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The Snowmelt-Runoff Model (SRM) User's Manual

J. Martinec,
A. Rango,
and E. Major



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The Snowmelt-Runoff Model (SRM) User's Manual

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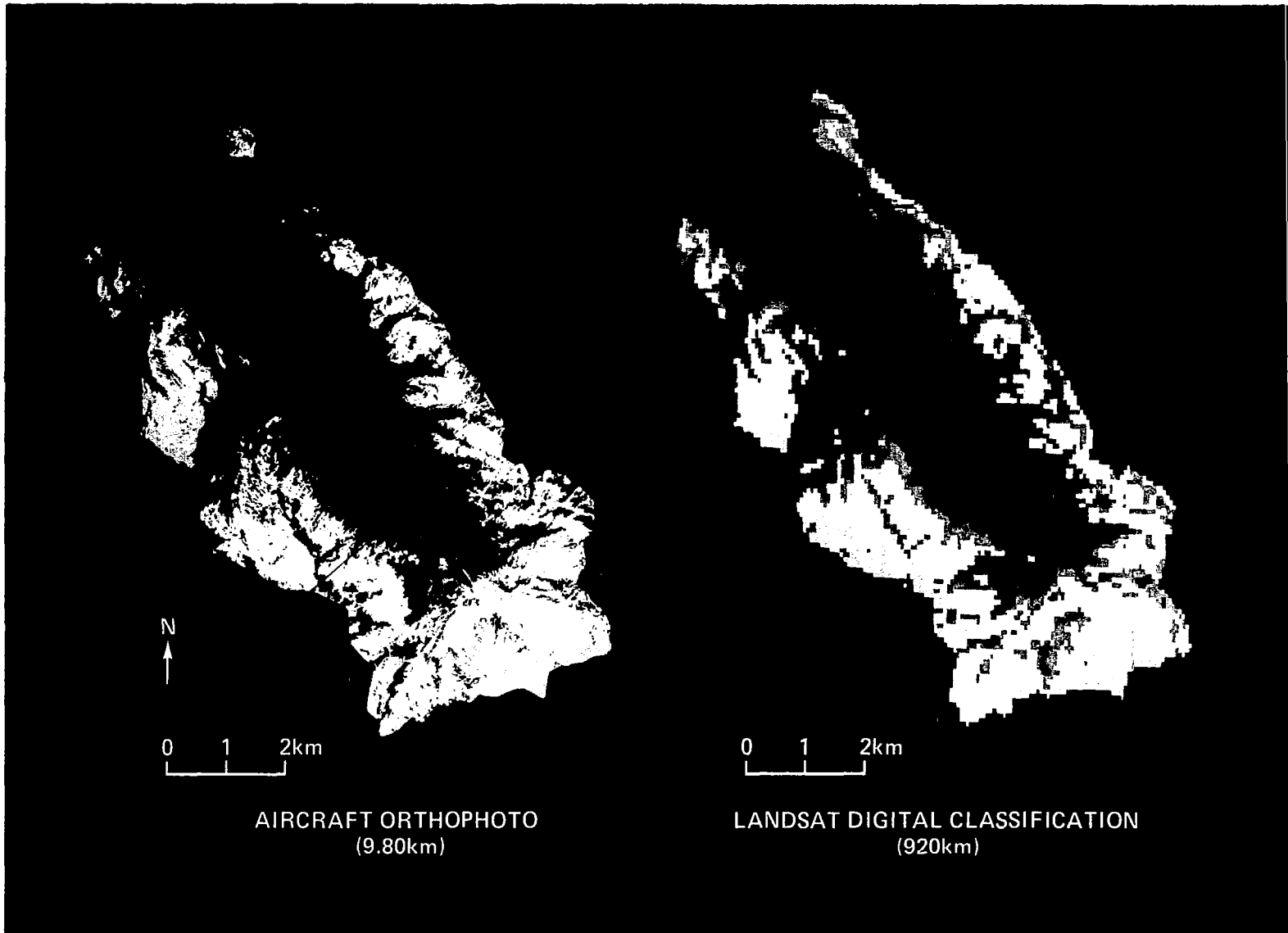
*Research and Data Systems, Inc.
Lanham, Maryland*

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Frontispiece. Comparison of snow cover in the representative basin Dischma (Swiss Alps) on 8 June 1976 from two different altitudes.

PREFACE

The purpose of this manual is to provide a means by which a user may apply the snowmelt-runoff model (SRM) unaided. To this effect, model structure, conditions of application, and data requirements, including remote sensing, are described. Guidance is given for determining various model variables and parameters. Possible sources of error are discussed and conversion of SRM from the simulation mode to the operational forecasting mode is explained. A computer program is presented for running SRM which should be easily adaptable to most systems used by water resources agencies.

In view of the variety of snowmelt conditions that may be encountered, it is not possible to foresee all situations in which the model may be applied. The authors will be glad to assist users with specific problems that may not be answered by the manual.

Special gratitude is extended to the Goddard Space Flight Center and the Federal Institute for Snow and Avalanche Research for their support of this international scientific cooperation.

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THE SNOWMELT-RUNOFF MODEL (SRM) USER'S MANUAL

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INTRODUCTION

The snowmelt-runoff model (SRM; also referred to in the literature as the "Martinec Model" or "Martinec-Rango Model") is designed to simulate and forecast daily streamflow in mountain basins where snowmelt is a major runoff factor. SRM was developed by Martinec (Reference 1) in small European basins. With the advent of satellite snow-cover data in the 1970s, it became possible to test SRM in larger basins. Using Landsat data the model was successfully applied to various basins in the U.S.A. (References 2,3, and 4). Figure 1 illustrates the relative size of some of the basins in which the model has been tested so far. Based on these tests, the model was adapted to a wide range of basin and data characteristics.

RANGE OF CONDITIONS FOR MODEL APPLICATION

Basin Conditions

The size of the basin to which SRM is applied does not yet seem to be a limiting factor. The model so far has been used on basins ranging from 2.65 km² to 4000 km² (Kings River, California; Reference 5) with no serious problems encountered. As pointed out by Rango and Martinec (Reference 6), however, the accuracy of simulation generally decreases as the basin size increases because of sparse hydrometeorological data networks.

As already mentioned, SRM is to be used in a mountain basin with significant snow accumulation. The total basin relief (amplitude of elevation) encountered on watersheds tested so far has ranged between 350 and 4000 m. No problems are envisaged in application of the model to basins with a greater total relief, however, in basins with less total relief problems may arise due to the fact that SRM may not be applicable to non-mountain basins.

SRM has been used in mountain basins ranging in climate conditions from humid to semi-arid with no serious limitations. It seems, however, that simulations tend to be less accurate when there are significant amounts of rainfall during the snowmelt period.

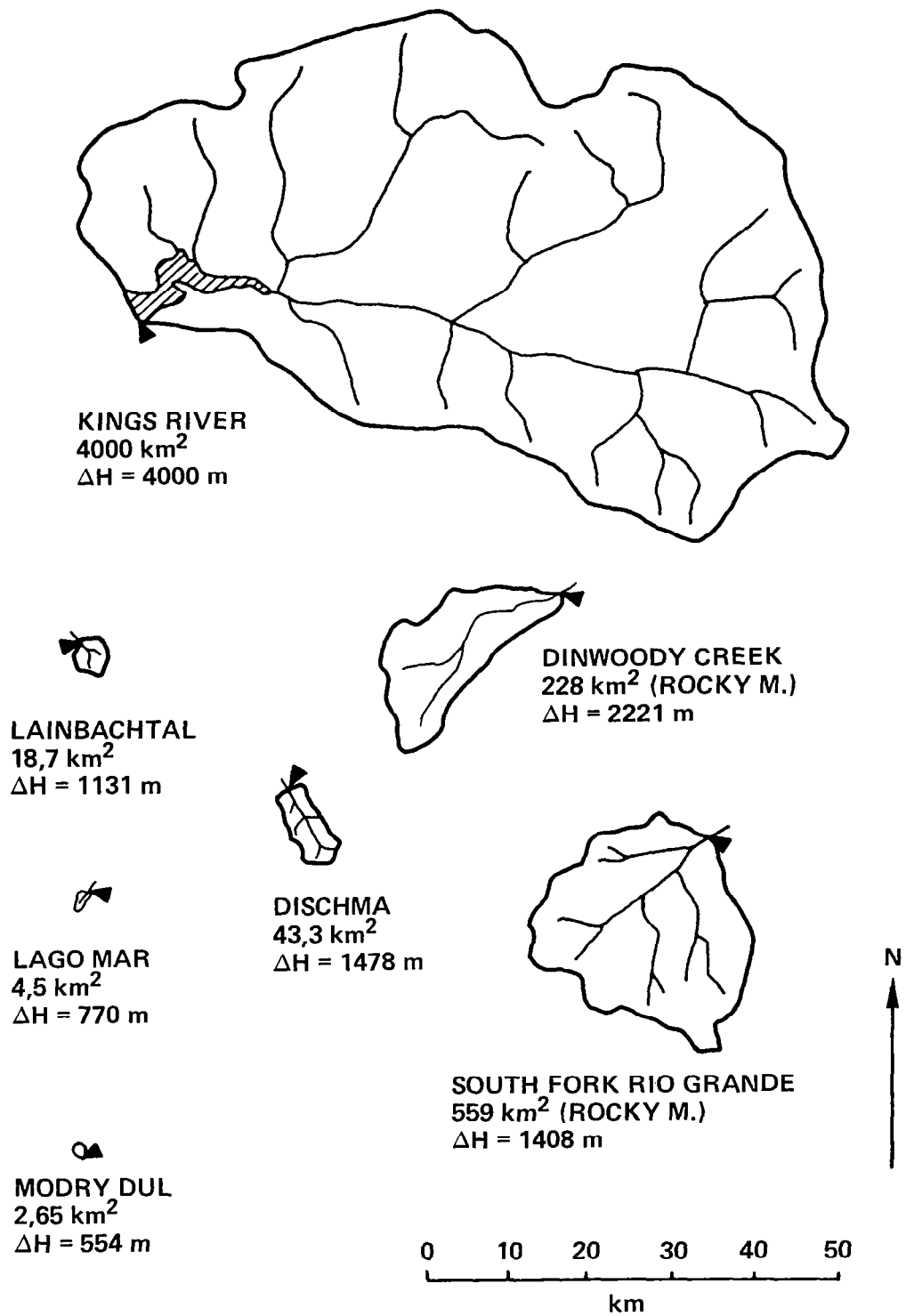


Figure 1. Area and total basin relief (ΔH) of a selection of basins in which the snowmelt-runoff model has been applied.

Data Quality

The model requires good daily air-temperature and precipitation data and periodical monitoring of snow-covered area in the given basin by satellites, aircraft, or visual observations. Long term historical data sets are not necessary (but helpful, if available) because little or no optimization (calibration) of the model parameters is necessary. The model can be run with as little as 1-2 years of record.

Daily discharge data from the basin are required to determine the recession coefficient and, otherwise, only to evaluate the accuracy of simulation. The discharge preceding the start of the snow-melt season (winter baseflow) must be known or estimated for initializing the model. Past continuous discharge records (hydrographs), if available, are useful to determine the time lag between the temperature and discharge cycles.

The optimum conditions for accurate simulation of runoff have been identified as follows (Reference 6): (1) temperature and precipitation are recorded at the mean elevation of the basin inside the basin boundaries (or at the zonal mean elevation for large basins); (2) snow cover is available reliably once per week to detect short-term variations in zonal areal extent; (3) several climatological stations are available for large basins, especially in areas with frequent summer precipitation events; and (4) several years of daily runoff records have been acquired for the determination of the recession coefficient. Decreases in accuracy will be expected as these optimum conditions are compromised. However, acceptable simulations will result even under the following minimum conditions; (1) temperature and precipitation data are observed outside the basin at a considerable horizontal and vertical distance; (2) snow-cover observations are only available two to three times during the snowmelt season; (3) climatological observations are not possible at multiple stations; and (4) no runoff records are available so that the recession coefficient must be estimated from the basin size (see section Recession Coefficient).

MODEL OUTPUT PRODUCTS

In the simulation mode, SRM produces daily discharge values from the start until the end of the snowmelt period (usually 1-6 months) using the actual sequence of temperatures and the depletion curves of the snow coverage obtained from snow-cover monitoring. Because updating is not necessary, no measured discharge values are required. Consequently, simulations can serve not only for model testing but also serve to establish discharge series in ungauged basins. Instead of real temperatures, hypothetical values can be substituted in order to simulate, for example, the effect of future changes of climate on the runoff. Seasonal volume simulations are obtained by summing the daily flows over the period of interest. Outside the snowmelt period, SRM can be operated but careful attention must be paid to the runoff coefficients in which are included the effects of evapotranspiration and soil moisture which are not as important during snowmelt.

For operational short-term discharge forecasts, SRM is run with similarly short-term temperature and precipitation forecasts and extrapolations of the snow-cover depletion curves. The forecasting period can be from 1 day to several weeks depending on the range of temperature forecasts. In such a forecast mode, periodical updating with actual temperatures and discharges and with recent snow-cover information is desirable. The model can also be used for seasonal forecasts of the expected runoff volumes ranging from several weeks to the total duration of the snowmelt season. Such forecasts are based on medium-range prediction techniques, climatological records, or on statistically determined sequences of temperatures and precipitation. An extrapolation of the snow-cover depletion curves taking into account the forecasted temperatures is also required.

MODEL STRUCTURE

Each day during the snowmelt season, the water produced from snowmelt and from rainfall is computed, superimposed on the calculated recession flow, and transformed into the daily discharge from the basin according to Equation (1).

$$Q_{n+1} = c_n [a_n (T_n + \Delta T_n) S_n + P_n] \frac{A \cdot 0.01}{86400} (1 - k_{n+1}) + Q_n k_{n+1} \quad (1)$$

- where
- Q = average daily discharge in $\text{m}^3 \text{s}^{-1}$
 - c = runoff coefficient expressing the losses as a ratio (runoff/precipitation)
 - a = degree-day factor ($\text{cm} \cdot ^\circ\text{C}^{-1} \cdot \text{d}^{-1}$) indicating the snowmelt depth resulting from 1 degree-day
 - T = number of degree-days ($^\circ\text{C} \cdot \text{d}$)
 - ΔT = the adjustment by temperature lapse rate necessary because of the altitude difference between the temperature station and the average hypsometric elevation of the basin or zone
 - S = ratio of the snow-covered area to the total area
 - P = precipitation contributing to runoff (cm). A preselected threshold temperature, T_{CRIT} , determines whether this contribution is rainfall and immediate.
 - A = area of the basin or zone in m^2
 - $\frac{0.01}{86400}$ = conversion from $\text{cm} \cdot \text{m}^2 \cdot \text{d}^{-1}$ to $\text{m}^3 \cdot \text{s}^{-1}$
 - k = recession coefficient indicating the decline of discharge in a period without snowmelt or rainfall: $k = \frac{Q_{m+1}}{Q_m}$
($m, m+1$ are the sequence of days during a true recession flow period)
 - n = sequence of days during the discharge computation period. Equation (1) is written for a time lag between the daily temperature cycle and the resulting discharge cycle of 18 hours. As a result, the number of degree-days measured on the n th day corresponds to the discharge on the $n+1$ day. Different lag times will result in the proportioning of day n snowmelt between discharges occurring on days $n, n+1$ and possibly $n+2$.

Data available in English units can be converted into the SI system and vice versa by the following conversion factors:

Conversion Factors

$Q[\text{m}^3 \text{s}^{-1}]$	=	$0.02832 Q[\text{ft}^3 \text{s}^{-1}]$
$Q[\text{ft}^3 \text{s}^{-1}]$	=	$35.31 Q[\text{m}^3 \text{s}^{-1}]$
$A[\text{km}^2]$	=	$2.59 A[\text{mi}^2]$
$A[\text{mi}^2]$	=	$0.386 A[\text{km}^2]$
$T[^\circ\text{C} \cdot \text{d}]$	=	$5/9 T[(^\circ\text{F}-32) \cdot \text{d}]$
$T[(^\circ\text{F}-32) \cdot \text{d}]$	=	$9/5 T[^\circ\text{C} \cdot \text{d}]$

$$\begin{aligned}
a[\text{cm}\cdot^{\circ}\text{C}^{-1}\cdot\text{d}^{-1}] &= 4.57 a[\text{in}\cdot(^{\circ}\text{F}-32)^{-1}\cdot\text{d}^{-1}] \\
a[\text{in}\cdot(^{\circ}\text{F}-32)^{-1}\cdot\text{d}^{-1}] &= 0.22 a[\text{cm}\cdot^{\circ}\text{C}^{-1}\cdot\text{d}^{-1}] \\
P[\text{cm}] &= 2.54 P[\text{in}] \\
P[\text{in}] &= 0.39 P[\text{cm}]
\end{aligned}$$

For Q in $\text{ft}^3 \text{ s}^{-1}$, a in $\text{in}\cdot(^{\circ}\text{F}-32)^{-1}\cdot\text{d}^{-1}$, T in $(^{\circ}\text{F}-32)^{-1}\cdot\text{d}$, P in in and A in mi^2 , the conversion constant 0.01/86400 in Equation (1) becomes 2323200/86400. For A in ft^2 , the conversion constant becomes 0.0833/86400.

In Equation (1), T , S , and P are variables to be measured or determined each day; whereas, c , a , k , and ΔT are parameters which are characteristic for a given basin or, more generally, for a given climate. The parameters are evaluated before hand from actual data, observations, or prior knowledge, or they are estimated by analogy from other basins. In addition, the area-elevation curve of the basin is required in order to determine the altitude difference for the extrapolation of temperature. If the elevation range of the basin exceeds 500 m, it is recommended to divide the basin into elevation zones of about 500 m each. For an elevation range of about 1500 m and three elevation zones A, B, and C, the model equation becomes:

$$\begin{aligned}
Q_{n+1} = & c_{A_n} [a_{A_n} (T_n + \Delta T_{A_n}) S_{A_n} + P_{A_n}] \frac{A_A \cdot 0.01}{86400} + \\
& c_{B_n} [a_{B_n} (T_n + \Delta T_{B_n}) S_{B_n} + P_{B_n}] \frac{A_B \cdot 0.01}{86400} + \\
& c_{C_n} [a_{C_n} (T_n + \Delta T_{C_n}) S_{C_n} + P_{C_n}] \frac{A_C \cdot 0.01}{86400} (1 - k_{n+1}) + Q_n k_{n+1}
\end{aligned} \quad (2)$$

The indices A, B, and C refer to the appropriate elevation zone, and, again, a time lag of 18 hours is assumed.

In the simulation mode, the model can function without updating during the snowmelt period. The discharge data serve only to evaluate the accuracy of the simulation. In ungauged basins the simulation is started with a discharge estimated by analogy to a nearby gauged basin. In the forecasting mode, if the discharge data are available, the model provides an option for updating on a periodic basis with actual discharge.

DETERMINATION OF MODEL VARIABLES AND PARAMETERS

Basin Characteristics

Basin and Zone Areas

The basin boundary is defined by the location of the streamgauge (or some arbitrary point on the streamcourse) and the watershed divide as identified on a topographic map. The basin boundary can be drawn on a variety of map scales. For the larger basins, a 1:250,000 scale map is adequate. After examining the elevation range between the streamgauge and the highest point in the basin (total basin relief), elevation zones can be delineated in intervals of about 500 m or 1500 ft. In addition to drawing the basin and zone boundaries, several intermediate topographic contour lines should be highlighted for later use in constructing the area-elevation curve. Once the boundaries and the contours have been determined, the areas formed by these boundaries should be planimetered, manually or automatically. Figure 2 shows the elevation zones and areas of the

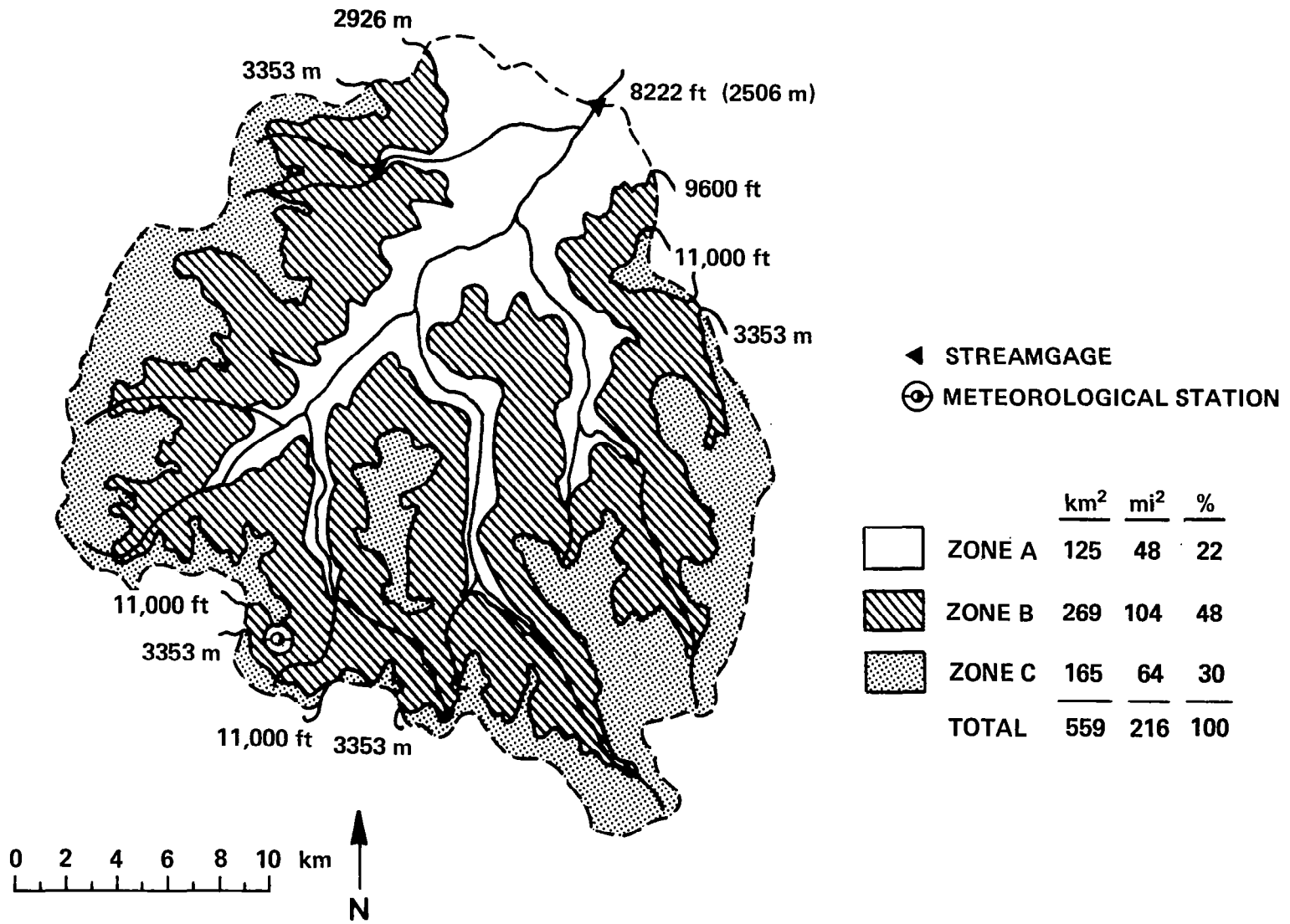


Figure 2. Elevation zones and areas of the South Fork of the Rio Grande basin, Colorado, U.S.A.

South Fork of the Rio Grande basin in Colorado, U.S.A. The elevation range of 1408 m dictated the division of the basin into three elevation zones. Once the zones are defined, the various model variables and parameters are applied to each zone for the calculation of snowmelt runoff. To facilitate this application, the mean hypsometric elevation of the zone must be determined through use of an area-elevation curve.

Area-Elevation Curve

By using the zone boundaries plus other selected contour lines in the basin, the areas enclosed by various elevation contours can be determined by planimetry. These data can be plotted (area vs. elevation) and an area-elevation (hypsometric) curve drawn as shown in Figure 3 for the South Fork basin. The zonal mean hypsometric elevation, \bar{h} , can then be determined from this curve by balancing the areas above and below the mean elevation as shown in Figure 3. The \bar{h} value is used as the elevation to which base station temperatures are extrapolated for the calculation of zonal degree-days.

Variables

Temperature and Degree-Days

Although a minimum of one temperature station is required in order to apply SRM to a given basin, the ideal situation would have temperature measurements made at the \bar{h} of each elevation zone. As this is usually not the case, the location of one temperature station at the mean hypsometric elevation of the entire basin would be desirable. Both of these situations minimize the vertical distance that temperatures would have to be extrapolated for application in the model. If this is not possible, the use of two stations, one at the bottom of the basin and one near the top would permit computation of an actual temperature lapse rate to be used in extrapolation to the various zones. Usually, however, data from only one temperature station at low elevation, and many times not even located inside the basin, must be used to calculate the degree-days for melting snow in the lowest to the highest elevation zones of the basin. When one station is used, a lapse rate has to be assumed in order to extrapolate degree-days from the base station to the appropriate mean hypsometric elevation.

Air temperature expressed in degree-days is used in SRM as an index of the complex energy balance leading to snowmelt. At stations where hourly readings are made, the number of degree-days for each 24-hour period is determined by summing the hourly temperatures and dividing by 24 and using 0°C as the base temperature. Where only maximum and minimum temperatures (T_{\max} , T_{\min}) are available, the number of degree-days (in°C) is determined as

$$T = \frac{T_{\max} + T_{\min}}{2} \quad (3)$$

The degree-day figures refer to the 24-hour period starting at 0600 hours with the corresponding discharge referring to periods shifted according to the time lag of the basin. As indicated by Linsley, *et al.* (Reference 7), all negative differences in the degree-day values in Equation (3) are taken as zero.

There are several methods for dealing with the actual temperatures used in calculating the degree-day value. When using the max-min approach, the most common way is to use the temperatures as they are recorded and calculate the average daily temperature. Garstka, *et al.* (Reference 8), however, indicate that in many parts of the mountainous western United States the fluctuation of

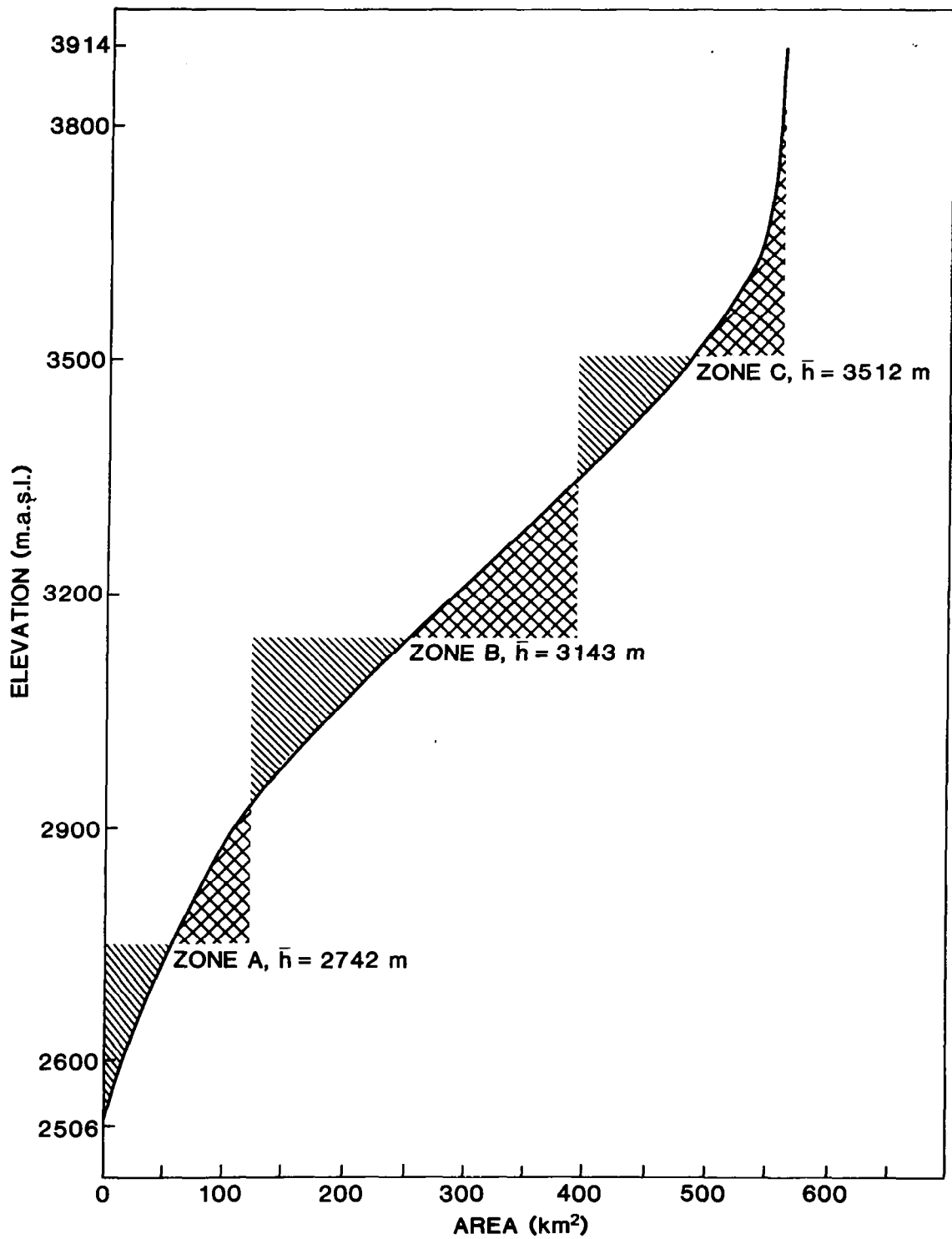


Figure 3. Determination of zonal mean hypsometric elevations (\bar{h}) using an area-elevation for the South Fork of the Rio Grande basin.

temperatures, especially the depression of the minimum, is very large so that the average temperature will many times turn out to be below 0°C indicating no degree-days. Even so, during part of the day snowmelt conditions may have prevailed due to temperatures reaching as high as 10–15°C. In order to counteract this problem, an effective minimum temperature approach can be used. In essence, whenever $T_{\min} < 0^\circ\text{C}$ it becomes $T_{\min} = 0^\circ\text{C}$ before being entered into Equation (3). It appears that this approach gives a better representation of the heat factor for use in snowmelt-runoff studies (Reference 8). Treating minimum temperatures below the freezing point as 0°C can also be employed when using hourly temperatures to calculate the degree-days. If all hourly temperatures of both T_{\max} and T_{\min} are below 0°C, however, then the degree-days are taken as zero. It is recommended to use the effective minimum temperature approach for calculating degree-days for use in SRM. The model and computer program can also accept the average temperature approach, however, if the user feels that it better represents the snowmelt conditions in a given basin.

The degree-days are extrapolated to an elevation zone by using a suitable lapse rate, δ , and the following equation.

$$\Delta T = \delta (h_{ST} - \bar{h}) \quad (4)$$

where

- ΔT = temperature lapse rate correction factor in °C
- δ = temperature lapse rate in °C per 100 m
- h_{ST} = altitude of the temperature station in m
- \bar{h} = zonal hypsometric mean elevation in m

The temperature lapse rate must be carefully determined, especially if the observation station is situated at a low altitude and the extrapolation of degree-days is made in only one direction (upwards). The lapse rate should be indicative of the mountainous region where the basin is located based on some kind of prior climatic knowledge. As the snowmelt season progresses, lapse rates may change depending on the basin. Such changes can be instituted every 15 days in SRM, if necessary. When applying SRM it is advisable to conduct a regional analysis of monthly lapse rates to determine the seasonal variation. In some cases it may be necessary to modify the mean monthly lapse rates obtained in such an analysis because of basin peculiarities (such as frequent temperature inversions) or an abnormal climatic progression in a particular year. In basins with little seasonal variation, a lapse rate of 0.65°C/100m has been found to be adequate.

Precipitation

It is even more difficult to obtain adequate precipitation data for a mountain basin than to obtain temperature data. The extrapolation of precipitation amounts from one or more base stations to zones in the basin must be done based on user knowledge of the study area. Location of a precipitation station at the mean hypsometric elevation would be the optimum situation.

If precipitation is determined to fall in the basin on a given day, a critical temperature, T_{CRIT} , must be examined to determine whether the precipitation is rain or snow. T_{CRIT} is usually selected to be slightly above the freezing point and may vary from basin to basin. The distinction between rain and snow is important in SRM because the rain contribution to runoff is on the same day that the rain occurs, whereas the snow contribution to runoff is delayed.

When the precipitation is determined to be snow, its delayed effect on runoff is treated differently depending on whether it falls over the snow-covered or snow-free portion of the basin. The new snow that falls over the previously snow-covered area is assumed to become part of the seasonal snowpack and its effect is included in the normal depletion curve of the snow coverage. The new snow falling over the snow-free area is considered as precipitation to be added to snowmelt, with this effect delayed until the next warm day. This precipitation is stored by SRM and then melted as soon as a sufficient number of degree-days has occurred. This may take place on the first day warm enough to produce snowmelt or on a series of days. The following example in Table 1 illustrates a case where 2.20 cm water equivalent of snow fell on day n and then was melted on the three successive days.

Table 1. Calculation of the melt of new snow deposited on a snow-free area
($P_n = 2.20$ cm; $T_{CRIT} = +1.0^\circ\text{C}$)

Day	a ($\text{cm} \cdot ^\circ\text{C}^{-1} \cdot \text{d}^{-1}$)	T ($^\circ\text{C} \cdot \text{d}$)	S	P (cm)	Melted Depth $a \cdot T(\text{cm})$	P Stored (cm)	P contributing to Runoff $a \cdot T \cdot (1-S)(\text{cm})$
n	0.45	0	0.72	2.20	0	2.20	0
n+1	0.45	0.11	0.70	0	0.05	2.15	0.02
n+2	0.45	2.70	0.68	0	1.22	0.93	0.39
n+3	0.45	3.70	0.66	0	0.93	0	0.32

In this example, S is decreasing on consecutive days because it is interpolated previously from the snow-cover depletion curve. In reality it should remain constant as long as the seasonal snowpack is covered with new snow, however, the model currently uses the incremental decrease of S shown in Table 1.

When the precipitation is determined to be rain, and it falls on a snow-free area, it becomes available to contribute to runoff immediately. When rain falls on snow, however, its effect on runoff depends upon the condition of the snowpack. Early in the snowmelt season rain falling on the snowpack is assumed to be retained by the snow, which is mostly dry and usually deep. This rainfall is not available for runoff. At some stage during snowmelt the snowpack is assumed to be ripe (the user must decide when), and any rain falling on the snow is transferred through the snow layer and becomes available to contribute to runoff the same as over the snow-free area. Both of these options are included in the computer program. In SRM the melting effect of rainfall is neglected.

Snow Coverage

The snow-cover variable, S, of a zone or basin is usually obtained from a depletion curve for input into SRM. A variety of sources of snow-cover data can be used to compile the depletion curves including ground observations (used for Modrý Důl), aircraft photography (Dischma), and satellite

imagery (all the large basins). If the data are available, it is recommended that satellite imagery be used since it is the easiest to analyze and also quite accurate depending on basin size (area minimums for various satellites: Landsat-10km²; NOAA-VHRR-200km²; and GOES-1000km²). To assist in the use of satellite imagery for snow-cover interpretations, a handbook of analysis techniques is available (Reference 9). Additional information on snow-cover interpretation techniques for Europe is given in Reference 10.

Photointerpretation of satellite snow images is used to delineate the snow line on a base map of the study basin (see Figure 2), and the area enclosed by the snow line in each elevation zone is planimeted to obtain the snow-covered area. The snow cover by elevation zone is then plotted against elapsed time to construct depletion curves such as those shown in Figure 4 for 1976 in the South Fork basin. For the snowmelt-runoff simulation, daily snow-cover values are taken from the depletion curves and input to SRM.

Snowstorms occurring during the snowmelt season can result in a temporary increase of snow cover, but generally with no significant hydrologic effect. The duration of this increase is usually shorter than the interval between snow-cover observations. If the snowstorm occurs shortly before the

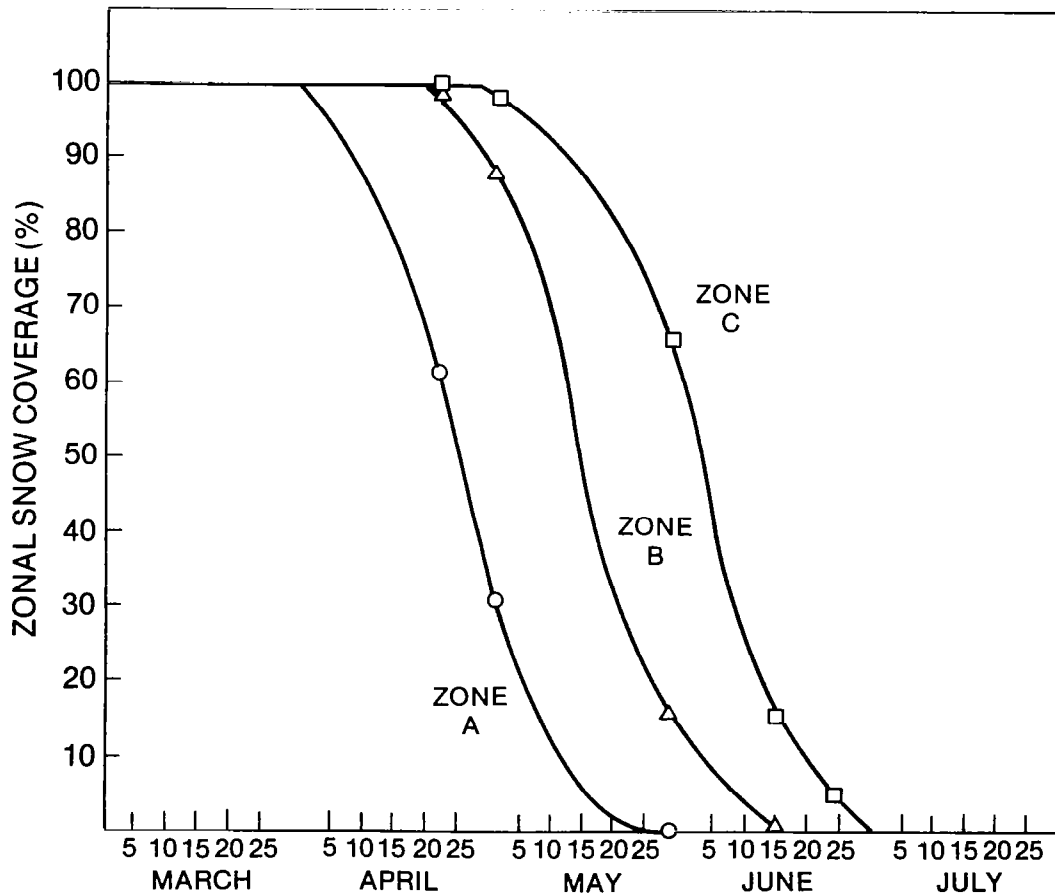


Figure 4. Landsat-derived snow-cover depletion curves for the South Fork of the Rio Grande basin for elevation zones, A, B, and C for 1976. Landsat snow-cover observations are plotted.

snow-cover observation, however, it may lead to the interpretation of exaggerated snow-covered areas and a distortion of the true depletion curves of the seasonal snowpack. It is recommended that such anomalous snow-cover values be disregarded and that the depletion curves be drawn only with reference to the snow cover accumulated before the beginning of the snowmelt period (seasonal or "old" snowpack), as illustrated in Figure 5. Precipitation and temperature records should be consulted in order to identify these transitory snow events when drawing the depletion curves. The transitory new snow is accounted for as stored precipitation eventually contributing to runoff as explained in the previous section.

In rare cases massive summer snowstorms can affect the snow coverage for several weeks. If such a situation is revealed by subsequent satellite data, it may be preferable to draw the depletion curves

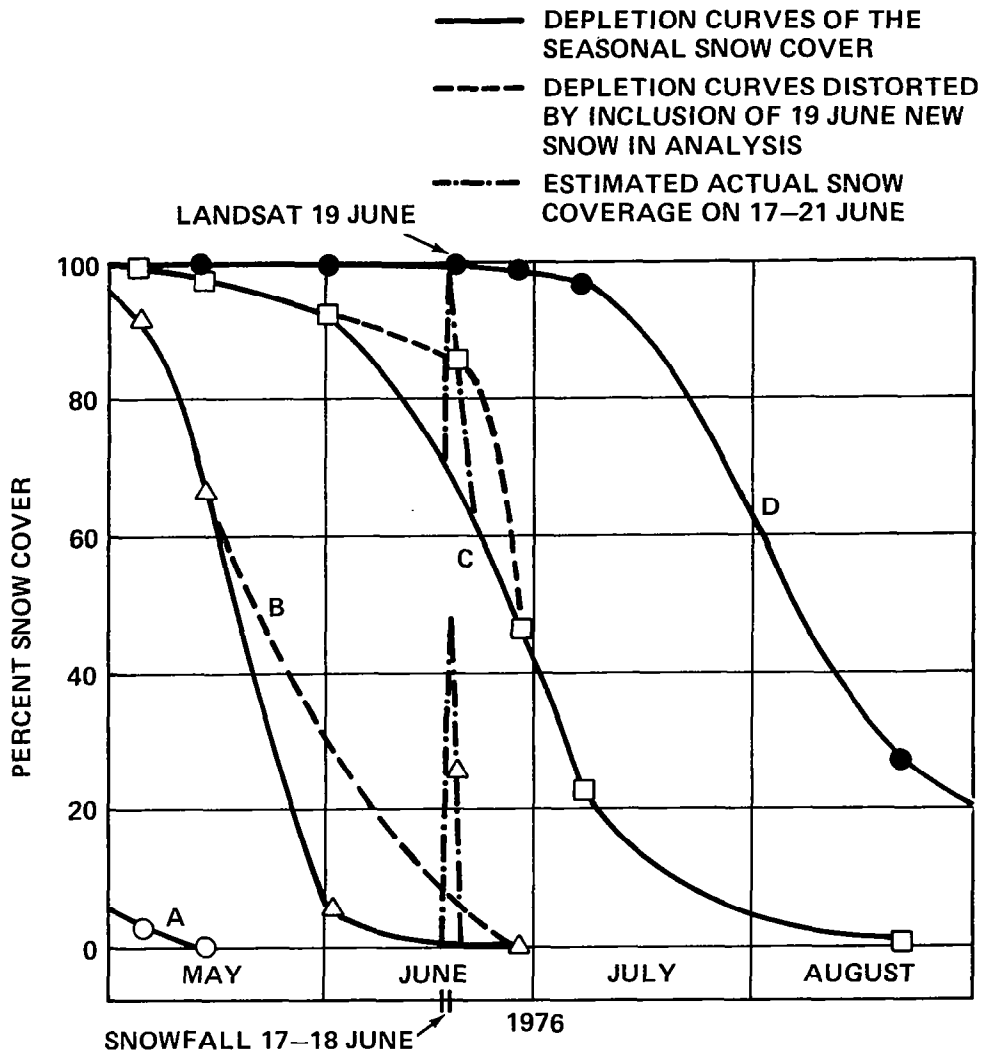


Figure 5. Seasonal and distorted depletion curves of snow coverage in the Dinwoody Creek basin, Wyoming, U.S.A. for elevation zones A, B, C, and D. A snow storm of 17-18 June deposited several cm water equivalent of new snow preceding the Landsat overpass of 19 June. The new snow in zones B and C was melted in 2-3 days.

according to this actual snow coverage. Because of this modification to the depletion curves, the model will melt more seasonal snow than before, but the amount of stored or new precipitation will be automatically reduced.

If runoff forecasts at the beginning of snowmelt are desired, a new approach must be used because the actual snow-cover depletion curves are not available, and in many cases, the snow-cover extent does not differ greatly between a dry and a wet year. The South Fork basin (559 km²) in Colorado was studied as an example. Although the runoff in the snowmelt season of 1979 was six times greater than it was in the drought year of 1977, there was little difference in the snow-cover extent of the upper elevation zones of the South Fork basin on 1 April. To provide a means for forecasting runoff, it is suggested that the depletion curves that normally relate the areal extent of the snow cover to elapsed time be modified to relate the snow coverage to the accumulated degree-days (Reference 11). This procedure is discussed in more detail in the chapter on Operation of the Model for Real-Time Forecasts.

Parameters

Runoff Coefficient

The average value of the runoff coefficient, c , for a basin for a year is given by the ratio of annual runoff/annual precipitation. It should be pointed out that because of a measurement catch deficit, rain gauges frequently underestimate winter precipitation (snow) in mountain basins. As a result, artificially elevated values of c may be calculated. In such a case, a synthesis of data from representative basins should provide guidance for assessing c in the absence of reliable, direct measurements.

Because the runoff coefficient is likely to vary throughout the year as a result of changing vegetation and soil moisture conditions, the SRM computer program permits changes in c every 15 days. Usually, c is higher for snowmelt than for rainfall. Therefore, the model can handle different runoff coefficients for snow, c_S , and for rain, c_R , as determined by the user. In basins studied, when snowmelt is concentrated in a short time period, c_S can approach 1.0. With prolonged snowmelt runoff in a semiarid region, c_S may go down to 0.3. In addition c will vary from zone to zone in a basin, and SRM has the capability to handle different c values by zonal input. It is possible that with rain falling in the low elevations of a semiarid basin, c_R may be 0.2, whereas at the same time in the high elevations with snow still melting, c_S can be 0.9. The selection of c requires first hand knowledge of the basin and its hydrologic behavior under different hydrometeorological conditions.

Degree-Day Factor

The degree-day approach is used as an index of the energy balance and the degree-day factor, a , is used to convert degree-days to snowmelt expressed in depth of water. The degree-day factor is variable throughout the melt period because the changing properties of snow influence the melting process. It is possible to measure the degree-day factor at a point using temperature measurements and a snow pressure pillow or lysimeter. The simultaneously accumulated degree-days and melt at a pressure pillow can be compared to calculate the degree-day factor for different times during the snowmelt season. Daily values are extremely variable so it is recommended to use a minimum of 3-5 days for averaging the degree-day factor. In addition, point measurements cannot be easily extrapolated to large areas. The point measurements can be used for information and then weighted depending on how well a specific station represents the hydrologic characteristics of a given zone (Reference 12).

In the absence of detailed data, the degree-day factor can be obtained from an empirical relation developed by Martinec (Reference 13):

$$a = 1.1 \frac{\rho_s}{\rho_w} \quad (5)$$

where

$$\begin{aligned} a &= \text{the degree-day factor in } \text{cm} \cdot ^\circ\text{C}^{-1} \cdot \text{d}^{-1} \\ \rho_s &= \text{density of snow} \\ \rho_w &= \text{density of water} \end{aligned}$$

The general seasonal increase in ρ_s can be used as an index of the seasonal increase of a . Large variations are expected if the melt season is long or there is a large difference in elevation in the basin. For Dinwoody Creek in Wyoming, a was gradually increased from 0.35 on 1 April to 0.60 on 30 September in the highest elevation zone (Reference 2).

A wide range of a values has been reported in the literature with a generally increasing as the snowpack ripens. There have been extreme values as low as $0.07 \text{ cm} \cdot ^\circ\text{C}^{-1} \cdot \text{d}^{-1}$ and as high as $0.92 \text{ cm} \cdot ^\circ\text{C}^{-1} \cdot \text{d}^{-1}$ reported (Reference 14), however, during the snowmelt season for undisturbed snow, the range is about $0.25 - 0.60 \text{ cm} \cdot ^\circ\text{C}^{-1} \cdot \text{d}^{-1}$. The fact that increasing a is related to increasing snow density as snowmelt progresses is in response to a number of factors. A greater density is usually associated with older snow with a lower albedo, thus a higher a value. In addition, high densities toward the end of the snowmelt season are also associated with increased liquid water content and low thermal quality of the snow. Because of these expected seasonal changes in a , SRM is structured to allow modifications of a every 15 days, if necessary. Because of different stages of snowpack ripening in different elevation zones, a can also be varied between zones. Sometimes the occurrence of a large, late season snowfall will produce depressed a values for several days due to the new low-density snow. The a values in the model can manually be modified and inserted to reflect these unusual snowmelt conditions.

Recession Coefficient

The recession coefficient, k , depends upon the current discharge in the following way:

$$k_{n+1} = xQ_n^y \quad (6)$$

where Q is the daily discharge and the constants x and y must be determined for the given basin. For this determination, daily discharge values for the snowmelt season or the whole year are used. The discharge on a given day, Q_n , is always plotted against the value on the following day, Q_{n+1} , as illustrated in Figure 6 for the Dischma basin in Switzerland. In Figure 6 any points above the 1 to 1 line refer to the rise of the hydrograph and the points below the line to the fall of the hydrograph. For purposes of this model and derivation of the recession equation, only points below the 1 to 1 line need to be plotted. Once these points have been plotted, an envelope line as shown in Figure 6 can be drawn to enclose most of the points. The lower envelope line represents the extreme discharge decline, i.e., the recession without any partial delay by possible precipitation or snowmelt. It is not recommended, however, to include all points inside this envelope at any cost, especially in the lower range of discharges. The reason for this is that some discharge values may be affected by non-typical phenomena such as icing conditions in the winter or the timing of rainfall which in a particular storm results in an abrupt decrease of discharge from one day to the next.

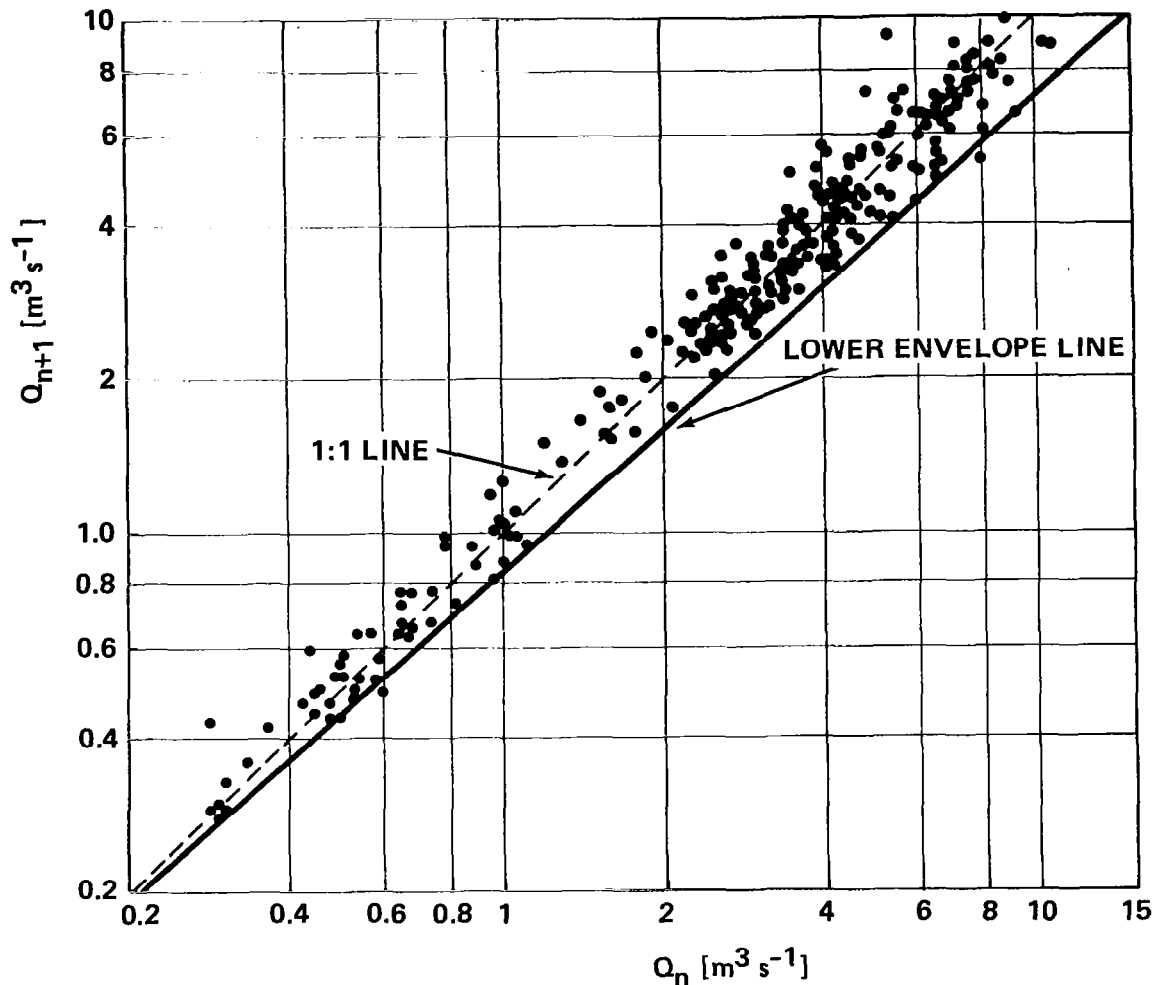


Figure 6. Recession flow plot, Q_n vs Q_{n+1} , for the Dischma basin in Switzerland with the lower envelope line drawn.

This lower envelope curve has been found to be valid on small size basins. When the model is applied to larger basins, however, it is recommended that the lower envelope curve be replaced with an average curve halfway between the lower envelope line and the 1 to 1 line. An average curve would also result from a least squares fit to the points, although the extra effort may not be justified. The average curve should probably be used on basins greater than about 50 km^2 . For year-round simulations, it was found useful to derive the constants x and y for Equation (6) separately for the summer and winter half year.

For the Dischma basin (43.3 km^2) the lower envelope curve is shown in Figure 6. The constants x and y needed in the recession equation are computed by reading off a pair of recession coefficients (k_1, k_2) from Figure 6 corresponding to discharges Q_1 and Q_2 and by solving the following equations:

$$k_1 = x \cdot Q_1^y \quad (7)$$

$$k_2 = x \cdot Q_2^y \quad (8)$$

$$\log k_1 = \log x + y \log Q_1 \quad (9)$$

$$\log k_2 = \log x + y \log Q_2 \quad (10)$$

If the discharge range allows selection of $Q_1 = 1.0 \text{ m}^3 \text{ sec}^{-1}$ and $Q_2 = 10.0 \text{ m}^3 \text{ sec}^{-1}$ the solution is simplified and Equations (9) and (10) become:

$$\log k_1 = \log x$$

$$x = k_1$$

$$\log k_2 = \log x + y$$

$$y = \log k_2 - \log k_1$$

For the Dischma basin in Figure 6,

$$k_1 = 0.85 \text{ (for } Q_1 = 1.0 \text{ m}^3 \text{ sec}^{-1}\text{)}$$

$$k_2 = 0.697 \text{ (for } Q_2 = 10.0 \text{ m}^3 \text{ sec}^{-1}\text{)}$$

$$x = 0.85$$

$$y = \log 0.697 - \log 0.85 = -0.086$$

The recession equation for Dischma using the lower envelope curve thus becomes

$$k_n = 0.85 Q_n^{-0.086} \quad (11)$$

For comparison of the recession equations of some of the previously studied basins, Figure 7 shows the plots and equations for five selected basins.

If no discharge data are available for a basin, recession coefficients can be estimated using the following formula (Reference 15):

$$k_{B2} = k_{B1} \sqrt[4]{A_{B1}/A_{B2}} \quad (12)$$

where A_{B1} and A_{B2} are the respective areas of the basins B1 and B2 and k_{B1} and k_{B2} are the recession coefficients for the corresponding runoff conditions, e.g., the average discharge, in both basins. If the constants x and y are known in basin B1, it follows that for basin B2:

$$k_{B2n} = \left[x_{B1} \left(\frac{\bar{Q}_{B1}}{\bar{Q}_{B2}} Q_{B2n-1} \right)^{y_{B1}} \right] \sqrt[4]{A_{B1}/A_{B2}} \quad (13)$$

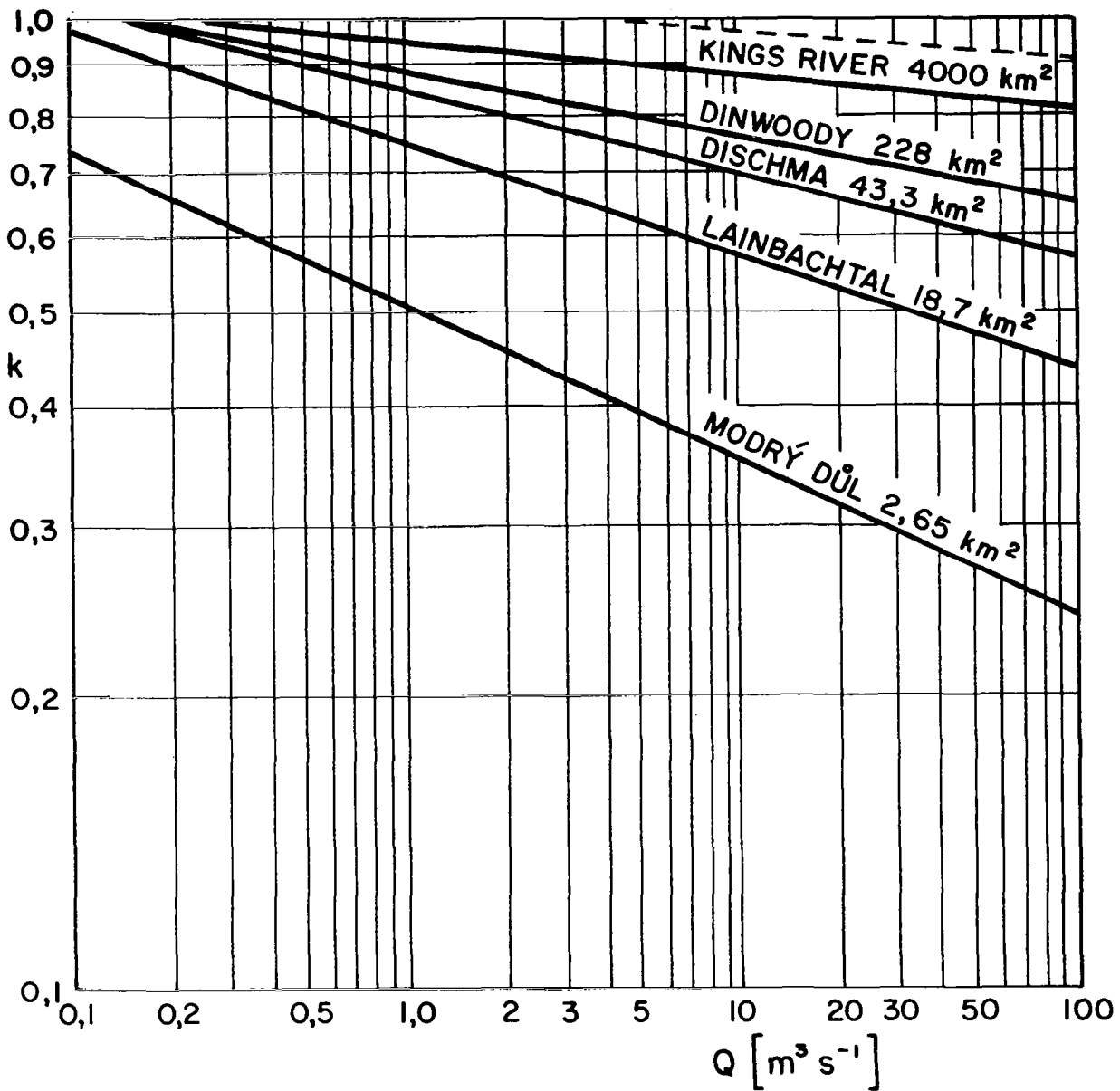


Figure 7. Relation of k and Q for basins of various sizes.

For example, if $x = 0.85$ and $y = -0.086$ have been derived for the Dischma basin, a relation for the Kings River basin is obtained by substituting $\bar{Q}_{\text{DISCHMA}} = 1.69 \text{ m}^3 \text{ sec}^{-1}$, $\bar{Q}_{\text{KINGS}} = 61.3 \text{ m}^3 \text{ sec}^{-1}$, $A_{\text{DISCHMA}} = 43.3 \text{ km}^2$, and $A_{\text{KINGS}} = 4000 \text{ km}^2$ into Equation (13).

$$k_{B2n} = \left[0.85 \left(\frac{1.69}{61.3} Q_{B2n-1} \right)^{-0.086} \right] \sqrt[4]{43.3/4000}$$

$$\begin{aligned}
k_{B2n} &= \left[0.85 \cdot 1.36 Q_{B2n-1}^{-0.086} \right]^{0.3226} \\
k_{B2n} &= \left[1.15 Q_{B2n-1}^{-0.086} \right]^{0.3226} \\
k_n &= 1.046 Q_{n-1}^{-0.0277} \tag{14}
\end{aligned}$$

Equation (14) is the recession equation for the Kings River basin using the lower envelope curve as derived by the size relationship of Equation (12). Because of the size of the Kings River basin, further analysis is needed to yield the recommended average curve for the type of plot shown in Figure 6.

Using this approach, SRM could be used to simulate discharge in ungauged basins. The equation for the recession coefficient of an ungauged basin could be obtained from utilization of Equation (12) and the recession data from an already studied basin. The simulation would start on the first day of the snowmelt period by substituting a value for Q_0 corresponding to the winter baseflow into Equation (6) to calculate k_1 . The winter baseflow value may be estimated by analogy with another basin or by measuring the discharge. Then k_1 and Q_0 are substituted into Equation (1) to calculate Q_1 . Once the computation has started, subsequent k values are determined each day from Equation (6) by substituting computed values of Q .

Time Lag

Equations (1) and (2) correspond to the most simple case of a time lag of 18 hours. In this case, the temperature rise at 06:00 hrs results in the rise of the hydrograph at 24:00 hrs. Therefore, degree-days determined for a certain day with a minimum at 06:00 hrs and a maximum at about 14:00 hrs correspond to a discharge starting at 00:00 hrs the next day (see Figure 8). If the time lag is not conveniently 18 hours, the computed discharge values may have to be shifted by a certain number of hours to facilitate comparison with published streamflow data. Examples of such shifts are presented in the following.

If the time lag is 6 hours, degree-days for the n th day result in a discharge starting at 12:00 hrs on the same day and ending at 12:00 hrs on day $n+1$ as shown in Figure 8. The next day's discharge (Q_{n+1}) is composed of about one half of the calculated input from day n and one half from day $n+1$. In the simple case of one elevation zone the equation for Q_{n+1} would be:

$$\begin{aligned}
Q_{n+1} &= \left\{ 0.5 c_n [a_n (T_n + \Delta T_n) S_n + 2 P_n] + \right. \\
&\quad \left. 0.5 c_{n+1} [a_{n+1} (T_{n+1} + \Delta T_{n+1}) S_{n+1}] \right\} \frac{A \cdot 0.01}{86400} (1 - k_{n+1}) \tag{15} \\
&\quad + Q_n k_{n+1}
\end{aligned}$$

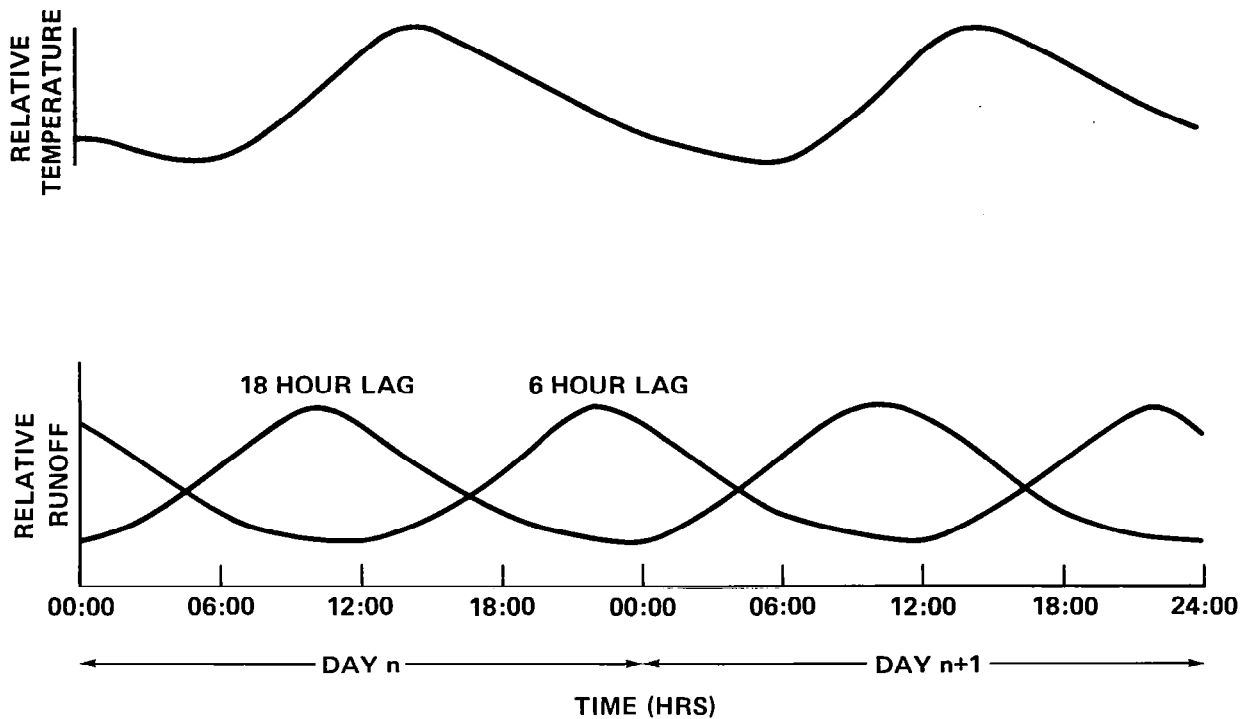


Figure 8. Daily fluctuations of temperature and discharge illustrating lag times of 6 and 18 hours.

In contrast to the snowmelt, the total amount of precipitation on the first day, P_n , and no precipitation from the second day, P_{n+1} , is included in the calculation of Q_{n+1} . Generally P_n refers to precipitation recorded between 08:00 hrs (day n) to 08:00 hrs (day n+1), and, with the time lag of 6 hours, it roughly corresponds to Q_{n+1} .

In large basins with multiple elevation zones, the time lag changes during the snowmelt season as a result of the changing spatial distribution of the snow cover with respect to the basin outlet. The ratio of inputs (or time lag correction factors) from the n and n+1 days used in Equation (6) would have to be changed accordingly, not only to account for different time lags for each zone, but also for how they change from the beginning to the end of the snowmelt season.

In order to obtain a more accurate split of the runoff from days n and n+1, Shafer, et al (Reference 12) recommend planimetry of the areas under the actual daily hydrographs to come

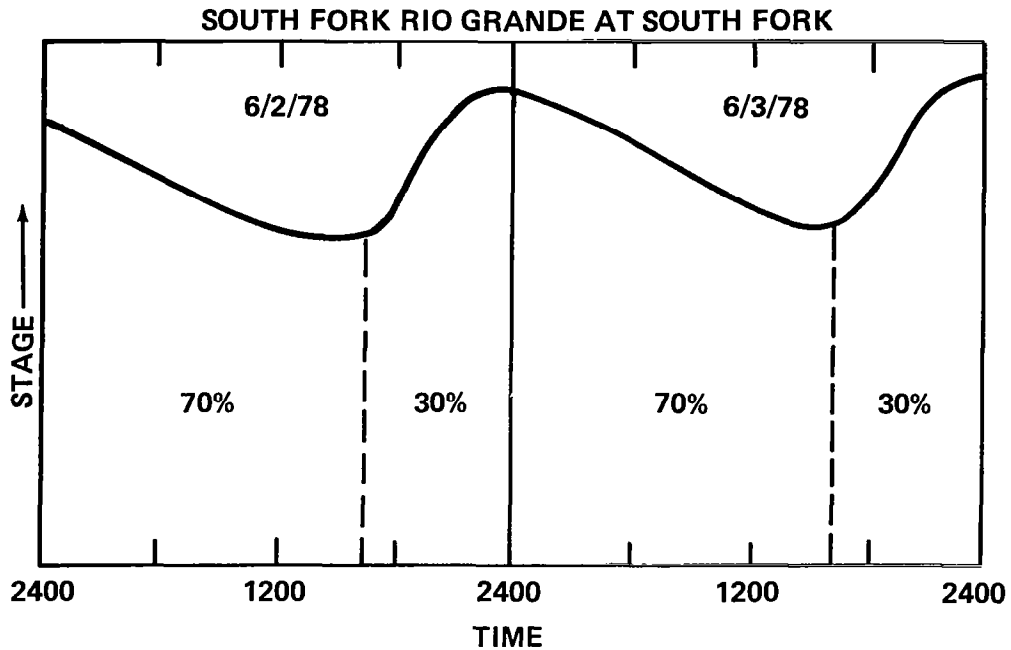


Figure 9. Planimetered hydrographs for determination of the time lag correction factors ($L_n = 0.7$, $L_{n+1} = 0.3$) for the South Fork basin in Colorado (from Reference 12).

up with the appropriate time lag correction factors (L) as shown in Figure 9. For some of the time lags encountered so far, the following L values may be utilized for determining the contributions to Q_{n+1} :

6 hours – $L_n = 0.5$, $L_{n+1} = 0.5$; 10 hours – $L_n = 0.7$, $L_{n+1} = 0.3$;

12 hours – $L_n = 0.75$, $L_{n+1} = 0.25$; 15 hours – $L_n = 0.8$, $L_{n+1} = 0.2$;

18 hours – $L_n = 1.0$, $L_{n+1} = 0.0$.

ASSESSMENT OF SIMULATION ACCURACY

One of the first steps to be followed in determining how well a model simulates actual flow conditions is a comparison plot of computed and measured hydrographs. Figure 10 illustrates this comparison for the South Fork basin in Colorado for the 1979 snowmelt season. In order to quantify the comparison, several goodness-of-fit measures may be added to the hydrograph plot. The computer program automatically calculates the percentage volume difference (D_V) between the measured (RO_M) and model-computed (RO_C) seasonal runoff as shown in Equation (16).

$$D_V = \frac{RO_M - RO_C}{RO_M} \cdot 100 \quad (16)$$

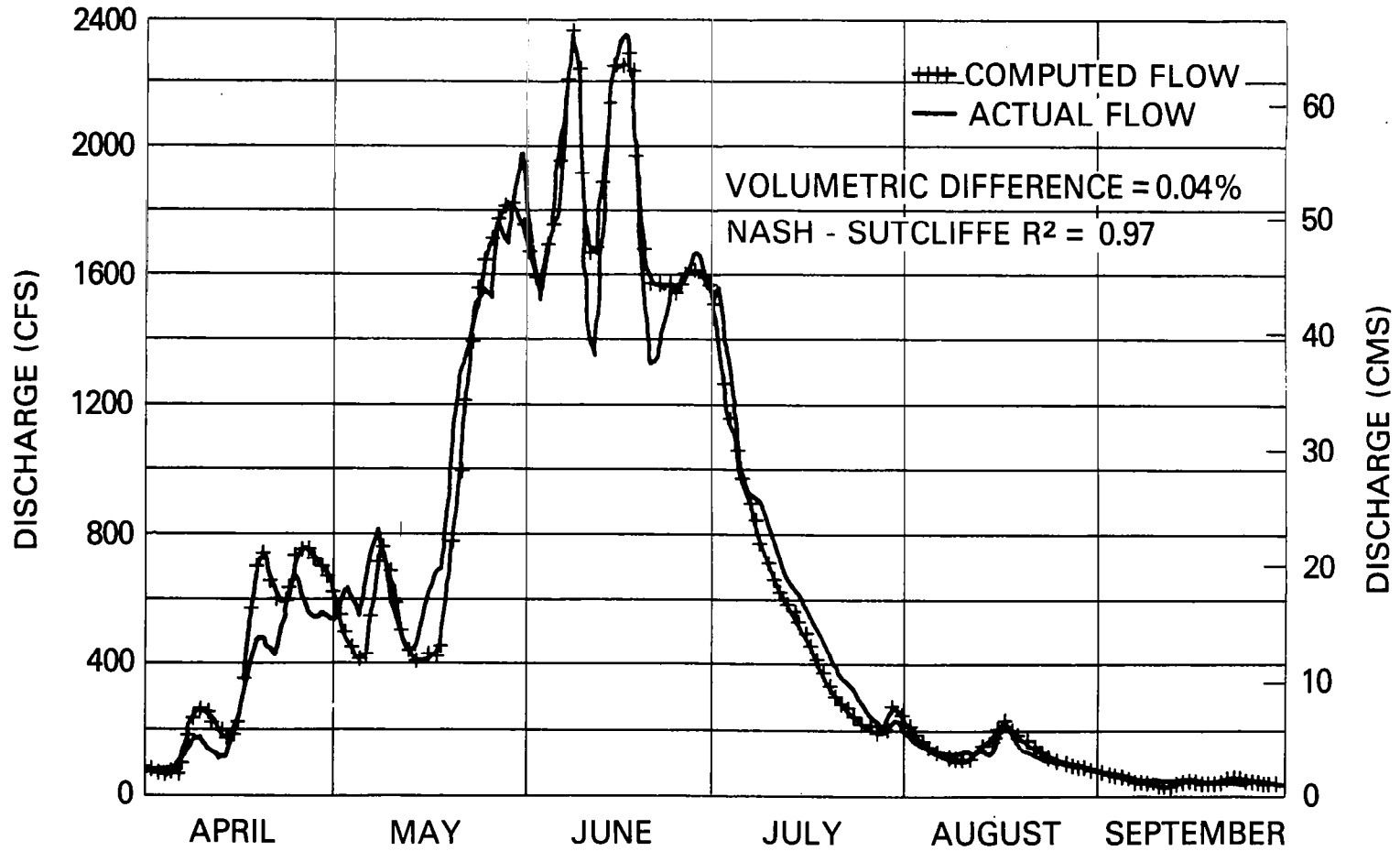


Figure 10. Simulated versus measured streamflow for the South Fork of the Rio Grande during the snowmelt season of 1979.

Model performance on a daily basis can be evaluated using the nondimensional Nash-Sutcliffe (Reference 16) R^2 value:

$$R^2 = 1 - \frac{\sum_{i=1}^n (q_i - q'_i)^2}{\sum_{i=1}^n (q_i - \bar{q})^2} \quad (17)$$

where

R^2 is a measure of model efficiency

q_i = observed daily discharge

q'_i = simulated daily discharge

\bar{q} = mean of observed discharge

n = number of daily discharge values.

The Nash-Sutcliffe R^2 value is analogous to the coefficient of determination and is a direct measure of the proportion of the variance of the recorded flows explained by the model (Reference 17). The SRM program also calculates and outputs this goodness-of-fit parameter to facilitate comparison of the correspondence of the daily flow values. Further examples of runoff simulation during snowmelt are given in Figures 11 and 12. Figure 13 shows a simulation extended to a whole year.

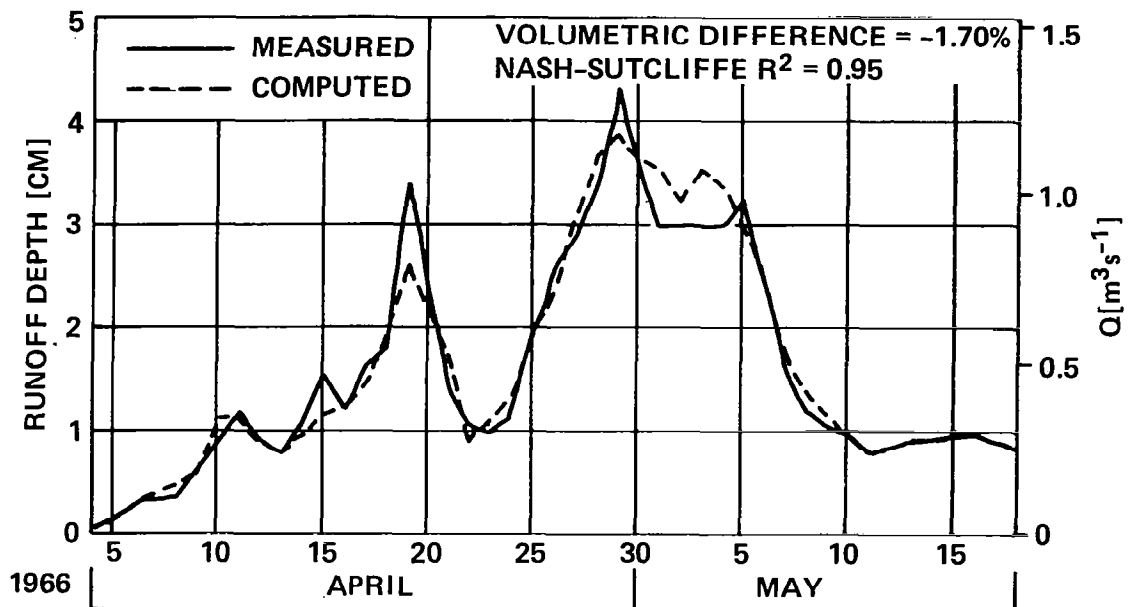


Figure 11. Snowmelt-runoff simulation for the basin Modrý Důl (2.65 km²), Czechoslovakia.

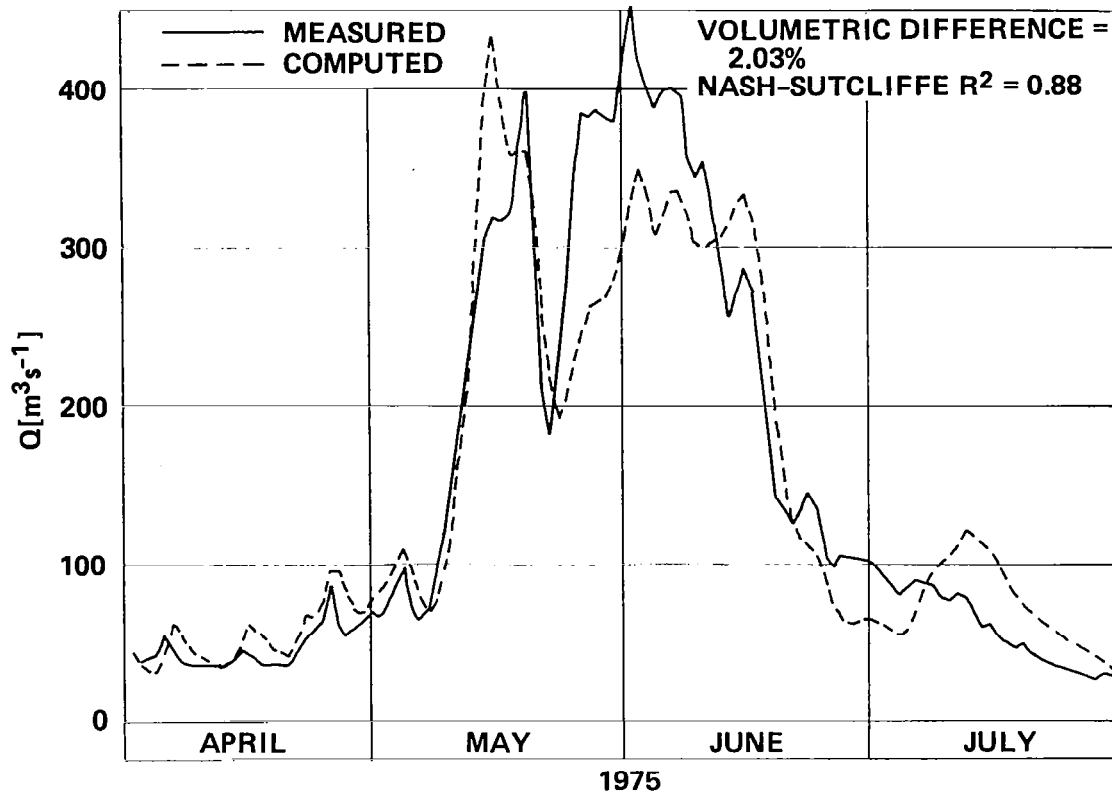


Figure 12. Snowmelt-runoff simulation for the Kings River basin (4000 km^2) in California, U.S.A. for 1975.

When running the model in the simulation mode, if a good agreement is not achieved initially, the following order of items to check in problem solving is recommended:

1. Re-evaluate the *snow cover depletion curves* to check that errors were not made in drawing the curves. This could result in a too high or too low computed runoff. One especially common error is the overlooking of a precipitation event occurring just before a satellite pass. The thin layer of transient snow cover that results causes an over estimation of the seasonal snow cover, S , which causes the depletion curve to be too high.
2. Reconsider the *lapse rate* used in the basin. Often times an average lapse rate may be too high or too low for a particular month resulting in the number of degree-days being too high or too low (especially for the upper elevations of the basin).
3. The *runoff coefficient* may require adjustment if the computed discharge is too high or too low. Typically, the runoff coefficient is the most difficult of the basin parameters to estimate accurately and should be examined closely after any gross errors due to discrepancies in snow cover and lapse rate have been ruled out.
4. The *degree-day factor* should be investigated after the runoff coefficient. Since the degree-day factor can be estimated initially from snow density measurements,

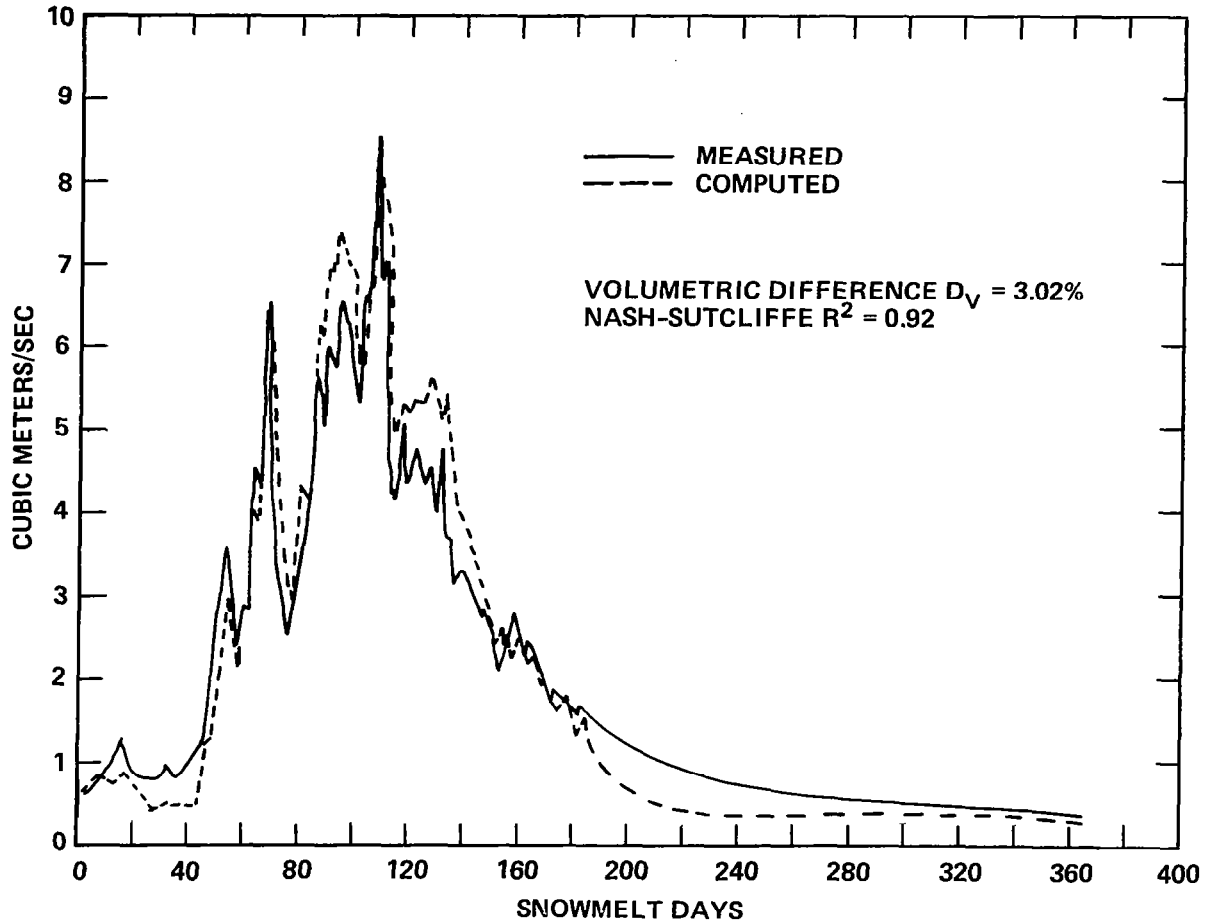


Figure 13. Simulated versus measured streamflow for the Dischma basin (43.3 km²) for April 1974 – March 1975 (365 days).

less probability of error may be expected. If, however, good snow density values are not available, adjustment of the degree-day factor may be necessary to have some effect on the runoff volume. Unusually high wind conditions may also result in the need to temporarily increase the degree-day factor, whereas new snow falling on the seasonal snowpack may cause a temporary decrease in the degree-day factor.

5. Discrepancies in *precipitation* input to SRM may result in two kinds of error. Precipitation values that are too high or low may result in similar effects on computed runoff. More importantly, peak flows may be missed altogether if precipitation stations in the basin are not properly measuring local rainfall variations, especially in summer. Rainfall data from nearby stations and corrections for gauge catch deficit may have to be considered to improve the quality of data.
6. The *recession coefficient* should be revised if the model reacts too quickly or too slowly in comparison with the actual hydrograph. If the computed hydrograph generally rises or drops too rapidly, recession coefficients are too low, probably as a result of including non representative points in

evaluating Equation (6) (Figure 6). Consideration should be given to which points to include when drawing the line. In addition, if the lower envelope curve is being used, other curves such as the average or even the three-quarters line should be tested as alternatives. On the other hand, if the hydrograph rises or drops too slowly the recession coefficients are too high. This usually results from insufficient data available for high flows when deriving Equation (6).

7. Discrepancies in the timing of flow peaks and valleys can be due to an incorrectly determined *time lag*. Re-evaluation of the time lag is called for with special consideration given to a seasonal change in the discharge time lag as the snow cover retreats to higher elevations further from the stream late in the snowmelt season. The model is setup to handle seasonal variations in the time lag.

OPERATION OF THE MODEL FOR REAL-TIME FORECASTS

A few modifications of the model are necessary to operate it in the forecast mode as opposed to operation in the simulation mode. Most important is acquisition of forecasts of the major input variables – temperature, precipitation, and snow cover – during the forecast period. The most difficult of these variables to forecast is precipitation. Generally, average daily values of precipitation or selected historical time series will have to be used. Temperature forecasts can be obtained for several days to one or two weeks. For longer durations, average values should be used and should be as good as forecasted values. The temperature forecasts are doubly important because of the effect of the temperature on the depletion of the snow cover.

The use of snow-cover depletion curves from prior years is not possible because the curves vary from year to year, and the actual curve for a given year is not known at the beginning of the snow-melt season. In order to forecast the snow-cover depletion, it is first necessary to modify the depletion curves by relating the snow coverage to accumulated degree-days instead of elapsed time.

When using standard depletion curves, which relate the percent of the basin or zone covered by snow to elapsed time during the snowmelt season, it isn't possible to detect extreme high or low accumulations of snow. In addition, a steep decrease of the snow-covered area in the standard depletion curve can reflect either a shallow snowpack or high melt rates. Conversely, a slow decrease results from either a deep snow cover or slow melt rates resulting from low temperatures. Such uncertainty can be eliminated using modified depletion curves that relate the snow-covered area to the accumulated number of degree-days.

Figure 14, 15, and 16 show such modified depletion curves derived for the years 1976, 1977, and 1979 for each elevation zone of the South Fork basin in Colorado. It is immediately evident that the same incremental number of degree-days results in a greater decrease in snow cover in 1977 than in 1979 as a result of the much below normal 1977 snowpack. Resulting runoff for the year 1976 falls between the high runoff year of 1979 and the record drought year of 1977 as do the modified depletion curves for 1976 in Figures 14, 15, and 16. In a future year, if a modified depletion curve in the first month of the snowmelt season takes a course similar to that of 1977, a small snow accumulation like 1977 is indicated. Similarly, large accumulations like 1979 and intermediate snow amounts like 1976 can be estimated from the course of the modified depletion curves in the initial stage of the snowmelt season. Note, however, that this technique for

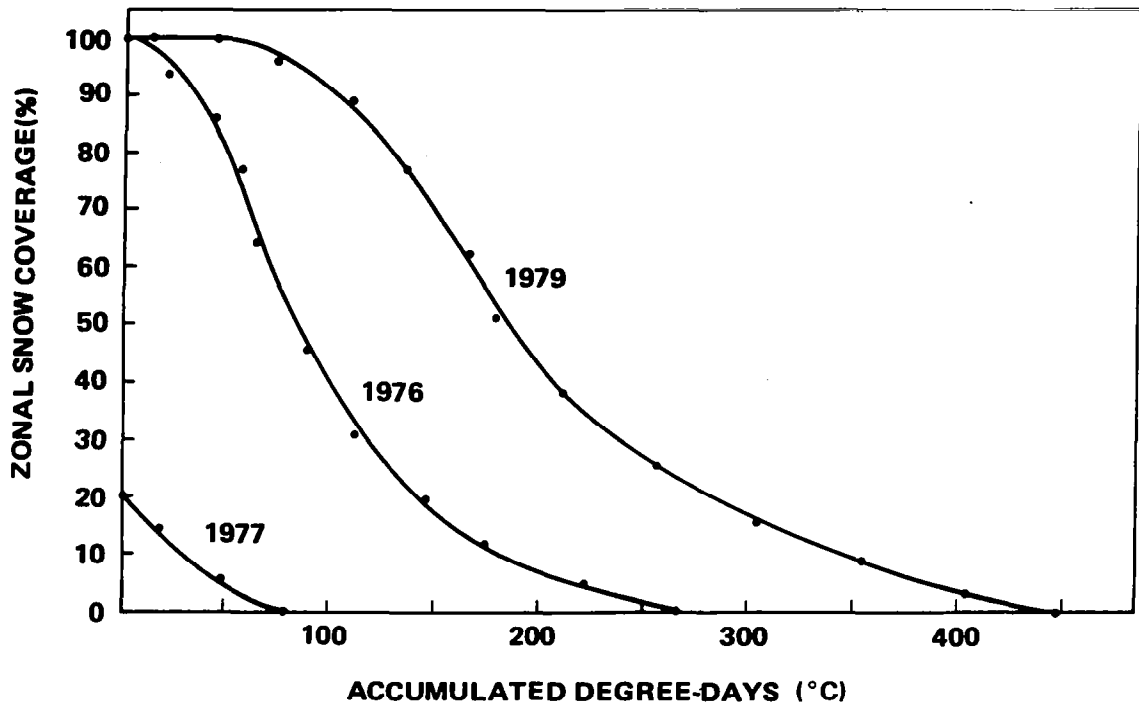


Figure 14. Depletion curves of snow coverage versus accumulated degree-days in elevation zone A of the South Fork basin in the years 1976, 1977, and 1979.

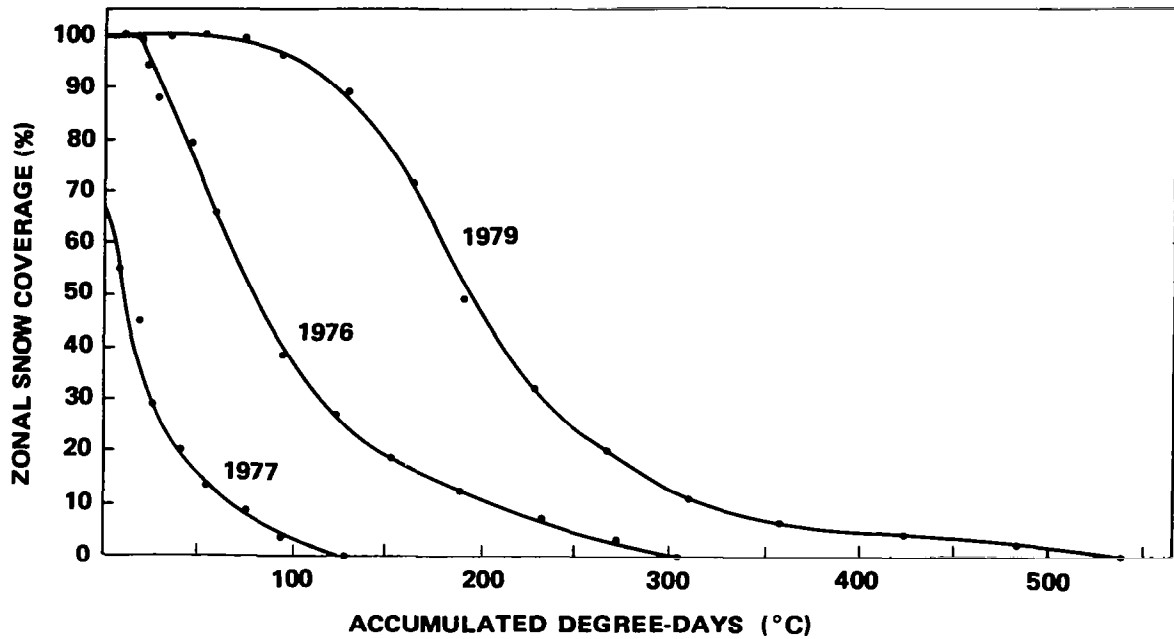


Figure 15. Depletion curves of snow coverage versus accumulated degree-days in elevation zone B of the South Fork basin in the years 1976, 1977, and 1979.

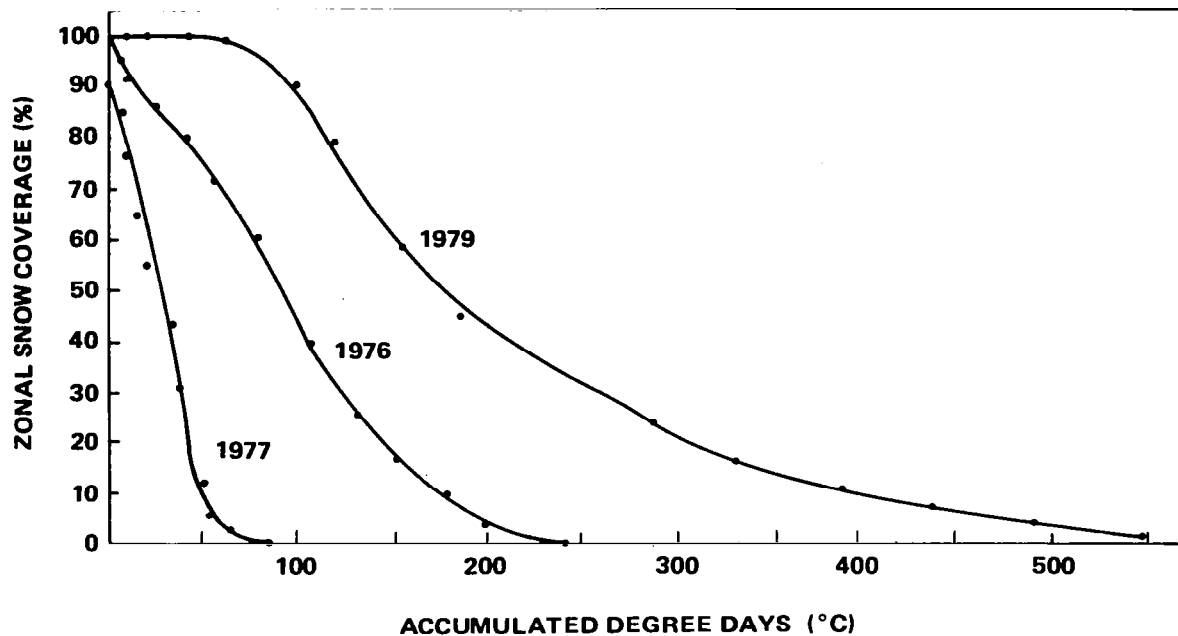


Figure 16. Depletion curves of snow coverage versus accumulated degree-days in elevation zone C of the South Fork basin in the years 1976, 1977 and 1979.

estimating relative snow accumulations is only valid for comparable precipitation amounts occurring during the snowmelt period. For example, exceptional spring and summer snowfalls can slow down the decrease of snow coverage even with a shallow initial snowpack.

To demonstrate the application of the method for operational purposes, assume that a forecast of the seasonal runoff volume is required on 1 April. The zonal snow-cover depletion curves for the snowmelt season are not yet known. As a result, an average snow accumulation must be assumed, and the corresponding modified depletion curves must be chosen. If conventional or automatically measured snow water equivalent values are available for the basin, a better estimate of the snow accumulation may be possible. In this case, a better choice of the appropriate modified depletion curve should result. After several weeks, the first evaluations of snow-covered area from satellite images can be related to the accumulated degree-days to determine whether the decrease of snow-covered area agrees with the initially chosen modified depletion curve. If the comparison is close, the snowmelt-model comparisons are continued until the disappearance of snow and the seasonal runoff volume is obtained as a total of the calculated daily flows. For these seasonal forecasts, the long-term average temperature for each day until the snow disappears can be used for the determination of the degree-day values. A further refinement would be the forecasting of short-term snowmelt runoff. This type of improvement would require the daily forecasts of temperature during the forecast period as previously mentioned.

If the decrease of snow-covered area has not occurred at the rate initially assumed on 1 April, e.g., it is considerably slower than indicated by the assumed modified depletion curve, a greater accumulation of snow for the basin is indicated. Consequently, the initial modified depletion curve is

rejected, and an updated forecast of the runoff volume is made by using the curve valid for a large accumulation of snow. The better the original estimate of snow accumulation, the less the original seasonal forecast will have to be modified. When several years of snow accumulation, satellite snow cover, and snowmelt-runoff data are available, a nomograph of modified depletion curves will be possible, with the appropriate depletion curve chosen by average snow water equivalent rather than similarity to some prior year as shown in Figure 17.

Figure 18 shows a modified depletion curve on the left that has hypothetically been selected based on the best knowledge available from snow accumulation data. If a discharge forecast is to be issued, for example, on May 15 for the following week, the depletion curve is extrapolated as follows. The snow coverage is, as shown in Figure 18, 80%. If 30 degree-days are forecasted for the next week, a drop in snow cover to 40% results, and the "normal" depletion curve is extrapolated as shown on the right side of Figure 18. Forecasted temperatures and extrapolated snow-covered areas are used to compute the meltwater production. If the forecast gives temperatures below the freezing point, the snow coverage will remain at 80% and no snowmelt will result.

In an operational situation, it is not necessary to continuously run the model with calculated streamflow as input data. SRM has the provision which allows updating with actual streamflow information every seven days. The use of real data for such updates will improve the accuracy of the forecasts.

Figure 19a shows a model runoff simulation for the Dinwoody Creek basin in Wyoming that had a measured discharge twice as high as the computed value on August 1. Updating the model with the actual discharge on August 1 improves the simulation as shown in Figure 19b. Even without updating, however, the initial discrepancy is soon eliminated automatically. This self-adjusting feature depends on careful assessment of Equation (6).

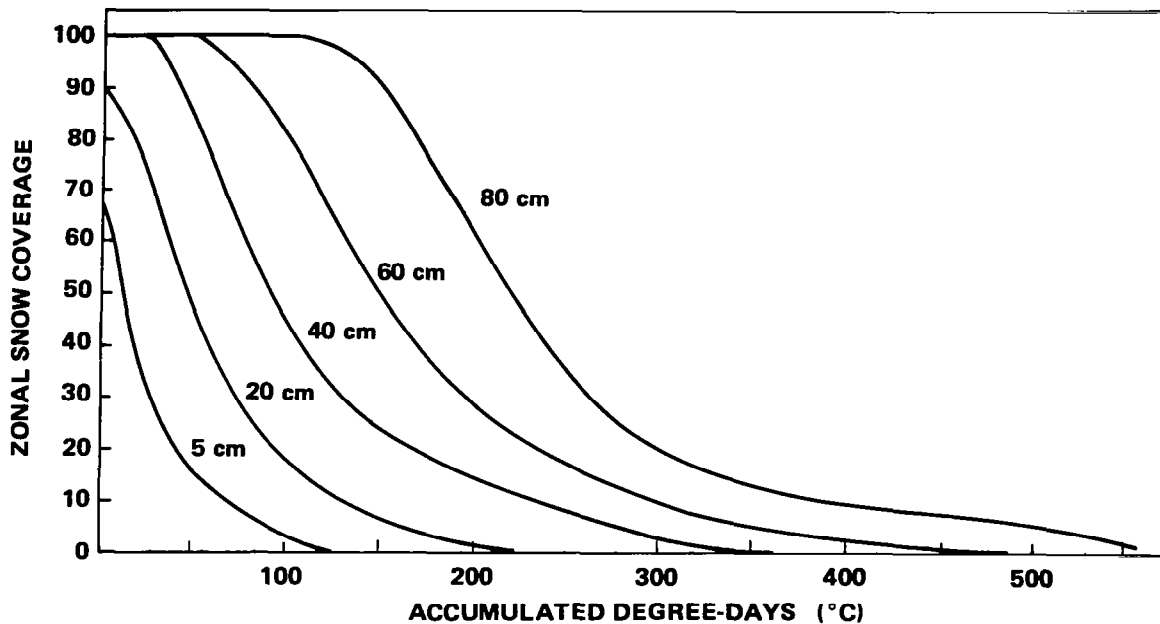


Figure 17. Nomograph for selection of modified depletion curve in zone B of the South Fork basin using estimated snow water equivalent (in cm) as the criterion.

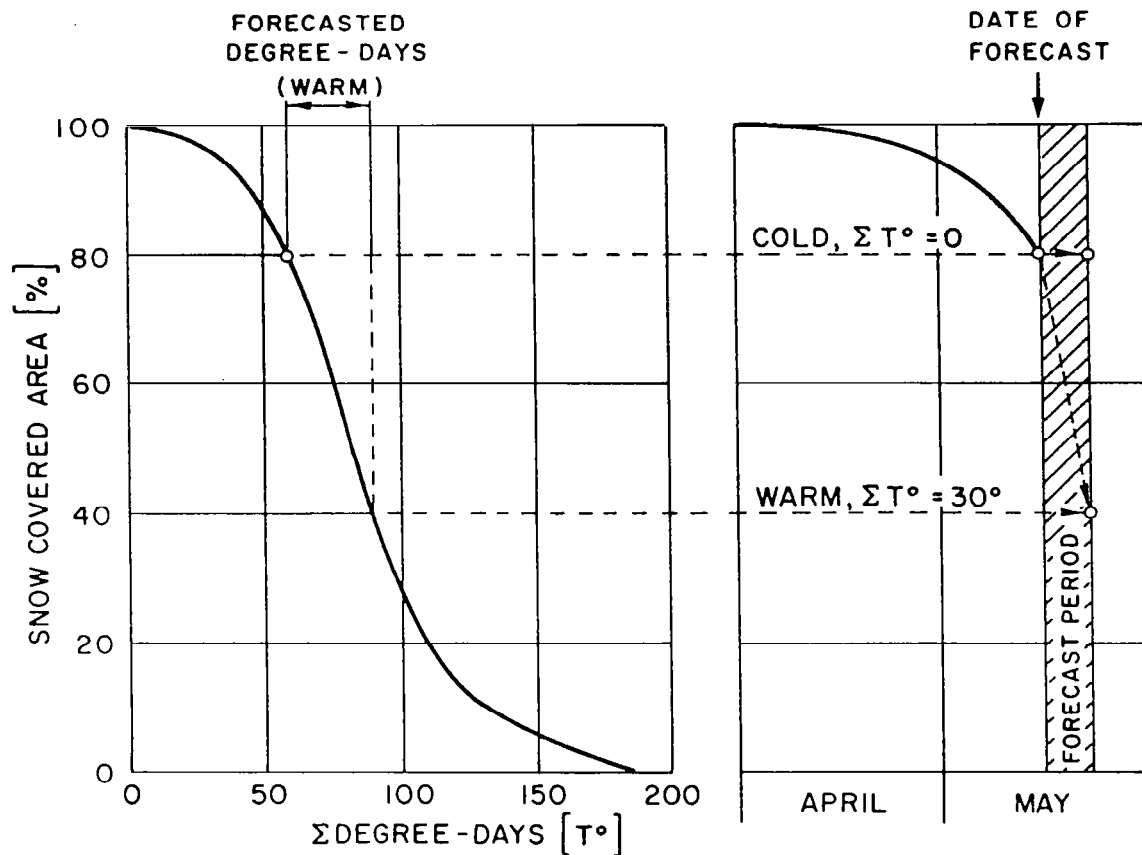


Figure 18. Graphical extrapolation of depletion curves of snow coverage using forecasted degree-days.

NECESSARY COMPUTING FACILITIES

For use of SRM in situations where manpower is not limited but computing resources may be, any pocket calculator with the function x^y is sufficient for day-to-day computation of the discharge. The pocket calculator can also be used in the same way for limited day-to-day forecasts of discharge. In addition, in the initial stages of setting up the computer program to run SRM, the pocket calculator can be indispensable in the checking of computations. The fact that the basic form of SRM (Equation 1) is relatively simple, which permits use of the now widely available pocket calculator, also opens the possibility that the model may be run in the field or at local offices as opposed to only at central computing facilities. Such flexibility increases the chances that SRM can be used in operational situations.

In utilizing the model, it is naturally more convenient to use a computer program (and a computer), an example of which is described in the following section. The use of the computer approach provides a great savings in time which is especially important for calculations of extended periods, such as the snowmelt runoff season or even a year. In addition, the computer program can easily handle many complicated calculations which become extremely tedious on a pocket calculator. Examples of this involve the different handling of precipitation depending on the form (rain vs. snow), the introduction of different time lags for different elevation zones, and the use of multiple climatic stations.

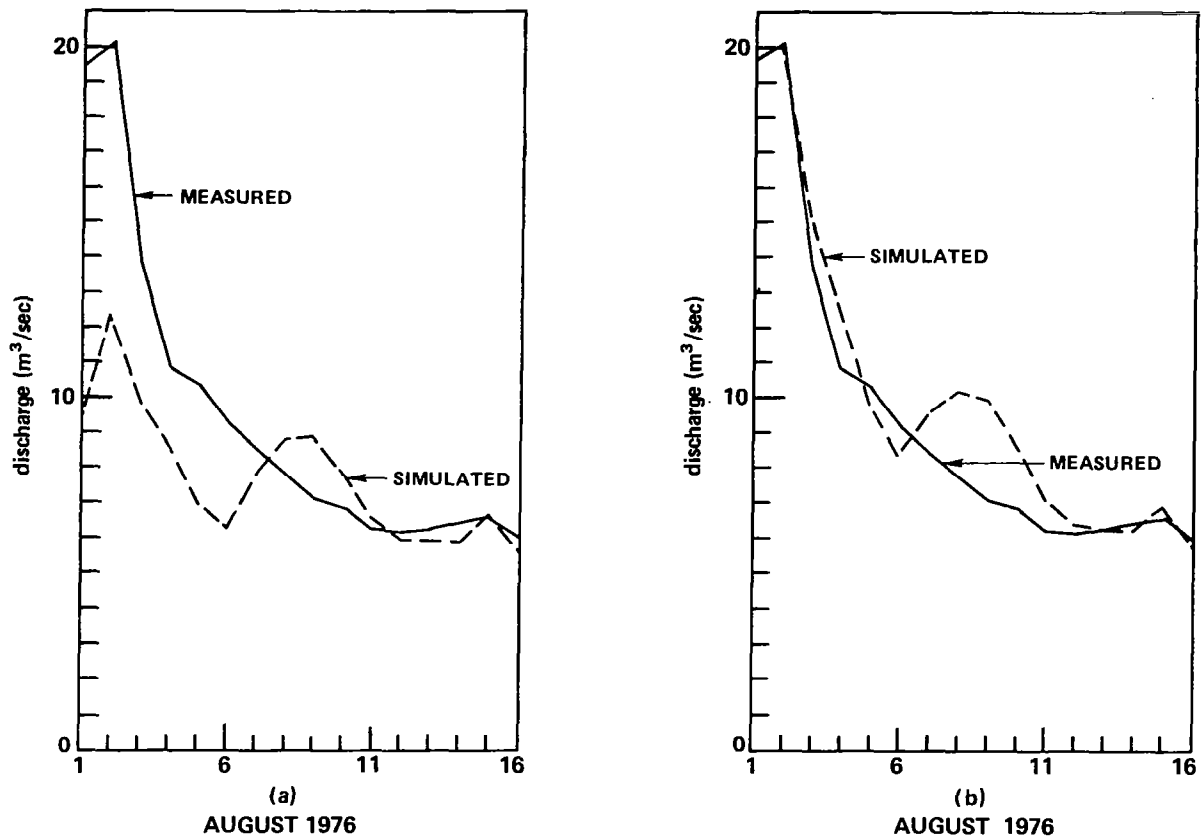


Figure 19. Discharge simulation in the Dinwoody Creek basin a) without updating and b) with updating with actual discharge on 1 August.

SRM is more flexible in its applications when the computerized approach is used. Several computer runs may be made in a short time period in order to demonstrate the effect of hypothetical changes of temperature on the resulting runoff in any desired number of variations.

In general, however, SRM does not require numerous runs because calibration is not necessary. The ease with which computer runs for various sets of parameters can be obtained should not lead to a replacement of the deterministic approach of the model by a "try and see" philosophy. The model is designed to operate with physically-based estimates of basin parameters which should not require much change after their initial selection. Inclusion of a self-calibrating routine might improve the accuracy of simulations, however, it would limit the use of the model to basins with historical data necessary for such optimizing. Also it would deprive the user of the possibility to detect errors in data sets.

The SRM computer program presented in this manual has been designed to operate on an IBM 3081 available at Goddard Space Flight Center (GSFC). However, the SRM program can execute on any 32-bit IBM computer using FORTRAN IV. The program can run on any minicomputer that utilizes FORTRAN IV with the NAMELIST feature, with minimum revisions (such as variable type declarations). Some versions of FORTRAN on some computers do not support the NAMELIST input

of data, particularly the DEC PDP FORTRAN or PDP FORTRAN-FOUR-PLUS. Consequently, major revisions would have to be made in subroutine READIN to read input data as formatted input. No changes, however, would have to be made in the program computations.

Some computers may have peripheral output devices that are not in 132-character length. If so, then some modifications would have to be made in the formatting of output data. Since formatting of output data is provided as an option in the program, the user may not want to exercise that option and simply print out the statistics (such as goodness of fit, etc.).

In order to execute the program on much smaller computers, such as microprocessors where execution time and core storage is limited, some major modifications would have to be made. All formatted output options can be eliminated, except for output statistics. The number of elevation zones can be cut down to reduce the size of the input arrays. The capability to process input temperatures can be eliminated, thus eliminating some input arrays. The user would have to provide input temperatures in degree-days and per zone, or at least provide a pre-determined lapse rate to extrapolate temperatures in degree-days to each elevation zone.

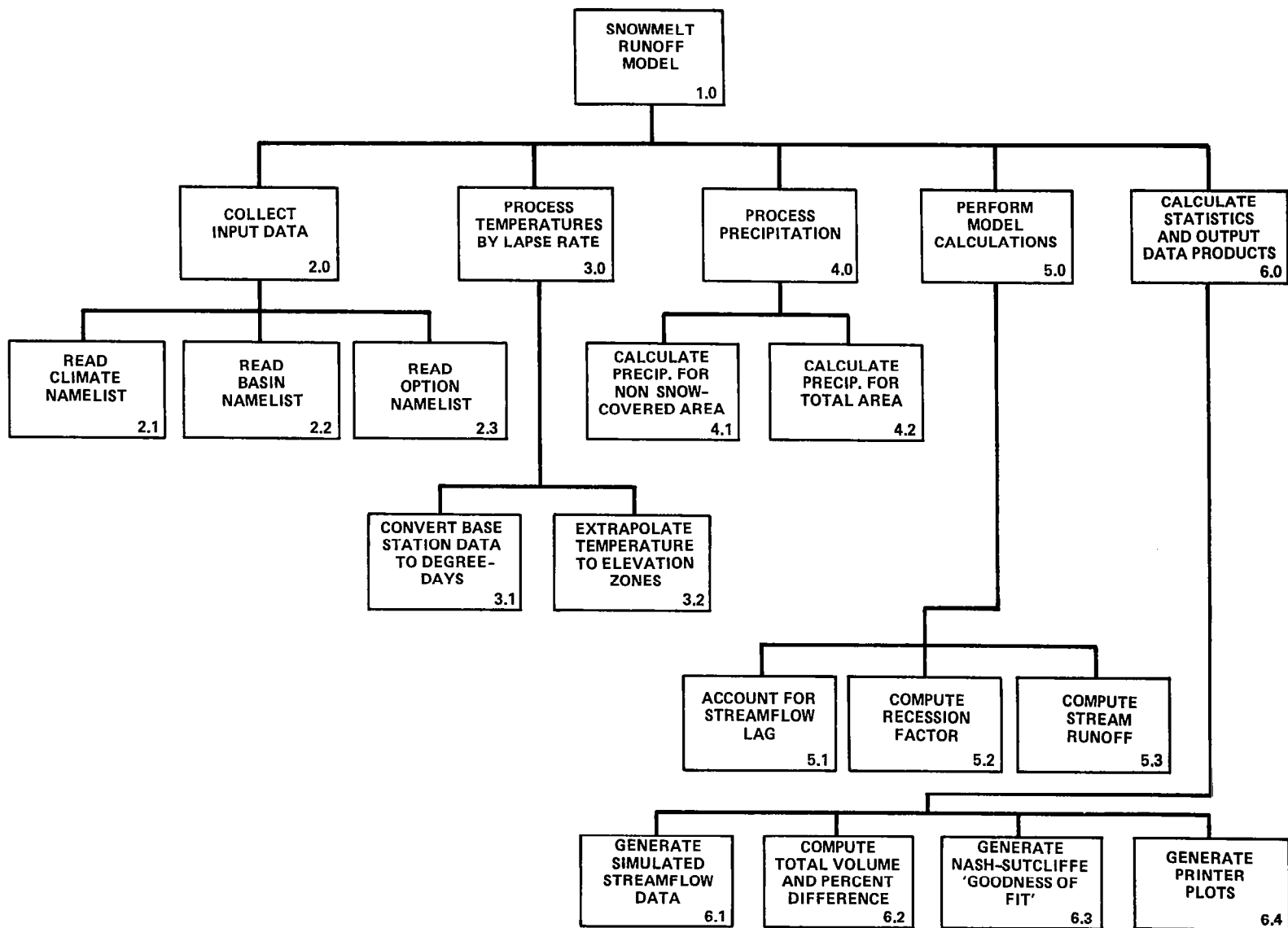
Presently, the SRM program can be run for a snowmelt season of variable length, and it can also be operated in both snowmelt and non-snowmelt situations for up to 366 days. Up to eight basin elevation zones can be accommodated. For a six-month snowmelt season, the computer requirements to execute the program on the GSFC IBM 3081 are as follows: CPU time = 3 sec.; I/O time = 35.4 sec. Total core requirements for compilation, linkage and loading of input data sets, producing printer plots and input temperature processing amount to approximately 170 K bytes of core.

COMPUTER PROGRAM

The SRM program has been implemented on the IBM 3081 at NASA's Goddard Space Flight Center in Greenbelt, Maryland and written in the FORTRAN IV language. The general block diagram for the SRM computer program is shown in Figure 20. A more detailed functional flow diagram is shown in Figure 21 with indications of inputs required, computations, and output products. The detailed program flow chart used in writing the program is shown in Appendix A. The FORTRAN IV source listing for the SRM program and compilation on the IBM 3081 at Goddard Space Flight Center is shown in Appendix B.

The SRM program can be executed using a batch job stream submitted via cards or via a cathode ray tube (CRT) terminal depending on the computer system configuration available as shown in Figure 22. If the user system maintains a time sharing system like the Time Sharing Option (TSO) on the IBM 3081, the user can interactively modify input parameters via a CRT provided the NAMELIST data can be stored on permanent disk files. If only batch job processing via cards is available, the user can manually modify the input card deck.

User control of output from the SRM program is by input program options. Plots of actual and predicted stream runoff are available as an option provided the FORTRAN PRPLOT software supplied in Appendix B is compiled with the SRM program and the user system facilities are capable of producing printer plots. All input data may be reproduced as output during each computer run as an option. Statistical parameters such as the Nash-Sutcliffe goodness-of-fit measure and percent seasonal differences are output automatically, provided that actual streamflow data are available.



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Figure 20. Functional flow chart of the snowmelt-runoff model computer program.

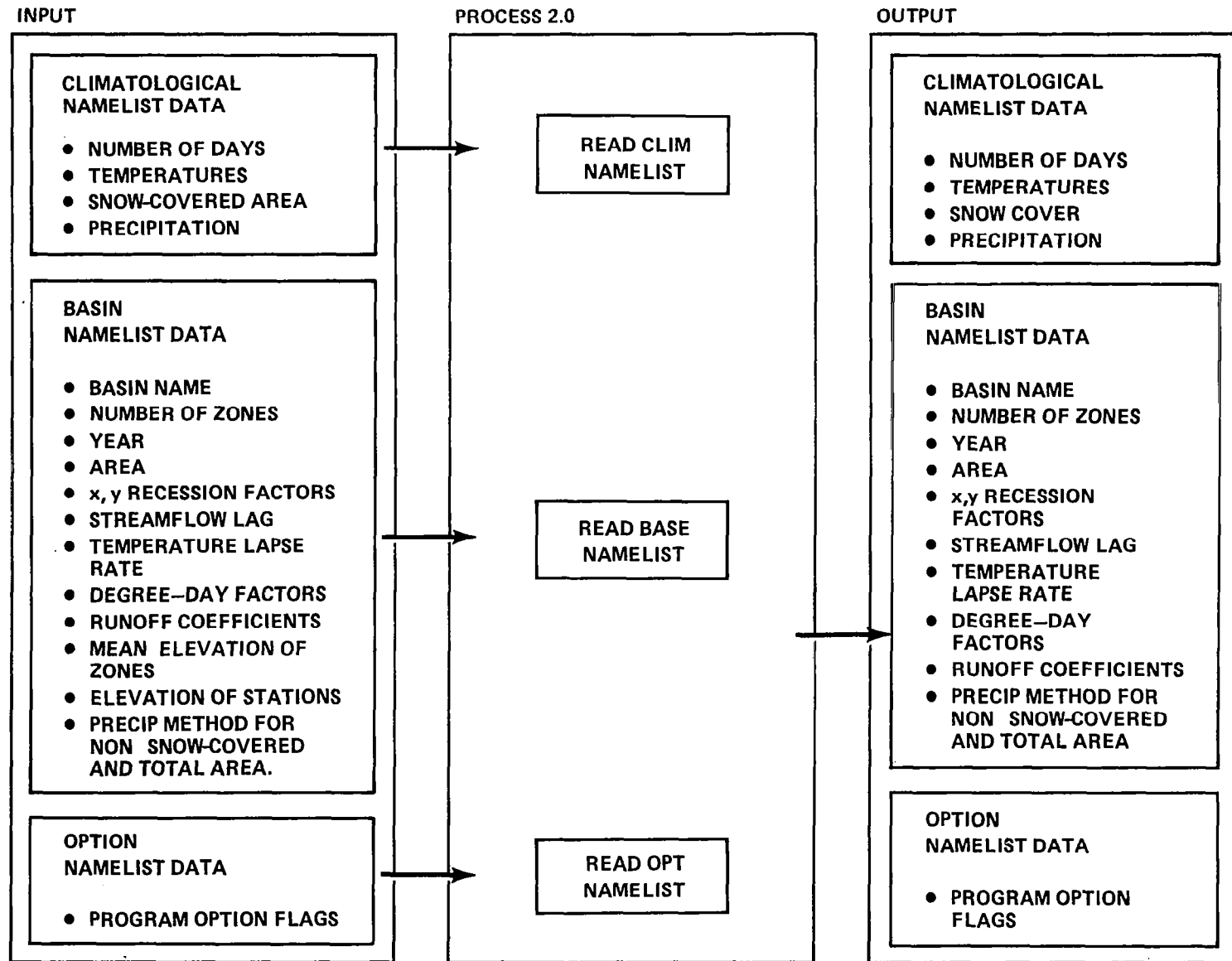
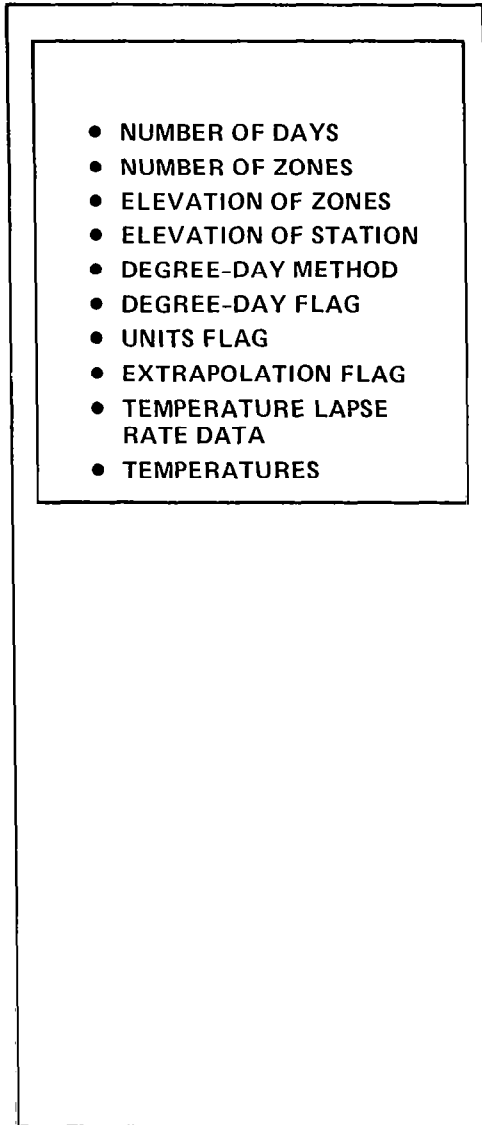
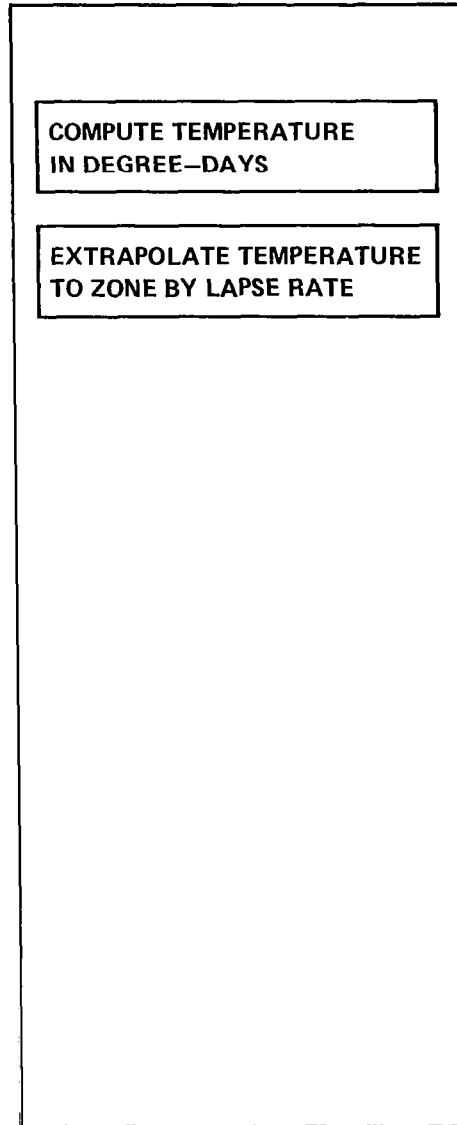


Figure 21a. Process-oriented flow chart of the computer program (reference 2.0 Collect Input Data in Figure 20).

INPUT



PROCESS 3.0



OUTPUT

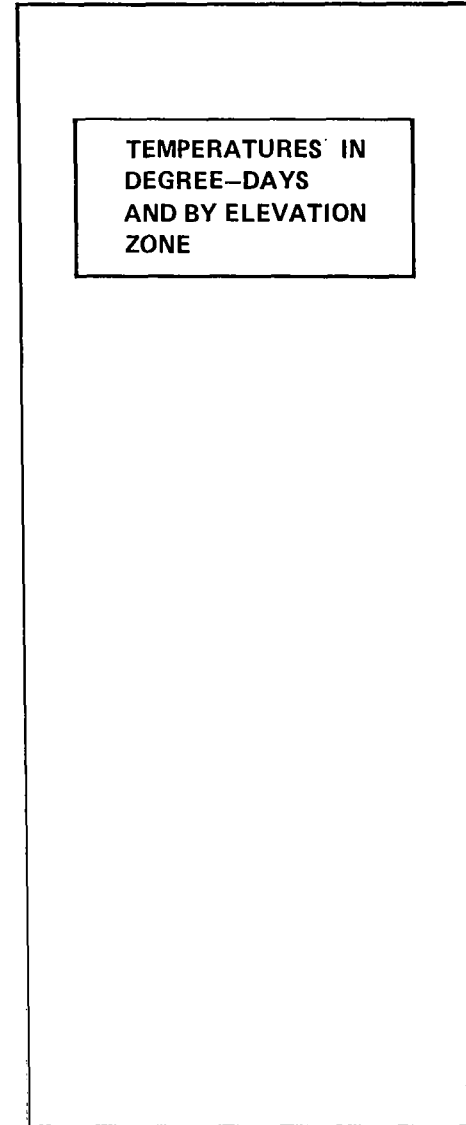


Figure 21b. Process-oriented flow chart of the computer program (reference 3.0 Process Temperatures by Lapse Rate in Figure 20).

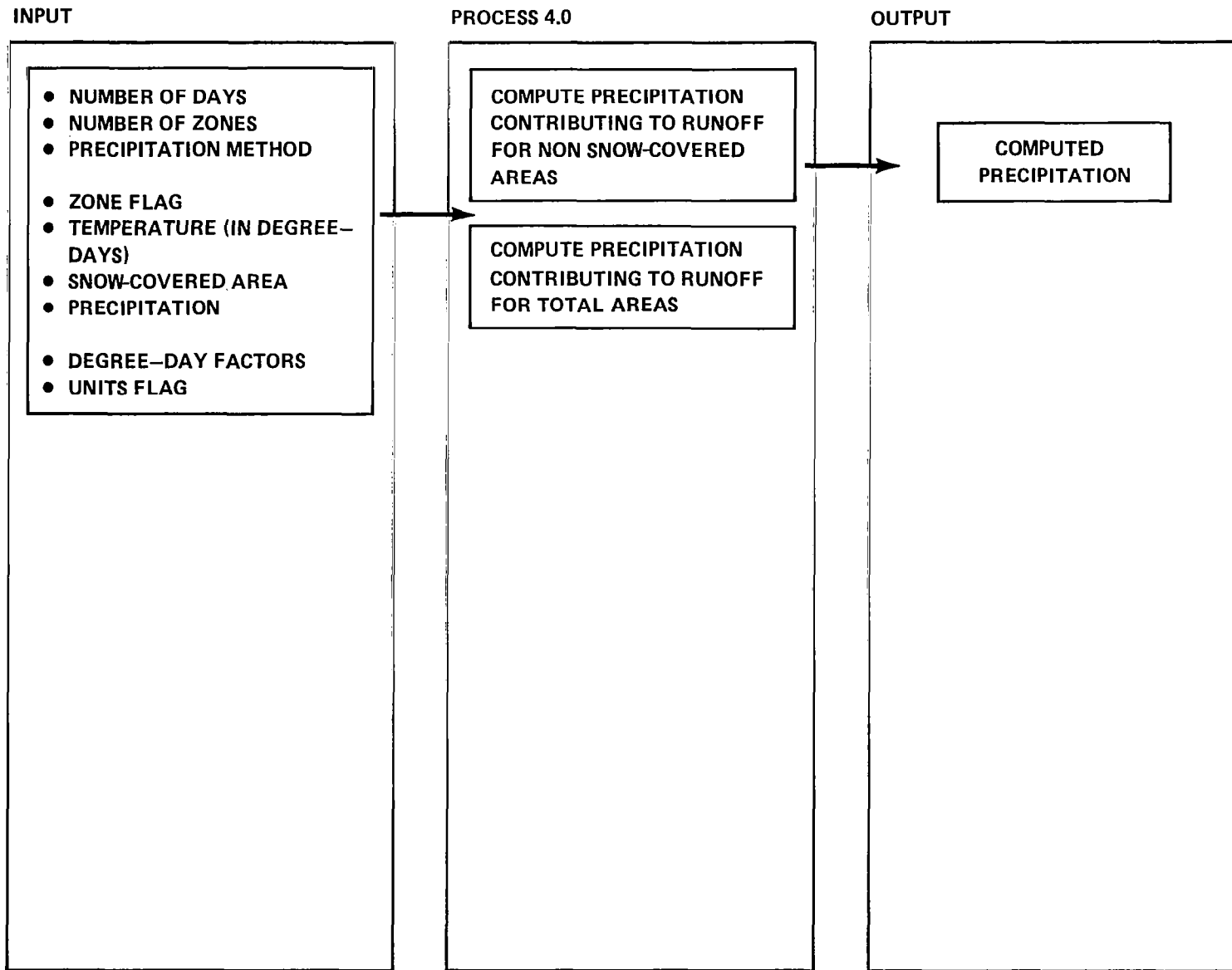


Figure 21c. Process-oriented flow chart of the computer program (reference 4.0 Process Precipitation in Figure 20).

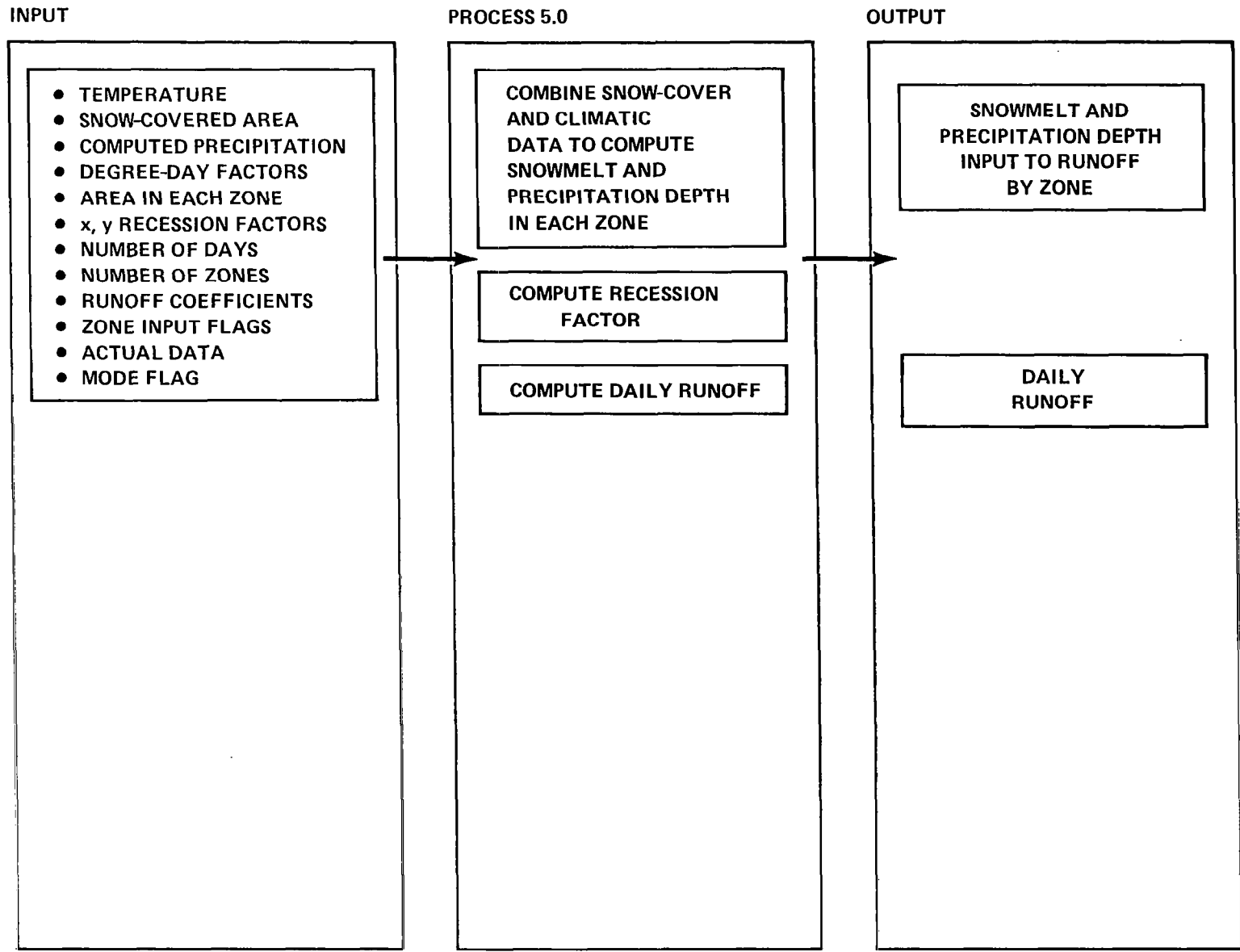


Figure 21d. Process-oriented flow chart of the computer program (reference 5.0 Perform Model Calculations in Figure 20).

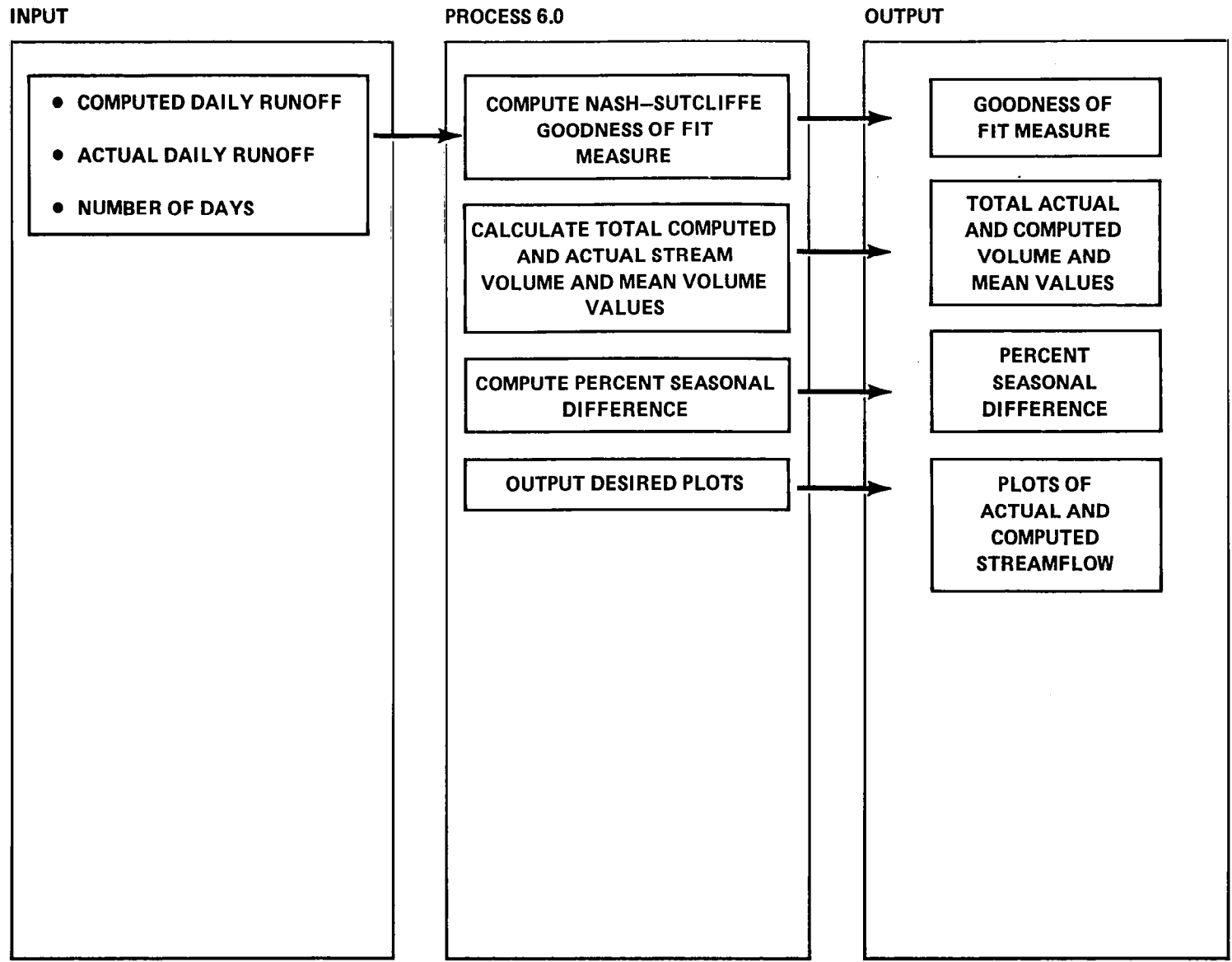


Figure 21e. Process-oriented flow chart of the computer program (reference 6.0 Calculate Statistics and Output Data Products in Figure 20).

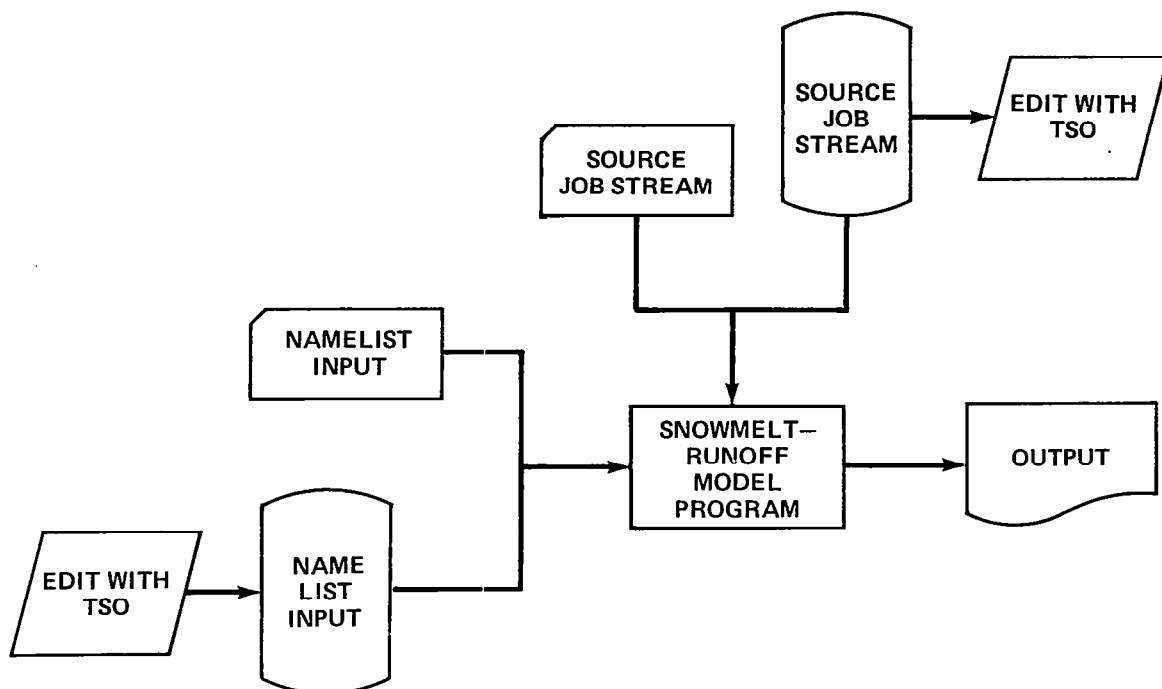


Figure 22. User perspective of snowmelt-runoff model program.

Program Input Requirements

In order to operate the SRM program, precipitation (PRECIP), temperature (T), and snow-covered area (S) must be evaluated on a daily basis (computer symbols for variables and parameters may differ from prior formulation symbols but can usually be recognized by all upper case letters). At the beginning of each computer run, the length of the simulation period in number of days (ND) must be designated (from 1 to 366). If the basin has a large elevation range, the total area must be divided into elevation zones as indicated previously. The total number of elevation zones (NZ) and the area of each zone (AREA) must be input to the program. The program has the capability for handling a total of eight elevation zones, if necessary.

Certain parameters for a specific basin must be evaluated for input to the model:

1. The adjustment by temperature lapse rate (ΔT in Equation 1 and DTLR in the computer program) determined every 15 days, if necessary, and for each elevation zone.
2. The degree day factors (a in Equation 1 and AN in the computer program) determined every 15 days.
3. The runoff coefficients (c in Equation 1 and CS or CR in the computer program) determined every 15 days.

4. The recession coefficient factors (x and y in Equation (6) and X and Y in the computer program, respectively). The recession coefficient, k, changes daily because of the changing discharge, Q, however, the constants x and y are derived one time for the given basin.
5. The percentage of the previous day's snowmelt appearing as runoff at the stream-gage, PDR.

Namelist Parameters

Data to be input to SRM will be handled through the FORTRAN NAMELIST feature. The NAMELISTs CLIM and BASE provide climatological and basin dependent parameters, respectively, whereas the NAMELIST OPT provides program control options to properly execute the SRM program. Use of the NAMELIST feature results in some specific requirements:

1. Column 1 of each card image must be blank,
2. In Column 2, the first card image must contain &CLIM, &BASE, or &OPT.
3. Data items must be separated by a comma.
4. The last item in the last card image must be &END.

Despite these requirements NAMELIST input is easier for the user than formatted input because placement of data in specific card columns is not necessary.

The NAMELIST CLIM contains climatological snowmelt-runoff parameters for a particular basin and is read in only once per snowmelt-runoff computer run. A description of each climatological NAMELIST parameter, including, type, symbol and units are provided in Table 2. Temperature (T) and precipitation (PRECIP) data are not required to be input by elevation zone but can be extrapolated to the elevation zone from the base station readings in the program. Snow-covered area (S) must be input by elevation zone. In order for the SRM program to operate correctly, daily temperature values must be in degree-days for each elevation zone. Temperatures may be input as measured average daily temperatures or as maximum (TMAX) and minimum (TMIN) values and, through application of the temperature lapse rate, be extrapolated to the appropriate elevation zone. Temperatures can also be input already calculated in degree-days where no extrapolation is necessary. All of the parameters in the climatological NAMELIST CLIM must be provided. If no actual streamflow data are available, the user should provide an estimated value for the ACTUAL parameter on day 1 of the snowmelt-runoff period. Figure 23 shows typical climatological NAMELIST input for a study basin in Switzerland.

The NAMELIST BASE contains basin dependent SRM parameters and can be read in several times allowing the user the capability of making several computer runs without having to read in all of the climatological NAMELIST parameters. A description of each basin NAMELIST parameter including type, symbol and units are provided in Table 3. In order to execute the SRM program certain minimal basin NAMELIST input is required. These parameters include:

1. Identifying Information
BASIN, NZ, IYEAR
2. Snowmelt-Runoff Model parameters
AREA, X, Y, PDR, DTLR, AN, CS, CR, IPR

Table 2. Description of Variables in NAMELIST CLIM

Variable	Symbol*	Type	Units		Description
			Metric	English	
ND	n	I*4	days	days	Number of snowmelt days
T	T _n	R*4	°C-day	°F-day	Temperature in degree-days
S	S _{zn}	R*4	%	%	Snow-cover area in each zone (100% = 1.0)
ACTUAL	Q _n	R*4	m ³ s ⁻¹	ft ³ s ⁻¹	Actual stream runoff
PRECIP	—	R*4	cm	in	Precipitation at base station
TMAX	—	R*4	°C	°F	Maximum daily temperature
TMIN	—	R*4	°C	°F	Minimum daily temperature
TCRIT	T _{CRIT}	R*4	°C	°F	Critical temperature to determine if precipitation is rain or snow.

*Note: The subscript n refers to number of snowmelt days; zn refers to number of snowmelt days per zone.

```

SCLIM
ND=365,
S=.88, .88, 48.875, .87, .87, .865, .865, .865, .86, .86, .855,
.85, .85, .845, .84, .835, .835, .83, .83, .825, .825, .82, .82,
.815, .81, .805, .80,
.80, .795, .795, .79, .785, .78, .775, .77, .765, .76, .76, .755,
.745, .735, .725, .717, .70, .68, .66, .64, .60, .56, .52, .48,
.44, .40, .37, .34, .31, .28, .25,
.23, .215, .20, .185, .179, .17, .16, .15, .14, .135, .125, .115,
.11, .105, .10, .095, .090, .085, .08, .075, .07, .065, .06, .055,
.05, .045, .04, .035, .035, .03,
.03, .025, .025, .02, .0183, .015, .01, .005, 23*0.,
31*0., 91*0., 121*1.0, 0.,
58.93, 58.925, 58.92, 58.915, 58.91, 38.905, .90, .90,
58.90, 38.895, .89, .89, .885, .885, 38.88, .877, .875, .87, .865,
.86, .855, .85, .845, .84, .835, .83, .825, .82, .815, .81, .80,
.80, .795, .79, .785, .776, .77, .77, .75, .74, .735, .725, .715,
.705, .695, .685, .67, .66, .65, .64, .63, .62, .61, .60, .59,
.58, .565, .55, .54, .53, .52,
.51, .50, .49, .48, .464, .45, .44, .43, .415, .40, .385, .37,
.36, .35, .34, .33, .32, .305, .29, .28, .27, .26, .245, .23, .22,
.21, .195, .18, .17, .16, .155,
.15, .145, .14, .13, .115, .11, .105, .10, .095, .085, .08, .075,
.0665, .05, .045, .04, .035, .03, .025, .02, .015, .01, .01, .05,
7*0., 91*0., 121*1.95, 0.,
.85, .845, .845, .84, .84, .835, .835, .83, .83, .83, .825, .825,
38.82, .815, .815, 38.81, 10*0.005,
158.805, .804, 94.80, 58.795, .79,
48.79, .786, 38.785, 38.78, 188.785, .79,
38.79, .795, .797, .795, .79, .785, .78, .775, .77, .76, .75, .74, .73,
.72, .71, .70, .69, .675, .66, .645, .63, .615, .60, .585, .57,
.56, .55, .54, .53,
.52, .51, .50, .49, .48, .47, .44, .45, .44, .435, .43, .42, .413,
.40, .385, .38, .37, .36, .35, .345, .34, .33, .32, .31, .30, .29,
.28, .27, .26, .255, .25, 918.25, 1218.90, 0.,
ACTUAL=.60, .63, .67, .71, .74, .75, .80, .84, .89, .95, .96, .99,
1.07, 1.23, 1.16, 1.01, .92, .85, .81, .78, .77, .77, .78,
.80, .76, .75, .74, .74, .80, .84,
.80, .76, .74, .77, .77, .76, .79, .87, .97, 1.10, 1.14, 1.12,
1.23, 1.47, 1.55, 1.85, 2.20, 2.48, 2.84, 2.93, 3.03, 3.51,
3.27, 2.72, 2.46, 2.40, 2.63, 2.83, 2.70, 3.04, 4.05,
4.51, 3.78, 4.02, 4.85, 5.83, 6.33, 4.92, 3.99, 3.63, 3.26, 2.92,
2.67, 2.43, 2.54, 2.84, 2.93, 3.17, 3.67, 3.41, 3.57, 4.11, 5.44,
5.28, 5.59, 4.81, 5.01, 6.10, 5.61, 5.93, 5.61,
3.62, 6.68, 6.53, 6.23, 6.06, 6.18, 6.20, 5.29, 5.21, 6.61, 6.52,
6.65, 6.84, 7.86, 8.72, 6.60, 7.16, 7.14, 5.34, 4.54, 4.48, 4.12,
4.06, 4.15, 5.08, 4.16, 4.31, 4.53, 4.39, 4.44, 4.81,
4.48, 4.23, 4.42, 4.32, 4.60, 4.04, 3.81, 4.90, 4.03, 3.60, 3.54,
3.24, 3.09, 3.11, 3.18, 3.24, 3.25, 3.17, 3.12, 2.99, 2.90, 2.83,
2.79, 2.67, 2.99, 2.55, 2.52, 2.45, 2.25, 2.13, 2.08,
2.57, 2.16, 2.16, 2.94, 2.38, 2.43, 2.52, 2.27, 2.17, 2.37, 2.19,
2.08, 2.02, 1.97, 1.93, 1.90, 1.82, 1.75, 1.72, 1.78, 1.73, 1.64,
1.58, 1.59, 1.55, 1.53, 1.52, 1.58, 1.61, 1.52,
1.52, 1.47, 1.41, 1.43, 1.39, 1.35, 1.30, 1.33, 1.29, 1.26, 1.23,
1.21, 1.15, 1.13, 1.11, 1.08, 1.07, 1.04, 2*1.03, 1.01, 0.99, 0.98,
0.96, 0.95, 0.94, 0.94, 0.93, 0.93, 0.91, 0.89,
0.88, 0.87, 0.86, 0.86, 0.84, 0.83, 0.82, 0.84, 0.81, 0.81, 0.78,
0.78, 0.78, 0.77, 0.76, 0.77, 0.77, 0.75, 0.77, 0.75, 0.74, 0.73,
0.72, 0.71, 0.71, 0.70, 0.71, 0.70, 0.71, 0.69,
0.69, 0.69, 0.67, 0.67, 0.67, 0.67, 0.67, 0.66, 0.66, 0.65, 0.65, 0.64,
0.63, 0.62, 0.60, 0.63, 0.63, 0.62, 0.61, 0.60, 0.59, 0.59, 0.57,
0.57, 0.56, 0.56, 0.56, 0.55, 0.55, 0.56, 0.52, 0.54,
0.56, 0.53, 0.52, 0.51, 0.51, 0.50, 0.50, 0.50, 0.50, 0.50, 0.50,
0.49, 0.49, 0.48, 0.47, 0.48, 0.49, 0.49, 0.48, 0.47, 0.47, 0.47,
0.46, 0.46, 0.46, 0.45, 0.45, 0.45, 0.45, 0.45, 0.44, 0.44,
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0.42, 0.42, 0.41, 0.41, 0.40, 0.40, 0.40, 0.40, 0.40, 0.40, 0.39,
0.39, 0.39, 0.39, 0.39, 0.39, 0.39,
0.39, 0.38, 0.39, 0.39, 0.38, 0.38, 0.38, 0.37, 0.37, 0.37, 0.37,
0.37, 0.37, 0.37, 0.37, 0.36, 0.36, 0.36, 0.36, 0.36, 0.36, 0.35,
0.36, 0.36, 0.35, 0.35, 0.34, 0.34, 0.34, 0.34, 0.34, 0.34,

```

Figure 23. Sample NAMELIST CLIM input for the Dischma basin, 1974.

```

PRECIP=.19, .06, 0.00, 0.00, .04, .34, 0.00, .01, 5*0.00, .10,
.03, .53, .13, .07, .02, 0.0, 0.00, .03, 0.00, .26, .59,
.31, .02, 0.00, .02, .13,
.21, .22, .03, 0.00, .45, .84, .09, .01, 0.00, 0.00, .27,
.98, 0.00, .02, .27, 5*0.00, .26, 0.00, 3.23, .48, .38, .03,
0.00, .52, .97, 0.00, .02,
1.49, 4*0.00, .37, .02, .06, .07, .41, .85, 1.06, 1.72, .03,
0.00, .66, 0.00, .70, 1.20, 0.00, 0.00, 1.41, .65, 1.59, .09,
0.00, 2.71, .83, 1.33, 1.82,
0.00, .57, 0.00, .89, 0.00, 0.00, 1.03, .03, 0.00, .74, .21,
0.00, 0.00, .20, 3.08, 0.00, .52, 2.96, 1.02, .22, .41, .37,
0.00, 0.00, 1.35, .17, 0.00, .21, 3*0.00,
.45, .05, .78, 0.00, 1.56, 0.00, 0.00, .66, 2.49, .09, .58,
.45, .01, 0.00, .01, 3*0.00, .13, .31, 0.00, .03, .39, .38,
.13, 0.00, .03, 1.97, .01, 2*0.00,
1.18, 0.0, 0.01, 2.13, 0.06, 0.00, 0.88, 0.00, 0.00, 0.88,
0.04, 8*0.00, 0.07, 1.50, 0.02, 0.82, 0.06, 0.35, 2.25,
2.59, 0.00, 2.11, 0.01,
0.12, 0.12, 0.24, 0.05, 0.01, 0.13, 0.05, 1.32, 0.49, 0.94,
0.11, 0.64, 0.20, 0.02, 0.27, 0.05, 0.03, 0.43, 0.00, 0.50,
1.06, 0.66, 0.04, 0.71, 0.30, 0.00, 0.71, 0.60, 1.07, 1.03,
0.21,
0.09, 0.28, 0.24, 0.00, 0.51, 5*0.00, 0.05, 5*0.00, 0.08,
0.00, 0.88, 0.06, 0.08, 0.00, 0.05, 0.00, 0.09, 0.27, 3.80,
0.53, 1.75, 0.61,
5.31, 0.74, 0.10, 0.00, 0.07, 0.40, 0.34, 0.42, 0.04, 0.00,
0.00, 0.03, 0.99, 0.20, 0.00, 0.19, 0.15, 1.76, 1.92, 0.28,
4*0.00, 0.01, 0.02, 0.11, 1.34, 1.21, 0.86, 0.15,
0.48, 0.03, 0.00, 0.00, 0.00, 0.09, 0.01, 1.66, 0.72, 8*0.00,
0.02, 0.13, 0.44, 0.02, 0.13, 0.07, 0.07, 0.01, 0.47, 0.00,
0.26, 2.18, 2.10, 0.29,
0.03, 0.07, 10*0.00, 0.20, 0.20, 0.09, 0.00, 0.01, 0.00, 0.09,
0.38, 0.03, 7*0.00,
6*0.00, 0.03, 0.01, 0.00, 0.11, 0.00, 0.00, 0.07, 0.57, 0.24,
0.36, 0.16, 0.40, 2.10, 0.33, 0.00, 0.00, 0.03, 0.06, 0.47,
0.49, 0.00, 0.00, 0.01, 0.39, 1.52, 0.03,
THAX=-.2, .4, 1.3, 3.7, -2.0, -.7, -.9, -.3, 1.6, -1.0, 1.0, .7,
3.0, 0.0, -7.2, -9.6, -9.0, -6.4, -6.3, -3.2, -4.4, -3.8, -.8,
-4.8, -5.9, -3.0, -4.8, -.3, 0.0, -1.7,
-1.1, -2.2, -2.0, .7, -3.0, -3.7, -3.0, -.7, -1.0, -.6, -1.7,
1.3, 6.8, 3.3, -.7, 2.8, 1.1, 4.2, 5.4, 2.6, 3.7, 2.9, -2.0,
-2.5, -.6, 4.1, 5.2, 3.0, 4.4, 5.1, 4.7,
3.0, 5.2, 8.7, 9.6, 10.3, 4.1, -.8, 1.5, 1.4, -1.8, -4.9,
-4.1, -2.4, 4.4, 5.1, 6.2, 6.3, 2.4, 2.9, 5.4, 5.5, 5.6, 5.7,
3.0, 7.6, 5.3, 3.0, 2.8, 3.8, 3.5,
8.2, 6.6, 6.7, 7.9, 9.6, 8.3, 3.2, 2.7, 8.0, 6.8, 10.3, 12.8,
12.0, 9.7, 9.0, 10.5, 5.9, 1.5, -.5, -1.1, .9, 3.6, 8.2, 13.4,
9.2, 11.0, 13.3, 13.3, 15.5, 14.2, 11.8,
13.2, 11.5, 14.8, 14.6, 10.2, 11.8, 13.5, 10.6, 4.4, 6.2, 3.0,
3.9, 13.5, 16.6, 16.7, 17.5, 17.0, 15.0, 11.7, 11.5, 14.7,
9.7, 8.0, 8.2, 6.8, 8.3, 4.4, 1.9, 9.0, 6.1, 8.5,
8.5, 8.3, 8.4, 4.5, 12.1, 8.6, 4.5, 10.1, 11.0, 6.4,
9.9, 11.5, 12.9, 13.2, 12.6, 11.5, 10.1, 10.2, 10.1, 5.0,
9.1, 4.0, 2.0, 0.2, -4.6, -4.8, 2.0, 2.4, -0.7, -2.4,
-5.7, -6.4, -5.7, -5.1, -5.2, -5.2, -5.0, -4.8, -6.1, -4.8,
-6.0, -5.9, -5.8, -8.0, -6.3, -9.5, -5.8, -1.5, -4.2, -3.1,
-9.0, -5.3, -7.9, -5.7, -0.5, -2.8, -2.0, -5.7, -10.2, -10.7,
-13.0,
-11.3, -8.0, -5.5, -6.5, -8.4, -1.7, 1.4, -0.5, 0.5, 0.5,
-2.0, -2.9, -5.2, -2.8, -0.3, 0.0, -2.1, -0.4, -2.5, -6.2,
-5.7, -0.3, 2.0, -1.6, -3.9, -8.0, -4.8, -3.0, -10.8, -7.0,
-6.1, -1.4, 0.7, 1.8, -1.2, -9.7, -6.2, -3.4, -0.3, -0.7,
-6.5, -12.3, -10.2, -11.0, -8.0, -9.3, -3.9, -5.4, -10.1, -3.3,
3.5, 3.7, 0.7, -1.9, -2.0, -0.5, -0.4, -0.8, -0.3, -1.4, -10.7,
-4.6, 0.2, -0.2, 0.8, -0.4, -3.4, -3.6, -7.6, -3.5, -1.0,
0.8, -1.2, -2.3, -0.4, 0.5, -4.2, -4.2, -4.7, -3.2, -4.5, -5.7,
-7.7, -4.9, -5.4, -2.4, -4.0, -3.9, -6.3, -4.8, -4.8, 1.4,
-2.6, 1.2, -3.8, -11.8, -4.5, -3.0, -2.3, 0.4, -1.0, 0.6, -1.4,
-4.1, -6.2, -9.2, -7.0, -8.8, -3.0, 2.1, -2.1, -7.4, -0.9,
-4.0, -4.9, -6.7, -4.2, -3.5, 1.0, -0.3, 1.6, -0.1, -2.8,
-4.5, -3.4, -4.8, -4.0, -2.3, -2.3, -4.7, -4.5, -5.9, -4.5,
-3.9, -6.6, -7.6, -8.2, -11.3, -8.8, -9.8, -2.2, -5.4, -9.5,
-12.5, -13.1, -4.7, -5.6, -5.3, -10.2, -11.3, -9.5,

```

Figure 23. (Continued)

```

THIN=-5.3, -6.2, -5.6, -3.4, -4.8, -7.4, -6.0, -6.4, -4.9, -5.3,
-7.4, -5.2, -3.9, -8.7, -12.2, -13.2, -14.6, 2*-15.1, -10.2,
-9.4, -9.5, -8.4, -9.1, -10.4, -10.7, -9.9, -5.4, -3.8, -4.8,
-6.2, -7.8, -7.6, -5.2, -6.7, -6.3, -8.0, -5.5, -6.7, -3.7,
-4.4, -7.5, 0.2, -4.4, -7.1, -3.8, -1.1, -3.7, -1.2, 0.1, -.7,
-3.2, -6.9, -7.8, -6.7, -5.2, -1.6, -3.9, -3.6, 0.0, 2.0
-2.4, -6.7, 1.5, 4.4, 3.3, -1.0, -5.9, -5.3, -6.3, -8.2, -7.7,
-6.1, -6.9, -4.7, 1.2, .1, .4, -3.0, -4.6, .2, 0.0, .1, 2.2,
-2.4, -1.4, 2.5, -.7, 0.0, -1.3, -1.3,
2.0, -.4, .7, -2.5, 1.3, 3.0, -2.8, -2.8, .6, 1.1, 2.0, 6.1,
6.8, 3.7, 1.4, 5.0, .8, -2.5, -3.1, -4.6, -1.7, -2.6, 1.0,
2.3, -1.2, -2.4, 4.4, 3.3, 5.3, 6.9, 5.3,
5.9, 6.1, 4.9, 7.3, 1.9, 2.2, 6.4, .5, .2, .2, -2.6, -2.9,
3.2, 8.6, 10.5, 11.8, 11.2, 7.8, 4.8, 6.0, 6.8, 5.1, 4.1, 3.6,
3.3, 3.4, -2.8, -4.4, 1.3, 2.1, 3.2,
0.0, 1.8, 4.0, -2.6, -0.5, -2.1, -4.6, 2.8, 6.0, 0.0, 2.1, 2.8,
4.5, 5.6, 6.4, 4.6, 3.8, 2.6, 3.5, 0.1, -1.5, -2.8, -7.0, -5.7,
-8.6, -7.5, -8.4, -1.7, -7.5, -8.8,
-9.8, -10.2, -11.9, -7.5, -10.4, -9.2, -8.6, -9.8, -9.8, -9.8, -8.6,
-10.7, -12.3, -13.2, -11.7, -12.5, -14.6, -7.1, -6.4, -9.1, -12.3,
-12.9, -12.9, -8.8, -8.2, -8.2, -8.0, -13.0, -13.6, -14.3, -17.1,
-15.1, -15.7, -13.0, -11.0, -12.5, -9.5, -6.8, -7.8, -5.4, -4.8,
-7.0, -7.7, -8.5, -7.4, -4.4, -3.0, -4.7, -5.4, -11.8, -12.8, -8.2,
-7.8, -2.8, -5.3, -12.0, -13.0, -9.4, -13.5, -13.0, -13.5,
-9.0, -10.4, -6.3, -2.0, -10.5, -11.7, -10.6, -6.5, -4.4, -7.0,
-12.5, -17.4, -16.7, -19.0, -11.9, -12.2, -10.2, -13.3, -13.4, -10.3,
-4.0, -1.9, -2.6, -7.9, -6.5, -5.3, -8.7, -8.8, -3.4, -14.8, -15.7,
-10.9, -11.0, -6.6, -6.2, -7.3, -4.6, -8.2, -11.5, -13.9, -7.5, -4.9,
-9.1, -7.2, -5.8, -5.8, -7.0, -6.3, -7.9, -9.3, -10.2, -10.0, -14.4,
-13.9, -8.2, -6.8, -9.7, -7.7, -13.8, -10.8, -10.1, -6.9,
-12.6, -12.6, -13.5, -14.8, -12.5, -5.6, -5.8, -6.8, -6.8, -6.8, -6.8,
-7.1, -9.3, -13.8, -13.8, -13.0, -11.9, -6.1, -7.9, -14.4, -14.4,
-6.6, -8.6, -12.3, -10.8, -10.1, -9.1, -4.5, -2.0, -6.1, -7.0, -8.8,
-9.3, -9.3, -10.0, -7.1, -8.1, -9.3, -7.9, -8.8, -8.1, -9.8, -9.6,
-11.6, -14.0, -15.7, -13.9, -18.1, -12.5, -12.9, -12.7, -15.2, -15.9,
-13.6, -7.9, -14.3, -18.0, -14.0, -15.2,
TCRIT=76*J, .15*2, .62*75, 61*75, 30*1.0, 31*2.0, 62*3.0, 28*3.0,
&END

```

Figure 23. (Continued)

Table 3. Description of Parameters in NAMELIST BASE

Parameter	Symbol*	Type	Units		Description
			Metric	English	
BASIN	—	R*8	—	—	Basin name
NZ	—	I*4	—	—	Number of elevation zones
IYEAR	—	I*4	—	—	Year of model run
AREA	A_z	R*8	m^2	ft^2	Area in each elevation zone
X	x	R*8	m^3s^{-1}	ft^3s^{-1}	X parameter in computing recession coefficient, K
Y	y	R*8	—	—	Y parameter in computing recession coefficient, K
PDR	—	R*4	—	—	Percentage of previous day runoff reaching the stream-gauge
PDM2	—	R*4	—	—	Percentage of runoff if more than 24 hours stream-flow lag.
DTLR	δ_{zn}	R*4	$^{\circ}C/100m$	$^{\circ}F/1000ft$	Average temperature lapse rate in degree-days
AN	a_{zn}	R*4	$cm \cdot ^{\circ}C \cdot d^{-1}$	$in \cdot ^{\circ}F \cdot d^{-1}$	Degree-day factors
CS	c_{Szn}	R*4	—	—	Snow runoff coefficient factor
CR	c_{Rzn}	R*4	—	—	Rain runoff coefficient factor
ZMEAN	\bar{h}	R*8	m	ft	Hypsometric mean elevation of each zone
STATN	h_{ST}	R*8	m	ft	Elevation of each base station
IPR	—	I*2	—	—	Precipitation method 0 = Non snow-covered areas 1 = Total areas

*Note: The subscript zn refers to number of snowmelt days per zone.

Table 3. (Continued)

Parameter	Symbol*	Type	Metric	Units		Description
					English	
MAXMIN	—	I*2	—	—	—	Flag to indicate if temperatures are input as maximum-minimum 0 = Temperatures input not as MAX-MIN 1 = Temperatures input as MAX-MIN
IEXT	—	I*2	—	—	—	Flag if temperatures are to be automatically extrapolated to elevation zone 0 = Extrapolate using pre-determined constant 1 = Automatically extrapolated using lapse rate
IDEGDY	—	I*2	—	—	—	Flag if temperature is to be computed in degree-days 0 = No computation necessary. Temperature already input in degree-days 1 = Compute temperature in degree-days

*Note: The subscript zn refers to number of snowmelt days per zone.

The SRM parameters, DTLR (if required), AN, CS, CR, and IPR are parameters that change throughout the snowmelt season. These are included in the basin NAMELIST so that the user can vary these parameters without having to input the climatological NAMELIST on each run. Figure 24 shows a typical basin NAMELIST input, again on the Dischma basin in Switzerland.

The NAMELIST OPT contains program control options to properly execute the SRM program. This NAMELIST can also be read several times allowing the user the capability of making several computer runs for a particular basin at one time. A description of each program option NAMELIST parameter including type and default value are provided in Table 4. Numerous program options are provided to the user such as plotting and printing options. The user may wish to operate in either metric or English units, so an option is provided for the appropriate conversion of units (UFLAG). It should be noted that the user must be consistent in inputting all data in either metric

```

1
&BASE
BASIN='DISCHMA ','BASIN ',
NZ=3,
IYEAR=1974,
AREA=8.9D6, 2.45D7, 9.9D6, 5*0.D0,
X=0.921D0,
Y=-0.0426D0,
QNS=0.56D0,
PDR=367*.5,
PDM2=367*0.,
DTLR=2928*0.65,
AN=15*.4,15*.45,31*.45,30*.50,46*.55,46*.60,123*.25,59*.3,0.,
    15*.4,15*.45,31*.45,30*.50,46*.55,46*.60,123*.25,59*.3,0.,
    15*.4,15*.45,31*.45,30*.50,46*.55,46*.60,123*.25,59*.3,0.,
CS=45*.95,16*.9,61*.85,31*.80,30*.9,182*.95,0.,
    45*.95,16*.9,61*.85,31*.80,30*.9,182*.95,0.,
    45*.95,16*.9,61*.85,31*.80,30*.9,182*.95,0.,
CR=91*1.0,123*0.7,151*0.6,
ZMEAN=1938.D0,2370.D0,2750.D0,5*0.D0,
STATN=2677.D0,
MAXMIN=1,
IEXT=1,
IDEGDY=1,
IPR=76*0,199*1,91*0,
    76*0,199*1,91*0,
    76*0,199*1,91*0,
&END

```

Figure 24. Sample NAMELIST BASE input for the Dischma basin, 1974.

Table 4. Description of Parameters in NAMELIST OPT

Parameter	Default	Type	Description
IRUN	1	I*4	Model run number
MODE	0	I*4	Simulation/Forecast mode flag 0 = Simulation 1 = Forecast
IPLT	0	I*2	Plotting option flag 0 = No plot 1 = Plot
IPRINT	0	I*2	Printing option flag 0 = No print 1 = Print
UFLAG	0	I*2	Units option flag 0 = Metric units 1 = English units
ACTFLG	1	I*2	Actual data flag 0 = No actual data available 1 = Actual data available
IZONE	3*1	I*2	Temperature, precipitation and runoff coefficient zone flag IZONE (1) = Temperature lapse rate IZONE (2) = Precipitation IZONE (3) = Runoff coefficients 0 = No zone input 1 = Input by zone
IDTFLG	0	I*2	Adjustment for temperature lapse rate data flag 0 = No temperature lapse rate data available 1 = Temperature lapse rate data available
MTHD	0	I*2	Degree-day temperature computation flag 0 = Mean method 1 = Effective minimum
ITPROC	0	I*2	Temperature processing flag to extrapolate temperatures and compute degree-days 0 = No temperature lapse rate processing 1 = Temperature lapse rate processing
IPRRUN	1	I*2	Runoff print option flag 0 = No print 1 = Print runoff values by zones
ISTMTH	4	I*4	Starting month of snowmelt run
IENMTH	9	I*4	Ending month of snowmelt run

or English units. No mixing of units is allowed and the unit option chosen must correspond to the units input into the program. In the event that no actual (measured) streamflow data is available, the user must input an initial actual streamflow value for the first day in place of actual data (ACTUAL (1)). An actual data flag must be set by the user indicating to the program that no actual data is available (ACTFLG). The model run identifying number, IRUN, is the only program option NAMELIST parameter required. All other NAMELIST parameters not specified will default to BLOCK DATA values which have been chosen to provide the basic options to properly execute the SRM program. Figure 25 shows typical program option NAMELIST input for the Dischma basin.

```
&OPT  
  IRUN=1,  
  MODE=0,  
  IPLT=0,  
  IPRINT=1,  
  UFLAG=0,  
  ACTFLG=1,  
  IZONE=0,0,0,  
  IDTFLG=1,  
  MTHD=0,  
  ITPROC=1,  
  IPRRUN=1,  
  ISTMTH=4,  
  IENMTH=7,  
&END
```

Figure 25. Sample NAMELIST OPT input for the Dischma basin, 1974.

Temperature Input Processing

The format in which temperature data are received can vary widely for each basin. Temperatures can be input as hourly readings, as average daily temperatures in degrees or degree-days, or as maximum and minimum values for one or two observing stations. Because the SRM computations for runoff will only accept temperature input in degree-days for each elevation zone, a certain amount of preprocessing is required if temperatures are not in that format.

To obtain temperatures in the proper format, a temperature preprocessing routine LAPSE is called to convert temperatures in degrees to degree-days (if they are not in that form) and to extrapolate degree-day temperatures to the elevation zones. When daily maximum and minimum temperatures are input, the temperature preprocessing routine LAPSE can be used to convert temperatures from degrees to degree-days. This is accomplished automatically in the program when the user sets the flags MAXMIN and IDEGDY to 1. The degree-day temperatures can be computed by setting the flag MTHD for effective minimum or mean method. The routine LAPSE can also accommodate temperatures that are input as an average daily value in degrees or as daily temperatures already converted to degree-days.

Additionally, the routine LAPSE will automatically extrapolate degree-day temperatures to the elevation zones according to Equation (4) provided the flag IEXT is set to 1. For the program to automatically extrapolate temperatures to the elevation zones the user must supply the mean elevation in each zone ZMEAN (\bar{h}), the elevation of the temperature base station, STATN (h_{ST}), and the average lapse rate DTLR (δ). In cases where the average lapse rate is predetermined for each elevation zone (rather than calculated from actual temperature data), no extrapolation is required beyond the addition of the lapse rate value to the degree-day temperature.

In special cases where temperatures are input hourly or as maximum-minimum from two stations, the modular routine PRETMP must be used to obtain the appropriate degree-day values for SRM. This routine is not part of the normal SRM processing and is included in Appendix C. PRETMP requires more storage capabilities and can be used as is or as a guideline for more detailed temperature preprocessing.

Precipitation Input Processing

The SRM program handles precipitation falling during snowmelt in several ways. First, based on a critical threshold temperature, a decision is made as to whether the precipitation is snow or rain. If it is snow and it falls on the existing snowpack, it is assumed to be melted along with the original snow later in the season as soon as the degree-day totals are sufficient. If it is snow and it falls on the snow-free area of the basin, the new snow is treated as transient snow and is melted right after the storm as soon as temperatures rise sufficiently. This input is treated merely as delayed rainfall. The situation with respect to rainfall is more complex because of the nature of the snowpack during the snowmelt season. In all cases rain falling on non snow-covered areas is automatically added to snowmelt by the model. In the early days of the snowmelt season, however, rain falling on the snow-covered region is assumed to fall on dry snow and it is held by the snowpack as part of the ripening process. Later in the snowmelt season over the snow-covered area, rain is assumed to fall on a ripe snowpack and this water is transmitted through the snow and added by the model to snowmelt.

Based on the progression of the snowmelt season, the program user must input daily the precipitation calculation method (IPR) desired (0 = rain added to snowmelt from snow-free areas only, i.e., a dry snowpack or 1 = rain added to snowmelt from all basin areas, i.e., a ripe snowpack).

Streamflow Input

Provision is made in the SRM program to take into account streamflow lag which can vary as the snowmelt season progresses. The streamflow lag is usually specified in hours, however, the effect on streamflow simulation in the model is expressed as the percentage of streamflow recorded on day n that is actually a result of snowmelt from the previous day ($n-1$). In the case of the South Fork basin in Colorado, it was determined that early in the snowmelt season approximately 70% of the streamflow recorded on day n is the result of the prior day's snowmelt amount, and 30% of the streamflow on day n is from snowmelt occurring on day n . The input to the program is therefore set at PDR = 0.70. Provision is also made in the model for when streamflow lag exceeds 18 hours. In this case there is no runoff contribution on day n from snowmelt occurring on day n . Streamflow occurring on day n is a result of snowmelt occurring on days $n-1$ and $n-2$. To reflect this situation, the input parameter PDM2 is set equal to the percentage of day n streamflow contribution resulting from day $n-2$ snowmelt.

The SRM program can be run in a streamflow simulation or forecast mode by specifying the MODE parameter in NAMELIST OPT. In the forecast mode, the model calculated daily streamflow value

can be updated every seventh day with measured streamflow for an entire snowmelt season run. In the default condition, SRM runs in the streamflow simulation mode.

Job Control Language

The snowmelt-runoff model program can be operated in a batch mode via card deck as shown in Figure 26. The only IBM 3081 Job Control Language (JCL) required to execute the program is shown below.

```
//JOB CARD                (User supplied Job and accounting information)

//EXEC FORTRAN           (Compiler type and options)

//SOURCE SYSIN DD*
    ●
    ●                    (Include FORTRAN source deck)
    ●

//EXEC LOADER            (Loader size and options)

//GO.FT06F001 SYSOUT =A   (Output device)

//DATA5 DD*
    ●
    ●                    (Include NAMELIST CLIM)
    ●
    ●                    (Include NAMELIST BASE)
    ●
    ●                    (Include NAMELIST OPT)

/*
```

Program Output Capabilities

The output of the SRM program consists of various numerical results and printer plots of the actual versus computed hydrographs. Depending on the purpose of the computer run, all or part of the output products may be produced.

The numerical output results consist of the measured versus calculated daily discharge rate for the snowmelt period (or entire year), the actual and computed total volume of streamflow for the snowmelt period (or entire year), the percent seasonal difference between the actual streamflow and the calculated streamflow (D_V), the mean actual and calculated streamflows, the Nash-Sutcliffe “goodness of fit” measure, the daily calculated snowmelt depth by elevation zone, and the computed daily precipitation values in each of the basin elevation zones. Table 5 provides a brief description of the output variables.

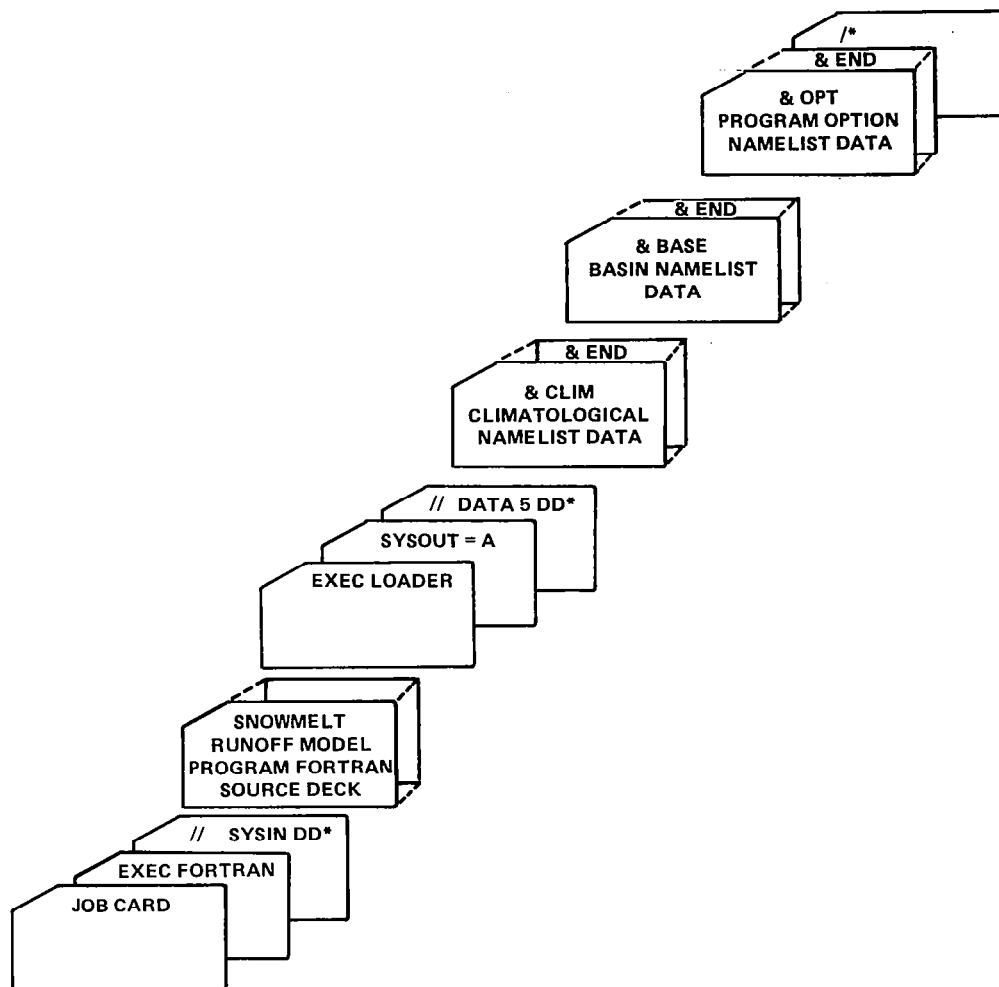


Figure 26. Sample card deck for input of snowmelt-runoff model program.

Table 5.
Description of Output Variables

Variable	Symbol	Type	Description
P	P_{zn}	R*4	Precipitation contributing to runoff in each zone assigned every day
RUNOF	—	R*4	Total depth (precipitation + snowmelt) contributing to runoff in each zone
QNP1X	Q_{n+1}	R*4	Computed stream runoff for next day
XNSR2	R^2	R*4	Nash-Sutcliffe 'goodness of fit' measure
VOL	—	R*4	Computed volume for predicted runoff
AVOL	—	R*4	Computed volume for actual runoff
PCT	D_v	R*4	Percent seasonal difference between actual and predicted runoff
AMEAN	—	R*4	Mean actual stream runoff
QMEAN	—	R*4	Mean computed stream runoff

A printer plot can be generated using the FORTRAN PRPLOT plotting package supplied with the snowmelt-runoff model. A listing for PRPLOT is included as part of Appendix B. The calculated and actual streamflows over the snowmelt-runoff season are plotted on the same graph as discharge rate vs. time. If no actual data is available then only the calculated runoff is plotted if desired. Figure 27 gives an example of some numerical results for the Dischma basin for 1974.

```

RUN # 1 BASIN=DISCHMA BASIN YEAR= 1974

MODE (0=SIMULATED,1=FORCAST)= 0

PROGRAM OPTIONS (0=OFF,1=ON)

PLOT OPTION= 0 PRINT OPTION= 1 UNITS(0=METRIC,1=ENGLISH)= 0
ACTUAL DATA FLAG= 1 ZONE INPUT DATA(TEMP.,PRECIP.,RUNOFF COEF.)= 0 0 0
LAPSE RATE DATA FLAG= 1 DEGREE-DAY METHOD(0=MEAN,1=EFFECTIVE MINIMUM)= 0
TEMPERATURE PROCESSING FLAG= 1 RUNOFF BY ZONE OUTPUT OPTION= 1
FLAG TO EXTRAPOLATE TEMPERATURES(0=EXTRAPOLATE USING GIVEN LAPSE RATES, 1=AUTOMATICALLY EXTRAPOLATE)= 1
FLAG TO COMPUTE DEGREE-DAYS= 1
FLAG TO INDICATE INPUT TEMPS ARE MAX-MIN= 1
START MONTH= 4 END MONTH= 7

NUMBER OF SNOWMELT DAYS= 122 NUMBER OF ELEVATION ZONES= 3

RECESSION COEFFICIENT FACTORS
X FACTOR= 0.921000 Y FACTOR=-0.042600
INITIAL RUNOFF VALUE= 0.560 LAG= 6 HOURS

AREA IN EACH ELEVATION ZONE
ZONE AREA (SQ. METERS )
1 0.8900E 07
2 0.2450E 08
3 0.9900E 07

HYPSOMETRIC MEAN ELEVATION IN EACH ZONE (METERS )
1 0.1938E 04
2 0.2370E 04
3 0.2750E 04

BASE STATION ELEVATION (METERS )
0.2677E 04

```

Figure 27. Snowmelt-runoff model results for the Dischma basin, 1974.

DAILY MAXIMUM AND MINIMUM TEMPERATURES

RANGO-MARTINEC MODEL FOR DISCHMA BASIN YEAR= 1974

DAY	APR		MAY		JUN		JUL	
	MAX TEMP	MIN TEMP	MAX TEMP	MIN TEMP	MAX TEMP	MIN TEMP	MAX TEMP	MIN TEMP
1	-0.20	-5.30	-1.10	-6.20	3.00	-2.40	8.20	2.00
2	0.40	-6.20	-2.20	-7.80	5.20	-6.70	6.60	-0.40
3	1.30	-5.60	-2.00	-7.60	8.70	1.50	6.70	0.70
4	3.70	-3.40	0.70	-5.20	9.60	4.40	7.90	-2.50
5	-2.00	-4.80	-3.00	-6.70	10.30	3.30	9.60	1.30
6	-0.70	-7.40	-3.70	-6.30	4.10	-1.00	8.30	3.00
7	-0.90	-6.00	-3.00	-8.00	-0.80	-5.90	3.20	-2.80
8	-0.30	-6.40	-0.70	-5.50	1.30	-3.30	2.70	-2.80
9	1.60	-4.90	-1.00	-6.70	1.40	-6.30	8.00	0.60
10	-1.00	-5.30	-0.60	-3.70	-1.80	-8.20	6.80	1.10
11	1.00	-7.40	-1.70	-4.40	-4.90	-7.70	10.30	2.00
12	0.70	-5.20	1.30	-7.50	-4.10	-6.10	12.80	6.10
13	3.00	-3.90	6.80	0.20	-2.40	-6.90	12.00	6.80
14	0.0	-8.70	3.30	-4.40	4.40	-4.70	9.70	3.70
15	-7.20	-12.20	-0.70	-7.10	5.10	1.20	9.00	1.40
16	-9.60	-13.20	2.80	-3.80	6.20	0.10	10.50	5.00
17	-9.00	-14.60	1.10	-1.10	6.30	0.40	5.90	0.80
18	-6.40	-15.10	4.20	-3.70	2.40	-3.00	1.50	-2.50
19	-6.30	-15.10	5.40	-1.20	2.90	-4.60	-0.50	-3.10
20	-3.20	-10.20	2.60	0.10	5.40	0.20	-1.10	-4.60
21	-4.40	-9.40	3.70	-0.70	5.50	0.0	0.90	-1.70
22	-3.80	-9.50	2.90	-3.20	5.60	0.10	3.60	-2.60
23	-0.80	-8.40	-2.00	-6.90	5.70	2.20	8.20	1.00
24	-4.80	-9.10	-2.50	-7.80	3.00	-2.40	13.40	2.30
25	-5.90	-10.40	-0.60	-6.70	7.60	-1.40	9.20	-1.20
26	-5.00	-10.70	4.10	-5.20	5.30	2.50	11.00	-2.40
27	-4.80	-9.90	5.20	-1.60	3.00	-0.70	13.30	4.40
28	-0.30	-8.40	3.00	-3.90	2.80	0.0	13.40	3.30
29	0.0	-3.80	4.40	-3.60	3.80	-1.30	15.50	5.30
30	-1.70	-4.80	5.10	0.0	3.50	-1.30	14.20	6.90
31	*****	*****	4.70	2.00	*****	*****	11.80	5.30

DEGREE-DAY FACTORS(AN), RUNOFF COEFFICIENTS FOR SNOW(CS), FOR RAIN(CR), PRECIP METHOD(PR)

RANGO-MARTINEC MODEL FOR DISCHMA BASIN YEAR= 1974

DATA FOR ZONE A

DAY	APR				MAY				JUN				JUL			
	AN	CS	CR	PR	AN	CS	CR	PR	AN	CS	CR	PR	AN	CS	CR	PR
1	0.40	0.95	1.00	0	0.45	0.95	1.00	0	0.50	0.85	1.00	0	0.55	0.85	0.70	1
2	0.40	0.95	1.00	0	0.45	0.95	1.00	0	0.50	0.85	1.00	0	0.55	0.85	0.70	1
3	0.40	0.95	1.00	0	0.45	0.95	1.00	0	0.50	0.85	1.00	0	0.55	0.85	0.70	1
4	0.40	0.95	1.00	0	0.45	0.95	1.00	0	0.50	0.85	1.00	0	0.55	0.85	0.70	1
5	0.40	0.95	1.00	0	0.45	0.95	1.00	0	0.50	0.85	1.00	0	0.55	0.85	0.70	1
6	0.40	0.95	1.00	0	0.45	0.95	1.00	0	0.50	0.85	1.00	0	0.55	0.85	0.70	1
7	0.40	0.95	1.00	0	0.45	0.95	1.00	0	0.50	0.85	1.00	0	0.55	0.85	0.70	1
8	0.40	0.95	1.00	0	0.45	0.95	1.00	0	0.50	0.85	1.00	0	0.55	0.85	0.70	1
9	0.40	0.95	1.00	0	0.45	0.95	1.00	0	0.50	0.85	1.00	0	0.55	0.85	0.70	1
10	0.40	0.95	1.00	0	0.45	0.95	1.00	0	0.50	0.85	1.00	0	0.55	0.85	0.70	1
11	0.40	0.95	1.00	0	0.45	0.95	1.00	0	0.50	0.85	1.00	0	0.55	0.85	0.70	1
12	0.40	0.95	1.00	0	0.45	0.95	1.00	0	0.50	0.85	1.00	0	0.55	0.85	0.70	1
13	0.40	0.95	1.00	0	0.45	0.95	1.00	0	0.50	0.85	1.00	0	0.55	0.85	0.70	1
14	0.40	0.95	1.00	0	0.45	0.95	1.00	0	0.50	0.85	1.00	0	0.55	0.85	0.70	1
15	0.40	0.95	1.00	0	0.45	0.95	1.00	0	0.50	0.85	1.00	0	0.55	0.85	0.70	1
16	0.45	0.95	1.00	0	0.45	0.90	1.00	0	0.50	0.85	1.00	1	0.55	0.85	0.70	1
17	0.45	0.95	1.00	0	0.45	0.90	1.00	0	0.50	0.85	1.00	1	0.55	0.85	0.70	1
18	0.45	0.95	1.00	0	0.45	0.90	1.00	0	0.50	0.85	1.00	1	0.55	0.85	0.70	1
19	0.45	0.95	1.00	0	0.45	0.90	1.00	0	0.50	0.85	1.00	1	0.55	0.85	0.70	1
20	0.45	0.95	1.00	0	0.45	0.90	1.00	0	0.50	0.85	1.00	1	0.55	0.85	0.70	1
21	0.45	0.95	1.00	0	0.45	0.90	1.00	0	0.50	0.85	1.00	1	0.55	0.85	0.70	1
22	0.45	0.95	1.00	0	0.45	0.90	1.00	0	0.50	0.85	1.00	1	0.55	0.85	0.70	1
23	0.45	0.95	1.00	0	0.45	0.90	1.00	0	0.50	0.85	1.00	1	0.55	0.85	0.70	1
24	0.45	0.95	1.00	0	0.45	0.90	1.00	0	0.50	0.85	1.00	1	0.55	0.85	0.70	1
25	0.45	0.95	1.00	0	0.45	0.90	1.00	0	0.50	0.85	1.00	1	0.55	0.85	0.70	1
26	0.45	0.95	1.00	0	0.45	0.90	1.00	0	0.50	0.85	1.00	1	0.55	0.85	0.70	1
27	0.45	0.95	1.00	0	0.45	0.90	1.00	0	0.50	0.85	1.00	1	0.55	0.85	0.70	1
28	0.45	0.95	1.00	0	0.45	0.90	1.00	0	0.50	0.85	1.00	1	0.55	0.85	0.70	1
29	0.45	0.95	1.00	0	0.45	0.90	1.00	0	0.50	0.85	1.00	1	0.55	0.85	0.70	1
30	0.45	0.95	1.00	0	0.45	0.90	1.00	0	0.50	0.85	1.00	1	0.55	0.85	0.70	1
31	****	****	****	*	0.45	0.90	1.00	0	****	****	****	*	0.55	0.85	0.70	1

Figure 27. (Continued)

LAPSE RATE(DTLR), CRITICAL TEMPERATURE(TCRT)

RANGO-MARTINEC MODEL FOR DISCHMA BASIN YEAR= 1974

DATA FOR ZONE A

DAY	APR		MAY		JUN		JUL	
	DTLR	TCRT	DTLR	TCRT	DTLR	TCRT	DTLR	TCRT
1	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
2	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
3	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
4	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
5	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
6	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
7	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
8	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
9	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
10	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
11	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
12	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
13	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
14	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
15	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
16	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
17	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
18	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
19	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
20	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
21	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
22	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
23	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
24	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
25	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
26	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
27	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
28	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
29	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
30	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
31	*****	****	0.65	3.00	*****	****	0.65	0.75

LAPSE RATE(DTLR), CRITICAL TEMPERATURE(TCRT)

RANGO-MARTINEC MODEL FOR DISCHMA BASIN YEAR= 1974

DATA FOR ZONE B

DAY	APR		MAY		JUN		JUL	
	DTLR	TCRT	DTLR	TCRT	DTLR	TCRT	DTLR	TCRT
1	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
2	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
3	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
4	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
5	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
6	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
7	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
8	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
9	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
10	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
11	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
12	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
13	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
14	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
15	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
16	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
17	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
18	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
19	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
20	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
21	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
22	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
23	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
24	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
25	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
26	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
27	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
28	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
29	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
30	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
31	*****	****	0.65	3.00	*****	****	0.65	0.75

Figure 27. (Continued)

LAPSE RATE(DTLR); CRITICAL TEMPERATURE(TCRT)

RANGO-MARTINEC MODEL FOR DISCHMA BASIN YEAR= 1974

DATA FOR ZONE C

DAY	APR		MAY		JUN		JUL	
	DTLR	TCRT	DTLR	TCRT	DTLR	TCRT	DTLR	TCRT
1	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
2	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
3	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
4	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
5	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
6	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
7	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
8	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
9	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
10	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
11	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
12	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
13	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
14	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
15	0.65	3.00	0.65	3.00	0.65	3.00	0.65	0.75
16	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
17	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
18	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
19	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
20	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
21	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
22	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
23	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
24	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
25	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
26	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
27	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
28	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
29	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
30	0.65	3.00	0.65	3.00	0.65	2.00	0.65	0.75
31	*****	****	0.65	3.00	*****	****	0.65	0.75

DAILY TEMP IN DEGREE-DAYS(DD);INFUT PRECIP(PREC); SNOW COVERED AREA IN %(SCA::)

RANGO-MARTINEC MODEL FOR DISCHMA BASIN YEAR= 1974

DATA FOR ZONE A

DAY	APR			MAY			JUN			JUL		
	DD	PREC	SCA	DD	PREC	SCA	DD	PREC	SCA	DD	PREC	SCA
1	2.05	0.19	0.880	1.15	0.21	0.800	5.10	1.49	0.230	9.90	0.0	0.030
2	1.90	0.06	0.880	0.0	0.22	0.795	4.05	0.0	0.215	7.90	0.57	0.025
3	2.65	0.0	0.875	0.00	0.03	0.795	9.90	0.0	0.200	8.50	0.0	0.025
4	4.95	0.0	0.875	2.55	0.0	0.790	11.80	0.0	0.185	7.50	0.89	0.020
5	1.40	0.04	0.875	0.0	0.45	0.785	11.60	0.0	0.179	10.25	0.0	0.018
6	0.75	0.34	0.875	0.0	0.84	0.780	6.35	0.37	0.170	10.45	0.0	0.015
7	1.35	0.0	0.870	0.0	0.09	0.775	1.45	0.02	0.160	5.00	1.03	0.010
8	1.45	0.01	0.870	1.70	0.01	0.770	2.90	0.06	0.150	4.75	0.03	0.005
9	3.15	0.0	0.865	0.95	0.0	0.765	2.35	0.07	0.140	9.10	0.0	0.0
10	1.65	0.0	0.865	2.65	0.0	0.760	0.0	0.41	0.135	8.75	0.74	0.0
11	1.60	0.0	0.865	1.75	0.27	0.760	0.0	0.85	0.125	10.95	0.21	0.0
12	2.55	0.0	0.860	1.70	0.98	0.755	0.0	1.06	0.115	14.25	0.0	0.0
13	4.35	0.0	0.860	8.30	0.0	0.745	0.15	1.72	0.110	14.20	0.0	0.0
14	0.45	0.10	0.855	4.25	0.02	0.735	4.65	0.03	0.105	11.50	0.20	0.0
15	0.0	0.03	0.850	0.90	0.27	0.725	7.95	0.0	0.100	10.00	3.08	0.0
16	0.0	0.53	0.850	4.30	0.0	0.717	7.95	0.66	0.095	12.55	0.0	0.0
17	0.0	0.13	0.845	4.80	0.0	0.700	8.15	0.0	0.090	8.15	0.52	0.0
18	0.0	0.07	0.840	5.05	0.0	0.680	4.50	0.70	0.085	4.30	2.96	0.0
19	0.0	0.02	0.835	6.90	0.0	0.660	3.95	1.20	0.080	3.00	1.02	0.0
20	0.0	0.0	0.835	6.15	0.0	0.640	7.60	0.0	0.075	1.95	0.22	0.0
21	0.0	0.0	0.830	6.30	0.26	0.600	7.55	0.0	0.070	4.40	0.41	0.0
22	0.0	0.03	0.830	4.65	0.0	0.560	7.65	1.41	0.065	5.30	0.37	0.0
23	0.20	0.0	0.825	0.35	3.23	0.520	8.75	0.65	0.060	9.40	0.0	0.0
24	0.0	0.26	0.825	0.0	0.48	0.480	5.10	1.59	0.055	12.65	0.0	0.0
25	0.0	0.59	0.820	1.15	0.38	0.440	7.90	0.09	0.050	8.80	1.35	0.0
26	0.0	0.31	0.820	4.25	0.03	0.400	8.70	0.0	0.045	9.10	0.17	0.0
27	0.0	0.02	0.815	6.60	0.0	0.370	5.95	2.71	0.040	13.65	0.0	0.0
28	1.95	0.0	0.810	4.35	0.52	0.340	6.20	0.83	0.035	13.10	0.21	0.0
29	2.90	0.02	0.805	5.20	0.97	0.310	6.05	1.33	0.035	15.20	0.0	0.0
30	1.55	0.13	0.800	7.35	0.0	0.280	5.90	1.82	0.030	15.35	0.0	0.0
31	*****	*****	*****	8.15	0.02	0.250	*****	*****	*****	13.35	0.0	0.0

Figure 27. (Continued)

DAILY TEMP IN DEGREE-DAYS(DD), INPUT PRECIP(PREC), SNOW COVERED AREA IN %(SCA::)

RANGO-MARTINEC MODEL FOR DISCHMA BASIN YEAR= 1974

DATA FOR ZONE B

DAY	APR			MAY			JUN			JUL		
	DD	PREC	SCA	DD	PREC	SCA	DD	PREC	SCA	DD	PREC	SCA
1	0.0	0.19	0.930	0.0	0.21	0.900	2.30	1.49	0.800	7.10	0.0	0.510
2	0.0	0.06	0.930	0.0	0.22	0.900	1.25	0.0	0.795	5.10	0.57	0.500
3	0.0	0.0	0.930	0.0	0.03	0.900	7.10	0.0	0.790	5.70	0.0	0.490
4	2.15	0.0	0.930	0.0	0.0	0.900	9.00	0.0	0.785	4.70	0.89	0.480
5	0.0	0.04	0.930	0.0	0.45	0.900	8.80	0.0	0.776	7.45	0.0	0.444
6	0.0	0.34	0.925	0.0	0.84	0.895	3.55	0.37	0.770	7.65	0.0	0.450
7	0.0	0.0	0.925	0.0	0.09	0.895	0.0	0.02	0.770	2.20	1.03	0.440
8	0.0	0.01	0.925	0.0	0.01	0.895	0.10	0.06	0.750	1.95	0.03	0.430
9	0.35	0.0	0.925	0.0	0.0	0.890	0.0	0.07	0.740	6.30	0.0	0.415
10	0.0	0.0	0.925	0.0	0.0	0.890	0.0	0.41	0.735	5.95	0.74	0.400
11	0.0	0.0	0.920	0.0	0.27	0.885	0.0	0.85	0.725	8.15	0.21	0.385
12	0.0	0.0	0.920	0.0	0.98	0.885	0.0	1.06	0.715	11.45	0.0	0.370
13	1.55	0.0	0.920	5.50	0.0	0.880	0.0	1.72	0.705	11.40	0.0	0.340
14	0.0	0.10	0.920	1.45	0.02	0.880	1.85	0.03	0.695	8.70	0.20	0.350
15	0.0	0.03	0.920	0.0	0.27	0.880	5.15	0.0	0.685	7.20	3.08	0.340
16	0.0	0.53	0.915	1.50	0.0	0.877	5.15	0.66	0.670	9.75	0.0	0.330
17	0.0	0.13	0.915	2.00	0.0	0.875	5.35	0.0	0.660	5.35	0.52	0.320
18	0.0	0.07	0.915	2.25	0.0	0.870	1.70	0.70	0.650	1.50	2.96	0.305
19	0.0	0.02	0.915	4.10	0.0	0.865	1.15	1.20	0.640	0.20	1.02	0.290
20	0.0	0.0	0.915	3.35	0.0	0.860	4.80	0.0	0.630	0.0	0.22	0.280
21	0.0	0.0	0.910	3.50	0.26	0.855	4.75	0.0	0.620	1.60	0.41	0.270
22	0.0	0.03	0.910	1.85	0.0	0.850	4.85	1.41	0.610	2.50	0.37	0.260
23	0.0	0.0	0.910	0.0	3.23	0.845	5.95	0.65	0.600	6.60	0.0	0.245
24	0.0	0.26	0.910	0.0	0.48	0.840	2.30	1.59	0.590	9.85	0.0	0.230
25	0.0	0.59	0.910	0.0	0.38	0.835	5.10	0.09	0.580	6.00	1.35	0.220
26	0.0	0.31	0.905	1.45	0.03	0.830	5.90	0.0	0.565	6.30	0.17	0.210
27	0.0	0.02	0.905	3.80	0.0	0.825	3.15	2.71	0.550	10.85	0.0	0.195
28	0.0	0.0	0.905	1.55	0.52	0.820	3.40	0.83	0.540	10.30	0.21	0.180
29	0.10	0.02	0.900	2.40	0.97	0.815	3.25	1.33	0.530	12.40	0.0	0.170
30	0.0	0.13	0.900	4.55	0.0	0.810	3.10	1.82	0.520	12.55	0.0	0.160
31	*****	*****	*****	5.35	0.02	0.800	*****	*****	*****	10.55	0.0	0.155

DAILY TEMP IN DEGREE-DAYS(DD), INPUT PRECIP(PREC), SNOW COVERED AREA IN %(SCA::)

RANGO-MARTINEC MODEL FOR DISCHMA BASIN YEAR= 1974

DATA FOR ZONE C

DAY	APR			MAY			JUN			JUL		
	DD	PREC	SCA	DD	PREC	SCA	DD	PREC	SCA	DD	PREC	SCA
1	0.0	0.19	0.850	0.0	0.21	0.805	0.0	1.49	0.790	4.63	0.0	0.790
2	0.0	0.06	0.845	0.0	0.22	0.805	0.0	0.0	0.790	2.63	0.57	0.790
3	0.0	0.0	0.845	0.0	0.03	0.805	4.63	0.0	0.790	3.23	0.0	0.790
4	0.0	0.0	0.840	0.0	0.0	0.805	6.53	0.0	0.790	2.23	0.89	0.795
5	0.0	0.04	0.840	0.0	0.45	0.805	6.33	0.0	0.786	4.98	0.0	0.797
6	0.0	0.34	0.835	0.0	0.84	0.805	1.08	0.37	0.785	5.18	0.0	0.795
7	0.0	0.0	0.835	0.0	0.09	0.805	0.0	0.02	0.785	0.0	1.03	0.790
8	0.0	0.01	0.830	0.0	0.01	0.805	0.0	0.06	0.785	0.0	0.03	0.785
9	0.0	0.0	0.830	0.0	0.0	0.805	0.0	0.07	0.780	3.83	0.0	0.780
10	0.0	0.0	0.830	0.0	0.0	0.805	0.0	0.41	0.780	3.48	0.74	0.775
11	0.0	0.0	0.825	0.0	0.27	0.805	0.0	0.85	0.780	5.68	0.21	0.770
12	0.0	0.0	0.825	0.0	0.98	0.805	0.0	1.06	0.785	8.98	0.0	0.760
13	0.0	0.0	0.820	3.03	0.0	0.805	0.0	1.72	0.785	8.93	0.0	0.750
14	0.0	0.10	0.820	0.0	0.02	0.805	0.0	0.03	0.785	6.23	0.20	0.740
15	0.0	0.03	0.820	0.0	0.27	0.805	2.68	0.0	0.785	4.73	3.08	0.730
16	0.0	0.53	0.815	0.0	0.0	0.804	2.68	0.66	0.785	7.28	0.0	0.720
17	0.0	0.13	0.815	0.0	0.0	0.800	2.88	0.0	0.785	2.88	0.52	0.710
18	0.0	0.07	0.810	0.0	0.0	0.800	0.0	0.70	0.785	0.0	2.96	0.700
19	0.0	0.02	0.810	1.63	0.0	0.800	0.0	1.20	0.785	0.0	1.02	0.690
20	0.0	0.0	0.810	0.88	0.0	0.800	2.33	0.0	0.785	0.0	0.22	0.675
21	0.0	0.0	0.805	1.03	0.26	0.800	2.28	0.0	0.785	0.0	0.41	0.660
22	0.0	0.03	0.805	0.0	0.0	0.800	2.38	1.41	0.785	0.03	0.37	0.645
23	0.0	0.0	0.805	0.0	3.23	0.800	3.48	0.65	0.785	4.13	0.0	0.630
24	0.0	0.26	0.805	0.0	0.48	0.800	0.0	1.59	0.785	7.38	0.0	0.615
25	0.0	0.59	0.805	0.0	0.38	0.800	2.63	0.09	0.785	3.53	1.35	0.600
26	0.0	0.31	0.805	0.0	0.03	0.795	3.43	0.0	0.785	3.83	0.17	0.585
27	0.0	0.02	0.805	1.33	0.0	0.795	0.68	2.71	0.785	8.38	0.0	0.570
28	0.0	0.0	0.805	0.0	0.52	0.795	0.93	0.83	0.785	7.83	0.21	0.560
29	0.0	0.02	0.805	0.0	0.97	0.795	0.78	1.33	0.785	9.93	0.0	0.550
30	0.0	0.13	0.805	2.08	0.0	0.795	0.63	1.82	0.790	10.08	0.0	0.540
31	*****	*****	*****	2.88	0.02	0.790	*****	*****	*****	8.08	0.0	0.530

Figure 27. (Continued)

DAILY SNOW DEPTH BY ZONE IN CM.***2(DPTH),

DAILY COMPUTED PRECIP CONTRIBUTING TO RUNOFF(CPRE)

RANGO-MARTINEC MODEL FOR DISCHMA BASIN YEAR= 1974

DATA FOR ZONE A

DAY	APR		MAY		JUN		JUL	
	DPTH	CPRE	DPTH	CPRE	DPTH	CPRE	DPTH	CPRE
1	0.723	0.0	0.415	0.0	1.734	1.147	0.163	0.0
2	0.670	0.0	0.0	0.0	0.436	0.0	0.679	0.570
3	0.960	0.031	0.001	0.0	0.990	0.0	0.117	0.0
4	1.734	0.0	1.149	0.241	1.092	0.0	0.973	0.890
5	0.491	0.0	0.0	0.0	1.039	0.0	0.103	0.0
6	0.264	0.0	0.0	0.0	0.847	0.307	0.084	0.0
7	0.520	0.049	0.0	0.0	0.116	0.0	1.058	1.030
8	0.506	0.0	0.590	0.0	0.218	0.0	0.043	0.030
9	1.092	0.001	0.429	0.101	0.165	0.0	0.0	0.0
10	0.572	0.0	1.194	0.287	0.0	0.0	0.740	0.740
11	0.555	0.0	0.600	0.0	0.0	0.0	0.210	0.210
12	0.878	0.0	0.379	0.0	0.0	0.0	0.0	0.0
13	1.498	0.0	3.191	0.407	0.008	0.0	0.0	0.0
14	0.155	0.0	1.412	0.005	2.354	2.109	0.200	0.200
15	0.0	0.0	0.295	0.0	2.075	1.677	3.080	3.080
16	0.0	0.0	1.465	0.076	1.038	0.660	0.0	0.0
17	0.0	0.0	1.513	0.0	0.367	0.0	0.520	0.520
18	0.0	0.0	1.546	0.0	0.891	0.700	2.960	2.960
19	0.0	0.0	2.050	0.0	1.358	1.200	1.020	1.020
20	0.0	0.0	1.772	0.0	0.285	0.0	0.220	0.220
21	0.0	0.0	1.806	0.104	0.264	0.0	0.410	0.410
22	0.0	0.0	1.173	0.0	1.639	1.410	0.370	0.370
23	0.092	0.016	0.083	0.0	0.913	0.650	0.0	0.0
24	0.0	0.0	0.0	0.0	1.730	1.590	0.0	0.0
25	0.0	0.0	0.228	0.0	0.288	0.090	1.350	1.350
26	0.0	0.0	1.932	1.166	0.196	0.0	0.170	0.170
27	0.0	0.0	2.470	1.371	2.829	2.710	0.0	0.0
28	0.879	0.167	1.009	0.343	0.939	0.830	0.210	0.210
29	1.052	0.0	1.395	0.669	1.416	1.330	0.0	0.0
30	0.759	0.0	0.927	0.0	1.909	1.820	0.0	0.0
31	*****	*****	0.932	0.015	*****	*****	0.0	0.0

DAILY SNOW DEPTH BY ZONE IN CM.***2(DPTH),

DAILY COMPUTED PRECIP CONTRIBUTING TO RUNOFF(CPRE)

RANGO-MARTINEC MODEL FOR DISCHMA BASIN YEAR= 1974

DATA FOR ZONE B

DAY	APR		MAY		JUN		JUL	
	DPTH	CPRE	DPTH	CPRE	DPTH	CPRE	DPTH	CPRE
1	0.0	0.0	0.0	0.0	0.918	0.0	1.990	0.0
2	0.0	0.0	0.0	0.0	0.623	0.128	1.971	0.570
3	0.0	0.0	0.0	0.0	2.985	0.182	1.535	0.0
4	0.816	0.018	0.0	0.0	3.531	0.0	2.130	0.890
5	0.0	0.0	0.0	0.0	3.413	0.0	1.900	0.0
6	0.0	0.0	0.0	0.0	1.450	0.085	1.892	0.0
7	0.0	0.0	0.0	0.0	0.0	0.0	1.561	1.030
8	0.0	0.0	0.0	0.0	0.036	0.0	0.490	0.030
9	0.138	0.010	0.0	0.0	0.0	0.0	1.437	0.0
10	0.0	0.0	0.0	0.0	0.0	0.0	2.048	0.740
11	0.0	0.0	0.0	0.0	0.0	0.0	1.935	0.210
12	0.0	0.0	0.0	0.0	0.0	0.0	2.329	0.0
13	0.589	0.020	2.473	0.297	0.0	0.0	2.256	0.0
14	0.0	0.0	0.572	0.0	0.641	0.0	1.874	0.200
15	0.0	0.0	0.0	0.0	2.573	0.810	4.426	3.080
16	0.0	0.0	0.673	0.083	2.927	1.204	1.769	0.0
17	0.0	0.0	0.898	0.112	1.764	0.0	1.461	0.520
18	0.0	0.0	1.010	0.131	0.351	0.0	3.211	2.960
19	0.0	0.0	1.672	0.078	0.367	0.0	0.031	0.0
20	0.0	0.0	1.295	0.0	2.214	0.703	0.0	0.0
21	0.0	0.0	1.383	0.038	1.471	0.0	1.288	1.051
22	0.0	0.0	0.706	0.0	2.888	1.410	0.995	0.638
23	0.0	0.0	0.0	0.0	2.434	0.650	0.889	0.0
24	0.0	0.0	0.0	0.0	2.267	1.590	1.245	0.0
25	0.0	0.0	0.0	0.0	1.568	0.090	2.075	1.350
26	0.0	0.0	0.540	0.0	1.665	0.0	0.897	0.170
27	0.0	0.0	1.708	0.299	3.575	2.710	1.163	0.0
28	0.0	0.0	0.570	0.0	1.747	0.830	1.229	0.210
29	0.039	0.0	0.879	0.0	2.190	1.330	1.159	0.0
30	0.0	0.0	2.045	0.389	2.625	1.820	1.104	0.0
31	*****	*****	2.300	0.375	*****	*****	0.899	0.0

Figure 27. (Continued)

DAILY SNOW DEPTH BY ZONE IN CM.M**2(DPTH),

DAILY COMPUTED PRECIP CONTRIBUTING TO RUNOFF(CPRE)

RANGO-MARTINEC MODEL FOR BISCHNA BASIN YEAR= 1974

DATA FOR ZONE C

DAY	APR		MAY		JUN		JUL	
	DPTH	CPRE	DPTH	CPRE	DPTH	CPRE	DPTH	CPRE
1	0.0	0.0	0.0	0.0	0.0	0.0	2.544	0.534
2	0.0	0.0	0.0	0.0	0.0	0.0	2.014	0.873
3	0.0	0.0	0.0	0.0	2.313	0.486	1.774	0.373
4	0.0	0.0	0.0	0.0	3.263	0.685	2.053	1.080
5	0.0	0.0	0.0	0.0	3.163	0.677	2.181	0.0
6	0.0	0.0	0.0	0.0	0.422	0.0	2.263	0.0
7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
9	0.0	0.0	0.0	0.0	0.0	0.0	1.874	0.233
10	0.0	0.0	0.0	0.0	0.0	0.0	2.221	0.740
11	0.0	0.0	0.0	0.0	0.0	0.0	2.614	0.210
12	0.0	0.0	0.0	0.0	0.0	0.0	3.752	0.0
13	0.0	0.0	1.361	0.265	0.0	0.0	3.682	0.0
14	0.0	0.0	0.0	0.0	0.0	0.0	2.734	0.200
15	0.0	0.0	0.0	0.0	1.338	0.288	4.977	3.080
16	0.0	0.0	0.0	0.0	1.998	0.948	2.881	0.0
17	0.0	0.0	0.0	0.0	1.438	0.307	1.643	0.520
18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
19	0.0	0.0	0.731	0.146	0.0	0.0	0.0	0.0
20	0.0	0.0	0.394	0.079	1.163	0.250	0.0	0.0
21	0.0	0.0	0.369	0.0	1.138	0.245	0.0	0.0
22	0.0	0.0	0.0	0.0	2.551	1.619	0.009	0.0
23	0.0	0.0	0.0	0.0	2.014	0.650	2.269	0.840
24	0.0	0.0	0.0	0.0	0.0	0.0	3.538	1.044
25	0.0	0.0	0.0	0.0	1.403	0.372	2.513	1.350
26	0.0	0.0	0.0	0.0	1.404	0.060	1.401	0.170
27	0.0	0.0	0.596	0.122	0.265	0.0	2.626	0.0
28	0.0	0.0	0.0	0.0	0.363	0.0	2.620	0.210
29	0.0	0.0	0.0	0.0	0.304	0.0	3.002	0.0
30	0.0	0.0	0.934	0.191	0.247	0.0	2.992	0.0
31	*****	*****	1.022	0.0	*****	*****	2.354	0.0

Figure 27. (Continued)

DAILY COMPUTED AND ACTUAL SNOWMELT RUNOFF DATA

RANGO-MARTINEC MODEL FOR DISCHMA BASIN YEAR= 1974

DAY	APR		MAY		JUN		JUL	
	COMPUTED	ACTUAL	COMPUTED	ACTUAL	COMPUTED	ACTUAL	COMPUTED	ACTUAL
1	0.564	0.600	0.453	0.800	3.941	4.510	7.367	5.620
2	0.571	0.630	0.441	0.760	3.808	3.780	7.323	6.680
3	0.584	0.670	0.421	0.760	4.119	4.020	7.142	6.550
4	0.689	0.710	0.427	0.770	5.118	4.850	7.024	6.230
5	0.786	0.760	0.434	0.770	6.163	5.830	7.026	6.060
6	0.757	0.750	0.414	0.760	6.513	6.330	6.994	6.180
7	0.732	0.800	0.396	0.790	5.900	4.920	6.762	6.200
8	0.716	0.840	0.391	0.870	5.066	3.990	6.140	5.290
9	0.733	0.890	0.396	0.970	4.383	3.630	5.710	5.210
10	0.751	0.950	0.413	1.100	3.801	3.260	5.784	6.610
11	0.737	0.960	0.434	1.140	3.307	2.920	5.992	6.520
12	0.735	0.990	0.440	1.120	2.894	2.670	6.323	4.650
13	0.817	1.070	0.695	1.230	2.548	2.430	6.743	6.840
14	0.873	1.230	1.111	1.470	2.482	2.540	6.950	7.860
15	0.814	1.160	1.153	1.550	2.991	2.840	7.649	8.720
16	0.756	1.010	1.199	1.850	3.879	2.930	8.245	6.600
17	0.705	0.920	1.390	2.200	4.464	3.170	7.910	7.160
18	0.689	0.850	1.619	2.480	4.418	3.670	7.752	7.140
19	0.618	0.810	1.999	2.840	4.122	3.410	7.278	5.340
20	0.581	0.780	2.439	2.930	4.194	3.570	6.234	4.540
21	0.547	0.770	2.784	3.030	4.434	4.110	5.541	4.480
22	0.517	0.770	2.957	3.510	4.980	5.440	5.129	4.120
23	0.492	0.780	2.779	3.270	5.760	5.280	4.872	4.060
24	0.470	0.800	2.455	2.720	6.159	5.590	4.923	4.150
25	0.447	0.760	2.188	2.460	6.240	4.810	5.205	5.080
26	0.426	0.750	2.141	2.400	6.136	5.010	5.258	4.160
27	0.407	0.740	2.493	2.630	6.594	6.100	5.144	4.310
28	0.408	0.740	2.776	2.830	7.015	5.610	5.188	4.530
29	0.433	0.800	2.804	2.700	6.972	5.930	5.250	4.390
30	0.452	0.840	3.111	3.040	7.197	5.610	5.306	4.440
31	*****	*****	3.652	4.050	*****	*****	5.265	4.810

TOTAL ACTUAL STREAMFLOW= 390.2161
 MEAN ACTUAL STREAMFLOW= 3.1985

TOTAL COMPUTED VOLUME= 406.6025
 MEAN COMPUTED VOLUME= 3.3328

GOODNESS OF FIT MEASURE= 0.9029

PERCENT SEASONAL DIFFERENCE= -4.1993

END OF DATA
 READY

Figure 27. (Continued)

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APPENDIX A
DETAILED PROGRAM FLOW CHARTS

- Figure A-1. Flow chart for subroutines of the snowmelt-runoff model program.
- Figure A-2. Flow diagram for DRVSNO, the main component of the snowmelt-runoff model.
- Figure A-3. Flow diagram for subroutine READIN.
- Figure A-4. Flow diagram for subroutine LAPSE.
- Figure A-5. Flow diagram for subroutine PRESNO.
- Figure A-6. Flow diagram for subroutine RUNOFF.
- Figure A-7. Flow diagram for subroutine GOOD.
- Figure A-8. Flow diagram for subroutine IOMTH.
- Figure A-9. Flow diagram for subroutine PLOTR.

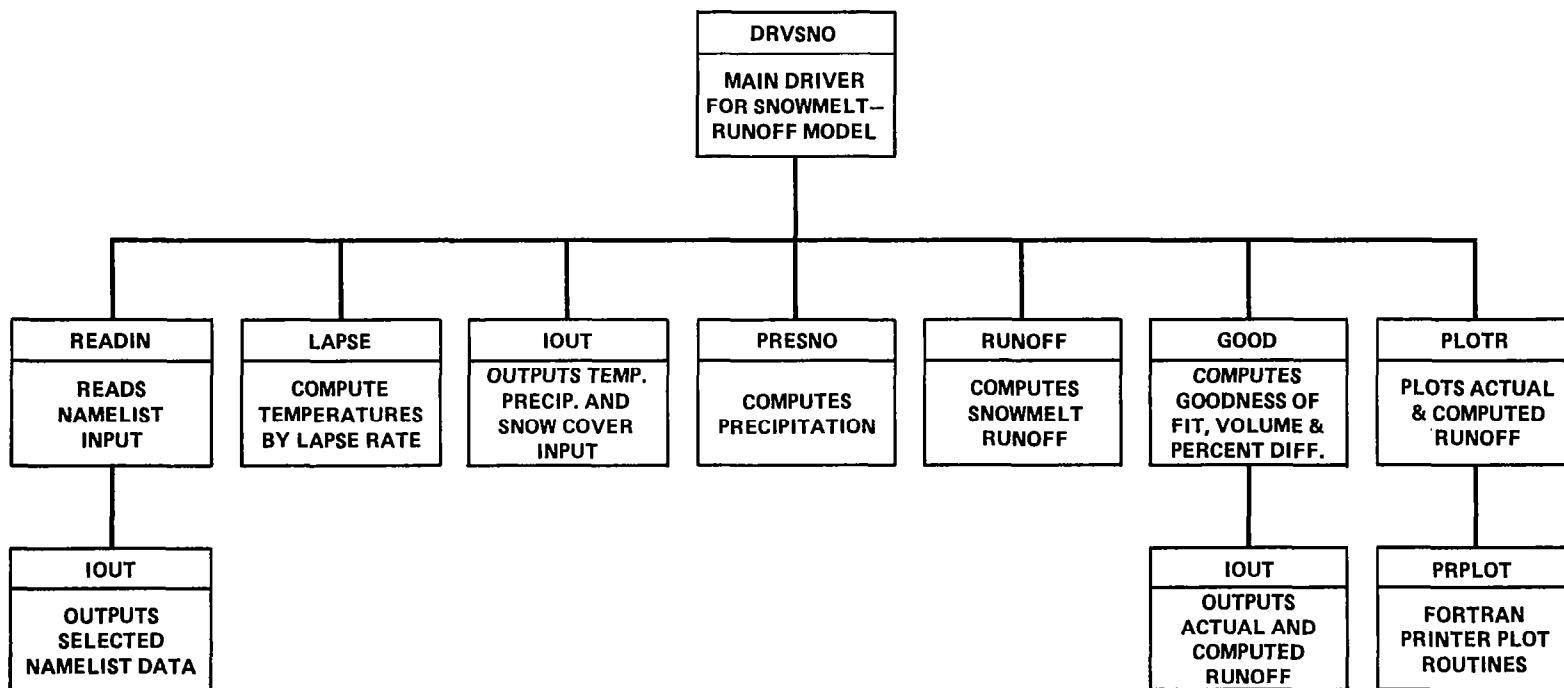


Figure A-1. Flow chart for subroutines of the snowmelt-runoff model program.

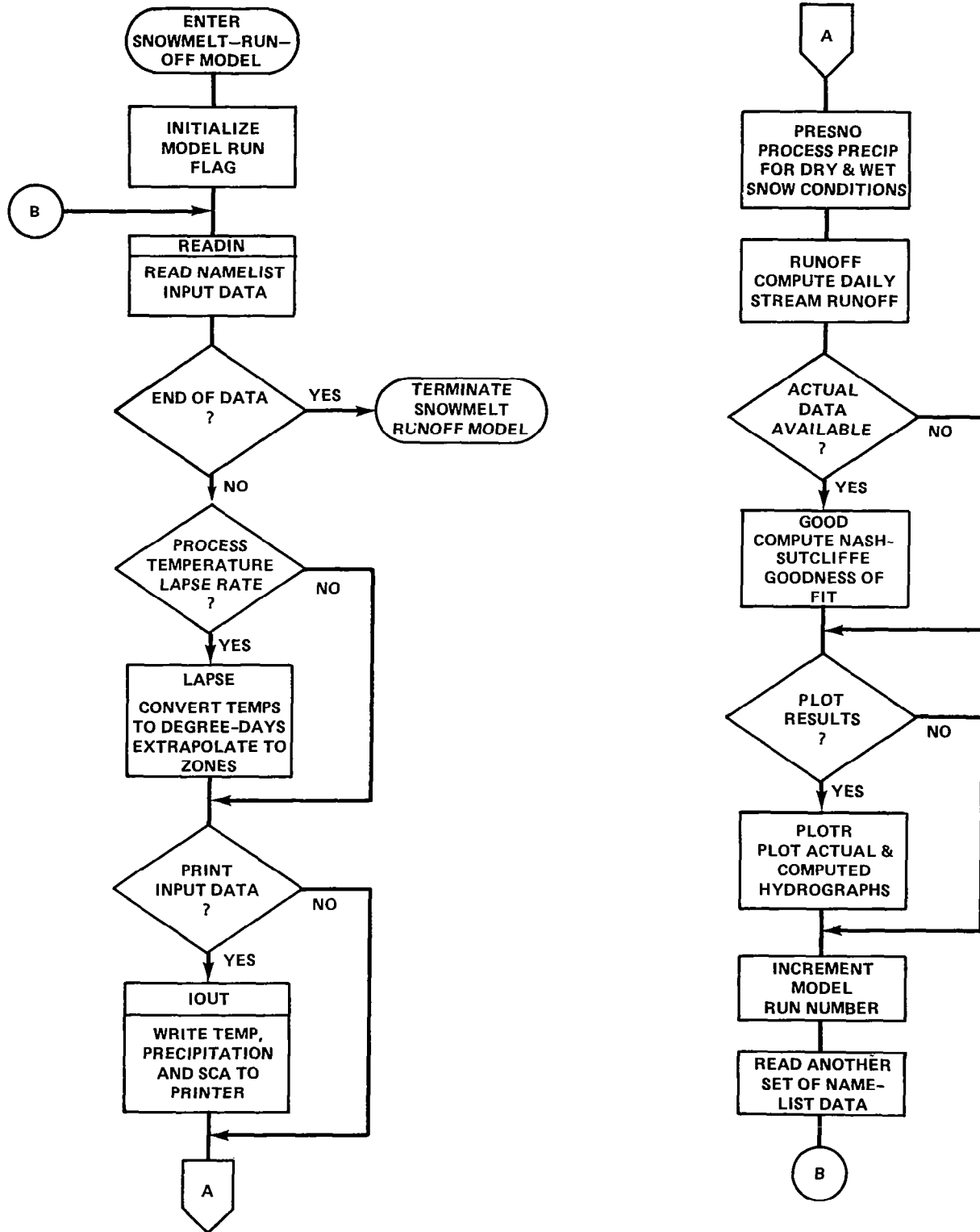


Figure A-2. Flow diagram for DRVSNO, the main component of the snowmelt-runoff model.

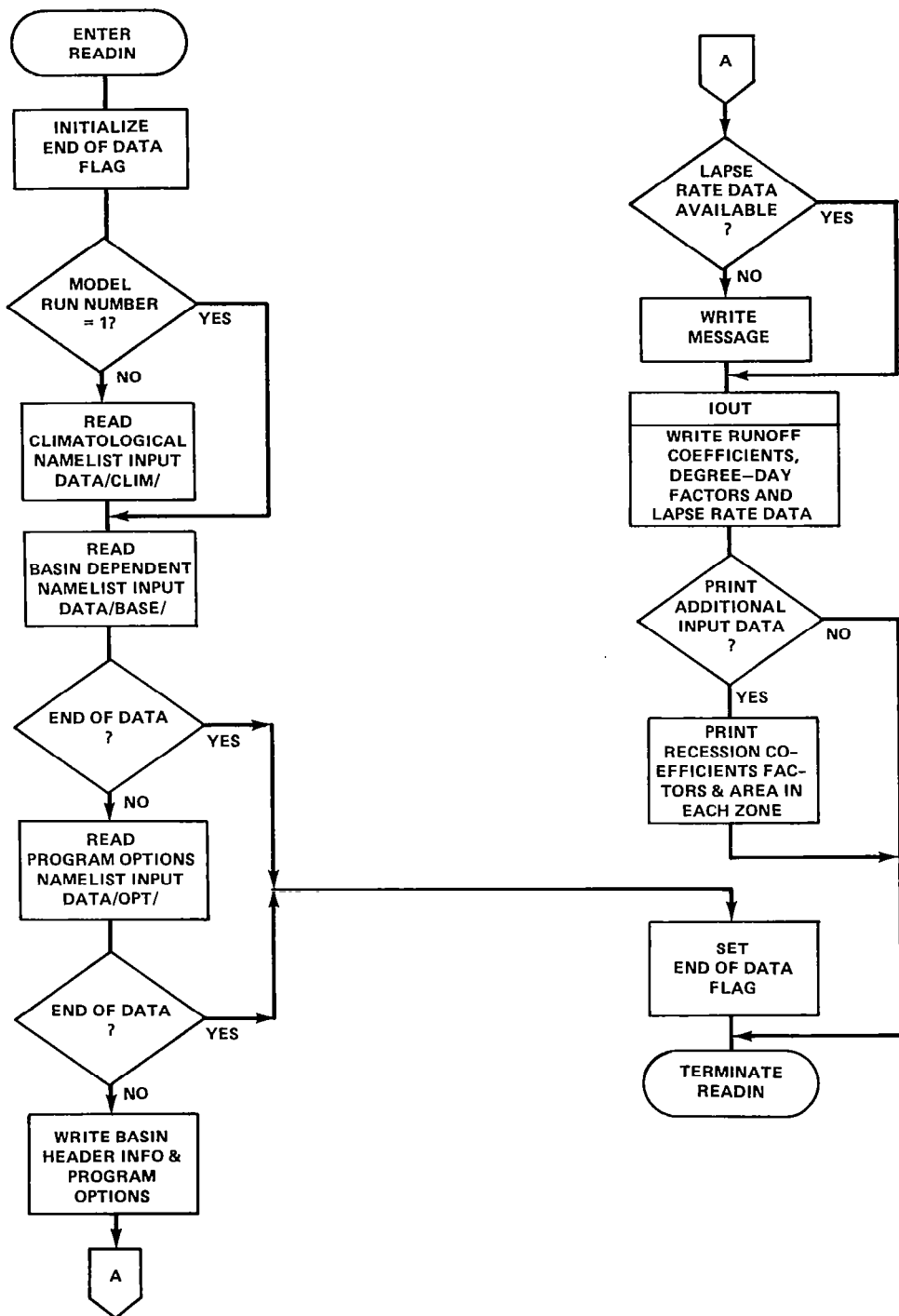


Figure A-3. Flow diagram for subroutine READIN.

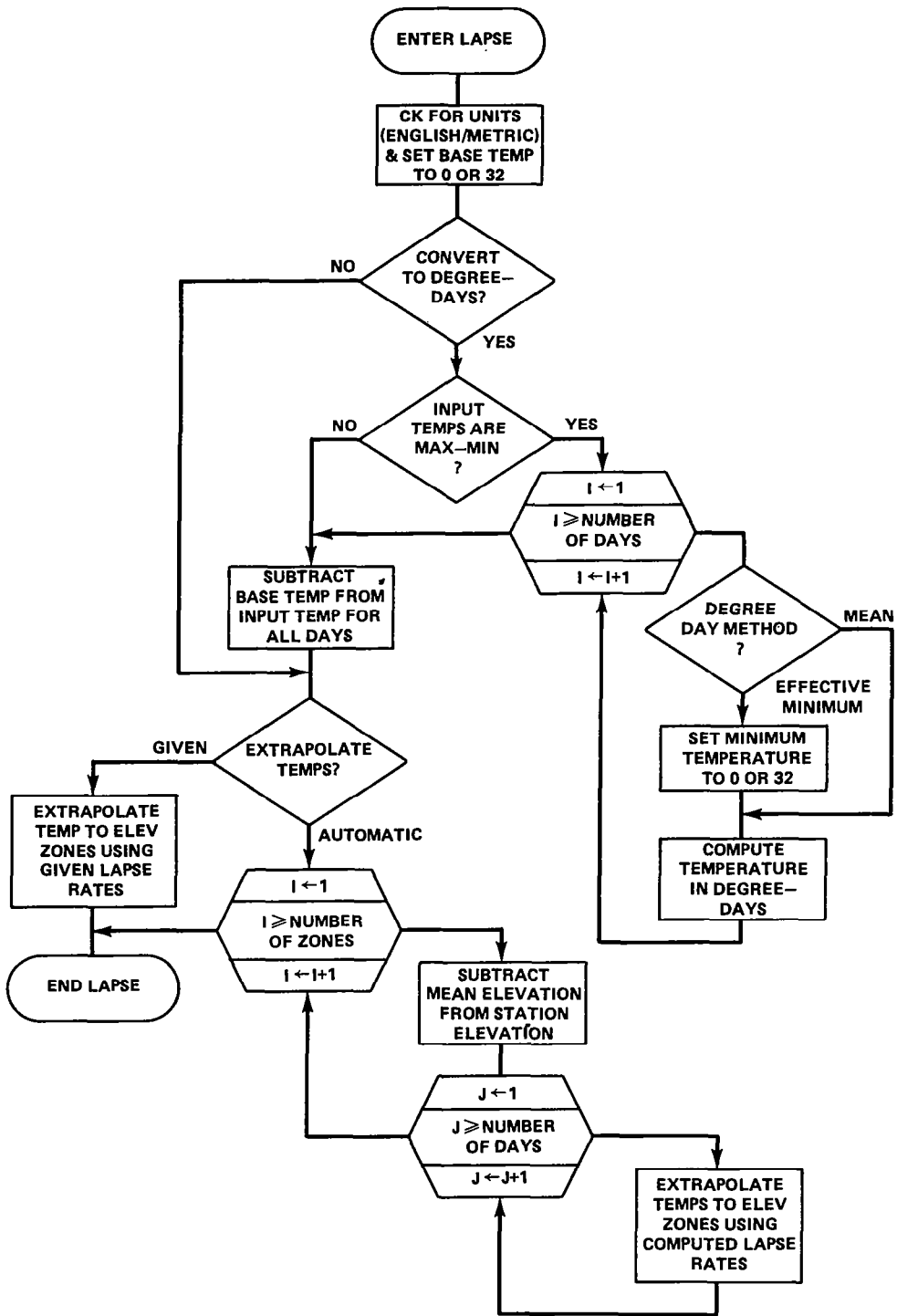


Figure A-4. Flow diagram for subroutine LAPSE.

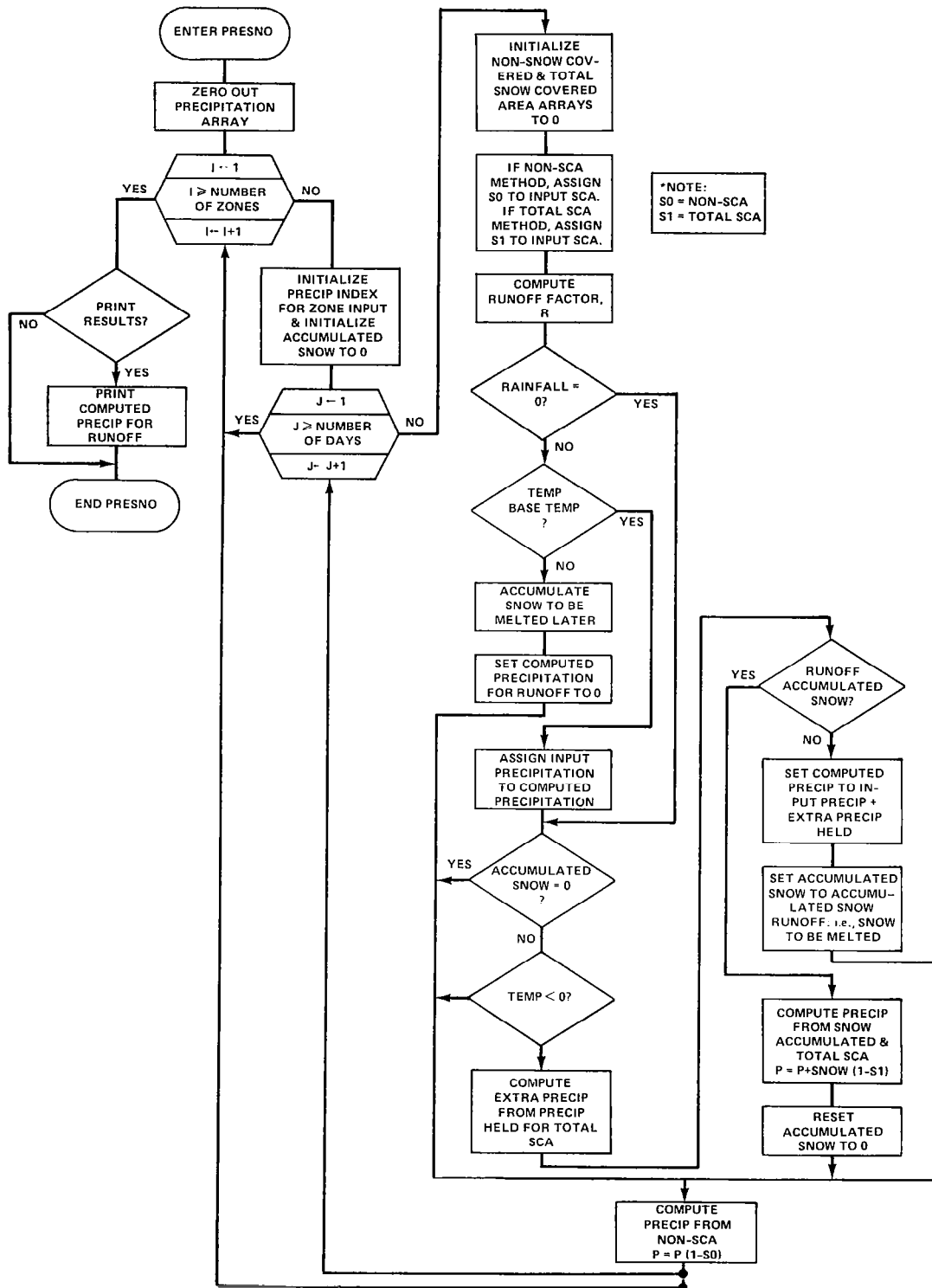


Figure A-5. Flow diagram for subroutine PRESNO.

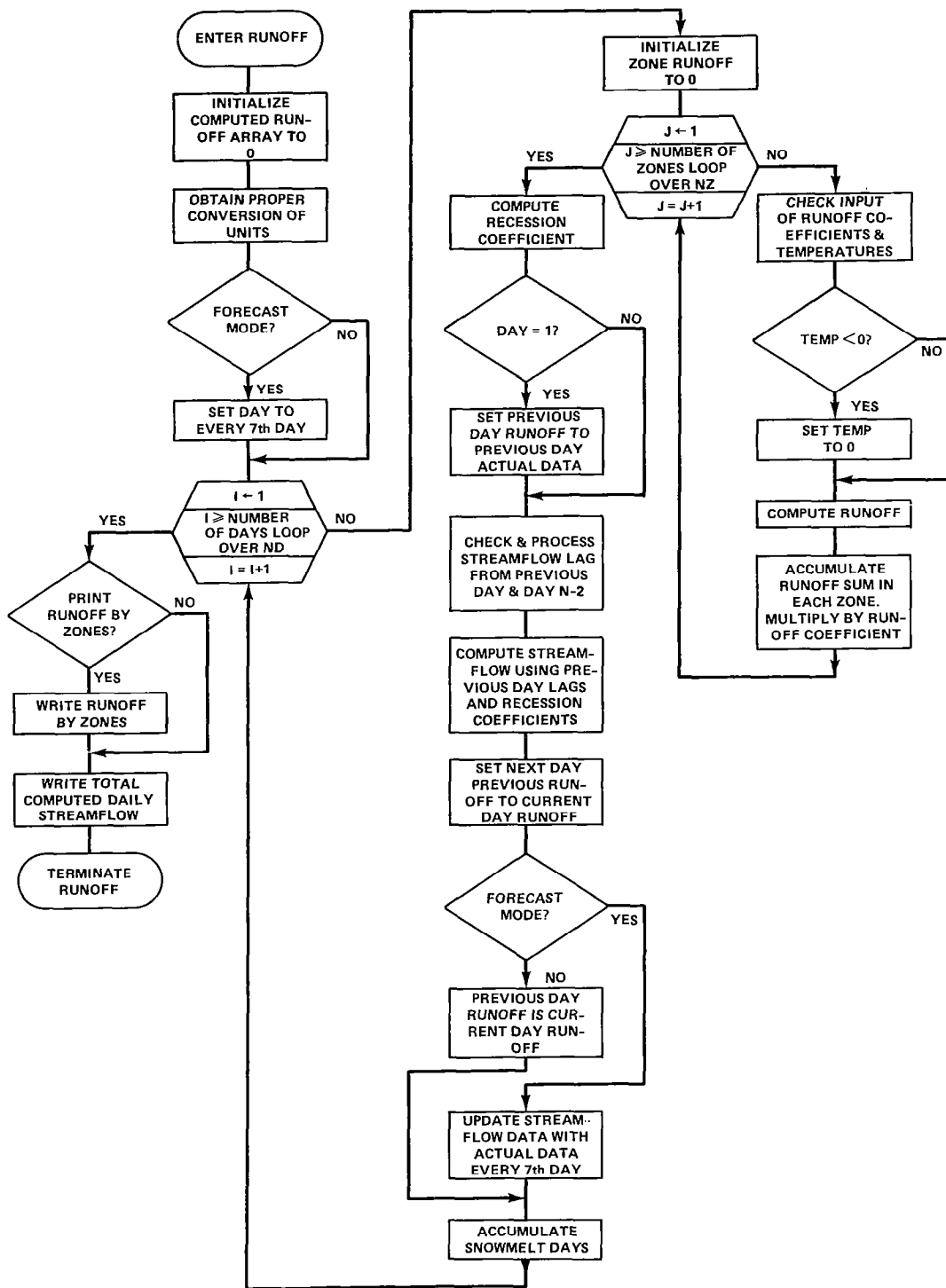


Figure A-6. Flow diagram for subroutine RUNOFF.

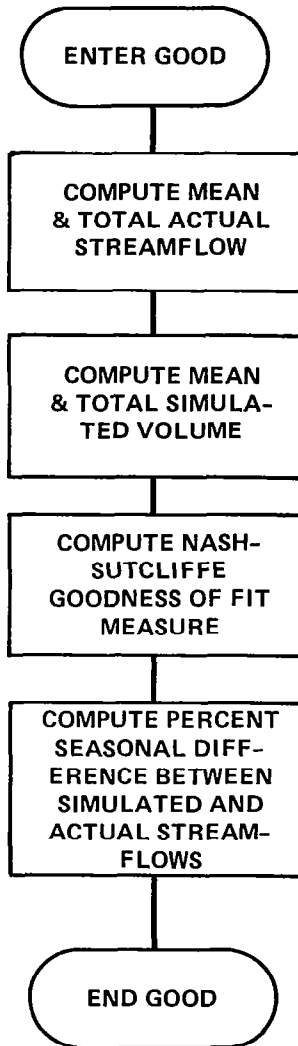


Figure A-7. Flow diagram for subroutine GOOD.

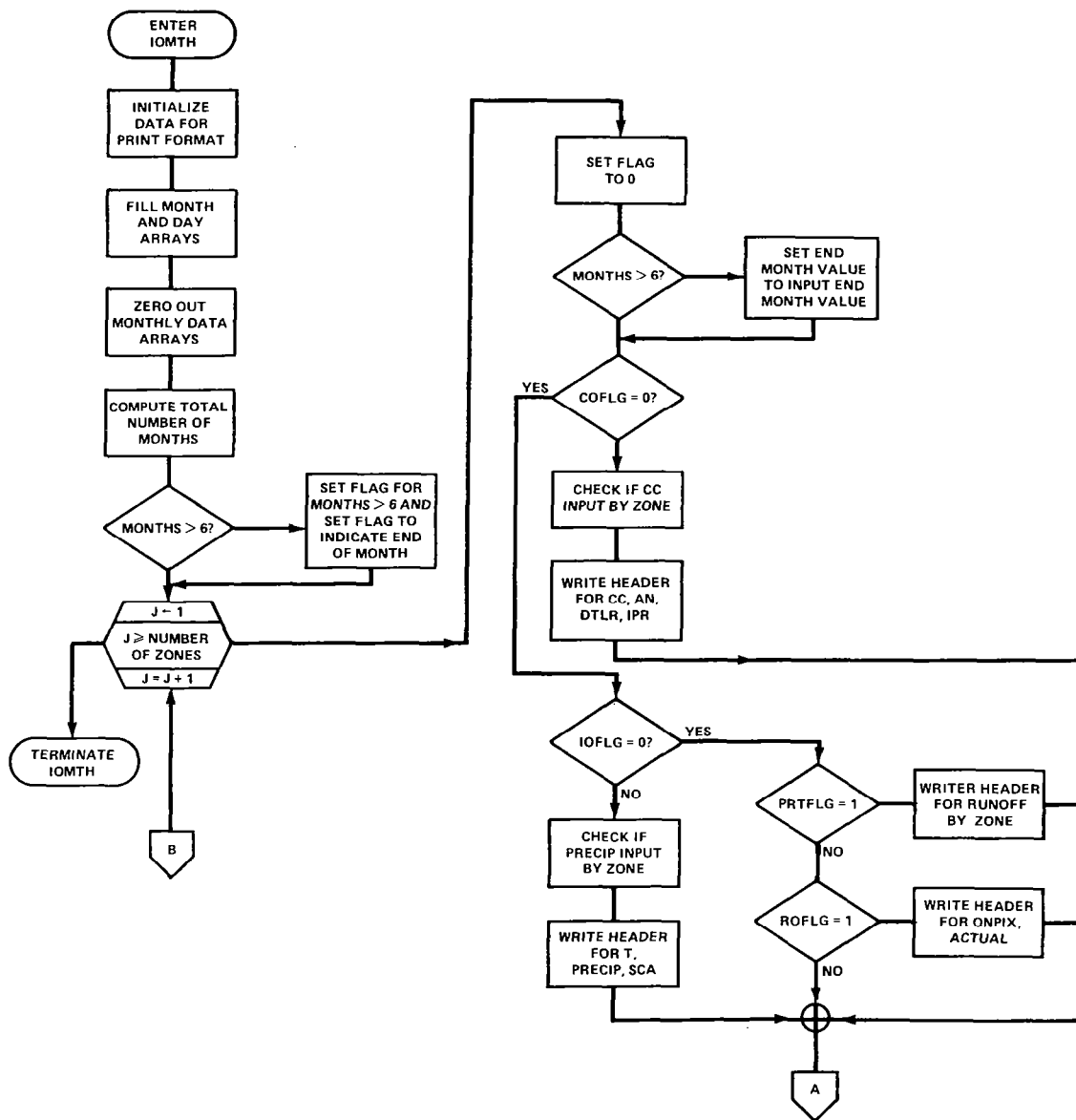


Figure A-8. Flow diagram for subroutine IOMTH.

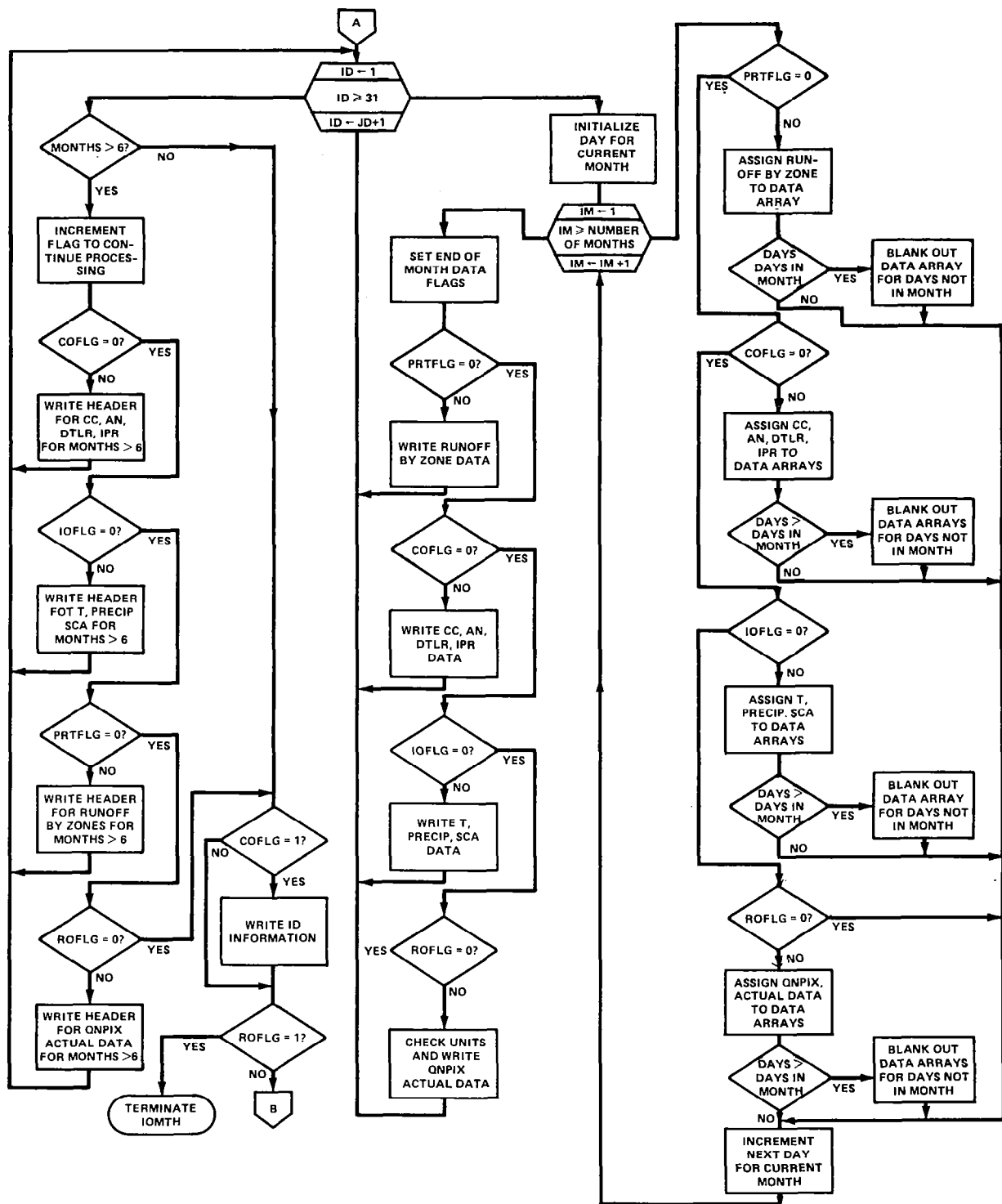


Figure A-8. (Continued)

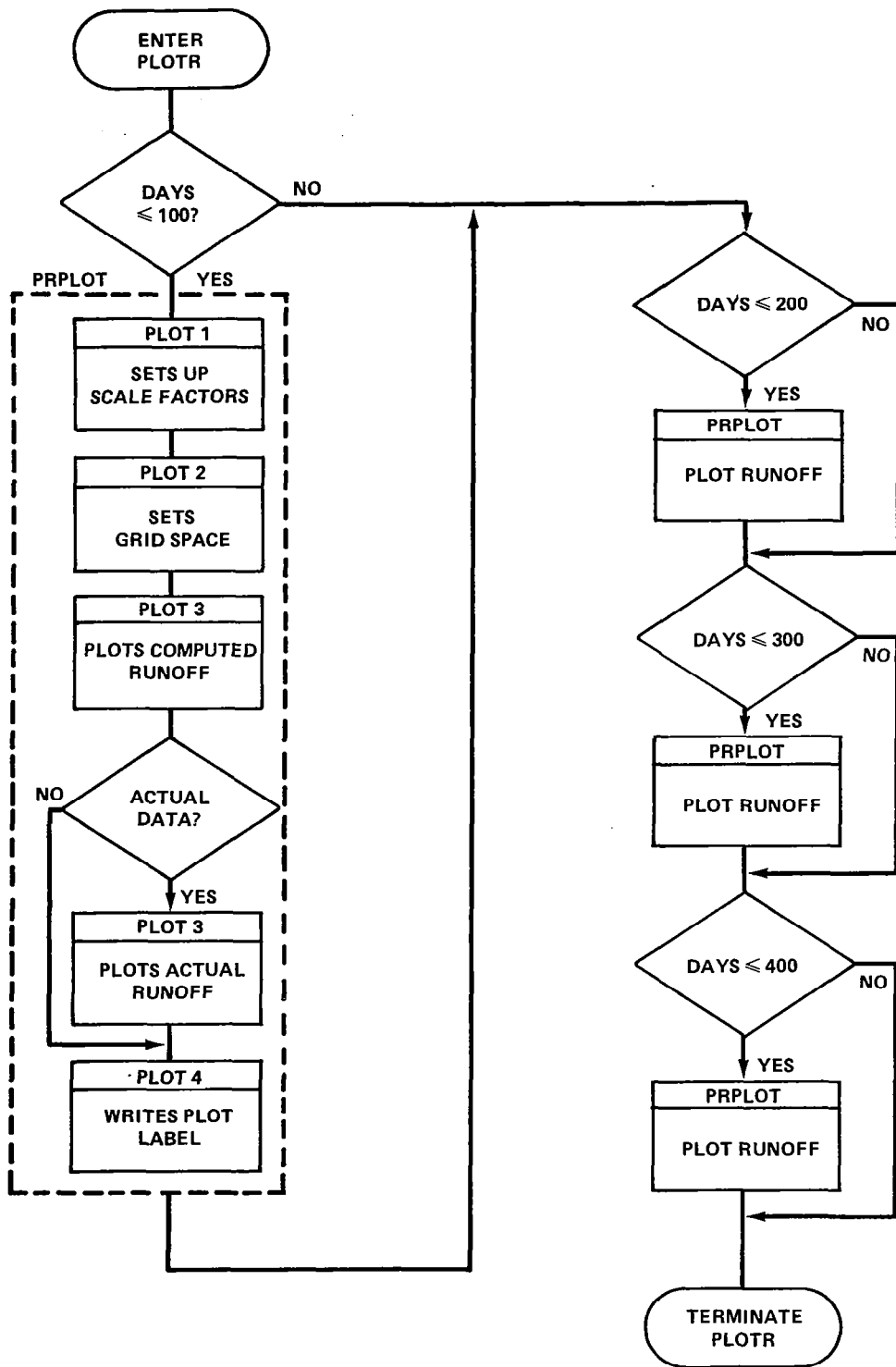


Figure A-9. Flow diagram for subroutine PLOTR.

APPENDIX B

FORTRAN Source Listing for the SRM Program and Subroutine PRPLOT with Compilation on the IBM 3081.

```

START  XX      XX  XXXXXXXXXXXX  XXXXXXXXXXXX  XXXXXXXXXXXX  XX      XX  XXXXXXXXXXXX  XXXXXXXXXXXX  XXX
START  XX      XX  XXXXXXXXXXXX  XXXXXXXXXXXX  XXXXXXXXXXXX  XXX      XX  XXXXXXXXXXXX  XXXXXXXXXXXX  XXXX
START  XX      XX  XX      XX  XX      XX  XX      XX  XX      XX  XX      XX  XX      XX  XX      XX  XX      XX
START  XX      XX  XX      XX  XX      XX  XX      XX  XX      XX  XX      XX  XX      XX  XX      XX  XX      XX
START  XXXX      XX  XX      XX  XXXXXXXXXXXX  XXXXXXXXXXXX  XX      XX  XXXXXXXXXXXX  XX      XX  XXXXXXXXXXXX
START  XXXX      XX  XX      XX  XXXXXXXXXXXX  XXXXXXXXXXXX  XX      XX  XXXXXXXXXXXX  XX      XX  XXXXXXXXXXXX
START  XX      XX  XX      XX  XX      XX  XX      XX  XX      XX  XX      XX  XX      XX  XX      XX  XX      XX
START  XX      XX  XX      XX  XX      XX  XX      XX  XX      XX  XX      XX  XX      XX  XX      XX  XX      XX
START  XX      XX  XX      XX  XXXXXXXXXXXX  XX      XX  XX      XX  XXXXXXXXXXXX  XX      XX  XXXXXXXXXXXX
START  XX      XX  XX      XX  XXXXXXXXXXXX  XX      XX  XX      XX  XXXXXXXXXXXX  XX      XX  XXXXXXXXXXXX

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```

START  XX      XXXXXXXXXXXX  XXXXXXXXXXXX  XX      XXXXXXXXXXXX  XX      XXXXXXXXXXXX  XXXXXXXXXXXX
START  XXX      XXXXXXXXXXXX  XXXXXXXXXXXX  XXX      XXXXXXXXXXXX  XXX      XXXXXXXXXXXX  XXXXXXXXXXXX
START  XXX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX
START  XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX
START  XX      XXXXXXXXX  XXXXXXXXXXXX  XX      XX      XX      XX      XX      XX      XX      XX      XX      XX
START  XX      XXXXXXXXXXXX  XXXXXXXXXXXX  XX      XX      XX      XX      XX      XX      XX      XX      XX      XX
START  XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX
START  XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX
START  XXXXXXXXX  XXXXXXXXX  XXXXXXXXXXXX  XXXXXXXXX  XX      XXXXXXXXX  XXXXXXXXXXXX  XXXXXXXXX
START  XXXXXXXXX  XXXXXXXXX  XXXXXXXXXXXX  XXXXXXXXX  XXXXXXXXX  XX      XXXXXXXXX  XXXXXXXXXXXX  XXXXXXXXX

```

```

START  XXXXXXXXXXXX  XXXXXXXXX  XXXXXXXXX  XXXXXXXXX  XXXXXXXXX  XXXXXXXXX  XXXXXXXXX  XX      XX
START  XXXXXXXXXXXX  XXXXXXXXX  XXXXXXXXX  XXXXXXXXX  XXXXXXXXX  XXXXXXXXX  XXXXXXXXX  XXXXXXXXX  XXX
START  XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX
START  XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX
START  XXXXXXXXX  XXXXXXXXX  XXXXXXXXX  XX      XX      XX      XX      XX      XX      XX      XX      XX      XX
START  XXXXXXXXX  XXXXXXXXX  XXXXXXXXX  XX      XX      XX      XX      XX      XX      XX      XX      XX      XX
START  XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX
START  XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX
START  XX      XX      XX      XXXXXXXXX  XXXXXXXXX  XX      XXXXXXXXX  XXXXXXXXX  XX      XXXXXXXXX
START  XX      XX      XX      XXXXXXXXX  XXXXXXXXX  XX      XXXXXXXXX  XXXXXXXXX  XX      XXXXXXXXX

```

```

START  X X X  XXXXXXXXXXX  XXXXXXXXXX  XXXXXXXXXX  XXXXXXXXXX  XXXXXXXXXX  XXXXXXXXXX  XXXXXXXXXX  XXXXXXXXXX
START  X X X  XXXXXXXXXXX  XXXXXXXXXX  XXXXXXXXXX  XXXXXXXXXX  XXXXXXXXXX  XXXXXXXXXX  XXXXXXXXXX  XXXXXXXXXX
START  XXX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX
START  XXX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX
START  X X X  XX      XX      XX      XX      XX      XX      XXXXXXXXXXX  XXXXXXXXXXX  XX      XX      XX
START  X X X  XX      XX      XX      XX      XX      XX      XXXXXXXXXXX  XXXXXXXXXXX  XX      XX      XX
START  XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX
START  XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX      XX
START  XXXXXXXXX  XXXXXXXXX  XXXXXXXXXX  XX      XXXXXXXXX  XXXXXXXXXX  XXXXXXXXXX  XXXXXXXXXX  XXXXXXXXXX
START  XXXXXXXXX  XXXXXXXXX  XXXXXXXXXX  XX      XXXXXXXXX  XXXXXXXXXX  XXXXXXXXXX  XXXXXXXXXX  XXXXXXXXXX

```

```

SNOW.MELT.RUNOFF.MODEL.FORT
00010      BLOCK DATA
00020 C
00030 C*****
00040 C
00050 C      FUNCTION - BLOCK DATA CONTAINS ALL OF THE NAMELIST AND
00060 C      OUTPUT VARIABLES IN ALL OF THE COMMON BLOCKS
00070 C      USED IN THE SNOWMELT-RUNOFF MODEL PROGRAM.
00080 C      DEFAULT VALUES ARE INDICATED WHERE APPLICABLE
00090 C
00100 C
00110 C
00120 C      COMMON BLOCK VARIABLES
00130 C      VARIABLE      COMMON      TYPE      DEFAULT      DESCRIPTION
00140 C      -----      -
00150 C      P              OUTDAT      R*4        -            PRECIPITATION CONTRIBUTING
00160 C              TO RUNOFF IN EACH ELEVATION
00170 C              ZONE(MET:CM;ENG:IN)
00180 C
00190 C      QNP1X          OUTDAT      R*4        -            COMPUTED AVERAGE DAILY
00200 C              STREAM RUNOFF(MET:M**3/SEC;
00210 C              ENG:FT**3/SEC)
00220 C
00230 C      XI            OUTDAT      R*4        -            ARRAY CONTAINING NUMBER OF
00240 C              DAYS FOR PLOT ROUTINE
00250 C
00260 C      TEMPT         OUTDAT      R*4        -            COMPUTED TEMPERATURE IN
00270 C              DEGREE-DAYS
00280 C
00290 C
00300 C
00310 C      NAMELIST /CLIM/ PARAMETERS
00320 C      CLIMATOLOGICAL DATA
00330 C
00340 C
00350 C      THAX          TBASE      R*4        -            MAXIMUM DAILY TEMPERATURES
00360 C              RECORDED FOR BASE STATION
00370 C              (MET:CM;ENG:F)
00380 C
00390 C      THIN          TBASE      R*4        -            MINIMUM DAILY TEMPERATURES
00400 C              RECORDED FOR BASE STATION
00410 C              (MET:CM;ENG:F)
00420 C
00430 C      T             CLIDAT      R*4        -            TEMPERATURE DATA EXPRESSED
00440 C              IN DEGREE-DAYS(MET:CM;
00450 C              ENG:F-D)
00460 C
00470 C      S             CLIDAT      R*4        -            SNOWCOVER AREA IN EACH
00480 C              ELEVATION ZONE(1.0=100%)
00490 C
00500 C      PRECIP        CLIDAT      R*4        -            DAILY MEASURED PRECIPITATION
00510 C              (MET:CM;ENG:IN)
00520 C
00530 C      ACTUAL        CLIDAT      R*4        -            ACTUAL STREAM RUNOFF FROM
00540 C              HISTORICAL DATA
00550 C              (MET:M**3/SEC;ENG:FT**3/SEC)
00560 C
00570 C      TCR11         CLIDAT      R*4        -            TEMPERATURE CONVERSION
00580 C              FACTOR FOR RAIN/SNOW CHECK
00590 C
00600 C      ND           CLIDAT      I*4        183         NUMBER OF SNOWMELT DAYS
00610 C
00620 C
00630 C      NAMELIST/BASE/ PARAMETERS
00640 C      BASIN DATA
00650 C
00660 C      BASIN         BASDAT      R*8        -            BASIN NAME
00670 C
00680 C      IYEAR         BASDAT      I*4        1979        MODEL YEAR
00690 C
00700 C      NZ           BASDAT      I*4        4           NUMBER OF ELEVATION ZONES
00710 C
00720 C      AREA         BASDAT      R*8        -            AREA IN EACH ELEVATION
00730 C              ZONE(MET:M**2;ENG:FT**2)
00740 C
00750 C      X            BASDAT      R*8        0.88480    X PARAMETER IN COMPUTING
00760 C              RECESSIION COEFFICIENT,K
00770 C
00780 C      Y            BASDAT      R*8        -0.067700  Y PARAMETER IN COMPUTING

```

00790 C					RECESSION COEFFICIENT,K
00800 C					
00810 C	PDR	GAGE	R*4	1.0	PREVIOUS DAY RUNOFF AT
00820 C					STREAM GAGE.
00830 C					
00840 C	PDM2	GAGE	R*4	0.0	PREVIOUS DAY-1 RUNOFF AT
00850 C					STREAM GAGE.
00860 C					
00870 C	QNS	GAGE	R*8	0.00	INITIAL RUNOFF VALUE.
00880 C					THIS VALUE SHOULD BE THE
00890 C					ACTUAL DATA VALUE DAY
00900 C					ACTUAL(1)-1.
00910 C					
00920 C	DTLR	BASDAT	R*4	-	ADJUSTMENT FOR TEMPERATURE
00930 C					LAPSE RATE(MET:C-D;
00940 C					ENG:F-J)
00950 C					
00960 C	AN	BASDAT	R*4	-	DEGREE DAY FACTORS
00970 C					(MET:CM/C/DAY;ENG:IN/F/DAY)
00980 C					
00990 C	CS	BASDAT	R*4	-	RUNOFF COEFFICIENTS
01000 C					FOR SNOW
01010 C					
01020 C	CR	BASDAT	R*4	-	RUNOFF COEFFICIENTS
01030 C					FOR RAIN
01040 C					
01050 C	IPR	BASDAT	I*2	-	PRECIPITATION METHOD OPTION
01060 C					0=NON-SNOW COVERED AREA
01070 C					1=TOTAL AREA
01080 C					
01090 C	ZMEAN	TRASE	R*8	-	HYPSOMETRIC MEAN ELEVATION
01100 C					OF EACH ZONE
01110 C					
01120 C	STATN	TRASE	R*8	-	ELEVATION OF BASE STATION
01130 C					
01140 C	MAXMIN	TRASE	I*2	0	FLAG TO INDICATE IF TEMPS
01150 C					ARE INPUT AS MAX-MIN
01160 C					0=TEMPS NOT AS MAX-MIN
01170 C					1=TEMPS INPUT AS MAX-MIN
01180 C					
01190 C	IEXT	TRASE	I*2	0	FLAG IF TEMPERATURES ARE TO
01200 C					BE AUTOMATICALLY EXTRAPOLATED
01210 C					TO ELEVATION ZONE.
01220 C					SINGLE STATION INPUT ONLY.
01230 C					0=EXTRAPOLATE USING GIVEN
01240 C					LAPSE RATES.
01250 C					1=AUTOMATICALLY EXTRAPOLATE
01260 C					
01270 C	IDEGMY	TRASE	I*2	1	FLAG IF TEMPERATURE IS TO BE
01280 C					COMPUTED IN DEGREE-DAYS
01290 C					0=NO COMPUTATION NECESSARY-
01300 C					TEMP IS INPUT IN DEGREE-
01310 C					DAYS.
01320 C					1=COMPUTE TEMP. IN DEGREE-
01330 C					DAYS.
01340 C					
01350 C					
01360 C					
01370 C					
01380 C					
01390 C	IRUN	OPTDAT	I*2	1	RUN SEQUENCE NUMBER
01400 C					
01410 C	MODE	OPTDAT	I*2	0	SNOWMELT MODE.
01420 C					0=SIMULATION MODE
01430 C					1=FORECAST MODE
01440 C					
01450 C	IPLT	OPTDAT	I*2	1	PLOT OPTION
01460 C					0=NO PLOT
01470 C					1=PLOT
01480 C					
01490 C	IFRINT	OPTDAT	I*2	0	FRINT OPTION
01500 C					0=NO PRINT
01510 C					1=PRINT
01520 C					
01530 C	UFLAG	OPTDAT	I*2	0	UNITS FLAG
01540 C					0=METRIC UNITS
01550 C					1=ENGLISH UNITS
01560 C					
01570 C	ACTFLG	OPTDAT	I*2	1	ACTUAL DATA FLAG
01580 C					0=NO ACTUAL DATA

NAMFLIST/UP1/ PARAMETERS
PROGRAM CONTROL AND OPTIONS

```

01590 C          1=ACTUAL DATA
01600 C
01610 C          IZONE      OPTDAT  I*2          3*0  ZONE DATA FLAG
01620 C          IZONE(1)=TEMPERATURE LAPSE
01630 C          RATE DATA
01640 C          IZONE(2)=PRECIPITATION DATA
01650 C          IZONE(3)=RUNOFF COEFFICIENTS
01660 C          0=NO ZONE DATA AVAILABLE
01670 C          1=DATA INPUT BY ZONES
01680 C
01690 C
01700 C          IDTFLG      OPTDAT  I*2          1    TEMPERATURE LAPSE RATE FLAG
01710 C          0=NO TEMPERATURE LAPSE RATE
01720 C          DATA AVAILABLE
01730 C          1=TEMPERATURE LAPSE RATE
01740 C          DATA AVAILABLE
01750 C
01760 C          MTHD         OPTDAT  I*2          1    METHOD USED TO COMPUTE
01770 C          TEMPERATURE IN DEGREE-
01780 C          DAYS IN TEMPERATURE PRE-
01790 C          PROCESSING ROUTINE
01800 C          0=MEAN METHOD
01810 C          1=EFFECTIVE MINIMUM METHOD
01820 C
01830 C          ITPROC       OPTDAT  I*2          1    TEMPERATURE PRE-PROCESSING
01840 C          FLAG.
01850 C          0=NO PRE-PROCESSING
01860 C          1=PREPROCESS TEMPERATURES
01870 C
01880 C          IPRRUN       OPTDAT  I*2          1    PRINT RUNOFF VALUES PER ZONE
01890 C          0=NO PRINT
01900 C          1=PRINT
01910 C
01920 C          ISTMTH       OPTDAT  I*4          4    INTEGER INDICATING START
01930 C          MONTH OF MODEL
01940 C
01950 C          IENMTH       OPTDAT  I*4          4    INTEGER INDICATING END
01960 C          MONTH OF MODEL
01970 C
01980 C          EXTERNAL REFERENCES - NONE
01990 C
02000 C          CALLED FROM - NONE
02010 C
02020 C          DESIGNER/PROGRAMMER - G.MAJOR, RESEARCH & DATA SYSTEMS, INC.
02030 C
02040 C          LANGUAGE/COMPUTER - FORTRAN IV/IBM 360/91 AT GSFC
02050 C
02060 C*****
02070 C
02080 C
02090 C          REAL*8 BASIN,AREA,X,Y,QNS,ZNEAN,STATN
02100 C
02110 C          INTEGER*2 JKUN,MODE,IPRRUN,IPL1,IPRIN1,UFLAG,ACTFLG,IZONE,
02120 C          1 IDTFLG,MTHD,ITPROC,MAXMIN,TEXT,IDEGBY,IPR
02130 C
02140 C          NAMELIST CLIMATOLOGICAL DATA COMMONS
02150 C
02160 C          COMMON/CLIRAT/1(366,8),S(366,8),PRECIP(366,8),ACTUAL(366),
02170 C          1 TCRT(366),ND
02180 C
02190 C          COMMON/TRASE/ZNEAN(8),STATN,THAX(366),THIN(366),MAXMIN,TEXT,
02200 C          1 IDEGBY
02210 C
02220 C          NAMELIST BASIN DATA COMMONS
02230 C
02240 C          COMMON/BASDAT/BASIN(2),AREA(8),X,Y,DILR(366,8),AN(366,8),
02250 C          1 CS(366,8),CR(366),NZ,IYEAR,IPR(366,8)
02260 C
02270 C
02280 C          NAMELIST OPTIONS COMMON
02290 C
02300 C          COMMON/OPTDAT/ISTMTH,IENMTH,IRUN,MODE,IPRRUN,IPL1,IPRINT,UFLAG,
02310 C          1 ACTFLG,IZONE(3),IDTFLG,MTHD,ITPROC
02320 C
02330 C          OUTPUT DATA COMMON
02340 C
02350 C          COMMON/OUTDAT/P(366,8),QNP1X(367),X1(367),TEMPT(366,8)
02360 C
02370 C          STREAMFLOW LAG AT STREAM GAGE COMMON
02380 C

```



```

02390          COMMON/GAGE/QNS,FDR(367),FDH2(367)
02400 C
02410 C          DATA STATEMENTS
02420 C
02430          DATA Y/2928*0.0/
02440          DATA S/2928*0.0/
02450          DATA PRECIP/2928*0.0/
02460          DATA ACTUAL/366*0.0/
02470          DATA TCRT/366*0./
02480          DATA ND/183/
02490          DATA THAX/366*0./
02500          DATA TMIN/366*0./
02510          DATA BASIN/'SOUTH FO','RK      '/
02520          DATA AREA/1.307,2.807,9.507,9.207,4*0.00/
02530          DATA X/0.88400/
02540          DATA Y/-0.067700/
02550          DATA QNS/0.00/
02560          DATA FDR/367*1./
02570          DATA FDM2/367*0./
02580          DATA OTLR/2928*0.0/
02590          DATA AN/2928*0.0/
02600          DATA CS/2928*0.0/
02610          DATA CR/366*0./
02620          DATA NZ/4/
02630          DATA JYFAK/1979/
02640          DATA IPR/2928*1/
02650          DATA ZMEAN/R*0.00/
02660          DATA STATN/0.00/
02670          DATA MAXMIN/1/
02680          DATA IEXT/0/
02690          DATA IDEGNY/1/
02700          DATA IKUN/1/
02710          DATA MORE/0/
02720          DATA IPLT/0/
02730          DATA IPRINT/0/
02740          DATA UNLAB/0/
02750          DATA ACTFLR/1/
02760          DATA IZONE/3*0/
02770          DATA INTFLR/1/
02780          DATA MTHD/0/
02790          DATA IIFROC/1/
02800          DATA IPRUN/1/
02810          DATA ISTMTH/4/
02820          DATA IENMTH/9/
02830          DATA P/2928*0.0/
02840          DATA QNFIX/367*0.0/
02850          DATA X3/367*0.0/
02860          DATA TEMPT/2928*0./
02870 C
02880          END
02890 C
02900 C          MAIN PROGRAM FOR SNOWMELT-RUNOFF MODEL (BRVSNO)
02910 C*****
02920 C
02930 C          FUNCTION - THIS IS THE MAIN PROGRAM DRIVER FOR THE SNOWMELT-
02940 C          RUNOFF MODEL PROGRAM AS DEVELOPED BY J.MARTINEC
02950 C          AND A. RANGO.
02960 C
02970 C          THE SNOWMELT-RUNOFF MODEL PROGRAM COMPUTES THE STREAM RUNOFF
02980 C          FOR ANY MOUNTAINOUS BASIN FOR ANY SNOWMELT SEASON UP TO 365
02990 C          DAYS AND ANY NUMBER OF ELEVATION ZONES UP TO 8 ZONES. THE
03000 C          BASIC INPUT PARAMETERS ARE SNOW COVERED AREA,TEMPERATURE,
03010 C          AND PRECIPITATION DATA. THE DATA MAY BE INPUT FOR EACH ZONE
03020 C          AND MAY BE INPUT IN EITHER METRIC OR ENGLISH UNITS.
03030 C          THE SNOWMELT-RUNOFF MODEL PROGRAM CAN BE OPERATED IN EITHER
03040 C          A SIMULATION MODE WHERE THE COMPUTED STREAM RUNOFF IS COMPARED
03050 C          TO ACTUAL STREAM RUNOFF(IF AVAILABLE) OR A FORECAST MODE WHERE
03060 C          THE STREAM RUNOFF IS COMPARED TO ACTUAL RUNOFF EVERY 7TH DAY.
03070 C
03080 C          INPUT PARAMETERS ARE READ INTO THE PROGRAM FROM THREE NAMELISTS,
03090 C          /CLIM/ CONTAINING CLIMATOLOGICAL DATA,/BASE/ CONTAINING BASIN
03100 C          DEPENDENT DATA, AND /OPT/ CONTAINING PROGRAM OPTIONS.
03110 C
03120 C          AS AN OPTION ALL INPUT PARAMETERS CAN BE REPRODUCED AS OUTPUT
03130 C          ON A MONTHLY BASIS. ALSO AS AN OPTION A PRINTER PLOT CAN BE
03140 C          PRODUCED WITH COMPUTED STREAMFLOW AND ACTUAL STREAMFLOW PLOTTED
03150 C          AS DISCHARGE RATE VS. NUMBER OF DAYS. A 'GOODNESS OF FIT' MEASURE
03160 C          AND TOTAL ACTUAL AND SIMULATED STREAMFLOW IS PRODUCED AS OUTPUT
03170 C
03180 C
03190 C
03200 C
03210 C          EXTERNAL REFERENCES--
03220 C          KEAUN - KEAUN IN NAMELIST AND OTHER INPUT DATA
03230 C          PRETMP - EXTRAPOLATES TEMPERATURES TO ELEVATION ZONE AND
03240 C          COMPUTES TEMPERATURES IN DEGREE-DAYS.
03250 C          PRESNO - CALCULATES PRECIPITATION CONTRIBUTING TO RUNOFF
03260 C          FOR EACH ELEVATION ZONE IN BASIN FROM DRY
03270 C          SNOW (NON-SNOW COVERED AREA) OR RIFE SNOW (TOTAL
03280 C          AREA) CONDITIONS.

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03290 C      RUNOFF - COMPUTES THE PREDICTED STREAM RUNOFF BASED ON THE
03300 C      SNOWMELT-RUNOFF MODEL EQUATIONS BY RANGO AND MARTINEZ
03310 C      GOOD - CALCULATES THE NASH-SUTCLIFFE GOODNESS OF FIT MEASURE
03320 C      AND COMPUTES THE MEAN ACTUAL STREAMFLOW, PREDICTED
03330 C      SEASONAL VOLUME AND PER CENT SEASONAL DIFFERENCE
03340 C      BETWEEN ACTUAL AND PREDICTED STREAMFLOW
03350 C      PLOTR - CONTAINS PLOT ROUTINES FROM THE FORTRAN PRPLOT
03360 C      PACKAGE TO PLOT ACTUAL AND PREDICTED STREAMFLOW
03370 C      IOUT - UTILITY PROGRAM TO OUTPUT RESULTS IN MONTHLY AND
03380 C      DAILY FORMAT.
03390 C
03400 C      CALLED FROM:
03410 C      NOTHING - THIS IS THE MAIN DRIVER
03420 C
03430 C      LANGUAGE/COMPUTER - FORTRAN IV/IBM 360/91 AT GSFC
03440 C
03450 C      DESIGNER/PROGRAMMER - G. NAJOK, RESEARCH & DATA SYSTEMS, INC.
03460 C
03470 C      REFERENCE - RANGO, A. AND MARTINEZ, J. (1979) APPLICATION OF A
03480 C      SNOWMELT-RUNOFF MODEL USING LANDSAT DATA,
03490 C      NORDIC HYDROLOGY, VOL. 10.
03500 C
03510 C*****
03520 C
03530 C
03540 C      REAL*8 BASIN,AREA,X,Y,QNS,ZNFAN,STAIN
03550 C
03560 C      INTEGER*2 IRIUN,MODE,IPRRUN,IPLOT,IPRINT,UFLAG,ACTFLG,IZONE,
03570 C      1 IDIFLG,MTHD,ITPROC,MAXMIN,IEXT,IDGBDY,IPR,IQFLG,ROFLG,
03580 C      2 COFLG,DTEFLG,IOFLG,FOFLG
03590 C
03600 C      DIMENSION RUND(366,B)
03610 C
03620 C***** COMMON BLOCKS *****
03630 C
03640 C      COMMON/CI DAT/I(366,B),S(366,B),PRECIP(366,B),ACTUAL(366,B),
03650 C      1 ITRT(366),ND
03660 C
03670 C      COMMON/TRASE/ZNFAN(B),STAIN,THAX(366),IRIN(366),MAXMIN,IEXT,
03680 C      1 IDGBDY
03690 C
03700 C      COMMON/OUTDAT/P(366,B),QNFIX(367),X1(367),TEMP(366,B)
03710 C
03720 C      COMMON/RASDAT/RASIN(2),AREA(B),X,Y,DTR(366,B),AM(366,B),
03730 C      1 CS(366,B),CR(366),NZ,IYFAR,IPR(366,B)
03740 C
03750 C      COMMON/OP1DAT/ISTMTH,IFNTH,IRUN,MODE,IPRRUN,IPLOT,IPRINT,UFLAG,
03760 C      1 ACTFLG,IZONE(3),IDIFLG,MTHD,ITPROC
03770 C
03780 C      COMMON/GAGE/QNS,PDR(367),FHMZ(367)
03790 C
03800 C
03810 C*****
03820 C      DATA RUND/2928*0.0/
03830 C
03840 C
03850 C      READ INPUT DATA -- CALL READIN
03860 C
03870 C
03880 C      ISET=0
03890 C      10 CALL READIN(ISET,TEND)
03900 C
03910 C      IF END OF DATA THEN TERMINATE PROGRAM
03920 C
03930 C      IF(IFND.GT.0) GO TO 30
03940 C
03950 C      CALL TEMPERATURE PRE-PROCESSING ROUTINE IF DESIRED -- CALL PRETMP
03960 C
03970 C      IF(ITPROC.EQ.1) CALL IAPSE(STAIN,ND,NZ,MAXMIN,TEMP,THAX,TRIN,
03980 C      1 DTR,UFLAG,MTHD,ZNFAN,IEXT,IDGBDY,T)
03990 C
04000 C      IF(TPRINT.EQ.0) GO TO 100
04010 C
04020 C      PRINT TEMPERATURE (IN DEGREE-DAYS), PRECIPITATION, AND SNOW
04030 C      COVERED AREA ON MONTHLY AND ZONAL BASIS --- CALL IOUT
04040 C
04050 C      IOFLG=1
04060 C      ROFLG=0
04070 C      COFLG=0
04080 C      DTEFLG=0
04090 C      IOFLG=0
04100 C      FOFLG=0
04110 C
04120 C      IF(ITPROC.EQ.1) GO TO 50
04130 C      DO 51 I=1,NZ
04140 C          DO 52 J=1,ND
04150 C              TEMP(I,J)=T(I,J)
04160 C      52 CONTINUE
04170 C      51 CONTINUE
04180 C
04190 C      50 CALL IOUT(NZ,BASIN,IYFAR,IZONE,ISTMTH,IFNTH,TEMP,PRECIP,S,

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04200      1 IPR,RUNOFF,QNP1X,ACTUAL,CS,AN,DTR,UFLAG,IOFLG,ROFLG,COFLG,
04210      2 DTFLG,THAX,THIN,TCRET,CR,P,TOFLG,POFLG)
04220 C
04230 C
04240 100      CONTINUE
04250 C
04260 C      CALL ROUTINE TO COMPUTE PRECIPITATION CONTRIBUTING TO RUNOFF
04270 C
04280 C      CALL PRESNO
04290 C
04300 C      COMPUTE PREDICTED RUNOFF -- CALL RUNOFF
04310 C
04320 C      CALL RUNOFF
04330 C
04340 C      CHECK IF ACTUAL DATA AVAILABLE
04350 C
04360 C      IF(ACTFLG.EQ.0) GO TO 900
04370 C
04380 C      COMPUTE RESULTS -- CALL GOOD
04390 C
04400 C
04410 C      CALL GOOD(QNP1X,ACTUAL,ND)
04420 C
04430 900      CONTINUE
04440 C
04450 C      CHECK IF PLOT IS DESIRED AND CALL PLOT ROUTINE --CALL PLOT
04460 C
04470 C      IF(IPLT.EQ.0) GO TO 20
04480 C
04490 C      CALL PLOT(QNP1X,ACTUAL,X1,ND,UFLAG,ACTFLG)
04500 C
04510 20      CONTINUE
04520 C
04530 C      CHECK IF NOT FIRST RUN AND SET FIRST RUN FLAG,ISET
04540 C
04550 C      ISET=ISET+1
04560 C
04570 C
04580 C      GO TO 10
04590 30      WRITE(6,1500)
04600 1500     FORMAT(' END OF DATA')
04610 C
04620 C      STOP
04630 C      END
04640 C      SURROUTINE READIN(ISET,IEND)
04650 C
04660 C*****
04670 C      FUNCTION - READS INPUT DATA FROM NAMELISTS /CLIM/,/BASE/,
04680 C      AND /OPT/, ALSO OUTPUTS HEADER INFORMATION
04690 C      AND,ON OPTION,WILL REPRODUCE ALL INPUT PARAMETERS.
04700 C
04710 C
04720 C      ARGUMENT LIST -
04730 C      VARIABLE TYPE IO DESCRIPTION
04740 C      -----
04750 C      ISET I*4 I FLAG TO INDICATE FIRST RUN OF MODEL
04760 C      IEND I*4 0 FLAG TO INDICATE END OF DATA
04770 C
04780 C      COMMON BLOCK VARIABLES USED -
04790 C      VARIABLE COMMON TYPE IO
04800 C      -----
04810 C      AREA BASDAT R*8 I
04820 C      X BASDAT R*8 I
04830 C      Y BASDAT R*8 I
04840 C      T CLIDAT R*4 I
04850 C      S CLIDAT R*4 0
04860 C      PRECIP CLIDAT R*4 I
04870 C      ACTUAL CLIDAT R*4 I
04880 C      CS BASDAT R*4 I
04890 C      DTR BASDAT R*4 0
04900 C      AN BASDAT R*4 0
04910 C      ND BASDAT I*4 I
04920 C      PDR GAGE R*4 I
04930 C      PDM2 GAGE R*4 I
04940 C      QNS GAGE R*8 I
04950 C      NZ CLIDAT I*4 I
04960 C      IRUN OPTDAT I*4 I
04970 C      MODE OPTDAT I*4 I
04980 C      BASIN BASDAT R*8 I
04990 C      IPLT OPTDAT I*2 I
05000 C      IPRINT OPTDAT I*2 I
05010 C      UFLAG OPTDAT I*2 I
05020 C      IZONE OPTDAT I*2 I
05030 C      IOFLG OPTDAT I*2 I
05040 C      THAX TRASE R*4 I
05050 C      THIN TRASE R*4 I
05060 C      ZMEAN TRASE R*8 I
05070 C      STATN TRASE R*8 I
05080 C      MAYNIN TRASE I*2 I
05090 C      METHD OPTDAT I*2 I

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05100 C      ITPROC      OPTDAT  1*2  1
05110 C
05120 C
05130 C
05140 C      EXTERNAL REFERENCES -
05150 C      IOUT - UTILITY ROUTINE TO OUTPUT RESULTS IN MONTHLY
05160 C      AND DAILY FORMAT.
05170 C
05180 C
05190 C      CALLED BY -- MAIN
05200 C
05210 C      COMPUTER/LANGUAGE -- IBM 360 AT GSEC/FURIKAN IV
05220 C
05230 C      DESIGNER/PROGRAMMER -- G.MAUR, RESEARCH & DATA SYSTEMS, INC.
05240 C
05250 C*****
05260 C
05270 C      REAL*8  BASIN,ARFA,X,Y,QNS,ZNEAN,STATN,UNITS(2),UNIT
05280 C
05290 C      INTEGER*2  IRUN,MODE,IPRRUN,IPLT,IPRINT,UFLAG,ACTFLG,IZONE,
05300 C      1  INTFLG,MTHD,ITPROC,MAXMIN,IEXT,IREGDY,IPR,IOFLG,ROFLG,
05310 C      2  COFLG,DTFLG,TOFLG,POFLG
05320 C
05330 C      DIMENSION RUNOF(366,8),TEMPT(366,8),AMUNIT(3),AEUNIT(3)
05340 C
05350 C      DATA RUNOF/2928*0.0/
05360 C      DATA TEMPT/2928*0./
05370 C      DATA UNITS/'METERS', 'FEET' //
05380 C      DATA AMUNIT/'SQ.', 'METERS', 'RS' //
05390 C      DATA AEUNIT/'SQ.', 'MILE', 'S' //
05400 C
05410 C***** COMMON BLOCKS *****
05420 C
05430 C      COMMON/CLIDAT/T(366,8),S(366,8),PRECIP(366,8),ACTUAL(366),
05440 C      1  TCRIT(366),ND
05450 C
05460 C      COMMON/TRASE/ZNEAN(8),STATN,TMAX(366),TMIN(366),MAXMIN,IEXT,
05470 C      1  IREGDY
05480 C
05490 C
05500 C      COMMON/OPTDAT/ISTHMH,IFNMTH,IRUN,MODE,IPRRUN,IPLT,IPRINT,UFLAG,
05510 C      1  ACTFLG,IZONE(3),IDTFLG,MTHD,ITPROC
05520 C
05530 C      COMMON/BASDAT/BASIN(2),AREA(8),X,Y,DTLR(366,8),AN(366,8),
05540 C      1  CS(366,8),CR(366),NZ,IYEAR,IPR(366,8)
05550 C
05560 C
05570 C      COMMON/BASE/QNS,PDR,PDM2(367)
05580 C
05590 C
05600 C*****
05610 C
05620 C
05630 C
05640 C***** INPUT NAMELIST *****
05650 C
05660 C      CLIMATOLOGICAL NAMELIST PARAMETERS
05670 C
05680 C      NAMELIST/CLIN/ND,1,S,ACTUAL,PRECIP,TMAX,TMIN,TCRIT
05690 C
05700 C      BASIN NAMELIST PARAMETERS
05710 C
05720 C      NAMELIST/BASE/BASIN,NZ,IYEAR,AREA,X,Y,QNS,PDR,PDM2,DTLR,AN,CS,
05730 C      1  CR,ZNEAN,STATN,MAXMIN,IEXT,IREGDY,IPR
05740 C
05750 C      PROGRAM OPTION NAMELIST PARAMETERS
05760 C
05770 C      NAMELIST/OPT/IRUN,MODE,IPLT,IPRINT,UFLAG,ACTFLG,IZONE,INTFLG,
05780 C      1  MTHD,ITPROC,IPRRUN,ISTHMH,IENMTH
05790 C
05800 C
05810 C
05820 C
05830 C      IEND=0
05840 C
05850 C      CHECK IF NOT FIRST RUN
05860 C
05870 C
05880 C      IF(ISET,GE,1) GO TO 10
05890 C
05900 C      READ CLIM NAMELIST FOR CLIMATOLOGICAL DATA
05910 C
05920 C      READ(5,CLIN,END=995)
05930 C 995  CONTINUE
05940 C
05950 C
05960 C      READ BASE AND OPT NAMELIST FOR BASIN AND PROGRAM OPTION DATA
05970 C
05980 C 10  READ(9,BASE,END=999)
05990 C      READ(9,OPT,END=999)

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06000      IF(UFLAG,EQ,0) UNIT=UNITS(1)
06010      IF(UFLAG,EQ,1) UNIT=UNITS(2)
06020 C
06030 C      WRITE RUN NUMBR AND BASIN NAME
06040 C
06050      WRITE(6,1500)
06060 C
06070      WRITE(6,2000) JKUN,BASIN,IYFAR
06080 C
06090 C      WRITE SNOWMFLT RUNOFF PROGRAM MODE
06100 C
06110      WRITE(6,2500) MODE
06120 C
06130 C      WRITE PROGRAM OPTIONS
06140 C
06150      WRITE(6,3000)
06160 3000  FORMAT(' PROGRAM OPTIONS (0=OFF,1=ON)')
06170      WRITE(6,3500) (PL), (PRINT,UFLAG,ACTFLG, (IZONE(I), I=1,3), IDTFLG,
06180      1 MTHD,ITPROC,IPRRUN,IFXT,IFGBDY,MAXMIN,ISTMTH,IENMTH)
06190 C
06200 C
06210 C      WRITE NUMBR OF SNOWMELT DAYS AND ELEVATION ZONES
06220 C
06230      WRITE(6,5000) ND,NZ
06240 C
06250 C      WRITE RECOSSION COEFFICIENT FACTORS X AND Y
06260 C
06270      IF(PDR(1),EQ,0.5) LAG=6
06280      IF(PDR(1),EQ,0.7) LAG=10
06290      IF(PDR(1),EQ,0.75) LAG=12
06300      IF(PDR(1),EQ,0.8) LAG=15
06310      IF(PDR(1),EQ,1.0) LAG=18
06320      WRITE(6,6000) X,Y,QNS,LAG
06330 C
06340 C      WRITE AREA IN EACH ELEVATION ZONE
06350 C
06360      IF(UFLAG,EQ,0) WRITE(6,6500) ARUNIT
06370      IF(UFLAG,EQ,1) WRITE(6,6500) AEUNIT
06380      WRITE(6,7000) (I,AREA(I),I=1,NZ)
06390 C
06400 C      WRITE HYPSONOMETRIC MEAN ELEVATION IN EACH ZONE
06410 C
06420      WRITE(6,6900) UNIT
06430      WRITE(6,7000) (T,ZMEAN(I),I=1,NZ)
06440 C
06450 C
06460 C      WRITE BASE STATION ELEVATION
06470 C
06480      WRITE(6,7600) UNIT
06490      WRITE(6,7700) STATN
06500 C
06510 C      CHECK IF LAPSE RATE DATA IS PROVIDED
06520 C
06530      IF(IDTFLG,EQ,0) WRITE(6,5500)
06540 C
06550 C      WRITE INPUT DATA IF IPRINT DATA FLAG IS SET
06560 C
06570      IF(IPRINT,EQ,0) GO TO 900
06580      IF(MAXMIN,EQ,0) GO TO 910
06590 C
06600      IOFLG=0
06610      ROFLG=0
06620      COFLG=0
06630      DTFLG=0
06640      TOFLG=1
06650      POFLG=0
06660      CALL IOUT(NZ,BASIN,IYEAR,IZONE,ISTMTH,IENMTH,TEMP,PRECIP,S,
06670      1 IPR,RUNOF,QNP1X,ACTUAL,CS,AN,BTLR,UFLAG,IOFLG,ROFLG,COFLG,
06680      2 DTFLG,TMAX,TMIN,TCRIT,CR,P,TOFLG,POFLG)
06690 C
06700 C      WRITE RUNOFF COEFFICIENTS,DEGREE DAY FACTORS AND PRECIPITATION
06710 C      METHOD ON MONTHLY AND ZONAL BASIS
06720 C
06730 910  IOFLG=0
06740      ROFLG=0
06750      COFLG=1
06760      DTFLG=0
06770      TOFLG=0
06780      POFLG=0
06790      CALL IOUT(NZ,BASIN,IYFAR,IZONE,ISTMTH,IENMTH,TEMP,PRECIP,S,
06800      1 IPR,RUNOF,QNP1X,ACTUAL,CS,AN,BTLR,UFLAG,IOFLG,ROFLG,COFLG,
06810      2 DTFLG,TMAX,TMIN,TCRIT,CR,P,TOFLG,POFLG)
06820 C
06830 C
06840 C      WRITE LAPSE RATE AND CRITICAL TEMPERATURE VALUES
06850 C
06860      IOFLG=0
06870      ROFLG=0
06880      COFLG=0
06890      DTFLG=1

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06900      POFLG=0
06910      TOFLG=0
06920      CALL JDU1(NZ,RASIN,1YFAK,I7ONE,1S1MTH,1FNH1H,1EMP1,PKFCIP,6,
06930      1 IPR,RUNOF,QNFI,ACTUAL,CS,AN,DTLR,UFLAG,IOFLG,ROFLG,COFLG,
06940      2 DTFLG,TMAX,THIN,1CRIT,CR,P,TOFLG,POFLG)
06950      GO TO 900
06960 C
06970 C      SET ENR FLAG
06980 C
06990 999  IFND=1
07000 C
07010 C
07020 900  RETURN
07030 1500  FORMAT('C',////////)
07040 2000  FORMAT('//SX,'RUN #',I5,2X,'BASIN=',2A8,2X,'YEAR=',15//)
07050 2500  FORMAT('// MODE (0=SIMULATED,1=-FURCAST)=',I3//)
07060 3500  FORMAT(' PLOT OPTION=',I2,2X,'PRINT OPTION=',I2,2X,'UNITS(0=',
07070      1 'METRIC,1=ENGLISH)=',(2//1X,'ACTUAL DATA FLAG=',I2,2X,'ZONE ',
07080      2 'INPUT DATA(TEMP,PRECIP,RUNOFF COFF.)=',3I2//)
07090      3 1X,'LAPSE RATE DATA FLAG=',I2,2X,'DEGREE-DAY METHOD(0=MEAN,',
07100      4 '1=EFFECTIVE MINIMUM)=',(2//)
07110      5 1X,'TEMPERATURE PROCESSING FLAG=',I2,2X,'RUNOFF BY ZONE OUTPUT',
07120      6 ' OPTION=',I2//)
07130      7 1X,'FLAG TO EXTRAPOLATE TEMPERATURES(0=EXTRAPOLATE USING',
07140      8 1X,'GIVEN LAPSE RATES, 1=AUTOMATICALLY EXTRAPOLATE)=',(2//)
07150      9 1X,'FLAG TO COMPUTE DEGREE-DAYS=',(2//)
07160      A 1X,'FLAG TO INDICATE INPUT TEMPS ARE MAX-MIN=',(2//)
07170      B 1X,'START MONTH=',I2,2X,'END MONTH=',I2//)
07180 5000  FORMAT('// NUMBER OF SNOWMELT DAYS=',I5,5X,'NUMBER OF ',
07190      1 'ELEVATION ZONES=',I5//)
07200 5500  FORMAT('//SX,'NO TEMPERATURE LAPSE RATE DATA INPUT//)
07210 6000  FORMAT('//SX,'RECESSION COEFFICIENT FACTORS'/' X FACTOR=',
07220      1 F9.6,' Y FACTOR=',F9.6// ' INITIAL RUNOFF VALUE=',F9.3,
07230      2 3X,'LAG=',I3,' HOURS')
07240 6500  FORMAT('//SX,'AREA IN EACH ELEVATION ZONE'//
07250      1 ' ZONE',5X,'AREA',1X,'('',3A4,'')')
07260 6900  FORMAT('//SX,'HYPSOMETRIC MEAN ELEVATION IN EACH ZONE',
07270      1 1X,'('',AB,'')//)
07280 7000  FORMAT(1X,I4,7X,E10.4)
07290 7400  FORMAT('//SX,'BASE STATION ELEVATION',
07300      1 1X,'('',AB,'')//)
07310 7700  FORMAT(5X,E10.4)
07320      END
07330      SUBROUTINE LAPSE(STATN,ND,NZ,MAXMIN,TEMP,TMAX,THIN,
07340      1 DTLR,UFLAG,MTHD,ZMEAN,TEXT,IDEGRY,T)
07350 C
07360 C*****
07370 C
07380 C      FUNCTION - LAPSE IS A MODULAR TEMPERATURE PRE-PROCESSING ROUTINE
07390 C      FOR INPUT TEMPERATURES EXPRESSED AS MAX-MIN OR
07400 C      TEMPERATURES NOT ALREADY IN DEGREE-DAYS OR EX-
07410 C      TRAPOLATED TO EACH ELEVATION ZONE. ROUTINE LAPSE
07420 C      TAKES MAX-MIN DAILY TEMPERATURES IN DEGREES FROM THE
07430 C      BASE STATION AND EXTRAPOLATES THE TEMPERATURE TO
07440 C      THE ZONE AND COMPUTES THE TEMPERATURE IN DEGREE-DAYS.
07450 C      DEGREE-DAYS CAN BE COMPUTED BY ONE OF TWO METHODS:
07460 C      MEAN OR EFFECTIVE MINIMUM. TEMPERATURES NOT IN
07470 C      DEGREE-DAYS OR INPUT PER ZONE CAN BE COMPUTED IN
07480 C      DEGREE-DAYS OR EXTRAPOLATED TO EACH ELEVATION
07490 C      ZONE IF LAPSE RATES ARE PROVIDED.
07500 C
07510 C      ARGUMENT LIST
07520 C      VARIABLE   TYPE   IO   DESCRIPTION
07530 C      -----
07540 C      STATN      R#8   I    ELEVATION OF RECORDING STATION
07550 C      ND         I#4   I    NUMBER OF SNOWMELT DAYS
07560 C      NZ         I#4   I    NUMBER OF ZONES
07570 C      MAXMIN     I#4   I    FLAG TO INDICATE IF TEMPS ARE MAX-MIN
07580 C      TMAX       R#4   I    MAXIMUM TEMPERATURES IN DEGREES
07590 C      THIN       R#4   I    MINIMUM TEMPERATURES IN DEGREES
07600 C      UFLAG      I#2   I    UNITS FLAG(ENGLISH OR METRIC)
07610 C      MTHD       I#2   I    METHOD OF COMPUTING DEGREE DAYS
07620 C              (EFFECTIVE MINIMUM OR MEAN)
07630 C      ZMEAN      R#8   I    'HYPSOMETRIC MEAN ELEVATION OF EACH ZONE
07640 C      TEXT       I#2   I    FLAG TO EXTRAPOLATE TO ELEVATION ZONES
07650 C      IDEGRY     I#2   I    FLAG TO COMPUTE DEGREE-DAYS
07660 C      TEMP       R#4   I    COMPUTED TEMPERATURE IN DEGREE DAYS
07670 C      T          R#4   I    TEMPERATURES IN DEGREES TO BE PROCESSED
07680 C
07690 C      EXTERNAL REFERENCES -- NONE.
07700 C
07710 C      CALLED BY -- MAIN (DRVSNO)
07720 C
07730 C      COMPUTER/LANGUAGE - IBM 360/91 AT GSFC/FORTRAN IV
07740 C
07750 C      DESIGNER/PROGRAMMER - G.MAJOR,RESEARCH & DATA SYSTEMS,INC.
07760 C
07770 C*****
07780 C

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07790 C
07800 DIMENSION ZCONST(8),TMAX(366),TMIN(366),ZMEAN(8),
07810 1 T(366,8),DTLR(366,8),TEMPT(366,8)
07820 C
07830 REAL*8 ZMEAN,STATN,ZCONST
07840 INTEGER*2 MAXMIN,MTHD,UFLAG,TEXT,IDEGRY
07850 C
07860 C
07870 IF(UFLAG.EQ.0) TU=0.
07880 IF(UFLAG.EQ.1) TU=32.
07890 C
07900 C
07910 C CHECK IF TEMPERATURE IS TO BE COMPUTED IN DEGREE-DAYS
07920 C
07930 IF(IDEGRY.EQ.0) GO TO 590
07940 C
07950 C CHECK IF TEMPERATURES ARE MAX-MIN
07960 C
07970 IF(MAXMIN.EQ.0) GO TO 52
07980 C
07990 C CHECK METHOD OF COMPUTING DEGREE DAYS
08000 C
08010 DO 600 J=1,NZ
08020 IF(MTHD.EQ.1) GO TO 22
08030 IF(MTHD.EQ.0) GO TO 23
08040 22 IF(UFLAG.EQ.0.AND.TMIN(I).LT.0.) TMIN(I)=0.0
08050 IF(UFLAG.EQ.1.AND.TMIN(I).LT.32.) TMIN(I)=32.0
08060 C
08070 C COMPUTE TEMPERATURE IN DEGREE DAYS
08080 C
08090 23 T(I,J)=((TMAX(I)+TMIN(I))/2.)-TU
08100 600 CONTINUE
08110 C
08120 GO TO 590
08130 52 CONTINUE
08140 DO 605 J=1,ND
08150 IF(MTHD.EQ.1) GO TO 53
08160 IF(MTHD.EQ.0) GO TO 54
08170 53 IF(UFLAG.EQ.0.AND.T(I,1).LT.0.) T(I,1)=0.
08180 IF(UFLAG.EQ.1.AND.T(I,1).LT.32.) T(I,1)=32.
08190 54 T(I,1)=T(I,1)-TU
08200 605 CONTINUE
08210 590 CONTINUE
08220 C
08230 C CHECK IF TEMPERATURE IS TO BE AUTOMATICALLY EXTRAPOLATED TO
08240 C ELEVATION ZONE. IF NOT, USE THE LAPSE RATES GIVEN AS INPUT
08250 C
08260 IF(TEXT.EQ.0) GO TO 950
08270 IF(UFLAG.EQ.0) ZCON=100.
08280 IF(UFLAG.EQ.1) ZCON=1000.
08290 DO 602 J=1,NZ
08300 ZCONST(J)=STATN-ZMEAN(J)
08310 DO 601 I=1,ND
08320 TEMPT(I,J)=T(I,1)+(ZCONST(J)/ZCON)*DTLR(1,1)
08330 601 CONTINUE
08340 602 CONTINUE
08350 GO TO 990
08360 950 CONTINUE
08370 C
08380 C EXTRAPOLATE TEMPERATURES USING THE GIVEN LAPSE RATES
08390 C
08400 DO 603 J=1,NZ
08410 DO 604 I=1,ND
08420 TEMPT(I,J)=T(1,1)+DTLR(I,J)
08430 604 CONTINUE
08440 603 CONTINUE
08450 C
08460 990 DO 700 I=1,ND
08470 DO 701 J=1,NZ
08480 IF(TEMPT(I,J).LE.0.) TEMPT(I,J)=0.0
08490 701 CONTINUE
08500 700 CONTINUE
08510 RETURN
08520 END
08530 C
08540 SUBROUTINE PRESNO
08550 C
08560 C*****
08570 C
08580 C FUNCTION - PRESNO COMPUTES THE PRECIPITATION CONTRIBUTING
08590 C TO RUNOFF IN EACH ELEVATION ZONE
08600 C FROM NON-SNOW COVERED AREAS OR FROM THE TOTAL
08610 C ZONE AREA. THE ALGORITHM FOR COMPUTING PRECIP
08620 C FROM NON-SNOW COVERED AREAS WAS DEVELOPED BY
08630 C RESOURCE CONSULTANTS, INC.
08640 C
08650 C COMMON BLOCK VARIABLES USED-
08660 C VARIABLE COMMON TYPE IO
08670 C -----
08680 C T CLIDAT R*4 I

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08690 C      S      CLIDAT R*4 I
08700 C      PRECIP CLIDAT R*4 I
08710 C      AN      BASDAT R*4 J
08720 C      P      OUTDAT R*4 O
08730 C      UFLAG  OPTDAT I*2 I
08740 C      IPR     BASDAT I*2 I
08750 C
08760 C      EXTERNAL REFERENCES - NONE
08770 C
08780 C      CALLED BY - MAIN
08790 C
08800 C      COMPUTER/LANGUAGE -- IBM 360/91 AT GSFC/FORTRAN IV
08810 C
08820 C      DESIGNER/PROGRAMMER -- G.MAJOR, RESEARCH & DATA SYSTEMS, INC.
08830 C
08840 C*****
08850 C
08860 C
08870 C      DIMENSION RUNOFF(366,B),THAX(366),THIN(366)
08880 C      REAL*8 BASIN,AREA,X,Y,SNOW,R,TZ,EP
08890 C      INTEGER*2 IKUN,MODE,IPRKUN,IPLT,IPRINT,UFLAG,ACTFLG,IZONE,
08900 C      1 IDIFLG,MTHD,IIPROC,IPR
08910 C
08920 C
08930 C
08940 C***** COMMON BLOCKS *****
08950 C
08960 C      COMMON/CLIDAT/T(366,B),S(366,B),PRECIP(366,B),ACTUAL(366),
08970 C      1 TCRT(366),ND
08980 C
08990 C      COMMON/OUTDAT/P(366,B),QNP1X(367),X1(367),TEMPT(366,B)
09000 C
09010 C      COMMON/OPTDAT/ISTKTH,IENMTH,IKUN,MODE,IPRKUN,IPLT,IPRINT,UFLAG,
09020 C      1 ACTFLG,IZONE(3),IDIFLG,MTHD,IIPROC
09030 C
09040 C      COMMON/BASDAT/BASIN(2),AREA(B),X,Y,BTLR(366,B),AN(366,B),
09050 C      1 CS(366,B),CR(366),NZ,IYEAR,IPR(366,B)
09060 C
09070 C
09080 C      ZERO OUT PRECIPITATION ARRAY FOR EACH RUN
09090 C
09100 C      DO 15 J=1,ND
09110 C          DO 16 I=1,NZ
09120 C              P(J,I)=0.0
09130 C      16 CONTINUE
09140 C      15 CONTINUE
09150 C
09160 C      DO 80 J=1,NZ
09170 C
09180 C      CHECK IF PRECIP INPUT IS BY ZONE
09190 C
09200 C      IF(IZONE(2).EQ.0) NPZ=1
09210 C      IF(IZONE(2).EQ.1) NPZ=J
09220 C
09230 C      INITIALIZE ACCUMULATED SNOW TO 0
09240 C
09250 C      SNOW=0.00
09260 C
09270 C      INITIALIZE NON-SNOW COVERED (SNOW0) AND TOTAL SIA (SNOW1)
09280 C      TO 0
09290 C
09300 C      DO 90 J=1,ND
09310 C          SNOW0=0.0
09320 C          SNOW1=0.0
09330 C          IF(IIPROC.EQ.0) TZ=T(I,J)
09340 C          IF(IIPROC.EQ.1) TZ=TEMPT(I,J)
09350 C
09360 C      CHECK WHICH PRECIP METHOD TO USE; IPR=0 IS FOR
09370 C      NON-SNOW COVERED AREAS AND IPR=1 IS FOR TOTAL AREA
09380 C
09390 C      IF(IPR(J,J).EQ.0) SNOW0=S(I,J)
09400 C      IF(IPR(I,J).EQ.1) SNOW1=S(I,J)
09410 C
09420 C      COMPUTE RUNOFF FACTOR
09430 C
09440 C      R=TZ*AN(I,J)
09450 C
09460 C      CHECK IF ANY PRECIPITATION IN ZONE
09470 C      IF NO PRECIPITATION THEN CHECK SNOW TO BE MELTED
09480 C
09490 C      IF(ABS(PRECIP(J,NPZ)).LT.0.00001) GO TO 12
09500 C
09510 C      CHECK FOR SNOWFALL IN ZONE
09520 C      IF TEMPERATURE IS LESS THAN INPUT CRITICAL TEMPERATURE
09530 C      THEN TREAT PRECIPITATION AS SNOWFALL
09540 C
09550 C      IF(TZ.GT.TCRT(I)) GO TO 11
09560 C
09570 C      ACCUMULATE SNOWFALL IN ZONE TO BE MELTED LATER
09580 C
09590 C      SNOW=SNOW+PRECIP(I,NPZ)

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09600 C
09610 C SET COMPUTED PRECIP TO 0 AND CALCULATE PRECIP FOR
09620 C RUNOFF FROM NON-SCA
09630 C
09640 C P(I,J)=0.0
09650 C GO TO 90
09660 C
09670 C ASSIGN INPUT PRECIP TO COMPUTED PRECIP
09680 C
09690 C 11 P(I,J)=PRECIP(1,NPZ)
09700 C
09710 C
09720 C CHECK PRECIPITATION IN ZONE TO BE MELTED
09730 C
09740 C 12 IF(DABS(SNOW).LT.0.0000100) GO TO 90
09750 C
09760 C CHECK TEMPERATURE IN ZONE,CALCULATE RUNOFF FROM PRECIP
09770 C HELD AND COMPUTE AMOUNT OF SNOW TO BE MELTED
09780 C
09790 C IF(TZ.LT.0.00) GO TO 90
09800 C EP=R*(1.-SNOW1)
09810 C IF(R.GT.SNOW) GO TO 13
09820 C P(I,J)=P(I,J)+EP
09830 C
09840 C SET ACCUMULATED SNOW TO SNOW MINUS RUNOFF
09850 C
09860 C SNOW=SNOW-R
09870 C GO TO 90
09880 C
09890 C CALCULATE EXTRA RUNOFF FROM PRECIP HELD
09900 C COMPUTE PRECIPITATION FROM SNOW ACCUMULATED AND TOTAL SCA
09910 C AND RESET ACCUMULATED SNOW TO 0
09920 C
09930 C 13 P(I,J)=P(I,J)+(SNOW*(1.-SNOW1))
09940 C SNOW=0.0
09950 C
09960 C COMPUTE PRECIPITATION FROM AMOUNT OF SNOW COVER
09970 C
09980 C 90 P(I,J)=P(I,J)*(1.-SNOW0)
09990 C 80 CONTINUE
10000 C
10010 C 999 RETURN
10020 C END
10030 C SUBROUTINE RUNOFF
10040 C
10050 C*****
10060 C
10070 C FUNCTION - THIS ROUTINE COMPUTES THE PREDICTED STREAM RUNOFF
10080 C BASED ON THE SNOWMELT-RUNOFF MODEL EQUATIONS BY
10090 C RANGO AND MARTINEC. RUNOFF CAN BE COMPUTED IN FORCAST
10100 C MODE BY UPDATING WITH ACTUAL DATA EVERY 7TH DAY.
10110 C
10120 C
10130 C COMMON BLOCK VARIABLES USED
10140 C


| VARIABLE | COMMON | TYPE  | IO  |
|----------|--------|-------|-----|
| -----    | -----  | ----- | --- |
| T        | CLIDAT | R*4   | I   |
| S        | CLIDAT | R*4   | I   |
| P        | OUTDAT | R*4   | I   |
| QNF1X    | OUTDAT | R*4   | 0   |
| DTLR     | BASDAT | R*4   | I   |
| AN       | BASDAT | R*4   | I   |
| X1       | OUTDAT | R*4   | 0   |
| AREA     | BASDAT | R*8   | I   |
| X        | BASDAT | R*8   | I   |
| Y        | BASDAT | R*8   | I   |
| ND       | CLIDAT | I*4   | I   |
| NZ       | BASDAT | I*4   | I   |
| CS       | BASDAT | R*4   | I   |
| CR       | BASDAT | R*4   | I   |
| UFLAG    | OPTDAT | I*2   | I   |
| ACTUAL   | CLIDAT | R*4   | I   |
| IZONE    | OPTDAT | I*2   | I   |
| MODE     | OPTDAT | I*4   | I   |
| PDR      | GAGE   | R*4   | I   |
| PDM2     | GAGE   | R*4   | I   |
| UNS      | GAGE   | R*8   | I   |


10150 C
10160 C
10170 C
10180 C
10190 C
10200 C
10210 C
10220 C
10230 C
10240 C
10250 C
10260 C
10270 C
10280 C
10290 C
10300 C
10310 C
10320 C
10330 C
10340 C
10350 C
10360 C
10370 C
10380 C
10390 C
10400 C
10410 C
10420 C
10430 C
10440 C
10450 C
10460 C
10470 C
10480 C
10490 C
EXTERNAL REFERENCES --
IOUT - UTILITY ROUTINE TO OUTPUT RESULTS IN MONTHLY AND
DAILY FORMAT.
CALLED BY -- MAIN
COMPUTER/LANGUAGE-- IBM 360/91 AT GSFC/FORTRAN IV
DESIGNER/PROGRAMMER -- G.HAJUR, RESEARCH & DATA SYSTEMS, INC.

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10500 C
10510 C*****
10520 DIMENSION Z(8),RUNOF(366,8)
10530 C
10540 REAL*8 ARG,QNS,ASUM,COV,PRUNOF(367),BASIN,AREA,X,Y,SUMRO
10550 INTEGER*2 IRUN,MODE,IPRRUN,IPLT,(PRINT,UFLAG,ACTFLG,IZONE,
10560 1 IDTFLG,HTHD,ITPROC,IPR,IOFLG,ROFLG,COFLG,DTFLG,IOFLG
10570 INTEGER*2 POFLG
10580 C
10590 C
10600 C****COMMON BLOCKS****
10610 C
10620 COMMON/CLIDAT/T(366,8),S(366,8),PRECIP(366,8),ACTUAL(366),
10630 1 TCRIT(366),ND
10640 C
10650 COMMON/OUTDAT/P(366,8),RNP1X(367),X1(367),TEMPT(366,8)
10660 C
10670 COMMON/OPTDAT/ISTH, IENH,IRUN,MODE,IPRRUN,IPLT,IPRINT,UFLAG,
10680 1 ACTFLG,IZONE(3),IDTFLG,HTHD,ITPROC
10690 C
10700 COMMON/BASDAT/BASIN(2),AREA(8),X,Y,DIIR(366,8),AN(366,8),
10710 1 CS(366,8),CR(366),NZ,IYEAR,IPR(366,8)
10720 C
10730 COMMON/GAGE/QNS,PDR(367),PDM2(367)
10740 C
10750 C
10760 C ZERO OUT RUNOFF ARRAY FOR EACH RUN
10770 C
10780 DO 10 I1=1,367
10790 GNP1X(I1)=0.0
10800 X1(I1)=0.0
10810 PRUNOF(I1)=0.0
10820 10 CONTINUE
10830 C
10840 C INITIALIZE RUNOFF AND CHECK UNITS FLAG
10850 C
10860 IF(UFLAG.EQ.0) COV=0.0100/86400.00
10870 IF(UFLAG.EQ.1) COV=0.083300/86400.00
10880 C
10890 C
10900 C COMBINE SNOW COVER AND PRECIPITATION DATA AND ACCUMULATE
10910 C FOR EACH ZONE.
10920 C
10930 C NDAY=0
10940 C
10950 C CHECK FORECAST MODE
10960 C
10970 IF(MODE.EQ.1) NDAY=7
10980 DO 3 I=1,ND
10990 ASUM=0.00
11000 DO 2 J=1,NZ
11010 C
11020 C CHECK IF TEMPERATURE AND RUNOFF COEFFICIENTS ARE INPUT
11030 C BY ZONES.
11040 C
11050 IF(IZONE(3).EQ.0) NCZ=1
11060 IF(IZONE(3).EQ.1) NCZ=J
11070 C
11080 IF(ITPROC.EQ.0) Z(J)=T(1,J)
11090 IF(ITPROC.EQ.1) Z(J)=TEMPT(I,J)
11100 IF(Z(J).LT.0.00) Z(J)=0.00
11110 C
11120 C COMPUTE SNOWMELT DEPTH IN EACH ZONE
11130 C
11140 RUNOF(I,J)=AN(I,J)*Z(J)*S(I,J)+P(1,J)
11150 C
11160 C CHECK RUNOFF COEFFICIENTS FOR RAIN OR SNOW (CR OR CS)
11170 C
11180 IF(CR(I).EQ.0.0) CR1=CS(I,NCZ)
11190 IF(CR(I).GT.0.0) CR1=CR(I)
11200 C
11210 C COMPUTE SNOWMELT RUNOFF
11220 C
11230 SUMRO=(CS(I,NCZ)*AN(I,J)*Z(J)*S(I,J)+CR1*P(I,J))*(AREA(J)*COV)
11240 ASUM=ASUM+SUMRO
11250 2 CONTINUE
11260 C
11270 C COMPUTE RECESSION COEFFICIENT FOR BASIN
11280 C
11290 ARG=1.00-(X*QNS**Y)
11300 IF(I.EQ.1) PRUNOF(I)=QNS
11310 C
11320 C CHECK FOR STREAMFLOW LAG
11330 C CHECK IF STREAMFLOW LAG IS FROM PREVIOUS(DAY N-1) RUNOFF
11340 C OR FROM DAY N-2 RUNOFF
11350 C
11360 IF(PDR(I).EQ.0.) PRUNOF(I)=PDM2(I)*PRUNOF(I-1)+(1.-PDM2(I))*
11370 1 PRUNOF(I)
11380 C
11390 IF(PDR(I).EQ.0.) PDR1=1.0

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11400      IF(PDR(I).GT.0.) PDR1=PDR(I)
11410 C
11420 C
11430 C      COMPUTE STREAMFLOW
11440 C
11450      QNP1X(I)=(PDR1*PRUNDF(I)+(1.-PDR1)*ASUM)*ARG+(X*QNS*(1.D0+Y))
11460      PRUNDF(I+1)=ASUM
11470 C
11480 C      IF IN FORECAST MODE SUBSTITUTE THE RUNOFF VALUE FOR THE
11490 C      NEXT DAY WITH THE ACTUAL RUNOFF VALUE EVERY SEVENTH DAY
11500 C
11510      IF(NDAY.EQ.J) GO TO 850
11520      UNS=QNP1X(I)
11530      GO TO 900
11540 850      IF(NDAY.GT.ND) NDAY=ND
11550      QNS=ACTUAL(NDAY)
11560      NDAY=NDAY+7
11570 900      CONTINUE
11580 C
11590      X1(I)=I
11600 3      CONTINUE
11610 C
11620      X1(ND+1)=X1(ND)+1.
11630 C
11640 C      WRITE PREDICTED STREAMFLOW FOR EACH ZONE
11650 C
11660      IF(IPRRUN.EQ.0) GO TO 100
11670 C
11680      IOFLG=0
11690      ROFLG=0
11700      COFLG=0
11710      DTFLG=0
11720      TOFLG=0
11730      POFLG=1
11740      CALL IOUT(NZ,BASIN,IYEAR,IZONE,1STMTH,IENMTH,T,PRECIP,S,IPK,
11750 1 RUNDF,QNP1X,ACTUAL,CS,AN,DTLR,UFLAG,IOFLG,ROFLG,COFLG,DTFLG,
11760 2 THAX,THIN,TCRIT,CR,P,TOFLG,POFLG)
11770 100      CONTINUE
11780 C
11790 C      WRITE COMPUTED AND ACTUAL SNOWMELT RUNOFF
11800 C
11810 C
11820      IOFLG=0
11830      ROFLG=1
11840      COFLG=0
11850      PRTFLG=0
11860      TOFLG=0
11870      POFLG=0
11880      CALL IOUT(NZ,BASIN,IYEAR,IZONE,1STMTH,IENMTH,T,PRECIP,S,IPR,
11890 1 RUNDF,QNP1X,ACTUAL,CS,AN,DTLR,UFLAG,IOFLG,ROFLG,COFLG,PRTFLG,
11900 2 THAX,THIN,TCRIT,CR,P,TOFLG,POFLG)
11910 C
11920 C
11930 C
11940 999      RETURN
11950      END
11960 C
11970 C
11980 C
11990 C
12000      SUBROUTINE GOOD(QNP1X,ACTUAL,ND)
12010 C
12020 C*****
12030 C
12040 C      FUNCTION - GOOD COMPUTES THE NASH-SUTCLIFFE GOODNESS OF FIT
12050 C      MEASURE AND CALCULATES THE TOTAL SIMULATED AND
12060 C      ACTUAL VOLUME AND THE PER CENT SEASONAL DIFFERENCE
12070 C      BETWEEN THE ACTUAL AND SIMULATED STREAM RUNOFF.
12080 C
12090 C
12100 C      ARGUMENT LIST -
12110 C      VARIABLE      TYPE  IO  DESCRIPTION
12120 C      -----      -
12130 C      QNP1X          R*4  I   ARRAY OF SIMULATED STREAM RUNOFF DATA
12140 C      ACTUAL         R*4  I   ARRAY OF ACTUAL STREAM RUNOFF DATA
12150 C      ND             I*4  I   NUMBER OF SNOWMELT DAYS
12160 C
12170 C      OUTPUTS:
12180 C      XNSR2 - NASH-SUTCLIFFE GOODNESS OF FIT MEASURE
12190 C      VOL   - TOTAL VOLUME OF COMPUTED STREAM RUNOFF
12200 C      ASUM  - TOTAL VOLUME OF ACTUAL STREAM RUNOFF
12210 C      PCT   - PER CENT SEASONAL DIFFERENCE BETWEEN ACTUAL
12220 C            AND SIMULATED STREAM RUNOFF
12230 C      AMEAN - MEAN ACTUAL STREAM RUNOFF
12240 C      QMEAN - MEAN COMPUTED STREAM RUNOFF
12250 C
12260 C
12270 C
12280 C      EXTERNAL REFERENCES -- NONE.
12290 C

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12300 C      CALLED BY -- MAIN.
12310 C
12320 C      COMPUTER/LANGUAGE - IBM 360/91 AT GSFC/FORTRAN IV
12330 C
12340 C      DESIGNER/PROGRAMMER -- G. MAJUR, RESEARCH & DATA SYSTEMS, INC.
12350 C
12360 C*****
12370 C
12380 C      DIMENSION QNP1X(367),ACTUAL(366)
12390 C
12400 C
12410 C      COMPUTE MEAN AND TOTAL ACTUAL STREAMFLOW
12420 C
12430 C      ASUM=0.0
12440 C      DO 10 I=1,ND
12450 C          ASUM=ASUM+ACTUAL(I)
12460 10 CONTINUE
12470 C      DAYS=ND
12480 C      AMEAN=ASUM/DAYS
12490 C      WRITE(6,5000) ASUM,AMEAN
12500 C
12510 C      CALCULATE TOTAL VOLUME
12520 C
12530 C      VOL=0.0
12540 C      DO 50 I=1,ND
12550 C          VOL=VOL+QNP1X(I)
12560 50 CONTINUE
12570 C
12580 C      QMEAN=VOL/DAYS
12590 C      WRITE(6,6000) VOL,QMEAN
12600 C
12610 C      CALCULATE NASH-SUTCLIFFE GOODNESS OF FIT MEASURE
12620 C
12630 C      E=0.0
12640 C      F=0.0
12650 C      ONEN=1./DAYS
12660 C      DO 30 I=1,ND
12670 C          E=E+(ACTUAL(I)-AMEAN)**2
12680 C          F=F+(ACTUAL(I)-QNP1X(I))**2
12690 30 CONTINUE
12700 C      XNSR2=(ONEN*E-ONEN*F)/(ONEN*E)
12710 C
12720 C      WRITE(6,5500) XNSR2
12730 C
12740 C      COMPUTE SEASONAL DIFFERENCE
12750 C
12760 C      PCT=((ASUM-VOL)/ASUM)*100.
12770 C
12780 C      WRITE(6,6500) PCT
12790 C
12800 6000 FORMAT(' TOTAL COMPUTED VOLUME= ',F15.4,/,
12810 1 ' MEAN COMPUTED VOLUME= ',F15.4//)
12820 5500 FORMAT(' GOODNESS OF FIT MEASURE=',F15.4//)
12830 5000 FORMAT(' TOTAL ACTUAL STREAMFLOW=',F15.4,/,
12840 1 ' MEAN ACTUAL STREAMFLOW= ',F15.4//)
12850 6500 FORMAT(' PERCENT SEASONAL DIFFERENCE=',F15.4//)
12860 C      RETURN
12870 C      END
12880 C      SURROUTINE IQOUT(NZ,BASIN,IYEAR,IZONE,ISTMTH,IENMTH,Y,PRECIP,S,
12890 1 IPR,RUNOF,QNP1X,ACTUAL,CS,AN,DTLR,UFLAG,IOFLG,ROFLG,COFLG,
12900 2 DTFLG,TMAX,TMIN,TCRJT,CR,P,TOFLG,POFLG)
12910 C
12920 C-----
12930 C
12940 C      FUNCTION - IQOUT IS A UTILITY ROUTINE TO PRINT OUT MONTHLY
12950 C      AND DAILY VALUES IN TABULAR FORM FOR VARIOUS
12960 C      SNOWMELT RUNOFF MODEL PARAMETERS.
12970 C
12980 C
12990 C      ARGUMENT LIST --
13000 C      VARIABLE  TYPE  IO  DESCRIPTION
13010 C      -----  ---  --  -----
13020 C      NZ        I*4  IO  NUMBER OF ZONES IN BASIN
13030 C      BASIN     R*8  IO  BASIN NAME
13040 C      IYEAR     I*4  IO  MODEL YEAR
13050 C      IZONE     I*2  I   FLAG FOR CHECKING IF INPUT IS BY ZONE
13060 C      ISTMTH    I*4  I   START MONTH
13070 C      IENMTH    I*4  I   END MONTH
13080 C      T         R*4  IO  TEMPERATURE DATA
13090 C      PRECIP    R*4  IO  PRECIPITATION DATA
13100 C      S         R*4  IO  SNOW COVERED AREA
13110 C      IPR       I*4  IO  PRECIPITATION METHOD
13120 C      RUNOF     R*4  IO  DEPTH BY ZONE
13130 C      QNP1X     R*4  IO  DAILY STREAM RUNOFF
13140 C      ACTUAL    R*4  IO  ACTUAL STREAM RUNOFF
13150 C      CS        R*4  IO  RUNOFF COEFFICIENTS FOR SNOW
13160 C      AN        R*4  IO  DEGREE DAY FACTORS
13170 C      DTLR      R*4  IO  TEMPERATURE LAISE RATE CORRECTION
13180 C      TMAX     R*4  IO  MAXIMUM TEMPERATURES
13190 C      TMIN     R*4  IO  MINIMUM TEMPERATURES

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13200 C      TCRIT      R*4      IO      CRITICAL TEMPERATURE
13210 C      CR          R*4      IO      RUNOFF COEFFICIENTS FOR RAIN
13220 C      P           R*4      IO      PRECIPITATION CONTRIBUTING TO RUNOFF
13230 C      UFLAG      I*2      I      UNITS FLAG
13240 C      IOFLG      I*2      I      FLAG IF TEMPERATURE,PRECIPITATION AND SNOW
13250 C      COVERED AREA IS TO BE OUTPUT
13260 C      ROFLG      I*2      I      FLAG IF DAILY AND ACTUAL STREAM RUNOFF IS TO
13270 C      OUTPUT
13280 C      COFLG      I*2      I      FLAG IF RUNOFF COEFFICIENTS,DEGREE DAY
13290 C      FACTORS AND PRECIPITATION METHOD INDEX
13300 C      ARE TO BE OUTPUT
13310 C      DTFLG      I*2      J      FLAG IF LAPSE RATE AND CRITICAL
13320 C      TEMPERATURE IS TO BE OUTPUT
13330 C      TOFLG      I*2      I      FLAG IF MAX-MIN,CRTITICAL TEMPS ARE TO
13340 C      BE OUTPUT
13350 C      POFLG      I*2      I      FLAG IF DEPTH BY ZONE AND COMPUTED
13360 C      PRECIPITATION CONTRIBUTING TO RUNOFF
13370 C      ARE TO BE OUTPUT
13380 C
13390 C      EXTERNAL REFERENCES - NONE.
13400 C
13410 C      CALLED FROM:
13420 C          SNOBRV
13430 C          READIN
13440 C          RUNOFF
13450 C          PRESNO
13460 C
13470 C      LANGUAGE/COMPUTER - FORTRAN IV/IBM 360/91 AT 05FC
13480 C
13490 C      PROGRAMMER/DESIGNER - G. MAJOR, RESEARCH & DATA SYSTEMS,INC.
13500 C
13510 C
13520 C -----
13530 C
13540 C      REAL*8 BASIN(2),CMP,ACT,TX,TN
13550 C      INTEGER*2 IZONE(3),UFLAG,IOFLG,ROFLG,COFLG,DTFLG,IPR(366,8),
13560 C      1      TOFLG,POFLG
13570 C
13580 C      DIMENSION NDAYS(24),MO(24),ARENAM(8),AO(12),BO(12),CO(12),
13590 C      1      T(366,8),PRECIP(366,8),S(366,8),RUNOF(366,8),QNP1X(367),
13600 C      2      ACTUAL(366),CS(366,8),AN(366,8),DTLR(366,8),INO(12),JP(12)
13610 C      DIMENSION C1(12),AA(12),DT(12),PRE(12),T1(12),P1(12),SN(12)
13620 C      DIMENSION CMP(12),ACT(12),TX(12),TN(12),TC(12),CR1(12),P2(12)
13630 C      DIMENSION P(366,8),THAX(366),THIN(366),TCRIT(366),CR(366)
13640 C
13650 C      DATA NDAYS/31,29,31,30,31,30,31,30,31,31,30,31,30,31,12*0/
13660 C      DATA ARENAM/'A','B','C','D','E','F','G','H'/
13670 C      DATA MO(1)/4HJAN /
13680 C      DATA MO(2)/4HFEB /
13690 C      DATA MO(3)/4HMAR /
13700 C      DATA MO(4)/4HAPR /
13710 C      DATA MO(5)/4HMAY /
13720 C      DATA MO(6)/4HJUN /
13730 C      DATA MO(7)/4HJUL /
13740 C      DATA MO(8)/4HAUG /
13750 C      DATA MO(9)/4HSEP /
13760 C      DATA MO(10)/4HOCT /
13770 C      DATA MO(11)/4HNOV /
13780 C      DATA MO(12)/4HDEC /
13790 C      DATA C1/12*'CS' //
13800 C      DATA AA/12*'AN' //
13810 C      DATA TX/12*'MAX TEMP'//
13820 C      DATA TN/12*'MIN TEMP'//
13830 C      DATA TC/12*'TCR1'//
13840 C      DATA CR1/12*'CR' //
13850 C      DATA DT/12*'DTLR'//
13860 C      DATA PRE/12*'PR' //
13870 C      DATA T1/12*'DD' //
13880 C      DATA P1/12*'PREC'//
13890 C      DATA SN/12*'SCA' //
13900 C      DATA CMP/12*'COMPUTED'//
13910 C      DATA ACT/12*'ACTUAL' //
13920 C      DATA P2/12*'CPRE'//
13930 C      DATA DP/12*'DPTH'//
13940 C
13950 C      DO 60 I=1,12
13960 C          J=I+12
13970 C          MO(J)=MO(I)
13980 C          NDAYS(J)=NDAYS(I)
13990 C          AO(I)=0.0
14000 C          BO(I)=0.0
14010 C          CO(I)=0.0
14020 C      60 CONTINUE
14030 C
14040 C      COMPUTE NUMBER OF MONTHS AND CHECK IF GREATER THAN 6
14050 C
14060 C      IBATZ=0
14070 C      NMONTH=(IENMTH-ISTMTH)+1
14080 C      NM1=NMONTH
14090 C      IF(NMONTH.GT.6) GO TO 20

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14100      GO TO 30
14110      20  IDATZ=1
14120      IEND=ISTMTH+5
14130      30  CONTINUE
14140      C
14150      C      CHECK IF MORE THAN 1 YEAR IS BEING MODELLED
14160      C
14170      IF(IENMTH.LE.12) IY=IYEAR
14180      IF(IENMTH.GT.12) IY=IYEAR+1
14190      C
14200      C      LOOP OVER NUMBER OF ZONES
14210      C
14220      DO 50 J=1,NZ
14230      IFLAG=0
14240      IF(IDATZ.EQ.0) IEND=1ENMTH
14250      WRITE(6,9999)
14260      C
14270      C      CHECK IF POFLG FOR COMPUTED PRECIP OUTPUT
14280      C
14290      IF(POFLG.EQ.0) GO TO 105
14300      WRITE(6,1201)
14310      WRITE(6,1000) BASIN,IYEAR,ARENAM(J),(MO(M1),M1=ISTMTH,IEND)
14320      IF(NMONTH.GT.6) NM1=6
14330      WRITE(6,1009) (DP(IN),P2(IN),IN=1,NM1)
14340      GO TO 300
14350      105  CONTINUE
14360      C
14370      C      CHECK COFLG FOR OUTPUT PARAMETERS
14380      C
14390      IF(COFLG.EQ.0) GO TO 100
14400      J1=J
14410      C
14420      C      CHECK IF INPUT IS BY ZONE AND WRITE OUT HEADER INFORMATION FOR
14430      C      RUNOFF COEFFICIENTS(CS),DEGREE DAY FACTORS(DN) AND TEMPERATURE
14440      C      LAPSE RATES(DTLR)
14450      C
14460      IF(IZONE(3).EQ.0) J1=1
14470      WRITE(6,1001)
14480      WRITE(6,1000) BASIN,IYEAR,ARENAM(J),(MO(M1),M1=ISTMTH,IEND)
14490      IF(NMONTH.GT.6) NM1=6
14500      WRITE(6,1010) (AA(IN),C1(IN),CR1(IN),PRE(IN),IN=1,NM1)
14510      GO TO 300
14520      100  CONTINUE
14530      C
14540      C      CHECK DTFLG FOR OUTPUT PARAMETERS
14550      C
14560      IF(DTFLG.EQ.0) GO TO 101
14570      WRITE(6,2001)
14580      WRITE(6,1000) BASIN,IYEAR,ARENAM(J),(MO(M1),M1=ISTMTH,IEND)
14590      IF(NMONTH.GT.6) NM1=6
14600      WRITE(6,1011) (DT(IN),TC(IN),IN=1,NM1)
14610      GO TO 300
14620      101  CONTINUE
14630      C
14640      C      CHECK IOFLG FOR OUTPUT PARAMETERS
14650      C
14660      IF(IOFLG.EQ.0) GO TO 110
14670      J2=J
14680      C
14690      C      CHECK IF INPUT BY ZONE
14700      C
14710      IF(IZONE(2).EQ.0) J2=1
14720      C
14730      C      WRITE HEADER INFORMATION FOR TEMPERATURE(T),PRECIPITATION
14740      C      (PRECIP),AND SNOW COVERED AREA(S).
14750      C
14760      WRITE(6,1501)
14770      WRITE(6,1000) BASIN,IYEAR,ARENAM(J),(MO(M1),M1=ISTMTH,IEND)
14780      IF(NMONTH.GT.6) NM1=6
14790      WRITE(6,1510) (T1(IN),P1(IN),SN(IN),IN=1,NM1)
14800      GO TO 300
14810      110  CONTINUE
14820      C
14830      C      CHECK ROFLG FOR OUTPUT PARAMETERS
14840      C
14850      IF(ROFLG.EQ.1) GO TO 130
14860      IF(TOFLG.EQ.1) GO TO 131
14870      GO TO 300
14880      C
14890      C      WRITE HEADER INFORMATION FOR SIMULATED RUNOFF (UNPIX) AND ACTUAL
14900      C      (ACTUAL) DATA
14910      C
14920      130  WRITE(6,2002)
14930      WRITE(6,3000) BASIN,IYEAR,(MO(M1),M1=ISTMTH,IEND)
14940      IF(NMONTH.GT.6) NM1=6
14950      WRITE(6,3010) (CHP(IN),ACT(IN),IN=1,NM1)
14960      GO TO 300
14970      C
14980      C      CHECK TOFLG AND OUTPUT MAX-MIN HEADER INFORMATION
14990      C

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15000 131 WRITE(6,3001)
15010 WRITE(6,3000) BASIN,IYEAR,(MO(M1),M1=1STMTH,1END)
15020 IF(NMONTH.GT.6) NM1=6
15030 WRITE(6,3020) (TX(IN),TN(1N),IN=1,NM1)
15040 300 CONTINUE
15050 C
15060 C CHECK FLAGS FOR WRITING DATA IF OVER 6 MONTHS DATA AVAILABLE
15070 C
15080 C
15090 C LOOP FOR NUMBER OF DAYS IN MONTH
15100 C
15110 5 DO 10 ID=1,31
15120 IWICH=ID
15130 IS=1STMTH
15140 DO 15 IM=1,NMONTH
15150 C
15160 C
15170 C CHECK POFLG FOR OUTPUT DATA AND BLANK OUT DAYS WHERE
15180 C NO DATA IS AVAILABLE
15190 C
15200 IF(POFLG.EQ.0) GO TO 155
15210 AD(IM)=RUNOF(IWICH,J)
15220 BO(IM)=P(IWICH,J)
15230 IF(MOD(IY,4).EQ.0) GO TO 81
15240 IF(IS.EQ.2.OR.IS.EQ.14.AND.ID.GE.29) GO TO 156
15250 81 IF(ID.GT.NDAYS(IS)) GO TO 156
15260 GO TO 180
15270 156 AD(IM)=999999.
15280 BO(IM)=999999.
15290 GO TO 180
15300 155 CONTINUE
15310 C
15320 C CHECK COFLG FOR OUTPUT DATA AND BLANK OUT DAYS WHERE DATA IS
15330 C NOT AVAILABLE
15340 C
15350 IF(COFLG.EQ.0) GO TO 160
15360 AD(IM)=AN(IWICH,J)
15370 BO(IM)=CS(IWICH,11)
15380 CO(IM)=CR(IWICH)
15390 IDO(IM)=IPR(IWICH,J)
15400 IF(MOD(IY,4).EQ.0) GO TO 82
15410 IF(IS.EQ.2.OR.IS.EQ.14.AND.ID.GE.29) GO TO 151
15420 82 IF(ID.GT.NDAYS(IS)) GO TO 151
15430 GO TO 180
15440 151 AD(IM)=999999.
15450 BO(IM)=999999.
15460 CO(IM)=999999.
15470 IDO(IM)=999
15480 GO TO 180
15490 160 CONTINUE
15500 C
15510 C CHECK DTFLG FOR OUPUT AND BLANK OUT DAYS WHERE NO DATA
15520 C IS AVAILABLE
15530 IF(DTFLG.EQ.0) GO TO 161
15540 AD(IM)=DTLR(IWICH,J)
15550 BO(IM)=TCRIT(IWICH)
15560 IF(MOD(IY,4).EQ.0) GO TO 162
15570 IF(IS.EQ.2.OR.IS.EQ.14.AND.ID.GE.29) GO TO 163
15580 162 IF(ID.GT.NDAYS(IS)) GO TO 163
15590 GO TO 180
15600 163 AD(IM)=999999.
15610 BO(IM)=999999.
15620 GO TO 180
15630 161 CONTINUE
15640 C
15650 C CHECK IOFLG FOR OUTPUT DATA AND BLANK OUT DAYS WHERE NO DATA
15660 C IS AVAILABLE
15670 C
15680 IF(IOFLG.EQ.0) GO TO 170
15690 AD(IM)=I(IWICH,J)
15700 BO(IM)=PRECIP(IWICH,J2)
15710 CO(IM)=S(IWICH,J)
15720 IF(MOD(IY,4).EQ.0) GO TO 83
15730 IF(IS.EQ.2.OR.IS.EQ.14.AND.ID.GE.29) GO TO 171
15740 83 IF(ID.GT.NDAYS(IS)) GO TO 171
15750 GO TO 180
15760 171 AD(IM)=999999.
15770 BO(IM)=999999.
15780 CO(IM)=999999.
15790 GO TO 180
15800 170 CONTINUE
15810 C
15820 C CHECK ROFLG FOR OUTPUT DATA AND BLANK OUT DAYS WHERE DATA IS
15830 C NOT AVAILABLE
15840 C
15850 IF(ROFLG.EQ.0) GO TO 182
15860 AD(IM)=QNP1X(IWICH)
15870 BO(IM)=ACTUAL(IWICH)
15880 IF(MOD(IY,4).EQ.0) GO TO 84
15890 IF(IS.EQ.2.OR.IS.EQ.14.AND.ID.GE.29) GO TO 181

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15900 84      (F(ID.GT.NDAYS(IS)) GO TO 181
15910      GO TO 180
15920 181     AD(IH)=9999999.
15930      RO(IH)=9999999.
15940      GO TO 180
15950 C
15960 C      CHECK TOFLG FOR OUTPUT DATA AND BLANK OUT DAYS WHERE
15970 C      NO DATA IS AVAILABLE
15980 C
15990 182     IF(TOFLG.EQ.0) GO TO 180
16000      AD(IH)=TMAX(IWICH)
16010      RO(IH)=THIN(IWICH)
16020      IF(MOD(IY,4).EQ.0) GO TO 85
16030      IF(IS.EQ.2.OR.IS.EQ.14.AND.ID.GE.29) GO TO 183
16040 85      IF(ID.GT.NDAYS(IS)) GO TO 183
16050      GO TO 180
16060 183     AD(IH)=9999999.
16070      RO(IH)=9999999.
16080 180     CONTINUE
16090 C
16100      IF(MOD(IY,4).EQ.0) GO TO 70
16110      IF(IS.EQ.2.OR.IS.EQ.14) GO TO 71
16120      GO TO 70
16130 71     NDY=NDAYS(IS)-1
16140      GO TO 72
16150 70     NDY=NDAYS(IS)
16160 C
16170 72     IWICH=IWICH+NDY
16180      IS=IS+1
16190 15     CONTINUE
16200 C
16210      IF(IDATZ.EQ.0) KEND=NMNTH
16220      IF(IDATZ.EQ.1) KEND=6
16230 C
16240 C      CHECK POFLG AND OUTPUT DATA
16250 C
16260      IF(POFLG.EQ.0) GO TO 199
16270      IF(IFLAG.EQ.0) WRITE(6,9009) ID,(AO(K),RO(K),K=1,KEND)
16280      IF(IFLAG.EQ.1) WRITE(6,9009) ID,(AO(K1),RO(K1),
16290 1      K1=7,NMMONTH)
16300      GO TO 10
16310 199    CONTINUE
16320 C
16330 C
16340 C      CHECK COFLG AND OUTPUT DATA
16350 C
16360      IF(COFLG.EQ.0) GO TO 210
16370      IF(IFLAG.EQ.0) WRITE(6,5500) ID,(AO(K),RO(K),CO(K),IDC(K),
16380 1      K=1,KEND)
16390      IF(IFLAG.EQ.1) WRITE(6,5500) ID,(AO(K1),RO(K1),CO(K1),
16400 1      IDC(K1),K1=7,NMMONTH)
16410 C
16420      GO TO 10
16430 210    CONTINUE
16440 C
16450 C      CHECK DTFLG AND OUTPUT DATA
16460 C
16470      IF(DTFLG.EQ.0) GO TO 221
16480      IF(IFLAG.EQ.0) WRITE(6,5011) ID,(AO(K),RO(K),K=1,KEND)
16490      IF(IFLAG.EQ.1) WRITE(6,5011) ID,(AO(K1),RO(K1),K1=7,NMMONTH)
16500      GO TO 10
16510 221    CONTINUE
16520 C
16530 C      CHECK JOFLG AND OUTPUT DATA
16540 C
16550      IF(JOFLG.EQ.0) GO TO 220
16560      IF(IFLAG.EQ.0) WRITE(6,6000) ID,(AO(K),RO(K),CO(K),
16570 1      K=1,KEND)
16580      IF(IFLAG.EQ.1) WRITE(6,6000) ID,(AO(K1),RO(K1),CO(K1),
16590 1      K1=7,NMMONTH)
16600      GO TO 10
16610 220    CONTINUE
16620 C
16630 C      CHECK ROFLG AND OUTPUT DATA
16640 C
16650      IF(ROFLG.EQ.0) GO TO 230
16660      IF(IFLAG.EQ.1) GO TO 40
16670      IF(UFLAG.EQ.1) WRITE(6,7000) ID,(AO(K),RO(K),K=1,KEND)
16680      IF(UFLAG.EQ.0) WRITE(6,7001) ID,(AO(K),RO(K),K=1,KEND)
16690 40      IF(IFLAG.EQ.0) GO TO 10
16700      IF(UFLAG.EQ.1) WRITE(6,7000) ID,(AO(K1),RO(K1),K1=7,NMMONTH)
16710      IF(UFLAG.EQ.0) WRITE(6,7001) ID,(AO(K1),RO(K1),K1=7,NMMONTH)
16720      GO TO 10
16730 230    CONTINUE
16740 C
16750 C      CHECK TOFLG AND OUTPUT DATA
16760 C
16770      IF(TOFLG.EQ.0) GO TO 232
16780      IF(IFLAG.EQ.0) WRITE(6,9000) ID,(AO(K),RO(K),
16790 1      K=1,KEND)

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16800          IF (IFLAG.EQ.1) WRITE(6,9000) IN,(MO(K1),MU(K1),
16810          1          K1=7,NMONTH)
16820          232 CONTINUE
16830          10 CONTINUE
16840 C
16850 C CHECK ALL FLAGS AGAIN AND OUTPUT DATA FOR OVER 6 MONTHS
16860 C
16870          IF (IFLAG.EQ.1) GO TO 51
16880          IF (IDATZ.EQ.1) IFLAG=IFLAG+1
16890          IF (IDATZ.EQ.0) GO TO 51
16900          IENM2=IENM+1
16910          IF (POFLG.EQ.0) GO TO 399
16920          WRITE(6,1201)
16930          WRITE(6,1000) BASIN,IYEAR,ARENAM(J),(MO(M2),M2=IENM2,IENMTH)
16940          WRITE(6,1009) (DP(IN),P2(IN),IN=7,NMONTH)
16950          GO TO 5
16960          399 CONTINUE
16970          IF (COFLG.EQ.0) GO TO 400
16980          WRITE(6,1001)
16990          WRITE(6,1000) BASIN,IYEAR,ARENAM(J),(MO(M2),M2=IENM2,IENMTH)
17000          WRITE(6,1010) (AA(IN),C1(IN),CR1(IN),PRE(IN),IN=7,NMONTH)
17010          GO TO 5
17020          400 CONTINUE
17030          IF (DTFLG.EQ.0) GO TO 401
17040          WRITE(6,2001)
17050          WRITE(6,1000) BASIN,IYEAR,ARENAM(J),(MO(M2),M2=IENM2,IENMTH)
17060          WRITE(6,1011) (DT(IN),TC(IN),IN=7,NMONTH)
17070          GO TO 5
17080          401 CONTINUE
17090          IF (IOFLG.EQ.0) GO TO 410
17100          WRITE(6,1501)
17110          WRITE(6,1000) BASIN,IYEAR,ARENAM(J),(MO(M2),M2=IENM2,IENMTH)
17120          WRITE(6,1510) (I1(IN),P1(IN),SN(IN),IN=7,NMONTH)
17130          GO TO 5
17140          410 CONTINUE
17150          IF (ROFLG.EQ.0) GO TO 421
17160          WRITE(6,2002)
17170          WRITE(6,3000) BASIN,IYEAR,(MO(M2),M2=IENM2,IENMTH)
17180          WRITE(6,3010) (CMP(IN),ACT(IN),IN=7,NMONTH)
17190          GO TO 5
17200          421 CONTINUE
17210          IF (TOFLG.EQ.0) GO TO 51
17220          WRITE(6,3001)
17230          WRITE(6,3000) BASIN,IYEAR,(MO(M2),M2=IENM2,IENMTH)
17240          WRITE(6,3020) (TX(IN),TN(IN),IN=7,NMONTH)
17250          GO TO 5
17260 C
17270          51 IF (COFLG.EQ.1) GO TO 50
17280          IF (ROFLG.EQ.1) GO TO 999
17290          IF (TOFLG.EQ.1) GO TO 999
17300          50 CONTINUE
17310          999 RETURN
17320 C
17330 C FORMAT STATEMENTS:
17340 C
17350          9999 FORMAT('C',////////)
17360          1000 FORMAT(/5X,'RANGO-MARTINEC MODEL FOR ',2A8,2X,'YEAR=',I5//
17370          1 10X,'DATA FOR ZONE',A5//
17380          2 1X,'DAY ',6X,6(A4,16X)//
17390          1010 FORMAT(6X,6(A4,2X,A4,1X,A4,2X,A4)//
17400          1011 FORMAT(5X,6(2X,A4,4X,A4,6X)//
17410          1510 FORMAT(6(4X,A4,1X,A4,3X,A4)//
17420          3000 FORMAT(/5X,'RANGO-MARTINEC MODEL FOR ',2A8,2X,'YEAR=',I5//
17430          1 1X,'DAY ',6X,6(A4,16X)//
17440          3010 FORMAT(2X,6(1X,A8,3X,A8)//
17450          3020 FORMAT(3X,6(1X,A8,1X,A8,2X)//
17460          5000 FORMAT(1X,I2,2X,6(6X,F10,3))
17470          5011 FORMAT(1X,I2,2X,6(F6.2,4X,F4.2,6X))
17480          5500 FORMAT(1X,I2,3X,6(F4.2,2X,F4.2,1X,F4.2,3X,I1,2X))
17490          6000 FORMAT(1X,I2,1X,6(F6.2,1X,F5.2,1X,F5.3,2X))
17500          7000 FORMAT(1X,I2,1X,6(F6.0,4X,F6.0,4X))
17510          7001 FORMAT(1X,I2,1X,6(F7.3,2X,F7.3,4X))
17520          9000 FORMAT(1X,I2,2X,6(F6.2,3X,F6.2,5X))
17530          1009 FORMAT(5X,6(2X,A4,4X,A4,6X)//
17540          9009 FORMAT(1X,I2,2X,6(1X,F5.3,3X,F5.3,6X))
17550          1201 FORMAT(/5X,'DAILY SNOW DEPTH BY ZONE IN CM,M**2(DPTH),
17560          1 DAILY COMPUTED PRECIP CONTRIBUTING TO RUNOFF(CPRE)//
17570          1001 FORMAT(/5X,'DEGREE-DAY FACTORS(AN),RUNOFF COEFFICIENTS FOR
17580          1 SNOW(CS), FOR RAIN(CR), PRECIP METHOD(PR)//
17590          1501 FORMAT(/5X,'DAILY TEMP IN DEGREE-DAYS(DD),INPUT PRECIP(PREC),
17600          1 SNOW COVERED AREA IN X(SCA)//
17610          2001 FORMAT(/5X,'LAPSE RATE(DTLR), CRITICAL TEMPERATURE(TCRT)//
17620          2002 FORMAT(/5X,'DAILY COMPUTED AND ACTUAL SNOWMELT RUNOFF DATA//
17630          3001 FORMAT(/5X,'DAILY MAXIMUM AND MINIMUM TEMPERATURES//
17640          END
17650          SURROUTINE PLOTR(QNP1X,ACTUAL,X1,N),UFLAG,ACTFLG)
17660 C
17670 C*****
17680 C
17690 C FUNCTION - PLOTR CALLS THE FORTRAN PRPLOT PRINTER-PLUT

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17700 C          PACKAGE TO PLOT ACTUAL AND SIMULATED STREAM
17710 C          RUNOFF AS A FUNCTION OF STREAM DISCHARGE VS.
17720 C          NUMBER OF SNOWMELT DAYS.
17730 C
17740 C
17750 C          ARGUMENT LIST -
17760 C          VARIABLE TYPE IO DESCRIPTION
17770 C          -----
17780 C          QNP1X R*4 IO ARRAY OF SIMULATED STREAM RUNOFF DATA
17790 C          ACTUAL R*4 IO ARRAY OF ACTUAL STREAM RUNOFF
17800 C          X1 R*4 IO ARRAY OF SNOWMELT DAYS
17810 C          ND I*4 I NUMBER OF SNOWMELT DAYS
17820 C          UFLAG I*2 I UNITS FLAG: 0=METRIC UNITS,1=ENGLISH UNITS
17830 C          ACTFLG I*2 I ACTUAL DATA FLAG: 0=NO ACTUAL DATA
17840 C          AVAILABLE,1=ACTUAL DATA AVAILABLE
17850 C
17860 C
17870 C
17880 C          EXTERNAL REFERENCES --
17890 C          PLOT1 - PRPLOT ROUTINE TO DETERMINE PLOT SCALE FACTORS AND
17900 C          DIMENSIONS OF LENGTH AND WIDTH OF PLOT IMAGE.
17910 C          PLOT2 - PRPLOT ROUTINE CONSTRUCTS GRID1 IMAGE IN CORE.
17920 C          PLOT3 - PRPLOT ROUTINE PUTS SPECIFIED CHARACTER IN POSITION
17930 C          CORRESPONDING TO VALUE(S) OF X AND Y.
17940 C          PLOT4 - PRPLOT ROUTINE WRITES IMAGE OF COMPLETED GRAPH ON
17950 C          UNIT FT06F001. PRINTS LABEL FOR ORIGINATE ON LEFT
17960 C          EDGE OF PLOT.
17970 C
17980 C
17990 C          CALLED BY -- MAIN
18000 C
18010 C          COMPUTER/LANGUAGE -- IBM 360/91 AT GSFC/FORTRAN IV
18020 C
18030 C          DESIGNER/PROGRAMMER -- G. MAJOR, RESEARCH & DATA SYSTEMS, INC.
18040 C
18050 C *****
18060 C
18070 C          DIMENSION GRID1(3500)
18080 C          DIMENSION DASH(3)
18090 C
18100 C          DATA CHAR/' '/
18110 C          DATA DASH/3*0.1/
18120 C
18130 C          DIMENSION QNP1X(367),X1(367),ACTUAL(366),ACTPLT(366)
18140 C
18150 C          INTEGER*2 UFLAG,ACTFLG
18160 C
18170 C          WRITE(6,1000)
18180 C1000  FORMAT(' SUBROUTINE PLOT ENTERED')
18190 C
18200 C          SCALE ACTUAL AND PREDICTED STREAM FLOW IF IN ENG. UNITS
18210 C
18220 C
18230 C          DO 5 I=1,ND
18240 C             QNP1X(I)=QNP1X(I)/100.
18250 C             ACTPLT(I)=ACTUAL(I)
18260 C          5  CONTINUE
18270 C
18280 C          IF(UFLAG.EQ.1) GO TO 120
18290 C          GO TO 130
18300 C120  DO 7 I=1,ND
18310 C             QNP1X(I)=QNP1X(I)/100.
18320 C             ACTPLT(I)=ACTUAL(I)/100.
18330 C          7  CONTINUE
18340 C          GO TO 131
18350 C130  CONTINUE
18360 C          DO 6 J2=1,ND
18370 C             ACTPLT(I2)=ACTUAL(I2)
18380 C          6  CONTINUE
18390 C
18400 C          SET UP PLOT FOR NUMBER OF DAYS .LE. 100
18410 C
18420 C133  IF(ND.LE.100) GO TO 10
18430 C          GO TO 20
18440 C10  CONTINUE
18450 C          WRITE(6,8)
18460 C          CALL PLOT1(0,10,10,10,10)
18470 C          CALL PLOT2(GRID1,100.,0.,50.,0.)
18480 C          ND1=ND-1
18490 C          CALL PLOT3('X',X1(1),QNP1X(1),ND)
18500 C          IF(ACTFLG.EQ.0) GO TO 11
18510 C          CALL PLOT3(' ',X1,ACTPLT,ND)
18520 C11  IF(UFLAG.EQ.0) CALL PLOT4(18,'CURIC METERS/SEC')
18530 C          IF(UFLAG.EQ.1) CALL PLOT4(28,'CURIC FEET/SEC SCALED BY 100')
18540 C          WRITE(6,9)
18550 C          9  FORMAT('//30X,'*-COMPUTED  =-ACTUAL')
18560 C          WRITE(6,8)
18570 C          8  FORMAT('C',////////)
18580 C20  CONTINUE
18590 C

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```

18600 C      SET UP PLOTS FOR NUMBER OF DAYS .LE. 200
18610 C
18620      IF(ND.GT.100.AND.ND.LE.200) GO TO 30
18630      GO TO 40
18640      30 CONTINUE
18650      WRITE(6,8)
18660      CALL PLOT1(0,10,10,10,10)
18670      CALL PLOT2(GRID1,100.,0.,50.,0.)
18680      CALL PLOT3('*',X1(1),QNP1X(1),100)
18690      IF(ACTFLG.EQ.0) GO TO 35
18700      CALL PLOT3(' ',X1,ACTPLT,100)
18710      35 IF(UFLAG.EQ.0) CALL PLOT4(18,'CURIC METERS/SEC')
18720      IF(UFLAG.EQ.1) CALL PLOT4(28,'CURIC FEET/SEC SCALED BY 100')
18730      WRITE(6,9)
18740      WRITE(6,8)
18750 C
18760 C      PLOT DAYS BETWEEN 100 AND 200
18770 C
18780      CALL PLOT1(0,10,10,10,10)
18790      CALL PLOT2(GRID1,200.,100.,50.,0.)
18800      ND1=(ND-100)+1
18810      CALL PLOT3('*',X1(100),QNP1X(100),ND1)
18820      IF(ACTFLG.EQ.0) GO TO 45
18830      ND2=(ND-100)+1
18840      CALL PLOT3(' ',X1(100),ACTPLT(100),ND1)
18850      45 IF(UFLAG.EQ.0) CALL PLOT4(18,'CURIC METERS/SEC')
18860      IF(UFLAG.EQ.1) CALL PLOT4(28,'CURIC FEET/SEC SCALED BY 100')
18870      WRITE(6,9)
18880      WRITE(6,8)
18890      40 CONTINUE
18900 C
18910 C      SET UP PLOTS FOR NUMBER OF DAYS .LE. 300
18920 C
18930      IF(ND.GT.200.AND.ND.LE.300) GO TO 50
18940      GO TO 60
18950      50 CONTINUE
18960      WRITE(6,8)
18970      CALL PLOT1(0,10,10,10,10)
18980      CALL PLOT2(GRID1,100.,0.,50.,0.)
18990      CALL PLOT3('*',X1(1),QNP1X(1),100)
19000      IF(ACTFLG.EQ.0) GO TO 55
19010      CALL PLOT3(' ',X1,ACTPLT,100)
19020      55 IF(UFLAG.EQ.0) CALL PLOT4(18,'CURIC METERS/SEC')
19030      IF(UFLAG.EQ.1) CALL PLOT4(28,'CURIC FEET/SEC SCALED BY 100')
19040      WRITE(6,9)
19050      WRITE(6,8)
19060 C
19070 C      PLOT BETWEEN DAYS 100 AND 200
19080 C
19090      CALL PLOT1(0,10,10,10,10)
19100      CALL PLOT2(GRID1,200.,100.,50.,0.)
19110      CALL PLOT3('*',X1(100),QNP1X(100),101)
19120      IF(ACTFLG.EQ.0) GO TO 65
19130      CALL PLOT3(' ',X1(100),ACTPLT(100),101)
19140      65 IF(UFLAG.EQ.0) CALL PLOT4(18,'CURIC METERS/SEC')
19150      IF(UFLAG.EQ.1) CALL PLOT4(28,'CURIC FEET/SEC SCALED BY 100.')
19160      WRITE(6,9)
19170      WRITE(6,8)
19180 C
19190 C      PLOT DAYS BETWEEN 200 AND 300
19200 C
19210      CALL PLOT1(0,10,10,10,10)
19220      CALL PLOT2(GRID1,300.,200.,50.,0.)
19230      ND1=(ND-200)+1
19240      CALL PLOT3('*',X1(200),QNP1X(200),ND1)
19250      IF(ACTFLG.EQ.0) GO TO 75
19260      ND2=(ND-200)+1
19270      CALL PLOT3(' ',X1(200),ACTPLT(200),ND1)
19280      75 IF(UFLAG.EQ.0) CALL PLOT4(18,'CURIC METERS/SEC')
19290      IF(UFLAG.EQ.1) CALL PLOT4(28,'CURIC FEET/SEC SCALED BY 100.')
19300      WRITE(6,9)
19310      WRITE(6,8)
19320      60 CONTINUE
19330 C
19340 C      SET UP PLOTS FOR NUMBER OF DAYS BETWEEN 300 AND 365
19350 C
19360      IF(ND.GT.300.AND.ND.LE.366) GO TO 70
19370      GO TO 80
19380      70 CONTINUE
19390      WRITE(6,8)
19400      CALL PLOT1(0,10,10,10,10)
19410      CALL PLOT2(GRID1,100.,0.,50.,0.)
19420      CALL PLOT3('*',X1(2),QNP1X(2),99)
19430      IF(ACTFLG.EQ.0) GO TO 85
19440      CALL PLOT3(' ',X1,ACTPLT,100)
19450      85 IF(UFLAG.EQ.0) CALL PLOT4(18,'CURIC METERS/SEC')
19460      IF(UFLAG.EQ.1) CALL PLOT4(28,'CURIC FEET/SEC SCALED BY 100.')
19470      WRITE(6,9)
19480      WRITE(6,8)
19490 C

```

```

19500 C      PLOT BETWEEN 100 AND 200 DAYS
19510 C
19520      CALL PLOT1(0,10,10,10,10)
19530      CALL PLOT2(GRID1,200,,100,,50,,0.)
19540      CALL PLOT3('* ',X1(100),QNP1X(100),101)
19550      IF(ACTFLG,EG,0) GO TO 95
19560      CALL PLOT3(' ',X1(100),ACTPLT(100),101)
19570 95      IF(UFLAG,EG,0) CALL PLOT4(18,'CURIC METERS/SEC')
19580      IF(UFLAG,EG,1) CALL PLOT4(28,'CURIC FEET/SEC SCALED BY 100.')
19590      WRITE(6,9)
19600      WRITE(6,8)
19610 C
19620 C      PLOT BETWEEN 200 AND 300 DAYS
19630 C
19640      CALL PLOT1(0,10,10,10,10)
19650      CALL PLOT2(GRID1,300,,200,,50,,0.)
19660      CALL PLOT3('* ',X1(200),QNP1X(200),101)
19670      IF(ACTFLG,EG,0) GO TO 105
19680      CALL PLOT3(' ',X1(200),ACTPLT(200),101)
19690 105     IF(UFLAG,EG,0) CALL PLOT4(18,'CURIC METERS/SEC')
19700      IF(UFLAG,EG,1) CALL PLOT4(28,'CURIC FEET/SEC SCALED BY 100.')
19710      WRITE(6,9)
19720      WRITE(6,8)
19730 C
19740 C      PLOT BETWEEN 300 AND 365 DAYS
19750 C
19760      CALL PLOT1(0,10,10,10,10)
19770      CALL PLOT2(GRID1,400,,300,,50,,0.)
19780      ND1=(ND-300)+1
19790      CALL PLOT3('* ',X1(300),QNP1X(300),ND1)
19800      IF(ACTFLG,EG,0) GO TO 115
19810 C      ND2=(ND-300)+1
19820      CALL PLOT3(' ',X1(300),ACTPLT(300),ND1)
19830 115     IF(UFLAG,EG,0) CALL PLOT4(18,'CURIC METERS/SEC')
19840      IF(UFLAG,EG,1) CALL PLOT4(28,'CURIC FEET/SEC SCALED BY 100.')
19850      WRITE(6,9)
19860      WRITE(6,8)
19870 80      CONTINUE
19880      RETURN.
19890      END

```

```

1
00010 SUBROUTINE PRPLOT
00020 C PETE SMIDINGER SUMMER 1964 MATH & COMP BR GSFC NASA
00030 IMPLICIT LOGICAL*(I), LOGICAL*(K)
00040 DIMENSION NSCALE(5),ABNOS(26),X(1),Y(1)
00050 LOGICAL*1 NOS(10) /'0','1','2','3','4','5','6','7','8','9'/
00060 LOGICAL*1 IMADE(1),CH,LABEL(1)
00070 LOGICAL*1 VC ,HC/'-','NC/'+'','BL/' /
00080 L ,HF/'F',HF1/'',HF2/'',
00090 DATA VC/'I'/
00100 C DATA VC/24F/
00110 LOGICAL*1 FOR1(19) /'(1XA1,FB, ,1X121A1)'/
00120 L ,FOR2(15) /'(1XA1, 9X121A1)'/
00130 L ,FOR3(19) /'(1HOF , , F , )'/
00140 DATA KPLOT1 ,FALSE, /, KPLOT2 ,FALSE, /
00150 DATA KABSC,KORD,KBOTGL /38,FALSE, /
00160 C
00170 ENTRY PLOT1(NSCALE,NHL,NSBH,NVL,NSBV)
00180 KPLOT1=.TRUE.
00190 KPLOT2=.FALSE.
00200 125 NH=IABS(NHL)
00210 NSH=IABS(NSBH)
00220 NV=IABS(NVL)
00230 NSV=IABS(NSBV)
00240 NSCL=NSCALE(1)
00250 IF(NH*NSH*NV*NSV.NE.0) GO TO 128
00260 WRITE (6,14)
00270 14 FORMAT(TS,'SOME PLOT1 ARG. ILLEGALLY 0')
00280 KPLOT1=.FALSE.
00290 RETURN
00300 128 KPLOT1=.TRUE.
00310 IF(NV.LE.25) GO TO 126
00320 WRITE (6,12)
00330 KPLOT1=.FALSE.
00340 12 FORMAT(TS,'NO. OF VERTICAL LINES >25')
00350 RETURN
00360 126 CONTINUE
00370 NVH=NV-1
00380 NVP=NV+1
00390 NDH=NH*NSH
00400 NDHP=NDH+1
00410 NDV=NV*NSV
00420 NDVP=NDV+1
00430 NING=(NDHP*NDVP)
00440 IF(NDV.LE.120) GO TO 130
00450 KPLOT1=.FALSE.
00460 WRITE (6,11)
00470 11 FORMAT(TS,'WIDTH OF GRAPH >121')
00480 RETURN
00490 130 CONTINUE
00500 IF(NSCL.EQ.0) GO TO 70
00510 FSY=10.*NSCALE(2)
00520 FSE=10.*NSCALE(4)
00530 IY=MIN0(IABS(NSCALE(3)),7)+1
00540 IX=MIN0(IABS(NSCALE(5)),9)+1
00550 GO TO 75
00540 70 FSY=1.
00570 FSX=1.
00580 IY=4
00590 IX=4
00595 IF(.NOT. KPLOT2) GO TO 75
00600 XI=MAX1(ABS(XMAX),ABS(YMAX),ABS(XMIN),ABS(YMIN))
00610 IP=XI
00620 IF(IP .GT. 99999) IY=1

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00630      IF(IP .GT. 9999) IY=2
00640      IF(IP .GT. 999) IY=3
00650 75   FOR1(10)=NOS(IY)
00660      NA=MIND(IY,NSV)-1
00670      NS=NA-MING(MA,120-NDV)
00680      NB=1-NS+NA
00690      I1=NB/10
00700      I2=NB-I1*10
00710      FOR3(6)=NOS(I1+1)
00720      FOR3(7)=NOS(I2+1)
00730      FOR3(9)=NOS(NA+1)
00740      IF(MU.DT.0) GO TO 90
00750      DO 80 J=11,18
00760 80   FOR3(J)=BL
00770      GO TO 100
00780 90   I1=MV/10
00790      I2=MV-I1*10
00800      FOR3(11)=NOS(I1+1)
00810      FOR3(12)=NOS(I2+1)
00820      FOR3(13)=HF
00830      I1=MSV/100
00840      I3=MSV-I1*100
00850      I2=I3/10
00860      I3=I3-I2*10
00870      FOR3(14)=NOS(I1+1)
00880      FOR3(15)=NOS(I2+1)
00890      FOR3(16)=NOS(I3+1)
00900      FOR3(17)=HF1
00910      FOR3(18)=FOR3(9)
00920 100  IF(KPLOT1) RETURN
00930      KPLOT1=.TRUE.
00940 C
00950      ENTRY PLOT2(IMAGE,XMAX,XMIN,YMAX,YMIN)
00960      KPLOT2=.TRUE.
00970      IF(KPLOT1) GO TO 210
00980      NSCL=0
00990      NH=5
01000      NSH=10
01010      NV=10
01020      NSV=10
01030      GO TO 128
01040 210  CONTINUE
01050      IF(.NOT.KPLOT)RETURN
01060      YMX=YMAX
01070      DM=(YMAX-YMIN)/FLOAT (NDM)
01080      DV=(XMAX-XMIN)/FLOAT (NDV)
01090      DO 220 I=1,NVP
01100 220  ABNOS(I)=(XMIN+FLOAT((I-1)*NSV)*DV)*FSX
01110      DO 225 I=1,NIMG
01120 225  IMAGE(I)=BL
01130      DO 240 I=1,NDHP
01140      I2=I*NDVP
01150      I1=I2-NDV
01160      KNHDR=MOD(I-1,NSH).NE.0
01170      IF(KNHDR) GO TO 230
01180      DO 228 J=11,12
01190 228  IMAGE(J)=HC
01200 230  CONTINUE
01210      DO 240 J=11,I2,NSV
01220      IF(KNHDR) GO TO 235
01230      IMAGE(J)=NC
01240      GO TO 240

```

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01250 235 IMAGE(J)=VC
01260 240 CONTINUE
01270 XMIN1=XMIN-DV/2.
01280 YMIN1=YMIN-DH/2.
01290 RETURN
01300 C
01310 ENTRY PLOT3(CH,X,Y,N3)
01320 300 IF(KPLOT2) GO TO 312
01330 301 WRITE (6,13)
01340 13 FORMAT(TS,'PLOT2 MUST BE CALLED')
01350 312 CONTINUE
01360 IF(.NOT.KPLOT) RETURN
01370 IF(N3.GT.0) GO TO 314
01380 KPLOT=.FALSE.
01390 WRITE (6,15)
01400 15 FORMAT(TS,'PLOT3, ARG2 < 0')
01410 RETURN
01420 314 DO 320 I=1,N3
01430 DUM1=(X(I)-XMIN1)/DV
01440 DUM2=(Y(I)-YMIN1)/DH
01450 IF(DUM1.LT.0.,OR.DUM2.LT.0.) GO TO 320
01460 IF(DUM1.GE.NDVP,OR.DUM2.GE.NDHP) GO TO 320
01470 MX=1+INT(DUM1)
01480 NY=1+INT(DUM2)
01490 315 J=(NDHP-NY)*NDVP+MX
01500 IMAGE(J)=CH
01510 320 CONTINUE
01520 RETURN
01530 C
01540 ENTRY PLOT4(NL,LABEL)
01550 ENTRY FPLLOT4(NL,LABEL)
01560 IF(.NOT.KPLOT) RETURN
01570 IF(.NOT.KPLOT2) GO TO 301
01580 DO 420 I=1,NDHP
01590 IF(I.EQ.NDHP.AND.KDOTGL) GO TO 420
01600 WL=BL
01610 IF(I.LE.NL) WL=LABEL(I)
01620 I2=I*NDVP
01630 I1=I2-NDV
01640 IF(MOD(I-1,NSH).EQ.0.AND..NOT.KORD) GO TO 410
01650 WRITE (6,FOR2) WL,(IMAGE(J),J=I1,I2)
01660 GO TO 420
01670 410 CONTINUE
01680 ORDNO=(YMX-FLOAT(I-1)*DH)*FSY
01690 WRITE (6,FOR1) WL,ORDNO,(IMAGE(J),J=I1,I2)
01700 420 CONTINUE
01710 IF(KABSC) GO TO 430
01720 WRITE (6,FOR3) (ABSOS(J),J=1,NVP)
01730 430 RETURN
01740 C
01750 ENTRY OMIT(LSW)
01760 KABSC=MOD(LSW,2).EQ.1
01770 KORD=MOD(LSW,4).GE.2
01780 KDOTGL=LSW.GE.4
01790 RETURN
01800 C
01810 ENTRY PLTAPE(ITAPE)
01820 C NOT YET
01830 RETURN
01840 END
END OF DATA

```

APPENDIX C
DETAILS OF TEMPERATURE PREPROCESSING SUBROUTINE PRETMP

Table C-1. Description of parameters in temperature preprocessing subroutine PRETMP.

Figure C-1. Process-oriented flow chart for PRETMP.

Figure C-2. Flow diagram for subroutine PRETMP.

Figure C-3. Source listing for subroutine PRETMP.

Table C-1

Parameter	Common	Type	Units		Description
			Metric	English	
TMAX1	TBASE	R*4	°C	°F	Maximum temperature at station #1
TMIN1	TBASE	R*4	°C	°F	Minimum temperature at station #1
TMAX2	TBASE	R*4	°C	°F	Maximum temperature at station #2
TMIN2	TBASE	R*4	°C	°F	Minimum temperature at station #2
THOUR1	TBASE	R*4	°C	°F	Hourly temperatures from station #1
THOUR2	TBASE	R*4	°C	°F	Hourly temperatures from station #1
T1	TBASE	R*4	°C	°F	Temperatures in degrees/degree-days from station #1
T2	TBASE	R*4	°C	°F	Temperatures in degrees/degree-days from station #2
DTLR	BASDAT	R*4	°C/100m	°F/1000ft	Average temperature lapse rate in degree-days
ZMEAN	TBASE	R*8	m	ft	Hypsometric mean elevation of each zone
STATN	TBASE	R*8	m	ft	Mean elevation of each base station
NSTATN	TBASE	I*4	—	—	Number of base stations
MAXMIN	TBASE	I*2	—	—	Flag to indicate if temperatures are maximum-minimum. 0 = Not MAX-MIN 1 = MAX-MIN
ND	CLIDAT	I*4	Days	Days	Number of snowmelt days
NZ	BASDAT	I*4	—	—	Number of elevation zones
UFLAG	OPTDAT	I*2	—	—	Units option flag 0 = Metric units 1 = English Units
MTHD	OPTDAT	I*2	—	—	Degree-day temperature computation flag 0 = Mean method 1 = Effective minimum
IEXT	TBASE	I*2	—	—	Flag indicates how temperatures are to be extrapolated to elevation zone 0 = Extrapolate using predetermined constant 1 = Automatically extrapolate using lapse rate

Table C-1 (cont.)

Parameter	Common	Type	Units		Description
			Metric	English	
IDEGDY	TBASE	I*2	—	—	Flag to indicate if temperatures are to be computed in degree-days. 0 = Do not compute 1 = Compute temps in degree-days
ITZ	TBASE	I*2	—	—	Flag to indicate if temperatures are from single zone or all zones 0 = All zones 1 = Single zone
IHOURL	TBASE	I*2	—	—	Flag to indicate if temperatures are input hourly 0 = No hourly temperatures 1 = Hourly temperatures

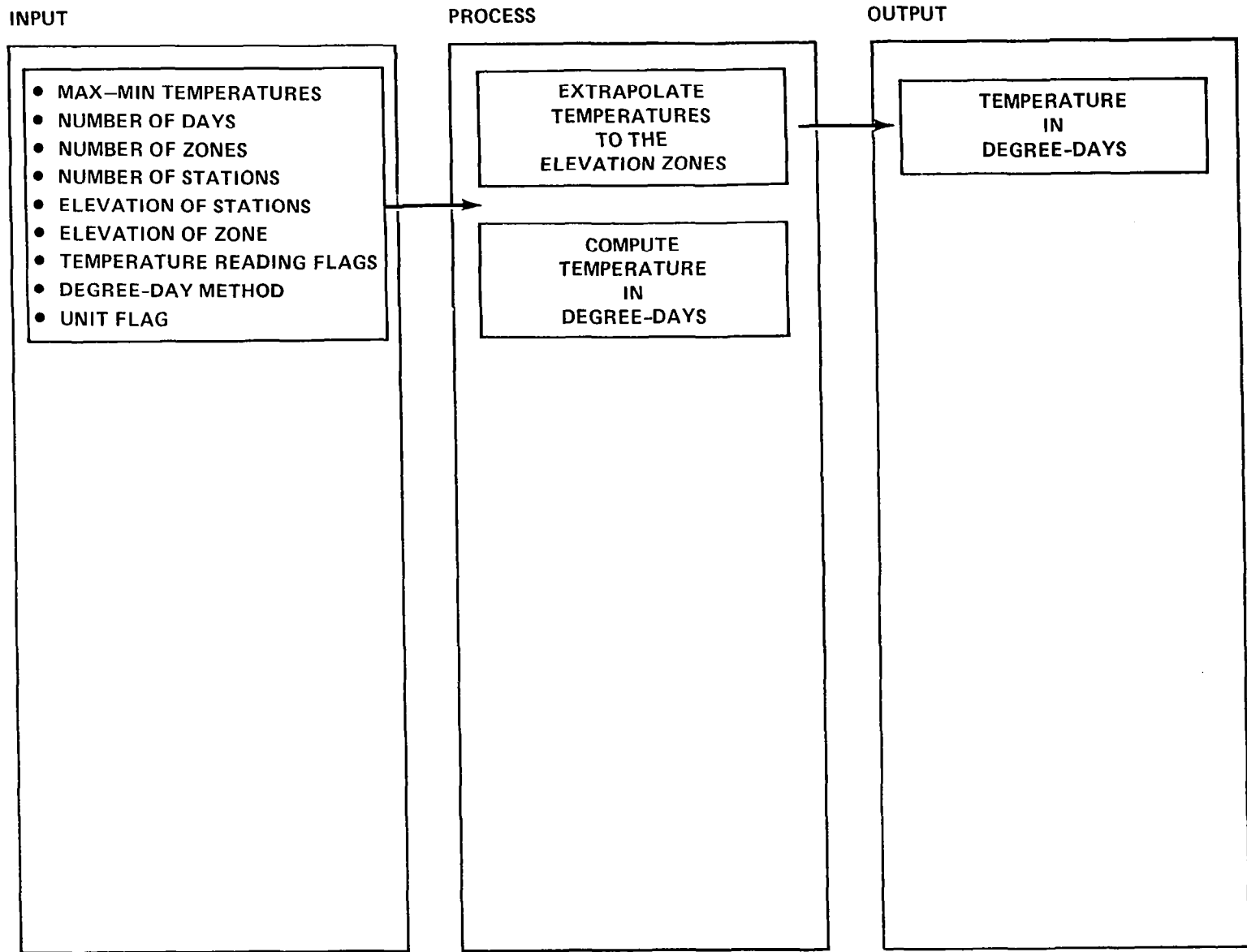


Figure C-1. Process-oriented flow chart for PRETMP.

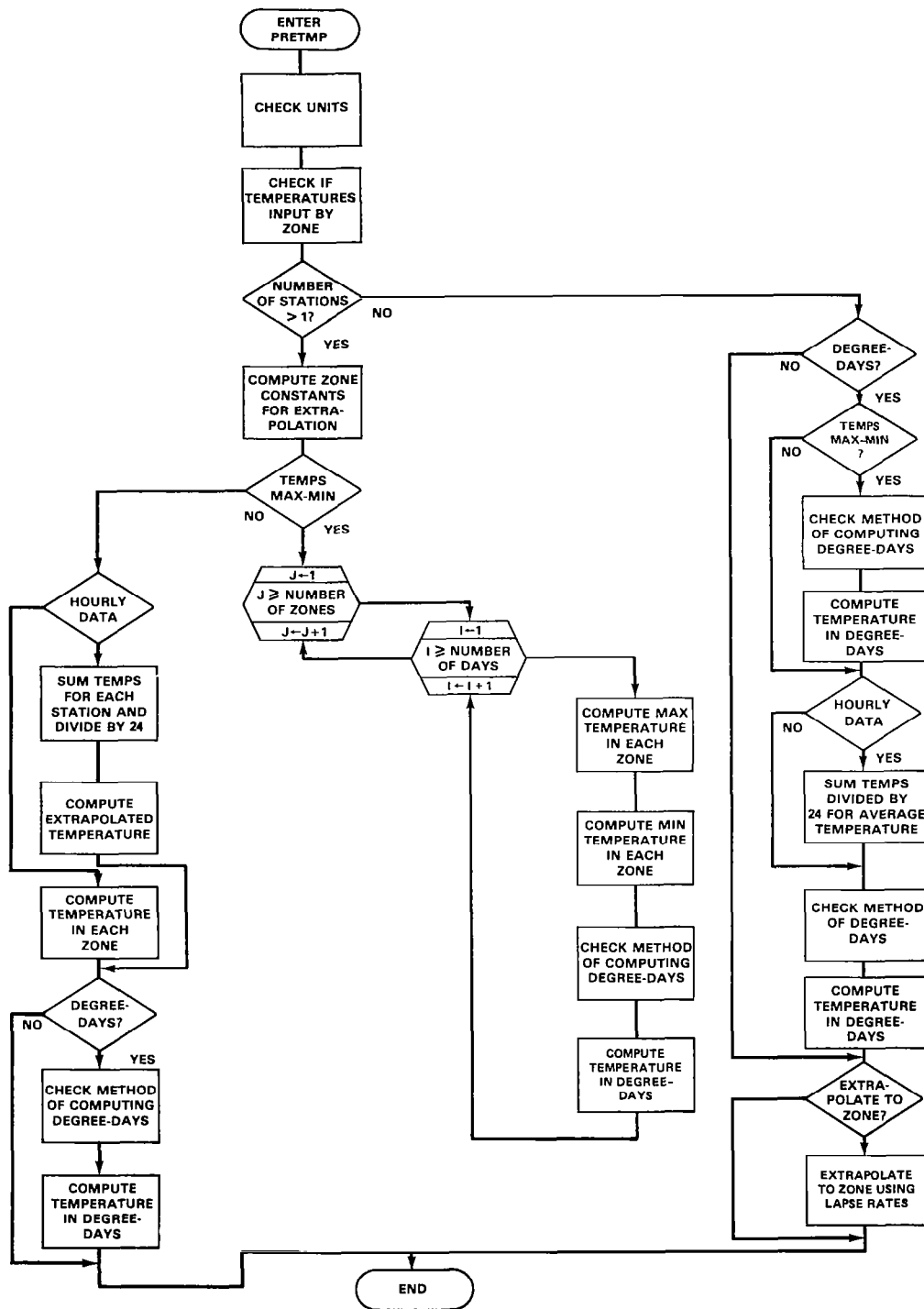


Figure C-2. Flow diagram for subroutine PRETMP.

```

00010 SUBROUTINE PRETMP(STATN,ND,NZ,ITMAX,ITMIN,TEMPT,THAX1,TMIN1,
00020 1 THAX2,TMIN2,DTLR,UFLAG,MTHD,ZMEAN,NSTATN,IEXT,IDEGDY,T)
00030 C
00040 C*****
00050 C
00060 C FUNCTION - PRETMP IS A MODULAR TEMPERATURE PREPROCESSING ROUTINE
00070 C TAKES MAX-MIN DAILY TEMPERATURES IN DEGREES FROM
00080 C EACH STATION AND EXTRAPOLATES THE TEMPERATURE TO
00090 C THE ZONE AND COMPUTES THE TEMPERATURE IN DEGREE-DAYS.
00100 C DEGREE-DAYS CAN BE COMPUTED BY ONE OF TWO METHODS
00110 C AS MEAN OR EFFECTIVE MINIMUM. TEMPERATURES CAN BE
00120 C INPUT AS SINGLE STATION VALUES OR AS HOURLY
00130 C TEMPERATURES.
00140 C
00150 C
00160 C ARGUMENT LIST
00170 C VARIABLE TYPE IO DESCRIPTION
00180 C -----
00190 C STATN R#8 I ELEVATION OF RECORDING STATION
00200 C ND I#4 I NUMBER OF SNOWMELT DAYS
00210 C NZ I#4 I NUMBER OF ZONES
00220 C ITMAX I#4 I DAY MAX TEMP IS RECORDED FOR EACH STATION
00230 C ITMIN I#4 I DAY MIN TEMP IS RECORDED FOR EACH STATION
00240 C THAX1 R#4 I MAX TEMPERATURE FOR STATION 1
00250 C TMIN1 R#4 I MIN TEMPERATURE FOR STATION 1
00260 C THAX2 R#4 I MAX TEMPERATURE FOR STATION 2
00270 C TMIN2 R#4 I MIN TEMPERATURE FOR STATION 2
00280 C UFLAG I#2 I UNITS FLAG(ENGLISH OR METRIC)
00290 C MTHD I#2 I METHOD OF COMPUTING DEGREE DAYS
00300 C (EFFECTIVE MINIMUM OR MEAN)
00310 C ZMEAN R#8 I HYPSONETRIC MEAN ELEVATION OF EACH ZONE
00320 C NSTATN I#2 I NUMBER OF TEMPERATURE RECORDING STATIONS
00330 C IEXT I#2 I FLAG TO EXTRAPOLATE TO ELEVATION ZONES
00340 C IDEGDY I#2 I FLAG TO COMPUTE DEGREE-DAYS
00350 C T R#4 O COMPUTED TEMPERATURE IN DEGREE DAYS
00360 C
00370 C EXTERNAL REFERENCES -- NONE.
00380 C
00390 C CALLED BY -- MAIN (DRVSNO)
00400 C
00410 C COMPUTER/LANGUAGE - IBM 360/91 AT GSFC/FORTRAN IV
00420 C
00430 C DESIGNER/PROGRAMMER - G.MAJOR,RESEARCH & DATA SYSTEMS,INC.
00440 C
00450 C*****
00460 C
00470 C
00480 C
00490 C DIMENSION ZCONST(8),ARENAH(8)
00500 C DIMENSION STATN(2),ITMAX(2),ITMIN(2),THAX1(365),TMIN1(365),
00510 1 THAX2(365),TMIN2(365),ZMEAN(8),T(365,8),DTLR(365,8),TEMPT(365,8)
00520 C
00530 C REAL*8 ZMEAN,STATN,ZCONST,STAIN
00540 C INTEGER*2 ITMAX,ITMIN,MTHD,ITPROC,UFLAG,NSTATN,IEXT,IDEGDY
00550 C
00560 C
00570 C IF(UFLAG.EQ.0) TU=0.
00580 C IF(UFLAG.EQ.1) TU=32.
00590 C
00600 C
00610 C CHECK NUMBER OF STATIONS
00620 C
00630 C IF(NSTATN.EQ.1) GO TO 900
00640 C

```

Figure C-3. Source listing for subroutine PRETMP.

```

00650 C      CALCULATE ZONE CONSTANTS BASED ON HYPSONETRIC MEAN ELEVATION
00660 C      OF ZONE AND ELEVATION OF STATION
00670 C
00680      STAINT=STATH(1)-STATN(2)
00690      DO 10 I=1,NZ
00700          ZCONST(I)=(ZMEAN(I)-STATN(1))/STAINT
00710 10      CONTINUE
00720 C
00730 C      CHECK UNITS
00740 C
00750 C
00760 C      CALCULATE TEMPERATURE IN DEGREE-DAYS FOR EACH ZONE
00770 C
00780      DO 30 J=1,NZ
00790          DO 20 I=1,ND
00800 C
00810 C          CHECK WHICH TEMPERATURE READINGS BELONG TO WHICH DAY FOR EACH
00820 C          STATION. IF ITMP IS 1 THEN THE READING IS FOR CURRENT DAY.
00830 C          IF ITMP IS 2 THEN THE READING IS FOR NEXT DAY.
00840 C
00850          IF(ITMAX(1).EQ.1) IX=I
00860          IF(ITMAX(1).EQ.2) IX=I+1
00870          IF(ITMAX(2).EQ.1) I2X=I
00880          IF(ITMAX(2).EQ.2) I2X=I+1
00890 C
00900          IF(ITMIN(1).EQ.1) IH=I
00910          IF(ITMIN(1).EQ.2) IH=I+1
00920          IF(ITMIN(2).EQ.1) I2M=I
00930          IF(ITMIN(2).EQ.2) I2M=I+1
00940 C
00950 C          COMPUTE MAX AND MIN TEMPERATURES FOR EACH ZONE
00960 C
00970          TMAX=ZCONST(J)*(TMAX1(IX)-TMAX2(I2X))
00980 C
00990          TMX=TMAX1(IX)+TMAX
01000 C          NOTE: SOUTH FORK BASIN PROCESSING ONLY
01010 C
01020          IF(J.EQ.3) GO TO 40
01030          GO TO 41
01040 40      IF(TM<GT.TMAX2(I2X)) TMX=TMAX2(I2X)
01050 41      CONTINUE
01060          TMIN=ZCONST(J)*(TMIN1(IH)-TMIN2(I2M))
01070          TMN=TMIN1(IH)+TMIN
01080 C
01090 CC          NOTE: SOUTH FORK BASIN PROCESSING ONLY
01100 C
01110          IF(J.EQ.3) GO TO 42
01120          GO TO 43
01130 42      IF(TM<GT.TMIN2(I2M)) TMN=TMIN2(I2M)
01140 43      CONTINUE
01150 C
01160 C          CHECK METHOD OF COMPUTING DEGREE-DAYS. IF MTHD IS 1 THEN USE
01170 C          EFFECTIVE MINIMUM METHOD. IF MTHD IS 0 USE MEAN METHOD.
01180 C
01190          IF(MTHD.EQ.1) GO TO 35
01200          IF(MTHD.EQ.0) GO TO 25
01210 C
01220 35      IF(UFLAG.EQ.0.AND.TMN.LT.0.) TMN=0.
01230          IF(UFLAG.EQ.1.AND.TMN.LT.32.) TMN=32.
01240 C
01250 C          COMPUTE TEMPERATURE IN DEGREE-DAYS
01260 C
01270 25      TEMPT(I,J)=((TMX+TMN)/2.)-TU
01280          IF(TEMPT(I,J).LT.0.) TEMPT(I,J)=0.

```

Figure C-3. (Continued)

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01290 20    CONTINUE
01300 30    CONTINUE
01310      GO TO 990
01320 900    CONTINUE
01330 C
01340 C    CHECK IF TEMPERATURE IS TO BE COMPUTED IN DEGREE-DAYS
01350 C
01360      IF(IDEGBY.EQ.0) GO TO 590
01370 C
01380 C    CHECK IF TEMPERATURES ARE MAX-MIN
01390 C
01400      IF(ITMAX(1).EQ.0) GO TO 52
01410 C
01420 C    CHECK METHOD OF COMPUTING DEGREE DAYS
01430 C
01440      DO 600 I=1,ND
01450          IF(MTHD.EQ.1) GO TO 22
01460          IF(MTHD.EQ.0) GO TO 23
01470 22      IF(UFLAG.EQ.0.AND.TMIN1(I).LT.0.) TMIN1(I)=0.0
01480          IF(UFLAG.EQ.1.AND.TMIN1(I).LT.32.) TMIN1(I)=32.0
01490 C*     COMPUTE TEMPERATURE IN DEGREE DAYS
01500 C
01510 23      T(I,1)=((TMAX1(I)+TMIN1(I))/2.)-TU
01520 C     IF(T(I,1).LT.0.0) T(I,1)=0.0
01530 600    CONTINUE
01540 C
01550          GO TO 590
01560 52      CONTINUE
01570          DO 605 I=1,ND
01580              IF(MTHD.EQ.1) GO TO 53
01590              IF(MTHD.EQ.0) GO TO 54
01600 53      IF(UFLAG.EQ.0.AND.T(I,1).LT.0.) T(I,1)=0.
01610              IF(UFLAG.EQ.1.AND.T(I,1).LT.32.) T(I,1)=32.
01620 54      T(I,1)=T(I,1)-TU
01630 605    CONTINUE
01640 590    CONTINUE
01650 C
01660 C    CHECK IF TEMPERATURE IS TO BE AUTOMATICALLY EXTRAPOLATED TO
01670 C    ELEVATION ZONE. IF NOT, USE THE LAPSE RATES GIVEN AS INPUT
01680 C
01690      IF(IEXT.EQ.0) GO TO 950
01700      IF(UFLAG.EQ.0) ZCON=100.
01710      IF(UFLAG.EQ.1) ZCON=1000.
01720      DO 602 J=1,NZ
01730          ZCONST(J)=STATN(1)-ZMEAN(J)
01740          DO 601 I=1,ND
01750              TEMPT(I,J)=T(I,1)+(ZCONST(J)/ZCON)*DTLR(I,1)
01760 601    CONTINUE
01770 602    CONTINUE
01780      GO TO 990
01790 950    CONTINUE
01800 C
01810 C    EXTRAPOLATE TEMPERATURES USING THE GIVEN LAPSE RATES
01820 C
01830      DO 603 J=1,NZ
01840          DO 604 I=1,ND
01850              TEMPT(I,J)=T(I,1)+DTLR(I,J)
01860 604    CONTINUE
01870 603    CONTINUE
01880 C
01890 990    RETURN

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Figure C-3. (Continued)

1. Report No. NASA RP-1100	2. Government Accession No.	3. Recipient's Catalog No.	
4. Title and Subtitle The Snowmelt-Runoff Model (SRM) User's Manual		5. Report Date April 1983	
		6. Performing Organization Code 924	
7. Author(s) J. Martinec, A. Rango, and E. Major		8. Performing Organization Report No. 83B0251	
9. Performing Organization Name and Address Goddard Space Flight Center Greenbelt, Maryland 20771		10. Work Unit No. 677-22-26	
		11. Contract or Grant No.	
		13. Type of Report and Period Covered Reference Publication	
12. Sponsoring Agency Name and Address National Aeronautics and Space Administration Washington, D.C. 20546		14. Sponsoring Agency Code	
15. Supplementary Notes J. Martinec: Federal Institute for Snow and Avalanche Research, Weissfluhjoch/Davos, Switzerland. A. Rango: Goddard Space Flight Center, Greenbelt, Maryland. E. Major: Research and Data Systems, Inc., Lanham, Maryland.			
16. Abstract The purpose of this manual is to provide a means by which a user may apply the snowmelt-runoff model (SRM) unaided. To this effect, model structure, conditions of application, and data requirements, including remote sensing, are described. Guidance is given for determining various model variables and parameters. Possible sources of error are discussed and conversion of SRM from the simulation mode to the operational forecasting mode is explained. A computer program is presented for running SRM which should be easily adaptable to most systems used by water resources agencies.			
17. Key Words (Selected by Author(s)) Snowmelt-Runoff Model, Remote Sensing, Data Requirements, Simulation, Forecasting, Computer Program		18. Distribution Statement Unclassified - Unlimited Subject Category 43	
19. Security Classif. (of this report) Unclassified	20. Security Classif. (of this page) Unclassified	21. No. of Pages 118	22. Price* A06