOOPTIMIZE LINECOUNT(57) SIZE(MAX) AUTOdbl(NONE)
*OPTIONS IN EFFECT*SOURCE EBCDIC NULIST NODECL OBJECT NOMAP NOFORMAT NOGUS(M) NOXREF NUALC NUANSF TERM FLA
STATISTICS SOURCE STATEMENTS = 319, PROGRAM SIZE = 15604, SUBPROGRAM NAME = CALL
STATISTICS NO DIAGNOSTICS GENERATED
***** END OF COMPILATION *****
316K BYTES OF CORE NOT USED

REQUESTED OPTIONS:

OPTIONS IN EFFECT: NAME(MAIN) NOOPTIMIZE LINCOUNT(57) SIZE(MAX) AUTOOBL(NONE) SOURCE EBCDIC NULIST NODUCK DEJECT NCMAP NUFORMAT NUGS(IM) NUXREF NCALC NUANSF TERM FL

```

ISN 0002      SUBROUTINE HOPS
ISN 0003      IMPLICIT REAL*8 (A-H,I-Z)
              GENU5522
              GENU5524
              GENU5526
              GENU5528
ISN 0004      DIMENSION ASUB(20,3)
ISN 0005      LOGICAL LADLAB,LCUNVG,LDEBUB,LEQUIL,LNR6,LKCAL
              GENU5530
              GENU5532
              GENU5534
ISN 0006      COMMON
              GENU5536
              1/CCHEM1/CPSUM,FR,PPLN,KGAS,KGASIN,SMINV,TKINV,TLN,LCUNVG,LNR6
              GENU5538
              1/CINDEX/ICU,ICUZ,IUNZ,IBZU,IUNZ,IUOZ,IHCP,ILC,ILN,IMAT,ITER,
              GENU5540
              2 JJ,INZ,IZZ,NS,NA,NGLIB,NGLUBP,NLM,NU,NSM
              GENU5542
              1/CPAKAM/ASUB,NI,NE,EMV,ER,HSUBU,NDEBUB,NS,PA,QU,Q1,Q2,Q3,Q4,KNUP,
              GENU5544
              2 SM,S1(20),S2(20),IK,LADLAB,LDEBUB,LEQUIL,LKCAL
              GENU5546
              1/CPEL/HC(20),SC(20),SMW(20),SSAVE(20),Z(20)
              GENU5548
              GENU5550
C *****
C THIS SUBROUTINE CALCULATES THE NON-DIMENSIONAL, 1-ATM VALUES OF
C ENTHALPY, SPECIFIC HEAT, AND ENTROPY FOR A GIVEN VALUE OF TEMPERATURE
C (DEG K) THE Z ARRAY IS REFERENCED AS HAVING ONLY ONE SUBSCRIPT
C TO SAVE INTERNAL SUBSCRIPT CALCULATIONS.
C Z(IC,1,IS) --- Z(IC+7*(IT-1)+7*(IS-1)) FOR Z(1,2,20)
C WHERE IC=1,7. COEF FOR TEMP RANGE II=1 OR 2. FOR SPECIES IS=1,NS.
C NOTE THAT THE FIRST 2 SUBSCRIPTS ARE REVERSED FROM THE
C GORDON AND MCBRIDE PRACTICE
C REFERENCE GORDON AND MCBRIDE (NASA SP-273, 1971)
C *****
ISN 0007      DATA ICIT/14/
              GENU5552
              GENU5554
              GENU5556
              GENU5558
              GENU5560
              GENU5562
              GENU5564
              GENU5566
              GENU5568
              GENU5570
ISN 0008      IT=0
ISN 0009      IF ((K.LT.1000.0) IT=1
              GENU5572
              GENU5574
              GENU5576
              GENU5578
              GENU5580
              GENU5582
              GENU5584
              GENU5586
              GENU5588
              GENU5590
              GENU5592
              GENU5594
              GENU5596
              GENU5598
              GENU5600
              GENU5602
              GENU5604
              GENU5606
              GENU5608
              GENU5610
              GENU5612
              GENU5614
              GENU5616
              GENU5618
              GENU5620
ISN 0017      DO IC 1=1,NS
ISN 0018      K=IT+ICIT+(I-1)
ISN 0019      CP1=Z(K+1)
ISN 0020      CP2=IK*Z(K+2)
ISN 0021      CP3=IKSU+Z(K+3)
ISN 0022      CP4=IKCU+Z(K+4)
ISN 0023      CP5=IK4+Z(K+5)
ISN 0024      CPSUM=CPSUM+(CP1+CP2+CP3+CP4+CP5)*SZ(I)
ISN 0025      HC(I)=0.2*CP5+0.25*CP4+0.3333333*CP3+0.5*CP2+CP1+(KINV*Z(K+6)
ISN 0026      10 CONTINUE
ISN 0027      RETURN
              GENU5622

```

C-----HCPS=2 ---- CPSUM, HC(1) AND SC(1) REQUIRED

```

C
C
20 CONTINUE
   DO 30 I=1,NS
   K=1+ILN(I)+(I-1)
   CP1=Z(K+1)
   CP2=TK+Z(K+2)
   CP3=TKSQ+Z(K+3)
   CP4=TKCU*Z(K+4)
   CP5=TK+Z(K+5)
   CPSUM=CPSUM+(CP1+CP2+CP3+CP4+CP5)*S2(I)
   HC(1)=0.2*CP5+0.25*CP4+0.33333333*CP3+0.5*CP2+CP1+TK*INV*Z(K+6)
   SC(1)=0.25*CP5+0.33333333*CP4+0.5*CP3+CP2+ILN*CP1+Z(K+7)
30 CONTINUE
RETURN
END

```

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GEN05622
GEN05624
GEN05626
GEN05628
GEN05630
GEN05632
GEN05634
GEN05636
GEN05638
GEN05640
GEN05642
GEN05644
GEN05646
GEN05648
GEN05650
GEN05652
GEN05654

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*OPTIONS IN EFFECT*NAME(MAIN) NOOPTIMIZE LINECOUNT(57) SIZE(MAX) AUTODBLE(NONE)

*OPTIONS IN EFFECT*SOURCE EBCDIC NDLIST NOBACK DEJECT NDMAP NOFORMAT NOJUSTIFY NOXREF NOALC NUANSF TERM FL

STATISTICS SOURCE STATEMENTS = 40, PROGRAM SIZE = 1300, SUBPROGRAM NAME = HCPS

STATISTICS NO DIAGNOSTICS GENERATED

***** END OF COMPILATION *****

372K BYTES OF CORE NOT USED

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	ELEMENTS		
C	12.011150	4.000000	
H	1.007970	1.000000	
O	15.499400	-2.000000	
N	14.000700	0.0	

THEMUM FOR CH4/AIR COMBUSTION

CH2	J	B/69	C	1.H	2.0	0.0	0.0	300.000	5000.000	
0.258492650+01	0.454999250-02	-0.109744150-05	0.292734140-04	-0.191185800-15						2
0.453555120+03	0.512550980+01	0.212770400+01	0.335123610-02	0.114525410-05						3
-0.255910700-08	0.114572500-11	0.453504440+03	0.520090200+01							4

CH3	J	B/69	C	1.H	2.0	0.0	0.0	300.000	5000.000	
0.254003270+01	0.000090800-02	-0.217405580-05	0.260425700-04	-0.227253000-15						2
0.184498150+03	0.550507510+01	0.340003500+01	0.583128+00-02	0.101100020-05						3
-0.180592360-06	0.000051820-12	0.105131040+03	0.241721920+01							4

CH4	J	B/61	C	1.H	4.00	0.00	0.0	300.000	5000.000	
0.150270720+01	0.007201900-01	-0.251015220-05	0.077709700-07	-0.442057000-15						2
-0.997010780+04	0.117071450+02	0.382019320+01	-0.397943810-02	0.2455063400-04						3
-0.227329200-07	0.090209570-11	0.101449500+03	0.800900750+00							4

HCU	J	12/70	H	1.0	1.0	1.0	0.0	300.000	5000.000	
0.347383400+01	0.543702270-02	-0.150320040-05	0.249260450-09	-0.170443310-15						2
0.395940050+04	0.004535400+01	0.308401920+01	-0.829744480-03	0.775008090-05						3
-0.706109020-08	0.199717300-11	0.405038000+04	0.485541330+01							4

CH2U	J	B/61	C	1.H	2.0	1.0	0.0	300.000	5000.000	
0.283042490+01	0.000022980-02	-0.268820470-05	0.479712560-09	-0.521184060-15						2
-0.152300310+05	0.785311090+01	0.519037850+01	-0.257017850-02	0.185468150-04						3
-0.178090770-07	0.555044510-11	0.150809470+03	0.475481030+01							4

CO	J	B/65	C	1.0	1.00	0.00	0.0	300.000	5000.000	
0.296400900+01	0.148915900-02	-0.578996840-06	0.103045770-09	-0.095555500-14						2
-0.142452280+05	0.654791500+01	0.571009280+01	-0.101909040-02	0.309235940-05						3
-0.203196740-08	0.259533490-12	0.145503100+03	0.295555510+01							4

CO2	J	B/65	C	1.0	2.00	0.00	0.0	300.000	5000.000	
0.440080410+01	0.309817190-02	-0.125925710-05	0.227415250-09	-0.155259540-15						2
-0.489014420+05	0.900559820+00	0.240077970+01	0.813509510-02	-0.000708160-05						3
0.200218010-08	0.032740390-15	-0.483775270+05	0.969514570+01							4

H	J	B/65	H	1.00	0.00	0.00	0.0	300.000	5000.000	
0.250000000+01	0.0	0.0	0.0	0.0						2
0.254716270+05	-0.400117030+00	0.250000000+01	0.0	0.0						3
0.0	0.0	0.254716270+05	-0.400117030+00							4

H2	J	B/61	H	2.0	0.0	0.0	0.0	300.000	5000.000	
0.316019010+01	0.511194040-03	0.520442100-07	0.549099730-10	-0.309453450-14						2
-0.077300420+03	0.290294210+01	0.305744510+01	0.207020000-02	-0.500991620-05						3
0.552105910-06	-0.181227090-11	0.988904740+03	0.229970500+01							4

H2U	J	B/61	H	2.0	1.00	0.00	0.0	300.000	5000.000	
0.271070330+01	0.794513740-02	-0.802243740-06	0.102200820-09	-0.404721450-14						2
-0.295058200+05	0.003050710+01	0.407012750+01	-0.110844990-02	0.415211800-05						3
-0.296374040-08	0.807021030-12	-0.302797220+05	-0.322700460+00							4

HD J 3/64 H 1.00 2.00 0.00 0.00 300.000 5000.000
 U.378662800+01 U.278664000-02 U.161687080-05 U.171839400-09 U.110218520-13 2
 U.116665000+04 U.481476110+01 U.350948500+01 U.114996700-02 U.587842590-05 3
 -0.777955190-08 U.276078830-11 U.138033310+04 U.682763250+01 4

N J 3/61 N 1.00 0.00 0.00 0.00 300.000 5000.000
 U.245026820+01 U.166614580-03 U.746533730-07 U.167465240-10 U.102598390-14 2
 U.561160400+05 U.444075010+01 U.250307140+01 U.218001810-04 U.542052870-07 3
 -0.564756020-10 U.209996440-13 U.560989040+05 U.416757640+01 4

NU J 0703 N 1.0 1.00 0.00 0.0 300.000 5000.000
 U.318960000+01 U.133122040-02 U.528993180-06 U.929193320-10 U.600479320-14 2
 U.982632900+04 U.064952200+01 U.440499210+01 U.341017850-02 U.790191900-05 3
 -0.611395160-08 U.159190760-11 U.974539340+04 U.299749800+01 4

NU2 J 9704 N 1.0 2.00 0.00 0.0 300.000 5000.000
 U.462407710+01 U.252605320-02 U.160949800-05 U.158792390-09 U.137593840-13 2
 U.228999000+04 U.133241360+01 U.345892360+01 U.260476640-02 U.668806070-05 3
 -0.955567250-08 U.36195880-11 U.281522850+04 U.831109830+01 4

N2 J 9705 N 2.0 0.0 0.0 0.0 310.000 5000.000
 U.289031940+01 U.151208080-02 U.577352710-06 U.998673930-10 U.65205550-14 2
 -0.950628440+05 U.040151480+01 U.567482610+01 U.120819060-02 U.732401020-05 3
 -0.652115590-09 U.125177550-12 U.106112880+04 U.255864280+01 4

NU J 12704 N 2.0 1.00 0.00 0.0 300.000 5000.000
 U.473006790+01 U.252006010-02 U.115581150-05 U.212006030-09 U.145046070-13 2
 U.310103200+04 U.112101010+01 U.260891960+01 U.069490110-02 U.001106240-05 3
 U.222150770-08 U.110503300-13 U.815901230+04 U.922609520+01 4

U J 0702 U 1.00 0.00 0.00 0.0 300.000 5000.000
 U.254205960+01 U.275506190-04 U.310280330-08 U.455106740-11 U.436015150-15 2
 U.292300050+05 U.492030600+01 U.294042870+01 U.163816650-02 U.242103160-05 3
 -0.166284920-08 U.389069040-12 U.291476440+05 U.296399490+01 4

UH J 1270 U 1.0 1.0 0.0 0.0 300.000 5000.000
 U.291312300+01 U.954102480-03 U.190843250-06 U.127307950-10 U.248039410-15 2
 U.396470600+04 U.542881350+01 U.383055180+01 U.107020140-02 U.548497570-06 3
 U.200455750-09 U.253842650-12 U.367158710+04 U.498054500+00 4

U2 J 9705 U 2.0 0.0 0.0 0.0 300.000 5000.000
 U.362195350+01 U.136182640-03 U.140522280-06 U.362015500-10 U.285456270-14 2
 -0.120198250+04 U.361509600+01 U.362559850+01 U.187821840-02 U.705545440-05 3
 -0.670551570-08 U.215559950-11 U.164752200+04 U.450527780+01 4

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MECHANISM - CY HALSMANS ULTRASYSTEM LM4/AJK

1. HCU	M	LU	H	H	17.398	-1.500	8461.000	HALU
CALCULATED REVERSE RATE DATA, STD DEV AND CORR COEF =					9.091	0.0	-1145.308	50.6350-0398.2930-02
2. HCU	H	LU	H2		7.477	1.000	0.0	HALU
CALCULATED REVERSE RATE DATA, STD DEV AND CORR COEF =					11.482	0.0	47022.495	99.8910-0399.9950-02
3. CH20	U	HCU	UH		8.201	1.000	2215.000	HALU
CALCULATED REVERSE RATE DATA, STD DEV AND CORR COEF =					16.541	0.0	10298.286	10.9350-0299.8810-02
4. HCU	UH	LU	H2U		7.477	1.000	0.0	HALU
CALCULATED REVERSE RATE DATA, STD DEV AND CORR COEF =					12.615	0.0	24014.418	80.2010-0399.9950-02
5. HCU	U	LU	UH		0.471	1.000	152.000	HALU
CALCULATED REVERSE RATE DATA, STD DEV AND CORR COEF =					11.024	0.0	46721.151	70.4710-0399.9950-02
6. CH3	U	CH20	H		9.201	0.500	1510.000	HALU
CALCULATED REVERSE RATE DATA, STD DEV AND CORR COEF =					12.262	0.0	25093.751	10.9350-0299.8810-02
7. CH4	U	CH3	UH		7.000	1.000	4128.000	HALU
CALCULATED REVERSE RATE DATA, STD DEV AND CORR COEF =					8.918	0.0	4466.562	10.9350-0299.8810-02

8.	CH4	H	DATA	LH3	H2	7.700	1.000	5635.000	WALU
	CALCULATED REVERSE RATE DATA,	STD DEV	AND CORR COEF =			9.975	0.0	6546.927	11.2210-0299.7010-02
9.	CH4	UH	DATA	LH3	H2U	10.477	0.0	2516.000	WALU
	CALCULATED REVERSE RATE DATA,	STD DEV	AND CORR COEF =			9.704	0.0	9964.260	31.0710-0399.9900-02
10.	HU0	U2	DATA	U0	HU2	7.903	0.0	0.0	WALU
	CALCULATED REVERSE RATE DATA,	STD DEV	AND CORR COEF =			10.259	0.0	16286.820	16.0030-0399.9900-02
11.	U0	UH	DATA	U0	H	1.602	0.500	0.0	WALU
	CALCULATED REVERSE RATE DATA,	STD DEV	AND CORR COEF =			10.473	0.0	11918.292	40.2300-0.99.9000-02
12.	U2	H	DATA	U0	U	12.000	0.0	5635.000	WALU
	CALCULATED REVERSE RATE DATA,	STD DEV	AND CORR COEF =			6.719	0.0	-12217.980	23.1800-0399.9900-02
13.	H	UH	DATA	H2	U	6.903	1.000	3525.000	WALU
	CALCULATED REVERSE RATE DATA,	STD DEV	AND CORR COEF =			10.942	0.0	6235.656	62.9990-0399.8900-02
14.	H2U	H	DATA	UH	H	12.477	0.0	52876.000	WALU
	CALCULATED REVERSE RATE DATA,	STD DEV	AND CORR COEF =			8.256	0.0	-1236.261	22.9400-0399.9900-02
15.	H	HU0	DATA	UH	UH	11.398	0.0	937.000	WALU
	CALCULATED REVERSE RATE DATA,	STD DEV	AND CORR COEF =			10.416	0.0	20915.265	42.2310-0399.9900-02
16.	UH	H2	DATA	H	H2U	10.390	0.0	2018.000	WALU
	CALCULATED REVERSE RATE DATA,	STD DEV	AND CORR COEF =			11.032	0.0	10295.472	15.1700-0399.9900-02
17.	H	U	DATA	LH	M	7.903	0.0	0.0	WALU
	CALCULATED REVERSE RATE DATA,	STD DEV	AND CORR COEF =			13.153	0.0	21481.213	61.9300-0410.0000-01
18.	UH	U	DATA	H	U2	10.398	0.0	0.0	WALU
	CALCULATED REVERSE RATE DATA,	STD DEV	AND CORR COEF =			11.495	0.0	8066.454	24.2100-0399.9900-02
19.	H	U2	DATA	HU2	M	7.176	0.0	503.500	WALU
	CALCULATED REVERSE RATE DATA,	STD DEV	AND CORR COEF =			12.317	0.0	23959.693	22.8000-0399.9900-02
20.	UH	UH	DATA	H2U	U	7.778	0.0	503.500	WALU
	CALCULATED REVERSE RATE DATA,	STD DEV	AND CORR COEF =			10.769	0.0	9148.788	17.1600-0399.9900-02
21.	UH	N	DATA	H	HU	8.778	0.500	4028.000	WALU
	CALCULATED REVERSE RATE DATA,	STD DEV	AND CORR COEF =			11.048	0.0	29029.744	14.1590-0310.0000-01
22.	H	N2U	DATA	UH	N2	10.903	0.0	1553.000	WALU
	CALCULATED REVERSE RATE DATA,	STD DEV	AND CORR COEF =			9.609	0.0	40513.129	11.2010-0399.9900-02
23.	H	HU	DATA	H2	U	11.176	0.0	0.0	WALU
	CALCULATED REVERSE RATE DATA,	STD DEV	AND CORR COEF =			10.831	0.0	37862.229	33.2200-0410.0000-01
24.	H	U2	DATA	HU	U	6.778	1.000	3172.000	WALU
	CALCULATED REVERSE RATE DATA,	STD DEV	AND CORR COEF =			9.791	0.0	20935.934	66.8200-0399.9696-02
25.	N2U	U	DATA	HU	HU	11.000	0.0	15000.000	WALU
	CALCULATED REVERSE RATE DATA,	STD DEV	AND CORR COEF =			9.480	0.0	34276.998	23.4300-0399.9900-02
26.	N2U	H	DATA	H2	U	11.000	0.0	25176.000	WALU
	CALCULATED REVERSE RATE DATA,	STD DEV	AND CORR COEF =			6.456	0.0	6624.916	8.0010-0399.8410-02
27.	HU0	UH0	DATA	UH2	UH2U	0.176	0.700	2014.000	WALU
	CALCULATED REVERSE RATE DATA,	STD DEV	AND CORR COEF =			11.176	0.0	-6657.06	29.1510-0459.9900-02
28.	HU0	UH4	DATA	UH2	UH0	8.903	0.000	4522.000	WALU
	CALCULATED REVERSE RATE DATA,	STD DEV	AND CORR COEF =			10.192	0.0	-2048.251	30.0000-0399.8946-02
29.	UH0	H	DATA	UH2	H2	8.201	0.700	1151.000	WALU
	CALCULATED REVERSE RATE DATA,	STD DEV	AND CORR COEF =			10.016	0.0	-41.007	29.1000-0310.2300-02
30.	UH0	UH	DATA	UH2	H2U	7.176	0.700	1067.000	WALU
	CALCULATED REVERSE RATE DATA,	STD DEV	AND CORR COEF =			10.926	0.0	1400.210	40.1100-0399.9900-02

31. CH2 UZ
CALCULATED REVERSE RATE DATA, STD DEV AND CORR COEF =

8.699
10.982

0.500
0.0

3525.000
34709.572

ALU
22.2540-0310.0000-01

32. CH3 U2
CALCULATED REVERSE RATE DATA, STD DEV AND CORR COEF =

10.477
10.499

0.0
0.0

15106.000
42055.852

64.0110-0440.0000-04

33. CH4 H
CALCULATED REVERSE RATE DATA, STD DEV AND CORR COEF =

14.301
9.287

0.0
0.0

44310.000
70319.941

NALU
74.2400-0399.9500-02

34. CH3 H02
CALCULATED REVERSE RATE DATA, STD DEV AND CORR COEF =

0.000
11.714

0.500
0.0

31.21.000
33073.393

NALU
48.0900-0410.0000-02

1.	CH3 H02	H	---	CU	H	M	
2.	H02	H	---	CU	H2		
3.	CH2U	U	---	H02	UH		
4.	H02	UH	---	CU	H2U		
5.	H02	U	---	CU	UH		
6.	CH3	U	---	CH2U	H		
7.	CH4	U	---	CH3	UH		
8.	CH4	H	---	CH3	H2		
9.	CH4	UH	---	CH3	H2U		
10.	H02	H2	---	CU	H02		
11.	CU	UH	---	CU2	H		
12.	CU2		M	---	CU	U	M
13.	H	UH		---	H2	U	
14.	H2U		M	---	UH	H	M
15.	H	H02		---	UH	UH	
16.	UH	H2		---	H	H2U	
17.	H	U	M	---	UH		M
18.	UH	U		---	H	U2	
19.	H	U2	M	---	H02		M
20.	UH	UH		---	H2U	U	
21.	UH	N		---	H	N0	
22.	H	N2U		---	UH	N?	
23.	N	N0		---	H2	U	
24.	N	U2		---	N0	U	
25.	N2U	U		---	N0	H?	
26.	N2U		M	---	N?	U	M
27.	H02	CH3		---	CH3	UH?	

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7.	CO2	44.0100+00	0.0	0.0
8.	H	10.0800+01	0.0	0.0
9.	H2	20.1590+01	0.0	0.0
10.	H2O	18.0150+00	0.0	0.0
11.	H2O	33.0070+00	0.0	0.0
12.	N	14.0070+00	0.0	0.0
13.	NO	30.0060+00	0.0	0.0
14.	NO2	46.0050+00	0.0	0.0
15.	N2	28.0130+00	0.0	0.0
16.	N2O	44.0130+00	0.0	0.0
17.	O	15.9990+00	0.0	0.0
18.	OH	17.0070+00	0.0	0.0
19.	O2	31.9990+00	0.0	0.0

TEMPERATURE = 10.0000+02 DEG K
 ENTHALPY = -22.8710+05 JOULES/KG
 PRESSURE = 10.0000+04 N/M**2
 DENSITY = 19.2990+02 KG/M**3
 MEAN MOL WT = 10.0430+00 KG/KGMOLE

REACTANTS-2 SAIRK							
O	2.00000	0.0	0.0	O2	1.00000	M	6
N	2.00000	0.0	0.0	N2	3.70000	M	6

*** REACTANT STREAM 2 ***

I	SPECIES	MOLECULAR WEIGHT (KGMOLE I)/(KG I)	MOLE NUMBERS (KGMOLE I)/(KG X)	MASS FRACTIONS (KG I)/(KG X)
1.	CH2	14.0270+00	0.0	0.0
2.	CH3	15.0350+00	0.0	0.0
3.	CH4	16.0430+00	0.0	0.0
4.	HCO	29.0150+00	0.0	0.0
5.	CH2O	30.0260+00	0.0	0.0
6.	CO	28.0110+00	0.0	0.0
7.	CO2	44.0100+00	0.0	0.0
8.	H	10.0800+01	0.0	0.0
9.	H2	20.1590+01	0.0	0.0
10.	H2O	18.0150+00	0.0	0.0
11.	H2O	33.0070+00	0.0	0.0
12.	N	14.0070+00	0.0	0.0
13.	NO	30.0060+00	0.0	0.0
14.	NO2	46.0050+00	0.0	0.0
15.	N2	28.0130+00	27.3790-03	70.0990-02
16.	N2O	44.0130+00	0.0	0.0
17.	O	15.9990+00	0.0	0.0
18.	OH	17.0070+00	0.0	0.0
19.	O2	31.9990+00	72.8180-04	23.3010-02

TEMPERATURE = 10.0000+02 DEG K
 ENTHALPY = 75.2910+04 JOULES/KG
 PRESSURE = 10.0000+04 N/M**2
 DENSITY = 34.7000+02 KG/M**3
 MEAN MOL WT = 20.0510+00 KG/KGMOLE

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KARE N

KASE= 1 LESSON= 0 MODEL= 1 MASSIV= 1 INERT= 2

UA	UB	UC	UD	UA	UB	UC	UD	RA	RH	FL	KL
0.3470+00	0.3470+00	0.4630+00	0.4630+00	0.1000+04	0.1000+04	0.1000+04	0.1000+04	0.0	0.0	0.3330+02	0.1000+02
XEND	XAUT	ACLAS1	IAN	PRESS	PREXP	NET	PKA1	AMACH			
0.0	0.0	0.2000+01	0.0	0.1000+06	0.0	0.0	0.1000+07				

7	U.0	U.0	U.0	U.0	U.0	U.0	U.0	U.0	U.0	U.0	U.0
	0.5260+00	0.5190+00	0.5200+01	0.1051+05	0.1580+00	0.2110+06	0.2630+00	0.3160+06	0.3600+00	0.4210+00	0.4740+00
			0.6320+00	0.6090+00	0.7370+00	0.7090+00	0.6420+00	0.6950+00			

ISTEP= 0 IAX= 0 IEND= 0 IOUT= 0 KIN= 3 KEX= 2 UAX= 0.3350+06 PSII= 0.0 PSIE= 0.7840+07
 RM1= 0.0 RME=-0.2340+02 ME1= 0.7840+07
 XU= 0.1000+29 UFLUX=-0.9150+08 PRESI= 0.0 AEXI= 0.0 FLUXI= 0.0
 -0.2690+42 -0.2690+42 -0.2690+42 -0.2690+42 -0.2690+42 -0.2690+42 -0.2690+42 -0.2690+42 -0.2690+42 -0.2690+42
 -0.2690+42 -0.2690+42 -0.2690+42 -0.2690+42 -0.2690+42 -0.2690+42 -0.2690+42 -0.2690+42 -0.2690+42 -0.2690+42

9	0.0	0.0140+01	0.2510+03	1.4480+03	1.6680+03	0.7020+03	0.7850+03	0.6060+03	0.4790+03	0.4950+03	0.4630+03
10	0.0	0.1100+02	0.1100+02	0.1270+02	0.1210+02	0.1560+02	0.1400+02	0.1450+02	0.1440+02	0.1240+02	0.1230+02
	0.3470+00	0.3470+00	0.3470+00	0.3470+00	0.3470+00	0.3470+00	0.3470+00	0.3470+00	0.3470+00	0.3470+00	0.3470+00

MASS FRACTIONS, ENTHALPY, TEMP, P74 EQUIV RATIO CELL CHARGING EMV (KGM 3-D), CELL RES TIME

SFA	CH2 NB	CH2	CH3	H2O	CH2U	LU	LU2	H	H2	H2O	H2	H2O	H2	H2O
								M (J/KG)	M (J/KG)	EM (KATM)	EM (KATM)	EM (KATM)	EM (KATM)	EM (KATM)
1	0.0	0.0	1.000+00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-2.290+06	1.000+03	1.000+06	0.0	0.0	0.0	0.0
2	0.0	0.0	1.000+00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-2.290+06	1.000+03	1.000+06	0.0	0.0	0.0	0.0
3	0.0	0.0	1.000+00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-2.290+06	1.000+03	1.000+06	0.0	0.0	0.0	0.0
4	0.0	0.0	1.000+00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-2.290+06	1.000+03	1.000+06	0.0	0.0	0.0	0.0
5	0.0	0.0	1.000+00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-2.290+06	1.000+03	1.000+06	0.0	0.0	0.0	0.0
6	0.0	0.0	1.000+00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-2.290+06	1.000+03	1.000+06	0.0	0.0	0.0	0.0
7	0.0	0.0	1.000+00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-2.290+06	1.000+03	1.000+06	0.0	0.0	0.0	0.0
8	0.0	0.0	1.000+00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-2.290+06	1.000+03	1.000+06	0.0	0.0	0.0	0.0
9	0.0	0.0	1.000+00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-2.290+06	1.000+03	1.000+06	0.0	0.0	0.0	0.0
10	0.0	0.0	1.000+00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-2.290+06	1.000+03	1.000+06	0.0	0.0	0.0	0.0
11	0.0	0.0	1.000+00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-2.290+06	1.000+03	1.000+06	0.0	0.0	0.0	0.0
12	0.0	0.0	1.000+00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-2.290+06	1.000+03	1.000+06	0.0	0.0	0.0	0.0

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13	0.0 0.0	0.0 0.0	1.000+00 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 -2.290+06	0.0 1.000+03	0.0 1.000+06	0.0 0.0	0.0 0.0
14	0.0 0.0	0.0 0.0	1.000+00 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 -2.290+06	0.0 1.000+03	0.0 1.000+06	0.0 0.0	0.0 0.0
15	0.0 0.0	0.0 0.0	1.000+00 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 -2.290+06	0.0 1.000+03	0.0 1.000+06	0.0 0.0	0.0 0.0
16	0.0 0.0	0.0 0.0	1.000+00 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 -2.290+06	0.0 1.000+03	0.0 1.000+06	0.0 0.0	0.0 0.0
17	0.0 0.0	0.0 0.0	1.000+00 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 -2.290+06	0.0 1.000+03	0.0 1.000+06	0.0 0.0	0.0 0.0
18	0.0 0.0	0.0 0.0	1.000+00 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 -2.290+06	0.0 1.000+03	0.0 1.000+06	0.0 0.0	0.0 0.0
19	0.0 0.0	0.0 0.0	1.000+00 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 -2.290+06	0.0 1.000+03	0.0 1.000+06	0.0 0.0	0.0 0.0
20	0.0 0.0	0.0 0.0	1.000+00 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 -2.290+06	0.0 1.000+03	0.0 1.000+06	0.0 0.0	0.0 0.0
21	0.0 0.0	0.0 0.0	1.000+00 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 -2.290+06	0.0 1.000+03	0.0 1.000+06	0.0 0.0	0.0 0.0
22	0.0 0.0	0.0 0.0	1.000+00 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 -2.290+06	0.0 1.000+03	0.0 1.000+06	0.0 0.0	0.0 0.0

ISIP= 1 IAX= 0 IEND= 6 IOUT= 0 KIN= 3 KEX= 2 UX= 0.3100-06 PSII= 0.0 PSIE= 0.1920-07
 RMI= 0.0 KAT= -0.2020-02 PEI= 0.7920-07
 XU= 0.3000-06 UFLUX= -0.9130-08 PRESSU= 0.0 AERU= 0.0 FLUXIJE= 0.0
 -0.2690+42 -0.2090+42 0.4890+08 -0.2690+42 -0.2690+42 -0.2690+42 -0.2690+42 -0.2690+42 -0.2690+42 -0.2690+42
 -0.2090+42 -0.2090+42 -0.2690+42 -0.2690+42 -0.2100-08 -0.2690+42 -0.2690+42 -0.2690+42 -0.2690+42 -0.2690+42 -0.2690+42

9	0.0 0.1120-02 0.3470+00 0.3470+00	0.5140-11 0.1170-02 0.3470+00 0.3470+00	0.3530-03 0.1220-02 0.3470+00 0.3470+00	0.4490-03 0.1270-02 0.3470+00 0.3470+00	0.6110-03 0.1370-02 0.3470+00 0.3470+00	0.7000-03 0.1370-02 0.3470+00 0.3470+00	0.7690-03 0.1410-02 0.3470+00 0.3470+00	0.8640-03 0.1450-02 0.3470+00 0.3470+00	0.9230-03 0.1500-02 0.3470+00 0.3470+00	0.9900-03 0.1530-02 0.3470+00 0.3470+00	0.4600-06 0.1530-02 0.3470+00 0.3470+00	0.2600-06 0.1530-02 0.3470+00 0.3470+00	0.2600-06 0.1530-02 0.3470+00 0.3470+00
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MASS FRACTIONS, ENTHALPY, TEMP, P/A ENVY RATIO CELL LOADING, ENV TRG/M J-DI, CELL RES TIME

STA.	CH2 NU	LH3 NU2	LH4 NU	HL11 NU2U	LH20 U	CO UM	CO2 U2	H M (J/KG)	H2 T (K)	H2O TU RATIO	H2O2 KG/M3-DI	M NU2I (S)
1	0.0 0.0	0.0 0.0	1.000+00 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 -2.290+06	0.0 1.000+03	0.0 1.000+06	0.0 0.0	0.0 0.0
2	0.0 0.0	0.0 0.0	1.000+00 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 -2.290+06	0.0 1.000+03	0.0 1.000+06	0.0 0.0	0.0 0.0
3	0.0 0.0	0.0 0.0	1.000+00 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 -2.290+06	0.0 1.000+03	0.0 1.000+06	0.0 0.0	0.0 0.0
4	0.0 0.0	0.0 0.0	1.000+00 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 -2.290+06	0.0 1.000+03	0.0 1.000+06	0.0 0.0	0.0 0.0
5	0.0 0.0	0.0 0.0	1.000+00 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 -2.290+06	0.0 1.000+03	0.0 1.000+06	0.0 0.0	0.0 0.0
6	0.0 0.0	0.0 0.0	1.000+00 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 -2.290+06	0.0 1.000+03	0.0 1.000+06	0.0 0.0	0.0 0.0
7	0.0 0.0	0.0 0.0	1.000+00 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 -2.290+06	0.0 1.000+03	0.0 1.000+06	0.0 0.0	0.0 0.0
8	0.0 0.0	0.0 0.0	1.000+00 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 -2.290+06	0.0 1.000+03	0.0 1.000+06	0.0 0.0	0.0 0.0

9	0.0 0.0	0.0 0.0	1.000+00 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 -2.290+06	0.0 1.000+03	0.0 1.000+06	0.0 0.0	0.0 1.000+06
10	0.0 0.0	0.0 0.0	1.000+00 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 -2.290+06	0.0 1.000+03	0.0 1.000+06	0.0 0.0	0.0 1.000+06
11	0.0 0.0	0.0 0.0	1.000+00 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 -2.290+06	0.0 1.000+03	0.0 1.000+06	0.0 0.0	0.0 1.000+06
12	0.0 0.0	0.0 0.0	1.000+00 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 -2.290+06	0.0 1.000+03	0.0 1.000+06	0.0 0.0	0.0 1.000+06
13	0.0 0.0	0.0 0.0	1.000+00 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 -2.290+06	0.0 1.000+03	0.0 1.000+06	0.0 0.0	0.0 1.000+06
14	0.0 0.0	0.0 0.0	1.000+00 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 -2.290+06	0.0 1.000+03	0.0 1.000+06	0.0 0.0	0.0 1.000+06
15	0.0 0.0	0.0 0.0	1.000+00 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 -2.290+06	0.0 1.000+03	0.0 1.000+06	0.0 0.0	0.0 1.000+06
16	0.0 0.0	0.0 0.0	1.000+00 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 -2.290+06	0.0 1.000+03	0.0 1.000+06	0.0 0.0	0.0 1.000+06
17	0.0 0.0	0.0 0.0	1.000+00 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 -2.290+06	0.0 1.000+03	0.0 1.000+06	0.0 0.0	0.0 1.000+06
18	0.0 0.0	0.0 0.0	1.000+00 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 -2.290+06	0.0 1.000+03	0.0 1.000+06	0.0 0.0	0.0 1.000+06
19	0.0 0.0	0.0 0.0	1.000+00 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 -2.290+06	0.0 1.000+03	0.0 1.000+06	0.0 0.0	0.0 1.000+06
20	0.0 0.0	0.0 0.0	1.000+00 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 -2.290+06	0.0 1.000+03	0.0 1.000+06	0.0 0.0	0.0 1.000+06
21	0.0 0.0	0.0 0.0	0.870-01 2.400-01	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 7.290-02	0.0 -1.340+06	0.0 1.000+03	0.0 3.760+01	0.0 0.0	0.0 1.000+06
22	0.0 0.0	0.0 0.0	0.0 7.670-01	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 2.330-01	0.0 7.530+05	0.0 1.000+03	0.0 0.0	0.0 0.0	0.0 0.0

ISTEP= 2 IAX= 0 IEND= 0 IOUT= 0 IIN= 3 IEX= 2 IUX= 0.2920-06 PSIE= 0.0 PSIE= 0.7990-07
 KMI= 0.0 KME= -0.2740-02 PEI= 0.7990-07
 XU= 0.6490-06 UFLUX= -0.7130-08 PRESSU= 0.0 AEAR= 0.0 FLUXIJJ=
 -0.2690-42 -0.2690-42 0.4900-00 -0.2690-42 -0.2690-42 -0.2690-42 -0.2690-42 -0.2690-42 -0.2690-42 -0.2690-42
 -0.2690-42 -0.2690-42 -0.2690-42 -0.2690-42 -0.2150-06 -0.2690-42 -0.2690-42 -0.2690-42 -0.2690-42 -0.2690-42

9	0.0	0.1000-04	0.3550-03	0.5010-03	0.6140-03	0.7090-03	0.7430-03	0.8680-03	0.9280-03	0.1000-02	0.1000-02	0.1000-02	0.1000-02
10	0.1120-02	0.1180-02	0.1250-02	0.1280-02	0.1330-02	0.1370-02	0.1420-02	0.1460-02	0.1500-02	0.1540-02	0.1580-02	0.1620-02	0.1660-02
	0.3470+00	0.3470+00	0.3470+00	0.3470+00	0.3470+00	0.3470+00	0.3470+00	0.3470+00	0.3470+00	0.3470+00	0.3470+00	0.3470+00	0.3470+00
	0.3470+00	0.3470+00	0.3470+00	0.3470+00	0.3470+00	0.3470+00	0.3470+00	0.3470+00	0.3470+00	0.3470+00	0.3470+00	0.3470+00	0.3470+00

MASS FRACTIONS, ENTHALPY, TEMP, F/A EQUIV RATIO CELL LOADING, EMV (MG/M 3-3), CELL RES TIME

STA.	CH2 NU	CH3 NU2	CH4 NU2	H2O NU2	CH2O U	CO U	CO2 U2	H h (U/KL)	H2 T (K)	H2O EMV (MG/M3)	H2O MG/M3-2	H MG/M3
1	0.0 0.0	0.0 0.0	1.000+00 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 -2.290+06	0.0 1.000+03	0.0 1.000+06	0.0 0.0	0.0 0.0
2	0.0 0.0	0.0 0.0	1.000+00 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 -2.290+06	0.0 1.000+03	0.0 1.000+06	0.0 0.0	0.0 0.0

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C-2