SUMMARY

Results in the form of pressure and load distributions for a related group of simulated launch vehicle configurations are presented. The configurations were selected so that the nose-cone and interstage transition-flare components were relatively close to one another and subject to mutual interference effects. Tests extended over a Mach number range from 0.40 to 1.20 at angles of attack from 0° to about 10°. The test Reynolds numbers, based on main stage diameter, were of the order of 0.98×10^{6}.

INTRODUCTION

In the past, considerable experimental effort has been directed to the determination of aerodynamic force, moment, and loading characteristics for launch vehicle configurations. (See refs. 1 to 10.) This experimental effort was required, in part, because of the lack of suitable theoretical methods which could be used to predict vehicle aerodynamic characteristics with the required accuracy, particularly in the transonic speed range. Also, the available experimental results were applied in the development of empirical methods which could be used to make relatively rapid estimates of aerodynamic load distributions for some launch vehicle configurations. (See ref. 3, for example.) The empirical methods were limited in their application, however, to cone-cylinders or to configurations having no local flow separation. More recently, analytical methods have become available. (See ref. 11, for example.) The analytical approaches, however, are generally restricted to cases for attached flows.

As part of the experimental effort noted earlier, investigations have been conducted in the Langley 8-Foot Transonic Pressure Tunnel and the Langley Unitary Plan Wind Tunnel in order to determine the effects on force, moment, and loading characteristics of systematic variations in the geometry for simulated launch vehicles. Results for a number of configurations for which the nose-cone and stage transition-flare components were separated by a cylinder of relatively high fineness ratio are available in references 5 to 9.

The investigation was conducted in the Langley 8-Foot Transonic Pressure Tunnel in order to determine the effects of systematic variations in geometry on the load distributions of a number of configurations for which the nose-cone and stage transition-flare components were located relatively close to one another and were, therefore, subject to mutual interference effects which, in many cases, caused flow separation to occur. The tests extended over a Mach number range from 0.40 to 1.20 and angles of attack from 0° to about 10°. Test Reynolds numbers, based on the main stage diameter, were of the order of 0.98×10^{6}. Transonic force and moment results for a number of identical configurations are given in reference 10.

SYMBOLS

Values are given in both SI and U.S. Customary Units. Measurements for this investigation were taken in U.S. Customary Units. Details concerning the use of SI Units, together with physical constants and conversion factors, are given in reference 12.

c_n body section normal-force coefficient, $\int_0^1 (C_{p,l} - C_{p,u})\, d\left(\frac{y}{r}\right)$

C_p pressure coefficient, $\frac{p_\ell - p}{q}$

D local diameter, cm (in.)

D_{ref} main-stage diameter, 7.87 cm (3.10 in.)

l model reference length, 127 cm (50 in.)

M Mach number

p free-stream static pressure, Pa (lb/ft^2)

p_ℓ local static pressure, Pa (lb/ft^2)

q free-stream dynamic pressure, Pa (lb/ft^2)

$q_{M=1.20}$ free-stream dynamic pressure at $M = 1.20$, Pa (lb/ft^2)

R Reynolds number based on main-stage diameter

r local body radius, cm (in.)

x longitudinal distance, measured from reference station 0 ahead of body, cm (in.)

y lateral distance, measured from body center line, cm (in.)

α true angle of attack, deg

α_{nom} nominal angle of attack of model center line (does not include corrections for deflection of model and support system due to load), deg

δ_F transition-flare half-angle, deg

δ_N nose-cone half-angle, deg

ϕ orifice row meridian angle, measured clockwise from the vertical as viewed from front, deg

Subscripts:

l lower

u upper

APPARATUS AND TESTS

Tunnel

The investigation was conducted in the Langley 8-Foot Transonic Pressure Tunnel. This facility is a single-return, rectangular, slotted-throat tunnel with controls that allow for the independent variation of Mach number, density, temperature, and humidity. The tunnel is designed to obtain aerodynamic data for speeds up to and through the speed of sound while minimizing the usual effects of blockage.

Model

The model used for the investigation was the variable-geometry model described in reference 5. For this investigation, the upper-stage cylinder fineness ratio was held constant at 1.42 for most configurations, and nose cones having half-angles from 15.3° to 30.0° were each tested in combination with interstage transition flares having half-angles from 5.0° to 30.0°. In addition, for one set of nose-cone and transition-flare components, the upper-stage fineness ratio was varied from 1.42 to 0. To aid the reader, model configurations are designated by a three-digit number according to the following arrangement:

First digit - nose-cone half-angle:

1	15.3°
2	22.5°
3	30.0°

Second digit - upper-stage fineness ratio:

2	1.42
3	.96
4	.50
5	0

Third digit - stage transition-flare half-angles:

1	5.0°
2	10.1°
3	15.0°
4	30.0°

For example, configuration 321 has a nose-cone half-angle of 30.0°, an upper-stage fineness ratio of 1.42, and a stage transition-flare half-angle of 5.0°. Model configurations are also listed in table 1.

Model pressure orifices were installed along four longitudinal rows which were located at meridian angles (measured clockwise from the vertical as viewed from the front) of 0°, 30°, 60°, and 90°. All orifice locations, which are indicated nondimensionally in the tables of results, are referenced to model station 0 which was located 127 cm (50 in.) forward of the model base. (See fig. 1(b).)

Tests and Procedure

The investigation was conducted at a stagnation pressure maintained at approximately 101.5 kPa (2120 lb/ft^2). All configurations were tested at an angle of attack of 0° through a Mach number range from 0.40 to 1.20. Results were also obtained over an angle-of-attack range from -10° to 10° at Mach numbers of 0.60, 0.80, 1.00, and 1.20. Average test Reynolds numbers and dynamic pressures are given in figure 2.

The investigation was conducted with a transition strip located at the juncture of the nose cone and upper stage. The transition strip was 0.254 cm (0.1 in.) wide and was composed of No. 80 carborundum grains set in a plastic adhesive.

Model pressures were measured by the use of six scanning valve units. Differential pressure transducers were utilized, with ranges selected to provide nearly maximum gage outputs for the expected maximum pressure levels. No force or moment measurements were made during this investigation.

Boundary Interference Effects

At the time of the wind-tunnel investigation, the effects of subsonic boundary interference in the slotted test section were considered negligible. More recently, however, boundary-wall interference effects have been identified at Mach numbers close to 1.00. (See ref. 13.) These effects approach a maximum at a Mach number of 1.00; however, on the basis of the results of reference 13, they are confined to the rearward 50 percent of the bodies tested. For this investigation, therefore, the variations in loads over the regions of primary interest are judged to be valid at a Mach number of 1.00. At supersonic speeds,

the experimental results are generally affected by boundary-reflected disturbances which occur at Mach numbers from slightly over 1.00 to those at which disturbances are reflected downstream of the model base. For this investigation, the model lengths were such that no reflected disturbances affected the results at a Mach number of 1.20. Schlieren photographs, however, and an examination of the results indicate that a disturbance originating at the tunnel wall has a slight but noticeable effect on the pressure distributions at a Mach number of 1.20 at model stations between about $x/l = 0.82$ and $x/l = 0.86$. Because this effect is slight and occurs well to the rear of the model components which were varied, it is judged to be negligible in configuration comparisons.

CORRECTIONS AND ACCURACY

Angles of attack presented in this paper should be considered as nominal angles for this reason: although corrections have been made for tunnel airflow angularity, none have been applied for deflections of the model and support system under load. Estimates of the true angles of attack can be made, however, based upon the static loadings of reference 7 and the force and moment characteristics for the present configurations given in reference 10. The true angle of attack may be determined (to within $\pm 0.1^{\circ}$) from the empirical expression

$$\alpha = \alpha_{nom}\left(1 + 0.015\,\frac{q}{q_{M=1.20}}\right)$$

where the values of dynamic pressure are obtained from figure 2.

A consideration of factors affecting the results of this investigation has indicated that pressure coefficients are generally accurate within ±0.01. However, in model regions of extremely varying pressures (for example, in the region of the juncture of the nose cone and upper stage or for conditions in which pressures are noticeably sensitive to small Mach number changes, such accuracies may not be expected. (See fig. 3.) Local deviations from the quoted free-stream Mach numbers did not exceed ±0.015.

DISCUSSION OF RESULTS

Results of this investigation are presented as pressure coefficients (tables 2 to 15) and section normal-force coefficients (tables 16 to 26). Since the orifice rows extended only 90° radially about the model, section normal-force coefficients were obtained by combining pressure distribution results at identical positive and negative angles of attack. Representative data from the tables have been selected for graphical presentation (figs. 4 to 10) and are plotted to show the general effects of configuration variables on the pressure coefficients and on the section normal-force coefficients (multiplied by a diameter ratio to give load distributions).

Pressure Distributions

Effect of nose angle, $\alpha = 0^{\circ}$.- The effects of a variation in nose-cone angle on the longitudinal pressure distributions are presented in figure 4 for configurations having stage transition-flare angles ranging from 5.0° to 30.0°. For the lowest stage transition-flare angle ($\delta_F = 5^{\circ}$, fig. 4(a)), the effects of varying nose-cone angle are relatively slight; the most noticeable result is a broadening of the negative pressure-coefficient peaks just downstream of the juncture of the nose cone and upper stage at Mach numbers of 0.80 and 0.90 as nose-cone angle is increased. As noted in reference 5, the broadening of these peaks is associated with increases in separation as the nose-cone angle and associated adverse pressure gradient are increased.

As the stage transition-flare angle is increased to 30.0° (figs. 4(b) to 4(d)), the effects are greatly amplified because of the increased adverse pressure gradients resulting from the flare-angle increase. In the extreme case, a significant region of separated flow is evident for configuration 324 ($\delta_N = 30^{\circ}$, $\delta_F = 30^{\circ}$) at a Mach number of 0.90 just downstream of the nose-cone juncture. (See fig. 4(d).) Separation is also evident just downstream of the juncture of the transition flare and main stage at a Mach number of 0.90. This separation is indicated by the broadening of the associated peaks for all transition-flare angles and for nose-cone half-angles of 15.0° and 22.5°. (See figs. 4(b) to 4(d).) The configurations which exhibit the greatest degree of separation downstream of the juncture of the nose cone and upper stage appear to have the least amount of separation downstream of the juncture of the stage transition flare and the main stage. (See fig. 4(d) where M = 0.90, for example.) This characteristic results from the fact that for low nose-cone angles, the flow apparently remains attached over the upper-stage surface. Therefore, the full effect of the transition-flare compression and overexpansion is felt, and an adverse pressure gradient severe enough to separate the flow downstream of the juncture of the transition flare and the main stage results. For the higher nose-cone angles, separation over the upper stage tends to mask the effect of the transition flare, so that from an aerodynamic standpoint, the flow acts as if it were approaching a transition flare of a significantly lower angle and probably reattaches at the corner between the transition flare and the main stage.

Effects of angle of attack.- The effects of a variation in angle of attack from -6° to 6° on the pressure coefficients in the top row ($\phi = 0^{\circ}$) are presented in figures 5 to 8. For a transition-flare angle of 5°, pressure distributions at angles of attack from -6° to 6° are very similar to those at 0° and show little variation in characteristics as Mach number is varied (figs. 5(a) to 8(a)). As the transition-flare angle is increased to 10.1°, however, a noticeable broadening of the pressure-coefficient peak for the nose cone and upper stage occurs. This broadening, indicative of separation, appears as the angle of attack is increased to 3° and 6° (figs. 7(b) and 8(b)).

Generally, increases in stage transition-flare angle to 15.0° and 30.0° result in an earlier onset of the noted separation effects with regard to both angle of attack and Mach number. For the higher flare angles, separation on the main stage becomes apparent at the higher Mach numbers. (See figs. 7(c) and 8(c), for example, at Mach numbers of 1.00 and 1.20.)

Loading Distributions

The effects of variations in nose-cone angle on the load distributions for angles of attack of 3° and 6° are presented in figures 9 and 10, respectively. As expected, the nose-cone and transition-flare components carry the greater portion of the loading. For configurations which experience a significant degree of separation (see, for example, configuration 324 at a Mach number of 0.80, fig. 10(d)), a notable portion of the load is carried by the upper stage.

SUMMARY OF RESULTS

Results of this investigation are presented as pressure coefficients and section normal-force coefficients. At low stage transition-flare angles, effects of varying nose-cone angle are slight. As stage transition-flare angle is increased, significant regions of flow separation occur. These regions are associated with increased adverse pressure gradients. Generally, increases in stage transition-flare angle to 30.0° result in an earlier onset of the noted separation effects with regard to both angle of attack and Mach number.

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February 4, 1980

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TABLE 1.- MODEL CONFIGURATIONS

Configuration	Nose-cone half-angle, deg	Upper-stage fineness ratio	Transition-flare half-angle, deg
121	15.3	1.42	5.0
221	22.5	↓	↓
321	30.0	↓	↓
122	15.3	↓	10.1
222	22.5	↓	↓
322	30.0	↓	↓
123	15.3	↓	15.0
223	22.5	↓	↓
323	30.0	↓	↓
124	15.3	↓	30.0
324	30.0	↓	30.0
133	15.3	.96	15.0
143	↓	.50	↓
153	↓	0	↓

TABLE 2.- PRESSURE COEFFICIENTS FOR CONFIGURATION 121

(a) M = 0.40 to 0.95; $\alpha = 0^\circ$

	x/l	C_p for - $\phi = 0^\circ$					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.328	.251	.282	.289	.312	.329	.356
	.338	.229	.251	.257	.281	.300	.328
	.348	.196	.220	.225	.250	.271	.301
	.358	.163	.176	.180	.208	.231	.267
	.378	.065	.075	.080	.115	.147	.192
	.388	-.045	-.037	-.026	.031	.078	.131
	.393	-.169	-.179	-.156	-.057	.006	.072
Upper stage	.399	-.857	-1.273	-1.287	-.968	-.830	-.697
	.404	-.224	-.301	-.408	-.992	-.916	-.798
	.409	-.123	-.155	-.192	-.396	-.809	-.709
	.419	-.045	-.055	-.059	-.103	-.198	-.553
	.429	.000	-.010	-.014	.018	.007	-.416
	.439	.022	.027	.024	.043	.088	-.012
	.449	.067	.072	.070	.083	.121	.135
Transition flare	.459	.179	.191	.190	.200	.225	.243
	.482	.055	.058	.056	.060	.076	.133
	.492	.033	.035	.032	.036	.043	.092
	.512	.033	.026	.015	.018	.023	.054
	.532	.011	-.005	-.009	-.017	-.010	.020
	.552	-.045	-.056	-.064	-.079	-.078	-.037
	.562	-.079	-.106	-.118	-.144	-.156	-.111
Main stage	.568	-.169	-.220	-.234	-.304	-.448	-.417
	.577	-.068	-.092	-.101	-.125	-.131	-.357
	.587	-.045	-.056	-.064	-.078	-.077	-.283
	.597	-.034	-.037	-.047	-.057	-.057	-.117
	.607	-.023	-.028	-.034	-.046	-.044	-.021
	.617	-.023	-.024	-.030	-.046	-.037	-.012
	.627	-.023	-.019	-.026	-.032	-.034	-.009
	.637	.000	-.010	-.018	-.028	-.023	-.009
	.657	.000	.004	-.008	-.022	-.016	-.010
	.677	.000	.005	-.008	-.017	-.013	-.013
	.697	.004	.009	-.005	-.011	-.011	-.012
	.737	.004	.010	-.004	-.009	-.010	-.013
	.777	.008	.013	.000	-.005	-.005	-.010
	.785	.011	.016	.005	-.002	-.002	-.005
	.817	.009	.008	.004	-.003	-.003	-.005
	.857	.006	.005	.000	-.006	-.006	-.009
	.877	.006	.005	.001	-.006	-.006	-.008
	.897	.004	.002	-.003	-.009	-.009	-.012

	x/l	C_p for - $\phi = -30^\circ$					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.338	.229	.242	.249	.267	.290	.319
	.348	.185	.203	.213	.236	.257	.288
	.358	.152	.172	.180	.205	.228	.260
	.378	.065	.070	.085	.108	.140	.186
	.388	-.045	-.042	-.030	.028	.075	.131
	.393	-.180	-.179	-.151	-.057	.006	.072
Upper stage	.399	-.823	-1.204	-1.433	-1.115	-.969	-.825
	.404	-.224	-.315	-.412	-1.013	-.916	-.795
	.409	-.112	-.146	-.188	-.389	-.832	-.731
	.419	-.045	-.055	-.059	-.096	-.191	-.547
	.429	.000	-.010	-.009	.018	.017	-.413
	.439	.022	.027	.024	.043	.088	-.002
	.449	.078	.081	.078	.090	.128	.138
Transition flare	.459	.191	.200	.194	.208	.232	.243
	.482	.055	.062	.060	.060	.076	.133
	.492	.033	.035	.032	.036	.043	.092
	.512	.033	.013	.015	.007	.013	.048
	.532	.000	-.010	-.014	-.021	-.017	.013
	.552	-.045	-.056	-.064	-.079	-.078	-.037
	.562	-.091	-.134	-.144	-.176	-.193	-.137
Main stage	.568	-.158	-.197	-.218	-.279	-.421	-.395
	.577	-.068	-.092	-.101	-.125	-.131	-.357
	.587	-.045	-.056	-.064	-.082	-.084	-.290
	.597	-.034	-.028	-.039	-.046	-.044	-.088
	.607	-.023	-.028	-.034	-.046	-.044	-.021
	.617	-.023	-.024	-.030	-.046	-.037	-.009
	.627	-.011	-.019	-.026	-.032	-.034	-.012
	.637	.000	-.010	-.018	-.028	-.027	-.012
	.657	-.004	.002	-.011	-.021	-.020	-.012
	.677	.004	.012	-.002	-.009	-.009	-.009
	.697	.000	.009	-.007	-.011	-.012	-.013
	.737	.004	.012	-.001	-.008	-.008	-.011
	.777	.011	.016	.005	-.002	-.002	-.005
	.785	.011	.016	.005	-.002	-.001	-.005
	.817	.009	.008	.003	-.003	-.003	-.005
	.857	.006	.004	.000	-.007	-.007	-.010
	.877	.004	.003	-.002	-.008	-.008	-.011
	.897	.003	.001	-.003	-.009	-.009	-.013
	.917	.003	.001	-.003	-.009	-.010	-.013
	.957	-.006	-.010	-.014	-.021	-.021	-.024
	.997	-.058	-.064	-.070	-.077	-.080	-.094

TABLE 2.- PRESSURE COEFFICIENTS FOR CONFIGURATION 121 - Continued

(a) M = 0.40 to 0.95; $\alpha = 0^\circ$ - Concluded

	x/l	C_p for - $\phi = -60^\circ$					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.338	.229	.242	.245	.267	.287	.319
	.348	.185	.203	.209	.232	.254	.285
	.358	.152	.163	.168	.198	.218	.254
	.378	.044	.057	.067	.101	.134	.180
	.388	-.056	-.051	-.039	.021	.065	.121
	.393	-.056	-.069	-.072	-.075	-.077	-.089
Upper stage	.399	-.778	-1.127	-1.237	-.965	-.837	-.710
	.404	-.224	-.319	-.425	-1.020	-.947	-.824
	.409	-.101	-.133	-.184	-.406	-.816	-.718
	.419	-.045	-.055	-.059	-.078	-.185	-.566
	.429	.000	-.010	-.014	.018	.034	-.419
	.439	.034	.031	.028	.043	.091	.004
	.449	.078	.077	.070	.083	.121	.144
Transition flare	.459	.179	.186	.186	.197	.225	.246
	.482	.055	.058	.052	.057	.073	.130
	.492	.033	.035	.032	.036	.043	.097
	.512	.033	.013	.015	.007	.013	.048
	.532	.000	-.010	-.014	-.021	-.017	.013
	.552	-.045	-.065	-.072	-.090	-.085	-.044
	.562	-.102	-.134	-.148	-.176	-.193	-.137
Main stage	.568	-.158	-.192	-.214	-.268	-.397	-.369
	.577	-.068	-.092	-.101	-.125	-.128	-.360
	.587	-.045	-.060	-.068	-.082	-.084	-.299
	.597	-.034	-.037	-.043	-.057	-.057	-.117
	.607	-.023	-.028	-.034	-.046	-.044	-.021
	.617	-.023	-.024	-.030	-.046	-.037	-.012
	.627	.000	-.019	-.022	-.032	-.034	-.012
	.637	.000	-.014	-.018	-.028	-.027	-.012
	.657	-.004	.001	-.009	-.020	-.018	-.012
	.677	.000	.005	-.007	-.014	-.014	-.011
	.697	.004	.010	-.004	-.009	-.010	-.010
	.737	.004	.012	-.001	-.007	-.008	-.011
	.777	.008	.015	.002	-.003	-.002	-.004
	.785	.008	.016	.005	-.004	-.003	-.007
	.817	.009	.009	.004	-.002	-.002	-.004
	.857	.006	.005	.000	-.007	-.007	-.010
	.877	.004	.004	-.001	-.008	-.007	-.011
	.897	.004	.002	-.003	-.008	-.009	-.011
	.917	.001	-.003	-.006	-.013	-.013	-.016
	.957	-.009	-.010	-.014	-.020	-.021	-.023
	.997	-.059	-.066	-.070	-.079	-.083	-.095

	x/l	C_p for - $\phi = -90^\circ$					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.328	.261	.287	.293	.316	.336	.362
	.338	.207	.225	.23	.255	.277	.307
	.358	.152	.163	.168	.194	.218	.251
	.378	.054	.057	.063	.101	.134	.180
	.393	-.203	-.207	-.185	-.082	-.023	.047
Upper stage	.399	-.755	-1.062	-1.007	-.904	-.776	-.655
	.419	-.045	-.051	-.051	-.039	-.158	-.559
	.439	.022	.027	.024	.036	.088	.014
Transition flare	.459	.191	.200	.194	.211	.235	.256
	.482	.055	.058	.052	.057	.073	.130
	.512	.022	.013	.011	.007	.013	.048
	.552	-.045	-.060	-.068	-.082	-.081	-.041
Main stage	.568	-.180	-.247	-.264	-.340	-.522	-.475
	.587	-.045	-.060	-.068	-.085	-.084	-.299
	.607	-.023	-.028	-.034	-.046	-.044	-.021
	.627	.000	-.019	-.022	-.032	-.034	-.012
	.657	-.004	.002	-.011	-.021	-.018	-.012
	.697	.000	.007	-.005	-.013	-.012	-.013
	.737	.004	.012	-.001	-.007	-.008	-.011
	.777	.008	.013	.002	-.004	-.004	-.006
	.785	.008	.015	.007	-.002	-.002	-.005
	.817	.010	.010	.005	-.001	-.001	-.002
	.857	.006	.005	.000	-.007	-.006	-.010
	.897	.003	.002	-.003	-.009	-.009	-.012

TABLE 2.- PRESSURE COEFFICIENTS FOR CONFIGURATION 121 - Continued

(b) $M = 0.60$; $\alpha = -10^\circ$ to 10°

		C_p for - $\phi = 0^\circ$						
	x/l	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.328	.438	.367	.305	.27	.205	.177	.119
	.338	.405	.334	.278	.[illegible]	.178	.144	.085
	.348	.372	.301	.250	.197	.150	.110	.052
	.358	.333	.262	.212	.158	.106	.066	.019
	.378	.228	.162	.106	.053	.006	-.029	-.083
	.388	.112	.041	-.004	-.054	-.108	-.138	-.181
	.393	-.021	-.095	-.153	-.203	-.239	-.275	-.312
Upper stage	.399	-.851	-.943	-1.001	-1.039	-1.064	-1.077	-1.086
	.404	-.181	-.220	-.249	-.276	-.278	-.291	-.294
	.409	-.078	-.112	-.124	-.151	-.147	-.154	-.151
	.419	-.010	-.032	-.044	-.059	-.056	-.057	-.054
	.429	.024	.002	-.004	-.020	-.010	-.012	-.015
	.439	.059	.042	.030	.015	.024	.023	.020
	.449	.104	.082	.076	.055	.070	.063	.054
	.459	.258	.230	.207	.169	.166	.148	.134
Transition flare	.482	.125	.092	.069	.043	.024	.017	.014
	.492	.103	.070	.041	.020	.007	.000	-.009
	.512	.080	.041	.030	.014	.001	-.012	-.032
	.532	.058	.025	.001	-.020	-.033	-.040	-.055
	.552	.013	-.015	-.045	-.066	-.079	-.081	-.084
	.562	-.062	-.084	-.096	-.112	-.114	-.115	-.118
Main stage	.568	-.118	-.164	-.193	-.208	-.210	-.183	-.180
	.577	-.044	-.061	-.079	-.088	-.102	-.092	-.09[illegible]
	.587	-.021	-.032	-.050	-.060	-.073	-.063	-.0[illegible]
	.597	-.010	-.021	-.033	-.048	-.056	-.046	-.03[illegible]
	.607	.001	-.015	-.027	-.037	-.045	-.034	-.02[illegible]
	.617	.001	-.009	-.021	-.031	-.039	-.029	-.026
	.627	.007	-.004	-.016	-.025	-.033	-.023	-.020
	.637	.017	.002	-.004	-.020	-.027	-.012	-.009
	.657	.021	.006	-.004	-.008	-.014	-.008	-.005
	.677	.025	.006	-.004	-.006	-.020	-.006	-.00[illegible]
	.697	.025	.008	.005	-.002	-.008	-.002	-.003
	.737	.027	.010	.000	-.004	-.006	-.002	-.005
	.777	.030	.014	.007	-.002	-.006	.002	-.003
	.785	.036	.017	.005	-.001	-.005	.008	.010
	.817	.036	.021	.010	.002	-.002	.004	.004
	.857	.029	.014	.005	-.001	-.004	-.001	-.004
	.877	.032	.016	.006	-.001	-.005	-.001	-.004
	.897	.026	.011	.002	-.004	-.008	-.004	-.009

		C_p for - $\phi = -30^\circ$						
	x/l	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.338	.377	.317	.272	.224	.178	.138	.089
	.348	.328	.284	.239	.191	.139	.105	.030
	.358	.294	.245	.206	.158	.106	.066	-.003
	.378	.189	.140	.095	.047	.006	-.040	-.100
	.388	.079	.030	-.016	-.060	-.102	-.143	-.198
	.393	-.056	-.113	-.159	-.203	-.239	-.281	-.330
Upper stage	.399	-.840	-.914	-.961	-.993	-1.035	-1.002	-.994
	.404	-.209	-.237	-.261	-.282	-.272	-.274	-.294
	.409	-.095	-.112	-.124	-.145	-.130	-.143	-.151
	.419	-.033	-.044	-.050	-.059	-.056	-.063	-.071
	.429	.002	-.004	-.010	-.020	-.010	-.012	-.026
	.439	.030	.025	.024	.015	.024	.017	.003
	.449	.087	.082	.076	.066	.075	.063	.048
Transition flare	.459	.246	.224	.207	.180	.178	.159	.122
	.482	.097	.092	.069	.048	.029	.022	.008
	.492	.080	.064	.041	.020	.007	.000	-.020
	.512	.069	.047	.024	.003	-.010	-.017	-.038
	.532	.035	.013	.001	-.020	-.039	-.046	-.066
	.552	-.010	-.021	-.045	-.066	-.079	-.086	-.107
	.562	-.096	-.113	-.125	-.140	-.143	-.150	-.153
Main stage	.568	-.147	-.164	-.187	-.191	-.193	-.183	-.175
	.577	-.061	-.078	-.079	-.088	-.102	-.092	-.095
	.587	-.038	-.049	-.056	-.060	-.073	-.069	-.066
	.597	-.027	-.027	-.033	-.042	-.045	-.046	-.043
	.607	-.021	-.021	-.027	-.037	-.045	-.040	-.043
	.617	-.010	-.015	-.021	-.031	-.039	-.029	-.037
	.627	-.010	-.015	-.016	-.025	-.033	-.029	-.032
	.637	-.010	-.004	-.016	-.020	-.027	-.023	-.032
	.657	.002	-.004	-.004	-.008	-.014	-.013	-.028
	.677	.009	.006	.000	-.002	-.012	-.008	-.024
	.697	.007	.002	-.004	-.002	-.012	-.010	-.024
	.737	.006	.002	.000	-.002	-.010	-.008	-.030
	.777	.011	.008	.003	-.00[illegible]	-.006	-.006	-.028
	.785	.007	.006	.003	-.00[illegible]	-.006	-.006	-.022
	.817	.009	.008	.006	.002	-.003	-.006	-.025
	.857	.004	.004	.001	-.003	-.006	-.009	-.028
	.8[illegible]	.003	.004	.000	-.003	-.007	-.010	-.029
	.897	.002	.002	-.001	-.004	-.009	-.013	-.029
	.917	-.002	.000	-.003	-.005	-.012	-.016	-.031
	.937	-.017	-.011	-.012	-.016	-.022	-.028	-.042
	.[illegible]	-.095	-.075	-.064	-.068	-.079	-.091	-.118

TABLE 2.- PRESSURE COEFFICIENTS FOR CONFIGURATION 121 - Continued

(b) M = 0.60; α = -10° to 10° - Concluded

	x/l	C_p for - ϕ = -60°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.338	.250	.262	.250	.219	.189	.149	.069
	.348	.222	.223	.217	.180	.150	.110	.036
	.358	.184	.190	.173	.141	.112	.072	-.003
	.378	.084	.090	.068	.042	.012	-.029	-.100
	.388	-.021	-.021	-.044	-.071	-.102	-.138	-.198
	.393	-.124	-.095	-.079	-.077	-.085	-.103	-.135
	.399	-.817	-.834	-.881	-.947	-1.007	-1.025	-1.045
Upper stage	.404	-.283	-.271	-.266	-.276	-.272	-.302	-.345
	.409	-.158	-.129	-.124	-.128	-.124	-.143	-.185
	.419	-.101	-.072	-.061	-.065	-.056	-.074	-.123
	.429	-.061	-.032	-.016	-.020	-.010	-.034	-.083
	.439	-.027	.008	.024	.015	.024	.006	-.043
	.449	.019	.053	.064	.055	.064	.046	.003
Transition flare	.459	.150	.179	.184	.169	.172	.148	.094
	.482	.013	.041	.052	.043	.024	.006	-.038
	.492	-.004	.025	.030	.020	.007	-.012	-.055
	.512	-.016	.019	.024	.003	-.010	-.023	-.072
	.532	-.039	-.015	-.010	-.020	-.039	-.058	-.095
	.552	-.096	-.067	-.068	-.071	-.085	-.104	-.141
	.562	-.159	-.136	-.131	-.140	-.148	-.161	-.193
Main stage	.568	-.233	-.192	-.187	-.185	-.193	-.200	-.237
	.577	-.136	-.095	-.084	-.088	-.102	-.114	-.135
	.587	-.107	-.072	-.061	-.065	-.073	-.080	-.112
	.597	-.090	-.055	-.044	-.042	-.056	-.069	-.089
	.607	-.084	-.049	-.033	-.037	-.045	-.052	-.077
	.617	-.078	-.044	-.027	-.031	-.039	-.052	-.072
	.627	-.073	-.032	-.016	-.025	-.033	-.046	-.056
	.637	-.067	-.027	-.016	-.020	-.027	-.040	-.060
	.657	-.054	-.021	-.012	-.006	-.018	-.025	-.053
	.677	-.047	-.017	-.008	-.005	-.017	-.024	-.049
	.697	-.040	-.013	-.004	-.004	-.016	-.023	-.045
	.737	-.052	-.019	-.006	-.002	-.014	-.019	-.034
	.777	-.052	-.013	.000	-.001	-.010	-.013	-.032
	.785	-.054	-.017	-.004	-.001	-.008	-.013	-.030
	.817	-.047	-.009	.002	.002	-.004	-.010	-.027
	.857	-.053	-.016	-.003	-.003	-.009	-.014	-.029
	.877	-.052	-.016	-.004	-.003	-.009	-.013	-.029
	.897	-.053	-.019	-.005	-.004	-.010	-.016	-.031
	.917	-.062	-.023	-.010	-.007	-.015	-.020	-.035
	.957	-.066	-.031	-.017	-.016	-.023	-.030	-.044
	.997	-.132	-.095	-.076	-.070	-.082	-.097	-.124

	x/l	C_p for - ϕ = -90°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.328	.167	.240	.267	.268	.261	.238	.168
	.358	.068	.124	.145	.141	.134	.116	.047
	.378	-.021	.030	.046	.042	.029	.011	-.049
	.393	-.290	-.244	-.228	-.226	-.239	-.252	-.301
	.399	-.834	-.834	-.881	-.902	-.909	-.939	-.977
Upper stage	.419	-.141	-.083	-.061	-.059	-.056	-.080	-.146
	.439	-.078	-.015	.013	.015	.018	-.012	-.077
Transition flare	.459	.098	.150	.178	.174	.183	.154	.088
	.482	-.050	.013	.035	.037	.029	.006	-.043
Main stage	.512	-.085	-.021	.001	.003	-.010	-.023	-.078
	.552	-.142	-.084	-.068	-.071	-.079	-.098	-.141
	.568	-.330	-.261	-.233	-.231	-.256	-.274	-.335
	.587	-.141	-.089	-.061	-.065	-.079	-.097	-.146
	.607	-.118	-.055	-.033	-.037	-.045	-.069	-.112
	.627	-.101	-.044	-.021	-.025	-.039	-.052	-.106
	.657	-.094	-.036	-.012	-.006	-.020	-.038	-.091
	.697	-.088	-.034	-.012	-.004	-.020	-.036	-.089
	.737	-.082	-.030	-.006	-.002	-.014	-.031	-.083
	.777	-.079	-.027	-.004	-.001	-.0.2	-.027	-.076
	.785	-.082	-.028	-.004	-.001	-.014	-.025	-.076
	.817	-.071	-.016	-.001	.003	-.005	-.020	-.069
	.857	-.074	-.023	-.005	-.002	-.010	-.027	-.073
	.897	-.075	-.027	-.009	-.004	-.012	-.030	-.076

TABLE [illegible].- PRESSURE COEFFICIENTS FOR CONFIGURATION [illegible] - Continued

(c) $M = [illegible]$; $\alpha = -10°$ to $10°$

Region	x/l	C_p for - $\phi = 0°$, $\alpha = -10°$	$\alpha = -6°$	$\alpha = -3°$	$\alpha = 0°$	$\alpha = 3°$	$\alpha = 6°$	$\alpha = 10°$
Nose	.328	.460	.394	.349	.303	.252	.200	.152
	.338	.447	.364	.316	.270	.219	.172	.119
	.348	.417	.334	.282	.237	.185	.139	.085
	.358	.373	.293	.245	.196	.144	.098	.044
	.378	.269	.193	.141	.095	.048	.001	-.046
	.388	.161	.089	.040	-.002	-.043	-.087	-.135
	.393	.042	-.023	-.067	-.105	-.147	-.183	-.227
	.399	-1.058	-1.066	-1.105	-1.127	-1.140	-1.154	-1.140
Upper stage	.404	-.328	-.467	-.506	-.518	-.525	-.519	-.483
	.409	-.106	-.176	-.226	-.289	-.338	-.370	-.365
	.419	[illegible]	-.042	-.050	-.055	-.073	-.106	-.134
	.429	.020	-.004	-.004	-.001	-.001	-.002	-.012
	.439	.059	.034	.030	.033	.030	.032	.038
	.449	.112	.084	.080	.075	.072	.067	.065
Transition flare	.459	.284	.245	.227	.194	.164	.140	.119
	.482	.152	.098	.075	.055	.045	.024	.015
	.492	.122	.068	.049	.033	.027	.002	-.012
	.512	.098	.045	.034	.010	[illegible]	-.010	-.047
	.532	.077	.022	.000	-.017	-.028	-.049	-.066
	.552	.024	-.031	-.054	-.075	-.086	-.103	-.109
	.562	-.065	-.108	-.124	-.129	-.126	-.134	-.136
Main stage	.568	-.187	-.254	-.262	-.259	-.243	-.221	-.200
	.577	-.060	-.096	-.104	-.109	-.108	-.106	-.104
	.587	-.045	-.058	-.066	-.067	-.070	-.071	-.066
	.597	[illegible]	-.042	-.044	-.048	[illegible]	-.048	-.046
	.607	[illegible]	-.031	-.035	-.036	-.039	-.041	-.035
	.617	[illegible]	-.027	-.031	-.037	-.031	-.033	-.027
	.627	[illegible]	-.019	-.023	-.024	-.027	-.025	-.023
	.637	[illegible]	[illegible]	-.016	-.017	-.020	-.018	-.016
	.657	.024	-.004	-.008	-.009	[illegible]	[illegible]	-.017
	.677	.026	-.003	-.008	-.007	-.010	-.010	-.012
	.697	.028	.000	-.005	-.005	-.008	-.007	-.009
	.737	.028	[illegible]	-.006	-.004	-.006	-.006	-.009
	.777	.037	.006	[illegible]	[illegible]	-.007	-.003	-.008
	.785	.038	[illegible]	.002	.001	[illegible]	.002	.006
	.817	.039	.002	.006	.002	.003	-.003	[illegible]
	.857	.032	.005	.000	[illegible]	[illegible]	-.008	-.009
	.877	.034	.007	[illegible]	[illegible]	[illegible]	-.007	-.007
	.897	.029	.002	-.003	-.004	-.004	-.011	-.013

Region	x/l	C_p for - $\phi = -90°$, $\alpha = -10°$	$\alpha = -6°$	$\alpha = -3°$	$\alpha = 0°$	$\alpha = 3°$	$\alpha = 6°$	$\alpha = 10°$
Nose	.338	.410	.345	.304	.259	.215	.165	.104
	.348	.369	.312	.271	.222	.182	.128	[illegible]
	.358	.336	.278	.234	.192	.144	.091	.029
	.378	.231	.174	.130	.088	.048	-.002	-.058
	.388	.131	.074	.033	-.002	-.043	-.091	-.143
	.393	.016	-.035	-.070	-.105	-.143	-.183	-.235
	.399	-1.220	-1.248	-1.267	-1.280	-1.302	-1.308	-1.306
Upper stage	.404	-.367	-.483	-.506	-.522	-.529	-.523	-.491
	.409	-.133	-.184	-.230	-.281	-.311	-.335	-.353
	.419	-.045	-.054	-.050	-.051	-.062	-.083	-.134
	.429	-.003	-.012	-.008	-.001	-.001	-.006	-.019
	.439	.032	.023	.027	.029	.030	.029	.023
	.449	.097	.084	.084	.083	.080	.071	.057
Transition flare	.459	.273	.245	.226	.206	.183	.155	.126
	.482	.122	.087	.071	.059	.049	.024	.007
	.492	.099	.064	.049	.033	.022	-.002	-.023
	.512	.077	.038	.022	.010	-.001	-.029	-.051
	.532	.050	.011	-.004	-.021	-.031	-.056	-.081
	.552	-.003	-.043	-.054	-.075	-.086	-.110	-.128
	.562	-.103	-.147	-.155	-.160	-.163	-.176	-.182
Main stage	.568	-.210	-.246	-.246	-.236	-.223	-.221	-.200
	.577	-.091	-.108	-.108	-.109	-.112	-.114	-.116
	.587	-.060	-.069	-.073	-.074	-.077	-.079	-.081
	.597	-.030	-.042	-.039	-.036	-.039	-.041	-.046
	.607	-.030	-.042	-.039	-.036	-.039	-.044	-.045
	.617	-.022	-.031	-.031	-.032	-.031	-.037	-.039
	.627	-.018	-.031	-.027	-.024	-.027	-.029	-.039
	.637	-.014	-.023	-.020	-.021	-.024	-.025	-.035
	.657	-.003	-.018	-.017	-.012	-.012	-.019	-.030
	.677	.008	-.004	-.007	-.003	-.007	-.012	-.027
	.697	.001	-.009	-.009	-.005	-.008	-.014	-.031
	.737	.004	-.008	-.005	-.003	-.007	-.011	-.032
	.777	.014	.000	.000	.003	-.002	-.009	-.028
	.785	.008	-.003	.000	.003	-.001	-.007	-.022
	.817	.012	.001	.002	.002	.002	-.011	-.025
	.857	.005	-.005	-.004	-.002	-.002	-.014	-.029
	.877	.004	-.006	-.004	-.003	-.003	-.015	-.030
	.897	.001	-.008	-.006	-.004	-.005	-.018	-.031
	.917	.001	-.008	-.007	-.005	-.006	-.020	-.033
	.957	-.011	-.020	-.016	[illegible]	-.019	-.034	-.045
	.997	-.093	-.086	-.072	-.071	-.079	-.100	-.124

TABLE 2.- PRESSURE COEFFICIENTS FOR CONFIGURATION 121 - Continued

(c) $M = 0.80$; $\alpha = -10^\circ$ to 10° - Concluded

		C_p for - $\beta = -60^\circ$						
	x/l	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.338	.295	.293	.278	.259	.226	.180	.104
	.348	.261	.256	.241	.222	.185	.143	.067
	.358	.224	.219	.204	.181	.152	.106	.033
	.378	.127	.122	.107	.084	.055	.009	-.054
	.388	.027	.022	.014	-.013	-.039	-.083	-.147
	.393	-.122	-.096	-.077	-.071	-.078	-.102	-.131
Upper stage	.399	-1.081	-1.082	-1.098	-1.118	-1.152	-1.192	-1.167
	.404	-.470	-.521	-.521	-.557	-.552	-.550	-.571
	.409	-.221	-.257	-.280	-.285	-.292	-.377	-.418
	.419	-.114	-.077	-.058	-.047	-.054	-.094	-.131
	.429	-.064	-.031	-.012	-.005	-.008	-.021	-.069
	.439	-.022	.007	.027	.033	.026	.009	-.027
Transition flare	.459	.028	.053	.072	.079	.068	.048	.015
	.459	.173	.199	.203	.190	.176	.147	.111
	.482	.035	.049	.056	.052	.049	.013	-.035
	.492	.012	.026	.034	.033	.022	-.006	-.054
	.512	-.003	.003	.011	.006	-.001	-.037	-.081
	.532	-.030	-.023	-.016	-.021	-.031	-.056	-.109
	.552	-.092	-.089	-.082	-.083	-.090	-.122	-.167
	.562	-.173	-.170	-.163	-.160	-.163	-.196	-.232
Main stage	.568	-.791	-.265	-.242	-.228	-.231	-.248	-.277
	.577	-.153	-.127	-.112	-.105	-.112	-.129	-.154
	.587	-.122	-.100	-.081	-.074	-.081	-.094	-.123
	.597	-.103	-.073	-.058	-.059	-.058	-.071	-.100
	.607	-.091	-.062	-.043	-.036	-.043	-.060	-.085
	.617	-.084	-.058	-.039	-.032	-.035	-.056	-.077
	.627	-.080	-.054	-.031	-.024	-.031	-.044	-.069
	.637	-.076	-.046	-.027	-.021	-.027	-.041	-.062
	.657	-.064	-.037	-.020	-.012	-.019	-.033	-.053
	.677	-.052	-.030	-.016	-.008	-.015	-.029	-.048
	.697	-.040	-.022	-.013	-.004	-.012	-.025	-.043
	.737	-.053	-.030	-.013	-.001	-.010	-.021	-.036
	.777	-.048	-.022	-.005	.001	-.006	-.018	-.031
	.785	-.055	-.027	-.004	.003	-.004	-.015	-.025
	.817	-.045	-.019	-.003	.003	-.001	-.015	-.027
	.857	-.052	-.025	-.008	-.002	-.004	-.018	-.030
	.877	-.051	-.026	-.009	-.003	-.005	-.018	-.030
	.897	-.052	-.026	-.009	-.003	-.006	-.020	-.032
	.917	-.059	-.036	-.016	-.008	-.011	-.025	-.035
	.957	-.065	-.039	-.021	-.016	-.020	-.035	-.046
	.997	-.134	-.106	-.084	-.073	-.080	-.104	-.129

		C_p for - $\beta = -30^\circ$						
	x/l	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.328	.213	.271	.293	.307	.297	.273	.212
	.358	.105	.152	.171	.181	.170	.143	.093
	.378	.016	.063	.078	.084	.074	.053	-.008
	.393	-.211	-.162	-.143	-.136	-.143	-.168	-.216
Upper stage	.399	-1.069	-1.055	-1.044	-1.037	-1.056	-1.073	-1.109
	.419	-.145	-.088	-.062	-.044	-.054	-.094	-.157
	.439	-.072	-.012	.019	.029	.019	-.006	-.077
Transition flare	.459	.124	.172	.187	.198	.195	.166	.107
	.482	-.034	.019	.045	.052	.049	.013	-.035
	.512	-.080	-.031	-.004	.006	.003	-.029	-.081
Main stage	.552	-.146	-.108	-.085	-.079	-.082	-.114	-.167
	.568	-.418	-.346	-.300	-.286	-.308	-.352	-.419
	.587	-.157	-.112	-.085	-.074	-.085	-.110	-.162
	.607	-.122	-.073	-.046	-.036	-.047	-.071	-.127
	.627	-.107	-.062	-.035	-.024	-.035	-.060	-.108
	.657	-.095	-.048	-.020	-.012	-.022	-.046	-.098
	.697	-.088	-.044	-.018	-.007	-.016	-.041	-.090
	.737	-.081	-.040	-.013	-.001	-.012	-.034	-.081
	.777	-.077	-.035	-.009	.001	-.008	-.030	-.075
	.785	-.081	-.037	-.007	.004	-.006	-.029	-.075
	.817	-.070	-.025	-.004	.004	-.001	-.025	-.068
	.857	-.072	-.033	-.011	-.001	-.006	-.032	-.073
	.897	-.075	-.037	-.013	-.004	-.009	-.035	-.074

TABLE 2.- PRESSURE COEFFICIENTS FOR CONFIGURATION 121 - Continued

(d) $M = 1.00$; $\alpha = -10^\circ$ to 10°

	x/l	C_p for - $\phi = 0^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.328	.583	.498	.443	.406	.355	.321	.264
	.338	.553	.474	.420	.377	.328	.289	.234
	.348	.524	.451	.396	.347	.301	.256	.205
	.358	.488	.412	.361	.315	.266	.221	.169
	.378	.412	.341	.293	.247	.201	.159	.104
	.388	.341	.276	.228	.190	.154	.117	.063
	.393	.270	.214	.174	.140	.103	.067	.021
Upper stage	.399	-.534	-.558	-.578	-.586	-.596	-.616	-.638
	.404	-.562	-.622	-.660	-.689	-.709	-.728	-.750
	.409	-.419	-.507	-.566	-.607	-.642	-.673	-.708
	.419	-.242	-.348	-.414	-.470	-.517	-.563	-.601
	.429	-.185	-.266	-.323	-.364	-.401	-.427	-.385
	.439	-.145	-.208	-.249	-.272	-.271	-.217	-.127
	.449	-.139	-.181	-.173	-.096	-.027	-.001	-.020
Transition flare	.459	.242	.212	.189	.163	.134	.103	.056
	.482	.169	.137	.114	.101	.087	.084	.091
	.492	.148	.110	.084	.074	.060	.057	.061
	.512	.133	.092	.072	.056	.039	.033	.022
	.532	.127	.083	.057	.044	.024	.012	-.002
	.552	.100	.056	.027	.007	-.012	-.034	-.048
	.562	.016	-.017	-.040	-.060	-.083	-.099	-.104
Main stage	.568	-.203	-.258	-.293	-.319	-.339	-.370	-.381
	.577	-.188	-.240	-.269	-.279	-.287	-.284	-.292
	.587	-.142	-.197	-.223	-.234	-.244	-.245	-.249
	.597	-.115	-.160	-.189	-.200	-.201	-.196	-.191
	.607	-.106	-.154	-.168	-.166	-.165	-.153	-.143
	.617	-.109	-.139	-.146	-.142	-.134	-.120	-.109
	.627	-.106	-.124	-.128	-.121	-.113	-.095	-.082
	.637	-.081	-.099	-.104	-.096	-.091	-.074	-.060
	.657	-.061	-.072	-.074	-.068	-.064	-.042	-.032
	.677	-.039	-.055	-.063	-.045	-.050	-.003	-.009
	.697	-.014	-.035	-.031	.012	-.015	.019	.010
	.737	.046	.039	.025	.024	.025	.022	.014
	.777	.056	.037	.023	.024	.027	.023	.017
	.785	.064	.044	.029	.029	.033	.033	.048
	.817	.062	.041	.027	.022	.021	.023	.028
	.857	.048	.026	.014	.011	.013	.009	.008
	.877	.051	.026	.012	.009	.011	.008	.006
	.897	.043	.017	.004	.004	.006	.003	-.004

	x/l	C_p for - $\phi = -30^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.338	.515	.456	.408	.365	.322	.280	.219
	.348	.482	.427	.378	.335	.292	.248	.187
	.358	.456	.397	.352	.309	.263	.218	.154
	.378	.376	.321	.275	.241	.201	.156	.095
	.388	.311	.264	.222	.190	.154	.112	.057
	.393	.240	.202	.165	.140	.109	.067	.016
Upper stage	.399	-.669	-.687	-.704	-.711	-.722	-.726	-.758
	.404	-.583	-.628	-.660	-.683	-.712	-.737	-.756
	.409	-.467	-.540	-.590	-.628	-.660	-.694	-.723
	.419	-.267	-.354	-.414	-.461	-.502	-.542	-.586
	.429	-.206	-.275	-.326	-.364	-.392	-.417	-.407
	.439	-.185	-.233	-.265	-.279	-.280	-.247	-.142
	.449	-.157	-.178	-.158	-.090	-.030	-.007	-.036
Transition flare	.459	.223	.212	.186	.166	.146	.109	.028
	.482	.139	.125	.108	.101	.090	.078	.055
	.492	.118	.101	.084	.074	.060	.057	.031
	.512	.106	.083	.066	.053	.039	.024	-.005
	.532	.097	.074	.051	.041	.021	.006	-.030
	.552	.067	.044	.021	.007	-.015	-.040	-.079
	.562	.001	-.026	-.055	-.078	-.104	-.136	-.174
Main stage	.568	-.252	-.273	-.293	-.307	-.323	-.330	-.329
	.577	-.219	-.252	-.275	-.283	-.290	-.300	-.316
	.587	-.173	-.206	-.229	-.237	-.247	-.254	-.268
	.597	-.115	-.139	-.153	-.154	-.159	-.156	-.155
	.607	-.142	-.163	-.174	-.170	-.171	-.162	-.161
	.617	-.142	-.151	-.153	-.142	-.137	-.126	-.127
	.627	-.139	-.139	-.131	-.121	-.116	-.104	-.106
	.637	-.115	-.114	-.110	-.099	-.098	-.083	-.088
	.657	-.091	-.085	-.081	-.070	-.070	-.054	-.058
	.677	-.051	-.055	-.059	-.042	-.050	-.006	-.033
	.697	-.040	-.044	-.022	.013	-.014	.011	-.018
	.737	.074	.029	.022	.025	.024	.015	-.017
	.777	.039	.033	.025	.027	.028	.016	-.012
	.785	.035	.032	.025	.029	.032	.019	.000
	.817	.037	.030	.024	.022	.021	.010	-.011
	.857	.022	.015	.009	.010	.011	-.001	-.016
	.877	.021	.011	.005	.007	.007	-.004	-.018
	.897	.016	.007	.000	.003	.004	-.007	-.019
	.917	.015	.007	-.001	.003	.002	-.008	-.020
	.957	.004	-.002	-.007	-.003	-.008	-.018	-.028
	.997	-.042	-.058	-.077	-.096	-.117	-.131	-.141

TABLE I.- PRESSURE COEFFICIENTS FOR CONFIGURATION 121 - Continued

(d) $M = 1.00$; $\alpha = -10^\circ$ to 10° - Concluded

	x/l	C_p for - $\phi = -30^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.338	.406	.403	.384	.365	.334	.295	.222
	.348	.376	.371	.355	.332	.301	.262	.190
	.358	.347	.347	.322	.303	.272	.230	.157
	.378	.276	.276	.257	.232	.207	.165	.094
	.388	.214	.214	.201	.182	.157	.118	.051
Upper stage	.393	-.192	-.151	-.128	-.121	-.131	-.150	-.189
	.399	-.589	-.586	-.600	-.607	-.621	-.668	-.699
	.404	-.653	-.668	-.688	-.711	-.721	-.740	-.769
	.409	-.516	-.549	-.587	-.619	-.651	-.685	-.729
	.419	-.373	-.418	-.453	-.479	-.496	-.518	-.547
	.429	-.306	-.324	-.347	-.364	-.380	-.408	-.446
	.439	-.273	-.266	-.274	-.276	-.283	-.305	-.291
	.449	-.245	-.208	-.152	-.093	-.064	-.052	-.063
Transition flare	.459	.123	.166	.168	.166	.155	.109	.044
	.482	.052	.089	.093	.095	.084	.063	.013
	.492	.037	.068	.072	.074	.060	.042	-.002
	.512	.028	.053	.05	.053	.039	.018	-.027
	.532	.016	.038	.039	.037	.021	.003	-.048
Main stage	.552	-.023	-.001	.000	-.002	-.015	-.044	-.094
	.562	-.091	-.066	-.070	-.078	-.098	-.127	-.174
	.568	-.322	-.298	-.293	-.289	-.296	-.321	-.371
	.577	-.298	-.288	-.284	-.283	-.296	-.330	-.381
	.587	-.252	-.246	-.241	-.243	-.256	-.275	-.301
	.597	-.237	-.215	-.208	-.203	-.214	-.226	-.249
	.607	-.222	-.191	-.177	-.170	-.174	-.184	-.204
	.617	-.222	-.172	-.159	-.142	-.149	-.153	-.173
	.627	-.206	-.160	-.140	-.121	-.122	-.126	-.146
	.637	-.185	-.136	-.113	-.102	-.104	-.107	-.124
	.657	-.144	-.099	-.084	-.069	-.075	-.072	-.081
	.677	-.109	-.074	-.046	-.028	-.049	-.036	-.050
	.697	-.073	-.048	-.008	.014	-.022	.001	-.020
	.737	-.029	.009	.016	.025	.022	.007	-.012
	.777	-.020	.011	.018	.026	.023	.010	-.006
	.785	-.032	.003	.016	.027	.027	.013	.000
	.817	-.016	.012	.020	.023	.020	.008	-.008
	.857	-.033	-.005	.004	.011	.009	-.004	-.016
	.877	-.033	-.007	.000	.007	.006	-.006	-.019
	.897	-.039	-.013	-.005	.004	.003	-.008	-.022
	.917	-.048	-.020	-.010	.000	-.002	-.012	-.023
	.957	-.049	-.021	-.010	-.003	-.009	-.018	-.029
	.997	-.107	-.091	-.093	-.098	-.115	-.132	-.152

	x/l	C_p for - $\phi = -5^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.328	.329	.383	.405	.406	.402	.384	.329
	.358	.231	.279	.296	.303	.292	.268	.216
	.378	.169	.223	.228	.232	.227	.212	.151
Upper stage	.393	.036	.090	.106	.114	.109	.082	.027
	.399	-.605	-.580	-.578	-.559	-.569	-.600	-.638
	.419	-.464	-.458	-.466	-.476	-.481	-.484	-.495
	.439	-.364	-.306	-.286	-.276	-.283	-.317	-.376
Transition flare	.459	.092	.142	.162	.175	.161	.133	.080
	.482	-.011	.059	.081	.095	.084	.063	-.005
Main stage	.512	-.042	.020	.042	.053	.045	.024	-.033
	.552	-.082	-.020	-.003	.004	.000	-.028	-.091
	.568	-.432	-.389	-.379	-.377	-.388	-.413	-.469
	.587	-.326	-.276	-.259	-.249	-.259	-.281	-.338
	.607	-.268	-.203	-.177	-.166	-.174	-.199	-.262
	.627	-.228	-.160	-.131	-.121	-.128	-.153	-.216
	.657	-.157	-.102	-.084	-.070	-.080	-.095	-.147
	.697	-.110	-.054	-.007	.014	-.042	-.011	-.064
	.737	-.056	-.003	.014	.025	.021	-.006	-.055
	.777	-.047	-.001	.015	.025	.022	-.005	-.049
	.785	-.057	-.003	.014	.027	.025	.004	-.038
	.817	-.041	.003	.018	.024	.021	.000	-.040
	.857	-.055	-.014	.003	.011	.007	-.017	-.056
	.897	-.062	-.022	-.007	.004	.001	-.024	-.061

TABLE 2.- PRESSURE COEFFICIENTS FOR CONFIGURATION 121 - Continued

(e) $M = 1.20$; $\alpha = -10^\circ$ to 10°

	x/l	C_p for - $\phi = 0^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.328	.516	.42	.359	.310	.272	.223	.186
	.338	.521	.430	.369	.323	.275	.233	.196
	.348	.526	.441	.380	.337	.277	.244	.207
	.358	.521	.430	.372	.326	.272	.244	.199
	.378	.503	.423	.372	.316	.275	.236	.193
	.388	.474	.407	.364	.316	.285	.233	.188
	.393	.437	.380	.343	.302	.272	.228	.178
Upper stage	.399	-.220	-.238	-.249	-.264	-.282	-.303	-.336
	.404	-.292	-.331	-.356	-.376	-.383	-.401	-.421
	.409	-.205	-.263	-.299	-.327	-.342	-.363	-.391
	.419	-.105	-.171	-.216	-.251	-.277	-.298	-.329
	.429	-.056	-.117	-.159	-.195	-.215	-.234	-.258
	.439	-.035	-.087	-.118	-.143	-.158	-.160	-.163
	.449	-.029	-.071	-.096	-.108	-.115	-.101	-.071
Transition flare	.459	.244	.192	.150	.130	.110	.105	.096
	.482	.158	.120	.111	.102	.098	.088	.087
	.492	.140	.106	.097	.083	.076	.066	.061
	.512	.134	.101	.087	.070	.052	.042	.034
	.532	.140	.109	.076	.064	.044	.029	.018
	.552	.150	.109	.079	.054	.036	.021	.012
	.562	.102	.072	.049	.024	.004	-.009	-.009
Main stage	.568	-.027	-.071	-.097	-.122	-.145	-.158	-.178
	.577	-.056	-.101	-.121	-.138	-.148	-.153	-.164
	.587	-.032	-.080	-.105	-.117	-.121	-.120	-.115
	.597	-.027	-.063	-.078	-.092	-.099	-.101	-.102
	.607	-.013	-.050	-.064	-.079	-.083	-.082	-.080
	.617	-.013	-.050	-.061	-.070	-.069	-.066	-.064
	.627	-.008	-.050	-.056	-.062	-.056	-.055	-.055
	.637	.001	-.036	-.040	-.046	-.045	-.044	-.034
	.657	-.008	-.034	-.042	-.040	-.030	-.024	-.026
	.677	-.001	-.012	-.028	-.028	-.025	-.017	-.020
	.697	.006	-.018	-.026	-.022	-.017	-.008	-.021
	.737	-.003	-.013	-.014	-.028	-.022	-.022	-.022
	.777	.024	-.005	-.023	-.018	-.023	-.023	-.012
	.785	.032	.000	-.012	-.012	-.016	-.006	-.014
	.817	.028	.004	.000	-.019	-.016	-.004	-.007
	.857	.025	.013	-.006	.000	.004	-.003	-.016
	.877	.036	.001	-.002	.001	-.001	.001	-.014
	.897	.016	.001	.003	-.002	-.007	-.011	-.021

	x/l	C_p for - $\phi = -30^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.338	.487	.415	.356	.316	.272	.228	.183
	.348	.484	.415	.364	.321	.267	.236	.188
	.358	.487	.415	.364	.323	.272	.241	.188
	.378	.468	.404	.361	.313	.275	.239	.186
	.388	.442	.394	.356	.313	.288	.239	.186
	.393	.408	.367	.338	.302	.275	.228	.170
Upper stage	.399	-.340	-.349	-.358	-.370	-.380	-.398	-.428
	.404	-.311	-.336	-.356	-.376	-.391	-.409	-.434
	.409	-.248	-.290	-.316	-.343	-.364	-.385	-.415
	.419	-.110	-.166	-.207	-.241	-.267	-.290	-.329
	.429	-.083	-.128	-.164	-.192	-.212	-.228	-.256
	.439	-.070	-.104	-.132	-.149	-.164	-.169	-.185
	.449	-.048	-.071	-.094	-.100	-.107	-.104	-.093
Transition flare	.459	.236	.197	.155	.136	.123	.108	.064
	.482	.118	.106	.103	.102	.098	.085	.055
	.492	.108	.098	.095	.083	.076	.061	.036
	.512	.110	.093	.084	.064	.052	.034	.007
	.532	.108	.098	.073	.062	.044	.023	-.007
	.552	.113	.093	.073	.051	.036	.010	-.017
	.562	.094	.069	.049	.019	-.004	-.034	-.067
Main stage	.568	-.081	-.104	-.116	-.133	-.151	-.158	-.153
	.577	-.081	-.118	-.132	-.146	-.151	-.150	-.169
	.587	-.051	-.088	-.099	-.111	-.124	-.128	-.145
	.597	-.027	-.050	-.056	-.062	-.067	-.071	-.083
	.607	-.043	-.063	-.072	-.079	-.083	-.090	-.104
	.617	-.035	-.058	-.061	-.068	-.069	-.074	-.083
	.627	-.037	-.061	-.059	-.062	-.061	-.063	-.069
	.637	-.032	-.050	-.048	-.051	-.053	-.050	-.058
	.657	-.024	-.034	-.041	-.038	-.024	-.030	-.048
	.677	-.017	-.012	-.022	-.020	-.024	-.023	-.047
	.697	-.026	-.026	-.024	-.026	-.027	-.023	-.052
	.737	-.028	-.024	-.019	-.025	-.023	-.030	-.054
	.777	.002	-.009	-.021	-.012	-.021	-.026	-.054
	.785	.006	-.006	-.011	-.004	-.014	-.021	-.037
	.817	.003	-.008	-.004	-.017	-.015	-.023	-.046
	.857	-.002	.006	-.006	-.009	-.007	-.021	-.046
	.877	.006	-.009	-.005	-.002	-.003	-.017	-.041
	.897	-.008	-.007	.000	.000	-.003	-.019	-.035
	.917	-.005	.000	-.002	-.004	-.005	-.017	-.031
	.957	-.010	-.011	-.010	-.014	-.015	-.017	-.031
	.997	.005	-.017	-.030	-.052	-.075	-.081	-.078

TABLE 2.- PRESSURE COEFFICIENTS FOR CONFIGURATION 121 - Concluded

(c) M = 1.20; α = -10° to 10° - Concluded

	x/l	C_p for - η = -.00°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.338	.374	.357	.335	.313	.283	.244	.186
	.348	.382	.357	.338	.316	.280	.249	.193
	.358	.378	.362	.335	.316	.277	.252	.193
	.378	.363	.357	.343	.310	.285	.257	.188
	.388	.342	.344	.338	.310	.296	.252	.183
	.393	-.171	-.148	-.130	-.122	-.129	-.161	-.192
	.399	-.293	-.287	-.285	-.299	-.320	-.346	-.388
Upper stage	.404	-.367	-.366	-.375	-.389	-.399	-.418	-.450
	.409	-.292	-.304	-.318	-.341	-.364	-.391	-.434
	.419	-.211	-.223	-.237	-.254	-.269	-.285	-.323
	.429	-.167	-.169	-.180	-.195	-.204	-.225	-.272
	.439	-.146	-.133	-.142	-.146	-.158	-.174	-.226
	.449	-.127	-.104	-.107	-.105	-.118	-.131	-.188
Transition flare	.459	.095	.118	.120	.125	.110	.086	.042
	.482	.033	.077	.092	.097	.090	.066	.018
	.492	.033	.072	.087	.081	.076	.050	.004
	.512	.030	.066	.076	.064	.052	.034	-.012
	.532	.030	.064	.063	.059	.044	.023	-.026
	.552	.022	.045	.047	.043	.028	-.001	-.039
	.562	.006	.018	.020	.011	-.004	-.028	-.067
Main stage	.568	-.143	-.137	-.129	-.138	-.148	-.158	-.199
	.577	-.143	-.137	-.129	-.133	-.151	-.169	-.218
	.587	-.124	-.118	-.110	-.111	-.129	-.147	-.191
	.597	-.113	-.107	-.097	-.092	-.107	-.128	-.164
	.607	-.113	-.093	-.089	-.079	-.088	-.107	-.142
	.617	-.116	-.090	-.075	-.068	-.077	-.090	-.123
	.627	-.116	-.088	-.067	-.062	-.069	-.085	-.104
	.637	-.108	-.066	-.056	-.051	-.053	-.069	-.083
	.657	-.091	-.034	-.031	-.020	-.022	-.045	-.071
	.677	-.084	-.040	-.028	-.022	-.027	-.042	-.068
	.697	-.077	-.045	-.024	-.025	-.031	-.039	-.066
	.737	-.082	-.044	-.026	-.025	-.028	-.043	-.055
	.777	-.057	-.034	-.023	-.013	-.021	-.030	-.046
	.785	-.048	-.035	-.017	-.006	-.017	-.024	-.045
	.817	-.052	-.019	-.008	-.014	-.016	-.028	-.046
	.857	-.060	-.014	-.012	-.013	-.021	-.028	-.045
	.877	-.049	-.027	-.006	-.002	-.006	-.019	-.041
	.897	-.061	-.025	-.007	.001	-.001	-.014	-.031
	.917	-.066	-.028	-.015	-.005	-.007	-.018	-.028
	.957	-.065	-.033	-.017	-.014	-.017	-.017	-.032
	.997	-.056	-.043	-.039	-.052	-.066	-.087	-.101

	x/l	C_p for - η = -.00°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.328	.256	.299	.311	.316	.317	.296	.259
	.358	.258	.294	.303	.313	.301	.288	.254
	.378	.253	.304	.311	.310	.304	.296	.243
Upper stage	.393	.198	.249	.285	.279	.285	.254	.196
	.399	-.329	-.295	-.296	-.264	-.306	-.325	-.363
	.419	-.281	-.253	-.251	-.257	-.261	-.271	-.304
	.439	-.221	-.166	-.153	-.146	-.153	-.171	-.226
Transition flare	.459	.006	.091	.115	.133	.115	.089	-.001
	.482	-.016	.058	.089	.097	.090	.064	-.009
	.512	-.038	.034	.065	.064	.060	.039	-.023
	.552	-.032	.018	.041	.048	.042	.007	-.039
Main stage	.568	-.211	-.191	-.178	-.179	-.183	-.199	-.248
	.587	-.181	-.150	-.127	-.114	-.126	-.150	-.213
	.607	-.176	-.118	-.094	-.079	-.094	-.118	-.191
	.627	-.162	-.085	-.070	-.062	-.069	-.093	-.159
	.657	-.124	-.053	-.026	-.021	-.028	-.059	-.118
	.697	-.125	-.068	-.037	-.029	-.041	-.060	-.124
	.737	-.106	-.056	-.030	-.028	-.029	-.056	-.110
	.777	-.073	-.043	-.021	-.015	-.020	-.045	-.093
	.785	-.083	-.047	-.023	-.011	-.019	-.042	-.095
	.817	-.071	-.024	-.008	-.009	-.015	-.037	-.083
	.857	-.075	-.027	-.014	-.009	-.028	-.046	-.083
	.897	-.083	-.037	-.015	-.004	-.005	-.023	-.072

TABLE 3.- PRESSURE COEFFICIENTS FOR CONFIGURATION 221

(a) M = 0.40 to 0.95; $\alpha = 0°$

		C_p for - $\phi = 0°$					
	x/l	M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.357	.380	.448	.455	.497	.525	.562
	.367	.292	.359	.366	.406	.433	.478
	.377	.171	.241	.250	.303	.340	.388
	.387	.051	.122	.134	.200	.246	.298
	.399	-1.477	-1.140	-1.203	-1.185	-1.024	-.885
	.404	-.331	-.698	-.736	-.907	-1.127	-.991
	.409	-.196	-.383	-.512	-.603	-.969	-.898
Upper stage	.419	-.083	-.072	-.137	-.317	-.367	-.691
	.429	-.038	-.008	-.016	-.077	-.182	-.525
	.439	-.004	.029	.025	.030	.044	-.170
	.449	.029	.070	.063	.080	.137	.081
	.459	.142	.175	.158	.165	.208	.202
	.482	.018	.056	.050	.058	.083	.151
	.492	.007	.038	.029	.033	.050	.110
Transition flare	.512	.007	.015	.009	.012	.017	.062
	.532	-.015	-.008	-.016	-.024	-.014	.027
	.552	-.073	-.054	-.067	-.086	-.078	-.034
	.562	-.141	-.124	-.143	-.169	-.184	-.134
	.568	-.174	-.206	-.222	-.276	-.373	-.404
	.577	-.084	-.091	-.100	-.125	-.132	-.359
	.587	-.061	-.058	-.067	-.082	-.078	-.272
Main stage	597	-.050	-.040	-.050	-.060	-.058	-.085
	.607	-.038	-.026	-.042	-.049	-.044	-.024
	.617	-.038	-.022	-.037	-.042	-.037	-.014
	.627	-.027	-.017	-.025	-.035	-.031	-.014
	.637	-.015	-.012	-.021	-.027	-.024	-.014
	.657	-.015	.000	-.012	-.019	-.016	-.013
	.677	-.015	.000	-.011	-.018	-.015	-.016
	.697	-.015	.003	-.008	-.014	-.012	-.015
	.737	-.012	.006	-.007	-.013	-.010	-.015
	.777	-.012	.009	-.002	-.009	-.007	-.012
	.785	-.008	.012	.000	-.007	-.001	-.009
	.817	-.007	.011	.001	-.005	-.003	-.008
	.857	-.008	.007	-.002	-.009	-.007	-.012
	.877	-.008	.008	-.002	-.009	-.006	-.011
	.897	-.011	.005	-.005	-.012	-.009	-.014

		C_p for - $\phi = -30°$					
	x/l	M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.367	.281	.354	.362	.403	.433	.472
	.377	.182	.261	.264	.312	.351	.394
	.387	.040	.113	.126	.193	.240	.295
	.399	-1.336	-1.066	-1.216	-1.232	-1.068	-.927
	.404	-.331	-.698	-.736	-.979	-1.140	-1.003
	.409	-.173	-.378	-.499	-.589	-1.026	-.911
Upper stage	.419	-.083	-.072	-.129	-.306	-.330	-.675
	.429	-.038	-.008	-.012	-.059	-.125	-.521
	.439	-.004	.024	.021	.033	.050	-.164
	.449	.041	.074	.067	.083	.134	.078
	.459	.153	.179	.166	.172	.228	.202
	.482	.018	.056	.050	.058	.083	.151
	.492	.007	.038	.029	.033	.050	.110
Transition flare	.512	.007	.015	.004	.001	.017	.059
	.532	-.027	-.008	-.016	-.027	-.017	.021
	.552	-.073	-.059	-.067	-.086	-.082	-.034
	.562	-.141	-.128	-.143	-.176	-.195	-.140
	.568	-.163	-.192	-.210	-.258	-.370	-.394
	.577	-.084	-.091	-.100	-.125	-.129	-.359
	.587	-.061	-.063	-.067	-.085	-.081	-.281
Main stage	.597	-.050	-.035	-.046	-.049	-.044	-.062
	.607	-.038	-.026	-.042	-.049	-.044	-.024
	.617	-.027	-.022	-.029	-.042	-.037	-.014
	.627	-.027	-.017	-.025	-.035	-.031	-.017
	.637	-.015	-.012	-.021	-.027	-.024	-.017
	.657	-.019	-.003	-.015	-.021	-.019	-.014
	.677	-.012	.006	-.005	-.013	-.009	-.011
	.697	-.015	.003	-.008	-.015	-.012	-.015
	.737	-.012	.006	-.005	-.012	-.009	-.014
	.777	-.008	.011	.000	-.006	-.003	-.008
	.785	-.008	.011	.000	-.006	-.001	-.009
	.817	-.007	.011	.001	-.005	-.003	-.008
	.857	-.009	.006	-.003	-.010	-.008	-.013
	.877	-.011	.006	-.004	-.011	-.009	-.013
	.897	-.012	.004	-.006	-.012	-.010	-.015
	.917	-.012	.003	-.006	-.013	-.011	-.015
	.957	-.023	-.007	-.017	-.023	-.022	-.026
	.997	-.072	-.061	-.073	-.083	-.082	-.095

TABLE 3.- PRESSURE COEFFICIENTS FOR CONFIGURATION 221 - Continued

(a) M = 0.40 to 0.95; α = 0° - Concluded

	x/l	C_p for - ϕ = -60°					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.367	.281	.350	.358	.399	.430	.469
	.377	.182	.252	.264	.308	.345	.394
	.387	.051	.118	.130	.197	.246	.301
	.399	-1.336	-1.330	-1.342	-1.123	-.969	-.834
	.404	-.331	-.657	-.732	-.911	-1.117	-.984
	.409	-.173	-.373	-.503	-.632	-1.013	-.901
	.419	-.094	-.062	-.100	-.296	-.353	-.684
	.429	-.038	-.008	-.008	-.045	-.138	-.528
Upper stage	.439	-.004	.029	.025	.044	.050	-.167
	.449	.029	.070	.063	.080	.134	.081
	.459	.142	.170	.158	.158	.224	.202
	.482	.018	.056	.050	.055	.083	.148
	.492	.007	.038	.029	.030	.050	.110
	.512	.007	.015	.004	.001	.017	.059
Transition flare	.532	-.038	-.008	-.016	-.027	-.017	.021
	.552	-.084	-.063	-.076	-.093	-.089	-.043
	.562	-.141	-.128	-.143	-.176	-.191	-.137
	.568	-.163	-.192	-.205	-.248	-.343	-.371
	.577	-.084	-.091	-.100	-.121	-.129	-.359
	.587	-.061	-.063	-.067	-.085	-.085	-.285
	.597	-.050	-.040	-.046	-.060	-.058	-.082
	.607	-.038	-.026	-.042	-.049	-.044	-.024
	.617	-.027	-.022	-.029	-.042	-.037	-.014
	.627	-.015	-.017	-.025	-.035	-.031	-.017
	.637	-.015	-.012	-.021	-.031	-.024	-.017
	.657	-.019	-.002	-.014	-.020	-.018	-.015
	.677	-.017	.002	-.010	-.017	-.015	-.015
	.697	-.015	.005	-.007	-.013	-.011	-.014
	.737	-.012	.006	-.004	-.012	-.009	-.013
	.777	-.008	.011	-.001	-.007	-.003	-.008
	.785	-.008	.011	.000	-.007	-.006	-.011
	.817	-.007	.011	.001	-.004	-.003	-.007
	.857	-.011	.006	-.003	-.010	-.007	-.013
	.877	-.011	.006	-.004	-.010	-.009	-.013
	.897	-.011	.005	-.004	-.012	-.009	-.014
	.917	-.014	.000	-.009	-.016	-.014	-.018
	.957	-.023	-.007	-.017	-.023	-.022	-.025
Main stage	.997	-.074	-.063	-.073	-.083	-.084	-.097

	x/l	C_p for - ϕ = -90°					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.357	.369	.435	.447	.487	.515	.553
	.377	.182	.261	.268	.315	.358	.400
	.387	.040	.140	.155	.218	.266	.319
	.399	-1.575	-1.506	-1.514	-1.228	-1.054	-.914
	.419	-.083	-.062	-.100	-.328	-.404	-.691
Upper stage	.439	-.004	.024	.021	.041	.017	-.164
	.459	.142	.175	.166	.158	.198	.202
	.482	.018	.056	.050	.055	.083	.148
	.512	-.015	.015	.004	.001	.017	.059
Transition flare	.552	-.084	-.063	-.076	-.089	-.085	-.040
	.568	-.197	-.234	-.252	-.305	-.411	-.478
	.587	-.061	-.063	-.071	-.089	-.085	-.288
	.607	-.038	-.026	-.042	-.049	-.044	-.024
	.627	-.015	-.017	-.025	-.035	-.031	-.017
	.657	-.019	-.003	-.015	-.021	-.018	-.016
	.697	-.015	.000	-.012	-.015	-.014	-.016
	.737	-.012	.008	-.004	-.013	-.009	-.013
	.777	-.008	.009	-.002	-.008	-.006	-.011
	.785	-.008	.009	-.002	-.008	-.003	-.011
	.817	-.005	.012	.003	-.003	-.001	-.005
	.857	-.009	.008	-.003	-.009	-.007	-.012
Main stage	.897	-.011	.005	-.005	-.012	-.010	-.014

TABLE 5.- PRESSURE COEFFICIENTS FOR CONFIGURATION 221 - Continued

(b) M = 0.60; α = -10° to 10°

	x/l	C_p for - ϕ = 0°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.357	.635	.551	.485	.420	.357	.290	.206
	.367	.540	.457	.390	.325	.262	.201	.128
	.377	.417	.328	.265	.203	.139	.083	.018
	.387	.295	.200	.139	.080	.017	-.035	-.093
	.399	-1.351	-1.495	-1.553	-1.528	-1.431	-1.235	-.941
Upper stage	.404	-.235	-.314	-.377	-.432	-.514	-.588	-.663
	.409	-.098	-.149	-.171	-.198	-.234	-.285	-.377
	.419	-.012	-.046	-.063	-.072	-.080	-.080	-.080
	.429	.028	.000	-.017	-.021	-.023	-.023	-.012
	.439	.067	.034	.023	.013	.011	.011	.017
	.449	.107	.079	.062	.059	.051	.051	.051
	.459	.255	.216	.193	.167	.148	.131	.108
Transition flare	.482	.135	.085	.062	.042	.023	.011	.011
	.492	.113	.062	.040	.025	.006	.000	-.012
	.512	.096	.039	.023	.019	.000	-.017	-.041
	.532	.067	.022	.000	-.015	-.029	-.046	-.058
	.552	.022	-.023	-.046	-.062	-.075	-.081	-.087
	.562	-.065	-.105	-.122	-.137	-.139	-.139	-.140
Main stage	.568	-.104	-.162	-.184	-.194	-.184	-.167	-.150
	.577	-.030	-.069	-.086	-.090	-.092	-.092	-.081
	.587	-.001	-.041	-.052	-.056	-.063	-.058	-.052
	.597	.005	-.029	-.040	-.044	-.046	-.040	-.035
	.607	.016	-.023	-.029	-.033	-.040	-.035	-.023
	.617	.016	-.012	-.023	-.027	-.029	-.029	-.018
	.627	.021	-.012	-.023	-.027	-.023	-.023	-.018
	.637	.027	-.001	-.012	-.021	-.023	-.012	-.006
	.657	.036	.004	-.004	-.002	-.004	-.008	.000
	.677	.036	.006	-.004	.000	-.006	-.006	.002
	.697	.040	.008	.000	.004	.000	-.002	.002
	.737	.040	.009	.002	.002	-.004	-.002	.000
	.777	.042	.013	.006	.006	.000	.000	.005
	.785	.047	.019	.008	.008	.002	.004	.015
	.817	.045	.019	.009	.006	.003	.003	.009
	.857	.038	.012	.004	.003	.000	-.002	.001
	.877	.039	.014	.004	.003	.000	-.002	.002
	.897	.034	.010	.001	.000	-.004	-.005	-.003

	x/l	C_p for - ϕ = -30°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.367	.501	.429	.379	.320	.262	.201	.128
	.377	.406	.328	.279	.225	.173	.111	.044
	.387	.250	.178	.122	.074	.017	-.035	-.099
	.399	-1.201	-1.310	-1.339	-1.326	-1.270	-1.206	-1.253
Upper stage	.404	-.258	-.320	-.365	-.426	-.480	-.537	-.583
	.409	-.109	-.143	-.166	-.181	-.206	-.251	-.309
	.419	-.035	-.057	-.069	-.072	-.080	-.080	-.092
	.429	.005	-.012	-.017	-.021	-.[illegible]	-.023	-.029
	.439	.039	.022	.017	.013	.[illegible]	.011	.005
	.449	.096	.074	.068	.065	.057	.051	.045
	.459	.244	.216	.193	.178	.153	.142	.119
Transition flare	.482	.107	.073	.062	.042	.028	.011	.005
	.492	.090	.062	.040	.025	.006	.000	-.018
	.512	.067	.034	.017	.008	-.012	-.029	-.041
	.532	.050	.011	-.006	-.021	-.035	-.052	-.064
	.552	-.001	-.023	-.046	-.062	-.075	-.087	-.105
	.562	-.082	-.110	-.128	-.137	-.145	-.151	-.151
Main stage	.568	-.139	-.173	-.184	-.182	-.184	-.173	-.156
	.577	-.058	-.081	-.086	-.090	-.092	-.092	-.093
	.587	-.030	-.052	-.058	-.061	-.063	-.063	-.064
	.597	-.01[illegible]	-.035	-.040	-.038	-.040	-.040	-.035
	.607	-.012	-.029	-.029	-.033	-.040	-.035	-.035
	.617	-.001	-.023	-.029	-.027	-.029	-.029	-.029
	.627	-.001	-.023	-.023	-.027	-.023	-.023	-.029
	.637	.005	-.012	-.012	-.021	-.023	-.023	-.023
	.657	.009	-.006	-.010	-.002	-.008	-.015	-.022
	.677	.020	.004	.000	.002	-.004	-.008	-.016
	.697	.015	-.002	-.004	.002	-.002	-.010	-.020
	.737	.015	.002	.000	.004	-.002	-.008	-.018
	.777	.024	.008	.004	.010	.000	-.006	-.018
	.785	.019	.004	.002	.008	.002	-.006	-.014
	.817	.017	.007	.006	.005	.002	-.004	-.017
	.857	.011	.002	.000	.002	-.002	-.008	-.020
	.877	.010	.000	.000	.002	-.003	-.010	-.020
	.897	.009	-.002	-.001	-.001	-.004	-.013	-.022
	.917	.008	-.002	-.004	-.001	-.007	-.016	-.025
	.957	-.008	-.014	-.013	-.011	-.018	-.027	-.035
	.997	-.087	-.077	-.064	-.064	-.074	-.090	-.112

TABLE 3.- PRESSURE COEFFICIENTS FOR CONFIGURATION 221 - Continued

(b) M = 0.60; α = -10° to 10° - Concluded

	x/l	C_p for - ϕ = -60°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.367	.373	.367	.345	.320	.279	.234	.145
	.377	.284	.273	.251	.225	.184	.134	.061
	.387	.150	.133	.111	.080	.045	.022	-.075
	.399	-1.397	-1.484	-1.541	-1.563	-1.633	-1.662	-1.559
Upper stage	.404	-.320	-.337	-.354	-.364	-.417	-.451	-.480
	.409	-.172	-.166	-.166	-.169	-.188	-.211	-.252
	.419	-.104	-.092	-.080	-.078	-.080	-.097	-.137
	.429	-.058	-.035	-.029	-.021	-.029	-.046	-.080
	.439	-.018	.005	.011	.013	.011	-.006	-.040
	.449	.022	.045	.057	.059	.051	.034	-.006
Transition flare	.459	.153	.170	.170	.167	.153	.136	.091
	.482	.028	.039	.040	.042	.023	.006	-.041
	.492	.011	.022	.023	.019	.006	-.012	-.053
	.512	-.001	.009	.011	.008	-.012	-.029	-.070
	.532	-.030	-.018	-.017	-.021	-.035	-.058	-.093
	.552	-.082	-.076	-.070	-.068	-.081	-.104	-.145
	.562	-.146	-.139	-.139	-.137	-.145	-.162	-.192
Main stage	.568	-.220	-.202	-.184	-.182	-.184	-.196	-.231
	.577	-.116	-.098	-.086	-.084	-.092	-.109	-.127
	.587	-.093	-.081	-.063	-.061	-.069	-.081	-.104
	.597	-.081	-.058	-.046	-.038	-.046	-.063	-.081
	.607	-.070	-.046	-.035	-.033	-.040	-.052	-.075
	.617	-.064	-.046	-.029	-.027	-.035	-.046	-.064
	.627	-.058	-.041	-.029	-.027	-.029	-.040	-.058
	.637	-.053	-.035	-.023	-.021	-.023	-.035	-.052
	.657	-.051	-.027	-.015	-.004	-.013	-.029	-.047
	.677	-.041	-.021	-.010	-.001	-.010	-.024	-.040
	.697	-.032	-.016	-.004	.002	-.006	-.019	-.033
	.737	-.041	-.020	-.006	.006	-.006	-.019	-.023
	.777	-.037	-.016	-.002	.008	-.002	-.015	-.023
	.785	-.041	-.018	-.004	.008	-.002	-.013	-.023
	.817	-.038	-.013	.000	.006	.000	-.010	-.019
	.857	-.042	-.017	-.004	.002	-.004	-.013	-.022
	.877	-.042	-.019	-.004	.002	-.005	-.013	-.022
	.897	-.045	-.019	-.006	.000	-.006	-.015	-.023
	.917	-.053	-.026	-.012	-.004	-.010	-.019	-.027
	.957	-.057	-.034	-.018	-.012	-.019	-.028	-.037
	.997	-.123	-.097	-.078	-.066	-.077	-.095	-.116

	x/l	C_p for - ϕ = -30°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.357	.328	.390	.412	.409	.401	.362	.284
	.377	.155	.195	.217	.225	.201	.178	.128
	.387	.022	.067	.078	.097	.067	.045	.005
	.399	-1.645	-1.651	-1.553	-1.753	-1.599	-1.662	-1.709
Upper stage	.419	-.143	-.097	-.080	-.072	-.080	-.103	-.155
	.439	-.069	-.017	.006	.013	.006	-.017	-.075
Transition flare	.459	.096	.148	.165	.173	.165	.142	.085
	.482	-.036	.011	.034	.042	.023	.006	-.041
	.512	-.076	-.029	-.006	.008	-.006	-.029	-.076
	.552	-.134	-.093	-.070	-.068	-.081	-.099	-.145
Main stage	.568	-.317	-.259	-.230	-.217	-.242	-.271	-.323
	.587	-.127	-.092	-.069	-.061	-.069	-.086	-.139
	.607	-.104	-.064	-.040	-.033	-.040	-.063	-.110
	.627	-.093	-.046	-.029	-.021	-.029	-.052	-.098
	.657	-.082	-.037	-.017	-.002	-.013	-.040	-.083
	.697	-.076	-.035	-.014	.000	-.013	-.037	-.079
	.737	-.068	-.029	-.008	.004	-.006	-.031	-.07
	.777	-.066	-.029	-.006	.008	-.008	-.027	-.070
	.785	-.070	-.029	-.006	.006	-.004	-.027	-.066
	.817	-.061	-.020	-.001	.008	-.001	-.020	-.059
	.857	-.067	-.026	-.006	.002	-.005	-.025	-.065
	.897	-.065	-.028	-.009	-.001	-.009	-.029	-.068

TABLE 5.- PRESSURE COEFFICIENTS FOR CONFIGURATION 221 - Continued

(c) M = 0.80; α = -10° to 10°

	x/l	C_p for - ϕ = 0°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.357	.688	.605	.540	.474	.411	.348	.264
	.367	.598	.511	.446	.384	.318	.262	.182
	.377	.482	.397	.333	.274	.213	.157	.084
	.387	.366	.282	.221	.163	.108	.052	-.013
	.399	-1.313	-1.338	-1.355	-1.337	-1.088	-.676	-.475
Upper stage	.404	-.673	-.774	-.764	-.731	-.684	-.599	-.477
	.409	-.351	-.479	-.530	-.558	-.565	-.553	-.512
	.419	-.017	-.060	-.127	-.236	-.320	-.369	-.420
	.429	.014	.005	.004	-.040	-.105	-.158	-.209
	.439	.048	.040	.038	.029	.003	-.031	-.055
	.449	.102	.085	.084	.071	.053	.034	.025
Transition flare	.459	.266	.227	.199	.155	.114	.080	.075
	.482	.136	.097	.080	.055	.041	.026	.025
	.492	.109	.070	.053	.033	.018	.007	-.002
	.512	.082	.051	.038	.010	-.005	-.020	-.041
	.532	.063	.024	.007	-.017	-.036	-.047	-.064
	.552	.010	-.026	-.047	-.072	-.087	-.098	-.103
	.562	-.103	-.123	-.137	-.150	-.145	-.145	-.150
Main stage	.568	-.191	-.235	-.244	-.246	-.218	-.186	-.176
	.577	-.071	-.092	-.101	-.110	-.109	-.101	-.102
	.587	-.036	-.053	-.062	-.071	-.075	-.066	-.067
	.597	-.021	-.037	-.047	-.052	-.055	-.051	-.048
	.607	-.009	-.026	-.031	-.044	-.044	-.039	-.036
	.617	-.006	-.022	-.027	-.037	-.036	-.031	-.033
	.627	.002	-.014	-.020	-.033	-.032	-.028	-.025
	.637	.009	-.006	-.016	-.021	-.024	-.020	-.021
	.657	.018	.005	-.004	-.015	-.014	-.013	-.011
	.677	.018	.005	-.004	-.013	-.013	-.012	-.011
	.697	.021	.008	.000	-.012	-.010	-.008	-.009
	.737	.021	.009	.000	-.008	-.005	-.008	-.009
	.777	.026	.014	.004	-.004	-.005	-.004	-.009
	.785	.031	.020	.009	-.002	.000	.002	.002
	.817	.034	.018	.010	-.001	-.002	-.002	-.004
	.857	.026	.012	.004	-.004	-.005	-.007	-.013
	.877	.028	.013	.006	-.003	-.005	-.007	-.013
	.897	.023	.008	.001	-.007	-.008	-.010	-.017

	x/l	C_p for - ϕ = -30°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.367	.553	.489	.435	.380	.318	.262	.178
	.377	.463	.399	.341	.290	.231	.172	.114
	.387	.321	.256	.210	.155	.108	.052	-.009
	.399	-1.356	-1.373	-1.382	-1.352	-.905	-.734	-.778
Upper stage	.404	-.681	-.824	-.779	-.735	-.715	-.664	-.589
	.409	-.293	-.440	-.534	-.562	-.588	-.599	-.550
	.419	-.051	-.096	-.112	-.217	-.304	-.334	-.362
	.429	-.013	-.003	.004	-.029	-.089	-.127	-.170
	.439	.022	.028	.034	.029	.007	-.020	-.048
	.449	.083	.085	.088	.075	.056	.042	.025
Transition flare	.459	.251	.231	.206	.166	.121	.103	.090
	.482	.105	.089	.080	.055	.045	.026	.014
	.492	.086	.062	.049	.033	.018	.003	-.013
	.512	.060	.039	.027	.006	-.009	-.028	-.044
	.532	.037	.013	.004	-.021	-.036	-.055	-.076
	.552	-.021	-.038	-.047	-.072	-.087	-.106	-.118
	.562	-.122	-.139	-.144	-.154	-.157	-.168	-.181
Main stage	.568	-.218	-.235	-.233	-.226	-.210	-.202	-.195
	.577	-.098	-.103	-.105	-.110	-.109	-.105	-.110
	.587	-.067	-.068	-.066	-.075	-.075	-.070	-.079
	.597	-.036	-.037	-.039	-.044	-.044	-.039	-.048
	.607	-.036	-.037	-.035	-.044	-.044	-.039	-.048
	.617	-.032	-.030	-.027	-.037	-.036	-.031	-.040
	.627	-.028	-.026	-.027	-.033	-.032	-.028	-.040
	.637	-.021	-.018	-.016	-.025	-.024	-.024	-.036
	.657	-.010	-.008	-.011	-.017	-.018	-.020	-.029
	.677	.001	.004	.000	-.008	-.009	-.012	-.025
	.697	-.005	-.001	-.004	-.012	-.011	-.013	-.029
	.737	-.003	.001	.000	-.007	-.009	-.011	-.027
	.777	.007	.009	.006	-.002	-.004	-.008	-.025
	.785	.001	.007	.005	.000	.000	-.004	-.020
	.817	.006	.007	.006	-.001	-.002	-.008	-.025
	.857	-.001	.001	.001	-.006	-.006	-.012	-.028
	.877	-.002	.000	-.001	-.006	-.007	-.013	-.029
	.897	-.003	-.002	-.002	-.008	-.009	-.015	-.030
	.917	-.004	-.002	-.003	-.008	-.011	-.018	-.033
	.957	-.018	-.014	-.012	-.019	-.022	-.031	-.045
	.997	-.098	-.079	-.069	-.076	-.084	-.098	-.123

TABLE 5.- PRESSURE COEFFICIENTS FOR CONFIGURATION 221 - Continued

(c) M = 0.80; α = -10° to 10° - Concluded

	x/l	C_p for - ϕ = -60°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.367	.426	.429	.405	.377	.336	.288	.201
	.377	.339	.331	.315	.283	.243	.205	.129
	.387	.273	.215	.191	.163	.130	.112	.013
Upper stage	.399	-1.259	-1.264	-1.277	-1.263	-1.270	-1.273	-.898
	.404	-.685	-.755	-.749	-.739	-.684	-.695	-.704
	.409	-.462	-.529	-.572	-.589	-.581	-.584	-.616
	.419	-.105	-.087	-.131	-.198	-.285	-.288	-.324
	.429	-.078	-.026	-.004	-.017	-.059	-.089	-.144
	.439	-.036	.009	.034	.033	.022	-.004	-.055
	.449	.014	.055	.072	.071	.056	.038	-.017
Transition flare	.459	.155	.185	.183	.155	.140	.129	.090
	.482	.018	.051	.061	.052	.041	.015	-.037
	.492	-.001	.032	.038	.013	.018	-.008	-.052
	.512	-.017	.009	.015	.006	-.009	-.028	-.080
	.532	-.044	-.018	-.012	-.021	-.036	-.055	-.107
	.552	-.110	-.084	-.070	-.080	-.091	-.117	-.161
	.562	-.192	-.166	-.152	-.154	-.161	-.187	-.228
Main stage	.568	-.296	-.254	-.233	-.222	-.222	-.237	-.269
	.577	-.160	-.123	-.105	-.110	-.109	-.120	-.149
	.587	-.133	-.095	-.078	-.075	-.082	-.086	-.118
	.597	-.106	-.068	-.054	-.056	-.059	-.062	-.098
	.607	-.094	-.057	-.039	-.044	-.044	-.055	-.083
	.617	-.094	-.053	-.035	-.037	-.040	-.047	-.071
	.627	-.090	-.049	-.027	-.033	-.036	-.043	-.071
	.637	-.083	-.041	-.027	-.025	-.028	-.039	-.060
	.657	-.072	-.028	-.014	-.016	-.019	-.032	-.052
	.677	-.060	-.021	-.011	-.012	-.016	-.028	-.046
	.697	-.048	-.014	-.007	-.008	-.014	-.025	-.040
	.737	-.060	-.017	-.007	-.007	-.010	-.020	-.037
	.777	-.056	-.017	-.001	-.003	-.010	-.016	-.031
	.785	-.062	-.018	-.003	-.003	-.005	-.013	-.027
	.817	-.052	-.012	.002	.000	-.004	-.013	-.028
	.857	-.058	-.019	-.004	-.005	-.008	-.017	-.030
	.877	-.057	-.020	-.005	-.006	-.009	-.017	-.030
	.897	-.059	-.020	-.006	-.007	-.010	-.018	-.032
	.917	-.067	-.027	-.010	-.012	-.015	-.023	-.035
	.957	-.069	-.034	-.018	-.019	-.023	-.033	-.048
	.997	-.140	-.098	-.079	-.078	-.085	-.102	-.127

	x/l	C_p for - ϕ = -90°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.357	.388	.451	.465	.467	.449	.423	.351
	.377	.212	.267	.281	.290	.269	.243	.189
	.387	.100	.147	.165	.189	.153	.130	.081
Upper stage	.399	-1.418	-1.408	-1.386	-1.379	-1.379	-1.397	-1.410
	.419	-.182	-.156	-.181	-.198	-.212	-.187	-.209
	.439	-.090	-.010	.027	.029	.018	-.020	-.098
Transition flare	.459	.106	.158	.176	.159	.167	.141	.090
	.482	-.048	.020	.049	.052	.041	.015	-.037
	.512	-.095	-.026	.000	.006	-.005	-.028	-.080
Main stage	.552	-.161	-.100	-.074	-.080	-.087	-.113	-.161
	.568	-.419	-.328	-.279	-.273	-.299	-.341	-.404
	.587	-.164	-.103	-.078	-.079	-.086	-.101	-.156
	.607	-.129	-.068	-.043	-.044	-.047	-.066	-.125
	.627	-.114	-.053	-.031	-.033	-.036	-.055	-.110
	.657	-.105	-.040	-.018	-.017	-.023	-.046	-.093
	.697	-.096	-.034	-.013	-.012	-.018	-.038	-.087
	.737	-.088	-.031	-.008	-.007	-.013	-.034	-.080
	.777	-.084	-.027	-.007	-.004	-.018	-.030	-.077
	.785	-.089	-.028	-.007	-.003	-.010	-.026	-.071
	.817	-.079	-.021	.000	.001	-.004	-.023	-.067
	.857	-.081	-.028	-.005	-.004	-.010	-.029	-.072
	.897	-.081	-.031	-.008	-.007	-.012	-.033	-.076

TABLE 5.- PRESSURE COEFFICIENTS FOR CONFIGURATION 221 - Continued

(d) M = 1.00; α = -10° to 10°

	x/l	C_p for - ϕ = 0°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.357	.814	.730	.672	.610	.547	.488	.412
	.367	.731	.650	.592	.529	.470	.407	.331
	.377	.637	.560	.502	.445	.388	.328	.255
	.387	.544	.471	.413	.340	.306	.249	.179
Upper stage	.399	-.719	-.742	-.753	-.777	-.786	-.792	-.803
	.404	-.721	-.791	-.836	-.869	-.896	-.918	-.944
	.409	-.544	-.657	-.726	-.778	-.829	-.869	-.904
	.419	-.303	-.435	-.522	-.592	-.665	-.720	-.770
	.429	-.208	-.313	-.382	-.443	-.497	-.546	-.307
	.439	-.166	-.243	-.293	-.327	-.345	-.265	-.230
	.449	-.157	-.212	-.229	-.174	-.079	-.046	-.157
Transition flare	.459	.193	.159	.148	.127	.097	.045	-.069
	.482	.141	.122	.096	.091	.082	.075	.065
	.492	.129	.098	.072	.066	.057	.051	.059
	.512	.123	.089	.063	.051	.039	.027	.022
	.532	.120	.083	.048	.039	.021	.006	-.008
	.552	.096	.059	.027	.006	-.019	-.040	-.061
Main stage	.562	.005	-.024	-.056	-.081	-.108	-.130	-.147
	.568	-.207	-.251	-.287	-.311	-.332	-.345	-.343
	.577	-.189	-.239	-.271	-.283	-.283	-.289	-.288
	.587	-.146	-.193	-.222	-.234	-.240	-.252	-.251
	.597	-.115	-.159	-.191	-.200	-.203	-.209	-.199
	.607	-.106	-.147	-.170	-.169	-.163	-.166	-.152
	.617	-.109	-.137	-.148	-.145	-.135	-.136	-.125
	.627	-.109	-.119	-.130	-.120	-.111	-.108	-.103
	.637	-.084	-.097	-.105	-.099	-.089	-.092	-.088
	.657	-.069	-.077	-.081	-.074	-.068	-.071	-.064
	.677	-.047	-.061	-.068	-.068	-.055	-.064	-.049
	.697	-.029	-.048	-.058	-.058	-.006	-.047	-.024
	.737	.051	.037	.025	.026	.034	.017	.017
	.777	.066	.049	.042	.039	.034	.030	.025
	.785	.072	.054	.047	.040	.039	.039	.048
	.817	.068	.046	.036	.031	.024	.028	.029
	.857	.050	.028	.020	.016	.012	.013	.008
	.877	.050	.028	.018	.013	.009	.010	.003
	.897	.040	.020	.010	.006	.004	.003	-.006

	x/l	C_p for - ϕ = -30°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.367	.686	.626	.580	.523	.470	.410	.328
	.377	.612	.551	.502	.455	.396	.339	.278
	.387	.499	.447	.401	.354	.306	.255	.185
Upper stage	.399	-.775	-.788	-.793	-.805	-.814	-.832	-.852
	.404	-.760	-.819	-.854	-.882	-.905	-.924	-.944
	.409	-.589	-.685	-.747	-.796	-.838	-.869	-.904
	.419	-.318	-.435	-.510	-.577	-.634	-.686	-.739
	.429	-.236	-.325	-.388	-.446	-.494	-.537	-.334
	.439	-.205	-.264	-.305	-.336	-.354	-.311	-.240
	.449	-.178	-.212	-.217	-.165	-.089	-.059	-.160
Transition flare	.459	.172	.159	.151	.130	.106	.054	-.069
	.482	.114	.113	.093	.091	.082	.072	.064
	.492	.102	.089	.069	.066	.057	.048	.037
	.512	.096	.080	.060	.048	.036	.018	.001
	.532	.090	.071	.045	.036	.018	.000	-.027
	.552	.063	.046	.018	.006	-.019	-.043	-.079
Main stage	.562	-.004	-.024	-.056	-.081	-.108	-.139	-.175
	.566	-.253	-.270	-.290	-.302	-.320	-.335	-.343
	.577	-.219	-.248	-.277	-.283	-.289	-.305	-.312
	.587	-.173	-.205	-.228	-.237	-.249	-.262	-.266
	.597	-.115	-.134	-.151	-.157	-.157	-.166	-.162
	.607	-.146	-.162	-.173	-.173	-.169	-.172	-.168
	.617	-.142	-.150	-.154	-.145	-.135	-.139	-.137
	.627	-.142	-.137	-.136	-.123	-.111	-.120	-.122
	.637	-.118	-.113	-.111	-.102	-.095	-.102	-.109
	.657	-.099	-.089	-.085	-.075	-.071	-.081	-.090
	.677	-.062	-.061	-.065	-.064	-.052	-.069	-.071
	.697	-.052	-.057	-.061	-.058	-.011	-.057	-.053
	.737	.029	.027	.023	.028	.034	.011	-.017
	.777	.048	.046	.043	.042	.035	.023	-.007
	.785	.042	.045	.042	.040	.039	.026	.001
	.817	.042	.037	.034	.031	.023	.015	-.009
	.857	.023	.017	.016	.016	.010	.003	-.015
	.877	.020	.015	.012	.010	.006	-.002	-.017
	.897	.015	.010	.007	.005	.003	-.009	-.020
	.917	.012	.007	.003	.003	.000	-.012	-.022
	.957	.002	-.003	-.005	-.006	-.009	-.024	-.031
	.997	-.044	-.059	-.077	-.101	-.117	-.141	-.148

TABLE 3.- PRESSURE COEFFICIENTS FOR CONFIGURATION 221 - Continued

(d) M = 1.00; α = -10° to 10° - Concluded

	x/l	C_p for - ϕ = -60°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.367	.570	.569	.550	.520	.482	.440	.355
	.377	.502	.495	.475	.446	.411	.377	.293
	.387	.410	.403	.389	.357	.327	.300	.206
Upper stage	.399	-.704	-.702	-.709	-.722	-.755	-.768	-.791
	.404	-.806	-.825	-.845	-.863	-.881	-.896	-.919
	.409	-.641	-.706	-.744	-.787	-.820	-.851	-.883
	.419	-.437	-.505	-.552	-.586	-.619	-.640	-.660
	.429	-.339	-.377	-.415	-.446	-.479	-.506	-.523
	.439	-.300	-.307	-.321	-.336	-.360	-.384	-.291
	.449	-.272	-.252	-.226	-.168	-.125	-.122	-.163
Transition flare	.459	.048	.116	.133	.130	.109	.076	-.017
	.482	.029	.077	.081	.087	.076	.048	-.023
	.492	.014	.056	.060	.066	.054	.030	-.020
	.512	.017	.046	.048	.048	.033	.012	-.033
	.532	.008	.037	.033	.036	.018	-.003	-.054
	.552	-.032	.001	-.004	-.003	-.019	-.047	-.101
	.562	-.097	-.064	-.072	-.081	-.102	-.127	-.175
Main stage	.568	-.327	-.294	-.290	-.286	-.298	-.329	-.377
	.577	-.302	-.285	-.287	-.283	-.298	-.335	-.389
	.587	-.256	-.242	-.247	-.249	-.258	-.283	-.312
	.597	-.238	-.214	-.210	-.203	-.209	-.237	-.260
	.607	-.229	-.187	-.179	-.173	-.172	-.194	-.214
	.617	-.222	-.171	-.157	-.145	-.145	-.166	-.186
	.627	-.207	-.162	-.139	-.123	-.120	-.142	-.162
	.637	-.186	-.134	-.117	-.102	-.102	-.123	-.146
	.657	-.155	-.105	-.088	-.075	-.076	-.099	-.114
	.677	-.121	-.086	-.074	-.066	-.051	-.086	-.088
	.697	-.086	-.067	-.060	-.056	-.026	-.073	-.061
	.737	-.021	.015	.021	.026	.032	.006	-.012
	.777	-.012	.022	.035	.042	.032	.021	-.001
	.785	-.023	.016	.031	.039	.034	.019	.001
	.817	-.013	.017	.029	.032	.022	.013	-.003
	.857	-.033	-.003	.012	.016	.008	.000	-.012
	.877	-.034	-.005	.007	.010	.004	-.004	-.017
	.897	-.040	-.010	.003	.006	.001	-.010	-.021
	.917	-.050	-.019	-.006	.000	-.004	-.015	-.024
	.957	-.052	-.020	-.009	-.006	-.010	-.024	-.033
	.997	-.110	-.091	-.092	-.104	-.114	-.141	-.159

	x/l	C_p for - ϕ = -90°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.357	.529	.587	.606	.601	.589	.559	.495
	.377	.383	.432	.449	.455	.431	.407	.349
	.387	.294	.355	.359	.381	.345	.321	.272
Upper stage	.399	-.799	-.797	-.777	-.796	-.786	-.795	-.812
	.419	-.538	-.566	-.583	-.595	-.594	-.589	-.575
	.439	-.407	-.356	-.342	-.336	-.348	-.372	-.416
Transition flare	.459	.035	.104	.127	.133	.127	.100	.028
	.482	-.035	.049	.072	.087	.076	.048	-.042
	.512	-.054	.016	.036	.048	.039	.015	-.042
	.552	-.088	-.021	-.007	.003	-.006	-.031	-.092
Main stage	.568	-.432	-.386	-.379	-.373	-.391	-.415	-.475
	.587	-.327	-.276	-.256	-.249	-.258	-.292	-.346
	.607	-.269	-.205	-.182	-.169	-.175	-.209	-.272
	.627	-.235	-.162	-.136	-.120	-.126	-.163	-.229
	.657	-.168	-.108	-.088	-.076	-.082	-.117	-.173
	.697	-.117	-.081	-.066	-.057	-.040	-.094	-.127
	.737	-.046	.004	.019	.028	.030	-.003	-.045
	.777	-.039	.010	.029	.040	.029	.006	-.038
	.785	-.050	.005	.029	.040	.032	.010	-.029
	.817	-.036	.007	.027	.033	.023	.007	-.033
	.857	-.054	-.011	.010	.016	.006	-.012	-.052
	.897	-.065	-.021	-.001	.006	-.001	-.024	-.061

TABLE 1.- PRESSURE COEFFICIENTS FOR CONFIGURATION 221 - Continued

(e) $M = 1.20$; $\alpha = -10°$ to $10°$

		C_p for - $\beta = 0°$						
	x/l	$\alpha = -10°$	$\alpha = -6°$	$\alpha = -3°$	$\alpha = 0°$	$\alpha = 3°$	$\alpha = 6°$	$\alpha = 10°$
Nose	.357	.896	.805	.739	.675	.613	.561	.489
	.367	.832	.749	.691	.625	.560	.505	.433
	.377	.762	.684	.630	.567	.510	.457	.384
	.387	.692	.619	.569	.509	.459	.408	.335
Upper stage	.399	-.376	-.395	-.407	-.416	-.424	-.431	-.448
	.404	-.407	-.464	-.495	-.522	-.541	-.556	-.578
	.409	-.795	-.374	-.425	-.468	-.500	-.529	-.554
	.419	-.133	-.231	-.295	-.349	-.394	-.434	-.475
	.429	-.062	-.146	-.202	-.251	-.294	-.328	-.370
	.439	-.032	-.110	-.148	-.184	-.210	-.225	-.226
	.449	-.035	-.084	-.118	-.137	-.145	-.128	-.077
Transition flare	.459	.227	.162	.122	.106	.099	.089	.064
	.482	.151	.105	.095	.090	.093	.089	.080
	.492	.132	.094	.087	.076	.074	.070	.061
	.512	.124	.092	.089	.068	.055	.048	.034
	.532	.130	.100	.073	.063	.042	.032	.018
	.552	.146	.102	.076	.052	.037	.024	.010
	.562	.108	.067	.044	.017	-.007	-.022	-.029
Main stage	.568	-.041	-.082	-.103	-.125	-.146	-.153	-.168
	.577	-.057	-.104	-.130	-.139	-.149	-.145	-.151
	.587	-.035	-.082	-.100	-.111	-.121	-.115	-.119
	.597	-.025	-.066	-.079	-.087	-.100	-.099	-.102
	.607	-.016	-.052	-.065	-.073	-.080	-.082	-.080
	.617	-.011	-.044	-.062	-.068	-.070	-.066	-.067
	.627	-.011	-.052	-.057	-.057	-.059	-.055	-.056
	.637	.000	-.038	-.040	-.048	-.045	-.044	-.037
	.657	-.011	-.035	-.041	-.039	-.029	-.025	-.022
	.677	.001	-.010	-.028	-.026	-.025	-.017	-.018
	.697	.007	-.017	-.025	-.019	-.015	-.010	-.019
	.737	-.002	-.014	-.016	-.026	-.020	-.022	-.014
	.777	.025	-.006	-.026	-.018	-.021	-.025	-.006
	.785	.033	.000	-.011	-.012	-.016	-.009	-.006
	.817	.027	.002	.001	-.017	-.015	-.005	-.014
	.857	.023	.014	-.006	.000	.003	-.003	-.016
	.877	.035	.001	-.003	.002	-.001	-.001	-.018
	.897	.016	-.001	.002	-.002	-.007	-.011	-.023

		C_p for - $\beta = -5°$						
	x/l	$\alpha = -10°$	$\alpha = -6°$	$\alpha = -3°$	$\alpha = 0°$	$\alpha = 3°$	$\alpha = 6°$	$\alpha = 10°$
Nose	.367	.787	.722	.673	.620	.563	.511	.433
	.377	.734	.672	.625	.572	.523	.468	.407
	.387	.655	.595	.554	.503	.459	.415	.343
Upper stage	.399	-.434	-.441	-.443	-.445	-.456	-.477	-.500
	.404	-.445	-.491	-.514	-.533	-.549	-.561	-.581
	.409	-.331	-.404	-.446	-.482	-.508	-.529	-.559
	.419	-.138	-.222	-.278	-.327	-.367	-.407	-.451
	.429	-.090	-.157	-.206	-.254	-.291	-.320	-.356
	.439	-.070	-.122	-.159	-.192	-.215	-.233	-.258
	.449	-.049	-.087	-.113	-.129	-.139	-.141	-.120
Transition flare	.459	.219	.170	.136	.117	.101	.089	.058
	.482	.111	.092	.092	.090	.093	.083	.058
	.492	.100	.083	.084	.076	.074	.065	.040
	.512	.097	.083	.076	.065	.050	.038	.013
	.532	.100	.092	.071	.060	.042	.027	-.001
	.552	.111	.089	.071	.052	.034	.013	-.012
	.562	.092	.067	.044	.017	-.007	-.028	-.064
Main stage	.568	-.085	-.107	-.117	-.133	-.149	-.156	-.160
	.577	-.093	-.120	-.133	-.141	-.152	-.153	-.171
	.587	-.057	-.090	-.100	-.106	-.121	-.126	-.146
	.597	-.025	-.052	-.059	-.062	-.070	-.071	-.086
	.607	-.044	-.066	-.073	-.073	-.091	-.088	-.102
	.617	-.038	-.060	-.062	-.065	-.072	-.071	-.083
	.627	-.035	-.060	-.059	-.059	-.061	-.060	-.072
	.637	-.030	-.055	-.047	-.048	-.053	-.052	-.058
	.657	-.023	-.034	-.040	-.033	-.026	-.030	-.048
	.677	-.015	-.010	-.024	-.020	-.024	-.024	-.047
	.697	-.024	-.027	-.026	-.024	-.025	-.023	-.051
	.737	-.027	-.026	-.021	-.025	-.021	-.031	-.051
	.777	.002	-.009	-.021	-.013	-.018	-.027	-.033
	.785	.008	-.008	-.009	-.008	-.014	-.020	-.038
	.817	.002	-.011	-.003	-.016	-.015	-.022	-.044
	.857	-.003	.006	-.006	-.008	-.008	-.020	-.048
	.877	.005	-.010	-.005	-.001	-.003	-.017	-.043
	.897	-.008	-.009	-.001	.001	-.003	-.018	-.036
	.917	-.010	-.001	-.002	-.004	-.005	-.017	-.033
	.957	-.011	-.014	-.010	-.014	-.015	-.017	-.032
	.997	-.001	-.019	-.030	-.052	-.074	-.081	-.078

TABLE 5.- PRESSURE COEFFICIENTS FOR CONFIGURATION 221 - Concluded

(e) M = 1.20; $\alpha = -10^\circ$ to 10° - Concluded

	x/l	C_p for - $\eta = -65^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.367	.668	.664	.646	.617	.581	.543	.454
	.377	.620	.617	.599	.570	.542	.503	.417
	.387	.554	.553	.535	.517	.494	.458	.359
	.399	-.365	-.359	-.366	-.386	-.399	-.417	-.442
Upper stage	.404	-.489	-.499	-.509	-.522	-.530	-.545	-.568
	.409	-.375	-.418	-.444	-.476	-.495	-.518	-.546
	.419	-.239	-.285	-.316	-.341	-.356	-.374	-.402
	.429	-.176	-.201	-.230	-.257	-.278	-.298	-.332
	.439	-.147	-.160	-.175	-.192	-.210	-.231	-.277
	.449	-.130	-.125	-.132	-.135	-.150	-.176	-.248
Transition flare	.459	.076	.092	.095	.101	.085	.065	.007
	.482	.011	.059	.082	.087	.085	.062	.005
	.492	.006	.057	.076	.076	.072	.048	-.001
	.512	.019	.057	.073	.065	.050	.032	-.015
	.532	.024	.057	.060	.060	.042	.027	-.026
	.552	.016	.040	.044	.038	.029	.000	-.037
	.562	.000	.013	.017	.009	-.007	-.028	-.054
Main stage	.568	-.151	-.137	-.130	-.133	-.146	-.159	-.201
	.577	-.151	-.142	-.128	-.130	-.149	-.170	-.222
	.587	-.126	-.126	-.111	-.109	-.141	-.148	-.190
	.597	-.115	-.107	-.098	-.089	-.108	-.126	-.165
	.607	-.115	-.099	-.087	-.076	-.086	-.107	-.143
	.617	-.120	-.096	-.073	-.068	-.075	-.090	-.121
	.627	-.120	-.090	-.068	-.059	-.070	-.085	-.102
	.637	-.112	-.066	-.059	-.048	-.056	-.066	-.086
	.657	-.089	-.036	-.030	-.018	-.023	-.046	-.069
	.677	-.082	-.040	-.028	-.021	-.027	-.043	-.067
	.697	-.076	-.045	-.026	-.024	-.031	-.039	-.064
	.737	-.081	-.044	-.026	-.023	-.022	-.043	-.052
	.777	-.061	-.035	-.023	-.013	-.019	-.029	-.045
	.785	-.047	-.037	-.018	-.008	-.016	-.023	-.043
	.817	-.054	-.021	-.008	-.013	-.016	-.028	-.046
	.857	-.061	-.016	-.013	-.012	-.019	-.027	-.045
	.877	-.052	-.028	-.006	-.002	-.005	-.018	-.041
	.897	-.061	-.027	-.007	.002	-.001	-.014	-.032
	.917	-.069	-.030	-.015	-.005	-.008	-.018	-.028
	.957	-.068	-.033	-.013	-.013	-.017	-.017	-.033
	.997	-.062	-.045	-.040	-.053	-.068	-.088	-.102

	x/l	C_p for - $\eta = -90^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.357	.607	.654	.673	.670	.635	.638	.573
	.377	.504	.548	.567	.580	.560	.535	.478
	.387	.443	.511	.509	.533	.502	.482	.423
	.399	-.464	-.452	-.435	-.446	-.434	-.444	-.461
Upper stage	.419	-.323	-.336	-.341	-.349	-.343	-.339	-.348
	.439	-.236	-.201	-.192	-.192	-.194	-.204	-.248
Transition flare	.459	-.024	.059	.095	.106	.093	.059	-.039
	.482	-.047	.040	.076	.087	.082	.051	-.034
	.512	-.044	.030	.060	.065	.055	.038	-.029
	.552	-.038	.013	.044	.044	.039	.008	-.037
Main stage	.568	-.222	-.194	-.177	-.174	-.182	-.197	-.250
	.587	-.183	-.153	-.122	-.111	-.127	-.151	-.214
	.607	-.178	-.123	-.095	-.076	-.094	-.121	-.190
	.627	-.161	-.088	-.070	-.059	-.070	-.090	-.160
	.657	-.120	-.054	-.029	-.018	-.026	-.059	-.116
	.697	-.124	-.069	-.038	-.026	-.040	-.061	-.122
	.737	-.105	-.058	-.032	-.025	-.026	-.057	-.109
	.777	-.073	-.043	-.024	-.014	-.019	-.044	-.091
	.785	-.083	-.048	-.025	-.010	-.017	-.043	-.093
	.817	-.074	-.027	-.009	-.008	-.016	-.035	-.084
	.857	-.079	-.028	-.015	-.007	-.027	-.046	-.083
	.897	-.083	-.039	-.015	-.004	-.005	-.022	-.072

TABLE 4.- PRESSURE COEFFICIENTS FOR CONFIGURATION 321

(a) M = 0.40 to 0.95; $\alpha = 0^\circ$

	x/l	C_p for - $\phi = 0^\circ$					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.371	.492	.552	.575	.627	.658	.700
	.381	.338	.396	.421	.480	.514	.562
	.391	.085	.173	.209	.291	.336	.391
	.399	-1.404	-1.072	-1.042	-.835	-.973	-.836
Upper stage	.404	-.409	-.864	-.844	-.686	-.999	-1.114
	.409	-.172	-.631	-.669	-.643	-.689	-.996
	.419	-.060	-.204	-.319	-.522	-.481	-.772
	.429	-.004	-.042	-.094	-.346	-.322	-.593
	.439	.030	.022	.010	-.153	-.174	-.242
	.449	.075	.063	.068	-.024	-.040	.030
Transition flare	.459	.176	.145	.151	.080	.081	.151
	.482	.053	.054	.064	.090	.091	.153
	.492	.053	.036	.043	.069	.075	.118
	.512	.041	.013	.018	.040	.041	.071
	.532	.019	-.010	-.007	-.002	.001	.026
	.552	-.038	-.061	-.057	-.068	-.071	-.038
	.562	-.095	-.126	-.129	-.140	-.160	-.138
Main stage	.568	-.129	-.203	-.208	-.237	-.284	-.402
	.577	-.049	-.093	-.095	-.107	-.121	-.347
	.587	-.015	-.060	-.061	-.071	-.077	-.202
	.597	-.004	-.047	-.044	-.053	-.053	-.047
	.607	-.004	-.033	-.032	-.038	-.043	-.018
	.617	.008	-.028	-.028	-.031	-.036	-.018
	.627	.008	-.023	-.019	-.028	-.030	-.018
	.637	.019	-.014	-.015	-.020	-.019	-.015
	.657	.019	-.007	-.007	-.014	-.016	-.015
	.677	.019	-.007	-.005	-.013	-.015	-.015
	.697	.023	-.002	-.002	-.011	-.011	-.014
	.737	.023	.000	-.001	-.010	-.010	-.015
	.777	.027	.004	.003	-.005	-.006	-.013
	.785	.027	.007	.008	-.002	-.002	-.010
	.817	.028	.005	.007	-.001	-.002	-.009
	.857	.025	.001	.004	-.005	-.006	-.012
	.877	.025	.002	.004	-.004	-.006	-.012
	.897	.024	-.001	.001	-.007	-.008	-.015

	x/l	C_p for - $\phi = -30^\circ$					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.371	.492	.548	.575	.623	.655	.696
	.381	.288	.358	.392	.456	.494	.544
	.391	.085	.169	.209	.288	.333	.391
	.399	-1.483	-.961	-.941	-.861	-1.198	-1.045
Upper stage	.404	-.409	-.813	-.781	-.672	-.999	-1.114
	.409	-.172	-.644	-.656	-.626	-.676	-.999
	.419	-.060	-.229	-.352	-.504	-.484	-.763
	.429	-.004	-.032	-.102	-.335	-.326	-.593
	.439	.030	.027	.010	-.167	-.184	-.242
	.449	.075	.072	.072	-.045	-.053	.026
Transition flare	.459	.176	.154	.147	.069	.071	.151
	.482	.053	.054	.064	.090	.091	.153
	.492	.053	.036	.043	.069	.075	.118
	.512	.030	.013	.018	.026	.034	.068
	.532	.008	-.014	-.011	-.010	-.006	.023
	.552	-.038	-.061	-.057	-.068	-.071	-.038
	.562	-.095	-.126	-.129	-.148	-.167	-.145
Main stage	.568	-.129	-.185	-.191	-.219	-.267	-.395
	.577	-.049	-.093	-.095	-.107	-.121	-.347
	.587	-.026	-.060	-.061	-.075	-.077	-.208
	.597	-.004	-.037	-.032	-.038	-.040	-.031
	.607	-.004	-.033	-.032	-.038	-.043	-.021
	.617	.008	-.028	-.028	-.031	-.036	-.018
	.627	.008	-.023	-.019	-.028	-.030	-.018
	.637	.019	-.019	-.015	-.020	-.023	-.018
	.657	.015	-.008	-.008	-.017	-.018	-.015
	.677	.023	-.002	.001	-.008	-.010	-.013
	.697	.019	-.002	-.002	-.011	-.013	-.015
	.737	.023	.001	.001	.008	-.009	-.014
	.777	.027	.006	.006	-.002	-.004	-.010
	.785	.027	.007	.008	-.002	-.004	-.010
	.817	.028	.005	.007	-.001	-.003	-.008
	.857	.025	.001	.003	-.006	-.007	-.013
	.877	.025	.000	.002	-.006	-.007	-.014
	.897	.022	-.003	.000	-.009	-.009	-.016
	.917	.022	-.003	.000	-.009	-.011	-.016
	.957	.013	-.014	-.011	-.020	-.021	-.027
	.997	-.035	-.067	-.067	-.079	-.083	-.096

TABLE 4.- PRESSURE COEFFICIENTS FOR CONFIGURATION 321 - Continued

(a) M = 0.40 to 0.95; $\alpha = 0^{\circ}$ - Concluded

	x/l	C_p for - $\phi = -60^{\circ}$					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.371	.481	.548	.571	.616	.652	.690
	.381	.316	.387	.413	.466	.504	.553
	.391	.085	.173	.209	.284	.333	.388
	.399	-1.119	-1.012	-.903	-.821	-.809	-.719
Upper stage	.404	-.375	-.736	-.698	-.643	-.676	-1.085
	.409	-.184	-.640	-.656	-.618	-.656	-1.002
	.419	-.060	-.297	-.415	-.515	-.555	-.779
	.429	-.004	-.042	-.131	-.353	-.410	-.590
	.439	.030	.036	.014	-.185	-.252	-.216
	.449	.075	.068	.072	-.053	-.100	.007
Transition flare	.459	.165	.145	.143	.058	.028	.138
	.482	.053	.054	.064	.090	.098	.153
	.492	.041	.036	.043	.069	.081	.118
	.512	.030	.013	.018	.026	.038	.064
	.532	.008	-.014	-.011	-.013	-.006	.023
	.552	-.038	-.065	-.066	-.075	-.074	-.047
	.562	-.095	-.126	-.129	-.148	-.160	-.145
Main stage	.568	-.129	-.185	-.187	-.212	-.244	-.366
	.577	-.049	-.093	-.091	-.107	-.115	-.347
	.587	-.026	-.065	-.061	-.075	-.081	-.208
	.597	-.004	-.042	-.040	-.049	-.053	-.044
	.607	-.004	-.033	-.032	-.038	-.043	-.021
	.617	.008	-.028	-.028	-.035	-.036	-.018
	.627	.008	-.023	-.019	-.028	-.030	-.018
	.637	.019	-.019	-.015	-.020	-.023	-.018
	.657	.015	-.008	-.008	-.017	-.017	-.016
	.677	.019	-.004	-.005	-.013	-.014	-.015
	.697	.023	.000	-.002	-.010	-.010	-.014
	.737	.023	.003	.001	-.008	-.008	-.014
	.777	.027	.004	.005	-.004	-.005	-.010
	.785	.027	.006	.006	-.005	-.005	-.011
	.817	.028	.005	.008	-.001	-.001	-.008
	.857	.025	.001	.003	-.006	-.007	-.013
	.877	.024	.000	.002	-.006	-.007	-.014
	.897	.024	-.001	.001	-.008	-.008	-.015
	.917	.021	-.005	-.003	-.012	-.013	-.020
	.957	.013	-.014	-.011	-.020	-.021	-.027
	.997	-.039	-.067	-.067	-.081	-.086	-.098

	x/l	C_p for - $\phi = -90$					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.371	.481	.543	.567	.616	.649	.690
	.391	.085	.173	.209	.284	.333	.388
	.399	-.755	-.702	-.655	-.622	-.622	-.800
Upper stage	.419	-.037	-.357	-.473	-.540	-.548	-.763
	.439	.030	.036	-.002	-.224	-.295	-.200
Transition flare	.459	.165	.141	.139	.051	-.016	.131
	.482	.053	.054	.068	.090	.088	.153
	.512	.030	.013	.018	.026	.038	.064
	.552	-.038	-.065	-.062	-.071	-.074	-.044
Main stage	.568	-.151	-.217	-.221	-.248	-.261	-.473
	.587	-.026	-.065	-.065	-.075	-.081	-.208
	.607	-.004	-.033	-.032	-.038	-.043	-.021
	.627	.008	-.023	-.019	-.028	-.030	-.018
	.657	.015	-.010	-.008	-.017	-.017	-.016
	.697	.019	-.002	-.002	-.012	-.013	-.016
	.737	.023	.001	.002	-.007	-.008	-.013
	.777	.027	.004	.003	-.004	-.005	-.011
	.785	.027	.004	.003	-.004	-.004	-.011
	.817	.030	.007	.009	.001	.001	-.006
	.857	.025	.001	.004	-.005	-.006	-.013
	.897	.022	-.001	.001	-.008	-.009	-.016

TABLE -.- PRESSURE COEFFICIENTS FOR CONFIGURATION 321 - Continued

(b) $M = 0.60$; $\alpha = -10^\circ$ to 10°

	x/l	C_p for - $\phi = 0^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.371	.735	.655	.584	.523	.445	.381	.279
	.381	.584	.493	.428	.366	.289	.230	.139
	.391	.344	.248	.177	.126	.060	.018	-.046
	.399	-1.273	-1.344	-1.325	-1.204	-1.163	-.993	-.722
Upper stage	.404	-.430	-.649	-.785	-.819	-.830	-.753	-.629
	.409	-.110	-.192	-.287	-.408	-.510	-.570	-.623
	.419	-.019	-.055	-.070	-.082	-.144	-.204	-.314
	.429	.016	-.009	-.024	-.019	-.041	-.056	-.097
	.439	.055	.025	.016	.015	-.001	.001	-.006
	.449	.101	.077	.061	.061	.039	.036	.034
Transition flare	.459	.249	.207	.181	.157	.113	.093	.068
	.482	.129	.082	.055	.049	.016	.013	.006
	.492	.106	.059	.033	.038	.004	.001	-.017
	.512	.095	.037	.021	.026	-.007	-.010	-.046
	.532	.061	.020	-.007	-.008	-.042	-.045	-.058
	.552	.021	-.021	-.054	-.054	-.082	-.074	-.087
	.562	-.065	-.108	-.129	-.118	-.135	-.126	-.133
Main stage	.568	-.111	-.165	-.186	-.181	-.180	-.154	-.144
	.577	-.036	-.072	-.082	-.083	-.093	-.085	-.087
	.587	-.007	-.044	-.053	-.054	-.065	-.056	-.058
	.597	.004	-.032	-.042	-.043	-.053	-.045	-.046
	.607	.009	-.020	-.030	-.031	-.042	-.033	-.035
	.617	.015	-.020	-.025	-.025	-.036	-.027	-.029
	.627	.015	-.015	-.019	-.019	-.030	-.022	-.023
	.637	.026	-.003	-.013	-.014	-.024	-.016	-.017
	.657	.028	.001	-.013	-.002	-.019	-.006	-.010
	.677	.028	.001	-.013	.000	-.015	-.004	-.010
	.697	.031	.003	-.009	.004	-.013	-.002	-.008
	.737	.031	.005	-.007	.000	-.011	-.002	-.010
	.777	.035	.010	-.003	.004	-.009	.002	-.006
	.785	.039	.012	-.001	.006	-.005	.005	.002
	.817	.039	.017	.003	.008	-.004	.003	-.004
	.857	.033	.010	-.002	.005	-.007	-.001	-.011
	.877	.035	.012	-.002	.005	-.007	-.001	-.010
	.897	.031	.008	-.005	.002	-.010	-.004	-.014

	x/l	C_p for - $\phi = -30^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.371	.702	.633	.573	.517	.451	.386	.285
	.381	.504	.432	.372	.319	.255	.205	.116
	.391	.305	.231	.171	.121	.060	.024	-.052
	.399	-1.429	-1.361	-1.331	-1.354	-1.093	-.877	-.809
Upper stage	.404	-.379	-.655	-.750	-.739	-.836	-.765	-.720
	.409	-.127	-.226	-.339	-.379	-.561	-.593	-.612
	.419	-.053	-.066	-.076	-.088	-.139	-.199	-.274
	.429	-.007	-.020	-.024	-.019	-.036	-.050	-.086
	.439	.027	.014	.010	.015	-.001	.001	-.011
	.449	.095	.077	.067	.066	.044	.036	.028
Transition flare	.459	.232	.207	.181	.157	.118	.104	.091
	.482	.101	.082	.055	.049	.021	.013	.000
	.492	.089	.054	.033	.038	.004	.001	-.023
	.512	.067	.037	.021	.015	-.019	-.022	-.046
	.532	.044	.008	-.007	-.008	-.042	-.045	-.070
	.552	-.002	-.026	-.054	-.054	-.082	-.080	-.104
Main stage	.562	-.083	-.119	-.135	-.118	-.140	-.138	-.151
	.568	-.140	-.170	-.180	-.169	-.174	-.160	-.161
	.577	-.059	-.084	-.088	-.083	-.093	-.085	-.098
	.587	-.036	-.055	-.059	-.054	-.070	-.062	-.069
	.597	-.019	-.032	-.036	-.037	-.047	-.039	-.046
	.607	-.013	-.032	-.030	-.031	-.042	-.033	-.040
	.617	-.013	-.026	-.025	-.025	-.036	-.027	-.035
	.627	-.007	-.020	-.025	-.019	-.030	-.022	-.029
	.637	-.002	-.015	-.019	-.014	-.024	-.016	-.029
	.657	.001	-.011	-.019	-.002	-.019	-.012	-.025
	.677	.012	-.001	-.009	.002	-.017	-.004	-.021
	.697	.004	-.007	-.013	.002	-.015	-.008	-.023
	.737	.008	-.003	-.009	.002	-.011	-.004	-.023
	.777	.014	.003	-.005	.006	-.007	.000	-.021
	.785	.010	.001	-.005	.006	-.007	.000	-.019
	.817	.013	.006	-.002	.008	-.004	-.001	-.020
	.857	.007	-.001	-.006	.004	-.008	-.005	-.025
	.877	.007	-.001	-.006	.002	-.009	-.007	-.025
	.897	.004	-.003	-.008	.001	-.010	-.009	-.025
	.917	.004	-.004	-.009	.001	-.013	-.012	-.029
	.957	-.012	-.016	-.019	-.010	-.023	-.023	-.041
	.997	-.091	-.077	-.071	-.063	-.080	-.085	-.115

TABLE 4.- PRESSURE COEFFICIENTS FOR CONFIGURATION 321 - Continued

(b) M = 0.60; α = -10° to 10° - Concluded

	x/l	C_p for - ϕ = -60°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.371	.573	.572	.545	.517	.467	.420	.318
	.381	.423	.404	.378	.350	.305	.264	.173
	.391	.194	.170	.143	.121	.071	.046	-.029
	.399	-1.261	-1.292	-1.290	-1.198	-1.215	-1.183	-1.144
Upper stage	.404	-.533	-.632	-.722	-.722	-.721	-.713	-.732
	.409	-.242	-.289	-.373	-.448	-.504	-.530	-.554
	.419	-.139	-.112	-.104	-.105	-.139	-.113	-.143
	.429	-.076	-.049	-.030	-.019	-.036	-.050	-.109
	.439	-.030	-.003	.004	.021	.004	-.010	-.057
	.449	.010	.037	.050	.061	.039	.024	-.017
Transition flare	.459	.141	.156	.152	.152	.118	.104	.080
	.482	.021	.037	.038	.049	.021	.007	-.046
	.492	.004	.020	.021	.032	.004	-.010	-.058
	.512	-.002	.003	.004	.015	-.019	-.028	-.075
	.532	-.030	-.021	-.025	-.014	-.042	-.057	-.099
	.552	-.088	-.073	-.071	-.060	-.082	-.097	-.145
	.562	-.152	-.142	-.141	-.118	-.140	-.149	-.192
Main stage	.568	-.221	-.199	-.186	-.169	-.180	-.189	-.231
	.577	-.123	-.101	-.088	-.083	-.093	-.102	-.133
	.587	-.099	-.078	-.065	-.054	-.070	-.074	-.110
	.597	-.082	-.061	-.048	-.037	-.053	-.056	-.087
	.607	-.071	-.049	-.036	-.031	-.042	-.045	-.075
	.617	-.071	-.049	-.030	-.025	-.036	-.039	-.069
	.627	-.065	-.044	-.030	-.019	-.030	-.039	-.063
	.637	-.059	-.038	-.025	-.014	-.030	-.027	-.058
	.657	-.059	-.032	-.025	-.002	-.022	-.024	-.050
	.677	-.048	-.025	-.019	.000	-.019	-.021	-.044
	.697	-.036	-.019	-.013	.002	-.015	-.018	-.039
	.737	-.050	-.022	-.015	.002	-.015	-.016	-.033
	.777	-.046	-.020	-.011	.006	-.011	-.010	-.029
	.785	-.050	-.022	-.013	.006	-.011	-.010	-.027
	.817	-.044	-.014	-.005	.009	-.006	-.007	-.025
	.857	-.051	-.020	-.011	.004	-.010	-.010	-.026
	.877	-.049	-.020	-.011	.003	-.010	-.010	-.027
	.897	-.050	-.020	-.012	.002	-.012	-.013	-.028
	.917	-.059	-.028	-.017	-.003	-.017	-.016	-.032
	.957	-.064	-.034	-.025	-.010	-.025	-.026	-.042
	.997	-.128	-.096	-.085	-.064	-.082	-.092	-.120

	x/l	C_p for - ϕ = -[illegible]°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.371	.428	.488	.512	.517	.501	.476	.402
	.391	.071	.108	.121	.126	.110	.102	.050
	.399	-1.071	-1.055	-.932	-.753	-.718	-.756	-.930
Upper stage	.419	-.173	-.112	-.122	-.082	-.150	-.130	-.154
	.439	-.087	-.020	.010	.032	.010	-.016	-.086
Transition flare	.459	.084	.128	.146	.157	.130	.127	.058
	.482	-.042	.008	.033	.049	.021	.013	-.046
	.512	-.083	-.032	-.007	.015	-.013	-.028	-.081
	.552	-.135	-.090	-.077	-.060	-.082	-.097	-.151
Main stage	.568	-.324	-.257	-.226	-.204	-.232	-.270	-.334
	.587	-.134	-.090	-.071	-.060	-.076	-.085	-.144
	.607	-.105	-.061	-.042	-.031	-.047	-.056	-.115
	.627	-.099	-.055	-.030	-.019	-.036	-.045	-.104
	.657	-.090	-.044	-.026	-.002	-.022	-.037	-.092
	.697	-.084	-.040	-.021	-.002	-.020	-.031	-.085
	.737	-.078	-.036	-.017	.002	-.015	-.027	-.079
	.777	-.075	-.032	-.015	.006	-.017	-.024	-.073
	.785	-.077	-.034	-.015	.006	-.013	-.024	-.071
	.817	-.068	-.023	-.007	.009	-.006	-.019	-.066
	.857	-.072	-.027	-.011	.005	-.012	-.023	-.069
	.897	-.072	-.032	-.015	.001	-.015	-.026	-.072

TABLE 4.- PRESSURE COEFFICIENTS FOR CONFIGURATION 321 - Continued

(c) M = 0.80; α = -10° to 10°

	x/l	C_p for - ϕ = 0°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.371	.813	.728	.663	.600	.531	.457	.363
	.381	.663	.578	.513	.450	.385	.311	.221
	.391	.449	.364	.307	.251	.190	.134	.055
	.399	-1.143	-1.149	-.999	-1.103	-.934	-.568	-.471
Upper stage	.404	-.939	-.887	-.796	-.846	-.785	-.519	-.450
	.409	-.466	-.680	-.700	-.715	-.678	-.550	-.500
	.419	-.051	-.242	-.412	-.404	-.428	-.515	-.519
	.429	-.001	-.C30	-.136	-.181	-.224	-.354	-.370
	.439	.037	.027	.011	-.043	-.082	-.181	-.197
	.449	.095	.C81	.079	.046	.014	-.054	-.078
Transition flare	.459	.259	.211	.179	.134	.087	.026	.003
	.482	.140	.100	.083	.065	.056	.026	.022
	.492	.117	.081	.060	.042	.037	.011	.007
	.512	.C94	.C54	.045	.015	.006	-.008	-.032
	.532	.071	.027	.003	-.020	-.025	-.051	-.059
	.552	.018	-.023	-.048	-.074	-.076	-.098	-.102
	.562	-.091	-.120	-.137	-.148	-.126	-.137	-.137
Main stage	.568	-.176	-.232	-.234	-.229	-.195	-.175	-.160
	.577	-.059	-.C93	-.098	-.105	-.098	-.101	-.101
	.587	-.024	-.C58	-.059	-.070	-.067	-.074	-.070
	.597	-.009	-.C38	-.044	-.051	-.052	-.058	-.055
	.607	-.002	-.027	-.032	-.043	-.040	-.047	-.043
	.617	.002	-.023	-.028	-.035	-.032	-.039	-.039
	.627	.010	-.C19	-.020	-.027	-.029	-.035	-.032
	.637	.017	-.007	-.013	-.020	-.021	-.027	-.028
	.657	.024	-.C02	-.009	-.016	-.011	-.020	-.017
	.677	.C24	.002	-.007	-.016	-.011	-.018	-.017
	.697	.026	.C03	-.005	-.012	-.008	-.016	-.016
	.737	.027	.C03	-.004	-.012	-.007	-.015	-.017
	.777	.030	.C10	.000	-.007	-.005	-.011	-.016
	.785	.037	.C14	.003	-.004	.000	-.005	-.006
	.817	.038	.C13	.006	-.003	.002	-.008	-.011
	.857	.029	.C08	.001	-.006	-.002	-.013	-.020
	.877	.033	.C09	.002	-.006	-.002	-.012	-.019
	.897	.028	.C04	-.002	-.009	-.004	-.016	-.025

	x/l	C_p for - ϕ = -30°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.371	.775	.709	.655	.592	.539	.461	.367
	.381	.595	.527	.477	.420	.366	.300	.215
	.391	.415	.345	.299	.247	.194	.138	.063
	.399	-1.427	-1.173	-.926	-1.006	-.775	-.571	-.525
Upper stage	.404	-.823	-.849	-.785	-.796	-.678	-.550	-.516
	.409	-.524	-.684	-.700	-.665	-.624	-.577	-.554
	.419	-.093	-.272	-.424	-.434	-.459	-.531	-.535
	.429	-.028	-.050	-.139	-.212	-.251	-.346	-.362
	.439	.010	.012	.003	-.058	-.101	-.173	-.193
	.449	.083	.081	.079	.038	.002	-.043	-.074
Transition flare	.459	.248	.211	.175	.118	.079	.038	.003
	.482	.110	.092	.C83	.065	.056	.026	.011
	.492	.090	.069	.056	.C42	.037	.011	-.005
	.512	.068	.046	.026	.007	.006	-.024	-.036
	.532	.048	.019	-.001	-.020	-.029	-.059	-.075
	.552	-.005	-.035	-.052	-.074	-.076	-.102	-.118
	.562	-.110	-.136	-.145	-.152	-.134	-.160	-.176
Main stage	.568	-.203	-.232	-.226	-.209	-.184	-.183	-.194
	.577	-.086	-.104	-.098	-.105	-.098	-.105	-.113
	.587	-.055	-.069	-.063	-.070	-.071	-.082	-.082
	.597	-.024	-.038	-.C36	-.039	-.040	-.047	-.051
	.607	-.028	-.038	-.036	-.043	-.040	-.051	-.055
	.617	-.021	-.031	-.028	-.035	-.032	-.043	-.051
	.627	-.017	-.027	-.024	-.C31	-.029	-.039	-.043
	.637	-.009	-.023	-.016	-.023	-.021	-.031	-.039
	.657	-.004	-.012	-.C14	-.C18	-.013	-.022	-.034
	.677	.007	-.001	-.005	-.009	-.008	-.018	-.029
	.697	.000	-.007	-.009	-.012	-.008	-.020	-.032
	.737	.003	-.003	-.005	-.009	-.007	-.017	-.030
	.777	.012	.003	.000	-.004	-.003	-.012	-.028
	.785	.005	-.001	-.001	-.C04	.000	-.009	-.023
	.817	.012	.003	.003	-.002	.001	-.011	-.026
	.857	.003	-.004	-.003	-.007	-.003	-.016	-.031
	.877	.003	-.005	-.004	-.008	-.004	-.017	-.032
	.897	.001	-.006	-.C05	-.010	-.006	-.019	-.033
	.917	.000	-.007	-.006	-.010	-.007	-.021	-.035
	.957	-.014	-.019	-.015	-.021	-.019	-.033	-.048
	.997	-.093	-.083	-.073	-.079	-.080	-.100	-.124

TABLE -.- PRESSURE COEFFICIENTS FOR CONFIGURATION 321 - Continued

(c) M = 0.80; α = -10° to 10° - Concluded

	x/l	C_p for - ϕ = -60°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.371	.648	.645	.629	.592	.554	.495	.393
	.381	.505	.492	.475	.438	.404	.348	.262
	.391	.314	.293	.273	.247	.212	.164	.089
Upper stage	.399	-1.003	-.951	-.957	-.847	-.802	-.929	-.910
	.404	-.854	-.780	-.743	-.669	-.655	-.730	-.746
	.409	-.612	-.718	-.677	-.665	-.609	-.596	-.604
	.419	-.297	-.372	-.424	-.527	-.474	-.454	-.439
	.429	-.109	-.142	-.193	-.262	-.263	-.281	-.300
	.439	-.063	-.023	-.028	-.062	-.094	-.135	-.177
	.449	-.009	.039	.053	.038	.006	-.035	-.078
Transition flare	.459	.140	.157	.141	.122	.083	.049	.026
	.482	.022	.058	.068	.065	.060	.019	-.040
	.492	.006	.035	.045	.042	.037	.003	-.055
	.512	-.009	.012	.018	.007	.002	-.031	-.075
	.532	-.032	-.015	-.013	-.020	-.029	-.063	-.106
	.552	-.099	-.077	-.075	-.078	-.079	-.117	-.157
	.562	-.181	-.159	-.153	-.152	-.142	-.180	-.223
Main stage	.568	-.288	-.255	-.222	-.206	-.195	-.225	-.268
	.577	-.148	-.124	-.102	-.101	-.098	-.120	-.148
	.587	-.117	-.093	-.075	-.074	-.071	-.093	-.121
	.597	-.098	-.069	-.051	-.051	-.052	-.066	-.094
	.607	-.086	-.058	-.040	-.043	-.040	-.058	-.082
	.617	-.083	-.054	-.032	-.035	-.036	-.055	-.074
	.627	-.079	-.050	-.028	-.031	-.029	-.047	-.074
	.637	-.071	-.042	-.020	-.023	-.021	-.039	-.063
	.657	-.066	-.034	-.018	-.018	-.017	-.034	-.055
	.677	-.054	-.027	-.013	-.014	-.014	-.031	-.051
	.697	-.041	-.019	-.009	-.011	-.011	-.028	-.046
	.737	-.054	-.025	-.009	-.009	-.008	-.022	-.039
	.777	-.050	-.019	-.005	-.005	-.005	-.018	-.034
	.785	-.056	-.025	-.007	-.005	-.003	-.017	-.033
	.817	-.047	-.017	-.002	-.002	.000	-.016	-.030
	.857	-.053	-.024	-.008	-.007	-.005	-.020	-.033
	.877	-.052	-.024	-.008	-.008	-.005	-.021	-.034
	.897	-.055	-.024	-.007	-.009	-.006	-.021	-.035
	.917	-.060	-.032	-.015	-.013	-.011	-.025	-.040
	.957	-.066	-.036	-.021	-.021	-.020	-.035	-.050
	.997	-.134	-.103	-.085	-.081	-.082	-.105	-.129

	x/l	C_p for - ϕ = -90°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.371	.505	.567	.592	.592	.584	.555	.487
	.391	.194	.229	.250	.247	.235	.217	.168
Upper stage	.399	-.801	-.753	-.720	-.641	-.689	-.746	-.782
	.419	-.470	-.518	-.535	-.538	-.493	-.477	-.485
	.439	-.143	-.088	-.066	-.108	-.090	-.093	-.135
Transition flare	.459	.060	.115	.125	.111	.117	.103	.061
	.482	-.044	.031	.068	.068	.067	.019	-.044
	.512	-.083	-.019	.007	.007	.010	-.028	-.083
Main stage	.552	-.145	-.097	-.075	-.078	-.076	-.113	-.161
	.568	-.400	-.325	-.265	-.237	-.269	-.338	-.412
	.587	-.148	-.104	-.075	-.074	-.079	-.109	-.160
	.607	-.117	-.069	-.040	-.043	-.040	-.070	-.121
	.627	-.106	-.058	-.028	-.031	-.029	-.058	-.109
	.657	-.096	-.044	-.022	-.020	-.017	-.047	-.098
	.697	-.089	-.040	-.016	-.013	-.012	-.042	-.089
	.737	-.083	-.034	-.013	-.009	-.009	-.035	-.084
	.777	-.078	-.031	-.009	-.007	-.007	-.031	-.078
	.785	-.081	-.034	-.011	-.007	-.009	-.031	-.074
	.817	-.071	-.024	-.003	-.001	.000	-.026	-.071
	.857	-.075	-.031	-.008	-.006	-.005	-.032	-.075
	.897	-.078	-.035	-.012	-.009	-.008	-.034	-.078

TABLE 4.- PRESSURE COEFFICIENTS FOR CONFIGURATION 321 - Continued

(d) M = 1.00; α = -10° to 10°

	x/l	C_p for - ϕ = 0°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.371	.942	.867	.807	.747	.677	.610	.518
	.381	.811	.733	.670	.616	.551	.482	.399
	.391	.641	.563	.506	.455	.399	.341	.268
Upper stage	.399	-.667	-.686	-.702	-.715	-.730	-.745	-.766
	.404	-.821	-.904	-.948	-.985	-1.018	-1.042	-1.035
	.409	-.607	-.733	-.811	-.875	-.930	-.972	-.907
	.419	-.330	-.489	-.582	-.667	-.743	-.810	-.602
	.429	-.226	-.343	-.426	-.499	-.569	-.627	-.510
	.439	-.174	-.263	-.322	-.371	-.398	-.249	-.391
	.449	-.165	-.230	-.252	-.197	-.095	-.096	-.254
Transition flare	.459	.195	.133	.123	.108	.066	-.014	-.126
	.482	.128	.106	.096	.087	.078	.075	.039
	.492	.110	.087	.075	.066	.060	.056	.048
	.512	.113	.081	.065	.054	.042	.032	.024
	.532	.119	.078	.05-	.038	.024	.008	-.007
	.552	.097	.054	.029	.008	-.019	-.042	-.062
Main stage	.562	.009	-.028	-.051	-.079	-.109	-.132	-.152
	.568	-.206	-.253	-.282	-.312	-.337	-.334	-.330
	.577	-.188	-.238	-.263	-.278	-.275	-.266	-.265
	.587	-.141	-.195	-.217	-.229	-.232	-.235	-.225
	.597	-.117	-.161	-.186	-.195	-.195	-.192	-.176
	.607	-.108	-.148	-.165	-.161	-.155	-.152	-.139
	.617	-.108	-.139	-.143	-.134	-.124	-.121	-.114
	.627	-.086	-.124	-.125	-.112	-.102	-.097	-.096
	.637	-.062	-.099	-.100	-.091	-.084	-.078	-.081
	.657	-.041	-.074	-.075	-.066	-.047	-.060	-.045
	.677	-.024	-.058	-.068	-.040	.008	-.040	-.015
	.697	.066	-.047	-.056	.028	.034	.007	.012
	.737	.070	.049	.033	.042	.042	.036	.029
	.777	.077	.052	.046	.043	.042	.037	.029
	.785	.070	.057	.047	.049	.050	.044	.045
	.817	.051	.049	.040	.028	.022	.027	.021
	.857	.051	.030	.023	.014	.012	.013	.001
	.877	.040	.029	.019	.012	.010	.011	.000
	.897		.018	.012	.008	.008	.005	-.008

	x/l	C_p for - ϕ = -30°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.371	.910	.852	.795	.744	.680	.616	.521
	.381	.758	.700	.647	.598	.544	.487	.396
	.391	.606	.548	.500	.452	.408	.347	.271
Upper stage	.399	-.877	-.893	-.906	-.915	-.918	-.927	-.945
	.404	-.843	-.908	-.948	-.985	-1.018	-1.045	-1.071
	.409	-.653	-.761	-.823	-.878	-.933	-.972	-1.004
	.419	-.354	-.492	-.579	-.652	-.716	-.777	-.644
	.429	-.253	-.361	-.432	-.505	-.557	-.609	-.464
	.439	-.213	-.288	-.334	-.377	-.401	-.298	-.358
	.449	-.183	-.230	-.243	-.191	-.102	-.096	-.223
Transition flare	.459	.177	.136	.129	.111	.069	-.001	-.101
	.482	.094	.096	.096	.087	.078	.068	.018
	.492	.082	.078	.075	.066	.060	.053	.027
	.512	.088	.072	.059	.050	.039	.026	.009
	.532	.088	.066	.050	.038	.021	.005	-.022
	.552	.067	.042	.023	-.054	-.019	-.042	-.075
Main stage	.562	.000	-.028	-.079	-.303	-.169	-.141	-.171
	.568	-.252	-.269	-.285	-.282	-.324	-.331	-.351
	.577	-.218	-.253	-.269	-.235	-.284	-.285	-.308
	.587	-.172	-.207	-.223	-.149	-.241	-.245	-.244
	.597	-.117	-.136	-.149	-.149	-.149	-.152	-.139
	.607	-.144	-.164	-.171	-.164	-.158	-.158	-.148
	.617	-.141	-.152	-.146	-.134	-.127	-.125	-.127
	.627	-.144	-.139	-.128	-.112	-.102	-.103	-.111
	.637	-.123	-.111	-.106	-.094	-.087	-.091	-.099
	.657	-.091	-.084	-.081	-.068	-.051	-.069	-.076
	.677	-.057	-.059	-.062	-.036	.011	-.047	-.046
	.697	-.050	-.056	-.057	.029	.031	-.001	-.020
	.737	.044	.041	.033	.043	.042	.030	-.007
	.777	.053	.048	.046	.046	.044	.031	-.005
	.785	.047	.045	.046	.050	.050	.032	.006
	.817	.044	.040	.037	.028	.020	.016	-.009
	.857	.023	.019	.013	.013	.010	.004	-.015
	.877	.019	.015	.008	.009	.008	.000	-.017
	.897	.014	.008	.008	.009	.007	-.004	-.020
	.917	.012	.007	.006	.001	.006	-.006	-.021
	.957	.004	-.001	-.003	-.004	-.004	-.018	-.031
	.997	-.042	-.057	-.075	-.093	-.111	-.133	-.150

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 321 - Continued

(d) M = 1.00; α = -10° to 10° - Concluded

	x/l	C_p for - ϕ = -60°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.371	.790	.792	.768	.735	.698	.648	.551
	.381	.665	.658	.637	.601	.566	.520	.434
	.391	.507	.500	.476	.452	.420	.377	.303
Upper stage	.399	-.555	-.566	-.588	-.603	-.622	-.643	-.685
	.404	-.885	-.917	-.936	-.957	-.979	-1.003	-1.032
	.409	-.742	-.801	-.841	-.899	-.927	-.942	-.962
	.419	-.497	-.584	-.631	-.670	-.704	-.719	-.711
	.429	-.363	-.419	-.460	-.499	-.538	-.569	-.483
	.439	-.314	-.333	-.350	-.374	-.398	-.404	-.342
	.449	-.281	-.275	-.249	-.181	-.135	-.133	-.235
Transition flare	.459	.064	.085	.105	.102	.057	.017	-.052
	.482	-.003	.060	.081	.087	.078	.047	-.047
	.492	-.009	.048	.065	.066	.060	.035	-.038
	.512	.006	.042	.050	.050	.039	.014	-.038
	.532	.006	.030	.038	.038	.021	-.004	-.056
Main stage	.552	-.031	-.004	.002	-.001	-.019	-.045	-.100
	.562	-.096	-.069	-.066	-.079	-.103	-.128	-.177
	.568	-.323	-.296	-.288	-.288	-.300	-.325	-.373
	.577	-.299	-.284	-.282	-.282	-.290	-.331	-.398
	.587	-.255	-.244	-.239	-.242	-.247	-.272	-.318
	.597	-.237	-.216	-.202	-.201	-.204	-.220	-.247
	.607	-.228	-.192	-.174	-.164	-.164	-.180	-.198
	.617	-.228	-.173	-.152	-.134	-.133	-.152	-.170
	.627	-.209	-.158	-.134	-.112	-.112	-.131	-.151
	.637	-.178	-.133	-.109	-.094	-.093	-.112	-.136
	.657	-.148	-.101	-.083	-.068	-.062	-.088	-.103
	.677	-.114	-.082	-.070	-.049	-.045	-.054	-.062
	.697	-.080	-.063	-.057	.030	.027	-.021	-.020
	.737	-.010	.022	.030	.044	.040	.023	.001
	.777	-.008	.025	.040	.046	.044	.024	.002
	.785	-.022	.019	.039	.048	.046	.026	.005
	.817	-.012	.019	.032	.029	.020	.015	-.006
	.857	-.034	-.001	.014	.013	.007	.001	-.016
	.877	-.037	-.006	.009	.010	.007	.002	-.019
	.897	-.040	-.011	.004	.010	.006	.005	-.021
	.917	-.051	-.019	-.004	.006	.003	-.010	-.025
	.957	-.050	-.019	-.006	.002	-.004	-.018	-.032
	.997	-.110	-.091	-.090	-.096	-.109	-.133	-.154

	x/l	C_p for - ϕ = -90°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.371	.653	.715	.735	.735	.727	.702	.637
	.391	.394	.438	.452	.452	.444	.425	.378
	.399	-.697	-.680	-.684	-.681	-.680	-.665	-.667
Upper stage	.419	-.614	-.639	-.649	-.661	-.661	-.655	-.632
	.439	-.397	-.395	-.380	-.374	-.386	-.404	-.428
Transition flare	.459	.003	.069	.084	.099	.085	.063	-.007
	.482	-.086	.033	.075	.087	.078	.044	-.069
	.512	-.065	.009	.041	.050	.042	.017	-.050
Main stage	.552	-.083	-.025	-.001	.002	-.004	-.029	-.097
	.568	-.434	-.392	-.377	-.374	-.386	-.411	-.468
	.587	-.329	-.278	-.251	-.242	-.253	-.285	-.342
	.607	-.280	-.201	-.174	-.161	-.167	-.198	-.274
	.627	-.212	-.158	-.128	-.112	-.118	-.152	-.213
	.657	-.166	-.109	-.084	-.068	-.073	-.107	-.165
	.697	-.089	-.068	-.061	.027	.018	-.063	-.086
	.737	-.039	.011	.028	.044	.038	.013	-.033
	.777	-.038	.013	.037	.046	.041	.013	-.034
	.785	-.050	.008	.035	.048	.044	.017	-.028
	.817	-.038	.008	.030	.030	.020	.007	-.039
	.857	-.058	-.011	.011	.013	.006	-.011	-.057
	.897	-.068	-.022	.001	.010	.003	-.020	-.062

TABLE 4.- PRESSURE COEFFICIENTS FOR CONFIGURATION 321 - Continued

(e) M = 1.20; $\alpha = -10^\circ$ to 10°

	x/l	C_p for - $\phi = 0^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.371	1.071	.992	.929	.870	.805	.739	.654
	.381	.951	.873	.812	.756	.696	.633	.551
	.391	.803	.732	.677	.624	.574	.519	.450
Upper stage	.399	-.333	-.352	-.370	-.368	-.381	-.396	-.416
	.404	-.496	-.560	-.597	-.627	-.654	-.672	-.694
	.409	-.341	-.441	-.499	-.548	-.588	-.620	-.653
	.419	-.148	-.267	-.339	-.404	-.461	-.512	-.566
	.429	-.066	-.164	-.230	-.293	-.347	-.389	-.444
	.439	-.031	-.112	-.165	-.211	-.246	-.270	-.265
	.449	-.023	-.090	-.130	-.152	-.167	-.150	-.080
Transition flare	.459	.229	.154	.109	.087	.074	.064	.031
	.482	.148	.099	.090	.087	.090	.088	.080
	.492	.126	.089	.082	.076	.074	.069	.066
	.512	.115	.086	.076	.073	.053	.048	.039
	.532	.126	.099	.073	.065	.044	.037	.023
	.552	.139	.105	.076	.052	.036	.021	.012
	.562	.107	.070	.044	.017	-.010	-.026	-.032
Main stage	.568	-.039	-.077	-.104	-.126	-.147	-.157	-.169
	.577	-.053	-.102	-.120	-.137	-.144	-.138	-.141
	.587	-.028	-.080	-.098	-.112	-.117	-.113	-.119
	.597	-.023	-.064	-.079	-.087	-.095	-.094	-.100
	.607	-.012	-.050	-.063	-.073	-.078	-.078	-.078
	.617	-.009	-.047	-.060	-.065	-.065	-.061	-.064
	.627	-.007	-.047	-.052	-.060	-.056	-.050	-.053
	.637	.004	-.036	-.038	-.046	-.043	-.042	-.034
	.657	-.007	-.034	-.039	-.037	-.030	-.025	-.022
	.677	.003	-.011	-.028	-.024	-.027	-.015	-.017
	.697	.016	-.018	-.023	-.020	-.014	-.009	-.021
	.737	.003	-.012	-.014	-.026	-.022	-.022	-.009
	.777	.027	-.006	-.025	-.019	-.024	-.025	-.001
	.785	.036	.001	-.014	-.013	-.018	-.008	-.005
	.817	.029	.002	.000	-.018	-.016	-.007	-.006
	.857	.026	.015	-.005	-.001	.002	-.005	-.015
	.877	.036	.001	-.003	.001	-.002	-.003	-.017
	.897	.018	-.001	.003	-.003	-.008	-.013	-.023

	x/l	C_p for - $\phi = -30^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.371	1.034	.976	.924	.870	.813	.750	.659
	.381	.901	.846	.795	.747	.695	.639	.557
	.391	.768	.716	.666	.624	.577	.527	.455
Upper stage	.399	-.498	-.506	-.519	-.530	-.532	-.553	-.567
	.404	-.509	-.563	-.597	-.624	-.654	-.675	-.697
	.409	-.387	-.465	-.513	-.556	-.594	-.623	-.656
	.419	-.153	-.253	-.323	-.385	-.439	-.484	-.539
	.429	-.091	-.177	-.239	-.293	-.338	-.378	-.417
	.439	-.069	-.134	-.179	-.217	-.249	-.272	-.300
	.449	-.047	-.093	-.124	-.146	-.165	-.167	-.134
Transition flare	.459	.224	.165	.122	.098	.082	.070	.012
	.482	.107	.083	.087	.087	.090	.080	.056
	.492	.094	.078	.079	.076	.074	.064	.045
	.512	.085	.081	.076	.065	.053	.040	.023
	.532	.096	.089	.071	.060	.044	.032	.004
	.552	.107	.091	.071	.049	.034	.016	-.004
	.562	.091	.070	.044	.017	-.010	-.031	-.059
Main stage	.568	-.083	-.105	-.115	-.134	-.147	-.157	-.163
	.577	-.075	-.116	-.128	-.139	-.147	-.146	-.163
	.587	-.053	-.085	-.098	-.106	-.117	-.121	-.141
	.597	-.023	-.047	-.054	-.060	-.065	-.064	-.078
	.607	-.039	-.061	-.068	-.076	-.078	-.086	-.097
	.617	-.034	-.053	-.060	-.065	-.070	-.069	-.081
	.627	-.034	-.058	-.054	-.060	-.059	-.058	-.067
	.637	-.028	-.053	-.046	-.049	-.048	-.047	-.053
	.657	-.021	-.034	-.039	-.035	-.027	-.027	-.046
	.677	-.013	-.011	-.022	-.021	-.025	-.023	-.047
	.697	-.023	-.026	-.024	-.022	-.023	-.023	-.051
	.737	-.023	-.024	-.018	-.024	-.022	-.030	-.048
	.777	.005	-.009	-.021	-.014	-.022	-.027	-.053
	.785	.010	-.009	-.014	-.009	-.014	-.020	-.038
	.817	.003	-.011	-.004	-.017	-.016	-.023	-.050
	.857	-.001	-.007	-.005	-.008	-.007	-.021	-.048
	.877	.007	-.009	-.004	-.002	-.004	-.018	-.043
	.897	-.007	-.009	-.002	.000	-.004	-.020	-.035
	.917	-.004	-.004	-.002	-.005	-.006	-.018	-.031
	.957	-.009	-.014	-.010	-.015	-.016	-.018	-.028
	.997	.008	-.018	-.031	-.054	-.077	-.083	-.076

TABLE 4.- PRESSURE COEFFICIENTS FOR CONFIGURATION 321 - Concluded

(e) M = 1.20; $\alpha = -10^\circ$ to 10° - Concluded

	x/l	C_p for - $\phi = -60^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.371	.922	.918	.897	.868	.832	.777	.691
	.381	.811	.798	.778	.748	.717	.668	.588
	.391	.673	.668	.650	.624	.593	.554	.484
Upper stage	.399	-.240	-.253	-.280	-.288	-.301	-.314	-.347
	.404	-.563	-.585	-.600	-.616	-.626	-.645	-.670
	.409	-.438	-.492	-.526	-.559	-.583	-.601	-.621
	.419	-.286	-.338	-.374	-.404	-.428	-.444	-.452
	.429	-.183	-.226	-.260	-.293	-.325	-.346	-.376
	.439	-.153	-.172	-.195	-.217	-.241	-.264	-.308
	.449	-.131	-.134	-.143	-.154	-.173	-.202	-.276
Transition flare	.459	.078	.078	.084	.079	.055	.032	-.026
	.482	.002	.051	.076	.087	.082	.056	-.010
	.492	-.007	.051	.073	.076	.074	.048	-.010
	.512	.010	.056	.071	.065	.053	.032	-.012
	.532	.021	.056	.060	.060	.044	.021	-.023
	.552	.021	.043	.044	.041	.026	.002	-.032
	.562	.007	.016	.019	.006	-.007	-.028	-.062
Main stage	.568	-.141	-.135	-.128	-.134	-.141	-.157	-.199
	.577	-.144	-.135	-.126	-.128	-.144	-.168	-.223
	.587	-.124	-.121	-.106	-.106	-.125	-.143	-.188
	.597	-.113	-.102	-.093	-.087	-.103	-.121	-.160
	.607	-.116	-.094	-.084	-.076	-.084	-.102	-.136
	.617	-.116	-.091	-.071	-.065	-.073	-.086	-.114
	.627	-.122	-.085	-.063	-.060	-.065	-.080	-.100
	.637	-.111	-.064	-.052	-.049	-.051	-.064	-.078
	.657	-.089	-.034	-.031	-.019	-.026	-.044	-.069
	.677	-.081	-.039	-.028	-.021	-.030	-.042	-.066
	.697	-.073	-.044	-.025	-.024	-.034	-.039	-.064
	.737	-.081	-.044	-.025	-.025	-.024	-.043	-.050
	.777	-.051	-.035	-.023	-.014	-.022	-.029	-.044
	.785	-.047	-.034	-.017	-.009	-.017	-.024	-.043
	.817	-.051	-.023	-.009	-.014	-.016	-.029	-.044
	.857	-.059	-.015	-.013	-.013	-.020	-.029	-.044
	.877	-.048	-.027	-.005	-.003	-.006	-.020	-.038
	.897	-.061	-.028	-.008	.001	-.002	-.014	-.029
	.917	-.065	-.031	-.015	-.005	-.008	-.018	-.026
	.957	-.065	-.039	-.013	-.014	-.018	-.017	-.030
	.997	-.056	-.046	-.040	-.054	-.069	-.089	-.100

	x/l	C_p for - $\phi = -90^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.371	.784	.843	.865	.865	.858	.832	.774
	.391	.564	.610	.624	.624	.617	.599	.551
Upper stage	.399	-.336	-.330	-.324	-.313	-.304	-.300	-.312
	.419	-.371	-.384	-.388	-.396	-.398	-.392	-.387
	.439	-.246	-.221	-.217	-.217	-.224	-.232	-.262
Transition flare	.459	-.045	.037	.068	.090	.066	.032	-.064
	.482	-.070	.035	.076	.087	.080	.043	-.057
	.512	-.054	.029	.057	.065	.055	.037	-.032
	.552	-.034	.018	.038	.044	.039	.010	-.032
Main stage	.568	-.215	-.190	-.175	-.175	-.180	-.195	-.251
	.587	-.182	-.146	-.117	-.109	-.122	-.149	-.212
	.607	-.176	-.118	-.087	-.076	-.086	-.116	-.188
	.627	-.157	-.085	-.065	-.060	-.065	-.088	-.158
	.657	-.119	-.094	-.028	-.020	-.027	-.056	-.114
	.697	-.121	-.067	-.036	-.026	-.042	-.059	-.119
	.737	-.102	-.057	-.032	-.025	-.026	-.055	-.108
	.777	-.072	-.043	-.023	-.015	-.023	-.044	-.092
	.785	-.082	-.048	-.021	-.010	-.019	-.043	-.093
	.817	-.071	-.027	-.009	-.009	-.016	-.037	-.081
	.857	-.076	-.028	-.015	-.008	-.026	-.047	-.082
	.897	-.082	-.040	-.015	-.005	-.005	-.023	-.069

TABLE 5.- PRESSURE COEFFICIENTS FOR CONFIGURATION 122

(a) M = 0.40 to 0.95; $\alpha = 0^\circ$

	x/l	C_p for - $\phi = 0^\circ$					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.382	-.420	.535	.607	.785	.837	.892
	.392	.227	.251	.261	.275	.294	.320
	.402	.182	.219	.224	.243	.264	.292
	.412	.149	.179	.179	.204	.228	.254
	.432	.060	.075	.084	.116	.144	.178
	.442	-.041	-.034	-.023	.031	.071	.118
	.447	-.168	-.165	-.142	-.056	.001	.058
Upper stage	.453	-.357	-.986	-.887	-.840	-.660	-.554
	.458	-.222	-.316	-.507	-.729	-.936	-.814
	.463	-.109	-.140	-.158	-.370	-.728	-.713
	.473	-.018	-.034	-.036	-.073	-.186	-.545
	.483	.027	.017	.015	.053	.025	-.037
	.493	.061	.063	.065	.093	.134	.114
	.503	.129	.132	.132	.162	.198	.233
	.513	.265	.283	.288	.302	.324	.343
Transition flare	.525	.118	.150	.157	.179	.211	.287
	.535	.061	.072	.069	.089	.120	.185
	.545	.016	.012	.011	.035	.063	.127
	.555	-.065	-.077	-.079	-.048	-.005	.056
	.565	-.307	-.409	-.434	-.361	-.287	-.192
	.568	-.419	-.584	-.664	-.930	-.810	-.684
Main stage	.577	-.121	-.160	-.172	-.183	-.652	-.566
	.587	-.076	-.095	-.100	-.088	-.181	-.478
	.597	-.053	-.062	-.070	-.066	-.036	-.390
	.607	-.030	-.044	-.053	-.052	-.022	-.269
	.617	-.018	-.034	-.040	-.041	-.026	-.060
	.627	-.018	-.025	-.032	-.037	-.026	.001
	.637	-.007	-.016	-.019	-.026	-.022	.016
	.657	-.003	-.009	-.015	-.018	-.019	.019
	.677	-.003	-.008	-.013	-.015	-.018	.007
	.697	.005	-.005	-.007	-.012	-.016	-.001
	.737	.005	-.002	-.006	-.010	-.014	-.010
	.777	.009	.000	-.002	-.006	-.010	-.0.0
	.785	.012	.008	.003	-.001	-.004	-.005
	.817	.014	.007	.002	-.001	-.006	-.007
	.857	.011	.004	-.001	-.004	-.009	-.011
	.877	.011	.005	.000	-.004	-.008	-.011
	.897	.009	.001	-.003	-.007	-.011	-.014

	x/l	C_p for - $\phi = -30^\circ$					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.392	.215	.246	.245	.268	.284	.314
	.402	.182	.206	.212	.233	.251	.279
	.412	.149	.174	.179	.201	.218	.251
	.432	.060	.071	.076	.112	.138	.175
	.442	-.053	-.034	-.027	.031	.071	.118
	.447	-.168	-.165	-.147	-.056	.001	.055
Upper stage	.453	-.903	-1.075	-1.219	-1.280	-1.122	-.989
	.458	-.211	-.320	-.457	-.827	-.912	-.794
	.463	-.098	-.131	-.170	-.378	-.799	-.720
	.473	-.018	-.034	-.036	-.051	-.162	-.542
	.483	.027	.017	.019	.057	.056	-.031
	.493	.061	.063	.065	.097	.137	.124
	.503	.129	.136	.141	.169	.202	.240
	.513	.276	.293	.292	.317	.341	.352
Transition flare	.525	.129	.150	.153	.176	.211	.284
	.535	.061	.067	.069	.089	.120	.185
	.545	.005	.003	.002	.021	.052	.111
	.555	-.065	-.095	-.096	-.067	-.022	.040
	.565	-.341	-.428	-.455	-.372	-.286	-.205
	.568	-.373	-.509	-.614	-.926	-.810	-.684
Main stage	.577	-.121	-.160	-.172	-.180	-.669	-.579
	.587	-.076	-.095	-.104	-.092	-.177	-.478
	.597	-.041	-.048	-.053	-.048	-.022	-.305
	.607	-.030	-.044	-.053	-.052	-.022	-.263
	.617	-.018	-.034	-.040	-.041	-.026	-.054
	.627	-.018	-.025	-.032	-.037	-.026	.001
	.637	-.007	-.016	-.023	-.026	-.026	.016
	.657	-.007	-.012	-.017	-.020	-.020	.017
	.677	.005	-.002	-.006	-.010	-.012	.011
	.697	.005	-.005	-.009	-.013	-.016	-.002
	.737	.005	.000	-.005	-.008	-.012	-.009
	.777	.012	.006	.001	-.002	-.006	-.006
	.785	.012	.008	.003	-.001	-.005	-.005
	.817	.014	.008	.002	-.001	-.006	-.007
	.857	.011	.003	-.002	-.005	-.009	-.012
	.877	.009	.002	-.003	-.006	-.011	-.013
	.897	.008	.001	-.004	-.007	-.012	-.015
	.917	.008	.000	-.004	-.008	-.013	-.016
	.957	-.001	-.011	-.015	-.019	-.024	-.027
	.997	-.053	-.064	-.071	-.074	-.084	-.095

TABLE 5.- PRESSURE COEFFICIENTS FOR CONFIGURATION 122 - Continued

(a) M = 0.40 to 0.95; $\alpha = 0^\circ$ - Concluded

	x/l	C_p for - $\phi = -60^\circ$					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.392	.215	.246	.245	.268	.284	.314
	.402	.182	.206	.208	.229	.248	.276
	.412	.149	.165	.171	.194	.214	.244
	.432	.049	.066	.072	.102	.134	.172
	.442	-.053	-.044	-.036	.024	.068	.115
	.447	-.076	-.067	-.078	-.078	-.088	-.100
Upper stage	.453	-.811	-1.187	-1.207	-.957	-.818	-.708
	.458	-.200	-.269	-.402	-1.027	-.939	-.817
	.463	-.086	-.122	-.128	-.331	-.793	-.697
	.473	-.018	-.039	-.036	-.012	-.101	-.558
	.483	.027	.017	.015	.046	.076	-.015
	.493	.073	.067	.065	.093	.134	.137
	.503	.129	.136	.137	.165	.198	.240
	.513	.287	.302	.300	.335	.358	.356
Transition flare	.525	.118	.141	.140	.165	.198	.268
	.535	.050	.067	.069	.089	.120	.185
	.545	.005	.003	.002	.021	.052	.111
	.555	-.088	-.105	-.109	-.074	-.026	.040
Main stage	.565	-.341	-.424	-.451	-.347	-.265	-.186
	.568	-.362	-.491	-.584	-.915	-.796	-.671
	.577	-.121	-.151	-.163	-.165	-.676	-.579
	.587	-.076	-.095	-.104	-.092	-.174	-.478
	.597	-.041	-.057	-.066	-.063	-.029	-.384
	.607	-.030	-.044	-.049	-.052	-.022	-.256
	.617	-.018	-.034	-.040	-.041	-.026	-.051
	.627	-.018	-.025	-.032	-.037	-.026	.001
	.637	-.007	-.016	-.023	-.026	-.026	.016
	.657	-.007	-.012	-.016	-.020	-.020	.017
	.677	-.001	-.007	-.011	-.015	-.017	.008
	.697	.005	-.002	-.006	-.010	-.014	-.001
	.737	.005	.000	-.005	-.008	-.012	-.009
	.777	.009	.005	.000	-.003	-.007	-.007
	.785	.009	.005	.001	-.003	-.007	-.008
	.817	.014	.007	.002	.000	-.005	-.006
	.857	.011	.003	-.002	-.005	-.009	-.012
	.877	.011	.003	-.002	-.005	-.010	-.013
	.897	.009	.002	-.004	-.007	-.012	-.015
	.917	.005	-.003	-.008	-.011	-.016	-.019
	.957	-.004	-.010	-.015	-.019	-.024	-.026
	.997	-.054	-.066	-.072	-.077	-.087	-.098

	x/l	C_p for - $\phi = -90^\circ$					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.382	.249	.291	.294	.314	.334	.358
	.392	-.891	.246	.331	.505	.574	.633
	.412	.149	.165	.171	.194	.214	.244
	.432	.049	.066	.068	.102	.134	.172
	.447	-.202	-.198	-.181	-.081	-.022	.033
Upper stage	.453	-.811	-1.299	-1.339	-1.034	-.887	-.774
	.473	-.018	-.034	-.036	.007	-.094	-.555
	.493	.061	.063	.061	.090	.131	.137
	.513	.287	.306	.304	.339	.365	.362
Transition flare	.535	.050	.067	.069	.089	.120	.185
Main stage	.565	-.341	-.438	-.459	-.358	-.275	-.195
	.568	-.396	-.565	-.673	-.933	-.813	-.690
	.587	-.076	-.099	-.104	-.092	-.177	-.488
	.607	-.030	-.044	-.049	-.052	-.022	-.253
	.627	-.018	-.025	-.032	-.034	-.026	.004
	.657	-.007	-.012	-.017	-.020	-.020	.016
	.697	.001	-.005	-.010	-.013	-.017	-.004
	.737	.005	.000	-.005	-.008	-.012	-.008
	.777	.009	.005	-.002	-.004	-.009	-.008
	.785	.009	.003	.000	-.004	-.009	-.008
	.817	.014	.009	.004	.001	-.004	-.004
	.857	.011	.003	-.001	-.004	-.009	-.012
	.897	.008	.001	-.004	-.007	-.012	-.015

TABLE 5.- PRESSURE COEFFICIENTS FOR CONFIGURATION 122 - Continued

(b) $M = 0.60$; $\alpha = -10^\circ$ to 10°

	x/l	C_p for - $\phi = 0^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.382	.368	.346	.344	.336	.336	.330	.330
	.392	.408	.330	.277	.229	.189	.144	.093
	.402	.379	.301	.254	.195	.155	.110	.059
	.412	.334	.256	.215	.162	.116	.076	.026
	.432	.233	.155	.113	.060	.026	-.020	-.067
	.442	.120	.042	.000	-.049	-.090	-.125	-.166
	.447	-.004	-.090	-.140	-.189	-.224	-.260	-.295
Upper stage	.453	-.828	-.908	-.951	-.988	-1.001	-1.001	-1.001
	.458	-.160	-.211	-.248	-.267	-.280	-.291	-.291
	.463	-.051	-.095	-.115	-.135	-.135	-.141	-.136
	.473	.019	-.015	-.029	-.037	-.037	-.043	-.032
	.483	.059	.032	.018	.010	.009	.009	.020
	.493	.105	.078	.064	.056	.055	.055	.061
	.503	.174	.147	.127	.119	.118	.113	.112
	.513	387	.336	.299	.274	.251	.228	.210
Transition flare	.525	.254	.192	.161	.130	.112	.095	.078
	.535	.174	.118	.086	.050	.032	.015	-.009
	.545	.122	.060	.046	.004	-.020	-.038	-.061
	.555	.053	-.009	-.046	-.078	-.102	-.126	-.138
	.565	-.251	-.319	-.346	-.365	-.366	-.372	-.372
Main stage	.568	-.442	-.498	-.512	-.514	-.503	-.486	-.498
	.577	-.086	-.131	-.139	-.153	-.154	-.160	-.154
	.587	-.039	-.079	-.081	-.095	-.090	-.090	-.084
	.597	-.016	-.049	-.052	-.066	-.061	-.061	-.049
	.607	-.004	-.032	-.040	-.048	-.043	-.038	-.032
	.617	.007	-.026	-.035	-.037	-.032	-.032	-.020
	.627	.007	-.020	-.023	-.031	-.026	-.020	-.014
	.637	.018	-.015	-.017	-.019	-.014	-.014	-.009
	.657	.021	-.001	-.007	-.012	-.006	-.005	.001
	.677	.025	-.001	-.005	-.010	-.004	-.003	.003
	.697	.031	.005	-.002	-.006	.002	-.001	.005
	.737	.029	.005	.001	-.004	.002	.001	.003
	.777	.035	.011	.006	-.002	.005	.005	.005
	.785	.041	.015	.006	.004	.009	.011	.019
	.817	.040	.014	.008	.002	.006	.007	.013
	.857	.033	.008	.005	-.002	.003	.003	.004
	.877	.036	.009	.005	-.002	.004	.004	.005
	.897	.029	.005	.002	-.005	.001	.000	-.001

	x/l	C_p for - $\phi = -30^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.392	.374	.313	.277	.224	.189	.144	.076
	.402	.334	.279	.237	.190	.150	.105	.042
	.412	.295	.245	.203	.156	.116	.071	.009
	.432	.199	.138	.102	.054	.015	-.026	-.084
	.442	.092	.031	-.005	-.054	-.090	-.131	-.184
	.447	-.045	-.108	-.146	-.194	-.224	-.260	-.306
Upper stage	.453	-.928	-.966	-.986	-1.006	-1.071	-1.065	-1.053
	.458	-.166	-.205	-.236	-.256	-.251	-.251	-.268
	.463	-.079	-.101	-.115	-.123	-.124	-.130	-.141
	.473	-.010	-.026	-.034	-.037	-.037	-.043	-.049
	.483	.036	.026	.012	.015	.015	.009	.003
	.493	.076	.066	.058	.056	.055	.049	.043
	.503	.157	.141	.127	.125	.124	.113	.101
	.513	.358	.330	.299	.280	.268	.239	.204
Transition flare	.525	.202	.169	.155	.130	.112	.089	.055
	.535	.151	.106	.086	.056	.032	.015	-.026
	.545	.093	.043	.018	-.008	-.026	-.050	-.085
	.555	.007	-.038	-.064	-.084	-.108	-.143	-.173
	.565	-.310	-.361	-.381	-.395	-.401	-.413	-.407
Main stage	.568	-.372	-.422	-.425	-.433	-.439	-.440	-.428
	.577	-.109	-.137	-.139	-.153	-.154	-.160	-.166
	.587	-.063	-.084	-.087	-.095	-.096	-.096	-.102
	.597	-.028	-.049	-.052	-.054	-.049	-.049	-.049
	.607	-.022	-.044	-.040	-.048	-.044	-.043	-.049
	.617	-.016	-.032	-.029	-.037	-.032	-.032	-.038
	.627	-.010	-.032	-.023	-.031	-.026	-.026	-.032
	.637	-.004	-.020	-.017	-.019	-.014	-.014	-.020
	.657	-.002	-.013	-.011	-.014	-.008	-.014	-.022
	.677	.009	-.001	-.002	-.004	.002	-.008	-.018
	.697	.004	-.007	-.003	-.006	-.001	-.008	-.020
	.737	.007	-.003	.001	-.002	.003	-.003	-.022
	.777	.015	.005	.006	.004	.007	-.001	-.020
	.785	.013	.001	.006	.004	.011	-.001	-.018
	.817	.013	.003	.005	.001	.005	-.002	-.020
	.857	.008	-.002	.001	-.003	.002	-.006	-.023
	.877	.006	-.003	-.001	-.004	.001	-.006	-.024
	.897	.004	-.005	-.002	-.005	-.001	-.009	-.025
	.917	.003	-.006	-.002	-.005	-.002	-.013	-.027
	.957	-.011	-.019	-.012	-.016	-.014	-.023	-.036
	.997	-.091	-.080	-.067	-.067	-.071	-.087	-.111

TABLE 5.- PRESSURE COEFFICIENTS FOR CONFIGURATION 122 - Continued

(b) M = 0.60; α = -10° to 10° - Concluded

	x/l	C_p for - ϕ = -60°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.392	.255	.256	.248	.224	.195	.155	.071
	.402	.227	.222	.215	.190	.161	.116	.042
	.412	.193	.189	.175	.150	.122	.082	.009
	.432	.092	.087	.079	.049	.026	-.020	-.084
	.442	-.016	-.026	-.035	-.066	-.084	-.125	-.190
	.447	-.115	-.096	-.075	-.078	-.073	-.084	-.125
	.453	-.852	-.890	-.939	-1.006	-1.041	-1.059	-1.106
Upper stage	.458	-.247	-.245	-.242	-.239	-.251	-.257	-.303
	.463	-.137	-.124	-.121	-.112	-.112	-.141	-.170
	.473	-.074	-.049	-.046	-.037	-.043	-.060	-.095
	.483	-.027	-.003	.006	.010	.009	-.014	-.055
	.493	.019	.043	.052	.061	.055	.032	-.003
	.503	.088	.112	.121	.125	.118	.095	.049
	.513	.278	.296	.288	.291	.274	.239	.187
Transition flare	.525	.088	.118	.127	.124	.107	.072	.015
	.535	.065	.066	.069	.050	.038	.009	-.050
	.545	.013	.014	.012	-.008	-.026	-.050	-.108
	.555	-.089	-.083	-.081	-.113	-.109	-.133	-.187
	.565	-.380	-.384	-.381	-.395	-.401	-.419	-.460
	.568	-.430	-.434	-.425	-.427	-.433	-.445	-.475
Main stage	.577	-.156	-.149	-.139	-.142	-.148	-.160	-.195
	.587	-.127	-.114	-.093	-.095	-.096	-.107	-.143
	.597	-.098	-.079	-.064	-.060	-.061	-.078	-.108
	.607	-.080	-.061	-.046	-.048	-.043	-.061	-.096
	.617	-.074	-.055	-.035	-.037	-.037	-.049	-.078
	.627	-.074	-.049	-.029	-.031	-.026	-.043	-.073
	.637	-.068	-.044	-.023	-.025	-.020	-.038	-.067
	.657	-.061	-.034	-.015	-.014	-.012	-.032	-.059
	.677	-.049	-.026	-.010	-.009	-.008	-.029	-.052
	.697	-.037	-.019	-.005	-.004	-.004	-.026	-.046
	.737	-.049	-.022	-.005	-.002	-.001	-.018	-.036
	.777	-.043	-.020	-.002	.002	.003	-.012	-.028
	.785	-.049	-.020	-.002	.002	.003	-.012	-.028
	.817	-.042	-.017	.002	.002	.002	-.009	-.025
	.857	-.046	-.022	-.005	-.003	-.001	-.013	-.026
	.877	-.046	-.023	-.004	-.003	-.001	-.012	-.025
	.897	-.049	-.023	-.005	-.008	-.002	-.013	-.026
	.917	-.056	-.029	-.012	-.008	-.007	-.018	-.030
	.957	-.063	-.037	-.017	-.016	-.015	-.027	-.039
	.997	-.128	-.101	-.077	-.071	-.074	-.093	-.118

	x/l	C_p for - ϕ = -90°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.382	.176	.239	.265	.274	.268	.240	.178
	.412	.080	.121	.147	.150	.144	.122	.059
	.432	-.004	.031	.045	.049	.043	.026	-.038
	.447	-.279	-.236	-.221	-.212	-.218	-.242	-.289
	.453	-.928	-.931	-.974	-1.000	-1.001	-1.019	-1.036
Upper stage	.473	-.108	-.061	-.046	-.037	-.043	-.066	-.118
	.493	-.027	.026	.046	.056	.049	.026	-.037
	.513	.214	.26	.288	.297	.291	.262	.204
Transition flare	.535	-.016	.026	.052	.050	.049	.026	-.032
	.565	-.462	-.425	-.404	-.406	-.401	-.425	-.472
	.568	-.535	-.498	-.483	-.479	-.486	-.504	-.544
Main stage	.587	-.162	-.131	-.099	-.095	-.096	-.119	-.172
	.607	-.121	-.079	-.052	-.048	-.043	-.067	-.125
	.627	-.103	-.061	-.035	-.031	-.032	-.049	-.108
	.657	-.092	-.046	-.019	-.014	-.016	-.043	-.096
	.697	-.082	-.040	-.011	-.008	-.010	-.036	-.084
	.737	-.078	-.034	-.007	-.002	-.002	-.030	-.081
	.777	-.073	-.030	-.003	.002	.002	-.026	-.075
	.785	-.078	-.030	-.007	.002	.002	-.024	-.073
	.817	-.068	-.024	-.001	.003	.003	-.019	-.067
	.857	-.070	-.030	-.005	-.002	-.003	-.024	-.070
	.897	-.072	-.033	-.008	-.005	-.006	-.028	-.073

TABLE 5.- PRESSURE COEFFICIENTS FOR CONFIGURATION 122 - Continued

(c) $M = 0.80$; $\alpha = -10^\circ$ to 10°

	x/l	C_p for - $\phi = 0^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.382	.727	.718	.713	.704	.696	.683	.678
	.392	.443	.372	.319	.271	.218	.175	.124
	.402	.416	.338	.284	.241	.188	.141	.090
	.412	.374	.293	.243	.199	.146	.099	.052
	.432	.272	.194	.144	.104	.055	.008	-.040
	.442	.165	.092	.049	.009	-.041	-.082	-.127
	.447	.051	-.015	-.059	-.097	-.140	-.180	-.217
	.453	-.788	-.793	-.829	-.801	-.796	-.812	-.858
Upper stage	.458	-.495	-.664	-.712	-.714	-.717	-.706	-.534
	.463	-.079	-.171	-.257	-.306	-.325	-.306	-.308
	.473	.010	-.007	-.016	-.010	-.025	-.046	-.079
	.483	.056	.032	.027	.036	.033	.032	.030
	.493	.111	.082	.077	.083	.075	.074	.076
	.503	.192	.163	.151	.157	.137	.128	.119
	.513	.413	.361	.329	.303	.261	.225	.189
Transition flare	.525	.288	.236	.197	.171	.137	.109	.092
	.535	.203	.151	.116	.086	.052	.024	.007
	.545	.153	.089	.059	.028	-.006	-.043	-.064
	.555	.072	.012	-.032	-.062	-.105	-.141	-.159
	.565	-.278	-.343	-.383	-.417	-.456	-.469	-.443
Main stage	.568	-.829	-.909	-.930	-.858	-.751	-.658	-.581
	.577	-.123	-.156	-.169	-.179	-.190	-.191	-.181
	.587	-.060	-.086	-.098	-.101	-.112	-.109	-.099
	.597	-.033	-.058	-.067	-.069	-.077	-.074	-.064
	.607	-.017	-.039	-.051	-.050	-.057	-.054	-.040
	.617	-.006	-.031	-.039	-.038	-.045	-.042	-.032
	.627	.002	-.019	-.031	-.030	-.037	-.035	-.021
	.637	.013	-.011	-.020	-.018	-.026	-.023	-.013
	.657	.019	-.002	-.014	-.013	-.015	-.012	-.009
	.677	.022	-.001	-.012	-.010	-.013	-.010	-.006
	.697	.026	.003	-.008	-.006	-.009	-.007	-.005
	.737	.026	.003	-.007	-.004	-.005	-.007	-.006
	.777	.031	.009	-.001	.001	-.002	-.002	-.005
	.785	.038	.015	.004	.005	.003	.005	.006
	.817	.039	.017	.005	.006	.001	.001	.001
	.857	.032	.010	.000	.002	-.002	-.005	-.006
	.877	.034	.012	.000	.002	-.001	-.005	-.005
	.897	.030	.007	-.007	.000	-.005	-.008	-.010

	x/l	C_p for - $\phi = -30^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.392	.408	.346	.303	.267	.218	.171	.105
	.402	.367	.316	.269	.229	.180	.133	.067
	.412	.332	.278	.231	.195	.142	.095	.033
	.432	.230	.175	.133	.100	.051	.004	-.056
	.442	.131	.076	.038	.005	-.037	-.086	-.143
	.447	.017	-.031	-.067	-.101	-.140	-.180	-.229
	.453	-1.401	-1.430	-1.443	-1.445	-1.433	-1.417	-1.011
Upper stage	.458	-.340	-.443	-.482	-.500	-.546	-.551	-.565
	.463	-.111	-.159	-.210	-.240	-.255	-.279	-.339
	.473	-.017	-.027	-.027	-.026	-.033	-.046	-.075
	.483	.033	.028	.027	.036	.029	.028	.022
	.493	.084	.074	.073	.079	.075	.066	.061
	.503	.173	.159	.155	.156	.141	.132	.115
	.513	.393	.361	.329	.307	.281	.252	.212
Transition flare	.525	.238	.20'	.185	.168	.137	.105	.072
	.535	.176	.136	.108	.083	.052	.020	-.009
	.545	.114	.070	.039	.017	-.022	-.055	-.088
	.555	.018	-.023	-.051	-.082	-.120	-.157	-.191
	.565	-.329	-.370	-.407	-.433	-.468	-.496	-.518
Main stage	.568	-.880	-.949	-.957	-.897	-.826	-.787	-.683
	.577	-.147	-.156	-.169	-.175	-.186	-.191	-.181
	.587	-.092	-.097	-.106	-.105	-.112	-.117	-.111
	.597	-.037	-.050	-.055	-.050	-.061	-.058	-.052
	.607	-.041	-.046	-.051	-.050	-.057	-.058	-.052
	.617	-.029	-.039	-.039	-.038	-.045	-.042	-.044
	.627	-.025	-.031	-.035	-.030	-.037	-.039	-.032
	.637	-.017	-.023	-.027	-.022	-.030	-.031	-.029
	.657	-.008	-.015	-.020	-.016	-.019	-.020	-.027
	.677	.005	-.002	-.008	-.005	-.009	-.014	-.022
	.697	.000	-.007	-.012	-.006	-.009	-.014	-.025
	.737	.004	-.003	-.008	-.003	-.006	-.010	-.027
	.777	.014	.006	.000	.004	-.001	-.007	-.026
	.785	.009	.003	.000	.004	.002	-.005	-.023
	.817	.012	.006	.002	.004	.000	-.008	-.027
	.857	.005	-.001	-.004	.000	-.004	-.011	-.030
	.877	.005	-.002	-.005	.000	-.005	-.013	-.030
	.897	.003	-.003	-.006	-.002	-.006	-.015	-.032
	.917	.004	-.003	-.006	-.002	-.008	-.019	-.033
	.957	-.011	-.015	-.016	-.012	-.020	-.031	-.045
	.997	-.091	-.082	-.075	-.068	-.081	-.097	-.122

TABLE 5.- PRESSURE COEFFICIENTS FOR CONFIGURATION 122 - Continued

(c) M = 0.80; α = -10° to 10° - Concluded

	x/l	C_p for - ϕ = -60°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.392	.291	.293	.277	.259	.226	.183	.105
	.402	.260	.255	.243	.225	.188	.145	.071
	.412	.226	.224	.205	.187	.154	.107	.033
	.432	.127	.130	.110	.092	.059	.016	-.056
	.442	.029	.027	.019	-.003	-.033	-.074	-.139
	.447	-.123	-.094	-.079	-.073	-.081	-.094	-.119
Upper stage	.453	-1.039	-1.045	-1.057	-1.068	-1.099	-1.115	-1.160
	.458	-.460	-.645	-.677	-.687	-.686	-.710	-.693
	.463	-.165	-.190	-.229	-.244	-.263	-.267	-.300
	.473	-.083	-.050	-.027	-.006	-.018	-.046	-.094
	.483	-.033	.004	.019	.032	.021	.001	-.044
	.493	.026	.059	.070	.083	.072	.051	.011
	.503	.103	.136	.147	.156	.137	.113	.072
	.513	.304	.322	.325	.319	.292	.260	.208
Transition flare	.525	.114	.151	.162	.160	.129	.093	.034
	.535	.083	.097	.089	.083	.056	.020	-.033
	.545	.025	.035	.027	.017	-.014	-.051	-.100
	.555	-.076	-.066	-.068	-.093	-.106	-.143	-.192
Main stage	.565	-.377	-.382	-.403	-.409	-.440	-.465	-.506
	.568	-.959	-.968	-.953	-.924	-.904	-.960	-.989
	.577	-.186	-.168	-.165	-.159	-.179	-.191	-.213
	.587	-.151	-.121	-.110	-.105	-.116	-.133	-.154
	.597	-.115	-.086	-.075	-.065	-.077	-.093	-.123
	.607	-.096	-.070	-.055	-.050	-.057	-.074	-.103
	.617	-.092	-.058	-.047	-.038	-.049	-.062	-.091
	.627	-.084	-.054	-.039	-.030	-.041	-.054	-.083
	.637	-.076	-.046	-.031	-.022	-.033	-.050	-.076
	.657	-.068	-.036	-.025	-.014	-.023	-.037	-.065
	.677	-.055	-.028	-.018	-.010	-.018	-.033	-.058
	.697	-.041	-.019	-.012	-.005	-.014	-.029	-.051
	.737	-.053	-.022	-.012	-.001	-.010	-.023	-.042
	.777	-.047	-.018	-.007	.003	-.006	-.018	-.035
	.785	-.054	-.022	-.008	.003	-.003	-.016	-.031
	.817	-.045	-.015	-.003	.005	-.003	-.014	-.028
	.857	-.050	-.021	-.007	.001	-.006	-.018	-.031
	.877	-.050	-.020	-.008	.001	-.006	-.018	-.030
	.897	-.052	-.021	-.009	.000	-.008	-.019	-.032
	.917	-.058	-.028	-.015	-.005	-.013	-.024	-.035
	.957	-.064	-.036	-.022	-.012	-.021	-.033	-.046
	.997	-.133	-.100	-.086	-.070	-.083	-.104	-.128

	x/l	C_p for - ϕ = -90°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.382	.211	.278	.296	.309	.302	.277	.211
	.412	.105	.160	.178	.187	.176	.148	.090
	.432	.021	.073	.083	.092	.078	.054	-.005
	.447	-.202	-.157	-.138	-.128	-.136	-.160	-.209
Upper stage	.453	-1.193	-1.186	-1.195	-1.190	-1.213	-1.225	-1.251
	.473	-.122	-.062	-.031	-.014	-.029	-.062	-.122
	.493	-.021	.039	.062	.079	.064	.035	-.032
	.513	.242	.299	.317	.327	.312	.287	.223
Transition flare	.535	.002	.055	.077	.083	.071	.039	-.017
	.565	-.471	-.442	-.430	-.421	-.428	-.449	-.479
Main stage	.568	-1.033	-.984	-.953	-.924	-.955	-.987	-1.024
	.587	-.182	-.133	-.114	-.105	-.120	-.144	-.193
	.607	-.131	-.078	-.059	-.050	-.061	-.090	-.138
	.627	-.115	-.058	-.039	-.030	-.041	-.066	-.115
	.657	-.097	-.048	-.026	-.016	-.027	-.050	-.103
	.697	-.091	-.039	-.020	-.008	-.018	-.043	-.097
	.737	-.082	-.033	-.014	-.003	-.011	-.035	-.086
	.777	-.078	-.030	-.011	.003	-.009	-.031	-.084
	.785	-.080	-.033	-.011	.001	-.009	-.029	-.076
	.817	-.069	-.023	-.004	.006	-.003	-.026	-.070
	.857	-.074	-.028	-.010	.001	-.009	-.031	-.076
	.897	-.075	-.031	-.012	-.002	-.011	-.033	-.077

TABLE 5.- PRESSURE COEFFICIENTS FOR CONFIGURATION 122 - Continued

(d) M = 1.00; α = -10° to 10°

	x/l	C_p for - ϕ = 0°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.382	.947	.958	.970	.980	.992	1.006	1.013
	.392	.542	.469	.415	.370	.325	.282	.228
	.402	.521	.442	.396	.346	.298	.255	.201
	.412	.482	.405	.354	.310	.265	.221	.165
	.432	.404	.333	.291	.247	.198	.155	.101
	.442	.334	.269	.227	.189	.147	.110	.059
	.447	.268	.206	.173	.135	.099	.064	.020
Upper stage	.453	-.376	-.405	-.421	-.435	-.454	-.471	-.498
	.458	-.579	-.636	-.673	-.700	-.722	-.732	-.753
	.463	-.416	-.509	-.565	-.607	-.644	-.670	-.542
	.473	-.249	-.352	-.416	-.471	-.521	-.321	-.249
	.483	-.181	-.265	-.320	-.363	-.159	-.123	-.208
	.493	-.128	-.175	-.119	-.001	.027	-.076	-.134
	.503	.239	.220	.211	.190	.107	.016	-.026
	.513	.507	.441	.377	.295	.190	.146	.097
Transition flare	.525	.411	.376	.351	.319	.254	.222	.186
	.535	.334	.293	.268	.251	.233	.213	.186
	.545	.300	.250	.219	.193	.174	.158	.134
	.555	.251	.204	.170	.134	.097	.075	.054
Main stage	.565	.027	-.018	-.049	-.098	-.164	-.194	-.218
	.568	-.510	-.532	-.551	-.572	-.566	-.579	-.585
	.577	-.329	-.398	-.438	-.463	-.438	-.423	-.432
	.587	-.229	-.311	-.354	-.385	-.391	-.398	-.407
	.597	-.163	-.236	-.279	-.313	-.335	-.345	-.338
	.607	-.138	-.199	-.236	-.257	-.263	-.258	-.223
	.617	-.129	-.177	-.198	-.204	-.197	-.183	-.154
	.627	-.123	-.158	-.164	-.160	-.144	-.127	-.107
	.637	-.107	-.130	-.127	-.123	-.107	-.096	-.079
	.657	-.092	-.096	-.088	-.079	-.070	-.061	-.052
	.677	-.049	-.068	-.065	-.063	-.057	-.052	-.046
	.697	-.022	-.044	-.046	-.046	-.042	-.038	-.038
	.737	-.009	-.026	-.029	-.031	-.031	-.030	-.037
	.777	.000	-.023	-.026	-.030	-.031	-.031	-.029
	.785	.014	-.013	-.019	-.022	-.022	-.020	-.003
	.817	.049	-.012	-.021	-.015	-.010	-.011	.015
	.857	.062	.034	.029	.026	.024	.022	.018
	.877	.066	.045	.035	.030	.029	.027	.018
	.897	.060	.038	.030	.027	.025	.023	.011

	x/l	C_p for - ϕ = -30°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.392	.509	.448	.406	.367	.322	.279	.216
	.402	.473	.420	.375	.331	.292	.245	.183
	.412	.446	.387	.348	.307	.259	.218	.153
	.432	.367	.315	.276	.240	.198	.155	.086
	.442	.304	.254	.221	.189	.150	.107	.047
	.447	.234	.194	.164	.132	.102	.061	.011
Upper stage	.453	-.824	-.837	-.843	-.851	-.858	-.831	-.889
	.458	-.592	-.633	-.657	-.681	-.703	-.726	-.747
	.463	-.459	-.528	-.577	-.610	-.644	-.676	-.703
	.473	-.270	-.361	-.419	-.462	-.508	-.512	-.267
	.483	-.205	-.277	-.323	-.353	-.261	-.129	-.199
	.493	-.168	-.182	-.104	.002	.030	-.067	-.113
	.503	.218	.213	.211	.193	.113	.047	-.004
	.513	.476	.429	.374	.304	.233	.186	.119
Transition flare	.525	.355	.348	.342	.322	.285	.250	.183
	.535	.306	.284	.262	.251	.236	.207	.162
	.545	.257	.228	.204	.183	.171	.139	.100
	.555	.196	.170	.146	.122	.094	.056	.017
Main stage	.565	-.017	-.046	-.074	-.108	-.133	-.168	-.202
	.568	-.519	-.532	-.548	-.572	-.591	-.607	-.635
	.577	-.372	-.423	-.454	-.472	-.494	-.529	-.569
	.587	-.251	-.317	-.357	-.385	-.391	-.401	-.419
	.597	-.154	-.199	-.223	-.241	-.251	-.258	-.251
	.607	-.166	-.211	-.236	-.2[illegible]	-.263	-.261	-.232
	.617	-.160	-.186	-.198	-	-.197	-.189	-.163
	.627	-.157	-.174	-.170	-	-.148	-.136	-.[illegible]
	.637	-.145	-.149	-.136	-.126	-.110	-.102	-.101
	.657	-.123	-.105	-.092	-.082	-.074	-.073	-.080
	.677	-.064	-.068	-.062	-.058	-.055	-.056	-.072
	.697	-.049	-.054	-.050	-.046	-.045	-.047	-.072
	.737	-.034	-.035	-.031	-.030	-.031	-.036	-.076
	.777	-.018	-.026	-.023	-.025	-.028	-.035	-.070
	.785	-.014	-.022	-.021	-.022	-.023	-.032	-.054
	.817	.022	-.022	-.023	-.016	-.013	-.023	-.032
	.857	.034	.024	.026	.026	.024	.013	-.013
	.877	.035	.031	.029	.029	.026	.016	-.014
	.897	.033	.028	.027	.026	.023	.014	-.013
	.917	.032	.024	.024	.024	.020	.011	-.014
	.957	.020	.011	.013	.011	.005	-.006	-.025
	.997	-.036	-.056	-.072	-.094	-.113	-.132	-.147

TABLE 5.- PRESSURE COEFFICIENTS FOR CONFIGURATION 122 - Continued

(d) $M = 1.00$; $\alpha = -10^\circ$ to 10° - Concluded

	x/l	C_p for - $\phi = -60^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.392	.401	.396	.381	.361	.331	.291	.216
	.402	.370	.366	.351	.331	.301	.261	.183
	.412	.340	.339	.321	.304	.271	.230	.153
	.432	.268	.269	.255	.237	.201	.164	.086
	.442	.207	.209	.203	.186	.153	.119	.044
	.447	-.192	-.155	-.139	-.132	-.138	-.155	-.186
	.453	-.536	-.556	-.568	-.582	-.589	-.615	-.664
Upper stage	.458	-.651	-.664	-.682	-.700	-.712	-.729	-.756
	.463	-.527	-.556	-.580	-.588	-.619	-.648	-.703
	.473	-.372	-.413	-.450	-.471	-.496	-.515	-.490
	.483	-.307	-.327	-.348	-.363	-.381	-.287	-.184
	.493	-.193	-.148	-.058	.008	.033	.004	-.066
	.503	.162	.192	.204	.196	.181	.130	.039
	.513	.375	.377	.349	.304	.292	.247	.174
Transition flare	.525	.223	.293	.318	.319	.297	.241	.134
	.535	.214	.241	.247	.251	.226	.185	.100
	.545	.171	.194	.192	.183	.171	.127	.054
	.555	.112	.138	.140	.119	.107	.068	-.002
	.565	-.070	-.059	-.074	-.092	-.108	-.131	-.180
Main stage	.568	-.560	-.542	-.545	-.556	-.569	-.585	-.619
	.577	-.457	-.461	-.467	-.472	-.494	-.526	-.575
	.587	-.347	-.358	-.373	-.388	-.416	-.448	-.500
	.597	-.285	-.292	-.298	-.310	-.322	-.351	-.407
	.607	-.257	-.252	-.248	-.254	-.257	-.267	-.298
	.617	-.248	-.224	-.205	-.204	-.201	-.214	-.245
	.627	-.248	-.199	-.170	-.163	-.157	-.170	-.198
	.637	-.229	-.164	-.136	-.126	-.119	-.139	-.163
	.657	-.167	-.119	-.092	-.080	-.082	-.098	-.125
	.677	-.127	-.090	-.071	-.062	-.066	-.081	-.107
	.697	-.088	-.061	-.049	-.045	-.050	-.065	-.089
	.737	-.092	-.054	-.035	-.030	-.035	-.050	-.077
	.777	-.081	-.049	-.031	-.026	-.033	-.047	-.066
	.795	-.082	-.049	-.030	-.025	-.030	-.043	-.059
	.817	-.020	-.039	-.025	-.016	-.020	-.034	-.025
	.857	-.020	.008	.022	.026	.021	.009	-.006
	.877	-.018	.013	.025	.029	.024	.014	-.005
	.897	-.022	.008	.023	.027	.022	.012	-.007
	.917	-.030	-.003	.016	.021	.016	.007	-.012
	.957	-.033	-.007	.008	.012	.003	-.006	-.024
	.997	-.103	-.089	-.088	-.097	-.112	-.132	-.154

	x/l	C_p for - $\phi = -90^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.382	.325	.378	.400	.406	.401	.381	.325
	.412	.228	.276	.294	.307	.292	.267	.210
	.432	.165	.215	.230	.237	.222	.200	.138
	.447	.032	.082	.107	.111	.105	.082	.023
	.453	-.658	-.646	-.646	-.645	-.661	-.671	-.711
Upper stage	.473	-.468	-.460	-.469	-.471	-.477	-.478	-.490
	.493	-.078	-.039	-.014	.011	-.007	-.036	-.066
	.513	.270	.318	.321	.301	.332	.321	.270
Transition flare	.535	.122	.207	.235	.251	.233	.192	.109
	.565	-.161	-.115	-.102	-.105	-.098	-.112	-.158
Main stage	.568	-.622	-.586	-.569	-.575	-.572	-.585	-.619
	.587	-.432	-.405	-.392	-.388	-.400	-.420	-.451
	.607	-.341	-.286	-.258	-.254	-.260	-.292	-.354
	.627	-.276	-.196	-.167	-.160	-.160	-.195	-.273
	.657	-.176	-.120	-.090	-.081	-.092	-.123	-.185
	.697	-.131	-.078	-.055	-.046	-.055	-.081	-.138
	.737	-.122	-.066	-.036	-.030	-.038	-.064	-.125
	.777	-.107	-.059	-.034	-.026	-.037	-.061	-.117
	.785	-.115	-.059	-.033	-.026	-.033	-.056	-.104
	.817	-.043	-.043	-.023	-.015	-.024	-.048	-.073
	.857	-.044	.001	.020	.026	.019	-.002	-.044
	.897	-.049	-.003	.019	.027	.019	-.001	-.048

TABLE 5.- PRESSURE COEFFICIENTS FOR CONFIGURATION 122 - Continued

(e) M = 1.20; α = -10° to 10°

	x/l	C_p for - ϕ = 0°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.382	1.308	1.290	1.275	1.259	1.227	1.198	1.185
	.392	.512	.422	.372	.315	.268	.227	.194
	.402	.523	.430	.377	.321	.281	.235	.202
	.412	.509	.425	.366	.315	.278	.235	.194
	.432	.499	.419	.361	.315	.270	.235	.189
	.442	.472	.403	.353	.318	.270	.230	.178
	.447	.436	.376	.337	.305	.262	.222	.173
Upper stage	.453	-.277	-.295	-.308	-.322	-.344	-.363	-.389
	.458	-.296	-.341	-.363	-.382	-.398	-.409	-.429
	.463	-.188	-.261	-.294	-.321	-.343	-.359	-.387
	.473	-.095	-.176	-.217	-.250	-.274	-.299	-.327
	.483	-.051	-.126	-.159	-.192	-.210	-.238	-.255
	.493	-.023	-.088	-.115	-.139	-.155	-.164	-.143
	.503	-.021	-.077	-.090	-.104	-.145	.037	.066
	.513	.363	.310	.289	.259	.221	.191	.162
Transition flare	.525	.393	.364	.334	.302	.270	.237	.225
	.535	.341	.301	.277	.255	.242	.218	.206
	.545	.341	.285	.261	.231	.212	.190	.181
	.555	.349	.287	.252	.214	.185	.160	.151
	.565	.220	.178	.148	.097	.045	.004	.031
Main stage	.568	-.226	-.250	-.269	-.285	-.301	-.315	-.363
	.577	-.143	-.186	-.213	-.232	-.240	-.240	-.260
	.587	-.085	-.136	-.171	-.191	-.201	-.207	-.213
	.597	-.062	-.108	-.135	-.155	-.171	-.182	-.194
	.607	-.037	-.083	-.113	-.132	-.143	-.151	-.158
	.617	-.032	-.078	-.099	-.116	-.118	-.121	-.122
	.627	-.023	-.066	-.085	-.096	-.096	-.093	-.091
	.637	-.010	-.053	-.066	-.074	-.071	-.071	-.061
	.657	-.017	-.051	-.059	-.057	-.047	-.041	-.035
	.677	-.015	-.028	-.041	-.039	-.034	-.023	-.025
	.697	-.002	-.031	-.036	-.030	-.019	-.013	-.022
	.737	-.014	-.022	-.022	-.033	-.025	-.024	-.013
	.777	.018	-.012	-.026	-.020	-.024	-.027	-.004
	.785	.026	-.004	-.016	-.013	-.016	-.013	-.006
	.817	.024	-.001	-.003	-.020	-.017	-.008	.009
	.857	.022	.011	-.008	-.001	.002	-.006	-.010
	.877	.032	-.002	-.003	.001	-.002	-.004	-.005
	.897	.014	-.002	.001	-.004	-.008	-.014	-.016

	x/l	C_p for - ϕ = -30°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.392	.477	.403	.361	.307	.276	.227	.183
	.402	.474	.406	.361	.307	.278	.227	.186
	.412	.474	.406	.358	.313	.278	.235	.183
	.432	.458	.401	.350	.313	.270	.238	.183
	.442	.440	.390	.348	.318	.276	.233	.175
	.447	.405	.363	.331	.305	.262	.222	.162
Upper stage	.453	-.469	-.478	-.484	-.492	-.505	-.519	-.536
	.458	-.307	-.341	-.354	-.365	-.376	-.400	-.426
	.463	-.235	-.286	-.308	-.327	-.345	-.370	-.407
	.473	-.117	-.184	-.211	-.239	-.263	-.293	-.327
	.483	-.076	-.132	-.162	-.184	-.208	-.230	-.253
	.493	-.062	-.110	-.126	-.145	-.161	-.172	-.176
	.503	-.043	-.080	-.085	-.093	-.059	.002	.061
	.513	.339	.307	.289	.264	.235	.202	.138
Transition flare	.525	.343	.342	.326	.302	.270	.237	.181
	.535	.321	.298	.277	.258	.242	.212	.176
	.545	.297	.263	.244	.220	.201	.174	.151
	.555	.291	.252	.231	.201	.177	.149	.118
	.565	.185	.153	.127	.086	.045	.004	-.055
Main stage	.568	-.229	-.247	-.263	-.285	-.298	-.309	-.302
	.577	-.168	-.203	-.221	-.235	-.246	-.257	-.269
	.587	-.110	-.150	-.174	-.191	-.204	-.218	-.244
	.597	-.057	-.083	-.105	-.113	-.121	-.129	-.144
	.607	-.068	-.097	-.116	-.132	-.143	-.151	-.163
	.617	-.051	-.080	-.099	-.110	-.118	-.123	-.127
	.627	-.051	-.078	-.088	-.099	-.098	-.101	-.102
	.637	-.040	-.066	-.074	-.077	-.076	-.079	-.077
	.657	-.036	-.046	-.057	-.050	-.040	-.046	-.057
	.677	-.029	-.029	-.035	-.032	-.032	-.033	-.051
	.697	-.039	-.041	-.035	-.034	-.031	-.027	-.053
	.737	-.037	-.033	-.026	-.031	-.024	-.034	-.050
	.777	-.005	-.017	-.022	-.014	-.023	-.030	-.054
	.785	.001	-.013	-.014	-.008	-.014	-.023	-.045
	.817	-.001	-.014	-.007	-.018	-.017	-.023	-.056
	.857	-.005	.004	-.007	-.010	-.008	-.022	-.060
	.877	.003	-.012	-.006	-.003	-.005	-.019	-.054
	.897	-.010	-.010	-.003	.000	-.005	-.021	-.044
	.917	-.009	-.003	-.003	-.005	-.006	-.019	-.036
	.957	-.012	-.014	-.011	-.015	-.015	-.019	-.032
	.997	.001	-.019	-.032	-.052	-.074	-.086	-.078

TABLE 5.- PRESSURE COEFFICIENTS FOR CONFIGURATION 122 - Concluded

(e) M = 1.20; $\alpha = -10^\circ$ to 10° - Concluded

	x/l	C_p for - $\phi = -60^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.392	.364	.347	.334	.307	.276	.241	.186
	.402	.372	.350	.334	.313	.281	.243	.191
	.412	.370	.358	.334	.310	.284	.243	.186
	.432	.359	.358	.331	.313	.286	.262	.186
	.442	.340	.342	.331	.315	.286	.249	.175
Upper stage	.447	-.179	-.156	-.138	-.133	-.140	-.157	-.186
	.453	-.221	-.231	-.241	-.261	-.282	-.310	-.356
	.458	-.362	-.369	-.374	-.379	-.392	-.409	-.445
	.463	-.288	-.303	-.305	-.307	-.332	-.367	-.420
	.473	-.199	-.223	-.236	-.244	-.260	-.288	-.332
	.483	-.161	-.176	-.178	-.186	-.205	-.227	-.272
	.493	-.142	-.140	- .34	-.145	-.155	-.180	-.228
	.503	-.120	-.107	-.098	-.098	-.100	-.100	-.052
Transition flare	.513	.226	.266	.275	.264	.251	.215	.146
	.525	.248	.293	.304	.299	.275	.237	.156
	.535	.234	.263	.266	.258	.242	.204	.135
	.545	.209	.227	.231	.220	.201	.166	.121
	.555	.207	.223	.231	.214	.197	.168	.123
	.565	.130	.134	.127	.097	.078	.056	.012
Main stage	.568	-.268	-.255	-.258	-.266	-.279	-.298	-.335
	.577	-.237	-.233	-.230	-.232	-.246	-.273	-.333
	.587	-.187	-.186	-.188	-.191	-.207	-.232	-.291
	.597	-.148	-.150	-.155	-.152	-.168	-.193	-.238
	.607	-.137	-.130	-.130	-.132	-.143	-.160	-.202
	.617	-.135	-.119	-.108	-.110	-.118	-.135	-.174
	.627	-.135	-.108	-.096	-.096	-.101	-.121	-.149
	.637	-.121	-.086	-.080	-.077	-.079	-.098	-.127
	.657	-.110	-.057	-.050	-.038	-.042	-.067	-.102
	.677	-.102	-.058	-.043	-.037	-.042	-.059	-.091
	.697	-.093	-.058	-.036	-.036	-.041	-.050	-.080
	.737	-.091	-.053	-.032	-.031	-.033	-.051	-.063
	.777	-.066	-.041	-.028	-.014	-.025	-.037	-.051
	.785	-.052	-.039	-.020	-.008	-.018	-.030	-.049
	.817	-.056	-.026	-.012	-.016	-.018	-.031	-.049
	.857	-.062	-.016	-.014	-.015	-.023	-.031	-.048
	.877	-.053	-.028	-.007	-.003	-.008	-.022	-.042
	.897	-.062	-.027	-.009	.001	-.002	-.016	-.032
	.917	-.068	-.031	-.016	-.005	-.008	-.020	-.029
	.957	-.068	-.035	-.014	-.014	-.018	-.018	-.033
	.997	-.060	-.046	-.041	-.053	-.068	-.088	-.101

	x/l	C_p for - $\phi = -30^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.382	.254	.290	.307	.318	.308	.297	.267
	.412	.257	.288	.310	.307	.303	.284	.245
	.432	.254	.304	.305	.315	.303	.292	.232
Upper stage	.447	.192	.250	.275	.280	.276	.252	.191
	.453	-.344	-.312	-.303	-.308	-.319	-.344	-.381
	.473	-.282	-.261	-.247	-.247	-.260	-.271	-.302
	.493	-.216	-.173	-.151	-.145	-.150	-.175	-.231
Transition flare	.513	.188	.244	.269	.264	.270	.243	.168
	.535	.155	.224	.255	.258	.250	.212	.137
Main stage	.565	.048	.080	.097	.091	.095	.084	.036
	.568	-.326	-.297	-.280	-.280	-.282	-.293	-.330
	.587	-.248	-.216	-.196	-.191	-.198	-.223	-.274
	.607	-.218	-.169	-.141	-.132	-.140	-.165	-.227
	.627	-.193	-.116	-.102	-.096	-.098	-.126	-.194
	.657	-.148	-.073	-.047	-.039	-.045	-.081	-.148
	.697	-.139	-.078	-.046	-.039	-.050	-.075	-.141
	.737	-.114	-.063	-.038	-.032	-.035	-.064	-.120
	.777	-.077	-.047	-.027	-.017	-.023	-.049	-.100
	.785	-.088	-.051	-.026	-.014	-.023	-.049	-.103
	.817	-.079	-.028	-.012	-.010	-.018	-.041	-.090
	.857	-.082	-.028	-.017	-.010	-.029	-.050	-.088
	.897	-.086	-.039	-.016	-.005	-.006	-.026	-.075

TABLE 6.- PRESSURE COEFFICIENTS FOR CONFIGURATION 222

(a) M = 0.40 to 0.95; $\alpha = 0^\circ$

	x/l	C_p for - $\phi = 0^\circ$					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.411		.445	.457	.495	.524	.563
	.421		.350	.367	.410	.438	.477
	.431		.235	.255	.307	.343	.387
	.441		.119	.144	.204	.248	.297
	.453		-1.249	-1.197	-1.210	-1.118	-.983
Upper stage	.458		-.661	-.710	-.670	-1.106	-.995
	.463		-.392	-.503	-.554	-.631	-.885
	.473		-.063	-.144	-.343	-.327	-.648
	.483		.016	.012	-.125	-.136	-.130
	.493		.062	.067	.031	.045	.009
	.503		.126	.126	.121	.154	.138
	.513		.265	.252	.219	.270	.255
Transition flare	.525		.144	.147	.172	.211	.299
	.535		.061	.067	.103	.130	.215
	.545		.011	.012	.042	.072	.148
	.555		-.074	-.078	-.053	-.006	.067
	.565		-.370	-.404	-.374	-.283	-.188
Main stage	.568		-.550	-.606	-.837	-.812	-.687
	.577		-.162	-.175	-.181	-.536	-.546
	.587		-.096	-.107	-.112	-.095	-.451
	.597		-.064	-.077	-.079	-.047	-.347
	.607		-.050	-.056	-.057	-.037	-.164
	.617		-.040	-.043	-.049	-.037	-.033
	.627		-.031	-.039	-.038	-.033	-.001
	.637		-.017	-.026	-.027	-.023	.012
	.657		-.011	-.019	-.013	-.018	.012
	.677		-.009	-.017	-.013	-.017	.000
	.697		-.006	-.012	-.008	-.013	-.005
	.737		-.003	-.010	-.008	-.012	-.012
	.777		.002	-.006	-.003	-.006	-.010
	.785		.006	.000	.001	-.001	-.006
	.817		.006	-.001	-.001	-.003	-.006
	.857		.003	-.004	-.005	-.007	-.010
	.877		.003	-.004	-.005	-.007	-.010
	.897		-.001	-.007	-.008	-.010	-.013

	x/l	C_p for - $\phi = -30^\circ$					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.421		.345	.358	.406	.434	.471
	.431		.255	.268	.321	.354	.395
	.441		.110	.131	.197	.241	.291
	.453		-1.239	-1.137	-1.140	-1.056	-.924
Upper stage	.458		-.642	-.685	-.634	-.907	-.998
	.463		-.383	-.512	-.554	-.600	-.898
	.473		-.063	-.144	-.347	-.364	-.532
	.483		.020	.012	-.125	-.163	-.130
	.493		.062	.067	.027	.018	-.020
	.503		.131	.130	.118	.137	.084
	.513		.265	.248	.215	.225	.229
Transition flare	.525		.144	.147	.172	.208	.302
	.535		.061	.067	.103	.130	.215
	.545		.002	-.001	.031	.062	.138
	.555		-.092	-.099	-.068	-.027	.051
	.565		-.403	-.425	-.389	-.318	-.211
Main stage	.568		-.498	-.567	-.852	-.819	-.693
	.577		-.162	-.175	-.181	-.443	-.540
	.587		-.101	-.107	-.112	-.106	-.438
	.597		-.054	-.060	-.060	-.040	-.278
	.607		-.050	-.056	-.057	-.040	-.154
	.617		-.040	-.043	-.046	-.037	-.033
	.627		-.031	-.039	-.038	-.033	-.004
	.637		-.017	-.026	-.031	-.026	.009
	.657		-.014	-.022	-.016	-.021	.009
	.677		-.003	-.012	-.008	-.012	.005
	.697		-.005	-.013	-.009	-.013	-.004
	.737		-.001	-.009	-.005	-.008	-.010
	.777		.003	-.002	.001	-.002	-.006
	.785		.006	.000	.002	-.001	-.006
	.817		.005	-.001	-.002	-.003	-.006
	.857		.001	-.004	-.007	-.007	-.012
	.877		.001	-.006	-.007	-.008	-.012
	.897		-.001	-.007	-.008	-.010	-.014
	.917		-.001	-.008	-.008	-.010	-.014
	.957		-.013	-.018	-.021	-.021	-.026
	.997		-.066	-.076	-.081	-.084	-.095

TABLE 6.- PRESSURE COEFFICIENTS FOR CONFIGURATION 222 - Continued

(a) M = 0.40 to 0.95; $\alpha = 0^\circ$ - Concluded

	x/l	C_p for - $\phi = -60^\circ$					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.421		.345	.358	.406	.431	.468
	.431		.255	.268	.314	.351	.389
	.441		.119	.144	.207	.248	.294
	.453		-1.155	-1.052	-1.041	-1.007	-.941
Upper stage	.458		-.651	-.694	-.634	-.935	-.995
	.463		-.378	-.512	-.554	-.580	-.898
	.473		-.049	-.140	-.354	-.375	-.503
	.483		.020	.016	-.125	-.163	-.130
	.493		.066	.071	.038	.028	-.020
	.503		.126	.126	.121	.140	.090
	.513		.265	.252	.212	.232	.193
Transition flare	.525		.135	.134	.164	.201	.296
	.535		.061	.067	.099	.130	.209
	.545		.002	-.001	.031	.062	.138
	.555		-.107	-.112	-.083	-.040	.042
Main stage	.565		-.398	-.417	-.374	-.304	-.211
	.568		-.456	-.512	-.822	-.795	-.667
	.577		-.157	-.171	-.181	-.433	-.523
	.587		-.101	-.107	-.112	-.106	-.445
	.597		-.059	-.069	-.075	-.051	-.350
	.607		-.050	-.056	-.057	-.040	-.151
	.617		-.040	-.043	-.046	-.037	-.036
	.627		-.031	-.039	-.038	-.033	-.004
	.637		-.022	-.026	-.031	-.026	.009
	.657		-.012	-.020	-.015	-.021	.010
	.677		-.008	-.015	-.011	-.016	.003
	.697		-.003	-.010	-.008	-.012	-.003
	.737		-.001	-.009	-.005	-.008	-.010
	.777		.003	-.003	.000	-.005	-.006
	.785		.003	-.003	.000	-.005	-.008
	.817		.006	-.001	-.002	-.003	-.005
	.857		.001	-.004	-.006	-.007	-.011
	.877		.001	-.005	-.007	-.008	-.012
	.897		.000	-.007	-.007	-.009	-.013
	.917		-.005	-.011	-.012	-.014	-.018
	.957		-.012	-.018	-.020	-.021	-.026
	.997		-.068	-.077	-.082	-.085	-.098

	x/l	C_p for - $\phi = -90^\circ$					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.411		.436	.449	.488	.518	.553
	.431		.241	.268	.314	.348	.389
	.441		.119	.136	.204	.248	.294
	.453		-1.253	-1.163	-1.092	-.997	-.865
Upper stage	.473		-.049	-.131	-.347	-.320	-.496
	.493		.062	.067	.035	.038	-.004
	.513		.274	.269	.223	.266	.232
Transition flare	.535		.061	.067	.103	.130	.215
Main stage	.565		-.408	-.430	-.382	-.301	-.204
	.568		-.517	-.589	-.866	-.822	-.693
	.587		-.101	-.111	-.112	-.099	-.445
	.607		-.050	-.056	-.057	-.040	-.147
	.627		-.031	-.039	-.038	-.033	-.004
	.657		-.014	-.022	-.016	-.021	.007
	.697		-.008	-.016	-.010	-.015	-.008
	.737		-.001	-.009	-.004	-.008	-.009
	.777		.002	-.005	-.002	-.005	-.009
	.785		.002	-.005	.000	-.006	-.008
	.817		.008	.001	.001	-.001	-.003
	.857		.002	-.004	-.005	-.007	-.011
	.897		-.001	-.007	-.008	-.010	-.014

TABLE 6.- PRESSURE COEFFICIENTS FOR CONFIGURATION 222 - Continued

(b) M = 0.60; α = -10° to 10°

	x/l	C_p for - $\phi = 0°$						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.411	.631	.547	.484	.419	.353	.285	.213
	.421	.546	.451	.388	.328	.257	.200	.123
	.431	.421	.326	.263	.209	.138	.086	.016
	.441	.297	.201	.139	.090	.019	-.027	-.090
Upper stage	.453	-1.246	-1.351	-1.421	-1.419	-1.382	-1.224	-.923
	.458	-.235	-.339	-.414	-.470	-.549	-.601	-.617
	.463	-.079	-.136	-.177	-.192	-.242	-.317	-.425
	.473	.008	-.031	-.055	-.053	-.062	-.068	-.106
	.483	.054	.015	-.003	.000	-.004	-.004	-.008
	.493	.101	.061	.044	.052	.042	.042	.039
	.503	.170	.136	.113	.115	.100	.094	.079
	.513	.372	.321	.286	.265	.221	.192	.148
Transition flare	.525	.244	.194	.159	.132	.100	.077	.056
	.535	.170	.113	.078	.052	.025	.002	-.020
	.545	.118	.061	.038	.005	-.021	-.051	-.067
	.555	.049	-.008	-.055	-.077	-.110	-.134	-.143
	.565	-.251	-.308	-.344	-.348	-.363	-.352	-.338
Main stage	.568	-.436	-.494	-.517	-.503	-.490	-.455	-.429
	.577	-.085	-.125	-.149	-.152	-.162	-.162	-.160
	.587	-.038	-.072	-.090	-.094	-.103	-.103	-.096
	.597	-.015	-.049	-.067	-.065	-.068	-.074	-.066
	.607	-.003	-.032	-.049	-.047	-.051	-.051	-.049
	.617	.008	-.026	-.043	-.041	-.045	-.039	-.037
	.627	.008	-.020	-.032	-.030	-.033	-.033	-.025
	.637	.019	-.008	-.026	-.024	-.021	-.022	-.020
	.657	.026	-.002	-.016	-.012	-.016	-.016	-.010
	.677	.026	.000	-.014	-.012	-.016	-.010	-.010
	.697	.032	.004	-.012	-.006	-.010	-.008	-.008
	.737	.032	.004	-.010	-.006	-.010	-.006	-.008
	.777	.036	.010	-.006	.000	-.004	-.004	-.004
	.785	.042	.013	.000	.002	-.002	.000	.004
	.817	.041	.015	.001	.002	-.001	.000	.002
	.857	.034	.010	-.004	-.001	-.004	-.005	-.005
	.877	.037	.011	-.004	-.001	-.004	-.004	-.005
	.897	.034	.007	-.006	-.003	-.007	-.008	-.011

	x/l	C_p for - $\phi = -30°$						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.421	.495	.428	.371	.322	.262	.200	.117
	.431	.399	.332	.269	.226	.166	.109	.038
	.441	.251	.179	.122	.073	.024	-.027	-.096
Upper stage	.453	-1.211	-1.345	-1.404	-1.419	-1.341	-1.283	-1.064
	.458	-.270	-.344	-.408	-.447	-.526	-.572	-.629
	.463	-.108	-.141	-.177	-.192	-.236	-.282	-.385
	.473	-.021	-.043	-.061	-.058	-.068	-.074	-.101
	.483	.031	.009	-.003	.006	-.004	-.010	-.014
	.493	.072	.055	.044	.052	.042	.036	.027
	.503	.153	.131	.119	.121	.106	.100	.073
	.513	.355	.315	.286	.265	.233	.210	.171
Transition flare	.525	.198	.171	.147	.126	.100	.077	.044
	.535	.146	.107	.078	.052	.025	.002	-.031
	.545	.089	.044	.009	-.006	-.033	-.063	-.090
	.555	-.003	-.043	-.073	-.083	-.127	-.151	-.179
	.565	-.309	-.356	-.385	-.383	-.393	-.405	-.403
Main stage	.568	-.389	-.435	-.453	-.445	-.443	-.449	-.435
	.577	-.109	-.131	-.149	-.152	-.162	-.168	-.168
	.587	-.068	-.078	-.090	-.094	-.103	-.103	-.107
	.597	-.033	-.049	-.061	-.093	-.062	-.063	-.060
	.607	-.027	-.037	-.049	-.047	-.051	-.057	-.055
	.617	-.015	-.032	-.043	-.035	-.045	-.045	-.043
	.627	-.015	-.026	-.037	-.030	-.033	-.033	-.037
	.637	-.009	-.020	-.026	-.024	-.021	-.027	-.025
	.657	.001	-.014	-.022	-.016	-.019	-.022	-.047
	.677	.010	-.002	-.012	-.006	-.012	-.016	-.023
	.697	.007	-.008	-.014	-.006	-.012	-.016	-.027
	.737	.007	-.002	-.012	-.002	-.008	-.010	-.027
	.777	.016	.004	-.006	.002	-.002	-.008	-.029
	.785	.014	.004	-.004	.002	-.002	-.006	-.025
	.817	.016	.005	-.003	.002	-.002	-.007	-.026
	.857	.009	.000	-.008	-.002	-.006	-.011	-.029
	.877	.008	-.001	-.009	-.002	-.007	-.012	-.029
	.897	.006	-.001	-.010	-.003	-.008	-.014	-.030
	.917	.006	-.004	-.011	-.004	-.010	-.018	-.033
	.957	-.009	-.017	-.022	-.015	-.020	-.029	-.044
	.997	-.089	-.081	-.074	-.068	-.080	-.091	-.117

TABLE 6.- PRESSURE COEFFICIENTS FOR CONFIGURATION 222 - Continued

(b) M = 0.60; α = -10° to 10° - Concluded

	x/l	C_p for - ϕ = -60°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.421	.365	.360	.343	.317	.279	.222	.145
	.431	.285	.269	.241	.220	.183	.143	.055
	.441	.155	.134	.105	.085	.047	.002	-.066
Upper stage	.453	-1.299	-1.368	-1.427	-1.419	-1.429	-1.453	-1.445
	.458	-.345	-.368	-.397	-.412	-.462	-.485	-.536
	.463	-.166	-.165	-.182	-.174	-.201	-.719	-.275
	.473	-.090	-.072	-.066	-.058	-.068	-.085	-.135
	.483	-.038	-.014	-.014	.000	-.010	-.027	-.077
	.493	.014	.032	.038	.052	.037	.025	-.025
	.503	.078	.102	.107	.115	.106	.088	.033
Transition flare	.513	.268	.281	.269	.265	.245	.721	.160
	.525	.083	.113	.118	.121	.094	.065	.004
	.535	.054	.067	.061	.052	.025	-.004	-.055
	.545	.008	.009	.003	-.006	-.033	-.063	-.114
	.555	-.100	-.089	-.090	-.106	-.117	-.146	-.192
Main stage	.565	-.380	-.379	-.385	-.383	-.393	-.422	-.461
	.568	-.430	-.429	-.435	-.421	-.431	-.449	-.482
	.577	-.167	-.154	-.155	-.152	-.162	-.174	-.207
	.587	-.126	-.108	-.102	-.094	-.103	-.115	-.148
	.597	-.097	-.072	-.073	-.059	-.068	-.080	-.119
	.607	-.085	-.061	-.055	-.047	-.056	-.068	-.101
	.617	-.079	-.055	-.043	-.035	-.045	-.057	-.090
	.627	-.074	-.049	-.038	-.030	-.039	-.051	-.078
	.637	-.068	-.037	-.032	-.024	-.027	-.045	-.072
	.657	-.060	-.034	-.028	-.014	-.023	-.039	-.066
	.677	-.048	-.026	-.022	-.010	-.019	-.034	-.060
	.697	-.037	-.018	-.016	-.006	-.016	-.029	-.053
	.737	-.046	-.024	-.018	-.004	-.010	-.025	-.045
	.777	-.048	-.022	-.014	.000	-.008	-.020	-.037
	.785	-.046	-.020	-.014	.002	-.006	-.020	-.035
	.817	-.041	-.015	-.009	.003	-.005	-.015	-.030
	.857	-.046	-.020	-.013	-.002	-.008	-.018	-.032
	.877	-.044	-.020	-.013	-.002	-.009	-.018	-.030
	.897	-.046	-.023	-.014	-.002	-.009	-.019	-.032
	.917	-.054	-.029	-.021	-.007	-.014	-.024	-.036
	.957	-.063	-.033	-.026	-.015	-.023	-.031	-.046
	.997	-.124	-.097	-.086	-.069	-.082	-.098	-.123

	x/l	C_p for - ϕ = -90°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.411	.319	.388	.405	.413	.393	.364	.292
	.431	.150	.201	.212	.220	.206	.177	.134
	.441	.025	.066	.065	.079	.070	.047	.009
Upper stage	.453	-1.633	-1.585	-1.562	-1.507	-1.505	-1.558	-1.591
	.473	-.131	-.083	-.072	-.058	-.068	-.085	-.153
	.493	-.038	.015	.032	.012	.037	.013	-.060
Transition flare	.513	.205	.246	.263	.271	.268	.250	.183
	.535	-.021	.027	.044	.052	.042	.013	-.043
Main stage	.565	-.468	-.426	-.409	-.389	-.404	-.434	-.479
	.568	-.536	-.494	-.482	-.462	-.484	-.507	-.552
	.587	-.167	-.125	-.108	-.094	-.103	-.127	-.178
	.607	-.120	-.072	-.061	-.047	-.056	-.074	-.131
	.627	-.103	-.055	-.038	-.030	-.039	-.057	-.113
	.657	-.093	-.045	-.030	-.016	-.025	-.051	-.104
	.697	-.085	-.041	-.026	-.008	-.021	-.043	-.096
	.737	-.080	-.034	-.020	-.004	-.014	-.037	-.088
	.777	-.076	-.032	-.014	.000	-.011	-.033	-.082
	.785	-.076	-.034	-.016	.000	-.010	-.039	-.080
	.817	-.067	-.023	-.009	.004	-.005	-.025	-.073
	.857	-.069	-.027	-.014	-.001	-.010	-.028	-.075
	.897	-.072	-.031	-.018	-.003	-.013	-.033	-.078

TABLE 6.- PRESSURE COEFFICIENTS FOR CONFIGURATION 222 - Continued

(c) M = 0.80; α = -10° to 10°

	x/l	C_p for - ϕ = 0°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.411	.692	.601	.539	.474	.411	.345	.271
	.421	.597	.514	.447	.387	.319	.254	.183
	.431	.480	.400	.337	.278	.215	.152	.090
	.441	.364	.285	.227	.170	.110	.056	-.003
Upper stage	.453	-1.357	-1.412	-1.350	-1.196	-.907	-.702	-.508
	.458	-.734	-.757	-.742	-.703	-.608	-.531	-.444
	.463	-.274	-.449	-.532	-.551	-.530	-.500	-.456
	.473	.003	-.047	-.146	-.259	-.328	-.367	-.366
	.483	.042	.035	.029	-.029	-.109	-.188	-.198
	.493	.096	.081	.084	.068	.023	-.036	-.054
	.503	.182	.159	.150	.130	.097	.054	.039
	.513	.395	.349	.305	.239	.171	.112	.098
Transition flare	.525	.286	.232	.196	.157	.116	.084	.074
	.535	.200	.147	.114	.076	.050	.022	.012
	.545	.146	.093	.060	.022	-.016	-.040	-.039
	.555	.069	.015	-.029	-.073	-.107	-.131	-.130
Main stage	.565	-.286	-.345	-.382	-.413	-.388	-.361	-.328
	.568	-.823	-.878	-.843	-.698	-.558	-.480	-.428
	.577	-.127	-.158	-.167	-.182	-.189	-.185	-.165
	.587	-.064	-.087	-.096	-.112	-.118	-.123	-.098
	.597	-.036	-.059	-.069	-.076	-.083	-.087	-.066
	.607	-.021	-.039	-.049	-.057	-.063	-.067	-.047
	.617	-.013	-.032	-.037	-.045	-.051	-.056	-.035
	.627	-.001	-.020	-.029	-.037	-.043	-.044	-.027
	.637	.006	-.012	-.017	-.029	-.031	-.036	-.015
	.657	.016	-.005	-.011	-.020	-.024	-.026	-.009
	.677	.018	-.003	-.010	-.019	-.021	-.023	-.007
	.697	.022	.001	-.008	-.015	-.017	-.019	-.005
	.737	.022	.003	-.003	-.012	-.014	-.018	-.006
	.777	.028	.008	.001	-.007	-.010	-.014	-.003
	.785	.035	.013	.006	-.003	-.005	-.008	.005
	.817	.036	.015	.007	-.002	-.005	-.011	-.001
	.857	.029	.010	.002	-.005	-.009	-.016	-.010
	.877	.032	.011	.004	-.004	-.009	-.016	-.010
	.897	.027	.007	.001	-.007	-.011	-.019	-.015

	x/l	C_p for - ϕ = -30°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.421	.551	.487	.440	.379	.319	.258	.179
	.431	.463	.400	.345	.291	.236	.182	.115
	.441	.372	.259	.211	.162	.114	.056	-.003
Upper stage	.453	-1.321	-1.329	-1.314	-1.121	-.922	-.710	-.611
	.458	-.667	-.714	-.688	-.676	-.620	-.535	-.479
	.463	-.285	-.472	-.544	-.555	-.538	-.504	-.471
	.473	-.032	-.059	-.158	-.255	-.316	-.359	-.358
	.483	.019	.027	.022	-.029	-.098	-.184	-.195
	.493	.069	.070	.080	.068	.031	-.036	-.054
	.503	.158	.155	.154	.134	.105	.054	.043
	.513	.368	.342	.305	.235	.178	.127	.121
Transition flare	.525	.228	.209	.184	.157	.116	.084	.059
	.535	.173	.139	.111	.076	.050	.022	.001
	.545	.111	.070	.041	.006	-.020	-.048	-.071
	.555	.015	-.016	-.049	-.089	-.119	-.151	-.166
Main stage	.565	-.329	-.376	-.409	-.429	-.416	-.432	-.459
	.568	-.874	-.913	-.851	-.686	-.574	-.567	-.590
	.577	-.150	-.161	-.167	-.182	-.185	-.185	-.165
	.587	-.095	-.098	-.104	-.112	-.122	-.126	-.110
	.597	-.048	-.055	-.053	-.060	-.067	-.071	-.055
	.607	-.044	-.051	-.049	-.057	-.063	-.067	-.055
	.617	-.036	-.039	-.037	-.045	-.051	-.056	-.043
	.627	-.028	-.032	-.033	-.037	-.043	-.048	-.035
	.637	-.021	-.024	-.025	-.029	-.031	-.040	-.031
	.657	-.013	-.017	-.017	-.024	-.026	-.033	-.024
	.677	.001	-.005	-.006	-.013	-.017	-.024	-.019
	.697	-.005	-.008	-.010	-.015	-.018	-.024	-.021
	.737	-.001	-.005	-.010	-.009	-.013	-.020	-.021
	.777	.010	.004	.002	-.003	-.008	-.016	-.019
	.785	.007	.003	.002	-.003	-.005	-.014	-.017
	.817	.009	.005	.004	-.002	-.006	-.016	-.021
	.857	.003	-.002	-.001	-.006	-.010	-.019	-.025
	.877	.001	-.002	-.002	-.007	-.011	-.022	-.026
	.897	.000	-.004	-.004	-.007	-.012	-.023	-.027
	.917	-.001	-.005	-.004	-.008	-.014	-.026	-.029
	.957	-.014	-.016	-.014	-.020	-.026	-.040	-.040
	.997	-.095	-.082	-.074	-.078	-.088	-.108	-.118

TABLE 6.- PRESSURE COEFFICIENTS FOR CONFIGURATION 222 - Continued

(c) M = 0.80; α = -10° to 10° - Concluded

	x/l	C_p for - ϕ = -60°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.421	.425	.422	.405	.379	.338	.288	.202
	.431	.342	.335	.318	.288	.247	.201	.126
	.441	.224	.213	.196	.170	.137	.094	.027
	.453	-1.301	-1.234	-1.129	-1.007	-.926	-.805	-.753
Upper stage	.458	-.706	-.722	-.707	-.672	-.667	-.582	-.565
	.463	-.531	-.554	-.559	-.559	-.573	-.543	-.530
	.473	-.079	-.129	-.193	-.259	-.289	-.363	-.358
	.483	-.048	.008	.010	-.025	-.062	-.149	-.159
	.493	.007	.058	.080	.072	.050	-.005	-.039
	.503	.088	.128	.142	.130	.113	.077	.032
	.513	.286	.314	.282	.239	.210	.193	.167
Transition flare	.525	.108	.147	.157	.146	.116	.077	.012
	.535	.080	.097	.095	.076	.050	.022	-.039
	.545	.026	.039	.029	.006	-.016	-.048	-.099
	.555	-.079	-.066	-.072	-.089	-.111	-.140	-.188
	.565	-.381	-.384	-.406	-.417	-.431	-.460	-.495
Main stage	.568	-.945	-.944	-.843	-.643	-.649	-.846	-.908
	.577	-.209	-.177	-.175	-.178	-.185	-.193	-.208
	.587	-.158	-.122	-.108	-.116	-.122	-.134	-.149
	.597	-.123	-.091	-.073	-.076	-.083	-.103	-.118
	.607	-.103	-.071	-.053	-.057	-.063	-.083	-.094
	.617	-.095	-.059	-.045	-.045	-.051	-.067	-.086
	.627	-.091	-.055	-.037	-.037	-.043	-.064	-.078
	.637	-.080	-.047	-.029	-.029	-.035	-.056	-.074
	.657	-.073	-.038	-.021	-.022	-.029	-.047	-.061
	.677	-.061	-.030	-.016	-.017	-.024	-.043	-.053
	.697	-.048	-.021	-.010	-.012	-.020	-.039	-.046
	.737	-.059	-.025	-.010	-.011	-.017	-.032	-.038
	.777	-.055	-.020	-.006	-.005	-.012	-.027	-.028
	.785	-.059	-.025	-.007	-.004	-.008	-.024	-.028
	.817	-.049	-.016	-.001	-.001	-.008	-.024	-.026
	.857	-.054	-.020	-.005	-.005	-.011	-.027	-.027
	.877	-.053	-.022	-.006	-.006	-.012	-.027	-.027
	.897	-.055	-.023	-.007	-.007	-.013	-.028	-.028
	.917	-.061	-.029	-.013	-.012	-.019	-.033	-.031
	.957	-.067	-.036	-.019	-.020	-.027	-.043	-.043
	.997	-.135	-.104	-.083	-.080	-.090	-.113	-.123

	x/l	C_p for - ϕ = -90°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.411	.383	.445	.470	.467	.456	.429	.358
	.431	.212	.266	.284	.284	.270	.250	.198
	.441	.106	.148	.170	.170	.156	.140	.096
	.453	-1.258	-1.203	-1.180	-1.125	-1.115	-1.116	-1.072
Upper stage	.473	-.235	-.222	-.228	-.255	-.265	-.278	-.249
	.493	-.048	.035	.064	.072	.058	.007	-.054
	.513	.224	.260	.254	.247	.256	.244	.202
Transition flare	.535	-.005	.058	.076	.076	.066	.038	-.023
	.565	-.476	-.436	-.437	-.425	-.439	-.452	-.479
	.568	-1.019	-.972	-.800	-.729	-.834	-.968	-.995
Main stage	.587	-.190	-.134	-.116	-.116	-.122	-.150	-.188
	.607	-.138	-.083	-.057	-.057	-.063	-.095	-.133
	.627	-.119	-.059	-.037	-.037	-.043	-.071	-.114
	.657	-.103	-.050	-.027	-.022	-.033	-.060	-.099
	.697	-.097	-.043	-.019	-.016	-.026	-.053	-.092
	.737	-.088	-.036	-.011	-.009	-.018	-.045	-.080
	.777	-.082	-.033	-.008	-.007	-.014	-.040	-.073
	.785	-.085	-.033	-.008	-.005	-.013	-.039	-.072
	.817	-.073	-.023	-.002	.001	-.008	-.033	-.067
	.857	-.077	-.030	-.006	-.005	-.013	-.039	-.070
	.897	-.079	-.033	-.010	-.007	-.016	-.043	-.072

TABLE I.- PRESSURE COEFFICIENTS FOR CONFIGURATION 222 - Continued

(a) M = 1.00; α = -10° to 10°

	x/l	C_p for - β = 0°						
		α = -10°	α = -5°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.411	.815	.728	.671	.609	.548	.492	.409
	.421	.737	.646	.589	.530	.470	.407	.331
	.431	.641	.552	.502	.445	.387	.329	.257
	.441	.546	.459	.414	.361	.303	.250	.183
Upper stage	.453	-.824	-.843	-.852	-.859	-.872	-.880	-.894
	.458	-.713	-.794	-.836	-.875	-.906	-.926	-.689
	.463	-.536	-.654	-.719	-.770	-.820	-.827	-.522
	.473	-.304	-.441	-.520	-.590	-.659	-.341	-.426
	.483	-.202	-.317	-.381	-.441	-.200	-.273	-.355
	.493	-.159	-.242	-.263	-.104	-.045	-.208	-.271
	.503	.166	.163	.160	.143	.032	-.112	-.172
	.513	.474	.406	.342	.254	.118	.009	-.051
Transition flare	.525	.399	.365	.344	.306	.195	.104	.066
	.535	.319	.282	.261	.244	.204	.144	.112
	.545	.291	.239	.218	.192	.164	.125	.100
	.555	.2[illegible]	.196	.166	.127	.084	.055	.035
Main stage	.565	.027	-.020	-.050	-.101	-.178	-.211	-.222
	.568	-.513	-.541	-.553	-.570	-.568	-.510	-.545
	.577	-.[illegible]35	-.407	-.437	-.461	-.411	-.357	-.367
	.587	-.[illegible]38	-.316	-.356	-.386	-.374	-.347	-.345
	.597	-.173	-.244	-.281	-.314	-.324	-.310	-.283
	.607	-.148	-.210	-.238	-.258	-.255	-.238	-.205
	.617	-.138	-.188	-.200	-.202	-.193	-.179	-.158
	.627	-.135	-.169	-.166	-.161	-.140	-.138	-.120
	.637	-.119	-.138	-.128	-.124	-.108	-.107	-.098
	.657	-.108	-.087	-.088	-.087	-.075	-.076	-.069
	.677	-.059	-.066	-.070	-.076	-.065	-.067	-.060
	.697	-.041	-.047	-.055	-.063	-.052	-.057	-.041
	.737	-.030	.001	-.044	-.058	-.023	-.038	-.018
	.777	.000	.024	.016	-.019	.014	.004	-.005
	.785	.016	.034	.024	.005	.023	.016	.012
	.817	.040	.038	.029	.017	.025	.018	.017
	.857	.046	.033	.027	.021	.023	.019	.012
	.877	.058	.035	.029	.023	.023	.020	.011
	.897	.056	.026	.022	.020	.019	.016	.003

	x/l	C_p for - β = -30°						
		α = -10°	α = -5°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.421	.688	.622	.577	.524	.470	.413	.328
	.431	.616	.549	.505	.451	.397	.344	.279
	.441	.501	.441	.399	.355	.306	.256	.183
Upper stage	.453	-.739	-.765	-.777	-.784	-.785	-.802	-.819
	.458	-.744	-.809	-.845	-.872	-.903	-.926	-.708
	.463	-.580	-.679	-.737	-.782	-.823	-.849	-.528
	.473	-.317	-.437	-.511	-.575	-.637	-.357	-.435
	.483	-.230	-.329	-.390	-.441	-.219	-.273	-.361
	.493	-.196	-.261	-.251	-.085	-.052	-.205	-.274
	.503	.156	.160	.160	.143	.017	-.118	-.172
	.513	.443	.388	.330	.245	.103	.005	-.051
Transition flare	.525	.341	.341	.335	.306	.247	.144	.075
	.535	.291	.273	.258	.244	.220	.156	.085
	.545	.245	.218	.200	.180	.164	.122	.066
	.555	.187	.162	.141	.115	.084	.042	-.011
Main stage	.565	-.016	-.051	-.079	-.118	-.159	-.180	-.219
	.568	-.529	-.547	-.562	-.580	-.608	-.635	-.664
	.577	-.379	-.432	-.453	-.464	-.433	-.466	-.501
	.587	-.263	-.326	-.359	-.383	-.374	-.354	-.358
	.597	-.166	-.207	-.228	-.245	-.246	-.235	-.217
	.607	-.182	-.219	-.241	-.255	-.255	-.238	-.208
	.617	-.169	-.198	-.200	-.205	-.193	-.182	-.164
	.627	-.169	-.182	-.169	-.161	-.146	-.141	-.136
	.637	-.157	-.148	-.134	-.127	-.111	-.113	-.114
	.657	-.125	-.101	-.093	-.090	-.079	-.086	-.096
	.677	-.078	-.068	-.068	-.071	-.063	-.072	-.082
	.697	-.071	-.059	-.060	-.064	-.055	-.065	-.075
	.737	-.054	-.002	-.044	-.055	-.022	-.042	-.053
	.777	-.013	.021	.018	-.014	.015	-.002	-.041
	.785	-.003	.024	.022	.008	.023	.006	-.031
	.817	.014	.030	.027	.016	.024	.009	-.020
	.857	.023	.023	.023	.020	.022	.012	-.014
	.877	.030	.021	.023	.021	.020	.010	-.011
	.897	.033	.016	.020	.019	.017	.008	-.012
	.917	.036	.014	.018	.018	.014	.003	-.012
	.957	.026	.003	.008	.005	.001	-.012	-.023
	.997	-.032	-.061	-.074	-.101	-.114	-.138	-.148

TABLE A.I.- PRESSURE COEFFICIENTS FOR CONFIGURATION 222 - Continued

(a) M = 1.00; α = -10° to 10° - Concluded

	x/l	C_p for - β = -5°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.421	.570	.565	.550	.524	.488	.437	.352
	.431	.501	.492	.477	.448	.412	.371	.285
	.441	.407	.398	.387	.361	.328	.286	.204
Upper stage	.453	-.811	-.815	-.805	-.806	-.810	-.817	-.828
	.458	-.806	-.831	-.849	-.866	-.891	-.911	-.918
	.463	-.642	-.707	-.746	-.779	-.820	-.836	-.689
	.473	-.437	-.512	-.554	-.587	-.618	-.576	-.423
	.483	-.329	-.385	-.415	-.448	-.426	-.261	-.327
	.493	-.230	-.230	-.198	-.085	-.052	-.171	-.228
	.503	.095	.135	.148	.140	.060	-.041	-.101
Transition flare	.513	.332	.332	.302	.247	.171	.113	.051
	.525	.211	.282	.311	.306	.281	.196	.072
	.535	.187	.224	.243	.241	.223	.159	.048
	.545	.147	.178	.188	.180	.164	.110	.020
	.555	.101	.126	.134	.117	.103	.056	-.029
Main stage	.565	-.076	-.067	-.076	-.109	-.112	-.139	-.193
	.568	-.563	-.547	-.547	-.555	-.571	-.591	-.633
	.577	-.472	-.472	-.469	-.464	-.496	-.535	-.589
	.587	-.363	-.373	-.378	-.386	-.405	-.463	-.517
	.597	-.297	-.304	-.306	-.314	-.311	-.325	-.383
	.607	-.276	-.263	-.256	-.255	-.249	-.247	-.261
	.617	-.266	-.232	-.203	-.202	-.196	-.201	-.214
	.627	-.263	-.191	-.169	-.161	-.155	-.163	-.183
	.637	-.232	-.157	-.134	-.127	-.121	-.141	-.167
	.657	-.172	-.118	-.094	-.088	-.084	-.108	-.134
	.677	-.141	-.092	-.076	-.075	-.072	-.095	-.113
	.697	-.109	-.066	-.059	-.062	-.059	-.082	-.091
	.737	-.107	-.020	-.047	-.055	-.030	-.059	-.053
	.777	-.071	.000	.009	-.013	.009	-.012	-.036
	.785	-.066	-.001	.010	.005	.016	-.006	-.031
	.817	-.039	.011	.022	.016	.022	.001	-.011
	.857	-.027	.003	.019	.021	.020	.007	-.007
	.877	-.020	.002	.018	.022	.019	.008	-.007
	.897	-.020	-.003	.016	.020	.015	.005	-.009
	.917	-.025	-.012	.009	.015	.010	-.001	-.011
	.957	-.024	-.015	.003	.006	-.001	-.013	-.022
	.997	-.098	-.094	-.089	-.103	-.112	-.137	-.154

	x/l	C_p for - β = -5°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.411	.528	.583	.604	.603	.588	.564	.497
	.431	.380	.422	.444	.445	.436	.413	.355
	.441	.298	.338	.360	.361	.349	.332	.273
Upper stage	.453	-.755	-.746	-.698	-.703	-.700	-.714	-.762
	.473	-.499	-.567	-.582	-.590	-.594	-.589	-.506
	.493	-.224	-.140	-.112	-.089	-.095	-.149	-.221
Transition flare	.513	.212	.246	.256	.251	.251	.243	.199
	.535	.082	.181	.231	.241	.229	.171	.066
Main stage	.565	-.174	-.120	-.104	-.112	-.103	-.123	-.168
	.568	-.629	-.594	-.575	-.573	-.574	-.591	-.626
	.587	-.447	-.419	-.397	-.389	-.405	-.432	-.470
	.607	-.363	-.285	-.256	-.255	-.252	-.297	-.373
	.627	-.254	-.182	-.163	-.158	-.155	-.179	-.248
	.657	-.190	-.120	-.093	-.089	-.092	-.129	-.189
	.697	-.150	-.081	-.066	-.065	-.066	-.099	-.147
	.737	-.125	-.029	-.042	-.054	-.035	-.078	-.105
	.777	-.089	-.010	.006	-.014	.005	-.025	-.080
	.785	-.087	-.010	.006	.004	.014	-.015	-.069
	.817	-.054	.003	.022	.018	.022	-.008	-.044
	.857	-.044	-.006	.018	.021	.018	-.005	-.042
	.897	-.039	-.013	.012	.019	.013	-.008	-.047

TABLE 6.- PRESSURE COEFFICIENTS FOR CONFIGURATION 222 - Continued

(e) $M = 1.20$; $\alpha = -10^\circ$ to 10°

	x/l	C_p for - $\phi = 0^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.411	.896	.802		.672	.614	.558	.484
	.421	.833	.745		.621	.562	.504	.427
	.431	.763	.682		.568	.511	.457	.382
	.441	.694	.619		.516	.460	.410	.336
Upper stage	.453	-.494	-.517		-.510	-.520	-.522	-.529
	.458	-.410	-.470		-.532	-.550	-.566	-.587
	.463	-.279	-.371		-.463	-.495	-.527	-.551
	.473	-.126	-.231		-.345	-.393	-.431	-.471
	.483	-.053	-.148		-.248	-.294	-.329	-.369
	.493	-.023	-.104		-.185	-.214	-.233	-.141
	.503	-.021	-.085		-.138	-.093	.024	.041
Transition flare	.513	.359	.294		.241	.206	.161	.096
	.525	.383	.348		.298	.260	.220	.167
	.535	.327	.290		.254	.236	.215	.186
	.545	.332	.277		.232	.208	.193	.169
	.555	.343	.282		.218	.184	.163	.137
	.565	.214	.173		.101	.042	-.001	-.031
Main stage	.568	-.230	-.252		-.287	-.305	-.321	-.336
	.577	-.143	-.188		-.231	-.241	-.229	-.217
	.587	-.086	-.138		-.190	-.202	-.201	-.209
	.597	-.062	-.108		-.153	-.169	-.179	-.189
	.607	-.037	-.086		-.131	-.144	-.149	-.150
	.617	-.034	-.077		-.115	-.119	-.118	-.114
	.627	-.024	-.069		-.095	-.094	-.090	-.086
	.637	-.013	-.055		-.073	-.072	-.071	-.061
	.657	-.016	-.048		-.057	-.047	-.037	-.033
	.677	-.015	-.026		-.040	-.034	-.023	-.023
	.697	-.004	-.031		-.030	-.019	-.011	-.020
	.737	-.014	-.022		-.033	-.025	-.024	-.010
	.777	.019	-.011		-.021	-.025	-.025	-.009
	.785	.028	-.004		-.013	-.016	-.012	.003
	.817	.025	.000		-.021	-.018	-.009	.004
	.857	.025	.011		-.002	.002	-.006	-.009
	.877	.033	-.001		-.001	-.003	-.005	-.007
	.897	.015	-.001		-.004	-.009	-.014	-.017

	x/l	C_p for - $\phi = -30^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.421	.785	.721		.615	.565	.510	.427
	.431	.730	.670		.572	.522	.469	.401
	.441	.649	.592		.510	.460	.418	.336
Upper stage	.453	-.388	-.403		-.424	-.437	-.452	-.460
	.458	-.426	-.479		-.527	-.548	-.566	-.587
	.463	-.316	-.390		-.474	-.501	-.527	-.557
	.473	-.134	-.231		-.337	-.374	-.406	-.452
	.483	-.083	-.159		-.251	-.289	-.324	-.356
	.493	-.061	-.123		-.191	-.217	-.241	-.210
	.503	-.042	-.090		-.127	-.101	-.010	.033
Transition flare	.513	.333	.286		.241	.212	.163	.085
	.525	.332	.326		.300	.263	.220	.159
	.535	.305	.288		.254	.236	.210	.169
	.545	.284	.255		.218	.198	.179	.153
	.555	.284	.249		.202	.173	.152	.115
	.565	.180	.146		.082	.039	.002	-.042
Main stage	.568	-.241	-.258		-.290	-.311	-.326	-.353
	.577	-.170	-.202		-.231	-.244	-.254	-.267
	.587	-.113	-.152		-.190	-.202	-.212	-.223
	.597	-.059	-.086		-.112	-.122	-.129	-.134
	.607	-.070	-.097		-.131	-.141	-.149	-.150
	.617	-.056	-.086		-.109	-.116	-.121	-.120
	.627	-.051	-.080		-.095	-.097	-.099	-.095
	.637	-.043	-.066		-.076	-.077	-.079	-.073
	.657	-.039	-.045		-.053	-.040	-.044	-.055
	.677	-.034	-.026		-.034	-.033	-.031	-.051
	.697	-.041	-.040		-.035	-.031	-.025	-.053
	.737	-.036	-.031		-.029	-.025	-.032	-.052
	.777	-.001	-.014		-.015	-.023	-.026	-.057
	.785	.005	-.011		-.008	-.012	-.020	-.049
	.817	.000	-.012		-.019	-.017	-.022	-.062
	.857	-.004	.004		-.011	-.009	-.021	-.060
	.877	.005	-.010		-.004	-.005	-.018	-.054
	.897	-.008	-.008		-.001	-.005	-.020	-.047
	.917	-.006	-.002		-.006	-.006	-.019	-.037
	.957	-.011	-.014		-.016	-.016	-.019	-.030
	.997	.004	-.019		-.053	-.075	-.089	-.079

TABLE 6.- PRESSURE COEFFICIENTS FOR CONFIGURATION 222 - Concluded

(e) M = 1.20; α = -10° to 10° - Concluded

	x/l	C_p for - ϕ = -65°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.421	.665	.662		.615	.581	.542	.452
	.431	.617	.611		.569	.533	.491	.406
	.441	.552	.552		.510	.479	.443	.358
Upper stage	.453	-.491	-.459		-.441	-.462	-.455	-.465
	.458	-.488	-.495		-.532	-.548	-.569	-.590
	.463	-.378	-.418		-.474	-.501	-.514	-.537
	.473	-.236	-.283		-.339	-.360	-.376	-.405
	.483	-.174	-.209		-.257	-.278	-.301	-.331
	.493	-.144	-.162		-.191	-.209	-.235	-.281
	.503	-.126	-.126		-.133	-.134	-.147	-.110
Transition flare	.513	.207	.239		.235	.212	.183	.115
	.525	.217	.274		.292	.266	.223	.134
	.535	.214	.249		.254	.236	.196	.115
	.545	.196	.217		.218	.198	.171	.104
	.555	.196	.214		.213	.193	.167	.118
Main stage	.565	.118	.129		.098	.072	.054	.008
	.568	-.273	-.258		-.270	-.277	-.301	-.336
	.577	-.241	-.236		-.231	-.247	-.274	-.328
	.587	-.192	-.191		-.190	-.205	-.235	-.295
	.597	-.156	-.149		-.153	-.163	-.190	-.248
	.607	-.140	-.133		-.128	-.141	-.157	-.198
	.617	-.140	-.122		-.109	-.116	-.132	-.167
	.627	-.140	-.108		-.095	-.102	-.118	-.145
	.637	-.119	-.086		-.078	-.080	-.096	-.125
	.657	-.115	-.057		-.039	-.042	-.065	-.101
	.677	-.105	-.057		-.038	-.041	-.056	-.090
	.697	-.094	-.057		-.037	-.040	-.047	-.079
	.737	-.092	-.051		-.029	-.031	-.049	-.060
	.777	-.059	-.039		-.015	-.023	-.036	-.050
	.785	-.052	-.037		-.009	-.018	-.027	-.049
	.817	-.054	-.024		-.016	-.018	-.031	-.048
	.857	-.061	-.016		-.016	-.023	-.030	-.047
	.877	-.050	-.029		-.004	-.008	-.021	-.041
	.897	-.061	-.027		.000	-.003	-.016	-.032
	.917	-.066	-.030		-.007	-.008	-.020	-.028
	.957	-.067	-.035		-.016	-.019	-.018	-.031
	.997	-.056	-.047		-.055	-.069	-.089	-.103

	x/l	C_p for - ϕ = -30°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.411	.602	.651		.664	.657	.634	.578
	.431	.494	.546		.567	.557	.537	.479
	.441	.439	.492		.510	.501	.483	.425
Upper stage	.453	-.415	-.364		-.351	-.356	-.374	-.426
	.473	-.324	-.333		-.345	-.346	-.346	-.345
	.493	-.233	-.206		-.191	-.195	-.208	-.248
Transition flare	.513	.145	.209		.241	.234	.217	.129
	.535	.132	.211		.257	.241	.201	.117
Main stage	.565	.036	.077		.092	.085	.078	.027
	.568	-.333	-.302		-.276	-.283	-.296	-.331
	.587	-.254	-.219		-.190	-.200	-.224	-.273
	.607	-.219	-.161		-.131	-.141	-.165	-.225
	.627	-.200	-.116		-.095	-.099	-.121	-.200
	.657	-.149	-.075		-.041	-.048	-.080	-.143
	.697	-.140	-.078		-.039	-.051	-.072	-.141
	.737	-.112	-.063		-.033	-.033	-.062	-.119
	.777	-.079	-.046		-.017	-.024	-.049	-.099
	.785	-.086	-.049		-.014	-.021	-.046	-.101
	.817	-.078	-.028		-.010	-.018	-.039	-.087
	.857	-.078	-.029		-.011	-.029	-.048	-.086
	.897	-.084	-.039		-.006	-.007	-.025	-.073

TABLE 7.- PRESSURE COEFFICIENTS FOR CONFIGURATION 322

(a) M = 0.40 to 0.95; α = 0°

	x/l	C_p for - $\phi = 0°$					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.426	.475	.558	.575	.629	.661	.694
	.436	.319	.402	.429	.481	.519	.563
	.446	.064	.187	.221	.299	.348	.400
	.453	-1.783	-.973	-.839	-.709	-.701	-.999
Upper stage	.458	-.400	-.779	-.704	-.569	-.532	-1.117
	.463	-.195	-.642	-.667	-.576	-.545	-.995
	.473	-.070	-.234	-.370	-.497	-.508	-.659
	.483	-.013	-.019	-.099	-.328	-.400	-.243
	.493	.032	.059	.038	-.160	-.262	-.105
	.503	.100	.114	.113	-.020	-.120	.035
	.513	.247	.223	.209	.095	.005	.163
Transition flare	.525	.100	.136	.146	.148	.119	.264
	.535	.032	.068	.080	.123	.133	.210
	.545	-.002	.013	.026	.066	.096	.150
	.555	-.083	-.070	-.063	-.027	.005	.077
	.565	-.325	-.354	-.355	-.326	-.283	-.181
Main stage	.568	-.438	-.509	-.538	-.613	-.662	-.684
	.577	-.151	-.158	-.163	-.168	-.175	-.548
	.587	-.094	-.098	-.100	-.103	-.104	-.429
	.597	-.071	-.065	-.071	-.074	-.070	-.284
	.607	-.048	-.051	-.054	-.056	-.053	-.087
	.617	-.048	-.042	-.041	-.045	-.042	-.019
	.627	-.036	-.033	-.037	-.038	-.036	-.003
	.637	-.025	-.019	-.024	-.027	-.025	.006
	.657	-.021	-.014	-.013	-.019	-.018	-.001
	.677	-.017	-.011	-.010	-.016	-.015	-.008
	.697	-.006	-.007	-.006	-.013	-.012	-.009
	.737	-.013	-.005	-.003	-.010	-.011	-.015
	.777	-.010	-.001	-.003	-.007	-.006	-.012
	.785	-.006	.004	.001	-.002	-.002	-.007
	.817	-.007	.004	.001	-.002	-.002	-.009
	.857	-.007	.000	-.002	-.006	-.006	-.014
	.877	-.007	.002	-.002	-.004	-.006	-.013
	.897	-.010	-.003	-.005	-.009	-.009	-.017

	x/l	C_p for - $\phi = -30°$					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.426	.475	.554	.575	.629	.657	.694
	.436	.275	.371	.896	.462	.501	.544
	.446	.075	.187	.217	.296	.344	.394
	.453	-1.449	-.843	-.742	-.571	-.643	-1.106
Upper stage	.458	-.547	-.715	-.646	-.536	-.521	-1.133
	.463	-.207	-.651	-.633	-.547	-.528	-.950
	.473	-.070	-.294	-.408	-.483	-.478	-.534
	.483	-.013	-.028	-.128	-.346	-.383	-.278
	.493	.043	.059	.026	-.188	-.278	-.153
	.503	.111	.118	.105	-.041	-.157	-.022
	.513	.236	.218	.196	.077	-.035	.125
Transition flare	.525	.100	.136	.146	.151	.122	.280
	.535	.032	.068	.080	.112	.116	.194
	.545	-.013	.009	.013	.055	.079	.137
	.555	-.083	-.084	-.079	-.042	-.002	.061
	.565	-.348	-.359	-.355	-.326	-.296	-.214
Main stage	.568	-.438	-.504	-.525	-.599	-.628	-.742
	.577	-.151	-.158	-.163	-.165	-.172	-.503
	.587	-.094	-.098	-.104	-.107	-.107	-.390
	.597	-.071	-.056	-.058	-.060	-.059	-.216
	.607	-.048	-.051	-.054	-.056	-.053	-.100
	.617	-.036	-.042	-.041	-.045	-.042	-.025
	.627	-.036	-.033	-.033	-.038	-.036	-.010
	.637	-.025	-.019	-.024	-.027	-.029	-.003
	.657	-.021	-.016	-.014	-.021	-.021	-.005
	.677	-.010	-.005	-.009	-.011	-.011	-.003
	.697	-.013	-.007	-.006	-.013	-.013	-.010
	.737	-.010	-.004	-.003	-.015	-.008	-.012
	.777	-.006	.003	-.002	-.003	-.004	-.008
	.785	-.006	.004	.001	-.002	-.002	-.008
	.817	-.006	.003	.001	-.002	-.002	-.009
	.857	-.007	-.001	-.004	-.007	-.007	-.015
	.877	-.009	-.002	-.005	-.007	-.008	-.015
	.897	-.010	-.003	-.006	-.009	-.010	-.017
	.917	-.012	-.004	-.006	-.010	-.010	-.018
	.957	-.022	-.015	-.017	-.021	-.022	-.029
	.997	-.071	-.069	-.074	-.083	-.088	-.101

TABLE 7.- PRESSURE COEFFICIENTS FOR CONFIGURATION 322 - Continued

(a) M = 0.40 to 0.95; $\alpha = 0^\circ$ - Concluded

	x/l	C_p for - $\phi = -60^\circ$					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.426	.475	.554	.575	.625	.654	.694
	.436	.308	.393	.416	.478	.512	.553
	.446	.075	.187	.217	.296	.344	.394
	.453	-1.495	-.922	-.843	-.738	-.688	-1.016
Upper stage	.458	-.513	-.742	-.700	-.583	-.515	-1.072
	.463	-.218	-.623	-.642	-.558	-.515	-.797
	.473	-.070	-.289	-.375	-.454	-.464	-.493
	.483	-.013	-.042	-.137	-.314	-.376	-.316
	.493	.043	.059	.022	-.181	-.272	-.185
	.503	.100	.114	.101	-.056	-.167	-.067
	.513	.236	.214	.196	.070	-.046	.074
Transition flare	.525	.100	.131	.138	.148	.129	.283
	.535	.032	.068	.080	.112	.112	.175
	.545	-.013	.004	.013	.055	.079	.137
	.555	-.106	-.103	-.096	-.060	-.015	.051
Main stage	.565	-.337	-.354	-.355	-.322	-.283	-.214
	.568	-.380	-.412	-.433	-.523	-.519	-.648
	.577	-.140	-.153	-.159	-.161	-.165	-.435
	.587	-.094	-.098	-.104	-.110	-.111	-.361
	.597	-.071	-.065	-.066	-.074	-.073	-.245
	.607	-.048	-.051	-.054	-.056	-.053	-.100
	.617	-.036	-.042	-.041	-.045	-.046	-.038
	.627	-.036	-.033	-.037	-.038	-.036	-.019
	.637	-.025	-.024	-.028	-.031	-.029	-.010
	.657	-.021	-.014	-.014	-.021	-.021	-.006
	.677	-.017	-.010	-.010	-.016	-.016	-.008
	.697	-.013	-.005	-.005	-.011	-.012	-.009
	.737	-.010	-.004	-.003	-.009	-.010	-.012
	.777	-.010	.001	-.002	-.004	-.005	-.011
	.785	-.006	.001	.000	-.004	-.004	-.011
	.817	-.004	.004	.002	-.001	-.002	-.008
	.857	-.009	-.001	-.004	-.007	-.007	-.015
	.877	-.009	-.001	-.004	-.007	-.008	-.015
	.897	-.010	-.002	-.005	-.008	-.008	-.016
	.917	-.013	-.007	-.010	-.013	-.014	-.021
	.957	-.022	-.015	-.018	-.021	-.023	-.030
	.997	-.074	-.072	-.075	-.085	-.089	-.105

	x/l	C_p for - $\phi = -30^\circ$					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.426	.475	.549	.571	.622	.654	.694
	.446	.075	.187	.225	.296	.344	.394
	.453	-1.277	-.802	-.733	-.647	-.619	-1.074
Upper stage	.473	-.048	-.344	-.450	-.500	-.471	-.483
	.493	.043	.063	.018	-.203	-.299	-.220
	.513	.236	.218	.196	.073	-.059	.061
Transition flare	.535	.032	.072	.084	.119	.099	.159
	.565	-.348	-.363	-.363	-.322	-.279	-.250
Main stage	.568	-.392	-.453	-.483	-.570	-.502	-.600
	.587	-.094	-.102	-.104	-.110	-.111	-.335
	.607	-.048	-.051	-.054	-.056	-.056	-.106
	.627	-.036	-.033	-.037	-.038	-.036	-.022
	.657	-.025	-.016	-.014	-.021	-.021	-.011
	.697	-.013	-.008	-.007	-.014	-.014	-.012
	.737	-.010	-.004	-.003	-.009	-.011	-.013
	.777	-.010	-.001	-.002	-.005	-.005	-.011
	.785	-.006	-.001	-.002	-.005	-.005	-.012
	.817	-.004	.005	.003	.000	-.001	-.007
	.857	-.009	.000	-.002	-.006	-.007	-.014
	.897	-.010	-.003	-.006	-.008	-.009	-.017

TABLE 7.- PRESSURE COEFFICIENTS FOR CONFIGURATION 322 - Continued

(b) M = 0.60; α = -10° to 10°

	x/l	C_p for - ϕ = 0°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.426	.728	.648	.590	.522	.457	.384	.281
	.436	.576	.479	.427	.369	.293	.238	.140
	.446	.333	.236	.184	.127	.068	.029	-.035
Upper stage	.453	-1.558	-1.489	-1.344	-1.258	-1.115	-.910	-.677
	.458	-.351	-.555	-.810	-.846	-.768	-.727	-.578
	.463	-.115	-.179	-.262	-.419	-.485	-.623	-.624
	.473	-.011	-.041	-.048	-.072	-.144	-.247	-.381
	.483	.041	.011	.004	-.003	-.011	-.051	-.127
	.493	.093	.063	.056	.043	.052	.024	-.012
	.503	.162	.132	.119	.107	.098	.070	.040
	.513	.369	.316	.286	.245	.196	.145	.092
Transition flare	.525	.230	.178	.147	.118	.086	.058	.028
	.535	.156	.097	.073	.049	.017	.001	-.024
	.545	.110	.046	.033	.003	-.029	-.052	-.071
	.555	.035	-.023	-.060	-.085	-.111	-.122	-.141
	.565	-.269	-.328	-.342	-.343	-.328	-.316	-.299
Main stage	.568	-.453	-.501	-.520	-.492	-.454	-.407	-.379
	.577	-.098	-.146	-.159	-.160	-.169	-.162	-.158
	.587	-.051	-.088	-.101	-.102	-.116	-.110	-.111
	.597	-.028	-.064	-.077	-.073	-.087	-.080	-.082
	.607	-.016	-.047	-.060	-.055	-.070	-.063	-.064
	.617	-.005	-.041	-.054	-.049	-.058	-.051	-.053
	.627	-.005	-.035	-.042	-.038	-.046	-.040	-.047
	.637	.006	-.023	-.037	-.032	-.040	-.034	-.035
	.657	.011	-.014	-.015	-.016	-.021	-.020	-.027
	.677	.013	-.014	-.011	-.014	-.019	-.018	-.026
	.697	.017	-.010	-.011	-.008	-.013	-.012	-.022
	.737	.017	-.008	-.011	-.007	-.011	-.012	-.024
	.777	.021	-.004	-.011	-.005	-.009	-.009	-.022
	.785	.026	.000	-.002	-.003	-.009	-.005	-.014
	.817	.029	.008	.000	.000	-.004	-.004	-.015
	.857	.022	.001	-.004	-.003	-.007	-.007	-.023
	.877	.025	.002	-.003	-.002	-.007	-.008	-.023
	.897	.021	-.002	-.007	-.005	-.010	-.011	-.027

	x/l	C_p for - ϕ = -30°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.426	.688	.620	.573	.527	.462	.390	.287
	.436	.497	.419	.376	.333	.274	.221	.132
	.446	.305	.219	.179	.138	.085	.052	-.024
Upper stage	.453	-1.388	-1.290	-1.169	-1.007	-.747	-.583	-.525
	.458	-.519	-.722	-.787	-.834	-.710	-.594	-.549
	.463	-.149	-.324	-.458	-.551	-.670	-.611	-.595
	.473	-.034	-.041	-.054	-.084	-.179	-.322	-.404
	.483	.018	.011	.016	.009	.018	-.068	-.145
	.493	.064	.051	.056	.049	.064	.024	-.018
	.503	.145	.132	.125	.112	.110	.076	.040
	.513	.346	.304	.280	.233	.202	.139	.109
Transition flare	.525	.179	.155	.142	.118	.086	.058	.017
	.535	.133	.091	.073	.049	.017	.001	-.035
	.545	.075	.028	.004	-.014	-.035	-.057	-.094
	.555	-.016	-.059	-.078	-.091	-.117	-.145	-.182
	.565	-.321	-.370	-.377	-.360	-.351	-.333	-.387
Main stage	.568	-.471	-.507	-.514	-.480	-.454	-.413	-.466
	.577	-.127	-.146	-.159	-.160	-.169	-.156	-.169
	.587	-.075	-.099	-.106	-.102	-.116	-.110	-.117
	.597	-.046	-.064	-.071	-.067	-.075	-.075	-.076
	.607	-.034	-.053	-.066	-.055	-.070	-.063	-.070
	.617	-.028	-.041	-.054	-.049	-.058	-.051	-.064
	.627	-.022	-.041	-.042	-.038	-.052	-.045	-.053
	.637	-.016	-.035	-.037	-.032	-.040	-.034	-.047
	.657	-.016	-.027	-.019	-.018	-.025	-.022	-.041
	.677	-.005	-.016	-.009	-.008	-.015	-.018	-.029
	.697	-.009	-.020	-.011	-.010	-.017	-.018	-.037
	.737	-.007	-.016	-.015	-.007	-.013	-.014	-.037
	.777	.003	-.010	-.005	-.012	-.013	-.011	-.035
	.785	-.001	-.012	-.013	-.005	-.005	-.009	-.033
	.817	.002	-.004	-.003	.000	-.004	-.008	-.034
	.857	-.004	-.009	-.008	-.004	-.008	-.012	-.036
	.877	-.006	-.011	-.009	-.005	-.008	-.013	-.038
	.897	-.007	-.012	-.010	-.005	-.011	-.015	-.039
	.917	-.007	-.014	-.012	-.007	-.012	-.017	-.041
	.957	-.022	-.025	-.021	-.018	-.024	-.030	-.051
	.997	-.106	-.089	-.077	-.070	-.080	-.095	-.128

TABLE 7.- PRESSURE COEFFICIENTS FOR CONFIGURATION 322 - Continued

(b) M = 0.60; α = -10° to 10° - Concluded

	x/l	C_p for - ϕ = -60°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.426	.559	.558	.545	.522	.479	.424	.320
	.436	.418	.405	.387	.358	.321	.283	.191
	.446	.192	.169	.156	.133	.113	.080	-.001
	.453	-1.470	-1.384	-1.274	-1.223	-.858	-.828	-.782
Upper stage	.458	-.582	-.699	-.747	-.748	-.670	-.657	-.687
	.463	-.242	-.335	-.441	-.465	-.583	-.571	-.612
	.473	-.097	-.070	-.071	-.112	-.219	-.305	-.347
	.483	-.057	-.018	.004	-.003	-.006	-.068	-.127
	.493	.001	.034	.050	.055	.064	.030	-.041
	.503	.070	.097	.113	.112	.104	.076	.011
	.513	.254	.264	.257	.233	.202	.185	.155
Transition flare	.525	.064	.097	.113	.106	.081	.047	-.018
	.535	.047	.051	.056	.043	.023	.001	-.071
	.545	-.005	-.006	-.002	-.014	-.041	-.057	-.123
	.555	-.112	-.104	-.094	-.114	-.119	-.146	-.206
	.565	-.398	-.393	-.377	-.360	-.351	-.398	-.457
Main stage	.568	-.453	-.449	-.421	-.399	-.390	-.430	-.478
	.577	-.180	-.169	-.159	-.154	-.169	-.174	-.216
	.587	-.139	-.122	-.112	-.102	-.116	-.121	-.158
	.597	-.110	-.088	-.083	-.073	-.081	-.086	-.128
	.607	-.098	-.070	-.066	-.055	-.070	-.075	-.111
	.617	-.086	-.070	-.060	-.049	-.058	-.063	-.099
	.627	-.086	-.064	-.048	-.038	-.052	-.057	-.093
	.637	-.075	-.053	-.042	-.032	-.040	-.051	-.088
	.657	-.077	-.051	-.025	-.018	-.027	-.038	-.076
	.677	-.063	-.042	-.018	-.013	-.023	-.034	-.070
	.697	-.050	-.033	-.011	-.008	-.019	-.030	-.064
	.737	-.059	-.037	-.013	-.012	-.013	-.026	-.055
	.777	-.059	-.033	-.009	-.008	-.011	-.020	-.047
	.785	-.059	-.033	-.013	-.014	-.009	-.020	-.045
	.817	-.053	-.026	-.009	.001	-.006	-.015	-.038
	.857	-.057	-.029	-.012	-.003	-.010	-.019	-.040
	.877	-.058	-.030	-.012	-.004	-.010	-.019	-.041
	.897	-.058	-.031	-.014	-.005	-.011	-.020	-.041
	.917	-.066	-.037	-.019	-.010	-.017	-.024	-.045
	.957	-.074	-.043	-.026	-.018	-.025	-.034	-.055
	.997	-.137	-.106	-.088	-.073	-.085	-.100	-.135

	x/l	C_p for - ϕ = -90°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.426	.418	.479	.511	.516	.508	.486	.416
	.446	.074	.107	.122	.138	.141	.125	.067
	.453	-1.149	-1.133	-1.105	-1.001	-.765	-.770	-.934
Upper stage	.473	-.172	-.127	-.135	-.118	-.219	-.230	-.185
	.493	-.063	.005	.050	.061	.069	.030	-.070
	.513	.185	.224	.246	.239	.236	.243	.166
Transition flare	.535	-.040	.017	.038	.049	.035	.013	-.059
	.565	-.480	-.416	-.389	-.366	-.375	-.415	-.487
	.568	-.547	-.490	-.468	-.440	-.454	-.494	-.559
Main stage	.587	-.180	-.140	-.118	-.108	-.122	-.133	-.192
	.607	-.133	-.088	-.071	-.055	-.070	-.080	-.146
	.627	-.116	-.070	-.054	-.038	-.052	-.063	-.128
	.657	-.108	-.058	-.023	-.018	-.031	-.049	-.109
	.697	-.100	-.053	-.021	-.012	-.023	-.044	-.105
	.737	-.094	-.047	-.013	-.008	-.017	-.038	-.098
	.777	-.088	-.043	-.011	-.008	-.013	-.034	-.094
	.785	-.090	-.047	-.011	-.003	-.013	-.032	-.088
	.817	-.079	-.032	-.009	.002	-.007	-.025	-.081
	.857	-.083	-.037	-.013	-.002	-.011	-.030	-.084
	.897	-.085	-.039	-.016	-.005	-.014	-.034	-.086

TABLE 7.- PRESSURE COEFFICIENTS FOR CONFIGURATION 322 - Continued

(c) $M = 0.80$; $\alpha = -10^\circ$ to 10°

	x/l	C_p for - $\phi = 0^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.426	.815		.667	.602	.532		.363
	.436	.664		.513	.446	.389		.228
	.446	.450		.310	.260	.205		.070
Upper stage	.453	-1.308		-.948	-.743	-.593		-.430
	.458	-.836		-.749	-.619	-.498		-.398
	.463	-.513		-.692	-.615	-.533		-.452
	.473	-.016		-.376	-.446	-.475		-.472
	.483	.034		-.091	-.211	-.313		-.352
	.493	.088		.047	-.034	-.140		-.202
	.503	.172		.136	.077	-.005		-.079
	.513	.386		.262	.177	.087		.006
Transition flare	.525	.279		.197	.157	.102		.040
	.535	.198		.124	.100	.063		.014
	.545	.149		.067	.047	.014		-.025
	.555	.068		-.022	-.046	-.068		-.099
Main stage	.565	-.278		-.366	-.339	-.287		-.256
	.568	-.804		-.725	-.558	-.429		-.328
	.577	-.125		-.169	-.166	-.157		-.145
	.587	-.043		-.096	-.100	-.103		-.095
	.597	-.035		-.068	-.073	-.075		-.068
	.607	-.020		-.049	-.054	-.056		-.052
	.617	-.008		-.037	-.042	-.044		-.037
	.627	-.001		-.030	-.038	-.037		-.033
	.637	.007		-.018	-.027	-.025		-.025
	.657	.018		-.011	-.014	-.018		-.016
	.677	.020		-.010	-.011	-.016		-.015
	.697	.024		-.005	-.007	-.012		-.012
	.737	.026		-.002	-.005	-.009		-.012
	.777	.029		.002	-.002	-.004		-.012
	.785	.036		.005	.003	.000		-.003
	.817	.037		.007	.004	-.001		-.008
	.857	.030		.001	.000	-.004		-.016
	.877	.031		.003	.001	-.004		-.016
	.897	.026		-.001	-.002	-.007		-.020

	x/l	C_p for - $\phi = -30^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.426	.710		.659	.598	.540		.371
	.436	.592		.483	.427	.376		.224
	.446	.416		.306	.256	.213		.077
Upper stage	.453	-1.296		-.871	-.754	-.511		-.582
	.458	-.817		-.707	-.623	-.471		-.499
	.463	-.559		-.680	-.600	-.498		-.502
	.473	-.074		-.407	-.430	-.467		-.479
	.483	.011		-.110	-.226	-.317		-.344
	.493	.057		.032	-.049	-.148		-.202
	.503	.149		.128	.070	-.017		-.033
	.513	.360		.247	.165	.079		.010
Transition flare	.525	.221		.189	.157	.106		.025
	.535	.171		.120	.100	.063		-.002
	.545	.110		.055	.035	.006		-.053
	.555	.015		-.041	-.062	-.084		-.150
Main stage	.565	-.329		-.386	-.347	-.307		-.373
	.568	-.921		-.729	-.555	-.437		-.507
	.577	-.148		-.166	-.166	-.153		-.153
	.587	-.090		-.100	-.104	-.103		-.107
	.597	-.047		-.057	-.058	-.060		-.064
	.607	-.043		-.049	-.054	-.056		-.060
	.617	-.035		-.037	-.042	-.044		-.048
	.627	-.028		-.033	-.038	-.037		-.048
	.637	-.020		-.022	-.027	-.029		-.037
	.657	-.010		-.017	-.018	-.021		-.032
	.677	.003		-.005	-.006	-.012		-.025
	.697	-.002		-.008	-.008	-.013		-.028
	.737	.001		-.005	-.005	-.009		-.026
	.777	.013		.003	.002	-.003		-.024
	.785	.007		.002	.002	.000		-.021
	.817	.010		.004	.004	-.001		-.023
	.857	.003		-.003	-.001	-.005		-.027
	.877	.003		-.003	-.001	-.006		-.029
	.897	.000		-.004	-.003	-.009		-.030
	.917	.000		-.006	-.004	-.009		-.032
	.957	-.014		-.016	-.015	-.021		-.044
	.997	-.098		-.076	-.073	-.084		-.122

TABLE 7.- PRESSURE COEFFICIENTS FOR CONFIGURATION 322 - Continued

(c) M = 0.80; α = -10° to 10° - Concluded

	x/l	C_p for - ϕ = -60°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.426	.649		.629	.598	.555		.401
	.436	.507		.475	.444	.408		.273
	.446	.311		.283	.252	.228		.104
	.453	-1.063		-1.007	-.820	-.597		-.586
Upper stage	.458	-.747		-.726	-.665	-.525		-.545
	.463	-.605		-.630	-.619	-.541		-.556
	.473	-.274		-.391	-.407	-.475		-.475
	.483	-.085		-.176	-.223	-.290		-.321
	.493	-.016		-.002	-.053	-.113		-.183
	.503	.065		.093	.058	.006		-.075
Transition flare	.513	.264		.212	.154	.106		.060
	.525	.095		.158	.157	.121		-.013
	.535	.076		.109	.100	.075		-.037
	.545	.019		.044	.031	.014		-.092
	.555	-.082		-.060	-.081	-.080		-.176
	.565	-.384		-.382	-.347	-.334		-.475
Main stage	.568	-.932		-.620	-.469	-.425		-.860
	.577	-.206		-.166	-.162	-.157		-.204
	.587	-.152		-.107	-.104	-.110		-.145
	.597	-.117		-.072	-.069	-.075		-.114
	.607	-.098		-.053	-.054	-.056		-.099
	.617	-.094		-.045	-.042	-.044		-.087
	.627	-.090		-.037	-.038	-.037		-.079
	.637	-.078		-.026	-.027	-.033		-.072
	.657	-.069		-.022	-.016	-.022		-.063
	.677	-.056		-.016	-.012	-.018		-.057
	.697	-.043		-.010	-.007	-.015		-.051
	.737	-.055		-.010	-.003	-.011		-.042
	.777	-.051		-.005	.001	-.007		-.034
	.785	-.055		-.006	.001	-.004		-.032
	.817	-.047		-.001	.004	-.002		-.029
	.857	-.052		-.006	-.001	-.006		-.031
	.877	-.052		-.007	-.001	-.007		-.031
	.897	-.053		-.008	-.001	-.008		-.034
	.917	-.059		-.013	-.007	-.014		-.036
	.957	-.068		-.020	-.015	-.021		-.047
	.997	-.137		-.086	-.077	-.084		-.127

	x/l	C_p for - ϕ = -90°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.426	.507		.592	.594	.589		.498
	.446	.195		.253	.256	.250		.190
	.453	-.931		-.804	-.768	-.675		-.753
Upper stage	.473	-.401		-.503	-.496	-.444		-.464
	.493	-.112		-.041	-.061	-.109		-.117
Transition flare	.513	.168		.182	.169	.140		.163
	.535	-.012		.097	.108	.094		-.021
	.565	-.473		-.393	-.351	-.365		-.471
Main stage	.568	-.998		-.632	-.539	-.545		-.989
	.587	-.183		-.111	-.108	-.110		-.184
	.607	-.136		-.057	-.054	-.056		-.134
	.627	-.117		-.037	-.034	-.037		-.118
	.657	-.099		-.024	-.021	-.025		-.102
	.697	-.091		-.018	-.008	-.021		-.094
	.737	-.082		-.011	-.003	-.012		-.083
	.777	-.080		-.008	-.001	-.008		-.078
	.785	-.084		-.009	-.001	-.007		-.074
	.817	-.070		-.002	.006	-.002		-.068
	.857	-.074		-.008	.000	-.007		-.073
	.897	-.075		-.011	-.003	-.010		-.075

TABLE 7.- PRESSURE COEFFICIENTS FOR CONFIGURATION 322 - Continued

(d) $M = 1.00$; $\alpha = -10^\circ$ to 10°

	x/l	C_p for - $\phi = 0^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.426	.944	.866	.801	.736	.674	.605	.516
	.436	.813	.735	.670	.607	.546	.480	.396
	.446	.639	.568	.506	.455	.399	.342	.268
Upper stage	.453	-.804	-.848	-.868	-.884	-.898	-.902	-.657
	.458	-.817	-.903	-.951	-.994	-1.026	-.849	-.484
	.463	-.606	-.741	-.813	-.877	-.934	-.687	-.512
	.473	-.330	-.484	-.584	-.669	-.649	-.522	-.536
	.483	-.190	-.334	-.418	-.498	-.264	-.408	-.496
	.493	-.110	-.254	-.321	-.146	-.172	-.295	-.417
	.503	.125	.131	.132	.104	-.071	-.179	-.310
	.513	.451	.393	.321	.705	.027	-.056	-.184
Transition flare	.525	.368	.353	.332	.293	.127	.041	-.066
	.535	.292	.267	.253	.244	.160	.087	.008
	.545	.268	.231	.211	.192	.139	.081	.030
	.555	.228	.191	.165	.132	.072	.017	-.007
	.565	.018	-.016	-.055	-.098	-.190	-.225	-.215
Main stage	.568	-.518	-.537	-.558	-.570	-.566	-.455	-.399
	.577	-.352	-.408	-.444	-.468	-.365	-.304	-.276
	.587	-.256	-.321	-.366	-.388	-.340	-.304	-.263
	.597	-.194	-.247	-.289	-.314	-.303	-.270	-.220
	.607	-.166	-.213	-.243	-.255	-.242	-.214	-.174
	.617	-.154	-.188	-.206	-.194	-.186	-.171	-.146
	.627	-.148	-.170	-.166	-.150	-.143	-.137	-.121
	.637	-.133	-.136	-.119	-.116	-.112	-.109	-.103
	.657	-.094	-.079	-.085	-.083	-.080	-.081	-.076
	.677	-.049	-.065	-.073	-.073	-.070	-.068	-.065
	.697	-.036	-.051	-.059	-.061	-.059	-.057	-.049
	.737	-.029	-.047	-.055	-.056	-.043	-.033	-.007
	.777	.026	.005	.012	.009	.017	.017	.015
	.785	.053	.032	.033	.028	.030	.030	.028
	.817	.065	.050	.040	.034	.032	.029	.020
	.857	.056	.040	.032	.029	.026	.021	.008
	.877	.060	.042	.032	.028	.024	.020	.006
	.897	.053	.035	.025	.021	.019	.015	-.001

	x/l	C_p for - $\phi = -30^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.426	.905	.851	.792	.739	.677	.617	.522
	.436	.754	.727	.646	.595	.541	.487	.396
	.446	.603	.547	.500	.452	.405	.357	.271
Upper stage	.453	-.946	-.959	-.974	-.989	-.991	-.995	-.762
	.458	-.872	-.946	-.987	-1.018	-1.041	-.904	-.548
	.463	-.682	-.790	-.853	-.905	-.949	-.717	-.552
	.473	-.336	-.487	-.581	-.657	-.576	-.528	-.545
	.483	-.174	-.349	-.428	-.498	-.255	-.402	-.490
	.493	-.150	-.275	-.311	-.109	-.178	-.298	-.411
	.503	.095	.128	.126	.089	-.087	-.179	-.310
	.513	.418	.381	.302	.187	.020	-.059	-.197
Transition flare	.525	.307	.325	.323	.256	.215	.072	-.078
	.535	.259	.261	.253	.244	.163	.087	-.026
	.545	.219	.210	.195	.183	.145	.078	-.010
	.555	.170	.158	.138	.113	.072	.017	-.057
	.565	-.028	-.047	-.077	-.120	-.184	-.209	-.246
Main stage	.568	-.592	-.602	-.620	-.632	-.640	-.671	-.711
	.577	-.395	-.432	-.459	-.465	-.387	-.381	-.421
	.587	-.281	-.330	-.366	-.389	-.343	-.316	-.294
	.597	-.185	-.213	-.234	-.249	-.232	-.211	-.183
	.607	-.200	-.225	-.246	-.249	-.245	-.217	-.186
	.617	-.188	-.198	-.206	-.194	-.186	-.171	-.158
	.627	-.182	-.185	-.169	-.157	-.146	-.140	-.140
	.637	-.170	-.145	-.126	-.119	-.115	-.119	-.127
	.657	-.111	-.094	-.090	-.086	-.085	-.090	-.105
	.677	-.066	-.067	-.069	-.067	-.066	-.071	-.089
	.697	-.066	-.064	-.064	-.062	-.061	-.065	-.082
	.737	-.053	-.055	-.057	-.055	-.044	-.037	-.044
	.777	.019	-.003	.012	.012	.018	.014	-.018
	.785	.049	.024	.030	.028	.028	.021	-.011
	.817	.040	.040	.037	.034	.031	.021	-.013
	.857	.031	.030	.027	.028	.023	.015	-.014
	.877	.030	.028	.026	.025	.021	.012	-.014
	.897	.029	.025	.021	.021	.018	.007	-.015
	.917	.028	.024	.018	.018	.014	.004	-.016
	.957	.016	.013	.007	.004	-.001	-.012	-.028
	.997	-.039	-.055	-.076	-.100	-.117	-.136	-.152

TABLE 7.- PRESSURE COEFFICIENTS FOR CONFIGURATION 322 - Continued

(d) M = 1.00; α = -10° to 10° - Concluded

	x/l	C_p for - ϕ = -60°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.426	.789	.786	.769	.736	.698	.647	.552
	.436	.663	.657	.631	.604	.564	.519	.435
	.446	.508	.502	.476	.449	.414	.378	.304
Upper stage	.453	-.854	-.860	-.878	-.890	-.892	-.899	-.842
	.458	-.945	-.979	-1.000	-1.018	-1.032	-1.008	-.628
	.463	-.719	-.823	-.871	-.908	-.937	-.837	-.604
	.473	-.352	-.566	-.623	-.669	-.692	-.528	-.561
	.483	-.269	-.407	-.464	-.507	-.304	-.381	-.484
	.493	-.239	-.272	-.253	-.097	-.169	-.255	-.383
	.503	-.006	.097	.108	.092	-.062	-.118	-.270
	.513	.283	.311	.266	.184	.091	.020	-.120
Transition flare	.525	.152	.249	.293	.296	.245	.145	-.063
	.535	.137	.210	.232	.244	.206	.120	-.026
	.545	.119	.173	.183	.183	.154	.087	-.029
	.555	.078	.123	.130	.110	.093	.036	-.062
	.565	-.093	-.065	-.077	-.108	-.125	-.154	-.218
Main stage	.568	-.574	-.553	-.552	-.564	-.578	-.603	-.652
	.577	-.487	-.475	-.474	-.465	-.489	-.538	-.606
	.587	-.386	-.377	-.382	-.385	-.371	-.433	-.526
	.597	-.321	-.306	-.311	-.311	-.291	-.291	-.328
	.607	-.296	-.269	-.258	-.249	-.232	-.220	-.223
	.617	-.284	-.232	-.203	-.194	-.186	-.180	-.189
	.627	-.275	-.185	-.163	-.157	-.152	-.153	-.174
	.637	-.200	-.148	-.129	-.119	-.121	-.134	-.164
	.657	-.161	-.114	-.093	-.085	-.090	-.107	-.138
	.677	-.134	-.094	-.078	-.077	-.077	-.094	-.117
	.697	-.107	-.074	-.063	-.060	-.065	-.080	-.097
	.737	-.104	-.071	-.060	-.054	-.050	-.056	-.044
	.777	-.027	-.012	.010	.012	.017	.006	-.014
	.785	-.033	-.002	.022	.025	.023	.013	-.010
	.817	-.013	.020	.033	.034	.030	.017	-.007
	.857	-.022	.009	.023	.028	.022	.011	-.010
	.877	-.023	.009	.021	.025	.020	.009	-.011
	.897	-.024	.006	.017	.022	.017	.005	-.014
	.917	-.034	-.001	.009	.014	.010	-.001	-.018
	.557	-.035	-.006	.001	.004	-.001	-.013	-.029
	.997	-.103	-.086	-.093	-.102	-.115	-.134	-.155

	x/l	C_p for - ϕ = -90°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.426	.651	.714	.733	.733	.725	.701	.641
	.446	.394	.439	.449	.449	.438	.426	.378
Upper stage	.453	-.984	-.978	-.983	-.989	-.984	-.985	-.981
	.473	-.514	-.633	-.669	-.678	-.674	-.598	-.524
	.493	-.333	-.205	-.149	-.085	-.142	-.212	-.334
	.513	.107	.219	.202	.181	.161	.172	.108
Transition flare	.535	.021	.167	.223	.244	.215	.148	.011
	.565	-.199	-.118	-.105	-.123	-.110	-.129	-.187
Main stage	.568	-.642	-.593	-.579	-.576	-.578	-.591	-.637
	.587	-.472	-.426	-.405	-.385	-.414	-.440	-.488
	.607	-.379	-.281	-.249	-.249	-.235	-.270	-.390
	.627	-.222	-.170	-.150	-.150	-.152	-.165	-.226
	.657	-.184	-.121	-.095	-.086	-.096	-.127	-.186
	.697	-.150	-.093	-.070	-.063	-.069	-.096	-.149
	.737	-.121	-.077	-.059	-.053	-.056	-.078	-.107
	.777	-.051	-.015	.009	.011	.012	-.006	-.052
	.785	-.059	-.009	.018	.022	.020	.004	-.042
	.817	-.035	.012	.030	.036	.030	.010	-.037
	.857	-.044	.001	.021	.029	.021	-.002	-.049
	.897	-.049	-.003	.014	.021	.013	-.008	-.055

TABLE 7.- PRESSURE COEFFICIENTS FOR CONFIGURATION 322 - Continued

(e) M = 1.20; α = -10° to 10°

	x/l	C_p for - ϕ = 0°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.426	1.071	.988	.927	.867	.808	.742	.648
	.436	.949	.869	.810	.756	.694	.633	.545
	.446	.800	.729	.675	.628	.577	.524	.449
Upper stage	.453	-.449	-.481	-.495	-.510	-.522	-.531	-.542
	.458	-.490	-.557	-.593	-.629	-.654	-.678	-.702
	.463	-.327	-.432	-.496	-.548	-.589	-.629	-.667
	.473	-.145	-.258	-.335	-.404	-.462	-.512	-.572
	.483	-.063	-.161	-.229	-.293	-.345	-.397	-.329
	.493	-.034	-.112	-.161	-.208	-.247	-.272	-.106
	.503	-.034	-.093	-.126	-.154	-.087	.041	-.060
	.513	.345	.281	.253	.225	.186	.128	.014
Transition flare	.525	.374	.340	.312	.292	.253	.200	.100
	.535	.320	.280	.261	.254	.240	.211	.154
	.545	.320	.269	.247	.230	.215	.198	.154
	.555	.331	.275	.244	.216	.191	.163	.127
	.565	.207	.172	.142	.103	.048	-.008	-.050
Main stage	.568	-.231	-.255	-.267	-.281	-.299	-.307	-.264
	.577	-.152	-.192	-.212	-.227	-.236	-.222	-.198
	.587	-.091	-.140	-.171	-.186	-.198	-.200	-.198
	.597	-.069	-.110	-.135	-.153	-.165	-.176	-.179
	.607	-.045	-.088	-.111	-.128	-.140	-.148	-.143
	.617	-.039	-.077	-.097	-.109	-.115	-.115	-.110
	.627	-.031	-.069	-.083	-.093	-.094	-.090	-.082
	.637	-.017	-.055	-.064	-.071	-.069	-.068	-.058
	.657	-.024	-.050	-.059	-.053	-.043	-.038	-.030
	.677	-.018	-.028	-.041	-.037	-.033	-.024	-.023
	.697	-.011	-.031	-.035	-.027	-.016	-.013	-.018
	.737	-.013	-.021	-.020	-.031	-.025	-.024	-.010
	.777	.017	-.011	-.028	-.021	-.024	-.026	-.011
	.785	.027	-.004	-.016	-.013	-.016	-.014	.000
	.817	.025	-.001	-.003	-.019	-.016	-.010	-.006
	.857	.022	.012	-.008	-.002	.002	-.007	-.017
	.877	.031	-.002	-.006	.000	-.002	-.005	-.013
	.897	.016	-.002	.001	-.004	-.007	-.016	-.023

	x/l	C_p for - ϕ = -30°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.426	1.028	.970	.919	.867	.810	.747	.654
	.436	.898	.840	.793	.745	.696	.641	.553
	.446	.768	.710	.667	.623	.582	.534	.452
Upper stage	.453	-.564	-.588	-.597	-.600	-.607	-.613	-.619
	.458	-.539	-.584	-.620	-.651	-.668	-.686	-.708
	.463	-.389	-.456	-.504	-.550	-.589	-.623	-.659
	.473	-.159	-.264	-.335	-.396	-.448	-.498	-.553
	.483	-.093	-.174	-.235	-.290	-.337	-.381	-.395
	.493	-.074	-.133	-.175	-.217	-.256	-.280	-.109
	.503	-.055	-.098	-.123	-.143	-.087	.014	-.063
	.513	.316	.278	.253	.228	.189	.130	.014
Transition flare	.525	.323	.315	.306	.292	.264	.208	.122
	.535	.296	.280	.261	.254	.240	.208	.146
	.545	.274	.245	.234	.222	.204	.181	.141
	.555	.269	.242	.223	.203	.180	.154	.103
	.565	.169	.145	.120	.084	.043	.000	-.030
Main stage	.568	-.272	-.288	-.300	-.312	-.334	-.346	-.384
	.577	-.176	-.206	-.218	-.229	-.239	-.252	-.280
	.587	-.116	-.154	-.174	-.186	-.198	-.206	-.211
	.597	-.067	-.091	-.105	-.112	-.121	-.129	-.129
	.607	-.078	-.099	-.116	-.125	-.137	-.148	-.146
	.617	-.061	-.085	-.097	-.106	-.115	-.121	-.118
	.627	-.059	-.082	-.086	-.093	-.096	-.099	-.096
	.637	-.050	-.066	-.070	-.073	-.074	-.079	-.071
	.657	-.039	-.048	-.052	-.050	-.040	-.044	-.053
	.677	-.036	-.028	-.036	-.031	-.031	-.030	-.050
	.697	-.041	-.041	-.035	-.033	-.029	-.025	-.053
	.737	-.038	-.033	-.025	-.029	-.024	-.033	-.053
	.777	- 006	-.015	-.024	-.012	-.021	-.028	-.060
	.785	.000	-.012	-.015	-.009	-.013	-.021	-.054
	.817	-.001	-.013	-.007	-.019	-.016	-.024	-.068
	.857	-.006	.004	-.009	-.009	-.007	-.022	-.064
	.877	.001	-.012	-.007	-.002	-.004	-.019	-.060
	.897	-.008	-.009	-.004	-.001	-.003	-.021	-.052
	.917	-.012	-.004	-.005	-.006	-.006	-.019	-.041
	.957	-.013	-.015	-.013	-.016	-.015	-.020	-.034
	.997	-.004	-.020	-.033	-.053	-.073	-.091	-.082

TABLE 7.- PRESSURE COEFFICIENTS FOR CONFIGURATION 322 - Concluded

(e) M = 1.20; α = -10° to 10° - Concluded

	x/l	C_p for - ϕ = -60°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.426	.914	.911	.895	.864	.834	.782	.685
	.436	.800	.795	.779	.748	.715	.670	.584
	.446	.[illegible]	.668	.646	.623	.596	.556	.481
Upper stage	.453	-.556	-.566	-.575	-.581	-.582	-.591	-.608
	.458	-.612	-.630	-.642	-.653	-.660	-.669	-.691
	.463	-.447	-.505	-.542	-.575	-.595	-.618	-.642
	.473	-.264	-.323	-.365	-.404	-.427	-.454	-.479
	.483	-.186	-.226	-.265	-.301	-.329	-.354	-.381
	.493	-.159	-.174	-.197	-.217	-.237	-.269	-.299
	.503	-.145	-.139	-.140	-.146	-.136	-.136	-.106
Transition flare	.513	.180	.221	.234	.225	.197	.160	.087
	.525	.204	.261	.282	.289	.264	.211	.111
	.535	.202	.249	.253	.254	.240	.190	.084
	.545	.180	.210	.223	.222	.204	.165	.081
	.555	.173	.208	.225	.219	.198	.167	.106
	.565	.112	.126	.120	.098	.072	.054	.005
Main stage	.568	-.278	-.263	-.259	-.268	-.277	-.299	-.338
	.577	-.248	-.241	-.229	-.229	-.241	-.272	-.327
	.587	-.198	-.189	-.182	-.186	-.198	-.236	-.294
	.597	-.163	-.151	-.152	-.147	-.159	-.189	-.258
	.607	-.149	-.132	-.127	-.125	-.137	-.156	-.209
	.617	-.148	-.121	-.105	-.106	-.115	-.132	-.168
	.627	-.146	-.107	-.094	-.093	-.099	-.118	-.146
	.637	-.130	-.088	-.078	-.076	-.077	-.096	-.121
	.657	-.121	-.061	-.051	-.037	-.043	-.066	-.099
	.677	-.107	-.059	-.043	-.036	-.042	-.057	-.089
	.697	-.093	-.057	-.036	-.034	-.041	-.048	-.079
	.737	-.096	-.052	-.032	-.030	-.030	-.050	-.062
	.777	-.048	-.039	-.027	-.013	-.025	-.036	-.050
	.785	-.056	-.040	-.019	-.009	-.017	-.029	-.049
	.817	-.058	-.023	-.012	-.017	-.016	-.032	-.051
	.857	-.067	-.017	-.015	-.013	-.020	-.031	-.049
	.877	-.056	-.030	-.008	-.003	-.006	-.023	-.045
	.897	-.063	-.029	-.010	.000	-.002	-.017	-.035
	.917	-.073	-.032	-.018	-.007	-.008	-.021	-.031
	.957	-.070	-.036	-.016	-.014	-.018	-.019	-.034
	.997	-.066	-.046	-.042	-.054	-.067	-.089	-.106

	x/l	C_p for - ϕ = -90°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.426	.776	.837	.858	.864	.858	.837	.773
	.446	.564	.604	.619	.623	.617	.601	.547
Upper stage	.453	-.619	-.612	-.614	-.611	-.599	-.602	-.608
	.473	-.376	-.394	-.406	-.412	-.405	-.403	-.395
	.493	-.262	-.226	-.218	-.219	-.220	-.234	-.264
Transition flare	.513	.115	.189	.218	.222	.213	.187	.116
	.535	.112	.202	.244	.257	.245	.198	.103
	.565	.023	.073	.088	.090	.089	.079	.019
Main stage	.568	-.335	-.299	-.281	-.279	-.282	-.294	-.335
	.587	-.256	-.217	-.193	-.183	-.195	-.222	-.277
	.607	-.210	-.159	-.138	-.128	-.137	-.170	-.231
	.627	-.212	-.118	-.100	-.093	-.096	-.123	-.209
	.657	-.148	-.077	-.048	-.040	-.047	-.080	-.142
	.697	-.142	-.078	-.046	-.034	-.048	-.071	-.137
	.737	-.115	-.063	-.038	-.031	-.032	-.063	-.118
	.777	-.082	-.048	-.027	-.018	-.024	-.049	-.098
	.785	-.093	-.051	-.028	-.010	-.022	-.048	-.102
	.817	-.081	-.029	-.013	-.011	-.016	-.041	-.091
	.857	-.087	-.030	-.017	-.009	-.027	-.049	-.089
	.897	-.087	-.041	-.017	-.006	-.006	-.026	-.078

TABLE [illegible].- PRESSURE COEFFICIENTS FOR CONFIGURATION 123

(a) M = 0.40 to 0.95; α = 0°

	x/l	C_p for - β = 0°					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.410	.224	.247	.263	.283	.294	.324
	.420	.191	.211	.227	.248	.271	.302
	.430	.158	.171	.186	.209	.231	.262
	.450	.069	.072	.088	.121	.146	.183
	.460	-.042	-.036	-.015	.037	.076	.127
	.465	-.166	-.175	-.137	-.049	.007	.067
	.471	-.760	-1.137	-1.173	-.917	-.779	-.657
Upper stage	.476	-.223	-.298	-.385	-.648	-.924	-.808
	.481	-.110	-.137	-.166	-.338	-.513	-.714
	.491	-.019	-.022	-.019	-.041	-.122	-.179
	.501	.026	.038	.044	.078	.069	-.001
	.511	.083	.098	.107	.140	.174	.141
	.521	.162	.190	.204	.234	.266	.289
	.531	.344	.374	.385	.407	.419	.412
Transition flare	.539	.205	.238	.251	.291	.333	.391
	.546	.115	.128	.143	.191	.239	.314
	.552	.026	.028	.044	.106	.155	.225
	.562	-.214	-.231	-.197	-.089	-.023	.053
Main stage	.568	-.611	-1.066	-1.343	-1.118	-.965	-.836
	.577	-.167	-.216	-.230	-.574	-.777	-.671
	.587	-.088	-.119	-.124	-.092	-.586	-.571
	.597	-.065	-.077	-.082	-.052	-.081	-.454
	.607	-.042	-.054	-.057	-.045	.003	-.351
	.617	-.031	-.045	-.048	-.038	.010	-.234
	.627	-.019	-.031	-.036	-.034	.003	-.069
	.637	-.008	-.022	-.027	-.027	-.003	-.005
	.657	-.004	-.013	-.012	-.016	-.012	.031
	.677	.003	-.010	-.009	-.012	-.011	.029
	.697	.003	-.007	-.006	-.010	-.011	.017
	.737	.003	-.004	-.005	-.009	-.012	.000
	.777	.011	.001	.002	-.008	-.010	-.001
	.785	.015	.006	.006	.001	-.002	.002
	.817	.011	.004	.005	.001	-.004	-.002
	.857	.011	.001	.001	-.002	-.007	-.007
	.877	.009	.002	.002	-.002	-.006	-.007
	.897	.006	-.001	-.001	-.004	-.009	-.010

	x/l	C_p for - β = -30°					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.410	.224	.242	.251	.272	.291	.321
	.420	.180	.202	.214	.237	.255	.287
	.430	.147	.166	.186	.209	.225	.258
	.450	.056	.068	.084	.118	.142	.183
	.460	-.042	-.041	-.019	.034	.073	.124
	.465	-.168	-.175	-.137	-.052	.007	.067
	.471	-.806	-1.133	-1.190	-1.074	-.926	-.793
Upper stage	.476	-.223	-.303	-.401	-.609	-.907	-.795
	.481	-.099	-.123	-.166	-.374	-.411	-.727
	.491	-.019	-.022	-.019	-.041	-.183	-.156
	.501	.037	.043	.048	.085	.055	-.024
	.511	.083	.098	.107	.140	.171	.108
	.521	.162	.199	.208	.237	.266	.254
	.531	.344	.383	.393	.414	.419	.370
Transition flare	.539	.205	.238	.251	.299	.336	.397
	.546	.071	.078	.098	.156	.195	.263
	.552	.026	.028	.048	.106	.155	.225
	.562	-.214	-.231	-.202	-.100	-.034	.043
Main stage	.568	-.565	-.909	-1.048	-1.068	-.924	-.794
	.577	-.167	-.207	-.221	-.509	-.791	-.681
	.587	-.088	-.119	-.124	-.081	-.538	-.529
	.597	-.054	-.064	-.065	-.041	-.057	-.344
	.607	-.042	-.054	-.057	-.045	.003	-.354
	.617	-.031	-.045	-.044	-.038	.007	-.244
	.627	-.019	-.031	-.036	-.034	.000	-.079
	.637	-.008	-.027	-.027	-.027	-.003	-.011
	.657	-.008	-.016	-.013	-.017	-.012	.029
	.677	.003	-.004	-.001	-.006	-.005	.032
	.697	.003	-.005	-.005	-.010	-.012	.016
	.737	.007	-.002	-.001	-.005	-.011	.002
	.777	.011	.003	.004	.000	-.005	.001
	.785	.015	.006	.008	.002	-.002	.002
	.817	.011	.004	.006	.001	-.003	-.001
	.857	.009	.000	.002	-.003	-.007	-.008
	.877	.008	.000	.001	-.003	-.008	-.009
	.897	.006	-.002	.000	-.005	-.010	-.011
	.917	.006	-.002	-.001	-.006	-.010	-.012
	.957	-.004	-.013	-.012	-.017	-.022	-.023
	.997	-.056	-.070	-.069	-.074	-.085	-.097

TABLE IV.- AERODYNAMIC COEFFICIENTS FOR CONFIGURATION 123 - Continued

(a) M = 0.40 to 0.95; α = 0° - Concluded

	x/l	C_p for -					
		ϕ = -90°					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.410	.224	.242	.251	.272	.291	.318
	.420	.180	.198	.214	.237	.255	.287
	.430	.147	.162	.178	.199	.222	.255
	.450	.047	.064	.080	.111	.142	.180
	.460	-.054	-.050	-.023	.027	.073	.121
	.465	-.076	-.082	-.074	-.074	-.085	-.099
	.471	-.943	-1.239	-1.300	-1.114	-.967	-.832
Upper stage	.476	-.201	-.294	-.401	-.416	-.887	-.821
	.481	-.087	-.109	-.149	-.363	-.411	-.614
	.491	-.019	-.022	-.015	-.027	-.176	-.163
	.501	.026	.038	.044	.082	.038	-.059
	.511	.083	.098	.107	.143	.174	.079
	.521	.162	.180	.200	.234	.259	.225
	.531	.344	.374	.376	.407	.392	.341
Transition flare	.539	.205	.238	.251	.299	.336	.397
	.546	.104	.128	.148	.199	.242	.311
	.552	.026	.024	.040	.102	.148	.219
	.562	-.214	-.241	-.210	-.104	-.044	.021
Main stage	.568	-.634	-1.075	-1.335	-1.118	-.968	-.836
	.577	-.167	-.247	-.217	-.473	-.794	-.636
	.587	-.088	-.119	-.124	-.081	-.521	-.516
	.597	-.054	-.073	-.078	-.049	-.071	-.425
	.607	-.031	-.054	-.057	-.045	.003	-.357
	.617	-.031	-.045	-.044	-.038	.003	-.251
	.627	-.019	-.031	-.036	-.034	-.003	-.082
	.637	-.008	-.027	-.027	-.027	-.006	-.014
	.657	-.004	-.014	-.013	-.017	-.011	.027
	.677	.000	-.009	-.009	-.012	-.013	-.023
	.697	.003	-.004	-.005	-.008	-.014	.018
	.737	.007	-.002	-.001	-.005	-.013	.003
	.777	.011	.001	.004	.000	-.005	.000
	.785	.011	.003	.005	.000	-.005	.000
	.817	.011	.005	.006	.002	-.003	-.001
	.857	.009	.001	.002	-.002	-.007	-.008
	.877	.008	.000	.001	-.003	-.008	-.009
	.897	.008	-.001	.000	-.004	-.009	-.010
	.917	.005	-.005	-.005	-.008	-.014	-.015
	.957	-.004	-.013	-.013	-.017	-.022	-.023
	.997	-.056	-.070	-.069	-.074	-.086	-.096

	x/l	C_p for -					
		ϕ = -90°					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.406	.257	.283	.296	.318	.337	.362
	.410	-1.103	.131	.227	.378	.446	.509
	.430	.147	.162	.178	.199	.225	.255
	.450	.047	.064	.080	.111	.142	.183
	.465	-.202	-.198	-.167	-.078	-.023	.039
	.471	-.840	-1.239	-1.228	-.928	-.786	-.660
Upper stage	.491	-.019	-.017	-.015	-.001	-.176	-.156
	.511	.083	.098	.107	.140	.171	.070
Transition flare	.531	.355	.383	.393	.425	.402	.312
	.552	.026	.024	.040	.102	.148	.219
Main stage	.568	-.702	-1.103	-1.251	-1.133	-.982	-.843
	.587	-.088	-.119	-.124	-.078	-.545	-.513
	.607	-.031	-.054	-.057	-.045	.003	-.354
	.627	-.019	-.031	-.036	-.034	-.003	-.089
	.657	-.008	-.016	-.015	-.018	-.013	.025
	.697	.003	-.007	-.006	-.011	-.013	.015
	.737	.007	-.002	-.001	-.005	-.010	.003
	.777	.011	.001	.002	.000	-.005	.000
	.785	.011	-.004	.002	.000	-.005	-.001
	.817	.014	.006	.007	.003	-.001	.001
	.857	.009	.001	.002	-.002	-.007	-.008
	.897	.008	-.002	.000	-.005	-.010	-.011

TABLE 8.- PRESSURE COEFFICIENTS FOR CONFIGURATION 123 - Continued

(b) M = 0.60; α = -10° to 10°

	x/l	C_p for - ϕ = 0°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.410	.392	.334	.275	.226	.188	.131	.087
	.420	.364	.306	.242	.193	.149	.098	.053
	.430	.320	.261	.208	.154	.115	.064	.020
	.450	.219	.161	.107	.058	.020	-.032	-.072
	.460	.107	.049	-.005	-.055	-.089	-.136	-.171
	.465	-.022	-.089	-.150	-.194	-.228	-.270	-.292
Upper stage	.471	-.752	-.836	-.909	-.936	-.952	-.982	-.970
	.476	-.172	-.203	-.247	-.262	-.273	-.286	-.279
	.481	-.068	-.088	-.120	-.130	-.135	-.147	-.129
	.491	.013	-.002	-.028	-.032	-.031	-.038	-.020
	.501	.064	.050	.030	.026	.027	.020	.038
	.511	.116	.108	.088	.084	.084	.078	.084
	.521	.214	.200	.180	.176	.171	.158	.153
	.531	.485	.442	.399	.354	.321	.291	.268
Transition flare	.539	.337	.289	.246	.213	.186	.156	.134
	.546	.246	.192	.149	.111	.083	.048	.026
	.552	.155	.101	.047	.008	-.019	-.055	-.073
	.562	-.092	-.153	-.208	-.247	-.275	-.312	-.311
Main stage	.568	-.699	-.765	-.826	-.830	-.805	-.801	-.812
	.577	-.132	-.158	-.190	-.205	-.199	-.211	-.199
	.587	-.063	-.088	-.115	-.119	-.112	-.125	-.107
	.597	-.034	-.054	-.080	-.084	-.071	-.078	-.066
	.607	-.022	-.036	-.057	-.061	-.048	-.055	-.037
	.617	-.016	-.025	-.045	-.049	-.037	-.044	-.026
	.627	-.005	-.019	-.034	-.038	-.025	-.026	-.014
	.637	.006	-.008	-.028	-.032	-.019	-.020	-.009
	.657	.011	.004	-.016	-.016	-.010	-.013	.001
	.677	.013	.006	-.010	-.013	-.006	-.009	.005
	.697	.017	.000	-.009	-.009	-.002	-.005	.005
	.737	.015	.010	-.009	-.009	.000	-.005	.003
	.777	.022	.016	-.007	-.003	.004	-.001	.007
	.785	.026	.021	.003	-.007	.008	.005	.019
	.817	.028	.020	.003	.000	.006	.001	.011
	.857	.022	.017	-.001	-.003	.003	-.004	.004
	.877	.023	.017	-.001	-.003	.003	-.004	.005
	.897	.018	.013	-.004	-.006	.001	-.007	.000

	x/l	C_p for - ϕ = -30°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.410	.364	.317	.270	.221	.183	.131	.070
	.420	.320	.278	.225	.187	.143	.098	.036
	.430	.292	.250	.197	.154	.110	.058	.003
	.450	.185	.144	.090	.053	.015	-.032	-.090
	.460	.073	.037	-.010	-.055	-.089	-.142	-.188
	.465	-.057	-.100	-.155	-.194	-.228	-.275	-.315
Upper stage	.471	-.793	-.859	-.932	-.953	-.998	-.994	-.958
	.476	-.201	-.221	-.258	-.268	-.267	-.274	-.273
	.481	-.080	-.088	-.114	-.118	-.117	-.130	-.129
	.491	-.011	-.008	-.034	-.032	-.031	-.043	-.037
	.501	.041	.044	.024	.026	.027	.020	.020
	.511	.093	.102	.082	.084	.084	.072	.072
	.521	.191	.200	.180	.176	.171	.158	.141
	.531	.456	.436	.393	.360	.338	.308	.262
Transition flare	.539	.177	.220	.229	.213	.192	.151	.094
	.546	.052	.078	.069	.065	.038	-.003	-.061
	.552	.126	.089	.047	.008	-.019	-.055	-.078
	.562	-.127	-.171	-.214	-.247	-.275	-.312	-.334
Main stage	.568	-.623	-.666	-.710	-.720	-.713	-.709	-.673
	.577	-.149	-.169	-.196	-.205	-.199	-.211	-.211
	.587	-.091	-.100	-.120	-.119	-.118	-.125	-.124
	.597	-.051	-.054	-.068	-.072	-.060	-.072	-.066
	.607	-.045	-.042	-.063	-.061	-.048	-.055	-.055
	.617	-.034	-.036	-.051	-.049	-.037	-.044	-.043
	.627	-.028	-.025	-.039	-.038	-.025	-.038	-.032
	.637	-.022	-.019	-.028	-.032	-.019	-.026	-.020
	.657	-.016	-.008	-.020	-.020	-.014	-.022	-.020
	.677	-.003	.002	-.010	-.009	-.002	-.015	-.016
	.697	-.014	.000	-.010	-.009	-.002	-.013	-.018
	.737	-.007	.002	-.009	-.005	.000	-.009	-.020
	.777	-.001	-.004	-.026	-.001	.004	-.007	-.020
	.785	-.001	.010	-.014	.001	.006	-.003	-.018
	.817	.003	.011	-.001	.000	.006	-.007	-.022
	.857	-.005	.005	-.005	-.003	.002	-.011	-.025
	.877	-.005	.004	-.007	-.005	.001	-.013	-.026
	.897	-.006	.002	-.007	-.006	.000	-.014	-.026
	.917	-.006	.002	-.008	-.006	-.003	-.018	-.028
	.957	-.023	-.011	-.019	-.017	-.013	-.030	-.038
	.997	-.105	-.074	-.071	-.073	-.074	-.096	-.115

TABLE 8.- PRESSURE COEFFICIENTS FOR CONFIGURATION 123 - Continued

(b) M = 0.60; α = -10° to 10° - Concluded

	x/l	C_p for - ϕ = -60°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.410	.247	.261	.242	.221	.194	.142	.064
	.420	.213	.228	.208	.182	.155	.109	.031
	.430	.180	.194	.169	.148	.121	.070	.003
	.450	.085	.093	.074	.042	.026	-.026	-.090
	.460	-.016	-.013	-.039	-.067	-.089	-.136	-.188
	.465	-.144	-.100	-.092	-.084	-.083	-.107	-.136
	.471	-.961	-.569	-1.054	-1.109	-1.131	-1.162	-1.161
Upper stage	.476	-.264	-.244	-.258	-.245	-.250	-.280	-.308
	.481	-.137	-.105	-.114	-.101	-.106	-.136	-.164
	.491	-.080	-.036	-.039	-.032	-.031	-.061	-.089
	.501	-.028	.021	.018	.026	.027	-.003	-.032
	.511	.030	.079	.076	.084	.084	.060	.026
	.521	.122	.165	.168	.176	.165	.135	.095
	.531	.353	.379	.364	.360	.344	.302	.251
Transition flare	.539	.274	.266	.235	.213	.192	.151	.105
	.546	.215	.203	.168	.105	.118	.077	.035
	.552	.024	.038	.018	.008	-.014	-.055	-.107
	.562	-.220	-.217	-.238	-.253	-.275	-.312	-.352
Main stage	.568	-.808	-.805	-.820	-.824	-.817	-.836	-.846
	.577	-.219	-.192	-.201	-.205	-.199	-.223	-.245
	.587	-.155	-.123	-.126	-.119	-.118	-.142	-.165
	.597	-.120	-.083	-.086	-.078	-.071	-.101	-.124
	.607	-.109	-.065	-.063	-.061	-.048	-.072	-.101
	.617	-.091	-.054	-.051	-.049	-.042	-.061	-.089
	.627	-.086	-.048	-.045	-.038	-.031	-.055	-.078
	.637	-.080	-.042	-.034	-.032	-.019	-.044	-.072
	.657	-.074	-.031	-.024	-.018	-.016	-.038	-.059
	.677	-.063	-.022	-.019	-.014	-.012	-.034	-.053
	.697	-.051	-.013	-.012	-.009	-.008	-.030	-.047
	.737	-.063	-.015	-.010	-.005	-.002	-.022	-.037
	.777	-.059	-.011	-.009	-.009	.000	-.019	-.030
	.785	-.063	-.013	-.009	-.001	.004	-.017	-.030
	.817	-.053	-.010	-.005	.000	.003	-.016	-.026
	.857	-.059	-.013	-.010	-.003	-.001	-.019	-.026
	.877	-.060	-.015	-.010	-.004	-.001	-.018	-.026
	.897	-.060	-.015	-.011	-.005	-.002	-.020	-.027
	.917	-.071	-.022	-.017	-.010	-.007	-.024	-.031
	.957	-.073	-.029	-.023	-.018	-.016	-.033	-.041
	.997	-.139	-.091	-.084	-.072	-.075	-.101	-.122

	x/l	C_p for - ϕ = -90°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.400	.163	.239	.253	.260	.261	.226	.159
	.430	.068	.133	.146	.148	.138	.109	.048
	.450	-.016	.043	.040	.042	.043	.014	-.043
	.465	-.277	-.222	-.219	-.212	-.216	-.246	-.286
	.471	-.972	-.958	-1.031	-1.011	-.998	-1.046	-1.045
Upper stage	.491	-.120	-.054	-.039	-.026	-.031	-.067	-.112
	.511	-.022	.056	.070	.084	.079	.043	-.009
	.531	.283	.350	.364	.372	.367	.337	.279
Transition flare	.552	-.057	-.002	.007	.008	.004	-.026	-.078
Main stage	.568	-.959	-.909	-.907	-.911	-.909	-.946	-.956
	.587	-.201	-.140	-.132	-.124	-.118	-.148	-.188
	.607	-.138	-.077	-.068	-.061	-.054	-.084	-.130
	.627	-.120	-.054	-.045	-.038	-.031	-.067	-.107
	.657	-.109	-.040	-.028	-.020	-.021	-.051	-.097
	.697	-.101	-.033	-.022	-.011	-.012	-.044	-.088
	.737	-.092	-.027	-.014	-.005	-.006	-.036	-.080
	.777	-.086	-.023	-.010	-.003	-.002	-.030	-.072
	.785	-.092	-.025	-.010	-.003	-.002	-.030	-.072
	.817	-.082	-.016	-.007	.002	.002	-.026	-.068
	.857	-.082	-.022	-.011	-.003	-.003	-.030	-.072
	.897	-.084	-.025	-.014	-.006	-.006	-.034	-.073

TABLE 8.- PRESSURE COEFFICIENTS FOR CONFIGURATION 123 - Continued

(c) $M = 0.80$; $\alpha = -10^\circ$ to 10°

	x/l	C_p for - $\phi = 0^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.410	.456	.370	.312	.262	.212	.169	.126
	.420	.422	.332	.292	.228	.178	.135	.092
	.430	.381	.295	.240	.190	.137	.094	.055
	.450	.279	.193	.143	.092	.046	.007	-.033
	.460	.174	.095	.045	-.004	-.049	-.090	-.123
	.465	.057	-.014	-.063	-.107	-.147	-.183	-.212
Upper stage	.471	-.982	-1.024	-1.053	-1.069	-1.078	-1.064	-1.015
	.476	-.294	-.441	-.500	-.505	-.510	-.485	-.428
	.481	-.073	-.138	-.202	-.257	-.305	-.314	-.293
	.491	.032	.001	-.012	-.021	-.041	-.055	-.064
	.501	.090	.060	.050	.049	.052	.054	.060
	.511	.156	.125	.116	.111	.110	.112	.122
	.521	.272	.238	.221	.204	.192	.178	.176
	.531	.547	.486	.438	.382	.331	.291	.258
Transition flare	.539	.414	.346	.306	.259	.216	.180	.155
	.546	.318	.239	.203	.159	.113	.084	.059
	.552	.234	.154	.115	.060	.021	-.016	-.041
	.562	.020	-.057	-.102	-.158	-.210	-.251	-.280
Main stage	.568	-1.193	-1.228	-1.253	-1.285	-1.293	-1.272	-1.071
	.577	-.132	-.178	-.210	-.239	-.267	-.272	-.266
	.587	-.066	-.096	-.109	-.126	-.138	-.136	-.134
	.597	-.035	-.061	-.070	-.083	-.088	-.082	-.076
	.607	-.015	-.045	-.055	-.064	-.065	-.055	-.045
	.617	-.003	-.034	-.043	-.052	-.053	-.043	-.029
	.627	.004	-.022	-.031	-.040	-.041	-.031	-.018
	.637	.016	-.010	-.020	-.033	-.033	-.024	-.006
	.657	.025	-.005	-.016	-.021	-.021	-.016	-.005
	.677	.030	-.001	-.012	-.016	-.017	-.012	-.001
	.697	.033	.001	-.008	-.013	-.014	-.008	-.001
	.737	.034	.003	-.008	-.012	-.010	-.008	-.002
	.777	.041	.008	-.002	-.005	-.010	-.003	-.001
	.785	.047	.014	.002	-.003	-.002	.001	.006
	.817	.047	.015	.003	-.003	-.004	-.002	.003
	.857	.041	.010	-.001	-.006	-.008	-.006	-.004
	.877	.043	.011	.000	-.006	-.008	-.007	-.004
	.897	.039	.008	-.003	-.008	-.010	-.011	-.008

	x/l	C_p for - $\phi = -30^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.410	.418	.348	.301	.254	.208	.165	.111
	.420	.381	.314	.267	.217	.171	.128	.073
	.430	.347	.280	.233	.186	.133	.094	.040
	.450	.245	.178	.131	.089	.046	.000	-.049
	.460	.144	.080	.037	-.006	-.045	-.090	-.134
	.465	.027	-.030	-.070	-.107	-.143	-.183	-.220
Upper stage	.471	-1.134	-1.188	-1.217	-1.237	-1.257	-1.072	-.965
	.476	-.321	-.429	-.473	-.490	-.506	-.524	-.479
	.481	-.089	-.146	-.214	-.273	-.297	-.314	-.308
	.491	.008	-.007	-.012	-.021	-.033	-.043	-.060
	.501	.070	.056	.050	.053	.052	.050	.048
	.511	.132	.118	.112	.111	.110	.108	.107
	.521	.252	.234	.221	.208	.195	.182	.172
	.531	.524	.478	.438	.394	.350	.318	.285
Transition flare	.539	.261	.273	.283	.263	.231	.195	.136
	.546	.127	.124	.130	.109	.078	.042	-.010
	.552	.207	.151	.111	.060	.024	-.012	-.041
	.562	-.019	-.085	-.122	-.162	-.214	-.251	-.284
Main stage	.568	-1.049	-1.069	-1.078	-1.102	-1.103	-1.097	-.970
	.577	-.198	-.322	-.374	-.348	-.329	-.319	-.313
	.587	-.073	-.084	-.090	-.114	-.135	-.136	-.142
	.597	-.038	-.049	-.055	-.064	-.072	-.070	-.068
	.607	-.038	-.049	-.055	-.064	-.065	-.062	-.053
	.617	-.031	-.038	-.043	-.052	-.053	-.047	-.037
	.627	-.023	-.034	-.035	-.044	-.045	-.039	-.029
	.637	-.011	-.022	-.028	-.033	-.037	-.031	-.021
	.657	-.001	-.017	-.020	-.021	-.024	-.024	-.019
	.677	.014	-.003	-.007	-.009	-.014	-.015	-.012
	.697	.007	-.007	-.012	-.013	-.015	-.015	-.016
	.737	.010	-.005	-.007	-.008	-.010	-.011	-.018
	.777	.019	.003	-.002	-.003	-.010	-.007	-.019
	.785	.017	.003	-.002	.000	-.006	-.008	-.018
	.817	.021	.005	.001	-.001	-.005	-.007	-.020
	.857	.014	-.001	-.004	-.005	-.009	-.012	-.025
	.877	.014	-.002	-.006	-.006	-.009	-.014	-.027
	.897	.012	-.003	-.007	-.008	-.011	-.015	-.028
	.917	.012	-.004	-.007	-.008	-.014	-.018	-.028
	.957	-.003	-.015	-.017	-.019	-.025	-.033	-.042
	.997	-.083	-.082	-.074	-.076	-.090	-.102	-.119

TABLE 8.- PRESSURE COEFFICIENTS FOR CONFIGURATION 123 - Continued

(c) M = 0.80; α = -10° to 10° - Concluded

	x/l	C_p for - ϕ = -60°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.410	.305	.295	.278	.250	.220	.180	.111
	.420	.272	.261	.240	.213	.182	.139	.073
	.430	.238	.223	.203	.179	.144	.105	.040
	.450	.144	.129	.112	.085	.050	.011	-.053
	.460	.046	.031	.015	-.009	-.041	-.082	-.134
	.465	-.120	-.100	-.090	-.083	-.092	-.102	-.127
	.471	-1.250	-1.262	-1.248	-1.284	-1.304	-1.275	-1.253
Upper stage	.476	-.437	-.491	-.528	-.509	-.553	-.558	-.537
	.481	-.174	-.239	-.279	-.277	-.270	-.283	-.312
	.491	-.054	-.026	-.020	-.017	-.022	-.035	-.076
	.501	.004	.032	.046	.049	.044	.027	-.006
	.511	.074	.102	.112	.111	.106	.089	.056
	.521	.179	.203	.209	.204	.195	.174	.141
	.531	.415	.424	.407	.378	.366	.337	.289
Transition flare	.539	.361	.323	.295	.263	.224	.184	.144
	.546	.301	.254	.231	.155	.157	.117	.077
	.552	.104	.093	.084	.056	.028	-.008	-.061
	.562	-.109	-.124	-.141	-.170	-.198	-.227	-.272
Main stage	.568	-1.252	-1.251	-1.264	-1.281	-1.290	-1.311	-1.308
	.577	-.221	-.213	-.210	-.219	-.236	-.261	-.321
	.587	-.151	-.127	-.117	-.126	-.131	-.140	-.169
	.597	-.116	-.088	-.078	-.083	-.092	-.101	-.123
	.607	-.097	-.069	-.059	-.064	-.068	-.078	-.107
	.617	-.089	-.061	-.051	-.052	-.057	-.066	-.088
	.627	-.081	-.057	-.043	-.044	-.049	-.055	-.080
	.637	-.070	-.049	-.035	-.037	-.041	-.047	-.076
	.657	-.063	-.039	-.025	-.022	-.027	-.040	-.064
	.677	-.048	-.029	-.019	-.017	-.023	-.036	-.039
	.697	-.033	-.020	-.013	-.012	-.018	-.031	-.053
	.737	-.044	-.022	-.012	-.009	-.014	-.024	-.041
	.777	-.040	-.018	-.007	-.004	-.010	-.018	-.032
	.785	-.045	-.023	-.007	-.003	-.010	-.017	-.031
	.817	-.039	-.016	-.002	-.002	-.008	-.017	-.024
	.857	-.041	-.020	-.008	-.006	-.011	-.019	-.026
	.877	-.041	-.020	-.009	-.007	-.012	-.019	-.027
	.897	-.041	-.022	-.009	-.007	-.013	-.020	-.027
	.917	-.050	-.027	-.015	-.012	-.017	-.025	-.032
	.957	-.055	-.034	-.021	-.021	-.027	-.035	-.042
	.997	-.124	-.102	-.083	-.077	-.090	-.105	-.123

	x/l	C_p for - ϕ = -90°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.400	.226	.276	.297	.299	.287	.267	.213
	.430	.121	.163	.180	.179	.167	.143	.092
	.450	.035	.073	.086	.085	.073	.049	.002
	.465	-.191	-.151	-.137	-.138	-.147	-.168	-.209
	.471	-1.137	-1.102	-1.103	-1.085	-1.082	-1.080	-1.105
Upper stage	.491	-.100	-.049	-.027	-.017	-.026	-.047	-.103
	.511	.024	.083	.104	.111	.099	.073	.021
	.531	.345	.389	.391	.398	.393	.372	.316
Transition flare	.552	.012	.047	.065	.056	.051	.027	-.018
Main stage	.568	-1.306	-1.294	-1.284	-1.293	-1.301	-1.303	-1.312
	.587	-.182	-.131	-.125	-.122	-.131	-.140	-.193
	.607	-.132	-.084	-.063	-.064	-.072	-.090	-.134
	.627	-.108	-.061	-.043	-.044	-.053	-.066	-.115
	.657	-.090	-.048	-.029	-.024	-.032	-.055	-.103
	.697	-.083	-.040	-.020	-.015	-.023	-.043	-.094
	.737	-.074	-.032	-.015	-.009	-.017	-.037	-.081
	.777	-.068	-.029	-.009	-.004	-.013	-.033	-.076
	.785	-.072	-.031	-.012	-.005	-.011	-.031	-.073
	.817	-.060	-.021	-.004	-.001	-.009	-.027	-.066
	.857	-.065	-.029	-.011	-.006	-.013	-.032	-.070
	.897	-.066	-.031	-.013	-.008	-.016	-.035	-.072

TABLE 8.- PRESSURE COEFFICIENTS FOR CONFIGURATION 123 - Continued

(d) M = 1.00; α = -10° to 10°

	x/l	C_p for - ϕ = 0°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.410	.545	.473	.416	.370	.322	.284	.232
	.420	.519	.443	.392	.346	.298	.251	.202
	.430	.483	.407	.356	.307	.262	.219	.166
	.450	.405	.336	.284	.241	.196	.153	.101
	.460	.336	.270	.228	.187	.145	.105	.059
	.465	.264	.213	.171	.130	.097	.060	.017
Upper stage	.471	-.489	-.514	-.536	-.547	-.560	-.577	-.603
	.476	-.566	-.632	-.666	-.692	-.714	-.715	-.547
	.481	-.428	-.518	-.570	-.612	-.637	-.364	-.279
	.491	-.252	-.357	-.416	-.467	-.131	-.169	-.195
	.501	-.129	-.234	-.151	-.005	-.054	-.120	-.146
	.511	.220	.195	.194	.131	.011	-.049	-.072
	.521	.383	.367	.349	.248	.116	.071	.036
	.531	.654	.580	.503	.341	.224	.201	.147
Transition flare	.539	.564	.524	.494	.404	.273	.253	.209
	.546	.479	.436	.411	.386	.279	.250	.215
	.552	.409	.363	.332	.312	.227	.204	.172
	.562	.260	.214	.177	.136	.050	.031	.008
Main stage	.568	-.661	-.677	-.696	-.707	-.722	-.721	-.755
	.577	-.414	-.482	-.537	-.552	-.429	-.424	-.456
	.587	-.296	-.383	-.44.	-.463	-.416	-.439	-.459
	.597	-.209	-.287	-.343	-.360	-.373	-.393	-.409
	.607	-.163	-.225	-.269	-.274	-.299	-.303	-.270
	.617	-.144	-.198	-.229	-.215	-.227	-.213	-.184
	.627	-.135	-.176	-.186	-.169	-.169	-.154	-.134
	.637	-.120	-.145	-.136	-.131	-.128	-.117	-.106
	.657	-.114	-.101	-.095	-.097	-.092	-.081	-.071
	.677	-.066	-.077	-.080	-.080	-.076	-.072	-.063
	.697	-.050	-.062	-.065	-.068	-.065	-.063	-.055
	.737	-.035	-.053	-.058	-.061	-.056	-.058	-.048
	.777	-.018	-.037	-.042	-.049	-.045	-.050	-.022
	.785	-.001	-.023	-.030	-.040	-.035	-.039	.007
	.817	.001	-.024	-.029	-.042	-.035	-.045	.021
	.857	.010	-.030	.024	-.042	.000	-.047	.024
	.877	.058	-.005	.037	.008	.026	-.026	.024
	.897	.062	.036	.035	.028	.029	-.001	.016

	x/l	C_p for - ϕ = -30°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.410	.510	.455	.404	.364	.325	.278	.220
	.420	.477	.425	.377	.334	.292	.242	.184
	.430	.447	.395	.350	.307	.265	.213	.151
	.450	.369	.321	.278	.235	.196	.150	.086
	.460	.309	.258	.222	.184	.145	.102	.050
	.465	.237	.198	.165	.130	.100	.060	.014
Upper stage	.471	-.616	-.641	-.663	-.681	-.699	-.682	-.748
	.476	-.585	-.629	-.657	-.683	-.708	-.728	-.510
	.481	-.483	-.558	-.601	-.640	-.652	-.561	-.288
	.491	-.274	-.363	-.419	-.427	-.125	-.176	-.205
	.501	-.153	-.231	-.108	.017	-.066	-.132	-.146
	.511	.195	.189	.188	.116	-.002	-.052	-.072
	.521	.359	.358	.336	.202	.109	.071	.033
	.531	.624	.565	.484	.310	.220	.204	.141
Transition flare	.539	.391	.451	.475	.462	.425	.366	.273
	.546	.287	.329	.344	.343	.312	.253	.166
	.552	.379	.351	.329	.312	.248	.223	.163
	.562	.226	.195	.165	.120	.075	.058	.008
Main stage	.568	-.646	-.652	-.668	-.667	-.692	-.721	-.768
	.577	-.475	-.529	-.566	-.552	-.475	-.631	-.610
	.587	-.308	-.380	-.430	-.422	-.410	-.442	-.456
	.597	-.185	-.238	-.275	-.271	-.283	-.297	-.301
	.607	-.197	-.244	-.278	-.277	-.296	-.300	-.280
	.617	-.179	-.207	-.229	-.221	-.227	-.216	-.202
	.627	-.172	-.191	-.192	-.178	-.175	-.164	-.159
	.637	-.160	-.164	-.145	-.138	-.135	-.130	-.128
	.657	-.145	-.109	-.099	-.099	-.095	-.094	-.096
	.677	-.082	-.078	-.075	-.075	-.073	-.077	-.086
	.697	-.078	-.071	-.068	-.069	-.067	-.072	-.083
	.737	-.061	-.061	-.058	-.059	-.055	-.063	-.079
	.777	-.037	-.042	-.041	-.046	-.044	-.056	-.059
	.785	-.030	-.033	-.033	-.039	-.036	-.049	-.039
	.817	-.028	-.033	-.031	-.042	-.037	-.054	-.024
	.857	-.019	-.041	.022	-.042	-.003	-.057	-.010
	.877	.028	-.026	.032	.009	.024	-.041	-.008
	.897	.036	.028	.032	.028	.028	-.016	-.007
	.917	.041	.038	.031	.029	.028	.006	-.007
	.957	.032	.027	.019	.017	.012	.003	-.017
	.997	-.033	-.048	-.070	-.095	-.109	-.127	-.143

TABLE 8.- PRESSURE COEFFICIENTS FOR CONFIGURATION 123 - Continued

(d) M = 1.00; α = -10° to 10° - Concluded

	x/l	C_p for - ϕ = -60°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.410	.402	.401	.383	.364	.331	.290	.220
	.420	.372	.368	.353	.334	.298	.257	.187
	.430	.345	.342	.323	.304	.268	.224	.154
	.450	.276	.276	.257	.235	.202	.162	.089
	.460	.216	.216	.204	.184	.151	.111	.044
Upper stage	.465	-.191	-.151	-.133	-.126	-.129	-.152	-.181
	.471	-.715	-.709	-.710	-.715	-.702	-.710	-.739
	.476	-.665	-.681	-.697	-.708	-.729	-.740	-.692
	.481	-.517	-.564	-.598	-.628	-.665	-.688	-.356
	.491	-.375	-.422	-.453	-.313	-.208	-.250	-.217
	.501	-.135	-.197	-.068	.011	-.066	-.086	-.158
	.511	.130	.167	.176	.088	.045	.031	-.060
	.521	.272	.318	.315	.174	.187	.164	.070
	.531	.503	.497	.447	.267	.310	.318	.221
Transition flare	.539	.500	.500	.484	.453	.370	.290	.258
	.546	.449	.445	.433	.395	.356	.282	.238
	.552	.275	.305	.308	.291	.282	.223	.130
	.562	.138	.156	.143	.099	.114	.073	.005
Main stage	.568	-.710	-.699	-.705	-.701	-.719	-.736	-.771
	.577	-.565	-.575	-.585	-.521	-.623	-.662	-.713
	.587	-.417	-.439	-.458	-.410	-.478	-.551	-.604
	.597	-.324	-.334	-.356	-.336	-.339	-.411	-.443
	.607	-.290	-.287	-.294	-.280	-.271	-.288	-.307
	.617	-.27.	-.250	-.232	-.227	-.218	-.229	-.261
	.627	-.271	-.216	-.182	-.181	-.175	-.192	-.224
	.637	-.253	-.167	-.145	-.144	-.141	-.158	-.196
	.657	-.183	-.129	-.102	-.098	-.101	-.119	-.147
	.677	-.150	-.104	-.085	-.082	-.086	-.104	-.127
	.697	-.117	-.079	-.067	-.067	-.071	-.090	-.107
	.737	-.117	-.077	-.060	-.058	-.061	-.078	-.087
	.777	-.101	-.062	-.045	-.046	-.048	-.067	-.058
	.785	-.100	-.059	-.041	-.042	-.043	-.063	-.040
	.817	-.090	-.054	-.033	-.040	-.040	-.061	-.015
	.857	-.062	-.058	.016	-.040	-.009	-.065	.002
	.877	-.021	-.032	.028	.009	.022	-.052	.003
	.897	-.019	.013	.028	.028	.027	-.026	.001
	.917	-.022	.012	.022	.026	.023	.005	-.003
	.957	-.023	.008	.014	.017	.011	.004	-.016
	.997	-.098	-.080	-.084	-.096	-.107	-.127	-.149

	x/l	C_p for - ϕ = -30°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.400	.327	.383	.404	.406	.397	.374	.322
	.430	.234	.282	.293	.304	.292	.263	.208
	.450	.171	.219	.231	.235	.223	.198	.136
Upper stage	.465	.037	.087	.102	.106	.100	.075	.014
	.471	-.625	-.576	-.561	-.554	-.544	-.546	-.596
	.491	-.277	-.456	-.463	-.230	-.480	-.484	-.245
	.511	.016	.112	.139	.079	.131	.111	.020
Transition flare	.531	.380	.432	.410	.264	.412	.417	.356
	.552	.184	.268	.296	.288	.288	.241	.154
Main stage	.568	-.757	-.727	-.724	-.707	-.722	-.736	-.768
	.587	-.513	-.491	-.483	-.413	-.481	-.507	-.536
	.607	-.383	-.327	-.285	-.280	-.274	-.337	-.394
	.627	-.296	-.194	-.170	-.178	-.172	-.207	-.280
	.657	-.201	-.134	-.105	-.101	-.109	-.143	-.207
	.697	-.162	-.099	-.074	-.070	-.076	-.106	-.161
	.737	-.146	-.087	-.062	-.057	-.064	-.093	-.139
	.777	-.129	-.073	-.048	-.048	-.052	-.082	-.114
	.785	-.134	-.073	-.046	-.043	-.048	-.077	-.096
	.817	-.106	-.060	-.033	-.039	-.040	-.069	-.055
	.857	-.062	-.060	.017	-.040	-.017	-.080	-.034
	.897	-.042	.005	.024	.028	.025	-.062	-.038

TABLE 8.- PRESSURE COEFFICIENTS FOR CONFIGURATION 123 - Continued

(e) M = 1.20; α = -10° to 10°

		C_p for - ϕ = 0°						
	x/l	α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.410	.509	.417	.363	.956 .308	.272	.230	.194
	.420	.519	.431	.371	.319	.282	.241	.199
	.430	.509	.425	.363	.311	.272	.241	.188
	.450	.495	.415	.358	.319	.269	.233	.183
	.460	.469	.399	.352	.313	.277	.230	.178
	.465	.431	.375	.334	.297	.264	.222	.172
Upper stage	.471	-.180	-.200	-.215	-.233	-.251	-.272	-.307
	.476	-.283	-.334	-.354	-.372	-.390	-.402	-.421
	.481	-.201	-.273	-.304	-.331	-.349	-.369	-.396
	.491	-.100	-.183	-.219	-.254	-.280	-.304	-.330
	.501	-.045	-.122	-.151	-.191	-.217	-.232	-.130
	.511	-.028	-.092	-.115	-.141	-.022	.097	.073
	.521	-.023	-.026	.102	.210	.203	.160	.128
	.531	.524	.441	.390	.320	.252	.213	.186
Transition flare	.539	.642	.579	.510	.414	.298	.234	.216
	.546	.574	.533	.500	.441	.333	.264	.243
	.552	.526	.479	.451	.414	.333	.267	.243
	.562	.428	.381	.348	.305	.230	.172	.140
Main stage	.568	-.334	-.354	-.371	-.387	-.386	-.384	-.403
	.577	-.185	-.241	-.272	-.288	-.259	-.236	-.227
	.587	-.133	-.197	-.239	-.255	-.251	-.247	-.254
	.597	-.081	-.145	-.184	-.208	-.221	-.230	-.246
	.607	-.050	-.109	-.146	-.166	-.188	-.200	-.205
	.617	-.039	-.092	-.121	-.139	-.154	-.161	-.155
	.627	-.025	-.076	-.099	-.114	-.124	-.123	-.108
	.637	-.014	-.059	-.079	-.087	-.091	-.090	-.073
	.657	-.020	-.056	-.067	-.066	-.055	-.045	-.035
	.677	-.019	-.031	-.043	-.043	-.038	-.025	-.021
	.697	-.010	-.038	-.043	-.033	-.021	-.012	-.017
	.737	-.018	-.026	-.026	-.036	-.026	-.023	-.008
	.777	.016	-.014	-.030	-.024	-.026	-.026	-.014
	.785	.024	-.008	-.019	-.016	-.016	-.012	-.005
	.817	.024	-.003	-.006	-.022	-.020	-.011	-.006
	.857	.022	.012	-.010	-.004	.001	-.006	-.013
	.877	.033	-.002	-.008	.000	-.003	-.006	-.010
	.897	.014	-.004	-.001	-.005	-.010	-.015	-.018

		C_p for - ϕ = -30°						
	x/l	α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.410	.477	.399	.355	.303	.277	.228	.183
	.420	.474	.409	.355	.305	.282	.233	.180
	.430	.474	.412	.355	.311	.274	.244	.178
	.450	.461	.399	.350	.316	.269	.236	.180
	.460	.439	.388	.347	.313	.277	.233	.172
	.465	.405	.361	.328	.297	.264	.225	.162
Upper stage	.471	-.291	-.311	-.325	-.341	-.362	-.385	-.415
	.476	-.303	-.336	-.354	-.369	-.382	-.408	-.435
	.481	-.245	-.301	-.326	-.350	-.368	-.394	-.421
	.491	-.108	-.180	-.214	-.245	-.272	-.301	-.336
	.501	-.075	-.133	-.159	-.191	-.214	-.232	-.116
	.511	-.061	-.108	-.126	-.147	-.044	.092	.070
	.521	-.042	-.015	.124	.216	.195	.138	.101
	.531	.496	.430	.377	.317	.244	.188	.142
Transition flare	.539	.493	.506	.478	.419	.396	.354	.265
	.546	.403	.444	.453	.438	.409	.365	.273
	.552	.496	.468	.448	.414	.355	.300	.243
	.562	.393	.362	.337	.297	.252	.207	.159
Main stage	.568	-.334	-.343	-.355	-.356	-.372	-.384	-.420
	.577	-.243	-.280	-.300	-.304	-.295	-.307	-.315
	.587	-.141	-.197	-.228	-.244	-.237	-.247	-.265
	.597	-.075	-.114	-.140	-.150	-.160	-.164	-.172
	.607	-.078	-.122	-.151	-.166	-.185	-.192	-.199
	.617	-.064	-.103	-.123	-.139	-.152	-.159	-.158
	.627	-.059	-.089	-.104	-.117	-.124	-.128	-.125
	.637	-.048	-.076	-.090	-.092	-.097	-.098	-.092
	.657	-.041	-.055	-.064	-.061	-.051	-.051	-.059
	.677	-.038	-.032	-.040	-.036	-.036	-.032	-.047
	.697	-.044	-.044	-.039	-.037	-.030	-.025	-.047
	.737	-.042	-.037	-.028	-.032	-.026	-.030	-.048
	.777	-.010	-.021	-.027	-.019	-.024	-.027	-.057
	.785	-.002	-.015	-.017	-.010	-.014	-.017	-.053
	.817	.000	-.015	-.009	-.019	-.018	-.022	-.069
	.857	-.006	.004	-.011	-.012	-.010	-.021	-.071
	.877	.003	-.012	-.010	-.004	-.005	-.018	-.065
	.897	-.010	-.011	-.005	-.002	-.006	-.020	-.058
	.917	-.009	-.006	-.005	-.006	-.006	-.019	-.046
	.957	-.012	-.015	-.014	-.016	-.016	-.019	-.037
	.997	-.001	-.021	-.036	-.054	-.072	-.091	-.081

TABLE 6.- PRESSURE COEFFICIENTS FOR CONFIGURATION 123 - Concluded

(e) M = 1.20; $\alpha = -10^\circ$ to 10° - Concluded

	x/l	C_p for - $\phi = -60^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.410	.365	.345	.328	.303	.280	.238	.186
	.420	.375	.356	.331	.311	.285	.249	.188
	.430	.373	.359	.328	.311	.282	.252	.180
	.450	.362	.351	.331	.313	.285	.254	.183
	.460	.341	.343	.328	.313	.288	.246	.175
	.465	-.188	-.161	-.143	-.139	-.141	-.164	-.202
Upper stage	.471	-.382	-.371	-.367	-.371	-.381	-.391	-.412
	.476	-.371	-.380	-.381	-.388	-.406	-.419	-.448
	.481	-.283	-.314	-.326	-.344	-.365	-.394	-.443
	.491	-.201	-.226	-.241	-.251	-.267	-.293	-.330
	.501	-.163	-.174	-.181	-.193	-.212	-.235	-.273
	.511	-.141	-.139	-.137	-.147	-.148	-.068	.032
	.521	-.105	.032	.154	.216	.203	.160	.084
Transition flare	.531	.384	.372	.357	.309	.280	.229	.145
	.539	.591	.555	.502	.417	.344	.286	.202
	.546	.548	.530	.497	.446	.376	.318	.239
	.552	.390	.419	.424	.408	.379	.337	.251
	.562	.306	.322	.315	.297	.276	.245	.173
Main stage	.568	-.386	-.373	-.374	-.378	-.386	-.406	-.444
	.577	-.315	-.315	-.314	-.310	-.336	-.373	-.422
	.587	-.229	-.244	-.250	-.241	-.276	-.313	-.370
	.597	-.174	-.183	-.195	-.194	-.212	-.247	-.312
	.607	-.155	-.153	-.157	-.164	-.168	-.183	-.224
	.617	-.144	-.139	-.135	-.139	-.143	-.153	-.183
	.627	-.141	-.122	-.118	-.120	-.124	-.137	-.169
	.637	-.125	-.103	-.093	-.095	-.097	-.112	-.144
	.657	-.123	-.064	-.055	-.047	-.051	-.076	-.119
	.677	-.111	-.062	-.047	-.043	-.046	-.063	-.104
	.697	-.099	-.061	-.039	-.038	-.042	-.050	-.088
	.737	-.098	-.055	-.034	-.032	-.033	-.051	-.066
	.777	-.069	-.042	-.029	-.020	-.027	-.038	-.053
	.785	-.058	-.041	-.023	-.011	-.020	-.029	-.051
	.817	-.057	-.028	-.014	-.016	-.019	-.032	-.051
	.857	-.064	-.017	-.017	-.018	-.025	-.032	-.049
	.877	-.054	-.029	-.010	-.005	-.010	-.022	-.044
	.897	-.064	-.029	-.012	-.001	-.004	-.018	-.035
	.917	-.071	-.033	-.018	-.007	-.009	-.021	-.031
	.957	-.069	-.036	-.017	-.016	-.020	-.019	-.034
	.997	-.061	-.047	-.045	-.055	-.067	-.089	-.106

	x/l	C_p for - $\phi = -30^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.400	.253	.289	.312	.311	.306	.294	.258
	.430	.255	.295	.302	.308	.304	.286	.236
	.450	.253	.300	.302	.316	.298	.289	.234
	.465	.194	.249	.275	.276	.269	.246	.188
Upper stage	.471	-.324	-.269	-.245	-.244	-.227	-.245	-.288
	.491	-.278	-.259	-.252	-.259	-.269	-.282	-.306
	.511	-.212	-.174	-.153	-.147	-.157	-.177	-.232
Transition flare	.531	.277	.312	.330	.306	.324	.300	.238
	.552	.306	.379	.407	.408	.401	.362	.278
Main stage	.568	-.430	-.401	-.391	-.378	-.391	-.406	-.439
	.587	-.306	-.280	-.261	-.241	-.265	-.288	-.329
	.607	-.235	-.189	-.176	-.164	-.174	-.203	-.246
	.627	-.216	-.136	-.118	-.117	-.116	-.137	-.227
	.657	-.153	-.080	-.055	-.049	-.055	-.088	-.154
	.697	-.147	-.082	-.048	-.043	-.052	-.075	-.150
	.737	-.118	-.066	-.041	-.034	-.034	-.063	-.125
	.777	-.083	-.049	-.028	-.020	-.024	-.049	-.103
	.785	-.093	-.053	-.029	-.015	-.023	-.049	-.106
	.817	-.083	-.030	-.015	-.010	-.019	-.041	-.093
	.857	-.086	-.030	-.019	-.013	-.032	-.051	-.090
	.897	-.089	-.042	-.018	-.006	-.007	-.027	-.078

TABLE 9.- PRESSURE COEFFICIENTS FOR CONFIGURATION 223

(a) $M = 0.40$ to 0.95; $\alpha = 0°$

	x/l	C_p for - $\phi = 0°$					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.428	.395	.436	.453	.499	.524	.561
	.438	.307	.346	.360	.408	.440	.474
	.448	.188	.231	.247	.306	.343	.384
	.458	.068	.115	.134	.203	.247	.294
	.471	-1.159	-1.173	-1.118	-1.062	-.943	-.813
Upper stage	.476	-.278	-.676	-.720	-.834	-.867	-.978
	.481	-.143	-.345	-.449	-.568	-.535	-.853
	.491	-.042	-.047	-.083	-.249	-.323	-.288
	.501	.014	.027	.034	-.038	-.111	-.163
	.511	.070	.086	.096	.084	.060	-.032
	.521	.149	.174	.180	.181	.174	.108
	.531	.339	.343	.338	.302	.312	.265
Transition flare	.539	.191	.212	.223	.246	.275	.331
	.546	.102	.121	.136	.182	.219	.306
	.552	.014	.026	.038	.093	.145	.230
	.562	-.235	-.233	-.206	-.114	-.045	.047
Main stage	.568	-.628	-1.005	-1.115	-1.110	-.971	-.830
	.577	-.189	-.222	-.725	-.290	-.722	-.619
	.587	-.110	-.130	-.129	-.106	-.220	-.520
	.597	-.076	-.088	-.087	-.074	-.048	-.401
	.607	-.054	-.065	-.062	-.060	-.024	-.289
	.617	-.042	-.052	-.050	-.049	-.024	-.148
	.627	-.031	-.042	-.041	-.038	-.024	-.052
	.637	-.020	-.033	-.029	-.031	-.021	-.010
	.657	-.016	-.022	-.019	-.021	-.017	.017
	.677	-.012	-.019	-.015	-.018	-.016	.010
	.697	-.009	-.016	-.011	-.014	-.014	.005
	.737	-.009	-.013	-.008	-.012	-.013	-.009
	.777	-.001	-.009	-.004	-.006	-.007	-.009
	.785	.003	-.002	.002	.000	-.002	-.007
	.817	-.001	-.002	.000	-.003	-.005	-.008
	.857	-.001	-.005	-.003	-.006	-.008	-.013
	.877	-.003	-.005	-.002	-.006	-.008	-.013
	.897	-.006	-.008	-.005	-.009	-.011	-.016

	x/l	C_p for - $\phi = -30°$					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.438	.307	.342	.360	.405	.430	.474
	.448	.198	.248	.267	.318	.355	.393
	.458	.057	.101	.130	.192	.244	.291
	.471	-1.283	-1.275	-1.248	-1.137	-1.054	-.919
Upper stage	.476	-.300	-.653	-.703	-.644	-.662	-.933
	.481	-.143	-.336	-.449	-.579	-.545	-.694
	.491	-.042	-.047	-.079	-.310	-.357	-.288
	.501	.014	.027	.038	-.035	-.142	-.163
	.511	.070	.086	.096	.091	.040	-.042
	.521	.160	.178	.180	.181	.168	.083
	.531	.339	.348	.342	.306	.268	.223
Transition flare	.539	.191	.217	.231	.253	.278	.350
	.546	.047	.076	.091	.139	.182	.274
	.552	.014	.026	.042	.093	.145	.217
	.562	-.235	-.237	-.210	-.129	-.075	.009
Main stage	.568	-.583	-.862	-.982	-1.059	-.921	-.776
	.577	-.177	-.213	-.217	-.268	-.668	-.558
	.587	-.110	-.130	-.129	-.106	-.216	-.481
	.597	-.076	-.070	-.070	-.060	-.044	-.318
	.607	-.054	-.065	-.062	-.060	-.027	-.298
	.617	-.042	-.052	-.050	-.049	-.027	-.164
	.627	-.031	-.042	-.041	-.042	-.027	-.055
	.637	-.020	-.033	-.033	-.023	-.024	-.010
	.657	-.020	-.024	-.020	-.020	-.020	.012
	.677	-.009	-.013	-.009	-.012	-.011	.015
	.697	-.009	-.016	-.011	-.014	-.014	.003
	.737	-.005	-.012	-.006	-.009	-.011	-.008
	.777	-.001	-.006	-.004	-.003	-.005	-.006
	.785	.003	-.002	.002	-.001	-.002	-.004
	.817	-.001	-.002	.000	-.003	-.004	-.008
	.857	-.003	-.007	-.004	-.007	-.009	-.015
	.877	-.004	-.007	-.004	-.008	-.010	-.015
	.897	-.006	-.008	-.006	-.009	-.011	-.017
	.917	-.006	-.008	-.006	-.010	-.011	-.018
	.957	-.016	-.020	-.018	-.021	-.023	-.030
	.997	-.069	-.076	-.076	-.080	-.088	-.104

TABLE 9.- PRESSURE COEFFICIENTS FOR CONFIGURATION 223 - Continued

(a) M = 0.40 to 0.95; $\alpha = 0^\circ$ - Concluded

	x/l	C_p for - $\phi = -60^\circ$					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.438	.307	.338	.360	.401	.430	.474
	.448	.198	.248	.267	.314	.348	.393
	.458	.068	.115	.138	.206	.247	.297
Upper stage	.471	-1.227	-1.095	-1.080	-1.054	-.987	-.855
	.476	-.289	-.662	-.691	-.636	-.682	-.965
	.481	-.143	-.368	-.474	-.547	-.538	-.674
	.491	-.042	-.042	-.083	-.314	-.343	-.285
	.501	.014	.031	.042	-.060	-.135	-.167
	.511	.070	.091	.101	.087	.040	-.045
	.521	.149	.174	.180	.173	.157	.083
	.531	.328	.334	.330	.277	.255	.217
Transition flare	.539	.191	.217	.223	.249	.282	.375
	.546	.091	.121	.132	.182	.225	.321
	.552	.014	.022	.038	.086	.132	.205
	.562	-.235	-.242	-.218	-.136	-.075	.009
Main stage	.568	-.639	-.991	-1.115	-1.113	-.971	-.821
	.577	-.177	-.213	-.217	-.254	-.671	-.564
	.587	-.110	-.130	-.133	-.114	-.199	-.452
	.597	-.076	-.084	-.083	-.074	-.054	-.372
	.607	-.054	-.065	-.062	-.060	-.031	-.298
	.617	-.042	-.052	-.050	-.049	-.031	-.167
	.627	-.031	-.042	-.041	-.042	-.031	-.058
	.637	-.020	-.033	-.033	-.035	-.027	-.016
	.657	-.020	-.024	-.020	-.023	-.020	.010
	.677	-.014	-.019	-.015	-.017	-.016	.012
	.697	-.009	-.013	-.009	-.012	-.013	.004
	.737	-.005	-.012	-.006	-.009	-.011	-.007
	.777	-.001	-.009	-.002	-.005	-.006	-.008
	.785	-.001	-.006	.002	-.002	-.005	-.007
	.817	.000	-.001	.001	-.002	-.004	-.008
	.857	-.003	-.006	-.004	-.007	-.009	-.014
	.877	-.004	-.007	-.004	-.007	-.009	-.015
	.897	-.006	-.007	-.005	-.008	-.011	-.016
	.917	-.009	-.013	-.010	-.014	-.015	-.021
	.957	-.016	-.019	-.018	-.021	-.023	-.030
	.997	-.069	-.076	-.075	-.081	-.088	-.104

	x/l	C_p for - $\phi = -90^\circ$					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.428	.384	.431	.449	.492	.518	.554
	.448	.198	.240	.263	.311	.348	.387
	.458	.068	.106	.134	.199	.244	.294
Upper stage	.471	-1.396	-1.243	-1.151	-1.159	-1.031	-.893
	.491	-.042	-.047	-.083	-.285	-.330	-.297
	.511	.070	.086	.101	.080	.033	-.045
Transition flare	.531	.339	.343	.334	.288	.268	.198
	.552	.003	.022	.038	.086	.136	.205
Main stage	.568	-.706	-1.037	-1.107	-1.128	-.978	-.834
	.587	-.110	-.130	-.133	-.110	-.186	-.449
	.607	-.054	-.065	-.062	-.060	-.034	-.295
	.627	-.031	-.042	-.041	-.042	-.031	-.058
	.657	-.020	-.024	-.020	-.024	-.021	.008
	.697	-.009	-.016	-.012	-.015	-.015	.001
	.737	-.005	-.012	-.006	-.009	-.011	-.007
	.777	-.001	-.009	-.005	-.006	-.007	-.008
	.785	-.001	-.009	-.008	-.005	-.006	-.008
	.817	.000	.000	.003	.000	-.003	-.006
	.857	-.003	-.005	-.003	-.007	-.008	-.014
	.897	-.006	-.008	-.006	-.009	-.011	-.017

TABLE 9.- PRESSURE COEFFICIENTS FOR CONFIGURATION 223 - Continued

(b) $M = 0.60$; $\alpha = -10^\circ$ to 10°

	x/l	C_p for - $\beta = 0^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.428		.551	.479	.425	.355	.294	.205
	.438		.457	.390	.326	.261	.205	.127
	.448		.332	.263	.204	.142	.089	.015
	.458		.208	.136	.082	.023	-.028	-.097
Upper stage	.471		-1.219	-1.321	-1.348	-1.283	-1.163	-1.049
	.476		-.265	-.327	-.383	-.472	-.547	-.656
	.481		-.123	-.151	-.172	-.193	-.227	-.331
	.491		-.020	-.042	-.046	-.050	-.045	-.051
	.501		.037	.020	.011	.012	.018	.023
	.511		.100	.077	.073	.075	.075	.068
	.521		.191	.168	.159	.149	.149	.125
	.531		.436	.385	.347	.309	.280	.228
Transition flare	.539		.285	.245	.208	.170	.141	.096
	.546		.189	.144	.106	.074	.046	.006
	.552		.099	.048	.010	-.028	-.051	-.092
	.562		-.153	-.210	-.242	-.270	-.287	-.305
Main stage	.568		-.770	-.814	-.801	-.771	-.709	-.664
	.577		-.169	-.191	-.207	-.211	-.205	-.212
	.587		-.089	-.117	-.127	-.125	-.119	-.126
	.597		-.060	-.083	-.086	-.085	-.074	-.086
	.607		-.043	-.060	-.064	-.062	-.051	-.063
	.617		-.031	-.048	-.052	-.045	-.039	-.046
	.627		-.020	-.037	-.041	-.039	-.028	-.034
	.637		-.014	-.031	-.029	-.028	-.017	-.023
	.657		-.003	-.018	-.020	-.018	-.009	-.011
	.677		-.010	-.014	-.018	-.014	-.005	-.010
	.697		.003	-.010	-.012	-.011	-.003	-.006
	.737		.005	-.012	-.012	-.009	-.001	-.008
	.777		.009	-.014	-.006	-.005	.003	-.006
	.785		.016	-.008	.003	-.001	.006	.002
	.817		.014	-.002	-.004	-.002	.003	-.004
	.857		.010	-.006	-.006	-.006	-.001	-.009
	.877		.010	-.005	-.006	-.006	-.001	-.009
	.897		.007	-.008	-.009	-.008	-.004	-.014

	x/l	C_p for - $\beta = -30^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	438		.435	.373	.315	.261	.211	.121
	.448		.335	.274	.226	.172	.122	.038
	.458		.185	.124	.071	.023	-.028	-.109
Upper stage	.471		-1.385	-1.447	-1.457	-1.415	-1.323	-1.112
	.476		-.305	-.345	-.388	-.444	-.490	-.587
	.481		-.134	-.162	-.166	-.187	-.210	-.274
	.491		-.031	-.048	-.052	-.050	-.051	-.068
	.501		.031	.015	.016	.012	.018	.006
	.511		.089	.072	.073	.075	.069	.051
	.521		.191	.168	.165	.155	.149	.120
	.531		.425	.385	.347	.320	.286	.239
Transition flare	.539		.217	.223	.208	.181	.153	.079
	.546		.076	.071	.061	.035	.006	-.069
	.552		.093	.048	.016	-.022	-.051	-.092
	.562		-.170	-.210	-.242	-.270	-.287	-.334
Main stage	.568		-.667	-.700	-.698	-.685	-.663	-.684
	.577		-.169	-.197	-.201	-.205	-.205	-.223
	.587		-.100	-.117	-.127	-.125	-.119	-.137
	.597		-.060	-.077	-.075	-.073	-.068	-.080
	.607		-.049	-.060	-.064	-.062	-.057	-.069
	.617		-.037	-.048	-.052	-.045	-.039	-.057
	.627		-.031	-.043	-.041	-.039	-.034	-.048
	.637		-.026	-.031	-.029	-.028	-.022	-.034
	.657		-.016	-.024	-.024	-.022	-.018	-.029
	.677		-.007	-.012	-.012	-.011	-.009	-.025
	.697		-.007	-.014	-.012	-.011	-.009	-.027
	.737		-.003	-.012	-.010	-.009	-.005	-.029
	.777		-.003	-.014	-.004	.001	-.001	-.029
	.785		.003	-.010	-.006	-.001	.001	-.027
	.817		.004	-.004	-.004	-.003	-.002	-.033
	.857		-.002	-.009	-.008	-.007	-.006	-.036
	.877		-.003	-.009	-.008	-.007	-.008	-.036
	.897		-.004	-.011	-.010	-.010	-.012	-.038
	.917		-.005	-.012	-.010	-.011	-.014	-.038
	.957		-.018	-.021	-.020	-.023	-.025	-.049
	.997		-.079	-.074	-.075	-.083	-.092	-.125

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 223 - Continued

(b) M = 0.60; α = -10° to 10° - Concluded

	x/l	C_p for - ϕ = -60°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.438		.374	.346	.320	.283	.233	.138
	.448		.280	.252	.220	.178	.139	.050
	.458		.141	.113	.077	.050	.017	-.069
Upper stage	.471		-1.391	-1.441	-1.445	-1.455	-1.444	-1.456
	.476		-.339	-.367	-.377	-.404	-.438	-.485
	.481		-.183	-.168	-.166	-.182	-.199	-.257
	.491		-.060	-.060	-.052	-.056	-.068	-.114
	.501		.003	.009	.011	.012	-.005	-.051
	.511		.066	.072	.073	.069	.058	.006
	.521		.157	.157	.165	.155	.137	.080
Transition flare	.531		.368	.351	.336	.320	.291	.228
	.539		.256	.234	.208	.175	.141	.084
	.546		.198	.168	.101	.110	.076	.019
	.552		.037	.026	.010	-.016	-.045	-.121
	.562		-.222	-.238	-.248	-.270	-.299	-.363
Main stage	.568		-.798	-.809	-.790	-.783	-.800	-.864
	.577		-.197	-.197	-.201	-.205	-.217	-.263
	.587		-.129	-.128	-.127	-.125	-.137	-.177
	.597		-.089	-.083	-.081	-.085	-.097	-.143
	.607		-.071	-.060	-.064	-.062	-.069	-.120
	.617		-.060	-.054	-.052	-.051	-.057	-.109
	.627		-.054	-.048	-.041	-.039	-.051	-.092
	.637		-.043	-.037	-.029	-.033	-.039	-.086
	.657		-.035	-.029	-.022	-.024	-.036	-.073
	.677		-.028	-.022	-.017	-.020	-.031	-.064
	.697		-.020	-.014	-.012	-.016	-.026	-.055
	.737		-.024	-.014	-.008	-.011	-.018	-.048
	.777		-.020	-.010	-.006	-.009	-.015	-.040
	.785		-.022	-.012	-.003	-.005	-.013	-.036
	.817		-.019	-.009	-.003	-.006	-.012	-.036
	.857		-.021	-.013	-.008	-.010	-.013	-.037
	.877		-.023	-.013	-.008	-.010	-.014	-.036
	.897		-.024	-.015	-.008	-.011	-.014	-.038
	.917		-.030	-.020	-.013	-.016	-.019	-.042
	.957		-.036	-.026	-.020	-.024	-.029	-.051
	.997		-.100	-.085	-.075	-.085	-.095	-.129

	x/l	C_p for - ϕ = -90°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.428		.396	.407	.409	.399	.377	.288
	.448		.208	.219	.215	.205	.189	.121
	.458		.069	.080	.077	.073	.072	.000
Upper stage	.471		-1.568	-1.567	-1.543	-1.570	-1.541	-1.576
	.491		-.077	-.060	-.052	-.050	-.074	-.137
	.511		.043	.060	.073	.064	.046	-.029
Transition flare	.531		.334	.339	.347	.349	.331	.262
	.552		-.003	.003	.010	.001	-.022	-.092
Main stage	.568		-.924	-.895	-.870	-.886	-.909	-.972
	.587		-.146	-.134	-.127	-.131	-.142	-.206
	.607		-.083	-.071	-.064	-.062	-.079	-.143
	.627		-.066	-.048	-.041	-.045	-.057	-.132
	.657		-.049	-.031	-.024	-.028	-.045	-.107
	.697		-.041	-.024	-.014	-.020	-.038	-.101
	737		-.033	-.018	-.008	-.014	-.030	-.088
	.777		-.031	-.014	-.004	-.011	-.028	-.086
	.785		-.033	-.014	-.006	-.011	-.030	-.080
	.817		-.027	-.009	-.002	-.006	.021	-.078
	.857		-.030	-.015	-.008	-.012	-.026	-.083
	.897		-.031	-.017	-.009	-.014	-.029	-.083

... -- PRESSURE COEFFICIENTS FOR CONFIGURATION 223 - Continued

(c) M = 0.80; α = -10° to 10°

	x/l	C_p for - $\phi = 0°$						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.428	.687	.604	.539	.477	.413	.349	.271
	.438	.598	.508	.446	.387	.320	.260	.182
	.448	.484	.394	.336	.278	.216	.160	.087
	.458	.371	.280	.226	.168	.111	.059	-.007
	.471	-1.062	-1.043	-1.166	-1.104	-.907	-.746	-.616
Upper stage	.476	-.764	-.803	-.787	-.734	-.657	-.570	-.494
	.481	-.232	-.539	-.515	-.528	-.538	-.520	-.494
	.491	.025	.005	-.074	-.152	-.250	-.295	-.329
	.501	.067	.055	.041	.024	-.039	-.100	-.145
	.511	.136	.120	.110	.108	.073	.027	-.015
	.521	.291	.224	.206	.188	.145	.103	.062
	.531	.520	.458	.402	.333	.234	.168	.119
Transition flare	.539	.396	.335	.291	.235	.170	.125	.095
	.546	.303	.236	.204	.166	.102	.064	.042
	.552	.222	.149	.113	.069	.011	-.023	-.042
	.562	.002	-.068	-.109	-.162	-.221	-.243	-.251
Main stage	.568	-1.198	-1.225	-1.259	-1.252	-1.029	-.802	-.676
	.577	-.144	-.184	-.204	-.222	-.239	-.230	-.226
	.587	-.075	-.102	-.116	-.122	-.139	-.134	-.130
	.597	-.044	-.068	-.078	-.084	-.093	-.092	-.084
	.607	-.025	-.052	-.059	-.061	-.070	-.069	-.057
	.617	-.013	-.041	-.047	-.045	-.054	-.050	-.042
	.627	-.006	-.029	-.035	-.034	-.043	-.038	-.030
	.637	.003	-.018	-.024	-.026	-.031	-.031	-.023
	.657	.016	-.007	-.016	-.015	-.022	-.019	-.013
	.677	.020	-.005	-.012	-.011	-.017	-.015	-.010
	.697	.024	-.002	-.009	-.007	-.013	-.012	-.007
	.737	.025	.006	-.009	-.003	-.011	-.009	-.009
	.777	.032	.007	-.001	.001	-.007	-.005	-.007
	.785	.041	.013	.004	.006	.000	.000	.000
	.817	.039	.013	.004	.004	-.002	-.003	-.007
	.857	.032	.008	-.001	.001	-.006	-.006	-.014
	.877	.033	.009	.000	.001	-.005	-.007	-.015
	.897	.029	.004	-.003	-.002	-.008	-.011	-.020

	x/l	C_p for - $\phi = -30°$						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.438	.557	.489	.435	.384	.324	.267	.182
	.448	.471	.396	.342	.294	.238	.182	.119
	.458	.326	.258	.211	.164	.111	.059	-.004
	.471	-1.309	-1.344	-1.3[illegible]	-1.185	-.880	-.731	-.619
Upper stage	.476	-.638	-.704	-.726	-.760	-.657	-.597	-.551
	.481	-.190	-.378	-.545	-.558	- 553	-.513	-.486
	.491	-.013	-.033	-.081	-.156	-.242	-.287	-.314
	.501	.048	.044	.049	.039	-.024	-.092	-.145
	.511	.110	.109	.107	.112	.076	.031	-.023
	.521	.232	.220	.206	.192	.145	.107	.065
	.531	.497	.454	.410	.338	.249	.191	.157
Transition flare	.539	.233	.263	.268	.243	.201	.166	.099
	.546	.112	.123	.124	.114	.079	.042	-.027
	.552	.188	.134	.109	.069	.011	-.019	-.046
	.562	-.033	-.095	-.129	-.166	-.221	-.243	-.266
Main stage	.568	-1.064	-1.098	-1.105	-1.083	-.963	-.933	-1.029
	.577	-.190	-.252	-.266	-.226	-.228	-.226	-.242
	.587	-.082	-.098	-.105	-.122	-.139	-.138	-.130
	.597	-.048	-.056	-.062	-.065	-.074	-.073	-.073
	.607	-.048	-.052	-.059	-.061	-.070	-.069	-.069
	.617	-.036	-.045	-.047	-.045	-.054	-.054	-.050
	.627	-.032	-.041	-.039	-.038	-.043	-.046	-.046
	.637	-.021	-.029	-.032	-.026	-.035	-.035	-.034
	.657	-.009	-.022	-.020	-.016	-.025	-.026	-.027
	.677	.004	-.006	-.009	-.004	-.013	-.017	-.019
	.697	-.003	-.010	-.012	-.007	-.015	-.017	-.020
	.737	-.004	-.009	-.009	-.003	-.009	-.012	-.022
	.777	.013	.002	.001	.002	-.008	-.008	-.023
	.785	.010	.000	.001	.006	-.002	-.008	-.020
	.817	.012	.001	.001	.004	-.003	-.006	-.028
	.857	.005	-.004	-.005	.000	-.007	-.011	-.032
	.877	.003	-.005	-.005	-.001	-.008	-.012	-.035
	.897	.003	-.007	-.006	-.003	-.009	-.015	-.035
	.917	.002	-.007	-.007	-.003	-.011	-.017	-.037
	.957	-.011	-.019	-.018	-.015	-.022	-.031	-.050
	.997	-.095	-.085	-.074	-.074	-.086	-.100	-.126

PRESSURE COEFFICIENTS FOR CONFIGURATION 223 - Continued

M = 0.80; α = -10° to 10° - Continued

	x	C_p for - β = [illegible] α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.439	.434	.424	.412	.384	.337	.288	.225
	.448	.352	.336	.344	.274	.253	.200	.123
	.458	.233	.217	.200	.175	.137	.098	.022
	.471	-1.251	-1.276	-1.191	-1.115	-.853	-.777	-.716
Upper stage	.476	-.659	-.730	-.685	-.662	-.645	-.674	-.584
	.481	-.424	-.651	-.535	-.532	-.546	-.543	-.532
	.491	-.375	-.394	-.475	-.495	-.251	-.287	-.323
	.501	-.075	.025	.038	.026	-.012	-.161	-.135
	.511	.044	.090	.107	.115	.092	.051	-.015
	.521	.152	.186	.191	.189	.157	.126	.069
	.531	.393	.412	.365	.315	.272	.249	.235
Transition flare	.539	.337	.331	.276	.239	.182	.136	.087
	.545	.265	.244	.222	.165	.135	.095	.045
	.552	.087	.092	.089	.065	.030	[illegible]	-.065
	.562	-.127	-.130	-.148	-.177	-.216	-.224	-.266
Main stage	.568	-1.256	-1.284	-1.267	-1.235	-1.244	-1.288	-1.317
	.577	-.227	-.215	-.235	-.211	-.221	-.226	-.303
	.587	-.153	-.129	-.128	-.126	-.135	-.138	-.165
	.597	-.125	-.095	-.097	-.080	-.089	-.100	-.134
	.607	-.106	-.079	-.082	-.057	-.073	-.084	-.115
	.617	-.098	-.072	-.055	-.045	-.054	-.069	-.100
	.627	-.094	-.061	-.047	-.034	-.047	-.058	-.092
	.637	-.087	-.052	-.035	-.026	-.039	-.050	-.084
	.657	-.073	-.041	-.025	-.016	-.027	-.040	-.072
	.677	-.058	-.037	-.019	-.011	-.022	-.035	-.064
	.697	-.045	-.023	-.014	-.006	-.017	-.031	-.057
	.717	-.054	-.025	-.012	-.002	-.013	-.024	-.044
	.777	-.047	-.022	-.007	.002	-.008	-.018	-.038
	.785	-.053	-.023	-.007	.003	-.007	-.017	-.036
	.817	-.045	-.017	-.002	.005	-.005	-.015	-.033
	.857	-.052	-.024	-.009	.000	-.009	-.018	-.035
	.877	-.052	-.024	-.009	.000	-.009	-.018	-.035
	.897	-.051	-.024	-.015	-.001	-.010	-.021	-.037
	.917	-.063	-.031	-.018	-.007	-.015	-.025	-.042
	.957	-.067	-.038	-.021	-.015	-.024	-.034	-.051
	.997	-.133	-.134	-.085	-.073	-.088	-.106	-.131

	x	C_p for - β = [illegible] α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.428	.357	.444	.472	.413	.454	.423	.353
	.448	.225	.269	.286	.287	.275	.252	.193
	.458	.110	.150	.167	.168	.156	.137	.089
	.471	-1.243	-1.201	-1.192	-1.143	-1.175	-1.131	-1.112
Upper stage	.491	-.178	-.205	-.204	-.191	-.200	-.215	-.237
	.511	-.017	.063	.091	.108	.092	.054	-.034
	.531	.317	.350	.329	.322	.314	.325	.284
Transition flare	.552	-.009	.043	.065	.065	.053	.090	-.034
Main stage	.568	-1.314	-1.298	-1.267	-1.206	-1.260	-1.293	-1.317
	.587	-.190	-.141	-.132	-.126	-.135	-.146	-.199
	.607	-.136	-.091	-.070	-.061	-.075	-.088	-.146
	.627	-.121	-.068	-.047	-.038	-.047	-.069	-.126
	.657	-.103	-.054	-.029	-.017	-.030	-.051	-.107
	.697	-.094	-.043	-.020	-.008	-.021	-.045	-.097
	.737	-.085	-.037	-.014	-.002	-.016	-.036	-.090
	.777	-.081	-.032	-.010	.002	-.012	-.033	-.084
	.785	-.084	-.034	-.011	.002	-.009	-.031	-.078
	.817	-.071	-.028	-.005	.006	-.005	-.024	-.074
	.857	-.076	-.031	-.010	.000	-.010	-.031	-.080
	.897	-.078	-.034	-.013	-.002	-.013	-.033	-.083

PRESSURE COEFFICIENTS FOR CONFIGURATION 223 - Continued

(a) M = 1.00; α = -10° to 10°

	x/l	C_p for - $\beta = 3^\circ$						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.424	.413	.731	.669	.609	.548	.490	.410
	.438	.732	.652	.589	.529	.465	.407	.330
	.448	.634	.560	.500	.442	.384	.329	.255
	.458	.539	.468	.411	.355	.302	.250	.179
Upper stage	.471	-.638	-.670	-.674	-.692	-.699	-.638	-.712
	.476	-.696	-.770	-.819	-.856	-.811	-.485	-.625
	.481	-.529	-.645	-.722	-.776	-.622	-.495	-.507
	.491	-.309	-.438	-.527	-.597	-.303	-.403	-.406
	.501	-.206	-.307	-.381	-.097	-.212	-.348	-.293
	.511	.144	.109	.107	.079	-.108	-.202	-.181
	.521	.351	.330	.299	.168	.011	-.078	-.065
	.531	.616	.543	.451	.259	.114	.115	.045
Transition flare	.539	.554	.519	.486	.376	.164	.174	.104
	.546	.473	.434	.413	.379	.185	.168	.128
	.552	.404	.359	.331	.307	.158	.143	.104
	.562	.253	.215	.178	.130	.001	-.013	-.035
Main stage	.568	-.661	-.681	-.697	-.712	-.637	-.655	-.750
	.577	-.414	-.488	-.532	-.553	-.374	-.362	-.398
	.587	-.307	-.396	-.449	-.461	-.374	-.380	-.401
	.597	-.222	-.299	-.348	-.363	-.344	-.343	-.343
	.607	-.176	-.234	-.272	-.277	-.283	-.261	-.230
	.617	-.161	-.204	-.226	-.206	-.221	-.194	-.166
	.627	-.152	-.183	-.177	-.162	-.170	-.145	-.126
	.637	-.133	-.143	-.122	-.125	-.136	-.111	-.099
	.657	-.117	-.086	-.046	-.090	-.094	-.078	-.066
	.677	-.096	-.067	-.073	-.076	-.079	-.062	-.058
	.697	-.043	-.051	-.059	-.060	-.068	-.049	-.046
	.737	-.022	-.038	-.042	-.044	-.054	-.039	-.044
	.777	-.007	-.016	-.026	-.026	-.029	-.034	-.038
	.785	.007	-.009	-.016	-.018	-.018	-.022	-.020
	.817	.007	-.005	-.014	-.026	-.027	-.013	.003
	.857	.054	.034	.025	.014	-.035	.020	.016
	.877	.064	.046	.036	.027	-.009	.026	.018
	.897	.058	.042	.032	.026	.016	.023	.012

	x/l	C_p for - $\beta = -3^\circ$						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.438	.686	.628	.580	.523	.468	.410	.330
	.448	.612	.551	.503	.449	.394	.339	.280
	.458	.497	.447	.403	.352	.302	.253	.182
Upper stage	.471	-.709	-.759	-.781	-.808	-.831	-.846	-.837
	.476	-.738	-.800	-.838	-.865	-.881	-.842	-.525
	.481	-.583	-.672	-.731	-.779	-.674	-.540	-.452
	.491	-.325	-.438	-.515	-.557	-.303	-.403	-.379
	.501	-.209	-.325	-.381	-.085	-.193	-.269	-.290
	.511	.123	.098	.107	.064	-.102	-.144	-.190
	.521	.320	.324	.287	.125	.004	-.001	-.080
	.531	.588	.528	.433	.216	.108	.112	.036
Transition flare	.539	.382	.434	.470	.412	.380	.324	.243
	.546	.277	.317	.343	.352	.302	.237	.131
	.552	.370	.350	.331	.292	.179	.159	.089
	.562	.217	.190	.166	.124	.031	.014	-.038
Main stage	.568	-.652	-.659	-.669	-.672	-.686	-.725	-.756
	.577	-.490	-.537	-.571	-.525	-.417	-.521	-.505
	.587	-.370	-.387	-.431	-.437	-.377	-.392	-.398
	.597	-.197	-.244	-.278	-.278	-.267	-.264	-.261
	.607	-.216	-.250	-.281	-.275	-.283	-.261	-.239
	.617	-.194	-.213	-.226	-.214	-.221	-.194	-.181
	.627	-.188	-.198	-.186	-.171	-.173	-.151	-.148
	.637	-.173	-.164	-.128	-.131	-.139	-.120	-.123
	.657	-.128	-.094	-.091	-.092	-.098	-.088	-.092
	.677	-.076	-.068	-.069	-.070	-.075	-.066	-.078
	.697	-.069	-.061	-.062	-.061	-.069	-.056	-.074
	.737	-.045	-.043	-.043	-.040	-.055	-.044	-.073
	.777	-.025	-.022	-.024	-.022	-.026	-.038	-.066
	.785	-.019	-.013	-.018	-.017	-.018	-.031	-.057
	.817	-.018	-.014	-.020	-.026	-.028	-.073	-.035
	.857	.030	.027	.018	.013	-.038	.013	-.008
	.877	.035	.033	.030	.025	-.014	.018	-.005
	.897	.034	.033	.029	.026	.014	.016	-.005
	.917	.034	.033	.027	.025	.022	.013	-.004
	.957	.022	.021	.017	.012	.011	-.005	-.017
	.997	-.040	-.051	-.071	-.097	-.113	-.130	-.145

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 223 - Continued

(a) M = .00; α = -10° to 10° - Concluded

	x/ℓ	C_p for - β = -0°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.436	.571	.569	.550	.520	.483	.440	.351
	.446	.538	.498	.479	.446	.409	.363	.286
	.456	.408	.406	.388	.361	.323	.283	.203
	.471	-.715	-.728	-.710	-.744	-.764	-.785	-.797
Upper stage	.476	-.808	-.825	-.847	-.865	-.884	-.897	-.604
	.481	-.647	-.694	-.737	-.776	-.799	-.747	-.470
	.491	-.404	-.505	-.548	-.572	-.342	-.354	-.382
	.501	-.230	-.371	-.368	-.064	-.184	-.214	-.293
	.511	.056	.089	.095	.043	-.081	-.102	-.1
	.521	.223	.281	.256	.128	.044	.048	-.033
	.531	.454	.464	.390	.216	.175	.191	.100
Transition flare	.539	.494	.491	.485	.406	.242	.177	.164
	.546	.441	.439	.434	.394	.259	.196	.166
	.552	.259	.302	.316	.295	.266	.207	.086
	.562	.124	.151	.148	.105	.100	.062	-.029
Main stage	.568	-.716	-.708	-.709	-.703	-.722	-.744	-.777
	.577	-.579	-.583	-.587	-.513	-.615	-.664	-.722
	.587	-.436	-.448	-.467	-.424	-.460	-.551	-.609
	.597	-.341	-.357	-.330	-.322	-.365	-.392	
	.607	-.307	-.293	-.293	-.275	-.258	-.255	-.267
	.617	-.295	-.259	-.226	-.217	-.209	-.197	-.221
	.627	-.286	-.216	-.171	-.171	-.173	-.163	-.197
	.637	-.237	-.161	-.131	-.134	-.139	-.142	-.175
	.657	-.171	-.111	-.094	-.092	-.102	-.109	-.136
	.677	-.139	-.091	-.077	-.075	-.087	-.091	-.114
	.697	-.106	-.070	-.060	-.059	-.073	-.073	-.093
	.737	-.101	-.059	-.049	-.039	-.060	-.058	-.076
	.777	-.086	-.045	-.031	-.025	-.029	-.049	-.065
	.785	-.087	-.041	-.029	-.022	-.023	-.044	-.058
	.817	-.072	-.029	-.022	-.025	-.030	-.035	-.035
	.857	-.021	.009	.015	.014	-.043	.008	-.002
	.877	-.016	.015	.026	.025	-.021	.013	.001
	.897	-.020	.014	.025	.027	.014	.013	.001
	.917	-.030	.006	.018	.022	.020	.007	-.002
	.957	-.032	.002	.012	.012	.010	-.005	-.014
	.997	-.103	-.083	-.085	-.098	-.111	-.129	-.151

	x/ℓ	C_p for - β = -30°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.428	.532	.586	.610	.606	.586	.564	.493
	.448	.382	.436	.450	.446	.435	.410	.351
	.458	.296	.347	.358	.358	.347	.327	.271
	.471	-.764	-.756	-.753	-.756	-.760	-.767	-.785
Upper stage	.491	-.388	-.566	-.588	-.548	-.546	-.534	-.345
	.511	-.075	.038	.049	.034	.001	.005	-.080
	.531	.296	.382	.329	.195	.297	.337	.288
Transition flare	.552	.148	.257	.301	.283	.281	.231	.125
Main stage	.568	-.768	-.733	-.724	-.718	-.725	-.741	-.774
	.587	-.539	-.500	-.489	-.469	-.499	-.518	-.551
	.607	-.405	-.335	-.281	-.275	-.261	-.328	-.404
	.627	-.252	-.179	-.156	-.171	-.167	-.175	-.252
	.657	-.193	-.120	-.095	-.094	-.108	-.132	-.194
	.697	-.144	-.088	-.066	-.062	-.078	-.091	-.145
	.737	-.128	-.067	-.045	-.039	-.063	-.072	-.124
	.777	-.109	-.054	-.034	-.026	-.032	-.062	-.112
	.785	-.114	-.055	-.033	-.024	-.026	-.058	-.103
	.817	-.080	-.032	-.023	-.023	-.029	-.047	-.078
	.857	-.043	.002	.014	.015	-.046	-.002	-.036
	.897	-.042	.003	.022	.026	.010	-.001	-.035

TABLE [illegible] - PRESSURE COEFFICIENTS FOR CONFIGURATION 223 - Continued

(e) M = 1.20; α = -10° to 10°

	x/l	C_p for - ϕ = 0°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.428	.886	.800	.733	.674	.614	.559	.483
	.438	.825	.745	.677	.622	.561	.504	.425
	.448	.755	.679	.619	.565	.510	.455	.380
	.458	.686	.613	.561	.508	.458	.406	.335
Upper stage	.471	-.310	-.339	-.339	-.349	-.360	-.373	-.384
	.476	-.340	-.453	-.489	-.516	-.543	-.558	-.577
	.481	-.276	-.372	-.424	-.467	-.505	-.537	-.558
	.491	-.124	-.234	-.291	-.345	-.396	-.436	-.387
	.501	-.053	-.150	-.201	-.250	-.298	-.328	-.108
	.511	-.024	-.106	-.147	-.182	-.057	.052	-.078
	.521	-.015	-.041	.052	.182	.119	.098	-.005
Transition flare	.531	.519	.425	.374	.312	.233	.161	.098
	.539	.628	.567	.499	.410	.274	.196	.151
	.546	.566	.522	.496	.445	.322	.242	.199
	.552	.518	.471	.445	.415	.330	.258	.215
	.562	.424	.375	.343	.308	.233	.172	.140
Main stage	.568	-.342	-.360	-.365	-.378	-.392	-.397	-.367
	.577	-.193	-.243	-.272	-.291	-.256	-.225	-.204
	.587	-.138	-.204	-.240	-.256	-.248	-.239	-.236
	.597	-.089	-.150	-.185	-.207	-.220	-.225	-.231
	.607	-.056	-.115	-.144	-.169	-.185	-.195	-.193
	.617	-.048	-.096	-.120	-.139	-.152	-.157	-.144
	.627	-.032	-.079	-.101	-.114	-.122	-.119	-.100
	.637	-.021	-.063	-.079	-.085	-.090	-.089	-.065
	.657	-.024	-.057	-.067	-.063	-.052	-.042	-.030
	.677	-.023	-.033	-.042	-.040	-.035	-.023	-.019
	.697	-.016	-.035	-.040	-.033	-.018	-.013	-.015
	.737	-.019	-.027	-.023	-.034	-.026	-.024	-.005
	.777	.016	-.011	-.027	-.021	-.024	-.027	-.011
	.785	.026	-.003	-.016	-.013	-.015	-.010	.000
	.817	.024	-.002	-.003	-.021	-.019	-.011	-.002
	.857	.020	.010	-.009	-.003	.001	-.008	-.011
	.877	.032	-.003	-.005	.000	-.004	-.006	-.009
	.897	.013	-.003	.001	-.004	-.009	-.015	-.017

	x/l	C_p for - ϕ = -30°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.438	.780	.719	.667	.616	.561	.511	.425
	.448	.728	.669	.622	.571	.519	.467	.401
	.458	.644	.595	.551	.506	.461	.417	.335
Upper stage	.471	-.375	-.415	-.434	-.447	-.458	-.482	-.496
	.476	-.422	-.475	-.500	-.521	-.540	-.558	-.588
	.481	-.314	-.391	-.432	-.464	-.499	-.526	-.561
	.491	-.137	-.234	-.288	-.337	-.380	-.417	-.428
	.501	-.078	-.158	-.206	-.250	-.293	-.306	-.103
	.511	-.059	-.122	-.158	-.190	-.087	.044	-.067
	.521	-.034	-.044	.071	.193	.171	.077	-.008
Transition flare	.531	.492	.415	.361	.304	.223	.133	.077
	.539	.478	.495	.472	.418	.375	.344	.282
	.546	.398	.434	.453	.439	.408	.365	.271
	.552	.489	.461	.445	.413	.349	.290	.226
	.562	.390	.359	.332	.297	.247	.202	.156
Main stage	.568	-.342	-.351	-.354	-.357	-.373	-.397	-.432
	.577	-.249	-.283	-.302	-.302	-.291	-.288	-.397
	.587	-.146	-.199	-.229	-.242	-.237	-.236	-.253
	.597	-.081	-.117	-.139	-.153	-.158	-.160	-.163
	.607	-.086	-.131	-.150	-.169	-.182	-.187	-.187
	.617	-.070	-.109	-.123	-.139	-.150	-.157	-.149
	.627	-.064	-.096	-.106	-.117	-.125	-.127	-.116
	.637	-.054	-.079	-.085	-.090	-.095	-.095	-.087
	.657	-.045	-.051	-.059	-.054	-.046	-.047	-.057
	.677	-.043	-.033	-.038	-.035	-.032	-.030	-.046
	.697	-.046	-.044	-.037	-.035	-.029	-.024	-.047
	.737	-.042	-.033	-.027	-.031	-.026	-.032	-.048
	.777	-.006	-.018	-.024	-.016	-.023	-.028	-.059
	.785	-.001	-.013	-.014	-.008	-.012	-.018	-.054
	.817	.000	-.013	-.006	-.018	-.017	-.022	-.066
	.857	-.007	.003	-.008	-.010	-.008	-.020	-.067
	.877	.003	-.014	-.006	-.002	-.005	-.018	-.062
	.897	-.010	-.010	-.003	-.001	-.005	-.020	-.054
	.917	-.010	-.004	-.004	-.005	-.007	-.018	-.042
	.957	-.011	-.015	-.012	-.016	-.017	-.019	-.033
	.997	.000	-.021	-.033	-.052	-.072	-.090	-.077

TABLE 9.- PRESSURE COEFFICIENTS FOR CONFIGURATION 223 - Concluded

(e) M = 1.20; α = -10° to 10° - Concluded

	x/l	C_p for - ϕ = -60°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.438	.665	.663	.643	.614	.580	.543	.448
	.448	.622	.613	.595	.569	.535	.490	.404
	.458	.551	.550	.535	.514	.480	.438	.356
Upper stage	.471	-.419	-.393	-.390	-.390	-.406	-.428	-.452
	.476	-.487	-.513	-.524	-.535	-.551	-.566	-.588
	.481	-.368	-.407	-.437	-.464	-.494	-.512	-.547
	.491	-.227	-.282	-.312	-.342	-.366	-.393	-.425
	.501	-.167	-.204	-.231	-.258	-.285	-.303	-.260
	.511	-.137	-.160	-.174	-.187	-.203	-.059	-.065
	.521	-.108	-.C25	.117	.195	.176	.101	.030
Transition flare	.531	.378	.355	.336	.304	.255	.196	.131
	.539	.574	.546	.496	.418	.332	.279	.218
	.546	.538	.519	.496	.453	.367	.317	.252
	.552	.390	.415	.426	.413	.381	.330	.234
	.562	.301	.316	.316	.297	.274	.239	.159
Main stage	.568	-.391	-.379	-.379	-.381	-.389	-.413	-.449
	.577	-.320	-.319	-.313	-.305	-.332	-.372	-.429
	.587	-.239	-.248	-.248	-.245	-.272	-.321	-.372
	.597	-.184	-.188	-.193	-.196	-.207	-.244	-.329
	.607	-.165	-.158	-.155	-.161	-.169	-.179	-.244
	.617	-.154	-.139	-.134	-.139	-.144	-.152	-.182
	.627	-.154	-.128	-.115	-.117	-.125	-.138	-.160
	.637	-.132	-.106	-.090	-.093	-.098	-.111	-.138
	.657	-.131	-.C66	-.057	-.044	-.049	-.076	-.113
	.677	-.115	-.C63	-.047	-.040	-.045	-.063	-.100
	.697	-.100	-.C60	-.037	-.037	-.041	-.050	-.086
	.737	-.097	-.053	-.032	-.031	-.032	-.052	-.064
	.777	-.065	-.C4C	-.026	-.017	-.025	-.037	-.052
	.785	-.054	-.C39	-.020	-.008	-.016	-.030	-.050
	.817	-.056	-.C25	-.011	-.016	-.018	-.033	-.048
	.857	-.063	-.C17	-.015	-.015	-.023	-.032	-.047
	.877	-.053	-.C31	-.007	-.003	-.008	-.022	-.041
	.897	-.062	-.029	-.009	.001	-.003	-.018	-.031
	.917	-.069	-.C32	-.017	-.007	-.010	-.021	-.028
	.957	-.068	-.C36	-.015	-.015	-.020	-.019	-.032
	.997	-.059	-.C47	-.042	-.053	-.066	-.089	-.104

	x/l	C_p for - ϕ = -90°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.428	.607	.655	.667	.669	.659	.633	.572
	.448	.496	.553	.569	.569	.556	.533	.475
	.458	.435	.489	.509	.508	.506	.480	.419
Upper stage	.471	-.416	-.4C1	-.399	-.4C1	-.406	-.411	-.439
	.491	-.322	-.334	-.342	-.350	-.355	-.349	-.352
	.511	-.232	-.204	-.190	-.187	-.198	-.211	-.252
Transition flare	.531	.272	.295	.304	.304	.290	.277	.231
	.552	.293	.372	.4C8	.413	.4C0	.360	.269
Main stage	.568	-.440	-.406	-.392	-.384	-.392	-.408	-.443
	.587	-.320	-.281	-.259	-.242	-.264	-.291	-.334
	.607	-.247	-.194	-.174	-.161	-.177	-.212	-.253
	.627	-.230	-.142	-.117	-.114	-.117	-.136	-.234
	.657	-.153	-.078	-.054	-.045	-.055	-.088	-.152
	.697	-.145	-.079	-.047	-.038	-.050	-.075	-.146
	.737	-.115	-.063	-.038	-.033	-.033	-.065	-.124
	.777	-.080	-.046	-.027	-.017	-.024	-.050	-.102
	.785	-.090	-.051	-.027	-.013	-.023	-.049	-.104
	.817	-.079	-.030	-.C12	-.010	-.019	-.041	-.090
	.857	-.082	-.030	-.017	-.010	-.031	-.050	-.087
	.897	-.085	-.041	-.017	-.C05	-.007	-.026	-.073

TABLE ... - PRESSURE COEFFICIENTS FOR CONFIGURATION 323

(a) M = 0.40 to 0.95; $\alpha = 0^\circ$

	x/l	C_p for - $\beta = 0^\circ$					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.443	.473	.553	.577	.634	.660	.697
	.453	.320	.407	.436	.488	.516	.560
	.463	.080	.203	.234	.308	.346	.393
Upper stage	.471	-1.366	-.748	-.661	-.545	-.583	-.692
	.476	-.625	-.558	-.471	-.403	-.409	-.490
	.481	-.220	-.536	-.488	-.396	-.402	-.477
	.491	-.052	-.360	-.413	-.389	-.395	-.452
	.501	.016	-.161	-.259	-.353	-.379	-.401
	.511	.072	.031	-.088	-.281	-.328	-.334
	.521	.151	.132	.066	-.177	-.257	-.257
	.531	.319	.241	.179	-.048	-.153	-.161
Transition flare	.539	-1.334	-.289	-.188	-.192	-.112	-.033
	.546	.093	.138	.164	.125	.059	.034
	.552	.015	.057	.090	.129	.096	.081
	.562	-.220	-.179	-.138	-.041	-.014	-.014
Main stage	.568	-.592	-.723	-.705	-.615	-.554	-.580
	.577	-.187	-.193	-.188	-.163	-.169	-.298
	.587	-.108	-.115	-.113	-.098	-.105	-.196
	.597	-.074	-.079	-.076	-.066	-.072	-.110
	.607	-.063	-.056	-.055	-.052	-.055	-.062
	.617	-.041	-.047	-.044	-.041	-.045	-.039
	.627	-.029	-.038	-.034	-.030	-.034	-.030
	.637	-.029	-.024	-.026	-.023	-.028	-.023
	.657	-.019	-.017	-.017	-.015	-.020	-.018
	.677	-.015	-.014	-.012	-.013	-.018	-.017
	.697	-.007	-.009	-.009	-.009	-.014	-.015
	.737	-.007	-.007	-.008	-.008	-.013	-.016
	.777	-.003	-.002	-.002	-.001	-.008	-.011
	.785	.001	.001	.006	.004	-.002	-.005
	.817	.001	.002	.003	.002	-.004	-.008
	.857	-.001	-.001	-.001	-.002	-.008	-.012
	.877	-.001	.000	.000	-.001	-.008	-.012
	.897	-.002	-.003	-.004	-.004	-.011	-.015

	x/l	C_p for - $\beta = -30^\circ$					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.443	.473	.553	.581	.628	.653	.694
	.453	.282	.380	.410	.468	.498	.542
	.463	.091	.207	.238	.308	.343	.390
Upper stage	.471	-.965	-.644	-.562	-.474	-.506	-.575
	.476	-.693	-.499	-.430	-.367	-.379	-.452
	.481	-.412	-.517	-.451	-.371	-.385	-.455
	.491	-.041	-.421	-.426	-.378	-.389	-.445
	.501	.027	-.193	-.292	-.353	-.375	-.404
	.511	.072	.008	-.113	-.288	-.335	-.343
	.521	.151	.127	.041	-.199	-.267	-.273
	.531	.308	.237	.162	-.077	-.163	-.183
Transition flare	.539	-1.907	-.376	-.242	-.091	.022	.128
	.546	-1.030	-.092	-.001	.027	.096	.191
	.552	.015	.057	.090	.094	.072	.037
	.562	-.220	-.175	-.138	-.045	-.028	-.046
Main stage	.568	-.535	-.595	-.576	-.439	-.406	-.468
	.577	-.176	-.184	-.176	-.156	-.163	-.263
	.587	-.108	-.115	-.113	-.102	-.109	-.196
	.597	-.063	-.060	-.059	-.048	-.055	-.084
	.607	-.052	-.056	-.055	-.052	-.055	-.062
	.617	-.041	-.047	-.042	-.041	-.045	-.042
	.627	-.029	-.038	-.034	-.030	-.038	-.036
	.637	-.029	-.028	-.026	-.023	-.031	-.026
	.657	-.019	-.020	-.018	-.018	-.023	-.021
	.677	-.007	-.007	-.006	-.008	-.013	-.013
	.697	-.011	-.009	-.009	-.009	-.014	-.016
	.737	-.007	-.004	-.005	-.008	-.011	-.014
	.777	-.003	-.002	.000	.001	-.006	-.009
	.785	.001	.004	.006	.004	-.002	-.006
	.817	.001	.003	.003	.002	-.004	-.008
	.857	-.002	-.001	-.001	-.003	-.009	-.013
	.877	-.002	-.003	-.002	-.003	-.010	-.014
	.897	-.004	-.004	-.004	-.005	-.012	-.016
	.917	-.004	-.005	-.005	-.006	-.012	-.016
	.957	-.014	-.016	-.016	-.017	-.025	-.029
	.997	-.066	-.074	-.077	-.081	-.091	-.104

TABLE II.- PRESSURE COEFFICIENTS FOR CONFIGURATION 201 - Continued

(a) M = 0.40 to 0.95; $\alpha = 0^{\circ}$ - Concluded

	x/l	C_p for - $\gamma = -60^{\circ}$					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.443	.473	.553	.581	.628	.653	.691
	.453	.309	.398	.428	.482	.509	.551
	.463	.091	.212	.242	.308	.346	.390
	.471	-.910	-.522	-.459	-.385	-.427	-.511
Upper stage	.476	-.704	-.453	-.401	-.342	-.368	-.436
	.481	-.423	-.472	-.413	-.349	-.368	-.442
	.491	-.041	-.417	-.405	-.367	-.379	-.439
	.501	.027	-.220	-.296	-.346	-.368	-.398
	.511	.072	-.015	-.138	-.285	-.328	-.337
	.521	.139	.104	.008	-.202	-.267	-.270
	.531	.286	.200	.120	-.095	-.176	-.186
Transition flare	.539	.181	.201	.205	.069	-.018	-.055
	.546	.093	.138	.155	.147	.079	.040
	.552	.004	.048	.073	.073	.036	.015
	.562	-.220	-.175	-.134	-.055	-.041	-.058
Main stage	.568	-.569	-.595	-.576	-.396	-.379	-.417
	.577	-.176	-.179	-.176	-.152	-.156	-.250
	.587	-.108	-.115	-.113	-.102	-.109	-.193
	.597	-.074	-.074	-.071	-.070	-.075	-.116
	.607	-.052	-.056	-.055	-.052	-.055	-.068
	.617	-.041	-.047	-.042	-.041	-.045	-.046
	.627	-.029	-.038	-.034	-.034	-.038	-.036
	.637	-.029	-.028	-.026	-.027	-.031	-.030
	.657	-.019	-.019	-.018	-.018	-.023	-.021
	.677	-.013	-.014	-.013	-.013	-.019	-.017
	.697	-.007	-.009	-.008	-.008	-.014	-.014
	.737	-.007	-.006	-.005	-.005	-.011	-.014
	.777	-.003	-.001	.000	.000	-.007	-.010
	.785	.001	-.001	.000	.000	-.006	-.009
	.817	.001	.003	.003	.002	-.004	-.007
	.857	-.001	-.001	-.001	-.003	-.009	-.013
	.877	-.002	-.002	-.002	-.003	-.010	-.014
	.897	-.002	-.003	-.004	-.004	-.011	-.015
	.917	-.007	-.007	-.008	-.009	-.016	-.020
	.957	-.014	-.015	-.016	-.018	-.024	-.029
	.997	-.068	-.075	-.077	-.081	-.092	-.104

	x/l	C_p for - $\gamma = -30^{\circ}$					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.443	.462	.557	.577	.628	.650	.691
	.463	.070	.207	.242	.304	.343	.390
	.471	-1.132	-.531	-.447	-.417	-.432	-.562
Upper stage	.491	-.052	-.412	-.405	-.367	-.385	-.439
	.511	.072	-.015	-.142	-.288	-.328	-.340
	.531	.308	.214	.133	-.095	-.183	-.186
Transition flare	.552	.004	.053	.073	.080	.052	.031
Main stage	.568	-.670	-.718	-.651	-.464	-.409	-.500
	.587	-.108	-.115	-.113	-.102	-.109	-.196
	.607	-.052	-.056	-.055	-.052	-.055	-.065
	.627	-.029	-.038	-.034	-.034	-.038	-.036
	.657	-.023	-.020	-.018	-.019	-.024	-.022
	.697	-.011	-.011	-.011	-.010	-.017	-.017
	.737	-.007	-.004	-.005	-.005	-.011	-.013
	.777	-.003	-.001	.000	-.005	-.007	-.010
	.785	-.003	-.001	.000	-.001	-.007	-.010
	.817	.004	.005	.005	.004	-.002	-.006
	.857	-.001	-.001	-.001	-.001	-.009	-.012
	.897	-.004	-.003	-.004	-.005	-.012	-.016

TABLE [illegible].- PRESSURE COEFFICIENTS FOR CONFIGURATION 323 - Continued

(b) $M = 0.60$; $\alpha = -10^\circ$ to 10°

	x/l	C_p for - $\phi = 0^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.443	.737	.655	.601	.527	.456	.385	.292
	.453	.582	.494	.435	.372	.306	.247	.159
	.463	.349	.262	.202	.150	.107	.058	.004
Upper stage	.471	-1.240	-1.290	-1.204	-.980	-.792	-.801	-.551
	.476	-.554	-.758	-.803	-.720	-.604	-.585	-.459
	.481	-.103	-.250	-.414	-.565	-.547	-.517	-.482
	.491	.017	-.016	-.037	-.160	-.301	-.328	-.402
	.501	.069	.042	.037	.023	-.073	-.106	-.190
	.511	.126	.099	.089	.086	.047	.026	-.036
	.521	.223	.190	.174	.155	.110	.094	.061
	.531	.480	.424	.374	.298	.202	.169	.130
Transition flare	.539	-.583	-.507	-.443	-.382	-.336	-.294	-.225
	.546	.248	.187	.149	.107	.069	.048	.032
	.552	.163	.097	.059	.023	-.010	-.026	-.036
	.562	-.080	-.153	-.191	-.211	-.216	-.208	-.207
Main stage	.568	-.657	-.741	-.751	-.668	-.547	-.471	-.413
	.577	-.125	-.164	-.186	-.188	-.193	-.180	-.167
	.587	-.057	-.096	-.106	-.114	-.119	-.111	-.099
	.597	-.028	-.061	-.071	-.074	-.084	-.077	-.070
	.607	-.011	-.044	-.054	-.057	-.061	-.054	-.047
	.617	-.005	-.033	-.043	-.045	-.050	-.043	-.036
	.627	.000	-.021	-.031	-.034	-.039	-.031	-.025
	.637	.011	-.016	-.020	-.022	-.033	-.026	-.013
	.657	.021	-.006	-.015	-.018	-.022	-.013	-.008
	.677	.023	-.004	-.013	-.013	-.018	-.009	-.006
	.697	.027	-.002	-.007	-.007	-.014	-.003	-.002
	.737	.027	-.014	-.007	-.005	-.010	-.003	-.004
	.777	.033	.009	.002	-.001	-.006	.001	-.002
	.785	.042	.017	.006	.001	-.008	.003	.007
	.817	.038	.014	.005	.003	-.002	.003	.001
	.857	.032	.008	.000	.000	-.005	-.001	-.007
	.877	.033	.008	.001	.001	-.005	-.001	-.007
	.897	.029	.005	-.003	-.002	-.008	-.004	-.011

	x/l	C_p for - $\phi = -30^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.443	.699	.638	.584	.527	.467	.396	.292
	.453	.510	.445	.393	.341	.289	.233	.148
	.463	.322	.251	.202	.156	.112	.069	.004
Upper stage	.471	-1.246	-1.171	-1.039	-.861	-.616	-.507	-.472
	.476	-.600	-.724	-.734	-.680	-.541	-.465	-.448
	.481	-.217	-.433	-.540	-.605	-.553	-.505	-.488
	.491	.000	-.016	-.071	-.188	-.341	-.386	-.430
	.501	.046	.036	.043	.023	-.079	-.128	-.213
	.511	.103	.087	.089	.086	.047	.020	-.036
	.521	.200	.184	.174	.155	.116	.100	.061
	.531	.446	.407	.363	.292	.202	.186	.170
Transition flare	.539	-.748	-.707	-.666	-.623	-.581	-.540	-.485
	.546	-.320	-.244	-.191	-.148	-.119	-.094	-.065
	.552	.135	.086	.053	.023	-.010	-.026	-.059
	.562	-.120	-.170	-.203	-.211	-.216	-.226	-.259
Main stage	.568	-.583	-.633	-.631	-.565	-.490	-.505	-.551
	.577	-.143	-.170	-.186	-.188	-.187	-.180	-.185
	.587	-.080	-.101	-.111	-.114	-.124	-.117	-.116
	.597	-.040	-.056	-.060	-.057	-.067	-.060	-.059
	.607	-.034	-.050	-.054	-.057	-.061	-.060	-.059
	.617	-.028	-.038	-.043	-.045	-.050	-.043	-.042
	.627	-.017	-.033	-.037	-.034	-.044	-.037	-.036
	.637	-.011	-.021	-.026	-.028	-.033	-.026	-.030
	.657	-.005	-.018	-.021	-.020	-.024	-.021	-.024
	.677	.007	-.006	-.009	-.005	-.014	-.011	-.016
	.697	.001	-.010	-.011	-.009	-.016	-.011	-.020
	.737	.005	-.006	-.005	-.003	-.010	-.005	-.020
	.777	.015	-.014	-.005	.001	-.006	-.001	-.020
	.785	.011	.002	.004	-.005	-.004	.001	-.016
	.817	.013	.002	.002	-.003	-.002	.000	-.018
	.857	.007	-.003	-.003	.000	-.006	-.005	-.021
	.877	.006	-.005	-.005	-.002	-.008	-.006	-.021
	.897	.004	-.005	-.006	-.003	-.009	-.008	-.024
	.917	.004	-.007	-.006	-.003	-.011	-.011	-.027
	.957	-.012	-.018	-.017	-.014	-.023	-.024	-.037
	.997	-.093	-.082	-.071	-.070	-.083	-.090	-.113

TABLE [illegible].- PRESSURE COEFFICIENTS FOR CONFIGURATION 323 - Continued

(b) M = 0.60; α = -10° to 10° - Concluded

	x/l	C_p for - β = -60°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.443	.582	.583	.562	.527	.478	.424	.326
	.453	.432	.422	.402	.366	.323	.285	.198
	.463	.222	.206	.185	.161	.123	.092	.021
Upper stage	.471	-1.008	-.871	-.807	-.668	-.605	-.626	-.642
	.476	-.703	-.701	-.694	-.588	-.559	-.574	-.591
	.481	-.423	-.575	-.569	-.577	-.564	-.574	-.585
	.491	-.057	-.078	-.163	-.280	-.353	-.357	-.368
	.501	-.023	.025	.037	.012	-.067	-.071	-.127
	.511	.035	.070	.094	.098	.070	.049	-.030
	.521	.126	.150	.157	.155	.127	.112	.050
Transition flare	.531	.338	.356	.323	.263	.247	.249	.210
	.539	.276	.255	.228	.192	.142	.110	.077
	.546	.221	.196	.173	.107	.098	.070	.034
	.552	.034	-.035	.037	.017	.001	-.026	-.093
	.562	-.211	-.216	-.214	-.211	-.227	-.260	-.328
Main stage	.568	-.737	-.741	-.694	-.588	-.639	-.711	-.768
	.577	-.211	-.193	-.186	-.182	-.193	-.203	-.236
	.587	-.148	-.130	-.117	-.114	-.124	-.128	-.162
	.597	-.108	-.084	-.077	-.074	-.084	-.088	-.122
	.607	-.091	-.067	-.060	-.057	-.061	-.066	-.099
	.617	-.085	-.061	-.049	-.045	-.050	-.060	-.087
	.627	-.074	-.056	-.043	-.034	-.044	-.048	-.076
	.637	-.068	-.044	-.031	-.028	-.033	-.043	-.070
	.657	-.071	-.047	-.025	-.018	-.026	-.039	-.067
	.677	-.059	-.034	-.019	-.011	-.022	-.032	-.060
	.697	-.046	-.022	-.013	-.005	-.018	-.025	-.053
	.737	-.054	-.026	-.013	-.003	-.012	-.019	-.043
	.777	-.052	-.020	-.007	.001	-.010	-.013	-.032
	.785	-.059	-.024	-.007	.001	-.006	-.011	-.030
	.817	-.043	-.017	-.003	.004	-.004	-.010	-.023
	.857	-.047	-.021	-.007	.000	-.008	-.012	-.026
	.877	-.047	-.022	-.009	-.002	-.008	-.013	-.026
	.897	-.048	-.023	-.009	-.002	-.010	-.013	-.027
	.917	-.054	-.030	-.015	-.007	-.014	-.019	-.031
	.957	-.063	-.036	-.021	-.014	-.024	-.027	-.040
	.997	-.130	-.100	-.081	-.070	-.084	-.094	-.120

	x/l	C_p for - β = -30°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.443	.438	.506	.518	.521	.506	.490	.420
	.463	.105	.145	.158	.150	.134	.125	.076
Upper stage	.471	-.900	-.774	-.728	-.702	-.803	-.892	-.948
	.491	-.177	-.233	-.249	-.257	-.227	-.180	-.196
	.511	-.028	.047	.077	.092	.070	.037	-.047
Transition flare	.531	.280	.310	.300	.286	.299	.312	.250
	.552	-.057	-.004	.014	.017	.007	-.014	-.070
Main stage	.568	-.903	-.861	-.763	-.714	-.793	-.848	-.916
	.587	-.188	-.141	-.123	-.114	-.130	-.140	-.190
	.607	-.131	-.078	-.060	-.057	-.067	-.077	-.127
	.627	-.108	-.061	-.043	-.034	-.044	-.060	-.110
	.657	-.103	-.055	-.031	-.018	-.030	-.048	-.104
	.697	-.095	-.045	-.021	-.011	-.022	-.056	-.094
	.737	-.087	-.040	-.013	-.003	-.016	-.056	-.089
	.777	-.083	-.034	-.009	.001	-.010	-.027	-.081
	.785	-.087	-.036	-.009	.001	-.010	-.025	-.077
	.817	-.067	-.025	-.005	.005	-.005	-.019	-.064
	.857	-.070	-.030	-.009	.000	-.010	-.024	-.070
	.897	-.072	-.032	-.011	-.002	-.013	-.028	-.072

TABLE 10.- PRESSURE COEFFICIENTS FOR CONFIGURATION 323 - Continued

(c) M = 0.80; α = -10° to 10°

	x/l	C_p for - ϕ = 0°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.443	.814	.732	.673	.604	.539	.465	.366
	.453	.661	.579	.524	.462	.393	.324	.235
	.463	.452	.374	.330	.276	.222	.163	.082
Upper stage	.471	-1.180	-.979	-.733	-.575	-.490	-.451	-.396
	.476	-.779	-.707	-.559	-.423	-.344	-.328	-.315
	.481	-.514	-.611	-.544	-.427	-.364	-.355	-.350
	.491	-.037	-.311	-.440	-.411	-.390	-.397	-.400
	.501	.067	-.026	-.240	-.334	-.348	-.355	-.369
	.511	.132	.120	-.029	-.211	-.244	-.239	-.269
	.521	.243	.228	.148	-.077	-.121	-.109	-.138
	.531	.509	.431	.306	.062	-.010	-.001	-.007
Transition flare	.539	-.199	-.172	-.148	-.134	-.114	-.097	-.088
	.546	.308	.262	.248	.163	.051	.037	.042
	.552	.221	.175	.161	.118	.017	.003	.004
	.562	.001	-.049	-.083	-.092	-.121	-.139	-.146
Main stage	.568	-1.214	-1.218	-1.171	-.669	-.417	-.355	-.353
	.577	-.145	-.169	-.182	-.177	-.167	-.155	-.154
	.587	-.076	-.092	-.102	-.107	-.114	-.105	-.096
	.597	-.041	-.061	-.067	-.073	-.083	-.074	-.065
	.607	-.026	-.042	-.048	-.054	-.064	-.055	-.046
	.617	-.014	-.030	-.036	-.046	-.048	-.039	-.034
	.627	-.003	-.019	-.029	-.034	-.041	-.032	-.027
	.637	.008	-.011	-.017	-.027	-.033	-.024	-.019
	.657	.020	-.002	-.009	-.018	-.021	-.015	-.009
	.677	.021	.002	-.006	-.016	-.018	-.010	-.008
	.697	.027	.007	.000	-.012	-.013	-.006	-.006
	.737	.028	.007	.000	-.010	-.010	-.005	-.009
	.777	.035	.015	.004	-.003	-.006	-.001	-.008
	.785	.042	.020	.012	.002	.001	.000	.001
	.817	.039	.019	.010	.000	-.002	.002	-.007
	.857	.030	.014	.006	-.003	-.005	-.003	-.015
	.877	.033	.015	.007	-.003	-.004	-.003	-.015
	.897	.029	.010	.003	-.006	-.008	-.006	-.020

	x/l	C_p for - ϕ = -30°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.443	.773	.713	.666	.600	.539	.473	.373
	.453	.599	.536	.492	.438	.384	.320	.231
	.463	.426	.359	.319	.276	.229	.167	.090
Upper stage	.471	-1.043	-.842	-.688	-.491	-.399	-.371	-.373
	.476	-.772	-.692	-.563	-.373	-.325	-.332	-.353
	.481	-.568	-.657	-.548	-.396	-.348	-.362	-.388
	.491	-.114	-.338	-.444	-.396	-.375	-.393	-.423
	.501	.047	-.049	-.232	-.338	-.337	-.355	-.388
	.511	.105	.093	-.036	-.234	-.244	-.251	-.296
	.521	.220	.212	.117	-.107	-.125	-.128	-.161
	.531	.478	.412	.267	.039	-.014	-.016	-.023
Transition flare	.539	-.149	-.149	-.144	-.146	-.137	-.132	-.127
	.546	.058	.084	.112	.110	.100	.094	.084
	.552	.190	.160	.161	.106	.017	-.001	-.034
	.562	-.037	-.076	-.102	-.092	-.121	-.159	-.211
Main stage	.568	-1.064	-1.084	-1.017	-.484	-.364	-.489	-.715
	.577	-.183	-.184	-.182	-.169	-.164	-.170	-.184
	.587	-.087	-.092	-.106	-.111	-.114	-.116	-.119
	.597	-.045	-.045	-.048	-.057	-.064	-.059	-.061
	.607	-.045	-.045	-.048	-.054	-.064	-.062	-.065
	.617	-.033	-.034	-.036	-.046	-.048	-.047	-.050
	.627	-.030	-.030	-.029	-.034	-.041	-.039	-.042
	.637	-.018	-.022	-.021	-.027	-.033	-.028	-.034
	.657	-.011	-.014	-.016	-.021	-.024	-.024	-.027
	.677	.003	.000	-.002	-.010	-.013	-.012	-.017
	.697	-.002	-.005	-.005	-.012	-.014	-.013	-.020
	.737	.002	-.002	-.002	-.007	-.010	-.009	-.021
	.777	.014	.008	.005	.004	-.005	-.004	-.021
	.785	.010	.008	.008	.001	.000	-.004	-.017
	.817	.011	.008	.007	.000	-.002	-.003	-.023
	.857	.004	.002	.002	-.004	-.007	-.006	-.027
	.877	.003	.001	.002	-.005	-.007	-.007	-.027
	.897	.001	.000	.000	-.007	-.009	-.009	-.029
	.917	.003	-.001	-.001	-.007	-.011	-.011	-.032
	.957	-.013	-.012	-.011	-.020	-.023	-.025	-.045
	.997	-.094	-.078	-.069	-.081	-.088	-.095	-.123

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 323 - Continued

(c) M = 0.80; α = -10° to 10° - Concluded

	x/l	C_p for - ϕ = -60°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.443	.657	.657	.640	.600	.561	.503	.407
	.453	.516	.504	.490	.455	.416	.361	.276
	.463	.322	.314	.300	.276	.240	.193	.112
Upper stage	.471	-.807	-.716	-.600	-.415	-.421	-.466	-.495
	.476	-.660	-.599	-.502	-.357	-.383	-.432	-.469
	.481	-.614	-.584	-.502	-.377	-.387	-.439	-.473
	.491	-.345	-.445	-.448	-.380	-.402	-.443	-.473
	.501	-.049	-.176	-.286	-.334	-.352	-.370	-.400
	.511	.032	.043	-.094	-.236	-.244	-.228	-.234
	.521	.132	.170	.071	-.119	-.121	-.062	-.084
	.531	.355	.347	.210	.004	.013	.076	.073
Transition flare	.539	.334	.319	.297	.148	.081	.060	.023
	.546	.280	.265	.263	.171	.093	.062	.023
	.552	.084	.114	.131	.084	.070	.037	-.050
	.562	-.126	-.111	-.113	-.092	-.125	-.182	-.246
Main stage	.568	-1.252	-1.238	-1.094	-.473	-.648	-1.085	-1.280
	.577	-.222	-.184	-.182	-.165	-.175	-.189	-.250
	.587	-.156	-.122	-.113	-.111	-.117	-.124	-.157
	.597	-.126	-.084	-.075	-.073	-.079	-.085	-.127
	.607	-.107	-.069	-.056	-.054	-.064	-.066	-.107
	.617	-.099	-.057	-.044	-.046	-.048	-.059	-.096
	.627	-.091	-.049	-.036	-.038	-.041	-.047	-.088
	.637	-.080	-.042	-.029	-.031	-.033	-.043	-.080
	.657	-.074	-.036	-.020	-.023	-.024	-.035	-.071
	.677	-.061	-.027	-.013	-.016	-.020	-.030	-.063
	.697	-.048	-.018	-.006	-.010	-.016	-.024	-.056
	.737	-.060	-.020	-.006	-.007	-.010	-.019	-.046
	.777	-.052	-.017	-.002	-.003	-.006	-.013	-.035
	.785	-.059	-.020	-.002	-.003	-.005	-.010	-.032
	.817	-.045	-.011	.003	.000	-.003	-.009	-.028
	.857	-.050	-.018	-.001	-.004	-.007	-.011	-.030
	.877	-.050	-.017	-.002	-.005	-.008	-.012	-.029
	.897	-.054	-.017	-.003	-.006	-.009	-.014	-.032
	.917	-.059	-.025	-.010	-.011	-.014	-.018	-.036
	.957	-.064	-.032	-.016	-.020	-.023	-.028	-.047
	.997	-.136	-.099	-.080	-.081	-.088	-.100	-.128

	x/l	C_p for - ϕ = -90°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.443	.516	.579	.602	.600	.587	.562	.493
	.463	.210	.254	.270	.276	.259	.234	.187
Upper stage	.471	-.654	-.625	-.554	-.460	-.524	-.618	-.655
	.491	-.487	-.465	-.425	-.377	-.429	-.470	-.488
	.511	-.087	-.095	-.163	-.238	-.202	-.116	-.130
Transition flare	.531	.255	.255	.141	.008	.121	.222	.216
	.552	-.010	.076	.112	.087	.104	.060	-.030
Main stage	.568	-1.310	-1.249	-.963	-.546	-.987	-1.247	-1.315
	.587	-.187	-.130	-.117	-.111	-.121	-.135	-.198
	.607	-.133	-.080	-.056	-.054	-.064	-.078	-.142
	.627	-.122	-.057	-.036	-.038	-.041	-.059	-.123
	.657	-.110	-.049	-.024	-.023	-.028	-.050	-.113
	.697	-.100	-.039	-.014	-.013	-.024	-.039	-.101
	.737	-.089	-.033	-.007	-.007	-.011	-.031	-.090
	.777	-.083	-.029	-.003	-.003	-.007	-.027	-.085
	.785	-.089	-.031	-.005	-.009	-.007	-.026	-.080
	.817	-.070	-.018	.002	.001	-.003	-.019	-.071
	.857	-.075	-.023	-.003	-.003	-.008	-.024	-.074
	.897	-.075	-.028	-.006	-.006	-.011	-.027	-.076

TABLE 10.- PRESSURE COEFFICIENTS FOR CONFIGURATION 323 - Continued

(d) M = 1.00; α = -10° to 10°

	x/l	C_p for - ϕ = 0°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.443	.941	.865	.813	.743	.676	.608	.517
	.453	.811	.732	.671	.612	.546	.483	.399
	.463	.636	.563	.508	.455	.400	.350	.271
	.471	-.832	-.852	-.866	-.868	-.645	-.522	-.493
Upper stage	.476	-.833	-.912	-.954	-.955	-.455	-.367	-.365
	.481	-.604	-.731	-.804	-.848	-.471	-.395	-.393
	.491	-.326	-.487	-.584	-.494	-.459	-.434	-.439
	.501	-.136	-.270	-.388	-.191	-.394	-.416	-.439
	.511	.044	.009	.044	-.059	-.293	-.349	-.393
	.521	.295	.259	.236	.032	-.189	-.257	-.301
	.531	.582	.476	.392	.136	-.101	-.144	-.157
Transition flare	.539	.040	.045	.052	.056	.072	.084	.092
	.546	.456	.415	.407	.300	-.015	-.058	.011
	.552	.393	.346	.329	.261	-.018	-.046	.023
	.562	.245	.204	.172	.086	-.104	-.119	-.063
Main stage	.568	-.662	-.682	-.700	-.695	-.425	-.297	-.307
	.577	-.424	-.499	-.538	-.500	-.260	-.236	-.228
	.587	-.320	-.413	-.458	-.399	-.248	-.242	-.240
	.597	-.234	-.316	-.357	-.283	-.232	-.229	-.213
	.607	-.188	-.254	-.278	-.243	-.211	-.199	-.170
	.617	-.170	-.221	-.226	-.194	-.186	-.171	-.139
	.627	-.161	-.199	-.162	-.154	-.162	-.147	-.112
	.637	-.142	-.144	-.107	-.124	-.137	-.122	-.093
	.657	-.131	-.086	-.085	-.099	-.111	-.097	-.076
	.677	-.057	-.075	-.077	-.085	-.090	-.080	-.064
	.697	-.045	-.064	-.063	-.070	-.074	-.065	-.047
	.737	-.030	-.058	-.046	-.062	-.052	-.046	-.025
	.777	.014	-.022	.018	-.042	-.001	-.004	-.005
	.785	.031	.009	.026	-.027	.013	.010	.013
	.817	.027	.027	.035	.026	.024	.019	.020
	.857	.055	.032	.031	.026	.024	.020	.015
	.877	.061	.039	.032	.028	.023	.021	.014
	.897	.055	.035	.025	.025	.018	.017	.007

	x/l	C_p for - ϕ = -30°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.443	.906	.844	.795	.737	.679	.620	.523
	.453	.754	.696	.647	.595	.541	.485	.400
	.463	.603	.548	.499	.452	.403	.350	.277
	.471	-.932	-.943	-.963	-.950	-.576	-.500	-.493
Upper stage	.476	-.855	-.921	-.960	-.983	-.431	-.379	-.390
	.481	-.677	-.796	-.862	-.906	-.443	-.407	-.414
	.491	-.311	-.471	-.584	-.582	-.440	-.440	-.457
	.501	-.155	-.264	-.321	-.203	-.382	-.425	-.454
	.511	.008	-.010	.031	-.047	-.290	-.367	-.411
	.521	.258	.232	.202	.045	-.196	-.288	-.329
	.531	.546	.452	.352	.146	-.101	-.196	-.231
Transition flare	.539	.230	.255	.290	.321	.398	.443	.492
	.546	.302	.282	.262	.237	.211	.247	.291
	.552	.357	.334	.323	.282	-.024	-.061	-.060
	.562	.206	.180	.154	.065	-.113	-.135	-.127
Main stage	.568	-.653	-.470	-.669	-.662	-.385	-.551	-.775
	.577	-.497	-.551	-.574	-.518	-.257	-.297	-.430
	.587	-.332	-.405	-.446	-.338	-.251	-.281	-.307
	.597	-.203	-.257	-.281	-.237	-.177	-.184	-.179
	.607	-.222	-.273	-.284	-.234	-.211	-.208	-.182
	.617	-.210	-.233	-.214	-.188	-.186	-.177	-.151
	.627	-.197	-.202	-.162	-.157	-.165	-.153	-.133
	.637	-.182	-.147	-.116	-.136	-.141	-.132	-.118
	.657	-.138	-.099	-.092	-.102	-.113	-.108	-.105
	.677	-.076	-.077	-.073	-.078	-.086	-.083	-.089
	.697	-.076	-.076	-.067	-.073	-.075	-.074	-.083
	.737	-.056	-.065	-.047	-.060	-.051	-.053	-.065
	.777	-.001	-.021	.015	-.038	-.002	-.008	-.048
	.785	.000	.001	.023	-.027	.016	.000	-.035
	.817	.000	.017	.031	.025	.024	.012	-.017
	.857	.029	.021	.028	.025	.022	.014	-.011
	.877	.031	.025	.027	.027	.020	.012	-.010
	.897	.030	.024	.022	.025	.016	.011	-.010
	.917	.030	.022	.022	.025	.014	.008	-.010
	.957	.018	.011	.012	.011	-.003	-.007	-.021
	.997	-.041	-.058	-.073	-.099	-.121	-.136	-.149

TABLE 10.- PRESSURE COEFFICIENTS FOR CONFIGURATION 323 - Continued

(d) M = 1.003; α = -10° to 10° - Concluded

	x/l	C_p for - ϕ = -60°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.443	.793	.791	.768	.737	.697	.643	.553
	.453	.665	.658	.638	.607	.563	.516	.437
	.463	.511	.497	.481	.455	.418	.374	.307
Upper stage	.471	-.784	-.783	-.782	-.789	-.542	-.525	-.523
	.476	-.907	-.964	-.984	-.961	-.452	-.456	-.463
	.481	-.601	-.771	-.856	-.891	-.465	-.468	-.475
	.491	-.357	-.438	-.565	-.539	-.459	-.474	-.497
	.501	-.271	-.291	-.263	-.179	-.400	-.440	-.472
	.511	-.106	-.095	-.042	-.038	-.315	-.370	-.399
	.521	.136	.128	.129	.054	-.226	-.272	-.271
	.531	.384	.336	.279	.143	-.119	-.159	-.161
Transition flare	.539	.471	.466	.467	.188	-.015	-.101	-.157
	.546	.422	.417	.426	.276	.014	-.055	-.104
	.552	.236	.276	.302	.164	.057	.081	.026
	.562	.107	.132	.133	.092	-.046	.003	-.063
Main stage	.568	-.720	-.713	-.706	-.671	-.630	-.734	-.787
	.577	-.586	-.591	-.590	-.530	-.318	-.581	-.720
	.587	-.448	-.465	-.474	-.405	-.284	-.379	-.622
	.597	-.359	-.364	-.360	-.304	-.248	-.275	-.372
	.607	-.326	-.316	-.269	-.231	-.211	-.211	-.231
	.617	-.307	-.245	-.192	-.188	-.186	-.177	-.191
	.627	-.301	-.187	-.159	-.157	-.162	-.159	-.176
	.637	-.243	-.150	-.125	-.133	-.141	-.147	-.167
	.657	-.180	-.123	-.098	-.101	-.110	-.126	-.156
	.677	-.150	-.105	-.082	-.086	-.093	-.109	-.133
	.697	-.120	-.087	-.067	-.070	-.076	-.092	-.109
	.737	-.109	-.083	-.049	-.059	-.055	-.071	-.068
	.777	-.069	-.034	.007	-.040	-.005	-.021	-.045
	.785	-.072	-.021	.014	-.030	.014	-.011	-.036
	.817	-.049	-.002	.028	.026	.025	.006	-.008
	.857	-.024	.004	.023	.026	.022	.010	-.003
	.877	-.021	.007	.022	.027	.020	.010	-.004
	.897	-.024	.004	.019	.027	.016	.009	-.005
	.917	-.033	-.002	.014	.021	.011	.004	-.009
	.957	-.036	-.007	.008	.012	-.002	-.009	-.020
	.997	-.107	-.089	-.085	-.100	-.118	-.132	-.153

	x/l	C_p for - ϕ = -90°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.443	.660	.717	.736	.737	.729	.706	.639
	.463	.399	.441	.451	.452	.442	.424	.375
Upper stage	.471	-.847	-.867	-.866	-.862	-.715	-.728	-.759
	.491	-.497	-.478	-.464	-.484	-.483	-.499	-.506
	.511	-.265	-.212	-.113	-.059	-.318	-.343	-.310
Transition flare	.531	.173	.140	.163	.139	-.027	.003	.108
	.552	.122	.225	.268	.258	.193	.208	.080
Main stage	.568	-.775	-.744	-.727	-.711	-.700	-.743	-.784
	.587	-.546	-.514	-.461	-.396	-.364	-.514	-.567
	.607	-.424	-.267	-.229	-.243	-.220	-.254	-.430
	.627	-.237	-.172	-.156	-.157	-.156	-.162	-.228
	.657	-.208	-.138	-.104	-.101	-.110	-.138	-.206
	.697	-.167	-.109	-.074	-.072	-.080	-.108	-.166
	.737	-.129	-.091	-.049	-.058	-.061	-.089	-.128
	.777	-.097	-.033	.004	-.042	-.013	-.047	-.100
	.785	-.107	-.029	.009	-.031	.010	-.024	-.084
	.817	-.059	-.010	.026	.027	.027	-.001	-.042
	.857	-.046	-.004	.022	.027	.021	-.002	-.044
	.897	-.050	-.006	.016	.026	.019	-.005	-.047

TABLE 10.- PRESSURE COEFFICIENTS FOR CONFIGURATION 323 - Continued

(e) M = 1.20; α = -10° to 10°

	x/l	C_p for - ϕ = 0°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.443	1.070	.589	.927	.869	.808	.739	.647
	.453	.948	.870	.813	.758	.698	.634	.547
	.463	.803	.727	.679	.626	.579	.528	.452
Upper stage	.471	-.473	-.497	-.503	-.517	-.527	-.536	-.544
	.476	-.502	-.567	-.600	-.631	-.654	-.672	-.644
	.481	-.333	-.436	-.497	-.549	-.592	-.628	-.432
	.491	-.151	-.270	-.342	-.410	-.470	-.467	-.345
	.501	-.070	-.169	-.231	-.293	-.350	-.138	-.282
	.511	-.037	-.115	-.165	-.209	.028	-.078	-.195
	.521	-.031	-.050	.074	.172	.115	-.005	-.103
	.531	.505	.410	.349	.275	.178	.101	.044
Transition flare	.539	.826	.720	.630	.555	.481	.418	.368
	.546	.561	.519	.491	.424	.266	.191	.178
	.552	.516	.468	.445	.408	.285	.209	.202
	.562	.419	.369	.341	.301	.194	.134	.140
Main stage	.568	-.342	-.354	-.367	-.383	-.393	-.234	-.296
	.577	-.192	-.243	-.269	-.285	-.219	-.168	-.168
	.587	-.140	-.205	-.236	-.253	-.222	-.204	-.195
	.597	-.091	-.148	-.182	-.204	-.206	-.201	-.198
	.607	-.061	-.115	-.143	-.163	-.178	-.176	-.171
	.617	-.050	-.099	-.119	-.136	-.149	-.144	-.133
	.627	-.037	-.085	-.100	-.111	-.119	-.111	-.095
	.637	-.023	-.066	-.078	-.081	-.086	-.084	-.062
	.657	-.030	-.064	-.071	-.063	-.054	-.046	-.033
	.677	-.031	-.038	-.044	-.041	-.040	-.025	-.022
	.697	-.023	-.037	-.038	-.031	-.019	-.014	-.020
	.737	-.016	-.026	-.025	-.034	-.029	-.027	-.010
	.777	.019	-.014	-.028	-.021	-.028	-.028	-.017
	.785	.029	-.005	-.017	-.013	-.017	-.011	-.005
	.817	.023	-.002	-.002	-.021	-.018	-.012	-.007
	.857	.020	.007	-.008	-.003	.000	-.008	-.017
	.877	.032	-.004	-.003	.000	-.004	-.007	-.015
	.897	.013	-.003	.000	-.005	-.009	-.017	-.023

	x/l	C_p for - ϕ = -30°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.443	1.030	.973	.921	.866	.811	.750	.653
	.453	.900	.842	.796	.746	.695	.639	.552
	.463	.769	.712	.671	.626	.579	.528	.452
Upper stage	.471	-.589	-.618	-.625	-.630	-.635	-.644	-.652
	.476	-.524	-.575	-.606	-.628	-.649	-.672	-.693
	.481	-.393	-.485	-.535	-.576	-.611	-.636	-.612
	.491	-.162	-.270	-.339	-.399	-.450	-.495	-.345
	.501	-.097	-.180	-.236	-.291	-.339	-.141	-.263
	.511	-.075	-.137	-.176	-.212	.020	-.073	-.176
	.521	-.048	-.039	.091	.175	.105	-.016	-.089
	.531	.475	.399	.344	.275	.170	.077	.014
Transition flare	.539	1.140	1.079	1.021	.962	.890	.826	.767
	.546	.992	.921	.860	.801	.722	.641	.582
	.552	.481	.455	.437	.402	.306	.260	.194
	.562	.384	.356	.327	.293	.218	.193	.135
Main stage	.568	-.344	-.352	-.353	-.364	-.374	-.402	-.446
	.577	-.252	-.286	-.296	-.296	-.244	-.342	-.4[illegible]
	.587	-.151	-.202	-.225	-.233	-.217	-.223	-.288
	.597	-.078	-.112	-.130	-.141	-.140	-.138	-.146
	.607	-.091	-.131	-.152	-.165	-.176	-.171	-.171
	.617	-.080	-.110	-.122	-.136	-.146	-.144	-.135
	.627	-.072	-.099	-.105	-.114	-.121	-.117	-.108
	.637	-.061	-.085	-.086	-.087	-.089	-.089	-.081
	.657	-.056	-.062	-.064	-.054	-.048	-.051	-.062
	.677	-.053	-.037	-.040	-.034	-.035	-.032	-.058
	.697	-.055	-.048	-.039	-.037	-.032	-.027	-.058
	.737	-.044	-.037	-.029	-.032	-.027	-.035	-.059
	.777	-.005	-.020	-.024	-.015	-.024	-.030	-.071
	.785	.001	-.015	-.015	-.008	-.012	-.020	-.063
	.817	-.002	-.014	-.007	-.019	-.017	-.023	-.072
	.857	-.008	.000	-.007	-.011	-.008	-.022	-.069
	.877	.003	-.014	-.007	-.002	-.005	-.019	-.063
	.897	-.011	-.011	-.004	-.002	-.005	-.021	-.056
	.917	-.010	-.005	-.004	-.006	-.007	-.019	-.045
	.957	-.013	-.017	-.012	-.017	-.016	-.020	-.038
	.997	.000	-.022	-.033	-.053	-.071	-.090	-.086

TABLE 10.- PRESSURE COEFFICIENTS FOR CONFIGURATION 323 - Concluded

(e) M = 1.20; α = -10° to 10° - Concluded

	x/ℓ	C_p for - ϕ = -60°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.443	.919	.915	.900	.869	.829	.779	.684
	.453	.809	.801	.779	.750	.719	.671	.581
	.463	.677	.669	.655	.626	.595	.555	.478
Upper stage	.471	-.476	-.475	-.482	-.493	-.500	-.512	-.533
	.476	-.578	-.607	-.625	-.642	-.652	-.663	-.682
	.481	-.448	-.504	-.535	-.568	-.595	-.614	-.636
	.491	-.268	-.333	-.372	-.405	-.434	-.462	-.451
	.501	-.187	-.232	-.266	-.299	-.328	-.326	-.228
	.511	-.157	-.175	-.192	-.206	-.105	-.070	-.152
	.521	-.118	-.009	.110	.177	.126	.041	-.029
Transition flare	.531	.358	.348	.319	.259	.202	.156	.110
	.539	.572	.540	.486	.392	.288	.193	.132
	.546	.535	.516	.491	.434	.331	.242	.170
	.552	.379	.404	.419	.397	.365	.319	.210
	.562	.293	.310	.309	.287	.266	.226	.137
Main stage	.568	-.393	-.379	-.372	-.372	-.385	-.413	-.459
	.577	-.325	-.319	-.312	-.293	-.336	-.375	-.446
	.587	-.241	-.248	-.247	-.236	-.274	-.326	-.389
	.597	-.192	-.191	-.192	-.190	-.195	-.266	-.345
	.607	-.173	-.164	-.157	-.160	-.159	-.176	-.288
	.617	-.165	-.148	-.135	-.136	-.135	-.144	-.190
	.627	-.165	-.134	-.116	-.114	-.119	-.125	-.154
	.637	-.143	-.112	-.089	-.089	-.089	-.100	-.133
	.657	-.155	-.068	-.057	-.046	.050	-.076	-.116
	.677	-.130	-.067	-.049	-.042	-.048	-.065	-.106
	.697	-.105	-.067	-.040	-.038	-.045	-.054	-.096
	.737	-.106	-.057	-.033	-.032	-.034	-.057	-.075
	.777	-.073	-.046	-.029	-.016	-.028	-.042	-.063
	.785	-.060	-.043	-.023	-.008	-.020	-.033	-.060
	.817	-.057	-.024	-.011	-.017	-.018	-.034	-.054
	.857	-.065	-.019	-.014	-.014	-.022	-.033	-.053
	.877	-.054	-.033	-.007	-.004	-.007	-.023	-.048
	.897	-.065	-.029	-.010	-.001	-.003	-.019	-.038
	.917	-.070	-.033	-.017	-.008	-.010	-.022	-.035
	.957	-.069	-.038	-.015	-.015	-.019	-.021	-.038
	.997	-.061	-.048	-.042	-.053	-.065	-.090	-.109

	x/ℓ	C_p for - ϕ = -90°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.443	.785	.844	.866	.866	.858	.837	.771
	.463	.566	.609	.623	.623	.618	.597	.544
Upper stage	.471	-.533	-.521	-.525	-.526	-.530	-.525	-.533
	.491	-.371	-.392	-.402	-.410	-.407	-.405	-.399
	.511	-.216	-.224	-.214	-.212	-.217	-.223	-.231
Transition flare	.531	.252	.277	.276	.264	.270	.264	.221
	.552	.285	.361	.402	.402	.392	.349	.261
Main stage	.568	-.445	-.412	-.394	-.389	-.396	-.413	-.451
	.587	-.328	-.289	-.258	-.236	-.266	-.293	-.348
	.607	-.257	-.199	-.176	-.165	-.176	-.212	-.269
	.627	-.246	-.134	-.114	-.114	-.110	-.138	-.252
	.657	-.161	-.082	-.054	-.047	-.056	-.090	-.161
	.697	-.156	-.089	-.050	-.038	-.056	-.083	-.158
	.737	-.127	-.069	-.039	-.035	-.036	-.070	-.139
	.777	-.089	-.052	-.029	-.019	-.027	-.056	-.115
	.785	-.100	-.057	-.029	-.013	-.025	-.055	-.118
	.817	-.082	-.030	-.011	-.012	-.018	-.043	-.096
	.857	-.085	-.032	-.017	-.010	-.030	-.052	-.095
	.897	-.088	-.040	-.017	-.006	-.007	-.027	-.082

TABLE 11.- PRESSURE COEFFICIENTS FOR CONFIGURATION 124

(a) M = 0.40 to 0.95; $\alpha = 0^\circ$

	x/l	C_p for - $\phi = 0^\circ$					
		α = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.428	.223	.256	.263	.279	.301	.329
	.438	.190	.220	.230	.247	.271	.301
	.448	.157	.179	.185	.205	.232	.266
	.468	.057	.080	.087	.113	.152	.194
	.478	-.032	-.028	-.016	.029	.079	.134
	.483	-.167	-.166	-.142	-.057	.003	.071
	.489	-.788	-1.144	-1.243	-.989	-.843	-.711
Upper stage	.494	-.203	-.250	-.320	-.449	-.413	-.348
	.499	-.089	-.112	-.134	-.308	-.308	-.234
	.509	.003	.004	.014	-.032	-.109	-.131
	.519	.060	.083	.102	.132	.103	.022
	.529	.139	.180	.200	.237	.246	.165
	.539	.276	.333	.343	.364	.355	.282
	.549	.447	.482	.491	.513	.475	.385
Transition flare	.554	.014	.027	.026	.022	.034	.031
	.558	.204	.314	.334	.391	.420	.421
Main stage	.568	-1.182	-.913	-.912	-1.477	-1.295	-1.117
	.577	-.271	-.691	-.743	-1.143	-.977	-.773
	.587	-.146	-.250	-.324	-.300	-.755	-.575
	.597	-.100	-.112	-.138	-.057	-.229	-.448
	.607	-.077	-.070	-.075	-.035	-.024	-.390
	.617	-.054	-.051	-.054	-.039	.016	-.341
	.627	-.043	-.042	-.041	-.039	.016	-.286
	.637	-.043	-.028	-.033	-.035	.012	-.202
	.657	-.021	-.020	-.022	-.031	-.003	.005
	.677	-.021	-.016	-.019	-.028	-.010	.031
	.697	-.013	-.013	-.013	-.026	-.012	.029
	.737	-.009	-.010	-.013	-.025	-.016	.011
	.777	-.005	-.006	-.007	-.017	-.010	.004
	.785	-.001	.000	-.001	-.012	-.004	.010
	.817	.000	-.001	-.004	-.014	-.006	-.003
	.857	-.001	-.005	-.008	-.017	-.011	-.011
	.877	-.001	-.004	-.006	-.017	-.011	-.011
	.897	-.004	-.007	-.010	-.020	-.014	-.015

	x/l	C_p for - $\phi = -30^\circ$					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.428	.223	.251	.255	.275	.301	.329
	.438	.190	.215	.222	.240	.265	.295
	.448	.157	.175	.181	.205	.232	.263
	.468	.057	.076	.083	.110	.145	.188
	.478	-.043	-.028	-.020	.029	.076	.134
	.483	-.167	-.170	-.146	-.064	-.004	.065
	.489	-.698	-.983	-1.046	-.906	-.772	-.641
Upper stage	.494	-.214	-.283	-.354	-.478	-.413	-.319
	.499	-.089	-.116	-.151	-.333	-.338	-.270
	.509	.003	.004	.018	-.046	-.120	-.140
	.519	.060	.088	.107	.136	.096	.016
	.529	.139	.180	.200	.237	.239	.155
	.539	.276	.333	.343	.361	.345	.272
	.549	.447	.482	.487	.502	.468	.382
Transition flare	.554	.395	.479	.483	.466	.447	.389
	.558	.238	.360	.371	.412	.431	.408
Main stage	.568	-1.182	-.932	-.966	-1.495	-1.305	-1.123
	.577	-.271	-.667	-.696	-1.114	-.974	-.734
	.587	-.146	-.292	-.345	-.304	-.741	-.565
	.597	-.077	-.098	-.117	-.042	-.171	-.364
	.607	-.077	-.065	-.075	-.035	-.021	-.400
	.617	-.054	-.047	-.050	-.039	.016	-.345
	.627	-.043	-.042	-.041	-.039	.012	-.289
	.637	-.043	-.028	-.033	-.035	.009	-.195
	.657	-.025	-.023	-.024	-.034	-.005	.003
	.677	-.013	-.010	-.015	-.023	-.003	.035
	.697	-.013	-.013	-.015	-.026	-.012	.029
	.737	-.009	-.010	-.012	-.022	-.012	.014
	.777	-.005	-.005	-.004	-.015	-.006	.007
	.785	-.001	.000	-.003	-.012	-.004	.010
	.817	.000	-.002	-.004	-.014	-.006	-.004
	.857	-.003	-.006	-.008	-.018	-.012	-.012
	.877	-.004	-.007	-.009	-.018	-.013	-.014
	.897	-.006	-.009	-.011	-.021	-.015	-.016
	.917	-.006	-.010	-.012	-.021	-.015	-.017
	.957	-.016	-.021	-.023	-.034	-.026	-.029
	.997	-.072	-.080	-.083	-.093	-.092	-.110

TABLE 11.- PRESSURE COEFFICIENTS FOR CONFIGURATION 12+ - Continued

(a) M = 0.40 to 0.95; $\alpha = 0^{\circ}$ - Concluded

	x/l	C_p for - $\phi = -60^{\circ}$					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.428	.223	.247	.255	.275	.298	.329
	.438	.190	.211	.218	.240	.265	.295
	.448	.157	.175	.177	.201	.232	.263
	.468	.057	.071	.079	.110	.145	.188
	.478	-.043	-.033	-.020	.029	.073	.131
	.483	-.077	-.088	-.091	-.096	-.092	-.110
	.489	-.743	-1.047	-1.184	-1.003	-.860	-.724
Upper stage	.494	-.203	-.283	-.354	-.456	-.362	-.285
	.499	-.089	-.112	-.151	-.377	-.335	-.266
	.509	.003	.004	.018	-.046	-.154	-.160
	.519	.060	.088	.102	.143	.096	.006
	.529	.139	.190	.204	.245	.250	.158
	.539	.276	.333	.343	.361	.352	.272
	.549	.447	.477	.487	.492	.451	.363
Transition flare	.554	.406	.488	.492	.491	.491	.440
	.558	-.635	-.093	.030	.180	.249	.315
	.562	.025	.155	.188	.273	.309	.347
Main stage	.568	-1.023	-.848	-.886	-1.499	-1.309	-1.126
	.577	-.339	-.686	-.713	-1.103	-.909	-.672
	.587	-.134	-.343	-.383	-.268	-.752	-.581
	.597	-.077	-.135	-.164	-.061	-.243	-.500
	.607	-.066	-.065	-.079	-.039	-.024	-.416
	.617	-.054	-.042	-.050	-.042	.016	-.345
	.627	-.043	-.037	-.041	-.042	.012	-.283
	.637	-.043	-.028	-.033	-.039	.009	-.189
	.657	-.025	-.020	-.022	-.032	-.004	.007
	.677	-.017	-.015	-.018	-.028	-.008	.020
	.697	-.009	-.011	-.013	-.025	-.011	.032
	.737	-.009	-.008	-.010	-.021	-.012	.017
	.777	-.005	-.008	-.007	-.017	-.009	.007
	.785	-.005	-.005	-.007	-.015	-.008	.006
	.817	.000	-.001	-.003	-.014	-.006	-.002
	.857	-.003	-.006	-.008	-.018	-.011	-.012
	.877	-.004	-.007	-.009	-.019	-.012	-.013
	.897	-.004	-.007	-.009	-.020	-.013	-.015
	.917	-.009	-.012	-.015	-.025	-.019	-.020
	.957	-.016	-.021	-.023	-.034	-.026	-.029
	.997	-.072	-.082	-.084	-.094	-.092	-.111

	x/l	C_p for - $\phi = -$					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.418	.267	.287	.300	.314	.338	.367
	.448	.157	.170	.173	.194	.222	.257
	.468	.057	.076	.083	.113	.145	.191
	.483	-.178	-.189	-.171	-.085	-.027	.046
Upper stage	.489	-.653	-.956	-1.012	-.802	-.677	-.557
	.509	.003	.004	.018	.001	-.092	-.124
	.529	.139	.190	.200	.237	.260	.187
Transition flare	.549	.447	.495	.504	.528	.499	.421
	.558	.238	.346	.359	.401	.437	.443
Main stage	.568	-1.011	-.830	-.869	-1.517	-1.329	-1.149
	.587	-.134	-.371	-.392	-.322	-.786	-.620
	.607	-.066	-.065	-.079	-.042	-.014	-.416
	.627	-.043	-.033	-.037	-.042	.019	-.273
	.657	-.025	-.021	-.022	-.032	-.004	.013
	.697	-.013	-.015	-.016	-.027	-.014	.032
	.737	-.009	-.010	-.010	-.021	-.012	.017
	.777	-.005	-.005	-.007	-.017	-.009	.006
	.785	-.005	-.006	-.007	-.018	-.009	.005
	.817	.002	.000	-.003	-.012	-.005	-.001
	.857	-.001	-.005	-.008	-.017	-.011	-.011
	.897	-.006	-.008	-.010	-.021	-.015	-.015

TABLE 11.- PRESSURE COEFFICIENTS FOR CONFIGURATION 124 - Continued

(b) M = 0.60; α = -10° to 10°

	x/l	C_p for - $\phi = 0°$						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.428	.414	.338	.286	.242	.188	.145	.092
	.438	.380	.310	.247	.208	.154	.117	.064
	.448	.341	.265	.243	.169	.121	.078	.025
	.468	.240	.164	.112	.073	.020	-.018	-.067
	.478	.133	.063	.005	-.034	-.083	-.116	-.158
	.483	-.002	-.074	-.138	-.172	-.215	-.242	-.285
	.489	-.765	-.837	-.924	-.935	-.968	-.971	-.967
Upper stage	.494	-.123	-.173	-.214	-.202	-.240	-.250	-.247
	.499	-.030	-.063	-.093	-.098	-.107	-.111	-.102
	.509	.057	.030	.006	.012	.003	-.001	.008
	.519	.120	.099	.076	.081	.078	.081	.089
	.529	.201	.186	.162	.168	.165	.162	.165
	.539	.364	.337	.319	.313	.299	.283	.263
	.549	.642	.574	.527	.469	.415	.364	.338
Transition flare	.554	.027	.029	.017	.029	.026	.028	.031
	.558	.403	.349	.302	.268	.225	.176	.156
Main stage	.568	-.963	-.972	-.990	-.978	-.930	-.898	-.866
	.577	-.256	-.410	-.486	-.486	-.507	-.504	-.519
	.587	-.065	-.098	-.139	-.156	-.200	-.238	-.252
	.597	-.042	-.063	-.087	-.092	-.119	-.140	-.148
	.607	-.025	-.051	-.069	-.063	-.072	-.087	-.084
	.617	-.019	-.034	-.058	-.046	-.055	-.059	-.055
	.627	-.007	-.028	-.046	-.040	-.043	-.047	-.038
	.637	-.002	-.017	-.035	-.029	-.032	-.035	-.027
	.657	.018	-.003	-.026	-.018	-.021	-.020	-.013
	.677	.022	.001	-.021	-.014	-.017	-.018	-.011
	.697	.026	-.005	-.015	-.008	-.013	-.012	-.009
	.737	.026	.008	-.015	-.006	-.009	-.012	-.009
	.777	.032	.012	-.019	-.001	-.004	-.008	-.009
	.785	.040	.018	-.003	-.010	-.004	-.006	-.003
	.817	.037	.016	-.004	.004	-.002	-.007	-.008
	.857	.032	.013	-.008	.000	-.005	-.011	-.015
	.877	.032	.013	-.007	.001	-.005	-.011	-.015
	.897	.029	.010	-.011	-.002	-.008	-.013	-.021

	x/l	C_p for - $\phi = -30°$						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.428	.380	.327	.269	.242	.188	.145	.075
	.438	.335	.287	.236	.202	.154	.106	.041
	.448	.307	.254	.196	.169	.121	.072	.019
	.468	.206	.152	.101	.062	.025	-.018	-.078
	.478	.105	.046	-.006	-.040	-.078	-.116	-.170
	.483	-.036	-.091	-.149	-.178	-.215	-.242	-.290
	.489	-.667	-.723	-.798	-.803	-.842	-.879	-.944
Upper stage	.494	-.169	-.208	-.243	-.237	-.264	-.273	-.270
	.499	-.042	-.069	-.098	-.098	-.107	-.116	-.113
	.509	.033	.024	.000	.012	.003	-.006	-.003
	.519	.103	.094	.076	.087	.078	.075	.072
	.529	.184	.175	.162	.168	.165	.162	.153
	.539	.340	.331	.319	.313	.299	.283	.263
	.549	.613	.569	.516	.469	.420	.393	.350
Transition flare	.554	.552	.531	.485	.451	.402	.359	.287
	.558	.421	.389	.342	.314	.265	.239	.185
Main stage	.568	-1.438	-1.320	-1.170	-.967	-.820	-.696	-.611
	.577	-.239	-.324	-.434	-.521	-.623	-.649	-.611
	.587	-.106	-.121	-.156	-.173	-.252	-.365	-.426
	.597	-.054	-.063	-.075	-.069	-.084	-.116	-.165
	.607	-.048	-.057	-.069	-.058	-.067	-.076	-.090
	.617	-.036	-.046	-.058	-.046	-.049	-.053	-.055
	.627	-.030	-.034	-.052	-.040	-.043	-.041	-.038
	.637	-.025	-.028	-.040	-.029	-.032	-.035	-.032
	.657	-.011	-.015	-.032	-.020	-.021	-.027	-.028
	.677	-.016	-.001	-.017	-.008	-.013	-.018	-.022
	.697	-.003	-.003	-.021	-.010	-.013	-.018	-.024
	.737	-.005	.001	-.017	-.003	-.009	-.016	-.024
	.777	.014	.010	-.015	.001	-.002	-.010	-.022
	.785	.009	-.003	-.011	.001	-.004	-.008	-.020
	.817	.010	.007	-.007	.003	-.002	-.010	-.021
	.857	.005	.003	-.012	-.001	-.006	-.014	-.026
	.877	.004	.003	-.013	-.001	-.006	-.015	-.027
	.897	.002	.000	-.014	-.002	-.009	-.017	-.030
	.917	.002	-.001	-.015	-.004	-.010	-.019	-.033
	.957	-.015	-.014	-.025	-.015	-.022	-.032	-.045
	.997	-.100	-.083	-.084	-.072	-.085	-.102	-.122

TABLE 11.- PRESSURE COEFFICIENTS FOR CONFIGURATION 124 - Continued

(b) $M = 0.60$; $\alpha = -10^\circ$ to 10° - Concluded

	x/l	C_p for - $\phi = -60^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.428	.262	.270	.247	.236	.199	.156	.075
	.438	.229	.242	.208	.202	.166	.128	.041
	.448	.195	.197	.179	.163	.132	.089	.013
	.468	.100	.102	.073	.068	.031	-.012	-.078
	.478	-.002	-.005	-.029	-.040	-.072	-.116	-.176
	.483	-.128	-.097	-.103	-.086	-.089	-.098	-.135
	.489	-.800	-.809	-.850	-.843	-.910	-.999	-1.013
Upper stage	.494	-.222	-.225	-.243	-.231	-.252	-.255	-.299
	.499	-.106	-.092	-.104	-.092	-.101	-.111	-.148
	.509	-.025	-.005	-.006	.006	-.003	-.018	-.050
	.519	.039	.070	.070	.08[illegible]	.073	.057	.014
	.529	.120	.157	.162	.1[illegible]	.165	.144	.107
	.539	.271	.302	.307	.31[illegible]	.304	.283	.234
	.549	.508	.511	.493	.469	.461	.422	.361
Transition flare	.554	.449	.469	.462	.462	.425	.381	.316
Main stage	.568	-.998	-.932	-.909	-.857	-.745	-.701	-.652
	.577	-.546	-.602	-.620	-.602	-.640	-.649	-.634
	.587	-.135	-.132	-.185	-.208	-.322	-.383	-.461
	.597	-.123	-.080	-.087	-.081	-.119	-.163	-.223
	.607	-.106	-.069	-.069	-.052	-.061	-.076	-.108
	.617	-.100	-.063	-.058	-.046	-.043	-.053	-.084
	.627	-.094	-.057	-.052	-.040	-.043	-.047	-.079
	.637	-.083	-.046	-.040	-.029	-.032	-.047	-.073
	.657	-.078	-.036	-.034	-.018	-.025	-.045	-.071
	.677	-.063	-.027	-.029	-.012	-.021	-.040	-.066
	.697	-.049	-.017	-.023	-.006	-.017	-.035	-.061
	.737	-.059	-.022	-.021	-.003	-.011	-.029	-.051
	.777	-.057	-.019	-.015	-.003	-.007	-.023	-.040
	.785	-.063	-.019	-.017	.001	-.007	-.020	-.040
	.817	-.046	-.011	-.012	.005	-.004	-.018	-.033
	.857	-.050	-.018	-.017	.000	-.009	-.020	-.033
	.877	-.049	-.018	-.017	-.001	-.009	-.021	-.032
	.897	-.051	-.018	-.019	-.002	-.009	-.022	-.034
	.917	-.058	-.023	-.023	-.007	-.015	-.027	-.038
	.957	-.068	-.032	-.032	-.015	-.023	-.037	-.047
	.997	-.135	-.101	-.097	-.073	-.087	-.106	-.128

	x/l	C_p for - $\phi = -30^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.418	.178	.248	.264	.275	.267	.241	.182
	.448	.071	.136	.151	.157	.143	.128	.064
	.468	-.002	.051	.061	.068	.048	.027	-.032
	.483	-.254	-.212	-.212	-.195	-.204	-.225	-.273
	.489	-.788	-.763	-.792	-.769	-.847	-.879	-.904
Upper stage	.509	-.065	-.017	-.006	.012	.003	-.024	-.079
	.529	.074	.140	.157	.174	.160	.127	.066
	.549	.421	.464	.464	.475	.478	.463	.408
Transition flare	.559	.238	.286	.297	.308	.305	.284	.230
Main stage	.568	-.830	-.833	-.863	-.834	-.785	-.788	-.808
	.587	-.297	-.260	-.249	-.243	-.298	-.325	-.322
	.607	-.140	-.074	-.069	-.052	-.055	-.076	-.142
	.627	-.123	-.063	-.052	-.034	-.038	-.064	-.119
	.657	-.111	-.048	-.038	-.018	-.027	-.056	-.115
	.697	-.102	-.040	-.030	-.010	-.021	-.049	-.102
	.737	-.092	-.032	-.023	-.003	-.013	-.064	-.094
	.777	-.088	-.030	-.019	-.001	-.009	-.037	-.088
	.785	-.092	-.032	-.019	-.001	-.009	-.035	-.086
	.817	-.071	-.019	-.012	.005	-.005	-.029	-.073
	.857	-.074	-.026	-.019	.000	-.009	-.034	-.078
	.897	-.077	-.027	-.021	-.003	-.012	-.036	-.080

TABLE 11.- PRESSURE COEFFICIENTS FOR CONFIGURATION 124 - Continued

(c) $M = 0.80$; $\alpha = -10^\circ$ to 10°

	x/l	C_p for - $\phi = 0^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.428	.448	.381	.324	.275	.226	.183	.123
	.438	.425	.351	.294	.241	.196	.149	.092
	.448	.380	.306	.248	.200	.150	.112	.055
	.468	.278	.207	.158	.105	.059	.021	-.033
	.478	.176	.109	.059	.011	-.028	-.067	-.114
	.483	.055	-.008	-.055	-.097	-.132	-.164	-.211
Upper stage	.489	-1.064	-1.093	-1.117	-1.135	-1.140	-1.129	-1.021
	.494	-.216	-.308	-.363	-.382	-.383	-.372	-.360
	.499	-.052	-.094	-.153	-.191	-.223	-.224	-.228
	.509	.065	.050	.034	.023	.003	.002	-.018
	.519	.143	.132	.120	.125	.116	.127	.115
	.529	.248	.237	.229	.222	.221	.213	.197
	.539	.435	.417	.397	.362	.334	.306	.267
	.549	.696	.639	.588	.518	.447	.392	.341
Transition flare	.554	.037	.042	.034	.034	.034	.037	.036
	.558	.524	.475	.421	.364	.295	.232	.178
Main stage	.568	-.952	-1.002	-.971	-.958	-.936	-.909	-.878
	.577	-.695	-.764	-.780	-.756	-.714	-.641	-.586
	.587	-.204	-.320	-.391	-.394	-.371	-.348	-.368
	.597	-.037	-.086	-.137	-.172	-.192	-.208	-.240
	.607	-.021	-.035	-.056	-.090	-.110	-.126	-.154
	.617	-.017	-.024	-.036	-.055	-.067	-.080	-.099
	.627	-.013	-.020	-.028	-.039	-.048	-.056	-.064
	.637	-.002	-.012	-.020	-.031	-.032	-.041	-.045
	.657	.014	-.001	-.014	-.018	-.023	-.021	-.024
	.677	.019	.001	-.012	-.015	-.017	-.015	-.017
	.697	.024	.006	-.007	-.011	-.014	-.011	-.014
	.737	.026	.004	-.007	-.011	-.013	-.010	-.015
	.777	.033	.014	.001	-.004	-.006	-.006	-.015
	.785	.041	.020	.005	-.001	-.003	-.001	-.010
	.817	.035	.018	.004	.000	-.004	-.004	-.015
	.857	.028	.012	-.001	-.004	-.008	-.007	-.023
	.877	.031	.014	.001	-.003	-.007	-.008	-.023
	.897	.026	.009	-.004	-.007	-.011	-.011	-.027

	x/l	C_p for - $\phi = -30^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.428	.414	.359	.313	.272	.226	.176	.108
	.438	.376	.325	.279	.234	.192	.138	.074
	.448	.342	.287	.241	.200	.158	.104	.047
	.468	.240	.189	.143	.102	.059	.021	-.044
	.478	.146	.094	.052	.011	-.028	-.067	-.126
	.483	.017	-.027	-.067	-.101	-.132	-.164	-.214
Upper stage	.489	-.990	-1.005	-1.017	-1.008	-.986	-.959	-.898
	.494	-.317	-.394	-.422	-.421	-.426	-.415	-.407
	.499	-.079	-.137	-.196	-.230	-.250	-.247	-.267
	.509	.041	.043	.034	.019	.003	-.002	-.021
	.519	.123	.128	.124	.128	.128	.123	.103
	.529	.225	.230	.225	.226	.221	.209	.185
	.539	.412	.405	.389	.362	.334	.310	.275
	.549	.661	.623	.580	.510	.451	.423	.372
Transition flare	.554	.647	.614	.552	.483	.421	.386	.328
	.558	.543	.498	.456	.391	.321	.274	.224
Main stage	.568	-1.623	-1.341	-1.131	-1.060	-.932	-.742	-.617
	.577	-.606	-.698	-.722	-.701	-.691	-.691	-.641
	.587	-.185	-.308	-.375	-.382	-.398	-.473	-.532
	.597	-.048	-.082	-.118	-.144	-.161	-.204	-.271
	.607	-.052	-.047	-.067	-.090	-.110	-.134	-.201
	.617	-.044	-.035	-.040	-.055	-.067	-.080	-.107
	.627	-.037	-.028	-.032	-.039	-.048	-.052	-.064
	.637	-.025	-.020	-.024	-.031	-.032	-.037	-.045
	.657	-.016	-.013	-.020	-.020	-.024	-.022	-.031
	.677	-.001	.000	-.009	-.011	-.016	-.015	-.026
	.697	-.004	-.004	-.012	-.012	-.014	-.015	-.028
	.737	-.002	-.001	-.009	-.008	-.011	-.011	-.029
	.777	.012	.008	-.006	-.002	-.004	-.008	-.029
	.785	.008	.007	.001	-.004	-.003	-.004	-.026
	.817	.008	.008	.001	-.001	-.005	-.007	-.027
	.857	.001	.002	-.005	-.005	-.009	-.011	-.032
	.877	.000	.001	-.006	-.006	-.010	-.013	-.032
	.897	-.002	-.001	-.008	-.008	-.011	-.015	-.035
	.917	-.003	.000	-.008	-.008	-.012	-.017	-.037
	.957	-.015	-.014	-.019	-.020	-.026	-.031	-.051
	.997	-.102	-.085	-.079	-.082	-.092	-.102	-.128

TABLE 11.- PRESSURE COEFFICIENTS FOR CONFIGURATION 124 - Continued

(c) M = 0.80; α = -10° to 10° - Concluded

	x/l	C_p for - ϕ = -60°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.428	.301	.302	.286	.272	.233	.191	.108
	.438	.267	.275	.248	.234	.196	.161	.074
	.448	.233	.238	.218	.196	.165	.119	.040
	.468	.134	.139	.120	.098	.071	.028	-.048
	.478	.044	.045	.025	.007	-.020	-.060	-.133
	.483	-.133	-.101	-.094	-.085	-.090	-.098	-.133
	.489	-1.180	-1.155	-1.137	-1.127	-1.129	-1.129	-1.153
Upper stage	.494	-.395	-.417	-.441	-.432	-.445	-.457	-.454
	.499	-.185	-.211	-.243	-.246	-.270	-.247	-.282
	.509	-.017	.023	.030	.027	.019	.010	-.037
	.519	.061	.105	.120	.128	.120	.104	.057
	.529	.162	.210	.225	.226	.217	.201	.154
	.539	.334	.374	.373	.362	.350	.329	.279
	.549	.556	.573	.537	.506	.494	.466	.403
Transition flare	.554	.532	.548	.513	.498	.471	.432	.389
Main stage	.568	-1.104	-.955	-.971	-.950	-.823	-.761	-.664
	.577	-.820	-.791	-.753	-.732	-.714	-.695	-.676
	.587	-.278	-.417	-.410	-.401	-.465	-.485	-.559
	.597	-.153	-.152	-.172	-.191	-.242	-.286	-.372
	.607	-.130	-.070	-.079	-.094	-.118	-.150	-.212
	.617	-.115	-.051	-.048	-.055	-.063	-.084	-.123
	.627	-.103	-.047	-.036	-.039	-.044	-.056	-.084
	.637	-.091	-.039	-.028	-.031	-.032	-.041	-.072
	.657	-.082	-.036	-.024	-.018	-.023	-.032	-.064
	.677	-.066	-.027	-.019	-.014	-.020	-.030	-.060
	.697	-.051	-.018	-.013	-.011	-.017	-.028	-.056
	.737	-.062	-.021	-.013	-.008	-.013	-.024	-.049
	.7	-.058	-.018	-.007	-.004	-.009	-.018	-.042
	.5	-.062	-.018	-.009	-.002	-.007	-.015	-.038
	.817	-.049	-.012	-.004	-.001	-.006	-.012	-.033
	.857	-.055	-.019	-.009	-.005	-.010	-.016	-.035
	.8?7	-.054	-.018	-.010	-.006	-.010	-.016	-.035
	.897	-.057	-.018	-.010	-.007	-.012	-.017	-.037
	.917	-.064	-.026	-.017	-.012	-.017	-.023	-.042
	.957	-.070	-.033	-.023	-.020	-.026	-.033	-.052
	.997	-.146	-.105	-.092	-.083	-.095	-.106	-.134

	x/l	C_p for - ϕ = -90°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.418	.214	.287	.309	.309	.309	.278	.217
	.448	.112	.173	.192	.189	.180	.157	.092
	.468	.032	.087	.101	.102	.086	.062	.005
	.483	-.195	-.143	-.132	-.128	-.136	-.156	-.211
	.489	-1.006	-.947	-.928	-.915	-.928	-.940	-.963
Upper stage	.509	-.056	.004	.023	.031	.023	.002	-.064
	.529	.116	.191	.217	.222	.214	.185	.115
	.549	.458	.514	.514	.518	.525	.505	.446
Transition flare	.558	.336	.372	.398	.379	.387	.370	.324
Main stage	.568	-.832	-.869	-.925	-.947	-.878	-.831	-.820
	.587	-.539	-.476	-.430	-.413	-.457	-.489	-.532
	.607	-.177	-.113	-.095	-.098	-.126	-.130	-.189
	.627	-.122	-.055	-.036	-.039	-.040	-.056	-.130
	.657	-.114	-.046	-.027	-.019	-.027	-.046	-.115
	.697	-.103	-.039	-.021	-.012	-.020	-.039	-.103
	.737	-.094	-.032	-.016	-.007	-.014	-.033	-.095
	.777	-.087	-.028	-.010	-.004	-.010	-.029	-.088
	.785	-.091	-.029	-.012	-.004	-.009	-.028	-.086
	.817	-.074	-.020	-.005	.001	-.006	-.020	-.074
	.857	-.079	-.025	-.010	-.004	-.011	-.026	-.078
	.897	-.082	-.028	-.014	-.007	-.014	-.030	-.082

TABLE 11.- PRESSURE COEFFICIENTS FOR CONFIGURATION 124 - Continued

(d) M = 1.00; $\alpha = -10^\circ$ to 10°

	x/l	C_p for - $\phi = 0^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.428	.551	.477	.426	.374	.332	.292	.238
	.438	.524	.452	.402	.350	.305	.262	.211
	.448	.485	.413	.366	.314	.269	.225	.178
	.468	.410	.338	.297	.245	.200	.159	.109
	.478	.337	.275	.237	.188	.149	.108	.064
	.483	.259	.209	.177	.134	.095	.060	.025
	.489	-.562	-.579	-.587	-.607	-.622	-.636	-.647
Upper stage	.494	-.558	-.621	-.651	-.339	-.206	-.180	-.185
	.499	-.406	-.500	-.552	-.166	-.153	-.152	-.160
	.509	.057	-.026	-.025	-.088	-.116	-.124	-.123
	.519	.264	.234	.164	.024	-.008	-.003	-.018
	.529	.385	.374	.347	.145	.129	.133	.097
	.539	.584	.563	.524	.253	.237	.245	.205
	.549	.823	.746	.657	.352	.318	.332	.301
Transition flare	.554	.053	.054	.052	.035	.044	.055	.046
	.558	.718	.685	.671	.426	.304	.296	.287
Main stage	.568	-.998	-1.018	-1.017	-.968	-.990	-1.026	-1.043
	.577	-.651	-.739	-.759	-.609	-.513	-.480	-.482
	.587	-.365	-.485	-.542	-.420	-.416	-.477	-.523
	.597	-.247	-.358	-.415	-.330	-.389	-.471	-.523
	.607	-.198	-.283	-.326	-.293	-.348	-.397	-.383
	.617	-.173	-.246	-.267	-.265	-.296	-.298	-.256
	.627	-.167	-.221	-.214	-.231	-.240	-.223	-.182
	.637	-.151	-.184	-.158	-.190	-.190	-.171	-.142
	.657	-.161	-.138	-.127	-.149	-.145	-.119	-.098
	.677	-.107	-.110	-.106	-.118	-.114	-.092	-.081
	.697	-.083	-.090	-.088	-.094	-.091	-.073	-.070
	.737	-.053	-.070	-.074	-.078	-.074	-.057	-.064
	.777	-.027	-.048	-.054	-.062	-.059	-.028	-.056
	.785	-.012	-.037	-.045	-.053	-.051	-.006	-.041
	.817	-.006	-.030	-.038	-.048	-.046	.013	-.043
	.857	-.016	-.036	-.044	-.053	-.045	.033	-.046
	.877	-.008	-.001	-.038	-.051	-.028	.036	-.035
	.897	.024	.039	-.008	-.049	.008	.032	-.016

	x/l	C_p for - $\phi = -30^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.428	.515	.458	.423	.374	.332	.286	.226
	.438	.479	.428	.393	.344	.302	.253	.190
	.448	.452	.395	.357	.311	.269	.222	.166
	.468	.370	.320	.285	.242	.200	.159	.100
	.478	.307	.260	.231	.188	.152	.111	.058
	.483	.226	.191	.168	.128	.095	.060	.019
	.489	-.528	-.533	-.535	-.548	-.560	-.575	-.581
Upper stage	.494	-.579	-.628	-.654	-.271	-.283	-.288	-.244
	.499	-.471	-.544	-.583	-.206	-.218	-.205	-.213
	.509	.035	-.023	-.028	-.100	-.091	-.081	-.123
	.519	.240	.222	.152	.027	.027	.019	-.027
	.529	.354	.361	.328	.145	.141	.130	.078
	.539	.553	.547	.511	.250	.246	.239	.187
	.549	.786	.730	.648	.346	.330	.316	.264
Transition flare	.554	.810	.786	.741	.356	.304	.330	.309
	.558	.731	.704	.689	.396	.331	.320	.272
Main stage	.568	-1.026	-1.034	-1.026	-.959	-.986	-1.035	-1.071
	.577	-.672	-.745	-.769	-.556	-.574	-.679	-.792
	.587	-.409	-.513	-.561	-.426	-.472	-.542	-.584
	.597	-.216	-.290	-.322	-.271	-.314	-.353	-.374
	.607	-.232	-.302	-.329	-.305	-.348	-.381	-.380
	.617	-.210	-.262	-.267	-.268	-.289	-.291	-.272
	.627	-.204	-.237	-.214	-.234	-.240	-.233	-.213
	.637	-.192	-.203	-.167	-.193	-.193	-.180	-.176
	.657	-.197	-.150	-.132	-.150	-.146	-.132	-.135
	.677	-.127	-.110	-.101	-.110	-.107	-.100	-.112
	.697	-.115	-.101	-.091	-.094	-.091	-.084	-.104
	.737	-.084	-.080	-.074	-.075	-.072	-.054	-.096
	.777	-.048	-.052	-.050	-.057	-.056	-.033	-.092
	.785	-.046	-.048	-.049	-.053	-.048	-.016	-.089
	.817	-.036	-.041	-.041	-.049	-.046	.002	-.089
	.857	-.046	-.047	-.047	-.054	-.047	.026	-.086
	.877	-.040	-.005	-.045	-.053	-.033	.027	-.076
	.897	.004	.029	-.013	-.050	.008	.024	-.056
	.917	.034	.033	.030	-.015	.025	.020	-.034
	.957	.033	.024	.032	.022	.017	.002	-.021
	.997	-.032	-.052	-.061	-.088	-.103	-.121	-.139

TABLE 11.- PRESSURE COEFFICIENTS FOR CONFIGURATION 124 - Continued

(d) M = 1.00; α = -10° to 10° - Concluded

	x/l	C_p for - ϕ = -60°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.428	.407	.404	.393	.371	.338	.298	.226
	.438	.373	.377	.363	.341	.308	.271	.193
	.448	.343	.344	.336	.311	.281	.234	.163
	.468	.271	.272	.267	.239	.212	.165	.097
	.478	.208	.215	.213	.188	.161	.114	.052
	.483	-.187	-.149	-.123	-.115	-.118	-.126	-.168
	.489	-.685	-.653	-.630	-.622	-.625	-.627	-.641
Upper stage	.494	-.663	-.683	-.688	-.234	-.246	-.326	-.238
	.499	-.505	-.544	-.456	-.197	-.206	-.217	-.210
	.509	-.015	-.048	-.075	-.107	-.128	-.121	-.157
	.519	.144	.135	.077	.014	-.014	.006	-.046
	.529	.271	.306	.263	.138	.132	.152	.094
	.539	.457	.498	.449	.241	.262	.307	.236
	.549	.655	.656	.589	.331	.373	.434	.360
Transition flare	.554	.688	.722	.674	.408	.441	.540	.495
Main stage	.568	-1.041	-1.037	-1.026	-.962	-1.011	-1.057	-1.077
	.577	-.765	-.792	-.778	-.497	-.686	-.859	-.928
	.587	-.523	-.572	-.580	-.451	-.534	-.676	-.761
	.597	-.378	-.426	-.437	-.389	-.429	-.493	-.578
	.607	-.331	-.345	-.326	-.321	-.330	-.344	-.374
	.617	-.316	-.302	-.257	-.268	-.265	-.276	-.309
	.627	-.309	-.256	-.214	-.228	-.224	-.236	-.275
	.637	-.294	-.206	-.167	-.193	-.187	-.198	-.241
	.657	-.243	-.169	-.136	-.144	-.145	-.158	-.203
	.677	-.201	-.140	-.113	-.118	-.120	-.133	-.175
	.697	-.159	-.111	-.090	-.092	-.096	-.107	-.147
	.737	-.146	-.098	-.077	-.072	-.076	-.084	-.121
	.777	-.122	-.079	-.058	-.059	-.060	-.055	-.101
	.785	-.124	-.078	-.058	-.057	-.056	-.034	-.096
	.817	-.101	-.059	-.044	-.048	-.048	-.010	-.085
	.857	-.104	-.064	-.051	-.053	-.052	.018	-.082
	.877	-.091	-.016	-.047	-.053	-.038	.021	-.075
	.897	-.039	.012	-.021	-.047	.001	.019	-.062
	.917	-.027	.008	.020	-.015	.022	.014	-.034
	.957	-.024	.005	.027	.025	.017	.000	-.013
	.997	-.098	-.083	-.075	-.088	-.102	-.120	-.140

	x/l	C_p for - ϕ = -5°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.418	.328	.386	.408	.407	.404	.383	.331
	.448	.226	.281	.309	.305	.293	.271	.220
	.468	.169	.221	.249	.242	.227	.201	.148
	.483	.028	.083	.111	.107	.098	.072	.022
Upper stage	.489	-.550	-.496	-.464	-.459	-.465	-.495	-.515
	.509	-.151	-.122	-.078	-.082	-.101	-.065	-.089
	.529	.156	.203	.161	.160	.219	.254	.171
	.549	.516	.560	.499	.383	.510	.583	.518
Transition flare	.558	.511	.606	.607	.450	.596	.583	.495
Main stage	.568	-1.075	-1.055	-1.026	-.990	-1.033	-1.057	-1.077
	.587	-.651	-.640	-.577	-.479	-.609	-.551	-.668
	.607	-.440	-.376	-.322	-.321	-.327	-.391	-.451
	.627	-.340	-.234	-.205	-.212	-.209	-.239	-.337
	.657	-.262	-.179	-.143	-.140	-.147	-.182	-.264
	.697	-.207	-.132	-.098	-.092	-.100	-.125	-.204
	.737	-.178	-.109	-.078	-.071	-.079	-.099	-.173
	.777	-.155	-.089	-.060	-.058	-.065	-.075	-.154
	.785	-.161	-.091	-.061	-.057	-.060	-.081	-.145
	.817	-.124	-.068	-.045	-.045	-.048	-.018	-.120
	.857	-.122	-.068	-.052	-.053	-.055	.007	-.133
	.897	-.053	.001	-.010	-.049	-.005	.006	-.123

TABLE 11.- PRESSURE COEFFICIENTS FOR CONFIGURATION 124 - Continued

(e) $M = 1.20$; $\alpha = -10^\circ$ to 10°

	x/l	C_p for - $\phi = 0^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.428	.506	.430	.364	.314	.277	.239	.192
	.438	.517	.435	.375	.322	.277	.247	.192
	.448	.506	.427	.359	.320	.269	.236	.181
	.468	.493	.416	.362	.317	.274	.231	.181
	.478	.466	.403	.359	.312	.274	.231	.176
	.483	.426	.376	.338	.298	.258	.220	.165
Upper stage	.489	-.243	-.258	-.273	-.289	-.310	-.328	-.359
	.494	-.289	-.332	-.350	-.371	-.385	-.391	-.279
	.499	-.203	-.266	-.292	-.324	-.343	-.102	-.070
	.509	-.112	-.183	-.220	-.253	.071	.001	-.056
	.519	-.066	-.123	-.013	.178	.117	.028	-.034
	.529	.299	.346	.293	.225	.162	.092	.032
	.539	.544	.421	.334	.247	.195	.139	.110
	.549	.635	.487	.387	.275	.211	.152	.154
Transition flare	.554	.060	.050	.049	.050	.048	.052	.054
	.558	.995	.893	.712	.414	.197	.128	.135
Main stage	.568	-.612	-.594	-.565	-.528	-.453	-.565	-.577
	.577	-.344	-.360	-.350	-.327	-.205	-.215	-.213
	.587	-.159	-.225	-.259	-.230	-.219	-.223	-.246
	.597	-.090	-.161	-.198	-.181	-.214	-.220	-.255
	.607	-.052	-.120	-.151	-.162	-.191	-.204	-.227
	.617	-.041	-.098	-.124	-.145	-.167	-.170	-.175
	.627	-.027	-.081	-.104	-.128	-.136	-.135	-.119
	.637	-.016	-.065	-.082	-.098	-.111	-.104	-.078
	.657	-.027	-.070	-.080	-.077	-.073	-.058	-.041
	.677	-.034	-.044	-.049	-.051	-.052	-.032	-.024
	.697	-.027	-.040	-.042	-.039	-.030	-.018	-.018
	.737	-.020	-.025	-.029	-.038	-.033	-.027	-.012
	.777	.015	-.012	-.021	-.024	-.028	-.026	-.016
	.785	.026	-.004	-.018	-.013	-.018	-.009	-.004
	.817	.021	-.002	-.005	-.021	-.018	-.010	-.010
	.857	.020	.010	-.009	-.002	-.001	-.005	-.014
	.877	.030	-.003	-.007	-.001	-.004	-.005	-.010
	.897	.013	-.003	-.001	-.005	-.009	-.013	-.017

	x/l	C_p for - $\phi = -30^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.428	.474	.411	.359	.314	.282	.233	.181
	.438	.471	.413	.359	.317	.274	.239	.173
	.448	.469	.408	.354	.317	.274	.236	.175
	.468	.453	.397	.354	.312	.274	.233	.173
	.478	.434	.389	.351	.312	.277	.236	.173
	.483	.388	.355	.327	.290	.258	.217	.157
Upper stage	.489	-.215	-.217	-.226	-.239	-.266	-.287	-.315
	.494	-.308	-.338	-.355	-.374	-.390	-.410	-.442
	.499	-.250	-.297	-.317	-.341	-.360	-.372	-.296
	.509	-.123	-.181	-.215	-.219	.051	-.010	-.050
	.519	-.096	-.128	.037	.175	.098	.042	.008
	.529	.288	.333	.288	.219	.140	.083	.057
	.539	.494	.399	.321	.244	.156	.108	.057
	.549	.616	.482	.381	.269	.167	.174	.137
Transition flare	.554	.875	.637	.462	.300	.200	.115	.103
	.558	.981	.887	.688	.341	.303	.373	.342
Main stage	.568	-.631	-.606	-.565	-.[illegible]	-.547	-.562	-.602
	.577	-.361	-.377	-.389	-.[illegible]75	-.338	-.419	-.486
	.587	-.192	-.247	-.261	-.228	-.244	-.341	-.442
	.597	-.088	-.128	-.148	-.145	-.150	-.176	-.219
	.607	-.082	-.131	-.154	-.164	-.[illegible]5	-.195	-.219
	.617	-.063	-.106	-.124	-.148	-.150	-.162	-.169
	.627	-.060	-.092	-.107	-.131	-.131	-.132	-.130
	.637	-.049	-.079	-.090	-.104	-.106	-.104	-.092
	.657	-.053	-.069	-.075	-.069	-.062	-.063	-.073
	.677	-.057	-.042	-.042	-.043	-.045	-.043	-.060
	.697	-.069	-.047	-.040	-.045	-.041	-.035	-.058
	.737	-.049	-.039	-.030	-.035	-.033	-.039	-.053
	.777	-.014	-.019	-.028	-.017	-.025	-.029	-.059
	.795	-.007	-.016	-.017	-.008	-.013	-.016	-.056
	.817	- 005	-.014	-.009	-.019	-.016	-.020	-.068
	.857	-.010	.002	-.010	-.011	-.010	-.018	-.068
	.877	-.001	-.013	-.007	-.004	-.006	-.015	-.064
	.897	.013	-.011	-.003	-.002	-.005	-.017	-.057
	.917	-.016	-.003	-.005	-.006	-.006	-.016	-.050
	.957	-.016	-.015	-.012	-.016	-.017	-.018	-.044
	.997	-.006	-.021	-.033	-.044	-.065	-.091	-.095

TABLE 11.- PRESSURE COEFFICIENTS FOR CONFIGURATION 124 - Concluded

(e) $M = 1.20$; $\alpha = -10^\circ$ to 10° - Concluded

	x/l	C_p for - $\phi = -60^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.428	.362	.352	.330	.312	.282	.247	.184
	.438	.367	.363	.327	.314	.282	.263	.181
	.448	.364	.360	.332	.314	.285	.249	.176
	.468	.348	.349	.332	.312	.288	.249	.179
	.478	.330	.339	.332	.312	.290	.252	.173
Upper stage	.483	-.204	-.168	-.153	-.144	-.146	-.169	-.211
	.489	-.368	-.327	-.311	-.302	-.299	-.317	-.359
	.494	-.377	-.379	-.383	-.385	-.396	-.413	-.453
	.499	-.294	-.310	-.317	-.330	-.351	-.380	-.437
	.509	-.220	-.225	-.239	-.230	-.1[illegible]	-.157	-.092
	.519	-.181	-.128	.106	.170	.084	.056	-.001
	.529	.268	.294	.265	.211	.156	.144	.063
	.539	.390	.344	.293	.236	.206	.202	.137
	.549	.459	.393	.334	.26[illegible]	.264	.260	.168
Transition flare	.554	.699	.550	.419	.371	.344	.324	.339
Main stage	.568	-.645	-.606	-.546	-.506	-.567	-.587	-.657
	.577	-.435	-.407	-.355	-.253	-.409	-.441	-.547
	.587	-.275	-.285	-.267	-.233	-.327	-.372	-.459
	.597	-.196	-.214	-.215	-.214	-.249	-.317	-.384
	.607	-.162	-.167	-.168	-.181	-.175	-.250	-.324
	.617	-.151	-.145	-.143	-.148	-.139	-.170	-.249
	.627	-.151	-.134	-.126	-.126	-.123	-.137	-.177
	.637	-.137	-.117	-.096	-.098	-.098	-.107	-.144
	.657	-.160	-.075	-.060	-.055	-.059	-.082	-.132
	.677	-.138	-.072	-.052	-.051	-.057	-.073	-.124
	.697	-.116	-.068	-.043	-.046	-.054	-.064	-.116
	.737	-.117	-.060	-.038	-.036	-.039	-.063	-.093
	.777	-.085	-.046	-.034	-.018	-.030	-.045	-.070
	.785	-.068	-.045	-.024	-.009	-.021	-.035	-.067
	.817	-.062	-.027	-.012	-.016	-.018	-.034	-.063
	.857	-.071	-.019	-.016	-.015	-.024	-.034	-.05[illegible]
	.877	-.061	-.032	-.009	-.004	-.009	-.024	-.0[illegible]
	.897	-.071	-.031	-.010	-.001	-.004	-.018	-.04[illegible]
	.917	-.079	-.032	-.018	-.008	-.010	-.023	-.0[illegible]
	.957	-.077	-.037	-.015	-.015	-.021	-.021	-.04[illegible]
	.997	-.070	-.047	-.042	-.053	-.061	-.084	-.113

	x/l	C_p for - $\phi = -[illegible]^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.418	.241	.288	.308	.309	.314	.297	.259
	.448	.244	.293	.303	.309	.298	.289	.235
	.468	.239	.296	.316	.317	.304	.287	.232
Upper stage	.483	.182	.250	.268	.274	.269	.249	.189
	.489	-.262	-.204	-.180	-.171	-.176	-.194	-.244
	.509	-.292	-.261	-.256	-.255	-.260	-.273	-.304
	.529	.188	.233	.238	.206	.253	.248	.192
	.549	.332	.322	.299	.294	.330	.334	.322
Transition flare	.558	.723	.648	.514	.479	.547	.631	.708
Main stage	.568	-.670	-.611	-.551	-.556	-.567	-.612	-.666
	.587	-.374	-.330	-.278	-.272	-.307	-.339	-.390
	.607	-.259	-.219	-.201	-.170	-.211	-.228	-.268
	.627	-.239	-.153	-.121	-.109	-.120	-.158	-.249
	.657	-.180	-.084	-.059	-.052	-.058	-.093	-.183
	.697	-.168	-.093	-.055	-.044	-.061	-.087	-.170
	.737	-.145	-.074	-.046	-.037	-.039	-.073	-.150
	.777	-.100	-.056	-.031	-.020	-.029	-.057	-.123
	.785	-.112	-.060	-.032	-.014	-.026	-.055	-.124
	.817	-.093	-.032	-.013	-.008	-.019	-.043	-.105
	.857	-.096	-.032	-.018	-.010	-.031	-.052	-.103
	.897	-.100	-.043	-.017	-.006	-.009	-.027	-.091

TABLE 12.- PRESSURE COEFFICIENTS FOR CONFIGURATION 324

(a) M = 0.40 to 0.95; $\alpha = 0^\circ$

	x/l	C_p for - $\phi = 0^\circ$					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.461	.487	.558	.586	.636	.658	.696
	.471	.334	.399	.433	.490	.518	.563
	.481	.095	.195	.232	.310	.342	.393
	.489	-1.148	-.739	-.554	-.378	-.367	-.467
Upper stage	.494	-.485	-.668	-.538	-.384	-.367	-.433
	.499	-.160	-.541	-.517	-.384	-.374	-.430
	.509	-.025	-.240	-.359	-.381	-.377	-.414
	.519	.053	-.017	-.151	-.331	-.357	-.356
	.529	.132	.120	.023	-.245	-.306	-.280
	.539	.255	.225	.152	-.134	-.232	-.219
	.549	.446	.347	.268	.020	-.091	-.092
Transition flare	.554	.030	.042	.043	.044	.046	.045
	.558	.196	.239	.260	.174	.089	.038
Main stage	.568	-1.237	-1.051	-1.036	-.903	-.710	-.653
	.577	-.238	-.327	-.297	-.202	-.216	-.369
	.587	-.138	-.154	-.139	-.120	-.118	-.289
	.597	-.093	-.104	-.093	-.081	-.078	-.187
	.607	-.059	-.076	-.064	-.059	-.057	-.089
	.617	-.048	-.058	-.052	-.048	-.047	-.038
	.627	-.037	-.049	-.039	-.038	-.037	-.022
	.637	-.025	-.040	-.031	-.027	-.027	-.012
	.657	-.019	-.023	-.021	-.021	-.021	-.011
	.677	-.015	-.018	-.016	-.018	-.019	-.012
	.697	-.007	-.011	-.011	-.013	-.015	-.012
	.737	-.003	-.010	-.009	-.013	-.014	-.014
	.777	.001	-.005	-.003	-.007	-.009	-.009
	.785	.005	.004	.004	.000	-.002	-.003
	.817	.003	.000	.001	-.002	-.004	-.006
	.857	.003	-.004	-.002	-.005	-.007	-.010
	.877	.003	-.003	-.002	-.005	-.007	-.010
	.897	.000	-.006	-.004	-.008	-.010	-.013

NO 324

	x/l	C_p for - $\phi = -30^\circ$					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.461	.487	.553	.582	.636	.652	.693
	.471	.291	.374	.407	.471	.497	.542
	.481	.095	.195	.232	.306	.342	.390
	.489	-1.159	-.622	-.513	-.381	-.370	-.461
Upper stage	.494	-.586	-.550	-.467	-.352	-.350	-.420
	.499	-.238	-.532	-.467	-.359	-.357	-.414
	.509	-.014	-.322	-.380	-.363	-.363	-.411
	.519	.053	-.067	-.205	-.327	-.347	-.366
	.529	.132	.102	-.023	-.263	-.306	-.299
	.539	.244	.211	.119	-.174	-.249	-.223
	.549	.423	.352	.247	-.023	-.118	-.117
Transition flare	.554	.373	.355	.317	.089	.000	-.012
	.558	.207	.266	.264	.114	.036	.020
Main stage	.568	-1.203	-1.042	-.991	-.656	-.532	-.621
	.577	-.238	-.308	-.272	-.195	-.205	-.347
	.587	-.138	-.154	-.139	-.120	-.125	-.277
	.597	-.070	-.072	-.064	-.056	-.057	-.133
	.607	-.059	-.072	-.064	-.059	-.061	-.089
	.617	-.048	-.058	-.052	-.048	-.047	-.044
	.627	-.037	-.049	-.039	-.038	-.037	-.025
	.637	-.025	-.040	-.031	-.031	-.031	-.015
	.657	-.019	-.024	-.022	-.023	-.025	-.012
	.677	-.011	-.011	-.011	-.013	-.013	-.007
	.697	-.011	-.011	-.012	-.014	-.015	-.012
	.737	-.003	-.006	-.006	-.009	-.013	-.012
	.777	.001	.000	.000	-.003	-.006	-.005
	.785	.005	.004	.004	-.002	-.002	-.004
	.817	.003	-.001	.001	-.002	-.004	-.006
	.857	.002	-.005	-.003	-.007	-.009	-.011
	.877	.002	-.005	-.004	-.007	-.009	-.012
	.897	-.001	-.007	-.006	-.010	-.011	-.014
	.917	-.001	-.007	-.006	-.010	-.012	-.014
	.957	-.012	-.019	-.018	-.022	-.024	-.027
	.997	-.065	-.078	-.079	-.087	-.093	-.103

TABLE A2.- PRESSURE COEFFICIENTS FOR CONFIGURATION 324 - Continued

(a) M = 0.40 to 0.95; α = 0° - Concluded

	x/l	C_p for - β = -90°					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.461	.487	.553	.582	.625	.652	.693
	.471	.323	.399	.429	.483	.511	.551
	.481	.095	.200	.240	.310	.342	.390
	.489	-1.192	-.541	-.463	-.374	-.384	-.464
Upper stage	.494	-.552	-.482	-.413	-.331	-.340	-.395
	.499	-.250	-.486	-.422	-.338	-.347	-.401
	.509	-.025	-.354	-.372	-.345	-.353	-.392
	.519	.053	-.126	-.230	-.320	-.337	-.353
	.529	.132	.065	-.068	-.263	-.296	-.299
	.539	.244	.179	.069	-.188	-.249	-.251
	.549	.412	.302	.202	-.077	-.155	-.159
Transition flare	.554	.373	.355	.313	.114	.019	-.006
	.558	-.037	.239	.227	.065	-.027	-.031
	.562	.030	.127	.174	.216	.208	.186
Main stage	.568	-1.147	-1.037	-.953	-.592	-.491	-.564
	.577	-.238	-.281	-.247	-.191	-.199	-.334
	.587	-.138	-.149	-.135	-.124	-.128	-.267
	.597	-.081	-.094	-.085	-.081	-.088	-.181
	.607	-.059	-.072	-.064	-.059	-.061	-.092
	.617	-.048	-.058	-.052	-.048	-.047	-.047
	.627	-.037	-.049	-.039	-.038	-.041	-.031
	.637	-.025	-.040	-.031	-.031	-.031	-.018
	.657	-.019	-.023	-.022	-.024	-.025	-.015
	.677	-.013	-.017	-.016	-.019	-.019	-.013
	.697	-.007	-.011	-.011	-.013	-.014	-.011
	.737	-.003	-.006	-.004	-.009	-.012	-.011
	.777	.001	-.001	-.002	-.007	-.007	-.007
	.785	.001	.000	.000	-.004	-.006	-.007
	.817	.005	.001	.001	-.002	-.004	-.005
	.857	.002	-.004	-.003	-.007	-.009	-.011
	.877	.000	-.005	-.004	-.007	-.009	-.012
	.897	.000	-.005	-.004	-.008	-.010	-.013
	.917	-.004	-.010	-.010	-.013	-.015	-.017
	.957	-.012	-.019	-.018	-.022	-.024	-.027
	.997	-.066	-.079	-.079	-.089	-.094	-.104

	x/l	C_p for - β = -90°					
		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
Nose	.461	.487	.553	.582	.629	.652	.690
	.481	.095	.209	.248	.310	.342	.390
	.489	-1.170	-.500	-.410	-.399	-.434	-.527
Upper stage	.509	-.014	-.363	-.359	-.338	-.350	-.385
	.529	.132	.024	-.106	-.259	-.296	-.302
	.549	.412	.261	.152	-.088	-.152	-.162
Transition flare	.558	.196	.207	.174	.026	-.034	-.053
Main stage	.568	-1.158	-1.005	-.870	-.549	-.542	-.631
	.587	-.126	-.149	-.135	-.124	-.128	-.258
	.607	-.059	-.072	-.064	-.063	-.064	-.092
	.627	-.037	-.049	-.039	-.038	-.041	-.031
	.657	-.019	-.024	-.024	-.026	-.026	-.017
	.697	-.011	-.013	-.012	-.016	-.018	-.014
	.737	-.003	-.006	-.009	-.009	-.012	-.011
	.777	.001	-.005	-.002	-.007	-.007	-.009
	.785	.001	-.006	-.002	-.007	-.008	-.010
	.817	.006	.002	.003	-.001	-.002	-.004
	.857	.002	-.004	-.002	-.006	-.008	-.011
	.897	-.001	-.007	-.006	-.009	-.011	-.014

TABLE 12.- PRESSURE COEFFICIENTS FOR CONFIGURATION 324 - Continued

(b) M = 0.60; α = -10° to 10°

324

	x/l	C_p for - $\phi = 0°$						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.461	.752	.659	.598	.531	.460	.390	.296
	.471	.592	.505	.432	.371	.311	.252	.163
	.481	.360	.261	.194	.150	.101	.059	-.008
	.489	-1.125	-1.094	-.988	-.846	-.761	-.663	-.488
Upper stage	.494	-.382	-.630	-.763	-.763	-.608	-.555	-.418
	.499	-.068	-.163	-.301	-.466	-.506	-.481	-.464
	.509	.040	.002	-.016	-.050	-.221	-.276	-.379
	.519	.109	.076	.070	.064	.007	-.048	-.134
	.529	.194	.167	.155	.143	.110	.078	.015
	.539	.354	.315	.292	.257	.190	.140	.094
	.549	.622	.555	.497	.428	.310	.220	.163
Transition flare	.554	.040	.036	.035	.035	.030	.043	.042
	.558	.399	.333	.276	.214	.136	.082	.059
Main stage	.568	-1.009	-1.052	-1.082	-1.059	-1.041	-.937	-.880
	.577	-.199	-.289	-.307	-.295	-.266	-.247	-.236
	.587	-.062	-.106	-.136	-.142	-.152	-.150	-.139
	.597	-.034	-.066	-.090	-.096	-.107	-.105	-.088
	.607	-.017	-.049	-.067	-.067	-.078	-.076	-.060
	.617	-.005	-.038	-.050	-.050	-.061	-.053	-.043
	.627	.006	-.027	-.039	-.039	-.050	-.042	-.031
	.637	.011	-.015	-.027	-.033	-.038	-.036	-.025
	.657	.019	-.009	-.020	-.021	-.026	-.016	-.014
	.677	.023	-.003	-.016	-.015	-.022	-.010	-.010
	.697	.027	-.003	-.010	-.009	-.016	-.006	-.008
	.737	.023	-.007	-.008	-.007	-.014	-.002	-.008
	.777	.035	.009	-.004	-.001	-.008	.000	-.008
	.785	.042	.015	.004	.001	-.002	.004	-.002
	.817	.038	.013	.003	.004	-.004	.003	-.008
	.857	.032	.009	-.001	.001	-.007	-.001	-.015
	.877	.035	.009	.000	.001	-.007	-.001	-.017
	.897	.029	.006	-.003	-.001	-.009	-.004	-.021

	x/l	C_p for - $\phi = -30°$						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.461	.708	.643	.587	.531	.466	.401	.296
	.471	.515	.447	.391	.341	.292	.238	.149
	.481	.321	.250	.194	.150	.118	.075	.003
	.489	-1.085	-.964	-1.044	-.812	-.535	-.448	-.432
Upper stage	.494	-.564	-.773	-.728	-.694	-.517	-.464	-.441
	.499	-.137	-.283	-.432	-.546	-.540	-.504	-.481
	.509	.018	.002	-.033	-.085	-.278	-.316	-.373
	.519	.086	.076	.070	.075	-.010	-.053	-.145
	.529	.166	.156	.150	.143	.104	.078	.009
	.539	.325	.310	.286	.252	.184	.152	.106
	.549	.599	.543	.491	.417	.292	.249	.231
Transition flare	.554	.534	.490	.445	.377	.277	.211	.177
	.558	.410	.361	.310	.242	.148	.105	.076
Main stage	.568	-1.386	-1.280	-1.179	-1.076	-1.019	-.994	-.794
	.577	-.211	-.283	-.301	-.284	-.255	-.270	-.510
	.587	-.097	-.123	-.136	-.142	-.152	-.156	-.202
	.597	-.040	-.061	-.067	-.067	-.078	-.076	-.077
	.607	-.040	-.055	-.067	-.067	-.078	-.076	-.071
	.617	-.028	-.044	-.050	-.050	-.061	-.053	-.054
	.627	-.023	-.032	-.039	-.039	-.050	-.048	-.048
	.637	-.011	-.027	-.027	-.033	-.038	-.036	-.037
	.657	-.009	-.020	-.024	-.023	-.030	-.025	-.039
	.677	.005	-.007	-.010	-.009	-.018	-.012	-.027
	.697	.001	-.009	-.014	-.011	-.016	-.012	-.027
	.737	.001	-.005	-.010	-.005	-.010	-.006	-.023
	.777	.015	.003	-.004	.001	-.004	.000	-.021
	.785	.011	.003	-.012	.001	-.004	.002	-.016
	.817	.013	.003	.000	.004	-.004	.000	-.021
	.857	.007	-.003	-.005	.001	-.007	-.004	-.027
	.877	.005	-.003	-.005	-.001	-.008	-.005	-.029
	.897	.004	-.004	-.007	-.003	-.010	-.007	-.030
	.917	.003	-.006	-.008	-.003	-.012	-.010	-.035
	.957	-.012	-.018	-.018	-.015	-.023	-.023	-.047
	.997	-.096	-.087	-.076	-.072	-.086	-.091	-.122

TABLE 12.- PRESSURE COEFFICIENTS FOR CONFIGURATION 324 - Continued

(b) M = 0.60; α = -10° to 10° - Concluded

	x/l	C_p for - ϕ = -60°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.461	.587	.582	.559	.531	.482	.429	.323
	.471	.437	.422	.393	.366	.333	.285	.196
	.481	.221	.195	.178	.161	.129	.092	.019
Upper stage	.489	-1.159	-1.043	-.801	-.711	-.699	-.742	-.754
	.494	-.581	-.676	-.671	-.603	-.574	-.572	-.578
	.499	-.285	-.397	-.529	-.529	-.534	-.543	-.555
	.509	-.051	-.044	-.107	-.170	-.243	-.247	-.299
	.519	.012	.042	.064	.064	.007	-.025	-.094
	.529	.097	.133	.150	.155	.116	.095	.020
	.539	.246	.270	.269	.235	.196	.186	.128
Transition flare	.549	.479	.481	.463	.383	.327	.351	.311
	.554	.416	.428	.416	.371	.316	.295	.278
Main stage	.568	-1.021	-1.035	-1.013	-1.065	-1.053	-.891	-.777
	.577	-.427	-.408	-.381	-.278	-.283	-.458	-.601
	.587	-.137	-.135	-.136	-.136	-.152	-.167	-.282
	.597	-.108	-.089	-.084	-.085	-.101	-.105	-.139
	.607	-.097	-.072	-.067	-.067	-.078	-.076	-.099
	.617	-.085	-.061	-.056	-.050	-.061	-.065	-.088
	.627	-.080	-.055	-.044	-.039	-.050	-.053	-.082
	.637	-.074	-.044	-.033	-.033	-.038	-.048	-.077
	.657	-.075	-.042	-.031	-.021	-.032	-.039	-.078
	.677	-.060	-.033	-.022	-.015	-.026	-.034	-.070
	.697	-.046	-.024	-.014	-.009	-.020	-.029	-.063
	.737	-.058	-.030	-.014	-.005	-.014	-.020	-.055
	.777	-.052	-.022	-.008	-.001	-.010	-.016	-.047
	.785	-.054	-.024	-.010	.001	-.008	-.012	-.043
	.817	-.041	-.016	-.004	.004	-.005	-.009	-.037
	.857	-.048	-.024	-.009	.000	-.009	-.013	-.037
	.877	-.048	-.021	-.009	-.001	-.010	-.012	-.035
	.897	-.050	-.024	-.011	-.002	-.011	-.014	-.036
	.917	-.057	-.029	-.016	-.006	-.015	-.019	-.041
	.957	-.063	-.036	-.024	-.015	-.025	-.028	-.050
	.997	-.130	-.105	-.089	-.072	-.087	-.097	-.128

NO 60

	x/l	C_p for - ϕ = -90°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.461	.443	.505	.521	.526	.510	.490	.417
	.481	.105	.145	.161	.161	.145	.131	.086
Upper stage	.489	-.961	-.856	-.699	-.705	-.795	-.793	-.906
	.509	-.137	-.158	-.238	-.187	-.186	-.150	-.162
	.529	.029	.099	.132	.143	.133	.106	.020
Transition flare	.549	.388	.429	.412	.360	.401	.437	.368
	.558	.214	.249	.242	.214	.221	.250	.188
Main stage	.568	-.907	-.961	-1.036	-1.070	-1.041	-.948	-.880
	.587	-.216	-.158	-.141	-.136	-.147	-.167	-.236
	.607	-.131	-.078	-.067	-.067	-.072	-.082	-.134
	.627	-.108	-.061	-.044	-.039	-.050	-.065	-.117
	.657	-.105	-.056	-.035	-.021	-.034	-.049	-.114
	.697	-.099	-.044	-.024	-.011	-.024	-.039	-.104
	.737	-.091	-.036	-.016	-.005	-.016	-.031	-.096
	.777	-.085	-.034	-.010	-.001	-.010	-.027	-.088
	.785	-.089	-.040	-.014	-.001	-.012	-.029	-.088
	.817	-.069	-.024	-.006	.006	-.007	-.019	-.077
	.857	-.073	-.028	-.010	.001	-.010	-.024	-.081
	.897	-.075	-.032	-.014	-.003	-.014	-.027	-.082

TABLE 12.- PRESSURE COEFFICIENTS FOR CONFIGURATION 324 - Continued

(c) M = 0.80; α = -10° to 10°

	x/l	C_p for - $\phi = 0^\circ$						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.461	.816	.733	.669	.608	.535	.468	.366
	.471	.668	.581	.520	.459	.394	.326	.235
	.481	.452	.376	.315	.273	.216	.159	.072
Upper stage	.489	-1.153	-1.037	-.582	-.431	-.490	-.540	-.428
	.494	-.723	-.767	-.579	-.435	-.379	-.377	-.363
	.499	-.358	-.513	-.549	-.427	-.391	-.396	-.386
	.509	.025	-.145	-.376	-.393	-.376	-.396	-.428
	.519	.121	.062	-.112	-.278	-.280	-.265	-.309
	.529	.228	.200	.099	-.144	-.161	-.120	-.152
	.539	.412	.365	.249	-.013	-.046	-.012	-.033
	.549	.665	.537	.402	.129	.046	.068	.067
Transition flare	.554	.059	.061	.049	.040	.038	.048	.043
	.558	.512	.450	.377	.232	.079	.041	.043
Main stage	.568	-1.137	-1.595	-1.426	-.999	-.759	-.687	-.711
	.577	-.600	-.410	-.391	-.239	-.230	-.235	-.225
	.587	-.121	-.126	-.146	-.128	-.146	-.158	-.152
	.597	-.037	-.072	-.085	-.086	-.103	-.112	-.098
	.607	-.013	-.046	-.058	-.063	-.077	-.081	-.071
	.617	-.010	-.034	-.047	-.052	-.061	-.062	-.052
	.627	.002	-.023	-.035	-.040	-.050	-.047	-.037
	.637	.013	-.011	-.027	-.029	-.038	-.035	-.025
	.657	.021	-.003	-.018	-.022	-.028	-.024	-.018
	.677	.026	-.001	-.014	-.018	-.021	-.017	-.014
	.697	.030	.005	-.010	-.014	-.016	-.011	-.014
	.737	.031	.006	-.007	-.014	-.013	-.009	-.017
	.777	.038	.012	-.001	-.007	-.008	-.005	-.015
	.785	.048	.019	.004	.000	-.002	.001	-.009
	.817	.042	.018	.004	-.002	-.004	-.002	-.013
	.857	.035	.012	-.001	-.005	-.007	-.007	-.022
	.877	.037	.014	.000	-.005	-.007	-.006	-.023
	.897	.033	.011	-.003	-.008	-.009	-.010	-.027

NO

	x/l	C_p for - $\phi = -30^\circ$						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.461	.775	.715	.657	.60[illegible]	.543	.475	.366
	.471	.597	.536	.485	.441	.383	.321	.222
	.481	.418	.358	.312	.273	.223	.167	.079
Upper stage	.489	-1.081	-.900	-.631	-.420	-.327	-.320	-.333
	.494	-.723	-.724	-.552	-.393	-.314	-.327	-.340
	.499	-.512	-.621	-.526	-.393	-.337	-.365	-.382
	.509	-.006	-.195	-.380	-.381	-.353	-.388	-.409
	.519	.102	.050	-.150	-.301	-.287	-.281	-.324
	.529	.198	.185	.053	-.182	-.180	-.150	-.194
	.539	.385	.350	.222	-.036	-.069	-.039	-.071
	.549	.631	.541	.379	.106	.019	.045	.028
Transition flare	.554	.602	.544	.437	.217	.072	.067	.047
	.558	.523	.476	.400	.217	.019	.018	-.010
Main stage	.568	-1.639	-1.468	-1.285	-.845	-.563	-.783	-.865
	.577	-.481	-.506	-.395	-.220	-.218	-.254	-.489
	.587	-.140	-.145	-.146	-.132	-.149	-.162	-.232
	.597	-.040	-.053	-.062	-.059	-.077	-.081	-.087
	.607	-.040	-.049	-.058	-.063	-.077	-.081	-.079
	.617	-.033	-.038	-.047	-.052	-.061	-.062	-.060
	.627	-.025	-.030	-.039	-.040	-.050	-.051	-.056
	.637	-.013	-.023	-.027	-.032	-.038	-.039	-.048
	.657	-.007	-.016	-.023	-.024	-.031	-.031	-.044
	.677	.008	-.002	-.011	-.012	-.019	-.018	-.033
	.697	.002	-.006	-.012	-.015	-.017	-.017	-.033
	.737	.006	-.002	-.008	-.009	-.014	-.011	-.033
	.777	.017	.008	.000	-.004	-.006	-.006	-.028
	.785	.015	.006	.000	-.001	-.003	-.003	-.024
	.817	.015	.008	.001	-.002	-.004	-.006	-.026
	.857	.009	.002	-.004	-.006	-.008	-.010	-.030
	.877	.008	.002	-.004	-.007	-.009	-.011	-.032
	.897	.006	.001	-.007	-.008	-.010	-.013	-.035
	.917	.005	-.001	-.007	-.009	-.012	-.015	-.039
	.957	-.008	-.012	-.017	-.021	-.024	-.029	-.052
	.997	-.094	-.084	-.079	-.083	-.091	-.102	-.130

TABLE 12.- PRESSURE COEFFICIENTS FOR CONFIGURATION 324 - Continued

(c) M = 0.80; α = -10° to 10° - Concluded

NC 80

	x/l	C_p for - ϕ = -60°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.461	.653	.655	.628	.608	.561	.501	.403
	.471	.511	.503	.479	.452	.416	.364	.273
	.481	.322	.309	.293	.273	.238	.193	.113
Upper stage	.489	-.811	-.634	-.513	-.386	-.372	-.540	-.572
	.494	-.646	-.602	-.491	-.347	-.322	-.407	-.489
	.499	-.566	-.598	-.495	-.358	-.345	-.426	-.474
	.509	-.228	-.333	-.414	-.354	-.349	-.400	-.435
	.519	.014	-.053	-.208	-.301	-.291	-.265	-.309
	.529	.113	.131	-.016	-.201	-.195	-.131	-.144
	.539	.286	.288	.149	-.086	-.084	-.016	-.010
	.549	.504	.468	.314	.041	.019	.107	.140
Transition flare	.554	.474	.480	.407	.206	.151	.199	.239
Main stage	.568	-1.152	-1.108	-1.162	-.776	-.782	-1.013	-.765
	.577	-.734	-.640	-.414	-.205	-.222	-.426	-.673
	.587	-.205	-.222	-.146	-.128	-.146	-.181	-.412
	.597	-.125	-.099	-.085	-.086	-.096	-.104	-.209
	.607	-.109	-.065	-.062	-.063	-.077	-.081	-.121
	.617	-.090	-.053	-.050	-.052	-.061	-.066	-.094
	.627	-.086	-.049	-.043	-.040	-.050	-.058	-.087
	.637	-.075	-.042	-.035	-.032	-.038	-.051	-.079
	.657	-.073	-.038	-.029	-.024	-.029	-.044	-.078
	.677	-.058	-.028	-.021	-.019	-.024	-.039	-.072
	.697	-.043	-.018	-.012	-.014	-.019	-.033	-.066
	.737	-.054	-.024	-.014	-.009	-.013	-.025	-.054
	.777	-.050	-.020	-.008	-.005	-.008	-.020	-.047
	.785	-.054	-.020	-.008	-.004	-.008	-.017	-.044
	.817	-.041	-.012	-.003	-.002	-.005	-.013	-.039
	.857	-.048	-.020	-.009	-.006	-.009	-.018	-.039
	.877	-.047	-.016	-.008	-.007	-.009	-.017	-.038
	.897	-.047	-.019	-.011	-.007	-.011	-.018	-.039
	.917	-.058	-.024	-.016	-.013	-.016	-.023	-.044
	.957	-.063	-.031	-.022	-.022	-.025	-.032	-.055
	.997	-.134	-.104	-.090	-.085	-.093	-.106	-.135

	x/l	C_p for - ϕ = -90°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.461	.519	.577	.594	.608	.587	.561	.496
	.481	.210	.253	.267	.277	.268	.241	.187
Upper stage	.489	-.648	-.665	-.525	-.370	-.448	-.571	-.717
	.509	-.424	-.391	-.414	-.339	-.379	-.411	-.428
	.529	-.010	-.007	-.127	-.213	-.184	-.066	-.041
	.549	.378	.365	.207	.002	.115	.298	.339
Transition flare	.558	.293	.337	.294	.093	.219	.316	.262
Main stage	.568	-.876	-1.008	-1.131	-.665	-1.065	-1.032	-.888
	.587	-.408	-.245	-.146	-.132	-.142	-.235	-.424
	.607	-.125	-.076	-.066	-.063	-.069	-.081	-.136
	.627	-.102	-.053	-.043	-.040	-.046	-.062	-.117
	.657	-.105	-.050	-.031	-.026	-.031	-.054	-.121
	.697	-.098	-.039	-.023	-.016	-.023	-.044	-.109
	.737	-.085	-.032	-.015	-.009	-.014	-.035	-.100
	.777	-.080	-.028	-.011	-.007	-.010	-.031	-.095
	.785	-.085	-.031	-.012	-.008	-.010	-.031	-.092
	.817	-.068	-.020	-.004	.000	-.004	-.023	-.079
	.857	-.071	-.025	-.009	-.006	-.009	-.028	-.083
	.897	-.073	-.028	-.013	-.009	-.013	-.031	-.086

TABLE 12.- PRESSURE COEFFICIENTS FOR CONFIGURATION 324 - Continued

(d) M = 1.00; $\alpha = -10^\circ$ to 10°

	x/l	C_p for - $\phi = 0^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.461	.945	.869	.805	.742	.677	.610	.515
	.471	.812	.730	.669	.609	.544	.486	.397
	.481	.638	.558	.501	.452	.393	.344	.273
Upper stage	.489	-.823	-.847	-.860	-.867	-.390	-.355	-.277
	.494	-.796	-.875	-.883	-.683	-.378	-.355	-.258
	.499	-.611	-.738	-.639	-.491	-.387	-.361	-.292
	.509	-.156	-.189	-.291	-.372	-.369	-.374	-.344
	.519	.130	-.119	-.200	-.284	-.292	-.310	-.322
	.529	.322	.201	.017	-.143	-.201	-.185	-.243
	.539	.560	.469	.236	-.012	-.131	-.087	-.121
	.549	.795	.600	.379	.107	-.073	-.038	.031
Transition flare	.554	.080	.084	.073	.063	.057	.061	.067
	.558	.713	.732	.659	.282	-.055	-.057	.079
Main stage	.568	-.992	-1.000	-.974	-.866	-.606	-.593	-.636
	.577	-.653	-.702	-.657	-.491	-.335	-.327	-.283
	.587	-.364	-.455	-.456	-.348	-.295	-.303	-.316
	.597	-.245	-.330	-.334	-.268	-.265	-.279	-.295
	.607	-.196	-.260	-.255	-.217	-.234	-.246	-.237
	.617	-.178	-.220	-.203	-.180	-.207	-.212	-.185
	.627	-.169	-.192	-.157	-.149	-.180	-.182	-.149
	.637	-.150	-.141	-.121	-.125	-.158	-.157	-.124
	.657	-.158	-.098	-.098	-.104	-.124	-.123	-.098
	.677	-.075	-.084	-.086	-.089	-.101	-.098	-.081
	.697	-.059	-.072	-.074	-.074	-.084	-.080	-.068
	.737	-.043	-.058	-.064	-.065	-.065	-.060	-.059
	.777	-.021	-.037	- 044	-.046	-.034	-.048	-.051
	.785	-.004	-.023	-.026	-.031	-.019	-.040	-.037
	.817	-.001	-.018	-.010	.027	-.005	-.031	-.029
	.857	-.001	.031	.025	.029	.015	-.003	-.001
	.877	.051	.045	.033	.030	.020	.014	.012
	.897	.061	.041	.031	.027	.017	.020	.015

	x/l	C_p for - $\phi = -30^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	.461	.904	.845	.794	.739	.677	.616	.524
	.471	.753	.694	.646	.594	.537	.483	.398
	.481	.602	.544	.498	.449	.396	.350	.273
Upper stage	.489	-.929	-.958	-.936	-.635	-.477	-.364	-.307
	.494	-.842	-.903	-.529	-.451	-.399	-.331	-.301
	.499	-.583	-.543	-.483	-.442	-.414	-.364	-.335
	.509	-.239	-.339	-.389	-.418	-.384	-.392	-.380
	.519	.057	-.147	-.267	-.342	-.305	-.322	-.362
	.529	.270	.113	-.133	-.235	-.213	-.212	-.292
	.539	.514	.402	.142	-.098	-.137	-.121	-.191
	.549	.743	.585	.337	.043	-.076	-.090	-.152
Transition flare	.554	.807	.726	.524	.159	-.042	-.057	-.100
	.558	.725	.747	.518	.198	-.030	-.078	-.100
Main stage	.568	-1.019	-1.019	-.904	-.732	-.676	-.727	-1.011
	.577	-.678	-.702	-.584	-.412	-.341	-.70	-.527
	.587	-.409	-.479	-.444	-.338	-.301	-.334	-.405
	.597	-.205	-.256	-.249	-.198	-.198	-.218	-.246
	.607	-.230	-.272	-.258	-.220	-.234	-.255	-.243
	.617	-.214	-.229	-.203	-.183	-.207	-.215	-.194
	.627	-.205	-.196	-.166	-.156	-.183	-.188	-.170
	.637	-.193	-.147	-.130	-.131	-.158	-.160	-.149
	.657	-.163	-.111	-.105	-.107	-.125	-.132	-.129
	.677	-.094	-.085	-.083	-.083	-.097	-.101	-.107
	.697	-.091	-.083	-.078	-.075	-.085	-.087	-.102
	.737	-.072	-.066	-.066	-.062	-.063	-.064	-.093
	.777	-.041	-.040	-.039	-.040	-.032	-.050	-.087
	.785	-.035	-.033	-.026	-.030	-.019	-.045	-.080
	.817	-.028	-.026	-.012	.028	-.007	-.039	-.069
	.857	-.026	.021	.020	.029	.015	-.011	-.038
	.877	.024	.032	.028	.029	.018	.007	-.018
	.897	.035	.031	.028	.026	.017	.015	-.010
	.917	.041	.031	.028	.025	.014	.017	-.009
	.957	.034	.020	.017	.009	-.004	.002	-.017
	.997	-.029	-.053	-.070	-.102	-.126	-.130	-.144

TABLE 12.- PRESSURE COEFFICIENTS FOR CONFIGURATION 324 - Continued

(d) M = 1.00; α = -10° to 10° - Concluded

NO 100

	x/l	C_p for - $\beta = -60°$						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.461	.791	.789	.770	.736	.698	.649	.554
	.471	.664	.656	.634	.603	.568	.522	.438
	.481	.513	.496	.474	.446	.414	.380	.305
Upper stage	.489	-.862	-.859	-.706	-.499	-.613	-.606	-.561
	.494	-.525	-.540	-.496	-.418	-.420	-.370	-.350
	.499	-.504	-.507	-.474	-.409	-.436	-.398	-.380
	.509	-.403	-.412	-.389	-.381	-.420	-.425	-.414
	.519	-.153	-.269	-.282	-.314	-.305	-.328	-.368
	.529	.091	-.034	-.163	-.229	-.176	-.175	-.231
	.539	.377	.195	-.044	-.146	-.109	-.117	-.139
	.549	.575	.414	.111	-.040	-.045	-.093	-.106
Transition flare	.554	.665	.609	.353	.105	.012	.043	.238
Main stage	.568	-1.031	-1.004	-.840	-.671	-.759	-.889	-1.051
	.577	-.745	-.702	-.505	-.348	-.390	-.544	-.853
	.587	-.519	-.516	-.401	-.311	-.326	-.416	-.713
	.597	-.382	-.388	-.328	-.265	-.283	-.331	-.493
	.607	-.333	-.299	-.258	-.220	-.241	-.258	-.277
	.617	-.315	-.235	-.209	-.186	-.207	-.215	-.216
	.627	-.315	-.192	-.175	-.159	-.183	-.188	-.200
	.637	-.275	-.156	-.145	-.134	-.158	-.166	-.191
	.657	-.195	-.134	-.113	-.111	-.124	-.146	-.190
	.677	-.167	-.113	-.096	-.093	-.106	-.126	-.165
	.697	-.139	-.093	-.078	-.075	-.087	-.107	-.140
	.737	-.133	-.085	-.068	-.061	-.067	-.083	-.113
	.777	-.113	-.064	-.046	-.042	-.037	-.064	-.094
	.785	-.112	-.061	-.035	-.036	-.024	-.061	-.088
	.817	-.087	-.043	-.013	.027	-.006	-.050	-.069
	.857	-.071	.006	.017	.029	.015	-.024	-.036
	.877	-.024	.014	.024	.029	.019	.003	-.010
	.897	-.016	.013	.025	.027	.017	.013	-.003
	.917	-.019	.006	.019	.021	.010	.013	-.003
	.957	-.019	.002	.012	.009	-.003	.001	-.012
	.997	-.095	-.087	-.088	-.106	-.122	-.127	-.148

	x/l	C_p for - $\beta = -30°$						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.461	.658	.715	.737	.739	.727	.705	.639
	.481	.398	.437	.451	.452	.441	.427	.379
Upper stage	.489	-.629	-.693	-.621	-.523	-.825	-.899	-.918
	.509	-.455	-.418	-.389	-.360	-.350	-.355	-.365
	.529	-.129	-.159	-.191	-.229	-.164	-.136	-.146
	.549	.335	.143	-.005	-.061	-.012	.069	.284
Transition flare	.558	.470	.432	.172	.042	.114	.308	.430
Main stage	.568	-1.068	-.982	-.804	-.668	-.798	-.959	-1.063
	.587	-.635	-.522	-.365	-.290	-.369	-.508	-.655
	.607	-.440	-.278	-.249	-.217	-.247	-.279	-.457
	.627	-.257	-.183	-.175	-.159	-.173	-.188	-.264
	.657	-.227	-.151	-.122	-.116	-.124	-.154	-.230
	.697	-.191	-.114	-.087	-.079	-.089	-.120	-.191
	.737	-.167	-.094	-.069	-.062	-.069	-.098	-.167
	.777	-.141	-.075	-.048	-.045	-.043	-.080	-.147
	.785	-.151	-.076	-.038	-.038	-.034	-.074	-.140
	.817	-.105	-.049	-.011	.026	-.008	-.060	-.112
	.857	-.070	.000	.017	.029	.015	-.053	-.101
	.897	-.040	.002	.021	.027	.015	.002	-.039

TABLE 12.- PRESSURE COEFFICIENTS FOR CONFIGURATION 324 - Continued

(e) M = 1.20; α = -10° to 10°

	x/l	C_p for - ϕ = 0°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.461	1.068	.992	.929	.872	.803	.740	.646
	.471	.950	.869	.813	.756	.696	.632	.543
	.481	.797	.724	.674	.625	.572	.519	.448
	.489	-.468	-.489	-.499	-.510	-.521	-.416	-.477
Upper stage	.494	-.481	-.550	-.588	-.617	-.571	-.313	-.349
	.499	-.348	-.442	-.498	-.547	-.430	-.303	-.311
	.509	-.142	-.268	-.344	-.403	-.189	-.259	-.270
	.519	-.052	-.143	-.192	.045	-.072	-.170	-.240
	.529	.236	.315	.245	.110	.034	-.053	-.164
	.539	.583	.448	.332	.197	.102	.047	-.053
	.549	.654	.516	.418	.292	.145	.102	.020
Transition flare	.554	.093	.075	.070	.073	.063	.068	.073
	.558	.959	.938	.877	.717	.175	.089	.036
Main stage	.568	-.614	-.607	-.604	-.609	-.588	-.455	-.539
	.577	-.361	-.398	-.425	-.438	-.235	-.181	-.210
	.587	-.177	-.255	-.295	-.316	-.194	-.189	-.213
	.597	-.109	-.187	-.225	-.235	-.183	-.189	-.216
	.607	-.066	-.138	-.168	-.151	-.167	-.172	-.189
	.617	-.052	-.113	-.132	-.113	-.148	-.148	-.143
	.627	-.038	-.094	-.111	-.091	-.124	-.118	-.099
	.637	-.028	-.075	-.084	-.069	-.099	-.091	-.064
	.657	-.038	-.076	-.070	-.065	-.069	-.057	-.037
	.677	-.044	-.036	-.042	-.046	-.051	-.032	-.024
	.697	-.031	-.034	-.037	-.031	-.033	-.023	-.022
	.737	-.015	-.024	-.026	-.035	-.035	-.029	-.013
	.777	.018	-.015	-.030	-.022	-.029	-.020	-.023
	.785	.028	-.006	-.017	-.012	-.021	-.009	-.010
	.817	.021	-.003	-.004	-.020	-.019	-.012	-.008
	.857	.021	.007	-.009	-.003	-.004	-.008	-.019
	.877	.032	-.004	-.004	.002	-.007	-.009	-.018
	.897	.013	-.002	-.001	-.005	-.009	-.017	-.022

NO 180

	x/l	C_p for - ϕ = -30°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.461	1.029	.971	.921	.869	.811	.751	.651
	.471	.896	.841	.795	.746	.693	.638	.550
	.481	.763	.711	.669	.622	.575	.525	.448
	.489	-.573	-.594	-.610	-.625	-.631	-.580	-.316
Upper stage	.494	-.524	-.575	-.610	-.639	-.525	-.373	-.216
	.499	-.386	-.472	-.528	-.571	-.362	-.322	-.227
	.509	-.152	-.255	-.311	-.243	-.189	-.243	-.248
	.519	-.052	-.124	-.029	-.012	-.067	-.148	-.235
	.529	.233	.299	.201	.061	.036	-.040	-.175
	.539	.523	.394	.261	.140	.102	.034	-.056
	.549	.629	.483	.372	.273	.140	.039	.064
Transition flare	.554	.913	.778	.642	.365	.183	.084	.129
	.558	.956	.882	.743	.546	.137	.063	.041
Main stage	.568	-.635	-.615	-.577	-.555	-.509	-.558	-.653
	.577	-.378	-.396	-.385	-.384	-.221	-.275	-.284
	.587	-.212	-.268	-.295	-.297	-.202	-.224	-.240
	.597	-.087	-.135	-.162	-.151	-.132	-.140	-.154
	.607	-.098	-.151	-.176	-.159	-.170	-.181	-.191
	.617	-.082	-.124	-.135	-.118	-.148	-.151	-.151
	.627	-.074	-.111	-.111	-.094	-.129	-.129	-.116
	.637	-.063	-.092	-.084	-.075	-.102	-.096	-.088
	.657	-.070	-.059	-.056	-.051	-.068	-.067	-.067
	.677	-.067	-.035	-.038	-.037	-.049	-.042	-.053
	.697	-.061	-.046	-.039	-.040	-.040	-.038	-.054
	.737	-.044	-.037	-.030	-.033	-.034	-.040	-.048
	.777	-.007	-.021	-.025	-.014	-.026	-.029	-.056
	.785	-.002	-.016	-.016	-.006	-.014	-.015	-.050
	.817	-.004	-.015	-.007	-.018	-.018	-.022	-.054
	.857	-.008	.001	-.008	-.010	-.009	-.019	-.054
	.877	.002	-.015	-.008	-.001	-.008	-.018	-.051
	.897	-.012	-.012	-.004	-.002	-.006	-.019	-.043
	.917	-.008	-.004	-.004	-.006	-.010	-.017	-.036
	.957	-.012	-.016	-.012	-.017	-.016	-.018	-.032
	.997	.000	-.022	-.034	-.047	-.068	-.090	-.080

TABLE 12.- PRESSURE COEFFICIENTS FOR CONFIGURATION 324 - Concluded

(e) M = 1.20; α = -10° to 10° - Concluded

	x/l	C_p for - ϕ = -60°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.461	.910	.916	.895	.869	.830	.777	.682
	.471	.802	.795	.777	.751	.714	.669	.580
	.481	.671	.663	.645	.622	.590	.554	.477
Upper stage	.489	-.530	-.532	-.537	-.550	-.561	-.555	-.448
	.494	-.573	-.599	-.618	-.633	-.609	-.495	-.219
	.499	-.410	-.477	-.501	-.552	-.452	-.322	-.224
	.509	-.182	-.236	-.211	-.126	-.159	-.221	-.238
	.519	-.112	-.113	-.062	-.026	-.064	-.151	-.213
	.529	.157	.190	.087	.053	.026	-.067	-.140
	.539	.382	.285	.172	.107	.066	-.010	-.015
Transition flare	.549	.442	.337	.264	.170	.112	.069	-.078
	.554	.750	.639	.465	.234	.319	.327	.399
Main stage	.568	-.652	-.615	-.555	-.517	-.569	-.604	-.691
	.577	-.454	-.423	-.366	-.254	-.324	-.452	-.593
	.587	-.302	-.306	-.287	-.216	-.243	-.360	-.517
	.597	-.226	-.241	-.230	-.189	-.189	-.265	-.389
	.607	-.185	-.195	-.178	-.161	-.162	-.183	-.229
	.617	-.174	-.168	-.138	-.140	-.135	-.145	-.170
	.627	-.171	-.143	-.111	-.121	-.118	-.126	-.140
	.637	-.152	-.105	-.084	-.091	-.094	-.096	-.126
	.657	-.174	-.067	-.056	-.053	-.058	-.079	-.119
	.677	-.142	-.067	-.051	-.047	-.055	-.072	-.108
	.697	-.110	-.066	-.044	-.041	-.052	-.065	-.097
	.737	-.110	-.058	-.034	-.034	-.036	-.063	-.071
	.777	-.076	-.047	-.032	-.017	-.030	-.046	-.058
	.785	-.064	-.044	-.023	-.010	-.021	-.034	-.057
	.817	-.058	-.025	-.012	-.017	-.018	-.035	-.048
	.857	-.066	-.020	-.014	-.011	-.021	-.033	-.045
	.877	-.055	-.033	-.009	-.004	-.008	-.023	-.040
	.897	-.066	-.029	-.011	-.001	-.004	-.019	-.030
	.917	-.070	-.032	-.017	-.008	-.011	-.023	-.027
	.957	-.069	-.037	-.015	-.015	-.019	-.021	-.029
	.997	-.060	-.047	-.041	-.054	-.062	-.086	-.105

NO 120

	x/l	C_p for - ϕ = -90°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
Nose	.461	.779	.840	.863	.867	.859	.835	.769
	.481	.560	.606	.621	.622	.617	.596	.546
Upper stage	.489	-.606	-.605	-.602	-.598	-.598	-.596	-.593
	.509	-.261	-.246	-.222	-.132	-.189	-.210	-.194
	.529	-.033	.017	-.005	.056	.061	.061	.031
Transition flare	.549	.236	.193	.136	.164	.218	.243	.205
	.558	.665	.602	.380	.236	.490	.616	.621
Main stage	.568	-.682	-.621	-.566	-.547	-.569	-.617	-.682
	.587	-.410	-.355	-.263	-.180	-.308	-.365	-.441
	.607	-.296	-.227	-.162	-.161	-.173	-.243	-.316
	.627	-.261	-.124	-.111	-.132	-.107	-.132	-.276
	.657	-.161	-.080	-.055	-.063	057	-.087	-.154
	.697	-.162	-.091	-.056	-.044	-.062	-.088	-.161
	.737	-.135	-.071	-.042	-.037	-.038	-.074	-.138
	.777	-.096	-.055	-.030	-.022	-.029	-.060	-.110
	.785	-.106	-.058	-.030	-.017	-.028	-.057	-.114
	.817	-.086	-.031	-.010	-.015	-.019	-.044	-.090
	.857	-.087	-.032	-.018	-.010	-.029	-.053	-.087
	.897	-.091	-.040	-.018	-.008	-.008	-.028	-.070

TABLE 13.- PRESSURE COEFFICIENTS FOR CONFIGURATION 133

(a) M = 0.40 to 1.20; $\alpha = 0^\circ$; $\phi = 0^\circ$

	x/l	C_p for -									
		M = 0.40	M = 0.60	M = 0.70	M = 0.75	M = 0.80	M = 0.85	M = 0.90	M = 0.95	M = 1.00	M = 1.20
Nose	.420	.089	.580	.709	.763	.820	.844	.785	.863	.912	1.062
	.430	.209	.234	.251	.259	.272	.273	.304	.328	.377	.307
	.440	.176	.201	.219	.227	.242	.242	.271	.297	.350	.315
	.450	.144	.162	.184	.186	.197	.204	.235	.259	.318	.315
	.470	.045	.061	.086	.093	.100	.113	.152	.184	.246	.307
	.480	-.043	-.040	-.022	-.009	.010	.033	.080	.125	.189	.304
	.485	-.180	-.176	-.158	-.138	-.097	-.055	.004	.062	.135	.291
	.491	-.750	-.888	-1.078	-1.205	-1.116	-.965	-.828	-.713	-.595	-.284
Upper stage	.496	-.202	-.229	-.251	-.311	-.399	-.462	-.485	-.626	-.671	-.366
	.501	-.089	-.097	-.095	-.110	-.179	-.268	-.261	-.219	-.199	-.323
	.511	.024	.029	.043	.050	.053	-.016	-.053	-.081	-.027	-.251
	.521	.126	.144	.167	.175	.184	.171	.144	.055	.060	.114
	.531	.318	.340	.360	.360	.358	.326	.297	.187	.161	.243
Transition flare	.540	.001	.012	.024	.024	.025	.016	.031	.028	.040	.047
	.546	.079	.091	.113	.135	.159	.189	.245	.292	.344	.428
	.552	-.010	.000	.019	.036	.063	.097	.155	.216	.292	.409
	.562	.247	-.258	-.238	-.210	-.160	-.103	-.036	.028	.116	.304
Main stage	.568	-.767	-.953	-1.078	-1.207	-1.281	-1.128	-.981	-.845	-.717	-.397
	.577	-.213	-.224	-.224	-.252	-.256	-.765	-.784	-.648	-.523	-.312
	.587	-.134	-.132	-.123	-.131	-.117	-.131	-.550	-.516	-.403	-.246
	.597	-.100	-.097	-.086	-.093	-.086	-.059	-.097	-.435	-.338	-.207
	.607	-.089	-.074	-.058	-.068	-.067	-.056	-.009	-.371	-.289	-.172
	.617	-.066	-.063	-.049	-.055	-.055	-.056	-.003	-.290	-.243	-.144
	.627	-.066	-.051	-.040	-.047	-.044	-.052	-.006	-.132	-.203	-.122
	.637	-.055	-.040	-.031	-.034	-.032	-.045	-.009	-.026	-.166	-.092
	.657	-.039	-.027	-.019	-.023	-.021	-.035	-.012	.023	-.131	-.073
	.677	-.029	-.023	-.016	-.018	-.019	-.032	-.016	.024	-.105	-.048
	.697	-.021	-.019	-.011	-.014	-.013	-.028	-.015	.015	-.084	-.038
	.737	-.017	-.017	-.008	-.012	-.010	-.027	-.015	-.003	-.069	-.040
	.777	-.015	-.011	-.003	-.006	-.006	-.021	-.010	-.007	-.056	-.025
	.785	-.013	-.009	.002	-.002	-.001	-.017	-.004	-.001	-.048	-.015
	.817	-.012	-.008	.001	-.001	-.002	-.017	-.006	-.006	-.042	-.022
	.857	-.014	-.010	-.003	-.004	-.005	-.021	-.010	-.012	-.035	-.004
	.877	-.014	-.010	-.003	-.004	-.004	-.020	-.009	-.012	-.005	-.001
	.897	-.017	-.014	-.006	-.007	-.008	-.024	-.012	-.016	.025	-.005

TABLE 13.- PRESSURE COEFFICIENTS FOR CONFIGURATION 133 - Continued

(b) M = 0.40 to 1.20; $\alpha = 0^\circ$; $\phi = -30^\circ$

	x/l	C_p for -									
		M = 0.40	M = 0.60	M = 0.70	M = 0.75	M = 0.80	M = 0.85	M = 0.90	M = 0.95	M = 1.00	M = 1.20
Nose	.430	.209	.223	.246	.255	.265	.267	.298	.322	.368	.304
	.440	.166	.189	.210	.223	.231	.235	.268	.290	.344	.310
	.450	.133	.156	.179	.186	.193	.200	.235	.256	.312	.310
	.470	.045	.056	.077	.085	.100	.109	.149	.181	.243	.304
	.480	-.043	-.045	-.026	-.013	.006	.033	.080	.122	.189	.304
	.485	-.178	-.170	-.158	-.138	-.101	-.055	.004	.059	.135	.288
	.491	-.750	-.882	-1.023	-1.110	-1.063	-.944	-.828	-.713	-.598	-.290
Upper stage	.496	-.213	-.241	-.270	-.344	-.426	-.434	-.417	-.397	-.434	-.369
	.501	-.078	-.386	-.095	-.122	-.225	-.326	-.308	-.268	-.209	-.342
	.511	.024	.029	.047	.054	.053	-.041	-.074	-.110	-.073	-.240
	.521	.126	.150	.171	.180	.188	.164	.127	.045	.050	.122
	.531	.318	.334	.350	.351	.351	.301	.273	.171	.143	.240
Transition flare	.540	.180	.204	.236	.247	.265	.285	.329	.378	.444	.422
	.546	.035	.046	.074	.086	.109	.140	.195	.267	.359	.439
	.552	-.010	.000	.019	.036	.063	.097	.152	.206	.268	.406
	.562	-.259	-.270	-.251	-.219	-.171	-.121	-.053	.016	.092	.298
Main stage	.568	-.643	-.769	-1.074	-1.325	-1.277	-1.118	-.964	-.822	-.690	-.386
	.577	-.213	-.224	-.219	-.231	-.225	-.765	-.767	-.622	-.465	-.314
	.587	-.134	-.137	-.127	-.135	-.121	-.117	-.533	-.510	-.381	-.246
	.597	-.100	-.097	-.077	-.084	-.082	-.059	-.070	-.332	-.258	-.152
	.607	-.078	-.074	-.058	-.068	-.067	-.056	-.009	-.368	-.292	-.169
	.617	-.066	-.063	-.049	-.055	-.052	-.056	-.006	-.293	-.252	-.144
	.627	-.066	-.051	-.040	-.047	-.044	-.052	-.009	-.132	-.209	-.125
	.637	-.055	-.040	-.031	-.034	-.036	-.045	-.012	-.029	-.172	-.098
	.657	-.033	-.029	-.023	-.025	-.024	-.037	-.016	.020	-.134	-.066
	.677	-.021	-.017	-.010	-.014	-.012	-.026	-.009	.030	-.099	-.040
	.697	-.021	-.019	-.011	-.015	-.013	-.028	-.015	.014	-.085	-.042
	.737	-.017	-.015	-.006	-.009	-.008	-.025	-.012	-.001	-.068	-.037
	.777	-.013	-.009	-.003	-.006	-.004	-.017	-.005	-.002	-.051	-.020
	.785	-.013	-.006	.002	-.002	-.001	-.016	-.004	-.001	-.047	.009
	.817	-.012	-.008	-.000	-.001	-.002	-.017	-.006	-.006	-.042	-.021
	.857	-.015	-.011	-.004	-.005	-.006	-.021	-.011	-.013	-.039	-.013
	.877	-.015	-.012	-.004	-.006	-.006	-.022	-.012	-.014	-.010	-.004
	.897	-.018	-.014	-.006	-.007	-.008	-.024	-.013	-.017	.023	-.002
	.917	-.018	-.014	-.006	-.008	-.008	-.025	-.013	-.017	.034	-.007
	.957	-.030	-.025	-.018	-.019	-.020	-.036	-.025	-.029	.023	-.017
	.997	-.081	-.080	-.073	-.077	-.077	-.096	-.089	-.104	-.088	-.055

TABLE 13.- PRESSURE COEFFICIENTS FOR CONFIGURATION 133 - Continued

(c) M = 0.40 to 1.20; $\alpha = 0^\circ$; $\phi = -60^\circ$

	x/l	C_p for -									
		M = 0.40	M = 0.60	M = 0.70	M = 0.75	M = 0.80	M = 0.85	M = 0.90	M = 0.95	M = 1.00	M = 1.20
Nose	.430	.198	.223	.246	.259	.268	.267	.301	.325	.371	.304
	.440	.166	.184	.215	.219	.231	.239	.265	.290	.342	.310
	.450	.133	.150	.175	.182	.193	.197	.232	.256	.312	.310
	.470	.034	.056	.077	.085	.100	.109	.149	.181	.243	.310
	.480	-.055	-.051	-.031	-.017	.006	.029	.077	.122	.189	.304
	.485	-.099	-.091	-.081	-.080	-.082	-.098	-.090	-.102	-.115	-.140
	.491	-.750	-.894	-.969	-1.064	-.990	-.872	-.747	-.643	-.525	-.235
Upper stage	.496	-.191	-.218	-.265	-.336	-.419	-.437	-.380	-.342	-.332	-.386
	.501	-.066	-.074	-.095	-.126	-.229	-.311	-.284	-.248	-.209	-.331
	.511	.024	.029	.043	.050	.053	-.041	-.091	-.113	-.070	-.254
	.521	.126	.144	.167	.175	.188	.160	.110	.032	.044	.149
	.531	.330	.351	.350	.351	.351	.297	.253	.155	.140	.232
Transition flare	.540	.180	.204	.232	.243	.261	.282	.322	.327	.368	.366
	.551	.079	.096	.123	.135	.159	.186	.239	.302	.380	.433
	.552	-.010	.000	.019	.036	.063	.097	.152	.197	.244	.398
	.562	-.259	-.270	-.247	-.219	-.171	-.117	-.057	.003	.074	.290
Main stage	.568	-.700	-.873	-1.152	-1.367	-1.277	-1.118	-.974	-.822	-.683	-.364
	.577	-.202	-.224	-.219	-.227	-.225	-.743	-.757	-.593	-.437	-.298
	.587	-.134	-.137	-.127	-.135	-.121	-.117	-.519	-.503	-.391	-.248
	.597	-.100	-.097	-.086	-.089	-.086	-.063	-.091	-.432	-.341	-.207
	.607	-.078	-.074	-.058	-.068	-.067	-.056	-.012	-.368	-.292	-.172
	.617	-.066	-.063	-.049	-.055	-.052	-.056	-.006	-.290	-.252	-.144
	.627	-.066	-.051	-.040	-.047	-.044	-.052	-.012	-.132	-.209	-.122
	.637	-.055	-.045	-.031	-.034	-.036	-.045	-.012	-.032	-.172	-.098
	.657	-.033	-.029	-.021	-.024	-.024	-.036	-.015	.020	-.133	-.053
	.677	-.013	-.006	-.002	-.002	.000	-.013	.002	.023	-.051	-.008
	.697	-.021	-.017	-.010	-.014	-.012	-.027	-.014	.015	-.084	-.044
	.737	-.017	-.015	-.006	-.009	-.008	-.023	-.011	-.001	-.067	-.035
	.777	-.013	-.009	-.003	-.005	-.005	-.018	-.009	-.005	-.053	-.020
	.795	-.013	-.006	-.011	-.003	-.004	-.017	-.006	-.006	-.050	-.010
	.817	-.011	-.007	.001	-.000	-.001	-.016	-.005	-.005	-.041	-.018
	.857	-.015	-.011	-.004	-.005	-.005	-.021	-.010	-.013	-.038	-.018
	.877	-.015	-.012	-.004	-.006	-.006	-.021	-.011	-.014	-.011	-.005
	.897	-.017	-.012	-.005	-.006	-.007	-.023	-.012	-.016	.025	-.001
	.917	-.021	-.018	-.010	-.011	-.012	-.028	-.017	-.020	.031	-.008
	.957	-.028	-.025	-.016	-.019	-.021	-.036	-.025	-.029	.023	-.016
	.997	-.082	-.082	-.075	-.077	-.078	-.098	-.091	-.105	-.090	-.054

TABLE 13.- PRESSURE COEFFICIENTS FOR CONFIGURATION 133 - Concluded

(d) M = 0.40 to 1.20; $\alpha = 0^{\circ}$; $\phi = -90^{\circ}$

	x/l	C_p for -									
		M = 0.40	M = 0.60	M = 0.70	M = 0.75	M = 0.80	M = 0.85	M = 0.90	M = 0.95	M = 1.00	M = 1.20
Nose	.420	.242	.267	.286	.296	.310	.315	.340	.366	.413	.302
	.430	.012	.513	.660	.719	.782	.877	.743	.813	.871	1.012
	.450	.133	.150	.170	.178	.190	.193	.225	.253	.309	.302
	.470	.034	.056	.077	.089	.104	.113	.149	.184	.246	.310
	.485	-.200	-.193	-.181	-.159	-.120	-.080	-.016	.037	.111	.272
	.491	-.772	-.865	-.992	-1.089	-1.017	-.890	-.750	-.643	-.525	-.222
Upper stage	.511	.024	.035	.047	.054	.057	-.041	-.101	-.123	-.064	-.254
	.531	.341	.368	.373	.368	.352	.304	.249	.148	.146	.243
Transition flare	.552	-.010	.000	.019	.032	.063	.097	.152	.197	.277	.406
Main stage	.568	-.767	-.970	-1.166	-1.367	-1.312	-1.150	-.998	-.851	-.726	-.399
	.587	-.134	-.137	.132	-.135	-.121	-.124	-.539	-.513	-.406	-.251
	.607	-.078	-.074	.058	-.068	-.067	-.056	-.012	-.371	-.289	-.172
	.627	-.066	-.051	-.040	-.047	-.044	-.052	-.012	-.126	-.203	-.120
	.657	-.033	-.029	-.023	-.025	-.024	-.037	-.016	.020	-.133	-.081
	.697	-.025	-.019	-.013	-.015	-.015	-.030	-.016	.012	-.087	-.046
	.737	-.017	-.015	-.005	-.009	-.008	-.023	-.011	.000	-.060	-.039
	.777	-.013	-.011	-.001	-.005	-.005	-.019	-.008	-.006	-.053	-.021
	.785	-.013	-.009	-.001	-.006	-.004	-.018	-.009	-.006	-.050	-.017
	.817	-.011	-.005	.002	.000	-.000	-.015	-.003	-.004	-.038	-.012
	.857	-.015	-.011	-.003	-.005	-.005	-.020	-.010	-.013	-.038	-.013
	.897	-.018	-.014	-.005	-.007	-.008	-.023	-.012	-.017	.025	-.007

TABLE 14.- PRESSURE COEFFICIENTS FOR CONFIGURATION 143

(a) M = 0.40 to 1.20; $\alpha = 0^\circ$; $\phi = 0^\circ$

	x/l	C_p for -									
		M = 0.40	M = 0.60	M = 0.70	M = 0.75	M = 0.80	M = 0.85	M = 0.90	M = 0.95	M = 1.00	M = 1.20
Nose	.440	-.257	.393	.561	.634	.705	.765	.827	.871	.928	1.109
	.430	.230	.243	.264	.269	.278	.290	.314	.329	.377	.320
	.460	.197	.215	.237	.237	.248	.259	.281	.304	.353	.330
	.470	.164	.176	.193	.201	.207	.224	.245	.267	.315	.322
	.490	.077	.087	.104	.107	.121	.140	.169	.192	.249	.317
	.500	.000	-.002	.015	.018	.035	.063	.100	.133	.196	.320
	.505	-.112	-.122	-.108	-.098	-.067	-.028	.024	.065	.133	.301
	.511	-.638	-.753	-.852	-.943	-.894	-.823	-.792	-.716	-.606	-.291
	.516	-.113	-.117	-.118	-.136	-.184	-.201	-.182	-.148	-.090	-.359
Upper stage	.521	.046	.050	.061	.056	.021	-.043	-.080	-.087	-.037	-.312
	.531	.305	.314	.318	.299	.256	.173	.103	.064	.085	.155
Transition flare	.540	.011	.021	.029	.027	.028	.032	.032	.028	.039	.050
	.546	.056	.077	.096	.117	.142	.192	.242	.284	.344	.408
	.552	-.022	-.014	.006	.018	.051	.096	.155	.211	.283	.347
	.562	-.259	-.266	-.245	-.215	-.164	-.107	-.032	.031	.114	.232
Main Stage	.568	-.767	-.960	-1.116	-1.340	-1.292	-1.122	-.979	-.857	-.734	-.405
	.577	-.214	-.220	-.228	-.257	-.284	-.820	-.803	-.690	-.575	-.337
	.587	-.135	-.128	-.127	-.136	-.118	-.122	-.660	-.571	-.467	-.255
	.597	-.101	-.094	-.086	-.090	-.087	-.043	-.212	-.491	-.397	-.219
	.607	-.079	-.065	-.063	-.069	-.072	-.039	-.012	-.421	-.338	-.181
	.617	-.067	-.054	-.049	-.052	-.056	-.039	.017	-.353	-.283	-.151
	.627	-.056	-.042	-.035	-.044	-.049	-.035	.017	-.225	-.237	-.127
	.637	-.045	-.036	-.026	-.031	-.037	-.025	.011	-.048	-.191	-.097
	.657	-.019	-.018	-.018	-.020	-.024	-.018	-.006	.027	-.147	-.077
	.667	-.019	-.016	-.013	-.015	-.020	-.016	-.010	.035	-.117	-.051
	.697	-.015	-.010	-.008	-.011	-.014	-.012	-.010	.028	-.093	-.040
	.737	-.011	-.008	-.005	-.008	-.013	-.009	-.011	.006	-.075	-.038
	.777	-.007	-.004	-.001	-.002	-.007	-.004	-.007	-.003	-.062	-.022
	.785	-.003	.003	.005	.003	-.002	.002	.000	.002	-.052	-.014
	.817	-.002	.001	.005	.001	-.003	.001	-.002	-.004	-.048	-.019
	.857	-.005	-.003	.002	-.002	-.007	-.004	-.006	-.011	-.052	-.001
	.877	-.005	-.002	.003	-.001	-.007	-.003	-.006	-.011	-.050	-.002
	.897	-.007	-.004	.000	-.004	-.010	-.006	-.009	-.015	-.049	-.003

TABLE 14.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1-3 - Continued

(c) M = 0.40 to 1.20; α = 0°; φ = -30°

	x/l	C_p for - M = 0.40	M = 0.60	M = 0.70	M = 0.75	M = 0.80	M = 0.85	M = 0.90	M = 0.95	M = 1.00	M = 1.20
Nose	[illegible]	.249	.237	.255	.261	.271	.287	.304	.322	.371	.317
	[illegible]	.137	.196	.284	.223	.241	.255	.275	.295	.344	.327
	[illegible]	.113	.176	.193	.196	.217	.220	.242	.254	.315	.322
	[illegible]	.077	.081	.154	.137	.147	.136	.166	.186	.240	.312
	[illegible]	.000	-.002	.115	.113	.033	.060	.100	.150	.196	.317
	[illegible]	-.112	-.122	-.103	-.098	-.067	-.028	.021	.065	.133	.301
	[illegible]	-.633	-.741	-.807	-.864	-.806	-.727	-.671	-.627	-.539	-.288
Upper stage	[illegible]	-.113	-.128	-.136	-.157	-.164	-.194	-.188	-.154	-.096	-.367
	[illegible]	.146	.030	.057	.036	-.033	-.093	-.110	-.106	-.056	-.249
	.531	.315	.390	.299	.267	.222	.160	.090	.048	.070	.144
Transition flare	[illegible]	.156	.154	.219	.228	.249	.277	.296	.300	.335	.394
	.546	.022	.032	.051	.078	.093	.142	.195	.249	.320	[illegible]
	.552	-.022	-.014	.006	.023	.055	.100	.159	.214	.283	.376
	.562	-.253	-.277	-.250	-.215	-.172	-.107	-.036	.028	.111	.254
Main stage	.565	-.643	-.762	-1.110	-1.352	-1.288	-1.119	-.972	-.841	-.716	-.389
	.577	-.214	-.220	-.223	-.236	-.249	-.827	-.803	-.690	-.575	-.329
	.587	-.135	-.134	-.131	-.136	-.122	-.097	-.660	-.575	-.479	-.263
	.597	-.079	-.071	-.053	-.073	-.068	-.032	-.144	-.379	-.298	-.151
	.607	-.079	-.065	-.063	-.069	-.072	-.039	-.009	-.417	-.335	-.176
	.617	-.056	-.054	-.044	-.052	-.056	-.039	.017	-.353	-.286	-.151
	.627	-.056	-.042	-.035	-.044	-.049	-.035	.014	-.231	-.243	-.129
	.637	-.045	-.036	-.026	-.036	-.041	-.028	.008	-.048	-.197	-.102
	.657	-.023	-.022	-.019	-.023	-.027	-.021	-.009	.023	-.150	-.068
	.687	-.015	-.010	-.008	-.009	-.013	-.009	-.004	.041	-.110	-.044
	.697	-.015	-.012	-.008	-.011	-.016	-.012	-.011	.027	-.094	-.045
	.737	-.007	-.006	-.003	-.005	-.011	-.008	-.009	.006	-.073	-.035
	.777	-.003	.003	.004	.001	-.003	.000	-.004	.001	-.057	-.015
	.795	-.003	.003	.005	.003	-.002	.002	.000	.002	-.051	-.007
	.827	-.002	.001	.005	.001	-.004	.000	-.002	-.004	-.048	-.017
	.857	-.005	-.003	.001	-.003	-.008	-.004	-.007	-.012	-.053	-.009
	.877	-.007	-.004	.001	-.004	-.009	-.005	-.008	-.013	-.053	.001
	.897	-.008	-.006	-.001	-.005	-.010	-.007	-.009	-.015	-.050	.000
	.927	-.008	-.005	-.001	-.006	-.010	-.007	-.009	-.016	-.002	-.004
	.957	-.020	-.016	-.012	-.016	-.021	-.018	-.022	-.027	.028	-.015
	.997	-.070	-.071	-.068	-.073	-.076	-.079	-.087	-.102	-.081	-.048

TABLE 14.- PRESSURE COEFFICIENTS FOR CONFIGURATION 143 - Continued

(c) $\bar{\chi}$ = 0.40 to 1.20; $\alpha = 0^\circ$; $\beta = -60^\circ$

	x/l	C_p for -									
		M = 0.40	M = 0.60	M = 0.70	M = 0.75	M = 0.80	M = 0.85	M = 0.90	M = 0.95	M = 1.00	M = 1.20
Nose	.430	.219	.231	.255	.261	.271	.287	.304	.326	.374	.317
	.460	.186	.196	.224	.229	.241	.255	.275	.295	.344	.322
	.470	.153	.165	.193	.196	.203	.217	.242	.261	.315	.320
	.490	.066	.076	.104	.107	.117	.133	.166	.186	.246	.314
	.500	-.011	-.013	.010	.018	.031	.060	.094	.127	.190	.317
	.505	-.078	-.082	-.076	-.077	-.079	-.082	-.089	-.105	-.113	-.128
	.511	-.626	-.736	-.748	-.810	-.783	-.706	-.634	-.579	-.497	-.231
Upper stage	.516	-.101	-.117	-.127	-.148	-.176	-.194	-.182	-.154	-.093	-.383
	.521	.057	.061	.057	.031	-.029	-.075	-.100	-.097	-.044	-.143
	.531	.328	.325	.286	.257	.214	.152	.087	.048	.073	-.133
Transition flare	.540	.156	.184	.209	.228	.249	.280	.292	.281	.305	.338
	.551	.056	.083	.096	.117	.146	.195	.249	.290	.344	.416
	.552	-.022	-.014	.006	.023	.051	.100	.159	.211	.280	.376
	.562	-.259	-.277	-.255	-.224	-.176	-.115	-.040	.022	.105	.281
Main stage	.568	-.700	-.697	-1.194	-1.411	-1.296	-1.122	-.972	-.841	-.716	-.380
	.577	-.214	-.220	-.223	-.232	-.246	-.798	-.796	-.681	-.562	-.323
	.587	-.135	-.134	-.131	-.136	-.122	-.097	-.660	-.575	-.470	-.260
	.597	-.090	-.088	-.081	-.090	-.087	-.039	-.188	-.491	-.397	-.217
	.607	-.079	-.065	-.058	-.069	-.068	-.039	-.009	-.417	-.335	-.178
	.617	-.056	-.054	-.044	-.052	-.056	-.039	-.017	-.353	-.283	-.148
	.627	-.056	-.042	-.035	-.044	-.049	-.035	.014	-.228	-.243	-.129
	.637	-.045	-.036	-.026	-.036	-.041	-.028	.008	-.052	-.197	-.102
	.657	-.023	-.020	-.019	-.021	-.025	-.021	-.007	.024	-.148	-.057
	.667	-.015	-.002	.002	.003	-.002	.004	.006	.028	-.060	-.010
	.697	-.015	-.010	-.008	-.011	-.014	-.011	-.009	.028	-.092	-.046
	.737	-.007	-.006	-.003	-.005	-.010	-.007	-.009	.007	-.073	-.035
	.777	-.003	.000	-.001	-.002	-.006	-.002	-.005	.000	-.058	-.017
	.785	-.003	-.004	.002	-.002	-.005	-.002	-.004	-.003	-.055	-.008
	.817	-.002	.002	.006	.001	-.003	.001	-.001	-.003	-.046	-.016
	.857	-.005	-.003	.001	-.002	-.008	-.004	-.007	-.012	-.053	-.011
	.877	-.007	-.003	.001	-.003	-.008	-.005	-.007	-.013	-.053	-.001
	.897	-.008	-.004	.000	-.004	-.009	-.006	-.009	-.015	-.048	.001
	.911	-.011	-.009	-.004	-.009	-.013	-.010	-.014	-.020	-.011	-.005
	.957	-.020	-.016	-.013	-.017	-.021	-.019	-.021	-.027	.030	-.013
	.997	-.072	-.073	-.070	-.075	-.079	-.080	-.089	-.104	-.083	-.050

TABLE 14.- PRESSURE COEFFICIENTS FOR CONFIGURATION 143 - Concluded

(d) M = 0.40 to 1.20; $\alpha = 0^{\circ}$; $\phi = -90^{\circ}$

	x/l	C_p for -									
		M = 0.40	M = 0.60	M = 0.70	M = 0.75	M = 0.80	M = 0.85	M = 0.90	M = 0.95	M = 1.00	M = 1.20
Nose	.440	.263	.276	.299	.302	.308	.325	.347	.367	.413	.312
	.430	-.257	.382	.548	.618	.690	.747	.818	.865	.925	1.093
	.470	.153	.165	.184	.192	.200	.213	.238	.258	.312	.314
	.490	.066	.081	.104	.107	.121	.136	.166	.192	.249	.320
	.505	-.145	-.139	-.130	-.118	-.090	-.053	.001	.043	.112	.280
	.511	-.626	-.713	-.775	-.848	-.852	-.756	-.654	-.586	-.494	-.231
Upper stage	.531	.339	.342	.318	.295	.253	.163	.093	.054	.079	.149
Transition flare	.552	-.022	-.014	.006	.018	.051	.100	.155	.211	.280	.378
Main stage	.568	-.790	-.994	-1.208	-1.432	-1.323	-1.151	-.999	-.867	-.740	-.410
	.587	-.135	-.134	-.131	-.136	-.122	-.104	-.667	-.584	-.476	-.263
	.607	-.079	-.065	-.058	-.069	-.068	-.039	-.009	-.417	-.335	-.178
	.627	-.056	-.042	-.035	-.044	-.049	-.035	-.014	-.225	-.237	-.127
	.657	-.023	-.022	-.019	-.021	-.027	-.022	-.009	.023	-.149	-.058
	.697	-.015	-.012	-.010	-.012	-.017	-.013	-.012	.026	-.094	-.044
	.737	-.007	-.006	-.003	-.005	-.009	-.005	-.009	.008	-.072	-.039
	.777	-.003	-.006	.000	-.002	-.006	-.003	-.005	-.001	-.058	-.019
	.785	-.003	-.002	-.008	-.002	-.007	-.002	-.005	-.004	-.056	-.013
	.817	-.001	.003	.007	.003	-.002	.001	.000	-.001	-.044	-.011
	.857	-.005	-.003	.002	-.002	-.007	-.004	-.007	-.011	-.052	-.007
	.897	-.008	-.005	-.001	-.005	-.010	-.007	-.009	-.015	-.048	-.005

TABLE 15.- PRESSURE COEFFICIENTS FOR CONFIGURATION 153

(a) M = 0.40 to 1.20; $\alpha = 0^\circ$; $\phi = 0^\circ$

	x/l	C_p for -									
		M = 0.40	M = 0.60	M = 0.70	M = 0.75	M = 0.80	M = 0.85	M = 0.90	M = 0.95	M = 1.00	M = 1.20
Nose	.461	-.555	.260	.446	.532	.601	.658	.720	.778	.833	1.015
	.471	.242	.255	.273	.277	.287	.306	.320	.346	.397	.325
	.481	.199	.233	.237	.249	.265	.278	.294	.321	.370	.325
	.491	.177	.199	.211	.220	.231	.250	.265	.296	.344	.317
	.511	.133	.144	.153	.164	.175	.195	.215	.247	.299	.325
	.521	.090	.110	.122	.135	.141	.167	.186	.222	.278	.325
	.525	.068	.094	.109	.115	.130	.153	.176	.216	.269	.330
	.532	.068	.088	.104	.111	.126	.153	.176	.216	.275	.346
Upper stage											
Transition flare	.539	.014	.016	.025	.031	.030	.035	.033	.033	.039	.051
	.546	-.009	-.006	.011	.022	.041	.074	.109	.156	.216	.319
	.552	-.076	-.069	-.053	-.036	-.008	.028	.069	.125	.186	.317
	.562	-.290	-.298	-.268	-.224	-.174	-.104	-.038	.033	.102	.293
Main stage	.568	-.763	-.950	-1.214	-1.471	-1.317	-1.145	-.996	-.863	-.738	-.400
	.577	-.234	-.241	-.281	-.361	-.474	-.886	-.888	-.776	-.662	-.351
	.587	-.144	-.138	-.144	-.148	-.178	-.291	-.740	-.655	-.551	-.291
	.597	-.110	-.098	-.094	-.090	-.077	-.090	-.402	-.568	-.475	-.245
	.607	-.087	-.069	-.071	-.069	-.054	-.018	-.092	-.488	-.401	-.209
	.617	-.076	-.058	-.053	-.052	-.050	-.014	.009	-.411	-.337	-.177
	.627	-.065	-.046	-.043	-.044	-.043	-.018	.031	-.328	-.279	-.150
	.637	-.053	-.035	-.034	-.032	-.031	-.018	.025	-.126	-.224	-.114
	.657	-.032	-.018	-.022	-.021	-.022	-.014	.009	.035	-.165	-.090
	.677	-.028	-.014	-.017	-.017	-.018	-.013	-.003	.057	-.125	-.058
	.697	-.024	-.008	-.010	-.012	-.014	-.009	-.007	.050	-.096	-.040
	.737	-.020	-.006	-.008	-.011	-.011	-.007	-.009	.021	-.074	-.040
	.777	-.016	-.002	-.002	-.005	-.005	-.002	-.007	.008	-.057	-.022
	.785	-.012	.004	.003	.001	.002	.004	-.001	.013	-.048	-.014
	.817	-.011	.003	.002	.001	-.001	.004	-.003	.004	-.043	-.019
	.857	-.012	-.001	-.002	-.003	-.004	.000	-.008	-.004	-.040	.000
	.877	-.012	-.001	-.001	-.002	-.004	.000	-.007	-.004	.012	.003
	.897	-.015	-.002	-.004	-.005	-.007	-.003	-.011	-.008	.033	-.004

TABLE 15.- PRESSURE COEFFICIENTS FOR CONFIGURATION 153 - Continued

(b) $M = 0.40$ to 1.20; $\alpha = 0°$; $\beta = -30°$

	x/l	C_p for -									
		M = 0.40	M = 0.60	M = 0.70	M = 0.75	M = 0.80	M = 0.85	M = 0.90	M = 0.95	M = 1.00	M = 1.20
Nose	.471	.221	.244	.264	.269	.280	.296	.314	.343	.368	.315
	.481	.199	.216	.228	.236	.250	.264	.281	.312	.361	.309
	.491	.166	.179	.206	.216	.227	.244	.261	.296	.341	.315
	.511	.122	.138	.149	.160	.171	.191	.209	.247	.299	.320
	.521	.096	.106	.117	.131	.138	.163	.186	.222	.278	.325
	.526	.068	.088	.100	.107	.123	.146	.170	.210	.266	.325
	.532	.057	.066	.082	.091	.104	.132	.153	.191	.252	.309
Upper stage											
Transition flare	.539	.025	.033	.052	.063	.075	.106	.136	.178	.234	.322
	.546	-.042	-.035	-.016	.002	.022	.057	.096	.147	.210	.336
	.552	-.076	-.069	-.053	-.036	-.008	.032	.073	.125	.186	.319
	.562	-.298	-.298	-.268	-.219	-.166	-.101	-.034	.036	.105	.295
Main stage	.566	-.650	-.779	-1.050	-1.325	-1.344	-1.173	-1.016	-.885	-.763	-.[illegible]
	.577	-.234	-.235	-.281	-.382	-.433	-.836	-.888	-.716	-.562	-.35[illegible]
	.587	-.144	-.138	-.144	-.148	-.185	-.294	-.763	-.671	-.564	-.294
	.597	-.099	-.078	-.075	-.069	-.088	-.165	-.287	-.443	-.365	-.177
	.607	-.087	-.069	-.071	-.069	-.064	-.018	-.081	-.479	-.395	-.204
	.617	-.076	-.068	-.053	-.052	-.050	-.014	.015	-.408	-.337	-.174
	.627	-.065	-.046	-.048	-.044	-.043	-.022	.031	-.331	-.282	-.150
	.637	-.053	-.035	-.034	-.036	-.035	-.022	.022	-.126	-.230	-.117
	.657	-.036	-.020	-.023	-.024	-.025	-.018	.006	.035	-.166	-.076
	.677	-.024	-.008	-.010	-.011	-.011	-.005	.003	.061	-.118	-.055
	.697	-.024	-.010	-.012	-.012	-.014	-.010	-.008	.049	-.096	-.050
	.737	-.016	-.004	-.005	-.006	-.008	-.005	-.008	.022	-.071	-.038
	.777	-.012	.000	.001	-.001	.000	.002	-.002	.013	-.052	-.014
	.795	-.012	.004	.003	.001	.002	.004	.000	.013	-.046	-.008
	.817	-.011	.003	.001	.001	-.001	.003	-.003	.004	-.043	-.017
	.857	-.014	-.002	-.003	-.003	-.005	-.001	-.008	-.006	-.042	-.008
	.877	-.014	-.002	-.003	-.004	-.006	-.001	-.009	-.007	.012	.001
	.897	-.017	-.004	-.006	-.005	-.008	-.003	-.011	-.009	.033	.000
	.917	-.017	-.004	-.006	-.006	-.008	-.004	-.011	-.010	.036	-.003
	.937	-.027	-.014	-.016	-.017	-.019	-.015	-.022	-.021	.026	-.015
	.957	-.061	-.059	-.073	-.075	-.077	-.076	-.088	-.097	-.077	-.046

TABLE 15.- PRESSURE COEFFICIENTS FOR CONFIGURATION 153 - Continued

(c) M = 0.40 to 1.20; $\alpha = 0^\circ$; $\phi = -60^\circ$

	x/l	C_p for -									
		M = 0.40	M = 0.60	M = 0.70	M = 0.75	M = 0.80	M = 0.85	M = 0.90	M = 0.95	M = 1.00	M = 1.20
Nose	.471	.221	.244	.255	.269	.280	.292	.310	.340	.388	.312
	.481	.188	.210	.228	.236	.246	.264	.278	.309	.358	.309
	.491	.166	.183	.197	.208	.220	.237	.251	.284	.335	.309
	.511	.111	.133	.144	.151	.164	.184	.206	.237	.293	.315
	.521	.079	.099	.113	.119	.134	.157	.176	.216	.269	.320
	.526	-.087	-.080	-.079	-.077	-.081	-.078	-.091	-.100	-.110	-.132
	.532	.035	.044	.055	.066	.078	.104	.130	.166	.228	.286
Upper stage											
Transition flare	.539	.025	.039	.052	.063	.079	.106	.139	.181	.240	.322
	.551	-.020	-.001	.016	.027	.045	.078	.109	.159	.219	.328
	.552	-.076	-.075	-.053	-.036	-.012	.025	.066	.125	.186	.319
	.562	-.290	-.298	-.268	-.224	-.170	-.104	-.038	.030	.105	.295
Main stage	.568	-.864	-1.002	-1.269	-1.492	-1.260	-1.102	-.949	-.821	-.695	-.373
	.577	-.222	-.229	-.272	-.353	-.474	-.911	-.905	-.792	-.674	-.365
	.590	-.144	-.138	-.144	-.148	-.166	-.283	-.763	-.671	-.567	-.299
	.597	-.099	-.092	-.098	-.090	-.070	-.075	-.385	-.571	-.478	-.248
	.607	-.087	-.069	-.071	-.065	-.054	-.014	-.071	-.479	-.395	-.204
	.617	-.076	-.058	-.057	-.052	-.050	-.018	.018	-.402	-.331	-.171
	.627	-.065	-.046	-.048	-.044	-.043	-.022	.031	-.328	-.282	-.147
	.637	-.053	-.035	-.034	-.036	-.035	-.022	.022	-.142	-.230	-.117
	.657	-.032	-.020	-.022	-.023	-.023	-.015	.006	.039	-.163	-.073
	.677	-.016	.002	.000	-.001	.002	.005	.010	.044	-.062	-.015
	.697	-.024	-.008	-.010	-.011	-.017	-.007	-.006	.051	-.093	-.050
	.737	-.016	-.004	-.005	-.006	-.007	-.004	-.008	.022	-.071	-.037
	.777	-.012	.000	.000	-.002	-.003	.000	-.005	.011	-.053	-.014
	.785	-.012	.002	.000	-.002	-.001	.002	-.003	.010	-.048	-.008
	.817	-.009	.003	.002	.001	.000	.004	-.003	.005	-.041	-.017
	.857	-.014	-.001	-.003	-.003	-.005	-.001	-.008	-.005	-.041	-.011
	.877	-.014	-.001	-.003	-.003	-.006	-.001	-.009	-.006	.011	.000
	.897	-.015	-.002	-.004	-.004	-.006	-.002	-.010	-.008	.034	.003
	.917	-.017	-.005	-.006	-.007	-.008	-.006	-.012	-.011	.036	-.003
	.957	-.027	-.014	-.016	-.017	-.019	-.015	-.022	-.021	.028	-.013
	.997	-.081	-.071	-.076	-.076	-.079	-.077	-.090	-.099	-.080	-.037

TABLE 15.- PRESSURE COEFFICIENTS FOR CONFIGURATION 153 - Concluded

(d) M = 0.40 to 1.20; $\alpha = 0^\circ$; $\phi = -90^\circ$

	x/l	C_p for -									
		M = 0.40	M = 0.60	M = 0.70	M = 0.75	M = 0.80	M = 0.85	M = 0.90	M = 0.95	M = 1.00	M = 1.20
Nose	.461	.253	.288	.299	.305	.317	.337	.353	.380	.433	.312
	.471	-.388	.327	.495	.572	.631	.689	.752	.806	.863	1.022
	.491	.166	.183	.197	.208	.216	.237	.255	.284	.335	.309
	.511	.111	.133	.144	.151	.164	.184	.206	.237	.290	.315
	.526	.057	.077	.082	.099	.111	.136	.157	.197	.255	.317
	.532	.024	.033	.033	.046	.053	.094	.120	.160	.216	.267
Upper stage											
Transition flare	.552	-.076	-.075	-.053	-.036	-.008	.028	.069	.125	.186	.322
Main stage	.568	-.819	-1.013	-1.237	-1.467	-1.306	-1.134	-.979	-.847	-.726	-.381
	.590	-.144	-.138	-.139	-.136	-.131	-.327	-.767	-.677	-.570	-.299
	.607	-.087	-.069	-.071	-.065	-.058	-.007	-.065	-.479	-.398	-.209
	.627	-.065	-.046	-.048	-.044	-.043	-.022	.035	-.322	-.273	-.147
	.657	-.032	-.020	-.022	-.024	-.025	-.018	.006	.041	-.164	-.073
	.697	-.024	-.010	-.012	-.014	-.014	-.011	-.008	.049	-.096	-.046
	.737	-.016	-.004	-.005	-.006	-.007	-.004	-.007	.022	-.070	-.041
	.777	-.012	.000	-.002	-.005	-.003	-.002	-.005	.010	-.053	-.018
	.785	-.012	.000	.000	-.002	-.003	.000	-.005	.008	-.050	-.012
	.817	-.009	.004	.003	.002	.002	.006	-.001	.007	-.039	-.011
	.857	-.012	-.001	-.002	-.003	-.004	.000	-.008	-.004	-.041	-.006
	.897	-.015	-.003	-.005	-.005	-.007	-.003	-.011	-.009	.034	-.003

TABLE 16.- SECTION NORMAL-FORCE COEFFICIENTS FOR CONFIGURATION 121

	x/l	c_n for $\alpha = 3^\circ$				$\alpha = 6^\circ$				$\alpha = 10^\circ$			
		M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20
Nose	.338	.0875	.0808	.0774	.0781	.1647	.1656	.1604	.1694	.2761	.2814	.2719	.2785
	.349	.0920	.0824	.0795	.0874	.1647	.1680	.1630	.1641	.2742	.2825	.2731	.2742
	.358	.0911	.0817	.0793	.0847	.1685	.1694	.1668	.1606	.2728	.2815	.2766	.2747
	.378	.0830	.0771	.0728	.0820	.1680	.1642	.1564	.1531	.2680	.2675	.2606	.2609
	.388	.0835	.0727	.0636	.0637	.1608	.1519	.1411	.1424	.2549	.2533	.2367	.2381
	.393	.0550	.0496	.0407	.0417	.1132	.0997	.0884	.0977	.1830	.1679	.1476	.1656
	.399	.0980	.0452	.0205	.0312	.1485	.0867	.0641	.0606	.2151	.0905	.1071	.1010
Upper stage	.404	.0142	.0269	.0461	.0303	.0446	.0407	.0990	.0676	.0871	.1293	.1632	.1152
	.409	.0082	.0639	.0729	.0488	.0282	.1580	.1590	.0983	.0516	.2280	.2614	.1714
	.419	.0028	.0088	.0778	.0520	.0146	.0342	.1686	.1062	.0354	.0707	.2868	.1880
	.429	-.0007	-.0054	.0597	.0430	.0074	-.0067	.1308	.0918	.0296	.0166	.1872	.1614
	.439	.0017	-.0013	.0149	.0292	.0088	-.0026	.0241	.0619	.0271	.0108	-.0131	.1109
	.449	.0017	.0052	-.1234	.0142	.0156	.0119	-.1775	.0315	.0344	.0325	-.1540	.0540
	.459	.0261	.0413	.0343	.0270	.0585	.0830	.0910	.0699	.1027	.1248	.1554	.1260
Transition flare	.482	.0387	.0197	.0176	.0062	.0611	.0578	.0427	.0207	.0836	.1085	.0689	.0486
	.492	.0314	.0218	.0204	.0167	.0575	.0557	.0415	.0335	.0882	.1091	.0723	.0594
	.512	.0348	.0223	.0238	.0309	.0559	.0565	.0526	.0510	.0931	.1180	.0941	.0829
	.532	.0365	.0240	.0276	.0269	.0572	.0577	.0591	.0660	.0914	.1198	.1087	.0982
	.552	.0295	.0232	.0302	.0327	.0572	.0581	.0729	.0734	.0806	.1131	.1236	.1109
	.562	.0185	.0043	.0415	.0419	.0326	.0282	.0887	.0792	.0503	.0734	.1328	.1209
Main stage	.568	.0091	-.0184	.0244	.0335	.0156	-.0252	.0601	.0519	.0282	-.0067	.0946	.0895
	.577	.0221	.0027	.0156	.0230	.0211	.0054	.0476	.0393	.0236	.0209	.0987	.0930
	.587	.0174	.0027	.0188	.0212	.0185	.0046	.0432	.0385	.0210	.0184	.0841	.0855
	.597	.0153	.0012	.0079	.0139	.0195	-.0001	.0205	.0271	.0127	.0133	.0397	.0619
	.607	.0160	.0012	-.0033	.0086	.0132	.0024	-.0035	.0244	.0124	.0117	.0086	.0527
	.617	.0159	-.0014	-.0129	.0059	.0135	.0029	-.0227	.0103	.0145	.0107	-.0265	.0341
	.627	.0184	.0012	-.0176	.0018	.0159	-.0034	-.0350	.0012	.0123	.0115	-.0448	.0191
	.637	.0152	.0027	-.0117	.0019	.0166	-.0003	-.0304	.0032	.0121	.0105	-.0417	.0078
	.657	.0087	-.0017	-.0107	-.0129	.0089	.0001	-.0311	.0004	.0174	.0145	-.0467	.0053
	.677	.0121	.0000	-.0057	-.0002	.0112	.0047	-.0486	.0068	.0210	.0208	-.0392	.0100
	.697	.0114	-.0002	-.0011	.0015	.0111	.0049	-.0554	-.0066	.0210	.0228	-.0371	.0122
	.737	.0091	-.0006	-.0033	.0042	.0068	-.0005	.0107	.0039	.0137	.0161	.0165	.0032
	.777	.0099	.0014	-.0043	-.0004	.0083	.0038	.0109	.0090	.0149	.0192	.0235	.0256
	.785	.0080	.0005	-.0085	.0022	.0054	-.0014	.0035	.0026	.0077	.0063	.0043	.0267
	.817	.0090	.0002	.0031	.0114	.0101	.0063	.0139	.0111	.0122	.0164	.0234	.0250
	.857	.0074	-.0020	-.0021	.0020	.0080	.0038	.0098	.0203	.0104	.0136	.0180	.0208
	.877	.0080	-.0015	-.0029	-.0006	.0086	.0036	.0099	-.0004	.0114	.0147	.0201	.0272
	.897	.0075	-.0010	-.0053	.0009	.0081	.0044	.0072	.0028	.0107	.0143	.0182	.0070

TABLE 17.- SECTION NORMAL-FORCE COEFFICIENTS FOR CONFIGURATION 221

	x/l	c_n for -											
		α = 3°				α = 6°				α = 10°			
		M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20
Nose	.367	.1056	.1062	.1016	.1027	.2089	.2098	.1988	.1943	.3438	.3443	.3297	.3274
	.377	.1006	.1031	.0972	.0937	.2043	.2011	.1900	.1838	.3341	.3232	.3135	.3073
	.387	.0998	.0936	.0896	.0813	.1879	.1804	.1731	.1629	.3270	.3113	.2985	.2904
	.399	-.0180	-.2534	.0360	.0228	-.0294	-.4089	.0578	.0473	-.0134	-.5860	.0878	.0764
Upper stage	.404	.1049	-.0721	.0502	.0339	.2004	-.1312	.1024	.0700	.3004	-.0763	.1747	.1288
	.409	.0407	.0336	.0931	.0644	.0952	.1033	.1855	.1296	.1807	.2049	.3140	.2268
	.419	.0086	.1882	.1120	.0762	.0195	.2700	.2258	.1601	.0533	.3139	.3742	.2757
	.429	.0035	.0861	.0968	.0755	.0147	.1157	.1949	.1498	.0325	.1443	.1405	.2457
	.439	.0049	.0247	.0481	.0518	.0146	.0418	.0568	.1042	.0352	.0608	.0259	.1766
	.449	.0096	.0268	-.1300	.0245	.0205	.0371	-.1562	.0538	.0457	.0545	-.0528	.0893
	.459	.0339	.0722	.0403	.0233	.0640	.1098	.0861	.0611	.1113	.1376	.1860	.1331
Transition flare	.482	.0302	.0318	.0105	-.0014	.0567	.0573	.0396	.0061	.0994	.0861	.0687	.0408
	.492	.0288	.0293	.0105	.0089	.0539	.0555	.0383	.0168	.0996	.0877	.0572	.0439
	.512	.0262	.0343	.0213	.0278	.0529	.0592	.0541	.0388	.1053	.0975	.0830	.0695
	.532	.0257	.0363	.0233	.0266	.0587	.0596	.0640	.0545	.1025	.1018	.1034	.0881
	.552	.0233	.0338	.0317	.0306	.0511	.0583	.0756	.0659	.0944	.0876	.1231	.1039
	.562	.0133	.0106	.0462	.0421	.0339	.0256	.0982	.0765	.0651	.0495	.1373	.1217
Main stage	.568	-.0001	-.0198	.0268	.0298	-.0014	-.0325	.0637	.0462	.0228	-.0241	.0899	.0819
	.577	.0061	.0060	.0126	.0207	.0148	.0021	.0560	.0347	.0308	.0076	.0976	.0840
	.587	.0075	.0083	.0177	.0259	.0084	-.0001	.0543	.0314	.0308	.0066	.0861	.0821
	.597	.0013	.0059	.0049	.0136	.0073	.0016	.0347	.0239	.0185	.0083	.0485	.0643
	.607	.0097	.0084	-.0058	.0107	.0073	.0032	.0121	.0196	.0208	.0066	.0141	.0505
	.617	.0038	.0074	-.0159	.0066	.0062	.0006	-.0068	.0062	.0192	.0001	-.0134	.0316
	.627	-.0001	.0086	-.0225	.0021	.0026	.0015	-.0180	-.0016	.0206	.0031	-.0286	.0176
	.637	.0072	.0058	-.0168	.0015	.0070	.0047	-.0102	.0005	.0189	.0039	-.0189	.0089
	.657	-.0017	.0072	-.0135	-.0118	.0071	.0108	-.0071	.0005	.0189	.0056	-.0219	.0042
	.677	.0019	.0079	-.0182	-.0011	.0082	.0136	.0042	.0080	.0219	.0113	-.0101	.0107
	.697	-.0001	.0083	-.0468	-.0004	.0068	.0134	.0022	-.0058	.0234	.0134	-.0113	.0121
	.737	.0021	.0059	-.0109	-.0003	.0063	.0104	.0146	.0039	.0150	.0073	.0223	-.0002
	.777	.0028	.0096	.0061	-.0040	.0082	.0111	.0142	.0091	.0194	.0106	.0267	.0219
	.785	.0005	.0038	.0019	.0018	.0056	.0066	.0096	.0012	.0130	.0006	.0119	.0261
	.817	.0032	.0088	.0103	.0115	.0068	.0115	.0151	.0085	.0146	.0113	.0254	.0244
	.857	.0019	.0067	.0062	.0014	.0061	.0087	.0081	.0188	.0127	.0083	.0162	.0204
	.877	.0025	.0069	.0056	-.0013	.0054	.0088	.0105	-.0011	.0124	.0093	.0183	.0271
	.897	.0024	.0068	.0035	.0004	.0062	.0092	.0114	.0006	.0121	.0092	.0164	.0083

TABLE 18.- SECTION NORMAL-FORCE COEFFICIENTS FOR CONFIGURATION 321

	x/l	c_n for -											
		$\alpha = 3^\circ$				$\alpha = 6^\circ$				$\alpha = 10^\circ$			
		M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20
Nose	.371	.1152	.1100	.1068	.1015	.2282	.2278	.2167	.2103	.3835	.3783	.3581	.3469
	.381	.1107	.1053	.0993	.0932	.2132	.2157	.2038	.1952	.3668	.3608	.3409	.3277
	.391	.1030	.0955	.0855	.0846	.1902	.1919	.1850	.1746	.3301	.3298	.3093	.2894
	.399	-.1641	-.1405	.0259	.0167	-.3209	-.3872	.0613	.0549	-.4266	-.5560	.1062	.0929
Upper stage	.404	.0442	-.0814	.0627	.0471	.1029	-.2283	.1243	.0963	.2659	-.2869	.2040	.1672
	.409	.1974	-.0643	.1083	.0775	.3388	-.1256	.2012	.1519	.4482	.0167	.3038	.2596
	.419	.0572	.0389	.1244	.0981	.0891	.2027	.2475	.1955	.1613	.3476	.2711	.3242
	.429	.0109	.0950	.1175	.0950	.0236	.2546	.2308	.1850	.0724	.3024	.2034	.3025
	.439	.0084	.0913	.0653	.0666	.0137	.1713	.0303	.1324	.0417	.1856	.1219	.2136
	.449	.0190	.0657	-.1418	.0372	.0313	.1126	-.1457	.0724	.0541	.1327	.0186	.1093
	.459	.0554	.0847	.0579	.0363	.0910	.1588	.1185	.0787	.1255	.2069	.2368	.1748
Transition flare	.482	.0301	.0207	.0120	-.0041	.0566	.0603	.0240	.0017	.0985	.0936	.0706	.0416
	.492	.0251	.0168	.0114	.0034	.0472	.0531	.0229	.0113	.1008	.0904	.0490	.0350
	.512	.0319	.0238	.0187	.0227	.0469	.0608	.0421	.0356	.1104	.0994	.0716	.0524
	.532	.0291	.0244	.0270	.0240	.0519	.0699	.0558	.0525	.1026	.1114	.1005	.0799
	.552	.0232	.0180	.0373	.0320	.0444	.0616	.0735	.0675	.0908	.0981	.1240	.0968
	.562	.0034	-.0119	.0516	.0452	.0149	.0221	.0945	.0814	.0600	.0550	.1411	.1219
Main stage	.568	-.0064	-.0372	.0341	.0287	-.0109	-.0463	.0564	.0496	.0209	-.0156	.0904	.0877
	.577	.0073	-.0011	.0124	.0210	.0041	.0011	.0393	.0348	.0320	.0206	.0962	.0898
	.587	.0096	.0038	.0144	.0174	.0039	.0093	.0368	.0316	.0297	.0232	.0750	.0835
	.597	.0096	.0040	.0030	.0123	.0039	.0071	.0157	.0223	.0249	.0200	.0276	.0604
	.607	.0095	.0040	-.0116	.0076	.0017	.0102	-.0061	.0201	.0234	.0189	-.0035	.0471
	.617	.0096	.0046	-.0202	.0060	-.0022	.0093	-.0237	.0077	.0187	.0187	-.0285	.0308
	.627	.0049	.0039	-.0247	.0039	.0003	.0075	-.0322	-.0014	.0172	.0187	-.0403	.0153
	.637	.0073	.0040	-.0181	.0017	-.0009	.0070	-.0221	-.0005	.0206	.0195	-.0286	.0053
	.657	.0004	-.0002	-.0270	-.0086	-.0014	.0080	-.0149	-.0011	.0152	.0174	-.0294	.0049
	.677	.0032	.0022	-.0576	.0018	.0006	.0136	-.0212	.0068	.0207	.0228	-.0331	.0117
	.697	.0023	.0012	-.0923	.0011	.0015	.0132	-.0526	-.0057	.0214	.0249	-.0461	.0155
	.737	.0014	.0011	-.0099	.0031	-.0006	.0085	.0070	.0039	.0152	.0177	.0241	-.0007
	.777	.0020	.0028	.0005	-.0008	-.0010	.0106	.0108	.0092	.0166	.0200	.0285	.0265
	.785	.0007	-.0015	-.0050	.0011	-.0030	.0046	.0056	.0020	.0110	.0118	.0123	.0268
	.817	.0029	.0008	.0164	.0114	.0030	.0103	.0165	.0093	.0153	.0198	.0304	.0263
	.857	.0019	-.0005	.0091	.0019	.0004	.0085	.0092	.0212	.0127	.0169	.0195	.0215
	.877	.0024	-.0004	.0054	.0000	.0012	.0087	.0085	.0012	.0142	.0190	.0193	.0281
	.897	.0022	.0005	.0009	.0008	.0021	.0087	.0050	.0013	.0133	.0179	.0169	.0076

TABLE 19.- SECTION NORMAL-FORCE COEFFICIENTS FOR CONFIGURATION 122

	x/l	c_n for -											
		$\alpha = 3°$				$\alpha = 6°$				$\alpha = 10°$			
		M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20
Nose	.392	.0782	.0799	.0759	.0838	.1543	.1637	.1569	.1617	.2720	.2755	.2702	.2688
	.402	.0810	.0820	.0782	.0784	.1603	.1665	.1591	.1628	.2712	.2775	.2718	.2685
	.412	.0810	.0804	.0783	.0742	.1575	.1688	.1574	.1617	.2661	.2782	.2722	.2693
	.432	.0782	.0756	.0757	.0726	.1525	.1608	.1511	.1492	.2590	.2664	.2612	.2572
	.442	.0763	.0738	.0691	.0675	.1463	.1488	.1354	.1434	.2515	.2498	.2373	.2457
	.447	.0503	.0491	.0423	.0462	.0957	.0988	.0866	.0937	.1776	.1603	.1457	.1620
	.453	.0884	.0055	.0232	.0345	.1337	.0295	.0391	.0664	.1999	-.0818	.1404	.1113
Upper stage	.459	.0171	.0304	.0427	.0248	.0426	.0803	.0872	.0567	.0960	.1950	.1478	.1147
	.463	.0046	.0483	.0627	.0382	.0297	.1133	.1368	.0843	.0591	.2030	.2010	.1724
	.473	.0019	.0006	.0798	.0444	.0184	.0155	.0939	.1002	.0367	.0492	.0489	.1957
	.483	-.0003	-.0030	-.0505	.0420	.0169	.0016	-.1101	.0873	.0340	.0157	-.0479	.1667
	.493	.0019	-.0011	-.1266	.0327	.0168	.0082	-.1334	.0598	.0330	.0237	-.0737	.1104
	.503	.0044	.0127	.0736	-.0202	.0266	.0291	.1410	-.0627	.0536	.0535	.2043	-.0904
	.513	.0305	.0496	.1253	.0480	.0866	.1022	.2226	.0921	.1422	.1671	.3255	.1621
Transition flare	.525	.0372	.0476	.0551	.0506	.0744	.0968	.0984	.0962	.1323	.1473	.1606	.1434
	.535	.0480	.0515	.0280	.0323	.0852	.1094	.0730	.0790	.1624	.1698	.1412	.1323
	.545	.0494	.0565	.0326	.0412	.0873	.1176	.0861	.0840	.1661	.1855	.1518	.1338
	.555	.0429	.0612	.0521	.0521	.0910	.1227	.1058	.0946	.1584	.1853	.1668	.1521
	.565	.0217	.0579	.0657	.0778	.0484	.1152	.1218	.1340	.1022	.1592	.1795	.1905
Main stage	.569	.0071	-.1161	.0306	.0309	.0086	-.1289	.0590	.0588	.0547	-.1250	.0885	.0912
	.577	.0129	.0182	.0268	.0229	.0209	.0323	.0749	.0516	.0555	.0394	.1521	.1089
	.587	.0067	.0083	.0404	.0269	.0046	.0184	.0927	.0635	.0331	.0185	.1746	.1280
	.597	-.0002	.0056	.0346	.0205	.0026	.0102	.0753	.0544	.0209	.0166	.1329	.1046
	.607	.0006	.0046	.0209	.0234	.0011	.0101	.0486	.0503	.0242	.0132	.0638	.0944
	.617	.0016	.0047	-.0023	.0163	-.0014	.0060	-.0014	.0339	.0169	.0123	.0062	.0688
	.627	.0005	.0031	-.0193	.0086	-.0051	.0069	-.0343	.0210	.0130	.0083	-.0370	.0430
	.637	-.0031	.0031	-.0219	.0016	-.0050	.0076	-.0374	.0147	.0120	.0106	-.0516	.0299
	.657	-.0027	-.0009	-.0162	-.0128	.0005	.0052	-.0301	.0015	.0119	.0131	-.0440	.0092
	.677	-.0023	.0005	-.0068	-.0039	.0044	.0094	-.0120	.0010	.0175	.0189	-.0061	.0067
	.697	-.0023	-.0002	-.0025	-.0040	.0052	.0096	-.0025	-.0131	.0190	.0213	.0133	.0048
	.737	-.0035	-.0020	.0006	.0006	-.0010	.0057	-.0004	.0002	.0122	.0154	.0168	-.0073
	.777	-.0023	.0002	.0043	-.0015	.0001	.0076	.0047	.0072	.0146	.0193	.0209	.0180
	.785	-.0047	-.0025	.0017	-.0006	-.0019	.0034	.0031	.0025	.0086	.0108	.0099	.0244
	.817	.0003	.0015	-.0088	.0100	-.0001	.0091	-.0018	.0077	.0124	.0176	.0313	.0218
	.857	-.0017	.0001	.0020	.0017	-.0011	.0065	.0064	.0206	.0197	.0149	.0237	.0228
	.877	-.0016	-.0001	.0033	-.0007	-.0021	.0073	.0100	.0003	.0108	.0145	.0256	.0269
	.897	-.0013	-.0003	.0036	.0001	-.0014	.0076	.0077	.0024	.0094	.0146	.0237	.0084

TABLE 20.- SECTION NORMAL-FORCE COEFFICIENTS FOR CONFIGURATION 222

	x/l	c_n for -											
		$\alpha = 3^\circ$				$\alpha = 6^\circ$				$\alpha = 10^\circ$			
		M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20
Nose	.421	.1017	.1069	.0979		.2092	.2106	.1944	.9394	.3449	.3415	.3333	.3301
	.431	.0957	.1026	.0981		.1996	.2030	.1869	.8761	.3387	.3238	.3174	.3126
	.441	.0922	.0920	.0885		.1929	.1861	.1710	.7837	.3248	.3012	.3077	.2928
	.453	-.0333	-.3482	.0106		-.0201	-.5992	.0247	-.4556	-.0755	-.7197	.0551	.0258
Upper stage	.458	.1068	-.0770	.0578		.2038	-.1853	.1124	-.4238	.3147	-.2053	.0278	.1492
	.463	.0471	.0034	.0894		.1228	.0200	.1639	-.2882	.2400	.1168	-.0035	.2286
	.473	.0051	.1472	.1102		.0266	.2957	-.0285	-.1071	.0787	.3369	.0699	.2814
	.483	-.0011	.1113	-.1066		.0178	.2035	-.0851	-.0369	.0496	.1898	.0877	.2512
	.493	.0013	.0465	-.1938		.0153	.0967	-.0552	-.0326	.0495	.1043	.0573	.1448
	.503	.0087	.0445	.1250		.0280	.0874	.2506	-.1582	.0724	.1041	.2941	-.0507
	.513	.0470	.1130	.1994		.0982	.1936	.3400	.3893	.1727	.2202	.4415	.2006
Transition flare	.525	.0433	.0636	.0839		.0858	.1151	.1780	.4215	.1404	.1587	.2447	.1563
	.535	.0490	.0584	.0379		.0986	.1079	.1072	.3598	.1623	.1646	.1906	.1300
	.545	.0465	.0615	.0373		.0998	.1154	.0941	.3276	.1670	.1696	.1710	.1302
	.555	.0461	.0627	.0559		.0975	.1202	.1115	.3416	.1551	.1657	.1840	.1500
	.565	.0108	.0150	.0786		.0480	.0576	.1283	.2835	.0923	.1089	.1893	.1939
Main stage	.568	-.0128	-.2607	.0315		.0037	-.2748	.0442	-.2079	.0378	-.2239	.0899	.0971
	.577	.0114	.0167	-.0028		.0316	.0231	.0271	-.1782	.0576	.0146	.1049	.0932
	.587	.0088	.0183	.0215		.0207	.0250	.0569	-.1134	.0390	.0102	.1287	.1167
	.597	-.0011	.0132	.0196		.0148	.0185	.0363	-.0717	.0330	.0079	.0834	.0995
	.607	.0014	.0132	.0068		.0155	.0185	.0074	-.0694	.0290	.0067	.0179	.0838
	.617	.0014	.0115	-.0079		.0093	.0158	-.0218	-.0741	.0264	.0042	-.0194	.0559
	.627	.0014	.0100	-.0212		.0071	.0159	-.0356	-.0747	.0187	.0035	-.0508	.0348
	.637	-.0048	.0084	-.0197		.0095	.0158	-.0279	-.0605	.0178	.0072	-.0493	.0266
	.657	-.0030	.0097	-.0126		.0087	.0149	-.0127	-.0524	.0300	.0058	-.0371	.0041
	.677	-.0010	.0110	-.0053		.0112	.0178	.0031	-.0424	.0268	.0108	-.0101	.0027
	.697	-.0019	.0099	-.0021		.0107	.0189	.0116	-.0631	.0299	.0116	-.0061	.0023
	.737	-.0055	.0074	-.0209		.0061	.0139	.0423	-.0387	.0224	.0056	-.0265	-.0083
	.777	-.0052	.0093	.0020		.0069	.0162	.0193	-.0179	.0227	.0079	-.0027	.0248
	.785	-.0042	.0061	-.0026		.0070	.0113	.0138	-.0188	.0200	.0039	-.0033	.0262
	.817	-.0014	.0099	.0017		.0083	.0177	.0173	-.0029	.0214	.0113	.0066	.0264
	.857	-.0028	.0090	.0012		.0076	.0159	.0057	.0179	.0188	.0092	.0139	.0242
	.877	-.0025	.0090	.0022		.0069	.0160	.0052	-.0159	.0188	.0097	.0221	.0288
	.897	-.0029	.0092	.0023		.0071	.0155	.0021	-.0104	.0194	.0097	.0259	.0104

TABLE 21.- SECTION NORMAL-FORCE COEFFICIENTS FOR CONFIGURATION 322

	x/l	c_n for -											
		α = 3°				α = 6°				α = 10°			
		M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20
Nose	.426	.1041	.1115	.1064	.0977	.2114		.2146	.2029	.3680	.3727	.3557	.3475
	.436	.1008	.1004	.1003	.0935	.1889		.2154	.1891	.3462	.3507	.3391	.3261
	.446	.0837	.0858	.0892	.0785	.1542		.1820	.1666	.3009	.3143	.3079	.2916
	.453	-.3975	-.4016	.0200	.0133	-.6542		.0435	.0334	-.8456	-.6982	-.1130	.0669
Upper stage	.458	-.0731	-.2394	.0531	.0412	-.0242		-.0172	.0861	.1127	-.3182	-.3428	.1518
	.463	.1981	-.1480	.0955	.0791	.3220		-.0355	.1612	.4568	-.0574	-.1229	.2721
	.473	.1354	.0839	.0442	.1014	.2605		.0090	.2094	.3417	.3561	.2210	.3500
	.483	.0072	.1842	-.1735	.0957	.0677		.0281	.1934	.1349	.3340	.2902	.2658
	.493	-.0077	.1634	-.1218	.0674	.0222		.0118	.1372	.0754	.2431	.2390	.0914
	.503	.0152	.1283	.2049	-.0252	.0463		.2872	-.0777	.0959	.2112	.3770	-.0070
	.513	.0764	.1540	.2570	.0575	.1403		.4057	.1214	.2029	.3169	.5674	.2393
Transition flare	.525	.0505	.0718	.1133	.0390	.0883		.2201	.0974	.1477	.1813	.3487	.1860
	.535	.0491	.0512	.0691	.0189	.0803		.1564	.0663	.1595	.1609	.2496	.1495
	.545	.0469	.0448	.0458	.0271	.0792		.1251	.0616	.1606	.1531	.2108	.1353
	.555	.0382	.0366	.0642	.0415	.0760		.1348	.0792	.1478	.1456	.2061	.1439
	.565	-.0240	-.0707	.0959	.0738	-.0153		.1527	.1317	.0583	.0504	.1960	.1867
Main stage	.568	-.0530	-.2698	.0210	.0291	-.0680		.0278	.0507	-.0101	-.3096	.0498	.0769
	.577	.0103	-.0116	-.0416	.0195	.0101		-.0189	.0385	.0465	.0061	.0412	.0852
	.587	.0093	.0042	-.0199	.0225	.0090		.0144	.0550	.0391	.0118	.0664	.1041
	.597	.0031	.0042	-.0054	.0165	.0075		-.0011	.0474	.0331	.0134	.0087	.0919
	.607	.0056	.0057	-.0119	.0198	.0100		-.0233	.0444	.0314	.0150	-.0348	.0762
	.617	.0016	.0040	-.0197	.0160	.0036		-.0364	.0277	.0313	.0093	-.0538	.0487
	.627	.0064	.0026	-.0190	.0085	-.0001		-.0395	.0162	.0251	.0115	-.0659	.0271
	.637	.0017	.0073	-.0092	.0027	.0016		-.0229	.0119	.0274	.0115	-.0391	.0145
	.657	.0046	.0037	-.0042	-.0122	-.0059		-.0042	-.0022	.0188	.0141	-.0164	-.0022
	.677	.0062	.0051	-.0024	-.0050	-.0013		.0021	-.0009	.0221	.0199	.0060	-.0012
	.697	.0061	.0058	-.0006	-.0051	-.0012		.0044	-.0147	.0269	.0223	.0053	.0001
	.737	-.0007	.0037	-.0119	-.0001	-.0040		-.0167	-.0001	.0199	.0143	-.0344	-.0093
	.777	.0034	.0044	-.0059	-.0029	-.0041		-.0176	.0079	.0201	.0171	.0120	.0198
	.785	-.0027	.0012	.0009	-.0013	-.0056		-.0047	.0013	.0165	.0107	.0121	.0245
	.817	-.0002	.0042	.0053	.0083	-.0001		.0139	.0100	.0185	.0161	.0290	.0306
	.857	-.0003	.0019	.0030	-.0012	-.0012		.0100	.0209	.0163	.0140	.0238	.0246
	.877	-.0005	.0028	.0039	-.0031	-.0014		.0121	.0005	.0174	.0151	.0255	.0296
	.897	-.0004	.0032	.0031	-.0015	-.0013		.0125	.0032	.0176	.0150	.0259	.0146

TABLE 22.- SECTION NORMAL-FORCE COEFFICIENTS FOR CONFIGURATION 123

	x/l	c_n for -											
		$\alpha = 3^\circ$				$\alpha = 6^\circ$				$\alpha = 10^\circ$			
		M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20
Nose	.410	.0756	.0856	.0767	.0737	.1730	.1693	.1627	.1582	.2675	.2837	.2671	.2681
	.420	.0772	.0879	.0803	.0698	.1723	.1730	.1658	.1609	.2646	.2853	.2703	.2728
	.430	.0769	.0894	.0803	.0736	.1762	.1723	.1676	.1565	.2615	.2844	.2741	.2761
	.450	.0710	.0833	.0776	.0729	.1668	.1656	.1601	.1492	.2527	.2749	.2651	.2623
	.460	.0724	.0789	.0725	.0631	.1678	.1599	.1462	.1428	.2432	.2580	.2428	.2461
	.465	.0440	.0497	.0414	.0417	.1159	.1022	.0917	.0920	.1641	.1655	.1437	.1644
	.471	.0689	.0460	.0164	.0294	.1708	-.0292	.0316	.0552	.2030	-.0635	.0895	.0928
Upper stage	.476	.0060	.0259	.0455	.0306	.0564	.0761	.0843	.0613	.0734	.1365	-.0225	.1180
	.481	.0012	.0538	.0646	.0439	.0437	.1276	.0155	.0941	.0459	.1982	-.1812	.1844
	.491	-.0039	.0155	-.2890	.0486	.0332	.0319	-.1927	.1051	.0225	.0596	-.1080	.2007
	.501	-.0038	-.0003	-.0409	.0512	.0273	.0057	-.1136	.0916	.0164	.0202	.0117	.0841
	.511	-.0038	.0048	.1749	-.0497	.0271	.0125	.2116	-.1547	.0179	.0260	.2570	-.1495
	.521	.0071	.0229	.2002	-.0732	.0392	.0472	.2504	-.1605	.0461	.0706	.2987	-.1730
	.531	.0498	.0778	.2300	.1187	.1194	.1477	.3101	.2113	.1726	.2184	.4335	.3230
Transition flare	.539	.0477	.0728	.1234	.1520	.1089	.1311	.1902	.2593	.1546	.2053	.2374	.3596
	.546	.0500	.0741	.0783	.1102	.1209	.1286	.1452	.1881	.1750	.2129	.2024	.2645
	.552	.0554	.0805	.0686	.0840	.1346	.1482	.1241	.1528	.1914	.2347	.2040	.2271
	.562	.0564	.0866	.0788	.0786	.1342	.1563	.1338	.1445	.1907	.2463	.2037	.2188
Main stage	.568	-.0059	.0305	.0215	.0152	.0384	.0473	.0534	.0379	.0633	-.0372	.0977	.0749
	.577	.0021	.0076	-.0446	.0045	.0424	.0432	.0620	.0341	.0519	.1205	.1253	.0838
	.587	-.0054	.0305	-.0057	.0172	.0264	.0357	.0855	.0611	.0277	.0512	.1774	.1381
	.597	-.0115	.0170	.0032	.0241	.0213	.0189	.0822	.0678	.0156	.0245	.1458	.1373
	.607	-.0137	.0104	.0042	.0285	.0127	.0114	.0412	.0626	.0042	.0172	.0661	.1149
	.617	-.0112	.0087	-.0068	.0231	.0105	.0082	-.0015	.0447	.0052	.0083	.0133	.0817
	.627	-.0137	.0088	-.0140	.0167	.0098	.0034	-.0264	.0328	.0004	.0073	-.0255	.0581
	.637	-.0115	.0098	-.0079	.0068	.0065	.0059	-.0238	.0199	-.0006	.0120	-.0398	.0399
	.657	-.0077	.0039	-.0032	-.0096	.0129	.0059	-.0151	.0010	-.0027	.0149	-.0447	.0088
	.677	-.0073	.0054	-.0013	-.0030	.0153	.0101	-.0015	-.0011	.0030	.0136	-.0090	.0009
	.697	-.0068	.0048	.0010	-.0078	.0134	.0104	.0052	-.0185	.0027	.0256	-.0010	-.0018
	.737	-.0089	.0027	-.0010	-.0013	.0110	.0054	.0024	-.0050	-.0026	.0184	-.0028	-.0138
	.777	-.0176	.0069	.0029	-.0030	.0085	.0063	.0109	.0037	-.0010	.0215	-.0090	.0187
	.785	-.0141	.0044	.0030	-.0035	.0105	.0048	.0118	-.0031	-.0054	.0178	-.0239	.0238
	.817	-.0069	.0065	.0065	.0091	.0140	.0093	.0166	.0066	.0021	.0202	-.0381	.0314
	.857	-.0080	.0046	.0262	.0004	.0136	.0077	.0139	.0206	-.0018	.0201	-.0345	.0274
	.877	-.0083	.0047	.0086	-.0030	.0129	.0087	.0197	.0000	-.0021	.0213	.0116	.0328
	.897	-.0082	.0052	.0031	-.0011	.0131	.0086	.0429	.0017	-.0016	.0212	.0196	.0141

TABLE 23.- SECTION NORMAL-FORCE COEFFICIENTS FOR CONFIGURATION 223

	x/l	c_n for -											
		α = 3°				α = 6°				α = 10°			
		M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20
Nose	.438	.1025	.1058	.1032	.0966	.2090	.2085	.2000	.1913		.3460	.3309	.3293
	.448	.1009	.0984	.1014	.0928	.2027	.1990	.1969	.1861		.3326	.3167	.3130
	.458	.0942	.0941	.0934	.0838	.1939	.1834	.1817	.1682		.3111	.2985	.2896
	.471	-.0156	-.3852	.0482	.0215	-.0151	-.5237	.0501	.0494		-.6053	.1028	.0792
Upper stage	.476	.0900	-.0737	.0306	.0404	.1837	-.1435	-.0245	.0812		-.1363	-.1867	.1539
	.481	.0261	.0153	-.0205	.0703	.0711	.0654	-.0658	.1378		.2259	-.1314	.2424
	.491	.0014	.1394	-.2251	.0848	.0172	.2549	-.0860	.1684		.3126	.0357	.2624
	.501	.0014	.0692	-.1927	.0807	.0135	.1275	-.0779	.1442		.1725	.0801	.0626
	.511	.0003	.0275	.2091	-.0372	.0172	.0706	.2513	-.1468		.1141	.3010	-.0141
	.521	.0109	.0532	.2713	-.0961	.0352	.0990	.3142	-.1346		.1469	.3757	-.0716
	.531	.0571	.1412	.3014	.1232	.1254	.2430	.3837	.2424		.2990	.5074	.3706
Transition flare	.539	.0597	.0964	.2191	.1630	.1094	.1598	.2626	.2636		.2345	.3063	.3465
	.546	.0561	.0798	.1474	.1159	.1147	.1400	.2007	.1821		.2222	.2592	.2619
	.552	.0637	.0858	.1239	.0854	.1279	.1415	.1682	.1552		.2219	.2569	.2434
	.562	.0514	.0885	.1163	.0787	.1118	.1410	.1629	.1440		.2118	.2354	.2217
Main stage	.568	-.0276	-.1219	-.0030	.0185	-.0159	-.1605	.0341	.0415		-.1179	.0879	.0656
	.577	.0114	.0001	-.0868	-.0005	.0315	.0089	-.0034	.0203		.0721	.0626	.1069
	.587	.0037	.0222	-.0427	.0153	.0186	.0281	.0415	.0539		.0331	.1277	.1226
	.597	.0002	.0080	-.0202	.0217	.0099	.0149	.0289	.0592		.0236	.0765	.1286
	.607	.0023	.0103	-.0116	.0284	.0036	.0130	-.0053	.0509		.0203	.0055	.1069
	.617	-.0037	.0046	-.0100	.0231	.0014	.0048	-.0366	.0304		.0130	-.0353	.0663
	.627	-.0046	.0031	-.0063	.0171	.0014	.0033	-.0503	.0266		.0105	-.0600	.0397
	.637	-.0037	.0047	.0111	.0101	-.0022	.0044	-.0332	.0145		.0139	-.0542	.0262
	.657	-.0028	.0043	.0081	-.0119	.0026	.0041	-.0055	-.0011		.0140	-.0417	-.0015
	.677	-.0012	.0043	.0082	-.0051	.0009	.0081	-.0012	-.0040		.0188	-.0096	-.0064
	.697	-.0002	.0035	.0105	-.0073	.0050	.0083	-.0009	-.0178		.0197	-.0033	-.0062
	.737	-.0036	.0013	.0141	.0007	.0001	.0030	.0005	-.0002		.0127	.0054	-.0154
	.777	-.0087	.0052	.0006	-.0015	-.0014	.0050	.0122	.0062		.0187	.0151	.0218
	.785	-.0085	.0019	-.0022	-.0027	-.0005	.0037	.0126	.0001		.0143	.0093	.0256
	.817	-.0018	.0041	.0095	.0108	.0034	.0056	.0079	.0091		.0214	-.0082	.0290
	.857	-.0025	.0017	.0607	.0014	.0007	.0038	.0103	.0194		.0187	.0161	.0245
	.877	-.0023	.0024	.0485	-.0003	.0014	.0045	.0118	-.0015		.0195	.0187	.0303
	.897	-.0022	.0021	.0150	.0009	.0012	.0049	.0114	.0022		.0209	.0176	.0109

TABLE 24.- SECTION NORMAL-FORCE COEFFICIENTS FOR CONFIGURATION 323

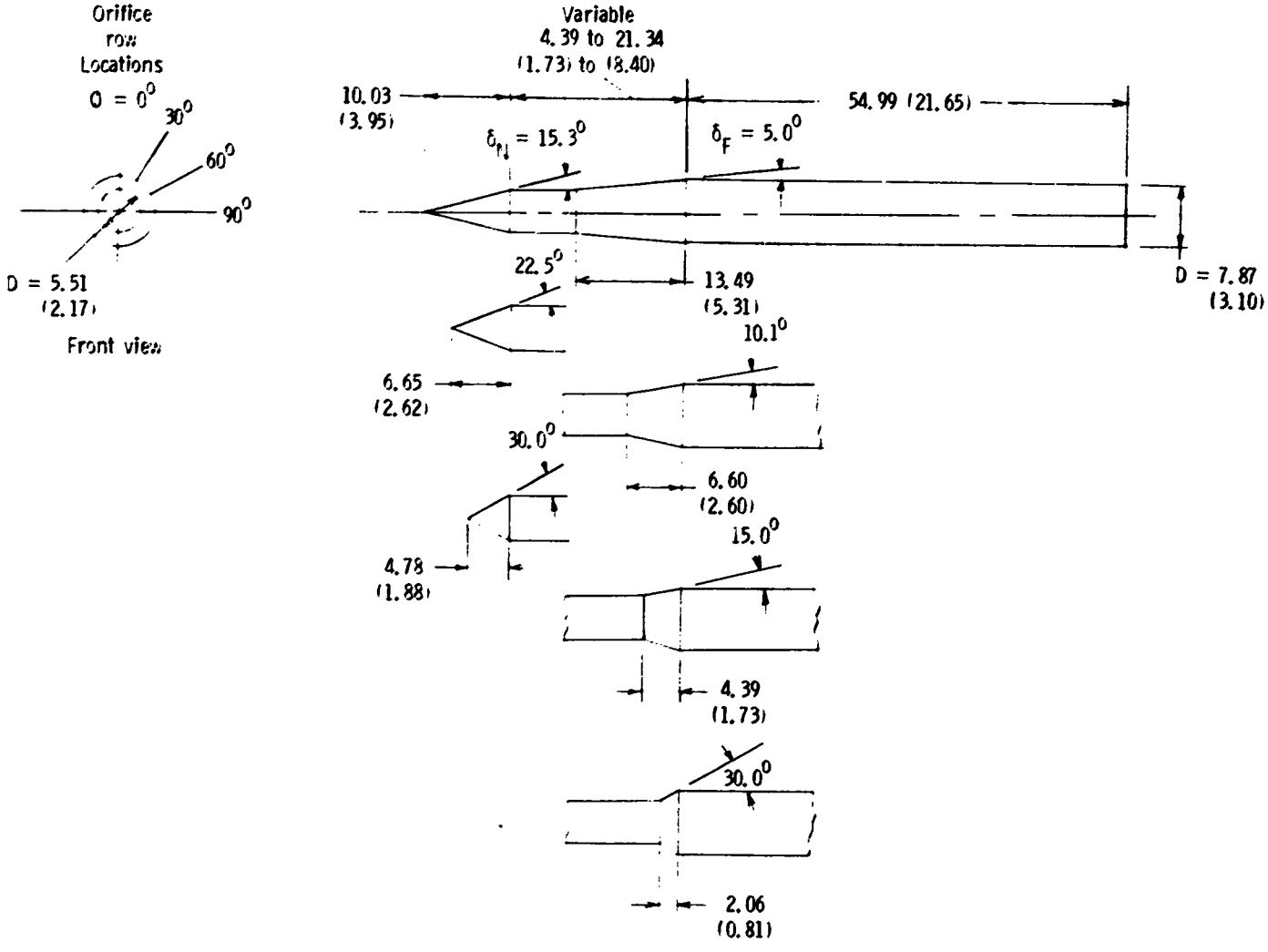
	x/l	c_n for -											
		$\alpha = 3^\circ$				$\alpha = 6^\circ$				$\alpha = 10^\circ$			
		M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20
Nose	.443	.1177	.1162	.1095	.1023	.2286	.2248	.2137	.2062	.3771	.3728	.3556	.3513
	.453	.1058	.1064	.1037	.0935	.2019	.2079	.2038	.1929	.3451	.3502	.3367	.3311
	.463	.0851	.0874	.0903	.0860	.1696	.1778	.1823	.1694	.2945	.3113	.3039	.2945
	.471	-.3524	-.2484	-.3065	.0179	-.4826	-.4202	-.3633	.0353	-.6266	-.5870	-.3654	.0663
Upper stage	.476	-.1818	-.1961	-.5545	.0416	-.1970	-.3050	-.5612	.0874	-.1302	-.3588	-.4849	.1453
	.481	.0364	-.1710	-.4110	.0783	.0943	-.2392	-.3631	.1532	.2658	-.1706	-.2077	.1891
	.491	.2510	-.0584	-.1320	.1012	.3394	.0419	-.0057	.1910	.4031	.2640	.1432	.1968
	.501	.1187	.0951	.0839	.0960	.1409	.2823	.1625	.0170	.2094	.4260	.2770	.1351
	.511	.0366	.1981	.3248	-.1613	.0532	.3375	.3440	-.0782	.1217	.3680	.3956	.0767
	.521	.0513	.2428	.4108	-.0228	.0728	.3139	.4996	-.0414	.1265	.3345	.5484	-.0041
	.531	.1376	.2708	.4670	.1594	.1949	.3885	.6154	.2833	.2484	.4419	.7159	.3982
Transition flare	.539	-.0229	.0805	.1581	.1720	-.0562	.0843	.1587	.3205	-.1146	.0961	.1531	.4455
	.546	.0237	.1258	.3004	.1776	.0307	.1384	.3328	.3066	.0351	.1658	.3396	.4095
	.552	.0565	.1176	.3244	.1132	.0994	.1377	.3331	.1755	.1788	.1978	.3427	.2612
	.562	.0164	.0223	.2479	.0970	.0543	.0843	.2571	.1571	.1351	.1549	.2775	.2324
Main stage	.568	-.1294	-.6298	-.2107	.0206	-.1293	-.5102	-.1337	.0038	-.0602	-.3378	-.0131	.0558
	.577	.0053	-.0141	-.3076	-.0222	.0120	-.0066	-.1681	.0267	.0373	.0143	-.0179	.1200
	.587	.0112	.0079	-.2085	.0046	.0094	.0134	-.1281	.0407	.0302	.0176	.0446	.1293
	.597	.0089	.0118	-.1192	.0111	.0074	.0090	-.0879	.0552	.0235	.0127	-.0097	.1182
	.607	.0050	.0134	-.0695	.0191	.0057	.0088	-.0833	.0359	.0219	.0131	-.0628	.1069
	.617	.0051	.0094	-.0228	.0165	.0036	.0079	-.0626	.0228	.0136	.0101	-.0796	.0525
	.627	.0051	.0093	.0028	.0119	.0011	.0058	-.0441	.0094	.0143	.0095	-.0904	.0240
	.637	.0065	.0102	.0239	.0027	.0035	.0060	-.0131	.0010	.0142	.0134	-.0697	.0130
	.657	.0037	.0081	.0197	-.0135	-.0001	.0067	.0072	-.0051	.0128	.0122	-.0367	-.0133
	.677	.0049	.0103	.0129	-.0035	.0024	.0086	.0050	-.0064	.0165	.0161	-.0007	-.0108
	.697	.0063	.0109	.0095	-.0052	.0019	.0091	.0015	-.0197	.0179	.0184	-.0011	-.0033
	.737	.0026	.0073	.0055	.0002	-.0063	.0053	-.0130	-.0008	.0122	.0122	-.0153	-.0090
	.777	.0038	.0079	.0162	-.0008	-.0064	.0067	-.0145	.0058	.0137	.0172	.0114	.0300
	.785	.0060	.0072	.0059	-.0022	-.0019	.0029	-.0043	-.0011	.0071	.0096	.0026	.0333
	.817	.0042	.0094	.0066	.0110	.0007	.0078	.0001	.0102	.0132	.0172	-.0093	.0333
	.857	.0029	.0090	.0045	.0018	-.0011	.0047	.0035	.0180	.0119	.0149	.0166	.0280
	.877	.0026	.0089	.0057	-.0007	-.0012	.0058	.0081	-.0016	.0115	.0151	.0203	.0344
	.897	.0031	.0087	.0055	-.0005	-.0011	.0062	.0075	.0030	.0122	.0148	.0190	.0150

TABLE 25.- SECTION NORMAL-FORCE COEFFICIENTS FOR CONFIGURATION 124

	x/l	c_n for -											
		$\alpha = 3^o$				$\alpha = 6^o$				$\alpha = 10^o$			
		M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20
Nose	.425	.0760	.0805	.0825	.0715	.1666	.1673	.1584	.1610	.2780	.2818	.2666	.2672
	.433	.0722	.0805	.0832	.0762	.1667	.1713	.161C	.1570	.2722	.2823	.2666	.2754
	.445	.0725	.0791	.0821	.0733	.1628	.1695	.16C4	.1612	.2677	.2774	.2639	.2734
	.454	.07C2	.0775	.0810	.0715	.1595	.1586	.1521	.1522	.2618	.2652	.2539	.258C
	.475	.0681	.0719	.0750	.0676	.1537	.1509	.1419	.139C	.2529	.2523	.2313	.2397
	.485	.0388	.0429	.0468	.0435	.1008	.C9C6	.C78C	.C924	.1722	.1559	.13C8	.1574
	.489	.0534	-.0098	.0164	.0196	.1747	-.0196	.0191	.0397	.2484	-.0578	.0153	.0636
Upper stage	.494	.0182	.0078	-.4422	.0275	.0572	.0410	-.3934	.0572	.1023	.0958	-.4034	.0815
	.499	.0059	.0500	-.3465	.0442	.0384	.0906	-.3569	.0176	.0634	.1578	-.2862	.0446
	.504	-.0015	.0247	.0701	-.2191	.0248	.0347	.0778	-.1406	.0368	.0533	.1664	-.0968
	.519	-.0031	-.0006	.1300	-.0474	.0175	.0040	.1926	-.1816	.0303	.0165	.2538	-.1246
	.524	-.0032	.0067	.1827	.1365	.0168	.0183	.2148	.2237	.0269	.0315	.2538	.2428
	.539	.0140	.0465	.2534	.1356	.0399	.0831	.2799	.2430	.0706	.1183	.3297	.3847
	.549	.0785	.1029	.2988	.1567	.1577	.1844	.3579	.2590	.2397	.2651	.4570	.4288
Transition flare	.554	.0453	.0683	.2700	.1337	.1041	.1389	.2532	.2974	.1577	.1838	.2770	.4529
	.558	.0488	.0805	.2302	.2774	.1010	.1473	.2453	.3896	.1528	.2096	.2847	.4618
Main stage	.564	-.2202	-.1489	-.0282	-.0257	-.3574	-.3366	.0111	-.0320	-.4904	-.5936	.0436	-.0145
	.577	.0867	-.0455	-.1758	-.0253	.1695	-.0744	-.0621	-.0056	.2469	-.0748	.0734	.0632
	.587	.1101	.0271	-.0851	.0086	.2359	.0995	.0537	.0728	.3090	.2944	.2082	.1961
	.597	.0250	.0599	-.0133	.0194	.0749	.1345	.0813	.0769	.1123	.2295	.2149	.1708
	.607	-.0041	.0466	.0151	.0213	.0193	.0900	.0583	.0813	.0321	.1254	.1217	.1652
	.617	-.0103	.0248	.0192	.0194	.0046	.0449	.0132	.0507	.0100	.0483	.0417	.1161
	.627	-.0078	.0141	.0210	.0156	.0032	.0225	-.0097	.0301	.0041	.0153	-.0075	.0614
	.637	-.0077	.0075	.0265	.0141	.0081	.0143	-.0155	.0155	.0051	.0103	-.0311	.0350
	.657	-.0090	.0030	.0134	-.0071	.0127	.0068	-.0165	-.0022	.0113	.0075	-.0566	-.0004
	.677	-.0061	.0045	.0072	.0040	.0174	.0113	-.0118	-.0027	.0232	.0159	-.0233	-.0076
	.697	-.0068	.0045	.0033	.0017	.0153	.0126	-.0126	-.0120	.0219	.0208	-.0124	-.0066
	.737	-.0096	.0024	-.0012	.0038	.0148	.0085	-.0156	.0019	.0123	.0148	-.0031	-.0107
	.777	-.0124	.0017	.0046	-.0036	.0138	.0113	-.0224	.0065	.0167	.0207	.0151	.0187
	.796	-.0067	.0030	.0032	-.0028	.0084	.0083	-.0392	-.0032	.0122	.0153	.0122	.0258
	.817	-.0062	.0052	.0059	.0090	.0152	.0112	-.0481	.0073	.0175	.0192	.0228	.0327
	.857	-.0067	.0036	.0010	.0015	.0132	.0087	-.0801	.0181	.0164	.0168	.0139	.0256
	.877	-.0067	.0038	-.0105	-.0011	.0140	.0100	-.0368	-.0016	.0168	.0178	.0139	.0311
	.897	-.0070	.0036	-.0211	.0003	.0142	.0105	.0004	-.0007	.0172	.0179	.0427	.0124

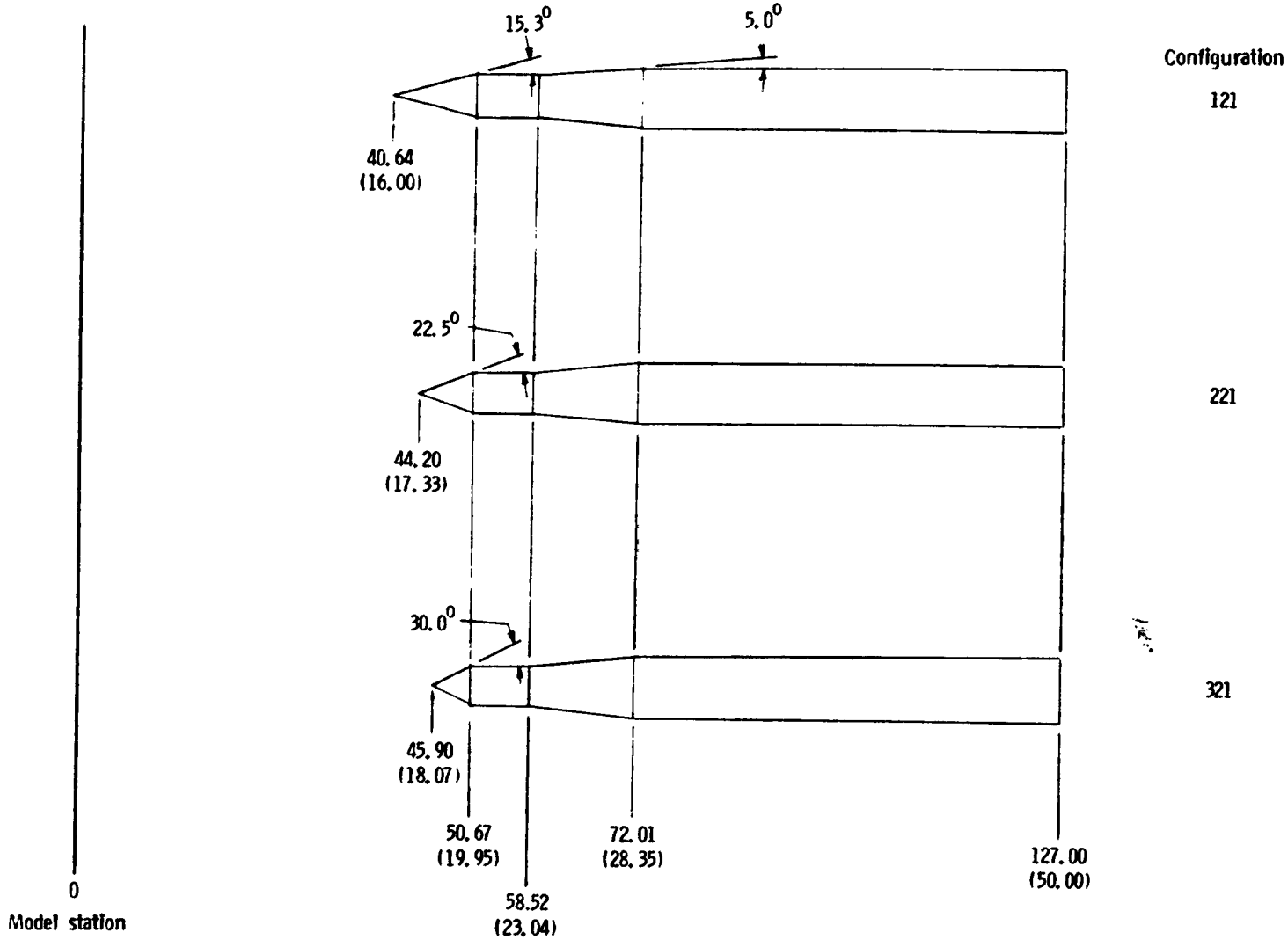
TABLE 26.- SECTION NORMAL-FORCE COEFFICIENTS FOR CONFIGURATION 324

	x/l	c_n for -											
		α = 3°				α = 6°				α = 10°			
		M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20
Nose	.461	.1139	.1058	.1076	.1015	.2254	.2242	.2128	.2070	.3854	.3771	.3550	.3482
	.471	.0942	.0974	.1015	.0954	.2014	.2057	.1957	.1909	.3508	.3540	.3366	.3298
	.481	.0740	.0827	.0917	.0851	.1621	.1776	.1779	.1697	.3007	.3146	.3068	.2908
	.489	-.2965	-.2005	-.3339	.0235	-.4345	-.3802	-.4597	-.0139	-.5835	-.5719	-.5039	-.1320
Upper stage	.494	-.1615	-.2139	-.2085	-.0405	-.1825	-.3337	-.4230	-.1811	-.0399	-.3047	-.4180	-.3026
	.499	.0951	-.1760	-.1061	-.1021	.2268	-.2010	-.2094	-.1586	.3469	-.0825	-.2282	-.1497
	.509	.2036	-.0386	.0307	-.1082	.2785	.1653	.0722	-.0128	.3607	.3567	.1060	.0927
	.519	.0703	.1306	.0472	-.0146	.1093	.2997	.1403	.0316	.1946	.4088	.3661	.1607
	.529	.0431	.2313	.0909	.1427	.0689	.3205	.2817	.3319	.1383	.3553	.4949	.3838
	.539	.0585	.2850	.2268	.1638	.1404	.3736	.4735	.3645	.1996	.4132	.6621	.5514
	.549	.1817	.3530	.3388	.2225	.2524	.4625	.6359	.3889	.3287	.5371	.8256	.5974
Transition flare	.554	.1088	.2526	.3671	.2412	.1623	.3067	.5482	.4021	.1959	.3180	.5348	.4569
	.559	.0976	.2213	.3897	.4093	.1617	.2792	.5156	.5284	.2140	.3228	.4771	.5839
Main stage	.566	-.0552	-.6069	-.2145	-.0250	-.2006	-.5319	-.2632	-.0654	-.3640	-.5699	-.0833	.0044
	.577	-.0692	-.1904	-.2231	-.1281	.0058	-.2318	-.2897	-.0884	.1982	-.1169	-.1049	-.0148
	.587	.0177	.0009	-.1270	-.0796	.0376	-.0031	-.1360	-.0107	.1216	.1314	.0686	.1115
	.597	.0155	.0150	-.0560	-.0395	.0222	.0229	-.0516	.0124	.0411	.0702	.0756	.1219
	.607	.0117	.0180	-.0215	-.0096	.0167	.0284	-.0277	.0150	.0240	.0344	-.0086	.0857
	.617	.0093	.0140	.0016	.0076	.0094	.0218	-.0159	.0093	.0204	.0229	-.0480	.0474
	.627	.0093	.0109	.0149	.0136	.0092	.0178	-.0079	.0058	.0203	.0217	-.0673	.0179
	.637	.0093	.0083	.0261	.0154	.0108	.0162	.0137	.0019	.0202	.0247	-.0594	.0079
	.647	.0043	.0058	.0191	.0051	.0023	.0137	.0195	.0034	.0210	.0263	-.0303	.0251
	.657	.0059	.0063	.0136	.0082	.0040	.0150	.0156	.0038	.0248	.0317	.0060	.0251
	.677	.0044	.0061	.0094	.0029	.0040	.0146	.0098	.0065	.0267	.0344	.0071	.0106
	.697	.0010	.0037	-.0011	.0043	-.0049	.0079	-.0010	.0043	.0155	.0271	.0035	.0153
	.737	.0014	.0037	-.0092	-.0012	.0012	.0093	.0067	.0055	.0224	.0294	.0174	.0213
	.777	-.0030	.0027	-.0096	-.0036	-.0017	.0069	.0092	-.0035	.0167	.0246	.0154	.0247
	.795	.0035	.0044	-.0058	.0106	.0007	.0107	.0111	.0098	.0225	.0288	.0148	.0228
	.817	.0025	.0026	.0053	.0018	-.0020	.0088	.0334	.0173	.0202	.0252	-.0099	.0191
	.857	.0030	.0037	.0095	.0003	-.0009	.0105	.0220	-.0017	.0199	.0263	.0201	.0265
	.897	.0028	.0028	.0114	-.0001	-.0006	.0098	.0114	.0027	.0194	.0269	.0234	.0059



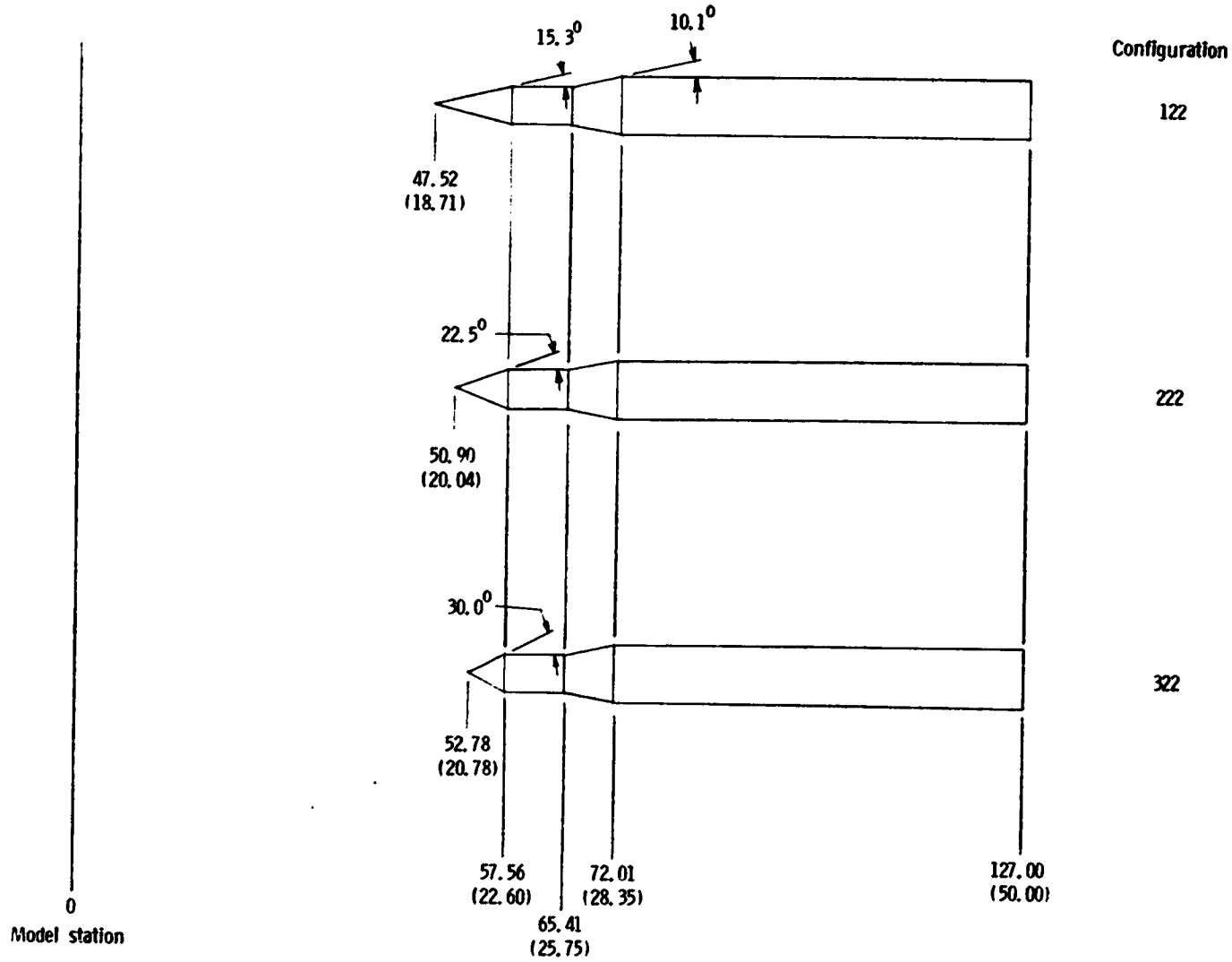
(a) Configuration geometry.

Figure 1.- Details of models. Dimensions are given in centimeters (inches) unless otherwise specified.



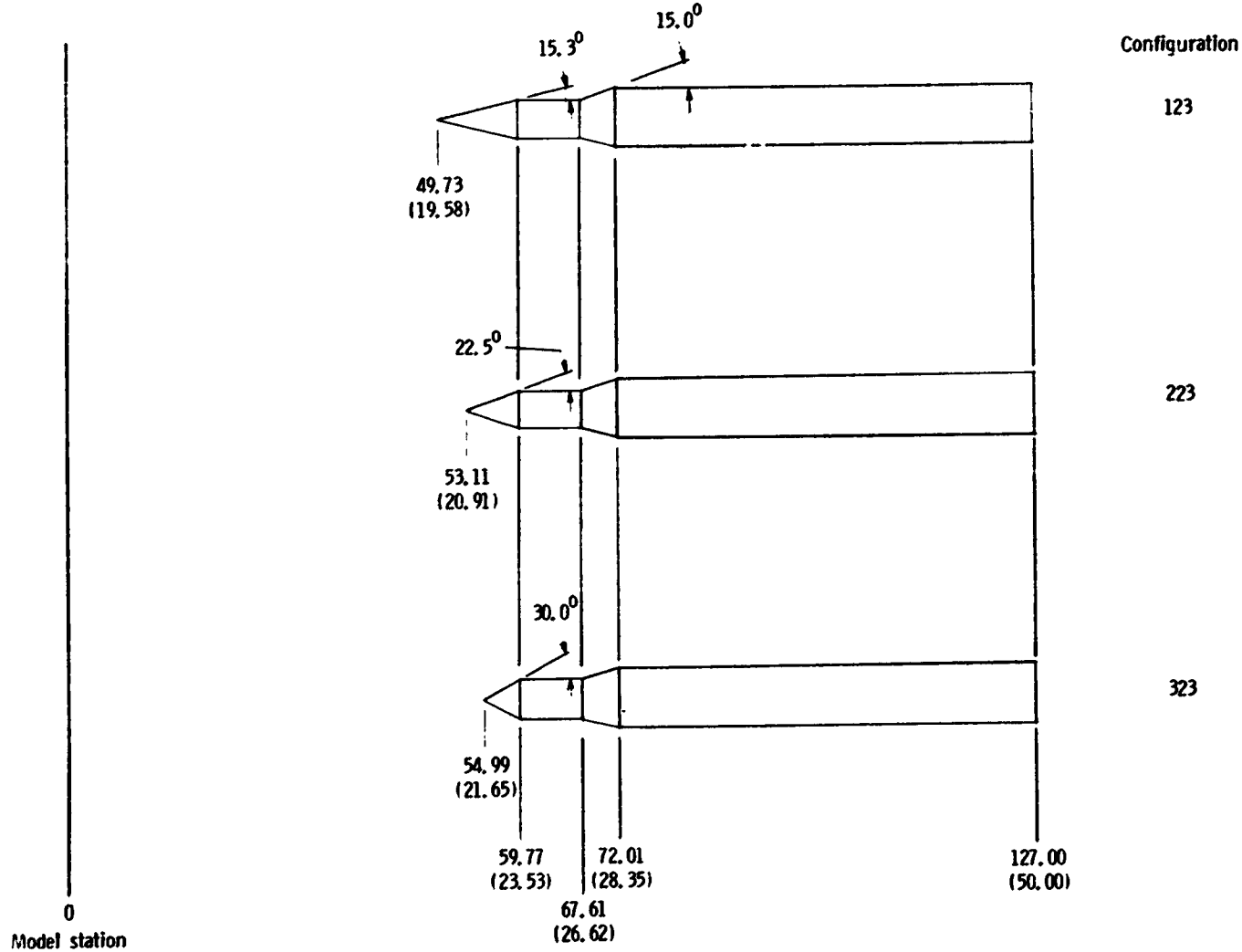
(b) Configurations 121, 221, and 321.

Figure 1.- Continued.



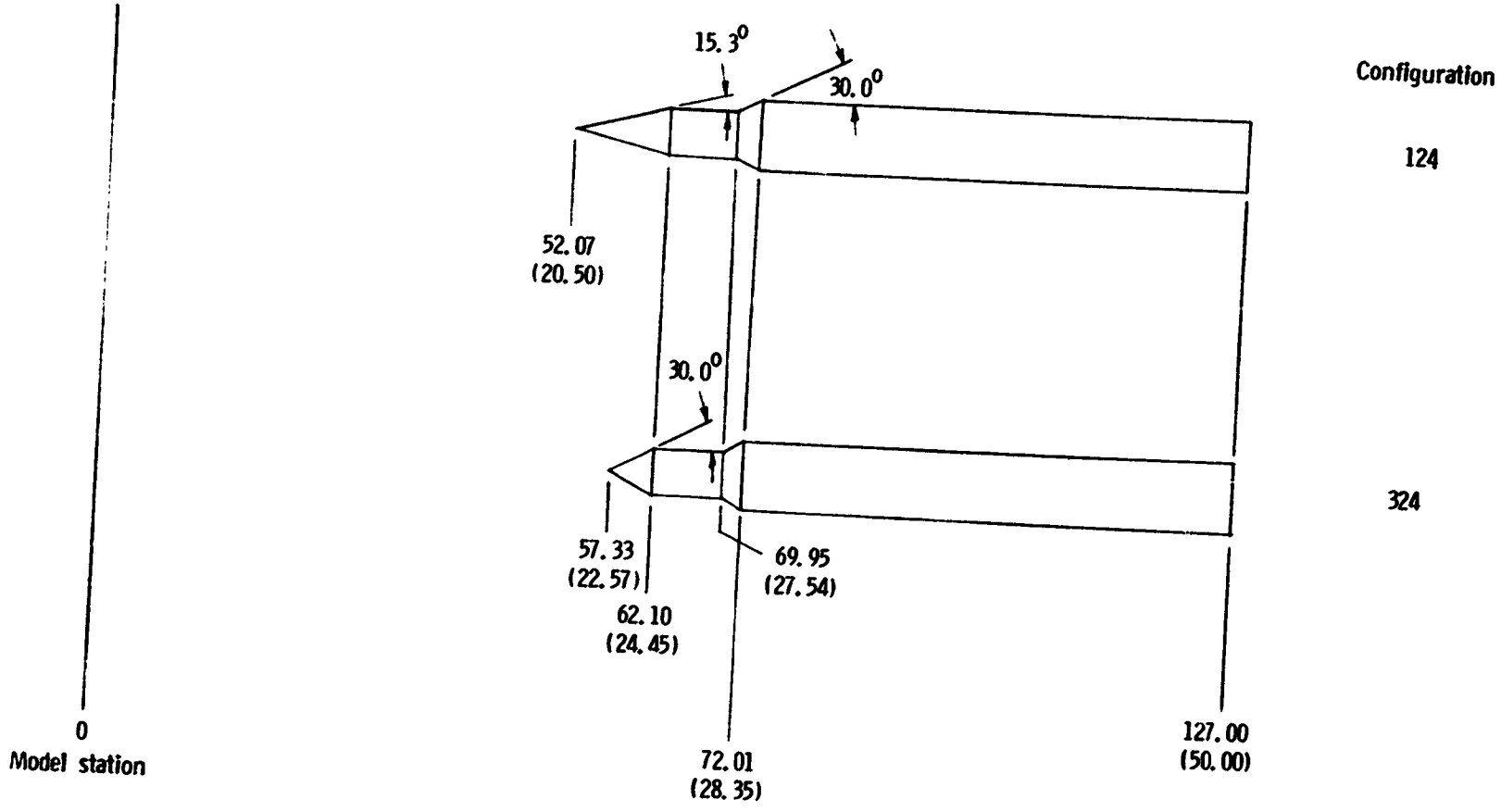
(c) Configurations 122, 222, and 322.

Figure 1.- Continued.



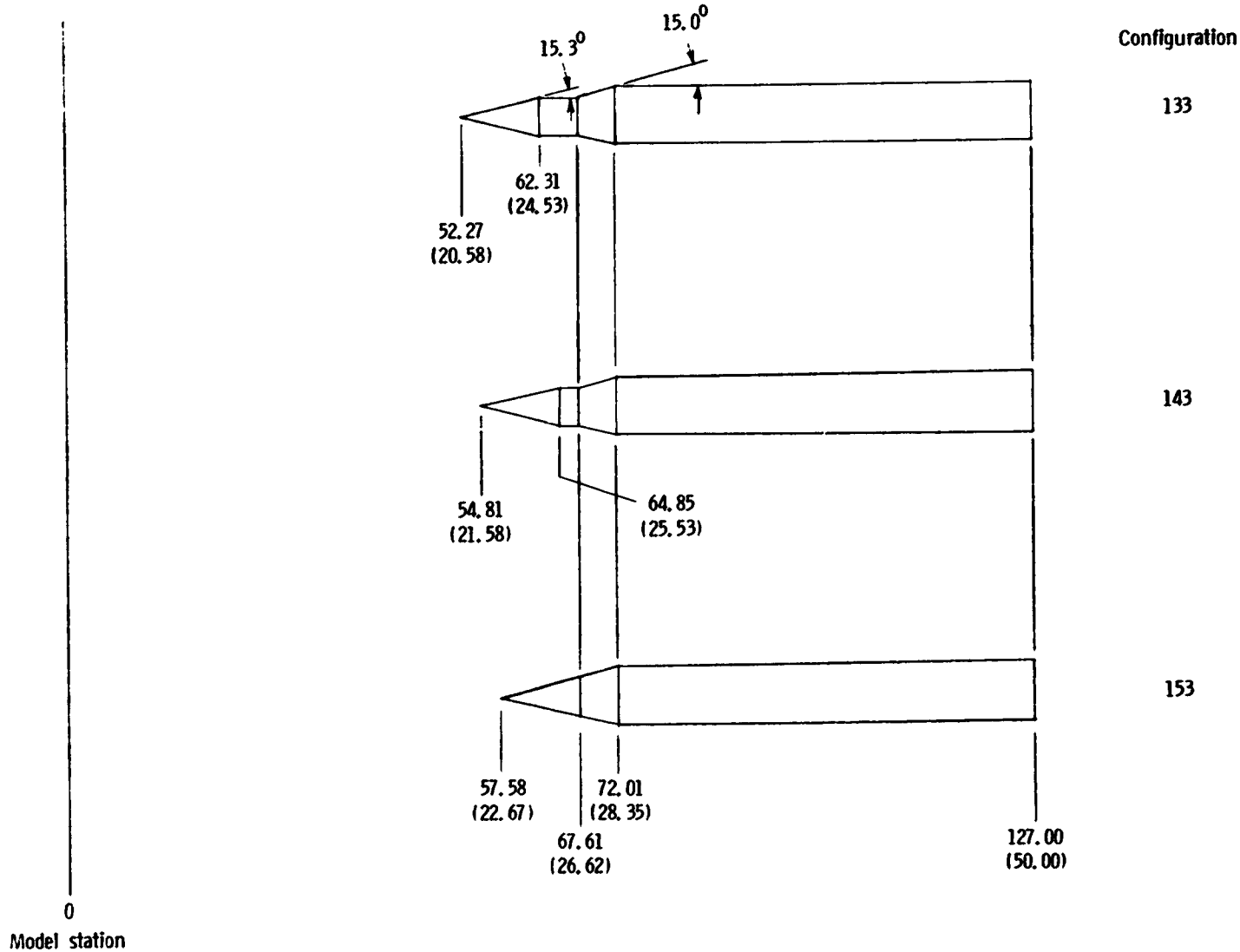
(d) Configurations 123, 223, and 323.

Figure 1.- Continued.



(e) Configurations 124 and 324.

Figure 1.- Continued.



(f) Configurations 133, 143, and 153.

Figure 1.- Concluded.

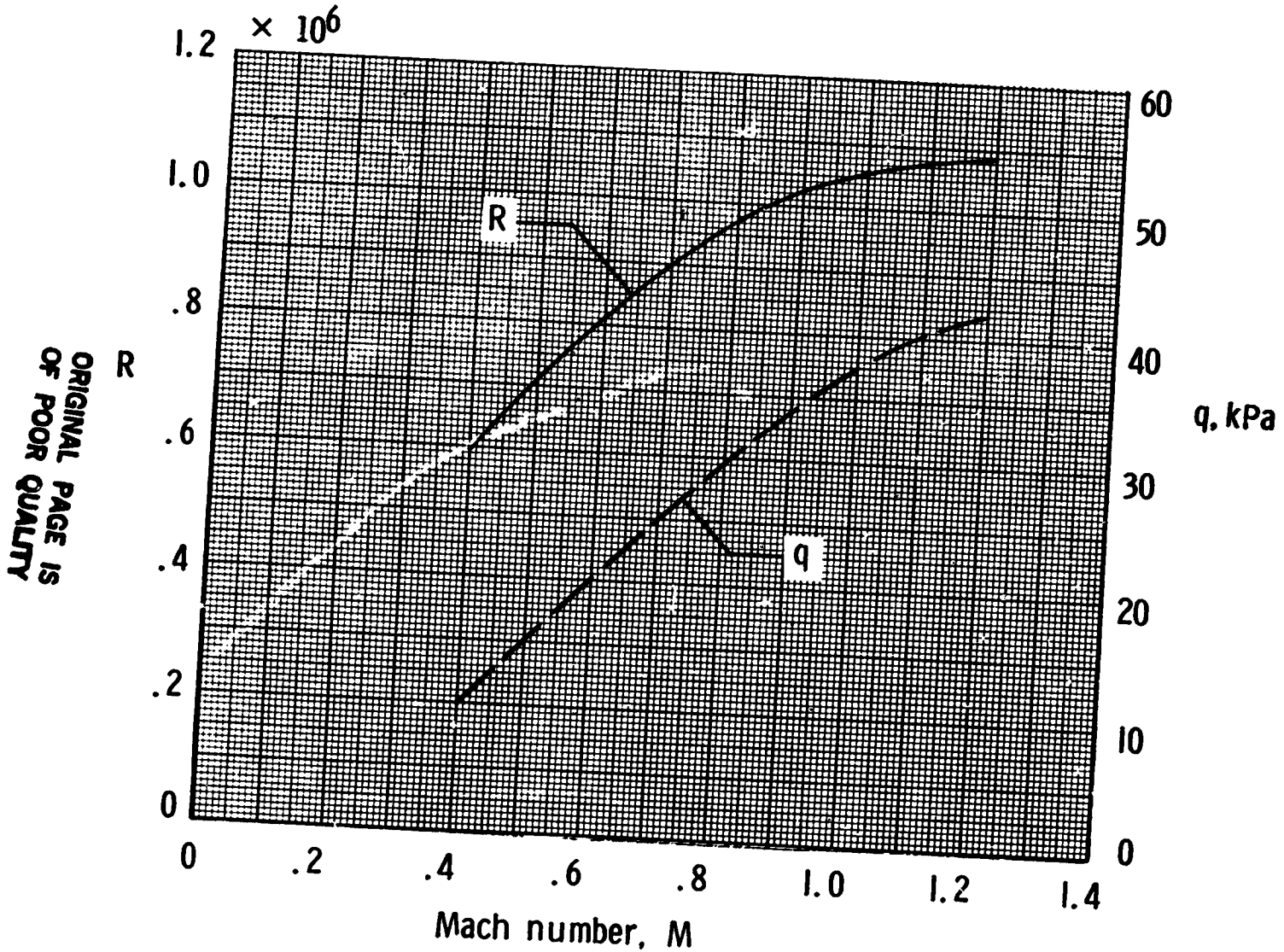
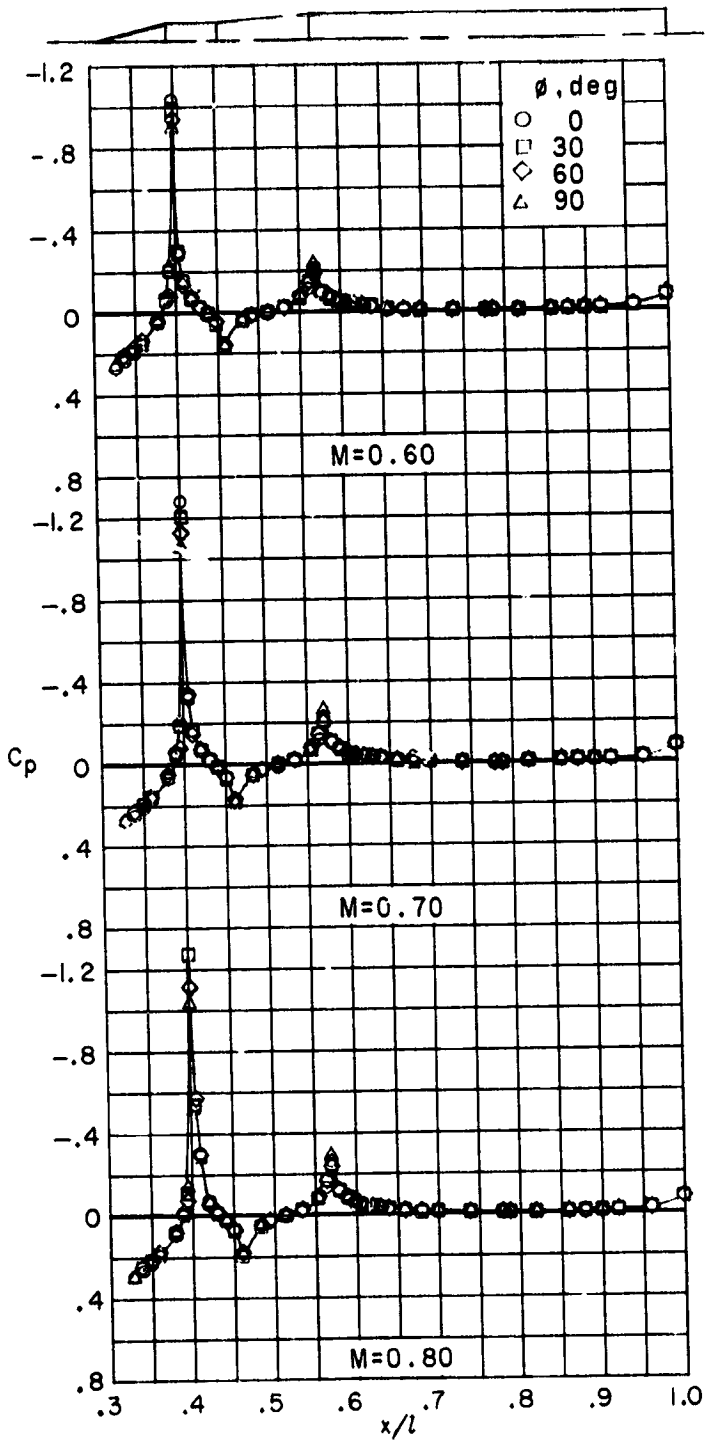
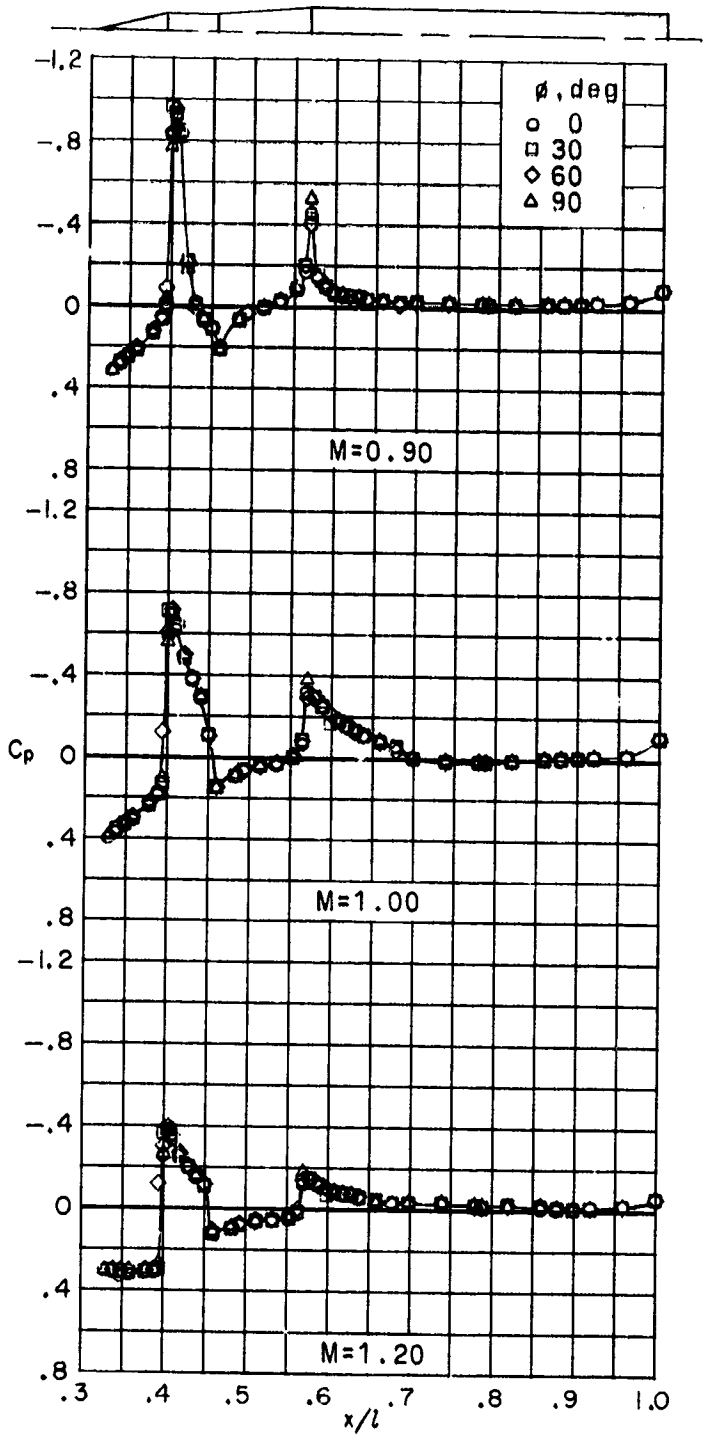


Figure 2.- Variation with Mach number of average test Reynolds number per meter and dynamic pressure.



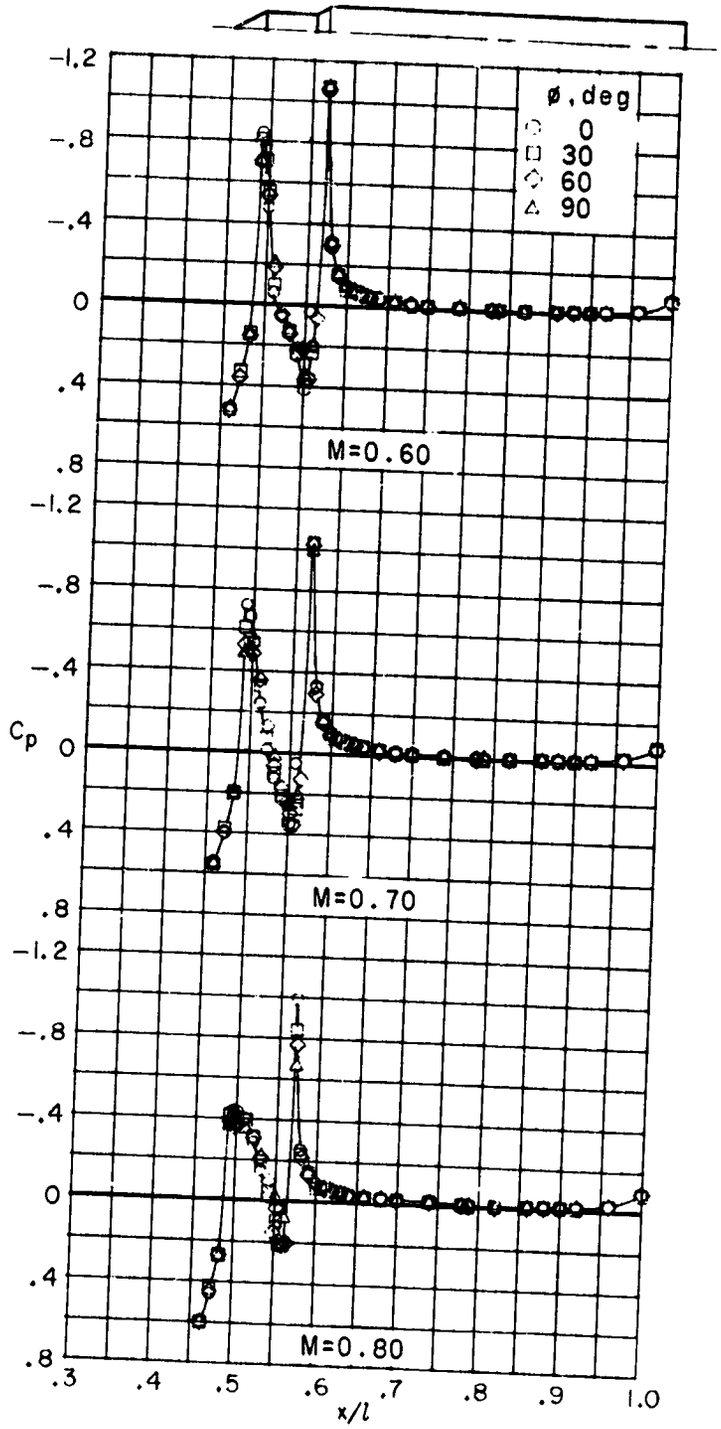
(a) Configuration 121, $\alpha = 0^{o}$.

Figure 3.- Comparison of surface pressure coefficients.



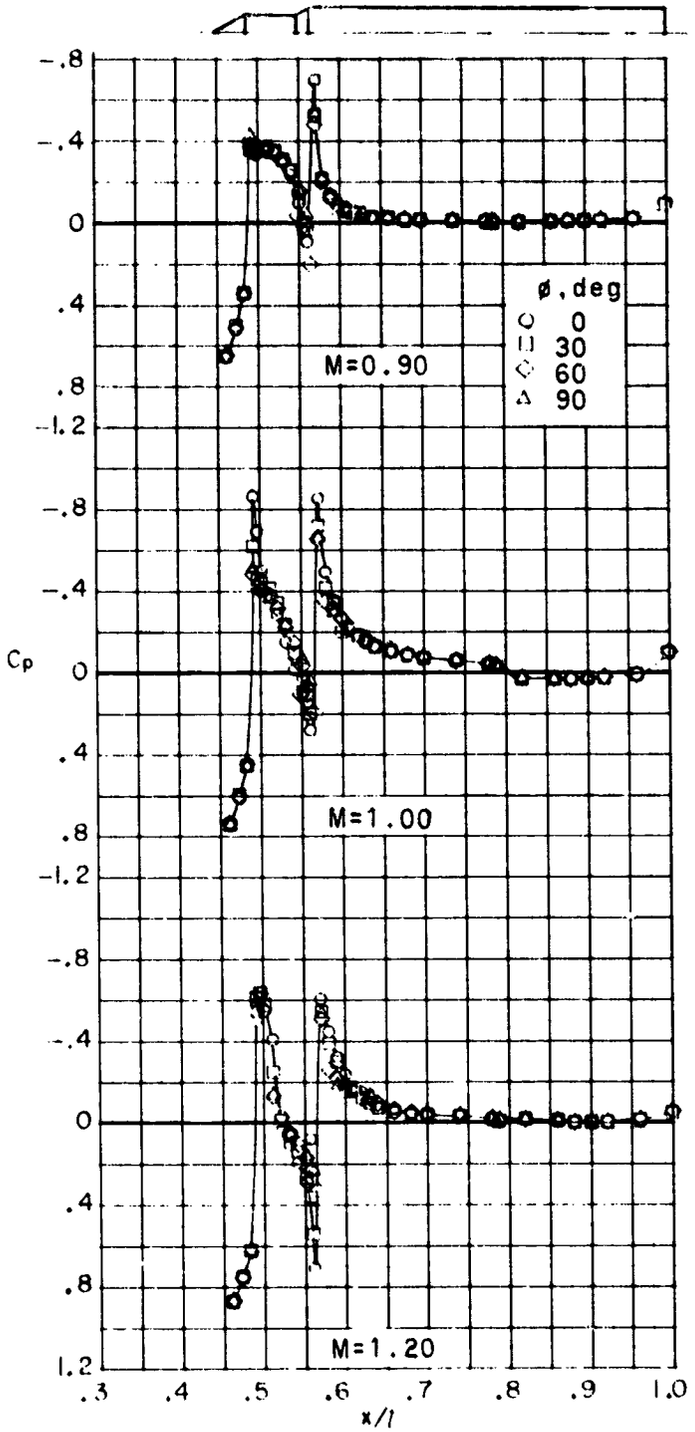
(a) Concluded.

Figure 3.- Continued.



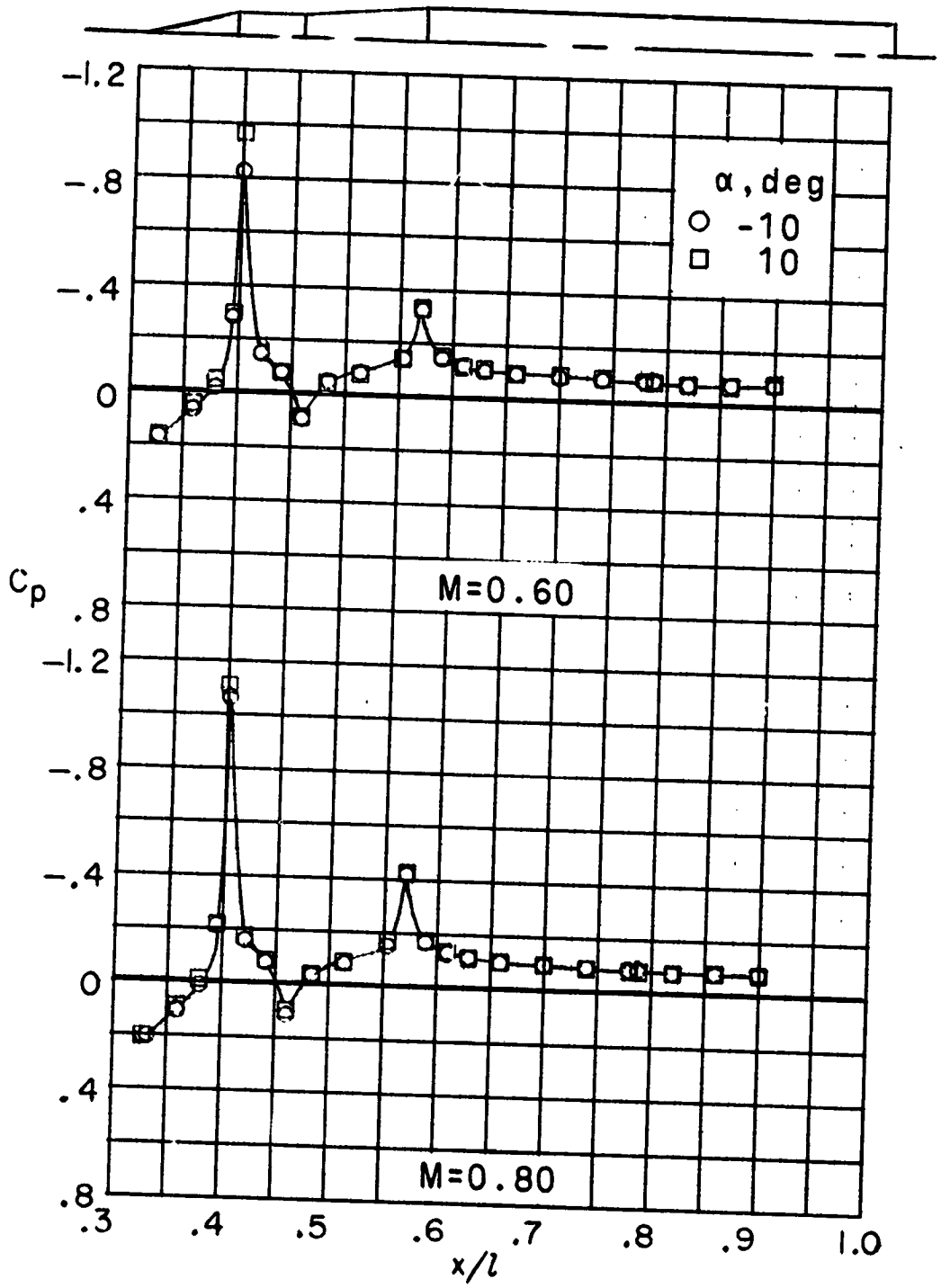
(b) Configuration 324, $\alpha = 0^{o}$.

Figure 3.- Continued.



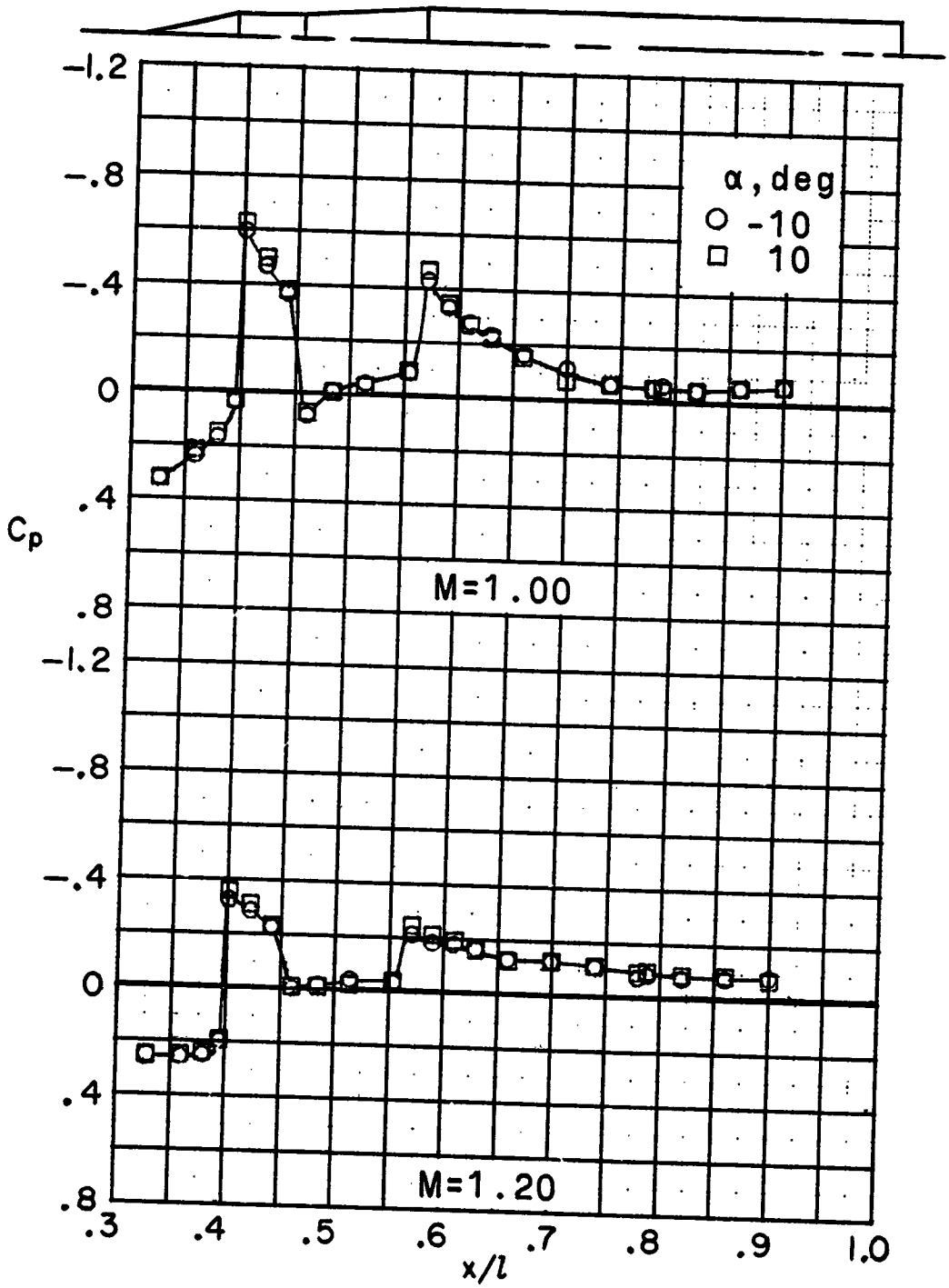
(b) Concluded.

Figure 3.- Continued.



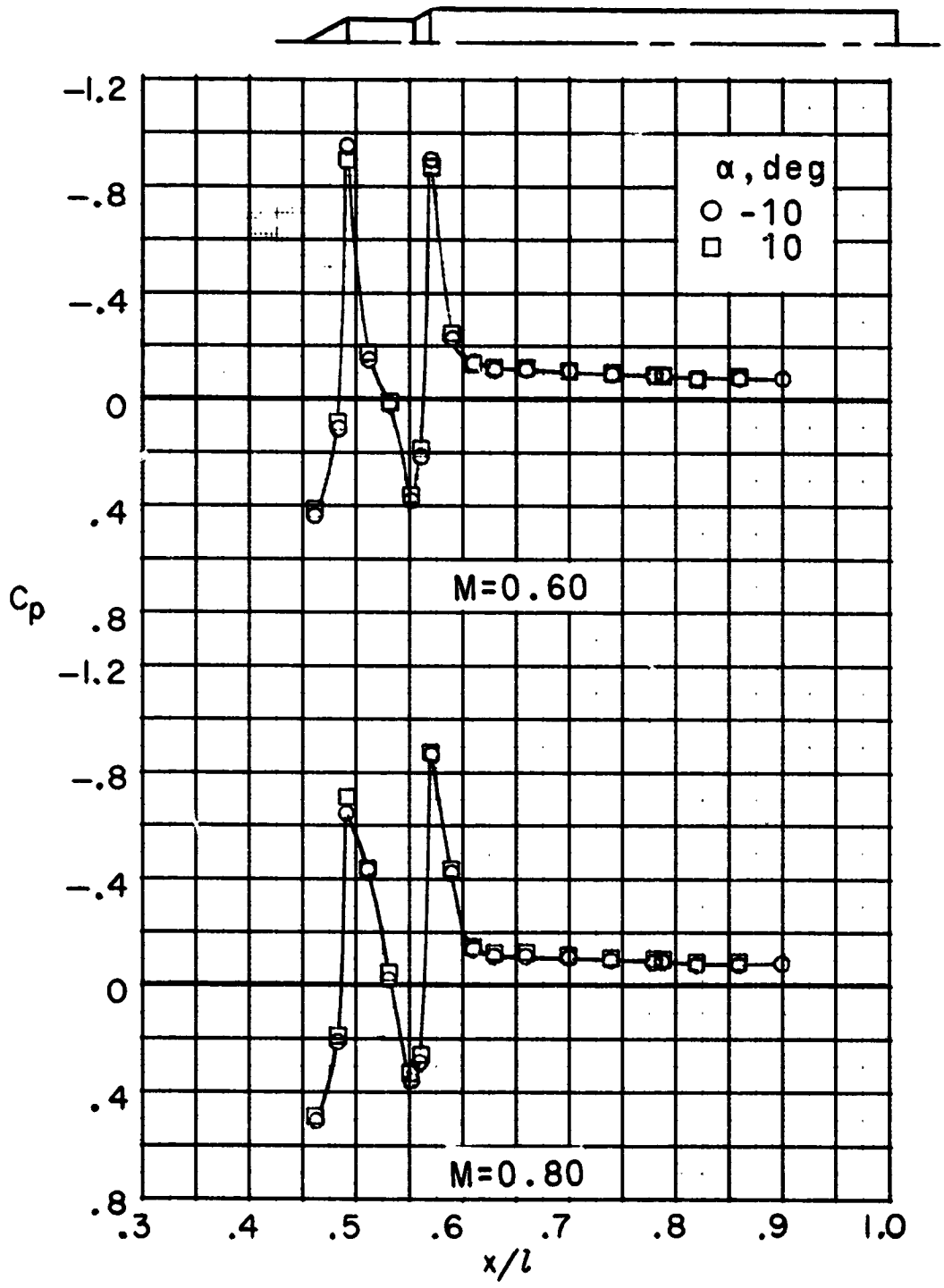
(c) Configuration 121, $\alpha = \pm 10^{o}$.

Figure 3.- Continued.



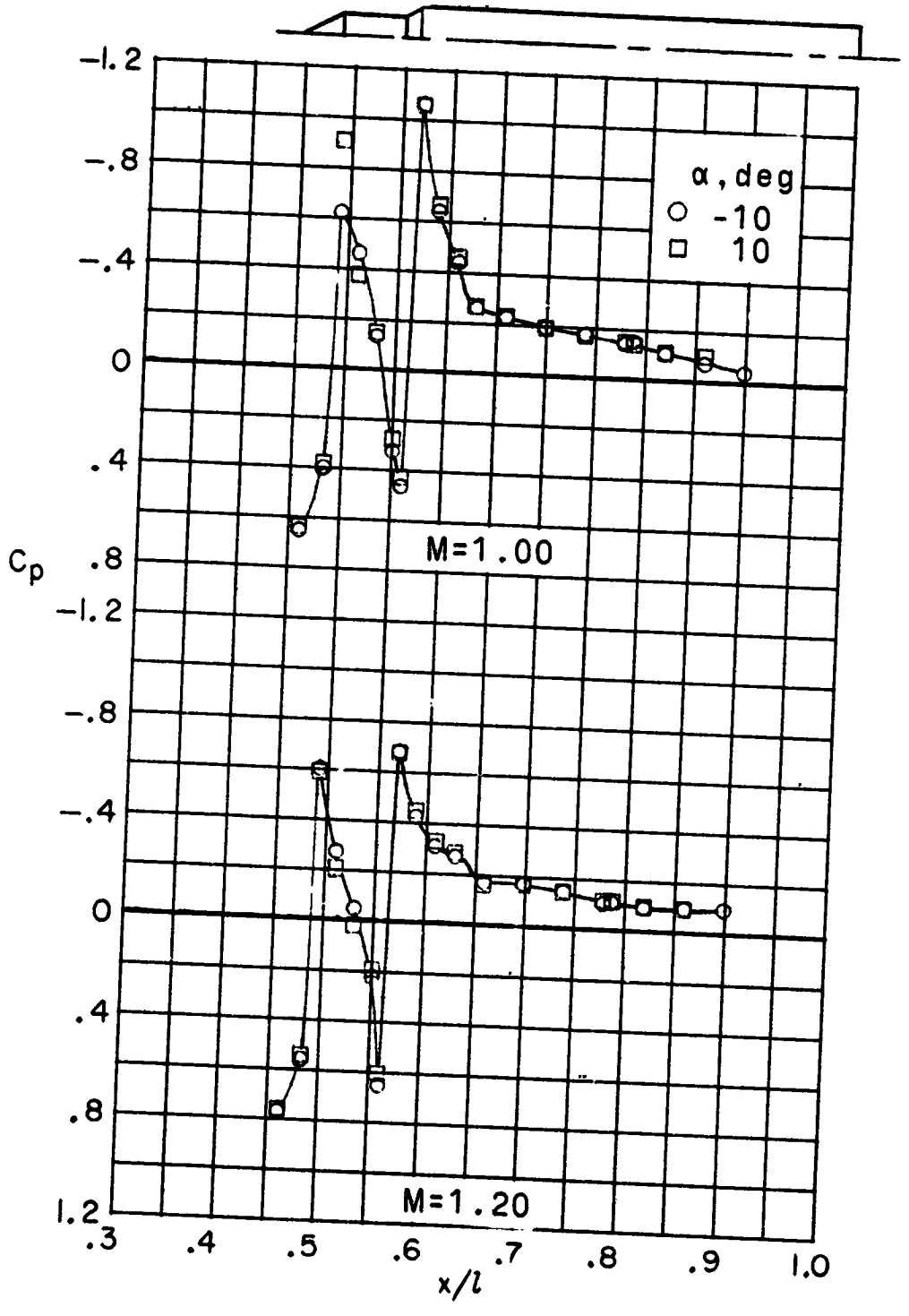
(c) Concluded.

Figure 3.- Continued.



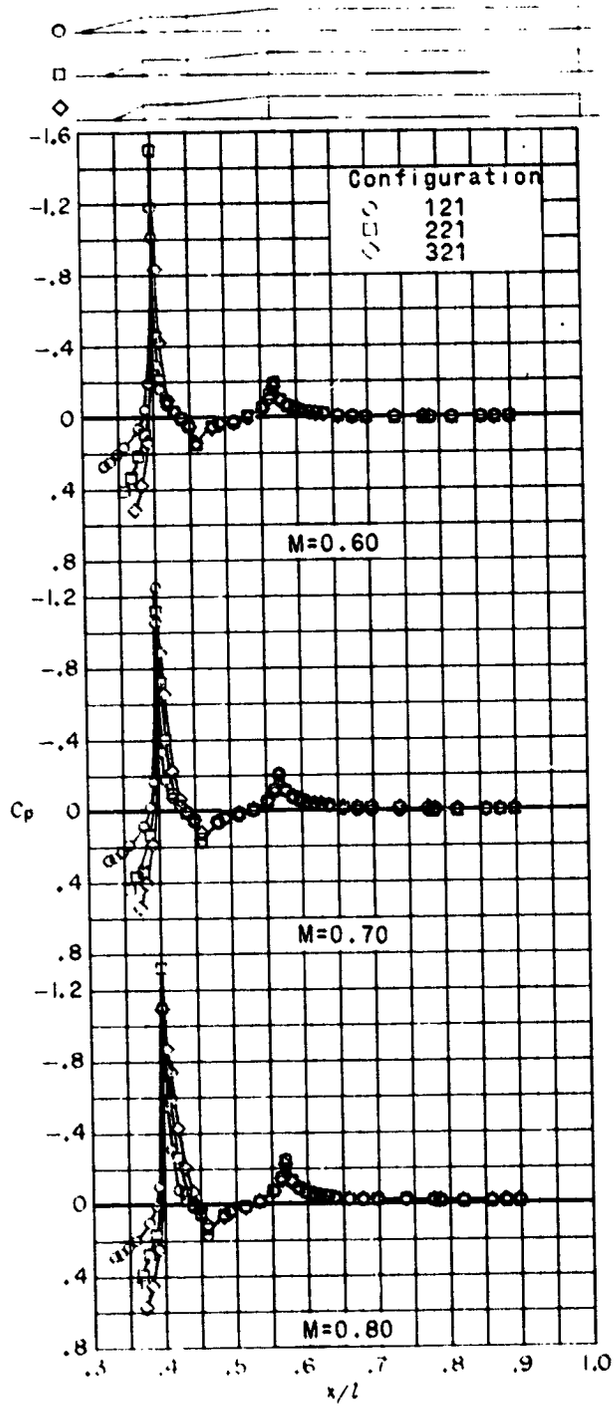
(d) Configuration 324, $\alpha = \pm 10^{o}$.

Figure 3.- Continued.



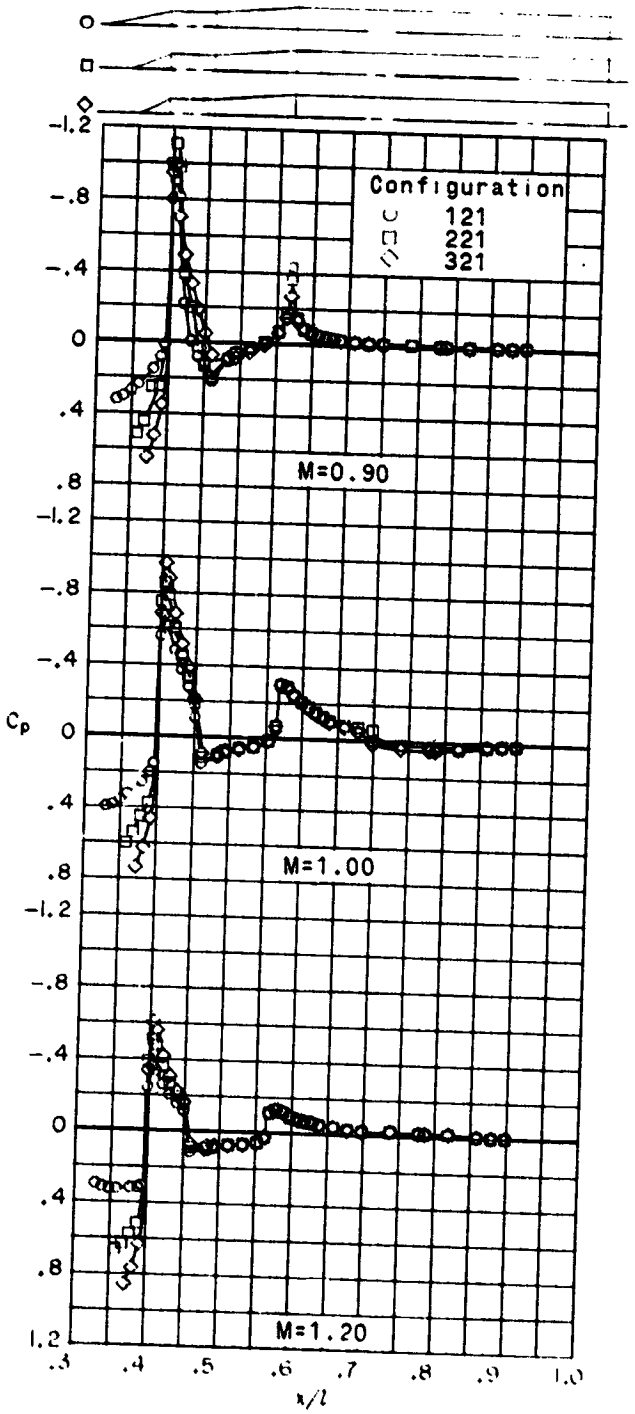
(d) Concluded.

Figure 3.- Concluded.



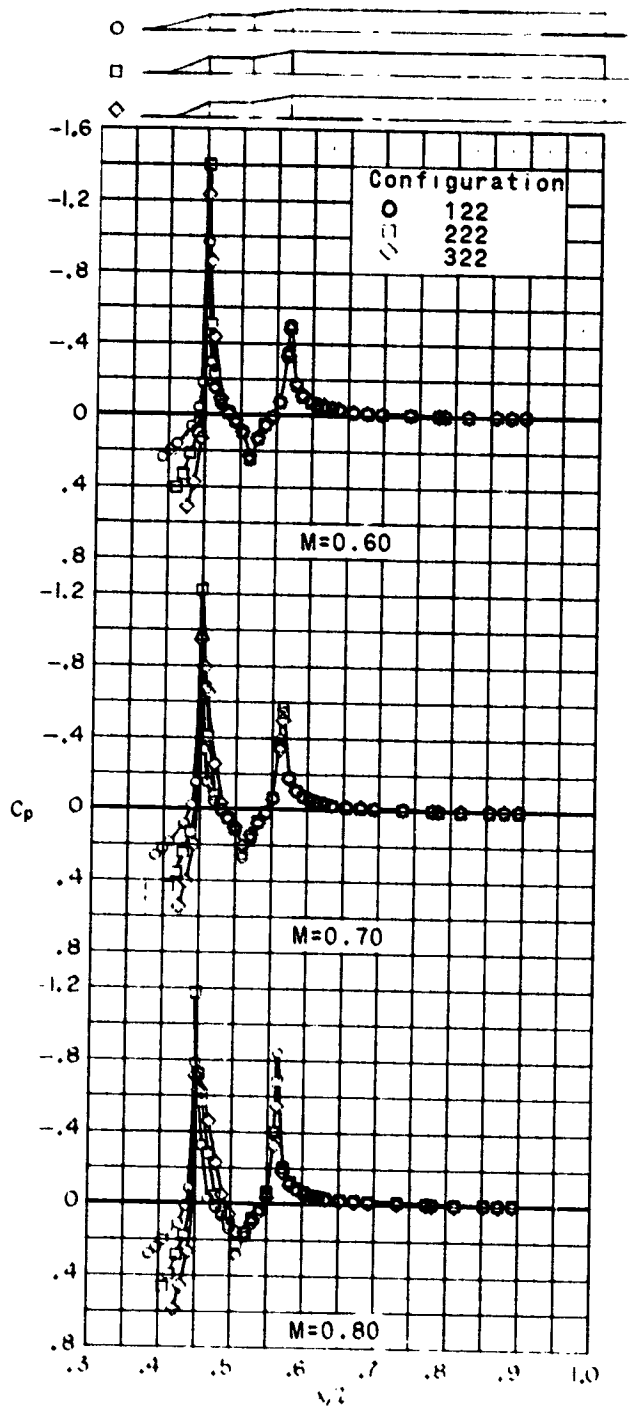
(a) $\delta_F = 5^o$.

Figure 4.- Effects of variation in nose-cone angle for $\phi = 0^o$ and $\alpha = 0^o$.



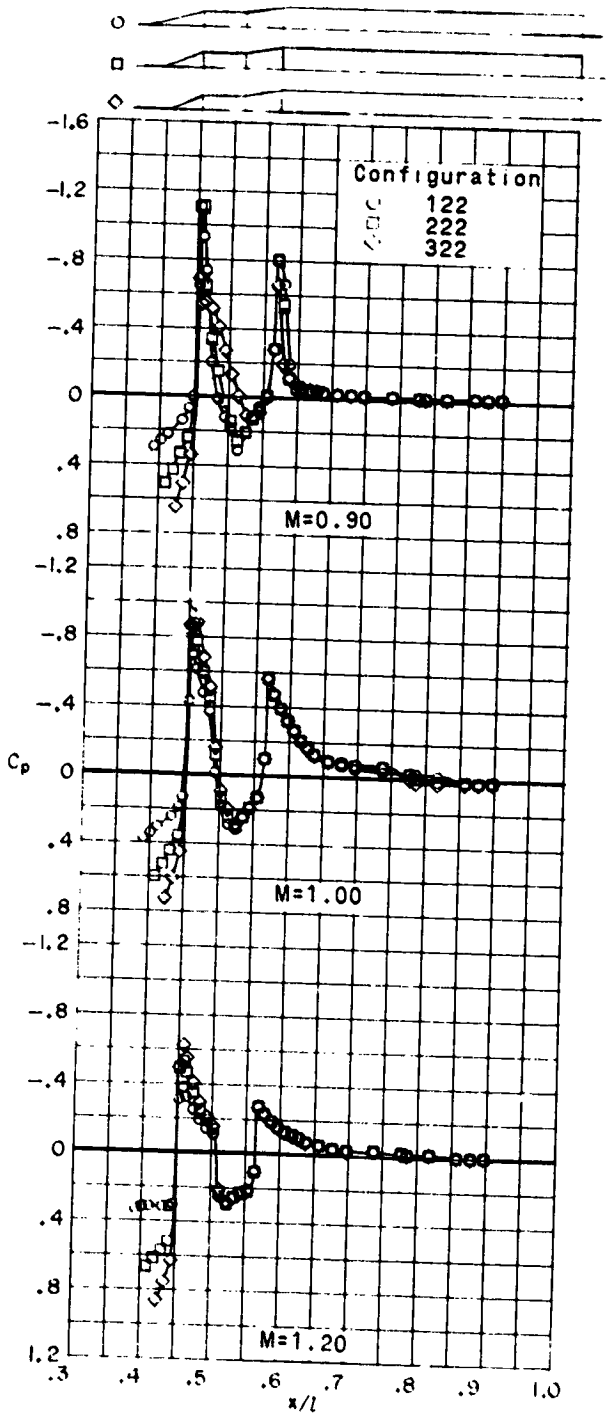
(a) Concluded.

Figure 4.- Continued.



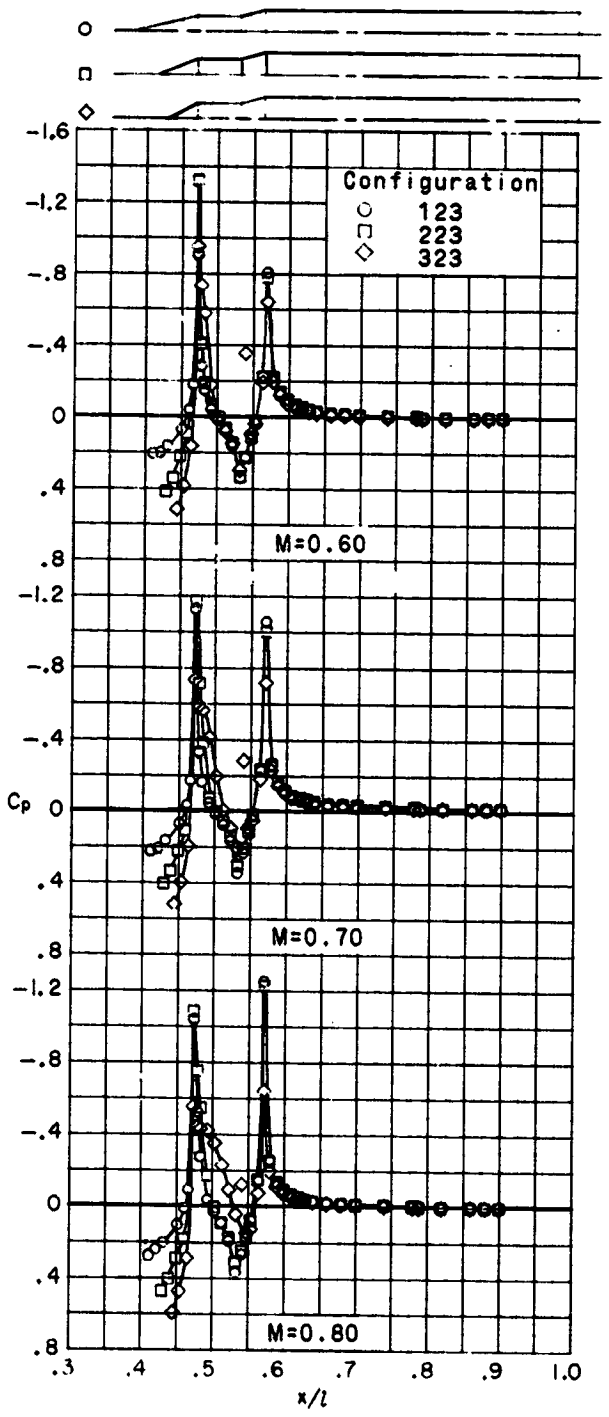
(b) $\delta_F = 10.1^o$.

Figure 4.- Continued.



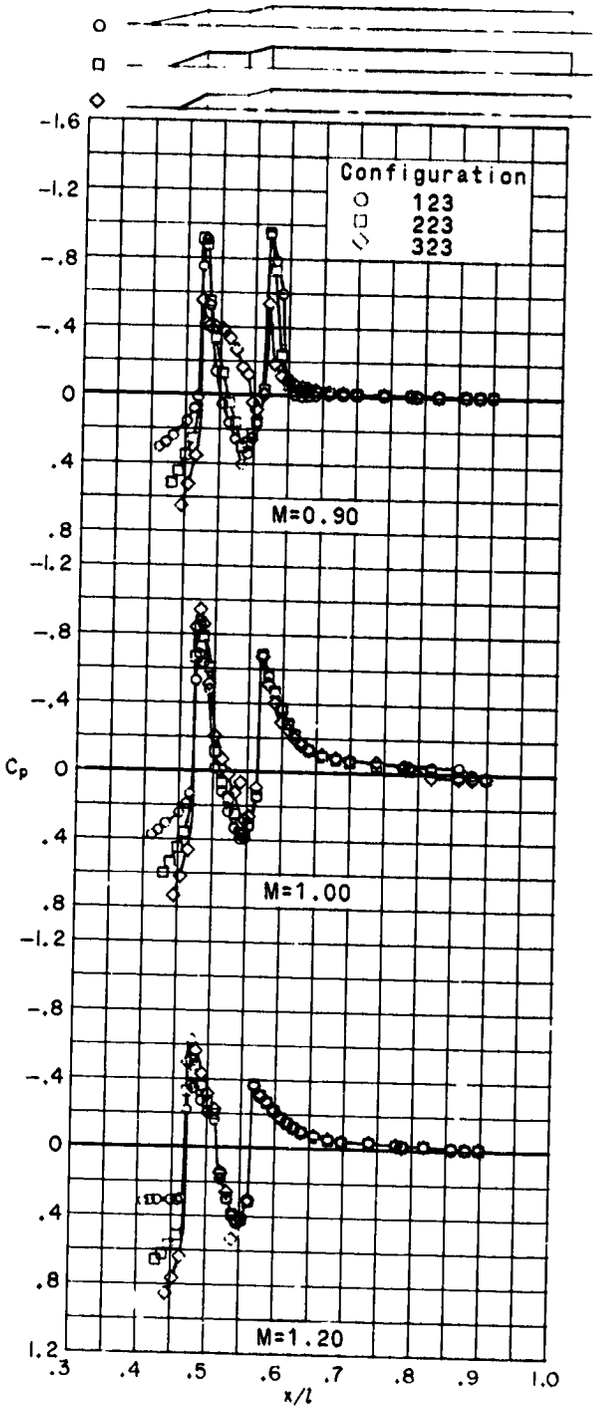
(b) Concluded.

Figure 4.- Continued.



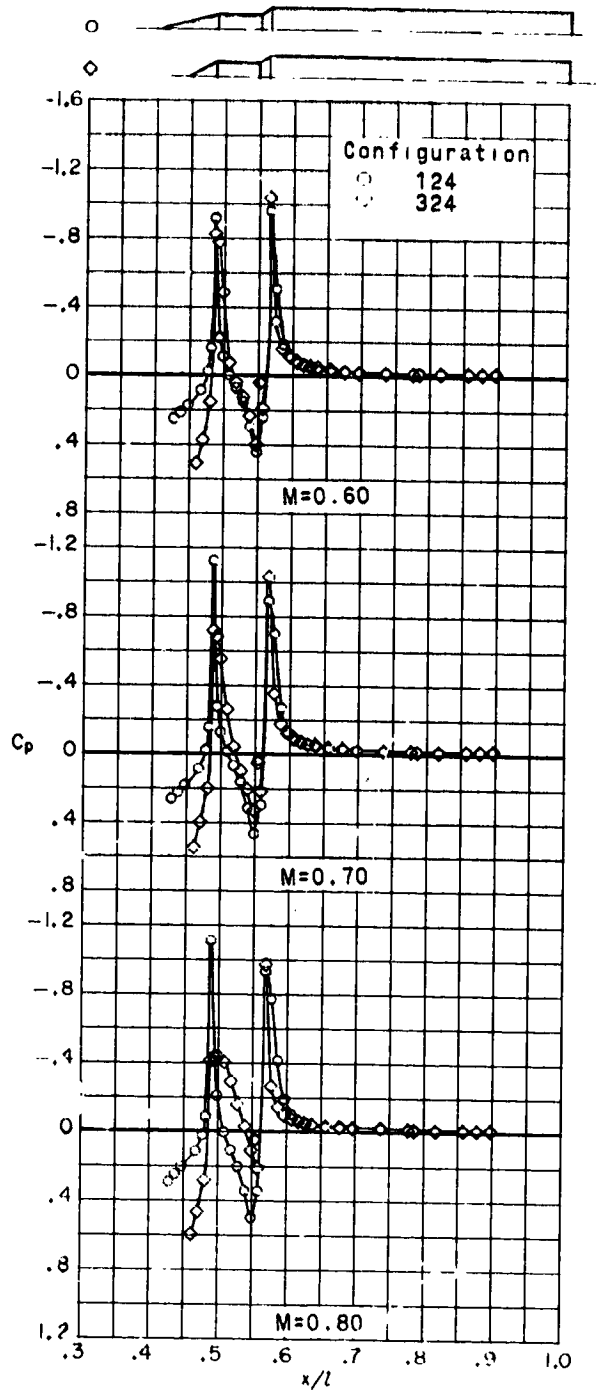
(c) $\delta_F = 15^o$.

Figure 4.- Continued.



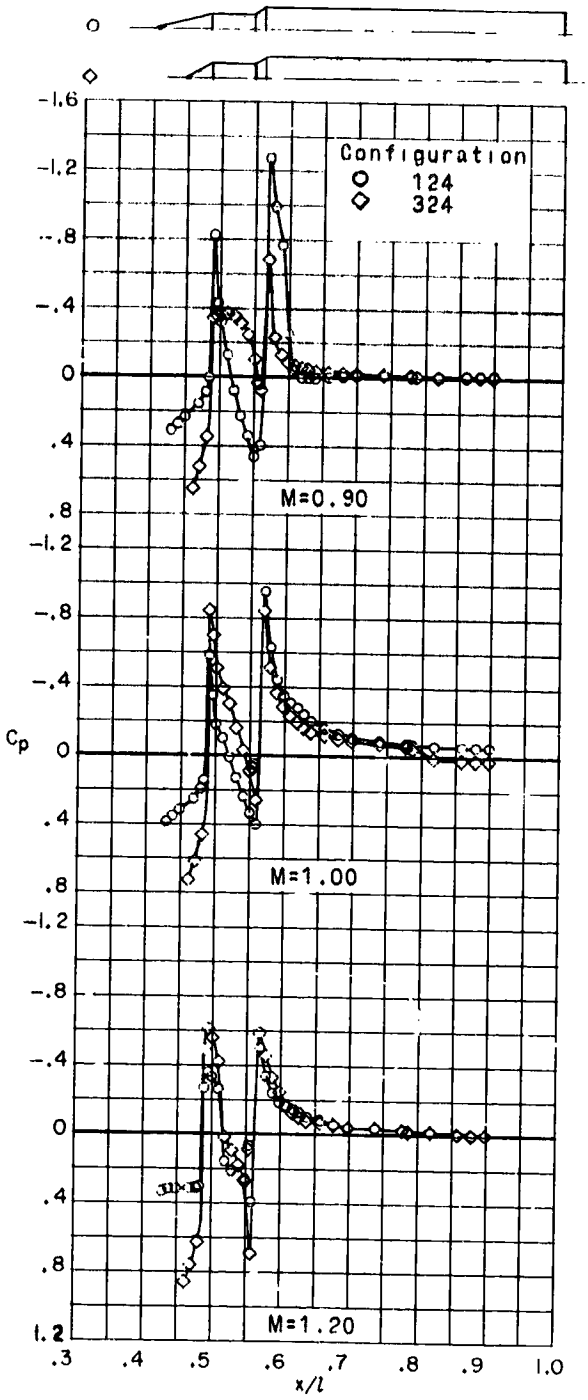
(c) Concluded.

Figure 4.- Continued.



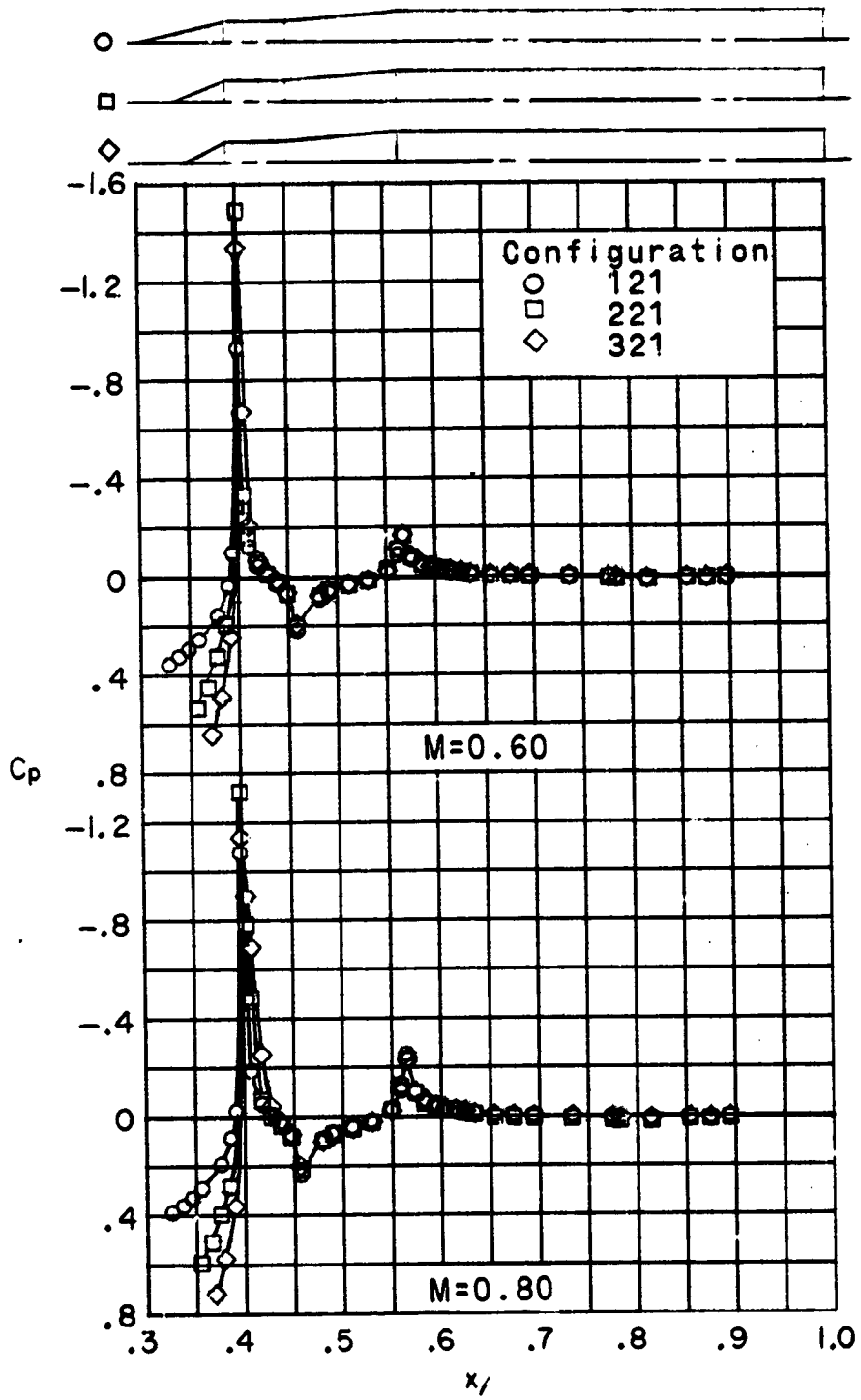
(d) $\delta_F = 30^o$.

Figure 4.- Continued.



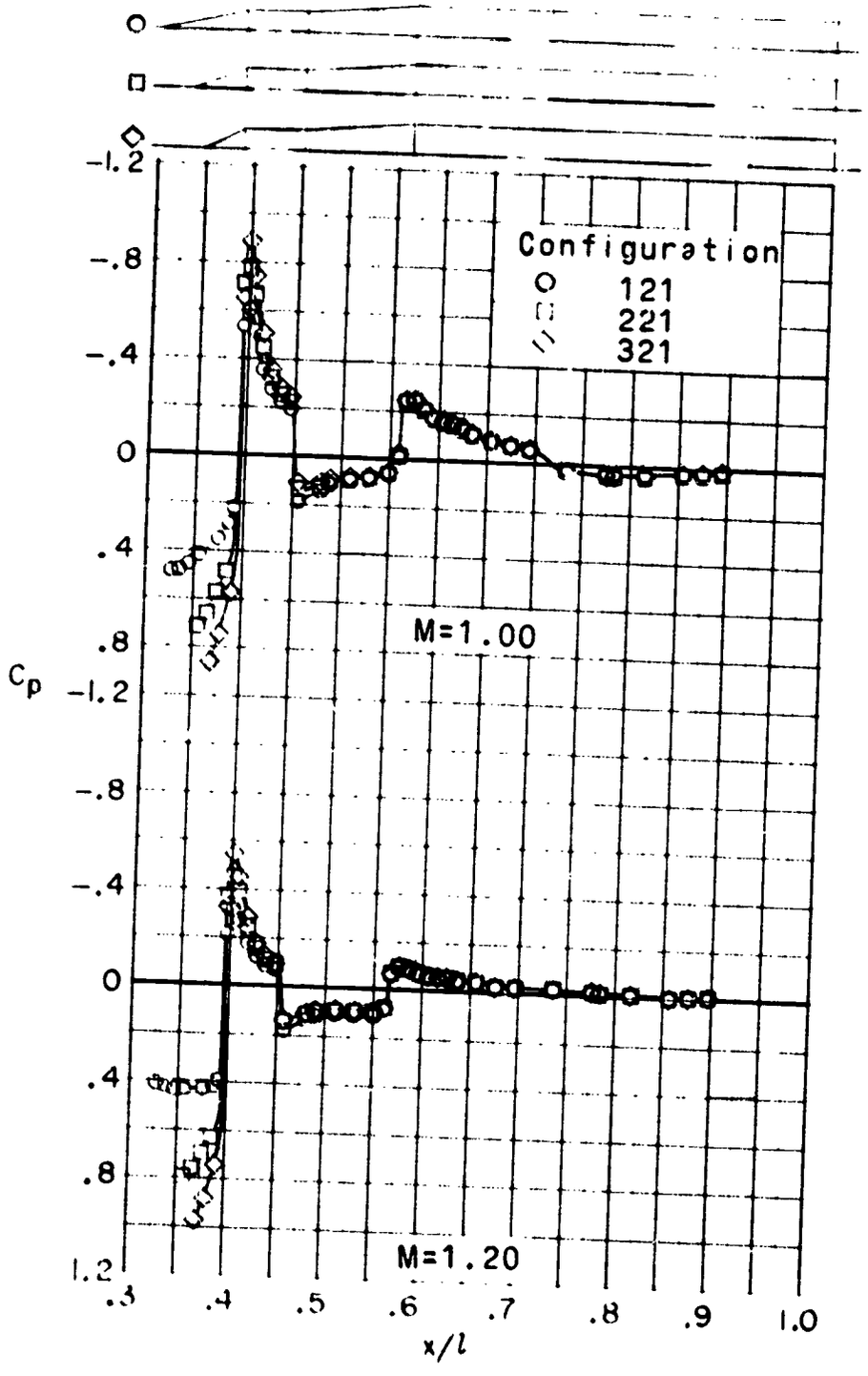
(d) Concluded.

Figure 4.- Concluded.



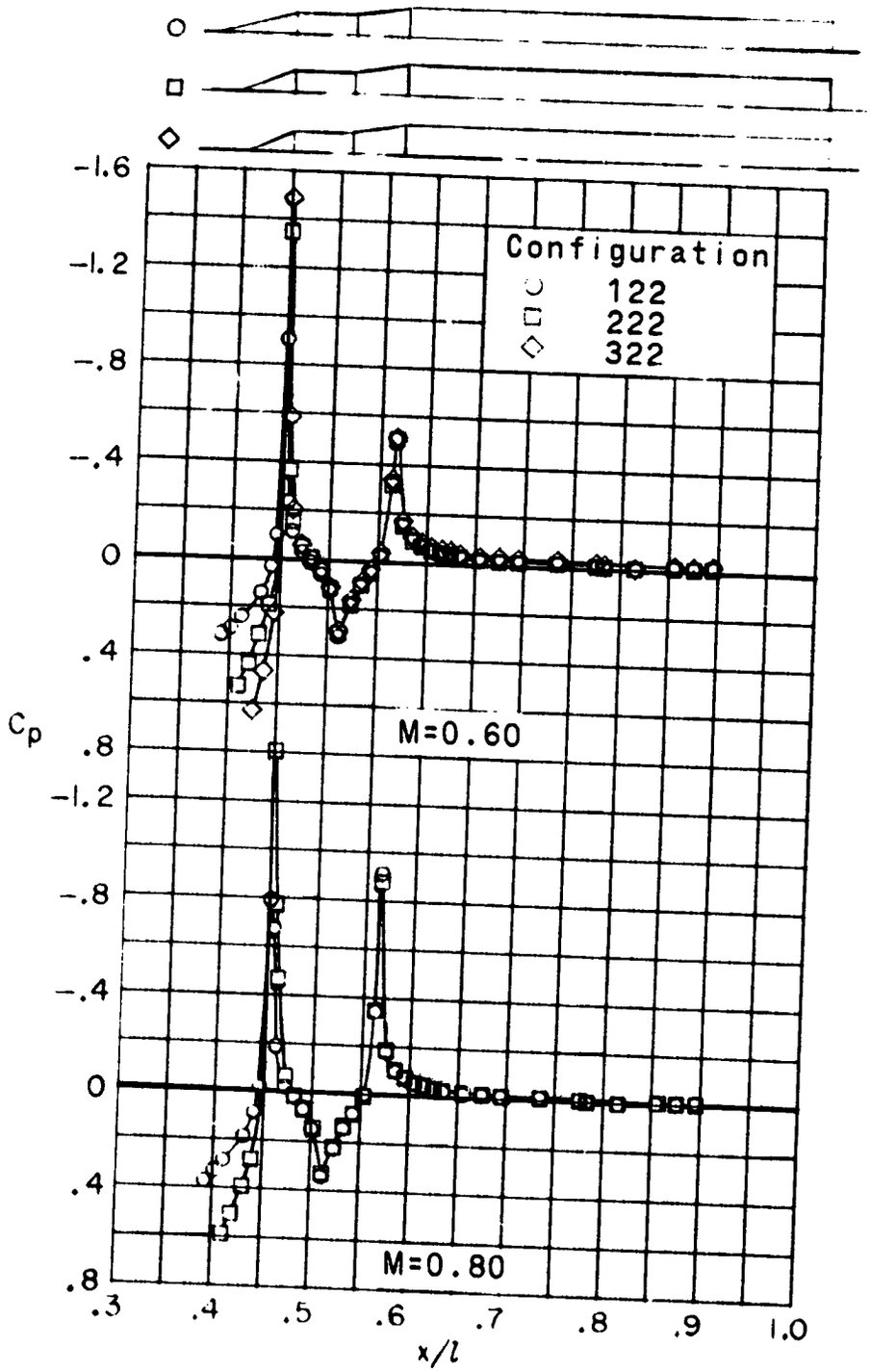
(a) $\delta_F = 5^o$.

Figure 5.- Effects of variation in nose-cone angle for $\phi = 0^o$ and $\alpha = -6^o$.



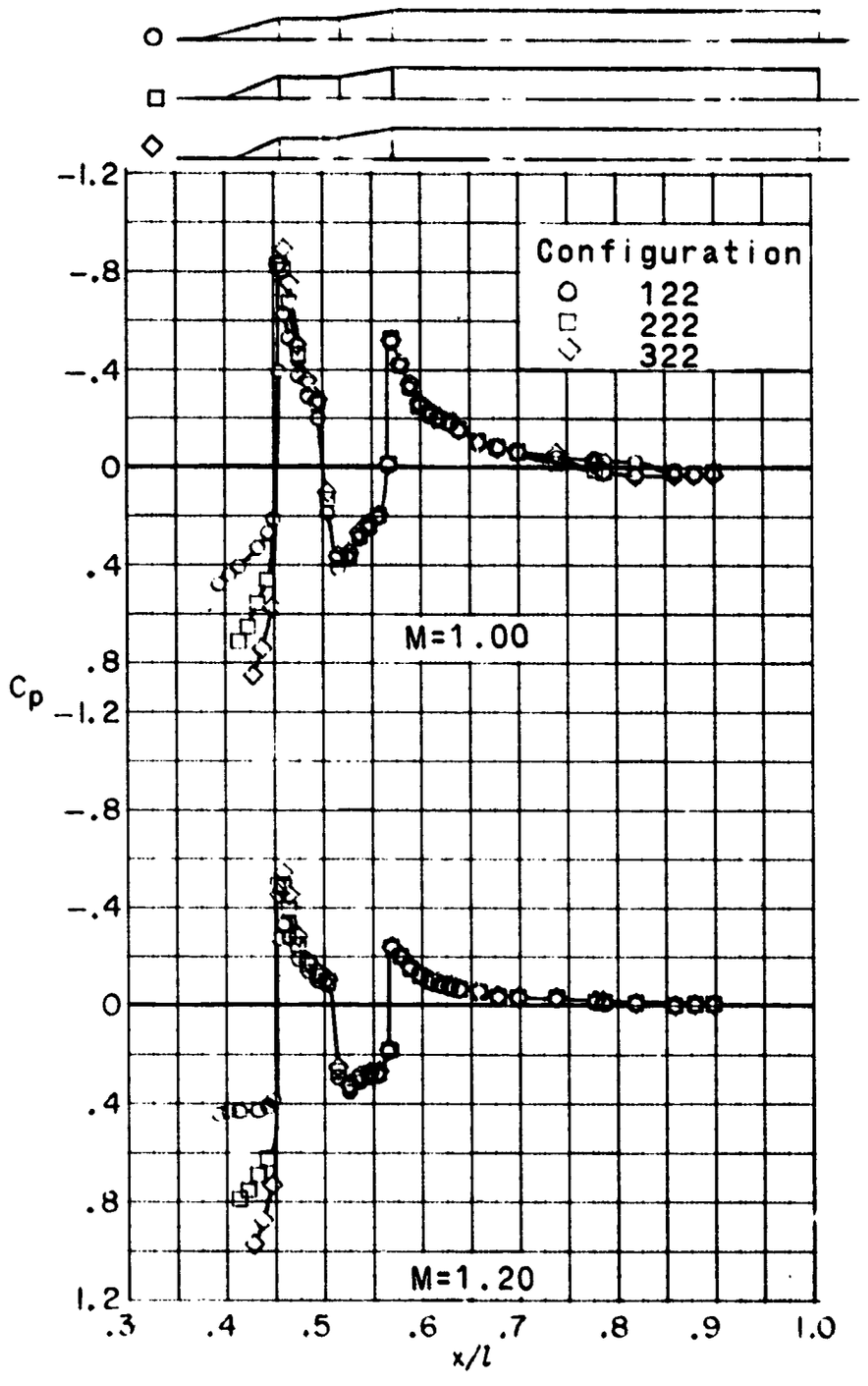
(a) Concluded.

Figure 5.- Continued.



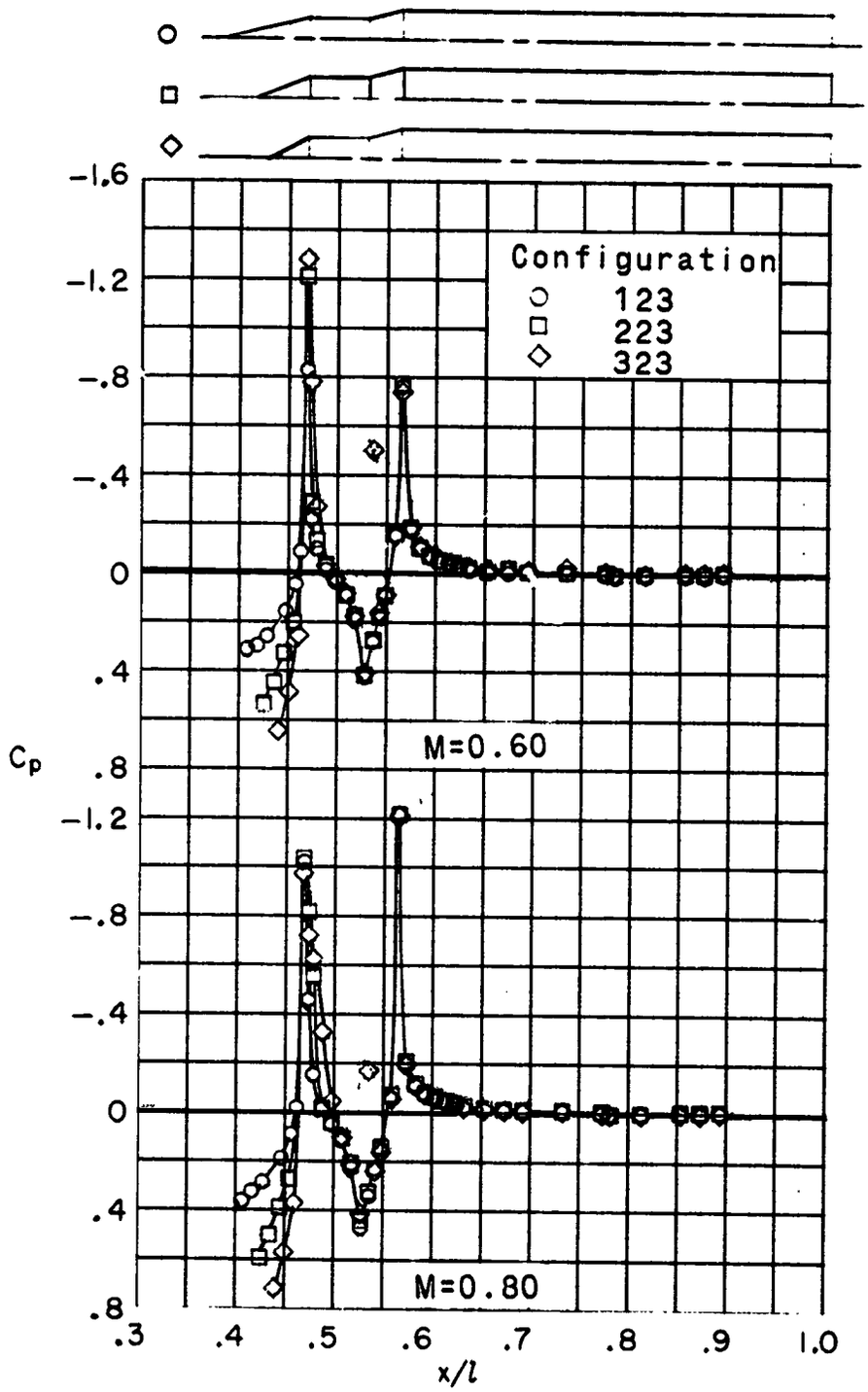
(b) $\delta_F = 10.1^o$.

Figure 5.- Continued.



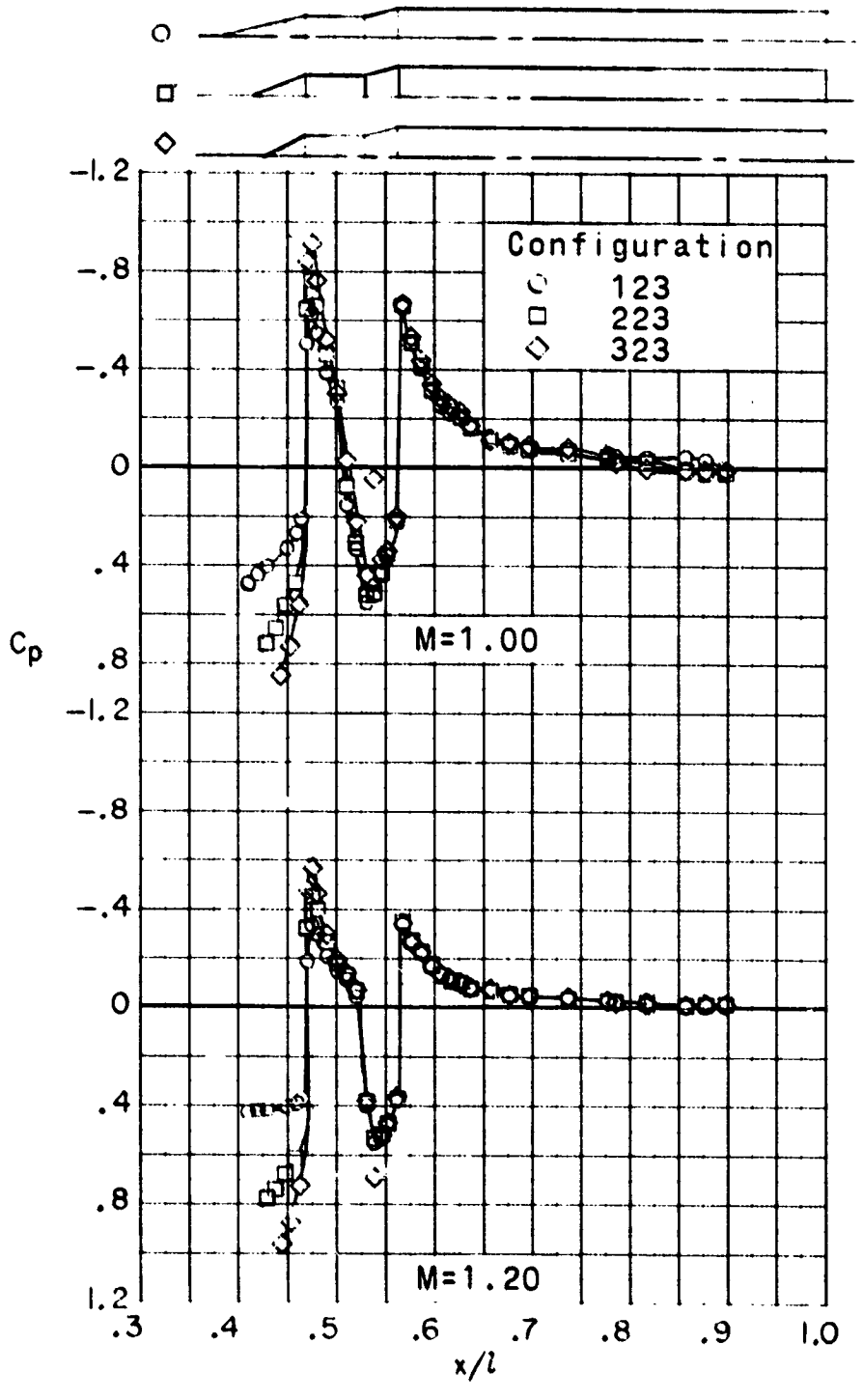
(b) Concluded.

Figure 5.- Continued.



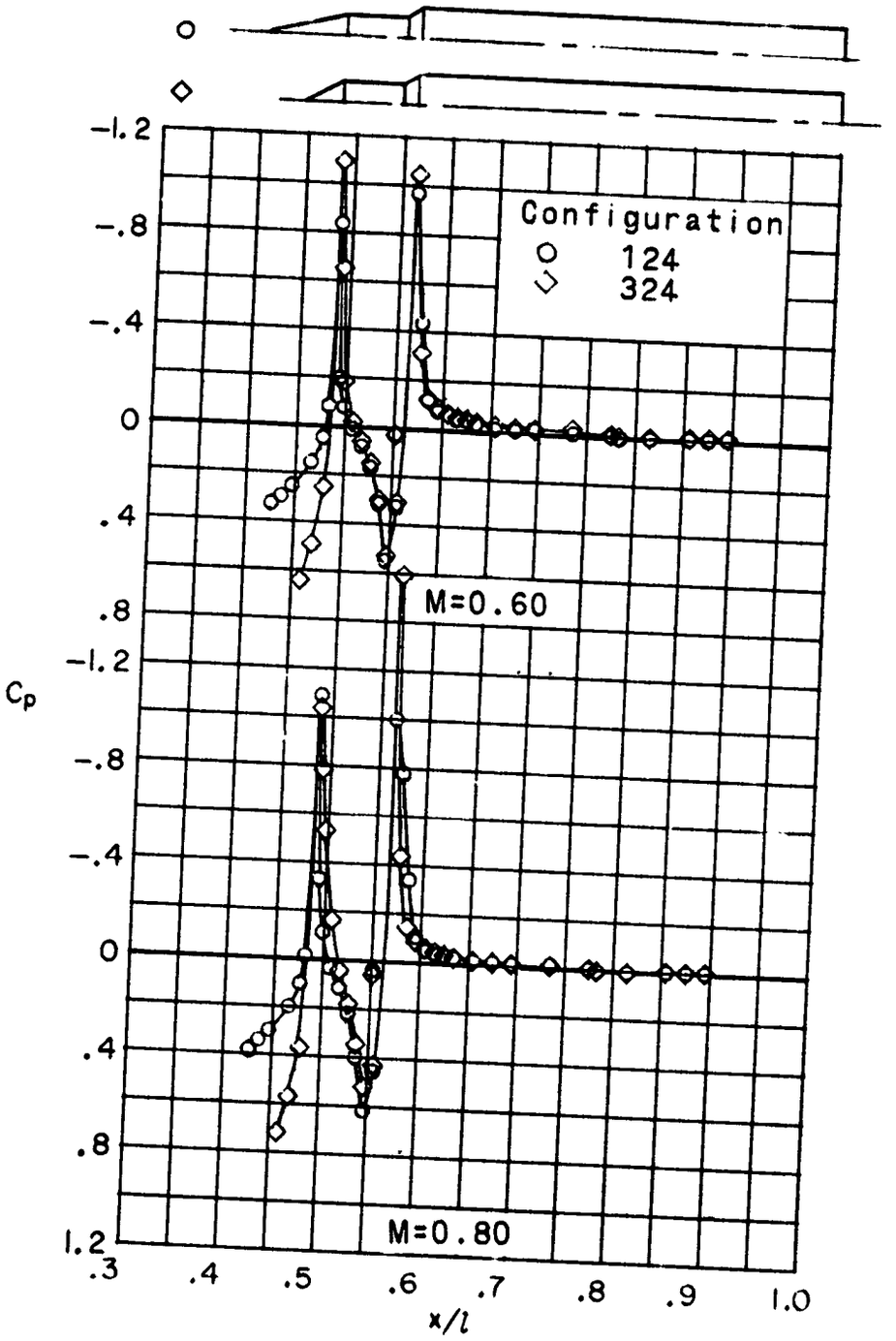
(c) $\delta_F = 15^o$.

Figure 5.- Continued.



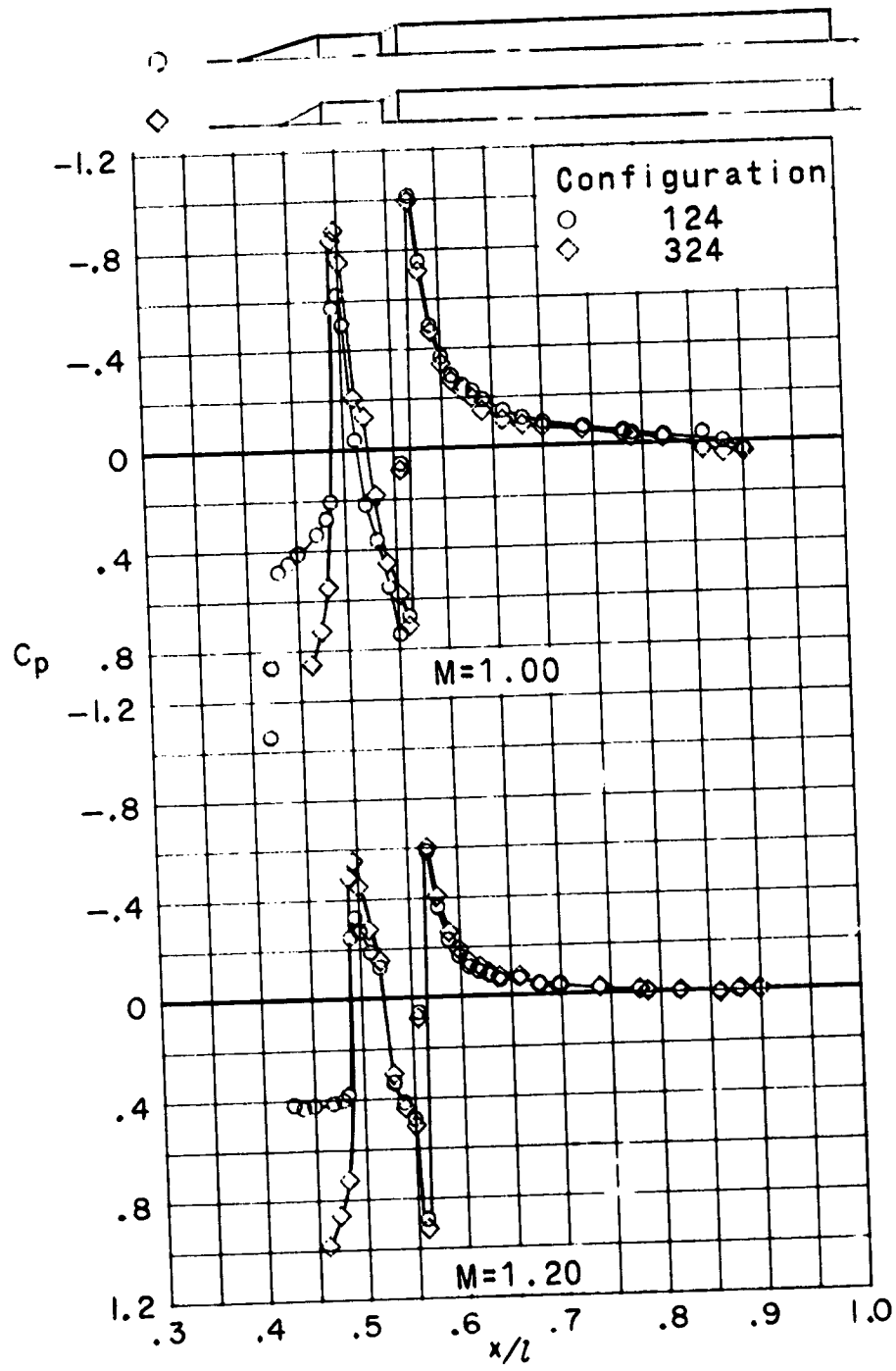
(c) Concluded.

Figure 5.- Continued.



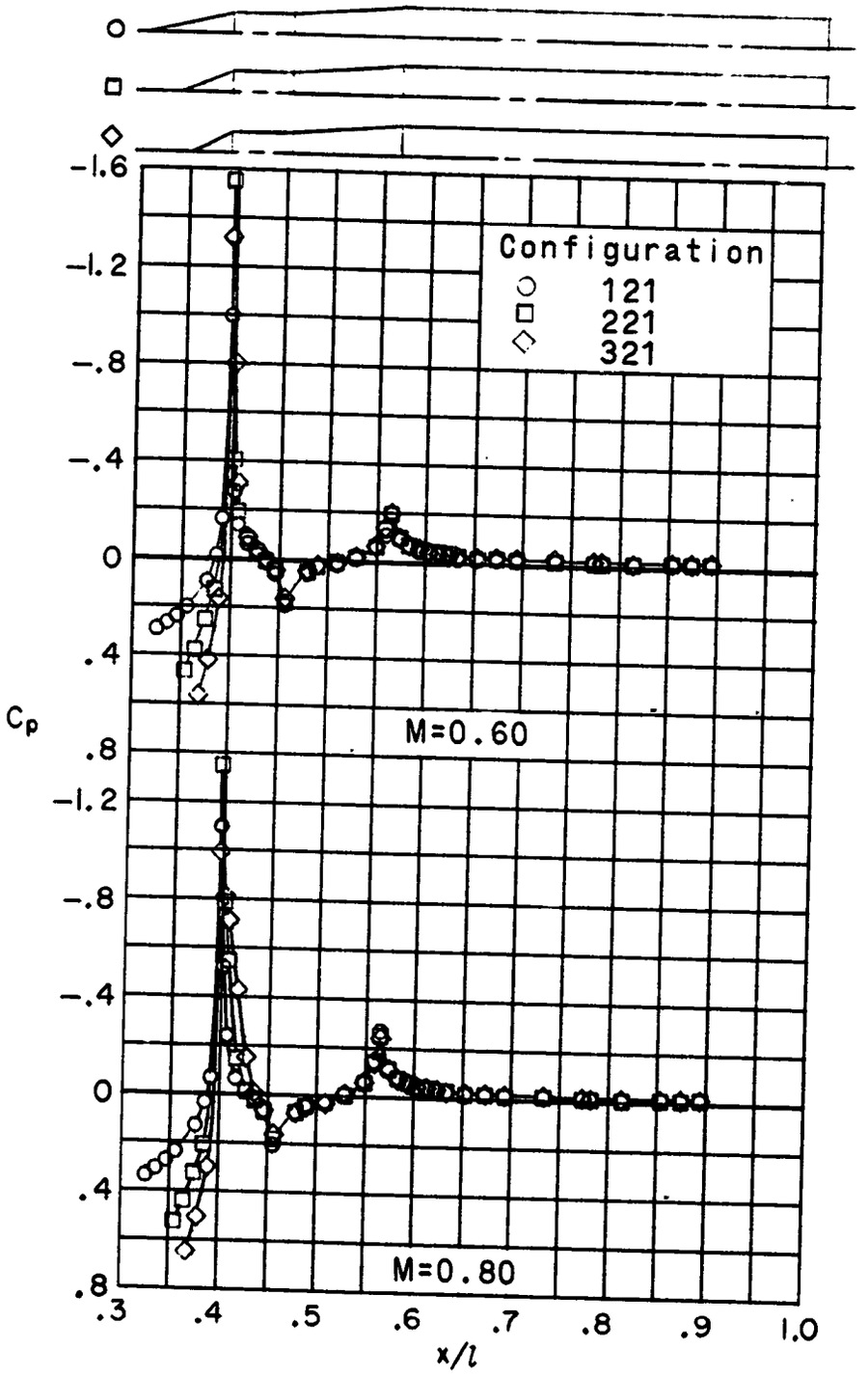
(d) $\delta_F = 30°$.

Figure 5.- Continued.



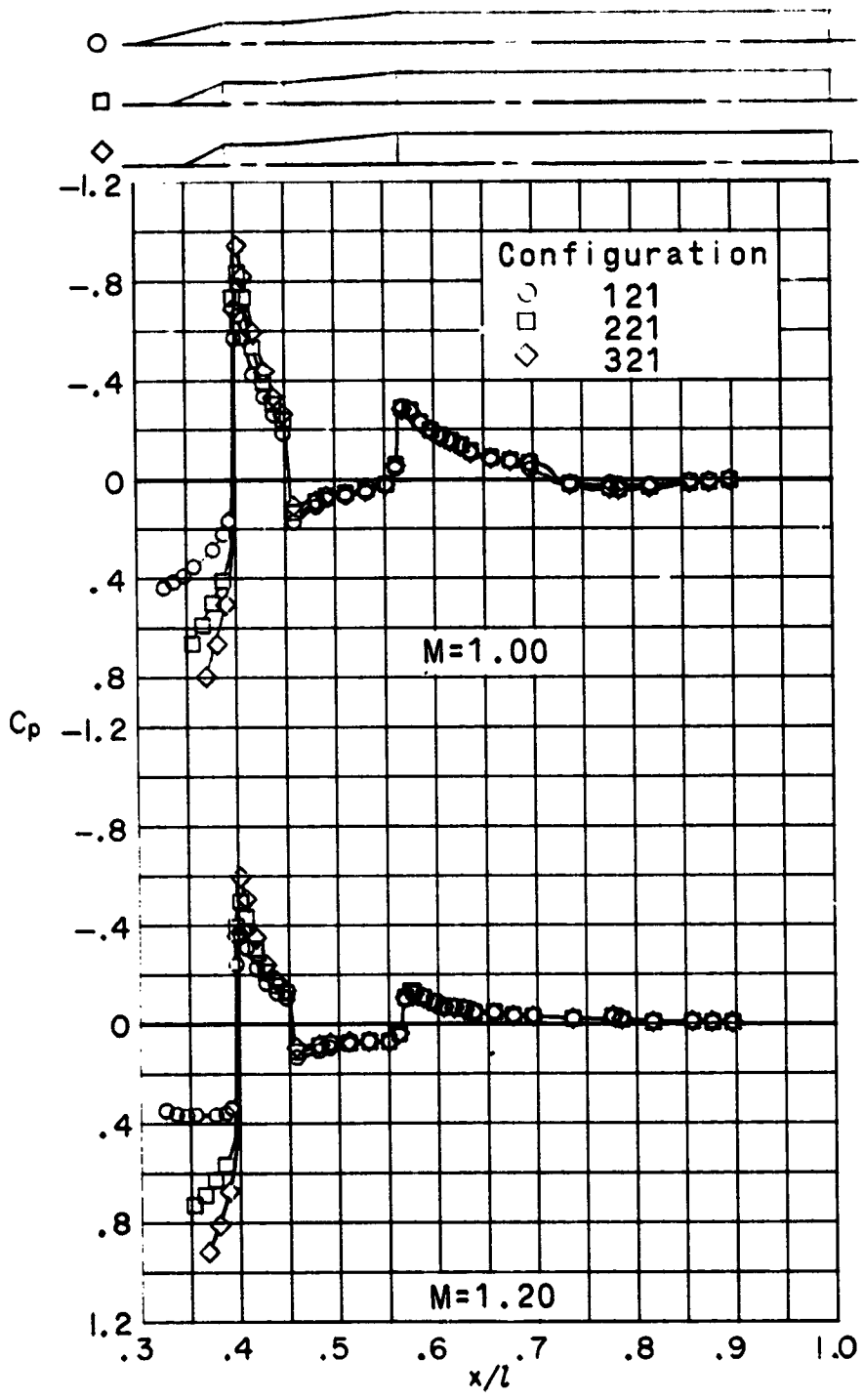
(d) Concluded.

Figure 5.- Concluded.



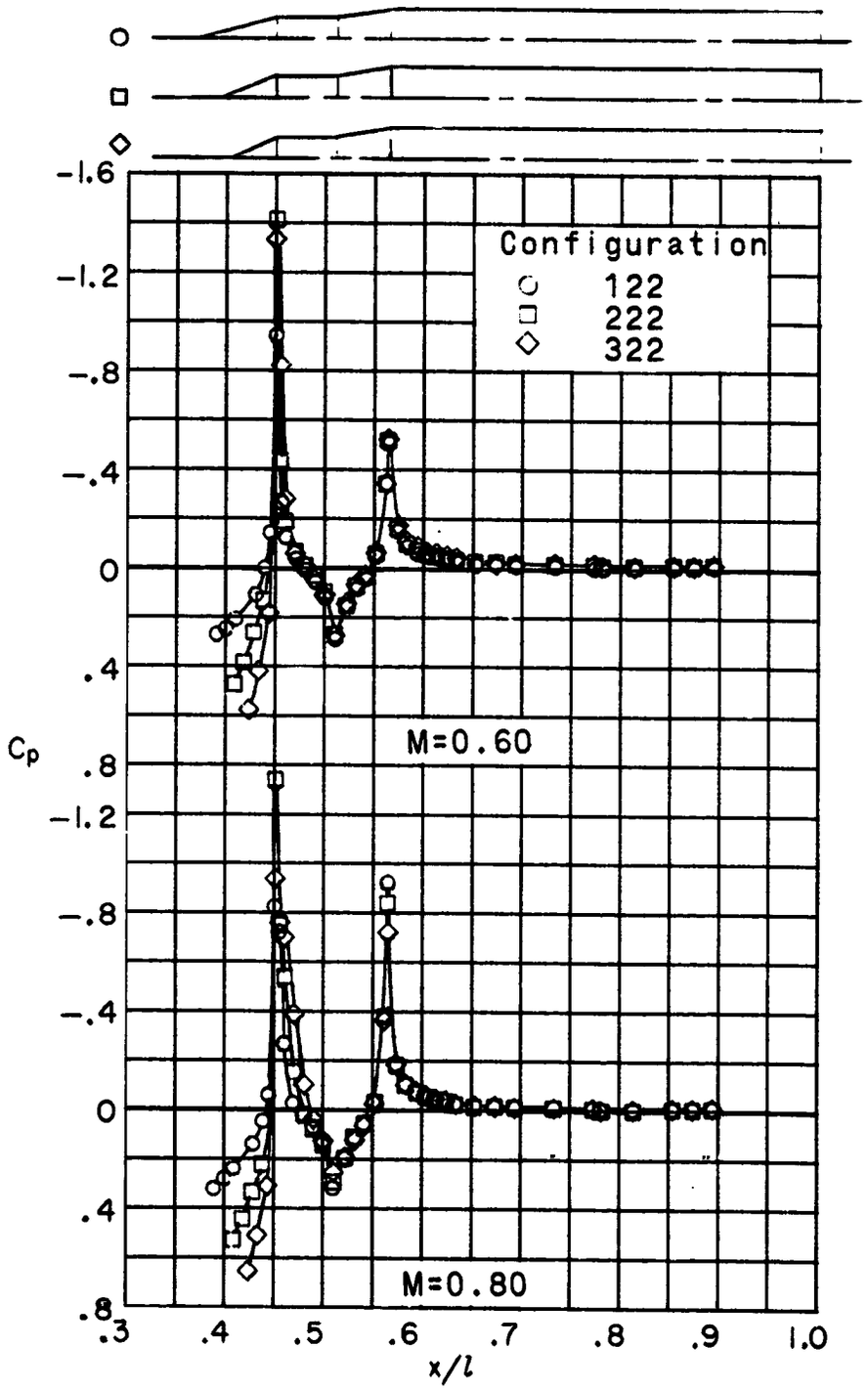
(a) $\delta_F = 5^o$.

Figure 6.- Effects of variation in nose-cone angle for $\phi = 0^o$ and $\alpha = -3^o$.



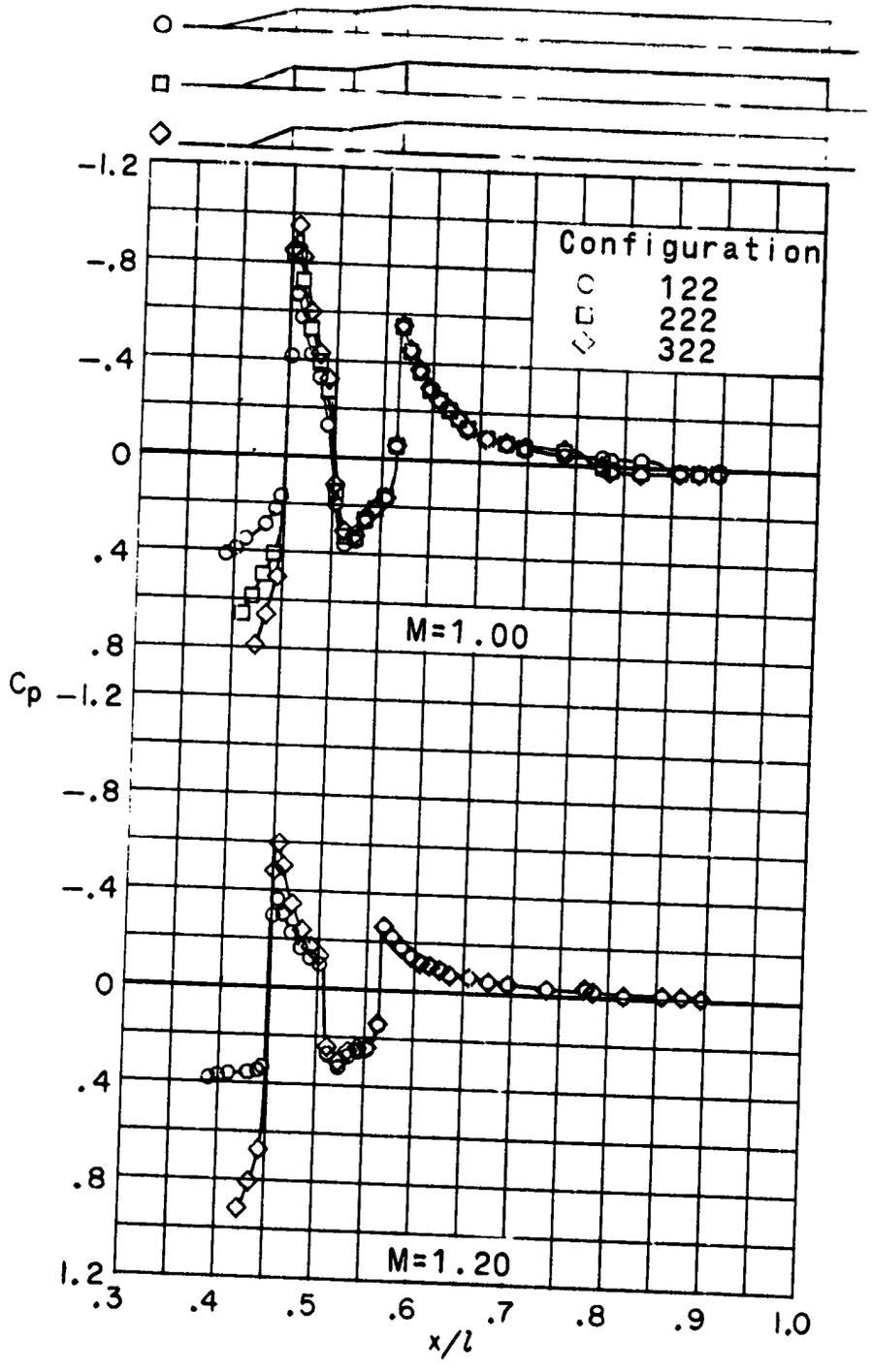
(a) Concluded.

Figure 6.- Continued.



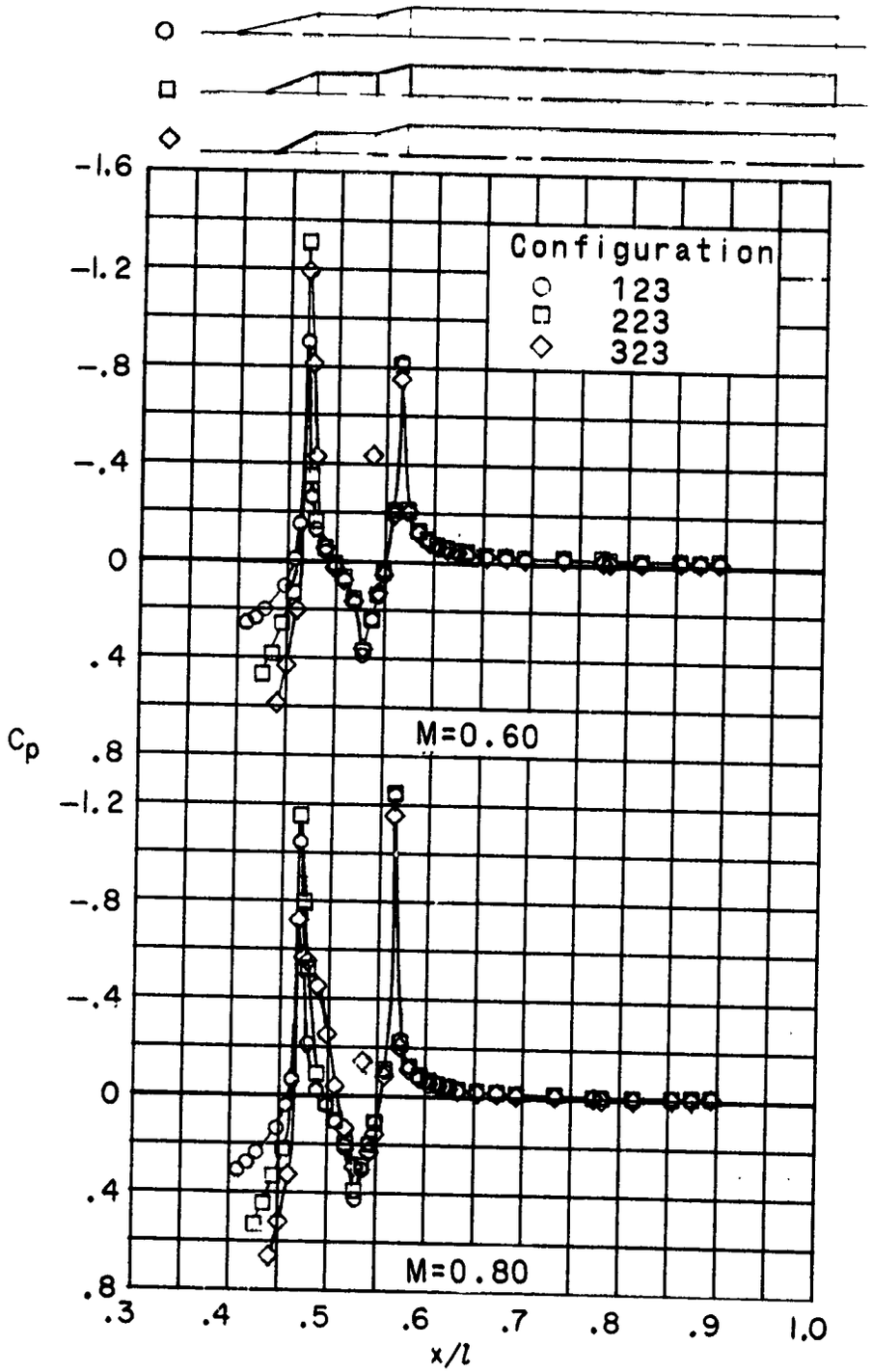
(b) $\delta_F = 10.1°$.

Figure 6.- Continued.



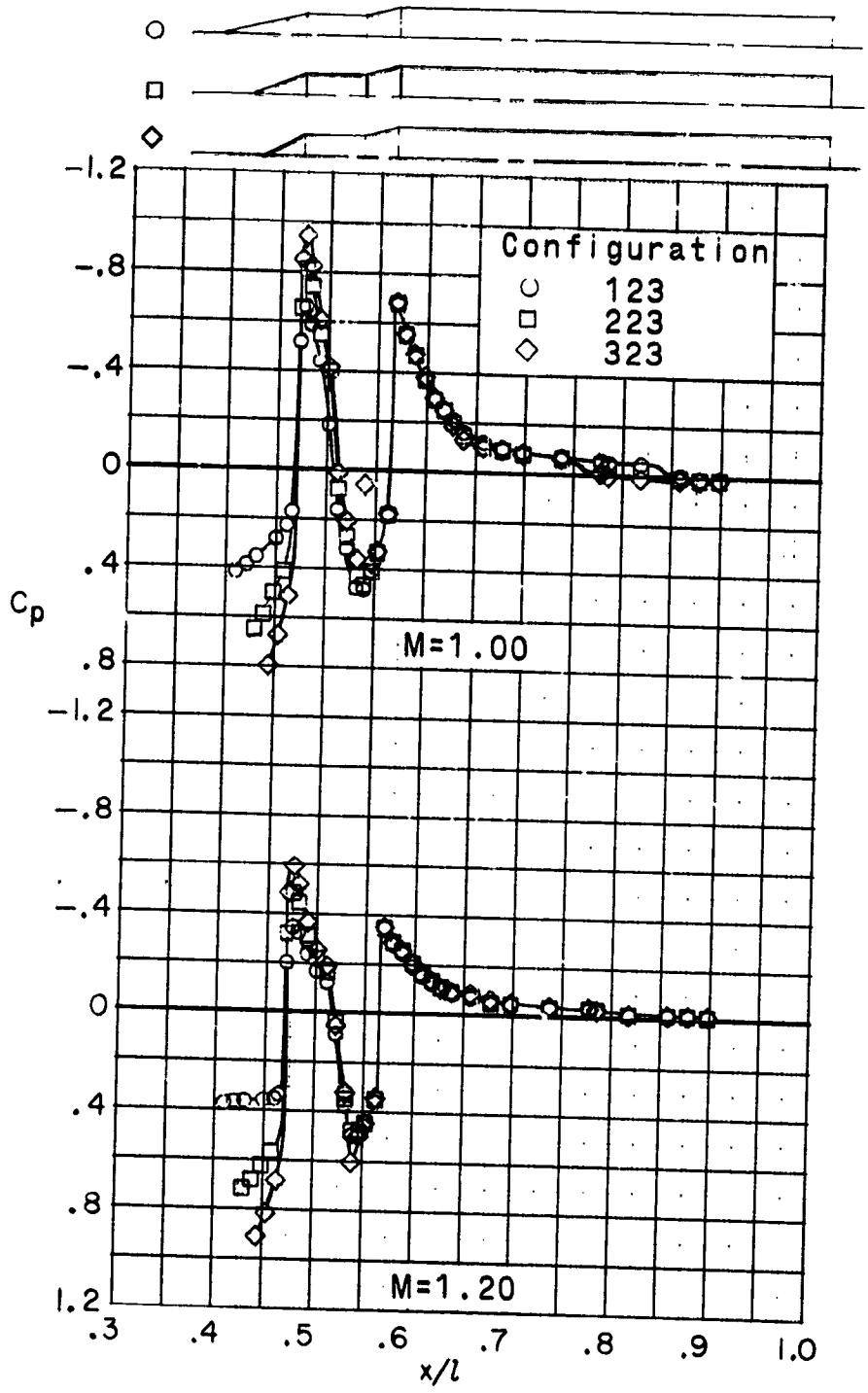
(b) Concluded.

Figure 6.- Continued.



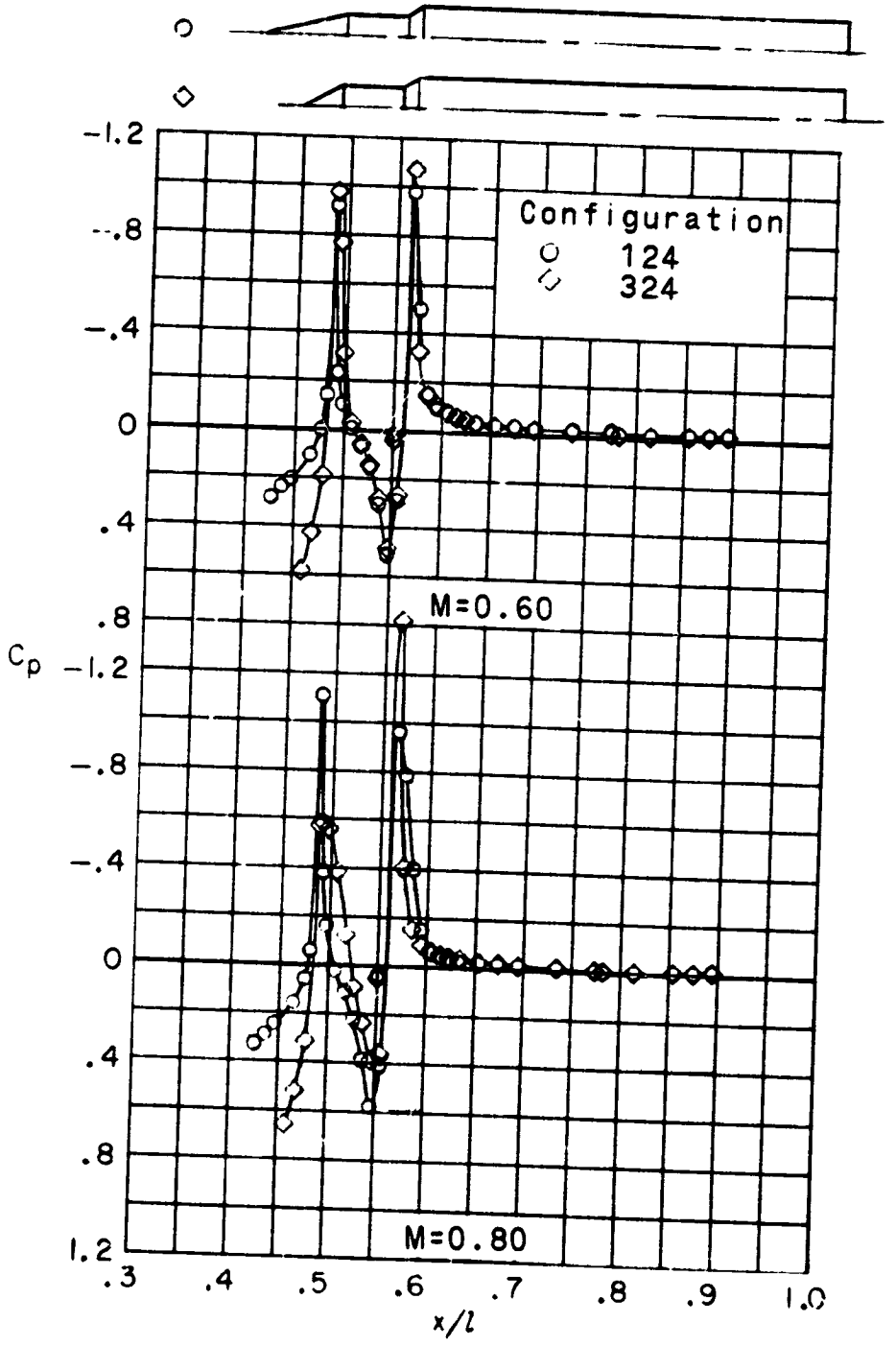
(c) $\delta_F = 15^o$.

Figure 6.- Continued.



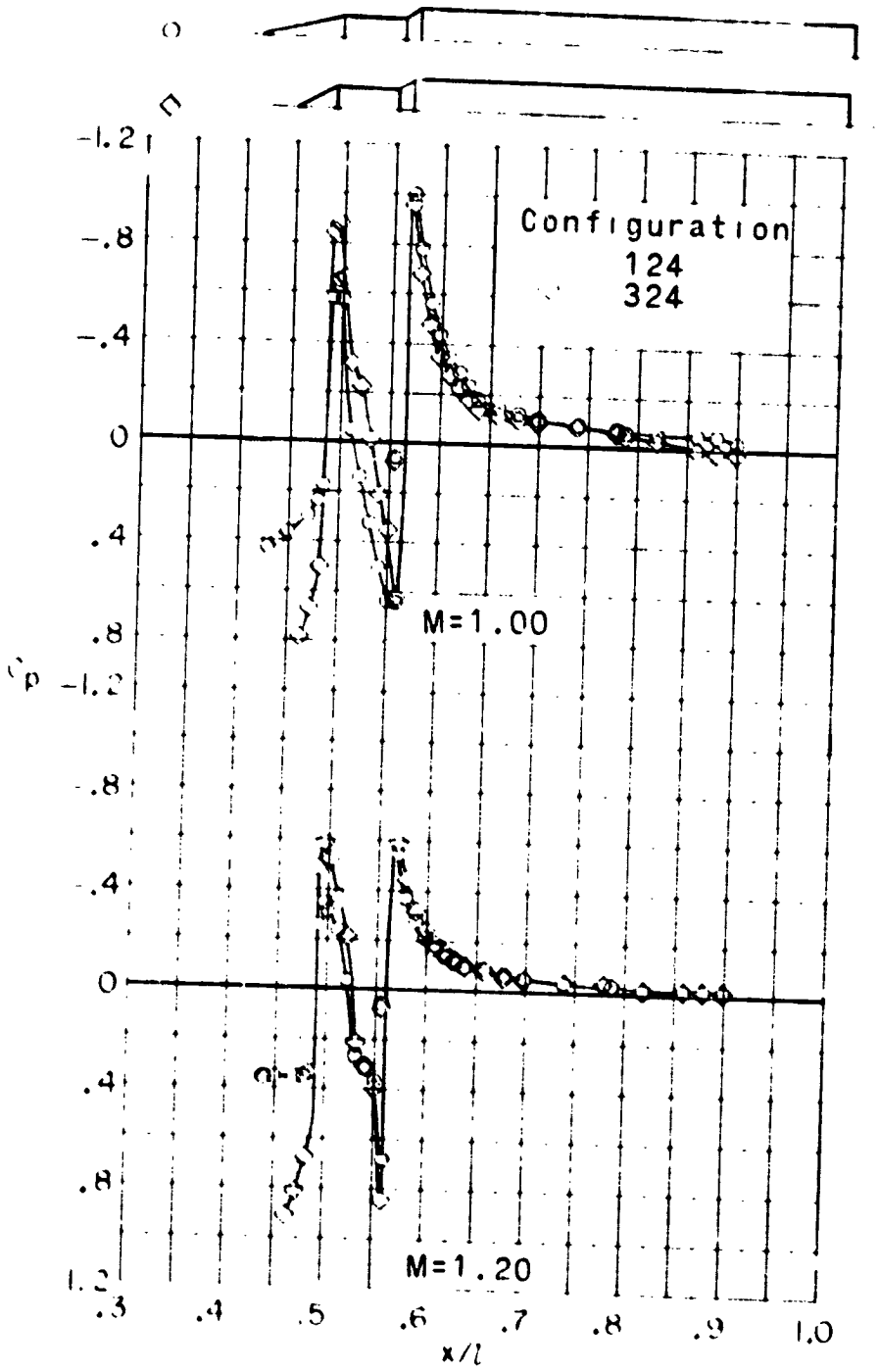
(c) Concluded.

Figure 6.- Continued.



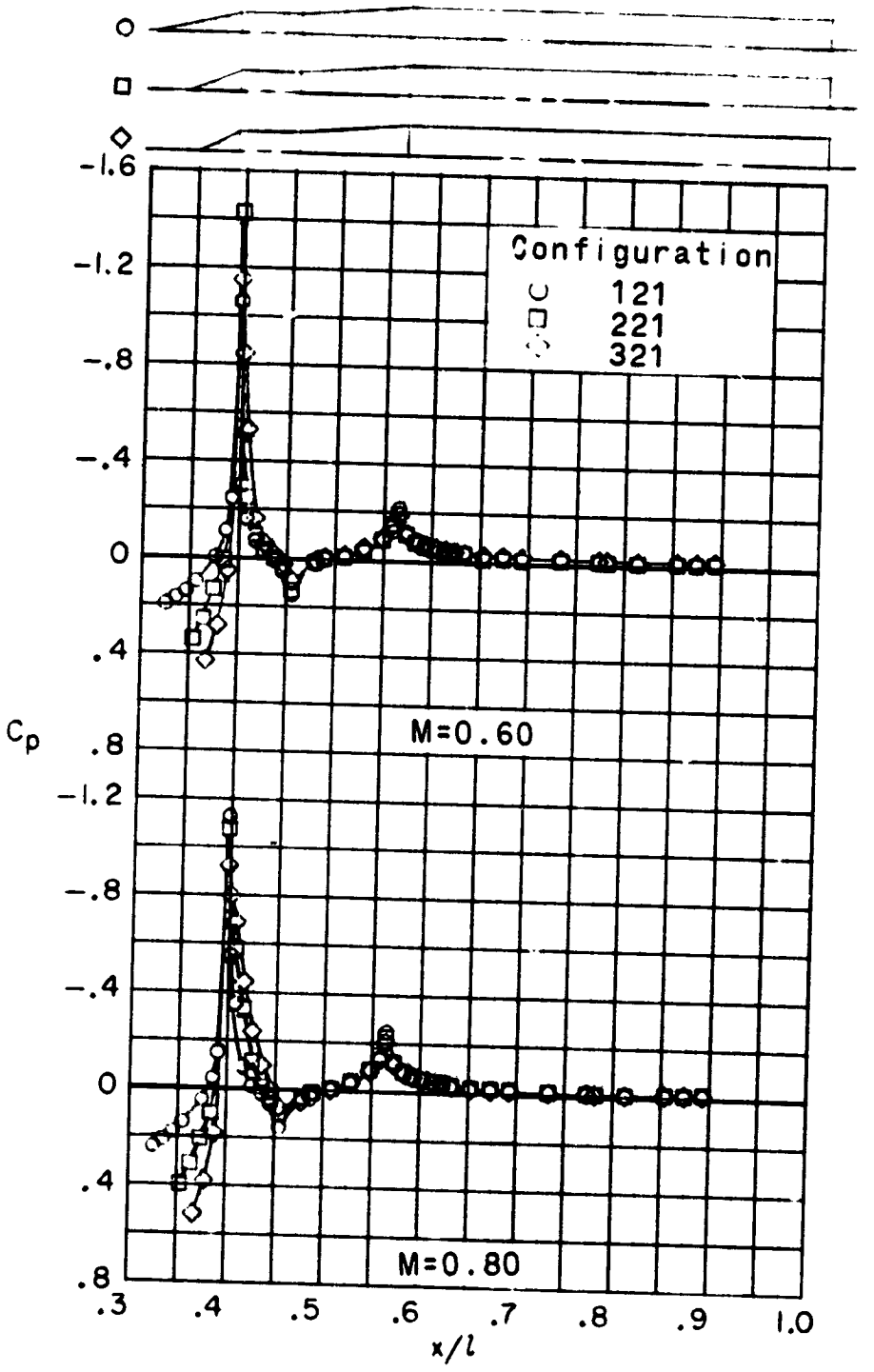
(d) $\delta_F = 30^o$.

Figure 6.- Continued.



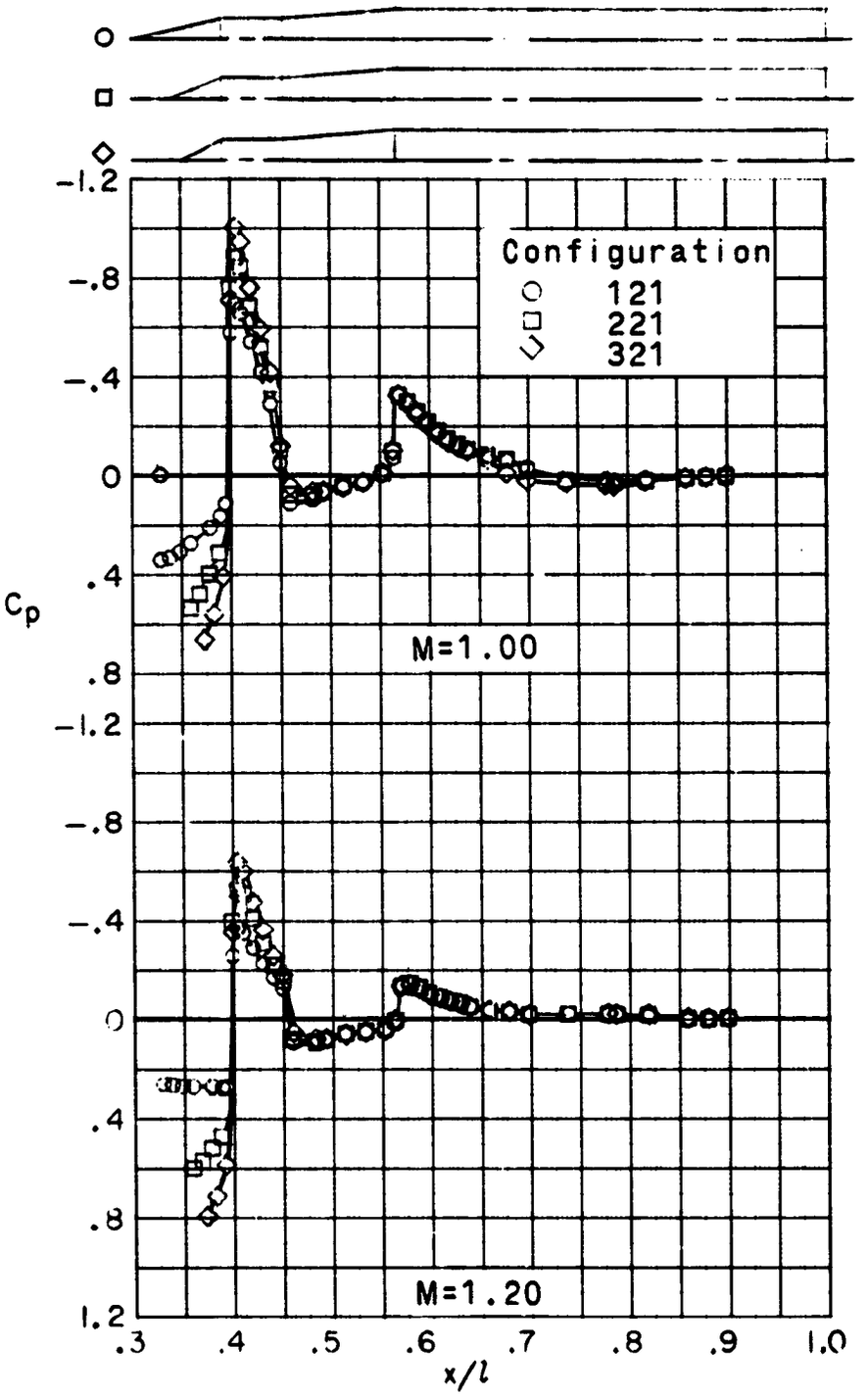
(d) Concluded.

Figure 6.- Concluded.



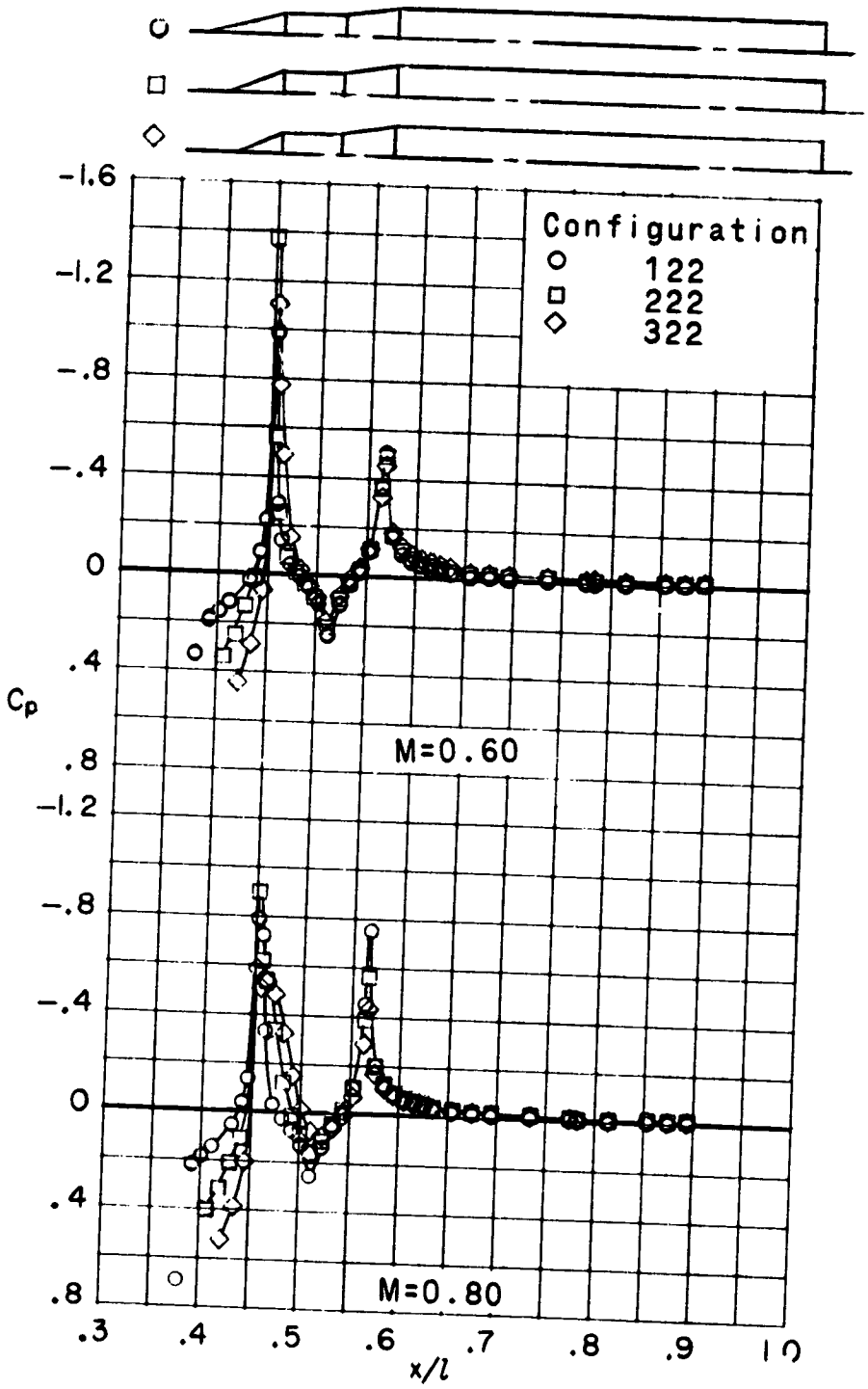
(a) $\delta_F = 5^o$.

Figure 7.- Effects of variation in nose-cone angle for $\phi = 0^o$ and $\alpha = 3^o$.



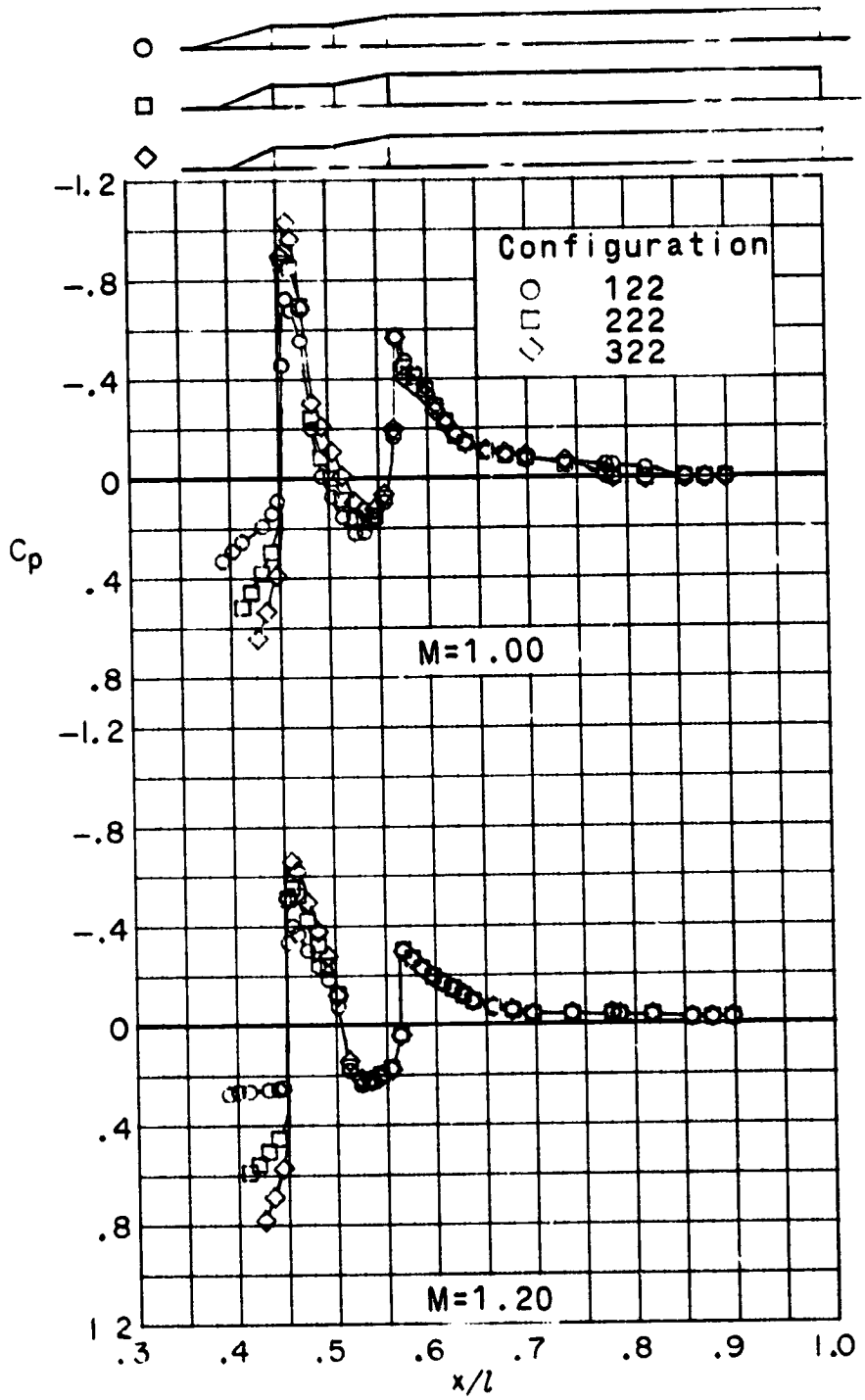
(a) Concluded.

Figure 7.- Continued.



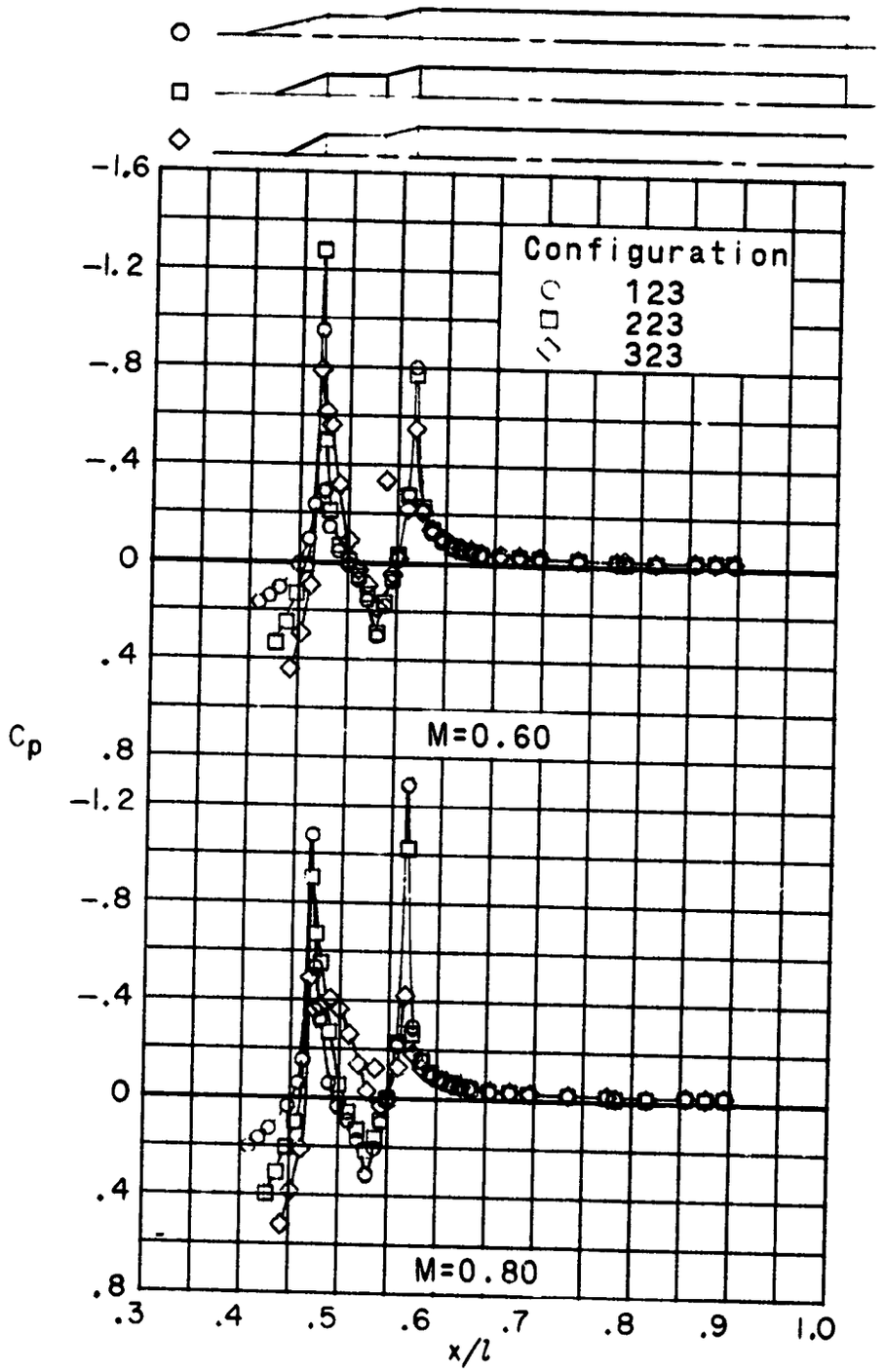
(b) $\delta_F = 10.1°$.

Figure 7.- Continued.



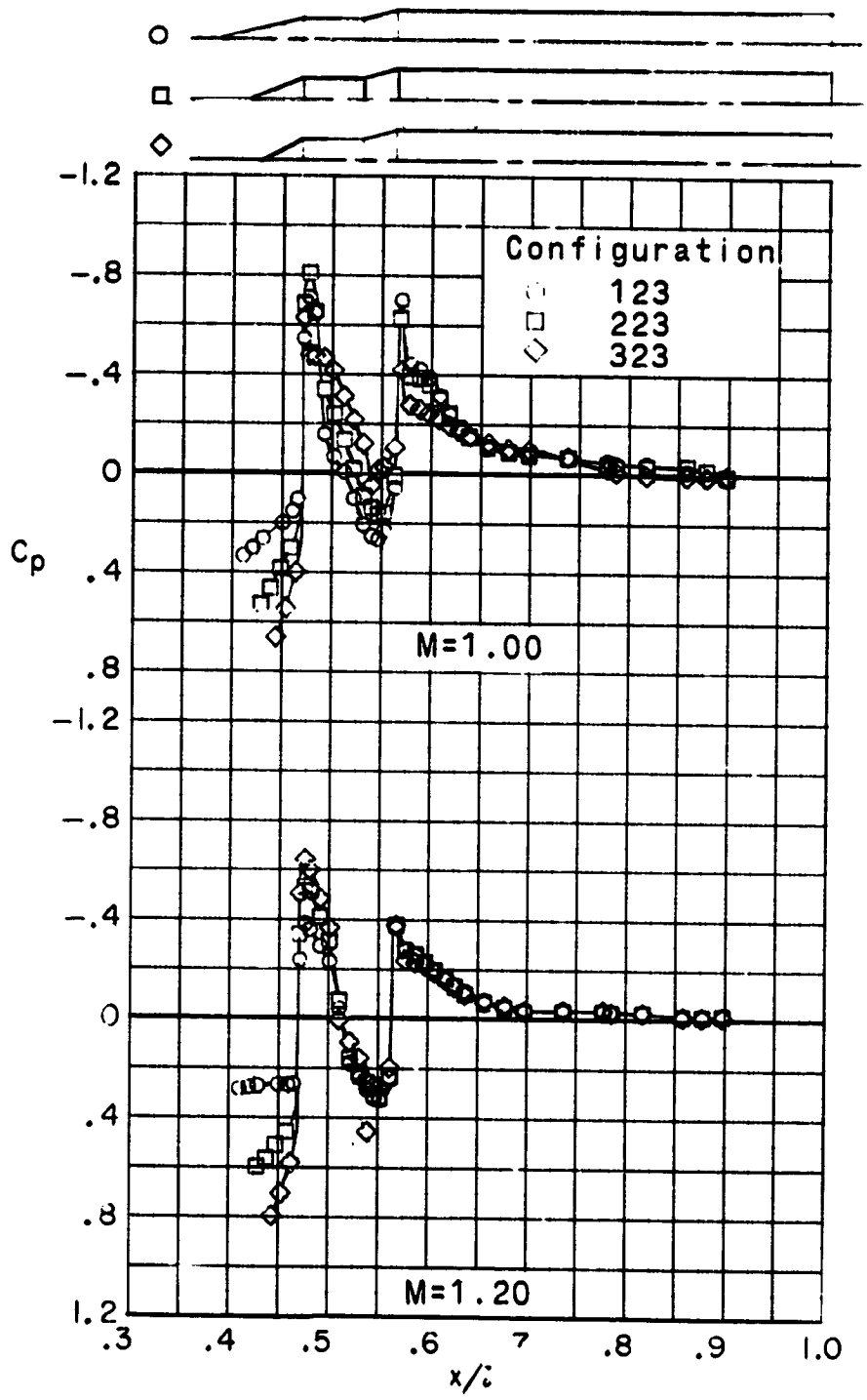
(b) Concluded.

Figure 7.- Continued.



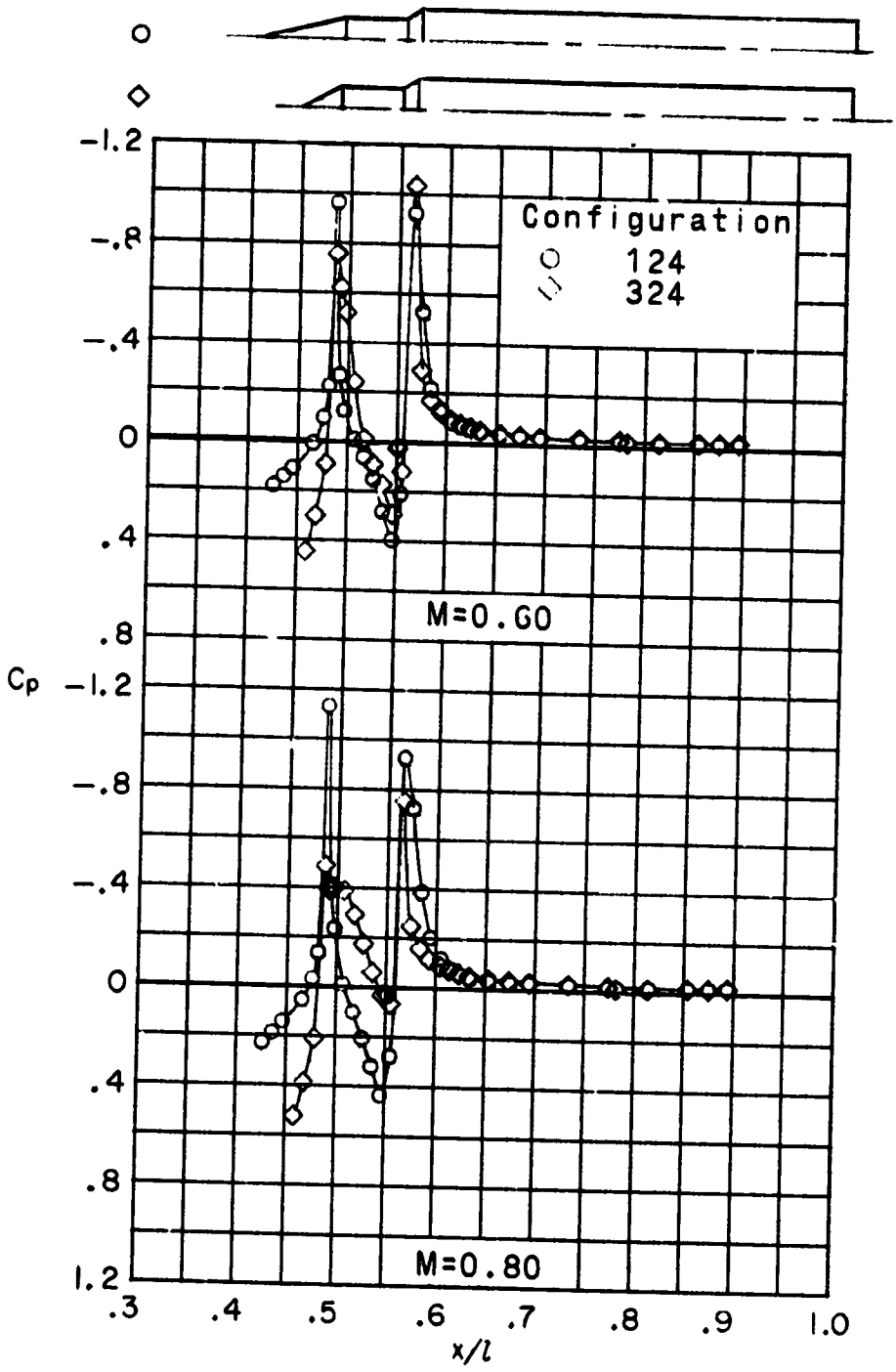
(c) $\delta_F = 15^o$.

Figure 7.- Continued.



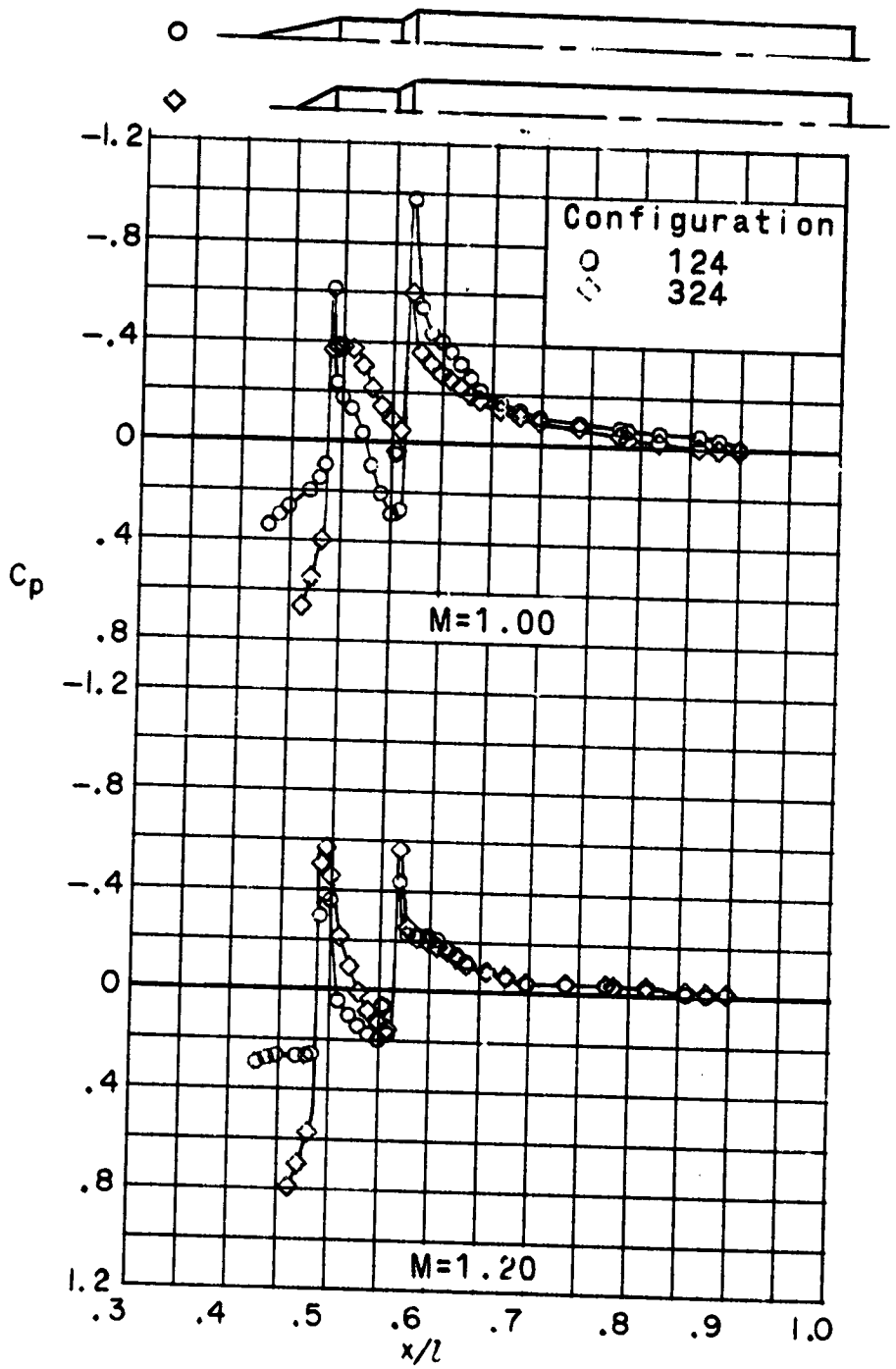
(c) Concluded.

Figure 7.- Continued.



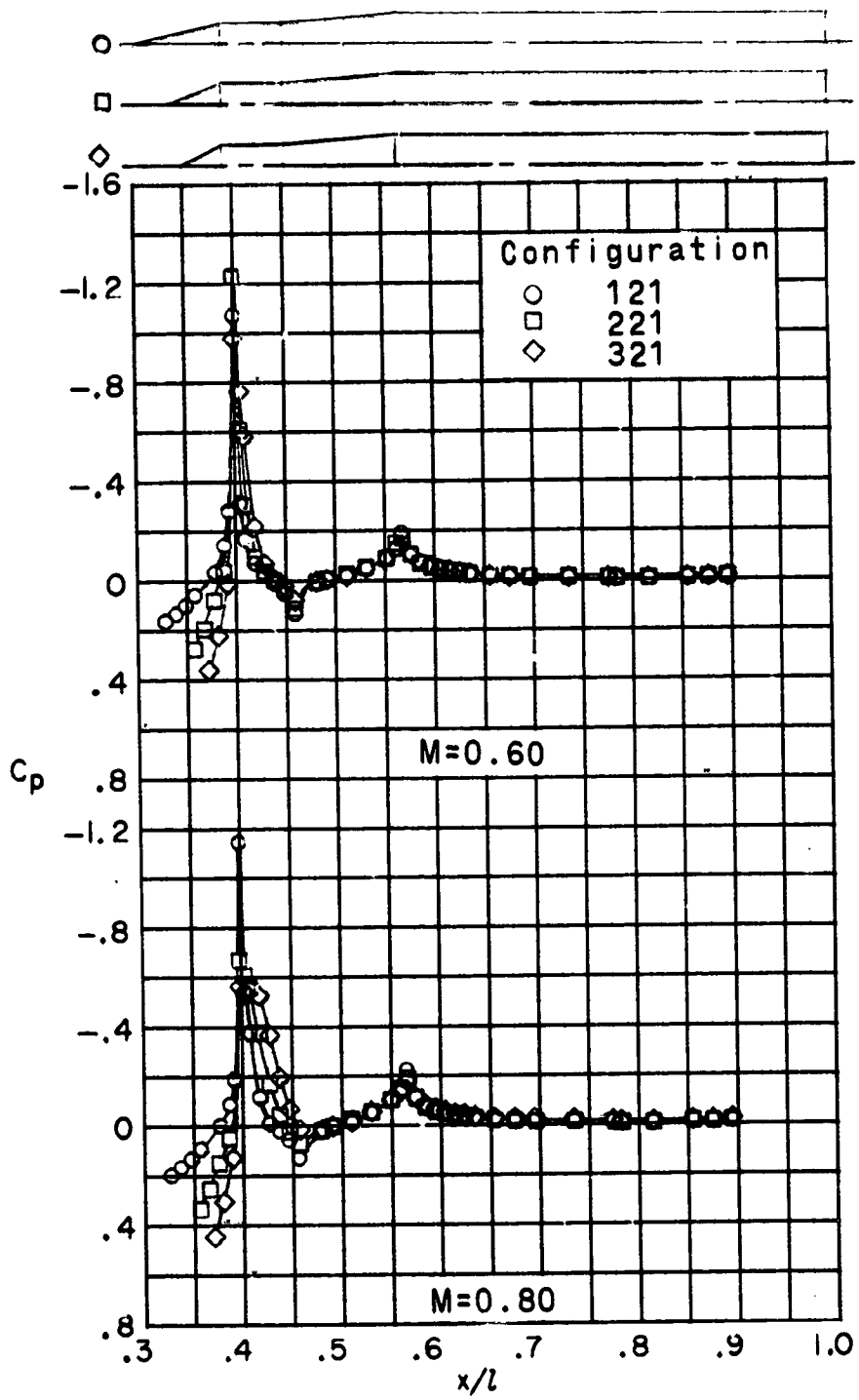
(d) $\delta_F = 30^o$.

Figure 7.- Continued.



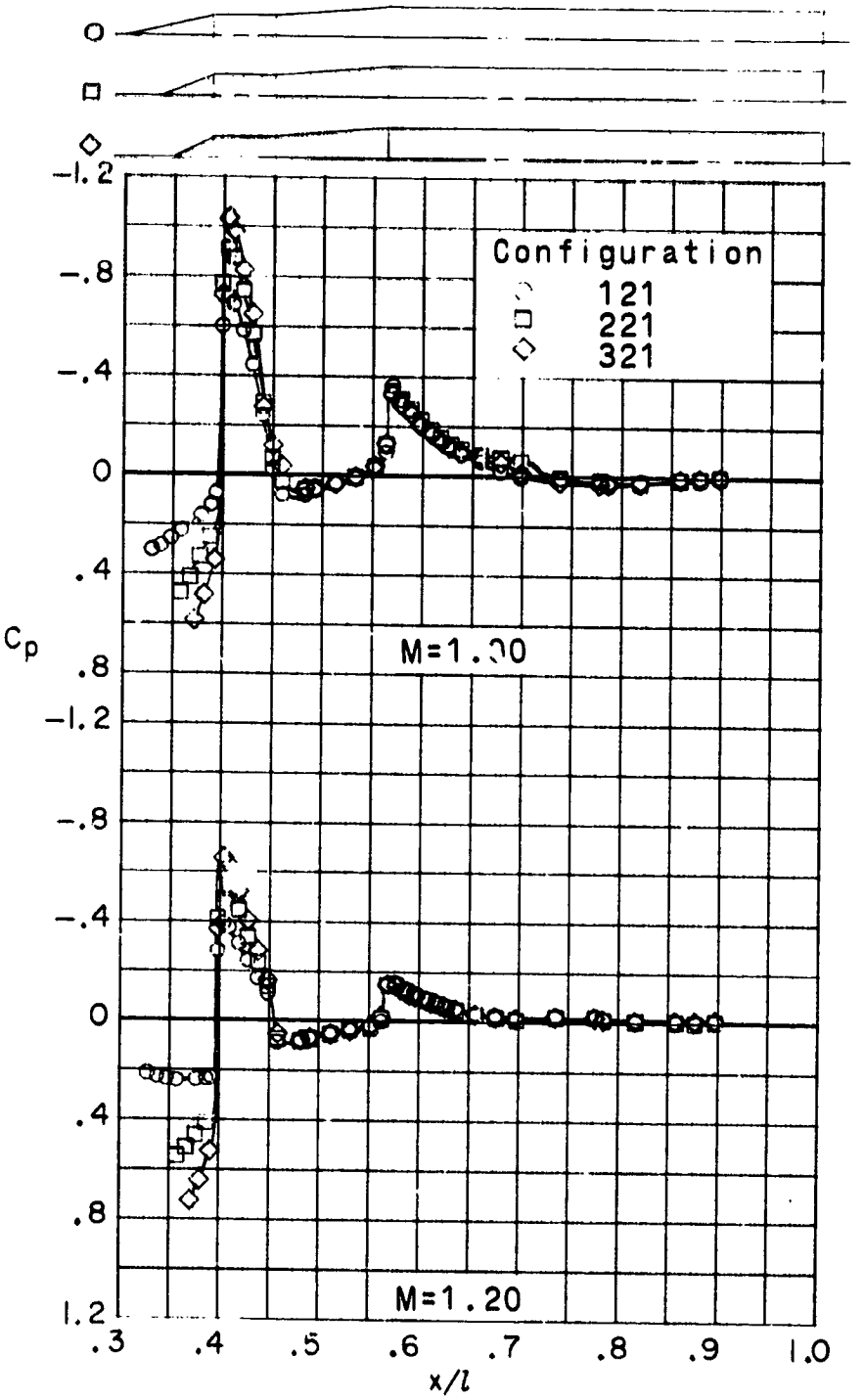
(d) Concluded.

Figure 7.- Concluded.



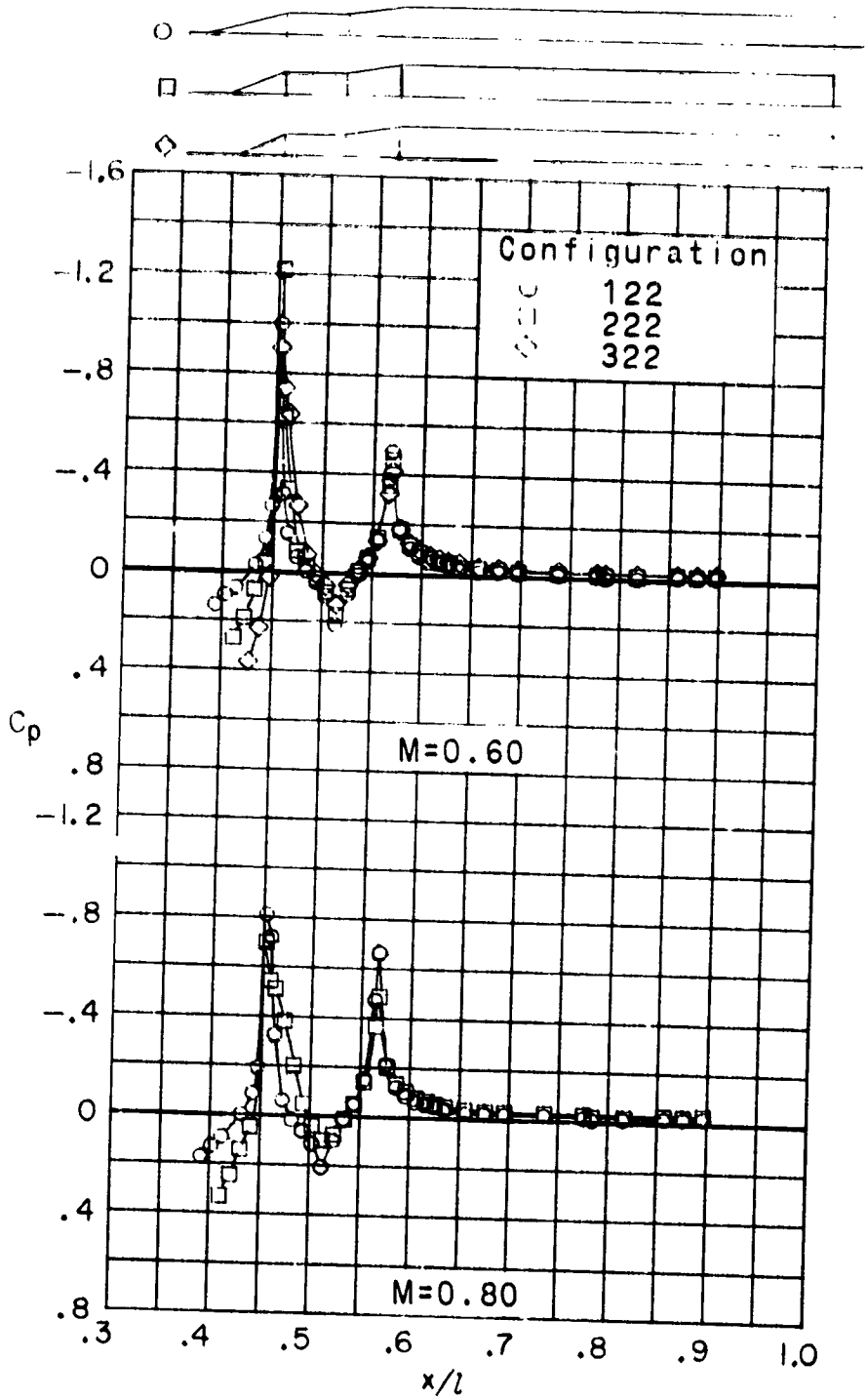
(a) $\delta_F = 5^o$.

Figure 8.- Effects of variation in nose-cone angle for $\phi = 0^o$ and $\alpha = 6^o$.



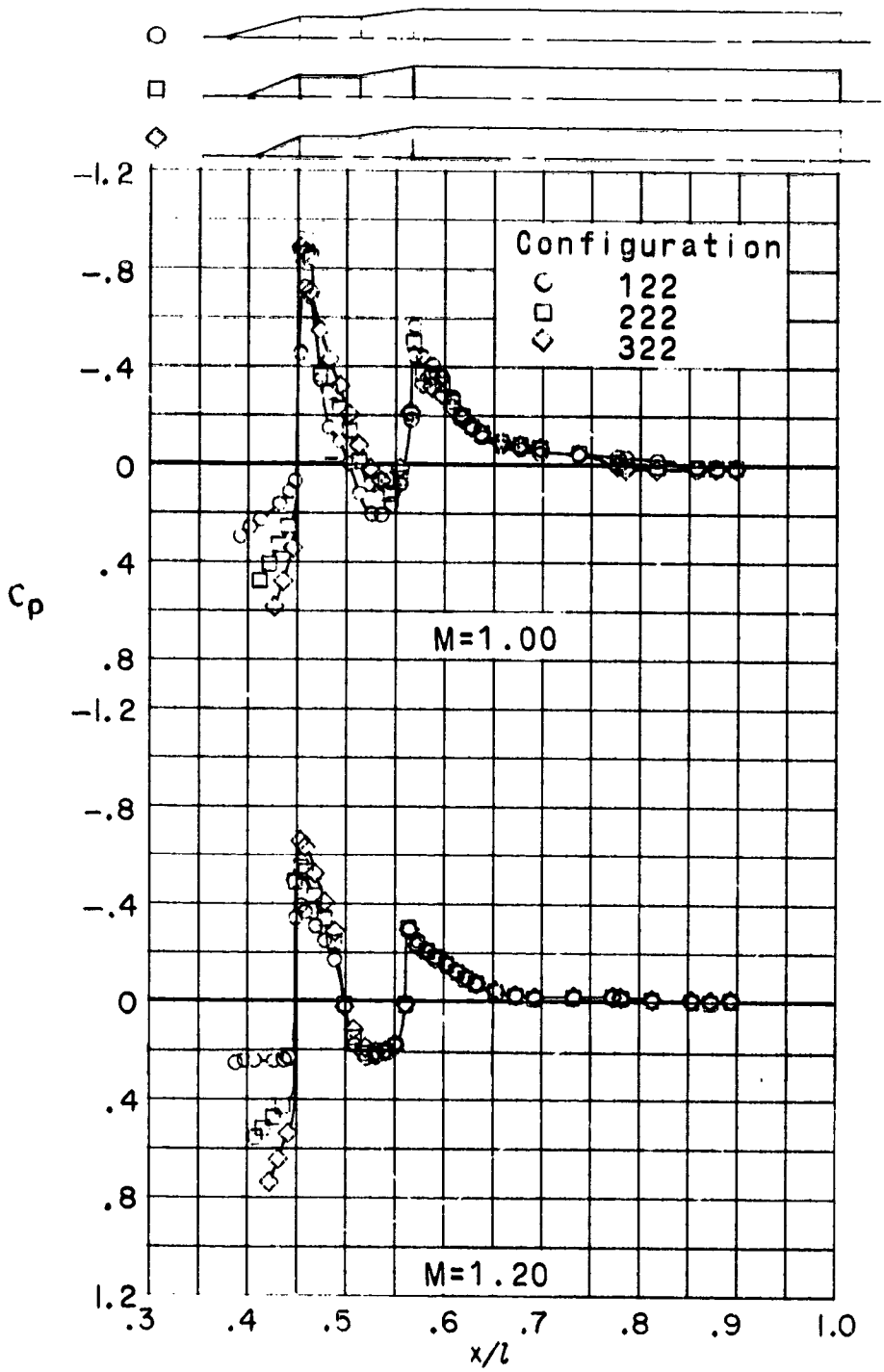
(a) Concluded.

Figure 8.- Continued.



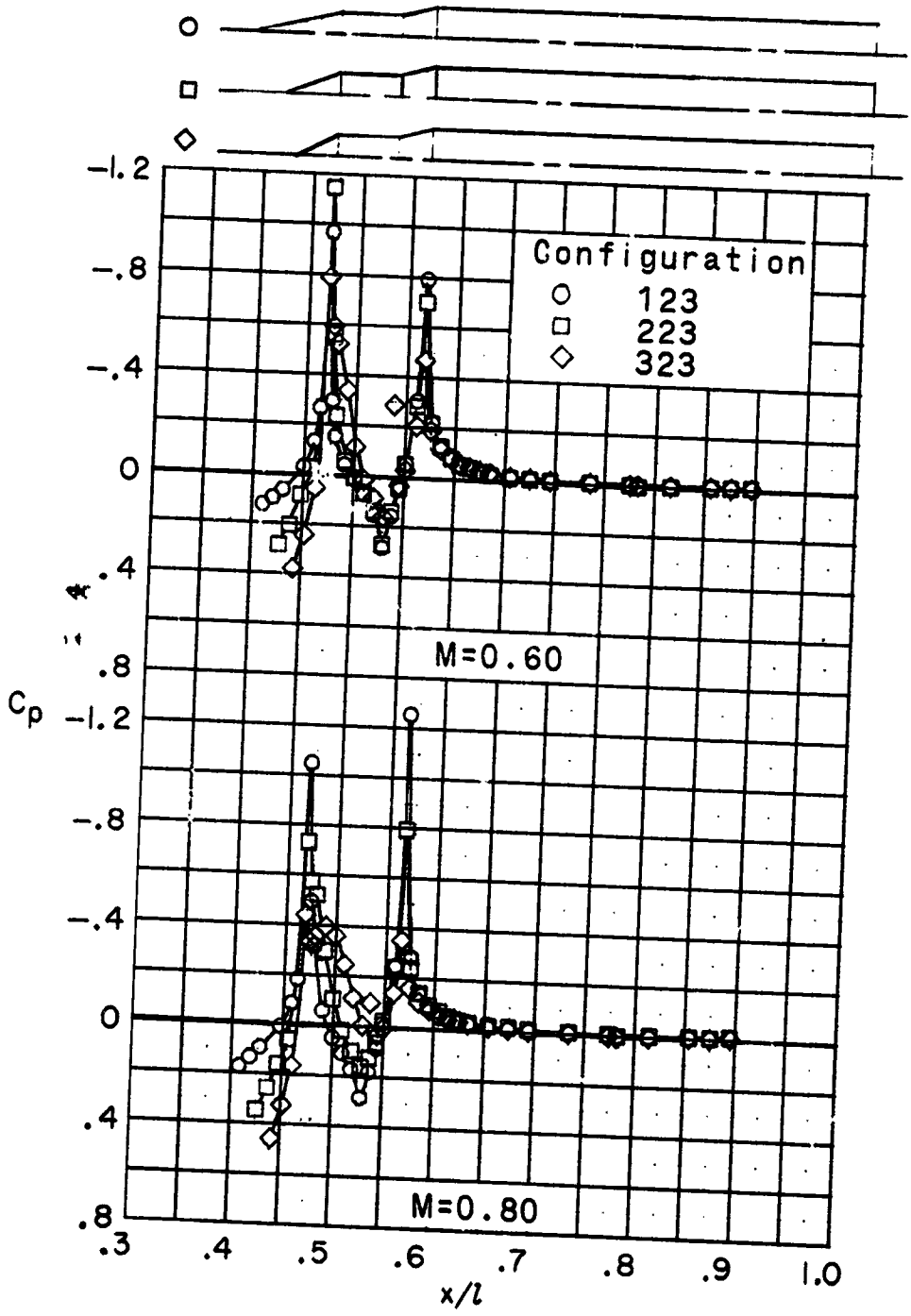
(b) $\delta_F = 10.1^o$.

Figure 8.- Continued.



(b) Concluded.

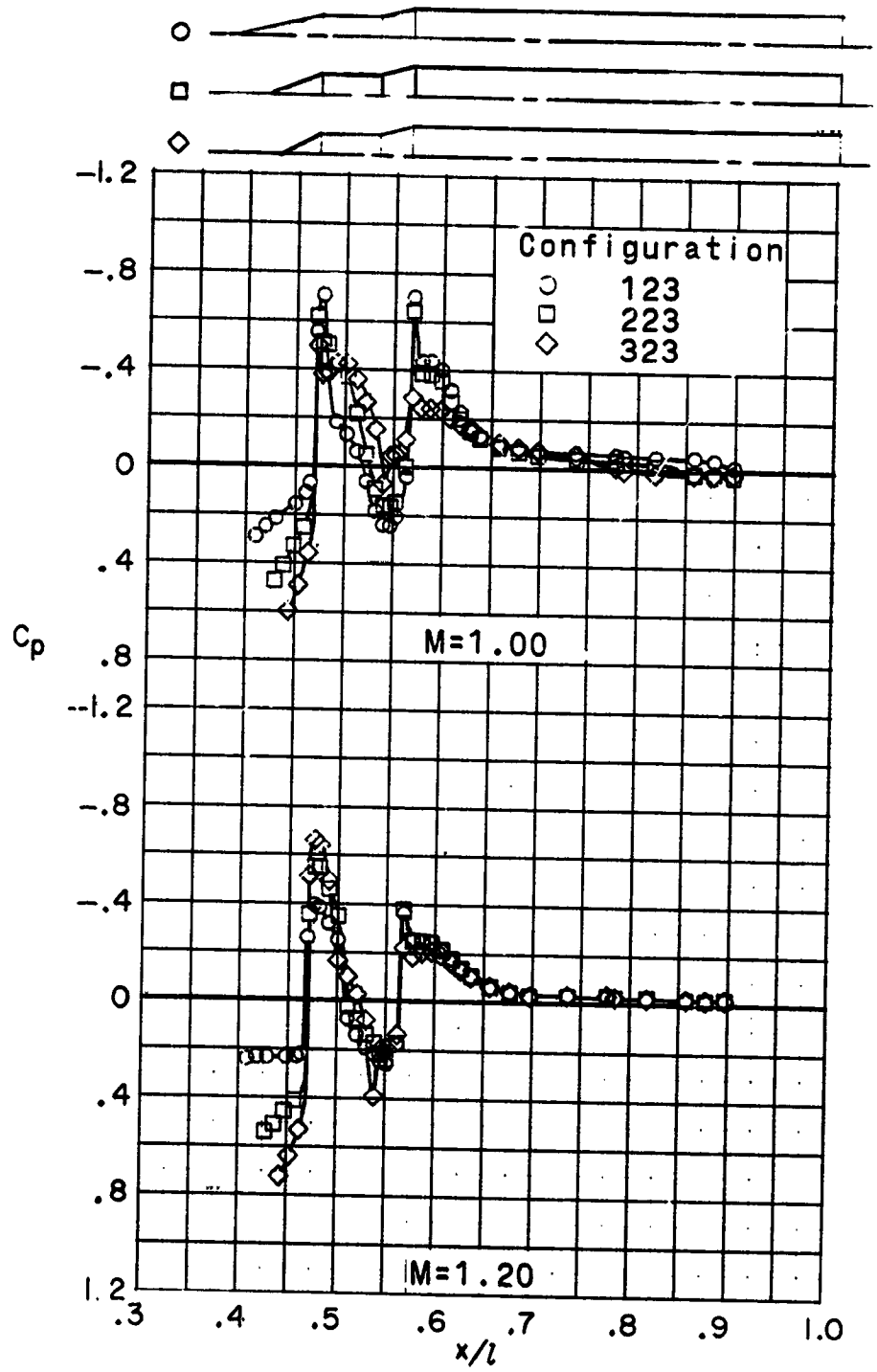
Figure 8.- Continued.



(c) $\delta_F = 15^o$.

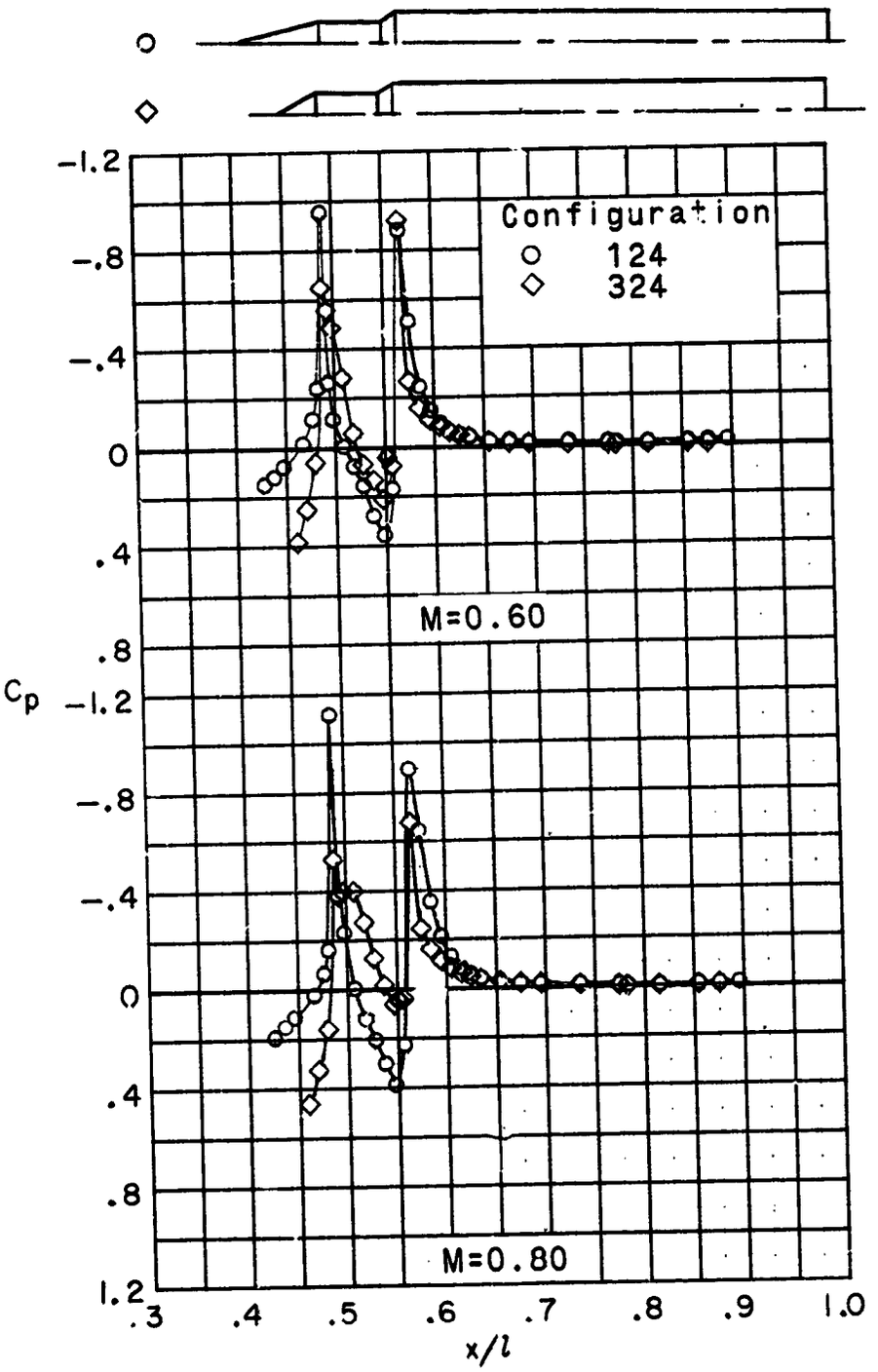
Figure 8.- Continued.

C-3



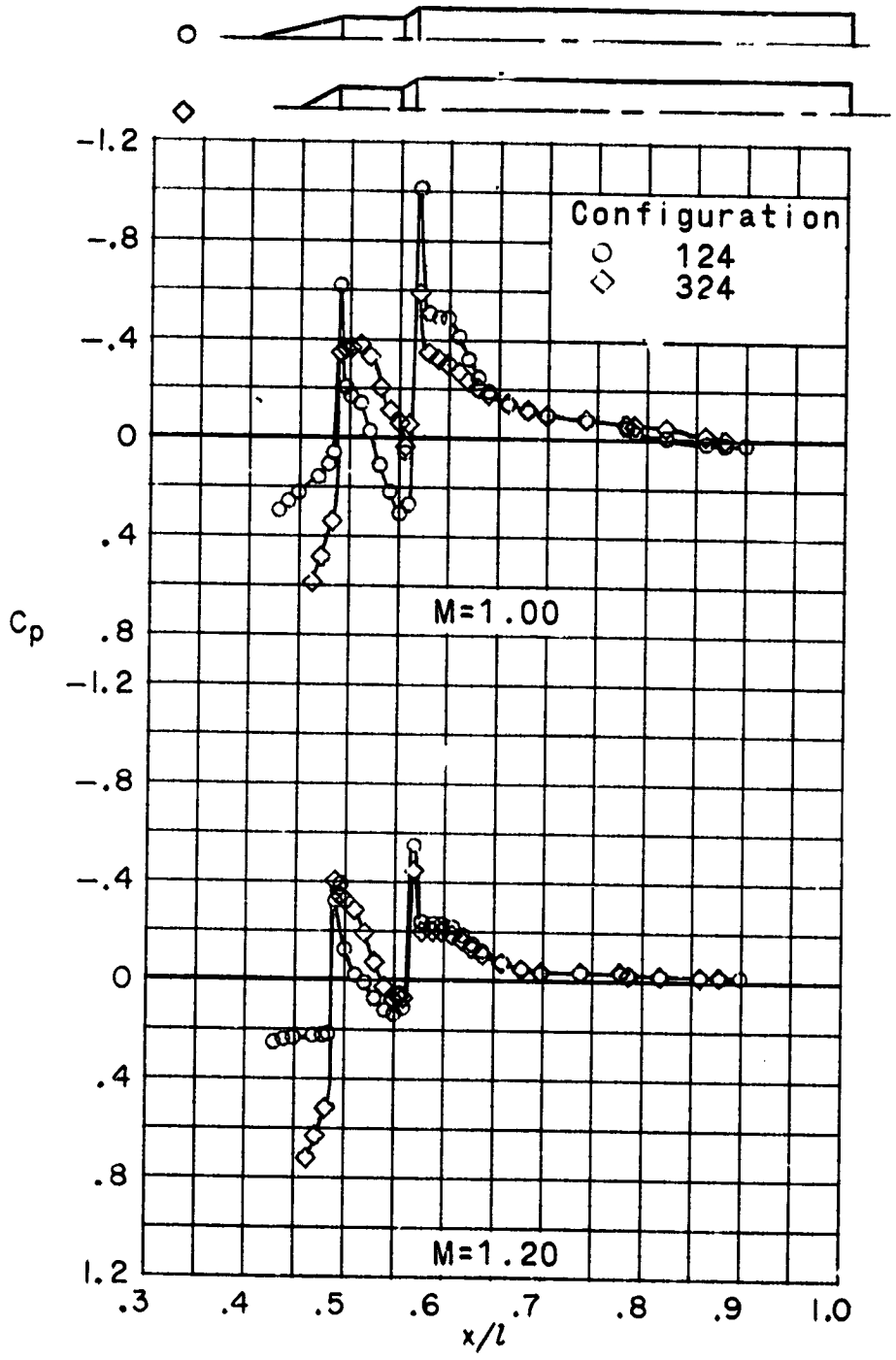
(c) Concluded.

Figure 8.- Continued.



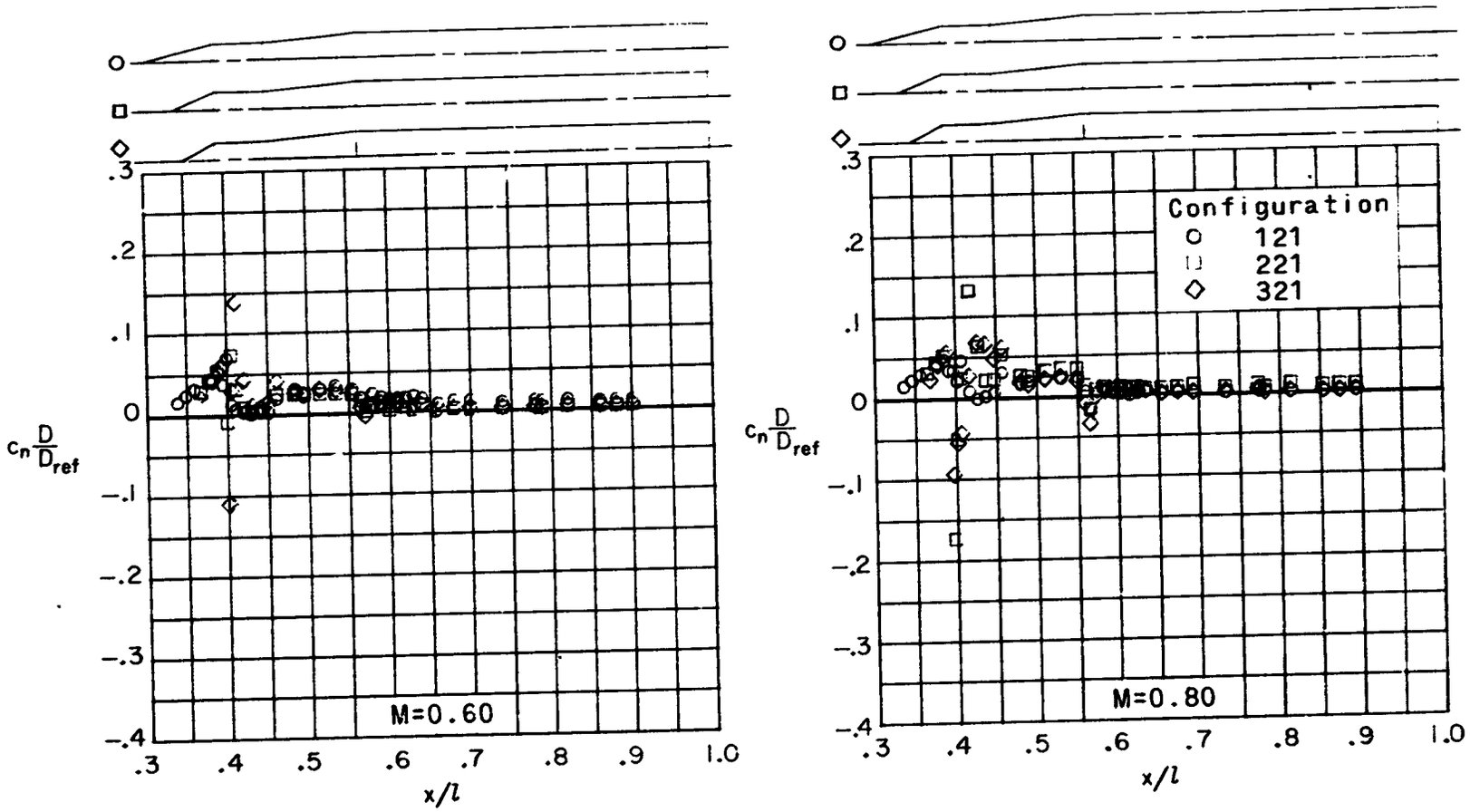
(d) $\delta_F = 30^o$.

Figure 8.- Continued.



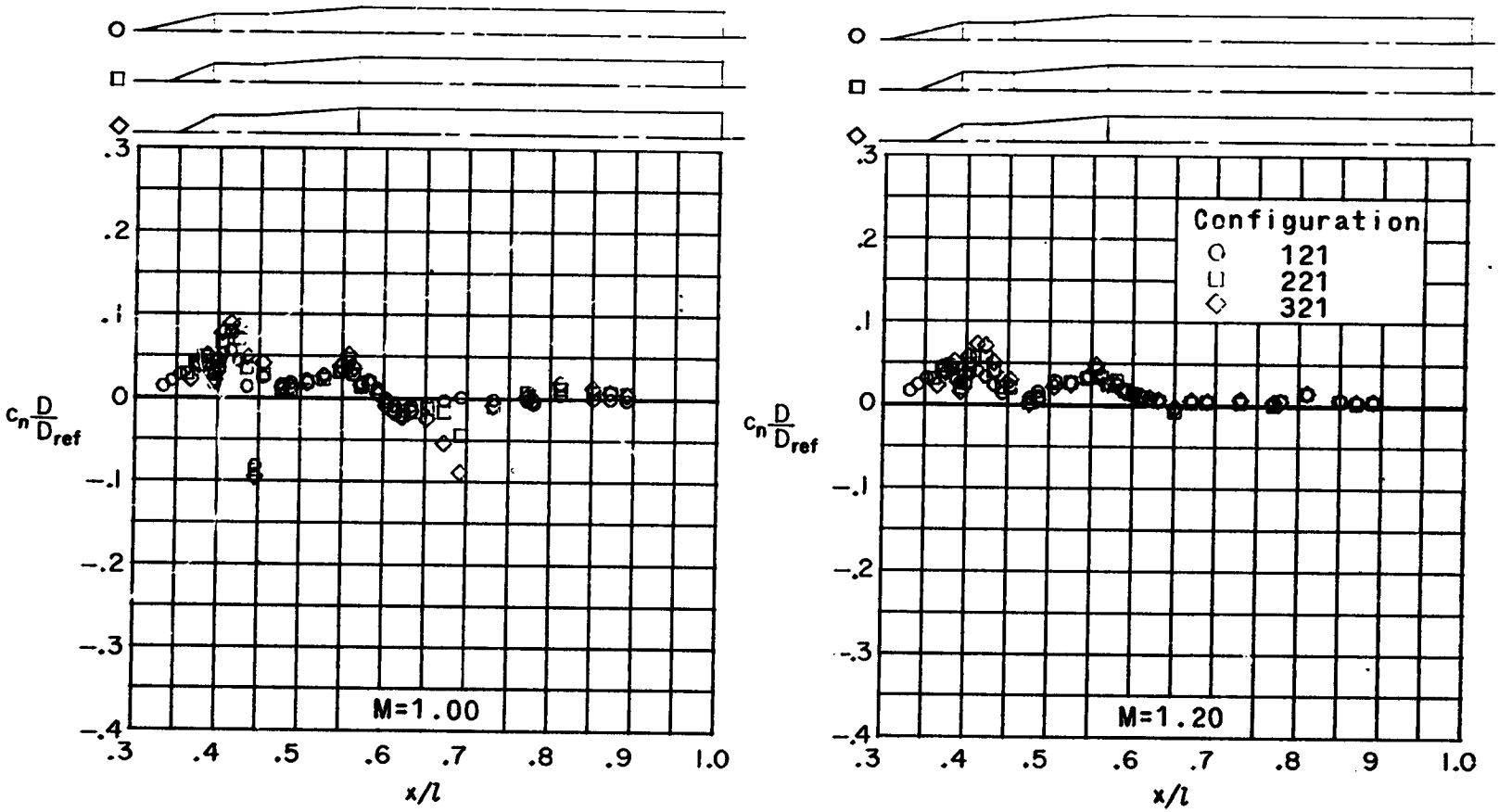
(d) Concluded.

Figure 8.- Concluded.



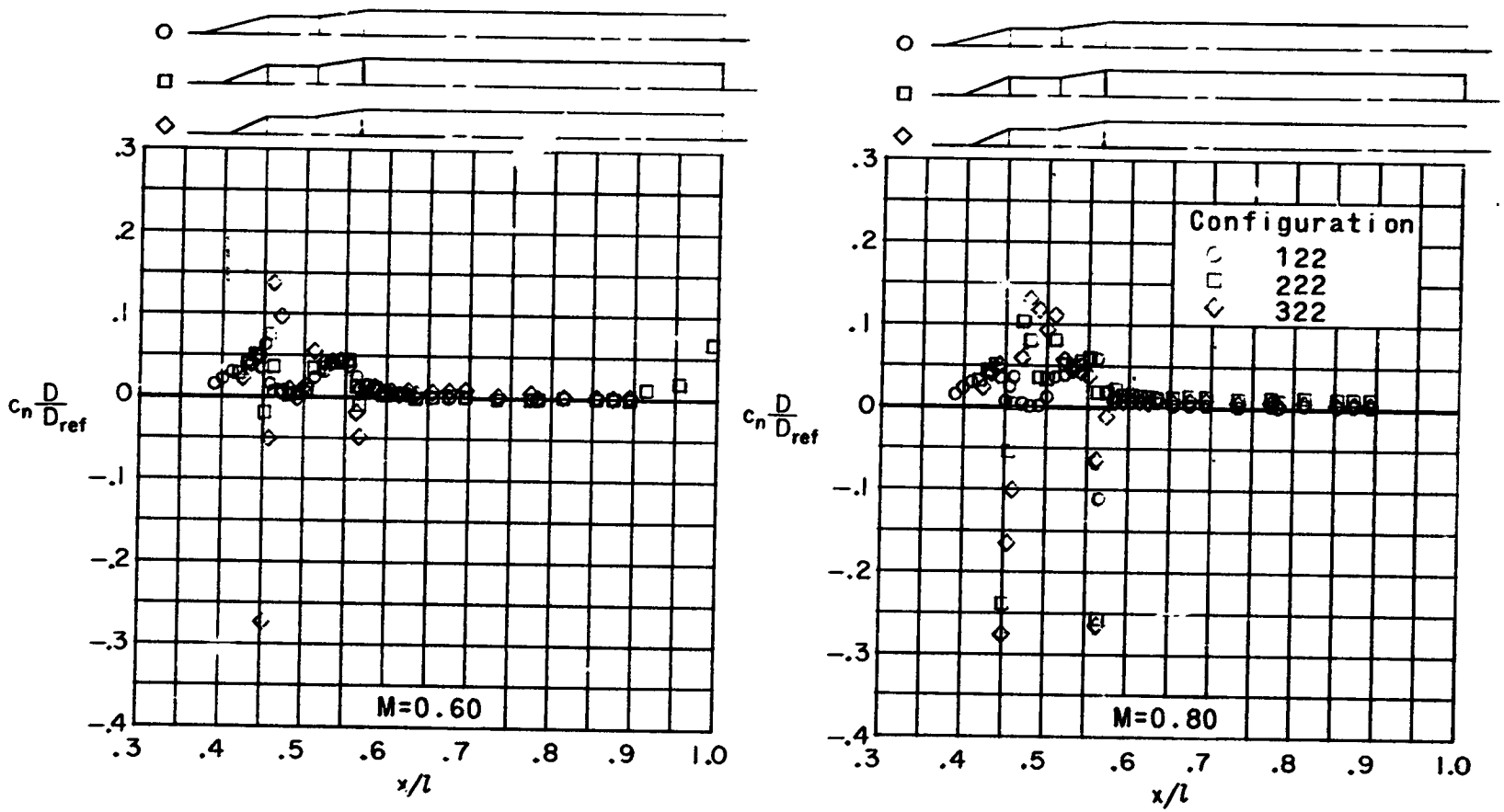
(a) $\delta_F = 5^o$.

Figure 9.- Effect of variation in nose-cone angle on load distributions at $\alpha = 3^o$.



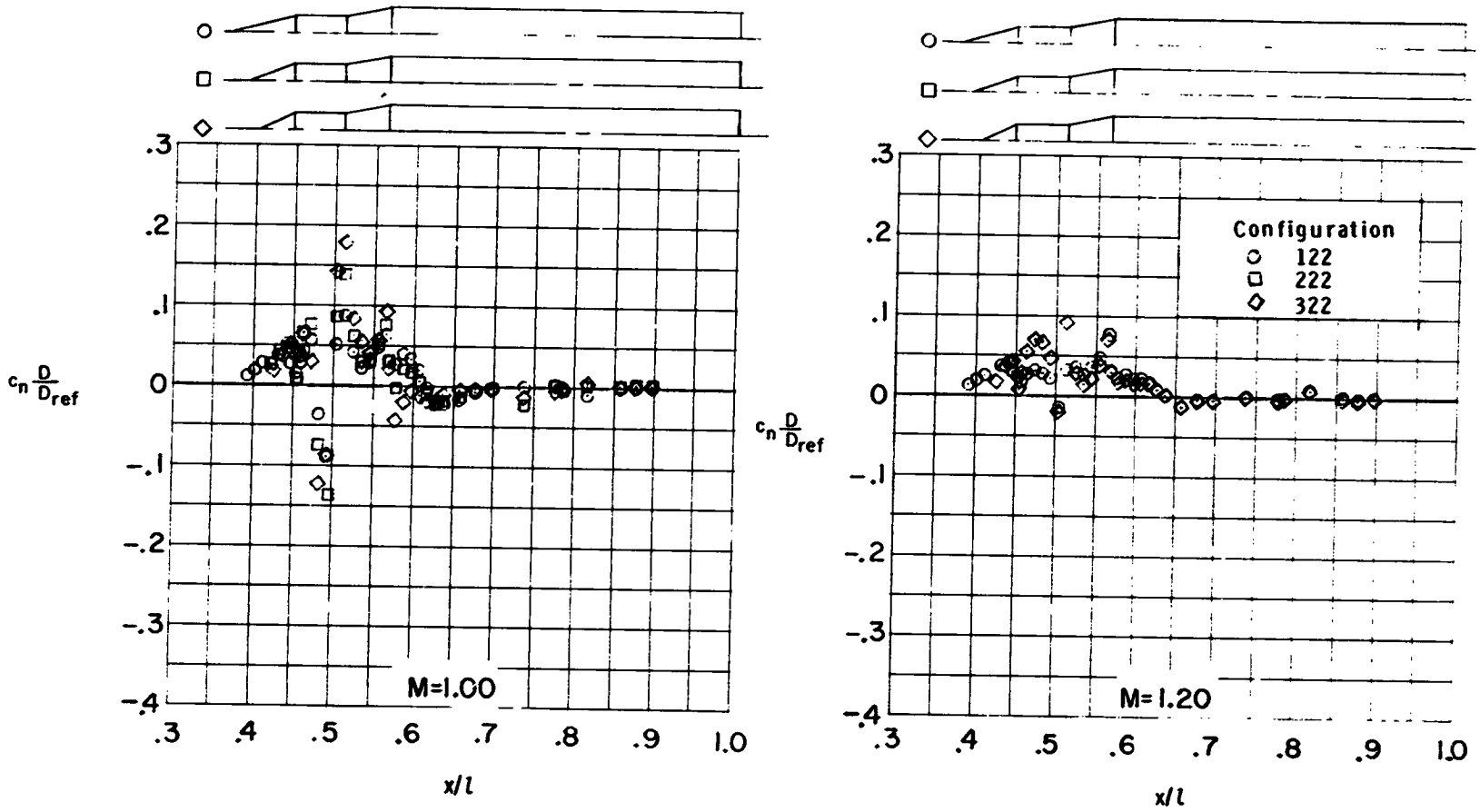
(a) Concluded.

Figure 9.- Continued.



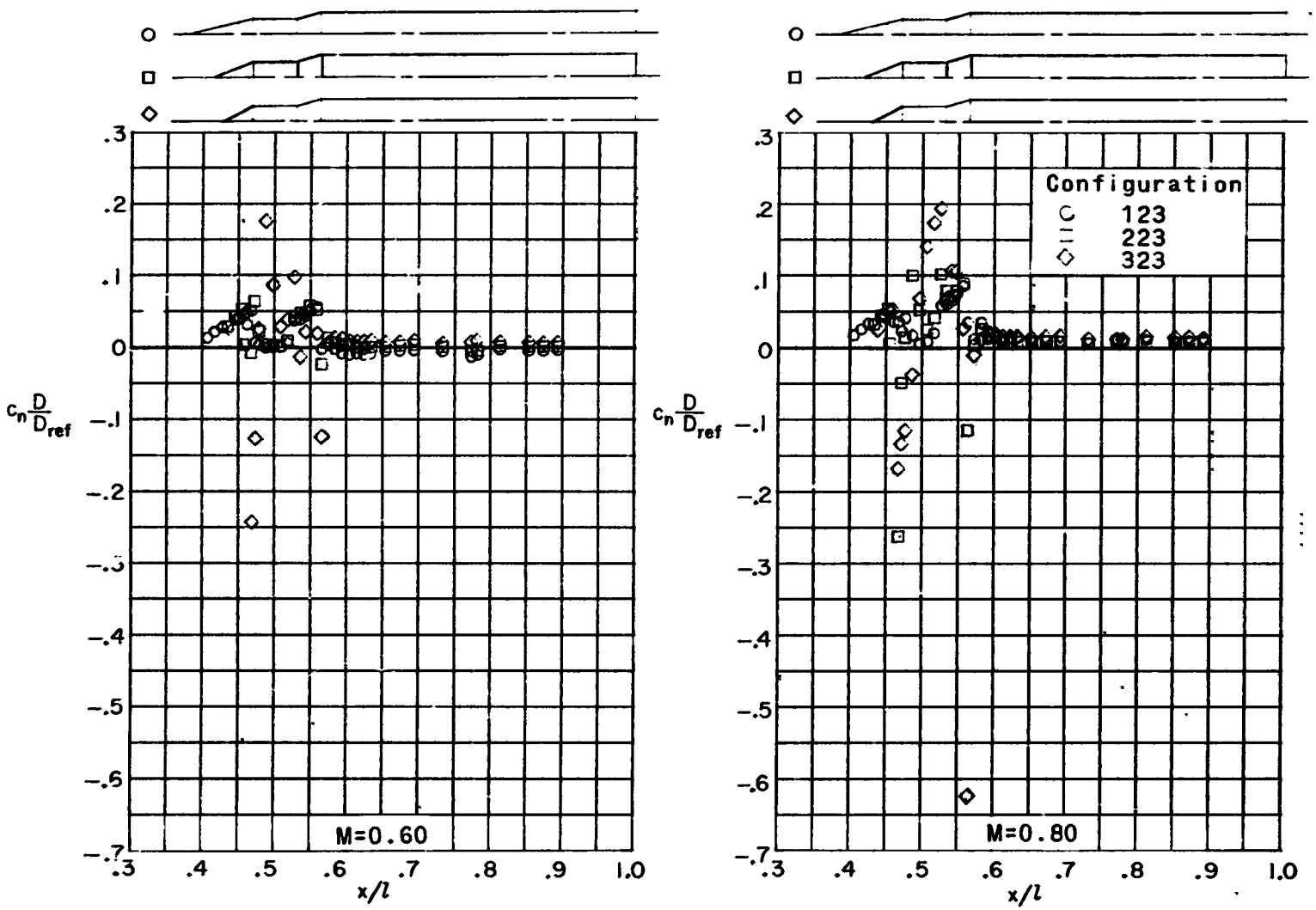
(b) $\delta_F = 10.1^o$.

Figure 9.- Continued.



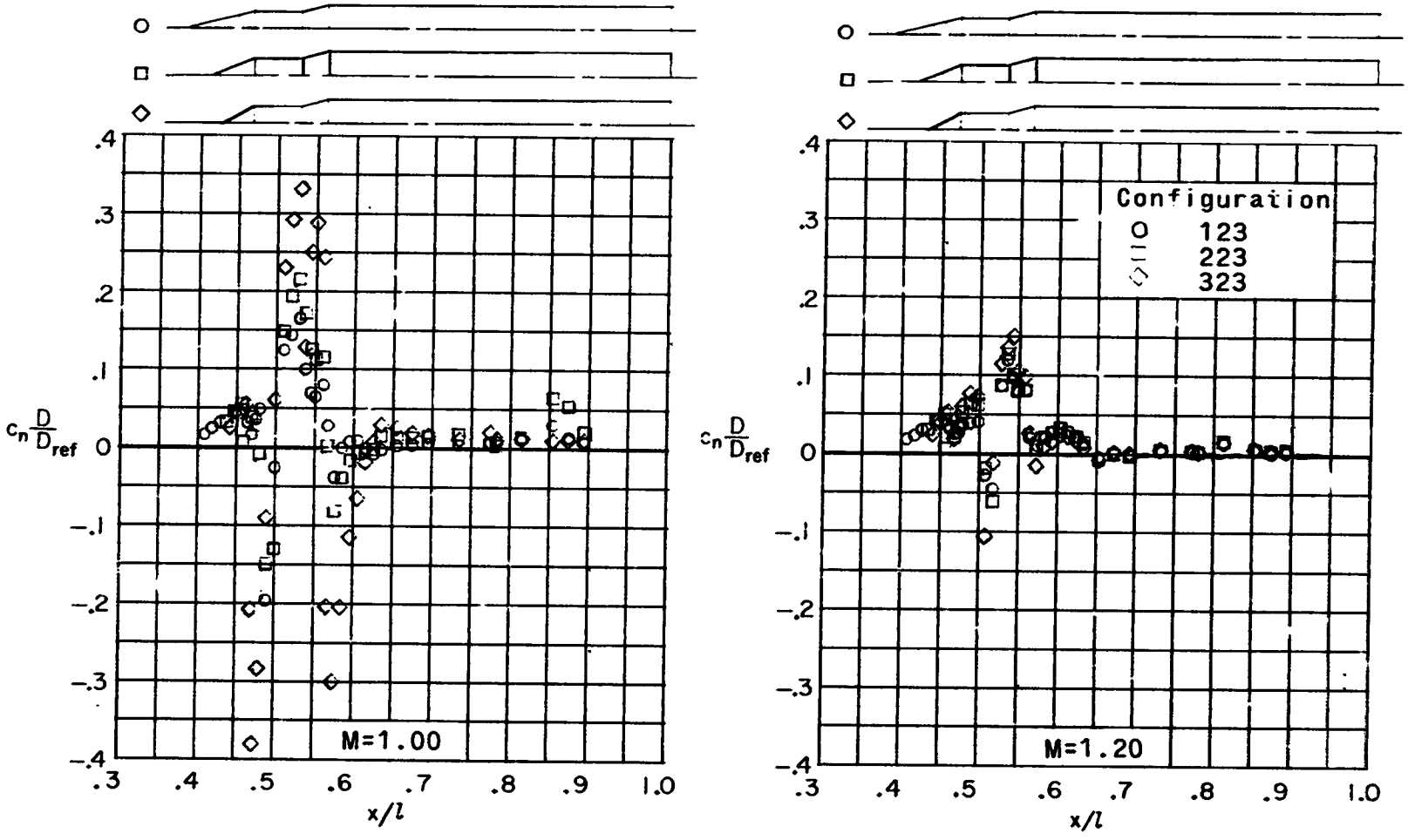
(b) Concluded.

Figure 9.- Continued.



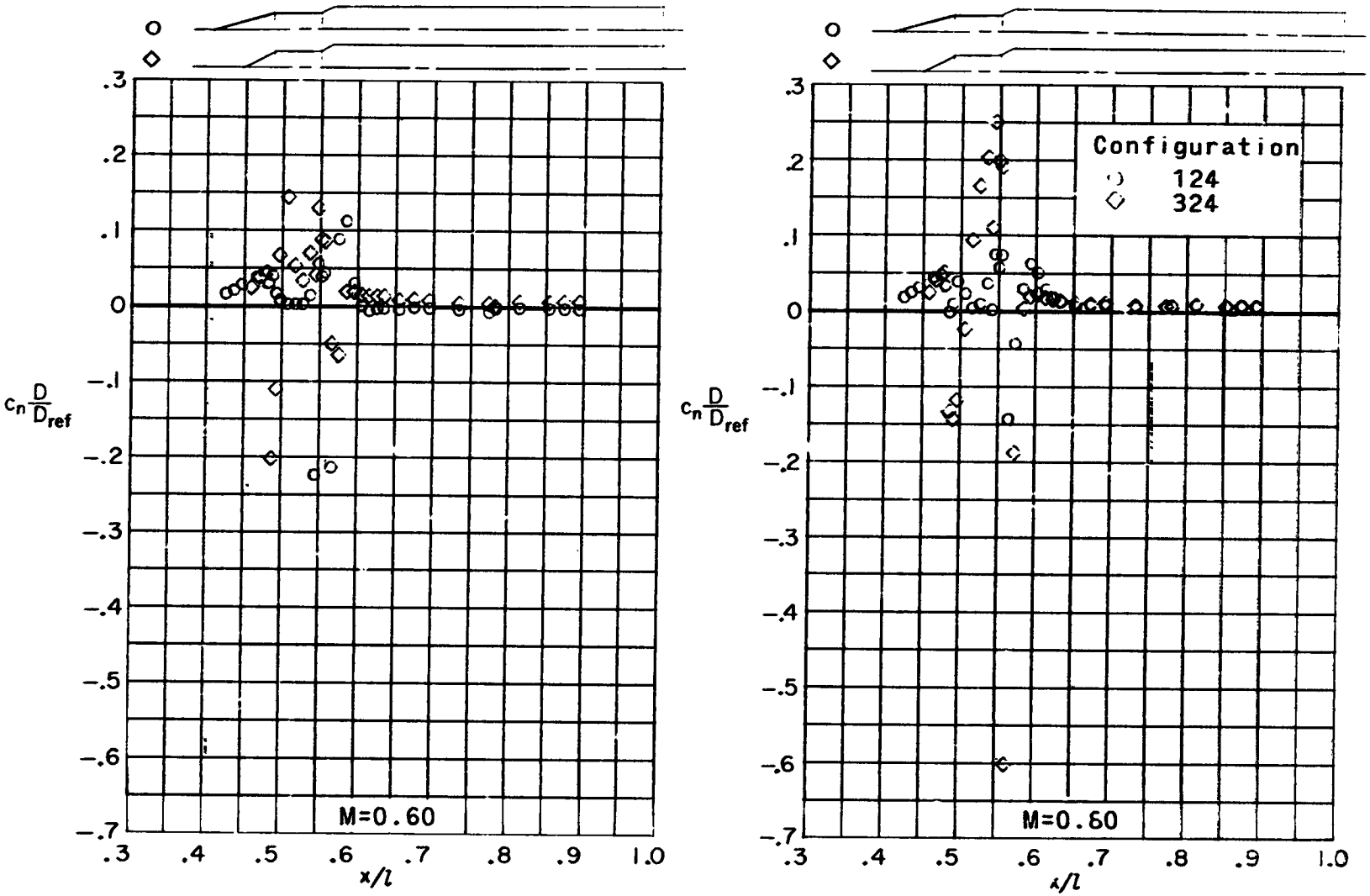
(c) $\delta_F = 15^o$.

Figure 9.- Continued.



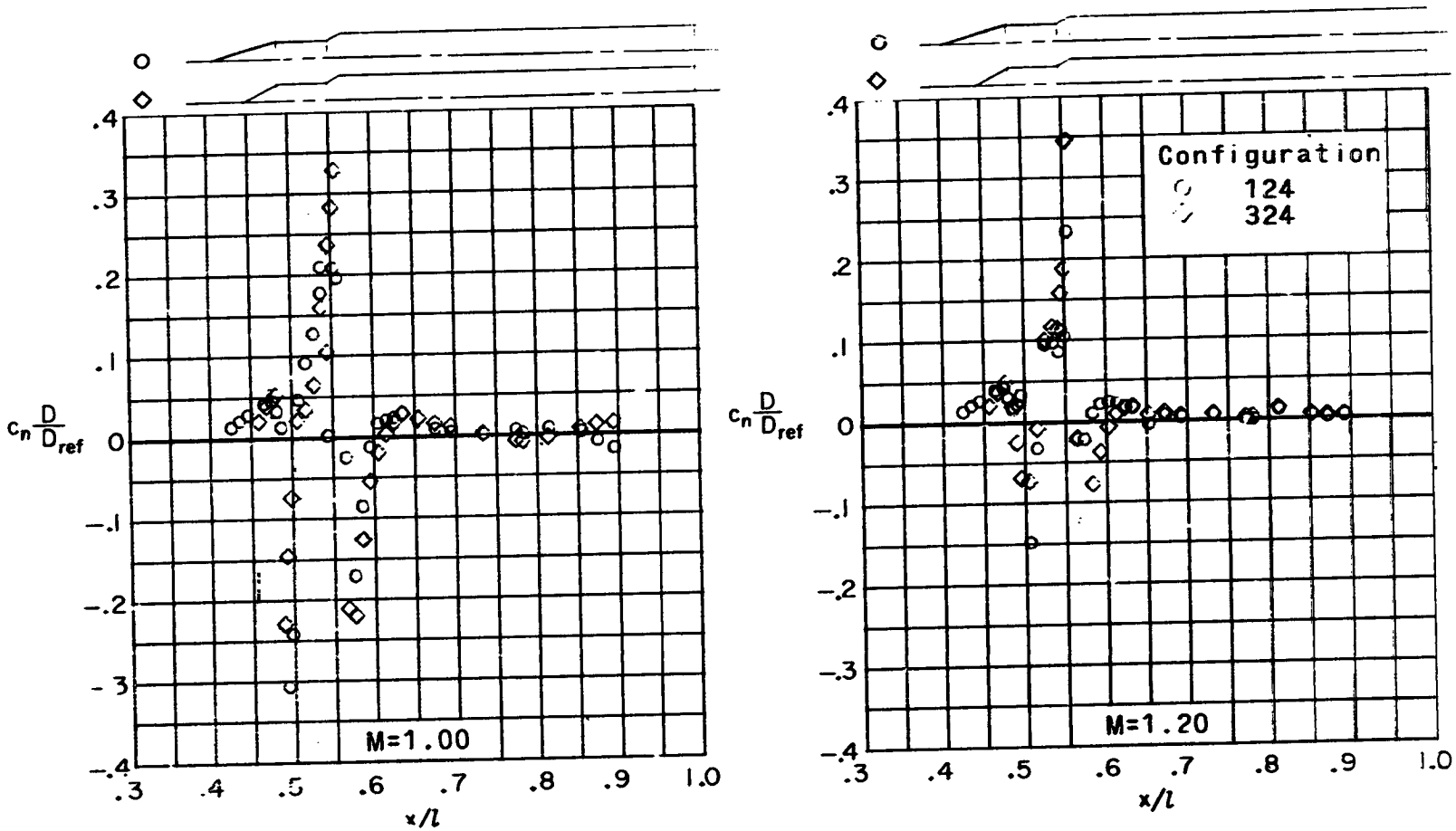
(c) Concluded.

Figure 9.- Continued.



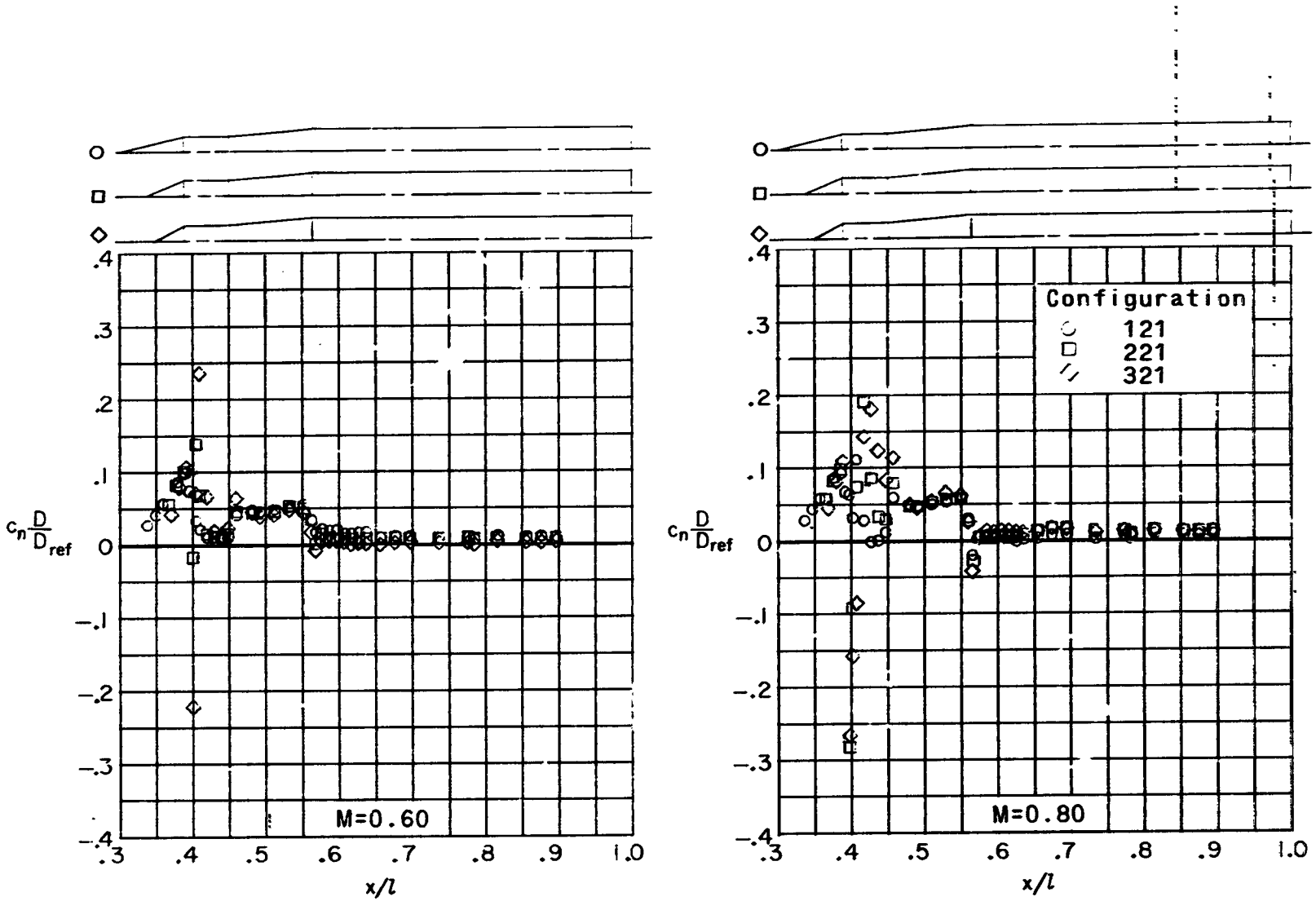
(d) $\delta_F = 30^o$.

Figure 9.- Continued.



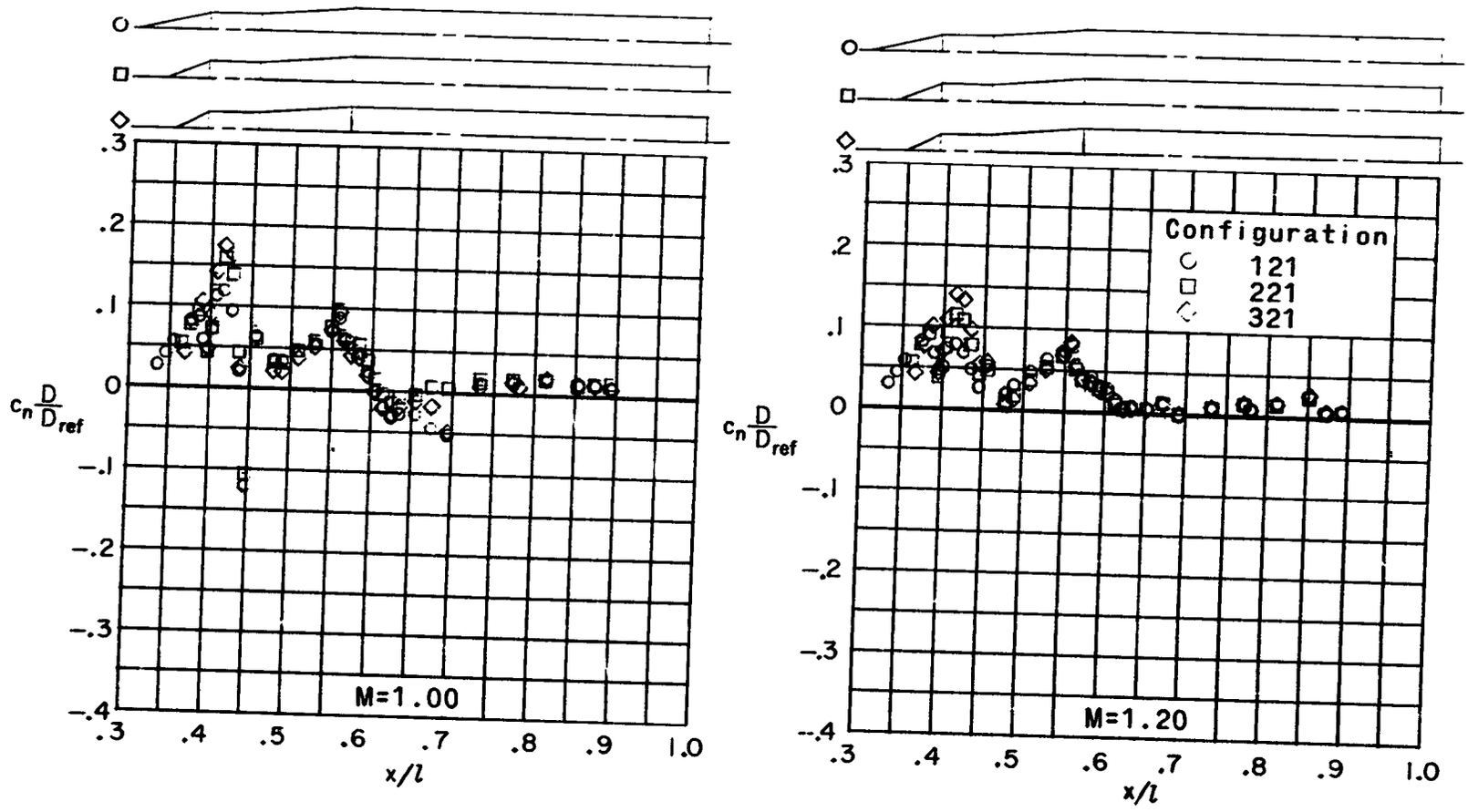
(d) Concluded.

Figure 9.- Concluded.



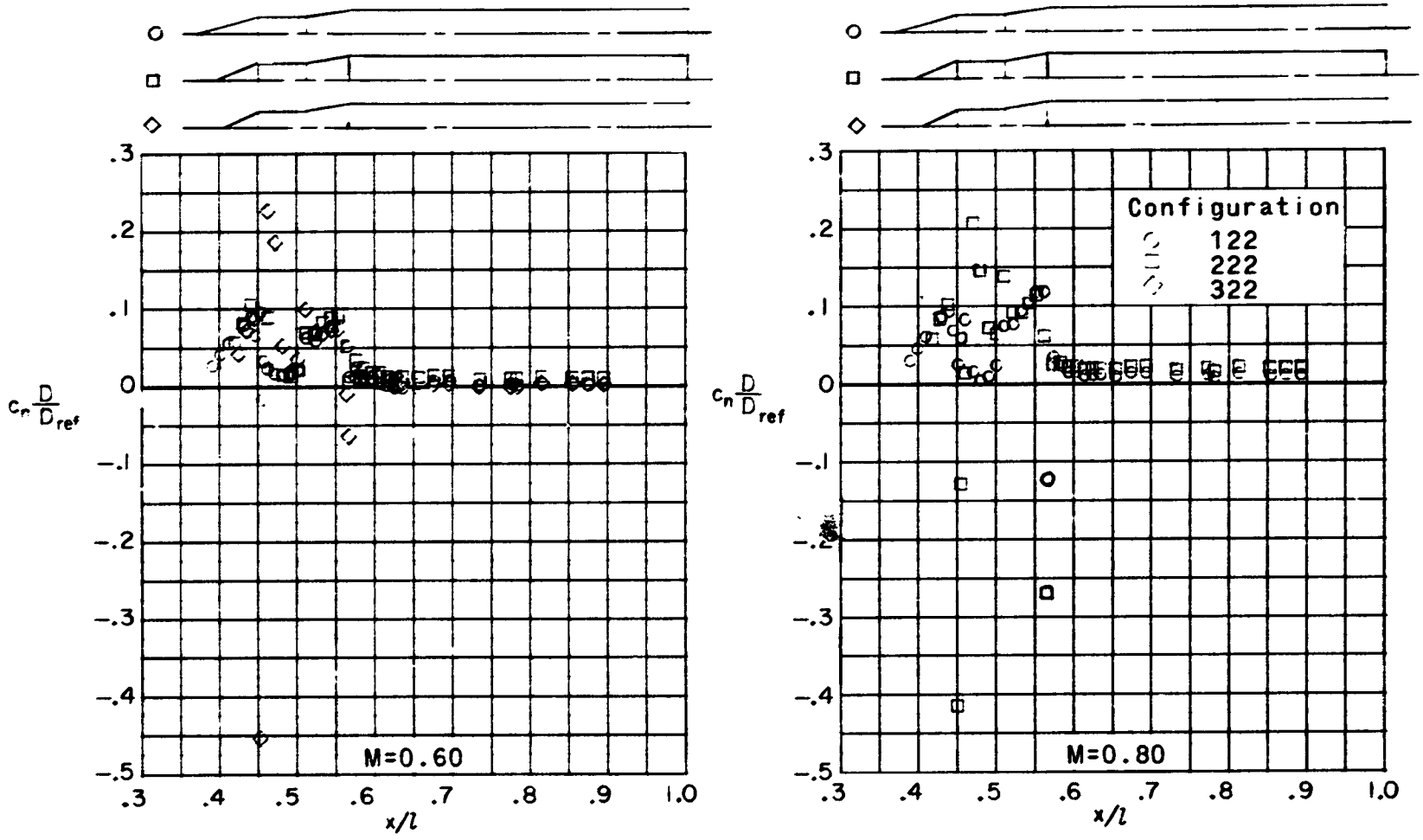
(a) $\delta_F = 5^o$

Figure 10.- Effect of variation in nose-cone angle on load distributions at $\alpha = 6^o$.



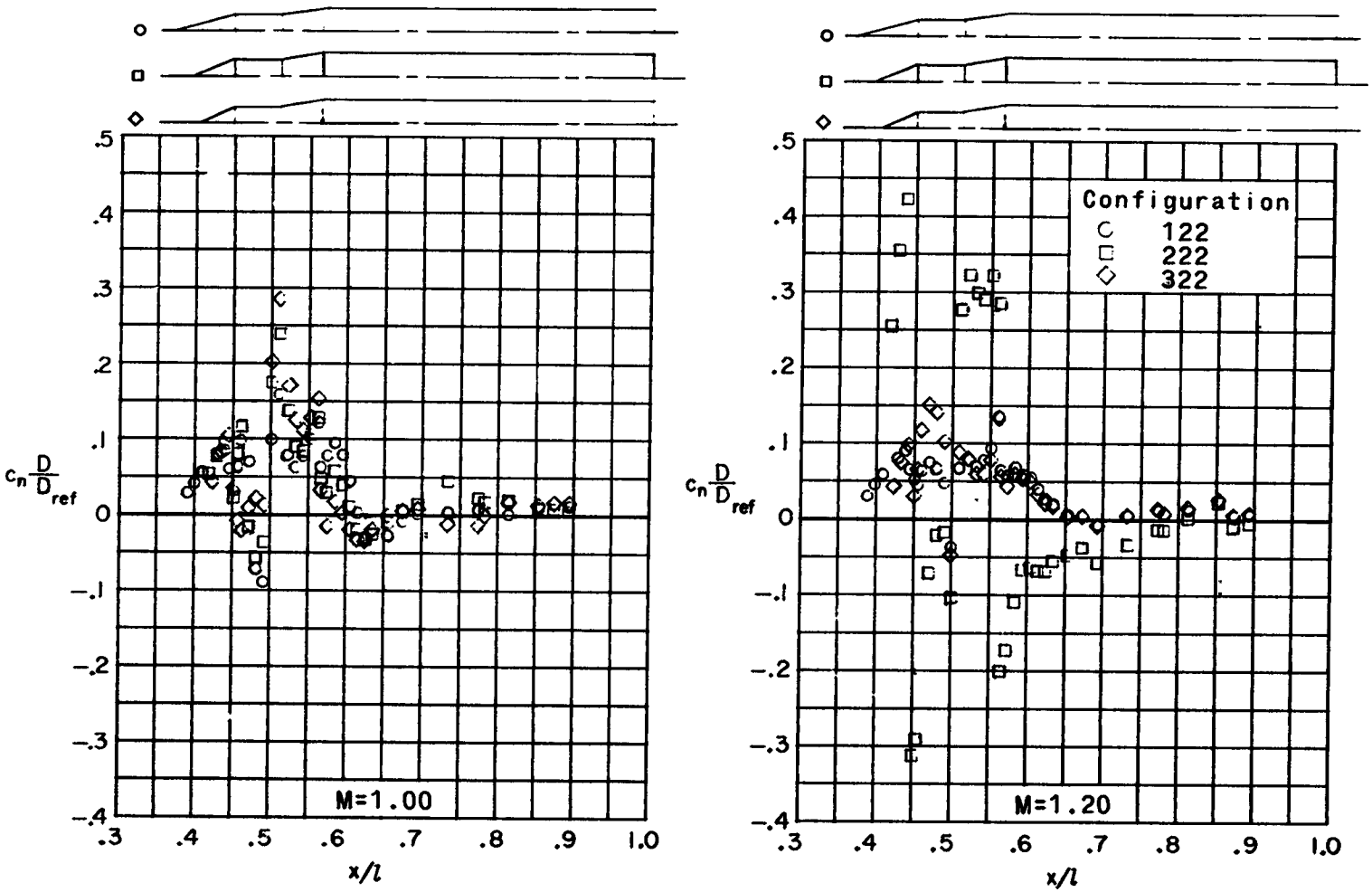
(a) Concluded.

Figure 10.- Continued.



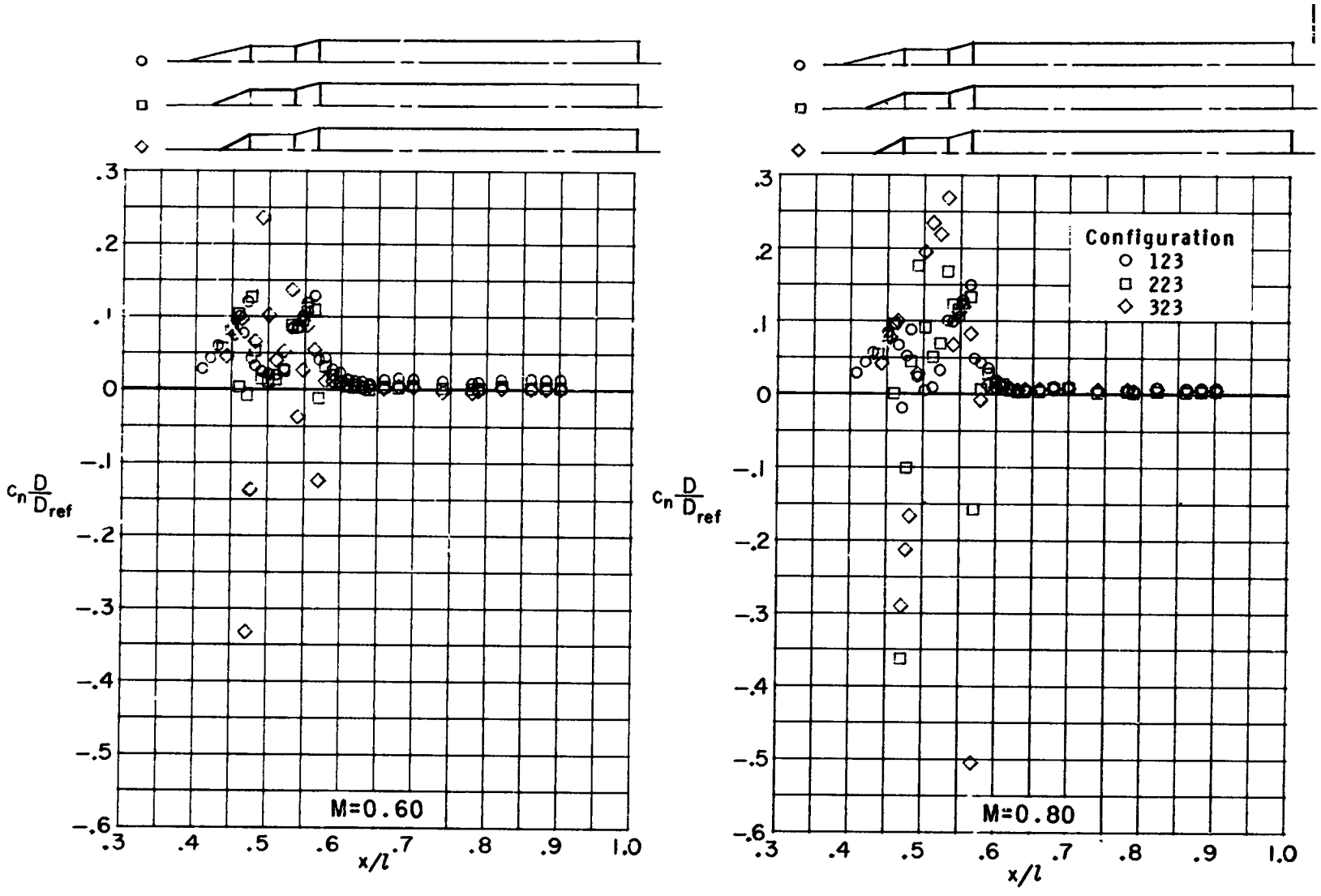
(b) $\delta_F = 10.1^o$.

Figure 10.- Continued.



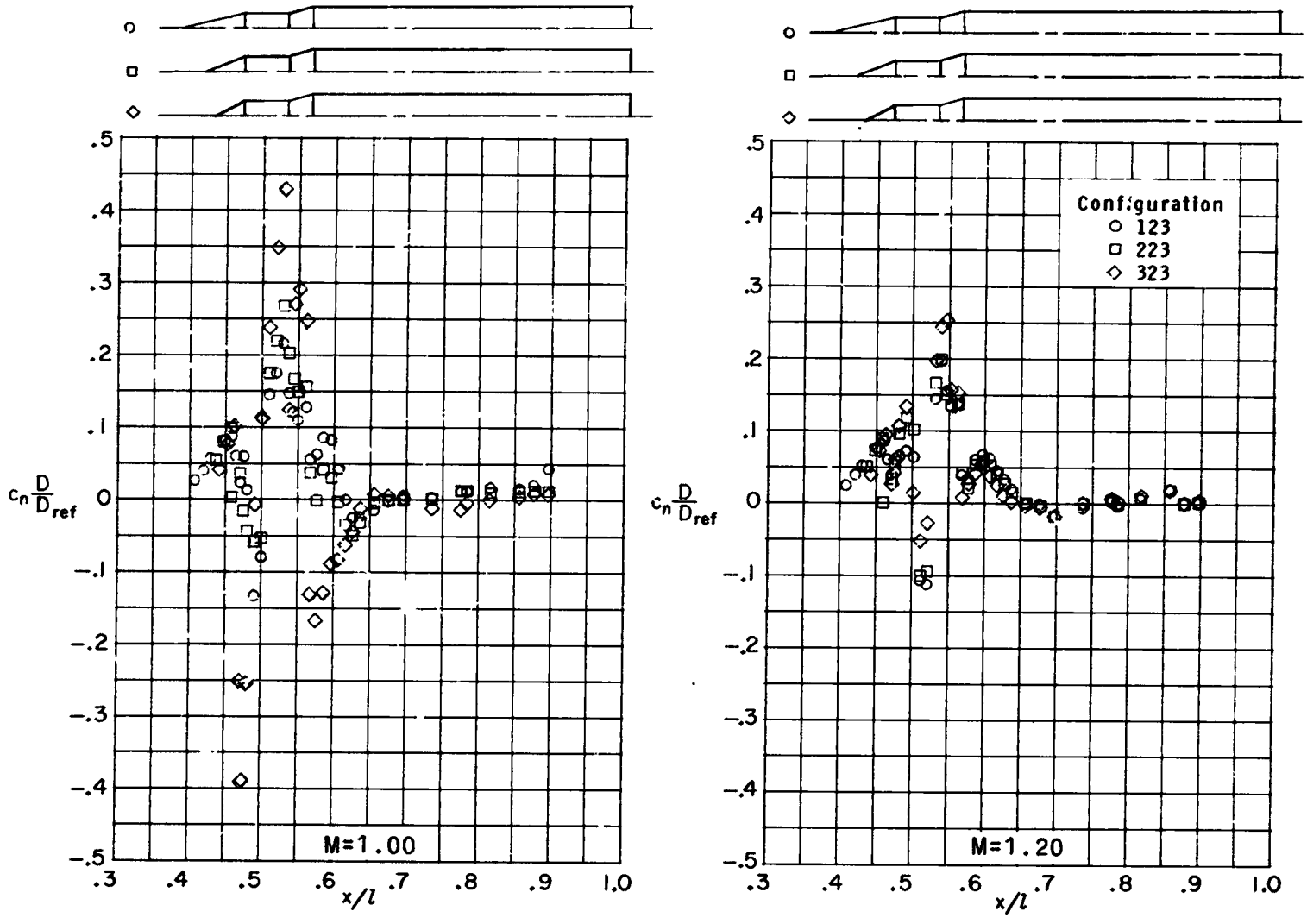
(b) Concluded.

Figure 10.- Continued.



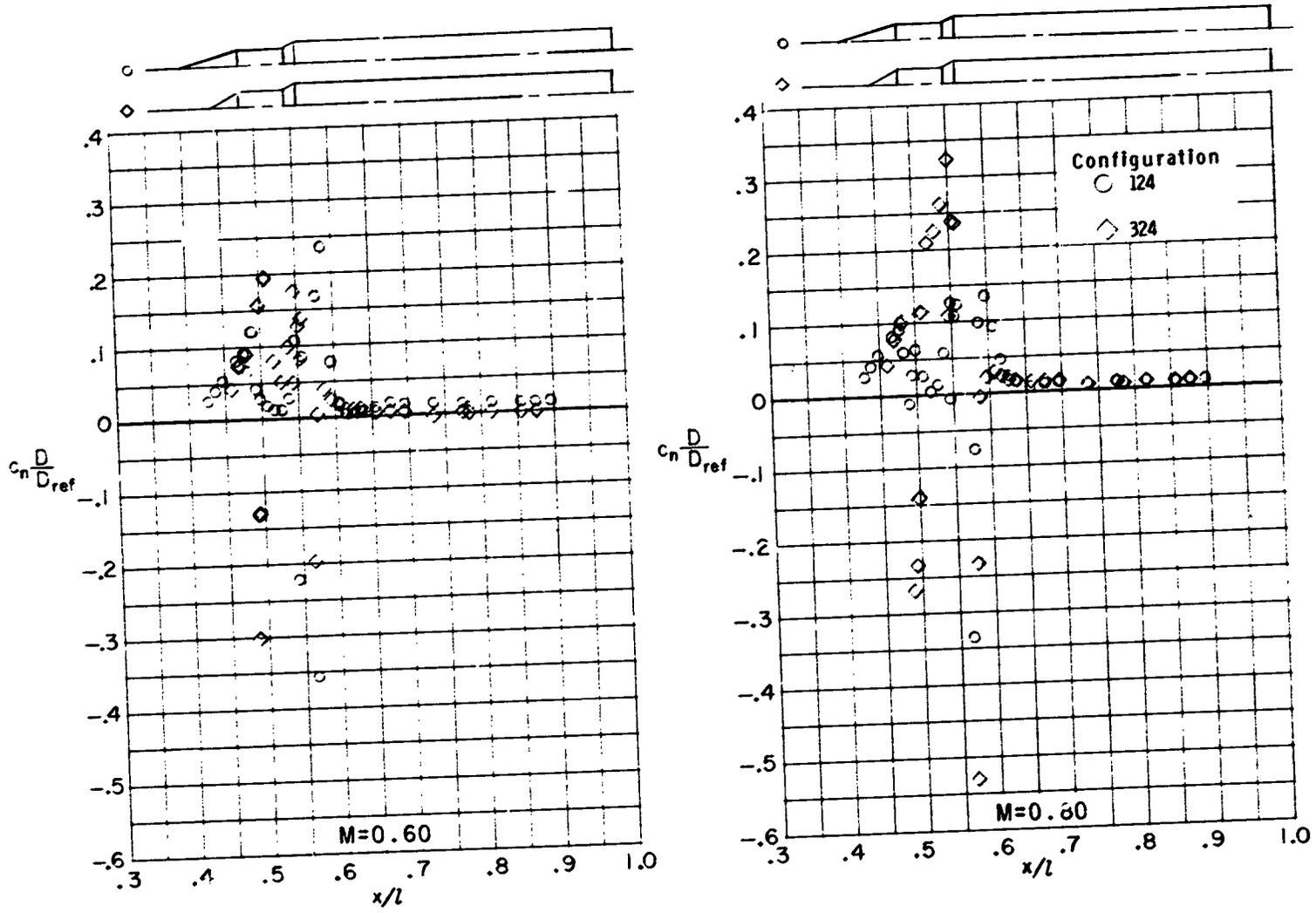
(c) $\delta_F = 15^o$.

Figure 10.- Continued.



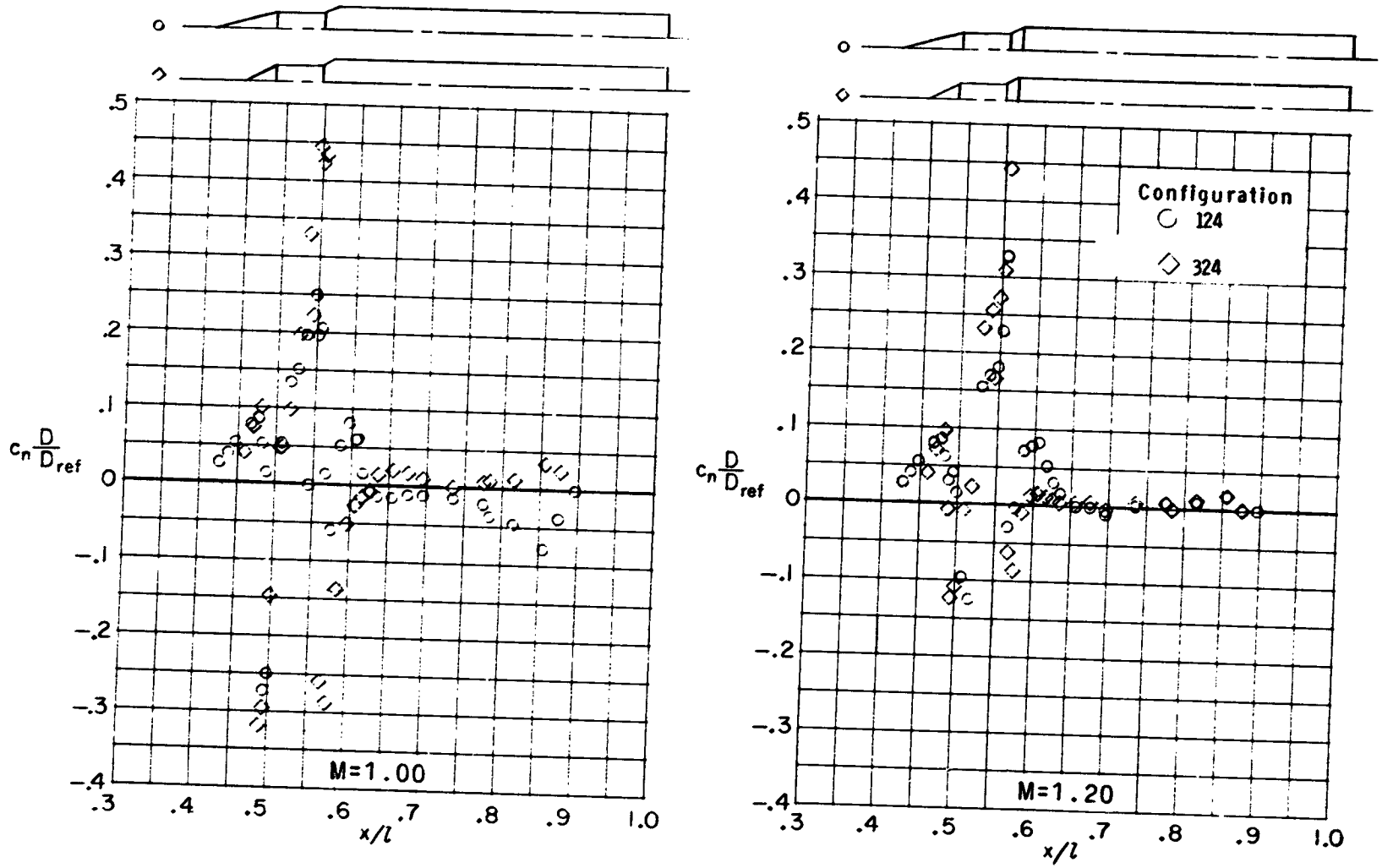
(c) Concluded.

Figure 10.- Continued.



(d) $\delta_F = 30^o$.

Figure 10.- Continued.



(d) Concluded.

Figure 10.- Concluded.