# Large-Area Silicon Sheet Task

A.D. Morrison, Chairman

Presentations were made by seven contractors and by JPL on silicon (Si) sheet efforts and related work.

Westinghouse Electric Corp. reviewed progress on the Si dendritic-web growth contract. A set of new computer models was used successfully to define a growth system configuration that was then built and used to grow web with lower thermally generated stress than has any configuration previously developed by empirical means.

Mobil Tyco Solar Energy Corp. which is conducting research on the edge-defined film-fed growth (EFG) method of making Si ribbon, reported that a significant increase in cell efficiency was demonstrated in large areas (50 cm<sup>2</sup>) of ribbon grown at high speed (3.5 cm/min). The best cells gave 11.7% efficiency (AMI and AR coated), just short of this year's goal of 12%.

In the Semix Inc. semicrystalline cast Si program, a technique was developed to determine base resistivity and carrier lifetime in semicrystalline wafers. Also, 100-cm<sup>2</sup> cells of 13.5% efficiency (AMI) were made in limited quantities.

Kayex Corp., which has just completed its effort on advanced Czochralski Si ingot growth, reviewed achievements since contract inception. These included automated growth of 150 kg of 15-cm-dia ingot material per crucible, with after-growth yields of greater than 90% at throughputs of 1.5 kg/h.

Cornell University reported on scanning transmission electron microscopy (STEM) and microprobe investigations of processed EFG ribbon. The following process-induced changes in the def t structure (as compared to unprocessed EFG ribbon) were noted:

- (1) Processing introduces regularly spaced, sub-boundary-like dislocation arrays in the bulk (ba e section) of the material.
- (2) Some (but not all) of the dislocation nodes in these networks act as nucleation centers for small (d < 100 Angstrom) precipitates.
- (3) Large precipitates (d  $\approx$  1  $\mu$ m) are formed in the bulk of the material.

The chemical composition of the large precipitates was studied by non-dispersive X-ray analysis in a JEOL 200 CX STEM and by dispersive analysis (for C) in a JEOL 733 Superprobe. Elements identified were Ti, Fe, W, Mo, Cl, Ca and C. None of these elements were found in the matrix. It appears that the precipitates act as gettering centers for impurities. C1 is traceable to the Cl bakeout of the graphite dies.

The structural arrangement and the electrical activity of dislocations at or close to the central twin plane in processed material was studied by electron-beam induced current (EBJC) microscopy on a shallow-bevel specimen.

The majority of the dislocations in the twin plane are regularly spaced and mostly straight arrays of dislocation of like sign, accommodating a tilt component. Dislocation density in the twin plane is high, and the dislocations are effective recombination centers. Inspection of straight sections under higher magnification shows that the electrical activity varies along the dislocation, possibly due to precipitates (TEM will be carried out after completion of EBIC to clarify this point). Temperature-dependent EBIC is being carried out in order to determine the electronic energy levels associated with the various sections.

JPL in-house research program results were presented on the electrical and structural properties of grain boundaries in silicon, particularly those concerning electrical and enhanced diffusion along the grain boundaries.

Temperature-dependence measurements of zero-bias conductance, a photo-conductivity technique, and deep-level transient spectroscopy (DLTS) were developed to investigate potential barrier, carrier recombination velocity, and electronic states, respectively. The studies of potential barrier have revealed that considerable variation in the activation energy along grain boundaries often exists, presumably due to variation of local disorders; the activation energy usually increases with annealing temperature, and the potential barrier decreases with increasing light intensity. The recombination velocity measurements show that the velocity increases with boundary state density and light intensity. The preliminary result from the DLTS experiments indicates a trend: the density of states generally increases with the distance from the edges of the band gap. However, the details vary considerably from sample to sample, a result that can be attributed to local variation of disorders.

A grooving and staining technique, secondary ion mass spectroscopy, and EBIC measurements in scanning electron microscopy were used to study enhanced diffusion of phosphorus at grain boundaries in polycrystalline silicon. The results shows that the enhanced diffusion occurs only at high-order grain boundaries baving high carrier recombination and the depth of the enhanced diffusion, ries drastically from boundary to boundary, making my quantitative measurement difficult unless the boundary can be characterized well.

The University of Illinois at Chicago is studying the fundamental mechanisms of abrasion and wear and the deformation of Si by a diamond in various fluid environments. The abrasion rates and depths of damage of <100> and <111> p-type Si in three fluid environments (acetone, ethanol, and water) were determined, and the surface deformation mechanism was found to change when the fluid was varied.

Applied Solar Energy Corp. presented results on the efficiency of solar cells made from EFG ribbon and Semix Inc. material. For EFG material, a baseline process was applied to ribbons grown with or without CO<sub>2</sub> in the ambient. In general, cells made from EFG ribbon grown in CO<sub>2</sub> performed better. However, the results from both groups were lower than those reported previously.

For the Semix material, work continued on Lagot 5848-13C. High-efficiency processes were applied and the results were presented. A series of more severe gettering achedules was performed on identified portions of the

ingot. It was shown that short-circuit current improved with gettering up to a limiting value (which was still below that of the control cell). Light-biased diffusion length measurements showed that there was a negative light-biased effect (the minority carrier diffusion length decreased) that limited the improvement of short-circuit current in the more severely gettered cells. Also, the baseline process was applied to 10 x 10-cm Semix wafers randomly selected (not from a single ingot).

# ADVANCED DENDRITIC WEB GROWTH DEVELOPMENT

WESTINGHOUSE ELECTRIC CORP.

iechnology	Report Date					
Single crystal rit . ; rowth	04/21/82					
Approach  Silicon dendritic web growth Contractor  Westinghouse Electric Corp. Research & Development Center JPL Contract 955843  Goals  Develop computer models for characterizing and understanding web growth  Develop experimental web growth machine for use with models  Demonstrate melt-replenished steady-state web growth  Demonstrate 25 cm²/minute web growth rats	Status  First generation computer models developed and verified  Experimental web growth machine completed and operational  Melt-replenished steady-state web growth demonstrated at intermediate growth rate of 7 cm <sup>2</sup> /min  Web growth rate of 27 cm <sup>2</sup> /minute demonstrated under transient conditions  Growth width To 5 cm demonstrated					

# **Program Emphasis**

- Deformation Is Major Limitation Of Ribbon Width And Throughput Rate
- Deformation is Correlated To Thermally Generated Stress
- Computer Models Provide Understanding Of Web Growth And Thermal Requirements For Stress Reduction And Optimized Throughput

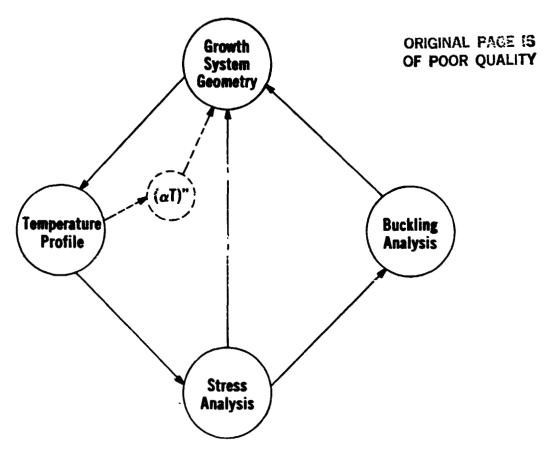
### **Principal Activity**

- Develop Computer Models For Web Growth
- Develop Experimental Web Growth Machine Capable
   Of Automated, Melt-Replenished, Steady-State Growth
- Utilize Computer Models And Experimental Growth Machine For Development Of Advanced Web Growth

Computer Models to Characterize Web Growth

- Compute Web Temperature Distribution Generated By A Specified Growth Configuration
- Compute Thermal Stress Generated By A Specified Web Temperature Distribution
- Compute The Critical Buckling Conditions For A Specified Thermal Stress

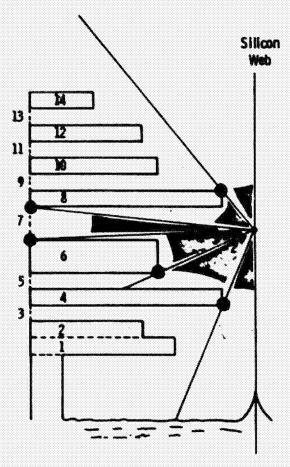
### **Application of Computer Models**



# **Status of Computer Models**

- Web Temperature Model Has Been Expanded To Be More Definative And Has Been Verified As Adequate For Next Generation Of Increased Web Throughput
- Thermal Stress Model Is Complete And Verified
- Critical Buckling Model Is Complete And Verified





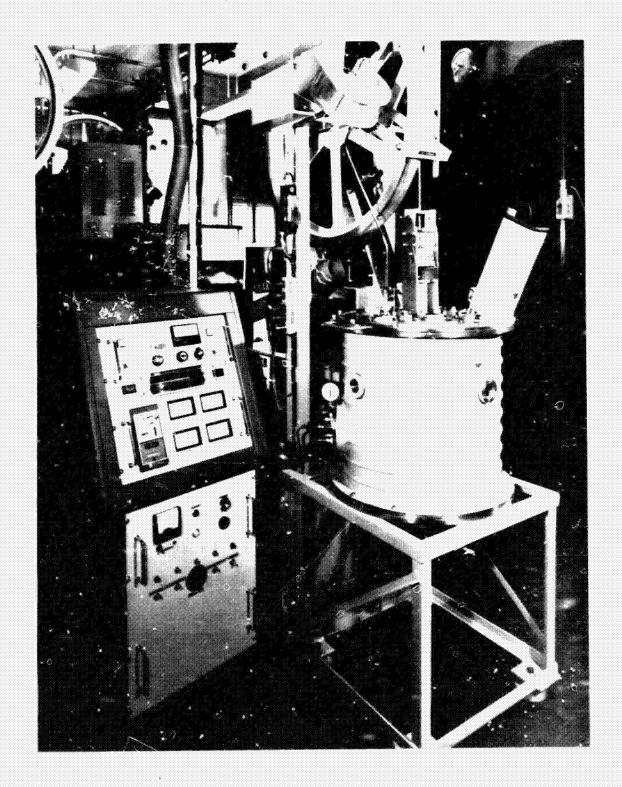
Steady-State Web Growth Is Necessary

- For Process Analysis, Understanding And Improvement
- For Subsequent Process Standardization

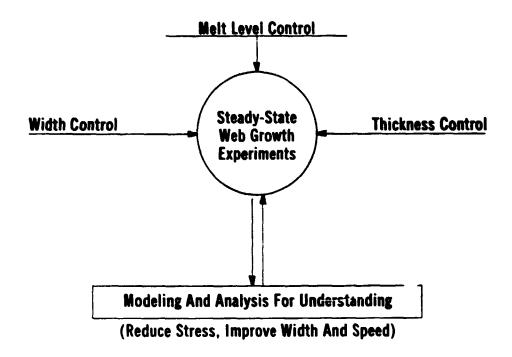
Experimental Web Growth Machine Provides Basic Requirements for Automated Steady-State Growth:

- Flat Temperature Profile In Growth Region Of Melt
- Controlled Constant Temperature
- Controlled Constant Melt Level
- Controlled Constant Thickness
- Controlled Constant Width

Dendritic Web Experimental Sheet Growth Unit (ESGU)



### Combined Use of Models and Experimental Web Growth



Results of First Use of Mudels

- In First Application Models Were Verified By Comparison With A Previously Characterized Growth Configuration. The Model Identified System Limitations And Suggested Modifications Which Resulted In Width Increase Of 25% (To 5 cm)
- Automated Steady-State Web Growth Achieved At Intermediate Rate (7 cm<sup>2</sup>/minute)
- Use Of Models Proven As Route For Understanding And Improvement Of Web Growth

#### **Problems and Concerns**

- <u>Present</u> None. Understanding And Improvement Of Process Proceeding As Planned
- <u>Future</u> Availability Of Low-Cost Polysilicon In Pellet Form

### Summary

- Computer Models Of Web Growth Completed And Verified
- Experimental Web Growth Machine Proven In Automated Steady-State Growth
- Web Growth Improved By Application Of Models

# **EDGE-DEFINED FILM-FED GROWTH**

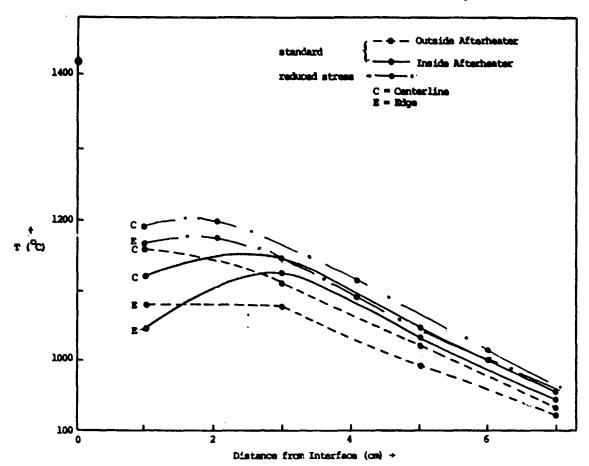
#### MOBIL TYCO SOLAR ENERGY CORP.

APPROACH MULTIPLE GROWTH OF 10 cm WIDE SILICON RIBBON AT 4 cm/minute.  CONTRACTOR MOBIL TYCO SOLAR ENERGY CORPORATION  GOALS  REDUCE STRESS AND IMPROVE FLATNESS OF RIBBON GROWN AT 4 cm/minute AND 200 µm THICKNESS.  DEMONSTRATE 12% CELL EFFICIENCY ON LARGE AREAS (50 cm²) FOR RIBBON GROWN IN HIGH SPEED SYSTEM.  DESIGN, CONSTRUCT AND OPERATE NEW MILLTIPLE RIBRON FURNACE FOR GROWTH  MILLTIPLE RIBRON FURNACE FOR GROWTH	TECHNOLOGY	REPORT DATE
MULTIPLE GROWTH OF 10 cm WIDE SILICON RIBBON AT 4 cm/minute.  • CARTRIDGE DESIGN CHANGES HAVE REDUCED RIBBON STRESS AND BUCKLING LEVELS FOR 200 µm THICK RIBBON TO LEVEL WHERE FABRICATION OF LARGE AREA CELLS IS POSSIBLE.  • LARGE AREA (50 cm²) CELLS OF 11.7%  (AM1 AND AR COATED) HAVE BEEN ACHIEVED FOR RIBBON GROWN IN HIGH SPEED SYSTEM (AT 3,5 cm/minute).  • NEW MULTIPLE RIBBON FURNACE HAS BEEN BUILT AND TESTED (OPERATION HAS BEEN SET ASIDE DUE TO REDUCTION OF PROGRAM).	LARGE AREA SILICON SHEET BY EFG	4/21/82
OF FOUR 10 CM WIDE RIBBONS.	MULTIPLE GROWTH OF 10 cm WIDE SILICON RIBBON AT 4 cm/minute.  CONTRACTOR MOBIL TYCO SOLAR ENERGY CORPORATION  GOALS  REDUCE STRESS AND IMPROVE FLATNESS OF RIBBON GROWN AT 4 cm/minute AND 200 µm Thickness.  DEMONSTRATE 12% CELL EFFICIENCY ON LARGE AREAS (50 cm²) FOR RIBBON GROWN IN HIGH SPEED SYSTEM.  DESIGN, CONSTRUCT AND OPERATE NEW MULTIPLE RIBBON FURNACE FOR GROWTH	<ul> <li>CARTRIDGE DESIGN CHANGES HAVE REDUCED RIBBON STRESS AND BUCKLING LEVELS FOR 200 µm THICK RIBBON TO LEVEL WHERE FABRICATION OF LARGE AREA CELLS IS POSSIBLE.</li> <li>LARGE AREA (50 cm²) CELLS OF 11.7% (AM1 AND AR COATED) HAVE BEEN ACHIEVED FOR RIBBON GROWN IN HIGH SPEED SYSTEM (AT 3.5 cm/minute).</li> <li>NEW MULTIPLE RIBBON FURNACE HAS BEEN BUILT AND TESTED (OPERATION HAS BEEN SET ASIDE DUE TO REDUCTION OF</li> </ul>

# Progress in Stress Studies

- INFLUENCE OF CARTRIDGE COMPONENT DESIGN ON STRESS AND BUCKLING LEVELS IN 10 cm WIDE RIBBON HAS BEEN IDENTIFIED:
  - TEMPERATURE FIELDS IN LINEAR COOLING PLATES OF SEVERAL DIFFERENT DESIGNS HAVE BEEN MEASURED.
  - IMPROVED FLATHESS WAS ACHIEVED IN 200 µm
    THICK RIBBON GROWN WITH A MODIFIED DESIGN
    CARTRIDGE.
  - CHANGE IN HORIZONTAL ISOTHERM SHAPE IS PROBABLE CAUSE FOR REDUCED STRESS AND BUCKLING LEVELS.

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Comparirm of center and edge temperature profiles in 10 cm cartridge linear cooling plates.

#### Stress Studies: Plans

- CAPABILITY IS NEEDED TO PREDICT: (1) MOVING RIBBON TEMPERATURE PROFILES GIVEN SYSTEM COMPONENT TEMPERA-TURES AND GEOMETRY, AND (11) STRESS DISTRIBUTIONS AND BUCKLING THRESHOLDS FROM RIBBON TEMPERATURE FIELDS.
- EMPIRICAL APPROACH WILL: (1) GUIDE THEORETICAL
   STUDIES AND ESTABLISH BOUNDARY CONDITIONS FOR MODELING,
   AND (11) ARRIVE AT REDUCED STRESS GROWTH CONFIGURATIONS
   THAT ARE COMPATIBLE WITH ACCEPTABLE GROWTH CONDITIONS
   AT 4 cm/min.

IMPORTANT TO SYNTHESIZE OUT OF THIS APPROACH A SYSTEM THAT WILL PRODUCE 200 PM THICK RIBBON AT 4 CM/MIN WITH SUFFICIENTLY LOW STRESS AND FLATNESS TO MEET DEMANDS IN YIELD AREA.

### Progress in Quality Improvement

- SIGNIFICANT IMPROVEMENT IN CELL EFFICIENCY OF HIGH SPEED GROWN RIBBON TO 11-12% HAS BEEN ACHIEVED.
  - AMBIENT CONTROL HAS PROVEN TO BE VERY IMPOR-TANT PARAMETER IN OBTAINING CONSISTENT ELECTRONIC QUALITY RIBBON.
  - RIBBON EXIT GAS SEAL, MORE UNIFORM INTERFACE GAS CONTROL SYSTEMS IMPLEMENTED SUCCESSFULLY.

SPV Diffusion Length Data for 10 cm Wide Ribbon Grown with Stretched Cartridge in Machine 17. Bulk Helt Doping was 4  $\Omega$ -cm for All Runs.

Run No. and Segment	M.Z. Argon Flow Rate (L/minute)	Cartridge Gus Composition	Cartridge Gas Flow Rute (L/minute)	Gas Scal	Speed (cm/minute)	(hw) T <sup>D</sup>
17-199-1A -1C	10	argon	1.5	ijΩ	3.0 - 3.2 3.8	23.0 35.0
17-200-1A	6	argon 0.45% (D <sub>2</sub>	1,0		3.5	33.0
-10	6	+ 45 ppm O2	1.8	110	3.8 - 3.9	43.0
17-201-1B -1D	<u>6</u> 3	argon	1,0	yes	3,3 3,3 - 3,4	33.6 30.0
17-202-1A	3				3.5 - 3.6	43.0
-1B -1C	2	argon	1.0	yœs	3.8 3.8	39.0 52.0
-110	0			-1-1-1-1-1	3.8	36.0
17-303-1A	6	0.17% (O <sub>2</sub>	1,0	yes	3,3	41.0
-1C		+ 18 ppm O2	1,2		3,5	45.0
17-201-1A		argon	1.0		3.5	79.0
-1C	6	0,29% (O₂ + 29 ppm O₂	1.4	yœs	3.5	36.0
17-205-1B	6	0.17% (O <sub>2</sub> + 17 ppm O <sub>2</sub>	1,2	yes	3,5	45.4

Solar Cell Data for Phosphine Processed Large Area (50 cm<sup>2</sup>) Solar Cells Made from 10 cm Wide Ribbons.

100 mW/cm<sup>2</sup>, Xenon Light, 28°C, AR Coated.

			Cell 1	Paramete	er8				
Run No.	Growth Ambient	Speed (cm/min)	Average Resistivity (N-cm)	Diffusion Length (μm)	sc <sub>2</sub> (mA/cm <sup>2</sup> )	v oc (V)	FF	η (%)	Mean n (%)
17–143	0.2% ∞₂	2,5	1.5	27	26.5 26.5 27.7 26.2 28.6 26.2 26.6	0.523 0.531 0.534 0.530 0.538 0.529 0.533	0.608 0.705 0.677 0.699 0.634 0.717 0.896	8.4 9,9 10.0 9.7 9.7 9.9	9.6
17-174	Quartz in melt	3.5	1.0	35	25.3 26.7	0.527 0.534	0.667 0.697	8.9 9.9	9.4
17-175	0.0% CO <sub>2</sub> + 30 ppm O <sub>2</sub>	3.5	1.0	<b>36</b>	26.8 27.7 26.1 27.5	0.539 0.545 0.537 0.547	0.735 0.706 0.720 0.641	10.6 10.7 10.1 9.7	10.3
17-178	1% 00 <sub>2</sub> + 100 ppm 0 <sub>2</sub>	3.5	1.0	34	26.4 26.2	0.518 0.517	0.696 0.642	9.5 8.7	9.1
17-181	0.23% CO₂ + 23 ppm O₂	3.5	4.0	43	29.0 28.8	0.525 0.522	0.603 0.713	9.2 10.7	10.0
17-204	Stretched cartridge with gas seal 0.29% CO <sub>2</sub> + 29 ppm O <sub>2</sub>	<b>3.</b> 5	4,0	36	29.1 28.3 29.7 29.3 29.8 30.5 29.8	0.517 0.530 0.541 0.546 0.537 0.542 0.546	0.726 0.629 0.688 0.732 0.704 0.669 0.716	11.6 9.5 11.1 11.7 11.3 11.1 11.7	11.1

### **EFG Ribbon Quality: Status**

- HIGH SPEED GPOWN RIBBON EFFICIENCIES AT 11-12% ARE STILL BELOW BEST EFG RIBBON AVAILABLE, WITH PAR-TICULAR SHORTFALL IN VOC AND FF.
- ISSUES TO SETTLE:
  - WHAT ARE UNDERLYING MATERIAL QUALITY DE-FICIENCIES?
  - CAN THIN RIBBON, PROCESSED WITH IMPROVED GETTERING AND BSF SCHEMES, ACHIEVE GOALS ON PRESENT MATERIAL?

### **Annealing Studies**

- HIGH TEMPERATURE HEAT TREATMENTS (800-1100°C) IN NITROGEN AND OXYGEN AMBIENTS LEAD TO CONSISTENT DEGRADATION OF (DARK) SPV DIFFUSION LENGTHS INDEPENDENTLY OF GROWTH CONDITIONS, INTERSTITIAL OXYGEN LEVEL OF RIBBON (CO<sub>2</sub> ON OR OFF, OR QUARTZ IN THE MELT).
- PH<sub>3</sub> TREATMENT DURING ANNEAL CAN IMPROVE DARK DIFFUSION LENGTH <u>AND</u> APPEARS TO BE NECESSARY TO PRODUCE LIGHT ENHANCEMENT.

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Schottky Barrier SPV Diffusion Leigth Measurements Before and After Heat Treatment of 10 om Wide Ribbon in an Oxygen Ambient.

			_		on Long			ion Langi Heat Tr		Rat	io (L <sub>A</sub> /L	в)
Heat Treatment	Growth Run	Growth Ambient	No. of Sample Pairs	X (j=)	s (um.)	s/x	X (1m)	s (jus)	s/x	x (hw)	s (pm)	s/x
	Œ		3		•		83.4	5.42	0.06			
5 hrs at 800°C in O <sub>2</sub> .	17-117	a. ;on	8 7	43.9 48.7	21.0 17.5	0.48 0.40	33,3 34,3	7.94 7.97	0,24 0,23	0,78 0.78	0.64 0.28	0,65 0,36
Sister sample measurement.	17-166	quartz in melt	8	48.2	21.3	0,44	35,5	15.8	0.44	0.77	0.30	0.39
measid dimere.	16-258	0,425 <i>l/min</i> of 1% 00 <sub>2</sub>	8	51.7	19.4	0.38	39,5	7.32	0, 19	0.88	0.40	0.45
	C'.	-	3				73.7	15.3	0.21			
50 mins at	17-117	argon	8	40.6	16.0	0.39	21.6	8,36	0.39	0.57	0.25	0.43
900°C in O <sub>2</sub> . Sister sample	17-166	quartz in melt	8 7	46.7 51.0	25.5 25.4	0.57 0.50	30,1 29.0	13.1 13.8	0.44 0.48	0.60	0.65 0.24	0.79
measurement.	16-250	0.425 L/min of 1% (D <sub>2</sub>	8	45.÷	10.9	0.24	28.9	8.71	0.30	0.65	0.14	0.22
7.5 hrs at	CZ	-	4	111.0	5,29	0.05	32.6	2,79	0.00	0.294	0.025	0.086
900°C in O₂.	17-148	argon	6	30.7	8.8	0.20	17.0	9.89	0.58	0.57	0.27	J.43
Sister sample measurement.	17-147	quartz in melt	6	37.2	13.9	0.37	15.7	14.3	0.91	0.41	0.36	0.87

 $<sup>\</sup>bar{x}$  = mean value; s = standard deviation.

Schottky Bar. SPV Diffusion Length Measurements Before and Afte. PH<sub>3</sub> Diffusion for 10 on Wide Bibbon

				Biffusion Lengt Refore Heat Tr							Ratio (L <sub>A</sub> /L <sub>B</sub> )		
lleat Treatment	Growth Run	Growth Ambient	No. of Sample Pairs	x (µm)	s (µm)	s/x	X (1m)	8 (Ma)	8/x	x (µm)	s (µm)	s/x	
9000 diffusion: 10 mins O <sub>2</sub> /N <sub>2</sub> +	cz	-	2	155.0	2.12	0.01	146.0	1.13	0.01	0.91	0.03	0.02	
30 mins Pin +	17-142	argon	7	28.3	12.0	0.42	38.8	11.6	0.30	1.43	0.31	22	
furnace cool to	17-174	quar'z in melt	7	31.3	6.86	0.22	27.6	5.76	0.21	0.02	0.32	0.35	
mins. Same sam- ple measurement.	17-175	0.3% CO <sub>2</sub> + 30 ppm O <sub>2</sub>	5 4	37.7 40.3	7.12 4.80	0.19 0.12	37.5 27.9	23.1 9.69	0.62 0.35	1.11 0.70	0.95 0.23	0.86 0.33	
	CZ		3	157.9	6.77	0.04	116.8	7.74	0.07	0.74	0.37	0.10	
800 <sup>0</sup> C diffusion:	17-117	argon	7	26.5	7.92	0.30	34.9	12.4	0.36	1.40	0.57	0.41	
1 hr in O <sub>2</sub> /N <sub>2</sub> + 1 hr in PN <sub>3</sub> +	17-175	0.3% 00₂ + 30 pμm 0₂	6	42.8	11.6	0.27	53.3	10.7	0.20	1.33	0.47	0.36	
4 hrs in O <sub>2</sub> /N <sub>2</sub> . 'Sister sample	17-177	1% CO <sub>2</sub> + 100 ppm O <sub>2</sub>	8	43.2	7.49	C.17	43.2	10.8	0.25	1.01	0.24	0.23	
measurument.	17-174	quartz in melt	7	46.4	15.4	0.33	44.3	15.6	0.35	0.96	0.19	0.20	

# Status of EFG Multiple-Ribbon Program: Needs

- NEW FURNACE FOR FOUR 10 cm WIDE RIBBONS IS OPERATIONAL WITH AUTOMATIC WIDTH CONTROL AND MELT REPLENISHMENT.
   WORK TO BE DONE CONCERNS:
  - ESTABLISHING RELIABILITY, LIFETIME FOR FURNACE COMPCMENTS IN LONG TERM OPERATION.
  - IMPLEMENTING AMBIENT CONTROL AT LEVEL WHICH ENSURES QUALITY CONSISTENCY.
- FUNDAMENTAL QUESTIONS REGARDING VIABILITY AND COST-EFFECTIVENESS OF FURNACE IN PRODUCTION MODE REMAIN:
  - YIELDS FOR THIN RIBBON MUST BE HIGH: LOW STRESS, FLATNESS AT 150-200 um THICKNESS, 4 cm/min are absolute necessity.
  - <u>SIMULTANEOUS</u> ACHIEVEMENT OF HISH DUTY RATE, CONSISTENT QUALITY, HIGH YIELDS MUST OCCUR.

#### **Problems and Concerns**

- STRESS AND NON-FLATNESS IN THIN (200 µm) RIBBON DO NOT PERMIT FABRICATION OF RIBBON GROWN AT HIGHEST SPEEDS (~4 cm/minute) INTO CELLS WITH ACCEPTABLE YIELDS.
- DEMONSTRATE THAT BEST CELL PERFORMANCE LEVELS OF 11-12% ACHIEVED IN SINGLE CARTRIDGE FURNACES CAN BE OBTAINED CON-SISTENTLY IN A MULTIPLE RIBBON FURNACE.
- DEMONSTRATE RELIABILITY OF MULTIPLE RIBBON FURNACE OPERATION OVER THE LONG TERM, WITH ACCEPTABLE DUTY RATES, THROUGHPUT AND MATERIAL QUALITY.

# SEMICRYSTALLINE PROCESS DEVELOPMENT

#### SEMIX INC.

TECHNOLOGY	REPORT DATE
LARGE AREA SILICON SHERT	April 22, 1987
APPROACH	STATUS
SEMICRYSTALLINE CRYSTALLIZATION PROCESS DEVELOR- MENT AND VERIFICATION	WORK IS CONTINUING TO DEVELOP AN UNDERSTANDING OF THE RASIC MECHANISMS IN THE CRYSTALLIZATION OF SEMICRYSTALLINE MATERIAL.
CONTRACTOR SINIX INCORPORATED	A TECHNIQUE MAS BEEN DEVELOPED TO DETERMINE BASE RESISTIVITY AND CARRIER LIPETIME IN SEMICRISTAL- LINE WAPERS. EXTENSIONS OF THIS TECHNOLOGY ARE BEING PURSUED FOR EVALUATION OF UCP BRICKS.
GOALS DIVESTIGATE STRUCTURAL PROPERTIES OF UCP INVESTIGAT.	SERCIX MAS ACRIEVED CELLS OF 13.5% EFFICIENCIES IN LIMITED QUARTITIES.
	MR MAVE CONFLETED THE DESIGN PHASE AND ENTERED THE PROCURENCIT AND CONSTRUCTION PHASE OF A PROTOTYPE 3 UCP SYSTEM CAPABLE OF SOLIDIFYING 42 KILOGRAMS OF
DENOWSTRATE 142 AND REFFICIENCY WITH 100 CM2 SOLAR CELLS.	CTI ICCU LE ARE INDESTALATION COM ACCOUNT
EVALUATE AND INVESTIGATE THE CRITICAL ELEMENTS NECESSARY FOR HIGH THROUGHPUT UCP SYSTEMS.	

### Principal Areas of Research

- A. FUNDAMENTAL STUDIES OF SEMICRYSTALLINE MATERIAL
- B. HIGH EFFICIENCY SEMICRYSTALLINE SOLAR CELLS
- C. WAFERING MECHANISMS

### Areas of Fundamental Study

#### CRYSTALLIZATION

INVESTIGATION OF THE ROLE OF MICROSTRUCTURE ON THE PERFORMANCE OF SEMICRYSTALLINE SILICON, MOST NOTABLY THROUGH:

GRAIN ORIENTATION STUDIES, AND INVESTIGATION OF STRUCTURAL IN-HOMOGENEITIES

#### CHARACTERIZATION

DEVELOPMENT OF TECHNIQUES FOR THE CHARACTERIZATION OF SEMICRYSTALLINE SILICON FOR BOTH:

RESISTIVITY
CARRIER LIFETIME

### Crystallization

PURPOSE:

TO DETERMINE THE ROLE OF GRAIN VOLUMES AND GRAIN BOUNDARIES ON THE QUALITY OF SEMICRYSTALLINE

MATERIAL.

APPROACH:

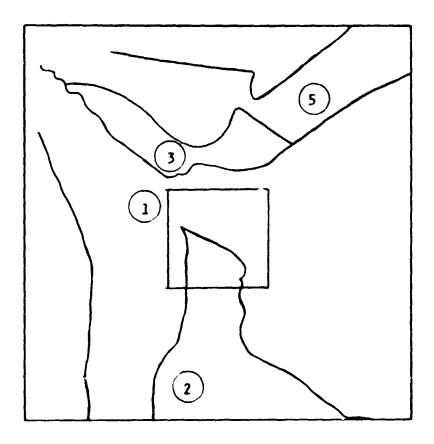
DETERMINATION OF THE RELATIVE ORIENTATION OF WEIGH BORING CRYSTALLITES.

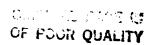
INVESTIGATION OF THE IMPACT OF MICROSTRUCTURAL DEFECTS ON CELL PROPERTIES:

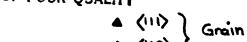
INDIVIDUAL DISLOCATIONS

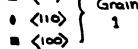
DISLOCATION SUBGRAIN BOUNDARIES

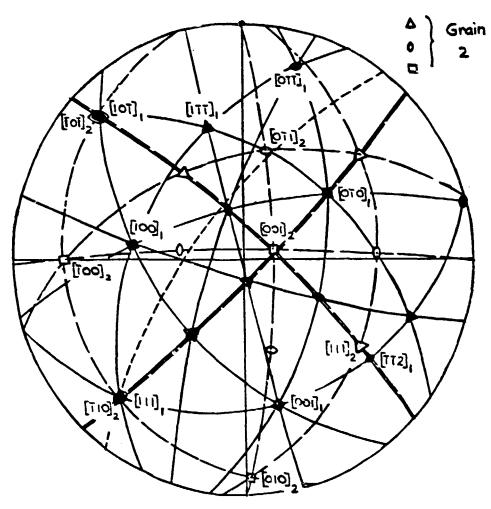
# Relative Positions of Grains in Sample Semicrystalline Material



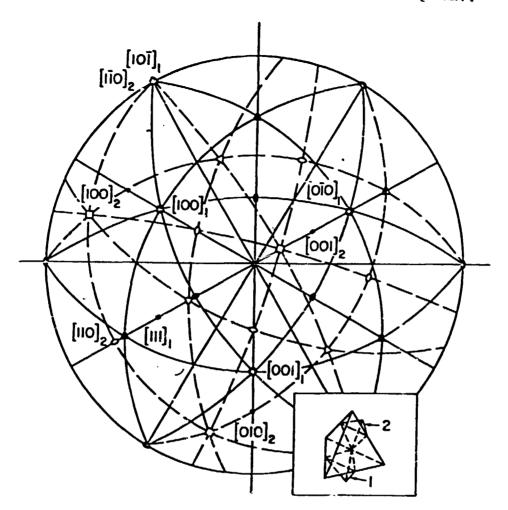




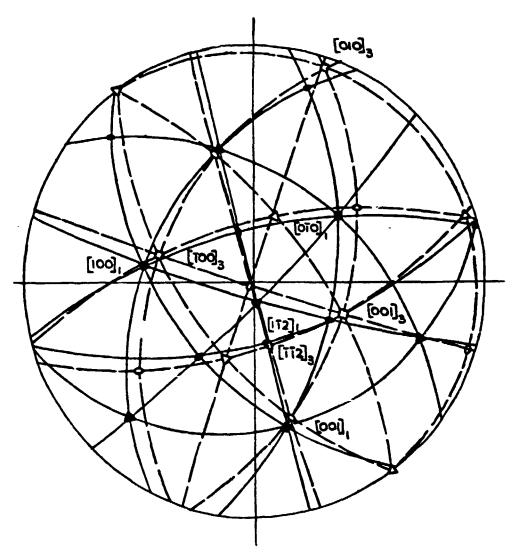




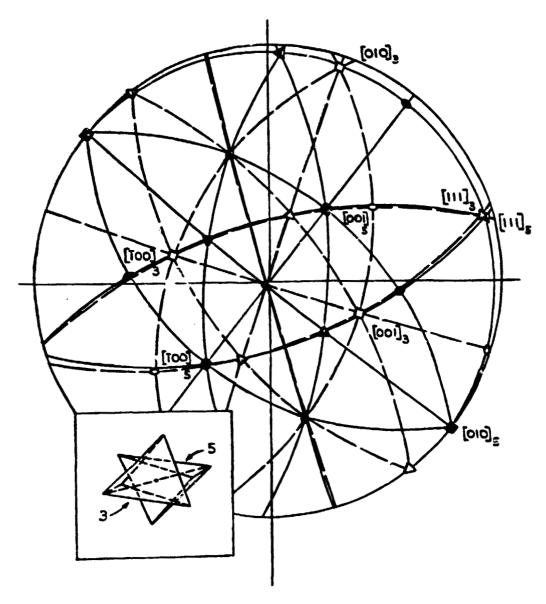
ORIENTATIONS OF GRAINS 1 and 2 IN SAMPLE SEMICRYSTALLINE MATERIAL



Second Order Orientation Relationship of Grains 1 and 2 in {111} Twin Geometry Relative to a Third Grain

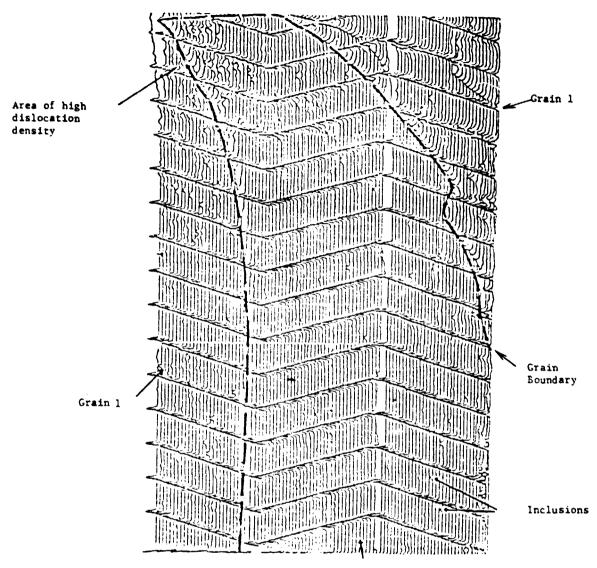


Orientation Relationship for Grains 1 and 3 of  $90^{\circ}$  Rotation About Nearly Common <112> Axes



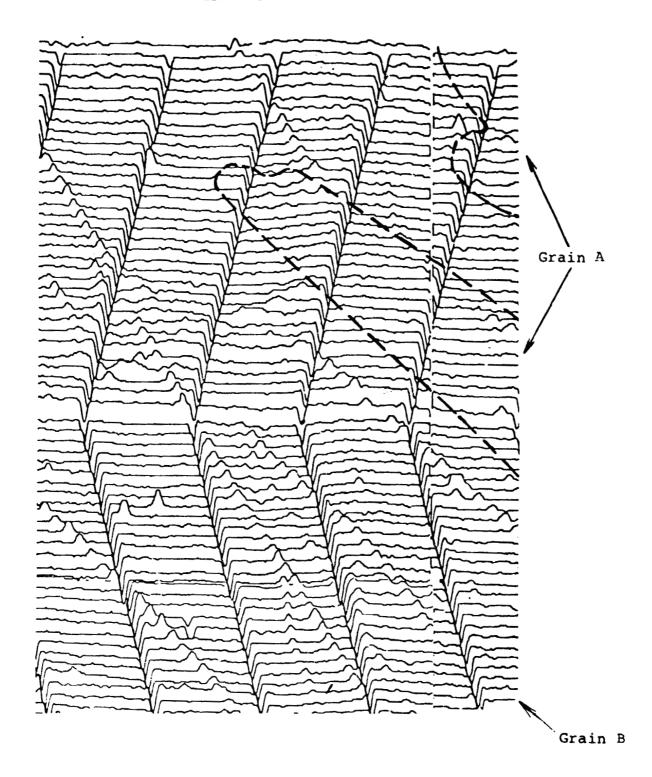
(111) Twin Orientation Relationship of Grains 3 and 5

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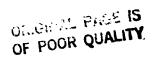
Grain 2

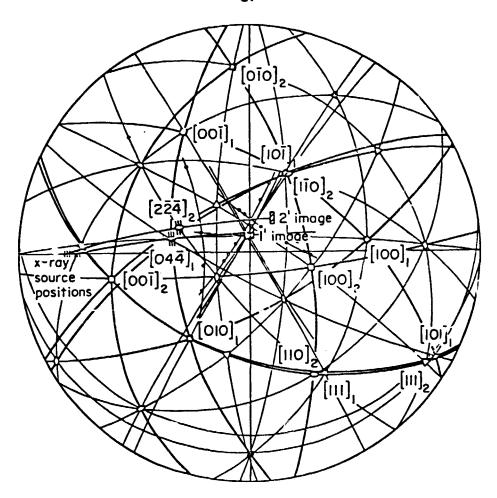
Scanning Photoresponse Pattern of an Area of a  $2\text{cm} \times 2\text{cm}$  13% AM1 Efficient Cell Showing the Location of the Grain Boundaries and an Area of High Dislocation Density



Scanning Photor(sponse Pattern of an Area of a 2cm. x 2cm. Cell, No. 4726-C3-4, Including the Location of the Electrically Inactive Grain Boundaries

Control of the second of the s





Second Order Twin Relationship of Grains , and 2 Oriented to Give  $(04\overline{4})_1$  and  $(2\overline{24})_2$  Skew Reflections

#### Conclusions

IN UCP SEMICRYSTALLINE SILICON, MOST GRAIN ORIENTATIONS APPEAR
TO BE CRYSTALLOGRAPHICALLY RELATED BY A MULTIPLE ORDER TWINHING RELATIONSHIP, AND MOST GRAIN BOUNDARY INTERFACES ARE CRYSTALLOGRAPHICALLY DETERMINED. AS LONG AS THE CRYSTALLOGRAPHICALLY
DETERMINED BOUNDARIES CONTAIN NO DISLOCATIONS, THE BOUNDARIES
SHOW NO DELETERIOUS ELECTRICAL BEHAVIOR.

BECAUSE OF THE LARGE GRAIN SIZE OF THIS MATERIAL, AND THE LOW DENSITY OF NON-CRYSTALLOGRAPHICALLY RELATED BOUNDARIES, GRAIN BOUNDARIES HAVE A MINIMAL EFFECT ON THE PHOTOVOLTAIC PROPERTIES OF SEMICRYSTALLINE SILICON.

MINIMIZING INTERNAL GRAIN DEFECTS THEM BECOMES THE KEY TO HIGH WAFER QUALITY.

THE INTERNAL GRAIN ORDER IS AFFECTED BY MANY FACTORS INCLUD-ING:

INCLUSIONS
INDIVIDUAL DISLOCATIONS
IMPURITIES
DISLOCATION SUBGRAIN BOUNDARIES

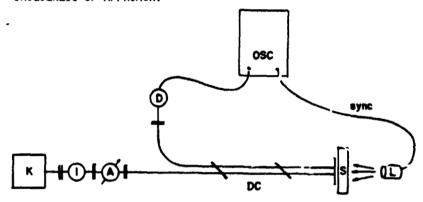
Occasionally, the large crystal will develop a subgrain defect structure. This structure is comprised of numerous subgrains that have grain diameters on the order of one millimeter or less and appear to be rotated by  $5^{\circ}$  -  $7^{\circ}$  about specific crystallographic directions such as a  $\langle 110 \rangle$  axis.

# Determination of Lifetimes in Semicrystailine 😂

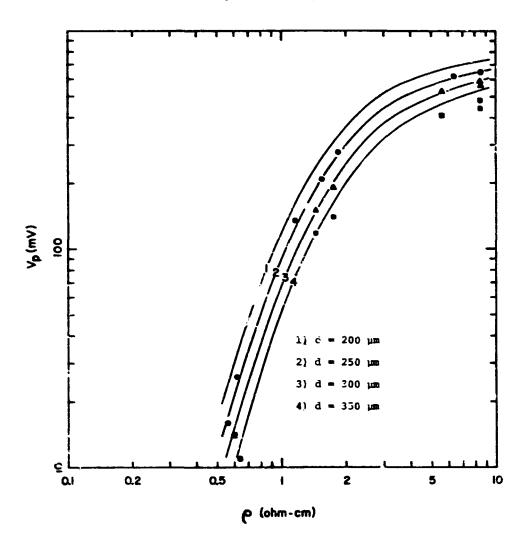
#### PURPOSE:

DEVELOP A CONTACTLESS TECHNIQUE FOR THE MEASUREMENT OF CARRIER LIFETIMES IN SEMICRYSTALLING MATERIAL.

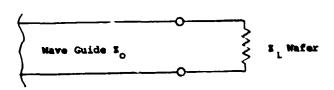
#### UNIQUENESS OF APPROACH:



# Variation in Measured Response vs Base Resistivity and Sample Thickness



### **Theoretical Model**



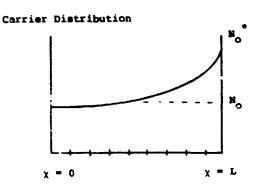
#### ASSUMPTIONS

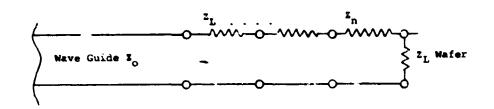
High Conductivity Limit

O >> we Exponential Carrier Distribution No Diffusion of Carriers No Surface Recombination Velocity Carriers Decay Exponentially with Time

$$N(t) = N_0^0 e^{-t/\tau}$$

### **Transmission-Line Model**





Reflection Coefficient

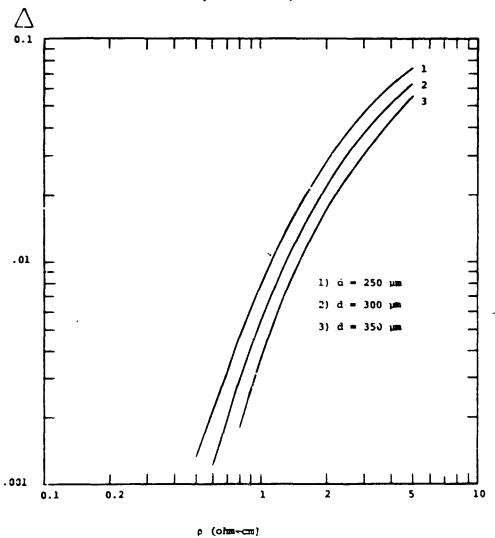
$$R = \frac{z_L - z_O}{z_L \cdot z_O} ; Rec N_O + N_O^*$$

Reflected Power

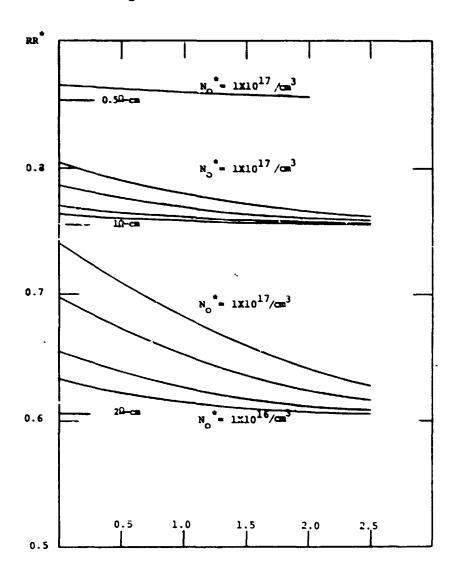
$$F_{M} = RR^{\bullet} \propto V_{M}$$

Wormalized Modulation

### Normalized Modulation Calculated vs Base Resistivity and Sample Thickness

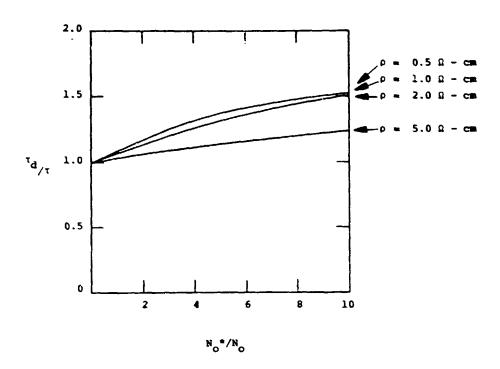


# Change in Reflected Power With Time



TIME (t)

## Variation in Measured Decay Time vs Base Resistivity and Generated Carrier Concentration



### Conclusions

THIS IS A RELIABLE TECHNIQUE FOR THE CHARACTERIZATION OF SEMI-CRYSTALLINE MATERIAL. THE MODEL ACCURATELY PREDICTS THE OB-SERVED BEHAVIOR ASSOCIATED WITH CHANGES IN BASE RESISTIVITY AND SUBSTANTIATES THE EMPIRICALLY OBSERVED BEHAVIOR FOR THE PREDICTION OF CAMPIER LIFETIMES.

SURFACE PASSIVATION IS NECESSARY TO OBTAIN CONSISTENT AND MEAN-INGFUL RESULTS.

THE MEASURED DECAY TIME IS SOME MULTIPLE OF THE CARRIER LIFETIME, DEPENDENT UPON THE:

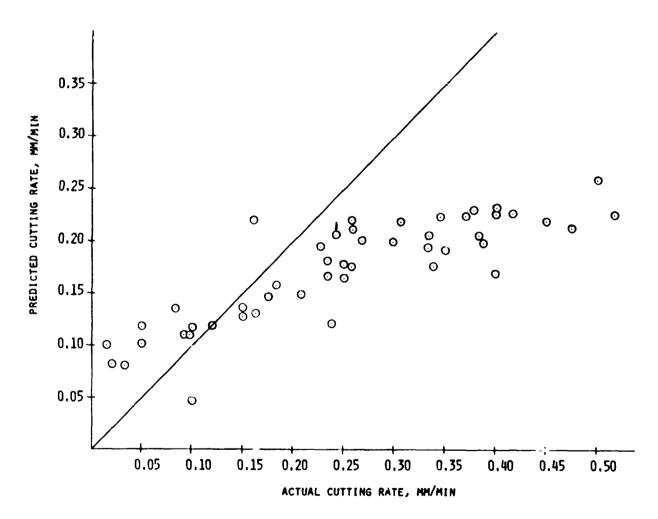
SAMPLE THICKNESS
BASE RESISTIVITY
ILLUMINATION INTENSITY

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## Wafering Mechanisms

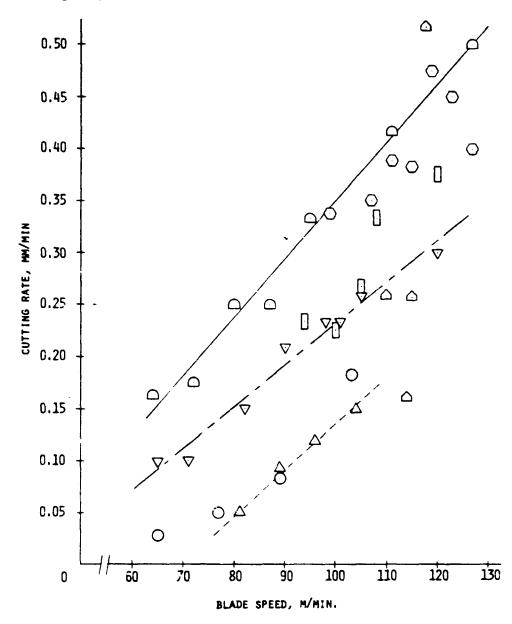
PURPOSE: TO DETERMINE IF THE HSMBS WAFERING TECHNOLOGY IS A VIABLE METHOD FOR THE ECONOMICAL PRODUCTION OF SHEET SILICON FOR PHOTOVOLTAICS.

**High-Speed MBS Saw** 

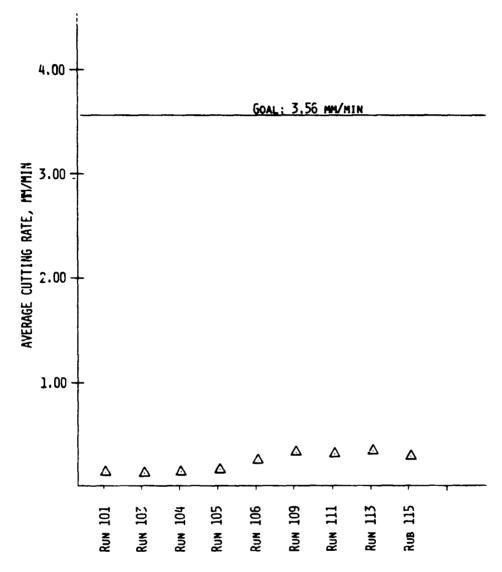




# High-Speed MBS Saw: Cutting Rate vs Blade Speed



High-Speed MBS Saw: Average Cutting Rates (Complete Runs Only)



### **Conclusions**

WITH THE HIGH MATERIALS COST ASSOCIATED WITH THE MBS TECHNOLOGY A CUTTING RATE OF 1M2/HR. IS NECESSARY.

BASED UPON THE RESEARCH PERFORMED THUS FAR, IT WOULD BE NECESSARY TO SUSTAIN A CUTTING RATE OF 3.5 MM/MIN.

THE CURRENT TECHNOLOGY IS NOT CAPABLE OF MEETING THIS CRITERIA.

## ADVANCED CZOCHRALSKI INGOT GROWTH

KAYEX CORP.

ADVANCED CZOCHRALSKI INGOT GROWTH

KAYEX CORPORATION APRIL 22, 1982

GOALS:

GROWTH OF 150 KG OF INGOTS FROM ONE CRUCIBLE USING PERIODIC MELT THIS CONTRACT REPLENISHMENT

DIAMETER 15 CM

THROUGHPUT - 2.5 KG/HR

RECHARGE MELTING RATE 25 KG/HR

AFTER-GROWTH YIELD 90%

**IMPROVED SENSORS FOR:** MELT TEMPERATURE

DIAMETER MELT LEVEL

PROTOTYPE EQUIPMENT FOR HIGH VOLUME JPL MOD 2000 → CG6000

PRODUCTION, TRANSFERABLE TO INDUSTRY

STATUS:

ONE 150 KG RUN PERFORMED DURING

**ACHIEVED** 

1.46 KG/HR, 150 KG RUN

14.3 KG/HR

ACHIEVED; 52% MONO, BALANCE POLY

MICROPROCESSOR CONTROLS PLUS CONSTRUCTED, INTERFACED & DEMONSTRATED

RLL 4/22/82

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ADVANC	ED)	<b>CZOCHRALSKI</b>
INGOT	GRO	WTH

KAYEX CORPORATION APRIL 22, 1982

### APPROACH:

CONSTRUCT AN IMPROVED CRYSTAL GROWER HAVING THE PERFORMANCE REQUIRED TO ACHIEVE GOALS

CONSTRUCT AN AUTOMATED SYSTEM WHICH WILL OFFER RELIABLE PERFORMANCE LEADING TO IMPROVED YIELDS AND REDUCED LABOR COST

CONDUCT PROCESS DEVELOPMENT ON LARGE SIZE CRYSTAL GROWTH, MELT REPLENISHMENT AND IMPROVED THROUGHPUT AND YIELDS

CONDUCT PARALLLL ANALYTICAL PROGRAM
TO HELP UNDERSTAND THE PROCESS

### STATUS:

INGOT SIZE ACHIEVED, BUT NOT THROUGHPU:

SYSTEM OPERATIONAL - INSUFFICIENT DATA TO CONFIRM YIELD & LABOR

INGOT SIZE 6" DIA x 37-1/2 KG ACHIEVED THROUGHPUT BELOW TARGET

FURNACE GAS ANALYSES
CRUCIBLE DEVITRIF, CATION STUDY
SOLAR CELL FAB AND TEST

RLL 4/22/82

# Program Plan, Revision 2

Advanced Csochraleki Growth For Technology Readiness	1980-> <1981										Reyal Corporation Optil 21, 1981									
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## Program Plan

THE PROGRAM PLAN CONSISTS OF, FIRST, A CONSTRUCTION PHASE, WHICH WAS COMPLETED IN THE FIRST FIVE MONTHS.

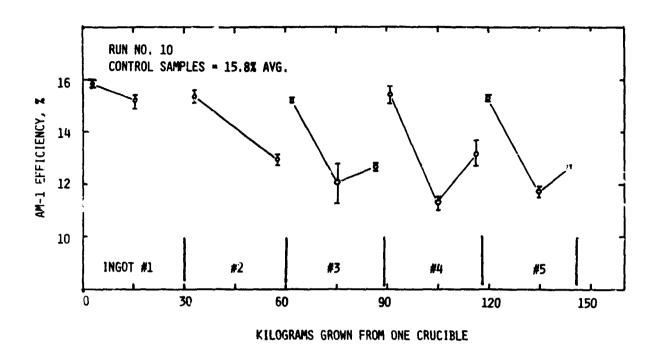
A PARALLEL SENSOR DEVELOPMENT PROGRAM WAS CARRIED OUT INITIALLY ON A SECOND COMMERCIAL MACHINE AND, SUBSEQUENTLY, THE SENSORS WERE INTERFACED TO THE JPL FACILITY.

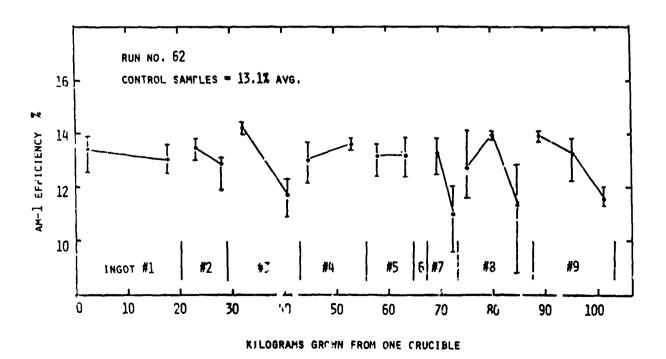
FOR A PERIOD OF TIME IN LATE 1981, VERY LITTLE EFFORT WAS EXPENDED, EXCEPT FOR THE CONTINUED DEVELOPMENT OF THE GAS ANALYSIS SYSTEM.

FOR THE LAST SEVERAL MONTHS, THE EFFORT WAS REDIRECTED THROUGH A TDM TO EMPHASIZE PROCESS UNDERSTANDING RATHER THAN EXTENSIVE DEMONSTRATION OF 150 KG RUNS.

THE EXPERIMENTAL WORK IS NOW COMPLETE AND THE FINAL DOCUMENTATION IS IN PROCESS.

## Solar Efficiency vs Kilograms Grown





ADVANCED	CZGCHRALSKI

INGOT GROWTY

KAYEX CORPORATION

DOE/JPL 955733

### PROBLEMS - CONCERNS

### PROBLEM AREA

### <u>APPROACH</u>

- YIELD OF MONOCRYSTAL, LOWER EFFICIENCY OF POLY MATERIAL
- STUDY STRUCTURE LOSS MECHANISMS, PRIMARILY MELT CONTAMINATION
  - CRUCIBLE DISSOLUTION
  - CRUCIBLE DEVITRIFICATION
  - GAS AMBIENT PURITY & FLOW
- THROUGHPUT 'S RELATED TO RATE IMPROVE HOT ZONE DESIGN LIMITING FACTORS

- MELTING RATE

- FURTHER WORK WITH RADIATION SHIELDING

- CORKSCREWING
- TEMPERATURE PROFILING OF MELT
- STABILIZATION OF MELT TEMPERATURE IMPROVED TUNING OF MICROPROCES-SOR TO SPEED UP STABILIZATION, SEEDING AND NECKING

### ADVANCED CZOCHRALSKI ENERGY DISPERSIVE X-RAY ANALYSIS OF ROSETTE DEFECTS ON INNER SURFACE OF USED CRUCIBLE

1. COMPOSITION AT RIM OF DEFECT

	ATOMIC			
	WEIGHT	ATOMIC	OXIDE	OXIDE
ELEMENT	PERCENT	<u>PERCENT</u>	FORMULA	PERCENT
12	87.39	89.92	\$102	91.53
S	1.97	1.78	SO₃¯	2,52
CL	6.15	5.01	CL	3.13
K	2.91	2,15	K <sub>2</sub> 0	1.75
CA	1.58	1.14	CÃO	1.09

2. COMPOSITION OF CENTER OF DEFECT AND BULK SIO2 GLASS CONTAINED NO DETECTABLE IMPURITIES.

RLL 4/21/82

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# CO and H<sub>2</sub> vs Run Time

IN AN ATTEMPT TO UNDERSTAND THE MECHANISM OF STRUCTURE LOSS, WE HAVE CONSTRUCTED A DEVICE WHICH SAMPLES AND ANALYZES THE GROWER EXHAUST GAS FOR CARBON MONOXIDE, HYDROGEN, AND WATER. IF CARBON IS CONTAMINATING THE MELT, IT WILL BE CONCENTRATED IN THE RESIDUAL MELT AND COULD LEAD SUBSEQUENTLY TO SILICON CARBIDE PRECIPITATION, AS MORE AND MORE CRYSTALS ARE GROWN.

CARBON MONOXIDE HAS BEEN FOUND IN SURPRISINGLY HIGH CONCENTRATIONS, AND IS A FUNCTION OF TEMPERATURE. APPROXIMATELY 5000 PPM ARE SEEN DURING MELTDOWN.

# **MATERIAL CHARACTERIZATION**

## **CORNELL UNIVERSITY**

TECHNOLOGY	REPORT DATE
LARGE AREA SILICON SHEET - ANALYSIS	April 17, 1982
APPROACH  Optical Microscopy and Etching. Transmission Electron Microscopy Electron beam Induced Current Microscopy Cherical Analysis (e, ion, neutron, mass spec). Cornell University/Material Science  GOALS Characterize structure and chemical composition of point, line and planar defects in un-processed LASS material. Characterize structure and chemical composition of point, line and planar defects in processed LASS material. Evaluate crystal growth/defect relation Evaluate processing/defect relation.	STATUS  EFG  TEN and STEM analysis of defects in processed EFG completed. Chemical make up of large precipitates identified.  WEB  RT EBIC of processed WEB completed.  Temperature dependent EBIC being carried out to determine local energy levels.  Rutherford backscattering completed.  HEM  Optical Microscopy and etching completed EBIC completed.  NEW ANALYTICAL TOOLS ADDED SINCE LAST PII  1) JEOL 200 CX STEM with EDX 2) Temperature dependent EBIC 3) General Ionix Accelerator for back-scattering analysis.

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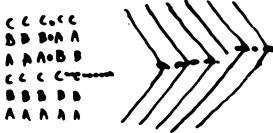
### **Coherent Twins**

- 60° rotation on (111) plane
   perfect first nearest neighbor fit
- Periodicity of threeSIGMA 3 boundary
- Small deviations from ideal twin are accommodated by DSC dislocations

b = (a/6) 112

These dislocations are the analogue of complete dislocations in small angle grain boundaries.

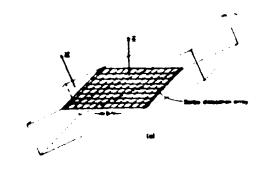
- Dislocations are necessarily associated with a step in the boundary
  - presents possibility to study effects of jogs.



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## **Twist Boundaries**

Network of screw dislocations



On (111) dislocations react to form hexagonal networks - low angle - twin relation.

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Horestra, J. 1959

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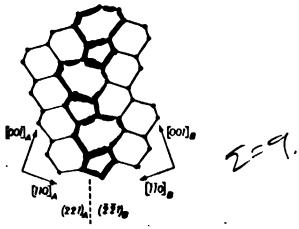


Fig. 6. Symmetrical tilt boundary with  $\theta_1 = 38^{\circ}57'$  and zig-zag arrangement of dislocations.

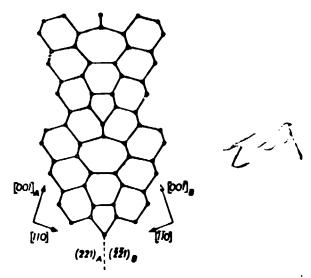
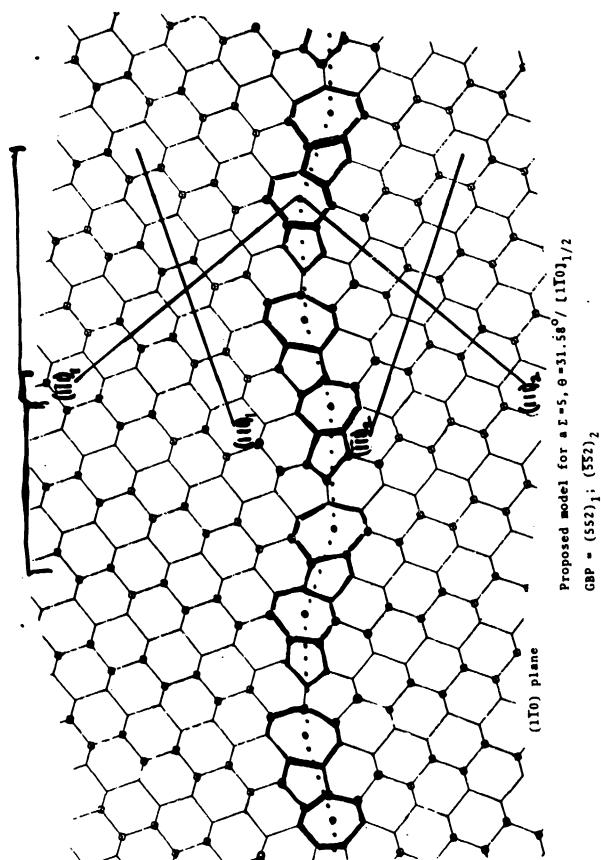


Fig. 7. As Fig. 6 but with overlapping dislocations, thus forming double dislocations.

For  $(\theta_1 = 31^\circ 35' = \arccos 23/27)$  the model in Thus



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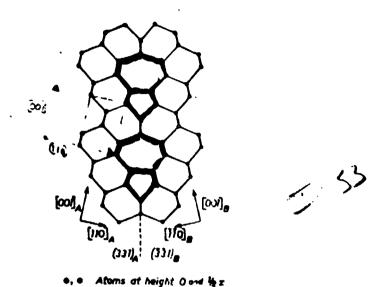
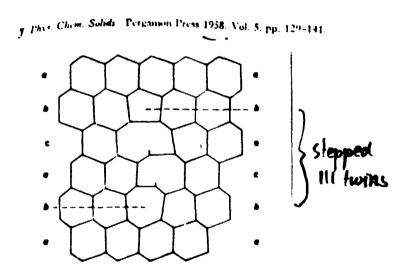


Fig. 5. Projection on ( $\overline{110}_{1}$  of a symmetrical tilt boundary with tilt axis [110], angle of tilt  $\theta_1 = 26^{\circ}32'$  and median plane (110). The height of the atoms above the plane of projection is expressed in  $z = \frac{1}{2}a\sqrt{2}$ , where a is the lattice constant.



### 8. DISLOCATIONS AND TWIN BOUNDARIES

As has been shown in Fig. 13(c), a shift of the twin boundary involves a partial dislocation. A shift of one (double) atomic plane involves a partial of type I, a shift of two planes one of type II, a shift of the. planes, however, involves a lattice defect of a different kind. The possible structure of it is shown in Fig. 19(a) for the diamond lattice and in Fig. 19(b) for the f.c.c. lattice. It is no dislocation as its Burgers vector is zero.

### Summary

### SIGMA = 3

- o BOUNDARY PER SE NOT ELECTRICALLY ACTIVE
- o ELECTRICAL ACTIVITY CORRELATES WITH PRESENCE OF PARTIAL DISLOCATIONS.
- o PARTIAL DISLOCATIONS SHOW ENHANCED ACTIVITY
  COMPATIBLE WITH JOG MODEL
- o EVIDENCE FOR KINK ACTIVITY FROM CURVED PARTIALS.

#### SIGMA - 9

- o 111/115 TWIN SHARES HABIT PLANE WITH FIRST ORDER TWIN - FREQUENTLY MIS-IDENTIFIED AS THE LATTER.
- o ELECTRICAL ACTIVITY COMPATIBLE WITH BROKEN BOND MODEL.
- ALTERNATING SECTIONS GIVE DOT-LIKE EBIC CONTRAST
   SIMILAR TO PARTIAL DISLOCATIONS IN FIRST ORDER TWINS.

### SIGMA - 27

- o CHARACTER OF BOUNDARY DEPENDS ON BOUNDARY PLANE VARIES OVER SHORT DISTANCES ( 0.1 um ).
- UNSYMMETRIC GBP CORRELATED TO DISSOCIATED BOUNDARIES: SIGMA27 - SIGMA9 • SIGMA 3
- o MICROFACETTING IN ACCORDANCE WITH HORNSTRA.
- o UNDISSOCIATED BOUNDARY ON SYMMETRIC GBP HAS STRUCTURE OF 5 and 7 MEMBERED RINGS SHOULD LEAD TO GAP STATES.

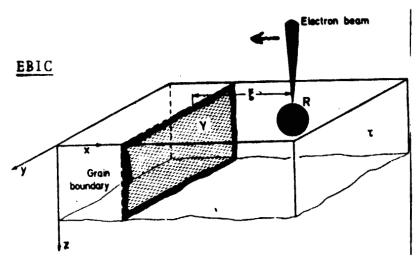
### Summary of Sigma = 27

- Undissociated 255/255 is symmetric.
   and located on second highest density
   CSL (highest 115/115)
- O Dissociated section is un-symmetric.

  Components: Symmetric SIGMA 9 112/112

  (2 nd highest after 111/115)
- o Largest facet is SIGMA 3 111/111 coherent twin
- o Other facet probably 111/115
- o 3 Step periodicity correlated to stacking sequence - Hornstra model of atomistic faceting. (Brockman).

## **Techniques**

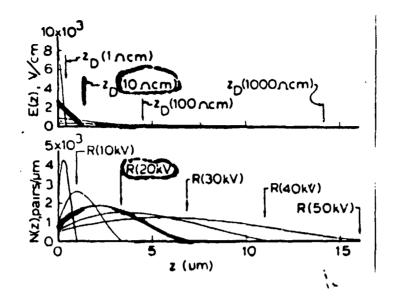


EBIC contrast of grain boundaries can be calculated by solving the 3-D diffusion equation under the following assumptions (J.Marek)

- o combination velocity at the boundary plane
- o  $R_{p}$  depletion layer thickness.

Typical operation conditions for 10 cm Si

Maximum contrast when  $R_p \simeq L$ .

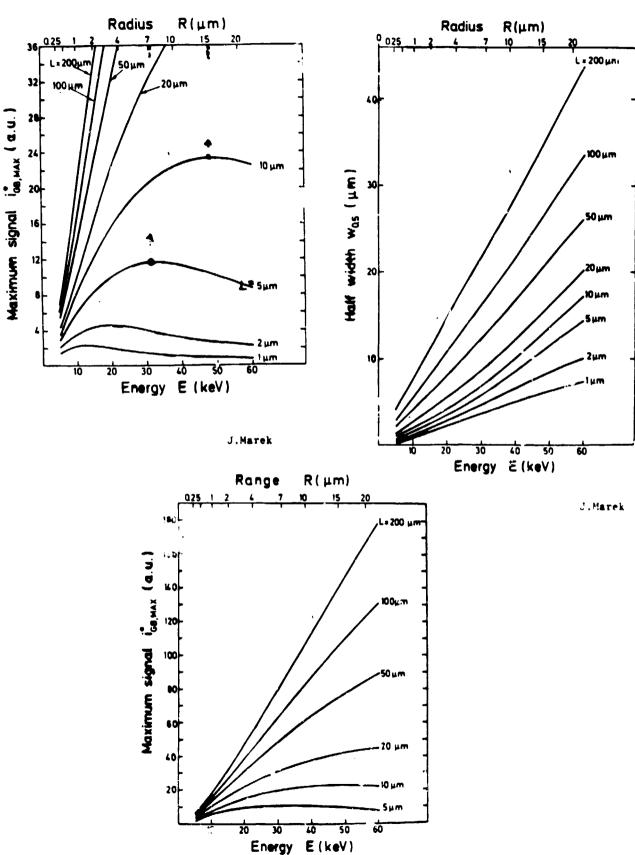


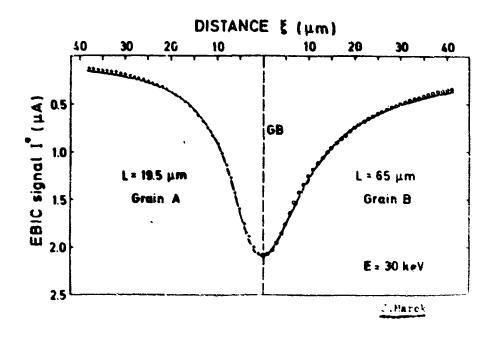
After Leamy et al.

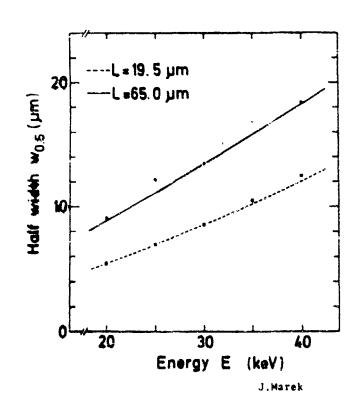
R = & E 1.75

Recent to such as indicated above.

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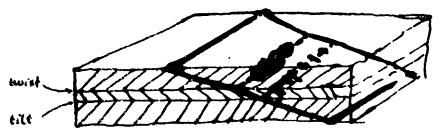






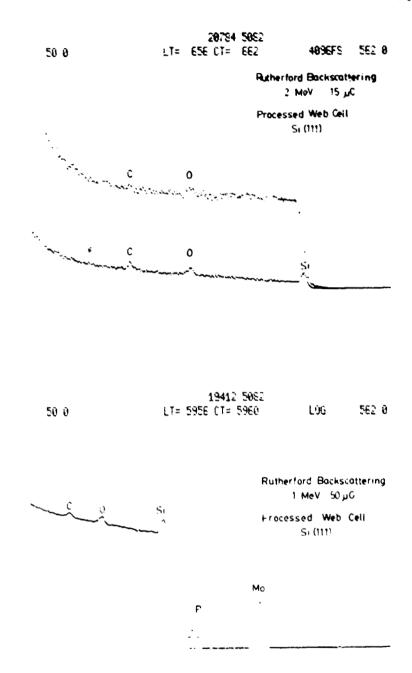
### Web

O Contains one or several twin planes in center plane of ribbon



- O Shallow bevel allows EBIC imaging of dislocation network on these twins
- O Rotational misfit of seconds of arc results in sufficiently large spacing to be resolved by EBIC.

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### **Problems and Concerns**

### • Statistics of Results .

Time and manpower restrictions confine analysis to a few specimen of a given material. Thus, some caution must be exercised when applying results to the population as a whole, especially for materials in which the crystal growth and processing techniques are continuously refined.

## **GRAIN BOUNDARY INVESTIGATION**

### **JET PROPULSION LABORATORY**

L.J. Cheng

**Participants** 

LI-JEN CHENG

**GERRY CROTTY** 

TAHER DAUD

KATHY DUMAS

**SANDY HYLAND** 

TOM MacCONNELL

RINDGE SHIMA

CHIN-MIIN SHYU

KATE STIKA

## **Objective**

TO DEVELOP BETTER POLYCRYSTALLINE SILICON SOLAR CELLS
THROUGH BETTER UNDERSTANDING OF THE BEHAVIOR OF GRAIN
BOUNDARIES IN SILICON

## **Approach**

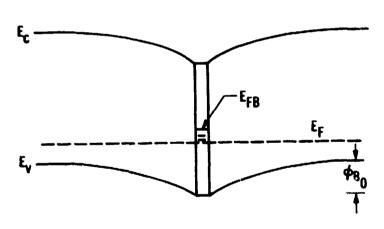
### EXPERIMENTAL STUDIES ON SAMPLES OF

- LARGE GRAIN SILICON INGOTS (WACKER, SEMIX, AND HEM)
- CZ BICRYSTALS WITH CONTROLLED LATTICE MISMATCH

## **Subjects Under Study**

- BICRYSTAL GROWTH
- ELECTRONIC TRANSPORT PHENOMENA
  - . POTENTIAL BARRILR
  - CARRIER RECOMBINATION
  - TRAPPING STATES
- ATOMIC TRANSPORT PHENOMENA
  - ENHANCED DIFFUSION OF IMPURITIES
  - IMPURITY GETTERING
- EFFECTS ON SOLAR CELL PERFORMANCE

# Energy-Band Diagram at Boundary Region for p-Type Si



$$\phi_{B_0} = E_A + T \frac{\partial \phi_{B_0}}{\partial T}$$

$$\phi_{B_0} = \frac{eQ^2}{8 \epsilon_0 \epsilon N_A}$$

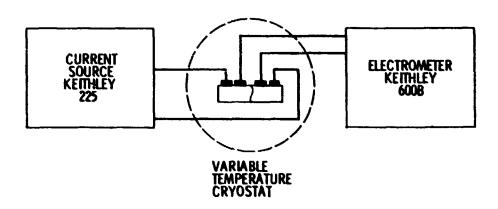
$$\phi_{B_0} = \frac{eQ^2}{8\epsilon_0 \in N_A}$$

$$Q = \frac{\epsilon_0 \in N_A}{C_0}$$

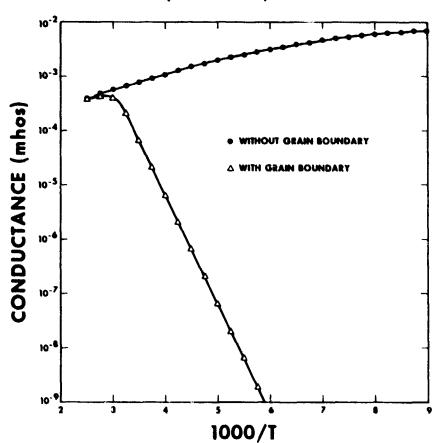
$$Q = \frac{\epsilon_0 \in N_A}{C_0}$$

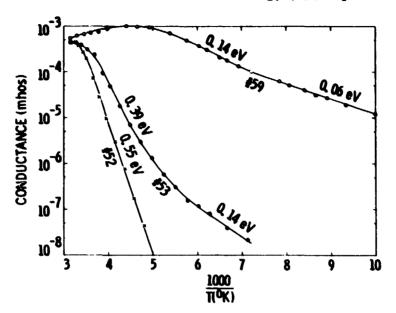
$$Q = \int_{E_{FB}}^{E_F} d(E, \sigma) dE$$

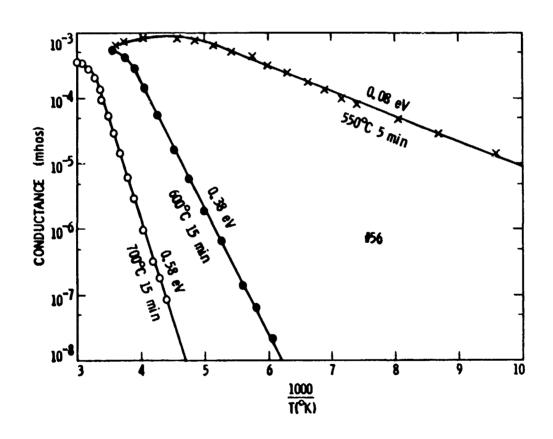
# Experimental Arrangement for Zero-Bias Conductance Measurements



## **Temperature Dependence**

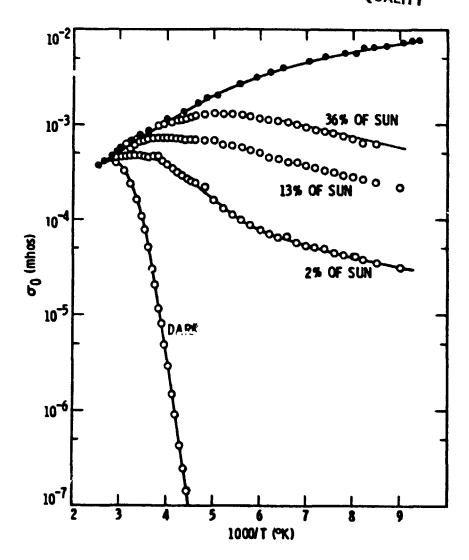






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### LARGE-AREA SILICON SHEET TASK

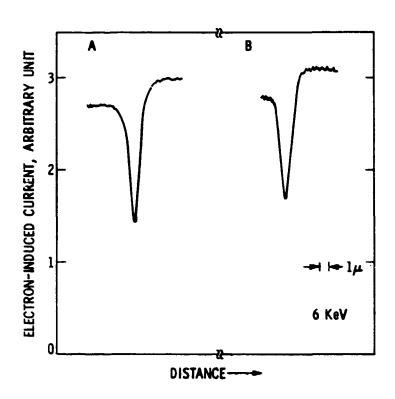


**Potential Barrier** 

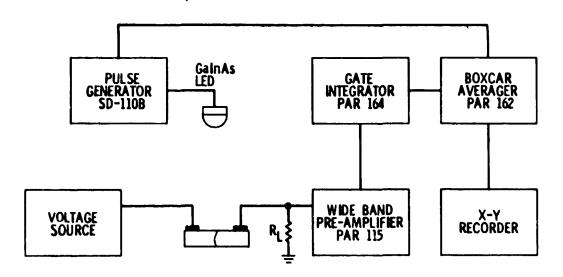
### **RESULTS:**

- CONSIDERABLE VARIATION IN EA ALONG GRAIN BOUNDARIES, PRESUMABLY DUE TO VARIATION OF LOCAL DISORDERS
- INCREASE OF EA WITH ANNEALING TEMPERATURE, LIKELY DUE TO LOCAL DEFECT CHANGES AND IMPURITY GETTERING
- ullet DECREASE OF  $\phi_B$  WITH LIGHT INTENSITY, CAUSED BY MINORITY CARRIER TRAPPING

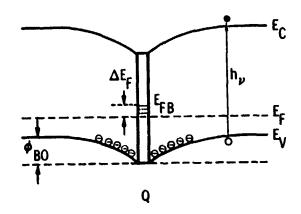
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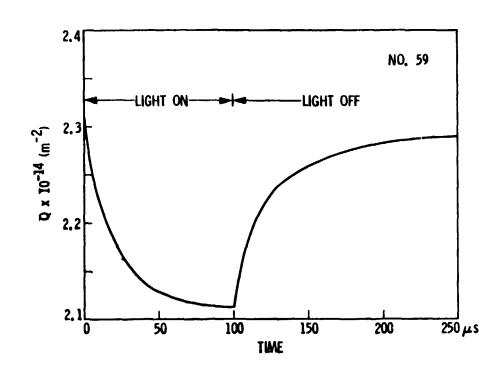
# **Experimental Arrangement for Photoconductivity Measurements**



# Light Effects on Grain Boundary Properties



- DECREASE OF Q
- INCREASE OF GO
- CREATION OF CARRIER RECOMBINATION CURRENT



### UNDER ILLUMINATION.

$$\frac{dQ}{dt}$$
 -  $J_{maj}$  -  $J_{min}$ 

### AND, IN THE DARK AFTER THE LIGHT IS OFF,

$$\frac{dQ}{dt} - j_{maj}$$

### WHERE

$$J_{\text{maj}} = (2cA - B) \exp(-(E_F + \phi_{B0})/kT)$$

$$J_{\text{min}} = \frac{D_e}{e L_e} (n_{\infty} - n_0)$$

### RECOMBINATION VELOCITY AT THE GRAIN BOUNDARY

## **Electrical Properties of Grain Boundaries**

Sample No.	Ea (eV)	$\frac{G_0}{(mho/m^2)}$	<b>∮</b> 80 (e¥)	Q (/m²)	I*	S (m/s)
51	0.55	5.98x10 <sup>2</sup>	0.12	5.66x10 <sup>14</sup>	0.661	2.5
					I	6.4
59	0.10	2.45x10 <sup>3</sup>	0.02	2.22x10 <sup>14</sup>	1	0.88
					1.81	1.09

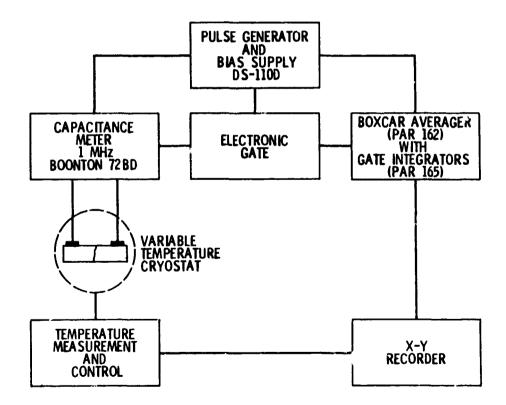
 $<sup>^{\</sup>pm}I$  = Light intensity which creates an equilibrium minority carrier density of  $1.08 \times 10^{18}$  electrons/m  $^3$  in the bulk of the sample.

## **Recombination Velocity**

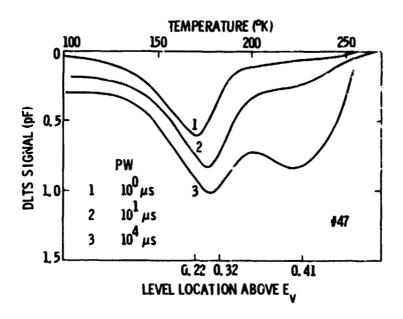
### **RESULTS:**

- DEVELOPED A TECHNIQUE USING PHOTOCONDUCTIVITY IN CONJUNCTION WITH  $\phi_{BO}$  (D) AND Q(D) MEASUREMENTS FOR THE MEASUREMENT OF MINORITY CARRIER RECOMBINATION VELOCITY AT THE GRAIN BOUNDARY
- OBSERVED INCREASES OF S WITH BOUNDARY STATE DENSITY AND LIGHT INTENSITY

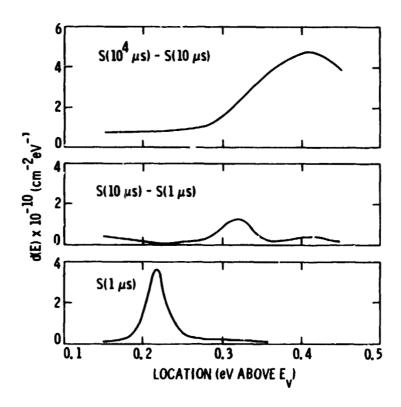
# **Experimental Arrangement for DLTS Measurements**



# Pulse Width Dependence



# Distribution of the Density of States

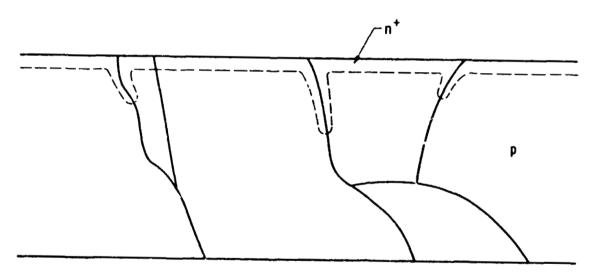


#### **Electronic States**

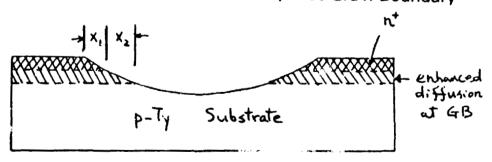
#### **RESULTS:**

- DEMONSTRATED THE APPLICATION OF DEEP LEVEL TRANSIENT SPECTROSCOPY
   (DLTS) IN THE STUDY OF ELECTRONIC STATES AT GRAIN BOUNDARIES OF SILICON
- OBSERVED A TREND THAT THE DENSITY OF GRAIN BOUNDARY STATES IS
   GENERALLY INCREASING WITH THE DISTANCE FROM THE EDGES OF THE BAND
   GAP. HOWEVER, THE DETAILS VARY CONSIDERABLY FROM SAMPLE TO
   SAMPLE WHICH CAN BE ATTRIBUTED TO LOCAL VARIATION OF DISORDERS

Cross Section of Phosphorus-Diffused Polycrystalline Silicon

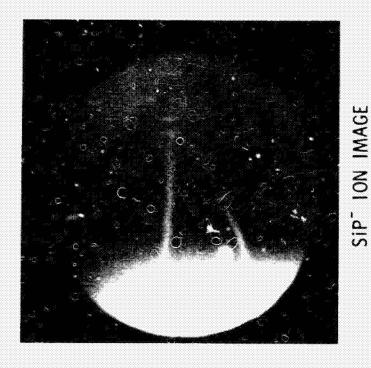


Cross Section of Grooved Sample at Grain Boundary



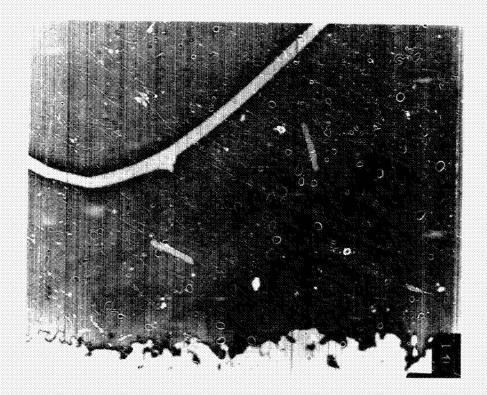
Staining !

F with light

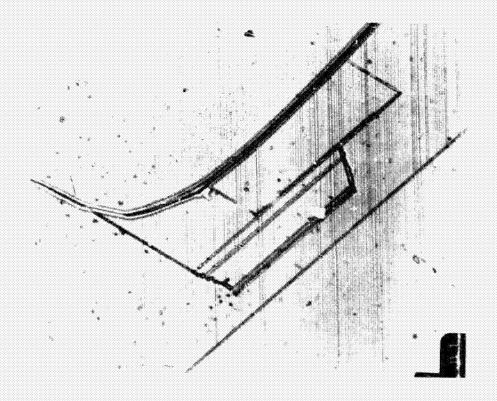


GROOVED AND STAINED

# **Grooved and Stained**

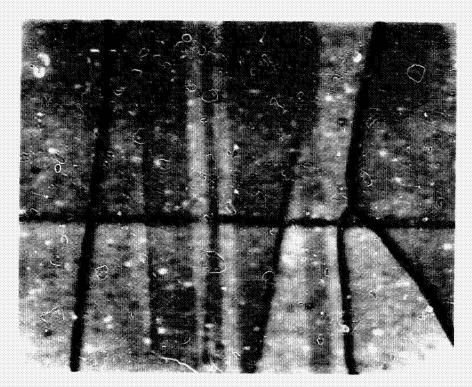


Sirtl-Etched

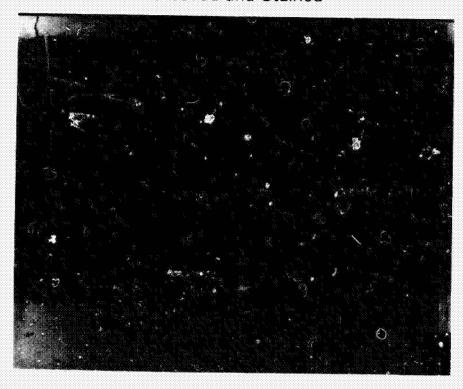


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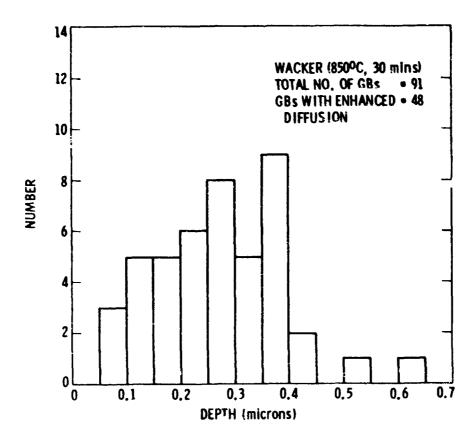
## EB!C



**Grooved and Stained** 



## Depth of Diffused Regions at Grain Boundaries



#### **Enhanced Diffusion of Phosphorus**

#### **RESULTS:**

- THE GROOVING AND STAINING TECHNIQUE IS A SUITABLE METHOD FOR THE OBSERVATION OF ENHANCED DIFFUSION OF PHOSPHOROUS AT GRAIN BOUNDARIES IN SILICON
- THE ENHANCED DIFFUSION OCCURS ONLY AT "HIGH-ORDER" GRAIN BOUNDARIES, GENERALLY ASSOCIATED WITH HIGH CARRIER RECOMBINATION
- THE DEPTH OF THE ENHANCED DIFFUSION VARIES DRASTICALLY FROM
  BOUNDARY TO BOUNDARY, WHICH MAKES THE QUANTITATIVE MEASUREMENT
  DIFFICULT UNLESS THE GRAIN BOUNDARY IS WELL CHARACTERIZED

## **Present Activities and Plans**

- DENSITY OF STATES, RECOMBINATION VELOCITY, AND BARRIER HEIGHT AS FUNCTIONS OF LATTICE MISMATCH AND PROCESS PARAMETERS (INCLUDING PASSIVATION)
- QUANTITATIVE STUDIES ON ENHANCED DIFFUSION OF PHOSPHOROUS
- IMPURITY BEHAVIOR (e.g., CARBON, AND OXYGEN)
- EFFECTS ON SOLAR CELL PERFORMANCE

# STUDY OF ABRASIVE-WEAR RATE OF SILICON

#### **UNIVERSITY OF ILLINOIS AT CHICAGO**

J. Clark D.S. Lim S. Danyluk

TECHNOLOGY	REPORT DATE
Materials Properties Modification	April 22, 1982 .
APPROACH	STATUS
An experimental program is carried out to study the fundamental mechanisms of abrasion and wear, and deformation of silicon by a single crystal diamond in various fluid environments.	The abrasion rate and depth of damage of (100) and (111) p-type silicon in three fluid environments has been determined. The surface deformation mechanism was found to change when the fluid was varied.
	The diamond geometry affects the wear rate.
CONTRACTOR University of Illnois at Chicago	There appears to be a correlation between the wear rate and the dielectric constant of the fluid. The brittle lateral crack model does
GOALS	not appear to describe the wear rates measured.
Develop a model for surface-mechanical property modification of silicon under the influences of fluid environments	

#### Introduction

Optical and scanning electron microscopy are used to determine the wear rate and deformation mechanism of diamond abrading (100) and (111) Cz silicon in water, ethanol and acetone. A multi-scratch experiment is used to determine the effects of normal force on the abrading diamond and fluid on the abrasion rate and depth of damage. These results are compared with a lateral crack model of abrasion of brittle materials.

#### Variables

Fluid, Temperature, Voltage, Photo-Irradiation, Normal Force  $(F_N)$ , Orientation, Abrasion Speed.

#### Data

Groove depth vs. variables, SEM of groove surface, depth of damage.

## **Analysis**

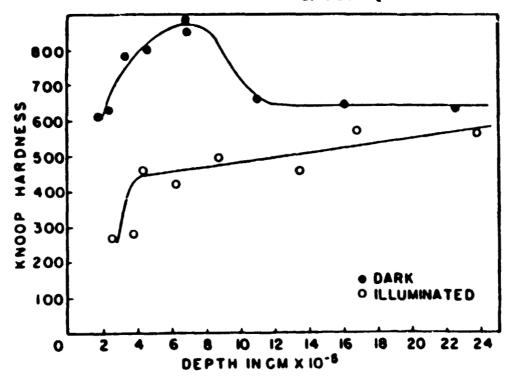
Stress analysis, depth of damage, lateral crack model.

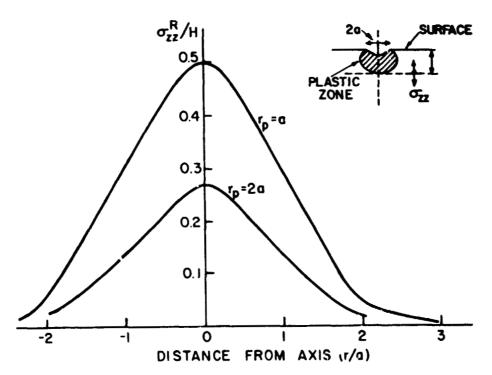
### **Summary of Results**

- 1. Wear rate varies by ~100% (acetone; ethanol; water).
- 2. Depth of damage larger for water than ethanol.
- 3. (100) and (111) wear rates are different.
- 4. Dielectric constant of the fluid related to the silicon hardness.
- 5. Lateral crack model describes wear rate when  $F_{N}$   $\stackrel{?}{\sim}$  60 g.

# Changes in Surface Hardness of Silicon

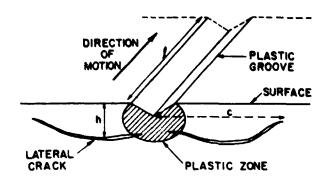
Reference	Effect	Percent Softening	Comments
Kuczynski and Hochman	Photon irradiation	70% softening	Intensity and surface preparation important; microhardness test
Ablova	H <sub>2</sub> O adsorption	Softening	Surface preparation and impurity content important; microhardness test
Westbrook and Gilman	Potential between indenter and crystal	60% softening	Disappeared at elevated temperatures; micro-hardness test
Yost and Williams	NaCl and Na <sub>4</sub> P <sub>2</sub> O <sub>7</sub>	50-80% softening depending on concentration	Zeta-potential measurements of crushed silicon
Cuthrell	CCl <sub>4</sub> and H <sub>2</sub> O adsorption	Not determined	Adsorption changed mode of drilling
This work	H <sub>2</sub> O, ethanol, acetone adsorption	Up to 70% soften- ing dependent on type of fluid and F <sub>N</sub>	Pyramid diamond scratch test

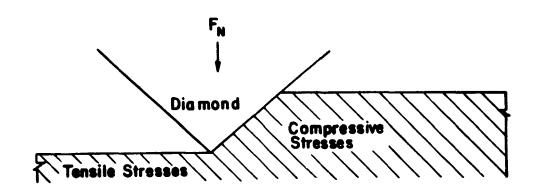


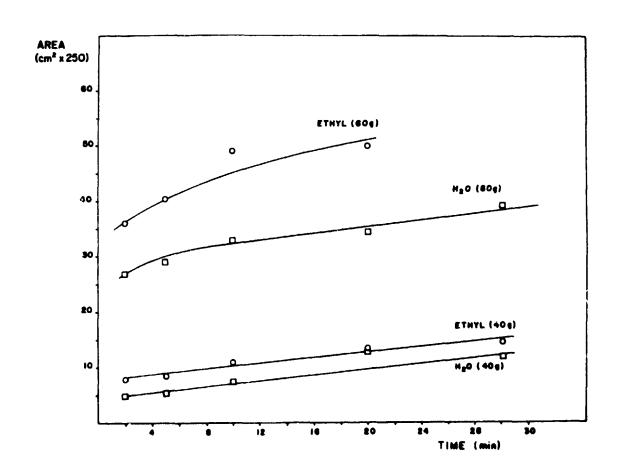


The spatial dependence of the residual tensile stress along a plane through the intersection of the plastic zone with the penetration axis: the stresses were estimated from an analytic elastic/plastic solution for a spherical cavity and an elastic solution for a half space.

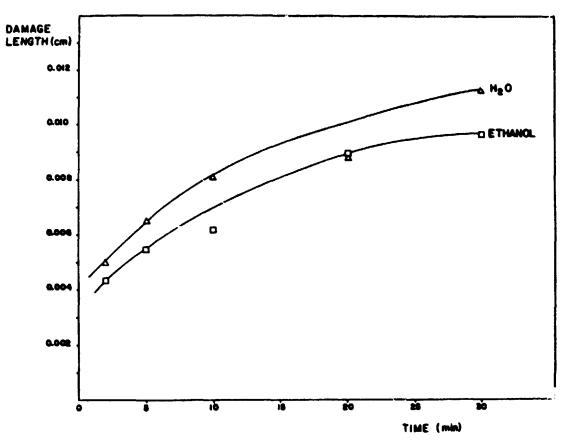
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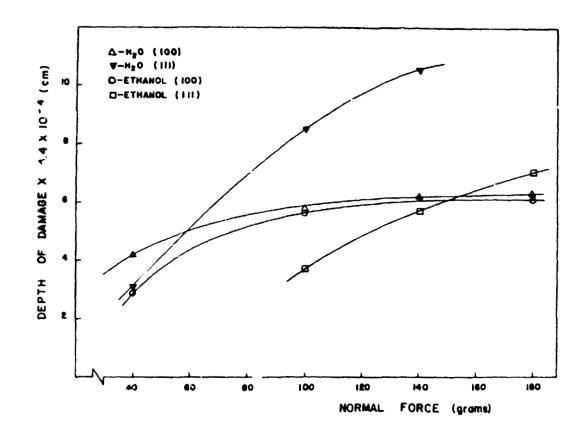


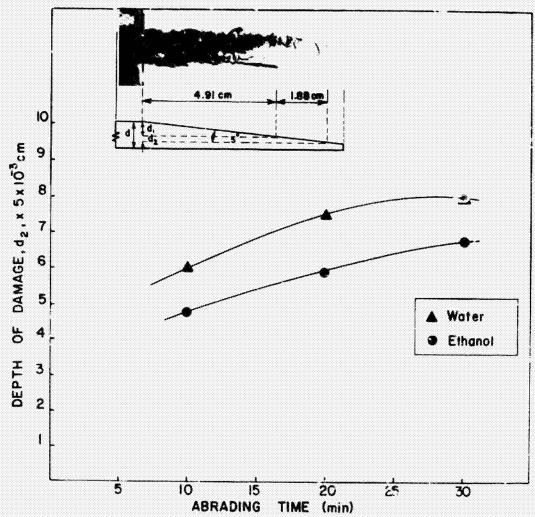


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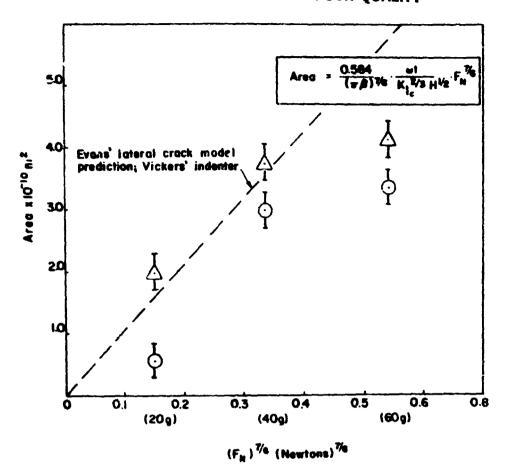


# Depth of Damage From Single Scratch Abrasion on Silicon





Depth of Damage in (100) p-Type Silicon Formed by a Diamond at Room Temperature vs Abrasion Time (min.). The Fluid Environment Was Varied. The Normal Force Was  $\rm F_N$  = 40 g.

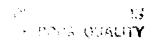


# **Problems and Concerns**

The diamond geometry changes during the abrasion experiments due to microcracking at the diamond surface.

The diamond vibration must be stabilized.

The temperature at point of contact between the diamond and the silicon is unknown.



# **SOLAR CELL FABRICATION AND ANALYSIS**

#### APPLIED SULAR ENERGY CORP.

LECHNOLOGA	ZEPORT BATE
SOLAR CELL FABRICATION & ANALYSIS	APRIL 22, 1952
APPROACH  1) FABRICATION OF SOLAR CELLS BY BASELINE  & ADVANCED PROCESSES POSSIBLY INCLUDING GETTERING AND ANNEALING.	STATUS
<ol> <li>ANALYSIS USING DAKK AND LIGHT 1-V, DIFFUSION LENGTH MEASUREMENTS, SPECTRAL RESPONSE.</li> </ol>	
CONTRACTOR APPLIED SOLAR ENERGY CORPORATION	
GOALS	
1) AN UNDERSTANDING OF THE MECHANISMS THAT LIMIT THE DEFICIENCIES OF SOLAR CELLS MADE FROM VARIOUS SILICON SHEETS.	
2' AN UNDERSTANDING OF THE EFFECT ON SOLAR CELL EFFICIENCY OF VARIATIONS IN GRONTH PARAMETERS.	

1. EFG (MOBILE TYCO)

10 CM WIDE MATERIAL GROWN WITH OR WITHOUT CO.

2. UCP (SEMIX)

HIGH EFFICIENCY PROCESS ON MATERIAL FROM INGOT 5464-13C. MORE SEVERE GETTERING ON MATERIAL FROM INGOT 5464-13C. 10 CM x 10 CM CELLS ON MATERIAL FROM RANDOM SOURCES.

3. HEM (CRYSTAL SYSTEM)
MORE SEVERE GETTERING ON MATERIAL FROM INGOTS 4141C AND
4148.

# Summary of Solar Cells Made From EFG 17-200 Series

~~~		Yoc (my)	Jsc (mA/cm)	OF (1)	(3)	REMARKS
	AVE.	495	22.5	71	7.9	
17-200-1A	S.D.	±10	<u>+</u> 1.5	<u>+4</u>	<b>+.7</b>	CO2 OFF
(4 CELLS)	RANGE	480-504	20.2-23.6	65-73	7.1-8.6	*
	AVE.	515	23.0	76	9.0	
17-200-113	S.D.	<u>+</u> 7	±1.2	<u>±1</u>	±.5	
(2 CELLS)	RANGE	510-520	22.1-23.8	75-77	8.6-9.3	
·	AVE.	529	24.2	74	9.4	1
17-200-1D	S.D.	<u>+</u> 5	±,2	<u>+</u> 3	<u>+</u> ,4	
(3 ŒLLS)	RANGE	524-534	24.0-24.3	70-76	9.0-9.7	
<del></del>	AVE.	505	22.6	73	8.3	
17-202-1C	S.D.	<u>+</u> 17	<u>+</u> 1.6	<u>+</u> 1	<u>+</u> .9	CO2 ON
(4 CELLS)	RANGE	486-516	20.8-24.2	72-74	7.4-9.2	_
	AVE.	499	21.0	73	7.7	
17-203-1D	S.D.	<u>±</u> 1	±.3	<u>±</u> 1	<u>*</u> .3	į
(5 CELT'S)	RANGE	498-500	20.8-21.?	72-74	7.5-7. <del>9</del>	
	AVE.	487	19.8	71	6.9	
17-203-1E	S.D.	±7	+1.4	<u>+4</u>	±.2	
(2 CELLS)	RANGE	482-492	18.8-20.8	68-74	6.7-7.0	
ACCUMULATIVE	AVE OF					
"CO2 ON" CELI	<b>_S</b>	508	22.4	<b>73</b>	8.4	
(13 CELLS)			j .			

C2 CONTROL	AVE.	583 ±2	27.9 ±.4	78 +1	12.6 ±.2
(4 CELLS)	RANGE	580-584	27.4-28.3	77-78	12.3-12.9

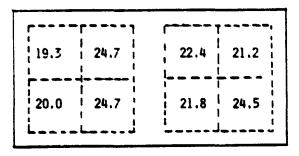
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# Summary of Solar Cells Made From 17-175 Series

		VOC (mV)	Jsc (mA/cm)	CFF (X)	(%)	REMARKS
17-175-1A-2 (7 CELLS)	AVE S.D. RANGE	519 <u>+</u> 8 504-530	21.2 <u>±</u> 1.15 19.8-22.8	72 5 62-75	7.9 <u>±</u> .8 6.4-9.0	
17-175-1A-6 (5 CELLS)	AVE S.D. RANGE	493 +34 434-518	20.1 +1.2 19.4-21.8	61 <u>+</u> 16 61-74	6.2 <u>+2</u> .1 2.7-8.3	co <sub>2</sub> off
ACCUMULATIVE A OF "CO <sub>2</sub> OFF" ( (12 CELLS)		508	20.7	67	7.2	
17-175-1E-52 (8 CELLS)	AVE S.D. RANGE	539 ±12 516-554	22.3 ±2.1 19.3-24.7	73 ±3 68-77	8.9 ±1.1 7.0-10.4	
17-175-1E-56 (6 CELLS)	AVE S.D. RANGE	505 +40.4 432-546	21.3 +2.4 17.6-22.6	59 +15 35-70	6.4 +2.2 3.4-9.1	CO <sub>2</sub> ON
ACCUMULATIVE A OF "CO <sub>2</sub> ON" CE (14 CELLS)		524	21.9	67	7.8	

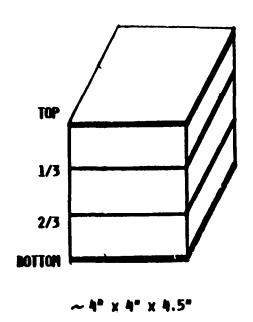
	AVE	585	28.2	75	12.4
CZ CONTROL	S.D.	<u>+</u> 2	±.6	<u>+3</u>	±.4
(4 CELLS)	RANGE	582-586	27.5-28.9	71-78	12.0-12.7

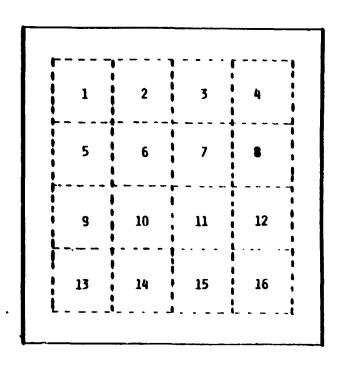
# Distribution of $J_{\text{SC}}$ on EFG Ribbon 17-175-1E-52



1 Janse free

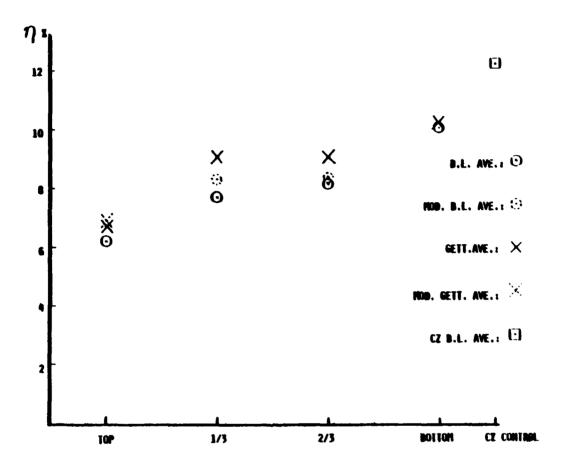
UCP Ingot No. 5848-13C





THE CELL'S # AND THEIR RELATIONS TO THE ORIENTATION OF THE QUARTER INGOT ARE MARKED

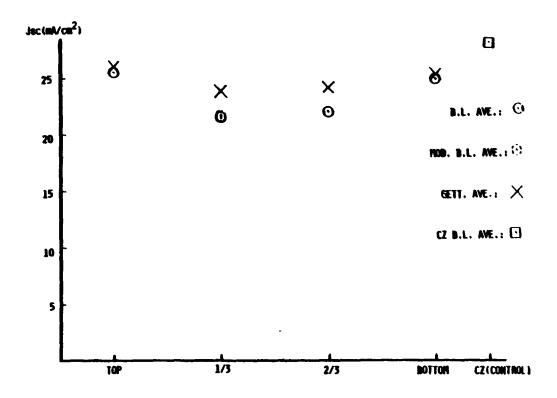
# Average Efficiency of Different Layers of Ingot 5840-13C



Summary of SJ, BSF and MLAR Cells From UCP Ingot 5848-13C

		Voc (mV)	Jac (mA/cm <sup>2</sup> )	CFF (%)	7) (%)
Evaporated AL BSF (UCP - 12 Calls)	A.V. S.D. RANGE	561 6 550-570	28.7 0.6 27.4–29.4	76 4 62-79	12.2 0.8 9.9-13.1
CZ Control (3 Cells)	A.V. S.D. RANGE	.993 1 .992-294	32.6 0.2 32.4-32.8	73 L 77-79	15.1 0.2 14.9-15.3

# Average J<sub>SC</sub> of Different Layers, Ingot 5848-18C



Summary of  $J_{SC}$  From Cells From More Severe Gettering Tests (UCP Ingot No. 5848-13C)

Gettering Treatment	Wafer	Ave. 3sc (mA/cm <sup>2</sup> )	Jsc* of The Cell Covered With SiO <sub>2</sub>
None	1/3 2/3	<b>22.5</b> 23.7	-
875 <sup>0</sup> C % Hr.	. 1/3 2/3	24.6 24.3	24.7 24.8
875 <sup>9</sup> C   Hr.	1/3 2/3	25 5 26.3	25 2 28.4
950°C I Hr.	1/3 2/3	27.0 26.3	24.8 25.9
CZ Control (No Treats	meni	28.>	
10 <b>50°</b> C 1 Hr.	1/3	26.2	25.9
CZ Control 'No Treat	nent)	28.2	

<sup>\*</sup>Jsc of the coll covered with CVD  ${\rm SiO_2}$  during gettering diffusion.

### Results of Light-Bias Minority Carrier Diffusion Length Study on Getter

PROCESS	CELLS	L <sub>Dl</sub> (, , , m) D.C. DARK	L <sub>D2</sub> ("4m) 0,05 SUN	L <sub>D3</sub> (Alm)	LD4 (AR) DARK AFTER LIGHT TURN OFF
BASELINE	2-1	11	16	17	12
8.75 <sup>0</sup> C 1/2 Hr GETTERING	2-4 2-8*	29 29	44 40	60	30
875 <sup>0</sup> C 1 HR GETTERING	2-13 2-9°	159 100	65 60	72	140
950 <sup>0</sup> C 1 HR GETTERING	2-12 2-15°	182 107	89 49	72	167
1050 <sup>0</sup> C 1 HR GETTERING	2-12 2-9°	212 135	116 62	69 81	244 117
CZ CONTROL	1	150	152	156	137

<sup>·</sup> CELLS WERE COVERED WITH S10Z DURING GETTERING DIFFUSION.

#### Summary of Results From 10 x 10 UCP Cells From Random Sources

	Voc (mV)	Jsc (mA/cm <sup>2</sup> )	CFF (%)	(%)
AVE.	553	26.9	72	10.8
S.D.	6	.9	1	۰,5
RANGE	546-558	25.2-27.6	72-74	10.0-11.3

AREA =  $98 \text{ cm}^2$  NO. OF CELLS = 6

# Comparison of J<sub>SC</sub> From HEM Cells Gettered for 1 h at 1050°C With HEM Baseline Cell From Corresponding Area

INGOT #	BASELINE JSC	GETTER JSC
41-41C	25.6	26.3
41-48	27.6	28.1