# NASA Contractor Report 3319

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Satellite Power Systems (SPS) Concept Definition Study

Volume II, Part 2 - System Engineering

G. M. Hanley

CONTRACT NAS8-32475 SEPTEMBER 1980





# NASA Contractor Report 3319

Satellite Power Systems (SPS)
Concept Definition Study
Volume II, Part 2 - System Engineering

G. M. Hanley Rockwell International Downey, California

Prepared for Marshall Space Flight Center under Contract NAS8-32475



Scientific and Technical Information Branch

1980



## **FOREWORD**

Volume II, System Engineering, is presented in two parts. Part 1 encompasses SPS system engineering aspects. Part 2 consists of a volume on SPS cost and programmatics; an appendix is included in Part 2 to cover the SPS WBS and cost estimates. Volume II of the SPS Concept Definition Study final report is submitted by Rockwell International through the Satellite Systems Division. All work was completed in response to NASA/MSFC Contract NAS8-32475, Exhibit C, dated March 28, 1978.

The SPS final report will provide the NASA with additional information on the selection of a viable SPS concept, and will furnish a basis for subsequent technology advancement and verification activities. Other volumes of the final report are listed as follows:

<u>Volume</u>	<u>Title</u>
I	Executive Summary
III	Experimentation/Verification Element Definition
IV	Transportation Analyses
v	Special-Emphasis Studies
VI	In-Depth Element Investigations
VII	Systems/Subsystems Requirements Data Book

The SPS-Program Manager, G. M. Hanley, may be contacted on any of the technical or management aspects of this report. He can be reached at 213/594-3911, Seal Beach, California.

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#### ACKNOWLEDGEMENTS

Since the publication of earlier Rockwell SPS cost, economic, and programmatic documentation—dating back to 1976—a continuing effort has been maintained to incorporate the latest program developments, expand the Rockwell SPS cost model; conduct comparative cost/economic analyses; prepare integrated schedules or networks; and define SPS program plans and resource requirements. The results of this work represent a professional contribution on the part of many individuals, where most of them have been with the SPS contract activity and supplementing company-sponsored efforts since the start of our effort. It is this contribution that requires acknowledgement.

The overall study activity was also supported by other business/industrial organizations and technical members of the SPS program team and their management, making it possible to reach the desired conclusions with the minimum of effort.

The Rockwell SPS program development team that contributed to the search, analyses, and results of this study are:

• Dr. L. R. Blue

Cost/Risk Programming

• W. Cooper

Cost Analysis

• D. E. Lundin

SPS Schedules/Networks

• A. D. Kazanowski

Resource Analysis

The overall SPS program development activity on SPS costs, schedules, program planning, resource analysis, and computer programming was completed under the direction of F. W. Von Flue.

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- · Engineering Cost Group
  - W. S. Rutledge
  - J. W. Hamaker
  - D. T. Taylor
- · Program Plans and Requirements Group
  - W. A. Ferguson
  - H. K. Turner

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# Satellite Systems Division Space Systems Group



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# 1.0 SPS COST AND PROGRAMMATICS

# 1.1 INTRODUCTION

U.S. energy demands continue to increase dramatically and the availability of traditional energy resources have become the focal point of national/international concern and economic balance. It is therefore important that alternate sources of energy be identified and evaluated as potential solutions to the law of supply and demand. In this regard, the possibility of generating large quantities of electrical power in space and transmitting it to earth offers a conceivable solution. However, economic and technological requirements of such a program needs to be established with confidence. This volume considers the cost and programmatic requirements for a recommended satellite power system reference concept evolving from a series of contracts and company-sponsored work completed by the Rockwell International Satellite Systems Division of the Space Systems Group.

The Rockwell SPS reference satellite and rectenna concept are illustrated in Figure 1.1-1. These configurations were used in the definition of costs and programmatics described in this volume. Typically, a single SPS provides 5 GW of electric power to the utility interface on the ground. The satellite is located in geosynchronous orbit and converts solar energy to dc electrical energy using large GaAlAs solar arrays at a concentration ratio of two suns. The dc electrical energy is conducted from the solar arrays to the microwave antenna where the energy is transformed to microwave RF energy. A large, 1-km-diameter, antenna beams the energy to a receiving antenna (rectenna) on the ground. The rectenna converts the RF energy, at very high efficiency, to dc electrical energy where it is collected and routed to conversion centers for subsequent input to the utility grid.

The overall scenario for SPS space transportation involvement is shown in Figure 1.1-2. Eight major elements comprise the transportation system:

- Shuttle
- SPS heavy-lift launch vehicle (HLLV)
- Electrical orbit transver vehicle (EOTV)
- Intraorbit transfer vehicle (IOTV)
- Personnel orbit transfer vehicle (POTV)
- Crew module (CM)
- · Leo propellant depot
- GEO propellant depot

The SPS HLLV is used to bring construction payload, crew expendables, and propellants for the EOTV and POTV. The IOTV is used to carry payloads over short

<sup>&</sup>lt;sup>1</sup>Satellite Power Systems (SPS) Concept Definition Study (NAS8-32475)—Exhibit C, March 1978; Exhibit A/B, March 1977; and the SPS Feasibility Study (NAS8-32161), August 1976.



Figure 1.1-1. SPS Reference Satellite and Rectenna Concept



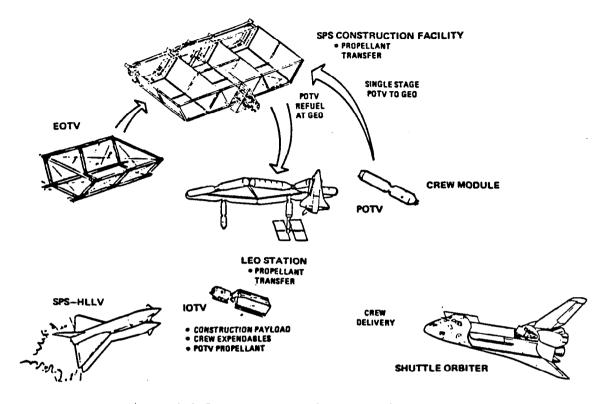


Figure 1.1-2. Transportation Operations Scenario

distances, e.g., between the SPS HLLV and the LEO station or EOTV, between the EOTV and space construction base (SCB), and between the Shuttle orbiter and the POTV. The EOTV carries payloads brought up in the HLLV between LEO and GEO. Because of the long flight duration of the EOTV, another vehicle (the POTV) is used to rapidly carry crew members between LEO and GEO. A crew module, capable of carrying 60 crew members, is needed to provide life support during crew transfer. The Space Shuttle provides transportation of crew, in its crew module, between earth and LEO.

The initial step in satellite precursor operations is to establish the LEO base as shown in the lower left of Figure 1.1-3. Crew and power modules are transported to LEO by Shuttle derivatives and assembled. When the base is fully operational, Shuttle external tanks are delivered and mated to form construction fixtures for SCB construction. Since the more economical HLLV will not be available, and since overall plans specify an EOTV test vehicle, it is probable that only the center trough of the SCB would be constructed initially. This trough would be used to fabricate the pilot plant EOTV with antenna. After proof of concept and SPS go-ahead, the remainder of the SCB would be completed, an initial fleet of EOTV's constructed, and the SCB transferred to GEO, using one or more EOTV's for propulsion and attitude control. Upon reaching GEO, satellite construction would commence, with the logistics support as shown at the right of the figure.

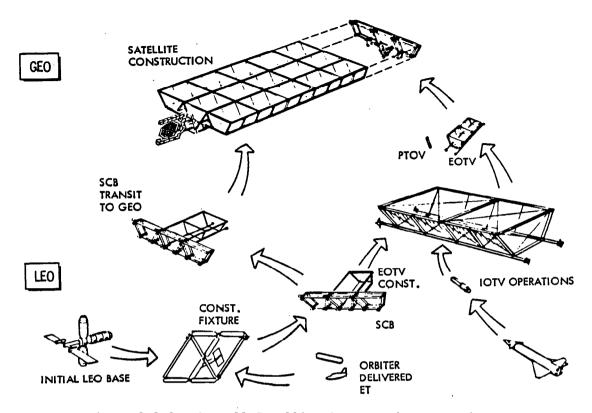


Figure 1.1-3. Overall Satellite Construction Scenario

This volume is divided into three sections that describe the program, study approach, and ground rules/guidelines (Section 1.0). Section 2.0 covers cost analysis definitions and summarizes SPS costs for each of the main elements—satellite, space construction and support, transportation/facilities, ground receiving station, and management/integration. Comparative assessments are presented along with a description of cost trades. SPS programmatic elements are presented in Section 3.0 to provide detail schedule/network information on the flow and sequence of design, development, construction, and operational activity. Included are some 13 program plans identifying operational requirements and considerations of the SPS program.

## 1.2 SPS GROUND RULES AND GUIDELINES

A series of ground rules and guidelines were used during the study to provide a common reference point for the uniform development of cost and programmatic elements of the SPS program. These considerations are itemized as follows.

1. The SPS WBS of Appendix A was used as the structure of program hardware, activities, and accounts.



- 2. Key dates of program planning:
  - 1980-1985 Ground-Based Exploratory Research Activities
  - 1981-1987 Key Technology Program Activities
  - 1990 Decision Point for SPS Commercialization (Phase C/D)
  - 2000 IOC of First SPS
- 3. Costs are reported at WBS level in terms of:
  - (a) Development cost and TFU (theoretical first unit)
  - (b) Initial capital investment average cost per satellite (Satellites TFU and No. 2 through No. 60)
  - (c) Replacement capital investment (RCI) cost and operations and maintenance (O&M) cost per satellite per year
- Cost estimates are projected in 1977 dollars and maximum use was made of past SPS studies and other associated data as appropriate.
- 5. SPS build rate will be two nominal 5-GW SPS systems per year for 30 years to provide a total capacity of 300 GW by 2030.
- 6. Overall SPS lifetime will be 30 years with minimum maintenance and no salvage value or disposition costs.
- Complete construction and assembly will occur at geosynchronous orbit.
- 8. Calculations are based on 0% launch losses.
- Program management and SE&I (management and integration) are costed at 5% of all other Level 2 costs.
- 10. 25% mass contingency is costed as a 15% cost contingency on SPS WBS items of the satellite (1.1), space construction and support (1.2), and transportation (1.3).

In order to promote a complete and understandable comparison of SPS concepts, and to maintain compatible economic and programmatic references, the SPS Work Breakdown Structure (WBS) Dictionary¹ was used as the baseline document for the definition and organization of program elements. This structure subdivided the program into lower-level elements within each major system grouping and associated the dictionary definition with special accounts and phases unique to the program. Accounts and phases were designated for the DDT&E; initial capital investment (covering initial procurement and placement of each SPS); replacement capital investment (capital asset replacement over the SPS operating life); and operations/maintenance (expendables and minor maintenance). This structural interface (Figure 1.2-1) provides the capability to view and analyze the SPS program from a number of programmatic, economic/cost, and management aspects. The WBS dictionary (Appendix A) was carefully maintained and updated throughout the study as the programmatic baseline.

<sup>&</sup>lt;sup>1</sup>SPS Work Breakdown Structure Dictionary, National Aeronautics and Space Administration, November 1978.

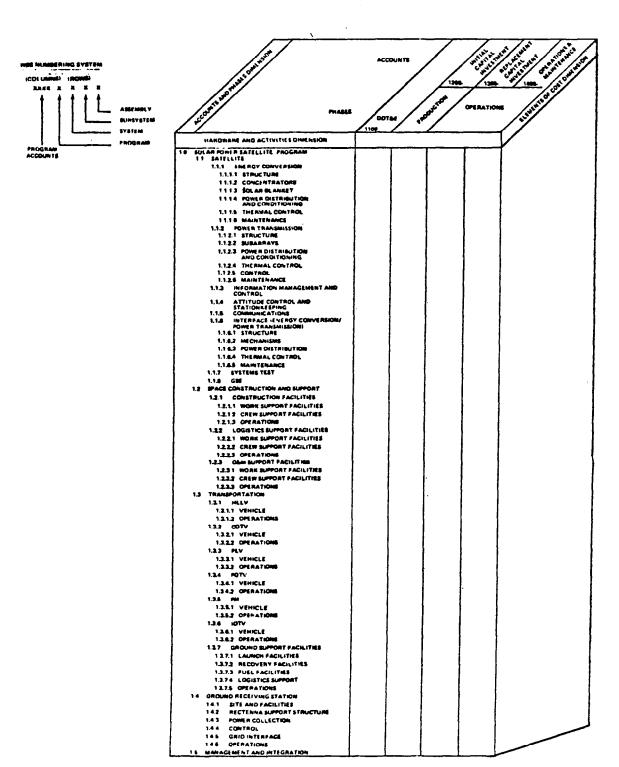


Figure 1.2-1. Satellite Power System Work Breakdown Structure



#### 1.3 STUDY TEAM AND INTERFACES

The SPS program development group functioned as an integral part of the overall SPS study team and participated in the progress and results of each task as it evolved. In addition to the daily interface with members of the Rockwell staff, discussions were held with representatives of the NASA/DOE. Supporting business/industrial representatives, such as those listed in Table 1.3-1, were contacted during the analysis and grass roots development of cost and programmatic estimates.

Table 1.3-1. Industry Contacts

ORGANIZATION	PURPOSE
SME (SOCIETY OF MANUFACTURING) ENGINEERS)	OBTAIN TECHNICAL DATA ON ROBOTICALS AND TECHNOLOGY STATUS
RIVERSIDE CEMENT CO.	RECTENNA CEMENT/CONCRETE REQUIREMENTS AND PROCESSES
MODERN ALLOYS, INC.	METHODS & EQUIPMENT FOR CONTINUOUS PLACEMENT OF RECTENNA PANEL CONCRETE FOOTINGS
SANDIA-SOLAR THERMAL	COMPARISON OF STTF CONSTRUCTION/HANDL- ING APPROACH WITH SPS RECTENNA REQ'TS
TOWNSEND & BOTTUM, CONST. MGRS, 10 MW SOLAR PLANE IN BARSTOW, CA	SITE PREPARATION AND CONSTRUCTION OPERATIONS
AMERICAN BRIDGE - A DIVISION OF UNITED STATES STEEL	STEEL REQ'TS & CONSTRUCTION APPROACH FOR INSTALLATION OF RECTENNA PANELS
ALPHA-BETA DISTRIBUTION CENTER	ANALYSIS OF MATERIALS HANDLING SYSTEMS
• CATAPILLAR	EARTH MOVING & GRADING EQUIPMENT
• INTERNATIONAL HARVESTER	EARTH MOVING & GRADING EQUIPMENT
SOUTHERN CALIFORNIA EDISON	DC/AC POWER DISTRIBUTION LINES/TOWERS

## 1.4 STUDY APPROACH

The objective of the study was to provide NASA with additional, accurate, and sufficient data and information to enable the selection of preferred viable SPS concepts by CY 1980 as a basis for subsequent technology advancement and verification activities in the CY 1980-1987 time frame. In this regard, the cost and programmatics contribution is documented in this final report. The results of each task evolved from two major activities: (1) a review and update of contract Exhibits A and B costs as reported in April 1978; and (2) the extensive analysis, selection, and determination of cost estimates, along with program plans/schedules applicable to the newly selected Rockwell SPS reference configuration of Exhibit C—especially the expansion of transportation and ground-receiving station data bases. All results of this work were consistent with SPS ground rules/guidelines and contract requirements covering four areas as detailed in the study plan:

- Cost Analysis
- Schedules/Networks
- · Planning Packages
- Program Plans

Figure 1.4-1 identifies the close interrelationship of these tasks, the source of data, and the flow of cost and programmatic information into applicable final report volume such as this Part 2 of Volume II—Systems Engineering that summarizes the activity in all areas.

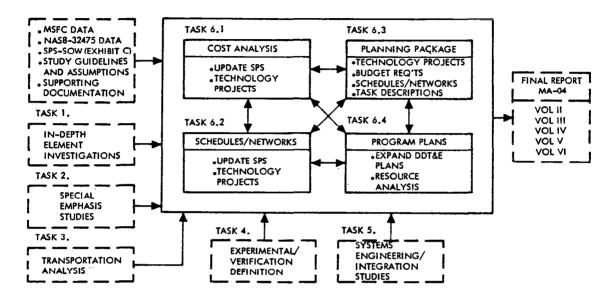


Figure 1.4-1. Cost and Programmatic Approach

## 2.0 COST ANALYSIS

## 2.1 INTRODUCTION

Results of SPS cost analyses, trades, and sensitivities are described in this section. Cost estimates of the Rockwell SPS baseline concept were updated in June of 1978, and shortly thereafter the reference NASA SPS concept replaced the earlier configuration. It is the reference configuration, with some design improvement, that was used in the development of cost and programmatics. The following discussion covers the costing approach/methodoloy; cost-effectiveness results; and SPS cost estimates, including time-phased costs of DDT&E and TFU.

## 2.2 SPS COSTING APPROACH

The SPS cost analysis has been performed on the Rockwell reference configuration discussed in this report. The Exhibit C study considered an SPS option of 60 units with an IOC in the year 2000 and the full 300-GW capability to become operational at the rate of two SPS's or 10 GW per year. The Rockwell cost model was structured to the NASA SPS Work Breakdown Structure and Dictionary of November 1978, utilized the MSFC CER data base, and incorporated grass roots analyses and information from the Rockwell CER data base. This continuous interaction to seek and establish better cost estimates has resulted in a higher degree of confidence in the resultant cost estimates, as compared with those of the Exhibit A/B final report. While the cost estimating relationships were developed to be as accurate as possible, it is too early in the definition process of the SPS to precisely predict either the final system point design or point estimate. However, it is believed that another step has been taken to predict the direction and relative magnitude of cost impacts and to aid in design determination/decisions of preferred concepts.

There are basically four types of cost equations in the model, corresponding to the four WBS accounts—DDT&E, initial capital investment, replacement capital investment, and operations and maintenance. The cost methodology is shown in detail in Appendix B as it covers CD (DDT&E), CTFU and CIPS (initial capital investment); CRCI (replacement capital investment); and CO&M (operations and maintenance). Appendix B also provides a brief narrative description of each CER, its application, input data, and the calculated value for each type of costs.

The DDT&E equation (CD) estimates the cost of design, development test/ evaluation and non-recurring costs. Separate factors were utilized to calculate the proportional assessment for management and integration and as a cost contingency for mass growth. In view of the gross nature of the level of information currently available on WBS 1.1.7—System Test (hardware/operations) and Ground Support Equipment—the cost of systems test was assumed at 100% of the satellite system ICI cost; whereas GSE was factored at 10% of the satellite DDT&E cost through 1.1.7.

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The applicable total system mass, area, or power was used as the inputs for DDT&E CER's. A development factor (DF) is included in the equation to adjust the cost to reflect only that portion of the total system mass, area, or power considered to be necessary for development of the complete system where it is not required to develop the total mass, area, or power. The CD cost equation also allows for the application of a complexity factor (CF) to adjust the cost results when it is determined that the item being estimated is either more or less complex than the CER base data.

The initial capital investment (ICI) cost equations estimate the initial capital investment cost of hardware items as a function of their mass, area, or power. The ICI cost equation is expressed in several different forms-CLRM, CTFU, CTB, and CIPS. The CLRM (cost of lowest repeating module) equation requires that the point estimate correspond to the mass, area, or power of the lowest repeating module (M). This is necessary because of the physical scale of the SPS and the production quantities required for many of the hardware elements. It is not reasonable to estimate the SPS initial capital investment cost as a historical function of the entire SPS mass, area, or power. Rather, it is desirable to cost the number of repeating modules required per satellite to establish the satellite theoretical first-unit cost (TFU), and then input the satellite TFU cost into a progress (learning) function for the quantity of satellites required to calculate the average unit cost (IPS). This calculation involves two steps in the cost equations. The first step (CLRM) is simply the portion of the equation which estimates the theoretical first repeating module cost as discussed above. The second step (CTFU) has the progress function incorporated into the equation for the quantity of repeat modules required per satellite. This is automatically taken into account with the progress over production quantities as required when calculating the cost to build (CTB). CTB calculations are then factored on the basis of a requirement to construct an SPS divided by the option quantity.

At the current level of SPS definition, it was difficult to define a repeating module. It is often impossible to know with any certainty just what portion of the total mass is appropriate to run through the equation as a module. It is just as difficult to identify how many distinct types or designs of modules will be required for any subsystem or assembly. In such cases, the study simply assumed a module mass (or area or power) based on an engineering best judgment.

Replacement capital investment (CRCI) CER's provide for the multiplication of the annual spares fraction (R) of each system by that system's cost to arrive at an RCI cost per satellite per year.

Operations and maintenance costs (CO&M) are estimated in terms of O&M cost per satellite per year. O&M costs include those expenditures incurred in day-to-day operations, beginning with SPS initial operating capability (IOC) and continuing over the life of each satellite. They consist of wages of O&M personnel, minor repairs and adjustments to systems to maintain an ordinarily efficient operating condition, expendables and consumables, launch costs for delivery and transfer of on-orbit personnel, and cargo resupply of expendables and consumables, etc. O&M costs are calculated by the use of a direct cost input or by an annual factor per SPS times the cost to build the particular system.



The cost methodology seeks to account for five separate effects which influence SPS cost: scaling, specification requirements, complexity, the degree of automation, and production progress. Scaling refers to the relationship in cost between items varying in size, but similar in type. Economies of scale usually ensure that such a relationship will not be strictly linear, but rather as size increases the cost per unit of size will decrease. The scope of this relationship is reflected by the equation exponent which results from the regression analysis of the data used to develop the cost estimating relationship.

Specification requirements have been accounted for by normalizing the CER data base to manned spacecraft specification levels, using factors from the RCA price model. From that model, an average cost factor to adjust MIL-SPEC to manned spacecraft is around 1.75 for DDT&E and 1.6 for production cost. Under the assumption that some relaxation of Apollo-type specifications can be made for the SPS, a factor of 1.5 was assumed for both DDT&E and production cost. Furthermore, it was assumed that a factor of 3.0 would adjust commercial specifications to SPS requirements; therefore, military or commercial cost data used in the CER's were adjusted upward by factors of 1.5 and 3.0, respectively.

The cost equations allow a complexity factor input to adjust the cost result when it is determined that the item being estimated is either more or less complex than the listed CER data base.

The degree of automation is accounted for in certain cost equations through an adjustment to the CER coefficient by the tooling factors given in Appendix B. The effect of tooling is dependent upon the annual production rate. Higher production rates allow harder tooling and, thus, effect cost reductions. The tooling factors are used only on those CER's which are based on historical aerospace programs with limited annual production rates. Tooling factors are not used (and thus are not exercised as part of the equations in Appendix B tables) on those CER's which are based on data already reflecting automated production techniques (e.g., the commercial electronics data for the microwave antenna CER).

Finally, the decreasing cost effects of progress, due to production process improvements or direct labor learning, are accounted for through standard progress functions. Many SPS components will be mass-produced in a capital intensive manner and will experience little labor learning. Other SPS hardware items, however, will be produced at very low annual rates much in the labor intensive manner of historical spacecraft programs and would therefore experience learning. (Technically distinguishable from learning—but still predictable with the same form of exponential function—are the effects of production process improvements. In this model, when progress functions are used, they are meant to account for both of these effects.) A constant relationship has been assumed between the progress fraction and the annual production rate.

<sup>&</sup>lt;sup>1</sup>Equipment Specification Cost Effect Study, Phase II, Final Report, November 30, 1976, by RCA Government Systems Division.

As required by the costing ground rules and assumptions, all CER's are in terms of 1977 dollars. The study did assume 1990 technology and 1990 supply/ demand conditions which, in some cases, resulted in differential (non-general) price inflation or deflation between 1977 and 1990 being included in the CER's. Specifically, it was assumed that composite raw material prices and some electronic component prices will decrease relative to general prices, while aluminum coil stock prices will increase relative to general prices. Such effects are allowed for by the CER's but only to the extent that the expected price changes differ from expected general price changes. The CER's affected are those for the antenna structure, power source structure, and microwave antenna.

#### 2.3 SPS COST ESTIMATES

Total program costs were developed for WBS sub-level elements of DDT&E, production, launch, orbital assembly/construction, ground operations, replacement capital, and operations/maintenance. This section will present summarized cost data and describe the elements contained in each program phase.

Tables 2.3-1 and 2.3-2 summarize cost information for each main segment and phase of the SPS program. Table 2.3-1 shows development cost data through the first full 5-GW operational satellite (TFU) including space transportation, construction, operations, and the ground receiving station plus grid interface and facilities needed to establish the SPS operational capability of the ground and space segments. As such, all cost estimates for the TFU include systems, equipment, facilities, and machinery that have a service life capable of

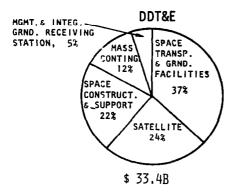
₩BS # DESCRIPTION DOTEE 1 SAFELLITE PUWER SYSTEM (SPS) PROGRAM 33-C1.762 51103.242 84505.000 SATELLITE SYSTEM 7950.922 1.1 7933.570 15884.492 1.2 SPACE CONSTRUCTION & SUPPORT 7331.160 8602.523 15933.703 12468.316 1.3 TRANSPORTATION 22866.199 GROUND RECEIVING STATION 115.699 3618.727 3734.427 ... MANAGEMENT AND INTEGRATION 1392.463 2151.918 3544.382 MASS CONTINGENCY 4160.031 5912.945 10072.977

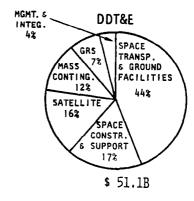
Table 2.3-1. SPS Program Development Cost

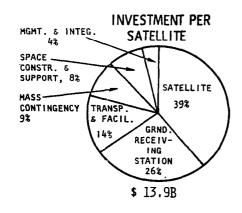
building more than one SPS. Table 2.3-2 summarizes (1) the investment per satellite (including ground station) of the option of 60 SPS's at a build rate of two 5-GW systems per year, and (2) the annual cost per satellite for replacement capital and operations/maintenance. Figure 2.3-1 illustrates a distribution of the costs as the program moves through its phases of DDT&E, TFU, and production/operations. The investment per satellite (average cost) includes the cost to build a 5-GW satellite, ground receiving station, and apportioned transportation/space construction requirements.

Table 2.3-2. SPS Program Average Cos	Table	2.3-2.	SPS	Program	<i>Average</i>	Cost
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WBS #	DESCRIPTION	INV PER SAT	** OPS RCI		AT PER YEAR TOTAL OPS	** TUTAL
1	SATELLITE POWER SYSTEM (SPS) PROGRAM	1 13677,008	451.531	193.713	645.244	14522.910
1.1	SATELLITE SYSTEM	5325.422	205.265	0.705	205.970	>531.391
1.2	SPACE CONSTRUCTION & SUPPORT	1148.332	51.428	11.274	62.701	1211.033
1.3	TRANSPORTATION -	1949.004	119.343	90.00	200.212	2149.216
1.4	GROUND RECEIVING STATION	3590 .622	0.275	78 .377	78.652	3669.474
1.5	MANAGEMENT AND INTEGRATION	600.674	18.815	8.561	27.377	628.055
1.6	MASS CUNTINGENCY	1263.413	56.405	13.927	70.332	1333.745







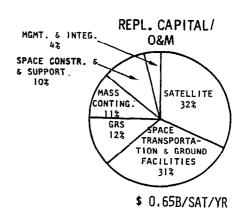


Figure 2.3-1. SPS Cost Relationships

#### DEVELOPMENT COST

The DDT&E phase consists of the one-time effort associated with designing, developing, and evaluating the components, subsystems, and systems required for the SPS project. It includes the development engineering, testing, and support necessary to translate a performance specification into a design. It encompasses the preparation of detailed drawings for system hardware fabrication, system integration and—depending on the system, subsystem, or component—structural, environmental, and other required tests. It includes the early supporting research and technology analyses, advanced study efforts and requirements definition related to the SPS microwave power transmission system, power conversion, structure and assembly and power distribution; component development; integrated ground test programs; the Geosat space tests and LEO Shuttle sortie demonstrations, both shared and dedicated. It also includes related Shuttle-derived HLLV transportation systems and development of an SPS prototype demonstration test article which, following demonstrations, will be upgraded to an operational EOTV. Also included are the analyses of data and the necessary redesign and retest activities to meet specifications; and ground support equipment, special test equipment, and other program-peculiar costs not associated with repetitive production. All DDT&E effort associated with SPS-related support systems such as transportation, space construction base, and assembly/support equipment necessary to accomplish the satellite DDT&E phase is also included.

DDT&E and TFU costs are combined in Figure 2.3-2, identifying major percentiles that make up the \$84.5 billion total. The SPS VTO/HL HLLV is a main contributor to the space transportation requirement along with the rectenna

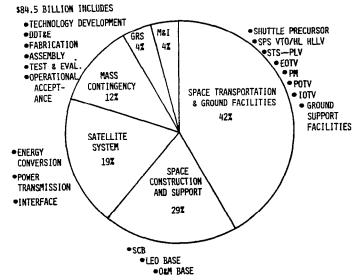


Figure 2.3-2. Cost Relationship Through the First SPS

support structure/power collection elements of the ground receiving station. TFU space transportation at \$19.67 billion is divided among vehicle fleet and operations breakdowns as shown in Figure 2.3-3, where the SPS VTO/HL HLLV identifies a five-vehicle requirement and 234 round-trip flights. Space Shuttle

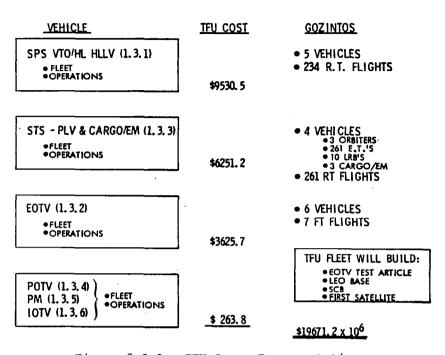


Figure 2.3-3. TFU Space Transportation

requirements represent vehicles and operations of the traffic model necessary to build the TFU and complete precursor activities covering the early program microwave test article, LEO base, satellite construction base (SCB), initial EOTV's; and to provide personnel during TFU fabrication/assembly and checkout activities. The SCB comprises over 76% of the \$8.6 billion estimated for space construction and support, with about \$4 billion required in work support facilities, and \$2.6 billion in crew support facilities. Energy conversion (25%) and power transmission (48%) comprise the majority of satellite system costs projected at \$7.95 billion. The TFU GRS breakdown identifies 88% of the cost in the rectenna support structure and power collector, with major costs in the steel panel/installation and antenna array elements as shown in Figure 2.3-4.

Costing of DDT&E for the space base elements, STS-HLLV, and the assembly and support equipment followed the more conventional method of determining DDT&E cost—that is, based upon total subsystem mass, area, or power. This technique was used mainly from the standpoint that the cost data utilized to develop the applicable CER's for these elements were comparable and were developed on the basis of total subsystem mass, area, or power. In the case of the satellite, comparable historical DDT&E cost data were just not available for the magnitude of the satellite subsystems.

In view of the physical size of the satellite subsystems and the large quantities required for certain parts and components, it was not considered reasonable to estimate the satellite subsystem DDT&E costs as a function of

the total mass, area, or power per satellite as is generally the method. Rather it was considered desirable to determine the satellite subsystem DDT&E costs by the application of a development factor.

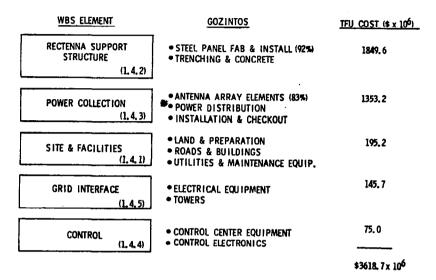


Figure 2.3-4. TFU Ground Receiving Station

The development factor was determined by engineering and, in general, was estimated at a factor considered appropriate to the development of total system or subsystem based on parameters of mass, area, or power. In some cases it was determined that the factor should be slightly higher or directly related to the development scenario of the particular system. For example, crew and work support modules of the LEO, SCB, or satellite operations and maintenance base are of common design but required at different times of the program. Appropriately then, development factors were assessed at 100% for modules required at the first point of usage, whereas a factor of lesser value was used on subsequent modules as a means of compensating for subsequent development or design integration costs.

## INVESTMENT AND OPERATIONS

Investment and operations costs developed during the study were presented in Table 2.3-2 and Figure 2.3-1. Investment costs were developed at two levels—initial capital investment (ICI) which is the cost of production, assembly, installation, transportation, and testing of each individual satellite produced, ground station system, and associated effort necessary to bring the power satellite on line to a full 5-GW operational capability; and replacement capital investment (RCI) which are those expenditures relating to capital asset replacement and major maintenance overhauls that are expected to last for more than one year and result in an improvement to the operating system. Replacement capital requirements for the systems used to construct the satellite through IOC are included in the initial capital investment costs. Costs for the fleet, for example, needed to support 0&M, are estimated and included as replacement capital investment. Operations costs consist of the effort required to operate and maintain the SPS project over its operational lifetime.



Investment per satellite is equivalent to the average unit cost of the total SPS requirement (TFU plus Satellites 2 through 60). This total average cost of \$13.88 billion includes a 15% cost contingency for growth in the mass of WBS elements 1.1, 1.2, and 1.3. Satellite system costs of \$5.33 billion are made up of power transmission (59%) and energy conversion (35%). The GRS estimate of \$3.59 billion is primarily in the rectenna support structure and power collection system. SPS replacement capital and operations/maintenance phases are estimated at a total annual cost of \$0.65 billion per year per SPS. The total average (investment) cost per nominal 5-GW satellite yields an investment cost of \$3010/kW.

An analysis of potential major cost drivers (Table 2.3-3) was prepared for the Rockwell SPS CR-2 reference configuration of March 1979. Over 90% of the costs are represented within each program phase DDT&E, TFU, average satellite, and RCI/O&M. Close review will show that certain elements are consistently cost drivers requiring programmatic studies and analyses of SPS design and technical approaches.

Table 2.3-3. Potential Cost Drivers Rockwell SPS Reference Configuration (March 1979)

	DDT&E	TFU	AVG. SATELLITE	RCI/O&M
MAJOR PROG, ELEMENT	\$33, 40B	\$51, 10B	\$13,888	\$0,658/ SAT/YR
PERCENTAGE OF TOTAL	95%	96%	91%	90%
Satellite Syst. (1, 1)	21%	15%	36%	30%
	• Ground test hardware & operations	● Power transmission	• Power transmission	Power transmission
	Power transmission	•Energy conversion	•Energy conversion	}
	Precursor EOTV	● EOTV test article		
Space Construction	22%	15%	7%	5%
& Support (1, 2)	Space construct, base	• Space construct, base	Satellite O&M base	Space construct, base
		1 '	Salomino outri baso	Space construct base
	• LEO base	• Satellite O&M base		
Transportation / Ground	35%	44%	12%	28%
Facilities (1.3)	SPS VTO-HL HLLV     Ground facilities     Pers. launch vehicle	SPS VTO-HL HLLV PLV EOTV Ground facilities	●SPS VTO-HL HLLV ●PLV	• SPS VTO-HL HELV • PLV
Ground Receiving		6%	23%	12%
Station (1.4)		• Rectenna support structure	Rectenna support structure	Operation
		Power collection	Power collection	
Management/Integration	17%	16%	13%	15%
(5%) and Mass Contin-	• Management & integra.	Management & integra.	•Management & integra.	Management & Integra
gency (15%)—(1.5, 1.6)	, , , , , , , , , , , , , , , , , , ,	1 -	1 -	
	<ul> <li>Mass contingency</li> </ul>	Mass contingency	• Mass contingency	• Mass contingency

#### SPS COST BY YEAR

A spreading function curve (ojive) was used in the time-phasing of costs against each main line item of the SPS WBS at a subsystem level. The cost spreading was projected for DDT&E and TFU costs by using various functions between the 20/80 and 80/20 curve spread. This approach provided distributions supporting a low front-end buildup with the flexibility to shift costs in a manner suitable to the phasing of subsystem development and start-up requirements.

Table 2.3-4 summarizes full-scale DDT&E and the incremental cost buildup leading to the TFU IOC by the year 2000. A relatively low profile prevails through the 1980's, reflecting activity of the ground-based experimental research and technology development programs on power transmission, PD&C, energy conversion, large space structures, and space transportation. The costs expand rapidly through the mid/late 1990's as the DDT&E activities accelerate and the Phase C/D programs begin on the satellite, space operations, transportation, and ground receiving station including facilities and equipment for hardware buildup in support of early launches, ground operations, and space construction tasks.

Table 2.3-4. DDT&E Plus TFU Cost By Year (\$ Millions).

YEAR			1.3-	1.4	1.5/1.6	TOTAL_
TEAR	4.4	<b>±• -</b> .	1.5	1.7	1.5/1.0	
1980	0.16	0.0	7.07	0.0	2.10	9.32
81	1.55	C.3	47.26	5.00	14.15	62.96
82	5.41	0.0	121.37	0.02	36.51	163.61
83	12.54	0.0	222.23	0.05	58.44	303.26
84	23.90	0.0	3+2.31	<b>6.09</b>	107.34	473.71
85	44.17	0.0	473.73	0.14	151.74	664.78
86	77.57	0.0	605.27	C.2C	199.50	885.83
87	126.38	127.61	777.32	0.25	244.03	1251.19
887	194.19	700.97	1060.75	0.29	294.25	2255.49
89	374.04	1385.59	1379.05	0.33	525.73	3544.75
90.	407.19	1812.37	1742.91	1.35	911.76	4935.58
91	072.72	1765.71	2281.03	2.03	1240.52	5955.59
92	945.4C	1158.46	2957.09	93.87	1451.14	6537.96
93	1445.54	501.35	30:2.37	364.65	1613.62	7007.59
94	20+7.56	659.73	3426.00	663.12	1628.74	8426.14
95	2534,40	1386.53	4017.93	798.15	1528.12	10265.13
96	20 1.31	1900.73	4350.34	755.63	1324.23	10944.24
97	4212.48	1963.53	3957.70	601.50	1040.33	9770.32
98	1423.47	1557.52	2 548 . 40	341.65	710.51	6331.62
99	603.89	835.79	1452.49	96.89	379.71	3364.70
000	157.39	176.82	259.51	10.40	103.67	715.38
	0.5	0.0	0.0	0.0	0.3	0.0
	2.0	0.0	3 • .	0.0	3.3	0.0
TOTA	5884.46	.5933-69	35334.97	3734.42	13617-33	54534.87

Figure 2.3-5 graphically displays the funding requirements and peak year distributions for DDT&E and TFU, where DDT&E costs peak at \$4.27 billion in 1991. This time period corresponds to the activation of Phase C/D operations on the TFU. The TFU costs peak at \$9.18 billion in 1996, which is the period of system/hardware production.

# 2.4 COST EFFECTIVENESS

During the study, a number of analyses were completed on the satellite, transportation, space construction, and ground station elements of the SPS program to develop specific system requirements for use in costing. These included traffic models, mass statements, system definitions, vehicle usages, and trade studies for cost assessments. The majority of these parameters are included in the discussions with appropriate CER's submitted in Appendix B.

Study activities completed under the Exhibit C contract include:

- A detail review and update of SPS economic/cost data as completed and submitted on the Rockwell SPS Point Design Concept of June 1978, focusing on operational requirements of the satellite, ground receiving station (rectenna), and transportation systems for that configuration. The analysis of space transportation elements identified construction and operations/maintenance flights, vehicle usages, and fleet attrition/spares.
- CER's were implemented and programmed on the computer as supplemented with the results of grass roots analysis and engineering assessments based on cost information in the NASA data base, Rockwell contracts, and company-sponsored studies.
- A transportation system study normalized cost data from NASA/Boeing contracts and the Rockwell Shuttle Growth contract study to project costs on the VTO-HL HLLV, Space Shuttle, orbiter, and PLV.
- A grass roots analysis was completed on the GRS to establish rectenna panel, concrete, power distribution, and supporting system costs. The results were compiled into line item estimates and total costs for GRS DDT&E, TFU and investment.

A rectenna panel payback analysis was completed to determine the cost effectiveness of a panel located in the perimeter of the rectenna farm. Revenue calculations were based on the incident microwave power per panel in the outer edge (Zone V) of the rectenna, as shown in Figure 2.4-1. The annual revenue from electric power was based on 40 mils per kWh, or \$350 per year. An average cost of \$5000 per panel was projected for the fixed costs, including some mark-up. Variable costs per panel considered replacements and 0&M projections. Figure 2.4-2 identifies a payback period for panels in Zone V as varying from 3.5 to 14 years. However, the analysis shows that a panel intercepting 6  $\rm W/m^2$  can break even in a 30-year period.

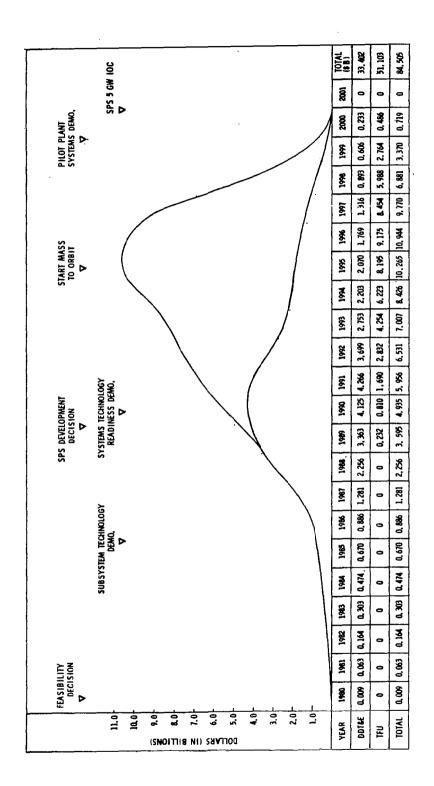
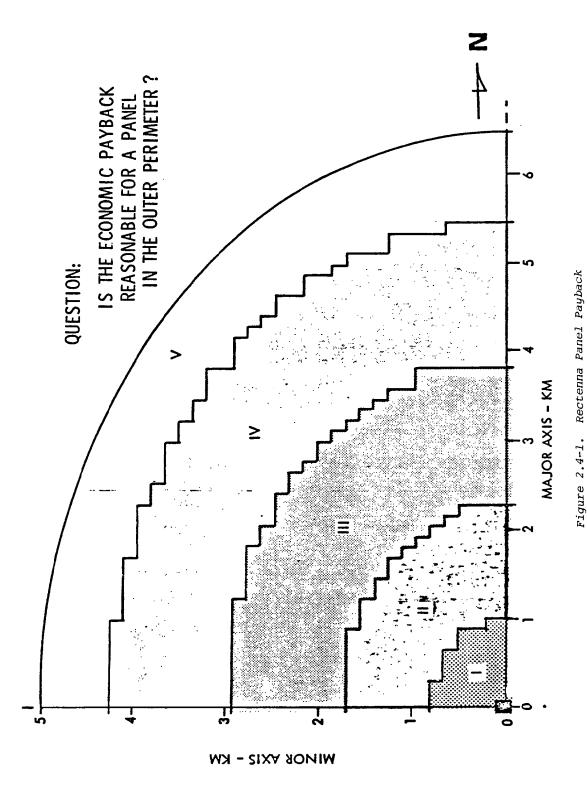


Figure 2.3-5. Time-Phased DDT&E and TFU Costs



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## 3.0 SPS PROGRAMMATICS

#### 3.1 INTRODUCTION

This section presents SPS program plans for the implementation of Phase C/D activities leading to the initial operational capability of the first SPS by the year 2000. These plans describe SPS program schedules and networks, critical items of system evolution/technology development, and the natural resource analysis.

Most key technological issues (as described in Volume III) will have been resolved prior to the main Phase C/D effort and, therefore, technology in that sense is not the real concern of this section of the report on plans. Rather, the size of the SPS undertaking, its producibility, testing, logistics, facilitization, and support requirements dictate the main program plan areas covered in this section (Table 3.1-1). As a secondary objective, planning areas requiring substantial effort in the immediate future were identified. This work concentrated on the definition of specific problems, the solution of which might require the longest lead times for accomplishment or implementation.

Table 3.1-1. SPS Program Plans

- Program Management
- Systems Engineering and Integration
- Design and Development
- Systems Testing
- Ground Support Equipment—D&D
- · Manufacturing

- · Product Assurance
- Facilities
- · Ground Operations
- Space Operations
- · Launch Operations
- · Specification Tree
- Natural Resource Analysis

The SPS is a vast undertaking, requiring commitments of significant magnitude and long duration. Therefore, a well planned and funded SPS program is essential and the orderly, in-phase development of program plans is necessary to the accomplishment of long-range objectives and in permitting budgetary requirements to be established with sufficient lead time to assure commitment.

Success of the SPS program is critically dependent on bringing together a number of related system projects. In addition to the satellite and ground station, as major items of operational hardware, associated programs such as the Space Transportation System and supporting SPS facilities should be conducted in parallel and time-phased to interface as an integral part of a coordinated SPS program. Failure to complete any of these program efforts, in keeping with the SPS master schedule, would result in a corresponding delay in the availability of an operational system to serve as a significant national power resource.

#### 3.2 PROGRAM PLANS APPROACH

The basic approach in plans development is to establish interrelationships between specific SPS program plan areas and elements of the WBS. Thirteen program plans (one divided into three sub-plans) were, therefore, identified and analyzed against elements of the SPS WBS. When combined with over 70 WBS elements, the resultant working-level matrix indicated 900 potential intercepts. At this time, however, we are concerned only with those intercepts for which long-range planning would be required or where the requirements analysis indicated major resource considerations, development or producibility concerns. areas of technology advancement, or support system sensitivity. Accordingly, Table 3.2-1 presents a summary of principal intercepts resulting from an evaluation of each plan at a working level, as compared with SPS reference solar photovoltaic design data. A total of 115 intercepts was established in three categories—A, B, and C. There are 27 Category A intercepts indicating the potential need of major resources, technology advancement, or support system requirements. Twenty-five Category B intercepts were secondary in magnitude, but important because of the long-term effort. A full description of these categories (including coverage of Category C) is presented in the following paragraphs.

- Category A—Implementation requires major resources in terms of manpower, dollars, raw materials or new facilities, etc. High-voltage test facilities for power distirbution equipment is an example. Major new system programs, critical to the overall SPS such as Shuttle-derived STS and EOTV, would also fall into this cateogry. HLLV, while not scheduled to support the prototype, needs to be time-phased to become operational by IOC to preserve program continuity. Therefore, HLLV would also be in Category A. New or greatly improved technology, requiring extensive and long-term development, would be placed in this category. One example would be high-rate production capability of thin-film GaAs solar blankets. Finally, items of special concern—but which may be of unknown magnitude—are placed in Category A. Examples would be verification of microwave beam control and utility interface considerations.
- Category B—Requires minor commitment of resources relative to Category A, but nonetheless, substantial long-term commitment may be required. An example would be verification tests of the rotary joint and slip rings.
- Category C—Certain programmatic aspects must be implemented and maintained over the long term to provide continuity and coordination. All planning areas should be maintained at some level of effort, and are so designated at the program management or SE&I levels.

Table 3.2-1. SPS Program Plans/DDT&E Relationship Matrix

SOL	SOLAR PHOTOVOLTAIC, CR-2 CONCEPT:					တ	SPS PROGRAM PLAN	96	AM	PLA	2				
CAT.	CAT. A – MAJOR RESOURCES, TECHNOLOGY ADV OR SUPPORT SYS PROGRAM REOD	-	2	က	4	2	7 9	80		9 GND 0	9 OPS	10	=	12	13
CAT. CRIT CAT.	Q ~ <u>-</u> -	MARG TNEMENT	TEGRATION	еи РИД ЕГОРМЕИТ	DESIGN &	ELOPMENT	DPACTURING TOUCE	LITIES	UND INTEG	THENANCE &	ट्यास्य	Seo es	NCH OPS	NOITADI	LYSIS
WBS NO.	WBSTITLE	NAM	NI W			DEA	IOAA				гое	SPAC	ראחו	SPEC	
	SATELLITE	А	C	A	A		ВС					А			ပ
1.1.	ENERGY CONVERSION			A	A		Λ	٧	ပ		ا د ا				ပ
1.1.2	POWER TRANSMISSION		-	A	-		8 8	83							
1.1.3	INFORMATION MANAGEMENT AND CONTROL														
1.1.4	ATTITUDE CONTROL AND STATIONKEEPING						၁								
1.1.5	COMMUNICATIONS			-	-	-				_					
1.1.6	INTERFACE		_	-	В										
1.1.7	SYSTEMS TEST	ပ		8	A	-	В		J		В				
1.1.8	359				_	J									
	SPACE CONSTRUCTION & SUPPORT	J	ر د	A	د		J					၁			
1.2.1	CONSTRUCTION FACILITIES (SCB)											၁			
1.2.2	LOGISTICS SUPPORT FACILITIES (LEO)											၁			
1.2.3	OSM SUPPORT FACILITIES											3			
			ļ	ŀ			ļ	ļ					Ì	ŀ	

Table 3.2-1. SPS Program Plans/DDT&E Relationship Matrix (Cont.)

	5	DURCE AVAIL.	ANA	၁							ပ	ပ							ں
	12	E NOITADIAIS	397 38T																3
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	4	TESTING	SAS		c	ე	c	၁			A	A					83		A
	3	ELOPMENT		В	A	A	В	4			ပ	C			В		ပ		J
	2	TEGRATION		၁	၁	ပ	C	၁			၁	J							Ĵ
	-	DARBNT TNEMENT	OR4 NAM	В	В	8	A	В			A	В							ပ
SOLAR PHOTOVOLTAIC, CR-2 CONCEPT:	CAT. A - MAJOR RESOURCES, TECHNOLOGY ADV OR SUPPORT SYS PROGRAM REOD	CAT. B — SECONDARY IN MAGNITUDE BUT CRITICAL REQUIRING LONGTERM EFFORT CAT. C — LONGTERM PROG PLANNING REQD (–) EVALUATED AT NEXT HIGHER LEVEL	WBS NO. WBS TITLE	.3 IRANSPORTATION	1.3.1 VTO-HL HLLV	1.3.2 EOTV	1.3.3 PLV	1.3.4 POTV	1.3.5 PM	1.3.6 IOTV	1.3.7 GROUND SUPPORT FACILITIES	1.4 GROUND RECEIVING STATION	1.4.1 SITE AND FACILITIES	1.4.2 RECTENNA SUPPORT STRUCTURE	1.4.3 POWER COLLECTION	1.4.4 CONTROL	1.4.5 GRID INTERFACE	1.4.6 OPERATIONS	1.5 MANAGEMENT AND INTEGRATION

The next step, as shown in Figure 3.2-1, was to prepare a summary planning sheet for each of the designated program plans. These were structured to include (1) a description of the plan; (2) a synopsis of requirements on technical and programmatic definition, associated with elements of the SPS point design description; (3) major resource considerations; and (4) a discussion section that established parameters, guidelines, assumptions, or constraints with regard to the respective plan. Areas considered critical or important to the completion of a specific WBS element were researched, identified, and studied. SPS point design requirements were constantly iterated during this period to develop line item descriptions, within identified categories, of Phase C/D DDT&E program planning concerns. The results of this work are presented on impact sheets as attached to the various plans included in a subsequent part of this section.

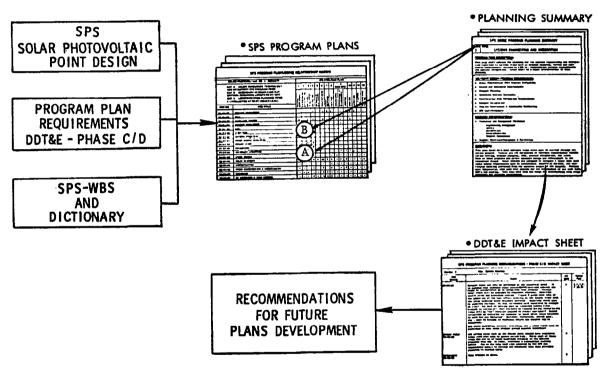


Figure 3.2-1. Program Plans Development Logic

#### 3.3 PROGRAM PLANS

The implementation of each plan entails a scope of work such that the summation of all plans will cover every facit of organization, management, and hardware/software activity necessary to carry out the Phase C/D SPS efforts. Although the implementation of certain planning activities may be delayed, it is necessary to conduct some effort in each plan area throughout all phases of the program for purposes of coordination and continuity.

Overall program planning requirements, schedules, milestones, and master network are contained in this part of the report. Program elements are described as they apply within the program plan area. Special emphasis is placed on any major or critical area that is likely to have an impact or add some degree of risk in meeting SPS program objectives, schedules, and cost constraints. Where appropriate, the data are supported with analyses or discussions to provide the applicable level of assessment based on the SPS concept definition at this time, such as that presented in Plan 13 on natural resources.

The planning data presented in this section are contained within the following program plan areas:

- Program Management—SPS schedules were developed over the program through year 2000, with emphasis on the 1980-1990 period. These schedules are developed to incorporate NASA, MSFC and DOE programmatic milestones applying to the DDT&E phases. On this basis, a series of SPS schedules showing design, development, technology advancement, production, operations, and initial phasing were developed and have been included in this plan.
- 2. Systems Engineering and Integration
- 3. Design and Development
- 4. Systems Testing
- 5. Ground Support Equipment (GSE) Design and Development
- 6. Manufacturing
- 7. Product Assurance
- 8. Facilities
- 9. Ground Operations
  - · Ground Integration
  - · Maintenance and Refurbishment
  - Logistics
- 10. Space Operations
- 11. Launch Operations
- 12. Specification Tree
- 13. Natural Resource Analysis

PLAN

TITLE

7

### PROGRAM MANAGEMENT

### PROGRAM PLAN DESCRIPTION

This plan shall include project schedules showing key milestones, test, decision points, interfaces with other program elements, hardware deliveries, facility requirements, major reviews, reporting requirements, etc.; and logic networks depicting major milestones and the interrelationship of events and activities throughout the design, development, operations, technology advancement, technology verification, and commercialization phases with the identification of critical paths. Any analyses necessary to support the defined program and schedules shall also be included. Particular emphasis shall be placed on the 1980-1990 time frame.

All major hardware and software—flight, as well as GSE—required for the development and operational phases, and identified in other sections, shall be scheduled including any hardware, equipment, and services required to be government-furnished and any long-lead hardware.

Major make-or-buy assumptions used in developing the recommended program shall be identified with supporting rationale.

### SPS GaAlas ROCKWELL REFERENCE CONFIGURATION PROGRAM REQUIREMENTS

- Solar Photovoltaic CR-2 Concept Definition
- · 30-Year Design Life with Maintenance
- Nominal 5-GW Busbar Output at End of Life
- · Satellite-DDT&E Configuration
- SPS Phase C/D DDT&E Program Coverage
- · 2000 IOC for SPS Operation
- State-of-the-Art Technology, 1987
- Technology Verification Period, 1981-1987
- · Planning in Accordance with SPS Work Breakdown Structure (November 1978)
- · SPS Schedule and Network Approach
- · Specify Key Milestones, Decision Points, Interfaces
- · Identify Make-or-Buy Approach

#### RESOURCE CONSIDERATIONS

- Technical and Management Personnel
  - Program Planning and Control
  - Engineering Management
  - Manufacturing Management
  - Contract Administration
- Support Management
- Quality Assurance Management
- Configuration Management
- Data Management
- · Support Materials, Equipment, and Facilities

PLAN

TITLE

## PROGRAM MANAGEMENT (Cont.)

#### DISCUSSION

The program management plan addresses all schedules, logic, budget planning, and decision-making functions. Its implementation produces only software. However, it is the only level at which all SPS activities are coordinated. It is also the level at which major system interfaces occur, such as between satellite/rectenna and satellite/STS. Therefore, although it represents no major impact on its own, it is essential that the plan be started early and updated continuously to reflect both current activity and future planning at this summary level.

Major systems which are coordinated through this plan are:

Satellite

- Transportation
- Space Construction and Support
- · Ground Receiving Station

One function of the plan is to assure continuity and an orderly transition from Phase C/D through IOC and into the operational phase. Often, large programs encounter peaks and valleys in funding and manpower needs. When these occur, the overall economy is normally elastic enough to accommodate such changes; but this is not the case for SPS. Due to the huge size of the SPS undertaking and the order-of-magnitude increase in resource requirements after IOC, it is essential to plan an orderly buildup as a continuous process during Phase C/D and beyond. Only in this way can a healthy economy be maintained and the solar resource be exploited without a large gap occurring between IOC and significant operational buildup. The program management plan provides the vehicle for planning this buildup and making the necessary transition. As an example, the HLLV will not be operational during the main Phase C/D. However, its development will require a major program which must be time-phased to integrate with the overall SPS in the IOC time frame as an essential element in follow-on construction and operation of multiple systems.

A summary SPS schedule is presented in Figure 1-1. It identifies ground-based exploratory research activities and key technology programs preceding the 1990 Phase C/D commercialization decision. The 335-MW EOTV precursor pilot plant is shown as an extension of the systems test activity. The 1990 C/D kick-off will activate work on all major elements leading to the SCB fabrication, EOTV test article assembly, transfer to GEO, and precursor testing/beam mapping. The growth Shuttle and Shuttle-derived cargo carrier will have an earlier start to transfer the necessary mass to orbit. Subsequent SPS VTO-HL HLLV operations will combine with the Shuttle for full-scale build of the TFU. The GRS is proceeding as an earth-based receiver of MW energy.

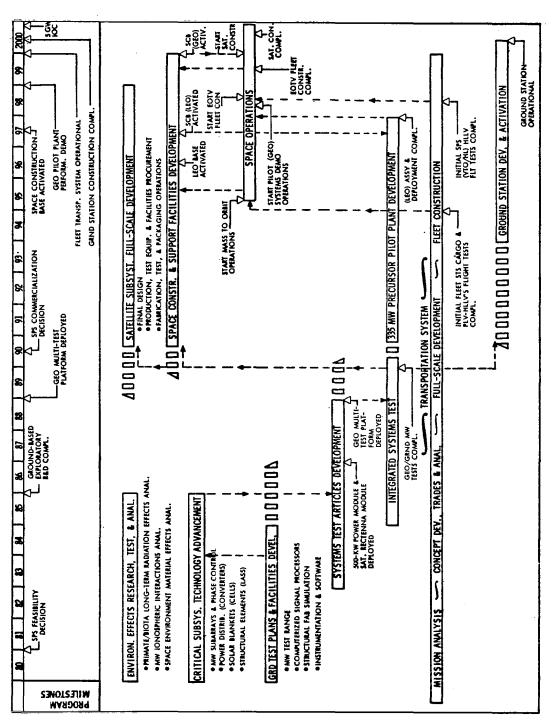


Figure 1-1. SPS Summary Schedule

PLAN |

PROGRAM MANAGEMENT (Cont.)

#### SPS Program Schedules

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The objectives, magnitude, complexity, and duration of the SPS program demand an orderly and logical approach that will provide full implementation of program projects to achieve an operational SPS consistent with the plan. Accordingly, a major requirement existed for the development of fully integrated schedules/networks at all levels of the multi-faceted WBS. To provide an overall control of the scheduling activity, control milestones were established and maintained in a logic network of integrated program activities (Figure 1-2).

The network divides the program milestones into four major sub-categories which include:

- · Technology verification and full-scale prototype development
- · Support facilities and equipment development, including transportation
- Major programmatic milestones
- · Continuation decision points

These milestones logically support succeeding events in their own subcategories and, in certain cases, will support or impact succeeding milestone events in other sub-categories.

The central catalyst for development of the satellite power system and its primary supporting equipment and facilities is the SPS decision category of milestones. Examination of the network will demonstrate that supporting equipment and facility developments encompass a scope of effort nearly equal to development of the satellite system itself; therefore, with due consideration taken for the technical lead times required for development of each major subsystem, an overall plan was established that incorporates parallel development of the several major subsystems in order that their timely completion supports major satellite system development objectives.

The decision milestone sequence was developed to program the flow of separate developmental subprograms. Timely promulgation of these decisions will undoubtedly exercise overriding impact on the program and its progress. Further, justification for each of these decision areas—for the most part—will be predicated on the achievement of specified goals within a subprogram and may be only casually related to the results of major efforts in other subprograms at that point in time. As an example, the long-lead technology required for development of an HLLV transportation system whose availability is critical to the construction and deployment of the initial satellite in the year 2000, necessitates initiation of a full-scale development program in the year 1988. This precedes a satellite systems technology readiness demonstration conducted with the "multi-test platform: test article by two full years.

### SUPPORT FACILITIES + BOUIPMENT DEVELOPMENT

SPS DECISION GATES

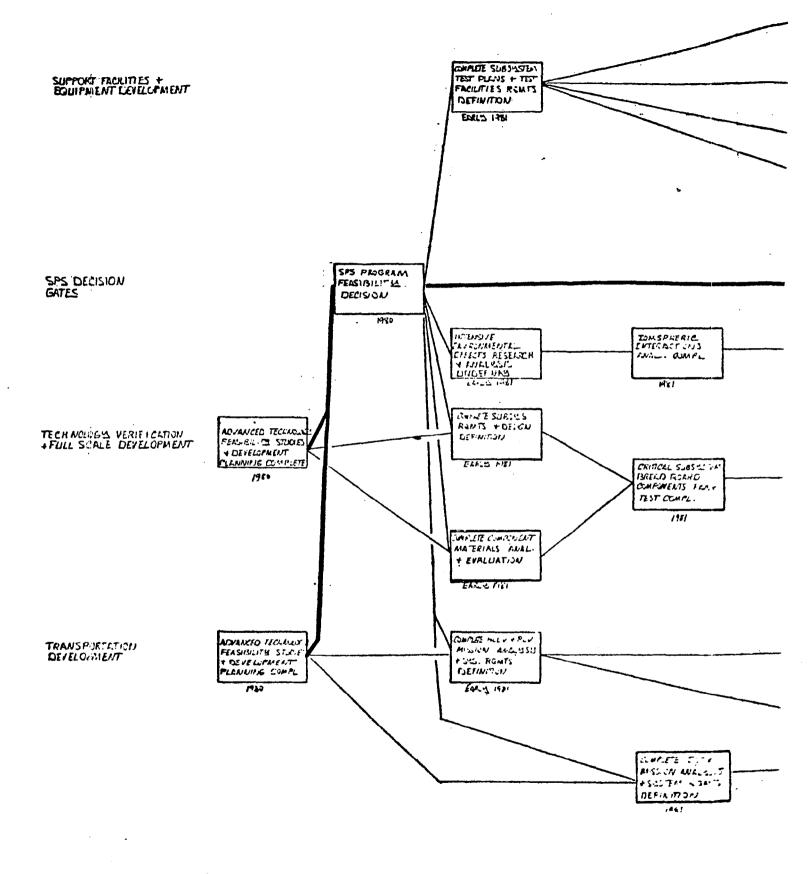
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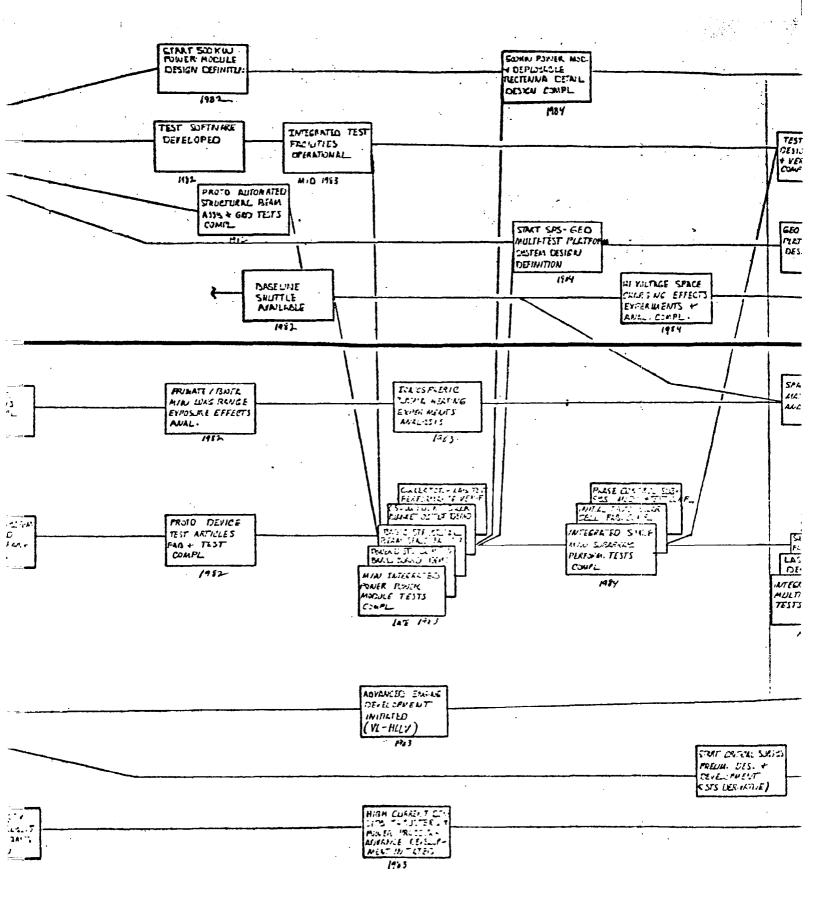
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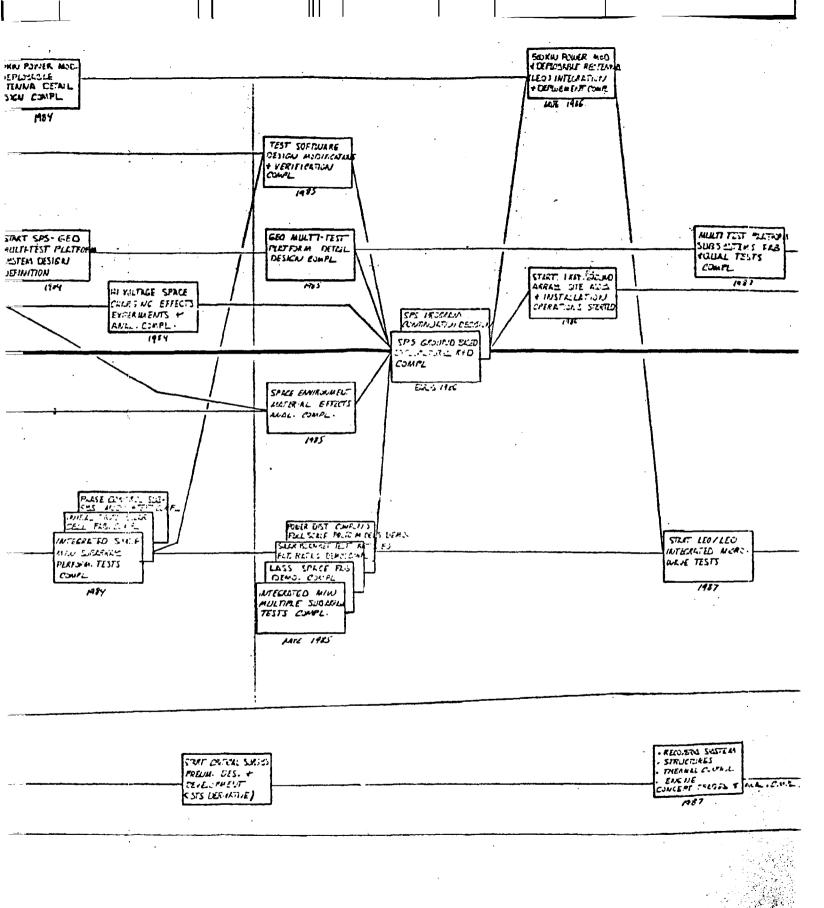
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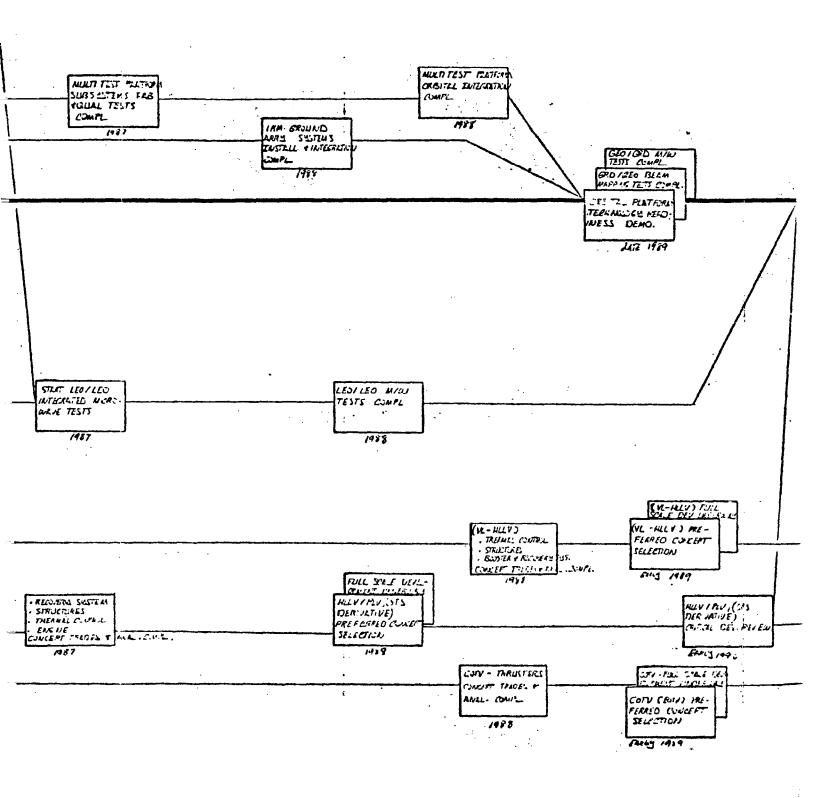
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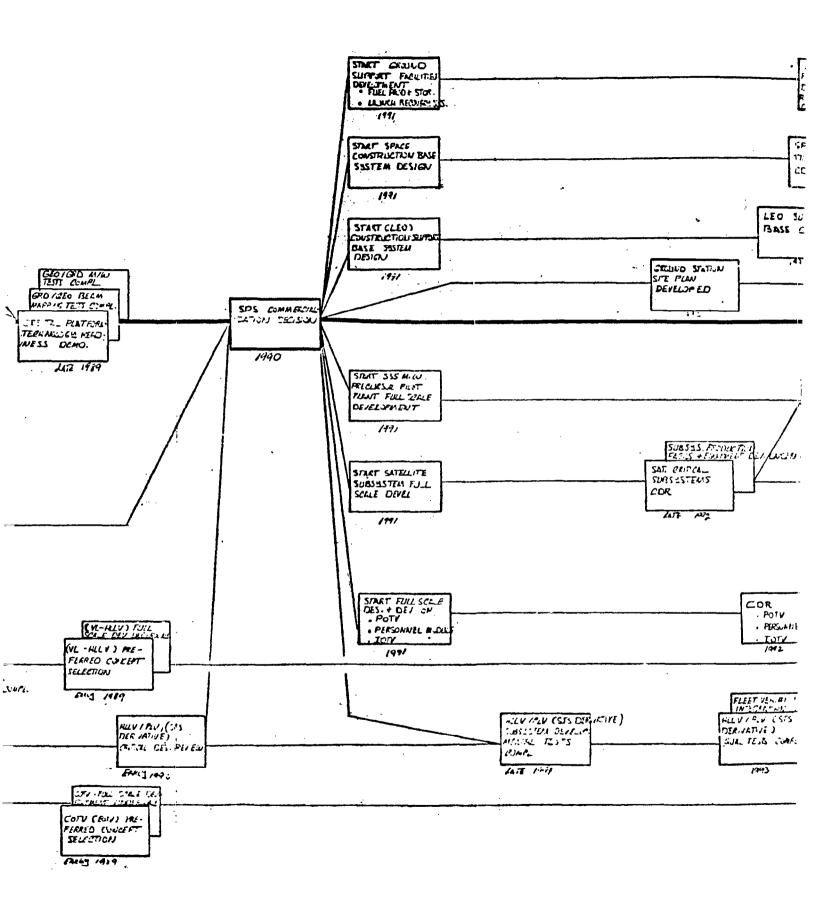


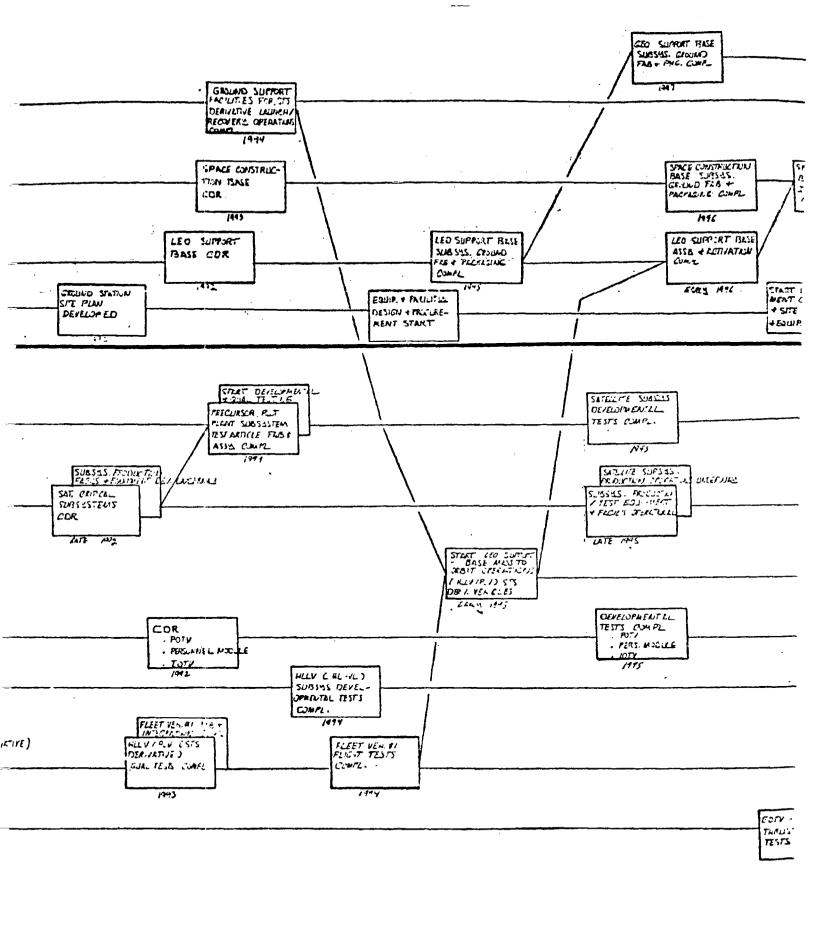
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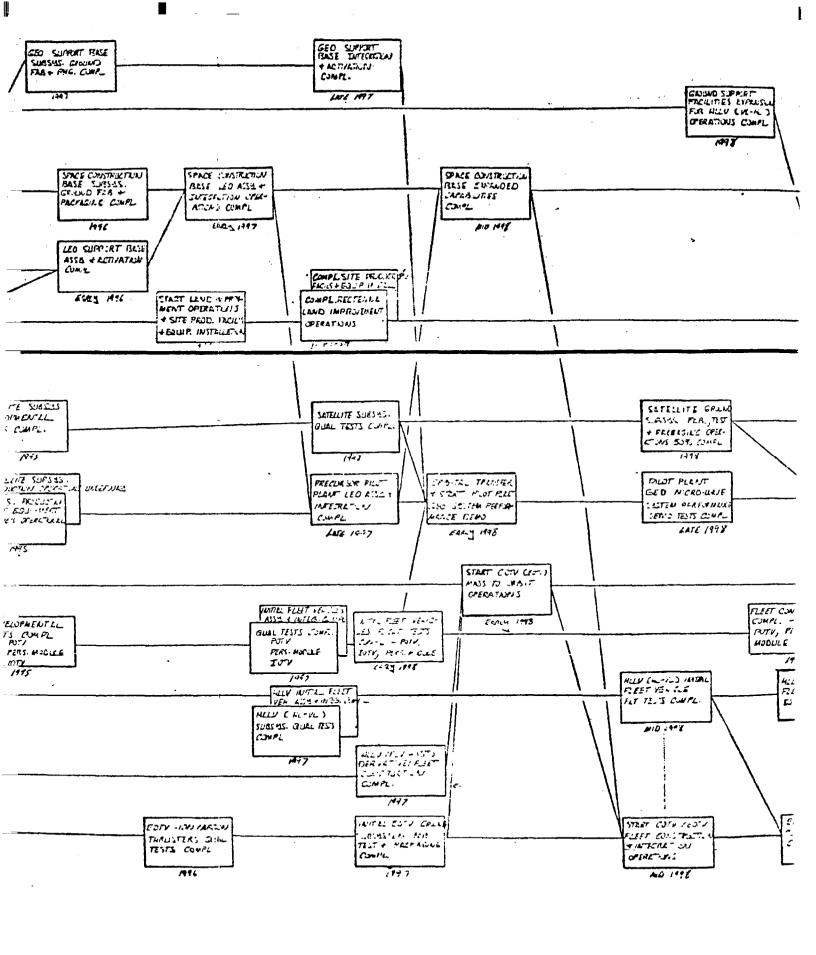


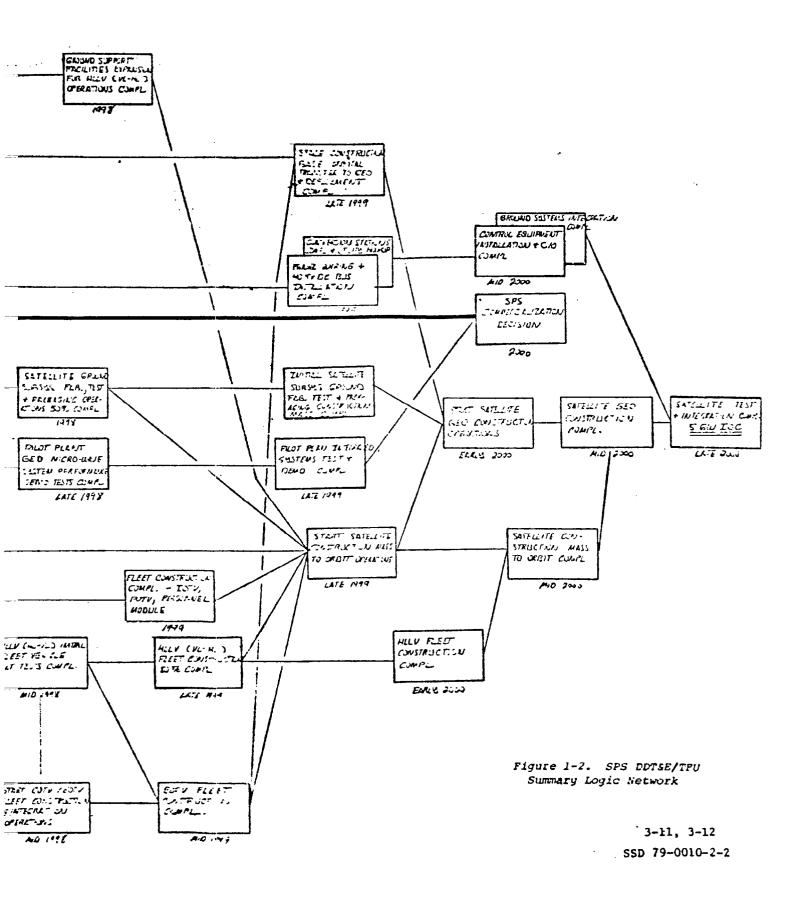












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TITLE

# PROGRAM MANAGEMENT (Cont.)

To delay a transportation development decision until a high-confidence level is achieved through the satellite systems demonstration would vitally impact the program capability to achieve IOC by the year 2000.

Other SPS program schedules have been prepared to identify (1) systems technology development tasks, as will be shown on the DDT&E Technology Advancement Program Schedule; (2) detail design, production engineering, equipment and production operations activities as will be shown on the DDT&E/TFU Full-Scale Development Schedule; (3) a "special emphasis" network on the technology development steps of a microwave transmission system; and (4) a phasing schedule on the site activation and construction sequence of the ground receiving station (GRS).

#### 1. SPS DDT&E Technology Advancement Program Schedule

The objective of this phase is to develop a system/subsystem technology base upon which a full-scale development program may systematically evolve. The schedule of Figure 1-3 addresses those key technology elements whose development is requisite to an overall SPS subsystem performance design and definition and the development of test equipment and facilities needed to support this technology effort. SPS hardware development in this phase is confined to experimental and limited prototype articles needed to prove out design concepts such as the areas covered in MPTS, power conversion, power distribution, and structures. The transportation effort during this phase is primarily directed at providing preliminary design definition to those vehicles needed for specific transportation missions further identified in subsequent program phases.

The culmination of this phase is through the integration of these subsystems into a GEO multi-test platform and application of this test article in performance of a total system technology readiness demonstration by late 1989.

#### 2. DDT&E/TFU-Full-Scale Development Program

The objective of this program phase is to produce and operate a full-scale prototype 5-GW satellite power generating system whose performance characteristics will be the basis of justification for continued satellite power systems commercial development. Therefore, the schedule of Figure 1-4 addresses only those tasks and program elements which directly impact development of prototype operational power system hardware/software plus development of equipment and facilities which directly support tasks aimed at this objective.

Included in this schedule are broad-based iterations of (1) designs and definitions of subsystem production hardware (based upon data, specifications, and experimental hardware developed during the technology verification program phase); (2) manufacturing technology, equipment, and facilities that need

SPS DDT+E PROGRAM SCHEDULE (TECHNOLOGY ADVANCEMENT PHASE)

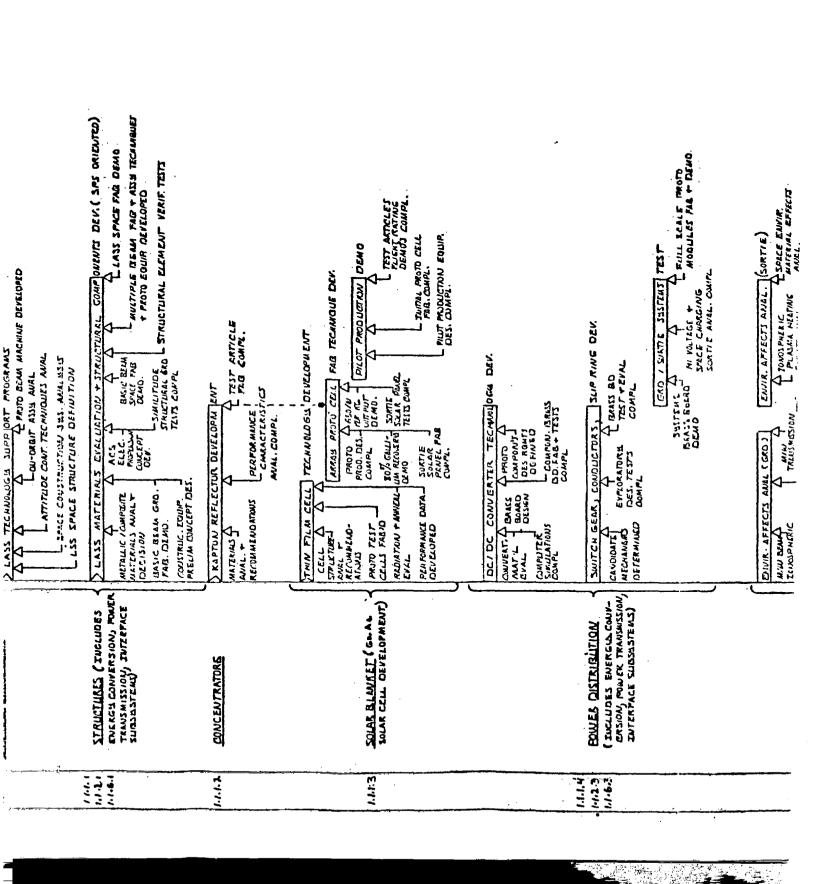
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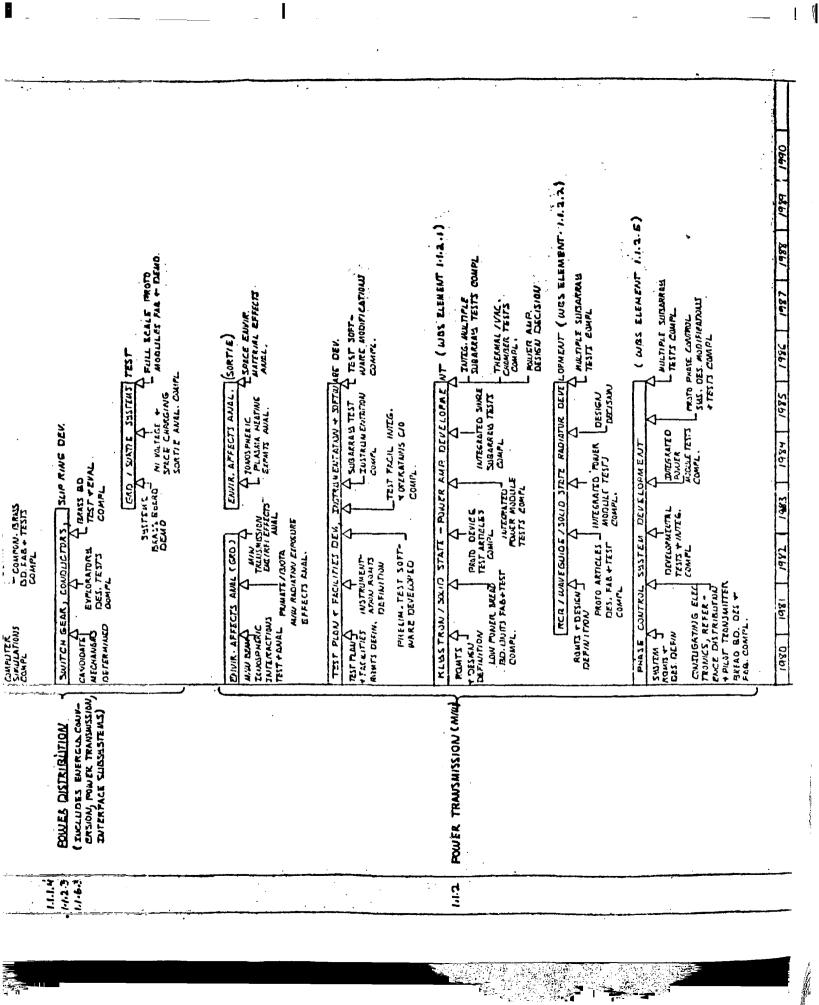
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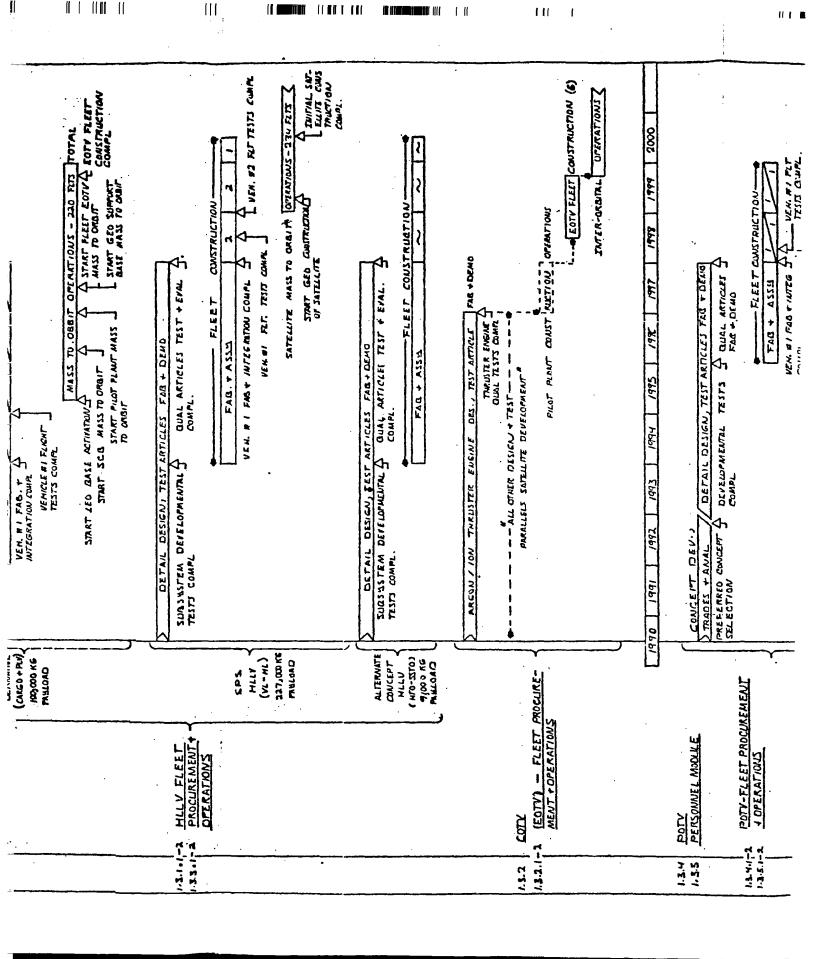
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Figure 1-4. SPS Program Schedule (DDT&E/TFU Development Phase)

PLAN | TITLE

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### PROGRAM MANAGEMENT (Cont.)

development; and (3) the prototype production operations and sequences. Emphasis in this schedule is also placed upon ground/space power system assembly and integration operations and the major equipment and facility development programs required to support these operations. The transportation schedule section is confined to those vehicles needing development for mission use during this particular program phase. It describes the phasing of (1) STS growth/derivative HLLV's which will be used to transport the mass to orbit, facilities, equipment, and personnel to LEO in support of the satellite construction base and its activation; (2) SPS-dedicated HLLV's (VTO-HL) to transport the main satellite construction mass to LEO; (3) the COTV (EOTV) which will be used for large interoribtal cargo mass transfer; and (4) the personnel and high-priority cargo-carrying space vehicles (IOTV, POTV. and PM). The ground station system/subsystem design, development, and construction scenario has been addressed as it will support the overall program. WBS numbers and titles are referenced in the margin, and have been used to provide the basic structure and layout for this schedule.

### 3. Special-Emphasis Network—Microwave Technology

Current technology exploration studies indicate that microwave technology advancement will be a single most-significant pacer in total program development. In order to illustrate the need for early resource allocation directed toward near-term technology exploration and test verification of the concepts now under consideration, a time-oriented logic network was developed as shown in Figure 1-5. It traces the full microwave scope of this effort and highlights program continuation decision gates at critical junctures.

Phase I (1980 through 1985) describes the tasks (including their timing and interrelationships) needed to define requirements, develop concepts, perform trades, conduct analysis on alternate designs, perform tests and evaluations on these alternative concepts and, finally, make a concept selection which will be the baseline for full-scale development.

The network also describes parallel development programs on ground test facilities, equipment, instrumentation, and software needed to support the engineering development process.

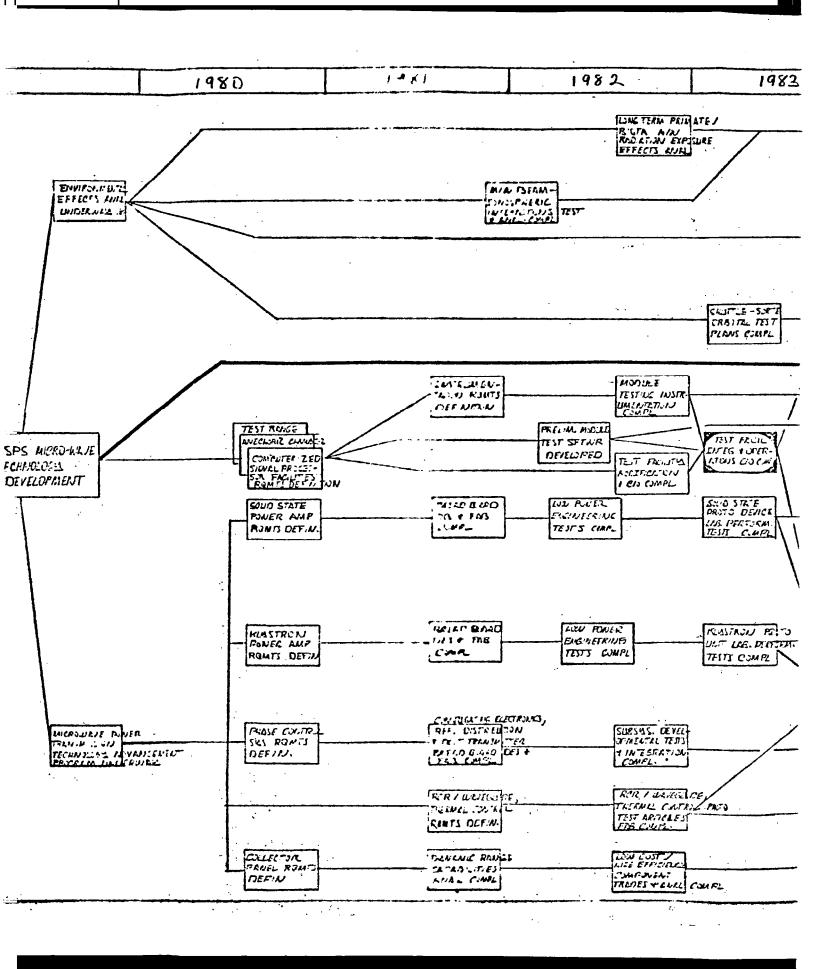
Phase II (1986 through 1989) describes the development of equipment and testarticles needed to provide performance verification of the complete microwave system alone, and the microwave system integrated with key elements of the multi-test platform program for a complete earth/ground-based technology demonstration scheduled for late 1989.

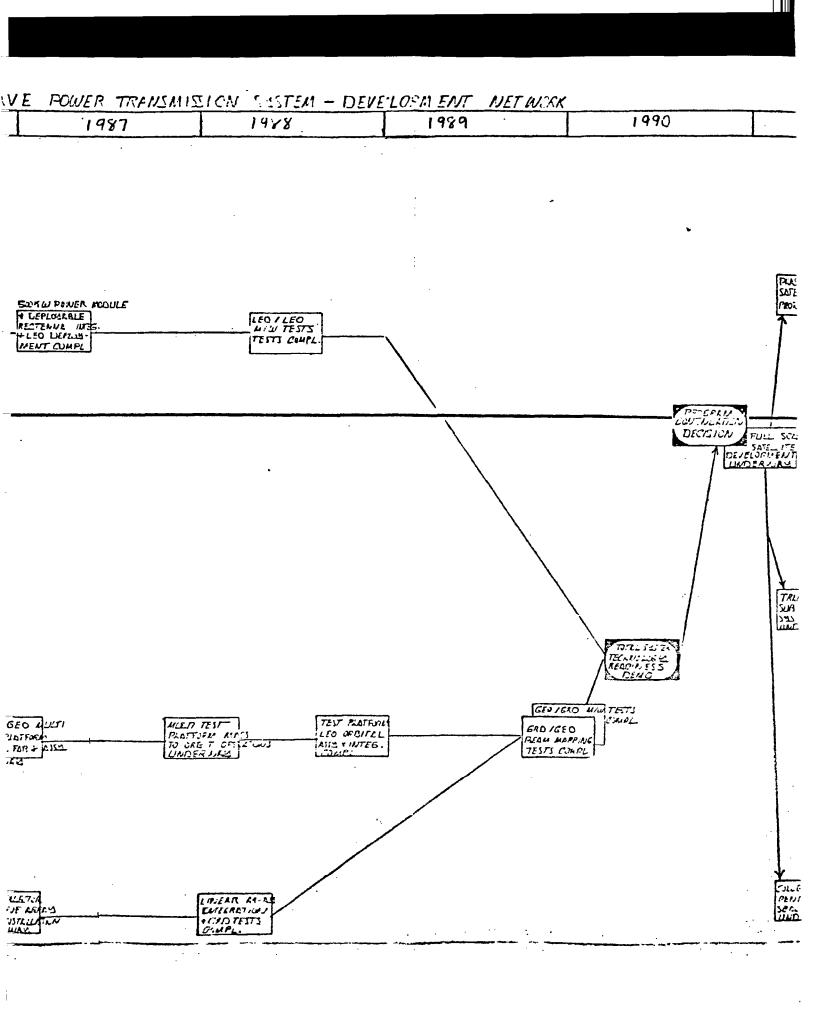
Phase III (1990 through 2000) describes the full-scale development of the subsystem along with the parallel development of all other satellite subsystems. The program culminates with a performance demonstration of multiple subarrays as integrated with other systems in the precursor pilot plant and, finally,

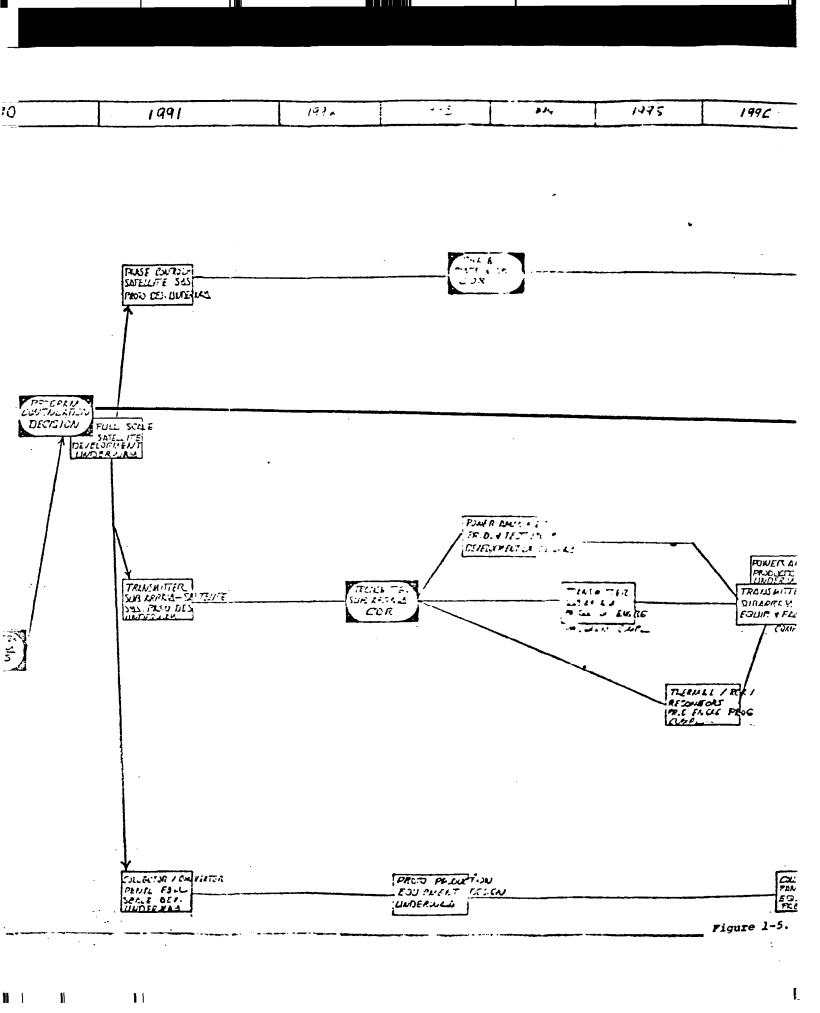
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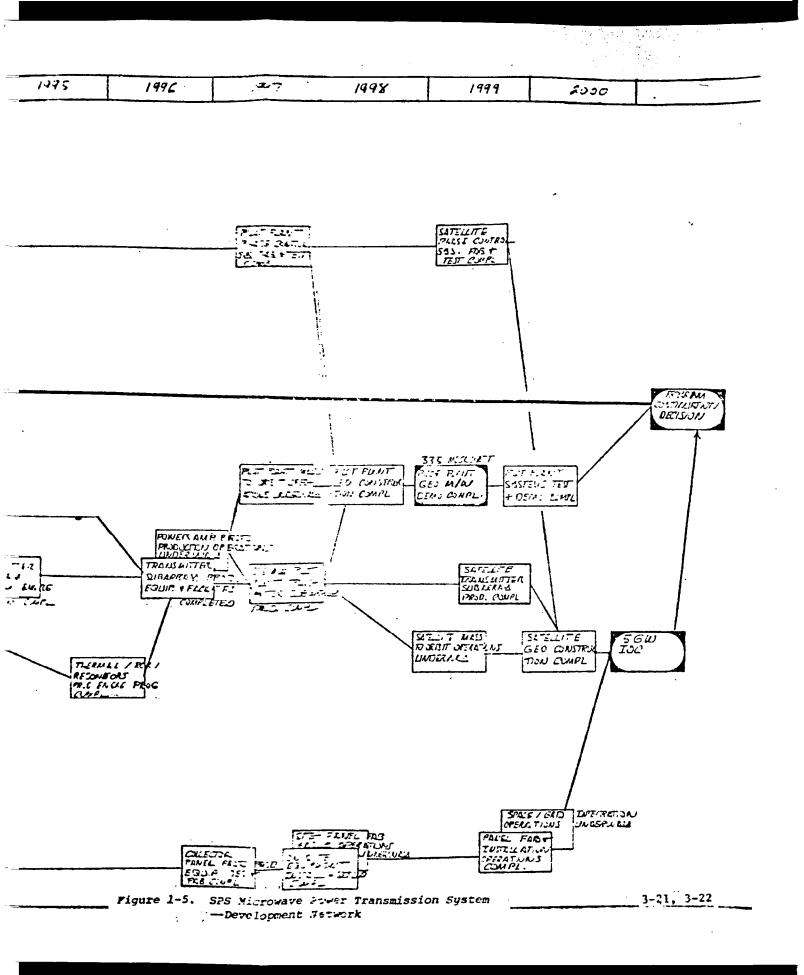
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PLAN TITLE

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## PROGRAM MANAGEMENT (Cont.)

in the all-up systems test of the 5-GW initial satellite. To reiterate, the results of earlier ground-based microwave technology development and performance verification activities will be a most significant factor in evaluating the feasibility of continued total system development.

#### 4. GRS Site Activation Schedule

A series of detail phasing schedules were developed on the activation of each of the first four ground station receiving sites (Figure 1-6). Operational sequences were identified for site survey, ground preparation, panel fabrication, concrete placement, facilities installation, and checkout activities. Contacts with A&E, equipment manufacturing, concrete, and construction firms provided additional information on the duration and sequence of operations from their experience on programs of this size. Figure 1-7 is an integrated summary schedule of major events in constructing the ground receiving station and emphasizes the utilization of construction equipment and its transfer from site to site as required to maintain the build-rate of two rectennas per year. It was concluded that the equipment from Site 1 would be available for use on Site 3. This information on equipment utilization, site sequencing, and equipment lifetimes was used to establish total resource requirements and cost estimates for the program.

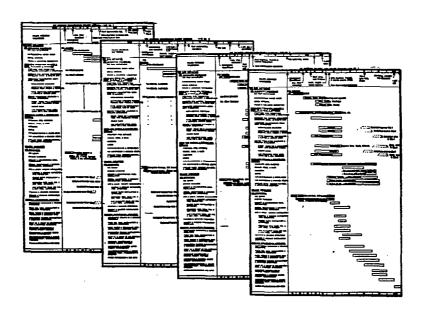


Figure 1-6. GRS Phasing Schedules

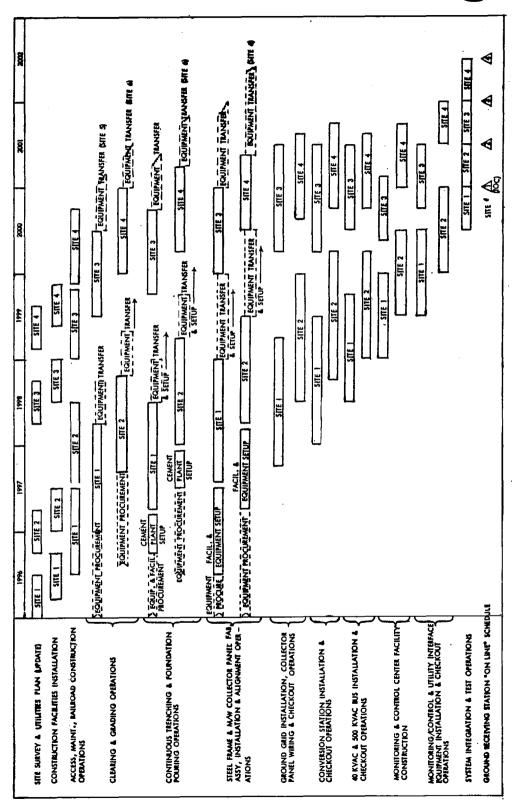


Figure 1-7. SPS Rectenna Construction Sequence Summary Schedule Flow

2

PLAN | TITLE

# SYSTEM ENGINEERING AND INTEGRATION

### PROGRAM PLAN DESCRIPTION

This plan shall address the planning for the systems engineering and integration functions to include items such as mission planning, system and subsystem requirements, interfaces (ICD's), verification testing requirements, and payload integration. Costs shall be a major consideration in this planning.

#### SPS POINT DESIGN PROGRAM REQUIREMENTS

- Solar Photovoltaic CR-2 Concept Definition
- · System and Subsystem Requirements
- · Mission Planning
- · Interface Control Documents
- · Verification Test Definition Requirements
- Payload Integration
- Systems Development and Operations Monitoring
- SPS Cost/Economics

### RESOURCE CONSIDERATIONS

- · Technical and Management Personnel
  - Engineering Management
  - Safety
  - Reliability
  - Maintainability
  - Support Management
- · Support Materials/Equipment and Facilities

#### DISCUSSION

This plan deals with many software items which must be carried through the entire program. Typical are the definition of hardware requirements verification testing, mission planning, ICD's, payload integration, and costs. Each of these elements may affect hardware design and development in the conceptual stages. Major systems are assigned to Category C under this plan since system requirements must be established, interfaces defined, and continuous updating performed from the earliest stages of the program. Perhaps most importantly, this plan will provide for the development of all cost data, CER's, and costing. These data will form the basis for establishing long-range budgeting for economic projections.

PLAN TITLE

3

# DESIGN AND DEVELOPMENT

#### PROGRAM PLAN DESCRIPTION

This plan shall address the design and development of the system and subsystems, including design engineering, development and qualification testing. The hardware and software to carry out these activities shall be identified. The technology and/or development status of each subsystem shall be discussed in sufficient detail to allow for a management assessment of program development risks.

### SPS POINT DESIGN PROGRAM REQUIREMENTS

- Solar Photovoltaic CR-2 Concept Definition
- System and Subsystem Drawing/Specification Requirements
- · Supporting Software and Hardware Requirements
- Development Program Definitions and Design Requirements
  - Structural elements—joining and stiffening
  - Beam machine development
  - Solar blanket design efficiency and reliability
  - Microwave reliability and efficiency requirements
  - Rectenna design optimization
  - Utility interface design requirements
- · Qualification Test Procedures and Requirements
- Design Interfaces of Systems/Subsystems

### RESOURCE CONSIDERATIONS

- · Technical and Management Personnel
  - Design, development, and qualification testing manpower
- · Supporting Hardware and Software
- · Support Materials/Equipment and Facilities

#### DISCUSSION

This plan provides for all design and, as such, produces drawings, specifications, and other software. It is a major engineering effort and therefore will have significant impact in terms of manpower requirements. However, there is reason to believe that these resources can be made available from existing technical labor markets, such as the aerospace industry, as needed. The same can be said for technology needs in terms of analytical tools, computer software, etc. Two areas are of present concern. First of all, the status of technology and development related to key subsystems and components must be determined and extrapolated to the time frame where needed for the SPS prototype. (Examples are klystrons and GaAs solar cells.) This will permit a risk assessment to be made and justify the allocation of resources to most critical developmental areas. For example, stockpiling of solar cells for the SPS prototype will require a production rate of about 500 MW per year

PLAN 3 TITLE

### DESIGN AND DEVELOPMENT (Cont.)

starting in the late 1980's. Risk assessments under this plan would be a basis for implementing major developmental effort on GaAs to provide thin-film, high-efficiency cells.

Secondly, developmental programs must be identified, planned, and carried out to assure that proof-of-concept will actually take place as scheduled. This effort assumes that the resolution of key issues or research activities will have been completed under technology development projects. It may, however, include development of equipment such as beam machines, development of large-scale, in-space life support and operational capability, and development of critical components or modules such as prototype solar blankets. Several critical long-range areas of concern are identified in Table 3-1.



Table 3-1. SPS DDT&E Program Planning Considerations (Phase C/D) Impact Sheet

of 2	CAT- EGORY	¥	æ		æ	<b>A</b>
TITLE: DESIGN AND DEVELOPMENT	IMPACT	Satellite design and supporting development will be a major undertaking due to size and complexity well beyond anything previously attempted in space.	The methods of designing the satellite construction base (SCB) and EOTV test article structure will evolve as smaller structural platforms for demonstration projects as designed and developed during earlier phases. The design	approach must be closely coordinated with the development of in-space processes and manufacturing equipment throughout the program. This will assure that the design of the structural elements, their joining and stiffening will be compatible with the most effective approach to manufacturing. Design and development of beam machines and fixtures specific to the SCB and EOTV are included under WBS 1.2. Capability for producing large structures in space must be developed.	Special consideration must be given to design and development to provide high reliability of the slip rings and brushes. Parts replacement must be considered.	Design and development of solar blankets must address the integrated power source at this level although most hardware-related effort will be at a lower level. Energy conversion is among the most critical subsystems requiring extensive development and long lead times. The design and development of the solar blanket will be, perhaps, the most critical item in the SPS. Considerable development will be required, extending over a long period before a suitable design evolves which combines the essential features of lightweight, high efficiency, high reliability, high proton damage resistance, satisfactory handling, and high production and low cost.
PLAN NO. 3	WBS ELEMENT	1.1 Satellite System	1.1.1.1, 1.1.2.1, 1.1.6.1 Structure		1.1.1.4, 1.1.6.2, 1.1.6.3 Rotary Joint, Mechanisms	1.1.1 Energy Conversion



Table 3-1. SPS DDT&E Program Planning Considerations (Phase  ${\it C/D}$ ) Impact Sheet

of 2	CAT- EGORY	А	ф	<b>4</b>	μ	ပ	A
TITLE: DESIGN AND DEVELOPMENT	1 1	Design and development of regulators, switch gear, circuit breakers, klystrons, beam control, etc., cathode structure will be extensive to assure high efficiency and reliability. Considerable investigations of alternate PDC subsystem and component approaches are foreseen.	Comprehensive overall effort involving two or more systems tests including hardware and operations plus design of all STE and facilities not included elsewhere. A major planning effort is required for development and qualification testing.	Design and development of SCB, LEO base, satellite O&M base, and support equipment is a major task involving such items as assembly fixtures, beam machines, teleoperators, etc. This is one of the most critical areas of development. ICD's must be considered throughout design and development. Concerns include life support, logistics, docking, flight control, personnel/cargo transfer, etc.	Major parallel programs on HLLV, EOTV, PLV, POTV, PM, and IOTV. Therefore, ICD's must be considered throughout design. Engine development and vehicle design critical for multimission use.	Because of large overall size and number of elements, must emphasize minimum use of materials; high reliability and low maintenance must be emphasized in overall design. Power collector design must permit mass production at mini-	mum cost with on-site fabrication of dipole panels. Converter stations require long-term planning and reliability in design. As the ultimate user, the utilities will have requirements for regulation and reliability. The value of SPS-generated power to the utility must be addressed by taking margin requirements, load factor, etc., into account. Power value and requirements can be expected to vary for each grid network with which an interface
PLAN NO. 3	WBS ELEMENT	1.1.2, 1.1.2.2 Power Transmis- sion/Subarrays	1.1.7 Systems Test	1.2 Space Construction and Support	1.3 Transportation	1.4 Ground Receiving Station, Dipole/ Rectifier Ele-	ments, Power Distribution and Conditioning, Utility Interface



PLAN 1 TITLE

### SYSTEMS TESTING

#### PROGRAM PLAN DEFINITION

This section shall address the approach to systems verification testing with supporting rationale. Also, the system test hardware and any unusual or unique facilities required to carry out the program shall be identified.

#### SPS POINT DESIGN PROGRAM REQUIREMENTS

- Solar Photovoltaic CR-2 Concept Definition
  - Solar blankets-27 x 10<sup>6</sup> m<sup>2</sup> per satellite
  - Power distribution and control
  - Rotary joint
  - Microwave power
  - Rectenna
  - Space transportation
- · System and Subsystem Verification Test Requirements
- System Test Hardware/Software Definition
- Unique Test Facilities—Ground and Space

### RESOURCE CONSIDERATIONS

- · Technical and Management Personnel
- Operational/Support Personnel
- Supporting Hardware and Software
- Support Materials/Equipment and Facilities
- Special/Unique Test Equipment

#### DISCUSSION

The overall testing hierarchy for Phase C/D consists of:

- Development
- Verification
- Production
- · Operations
- Qualification

This plan addresses system verification and includes any tests which involve two or more subsystems and are for the purpose of verifying that the systems will perform to specifications. Verification tests may be performed on either end-item prototype hardware or on hardware specifically designated for verification purposes. For example, the first flight tests of the EOTV will be in orbit and presumably will be of short duration to verify performance prior to actual use of the vehicle for interorbital transfer. The EOTV in this case is a deliverable operational end item. On the other hand, verification tests of beam accuracy, control, and safety interlocks may be conducted during final phases of the GEOSAT, as shown in Figure 4-1. These tests are critical to SPS acceptance and will be conducted on an interim test platform.

SPS DDT&E PROGRAM PLANNING SUMMARY
PLAN TITLE  SYSTEMS TESTING (Cont.)
GOAL CR2 SOLAR ARRAY DEVELOPMENT  SILICON CR1 SEPS BUS  GEOSAT  INVERTED TEST RANGE  LARGE POWER MODULE  SP5 ORBITAL TEST ARTICLE

Figure 4-1. SPS Multi-Test Platform Evolution

It remains to be resolved at what levels of assembly actual systems tests will take place and what scope these tests will assume. However, Table 4-1 identifies several areas of concern for reference at this point in time as they apply to main elements of the SPS program.

Table 4-1. SPS DDT&E Program Planning Considerations (Phase C/D) Impact Sheet

,	CAT- EGORY	∢	м	<b>A</b>	∢
TITLE: SYSTEMS TESTING	IMPACT	Certain tests can only be performed at the satellite level. It is assumed that combined power source/MMPTS/attitude control, etc., would be accomplished as an integrated test program. Systems-level tests will be preceded by component checkout, interface verification, and subsystem testing. Questions which must be answered include: In what increments will a satellite be brought on line? How much of the antenna must be installed before first blanket is activated? Must blankets be covered during installation? (They will be "hot" whenever exposed to direct sunlight.) Should reflectors be installed? Rectenna converters, switch gear, etc., must be brought to readiness before any blanket can be connected. In addition, are there stability, control, switching, etc., tests which must be performed at this level without ground station interface?	All moving parts such as the rotary joint should have extensive long-term test data to assure reliability. While each of these items may not be of major magnitude relative to the systems programs they may, in total, represent a substantial testing effort. Due to the long lead time involved on the SPS, the opportunity exists to develop the necessary test data provided planning is started early.	Similar questions arise. What is the testing concept and sequence? For test purposes, will the smallest unit be a single blanket (say, 750x25 m)? How will power source modules include switch gear, regulators, etc., for testing purposes?	The SPS will require approximately $27\times10^6$ m <sup>2</sup> of solar blankets starting in 1996 for delivery and installation through 2000. Buildup will require average production of $675\times10^6$ m <sup>2</sup> /year for four years starting in 1996. Testing will require ten or more "blimp hangar" size test stands capable of testing blankets on a three-shift basis. Testing of each solar blanket would be done
PLAN NO. 4	WBS ELEMENT	1.1 Satellite System, Rotary Joint, Mechanisms		1.1.1 Energy Conversion	1.1.1.3 Solar Blankets



Table 4-1. SPS DDT&E Program Planning Considerations (Phase C/D) Impact Sheet

,	CAT- EGORY		<b>∀</b>	æ	<b>V</b>	₩	<b>A</b>	æ
TITLE: SYSTEMS TESTING	IMPACT	on test stands adjacent to the factory. These stands would each have solar spectrum simulation capability. Test stands will be located at factory sites.	High-rate, high-voltage (45 kV) testing of equipment will be involved. Question: What special problems and requirements are involved in high-voltage testing of regulators and switch gear and dc/dc converters?	Verification tests must satisfy beam control and interlock capability relative to safety concerns. High-rate, high-voltage testing at component level for klystrons, driver amplifiers, etc. High-rate, high-voltage testing of conduction network at subsystem level and at component level of switch gear, conditioning electronics.	Comprehensive test requirements needed. Includes all ground systems tests involving two or more subsystems for purposes of qualification and development. Does not include individual component tests such as solar blankets, klystrons, etc. Does not include flight hardware.	Large facilities will be required for systems tests, particularly those in conjunction with energy conversion and STS.	Tests must verify 580,500 dipole subarrays plus distribution and conditioning system. Coordination of rectenna construction and operation with the satellite power source and/or MPTS must assure the phased buildup of an integrated power system. What systems level tests must be conducted?	Utility must be prepared to accept interim and incremental power as part of systems testing.
PLAN NO. 4	WBS ELEMENT		1.1.1.4 Power Distribution and Conditioning	1.1.2 Power Transmission, RF Generation & Beam Control, Power Distribu-	1.1.7 Systems Test & Operations	1.3.7 Facilities	1.4 Ground Receiving Station	1.4.5 Utility Interface

 ${\it rable 4-1.} \\ {\it SPS DDT\&E Program Planning Considerations (Phase C/D) Impact Sheet}$ 

	CAT- EGORY	₽
TITLE: SYSTEMS TESTING	IMPACT	This level brings together major systems and requirements, a substantial longtern commitment for systems testing. The satellite/rectenna, for example, will undergo combined testing at various times during phased buildup of the prototype which will take place over a period of years. STS, OTV, and control interfaces must be tested and verified at this level.
PLAN NO. 4	WBS ELEMENT	1,5 Program Management

PLAN 5 TITLE

# GROUND SUPPORT EQUIPMENT (GSE) DESIGN AND DEVELOPMENT

#### PROGRAM PLAN DEFINITIONS

This plan shall address the design and development of the GSE and its associated software required for checkout of the systems and subsystems at the warious locations, i.e., factory, launch site, etc. The hardware required in the design and development of the GSE shall be identified.

#### SPS POINT DESIGN PROGRAM REQUIREMENTS

- Solar Photovoltaic CR-2 Concept Definition
- · GSE Design/Drawing and Specification Requirements
- · Supporting Software and Hardware Checkout Requirements

### RESOURCE CONSIDERATIONS

- Technical and Management Personnel
- Supporting Hardware and Software
- · Support Materials/Equipment and Facilities

### DISCUSSION

In total, GSE requirements will be substantial, particularly in support of launch and transport vehicles. Individual support equipment for satellite/rectenna systems, however, should not require major expenditure of resources percentagewise. Long-range planning should be a natural fallout of the design process which must consider those items that are larger in size or quantity, such as the solar blankets or rectenna dipole panels, methods of transporting, servicing, and handling (Table 5-1).



Table 5-1. SPS DDT&E Program Planning Considerations (Phase C/D) Impact Sheet

of 1	CAT- EGORY	C	၁	ပ	Ů		
Sheet 1. TITLE: GSE DESIGN AND DEVELOPMENT	IMPACT	Equipment to handle, transport, deploy, and service solar blankets after manufacture may be critical due to large size and fragile nature of blankets.	Major system program/major support equipment	Heavy investment required for solar blanket and high-voltage testing.	Checkout, maintenance, repair, and replacement of large number of dipole panels in place may require special support equipment exclusive of test gear.	Note. Although GSE will represent a substantial investment, neither the resource allocation and planning nor technology appear to be of sufficient criticality for consideration at this time.	
PLAN NO. 5	WBS ELEMENT	1.1.1.3 Solar Blankets	1.3 Transportation	1.3.7 Facilities	1.4 Ground Receiving Station		

PLAN | TITLE

6

MANUFACTURING PLAN

### PROGRAM PLAN DESCRIPTION

This plan shall address the manufacturing requirements for all the development and deliverable hardware (flight systems and GSE) required in the program. Included shall be a compilation of all the hardware and software requirements from other sections. The major make-or-buy assumptions identified in the section on program management shall be used as a basis for developing the manufacturing requirements. Particular emphasis shall be placed on any unusual or unique facilities, tooling, and STE required to support the manufacturing activities and any advancements in the manufacturing processes and related technology that could impact the program. Quality control requirements shall also be assessed.

### SPS POINT DESIGN PROGRAM REQUIREMENTS

- Solar Photovoltaic CR-2 Concept Definition
  - Structure
  - Solar blankets,  $27 \times 10^6$  m<sup>2</sup> per satellite
  - Power distribution and conditioning
  - Microwave power
  - Rectenna
- Flight and Ground System Manufacturing Requirements and Producibility Rates
- · Unique Manufacturing Facilities—Ground and Space
- · Special Test Equipment and Support Tooling
- · Quality Control Support Requirements

#### RESOURCE CONSIDERATIONS

- Technical and management personnel
- · Operational/support personnel
- · Supporting hardware and software
- Support materials/equipment and facilities
- · Special/unique test equipment

### DISCUSSION

This plan covers all deliverable hardware. As such it includes ground systems, flight systems, and GSE. Make-or-buy assumptions of the program management plan will be used to develop detailed manufacturing plans which relate to a particular supplier of specific hardware. Such plans obviously are strongly dependent on having a firm design concept established. Unique facilities, tooling, and STE required to support manufacturing activities must be identified. High-voltage test equipment, for example, must be developed for use in manufacturing the multitude of items, indicated in Figure 6-1, at the component level (such as switch gear, regulator, and circuit breakers). Quality control requirements and procedures must be identified and developed. Again, these are strongly dependent on the design concept.

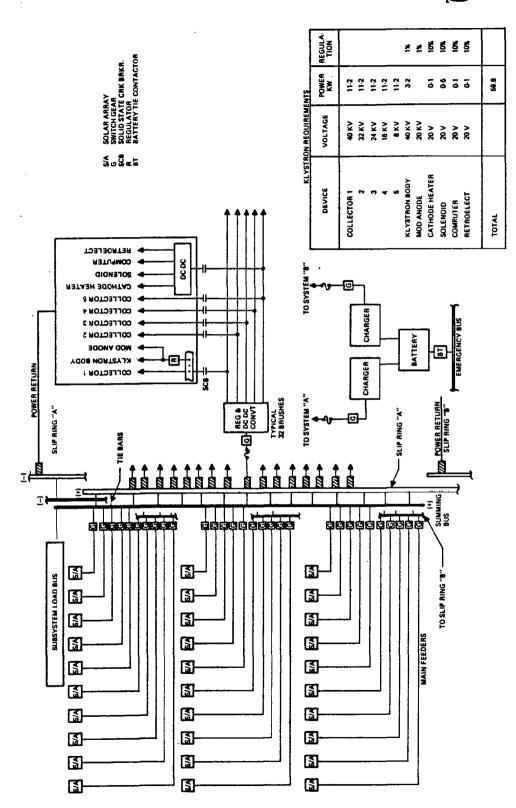


Figure 6-1. SPS Power Distribution

PLAN | TITLE

6

# MANUFACTURING PLAN (Cont.)

Development of high-production, thin-film GaAs technology is probably the most critical item and will require a long-term, well-funded program. An equivalent amount of GaAs production will be required in the same time frame to support buildup of a prototype stockpile and continuation in support of the operational SPS fabrication.

Large investments will also be required to manufacture power distribution, conditioning, and transmission components. Examples are switch gears, converters, and klystrons. (Assembly of the satellite as a power station would be covered under Plan 10, Space Operations.) Such items as beam machine complexes, templates, etc., must be developed specific to the prototype. These may differ considerably from those necessary to support construction of the Nth satellite due to the longer period permitted for staged fabrication of the former. A multitude of special assembly, fabrication, inspection, and test techniques must be developed which pertain to manufacturing in orbit. Some items may be partially fabricated and assembled under this plan with completion under Plan 10 (Space Operations). "Waveguides" is an example. These may be built as full box sections or in half-sections to save volume. latter would then be transported to the satellite and assembled. Manufacturing and product assurance techniques must be such that waveguides can be placed into operation with "zero" defects since internal arcing due to burrs or whiskers would result in early failure of the guide.

An assumed buildup for one of the most critical items (solar blankets) is presented in Figure 6-2 in order to provide some perspective for the scope of the required manufacturing effort. It should be noted that production will peak at 1145 m per hour in 1997, and will need to increase in subsequent years to support the mature commercial program. Table 6-1 broadly addresses some of the manufacturing facilities development tasks needed to support subsystem production for planned prototype and commercial space operations.

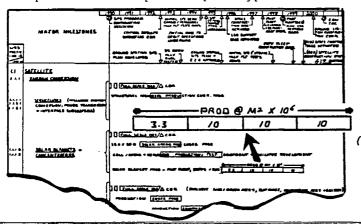


Figure 6-2.
SPS Program Schedule
(DDT&E/TFU Development
Phase)

Table 6-1. SPS DDT&E Program Planning Considerations (Phase  $\mathcal{C}/\mathcal{D}$ ) Impact Sheet

3 🖫	quired. A to sup-1996 meeting	e compondomplexity of nof numbers lus , and	made to B
IMPACT Once noint design is firm an overall satellite manufacturing plan mu	Once point design is firm, an overall satellite manufacturing plan must be provided in detail.  For the prototype SPS alone, a $27\times10^6$ m² area of solar blankets is required. Starting in 1996 it is suggested that a production rate be developed to support test, TFU, and follow-on production. Average production during 1996 would be 3.3×10 <sup>6</sup> m² per year. The development of GaAs solar blankets meeting production, reliability, efficiency, and weight goals will be a major SPS technical challenge.	Problems relate to the large quantity of high-voltage, highly reliable components which must be produced. Figure 6-1 provided some idea of the complexity of the power distribution subsystem. High-rate, automatic production of 1-mil aluminum wire junctions with zero defects is required. Large numbers of regulators, switch gears, and dc/dc converters will be involved, plus system complexity with IMS control for array regulation, load control, and associated interfaces.	Comments similar to the above apply to the MWPTS. If a decision were made to
SS ELEMENT	1.1 Satellite System 1.1.1.3 Solar Blankets	1.1.1.4 Power Distribution and Conditioning	1.1.2.2 Microwave

Table 6-1. SPS DDT&E Program Planning Considerations (Phase C/D) Impact Sheet

CAT- EGORY	В	ပ	ິນ	<b>4</b>	ပ	4
TITLE: MANUFACTURING IMPACT	Test articles for all components and subsystems will be built for qualification testing. This does not include flight or operational hardware.	Includes <u>all</u> special support equipment (teleoperators, beam machines, etc.) to assemble, check out and maintain the satellite system.	Each transportation element requires a separate manufacturing plan as part of the individual program effort.	Manufacturing requirements for solar blankets, power conditioning and distribution components and rectenna modules will require extensive facilities.	Arrays will require roughly 4 million pedestals plus provisions for mounting switch gear, dc/dc connectors and cable runs. Large undertaking for planning purposes but not a technical problem.	Similar technology could be used as for the solar blankets. However, modules could be of more manageable size. Weight will not be a problem but strength/ weatherability will be factors not encountered in space. High-rate production must be accomplished on site for production of over 11,400,000 multilayered panels of four types assembled into 580,500 subarrays.
PLAN NO. 6 WBS ELEMENT	1.1.7 System Test Hardware	1.2 Space Construction and Support	l.3 Transporta- tion	1.3.7 Facilities	1.4.2 Support Structures	1.4.3 Dipole/ Rectivier Ele- ments (Power Collection)

PLAN | 1

4 | TITLE

PRODUCT ASSURANCE

#### PROGRAM PLAN DEFINITION

This plan shall address the program requirements for quality assurance, reliability assurance, and systems safety. NHB 5300.4 (ID-1) shall be used as a guide in developing these requirements.

### SPS POINT DESIGN PROGRAM REQUIREMENTS

- Solar Photovoltaic CR-2 Concept Definition
- Quality Assurance Requirements—NHB 5300.4 (ID-1)
- Reliability Assurance Requirements—NHB 5300.4 (ID-1)
- Systems Safety Requirements—NHB 5300.4 (ID-1)

#### RESOURCE CONSIDERATIONS

- · Technical and Management Personnel
- · Support Equipment/Facilities and Software

#### DISCUSSION

Product assurance plans, comprising the disciplines of safety, reliability, and quality assurance, will provide direction for the overall satellite system. These plans will be applicable to vehicle contractors (SPS, HLLV, COTV, STS, and support equipment) and site contractors (ground receiving station). The plans, reflecting NHB 5300.4 (ID-1) requirements and associated data reporting requirements, will provide the basis for more detailed plans at the various vehicle and site levels during design/development, manufacturing, test, and operations. Subsequently, plans will be required from the industrial subcontractors. The scope of these plans will vary, depending on the type of procurement.

Quality assurance plans relate primarily to the vehicles; site (facility) operations normally are administrated through quality procedural manuals covering all quality aspects of site operations. These manuals will be compatible with overall program quality requirements.

While the implementation of product assurance plans will entail a relatively small expenditure of resources, the consideration entailed in product assurance may have far reaching effects in terms of providing for reliability and safety of equipment and personnel.

NHB 5300.4 (ID-1) provides guidelines for development of product assurance plans relative to the Space Shuttle. These plans encompass the areas of safety, reliability, maintainability, and quality assurance. While each of these will require planning unique to the SPS, the area overriding concern is safety. The logistics, fabrication, operation, and maintenance activities associated with the satellite system will require manned space activity well beyond any previous space endeavor. Due to the large size of the satellite,

PLAN TITLE

-7

# PRODUCT ASSURANCE (Cont.)

rapid means of transporting men and materials to the most remote areas must be developed. This, along with associated inspection and maintenance must be accomplished safely with minimal need to shut down any portion of the high-voltage grid. Replacement of certain items might be scheduled for periods of eclipse; however, most activities will take place aboard a fully operating power station.

Ground safety will also be of concern. Consider the rectenna site, for example. Besides the microwave potential hazard, the high ac or dc voltage conditioning equipment represents potential lethal voltages to maintenance personnel required to repair or service that equipment. The heights of the various equipments represent an occupational hazard relative to falls or tool droppage. Also, lightning strike potential is affected by the heights, conductors, and array size.

Considerations for other major systems and subsystems are similar in scope. Routine in-orbital operations, for example, will be undertaken on a large scale. Life support and safety will be major drivers in the design of each space system. The more significant product assurance considerations are summarized in Table 7-1.

Table 7. SPS DDT&E Program Planning Considerations (Phase C/D) Impact Sheet

)f 1		CAT- EGORY	၁	ပ	Ü	<b>8</b>	ပ	Ф
Sheet 1 of	TITLE: PRODUCT ASSURANCE	IMPACT	Product assurance elements must be established which apply to daily operations in the major manufacturing, installation, and operations in space. Safety aspects must consider protection of personnel and equipment during inspection, maintenance, repair, and replacement operations in the midst of an operating antenna or solar blanket field.	System safety and reliability will be addressed at the system level since inspection, M/R, etc., must be performed on equipment with the photovoltaics and concentrators operating in combination.	27,500 m <sup>2</sup> or more of solar blankets will be produced each day with associated checkout, inspection and repair. This element includes product assurance considerations on the ground and in orbit.	Verification of pointing accuracy and interlock capability will be essential to public acceptance of SPS. Quality assurance considerations will relate to producing zero-defect waveguide assemblies in orbit.	Safety aspects of fueling and performance M&R, etc., of multiple thrusters of the attitude control and stationkeeping system.	The product assurance plan will not entail substantial financial commitment in itself relative to some other plans. However, it is assigned to a high category at the summary level to emphasize the critical impact of safety and reliability on the SPS. Requirements established by the product assurance plan will have a strong influence on design and may result in considerable budgetary impact in testing, manufacturing, and operations.
	PLAN NO. 7	WBS ELEMENT	1.1 Satellite System	1.1.1 Energy Conversion	1.1.1.3 Solar Blankets	1.1.2 Power Transmission	1.1.4 ACS	1.5 Program Management

.

PLAN TITLE

8

### **FACILITIES**

### PROGRAM PLAN DEFINITION

This plan shall provide a compilation of the facility requirements (identified in other sections) for the total program, including development, testing, manufacturing, checkout, and operations. Budgetary estimates shall be provided for the major/critical new facilities and/or major modifications. Options shall be described which will assist in determining whether these costs shall be contractor capital equipment or government facilities. Usage schedules shall be determined and any known conflicts shall be identified.

### SPS POINT DESIGN PROGRAM REQUIREMENTS

- Solar Photovoltaic CR-2 Concept Definition
  - Development facilities requirements
  - Testing facilities requirements
  - Manufacturing facilities requirements
  - Checkout and operations facilities requirements
  - Ground support requirements
- · Requirements for Major/Critical New Facilities
  - Financial and organizational concept financing
    - ·Space segment
    - ·Ground segment

### RESOURCE CONSIDERATIONS

- · Technical and Management Personnel
- · Architectural and Engineering Capability
- · Maintenance and Operational Workers
- · Site and Facilities Availability
- Materials and Support Equipment
- Heavy Construction/Industrial Equipment

### DISCUSSION

Major facilities will be required for manufacturing, testing, ground support, and warehousing—such as those related to power generation and transmission. The same will apply to major systems such as STS and HLLV which must include launch, recovery, and refurbishment facilities (Table 8-1).



Table 8. SPS DDT&E Program Planning Considerations (Phase C/D) Impact Sheet

1 of 1	CAT- EGORY	A	¥	<b>£</b>	₩	<b>м</b>	<b>4</b>	·
Sheet 1 TITLE: FACILITIES	IMPACT	Production, test, storage facilities	Production and high-voltage test facilities	Production and high-voltage test facilities	This will provide facilities resulting from requirements generated under other plans. Of particular concern are STS launch/recovery and logistics/payload integration facilities.	Production facilities for rectenna support structures and power collectors Includes all land, site preparation, buildings, access, and utilities interface for rectenna and other elements of ground station. Site may encompass over 150 km². Several thousand workers must be accommodated during construction, with considerable reduction when the site is placed into operation.	Top-level planning function; major cost commitment required in subordinate areas indicated.	
PLAN NO. 8	WBS ELEMENT	1.1.1.3 Solar Blankets	1.1.1.4, 1.1.2.3, 1.1.6.3 Power Distribution and Conditioning	1.1.2 Power Transmission	1.3.7 Facilities	Ground Receiving Station	1.5 Program Management	

PLAN | TITLE

9a

GROUND OPERATIONS—Ground Integration

### PROGRAM PLAN DEFINITION

This plan will cover integration of equipment and instruments into payloads. (Launch site integration of payloads into vehicle carriers will be covered under Space Operations, Plan 10.) An assessment of the manpower, facilities, equipment, and hardware to support these ground integration activities is required.

### SPS POINT DESIGN PROGRAM REQUIREMENTS

- Solar Photovoltaic CR-2 Concept Definition
  - Operational instruments and payload integration requirements
  - Launch site/vehicle carrier definitions
  - Supporting equipment and facility requirements
  - Test and verification requirements

### RESOURCE CONSIDERATIONS

- Technical and Management Personnel
- · Supporting Hardware and Software
- · Test Equipment and Facilities

### DISCUSSION

Ground integration will have no major impact; however, early consideration should influence certain designs (i.e., waveguides) to assure optimum mix of payloads for STS. Table 9a-1 identifies ground assembly and integration considerations relative to its programmatic impact.

Table 9a-1. SPS DDT&E Program Planning Considerations (Phase C/D) Impact Sheet

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	CAT- EGORY	U	ນ	<u></u>		 		·	
TITLE: Ground Operations—Ground Integration	IMPACT	The integration task is comprehensive involving all aspects of assembly, test, and checkout of components, subsystems, etc., into payloads. This includes automated and, in some cases, sortie payloads. Integration aspects must be considered in all phases of design to assure optimum combination of payload space and weight resulting in minimum flights to orbit.	Provides consideration for policy and procedure required to conduct operations and integration.						
PLAN NO. 9a	WBS ELEMENT	1.1.7 Systems Test Operations	1.5 Management and Integration						
	····				3-52	 -	 		

PLAN TITLE

9h

GROUND OPERATIONS—Maintenance and Refurbishment

### PROGRAM PLAN DEFINITION

This plan will provide identification of expected maintenance and refurbishment requirements, assessment of how these activities would be accomplished and the resources required, i.e., manpower, facilities, and equipment.

### SPS POINT DESIGN PROGRAM REQUIREMENTS

- Solar Photovoltaic CR-2 Concept Definition
  - Rectenna maintenance and refurbishment requirements
  - Shuttle-derived HLLV maintenance/refurbishment requirements
  - Launch site operations

### RESOURCE CONSIDERATIONS

- Technical and Management Personnel
- · Operations and Maintenance Personnel
- · Support Equipment and Facilities
- Special/Unique Refurbishment Equipment
  - Rectenna panel checkout
  - Shuttle-derived HLLV

### DISCUSSION

This plan will entail major effort primarily in the areas of rectenna and STS. The 5-GW rectenna site will, for example, contain 580,500 rectenna dipole panels (9.33 m high by 14.69 m long) covering an area of 78.5 million square meters.

Refurbishment techniques for STS should derive directly from the Shuttle. The STS M&R plan area, while substantial will evolve over several years as the prototype ground station and launch/transportation system are being developed and brought up to operational status.

The requirements for inspection, cleaning, maintenance, and some replacement of failed panels will require a sizeable direct labor force and supporting equipment to maintain the operational antenna once installed (Table 9b-1).

Table 9b-1, SPS DDTE Program Planning Considerations (Phase C/D) Impact Sheet

PLAN NO. 9b	TITLE: GROUND OPERATIONS-Maintenance and Refurbishment	
WBS ELEMENT	IMPACT	CAT- EGORY
1.4.6 Operation	Maintenance and refurbishment will cover all areas of ground stations including dipole subarrays and all associated power conditioning, distribution, and interface equipment.	ပ
1.5 Management and Integration	Policy and procedural requirements necessary for maintenance and refurbishment are included.	v

PLAN | TITLE

9c

GROUND OPERATIONS - Logistics

#### PROGRAM PLAN DESCRIPTION

This plan will address logistic requirements to include planning, warehousing, facilities and equipment, transportation, training, manpower, operations supply and maintenance, etc., utilizing the spare parts requirements identified in other sections.

### SPS POINT DESIGN PROGRAM REQUIREMENTS

- Solar Photovoltaic CR-2 Concept Definition
- SPS Training Requirements
- Warehousing Operations—Spares
- · Logistic Support Definitions—Provisioning
- · Facilities and Equipment Requirements—Spares Depots
- · Logistics and Transportation Requirements-Spares
- Operational Supplies and Maintenance

#### RESOURCE CONSIDERATIONS

- · Technical and Management Personnel
  - Logistics Planners
  - Training Personnel
  - Operational/Support Personnel
- · Transportation Systems
- · Support Materials/Equipment and Facilities

### DISCUSSION

While logistics for the purpose of supporting the SPS alone will be fairly extensive, the major impact of the Phase C/D logistics plan is that it be prototypical of the plan for the following operational phase. This approach is essential since the plan must provide for rapid, orderly expansion toward the end of Phase C/D. Considerations include such items as land transportation networks, training schools and planning facilities for stockpiling and warehousing of materials. Figure 9c-1 provides some indication of the scope of the logistics activities for the launch site, for example. Key elements will include the final selection and design of launch and transport vehicles, all of which must be supplied with trained flight and support crews, fuel, and spare parts. Similar flow charts must be developed for the rectenna site and for the overall logistics ground network. Subplans for space logistics would be a part of Plan 10, Space Operations.

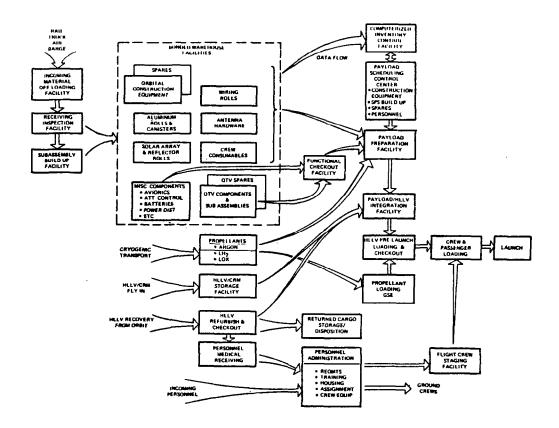


Figure 9c-1. Launch Site Logistics

PLAN | TITLE

10

### SPACE OPERATIONS

### PROGRAM PLAN DESCRIPTION

This plan shall address all of the activities associated with space/mission operations. Mission operations cover those activities from liftoff through on-line operations including ground operations, and shall include the requirements for manpower, facilities, and equipment to support the various ground and orbital on-site operations. (Actual procurement and training of manpower, construction of facilities, etc., will take place under the respective plans such as 9c (Logistics) and 8 (Facilities).

### SPS POINT DESIGN PROGRAM REQUIREMENTS

- Solar Photovoltaic CR-2 Concept Definition
- Mission Planning Definitions (Plan 2)
- · Transportation System Definitions
- · Orbital Operations Definitions
- Space/Ground Operational Interfaces
- Operational Hardware/Software Requirements

#### RESOURCE CONSIDERATIONS

- · Technical and Management Personnel
- Operational and Support Personnel
- · Supporting Hardware and Software
- Materials/Equipment and Facilities

### DISCUSSION

The conduct of large-scale space operations leading to routine construction operation and maintenance of space complexes such as SPS represents, perhaps, the major challenge in space for the remainder of this century. To fully exploit the potential that space provides will require devoting extensive resources and long-range planning to space programs of which SPS is the major one foreseen. The Space Operations Plan will require a breakdown into subplans which could include the following:

- Construction (Manufacturing)
- · Space Base
- Logistics (including Life Support)
- · Maintenance and Refurbishment
- Interstation/Interorbital Transportation
- Product Assurance (including Safety)
- Ground Support (i.e., operations, not logistics/facilities planning and operation, not construction)

PLAN TITLE

10

# SPACE OPERATIONS (Cont.)

Some of the above such as construction, manufacturing and product assurance are now incorporated as part of existing plans. Consideration might be given to including these unique facets of the Space Operations Plan.

Operational control will include both on-station operations, such as satellite construction, and control of transportation vehicle and construction bases. Planning considerations of space operations are shown in Table 10-1.



Table 10-1. SPS DDT&E Program Planning Considerations (Phase  ${\it C/D}$ ) Impact Sheet

1g A	ac- mud
Operations performed on the satellite as a power-generating and transmitti station. Does not include checkout of satellite proper or its subsystems.	Manufacturing of the production satellites is based on orientation of beam machines in a complex, spatially controlled by a full cross-section template, as shown in Figure 10-1. The resulting manufacturing sequence provides for full construction in a total elapsed time and requires supporting several hundred men in orbit. The EOTY, on the other hand, will be assembled to permit wide flexibility in sequencing and rate of assembly. Considerable study will be required to identify an optimum approach to continuous manufacturing. This must be followed by development and demonstration on the ground and in space of equipment (i.e., beam machines) and operations (i.e., joining) applicable to the prototype.  Efgure 10-1.  Figure 10-1.  Escanding  Scenario  Scenario  Scenario  Scenario  ONNIALIO MASE  ONNIALIO MASE
1.1 Satellite System	1.1.1.1, 1.1.2.1, 1.1.6.1 Structure
	Operations performed on the satellite as a power-generating and transmitting station. Does not include checkout of satellite proper or its subsystems.

 ${\it Table~10-1.} \\ {\it SPS~DDT\&E~Program~Planning~Considerations~(Phase~C/D)~Impact~Sheet}$ 

2 of 2	CAT- EGORY	O O	၁	A			
TITLE: SPACE OPERATIONS	IMPACT	Solar blankets operational capability for larger-scale assembly, checkout, and maintenance in orbit represents the significant challenge to SPS.  Included also are the power transmission system elements.	Operational requirement planning and control.	Summary planning functions integrating all major flight and supporting ground systems.			
PLAN NO. 10	WBS ELEMENT	1.2 Space Construc- tion & Support	1.3 Transportation	1.5 Program Management	3–60		

PLAN TITLE

11

# LAUNCH OPERATIONS

### PROGRAM PLAN DESCRIPTIONS

This plan shall address all the activities associated with launch operations. Launch operations cover those activities from arrival of the payload at the launch site until liftoff. This shall include, but not be limited to, handling, inspection, assembly/integration/installation, checkout, calibration, etc.

### SPS POINT DESIGN PROGRAM REQUIREMENTS

- Solar Photovoltaic Cr-2 Concept Definition
- Launch Site Payload Integration Definitions (Plan 9a)
- Transportation System Definitions
- Launch Site Facility Definition (Plan 8)
- · Launch Site Support Equipment Utilization
- Test and Verification Definition (Plan 4)

#### RESOURCE CONSIDERATIONS

- Technical and Management Personnel
- Operations and Maintenance Personnel
- · Support Equipment and Facilities
- Special/Unique Processing Equipment/Facilities

### DISCUSSION

Launch operations will involve expanding the capability already developed under the basic Shuttle program. Because of the number and frequency of launches, this will require considerable expansion of current launch facilities. As with the Logistics Plan, however, the major impact is to incorporate within the plan and its implementation the tremendous capability needed for multiple daily flights of HLLV's and provisions for rapid turnaround needed during post-IOC period. Important considerations are shown in Table 11-1.

Table 11-1. SPS DDT&E Program Planning Considerations (Phase  $\mathcal{C}/\mathcal{D}$ ) Impact Sheet

Γ	CAT- EGORY	υ ·	м	Д
TITLE: LAUNCH OPERATIONS	IMPACT	Operational policy and procedure planning required for the handling of STS and VTO/HL HLLV vehicle turnaround.	Facilities planning requirements will be needed to support STS and VTO/HL HLLV operations. Included are facilities for launch, recovery, fuel, logistics support, and operations.	Due to the large number of launches and long period over which launch operations will take place the development of routine, rapid turnaround capability will be a major undertaking. Estimates are that in the order of 200 launches of a Shuttle-derived HLLV will be required to support precursor/prototype assembly over the period 1996 through 1008. This is an average of almost two launches per week.
PLAN NO. 11	WBS ELEMENT	1,3 Transportation Operations	1.3.7 Facilities	Management and Integration

# SPS DDT&E PROGRAM PLANNING SUMMARY

PLAN

TITLE

12

# SPECIFICATION TREE

# PROGRAM PLAN DESCRIPTIONS

A specification tree shall be developed, beginning with the project level at the top.

# SPS POINT DESIGN PROGRAM REQUIREMENTS

- Solar Photovoltaic CR-2 Concept Definition
- System and Subsystem Definitions
- Make-or-Buy Decisions (Plan 1)
- Development and Procurement Definitions

# RESOURCE CONSIDERATIONS

- · Technical and Management Personnel
- Support Materials/Equipment and Facilities

# DISCUSSION

This plan might be incorporated under Plan 1 or 2 and should be maintained as a natural part of the top-level planning function.

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•			



# SPS DDT&E PROGRAM PLANNING SUMMARY

PLAN | TITLE

13

NATURAL RESOURCES ANALYSIS

# PROGRAM PLAN DESCRIPTION

This plan assesses the degree and rate of consumption of critical materials, the degree of utilization of both material extraction and production plants, and the sensitivity of this consumption toward meeting the program objectives, major milestones, and the initial operational capability of the Satellite Power System (SPS). It expressly covers a natural resource analysis of only the first Rockwell SPS reference configuration.

#### SPS PROGRAM REQUIREMENTS

Program requirements and detail system definitions are based on the SPS reference configuration of a three trough planar array with an end mounted tension web antenna. Programmatic ground rules and guidelines are:

- · Key dates for program planning:
  - 1981-1987 Key Technology Program Activities
    - 1990 Decision Point for SPS Commercialization (Phase C/D)
    - 2000 IOC of First SPS including Ground Receiving Station
- SPS build rate at two nominally 5 GW SPS's/year for 30 years to provide a 60 system capability by 2030.

The resource analysis considered these ground rules and SPS program schedules to identify the timing of system acquisitions and main operational elements. The following paragraphs summarize the analyses for use in identifying potential impact on U.S. productive capacity.

#### SPS PROGRAM ELEMENTS

Main elements of the SPS program include the satellite; space construction bases and support assembly equipment; space transportation and ground facilities; the ground receiving station; and management/integration activities Principal resource requirements of the satellite, space construction, ground receiving station, and transportation elements are discussed in the following paragraphs.

# Satellite System

The elements/systems of a space satellite are grouped into the categories of - energy conversion, power transmission/antenna, information management and control, attitude control and stationkeeping, and communications. Each of these items were analyzed and researched for its major resource requirement that focused on structures, concentrators, solar blankets, power distribution

and conditioning, and the klystron power module. A 25% weight growth factor was added to the basic system design weight statement for resource calculations. This is equivalent to the normal factor used in calculating the total mass to provide for contingency.

Structure. The primary structure which supports the solar array and antenna segment is composed of graphite impregnated composites. The total weight of the composites is  $1.028\times10^6$  kg or 2,265,000 lb. Approximately 30% by weight would be graphite  $(0.309\times10^6$  kg/681,200 lb); 15% by weight would be glass fibers  $(0.154\times10^6$  kg/339,570 lb); and 55% resin  $(0.565\times10^6$  kg/1,246,000 lb). The secondary structure/mechanisms of the solar arrays and antenna segments are considered mainly of aluminum and weighs  $1.769\times10^6$  kg or 3,900,000 lb.

Concentrators. The concentrators (reflectors) consist of aluminum coated 0.5 mil Kapton - Type H sheet. The total weight is  $1.296\times10^6$  kg or 2.857,000 lb of which  $1.283\times10^6$  kg or 2.828,000 lb is Kapton and  $.013\times10^6$  kg or 29,000 lb is aluminum.

Solar Blanket. The solar blanket consists of a variety of materials as listed in Table 13-1. The total amounts required are factored from the work completed under Arthur D. Little contract with NASA (NAS9-15294).

	AMOUNT	REQUIRED
MATERIAL	10 <sup>6</sup> kg	× 10 <sup>6</sup> 1b
ALUMINUM GALLIUM ARSENIC (99.999%) SELENIUM (00.999%) ZINC (99.999%) ALUMINUM (99.999%) SILVER GOLD TIN SAPPHIRE (Al <sub>2</sub> O <sub>3</sub> ) COPPER TEFLON	0.008 0.432 0.465 34 kg 11 kg 0.005 0.172 1.640 0.488 2.700 0.476 0.915	0.018 0.952 1.025 75 1b 24 1b 0.011 0.379 3.615 1.076 5.952 1.049 2.017
KAPTON	1.219	2.687
TOTAL	8.518	18.781

Table 13-1. Solar Blanket Material Mass

Power Distribution and Conditioning. This category includes the power conditioning equipment and conductors in both the solar array and the antenna. Also included are the power-transmitting slip rings. The total weight of power distribution and conditioning equipment, etc., amounts to  $8.884 \times 10^6$  kg, or  $19.585 \times 10^6$  lb and consists of the following materials (Table 13-2):

Table 13-2. PD&C Materials

	AMOUNT REQUIRED		
MATERIAL	× 10 <sup>6</sup> kg	× 10 <sup>6</sup> 1b	
ALUMINUM	6.824	15.044	
STEEL	0.506	1.115	
TITANIUM	0.028	0.062	
COPPER	0.839	1.850	
PLASTICS	0.681	1.501	
SILVER	0.006	0.013	
TOTAL	8.884	19.585	

<u>Power Modules (Klystrons)</u>. The weight of klystrons required on the SPS is estimated to be  $5.206 \times 10^{5}$  kg or  $11,477 \times 10^{6}$  lb. The materials required for their construction are listed in Table 13-3.

Table 13-3. Power Module Composition

	AMOUNT	REQUIRED
MATERIAL	× 10 <sup>6</sup> kg	× 10 <sup>6</sup> 1b
ALUMINUM	0.265	0.584
STEEL	0.690	1.521
COPPER	2.550	5.621
ALNICO-V	1.010	2.227
54% Fe	0.545	1.201
24% Co	0.242	0.533
14% Ni	0.141	0.311
8% A1	0.081	0.179
ALUMINUM OXIDE	0.531	1.171
GRAPHITE EPOXY	0.160	0.353
30% GRAPHITE	0.048	0.106
15% GLASS FIBER	0.024	0.053
55% RESIN	0.088	0.194
TOTAL	5.206	11.477

Material Requirements for Main Elements of the Satellite System. A tabulation of satellite system material requirements in each of the study areas is presented in Table 13-4. The total weight of  $26.700 \times 10^6$  kg or  $58.873 \times 10^6$ lb is distributed over 22 materials as listed.

#### Ground Receiving Station (GRS) Definition

Key elements of the ground receiving station that might impact resource availability consists of the site and facilities requirements, the rectenna support structure, and the power collection system requirements. Other elements such as conversion stations, the grid interface and the operations requirements are basically identical to those required by conventional power

Table	13-4.	Material Reguir	Requirements for M	for Main Satellite		ments	
	STRUCTURE/	CONCEN-	SOLAR		POWER	TOTAL	WEIGHT
MATERIAL		TRATORS x 10 <sup>6</sup> KG	BLANKET x 10 <sup>6</sup> KG	& COND. x 10 <sup>6</sup> KG	(KLYSTRONS) x 10 <sup>6</sup> KG	$^{\mathrm{KG}}_{\mathrm{x}}$ 106	LB <b>x</b> 10 <sup>6</sup>
	1.769	0.013	0.013	6.824	0.346	8,965	19.768
ALUMINUM OXIDE					0.531	0.531	1.171
ARSENIC COBALT			0.465		0.242	0.465	1.025
COPPER			0.476	0.839	2.550	3.865	8,520
GALLIUM	( ,		0.432			0.432	0.952
GLASS FIBER	0.154		1 640*		0.024	0.178	0.392
GRAPHITE	0.309		050.1		0.048	0.357	0.787
IRON					0.545	0.545	1.201
KAPTON		1,283	1.219			2.502	5.517
NICKEL					0.141	0.141	0.311
PLASTIC	i c			0.681	0	0.681	1.501
REDIN CARDITION	0.505		6		0.088	0.653	1.440
SAPPHIRE			2.700			2.700	5,952
SILVER			(34 AG) 0 172	900 0		(34 kg)	(97 67)
STEEL		-	  -  -	0.506	0.690	1,196	2.637
TEFLON			0.915			0.915	2.017
TIN		•	0.488	,		0.488	1.076
TITANIOM				0.028	_	ö	$\circ$
ZINC			(11 KG)			(11 KG)	(24 LB)
SUBTOTAL	2.797	1.296	8.518	8,884	5.205	26.700	58.873
OTHER (ACS & THERMAI	IAL.)					6.318	13.931
				TOTAL	TOTAL WEIGHT	33.018	72.804
*Not aconomically fe	feasible Assume	the use of	an aluminum	base material	al.		
CCOMPACTED )							

generating systems and are not anticipated to impose significant resource rerequirements. Likewise, the control system, while unique to the GRS concept, is not anticipated to require either unusual types or large quantities of natural resources.

Site and Facilities. The ground receiving station will require an area of approximately 35,000 acres. The rectenna field will occupy approximately 25,000 acres with a surrounding buffer zone of 10,000 acres. The land will need to be cleared and leveled and a rainfall run-off system would need to be constructed. Several alternative layouts were examined, however, the amount of excavation and concrete was found to be relatively insensitive to the layout alternatives. Concrete footings (2 parallel rows) would need to be poured for each row of antenna panels. Concrete requirements for GRS rectenna panel footings and for the water channels were translated into the constituent materials (see Table 13-5).

Table 13-5. Cement/Aggregate Requirements

CEMENT SAND ROCK (APPROX. 1" - 1-1/2") WATER	949,000 TONS 2,827,000 3,695,000 606,000
REINFORCING ROD	8,077,000 TONS 19,000 TONS

It was assumed that the access road between panels would consist of a 6 inch deep layer of gravel. The gravel requirements for the access roads would be 9,791,000 yd or approximately 13,707,000 tons. Requirements associated with construction of 10 miles of access roads and 23 miles of perimeter roads plus 20 miles of access railroad, and 25 miles of perimeter railroad were not considered to impose abnormal requirements on natural resources or production capacities.

Rectenna Support Structure. The rectenna support structure consists of steel hat sections, I beams, tube braces, fittings and hardware along with miscellaneous items. The total weight of steel required for rectenna support was calculated to be 1666.7 kg or 3674 lb per panel, or a total of  $967.5 \times 10^6 \text{ kg}$  or  $2132.9 \times 10^6 \text{ lb}$  for the 580,500 panels in the rectenna array.

Power Collection. The power collection occurs in the panel array elements mounted on the rectenna panels. The elements consist of three 0.5" layers of a dielectric (plastic compound) that separates four layers of 0.0039 inches of copper, clad to 0.001 inches of Mylar. Interspersed within each panel are 735 diodes, or a total of  $426.67 \times 10^6$  diodes in the total array of 580,500 panels. The one ounce diodes consist of 44% tungsten, 40% copper, 15% gallium arsenide and 1% gold and other exotic materials. Consequently, the total material requirements for the power collection portion of a single rectenna are itemized in Table 13-6. Miscellaneous materials such as copper wiring, J-boxes, etc., were not considered to severely impact either material availability or production capacity.



Table 13-6. Diode Materials per Rectenna

		REQUIRED
MATERIAL	kg×10 <sup>6</sup>	16×10 <sup>6</sup>
PLASTIC DIELECTRIC	169.96	374.68
MYLAR	11.32	24.95
COPPER (COATED OR MYLAR)	46.13	101.70
DIODES TUNGSTEN COPPER GALLIUM ARSENIDE GOLD/EXOTICS	5.32 4.84 1.81 0.12	11.73 10.67 4.00 .27

# Space Transportation System Definition

The SPS program will require six new vehicle or growth developments. The listing of vehicles needed to complete the first satellite for an initial operating capability is shown in Table 13-7.

Table 13-7. SPS Fleet/Operations for First Satellite

	NO. OF VEHICLES	NO. OF FLTS.
PERSONNEL LAUNCH VEHICLE (PLV) SHUTTLE GROWTH	2	60
HEAVY LIFT LAUNCH VEHICLE (HLLV)	5	234
PERSONAL ORBITAL TRANSFER VEHICLE (POTV)	4	45
INTERORBITAL TRANSFER VEHICLE (IOTV)	4	408
CARGO ORBITAL TRANSFER VEHICLE-ELECTRICAL (EOTV)	6	7
PERSONAL MODULE (PM - USED WITH POTV)	4	60

In order to be available when required, the development times for the six vehicles would overlap. The vehicles will require large quantities of propellants and possibly the construction of new propellant production facilities. The total annual propellant quantity estimated to be required in support of the construction of the first SPS is shown in Table 13-8. The actual quantities required would be somewhat larger than the amounts shown because losses due to boil-off, evaporation, etc., have not been included.

# SPS PROGRAMMATIC DEFINITION

Quantities of natural resources required for construction of the SPS, while significant in themselves, may nevertheless be misleading because it is the rate of resource requirements that governs their impact. The elements required for the satellite system (i.e., transportation systems, bases, etc.) will be constructed over a number of years. Thus, the resource requirements

Table 13-8. Propellant Requirements for First Satellite

	× 10 <sup>6</sup> kg			
VEHICLE	LOX	LH <sub>2</sub>	RP	ARGON
PLV HLLV POTV IOTV EOTV	69.960 990.288 2.526 0.105	11.640 80.028 0.421 0.018	201.006	4.690
TOTAL	1062.879	92.107	201.006	4.690
MILLIONS OF LB	2343.117	203.050	443.118	10.339

can be spread over a commensurate period. On the other hand, the ground receiving station is scheduled for IOC approximately four to five years after start of site preparation on the first GRS. Examination of the domestic availability of many of the resources required by the SPS can readily result in the identification of those resource requirements that would not present substantial problems. Similarly, those resource requirements that might tax the current productive capacity of the U.S. can at least be flagged for more detailed analyses in light of the schedules of GRS requirements as shown in Figure 13-1.

# RESOURCE REQUIREMENTS

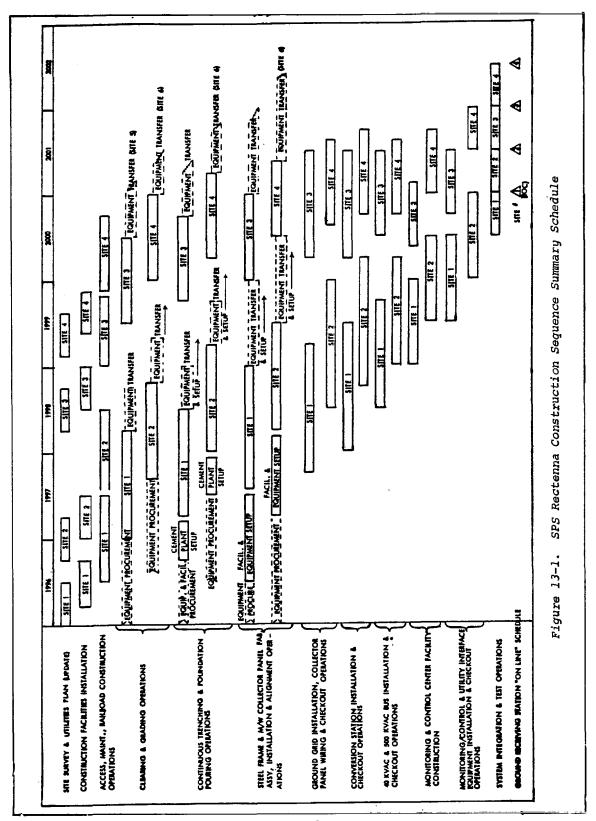
Basic resources considered were: 1) material requirements (i.e., mineral, metal, plastic, etc.); 2) production capacity for processing the materials; and 3) manpower - principal areas of skilled manpower essential for the development and implementation of main elements that comprise the SPS program.

#### Materials

In assessing the material resources, primary emphasis is placed on the indigenous U.S. supply. However, in some cases such as bauxite which is the basic source of aluminum, the annual U.S. imports from diverse sources are judged to be a more accurate measure of aluminum availability than U.S. bauxite production alone. In other cases, the SPS mineral requirements are assessed in terms of their impact on U.S. government stockpiles.

# Production Capacity

The production capacity is assessed in terms of the SPS demand versus the U.S. ability to readily expand its productive capacity to meet new requirements. A major impediment to ready expansion centers is based on the availability of relatively low cost energy sources. New industry may have difficulty in finding readily available locations with low cost energy sources. This is particularly true for production of energy intensive materials such as aluminum or sapphire.





#### Manpower

Requirements for skilled manpower can impose constraints on major developments based on the magnitude of SPS and its required disciplines. Two categories of important manpower considerations have been recognized. The first is the engineering manpower necessary for the concurrent development of five new major transportation systems in addition to the simultaneous development of the space bases and the satellite system. The second potential manpower constraint stems from the radiation exposure limitations on the satellite system construction crew. Two crews of 317 each will be required to man the SCB during construction of the first SPS. A work cycle of 3 months in orbit and 6 months on earth is planned for the construction period. This requires 3 full construction crews, plus a complete crew replacement every 3 years without attrition on the basis that five 3-month tours in orbit will result in a maximum lifetime radiation exposure. Consequently, hundreds of satellite construction workers will need to be recruited and trained continuously.

#### RESOURCE CONSIDERATIONS

Manpower and material requirements imposed by the development and construction of the SPS were identified and analyzed in terms of appropriate manpower and material availability within the U.S. Several potential problem areas were identified.

#### TECHNICAL AND MANAGEMENT PERSONNEL

Development of eight major systems are required for SPS transportation and space base requirements. These are:

- 1. Personnel Launch Vehicle/Shuttle Growth Vehicle
- 2. Heavy Lift Launch Vehicle (VTO/HL)
- Personnel Orbital Transfer Vehicle (POTV)
- 4. Interorbital Transfer Vehicle (IOTV)
- 5. Cargo Orbital Transfer Vehicle (COTV)
- 6. Space Construction Base (SCB)
- 7. Low Earth Orbit Base
- 8. Satellite O&M Base

Three major bases are required in the development and implementation of the SPS, namely the Space Construction Base (SCB), a Low Earth Orbit (LEO) Base and the Satellite O&M Base. The SCB, located in geosynchronous orbit, contains 33 tribeam fabricators (198 beam machines) as well as solar blanket and reflector dispensing areas. It also contains a central and auxiliary

habitats, landing area, and warehouse facilities. All of the basic elements of the satellite are constructed through the use of the SCB. The LEO Base is basically a supporting facility for staging cargo and propellants for transfer to GEO. The O&M Base is primarily the maintenance facility for the operational satellite. It contains maintenance supplies as well as a habitat for the maintenance/operations personnel.

Each of these developments constitutes a major program, requiring thousands of skilled engineers. The development schedules for most of these programs will overlap. In view of the current tight supply of skilled aerospace engineers, the unavailability of technical personnel may constitute a major impediment to the establishment of an SPS in accord with the planned schedules.

Another manpower consideration is the manning level for satellite construction. Required crew rotations to support construction of 60 satellites total 120, which results in 24 crews or 14,400 men. Applying a 20% attrition factor (resignations, etc.) raises this figure to 17,280. Similarly, 3,660 maintenance crew rotations at 30 men per crew and including attrition generate a requirement for 26,352 men. An additional 691 men are needed to operate one LEO facility for 30 years.

The need to recruit and train personnel and to develop the required facilities and materials for the programs/courses represent an important aspect of this overall activity.

#### MATERIALS

A review of materials required for construction of the satellite system and ground receiving station identifies several potential problem areas of material availability. Table 13-9 summarizes eight materials that can pose limitations on SPS requirements. Considerations on material availability are presented in the following paragraphs.

Table 13-9. Significant Satellite and GRS Resource Needs

١.	COBALT:	533,000 lb required. IMPORTS FROM PRIMARY SOURCE - ZAIRE - SUSCEPTIBLE TO INTERRUPTION.
2.	GALLIUM:	2,878,000 16 REQUIRED
3.	GOLD	3,750,000 1b REQUIRED
4.	KAPTON:	5,517,000 16 REQUIRED
5.	SAPPHIRE:	5,952,000 16 REQUIRED
6.	SILVER:	392,000 16 REQUIRED
7.	TEFLON:	2,017,000 16 REQUIRED
8.	TUNGSTEN:	11,730,000 16 REQUIRED



# DISCUSSION

#### COBALT

Klystron magnets are assumed to be made of AlNico-V which consists of 24% cobalt. This translates into a cobalt requirement of 533,000 lb. Over 60% of world cobalt production comes from Zaire, principally from Shaba Province. Military conflicts in that region have significantly reduced cobalt production. In 1977, the U.S. imported 17.7 million lb of cobalt. Another 624,000 lb were reclaimed from recycled alloys. The government stockpiles contain approximately 40 million lb of cobalt. There has been no domestic mining of cobalt since 1970. If the price increased from the current \$20 per lb to approximately \$60 to \$80 per lb, then it is expected that domestic production would be quite likely (in limited quantities). Inasmuch as cobalt is in short supply and the SPS would require approximately 3% of the total annual import or 1.33% of the stockpiled amount (if 40 million pounds still remain), cobalt availability should be monitored to track its possible impact on the SPS program.

#### GALLIUM

Approximately 2,878,000 lb of gallium are required by the SPS program. Gallium is obtained as a by-product of the processing of bauxite into alumina. Sufficient gallium is extracted to meet the demand. The current potential supply of gallium from domestically processed bauxite is over 2 million lb annually. By projecting the anticipated growth of the U.S. aluminum industry to the mid-1990's, the domestically processed bauxite would yield over 5 million lb of gallium annually. However, at present, it appears that the SPS gallium requirements will support program requirements and greater production/recovery is projected for the 1990 gallium production capacity.

#### GOLD

The 3,750,000 lb of gold required exceeds recent U.S. annual gold production. Approximately 45% of the gold produced in the U.S. is obtained as a by-product from other metal production, primarily copper. In 1977, approximately 75,000 lb of gold were produced domestically, at a value of \$148 per troy ounce. With gold currently selling at about \$240 per troy ounce, some increased production can be expected, but far short of the SPS requirements. The U.S. Treasury stockpile currently contains approximately 18.5 million lb of gold. Thus, the SPS requirement would constitute approximately 20% of our gold reserve. A substitute material will likely need to be developed to replace the gold requirements of the solar blanket.

#### KAPTON (POLYAMIDE)

The current U.S. production of polyamides is estimated to be between 4.0 and 5.0 million lb and expanding. In order to supply the 5,517,000 lb required by the SPS, the production capacity would need to be doubled or stockpiles built up. This could readily be accomplished given sufficient lead time.

#### SAPPHIRE

The aluminum oxide necessary to produce 5,952,000 lb of sapphire ribbon is readily available. The sapphire ribbon availability problem stems primarily from the technology requirements. The crystal growth is a relatively slow process. Considerable research is being performed to resolve the problems associated with sapphire ribbon production. Sapphire ribbon production advances should be monitored so that sufficient production facilities will be available to meet the demand.

#### SILVER

In 1977, the U.S. production of silver amounted to 2,617,000 lb. The 392,000 lb of silver required by the SPS thus constitutes 15% of the annual U.S. production. Silver usage in the United States amounted to approximately 11.0 million lb in 1978. The U.S. government holds a reserve of silver in the strategic stockpile on the order of 8,800,000 lb. The SPS requirement constitutes only 4.5% of the stockpiled amount. Approximately 70% of the silver produced in the U.S. is a by-product or co-product of other metal production -- chiefly copper, lead, and zinc. The 40% increase in the value of silver during the past year will serve to stimulate additional production, both domestically and world-wide.

#### TEFLON

The SPS requirement for Teflon was established at 2,017,000 lb or 34% of the 6 million pounds estimated to have been produced in 1977. Productive capacity is readily expandable, given sufficient lead time.

#### TUNGSTEN

The 11,730,000 1b of tungsten required by the SPS constitutes approximately 14% of the annual world production, or 50% more than the total U.S. production of tungsten in 1974. The total annual U.S. consumption of tungsten is on the order of 15 million pounds. U.S. Government stockpiles contain about 110 million pounds of tungsten or 9.4 times the SPS requirement. Consequently, the tungsten requirement of the SPS could present a major problem. Use of alternative materials for the tungsten in the panel diodes should be investigated.

#### SUMMARY

The above analyses have been based on the construction of one SPS. A construction rate of two SPS per year, for even several years, could substantially compound the material resources availability problems described. A list of data sources used in this analysis are presented in Table 13-10.

# Table 13-10. Key Data References

BATTELLE-PACIFIC NORTHWEST LABS DOCUMENTATION

MINERAL FACTS AND PROBLEMS, 1975 EDITION, U.S. DEPARTMENT OF INTERIOR

SURVEY OF AVAILABILITY AND ECONOMICAL EXTRACTABILITY OF GALLIUM FROM EARTH RESOURCES, ALUMINUM COMPANY OF AMERICA, 1 OCTOBER 1976

STATISTICAL ABSTRACT OF THE UNITED STATES 1976, U.S. DEPARTMENT OF COMMERCE

THE WORLD ALMANAC AND BOOK OF FACTS, 1979, GROSSET AND DUNLAP

STATISTICAL ABSTRACTS OF THE UNITED STATES - 1976

MINERAL FACTS AND PROBLEMS (1975), U.S. DEPARTMENT OF INTERIOR

UNITED STATES MINERAL RESOURCES, U.S. DEPARTMENT OF INTERIOR (1973)

CHEMICAL INFORMATION SERVICE S.R.I.

SOCIETY OF THE PLASTICS INDUSTRY

TYCO LABORATORIES, INC. - SAPHIKON DIVISION

UNION CARBIDE CORP. - ELECTRONICS DIVISION

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ALUMINUM COMPANY OF AMERICA REPORT

MODERN PLASTICS

# 4.0 CONCLUSIONS/RECOMMENDATIONS

This section presents summary comments on the methods and rationale followed in arriving at the results documented in this report. Suggestions are also provided in those areas where further analysis or evaluation will enhance SPS cost and programmatic definitions.

#### 4.1 SPS COST ESTIMATES

 $\checkmark$  The costing approach in this study considered an SPS option of 60 units with an IOC in the year 2000 and the full 300-GW capability to become operational at the rate of two SPS's or 10 GW per year.

✓ Cost estimates developed in this report are the extended products of a Rockwell cost data base uniquely formed for the SPS program. Main elements are categorized into (1) satellite (using MSFC and Rockwell CER's), (2) space construction and assembly (Rockwell CER's with space station backup), (3) transportation (Space Shuttle, company-sponsored studies, Boeing cost data), and (4) the ground receiving station (a grass roots analysis). This same data base was expanded to incorporate cost and programmatic information from discussions with-business and industry leaders. These discussions were supplemented by the use of selected literature and periodicals to obtain supporting data. Business/industry and literature sources are listed in Table 4.1-1.

 $\checkmark$  The Rockwell cost model and computer program can be used to calculate the costs for differing options in conjunction with an appropriate technical definition, traffic model projection, and operations scenario.

✓ A special factor was used when calculating the development cost of a system/subsystem and was based on the overall program scenario of that particular system. For example, crew and work support modules of the LEO, SCB, or satellite operations and maintenance base are of a common design, although required at differing times in accordance with the program schedule. Appropriately then, development factors were used to project costs at a 100-percent factor for the first module—whereas a lesser factor was used for subsequent requirements of the same modules to cover any revised development or integration need when being used in other applications. This represents a realistic programmatic approach to costing. Other areas should be studied for the use of this same logic.

 $\checkmark$  TFU costs projected for an SPS operational capability of the ground and space segments include estimates for initial space transportation fleets, satellite construction, operations, and the ground receiving station plus electric utility grid interface and supporting facilities. As such, all cost estimates for the TFU include the full cost of systems, equipment, facilities, and machinery that may have a service life capable of building more than one SPS. Therefore, the TFU cost represents a level of investment that can be expected when building a single-unit SPS option.

Table 4.1-1. Business/Industry and Literature Sources

Organization	Purpose
American Bridge—A division of U.S. Steel	To develop steel requirements, costs, and opera- tions definition for procurement and installation of rectenna support structure.
Riverside Cement—A division of American Cement Corporation; and C. S. Johnson Co.	Provide consultation on cement/concrete specifi- cation operational methods; processing/handling equipment.
Townsend & Bottum, Inc., (construction manager) 10-MW Solar PlantBarstown, CA	Discuss site preparation, construction operations/ sequencing, plus activation requirements.
Southern California Edison	To discuss dc/ac power distribution and conversion requirements and obtain cost estimates on installation of lines/towers.
Modern Alloys, Inc.; and Miller Formless Co.	To discuss use and application of equipment/crew for continuous concrete pour of rectenna support structure footing.
Caterpillar; International Harvester; and JETCO, Inc.	Obtain prices on earth moving, grading, and trenching equipment
Literatur	e Sources
The Richardson Rapid System 1978-1979 Edition	Construction labor and operations prices
Engineering News Record—1977, a weekly McGraw-Hill publication	Cement, aggregate and labor prices
National Construction Estimating Guide (NCE)	Construction operations







 $\checkmark$  SPS investment (ICI) costs in this study represent the average of a 60-unit option covering the cost of production, assembly, installation, transportation, and testing needed to produce individual satellites, transportation systems, and ground receiving stations—including required support. SPS operations costs consist of the effort required to operate and maintain the SPS program (including replacement capital items) over its operational lifetime of 30 years.

 $\checkmark$  Further study is required to identify and analyze SPS cost drivers. This should be an integrated process where technical and program development activities confirm and optimize SPS designs, or technical approaches, for cost-effective results.

✓ Several ground receiving station issues require further design definition. These include rectenna lightning protection, support structure optimization, and the rectenna drainage approach. In addition, the space transportation (HLLV) concept needs further definition.

#### 4.2 ROCKWELL COST MODEL

√ The Rockwell SPS cost model was expanded from its earlier version (Exhibit A/B) to (1) provide for newly added input requirements, (2) handle these new requirements when making cost calculations, and (3) provide a more versatile model. There are now six basic input categories: (1) line item name and units; (2) estimating relationships (CDCER, CICER); (3) design parameters such as CF, DF, and TF; (4) programmatic definitions ( $Z_1$  to  $Z_5$ ); (5) summing information; and (6) the addition of a "comments" section on each cost sheet to document unique technical or estimating characteristics of the line item. Although not required at this time, it is possible to expand the model with an input for use when calculating the complexity of development cost estimates (CFD) as compared with the complexity factor (CFI) as may be needed to calculate investment costs.

√ Changes to the cost model and computer program have simplified the approach when making inputs to the computer. Previously, fixed locations required careful input preparations on a line item by line item basis. This approach was revised to provide the computer with a simplified input procedure and table that will automatically accept and organize the input by WBS hierarchy. This change has resulted in a more flexible computer program and has significantly reduced the time previously required to organize and prepare input sheets.

√ The addition of a CTB (cost to build) capability in the cost model provides individual system/subsystem costs, with learning, over the total quantity to be produced under the option. This base figure is then used to calculate the average unit cost and the replacement capital cost per SPS if attrition prevails. An additional feature of the program categorizes the cost to construct a satellite option  $(Z_4)$  and that needed to support O&M requirements of a satellite option  $(Z_5)$  when making calculations affecting each area.

#### 4.3 RESOURCES ANALYSIS

A review of materials required for the construction of the satellite system and ground receiving station identified areas for potential investigation of material availability. These requirements should be more closely analyzed in conjunction with the characteristics of design and potential system improvements. The solar blankets and RF devices are typical examples of resource sensitive items.

#### 4.4 SPS PROGRAMMATICS

Ground-based experimental research and technology advancement programs require further definition as they relate to the Rockwell SPS reference configuration. An overall view of critical technology items should result in a technical definition, interface requirements, expected results, and an integrated schedule/network of the steps required for ultimate resolution. These "planning packages" of data should incorporate NASA decision points and coincide with NASA budget inputs.

# APPENDIX A SATELLITE POWER SYSTEM WORK BREAKDOWN STRUCTURE DICTIONARY

SOLAR PHOTOVOLTAIC GaAlAs CONCENTRATION RATIO (CR) - 2 THREE-TROUGH COPLANAR END-MOUNTED ANTENNA

# APPENDIX A SATELLITE POWER SYSTEM WORK BREAKDOWN STRUCTURE DICTIONARY

#### INTRODUCTION

Generally a work breakdown structure (WBS) is thought to be a productoriented family tree composed of all the hardware, software, services, and other tasks necessary to define the program. It offers visual display, relates project elements, and defines the work to be accomplished. The WBS is then a tool for facilitating communications and understanding a complex program by dividing this program into less complex, more manageable subdivisions or elements. It is most desirable that the WBS provide a uniform basis for management and control, cost estimating, budgeting and reporting, scheduling activities, organizational structuring, specification tree generation, weight allocation and control, procurement and contracting activities, and serve as a tool for program evaluation. Therefore, the WBS developed and defined herein is primarily tailored to the unique cost, economic, and programmatic requirements of the Satellite Power System (SPS). It is designed to allow a standard and logical format for estimating SPS project cost, while at the same time permitting cost and economic comparisons of SPS to alternate and competitive candidates for producing power.

#### WBS MATRIX

The total WBS matrix shown in Figure A-l is a three-dimensional structure that shows the interrelationship of (1) the hardware and activities dimension, (2) the accounts and phases dimension, and (3) the elements of cost dimension. This latter dimension is not further developed at this time, but is provided to show the overall expansion capability built into the WBS matrix. This dimension will become more important in later years when the SPS program approaches a Phase C/D start and is defined to the extent that the elements of cost can be planned and estimated with realism.

There is, of course, the fourth dimension of time which cannot be graphically shown but must be considered also. Each entry on the other three dimensions varies with time, and it is necessary to know these cost values by year for budget planning and approval, and to establish cost streams for discounting purposes.

While a multiple-dimensional approach may at first appear unduly complex, it actually provides benefits that far outweigh any such concern. This structural interrelationship provides the capability to view and analyze the SPS from a number of different financial and management aspects. Costs may be summed by hardware groupings, phases, functions, etc. The WBS may be used in a number of three-dimensional, two-dimensional, or single-listing format applications.

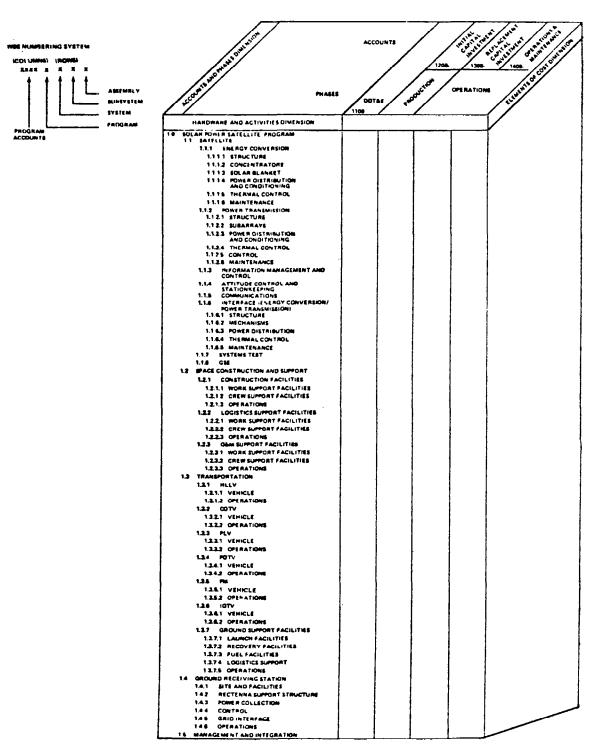


Figure A-1. Satellite Power System Work Breakdown Structure

#### ACCOUNTS AND PHASES DIMENSION

The accounts and phases dimension differs somewhat from the typical breakout for government aerospace programs in that it has been developed to also
accommodate the financial involvement of the private sector, hence, the inclusion of the breakout of financial divisions or "accounts." Distinctions have
been made between capital expenditures, which are recoverable by annual depreciation charges and are not deductible as expenses, and operation and maintenance charges against income, which are deductible as expenses in the year
incurred.

To accomplish this objective, four financial accounts have been established. Design, development, test, and evaluation (DDT&E) includes the one-time costs associated with the development of components, subsystems, and systems required for the SPS project. Initial capital investment includes the costs associated with initial procurement and emplacement of the SPS plant and equipment. Replacement capital investment includes the costs associated with capital asset replacements over the operating life of the SPS (e.g., subsystem spare parts, overhauls, etc.). Operations and maintenance (O&M) includes the costs of expendables (e.g., propellants for the propulsion subsystem thrusters), minor maintenance, repair crews, etc. The interrelationship of the financial accounts to the normal aerospace program phases of DDT&E, investment, and operations are also shown in this dimension of the WBS matrix to permit traceability to these more commonly recognized therms.

#### HARDWARE AND ACTIVITIES WBS DIMENSION

The hardware and activities WBS dimension contains hardware elements of the satellite system and ground system subdivided into subsystems and assemblies. Inherent within this dimension is the capability for further subdivision to lower levels of detail limited only by the realism of the requirements.

Required support hardware, possibly developed under the sponsorship of other programs, is also displayed here for completeness and includes such items as space construction and support equipment and transportation vehicles. Some or all of these support elements may be developed for multiple project applications. A determination will be made later as to how much, if any, of the development costs of these support elements should be charged against the SPS program.

Each of the elements of support hardware is broken out only at a summary level within the SPS WBS. However, they each have their own detailed WBS which could be displayed in depth under the SPS WBS if required.

Finally, the hardware and activities WBS dimension also includes the necessary activities of management, integration, operations, etc., required to accomplish the overall SPS missions.

#### DICTIONARY ORGANIZATION

The SPS dictionary is divided into:

- A graphic display of the three-dimensional WBS matrix (Figure A-1)
- (2) The definitions of terms of the accounts and phases dimension (pages A-5 and A-6)
- (3) The definitions of terms of the WBS hardware and activities dimension (pages A-7 through A-16)

A systematic numerical coding system coordinates the rows of the hardware and activities dimension to the columns of the accounts and phases dimension such that all matrix locations are identifiable by WBS number.

Since each matrix position corresponds to one particular row of the hard-ware and activities dimension and also to one particular column of the accounts and phases dimension, a complete definition of any matrix position is constructed by combining the definitions from the two applicable dimensions. That is, to avoid repetition, definitions are provided only once for each hardware and activities dimension row and only once for each accounts and phases dimension column, and a complete definition for any matrix position is a combination of these two definitions.

#### DEFINITIONS OF ACCOUNTS AND PHASES

1100-DESIGN, DEVELOPMENT, TEST, AND EVALUATION (DDT&E)

The DDT&E account/phase consists of the one-time costs associated with designing, developing, testing, and evaluating the components, subsystems, and systems required for the SPS project. It includes the development engineering, testing, and support necessary to translate a performance specification into a design. It encompasses the preparation of detailed drawings for system hardware fabrication, system integration, and (depending on the system, subsystem, or component) structural, environmental, and other required tests. It includes all ground tests, sortie tests, subscale and full-scale SPS tests, and all hardware fabrication required for such tests. Also included are the analysis of data and whatever redesign and retest activities are necessary to meet specifications. It also includes ground support equipment, special test equipment, and other program-peculiar costs not associated with repetitive production. All SPS related support systems such as transportation, space construction base, and assembly/support equipment necessary to accomplish the DDT&E phase are included at present for completeness. It may later be determined that some of these support systems will exist with or without SPS; therefore, they may not be chargeable to the SPS project.

#### 1200-INITIAL CAPITAL INVESTMENT

The initial capital investment account is a summation of those plant and equipment expenditures made for the initial procurement and installation of each full-scale SPS. That is, this account collects the production, assembly, installation, transportation, test, etc., costs of each individual satellite and ground station that is associated with, and necessary to, bringing the power plant online (in government aerospace terminology, this corresponds to costs in the investment phase). Examples of costs collected in this account are the procurement cost and launch cost of the satellite system itself, the procurement cost of the ground system (including installation), and all other necessary costs to achieve this end such as those attributable to space stations, launch vehicle fleets, etc. Also included is pro rata share of such functional costs as program management, SE&I, etc., related to the foregoing systems. Only costs incurred after the end of the DDT&E phase and prior to the initial operational capability (IOC) of each SPS are collected in this account.

#### 1300-REPLACEMENT CAPITAL INVESTMENT

The replacement capital investment account is a summation of those plant and equipment expenditures made for capital asset replacement and major overhauls that are expected to last more than one year and result in an improvement to the operating system. Examples of costs collected in this account are the costs of spares, their installation and associated launch costs or ground transportation costs, permanent improvements in the system such as rotary joint replacement, installation of improved design satellite control equipment, etc.,



as well as pro rata shares of functional costs. These expenditures begin at the IOC and continue over the life of each SPS.

#### 1400-OPERATIONS AND MAINTENANCE (O&M)

The O&M account is a summation of those expenditures incurred in the day-to-day operations beginning with the IOC and continuing over the life of each SPS. Examples of costs collected in this account are wages of operations and maintenance personnel, minor repairs and adjustments to systems to maintain an ordinarily efficient operating condition, expendables and consumables, launch costs for transfer of on-orbit personnel and resupply of expendables and consumables, etc.

#### DEFINITIONS OF HARDWARE AND ACTIVITIES

#### 1.0 SATELLITE POWER SYSTEM PROGRAM

The program includes all the elements of hardware, software, and activities required for the design, development, production, assembly, transportation, operations, and maintenance of the SPS program systems. Included are the satellite and ground receiving station systems, as well as the necessary support systems such as space construction and sup- t and transportation.

# 1.1 SATELLITE

This element includes the hardware and software located in geosynchronous orbit (GEO) for the collection of solar energy, conversion to electrical energy, and transmission of electrical energy in microwave form to earth.

#### 1.1.1 ENERGY CONVERSION

This element includes the components required to collect solar energy, convert the solar energy to electrical energy, condition the electrical energy, and transport it to the interface wubsystem (WBS No. 1.1.6).

#### 1.1.1.1 STRUCTURE

This element includes all necessary members to support the concentrators, solar blankets, and other energy conversion subsystem hardware. It includes structural beams, beam couplers, cables, tensioning devices, and secondary structures which are required as an interface between the primary structure and the mounting attach points of components, assemblies, and subsystems.

# 1.1.1.2 CONCENTRATORS

This element concentrates the solar energy onto the solar blanket to increase the energy density on the conversion device. It includes the reflective material and any integral attach points required for mounting. Excluded are tools and support equipment required for deployment and tensioning.

#### 1.1.1.3 SOLAR BLANKET

This element converts solar energy to electrical energy and provides power to the power distribution and conditioning buses. It includes the photovoltaic conversion cells, coverplates, substrate, electrical interconnects, and any integral attach points required for mounting. Excluded are tools and support equipment required for deployment and tensioning.

#### 1.1.1.4 POWER DISTRIBUTION AND CONDITIONING

This element includes the power conductors, switch gear, and conditioning equipment and slip rings required to transfer power from the solar blanket to the interface subsystem power distribution elements. Also included are electrical cables and harnesses required to distribute power to equipment located on

the energy conversion structure, plus batteries or storage medium for information system and attitude control. Excluded are data buses which are included in the information management and control subsystem (WBS No. 1.1.3).

#### 1.1.1.5 THERMAL CONTROL

This element includes any component used to modify the temperature of the energy conversion subsystem components. It includes oldplates, heat transfer, and radiator devices, as well as insulation, thermal control coatings, and finishes. Excluded are paints or finishes applied to components during their manufacturing sequence.

#### 1.1.1.6 MAINTENANCE

This element provides for in-place repair or replacement of components and includes work stations, tracks, access ways, and in situ repair equipment.

#### 1.1.2 POWER TRANSMISSION

This element receives dc electrical power from the interface subsystem, conditions the power, converts it to microwave energy, and radiates the energy to the ground receiving station. Included are power distributions from the interface subsystem, dc-to-RF conversion devices, control and monitoring equipment, and antenna radiating elements.

#### 1.1.2.1 STRUCTURE

This element includes all members necessary to support the transmitter subarrays and other power transmission subsystem hardware. It includes structural beams, beam couplers, cables, tensioning devices, and secondary structures.

#### 1.1.2.2 TRANSMITTER SUBARRAYS

This element includes all the hardware required for generation, distribution, phase control, and radiation of microwave energy. This includes the subarray structure, waveguides, power amplifiers, phase control electronics, and power harnesses. Also included are thermal control devices and finishes that are manufactured as an integral part of the subarray.

#### 1.1.2.3 POWER DISTRIBUTION AND CONDITIONING

This element includes the power conductors, switch gear, and conditioning equipment required to transfer power from the interface subsystem to the subarray wiring harnesses and to any other power-consuming/storage equipment located on the power transmission structure, such as batteries.

#### 1.1.2.4 THERMAL CONTROL

This element includes any component used to modify the temperature of power transmission subsystem components. It includes coldplates, heat transfer and radiator devices, as well as insulation, thermal control coatings, and finishes. Excluded are paints and finishes applied to components during their

manufacturing sequence and thermal control devices that are an integral part of another component.

#### 1.1.2.5 CONTROL

This element provides the reference phase for all subarray phase conjugating circuits. This includes the reference oscillator signal distribution and frequency conversion equipment plus components that commonly serve all subarrays.

#### 1.1.2.6 MAINTENANCE

This element provides for in-place repair or replacement of components and includes work stations, tracks, access ways, and in situ repair equipment.

#### 1.1.3 INFORMATION MANAGEMENT AND CONTROL

This element includes those components that process information on board the satellite. This includes sensing, signal conditioning, formatting, computations, formulation and signal routing.

#### 1.1.4 ATTITUDE CONTROL AND STATIONKEEPING

This element includes the components required to orient and maintain the satellite's position and attitude in GEO. Included are sensors, reaction wheels, chemical and electric propulsion hardware, and propellants.

#### 1.1.5 COMMUNICATIONS

This element includes the hardware to transmit and receive intelligence among the various SPS elements. This includes communication of both data and voice between the SPS and the control center, as well as among the various cargo and personnel vehicles. Excluded is intravehicular and intrasatellite communications.

#### 1.1.6 INTERFACE (ENERGY CONVERSION/POWER TRANSMISSION)

This element provides the movable interface between the energy conversion subsystem and the power transmission subsystem. A 360° rotary joint and an antenna elevation mechanism are required to maintain proper alignment of the transmitter with the ground receiving station. Included are structure, mechanisms, power distribution, thermal control, and maintenance hardware.

#### 1.1.6.1 STRUCTURE

This element includes all members necessary to provide a mechanical interface between the primary structures of the energy conversion subsystem and the power transmission subsystem. It includes beams, beam couplers, cables, tensioning devices, and secondary structures. Excluded are elements of the drive assembly which are included in mechanisms (WBS No. 1.1.6.2).

#### 1.1.6.2 MECHANISMS

This element includes the components required to rotate and elevate the power transmission subsystem. Included are the drive ring, bearings, gear drives and drive motors.

#### 1.1.6.3 POWER DISTRIBUTION

This element provides for the transfer of electrical power through the interface. It includes slip rings, brush assemblies, feeders, and insulation.

# 1.1.6.4 THERMAL CONTROL

This element includes any component used to modify the temperature of interface subsystem components. It includes coldplates, heat transfer and radiator devices, as well as insulation, thermal control coatings, and finishes. Excluded are paints or finishes applied to components during their manufacturing sequence.

#### 1.1.6.5 MAINTENANCE

This element provides for in-place repair or replacement of components and includes work stations, tracks, access ways, and in situ repair equipment.

#### 1.1.7 SYSTEMS TEST

This element includes the hardware, software, and activities required for ground-based systems tests including qualification tests and other development tests involving two or more subsystems or assemblies. It includes the production, assembly, integration, and checkout of satellite system hardware into a full or partial system test article. It also includes the design, development, and manufacture of special test equipment, test fixtures, and test facilities that are not included in other elements such as ground support faciliteis. Also included are the planning, documentation, and actual test operations.

#### 1.1.8 GROUND SUPPORT EQUIPMENT (GSE)

This element includes all ground-based hardware required in support of handling, servicing, test, and checkout of the satellite subsystems. It also includes special hardware required for simulations and training.

# 1.1.9 PRECURSOR TEST ARTICLE

The precursor pilot plan test article and operations are included in this element. It represents a test vehicle that consists of an energy conversion, interface, and power transmission segment.

### 1.2 SPACE CONSTRUCTION AND SUPPORT

This element includes all hardware and activities required to assemble, check out, operate, and maintain the satellite system. Included are space stations, construction facilities, support facilities and equipment, and manpower operations.

#### 1.2.1 CONSTRUCTION FACILITIES

This element includes the facilities, equipment, and operations required to assemble and check out the satellite system. Included are crew life support facilities, the central control facility, fabrication and assembly facilities, cargo depots, and operations.

#### 1.2.1.1 WORK SUPPORT FACILITIES

This element includes the facilities and equipment required for satellite assembly and checkout. Included are beam fabricators, manipulators, assembly jigs, installation and deployment equipment, and cargo storage depots. Excluded are the facilities related to crew support.

#### 1.2.1.2 CREW SUPPORT FACILITIES

This element includes the facilities and equipment required for the life support and well-being of the crew members. Included are living quarters, center control facilities, recreation facilities, and health facilities of the satellite construction base.

#### 1.2.1.3 OPERATIONS

This element includes the planning, development, and conduct of operations at the construction facility. It includes both the direct and support personnel and the expendable maintenance supplies required for satellite assembly and checkout.

# 1.2.2 LOGISTICS SUPPORT FACILITIES

This element includes the hardware, software, and operations required in low earth orbit (LEO) to support the construction and operations and maintenance of the satellite system. Included are crew life support facilities, cargo and propellant depots, and vehicle servicing facilities necessary for the receiving, storage, and transfer of cargo and personnel destined for a construction base or operational satellite located in GEO.

#### 1.2.2.1 WORK SUPPORT FACILITIES

This element includes the facilities and equipment required to provide logistics support in LEO. Included are heavy-lift launch vehicle (HLLV) and orbital transfer vehicle (OTV) docking stations, payload handling equipment, and cargo and propellant storage depots. Excluded are facilities related to crew support.

#### 1.2.2.2 CREW SUPPORT FACILITIES

This element includes the facilities and equipment required for the life support and well-being of the crew members. Included are living quarters, recreation facilities, and health facilities of the LEO Base.

#### 1.2.2.3 OPERATIONS

This element includes the planning, development, and conduct of operations at the logistics support facility. It includes both the direct and support personnel and the expendable maintenance supplies required for logistics support.

#### 1.2.3 O&M SUPPORT FACILITIES

This element includes the facilities, equipment, and operations required in GEO to support the operations and maintenance of the satellite system. Included are the on-orbit monitor and control facility and the life support facilities and equipment required to provide comfortable, safe living quarters for the resident crew members.

#### 1.2.3.1 WORK SUPPORT FACILITIES

This element includes the facilities and equipment required for operation and maintenance of the satellite system. Included are satellite monitor and control stations and any centralized repair facilities not included under maintenance (WBS Numbers 1.1.1.6, 1.1.2.6, and 1.1.6.5).

#### 1.2.3.2 CREW SUPPORT FACILITIES

This element includes the facilities and equipment required for the life support and well-being of the crew members. Included are living quarters, recreation facilities, and health facilities.

#### 1.2.3.3 OPERATIONS

This element includes the planning, development, and conduct of operations at the O&M support facility. It includes both the direct and support personnel and the expendable maintenance supplies required in GEO for satellite operations and maintenance.

#### 1.3 TRANSPORTATION

This element includes all space transportation required to support the satellite system assembly and operation; and the ground support facilities to provide a launch, recovery, propellant, logistics, and operational capability. Included are the launch to LEO and the orbit-to-orbit transfer of all hardware, materials, and personnel required during the construction and lifetime operation of the satellite system.

#### 1.3.1 HEAVY-LIFT LAUNCH VEHICLE (HLLV)

This element includes the HLLV vehicles and operations required to support the satellite system assembly and operation. Included is the launch to LEO of all space construction and support equipment, satellite system hardware, OTV's, propellants, and other consumables required throughout the satellite lifetime.

# 1.3.1.1 HLLV VEHICLE

This element includes the vehicle fleet procurement required to support the SPS project.

#### 1.3.1.2 HLLV OPERATIONS

This element includes the necessary vehicle operations (user charge per flight including payload integration) required to support the SPS project.

# 1.3.2 CARGO ORBITAL TRANSFER VEHICLE (COTV)

This element includes the COTV vehicles and operations required to support the satellite system assembly and operation. Included is the LEO-to-GEO transfer of space construction and support equipment, satellite system hardware, spares, and propellants required throughout the satellite lifetime.

#### 1.3.2.1 COTV VEHICLES

This element includes the vehicle fleet procurement required to support the SPS project.

#### 1.3.2.2 COTV OPERATIONS

This element includes the necessary vehicle operations (user charge per flight including payload integration) required to support the SPS project.

#### 1.3.3 PERSONNEL LAUNCH VEHICLE (PLV)

This element includes the PLV and cargo vehicles of the growth Shuttle and operations required to support the satellite system assembly and operation. Included is the launch to LEO and return of all personnel and priority cargo required throughout the satellite construction period and operational lifetime.

# 1.3.3.1 PLV VEHICLES

This element includes the vehicle fleet procurement required to support the SPS project. Included are the vehicles for personnel transfer from earth to LEO and for cargo transfer as needed to support elements of the precursor phase of program development.

#### 1.3.3.2 PLV OPERATIONS

This element includes the necessary vehicle operations (user charge per flight including payload integration) required to support the SPS project.

#### 1.3.4 PERSONNEL ORBITAL TRANSFER VEHICLE (POTV)

This element includes the POTV vehicles and operations required to support the satellite system assembly and operation. Included is the LEO to GEO and return transfer of all personnel and priority cargo required throughout the satellite construction and operational periods.

#### 1.3.4.1 POTV VEHICLES

This element includes the vehicle fleet procurement required to support the SPS project.

#### 1.3.4.2 POTV OPERATIONS

This element includes the necessary vehicle operations (user charge per flight including payload integration) required to support the SPS project.

#### 1.3.5 PERSONNEL MODULE (PM)

This element includes the PM units and operations required to support the satellite system assembly and operation. Included is the LEO to GEO and return transfer of all personnel and critical hardware items required throughout the satellite construction and operational periods. The PM provides a crew habitat during the orbit-to-orbit transfers of personnel.

#### 1.3.5.1 PM VEHICLES

This element includes the PM unit procurement required to support the SPS project.

#### 1.3.5.2 PM OPERATIONS

This element includes the necessary operations (user charge per flight including payload integration) required to support the SPS project.

# 1.3.6 INTRA-ORBITAL TRANSFER VEHICLE (IOTV)

This element includes the IOTV vehicles and operations required to support the satellite system assembly and operation. Included is the intra-orbit transfer of cargo between the HLLV, COTV, construction facility, logistics support facility, and operational satellites.

#### 1.3.6.1 IOTV VEHICLES

This element includes the necessary vehicle fleet procurement required to support the SPS project.

#### 1.3.6.2 IOTV OPERATIONS

This element includes the necessary vehicle operations (recurring refurbishment and propellant costs) required to support the SPS project.

# 1.3.7 GROUND SUPPORT FACILITIES

This element includes all land, buildings, roads, shops, etc., required to support the cargo handling, launching, recovering, refurbishment, and operations of the space transportation system.

# 1.3.7.1 LAUNCH FACILITIES

This element includes the design and construction of the actual launch facility and its associated equipment. Included are land, buildings, and equipment required to support the various crews. It also includes the required control centers and administrative facilities.

#### 1.3.7.2 RECOVERY FACILITIES

This element covers the design, construction, and equipping of the actual recovery facilities.

#### 1.3.7.3 FUEL FACILITIES

This element includes fuel production facilities, storage and handling facilities, transportation, and delivery and safety facilities for both the fuel and the oxidizer. Also included are the facilities for fuels used in the various orbital transfer facilities.

#### 1.3.7.4 LOGISTICS SUPPORT

This element includes the land, buildings, and handling equipment for the receiving, inspection, and storage and packaging of all payloads to be launched except for fuels and oxidizers.

#### 1.3.7.5 OPERATIONS

This element includes the planning, development, and conduct of operations at the ground support facilities. It includes both the direct and support personnel and the expendable maintenance supplies required for the ground support facilities operation and maintenance.

#### 1.4 GROUND RECEIVING STATION

This element includes the land, facilities, and equipment that comprise the ground subsystems utilized to receive the radiated microwave power beam and to provide the power at the required voltage and type of current for entry into the national power grid. Also included are the equipment and facilities necessary to provide operational control over the satellite.

#### 1.4.1 SITE AND FACILITIES

This element encompasses the site and facilities for the ground receiving station system which includes the rectenna, grid interface, and satellite control subsystems. Included are the land, site preparation, roads, fences, utilities, lightning protection, buildings, and maintenance equipment required to house and support the other ground station subsystems.

# 1.4.2 RECTENNA SUPPORT STRUCTURE

This element includes the hardware, materials (steel and concrete), and assembly operations necessary to erect the physical support for the rectenna array elements of WBS No. 1.4.3.

#### 1.4.3 POWER COLLECTION

This element includes the antenna array elements associated with the actual reception and rectification of the microwave radiation. These elements are in series and parallel as required to deliver the required output voltage and

current. Also included are those components that accept the dc power from the array elements and route, control, convert, and switch this power for delivery to power conversion stations of the grid interface.

#### 1.4.4 CONTROL

This element includes the hardware that will be used to monitor and control the satellite from the ground. Included are telemetry, tracking, communications, monitoring of microwave beam characteristics, computing phase corrections, and providing frequency standard signals for the satellite. Functional requirements provide for signal conditioning, formatting, software, computations, and signal routing.

#### 1.4.5 GRID INTERFACE

This element includes the power conversion equipment that receives the electrical power from the power collection subsystem and conditions/converts it to a high voltage dc or ac power acceptable for input into the national power grid. Also included are those components necessary to route, control, and switch this power into the national power grid.

#### 1.4.6 OPERATIONS

This element includes the planning, development, and conduct of operations at the ground receiving station. It includes both the direct and support personnel and the expendable maintenance supplies required for the ground station operation and maintenance.

#### 1.5 MANAGEMENT AND INTEGRATION

This element includes all efforts and material required for management and integration functions at the systems level and program level. It encompasses the following functions:

- a) Program Administration
- b) Program Planning and Control
- c) Contracts Administration
- d) Engineering Management
- e) Manufacturing Management
- (f) Support Management
- (g) Quality Assurance Management
- (h) Configuration Management
- (i) Data Management
- (j) Systems Engineering and Integration

This element sums all of the direct effort required to provide management control, including planning, organizing, directing, and coordinating the project to ensure that overall project objectives are accomplished. These efforts overlay the functional work areas (e.g., engineering, manufacturing, etc.) and assure that they are properly integrated. This element also includes the efforts required in the coordination, gathering, and dissemination of management information. Also included are the engineering efforts related to the establishment and maintenance of a technical baseline for a system by generation of system configuration parameters, criteria, and requirements. It includes requirements analysis and integration, system definition, system test definition, interfaces, safety, reliability and maintainability. It also includes those efforts required to monitor the system development and operations to ensure that the design conforms to the baseline specifications.

# APPENDIX B SATELLITE POWER SYSTEM COST ESTIMATING RELATIONSHIPS (CERs)

SOLAR PHOTOVOLTAIC GAALAS
CONCENTRATION RATIO (CR) - 2
THREE-TROUGH COPLANAR
END-MOUNTED ANTENNA
CONFIGURATION

## APPENDIX B SATELLITE POWER SYSTEM COST ESTIMATING RELATIONSHIPS (CERs)

#### **B.O INTRODUCTION**

This appendix contains the cost analyses and a description of cost elements that comprise the SPS program. Each item is presented in accordance with the work breakdown structure of Appendix A and is responsive to the Rockwell reference configuration defined under Exhibit C of NASS-32475 — a 3-trough planar array with an end mounted tension web antenna (Figure B-1).

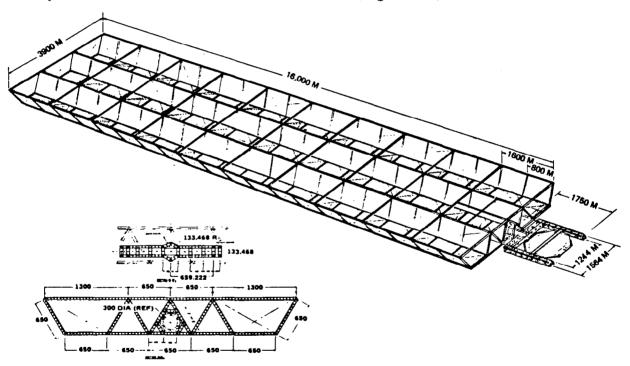


Figure B-1. SPS Reference Configuration

Subsequent sections of this appendix describe the definitions and ground rules used during the cost analysis; the methodology followed in developing estimates and the computer program; plus a detailed discussion of each subsystem, assembly, or component used in the analysis. These descriptions include design input parameters, cost estimates, scaling exponents/factors, and supporting computer program cost model equations for each of the WBS items.

#### B.1 COSTING GROUND RULES AND GUIDELINES

The following major ground rules and assumptions were used in the performance of this study:

- The SPS WBS of Appendix A was used as the structure of program hardware, activities and accounts.
- 2. Key dates of program planning:

1980 - 1985	Ground Based Exploratory Research Activities
1981 - 1987	Key Technology Program Activities
1990	Decision Point for SPS Commercialization (Phase C/D)
2000	IOC of First SPS

- 3. Costs are reported at WBS level in terms of:
  - (a) Development cost and TFU (theoretical first unit).
  - (b) Initial capital investment average cost per satellite (Satellites TFU and No. 2 through No. 60).
  - (c) Replacement capital investment (RCI) cost and operations and maintenance (O&M) cost per satellite per year.
- 4. Cost estimates are projected in 1977 dollars and maximum use was made of past SPS studies and other associated data as appropriate.
- 5. SPS build rate will be two nominal 5 GW SPS systems per year for 30 years to provide a total capacity of 300 GWs by 2030.
- 6. Overall SPS lifetime will be 30 years with minimum maintenance and no salvage value or disposition costs.
- Complete construction and assembly will occur at GEO synchronous orbit.
- 8. Calculations based on 0% launch losses.
- 9. Program management and SE&I (management and integration) are costed at 5% of all other level 2 costs.
- 10. 25% mass contingency is costed as a 15% cost contingency on items 1.1, 1.2, and 1.3 of the SPS WBS.

#### B.2 COSTING METHODOLOGY

The approach followed in developing cost estimates for the SPS Program was based on the maximum use of contract and company sponsored work. The basic Rockwell - NASA/MSFC computer cost model was expanded considerably to incorporate the requirements of a revised WBS structure (Appendix A). The data base

### Satellite Systems Division Space Systems Group Rockwell International

of existing and proved CERs was expanded by grass roots analysis and specific engineering estimates on the flight vehicles and ground receiving station to provide cost projections based on industrial/consultant experience and on similar contract effort such as those of the Rockwell Space Shuttle and Space Station programs. Costing of some WBS elements utilized previously developed data with slight modification to incorporate reference systems specifications.

There are a series of equations that were used to deal with the four basic types of cost accounts and phases of the program -- DDT&E, initial capital investment, replacement capital investment, and operations and maintenance.

The DDT&E equation (CD) estimates the cost of the design, development, and test/evaluation of WBS line items for the satellite, space construction and support, transportation, and ground receiving station, plus management and integration support. Management and integration are costed as a separate line item at 5% of all other level two costs of the WBS. Because of the gross nature of the level of information/definition on systems test and GSE (ground support equipment), the cost of system test hardware, and system test operations, has been assumed to be one-half of the satellite system first-unit costs. A 10% factor of satellite DDT&E is used for GSE.

The appropriate inputs for the DDT&E CERs are the applicable total system mass, area, or power. A development factor is provided in the equation (DF) to adjust the cost to reflect only that portion of the total system mass, area or power considered necessary for development of the complete system where it is not required to develop the total mass, area or power. The CD cost equation also allows for the application of a complexity factor (CF) to adjust the cost results when it is determined that the item being estimated is either more or less complex than the CER base data.

The initial capital investment (ICI) cost equations estimate the initial capital investment cost of hardware items as a function of their mass, area or power. The ICI cost equation is expressed in four different forms -- CLRM, CTFU, CTB, and CIPS. The CLRM (cost of lowest repeating module) equation requires that the input correspond to the mass, area or power of the lowest repeating module (M). This is necessary because of the physical scale of the SPS and the production quantities required for many of the hardware elements. It is not reasonable to estimate the SPS initial capital investment cost as a historical function of the entire SPS mass, area or power. Instead, it is desirable to cost the number of repeating modules required per satellite to establish the satellite theoretical first-unit cost (TFU), and to input the satellite TFU cost into a progress (learning) function for the quantity of satellites required to calculate the average unit cost (CTB - cost to build). This calculation involves two steps in the cost equations. The first step (CLRM) is simply the portion of the equation which estimates the theoretical first repeating module cost as discussed above. The second step (CTFU) has the progress function incorporated into the equation for the quantity of repeat modules required for the first satellite. It automatically takes into account the progress over production quantities required when calculating the cost to build an average unit over the total option quantity. This CTB calculation is then the basis of CIPS, where the number of units to construct a satellite option are divided by the option quantity and then multiplied by the

CTB. In some ICI cost equations, such as those of SPS transportation, the space vehicle has a service life that is greater than that needed to construct a single satellite. The CIPS equation provides the cost model with a needed program flexibility.

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At the current level of SPS definition, it was difficult to decide just what is a repeating module. It is often impossible to know with any certainty just what portion of the total mass is appropriate to run through the equation as a module. It is just as difficult to identify how many distinct types or designs of modules will be required for any subsystem or assembly. In such cases, the study simply assumed a module mass (or area or power) based on engineering best judgment.

Replacement capital investment (CRCI) CERs simply provide for the multiplication of the annual spares fraction (R) of each system by that system's cost to build in order to arrive at an RCI cost per satellite per year.

Operations and maintenance costs (CO&M) are estimated in terms of O&M cost per satellite per year. O&M costs include those expenditures incurred in day-to-day operations beginning with SPS initial operating capability (IOC) and continuing over the life of each satellite. They consist of wages of operations and maintenance personnel, minor repairs and adjustments to systems to maintain an ordinarily efficient operating condition, expendables and consumables, launch costs for delivery and transfer of on-orbit personnel and cargo resupply of expendables and consumables, etc.

The cost methodology seeks to account for five separate effects which influence SPS cost. These are scaling, specification requirements, complexity, the degree of automation, and production progress. Scaling refers to the relationship in cost between items varying in size, but similar in type. Economies of scale usually assure that such a relationship will not be strictly linear, but rather as size increases, cost per unit of size will decrease. The slope of this relationship is reflected by the equation exponent which results from the regression analysis of the data used to develop the cost estimating relationship.

Specification requirements have been accounted for by normalizing the CER data base to manned spacecraft specification levels using factors from the RCA Price Model. From that model, an average cost factor to adjust MILSPEC to manned spacecraft is around 1.75 for DDT&E and 1.6 for production cost. Under the assumption that some relaxation of Apollo-type specifications can be made for the SPS, a factor of 1.5 was assumed for both DDT&E and production cost. Furthermore, it was assumed that a factor of 3.0 would adjust commercial specifications to SPS requirements. Therefore, military or commercial cost data used in the CERs were adjusted upward by factors of 1.5 and 3.0, respectively.

The cost equations allow a complexity factor input to adjust the cost result when it is determined that the item being estimated is either more or less complex than the listed CER data base.

<sup>&</sup>lt;sup>1</sup>Equipment Specification Cost Effect Study, Phase II Final Report, Nov. 30, 1976, by RCA Government Systems Division



The degree of automation is accounted for in certain cost equations through an adjustment to the CER coefficient by the tooling factors given in Table B-1. The effect of tooling is dependent upon the annual production rate. Higher production rates allow harder tooling and, thus, effect cost reductions. The tooling factors are used only on those CERs which are based on historical aerospace programs with limited annual production rates. Tooling factors are not used on those CERs which are based on data already reflecting automated production techniques (e.g., the commercial electronics data for the microwave antenna CER).

AVERAGE ANNUAL PRODUCTION RATE (AAPR)	TOOLING Factor (TF)	PROGRESS FRACTION (多)
1-2	1-0	0.80
3-5	0.9	0.80
6-9	0.8	0.80
10-19	0.7	0.85
20-39	0.6	0.85
40-69	0.5	0.85
70-109	0.4	0.85
110-159	0.3	0.90
160-219	0.2	0.90
220-999	(AAPR) -0.35	0.90
1000-9999	(AAPR)-0.35	0.95
10,000	(AAPR) -4.35	0.98

Table B-1. SPS Tooling Factors

The decreasing cost effects of progress due to production process improvements or direct labor learning are accounted for through standard progress functions. Many SPS components will be mass produced in a capital intensive manner and will experience little labor learning. Other SPS hardware items, however, will be produced at very low annual rates, much in the labor-intensive manner of historical spacecraft programs, and therefore would experience learning. (Technically distinguishable from learning, but still predictable with the same form of exponential function, are the effects of production process improvement. In this model, when progress functions are used, they are meant to account for both of these effects.) A constant relationship has been assumed between the progress fraction and the annual production rate as given in Table B-1.

As required by the costing ground rules and assumptions, all CERs are in terms of 1977 dollars. The study did assume 1990 technology and 1990 supply/demand conditions which, in some cases, resulted in differential (non-general) price inflation or deflation between 1977 and 1990 being included in the CERs. Specifically, it was assumed that composite raw material prices and some electronic component prices will decrease relative to general prices while aluminum coil stock prices will increase relative to general prices. Such effects are allowed for by the CERs, but only to the extent that the expected price changes differ from expected general price changes. The CERs affected are the antenna structure CER, the power source structure CER, and the microwave antenna CER.

Definitions of SPS cost model terms and equation abbreviations are presented in Table B-2.

Table B-2. Definitions of SPS Cost Model Elements

С	- COST IN MILLIONS OF 1977 DOLLARS
CD	= DDT&E COST
CDCER	- DDT&E COST ESTIMATING RELATIONSHIP (CER)
CDEXP	- DDT&E SCALING EXPONENT
CER	= COST ESTIMATING RELATIONSHIP
CF	= COMPLEXITY FACTOR
CICER	= INITIAL CAPITAL INVESTMENT COST ESTIMATING RELATIONSHIP (CER)
CIEXP	- INITIAL CAPITAL INVESTMENT COST SCALING EXPONENT
СТВ	- COST TO BUILD AN ITEM
CIPS	- INVESTMENT PER SATELLITE COST
CLRH	- LOWEST REPEATING MODULE COST
COSM	- OPERATIONS AND MAINTENANCE COST PER SATELLITE PER YEAR
CRCI	- REPLACEMENT CAPITAL INVESTMENT COST PER SATELLITE PER YEAR
CTFU	- THEORETICAL FIRST UNIT COST
DDT&E	= DESIGN, DEVELOPMENT, TEST AND EVALUATION
DF	= DEVELOPMENT FRACTION
E	= 1.0 + LOG (PH1) ÷ LOG (2.0)
ıcı	- INITIAL CAPITAL INVESTMENT
INV. PER SAT.	- AVERAGE UNIT INVESTMENT COST (2 THRU N)
м	- MASS, POWER, AREA OF LOWEST REPEATING MODULE
#RM	- NUMBER OF REPEATING MODULES
OPS	= OPERATIONS
MaO	- OPERATIONS AND MAINTENANCE COST PER SATELLITE PER YEAR
PHE	= PROGRESS FRACTION
R	- ANNUAL SPARES FRACTION
RCT	= REPLACEMENT CAPITAL INVESTMENT COST PER SATELLITE PER YEAR
T	TOTAL (MASS, POWER, AREA) PER SATELLITE
TF	- TOOLING FACTOR
TFU	- THEORETICAL FIRST UNIT
<b>Z</b> 1	- TFU REQUIREMENT
Z2	- SPS OPTION QUANTITY
<b>Z</b> 3	- TOTAL SPS REQUIREMENT PER OPTION
Z4	- ITEMS NEEDED TO CONSTRUCT SATELLITE OPTION
25	- ITEMS NEEDED FOR ORM OF THE SATELLITE OPTION

#### B.3 SPS PROGRAM COST BREAKDOWNS

An overall cost relationship for the SPS program is shown in Figure B-2. Principal areas of SPS costing are represented to indicate the emphasis on expenditures as the program moves from one phase to the next.

Subsequent tables summarize the cost data used in developing Figure B-2. They reflect SPS-related development cost DDT&E (CD) data through the first 5-GW satellite (TFU). Table B-3 includes space construction/support, transportation

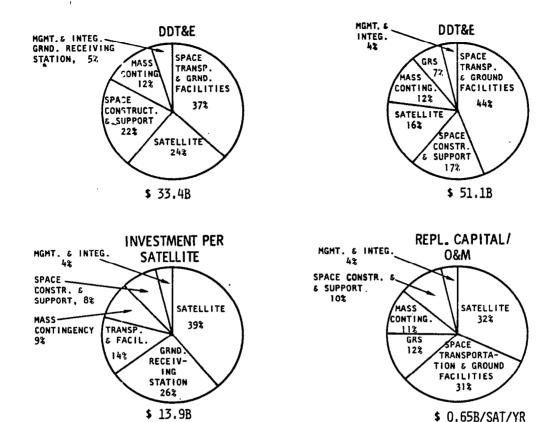


Figure B-2. SPS Cost Relationships

vehicles/operations, and the ground receiving station needed to establish SPS operational capability. This means that the TFU cost includes elements with a lifetime capability of building more than one SPS. Table B-4 summarizes the investment cost per satellite (CIPS) and the replacement capital investment cost (CRCI) plus operations and maintenance (CO&M) per satellite per year.

Table B-3. SPS Program Development Cost

	UE	VELOPMENT	
DESCRIPTION	SOTCE	TFU	TOTAL
SAFELLITE PUNER SYSTEM (SPS) PROGRAM	33-01.702	51103.2-2	84505.000
SATELLITE SYSTEM		7950.922	15894.492
SPACE CONSTRUCTION & SUPPORT	7331.100	8602.523	15933.703
THANSPURTATION	12463.316	22850.199	35335.016
GROUND RECEIVING STATION	115.699	3618.727	3734.427
MANAGEMENT AND INTEGRATION .	1392.463	2151.918	35++ . 3 82
MASS CONTINUENCY	4160.031	5912.945	10072.977
	SAFELLTIE POWER SYSTEM (SPS) PROGRAM  SATELLITE SYSTEM  SPACE CONSTRUCTION & SUPPORT  TRANSPORTATION  GROUND RECEIVING STATION  MANAGEMENT AND INTEGRATION	DOTGE	SAFELLTIE PUHEN SYSTEM (SPS) PROGRAM       33-01.702       51103.2-2         SATELLITE SYSTEM       7933.570       7950.422         SPACE CUNSTRUCTION & SUPPORT       7331.160       8602.523         TRANSPURTATION       12463.316       22860.199         GROJNO FECCIVING STATION       115.699       3618.727         MANAGEMENT AND INTEGRATION       1392.463       2151.918

Table B-4. SPS Program Average Cost

₩25 #	UESCRIPTION	INV PER SAT	104 \$40 **		AT PER YEAR TOTAL OPS	** TUTAL
1	SATELLITE PUWER SYSTEM (SPS) P	ROGRAM 13577.008	451.531	193.713	645.244	14522.910
1.1	SATELLITE SYSTEM	5325 • 422	205.265	C.755	265.470	>531.391
1.2	SPACE CONSTRUCTION & SUPPORT	1148.332	51.42a	11.274	62.701	1211.033
1.3	TKANSPUKTAT LUN	1949.00	119.343	80.869	200.212	2149.216
1.4	GROUND RECEIVING STATION	3590.622	0.275	76.377	78.652	3669.474
1.5	MANAGEMENT AND INTEGRATION	600 . 674	18.815	8.561	27.377	628.055
1.6	MASS CUNTINGENCY	1263.413	56.405	13.927	70.332	1333.745

#### B.3.1 DEVELOPMENT COST (DDT&E) AND THEORETICAL FIRST UNIT (TFU)

The total program DDT&E and TFU cost for a first full-up nominal 5-GW SPS system is \$84.5 billion. The DDT&E of \$33.4 billion and the \$51.1 billion for the TFU are detailed by SPS WBS line item in a subsequent table. Detailed DDT&E cost breakdowns show that over 60% of the DDT&E cost is identifiable to transportation and support systems, and the satellite system.

In view of the physical size of the satellite and supportive subsystems and the large quantities required for certain parts and components, it was not considered reasonable to estimate the DDT&E costs as a function of the total mass, area, or power per subsystem—which is generally the method; instead, it was considered desirable to determine the DDT&E costs by application of a development factor (DF). In general, the DF was applied on the basis of a particular system/component in conjunction with the engineering staff and as related to the program development scenario and the usage/availability of the system when needed. For example, the 335-MW EOTV precursor test article is required early in the program for MW verification. The SCB will build this unit first and the DDT&E effort on the many components must be satisfied before items can be made available. Typical items include the structure, concentrators, solar cells, power distribution, and supporting systems that are design verifications of the full-up SPS satellite. As a result of this approach, a 1.0 DF was used on components of the EOTV test article; whereas on other usages of these systems, such as on the EOTV's or similar systems of the satellite itself, a reduced factor was applied in recognition of the earlier completed DDT&E effort. This rationale was also followed in other areas of the SPS program cost analysis.

DDT&E and TFU cost breakdowns are shown in Table B-5. The TFU listing reflects a somewhat different makeup of costs when compared to the DDT&E costs. TFU estimates of \$51.1 billion include the full dollar assessment for an initial satellite and ground receiving station, include space transportation fleets; the LEO, SCB, and support assembly equipment; and the facilities needed to establish a 5-GW SPS operational capability. This means that the TFU cost includes elements with a lifetime capability of servicing/building more than one SPS system. In this regard, analysis will show that transportation and space construction and support equipment represent the largest portion of total TFU costs. However, these systems will be used to construct remaining satellites.

ROCKWELL SPS CK-2 REFERENCE CONFIGURATION E B-5. SATELLITE POWER SYSTEM (SPS) PAGGRAM DEVELOPMENT COST TABLE B-5.

			DEVELOPMENT	•
WES # DE	SCRIPTION	DDT&E	TFU	TOTAL
	SATELLITE POWER SYSTEM (SPS) PROGRAM	33401.762	51103.242	84505.000
1.1	SATELLITE SYSTEM	7933.570	7950.922	15884.492
1.1.1	ENERGY CUNVERSION	118.065	2007,983	2126,048
1.1.1.1	SIRUCTURE	71.066	104.608	67
7	PRIMARY STRUCTURE	47.821	35.100	82.921
~	SECUNDARY STRUCTURE	23.245	804.69	92,753
1.1.2	CUNCENTRATORS	ى• 0	75.637	5.6
.1.1.3	SOLAR BLANKETS	0.0	1651,832	1651,832
1.1.1.4	PUWER DIST. E. CUNDITIUNG	666 * 94	126,986	173.984
. 1 . 1 . 4 . 1	SWITCH GLAR & CONVERTERS	3.582	89.123	92.104
1.1.1.4.2	CONDUCTURS & INSULATION	6.234	9.468	15.702
1. 1. 4.3	SLIP RINGS	7,392	27.626	35 0 18
4	BATTERIES	2.001	0.338	5 • 3 3 9
1.1.4.5	BATTERY POGC	•	0.430	25.220
1.1.5	THERMAL CONTROL	J•0	0.0	0.0
1.1.6	MAINTENANCE	0.0	48.921	48.921
1.1.1.6.1	MAINTENANCE - FREE FLYERS	0.0	29.299	29 • 2 59
1. 1. 1. 0. 2	MANNED MANIPULATUR	0.0	19,203	19,203
1.1.1.6.3	TRACKS & ACCESS WAYS	0.0	0.420	0.420
1.1.2	POWER TRANSMISSION	m	3816.522	9.6
1.1.2.1	STRUCTURE	26.007	49,349	75.356
1.1.2.1.1	PRIMARY STRUCTURE		3.350	10.651
1.1.2.1.2	SECONDARY STRUCTURE	18.705	T)	4.7
1.1.2.4	TRANSMITIEK SUBARKAYS - KLYSTRONS	•	2702,309	30
1.1.2.2.1	KLYSTRUN DUTRE	å	O	S
1.1.2.2.2	KLYSTRON ICI, R, OCM	೪	.30	2702.309
1.1.2.3	PUWER DIST. & CONDITIONING	12.393	769.800	782.193
1.1.2.3.1	SWITCH GEAR & CONVERTERS	7	.33	
1.1.2.3.2	CONDUCTURS & INSULATION	5.262	5.348	
1.1.2.3.3	BATTERILS	0	12,115	12,115
•	UNIKOL	• 13	_	7.19
1.1.2.5	· PHASE	.37	20.050	20.423
. 4. 5	FREQUENCY GEN	• 10	001.0	0.200
1.1.2.5.2	. –	0.203	12.180	<b>ن</b>
1.1.2.5.3	DIST. SYSTEM, DEVICES	0.	7.776	7.840

KUCKWELL SPS CR-2 REFERENCE CONFIGURATION SALE B-5. SATELLITE POWER SYSTEM (SPS) PROGRAM DEVELOPMENT COST

WBS # DE	DESCRIPTION	DDTGE	TFU	TOTAL
1.1.2.6	MAINTENANCE	712.666	9	179.613
1.2.6.1	MAINTENANCE - FREE FLYERS	0.0	•	M
2.0.2		-	o	91,280
. 2. 6.3	ON-CRANE CUNTRUL CENTER	621,600	30,305	
4.9.	TRACKS & ALCESS WAYS	0.0	•	090.0
	INFORMATION MGMI. 6 CONTRUC	72,565	196.897	•
1.3.1	MASTER CUNIKUL COMPUTER	16,127	7.845	23.972
-2	DISPLAYS & CONTROLS	10.745	•	11.956
1.1.3.3	SUPERVISORY COMPUTER	•	2,325	5.078
4.	REMUTE CUMPUTER	2.643	•	•
3.6	BUS CONTROL UNIT	•	•	7.354
;	MICROPROCESSORS	•	- +	•
5.7	REMOTE ACQUISITION & CONTROL	•	•	8
1.1.3.8	SUBMULTIPLEXURS	•	9	6
٠. ٩. ٠.	INSTRUMENTALION	•	•	102,192
1.1.3.	OPTICAL FIBER	ċ	•	1.4
1.1.3.11		•	•	5
1.1.4	ATTITUDE CUNTROL & STATIONKEEPING	•	72.488	40
٠١.	ACSS HAKUWARE	•	•	•
	ACSS PROPELLANT	•	•	0.0
'n	COMMUNICATIONS	•	•	0.0
÷	~	•	0.0	0.0
_	SATELLITE TO RESUPPLY VEHICLES	o•0	0.0	0.0
Š	SATELLITE INTERCOM	•	0.0	0.0
<u>,</u>	INTERFACE	÷	118.500	χ
. 6. 1	STRUCIURE	35.115	76.827	٥.
.0.1.	4.1	اھ پسر	000 • 9	Ó
1.1.0.1.2	דאטנדט.	3	•	m
1.1.6.2	MECHANISMS I INTERFACE	15.225	7.878	23 - 1 03
. o .	oi jact	• !	7.003	9
.6.3.	CUNDUCTUR & INSULATION	5.178	5.068	0.2
÷ Ç.	SLIP KING BRUSHES	•	1.935	۲.
1.1.0.4	THEKMAL CUNIROL	•	ċ	0.0
		0.0	20.852	26.852
1.1.6.5.1	MAINTENANCE - FREE FLYERS	0.0		iù iù

RÜCKWELL SPS CR-2 REFERENCE CONFIGURATION SATELLITE POWER SYSTEM (SPS) PROGRAM DEVELOPMENT COST

			. UE	VELOPMENT	
	WBS # DES	DESCRIPTION	DOTEE	1FU	TOTAL
	1.1.6.5.2	MANNED MANIPULATUR	•	19.203	19.203
	1.1.6.5.3	TRACKS & ACCLSS WAYS	o•0	0.120	7
	1.1.7	1E5T	17.1	•	4.5
	1.1.7.1	STEM GROUND TEST	2662,711	0.0	2662.711
	1.1.7.2	ROUND TEST		0.0	2.7
	1.1.b		~	0.0	1.2
	•	PRECURSOR	748.653	•	7.1
	1.1.9.1	COIV PRECURSOR VEHICLE	148 %53	1737.844	5.4
	.1.9.1	PRIMARY STRUCTURE - E.C.	E98+68	*: 	1.4
	1.1.9.1.2	SECONDAKY STRUCTURE - E.C.	•	533.576	4.75
	.1.9.1.3	CONCENTRATOR - E.C.	7.869	2.817	10.686
	.1.9.1.4	SULAR BLANKET -E.C.	47.C41	60.300	107,341
	.l.>.i.5	SWITCHGLAK & CUNVERTERS -E.C.	•	$\sim$	7
		CUNDUCIORS & INSULATION - E.C.	7.048	1.431	•
B-	~	u L	12 • 190	0.63	632.823
-11	. 9. I. 8	SLIPRINGS - PRECURSOR	54.565	30.980	85.
L		TURE - IN	152.844	000.9	Ď
	.1.5.1.10	SECONDARY STRUCTURE - INTERFACE	15,155	•	19.202
	1.6.1.11	INTERFACE	а 2	221.647	5.0
	.1.9.1.12	.1	866.8	0.211	4.204
	,,,	<u>т</u>		• 1	161.4
	~	PRIMARY SIRUCTURE - POWER TRANS	20.936	•	1.1
	=======================================	TRUCTURE - FOMER	•	•	19.587
	.1.5.1.16	AYS - KLYS	0.0	141.497	141.497
	.1. %.1.1	VERTERS - P.T. PRECUR	~	۲.	57
	1.1.9.1.18	ULATION - P.		•	4.387
	1.1.9.1.19		27, 166	11.501	38.607
	.1.5.1.2	- INSULATION - PREC	'n	•	'n
	.1.9.1.2	NCE FREQUENCY GENERATOR - P	005.0	•	•
	1.1.9.1.22	DIST. SYSIEM, COAKIAL CABLE	•1	• 1	0.775
	1.1.5.1.23	• SYSTEM DEVICES	0.622	•	3
	7	SMITIER SUBAKNAYS	148.707	0.0	148.707
	1.1.5.2	PRECURSOR OPERAT	0.0	0.63	9.0
	7.5	_	331.18	602.52	33.70
	1.2.1	CONSTRUCTION FACILITIES	3653.244	6575.176	10228.422

KOCKWELL SPS CR-2 REFERENCE CONFIGURATION
TABLE B-5. SATELLITE POWER SYSTEM (SPS) PROGRAM DEVELOPMENT COST

			DEN	DE VE LOPMENT	
3	ES #	DESCRIPTION	DUTRE	150	TOTAL
	1.2.1.1	WGRK SUPPORT FACILITIES	3692,417	3956.069	7048.484
	1.2.1.1.1	BEAM MACHINE	2.000	83.150	85.150
		BEAM MACHINE CASSETTES	008 0	5.7	1
	.1.1.3	CABLE ATTACHMENT MACHINE	1.13	28.228	32.528
	. 1. 1.4	REMOTE MANIPULATOR	038•9	060.390	5
	1, 1, 5	BLANKET DISPENSER MACHINE	. eį	26.154	30 1 54
	2.1.1.6	<u></u>	008.0	9.076	9.87
	. 1.1.7	KEFLECTOR DISPENSER MACHINE	000 • 9	65	10.651
	.1.1.8	٠.	000 • 1	2.721	3.721
	1.1.	CABLE/CATENARY DISPENSER MACHINES	2.200	. 78	8
	.1.	ANTENNA PANEL INS. EUPI.		200.272	280.272
	. Z. 1. 1.	GANTRY/CHANES	13,600	3	98,634
	.2.1.1.	CARGO STURAGE DEPUIS	•	.55	S
	.2.1.1.	FAB FIXTURE	2105.128	444	7.5
I	.1.1.	AIRLOCK DOCKING MODULE (ADM)	3.0 0	30	2.3
3-3	.1.1.	DWW)	0.0	87	1213.870
<b>L2</b>	-		$\circ$		5.4
	2. 1. 1.	PRESSURIZED STURAGE MODULE (PSM)	793 • 710	805.657	1599.367
	. 2. 1. 2	CREW SUPPURT FACILITIES-SCB	•	• 29	—
	.1.2.	AIRLUCK DUCKING MODULE-ADM	31.152	3.41	104.565
	. 1. 2.	IUD ULE-CHM	0	1634-456	1634.455
	.1.2.	CONSUMABLES LUGISTICS MODULE-CLM		604.675	604.675
	7.7.		343.200	1.16	364.360
	4.1.2.	CREW SUPPURT MODULE-CSM	186.480	785.957	3
	.2.1.3		•	8.61	30
	1.2.1.3.1	OPERATIONS, CONSTRUCTION CREW	0.0	19.781	7.6
	.1.3.	UREITAL UPERATIONS, CONSI. PROV.	•	<b></b>	9
	7.	SFICS SUPPURT FACILIF	677.	.15	50
	. 4. 1	WURK SUPPORT FACILITIES	14.	7	3401.179
	. 2. į. t	BASE MEMT. MUDULE - EMM	*		5.5
	.2.1.2	MODULE-PM	50.0	.37	5.37
	. 2.2		65.9	328.782	1.72
		CREW HABITABILITY MCDULE-CHM	9	101.928	64.20
	~!	AABLES LUGIS	0.0	0.0	35.0
	1.2.4.2.3	CREW SUPPURT MUDULE/EVA	335.664	156.759	492.423

KUCKWELL SPS CK-2 REFERENCE CONFIGURATION: B-5. SATELLITE POWER SYSTEM (SPS) PRUGRAM DEVELOPMENT COST TABLE B-5.

			DE VELOPMENT	
MES #	UESCRIPTION	DUTEE	TFU	TOTAL
1.2.2.	2 UPERATIONS	•	2.182	2.182
1.2.2.	3.1 LEO OPERATIONS CREM	0.0	1.498	1.498
7.	CREW PRUVISION	•	0.684	789°0
2.3	UEM SUPPURT FACIL	0.0	0.19	0
•	I MORK SUPPORT FACILITIES	•	763.578	763.578
	AIRLOCK DOCKING M	•	44.520	44.520
.2.3	.2 BASE MGMT MUDULE-	0.0	81	8.0
.2.3.	PRESSURIZED STORA	•	408 • 244	408 . 244
1, 2, 3,		0.0	-	343 893
.5.3.	.1 AIRLOCK DOCKING MC	•	15,111	15,111
.2.3.	.2 CREW HABITABILITY MODULE-CH	•	101.928	101,928
(J)	: م	0.0	70.095	70.095
.2.3.	CREW SUPPORT MODU	•	156.759	156.759
.2.3.		•	2.727	2.727
.2.3.	.1 SATELLITE UPERATI	0 0	1,872	1,872
1.2.3.	-2	•	0.855	0.855
	<b>TRANSPORTATION</b>	468.	22866.199	35335.016
÷	SPS-HEAVY LIFT LAUNCH VEHICLE (HLLV)	8600.000	9530,492	18130,492
3.	SPS-HLLV FLEET	<b>6</b> 00.	8950.176	17550.176
1.5.1.2	SPS-HLLV UPERATIO	•	å	580.320
7.8.7	CARGO URBITAL TRANSFER VEHICLE (COTV)	31.818	•!	3657,538
3.2.		31.818	÷	3653.128
2.	۳.	3.530		13.197
5. 4.	ا انہ	•	•	2483 - 332
3.2.	'n	1.685	15.	17,563
3.2.	.4 SULAR BLANKET	•	•	5.78
3.2.	Ų	0	8.760	10.814
3.6.	. CONCOCTORS AND IN	2.205	8.584	0.7
3.2.	1.7 ACS HARDWAKE	•	762.015	771.712
1.3.2.		0.0	0.0	0.0
3. 2.	2 COTV OPERATIONS	•	•	4
7	PERSONNEL LAUNCH VEHICLE(PLV)	49.0	-	00.2
1.3.3.	I STS-PLV FLEET	1549.000	3908.082	-
٠5.	.1 STS-PLV ORBITER	•	å	82.5
1.3.3.	1.2 STS-PLV EXTERNAL TANK	O•O	606.205	606.205

ROCKWELL SPS UK-2 KEFERENCE CONFICURATIUN E B-5. SATELLITE PUWER SYSTEM (SPS) PRUGKAM DEVELOPMENT COST TABLE B-5.

			DEVELOPMENT	
WbS # DE	DESCRIPTION	<b>DDT&amp;E</b>	TFU	TOTAL
1.3.3.1.3	STS-PLV LIG. RUCKET BUOSTER	7	8	2177.985
1.3.3.1.4	ER AND		Š	96.06
1.3.3.2	J. J.		343.	343.15
•	PLV OPERATIONS	O O		1214.400
. 3. 2.	9	•	128.	128.75
4.6	PERSONNEL ORBITAL TRANS VEHICLE	50.	9	0.6 • 2
3		•	4	04.76
1.3.4.2	POIV-UPERAIIUNS	•	•	.51
•	PERSUNNEL MODULE(PM)	ဘ.		3
3.	PM FLEET	18.	ä	16.6
1.3.5.2	PM OPERATIONS	၁•0	•	ᠬ
1.3.6	INTRAURBITAL TRANSFER VEHICLE(IDIV)	•	•	05.5
.3. ć. l	IOTV FLEET	0	•	4
	IOTV UPERATIONS	•	•	G.
1.3	GRUUNU SUPPURI FACILITIES	1720.000		•
1.3.7.1		Ċ	o	3
7	RECOVERY FACILITIES	•	•	
•	FUEL FACILITIES	•	•	•
	LOGISTICS SUPPORT	0.0	•	0.0
1.3.7.5	OPERATIONS	•	•	•
1.4	GROUND RECEIVING STALTON	•	~	34.4
1.4.1	SITE AND FACILITIES	•		7
1.1	LAND AND PREPARATION	•	•	05.3
Low to low	LAND	•		0
l. l.	LAND PREPARATION	•	÷	ď
4.1.2	ROADS AND FENCES	•	. •	۲.
7	RAILS AND KUADS	•	-	73 - 7 10
4. 1.	FENCING	•	•	4.
-	UTILITIES	•	•	7
<b>.</b>	BUILDINGS	•	•	4
1.4.1	i:J	•		3
7	CUNV. STA. & MUNITUR/CUNTRUL FAC.	•	•	7
I. 5	MAINTENANCE EGPT.	•		
• 1•6 •	LIGHTNING PROTECTION	<u>ي</u>	ပ ပ	Ç
	SITE & FACILITIES UDICE	1.000	•	1.000

RUCKWELL SPS CK-2 REFERENCE CONFIGURATION TABLE B-5. SAFELLITE POWER SYSTEM (SPS) PRUGRAM DEVELUPMENT CUST

		DEN	/ELOPMENT	
WBS # UE	DESCRIPTION	<b>DDT</b> ££	TFU	TOTAL
1.4.2	RECTENNA SUPPORT STRUCTURE	2.000	1849.629	1851.629
1.4.2.1	AB.	0.0	1696.508	1696.508
1.4.2.1.1	HAT SECTIONS	0 0	359,228	359.228
1.4.2.1.2	WIDE FLANGES	o•0	295.173	295.173
1.4.2.1.3	TUBE BRACES & HAKUMARE	0.0	431,346	431.346
1.4.2.1.4	ASSEMBLY & INSTALLATION	0.0	610.762	610.762
c.	TRENCHING & CONCRETE INSTALLATION	ئ 0	153,121	153,121
1.4.2.2.1	FOOTING CONCRETE & RE-BAR	٥ <b>•</b> 0	70.821	70.821
1.4.2.2.2	MACHINGERY & EQUIPMENT	0.0	22,360	22.360
1.4.2.2.3	CONSTRUCTION OPERALIONS	٠ ٥	59.940	59.940
1.4.2.3	SUPPORT STRUCTURE DDT&E	7.000	0.0	7.000
1.4.3	POWER CULLECTION	3,000	1353,211	1356.211
å	ANTENNA AKKAY ELEMENTS	•	1127,331	1127,331
1.4.3.2	POWER DISTRIBUTION SYSTEM	0.0	099.69	099.69
1.4.3.3	INSTALLATION & CHECKOUT	0.0	156,220	156.220
1.4.3.4	POWER CULLECTION-DOTE:	3.000	o.0	3.000
1.4.4	CONTAUL	10.000	15.000	85.000
1.4.4.1	CONTROL CENTER EQUIPMENT	၁•၀	15,000	15.000
1.4.4.2	ELECTRU	0.0	000.09	000.09
1.4.4.3	CONTROL JOTEE	10.000	0.0	10.000
1.4.5	GRID INTERFACE	660.66	145.690	245,389
1.4.5.1	ELECTRICAL EQUIPMENT	9 <b>•</b> 0	145.690	145.690
1.4.5.2	GRID INTERFACE-DOTAE	669.65	•	669°66
1.4.6	UPERALIONS	<u>ي</u> 0	0.0	0.0
1.4.6.1	GRER. & MAINT. PERSONNEL	၁•0	•	0.0
1.4.6.2	MAINT. MAILLIAL	တ က		O • O
	5	1592.463	2151-918	3544 • 382
1.6	MASS CONTINGENCY	4160.031	å	10072.977

#### **B.3.2** INVESTMENT AND OPERATIONS

Detailed investment and RCI/O&M cost data are shown in Table B-6. Investment costs were developed at two levels:

- (1) Initial capital investment (ICI), which is the cost of production, assembly, installation, transportation, and tests of each individual satellite produced, and the ground station system and associated effort necessary to bring the power satellite on line to a 5-GW operational capability.
- (2) Replacement capital investment (RCI), which are those expenditures relating to capital asset replacement and major maintenance overhauls/spares that are expected to last for more than one year or result in an improvement to the operating system.

Costs for the transportation fleet needed to construct the satellites are included in the ICI; whereas, the fleet required for O&M of the satellite over the 30 years is included in the O&M cost. Replacement capital investment is included in the RCI column.

Investment per satellite is equivalent to the average unit cost of the total SPS requirement—TFU plus satellites and supporting program elements for the 60-SPS option. Total average ICI cost is projected at \$13.9 billion. Annual SPS estimates are placed at \$0.45 billion for RCI and \$0.20 billion for O&M.

ROCKWELL SPS CK-2 REFERENCE CONFIGURATION SACE COST (ABLE B-6.

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₩ b5 # DE	DESCRIPTION	INV PER SAT	** UPS (	COST PER SA OGM T	T PER YEAR OTAL OPS	** TOTAL
1	SATELLITE POWER SYSTEM (SPS) PROGRAM	13877.60	451.531	193.713		2.91
1.1	SATELLITE SYSTEM	325.4	02.50	۲.	5.97	531.39
i o l o i	ENERGY CONVERSION	851 • 6	50		15.	856-13
1.1.1.1	STRUCTURE	6.7	.13	•	• 19	86.9
-:	PRIMARY STRUCTURE	35.100	•	0.0	0.070	35.170
- 1	SECONDARY STRUCTURE	1.00	.12	•	.12	1.81
	CONCENTRATORS	7.1	.13	•	• 13	7.31
	SOLAR BLANKETS	1556.692	• 11	•	• 11	08.
1.1.1.4	POWER DIST. E_CONCITTONG	•.	•	•1	. 17	7
1.1.1.4.1	SWITCH GEAR & CONVERTERS	0.9	က	•	•	60.
1.1.1.4.2	CONDUCTORS & INSULATION	4.	•	•	•	440
4	SLIP KINGS	3	• 15	•i	51.	96
	BATTEKIES	3	•	•	•	•25
٠. د	BATTERY PD&C	4	S	•	00.	.32
Ŋ	THERMAL CONTROL	Ü	•1	•	ပ	
1.1.1.0	MAINTENANCE	0.6	.89	•	. 89	.89
1.1.1.6.1	MAINTENANCE - FREE FLYERS	3	• 58	•	. 58	16.
7.0.1	MANNED MANIPULATUR	5.1	30	•	30	500
1.1.1.6.3	TRACKS & ACCESS WAYS	0	0.001	0.0	0.001	0
<b>~</b> 1	PUWER TRANSMISSIDN	<b>₽</b>	•43	•	. 42	86
	STRUCTURE	4.1	08	•	880.0	• 26
	PRIMARY STAUCTURE	٣,	90.	•	3.	35
		40.8	.03	•	0.08	40.90
1.1.2.2	TRANSMITTER SUBARKAYS - KLYSTRONS	2	3	•	154.854	65
1.1.2.2.1	KLYSTKON ODICE	0	ċ	•	ં	o
1.1.2.2.2		2.8	•	0		77.
1.1.2.3		76.4	4	•.	4.92	933
1.1.2.3.1	SWITCH GEAR & CONVERLERS	12.5	4.17		4.17	40.72
1.1.2.3.2	S & INSULATI	3	0.0	0	0.	.1
3.3		S .	. 28	•	. 75	9.26
	THERMAL CONTRUL - INSULATION	'n	•	•	٠	500
1.1.2.5	CUNTRUL - PHASE REFERENCE	္	97.	•	.21	32
1.1.2.5.1	¥	٠ ت		0.		0.113
1.1.2.5.2	DIST. SYSTEM, CUANTAL CABLE	₹.	•	•	0	8
1.1.2.5.3	DISI. SYSTEM, DEVICES	٠.	0.259	•	•	8.029

RUCKWELL SPS CR-2 KEFERENCE CONFIGURATION E B-6. SATELLITE POWER SYSTEM (SPS) PROGRAM AVERAGE COST TABLE B-6.

			P.S	S		* TOTAL
WBS # DE	DESCRIPTION	INV PER SAT	RC I	DEM TO	TAL OPS	
1.1.2.6	MAINTENANCE	5.	.93		93	1.77
1.1.2.6.1			.57	•	.57	.36
1.1.2.6.2		0.2	CO		00	0.22
1.1.2.0.3				•		32,139
1.1.2.6.4		<u>.</u>	00.	•	00	•06
1.1.3	INFURMATION MGMT. & CCNTRUL	7	63	•	63	982
_	MASTER CONTRUL CUMPUTLR	9.	3.	•	.02	.68
.Z	DISPLAYS & CUNTRULS	•	00.	•	00.	45
ia)	SUPERVISURY COMPUTER	2	ŤÖ.	•	.01	6.97
	REMOTE CUMPUTER	•2	.02	•	. 02	.26
	BUS CONTROL UNIT	~	• 05	•	• 05	.17
1	MICKOPROCESSORS	3	5	•	05	13
.3.7	REMOTE ACQUISITION & CUNTROL	5.5	• 05		• 05	•56
.71	SUBMULTIPLEXURS	•	• 58	•	.58	9.26
	INSTRUMENTATION	5.8	• 65	•	65	50
1.1.3.10	OPTICAL FIBER	: ) •	<u>o</u>	•	99	0.58
	CAB LE S/HAKN ESS	0.9	• 16	•	• 16	•20
1.1.4	ATTITUDE CONTROL & STATIONKEEPING	7	53	•	• 66	41
1.1.4.1	ACSS HARDWAKE	3.7	• 53	• 04	. 58	5
1.1.4.2	ACSS PROPELLANI	0	•	•	9	80,
1.1.5	COMMUNICATIONS	•	• 1	•		-
1.1.5.1	SATELLITE TO GROOND	•	•	•	•	_
1.1.5.2	SATELLITE TO RESUPPLY VEHICLES	၁• ပ ပ	ာ• 0	0.0	0.0	0.0
1.1.5.3	SATELLITE INTERCOM	ان	• !	•	•	0
1.1.6	INTERFACE	<b>.</b> 92	• 15	•	m	16
1.1.6.1	STRUCTURE	8.80	• 13	•	• 13	66
6.1.	PRIMARY SIRUCTURE	00.	नं ए	•	<b>TO</b> •	10
1.1.6.1.2	SECONDARY STRUCTURE	• 36	. 12	•	.12	86
1.1.6.2	MECHANISMS - INTERFACE	82	50.	•	. 13	95
1.1.0.3	FUWER DISTRIBUTION	5	•	•	0	6.524
1.1.0.5.1	CONDUCTUR & INSULATION	90.	٥.	•	0	• 0 6
1.1.6.3.2	SLIP KING BRUSHES	1 4 4	•	•	•	.45
1.1.6.4	THERMAL CONTROL	တ <u>ု</u> ပ	•	•		Ö
1.1.6.5		21.738	• 94	•	•	•
1.1.0.5.1	MAINTENANCE - FREE FLYERS	.44	0.642	•	0.642	90.

ROCKWELL SPS CK-2 REFERENCE CONFICURATION SALL B-6. SATELLITE POWER SYSTEM (SPS) PROGRAM AVERAGE COST

MBS # DE	DESCRIPTION	INV PER SAT	** 0PS C RC1	UST PER SA	T PER YEAR OTAL UPS	** TOTAL
6.5		15 - 198	.3	0.0	0.304	.50
1.1.6.5.3	4.3	0.120	Ģ	0.0	ō	0.120
1.1.7	SYSTEMS TEST	0.0	0.0	0.0	0	0
1.1.7.1	SROUND TEST HA	0.0	0.0	0.0	o•0	0.0
1.1.7.2	SYSTEM GROUND TEST OF ERATIONS	0.0	0.0	0.0	0.0	0.0
1. l. u	GROUND SUPPORT ECUIPMENT	0	0.0	0.0	0.0	0.0
٠,	COTV - PRECURSUR	0.0	0.0	0.0	•	0.0
1.1.7.1	COIV PRECURSOR VEHICLE	0.0	0.0	0.0	0.0	0.0
1.1.9.1.1	PKIMAKY SIRUCIUKE - E.C.	ن 0	0.0	0.0	0.0	0.0
1.1.9.1.2	SECONDARY STRUCTURE - E.C.	0.0	•	0.0	0.0	0.0
1.1.9.1.3	CONCENTRATUR - E.C.	0.0	0.0	0.0	0.0	0.0
1,1,9,1,4	SOLAR BLANKET -E.C.	0.0	0.0	0.0	0.0	0.0
1.1.5.1.5	SWITCHGEAR & CONVERTE	0.0	0.0	0.0	0.0	0.0
1.1.5.1.6	CONDUCTURS & INSULATION - E.C.	ئ. د	•		•	0.0
1.1.9.1.7	ACS HARDWAKE - E.C.	0	0	0.0	0.0	0.0
1.1.9.1.8	SLIPRINGS - PRECURSOR	0	•	•	•	0.0
1.1.9.1.9	PRIMARY STRUCTURE - INTERFACE	J. 0	•	0.0	0.0	0.0
1.1.9.1.10	SECUNDARY STRUCTURE - INTERFACE	0.0	0•0	0.0	0.0	0.0
9.1.1	MECHANISMS - INTERFACE	၁• ၁	•	•	•	0.0
1.1.9.1.12	CONDUCTURS & INSULATION	J.0	၁•့	•	•	0.0
1.1.9.1.13	SLIPRING BRUSHES - PRECURS	•	ر ن ن	•	0.0	0.0
1.1.9.1.14	PRIMARY STRUCTURE - POW	•	•	•	•	0.0
1.1.9.1.15	SECONDARY STRUCTURE - POWER TRAN	0.0	0.0	0.0	•	0.0
1.1.9.1.10	TRANSMITTER SUBAKKAYS - KLYSTRONS I	•	0.0	•	•	0.0
1.1.9.1.17	SWITCHGEAR & CONVERTERS - P.T. PR	•	•	٠	0.0	0.0
1.1.9.1.18	CONDUCTORS & INSULATION - P.T. PREC	0.0	ن ن ن	٠	0.0	0.0
1.1.9.1.19	BATTERIES - P.I. PRECORDUR	ပ <b>ု</b> က	٠ ٥	•	•	0.0
1.1.9.1.20	THERMAL CONTROL - INSULATION - PR	•	•	0.0	•	0.0
. 9. 1. 2	REFERENCE FREQUENCY GENERATOR - PRE	0.0	o•0	•	•	•
1.1.7.1.22	DIST. SYSTEM, COAXIAL CABLE	0	၁	<b>ن</b> ت	0.0	0.0
•		0.0		G•0	0.0	
. 5.1.2	TRANSMITTER SUBAKKAYS - KLYSTRONS DU	<b>ာ</b> ဇ	0.0	o• o		0.0
1.1.4.2	Ę	਼	် (	•	<u>ن</u>	: ز
	SPACE CONSTRUCTION & SUPPORT	1148.332	4.	11.274	<b>7.1</b> 0	
1.2.1	CONSTRUCTION FACILITIES	123.606	19.081	11.274	30.355 ,	153,961

KUCKWELL SPS CK-2 REFERENCE CONFIGURATION TABLE B-6. SATELLITE POWER SYSTEM (SPS) PRUGRAM AVERAGE COST

WBS # DE	DESCRIPTION	INV PER SAT	** OPS C RCI	COST PER SA'	T PER YEAR **	TOTAL
	MORK SUPPURE FACILITIES	66 • 625	13.784	10 G	In a	00
1.2.1.1.2	BEAM MACHINE CASSETTES	0	• -		60	0.188
	шı	. 4	· (C)	, <b>~</b>		.61
1.4	REMOTE MANIPULATOR	6	0.036	6	96.	44.
. 2. 1. 1. 5.	BLANKET DISPENSER MACHINE	4.	•	7	18	64
.2.1.1.6	SULAR BLANKET CASSETTES	2	000 • 0		11.	•38
1.1	REFLECTUR DISPENSER MACHINE	0	•	•	.04	.12
.2.1.1.3		0	•	0	<u>•</u> 05	\$0.
1.2.1.1.9	CABLE/CATENARY DISPENSER MACHINES	<b>.</b>	•		. 16	•54
1.2.1.1.16	ANTENNA PANEL INS. EL	4	•	7	• 75	•0•
1.2.1.1.11	GANTRY/CRANES	4	•	9	09	100
1.2.1.1.12	CAKGU STUKAGE DEPUTS	7	•	•	99.	•72
1.2.1.1.13	FAB FIXIURE	۳,	•	•		7
1.2.1.1.14	AIRLOCK DOCKING MODULE (ADM)	0	S.S.	•	. 28	•32
1.2.1.1.15	BASE MGMT. MODULE (BMP	0.2	•	•	90.	6.30
1.2.1.1.16	POWER MODULE (PM)	7.9	.37	•	.37	3.30
1.4.1.1.17	PRESSURIZED STORAGE MODUL	4.	5	•	10.	44.
1.2.1.2	CREW SUPPORT FACILITIES-SCB	3.1	2.297	•		8.46
1.2.1.2.1	AIRLOCK DOCKING MODULE-ADM	1.2	67.	•	• 29	1.51
1.2.1.2.2	F-CHM	7	. 92	•	<u>.</u> 92	• Î •
1.2.1.2.3	CONSUMABLES LOGISTICS MODULE-CLM	0.0	• 34	•	•34	1.42
	SHIELDING	6	• 02	•	• 02	.37
VI I	CREW SUPPORT MODULE -C SM	3	17	•	.71	5.98
w.	OPERATIONS	4.	•	•	0	•41
. 3.1	VST FUCT 10N CR	χ.	•	•	•	68.
1.2.1.3.2	NST. PRUV.	3	၀.	•	0	15
.2.2	STICS SURPORT FACILIFIE	ί.	• 29	•	•29	4.64
. 7	WURK SUPPORT FACILITIES	٠,	. 72	•	. 72	64.
1.2.2.2.1	BASE MGMT. MUDULE-BAM	-	.21	•	.21	1.39
7	POWER MUDOLE-PM	Š	.55	•	. 50	<b>50</b> 0
.2.2.2	S S	4	.57	•	.57	2.05
. 2.2.	<u>.</u> Ц	Ò	• G3	•	• 03	<u>. 73</u>
1.2.2.2.2			1.402	•		.57
1.2.2.2.3	CREW SUPPURT MUDULE/EVA	ç	• 13	•	• 13	•74

RUCKWELL SPS CR-2 REFERENCE CONFIGURATION B-6. SATELLITE POWER SYSTEM (SPS) PROGRAM AVERAGE COST 1ABLE B-6.

\*\* OPS CUST PER SAT PER YEAR \*\* TOTAL

1

WbS # DE	SCKIPTION	INV PER SAT	KC I	T M30	OTAL OPS	
2.3	OPEKA110NS	1.091	•	0.0		60.
3.1	LEO DPERATIONS CREW	0.749	•	0.0	•	0.749
N	LEO CREW PROVISIONS	0.342	•	0.0	•	•
5.5	U&M SUPPURT FACILITIES - SATELLITE	38.3	9	0.0	14.047	1022,433
5.1	WORK SUPPORT FACILITIES	.18	.77	0•0	.77	6.66
7	AIRLOCK DOCKING MODULE-ADM	5	• 26	0.0	• 26	40,323
3.1.5		83.32	.66	0.0	• 66	86.88
2.3.1.5	~	38.	1.844	0.0	. 84	370.649
2.3.2	-	13.47	6.273	0	6.270	319.745
2.3.2.1		13.77	.27	0.0	.27	40.4
7.7	JULE-CH	2.91	•	0.0	1.858	4
2.3	1.7	68	1,278	0.0	.27	65.173
2.3.2.4	: 41	2.B	.85	0.0	2.858	5.7
1.2.3.3		2.727	0.0	0.0	•	2.727
1.5	SATELLITE UPERATIONS CREW	• i	•1	0	•	1.872
1.2.3.3.2	SIONS		•	0.0	•	0.855
<b>1</b>	TRANSPORTATION	9.0		86	00.21	49.2
ان. م	SPS-HEAVY LIFT LAUNCH VEHICLE (HLLV)	5.4	79.642	ന	9.01	39
3.1.1	SPS-HLLV FLLET	٦.٧	9.64	3	23.89	8
1.2	SPS-HLLV UPEKATIONS	469.367	o•9	7	5.11	504.502
3.2	CARGO ORBITAL FRANSFER VEHICLE(COTV)	() ()	. 55	5	32	18.67
3, 2, 1		5.6	55	23	•19	13.87
<b>-</b>	PRIMARY STRUCTURE	ð	•	0.017	0	Ď
3.2.1.2	SECUNDARY STRUCTURE	1	36	نان: ال	69.	663
3,2,1,3	CONCENTRATOR	0.914	$\circ$	20	. 03	0.951
3.2.1.4	SULAK BLANKEI	္	• 19	2	• 8C	.87
3.2.1.5	SWITCHGEAR AND CONVERTERS	1	00.	Ğ	10	48
3.2.1.6	CONDUCTORS AND INSULATION	3	00•	7	.01	54
3.2.1.7	ACS HAKUWAKL		• Зн	2 1	99.	08.
3.2.1.8	INFO. MGMT. AND CUNTRUL	);  -	• 1	o	•	•
3.2.2	COTV OPERATIONS	.66	•	23	. 13	.80
	SONNE	.75	12.995	5	5.42	19.69
.5.	7 J d-	a8 <u>•</u> 43	44	40	*C •	~
1.5.3.1.1	<u>.</u>	100.340	5.197	8.250	4.0	-
1.3.3.1.2	STS-PLV EXTERMAL TANK	.67	٠	3		
			•			

KUCKWELL SPS CK-2 REFERENCE CONFIGURATION TABLE B-6. SATELLITE POWER SYSTEM (SPS) PROGRAM AVERAGE COST

WBS # DE						
		INV PER SAT	KC I	) L W30	UTAL OPS	
. 3. 1.3	STS-PLV LIQ. RUCKET BOOSTER	3.99	1 .		1 -	3.65
1.3.3.1.4	SIS CARGU CARRICR AND EM		ပ <b>ု</b>	_	-	•
	PLV & STS-HLLV UP LRAT IONS	5.31	لم	B	88	54.20
3.2.1	PLV UPERATIONS	16.50		•	_	5.38
	STS HELV CAKGO OPERATIONS	8.81		•	0	8.81
1.4.4	PERSONNEL URBITAL TRANS VEHICLE	48	13	25	66	47
٠,	POTV-FLEET	C R	7	814	92	.72
4.6	PUIV-OPERATIONS	. 6ê	•	•	-	.75
v	PERSONNEL MODULE(PM)	67		12	32	10
5.1	PM FLEET	7.	19	.07	.27	01
N.	PM OPERATIONS	10.		0.5	60	.59
,	INTRAURBITAL TRANSFER VEHICLE (IDTV)	47	.26	404	31	18
	10TV FLEET	38	•	40.	30	69.
6.2	IOTV OPERATIONS	•0°		00	00	.08
1.3.7	GROUND SUPPORT PACILITIES	* 1.55	•	7	32	57
7.1	ES	0	0	•	0	0
	RECUVERY FACILITIES	•		•	•	•
ر. ادي	FUEL FACILITIES		• (		- 6	
7.4	ĸ.	•		•	•	0.0
7.5		•		•		•
1.4	GROUND RECEIVING STATION	8 · C				14.69
1.4.1	IND FACIL	88.9	• 20	•	. 20	.13
1.4.1.1	LAND AND PREPARATION	7.6	•	•		11.
1.4. 1. 1. 1		5.0	•1	•	•	000
1.4.1.1.2	LAND PREPARATION	64.119	0.0	0.0	0.0	64.119
1.4.1.2	KDADS AND HENCES	4.1	٠	•	•	.13
1.2.	KAILS AND KUADS	7 = 6	•	•	•:	<u>-</u> 1
1.4.1.2.2	FENCING	4.	•	•		•42
1.4.1.3	UTILITIES	-5		•	•	•20
• 4•	BUILDINGS	4	• 1	•	• 1	14.
<b>:</b>	GE+MAINTENANCE	٠,٠	•	•		•30
1.4.1.4.2	CUNV. 51A. & MUNITUR/CUNTRUL FAC.	٦.	•	•	•	.17
1.04 0 1.0 E	MAINTENANCE ENPT.	000.4	•	•	•:	<u>.</u> 20
₹.	LIGHTNING PROTECTION	•	•	•	•	•
1.4.1.7	SITE & FACILITIES DUTWE	•	•	•	o • •	•

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION TABLE B-6. SATELLITE POWER SYSTEM (SPS) PROGRAM AVERAGE COST

	: !		** UPS C	COST PER SAT	PER YEAR	** TOTAL
WBS # DE	DESCRIPTION	INV PER SAT	KC1	06M TOTA	TAL OPS	
1.4.2	RECTENNA SUPPURT STRUCTURE	1827.949	0.075	0.447	0.522	1828.521
1.4.2.1	STEEL PANEL FAB. & INSTALLATION	1696.493	o•0	•	0.0	1696.493
1.4.2.1.1	HAT SECTIONS	359.224		0.0	0.0	359.224
1.4.2.1.2	MIDE FLANGES	295.170	0.0	•		295.170
1.4.2.1.3	TUBE BKACES & HARDWAKE	431,343	o•0	0.0	0.0	431.343
1.4.2.1.4	ASSEMBLY & INSTALLATION	610.756	0.0	0.0		610.756
1.4.2.2	TRENCHING & CONCRETE INSTALLATION	Å,	0.075	144.0	•	
1.4.2.2.1		g. C	•	0.0	•	70.820
1.4.2.2.2	MACHINGERY & EQUIPMENT	0 • 745	•	144.0	•	1,267
1-4-2-2-3	CONSTRUCTION OPERALIONS	3.	0.0	0.0	•	69.940
1.4.2.3	SUPPORT STRUCTURE DDT EE	ပ <b>့</b> 0	•	0.0		0.0
4.4.3	POWER CULLECTION	1353 - 200	el.	0.0	•	1353.200
1.4.3.1	ANTENNA AKKAY ELEMENTS	1127.321	•	o• o	•	1127,321
1.4.3.2	POWER DISTRIBUTION SYSTEM	69 • 69	•	•	•	69 • 69
1.4.3.3	INSTALLATION & CHECKOUF	156.220	•	0.0	O • O	156.220
1.4.3.4	ULLECTION-DUTS	G.	•	0.0	•	0.0
1.4.4	CONTRUL	15.000	0.0	0.0	•	75.000
1.4.4.1	CONTRUL CENTER EDUIPMENT	15.000	•	•	0.0	000-41
1.4.4.2	CONTROL ELECTRUNICS	000°C9	•	0.0	•	000-09
1.4.4.3	CONTROL DDISE	0.0	•	•	0.0	0.0
1.4.5	GRID INTERFACE	49.	•.		•	145,690
1.4.5.1	ELECTRICAL EQUIPMENT	145.690	•	0.0	•	145.690
1.4.5.2	GRID INTERPACE-DUIGE	•	•	0.0	0.0	0.0
,	OPERATIONS	J• 0	•	77.930	77,930	77.930
	OPER. & MAINT. PERSONNEL	•	•		<b>.</b>	080
1.4.6.2	MAINT. MATERIAL	•	•	13,130	13,130	13,130
1.5	MANAGEMENT AND INTEGRATION	619.009		8.561	27,377	628,055
l•o	MASS CONTINGENCY	1263.413	56.405	2	70.332	1333.745

#### 1.0 SATELLITE POWER SYSTEM (SPS) PROGRAM

The program elements described in this section include all the elements of hardware, software, and activities required for the design, development, production, assembly, transportation, operations and maintenance of the Satellite Power Systems Program. Included are the satellite and ground receiving station systems as well as the necessary support systems such as space construction and assembly equipment, plus transportation.

Cost estimates are presented for DDT&E, Theoretical First Unit (TFU), investment per satellite, replacement capital investment, and operations/maintenance for SPS program elements in the following categories:

- Satellite
- · Space Construction and Support
- · Transportation
- · Ground Receiving Station
- · Management and Integration
- · Mass Contingency

#### 1.1 SATELLITE

Elements of the satellite costed in this section include the hardware and software located in geosynchronous orbit for the collection of solar energy, its conversion to electrical energy, and the transmission of this electrical energy in microwave form to earth.

The satellite concept is of a planar array using GaAlAs photovoltaic cells with a solar reflector (concentrator) to provide a concentration ratio of 2.0 suns. The concept consists of 3 main bays with 10 subsections in each of the main bays and is 16,000 meters long by 3900 meters wide with an end mounted antenna adding another 1750 meters to the length (Figure 1.1-1). The total dry weight of the satellite is 26.416×10<sup>5</sup> kg (Table 1.1-1). It has a primary structure of composites, GaAlAs solar cells, and a microwave antenna using the klystron power module as a source for the generation of MW energy.

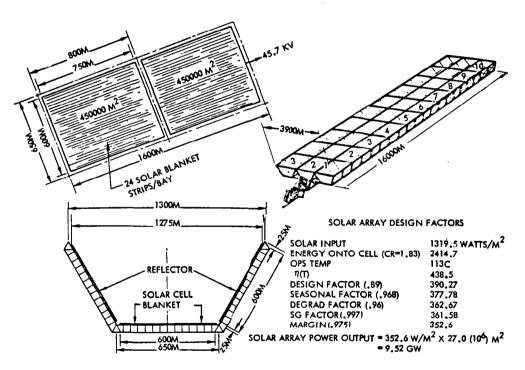


Figure 1.1-1. Solar Array Dimensions

The satellite has been divided into a number of main elements that are included in the following items as described in the SPS-WBS of Appendix A.

- 1.1.1 Energy Conversion
- 1.1.2 Power Transmission
- 1.1.3 Information Management and Control

- 1.1.4 Attitude Control and Stationkeeping
- 1.1.5 Communications
- 1.1.6 Interface
- 1.1.7 Systems Test
- 1.1.8 Ground Support Equipment
- 1.1.9 Precursor Test Article

Table 1.1-1. Solar Photovoltaic Power Conversion Mass Statement -  $\sim 10^5$  kg End-Mounted Antenna

SUBSYSTEM	CO-PLANAR (3 TROUGH)
COLLECTOR ARRAY	
STRUCTURE AND MECHANISMS	1.260
PRIMARY STRUCTURE	.702
SECONDARY STRUCTURE	. 358
MECHANISM	.200
ATTITUDE CONTROL	(0.116)
POWER SOURCE	(7.855)
SOLAR PANELS	6.818
SOLAR REFLECTORS	1.037
POWER DISTRIBUTION AND CONTROL	(2.603)
POWER CONDITIONING EQUIPMENT	(.193)
POWER DISTRIBUTION	(2.410)
CONDUCTORS AND INSULATION	(2.367)
SLIP RINGS	.043
INFORMATION MANAGEMENT & CONTROL	(.050)
DATA PROCESSING	.021
INSTRUMENTATION	.029
TOTAL ARRAY, DRY	11.884
ANTENNA SECTION	
STRUCTURE & MECHANISM	(0.977)
PRIMARY STRUCTURE	.120
SECONDARY STRUCTURE	.599
ANTENNA	.067
MECHANISH	.191
THERMAL CONTROL	1.408
KLYSTRON COOLING	.851
INSULATION	.557
RADIATOR	-
MICROWAVE POWER	(7.012)
KLYSTRONS	4.250
ATT. SEN. ELECTRONICS & PHASE CONTROL	.142
WAVEGUIDES	2.620
POWER DISTRIBUTION & CONTROL	(4.505)
POWER CONDITIONING EQUIPMENT	1.901
POWER DISTRIBUTION	(2.604)
CONDUCTOR & INSULATION	(2.587)
SLIP RING BRUSHES	.017
INFORMATION MANAGEMENT & CONTROL	(.630)
DATA PROCESSING	.380
INSTRUMENTATION	.250
TOTAL ANTENNA SECTION	14.532
TOTAL SPS DRY	26.416

#### 1.1.1 ENERGY CONVERSION

This element includes the components required to collect solar energy, convert the solar energy to electrical energy, condition the electrical energy, and transport it to the interface subsystem (WBS No. 1.1.6).

The satellite structure, solar cells/blankets, concentrators, and power distribution/conditioning subsystems are included in this element plus the necessary maintenance requirements to support operations.

#### \_ 1.1.1.1 STRUCTURE

This element includes all necessary members to support the concentrators, solar blankets, and other energy conversion subsystem hardware. It includes structural beams, beam couplers, cables, tensioning devices, and secondary structures which are required as an interface between the primary structure and the mounting attach points of components, assemblies, and subsystems.

#### 1.1.1.1.1 Primary Structure

The primary SPS structure assemblies are made up, basically, of tribeam girders, tension cables, and joints. The fabrication and assembly of these structures are accomplished on orbit by beam machines and supporting auxiliary equipment. These structural elements are made of a graphite fiber reinforced composite that must individually withstand the forces, torques, and dynamics imposed by the construction process. Once built into an assembly level, the structure must have sufficient strength and stiffness to withstand the forces of the environment (gravity-gradient torques), the attitude control system (forces and frequencies), and the operational equipment (rotary jointsk microwave induced thermal environment).

The SPS requirement for low thermal distortion, under high thermal stress, dictates the need for a material with a very low coefficient of expansion. The most likely candidate, at this time, is a graphite composite material.

The energy conversion structure D&D CER was developed using graphite composite data obtained from NASA's Redstar Data Base. Tooling cost was excluded under the assumption that this cost would be incurred in the development of orbital fabrication equipment. The following data points were used:

- · Space Telescope Shell
- · ATS-F Truss
- HEAO Optical Bench
- · Shuttle Payload Bay Doors

The primary structure ICI is the cost of raw materials only since the costs associated with fabrication and assembly are charged against orbital assembly and support equipment. The structure ICI cost equation is based on raw composite material stock (prepregnated graphite) cost. These material costs are based on vendor quotes obtained from Hercules, Fiberrite and Union Carbide.

Range of Data

D&D: 30.0 to 2000.0 kg

ICI: Unlimited

#### 1.1.1.1.2 Secondary Structure

The secondary structure consists of the passive interface attachment between the primary structure and operational subsystems. The structural members are made of aluminum with the ability to articulate, rotate, or otherwise support/allow motion between the primary structure and other subsystem elements.

This element includes all structure, consisting of mounting brackets, clamps and installation structure required as an interface and mounting attach points of components, assemblies, and subsystems. It also includes any structure required between two or more components or assemblies.

Development of the secondary structure CER for DDT&E was based on cost data contained in the MSFC Redstar Data Base. Data from a variety of launch vehicle and unmanned satellite programs were available and the applicable data points are listed below:

- S-IVB Interstage
- S-IC Forward Skirt
- X-IC Intertank
- Solar Telescope Housing Assembly (ASM)
- Common Mount Assembly ASM)
- Telescope Gimbal Assembly (ASM)
- Common Mount Actuators (ASM)
- Telescope Gimbal Actuators (ASM)
- Array Platform Elevation Pointing Actuator (ASM)
- UV Gimbal Mount Actuators (ASM)
- UV Instrument Mount Assembly (ASM)
- Solar Array and Boom Structure (ATS-F)
- Squib Interface Unit (ATS-F)
- Interstage (Centaur)
- Nose Shroud (Centaur)
- · Fixed Airlock Shroud (Skylab)
- Payload Shroud (Skylab)
- Pallet Segment (Spacelab)
- OSO-1
- · ATS-F
- · S-II

The ICI production cost CER was based upon an Engineering Cost estimate.

#### Range of Data:

DDT&E: 6.0 to 15,000.0 kg ICI: 6.0 to 15,000.0 kg

Input parameters T&M are in kilograms of mass.

#### 1.1.1.1.3 Cost Estimates

Table 1.1.1.1.1 and 1.1.1.1.2 cover cost estimates associated with the primary and secondary structures.

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.1.1.1 PRIMARY STRUCTURE TABLE

		INPUT P	INPUT PARAMETERS			INPUT CO	INPUT COEFFICIENTS
	Ţ=	702000.000	_ <del> </del>	1.000000		CDCER=	0.023000
	# <u></u>	11700.0000	=W30	0.0		COEXP=	0.800000
	CF.	1.000000	<b>-17</b>	1.000000		CICER=	0.000050
	PH I=	1.000000	12=	000000*09		CI EXP=	1.000000
	<b>R</b> =	0.002000	73=	900000009			
	DF=	0.02000	= 7 7	60.00000	= 57	0.0	
	CALCU	CALCULATED VALUES	KG	SUM TO 1.	1.1.1.1		S, MILL IONS
<b>3</b> ,	CD=CDCER X	CD=CDCER X (T X OF 1XX(CDEXP)	X CF		:	!	47.821
Ç	CLRM=CICER	CLRM=CICER X (M)XX(CIEXP) X C	CF X TF				0.585
	#RM =T / M						60.000
-31	E = 1.0 +	=1.0 + LOG(PHI) / LOG(2.0	• 0)				1,000
J	ST FU= (CLRM	CTFU=(CLRM / E)X((#RM X Z1+.5)XX(E)		-0.5XX(E))			35.100
	CTB = ((CLRM/E)X((#RM	×	23 + 0.5) XX(	0.5)XX(E) -0.5XX(E))		1 / 23	35.100
·	CIPS=CTB*Z4/22	4/12					35.100
	CRCI	=CTB X R					0.070
	CCEM =	CCEM = 0EM OR CTB*25/22/ENYR	/ENYR				0.0
٠	COMMENTS				1 1		

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION I.1.1.1.1.2 SECONDARY STRUCTURE TABLE

	:	INPUT PARA	ARAMETERS			IN I	UT CO	INPUT COEFFICIENTS
	<u>"</u>	358000.000	<b>=</b> 4₽	0.007300		CDC ER=		0.156000
	- X	5.000000	0£M=	0.0		CDEXP=		0.511000
	C F=	1.000000	<b>-17</b>	1.000000		CI CER=		0.101000
	PH I=	0.980000	2 2=	60.00000		CI EXP=		0.355000
	R=	0.002000	73=	60.00000				
	DF=	0.00050.0	<b>2</b> 4 =	000000:09	= 57		0.0	·
	CALCU	CALCULATED VALUES	KG	SUM TO 1.	1.1.1.1			S, MILL IONS
	CD=CDCER X	CD=CDCER X (T X DF)XX(CDEXP)	X CF			,		23.245
	CLRM=CICER	X (M)XX(CIEXP)	X CF X TF				•	0.001
	#RM =1 / M							71600,000
	E =1.0 +	=1.0 + LOG(PHI) / LOG(2.0)	.0)			. !		0.971
B-32	CTFU=(CLRM	CTFU=(CLRM / E)X((#RM X Z1+.5)	XX(E)	-0.5XX(E))				805.69
	CTB = ((CLRM/E)X((#RM	×	Z3 + 0.51XX(	0.5)XX(E) -0.5XX(E))		1 / 23		61.689
	CIPS=CTB*24/Z2	4/12			1		i !	689*19
	CRCI	=CTB X R						0.123
	= W300	COEM = OEM OR CT8*25/22/EN	/ ENYR					0.0
	COMMENTS		: : : :		!			



#### 1.1.1.2 CONCENTRATORS

This element concentrates the solar energy onto the solar blanket to increase the energy density on the conversion device. It includes the reflective material and any integral attach points required for mounting. Excluded are tools and support equipment required for deployment and tensioning.

Concentrator membranes are used to reflect the sun onto the solar cell surfaces and obtain a nominal concentration ratio of 2. The concentrator is made of (0.5-mil) aluminized Kapton. The membrane has a mass of 0.018 kg/m² and is mounted on the structure using attachments and tensioning devices. Excluded are tools and support equipment required for deployment.

The DDT&E CER (CD) is based on thin sheet aluminum vendor data. The ICI CER for concentrators is based on Rockwell data for Type H Kapton material with an aluminized coating. As concentrator thickness decreases, cost per unit area decreases due to the diminished material requirements. However, at around 25 microns (1 mil), the cost reductions are cancelled by the increased difficulty of processing thin materials and the overall cost per unit area begins to rise. Rockwell data from Dupont indicates that the current cost of 0.5 mil concentrator for the SPS would be about \$4.73 per square meter. At increased demand and increased yields, cost could potentially reach \$1.61 per square meter. However, the most likely value, and the value on which the concentrator ICI CER is based, was quoted at \$2.58 per square meter. For the purposes of the CER this was rounded to \$3.00 per square meter to include sensors and mounting attachments and scaled at a slope of 0.95 to reflect anticipated large array economies.

Range of Data

DDT&E: 100 M<sup>2</sup>- 100,000 M<sup>2</sup>

ICI: Unlimited

Input parameters T&M are in square meters, see Table 1.1.1.2.

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.1.2 CONCENTRATORS TABLE

i	dNI	INPUT PARAM	IETERS	:		N	OUT COE	INPUT COEFFICIENTS
		-	#. #	1.000000		CDCER=		0.0
	M= 450000.000	30	W.	0.0		COEXP=		0.0
	CF= 1.00000	<b>Z</b> 00		1.000000		CICER=		0.00003
			.2=	000000.09		CI EXP=		0.95000
İ		: ! !	23=	60.000000				
	DF= 1.000000		-t-	000000009	= 57		0.0	
1	CALCUL ATED VALUES	S	SQ M	SUN TO	1.1.1			S'HILL IONS
	CD=CDCER X (T X DF)XX(CDEXP)	DEXP) X	CF	:	:	1	;	0.0
	CLRM=CICER X (M)XX(CIEXP)	P) X CF	X TF					0.704
	#RM =T / M							120.000
İ	E =1.0 + LOG(PHI) / LOG(2.0)							0.971
B-34	CTFU={CLRM / E)X((#RM X Z1+.5)X	Z1+•51)	X(E)	-0.5XX(E))	•			75.637
İ	CTB = ((CLRM/E)X((#RM X	73 +	0.5) XX(E)	0.5) XX(E) -0.5XX(E))		1 / 23		67.184
1	CIPS=CT8*24/22		;				 	67.183
1	CRCI =CT8 X R							0.134
	COEM = 06M OR CTB*Z	CT B*25/22/ENYR	Æ					0.0
	COMMENTS			•	; ;			



#### 1.1.1.3 SOLAR BLANKET

This element converts solar energy to electrical energy and provides power to the power distribution and conditioning buses. It includes the photovoltaic conversion cells, cover-plates, substrate, electrical interconnects, and any integral attach points required for mounting. Excluded are tools and support equipment required for deployment and tensioning.

Gallium aluminum arsenide (GaAlAs) cells have been selected. The cell consists of GaAs junction with a GaAlAs window, substrate, adhesive, current collectors, and an anti-reflective coating. The solar blanket consists of a Kapton membrane upon which the cells are fastened with a thermo-setting FEP adhesive. Also included in the blanket are the interconnects, thermal coating, attachments/tensioning devices, and sensors.

Historical cost data on solar arrays from previous satellite programs were readily available from the Redstar Data Base and were used to develop the CD CER. However, due to the rapidly changing technology, historical data is not applicable for use in estimating the SPS solar blanket production cost. The Department of Energy (DOE) has initiated the U.S. Photovoltaic Conversion Program. Two main objectives of this program are to develop by 1990 the technological and industrial capability to produce silicon solar arrays at a price of less than \$500 per peak KWe and to establish by 2000 the viability of even lower-cost (\$100 to \$300 per KWe) and/or more efficient alternatives utilizing novel materials and devices. Since it is generally believed throughout the photovoltaic industry that low cost solar arrays are achievable and dependent on the demand for high production rates and since some progress toward meeting the DOE goal has already been made, it was decided to base the SPS solar array cost estimates on projected costs rather than historical costs.

The CD CER was based on solar array historical cost data from the following programs.

- Skylab (OWS)
- Skylab (ATM)
- FRUSA
- SEPS (Est.)

The cost of array structure and mechanisms was not included so that the data would be compatible with the SPS concept of on-orbit structure fabrication and assembly. Although there is a large difference in size between the above arrays and the SPS array, the SPS array will consist of a large number of smaller units. The development fraction (DF) was utilized to normalize the CD cost to reflect cost of only that portion of the total solar array area required to develop the power system.

The initial capital investment CER (CI) cost estimate for material and production processing was based upon information contained in the Arthur D. Little report of March 1978 as prepared under Contract NAS9-15294 with NASA/JSC. The materials cost of \$33/M² and a fabrication cost of \$34/M² total \$67/M² for a gallium arsenide solar cell array. This assessment is consistent with work completed under Rockwell company sponsored activity based on 1977 prices and assuming 1990 technology.

Range of Data:

DDT&E: 10-300 square meters

ICI: Unlimited

Cost estimates are shown in Table 1.1.1.3.

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.1.3 SOLAR BLANKETS TABLE

INPUT COEFFICIENTS				P= 1.000000		0*0	\$, MILLIONS	0.0	1.256	1440.000	0.986	1651,832	1556.693	1556.692	3,113	0.0	
	000 CDCER=		000 CICER=			=57 000	T0 1.1.1						E1) 1 / 23				
AMETERS				22= 60.000			SQ M SUN TO	X CF	)F X TF		00	5) XX(E) -0.5XX(E))	+ 0.5) XX(E) -0.5XX(E)			ENYR	
INPUT PARAMETERS		000	1.000000	000066.0	0.002000	1.000000	CALCUL ATED VALUES	CD=CDCER X (T X DF)XX(CDEXP)	CLRM=CICER X (M)XX(CIEXP) X CF	Z	=1.0 + LOG(PHI) / LOG(2.0)	CTFU=(CLRM / E)X((#RM X 21+.5)	CTB = ((CLRM/E)X((#RM X Z3	24/12	=CTB X R	= 06M OR CTB*25/22/ENYR	
	<u> </u>	*	CF=	=1 H d	R=	0F=	CALCI	CO=COCER )	CLRM=CICEF	#RM = 1 / F	E = 1.0	B-37	CTB = ((CLF	CIPS=CTB*24/22	CRCI	= W300	

## 1.1.1.4 POWER DISTRIBUTION AND CONDITIONING (PD&C)

This element includes the various power feeders, switching and conditioning equipments necessary to deliver power at the required voltage and power levels throughout the satellite. An energy storage system is included, as a power source, to supply minimum power to the various subsystems during eclipse periods. Data buses are not a part of this element as they are included in the information management and control subsystem (WBS No. 1.1.3).

The PD&C system receives power from the solar photovoltaic power generation system and provides for the power conditioning and switching required to deliver the power, through its distribution network, to the satellite power transmission system. Electrical power is transferred from the solar array distribution network through a rotary joint, utilizing slip rings and brushes, to the microwave antenna distribution and conditioning system for the delivery of power at the required levels. The life expectancy of the PD&C is 30 years with the exception of the energy storage system (batteries), which is projected to have a life expectancy of 15 years.

## 1.1.1.4.1 Switches and Converters

Switches will be used to perform various functions and will be monitored and controlled through the IMCS. Switchgears will:

- · Isolate solar array blankets for maintenance work
- Provide voltage regulation of solar array output by selective switching of isolation switchgears
- Control voltage and currents through the IMCS system for short circuit protection
- · Prevention of large line transients
- · Systematic start-up and shut-down of array during eclipse periods
- · Control various loads

The primary switches will be of the Penning cross-field tube design. Functions controlled by these switches will be monitored by the IMCS to determine their status and establish the opening or closing position as required. Basically, the switches are held in a closed state during the operational mode. During start-up and shut-down operations, switches will be monitored by the IMCS, and when certain voltage levels are reached, a command signal will open or close switches as needed.

The power converter and conditioners convert the existing bus voltages to the subsystem voltage required for the various subsystem loads. The output tolerances will be based on the using subsystem interface requirements. The power converters are utilized in the GEO mode of operation.

# 1.1.1.4.2 Conductors and Insulation

Main feeders are generally sized to minimize the combined mass of itself and the solar array mass, considering power requirements, efficiency, and the variation in resistivity with operating temperature. The power distribution system utilizes flat aluminum (6101/T6) feeders where feasible, and round conductors for those subsystems where flat conductors are not feasible.

The CD CER was based on historical cost data obtained from the Redstar Data Base on the following satellite programs.

- DSCS-II • ATS-F
- ATS-FOSO-IATS-EHEAO

· ATS-A

• ATS-B

The ICI CER was based on preprocessed aluminum material cost data and the use of 6101/T6 aluminum. Differential aluminum inflation between current prices and expected mid 1986 prices was included. Cost data was obtained from the following manufacturers:

- · Reynolds Metals
- · Alcoa Aluminum
- · Amchem Products, Inc.
- · The Yoder Company

## Range of Data:

DDT&E: 20 to 150 kilograms

ICI: Unlimited

## 1.1.1.4.3 Slip Rings

The slip ring portion of the rotary joint is included in the PD&C of the Energy Conversion segment. The slip rings consist of an aluminum core with coin silver cladding on each slip ring. The core cross section is  $33.7~{\rm cm}^2$ . The slip ring diameter is .3 km with a length of .94 km. Each slip ring weighs  $10,715~{\rm kg}$  with a total weight of  $42,860~{\rm kg}$  for the required 4 slip rings.

The cost data for the slip rings cost data are based upon large ground commercial and military slip rings. Since all but one of the base data slip rings were designed for ground application, it was decided that these data should not be used as a basis for estimating DDT&E costs. It was determined that the data should be used only as a basis for estimating ICI production costs and then only after applying complexity and specification uprating factors. The following factors were applied:

Complexity Factor 
$$\times$$
 3
Specification Uprating Factor  $\times$  3
Total  $\times$  9

The ICI production cost CER was based on data provided by the following manufacturers.

Manufacturer	Application
Poly-Scientific	High energy
Poly-Scientific	Radar
Electro-Tec	Navy destroyer propeller system
Electro-Tec	Satellite solar array
I.E.C.	Navy shipboard hoist

Due to the relatively low production rate of 1 to 5 units per year, the tooling factor is assumed to be 1.0.

The DDT&E cost was estimated with a CER developed for secondary structure which consisted of space qualified hardware of approximately the same complexity. See the discussion of the secondary structure CER.

Range of Data.

## 1.1.1.4.4 Batteries

\* Z

Batteries will be utilized during ecliptic periods to provide minimum energy required by the energy conversion subsystems. The batteries will be of a sodium chloride design, having a density of at least 200 watt hours/kg.

The DDT&E and the ICI CER's were developed using battery data from the manned/unmanned spacecraft list below:

• APOLLO Lunar Module • APOLLO Lunar Rover • ATS-E • OSO-I

Range of Data:

DDT&E: 1.0 to 180.0 kg ICI: 1.0 to 180.0 kg

# 1.1.1.4.5 Battery PD&C

This element provides the mechanism for the charging of the satellite batteries and the distribution and regulation of power to and from the batteries. Included are the battery chargers, power regulators, power conditioning and power conditioning equipment which directly interface with the battery subsystem.

The DDT&E and the ICI CER's were developed using data from the manned and unmanned spacecraft below:

• APOLLO Lunar Module • GEMINI • APOLLO Lunar Rover • HAWKEYE

# Satellite Systems Division Space Systems Group Rockwell International

• ATS-E

• OSO-I

• ATS-F

Range of Data:

DDT&E: 2.0 to 68.0 kg ICI: 2.0 to 68.0 kg

# 1.1.1.4.6 PD&C Cost Estimates

Cost calculations developed from the CER's discussed in the preceding paragraphs are presented in the following tables:

<u>Table</u>	Description
1.1.1.4.1	Switch Gear and Converters
1.1.1.4.2	Conductors and Insulation
1.1.1.4.3	Slip Rings
1.1.1.4.4	Batteries
1.1.1.4.5	Battery PD&C

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.1.4.1 SWITCH GEAR & CONVERTERS TABLE

grande (\* 1865) 1<sup>7</sup>

INPUT PARAM	ARAMETERS		INPUT CO	INPUT COEFFICIENTS
T= 187000,000	<b>1</b> F=	1.000000	CDCER=	0.158000
.M= 3117.00000	=W30	0.0	CDEXP=	0.297000
	<b>71=</b>	1.000000	CI CER=	0.000400
	22=	60.000000	CI EXP=	1.000000
R≈ 0.0	73=	60.00000		
DF= 0.05000	<b>24=</b>		0.0 = 52	
CALCULATED VALUES	KG	SUM TO 1.1.1.4	• 4	S, MILL IONS
CD=CDCER X (T X DF)XX(CDEXP)	) X CF			3.582
CLRM=CICER X (M)XX(CIEXP) X	X CF X TF			1.870
#RM =T / M				59.994
E = 1.0 + LOG(PHI) / LOG(2.0)	.03			0.926
CTFU=(CLRM / E)X((#RM X 21+	Z1+.5)XX(E) -0.	-0.5xx(E))		89.123
CTB = ((CLRM/E)X((#RM X Z	23 + 0.5) XX(E	0.5)XX(E) -0.5XX(E)	1 / 23	660.99
CIPS=CTB*24/22				66.093
CRCI =CTB X R				0.0
CC&M = 0&M OR CTB*25/22/ENY	2/ENYR			0.0
COMMENTS				

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.1.4.2 CONDUCTORS & INSULATION TABL E

1

	d TUPUI	INPUT PARAMETERS			INPL	JT COE	INPUT COEFFICIENTS
	T= 2367000.00	_ <b>∓</b> F≒	1.000000		CDC ER=		0.158000
		0 £M=	0.0		COEXP=		0.297000
	CF= 1.000000	21=	1.000000		CICER=		0.00000
	PH I= 1.000000	22=	000000.09		CIEXP=		1.000000
	R= 0.0	73=	000000.09				
	DF= 0.10000	<b>7</b>	000000009	= 57	0	0.0	
	CALCULATED VALUES	KG	SUN TO 1	1.1.1.4			S+MILLIONS
i	CD=CDCER X (T X DF)XX(CDEXP) X	) X CF		:	;		6.234
•	CLRM=CICER X (M)XX(CIEXP) X	X CF X TF					0.079
В	#RM = 1 / M				-		120,000
-43	E =1.0 + LOG(PHI) / LOG(2.0)	• 0)					1.000
	CTFU=(CLRM / E)X((#RM X Z1+.5)	XX(E)	-0.5XX(E))				89**6
	CTB = ((CLRM/E)X((#RM X 2	23 + 0.5)XX(E	0.5)XX(E) -0.5XX(E))		1 / 23		9.468
:	CIPS=CTB*24/22			:			9.468
1	CRCI =CTB X R						0.0
	CCEM = 06M OR CTB*25/22/EN	/ENVR					0.0
	COMMENTS	ì		:			

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.1.4.3 SLIP RINGS TABLE

:		INPUT PARA	PARAMETERS	!		INPUT CO	INPUT COEFFICIENTS
İ	ii ⊨	43000.0000	TF=	1.000000		CDC ER=	0.156000
	1	10750.0000	=W30	0.0		CDEXP=	0.511000
	C F≂	1.500000	21=	1.000000		CICER=	0.000764
	PHI≈	000006*0	22=	60.00000		CI EXP=	0.95000
į		0.010000	i t	60.000000			
	DF=	0.02000		60.00000	= 57	0.0	
	CAL CUL ATED	ATED VALUES	KG	SUM TO	1.1.1.4		\$, MILLIONS
:	CD=CDCER X	CD=CDCER X (T X DF)XX(CDEXP) X	(P) X CF				7.392
	CLRM=CICER	CLRM=CICER X (M)XX(CIEXP)	X CF X TF				7.745
B-	#RM =T / M						4.000
-44	E =1.0 +	=1.0 + LOG(PHI) / LOG(2.0)	2.0)				0.848
	CTFU=(CLRM	/ E)X((#RM X	Z1+.5)XX(E) -0.	-0.5XX(E))			-27.626
	CT.B = ((CLRM/E)X((#RM	1/E)X((#RM X	Z3 + 0.51 XX(E	0.5) XX(E) -0.5XX(E)		1 / 23	15,825
	CIPS=CTB*Z4/Z2	172	;		:		15.825
	- CRCI -	=CTB X R					0.158
	= M300	06M OR CTB*25/22/ENYR	22/ENYR				0.0
,	COMMENTS		- ·				

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.1.4.4 BATTERIES TABL E

CD=CDCER X (T X DF)XX(CDEXP) X	06M= 21= 22= 23= 24= KG	0.075600 0.010000 1.000000 60.000000 60.000000 60.000000	75=	CDCER= CDEXP= CICER= CIEXP= 0.0	0.037000 0.734000 0.028000 0.241000 \$,MILL IONS
#RM = T / M E = 1.0 + LOG(PHI) / LOG(2.0) CTFU=(CLRM / E)X((#RM X Z1+.5)	XX(E)	-0.5xx(E))			80.000 0.926 0.338
CTB = ({CLRM/E)X((#RM X Z3 + CIPS=CTB*Z4/Z2 CRCI = CTB X R CCEM = 0&M OR CTB*Z5/Z2/EN	+ 0.5) XX(E)	+ 0.5) XX(E) -0.5XX(E))		1 / 23	0.238 0.238 0.008

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.1.4.5 BATTERY POSC TABLE

2000.00000 TF= 0.043000 CDCFR= 0.05300  250.000000 0EM= 0.0  1.000000 CTER= 0.895000  1.000000 CTER= 0.895000  0.9500000 Z3= 60.000000 CTERP= 0.85900  0.0500000 Z4= 60.000000 CTERP= 0.85900  0.500000 Z4= 60.000000 CTERP= 0.85900  0.500000 Z4= 60.000000 CTERP= 0.85900  0.500000 Z4= 60.000000 CTERPP  X (T X DF)XX(CDEXP) X CF  ER X (M)XX(CIEXP) X CF X TF  M  + LOG(PHI) / LOG(2.0)  - LOG(PHI		INPUT PARAM	ARAMETERS			i NPUT : CO	INPOT COEFFICIENTS
250.00000	≂ <u>L</u>	2000.00000		0.043000	202	FR =	0.053000
1.000000	ij.	250.00000	=W30	0.0	(302)	(P=	0.0008.0
0.950000	C.F.=	1.000000	21=	1.000000	313	#R=	0.012000
0.010000	=1 Hd	0.00056.0	22=	000000.09	C1 E)	( b =	0.859000
0.500000	R=	0.01000	23=	60.00000			
ATED VALUES KG SUM TO 1.1.1.4  (T X OF)XX(CDEXP) X CF  X (M)XX(CIEXP) X CF X TF  X (M)XX(CIEXP) X CF X TF  CG(PHI) / LOG(2.0)  / E)X((#RM X Z1+.5)XX(E) -0.5XX(E))  / E)X((#RM X Z3 + 0.5)XX(E) -0.5XX(E))  / C)X((#RM X Z3 + 0.5)XX(E) -0.5XX(E))	D F=	0.50000		000000009	= 57	0.0	
(T X DF)XX(CDEXP) X CF  X (M)XX(CIEXP) X CF X TF  LOG(PHI) / LOG(2.0)  LOG(PHI) / LOG(2.0)  / E)X((#RM X Z1+.5)XX(E) -0.5XX(E))  /E)X((#RM X Z3 + 0.5)XX(E) -0.5XX(E))  / C)X((#RM X Z3 + 0.5)XX(E) -0.5XX(E))  / E)X((#RM X Z3 + 0.5)XX(E) -0.5XX(E))  / E)X((#RM X Z1+.5)XX(E) -0.5XX(E))  / E)X((#RM X Z1+.5)XX(E) -0.5XX(E))	CALCUI	.ATED VALUES	KG		4.1.4		\$, MILL IONS
RM=CICER X (M)XX(CIEXP) X CF X TF  M = T / M  = 1.0 + LOG(PHI) / LOG(2.0)  FU=(CLRM / E)X((#RM X Z1+.5)XX(E) -0.5XX(E))  B =((CLRM/E)X((#RM X Z3 + 0.5)XX(E) -0.5XX(E))  PS=CTB*Z4/Z2  CRCI = CTB X R  CGEM = DEM OR CTB*Z5/Z2/ENYR	CD=CDCER X	(T X DF)XX(CDEXF	×		:		24.790
M = T / M = 1.0 + LOG(PHI) / LOG(2.0)  FU=(CLRM / E)X((#RM X Z1+.5)XX(E) -0.5XX(E))  B =((CLRM/E)X((#RM X Z3 + 0.5)XX(E) -0.5XX(E))  PS=CTB*Z4/Z2  CRCI =CTB X R  CGEM = DEM OR CTB*Z5/Z2/ENYR	CLRM=CICER		CF X				0.059
=1.0 + LOG(PHI) / LOG(2.0)  FU=(CLRM / E)X((#RM X Z1+.5)XX(E) -0.5XX(E))  B =((CLRM/E)X((#RM X Z3 + 0.5)XX(E) -0.5XX(E))  PS=CTB*Z4/Z2  CRCI =CTB X R  CGEM = OEM OR CTB*Z5/Z2/ENYR	T=						8.000
)X((#RM X Z1+.5)XX(E) -0.5XX(E)) X((#RM X Z3 + 0.5)XX(E) -0.5XX(E)) X R  X R  OR CTB*Z5/Z2/ENYR		LOG(PHI) / LOG(2	.0)				0.926
X((#RM X Z3 + 0.5)XX(E) -0.5XX(E)) ) / Z3  X R  OR CTB*Z5/Z2/ENYR	CTFU=(CLRM	×	X(E)	.5XX(E))			0.430
X R OR CTB*25/22/ENYR	CTB = ((CLR	×	+	E) -0.5XX(E))		67 /	0.324
=CTB X R = DEM OR CTB*Z5/Z2/ENYR	CIPS=CTB*Z	+/22			: : : : :		0.324
= 06M OR CTB*25/22/ENYR	1	×					0.003
	# W30 ⊃	98					0.0
	COMMENTS					!	

# 1.1.1.5 THERMAL CONTROL

This element includes any component used to modify the temperature of the energy conversion subsystem components. It includes cold plates, heat transfer and radiator devices as well as insulation, thermal control coatings and finishes. Excluded are paints or finishes applied to components during their manufacturing sequence.

## 1.1.1.6 MAINTENANCE

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This element provides for in-place repair or replacement of components and includes work stations, tracks, access ways, and in situ repair equipment.

The maintenance requirements of this element are related to the energy conversion section of the satellite covering the main structure, concentrators, solar blankets, and power distribution/conditioning. Some of the items of maintenance equipment will be commonly used on the satellite power transmission and interface segments. In these cases, the costs have been apportioned to the related WBS element. Maintenance requirements are listed in Table 1.1.1.6 and costs are presented in Tables 1.1.1.6.1, 1.1.1.6.2 and 1.1.1.6.3.

Table 1.1.1.6 Maintenance Requirements

WBS NÓ.	MAINTENANCE ITEM DESCRIPTION	1.1.1.6 ENERGY CONVERSION
1.1.1.6.1	"Free-Flyers" or Barge for Cargo and Personnel (Common Use Item)	0.8 Vehicle Utilization
1.1.1.6.2	Manned Manipulator Module Tracks and Access Ways	l Vehicle 84,000 kg

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.11.1.6.1 MAINTENANCE - FREE FLYERS TABL E

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INPUT PAR	PARAMETERS		: : : : : : : : : : : : : : : : : : : :	INPUT CO	COEFFICIENTS
T= 5000.00000	TF=	1.000000		CDC ER=	0.0
M= 5000.00000		0.0		CDEXP=	0.0
CF= 1.25000		0.00008.0		CI CER=	0.005798
		60.000000		CI EXP=	1.000000
	23=	48.000000			
DF= 1.000000	<b>5</b> 4=	48.000000	= 57	0*0	
CALCULATED VALUES	KG	SUM TO	9.1.1.1		S.MILL IONS
CD=CDCER X (T X DF)XX(CDEXP)	(P) X CF				0.0
CLRM=CICER X (M)XX(CIEXP)	X CF X TF				36.238
#RM =T / M					1.000
E =1.0 + LOG(PHI) / LOG(2.0)	(2.0)		-		0.926
CTFU=(CLRM / E)X((#RM X Z	21+•5)XX(E) -0.	-0.5XX(E))			29.299
CTB = ((CLRM/F)X((#RM X	Z3 + 0.5) XX(E	0.5)XX(E) -0.5XX(E))		1 / 23	29.240
CIPS=CTB*Z4/Z2			:		23.392
CRCI = CTB X R					0.585
COEM = OEM OR CTB*25/22/E	22/ENYR				0.0
COMMENTS					

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.1.6.2 MANNED MANIPULATOR TABLE

	INPUT PARA	ARAMETERS		;	I NPUT CO	INPUT COEFFICIENTS
<b>"</b>	3000-0000	TF=	1.000000	000	CDCER=	0.0
<u>"</u>	3000.00000	=W30	0.0	200	CDEXP=	0.0
C F=	1.100000	21=	1.000000	010	CICER=	0.005798
PHI=	0.950000	22=	00000000	210	:XP=	1.000000
# &	0.02000	73=	60.000000			
0F=	1.000000	= + 7	00000009	= 57	0.0	
CALCUL	CALCULATED VALUES	KG	SUM TO 1.1	1.1.1.6		\$, MILL IONS
CD=CDCER X	CD=CDCER X (T X DF)XX(CDEXP) X	XCF		1	•	0.0
CLRM=CICER	X (M)XX(CIEXP) X	CF X TF				19.133
#RM =T / M					,	1.000
E = 1.0 +	=1.0 + LOG(PHI) / LOG(2.0)	.01			1	976*0
CTFU=(CLRM	CTFU=(CLRM / E)X((#RM X Z1+.5)	XX(E)	-0.5XX(E))			19.203
CTB = ((CLRM/E)X((#RM	×	Z3 + 0.51XX(E)	E) -0.5XX(E))		/ 23	15.198
CIPS=CTB*24/Z2	4/12					15.198
CRCI =	=CTB X R			٠		0.304
= W300	0£M OR CTB*25/22/ENYR	ZENYR				0.0
COMMENTS						

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.1.6.3 TRACKS & ACCESS WAYS TABLE

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I		1				
_=_	84000.0000	TF=	1.000000		CDCER=	0.0
# <b>X</b>	84000.0000	0£M=	0.0		CDEXP=	0.0
C F≅	1.000000	=17	1.000000		CICER=	0.000005
=1 Hd	1.000000	22=	000000.09		CI EXP=	1.000000
<b>*</b>	0.002000	<b>-67</b>	000000-09			
0 F=	0.20000	= + 7	00000009	= 57	0.0	
CALCUL	CALCULATED VALUES	KG	SUM TO	1.1.1.6		\$, MILL IONS
CD=CDCER X	CO=COCER X (T X OF)XX(COEXP)	) X CF		:		0.0
CLRM=CICER	CLRM=CICER X (M)XX(CIEXP) X CF	CF X TF				0.420
#RM =T / M						1.000
E = 1.0 +	=1.0 + LOG(PHI) / LOG(2.0)	10.			The second secon	1.000
CTFU=(CLRM /	/ EIX((#RM X Z1+.5	XX(E)	-0.5XX(E))			0.420
CTB = ((CLRM/E)X((#RM	×	Z3 + 0.51XX(E	0.51XX(E) -0.5XX(E))		1 / 23	0.420
CIPS=CTB*24/22	:	i				0.420
CRCI =	=CTB X R					100.0
= W300	0£M OR CT8*Z5/Z2/ENYR	/ENYR				0.0
COMMENTS						

#### 1.1.2 MW POWER TRANSMISSION

This element receives do electrical power from the interface subsystem, conditions the power, converts it to microwave energy and radiates the energy to the ground receiving station. Included are power distribution from the interface subsystem, do to RF conversion devices, control and monitoring equipment, and antenna radiating elements.

Costs in this section include those of the antenna structure and sub-arrays with their klystrons; the power distribution and conditioning system; thermal control; phase reference system; and maintenance requirements. The MW antenna system is illustrated in Figure 1.1-2 and illustrates the basic configuration, including overall dimensions of the selected antenna structure concept.

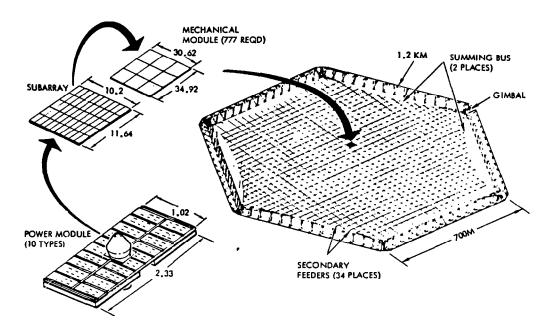


Figure 1.1-2. Microwave Transmission System
- Satellite Antenna

The smallest antenna building block is the power module, which varies in size from the one illustrated (which is used at the center portion of the antenna) to 3.40 by 5.82 meters at the periphery of the antenna. Ten different power module sizes are used to comprise the antenna element. Each power module has a klystron located in its center. The power modules are arranged into subarrays measuring 10.2 by 11.64 meters. Each subarray has its own phase control electronics. Nine subarrays are connected to form a mechanical module 30.82 by 34.92 meters.

#### 1.1.2.1 STRUCTURE

This element includes all members necessary to support the transmitter subarrays and other power transmission subsystem hardware. It includes structural beams, beam couplers, cables, tensioning devices, and secondary structures.

# 1.1.2.1.1 Primary Structure

This element includes the basic supporting framework of the microwave antenna power transmission system up to the interface connection. The antenna primary structure has three main components — a tension web made from composite wires or tapes; a catenary cable that transfers the web tension to the verticies; and the octogonal compression frame. The antenna frame provides a structural support but does not include the wave guides or radio frequency assemblies associated with the microwave subsystem.

This element is limited to primary load carrying structure and does not include other secondary structure such as equipment mounts, platforms, and space equipment supports.

The SPS requirement for low thermal distortion, under high thermal stress, dictates the need for a material with a very low coefficient of expansion. The most likely candidate, at this time, is a graphite composite material.

The antenna structure D&D CER was developed using graphite composite data obtained from NASA's Redstar Data Base. Tooling cost was excluded under the assumption that this cost would be incurred in the development of orbital fabrication equipment. The following data points were used:

- · Space Telescope Shell
- · ATS-F Truss
- HEAO Optical Bench
- · Shuttle Payload Bay Doors

The antenna structure ICI is the cost of raw materials only since the costs associated with fabrication and assembly are charged against orbital assembly and support equipment. The antenna structure ICI cost equation is based on raw composite material stock (prepregnated graphite) cost. These material costs are based on vendor quotes obtained from Hercules, Fiberrite and Union Carbide.

#### Range of Data:

D&D: 30,0 to 2000.0 kg

ICI: Unlimited

# 1.1.2.1.2 Secondary Structure

The secondary structure consists of the passive interface attachment between the primary structure and operational subsystems. The structural members are made of aluminum with the ability to articulate, rotate, or otherwise support/allow motion between the primary structure and other subsystem elements.

This element includes all structure, consisting of mounting brackets, clamps and installation structure required as an interface and mounting attach points of components, assemblies, and subsystems. It also includes any structure required between two or more components or assemblies.

Development of the secondary structure CER for DDT&E was based on cost contained in the MSFC Redstar Data Base. Data from a variety of launch vehicle and unmanned sate-lite programs were available and the applicable data points are listed below:

- S-IVB Interstage
- · S-IC Forward Skirt
- S-IC Intertank
- Solar Telescope Housing Assembly (ASM)
  - Common Mount Assembly (ASM)
  - Telescope Gimbal Assembly (ASM)
  - Common Mount Actuators (ASM)
  - Telescope Gimbal Actuators (ASM)
  - Array Platform Elevation Pointing Actuator (ASM)
  - UV Gimbal Mount Actuators (ASM)
  - UV Instrument Mount Assembly (ASM)

- Solar Array and Boom Structure (ATS-F)
- Squib Interface Unit (ATS-F)
- Interstage (Centaur)
- Nose Shroud (Centaur)
- Fixed Airlock Shroud (Skylab)
- Payload Shroud (Skylab)
- Pallet Segment (Spacelab)
- · 0S0-1
- ATS-F
- S-II

The ICI production cost CER was based upon an Engineering Cost estimate.

# Range of Data:

DDT&E: 6.0 to 15,000.0 kg ICI: 6.0 to 15,000.0 kg

# 1.1.2.1.3 Cost Estimates

Input parameters T&M are in kilograms of mass, see Tables 1.1.2.1.1 and 1.1.2.1.2.

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.2.1.1 PRIMARY STRUCTURE TABLE

i		INPUT PAR	ARAMETERS			INPUT	INPUT COEFFICIENTS
	=	0000.00079	TF=	1.000000		COC FR =	0.023000
1	=	8375.00000	=W30	0.0		COEXP=	0.800000
	CF=	1.000000	<b>517</b>	1.000000		CI CER=	0.000050
	PH I=	1.000000	22=	00000000		CI EXP=	1.000000
{	<b>8</b>	0.002000	23=	00000009			
	0F=	0.020000	= + 7	000000009	= 57	0.0	
İ	CALCUL	CAL CUL ATED VALUES	KG	SUM TO 1.1	1.1.2.1		S, MILL IONS
i	CD=CDCER X	CD=CDCER X (T X DF)XX(CDEXP)	X CF				7.301
	CLRM=CICER	CLRM=CICER X (M)XX(CIEXP) X	X CF X TF				0.419
B-5	#RM =T / M						8.000
; 55	E = 1.0 +	=1.0 + LOG(PHI) / LOG(2.0)	.01				1.000
	CT FU= (CLRM	CTFU=(CLRM / E)X((#RM X Z1+.5)	XX(E)	-0.5XX(E))			3,350
1	CTB = ((CLRM/E)X((#RM	×	Z3 + 0.51XX(E)	:) -0.5XX(E3)		1 / 23	3.350
!	CIPS=CTB*Z4/Z2	172			:		3.350
İ	CRCI =	=CTB X R					0.007
	= W300	OEM OR CT8*25/22/E	/ENYR				0.0
į	COMMENTS				:		

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.2.1.2 SECONDARY STRUCTURE TABLE

T. OF

1		INPUT	INPUT PARAMETERS		!	INPUT CO	INPUT COEFFICIENTS
	<b>=</b>	234000.000	TF=	0.007300		CDCER=	0.156000
	==	5.000000	-W30	0.0		CDEXP=	0.511000
	CF=	1.000000	21=	1.000000		CI CER=	0.101000
	=I Hd		= 27	000000000		CI EXP=	0.355000
	<b>8</b>	0.002000	23=	0000009			
	DF=	0.05000	= + 7	000000*09	= 57	0.0	
	CALCU	CALCULATED VALUES	KG	SUM TO 1.1	1.1.2.1		\$, MILLIONS
į	CD=CDCER X	CO-COCER X (T X DF)XX(CDEXP)	X CF				18.705
	CLRM=CICER	X (M)XX(CIEXP) X	CF X TF				0.001
<sub>B-</sub>	#RM =T / M						46800.000
56	E = 1.0 +	=1.0 + LOG(PHI) / LOG(2.0)	•0)		:		0.971
	CTFU=(CLRM	CTFU=(CLRM / E)X((#RM X ZI+.5)	XX(E)	-0.5XX(E))			666*54
	CTB = ((CLR	CTB = ((CLRM/E)X((#RM X Z	Z3 + 0.51XX(E	0.5) XX(E) -0.5XX(E))		1 / 23	40 • 825
:	CIP'S=CTB*Z4/Z2	4/12			:		40.825
]	CRCI	=CTB X R					0.082
	CCEM =	: 0£M OR CT8*25/22/ENYR	/ ENYR				0.0
	COMMENTS				l 		

## 1.1.2.2 TRANSMITTER SUBARRAY/KLYSTRONS

This element includes all the hardware required for generation, distribution, phase control and radiation of microwave energy. This includes the subarray structure, wave guides, power amplifiers, control devices, and power harnesses. Also included are thermal control devices and finishes that are manufactured as an integral part of the subarray.

RF generators convert the direct current (dc) electric power to RF microwave power. Klystrons are used in this system as the high power RF transmitting devices. Wave guides receive the RF power from the generator and radiate it to the ground-based rectenna.

Historical data for some twenty phased array radars ranging over a period of the last twenty years were extracted from the Redstar Data Base and/or obtained from various contractors. The data were analyzed, normalized and the costs were adjusted to reflect 1977 dollars. In addition, for all costs utilized, the facility receiver subsystem hardware, data subsystem costs and basic facility/housing costs were removed.

The application of phased array radar costs to the development cost estimates of the microwave antenna was pertinent since the design and development of these physically large ground installations was conducted in much the same manner that is being utilized for the SPS. The ground array radiating elements were assembled in subarray panels, complete with the radiating elements, wave guide, and cabling. The subarrays were then mounted into the facility framework, subarray cabling, and plumbing connection completed at system level and confidence testing conducted. The same general assembly philosophy is expected to be followed for the microwave antenna, the difference being that the microwave antenna will be totally assembled in the space environment.

The D&D CER was based on data from four DOD classified projects identified only as Projects 21, 22, 23, and 24 as well as the Cobra Dane, AN/SPS-48 and SAM-D (PATRIOT) radar systems.

A different approach was taken to develop the TFU CERs. After reviewing the various radar systems' cost, it was determined that not enough insight was afforded into the components; therefore, a "grass-roots" approach was undertaken.

For purposes of developing a "grass-roots" estimate for the TFU, a segment of the antenna measuring 2.4 m² was assumed to be the Lowest Replaceable Unit (LRU). In addition, to arrive at an "average" LRU, it was necessary to evenly distribute all components over the antenna. Enclosed tables list the components and their estimated cost for both the klystron and amplitron configurations. The required components were determined through analysis. Letters and telephone calls were directed to hardware manufacturers requesting technical data and cost quotes for the specified components. Where multiple quotes were obtained, the average cost was used. In some instances, estimates had to be relied upon. It was further assumed that the components are the same in each configuration with only the power tubes changing with the exception of the klystron configuration where the IRF amplifier is different.

Data contained in the Redstar Data Base were utilized to develop integration factors which were added to the vendor quotes. To account for the cost associated with voltage measurement instrumentation for the microwave antenna, a 20% instrument factor was also applied to the vendor quotes. The individual cost estimates, developed for each type of power tube, were utilized to develop CERs based on the area of one LRU. For the purpose of developing these CERs, three different LRU sizes were assumed – 2.4 m², 24 m², and 240 m². It is necessary for the user to determine the size and number of LRUs required for any given antenna configuration. It is also necessary for the user to consider any learning that may occur.

# Range of Data:

D&D: 1000 to 100,000 kilowatts

ICI: Unlimited

Table 1.1.2.2.1 expresses the DDT&E cost estimate  $[C_D=.067(P_T)^{0.507}(CF)]$  to facilitate the use of antenna power in kilowatts as the input factor. Table 1.1.2.2.2 shows the  $C_{I,LRU}=.00327(A_{LRU})^{1.000}$  where A is in square meters. A complexity factor of 1.25 is used to compensate for the klystron kilowatt power rating as used in the data base.

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.2.2.1 KLYSTRON DDT&E TABLE

	i !	INPUT PAR	ARAMETERS			INP	JT COE	INPUT COEFFICIENTS
	=	00.0000679	TF=	1.000000		CDC ER =		0.205000
1	¥	6790000.00	=W30	0.0		CDEXP=		0.507000
	C.F.=	1.250000	=17	1.000000		CICER=		0.0
		0.00086.0	72=	60.00000		CI EXP=		0.0
İ	ا « «	0.0	23=	180,000000	: 			
	0F=	0.02000	= + 7	000000.09	=97	•	0.0	
	CALCI	CALCULATED VALUES	X	SUM TO 1.	1.1.2.2			S. MILL IONS
:	CD=CDCER X	(T X DF)XX(CDEXP)	XCF		!	: ! !	1	102.576
	CLRM=CICER	X (M)XX(CIEXP) X	CF X TF				•	0.0
<sub>B</sub> .	#RM =T / M							1.000
-59	E = 1.0 +	=1.0 + LOG(PHI) / LOG(2.0	(0*		.:	:		0.971
	CTFU=(CLRA	CTFU=(CLRM / E)X((#RM X Z1+	Z1+.5)XX(E) -0.	-0.5XX(E))				0.0
	CTB = ((CLF	CTB = ((CLRM/E)X((#RM X Z	Z3 + 0.5) XX(E	0.5) XX(E) -0.5XX(E) }		1 / 23		0.0
I	CIPS=CTB*Z4/Z2	24/22						0.0
1	CRCI	=CTB X R						0.0
	= W300	= 0£M OR CT8*Z5/Z2/E	/ENYR					0.0
1	COMMENTS			:	:		1	

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.2.2.2 KLYSTRON ICI, R. O&M TABLE

INPUT COEFFICIENTS	0.0	0.0	0.003270	1.000000			\$, MILL IONS	0.0	0.486	6993.332	0.971	2702.309	2322.804	2322.804	154.854	0.0	
I NPUT CC	CDC ER =	CDEXP=	CICER=	CI EXP=		0.0 = 52	• 2						1 / 23				
	1.000000	0.0	1.000000	00000000	180.000000	Z 000000°09	SUM TO 1.1.2.2					-0.5XX(E))	0.5) XX(E) -0.5X X(E)				
INPUT PARAMETERS	TF=	=W30	21=	2.2=	23=	= 4 7	SQ M	) X CF	CF X TF		•0)	ZI+•5)XX(E) -0•	Z3 + 0.5)XX(E			/ENYR	
INPUT	830808.000	118.800003	1.250000	0.980000	0.066667	0.020000	ATED VALUES	(T X DF)XX(CDEXP)	X (M)XX(CIEXP) X		+ LOG(PHI) / LOG(2.0)	/ E)X((#RM X	×	17.2	=CTB X R	06M OR CTB*25/22/EN	
	<u> </u>	1	C.F₌	=IHd	æ	0F=	CAL CUL ATED	CD=CDCER X	CLRM=CICER	B #RM = T / M	-00 E =1.0 +	CTFU=(CLRM	CTB = ((CLRM/E)X((#RM	CIPS=CTB*Z4/Z2	CRCI =	≡ W300	COMMENTS

#### 1.1.2.3 POWER DISTRIBUTION AND CONDITIONING (PD&C)

This element includes the various power feeders, switching, and conditioning equipment s necessary to deliver power at the required voltage and power levels for the power transmission section (antenna portion) of the satellite. An energy storage system is included to supply power to keep the power transmission system at a ready state and for housekeeping requirements during eclipse periods. Data buses are not a part of this element as they are included in the information management and control subsystem (WBS No. 1.1.3).

The PD&C system receives power from the interface (Energy Conversion/Power Transmission) system and provides for the power conditioning and switching required to deliver the power, through the distribution network, to the microwave energy conversion units. On the rotating member, power is conducted through switch gears to dc/dc converters which output the six primary voltages required by the Klystrons. Each voltage is conducted to a summing bus through switch gears and power feeders and on through switch gear at the mechanical modules for use at the subarrays to provide power at the 135,864 Klystrons.

Batteries and battery conditioning equipment are included also to provide the stored energy to power the heater requirements which keep the Klystrons at a ready mode during the eclipse periods. The batteries will also provide power for the necessary housekeeping activities, i.e., stationkeeping, IMCS, TT&C, etc., during this period.

#### 1.1.2.3.1 Switches and Power Conditioning

Switches will be used to perform operational functions as monitored through the IMCS. Switch gears will:

- Isolate converters, main feeders, secondary feeders, mechanical modules, subarrays and Klystrons for maintenance work
- Provide split bus power feed to offer redundancy to some modules in event of failure of a converter or summing bus
- Control power through the IMCS for:
  - · short circuit protection
  - systematic start-up and shut-downs to prevent surges during eclipse periods
  - · control various loads

The basic switches will be of the Penning cross-field tube design and monitored and controlled by the IMCS. The IMCS will will determine their status and functionally connect them to the proper feeder and summing bus as conditions may direct.

The power converter and conditioners convert the existing bus voltages to the subsystem voltage required for the various subsystem loads. The output tolerances will be based on using subsystem interface requirements. The power converters are utilized in the GEO mode of operation.

# 1.1.2.3.2 Conductors and Insulation

The summing buses, main feeders and secondary feeders are generally sized to minimize the combined mass of itself and the satellite mass, considering the power requirements, efficiency, and variation in resistivity with temperature. The PD&C utilized aluminum (6101-T6) conductors.

## 1.1.2.3.3 Batteries

Batteries will be utilized during the ecliptic periods to provide minimum energy to keep the Klystrons warmed to a ready state and as necessary during the required housekeeping tasks. The batteries will be a sodium chloride type having the capability of providing 200 watt hours/kg.

The battery PD&C costing is included in the earlier sections of 1.1.2.3.2 and 1.1.2.3.1. This element consists of the mechanisms for the charging of batteries and the distribution and regulation of power to and from the battery. This function will be monitored and controlled by the IMCS. Included are the battery chargers, power regulators, diodes, power regulators, and power conditioning equipment that directly interfaces with the battery system.

## 1.1.2.3.4 PD&C Cost Estimates

The CER's used in this section are the same as those described in Section 1.1.1.4. The following tables itemize the design/cost parameters and identify the cost estimates in each area.

<u>Table</u>	Description
1.1.2.3.1	Switch Gear and Converters
1.1.2.3.2	Conductors and Insulation
1.1.2.3.3	Batteries

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.2.3.1 SWITCH GEAR & CONVERTERS TABLE

	INPUT PAR	ARAMETERS			INPL	JT C0 E	INPUT COEFFICIENTS
=	1901000.00	TF=	1.000000		CDC ER=		0.158000
11	2447.00000	=W30	0.0		CDEXP=		0.297000
C.F=	1.500000	-17	1.000000		CI CER≈		0.000400
=1 Hd	0.950000	22=	000000009		CI EXP=		1.000000
R=	0.066667	23=	180.00000			] 	
DF=	0.050000	= + 7	000000*09	= 57	J	0.0	
ALCI	CALCULATED VALUES	KG	SUM TO 1.1	1.1.2.3			S, MILL IONS
ER.	CD=COCER X (T X DF)XX(CDEXP)	XCF			!		7.132
ICE	CLRM=CICER X (M)XX(CIEXP) X C	CF X TF					1.468
H / 1=	-						176.870
0	=1.0 + LOG(PHI) / LOG(2.0	.00					0.926
ICLRA	CTFU=(CLRM / E)X((#RM X 21+.5	)XX(E)	-0.5XX(E))				752.336
ICCL	CTB = ((CLRM/E)X((#RM X Z	Z3 + 0.51XX(	+ 0.51XX(E) -0.5XX(E)		1 / 23		512.556
T8*!	CIPS=CTB*24/22						512,556
CRCI	=CTB X R						34.171
= W300	= 08M OR CTB*25/22/ENYR	/ ENYR					0.0
COMMENTS				;		!	

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.2.3.2 CONDUCTORS & INSULATION TABL E

INPUT COEFFICIENTS	0.158000	0.297000	0.000004	1.000000			S.MILLIONS	5.262	0.007	777.325	1.000	5-348	5-348	5.348	0.0	0•0	
INPUT CO	CDC ER=	CDEXP=	CICER=	CI EXP≖		0.0							) / 23				
	1.000000	0.0	1.000000	0000000	60.00000	= 57 0000000*09	SUM TO 1.1.2.3					•5xx(E))	E) -0.5XX(E))				
ARAMETERS	<b>TF</b> =	=W30	21=	<b>12=</b>	23=	= + 7	KG	X CF	CF X TF		(0.	•5)XX(E) -0	Z3 + 0.5) XX(E)			/ENYR	
INPUT PARAM	1337000.00	1720.00000	1.000000	1.000000	0.0	0.100000	CALCULATED VALUES	CD=CDCER X (T X DF)XX(CDEXP) X	X (M)XX(CIEXP) X		=1.0 + LOG(PHI) / LOG(2.0)	CTFU= (CLRM / E)X((#RM X Z1+.5)XX(E) -0.5XX(E))	×	4/12	=CTB X R	06M OR CTB*25/22/ENY	
	۳	- II =	C.F=	PH I=	= &	DF=	CALCUI	CO=COCER X	CLRM=CICER	B #RM = 1 / M	ш	CTFU= (CLRM	CTB = ((CLRM/E)X((#RM	CIPS=CTB*24/22	CRCI	CC6M=	

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.2.3.3 BATTERIES TABLE

1.00000	AMETER S TF=
1.000000 60.000000 120.000000 60.000000 50.00	
120.000000	
60.000000 25= 0.0 SUM TO 1.1.2.3 XX(E)) -0.5XX(E)) 1 / Z3	
SUM TO 1.1.2.3  3800.00  XX(E))  -0.5XX(E))  1 / Z3	
3800.000 0.926 -0.5xx(E1) 1 / Z3	KG
3800.000 0.926 -0.5xx(E1) 1 / 23	
3800.000 0.926 -0.5xx(E1) 1 / Z3	Ŧ
0.926 -0.5xx(E1) 1 / 23	
-0.5xx(E1) 1 / 23	;
-0.5xx(E1) 1 / 23	XX(E) -
8.502 0.283 0.475	0.5)xx(E)
0.283	:
0.475	

#### 1.1.2.4 THERMAL CONTROL

This element includes any component used to modify the temperature of power transmission subsystem components. It includes cold plates, heat transfer and radiator devices as well as insulation, thermal control coatings and finishes. Excluded are paints and finishes applied to components during during their manufacturing sequence and thermal control devices that are an integral part of another component.

The multi-layer insulation panels are required for the back surface of the resonant cavity radiators to restrict waste heat leaks which could increase temperatures of electronics to unacceptable levels. This insulation is coated externally with low absorptivity/emissivity materials to limit the absorbed solar flux to which the surface is exposed during part of the orbit.

The insulation CER's are based upon secondary structure CER's where the secondary structure CER's were considered comparable to the requirements of insulation in its application on the antenna.

Table 1.1.2.4 presents cost estimates for thermal control.

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.2.4 THERMAL CONTROL - INSULATION TABLE

#### 1.1.2.5 CONTROL-PHASE REFERENCE

This element provides the reference phase for all subarray phase conjugating circuits and includes the reference oscillator signal distribution, and frequency conversion equipment. It covers components/equipment that commonly serve all subarrays.

The transmitted signal is formed from the pilot beam by means of the retroelectronics where one circuit is required per subarray. A servo system is needed to transfer the required reference phase from a central point to a mechanical module, where it is distributed to the nine subarrays. The main items included in this subsystem are shown in Table 1.1.2.5.

WBS NO:	ITEM/ DESCRIPTION	QUANTITY PER SATELLITE
1.2.5.1	REFERENCE FREQUENCY GENERATOR	1 SET (777 POWER AMPLIFIERS, 1-4 REGULATORS)
1252	COAY CARLE	777 9579

Table 1.1.2.5 Control-Phase Reference

DEVICES FOR USE ON FREQUENCY

DISTRIBUTION SYSTEM

Tables 1.1.2.5.1, 1.1.2.5.2 and 1.1.2.5.3 present the engineering estimates for these items.

777 **SETS** 

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.2.5.1 REFERENCE FREQUENCY GENERATOR TABLE

	INPUT PA	ARAMETERS		     	INPUT CO	INPUT COEFFICIENTS
<u>  </u>	1.000000	TF=	1.000000		CDCER=	0.00000
II.	1.000000	-W30	0.010000		CDEXP=	1.000000
C F≅	1.000000	<b>Z1=</b>	1.000000		CICER=	0.100000
=1 Hd	1.000000	22=	60.000000		CI EXP=	1.000000
<b>&amp;</b>	0.033333		120.000000			
0F=	0.200000	= + 7	000000*09	= 57	0.0	
CALCULA	CALCULATED VALUES	SET	SUM TO 1.	1.1.2.5		S, MILL IONS
CD=CDCER X (1	CD=CDCER X (T X DF)XXLCDEXP)	X CF		: : : !		0.100
CLRM=CICER X	CLRM=CICER X (M)XX(CIEXP) X	K CF X TF				0.100
M / L= WX# B-						1.000
w	=1.0 + LOG(PHI) / LOG(2.	.01			•	1.000
CTFU=(CLRM /	CTFU=(CLRM / E)X((#RM X Z1+.	5)XX(E)	-0.5XX(E))			0.100
CTB = ((CLRM/E)X((#RM	×	Z3 + 0.51 XX	+ 0.5) XX(E) -0.5XX(E))		) / 23	0.100
CIPS=CTB*24/22	7.7					0.100
CRCI = CTB	78 × R					0.003
30 = W300	0EM OR CT 8*25/22/	2/ENYR				0.010
COMMENTS						

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.2.5.2 DIST. SYSTEM, COAXIAL CABLE TABLE

1		INPUT PARAM	ARAMETERS			INP	UT COE	INPUT COEFFICIENTS
	<u>"</u>	203000.000	TF=	1.000000		CDC ER =		0.000005
	¥	261.000000	=W30	0.0		CDEXP=		1.000000
	C.F=	1.000000	71=	1.000000		CI CER=		0.000000
	=IHd	1.000000	-27	000000000		CI EXP=		1.000000
]	# CX	0.0	13=	60,00000				A THE REST OF THE PARTY OF THE
	DF=	0.20000	= 7 7	000000*09	= 57		0.0	·
	CALCU	CALCULATED VALUES	Σ	SUM TO 1.	1-1-2.5			S. MILL IONS
;	CD=CDCER X	CD=CDCER X (T X DF)XX(CDEXP)	X CF		1		:	0.203
	CLRM=CICER	X (M)XX(CIEXP)	X CF X TF					0.016
B-	#RM =T / M							177.778
-70	E =1.0+	=1.0 + LOG(PHI) / LOG(2.0)	• 01					1.000
	CTFU=(CLRM /	E)X((#RM X	Z1+.51XX(E) -0.	-0.5XX(E))				12.180
	CTB = ((CLR	CTB = ((CLRM/E)X((#RM X Z	Z3 + 0.5) XX(E	0.5)XX(E) -0.5XX(E))		1 / 23		12.180
:	CIPS=CTB*Z4/Z2	4/22				:		12.180
	CRCI	=CTB X R						0.0
	= W300	. 06M OR CTB*25/22/ENYR	/ ENY R.					0.0
1	COMMENTS						 	

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.2.5.3 DIST. SYSTEM, DEVICES TABLE

[		INPUT PA	ARAMETERS		; !	INPUT	INPUT COEFFICIENTS
	<del>!!</del>	1554.00000	TF≖	1.000000		CDCER=	0.000225
	<u>"</u>	2.000000	=W30	0.0		COEXP=	1.000000
	CF≡	1.000000	21=	1.000000		CI CER=	0.005000
	PH I=	1.000000	<b>75=</b>	000000.09		CI EXP=	1.000000
İ	<b>8</b>	0.033333	Z3=	120.000000			
	DF=	0.20000	= + 2	000000009	= 57	0.0	
	CAL CUL ATED	ATED VALUES	KG	SUM TO 1.	1.1.2.5		S+ MILL IONS
İ	CD=CDCER X	CD=CDCER X (T X DF)XX(CDEXP)	X CF				0.070
	CLRM=CICER )	CLRM=CICER X (M)XX(CIEXP) X	CF X TF				0.010
B-	#RM =T / M						777.000
·71	E =1.0 + [	=1.0 + LOG(PHI) / LOG(2.	• 0)				1.000
	CTFU=(CLRM ,	CTFU=(CLRM / E)X((#RM X Z1+.	5) XX(E)	-0.5XX(E))			077.1
}	CTB = ((CLRM/E)X((#RM	×	Z3 + 0.51 XX(	+ 0.5) XX(E) -0.5XX(E))		1 / 23	017.7
ļ	CIPS=CTB*Z4/Z2	/7.2			:		07.77
	CRCI =(	=CTB X R					0.259
	) = W300	0&M OR CT8*25/22/	/ENYR				0.0
:	COMMENTS				!		

## 1.1.2.6 MAINTENANCE

This element provides for in-place repair or replacement of components and includes work stations, tracks, access ways, and insitu repair equipment.

Maintenance requirements of this element are related to the power transmission (antenna) section of the satellite covering the structures; subarrays (Klystrons); power distribution/conditioning and energy storage; thermal control, and control elements. Some of the maintenance equipment are multipurpose and are therefore costed against the applicable maintenance items on an apportioned basis.

Maintenance requirements for this element are presented in Table 1.1.2.6 and cost estimates are projected in Tables 1.1.2.6.1, 1.1.2.6.2, 1.1.2.6.3, and 1.1.2.6.4.

**WBS** MAINTENANCE ITEM 1.1.2.6 POWER NO. DESCRIPTION TRANSMISSION 1.1.2.6.1 "FREE-FLYERS" OR BARGE FOR I VEHICLE UTILIZATION CARGO AND PERSONNEL (COMMON USE ITEM) SET 1.1.2.6.2 GANTRY CRANE AT ANTENNA SET ON-CRANE CONTROL CENTER, 1.1.2.6.3 HOISTS, EQUIPMENT TEST GEAR, ROBOT I CALS TRACKS AND ACCESSWAYS 12000 kg 1.1.2.6.4

Table 1.1.2.6 Maintenance Requirements

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.2.6.1 MAINTENANCE - FREE FLYERS TABLE

	INPUT PAR	AMETERS			INPUT CO	INPUT COEFFICIENTS
<b>_</b>	5000.00000	<b>∓</b> F=	1.000000	000	CDCER=	0.0
# <b>*</b>	5000.00000	=W30	0.0	200	XP=	0.0
CF=	1.250000	=17	1.000000	010	CICER=	0.005798
₽H [=	0.950000	12=	00000009	CIE	CI EXP=	1.000000
<b>%</b>	0.02000	73=	60.00000			
DF=	1.000000	= 4 Z	000000*09	= 57	0.0	
CALCULATED	ATED VALUES	KG	SUM TO 1.	1.1.2.6		SHILL FONS
CD=CDCER X	CD=CDCER X (T X DF)XX(CDEXP)	Y ČF		;		0.0
CL RM=CICER	CLRM=CICER X (M)XX(CIEXP) X CF	CF X TF				36.238
#RM = T / M						1.000
E =1.0 +	=1.0 + LOG(PHI) / LOG12.0	.0)				0.926
CTFU= (CLRM	CTFU=(CLRM / E)X((#RM X 21+.5	+.5)XX(E) -0.5XX(E))	).5XX(E))			36.368
CTB = ((CLRM/E)X((#RM X		73 + 0.5) XX(	0.5) XX(E) -0.5XX(E))	-	/ 23	28.784
CIPS=CTB*Z4/Z2	/12	:				28.784
CRCI =	=CTB X R					0.576
= W300	COEM = OEM OR CT8*25/22/ENYR	/ ENYR				0.0
COMMENTS				!		

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.2.6.2 GANTRY CRANE TABLE

	INPUT PARAM	ARAMETERS			INPUT CO	INPUT COEFFICIENTS
<b>_</b>	40000.0000	TF=	1.000000		CDC ER=	0.234000
## #	40000.0000	=W30	0.0		CDEXP=	0.653000
CF	1.100000	21=	1.000000		CI CER=	0.00000
=IHd	1.000000	22=	000000.09		C1 EXP=	1.000000
R=	0.002000	<u>7</u> 3=	000000.09			
DF=	0.20000	<b>7 4</b> =	000000009	= 57	0.0	
CALCUI	CALCULATED VALUES	KG	SUM TO	1.1.2.6		\$, MILL IONS
CD=CDCER X	(T X DF)XX(CDEXP)	X CF				91,060
CLRM=CICER	X (M)XX(CIEXP) X	X CF X TF				0.220
#RM =T / M						1.000
E = 1.0 +	=1.0 + LOG(PHI) / LOG(2.0)	•0)				1.000
CTFU=(CLRM	CTFU=(CLRM / E)X((#RM X 21+	Z1+.5)XX(E) -0	-0.5XX(E))	,		0.220
CTB = ((CLRM/E)X((#RM	4/E)X((#RM X Z3	+	0.51XX(E) -0.5XX(E))		1 / 23	0.220
CIPS=CTB*24/22	4/12					0.220
1282	=CTB X R					00000
= W3D2	06M OR CTB*25/Z2/ENY	/ENYR				0.0
COMMENTS				:		

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.2.6.3 ON-CRANE CONTROL CENTER TABL E

INPUT COEFFICIENTS	0.012432	1.000000	0.005798	1.000000			S. MILL IONS	621.600	289.900	1.000	0.926	30 • 3 05	267.824	26.782	5.356	0.0	
INPUT CO	COC ER=	CDEXP=	CICER=	CI EXP=		0.0							1 / 23			. '	
:						= 57	1.1.2.6										:
	1.000000	0.0	0.00000	60,000000	000000.9	00000009	SUM TO					-0.5XX(E))	+ 0.5)XX(E) -0.5XX(E))				
ARAMETERS	<b>∓</b> F=	=W30	21=	2.2=		= 7 7	KG	) X CF	X CF X TF		(0.	5)XX(E)	Z3 + 0.5) XX(			2/ENYR	•
INPUT PA	50000,0000	50000.0000	1.000000	0.00056.0	0.02000	1.000000	CALCULATED VALUES	(T X DF)XX(CDEXP)	X (M)XX(CIEXP) >		=1.0 + LOG(PHI) / LOG(2.0)	CTFU=(CLRM / E)X((#RM X Z1+.	×	*/22	=CTB X R	0£M OR CT8*25/22/	
	## 	11 2	C F=	=1 Hd	2	0F=	CALCUI	CO=COCER X	CLRM=CICER	#RM = 1 M	+ 0. II II	CTFU=(CLRM	CTB =: ((CLRM/E)X((#RM	CIPS=CTB*24/22	CRCI	≡ W3DD	COMMENTS

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.2.6.4 TRACKS & ACCESS WAYS TABLE

INPUT PARA T= 12000.0000	ARAMETERS TF=	1.000000	INF COCER=	PUT COE	INPUT COEFFICIENTS = 0.0
12000.0000	= W3 O	0.0	CDEXP=		0.0
1.000000	21=	1.000000	CI CER=		0.00000
1.000000	22=	000000.09	CI EXP=		1.000000
0.002000	23=	000000.09			
1.000000	= 7 7	000000009	= 57	0.0	
CALCULATED VALUES	KG	SUM TO 1.	1.1.2.6		\$, MILL IONS
(T X DF)XX(CDEXP	) X CF		;	!	0.0
(M)XX(CIEXP) X	CF X TF				090°0
					1.000
+ LOG(PHI) / LOG(2.0)	.0)				1.000
E)X((#RM X Z1+	Z1+.5) XX(E) -0.5XX(E))	5XX(E))			090°0
CTB = ((CLRM/E)X((#RM X Z	Z3 + 0.5) XX(E)	) -0.5XX(E))	) / 23		090*0
CIPS=CTB*Z4/Z2				; ;	090.0
CTB X R					000*0
06M OR CT8*Z5/Z2/ENYR	ZENYR .				0.0

#### 1.1.3 INFORMATION MANAGEMENT AND CONTROL

This element includes those components that process information onboard the satellite. This includes sensing, signal conditioning, formatting, computations, and signal routing.

The information management and control subsystem (IMCS) provides the interconnecting elements between and within all the various satellites and ground-based operational subsystems. The IMCS also provides operational control of both the satellite and ground systems as well as providing all subsystem processing support for all but very special functions.

The satellite IMCS consists of the on-board processing equipment [central processing units (CPU) and memories], the inter- and intra-subsystem data network (data buses), the man-machine interfaces (display/control), and intersystem communication links, including RF, but excepting those specifically provided for the control and transfer of primary power, and all elements provided to accommodate activities related to system security, safety, or any other operation necessary to the continuing operation of the SPS.

Because of the early stage of program analysis, only those requirements imposed upon the IMCS by a limited number of satellite operations have been identified. The identified requirements generally are limited to those associated with the immediate operations of an active satellite. Auxiliary functions such as ground/space communications, display/control, safety, security, etc., will be added when data become available.

The usage and application of IMCS items is identified in Table 1.1-3 and provides direct association with the subsystem functions.

	INSTRU	MENTATION	DATA A	CQUISITION	DATA	PR	OCE	SSING	CONTR	OL	
ELEMENT DESCRIPTION	SENSORS	SIGNAL CONDITIONING	SOFTWARE	SIGNAL ROUTING	SOFTWARE	FORMATTING	COMPUTATION	DISPLAY GENERATION	DISPLAYS 6 CONTROLS	SIGNAL, CONDITIONING	WBS NO.
MASTER CONTROL COMPUTER					x	x	x	x			1.1.3.1
DISPLAYS CONTROL	1				x	X	X	X	x		1.1.3.2
SUPERVISORY COMPUTER	1				x	X	X	1	ĺ		1.1.3.3
REMOTE COMPUTER	ļ				x	x	X				1.1.3.4
BUS CONTROL UNIT	İ		x	X	х	X	X				1.1.3.5
MICROPROCESSORS	l				х	X	X				1.1.3.6
REMOTE ACQ. & CONTROL	l		x	x	х	X	X			X	1.1.3.7
SUB-MULTIPLEXER	1		x	х .	х	X	X				1.1.3.8
INSTRUMENTATION	х	X									1.1.3.9
FIBER OPTICS				x							1.1.3.10
CABLES & HARNESSES	×	x	×	x	x	X	X	x	×	x	1.1.3.11

Table 1.1-3. Usage/Application Matrix per Satellite

These items have been separated into general hardware groups for costing purposes.

### COMPUTERS

Historical cost data were obtained for computers from the Redstar Data Base system and are listed below:

• Gemini-3

• Viking Lander

Minuteman

• MOL

Skylab

• HEAO

A 50% integration factor was included in the DDT&E CER's to allow for subsystem level costs.

Range of Data:

DDT&E and ICI: 1.8 to 75.7 kilograms

### ELECTRONIC COMPONENTS

The electronic components associated with Avionics include the Submultiplexors, Remote Acquisition Units, Microprocessors, Bus Control Units and instrumentation.

Development of an electronic components CER was based on the selected components of the ATS-F and OSO-8 spacecraft. These 19 electronic components are listed below:

ATS-F

0S0-8

Aux. Digital Sun Sensors

Monopulse Unit

Wide Band Data Unit

C Band Data Unit

S/L Band Transmitter

VHF Receiver Command Decoder

Data Acq. & Control Unit

Data Switching Unit

Solar Power Supply

Power Supply

Control Decoder/Demodulator

Remote Decoder

PCM Decoder

Format Generator

Wheel Clock

Sail Clock

S Band Transmitter

VHF Transmitter

Range of Data:

DDT&E and ICI: 1.1 to 19.6 kilograms

### DATA BUS

This element consists of both copper wire and fiber optics. Historical cost data were obtained from the Redstar Data Base to produce the data bus DDT&E CER. Commercial prices were used for the data bus ICI CER.

Production cost information obtained from private industry for "off-the-shelf" fiber optics and copper wire are listed below:

# FIBER OPTICS:

Manufacturer	<u>Type</u>	Characteristics	Cost per Meter
ITT Electro-Optical Products Division	GG-02	Single Fiber 50 m Dia.	(1-10 km) \$3.25
	GS-02	Single Fiber 50 m Dia.	\$2.50
Valtec Fiberoptics Division	MG-05	Single Fiber 65 m Dia.	\$2.50
Galileo Electro- Optics Corporation	-	Single Fiber 88 m Dia.	\$1.58
	Average	cost per meter	\$2.40

One industry spokesman estimates that the cost of optical fibers would likely decrease to 40% by 1980. This study assumes a \$2.40 per meter average price reduced by 40% to \$1.44 per meter.

# COPPER WIRE:

Manufacturer	Characteristics	Cost per Meter
Dearborn Wire & Cable	22 gage stranded silver plate	\$0.807
Standard Wire & Cable	22 gage stranded silver plate	\$0.7 <b>0</b> 5
Karen, Inc.	22 gage, 2 conductor silver plate	\$0.807
Mil-Spec Wire & Cable Corporation	22 gage, 19-30 stranded	\$0.610
	Average cost per meter	\$0.732

Instrumentation input parameters T&M are in kilograms.

Cost estimates for the items of Table 1.1-3 are presented in Tables 1.1.3.1 through 1.1.3.11 inclusive.

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.3.1 MASTER CONTROL COMPUTER TABLE

		d TUPUT	INPUT PARAMETERS			ŽI	INPUT COF	COEFFICIENTS
	<u>"</u>	1000.00000	TF:	000006*0		CDCER=		0.633000
	# <u></u>	200,000000	=W30	0.0		CDEXP=		0.521000
	C F=	1.000000	=17	1.000000		CICER=		0.172000
	PH I≍	0.00008.0	22=	60.00000		CI EXP =		0.535000
	<b>A</b>	0.010000	73=	60.00000				
	0 F=	0.50000	= + 7	000000•09	<b>≈ 97</b>		0.0	
	CALCUL	CALCULATED VALUES	KG	SUM TO 1.	1.1.3			\$, MILL IONS
ï	CO=COCER X	(T X DF)XX(CDEXP)	) X CF					16.127
	CLRM=CICER	X (M)XX(CIEXP)	X CF X TF					4.302
В-	#RM =T / M							2.000
-80	E =1.0 +	=1.0 + LOG(PHI) / LOG(2.0)	• 0 •		**			0.678
	CTFU=(CLRM	/ E)X((#RM X Z1+.5)	XX(E)	-0.5XX(E))				7.845
	CTB = ((CLRM/E)X((#RM	×	Z3 + 0.5)XX(E	0.5)XX(E) -0.5XX(E))		1 / 23		2.659
	CIPS=CTB*24/22							2.659
	CRCI =	CTB X R						0.027
	# W300	06M OR CT8*25/22/EN	/ENYR					0.0
•	COMMENTS					1		

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.3.2 DISPLAYS & CONTROLS TABLE

İ		INPUT PAR	SARAMETERS .		:	INP	JT COE	INPUT COEFFICIENTS
	<u>=</u>	200.000000	TF=	0.90000		COCER=		0.102000
	¥	200.000000	=W30	0.0		CDEXP=		0.8 79000
	CF.	1.000000	7.1=	1.000000		CICER=		0.069000
	₽HI≃	000008.0	=27	000000009		CI EXP=		0.557000
! 	**	0.010000		000000009				
	0F=	1.000000	= 7 7	000000009	= 57		0.0	
	CAL CUL A	CALCULATED VALUES	KG	SUM TO 1	1.1.3			S.MILLIONS
	CD=CDCER X (	CD=COCER X (T X DF)XX(CDEXP)	) X CF		:		-	10.745
	CLRM=CICER X	CLRM=CICER X (M)XX(CIEXP) X	X CF X TF					1.188
В-	#RM =T / M							1.000
-81	E =1.0 + L(	=1.0 + LOG(PHI) / LOG(2.	2 • 0)					0.678
	CTFU=(CLRM /	CTFU=(CLRM / E)X((#RM X Z1+.	5) XX(E)	-0.5XX(E))				1.211
	CTB = ((CLRM/E)X((#RM	×	23 + 0.5) XX(	+ 0.5) XX(E) -0.5XX(E))		) / 23		0.453
	CIPS=CT8*Z4/Z2						: : :	0.453
	CRCI =CTB	TB X R						0.005
	0 = W300	COEM = 0EM OR CT8*25/22/ENYR	2/ENYR					0.0
i	COMMENTS							

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.3.3 SUPERVISORY COMPUTER TABLE

		ָ ב נ	000001		10000		000000000000000000000000000000000000000
M= 14.00	14.000000	0 	0.0		CDEXP=		0.521000
	1.000000	=17	1.000000		CI CER=		0.172000
	50000	2.2=	60.000000		CI EXP=		0.535000
	0.01000	23=	000000009				
DF= 0.2(	00000	= + 7	000000009	= 57		0.0	
CALCULATED VALUES	ES	KG	SUM TO 1.	1.1.3			S+ MILL FONS
CD=CDCER X (T X DF)XX(CDEXP)	X(CDEXP)	X CF					2,753
CLRM=CICER X (M)XX(CIEXP)	×	CF X TF					767.0
=1 / H							000°9
=1.0 + LOG(PHI) / LOG(2.0)	/ LOG(2.	0)					0.766
CTFU=(CLRM / E)X((#RM	M X Z1+.5)	XX(E)	-0.5XX(E))				2,325
CTB = ((CLRM/E)X((#RM	x 23	+	0.5)XX(E) -0.5XX(E))		1 / 23		696*0
CIPS=CTB*24/22							696*0
CRCI = CTB X R							010.0
COEM = OEM OR CTI	CT8*25/22/ENYR	ENYR					0.0

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.3.4 REMOTE COMPUTER TABL E

!		INPUT PAR	ARAMETERS			INPUT	INPUT COEFFICIENTS
	<u>"</u>	518.000000	ŢF=	0.40000		CDCER=	0.633000
ì	<b>!</b>	14.000000	=W30	0.0		CDEXP=	0.521000
	CF=	1.000000	7.1=	1.000000		CI CER=	0.172000
	PHI=	0.850000	N	000000000		CI EXP=	0.535000
i	11	0.010000	73=	000000009		•	
	DF=	0.030000	= + 7	00000009	= 57	0.0	
	CALCULA	CALCULATED VALUES	KG	SUM TO 1.	1.1.3		S.MILL IONS
;	CD=CDCER X (	CD=COCER X (T X DF)XX(CDEXP)	) X CF				2.643
	CLRM=CICER X	CLRM=CICER X (M)XX(CIEXP) X C	CF X TF				0.282
В-	#PM =1 / M						37.000
-83	E =1.0 + L(	=1.0 + LOG(PHI) / LOG(2.0	.00		!		0.766
	CTFU=(CLRM / E)X((#RM	E)X((#RM X Z1+.5	)XX(E)	-0.5XX(E)}			969°5
(	CTB = ((CLRM/F)X((#RM	×	23 + 0.5) XX(	0.5) XX(E) -0.5XX(E))		1 / 23	2.238
;	CIPS=CTB*Z4/Z2	7.5					2.238
	CRCI =CTB	78 X R					0.022
	0 = W300	06M OR CT8*25/22/E	/ENYR				0.0
:	COMMENTS						

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.3.5 BUS CONTROL UNIT TABLE

!		INPUT	PARAMETERS			INPUT CO	INPUT COEFFICIENTS
	<u>"</u>	4110.00000	<b>∓</b> F=	0.076000	ວັ	CDC ER =	0.102000
	¥	5.000000	=W3 O	0.0	5	)EXP=	0.879000
	CF=	1.000000	21=	1.000000	ວ	CER=	0.069000
	PHI=	0.950000	-22	000000.09	5	EXP=	0.557000
1	a.	0.01000	£3=	000000009			
	0F=	0.001200	= + 7	00000009	= 57	0.0	
1	CALCUL	CALCULATED VALUES	KG	SUM TO 1.	1.1.3		S.MILL IONS
1	CD=CDCER X	(T X DF)XX(CDEXP)	) X CF			:	0.415
	CLRM=CICER	X (M)XX(CIEXP) X	CF X TF				0.013
B-6	#RM =T / M						822,000
,	E =1.0 +	+ LOG(PHI) / LOG(2.0)	• 0)	-			0.926
	CTFU=(CLRM	/ E)X((#RM X Z1+.51	XX(E)	-0.5XX(E))			0 * 6 * 9 * 0
	CTB = ((CLRM/E)X((#RM	×	Z3 + 0.5) XX(E)	E) -0.5xX(E))		62 / (	5.128
i i	CIPS=CTB*24/22	./12					5.128
	CRCI =	=CTB X R					0.051
	= W300	06M OR CTB*Z5/Z2/EN	/ENYR				0.0
	COMMENTS						

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.3.6 MICROPROCESSORS TABLE

INPUT COEFFICIENTS	0.102000	0.8 79000	000690.0	0.557000			\$, MILL IONS	0.431	0.013	792.000	0.926	188.9	5*085	5*085	0.051	0.0	
INPUT CO	CDCER=	CDEXP=	CI CER=	CI EXP=		0.0							1 / 23				
	0.078000	0.0	1.000000	0000000	60.00000	= 57 0000000*09	SUM TO 1.1.3					-0.5XX(E))	+ 0.5) XX(E) -0.5XX(E))				
ARÄMETERS	TF=	=W30	<b>5</b> 1 =		73=	= + 7	KG	X CF	CF X TF		.0)	5) XX(E)	Z3 + 0.5) XX(			/ENYR	
INPUT PA	3960,00000	2.000000	1.000000	0.00056.0	0.010000	0.001300	CALCULATED VALUES	CD=COCER X (T X DF)XX(CDEXP	CLRM=CICER X (M) XX(CIEXP) X		=1.0 + LOG(PHI) / LOG(2.	CTFU=(CLRM / E)X((#RM X Z1+.	×	.72	=CTB X R	06M OR CT8*25/22/	
	11	<del>"</del>	# #	PH I=	<b>4</b>	0F=	CALCUL	CD=CDCER X	CLRM=CICER )	#RM = 1 / M	= 1°0 + C	CTFU=(CLRM ,	CTB = ((CLRM/E)X((#RM	CIPS=CTB*24/22	CRCI =(	) = W3D3	COMMENTS

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.3.7 REMOTE ACQUISITION & CONTROL TABLE

: <b>1</b>	1	INPUT PARA	PARAMETERS TF=	0.069000	1	INP	UT COE	INPUT COEFFICIENTS  0.10200
- 2		5.000000	=W30	0.0		CDEXP=		0.879000
C.F.	11	1.000000	21=	1.000000		CI CER=		000690.0
PH [=	11	0.950000	12=	000000000		CIEXP=		0.557000
<b>8</b>		00001000	73=	000000009				
0F=	и	0.001000	= 7 7	000000009	= 57		0.0	
Ü	AL CUL A	CALCULATED VALUES	KG	SUM TO 1.	1.1.3			\$ • WILLIONS
כס=כסכ	ER X	CD=CDCER X (T X DF)XX(CDEXP)	P) X CF				1	0.414
CLRM=CICER		X (M)XX(CIEXP)	X CF X TF					0.012
#RM =T /	¥ \							985.000
= 1	• 0 + L(	1.0 + LOG(PHI) / LOG(2.0)	2.0)		:			0.926
CT FU= ( CLRM	CLRM /	E)X((#RM X Z1.	Z1+.5)XX(E) -0	-0.5XX(E))				7.450
CTB = (	(CLRM/E	=((CLRM/E)X((#RM X	Z3 + 0.51 XX(E)	E) -0.5XX(E))		1 / 23		5.505
CIPS=C	CIPS=CTB*24/22	2.2						5.505
CRCI	CI = CTB	TB X R						0.055
Ü	COEM = 08	0&M OR CT8*25/22/EN	2/ENYR					0.0
COMMENTS	TS						# # ! : :	

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.3.8 SUBMULTIPLEXORS TABLE

	INPUT PAR	ARAMETERS			INPUT CO	INPUT COEFFICIENTS
<b>T</b> ≈	93000.0000	TF=	0.022000	CDC ER=	n	0.102000
<b>₩</b>	3.00000	=W30	0.0	CDEXP	19	0.8 79000
C F=	1.000000	=12	1.000000	CICER=	şı	0.06900
PH I=	0.980000	-27	00000009	CIEXP	11	0.557000
<b>"</b>	0.010000	23=	60.00000			
0F=	0.000032	= + 7		= 57	0.0	
CALCUI	CALCULATED VALUES	KG	SUM TO 1.1.3	3		S, MILLIONS
CD=CDCER X	CD=CDCER X (T X DF)XX(CDEXP)	XCF		:		0.266
CLRM=CICER	X (M)XX(CIEXP) X	CF X TF				0.003
HRM = T / M						31000.000
+ 0•III	=1.0 + LOG(PHI) / LOG(2.0	• 0)		***************************************		0.971
CTFU={CLRM /	/ E)X((#RM X Z1+.	5) XX(E)	-0.5XX(E))			66.119
CTB = ((CLRM/E)X((#RM	×	23 + 0.5) XX(	+ 0.5) XX(E) -0.5XX(E))	` `	/ 23	58.682
CIPS=CTB*24/22	4/22					58.682
CRCI	=CTB X R					0.587
= W3D0	06M OR CTB*25/22/	/ENYR				0.0
COMMENTS						

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.3.9 INSTRUMENTATION TABLE

	INPUT PARAM	ARAMETER S			INPUT CO	INPUT COEFFICIENTS
=	280000.000	TF=	1.000000	CDC ER=	#	0.000100
<b>=</b>	0.074100	=W30	0.0	CDEXP	91	1.000000
C F=	1.000000	21=	1.000000	CICER	11	0.000400
PH I=	0.980000	=27	000000009	CI EXP=	ĮĮ.	1.000000
<b>8</b>	0.010000	73=	60.00000			
0F=	1.000000	= 47	000000.09	= 57	0.0	
CALC	CALCULATED VALUES	KG	SUM TO 1.	1.3		S'WILLIONS
CD=CDCER )	CD=CDCER X (T X DF)XX(CDEXP)	X CF				28.000
CLRM=CICE	CLRM=CICER X (M)XX(CIEXP) X	CF X TF				000*0
#RM = 1 / M	<b>.</b>					3778676.00
88- E = 1•0	=1.0 + LOG(PHI) / LOG(2.0)	.0)				0.971
CTFU=(CLR!	CTFU=(CLRM / E)X((#RM X Z1+	Z1+.5)XX(E) -0.	-0.5XX(E))			74.192
CTB = ((CL)	CTB =([CLRM/E)X((#RM X Z	Z3 + 0.51 XX(	0.5) XX(E) -0.5XX(E))	) / 23	23	65.846
CIPS=CTB*24/22	74/12				: :	65.846
CRCI	=CTB X R					0.658
: M300	COEM = 0EM OR CTB*25/22/ENYR	/ENYR				0.0
COMMENTS		:				

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.3.10 OPTICAL FIBER TABLE

		INPUT P	PARAMETERS			INPUT CD	INPUT COEFFICIENTS
	<u>"</u>	62.000000	TF=	1.000000	כם	CER=	0.237000
1	- 2	62.000000	=W30	0.0	5	EXP=	0.297000
	C.F.	1.000000	=17	1.000000	CI	CICER=	0.010219
	PHI=	000086.0		000000.09	10	EXP=	1.000000
	~	0.010000	73=	000000.09			**
	0F=	1.000000	= + 7	000000009	= 57	0.0	
	CALCULAT	CALCULATED VALUES	KG	SUM TO 1.	1.1.3		S. MILL IONS
	CD=CDCER X (T	CD=COCER X (T X DF)XX(CDEXP)	) X CF				0.807
	CLRM=CICER X	(M)XX(CIEXP) X	CF X TF				0.634
1	#RM =T / M						1.000
1	E = 1.0 + LDC	1.0 + LOG(PHI) / LOG(2.	.0)				0.971
	CTFU=(CLRM / E)X((#RM	E)X((#RM X Z1+.	5) XX(E)	-0.5XX(E)}			0.634
1	CTB = ((CLRM/E)X((#RM	×	Z3 + 0.51XX(E	+ 0.51XX(E) -0.5XX(E)		1 23	0.578
	CIPS=CTB*Z4/Z2	2			!		0.578
1	CRCI =CTB	8 × R					900.0
	M30 = M300	M DR CT8*25/22/	/ENYR.				0.0
	COMMENTS						

ROCKWELL SPS\_CR-2 REFERENCE CONFIGURATION 1.1.3.11 CABLES/HARNESS TABLE

		A TUPUI	PARAMETERS			IN	יטד כס	INPUT COEFFICIENTS
	<b>=</b>	293000.000	TF=	1.000000		COCER=		0.237000
	1	293000.000	-M30	0.0		CDEXP=		0.297000
	CF≅	1.000000	=17	1.000000		CI CER=		0.000060
	=1 Hd	0.980000	2.2=	000000.09		CIEXP=		1.000000
į	~	0.010000	73=	000000009				
	DF=	1.000000	= + 7	000000*09	= 57		0.0	
	CALCUI	CALCULATED VALUES	KG	SUM TO 1.	1.1.3			\$, MILLIONS
1	CD=CDCER X	CD=CDCER X (T X DF)XX(CDEXP)	) X CF				; ;	6963
	CLRM=CICER	X (M)XX(CIEXP) X	CF X TF					17.580
В-	#RM =T / M				ļ.  -			1.000
90	= 1.0 +	=1.0 + LOG(PHI) / LOG(2.0)	• 01					0.971
	CTFU=(CLRM /	/ E)X((#RM X Z1+.5)	XX(E)	-0.5XX(E)				17.604
	CTB = ((CLRM/E)X((#RM	×	23 + 0.51 XX(E	0.51XX(E) -0.5XX(E))		1 / 23		16.047
1	CIPS=CTB*Z4/Z2	4/12			         			16.047
	CRCI	=CTB X R						0.160
	= W300	0&M OR CT8*25/22/ENYR	/ENYR					0.0
1	COMMENTS						 	

#### 1.1.4 ATTITUDE CONTROL AND STATIONKEEPING

This element includes the components required to orient and maintain the satellite's position and attitude in geosynchronous orbit. Included are sensors, reaction wheels, chemical and electric propulsion hardware and propellants.

The baseline ACSS features an argon ion bombardment thruster RCS whose characteristics are:

- · Thrusters located in 4 modules at each corner of the satellite
- Each module has 16 thrusters
- Cryogenic propellant storage-electric refrigeration with heat loss makeup
- · Hemispherical plume characteristics
- · Serviceable in place

The system operates on an average of 36 thrusters. A total of 64 thrusters are included to provide the required redundancy. The redundancy was based on an annual maintenance/servicing interval, 5000 hour thruster grid lifetime and 5-year thruster MTBF. Sixteen thrusters are located on the lower portion of each corner of the spacecraft. Each thruster is gimbaled individually to facilitate thruster servicing, to permit operation of adjacent thrusters during servicing, and to provide the redundancy. The thrusters nominally provide a force approximately in the direction of the sun to counter the solar pressure force (stationkeeping) which is the dominant thruster requirement. The thrusters are gimbaled through small angles (as illustrated) and differentially throttled to provide the remaining forces and torques for attitude control and stationkeeping.

Sensors that make up the attitude reference determination system include:

- CDD Sun Sensor (1/System)
- CCD Star Sensors (2/Systems)
- Electrostatic or laser gyros (3/System)
- · Dedicated mini processor

The attitude reference determination system features Charge Coupled Device (CCD), star and sun sensors as well as electrostatic or laser gyros and dedicated microprocessors. Seven attitude reference determination units are located at various locations on the satellite in order to sense thermal and dynamic body bending, and to desensitize the system to these disturbances. The control algorithms will feature statistical estimators for determining principal axis orientation, body bending state observers or estimators, and a quasi-linear propulsion thrust command policy to provide precise control and minimize structural bending excitation.

The mass properties of the ACSS are summarized in Table 1.1-4. This summary includes the mass of individual elements and propellant weight on an annual basis.

Table 1.1-4. ACSS Mass Summary

ITEM	MASS (x 10 <sup>+3</sup> KG)
ATTITUDE REFERENCE DETERMINATION SYSTEMS (7)	0,32
THRUSTERS—INCLUDING SUPPORT STRUCTURE, 64 @ 120 kg/Thruster	7.68
THRUSTER GIMBALS AND MOUNTING	3, 98
TANKS, LINES, REFRIGERATION	15.07
POWER PROCESSING EQUIPMENT	88, 95
TOTAL (DRY)	116, 00
ARGON PROPELLANT—ANNUAL REQUIREMENT	85, 39
TOTAL (WITH PROPELLANT)	201, 39

Historical cost data were obtained from NASA's Redstar Data Base. Historical data relative to electrical propulsion is limited, consequently, study data have been utilized where necessary. Ion bombardment thrusters are Argon propellants with a low thrust but a significantly higher specific impulse, thus reducing propellant resupply cost.

Development of the propulsion subsystem CER's was based on the spacecraft programs listed below:

SEPS (Boeing) Study SEPS (Rockwell) Study ATS-F (Ion Experiment)
Rockwell SPS Study

SERT-II

SERT-C Study

Range of Data:

DDT&E and ICI: 18.0 to 107,500.0 kg

Input parameters T&M are in kilograms.

Tables 1.1.4.1 and 1.1.4.2 contain the costs for this element.

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.4.1 ACSS HARDWARE TABLE

	INPUT PAR	ARAMETERS			INPUT CO	INPUT COEFFICIENTS
<b>=</b>	116000.000	TF=	0.105900	COCER=	11	1.122000
1	1812.00000	0£M=	0.046620	COEXP=	19	0.190000
C.F.	1.000000	21=	1.000000	CICER	II	0.057000
=I Hd	0.0006	22=	000000.09	CIEXP	#1	0.729000
<b>a</b>	0.010000		00000009			
DF=	00000 8.0	= 47	000000009	= 57	0.0	
CALCL	CALCULATED VALUES	KG	SUM TO 1.	1.1.4		S, MILLIONS
CD=CDCER X	CD=CDCER X (T X DF)XX(CDEXP)	) X CF				8.183
CLRM=CICEF	CLRM=CICER X (M)XX(CIEXP) X C	CF X TF				1.432
#RM =T / M	-					64.018
E =1.0 +	=1.0 + LOG(PHI) / LOG(2.0	•0)				0.926
CTFŲ=(CLR≯	CTFU=(CLRM / E)X((#RM X 21+.5	) XX(E)	-0.5XX(E))			72.488
CTB = ((CLA	CTB =((CLRM/E)X((#RM X Z	Z3 + 0.5) XX(8	0.5) XX(E) -0.5XX(E))	1 / 23	23	53.746
CIPS=CTB*24/Z2	74/12					53.746
CRCI	=CTB X R					0.537
= W300	= 06M OR CTB*25/22/E	/ENYR				0.047
COMMENTS		:				

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.4.2 ACSS PROPELLANT TABL E

= 1					INTO COEFFICIENTS
	1.000000	<u> </u>	1.000000	COCER=	0.0
	1.000000	=W30	0.085390	CDEXP=	0.0
C F=	1.000000	71= .	1.000000	CICER=	0.0
	1.000000	75=	000000.09	CIEXP=	0.0
	0.0	23=	000000.09		
0F=	1.000000	_ = <b>5</b> Z	000000009	0.0 = 52	
CALCULATED VALUES	/ALUES		SUM TO 1.	1.1.4	\$.MILLIONS
CD=CDCER X (T X D	DF)XX(CDEXP)	X CF			0.0
CLRM=CICER X (M)X	(M)XX(CIEXP) X	CF X TF			0.0
#RM = 1 / M					1.000
E =1.0 + LOG(PHI) / LOG(2.0)	(1) / 106(2	• 0)			1,000
CTFU=(CLRM / E)X(	E)X((#RM X 21+	Z1+.5)XX(E) -0.	-0.5XX(E))		0.0
CTB = ((CLRM/E)X((#RM	#RM X Z3	+	0.5) XX(E) -0.5XX(E))	) / 23	0*0
CIPS=CTB*Z4/Z2		: :			0.0
CRCI =CTB X	( R				0.0
COEM = OEM OR	CTB*25/22/ENYR	/ENYR			0.085

# 1.1.5 COMMUNICATIONS

This element includes the hardware to transmit and receive intelligence among the various SPS elements. It includes communication of both data and voice between the SPS and the control center, as well as among the various cargo and personnel vehicles. Excluded is intravehicular and intrasatellite communications.

# 1.1.6 INTERFACE (ENERGY CONVERSION/POWER TRANSMISSION)

This element provides the movable interface between the energy conversion subsystem and the power transmission subsystem. A 360° rotary joint and an antenna elevation mechanism are required to maintain proper alignment of the transmitter with the ground receiving station. Included are structure, mechanisms, power distribution, and maintenance hardware.

The interface is utilized to 1) transfer energy from the slip ring to the antenna via transmission brushes, and 2) act as the structural support member between the main satellite and the antenna. The elements of this movable interface (Figure 1.1-6) are described in the following subsections.

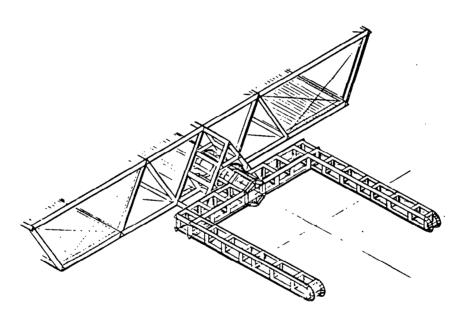


Figure 1.1-6. Energy Conversion/Power
Transmission Interface

#### 1.1.6.1 STRUCTURE

This element includes all members necessary to provide a mechanical interface between the primary structures of the energy conversion subsystem and the power transmission subsystem. It includes beams, beam couplers, cables, tensioning devices, and secondary structures. Excluded are elements of the drive assembly which are included in mechanisms (WBS No. 1.1.6.2).

# 1.1.6.1.1 Primary Structure

The basic supporting structure of the movable interface is included in this element. It is the primary load carrying structure and does not include the secondary structure that is required to support transmission buses or equipment.

The SPS requirement for low thermal distortion, under high thermal stress, dictates the need for a material with a very low coefficient of expansion. The most likely candidate, at this time, is a graphite composite material.

The interface primary structure D&D CER was developed using graphite composite data obtained from NASA's Redstar Data Base. Tooling cost was excluded under the assumption that this cost would be incurred in the development of orbital fabrication equipment. The following data points were used:

- · Space Telescope Shell
- ATS-F Truss
- · HEAO Optical Bench
- · Shuttle Payload Bay Doors

The interface structure ICI is the cost of raw materials only since the costs associated with fabrication and assembly are charged against orbital assembly and support equipment. The structure ICI cost equation is based on raw composite material stock (prepregnated graphite) cost. These material costs are based on vendor quotes obtained from Hercules, Fiberrite and Union Carbide.

# Range of Data:

D&D: 30.0 to 2000.0 kg

ICI: Unlimited

#### 1.1.6.1.2 Secondary Structure

The secondary structure consists of the passive interface attachment between the primary structure and operational subsystems. The structural members are made of aluminum with the ability to articulate, rotate, or otherwise support/allow motion between the primary structure and other subsystem elements.

This element includes all structure, consisting of mounting brackets, clamps and installation structure required as an interface and mounting attach

points of components, assemblies, and subsystems. It also includes any structure required between two or more components or assemblies.

Development of the secondary structure CER for DDT&E was based on cost data contained in the MSFC Redstar Data Base. Data from a variety of launch vehicle and unmanned satellite programs were available and the applicable data points are listed below:

• S-IVB Interstage

UNI

- S-IC Forward Skirt
- S-IC Intertank
- Solar Telescope Housing Assembly (ASM)
- Common Mount Assembly (ASM)
- Telescope Gimbal Assembly (ASM)
- Common Mount Actuators (ASM)
- Telescope Gimbal Actuators (ASM)
- Array Platform Elevation Pointing Actuator (ASM)
- UV Gimbal Mount Actuators (ASM)
- UV Instrument Mount Assembly (ASM)

- Solar Array and Boom Structure (ATS-F)
- Squib Interface Unit (ATS-F)
- Interstage (Centaur)
- Nose Shroud (Centaur)
- Fixed Airlock Shroud (Skylab)
- Payload Shroud (Skylab)
- Pallet Segment (Spacelab)
- OSO-1
- ATS-F
- S-II

The ICI production cost CER was based upon an Engineering Cost estimate.

# Range of Data:

DDT&E: 6.0 to 15,000.0 kg ICI: 6.0 to 15,000.0 kg

Input parameters T&M are in kilograms of mass.

# 1.1.6.1.3 Cost Estimates

Primary and secondary structure costs are presented in Table 1.1.6.1.1 and 1.1.6.1.2 respectively.

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.6.1.1 PRIMARY STRUCTURE TABLE

İ		INPUT PAR	ARAMETERS			TUPUT	INPUT COEFFICIENTS
	<b>₩</b>	120000.000	<b>T</b> F=	1.000000		CDCER≈	0.023000
	1	20000.0000	0£M=	0.0		CDEXP=	0.80000
	CF=	1.000000	=17	1.000000		CI CER=	0.000050
	=1 Hd	1.000000	, =27	60.00000		CIEXP=	1.000000
	R	0.002000	23=	60.00000			
	DF≕	0.020000	= 7 7	60.00000	= 57	0.0	
	CALCU	CALCULATED VALUES	KG	SUM TO 1.	1.9.1.		S+HILL IONS
	CD=CDCER X	CD=CDCER X (T X DF)XX(CDEXP)	X CF				11.638
	CLRM=CICER	CLRM=CICER X (M)XX(CIEXP)	X CF X TF				1.000
В-	#RM =T / M						000*9
-99 <sup>†</sup>	E = 1.0 +	=1.0 + LOG(PHI) / LOG(2.0	(0•				1.000
	CTFU=(CLRM	CTFU=(CLRM / E)X((#RM X Z1+.5)XX(E)		-0.5XX(E))			0000*9
	CTB = ((CLRM/E)X((#RM	×	Z3 + 0.5)XX(	0.5)XX(E) -0.5XX(E))		1 / 23	000*9
	CIPS=CTB*Z4/Z2	4/12			!		000*9
	CRCI =	=CTB X R					0.012
	= W3DD	CCEM = OEM OR CTB*25/22/ENYR	/ENYR				0.0
:	COMMENTS		;		•		

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.6.1.2 SECONDARY STRUCTURE TABLE

	INPUT PARA	ARAMETERS			INPUT CO	INPUT COEFFICIENTS
<b>=</b>	365000.000	TF=	0.007300	CDCER=	11	0 • 1 56000
=W	5.000000	-M30	0.0	CDEXP=	II (	0.511000
C F=	1.000000	21=	1.000000	CICER=		0.101000
=I Hd	0.00086.0	22=	000000.09	<b>CIEXP</b> ≈	"	0.355000
:   12   02	0.002000	23=	000000.09			
0F=	0.00050.0	= + 7	000000.09	= 57	0.0	
CALCUL	CALCULATED VALUES	KG	SUM TO 1.	1.6.1		S, MILL IONS
CD=CDCER X	(T X DF)XX(CDEXP)	X CF	: : : : : : : : : : : : : : : : : : : :			23.476
CLRM=CICER )	X (M)XX(CIEXP) X	CF X TF.				0.001
#RM =T / M						73000.000
E =1.0 + L	1.0 + LOG(PHI) / LOG(2.0)	• 0)				0.971
CTFU=(CLRM /	/ E)X((#RM X Z1+.	5) XX(E)	-0.5XX(E))			70.827
CTB = ((CLRM/E)X((#RM	/E)X((#RM X Z3	+	0.5) XX(E) -0.5XX(E)	) / 23	23	62.860
CIPS=CTB*24/22	/122					62.860
CRCI =(	=CTB X R					0.126
C 0 EM =	OEM OR CTB*25/22/EN	/ ENYR				0.0
COMMENTS				i		

### 1.1.6.2 MECHANISMS

This element includes the components required to rotate and elevate the power transmission subsystem. Included are the drive ring, bearings, gear drives, and drive motors.

The structural mechanisms consist of active structural subassemblies that articulate, rotate, or otherwise cause or allow motion between the primary structure and other subsystem elements or between subsystem elements themselves.

The ICI production cost CER was based on data provided by the following manufacturers:

Manufacturer	Application
Poly-Scientific	High energy
Poly-Scientific	Radar
Electro-Tec	Navy destroyer propeller system
Electro-Tec	Satellite solar array
I.E.C.	Navy shipboard hoist

Due to the difference in complexity and the specification requirements differences between ground and space qualified equipment, the following factors were applied.

Complexity Factor	×	3
Specification Uprating Factor	×	3
Total	×	9

# Range of Data:

DDT&E: 6.0 to 15,000.0 kg ICI: 6.0 to 15,000.0 kg

Input parameters T&M are in kilograms of mass, see Table 1.1.6.2.

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.6.2 MECHANISMS - INTERFACE TABLE

**1** 

	INPUT	PARAMETERS			INPUT CO	INPUT COEFFICIENTS
ŗ	391000.000	TF=	0.054900		CDC ER =	0.156000
Ξ	391.000000	0£M=	0.078000		CDEXP=	0.511000
CF.	1.000000	<b>512</b>	1.000000		CI CER=	0.000764
=I Hd	0.950000	7.5=	60.00000		CI EXP≈	0.05000
<b>*</b>	0.010000	23=	60.00000			
DF=	0.020000	= + 7	00000009	= 57	0.0	
CALCU	CALCULATED VALUES	KG	SUM TO 1.1.6	9.		S, MILL IONS
CD=CDCER X	CD=CDCER X (T X DF)XX(CDEXP) X	XCF				15.225
CLRM=CICER	X (M)XX(CIEXP) X	CF X TF				0.012
HRM = 1 / M						1000.000
+ 0°T = w	=1.0 + LOG(PHI) / LOG(2.0)	•0)				0.926
CTFU= (CLRM	CTFU=(CLRM / E)X((#RM X Z1+	Z1+.5)XX(E) -0.	-0.5XX(E))		·	7.878
CTB = ((CLR	CTB = ((CLRM/E)X((#RM X Z	Z3 + 0.51XX(E	0.5) XX(E) -0.5XX(E))		1 / 23	5.821
CIPS=CTB*Z4/Z2	4/22					5.821
CRCI	=CTB X R					0.058
= W300	OEM OR CT8*25/22/ENY	/ENYR				0.078
COMMENTS				ĺ		

#### 1.1.6.3 POWER DISTRIBUTION

This element transmits the electrical power from the rotary joint to the microwave power transmission system. The PD&C system consists of power risers which are coupled to the pickup shoebrushes on the rotary joint and routed on the antenna support yolk (interface) to the isolation switches on the antenna proper. There are two sets of slip rings. One positive and one negative, at the rotary joint. Sixteen brushes are needed per slip ring. The life expectancy of the PD&C is 30 years with calculated replacements of the slip ring.

### 1.1.6.3.1 Conductors and Insulation

The power risers are sized to minimize the mass of itself and the satellite mass, considering power requirements, efficiency and variation in resistivity with operating temperature. The power risers are made of multiple round aluminum (6101-T6) conductors with 1 mm kapton insulation.

# 1.1.6.3.2 Pickup Shoe Brushes

The pickup shoe brush portion of the rotary joint is included in the power distribution of the interface segment. Sixty-four pickup shoe brush assemblies are required per satellite. The brush material is 75%  $M_0S_2$  and 25%  $M_0tTa$  with a contact surface area per brush of 863 cm². The shoe dimension is 2.72 m × 12.7 am × 19 am with a total weight of 11341 kg for 64 pickup shoe brushes.

### 1.1.6.3.3 Power Distribution Cost Estimates

The CER presented in section 1.1.1.4.2 was used for the conductors and insulation. An extension of this CER was used for the brushes of section 1.1.6.3.2. The cost estimates for interface power distribution are presented in Tables 1.1.6.3.1 and 1.1.6.3.2.

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.6.3.1 CONDUCTOR & INSULATION TABLE

;	:	INPUT PARAM	ARAMETERS		:	INPUT CO	INPUT COEFFICIENTS	
	<u>"</u>	1267000.00	TF=	1.000000		CDC ER =	0.158000	
	Ĭ¥.	39594.0000	=W30	0.0		COEXP=	0 0 2 2 9 7 0 0 0	
	CF.	1.000000	<b>11=</b>	1.000000		CICER=	0.00004	
	=1 H d	1.000000	2 2=	000000.09		CI EXP=	1.000000	
i	<b>8</b>	0.0	73=	60.00000				
	DF=	0.100000	= 7 7	000000.09	= 57	0.0		
	CALCI	CALCULATED VALUES	KG	SUN TO 1.	1.1.6.3		S, MILLIONS	•
	CD=CDCFR )	CD=CDCFR X (T X DF)XX(CDEXP)	X CF		:	:	5.178	
	CLRM=CICE	CLRM=CICER X (M)XX(CIEXP) X	CF X TF				0.158	
I R.	#RM =T / N	Σ					32,000	
-104	E =1.0	=1.0 + LOG(PHI) / LOG(2.0)	.01				1.000	
	CT FU= (CLR)	CTFU=(CLRM / E)X((#RM X Z1+.5)	XX(E)	-0.5XX(E))			5.068	
	CTB = ((CL)	CTB = ((CLRM/E)X((#RM X Z3	+	0.51XX(E) -0.5XX(E))		) / 23	5.068	
	CIPS=CTB*24/22	24/22			:		5.068	
	CRCI	=CTB X R					0.0	
	" W3D0	= OEM OR CTB*25/22/ENYR	/ENYR				0.0	
i	COMMENTS				:			

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.6.3.2 SLIP RING BRUSHES TABLE

!		INPUT PAR	ARAMETERS		:	UANI	INPUT COEFFICIENTS	CIENTS
	<b>=</b>	11341,0000	<b>∓</b> ₽=	1.000000		CDCER=	0	0.158000
	1 2	531,000000	=W30	0.0		CDEXP=	0	.297000
	CF=	1.000000	=17	1.000000		CICER=	0	. 000500
	=I Hd	0.950000	= 27	00000000		CIEXP=	<b></b> 1	.000000
ļ	2	0.010000	73=	60.000000				
	DF=	0.02000	= + 7	000000.09	= 57	0	0.0	,
1	CALCUL	CALCULATED VALUES	KG	SUM TO 1.1	1.1.6.3			S+MILL IONS
;	CD=CDCFR X	(T X DF)XX(CDEXP	) X CF					0.791
	CLRM=CICER	X (M)XX(CIEXP) X	CF X TF					0.106
В-	#RM =T / M							21.358
105	E =1.0 +	+ LOG(PHI) / LOG(2.	• 0)		1			926*0.
	CT FU= (CLRM	CTFU=(CLRM / E)X((#RM X Z1+.	5) XX(E)	-0.5XX(E))				1.935
1	CTB = ((CLRM	=((CLRM/E)X((#RM X Z	Z3 + 0.5) XX(E)	E) -0.5XX(E))		1 / 23		1.442
; ;	CIPS=CTB*Z4/Z2	+/22						1.442
1	CRCI =	=CTB X R						0.014
	= W300	06M OR CTB*25/22/	ZENYR					0.0
İ	COMMENTS			:	:			

# 1.1.6.4 THERMAL CONTROL

This element includes any component used to modify the temperature of interface subsystem components. It includes cold plates, heat transfer and radiator devices as well as insulation, thermal control coatings and finishes. Excluded are paints or finishes applied to components during their manufacturing sequence. No thermal control requirements are defined for the interface.

#### 1.1.6.5 MAINTENANCE

This element provides for in-place repair or replacement of components and includes work stations, tracks, access ways, and insitu repair equipment.

Maintenance requirements are related to the equipment and facilities needed to transport men and material to the work station. Some of the same equipment required for maintenance at the site is used commonly in the performance of work at other sites. The CER's accommodate this usage. Table 1.1.6.5 identifies the requirements, and cost estimates are provided in Tables 1.1.6.5.1, 1.1.6.5.2, and 1.1.6.5.3.

Table 1.1.6.5 Maintenance Requirements

WBS NO.	MAINTENANCE ITEM DESCRIPTION	1.1.6.5 INTERFACE
1.1.6.5.1	"FREE-FLYERS" OR BARGE FOR CARGO AND PERSONNEL (COMMON USE ITEM)	.2 VEHICLE UTILIZATION
1.1.6.5.2	MANNED MANIPULATOR MODULE	1 VEHICLE
1.1.6.5.3	TRACKS AND ACCESS WAYS	24000 kg

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.6.5.1 MAINTENANCE - FREE FLYERS TABLE

	INPUT PARA	ARAMETERS		!	INPUT	INPUT COEFFICIENTS
# <b>_</b>	5000.00000	TF≂	1.000000		CDC ER=	0.0
#E	5000.00000	= W3 O	0.0		CDEXP=	0.0
CF=	1.250000	21=	0.20000		CI CER=	0.005798
=IHd	0 0 0 0 2 2 2 2 2 2 2 2 2 2	22=	00000000	_	CI EXP=	1.000000
<b>8</b>	0.02000	73=	12.000000			
0F=	1.000000	= + 7	12.000000	= 57	0.0	
CALCULA	CALCULATED VALUES	KG	SUM TO 1.1	1.1.6.5		S. MILL IONS
CD=CDCER X (	CD=CDCER X (T X DF)XX(CDEXP) X	X CF		1		0.0
CLRM=CICER X	(M)XX(CIEXP) X	CF X TF				36.238
R #RM = I / M						1.000
108	+ LOG(PHI) / LOG(2.0)	(0.				0.926
CTFU=(CLRM /	E)X((#RM X	21+.5)XX(E) -0	-0.5XX(E))			7.530
CTB = ((CLRM/E)X((#RM	×	23 + 0.51XX(	0.5)XX(E) -0.5XX(E))		1 / 23	32.098
CIPS=CTB*24/22	:	:		:		6.420
CRCI = C	CTB X R					0.642
) = W300	06M OR CT8*25/22/EN	/ENYR				0.0
COMMENTS		:				

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.6.5.2 MANNED MANIPULATOR TABL E

		INPUT PAR	ARAMETERS		i	a N I	UT COE	INPUT COEFFICIENTS
	=_	3000.00000	TF=	1.000000		COCER=		0.0
	1 2	3000.0000	=W30	0.0		CDEXP=		0.0
	C.F=	1.100000	21=	1.000000		CICER=		0.005798
	PHI=	0 0 0 0 2 2 2 2 2 2 2 2 2 2 2	22=	000000000		CI EXP=		1.000000
	*	0.02000	7.3=	000000*09				
	DF≕	1.000000	= 7 7	00000009	= 57		0.0	
	CALCULA	CALCULATED VALUES	KG	SUM TO 1.	1.1.6.5			S* MILL IONS
į	CD=CDCER X (	CD=CDCER X (T X DF)XX(CDEXP)	X CF					0.0
	CLRM=CICER X	(M)XX(CIEXP) X	CF X TF					19.133
B-	#RM =T / M							1.000
109	E = 1.0 + L	=1.0 + LOG(PHI) / LOG(2.0						0.926
	CTFU=(CLRM /	E)X((#RM X	Z1+.5)XX(E) -0	-0.5XX(E))				19.203
	CTB = ((CLRM/E)X((#RM	E)X((#RM X Z3	ļ	+ 0.5) XX(E) -0.5XX(E)		1 / 23		15.198
:	CIPS=CTB*Z4/Z2	22.	· !					15.198
	CRCI =C	=CTB X R						0.304
	D = W300	0£M OR CT8*25/22/	/ ENYR					0.0
:	COMMENTS				:			

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.6.5.3 TRACKS & ACCESS WAYS TABLE

	INPUT PARAM	ARAMETERS		NI	OUT COEF	INPUT COEFFICIENTS
<b>∓</b>	24000.0000		1.000000	CDC ER=		0.0
₩.	24000.0000	0 £M=	0.0	COEXP=		0.0
C.F.=	1.000000	-17	1.000000	CI CER=		0.00000
=1 Hd	1.000000	2.2=	000000.09	CI EXP=		1.000000
<b></b>	0.002000	Z3=	00000009			
0F=	1.000000	<b>5</b> 4=	000000.09	= 57	0.0	
CAL	CALCULATED VALUES	KG	SUM TO 1.	1.1.6.5		\$ MILLIONS
CD=CDCE	CD=CDCER X (T X DF)XX(CDEXP) X	) X CF				0•0
CLRM=CI(	CLRM=CICER X (M)XX(CIEXP) X	CF X TF				0.120
B-#RM =T	Σ /					1.000
ا ا س ا	=1.0 + LOG(PHI) / LOG(2.0)	•0)				1.000
CTFU=(CI	CTFU=(CLRM / E)X((#RM X 21+	Z1+.5)XX(E) -0.5XX(E))	,5XX(E))			0.120
CTB = ((	CTB =((CLRM/E)X((#RM X 2	Z3 + 0.5)XX(E	0.5) XX(E) -0.5XX(E))	1 / 23		0.120
CIPS=CTB*Z4/Z2	8*24/22					0.120
CRCI	I =CTB X R					000.0
COEM	M = 06M OR CTB*25/22/ENY	/ENYR				0.0
COMMENTS						

## 1.1.7 SYSTEMS TEST

This element includes the hardware, software, and activities required for ground-based systems test including qualification tests and other development tests involving two or more subsystems or assemblies. It includes the production, assembly, integration, and checkout of satellite system hardware into a full or partial system test article. It also includes the design, development, and manufacture of special test equipment, test fixtures, and test facilities that are not included in other elements such as ground support facilities. Also included are the planning, documentation, and actual test operations.

Tables 1.1.7.1 and 1.1.7.2 document DDT&E cost estimates respectively for hardware and operations based on individual calculations equal to 50% of the satellite ICI.

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.7.1 SYSTEM GROUND TEST HARDWARE TABLE

		INPUT PAR	ARAMETERS		: : :	INPUT	INPUT COEFFICIENTS
	H	0.0	TF=	1.000000		CDCER=	0.0
	***************************************	0.0	=W30	0.0		CDEXP=	0.0
	C.F.	0.0	<b>-17</b>	1.000000		CICER=	0.0
	PHI=	1.000000	Z 2=	000000.09		CIEXP=	0.0
	# CX	0.0	=67	60,000000			
	0F=	1.000000		000000009	<b>= 57</b>	0.0	
	CALCULAT	CALCULATED VALUES	SET	SUM TO 1	1.1		\$, MILL IONS
!	CD=CDCER X (T	(T X DF)XX(CDEXP)	) X CF		!	:	2662.711
	.CLRM=CICER X	.CLRM=CICER X (M)XX(CIEXP) X CI	CFXTF				0.0
В-	#RM = T / M						0.0
<b>-112</b>	E = 1.0 + LO	=1.0 + LOG(PHI) / LOG(2.0	.01				0*0
	CTFU=(CLRM / E)X((#RM X	E)X((#RM'X 21+.5	• 5) XX(E) -0.5XX(E)	•5XX(E))			0.0
	CTB = ((CLRM/E)X((#RM	×	23 + 0.51XX(E)	E) -0.5xx(E))		) / 23	0.0
!	CIPS=CTB*Z4/Z2	2			1		0.0
	CRCI = CTB	B X R					0*0
	90 = W3D0	OEM OR CT8*25/22/ENYR	/ENYR				0.0
	COMMENTS DDT&E = 5	50% OF SATELLITE	E ICI		· · · · · · · · · · · · · · · · · · ·		

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.7.2 SYSTEM GROUND TEST OPERATIONS TABLE

		ANATORIAS				ואוסו כמפונונו באוס
<del>!!</del>	0.0	TF=	1.000000	5	CDCER=	0.0
#	0.0	0 £M=	0.0	2	)EXP=	0.0
CF=	0.0	21≒	1.000000	Ü	ICER=	0.0
PH I=	1.000000	22=	00000009	CI	CIEXP=	0.0
<b>%</b>	0.0	<u>7</u> 3=	00000009			
DF=	1.000000	= 4 7	000000.09	= 57	0*0	
CALCULA	CALCULATED VALUES	SET	SUM TO 1.1.7	7.		SWITT IONS
D=CDCER X (1	CO=CDCER X (T X DF)XX(CDEXP)	X CF				2662.711
LRM=CICER X	CLRM=CICER X (M)XX(CIEXP) X	CF X TF				0.0
#RM =T / M						0.0
E = 1.0 + LC	=1.0 + LOG(PHI) / LOG(2.0	•01		     		0•0
TFU= (CLRM /	CTFU=(CLRM / E)X((#RM X Z1+.	5) XX(E)	-0.5XX(E)}			0.0
CTB = ((CLRM/E)X((#RM	×	Z3 + 0.51XX(	+ 0.5)XX(E) -0.5XX(E))		1 7 23	0.0
CIPS=CTB*Z4/Z2						0.0
CRCI =CTB	78 X R					0.0
30 = W300	06M OR CT B*Z5/Z2/ENYR	/ENYR	•			0 • 0
COMMENTS DDT&E TES	TEST OPS = 50% OF	SATELLITE	101	1		

# 1.1.8 GROUND SUPPORT EQUIPMENT (GSE)

This element includes all ground-based hardware required in support of handling, servicing, test, and checkout of the satellite subsystems. It also includes special hardware required for simulations and training.

Costs for design, development, manufacture, acceptance, qualification, and maintenance of the GSE equipment are included. It is recognized that various equipments can serve multipurposes. For example, a developmental mockup may later serve as a training aid after it has served its original purposes. In these instances, the acquisition cost is charged to the original or first purpose use, and subsequent usage will incur only the recurring operations and maintenance costs.

GSE costs from several launch vehicle, manned spacecraft and unmanned satellites were analyzed to determine their applicability to SPS GSE requirements. From these data, a percentage factor was developed which was used to estimate SPS ground support equipment costs. This factor is expressed by the equation CD = 0.10 (C); where C = DDT&E cost of the satellite system. See Table 1.1.8.

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.8 GROUND SUPPORT EQUIPMENT

TABLE

	INPUT P	INPUT PARAMETERS		<b>1</b>	IPUT COEF	INPUT COEFFICIENTS
<b></b>	0.0	TF≍	1.000000	COCER		0.0
==	0.0	=W30	0.0	COEXP=		0.0
C.F=	0.0	21=	1.000000	CICER=		0.0
PH I=	1.000000	7.5=	00000000	CIEXP=		0.0
R.	0.0	73=	60.00000			
0F=	1.000000	= + 7	000000*09	= 57	0.0	
CALCULAT	CALCULATED VALUES	SET	SUM TO 1.	1		\$ MILLIONS
CD=CDCER X (T	CO=COCER X (T X DF)XX(COEXP)	) X CF			i i	721.234
CLRM=CICER X (M)XX(CIEXP)	(M)XX(CIEXP) X	CF X TF				0.0
#RM =T / M						0.0
E =1.0 + LO	=1.0 + LOG(PHI) / LOG(2.	• 01				0.0
CTFU=(CLRM / E)X((#RM X	E)X((#RM X 21+.	5) XX(E)	-0.5XX(E))			0.0
CTB =((CLRM/E)X((#RM	×	Z3 + 0.51XX(	+ 0.5)XX(E) -0.5XX(E))	1 / 23		0.0
CIPS=CTB*24/22	2					0.0
CRCI =CTB	B X R					0.0
130 = M333	08M OR CT8*25/22/	/ ENYR				0.0
COMMENTS DDT&E G	GSE = 10% OF SATI	TELLITE DOTEE	SE ABOVE		!	

### 1.1.9 PRECURSOR TEST ARTICLE

The 335 MW pilot plant precursor test article and operations is included in this element. It represents the technology verification space system combining the energy conversion, interface, and power transmission segments of the SPS satellite. The configuration will be constructed by the satellite construction base where the sequence is to build the slip ring/rotary joint housing structure followed by the interface hub and yoke base plus the 1st bay of the solar array. Slip rings are installed and the solar concerter portion is completed as the yoke (interface) arms are fabricated. The antenna construction and maintenance platform is attached to provide facilities for the antenna fabrication and installation of required power modules. The completed EOTV/Demo unit is illustrated in Figure 1.1.9.

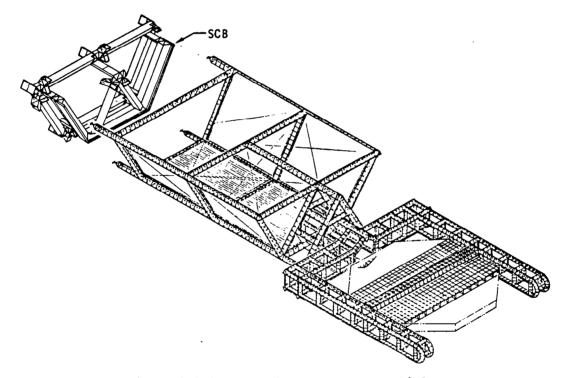


Figure 1.1.9 EOTV Precursor Test Article

#### 1.1.9.1 EOTV PRECURSOR VEHICLE

This element covers the vehicle procurement required to support the integrated test and demonstration program.

The energy conversion segment of the vehicle consists of primary and secondary structure, concentrators, solar blankets, switchgear and converters, conductors/insulation, attitude control and information management subsystems. The interface segment includes the primary and secondary structure, mechanisms, conductors/insulation and slip ring brushes.

The precursor power transmission segment will be representative of the full-up satellite antenna to the extent of using identically available components for the required power levels of the test article. It will include structures, transmitter subarrays, power distribution and conditioning, batteries, insulation, and phase control elements.

· CER's used in this section are the same as those used in the particular elements of earlier satellite sections. DDT&E is, however, a main cost item in these categories as the systems/subsystems will require substantial development activities, whereas the other satellite systems/subsystems will capitalize from this development work.

Cost estimates for the precursor test article are presented in the following tables:

<u>Tables</u>	Segment
1.1.9.1.1 thru 1.1.9.1.8	Energy Conversion
1.1.9.1.9 thru 1.1.9.1.13	Interface
1.1.9.1.14 thru 1.1.9.1.24	Power Transmission

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.9.1.1 PRIMARY STRUCTURE - E.C. TABLE

INPUT PARA T= 30890.0000	RAMETERS TF=	1.000000		INPUT COCER=	INPUT COEFFICIENTS = 0.023000	
2059.00000	=W30	0.0		CDEXP=	000008 * 0	
1.000000	<b>51</b> =	1.000000		CICER=	0.000050	
1.000000	7.5=	000000.09		CI EXP=	1.00000	:
0.0	23=	0.0				
1.000000	= + 7	00000000	= 57	0.0	0	
CALCUL ATED VALUES	KG	SUM TO 1.	1.9.1		•	S, MILL IONS
CD=CDCER X (T X DF)XX(CDEXP)	X CF				8	89.863
CLRM=CICER X (M)XX(CIEXP) X CF	CF X TF					0.103
					15.002	
=1.0 + LOG(PHI) / LOG(2.0)	0)			:	1.000	1
CTFU=(CLRM / E)X((#RM X Z1+.5)	XX(E)	-0.5XX(E))				1.544
CTB = ((CLRM/E)X((#RM X Z3	+	0.5)XX(E) -0.5XX(E))		1 / 23		0.0
CIPS=CTB*Z4/Z2						0.0
=CTB X R						0.0
O&M OR CT8*25/22/ENYR	ENYR					0.0
			:			:

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.9.1.2 SECONDARY STRUCTURE - E.C. TABLE

Ī

1		INPUT PAR	ARAMETERS		!	UNPU	INPUT COEFFICIENTS	
	  -	14918.0000	<b>-</b> F=	1.000000		CDCER=	0.156000	
	# <b>E</b>	5.000000	= W3 O	0.0		COEXP=	0.511000	
	CF.	1.000000	7 1=	1.000000		CI CER=	0.101000	
	=I Hd	1.000000	22=	000000.09		CI EXP=	0.355000	
ĺ	<b>8</b>	0.0	73=	0.0				
	DF=	1.000000	= + 7	000000*09	= 57	0	0.0	
	CALCUL	CALCULATED VALUES	KG	SUM TO 1	1.6.1.1		2.48	S, MILL IONS
	CD=CDCER X	CD=CDCER X (T X DF)XX(CDEXP)	X CF		î.		21.	21 - 178
	CLRM=CICER	CLRM=CICER X (M)XX(CIEXP) X	CF X TF				0	0.179
В-	#RM =T / M						2983.600	
119	E =1.0 +	=1.0 + LOG(PHI) / LOG(2.	• 00				1.000	
	CTFU= (CLRM	CTFU=(CLRM / E)X((#RM X Z1+.	.5)XX(E) -0.5XX(E)	).5XX(E))			533,	533.576
	CTB = ((CLRM/E)X((#RM	×	23 + 0.5) XX(E)	E) -0.5XX(E))		1 / 23	0	0.0
•	CIPS=CTB*Z4/Z2	7.7.5			; ; ;		0	0.0
	CRCI =	=CTB X R					0.0	0
	= M3DC	08M OR CT8*25/22/	/ENYR				0	0.0
i	COMMENTS				•			

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.9.1.3 CONCENTRATOR - E.C. TABL E

	1			
1800000.00	_	1-000000	COCER=	0.027000
420000.000	O E.M ≡	0.0	CDEXP=	0.394000
1.000000	21=	1.000000	CICER=	0.00003
1.000000	75=	00000000	CIEXP=	0 0 0 0 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
0.0	73=	0.0		
1.000000	= + 7	00000000	0 = 57	0.0
CALCULATED VALUES	SQ M	SUM TO 1.1.	.1.9.1	\$ MILL IONS
CO=COCER X (T X OF)XX(CDEXP)	X CF			7.869
CLRM=CICER X (M)XX(CIEXP) X	X CF X TF			, 0 • 704
Σ				4.000
=1.0 + LOG(PHI) / LOG(2.0)	(0)			1.000
CTFU=(CLRM / E)X((#RM X 21+.5)	XX(E)	-0.5xx(E))		2.817
CTB = ((CLRM/E)X((#RM X Z3	+	0.5) XX(E) -0.5X X(E)	) / 23	0.0
CIPS=CTB*24/22				0.0
=CTB X R				0.0
COEM = 0EM OR CTB*25/22/ENYR	/ENYR			0.0

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.9.1.4 SOLAR BLANKET -E.C. TABLE

		INPUT PAR	ARAMETER S		1	IN	OUT COE	INPUT COEFFICIENTS
	=	00000006	TF=	1.000000		CDC ER=		0.161400
	# SE	18750.0000	=W30	0.0		CDEXP=	-	0.394000
	CF=	1.000000	2.1=	1.000000		CICER=		0.000067
	=JHd	1.000000	22=	000000.09		CIEXP=		1.000000
!	R=	0.0		0.0				
	DF=	2.000000	= 7 7	000000*09	= 57		0.0	
	CALCU	CALCULATED VALUES	KG	SUM TO 1.	1.6.1.1			S, MILL IONS
	CD=CDCER X	CD=CDCER X (T X DF)XX(CDEXP)	) X CF		:	:	1	47.041
	CLRM=CICER	CLRM=CICER X (M)XX(CIEXP) X C	CF X TF					1.256
B-	#RM =T / M							48.000
121	E =1.0 +	=1.0 + LOG(PHI) / LOG(2.0	• 0)		;    -  -			1.000
	CT FU= ( CLRM	CTFU=(CLRM / E)X((#RM X Z1+.5	5)XX(E) -0.5XX(E)	5XX(E))				006.09
	CTB = [[CLR	CTB = ((CLRM/E)X((#RM X Z	Z3 + 0.5)XX(E	+ 0.5)XX(E) -0.5XX(E))		1 / 23		0*0
i i	CIPS=CTB*24/Z2	4/12	:	 	;	:		0.0
	CRCI	=CTB X R						0.0
	C 06M =	: OEM OR CT8*25/22/ENYR	/ENYR					0.0
į	COMMENTS					: : : : : : : : : : : : : : : : : : : :		

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.9.1.5 SWITCHGEAR & CONVERTERS -E.C. TABLE

	INPUT	PARAMETERS			INPUT CO	INPUT COEFFICIENTS
ļi L	2875.00000	TF=	1.000000	CDCER=	"	0.158000
I	719.000000	=W30	. 0.0	CDEXP	<b>‡1</b>	0.297000
CF=	1.500000	<b>512</b>	1.000000	CICER	II	0.000400
=I Hd	1.000000	22=	000000.09	CI EXP=	13	1.000000
<b>8</b>	0.0	23=	0.0			
DF=	3.000000	= + 7	000000.09	= 57	0.0	
CALCUL	CALCULATED VALUES	KG	SUM TO 1.	1.1.9.1		S.MILLIONS
CD=CDCER X	(T X DF)XX(CDEXP)	X CF			1	3.497
CLRM=CICER	CLRM=CICER X (M)XX(CIEXP) X CF	CFXTF				0.431
** ** ** ** **						3.999
+ 0•1 "	=1.0 + LOG(PHI) / LOG(2.0)	.0)				1.000
CTFU= (CLRM	CTFU=(CLRM / E)X((#RM X Z1+.5)	5) XX(E) -0.5XX(E))	,5XX(E))			1.725
CTB = ((CLRM/E)X((#RM	×	Z3 + 0.51XX(E	0.51XX(E) -0.5XX(E))	1 / 23	23	0.0
CIPS=CTB*24/22	.722				;	0.0
CRCI =	=CTB X R					0.0
= W3DD	OEM OR CT8*25/22/ENYR	/ ENYR				0.0
COMMENTS				:		

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.9.1.6 CONDUCTORS & INSULATION - E.C. TABLE

		INPUT	PARAMETERS			INPUT CO	COEFFICIENTS
	<u>"</u>	357675.000	<b>T</b> F=	1.000000		COC ER =	0.158000
	<u>"</u>	7452.00000	=W3 O	0.0		CDEXP=	0.297000
	CF=	1.000000	21=	1.000000		CI CER=	0.00000
	=IHd	1.000000	2.2=	60.00000		CI EXP=	1.000000
!	# #	0.0	23=	0.0			
	0 F=	1.000000	<b>24=</b>	00000000	= 57	0.0	
	CALCU	CALCULATED VALUES	KG	SUN TO 1.	1.9.1		S. MILL IONS
:	CD=CDCER X	(T X DF)XX(CDEXP)	) X CF				7.048
	CLRM=CICER	CLRM=CICER X (M)XX(CIEXP) X	CF X TF				0.030
B-	#RM =T / M						47.997
123	E =1.0 +	=1.0 + LOG(PHI) / LOG(2.	.0)	,	1		1.000
	CTFU=(CLRM	CTFU=(CLRM / E)X((#RM X_Z1+.	5) XX(E)	-0.5XX(E))			1.431
İ	CTB = ((CLR	CTB = ((CLRM/E)X((#RM X 2	Z3 + 0.51XX(E	+ 0.51XX(E) -0.5XX(E)		1 / 23	0.0
:	CIPS=CTB*Z4/Z2	4/12	:				0.0
	CRCI	=CTB X R		•			0.0
	= WYOO	GEM OR CT8*25/22/	/ENYR				0.0
•	COMMENTS		:		i    -  -  -		

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.9.1.7 ACS HAROWARE - E.C. TABLE

	INPUT	INPUT PARAMETERS	1		INPUT CO	INPUT COEFFICIENTS
. "	283557.000	<b>TF</b> =	0.300000		COCER=	1.122000
11 <b>2</b>	1970.00000	=W30	0.0		CDEXP=	0.190000
C F≡	1.000000	21=	1.000000		CI CER=	0.057000
=1Hd	1.000000	<b>75=</b>	000000.09		CI EXP≖	0.729000
R =	0.0	23=	0.0			
DF=	1.000000	= + 2	000000009	= 57	0.0	
CALCUL	CALCULATED VALUES	KG	SUM TO 1.	1.6.1.1		S. MILL IONS
CD=CDCER X	CD=CDCER X (T X DF)XX(CDEXP)	) X CF		:		12.190
CLRM=CICER	CLRM=CICER X (M)XX(CIEXP)	X CF X TF				4.312
B #RM = 1 / M						143,938
+ 0• 1	E =1.0 + LOG(PHI) / LOG(2.0)	.0)				1.000
CT FU= (CL RM	CTFU=(CLRM / E)X((#RM X 21+.5)	XX(E)	-0.5XX(E))			620.634
CTB = ((CLRM/E)X((#RM	×	Z3 + 0.51XX	0.51XX(E) -0.5XX(E))		1 / 23	0.0
CIPS=CTB*24/22	172					0.0
CRCI =	=CTB X R					0.0
= W300	CO&M = O&M OR CT8*25/22/EN	2/ENYR				0.0
COMMENTS						

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.9.1.8 SLIPRINGS - PRECURSOR TABLE

INPUT COEFFICIENTS	0.156000	0.511000	0.000764			S.MILL IONS	54.565	7.745	4*000	1.000	30.980	0.0	0.0	0.0	0.0	
INPUT CO	CDC ER=	CDEXP=	CICER= CIFXP=		0.0		. :					1 / 23				
	1.000000	0.0	1.000000	0.0	= 97 0000000 79=	SUM TO 1.1.9.1					-0.5XX(E))	+ 0.5)XX(E) -0.5XX(E))				
ARAMETERS	TF=	= W3 O	21= 72=	73=	= 4 7	KG	X CF	X CF X TF		.0)	5) XX(E)	Z3 + 0.5) XX(			/ ENYR	
INPUT PA	43000.0000	10750.0000	1.500000	0.0	1.000000	CALCULATED VALUES	CD=CDCER X (T X DF)XX(CDEXP)	CLRM=CICER X (M)XX(CIEXP) >		=1.0 + LOG(PHI) / LOG(2.	CTFU=(CLRM / E)X((#RM X Z1+.	×	./22	=CTB X R	0£M OR CT8*25/22/	:
	=	1i <b>X</b>	PH T	<b>8</b>	0F=	CALCUL	CD=CDCER X	CLRM=CICER	HRM =T / M	+ 0 1 1 1 125	CTFU= (CLRM	CTB = ((CLRM/E)X((#RM	CIPS=CTB*24/22	= ICRCI	= W3DD	COMMENTS

ROCKWFLL SPS CR-2 REFERENCE CONFIGURATION 1.1.9.1.9 PRIMARY STRUCTURE - INTERFACE TABLE

	INPUT PARAM	ARAMETERS			INPUT	INPUT COEFFICIENTS
<u> </u>	120000.000	<b>1</b> F=	1.000000		CDCER=	0.023000
3	200.000000	=W30	0.0		COEXP=	0.800000
C F±	1.000000	21=	1.000000		CICER=	0.000050
=1 Hd	1.000000	=27	000000*09		CI EXP=	1.000000
<b>*</b>	0.0	23=	0.0			
DF=	0.50000	= + 7	000000.09	= 57	0.0	
CALCU	CALCULATED VALUES	KG	SUM TO 1.	1.6.1.1		S, MILL IONS
CD=CDCER X	CD=CDCER X (T X DF)XX(CDEXP) X	X CF				152.844
CLRM=CICER	CLRM=CICER X (M)XX(CIEXP) X CF	CF X TF				0.010
M # # # # # # # # # # # # # # # # # # #						000.009
126	=1.0 + LOG(PHI) / LOG(2.0)	.03	-			1.000
CTFU=(CLRN	CTFU=(CLRM / E)X((#RM X Z1+.5)X	X(E)	-0.5XX(E))			000*9
CTB = ((CLF	CTB = ((CLRM/E)X((#RM X Z	13 + 0.51XX(	0.51XX(E) -0.5XX(E))		1 / 23	0.0
CIPS=CTB*24/22	14/12					0.0
CRCI	=CTB X R					0.0
= W3D0	: O&M OR CTB*25/22/ENY	/ENYR				0.0
COMMENTS				:		

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.9.1.10 SECONDARY STRUCTURE - INTERFACE TABLE

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.9.1.11 MECHANISMS - INTERFACE TABLE

	INPUI	PARAMETERS		Z	INPUT COE	COEFFICIENTS
H	391000.000	TF=	1.000000	COCER		0.156000
= 2	391.000000	=W30	0.0	CDEXP=		0.511000
CF=	1.000000	<b>-17</b>	1.000000	CICER=		0.000764
=I Hd	1,000000	=27	000000000	CI EXP=		0.950000
<b>.</b>	0.0	<u>7</u> 3=	0.0			
0F=	0.50000	= + 2	00000009	= 57	0.0	
CALCU	CALCULATED VALUES	KG	SUM TO 1.	.1.9.1		S, MILL IONS
CD=CDCER X	(T X DF)XX(CDEXP) X	X CF				78.868
CLRM=CICER	CLRM=CICER X (M)XX(CIEXP) X CF	CF X TF				0.222
M / 1= MR# B						1 000.000
+ 0• II II II	=1.0 + LOG(PHI) / LOG(2.0)	.00				1.000
CTFU= (CLRM	CTFU=(CLRM / E)X((#RM X 21+.5)	XX(E)	-0.5XX(E))			221.647
CTB = ((CLR	CTB = ((CLRM/E)X((#RM X Z	Z3 + 0.51XX(	0.5)XX(E) -0.5XX(E))	1 / 13		0.0
CIPS=CTB*24/22	14/12	:			: :	0.0
CRCI	=CTB X R					0.0
= W3DD	= 06M OR CT8*25/22/EN	Z ENYR				0.0
COMMENTS				:	į	

RDCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.9.1.12 CONDUCTORS & INSULATION TABLE

INPUT PAR	PARAMETERS			INPUT CO	INPUT COEFFICIENTS
T= 52790,0000	TF=	1.000000	<u> </u>	CDC ER =	0.158000
M= 1650.0000	=W30	0.0		COEXP=	0.297000
CF= 1.000000	21=	1.000000		CI CER=	0.00004
PHI= 1.000000	2.2=	60.00000		CIEXP=	1.000000
	23=	0.0			
DF= 1.000000	= + 7	00000000	= <b>57</b>	0.0	
CALCULATED VALUES	KG	SUM TO 1.1	1.6.1.1		S, MILL IONS
CD=CDCER X (T X DF)XX(CDEXP)	P) X CF		; ;		3,993
CLRM=CICER X (M)XX(CIEXP) X	X CF X TF				0.007
					31.994
129 = 1.0 + LOG(PHI) / LOG(2.0	2.01		; ;		1.000
FU=(CLRM / E)X((#RM X	21+.5)XX(E) -0.	-0.5XX(E))			0.211
CTB = ((CLRM/E)X((#RM X Z	Z3 + 0.5) XX(E	0.5)XX(E) -0.5XX(E))		1 / 23	0.0
CIPS=CTB*Z4/Z2			!		0.0
CRCI = CTB X R					0*0
CCEM = 06M OR CTB*25/22/E	2/ENYR				0.0
COMMENTS	1				

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.9.1.13 SLIPRING BRUSHES - PRECURSOR TABLE

	NPUT P	PARAMETERS		dN 1	INPUT COEFFICIENTS	I C I ENTS
=_	11341.0000	TF=	1.000000	COCER=		0.158000
II E	531.000000	=W30	0.0	COEXP=		0.297000
C F	1.000000	21=	1.000000	CICER=		0.000200
=I Hd	1.000000	22=	60.00000	CIEXP=		1.000000
<b>"</b>	0.0	73=	0.0			
0F=	1.000000	= + 7	000000009	= 57	0.0	
CALCUL	CALCUL ATED VALUES	KG	SUM TO 1.	1.1.9.1		S.MILL IONS
CD=CDCER X	(T X DF)XX(CDEXP)	) X CF				2.529
CLRM=CICER	X (M)XX(CIEXP) X	X CF X TF				0.106
M / 1= MR# B-						21,358
+ 0 1 1 1 1 30	=1.0 + LOG(PHI) / LOG(2.0)	(0.				1.000
CTFU= (CLRM	/ E)X((#RM X Z1+.5)	XX(E)	-0.5XX(E))			2.268
CTB = ((CLRM/E)X((#RM	×	Z3 + 0.5) XX(	0.5) XX(E) -0.5XX(E))	1 / 23		0.0
CIPS=CT8*24/22	./12					0.0
CRCI =	=CTB X R					0.0
≡ ₩3DO	06M OR CT8*25/22/EN	/ENYR				0.0
COMMENTS	:					

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION I.1.9.1.14 PRIMARY STRUCTURE - POWER TRANS TABLE

INPUT COEFFICIENTS	0.023000	0.800000	0.000050	1.000000			S'HILLIONS	20.936	0.063	4.000	1.000	0.250	0.0	0.0	0.0	0.0	
INPUT CO	CDC ER=	COEXP=	CI CER=	CI EXP=		0.0							1 / 23				
	1.000000	0.0	1.000000	00000009	0.0	<b>= 57</b> 000000 <b>* 59 =</b>	SUM TO 1.1.9.1					-0.5XX(E))	+ 0.5)xx(E) -0.5xx(E))				;
ARAMETERS	<b>∓</b> 41	= W3 O	71=	2 2=	73=	= 4 7	KG	X CF	CF X TF		•0)	5) XX(E)	Z3 + 0.51X	:		/ENYR	:
INPUT PA	5000.00000	1250.00000	1.000000	1.000000	0.0	1.000000	CALCULATED VALUES	CD=CDCER X (T X DF)XX(CDEXP)	CLRM=CICER X (M)XX(CIEXP) X		=1.0 + LOG(PHI) / LOG(2.	CTFU=(CLRM / E)X((#RM X 21+.	CTB = ((CLRM/E)X((#RM X Z		=CTB X R	06M OR CT8*25/22/	
	#	<u>:</u>	CF=	=I Hd	<b>8</b>	0F=	CALCUI	CO=COCER X	CLRM=CICER	HRM = 1 / M	+ 0 · 1 · · · · · · · · · · · · · · · · ·	CTFU=(CLRM	CTB = ((CLR)	CIPS=CTB*Z4/Z2	CRCI	≡ W3Ü ⊃	COMMENTS

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.9.1.15 SECONDARY STRUCTURE - POWER TRANS TABLE

00000	S	CDEXP=	INPUT COEFFICIENTS = 0.156000 = 0.511000
ES KG SUM TO 1.1.9.1  X(CDEXP) X CF  IEXP) X CF X TF  // LOG(2.0)  M X Z1+.51XX(E) -0.5XX(E))  X Z3 + 0.51XX(E) -0.5XX(E))  B*Z5/Z2/ENYR	21= 22= 23= 24=	CICER= CIEXP=	0.101000 0.355000
X(CDEXP) X CF X TF  IEXP) X CF X TF  // LOG(2.0)  M X 21+.5)XX(E) -0.5XX(E))  X Z3 + 0.5)XX(E) -0.5XX(E))  // LOG(2.0)  A X Z3 + 0.5)XX(E) -0.5XX(E)  8*25/Z2/ENYR	SUM TO 1	1.6.	S.MILLIONS
IEXP) X CF X TF  1950.000  1 L06(2.0)  M X Z1+.51XX(E) -0.5XX(E))  X Z3 + 0.51XX(E) -0.5XX(E)  8*Z5/Z2/ENYR			17.041
/ LOG(2.0)  M X 21+.51xX(E) -0.5xX(E))  X 23 + 0.51xX(E) -0.5xX(E))  ) / 23  8*25/22/ENYR	C F X		0.001
/ LOG(2.0)  M X 21+.51XX(E) -0.5XX(E))  X Z3 + 0.51XX(E) -0.5XX(E))  1.000			1950.000
M X 21+.51XX(E) -0.5XX(E))  X Z3 + 0.51XX(E) -0.5XX(E))	=1.0 + LOG(PHI) / LOG(2.0)		1.000
X Z3 + 0.51XX(E) -0.5XX(E))	Z1+.5)XX(E)		2.546
R CT B*25/22/ENYR	+ EZ	1 / 23	0.0
R CT B*25/22/ENYR			0.0
CT B* 25/22/ ENYR	- 1		0.0
	O&M OR CTB*25/22/ENYR		0.0

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.9.1.16 TRANSMITTER SUBARRAYS - KLYSTRONS ICI TABLE

		INPUT PAR	ARAMETERS			INPUT	INPUT COEFFICIENTS
	=	34617.0000	<b>1</b> F=	1.000000		CDC ER =	0.0
	¥.	118.800003	=W30	0.0		CDEXP=	0.0
	CF₌	1.250000	=17	1.000000		CICER=	0.003270
	=I Hd	1.000000	12=	000000.09		CI EXP=	1.000000
	æ	0.0	7.3=	0.0			
	DF=	1.000000	= 7 7	60.000000	= 57	0.0	
İ	CALCUL	CALCULATED VALUES	SQ M	SUM TO	1.6.1.1		\$, MILL IONS
1	CD=CDCER X	CD=CDCER X (T X DF)XX(CDEXP)	) X CF				0.0
	CLRM=CICER	CLRM=CICER X (M)XX(CIEXP) X C	CF X TF				0.486
В-	#RM =T / M						291,389
133	E = 1.0 +	=1.0 + LOG(PHI) / LOG(2.0)	.01				1,000
	CTFU=(CLRM	CTFU=(CLRM / E)X((#RM X 21+.5)	XX(E)	-0.5XX(E))			141.497
	CTB = ((CLRM/E)X((#RM	×	Z3 + 0.51XX(E	0.51XX(E) -0.5XX(E))		1 / 23	0*0
·	CIPS=CTB*Z4/Z2	17.2	1 : : : : : : : : : : : : : : : : : : :		***		0.0
	CRCI =	=CTB X R					0.0
	= W3D0	06M OR CT8*25/22/ENYR	/ENYR				0.0
	COMMENTS	:					

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.9.1.17 SWITCHGEAR & CONVERTERS - P.T. PRECURSOR TABLE

	INPUT PARAMETERS	ARAMETERS			NPUT CO	INPUT COEFFICIENTS
# <b>.</b>	79200.0000	_ ₹F	1.000000	CDCER=		0.158000
II E	2447.00000	=W30	0.0	COEXP=		0.297000
CF≡	1.500000	21=	1.000000	CICER=		0.000400
PH I=	1.000000	<b>22=</b>	000000.09	CI EXP=		1.000000
R=	0.0	23=	0.0			
DF=	1.000000	= 47	00000000	= 57	0.0	
CALCULATED	ATED VALUES	KG	SUM TO 1.	1.1.9.1		S, MILL IONS
CD=CDCER X	CD=CDCER X (T X DF)XX(CDEXP) X	) X CF			and the second s	6.756
CLRM=CICER	CLRM=CICER X (M)XX(CIEXP) X CF	CF X TF				1.468
M / L WW# B						32,366
+ 0 1 1 134	=1.0 + LOG(PHI) / LOG(2.0)	.0)				1,000
CTFU=(CLRM	CTFU=(CLRM / E)X((#RM X Z1+.5)	.5) XX(E) -0.5XX(E)	5xx(E))			47.520
CTB = ((CLRM/E)X((#RM X		Z3 + 0.5) XX(E	0.5)XX(E) -0.5XX(E))	1 / 23	3	0.0
CIPS=CTB*24/Z2	/12					0.0
CRCI =(	=CTB X R					0.0
= W300	06M OR CT8*Z5/Z2/ENYR	/ENYR				0.0
COMMENTS					:	

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.9.1.18 CONDUCTORS & INSULATION - P.T. PRECURSOR TABLE

1	1	:	INPUT	INPUT PARAMETERS		!	Z	UT COE	INPUT COEFFICIENTS
		= 1	0000*00009	TF=	1,000000	:	CDC FR =		0.158000
1		<b>*</b>	1720.00000	=W30	0.0		CDEXP=		0.297000
		CF=	1.000000	<b>51</b> =	1.000000		CICER=		0.000004
		PH [=	1.000000	22=	000000-09	į	CI EXP=		1.000000
•		, A	0.0	3	0.0				
		0F=	1.000000	= + 7	000000009	= 57		0.0	
•		· CAL CUL	CALCULATED VALUES	KG	SUM TO 1.	1.6.1.1			\$ • MILL IONS
		CD=CDCER X	CD=CDCER X (T X DF)XX(CDEXP)	X CF				:	4.147
		CLRM=CICFR	CLRM=CICFR X (M)XX(CIEXP) X	CF X TF					0.007
	B-	#RM =T / M							34.884
	135	E =1.0 +	=1.0 + LOG(PHI) / LOG(2.0	.0)		i 1 1		ļ	1.000
		CTFU=(CLRM	CTFU=(CLRM / E)X((#RM X 21+.5)XX(E)		-0.5XX(E))				0.240
		CTB = ((CLRM/E)X((#RM	×	Z3 + 0.5) XX(	0.5) XX(E) -0.5XX(E))		1 / 23		0.0
		CIPS=CTB*Z4/Z2	./122			!		} :	0.0
	1	CRCI =	=CTB X R						0.0
		= M300	O&M OR CT8*25/22/ENYR	/ENYR					0•0
		COMMENTS		:		:			

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.9.1.19 BATTERIES - P.T. PRECURSOR TABL E

	INPUT PARAM	ARAMETERS			NPUT CO	INPUT COEFFICIENTS
<b>⊢</b>	8000.00000	TF=	1.000000	CDCER=		0.037000
	50.00000	=W30	0.0	CDEXP	44	0.734000
C F=	1.000000	<b>~17</b>	1.000000	CICER=		0.028000
=I Hd	1.000000	12=	0000000	CI EXP=		0.241000
	0.0	23=	0.0			
0F=	1.000000	= + 7	000000.09	= 57	0.0	
CALCUL	CALCULATED VALUES	KG	SUM TO 1.1.9.1	9.1		S*MILL IONS
CD=CDCFR X	CD=CDCER X (T X DF)XX(CDEXP) X	XCF			!	27.106
CLRM=CICER	CLRM=CICER X (M)XX(CIEXP) X CF	CF X TF				0.072
B #RM = T / M						160.000
+ 0+ 1 136	=1,0 + LOG(PHI) / LOG(2,0)	[0.			*	1.000
CTFU= (CLRM	CTFU=(CLRM / E)X((#RM X Z1+	Z1+.5)XX(E) -0.	-0.5XX(E))			11.501
CTB = ((CLRM/E)X((#RM	×	Z3 + 0.51XX(E	0.5)XX(E) -0.5XX(E))	1 / 23	£2	0.0
CIPS=CTB*24/Z2	722	•		:		0.0
CRCI =	=CTB X R					0.0
= W3DO	COEM = OEM OR CTB*25/22/ENYR	/ENYR				0.0
COMMENTS		ŧ		:		

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.9.1.20 THERMAL CONTROL - INSULATION - PRECURSOR TABLE

	INPUT PAR	RAMETERS			INPUT	INPUT COEFFICIENTS
T= 23200	23200.0000	. TF=	0.048000	,	CDCER=	0.156000
<b>→</b>	4.000000	=W30	0.0		CDEXP=	0.511000
CF=	1.000000	=17	1.000000		CI CER=	0.101000
	1.000000	<b>22=</b>	000000.09		CI EXP=	0.355000
) = <b>A</b>	0.0	23=	0.0			
	00000001	= + 7	000000.09	= 57	0.0	0
CALCULATED VALUES	ALUES	KG	SUN TO 1.	1.6.1.1		S.MILL IONS
CD=CDCER X (T X DF)XX(CDEXP)	F)XX(CDEXP)	X CF		:		58.539
CLRM=CICER X (M)XX	X (M)XX(CIEXP) X	CF X TF				0.008
B #RM =T / M						5800.000
137 = 1.0 + LOG(PHI) / LOG(2.0	I) / LOG(2.	0)				1.000
CTFU=(CLRM / E)X((#RM X		)XX(E)	-0.5XX(E))			45.996
CTB = ((CLRM/E)X((#RM	#RM X 23	1	+ 0.51XX(E) -0.5XX(E))		1 / 23	0.0
CIPS=CT8*Z4/Z2	:	:				0.0
CRCI = CTB X	~					0.0
CCEM = OCM OR	CT 8*25/22/	ENYR				0.0
COMMENTS						

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION
1.1.9.1.21 REFERENCE FREQUENCY GENERATOR - PRECURSOR TABLE

INPUT PARAMETERS  00000	INPUT COEFFICIENTS	CDC ER=	CDEXP= 1.000000	CICER=	CIEXP=		0.0 = 22 0	1.1.9.1 \$, MILL TONS	009.0	0.100	1.000	1.000	001.0	0.0	} 1		
T= 1.000000 CF= 1.000000 CF= 1.000000 DF= 1.000000  CALCULATED VALUES  CALCULATED VALUES  CALCULATED VALUES  CALCULATED VALUES  TRM=T / M  = 1.0 + LOG(PHI) / LOG(2.0000)  TFU=(CLRM / E)X((#RM X Z1+.0000))								SUM TO		×				0.51XX(E) -0.5XX(E))			
	INPUT PARA	1.000000	1.00000	1.000000	1.000000	0.0	1.000000	CALCULATED VALUES		RM=CICER X (M)XX(CIEXP) X CF		÷		1		CIPS=CTB*24/Z2	IPS=CTB*24/Z2 CRCI =CTB X R

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.9.1.22 DIST. SYSTEM, COAXIAL CABLE TABLE

	INPUT PAR	ARAMETERS		1	VPUT CO	INPUT COEFFICIENTS
• # #	8613.00000	<b>∓</b> F=	1.000000	CDC ER=		0.000030
*	261.000000	=W30	0.0	COEXP=		1.000000
C F=	1.000000	21=	1.000000	CI CER=		0.000000
=I Hd	1.000000	22=	000000.09	CI EXP=		1.000000
# <b>&amp;</b>	0.0	23=	0.0			
0 F=	1.000000	= + 7	000000009	= 57	0.0	
CALCUL	CALCULATED VALUES	Σ	SUM TO 1.	1.1.9.1		\$, MILLIONS
CD=CDCER X	CD=CDCER X (T X DF)XX(CDEXP)	XCF				0.258
CLRM=CICER }	CLRM=CICER X (M)XX(CIEXP) X CF	CF X TF				0.016
M / L= W8# B-						33,000
+ 0 1 1 1 139	=1.0 + LOG(PHI) / LOG(2.0	•0)				1.000
CTFU=(CLRM ,	CTFU=(CLRM / E)X((#RM X 21+.5	.5)XX(E) -0.5XX(E))	.5XX(E))			0.517
CTB = ((CLRM/E)X((#RM	×	Z3 + 0.51XX(	0.5)XX(E) -0.5XX(E))	1 / 23	3	0.0
CIPS=CTB*Z4/Z2	/12					0.0
CRCI =(	=CTB X R					0.0
CCEM =	06M OR CTB*25/22/ENYR	/ENYR				0.0
COMMENTS	1					

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.9.1.23 DIST. SYSTEM DEVICES TABLE

		INPUT PARA	ARAMETERS		;	INP	JT COE	INPUT COEFFICIENTS
	<u>-</u>	100.00000	TF≈	1.000000		CDCER=		0.000225
	# <b>X</b>	2.000000	=W30	0.0		COEXP=		1.000000
	CF.	1.000000	7.1=	1.000000		CICER=		0.005000
	= [ Hd	1.000000	12=	000000.09		CI EXP≖	7	1.000000
	<b>4</b> =	0.0	<u>7</u> 3=	0.0				
	DF=	1.000000	= + 7	00000009	= 57		0.0	
	CALCULA	CALCULATED VALUES	KG	SUM TO 1.	1.6.1.1			S.MILL IONS
	CD=CDCER X (	CD=CDCER X (T X DF1XX(CDEXP) X	X CF		:	* i		0.022
	CLRM=CICER X	X (M)XX(CIEXP) X	CF X TF					0.010
В-	#RM = 1 / M							50.000
-140	E = 1.0 + L(	=1.0 + LOG(PHI) / LOG(2.0)	• 0 •					1.000
	CTFU=(CLRM / E)X((#RM	E)X((#RM X Z1+.5)	XX(E)	-0.5XX(E))				005*0
	CTB = ((CLRM/E)X((#RM	×	Z3 + 0.51 XX(	0.5)XX(E) -0.5XX(E)		1 / 23		0*0
i !	CIPS=CTB*Z4/Z2							0.0
	CRCI =CTB	TB X R						0.0
	C 08M = 0	08M OR CT8*25/22/ENYR	/ENYR					0.0
!	COMMENTS	)				:		

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.9.1.24 TRANSMITTER SUBARRAYS - KLYSTRONS DDTEE TABLE

	INPUT PARA	APAMETERS	i		INPUT COF	INPUT COEFFICIENTS
<u>"</u>	282500.000	TF=	1.000000		CDC ER =	0.205000
<u></u>	282 500.000	= W3 O	0.0		CDEXP=	0.507000
CF₌	1.250000	=17	1.000000		CICER=	0.0
_ =IHq	1.000000	<b>22=</b>	60.00000		CIEXP=	0.0
<b>4</b>	0.0	_ <u>7</u> 3=	0.0			
0F=	1.000000	= 7 7	000000009	= 57	0.0	
CALCU	CALCULATED VALUES	X	SUM TO 1.1.9.1	9.1		\$, MILL IONS
CD=CDCER X	CO=CDCER X (T X DF)XX(CDEXP)	X CF		:		148,707
CLRM=CICER	CLRM=CICER X (M)XX(CIEXP) X CF	CF X TF				0.0
B- #RM =1 / M						1.000
-141	=1.0 + LOG(PHI) / LOG(2.0)	.01				1.000
F	CTFU=(CLRM / E)X((#RM X Z1+.5)	XX(E)	-0.5XX(E))			0.0
CTB = ((CLR	CTB = ((CLRM/E)X((#RM X Z	Z3 + 0.51XX(E	0.5) XX(E) -0.5X X(E))		1 / 23	0.0
CIPS=CTB*Z4/Z2	.4/12	i				0.0
CRCI	=CTB X R					0.0
= W300	: DEM OR CTB*Z5/Z2/ENYR	/ ENYR				0.0
COMMENTS	• • • • • • • • • • • • • • • • • • •	;		!		

## 1.1.9.2 EOTV PRECURSOR OPERATIONS

This element includes the necessary vehicle operations (user charge per flight including payload integration) required to support the precursor test activity.

Cost estimates are presented in Table 1.1.9.2.

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.1.9.2 COTV PRECURSOR OPERATIONS TABLE

NI	PARA	ERS		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	INPU	T COE	INPUT COEFFICIENTS
1.00000			1.000000		CDCER=		0.0
1.00000	ធ ()		0.0		CDEXP=		0.0
1.000	000 Z1=		1.000000		CICER=		0.630000
1.000000			50.00000		CI EXP=		1.000000
0.0	<b>-62</b>		0.0				
1.00000	900 Z4=		000000-09	= 57	0	0.0	
CALCULATED VALUES	FLIGHT	11	SUM TO 1.	6-1-9			S+MILLIONS
CD=CDCER X (T X DF)XX(CDEXP)	CDEXP) X CF	:			:	:	0.0
CLRM=CICER X (M)XX(CIEXP)	XP) X CF X TF	TF.					0.630
/ W							1.000
E =1.0 + LOG(PHI) / LOG(2.	L06(2.0)	!				***************************************	1.000
CTFU=(CLRM / E)X((#RM X 21+.	X 21+.5) XX(E)	E) -0.5XX(E))	(6))				0.630
CTB = ((CLRM/E)X((#RM X	23	+ 0.5) XX(E) -0.5XX(E))	0.5XX(E))		) / 23		0.0
CIPS=CT8*24/22			!	!			0.0
CRCI =CTB X R							0.0
CO&M = O&M OR CT8*25/22/	25/22/ENYR						0.0

## 1.2 SPACE CONSTRUCTION AND SUPPORT

This element includes all hardware and activities required to assemble, checkout, operate, and maintain the satellite system. Included are space stations, construction facilities, support facilities and equipment, and manpower operations.

The Rockwell reference configuration is used as a baseline for the development of a satellite construction scenario and construction systems/equipment. Precursor operations incident to the establishment of orbital support facilities were identified and the satellite construction sequences and procedures were developed.

The overall scenario leading to establishment of satellite construction support facilities and to satellite construction is shown in Figure 1.2-1. Initial operations entail use of the growth shuttle and the shuttle derived HLLV for transporting men and material to LEO for the precursor phase of the program. Subsequently, during the 30 year satellite construction phase, the sps HLLV will become the primary transportation element for delivering construction mass to LEO and the shuttle HLLV will be used for personnel transfer to LEO.

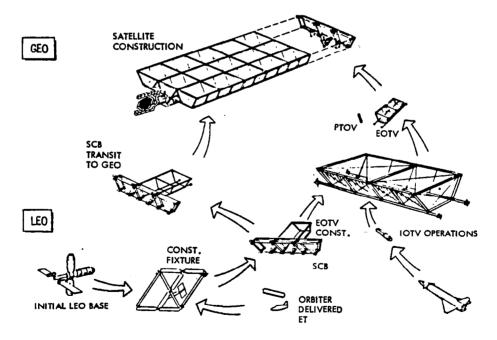


Figure 1.2-1. Overall Satellite Construction Scenario

The initial step in satellite precursor operations is establishment of a LEO base as shown in the lower left of the figure. Crew and power modules are transported to LEO by shuttle derivatives and assembled. When the base is fully operational, shuttle external tanks are delivered and mated to form

construction fixtures for the Satellite Construction Base (SCB) construction. The figure shows a completed SCB. Since the more economical SPS HLLV will not be available during this phase of the program, and since overall plans specify an EOTV test article, it is possible that only the center section of the SCB would be constructed initially. This trough would be used to fabricate the pilot plant EOTV test article with an end-mounted antenna. After proof of concept, the remainder of the SCB would be completed along with sufficient EOTVs to support initial satellite construction operations. The SCB will then be transferred to GEO, using one or more EOTVs for propulsion and attitude control. Upon reaching GEO, satellite construction would commence, with the logistics support as shown at the right of the figure.

The energy conversion segment of the satellite structure is constructed by the integrated SCB in a single pass. Satellite longerons of a length sufficient to connect the triangular frames of the slip ring support structure are fabricated, followed by construction of the slip ring interface structure, and the first satellite structure frame. The SCB then proceeds to fabricate/install the remainder of the satellite structure and solar converter. Construction of the slip rings, and yoke (interface) takes place concurrently using free flying fabrication facilities to support this building process (Figure 1.2-2).

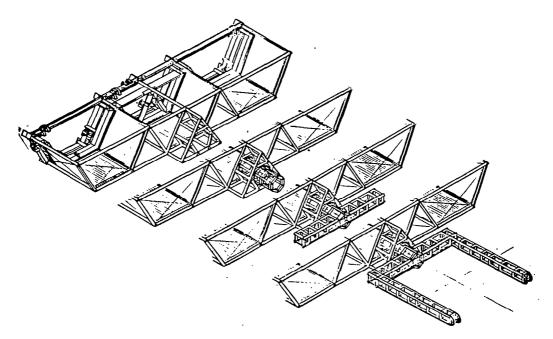


Figure 1.2-2. Antenna Supporting Structure Assembly Sequence

This section addresses the facilities/equipment, and operations required to support SPS work, crew, and operational requirements during the SPS program. Section 1.2.1 deals with the construction facilities; and Section 1.2.2 deals with the work and crew requirements at LEO. Section 1.2.3 covers the requirements in GEO to support operations and maintenance of the satellite.

#### 1.2.1 CONSTRUCTION FACILITIES

This element includes the facilities, equipment, and operations required to assemble and checkout the satellite system. Included are crew life support facilities, the central control facility, fabrication and assembly facilities, cargo depots, and operations.

The satellites are constructed in GEO, each satellite being constructed at its designated longitudinal location. The SCB supports construction of two satellites per year during the program and serves as headquarters for operations and activities necessary to construct such items as the satellite, antenna interface, antenna, and EOTV. The SCB is constructed of composites and consists of the fabrication fixture, construction equipment, and base support facilities.

The construction fixture is in the form of three troughs, corresponding to the satellite configuration, which permits simultaneous construction of all troughs. Additional structural members are located in the middle trough and are used as support for the rotary joint/antenna structure. Figure 1.2-3 illustrates the construction base and shows the location of work and crew facilities.

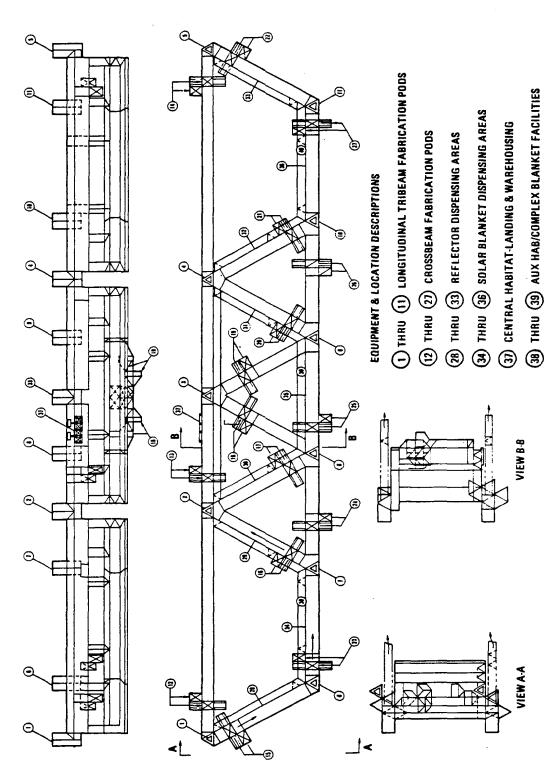
The SCB fabrication fixture assembly and support equipment, and the crew/work modules on the base are itemized in Table 1.2.1. SCB modules used to support the crew/work activities are of various internal configurations to accommodate specific functional requirements. All modules are of the same diameter and most are of the same length, their dimensions and mass being in compliance with space transportation system constraints. The modules are located on the fab fixture along with the assembly and support equipment.

The Airlock Docking Module (ADM) is used to join the other base modules to provide docking accommodations for other elements such as crew transport modules, consumables logistics modules (CLM) and intra-base logistics vehicles, and for transfer of personnel and equipment between different pressure environments. The Crew Habitability Module (CHM) provides stateroom and personal hygiene facilities, and support systems for 24 to 30 crew members. The Base Management Module (BMM) houses the operational communications and control systems for the base. Power Modules (PM) are photovoltaic power systems (collectors, converters, conditioners, and storage) which support all base power requirements. Pressurized Storage Modules (PSM) provide an area for storage and workshop accommodations. Shielding (SHD) is provided in selected modules to protect against solar flare radiation. The Crew Support Module (SM) provides the galley, recreational and medical facilities and support subsystems. Work support, crew, and operational requirements are discussed in the following paragraphs.

#### 1.2.1.1 WORK SUPPORT FACILITIES - SCB

This element includes work facilities and equipment required for satellite assembly and checkout. Included are beam fabricators, manipulators, assembly jigs, installation and deployment equipment, and cargo storage depots. Excluded are the facilities related to crew support.

Figure 1.2-3. Satellite Construction Base (SCB)



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Table 1.2.1 Total Space Construction and Support Equipment Requirements

· .			ACE RUCTION SE
SYSTEM Description	ABBREVIATION	WORK SUPPORT FACILITIES	CREW SUPPORT FACILITIES
BASE MODULES:			
AIRLOCK DOCKING MODULE CREW HABITABILITY MODULE CONSUMABLES LOGISTICS MODULE BASE MANAGEMENT MODULE CREW SUPPORT MODULE/EVA POWER MODULE PRESSURIZED STORAGE MODULE SHIELDING CREW SUPPORT MODULE CREW REQUIREMENTS  ASSEMBLY AND SUPPORT EQUIPMENT: BEAM MACHINES BEAM MACHINES CABLE ATTACHMENT MACHINES	ADM CHM CLM BMM CSM/EVA PM PSM SHD CSM	17 4 4 4 8 198 3618 72	5 17 9 8 3 317 AVG. 504 PEAK
REMOTE MANIPULATOR SOLAR BLANKET DISPENSER MACHINE SOLAR BLANKET CASSETTES REFLECTOR DISPENSER MACHINES REFLECTOR CASSETTES CABLE/CATEMARY DISPENSERS ANTENNA PANEL INSTALL. EQUIP. GANTRY/CRANES CARGO STORAGE DEPOT SCB FAB FIXTURE		110 72 5760 6 360 84 1 12	

SCB modules used mainly in the support of construction operations include a total of 17 ADMs, 4 BMMs, 4 PMs, and 4 PSMs. The CERs used for these modules were based on Rockwell Space Station studies.

All SPS unique fabrication/orbital construction assembly and support equipment is included in this section (reference Table 1.2.1). Included are the tribeam fabricators, cable attachment machines, solar blanket/concentrator dispensing machines, and antenna panel installation equipment. Each of these requirements were analyzed for equipment usage, replacement factors, O&M, and projected costs based on engineering estimates of design characteristics. The items of assembly and support equipment and base modules remain on the SCB as it transfers from one construction site to another. Cost estimates for these items are presented in Tables 1.2.1.1.1 through 1.2.1.1.17.

# 1.2.1.2 CREW SUPPORT FACILITIES - SCB

This element includes the facilities and equipment required for the life support and well-being of the crew members. Included are living quarters, central control facilities, recreation facilities, and health facilities of the satellite construction base.

Crew support facilities include 5 ADMs, 17 CHMs, 9 CLMs, 8 SLDs, and 3 CSMs. Detail cost sheets on these components are identified in Tables 1.2.1.2.1 through 1.2.1.2.5.

### 1.2.1.3 OPERATIONS

This element includes the planning, development, and conduct of operations at the construction facility. It includes both the direct and support personnel and the expendable maintenance supplies for satellite assembly and checkout.

This element has been divided into the subelements of operations (Table 1.2.1.3.1) and consumables (Table 1.2.1.3.2) where an average crew of 317 persons is required to man the SCB over the normal six month fabrication period. A crew rotation is scheduled for every three months. Consumables for the SCB are calculated at 3.6 kg/person/day.

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.2.1.1.1 BEAM MACHINE TABL E

	INPUT PARAM	PARAMETERS		JUNI	INPUT COEFFICIENTS
<u> </u>	1.000000	TF=	1.000000	CDCER=	2.000000
11 2	1.000000	= M3 O	. 0005650	CDEXP=	1.000000
C F≅	1.000000	21=	198.000000	CICER=	0.70000
≈1 Hd	0.920000	<b>-27</b>	000000.09	CI EXP=	1.000000
~	0.0	<u>73=</u>	198.000000		A CANADA A CANADA A CANADA CAN
0F=	1.000000	= 4 2	198.000000	) = 57	0.0
CALCULAT	CALCULATED VALUES		SUM TD 1.	1.2.1.1	\$, MILL IONS
CD=CDCER X (1	(T X DF)XX(CDEXP) X	P) X CF	:	:	2.000
CLRM=CICER X	CLRM=CICER X (M)XX(CIEXP)	X CF X TF			0.700
HRM = 1 / M					1.000
+ 0•I = 150	=1.0 + LOG(PHI) / LOG(2.0)	2.01			0.880
CTFU=(CLRM / E)X((#RM X		Z1+.5)XX(E) -(	-0.5xx(E))		83.150
CTB = ((CLRM/E)X((#RM	)X((#RM X	Z3 + 0.5) XX(	0.5) XX(E) -0.5XX(E)	1 / 23	0.420
CIPS=CTB*Z4/Z2		:			1.386
CRCI = CTB	rb x R				0.0
0 = W300 ·	06M OR CT B*25/22/ENY	2/ENYR			0.594
COMMENTS	!				

ROCKWELL 'SPS CR-2 REFERENCE CONFIGURATION I.2.1.1.2 BEAM MACHINE CASSETTES TABLE

•						
' <u>  </u>	1.000000	<b>TF</b> =	1.000000		CDCER=	0.800000
===	1.000000	0£M=	0.090450		COEXP=	1.000000
C.F.	1.000000	=17	1206.00000		CI CER=	0.008200
=1 Hd	0.0006.0	22=	60.00000		CIEXP=	1.000000
**	0.066667		3618.00000			
DF=	1.000000	= 7 7	1206.00000	= 57	0.0	
CALCULAT	CALCULATED VALUES		SUM TO 1.	1.2.1.1		S.MILL IONS
CO=COCER X (T	(T X DF)XX(CDEXP)	XCF				008.0
CLRM=CICER X (M)XX(CIEXP)		X CF X TF				0.008
#RM =T / M						1.000
E =1.0 + LO	=1.0 + LOG(PHI) / LOG(2.0	0.		)     		976*0
CTFU=(CLRM / E)X((#RM X		Z1+.5)XX(E) -	-0.5XX(E))			6.315
CTB = ((CLRM/E)X((#RM	)X((#RM X Z3	+	0.5) XX(E) -0.5XX(E))		1 / 23	0.005
CIPS=CTB*Z4/Z2				1		160.0
CRCI =CTB	8 × ×					00000
CC6M = 06	O&M OR CT8*25/22/E	JENYR				060.0
COMMENTS		:		1		

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.2.1.1.3 CABLE ATTACHMENT MACHINE TABLE

	INPUT PARAM	ARAMETERS			INPUT CO	INPUT COEFFICIENTS
<b>=</b>	1.000000	TF=	1.000000	CDC	CDCER=	4.30000
Ψ	1.000000	=W30	0.144000	300	XP=	1.000000
C.F.=	1.000000	21=	72.000000	010	ER=	0.500000
=1 Hd	0.0006.0	22=	000000.09	213	CI EXP=	1.000000
<b>8</b>	0.0	23=	72.000000			
0 F=	1.000000	= + 7	72.000000	= 57	0.0	
CALCULATED	ED VALUES		SUM TO 1.	1.2.1.1		\$, MILL IONS
CD=CDCER X (T	CD=CDCER X (T X DF)XX(CDEXP)	X CF				4.300
CLRM=CICER X	CLRM=CICER X (M)XX(CIEXP) X	CF X TF				00 - 200
#RM = T / M						1.000
)07 + 0•1 = H	=1.0 + LOG(PHI) / LOG(2.0)	(0.				0.926
CTFU=(CLRM / E)X((#RM X		Z1+.5)XX(E) -(	-0.5XX(E))			28.228
CTB = ((CLRM/E)X((#RM	)X((#RM X Z3	+	0.5)XX(E) -0.5XX(E))		62 /	0.392
CIPS=CTB*24/22						0.470
CRCI =CTB	8 X R					0.0
CO6M = 08	0£4 OR CT8*25/22/ENY	/ENYR				0.144
COMMENTS	T.			:	; ; ;	

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.2.1.1.4 REMOTE MANIPULATOR TABLE

,		INPUT PAR	ARAMETERS			INPUT	INPUT COEFFICIENTS
	<u>"</u>	1.000000	TF=	1.000000		CDC ER=	, 880000,
	E	1.000000	=W30	1.925000		COEXP=	1.000000
	<u>"</u>	1.000000	<u>71=</u>	55.000000		CI CER=	1.200000
	bH I=	0.00086.0	22=	60.00000		CI EXP=	1.000000
Ì	R=	0.033333	73=	110.000000	!		The state of the s
	0 F=	1.000000	= + 7	25.000000	= 57	0.0	
	CALCULATED	ED VALUES .		SUM TO 1.	1.2.1.1		\$, MILL IONS
	CD=CDCER X (T	CD=CDCER X (T X DF)XX(CDEXP)	X CF	:	, k		088°9
	CLRM=CICER X (M)XX(CIEXP)		X CF X TF	·			1.200
В-	#RM = 1 / M						1.000
153	E =1.0 + LOG(PHI)	S(PHI) / LOG(2.0	.0)			-	0.971
	CTFU=(CLRM / E	E)X((#RM X Z1+	Z1+.5)XX(E) -(	-0.5XX(E))			066.09
	CTB = ((CLRM/E)X((#RM	)X((#RM X Z3	+	0.5)XX(E) -0.5XX(E))		1 / 23	1.077
1	CIPS=CTB*24/22						186.0
	CRCI = CTB	B X R					0.036
	N30 = M300	06M OR CT8*25/22/ENYR	/ENYR				1.925
!	COMMENTS				:		

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.2.1.1.5 BLANKET DISPENSER MACHINE TABLE

	INPUT PARAM	ARAMETERS			INPUT CO	INPUT COEFFICIENTS
H	1.000000	TF≈	1.000000		CDCER=	4.000000
12	1.000000	±W30	0.180000		CDEXP=	1.000000
C.F.	1.000000		72.000000		CI CER=	0.40000
=IHd	0.980000	22=	000000*09		CI EXP=	1.000000
ď	0.0	73=	72.000000			
DF=	1.000000	= + 7	72.000000	= <b>57</b>	0.0	
CALCULAT	CALCULATED VALUES		SUM TO 1.	1.2.1.1		S, MILL IONS
CD=CDCER X (T	(T X DF)XX(COEXP) X	X CF		:	:	4.000
CLRM=CICER X	CLRM=CICER X (M)XX(CIEXP) X CF	CF X TF				00**0
#RZ = 1 / Z						1,000
E =1.0 + LO	=1.0 + LOG(PHI) / LOG(2.0)	.01				0.971
CTFU=(CLRM / E)X((#RM X		Z1+.5)XX(E) -0.	-0.5xx(E))			26.154
CTB = ((CLRM/E)X((#RM	×	Z3 + 0.51 XX (E	0.5) XX(E) -0.5XX(E))		1 / 23	0.363
CIPS=CTB*24/22	2			:		0.436
CRCI = CTB	вхк					0.0
30 = W300	06M OR CT8*25/22/ENY	/ ENYR				0.180
COMMENTS				:		

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.2.1.1.6 SOLAR BLANKET CASSETTES TABL E

	INPUT PAR	ARAMETERS		dNI	INPUT COEFFICIENTS
<u>u</u>	1.000000	<b>TF</b> =	1.000000	CDCER=	0.800000
1	1.000000	= M3 O	0.115200	COEXP=	1.000000
CF≡	1.000000	21=	1440.00000	CICER=	0.01000
=IHd	0.950000	7.5=	000000.09	CIEXP=	1.000000
<b>a</b> x	0.066667	23=	5760.00000		
0F=	1.000000	= + 7	2880.00000	= 57	0.0
CALCULAT	CALCULATED VALUES		SUM TO 1.	1.2.1.1	\$, MILLIONS
CD=CDCFR X (T	CD=CDCER X (T X DF)XX(CDEXP)	XCF			008.0
CLRM=CICER X	CLRM=CICER X (M)XX(CIEXP) X	( CF X TF			0.010
N /  = NX# B-					1.000
+ 0.1 = m	=1.0 + LOG(PHI) / LOG(2.0	.0)			0.926
CTFU=(CLRM / E)X((#RM X	E)X((#RM X 21+.	5) XX(E)	-0.5xx(E))		9.076
CTB = ((CLRM/E)X((#RM	×	Z3 + 0.5) XX	+ 0.5)XX(E) -0.5XX(E)	1 / 23	900*0
CIPS=CTB*Z4/Z2	2	•			0.273
CRCI = CTB	вхк				00000
30 = W300	CO&M = O&M OR CT8*25/22/ENYR	ZENYR .			0.115
COMMENTS			i		

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.2.1.1.7 REFLECTOR DISPENSER MACHINE TABLE

		INPUT PARA	ARAMETERS			INPUT	INPUT COEFFICIENTS
	#	1.000000	17 =	1.000000		CDCER=	00000009
	¥.	1.000000	-M30	0.048000		CDEXP=	1.000000
	CF=	1.000000	=17	6.000000		CICER=	0.800000
	=1 Hd	000086.0	22=	000000.09		CI EXP=	1.000000
ļ	8	0.0	73=	000000.9			
	0F=	1.000000	= + 7	000000.9	= 57	0.0	
	CALCULATED VALUES	D VALUES		SUM TO 1.	1.2.1.1		S, MILL IONS
	CD=CDCER X (T X DF)XX(CDEXP)	X DF)XX(CDEXP	) X CF		:	:	000*9
	CLRM=CICER X (	X (M)XX(CIEXP) X	X CF X TF				0.800
В-	#RM =T / M						1.000
156	w	=1.0 + LOG(PHI) / LOG(2.0)	.0)				0.971
	CTFU=(CLRM / E)X((#RM X Z1+.5)	)X((#RM X ZI+	XX(E)	-0.5XX(E))			4.651
	CTB = ((CLRM/E)X((#RM	×	Z3 + 0.5) XX(E	0.5)XX(E) -0.5XX(E))		1 / 23	0.775
	CIPS=CTB*Z4/Z2				i		0.078
	CRCI =CTB	×				-	0.0
	M30 = M300	OR CT8*25/22/EN	/ENYR				0.048
	COMMENTS				:	; ; ;	A constant constant of the con

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.2.1.1.8 REFLECTOR CASSETTES TABLE

INPUT COEFFICIENTS	1.000000	1.000000	0.030000	1.000000		0.0	\$+ HILL IONS	1.000	0.030	1.000	0.926	2.721	0.021	0.042	0.001	0.054	
dN I	COC ER=	CDEXP=	CI CER=	CIEXP=				:					) / 23				
	1.000000	0.054000	120.000000	00000000	360.00000	120.000000 25=	SUM TO 1.2.1.1					-0.5XX(E))	+ 0.5)XX(E) -0.5XX(E))				
ARAMETERS	<b>1</b> F=	=W30	21=	22=	_£2=	<b>- 4 7</b>		X CF	CF X TF		.00	) XX(E)	Z3 + 0.5) XX			/ENYR	
INPUT PAR	1.000000	1.000000	1.000000	0.0006.0	0.066667	1.000000	CALCULATED VALUES	CD=CDCER X (T X DF)XX(CDEXP)	CLRM=CICER X (M)XX(CIEXP) X		=1.0 + LOG(PHI) / LOG(2.0	E)X((#RM X Z1+.5	×	27	rb x R	06M OR CTB*25/22/E	
	<del>  </del>	# <u>\$</u>	₽ E	PH I=	<b>8</b>	0 F=	CALCULAT	CD=CDCER X (1	CLRM=CICER X	#RM = T / M	+ 0°1 "	CTFU=(CLRM / E)X((#RM	CTB = ((CLRM/E)X((#RM	C1PS=CTB*Z4/Z2	CRCI = CTB	30 = W3JJ	COMMENTS

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.2.1.1.9 CABLE/CATENARY DISPENSER MACHINES TABLE

	INPUT PARAM	ARAMETERS			INPUT CO	INPUT COEFFICIENTS
=_	1.000000	1F=	1.000000		CDCER=	2.200000
<b>=</b>	1.000000	=W30	0.168000		CDEXP=	1.000000
C F=	1.000000	=17	84.000000		CICER=	0.300000
=I Hd	0.086.0	22=	000000.09		CI EXP=	1.000000
# <del>**</del>	0.0	23=	84.000000			
0F=	1.000000	= + 2	84.000000	= 57	0.0	
CALCULATED	ED VALUES		NOT MUS	1.2.1.1		S, MILLIONS
CD=CDCER X (T	CD=CDCER X (T X OF)XX(CDEXP)	X CF		!		2.200
CLRM=CICER X	X (M)XX(CIEXP) X	CF X TF				00.300
M / HRM =T / M						1.000
158	=1.0 + LOG(PHI) / LOG(2.0)	•0)				0.971
CTFU=(CLRM / E)X((#RM X		Z1+.5)XX(E) -0	-0.5XX(E))			22.786
CTB = ((CLRM/E)X((#RM	×	Z3 + 0.51XX(	0.5) XX(E) -0.5XX(E))		1 / 23	0.271
CIPS=CT8*24/22	2					0.380
CRCI =CTB	ВХК					0.0
30 = W3D3	O&M OR CTB*25/22/ENY	/ ENYR				0.168
COMMENTS			: :			

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.2.1.1.10 ANTENNA PANEL INS. EQPT. TABLE

	INPUT PAR	ARAMETERS		:	INPUT	INPUT COEFFICIENTS
=	1.000000	TF=	1.000000	U	CDC ER =	0000000000
12	1.000000	=M30	6.755000	S	CDEXP=	1.000000
CF=	1.000000	71=	1.000000	O	:I CER=	200.00000
PH I=	0.00086.0	<b>22=</b>	60.00000	O	CI EXP=	1.000000
# <b>&amp;</b>	0.0	23=	1.000000			
0F=	0.133333	= + 7	1.000000	= 57	0.0	
CALCULA	CALCULATED VALUES	SET	SUM TO 1.2	1.2.1.1		S.MILLIONS
CD=CDCER X (	CD=COCER X (T X DF)XX(CDEXP)	X CF				80.000
CLRM=CICER X	CLRM=CICER X (M)XX(CIEXP) X C	CF X TF				200.000
# # # # # # # # # # # # # # # # # # #						1.000
+ 0.1 " u	=1.0 + LOG(PHI) / LOG(2.0	.00				0.971
CTFU=(CLPM /	CTFU=(CLPM / E)X((#RM X 21+.5	) XX(E)	-0.5XX(E))			200.272
CTB = ((CLRM/E)X((#RM	×	Z3 + 0.5) XX(E	0.5) XX(E) -0.5XX(E))		1 / 23	200.272
CIPS=CTB*Z4/Z2	7.7			!		3.338
CRCI = CTB	TB X R					0•0
0 = W300	06M OR CT8*25/22/E	/ENYR				6.755
COMMENTS	!					

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.2.1.1.11 GANTRY/CRANES TABLE

INPUT 1.000000	PARAMETERS TF=	1.000000	NPUT	COEFFICIENTS 17.000000
1.000000	=W30	000009.0	CDEXP=	1.000000
1.000000	2.1=	12.000000	CI CER =	8.000000
0.950000	22=	00000000	CI EXP=	1.000000
	23=	12.000000		
0.800000	= +7		0.0 = 52	·
CALCULATED VALUES		SUM TO 1.2.1.1		\$, MILL IONS
DF)XX(CDEXP)	P) X CF			13.600
CLRM=CICER X (M) XX(CIEXP)	X CF X TF			8.000
				1.000
=1.0 + LOG(PHI) / LOG(2.0)	2.0)			0.926
CTFU=(CLRM / E)X((#RM X Z1	Z1+.5)XX(E) -0.	-0.5XX(E))		85.034
CTB = ((CLRM/E)X((#RM X	Z3 + 0.5) XX(E	0.5) XX(E) -0.5XX(E))	) / 23	7.086
				1.417
				0*0
OR CTB*25/22/ENYR	2/ENYR			009*0
	:			

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.2.1.1.12 CARGO STORAGE DEPOTS TABLE

INPUT COEFFICIENTS	CDC ER= 15.000000			CIEXP= 1.000000		0.0 = 52	1.1 S, MILLIONS	12.000	2.000	1.000	976-0	7.559	1 / 23	0.126	0.0	009*0
reas	1.000000		4.000000	0000000	4.000000	4.000000	SUN TO 1.2.1.1		TF.			(E) -0.5xx(E))	0.5) XX(E) -0.5XX(E))			
INPUT PARAMETERS	1.000000 TF=	1.000000 0£M=	1.000000 21=	0000	E Z 0°0	- <b>7</b> 000008*0	CALCULATED VALUES	CD=CDCER X (T X DF)XX(CDEXP) X CF	CLRM=CICER X (M)XX(CIEXP) X CF X		=1.0 + LOG(PHI) / LOG(2.0)	CTFU=(CLRM / E)X((#RM X Z1+.5)XX(E)	X 23 +	27	TB X R	06M 08 CT 8*25/22/ENYR
	#	X.	C.F.=	≃IHd	102	DF=	CALCULAI	CD=CDCER X (1	CLRM=CICER X	- #RM = T / M	+ 0•I= H	CTFU=(CLRM /	CTB = ((CLRM/E)X((#RM	CIPS=CTB*24/22	CRCI = CTB	C E M = 08

COMMENTS

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.2.1.1.13 FAB FIXTURE TABL E

INPUT PARA	ARAMETERS TE			INPUT CO	INPUT COEFFICIENTS
5000.0000	= H = 0	0.00000		CDEXP=	0.800000
1.00000	71=	1.000000		CICER=	0.000050
1.000000	12=	000000.09	U	:IEXP=	1.000000
0.0	23=	1.000000			
1.000000	= 7 7	1.000000	= 57	0.0	
CALCUL ATED VALUES	KG	SUM TO 1.2	1.2.1.1		\$, MILL IONS
CD=CDCER X (T X DF)XX(CDEXP) X	) X CF		:		2165-128
CLRM=CICER X (M)XX(CIEXP)	X CF X TF				0.250
Σ					329.780
=1.0 + LOG(PHI) / LOG(2.0)	(0.3				1.000
CTFU=(CLRM / E)X((#RM X Z1+.5)	XX(E)	-0.5XX(E))			82.445
CTB = ((CLRM/E)X((#RM X )	Z3 + 0.5) XX(E	0.5)XX(E) -0.5XX(E))		1 / 23	82.445
CIPS=CTB*24/22					1.374
=CTB X R					0.0
COEM = OEM OR CTB*25/22/ENYR	2/ENYR				0.0
			:		

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.2.1.1.14 AIRLOCK DOCKING MODULE (ADM) TABLE

	INPUT PAR	ARAMETERS		du I	UT COEF	INPUT COEFFICIENTS
<u>!</u>	2500.00000	¶F=	1.000000	CDCER=		0.0
=	2500.00000	=W30	0.0	CDEXP=		0.0
C F≡	1.000000	21=	17.000000	CICER=		0.006036
PH I=	0.086.0	=27	0000009	CIEXP=		1.000000
= &	0.02000	23=	17.000000			
DF=	1.000000	= + 7		= 57	0.0	
CAL CUL	CAL CUL ATED VALUES	KG	SUM TO 1.2.1.1	.1		S.MILLIONS
CD=CDCER X	(T X DF)XX(CDEXP)	) X CF		:		0.0
CLRM=CICER	CLRM=CICER X (M)XX(CIEXP) X C	( CF X TF				15.090
B #RM = T / M						1.000
+ 0 1 1 1 163	1.0 + LOG(PHI) / LOG(2.0)	.0)				0.971
CTFU=(CLRM	CTFU=(CLRM / E)X((#RM X Z1+.5)	5)XX(E) -0.5XX(E))	•5XX(E))			242.302
CTB = ((CLRM	=((CLRM/E)X((#RM X Z	Z3 + 0.5) XX(E)	E) -0.5XX(E))	1 / 23		14.253
CIPS=CTB*24/22	/22					4.038
CRCI =	=CTB x R					0.285
= W3DD	08M OR CT8*25/22/E	Z/ENYR				0.0
COMMENTS SEE 1.2.1.2.1	.1.2.1 FOR DDTEE					

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.2.1.1.15 BASE MGMT. MODULE (BMM) TABLE

	INPUT PARA	ARAMETERS			IND	UT COE	INPUT COEFFICIENTS
<u>"</u>	27000.0000	TF=	1,000000		CDCER=		0.0
¥	27000.0000	-W30	0*0		CDEXP=		0.0
C.F.	1.000000	2.1=	4.000000		CICER=		0.011496
=I Hd	0.980000	22=	000000.09		CI EXP=		1.000000
<b>8</b>	0.02000	23=	4.000000				
DF=	. 1.000000	<b>2</b> 4=	4.000000	= 57		0.0	
CALCULATED	LATED VALUES	KG	SUM TO 1.	.2.1.1			S, MILLIONS
CD=CDCER X	(T X DFIXX(CDEXP) X	X CF					0.0
CLRM=CICER	X (M)XX(CIEXP) X CF	CF X TF					310,392
M / L= MH# B							1.000
+ 0.1 = u	=1.0 + LOG(PHI) / LOG(2.0)	,00			; ;	!	0.971
CT FU= (CLRM	CTFU=(CLRM / E)X((#RM X Z1+.5)	XX(E)	-0.5XX(E))				1213.870
CTB = ((CLRM/E)X((#RM	×	Z3 + 0.51XX(E	0.5)XX(E) -0.5XX(E))		1 / 23		303.467
CIPS=CTB*24/22	4/12			!			20.231
CRCI	=CTB X R	e desidence e quadro à cumptoria de 19 millo 1884 e interes malarité e qu					690°9
= W300	0£M OR CTB*25/22/EN	/ENYR		•			0.0
COMMENTS SEE 1.	ENTS SEE 1.2.2.1.1 FOR DDTEE		:	;		:	

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.2.1.1.16 POWER MODULE (PM) TABLE

	PUPUT	INPUT PARAMETERS		: 1	INPUT CO	INPUT COEFFICIENTS
н Н	250.000000	= <del>L</del>	1.000000	U	CDC ER =	0.0
# <b>E</b>	250.00000	=W30	0.0		CDEXP=	0.0
C Fi≘	1.000000	<b>21=</b>	4.000000	U	:ICER=	1.100000
=IHd	0.00086.0	22=	0000000	U	CIEXP=	1.000000
8	0.02000	73=	4.000000	! !		
0F=	1.000000	= + 7	4.000000	= 57	0.0	
CALCUL ATED	TED VALUES	X	SUM TO 1.2.	1.1		S, MILL IONS
CD=CDCER X (	X (T X DF)XX(CDEXP)	) X CF		;		0.0
CLRM=CICER X	CLRM=CICER X (M)XX(CIEXP) X	X CF X TF				275.000
# #RM = T / M						1.000
+ 0•1 " u	=1.0 + LOG(PHI) / LOG(2.0	.00				0.971
CTFU=(CLRM /	CTFU=(CLRM / E)X((#RM X 21+.5	.5) XX(E) -0.5XX(E))	).5xx(E))			. 1075.459
CTB = ((CLRM/	=((CLRM/E)X((#RM X Z	Z3 + 0.5) XX(	0.5)XX(E) -0.5XX(E))		) / 23	268.865
CIPS=CT8*24/22	.72	:			personal designation of the contract of the co	17.924
CRCI = C	=CTB X R					5.377
) = W3D3	06M OR CTB*Z5/Z2/ENYR	/ENYR			,	0.0
COMMENTS SEE 1.2.	ENTS SEE 1.2.2.1.2 FOR DDTGE					

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.2.1.1.17 PRESSURIZED STORAGE MODULE (PSM) TABLE

!	INPUT PARA	ARAMETERS			NANI	INPUT COEFFICIENTS	ICI ENTS
#	15000.0000	TF≒	1.000000		CDC ER=	0	0.052914
<u>"</u>	15000.0000	=W30	0.0		CDEXP=	~	000000
C.F.	1.000000	<b>71</b> =	4.000000		CICER=	0	0.013734
=I Hd	000086.0	22=	60,000000		CI EXP=	7	1.000000
<b>a</b>	0.010000	73=	4.000000				
0 F=	1.000000	<b>2</b> 4=	4.000000	= 57	0	0.0	
CALCULATED	ATED VALUES	KG	SUM TO 1.	1.2.1.1			S.MILLIONS
CD=CDCER X	(T X DF)XX(CDEXP)	) X CF		:		:	793.710
CLRM=CICER	X (M)XX(CIEXP) X	CF X TF				•	206.010
M / L= MH# B-							1.000
+ - - - - - - - - - - - - - - - - - - -	=1.0 + LOG(PHI) / LOG(2.0)	• 0)		.			0.971
CT FU= ( CLRM	CTFU=(CLRM / E)X((#RM X 21+.5)	XX(E)	-0.5XX(E))				805.657
CTB = ((CLRM/E)X((#RM	×	Z3 + 0.5)XX(E	0.5)XX(E) -0.5XX(E)		1 / 23		201.414
CIPS=CT8*Z4/Z2	./72	:		!	· · · · · · · · · · · · · · · · · · ·		13.428
= IORO	=CTB X R						2.014
= W300	06M OR CT8*25/22/ENYR	/ENYR					0.0
COMMENTS		:					

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.2.1.2.1 AIRLOCK DOCKING MODULE-ADM TABL E

INPUT PARAMETERS INPUT COEFFICIENTS	500.00000 TF= 1.000000 COCER= 0.012461	0.0 COEXP=	0 Z1= 5.000000 CICER=	0.980000 Z2= 60.000000 CIEXP= 1.000000	23= 5.000000	= + 7	VALUES KG SUM TO 1.2.1.2 S.MILLIONS	DF)XX(CDEXP) X CF	)XX(CIEXP) X CF X TF 15.090	1.000	PHI) / LOG(2.0)	X((#RM X 21+.5)XX(E) -0.5XX(E)) 73.413	((#RM X Z3 + 0.5)XX(E) -0.5XX(E)) ) / Z3 14.683	1.224	X R 0.294	
INPUT PAR	2500.00000	2500.00000	1.000000	0.086.0	0.02000	1.000000	1	CD=CDCER X (T X DF)XX(CDEXP)			=1.0 + LOG(PHI) / LOG(2.0	×	×		1	GANS/CZ/SZ#BIJ GO M30
	H	<u> </u>	C.F.	=IHd	# <b>*</b>	DF=	CALCULATED	CD=CDCER X	CLRM=CICER )	₩ / L= ₩8#	+ 0•1 "	CTFU=(CLRM / E)X((#RM	CTB = ((CLRM/E)X((#RM	CIPS=CTB*Z4/Z2	CRCI =(	T M SU J

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.2.1.2.2 CREW HABITABILITY MODULE-CHM TABLE

<u>  </u>	27000.0000	TF=	1.000000	S	.DCER=	0.0
¥	27000.0000	=W30	0.0	3	CDEXP=	0.0
C F=	1.000000	<b>71</b> '=	17.000000	S	ICER=	0.003770
=I H d	0.00086.0	22=	000000.09	S	CIEXP=	1.000000
۳ ۳	0.02000	73=	17.000000			
0F=	1.000000	= + 7	17.000000	= 57	0.0	
CALCUI	CALCULATED VALUES	KG	SUM TO 1.	1.2.1.2		\$+MILLIONS
CD=COCER X	(T X DF)XX(CDEXP)	X CF		:		0.0
CLRM=CICER	X (M)XX(CIEXP) X	CF X TF				101.790
#RM =T / M						1.000
+ 0 · 1 = 3	=1.0 + LOG(PHI) / LOG(2.0)	(0.			!	0.971
CT FU= ( CLRM	/ E)X((#RM X 21+	Z1+.5)XX(E) -0	-0.5XX(E))			1634.456
CTB = ((CLRM/E)X((#RM	4/E)X((#RM X Z3	3 + 0.51 XX(E)	E) -0.5XX(E))		1 / 23	96.144
CIPS=CTB*Z4/Z2	4/22			:		27.241
CRCI	=CTB X R					1.923
C 0.6.M =	08M OR CT8*25/22/ENY	/ ENYR				0.0

SEE 1.2.2.1 FOR DDT&E

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.2.1.2.3 CONSUMABLES LOGISTICS MODULE-CLM TABLE

INPUT	INPUT PARAMETERS			INPUT	INPUT COEFFICIENTS
T= 5000,00000	TF=	1.000000		COCER=	0.0
M= 5000,00000	= W30	0.0		CDEXP=	0.0
CF= 1.000000		00000006		CICER=	0.014000
		00000000		CI EXP=	1.000000
R= 0.02000	23=	00000006			
DF= 1.00000		000000*6	= 57	0.0	
CALCULATED VALUES	KG	SUM TO 1.2	.1.2		\$, MILL IONS
CD=CDCER X (T X DF)XX(CDEXP) X	(P) X CF		· !		0.0
CLRM=CICER X (M)XX(CIEXP)	X CF X TF				70.000
W #RM = T / M					1.000
6 E = 1.0 + LOG(PHI) / LOG(2.0)	2.0)				179.0
CTFU=(CLRM / E)X((#RM X 21	Z1+.5)XX(E) -(	XX(E) -0.5XX(E))			604.675
CTB = ((CLRM/E)X((#RM X	XX (5.0 + EZ	0.5) XX(E) -0.5XX(E))		1 / 23	67.186
CIPS=CTB*Z4/Z2					10.078
CRCI =CTB X R					1.344
COEM = OEM OR CTB*25/22/EN	22/ENYR				0.0
COMMENTS SEE 1.2.2.2.2 FOR DDTEE	u	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	:		

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.2.1.2.4 SHIELDING TABLE

TF= 1.00000 CDCER= 0.15600  0.00	!			
Z1= 8.000000 Z2= 60.000000 Z3= 8.000000 Z4= 8.000000 Z4= 8.000000 X CF X CF F X TF 1.000 1.		1.000000	COCER=	0.156000
22= 60.000000 CIEXP= 0.35500 23= 8.000000 Z5= 0.0  X CF  X CF  F X TF  F X TF  1.0000  1.0000  1.0000  1.0000  1.0000  1.0000  1.0000  1.0000  1.0000  1.000	7 0(	000000.8	CICER=	0.101000
Z3= 8.000000 Z5= 0.0  KG SUM TO 1.2.1.2  F X TF  F X TF  1) XX(E) -0.5XX(E))  + 0.5) XX(E) -0.5XX(E))  NYR	7	60.00000	=dX3IO	0.355000
X CF  X CF  X CF  F X TF  F X TF  1.000  1)  1.000  1)  1.000  1)  1.000  1.000  1.000  1.000  1.000  1.000  1.000  1.000  1.000  1.000  1.000  1.000  1.000  1.000  1.000  1.000  1.000  1.000	7	8.000000		
KG SUM TO 1.2.1.2  X CF F X TF F X TF  () XX(E) -0.5XX(E) F X TF  () XX(E)	7	000000		
x CF F x TF I) 00-971 I) xx(E) -0.5xx(E))	CALCULATED VALUES KG		1.2	S, MILL IONS
1EXP) X CF X TF  1.000  1.000  1.000  1.000  1.000  1.000  1.000  1.000  2  2  X 23 + 0.5) XX(E) -0.5XX(E))  1.000  8*25/22/ENYR				343,200
/ LOG(2.0) M X Z1+.5)XX(E) -0.5XX(E)) X Z3 + 0.5)XX(E) -0.5XX(E))  8*25/22/ENYR	CF X			2.748
/ LOG(2.0) M X 21+.5) XX(E) -0.5XX(E)) X 23 + 0.5) XX(E) -0.5XX(E)) ) / 23 8*25/22/ENYR				1.000
M X 21+.5)XX(E) -0.5XX(E))  X 23 + 0.5)XX(E) -0.5XX(E))  B*25/22/ENYR	=1.0 + LOG(PHI) / LOG(2.0)			0.971
X 23 + 0.5)XX(E) -0.5XX(E))	21+.5)			21.160
	+ 67	1	1.7.23	2.645
				0.353
	×			0.026
	OR CT8*25/22/ENYR			0.0

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.2.1.2.5 CREW SUPPORT MODULE-CSM TABLE

	INPUT P	PARAMETERS			INPUT CO	COEFFICIENTS
 	15000.0000	TF=	1.000000	J	CDC ER=	0.012432
# *	15000.0000	=W30	0.0	ပ 	DEXP=	1.000000
C.F=	1.000000	-17	3.000000	S	ICER=	. 861500.0
₽HI≃	000086.0	75=	60.00000	ပ	CI EXP=	1.000000
<b>a</b>	0.02000	23=	3.000000			
0 F=	1.000000	= + 7	3.000000	= 57	0.0	
CALCUL	CALCULATED VALUES	KG	SUM TO 1.2	1.2.1.2		S'HILL IONS
CD=CDCER X	CO=COCER X (T X DF)XX(COEXP)	X CF	1		1	186.480
CLRM=CICER	CLRM=CICER X (M)XX(CIEXP) X CF	CF X TF				86.970
#RM =T / M						1.000
E =1.0 +	=1.0 + LOG(PHI) / LOG(2.0	.0)				0.971
CTFU= (CLRM	CTFU=(CLRM / E)X((#RM X 21+.5	XX(E)	-0.5XX(E))			256.587
CTB = ((CLRM/E)X((#RM	×	Z3 + 0.51XX(E)	:) -0.5xx(E))		1 / 23	85.529
CIPS=CTB*24/22	1/12	:				4.276
CRCI =	=CTB X R				e de la companya de la companya de la companya de la companya de la companya de la companya de la companya de	1.711
= W3JJ	06M OR CT8*25/22/ENYR	/ENYR				0.0
COMMENTS						

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ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.2.1.3.1 OPERATIONS, CONSTRUCTION CREW TABLE

	INPUT PAR	ARAMETERS		1	INPUT CO	INPUT COEFFICIENTS
=	317.000000	TF=	1.000000	J	CDCER=	0.0
1	317.000000	=W30	0.0		COEXP=	0.0
CF≒	1.000000	=17	1.000000		CICER=	0.062400
=IHd	1.000000	12=	000000.09		CI EXP=	1.000000
# C	0.0	23=	31.000000			
DF=	1.000000	= + 2	30.00000	= 57	0.0	
CALCULAT	CALCULATED VALUES	MEN	SUM TO 1.	1.2.1.3		S, MILL IONS
CD=CDCER X (T X DF)XX(CDEXP)	X DF)XX(CDEXP	X CF		; ; ;		0.0
CLRM=CICER X	CLRM=CICER X (M)XX(CIEXP) X CF	CF X TF				19,781
- #RM = T / M						1.000
)07 + 0°7 = H	=1.0 + LOG(PHI) / LOG(2.0	.00				1.000
CTFU=(CLRM / E)X((#RM X	E)X((#RM X 21+.5	5)XX(E) -0.5XX(E))	).5XX(E))			19.781
CTB = ((CLRM/E)X((#RM	×	Z3 + 0.51XX(	+ 0.5) XX(E) -0.5XX(E)		1 / 23	19.781
CIPS=CTB*24/22	2			:		068*6
CRCI =CTB	x x					0.0
COEM = OEM	06M OR CT8*25/22/ENYR	Z/ENYR				0.0
COMMENTS						

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION TABLE --1.2.1.3.2 ORBITAL OPERATIONS, CONST. PROV.

<u> 1</u>	410832.000	<b>1</b>	1.000000	CDC ER=	# ~	0.0
11 2	410832.000	=₩30	0.0	CDEX	P=	0.0
C F=	1.000000	21=	1.000000	CICER=	<b>₩</b>	0.000022
PHI=	1.000000	22=	000000.09	CIEX	<b>b</b> =	1.000000
&	0.0	73=	31.000000			
0F≖	1.000000	= 7 7	30.00000	= 57	0.0	
CALCI	CALCULATED VALUES	KG	SUM TO 1.	1.2.1.3		* WILLIONS
CD=CDCER X	X (T X DF)XX(CDEXP)	P) X CF				0.0
CLRM=CICER	X (M)XX(CIEXP)	X CF X TF				9.038
#RM =T /	Σ					1,000
E =1.0	=1.0 + LOG(PHI) / LOG(2.0)	2.01				1.000
CT FU= (CLR)	CTFU=(CLRM / E)X((#RM X 2)	Z1+.5)XX(E) -0.	-0.5XX(E))			9.038
CTB = ((CL)	CTB = ((CLRM/E)X((#RM X	Z3 + 0.5) XX(E	0.5) XX(E) -0.5XX(E))	•	67 /	9.038
CIPS=CTB*Z4/Z2	24/22					4.519
CRCI	=CTB X R					0.0
= M3OO	= 06M OR CT8*25/22/ENY	2/ENYR				0.0
COMMENTS						

### 1.2.2 LOGISTICS SUPPORT FACILITIES - LEO

This element includes the hardware, software and operations required in LEO to support the construction and operations and maintenance of the satellite system. Included are crew life support facilities, cargo and propellant depots, and vehicle servicing facilities necessary for the receiving and transfer of cargo and personnel distined for a construction base or operational satellite located in GEO.

LEO support operations will require a permanent crew of 24 at the LEO facility. These personnel will provide supervisory activities for transfer of up and down payloads between the HLLV and OTVs. They also perform the scheduled maintenance required by the electric propulsion OTV, such as changeout of ion thruster screens. Included are work and crew support facilities (Table 1.2.2) plus required operations.

SYSTEM Description	ABBREVIATION	WORK SUPPORT FACILITIES	CREW SUPPORT FACILITIES
CREW HABITABILITY MODULE	СНМ		1
CONSUMABLES LOGISTICS MODULE	CLM		t
BASE MANAGEMENT MODULE	вим	1	
CREW SUPPORT MODULE/EVA	CSM/EVA		1
POWER MODULE	PM	1	

Table 1.2.2 LEO Base Modules

# 1.2.2.1 WORK SUPPORT FACILITIES

This element includes the facilities and equipment required to provide logistics support in LEO. Included are HLLV and OTV docking stations, payload handling equipment, and cargo and propellant storage depots. Excluded are facilities related to crew support.

A 100 kW solar array power module and the base management module are work support facilities. Cost estimates contained in Tables 1.2.2.1.1 and 1.2.2.1.2 were based on Rockwell Space Station studies.

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.2.2.1.1 BASE MGMT. MODULE-BMM TABLE

	INPUT PARAM	ARAMETERS			INPUT CO	INPUT COEFFICIENTS
<del>"</del>	27000.0000	TF=	1.000000		CDC ER =	0.091296
## H	27000.0000	-W30	0.0		CDEXP=	1.000000
C F=	1.000000	21=	1.000000		CICER≈	0.011496
=l Hd	0.980000	22=	000000.09		CI EXP≈	1.000000
#	0.02000		1.000000			
0F=	1.000000	= 7 7	1.000000	= 57	0.0	
CALCUI	CALCUL ATED VALUES	KG	SUM TO 1.2	1.2.2.1		S.MILLIONS
CD=CDCER X	CD=CDCER X (T X DF)XX(CDEXP) X	X CF				2464.993
CLRM=CICER	X (M)XX(CIEXP) X	CF X TF				310. 392
#RM = T / M						1.000
+ 0• 1 -176	=1.0 + LOG(PHI) / LOG(2.0)	• 0)		!		0.971
CTFU= (CLRM	/ E)X((#RM X Z1+.5)	XX(E)	-0.5XX(E))			310.814
CTB = ((CLRM/E)X((#RM	×	Z3 + 0.51 XX(	0.5)XX(E) -0.5XX(E))		1 / 23	310.814
CIPS=CTB*24/22	4/12				manufacture and the second sec	5.180
CRCI	=CTB X R					6.216
= CCEM =	06M OR CTB*Z5/Z2/EN	/ENYR				0.0
COMMENTS						And the second s

ROCKWELL SPS CR-2 RÉFERENCE CONFIGURATION 1.2.2.1.2 POWER MODULE-PM TABLE

	INPUT P	PARAMETERS		· :	INPUT CO	INPUT COEFFICIENTS
<u>=</u>	250,000000	<b>1</b> F ≈	1.000000		CDCER=	1.400000
#	250,000000	=W30	0.0		CDEXP=	1.000000
C.F.	1.000000	=17	1.000000		CICER=	1.100000
₽HI≃	0.00086.0	7.5=	60,00000		CI EXP=	1.000000
æ.	0.02000	73=	1.000000			
DF=	1.000000	= 4 7	1.000000	= 57	0.0	
CALCUL	CALCULATED VALUES	X	SUM TO 1.	1.2.2.1		S.MILLIONS
CD=CDCER X	CD=COCER X (T X DF)XX(CDEXP)	X CF				350.000
CLRM=CICER )	CLRM=CICER X (M)XX(CIEXP) X C	CFXTF				275.000
#RM =T / M						1.000
+ 0. III	=1.0 + LOG(PHI) / LOG(2.0)	• 01				0.971
CTFU={CLRM ,	CTFU=[CLRM / E)X((#RM X 21+.5)	XX(E)	-0.5XX(E))			275,373
CTB = ((CLRM/E)X((#RM	×	13 + 0.51 XX(	0.5) XX(E) -0.5XX(E))		1 / 23	275,373
CIPS=CTB*24/22		t		!		4.590
CRCI = (	=CTB X R					5.507
CCEM =	06M OR CT8*Z5/Z2/ENYR	/ENYR .				0.0
COMMENTS						

### 1.2.2.2 CREW SUPPORT FACILITIES

This element includes the facilities and equipment required for the life support and well-being of the crew members. Included are living quarters, recreation facilities, and health facilities at LEO.

The crew habitability module and crew support module/EVA are the same basic configuration as for those on the SCB. However, the crew support module has an airlock and EVA preparation area. A consumables logistics module is the third element of crew support facilities.

CERs used for crew support facilities were based upon Rockwell Space Station studies. See Tables 1.2.2.2.1, 1.2.2.2.2, and 1.2.2.2.3.

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.2.2.2.1 CREW HABITABILITY MODULE-CHM TABLE

	INPUT PAR	ARAMETERS			INPUT	INPUT COEFFICIENTS
ř.	27000.0000	TF=	1.000000		CDC ER =	0.009714
1) 2	27000.0000	= W30	0.0		CDEXP=	1.000000
CF.	1.000000	<b>51</b> =	1.000000		CI CER=	0.003770
=1Hd	0.00086.0	<b>2.2=</b>	000000.09		CI EXP=	1.000000
ii œ	0.02000	Z3=	1.000000			
0F=	1.000000	= 4 2	1.000000	= 57	0.0	
CALCUL	CALCULATED VALUES	KG	SUM TO	1.2.2.2		\$, MILL IONS
CD=CDCER X	CD=COCER X (T X DF)XX(CDEXP)	X CF				262.278
CLRM=CICER	X (M)XX(CIEXP) X	CF X TF				101.790
H #RM =T / M						1.000
+ 0.1 "	=1.0 + LOG(PHI) / LOG(2.0	.00				0.971
CTFU=(CLRM	/ E)X((#RM X Z1+	Z1+.5)XX(E) -0.	-0.5XX(E))			101.928
CTB = ((CLRM/E)X((#RM	4/E)X((#RM X Z3	+	0.51XX(E) -0.5XX(E))		) / 23	101.928
CIPS=CTB*Z4/Z2	+122					1.699
CRCI =	=CTB X R					2.039
= W300	06M OR CT8*25/22/E	/ENYR				0.0
COMMENTS	1			:		

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.2.2.2.2 CONSUMABLES LOGISTICS MODULE TABLE

INPUT PARAM	PARAMETERS			INPUT CO	COEFFICIENTS
2000.00000	_ _ ∓ _ =	1.000000		CDCER=	0.053000
5000.00000	=W30	0.0		COEXP=	1.000000
1.000000	=17	1.000000		CICER=	0.014000
0.00086.0	12=	000000009		CI EXP=	1.000000
0.02000	73=	1.000000			
1.000000	= + 7	1.000000	= 57	0.0	
CALCULATED VALUES	KG	SUM TO 1	1.2.2.2		S, MILLIONS
CD=CDCER X (T X DF)XX(CDEXP)	P) X CF				265.000
CLRM=CICER X (M)XX(CIEXP)	X CF X TF				70.000
Σ					1.000
=1.0 + LOG(PHI) / LOG(2.0)	2.0)				0.971
CTFU=(CLRM / E)X((#RM X ZI	ZI+.5)XX(E) -0	-0.5XX(E))			70.095
CTB = ((CLRM/E)X((#RM X	23 + 0.51XX(	0.5)XX(E) -0.5XX(E))		1 / 23	70.095
CIPS=CT8*24/22	: :				1.168
=CTB X R					1.402
= 06M OR CTB*25/22/ENN	2/ENYR				0.0
			:		

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.2.2.2.3 CREW SUPPORT MODULE/EVA TABLE

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	INPUT PAR	ARAMETERS	1	i	INPUT CO	INPUT COEFFICIENTS
<u>  </u>	27000.0000	16=	1.000000		CDCER=	0.012432
¥	27000,0000	=W30	0.0		CDEXP=	1.000000
C F=	1.000000	<b>~17</b>	1.000000		CICER=	0.005798
=1 H d	0.980000	22=	000000.09		CIEXP=	1.000000
4	0.02000	23=	1.000000	1		
DF=	1.000000	= + 7	1.000000	= 57	0.0	
CALC	CALCULATED VALUES	KG	SUM TO 1.	1.2.2.2		S, MILL IONS
CD=CDCER	CD=COCER X (T X DF)XX(CDEXP)	) X CF				335.664
CLRM=CICER	R X (M)XX(CIEXP) X	CF X TF				156.546
#RM =T /	Σ					1.000
0°1"	=1.0 + LOG(PHI) / LOG(2.0)	.0)				0.971
CTFU=(CLR	CTFU=(CLRM / E)X((#RM X Z1+.5)	XX(E)	-0.5XX(E))			156.759
CTB = ((CL	CTB = ((CLRM/E)X((#RM X Z	23 + 0.51XX(E)	) -0.5xx(E))		1 / 23	156,759
CIPS=CTB*Z4/Z2	27/57			:		2.613
CRCI	=CTB X R					3.135
W300	= 06M OR CT8*25/22/F	/FNYR				0.0
COMMENTS	:			:		

# 1.2.2.3 OPERATIONS

This element includes the planning, development, and conduct of operations at the logistics support facility. It includes both the direct and support personnel and the expendable maintenance supplies required for logistics support.

An average of 24 crew members are required at the LEO Base to support orbital operations. Engineering estimates were made of the operations and consumable requirements at LEO. See Tables 1.2.2.3.1 and 1.2.2.3.2.

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.2.2.3.1 LEO OPERATIONS CREW TABLE

		INPUT PAR	ARAMETERS			INPU	INPUT COEFFICIENTS	I ENT S
	=	24.000000	<b>1</b> F=	1.000000		CDCER=	0.0	0
	¥.	24.000000	=W30	0.0	<u>.</u>	CDEXP=	0•0	0
	C.F=	1.000000	2.1=	1.000000		CI CER=	0.0	0.062400
	=1 Hd	1.000000	=77	000000.09		C1EXP=	1.0	000000
i	<b>8</b> =	0.0	23=	31.000000				
	0 F=	1.000000	= + 7	30.00000	= 57	Ö	0.0	
	CALCULAT	CALCULATED VALUES	MEN	SUM TO 1.	1.2.2.3			* WILLIONS
	CD=CDCER X (T	(T X DF)XX(CDEXP)	X CF			:		0.0
	CLRM=CICER X	(M)XX(CIEXP) X C	CF X TF					1.498
В-	#RM = T / M							1.000
183	E = 1.0 + LO	1.0 + LOG(PHI) / LOG(2.0	.0)		!		- ;	1.000
	CTFU=(CLRM / E)X((#RM X	E)X((#RM X Z1+.5	)XX(E)	-0.5XX(E))		•		1.498
	CTB = ((CLRM/E)X((#RM	)X((#RM X Z3	3 + 0.5) XX(E)	E) -0.5XX(E))		) / 23		1.498
;	CIPS=CTB*Z4/Z2	2			:			0.749
	CRCI = CTB	вхк						0.0
	M30 = M300	M OR CTB*25/22/E	/ ENYR					0.0
!	COMMENTS	:		1	:	:		

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.2.2.3.2 LEO CREW PROVISIONS TABLE

31104-0000	RAMETERS TE	1.000000	· · · · · · · · · · · · · · · · · · ·	INPUT CO	INPUT COEFFICIENTS
0000	=W30	0.0		CDEXP=	0.0
1.000000	. =17	1.000000		CICER=	0.000022
000000	<b>22=</b>	000000.09		CI EXP=	1.000000
0.0	-62	31.000000			
1.000000	= + 7	30.000000	= 57	0.0	
VALUES	KG	SUM TO 1	1.2.2.3		S.MILLIONS
CD=CDCER X (T X DF)XX(CDEXP) X	X CF		1		0.0
CLRM=CICER X (M)XX(CIEXP) X	CF X TF			,	0.684
					1.000
=1.0 + LOG(PHI) / LOG(2.0)	(0)				1.000
CTFU=(CLRM / E)X((#RM X Z1+.5)X	X(E)	-0.5XX(E))			0.684
CTB = ((CLRM/E)X((#RM X Z3	+	0.5)XX(E) -0.5XX(E))		1 / 23	0.684
	f				0.342
œ					0•0
06M OR CTB*Z5/Z2/ENY	/ ENYR				0.0
:			i :	! ! !	

### 1,2,3 SATELLITE O&M SUPPORT FACILITIES

This element includes the facilities, equipment, and operations required in GEO to support the operations and maintenance of the satellite system. Included are the on-orbit monitor and control facility and the life support facilities and equipment required to provide confortable safe living quarters for the resident crew members.

A permanent satellite operations and maintenance base is installed on each satellite at a location near the antenna to provide best access to all systems of the satellite. The base has facilities for both the crew and for storage of maintenance material, and installation/repair equipment. Table 1.2.3 identifies the supporting facilities.

SYSTEM Description	ABBREVIATION	WORK SUPPORT FACILITIES	CREW SUPPORT FACILITIES
AIRLOCK DOCKING MODULE	ADM	3	1
CREW HABITABILITY HODULE	CHM		1
CONSUMABLES LOGISTICS MODULE	CLM		1
BASE MANAGEMENT MODULE	вим	1	
CREW SUPPORT MODULE/EVA	CSM/EVA		1
PRESSURIZED STORAGE MODULE	PSM	2	

Table 1.2.3 Satellite O&M Base

### 1.2.3.1 WORK SUPPORT FACILITIES

This element includes the facilities and equipment required for operation and maintenance of the satellite system. Included are satellite monitor and control stations and any centralized repair facilities not included under maintenance.

The ADM is required at four places for the integration of other modules comprising the satellite O&M base. Three of these modules are to be used primarily for work support operations. The satellite BMM incorporates a monitoring and fault isolation capability for the SPS satellite subsystems as well as the controls required for alternate operational modes and functional isolation of selected subsystems for maintenance. The cost estimates of these modules and the PSM are shown in Tables 1.2.3.1.1, 1.2.3.1.2 and 1.2.3.1.3. The CERs are based on Rockwell Space Station studies.

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.2.3.1.1 AIRLOCK DOCKING MODULE-ADM TABLE

1		INPUT PARA	ARAMETERS			NI	UT CO	INPUT COEFFICIENTS
	<u>"</u>	2500.00000	<b>1</b> F≈	1.000000		CDCER=		0.0
	¥	2500.00000	=W30	0.0		CDEXP=		0.0
	CF.	1.000000	21=	3.000000		CI CER=		0.006036
	=1 Hd	0.980000	22=	000000000		CIEXP=		1.000000
į	**	0.02000	73=	180.00000				
	0F=	1.000000	= 47	180.000000	= 57		0.0	
	CAL CUL ATED	TED VALUES	KG	SUM TO 1.	.2.3.1			\$, MILLIONS
	CD=CDCER X (	(T X DF)XX(CDEXP)	X CF		1	:		0.0
	CLRM=CICER X	X (M)XX(CIEXP) X CF	CF X TF					15.090
B-	#RM =T / M							1.000
186	ш	=1.0 + LOG(PHI) / LOG(2.0)	•0)					0.971
	CTFU=(CLRM /	CTFU=(CLRM / E)X((#RM X Z1+.5	•5)XX(E) -0.5XX(E))	•5XX(E))				44.520
	CTB = ((CLRM/	=((CLRM/E)X((#RM X Z	Z3 + 0.5)XX(E)	E) -0.5XX(E))		1 / 23		13,352
!	CIPS=CTB*24/22	.72						40.056
	CRCI = C	=CTB X R						0.267
	) = W30)	06M OR CT8*25/22/ENYR	/ENYR					0.0
	COMMENTS SEF 1.2.1.2.1	.1.2.1 FOR DDTEE			: :	:	; ; ;	

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.2.3.1.2 BASE MGMT MODULE-BMM TABLE

	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	INPUT	INPUT PARAMETERS		!	INPUT CO	INPUT COEFFICIENTS
	- <u>-</u>	27000.0000	<b>∓</b> F=	1.000000		COCER=	0.0
	=======================================	27000.0000	=W30	0.0		CDEXP=	0.0
U	CF≅	1.000000	-17	1.000000		CICER=	0.011496
H.d.	PHI=	0.086.0	22=	000000.09		CI EXP=	1.000000
	<u>م</u> =	0.02000	23=	00000009			
<b>a</b>	DF=	1.000000	= + 7	00000000	<b>72</b> =	0.0	
	CALCUL	CALCULATED VALUES	KG	SUM TO L.	1.2.3.1		S, MILL IONS
0)=0)	CER X	CD=CDCER X (T X DF)XX(CDEXP)	XCF		:		0.0
CL RM=	CICER	CLRM=CICER X (M)XX(CIEXP) X CF	CF X TF				310,392
1	#RM =T / M						1.000
ய 187	1.0 + 1	=1.0 + LOG(PHI) / LOG(2.	•0)				0.971
CT FU=	CLRM ,	CTFU=[CLRM / E)XI(#RM X 21+.	5) XX(E)	-0.5XX(E))		·	310.814
CTB =	CCLRM,	CTB = ((CLRM/E)X((#RM X Z3	3 + 0.51XX(E)	E) -0.5XX(E))		) / 23	283,323
_CIPS=	CIPS=CTB*24/22	/12					283.322
٥	CRCI =(	=CTB X R					5.666
U	) = W30	CO&M = O&M OR CTB*25/22/ENYR	/ ENYR				0.0
COMMENTS	NTS	ENTS SEE 1.2.2.1.1 FOR DOTEE					

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.2.3.1.3 PRESSURIZED STORAGE MODULE-PSM TABLE

· · · · · · · · · · · · · · · · · · ·	INPUT PARA	ARAMETERS			INPUT	INPUT COEFFICIENTS
=_	15000,0000	TF≈	1.000000	S	CDCER=	0.0
1	15000.0000	=W30	0.0	<b>)</b>	DEXP=	0.0
CF:	1.00000	Z1= 7.2=	2.000000	ن د	CICER	0.013734
***	0.010000	73=	120-00000	)   	1	0000
DF=	1.00000	<u>-</u> <del>-</del> <del>-</del> <del>-</del> <del>-</del> <del>-</del> <del>-</del> <del>-</del> <del>-</del> <del>-</del> <del>-</del>	120.000000	= 57	0.0	0
CALCULATED	ATED VALUES	KG	SUM TO 1.	.2.3.1		S.MILLIONS
CD=CDCER X	(T X DF)XX[CDEXP) X	XCF				0.0
CLRM=CICER	CLRM=CICER X (M)XX(CIEXP) X	X CF X TF				206.010-
#RM =T / M						1.000
E =1.0 +	=1.0 + LOG(PHI) / LOG(2.0)	.0)				0,971
CTFU=(CLRM /	E)X((#RM X	Z1+.5)XX(E) -0	-0.5XX(E))			408.244
CTB = ((CLRM/E)X((#RM	×	13 + 0.51XX	0.5)XX(E) -0.5XX(E))		) / 23	184.403
CIPS=CTB*24/22		:			:	368.805
CRCI =	=CTB X R					1.844
= W300	O&M OR CT8*25/22/EN	2/ENYR				0.0
COMMENTS See 1.2	1.2.1.1.17 FOR ODTEE				:	

# 1.2.3.2 CREW SUPPORT FACILITIES

This element includes the facilities and equipment required for the life support and well-being of the crew members. Included are living quarters, recreation facilities, and health facilities.

The combination crew support and EVA module (CSM/EVA) has the same internal function as for the SCB, but occupies only half of the module. The other half is an integrated multi-crew member EVA preparation area and airlock station.

The ADM, CHM, CLM and CSM/EVA modules are costed in Tables 1.2.3.2.1, 1.2.3.2.2, 1.2.3.2.3, and 1.2.3.2.4. The estimates are based on Rockwell's Space Station studies.

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.2.3.2.1 AIRLOCK DOCKING MODULE-ADM TABLE

= ± u	INPUT PARA 2500.00000 2500.00000	ARAMETERS TF= 05M=	1.000000	1	CDCER= CDEXP=	INPUT COEFFICIENTS = 0.0 = 0.0
=1 Hd	0.00000	=27	60.00000		CI EXP=	1.000000
т. П-1-	1.000000	24= 24=	0000000009	= 57	0.0	
CALCULATED	TED VALUES	KG	SUM TO 1.	1.2.3.2		S, MILL IONS
CD=CDCER X (T X	T X DEXXICOEXP	X CF		!		0*0
CLRM=CICER X	X (M)XX(CIEXP) X	CF X TF				15.090
#RM =T / M						1.000
E =1.0 + L	=1.0 + LOG(PHI) / LOG(2.0)	(0•				0.971
CTFU=(CLRM / E)X((#RM	/ E)X((#RM X Z1+.5	)XX(E)	-0.5xx(E))			111.21
CTB =((CLRM/E)X((#RM	×	Z3 + 0.5)XX(	0.5)XX(E) -0.5XX(E))		) / 23	13.774
CIPS=CTB*24/Z2				!		13.774
CRCI = C	CTB X R					0.275
C C EM = C	OEM OR CTB*25/22/ENYR.	/ENYR.				0.0
COMMENTS SEE 1.2.	1.2.1.2.1 FOR DDTEE					

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.2.3.2.2 CREW HABITABILITY MODULE-CHM TABLE

		INPUT PA	ARAMETERS		:	Z	PUT CO	INPUT COEFFICIENTS
	<u>"</u>	27000.0000	<b>∓</b> = <b>∓</b>	1.000000		CDCER=		0.0
	¥	27000.0000	=W30	0.0		CDEXP=		0.0
	C F	1.000000	=12	1.000000		CICER=		0.003770
	=1 Hd	0.00086.0	=22	000000.09		CI EXP=	-	1.000000
	#	0.02000	23=	000000.09				
	0F=	1.000000	= + 7	000000009	= 57		0.0	
	CALCULATED	ATED VALUES	KG	SUM TO 1.	2.8.2			\$, MILL IONS
i	CD=CDCER X	CD=CDCER X (T X DF)XX(CDEXP)	X CF					0.0
	CLRM=CICER	CLRM=CICER X (M)XX(CIEXP) X	CF X TF					101.790
В-	#RM =T / M							1.000
-191	E =1.0 +	1.0 + LOG(PHI) / LOG(2.	• 0)					0.971
	CTFU= (CLRM	CTFU=(CLRM / E)X((#RM X 21+.	5) XX(E)	-0.5XX(E))				101.928
	CTB = ((CLRM/E)X((#RM	×	Z3 + 0.51XX(E)	E) -0.5XX(E))		1 / 23		92.913
:	CIPS=CTB*24/22				1			92.913
	CRCI	=CTB X R						1.858
	= M3DD	06M OR CTB*25/22/	/ ENYR					0.0
į	COMMENTS SEE 1.2	ENTS SEE 1.2.2.2.1 FOR DDTGE			:	1		

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.2.3.2.3 CONSUMABLES LOGISTICS MODULE-CLM: TABLE

	INPUT	PARAMETERS			INPUT CO	INPUT COEFFICIENTS
<u>=</u>	5000.00000	TF=	1.000000		CDC ER =	0.0
<u> </u>	5000.00000	=W30	0.0		CDEXP=	0.0
C F≅	1.000000	71=	1.000000		CICER=	0.014000
=1 H d	0.00086.0	22=	60.000000		CI EXP=	1.000000
<b>a</b>	0.00000	73=	000000009			
DF=	1.000000	= + 7	000000009	= 57	0.0	
CALCULATED	ATED VALUES	KG	SUM TO	1.2.3.2		\$, MILLIONS
CD=CDCER X	(T X DF)XX(CDEXP	XCF		!		0.0
CLRM=CICER	X (M)XX(CIEXP) X	CF X TF				70.000
M / L= M8# B-						1,000
+ 0. 1. 192	=1.0 + LOG(PHI) / LOG(2.0)	• 0)	-			0.971
CTFU=(CLRM	/ E)X((#RM X Z1+	Z1+.5)XX(E) -0	-0.5XX(E))			70.095
CTB = ((CLRM/E)X((#RM	×	Z3 + 0.51XX(	0.51XX(E) -0.5XX(E))	!   	) / 23	63,895
CIPS=CTB*Z4/Z2	/22			!		63.895
CRCI =	=CTB X R					1.278
= W3D0	= 06M OR CT8*25/22/ENYR	/ ENYR				0.0
COMMENTS SEE 1.2.2.2.2.2	.2.2.2 FOR DDTEE					

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.2.3.2.4 CREW SUPPORT MODULE/EVA TABLE

İ		INPUT PAR	ARAMETERS		i t	IND	UT CO	INPUT COEFFICIENTS
	<b>1</b> ≃	27000.0000	TF≔	1.000000		CDCER=		0.0
	¥.	27000,0000	OEM=	0.0		CDEXP=		0.0
	CF≒	1.000000	<b>71</b> =	1.000000		CICER=		0.005798
	=] Hd	0.00086.0	<b>5</b> 2 =	000000009		CI EXP=		1.000000
į .	# CX	0.02000	23=	000000009				
	DF=	1.000000	= + 2	000000.09	= 57		0.0	
	CALCUL	CALCULATED VALUES	KG	SUM TO 1.	1.2.3.2			S, MILL TONS
	CD=CDCER X	CD=CDCER X (T X DF)XX(CDEXP)	X CF		;	,	; !	0.0
	CLRM=CICER	CLRM=CICER X (M)XX(CIEXP) X						156,546
В-	#RM =T / M							1.000
193	E = 1.0 +	=1.0 + LOG(PHI) / LOG(2.	.0)					0.971
	CTFU=(CLRM	CTFU=(CLRM / E)X((#RM X Z1+.5)XX(E) -0.5XX(E))	•5)XX(E) -0.	,5XX(E))				156.759
	CTB = ((CLRM/E)X((#RM	/E)X((#RM X Z3		+ 0.5) XX(E) -0.5XX(E))		1 / 23		142.894
!	CIPS=CTB*Z4/Z2	722				***************************************		142.894
	CRCI =	=CTB X R						2.858
	= W3DD	CCEM = OEM OR CTB*Z5/Z2/ENYR	/ ENYR					0.0
	COMMENTS SEE 1.2.2.2.3	.2.2.3 FOR DDT&E						

### 1.2.3.3 OPERATIONS

This element includes the planning, development, and conduct of operations at the O&M support facility. It includes both the direct and support personnel and the expendable maintenance supplies required in GEO for satellite operations and maintenance.

The satellite operations base crew is manned by 30 persons on a continuous basis throughout the year. This crew and supporting provisions are costed in Tables 1.2.3.3.1 and 1.2.3.3.2 based on engineering estimates.

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.2.3.3.1 SATELLITE OPERATIONS CREW TABLE

İ		INPUT PARA	PARAMETERS		:	INPUT	INPUT COEFFICIENTS
	#! 	30.00000	<b>1</b> ₽=	1.000000		CDCER=	0.0
İ	<u> </u>	30.00000	=W30	0.0		CDEXP=	0.0
	CF=	1.000000	=17	1.000000		CICER=	0.062400
	PH1=	1.000000	22=	0000000		CI EXP=	1.000000
	<b></b>	0.0	73=	000000009			
	DF=	1.000000	<b>2</b> 4=	00000009	<b>- 57</b>	0.0	
	CALCULATED	D VALUES	MEN	SUM TO 1.	1.2.3.3		S, MILL IONS
:	CD=CDCER X (T X DF)XX(CDEXP) X	X DF)XX(CDEX	P) X CF				0.0
	CLRM=CICER X (M)XX(CIEXP) X CF	M)XX(CIEXP)	X CF X TF				1.872
В-	#RM =T / M						1.000
-195	E =1.0 + LOG	=1.0 + LOG(PHI) / LOG(2.0)	2.0)				1,000
	CTFU=(CLRM / E)X((#RM X Z1+.5	3) X ( (#RM X ZI	-	XX(E) -0.5XX(E))			1.872
,	CTB = ((CLRM/E)X((#RM	×	23 + 0.5) XX	0.5) XX(E) -0.5XX(E))		) / 23	1.872
į	CIPS=CTB*24/22						1.872
ļ	CRCI =CTB	X X				·	0*0
	130 = M333	08M OR CT8*25/22/ENYR	2/ENYR				0.0
!	COMMENTS		1 1 2 2 2 4				

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.2.3.3.2 SATELLITE CREW PROVISIONS TABLE

-	INFU-L-PAKAM	NAME I ENS			I NAOI	INFO! CUEPTICIENIS
T= 38880,0000	000		1.000000		COCER=	0.0
3888	000	=W30	0.0		CDEXP=	0.0
CF= 1.00	1.000000	21=	1.000000		CI CER=	0.000022
PH I= 1.00	1.000000	Z 2=	00000009		CI EXP=	1.000000
R= 0.0		23=	00000009			
DF= 1.0(	000000	= 47	6000000	= 57	0.0	0
CALCULATED VALUES	ES	KG	SUM TO 1.	1.2.3.3		\$+WILLIONS
CD=CDCER X (T X DF)XX(CDEXP) X	X ( CDEXP)	X CF		:		0.0
CLRM=CICER X (M)XX(CIEXP)	×	CF X TF		•		0.855
=T / M						1,000
=1.0 + LOG(PHI) / LOG(2.0)	/ 106(2.	(0)				1.000
CTFU=(CLRM / E)X((#RM X	M X Z1+.5)	XX(E)	-0.5XX(E))			0.855
CTB = ((CLRM/E)X((#RM	x 23	+	0.5) XX(E) -0.5XX(E))		1 / 23	0.855
CIPS=CTB*24/22	: : :					0.855
CRCI =CTB X R						0.0
CCEM = DEM OR CTI	CT B*25/22/ENYR	ENYR				0.0
	,	•				

I

### 1.3 TRANSPORTATION

This element of the costing includes all space transportation required to support the satellite system assembly and operation. Included are transportation requirements supporting the precursor activity, launch to LEO, orbit—to—orbit transfer of all hardware, materials, and personnel, and intra—orbit movement of cargo during the construction and lifetime operation of the satellite system.

The overall scenario for SPS space transportation systems consists of seven major elements -- Space Shuttle derivatives for personnel (PLV) and precursor cargo (STS-HLLV); SPS heavy lift launch vehicle (HLLV); electric orbit transfer vehicle (EOTV); intra-orbit transfer vehicle (IOTV); personnel orbit transfer vehicle (POTV); personnel module (PM); and orbital/ground support facilities. Transportation requirements and concepts for SPS vary as a function of program phase. During the verification planning period (1981 - 1987), the baseline Shuttle is used to conduct sortie missions. Later in the verification program "growth" Shuttle is used to deliver personnel and cargo to LEO. The Shuttle derived HLLV is also employed early in the program for LEO fabrication of the space construction base plus support in building the precursor satellite (EOTV) test model. Figure 1.3-1 illustrates early program systems and identifies the SPS VTO/HL HLLV that will be needed for the fabrication of flight EOTVs and the mass-to-orbit requirements of satellite construction.

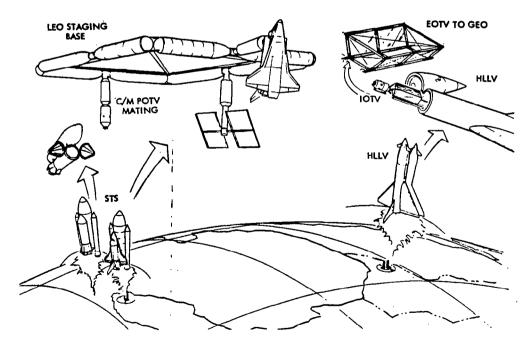


Figure 1.3-1. SPS Transportation System - LEO Operations
Operational Program

R.T. FLIGHTS PER VEHICLE

Geosynchronous orbit is the eventual destination of SPS construction materials/equipment, personnel, and supplies. The crews will be transported from earth to LEO by the growth Shuttle containing the personnel module (PM) where the PM will then be carried to GEO by the POTV. Cargo will be delivered to LEO by the SPS VTO/HL-HLLV configuration, transferred to the EOTV by IOTV's, transported to GEO by the EOTV, and off-loaded by IOTV's. Additional detail on the individual vehicles is presented in later subsections.

Mass-to-orbit requirements for construction, propellant, and operations/maintenance activities were established in accordance with the mission profile and build schedule of two SPS satellites per year with a first unit (TFU) by the end of year 2000. These calculations were based on a round trip vehicle life as shown in Table 1.3-1.

Table 1.3-1. Vehicle Life with Maintenance

STS GROWTH VEHICLE FOR PLV/CARGO	100
SPS-VTO/HL HEAVY LIFT LAUNCH VEHICLE	300
EOTV-CARGO (ELECTRIC) ORBIT TRANSFER VEH.	20
POTV-PERSONNEL ORBIT TRANSFER VEHICLE	100
IOTV-INTRO-ORBIT TRANSFER VEHICLE	200

VEHICLE

Table 1.3-2 shows the vehicle fleet and vehicle flight requirements to build the first SPS satellite, LEO construction base, and the EOTV test vehicle. These calculations were based on the mass-to-LEO and GEO for personnel, materials, and supplies identified to each of the transportation modes. Precursor activities can be completed by utilizing (1) the two existing TFU personnel modules (PMs); and (2) an additional PLV over the two needed for the TFU. Two Shuttle launch vehicle sets will be combined with a cargo container/engine module to transport materials to LEO for the precursor activity. TFU vehicle requirements are based on mission timelines, turnaround schedules, and flight profiles.

Table 1.3-3 tabulates the total program transportation requirements and the number of flights per vehicle as needed to construct the satellites and to provide operations and maintenance after IOC. These calculations are the basis for developing overall fleet requirements for a 60-unit SPS program, but do not include the precursor effort identified in Table 1.3-2 nor the additional vehicles needed for attrition/spares or overhaul (replacement capital investment).

Table 1.3-2. TFU Transportation Requirements

	MASS x	10 <sup>6</sup> KG			EHICLE 1	FLIGHTS			
	LE0	GEO	PLV	HLLV	POTV	EOTV	LEO	TV GEO	
SATELLITE CONST. MAINT. & PACKAGING	37.12	37.12	45	163.5	45	6.5	164	164	
CREW CONSUMABLES & PKG.	0.98	0.94	_	4.3	-	0.2	4	4	
POTV PROPELLANTS & PKG.	2.91	1.46	-	12.8	-	0.3	13	. 6	
EOTV CONST., MAINT. & PKG.	7.20	-	15	31.7	-	-	32	-	
EOTV PROPELLANTS & PKG.	4.79	-	-	21.1	- '	-	21	-	
IOTV PROPELLANTS & PKG.	0.13	0.06	-	0.6	-	-	1	-	
·	<u> </u>		i	1			235	174	
TOTAL	TOTAL 53.13 39.				45	7.0	4	09	
TFU FLEET VEHICLE REQUIREME	NTS		2_	5	4	6	4		
GROWTH SHUTTLE VEHICLE/OPER REQUIREMENTS FOR PRECURSOR (LEO BASE, SPACE CONSTRUCT)	ACTIVITI			72 FLIGH 1 VEHIC			29 FLIGH VEHICLE		
EOTV TEST VEHICLE - EOTV'S)	UN DAGE,	nii <b>u</b>	PEI	RSONNEL	(PLV)		CARRIER/ AND LAU		

Table 1.3-3. Total Program Transportation Requirements

	MASS x	10 <sup>6</sup> KG		v	EHICLE 1	LIGHTS		
			PLV	HLLV	POTV	EOTV	I	TV
	LEO	GEO					LEO	GEO
SATELLITE CONSTRUCTION OPERATIONS & MAINTENANCE	2197.8 1803.0	2197.8 1803.0	1340 3694	9682 7943	1220 3660	425.1 348.7	9682 7943	9682 7943
CREW CONSUMABLES CONSTRUCTION OPERATIONS & MAINTENANCE	31.5 86.8	28.7 86.0	-	139 382	-	5.6 16.6	139 382	126 379
POTV PROPELLANTS CONSTRUCTION OPERATIONS & MAINTENANCE	82.7 267.8	41.4 133.8	-	364 1180	-	8.0 25.9	364 1180	r82 589
EOTY CONSTRUCTION CONSTRUCTION OPERATIONS & MAINTENANCE	28.2 22.2	24.2 19.0	-	124 98	-	4.7 3.7	124 98	107 84
EOTV PROPELLANTS CONSTRUCTION OPERATIONS & MAINTENANCE	340.3 304.0	2.0 -	Ξ	1499 1339	-	0.4	1499 1339	9
IOTV PROPELLANTS CONSTRUCTION OPERATIONS & MAINTENANCE	7.2 6.6	3.3 3.0	-	32 29	-	0.6 0.6	32 29	15 13
SUMMARY CONSTRUCTION OPERATIONS & MAINTENANCE TOTAL	2687.7 2490.4 5178.1	2297.4 2044.8 4342.2	1340 3694 5034	11840 10971 22811	1220 3660 4880	444 396 840	11840 10971 22811	10121 9008 19129
VEHICLE FLEET CONSTRUCTION OPERATIONS & MAINTENANCE		-	14 37	39 37	12 37	22 20	10	10
TOTAL			51	76	49	42	2	10

# 1.3.1 SPS HEAVY LIFT LAUNCH VEHICLE (HLLV)

The SPS HLLV is shown in Figure 1.3-2 and has a payload capability of 227,000 kg with a vertical take-off and horizontal landing feature. The SPS HLLV is used to bring space construction and support equipment payloads, satellite system hardware, OTVs, consumables and crew expendables, and propellants from earth to LEO. This element covers the SPS HLLV vehicles and operations required to support the satellite system assembly and operation during a 30 year life. Ground rules and guidelines applicable to the HLLV are summarized in Table 1.3-4.

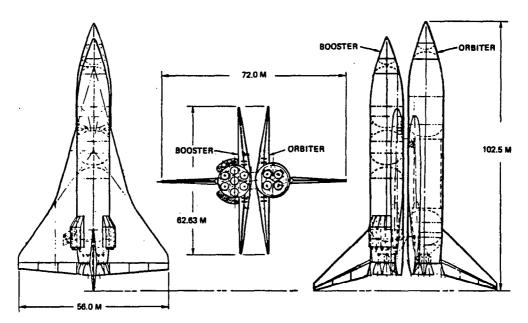


Figure 1.3-2. SPS Transportation System Launch Configuration

Table 1.3-4. HLLV Ground Rules/Assumptions

TWO-STAGE VERTICAL TAKEOFF/HORIZONTAL LANDING (VTO/HL)

FLY BACK CAPABILITY BOTH STAGES - ABES FIRST STAGE ONLY

PARALLEL BURN WITH PROPELLANT CROSSFEED

LOX/RP FIRST STAGE - LOX/LH2 SECOND STAGE

HI P<sub>C</sub> GAS GENERATOR CYCLE ENGINE - FIRST STAGE [I<sub>S</sub> (VAC) = 352 SEC.]

HI P<sub>C</sub> STAGED COMBUSTION ENGINE - SECOND STAGE [I<sub>S</sub> (VAC) = 466 SEC.]

STAGING VELOCITY - HEAT SINK BOOSTER COMPATIBLE

CIRCA 1990 TECHNOLOGY BASE - BAC/MMC WEIGHT REDUCTION DATA

ORBITAL PARAMETERS - 487 KM @ 31.6°

PAYLOAD CAPABILITY - 227×10³ KG UP/45 KG DOWN

THRUST/WEIGHT - 1.30 LIFTOFF/3.0 MAX

152 WEIGHT GROWTH ALLOWANCE/0.75% AV MARGIN

### 1.3.1.1 SPS HLLV FLEET

A total of 76 HLLV vehicles are required to handle the mass flow requirements throughout the 60 year SPS program. Thirty-nine vehicles are required for the construction of 60 satellites and 37 vehicles are needed for operation and maintenance during the 30 year satellite lifetime.

Data used in projecting estimates for the HLLV and supporting flight costs were factored from the NASA/JSC contract NAS9-15196. Specific changes were made to consider the reference HLLV design configuration; vehicle complexity factors — engines, ablative shield, propellant valves, and system/subsystem design; plus the greater mass of the Orbiter/booster as compared with current experience and Rockwell Space Shuttle contract work.

HLLV capital asset replacements, major overhaul requirements, spares provisioning, and system lifetimes were projected as being equivalent to two vehicle replacements for each of the SPS fleet vehicles. These calculations are reflected as an annual cost per satellite over the 30 year period.

The DDT&E cost estimate was developed from a careful evaluation of the NAS9-15196 data base and a comparative factoring of these data as compared with data directly applicable to the Space Shuttle program.

See Table 1.3.1.1 for the SPS HLLV cost computer program tabulation.

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.3.1.1 SPS-HLLV FLEET TABL E

1.000000	<b>1</b> F≃	1.000000		CDCER=	8600.00000
000	-W30	0.0		CDEXP=	1.000000
1.000000	21=	5.000000		CICER=	2000.00000
000	<b>22=</b>	000000*09	-	CIEXP=	1.000000
440	Z3=	228.000000		**************************************	
000000	= + 7	39.000000	= 57	37.(	37.000000
	SET	SUM TO 1.	1.1		\$, MILL IONS
DF)XX(CDEXP)	X CF		:		8600.000
(M)XX(CIEXP) X C	.F X TF				2000.000
					1.000
L06(2.0					0.880
X Z1+•9	XX(E)	5XX(E))			8950.176
X 23	+ 0.5) XX (E	) -0.5xx(E))		1 / 23	1180.031
					767.020
					99.642
15/12/1	a A N				24.256
:			:	i : : :	
	0.920000 0.084440 1.000000 ALUES (ALUES (X(CIEXP) X C (X(CIEXP) X C (I#RM X Z1+.5 (R (R (R (R (R	XP) X X CF X CF X CF 11.51X 11.51X 22/ENY	Z2= 60.00000 Z3= 228.000000 Z4= 39.000000 SET SUM TD X CF X TF X CF X TF X CF X TF Z2/ENYR	Z2= 60.00000 Z3= 228.000000 Z4= 39.000000 SET SUM TD 1.3. X CF X TF X CF X TF Z2 ENYR	Z2= 60.00000 CIEXP= Z3= 228.00000 Z5= Z4= 39.00000 Z5= SET SUM TD 1.3.1 X CF X TF X CF X TF Z3 + 0.51XX(E) -0.5XX(E))

### 1.3.1.2 SPS HLLV OPERATIONS

This element includes the necessary vehicle operations (user charge per flight including payload integration) required to support the SPS program. The HLLV has a lifetime capability of 300 flights.

There are a total of 22.811 round trip flights required to support the 60 year program where approximately 227,000 kg is delivered per flight. These are grouped into a total of 11840 flights for construction and 10,971 flights for operations and maintenance. The TFU requires a total of 234 flights to carry the necessary mass to orbit. On the average of 60 satellites, approximately 197 flights are needed for satellite construction and 6 flights are required for annual operations and maintenance per satellite.

The projected cost per HLLV flight is based on contract data (reference NAS9-15196) that was factored and revised to arrive at a propellant, payload integration, and supporting operational cost by evaluation against such things as propellant costs versus HLLV requirements. See Table 1.3.1.2.

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.3.1.2 SPS-HLLV OPERATIONS TABLE

	INPUT PARAM	PARAMETERS			INPUT COEFFICIENTS	FICIENTS
H H	1.000000	TF=	1.000000	202	=R=	0.0
≡ <b>X</b>	1.000000	=W30	0.0	(302)	(P=	0.0
C F=	1.000000	21=	234.000000	<b>01</b> 0	FR=	2.480000
=] Hd	1.000000	7.2=	00000009	CI EXP=	=d)	1.000000
<b>R</b> =	0.0		22811.0000			
0F=	1.000000	= + 7	11840.0000	= 57	10971.0000	
CALCULATED VALUES	D VALUES	FLIGHT	SUM TO 1.	1.3.1		S,MILLIONS
CD=CDCER X (T X DF)XX(CDEXP) X	X DE ) XX ( CD EXI	P) X CF				0.0
CLRM=CICER X (	X (M)XX(CIEXP)	X CF X TF				2.480
B #RM = 1 / M						1.000
901 + 0 • 1 = 3 4	=1.0 + LOG(PHI) / LOG(2.0)	2.01				1.000
CTFU=(CLRM / E)X((#RM X	)X((#RM X ZI	ZI+.5)XX(E) -C	X(E) -0.5XX(E))			580.320
CTB = ((CLRM/E)X((#RM	×	Z3 + 0.51XX(	0.51XX(E) -0.5XX(E))		/ 23	2.480
CIPS=CTB*Z4/Z2						489.387
CRCI = CTB	×					0.0
M30 = M3JJ	06M OR CTB*25/22/ENY	2/ENYR				15.116
COMMENTS						

## 1.3.2 CARGO ORBITAL TRANSFER VEHICLE (COTV)

This element includes the COTV vehicle and operations required to support the satellite system assembly and operation. Included is the LEO-to-GEO transfer of space construction and support equipment, satellite system hardware, spares, and propellants required throughout the satellite lifetime.

The Rockwell cargo orbital transfer vehicle is a high specific impulse configuration that is possible with electric propulsion. The concept is shown in Figure 1.3-3 and has a payload capability of  $5.17\times10^6$  kg (equivalent to 23 HLLV payloads) with a 6 month round trip time per flight.

COTV fleet procurement and operations are detailed in sections 1.3.2.1 and 1.3.2.2, respectively.

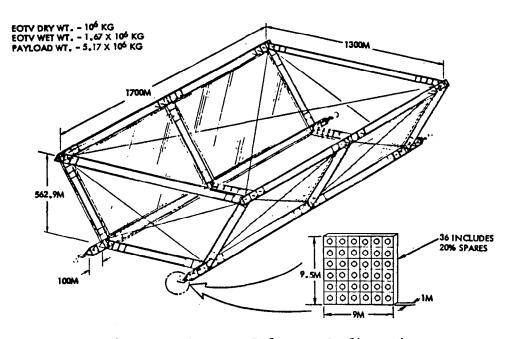


Figure 1.3-3. EOTV Reference Configuration

#### 1.3.2.1 COTY FLEET

This element includes the vehicle fleet procurement required for the SPS.

The electric OTV structural configuration is essentially the same as that employed for the satellite bay. It has a weight of 871,753 kg's. The EOTV weight and payload summary is shown in Table 1.3-5.

SOLAR ARRAY		588,196
CELL/STRUCTURE	299,756	200,000
POWER CONDITIONING	288.440	
THRUSTER ARRAY (4)	200,110	96,685
	10,979	30,003
THRUSTERS/STRUCTURE		
CONDUCTORS	4,607	
BEAMS/GIMBALS	2,256	
PROPELLANT TANKS	78,843	
ATTITUDE CONTROL SYSTEM		186,872
POWER SUPPLY (INCL. ENERGY STORAGE)	184.882	
SYSTEM COMPONENTS	274	
PROPELLANT TANKS	1.716	
EOTY INERT WEIGHT	.,,,,	871,753
25% GROWTH		217.938
- <del>-</del>		1,089,691
TOTAL INERT WEIGHT		666,660
PROPELLANT WEIGHT		000,000
TRANSFER PROPELLANT	655,219	
ACS PROPELLANT	11,441	_
EOTV LOADED WEIGHT		1,756,351
PAYLOAD WEIGHT		5,171,318
LEO DEPARTURE WEIGHT		6,927,669

Table 1.3-5. EOTV Weight Summary (kg) (GaAlAs)

The thruster array consists of 36 units at four locations for a total of 144 thrusters with a maximum of 64 thrusters operable simultaneously. The total attitude control system and thruster array mass is equal to 283,557 kg's per EOTV.

The EOTV CERs are the same as those used for the satellite costs on the same subsystem elements. The replacement capital investment calculation is based on an attrition factor of 5-6% of each flight vehicle. Table 1.3-6 lists the elements of cost for the EOTV.

WBS NO.	DESCRIPTION
1.3.2.1.1	PRIMARY STRUCTURE
1.3.2.1.2	SECONDARY STRUCTURE
1.3.2.1.3	CONCENTRATOR
1.3.2.1.4	SOLAR BLANKET
1.3.2.1.5	SWITCHGEAR AND CONVERTERS
1.3.2.1.6	CONDUCTORS AND INSULATION
1.3.2.1.7	ACS HARDWARE
1.3.2.1.8	INFO MANAGEMENT AND CONTROL

Table 1.3-6. EOTV Cost Elements

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.3.2.1.1 PRIMARY STRUCTURE TABL E

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.3.2.1.2 SECONDARY STRUCTURE TABLE

		INTO! TAKAMETEKS			INTE	
#I	14918.0000	TF=	1.000000		CDC ER=	0.156000
11 2	5.000000	0£M=	0.0		CDEXP=	0.511000
C.F=	1.000000	21=	0000009		CI CER=	0.101000
₽ĤI≍	0.086.0	22=	60.000000		CI EXP=	0.355000
<b>«</b>	0.003500	-62	44.000000			
0F=	0.05000	= + 7	22.000000	= 97	20.0(	20•00000
CALCULATED	ATED VALUES	KG	SUM TO 1.3	1.3.2.1		S.MILL IONS
CD=CDCER X	CD=CDCER X (T X DF)XX(CDEXP)	XCF				4.582
CLRM=CICER	X (M)XX(CIEXP) X	CF X TF				0.179
#RM =T / M					-	2983.600
E = 1.0 +	=1.0 + LOG(PHI) / LOG(2.0)	.01				0.971
CTFU=(CLRM	CTFU=(CLRM / E)X((#RM X Z1+.5)	, 5) XX(E) -0.5XX(E))	5XX(E))		•	2478.750
CTB = ((CLRM	=((CLRM/E)X((#RM X Z3	3 + 0.5)XX(E)	) -0.5xx(E))		1 / 23	389.820
CIPS=CTB*Z4/Z2	172					142.934
CRCI =	=CTB X R					1.364
= W3DO	06M OR CTB*25/22/ENYR	/ENYR				4.331

İ

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.3.2.1.3 CONCENTRATOR TABLE

1.000000   21
= 44.000000 = 22.000000
F F TF
F TF (E) -0.5xx(E)) (5) xx(E) -0.5xx(E)) (1
4.000 (E) -0.5xx(E)) 1 / 23
(E) -0.5xx(E)) (5) xx(E) -0.5xx(E)) (7.23
(E) -0.5XX(E)) 1 ( ) / 23
(E) -0.5xx(E)) .5)xx(E) -0.5xx(E))
.5) XX(E) -0.5XX(E)) ) / 23

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.3.2.1.4 SOLAR BLANKET TABLE

T= 90000 CF= PHI= R= DF= CALCULATED \ CLRM=CICER X (M)) CLRM=CICER X (M)) #RM = T / M E = 1.0 + LOG(PH E = 1.0 + LOG(PH CTFU=(CLRM/E)X(COMPENTS)	INPUT PARAMETERS	TF= 1.000000 CDCER=	0.0 CDEXP=	00 21=	22= 60.00000 CIEXP=	23= 44.00000	= + 2	/ALUES SQ M SUM TO 1.3.2.1 \$, MILLIONS	7.664	(X(CIEXP) X CF X TF 1.256	48.000	11) / LDG(2.0)	((#RM X 21+.5)XX(E) -0.5XX(E))	[#RM X Z3 + 0.51XX(E) -0.5XX(E)) ) / Z3 54.757	220.077	( R	CTB*Z5/Z2/ENYR	
	INPUT PARAMET		18750.0000 DEM=	00			0.020000 24=	VALUES SQ	(T X DF)XX(CDEXP) X CF	ш		LOG(PHI) / LOG(2.0)	E)X((#RM X Z1+.5)	73 +	27.	×	OR CT8*25/22/E	

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.3.2.1.5 SWITCHGEAR AND CONVERTERS TABLE

7= 2	1					
	2875.00000	TF=	1.000000	000	ER =	0.158000
# <b>U</b>	719.000000	=W30	0.0	CDE	XP=	0.297000
5	1.500000	21=	9.000000	010	ER=	0.000400
₽H I=	0.950000	2 2=	60.00000	CIE	CI EXP=	1.000000
<b>~</b>	0.001111	23=	44.000000			ļ
DF=	0.500000	= + 7	22.000000	= 57	20.00000	0
CALCULATED VALUES	VALUES	KG	SUM TO 1.3	1.3.2.1		S, MILLIONS
CD=CDCER X (T X DF)XX(CDEXP)	OF JXX(CDEXP	XCF				2.054
CLRM=CICER X (M	X (M)XX(CIEXP) X	CF X TF				0.431
#RM =T / M						3,999
E = 1.0 + LOG(	=1.0 + LOG(PHI) / LOG(2.0)	.0)				0.926
CTFU=(CLRM / E)X((#RM.X	X((#RM_X 21+.5)	XX(E)	-0.5XX(E))			8.760
CTB = ([CLRM/E)X([#RM	[[#RM X 23	+	0.5)XX(E) -0.5XX(E))		/ 23	1.268
CIPS=CTB*24/22				; ; ;		0.465
CRCI = CTB	×					0.001
CCEM = OEM OR	OR CT8*25/22/ENYR	/ENYR				0.014

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.3.2.1.6 CONDUCTORS AND INSULATION TABLE

PUT PARAMETERS INPUT COEF!  TF= 1.000000 CDCER=	0 21= 0 22=	Z3= 44.000000 Z4= 22.000000 Z5= 20.000000	LUES KG SUM TO 1.3.2.1 \$, MILLIONS	)XX(CDEXP) X CF	(CIEXP) X CF X TF 0.030	166.14	1.000	#RM X Z1+.5) XX(E) -0.5XX(E)) 8.584	RM X Z3 + 0.5)XX(E) -0.5XX(E)) ) / Z3 1.431	0.525	R 0.002
INPUT PAR 357675.000		0.020000	CALCULATED VALUES	CO=COCER X (T X DF)XX(CDEXP) X		#RM =1 / M	E =1.0 + LOG(PHI) / LOG(2.0)	CTFU=(CLRM / E)X((#RM X ZI+.5)		C1PS=C1B*24/22	CRCI =CTB X R

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.3.2.1.7 ACS HARDWARE TABLE

	INPUT P	PARAMETERS			INPUT	INPUT COEFFICIENTS
## 	283557.000	TF=	0.093800		CDCER=	1.122000
¥.	1970.00000	= W3 O	0.0		CDEXP=	0.190000
CF=	1.000000	21=	6.000000		CI CER=	0.057000
=I Hd	0.950000	22=	000000.09		CI EXP =	0.729000
<b>2</b>	0.003500	73=	44.000000	 		
0F=	00000 8.0	= + 7		= 57	20.00000	0000
CALCU	CALCULATED VALUES	KG	SUM TO 1.3.2.1	2.1		S'HILLIONS
CD=COCER X	CD=CDCER X (T X DF)XX(CDEXP)	XCF	:		: !	169.6
CLRM=CICER	CLRM=CICER X (M)XX(CIEXP) X	CF X TF				1.348
#RM =T / M						143,938
+; 0•I" ш.	=1.0 + LOG(PHI) / LOG(2.0	.0)				0.926
CTFU=(CLRM	CTFU=(CLRM / E)X((#RM X 21+.5	) XX(E)	-0.5XX(E))			762.015
CTB = ((CLR	CTB = ((CLRM/E)X((#RM X Z	Z3 + 0.5)XX(	+ 0.5)XX(E) -0.5XX(E))		1 / 23	109.634
CIPS=CTB*24/Z2	4/22			i i t		40.199
CRCI	=CTB X R					0.384
= M3DO	06M OR CTB*25/22/E	/ENYR				1.218
COMMENTS	:			!		

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.3.2.1.8 INFO. MGMT. AND CONTROL TABLE

!		INPUT PARAM	ARAMETERS			INPUT CO	INPUT COEFFICIENTS	
	F	0.0	<b>1</b> F≡	1.000000		CDCER=	0.0	
İ	113	0.0	=W30	0.0		CDEXP=	0.0	
	€F=	0.0	z12	00000009		CICER=	0.0	
	PH I=	1.000000	22=	000000.09		CI EXP=	0.0	
İ	2	0.0	23=	60.00000				
	DF=	1.000000	= + 7	000000009	= 57	0.0		
	CALCULATED VALUES	D VALUES	•	SUM TO 1	1.3.2.1			S, MILL IONS
:	CD=CDCER X (T X DF)XX(CDEXP)	X DF 1XX (CDEXP	) X CF		:		***************************************	0.0
	CLRM=CICER X (M)XX(CIEXP)	(M)XX(CIEXP) X	CF X TF					0.0
В-	#RM = 1 / M						0.0	
214	E = 1.0 + LOG	=1.0 + LOG(PHI) / LOG(2.0)	.00	X			0.0	
	CTFU=(CLRM / E)X((#RM X ZI+.5)X	=)X((#RM X ZI+	X(E)	-0.5XX(E))				0.0
	CTB = ((CLRM/E)X((#RM	×	Z3 + 0.5) XX(E	0.5) XX(E) -0.5XX(E))		) / 23		0.0
:	CIPS=CTB*Z4/Z2							0.0
ļ	CRCI =CTB	8 × R						0.0
	N30 = M300	06M OR CTB*25/22/ENY	/ ENYR					0.0
	COMMENTS							:

# 1.3.2.2 COTV OPERATIONS

Necessary vehicle operations (user charge per flight including payload integration) is included in this element.

The flight life of the EOTV is estimated at 20 round trips from LEO to GEO. Four hundred forty-four flights are required for the construction of 60 satellites and an additional 396 flights will maintain the operational satellites for the 30 year period. Seven flights are required to build the first satellite.

The calculations used in this cost estimate are presented in Table 1.3.2.2.

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.3.2.2 COTV OPERATIONS TABLE

INPUT COEFFICIENTS	0.0	0.0	0.630000	1.000000		000	S, MILLIONS	0.0	0.630	1,000	1.000	4.410	0.630	4.662	0.0	0.139	
INPUT CO	CDCER=	CDEXP=	CI CER=	CI EXP=		396.00000	2						) / 23				
	1.000000	0.0	7.000000	000000.09	840.000000	444.000000	SUM TO 1.3.2					-0.5xx(E))	0.5)XX(E) -0.5XX(E))				
ARAMETERS	_ ∓ <del>F</del> =	0.6M=	-17	7.2=	23=	<b>- 7 7 -</b>	FLIGHT	) X CF	X CF X TF		.03	Z1+.5)XX(E) -0	Z3 + 0.51XX(	:		2/ENYR	
INPUT PARAMET	1.000000	1.000000	1.000000	1.000000	0.0	1.000000	VALUES	(T X DF)XX(CDEXP)	(M)XX(CIEXP)		PHI) / LOG(2.0)	E)X((#RM X 214	   ×	:	×	OR CT8*25/22/EN	:
	<u>-</u> L	M	CF=	=1Hd	<b>a</b>	0F=	CALCULATED VALUES	CD=CDCER X (T X	CLRM=CICER X (M	B #RM = T / M	(1Hd)907 + 0°1 = 3 216	CTFU=(CLRM / E)	CTB = ((CLRM/E)X((#RM	CIPS=CTB*24/22	CRCI = CTB	M30 = M300	COMMENTS

#### 1.3.3 PERSONNEL LAUNCH VEHICLE (PLV)

This element includes the space shuttle growth vehicles and operations required to support the satellite system assembly and operation. Included is the launch to LEO and return of all personnel and priority cargo required throughout the satellite construction period and operational lifetime.

In addition to the earth-to-LEO transfer of personnel during satellite construction and operational periods, the space shuttle growth vehicle will 1) accommodate the transfer of personnel and 2) with the cargo/engine module adaptation, will transfer the cargo/material needed for precursor activities dealing with the LEO Base, Space Construction Base, and the initial EOTV-335 mW precursor test article. Shuttle goowth vehicle and flight requirements for the SPS Grogram are identified in Table 1.3.3.

Table 1.3.3. Shuttle Growth Vehicle and Flight Requirements

VEH I CLE/ I TEM	PRECINSOL	THOS SERIES		SATELLITE	, , , , , , , , , , , , , , , , , , ,	TOTAL POPULACI	PLV WEST	CARCO
DESCRIPTION	\&&&	3/ Ē	1 \$ 3	\$ 5	*/ \$ {	<b>\$</b> /\${	\$\\ \display	127
			IICLE RE	QUIREM				<del></del>
SHUTTLE ORBITER (STANDARD VERSION)	(1)	(3)	15	37	26	78	1 EA	
SHUTTLE CARGO CARRIER & MODULE	2				1	3		1 EA
EXTERNAL TANK	(201)	(60)	1541	3694		5235	1 EA	1 EA
LIQUID ROCKET BOOSTER	(6)	(10)	34	74	216	324	2 EA	2 EA
		FL	IGHT RE	QUIREME	NTS			
PERSONNEL LAUNCH VEHICLE (PLV)	(72)	(60)	1412	3694		5106		
CARGO CARRIER LAUNCH VEH. MODULE	129-					129		

The Personnel Launch Vehicle (PLV) is described in section 1.3.3.1 along with the Shuttle derived cargo carrier and engine module required to support the precursor program. PLV operations are described in section 1.3.3.2. The Personnel Module is covered in section 1.3.5.1.

#### 1.3.3.1 PLV FLEET

This element includes the vehicle fleet procurement required to support the SPS program. Included are the vehicles for personnel transfer from earth to LEO and for cargo as needed to support the precursor phase of SPS program development.

The PLV consists of a standard Shuttle Orbiter, an external tank, and two liquid rocket boosters. The cargo vehicle configuration is achieved by replacing the orbiter with a cargo carrier and engine module. The external tank and liquid rocket booster (Figure 1.3.3) are common systems used on the Shuttle derived personnel and cargo vehicles. The integral, SSME-35 powered concept requires four engines with a thrust-to-weight ratio at lift-off of 1.335, which is adequate for both nominal and abort trajectories.

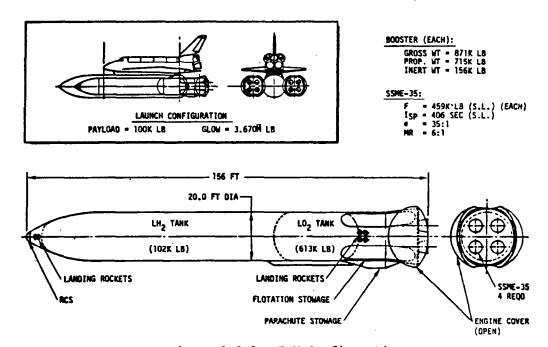


Figure 1.3.3. PLV Configuration

Cost estimates were developed from work produced under the Rockwell Shuttle Growth Study Contract NAS8-32015 of May, 1977. DDT&E, Shuttle Orbiter, external tank, liquid rocket booster, the engine module costs, and projections on operational requirements were identified by comparative evaluation with the Shuttle growth data base. Many different concepts for reducing Shuttle operations costs were examined in the study, but overall cost characteristics clearly reflected the choice of propulsion which lead to the SSME-35 powered LRB as a considered alternative.

Elements of the STS PLV and cargo fleet were individually analyzed on the basis of systems per vehicle, vehicle life, asset rep lacement and operational aspects. A PLV orbiter 30 year replacement factor of 0.5 equivalent vehicles

was used for each orbiter in the fleet. The external tank is an expended item after each flight and the LRBs are to be replaced on the basis of two boosters for each one in the fleet. An attrition/spares factof of 0.5 equivalent vehicles is also used for the cargo/engine module.

DDT&E and system cost estimates are identified in the following tables:

Table No.	<u>Item</u>
1.3.3.1.1	STS-PLV Orbiter
1.3.3.1.2	STS-PLV External Tank
1.3.3.1.3	STS-PLV Liquid Rocket Booster
1.3.3.1.4	STS-Cargo Carrier and Engine Module

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.3.3.1.1 STS-PLV ORBITER TABL E

1.	1.000000	TF=	1.000000	CDC ER=	0.0	
11 2	1.000000	=W30	0.0	CDEXP		
C F=	1.000000	=17	3.000000	CICER		000000
=1Hd	0.920000	=27	000000.09	CI EXP=		1.000000
R= R=	0.014444		78.000000			and the same of th
0F=	1.000000	= + 7	15.000000	= 57	37.000000	
CAL CUL ATED	D VALUES	SET	SUM TO 1.	1.3.3.1		S.MILL IONS
CD=CDCER X (T X	X DF1XX(CDEXP)	Y ČF			:	0.0
CLRM=CICER X (	X (M)XX(CIEXP) X CF	CF X TF				600.000
#RM =T / M						1.000
E = 1.0 + LOC	=1.0 + LOG(PHI) / LOG(2.0)	• 0)				0.880
CTFU=(CLRM / E)X((#RM X 21+.5)XX(E) -0.5XX(E))	E)X((#RM X 21+	5)XX(E) -(	).5XX(E))			1682.531
CTB = ((CLRM/E)X((#RM	×	Z3 + 0.5) XX(	0.5) XX(E) -0.5XX(E))	1 / 23	23	401.360
CIPS=CTB*Z4/Z2		:				100.340
CRCI =CTB	3 X R					5.797
130 = M300	O&M OR CT8*25/22/ENY	/ENYR				8.250
COMMENTS	:					

RUCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.3.3.1.2 STS-PLV EXTERNAL TANK TABL E

	INPUT PARA	ARAMETERS		:	INPUT COEFFICIENTS	FICIENTS
ii H	1.000000	TF=	1.000000		CDC ER =	0.0
# <b>X</b>	1.000000	=W30	0.0		CDEXP=	0.0
CF=	1.000000	<b>-17</b>	261.000000		CI CER=	4.000000
=IHd	0.920000	22=	60.00000		CI EXP=	1.000000
R=	0.0	73=	5235.00000			
0F=	1.000000	= + 7	1541.00000	= 57	3694.00000	
CALCULAT	CALCULATED VALUES	SET	SUM TO 1.	1.3.3.1	er dry, my de la companya de la companya de la companya de la companya de la companya de la companya de la comp	S. MILLIONS
CD=CDCER X (T	CD=CDCER X (T X DF)XX(CDEXP)	) X CF				0.0
CLRM=CICER X	CLRM=CICER X (M)XX(CIEXP) X CF	CF X TF				4.000
B #RM =T / M						1,000
от + 0°1 « ш	=1.0 + LOG(PHI) / LOG(2.0)	• 0)				0.880
CTFU=(CLRM /	CTFU=(CLRM / E)X((#RM X 21+.5)	XX(E)	-0.5XX(E))			606.205
CTB = ((CLRM/E)X((#RM X		23 + 0.5) XX(	0.5) XX(E) -0.5XX(E))		1 / 23	1.623
CIPS=CTB*24/Z2	2					41.679
CRCI =CTB	X X					0.0
130 = M300	O&M OR CT8*25/22/EN	/ENYR				3.330
COMMENTS						

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.3.3.1.3 STS-PLV LIQ. ROCKET BOOSTER TABLE

	INPUT PARAM	ARAMETERS			INPUT	INPUT COEFFICIENTS
<b>=</b> L	1.000000	<b>1</b> F≈	1.000000		CDCER=	1304.00000
ij Ž	1.000000	=W30	0.0		CDEXP=	1.000000
C F=	1.000000	21=	5.000000		CI CER =	195,300003
₽H1=	0.92000	. = 22	60.000000		CI EXP=	1.000000
<u>م</u>	0.00090.0	23=	162.000000			
0 F=	1.000000	= + 7	17.000000	= 57	37.	37.000000
CALCULATED	ATED VALUES	SET	SUM TO	1.3.3.1		S, MILL IONS
CD=CDCER X	(T X DF)XX(CDEXP)	) X CF				1304.000
CLRM=CICER	X (M) XX(CIEXP)	X CF X TF				195.300
HRM =T / M		-				1.000
+ 0•1 " "	=1.0 + LOG(PHI) / LOG(2.0)	2.03				0.880
CTFU=(CLRM /	E)X((#RM X	Z1+.5)XX(E) -0	-0.5XX(E))			873.985
CTB = ((CLRM/E)X((#RM	×	Z3 + 0.5) XX(	0.5)XX(E) -0.5XX(E))		1 / 23	119.967
CIPS=CTB*24/22	/12	:				33,991
CRCI =	=CTB X R					7.198
= W300	O&M OR CTB*25/22/ENY	2/ENYR				2.466
COMMENTS				1		

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.3.3.1.4 STS CARGO CARRIER AND EM TABLE

INPUT PAR	₹		!	INPUT	INPUT COEFFICIENTS
		1.000000		CDCER =	245.000000
00000°T ==	)	0.0	۰	DEXP=	1.000000
	=17	3.000000	C	CI CER=	265.800049
PHI= 0.920000		60.00000	٥	IEXP=	1.000000
	73=	3.00000			
DF= 1.000000	= + 7	3.000000	= 57	0.0	
CALCUL ATED VALUES	44	SUM TO 1.3.3.1	3.1		\$ • MILL IONS
CO=COCER X (T X DF)XX(COEXP)	(P) X CF		:		245,000
CLRM=CICER X (M)XX(CIEXP) X C	X CF X TF				265.800
#RM =T / M					1.000
=1.0 + LOG(PHI) / LOG(2.0	2.01				0880
CTFU=(CLRM / E)X((#RM X Z1	)XX(E)	-0.5XX(E))			745.362
CTB = ((CLRM/E)X((#RM X	Z3 + 0.5) XX(	0.5) XX(E) -0.5XX(E))		1 / 23	248.454
CIPS=CTB*24/22	:		 		12,423
CRCI =CTB X R					0*0
CO&M = O&M OR CTB*Z5/Z2/ENYR	22/ENYR				0•0
COMMENTS					

## 1.3.3.2 PLV OPERATIONS

This element includes the necessary vehicle operations (user charge per flight including payload integration) required to support the SPS program.

A total of 5,235 flights are required of the Shuttle derived personnel and cargo vehicle -- 1,412 for construction, 3,694 for operations, and 129 for the precursor program. The 1,412 PLV flights for construction include 72 for the precursor effort and 60 for the TFU satellite.

Cost estimates per flight were projected after an engineering analysis of the operational costs and vehicle elements identified in the Rockwell Shuttle Growth Study (NAS8-32015). Tables 1.3.3.2.1 and 1.3.3.2.2 cover operational cost estimates.

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.3.3.2.1 PLV OPERATIONS TABLE

I.

ĺ

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.3.3.2.2 STS HLLV CARGO OPERATIONS TABLE

:	INPUT	PARAMETERS		i i !	INPUT CO	INPUT COEFFICIENTS
<u>"</u> .	1.000000	TF=	1.000000		CDCER=	0.0
# <b>E</b>	1.000000	-W30	0.0		CDEXP=	0.0
CF=	1.000000	<b>Z 1 =</b>	129.000000		CICER=	8.750000
=I Hd	1.000000	22=	000000.09		CI EXP=	1.000000
11	0.0	=€7	129,000000			
DF=	1.000000	<b>2</b> 4=	129.000000	= 57	0.0	
CALCULATED	D VALUES	49	SUM TO 1.	1.3.3.2		S, MILLIONS
CD=CDCER X (T X DF)XX(CDEXP)	X DF )XX(CDEXP	X CF			:	0.0
CLRM=CICER X (M)XX(CIEXP)		X CF X TF			·	8 . 7 50
M / 1= M8# B						1.000
907 + 0°1 = 3	=1.0 + LOG(PHI) / LOG(2.0)	• 0)		         		1.000
CTFU=(CLRM / E)X((#RM X 21+.5)	)X((#RM X Z1+	•5)XX(E) -0.5XX(E))	•5XX(E))			1128.750
CTB = ((CLRM/E)X((#RM	×	Z3 + 0.51 XX(	0.5) XX(E) -0.5XX(E)		1 / 23	8.750
CIPS=CTB*Z4/Z2						18.813
CRCI =CTB	α ×					0.0
C08M = 08M	06M OR CTB*Z5/Z2/ENYR	/ ENYR				0.0
COMMENTS	:			:		

# 1.3.4 PERSONNEL ORBITAL TRANSFER VEHICLE (POTV)

This element includes the POTV vehicles and operations required to support the satellite system assembly and operation. Included is the LEO-to-GEO and return of all personnel and priority cargo required throughout the satellite construction and operational periods.

All of the POTV options evaluated utilize a single stage propulsive element that is fueled in LEO and refueled in GEO for the return flight. The reference configuration is illustrated in Figure 1.3.4 where the POTV (a propulsive stage) is capable of transporting a 60-man personnel module (PM) of 18,000 kg. The vehicle is costed in section 1.3.4.1 and POTV operations are covered in section 1.3.4.2.

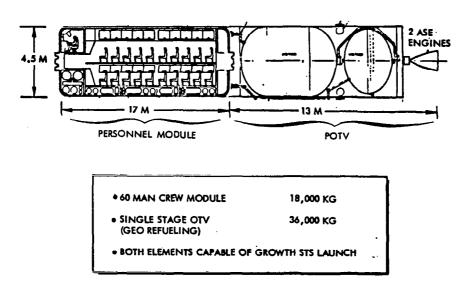


Figure 1.3.4. POTV Configuration

#### 1.3.4.1 POTV FLEET

The vehicle fleet procurement required to support the SPS program is included in this element. The POTV is a single stage OTV of 36,000 kg with refueling at GEO for the return to LEO. Propellants are carried from LEO to GEO by the EOTV. The SPS HLLV carries the construction, crew expendables, and POTV propellants to LEO. The Shuttle Orbiter carries the crew in a personnel module (PM) to LEO for transfer to the POTV.

The single stage OTV configuration selected is a scaled version of those concepts presented in the BAC FSTSA NAS9-24323 contract and engineering analyses presented in Exhibits A/B of the Rockwell contract NAS8-32475. DDT&E estimates considered fewer engines, a significant difference in mass, and the degree of development required for the engines. Engineering analyses of available vehicle estimates projected a POTV cost based on the design and complexity of the vehicle.

POTV cost estimates are presented in Table 1.3.4.1 for a total fleet of 196 vehicles with: 1) 12 for personnel involved in satellite construction, 2) 37 for SPS operational activities, and 3) an attrition factor of 3 equivalent vehicles to keep the fleet fully operational.

# ROCKWELL SPS CR-2 REFERENCE CONFIGURATION

TABLE 1.3.4.1 POTV-FLEET

		INPUT P	ARAMETERS			INPUT	COEFFICIENTS
	T=	1.000000	TF=	1.000000		CDCER=	350.000000
	M=	1.000000	=M3O	0.0		CDEXP=	1.00000
	C F=	1.000000	Z 1 =	4.000000		CICER=	15.000000
	PH I≃	0.920000	Z 2 =	60.000000		CIEXP=	1.00000
	R=	0.081667	Z3=	196.000000			
	DF=	1.000000	Z 4=	12.000000	25 =	37.	000000
	CALCULATE	D VALUES	SET	SUM TO	1.3.4	***	\$, MILLIONS
CD:	CDCER X (T	X DF1XX(CDEXP	) X CF			And the second second second second	350.000
CLI	RM=CICER X (	M)XX(CIEXP) X	CF X TF				15.000
#R	M = T / M	· · · · · · · · · · · · · · · · · · ·					1.000
#RI	=1.0 + LOG	(PHI) / LOG(2	.0)	· _ · · · · · · · · · · · · · · · · · ·			0.880
CT	FU=(CLRM / E	)X((#RM X Z1+	.5)XX(E) -0	.5XX(E))		·	54.764
CT	B = ((CLRM/E)	X((#RM X Z	3 + 0.5)XX(	E) -0.5XX(E))		) / Z3	9.010
CI	PS=CTB*Z4/Z2						1.802
	CRCI =CTB	X R			· · · · · · · · · · · · · · · · · · ·		0.736

#### 1.3.4.2 POTV OPERATIONS

This element includes the necessary vehicle operations (user charge per flight including payload integration) required to support the SPS program with required personnel.

The primary operational cost of the POTV is the cost of fuel. A total of 4,880 flights were costed on this basis where 1,220 flights were for satellite construction; 3,660 for operations and maintenance; and 45 of the 1,220 needed to support TFU activities. Table 1.3.4.2 presents the results of this analysis.

# ROCKWELL SPS CR-2 REFERENCE CONFIGURATION TABLE 1.3.4.2 POTV-OPERATIONS

		INPUT P	ÄRAMETERS			INPUT COEF	FICIENTS
	T=	1.000000	TF=	1.000000	CD	CER=	0.0
<del></del>	M=	1.000000	=M30	0.0	CD	EXP=	0.0
	CF=	1.000000	Z 1 =	45.000000	CI	CER=	0.033742
P	PHI=	1.000000	2 2=	60.000000	CI	EXP=	1.000000
	R=	0.0	73=	4880.00000			
	DF=	1.000000	Z 4=	1220.00000	<b>25 =</b>	3660.00000	
	CALCULATED	VALUES	\$	SUM TO 1.	.3.4		\$, MILLIONS
CD=C	DCER X (T X	DF ) X X ( CDEXP	X CF				0.0
CLRM	M=CICER X (M.	XX(CIEXP) X	CF X TF				0.034
#R·M	=T / M					<u> </u>	1.000
E	=1.0 + LOG(	PHI) / LOG(2	_0)				1.000
CTFU	J=(CLRM / E)	K((#RM X Z1+	.5)XX(E) -	0.5XX(E))			1.518
СТВ	=((CLRM/E)X	[(#RM X Z	3 + 0.5)XX	((E) -0.5XX(E))	}	/ Z3	0.034
CIPS	S=CTB*Z4/Z2	· · · · · · · · · · · · · · · · · · ·					0.686
	CRCI = CTB	X R	·				0.0
				·			,

# 1.3.5 PERSONNEL MODULE (PM)

This element includes the PM units and operations required to support the satellite system assembly and operation. Included in the earth-to-LEO-to-GEO and return transfer of all personnel and critical hardware items required throughout the satellite construction and operational periods. The PM provides a crew habitat during the orbit-to-orbit transfers of personnel as well as during the trip from earth. An illustration of the PM was shown in Figure 1.3.4. It has a 60-man capacity and is approximately 17 m long by 4.5 m in diameter. The Shuttle is used for the earth-to-LEO transfer and the POTV handles the round trip movement from LEO-GEO-LEO.

## 1.3.5.1 PM FLEET

Procurement of the PM as required to support the SPS program is covered in this element. The PM is operated by a pilot and co-pilot and contains the major systems of life support, communication, seating, and support facilities. A total of 4 PMs are needed to support the program and 2 equivalent PMs are considered sufficient to provide spares and major overhaul components during the program. Four vehicles will be required to build the satellite TFU and early program supporting elements such as the LEO Base and SCB.

Engineering cost projections were based on Rockwell company-funded studies of 1976 where DDT&E, a pair of 68 passenger modules, and the orbiter modification kits were costed from internal design specifications. PM fleet procurement costs are presented in Table 1.3.5.1.

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.3.5.1 PM FLEET TABLE

	INPUT PARAM	ARAMETERS			INPUT	INPUT COEFFICIENTS
# #	1.000000	TF=	1.000000		CDCER=	118.000000
Ľ	1.000000	0 £M=	0.0		CDEXP=	1.000000
CF=	1.000000		4.000000		CI CER=	54,399994
⇒I Hd	0.920000	<b>22=</b>	60.00000		CI EXP=	1.000000
R	0.004444	73=	12.000300			
DF=	1.000000		1.000000	= 57	3.0	3.000000
CALCULATED	ED VALUES	SET	SUM TO 1.3.5	5		S, MILL IONS
CD=CDCER_X (T	CD=CDCER X (T X DF)XX(CDEXP) X	) X CF		!		118.000
CLRM=CICER X	X (M)XX(CIEXP) X	CF X TF				54.400
#RM =T / M						1,000
07 + 0·1 = u = -234	=1.0 + LOG(PHI) / LOG(2.0)	.0)				0.880
CTFU=(CLRM / E)X((#RM X		Z1+.5) XX(E) -0.	-0.5XX(E))			198.610
CTB = ((CLRM/E)X((#RM	×	Z3 + 0.5) XX(E	0.5)XX(E) -0.5XX(E))		1 / 23	44.737
CIPS=CTB*Z4/Z2				 		0.746
CRCI = CTB	B X R					0.199
130 = M300	OEM OR CT8*25/22/ENY	/ENYR				0.075
COMMENTS				:		

## 1.3.5.2 PM OPERATIONS

This element includes the necessary operations (user charge per flight including payload integration) required to support the SPS program.

A PM crew (pilot and co-pilot) will command the module during earth-to-LEO trips on the Shuttle and complete the procedures of leaving the Shuttle and making the POTV hook-up for transfer to GEO. The crew will monitor passenger off-loading/transfer to and from the LEO Base, SCB, or satellite O&M Base. Two man-days are calculated per trip which includes a rest period at GEO and a day off after the trip. An average of 4,993 round trip flights are projected from earth to GEO and back. A total of 132 flights are needed for the precursor and TFU programs. The engineering estimates of PM operations are presented in Figure 1.3.5.2.

ROCKWELL SPS CR-2 REFERENCE CUNFIGURATION 1.3.5.2 PM OPERATIONS TABL E

	INPUT PARAN	ARAMETEPS		· ·	INPUT COEFFICIENTS	FICTENTS
ii.	1.000000	TF=	1.000000		CDCER=	0.0
# <b>\S</b>	1.000000	=W30	0.0		CDEXP=	0.0
C F≡	1.000000	=17	132.000000		CICER=	0.025000
₽HI≂	1.000000	2.2=	00000000		CIEXP=	1.000000
= <del>~</del>	0.0		4993.00000			
0F=	1.000000	= + 7	1316.00000	= 57	3677.00000	
CALCULATED VALUES	D VALUES	FLIGHT	SUM TO 1.	1.3.5		S.MILL IONS
CD=CDCER X (T	(T X DF)XX(CDEXP)	X CF				0.0
CLRM=CICER X [	(M)XX(CIEXP) X	CF X TF				0.025
#RM =T / M						1.000
E =1.0 + LOG	=1.0 + LOG(PHI) / LOG(2.0)	• 0)				1.000
CTFU=(CLRM / E	E)X((#RM X 21+.5)	XX(E)	-0.5XX(E))			3.300
CTB = ((CLRM/E)X((#RM	×	XX (5.0 + EZ	0.5) XX(E) -0.5X X(E))		1 / 23	0.025
CIPS=CTB*Z4/Z2						0.548
CRCI =CTB	××					0*0
~30 ≈ M303	06M OR CT8*25/22/EN	/ENYR				0.051
COMMENTS						

1

# 1.3.6 INTRA-ORBITAL TRANSFER VEHICLE (IOTV)

This element includes the IOTV vehicles and operations required to support the satellite system assembly and operation. Included is the intra-orbit transfer of cargo between the HLLV, EOTV, construction facility, logistics support facility, and operational satellites.

#### 1.3.6.1 IOTV FLEET

This element includes the necessary vehicle fleet procurement required to support the SPS program. The IOTV has been synthesized in terms of application and concept only. IOTV elements considered here are powered by a chemical (LOX/LH2) propulsion system. At least three distinct applications have been identified; (1) the need to transfer cargo from the HLLV to the EOTV in LEO and from the EOTV to the SPS construction base in GEO; (2) the need to move materials about the SPS construction base; and (3) the probable need to move men or materials between operational SPSs. Clearly the POTV, used for transfer of personnel from LEO to GEO and return, is too large to satisfy all intra-orbit requirements. A "free-flyer" teleoperator concept would appear to be a logical solution to the problem. A propulsive element was synthesized to satisfy the cargo transfer application from HLLV-EOTV-SPS base in order to quantify potential on-orbit propellant requirements. Pertinent IOTV parameters are summarized in Table 1.3.6.

SUBSYSTEM	WEIGHT (kg)
ENGINE (1 ASE)	245
PROPELLANT TANKS	15
STRUCTURE AND LINES	15
DOCKING RING	100
ATTITUDE CONTROL	50
OTHER	100
SUBTOTAL	525
GROWTH (10%)	53
TOTAL INERT	578
PROPELLANT	300
TOTAL LOADED	878

Table 1.3.6. IOTV Design Parameters

A total of 840 IOTVs are needed to maintain intra-orbit cargo/operations flow during the program. One hundred ten vehicles will accomplish the construction phase and 100 vehicles are needed for satellite O&M. An attrition/spares fleet of equivalent vehicles was projected on the ratio of 3 units for each of the operational vehicles.

Cost estimates for the IOTV are engineering assessments based on POTV designs and similarities such as those of the common advanced space engine (ASE). Table 1.3.6.1 displays the applicable cost data.

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.3.6.1 TABL E

:		INPUT PAR	ARÄMETERS			INPUT	INPUT COEFFICIENTS
	ï	1.000000	<b>∓</b> F=	1.000000		CDCER=	100 000000
	¥	1.000000	=W30	0.0		CDEXP=	1.000000
	C F=	1.000000	2.1.=	4.000000		CICER=	1.500000
	=IHd	0.920000	22=	60.00000		CIEXP=	1.000000
İ	<b>8</b>	0.350000		840.000000			
	0 F=	1.000000	= + 7	110.000000	= 57	100.000000	0000
İ	CALCULATED VALUES	D VALUES	SET	SUM TO 1.	.3.6		S* MILL IONS
į	CD=CDCER X (T X DF)XX(CDEXP)	X DF)XX(CDEXP	) X CF		1		100.000
	CLRM=CICER X (	(M)XX(CIEXP) X	CF X TF				1.500
В-	#RM = 1 / M						1.000
239	E =1.0 + L06	=1.0 + LOG(PHI) / LOG(2.0	(0.				0.880
	CTFU=(CLRM / E)X((#RM X	)X((#RM X 21+.5	XX(E)	-0.5XX(E))			5.476
	CTB = ((CLRM/E)X((#RM	×	Z3 + 0.5) XX(E)	(E) -0.5XX(E))		1 / 23	0.758
1	CIPS=CTB*Z4/Z2						1.389
	CRCI =CTB	×					0.265
	N30 = M300	06M OR CT8*25/22/E	/ENYR				0.042
į	COMMENTS						

1 1111 11 111 1

Satellite Systems Division
Space Systems Group
Rockwell
International

# 1.3.6.2 IOTV OPERATIONS

+ +

This element includes the necessary vehicle operations and propellant costs required to support the SPS program. It includes the on-orbit operational cost of transferring cargo at LEO and GEO.

A total of 41,940 IOTV flights are planned for LEO and GEO construction and operations/maintenance requirements of the program. The 22,811 flights needed for construction and the 19,979 for operations and maintenance are considered as equal missions for the purpose of costing. The propellant requirements were averaged and calculated at 1977 dollars of 0.07/kg for LO<sub>2</sub> and 3.27/kg for LH<sub>2</sub>. A 40% mark-up was added per flight for other operational and maintenance charges. See Table 1.3.6.2.

# ROCKWELL SPS CR-2 REFERENCE CONFIGURATION TABLE 1.3.6.2 IOTV OPERATIONS

	INPUT	PARAMETERS			INPUT COEF	FICIENTS
<b>T</b> =	1.000000	TF=	1.000000		CDCER=	0.0
M=	1.000000	=M30	0.0		CDEXP=	0.0
CF=	1.000000	<b>Z1</b> =	408.000000		CICER=	0.000222
PH <b>I</b> =	1.000000	Z 2=	60.00000		CIEXP=	1.00000
R=	0.0	73=	41940.0000			
DF=	1.000000	Z 4=	21961.0000	<b>Z5</b> =	19979.0000	
CALC	ULATED VALUES	FLIGHT	SUM TO	1.3.6		\$, MILL ION
CD=CDCER	X (T X DF)XX(CDEX	P) X CF	·····			0.0
CLRM=CICE	R X (M)XX(CTEXP)	X CF X TF				0.000
#RM =T /	М			·····		1.000
E = 1.0	+ LOG(PHI) / LOG(	2.0)				1.000
CT FU= ( CLR	M / E)X((#RM X Z1	+.5)XX(E)	-0.5XX(E))			0.091
CTB = ((CL	RM/E)X((#RM X	Z3 + 0.5)X	X(E) -0.5XX(E))		1 / 23	0.000
CIPS=CTB*	24/22	- ·				0.081
CRCI	=CTB X R					0.0

#### 1.3.7 GROUND SUPPORT FACILITIES

This element includes all land, buildings, roads, shops, etc., required to support the cargo handling, launching, recovering, refurbishment, and operations of the space transportation system.

#### 1.3.7.1 LAUNCH FACILITIES

This element includes the design and construction of the actual launch facility and its associated equipment. Included are land, buildings, and equipment required to support the various crews. It also includes the required control centers and administrative facilities.

#### 1.3.7.2 RECOVERY FACILITIES

This element covers the design, construction, and equipping of the actual recovery facilities.

#### 1.3.7.3 FUEL FACILITIES

This element includes fuel production facilities, storage and handling facilities, transportation, and delivery and safety facilities for both the fuel and the oxidizer. Also included are the facilities for fuels used in the various orbital transfer facilities)

#### 1.3.7.4 LOGISTICS SUPPORT

This element includes the land, buildings, and handling equipment for the receiving, inspection, and storage and packaging of all payloads to be launched except for fuels and oxidizers.

#### 1.3.7.5 OPERATIONS

This element includes the planning, development, and conduct of operations at the ground support facilities. It includes both the direct and support personnel and the expendable maintenance supplies required for the ground support facilities operation and maintenance.

A cost estimate for ground support facilities is projected in Table 1.3.7 based on the Boeing final report, NAS9-14710, dated September 1977, Volume 4, Cost Estimates. It is judged that there is little difference in the cost of facilities in this report as compared with those projected for the transportation and operations requirements of this study.

ROCKWELL SPS CK-2 REFERENCE CONFIGURATION TABLE 1.3.7 GROUND SUPPURT FACILITIES

1.030000   1F=		INPUT PAK	PAK AMET EKS		ZI	INPUT CO	COEFFICIENTS
1.000000	=1	1.000000		1.4660000	CDCER=		1720.0000
1.650000	<b>8</b>	1.000000		1.775600	CDEXP=		0.0
1.000000	CF:	1.600000		1.000000	CI CER=		3195,00000
0.001111	PHI	1.000000		-	CIEXP=		0.0
1.000000 24= 1.00000 25= 0.0  D VALUES  X DF)XX(CUEXP) X CF  M)XX(CIEXP) X CF X TF  M)XX(CIEXP) X CF X TF  (PH1) / LUG(2.0)  X((#RM X 21+.5)XX(E) -0.5XX(E))  X((#RM X 23 + 0.5)XX(E) -0.5XX(E))  X R  X R  UR CTB*L5/22/ENYK	<b>X</b>	0.051111		1.00000			
D VALUES  X DF)XX(CDEXP) X CF  M)XX(CIEXP) X CF X TF  M)XX(CIEXP) X CF X TF  (PH1) / LGG(2.0)  X((#RM X 21+.5)XX(E) -0.5XX(E))  X((#RM X 23 + C.5)XX(E) -0.5XX(E))  X R  X R  UR CTB*L5/Z2/ENYK	0 F=	1.000000		1.000000	=<7	0.0	
X DF!XX(CLEXP) X CF X TF M)XX(CLEXP) X CF X TF (PH1) / LUG(2.0)  X((#KM X 21+.5)XX(E) -0.5XX(E))  X((#KM X 23 + C.5)XX(E) -0.5XX(E))  X R  X R  UR CTB*25/22/ENYK	CALCULAT	ED VALUES		-			\$,MILLIONS
M)XX(CIEXP) X CF X TF  (PH1) / LGG(2.0)  X((#KM X 21+.5)XX(E) -0.5XX(E))  X((#KM X 23 + 6.5)XX(E) -0.5XX(E))  X R  X R  UR CTB*L5/22/ENYK	CD=CDCER_X_(T	X DF) XX (CLEX			The state of the s		1720.000
(PH1) / LGG(2.0) )X((#KM X 21+.5)XX(E) -0.5XX(E)) X((#KM X 23 + 6.5)XX(E) -0.5XX(E)) X R X R UR CTD*25/22/ENYK	CLRM=CICER X	(M)XX(CIEXP)	CF				3195.000
(PHI) / LOG(12.0) )X((#KM X 21+.5)XX(E) -0.5XX(E)) X((#KM X 23 + C.5)XX(E) -0.5XX(E)) X R X R UR CTB*L5/22/ENYK							1.000
)X((#KM X 21+.5)XX(E) -0.5XX(E)) X((#KM X 23 + 6.5)XX(E) -0.5XX(E)) X R  UR CTB*25/22/ENYK		16(PH1) / LOG(	2.0)				₹ 000
X((#KM X	CTFU= (CLRM /	E)X((#KM X 21	) XX(E)	•5xx(E))			3195.000
X R UR CTB*25/22/E	CIB = (ICLRM/E	)X((#KM X	+	E) -0.5XX(E))	1 / 23	_	3195.000
=CT8 X R = UEM UR CT3*25/E	C 1P S= C1 B * Z 4 / Z						53.250
- UEM UR CTB*25/22/E	C RC I =CT	×					3.550
T. T. M. M. M. M. M. M. M. M. M. M. M. M. M.	30 ± M303	.M UR CTB*25/2	2/ENYR				1.775
	CUMMENTS						

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#### 1.4 GROUND RECEIVING STATION

The ground receiving station (GRS) is designed to accept power from a single satellite and to provide a nominal 5 GW of power to the utility interface. As shown in Figure 1.4-1, a typical receiving station would be located at 34° N latitude with rectenna panels covering an elliptical area of 13 km in the north-south direction and 10 km in the east-west direction. This area is surrounded by another elliptical segment to house the power conversion equipment and to provide for the operational facilities of the receiving station. A summary of point design characteristics are presented in Table 1.4-1.

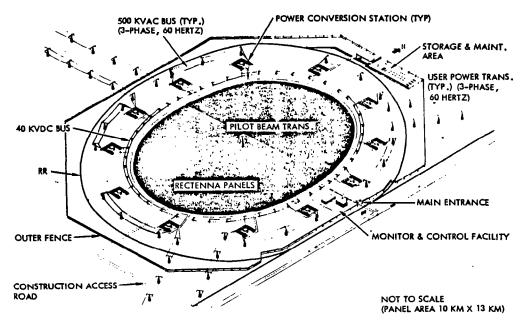


Figure 1.4-1. Operational Ground Receiving Facility (Rectenna) - Typical

Table 1.4-1. System Point Design Characteristics

SIZE (lon)	10×13
TOTAL GROUND AREA (km) <sup>2</sup>	102.1
TOTAL PANEL AREA (km)2	79.53
AREA PER PANEL (9.33×14.69 m)	137.0
NUMBER OF PANELS	580,500
NUMBER OF DIODES	330×10 <sup>6</sup>
RECTENNA EFFICIENCY (%)	89
VOLTAGE OUTPUT PER STRING (kV dc)	40+
VOLTAGE OUTPUT TO UTILITY (kV ac)	500
POWER OUTPUT (GW) AT UTILITY INTER-TI	E 4.61*

This ground based element of the SPS is comprised of the land, facilities, equipment, and hardware/software systems to receive the radiated microwave power beam and to provide the power at the required voltage and type of current for entry into the national power grid. It also includes the equipment, facilities, and hardware/software necessary to provide operational control over the satellite; and a reliable means of monitoring and controlling ground based systems and equipment.

Major objectives of the SPS ground system design are: (1) to provide low maintenance subsystems and equipment capable of handling the designed power levels; (2) to assure that the overall station will provide dependable service for at least 30 years; (3) to minimize the size of operational crews and costs; and (4) to economically optimize system performance.

There are nine major activities involved in the overall GRS construction process. After the survey and clearing, utilities and supporting facilities are installed while the site is leveled and graded. Trenching and concrete pouring precede the installation of rectenna panels, after which electrical hook-up, converter stations, and monitoring facilities are installed. 40 kV dc and 500 kV ac buses are then interconnected and procedures take place for system checkout. Cost effective utilization of equipment and personnel was identified after the development and integration of detail phasing schedules on each of the first four ground stations. Contacts with A&E, equipment manufacturers, concrete, and construction firms provided additional information on the duration and sequence of operations based on their experience with programs of this type. Figure 1.4-2 is an integrated summary schedule of major events in constructing the ground receiving station where emphasis is placed on the utilization of construction equipments and their transfer from site to site as required to maintain the build rate of two stations per year. It was concluded that the equipment from Site 1 would be available for use on Site 3. This information on equipment/manpower utilization, site sequencing, and equipment lifetimes is used in this analysis to establish total resource requirements for the program.

The ground receiving station was divided into several main elements for the purpose of associating cost and programmatic definitions. These elements include (1) site and facilities, (2) rectenna support structure, (3) power collection, (4) control, (5) grid interface, and (6) operations. SPS design definitions and specification requirements were analyzed to provide realistic cost estimates and resource definitions for each element as explained in the following sections.

Internal resources, cost estimating relationships, and prior cost analyses were supplemented by: 1) direct contact with business, industry, and institutional organizations, and 2) a literature search of various publications to obtain realistic cost estimates and operational definitions directly applicable to the unique requirements of the GRS. A list of principal organizations and literature sources are presented in Table 1.4-2.

A summary of the costs associated with the GRS is presented in Table 1.4-3. The detail supporting these costs is presented in the subsequent pages of this section.

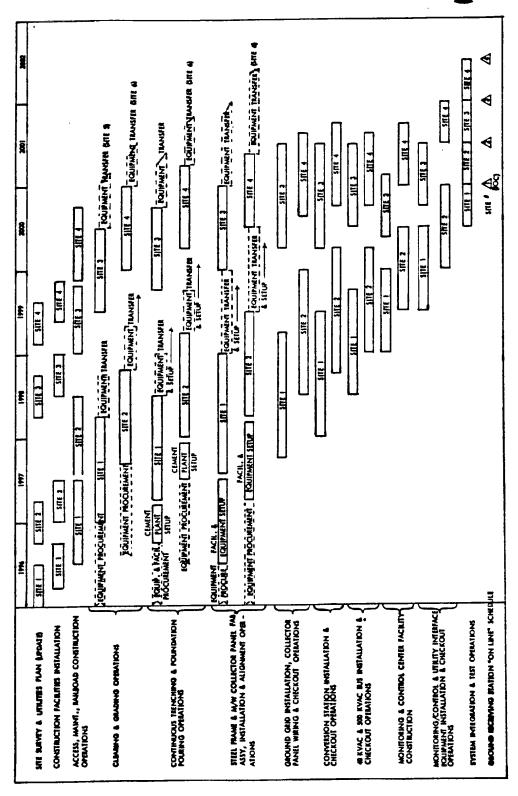


Figure 1.4-2. Rectenna Construction Sequence Summary Schedule

Table 1.4-2. Organizations and Literature Sources
Supporting GRS Definition

ORGANIZATION	PURPOSE
AMERICAN BRIDGE - A DIVISION OF U.S. STEEL	TO DEVELOP STEEL REQUIREMENTS, COSTS AND OPERATIONS DEFINITION FOR PRO- CUREMENT AND INSTALLATION OF RECTENNA SUPPORT STRUCTURE
RIVERSIDE CEMENT A DIVISION OF AMERICAN CEMENT CORPORATION;     AND C. S. JOHNSON, CO.	PROVIDE CONSULTATION ON CEMENT/CONCRETE SPECIFICATIONS, OPERATIONAL METHODS, PROCESSING/HANDLING EQUIPMENT, AND CONCRETE PLANT
• TOWNSEND & BOTTUM, INC., CONSTRUCTION MANAGER, TEN MW SOLAR PLANT - BARSTOW, CA.	DISCUSS SITE PREPARATION, CONSTRUCTION OPERATIONS/SEQUENCING, PLUS ACTIVATION REQUIREMENTS
SOUTHERN CALIFORNIA EDISON	TO DISCUSS DC/AC POWER DISTRIBUTION AND CONVERSION REQUIREMENTS, AND OBTAIN COST ESTIMATES ON INSTALLATION OF LINES/TOWERS
• MODERN ALLOYS, INC.; AND MILLER FORMLESS CO.	TO DISCUSS USE AND APPLICATION OF EQUIPMENT/CREW FOR CONTINUOUS CONCRETE POUR OF RECTENNA SUPPORT STRUCTURE FOOTINGS
CATERPILLAR; INTERNATIONAL     HARVESTER; AND JETCO, INC.	OBTAIN PRICES ON EARTH MOVING, GRADING AND TRENCHING EQUIPMENT
LITERATURE SOURCES	
• THE RICHARDSON RAPID SYSTEM 1978-1979 EDITION	CONSTRUCTION LABOR AND OPERATIONS PRICES
ENGINEERING NEWS RECORD - 1977     A WEEKLY McGRAW-HILL     PUBLICATION	CEMENT, AGGREGATE AND LABOR PRICES
NATIONAL CONSTRUCTION ESTIMATING GUIDE (NCE)	CONSTRUCTION OPERATIONS

Table 1.4-3. GRS Cost Summary (\$ Millions)

WBS NO.		DDT&E	TFU	101	RC1/ 06M
1.4.1	SITE AND FACILITIES	1.0	195.2	188.9	.2
1.4.2	RECTENNA SUPPORT STRUCTURE	2.0	1849.6	1828.	5
1.4.3	POWER COLLECTION	3.0	1353.2	1353.2	-
1.4.4	CONTROL	10.0	75.0	75.0	-
1.4.5	GRID INTERFACE	99.7	145.7	145.7	-
1.4.6	OPERATIONS	÷	-	-	77.9

#### 1.4.1 SITE AND FACILITIES

The ground receiving station is located on a site of 35,000 acres where over 25,000 acres of a central ellipse, or 72% of the total acreage, is used for rectenna panels. The area surrounding the inner ellipse is allocated for maintenance/control facilities, access roads, converter stations, and the rows of towers that support the 40 kW dc and 500 kV ac cables. The GRS perimeter is fenced for security reasons.

The sequence of construction operations begins with site identification, environmental impact studies, zoning/permits, surveys, utility/road installation, and supporting facilities. After reference coordinates are established, the site is cleared, leveled, and followed with precise grading for panel foundations, fabrication facilities, installation and GRS site completion. This includes concrete mixing plants, rectenna panel fabrication factories, crew accommodations, warehousing, and support facilities as shown in Figure 1.4-3. The GRS DDT&E effort will be a valuable asset to all GRS sites by providing designs, analyses, and procurement specifications for commonly used buildings and facilities.

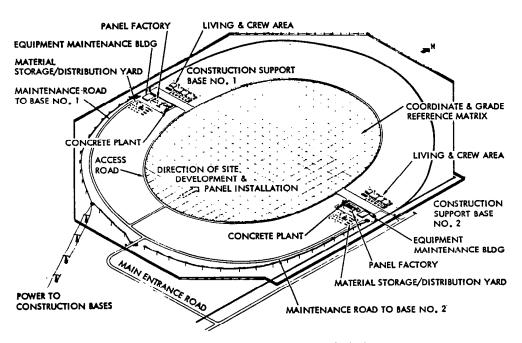


Figure 1.4-3. Support Facilities

Clearing and leveling operations will occur at a number of locations within the panel farm perimeter. These operations consist of tree removal (if required), grading, and leveling the terrain to acceptable slope angles, and removing excess dirt. Sixteen areas of the ellipse would be cleared and leveled simultaneously. Bulldozers will make the initial cut, scrapers will grade to more precise requirements, and an estimate was made of one crew of 13 men

to grade eight acres per day. The crew and equipment required to prepare a 35,000 acre site was established based on a single shift that would level 130 acres per day to meet a nine month schedule.

Costs developed for the site and facilities are divided into the elements of land, site preparation, roads and fence, utilities, buildings and facilities, maintenance equipment, lightning protection, and DDT&E. Basic design parameters used in this costing are presented in Table 1.4-4. The DDT&E, investment, and operations cost established for each element are tabulated as follows:

Table 1.4-4. Site and Facilities Requirements

ITEM	UNIT PARAMETER
LAND/FENCING	35,000 ACRES
GRADING/LEVELING	HEAVY EQUIPMENT/CREW SIZE
PREPARATION	SURVEY, EIR, PERMITS, ASE PLANNING
UTILITIES	WATER, ELECTRICITY, GAS, SEWAGE
ROADS/RAILS	ROADS 35 MILES; RAILS 45 MILES
FACILITIES	CONVERSION STATION, MONITOR & CONTROL, MAINTENANCE/STORAGE
DRA I NAGE	6" GRAVEL FOR COMBINATION ACCESS- WAY & DRAINAGE BETWEEN PANEL ROWS
LIGHTNING PROTECTION	TBD

Table	1.4.1.1	Land and Preparation (Land - 1.4.1.1.1, Preparation - 1.4.1.1.2)
Table	1.4.1.2	Roads and Rences (Rails & Roads - 1.4.1.2.1, Fencing - 1.4.1.2.2)
Table	1.4.1.3	Utilities
Table	1.4.1.4	Buildings and Facilities (Storage/Maintenance - 1.4.1.4.1, Converter Station - 1.4.1.4.2)
Table	1.4.1.5	Maintenance Equipment
Table	1.4.1.6	Lightning Protection System
Table	1.4.1.7	Site & Facilities DDT&E

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.4.1.1.1 LAND TABLE

INPUT PAR	PARAMETERS			INPUT CO	INPUT COEFFICIENTS
T= 35000,0000	<b>TF</b> =	1.000000		CDC ER =	0.0
M= 35000,0000	=W30	0.0		CDEXP=	0.0
CF= 1.000000		1.000000		CI CER=	0.001000
PHI= 1.000000	7.2=	00000000	!	CI EXP=	1.000000
		60.00000			
DF= 1.000000	= + 7	00000009	= 57	0.0	
CALCULATED VALUES	ACRES	SUM TO 1.4	1.4.1.1		\$ MILLIONS
CD=CDCER X (T X DF)XX(CDEXP)	(P) X CF		i	: : : :	0.0
CLRM=CICER X (M)XX(CIEXP)	X CF X TF				35.000
#RM =T / M					1,000
E =1.0 + LOG(PHI) / LOG(2.0	2.0)		:		1.000
CTFU=[CLRM / E]X((#RM X Z]	Z1+.51XX(E) -0	-0.5XX(E))			35.000
CTB = ((CLRM/E)X((#RM X	Z3 + 0.5) XX(	0.5)XX(E) -0.5XX(E))		1 / 23	35.000
CIPS=CTB*24/22			:	:	35.000
CRCI =CTB X R					0.0
COEM = OEM OR CTB*Z5/Z2/ENYR	22/ENYR				0.0
COMMENTS			•		

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.4.1.1.2 LAND PREPARATION TABL E

	INPUT PARA	ARAMETERS		:	INPU	INPUT COEFFICIENTS
H	35000.0000	<b>∓</b> F=	1.000000		CDCER=	0.0
1	35000.0000	=W30	0.0		CDEXP=	0.0
C F=	1.000000	2.1=	1.000000		CI C ER =	0.002007
=IHd	0.086.0	22=	60.000000		CI EXP=	1.000000
= &	0.0	23=	60.00000			44
DF=	1.000000	= + 7	00000000	= 57	0	0.0
CALCULA	CALCULATED VALUES	ACRES	SUM TO 1.	1.4.1.1		S, MILL IONS
CD=CDCER X (	(T X DF)XX(CDEXP	XCF			:	0.0
CLRM=CICER X	(M)XX(CIEXP) X	CF X TF	٠			70.245
# #RM = 1 / M						1.000
+ 0•1 ш 252	=1.0 + LOG(PHI) / LOG(2.0)	• 0)				0.971
CTFU= (CLRM /	E)X((#RM X 21+.5)	XX(E)	-0.5XX(E)			70.341
CTB = ((CLRM/E)X((#RM	×	Z3 + 0.51XX(E)	E) -0.5XX(E))		1 / 23	64.119
CIPS=CT8*24/22	7.2			; ;		64.119
CRCI =CTB	TB X R					0.0
0 = W3D3	06M OR CTB*Z5/Z2/ENYR	/ENYR				0.0
COMMENTS						

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.4.1.2.1 RAILS AND ROADS TABLE

	INPUT PAR	ARAMETERS			INPUT	INPUT COEFFICIENTS
<u>-</u>	1.000000	<b>T</b> F=	1.000000		CDCER=	0.0
H <b>X</b>	1.000000	-M30	0.0		COEXP=	0.0
CF=	1.000000	7.1=	1.000000		CI CER=	73.710007
=IHd	1.000000	22=	000000.09		CI EXP=	1.000000
# <b>&amp;</b>	0.0	23=	000000009			
0F=	1.000000	= 4 2	000000009	= 57	0.0	
CALCULATED	VALUES	SET	SUM TO 1	1.4.1.2		S, MILL IONS
CD=CDCER X (T X DF)XX(CDEXP)	DF)XX(CDEXP	XCF		1 1		0.0
CLRM=CICER X (M)XX(CIEXP)	)XX(CIEXP) X	CF X TF				73.710
B #RM = 1 / M						1.000
)907 + 0°1 = 3°253	=1.0 + LOG(PHI) / LOG(2.0	.0)				1.000
CTFU=(CLRM / E)X((#RM X	X((#RM X Z1+.5	) XX(E)	-0.5XX(E)			73.710
CTB = ((CLRM/E)X((#RM	CC#RM X Z3	1	+ 0.5) XX(E) -0.5XX(E))		1 / 23	73.710
CIPS=CTB*24/22		:				73.710
CRCI = CTB	×					0*0
M30 = M30)	08M OR CT8*25/22/E	/ENYR				0.0
COMMENTS				:		

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.4.1.2.2 FENCING TABLE

	INPUT P	PARAMETERS			INPUT CO	COEFFICIENTS
<u>"</u>	42671.0000	TF≕	1.000000		CDC ER=	0.0
ij.	42671.0000	0£M=	0.0		CDEXP=	0.0
C.F=	1.000000	21=	1.000000		CI CER=	0.000011
=1 Hd	0.980000	22=	000000.09		CI EXP=	1.000000
<b>&amp;</b>	0.0	23=	000000.09			
0F=	1.000000	= + 7	000000*09	= 57	0.0	
CALCUI	CALCULATED VALUES	I	SUM TO 1.4	1.4.1.2		S.MILLIONS
CD=COCER X	CD=COCER X (T X DF)XX(CDEXP)	X CF				0.0
CLRM=CICER	CLRM=CICER X (M)XX(CIEXP) X	X CF X TF				0.469
M / 1= M H# B-						1.000
:	E = 1.0 + LOG(PHI) / LOG(2.0)	•0)		1		0.971
CTFU=(CLRM	CTFU=(CLRM / E)X((#RM X Z1+.5)XX(E)		-0.5XX(E))			0.470
CTB = ((CLRM/E)X((#RM	×	Z3 + 0.5) XX(E)	:) -0.5xx(E)		1 / 23	0.428
CIPS=CTB*24/22	4/12					0.428
CRCI	=CTB X R					0.0
CO&M =	0£M OR CT8*25/22/ENYR	/ ENYR				0.0
COMMENTS		:				

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.4.1.3 UTILITIES TABLE

INPUT PARAMETERS INPUT COEFFICIENTS	TF= 06M= Z1= Z2=	3= 60.000000 25= 0.0	ED VALUES SET SUM TO 1.4.1 \$, MILLIONS	(T X DF)XX(CDEXP) X CF	(M)XX(CIEXP) X CF X TF 0.200	1.000	G(PHI) / LOG(2.0)	E)X((#RM X 21+.5)XX(E) -0.5XX(E)	)X((#RM X Z3 + 0.5)XX(E) -0.5XX(E))		0.200	w ×
UANI		R= 0.0 DF= 1.00000	CALCULATED VALUES	CD=CDCER X (T X DF)XX(CD	CLRM=CICER X (M)XX(CIEXP) X	B #RM = T / M	E = 1.0 + LOG(PHI) / LOG(2.0	CTFU=(CLRM / E)X((#RM X 21+.5	CTB = ((CLRM/E)X((#RM X	CIPS=CT8*24/72		×

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.4.1.4.1 STORAGE, MAINTENANCE TABLE

INPUT PARAM				INPUT CO	INPUT COEFFICIENTS	:
1.000000	# <del> </del>   <del> </del>	1.000000	COCER		0.0	
1.000000		1.000000	CICER	1 11	1.300000	
1.000000		0000000	CIEXP	II.	1.000000	
0.0	Z3=	60.00000				
1.000000	= 7 7	000000.09	= 57	0.0		
CALCULATED VALUFS	4	SUM TO 1.4.1.4	<b>4.</b> 1		¥ * \$	S, MILL IONS
CD=CDCER X (T X DF)XX(CDEXP) X	XCF		:	:	0.0	0.
CLRM=CICER X (M)XX(CIEXP) X CF	CF X TF				<b>9</b>	1.300
					1.000	
=1.0 + LOG(PHI) / LOG(2.0)	• 01				1.000	:
CTFU=(CLRM / E)X((#RM X 21+.5)		KX(E) -0.5XX(E))			1.	1.300
CTB. = ((CLRM/E)X((#RM X Z3	+	0.51XX(E) -0.5XX(E))	1 / 23	23	1.	1.300
CIPS=CTB*24/22					•	1.300
=CTB X R					0.0	0
0£M OR CT8*25/22/ENYR	/ENYR	·			0.0	0
1 :	:			:		:

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.4.1.4.2 CONV. STA. & MONITOR/CONTROL FAC. TABLE

!		INPUT PAR	ARAMETERS			INI	UT COE	INPUT COEFFICIENTS
	<u>"</u>	21290.0000	<b>⊤</b> F=	1.000000		CDC ER =		0.0
	¥	21290.0000	=W30	0.0		CDEXP=		0.0
	C.F=	1.000000	21=	1.000000		CI CER≈		0.000478
	PH I=	1.000000	= 2 2	000000.09		CIEXP=		1.000000
ļ	-	0.0	23=	000000.09				
	0F=	1.000000	<b>5</b>	000000*09	= 57		0.0	
	CALCUI	CALCULATED VALUES	SO H	SUM TO 1	1.4.1.4			S, MILL IONS
:	CD=CDCER X	CD=CDCER X (T X DF)XX(CDEXP)	) X CF		!		:	0.0
	CLRM=CICER	CLRM=CICER X (M)XX(CIEXP) X C	CF X TF					10.177
B-2	#RM =T / M							1.000
257	E =1.0 +	=1.0 + LOG(PHI) / LOG(2.0	.01					1.000
	CT FU= ( CLRM	CTFU=(CLRM / E)X((#RM X Z1+.5	.5) XX(E) -0.5XX(E))	.5xx(E))		-		10.177
	CTB = ((CLRM/E)X((#RM	×	Z3 + 0.51XX(E	+ 0.5) XX(E) -0.5XX(E))		1 / 23		10.177
į	CIPS=CTB*24/22	4/22						10.177
	CRCI =	=CTB X R						0.0
	= W300	CO&M = 0&M OR CTB*25/22/E	/ENYR					0.0
:	COMMENTS		;		•			

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.4.1.5 MAINTENANCE EQPT. TABLE

INPUT P	INPUT PARAMETERS			INPUT CO	INPUT COEFFICIENTS
T= 1.000000	. TF=	1.000000		CDCER=	0.0
M= 1.00000	=W30	0.0		CDEXP=	0.0
CF= 1.000000	7.1=	1.000000		CICER=	4.000000
	22=	000000*09		CI EXP=	1.000000
R= 0.05000	73=	000000.09			
DF= 1.000000	= 4 7	000000000	= 57	0.0	
CALCULATED VALUES	<b>~</b>	SUM TO 1.	1.4.1		S.MILL IONS
CD=CDCER X (T X DF)XX(CDEXP)	P) X CF		:		0.0
CLRM=CICER X (M)XX(CIEXP) X	X CF X TF				4.000
M / 1= MX# B-					1.000
8 E =1.0 + LOG(PHI) / LOG(2.0)	2.0)				1.000
CTFU=(CLRM / E)X((#RM X 21+.5)X	+.5)XX(E) -0.5XX(E))	5XX(E))			4.000
CTB = ((CLRM/E)X((#RM X 2	23 + 0.5) XX(E	0.5)XX(E) -0.5XX(E))		1 / 23	4.000
CIPS=CT8*Z4/Z2	:				4.000
CPCI =CTB X R					0.200
CO&M = O&M OR CT8*25/22/ENYR	2/ENYR				0.0
COMMENTS					

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.4.1.6 LIGHTNING PROTECTION TABLE

i		INPUT PARA	ARAMETERS		: 	INPUT	INPUT COEFFICIENTS	
	<u>;;</u>	0.0	<b>≠</b> ₽=	1.000000		CDC ER=	0.0	
	#	0.0	=W30	0.0		CDEXP=	0.0	
	C.F.	0.0	21=	1.000000		CICER=	0.0	
	PH [=	1.000000	12=	000000.09		CI EXP=	0.0	
	<b>*</b>	0.0	73=	00000009				
	0 F=	1.000000	= + 7	00000000	= 57	0.0		
	CALCULAT	CALCULATED VALUES	49	SUM TO 1.	1.4.1		1W.\$	S, MILL IONS
	CD=CDCER X (T	CD=CDCER X (T X DF)XX(CDEXP)	XCF		 		0.0	:
	CLRM=CICER X	CLRM=CICER X (M)XX(CIEXP) X CF	CF X TF				0.0	
B-2	#RM =T / M						0.0	
259	E = 1.0 + LO	E =1.0 + LOG(PHI) / LOG(2.0)	10.				0.0	
	CTFU=(CLRM /	CTFU=(CLRM / E)X((#RM X Z1+.5)	•5) XX(E) -0.5XX(E))	5XX(E))			0.0	•
	CTB = ((CLRM/E)X((#RM	×	Z3 + 0.5)XX(E	0.5)XX(E) -0.5XX(E))		1 / 23	0.0	
1	CIPS=CTB*24/22				:		0.0	
	CRCI = CTB	.B × R					0.0	
	30 = W300	0£M OR CT8*Z5/Z2/ENYR	/ENYR				0.0	
!	COMMENTS							;

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.4.1.7 SITE & FACILITIES DOT&E TABL E

	: :	INPUT PARAMETERS	· · · · · · · · · · · · · · · · · · ·	:	INPUT CO	INPUT COEFFICIENTS
<u> </u>	1.000000	TF=	1.000000	ວ	COC ER =	1.000000
===	1.000000	=W30	0.0	33	)EXP=	1.000000
CF=	i.000000	71=	1.000000	5	ICER=	0.0
=IHd	1.000000	12=	000000*09	5	CI EXP=	0.0
<b>*</b>	0.0	23=	60.00000			
D.F= .	1.000000	= + 7	000000009	= 57	0.0	
CALCULAT	CALCULATED VALUES	s	SUM TO 1.	4.1		\$ MILL IONS
CER X (T	CD=CDCER X (T X DF)XX(CDEXP) X C	) X CF				1.000
CICER X	CLRM=CICER X (M)XX(CIEXP) X CF	CF X TF				0.0
=T / M						1.000
1.0 + LC	=1.0 + LOG(PHI) / LOG(2.0)	0.			;	000•1
CCLRM /	CTFU=(CLRM / E)X((#RM X 21+.5)XX	(E)	-0.5XX(E))			0.0
CTB = ((CLRM/E)X((#RM	×	Z3 + 0.5) XX(	.5) XX(E) -0.5XX(E))		62 / (	0.0
CIPS=CT8*24/22						0.0
CRCI =CTB	8 X R					0.0
30 = W300	08M OR CT8*Z5/Z2/ENYR	/ENYR				0.0
COMMENTS				· !	•	

## 1.4.2 RECTENNA SUPPORT STRUCTURE

The rectenna farm area of  $102.1~(\mathrm{km})^2$  is covered by 580,500 panels that have a total mW intercept area of  $79.53~(\mathrm{km})^2$ . Each panel  $(9.33~\mathrm{m}\times14.69~\mathrm{m})$  is tilted at an angle of  $40^\circ$  to the horizontal and is mounted on two continuous ribbons of concrete as shown in Figure 1.4-4. The procurement, fabrication, assembly and installation of the steel rectenna support structure, and the supporting foundation placement are costed in this section and represent the results of consultation and discussions with industrial/construction contacts.

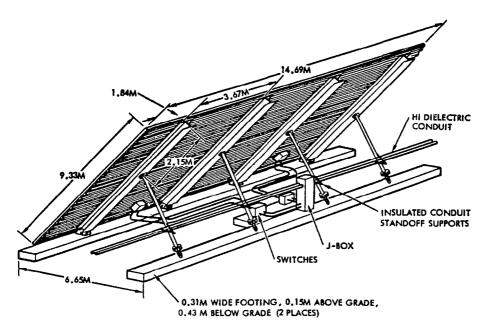


Figure 1.4-4. Panel Installation

# 1.4.2.1 PANEL STRUCTURE

The rectenna panel structure is comprised of four standard size eightinch (wide flange) I beams, supporting tube braces, and 18 hat-shaped sections for the mounting of the power collection electronic elements. Tube braces, steel cast fittings and attachment hardware are used to support the panel on the continuous footing as shown in Figure 1.4-5.

A detail analysis of the support structure was completed to identify the amount of material needed; fabrication, operations, assembly, and installation requirements; plus an estimate of manpower and equipments needed to produce the average daily production of 2150 panels over the nine month period. The cost of material for a rectenna panel is shown in 1.4-6.

The rectenna panel hat section serves as a mounting surface for the laminated-copper-clad mylar array elements. (See section 1.4.3, Power Collection). Adhesives will be used to mount the elements to the structure to

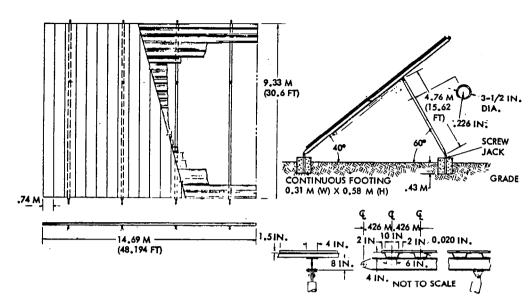


Figure 1.4-5. Rectenna Array Support Structure

ITEM/DESCRIPTION	DIMENSIONAL DATA	NUMBER REQ'D	TOTAL WETGHT	PREFAB & DELIVERED COST/PANEL (DOLLARS)
HAT SECTIONS	14.69M 6" 4" LONG 2"	18	1288# 584.25 kg	\$618.24
I-BEAMS	9.33M 3.94" LONG 0.170 7.90"	4	1589# 720.75 kg	\$508.48
TUBE BRACES	0.204	4	1104#	\$773.76
	4.76M LONG 3.50"	}	500.75 kg	
HARDWARE FITTINGS & WELDING ROD		4 SETS		
RETURNED SCRAP ALLOWANCE			-307# -139 kg	\$30.70
TOTAL MATERIAL PER PANEL			3674# 1666.75 kg	\$1869.78

Figure 1.4-6. Rectenna Panel Support Structure

provide continuous support and added strength with a minimum of localized panel deflection.

The basic hat section is formed at the rectenna site from 0.020" galvanized steel sheet stock by processing through a set of forming rollers in a continuous manner. The forming machine (Yoder mill) accommodates widths of rolled mill stock sufficient to produce the finished hat sections ready for assembly to the I-beams.

Four standard wide-flange 8-inch galvanized steel I-beams are required in lengths of 9.33 m for each rectenna panel. This material will be delivered to the site in precut lengths for hole punching and the addition of brackets/machined castings for the support braces and panel mounting.

Four 3.5" diameter tube braces of galvanized steel are cut to a length of 4.76 m and preassembled to the fittings/hardware. Anchors, brackets, clips, hangers, etc., are fabricated or cast of carbon steel material and galvanized prior to machining at the site. All these items are scheduled to combine with the hat sections and I-beams at a centralized facility for assembly. A concept for such a facility is shown in Figure 1.4-7. The factory has multiple assembly lines where each line has a materials feed section, steel assembly facilities, electron ics assembly and checkout section. It was assumed that one line using automated procedures could assemble and checkout a panel in 40 minutes. On this basis, seventy-two assembly lines operating 20 hours per day, seven days a week are required to produce 580,500 panels in the allocated 270 days. Eight additional requirements are summarized in the lower left of the figure.

After the panels have been checked, they are placed on an overhead conveying system and transported to loading stalls, where they are assembled into 9-panel magazines and loaded on specially designed trucks for delivery to the point of installation.

Specialized equipment is required to deliver the panels from the factory to the installation point and to install them because of their large dimensions. After consultation with industrial sources on large equipment handling, a concept for a specialized machine was developed (Figure 1.4-8). The front and rear wheel pairs are each steerable as a unit and have provisions for height adjustment. The panels are transferred in magazines and lifted by means of fixtures mounted in vertical rails. They can be translated laterally and longitudinally for final positioning before attachment to the footings.

## 1.4.2.2 TRENCHING AND CONCRETE FOOTINGS

A trade-off which considered eight individual footings versus continuous footings was made. A maximum wind force of 90 m/hr was assumed. It was determined that the amount of concrete required for either approach was essentially the same, but that the continuous footing concept was easier to install and required fewer operations and less capital equipment.

Each panel is secured to the footings at eight locations by fixtures which are imbedded in the concrete during the pouring operation. Mounting attachments which provide for longitudinal and lateral adjustment are secured to the fittings. Screw jacks on each of the rear attach points provide for panel adjustment and alignment.

The footings of continuous concrete are 0.43 meters deep, 0.31 meters wide, and project 0.15 meters above ground level. Two footings are excavated simultaneously by trenchers which feed the removed dirt into a truck. Approximately  $17\times10^5$  meters of trenches must be excavated. To accomplish this, 38 trenchers are required, each trencher excavating 90 meters per hour.

Figure 1.4-7. Central Panel Factory

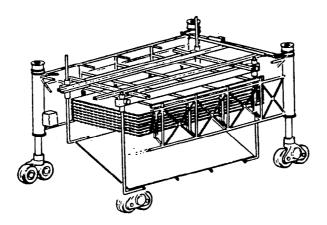


Figure 1.4-8. Panel Loading Sequence

Table 1.4-5 summarizes crew and equipment requirements compatible with the nine month schedule to prepare 1088 panel rows per rectenna.

Table 1.4-5. Concrete Foo	ting Equipment/Crew
---------------------------	---------------------

	SITE CONSTRUCTION QUANTITY	1977 UNIT PRICE (DOLLARS)	TOTAL COST
TRENCHERS - JW-2	38	\$70,000	\$2,660,000
DUMP TRUCKS - 992C	26	\$350,000	\$9,100,000
CONCRETE DELIVERY VEHICLES - 10 C.Y.	190	\$50,000	\$9,500,000
CONCRETE FORMING MACHINES	10	\$60,000	\$600,000
CONCRETE CENTRAL MIX PAVING PLANTS	2	\$250,000	\$500,000
TOTAL COST			\$22,360,000
TRENCHING & CONCRETE CREW PERSONNEL	1480		

Each rectenna panel will be mounted and aligned on 6.8 cu yds of concrete placed by concrete formers such as those commonly used in freeway divider construction. The formers extrude a shaped ribbon at rates of 6 meters per minute. Reinforcing steel and panel attach fittings are inserted as the concrete is vibrated during the extrusion process. Concrete footing requirements for the rectenna panels are shown in Table 1.4-6.

Table 1.4-6. Concrete Footing Requirements

ITEM/DESCRIPTION	1977 \$ (MILL PRICE DELIVERED)	INGREDIENTS FOR 6.8 CU.YDS.	MATERIAL COST DELIVERED (1977 DOLLARS)
CEMENT (5 SACK) (94# SACK)	\$42/TON	3196#	\$67.12
SAND	\$4.51/TON	9520#	\$21.47
ROCK 1"-11"	\$4.39/TON	12444#	\$27.31
WATER	-	2040#	Ø
REINFORCING STEEL - #4	\$0.10/LB	64#	\$6.44
TOTAL/PANEL		27264#	\$122.34

DELIVERED 1977 MILL PRICES PER ENGINEERING NEWS RECORD (ENR) - McGRAW HILL, AN INDUSTRY PUBLICATION

# 1.4.2.3 COST ESTIMATES

DDT&E, investment, construction/installation, and operations costs of the rectenna support structures (less electronic elements) and the concrete footings are identified in the following tables:

Table 1.4.2.1.1	Hat Sections
Table 1.4.2.1.2	Wide Flanges
Table 1.4.2.1.3	Tube Braces & Hardware
Table 1.4.2.1.4	Assembly & Installation
Table 1.4.2.2.1	Footing Concrete & Rebar
Table 1.4.2.2.2	Machinery & Equipment
Table 1.4.2.2.3	Construction Operations
Table 1.4.2.3	Support Structure DDT&E

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.4.2.1.1 HAT SECTIONS TABLE

		INPUT	INPUT PARAMETERS		;	INPUT	INPUT COEFFICIENTS
	T=	580500.000	TF=	1.000000		CDCER=	0.0
	포	1.000000	-W3()	0.0		CDEXP=	0.0
	- <b>CF</b>	1.000000	21=	1.000000		CICER=	0.000619
	=] Hd	1.000000	12=	000000.09		CI EXP=	1.000000
	& ¢	0.0		00000009	1		
	n⊬=	I • 000000	=+7	000000.09	= 97	0•0	0
1	CALCUL	CALCULATED VALUES	PANEL	SUM TO 1.	.4.2.1		\$, MILLIONS
•	CD=CDCER X	CD=CDCER X (T X DF)XX(CDEXP)	X CF		;		0.0
	CLRM=CICER	CLRM=CICER X (M)XX(CIEXP) X	CF X TF				0.001
В-	#RM =T / M						580500.000
-267	ш	=1.0 + LOG(PHI) / LOG(2.0	.0)				1.000
	CTFU=(CLRM	CTFU=(CLRM / E)X((#RM X ZI+.	5) XX(E)	-0.5XX(E))			359.228
	CTB = ((CLRM/E)X((#RM	×	Z3 + 0.5) XX(E)	E1 -0.5XX(E))		1 / 23	359.224
:	CIPS=CTB*Z4/Z2	7.72			; 		359.224
	CRCI =	=CTB X R					0.0
	= M3DD	06M OR CTB*25/22/	/ENYR				0.0
!	COMMENTS EACH PANE WITH COST \$1.0587KG	PANEL USES 18 HAT COST ESTIMATE(USS)	S	ECTIONS TOTALING 584.25 KG (1288LBS)	(1288	LBS)	

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.4.2.1.2 WIDE FLANGES TABLE

	INPUT PARA	PARAMETERS			INPUT CO	INPUT COEFFICIENTS
į.	580500.000	TF=	1.000000	CDC	CDCER=	0.0
¥	1.000000	=W30	0.0	COE	COEXP=	0.0
CF≡	1.000000	21=	1.000000	212	ER≖	0.000508
=I Hd	1.000000	2.2=	00000000	CIE	CI EXP=	1.000000
R=	0.0	23=	000000009			
0F=	1.000000	= 47	000000009	= 57	0.0	
CALCI	CALCULATED VALUES	PANEL	SUM TO 1.4	1.4.2.1		S, MILL IONS
CD=CD CER )	CD=CDCER X (T X DF)XX(CDEXP)	P) X CF				0.0
CLRM=CICE	CLRM=CICER X (M)XX(CIEXP)	X CF X TF				0.001
M / L= MN# B	4					580500.000
о П Ш	=1.0 + LOG(PHI) / LOG(2.0)	2.0)				1.000
CT FU= (CLR)	CTFU=(CLRM / E)X((#RM X Z1+.5)	+.5)XX(E) -0.5XX(E))	•5XX(E))			295.173
CTB = ((CLF	CTB = ((CLRM/E)X((#RM X	23 + 0.5)XX(E)	E) -0.5XX(E))	-	/ 23	295.170
CIPS=CTB*24/22	14/12				:	295.170
CRCI	=CTB X R					0.0
• W3DD	= 06M OR CTB*25/22/EN	2/ENYR				0.0
COMMENTS				`! !		

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.4.2.1.3 TUBE BRACES & HARDWARE TABLE

}		INPUT PARA	ARAMETERS		:	INPUT CO	INPUT COEFFICIENTS
i	<b>!!</b> <b>⊢</b>	580500.000	<b>T</b> F=	1.00000		CDCER=	0.0
1	Ĭ.	1.000000	=W30	0.0		COEXP=	0.0
	C F=	1.000000	<b>-17</b>	1.000000		CICER=	0.000743
	=IHd	1.000000	22=	60.00000		CI EXP=	1.000000
i	# # # # # # # # # # # # # # # # # # #	0.0	73=	000000009			
	DF=	1.000000	= + 7	000000009	= 57	0.0	
1	CALCU	CALCULATED VALUES	PANEL	SUM TO 1.4	1.4.2.1		S'HILL IONS
	CD=CDCER X	CD=COCER X (T X DF)XX(CDEXP)	) X CF		!		0.0
	CLRM=CICER	CLRM=CICER X (M)XX(CIEXP) X	X CF X TF				0.001
1 -	#RM = T / M						580500,000
269	E = 1.0 +	=1.0 + LOG(PHI) / LOG(2.0)	(0•				1.000
		CTFU=(CLRM / E)X((#RM X 21+.5	•5)XX(E) -0•5XX(E))	5XX(E))			431,346
1	CTB = ((CLR	CTB = ((CLRM/E)X((#RM X Z	Z3 + 0.5) XX(E	0.5) XX(E) -0.5XX(E))		1 / 23	431.343
•	CIPS=CT8*24/22	4/12					431.343
	CRCI	=CTB X R					0.0
	= W3JJ	06M OR CT8*25/22/EN	/ENYR				0.0
	COMMENTS INCLUD FRONT	INCLUDES 4 TUBE BRACES 4.76M LONG, FRONT & REAR CLEVIS FITTINGS, CAST MOUNTINGS, WELD ROD.	4.76M LONG,	OUNTINGS, WELD RO	. 0		
		OVIDES FOR DVERME	L SCORF MEEC	MAINCE O.			

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.4.2.1.4 ASSEMBLY & INSTALLATION TABLE

		INPUT PARAM	ARAMETERS			dNI	UT COE	INPUT COEFFICIENTS
	<u></u>	580500.000	TF=	1.000000		CDCER=		0.0
	N.	1.000000	=W30	0.0		CDEXP=		0.0
	C.F.	1.000000	<b>7</b> 1 =	1.000000		CI CER=		0.001052
	=I Hd	1.000000	22=	000000.09		CI EXP=		1.000000
	<b>8</b>	0.0	23=	000000.09				
	DF=	1.00000	= 7 7	000000*09	= 57		0.0	
	CALCUL ATED	LATED VALUES	PANEL	SUM TO 1.	1.4.2.1			S, MILL IONS
:	CD=CDCER X	CD=CDCER X (T X DF)XX(CDEXP) X	) X CF				:	0.0
	CLRM=CICER	CLRM=CICER X (M)XX(CIEXP) X	CF X TF					0.001
В-	#RM =T / M							580500.000
270	E =1.0 +	=1.0 + LOG(PHI) / LOG(2.0)	.0)					1.000
	CTFU= (CLRM	CTFU=(CLRM / E)X((#RM X Z1+.5)	XX(E)	-0.5XX(E))				610.762
	CTB = ((CLR	CTB = ((CLRM/E)X((#RM X Z	Z3 + 0.5) XX(E	0.5)XX(E) -0.5XX(E))		1 / 23		610.757
1	C1PS=CTB*24/22	4/12						610.756
	CRCI	=CTB X R						0.0
	= M300	0£M OR CTB*25/22/EN	/ENYR					0.0
:	COMMENTS	:			i i	!		

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.4.2.2.1 FOOTING CONCRETE & RE-BAR TABLE

		TUPNI	INPUT PARAMETERS			INPUT CO	INPUT COEFFICIENTS
	<u>"</u>	580500.000	<b>∓</b> F=	1.000300		CDCER=	0.0
	₹	1.000000	=W30	0.0		CDEXP=	0.0
	C.F.=	1.000000	21=	1.000000		CI CER=	0.000122
	=IHd	1.000000	22=	60.00000		CI EXP=	1.000000
	<b>6</b> ′	0.0	73=	00000009			
	0 F=	1.000000	= 4 7	000000*09	= 57	0.0	
	CALCUL	CALCULATED VALUES	PANEL	SUM TO 1.	1.4.2.2		S, MILL IONS
1	CD=CDCER X	CD=COCER X (T X DF)XX(CDEXP)	) X CF				0.0
	CLRM=CICER	CLRM=CICER X (M)XX(CIEXP) X	CF X TF				000*0
В-	#RM = 1 / M						580500.000
·271	w	=1.0 + tOG(PHI) / LOG(2	.0)				1.000
	CTFU= (CLRM	CTFU=(CLRM / E)X((#RM X 21+.	5) XX(E)	-0.5XX(E))			70.821
	CTB = ((CLRM/E)X((#RM	×	)XX(5°0 + EZ	0.5)XX(E) -0.5XX(E))		) / 23	70.820
!	CIPS=CTB*Z4/Z2	./22					70.820
	= IOSO	=CTB X R					0.0
	= W333	06M OR CT8*25/22/	/ENYR				0.0
	COMMENTS CCNCRETE MIX 3196 12444 LB	ESTIMATED A LBS CEMENT, S 1-1.5 INCH	17 6.8 CU YDS OF 9520 LBS SAND, 1 ROCK.	F 5 SACK CEMENT.			

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.4.2.2.2 MACHINGERY & EQUIPMENT TABLE

	INPUT PARAM	ARAMETERS			INPUT CO	I NPUT COEFFICIENTS
<u>!</u>	1.000000	TF=	1.000000	_	CDCER=	0.0
: N	1.000000	=W30	0.447200		COEXP=	0.0
CF=	1.000000	21=	1.000000		CI CER=	22.360001
<b>-1</b> Hd	1.000000	22=	000000.09	•	CIEXP=	1.000000
4	0.003333	23=	8.000000			
DF=	1.000000	= 47	2.000000	= 57	0.0	
CALCULAT	CALCULATED VALUES	SET	SUM TO 1.	1.4.2.2		S+ MILL IONS
CD=CDCER X (T	CD=CDCER X (T X DF)XX(CDEXP)	XCF		;		0.0
CLRM=CICER X	(M)XX(CIEXP) X	CF X TF				22,360
#RM = T / M						1.000
E =1.0 + LO	=1.0 + LOG(PHI) / LOG(2.0)	• 0)				1.000
CTFU=(CLRM / E)X((#RM X		Z1+.5)XX(E) -0	-0.5XX(E))			22.360
CTB = ((CLRM/E)X((#RM	×	Z3 + 0.51XX(	0.51XX(E) -0.5XX(E))		) / 23	22.360
CIPS=CTB*Z4/Z2	7.7					0.745
CRCI =CTB	rb x R					0.075
30 = W300	OEM OR CTB*Z5/Z2/ENY	2/ENYR				0.447
COMMENTS	!					

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.4.2.2.3 CONSTRUCTION OPERATIONS TABLE

INPUT COEFFICIENTS	0.0	0.0	0.000150	1.000000			\$, MILL IONS	0.0	29.940	1.000	1.000	59.940	59.940	59.940	0.0	0.0	
INPUT CO	CDCER=	CDEXP=	CICER=	CI EXP=		0.0							1 / 23				
:					) 	= 57	1.4.2.2	:						: !			;
	1.000000	0.0	1.000000	000000000	000000*09	000000000	SUM TO 1.					XX(E) -0.5XX(E))	(E) -0.5XX(E))				
ARAMETERS	TF=	=W30	=17	12=	23=	= + 7	MANDAYS	X CF	CF X TF		(0.		Z3 + 0.51XX(E)			Z/ENYR	
INPUT PARA	399600.000	399 600 . 000	1.000000	1.000000	0.0	1.000000	CALCULATED VALUES	CD=CDCER X (T X DF)XX(CDEXP) X	CLRM=CICER X (M)XX(CIEXP) X CF		=1.0 + LOG(PHI) / LOG(2.0)	CTFU=(CLRM / E)X((#RM X Z1+.5)	CTB = ((CLRM/E)X((#RM X Z	4/72	=CTB X R	06M OR CTB*25/22/EN	!
	<u>  </u>	3	C F=	≃] Hd	<b>~</b>	DF=	CALCU	CD=CDCER X	CLRM=CICER	M / 1= M8# B-2	u.	CT FU= ( CL RM	CTB = ((CLR	CIPS=CTB*Z4/Z2	CRCI	= W3J3	COMMENTS

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.4.2.3 SUPPORT STRUCTURE DDT&E TABLE

INPUT COEFFICIENTS	2.000000	0.300000	0.0	0.0			S* WILL IONS	2.000	0.0	1.000	1.000	0 • 0	0.0	0.0	0.0	0.0	
INPUT CC	CDCER =	CDEXP=	CICER=	CIEXP=		0.0 = 52	2						1 / 23				
	1.300000	0.0	1.000000	00000000	60.00000	00000009	SUM TO 1.4.2					XX(E) -0.5XX(E))	0.5)XX(E) -0.5XX(E))				
PARAMETERS	TF=	=W30	21=	12=	73=	= 7 7	SET	) x CF	CF X TF		.00	Z1+.5)XX(E) -(	Z3 + 0.5) XX(	:		/ENYR	· · · · · · · · · · · · · · · · · · ·
INPUT	1.000000	1.000000	1.000000	1.000000	0.0	1.000000	CALCULATED VALUES	CD=CDCER X (T X DF)XX(CDEXP) X	CLRM=CICER X (M)XX(CIEXP) X CF		=1.0 + LOG(PHI) / LOG(2.0)	E)X((#RM X 21+	×	22	78 × R	CCEM = OEM OR CTB*Z5/Z2/ENYR	
!	11 —	¥	CF≈	=I Hd	<b>*</b>	DF≈	CALCULAT	CD=CDCER X ()	CLRM=CICER X	B #RM = T / M	<b>u</b>	CTFU=(CLRM / E)X((#RM X	CTB = ((CLRM/E)X((#RM	CIPS=CTB*24/22	CRCI = CTB	10 = W3JJ	COMMENTS



## 1.4.3 POWER COLLECTION

This element of the GRS includes the rectenna array elements associated with the actual reception and rectification of the microwave radiation. These elements are in series and parallel as required to deliver the line output voltage and current. Also included are those components that accept the dc power from the array elements and route, control, convert, and switch this power for delivery to the power conversion stations of the grid interface.

The rectifier assembly consists of a GaAs diode and input/output filters. The outputs of the rectifier circuit are series connected to output 40+ kV (Figure 1.4-9). The regulation assembly accepts the voltage from the series connected rectenna diodes and adjusts the voltage output to the power distribution feeders to a value consistent with positive current flow. The rectenna array elements are  $0.735\times9.33$  m in size and 20 elements are combined per panel with diode circuitry equivalent to the mW density pattern. A total of 735 diodes or diode equivalents are required per average panel with a rectenna total of  $330\times10^6$  diodes as shown in Figure 1.4-10.

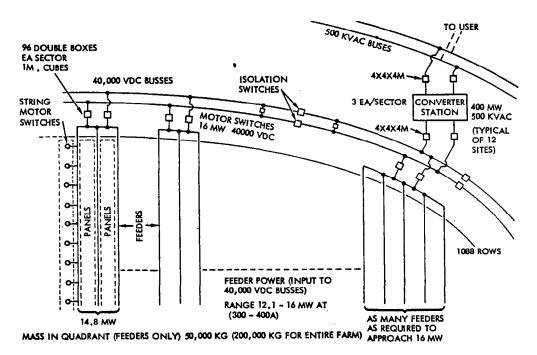


Figure 1.4-9. Rectenna Schematic Block Diagram
- Preliminary

The electronic array element of the antenna is a multilayered copper/dielectric sandwich panel material. Resource/mass projections are identified in Table 1.4-7. These calculations were based on the array cross section and panel requirements shown in Figure 1.4-11. Costs were determined from

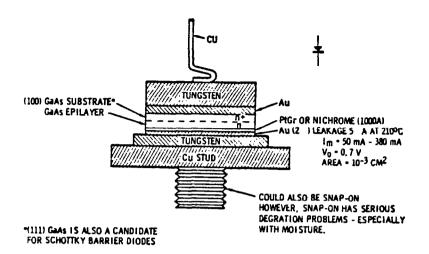


Figure 1.4-10. Diode Concept

Table 1.4-7. Resource Requirements Rectenna Dipole
- Bow-Tie - Panel Array Elements

580,500 RECTENNA PANE	LS
• DIFLECTRIC	
PLASTIC COMPOUND — 3.5 LB/FT <sup>3</sup> , 0.4375 LB/FT <sup>2</sup> x 856.4 x 10 <sup>6</sup> FT <sup>2</sup>	374.68 x 10 <sup>6</sup> LB
• MYLAR	
0.001-IN. THICKNESS AT 87.36 LB/FT <sup>3</sup> , 0.02913 LB/FT <sup>2</sup> x 856.4 x 10 <sup>6</sup> FT <sup>2</sup>	24.95 x 10 <sup>6</sup> LB
• COPPER	
0.0039 THICKNESS AT 556.6 LB/FT <sup>3</sup> , 0.118753 LB/FT <sup>2</sup> x 856.4 x 10 <sup>6</sup> FT <sup>2</sup>	101.70 x 10 <sup>6</sup> LB
• DIODES	
1 OZ. PER 426.67 x 10 <sup>6</sup> DIODES OR EQUIV	26.67 x 10 <sup>6</sup> LB
TOTAL	528 x 10 <sup>6</sup> LB
	909.6 LB/PANEL 412.6 KG/PANEL

estimating guides/industrial contacts and combined with the cost of switches and regulators needed at each panel to provide a total cost estimate of \$1942 for the antenna array elements.

The power collection and distribution system consists of all field feeders (collectors), supporting switchgear, 40 kV dc buses to the power converters, and the towers/footings needed to support the transmission lines. Approximately 330,000 switchgears, 10<sup>7</sup> meters of feeder cables, miscellaneous junction boxes, etc., must be delivered and installed at the panel sites. Tractor/trailer trucks are used for this purpose and proceed through the panel rows,

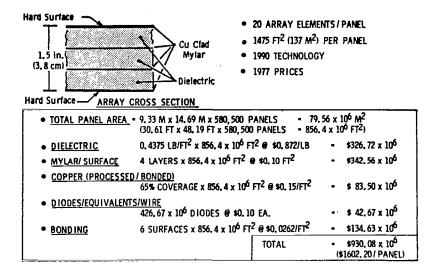


Figure 1.4-11. Rectenna Dipole - Bow-Tie Panel Array Elements

delivering material at each panel. Additional trucks with reels playout the feeders, which then are installed in conduits and spliced to panel connections by the electrical installation crew. Contacts with a utility company indicate a requirement of 8 manhours to hookup one panel. On this basis, the manpower and equipment projections were established for a 20 hour 7 day week.

Equipment for electrical hookup and checkout of completed panels was calculated on the basis of acquisition cost prorated over the service life and utilization period at a particular site. Total crew requirements of 4196 personnel and the schedule period were the basis of calculating man-day requirements of 755,280. The amortized cost of equipment and labor were combined for the total cost factor.

DDT&E power collection costs are associated with the design and verification of bow-tie electronic panels/bonding processes, connectors, and large switchgear to optimize the voltage/current ratios and element/wiring configuration. Cost estimates are provided in the following areas:

Table 1.4.3.1	Antenna Array Elements
Table 1.4.3.2	Power Distribution System
Table 1.4.3.3	Installation and Checkout
Table 1.4.3.4	Power Collection DDT&E

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.4.3.1 ANTENNA ARRAY ELEMENTS TABLE

INPUT PARAM				INPUT	INPUT COEFFICIENTS
580500.000	1F= 0&M=	1.000000	U U	COCER= COEXP=	0.0
1.000000	Z1 =	1.000000	S	CI CER=	0.001942
1.000000	22=	000000000	ن	I EXP=	1.000000
0.0	73=	60.00000			
1.000000	= 7 7	60.00000	= 57	0.0	
CALCULATED VALUES	PANEL	SUM TO 1.4.3	63		SWILL IONS
CO=COCER X (T X DF)XX(COEXP)	X CF				0.0
X (M)XX(CIEXP) X	X CF X TF				0.002
					580500.000
=1.0 + LOG(PHI) / LOG(2.0)	(0.				1.000
CTFU=(CLRM / E)X((#RM X 21+	Z1+.5)XX(E) -0.	-0.5xx(E1)		,	1127.331
CTB = ((CLRM/E)X((#RM X Z	Z3 + 0.5)XX(E	0.5)XX(E) -0.5XX(E)		67 / (	1127.322
CIPS=CTB*Z4/Z2					1127.321
=CTB X R					0.0
COEM = 06M OR CTB*Z5/Z2/ENYR	/ENYR				0.0
:				:	

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.4.3.2 POWER DISTRIBUTION SYSTEM TABLE

	INPUT PA	ARAMETERS			INPUT	INPUT COEFFICIENTS
<b>1</b> =	580500.000	TF=	1.000000		CDCER=	0.0
¥.	1.000000	=W30	0.0		<b>CDEXP</b> =	0.0
CF=	1.000000	Z 1 =	1.000000		CICER=	0.000120
=1 Hd	1.000000	75=	60.00000		CI EXP=	1.00000
<b></b>	0.0		000000.09			
0F=	1.000000	= 77	000000009	= 57	0.0	
CALCUI	CALCULATED VALUES	PANEL	SUM TO 1.4.3	.3		S* MILL IONS
CD=CDCER X	CD=CDCER X (T X DF)XX(CDEXP)	) X CF		; ; !		0.0
CLRM=CICER	CLRM=CICER X (M)XX(CIEXP)	X CF X TF				000*0
#RM =T / M						580500.000
E =1.0 +	=1.0 + LOG(PHI) / LOG(2.	(0•				1.000
CT FU=(CLRM	CTFU=(CLRM / E)X((#RM X Z1+.	5)XX(E)	-0.5XX(E))			099*69
CTB = ((CLRM/E)X((#RM	×	23 + 0.5) XX(	0.5) XX(E) -0.5XX(E) )		1 / 23	659*69
CIPS=CTB*Z4/Z2	4/12					69•69
CRCI	=CTB X R					0.0
= W300	OEM OR CTB*25/22/	2/ENYR				0.0
COMMENTS	:	•		!		

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.4.3.3 INSTALLATION & CHECKOUT TABLE

	INPUT PARAM	PARAMETERS		:	INPUT CO	INPUT COEFFICIENTS
<u>#</u>	781100.000	<b>-</b> ₹	1.000000		CDCER=	0.0
11	4340.00000	=W30	0.0		COEXP=	0.0
C F=	1.000000	=17	1.000000		CI CER=	0.000200
=1 H d	1.000000	22=	000000.09		CI EXP=	1.000000
R.	0.0	73=	60.000000			
0F=	1.000000	= 7 7	00000009	= 57	0.0	
CALCUL	CALCULATED VALUES	MANDAYS	SUM TO 1.	1.4.3		S.MILLIONS
DCER X	CD=CDCER X (T X DF)XX(CDEXP) X	P) X CF		:	-	0.0
CLRM=CICER	X (M)XX(CIEXP)	X CF X TF				0.868
M / 1=						179.977
=1.0 +	=1.0 + LOG(PHI) / LOG(2.0)	2.01				1,000
= ( CLRM	CTFU=(CLRM / E)X((#RM X Z1+.5)X	X(E)	-0.5xx(E))			156.220
= ((CLR	CTB = ((CLRM/E)X((#RM X	Z3 + 0.51XX(	0.5)XX(E) -0.5XX(E))		1 / 23	156.220
CI PS=CTB*24/22	4/22					156.220
CRCI	=CTB x R					0.0
C 0 8 M =	06M OR CTB*25/22/ENY	2/ENYR				0.0
COMMENTS						

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.4.3.4 POWER COLLECTION-DDT&E TABLE

INPUT COEFFICIENTS	3.000000	0.300000	0.0	0.0			S+ MILL IONS	3.000	0.0	1.000	1.000	0•0	0.0	0.0	0.0	0.0	
INPUT	CDCER=	CDEXP=	CICER=	CIEXP=		0.0						٠	1 / 23				
	1.000000	0.0	1.000000	60.000000	60.00000	= 57 0000000*09	SUM TO 1.4.3					-0.5XX(E)	0.5) XX(E) -0.5XX(E))				
ARAMETERS	<b>∓</b> F=	=W3 O	<b>51</b> =	22=	23=	= 4 Z	SET	X CF	CF X TF		. (0•	5) XX(E)	73 + 0.5) XX(			/ENYR	
INPUT PA	1.000000	1.000000	1.000000	1.000000	0.0	1.000000	CALCULATED VALUES	X DF1XX(CDEXP	(M)XX(CIEXP) X		=1.0 + LOG(PHI) / LOG(2.	CTFU=(CLRM / E)X((#RM X 21+.	×		X X	I OR CT8*25/22/	
	<u>=</u>	#	CF=	=1 Hd	# <b>&amp;</b>	0F=	CALCULATE	CD=CDCER X (T X DF)XX(CDEXP)	CLRM=CICER X (M)XX(CIEXP)	#RM =T / M	m;	CTFU=(CLRM / E	CTB = ((CLRM/E)X((#RM	CIPS=CTB*24/22	CRCI =CTB	M30 = M300	COMMENTS
							-	1		B-2	281						į

## 1.4.4 CONTROL

The telemetry, tracking, communications, monitoring of microwave beam characteristics, computing phase corrections, and the equipment needed to provide frequency standard signals for the satellite are included in this section. This hardware will be used to monitor and control the satellite from the ground.

The following monitor and control functions are performed:

- 1. Tracking, using ground-based radars to monitor the orbital stability of the satellite.
- 2. Beam monitoring and control, using ground equipment for adaptive or command control of the satellite microwave beam.
- 3. Data management, using equipment required to analyze signals and data from the satellite and ground-based systems to compute control signals and corrective data to maintain safe and optimum performance.
- 4. Communications, using equipment required to maintain communications between the ground station and the SPS satellite. Included are the communications with the crew, and telemetry and command equipment not included in the beam monitoring and control assembly.

At this time, the cost effort is divided into the three categories of control center equipment, beam control electronics, and DDT&E. Two sets of full-up IBM 370, or equivalents, a complete display center, and a manned control room are envisioned as basic elements of the control center. Beam control electronics would consist of control sensors and dual frequency transmitters. The overall DDT&E and hardware costs were projected by engineering. The exacting requirement of this rectenna operation will require further study in future contract activity to define the technical and performance standards. It should also be noted that system and operational requirements are needed to define adequate software/programming considerations.

Cost estimates are presented as follows:

Table 1.4.4.1 Control Center Equipment

Table 1.4.4.2 Control Electronics

Table 1.4.4.3 Control DDT&E

RDCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.4.4.1 CONTROL CENTER EQUIPMENT TABLE

INPUT PAR T= 1.000000	RAMETERS TF=	1.000000	i ·	INF	UT CO	INPUT COEFFICIENTS = 0.0
1.000000	06M= Z1= 72=	0.0		CDEXP= CICER= CIEXP=		15.000000
0.0	73=	60.000000	= 57		0.0	
CALCULATED VALUES	SET	SUM TO 1.	1.4.4			\$ HILL IONS
CD=CDCER X (T X DF)XX[CDEXP]	X CF			i	1	0.00
CLRM=CICER X (M)XX(CIEXP) X	CF X TF					15.000
						1.000
=1.0 + LOG(PHI) / LOG(2.	(0)					1.000
CTFU=(CLRM / E)X((#RM X 21+.	5) XX(E)	-0.5XX(E))				15.000
CTB = ((CLRM/E)X((#RM X Z3	į	+ 0.5)XX(E) -0.5XX(E)		) / 23		15.000
CIPS=CTB*Z4/Z2						15.000
=CTB X R						0.0
CCEM = 0EM OR CTB*25/22/ENYR	ENYR					0.0

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.4.4.2 CONTROL ELECTRONICS TABLE

	INPUT P	PARAMETERS			INPUT CO	CO EFFI CI ENTS
=	1.000000	TF=	1.000000		CDC ER =	0.0
¥	1.000000	-W30	0.0		COEXP=	0.0
C F=	1.000000	21=	1.000000		CICER=	000000.09
Φ.	1.000000	22=	000000.09		CI EXP=	1.000000
i	0.0	23=	00000009			
DF=	1.000000	= + 7	000000.09	= 57	0.0	
CALCULAT	CALCULATED VALUES	SET	SUM TO 1.	1.4.4		S, MILL IONS
CD=CDCER X (T	(T X DF)XX(CDEXP)	) X CF		:		0.0
CLRM=CICER X (M)XX(CIEXP)		X CF X TF				000*09
#RM =T / M						1.000
E =1.0 + LO	=1.0 + LOG(PHI) / LOG(2.0)	•0)				1.000
CTFU=(CLRM / E)X((#RM	×	Z1+.5)XX(E) -0.	-0.5XX(E))			000.09
CTB = ((CLRM/E)X((#RM	×	1) XX (5°0 + EZ	.5) XX(E) -0.5XX(E))		1 / 23	000*09
CIPS=CTB*Z4/Z2	2			: !		000•09
CRCI =CTB	ВХК					0 • 0
CCEM = DEM	M OR CT8*25/22/ENYR	/ENYR				0.0
COMMENTS	:					

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION \*\*3 CONTROL DDIEE TABLE

		INPUT PAR	ARAMETERS			Z	PUT CO	INPUT COEFFICIENTS	
	II F	1.000000	TF=	1.000000		CDC ER=		10.00000	
:	¥	1.000000	=W30	0.0		CDEXP=		1.000000	į
	CF=	1.000000	21=	1.000000		CICER=		0.0	
	PHI=		22=	000000000		CIEXP=		0.0	
	 	0.0	23=	60,000000			:	· · · · · · · · · · · · · · · · · · ·	
	DF=	1.000000	= + 2	000000.09	= 57		0.0		
:	CALCULATED VALUES	VALUES	SET	SUM TO 1.4.4	4.4			\$+ MILL TONS	S
	CD=CDCER X (T X DF)XX(CDEXP)	DF)XX(CDEXP	X CF					10.000	
	CLRM=CICER X (M)XX(CIEXP) X CF	)XX(CIEXP) X	CF X TF				•	0.0	
В-	#RM =T / M							1,000	i
285	E = 1.0 + LOG	=1.0 + LOG(PHI) / LOG(2.0)	(0)					<u>1.000</u>	

=CT8*Z4/Z2

23 + 0.51xx(E) - 0.5xx(E)

CTB = ((CLRM/E)X((#RM X

CTFU= (CLRM / E)X((#RM X 21+.5)XX(E) -0.5XX(E))

0.0

0.0

COMMENTS

## 1.4.5 GRID INTERFACE

This element includes the power conversion equipment that receives electrical power from the power collection system and conditions/converts it to a high voltage dc or ac power acceptable for input into the national power grid.

The converter stations accept 40 kV dc power and output 500 kV ac or dc. The concept utilizes a solid-state inversion/step-up concept typified by an existing dc - ac conversion station located in Sylmar, California. Although specific design details of this system await clarification in a future study effort, an analysis and cost estimate was prepared as shown in Table 1.4-8. The CER for DDT&E were derived from cost estimates in the "Technical Study Report on Pacific Northwest-Southwest dc inter-tie," prepared by the Bonneville Power Administration in February, 1976. This DDT&E estimate was based on six cost quotations which Bonneville received on a 1.44 GW and a 2.20 inter-tie. The total cost for the 1.44 GW terminal ( $$156.7\ \overline{\rm M}$ ) was allocated as 30% DDT&E and 70% ICI. This judgment was based on the assumption that most of the facility will be a standard design.

Table 1.4-8. Grid Interface (WBS 1.4.5)

ITEM DESCRIPTION	SPECIFICATION	GRS QUANTITY	PROJECTED UNIT COST	TOTAL (1977 \$)
CONVERTER: STATIONS	400 mW 500 kV ac or kV dc	12 EA.	\$10×10 <sup>6</sup>	\$120×10 <sup>6</sup>
ISOLATION SWITCH- GEAR	4×4×4 m	24 EA	\$400,000 EA	\$0.96×10 <sup>6</sup>
FILTER YARDS		12	\$100,000 EA	\$1.2×10 <sup>6</sup>
INTERCONNECT TOWERS & FOUNDATION	500 kV ac TOWERS	90 EA		\$12.741×10 <sup>6</sup>
INTERCONNECT TRANSMISSION CABLE		12 LINES	\$90,000/MI	\$10.789×10 <sup>6</sup>
TOTAL/GRS '				\$145.69×10 <sup>6</sup>

Cost estimates are presented in Table 1.4.5.1 on electrical equipment and in Table 1.4.5.2 on DDT&E.

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.4.5.1 ELECTRICAL EQUIPMENT TABLE

	•	INPUT P	INPUT PARĀMETERS			INPUT	INPUT COEFFICIENTS
	<b>!!</b> <b>├</b>	1.000000	T F ::	1.000000		CDCER=	0.0
:	¥	1.000000	=W30	0.0		CDEXP=	0.0
	CF=	1.000000	21=	1.000000		CI CER=	145.690002
	=I Hd		12=	000000.09		CI EXP=	1.000000
		0.0	73=	60.000000			
	0F=	1.000000	<b>2</b> 4=	60.000000	= 57	0.0	
i	CAL CUL ATED	VALUES	SET	SUM TO	1.4.5		S, MILL IONS
	CD=CDCER X (T X DF)XX(CDEXP)	OF)XX(CDEXP	X CF	,		:	0.40
	CLRM=CICER X IN	X (M)XX(CIEXP) X CI	CF X TF				145.690
В-	#RM =T / M						1.000
287	E =1.0 + LOG(	=1.0 + LOG(PHI) / LOG(2.0)	(ō·				1,000
	CTFU=(CLRM / E)X((#RM X	X((#RM X Z1+.5	.5)XX(E) -0.5XX(E)	.5xx(E))			145.690
ì	CTB = ((CLRM/E)X((#RM	×	Z3 + 0.51XX(E	0.5)XX(E) -0.5XX(E))		1 / 23	145.690
	CIPS=CTB*24/22					:	145.690
	CRCI = CTB	×					0*0
	COEM = DEM OR	OR CTB*25/22/ENYR	/ENYR				0.0

J,

COMMENTS

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.4.5.2 GRID INTERFACE-DDTEE TABLE

INPUT COEFFICIENTS	37.714996	0.60400	0.0	0.0		0.0	\$ MILLIONS	669*66	0.0	1.000	1,000	0.0	0.0	1. <b>0.0</b> 1	0.0	c
ZI	CDC ER=	COEXP=	CI CER=	CI EXP=		= 57	.4.5						1 / 23	:		
	1.000000	0.0	1.000000	00000009	60.00000	000000.09	SUN TO 1.					X(E) -0.5XX(E))	E) -0.5XX(E))	:		
PARAMETERS	TF=	=W30	21=	12=	Z3 =	<b>24=</b>	GW	P) X CF	X CF X TF		2.0)	+.5) XX(E) -0	Z3 + 0.5) XX(E)			2 / FNYR
INPUT PARAM	5.000000	5.000000	1.000000	1.000000	0.0	1.000000	CALCULATED VALUES	CO=COCER X (T X OF)XX(COEXP)	(M)XX(CIEXP)		LOG(PHI) / LOG(2.0)	CTFU=(CLRM / E)X((#RM X Z1+.5)X	×	22	=CTB X R	DEM OR CIB*75/72/FNYR
	<u>~</u>	: : : :	CF₌	₽H I=	e.	DF=	CALCULA	CD=CDCER X (	CLRM=CICFR X	#RM =T / M	7 + C•I = 388	CTFU=(CLRM /	CTB = ((CLRM/F)X((#RM	CIPS=CTB*24/22	CRCI =C	U # 8300

COMMENTS

## 1.4.6 OPERATIONS

This element includes the planning, development, and conduct of operations at the ground receiving station. It includes both the direct and support personnel and the expendable maintenance supplies required for the ground station operation and maintenance.

Operations and maintenance personnel required after IOC are identified as a 300 personnel staff to provide a 24 hour operation, maintenance/repair, security, and administrative support (Table 1.4-9). A cost estimate for maintenance material (expendables, trucks, and equipment); standby auxiliary power; and test/support equipment is also identified in the table.

Table 1.4-9. Operations Requirements

ITEM	SHIFT	NO.	TOTAL	1977 DOLLARS
OPERATIONS & MAINTENANCE PERSONNEL			•	
COMMAND & CONTROL CENTER (PERSONNEL + SUPERVISORY)	1 2 3	30 30 20	80	
CONVERTER STATION (TOTAL FOR 12 STATIONS)	1 2 3	36 36 36	108	
24-HOUR MAINTENANCE, REPAIR, SECURITY, & G&A/SUPPORT	:	112	112 300	
MAINTENANCE MATERIAL				\$13.13×10 <sup>6</sup>
EXPENDABLES, TRUCKS, EQUIP., UTILITIES, TEST/SUPPORT EQUIP.				

Cost estimates are shown in Table 1.4.6.1 for operations and maintenance personnel and in Table 1.4.6.2 for maintenance material.

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 5.1 OPER. & MAINT. PERSONNEL 1.4.6.1 TABLE

FFICIENTS	0.0	0.0	0.0	0.0			\$, MILL IONS	0	0.0	1.000	1.000	0 • 0	0*0	0.0	0 • 0	64.800
INPUT COEFFICIENTS	CDC ER =	CDEXP=	CI CER=	CI EXP=		0.0							) / 23	:		
	1.000000	64.800003	1.000000	60.00000	60.00000	<b>90°00000°09</b>	SUM TO 1.4.6					-0.5XX(E))	E) -0.5XX(E))	:		
INPUT PARAMETERS	_	300.00000 0£M=	1.000000 21=	7	0.0		CALCULATED VALUES MAN-DAYS	(T X DF)XX(CDEXP) X CF	CLRM=CICER X (M)XX(CIEXP) X CF X TF		=1.0 + LOG(PHI) / LOG(2.0)	/ E)X((#RM X 21+.5)XX(E) -0.	)X((#RM X 23 + 0.5)XX(E)	2	B X R	M OR CT8*25/22/ENYR
	=	1 2	C.F=	PH I=	#¥	0F=	CALCULAT	CD=CDCFR X (T	CLRM=CICER X	B #RM =T / M	-290 E = 1•0 + F0	= ( CLRM	CTB = ((CLRM/E)X((#RM	CIPS=CTB*24/22	CRCI = CTB	W30 = W303

360 DAYS/YR \* 3 SHIFTS/DAY \* 300 MANDAYS/SHIFT \* \$200/MANDAY

COMMENTS

ROCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.4.6.2 MAINT. MATERIAL TABLE

	INPUT PARA	ARAMETERS			Z	PUT COE	INPUT COEFFICIENTS	
<u>"</u>	1.000000	TF=	1.000000		CDCER=		0.0	
¥	1.000000	=W30	13.130000		COEXP=		0.0	
C.F=	1.000000	≥17=	1.000000		CICER=		0.0	
PH I=	1.000000	22=	000000000		CI EXP=	·	0.0	
ex.	0.0	23=	60.00000					
DF=	1.000000	= 7 7	000000009	= 57		0.0		
CALCULATED	ED VALUES	SET	SUM TO 1.	4.6			S, MILL IONS	ONS
CD=CDCER X (T	(T X DF)XX(CDEXP)	) X CF					0*0.	
CLRM=CICER X	X (M)XX(CIEXP) X	CF X TF					0.0	
#RM = 1 / M							1.000	
07 + 0*1 = # ± 291	=1.0 + LOG(PHI) / LOG(2.0)	• 03					1.000	
) = N = (	E)X((#RM X Z1+.5)	XX(E)	-0.5XX(E))				0.0	
CTB = ((CLRM/E)X((#RM	<b>×</b>	23 + 0.5) XX(E)	E) -0.5xx(E))		) / 23		0.0	
CIPS=CTB*Z4/Z2	2		·			į	0.0	
CRCI = CTB	X X						0.0	
M30 = M303	M OR CT8*25/22/EN	/ENYR					13.130	
COMMENTS								

# 1.5 MANAGEMENT AND INTEGRATION

This element includes all efforts and material required for management and integration functions at the systems level and program level. It encompasses the following functions:

- 1. Program Administration
- 2. Program Planning and Control
- 3. Contracts Administration
- 4. Engineering Management
- 5. Manufacturing Management
- 6. Support Management
- 7. Quality Assurance Management
- 8. Configuration Management
- 9. Data Management
- 10. Systems Engineering and Integration.

This element sums all of the direct effort required to provide management control including planning, organizing, directing, and coordinating the project to ensure that overall project objectives are accomplished. These efforts overlay the functional work areas (e.g., engineering, manufacturing, etc.) and assure that they are properly integrated. This element also includes the efforts required in the coordination, gathering, and dissemination of management information. Also included are the engineering efforts related to the establishment and maintenance of a technical baseline for a system by generation of system configuration parameters, criteria, and requirements. It includes requirements analysis and integration, system definition, system test definition, interfaces, safety, reliability, and maintainability. It also includes those efforts required to monitor the system development and operations to ensure that the design conforms to the baseline specifications.

The management and integration function for DDT&E, TFU :ICI, RCI and O&M are estimated at a cost equal to 5% of the corresponding total dollar estimates for WBS elements 1.1 through 1.4 within each area. Table 1.5 presents this tabulation.

RUCKWELL SPS CR-2 REFERENCE CONFIGURATION 1.5 MANAGEMENT AND INTEGRATION

TABLE

	INPUT PARA	P AR AMET ERS			INPUT CO	INPUT COEFFICIENTS
	0.0	TF=	1 • 00 0000	CDCER	R =	0.0
Ë	0.0	-M30	0.0	COEXP=	P=	0.0
C F=	0.0	21=	1.000000	CICER=	# <b>*</b>	0.0
#[ H.	1.000000	2.2=	9000009	CI EXP=	₽=	0.0
	၁•၀	=c.7	60.000.09			
D F=	1.000000	<b>5</b> 4=	000000*09	<b>-57</b>	0.0	
CALCULAT	CALCULATED VALUES	5% * ALL	SUM TO 1			\$ PHILLIONS
CD=CDCER X ()	CD=CDCER X (I X DF)XX(CDEXP) X	P) X CF				1392,463
CLKM=CICER X	CLKM=CICER X (M)XX(CIEXP) X C⊦	X CF X IF				0
#RM = 1 / M						0.0
ı.	=1.0 + LOG(PH1) / LUG(2.0)	2.0)		-		0.0
26 CIFU= (CLRM /	CIFU=(CLRM / E)X((#KM X Z1+.5)	XX(E)	-c.5xx(E))			2151.918
CTB = ((CLRM/E)X((#RM X		23 + 0.5) XX (E)	E) -0.5XX(E))		/ 23	0.0
C1PS=CTE*24/22	7.5					600.679
CRCI =CTB X K	FB X K	den en en en en en en en en en en en en e				18.815
C	COEM = UEM UR CTB*25/22/EN	2/ENYR		·		8.561
CUMMENTS DDT&E+TFU CALCULATE FOK WES	DUTRESTFUSICISKOLS AND URM CALCULATED AT 5% OF CORRES FOR WES 1.1 THROUGH 1.4	UEM ARE RESPONDING TOTALS	TOTALS	:		-

# 1.6 MASS CONTINGENCY

, and a

A cost contingency has been added to the SPS Program to provide for potential growth due to increased weight as a result of design/development activities that would affect the procurement of systems during any phase of the program. This allowance is costed as a 15% bottom line contingency to the DDT&E, TFU, ICI, RCI and O&M elements of the program. Table 1.6 reflects the total amounts in each of these areas based on the totals of items 1.1, 1.2, and 1.3.

RUCKWELL SPS CK-2 REFERENCE CONFIGURATION MASS CONTINGENCY

1.6

TABLE

	INPUT PAK	AKAMET EKS		:	INPUT CO	INPUT COEFFICIENTS
	ڻ• ر	#	1.000000		CDCER=	0.0
:	0.0	U£M=	0.0		CDEXP=	0.0
	ن ن ت	=17	1.000000		CICEK=	0.0
	1.000000	2.2=	00000000		C1 EXP=	0.0
	0.0	23=	00000000			
	000000	<b>- 7 7 -</b>	00000000	=57	0.0	
CALCULATED	ED VALUES		SUM TO 1			S,MILLIONS
1)	CD=CDCEK X (T X DF)XX(CDEXP)	) X CF				4160,031
×	CLRM=CICER X (M)XX(CIEXP) X C	CF X 1F				0.0
#KM = 1 / M						0.0
	E = 1.0 + LOG(PHI) / LUG(2.0	(0,				0.0
<u></u>	C1FU=(CLKM / E)X((#KM x 21+.5)XX(E) -0.5XX(E))	5)XX(E) -(	).5XX(E))			5912.945
RM/E	CTB = ((CLRM/E)X((#RM X Z	13 + 6.5) XX (C	0.5) XX(E) -0.5XX(E))		) / 23	0.0
C1PS=C18*24/22	2					1263.413
=C.T	CKCI =CTB X K	M. A MARCOLINA MARCOLINA DE LA COMPONIO DEL COMPONIO DEL COMPONIO DE LA COMPONIO DEL COMPONIO DE LA COMPONIO DEL COMPONIO DE LA COMPONIO DE LA COMPONIO DE LA COMPONIO DE LA COMPONIO DE LA COMPONIO DE LA COMPONIO DE LA COMPONIO DE LA COMPONIO DE LA COMPONIO DE LA COMPONIO DE LA COMPONIO DE LA COMPONIO DE LA COMPONIO DE LA COMPONIO DEL COMPONIO DE LA COMPONIO DEL COMPONIO DE LA COMPONIO DE LA COMPONIO DEL COMPONIO DE LA COMPONIO DEL				56.405
30. =	CO&M = U&M OR CTb*25/22/ENYK	ZENYK	,		•	13.927
A S S	ENTS A 25% MASS CONTINGENCY IS AS A 15% COST CONTINGENCY	1S COS 1ED	1.2, 1.3			

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