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FINAL REPORT

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DEPLOYABLE ANTENNA STUDY Final Report
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MECHANICALLY SCANNED

DEPLOYABLE

ANTENNA STUDY



PREPARED FOR
GODDARD SPACEFLIGHT CENTER

9 MARCH 1983

 HARRIS

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FINAL REPORT

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1.0

INTRODUCTION AND EXECUTIVE SUMMARY

This report presents the conceptual design of a Mechanically Scanned Deployable Antenna which can be launched by the STS (Space Shuttle) to provide radiometric brightness temperature maps of the earth and oceans at selected frequency bands in the frequency range of 1.4 GHz to 11 GHz. Unlike previous scanning radiometric systems, multiple radiometers for each frequency are required in order to fill in the resolution cells across the swath created by the 15 meter diameter spin stabilized system. This multiple beam radiometric system (reference Figure 1.0-1) is sometimes designated as a "whiskbroom" system in that it combines the techniques of the scanning and "pushbroom" type systems.

The scope of the study includes (a) the definition of the feed system including possible feed elements and location, (b) determination of the fundamental reflector-feed offset geometry including offset angles and f/D ratio, (c) preliminary estimates of the beam efficiency of the feed reflector system, (d) a summary of reflector mesh losses at the proposed radiometric frequency bands, (e) an overall conceptual configuration design and (f) preliminary structural and thermal analyses.

This Final Report is organized as follows:

- Section 2.0 - Requirements Summary.
- Section 3.0 - Description of the Conceptual Design.
- Section 4.0 - Projected System Performance.
- Appendix - Detailed Description of the NLSA (Harris Proprietary Non-Linear Structural Analysis Program) Model of the Design.

The Mechanically Scanned Deployable Antenna (MSDA) is a 15 meter offset fed parabolic antenna designed for use in a mechanically scanned spaceborne sensor system. The sensor measures brightness temperatures and normalized backscatter coefficients to determine sea surface temperatures

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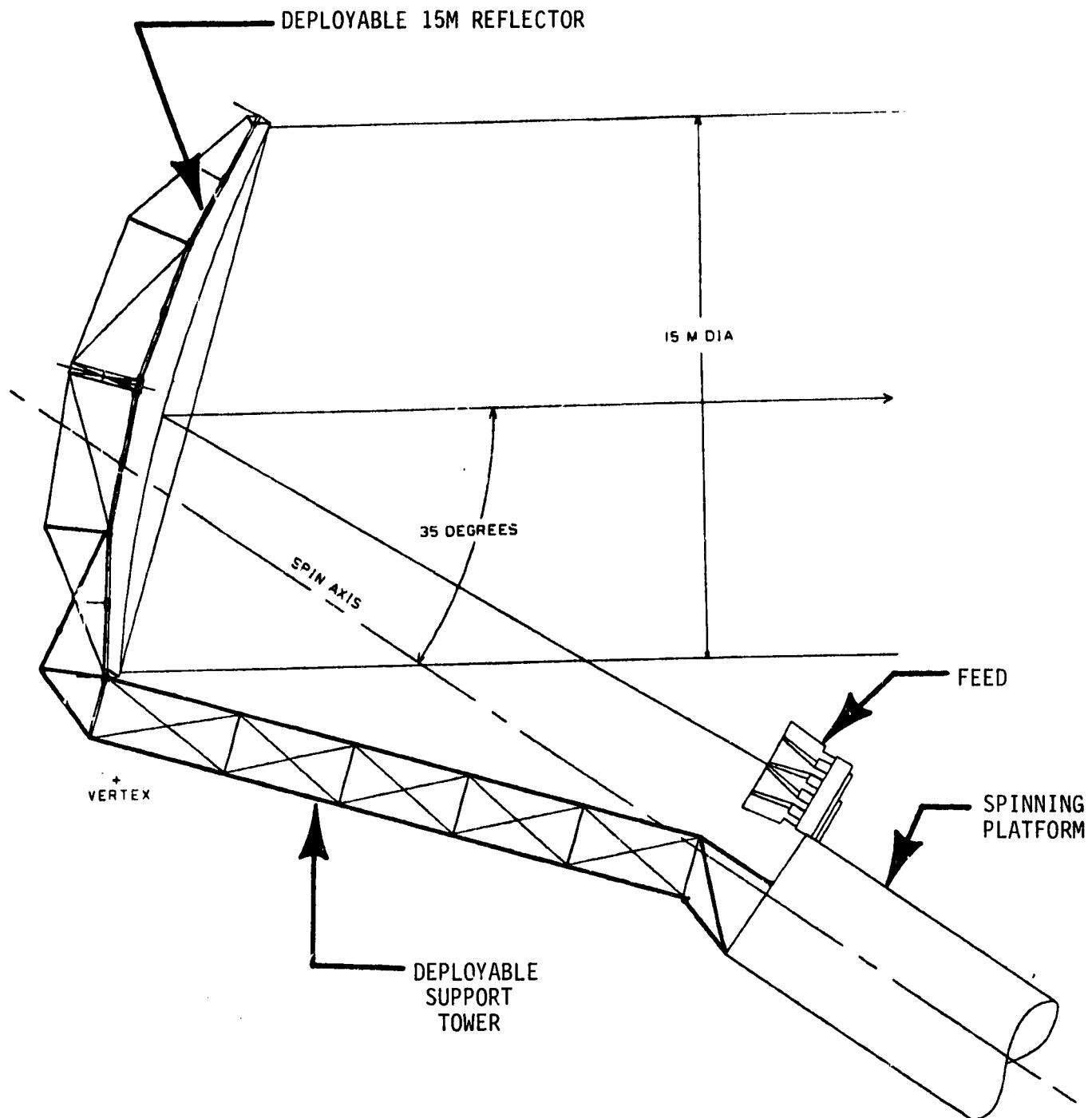


Figure 1.0-1. Deployed Radiometer System

(SST), wind speed, soil moisture, and precipitation (active channel) from a low orbiting satellite (700 KM). The antenna improves up to 4 times the spatial resolution for sea surface temperature over the Large Antenna Multi-frequency Microwave Radiometer (LAMMR).

Based upon the background of such remote sensing needs, the MSDA system was conceived with the detailed requirements in Section 2.0, Table 2.0. The basic system under consideration is a scanning antenna, where the feed and reflector system are fixed relative to the spacecraft bus and the entire system is spun at a 6 rpm rate. At this rate, chosen deliberately slow in order to allow a flexible deployable antenna, a single-beam one-radiometer-per-frequency system will not have contiguous beams at the end of each rotation due to spacecraft motion relative to the earth's surface. Therefore, a multibeam antenna with an independent radiometer connected to each beam at each frequency is required. Such a system, or so called "whiskbroom" radiometer is depicted in Figure 1.0-2.

Use of a multibeam feed, while simplifying and improving system radiometer performance, necessitates use of much heavier feed hardware and electronics. One must then trade supporting either the feed or the reflector from a boom. Since they both weigh approximately the same the structural trade is of minor concern. Thus the conceptual approach supports the reflector with the boom allowing the feed to reside on the bus itself, thereby minimizing transmission losses from feed to receiver.

The conceptual antenna feed system developed by Harris Government Electronic Systems Division (GESD) is an offset fed, 15M, deployable reflector antenna connected to the main spacecraft by an 18M deployable boom. The offset angle of approximately 35° was chosen to place the feed hardware sufficiently out of the projected reflector aperture to minimize diffractions. The deployable mast and reflector system stows in a launch configuration next to the feed on the spacecraft. The total weight of the tower support and deployment structure is about 394 pounds. The antenna feeds weigh 184 pounds assuming that corrugated horns are used as the baseline design. The baseline narrow-angle corrugated horns at 1.4 GHz, 4.3 GHz, 5.1* GHz and 11.0 GHz horns exhibit low spill-over

*4.3 and 5.1 GHz in one horn.

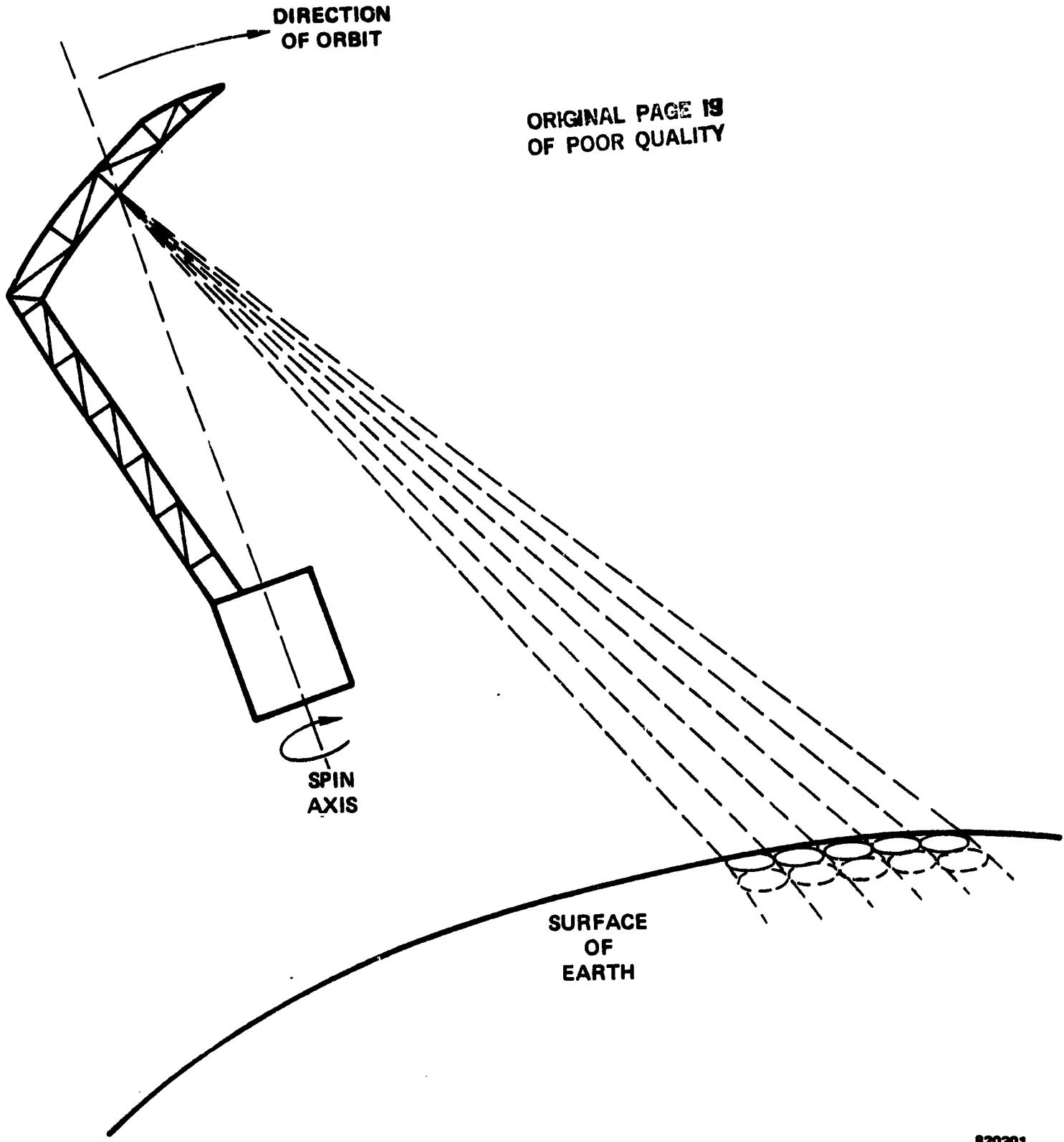


Figure 1.0-2. Whiskbroom Scanning Radiometer System

efficiencies (<5%). These horns, when placed physically in-line and adjacent, produce a surface resolution cell pattern with missing alternating cells. In order to fill in the empty cells, the time scanning whiskbroom feature of the system is used with horns placed on the side and staggered in between the first line of horns. We may physically stagger the horns in this manner with minimum degradation in performance due to the offset f/D ratio of 1.2. Such a large f/D ratio was chosen not only to allow scanning but to reduce the cross-polarization levels to about -30 dB. The preliminary beam efficiency calculations (Figure 1.0-3) indicate that the specification of 90% can be met even for four or five horn displacements off-axis.

The electrical properties of the mesh surface were investigated and all data from past programs was compiled and reviewed. This surface loss property is of particular concern in space radiometric applications due to the environmental effects upon the antenna loss. All present data and modeling calculations for the 10 openings per inch gold-plated molybdenum mesh chosen for this application indicate that loss values less than 0.1 dB are possible for frequencies up to 11.0 GHz. No significant change in the mesh reflector surface impedance is expected under changing solar conditions.

The mechanical-thermal analysis performed on the Harris concept clearly indicate that the spin effects produce only minor distortions. Indeed the antenna can be dynamically balanced by changing the attachment location on the spacecraft. The largest distortion is an axial defocus of about 0.628 inches due to thermal gradients. Axial defocusing in such long focal length optics systems is generally acceptable. The RMS surface tolerance error for this design degrades the beam efficiency of the antenna system at X-Band to a value below 90%.

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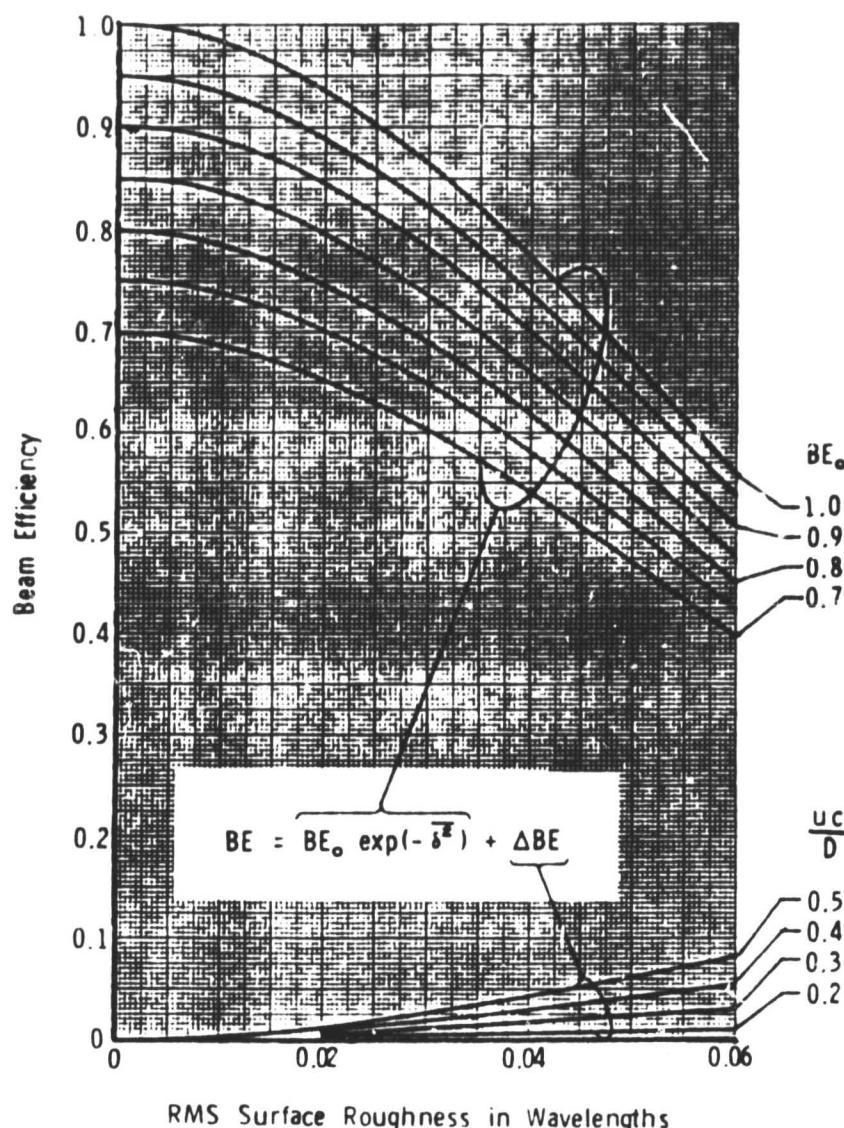


Figure 1.0-3. Beam Efficiency of a Random Rough Surface Reflector

2.0

REQUIREMENTS

The MSDA system is a mechanically scanned radiometric system attached to a spinning spacecraft. The basic requirements for the system are given in Table 2.0.

Table 2.0. Requirements for the MSDA System

Stowed Volume	4M Diameter Cylinder X 7 Meters Long
Stowed Resonant Frequency	25 Hz
Scanning Resonant Frequency	12 Hz
Platform Spin Rate	6 rpm
Conical Scan Axis	35°
Altitude	700 KM
Orbit	Sun-Synchronous
Aperture Size	15M
Operating Frequencies	1.4, 4.3, 5.1, 11 GHz
Beamwidth	1.03 (1.4 GHz), 0.35 (4.3 GHz) 0.3 (5.1 GHz), 0.35 (11 GHz)
Number of Beams in Track	5 (1.414 GHz), 11 (4.3, 5.1 GHz) 11 (11 GHz)
Beam Efficiency	90%
Surface Mesh Loss	<0.1 dB
Cross-Polarization	>28 dB

In addition to these basic requirements, the system must be dynamically balanced and capable of being launched in a single shuttle flight.

3.0 PRELIMINARY DESIGN

3.1 Stowed System Description

The stowed radiometer system, Figure 3.1, is mounted to the forward bulkhead of the spacecraft. The tower and reflector stow above the feed assembly. The reflector is supported both by the tower and by a pair of auxiliary support trusses (not shown) that reach from the forward bulkhead of the spacecraft to support the reflector hub.

3.2 Deployed System Description

The deployed radiometer system, Figure 3.2, consists of the spacecraft, with the feed/radiometer assembly attached, the tower support and deployment structure consisting of a four-bar linkage formed from a supporting truss and a screw-jack assembly, a deploying, rigid, three-sided tower, and the deployable reflector. The reflector surface forms a section of a paraboloid, 15 meters in diameter, starting 3 meters out from the vertex of the parent parabola. The entire rigid assembly, including the spacecraft, spins about the axis of the spacecraft, sweeping a 70 degree included-angle cone. In normal use, the feed points away from the Earth and the reflector collimates the beam and reflects it back toward the Earth. Thus, the rotation traces overlapping circles across its track along the ground.

To select this configuration, a trade between supporting the feed or reflector from the boom became apparent. By placing the feed on the spacecraft, the multiple horns are in close proximity to the receivers and on-board power supplies and processors. The weights of the reflector and feed are 225 and 184 lbs respectively, thus supporting the reflector from the boom or the feed from the boom present similar structural problems. Because of the advantages of having the feed in close proximity to the bus, the configuration as shown is selected. While this does not meet the 12 Hz fundamental frequency, the effects of lower stiffness is addressed in Section 4.0.

3.3 Deployment Sequence

The radiometer system reaches orbit with the tower and reflector stowed. Upon reaching orbit, the reflector support braces swing away, freeing the reflector. The screw jack then retracts, Figure 3.3-1, rotating the

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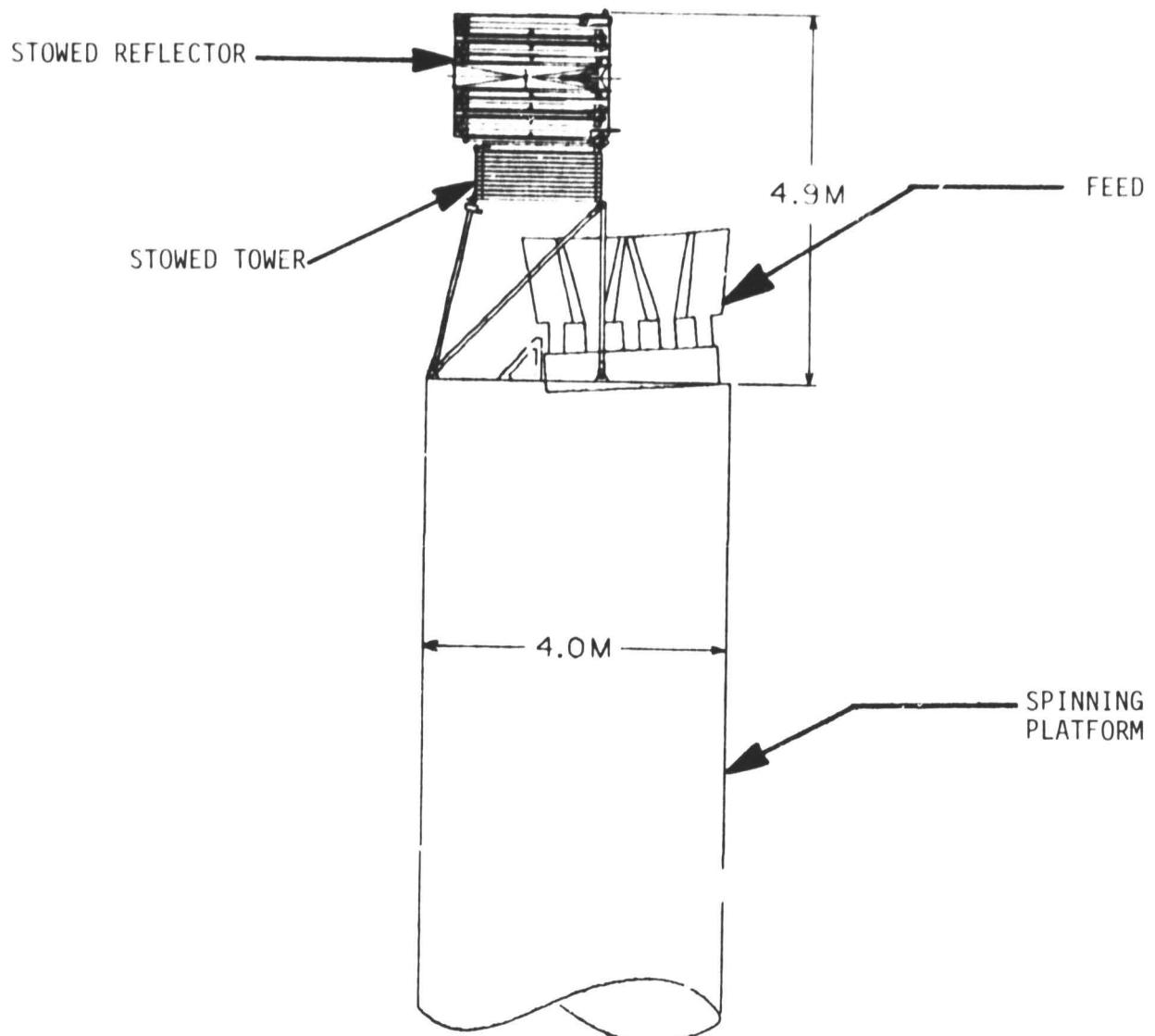


Figure 3.1. Stowed Radiometer System

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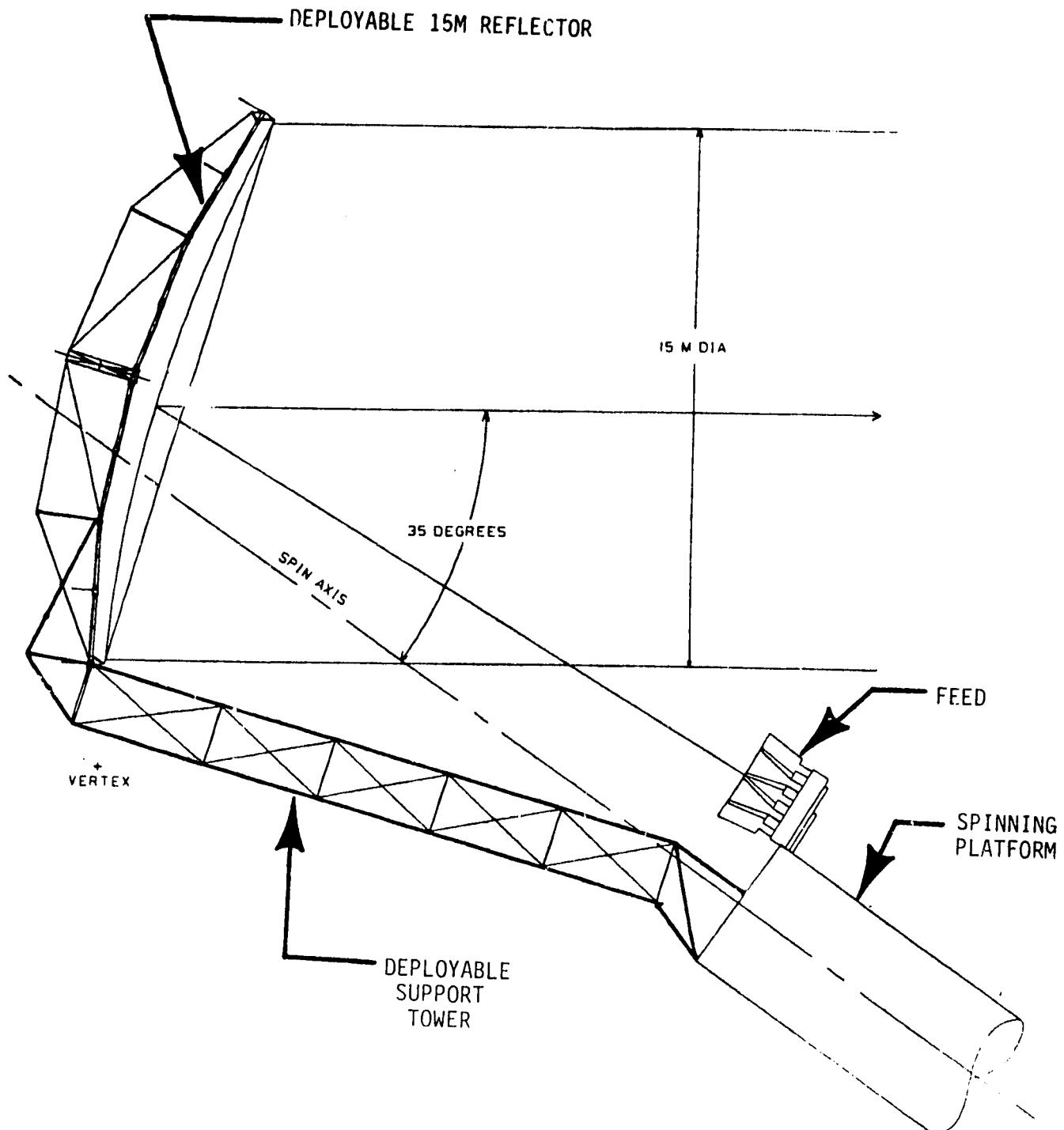


Figure 3.2. Deployed Radiometer System

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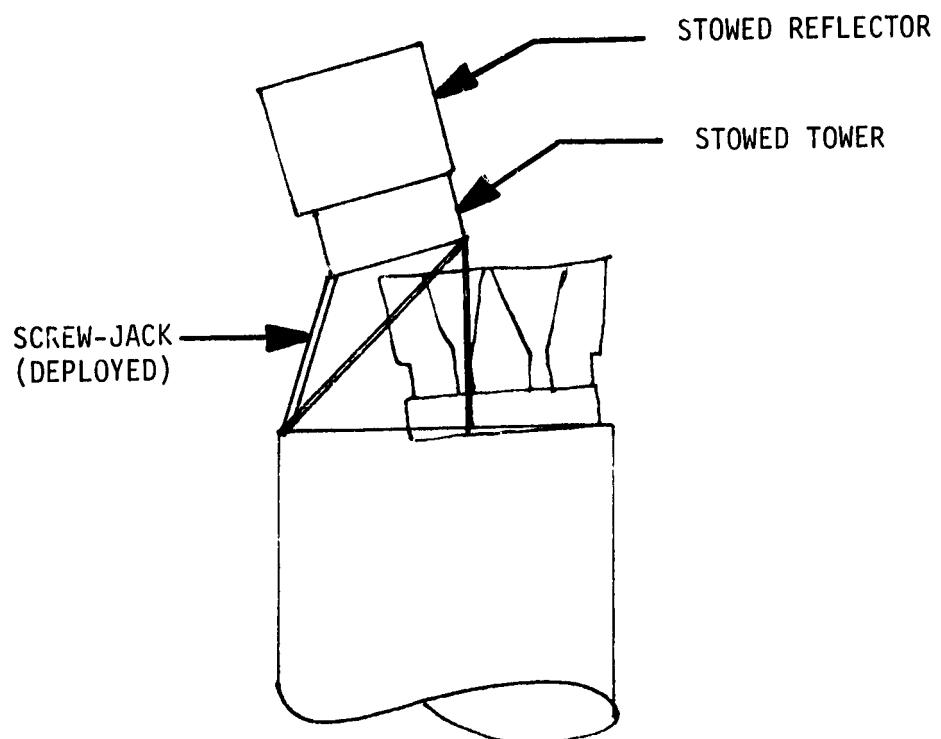


Figure 3.3-1. Tower is Rotated by Screw-Jack During First Stage of Deployment

tower and reflector to their final offset angle. The tower deploys, Figure 3.3-2, carrying the stowed reflector with it. The last section of the tower forms the transition between the triangular section of the tower and the two folded reflector ribs. Next, the reflector deploys, Figure 3.3-3. The reflector is deployed by the gearmotor and ballscrew assembly located in the hub. As the reflector unfolds, the rib-to-tower transition segments, located at the ends of two of the ribs, also unfold being driven and controlled by the same linkage that deploys the rest of the reflector. As deployment nears completion, two folded struts on each of the two reflector mounting ribs are pulled straight. As they come straight, the folding joints lock, making the struts rigid and capable of withstanding compressive loads. As the reflector deploys and the ribs separate, the last section of the tower opens laterally, completing the triangular section out to the reflector. Finally, the feed assembly deploys laterally, Figure 3.3-4, to its proper position with respect to the reflector. At this point, the radiometer system is a rigid assembly, capable of withstanding torsional and moment loads in any direction, and with its spin balance axis coincident with the centerline of the spacecraft.

3.4 Feed Preliminary Design

A sketch detailing the layout of the feed array appears in Figure 3.4-1. The circles represent the outer contours of the corrugated feed horns as viewed from the antenna along the principal axis. The vertical axis (y_f) in Figure 3.4-1 corresponds to the vertical feed axis appearing in the antenna system geometry sketch (Figure 3.4-2). Feed horns are numbered 1 thru 27 for simplification of identification. The coordinates of the geometric center of each feed, as measured in the feed plane (Figure 3.4-1), are listed in Table 3.4-1.

A corrugated conical horn is considered to be an ideal feed for a parabolic reflector system because of its high efficiency, nearly equal E- and H-plane beamwidths, and a wide frequency bandwidth. Typically, at C-band or higher frequencies, the entire horn is made from aluminum, either cast or machined in sections. At L-band the horn can be fabricated from aluminum sheet. The latter technique requires each corrugation ring to be machined separately, then inserted into an aluminum cone. The corrugation depth of each feed is

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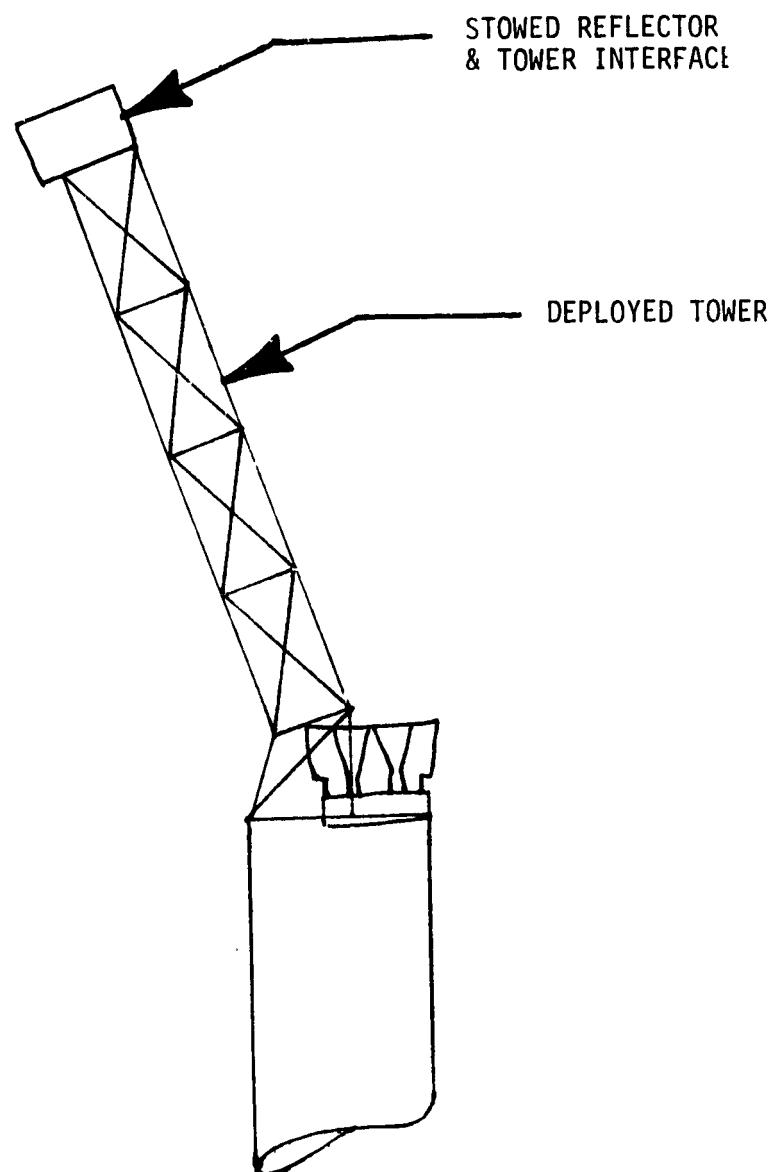


Figure 3.3-2. Tower Deploys and attaches to Support Reflector

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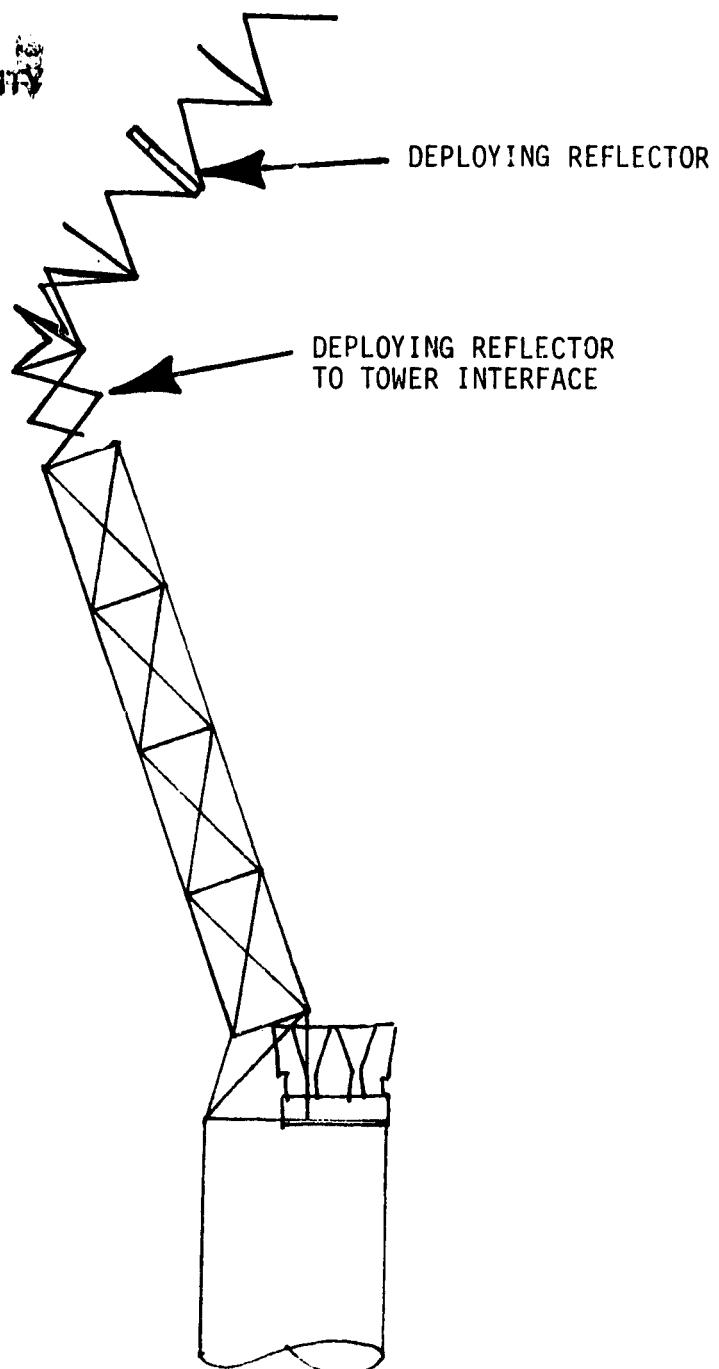


Figure 3.3-3. The Deploying Reflector Drives the Tower Interface

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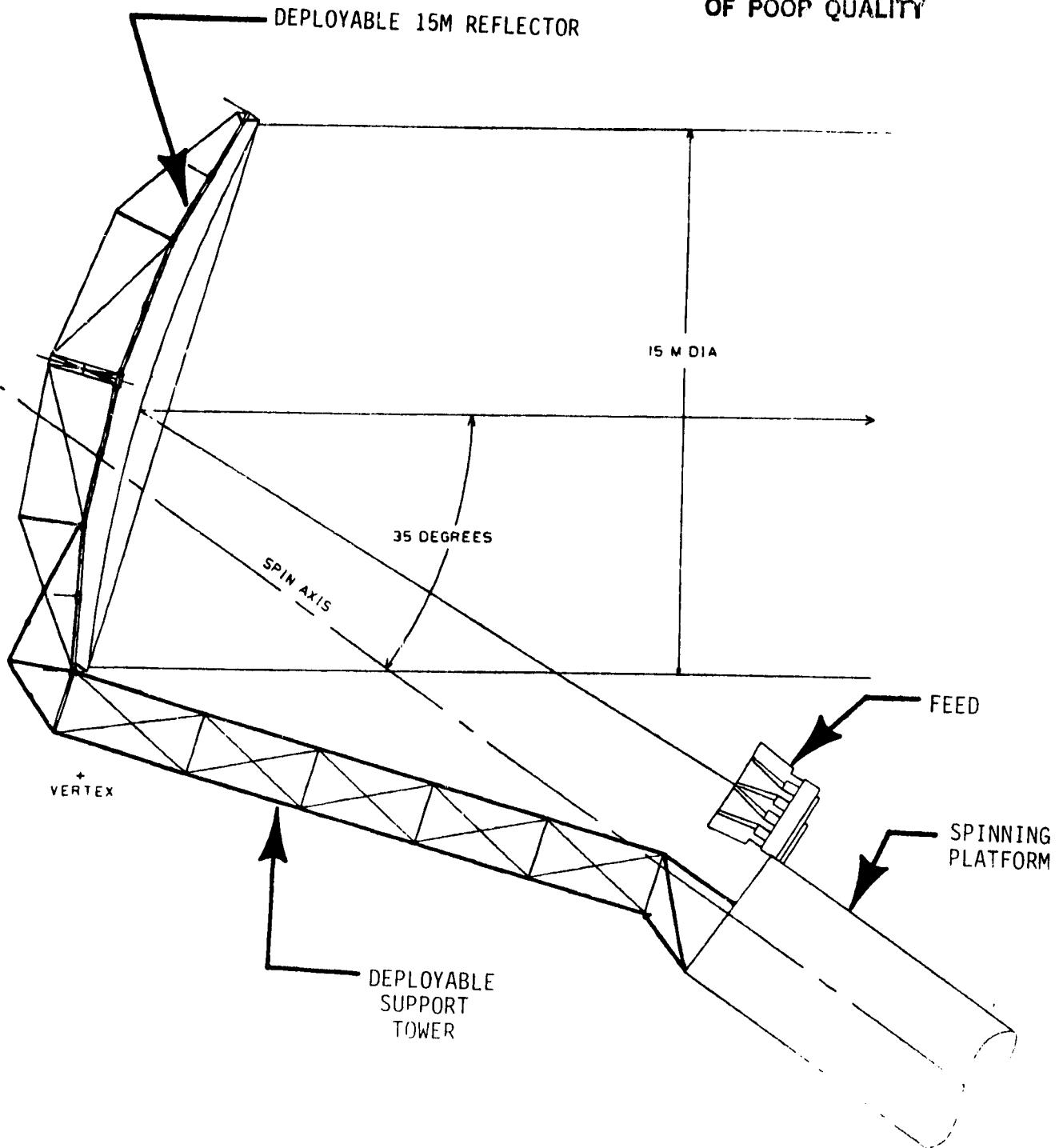


Figure 3.3-4. The Feed Slides Out and Latches In-Place

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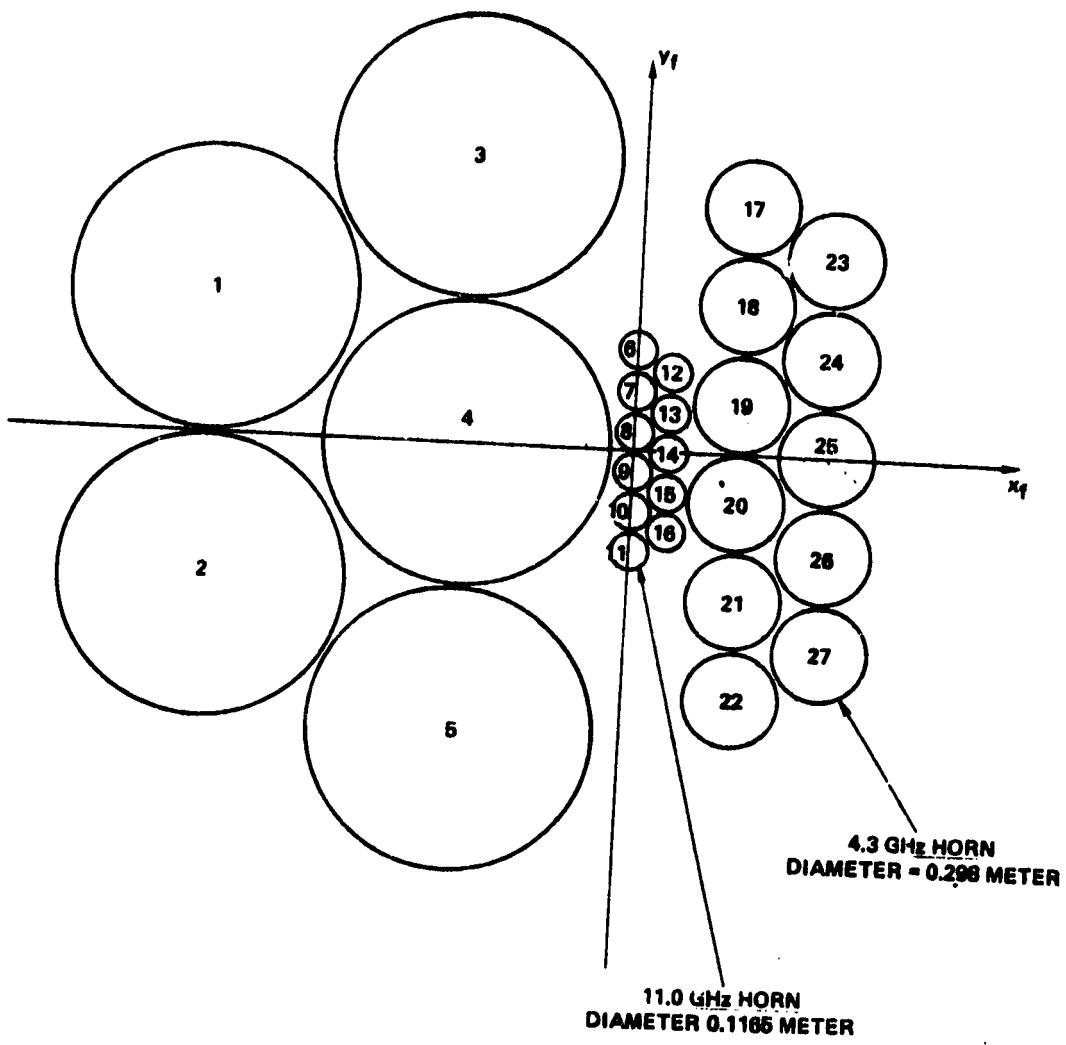
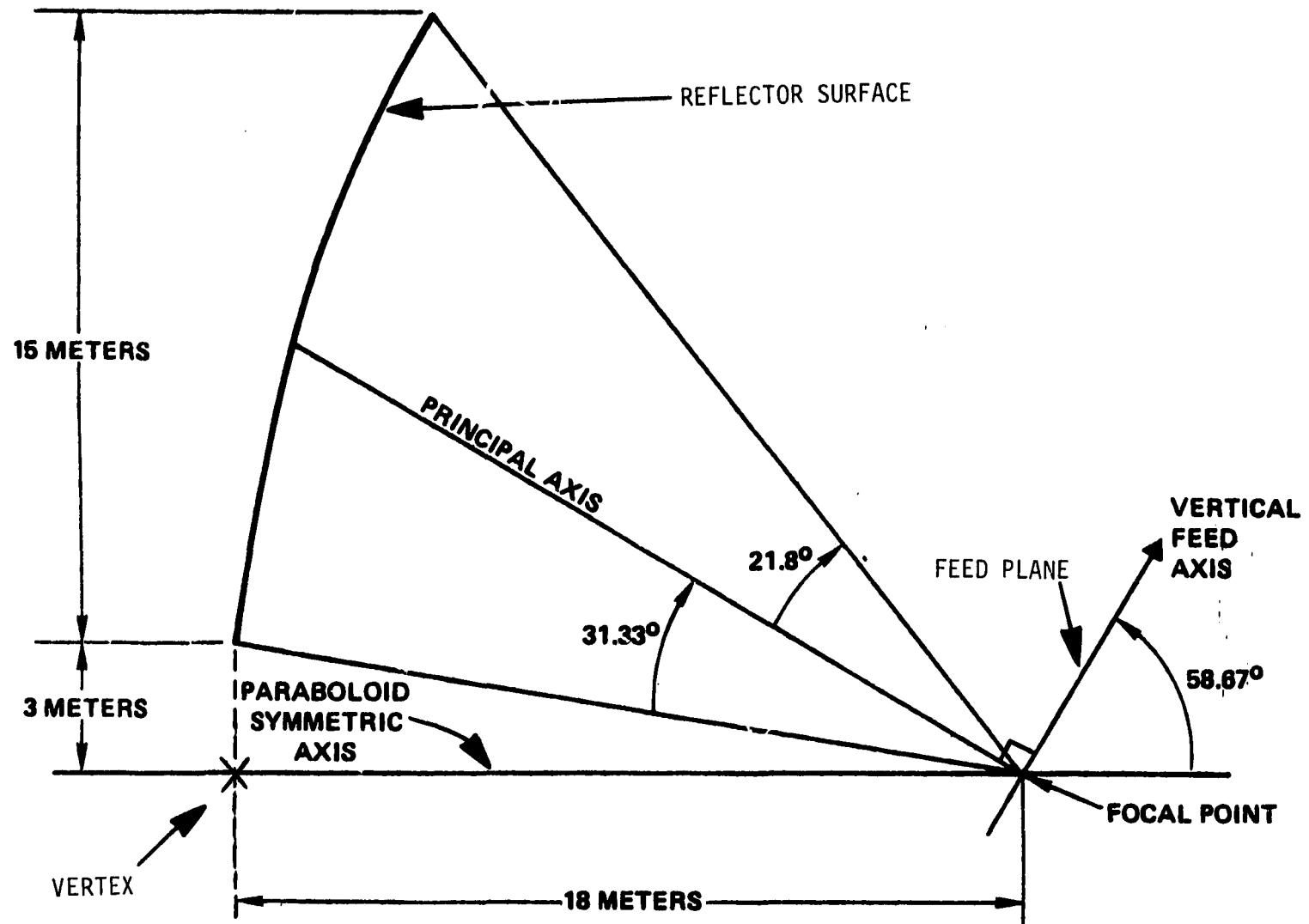


Figure 3.4-1. Feed Array Layout

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Figure 3.4-2. Antenna System Geometry

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Table 3.4-1.

Feed Number	X_f -Displacement (meters)	Y_f -Displacement (meters)
1	-1.300	0.455
2	-1.300	-0.455
3	-0.513	0.909
4	-0.513	0.000
5	-0.513	-0.909
6	0.0	0.291
7	0.0	0.175
8	0.0	+0.058
9	0.0	-0.058
10	0.0	-0.175
11	0.0	-0.291
12	0.101	0.233
13	0.101	0.117
14	0.101	0.000
15	0.101	-0.117
16	0.101	-0.233
17	0.308	0.745
18	0.308	0.447
19	0.308	0.149
20	0.308	-0.149
21	0.308	-0.447
22	0.308	-0.745
23	0.566	0.596
24	0.566	0.298
25	0.566	0.000
26	0.566	-0.298
27	0.566	-0.596

assumed to be $3/8\lambda$. The remaining physical dimensions are listed in Table 3.4-2, with an associated sketch in Figure 3.4-3. It should be noted that the length, L, of the horn is approximate in that it is calculated assuming a circular waveguide radius of 0.5λ . Other horn types such as the Potter horn can be useful for this application at 1.4 GHz and 11.0 GHz due to the narrowband performance required. It should be noted that in this preliminary design, the 11.0 GHz horns produce a 0.16° beamwidth. Ways of increasing the beamwidth to 0.35° are discussed in Paragraph 4.4.

3.5

Tower Design

The design requirements of the deploying tower are as follows:

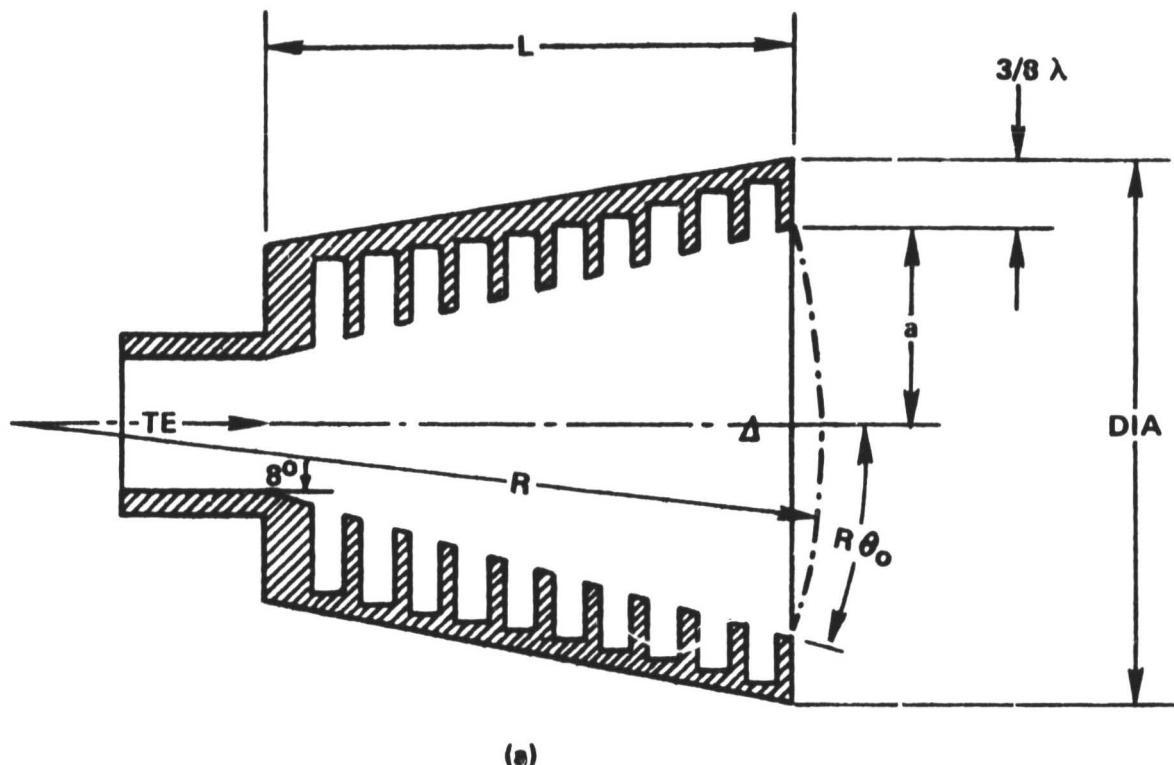
- Small stowed package (25 inch height envelope)
- High stiffness (dynamic loads)
- Structural capability during deployment (stiffness of partially open structure)
- Repeatable joints (repeatable tower length)
- No rotation during deployment (electrical interfaces)

The proposed tower design meets all of these requirements and creates a stable link between the reflector and the spacecraft (Figure 3.5-1). The tower design was developed by HGESD on IR&D Program No. 82-4150. On this IR&D program a breadboard model of the tower design has been built and tested. Figure 3.5-2 shows the tower model. The tower is constructed of four identical structural bays and one adapter bay. Tower bay dimensions and element descriptions are shown in Figure 3.5-3. The tower is a folding triangular truss structure, that deploys as shown in Figure 3.5-4. Note that the basic tower design is easily scaled to fit a wide range of applications and requires no built-in twist during deployment. These features make it more attractive than an astromast type design.

During deployment the longerons unfold and latch at joints in the center and at each bay interface. As all three longerons unfold simultaneously, the upper and lower bay platforms move farther apart, increasing bay height. When the tower is stowed, the rod diagonals are elastically buckled outward into a circular arc. This stored energy is used to deploy the tower. The longerons are stowed along side the platforms, from corner to corner. Deployment of the tower is controlled by a central lanyard as depicted in Figure 3.5-5. Addition of delatch cords also allows restow of the tower if required.

Table 3.4-2. Feed Geometry

<u>1.414 GHz Horn</u>		<u>4.3 GHz Horn</u>	<u>11.0 GHz Horn</u>
a	= 0.375 meter	a	= 0.123 meter
R	= 1.60 meter	R	= 0.526 meter
θ_0	= 13.555°	θ_0	= 13.52°
Δ	= 0.21 wavelength	Δ	= 0.209 wavelength
D_{1A}	= 0.909 meter	D_{aA}	= 0.298 meter
L	= 1.33 meter	L	= 0.439 meter



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Figure 3.4-3. Corrugated Feed Horn Geometry

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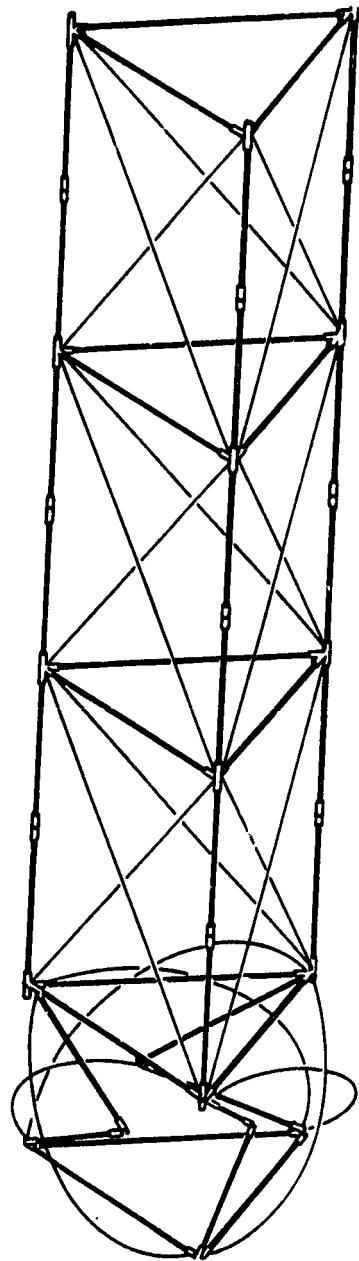


Figure 3.5-1. Five Sections of the Deployable Tower Form the 18M Tower

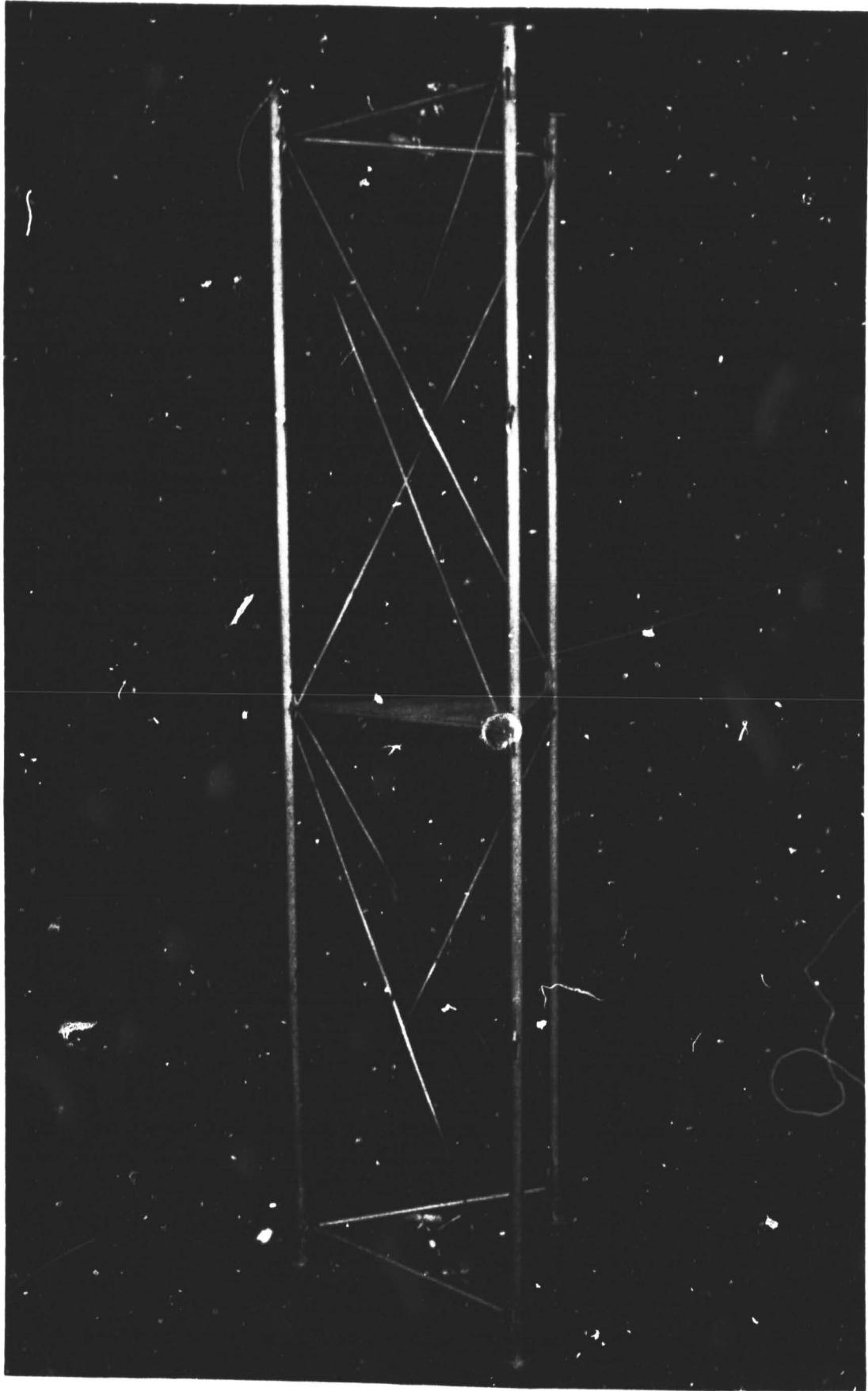
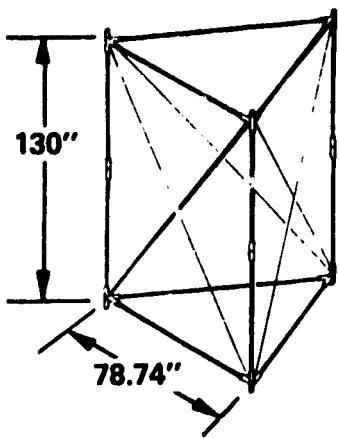


Figure 3.5-2. The Tower Design Has Been Built and
Tested on IR&D Program No. 82-4150.



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LONGERONS

2.0 INCH OD

0.060 INCH THICK GFRP

PLATFORM MEMBERS

1.0 INCH OD

0.020 INCH THICK GFRP

LONGERON AND PLATFORM GFRP

MODULUS E = 18×10^6 PSI

CTE = $0.1 \times 10^{-6}/^{\circ}\text{F}$

($0^{\circ}_2, +50^{\circ}$ HMS LAYUP)

DIAGONALS

0.025 INCH OD GFRP ROD

MODULUS E = 29×10^6 PSI

CTE = $-0.12 \times 10^{-6}/^{\circ}\text{F}$

TOWER PROPERTIES

BENDING STIFFNESS, EI = 2×10^{10} PSI

AXIAL STIFFNESS, EA = 2×10^7 LB

BENDING, $M_{CR} = 1.96 \times 10^5$ IN-LB*

COMPRESSION, $P_{CR} = 2530$ LB*

WEIGHT = 120 POUNDS

TORSIONAL STIFFNESS = 0.5×10^6 IN*/RAD TOTAL TOWER

*LOCAL LONGERON CONDITION

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Figure 3.5-3. Tower Design and Performance Parameters

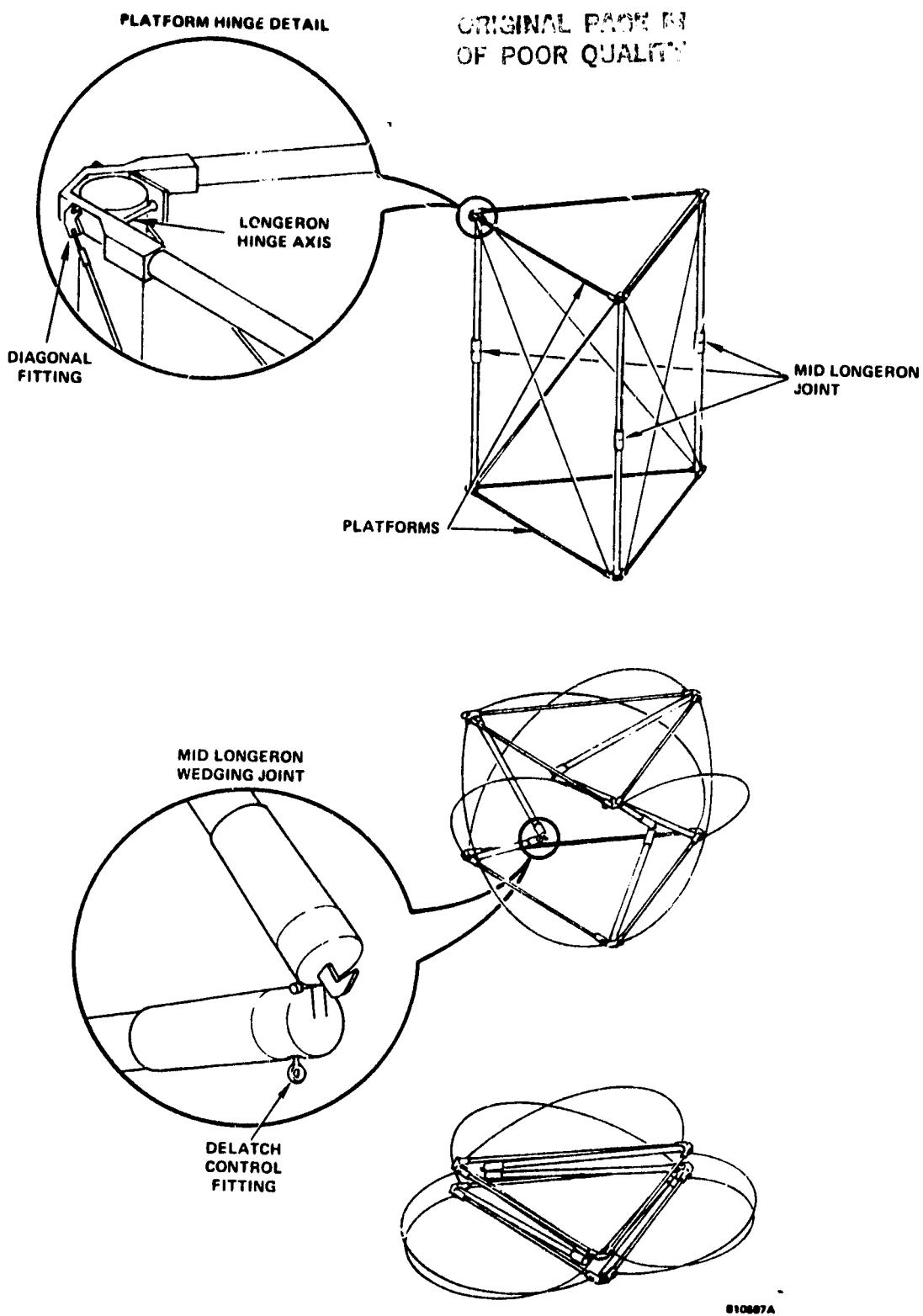
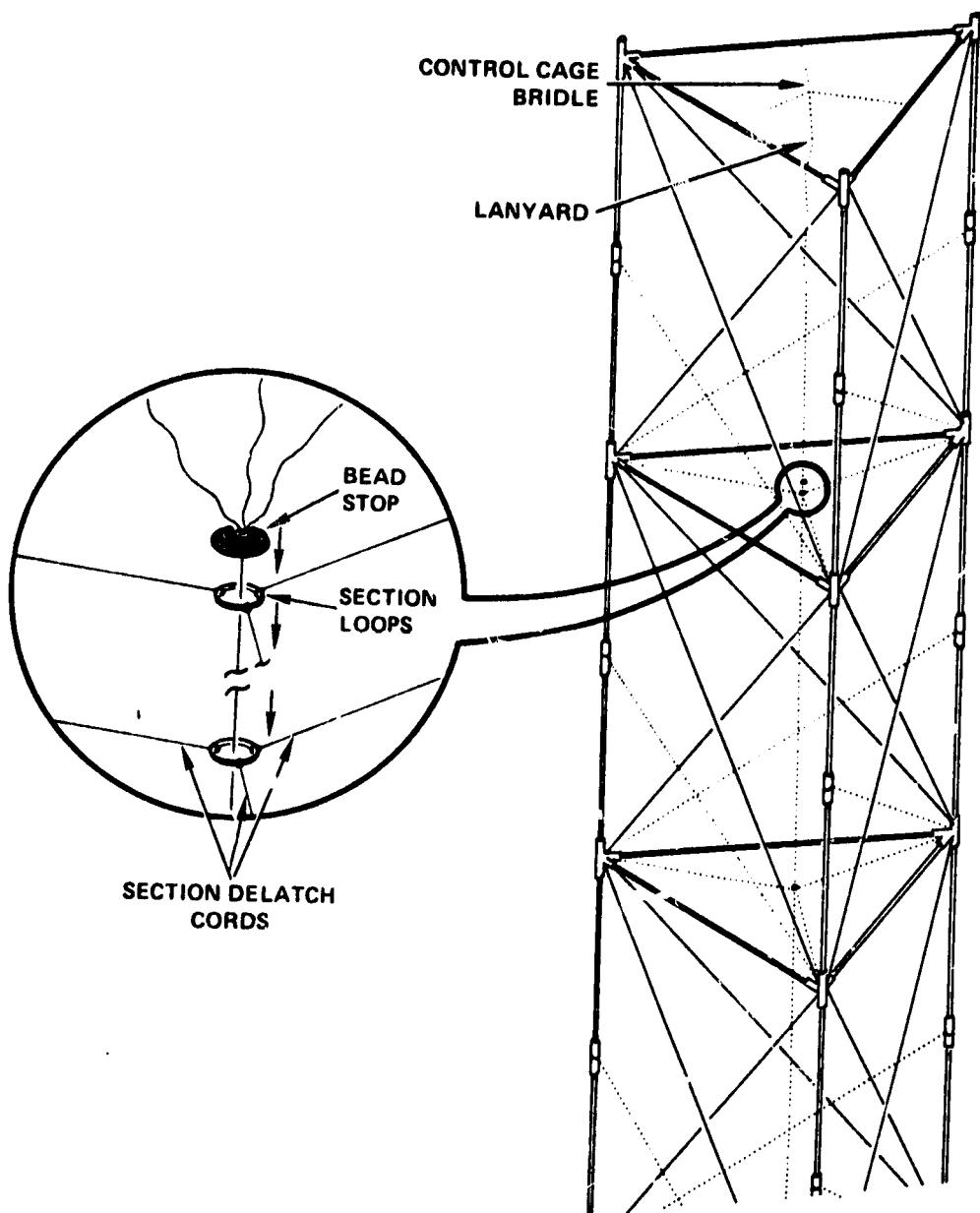


Figure 3.5-4. Tower Deployment Sequence

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Figure 3.5-5. A Central Lanyard Controls Deployment of the Tower Sections.

3.6

FRR Reflector Design Description

Figure 3.6 illustrates the basic Folded Radial Rib Reflector (FRR). The FRR concept uses a highly efficient truss design to provide a high FRR stiffness to weight ratio. The rib structure of the truss is segmented with articulating joints to give a compact stowed package. This design is then mated with the mesh surface design as used on the TDRSS antenna. The potential benefits of the concept are:

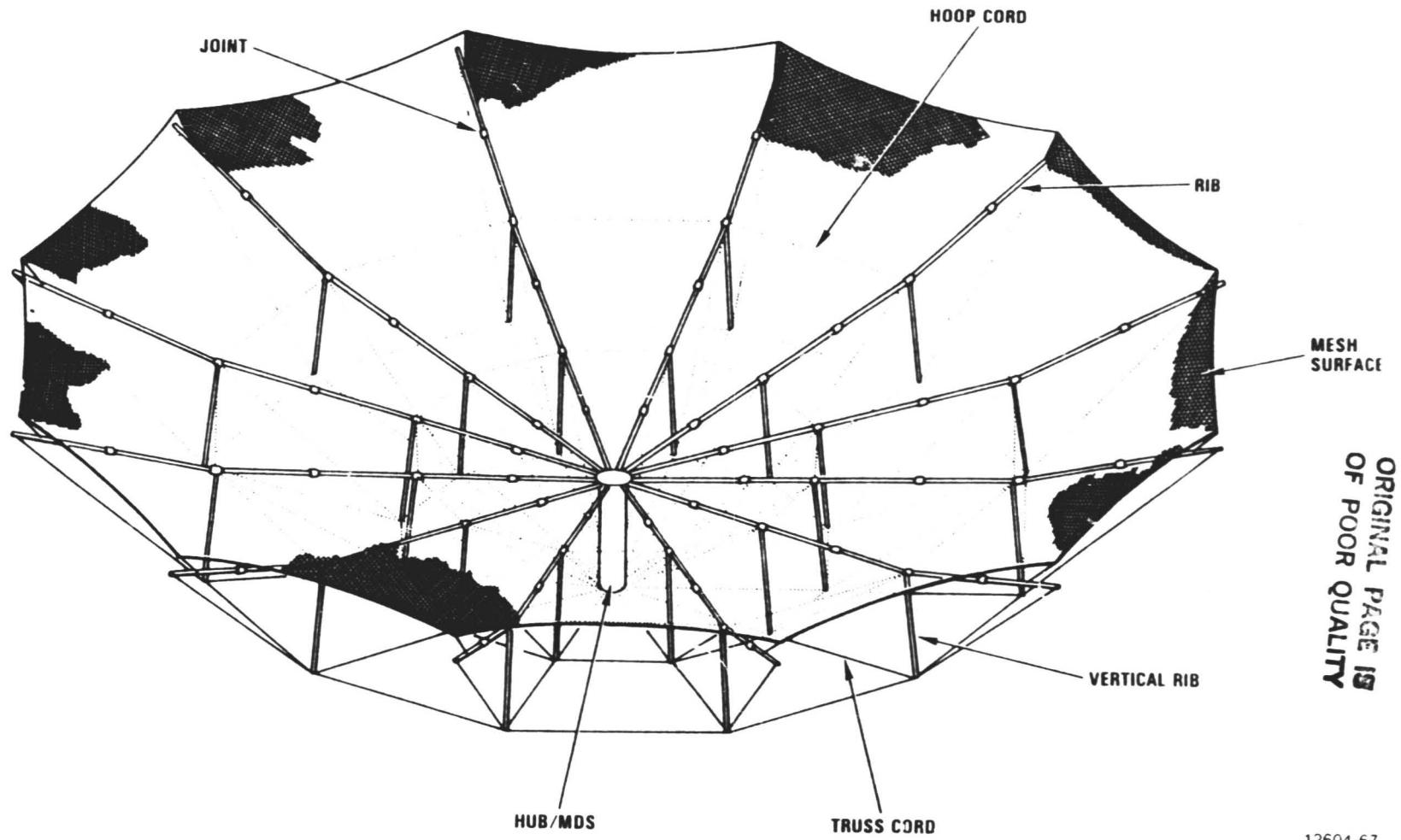
- Compact Packaging
- High Reflector Surface Accuracy
- High Stowed and Deployed Stiffness
- Low Weight
- Low Moments of Inertia
- Slow, Motor Controlled Deployment

3.6.1

FRR Structure Design

The baseline FRR design, illustrated in Figure 3.6.1-1 shows the elements of the truss rib as well as the members which connect adjacent ribs. Figure 3.6.1-2 shows the side view of a single rib attached to the reflector hub. Latching joints are shown at two locations, inboard and outboard of the intersection of the radial rib members and the compressive, vertical strut. These latching joints must lock to form inboard and outboard rigid members. The non-latching joint between them remains free to rotate in the plane of the truss preserving the structural characteristics of the pinjointed truss. These joints are discussed later in this paragraph.

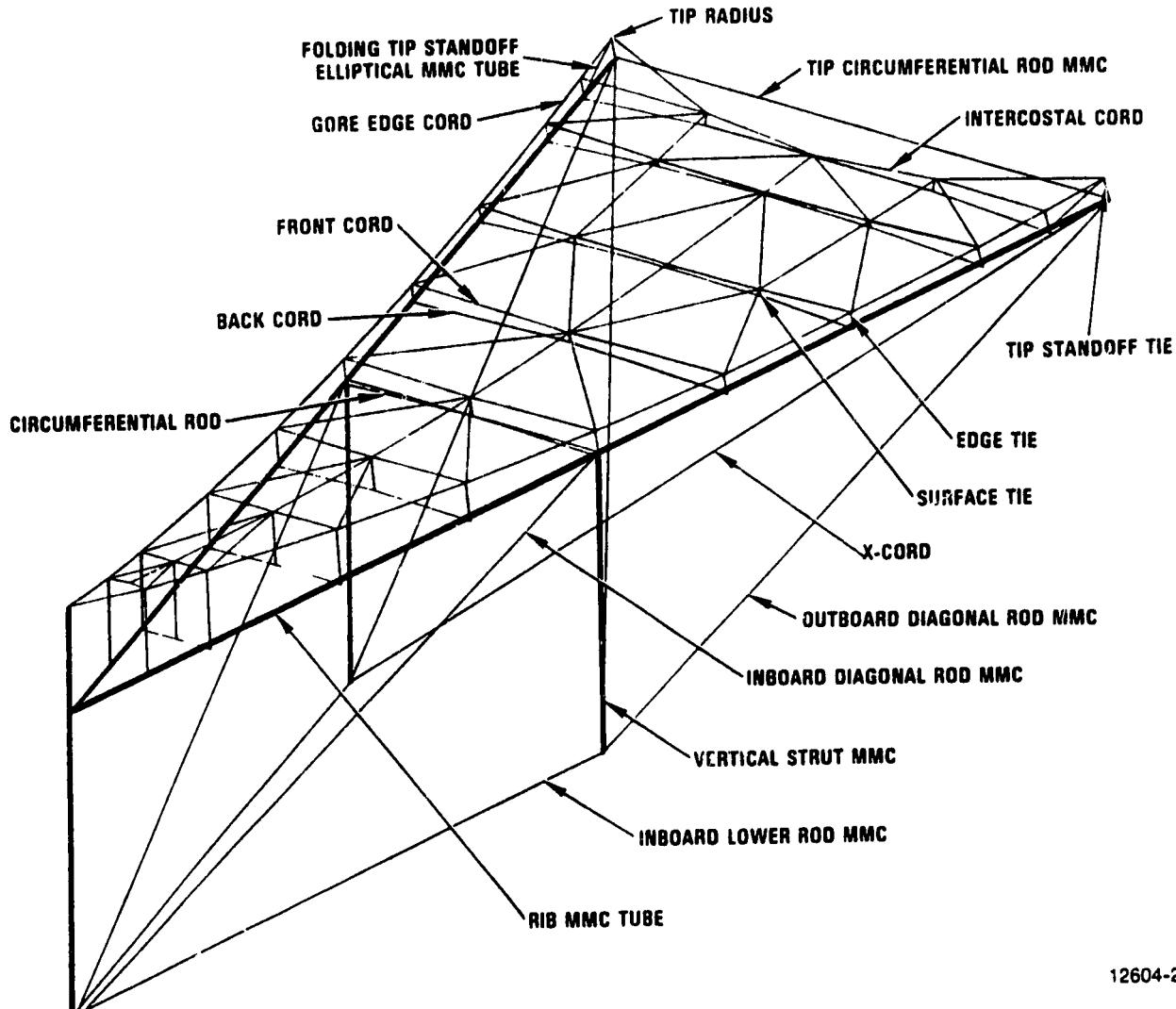
Figure 3.6.1-2 also shows the location of joints in the solid, graphite composite rods which form the truss. The placement of these joints is selected to allow the truss to fold and deploy with only planar motion. Figures 3.6.1-3 through 3.6.1-5 illustrate the FRR rib deployment sequence. Small clips, or rod guides, attach to the main structural members and joints to support the tension rods while stowed. The deployment of the rib pulls the rods free from the rod guides. As discussed previously, a four-bar linkage connecting the radial rib members synchronizes and controls the deployment.



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Figure 3.6. Basic Folded Radial Rib Antenna

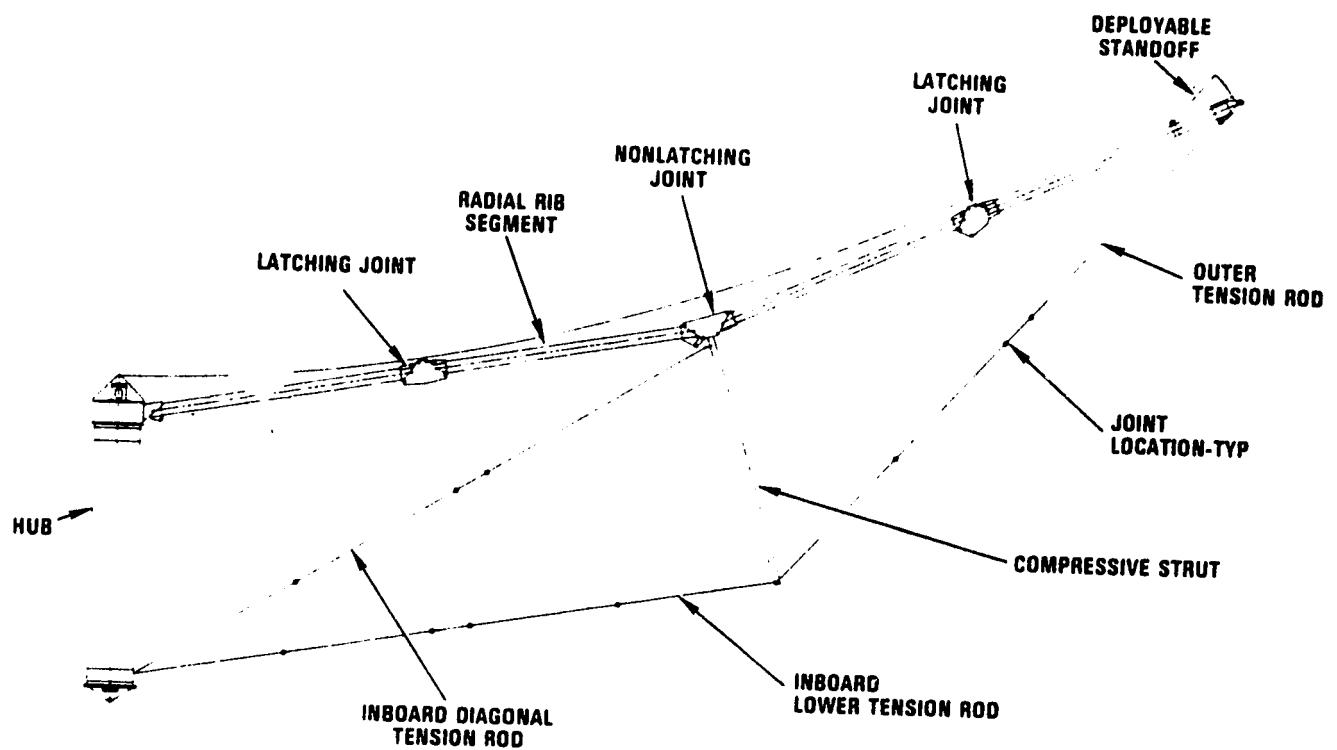
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Figure 3.6.1-1. FRR - Two Rib Geometry and Materials

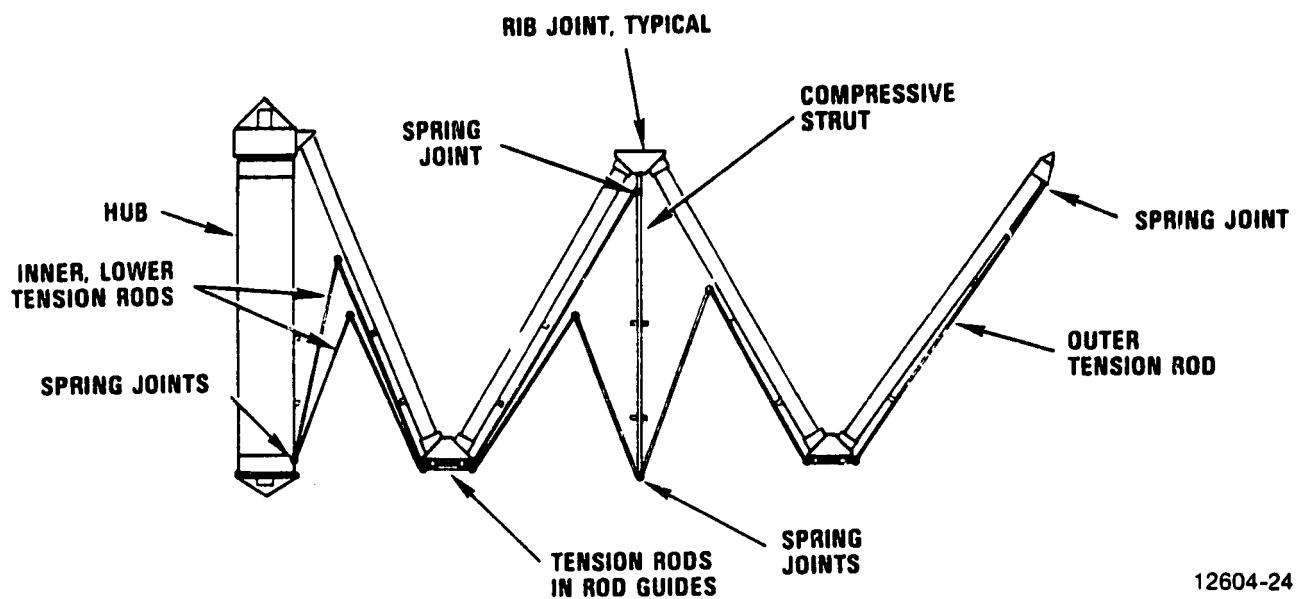
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Figure 3.6.1-2. FRR - Single Truss (Side View)

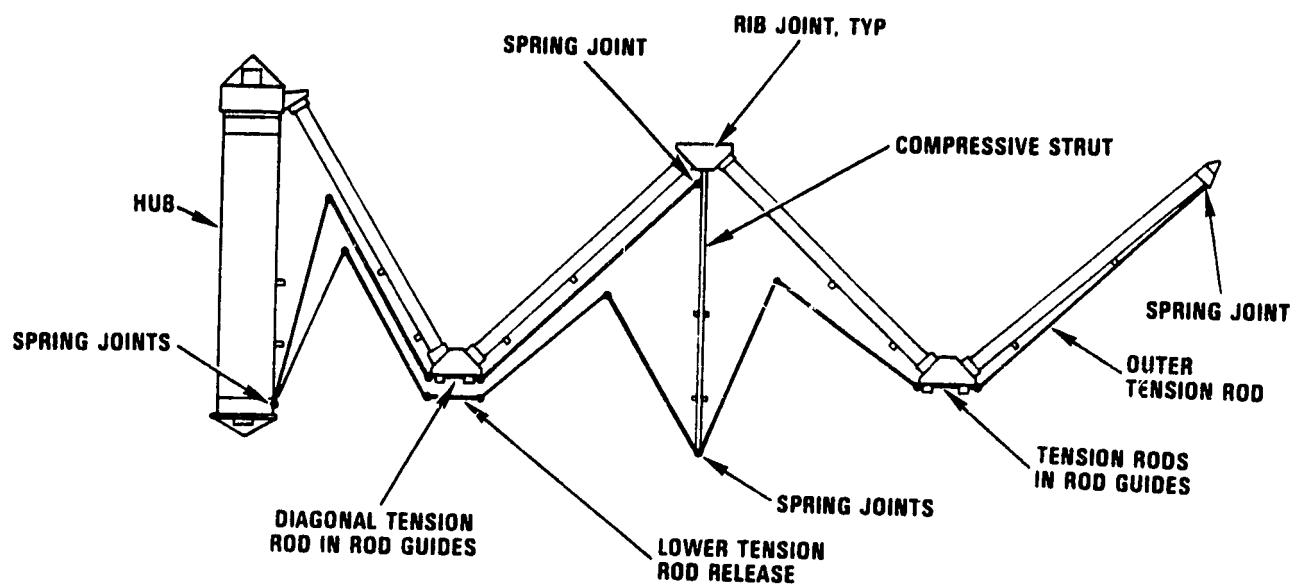
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Figure 3.6.1-3. Rib Deployment Initial Phase

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Figure 3.6.1-4. Rib Deployment Sequence Intermediate Phase

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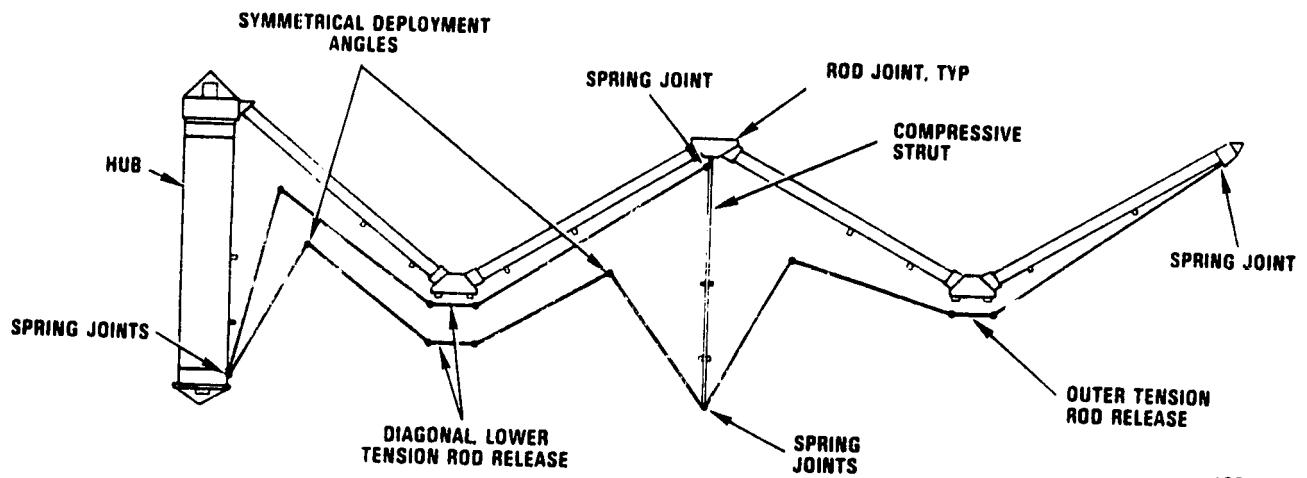


Figure 3.6.1-5. Rib Deployment Sequence - Final Phase

Figure 3.6.1-6 shows the 12-rib structure fully stowed. Mesh and surface cords have been omitted for clarity. In this position all tension rods are folded and held in the tension rod guides. Deploying standoffs at the rib tips are held parallel to the ribs by clips.

The rib launch restraint design is shown in Figure 3.6.1-7. The restraint spoke attached to the rib tip and outer joint is made from a titanium cable with a ball fastened to the free end. These balls are held inside sockets during a deployment sequence by actuation of non-explosive initiators in the restraints. The spokes (with balls) remain attached to the rib, but do not interfere with the reflective surface. The proper preload in the spokes, while stowed, locks the ribs together. This concept has been successfully used in the Tracking and Data Relay Satellite Antenna.

The Mechanical Drive System (MDS) controls the deployment of the reflector. It is located at the upper end of the hub (see Figure 3.6.1-8) and is attached to the innermost radial-rib member. Deployment force is transmitted to the other three radial members by the four-bar linkage. Tension rods are pulled free from the tension rod guides and clips by the rib action. Figure 3.6.1-9 shows more detail of the MDS with the right-half stowed and the left-half deployed. A threaded carrier, moved by the drive screw rotation, is shown in both positions. Linkages drive the 12 ribs to their deployed positions simultaneously. Once fully deployed with the inner and outer rib joints latched, the rib assumes the characteristics of a pinned-end truss. Restowing the reflector is possible by releasing the latched joints and reversing the drive motor. Restowage on-orbit is not a requirement of the anticipated mission application, but is valuable for ground handling capability.

The proposed latching joint for the radial rib members is shown in Figure 3.6.1-10. The mechanism is similar to a compass divider where the drive link roller slides inside tracks. This results in symmetric deployment of the link rollers. It is lightweight and has a high deployed stiffness when fully preloaded. Latching is accomplished by the overcenter travel of the drive link roller. This same joint can be constructed to be nonlatching by preventing the overcenter travel. Figure 3.6.1-11 illustrates the deployed joint.

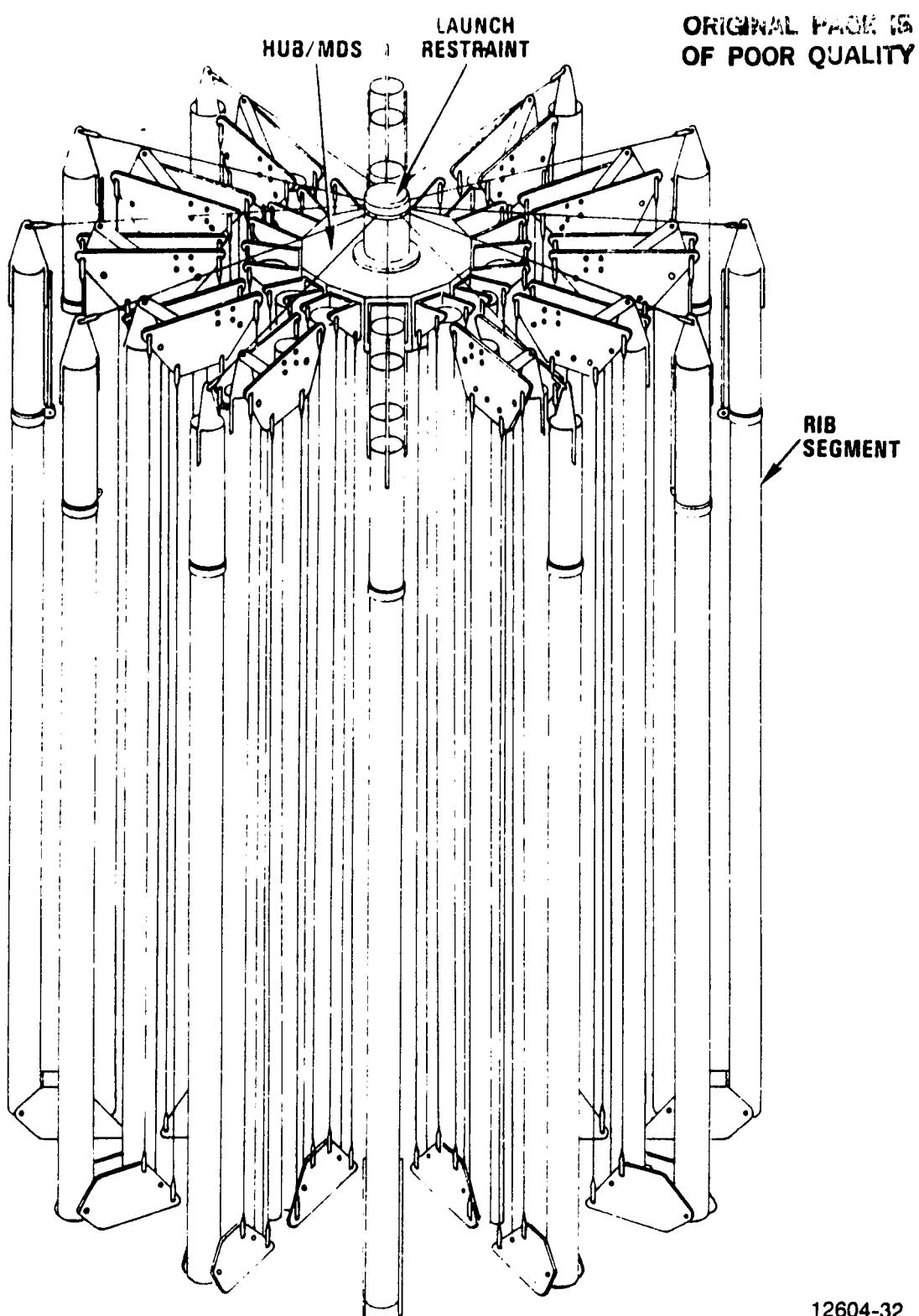
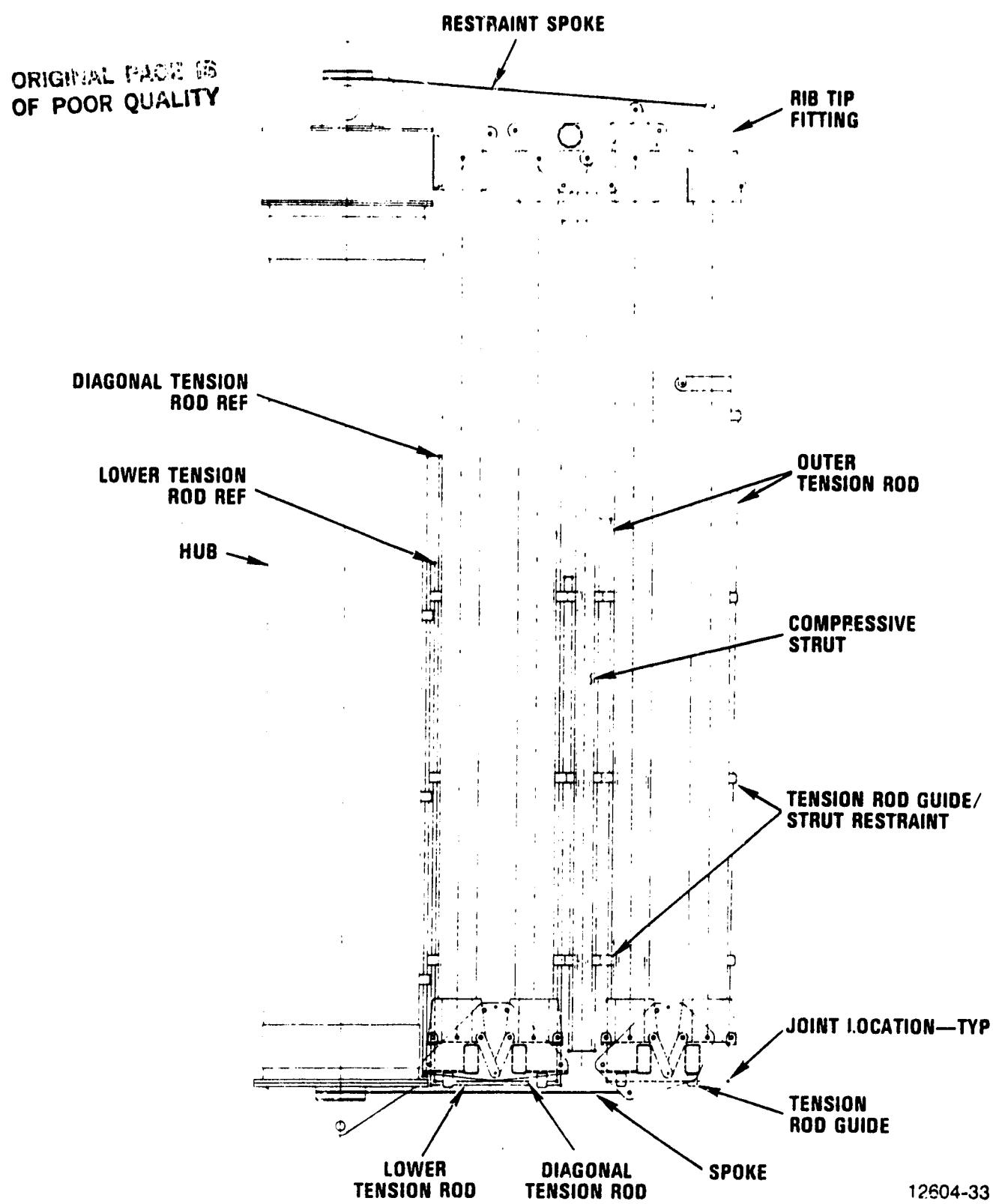


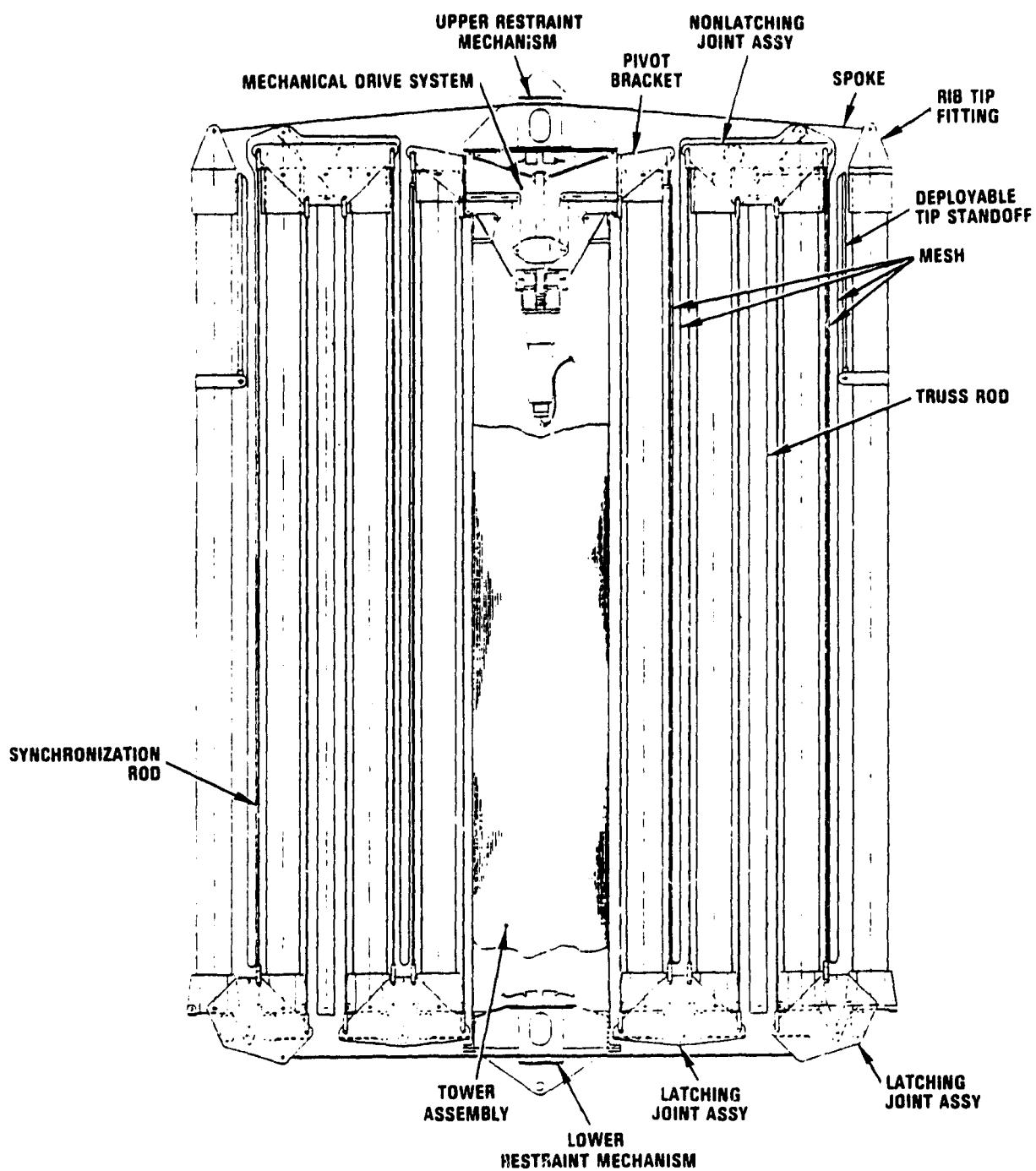
Figure 3.6.1-6. FRR Stowed Reflector (Shown Without Mesh)



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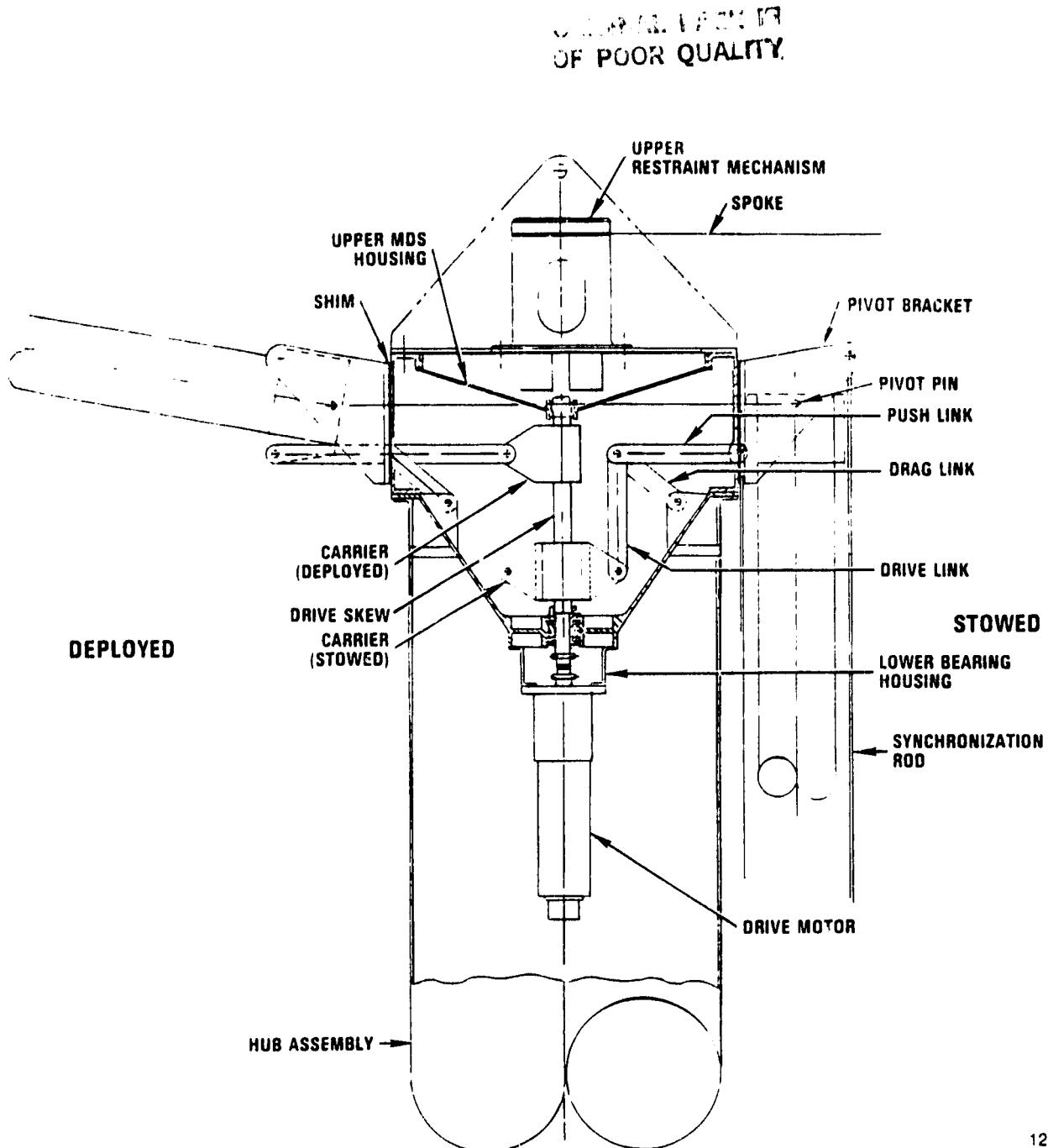
Figure 3.6.1-7. Rib Launch Restraint Design

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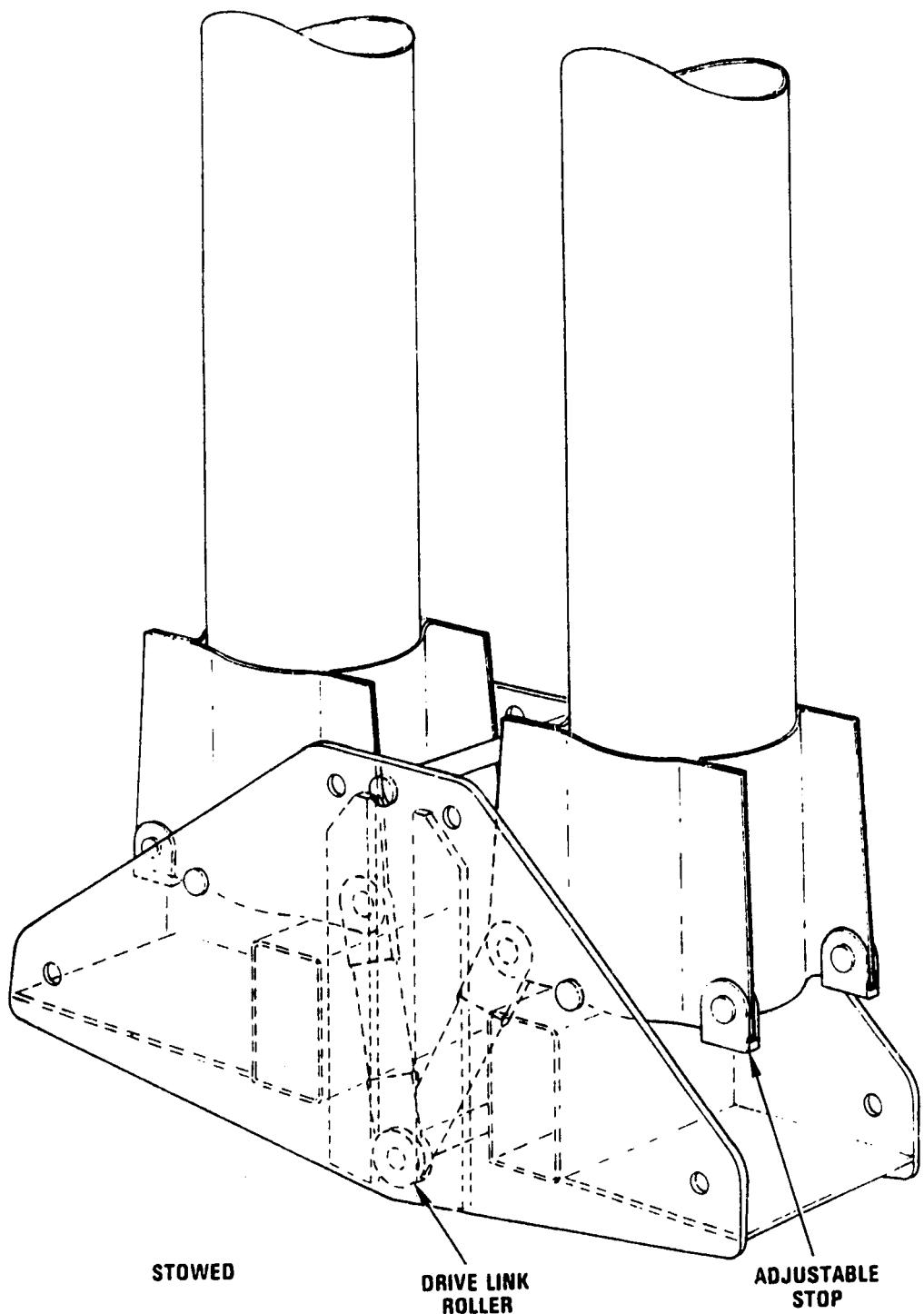
Figure 3.6.1-8. FRR - Stowed Antenna Assembly (Section)



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Figure 3.6.1-9. FRR - Mechanical Drive System and Restraint Mechanism

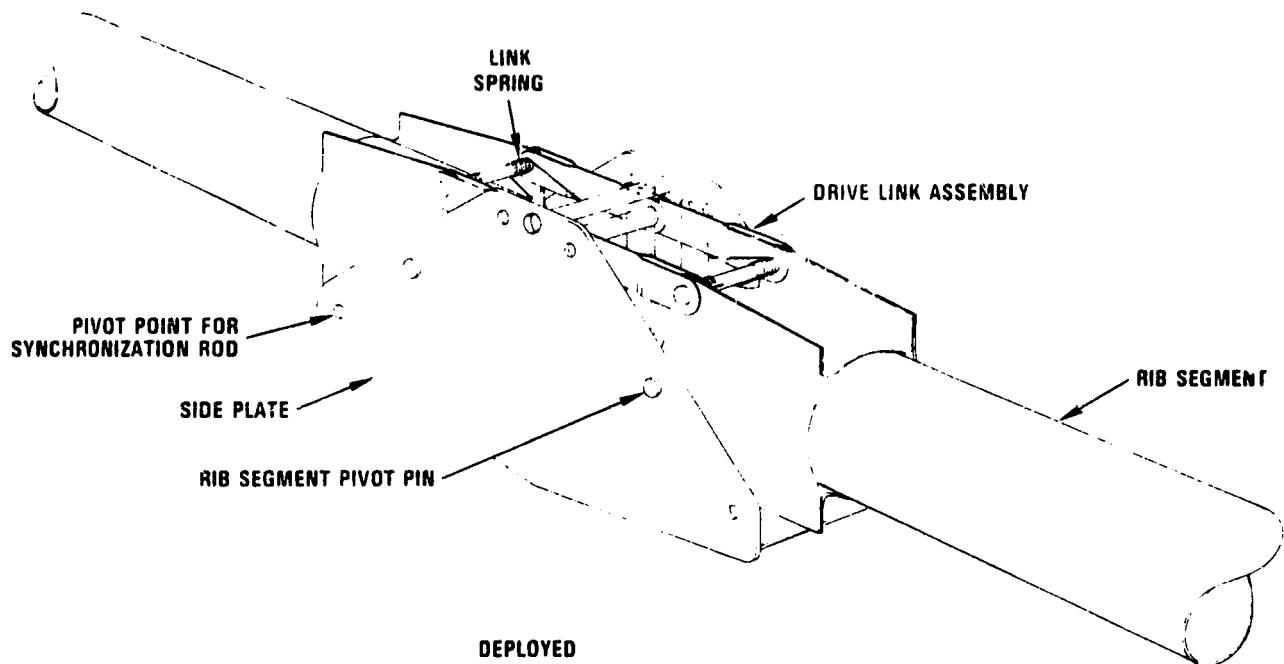
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Figure 3.6.1-10. Latching Joint, Stowed Position

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Figure 3.6.1-11. Latching Joint Deployed (Operational) Position

3.6.2

Surface Design

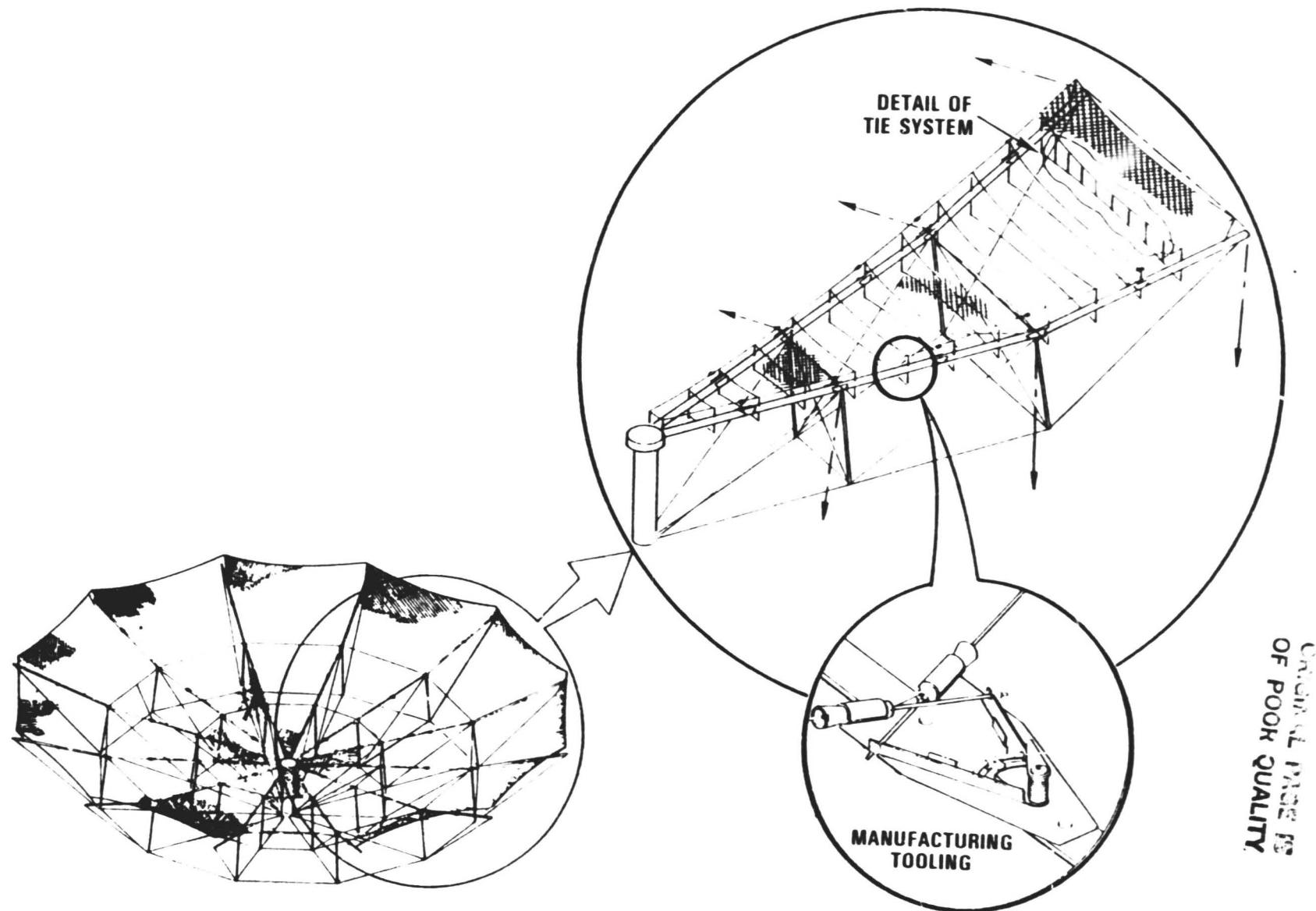
The surface design used on the FRR structure is a dual drawing surface system. The design involves the placement of a secondary structure behind the primary reflective surface and joining the two with a sufficient number of ties to achieve the desired surface accuracy. Figures 3.6.2-1 and 3.6.2-2 illustrate the dual drawing surface concept, showing the placement of the connecting ties.

The implementation of this surface involves the use of a gold plated mesh to form the reflective surface, multistrand graphite cords to create the surface contour, graphite epoxy strips to establish gore boundaries, and adjustable standoffs by which the reflective surface assembly is attached to the graphite radial ribs. The reflective mesh is a 0.0012 inch diameter gold plated molybdenum wire knitted into a tricot pattern with ten openings per inch. Molybdenum with its high strength, low coefficient of thermal expansion, and excellent plating characteristics results in a highly reflective surface with relatively low tensions, good resistance to handling, and minimal thermal interaction with the graphite cord and graphite rib supporting structure. Pre-plating with gold assures minimal interfilament friction with uniform, optimum thickness for RF reflectivity. The tricot knit is most familiar as the double-knit fabrics that are popular for their ability to "give" in two directions without unravelling at the edges or with broken strands.

Structural and RF properties of the mesh are discussed in Section 4.0.

Multistrand graphite cords are used to form a thermal insensitive substructure which combines with the GFRP ribs to form a foundation for the mesh. The circumferential arrangement of cords increases the effective resistance of the ribs to axisymmetric loading produced by thermally induced mesh tension variations. The negative thermal coefficient of expansion of the cords interacts with the rib and mesh thermal properties to produce a near optimum condition for thermal stability.

Cords on the front (feed) side of the reflector are drawn into the desired parabolic contour by connecting these front cords to a parallel set of cords located behind the ribs through a number of Beta-glass ties. The ties are made of Beta-glass to provide a measure of handling strength (15 pounds tension) and for ease of joining.



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Figure 3.6.2-1. The Contour and Contour Attachment Design Utilizes Technology from the TDRSS Program

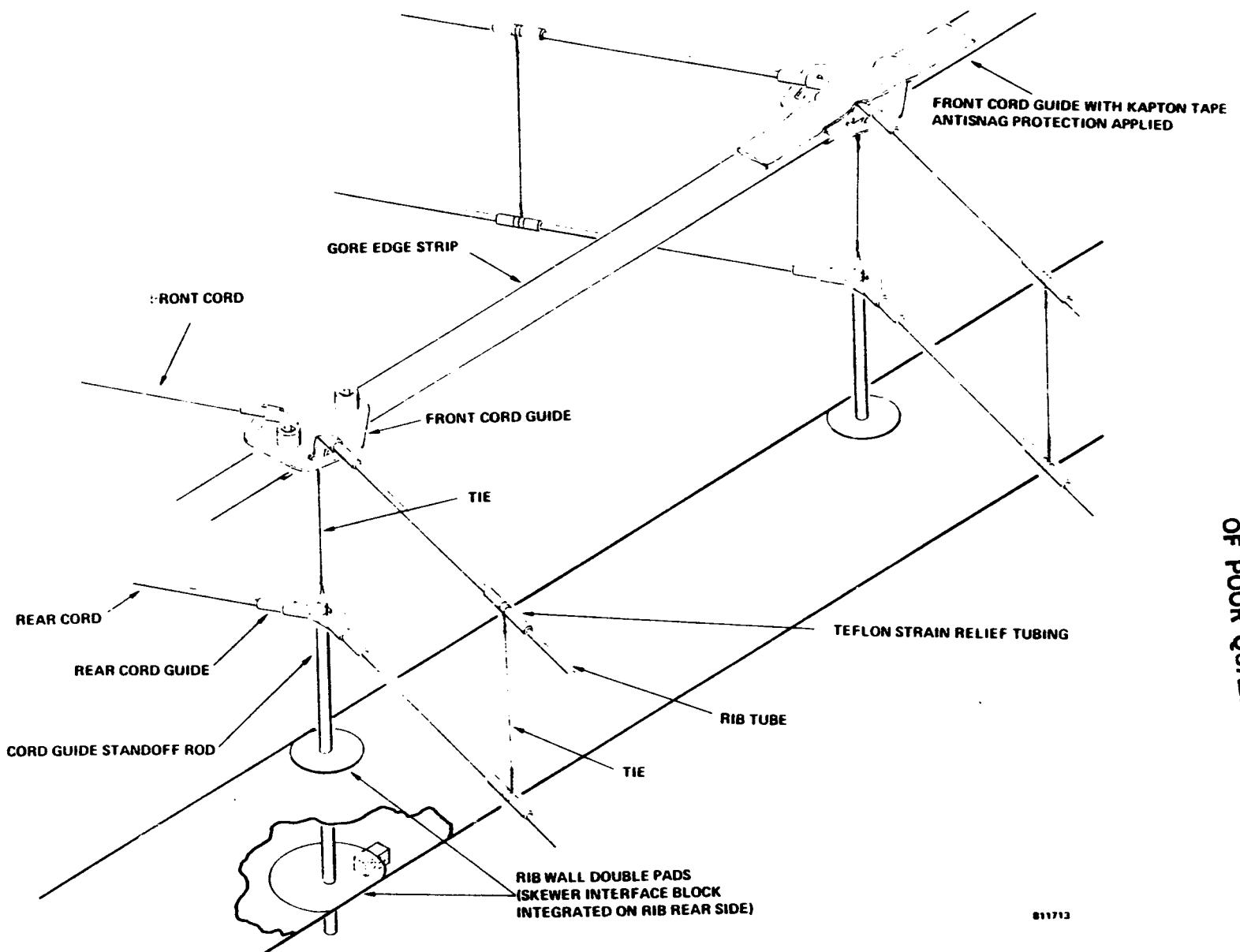


Figure 3.6.2-2. Rib Segment and Cord Interfaces

The mesh is bonded to unidirectional graphite strips over each rib. Strips from adjacent gores are overlapped with a mesh-to-mesh interface, riveted together, and suspended by rib standoffs. A deployable standoff at the rib tip defines the location of the strip at the periphery of the reflector and adjustable ties provide axial "float" in the remaining locations. Invar hinges allow the edge strips to fold for stowage.

4.0 SYSTEM PERFORMANCE

4.1 Weight and Stowed Volume

The complete radiometer system, including polarizers, horns, tower and reflector, but not including the radiometer circuitry and its packaging, weighs 578 pounds, Table 4.1, and stows in a volume 4.0 meters in diameter, 4.9 meters long. A detailed weight distribution is included in the Appendix.

4.2 Deployed Analytic Model Description

To estimate performance of the offset fed reflector and tower system, the finite element model (FEM) of Figures 4.2-1 through 4.2-5 was developed. The model, consisting of 200 nodes, simulates all members of the FRR rib and truss backup structure and condenses the RF reflective surface into 4 cord pairs and 12 mesh elements per gore. The reflective contour itself is represented by 85 surface nodes to accurately characterize RF performance. A detail listing of the model is presented in the Appendix.

As with all structures of this nature, the stiffness of the system depends upon, to some extent, the pretension in the mesh and cord elements. This pretension stiffness is modelled with pretensional "stringer" elements and triangular, pretensioned, orthotropic "membrane" elements. The single gore of Figure 4.2-6 indicates the preloads associated with each member, including the compression loads in the ribs and vertical strut. For details of member sizes, material properties, etc., reference the Appendix.

4.3 Deployed Analyses

Having generated model of the deployed system, performance of the spinning reflector is estimated. The effects of the 6 rpm spin rate, thermal environment and basic vibrational modes are investigated.

Table 4.1. Weight Budget

		<u>Weight (Pounds)</u>
Feed Horns and Polarizers		
1.4 GHz	5 @ 28 lbs. ea.	= 140
4.3 GHz	11 @ 3.2 lbs. ea.	= 35
11 GHz	11 @ 0.8 lbs. ea.	= 9
Tower Support and Deployment Structure		46
Tower		95
Reflector		225
Cabling		<u>28</u>
Total Weight		578 Pounds

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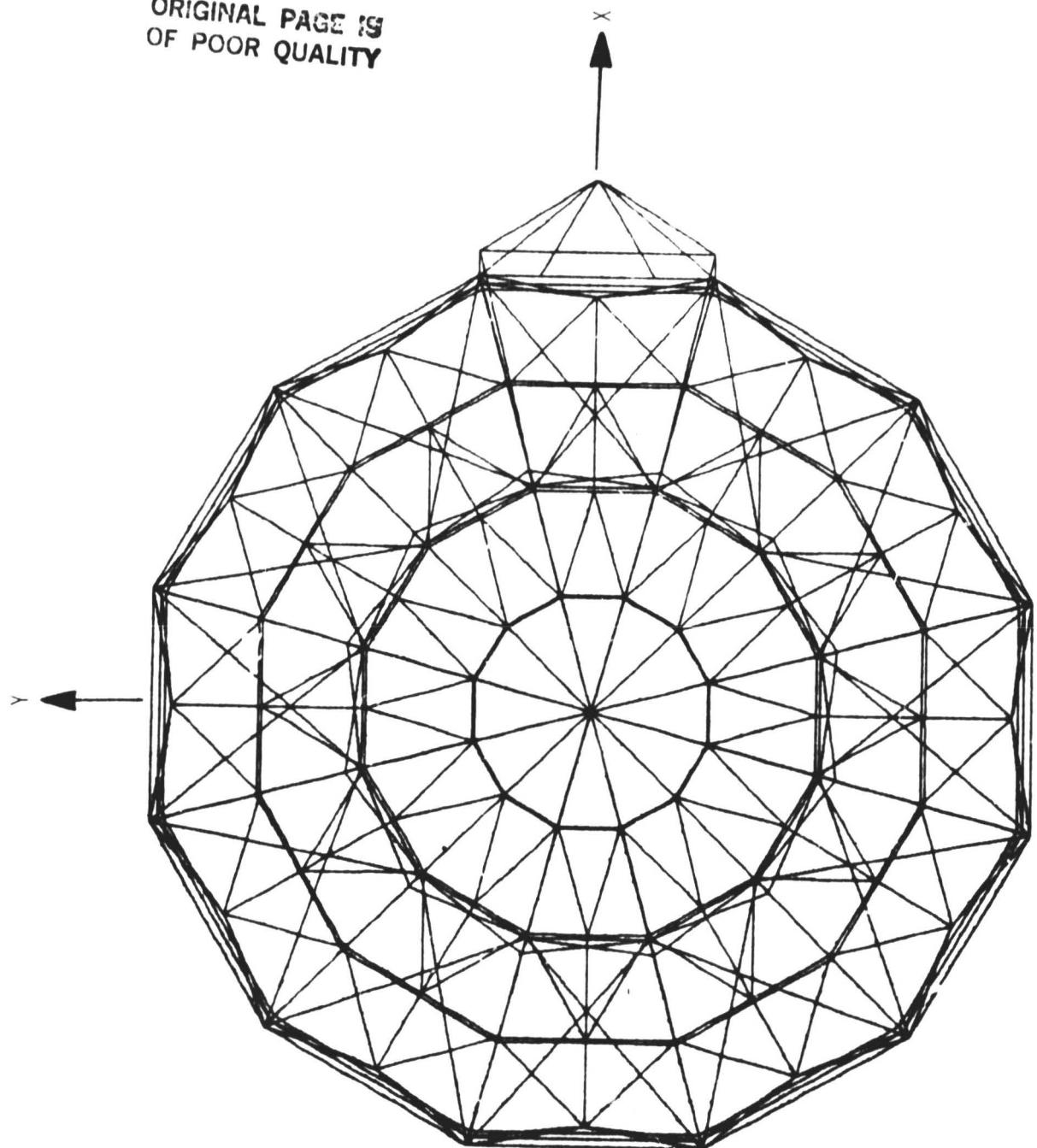


Figure 4.2-1. MSDA Finite Element Model

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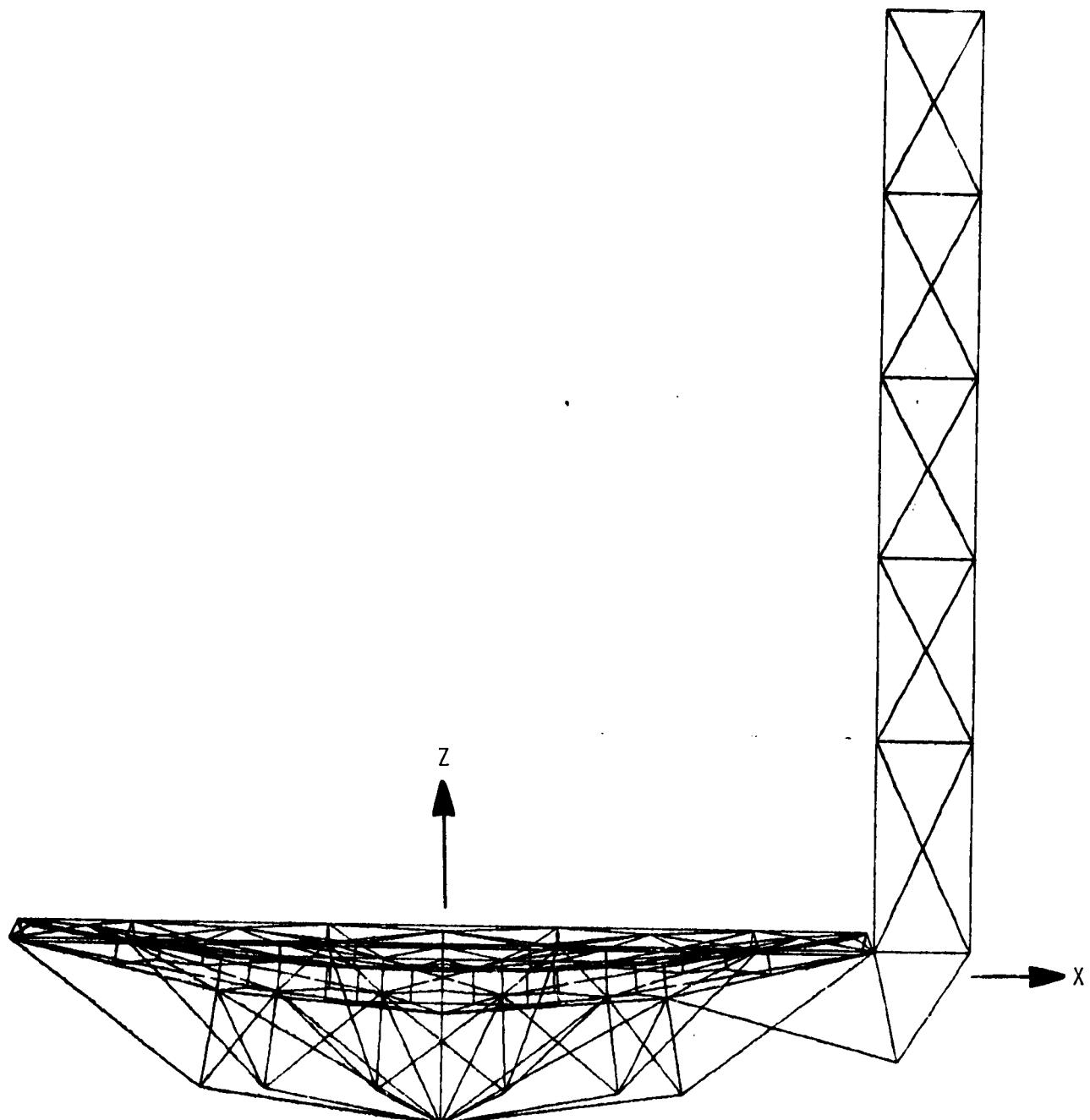


Figure 4.2-2. MSDA Finite Element Model

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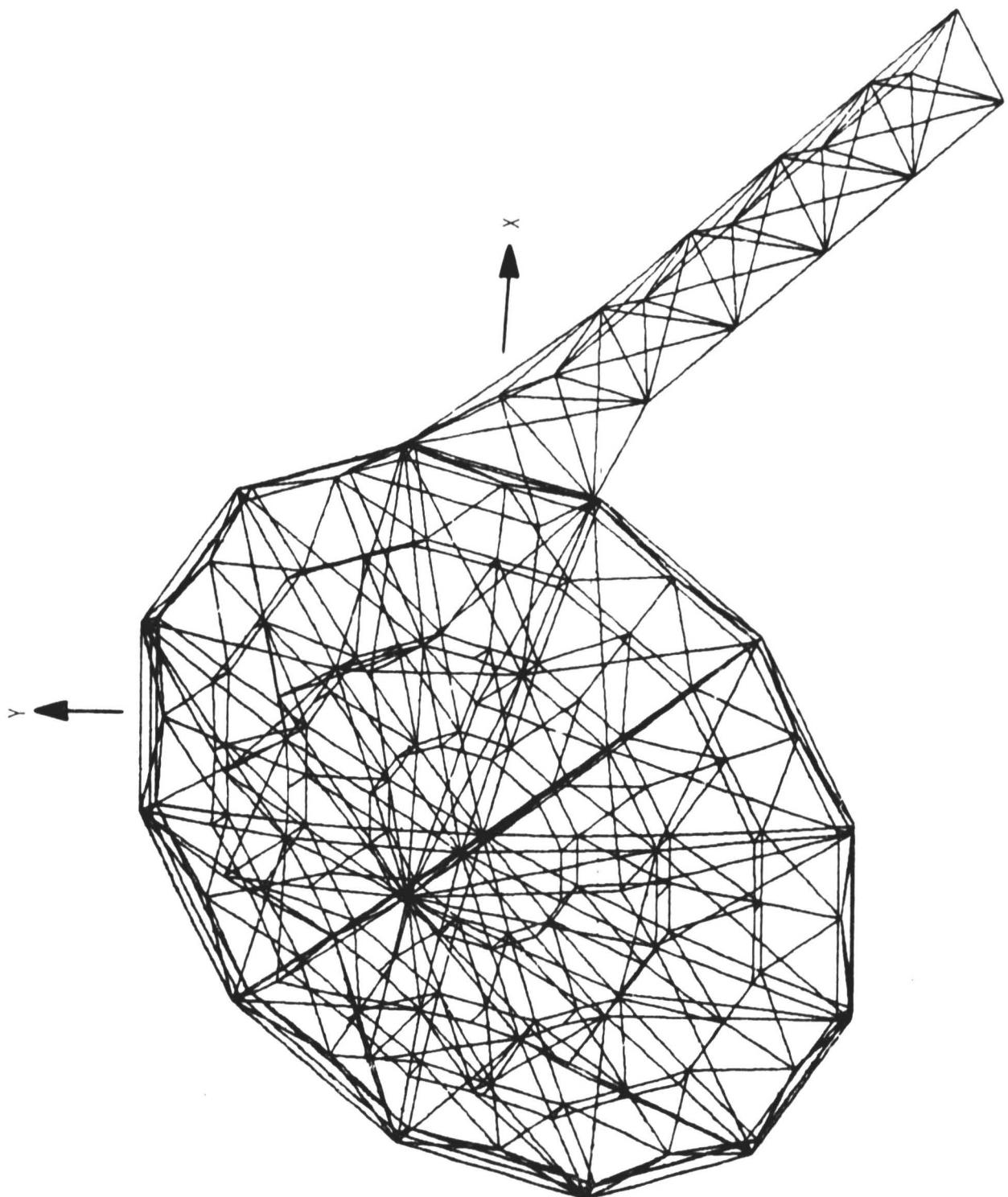


Figure 4.2-3. MSDA Finite Element Model

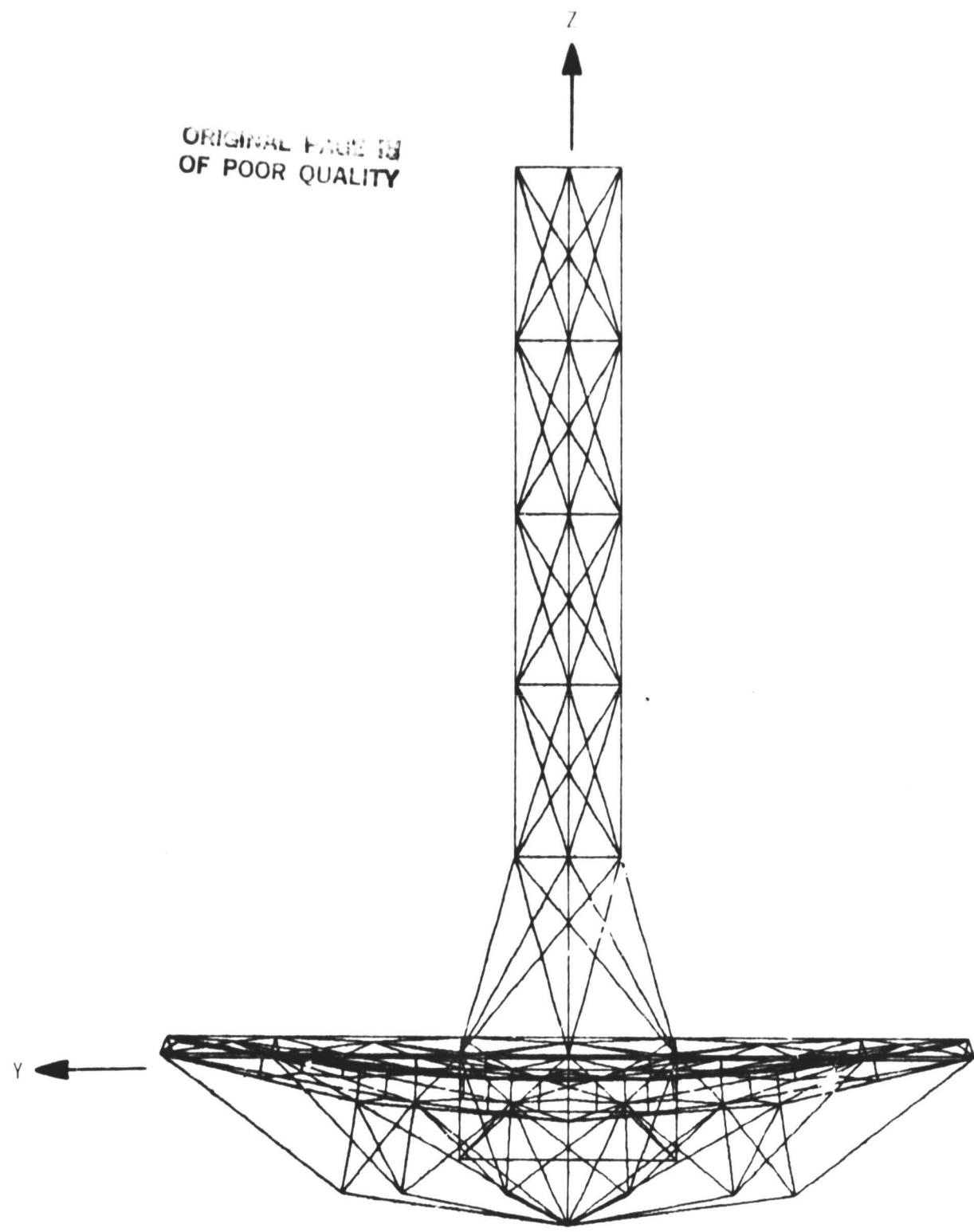


Figure 4.2-4. MSDA Finite Element Model

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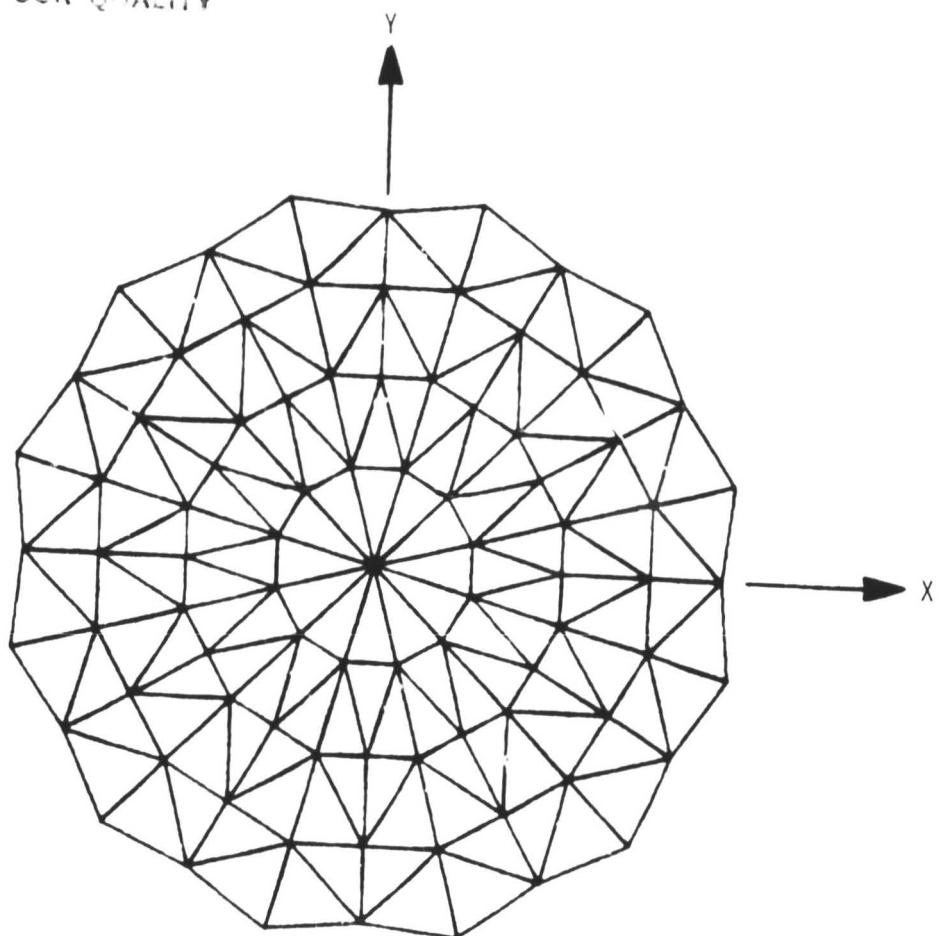
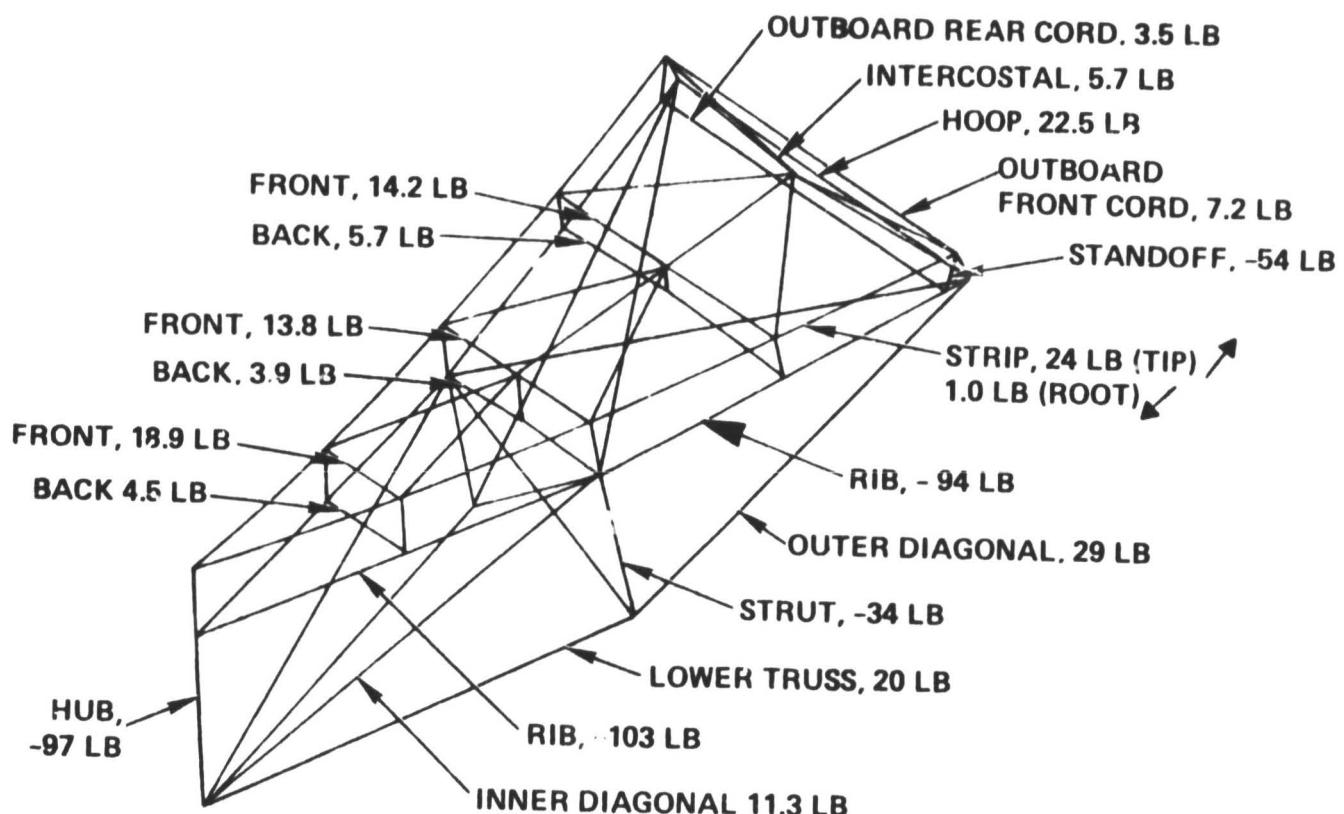


Figure 4.2-5. Mesh Surface Modelled with 144 Triangular
Membrane Elements Connecting 85 Nodes

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Figure 4.2-6. Structural Preloads are Included in the Modelling Process

4.3.1

Dynamic and Spin Effects

The most important aspect of this effort is to quantify the effect of the 6 rpm spin rate on surface performance. This task consisted of two parts: align the reflector and spin axis to balance the tower and reflector system, and predict surface distortions at 6 rpm. Dynamic balancing of the system is achieved by positioning the spin axis so that it passes through the CG of the system. The final geometry selected to achieve this goal is depicted in Figure 4.3.1. The weight moments of inertia of the structure about the axis system defined in the figure are:

Structure Weight: 319.7 lb. (includes tower and reflector,
excludes feed and cabling)

Center of Mass $\left\{ \begin{array}{l} \bar{x} = 69.16 \text{ inches} \\ \bar{y} = 0.0 \text{ inches} \\ \bar{z} = 0.0 \text{ inches} \end{array} \right.$

$$I_{XX} = 1.0331 \times 10^7 \text{ in}^2 \text{ lb}$$

$$I_{YY} = 2.0521 \times 10^7 \text{ in}^2 \text{ lb}$$

$$I_{ZZ} = 2.3537 \times 10^7 \text{ in}^2 \text{ lb}$$

$$I_{XY} = 4.7458 \times 10^6 \text{ in}^2 \text{ lb}$$

$$I_{XZ} = 0.0 \text{ in}^2 \text{ lb}$$

$$I_{YZ} = 0.0 \text{ in}^2 \text{ lb}$$

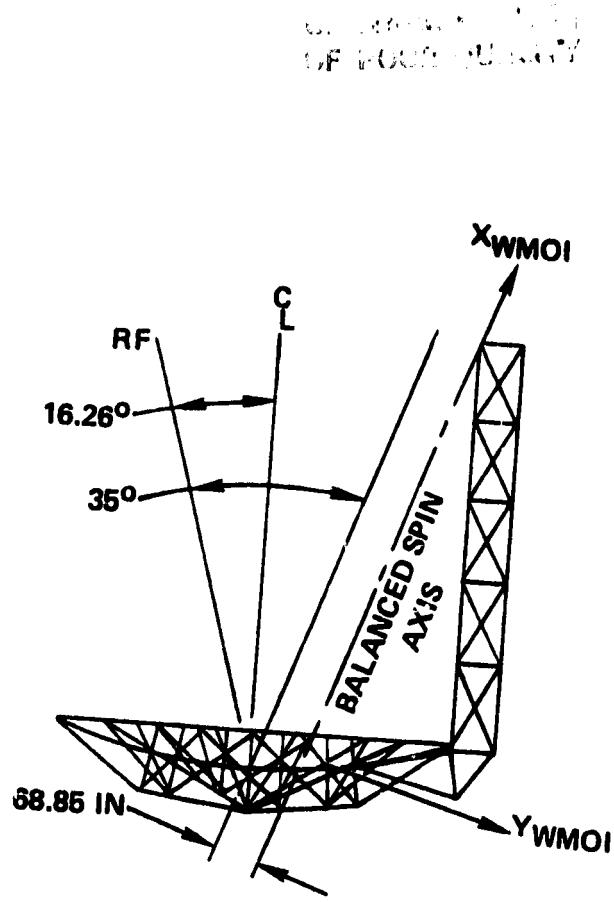
At a spin rate of 6 rpm the surface distorts, in terms of parabolic parameters, by:

Defocus (ΔF) -0.126 inches

Surface Roughness RMS 0.007 inches

Mechanical Mispointing 0.021 degree

The negative defocus, opposite of what one might expect, results from the compliance of the truss rods and high axial stiffness in the rib members. Spinning causes a small elongation in the upper (rib) members and a larger



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Figure 4.3.1. An Offset Spin Axis Dynamically Balances the Reflector System

elongation in the lower (rod) truss members forcing the reflector to close and hence drive the defocus negative. Given adequate knowledge of the spin rate, geometry and mass properties, all or at least a significant amount of this defocus can be removed by biasing the antenna during manufacture.

The two lowest natural modes of the antenna were found by eigenvalue extraction to be:

0.55 Hz combination of tower twist and bending mode.

1.54 Hz rocking of the antenna about the tower to reflector interface.

4.4

RF Performance

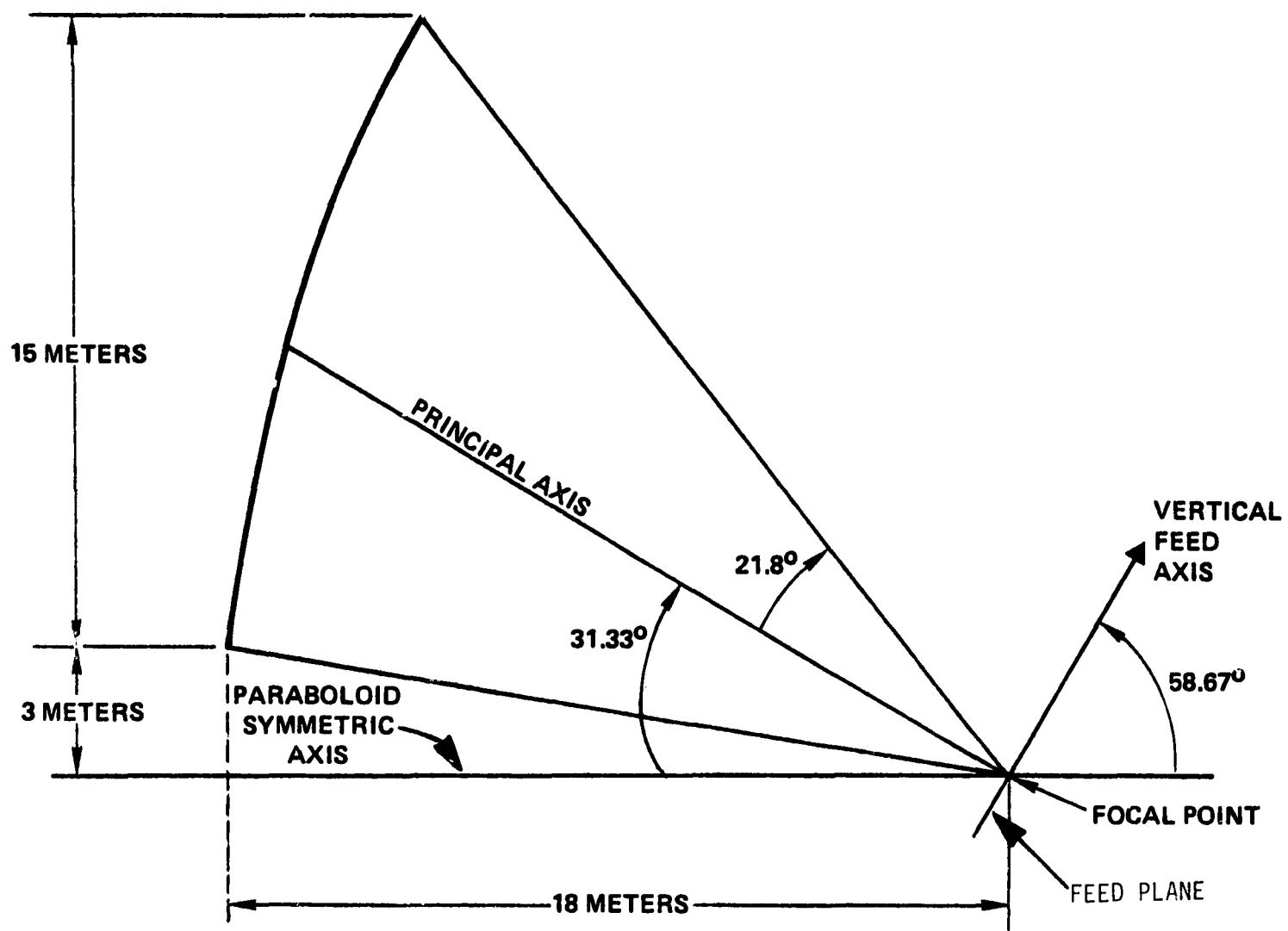
An initial tradeoff study was performed to define the possible range of f/D ratios, feed aperture sizes, and feed spacings. Baseline parameters used in this analysis were an operational frequency of 4.3 GHz, a circular feed aperture, a 15 meter offset reflector, feeds located at, or in a plane containing, the focal point of the paraboloid, and a circularly symmetric far-field pattern with a cosine amplitude and phase distribution. This feed pattern is characteristic of a wideband corrugated conical horn as described in Reference (1), with the aperture amplitude and phase distributions given by:

$$A(r) = \cos\left(\frac{\pi r}{2a}\right)$$
$$P(r) = \pi \left(1 - \cos\frac{\pi r}{2a}\right)$$

where A is the aperture radius and r ranges from 0 to A. The variable for the tradeoff study were f/D ratio, aperture radius, feed spacing, and reflector offset.

For this analysis, it is assumed that the phase center of each feed horn is located near the aperture plane, thereby allowing all feed apertures to lie in the feed plane as defined in Figure 4.4-1. The principal axis, defined to be orthogonal to the feed plane, bisects the angle which subtends the reflector when viewed from the focal point. This then determines the feed tilt angle.

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Figure 4.4-1. Antenna System Geometry

The initial tradeoff study was performed at 4.3 GHz, using the above mentioned wideband feed horn. To obtain low cross-polarization levels in the secondary beam, f/D ratios greater than 0.5 are necessary in accordance with Figure 4 of Reference (3). Values for f/D of 0.5, 0.7, and 0.9 were then chosen. In order to meet the high beam efficiency requirement (>90%), reflector edge illumination in the range -10 dB to -20 dB is needed. It was determined that this requirement leads to an exceedingly large wideband feed horn. As a compromise, the edge illumination requirement was relaxed to -7 dB, resulting in a 0.45 meter aperture radius with approximately 65% beam efficiency. Two patterns were then computed for each f/D ratio; the first, with the feed horn located at the focus, and the second, with the feed offset one diameter along the vertical feed axis (feeds adjacent to one another). It was found in each case that the far-field beam crossover points were in the range of 20 dB to 25 dB down from the peak value. To obtain a continuous mapping of the earth's surface, it is necessary for the beam overlay to fall within 3 dB to 6 dB down from the maximum value of the beam. The wideband horn, therefore, appears to be unacceptable for this design unless unreasonably large feed dimensions can be tolerated.

To reduce the overall size of the feed and attempt to meet the far-field beam crossover and beam efficiency requirements, a narrowband corrugated conical horn was selected. A procedure identical to the one followed for the wideband feed analysis was used in this analyses. The assumed horn aperture amplitude and phase distribution is given by:

$$A(r) = \cos \left(\frac{\pi r}{2a} \right)$$

$$P(r) = \Delta\pi \left(1 - \cos \frac{\pi r}{2a} \right)$$

At 4.3 GHz, using an aperture radius of 0.123 meter, the calculated radiation patterns revealed that the far-field beam crossover points were still greater than 15 dB down from the beam peak. It was noted at this point that a feed horn offset one-half the diameter of the aperture would yield a far-field beam displacement of approximately one beamwidth, which corresponds to a 3 dB to 4 dB beam overlay. With the sweep scanning nature of this antenna in mind, a 3 dB to 6 dB beam crossover can then be obtained with the feed layout of Figure 4.4-2.

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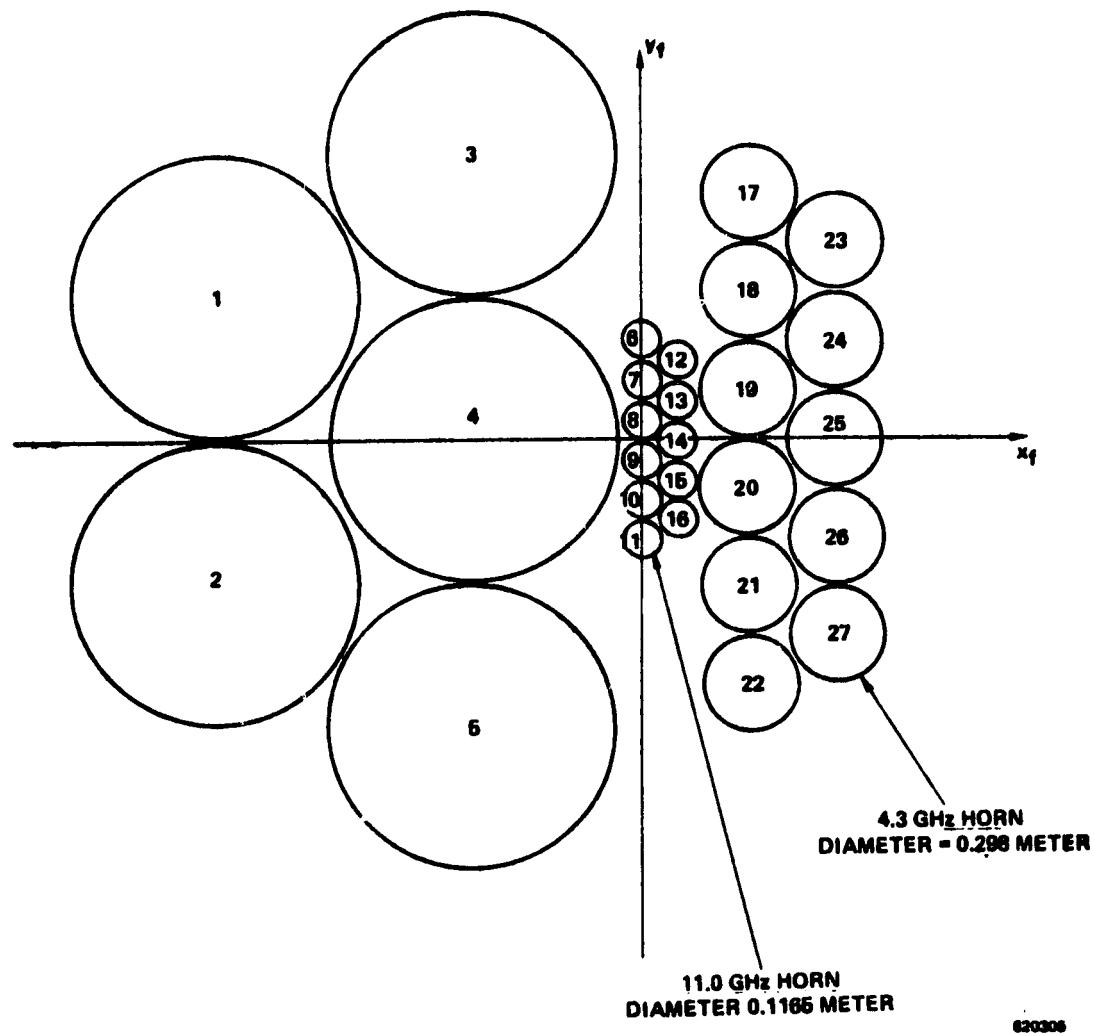


Figure 4.4-2.

Using the feed arrangement, it is then possible to choose the lower f/D ratio (=0.5), yielding a shorter boom length. The remaining analysis was then performed using the antenna system geometry of Figure 4.4-1.

The narrowband corrugated conical horn design procedure given in Reference (2) was then used to refine the design of the 4.3 GHz horn, and this design was scaled to 1.414 GHz and 11.0 GHz. Final design parameters for each horn are given in Table 4.4-1, with an associated sketch in Figure 4.4-3. The feed beam efficiency is approximately 93% and reflector edge illumination is -12 dB. A corrugation depth of $3\lambda/8$ was assumed, adding $3\lambda/4$ to the total diameter. The final feed horn layout as it appears in the feed plane is seen in Figure 4.4-4.

Computer analysis was performed on the 4.3 GHz case to verify the 3 dB to 6 dB beam overlay. A computer run catalog appears in Table 4.4-2 with the corresponding plots in Figures 4.4-5 through 4.4-10. Only a vertical offset was considered for this analysis, i.e., x_f - offset equal to zero. Beam crossover, for each scan case, lies between 4 dB and 6 dB, with a 3 dB beamwidth of approximately 0.32° . The maximum cross-polarization level was 29.86 dB below the beam peak. This compares favorably with the predicted value in Reference (2). At the maximum feed offset position, gain loss due to scan was less than 1 dB.

Entering the curve in Figure 4.4-11 and assuming a 93% beam efficiency in the perfect reflector case, and a roughness of 0.01λ , the proposed design is close to 90% beam efficiency. Further refinement in these calculations are required to obtain precise calculations.

4.5 Mesh Analyses

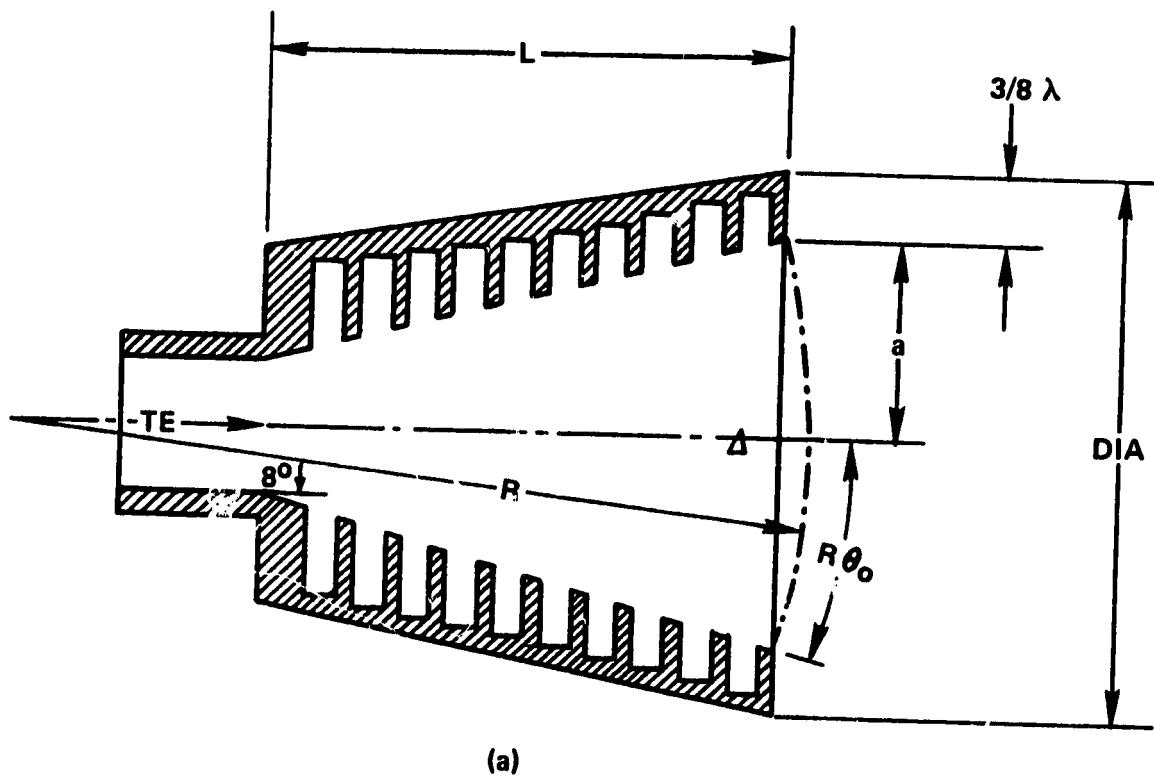
The most commonly used mesh is composed of gold-plated molybdenum wire 1.2 thousandths of an inch in diameter. A closeup view of the wire knitted onto a conducting mesh is shown in Figure 4.5-1 which also shows an optical target located on the surface.

Table 4.4-1. Feed Geometry

<u>1.414 GHz Horn</u>	<u>4.3 GHz Horn</u>	<u>*11.0 GHz Horn</u>
a = 0.375 meter	a = 0.123 meter	a = 0.048 meter
R = 1.60 meter	R = 0.526 meter	R = 0.206 meter
θ_0 = 13.555°	θ_0 = 13.52°	θ_0 = 13.47°
Δ = 0.21 wavelength	Δ = 0.209 wavelength	Δ = 0.208 wavelength
Dia = 0.909 meter	Dia = 0.298 meter	Dia = 0.1165 meter

*The 11.0 GHz horn was obtained by scaling the 4.3 GHz design. This smaller horn then results in a far field beamwidth of 0.16°, approximately one-half the desired 0.35°. To increase the beamwidth several approaches are available.

1. Increase the size of the horn, thereby under-illuminating the disk and increasing the beamwidth. This would require moving the 4.3 GHz feeds to make additional space available for these larger horns.
2. Defocus the 11.0 GHz feeds along the principal axis toward the reflector, producing a quadratic phase distribution in the aperture of the dish, thereby increasing the beamwidth.
3. Loading of the existing feeds to under-illuminate the reflector, and thereby increase the beamwidth.



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Figure 4.4-3.

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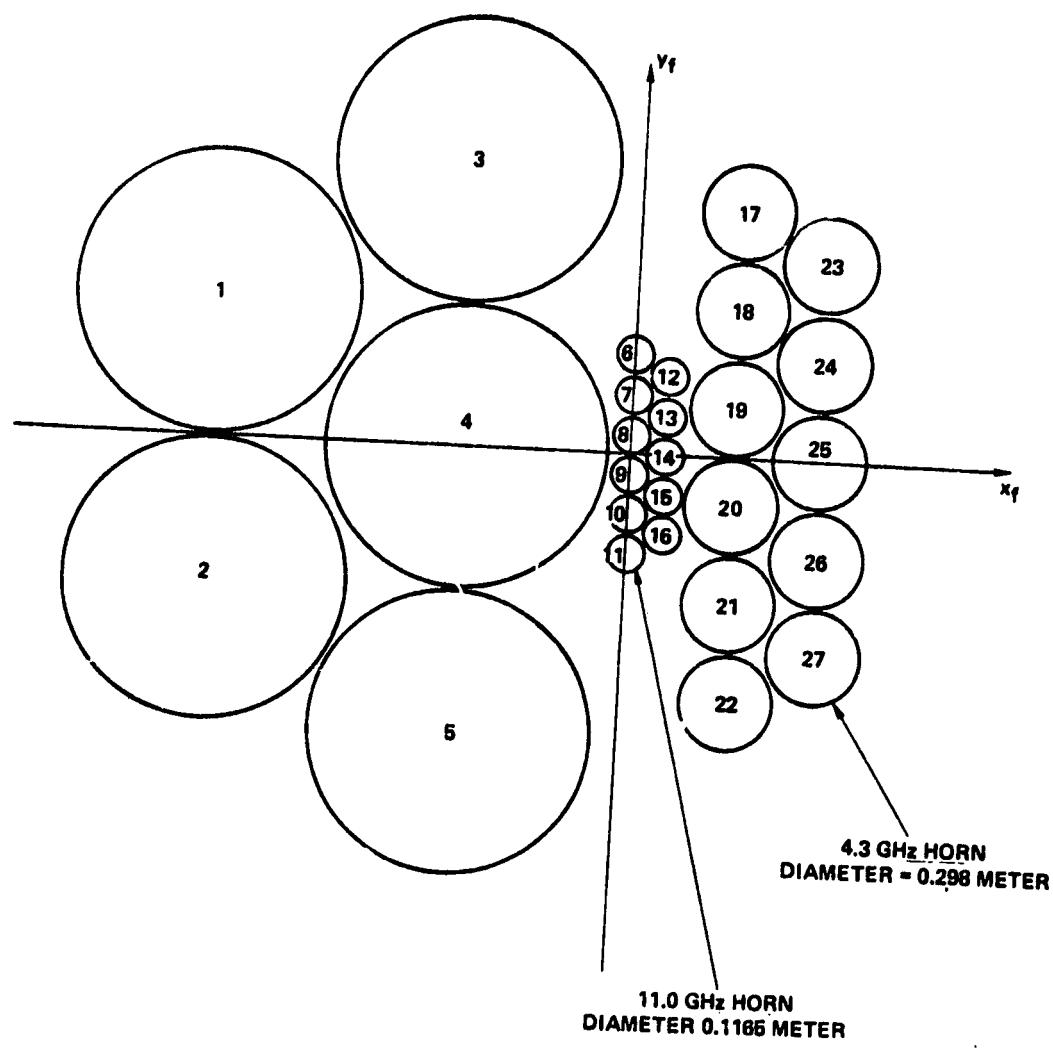


Figure 4.4-4. Feed Array Layout

Table 4.4-2. Computer Run Catalog

<u>Y-Offset (Meters)</u>	<u>Figure Number</u>	<u>Corresponding Feed Horn Number in Figure 3.2.3.3-4</u>
0.0	5	25
0.149	6	19
0.298	7	24
0.447	8	18
0.596	9	23
0.745	10	17

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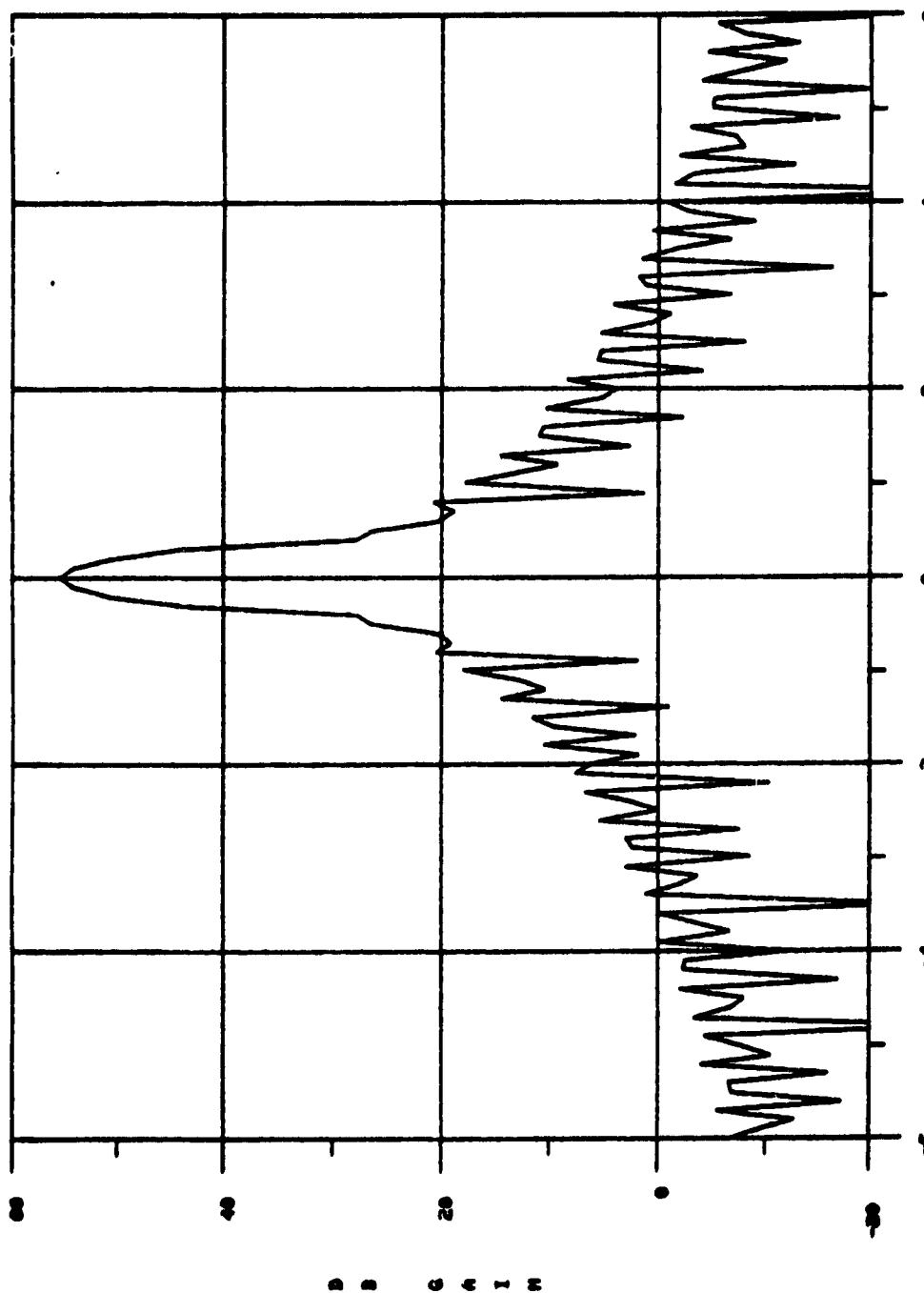


Figure 4.4-5.

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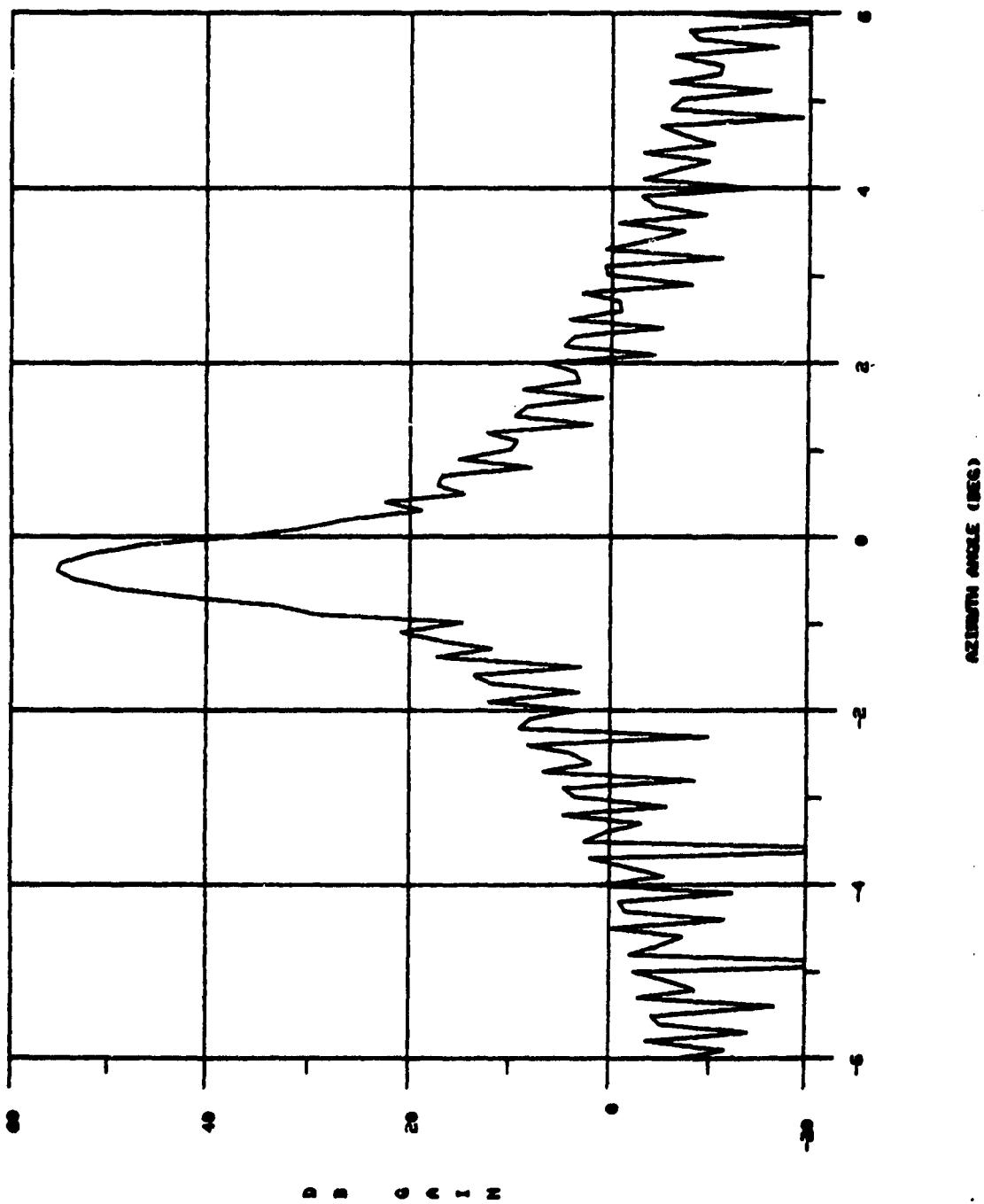


Figure 4.4-6.

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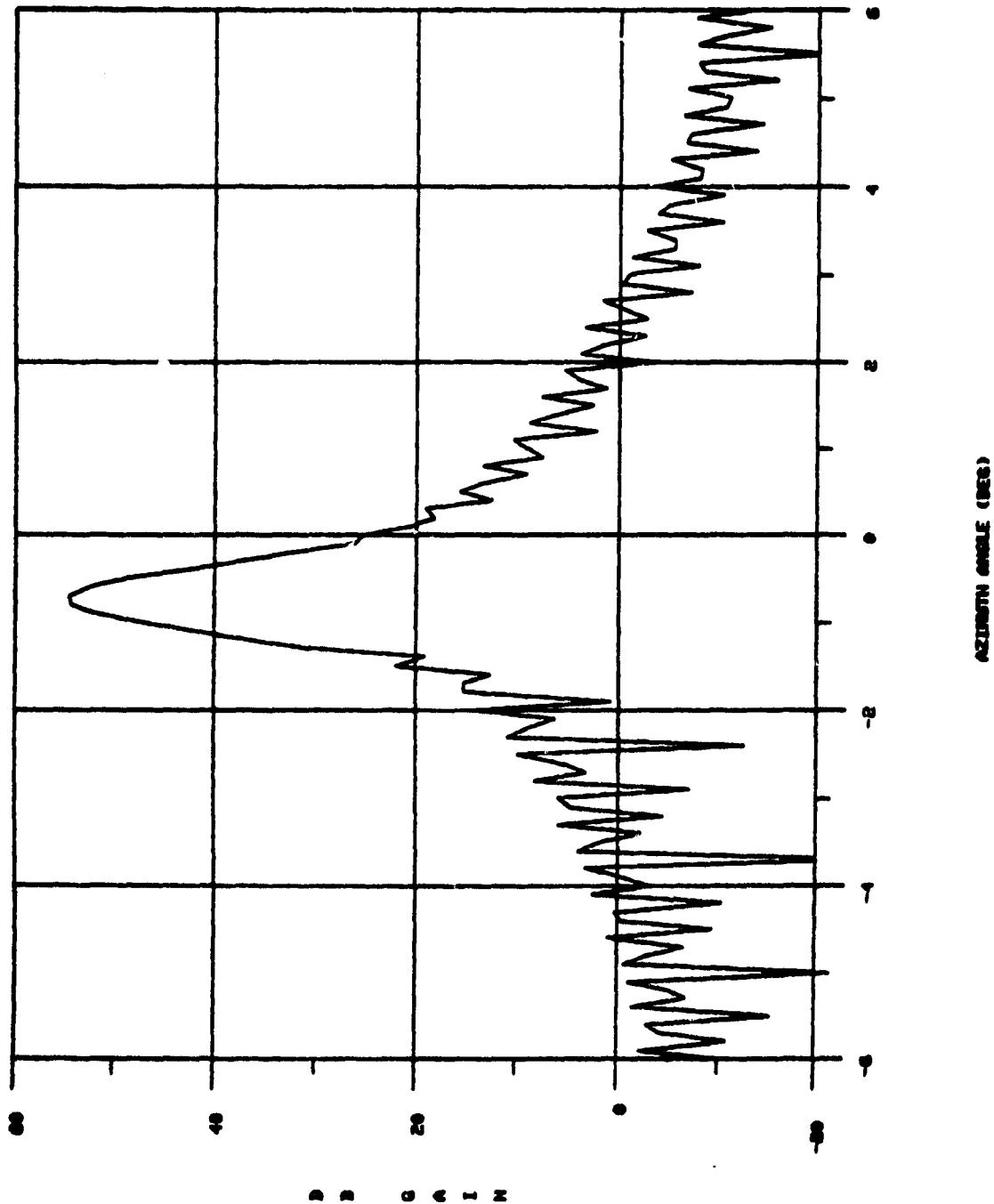


Figure 4.4-7.

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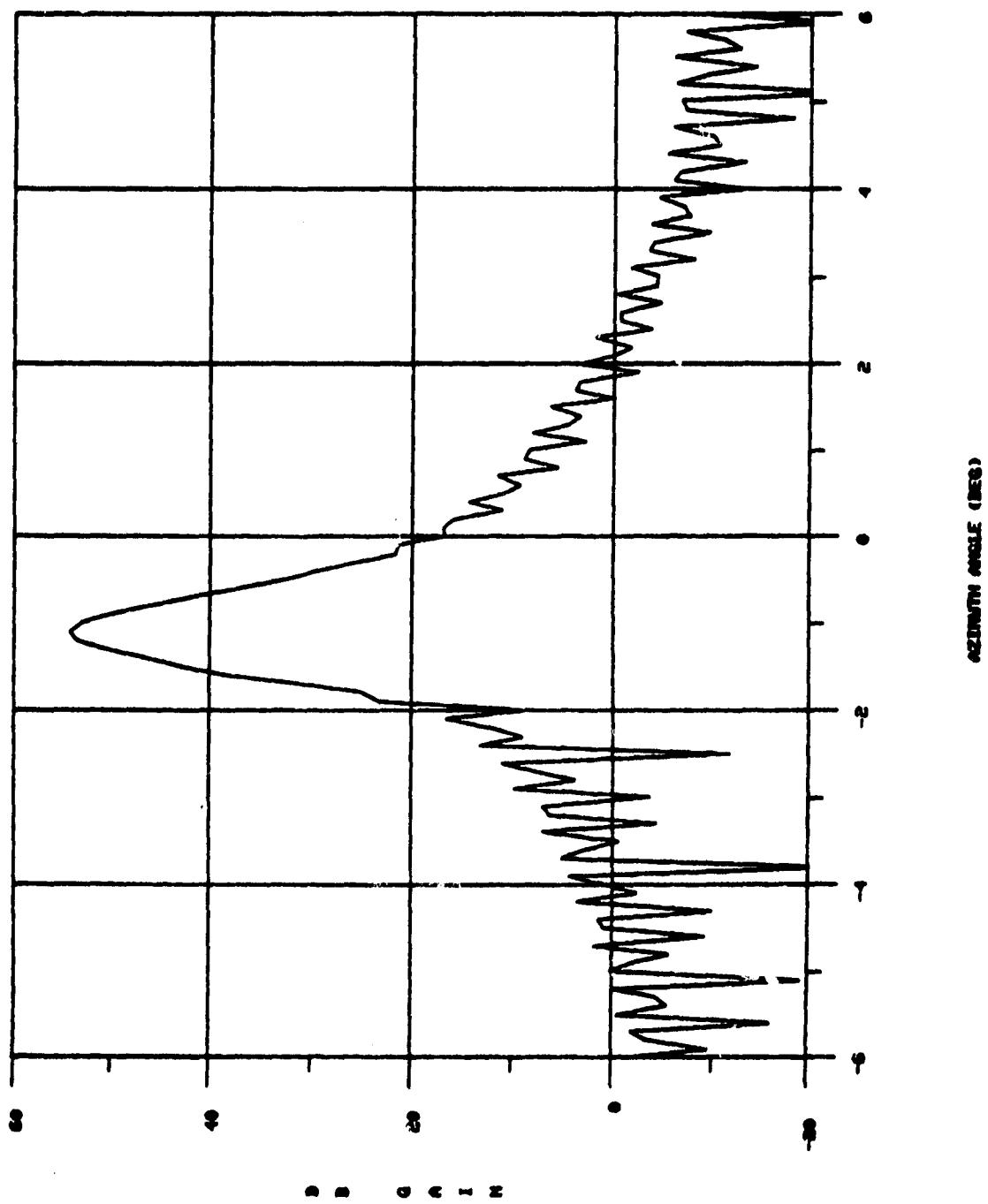


Figure 4.4-8.

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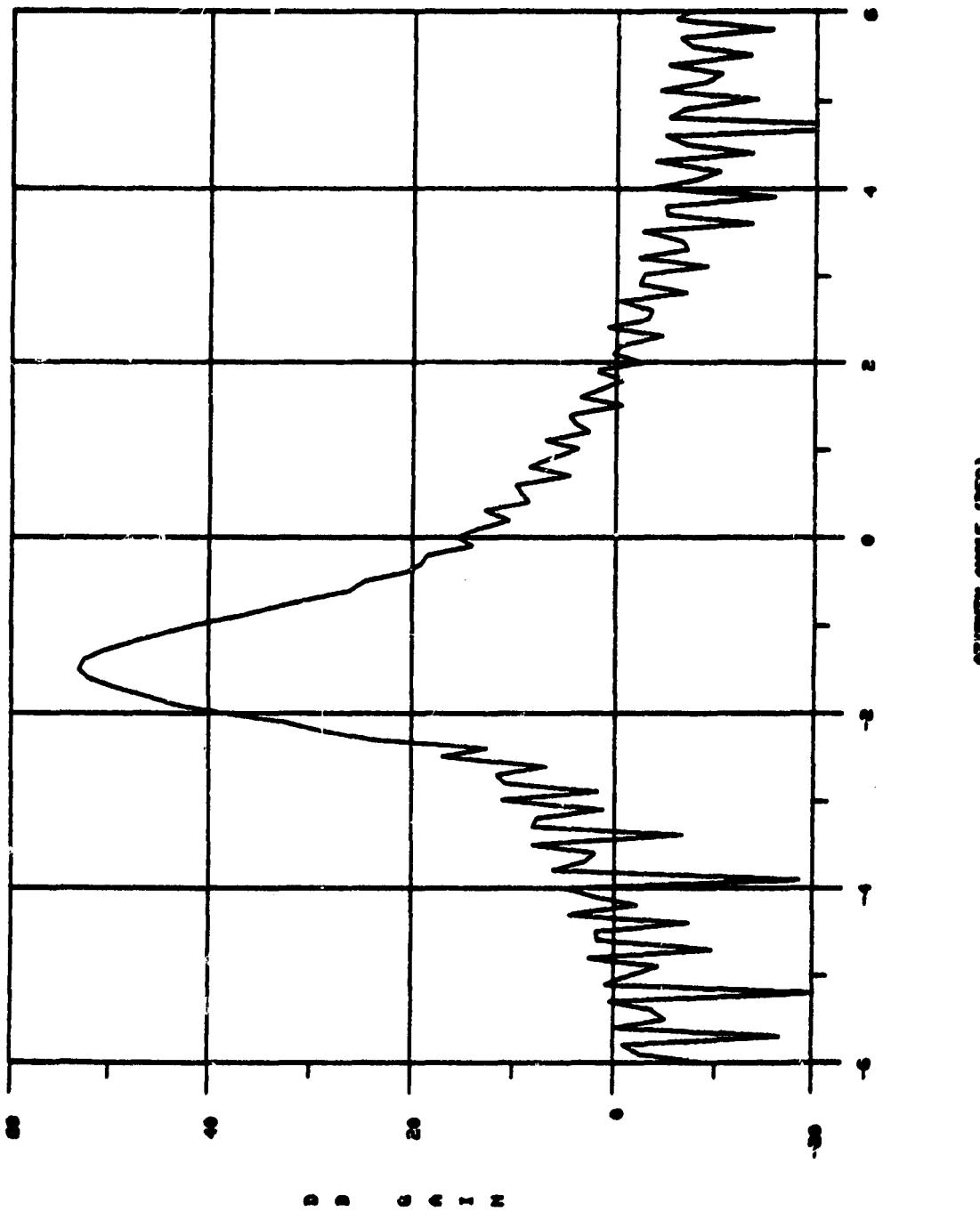


Figure 4.4-9.

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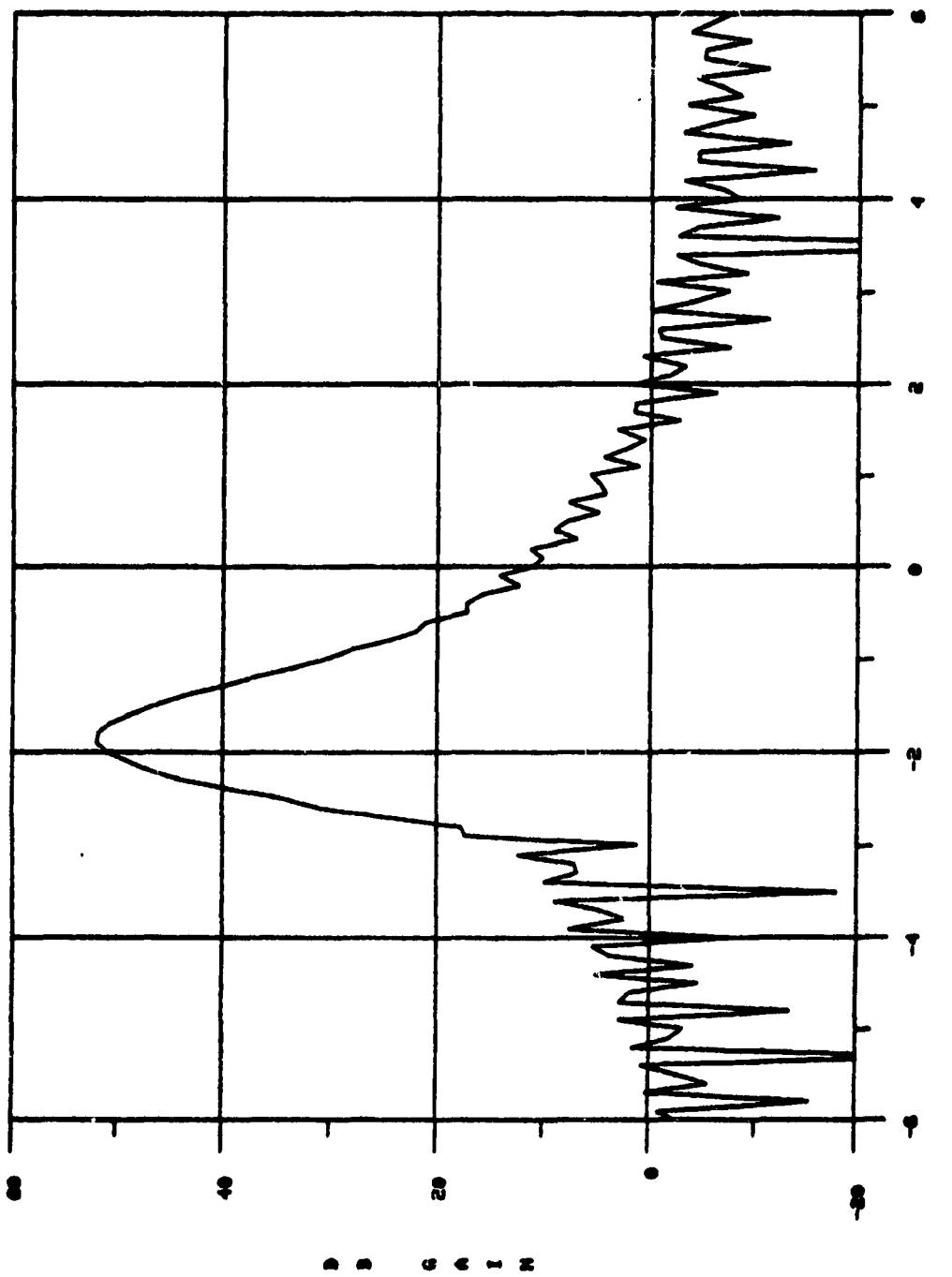


Figure 4.4-10.

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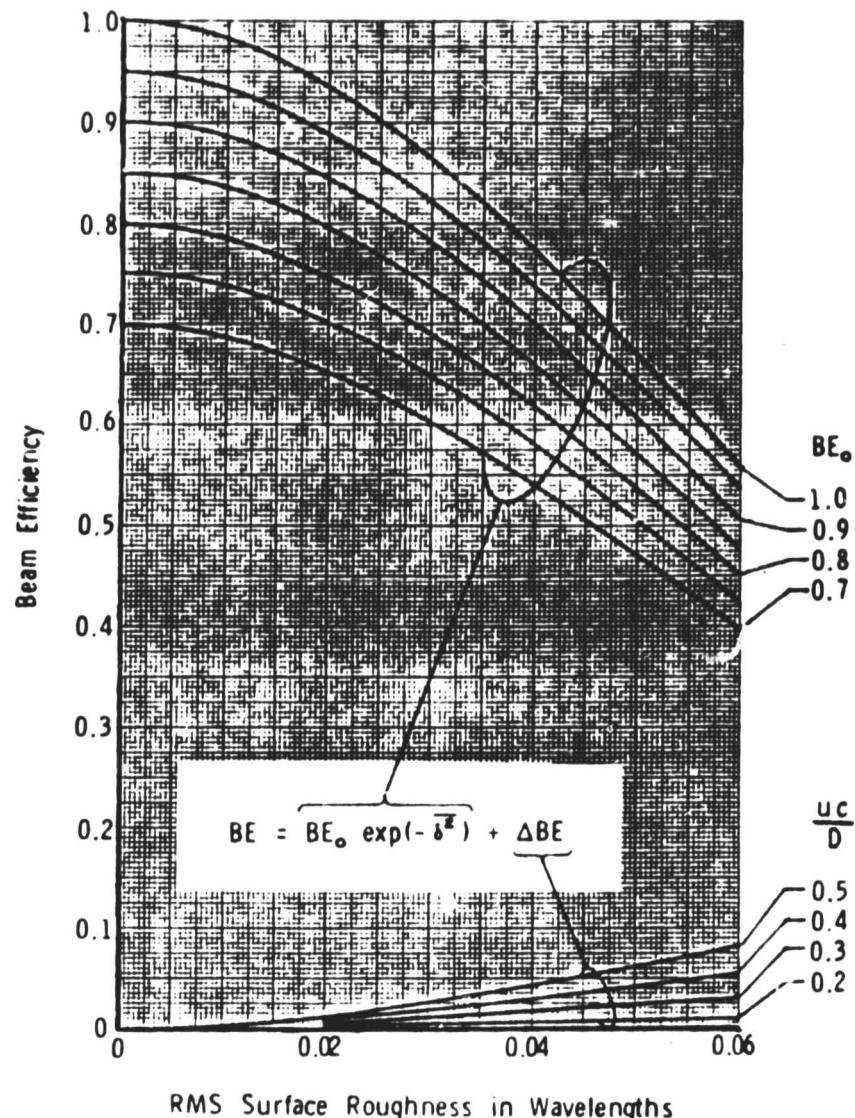


Figure 4.4-11. Beam Efficiency of a Random Rough Surface Reflector

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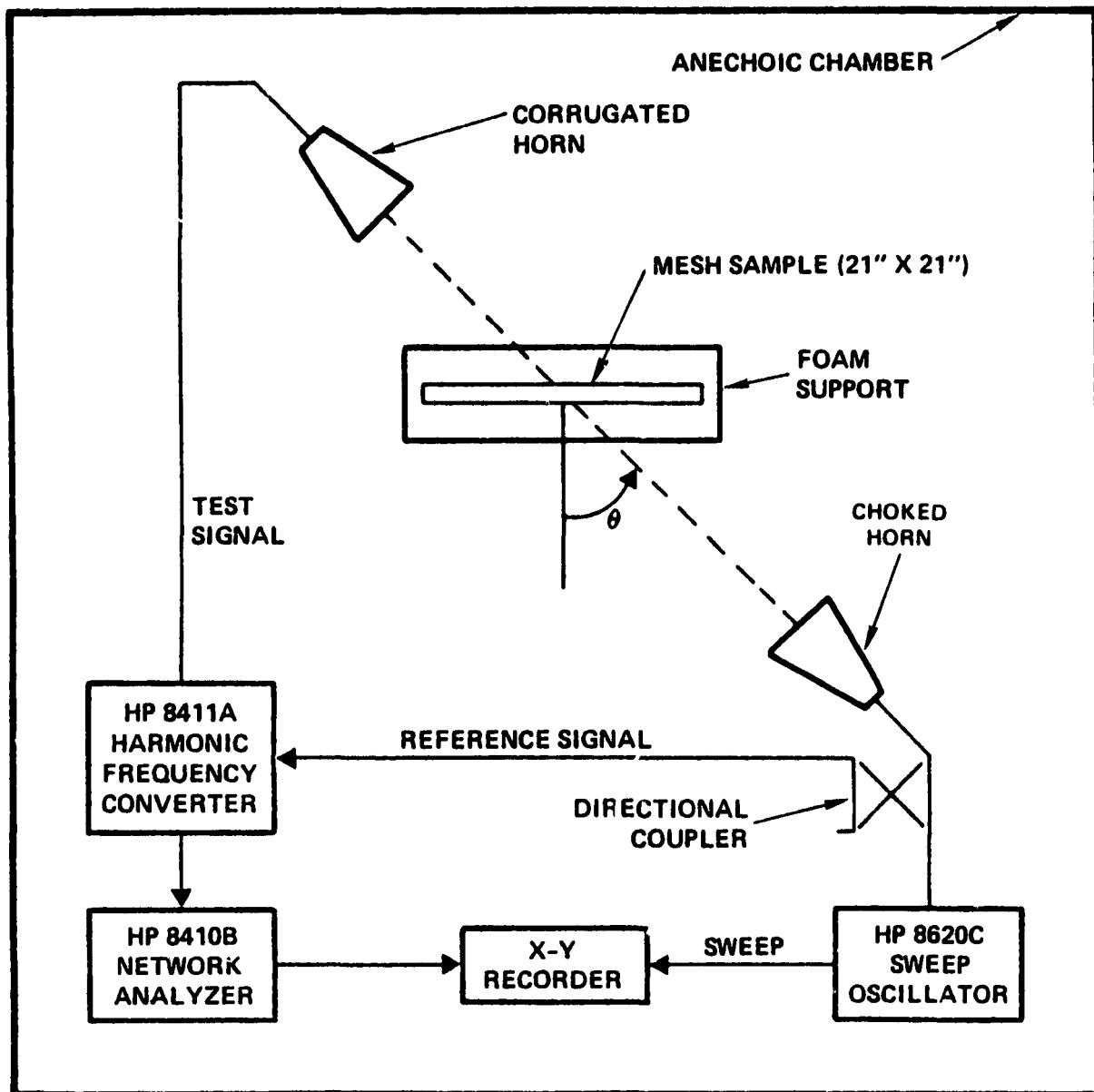


F3-5

Figure 4.5-1.

A number of methods have been used to characterize the electrical properties including waveguide sample insertion methods, free space transmission methods, etc. The most common method presently used at Harris is the free space method shown in Figure 4.5-2. Here a sweeper method is used which allows the clear resolution of any space standing waves between the horns and the sample holder. Measurements are readily made over a wide range of frequencies and incidence angles. Using this system extensive measurements of transmissivity loss have been made, a sample of which is given in Figure 4.5-3. The calculations shown in Figure 4.5-3 were performed by a mesh analysis program developed and verified in extensive measurements on the TDRSS program. The basic theoretical model of the mesh is given in Figure 4.5-4. This model which includes the surface impedance and junction impedances is very adequate for mesh with up to 10 openings per inch. For such mesh, as found on TDRSS, if the openings are in the order of 0.1 wavelengths, polarization effects can result in different loss values.

FREE SPACE TRANSMISSIVITY MEASUREMENT SYSTEM



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Figure 4.5-2.

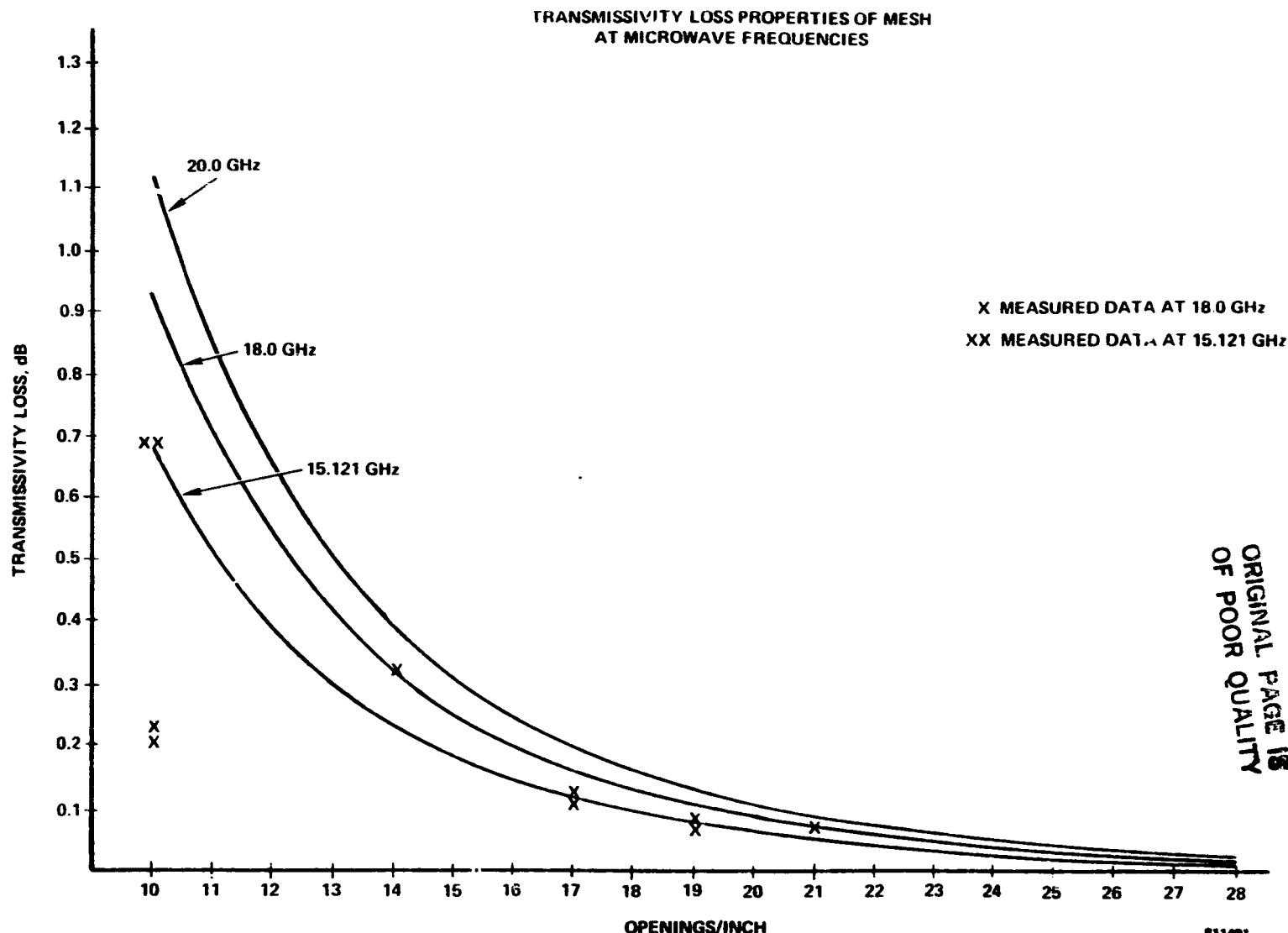
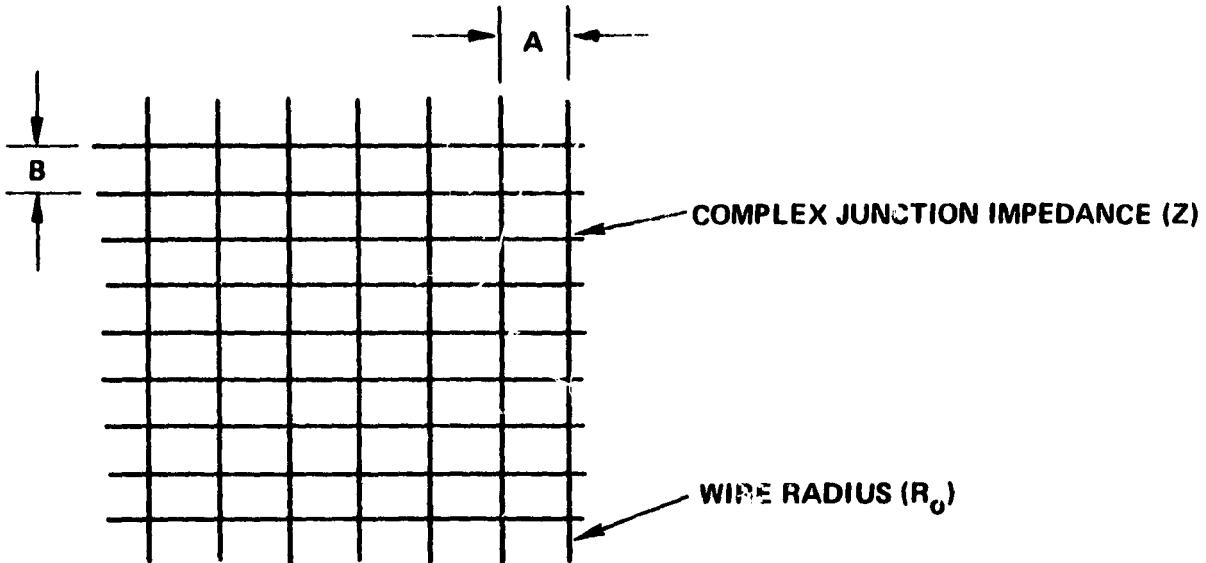


Figure 4.5-3.

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- AVERAGE BOUNDARY CONDITIONS
- INCLUDES CONDUCTIVITY LOSS
- JUNCTION IMPEDANCE CAN BE CAPACITIVE OR INDUCTIVE
- CALCULATES CROSS POLARIZATION TERMS DUE TO SURFACE IMPEDANCE

THEORETICAL MODEL OF MESH

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Figure 4.5-4.

REFERENCES

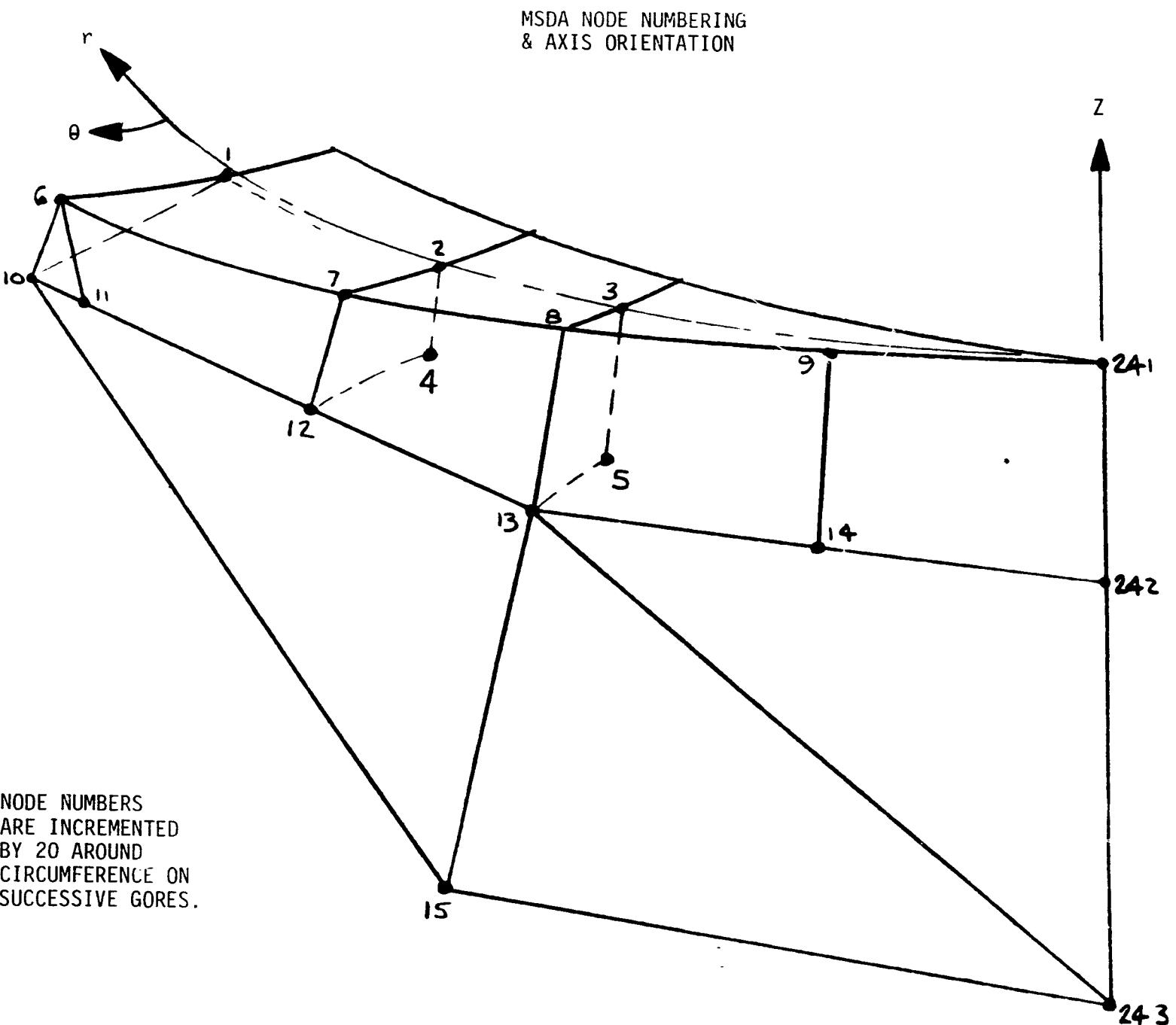
- Reference (1) "High Resolution Passive Microwave Satellites" edited by D. H. Staelin and P. W. Rosenkramfz, Research Laboratory for Electronics, MIT, Cambridge, Massachusetts, 02139, 14 April 1978.
- Reference (2) Bruce Mac A. Thomas, "Design of Corrugated Conical Horns," IEEE Transactions on Antennas and Propagation, AP-26, No. 2, March 1978, pp 367-372.
- Reference (3) Ta-shing Chu and R. H. Turrin, "Depolarization Properties of Offset Reflector Antennas," IEEE Transactions on Antennas and Propagation, AP-21, May, 1973, pp 339-345.

APPENDIX

ANALYTIC MODEL

The finite element presented herein employs the Non-Linear Structural Analysis (NLSA) program, a general purpose finite element program proprietary to Harris, Government Electronic Systems Division. While the model does not employ NASTRAN, the inputs presented are readily adapted to NASTRAN.

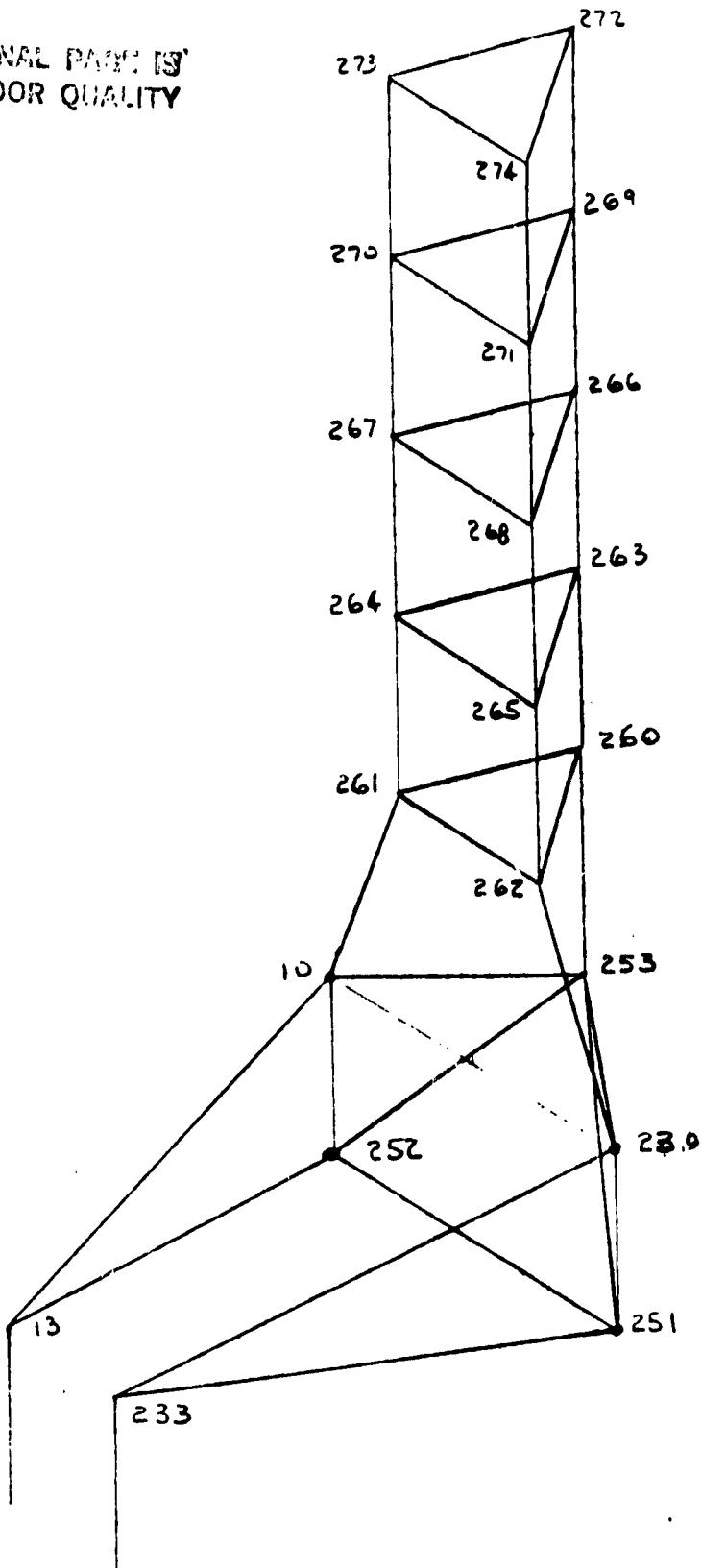
In the listing that follows, the reader will find the raw data for material properties definition, node point geometry, stringer, mesh, and beam element connecturaties, beam crossectional data and a complete nodal weight distribution. In addition, the data is listed in convenient, easy-to-read tables.



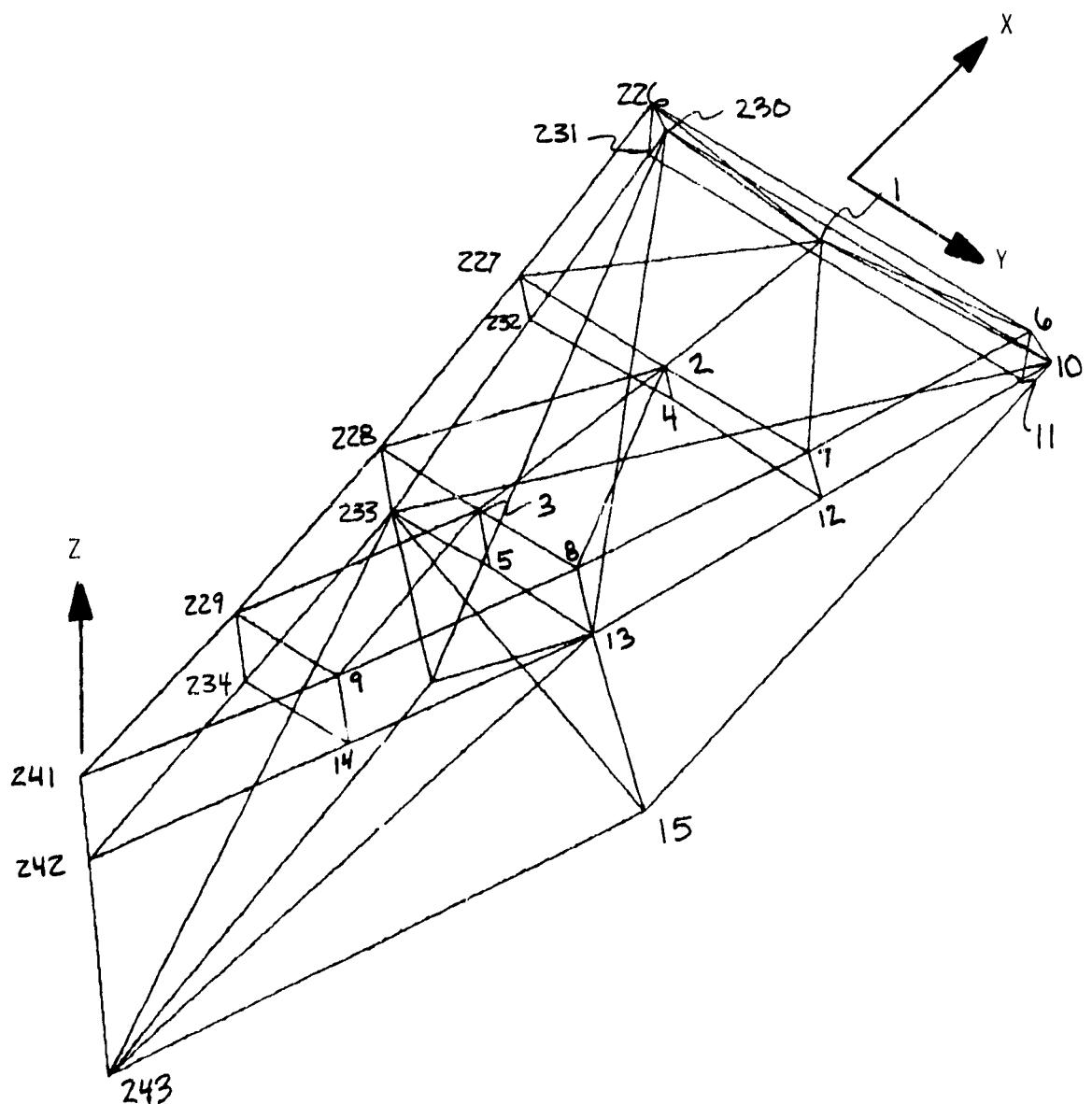
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MSDA TOWER MODEL
NODE NUMBERS

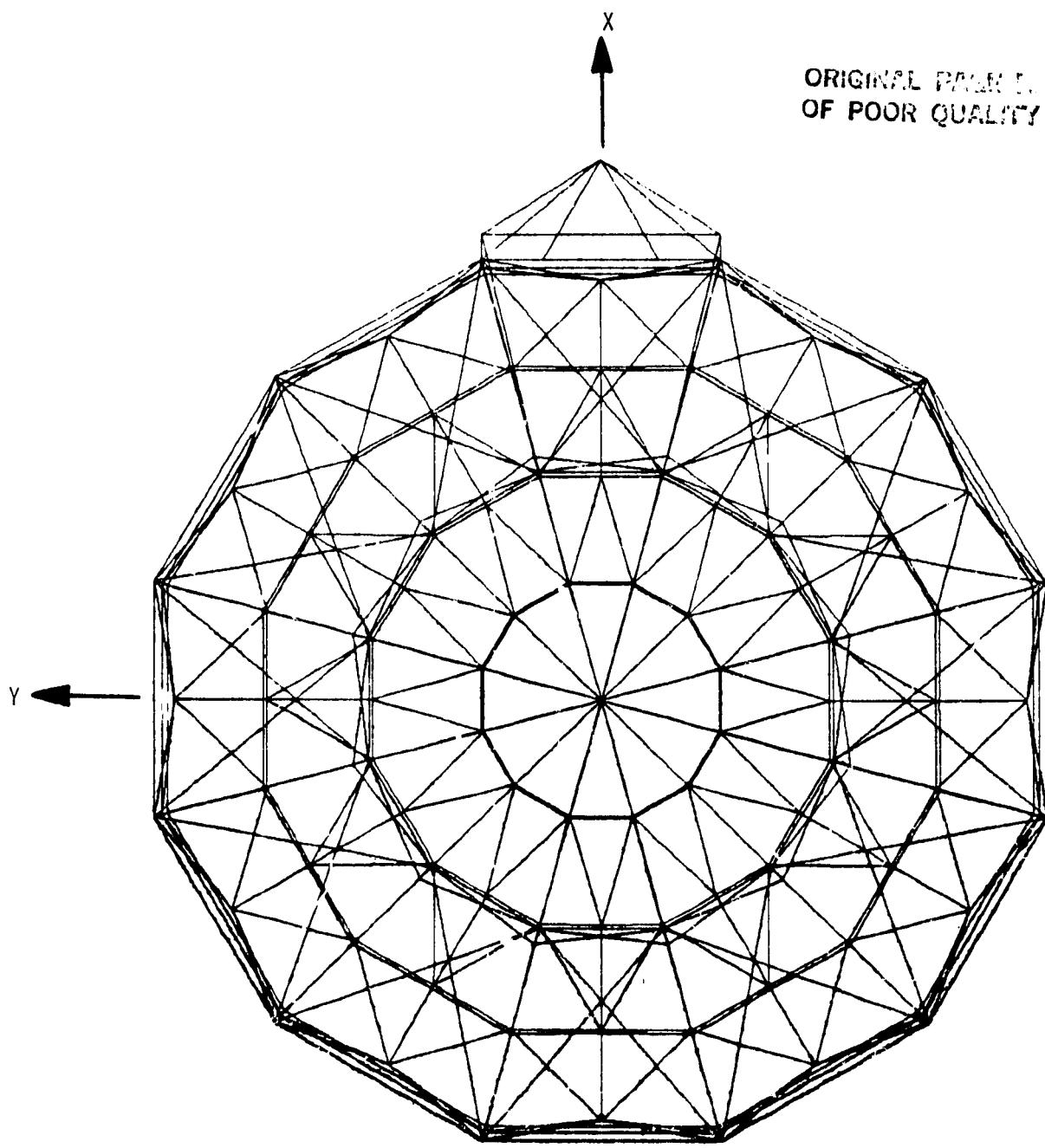
NOTE: DIAGONALS ARE
 OMITTED FOR
 CLARITY



WATER LEVELS
OF POOR QUALITY

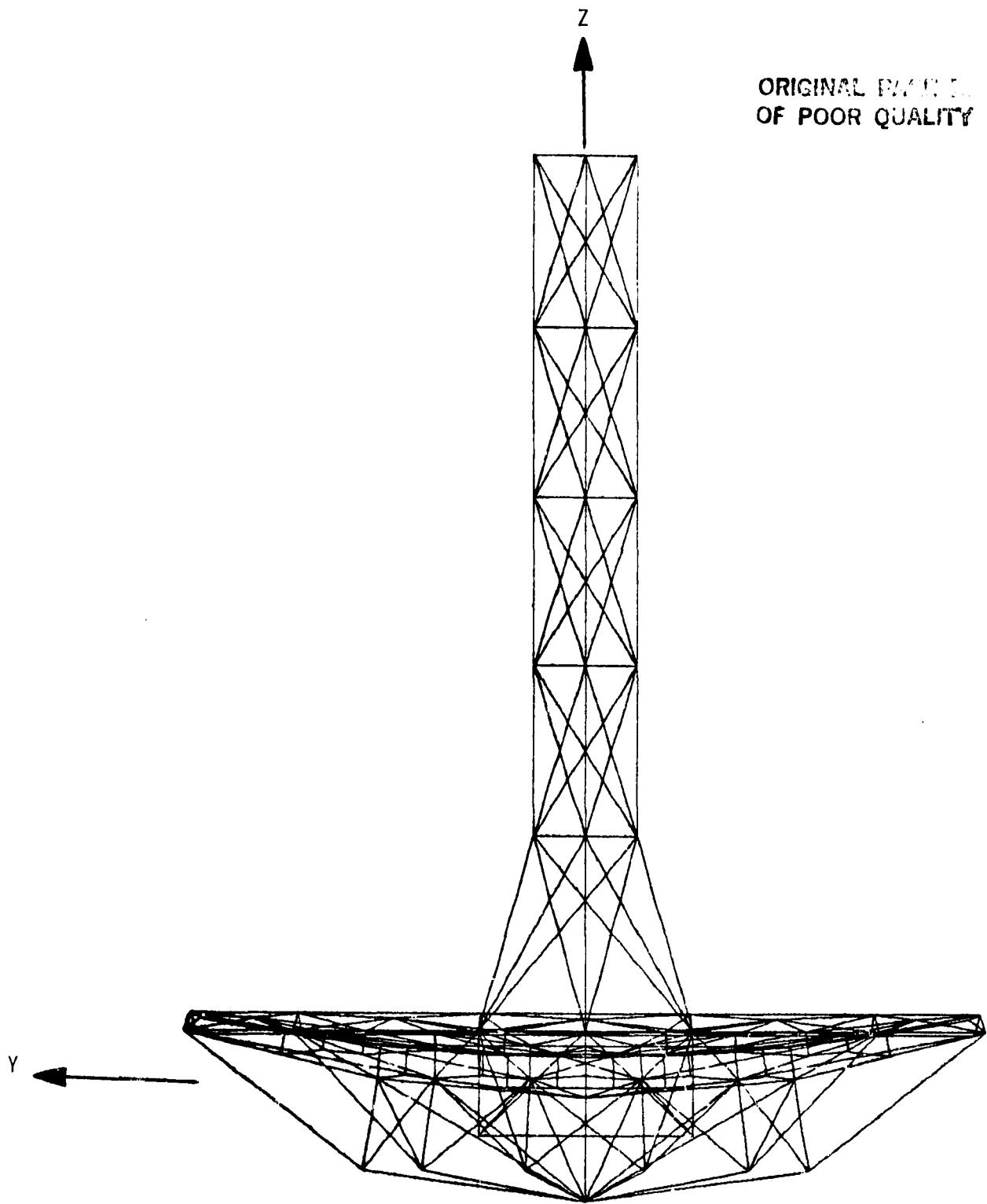


MSDA MODEL - SINGLE GORE PLOT
(SELECT NODE NUMBERS SHOWN)



MSDA (W/TOWER) MODEL, TOP VIEW (X-Y PLANE)

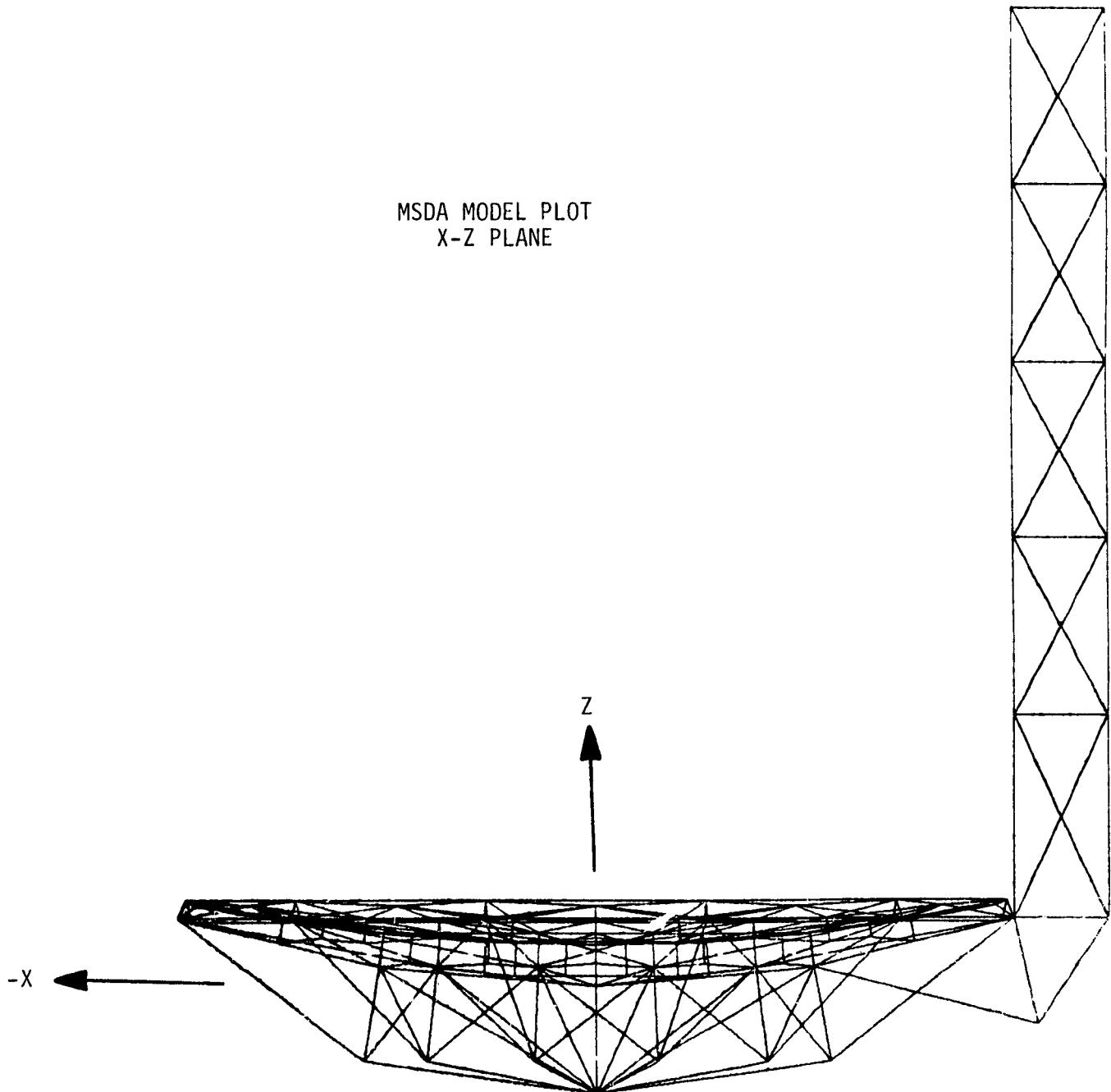
ORIGINAL PLOT
OF POOR QUALITY



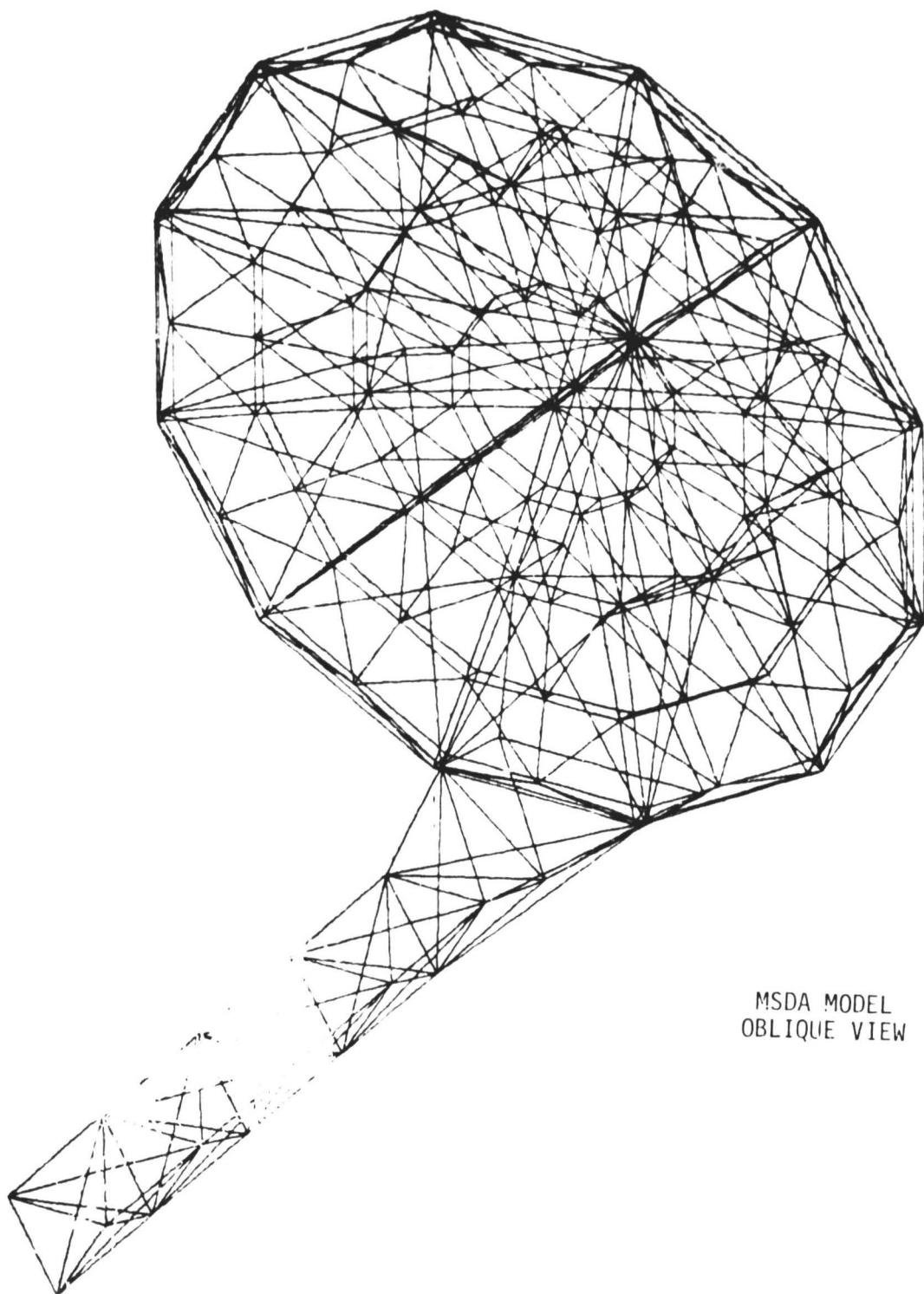
MSDA MODEL PLOT Z-Y PLANE

ORIGINAL MODEL
OF POOR QUALITY

MSDA MODEL PLOT
X-Z PLANE



ORIGIN OF THE
OF POOL CLOUD



MSDA MODEL
OBlique VIEW

ECHOSON

MECHANICALLY SCANNED DEPLOYABLE ANTENNA
DEPLOYED MODEL

CARD DECK FOR USE ON THE NON-LINEAR STRUCTURAL ANALYSIS

FUR FURTHER INFORMATION CONTACT:
RICK HARLESS (305) 729-2207 OR
RICK DEADWYLER (305) 727-4239
HARRIS GOVERNMENT ELECTRONIC SYSTEMS DIVISION
P.O. BOX 27
MELBOURNE FLORIDA 32901

IC	NO	NAME	T,D,X	G,D,Y	D1	DXY	DENSITY	CRT-X	CRT-Y	
21.			708.002							
22.			1 1 0 0 0 0		5 .6283105		6		.002500	
23.										
24.										
25.	IC	NO	NAME	T,D,X	G,D,Y	D1	DXY	DENSITY	CRT-X	CRT-Y
26.		1	MESH	2.50	.00	1.20	.80		1.0	
27.		2FRONT		1494.					1.0	
28.		3 BACK		1494.					1.0	
29.		4OBINT		2988.					1.0	
30.		5 INT		30.					1.0	
31.		6SUTIL		300.					1.0	
32.		7STRIP		15.7E+6					1.0	
33.		8STRIP		15.7E+6					1.0	
34.		9 HUB		18.3E+6					1.0	
35.		10 RIB		16.3E+6					1.0	
36.		11 HOD		29.6E+6					1.0	
37.		12 HOC		29.6E+6					1.0	
38.		13TCURD		660000.					1.0	
39.		14 HUB		18.3E+6					1.0	
40.		15 HUB		18.3E+6					1.0	
41.		16STRUT		16.3E+6					1.0	
42.		17STRUT		16.3E+6					1.0	
43.		181IPSU		16.3E+6					1.0	
44.		191IPS0		18.3E+6					1.0	
45.		20INTY		2988.					1.0	
46.		21NDU								
47.		22GLUH								
48.		23								
49.	IC	NODE	REFLECTOR COORDINATES	X	Y	Z				
50.		1		3 288.97877	0.00000	29.43500				
51.		2		3 227.35321	0.00000	18.23453				
52.		3		3 154.72062	0.00000	8.44484				
53.		4		3 229.45156	0.00000	5.18960				
54.		5		3 157.17047	0.00000	-13.98591				

ORIGINAL FILE IS
OF POOR QUALITY

56	6	3	247.09549	79.60040	35.57418
57	7	5	227.15425	60.48540	19.50470
58	8	3	154.65475	41.43962	9.04544
59	9	3	79.41529	21.41324	2.41441
60	10	3	502.64581	61.049370	19.59000
61	11	3	293.25315	76.57694	17.25500
62	12	3	230.04815	61.03853	1.54500
63	13	3	157.44494	42.18725	-16.49400
64	14	3	81.37152	21.40343	-23.38900
65	15	3	168.46906	45.14115	-86.57600
66	16	0	0.00000	0.00000	0.00000
67	17	0	0.00000	0.00000	0.00000
68	18	0	0.00000	0.00000	0.00000
69	19	0	0.00000	0.00000	0.00000
70	20	0	0.00000	0.00000	0.00000
71	21	3	250.26292	144.48937	29.43596
72	22	3	196.89306	113.67660	18.23453
73	23	3	135.99199	77.36031	6.44484
74	24	3	198.71087	114.72578	5.18960
75	25	3	136.11362	78.58524	-13.98592
76	26	3	217.48929	217.48929	33.37418
77	27	3	166.28845	166.28845	19.50470
78	28	3	113.21513	113.21513	9.04584
79	29	3	58.50205	58.50205	2.41491
80	30	3	221.55211	221.55211	19.59000
81	31	3	214.67620	214.67620	17.25500
82	32	3	168.39960	168.39960	1.54300
83	33	3	115.25770	115.25770	-16.49900
84	34	3	59.56809	59.56809	-23.38900
85	35	3	123.32791	123.32791	-86.57600
86	36	0	0.00000	0.00000	0.00000
87	37	0	0.00000	0.00000	0.00000
88	38	0	0.00000	0.00000	0.00000
89	39	0	0.00000	0.00000	0.00000
90	40	0	0.00000	0.00000	0.00000
91	41	3	144.48937	250.26292	29.43596
92	42	3	113.67660	196.89306	18.23453
93	43	5	77.36031	135.99199	6.44484
94	44	3	114.72578	198.71087	5.18960
95	45	3	78.58524	136.11362	-13.98592
96	46	3	61.049370	302.04581	19.59000
97	47	3	78.57694	293.25315	17.25500
98	48	3	60.46580	227.15425	19.50470
99	49	3	41.43962	157.44494	-16.49900
100	50	3	21.41324	79.91529	2.41491
101	51	3	61.049370	302.04581	19.59000
102	52	0	0.00000	0.00000	0.00000
103	53	0	0.00000	0.00000	0.00000
104	54	3	21.40343	81.37152	-23.38900
105	55	3	45.14115	168.46906	-86.57600
106	56	0	0.00000	0.00000	0.00000
107	57	0	0.00000	0.00000	0.00000
108	58	0	0.00000	0.00000	0.00000
109	59	0	0.00000	0.00000	0.00000
110	60	0	0.00000	0.00000	0.00000

ORIGINAL PAGE IS
OF POOR QUALITY

0*****1*****2*****3*****4*****5*****6*****7*****8

111.	:	61	3	0.00000	288.47873	29.43596
112.	:	62	5	0.00000	227.35321	18.23453
113.	:	63	3	0.00000	154.72062	8.44484
114.	:	64	3	0.00000	229.45156	5.18960
115.	:	65	3	0.00000	157.17047	-13.98591
116.	:	66	3	-79.60660	297.09589	33.37419
117.	:	67	3	-10.86580	227.15425	19.50970
118.	:	68	3	-41.43962	154.65475	9.04384
119.	:	69	3	-71.41324	79.91529	2.41491
120.	:	70	3	-81.09370	302.64581	19.59000
121.	:	71	3	-78.57694	293.25315	17.25500
122.	:	72	3	-61.63853	230.03813	1.54300
123.	:	73	3	-42.18725	157.44494	-16.49900
124.	:	74	3	-21.80343	21.37152	-23.38900
125.	:	75	3	-45.1.115	168.46906	-86.57600
126.	:	76	0	0.00000	0.00000	0.00000
127.	:	77	0	0.00000	0.00000	0.00000
128.	:	78	0	0.00030	0.00000	0.00000
129.	:	79	0	0.00000	0.00000	0.00000
130.	:	80	0	0.00000	0.00000	0.00000
131.	:	81	3	-144.48937	250.26292	29.43596
132.	:	82	3	-113.67660	196.89366	18.23453
133.	:	83	3	-77.36031	133.99199	8.44484
134.	:	84	3	-114.72578	198.71087	5.18960
135.	:	85	3	-78.58524	136.11362	-13.98592
136.	:	86	3	-217.48929	217.48929	33.37418
137.	:	87	3	-166.28845	166.28845	19.50970
138.	:	88	3	-113.21513	113.21513	9.04384
139.	:	89	3	-58.50205	58.50205	2.41491
140.	:	90	3	-221.55211	221.55211	19.59000
141.	:	91	3	-214.67620	214.67620	17.25500
142.	:	92	3	-168.34960	168.39960	1.54300
143.	:	93	3	-115.25770	115.25770	-16.49900
144.	:	94	3	-59.56809	59.56809	-23.38900
145.	:	95	3	-123.32791	123.32791	-86.57600
146.	:	96	0	0.00000	0.00000	0.00000
147.	:	97	0	0.00000	0.00000	0.00000
148.	:	98	0	0.00000	0.00000	0.00000
149.	:	99	0	0.00000	0.00000	0.00000
150.	:	100	0	0.00000	0.00030	0.00000
151.	:	101	3	-250.26292	144.48937	29.43596
152.	:	102	3	-196.89366	113.67660	18.23453
153.	:	103	3	-133.99199	77.36031	8.44484
154.	:	104	3	-198.71087	114.72578	5.18960
155.	:	105	3	-136.11362	78.58524	-13.98592
156.	:	106	3	-297.09589	79.60660	33.37419
157.	:	107	3	-227.15425	60.86580	19.50970
158.	:	108	3	-154.65475	41.43962	9.04384
159.	:	109	3	-79.91529	21.41324	2.41491
160.	:	110	3	-302.64581	81.09370	19.59000
161.	:	111	3	-243.25315	78.57694	17.25500
162.	:	112	3	-230.03813	61.63853	1.54300
163.	:	113	3	-157.44494	42.18725	-16.49900
164.	:	114	3	-81.37152	21.80343	-23.38900
165.	:	115	3	-168.46906	45.14115	-86.57600

**ORIGINAL PAGE IS
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OF POOR QUALITY

281.	171	3 -78.57694-29.225315	17.25600
222.	172	3 -61.93453-230.03113	1.54500
273.	173	3 -42.18725-157.44494	-16.49400
224.	174	3 -21.0343-81.37152	-23.36900
225.	175	3 -45.14115-68.46906	-86.57600
226.	176	0 0.0000	0.00000
227.	177	0 0.0000	0.00000
228.	178	0 0.0000	0.00000
229.	179	0 0.0000	0.00000
230.	180	0 0.0000	0.00000
231.	181	3 0.0000-288.47113	29.43596
232.	182	3 0.0000-227.35321	16.23451
233.	183	3 0.0000-154.20062	0.48884
234.	184	3 0.0000-229.45156	5.98601
235.	185	3 0.0000-157.17047	-13.9891
236.	186	3 79.60660-297.09589	33.37419
237.	187	3 60.86580-227.15425	19.50970
238.	188	3 41.43962-154.65475	9.03384
239.	189	3 21.41324-79.91529	2.41491
240.	190	3 51.09370-302.64651	19.59000
241.	191	3 74.57694-264.52351	17.25500
242.	192	3 41.34853-230.03163	1.54300
243.	193	3 42.18225-157.44494	-16.49400
244.	194	3 21.0343-81.37152	-23.36900
245.	195	3 45.14115-168.46906	-86.57600
246.	196	0 0.0000	0.00000
247.	197	0 0.0000	0.00000
248.	198	0 0.0000	0.00000
249.	199	0 0.0000	0.00000
250.	200	0 0.0000	0.00000
251.	201	3 144.46937-250.20292	29.43596
252.	202	3 113.67660-196.49366	18.23453
253.	203	3 77.36031-133.99199	8.44484
254.	204	3 114.72578-198.71087	5.18960
255.	205	3 76.58524-136.11362	-13.98592
256.	206	3 217.48429-217.48429	33.37418
257.	207	3 166.28845-160.28845	19.50970
202.	208	3 113.25115-115.21513	9.03384
258.	209	3 54.50205-58.50205	2.41491
259.	210	3 221.55211-221.55211	19.59000
260.	211	3 214.67620-214.67620	1.25500
261.	212	3 166.59960-166.59960	1.54300
266.	213	3 113.25770-115.25770	-16.49400
267.	214	3 59.56809-59.56809	-23.36900
268.	215	0 0.0000	0.00000
269.	216	0 0.0000	0.00000
270.	217	0 0.0000	0.00000
271.	221	3 250.26292-144.48937	29.43596
272.	222	3 196.69366-115.67660	18.23453
273.	223	3 133.99199-77.36031	8.44484
274.	224	3 198.71087-114.72578	5.18960
275.	225	3 136.11362-78.58524	-13.98592

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276. : 226 3 297.09584 -79.60660 33.37418
277. : 227 3 227.15425 -60.86580 19.50970
278. : 228 3 154.65475 -41.43962 9.04384
279. : 229 3 79.41524 -21.41524 2.41491
280. : 230 3 302.64581 -81.09570 19.59000
281. : 231 3 293.25315 -78.57694 17.25500
282. : 232 3 230.03813 -61.63853 1.54300
283. : 233 3 157.44494 -42.18725 -16.49900
284. : 234 3 81.37152 -21.40343 -23.38900
285. : 235 3 1e8.46406 -45.14115 -86.57600
286. : 236 0 0.00000 0.00000 0.00000
287. : 237 0 0.00000 0.00000 0.00000
288. : 238 0 0.00000 0.00000 0.00000
289. : 239 0 0.00000 0.00000 0.00000
290. : 240 0 0.00000 0.00000 0.00000
291. : 241 3 0.00000 0.00000 0.06000
292. : 242 3 0.00000 0.00000 -30.75900
293. : 243 3 0.00000 0.00000-104.86300
294. :END
295. :GLUH
296. :C ADDITIONAL COORDINATES FOR DEFINITION OF SPECIAL COORDINATE SYSTEMS
297. :C NODE X Y Z
298. : 245 0.0 0.0 0.0
299. : 246 422.340 0.0 61.718
300. : 247 223.920 0.0 742.032
301. : 248 72.704 0.0 0.0
302. : 249 394.428 0.0 946.986
303. : 250 1000. 0.0 100.
304. :END
305. :SYS1
306. :C THESE SPECIAL COORDINATE SYSTEMS ARE USED AS FOLLOWS
307. :C SYSTEM 3 IS A CYLINDRICAL POLAR SYSTEM FOR DISPLAY OF STRUCTURAL
308. :C DISPLACEMENTS. THE GLOBAL 'Z' AXIS IS THE AXIS OF SYMMETRY.
309. :C THUS IN VIEWING DISPLACEMENTS, DOF1 IS A RADIAL DISPLACEMENT
310. :C AND DOF2 AND DOF3 ARE CIRCUMFERENTIAL AND BORE AXIS 'OR Z'
311. :C DISPLACEMENTS.
312. :C NOTE, FORCES (APPLIED LOADS) ARE ALSO IN THIS SYSTEM.
313. :C SYSTEM 5 IS A CARTESIAN SYSTEM THAT DEFINES THE VERTEX AND
314. :C BORE AXIS OF THE OFFSET PARABOLA. JA (246) TO JB (247)
315. :C DEFINES THE BORE AXIS (POINTING DIRECTION) OF THE ANTENNA.
316. :C SYSTEM 6 IS A SYSTEM THAT DEFINES THE SPIN AXIS OF THE SYSTEM
317. :C WITH RESPECT TO THE REFLECTOR.
318. :C JA (248) TO JB (249) DEFINES THE SPIN AXIS.
319. :C THIS SYSTEM IS ALSO USED TO DISPLAY THE WEIGHT MOMENTS OF
320. :C INERTIA OF THE SYSTEM.
321. : 6 248 249 250
322. : 3 3
323. : 5 246 247 250
324. :END
325. :STRI
326. :C STRINGER ELEMENT TABLE.
327. :C THESE ARE PRETENSIONED, AXIAL LOAD ELEMENTS.
328. :C JA JB MATL AREA PRELOAD
329. :C THESE ARE OUTBOARD INTERCOSTALS
330. : 1 6 4 1.00 5.69

0*****1*****2*****3*****4*****5*****6*****7*****8

331.	:	21	26	4	1.00	5.69
332.	:	41	46	4	1.00	5.69
333.	:	61	66	4	1.00	5.69
334.	:	81	86	4	1.00	5.69
335.	:	101	106	4	1.00	5.69
336.	:	121	126	4	1.00	5.69
337.	:	141	146	4	1.00	5.69
338.	:	161	166	4	1.00	5.69
339.	:	181	186	4	1.00	5.69
340.	:	201	206	4	1.00	5.69
341.	:	221	226	4	1.00	5.69
342.	:	6	21	4	1.00	5.69
343.	:	26	41	4	1.00	5.69
344.	:	46	61	4	1.00	5.69
345.	:	66	81	4	1.00	5.69
346.	:	86	101	4	1.00	5.69
347.	:	106	121	4	1.00	5.69
348.	:	126	141	4	1.00	5.69
349.	:	146	161	4	1.00	5.69
350.	:	166	181	4	1.00	5.69
351.	:	186	201	4	1.00	5.69
352.	:	206	221	4	1.00	5.69
353.	:	226	1	4	1.00	5.69
354.	:C	THESE ARE FRONT SURFACE COORDS				
355.	:	6	26	2	5.00	7.19
356.	:	26	46	2	5.00	7.19
357.	:	46	66	2	5.00	7.19
358.	:	66	86	2	5.00	7.19
359.	:	86	106	2	5.00	7.19
360.	:	106	126	2	5.00	7.19
361.	:	126	146	2	5.00	7.19
362.	:	146	166	2	5.00	7.19
363.	:	166	186	2	5.00	7.19
364.	:	186	206	2	5.00	7.19
365.	:	206	226	2	5.00	7.19
366.	:	226	6	2	5.00	7.19
367.	:	2	7	2	10.0	14.2
368.	:	22	27	2	10.0	14.2
369.	:	42	47	2	10.0	14.2
370.	:	62	67	2	10.0	14.2
371.	:	82	87	2	10.0	14.2
372.	:	102	107	2	10.0	14.2
373.	:	122	127	2	10.0	14.2
374.	:	142	147	2	10.0	14.2
375.	:	162	167	2	10.0	14.2
376.	:	182	187	2	10.0	14.2
377.	:	202	207	2	10.0	14.2
378.	:	222	227	2	10.0	14.2
379.	:	7	22	2	10.0	14.2
380.	:	27	42	2	10.0	14.2
381.	:	47	62	2	10.0	14.2
382.	:	67	82	2	10.0	14.2
383.	:	87	102	2	10.0	14.2
384.	:	107	122	2	10.0	14.2
385.	:	127	142	2	10.0	14.2

CRITICAL POINTS
OF POOR QUALITY

**ORIGINAL PAGE IS
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ORIGINAL PLATE
OF POOR QUALITY

441	24	32	3	10.0	5.72
442	44	52	3	10.0	5.72
443	64	72	3	10.0	5.72
444	64	92	3	10.0	5.72
445	104	112	3	10.0	5.72
446	124	132	3	10.0	5.72
447	144	152	3	10.0	5.72
448	164	172	3	10.0	5.72
449	184	192	3	10.0	5.72
450	204	212	3	10.0	5.72
451	224	232	3	10.0	5.72
452	12	24	3	10.0	5.72
453	32	44	3	10.0	5.72
454	52	64	3	10.0	5.72
455	72	84	3	10.0	5.72
456	92	104	3	10.0	5.72
457	112	124	3	10.0	5.72
458	132	144	3	10.0	5.72
459	152	164	3	10.0	5.72
460	172	184	3	10.0	5.72
461	192	204	3	10.0	5.72
462	212	224	3	10.0	5.72
463	232	4	3	10.0	5.72
464	5	13	3	10.0	5.89
465	25	33	3	10.0	5.89
466	45	53	3	10.0	5.89
467	65	73	3	10.0	5.89
468	85	93	3	10.0	5.89
469	105	113	3	10.0	5.89
470	125	133	3	10.0	5.89
471	145	153	3	10.0	5.89
472	165	173	3	10.0	5.89
473	185	193	3	10.0	5.89
474	205	213	3	10.0	5.89
475	225	233	3	10.0	5.89
476	13	25	3	10.0	5.89
477	33	45	3	10.0	5.89
478	53	65	3	10.0	5.89
479	73	85	3	10.0	5.89
480	93	105	3	10.0	5.89
481	113	125	3	10.0	5.89
482	133	145	3	10.0	5.89
483	153	165	3	10.0	5.89
484	173	185	3	10.0	5.89
485	193	205	3	10.0	5.89
486	213	225	3	10.0	5.89
487	233	5	3	10.0	5.89
488	14	34	3	12.0	4.50
489	34	54	3	15.0	4.50
490	54	74	3	15.0	4.50
491	74	94	3	15.0	4.50
492	94	114	3	15.0	4.50
493	114	134	3	15.0	4.50
494	134	154	3	15.0	4.50
495	154	174	3	15.0	4.50

**ORIGINAL PRINTING
OF POOR QUALITY**

		THE OUTBOARD DIAGONALS		THE VERTICAL LINES	
446.	174	194	3	15.0	4.50
497.	194	214	3	15.0	4.50
448.	214	234	3	15.0	4.50
499.	234	14	3	15.0	4.50
500.	101	110	20	1.00	1.24
501.	201	210	20	1.00	1.24
502.	221	230	20	1.00	1.24
503.	10	21	20	1.00	1.24
504.	61	70	20	1.00	1.24
505.	61	90	20	1.00	1.24
506.	101	110	20	1.00	1.24
507.	141	150	20	1.00	1.24
508.	161	170	20	1.00	1.24
509.	181	190	20	1.00	1.24
510.	201	210	20	1.00	1.24
511.	221	230	20	1.00	1.24
512.	10	21	20	1.00	1.24
513.	30	41	20	1.00	1.24
514.	50	61	20	1.00	1.24
515.	70	81	20	1.00	1.24
516.	79	91	20	1.00	1.24
517.	90	101	20	1.00	1.24
518.	110	121	20	1.00	1.24
519.	130	141	20	1.00	1.24
520.	150	161	20	1.00	1.24
521.	170	181	20	1.00	1.24
522.	190	201	20	1.00	1.24
523.	210	221	20	1.00	1.24
524.	230	1	20	1.00	1.24
525.	250	2	20	1.00	1.24
526.	270	22	5	10.0	0.685
527.	29	24	5	10.0	0.685
528.	42	44	5	10.0	0.685
529.	62	64	5	10.0	0.685
530.	82	84	5	10.0	0.685
531.	102	104	5	10.0	0.685
532.	122	124	5	10.0	0.685
533.	142	144	5	10.0	0.685
534.	162	164	5	10.0	0.685
535.	182	184	5	10.0	0.685
536.	202	204	5	10.0	0.685
537.	222	224	5	10.0	0.685
538.	23	5	5	10.0	0.685
539.	25	25	5	10.0	0.685
540.	43	45	5	10.0	0.465
541.	63	65	5	10.0	0.465
542.	83	85	5	10.0	0.465
543.	103	105	5	10.0	0.465
544.	123	125	5	10.0	0.465
545.	143	145	5	10.0	0.465
546.	163	165	5	10.0	0.465
547.	183	185	5	10.0	0.465
548.	203	205	5	10.0	0.465
549.	223	225	5	10.0	0.465
550.	243	245	6	5.00	51.1

**ORIGINAL PAGE IS
OF POOR QUALITY**

0*****2*****3*****6*****7*****8

551	26	30	6	5.00	51.1
552	46	50	6	5.00	51.1
553	66	70	6	5.00	51.1
554	86	90	6	5.00	51.1
555	106	110	6	5.00	51.1
556	126	130	6	5.00	51.1
557	146	150	6	5.00	51.1
558	166	170	6	5.00	51.1
559	186	190	6	5.00	51.1
560	206	210	6	5.00	51.1
561	226	230	6	5.00	51.1
562	7	12	6	10.0	1.73
563	27	32	6	10.0	1.73
564	47	52	6	10.0	1.73
565	67	72	6	10.0	1.73
566	87	92	6	10.0	1.73
567	107	112	6	10.0	1.73
568	127	132	6	10.0	1.73
569	147	152	6	10.0	1.73
570	167	172	6	10.0	1.73
571	187	192	6	10.0	1.73
572	207	212	6	10.0	1.73
573	227	232	6	10.0	1.73
574	8	13	6	10.0	1.19
575	25	33	6	10.0	1.19
576	48	53	6	10.0	1.19
577	68	73	6	10.0	1.19
578	88	93	6	10.0	1.19
579	108	113	6	10.0	1.19
580	128	133	6	10.0	1.19
581	148	153	6	10.0	1.19
582	168	173	6	10.0	1.19
583	188	193	6	10.0	1.19
584	208	213	6	10.0	1.19
585	228	233	6	10.0	1.19
586	9	14	6	15.0	0.946
587	29	34	6	15.0	0.946
588	69	54	6	15.0	0.946
589	69	74	6	15.0	0.946
590	89	94	6	15.0	0.946
591	109	114	6	15.0	0.946
592	129	134	6	15.0	0.946
593	149	154	6	15.0	0.946
594	169	174	6	15.0	0.946
595	189	194	6	15.0	0.946
596	209	214	6	15.0	0.946
597	229	234	6	15.0	0.946
598	249	242	6	12.0	0.505
599	11	11	18	2.770E-03	-54.1
600	21	21	18	2.770E-03	-54.1
601	31	31	18	2.770E-03	-54.1
602	51	51	18	2.770E-03	-54.1
603	71	71	18	2.770E-03	-54.1
604	91	91	18	2.770E-03	-54.1
605	111	106	18	2.770E-03	-54.1

THESE ARE THE TIP STANDOFFS (COMPRESSION MEMBERS)

ORIGINAL PAGE IS
OF POOR QUALITY

606.	126	131	16 2.770E-05	-54.1
607.	146	151	16 2.770E-05	-54.1
608.	166	171	16 2.770E-05	-54.1
609.	186	191	16 2.770E-05	-54.1
610.	206	211	16 2.770E-05	-54.1
611.	226	231	16 2.770E-05	-54.1
612.	C	THESE ARE THE FRONT RUUNIAY LUPUS		
613.	0	7	7 1.970E-02	24.0
614.	20	27	7 1.970E-02	24.0
615.	46	47	7 1.970E-02	24.0
616.	66	67	7 1.970E-02	24.0
617.	86	87	7 1.970E-02	24.0
618.	106	107	7 1.970E-02	24.0
619.	126	127	7 1.970E-02	24.0
620.	146	147	7 1.970E-02	24.0
621.	166	167	7 1.970E-02	24.0
622.	186	187	7 1.970E-02	24.0
623.	206	207	7 1.970E-02	24.0
624.	226	227	7 1.970E-02	24.0
625.	7	6	7 1.970E-02	17.1
626.	27	28	7 1.970E-02	17.1
627.	47	48	7 1.970E-02	17.1
628.	67	68	7 1.970E-02	17.1
629.	87	88	7 1.970E-02	17.1
630.	107	108	7 1.970E-02	17.1
631.	127	128	7 1.970E-02	17.1
632.	147	148	7 1.970E-02	17.1
633.	167	168	7 1.970E-02	17.1
634.	187	188	7 1.970E-02	17.1
635.	207	208	7 1.970E-02	17.1
636.	227	228	7 1.970E-02	17.1
637.	8	9	7 1.970E-02	10.4
638.	28	29	7 1.970E-02	10.4
639.	48	49	7 1.970E-02	10.4
640.	68	69	7 1.970E-02	10.4
641.	88	89	7 1.970E-02	10.4
642.	108	109	7 1.970E-02	10.4
643.	128	129	7 1.970E-02	10.4
644.	148	149	7 1.970E-02	10.4
645.	168	169	7 1.970E-02	10.4
646.	188	189	7 1.970E-02	10.4
647.	208	209	7 1.970E-02	10.4
648.	228	229	7 1.970E-02	10.4
649.	9	241	7 1.000E-08	1.000
650.	29	241	7 1.000E-08	1.000
651.	49	241	7 1.000E-08	1.000
652.	69	241	7 1.000E-08	1.000
653.	89	241	7 1.000E-08	1.000
654.	109	241	7 1.000E-08	1.000
655.	129	241	7 1.000E-08	1.000
656.	149	241	7 1.000E-08	1.000
657.	169	241	7 1.000E-08	1.000
658.	189	241	7 1.000E-08	1.000
659.	209	241	7 1.000E-08	1.000
660.	229	241	7 1.000E-08	1.000

ORIGINAL PAGE IS
OF POOR QUALITY

0*****1*****2*****3*****4*****5*****6*****7*****8

:C THESE ARE THE RIAs (COMPRESSION MEMPHIS)

601-

662-	10	11	9	0.295	-64.9
663-	30	31	9	0.295	-64.9
664-	50	51	9	0.295	-64.9
665-	70	71	9	0.295	-64.9
666-	90	91	9	0.295	-64.9
667-	110	111	9	0.295	-64.9
668-	130	131	9	0.295	-64.9
669-	150	151	9	0.295	-64.9
670-	170	171	9	0.295	-64.9
671-	190	191	9	0.295	-64.9
672-	210	211	9	0.295	-64.9
673-	230	231	9	0.295	-64.9
674-	11	12	9	0.295	-91.6
675-	31	32	9	0.295	-91.6
676-	51	52	9	0.295	-91.6
677-	71	72	9	0.295	-91.6
678-	91	92	9	0.295	-91.6
679-	111	112	9	0.295	-91.6
680-	131	132	9	0.295	-91.6
681-	151	152	9	0.295	-91.6
682-	171	172	9	0.295	-91.6
683-	191	192	9	0.295	-91.6
684-	211	212	9	0.295	-91.6
685-	231	232	9	0.295	-91.6
686-	12	13	9	0.295	-94.5
687-	32	33	9	0.295	-94.5
688-	52	53	9	0.295	-94.5
689-	72	73	9	0.295	-94.5
690-	92	93	9	0.295	-94.5
691-	112	113	9	0.295	-94.5
692-	132	133	9	0.295	-94.5
693-	152	153	9	0.295	-94.5
694-	172	173	9	0.295	-94.5
695-	192	193	9	0.295	-94.5
696-	212	213	9	0.295	-94.5
697-	232	233	9	0.295	-94.5
698-	13	14	9	0.295	-101.
699-	33	34	9	0.295	-101.
700-	53	54	9	0.295	-101.
705-	153	154	9	0.295	-101.
706-	173	174	9	0.295	-101.
707-	193	194	9	0.295	-101.
708-	213	214	9	0.295	-101.
709-	233	234	9	0.295	-101.
710-	14	242	9	0.295	-103.
711-	34	242	9	0.295	-103.
712-	54	242	9	0.295	-103.
713-	74	242	9	0.295	-103.
714-	94	242	9	0.295	-103.
715-	114	242	9	0.295	-103.

**ORIGINAL PAGE IS
OF POOR QUALITY**

**ORIGINAL PAGE IS
OF POOR QUALITY**

771.	233	243	11	1.636E-02	11.3
772.	10	30	11	1.00	22.5
773.	50	50	11	1.00	22.5
774.	50	70	11	1.00	22.5
775.	70	90	11	1.00	22.5
776.	90	110	11	1.00	22.5
777.	110	130	11	1.00	22.5
778.	130	150	11	1.00	22.5
779.	150	150	11	1.00	22.5
780.	170	170	11	1.00	22.5
781.	170	190	11	1.00	22.5
782.	190	210	11	1.00	22.5
783.	210	230	11	1.00	22.5
784.	230	10	11	1.00	22.5
785.	10	33	15	1.00	10.00
786.	33	50	13	1.00	10.00
787.	50	73	13	1.00	10.00
788.	73	90	13	1.00	10.00
789.	90	113	13	1.00	10.00
790.	113	130	13	1.00	10.00
791.	130	153	13	1.00	10.00
792.	153	170	13	1.00	10.00
793.	170	193	13	1.00	10.00
794.	193	210	13	1.00	10.00
795.	210	233	13	1.00	10.00
796.	233	10	13	1.00	10.00
797.	13	35	13	1.00	15.0
798.	33	55	13	1.00	15.0
799.	55	75	13	1.00	15.0
800.	75	95	13	1.00	15.0
801.	95	115	13	1.00	15.0
802.	113	135	13	1.00	15.0
803.	133	155	13	1.00	15.0
804.	153	175	13	1.00	15.0
805.	173	195	13	1.00	15.0
806.	193	215	13	1.00	15.0
807.	213	235	13	1.00	15.0
808.	233	15	13	1.00	15.0
809.	33	15	13	1.00	15.0
810.	53	35	13	1.00	15.0
811.	73	55	13	1.00	15.0
812.	93	75	13	1.00	15.0
813.	113	95	13	1.00	15.0
814.	133	115	13	1.00	15.0
815.	153	135	13	1.00	15.0
816.	173	155	13	1.00	15.0
817.	193	175	13	1.00	15.0
818.	213	195	13	1.00	15.0
819.	233	215	13	1.00	15.0
820.	15	235	13	1.00	15.0
821.	242	243	14	5.56	-97.4
822.	30	53	13	1.00	10.00
823.	53	70	13	1.00	10.00

ORIGINAL PAGE IS
OF POOR QUALITY

**ORIGINAL EDITION
OF POOR QUALITY**

Установка и настройка 2000/2000/3000/4000/5000/6000

ITEM	MEMBRANE MATERIAL AXES ROTATION ANGLES.
986.	
987.	
988.	
989.	
990.	
IC	ANGLE
IC ELEMENT NUBS.	
:	1 12 1
:	37 48 1
:	6 6 6
:	6 6 -6
	0.4503
	-0.4503

ORIGINAL FILE
OF POOR QUALITY

**ORIGINAL PAGE IS
OF POOR QUALITY**

ORIGINAL PAGE IS
OF POOR QUALITY

1101	30	0.461	-1.677E-12	0.00
1102	31	1.49	-5.421E-12	0.00
1103	32	2.75	-1.000E-11	0.00
1104	33	4.15	-1.510E-11	0.00
1105	34	3.11	-1.131E-11	0.00
1106	35	1.23	-4.475E-12	0.00
1107	36	0.00	0.00	0.00
1108	37	0.00	0.00	0.00
1109	38	0.00	0.00	0.00
1110	39	0.00	0.00	0.00
1111	40	0.00	0.00	0.00
1112	41	9.143E-02	-3.326E-13	0.00
1113	42	0.152	-5.530E-13	0.00
1114	43	0.118	-4.293E-13	0.00
1115	44	1.659E-02	-6.763E-14	0.00
1116	45	1.279E-02	-4.653E-14	0.00
1117	46	0.193	-7.021E-13	0.00
1118	47	0.354	-1.268E-12	0.00
1119	48	0.311	-1.131E-12	0.00
1120	49	0.321	-1.168E-12	0.00
1121	50	0.461	-1.677E-12	0.00
1122	51	1.49	-5.421E-12	0.00
1123	52	2.75	-1.000E-11	0.00
1124	53	4.15	-1.510E-11	0.00
1125	54	3.11	-1.131E-11	0.00
1126	55	1.23	-4.475E-12	0.00
1127	56	0.00	0.00	0.00
1128	57	0.00	0.00	0.00
1129	58	0.00	0.00	0.00
1130	59	0.00	0.00	0.00
1131	60	0.00	0.00	0.00
1132	61	9.143E-02	-3.326E-13	0.00
1133	62	0.152	-5.530E-13	0.00
1134	63	0.118	-4.293E-13	0.00
1135	64	1.659E-02	-6.763E-14	0.00
1136	65	1.279E-02	-4.653E-14	0.00
1137	66	0.193	-7.021E-13	0.00
1138	67	0.354	-1.268E-12	0.00
1139	68	0.311	-1.131E-12	0.00
1140	69	0.321	-1.168E-12	0.00
1141	70	0.461	-1.677E-12	0.00
1142	71	1.49	-5.421E-12	0.00
1143	72	2.75	-1.000E-11	0.00
1144	73	4.15	-1.510E-11	0.00
1145	74	3.11	-1.131E-11	0.00
1146	75	1.23	-4.475E-12	0.00
1147	76	0.00	0.00	0.00
1148	77	0.00	0.00	0.00
1149	78	0.00	0.00	0.00
1150	79	0.00	0.00	0.00
1151	80	0.00	0.00	0.00
1152	81	9.143E-02	-3.326E-13	0.00
1153	82	0.152	-5.530E-13	0.00
1154	83	0.118	-4.293E-13	0.00
1155	84	1.659E-02	-6.763E-14	0.00

ORIGINAL PAGE IS
OF POOR QUALITY

1156.	85	1.279E-02-4.653E-14	0.00
1157.	86	0.193	-7.021E-13
1158.	87	0.354	-1.288E-12
1159.	88	0.311	-1.131E-12
1160.	89	0.321	-1.168E-12
1161.	90	0.461	-1.677E-12
1162.	91	1.49	-5.421E-12
1163.	92	2.75	-1.000E-11
1164.	93	4.15	-1.540E-11
1165.	94	3.11	-1.151E-11
1166.	95	1.23	-4.475E-12
1167.	96	0.00	0.00
1168.	97	0.00	0.00
1169.	98	0.00	0.00
1170.	99	0.00	0.00
1171.	100	0.00	0.00
1172.	101	0.143E-02-3.326E-13	0.00
1173.	102	0.152	-5.530E-13
1174.	103	0.118	-4.293E-13
1175.	104	1.859E-02-6.753E-14	0.00
1176.	105	1.279E-02-4.653E-14	0.00
1177.	106	0.193	-7.021E-13
1178.	107	0.354	-1.288E-12
1179.	108	0.311	-1.131E-12
1180.	109	0.321	-1.168E-12
1181.	110	0.461	-1.677E-12
1182.	111	1.49	-5.421E-12
1183.	112	2.75	-1.000E-11
1184.	113	4.15	-1.540E-11
1185.	114	3.11	-1.151E-11
1186.	115	1.23	-4.475E-12
1187.	116	0.00	0.00
1188.	117	0.00	0.00
1189.	118	0.00	0.00
1190.	119	0.00	0.00
1191.	120	0.00	0.00
1192.	121	9.143E-02-3.326E-13	0.00
1193.	122	0.152	-5.530E-13
1194.	123	0.118	-4.293E-13
1195.	124	1.859E-02-6.763E-14	0.00
1196.	125	1.279E-02-4.653E-14	0.00
1197.	126	0.193	-7.021E-13
1198.	127	0.354	-1.288E-12
1199.	128	0.311	-1.131E-12
1200.	129	0.321	-1.168E-12
1201.	130	0.461	-1.677E-12
1202.	131	1.49	-5.421E-12
1203.	132	2.75	-1.000E-11
1204.	133	4.15	-1.540E-11
1205.	134	3.11	-1.151E-11
1206.	135	1.23	-4.475E-12
1207.	136	0.00	0.00
1208.	137	0.76	0.00
1209.	138	0.00	0.00
1210.	139	0.00	0.00

ORIGINAL PAGE IS
OF POOR QUALITY

1211	140	0.00	0.00	0.00	0.00
1212	141	$9.143E-02-3.326t-13$	0.00	0.00	0.00
1213	142	$-5.530t-13$	0.00	0.00	0.00
1214	143	0.152	$-5.530t-13$	0.00	0.00
1215	144	0.118	$-4.293t-13$	0.00	0.00
1216	145	$1.859E-02-6.763t-14$	0.00	0.00	0.00
1217	146	$1.279E-02-4.653t-14$	0.00	0.00	0.00
1218	147	0.193	$-7.021t-13$	0.00	0.00
1219	148	0.354	$-1.288t-12$	0.00	0.00
1220	149	0.311	$-1.131t-12$	0.00	0.00
1221	150	0.321	$-1.168t-12$	0.00	0.00
1222	151	0.461	$-1.677t-12$	0.00	0.00
1223	152	1.49	$-5.421t-12$	0.00	0.00
1224	153	2.75	$-1.000t-11$	0.00	0.00
1225	154	4.15	$-1.510t-11$	0.00	0.00
1226	155	3.11	$-1.131t-11$	0.00	0.00
1227	156	1.23	$-4.475t-12$	0.00	0.00
1228	157	0.90	0.00	0.00	0.00
1229	158	0.00	0.00	0.00	0.00
1230	159	0.00	0.00	0.00	0.00
1231	160	0.00	0.00	0.00	0.00
1232	161	$9.143E-02-3.326t-13$	0.00	0.00	0.00
1233	162	0.152	$-5.530t-13$	0.00	0.00
1234	163	0.118	$-4.293t-13$	0.00	0.00
1235	164	$1.859E-02-6.763t-14$	0.00	0.00	0.00
1236	165	$1.279E-02-4.653t-14$	0.00	0.00	0.00
1237	166	0.193	$-7.021t-13$	0.00	0.00
1238	167	0.354	$-1.288t-12$	0.00	0.00
1239	168	0.311	$-1.131t-12$	0.00	0.00
1240	169	0.321	$-1.168t-12$	0.00	0.00
1241	170	0.461	$-1.677t-12$	0.00	0.00
1242	171	1.49	$-5.421t-12$	0.00	0.00
1243	172	2.75	$-1.000t-11$	0.00	0.00
1244	173	4.15	$-1.510t-11$	0.00	0.00
1245	174	3.11	$-1.131t-11$	0.00	0.00
1246	175	1.23	$-4.475t-12$	0.00	0.00
1247	176	0.90	0.00	0.00	0.00
1248	177	0.00	0.00	0.00	0.00
1249	178	0.00	0.00	0.00	0.00
1250	179	0.00	0.00	0.00	0.00
1251	180	0.00	0.00	0.00	0.00
1252	181	$9.143E-02-3.326t-13$	0.00	0.00	0.00
1253	182	0.152	$-5.530t-13$	0.00	0.00
1254	183	0.118	$-4.293t-13$	0.00	0.00
1255	184	$1.859E-02-6.763t-14$	0.00	0.00	0.00
1256	185	$1.279E-02-4.653t-14$	0.00	0.00	0.00
1257	186	0.193	$-7.021t-13$	0.00	0.00
1258	187	0.354	$-1.288t-12$	0.00	0.00
1259	188	0.311	$-1.131t-12$	0.00	0.00
1260	189	0.321	$-1.168t-12$	0.00	0.00
1261	190	0.461	$-1.677t-12$	0.00	0.00
1262	191	1.45	$-5.421t-12$	0.00	0.00
1263	192	2.75	$-1.000t-11$	0.00	0.00
1264	193	4.15	$-1.510t-11$	0.00	0.00
1265	194	3.11	$-1.131t-11$	0.00	0.00

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MECHANICALLY SCANNED DEPLOYABLE ANTENNA

DEPLOYED MODE

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MUSICAL FORMS AND SYSTEMS IN THE SONGS

XOB 80.0.4

FURTHER INFORMATION CONTACT:

KICK HAWKLESS (305) 729-2207 08

ביכר של אדריכל צביה (1905-1972)

BEGIN PROCESSING MATL FILE.
BEGIN PROCESSING GLOB FILE.
BEGIN PROCESSING GLOB FILE.
BEGIN PROCESSING SYSI FILE.
BEGIN PROCESSING STRI FILE.
BEGIN PROCESSING MEMB FILE.
BEGIN PROCESSING TUM FILE.
BEGIN PROCESSING BEAM FILE.
BEGIN PROCESSING DATA FILE.
BEGIN PROCESSING MATL FILE.
BEGIN PROCESSING GLOB FILE.
BEGIN PROCESSING DATA FILE.
BEGIN PROCESSING BEAM FILE.
BEGIN PROCESSING REST FILE.

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THE FOLLOWING NUDGES ARE REFERENCE NUDGES ONLY

16	17	18	19	20	36	37	38	39	40	56	57	58	59	60	76	77	78	79	80
96	97	98	99	100	116	117	118	119	120	136	137	138	139	140	156	157	158	159	160
176	177	178	179	180	196	197	198	199	200	216	217	218	219	220	236	237	238	239	240
244	245	246	247	248	249	250	254	255	256	257	258	259							

BEGIN PROCESSING WIGHT FILE.
BEGIN PROCESSING DUNE FILE.

THE FOLLOWING FILES WHERE PROCESSED IN THE ORDER SHOWN.

1. MATL
2. GLOB
3. GLOB
4. SYST
5. STRI
6. MEMB
7. EDM
8. BEAM
9. DATA
10. MATL
11. GLOB
12. DATA
13. BEAM
14. REST
15. WHT
16. DUNE

OUTPUT FOR RESTART 10
MATERIALS OUTPUT FOR RESTART 22
GLOBAL COORDINATES OUTPUT 274
SYST OUTPUT 6
STRI, MEMB, BEAM OUTPUT 494 144 202
DATA OUTPUT 13

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MATERIAL TABLE

NO.	NAME	DX,E	DY,E	D1	DXY	WEIGHT	CTE X	CTE Y
1	MESH	2.5	0.80	1.2	0.80	0.0	1.0	1.0
2	FRONT	1.49E+03	0.0	0.0	0.0	0.0	1.0	0.0
3	BACK	1.49E+03	0.0	0.0	0.0	0.0	1.0	0.0
4	OBINT	2.94E+03	0.0	0.0	0.0	0.0	1.0	0.0
5	TIE	30.	0.0	0.0	0.0	0.0	1.0	0.0
6	SCTIF	3.00E+02	0.0	0.0	0.0	0.0	1.0	0.0
7	STRIP	1.37E+07	0.0	0.0	0.0	0.0	1.0	0.0
8	STRIP	1.37E+07	6.50E+05	0.0	0.0	0.0	1.0	0.0
9	KIH	1.43E+07	0.0	0.0	0.0	0.0	1.0	0.0
10	KIB	1.43E+07	2.72E+06	0.0	0.0	0.0	1.0	0.0
11	RUU	2.96E+07	0.0	0.0	0.0	0.0	1.0	0.0
12	HOD	2.96E+07	6.50E+05	0.0	0.0	0.0	1.0	0.0
13	TCUND	6.60E+04	0.0	0.0	0.0	0.0	1.0	0.0
14	HUB	1.43E+07	0.0	0.0	0.0	0.0	1.0	0.0
15	HUB	1.43E+07	2.72E+06	0.0	0.0	0.0	1.0	0.0
16	STRUT	1.43E+07	0.0	0.0	0.0	0.0	1.0	0.0
17	STRUT	1.43E+07	2.72E+06	0.0	0.0	0.0	1.0	0.0
18	TIPSU	1.43E+07	0.0	0.0	0.0	0.0	1.0	0.0
19	TIPSU	1.43E+07	2.72E+06	0.0	0.0	0.0	1.0	0.0
20	IMTY	2.94E+03	0.0	0.0	0.0	0.0	1.0	0.0
21	TGRPH	1.80E+07	4.00E+06	0.0	0.0	8.10E-02	0.0	0.0
22	ANTG	1.80E+07	4.00E+06	0.0	0.0	0.0	0.0	0.0

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NUDAL COORDINATE TABLE

			X	Y	Z	NODAL SYS	X	Y	Z	NODAL SYS	X	Y	Z	NODAL SYS	X	Y	Z
1	3	288.979	0.000	29.436	2	3	227.353	0.000	16.235	3	229.452	0.000	16.190	3	229.452	0.000	16.190
3	3	154.721	0.000	8.445	4	3	297.096	79.607	33.374	3	154.655	41.440	9.044	3	154.655	41.440	9.044
5	3	157.170	0.000	-13.946	6	3	302.646	81.094	19.590	3	230.038	81.639	1.543	3	230.038	81.639	1.543
7	3	227.154	60.866	15.510	8	3	216.400	21.572	-23.369	3	198.711	114.726	5.190	3	198.711	114.726	5.190
9	3	74.915	21.413	2.415	10	3	217.484	217.484	33.374	3	113.215	113.215	9.044	3	113.215	113.215	9.044
11	3	293.253	74.577	17.255	12	3	221.552	221.552	19.590	3	168.400	166.400	1.543	3	168.400	166.400	1.543
13	3	147.475	42.187	-16.444	14	3	196.694	113.677	16.235	3	59.588	59.588	-23.369	3	59.588	59.588	-23.369
15	3	168.464	45.141	-66.576	16	0	0.000	0.000	0.000	0	0.000	0.000	0.000	0	0.000	0.000	0.000
17	0	0.000	0.000	0.000	18	0	0.000	0.000	0.000	0	0.000	0.000	0.000	0	0.000	0.000	0.000
19	0	0.000	0.000	0.000	20	0	0.000	0.000	0.000	0	0.000	0.000	0.000	0	0.000	0.000	0.000
21	3	250.263	146.489	29.436	22	3	196.694	113.677	16.235	3	113.677	196.694	16.235	3	113.677	196.694	16.235
23	3	133.492	77.360	8.445	24	3	198.711	114.726	5.190	3	217.484	217.484	33.374	3	217.484	217.484	33.374
25	3	136.114	76.585	-13.986	26	3	113.215	113.215	9.044	3	221.552	221.552	19.590	3	221.552	221.552	19.590
27	3	166.248	166.284	19.510	28	3	168.400	166.400	1.543	3	59.588	59.588	-23.369	3	59.588	59.588	-23.369
29	3	58.502	58.502	2.415	30	3	81.094	302.646	19.590	3	41.440	154.655	9.044	3	41.440	154.655	9.044
31	3	214.676	214.676	17.255	32	3	61.639	230.038	1.543	3	81.094	302.646	19.590	3	81.094	302.646	19.590
33	3	115.254	115.254	-16.494	34	3	21.803	81.372	-23.369	3	21.803	81.372	-23.369	3	21.803	81.372	-23.369
35	3	123.328	123.328	-86.576	36	0	0.000	0.000	0.000	0	0.000	0.000	0.000	0	0.000	0.000	0.000
37	0	0.000	0.000	0.000	38	0	0.000	0.000	0.000	0	0.000	0.000	0.000	0	0.000	0.000	0.000
39	0	0.000	0.000	0.000	40	0	0.000	0.000	0.000	0	0.000	0.000	0.000	0	0.000	0.000	0.000
41	3	144.464	250.263	29.436	42	3	113.677	196.694	16.235	3	113.677	196.694	16.235	3	113.677	196.694	16.235
43	3	77.360	133.492	8.445	44	3	114.726	198.711	5.190	3	79.607	247.046	33.374	3	79.607	247.046	33.374
45	3	78.545	136.114	-13.986	46	3	41.440	154.655	9.044	3	41.440	154.655	9.044	3	41.440	154.655	9.044
47	3	60.866	227.154	19.510	48	3	81.094	302.646	19.590	3	61.639	230.038	1.543	3	61.639	230.038	1.543
49	3	21.413	79.915	2.415	50	3	21.803	81.372	-23.369	3	21.803	81.372	-23.369	3	21.803	81.372	-23.369
51	3	78.577	295.253	17.255	52	3	21.803	81.372	-23.369	3	21.803	81.372	-23.369	3	21.803	81.372	-23.369
53	3	42.187	157.445	-16.499	54	3	21.803	81.372	-23.369	3	21.803	81.372	-23.369	3	21.803	81.372	-23.369
55	3	45.141	168.469	-86.576	56	0	0.000	0.000	0.000	0	0.000	0.000	0.000	0	0.000	0.000	0.000
57	0	0.000	0.000	0.000	58	0	0.000	0.000	0.000	0	0.000	0.000	0.000	0	0.000	0.000	0.000
59	0	0.000	0.000	0.000	60	0	0.000	0.000	0.000	0	0.000	0.000	0.000	0	0.000	0.000	0.000
61	3	0.000	284.979	29.436	62	3	0.000	227.353	16.235	3	0.000	227.353	16.235	3	0.000	227.353	16.235
63	3	0.000	154.721	8.445	64	3	0.000	229.452	5.190	3	0.000	229.452	5.190	3	0.000	229.452	5.190
65	3	0.000	157.170	-13.946	66	3	-79.607	297.096	33.374	3	0.000	0.000	0.000	3	0.000	0.000	0.000
67	3	-60.866	227.154	9.510	66	3	-41.440	154.655	9.044	3	-41.440	154.655	9.044	3	-41.440	154.655	9.044
69	3	-21.413	79.915	415	70	4	-61.639	302.646	1.543	3	-61.639	302.646	1.543	3	-61.639	302.646	1.543
71	3	-71.517	295.253	17.255	72	3	-61.639	302.646	1.543	3	-61.639	302.646	1.543	3	-61.639	302.646	1.543
73	3	-42.187	157.445	-16.499	74	3	-21.803	81.372	-23.369	3	-21.803	81.372	-23.369	3	-21.803	81.372	-23.369
75	3	-45.141	168.469	-86.576	76	0	0.000	0.000	0.000	0	0.000	0.000	0.000	0	0.000	0.000	0.000
77	0	0.000	0.000	0.000	78	0	0.000	0.000	0.000	0	0.000	0.000	0.000	0	0.000	0.000	0.000
79	0	0.000	0.000	0.000	80	0	0.000	0.000	0.000	0	0.000	0.000	0.000	0	0.000	0.000	0.000
81	3	-144.464	250.263	29.436	82	3	-113.677	196.694	16.235	3	-113.677	196.694	16.235	3	-113.677	196.694	16.235
83	3	-17.360	133.492	8.445	84	3	-114.726	198.711	5.190	3	-114.726	198.711	5.190	3	-114.726	198.711	5.190
85	3	-78.585	136.114	-13.986	86	3	-217.489	217.489	33.374	3	-217.489	217.489	33.374	3	-217.489	217.489	33.374
87	3	-166.288	166.286	19.510	86	3	-113.215	113.215	9.044	3	-113.215	113.215	9.044	3	-113.215	113.215	9.044
89	3	-56.502	58.502	2.415	90	3	-221.552	221.552	1.543	3	-221.552	221.552	1.543	3	-221.552	221.552	1.543
91	3	-214.676	214.676	17.255	92	3	-168.400	168.400	1.543	3	-168.400	168.400	1.543	3	-168.400	168.400	1.543
93	3	-115.250	115.250	-16.499	94	3	-59.568	59.568	-23.369	3	-59.568	59.568	-23.369	3	-59.568	59.568	-23.369
95	3	-123.320	123.320	-86.576	96	0	0.000	0.000	0.000	0	0.000	0.000	0.000	0	0.000	0.000	0.000
97	0	0.000	0.000	0.000	98	0	0.000	0.000	0.000	0	0.000	0.000	0.000	0	0.000	0.000	0.000
99	0	0.000	0.000	0.000	100	0	0.000	0.000	0.000	0	0.000	0.000	0.000	0	0.000	0.000	0.000

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NUDAL COORDINATE TABLE

NUDLE SYS	X	Y	Z	NUDLE SYS	X	Y	Z
101	-250.263	144.489	29.436	102	3	-196.894	113.677
103	-133.492	77.360	8.445	104	3	-198.711	114.726
105	-156.114	78.585	-13.966	106	3	-297.096	79.607
107	-227.154	60.866	19.510	108	3	-154.655	41.440
109	-79.915	21.913	2.415	110	3	-302.646	81.094
111	-293.253	76.577	17.215	112	3	-230.056	61.634
113	-157.415	46.167	81.494	114	3	-81.372	21.803
115	-164.469	41.141	89.176	116	0	0.000	0.000
117	0	0.000	0.000	118	0	0.000	0.000
119	0	0.000	0.000	120	0	0.000	0.000
121	3	-286.479	0.000	122	3	-227.353	0.000
123	3	-154.721	0.000	124	3	-229.452	0.000
125	3	-167.170	0.000	126	3	-247.066	-19.607
127	3	-227.154	60.866	128	3	-154.655	41.440
129	3	-79.915	21.913	130	3	-302.646	81.094
131	3	-293.253	76.577	132	3	-230.056	61.634
133	3	-157.415	46.167	134	3	-81.372	21.803
135	3	-168.469	-45.141	136	0	0.000	0.000
137	0	0.000	0.000	138	0	0.000	0.000
139	0	0.000	0.000	140	0	0.000	0.000
141	3	-250.263	-144.469	142	3	-196.894	-113.677
143	3	-133.492	-77.360	144	3	-198.711	114.726
145	3	-136.114	-78.585	146	3	-217.466	-217.469
147	3	-166.288	-166.288	148	3	-113.215	113.215
149	3	-58.502	-58.502	150	3	-221.552	-221.552
151	3	-214.676	-214.676	152	3	-168.400	-168.400
153	3	-115.258	-115.258	154	3	-59.568	-59.568
155	3	-123.328	-123.328	156	0	0.000	0.000
157	0	0.000	0.000	158	0	0.000	0.000
159	0	0.000	0.000	160	0	0.000	0.000
161	3	-144.489	-250.263	162	3	-113.677	-196.894
163	3	-77.360	-133.492	164	3	-114.726	-198.711
165	3	-78.585	-136.114	166	3	-79.607	-297.096
167	3	-60.866	-227.154	168	3	-41.440	-154.655
169	3	-21.415	-79.915	170	3	-61.094	-302.646
171	3	-78.577	-293.253	172	3	-61.634	-230.418
173	3	-42.167	-157.445	174	3	-21.803	-81.372
175	3	-45.141	-168.469	176	0	0.000	0.000
177	0	0.000	0.000	178	0	0.000	0.000
179	0	0.000	0.000	180	0	0.000	0.000
181	3	0.000	-268.979	182	3	0.000	-227.353
183	3	0.000	-154.721	184	3	0.000	-229.452
185	3	0.000	-157.170	186	3	79.607	-297.096
187	3	60.866	-227.54	188	3	41.440	-154.655
189	3	21.413	-79.915	190	3	61.094	-302.646
191	3	78.577	-293.253	192	3	61.634	-230.418
193	3	42.167	-157.445	194	3	21.803	-81.372
195	3	45.141	-168.469	196	0	0.000	0.000
197	0	0.000	0.000	198	0	0.000	0.000
199	0	0.000	0.000	200	0	0.000	0.000

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NUDAL COORDINATE TABLE

NODE	SYS	X	Y	Z	NUDAL	SYS	X	Y	Z
201	3	144.449	-250.263	29.436	202	3	113.677	-196.844	16.255
203	3	77.560	-133.992	6.445	204	3	114.726	-198.711	5.190
205	3	76.585	-136.114	-13.966	206	3	217.489	-217.489	35.574
207	3	166.288	-166.288	19.310	208	3	113.215	9.044	
209	3	58.502	-58.502	2.415	210	3	221.552	19.590	
211	3	214.676	-214.676	17.265	212	3	168.400	1.543	
213	3	115.254	-115.254	-16.494	214	3	59.568	-59.568	-23.569
215	3	123.524	-123.524	-236.524	216	0	0.000	0.000	0.000
217	0	0.000	0.000	0.000	218	0	0.000	0.000	0.000
219	0	0.000	0.000	0.000	220	0	0.000	0.000	0.000
221	3	250.263	-140.469	29.436	222	3	196.894	-113.677	16.255
223	3	133.992	-77.360	6.445	224	3	198.711	-114.726	5.190
225	3	156.114	-78.585	-1.966	226	3	297.046	-79.607	35.574
227	3	227.154	-60.866	19.510	228	3	154.055	-41.440	9.044
229	3	79.415	-21.413	6.415	230	3	302.646	-81.094	19.590
231	3	293.253	-78.577	17.255	232	3	230.058	-61.639	1.543
233	3	157.445	-42.187	-16.499	234	3	81.372	-21.603	-23.369
235	3	168.469	-45.141	-86.576	236	0	0.000	0.000	0.000
237	0	0.000	0.000	0.000	238	0	0.000	0.000	0.000
239	0	0.000	0.000	0.000	240	0	0.000	0.000	0.000
241	3	0.000	0.000	0.000	242	3	0.000	0.000	-30.759
243	3	11.000	0.000	-109.663	244	0	0.000	0.000	0.000
245	0	0.000	0.000	0.000	246	0	422.340	0.000	61.718
247	0	223.420	0.000	742.032	248	0	72.704	0.000	0.000
249	0	394.428	0.000	946.946	250	0	100.000	0.000	100.000
251	3	320.000	-81.094	-60.000	252	3	320.000	61.094	-60.000
253	3	370.637	0.000	19.540	254	0	0.000	0.000	0.000
255	0	0.000	0.000	0.000	256	0	0.000	0.000	0.000
257	0	0.000	0.000	0.000	258	0	0.000	0.000	0.000
259	0	0.000	0.000	0.000	260	3	370.637	0.000	169.590
261	3	302.646	39.370	169.540	262	3	302.646	-39.370	169.590
263	3	370.637	0.000	299.590	264	3	302.646	-39.370	299.590
265	3	302.646	-39.370	299.590	266	3	370.637	0.000	429.590
267	3	302.646	39.370	429.590	268	3	302.646	-39.370	429.590
269	3	370.637	0.000	559.590	270	3	302.646	-39.370	559.590
271	3	302.646	-39.370	559.590	272	3	370.637	0.000	689.590
273	3	302.646	39.370	669.590	274	3	302.646	-39.370	689.590

ORIGINAL PAGE IS
OF POOR QUALITY

NO.	TYPE	NA	NB	NC
1		0		
2		0		
3		3		
4		0		
5		5		
6		0		
7		246	247	250
8		248	249	250

ORIGINAL PAGE IS
OF POOR QUALITY

NO.	JH	PAI.	NAME	LENGTH	AREA	FORCE	TEMP.
1	1	6	UHINT	80.1162	1.00	5.69	0.00
2	21	26	UHINT	80.1162	1.00	5.69	0.00
3	41	46	UHINT	80.1162	1.00	5.69	0.00
4	61	66	UHINT	80.1162	1.00	5.69	0.00
5	81	86	UHINT	80.1162	1.00	5.69	0.00
6	101	106	UHINT	80.1162	1.00	5.69	0.00
7	121	126	UHINT	80.1162	1.00	5.69	0.00
8	141	146	UHINT	80.1162	1.00	5.69	0.00
9	161	166	UHINT	80.1162	1.00	5.69	0.00
10	181	186	UHINT	80.1162	1.00	5.69	0.00
11	201	206	UHINT	80.1162	1.00	5.69	0.00
12	221	226	UHINT	80.1162	1.00	5.69	0.00
13	6	21	UHINT	80.1162	1.00	5.69	0.00
14	26	41	UHINT	80.1162	1.00	5.69	0.00
15	46	61	UHINT	80.1162	1.00	5.69	0.00
16	66	81	UHINT	80.1162	1.00	5.69	0.00
17	86	101	UHINT	80.1162	1.00	5.69	0.00
18	106	121	UHINT	80.1162	1.00	5.69	0.00
19	126	141	UHINT	80.1162	1.00	5.69	0.00
20	146	161	UHINT	80.1162	1.00	5.69	0.00
21	166	181	UHINT	80.1162	1.00	5.69	0.00
22	186	201	UHINT	80.1162	1.00	5.69	0.00
23	206	221	UHINT	80.1162	1.00	5.69	0.00
24	226	1	UHINT	80.1162	1.00	5.69	0.00
25	6	26	FRONT	159.2132	5.00	7.19	0.00
26	26	46	FRONT	159.2132	5.00	7.19	0.00
27	46	66	FRONT	159.2132	5.00	7.19	0.00
28	66	86	FRONT	159.2132	5.00	7.19	0.00
29	86	106	FRONT	159.2132	5.00	7.19	0.00
30	106	126	FRONT	159.2132	5.00	7.19	0.00
31	126	146	FRONT	159.2132	5.00	7.19	0.00
32	146	166	FRONT	159.2132	5.00	7.19	0.00
33	166	186	FRONT	159.2132	5.00	7.19	0.00
34	186	206	FRONT	159.2132	5.00	7.19	0.00
35	206	226	FRONT	159.2132	5.00	7.19	0.00
36	226	6	FRONT	159.2132	5.00	7.19	0.00
37	2	7	FRONT	60.6795	10.0	14.2	0.00
38	22	27	FRONT	60.6795	10.0	14.2	0.00
39	42	47	FRONT	60.6795	10.0	14.2	0.00
40	62	67	FRONT	60.6795	10.0	14.2	0.00
41	82	87	FRONT	60.6795	10.0	14.2	0.00
42	102	107	FRONT	60.6795	10.0	14.2	0.00
43	122	127	FRONT	60.6795	10.0	14.2	0.00
44	142	147	FRONT	60.6795	10.0	14.2	0.00
45	162	167	FRONT	60.6795	10.0	14.2	0.00
46	182	187	FRONT	60.6795	10.0	14.2	0.00
47	202	207	FRONT	60.6795	10.0	14.2	0.00
48	222	227	FRONT	60.6795	10.0	14.2	0.00
49	7	22	FRONT	60.6795	10.0	14.2	0.00
50	27	42	FRONT	60.6795	10.0	14.2	0.00

ORIGINAL PAGE IS
OF POOR QUALITY

NO.	JH	MATERIAL	NAME	LENGTH	STRINGER ELEMENTS		FORCE	ITEMP.
					AREA	ITEMP.		
51	47	62	2 FRUNIT	60.8795	10.0	14.2	0.00	0.00
52	67	H2	2 FRUNIT	60.8795	10.0	14.2	0.00	0.00
53	87	102	2 FRUNIT	60.8795	10.0	14.2	0.00	0.00
54	107	122	2 FRUNIT	60.8795	10.0	14.2	0.00	0.00
55	127	142	2 FRUNIT	60.8795	10.0	14.2	0.00	0.00
56	147	162	2 FRUNIT	60.8795	10.0	14.2	0.00	0.00
57	167	182	2 FRUNIT	60.8795	10.0	14.2	0.00	0.00
58	187	202	2 FRUNIT	60.8795	10.0	14.2	0.00	0.00
59	207	222	2 FRUNIT	60.8795	10.0	14.2	0.00	0.00
60	227	2	FRUNIT	60.8795	10.0	14.2	0.00	0.00
61	3	H8	2 FRUNIT	41.4440	10.0	15.6	0.00	0.00
62	23	24	2 FRUNIT	41.4440	10.0	15.6	0.00	0.00
63	43	46	2 FRUNIT	41.4440	10.0	15.6	0.00	0.00
64	63	CH	2 FRUNIT	41.4440	10.0	15.6	0.00	0.00
65	83	H8	2 FRUNIT	41.4440	10.0	15.6	0.00	0.00
66	103	108	2 FRUNIT	41.4440	10.0	15.6	0.00	0.00
67	123	128	2 FRUNIT	41.4440	10.0	15.6	0.00	0.00
68	143	148	2 FRUNIT	41.4440	10.0	15.6	0.00	0.00
69	163	168	2 FRUNIT	41.4440	10.0	15.6	0.00	0.00
70	183	188	2 FRUNIT	41.4440	10.0	15.6	0.00	0.00
71	203	208	2 FRUNIT	41.4440	10.0	15.6	0.00	0.00
72	223	224	2 FRONT	41.4440	10.0	15.6	0.00	0.00
73	8	23	2 FRUNIT	41.4440	10.0	15.6	0.00	0.00
74	26	43	2 FRUNIT	41.4440	10.0	15.6	0.00	0.00
75	48	63	2 FRUNIT	41.4440	10.0	15.6	0.00	0.00
76	68	H3	2 FRUNIT	41.4440	10.0	15.6	0.00	0.00
77	88	103	2 FRONT	41.4440	10.0	15.6	0.00	0.00
78	108	123	2 FRUNIT	41.4440	10.0	15.6	0.00	0.00
79	128	143	2 FRUNIT	41.4440	10.0	15.6	0.00	0.00
80	148	163	2 FRUNIT	41.4440	10.0	15.6	0.00	0.00
81	168	183	2 FRUNIT	41.4440	10.0	15.6	0.00	0.00
82	188	203	2 FRUNIT	41.4440	10.0	15.6	0.00	0.00
83	208	223	2 FRONT	41.4440	10.0	15.6	0.00	0.00
84	228	3	2 FRUNIT	41.4440	10.0	15.6	0.00	0.00
85	4	24	2 FRUNIT	42.8265	15.0	16.9	0.00	0.00
86	29	49	2 FRUNIT	42.8265	15.0	16.9	0.00	0.00
87	44	64	2 FRUNIT	42.8265	15.0	16.9	0.00	0.00
88	69	H4	2 FRUNIT	42.8265	15.0	16.9	0.00	0.00
89	89	104	2 FRUNIT	42.8265	15.0	16.9	0.00	0.00
90	109	129	2 FRUNIT	42.8265	15.0	16.9	0.00	0.00
91	129	149	2 FRUNIT	42.8265	15.0	16.9	0.00	0.00
92	149	164	2 FRUNIT	42.8265	15.0	16.9	0.00	0.00
93	169	189	2 FRUNIT	42.8265	15.0	16.9	0.00	0.00
94	189	204	2 FRUNIT	42.8265	15.0	16.9	0.00	0.00
95	209	224	2 FRUNIT	42.8265	15.0	16.9	0.00	0.00
96	229	9	2 FRUNIT	42.8265	15.0	16.9	0.00	0.00
97	11	31	3 HACK	157.1539	5.00	3.50	0.00	0.00
98	31	51	3 BACK	157.1539	5.00	3.50	0.00	0.00
99	51	71	3 BACK	157.1539	5.00	3.50	0.00	0.00
100	71	91	3 BACK	157.1539	5.00	3.50	0.00	0.00

ORIGINAL PAGE IS
OF POOR QUALITY

NO.	JH	MATERIAL	NAME	LENGTH	AREA	FORCE	TEMP.
101	91	JH	HACK	157	1539	5.00	3.50
102	111	JH	HACK	157	1539	5.00	3.50
103	131	JH	HACK	157	1539	5.00	3.50
104	151	JH	HACK	157	1539	5.00	3.50
105	171	JH	HACK	157	1539	5.00	3.50
106	191	JH	HACK	157	1539	5.00	3.50
107	211	JH	HACK	157	1539	5.00	3.50
108	231	JH	HACK	157	1539	5.00	3.50
109	4	JH	HACK	61	7491	10.0	5.72
110	24	JH	HACK	61	7491	10.0	5.72
111	44	JH	HACK	61	7491	10.0	5.72
112	64	JH	HACK	61	7491	10.0	5.72
113	84	JH	HACK	61	7491	10.0	5.72
114	104	JH	HACK	61	7491	10.0	5.72
115	124	JH	HACK	61	7491	10.0	5.72
116	144	JH	HACK	61	7491	10.0	5.72
117	164	JH	HACK	61	7491	10.0	5.72
118	184	JH	HACK	61	7491	10.0	5.72
119	204	JH	HACK	61	7491	10.0	5.72
120	224	JH	HACK	61	7491	10.0	5.72
121	12	JH	HACK	61	7491	10.0	5.72
122	32	JH	HACK	61	7491	10.0	5.72
123	52	JH	HACK	61	7491	10.0	5.72
124	72	JH	HACK	61	7491	10.0	5.72
125	92	JH	HACK	61	7491	10.0	5.72
126	112	JH	HACK	61	7491	10.0	5.72
127	132	JH	HACK	61	7491	10.0	5.72
128	152	JH	HACK	61	7491	10.0	5.72
129	172	JH	HACK	61	7491	10.0	5.72
130	192	JH	HACK	61	7491	10.0	5.72
131	212	JH	HACK	61	7491	10.0	5.72
132	232	JH	HACK	61	7491	10.0	5.72
133	5	JH	HACK	42	2629	10.0	3.89
134	25	JH	HACK	42	2629	10.0	3.89
135	45	JH	HACK	42	2629	10.0	3.89
136	65	JH	HACK	42	2629	10.0	3.89
137	85	JH	HACK	42	2629	10.0	3.89
138	105	JH	HACK	42	2629	10.0	3.89
139	125	JH	HACK	42	2629	10.0	3.89
140	145	JH	HACK	42	2629	10.0	3.89
141	165	JH	HACK	42	2629	10.0	3.89
142	185	JH	HACK	42	2629	10.0	3.89
143	205	JH	HACK	42	2629	10.0	3.89
144	225	JH	HACK	42	2629	10.0	3.89
145	13	JH	HACK	42	2629	10.0	3.89
146	33	JH	HACK	42	2629	10.0	3.89
147	53	JH	HACK	42	2629	10.0	3.89
148	73	JH	HACK	42	2629	10.0	3.89
149	93	JH	HACK	42	2629	10.0	3.89
150	113	JH	HACK	42	2629	10.0	3.89

ORIGINAL PLATE IS
OF POOR QUALITY

No.	JA	JH	MAT.	NAME	LENGTH	AREA	TEMP.	TURGE	STRENGTH ELEMENTS
151	133	145	152	165	3	BACK	42.2629	10.0	3.69
			153	173	3	BACK	42.2629	10.0	3.69
			154	193	3	HACK	42.2629	10.0	3.69
			155	213	223	3	HACK	42.2629	10.0
			156	233	3	HACK	42.2629	10.0	3.69
			157	14	3	HACK	43.6069	15.0	4.50
			158	34	3	HACK	43.6069	15.0	4.50
			159	54	3	HACK	43.6069	15.0	4.50
			160	74	3	HACK	43.6069	15.0	4.50
			161	94	3	HACK	43.6069	15.0	4.50
			162	114	3	BALK	43.6069	15.0	4.50
			163	134	3	BALK	43.6069	15.0	4.50
			164	154	3	BALK	43.6069	15.0	4.50
			165	174	3	HACK	43.6069	15.0	4.50
			166	194	3	HACK	43.6069	15.0	4.50
			167	214	3	HACK	43.6069	15.0	4.50
			168	234	3	HACK	43.6069	15.0	4.50
			169	1	10	INITY	42.6240	1.00	1.24
			170	30	20	INITY	62.8246	1.00	1.24
			171	50	20	INITY	82.8246	1.00	1.24
			172	70	20	INITY	82.8246	1.00	1.24
			173	81	90	INITY	62.8240	1.00	1.24
			174	101	110	INITY	82.8246	1.00	1.24
			175	121	130	INITY	82.8246	1.00	1.24
			176	141	150	INITY	82.8246	1.00	1.24
			177	161	170	INITY	82.8246	1.00	1.24
			178	181	190	INITY	82.8246	1.00	1.24
			179	201	210	INITY	82.8246	1.00	1.24
			180	221	230	INITY	82.8246	1.00	1.24
			181	10	21	INITY	82.8246	1.00	1.24
			182	30	41	INITY	82.8246	1.00	1.24
			183	50	61	INITY	82.8246	1.00	1.24
			184	70	81	INITY	82.8246	1.00	1.24
			185	90	101	INITY	82.8246	1.00	1.24
			186	110	121	INITY	82.8246	1.00	1.24
			187	130	141	INITY	82.8246	1.00	1.24
			188	150	161	INITY	82.8246	1.00	1.24
			189	170	181	INITY	82.8246	1.00	1.24
			190	190	201	INITY	82.8246	1.00	0.685
			191	210	221	INITY	82.8246	1.00	0.685
			192	230	1	INITY	82.8246	1.00	0.685
			193	2	4	INIT	13.2126	1.00	0.685
			194	22	24	INIT	13.2126	1.00	0.685
			195	42	44	INIT	13.2126	1.00	0.685
			196	62	64	INIT	13.2126	1.00	0.685
			197	82	84	INIT	13.2126	1.00	0.685
			198	102	104	INIT	13.2126	1.00	0.685
			199	122	124	INIT	13.2126	1.00	0.685
			200	142	144	INIT	13.2126	1.00	0.685

ORIGINAL PAGE IS
OF POOR QUALITY

NU.	JH	MAT.	NAME	STRENGTH ELEMENTS	AREA	FORCE	TEMP.
201	162	164	5	11E	13.2126	.10.0	0.685
202	182	184	5	11E	13.2126	.10.0	0.685
203	202	204	5	11E	13.2126	.10.0	0.685
204	222	224	5	11E	13.2126	.10.0	0.685
205	5	5	5	11E	22.5641	.10.0	0.465
206	25	25	5	11E	22.5641	.10.0	0.465
207	43	45	5	11E	22.5641	.10.0	0.465
208	63	65	5	11E	22.5641	.10.0	0.465
209	83	85	5	11E	22.5641	.10.0	0.465
210	103	105	5	11E	22.5641	.10.0	0.465
211	123	125	5	11E	22.5641	.10.0	0.465
212	143	145	5	11E	22.5641	.10.0	0.465
213	163	165	5	11E	22.5641	.10.0	0.465
214	183	185	5	11E	22.5641	.10.0	0.465
215	203	205	5	11E	22.5641	.10.0	0.465
216	223	225	5	11E	22.5641	.10.0	0.465
217	6	10	6	S01E	14.9337	.5.00	51.1
218	26	30	6	S01E	14.9337	.5.00	51.1
219	46	50	6	S01E	14.9338	.5.00	51.1
220	66	70	6	S01E	14.9338	.5.00	51.1
221	86	90	6	S01E	14.9337	.5.00	51.1
222	106	110	6	S01E	14.9338	.5.00	51.1
223	126	130	6	S01E	14.9338	.5.00	51.1
224	146	150	6	S01E	14.9337	.5.00	51.1
225	166	170	6	S01E	14.9338	.5.00	51.1
226	186	190	6	S01E	14.9338	.5.00	51.1
227	206	210	6	S01E	14.9337	.5.00	51.1
228	226	230	6	S01E	14.9337	.5.00	51.1
229	7	12	6	S01E	16.2131	.10.0	1.73
230	27	32	6	S01E	16.2131	.10.0	1.73
231	47	52	6	S01E	16.2131	.10.0	1.73
232	67	72	6	S01E	16.2131	.10.0	1.73
233	87	92	6	S01E	16.2131	.10.0	1.73
234	107	112	6	S01E	16.2131	.10.0	1.73
235	127	132	6	S01E	16.2131	.10.0	1.73
236	147	152	6	S01E	16.2131	.10.0	1.73
237	167	172	6	S01E	16.2131	.10.0	1.73
238	187	192	6	S01E	16.2131	.10.0	1.73
239	207	212	6	S01E	16.2131	.10.0	1.73
240	227	232	6	S01E	16.2131	.10.0	1.73
241	4	13	6	S01E	25.7057	.10.0	1.19
242	28	33	6	S01E	25.7057	.10.0	1.19
243	48	53	6	S01E	25.7057	.10.0	1.19
244	68	73	6	S01E	25.7057	.10.0	1.19
245	88	93	6	S01E	25.7057	.10.0	1.19
246	108	113	6	S01E	25.7057	.10.0	1.19
247	128	133	6	S01E	25.7057	.10.0	1.19
248	148	153	6	S01E	25.7057	.10.0	1.19
249	168	173	6	S01E	25.7057	.10.0	1.19
250	188	193	6	S01E	25.7057	.10.0	1.19

ORIGINAL PAGE IS
OF POOR QUALITY

					STRINGER ELEMENTS	LENGTH	AREA	FURLE	TEMP.
NO.	JA	JH	MAT.	NAME					
251	204	213	6	S011T	25.7057	10.0	1.19	0.00	0.00
252	226	233	6	S011T	25.7057	10.0	1.19	0.00	0.00
253	9	14	6	S011T	25.6479	15.0	0.948	0.00	0.00
254	29	34	6	S011T	25.6479	15.0	0.948	0.00	0.00
255	49	54	6	S011T	25.8479	15.0	0.948	0.00	0.00
256	69	74	6	S011T	25.6479	15.0	0.948	0.00	0.00
257	89	94	6	S011T	25.6479	15.0	0.948	0.00	0.00
258	109	114	6	S011T	25.6479	15.0	0.948	0.00	0.00
259	129	134	6	S011T	25.6479	15.0	0.948	0.00	0.00
260	149	154	6	S011T	25.6479	15.0	0.948	0.00	0.00
261	169	174	6	S011T	25.6479	15.0	0.948	0.00	0.00
262	189	194	6	S011T	25.6479	15.0	0.948	0.00	0.00
263	209	214	6	S011T	25.6479	15.0	0.948	0.00	0.00
264	229	234	6	S011T	25.6479	15.0	0.948	0.00	0.00
265	241	242	6	S011T	30.7590	12.0	0.505	0.00	0.00
266	0	11	18	TIPSO	16.6029	2.770L-03	-54.1	0.00	0.00
267	26	31	18	TIPSO	16.6029	2.770L-03	-54.1	0.00	0.00
268	46	51	18	TIPSO	16.6029	2.770L-03	-54.1	0.00	0.00
269	66	71	18	TIPSO	16.6029	2.770L-03	-54.1	0.00	0.00
270	86	91	18	TIPSO	16.6029	2.770E-03	-54.1	0.00	0.00
271	106	111	18	TIPSO	16.6029	2.770E-03	-54.1	0.00	0.00
272	126	131	18	TIPSO	16.6029	2.770E-03	-54.1	0.00	0.00
273	146	151	18	TIPSO	16.6029	2.770E-03	-54.1	0.00	0.00
274	166	171	18	TIPSO	16.6029	2.770E-03	-54.1	0.00	0.00
275	186	191	18	TIPSO	16.6029	2.770E-03	-54.1	0.00	0.00
276	206	211	18	TIPSO	16.6029	2.770E-03	-54.1	0.00	0.00
277	226	231	18	TIPSO	16.6029	2.770E-03	-54.1	0.00	0.00
278	6	7	7	SIRIP	73.7243	1.470L-02	24.0	0.00	0.00
279	26	27	7	SIRIP	73.7243	1.470L-02	24.0	0.00	0.00
280	46	47	7	SIRIP	73.7243	1.470L-02	24.0	0.00	0.00
281	66	67	7	SIRIP	73.7243	1.470L-02	24.0	0.00	0.00
282	86	87	7	SIRIP	73.7243	1.470L-02	24.0	0.00	0.00
283	106	107	7	SIRIP	73.7243	1.470L-02	24.0	0.00	0.00
284	126	127	7	SIRIP	73.7243	1.470L-02	24.0	0.00	0.00
285	146	147	7	SIRIP	73.7243	1.470L-02	24.0	0.00	0.00
286	166	167	7	SIRIP	73.7243	1.470L-02	24.0	0.00	0.00
287	186	187	7	SIRIP	73.7243	1.470L-02	24.0	0.00	0.00
288	206	207	7	SIRIP	73.7243	1.470L-02	24.0	0.00	0.00
289	226	227	7	SIRIP	73.7243	1.470L-02	24.0	0.00	0.00
290	7	8	7	SIRIP	75.7832	1.470L-02	17.1	0.00	0.00
291	27	28	7	SIRIP	75.7H32	1.470L-02	17.1	0.00	0.00
292	47	48	7	SIRIP	75.7H32	1.470L-02	17.1	0.00	0.00
293	67	68	7	SIRIP	75.7H32	1.470L-02	17.1	0.00	0.00
294	87	88	7	SIRIP	75.7H32	1.470L-02	17.1	0.00	0.00
295	107	108	7	SIRIP	75.7H32	1.470L-02	17.1	0.00	0.00
296	127	128	7	SIRIP	75.7H32	1.470L-02	17.1	0.00	0.00
297	147	148	7	SIRIP	75.7832	1.470L-02	17.1	0.00	0.00
298	167	168	7	SIRIP	75.7832	1.470L-02	17.1	0.00	0.00
299	187	188	7	SIRIP	75.7832	1.470L-02	17.1	0.00	0.00
300	207	208	7	SIRIP	75.7832	1.470L-02	17.1	0.00	0.00

ORIGINAL FILM
OF POOR QUALITY

NO.	JA	JH	MAT.	WART.	STRENGTH ELEMENTS	LENGTH	AREA	FURLE	TEMP.
501	227	228	7	SIRIP	75.7432	1.970E-02	17.1	0.00	
502	8	9	7	SIRIP	77.6594	1.970E-02	10.4	0.00	
503	28	29	7	SIRIP	77.6594	1.970E-02	10.4	0.00	
504	48	49	7	SIRIP	77.6594	1.970E-02	10.4	0.00	
505	68	69	7	SIRIP	77.6594	1.970E-02	10.4	0.00	
506	88	89	7	SIRIP	77.6594	1.970E-02	10.4	0.00	
507	104	105	7	SIRIP	77.6594	1.970E-02	10.4	0.00	
508	124	125	7	SIRIP	77.6594	1.970E-02	10.4	0.00	
509	144	145	7	SIRIP	77.6594	1.970E-02	10.4	0.00	
510	164	165	7	SIRIP	77.6594	1.970E-02	10.4	0.00	
511	184	185	7	SIRIP	77.6594	1.970E-02	10.4	0.00	
512	208	209	7	SIRIP	77.6594	1.970E-02	10.4	0.00	
513	224	225	7	SIRIP	77.6594	1.970E-02	10.4	0.00	
514	244	245	7	SIRIP	82.7696	1.000E-08	1.00	0.00	
515	24	241	7	SIRIP	82.7696	1.000E-08	1.00	0.00	
516	49	241	7	SIRIP	82.7696	1.000E-08	1.00	0.00	
517	69	241	7	SIRIP	82.7696	1.000E-08	1.00	0.00	
518	89	241	7	SIRIP	82.7696	1.000E-08	1.00	0.00	
519	104	241	7	SIRIP	82.7696	1.000E-08	1.00	0.00	
520	120	241	7	SIRIP	82.7696	1.000E-08	1.00	0.00	
521	149	241	7	SIRIP	82.7696	1.000E-08	1.00	0.00	
522	169	241	7	SIRIP	82.7696	1.000E-08	1.00	0.00	
523	189	241	2	SIRIP	82.7696	1.000E-08	1.00	0.00	
524	209	241	7	SIRIP	82.7696	1.000E-08	1.00	0.00	
A-525	229	241	7	SIRIP	82.7696	1.000E-08	1.00	0.00	
526	10	11	9	RIB	10.0004	0.295	-64.9	0.00	
527	30	31	9	RIB	10.0004	0.295	-64.9	0.00	
528	50	51	9	RIB	10.0004	0.295	-64.9	0.00	
529	70	71	9	RIB	10.0004	0.295	-64.9	0.00	
530	90	91	9	RIB	10.0004	0.295	-64.9	0.00	
531	110	111	9	RIB	10.0004	0.295	-64.9	0.00	
532	130	131	9	RIB	10.0004	0.295	-64.9	0.00	
533	150	151	9	RIB	10.0004	0.295	-64.9	0.00	
534	170	171	9	RIB	10.0004	0.295	-64.9	0.00	
535	190	191	9	RIB	10.0004	0.295	-64.9	0.00	
536	210	211	9	RIB	10.0004	0.295	-64.9	0.00	
537	230	231	9	RIB	10.0004	0.295	-64.9	0.00	
538	11	12	9	RIB	67.3046	0.295	-91.6	0.00	
539	31	32	9	RIB	67.3046	0.295	-91.6	0.00	
540	51	52	9	RIB	67.3046	0.295	-91.6	0.00	
541	71	72	9	RIB	67.3046	0.295	-91.6	0.00	
542	91	92	9	RIB	67.3046	0.295	-91.6	0.00	
543	111	112	9	RIB	67.3046	0.295	-91.6	0.00	
544	131	132	9	RIB	67.3046	0.295	-91.6	0.00	
545	151	152	9	RIB	67.3046	0.295	-91.6	0.00	
546	171	172	9	RIB	67.3046	0.295	-91.6	0.00	
547	191	192	9	RIB	67.3046	0.295	-91.6	0.00	
548	211	212	9	RIB	67.3046	0.295	-91.6	0.00	
549	231	232	9	RIB	67.3046	0.295	-91.6	0.00	
550	12	13	9	RIB	77.2893	0.295	-94.3	0.00	

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**ORIGINAL PAGE IS
OF POOR QUALITY**

No.	JH	MAT.	NARL	LENGTH	STRINGER ELEMENTS		FURLE	TEMP.
					AHTA	RIB		
351	32	33	9	RIB	77.2893	0.295	-94.3	0.00
352	52	53	9	RIB	77.2893	0.295	-94.3	0.00
353	72	73	9	RIB	77.2893	0.295	-94.3	0.00
354	92	93	9	RIB	77.2893	0.295	-94.3	0.00
355	112	113	9	RIB	77.2893	0.295	-94.3	0.00
356	132	133	9	RIB	77.2893	0.295	-94.3	0.00
357	152	153	9	RIB	77.2893	0.295	-94.3	0.00
358	172	173	9	RIB	77.2893	0.295	-94.3	0.00
359	192	193	9	RIB	77.2893	0.295	-94.3	0.00
360	212	213	9	RIB	77.2893	0.295	-94.3	0.00
361	232	233	9	RIB	77.2893	0.295	-94.3	0.00
362	13	14	9	RIB	79.0578	0.295	-101.	0.00
363	33	34	9	RIB	79.0578	0.295	-101.	0.00
364	53	54	9	RIB	79.0578	0.295	-101.	0.00
365	73	74	9	RIB	79.0578	0.295	-101.	0.00
366	93	94	9	RIB	79.0578	0.295	-101.	0.00
367	113	114	9	RIB	79.0578	0.295	-101.	0.00
368	133	134	9	RIB	79.0578	0.295	-101.	0.00
369	153	154	9	RIB	79.0578	0.295	-101.	0.00
370	173	174	9	RIB	79.0578	0.295	-101.	0.00
371	193	194	9	RIB	79.0578	0.295	-101.	0.00
372	213	214	9	RIB	79.0578	0.295	-101.	0.00
373	233	234	9	RIB	79.0578	0.295	-101.	0.00
374	14	242	9	RIB	84.5638	0.295	-103.	0.00
375	34	242	9	RIB	84.5638	0.295	-103.	0.00
376	54	242	9	RIB	84.5638	0.295	-103.	0.00
377	74	242	9	RIB	84.5638	0.295	-103.	0.00
378	94	242	9	RIB	84.5638	0.295	-103.	0.00
379	114	242	9	RIB	84.5638	0.295	-103.	0.00
380	134	242	9	RIB	84.5638	0.295	-103.	0.00
381	154	242	9	RIB	84.5638	0.295	-103.	0.00
382	174	242	9	RIB	84.5638	0.295	-103.	0.00
383	194	242	9	RIB	84.5638	0.295	-103.	0.00
384	214	242	9	RIB	84.5638	0.295	-103.	0.00
385	234	242	9	RIB	84.5638	0.295	-103.	0.00
386	13	15	16	SIRUT	71.0003	0.146	-34.1	0.00
387	33	35	16	SIRUT	71.0003	0.146	-34.1	0.00
388	53	55	16	SIRUT	71.0003	0.146	-34.1	0.00
389	73	75	16	SIRUT	71.0003	0.146	-34.1	0.00
390	93	95	16	SIRUT	71.0003	0.146	-34.1	0.00
391	113	115	16	SIRUT	71.0003	0.146	-34.1	0.00
392	133	135	16	SIRUT	71.0003	0.146	-34.1	0.00
393	153	155	16	SIRUT	71.0003	0.146	-34.1	0.00
394	173	175	16	SIRUT	71.0003	0.146	-34.1	0.00
395	193	195	16	SIRUT	71.0003	0.146	-34.1	0.00
396	213	215	16	SIRUT	71.0003	0.146	-34.1	0.00
397	233	235	16	SIRUT	71.0003	0.146	-34.1	0.00
398	10	15	11	RUD	174.6348	1.636E-02	28.9	0.00
399	30	35	11	RUD	174.6348	1.636E-02	28.9	0.00
400	50	55	11	RUD	174.6348	1.636E-02	28.9	0.00

ORIGINAL PAGE IS
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NU.	JA	JH	MAI.	NAM	LENGTH	AREA	FORCE	TEMP.
401	70	75	11	KUD	174.8348	1.636L-02	26.9	0.00
402	90	95	11	KUD	174.6348	1.636L-02	26.9	0.00
403	110	115	11	KUD	174.6348	1.636L-02	26.9	0.00
404	130	135	11	KUD	174.8348	1.636L-02	26.9	0.00
405	150	155	11	KUD	174.8348	1.636L-02	26.9	0.00
406	170	175	11	KUD	174.8348	1.636L-02	26.9	0.00
407	190	195	11	KUD	174.8348	1.636L-02	26.9	0.00
408	210	215	11	KUD	174.8348	1.636L-02	26.9	0.00
409	230	235	11	KUD	174.8348	1.636L-02	26.9	0.00
410	15	243	11	KUD	175.4347	1.636L-02	14.6	0.00
411	35	243	11	KUD	175.4347	1.636L-02	14.6	0.00
412	55	243	11	KUD	175.4347	1.636L-02	14.6	0.00
413	75	243	11	KUD	175.4347	1.636L-02	14.6	0.00
414	95	243	11	KUD	175.4347	1.636L-02	14.6	0.00
415	115	243	11	KUD	175.4347	1.636L-02	14.6	0.00
416	135	243	11	KUD	175.4347	1.636L-02	14.6	0.00
417	155	243	11	KUD	175.4347	1.636L-02	14.6	0.00
418	175	243	11	KUD	175.4347	1.636L-02	14.6	0.00
419	195	243	11	KUD	175.4347	1.636L-02	14.6	0.00
420	215	243	11	KUD	175.4347	1.636L-02	14.6	0.00
421	235	243	11	KUD	175.4347	1.636L-02	14.6	0.00
422	13	243	11	KUD	187.8144	1.636E-02	11.3	0.00
423	33	243	11	KUD	187.4444	1.636E-02	11.3	0.00
424	53	243	11	KUD	187.8444	1.636E-02	11.3	0.00
425	73	243	11	KUD	187.8444	1.636E-02	11.3	0.00
426	93	243	11	KUD	187.8444	1.636E-02	11.3	0.00
427	113	243	11	KUD	187.8444	1.636E-02	11.3	0.00
428	133	243	11	KUD	187.8444	1.636E-02	11.3	0.00
429	153	243	11	KUD	187.8444	1.636E-02	11.3	0.00
430	173	243	11	KUD	187.8444	1.636E-02	11.3	0.00
431	193	243	11	KUD	187.8444	1.636E-02	11.3	0.00
432	213	243	11	KUD	187.8444	1.636E-02	11.3	0.00
433	233	243	11	KUD	187.8444	1.636E-02	11.3	0.00
434	10	30	11	KUD	182.1374	1.00	22.5	0.00
435	30	50	11	KUD	182.1374	1.00	22.5	0.00
436	50	70	11	KUD	162.1474	1.00	22.5	0.00
437	70	90	11	KUD	162.1474	1.00	22.5	0.00
438	90	110	11	KUD	162.1474	1.00	22.5	0.00
439	110	130	11	KUD	162.1474	1.00	22.5	0.00
440	130	150	11	KUD	162.1474	1.00	22.5	0.00
441	150	170	11	KUD	162.1474	1.00	22.5	0.00
442	170	190	11	KUD	162.1674	1.00	22.5	0.00
443	190	210	11	KUD	162.1874	1.00	22.5	0.00
444	210	230	11	KUD	162.1874	1.00	22.5	0.00
445	230	19	11	KUD	162.1874	1.00	22.5	0.00
446	10	33	13	ICURU	193.8657	1.00	10.0	0.00
447	33	50	13	TCURD	193.8657	1.00	10.0	0.00
448	50	73	13	TCORD	193.8657	1.00	10.0	0.00
449	73	90	13	TCORD	193.8657	1.00	10.0	0.00
450	90	113	13	TCORD	193.8657	1.00	10.0	0.00

ORIGINAL PAGE IS
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NU.	JH	MAI.	NAME	STRENGTH ELEMENTS	LENGTH	AHT A	FORCE	ITEM P.
451	113	130	13	TCURU	193.6657	1.00	10.0	0.00
452	130	153	13	TCURL	193.6657	1.00	10.0	0.00
453	153	170	13	TCURD	193.6657	1.00	10.0	0.00
454	170	193	13	TCURD	193.6657	1.00	10.0	0.00
455	193	210	13	TCURD	193.6657	1.00	10.0	0.00
456	210	233	13	TCURD	193.6657	1.00	10.0	0.00
457	233	10	13	TCURD	193.6657	1.00	10.0	0.00
458	13	35	13	TCURU	112.5103	1.00	15.0	0.00
459	33	55	13	TCURD	112.5103	1.00	15.0	0.00
460	53	75	13	TCURU	112.5103	1.00	15.0	0.00
461	73	95	13	TCURD	112.5103	1.00	15.0	0.00
462	93	115	13	TCURD	112.5103	1.00	15.0	0.00
463	113	135	13	TCURD	112.5103	1.00	15.0	0.00
464	133	155	13	TCURU	112.5103	1.00	15.0	0.00
465	153	175	13	TCURU	112.5103	1.00	15.0	0.00
466	173	195	13	TCURL	112.5103	1.00	15.0	0.00
467	193	215	13	TCURD	112.5103	1.00	15.0	0.00
468	213	235	13	TCURD	112.5103	1.00	15.0	0.00
469	233	15	13	TCURD	112.5103	1.00	15.0	0.00
470	33	15	13	TCORD	112.5103	1.00	15.0	0.00
471	53	35	13	TCURD	112.5103	1.00	15.0	0.00
472	73	55	13	TCORD	112.5103	1.00	15.0	0.00
473	93	75	13	TCURL	112.5103	1.00	15.0	0.00
474	113	95	13	TCURD	112.5103	1.00	15.0	0.00
475	133	115	13	TCURD	112.5103	1.00	15.0	0.00
476	153	135	13	TCURD	112.5103	1.00	15.0	0.00
477	173	155	13	TCURD	112.5103	1.00	15.0	0.00
478	193	175	13	TCURD	112.5103	1.00	15.0	0.00
479	213	195	13	TCURL	112.5103	1.00	15.0	0.00
480	233	215	13	TCURD	112.5103	1.00	15.0	0.00
481	13	235	13	TCURD	112.5103	1.00	15.0	0.00
482	242	243	14	MUM	79.1040	5.56	-47.4	0.00
483	30	55	13	TCURU	193.6657	1.00	10.0	0.00
484	53	70	13	TCURD	193.6657	1.00	10.0	0.00
485	70	43	13	TCURU	193.6657	1.00	10.0	0.00
486	93	110	13	TCURD	193.6657	1.00	10.0	0.00
487	110	133	13	TCURL	193.6657	1.00	10.0	0.00
488	133	150	13	TCURD	193.6657	1.00	10.0	0.00
489	150	173	13	TCURD	193.6657	1.00	10.0	0.00
490	173	190	13	TCURD	193.6657	1.00	10.0	0.00
491	190	213	13	TCORD	193.6657	1.00	10.0	0.00
492	213	230	13	TCURD	193.6657	1.00	10.0	0.00
493	230	13	30	TCURD	193.6657	1.00	10.0	0.00
494	13	30	13	TCURD	193.6657	1.00	10.0	0.00

MEMBRANE ELEMENTS

NO.	JA	JB	JC	MAT.	NAME	AREA	ANGLE	ANGLE	ANGLE	NX	NY	NXY	TEMP.	PRES.	MATL.	STRESS
							A	B	C							ANGLE
1	1	6	7	1	MESH	2.70E+03	52.0	69.0	58.9	1.01E-02	1.98E-02	-1.16E-03	0.0	0.0	6.5	0.0
2	21	26	27	1	MESH	2.70E+03	52.0	69.0	58.9	1.01E-02	1.98E-02	-1.16E-03	0.0	0.0	6.5	0.0
3	41	46	47	1	MESH	2.70E+03	52.0	69.0	58.9	1.01E-02	1.98E-02	-1.16E-03	0.0	0.0	6.5	0.0
4	61	66	67	1	MESH	2.70E+03	52.0	69.0	58.9	1.01E-02	1.98E-02	-1.16E-03	0.0	0.0	6.5	0.0
5	81	86	87	1	MESH	2.70E+03	52.0	69.0	58.9	1.01E-02	1.98E-02	-1.16E-03	0.0	0.0	6.5	0.0
6	101	106	107	1	MESH	2.70E+03	52.0	69.0	58.9	1.01E-02	1.98E-02	-1.16E-03	0.0	0.0	6.5	0.0
7	121	126	127	1	MESH	2.70E+03	52.0	69.0	58.9	1.01E-02	1.98E-02	-1.16E-03	0.0	0.0	6.5	0.0
8	141	146	147	1	MESH	2.70E+03	52.0	69.0	58.9	1.01E-02	1.98E-02	-1.16E-03	0.0	0.0	6.5	0.0
9	161	166	167	1	MESH	2.70E+03	52.0	69.0	58.9	1.01E-02	1.98E-02	-1.16E-03	0.0	0.0	6.5	0.0
10	181	186	187	1	MESH	2.70E+03	52.0	69.0	58.9	1.01E-02	1.98E-02	-1.16E-03	0.0	0.0	6.5	0.0
11	201	206	207	1	MESH	2.70E+03	52.0	69.0	58.9	1.01E-02	1.98E-02	-1.16E-03	0.0	0.0	6.5	0.0
12	221	226	227	1	MESH	2.70E+03	52.0	69.0	58.9	1.01E-02	1.98E-02	-1.16E-03	0.0	0.0	6.5	0.0
13	7	c	1	1	MESH	1.91E+03	45.8	90.0	44.2	9.94E-03	1.99E-02	2.66E-06	0.0	0.0	0.0	0.0
14	27	22	21	1	MESH	1.91E+03	45.8	90.0	44.2	9.94E-03	1.99E-02	2.66E-06	0.0	0.0	0.0	0.0
15	47	42	41	1	MESH	1.91E+03	45.8	90.0	44.2	9.94E-03	1.99E-02	2.66E-06	0.0	0.0	0.0	0.0
16	67	62	61	1	MESH	1.91E+03	45.8	90.0	44.2	9.94E-03	1.99E-02	2.66E-06	0.0	0.0	0.0	0.0
17	87	82	81	1	MESH	1.91E+03	45.8	90.0	44.2	9.94E-03	1.99E-02	2.66E-06	0.0	0.0	0.0	0.0
18	107	102	101	1	MESH	1.91E+03	45.8	90.0	44.2	9.94E-03	1.99E-02	2.66E-06	0.0	0.0	0.0	0.0
19	127	122	121	1	MESH	1.91E+03	45.8	90.0	44.2	9.94E-03	1.99E-02	2.66E-06	0.0	0.0	0.0	0.0
20	147	142	141	1	MESH	1.91E+03	45.8	90.0	44.2	9.94E-03	1.99E-02	2.66E-06	0.0	0.0	0.0	0.0
21	167	162	161	1	MESH	1.91E+03	45.8	90.0	44.2	9.94E-03	1.99E-02	2.66E-06	0.0	0.0	0.0	0.0
22	187	182	181	1	MESH	1.91E+03	45.8	90.0	44.2	9.94E-03	1.99E-02	2.66E-06	0.0	0.0	0.0	0.0
23	207	202	201	1	MESH	1.91E+03	45.8	90.0	44.2	9.94E-03	1.99E-02	2.66E-06	0.0	0.0	0.0	0.0
24	227	222	221	1	MESH	1.91E+03	45.8	90.0	44.2	9.94E-03	1.99E-02	2.66E-06	0.0	0.0	0.0	0.0
25	2	227	1	1	MESH	1.91E+03	90.0	45.8	44.2	9.94E-03	1.99E-02	-2.66E-06	0.0	0.0	0.0	0.0
26	22	7	21	1	MESH	1.91E+03	90.0	45.8	44.2	9.94E-03	1.99E-02	-2.66E-06	0.0	0.0	0.0	0.0
27	42	27	41	1	MESH	1.91E+03	90.0	45.8	44.2	9.94E-03	1.99E-02	-2.66E-06	0.0	0.0	0.0	0.0
28	62	41	61	1	MESH	1.91E+03	90.0	45.8	44.2	9.94E-03	1.99E-02	-2.66E-06	0.0	0.0	0.0	0.0
29	82	67	61	1	MESH	1.91E+03	90.0	45.8	44.2	9.94E-03	1.99E-02	-2.66E-06	0.0	0.0	0.0	0.0
30	102	87	101	1	MESH	1.91E+03	90.0	45.8	44.2	9.94E-03	1.99E-02	-2.66E-06	0.0	0.0	0.0	0.0
31	122	107	121	1	MESH	1.91E+03	90.0	45.8	44.2	9.94E-03	1.99E-02	-2.66E-06	0.0	0.0	0.0	0.0
32	142	127	141	1	MESH	1.91E+03	90.0	45.8	44.2	9.94E-03	1.99E-02	-2.66E-06	0.0	0.0	0.0	0.0
33	162	147	161	1	MESH	1.91E+03	90.0	45.8	44.2	9.94E-03	1.99E-02	-2.66E-06	0.0	0.0	0.0	0.0
34	182	167	181	1	MESH	1.91E+03	90.0	45.8	44.2	9.94E-03	1.99E-02	-2.66E-06	0.0	0.0	0.0	0.0
35	202	187	201	1	MESH	1.91E+03	90.0	45.8	44.2	9.94E-03	1.99E-02	-2.66E-06	0.0	0.0	0.0	0.0
36	222	207	221	1	MESH	1.91E+03	90.0	45.8	44.2	9.94E-03	1.99E-02	-2.66E-06	0.0	0.0	0.0	0.0
37	226	1	227	1	MESH	2.70E+03	69.0	52.0	58.9	1.01E-02	1.98E-02	1.16E-03	0.0	0.0	-6.5	0.0
38	6	21	7	1	MESH	2.70E+03	69.0	52.0	58.9	1.01E-02	1.98E-02	1.16E-03	0.0	0.0	-6.5	0.0
39	26	41	27	1	MESH	2.70E+03	69.0	52.0	58.9	1.01E-02	1.98E-02	1.16E-03	0.0	0.0	-6.5	0.0
40	46	61	47	1	MESH	2.70E+03	69.0	52.0	58.9	1.01E-02	1.98E-02	1.16E-03	0.0	0.0	-6.5	0.0
41	66	81	67	1	MESH	2.70E+03	69.0	52.0	58.9	1.01E-02	1.98E-02	1.16E-03	0.0	0.0	-6.5	0.0
42	86	101	87	1	MESH	2.70E+03	69.0	52.0	58.9	1.01E-02	1.98E-02	1.16E-03	0.0	0.0	-6.5	0.0
43	106	121	107	1	MESH	2.70E+03	69.0	52.0	58.9	1.01E-02	1.98E-02	1.16E-03	0.0	0.0	-6.5	0.0
44	126	141	127	1	MESH	2.70E+03	69.0	52.0	58.9	1.01E-02	1.98E-02	1.16E-03	0.0	0.0	-6.5	0.0
45	146	161	147	1	MESH	2.70E+03	69.0	52.0	58.9	1.01E-02	1.98E-02	1.16E-03	0.0	0.0	-6.5	0.0
46	166	181	167	1	MESH	2.70E+03	69.0	52.0	58.9	1.01E-02	1.98E-02	1.16E-03	0.0	0.0	-6.5	0.0
47	186	201	187	1	MESH	2.70E+03	69.0	52.0	58.9	1.01E-02	1.98E-02	1.16E-03	0.0	0.0	-6.5	0.0
48	206	221	207	1	MESH	2.70E+03	69.0	52.0	58.9	1.01E-02	1.98E-02	1.16E-03	0.0	0.0	-6.5	0.0
49	2	7	8	1	MESH	2.23E+03	60.5	75.2	44.4	9.99E-03	2.00E-02	-1.32E-06	0.0	0.0	0.0	0.0
50	22	27	28	1	MESH	2.23E+03	60.5	75.2	44.4	9.99E-03	2.00E-02	-1.33E-06	0.0	0.0	0.0	0.0

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MEMBRANE ELEMENTS

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OF POOR QUALITY

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HEAP PROPERTY TABLE

PROP NO.	AREA	J	I	I2	SF2	SF3	H2	H3	NAME
1	1.970E-02	4.210E-06	2.104E-06	2.418E-04	0.44	0.44	0.000	0.000	STRIP
2	0.187	0.416	0.204	0.204	0.53	0.53	0.000	0.000	RIB
3	1.636E-02	4.266E-05	0.213	0.213	0.69	0.69	0.000	0.000	KUD
4	3.56	133.	66.3	66.3	0.53	0.53	0.000	0.000	HUB
5	0.146	8.318E-02	4.160E-02	4.160E-02	0.53	0.53	0.000	0.000	SIRUT
6	2.770E-03	3.504E-04	1.752E-04	1.752E-04	0.20	0.20	0.000	0.000	TIPSO
7	0.00	0.00	0.00	0.00	0.00	0.00	0.000	0.000	
8	0.00	0.00	0.00	0.00	0.00	0.00	0.000	0.000	
9	0.00	0.00	0.00	0.00	0.00	0.00	0.000	0.000	
10	0.251	0.00	0.00	0.00	0.00	0.00	0.000	0.000	
11	4.900E-02	0.00	0.00	0.00	0.00	0.00	0.000	0.000	LUNG
12	0.125	0.00	0.00	0.00	0.00	0.00	0.000	0.000	DIAG
13	0.500	2.00	1.00	1.00	0.00	0.00	0.000	0.000	PLAT
							0.000	0.000	ANT

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HLAN CONNECTIVITY TABLE

	BLK#	NO.	JA	JB	JC	MAI.	NAME	PROP.	PROP.	NAME	FIXITY	LENGTH	WEIGHT	FIX	TA	TH	TYA	TRB	TA	TZB
2	1	10				RIB	2	RIB	2	RIB	110101010	10.000	0.0	0.E+00						
2	2	30	31	20	10	KIB	2	RIB	2	RIB	110101010	10.000	0.0	0.E+00						
2	3	50	51	40	10	RIB	2	RIB	2	RIB	110101010	10.000	0.0	0.E+00						
2	4	70	71	60	10	RIB	2	RIB	2	RIB	110101010	10.000	0.0	0.E+00						
2	5	90	91	60	10	RIB	2	RIB	2	RIB	110101010	10.000	0.0	0.E+00						
2	6	110	111	100	10	RIB	2	RIB	2	RIB	110101010	10.000	0.0	0.E+00						
2	7	130	131	120	10	RIB	2	RIB	2	RIB	110101010	10.000	0.0	0.E+00						
2	8	150	151	140	10	KIB	2	RIB	2	RIB	110101010	10.000	0.0	0.E+00						
2	9	170	171	160	10	KIB	2	RIB	2	RIB	110101010	10.000	0.0	0.E+00						
2	10	190	191	180	10	KIB	2	RIB	2	RIB	110101010	10.000	0.0	0.E+00						
2	11	210	211	200	10	KIB	2	RIB	2	RIB	110101010	10.000	0.0	0.E+00						
2	12	230	231	220	10	RIB	2	RIB	2	RIB	110101010	10.000	0.0	0.E+00						
2	13	11	12	0	10	KIB	2	RIB	2	RIB	110101010	67.305	0.0	0.E+00						
2	14	31	32	20	10	KIB	2	RIB	2	RIB	110101010	67.305	0.0	0.E+00						
2	15	51	52	40	10	KIB	2	RIB	2	RIB	110101010	67.305	0.0	0.E+00						
2	16	71	72	60	10	KIB	2	RIB	2	RIB	110101010	67.305	0.0	0.E+00						
2	17	91	92	80	10	KIB	2	RIB	2	RIB	110101010	67.305	0.0	0.E+00						
2	18	112	113	100	10	KIB	2	RIB	2	RIB	110101010	67.305	0.0	0.E+00						
2	19	131	132	120	10	KIB	2	RIB	2	RIB	110101010	67.305	0.0	0.E+00						
2	20	151	152	140	10	KIB	2	RIB	2	RIB	110101010	67.305	0.0	0.E+00						
2	21	171	172	160	10	KIB	2	RIB	2	RIB	110101010	67.305	0.0	0.E+00						
2	22	191	192	180	10	KIB	2	RIB	2	RIB	110101010	67.305	0.0	0.E+00						
2	23	211	212	200	10	KIB	2	RIB	2	RIB	110101010	67.305	0.0	0.E+00						
2	24	231	232	220	10	KIB	2	RIB	2	RIB	110101010	67.305	0.0	0.E+00						
2	25	12	13	7	10	KIB	2	RIB	2	RIB	110101010	77.289	0.0	0.E+00						
2	26	32	33	27	10	KIB	2	RIB	2	RIB	110101010	77.289	0.0	0.E+00						
2	27	52	53	47	10	KIB	2	RIB	2	RIB	110101010	77.289	0.0	0.E+00						
2	28	72	73	67	10	KIB	2	RIB	2	RIB	110101010	77.289	0.0	0.E+00						
2	29	92	93	87	10	KIB	2	RIB	2	RIB	110101010	77.289	0.0	0.E+00						
2	30	112	113	107	10	KIB	2	RIB	2	RIB	110101010	77.289	0.0	0.E+00						
2	31	132	133	127	10	KIB	2	RIB	2	RIB	110101010	77.289	0.0	0.E+00						
2	32	152	153	147	10	KIB	2	RIB	2	RIB	110101010	77.289	0.0	0.E+00						
2	33	172	173	167	10	KIB	2	RIB	2	RIB	110101010	77.289	0.0	0.E+00						
2	34	192	193	187	10	KIB	2	RIB	2	RIB	110101010	77.289	0.0	0.E+00						
2	35	212	213	207	10	KIB	2	RIB	2	RIB	110101010	77.289	0.0	0.E+00						
2	36	232	233	227	10	KIB	2	RIB	2	RIB	110101010	77.289	0.0	0.E+00						
2	37	13	14	14	10	KIB	2	RIB	2	RIB	110101010	79.058	0.0	0.E+00						
2	38	33	34	25	10	KIB	2	RIB	2	RIB	110101010	79.058	0.0	0.E+00						
2	39	53	54	48	10	KIB	2	RIB	2	RIB	110101010	79.058	0.0	0.E+00						
2	40	73	74	68	10	KIB	2	RIB	2	RIB	110101010	79.058	0.0	0.E+00						
2	41	93	94	86	10	KIB	2	RIB	2	RIB	110101010	79.058	0.0	0.E+00						
2	42	113	114	104	10	KIB	2	RIB	2	RIB	110101010	79.058	0.0	0.E+00						
2	43	133	134	128	10	KIB	2	RIB	2	RIB	110101010	79.058	0.0	0.E+00						
2	44	153	154	146	10	KIB	2	RIB	2	RIB	110101010	79.058	0.0	0.E+00						
2	45	173	174	168	10	KIB	2	RIB	2	RIB	110101010	79.058	0.0	0.E+00						
2	46	193	194	188	10	KIB	2	RIB	2	RIB	110101010	79.058	0.0	0.E+00						
2	47	213	214	208	10	KIB	2	RIB	2	RIB	110101010	79.058	0.0	0.E+00						
2	48	233	234	228	10	KIB	2	RIB	2	RIB	110101010	79.058	0.0	0.E+00						
2	49	14	242	242	29	KIB	2	RIB	2	RIB	110001010	84.564	0.0	0.E+00						
2	50	34	34	29	10	KIB	2	RIB	2	RIB	110001010	84.564	0.0	0.E+00						

BEAM CONNECTIVITY TABLE

BEAM NU.	JA	JB	JC	MAT. NU.	MAT. NAME	PROP. NO.	PROP. NAME	FIXITY	LENGTH	FIX	WEIGHT	TA	TB	TYA	TYB	TZA	TZB
51	54	242	49	10	RIB	2	RIB	110001010	84.564	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
52	74	242	69	10	RIB	2	RIB	110001010	84.564	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
53	94	242	89	10	RIB	2	RIB	110001010	84.564	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
54	114	242	109	10	RIB	2	RIB	110001010	84.564	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
55	134	242	129	10	RIB	2	RIB	110001010	84.564	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
56	154	242	144	10	RIB	2	RIB	110001010	84.564	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
57	174	242	169	10	RIB	2	RIB	110001010	84.564	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
58	194	242	184	10	RIB	2	RIB	110001010	84.564	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
59	214	242	204	10	RIB	2	RIB	110001010	84.564	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
60	234	242	229	10	RIB	2	RIB	110001010	84.564	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
61	13	15	12	17	STRUT	5	STRUT	100101010	71.000	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
62	33	35	32	17	STRUT	5	STRUT	100101010	71.000	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
63	53	55	52	17	STRUT	5	STRUT	100101010	71.000	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
64	73	75	72	17	STRUT	5	STRUT	100101010	71.000	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
65	93	95	42	17	STRUT	5	STRUT	100101010	71.000	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
66	113	115	112	17	STRUT	5	STRUT	100101010	71.000	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
67	133	135	132	17	STRUT	5	STRUT	100101010	71.000	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
68	153	155	152	17	STRUT	5	STRUT	100101010	71.000	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
69	173	175	172	17	STRUT	5	STRUT	100101010	71.000	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
70	193	195	192	17	STRUT	5	STRUT	100101010	71.000	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
71	213	215	212	17	STRUT	5	STRUT	100101010	71.000	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
72	233	235	232	17	STRUT	5	STRUT	100101010	71.000	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
73	242	243	14	15	HUB	4	HUB	110101010	79.104	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
74	6	11	10	19	TIPSO	6	TIPSO	100001010	16.603	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
75	26	31	30	19	TIPSO	6	TIPSO	100001010	16.603	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
76	46	51	50	19	TIPSO	6	TIPSO	100001010	16.603	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
77	66	71	70	19	TIPSO	6	TIPSO	100001010	16.603	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
78	86	91	90	19	TIPSO	6	TIPSO	100001010	16.603	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
79	106	111	110	14	TIPSO	6	TIPSO	100001010	16.603	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
80	126	131	130	19	TIPSO	6	TIPSO	100001010	16.603	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
81	146	151	150	19	TIPSO	6	TIPSO	100001010	16.603	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
82	166	171	170	19	TIPSO	6	TIPSO	100001010	16.603	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
83	186	191	190	19	TIPSO	6	TIPSO	100001010	16.603	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
84	206	211	210	19	TIPSO	6	TIPSO	100001010	16.603	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
85	226	231	230	19	TIPSO	6	TIPSO	100001010	16.603	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
86	6	7	10	8	STRIP	1	STRIP	110101010	73.724	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
87	26	27	30	8	STRIP	1	STRIP	110101010	73.724	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
88	46	47	50	8	STRIP	1	STRIP	110101010	73.724	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
89	66	67	70	8	STRIP	1	STRIP	110101010	73.724	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
90	86	87	90	8	STRIP	1	STRIP	110101010	73.724	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
91	106	107	110	8	STRIP	1	STRIP	110101010	73.724	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
92	126	127	130	8	STRIP	1	STRIP	110101010	73.724	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
93	146	147	150	8	STRIP	1	STRIP	110101010	73.724	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
94	166	167	170	8	STRIP	1	STRIP	110101010	73.724	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
95	186	187	190	8	STRIP	1	STRIP	110101010	73.724	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
96	206	207	210	8	STRIP	1	STRIP	110101010	73.724	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
97	226	227	230	8	STRIP	1	STRIP	110101010	73.724	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
98	7	8	12	8	STRIP	1	STRIP	110101010	75.783	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
99	27	28	32	8	STRIP	1	STRIP	110101010	75.783	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
100	47	48	52	8	STRIP	1	STRIP	110101010	75.783	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	

HEAM CONNECTIVITY TABLE

BEAM NO.	JA	JH	JG	MAT. NO.	MAT. NAML	PROP. NU.	PROP. NAME	FIXITY	LENGTH	FIX	WEIGHT	TA	TB	TYA	TYB	TZA	TZB
101	67	68	72	8	STRIP	1	STRIP	110101010	75.783	0.0	0.E+00	0.E+00	0.E+00	0.F+00	0.E+00	0.E+00	
102	87	88	92	8	STRIP	1	STRIP	110101010	75.783	0.0	0.E+00	0.F+00	0.E+00	0.E+00	0.E+00	0.E+00	
103	107	108	112	8	STRIP	1	STRIP	110101010	75.783	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
104	127	128	132	8	STRIP	1	STRIP	110101010	75.783	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
105	147	148	152	8	STRIP	1	STRIP	110101010	75.783	0.0	0.E+00	0.F+00	0.E+00	0.E+00	0.E+00	0.E+00	
106	167	168	172	8	STRIP	1	STRIP	110101010	75.783	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
107	187	188	192	8	STRIP	1	STRIP	110101010	75.783	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
108	207	208	212	8	STRIP	1	STRIP	110101010	75.783	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
109	227	228	232	8	STRIP	1	STRIP	110101010	75.783	0.0	0.E+00	0.F+00	0.E+00	0.E+00	0.E+00	0.E+00	
110	8	9	13	8	STRIP	1	STRIP	110101010	77.659	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
111	28	29	33	8	STRIP	1	STRIP	110101010	77.659	0.0	0.E+00	0.F+00	0.E+00	0.E+00	0.E+00	0.E+00	
112	48	49	53	8	STRIP	1	STRIP	110101010	77.659	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
113	68	69	73	8	STRIP	1	STRIP	110101010	77.659	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
114	88	89	93	8	STRIP	1	STRIP	110101010	77.659	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
115	108	109	113	8	STRIP	1	STRIP	110101010	77.659	0.0	0.E+00	0.F+00	0.E+00	0.E+00	0.E+00	0.E+00	
116	128	129	133	8	STRIP	1	STRIP	110101010	77.659	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
117	148	149	153	8	STRIP	1	STRIP	110101010	77.659	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
118	168	169	173	8	STRIP	1	STRIP	110101010	77.659	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
119	188	189	193	8	STRIP	1	STRIP	110101010	77.659	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
120	208	209	213	8	STRIP	1	STRIP	110101010	77.659	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
121	228	229	233	8	STRIP	1	STRIP	110101010	77.659	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
122	9	241	14	8	STRIP	1	STRIP	110101010	82.770	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
123	29	241	34	8	STRIP	1	STRIP	110101010	82.770	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
124	49	241	54	8	STRIP	1	STRIP	110101010	82.770	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
125	69	241	74	8	STRIP	1	STRIP	110101010	82.770	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
126	89	241	94	8	STRIP	1	STRIP	110101010	82.770	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
127	109	241	114	8	STRIP	1	STRIP	110101010	82.770	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
128	129	241	134	8	STRIP	1	STRIP	110101010	82.770	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
129	149	241	154	8	STRIP	1	STRIP	110101010	82.770	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
130	169	241	174	8	STRIP	1	STRIP	110101010	82.770	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
131	189	241	194	8	STRIP	1	STRIP	110101010	82.770	0.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
132	209	241	214	8	STRIP	1	STRIP	110101010	82.770	0.0	0.E+00	0.F+00	0.E+00	0.E+00	0.E+00	0.E+00	
133	229	241	234	8	STRIP	1	STRIP	110101010	82.770	0.0	0.E+00	0.F+00	0.E+00	0.E+00	0.E+00	0.E+00	
134	251	252	0	21	TGRPH	10	LONG	10000000000	162.19	B-B	3.3	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00
135	251	253	0	21	TGRPH	10	LONG	10000000000	124.48	B-B	2.5	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00
136	252	253	0	21	TGRPH	10	LONG	10000000000	124.48	B-B	2.5	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00
137	230	253	0	21	TGRPH	10	LONG	10000000000	105.95	B-B	2.2	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00
138	10	253	0	21	TGRPH	10	LONG	10000000000	105.95	B-B	2.2	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00
139	251	230	0	21	TGRPH	10	LONG	10000000000	81.460	B-B	1.7	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00
140	252	10	0	21	TGRPH	10	LONG	10000000000	81.460	B-B	1.7	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00
141	251	233	0	21	TGRPH	10	LONG	10000000000	172.71	B-B	5.5	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00
142	252	13	0	21	TGRPH	10	LONG	10000000000	172.71	B-B	5.5	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00
143	230	262	0	21	TGRPH	10	LONG	10000000000	155.69	B-B	3.2	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00
144	10	261	0	21	TGRPH	10	LONG	10000000000	155.69	B-B	3.2	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00
145	253	260	0	21	TGRPH	10	LONG	10000000000	150.00	B-B	3.0	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00
146	260	263	0	21	TGRPH	10	LONG	10000000000	130.00	B-B	2.6	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00
147	263	266	0	21	TGRPH	10	LONG	10000000000	130.00	B-B	2.6	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00
148	266	269	0	21	TGRPH	10	LONG	10000000000	130.00	B-B	2.6	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00
149	269	272	0	21	TGRPH	10	LONG	10000000000	130.00	B-B	2.6	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00
150	261	264	0	21	TGRPH	10	LONG	10000000000	130.00	B-B	2.6	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00

ORIGINAL FILE
OF POOR QUALITY

HEAM CONNECTIVITY TABLE

HEAM NO.	JA	JB	JC	MAT. NO.	MAT. NAME	PRUP. NO.	PRUP. NAME	FIXITY	LENGTH	FIX	WEIGHT	TA	TB	TYA	TYB	TZA	TZB
151	264	267	0	21	TGRPH	10	LUNG	1000000000	130.00	H-B	2.6	0.E+00	0.E+00	0.E+00	0.L+00	0.E+00	0.E+00
152	267	270	0	21	TGRPH	10	LUNG	1000000000	130.00	B-B	2.6	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00
153	270	273	0	21	TGRPH	10	LUNG	1000000000	130.00	B-B	2.6	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00
154	262	265	0	21	TGRPH	10	LONG	1000000000	130.00	B-B	2.6	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00
155	265	268	0	21	TGRPH	10	LONG	1000000000	130.00	H-B	2.6	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00
156	268	271	0	21	TGRPH	10	LONG	1000000000	130.00	B-B	2.6	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00
157	271	274	0	21	TGRPH	10	LUNG	1000000000	130.00	B-B	2.6	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00
158	260	261	0	21	TGRPH	12	PLAT	1000000000	78.740	B-B0.80	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
159	263	264	0	21	TGRPH	12	PLAT	1000000000	78.740	B-B0.80	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
160	266	267	0	21	TGRPH	12	PLAT	1000000000	78.740	B-B0.80	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
161	269	270	0	21	TGRPH	12	PLAT	1000000000	78.740	H-B0.80	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
162	272	273	0	21	TGRPH	12	PLAT	1000000000	78.740	H-B0.80	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
163	261	262	0	21	TGRPH	12	PLAT	1000000000	78.740	B-B0.80	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
164	264	265	0	21	TGRPH	12	PLAT	1000000000	78.740	B-B0.80	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
165	267	268	0	21	TGRPH	12	PLAT	1000000000	78.740	B-B0.80	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
166	270	271	0	21	TGRPH	12	PLAT	1000000000	78.740	H-B0.80	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
167	273	274	0	21	TGRPH	12	PLAT	1000000000	78.740	H-B0.80	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
168	260	261	0	21	TGRPH	12	PLAT	1000000000	78.740	B-B0.80	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
169	265	263	0	21	TGRPH	12	PLAT	1000000000	78.740	B-B0.80	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
170	268	266	0	21	TGRPH	12	PLAT	1000000000	78.740	B-B0.80	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
171	271	264	0	21	TGRPH	12	PLAT	1000000000	78.740	H-B0.80	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	0.E+00	
172	274	272	0	21	TGRPH	12	PLAT	1000000000	78.740	H-H0.80	0.E+00	0.E+00	0.E+00	0.U.L+00	0.U.E+00	0.U.E+00	
173	10	262	0	21	TGRPH	11	DIAG	1000000000	192.38	B-B0.76	0.E+00	0.E+00	0.E+00	0.U.E+00	0.E+00	0.U.E+00	
174	230	261	0	21	TGRPH	11	DIAG	1000000000	192.38	B-B0.76	0.E+00	0.E+00	0.E+00	0.U.E+00	0.E+00	0.U.E+00	
175	230	260	0	21	TGRPH	11	DIAG	1000000000	163.65	B-B0.73	0.E+00	0.E+00	0.E+00	0.U.E+00	0.E+00	0.U.E+00	
176	253	262	0	21	TGRPH	11	DIAG	1000000000	169.41	B-B0.67	0.E+00	0.E+00	0.U.E+00	0.U.L+00	0.U.E+00	0.U.E+00	
177	253	261	0	21	TGRPH	11	DIAG	1000000000	169.41	B-B0.67	0.E+00	0.E+00	0.U.E+00	0.U.E+00	0.U.E+00	0.U.E+00	
178	10	260	0	21	TGRPH	11	DIAG	1000000000	183.65	B-B0.73	0.E+00	0.E+00	0.E+00	0.U.E+00	0.E+00	0.U.E+00	
179	262	263	0	21	TGRPH	11	DIAG	1000000000	151.99	H-H0.60	0.E+00	0.E+00	0.E+00	0.U.E+00	0.E+00	0.U.E+00	
180	265	260	0	21	TGRPH	11	DIAG	1000000000	151.99	B-B0.60	0.E+00	0.E+00	0.U.E+00	0.U.E+00	0.U.E+00	0.U.E+00	
181	268	264	0	21	TGRPH	11	DIAG	1000000000	151.99	B-B0.60	0.E+00	0.E+00	0.U.E+00	0.U.E+00	0.U.E+00	0.U.E+00	
182	271	272	0	21	TGRPH	11	DIAG	1000000000	151.99	B-B0.60	0.E+00	0.E+00	0.U.E+00	0.U.E+00	0.U.E+00	0.U.E+00	
183	260	265	0	21	TGRPH	11	DIAG	1000000000	151.99	B-B0.60	0.E+00	0.E+00	0.U.E+00	0.U.E+00	0.U.E+00	0.U.E+00	
184	263	268	0	21	TGRPH	11	DIAG	1000000000	151.99	B-B0.60	0.E+00	0.E+00	0.U.E+00	0.U.E+00	0.U.E+00	0.U.E+00	
185	266	271	0	21	TGRPH	11	DIAG	1000000000	151.99	H-H0.60	0.E+00	0.E+00	0.U.E+00	0.U.E+00	0.U.E+00	0.U.E+00	
186	269	274	0	21	TGRPH	11	DIAG	1000000000	151.99	H-H0.60	0.E+00	0.E+00	0.U.E+00	0.U.E+00	0.U.E+00	0.U.E+00	
187	260	264	0	21	TGRPH	11	DIAG	1000000000	151.99	B-B0.60	0.E+00	0.E+00	0.U.E+00	0.U.E+00	0.U.E+00	0.U.E+00	
188	263	267	0	21	TGRPH	11	DIAG	1000000000	151.99	B-B0.60	0.E+00	0.E+00	0.U.E+00	0.U.E+00	0.U.E+00	0.U.E+00	
189	266	270	0	21	TGRPH	11	DIAG	1000000000	151.99	B-B0.60	0.E+00	0.E+00	0.U.E+00	0.U.E+00	0.U.E+00	0.U.E+00	
190	269	273	0	21	TGRPH	11	DIAG	1000000000	151.99	B-B0.60	0.E+00	0.E+00	0.U.E+00	0.U.E+00	0.U.E+00	0.U.E+00	
191	261	263	0	21	TGRPH	11	DIAG	1000000000	151.99	B-B0.60	0.E+00	0.E+00	0.U.E+00	0.U.E+00	0.U.E+00	0.U.E+00	
192	264	266	0	21	TGRPH	11	DIAG	1000000000	151.99	B-B0.60	0.E+00	0.E+00	0.U.E+00	0.U.E+00	0.U.E+00	0.U.E+00	
193	267	269	0	21	TGRPH	11	DIAG	1000000000	151.99	B-B0.60	0.E+00	0.E+00	0.U.E+00	0.U.E+00	0.U.E+00	0.U.E+00	
194	270	272	0	21	TGRPH	11	DIAG	1000000000	151.99	B-B0.60	0.E+00	0.E+00	0.U.E+00	0.U.E+00	0.U.E+00	0.U.E+00	
195	261	265	0	21	TGRPH	11	DIAG	1000000000	151.99	B-B0.60	0.E+00	0.E+00	0.U.E+00	0.U.E+00	0.U.E+00	0.U.E+00	
196	264	268	0	21	TGRPH	11	DIAG	1000000000	151.99	B-B0.60	0.E+00	0.E+00	0.U.E+00	0.U.E+00	0.U.E+00	0.U.E+00	
197	267	271	0	21	TGRPH	11	DIAG	1000000000	151.99	B-B0.60	0.E+00	0.E+00	0.U.E+00	0.U.E+00	0.U.E+00	0.U.E+00	
198	270	274	0	21	TGRPH	11	DIAG	1000000000	151.99	B-B0.60	0.E+00	0.E+00	0.U.E+00	0.U.E+00	0.U.E+00	0.U.E+00	
199	262	264	0	21	TGRPH	11	DIAG	1000000000	151.99	B-B0.60	0.E+00	0.E+00	0.U.E+00	0.U.E+00	0.U.E+00	0.U.E+00	
200	265	267	0	21	TGRPH	11	DIAG	1000000000	151.99	B-B0.60	0.E+00	0.E+00	0.U.E+00	0.U.E+00	0.U.E+00	0.U.E+00	

BEAM CONNECTIVITY TABLE

BEAM NO.	JA	JH	JC	MAT. NO.	MAT. NAME	PROP. NO.	PROP. NAME	FLXITY	LENTH	FIX	WEIGHT	TA	TB	TC	TD	TE	TF
201	268	270	0	21	TGRPH	11	DIAG	1000000000	151.99	B-B0.60	0.E+00						
202	271	273	0	21	TGRPH	11	DIAG	1000000000	151.99	B-B0.60	0.E+00						

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NUDAL WEIGHTS (IN ADDITION TO DISTRIBUTED WEIGHTS)

NODE	WEIGHT	NODE	WEIGHT	NODE	WEIGHT	NODE	WEIGHT	NODE	WEIGHT	NODE	WEIGHT	NODE	WEIGHT	
0	1 .91430E-01	2	.15200	3	.11800	4	.18590E-01	5	.12790E-01	6	.19300	7	.35400	
0	6 .19300	8	.31100	9	.32100	10	.47000	11	.14900	12	.27500	13	.59100	
0	11 .14900	14	.31100	15	.12300	16	.00000	17	.00000	18	.00000	19	.00000	
0	16 .00000	20	.00000	21	.91430E-01	22	.15200	23	.11800	24	.18590E-01	25	.12790E-01	
0	26 .19300	26	.35400	27	.31100	28	.31100	29	.32100	30	.46100	31	.14900	
0	31 .14900	32	.27500	33	.41500	34	.31100	35	.12300	36	.00000	37	.00000	
0	36 .00000	38	.00000	39	.00000	40	.00000	41	.91430E-01	42	.15200	43	.11800	
0	46 .19300	44	.18590E-01	45	.12790E-01	46	.35400	47	.31100	48	.31100	49	.32100	
0	51 .14900	52	.27500	53	.41500	54	.51100	55	.12300	56	.00000	57	.00000	
0	56 .00000	58	.00000	59	.00000	60	.00000	61	.91430E-01	62	.15200	63	.11800	
0	66 .19300	64	.18590E-01	65	.12790E-01	66	.35400	67	.31100	68	.31100	69	.32100	
0	71 .14900	72	.27500	73	.41500	74	.51100	75	.12300	76	.00000	77	.00000	
0	76 .00000	78	.00000	79	.00000	80	.00000	81	.91430E-01	82	.15200	83	.11800	
0	81 .91430E-01	84	.18590E-01	85	.12790E-01	86	.35400	87	.31100	88	.31100	89	.32100	
0	91 .19300	92	.27500	93	.41500	94	.51100	95	.12300	96	.00000	97	.00000	
0	96 .00000	98	.00000	99	.00000	100	.00000	101	.91430E-01	102	.15200	103	.11800	
0	101 .91430E-01	104	.18590E-01	105	.12790E-01	106	.19300	107	.35400	108	.31100	109	.32100	
0	111 .14900	112	.27500	113	.41500	114	.51100	115	.12300	116	.00000	117	.00000	
0	116 .00000	118	.00000	119	.00000	120	.00000	121	.91430E-01	122	.15200	123	.11800	
0	121 .91430E-01	124	.18590E-01	125	.12790E-01	126	.19300	127	.35400	128	.31100	129	.32100	
0	131 .14900	132	.27500	133	.41500	134	.51100	135	.12300	136	.00000	137	.00000	
0	136 .00000	138	.00000	139	.00000	140	.00000	141	.91430E-01	142	.15200	143	.11800	
0	146 .19300	147	.35400	148	.31100	149	.32100	150	.46100	151 .14900	152	.27500	153	.41500
0	151 .14900	154	.51100	155	.12300	156	.00000	157	.00000	158	.00000	159	.00000	
0	161 .91430E-01	160	.10590E-01	161	.12790E-01	162	.15200	163	.11800	164	.18590E-01	165	.12790E-01	
0	166 .19300	167	.35400	168	.31100	169	.31100	170	.46100	171 .14900	172	.27500	173	.41500
0	171 .14900	174	.51100	175	.12300	176	.00000	177	.00000	178	.00000	179	.00000	
0	176 .00000	180	.00000	181	.91430E-01	182	.15200	183	.11800	184	.18590E-01	185	.12790E-01	
0	186 .19300	187	.35400	188	.31100	189	.31100	190	.46100	191 .14900	192	.27500	193	.41500
0	191 .14900	194	.51100	195	.12300	196	.00000	197	.00000	198	.00000	199	.00000	
0	196 .00000	200	.00000	201	.91430E-01	202	.15200	203	.11800	204	.18590E-01	205	.12790E-01	
0	201 .91430E-01	206	.19300	207	.35400	208	.31100	209	.31100	210	.46100	211 .14900	212	.27500
0	211 .14900	213	.41500	214	.51100	215	.12300	216	.00000	217	.00000	218	.00000	
0	216 .00000	219	.00000	220	.00000	221	.91430E-01	222	.15200	223	.11800	224	.18590E-01	
0	221 .91430E-01	225	.12790E-01	226	.19300	227	.35400	228	.31100	229	.32100	230	.47000	
0	231 .14900	232	.27500	233	.41500	234	.51100	235	.12300	236	.00000	237	.00000	
0	236 .00000	238	.00000	239	.00000	240	.00000	241 .19300	242	.31100	243	.46000	244	.00000
0	241 .19300	245	.00000	246	.00000	247	.00000	248	.00000	249	.00000	250	.00000	
0	246 .00000	251	.50000	252	.50000	253	.60000	254	.00000	255	.00000	256	.00000	
0	256 .00000	257	.00000	258	.00000	259	.00000	260	.49800	261	.50200	262	.46500	
0	261 .50200	263	.46500	264	.46500	265	.46500	266	.46500	267	.46500	268	.46500	
0	266 .46500	269	.46500	270	.46500	271	.46500	272	.27200	273	.27200	274	.27200	

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THE ELLIPTICAL AND HYPERBOLIC SYSTEMS DEFINED BY J_A, J_H, J_C = 248 249 250 ARE:

0.31965E+03	0.00000E+01	0.00000E+01	0.00000E+01	0.27176E-05	0.22034E+01
0.00000E+01	0.51965E+03	0.00000E+01	0.00000E+01	0.27176E-05	0.00000E+01
0.00000E+01	0.00000E+01	0.31965E+03	0.22034E+03	0.22106E+05	0.22106E+05
0.00000E+01	0.27176E-05	0.22034E+01	0.00000E+01	0.00000E+05	0.00000E+01
-0.27176E-05	0.00000E+01	0.22034E+01	0.10331E+01	0.47458E+07	0.38624E-04
0.22034E+01	0.22106E+05	0.00000E+01	0.22210E+05	0.20521E+08	0.10824E-03
				0.23537E+08	

FORCES APPLIED W.H.T. ASSEMBLY D.O.F.

NODE	SYS	DOF 1	DOF 2	DOF 3	DOF 4	DOF 5	DOF 6
------	-----	-------	-------	-------	-------	-------	-------

TOTAL FORCE FOR DOF 1 = 0.0000
TOTAL FORCE FOR DOF 2 = 0.0000
TOTAL FORCE FOR DOF 3 = 0.0000
TOTAL FORCE FOR DOF 4 = 0.0000
TOTAL FORCE FOR DOF 5 = 0.0000
TOTAL FORCE FOR DOF 6 = 0.0000

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NODE VS. DUF TABLE

NODE	SYS	LNUF	ENU	BAND	NODE	SYS	LNUF	ENU	BAND	NODE	SYS	LNUF	ENU	BAND	NODE	SYS	LNUF	ENU	BAND	
1	3	111000	1	1	2	3	111000	1	1	3	111000	1	1	1	3	111000	1	1	1	
4	3	111000	10	7	5	3	111000	13	7	6	3	111111	16	16	7	3	111111	16	16	
7	3	111111	22	22	4	3	111111	28	25	9	3	111111	34	28	4	3	111111	34	28	
10	3	111111	40	40	11	3	111111	40	31	12	3	111111	52	43	5	3	111111	52	43	
13	3	111111	58	46	14	3	111111	64	31	15	3	111111	70	31	6	3	111111	70	31	
16	0	0	0	-2	17	0	0	-2	16	0	0	0	-2	16	0	0	0	-2	16	
19	0	0	3	-2	20	0	0	-2	21	3	111000	76	61	7	3	111000	76	61		
22	3	111000	79	58	23	3	111000	82	55	24	3	111000	85	34	8	3	111000	85	34	
25	3	111000	88	31	26	3	111111	91	76	27	3	111111	97	22	9	3	111111	97	22	
28	3	111111	103	25	29	3	111111	109	70	30	3	111111	115	76	10	3	111111	115	76	
31	3	111111	121	76	32	3	111111	127	43	33	3	111111	133	94	11	3	111111	133	94	
34	3	111111	139	76	35	3	111111	145	88	36	0	0	0	12	3	111111	145	88		
37	0	0	-2	38	0	0	-2	39	0	0	0	0	-2	39	0	0	0	-2	39	
40	0	0	0	-2	41	0	0	-2	42	0	0	0	0	-2	42	0	0	0	-2	42
43	3	111000	157	55	44	3	111000	160	34	45	3	111000	163	31	13	3	111000	163	31	
46	3	111111	166	76	50	3	111111	172	22	48	3	111111	178	25	14	3	111111	178	25	
49	3	111111	184	76	50	3	111111	190	76	51	3	111111	196	76	15	3	111111	196	76	
52	3	111111	202	43	51	3	111111	208	94	54	3	111111	214	76	16	3	111111	214	76	
55	3	111111	220	68	56	0	0	-2	57	0	0	0	-2	57	0	0	0	-2	57	
58	0	0	0	-2	59	0	0	-2	60	0	0	0	-2	60	0	0	0	-2	60	
61	3	111000	226	61	62	3	111000	229	58	63	3	111000	232	55	15	3	111000	232	55	
64	3	111000	235	34	65	3	111000	238	31	66	3	111111	241	76	18	3	111111	241	76	
67	3	111111	247	22	68	3	111111	253	25	69	3	111111	259	76	21	3	111111	259	76	
70	3	111111	265	76	71	3	111111	271	76	72	3	111111	277	43	24	3	111111	277	43	
73	3	111111	283	94	74	3	111111	289	76	75	3	111111	295	86	27	3	111111	295	86	
76	0	0	0	-2	77	0	0	-2	78	0	0	0	-2	78	0	0	0	-2	78	
79	0	0	0	-2	80	0	0	-2	80	0	0	0	-2	81	0	0	0	-2	81	
82	0	0	0	-2	83	0	0	-2	83	0	0	0	-2	84	0	0	0	-2	84	
85	3	111000	313	31	86	3	111000	307	55	84	3	111000	310	34	8	3	111000	310	34	
88	3	111111	326	25	89	3	111111	334	76	93	3	111111	340	76	94	3	111111	340	76	
91	3	111111	346	76	92	3	111111	352	43	93	3	111111	358	94	95	3	111111	358	94	
94	3	111111	364	76	95	3	111111	370	88	96	0	0	0	0	0	0	0	0	0	
97	0	0	0	-2	98	0	0	-2	99	0	0	0	-2	99	0	0	0	-2	99	
100	0	0	0	-2	101	0	0	-2	101	0	0	0	-2	102	0	0	0	-2	102	
103	3	111000	382	55	104	3	111000	385	34	105	3	111000	388	31	106	3	111000	388	31	
106	3	111111	391	76	107	3	111111	397	22	108	3	111111	403	25	109	3	111111	403	25	
109	3	111111	409	76	110	3	111111	415	76	111	3	111111	421	76	112	3	111111	421	76	
112	3	111111	427	43	113	3	111111	433	94	114	3	111111	439	76	115	3	111111	439	76	
115	3	111111	445	44	116	0	0	0	117	0	0	0	0	0	0	0	0	0	0	
118	0	0	0	-2	119	0	0	-2	120	0	0	0	-2	120	0	0	0	-2	120	
121	3	111000	451	61	122	3	111000	454	58	123	3	111000	457	55	124	3	111000	457	55	
124	3	111000	460	34	125	3	111000	463	31	126	3	111000	466	76	127	3	111000	466	76	
127	3	111111	472	22	128	3	111111	478	25	129	3	111111	484	76	130	3	111111	484	76	
130	3	111111	490	76	131	3	111111	496	76	132	3	111111	502	43	133	3	111111	502	43	
133	3	111111	508	44	134	3	111111	514	76	135	3	111111	520	66	136	3	111111	520	66	
136	0	0	0	-2	137	0	0	-2	138	0	0	0	-2	138	0	0	0	-2	138	
139	0	0	0	-2	140	0	0	-2	141	0	0	0	-2	141	0	0	0	-2	141	
142	3	111000	529	54	143	3	111000	532	55	144	3	111000	535	54	145	3	111000	535	54	
145	3	111111	533	25	146	3	111111	541	76	147	3	111111	547	22	148	3	111111	547	22	
151	3	111111	571	76	152	3	111111	577	43	153	3	111111	583	94	154	3	111111	583	94	
157	0	0	0	-2	158	0	0	-2	159	0	0	0	-2	159	0	0	0	-2	159	
160	0	0	0	-2	161	0	0	-2	162	0	0	0	-2	162	0	0	0	-2	162	
163	3	111000	607	55	164	3	111000	610	34	165	3	111000	615	31	166	3	111000	615	31	
166	3	111111	616	76	167	0	0	0	0	0	0	0	0	0	0	0	0	0	0	

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169	3 111111	634	76	170	3 111111	640	-2	171	3 111111	646	76
172	3 111111	652	43	173	3 111111	658	94	174	3 111111	664	76
175	3 111111	670	88	176	0 0 0	0 0	-2	177	0 0 0	0 0	-2
178	0 0 0	0 -2	179	0 0 0	0 0	-2	180	0 0 0	0 0	0 0	-2
181	3 111000	676	61	182	3 111000	679	58	183	3 111000	682	55
184	3 111000	685	34	185	3 111000	688	51	186	3 111111	691	76
187	3 111111	697	72	188	3 111111	703	25	189	3 111111	709	76
190	3 111111	715	76	191	3 111111	721	76	192	3 111111	727	43
193	3 111111	733	94	194	3 111111	737	76	195	3 111111	745	84
196	0 0 0	0 -2	197	0 0 0	0 0	-2	198	0 0 0	0 0	0 0	-2
199	0 0 0	0 -2	200	0 0 0	0 0	-2	201	3 111000	751	61	
202	3 111000	754	58	203	3 111000	757	55	204	3 111000	760	34
205	3 111000	763	31	206	3 111111	766	76	207	3 111111	772	22
208	3 111111	778	25	209	3 111111	784	76	210	3 111111	790	76
211	3 111111	796	76	212	3 111111	802	43	213	3 111111	808	94
214	3 111111	814	76	215	3 111111	820	88	216	0 0 0	0 0	-2
217	0 0 0	0 -2	218	0 0 0	0 0	-2	219	0 0 0	0 0	0 0	-2
220	0 0 0	0 -2	221	3 111000	826	61	222	3 111000	829	58	
223	3 111000	832	55	224	3 111000	835	34	225	3 111000	838	31
226	3 111111	841	841	227	3 111111	847	847	228	3 111111	853	850
229	3 111111	859	853	230	3 111111	865	865	231	3 111111	871	826
232	3 111111	877	868	233	3 111111	883	871	234	3 111111	884	826
235	3 111111	895	838	236	0 0 0	0 0	-2	237	0 0 0	0 0	-2
238	0 0 0	0 -2	239	0 0 0	0 0	-2	240	0 0 0	0 0	0 0	-2
241	3 111111	901	868	242	3 111111	907	844	243	3 111111	913	856
244	0 0 0	0 -2	245	0 0 0	0 0	-2	246	0 0 0	0 0	0 0	-2
247	0 0 0	0 -2	248	0 0 0	0 0	-2	249	0 0 0	0 0	0 0	-2
250	0 0 0	0 -2	251	3 111000	919	55	252	3 111000	922	883	
253	3 111000	925	886	254	0 0 0	0 0	-2	255	0 0 0	0 0	-2
256	0 0 0	0 -2	257	0 0 0	0 0	-2	258	0 0 0	0 0	0 0	-2
254	0 0 0	0 -2	260	3 111000	928	889	261	3 111000	931	892	
262	3 111000	934	895	263	3 111000	937	10	264	3 111000	940	13
265	3 111000	943	16	266	3 111000	946	10	267	3 111000	949	13
268	3 111000	952	16	269	3 111000	955	10	270	3 111000	958	13
271	3 111000	961	16	272	3 0 0	0 0	-2	273	3 0 0	0 0	-2
274	3 0 0	0 -2									

THE LARGEST STRUCTURAL NUOE NUMBER = 274
THE TOTAL NUMBER OF EQUATIONS = 963
THE TOTAL NUMBER OF RELOADS = 131193
THE MAXIMUM D.O.F. AT ANY NUOE = 6
THE NUMBER OF SOLUTION INCREMENTS = 1
THE VALUE OF THE GROUND SPRING = 0.100000E+31
THE GRAVITY DIRELCTION IS FROM NUOE 248 TO NUOE 249
THE ROTATION LIMIT = 0.100000E+02

INGHITS = 0 INGHITM = 0 INGHITH = 0
ITEMPS = 0 ITEMPM = 0 ITEMPH = 0
IPRESHN = 0
LOCG = 0 LOCS = 0 LOCN = 0
INPUT = 1 ISTART = 0 IRROOT = 1
ITER = 0 LUCH = 0 LOCRT = 0
IFORCE = 0 LOCSTF = 10 NRFRMK = 0
NASTY = 0 IRSTR1 = 0 IPHET = 0
IPGLUH = 0 IPSTR1 = 0 IPMEMH = 0
IPHIMP = 0 IPBEAM = 0 IPFGLU = 0
IPDOP = 0 IPDISP = 0 IPDGLH = 0
IPSTHL = 0 IPDML = 0 IPBML = 0
IPKU = 0 F = 0.7097E-03 ZOU = 0.0000E+01

FMAXA = 0.0900E+01
• ASG,T 1.,D/// 144044 .
• ASG,T 2.,D/// 144044 .
• ASG,T 3.,D/// 144044 .

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INPUT DATA PROCESSED AND CHECKED. EXECUTION NOT REQUESTED

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