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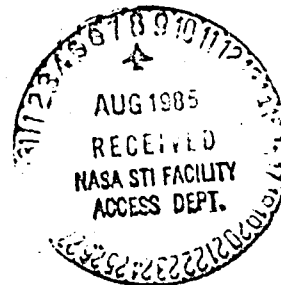
FUSELAGE UPWASH EFFECTS ON
RSRA ROTOR SYSTEMS

J. Cowan
L. Dadone

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RSRA ROTOR SYSTEMS

J. Cowan
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Philadelphia, Pennsylvania

Prepared for
Ames Research Center
under Contract NAS2-11307

August 1985



National Aeronautics and
Space Administration

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LIST OF SYMBOLS

| | |
|-------|--|
| C_d | Blade element drag coefficient, drag/qc |
| C_l | Blade element lift coefficient, lift/qc |
| C_m | Blade element pitching moment coefficient about the quarter chord, moment/qc ² |
| D | Rotor diameter, ft |
| DE | Rotor equivalent drag, rotor power/V-X, pounds |
| fe | Flat plate equivalent area, ft ² |
| FZF | Vertical hub force fourth harmonic amplitude, lbs |
| GW | Gross Weight, pounds |
| L | Wing lift, pounds |
| M | Mach number |
| P | Auxiliary thrust, pounds |
| PLL | Pitch link vibratory load, lbs |
| q | Dynamic pressure, $\frac{1}{2}\rho V_\infty^2$ |
| Q_n | nth harmonic of rotor torque, ft-pounds |
| Q_0 | Steady or average rotor torque, ft-pounds |
| R | Blade radius, ft |
| T | Vertical component of rotor thrust, pounds |
| T_n | nth harmonic of rotor thrust, pounds Also, particular value of T in Tables II and III, pounds |
| T_0 | Steady or average rotor thrust, pounds |
| UP | Nondimensional difference between out-of-disk velocity component in the presence of fuselage/wings/engines and out-of-disk velocity component in the absence of fuselage/wings/engines |
| UT | Nondimensional difference between in-disk chordwise velocity component in the presence of fuselage/wings/engines and in-disk chordwise velocity component in the absence of fuselage/wings/engines |

LIST OF SYMBOLS
(Continued)

- V Flight velocity, ft/sec or knots
- V_T Rotor tip speed, ft/sec
- x Fuselage station in fuselage coordinate system, in
- X Rotor propulsive force, pounds
- \bar{X} Nondimensional rotor propulsive force, $X/qD^2\sigma$
- y Buttline in fuselage coordinate system, in
- z Waterline in fuselage coordinate system, in
- α_s Rotor shaft angle, degrees
- ΔU_P Same as UP but not nondimensionalized by rotor tip speed, ft/sec
- ΔU_T Same as UT but not nondimensionalized by rotor tip speed, ft/sec
- μ' Nondimensional flight velocity, V/V_T
- σ Rotor solidity
- ψ Blade azimuth angle, degrees

1.0 SUMMARY

The effects of RSRA fuselage configurations on rotor performance and loads have been quantified analytically by means of currently available potential flow and rotor analysis methods.

Four configurations of the Rotor Systems Research Aircraft (RSRA) were considered in this study. They were:

- 1) Fuselage alone (conventional helicopter)
- 2) Fuselage with auxiliary propulsion
- 3) Fuselage with wings (auxiliary lift)
- 4) Fuselage with both auxiliary lift and propulsion

The rotor system investigated was identical to a CH-47D front rotor except that it had four instead of three blades. Two scaled-down versions of the same rotor were also analyzed to determine the effect of rotor scale on the fuselage upwash effects.

The flight conditions considered for the upwash study are discussed. The potential flow models for the RSRA configuration, with and without the wings and the auxiliary propulsion system, are presented. The results of fuselage/wing/propulsion system upwash on performance and loads are also presented.

The plethora of data resulting from this study reflected the existence of complicated flow interactions and did not lend itself to straightforward interpretation in all cases. More often than not though, neglecting fuselage upwash causes an underestimation of performance and an underestimation of loads.

The appendices contain potential flow model coordinates, upwash value tabulations, loads analysis comparisons supplementary to those shown in figures, and examples of surface plots.

2.0 INTRODUCTION

The proximity of the fuselage to the rotor of a helicopter has a significant effect on the flow environment at the rotor. Recent flight tests (particularly the YUH-61A flight test experience) have shown that rotor/fuselage separation is one of the dominant parameters in determining rotor-induced vibratory loads, with associated detrimental effects ranging from pilot/passenger discomfort to reduced fatigue life of blades and control system, and to a possible degradation of performance and rotor limits. The fuselage proximity effects would be further magnified on helicopters utilizing auxiliary means of lift and propulsion because of the additional flow changes introduced by wings and fans.

The Rotor System Research Aircraft (RSRA) is the ideal system to explore combinations of rotors with auxiliary lift and auxiliary propulsion devices, but the understanding of the results of a flight test program would be strongly influenced by the degree to which mutual interference effects between helicopter components can be quantified.

The analytical methods necessary to assess fuselage, wing, and propulsion system effects on the flow field have been sufficiently improved to allow calculations of this nature to be carried out on computers having an adequate capacity. At the same time rotor loads and performance analysis methods have been developed which successfully predict the characteristics of helicopter rotors at all but the more extreme flight conditions.

The combination of three-dimensional potential flow and rotor loads/performance analysis methods has been the subject of research during recent years. The preliminary results have been encouraging, and data handling procedures have been developed which have considerably reduced the interface problems between potential flow and rotor analysis codes.

During this study, an approximation to the effects of fuselage/wing/engine proximity was determined by the coupling of a three-dimensional potential flow program with rotor loads and performance analyses. The approximation was made in order to assess the character of these effects on loads and performance. A close approximation would have involved an iterative process - determining the influence of fuselage/wing/engine proximity on loads and performance, determining the influence of rotor-induced downwash on the potential flow about the structures, and repeating the cycle. This study was limited to using only the first step, determining the initial influence of structural proximity on the rotor environment. The iterative process was outside the scope of the present study.

Previous efforts to determine the effects of fuselage proximity on rotor loads and performance were limited by the crudeness of the potential flow models or the rotor analyses. Two of these efforts were reported by Rahnema (Reference 1) and by Bain and Landgrebe (Reference 2). Rahnema investigated the alleviation of rotor loads with calculations that used only a single point source in a uniform free stream to model the flow about a fuselage. Bain and Landgrebe used a lifting line for the wing of a compound helicopter. The present study, by contrast, uses a fully three-dimensional panel method with wing vorticity distributed chordwise to model the flow about aerodynamic bodies.

3.0 A GENERAL DESCRIPTION OF FUSELAGE/WING/ENGINE UPWASH EFFECTS AND OF THEIR MODELING

Although isolated rotor tests and calculations are most often employed in the definition of advanced rotor systems, it is understood that the final success of a rotor system depends on its integration with fuselage components. In particular, test and theory have shown that the placement of the rotor with respect to the fuselage of a helicopter introduces changes in the rotor flow field which must be accounted for to determine realistic load and performance levels.

The presence of substantial lifting elements on the fuselage and the effect of auxiliary propulsion devices is very likely to increase the influence of the fuselage upwash on rotor performance and loads, making it even more critical that well documented rotor placement guidelines be established. Establishing these guidelines is outside the scope of the present study, but such establishing must be based on analyses such as those reported herein or data gathered from tests.

The overall effects of fuselage/wing/engine upwash on a rotor were the object of this investigation. Considering only a single blade element, the structure induces an increment to the velocity component normal to the local free stream which would exist if no other structures were near the rotor. This increment changes the local angle of attack and, therefore, the airloads, flapping, and stresses.

The flow about three-dimensional bodies can be evaluated by computational potential flow methods, as well as methods involving more fundamental, and therefore more complex and expensive, approaches. In particular, the singularity panel methods are the simplest and least expensive for 3-D flow. They are adequate for the present purpose, since the effects of viscosity and vorticity, neglected by such methods, are significant only close to the fuselage/wings/engines, not in the off-body region where the rotor blades are located.

To obtain a 3-D potential flow solution with TEA-230 (Reference 3), a panel method, the surface of a body is approximated by a number of flat, or nearly flat surfaces (panels), where the size of the panels is dictated by the local surface curvature and by the need for accuracy in the calculated surface velocities. A potential flow solution for a given body is then obtained by prescribing, among other conditions, the requirement that there be no flow through the panels. Local velocities are then estimated at the centroid of each panel and at any required point off the body.

Figure 3-1 illustrates the overall logic in carrying out rotor/fuselage upwash interaction calculations. The rotor analysis program shown in the diagram is the B-65 performance code, Reference 4. The C-60 loads analysis, Reference 5, can be introduced in the same way.

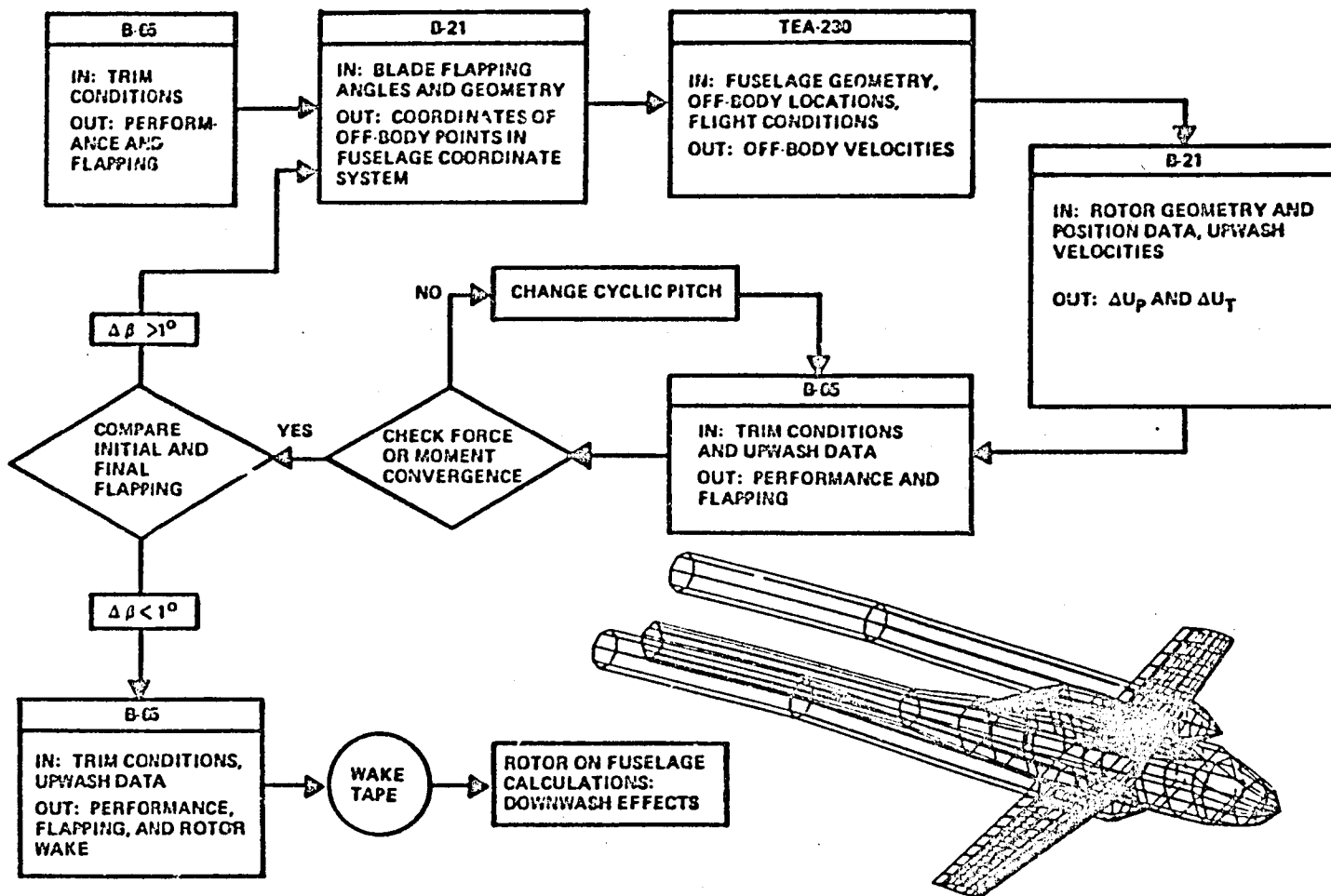


Figure 3-1. Single Rotor Upwash Calculation Procedure

The process is started with isolated rotor trim conditions. The initial blade flapping schedule is used by the B-21 processor code to calculate the coordinates of blade computation points in the fuselage coordinate system. The off-body point coordinates are then input into the 3-D analysis (TEA-230) and off-body velocities are calculated. The B-21 code converts the off-body velocities into incremental rotor velocities which are introduced into B-65 or C-60. Finally, B-65 or C-60 is run until a solution is obtained which satisfies the required trim in the presence of the fuselage upwash velocities at the blade computation points. The process is repeated only if substantial changes in blade flapping angles take place.

The manipulation of output from one program into input for another is performed automatically by the B-21 code. The only manual operations necessary are entering some of the B-65 or C-60 output into B-21 input, merging the B-21 output into TEA-230, and merging some of the TEA-230 output into the final B-21 input.

4.0 DESCRIPTION OF THE CODES USED

4.1 The B-65 Rotor Performance Analysis

The Rotor Performance Analysis, B-65, is described in Reference 4. The code was developed at Boeing Vertol. The basis for the code is a model of the wake trailed by each blade, which wake is represented by groups of straight vortex segments with linearly varying vorticity from one end to the other of each segment. A root and a tip vortex are rolled up after a fixed azimuthal interval (1/8th of a revolution) at a radial location which is determined from the instantaneous spanwise blade loading (Betz criteria). The vortex sheet trailed by each blade is modeled by a system of vortices identified as the near-wake, attached to the blade quarter chord line and trailed 1/24th of a revolution ($\Delta\Psi = 15^\circ$), and a mid-wake, which extends for two additional time intervals ($\Delta\Psi = 30^\circ$) beyond the near-wake.

As the B-65 code subdivides a rotor blade into 13 spanwise segments of equal length, cutout to tip, the vortex sheet trailed by each blade is represented by 13 horseshoe vortices. Except for the initial Betz rollup criteria which set the spanwise location of the tip vortices, the wake model is otherwise rigid, and its displacement is a combination of flight kinematics with a uniform induced downwash velocity.

Blade elastic properties are represented by a modal approach. Two flap bending and one torsion mode are used to model the elastic properties. The aerodynamic formulation, based on a lifting line system, includes an approximation of unsteady effects, dynamic stall delay, radial flow, reverse flow, and three-dimensional tip relief effects.

The sectional characteristics are obtained by look-up and interpolation of tables of two-dimensional airfoil data compiled from experimental or analytical sources. The tabulated airfoil characteristics are listed in the following sequence:

- (a) Lift Coefficient, C_l . Presented as a function of angle of attack at fixed Mach number levels, for angles from 0° to 20° , and from -20° (340°) back to 0° (360°), for Mach numbers from $M = 0.0$ to $M = 1.0$. Lift data from 20° to 340° is simulated by equations based on test data for the NACA 0012 airfoil, Reference 4. These equations are independent of Mach number as they are meant to approximate the high angle-of-attack flow conditions inside the reverse flow circle.
- (b) Drag Coefficient, C_d . Drag is presented as a function of Mach number, for $M = 0.0$ to $M = 1.0$, at constant angle of attack levels over an angle of attack range which can be specified in the input. Outside of the specified angle of attack range the drag is approximated by equations independent of Mach number and based on NACA 0012 test data.

(c) Pitching Moment Coefficient, C_m . Pitching moments are tabulated as a function of Mach number, from $M = 0.0$ to $M = 1.0$, for angles of attack from 0° to 16° , and from -16° (344°) to 0° (360°). Equations based on NACA 0012 data cover the rest of the high angle of attack range.

B-65 output consists of airload and power distributions across the blades at 24 azimuthal locations. It also includes the distribution of elastic twist and deflections at those locations. Flapping angle is output in harmonic form and the other distributions can be harmonically analyzed. No specific number of harmonics is modeled because flapping is determined by solving a differential equation for flapping angle instead of simply finding the Fourier coefficients of an assumed harmonic behavior.

The accuracy of this code is reflected in Figure 4-1. In this figure, "Configuration 6" designates a particular blade planform, "BVWT" means Boeing Vertol Wind Tunnel, "BVWT 256" is a particular wind tunnel test, and "WOZ" means "wind-off zero."

4.2 The C-60 Dynamics Loads Analysis

The Dynamics Loads Analysis was developed at Boeing Vertol by the Rotor Dynamics Group. A detailed description of C-60 can be found in Reference 5.

C-60 uses a lumped-mass representation of a rotor blade, including up to 25 masses. The elastic properties are represented by elastic, massless rods connecting the masses. The airloads are evaluated on a relatively coarse radial and azimuthal grid from which dense airload distributions can be generated by interpolation and harmonic analysis.

Although C-60 has provisions for a trailed vortex sheet, satisfactory airloads have been calculated by means of induced velocities from the root and tip vortices only.

Without the limitations of the modal approach of B-65, the C-60 analysis can evaluate the motions and deflections of a rotor blade in whatever complexity the dynamics and aerodynamics of the problem dictate. Blade and control loads can be then defined and analyzed in detail with the harmonic content.

C-60 output consists of airload and internal load distributions across the blades at 24 azimuthal locations. It also includes pitch link and hub loads. Ten harmonics of the blade can be and were modeled, in order to obtain the highest definition of the above distributions. The accuracy of this code is reflected in Figure 4-2.

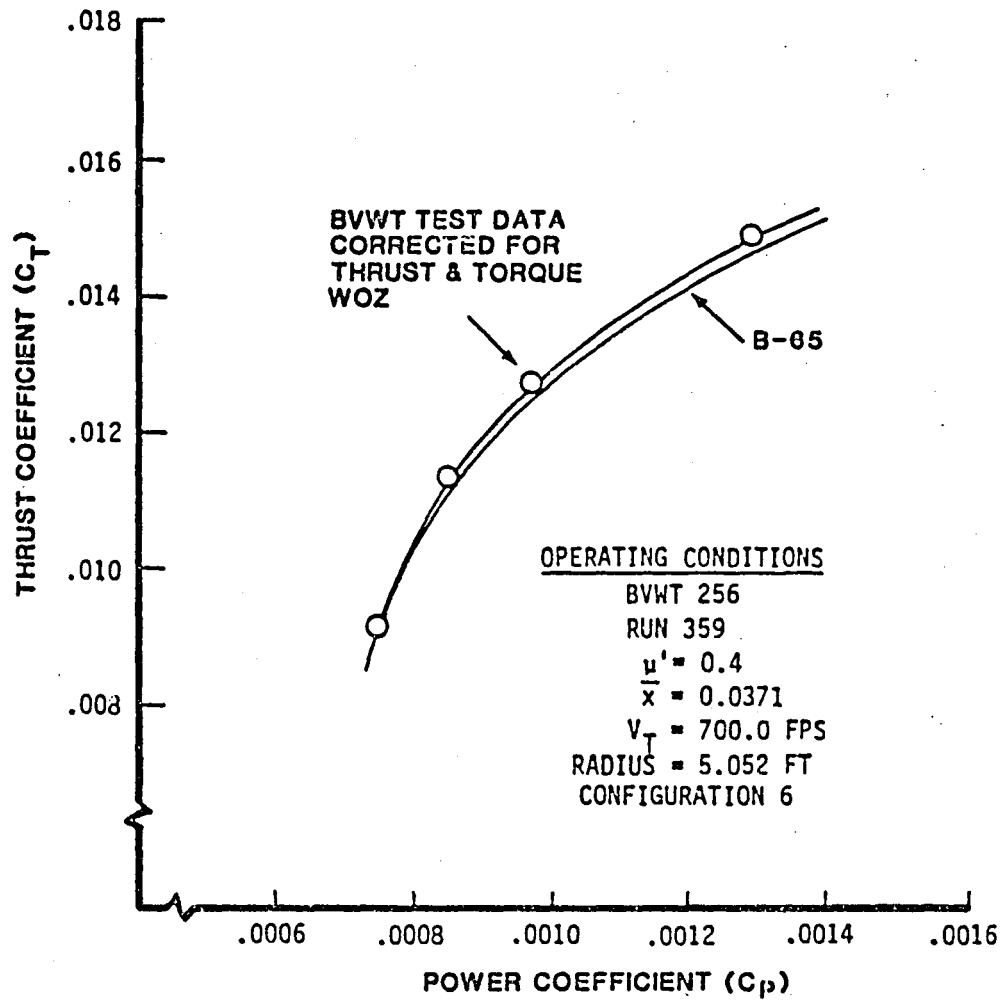


Figure 4-1. Comparison of Measured and Calculated Rotor Performance

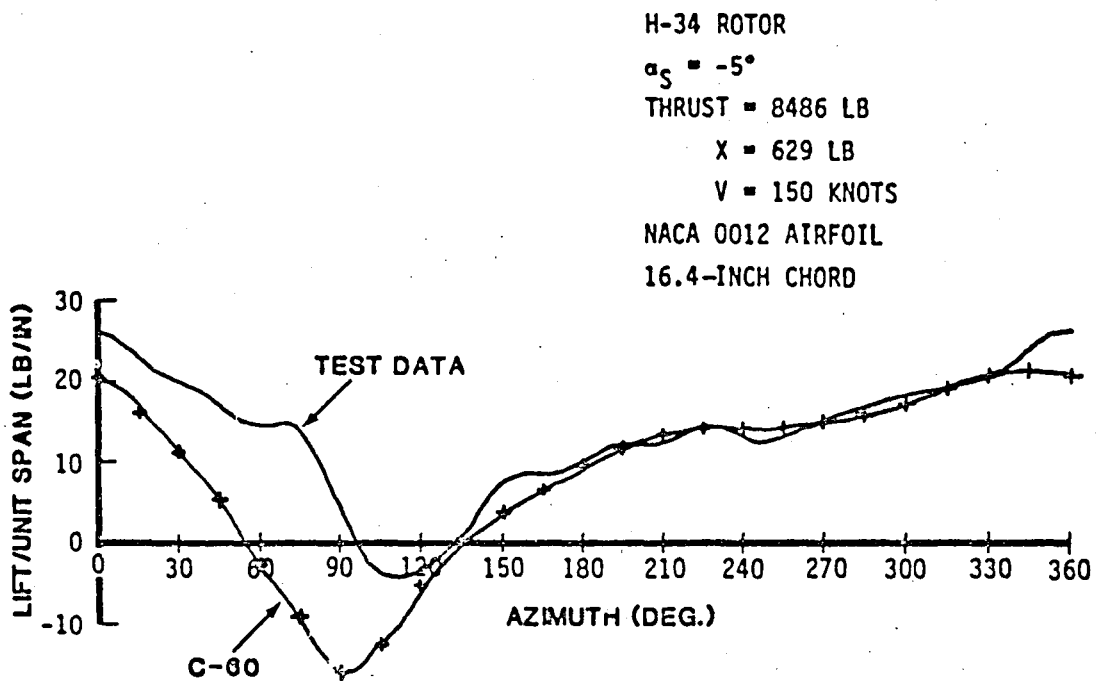


Figure 4-2. Comparison of Measured and Calculated Lift per Unit Span

4.3 The B-21 Rotor/Wake/Fuselage Interaction Processor

The B-21 Rotor/Wake/Fuselage Interaction Code was developed at Boeing Vertol. This code carries out all interface calculations necessary to couple a 3-D potential flow analysis, in particular TEA-230, with a rotor performance or loads analysis.

B-21 takes the flapping angle Fourier coefficients from B-65 output plus the rotor geometry and finds from these the coordinates in the fuselage coordinate system of all blade computational points at all azimuths. These computational points are output from B-21 in exactly the format required for off-body velocity computation by TEA-230. They are then simply merged with the on-body geometry of TEA-230 input. The off-body velocities as they appear in TEA-230 output then serve as another B-21 input without manipulation.

4.4 The TEA-230 Potential Flow Analysis

The three-dimensional potential flow analysis, TEA-230 (Boeing/Seattle), can simulate lifting and non-lifting bodies and engine flow. The code has provisions for on-body and off-body velocity calculations. To obtain a 3-D potential flow solution the surfaces of the body are approximated, as mentioned in Section 3, by a number of flat, or nearly flat surfaces (panels). A potential flow solution on the surface of a given body is then obtained by prescribing, among other conditions, the requirement that there be no flow through the panels. Local velocities and therefore pressures are then estimated at the centroid of each panel and at any required point off the body.

The TEA-230 analysis used in this study is described in detail in Reference 3.

5.0 DESCRIPTION OF RSRA CONFIGURATION AND FLIGHT CONDITIONS

A potential flow model of the RSRA fuselage was defined with provisions to combine the following components:

- A. The body of the fuselage, including the tail boom, but no tail surfaces.
- B. Wings and wing/fuselage fairing areas.
- C. Engines providing auxiliary propulsion.
- D. An approximate model of separated regions behind the fuselage and engines.

The individual and combined elements of the potential flow model were processed through diagnostic programs to verify the quality of the paneling. Computer-generated plots were provided to document the mathematical models.

The fuselage model was only as detailed as necessary to evaluate upwash velocities at the main rotor.

The matrix of operating conditions with and without auxiliary lift, and with and without auxiliary propulsion, were defined. The fuselage and rotor configurations were limited to:

- A. The basic fuselage.
- B. The basic fuselage with one set of wings.
- C. The basic fuselage with auxiliary propulsion.
- D. The basic fuselage with wings and auxiliary propulsion.
- E. Three rotor diameters at one hub position.

Fuselage upwash and rotor performance calculations were carried out for three rotor diameters, three gross weight levels, two auxiliary lift levels, four auxiliary propulsion levels, and combinations of both auxiliary lift and propulsion. All three rotors were set at the same height above the fuselage and, for the purposes of the current study, this height was not varied from the current RSRA configuration since such variation would require redesign of the RSRA.

A summary of the computation conditions is presented in Table I. The relationships of the parameters defining the flight conditions to the gross weights and flight velocities selected are shown in Table II, along with identification of the effects illustrated by various comparisons among the flight conditions. Table II is read in the following way: The numbers labeled "CONDITION" refer to the 27 flight conditions. The numbers opposite the key parameters GW, T, etc., refer to specific values; e.g., "1" in the row opposite "GW" means the gross weight is GW₁ (flight conditions 1, 2, 5, 6, etc.). The "2" in the

row opposite "T" means the vertical component of rotor thrust is T_2 (flight conditions 3, 4, 5, 6, etc.). These key parameter values are defined in Table II.

The conditions shown in Table I were based on the relationships shown in Table II plus both the necessity of not letting the thrusts, gross weights, and velocities be unrealistic for the RSRA, and the desirability of not letting the different values of those same parameters be too close together, thus making the effects of the differences difficult to detect. These conflicting requirements left little room for arbitrariness in the choices of computational conditions.

TABLE I

RSRA UPWASH STUDY FLIGHT CONDITIONS

| <u>CONDITION</u> | <u>GROSS WEIGHT (POUNDS)</u> | <u>VERTICAL COMPONENT OF ROTOR THRUST (POUNDS)</u> | <u>FLIGHT VELOCITY (KNOTS)</u> | <u>WING LIFT (POUNDS)</u> | <u>AUXILIARY THRUST (POUNDS)</u> | <u>ROTOR DIAMETER (FEET)</u> |
|------------------|------------------------------|--|--------------------------------|---------------------------|----------------------------------|------------------------------|
| 1 | 26,400 | 26,400 | 112.5 | 0 | 0 | 60 |
| 2 | 26,400 | 26,400 | 162.5 | 0 | 0 | 60 |
| 3 | 18,333.3 | 18,333.3 | 112.5 | 0 | 0 | 60 |
| 4 | 18,333.3 | 18,333.3 | 162.5 | 0 | 0 | 60 |
| 5 | 26,400 | 18,333.3 | 112.5 | 8,066.7 | 0 | 60 |
| 6 | 26,400 | 18,333.3 | 162.5 | 8,066.7 | 0 | 60 |
| 7 | 18,333.3 | 18,333.3 | 112.5 | 0 | 983 | 60 |
| 8 | 18,333.3 | 18,333.3 | 162.5 | 0 | 2,051 | 60 |
| 9 | 26,400 | 18,333.3 | 112.5 | 8,066.7 | 983 | 60 |
| 10 | 26,400 | 18,333.3 | 162.5 | 8,066.7 | 2,051 | 60 |
| 11 | 18,333.3 | 18,333.3 | 112.5 | 0 | 0 | 50 |
| 12 | 18,333.3 | 18,333.3 | 162.5 | 0 | 0 | 50 |
| 13 | 18,333.3 | 18,333.3 | 112.5 | 0 | 983 | 50 |
| 14 | 18,333.3 | 18,333.3 | 162.5 | 0 | 2,051 | 50 |
| 15 | 26,400 | 18,333.3 | 112.5 | 8,066.7 | 0 | 50 |
| 16 | 26,400 | 18,333.3 | 162.5 | 8,066.7 | 0 | 50 |
| 17 | 26,400 | 18,333.3 | 112.5 | 8,066.7 | 983 | 50 |
| 18 | 26,400 | 18,333.3 | 162.5 | 8,066.7 | 2,051 | 50 |
| 19 | 22,366.7 | 22,366.7 | 162.5 | 0 | 0 | 60 |
| 20 | 22,366.7 | 18,333.3 | 162.5 | 4,033.3 | 0 | 60 |
| 21 | 22,366.7 | 18,333.3 | 162.5 | 4,033.3 | 2,051 | 60 |
| 22 | 18,333.3 | 18,333.3 | 162.5 | 0 | 1,025.5 | 60 |
| 23 | 22,366.7 | 18,333.3 | 162.5 | 4,033.3 | 1,025.5 | 60 |
| 24 | 22,366.7 | 22,366.7 | 162.5 | 0 | 0 | 55.2 |
| 25 | 26,400 | 26,400 | 137.5 | 0 | 0 | 60 |
| 26 | 26,400 | 18,333.3 | 137.5 | 8,066.7 | 0 | 60 |
| 27 | 18,333.3 | 18,333.3 | 137.5 | 0 | 1,468.5 | 60 |

TABLE II. RSRA UPWASH STUDY

DEFINITION OF KEY PARAMETER VARIATION

$$GW_1 = T_1; GW_2 = T_2; GW_3 = \frac{GW_1 + GW_2}{2}; GW_1 > GW_2$$

$$V_2 > V_1 \quad V_3 = (V_1 + V_2)/2$$

$$L_1 = GW_1 - T_2; L_2 = L_1/2 = GW_3 - T_2$$

$$D_2 = D_1 \sqrt{\frac{GW_2}{GW_1}}; \quad D_3 = D_1 \sqrt{\frac{GW_3}{GW_1}}$$

$$P_1 = f_0 q_1, P_2 = f_0 q_2, P_3 = \frac{f_0 q_2}{2}, P_4 = f_0 q_3$$

| CONDITION VARIABLE | LARGE DIAMETER | | | | | | | | | | SMALL DIAMETER | | | | | | | | LINEARITY CHECK | | | | | | | | |
|-------------------------|--|---|---|---|---|---|---|---|---|----|----------------|----|----|----|----|----|----|----|-----------------|----|----|----|----|----|----|----|----|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 |
| GW | 1 | 1 | 2 | 2 | 1 | 1 | 2 | 2 | 1 | 1 | 2 | 2 | 2 | 2 | 1 | 1 | 1 | 1 | 3 | 3 | 3 | 2 | 3 | 3 | 1 | 1 | 2 |
| T | 1 | 1 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 3 | 2 | 2 | 2 | 2 | 3 | 1 | 2 | 2 | |
| V | 1 | 2 | 1 | 2 | 1 | 2 | 1 | 2 | 1 | 2 | 1 | 2 | 1 | 2 | 1 | 2 | 1 | 2 | 2 | 2 | 2 | 2 | 2 | 3 | 3 | 3 | |
| L | - | - | - | - | 1 | 1 | - | - | 1 | 1 | - | - | - | - | 1 | 1 | 1 | 1 | - | 2 | 2 | - | 2 | - | - | 1 | - |
| P | - | - | - | - | - | - | 1 | 2 | 1 | 2 | - | - | 1 | 2 | - | - | 1 | 2 | - | - | 2 | 3 | 3 | - | - | - | 4 |
| DIA | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 1 | 1 | 1 | 1 | 1 | 3 | 1 | 1 | 1 |
| EFFECT OF VELOCITY | [Diagram showing velocity effect with circles and lines] | | | | | | | | | | | | | | | | | | | | | | | | | | |
| EFFECT OF DISK LOAD | [Diagram showing disk load effect with circles and lines] | | | | | | | | | | | | | | | | | | | | | | | | | | |
| EFFECT OF WING LIFT | [Diagram showing wing lift effect with circles and lines, includes 'X=0'] | | | | | | | | | | | | | | | | | | | | | | | | | | |
| EFFECT OF PROP FORCE | [Diagram showing prop force effect with circles and lines, includes 'WITH LIFT'] | | | | | | | | | | | | | | | | | | | | | | | | | | |
| EFFECT OF LIFT & PROP F | [Diagram showing lift & prop force effect with circles and lines] | | | | | | | | | | | | | | | | | | | | | | | | | | |
| EFFECT OF DIAMETER | [Diagram showing diameter effect with circles and lines, includes 'DISK LOAD = CONST', 'GW = CONST', 'GW = CONST & X = 0', 'GW&L = CONST', 'GW&L = CONST & X = 0'] | | | | | | | | | | | | | | | | | | | | | | | | | | |

TABLE III
VALUES OF KEY PARAMETERS

| | | | |
|--------|---|----------|--------|
| GW_1 | = | 26,400 | pounds |
| GW_2 | = | 18,333.3 | pounds |
| GW_3 | = | 22,366.7 | pounds |
| T_1 | = | 26,400 | pounds |
| T_2 | = | 18,333.3 | pounds |
| T_3 | = | 22,366.7 | pounds |
| V_1 | = | 112.5 | knots |
| V_2 | = | 162.5 | knots |
| V_3 | = | 137.5 | knots |
| L_1 | = | 8,066.7 | pounds |
| L_2 | = | 4,033.3 | pounds |
| D_1 | = | 60 | feet |
| D_2 | = | 50 | feet |
| D_3 | = | 55.2 | feet |
| P_1 | = | 983 | pounds |
| P_2 | = | 2,051 | pounds |
| P_3 | = | 1,025.5 | pounds |
| P_4 | = | 1,468.5 | pounds |

6.0 POTENTIAL FLOW MODELS OF THE RSRA

There were four significantly different potential flow models used in this study: the RSRA fuselage (Figures 6-1 and 6-2), the fuselage with auxiliary propulsion engines (Figures 6-3 and 6-4), the fuselage with auxiliary wings (Figures 6-5 and 6-6), and the fuselage with both auxiliary wings and auxiliary engines (Figures 6-7 and 6-8). Two more combinations of fuselage and auxiliary wings, one with and one without auxiliary engines, were used. The wings of these were at different incidence angles. They strongly resembled the combinations in Figures 6-5 and 6-7.

In all of these models the tail surfaces and engine supports were omitted. The cylindrical tube behind each truncated fuselage is used to represent, in rough approximation, the aft fuselage, fuselage boundary layer, and fuselage wake. The cylindrical tubes behind the engines are used to approximate the exhaust jets.

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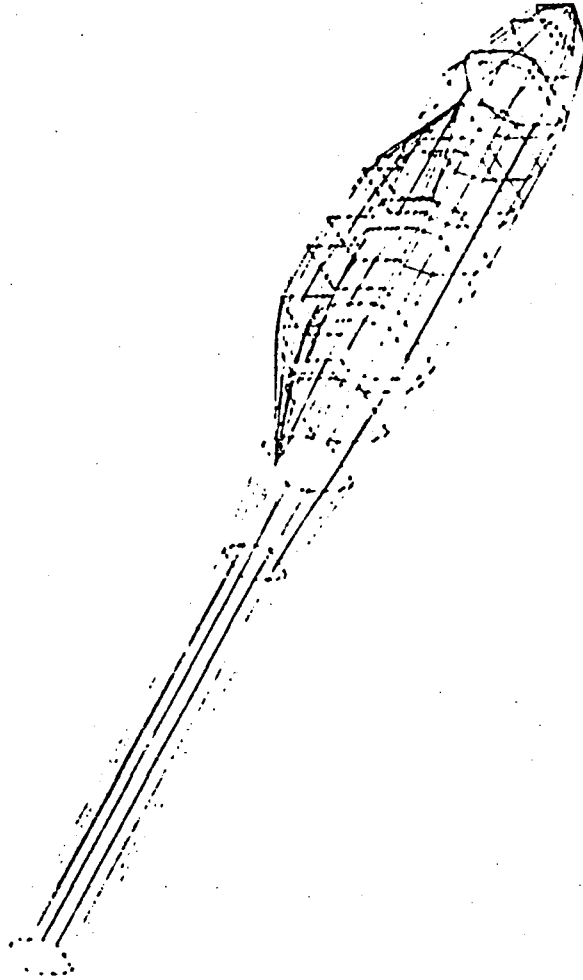


Figure 6-1. Potential Flow Model of the RSRA Fuselage.

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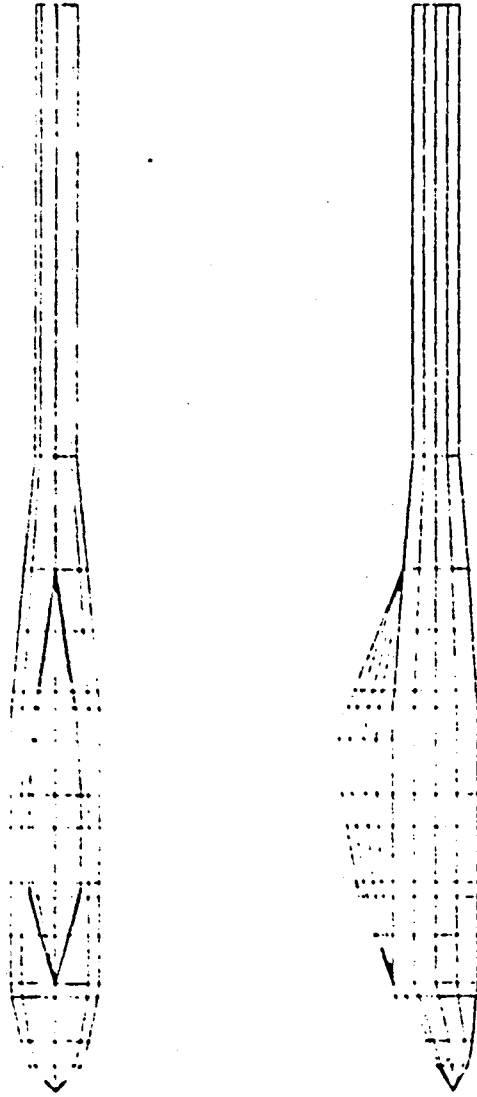


Figure 6-2. Potential Flow Model of the RSRA Fuselage. Top and Side Views.

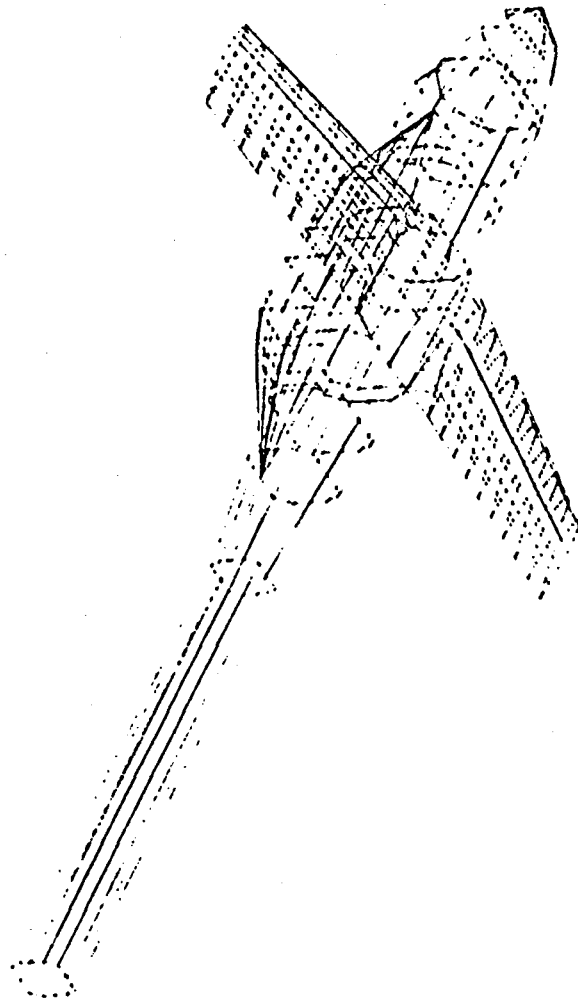
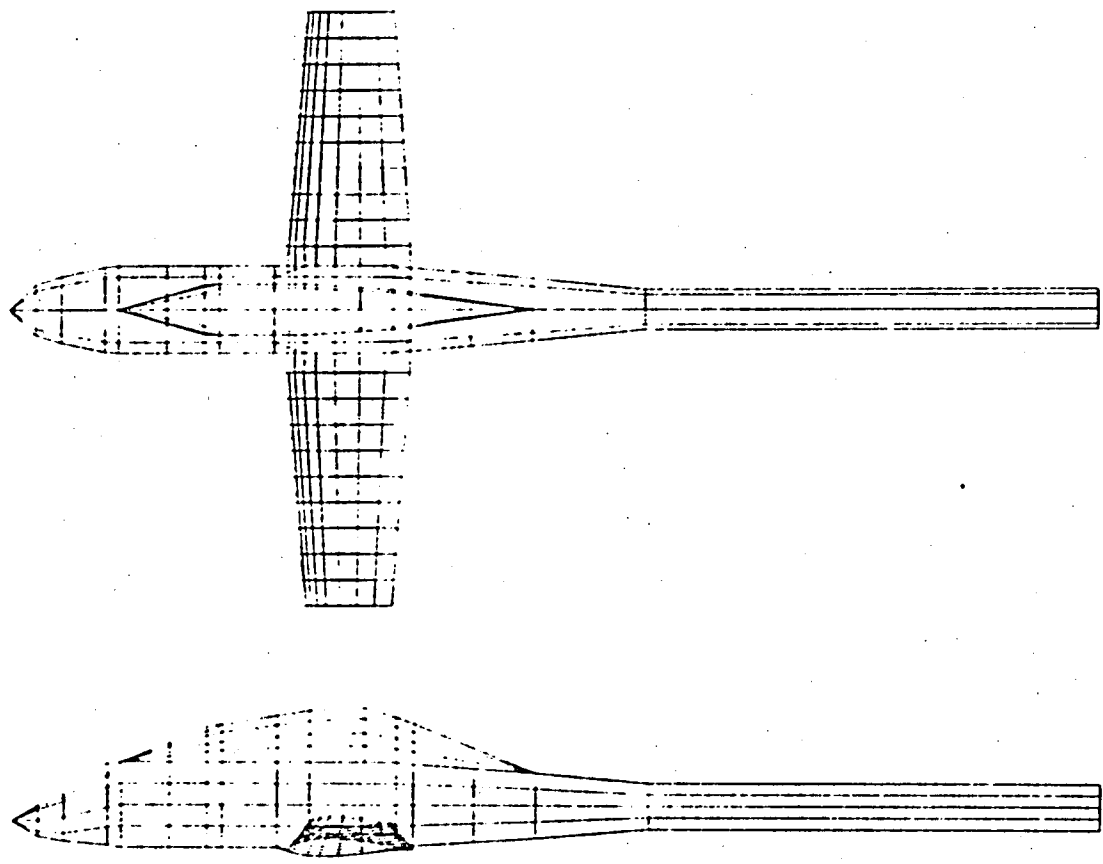


Figure 6-3. Potential Flow Model of the RSRA Fuselage with Auxiliary Wings.



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Figure 6-4. Potential Flow Model of the RSRA Fuselage with Auxiliary Wings.
Top and Side Views.

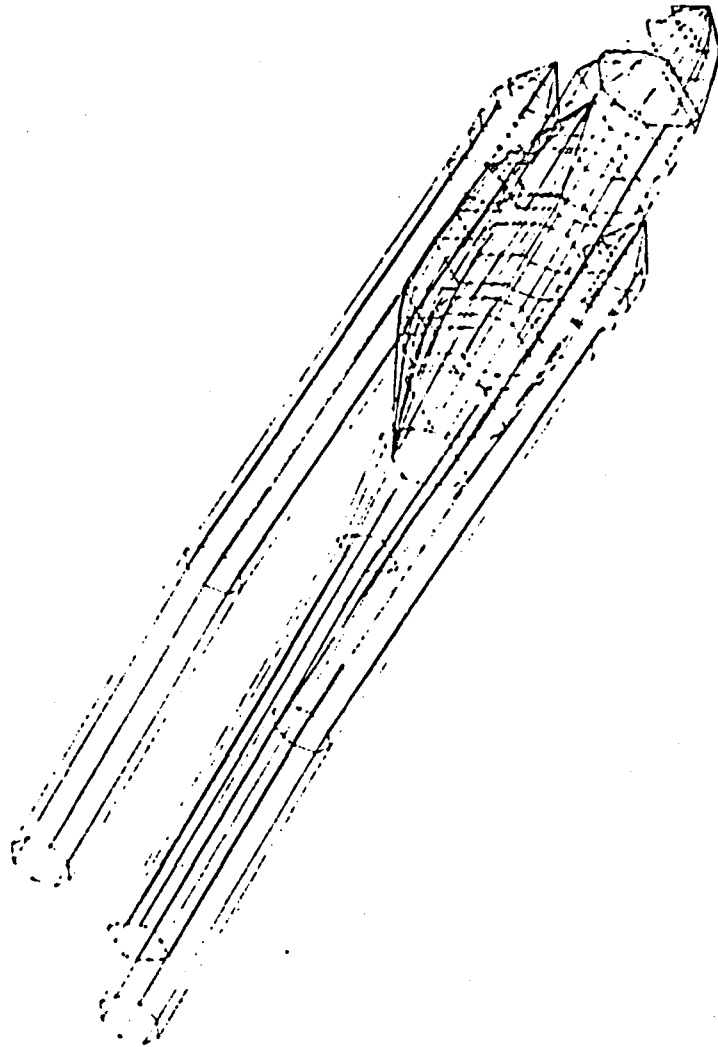


Figure 6-5. Potential Flow Model of the RSRA Fuselage with Auxiliary Engines.

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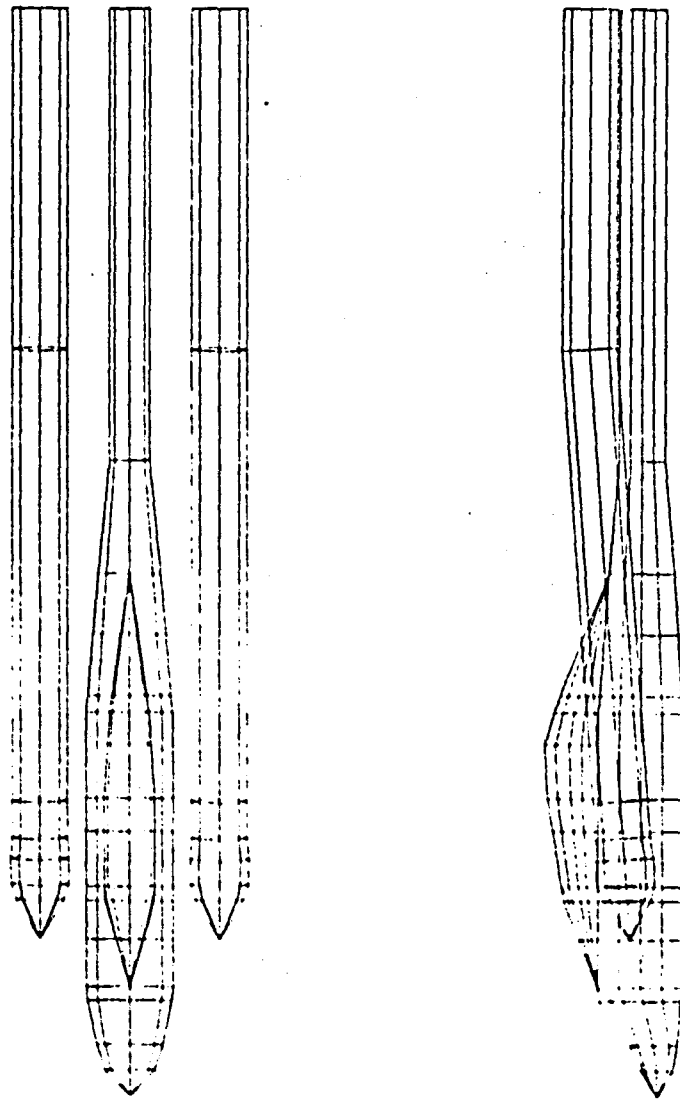


Figure 6-6. Potential Flow Model of the RSRA Fuselage with Auxiliary Engines.
Top and Side Views.

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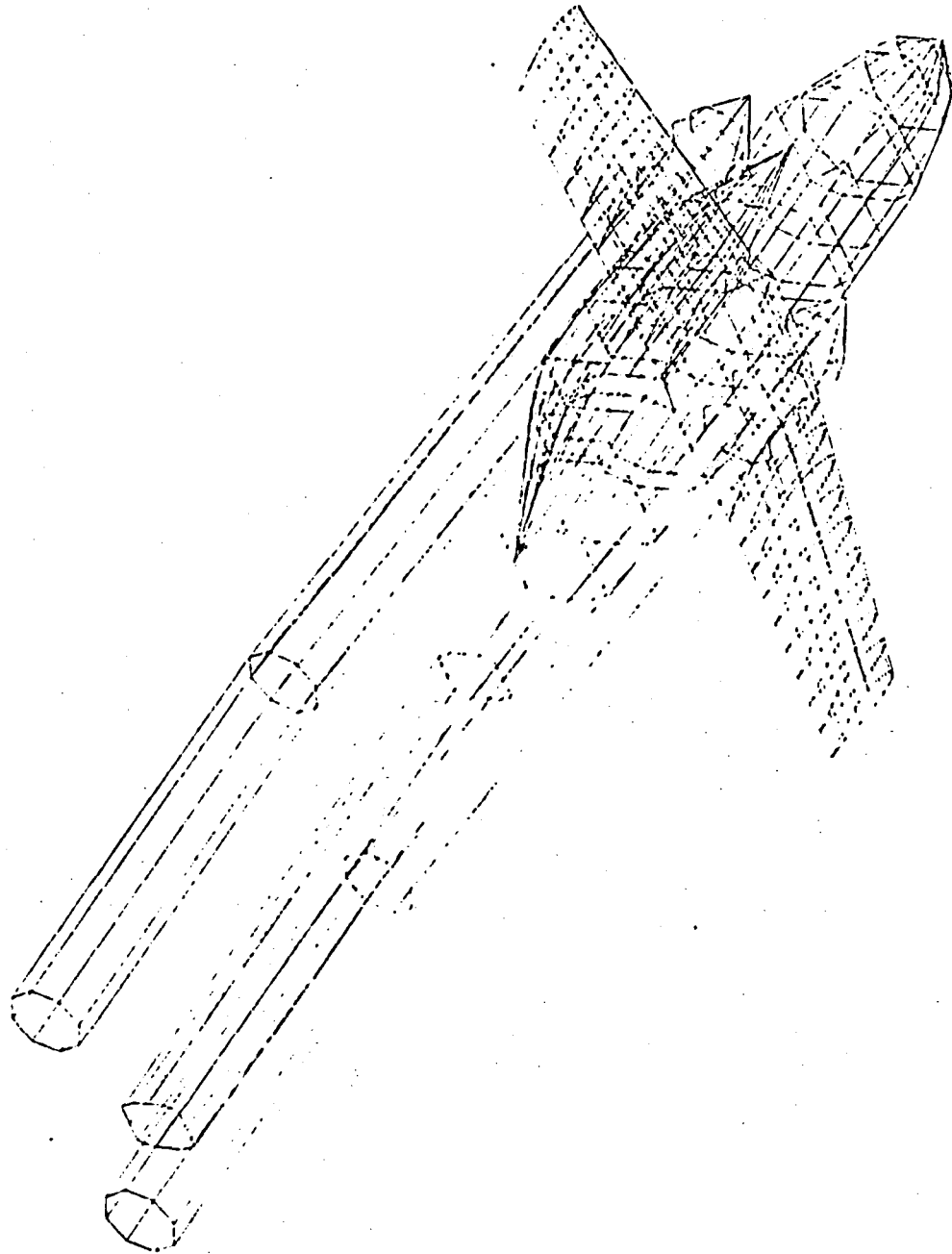


Figure 6-7. Potential Flow Model of Complete RSPA Configuration.

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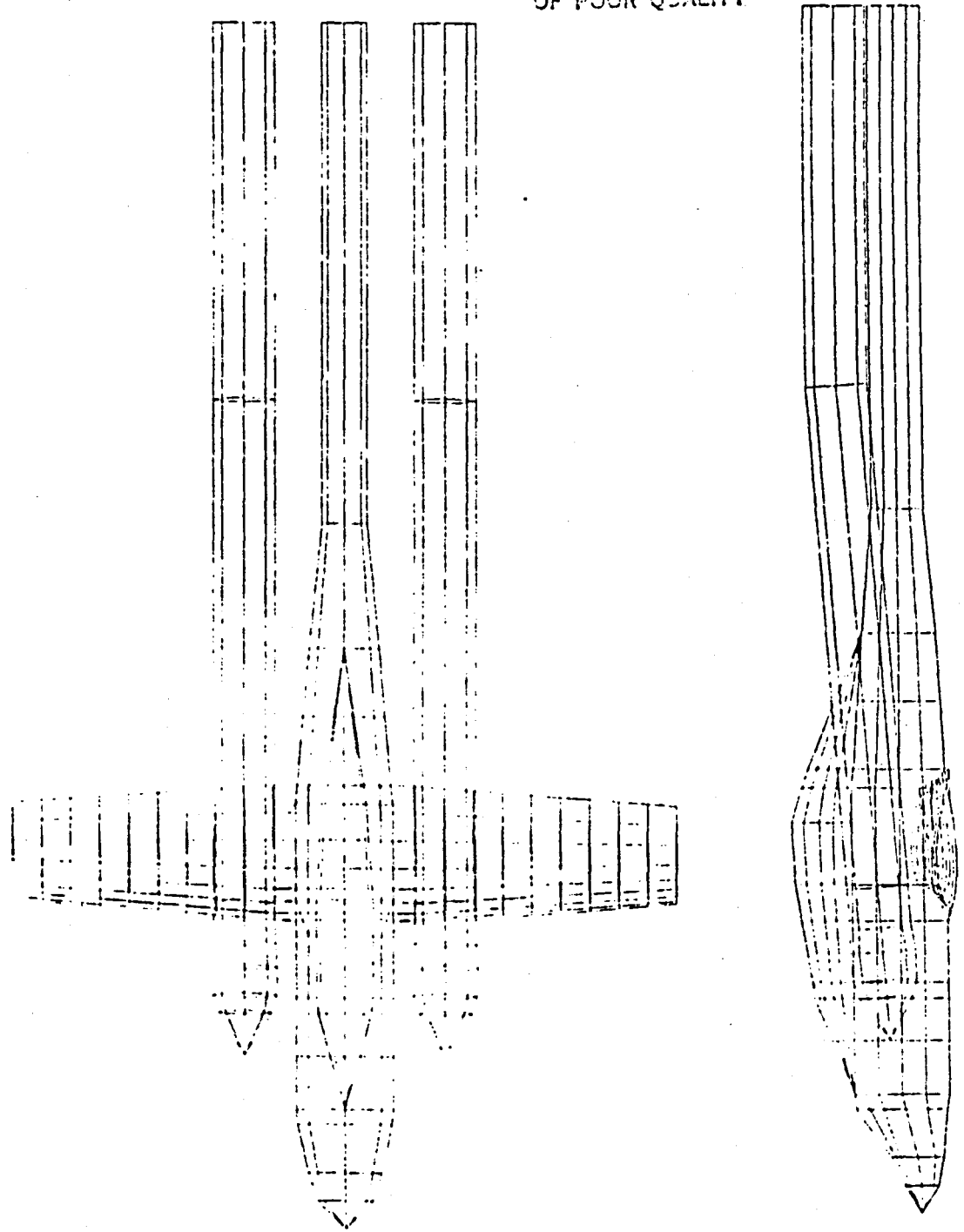


Figure 6-8. Potential Flow Model of Complete RSRA Configuration. Top and Side Views.

7.0 DESCRIPTION OF MAIN ROTOR CHARACTERISTICS

The rotor used in this study is identical to a CH-47D front rotor except that it has four instead of three blades. The radius of this rotor is 30 feet and the chord 32 inches. The airfoil, from the cutout at 21% of the radius to 85% of the radius, is the Boeing Vertol VR-7. At the tip, the airfoil is the VR-8. The airfoil of the last 15% of the blade is a linear transition between these two. The VR-7 is 12% thick, the VR-8 is 8%. The planform of the blade is rectangular. The twist is linear, decreasing 7.63° between the cutout and 85% of the radius and another 0.7° between the 85% point and the tip. For some of the flight conditions, a 25-foot Mach-scaled version of the same rotor is used, and, for condition 24, a 27.61 foot rotor, also Mach-scaled, as defined in Table II. Mach scaling here means that velocities (and therefore Mach numbers) and densities are conserved as lengths are changed in the scaling process. Therefore, airfoil shapes, disk loadings, twist angles, pressures, thicknesses as fractions of chord, and moduli of elasticity are conserved, but masses, lengths, forces, areas, volumes, and accelerations are not. Masses are proportional to the cube of the rotor radius, while lengths are proportional to the radius itself. Forces, except for weight, which is not scaled correctly, are proportional to the square of the radius. Areas and volumes are proportional to the second and third powers of the radius, while accelerations are inversely proportional to the first power. In particular, the 25-foot radius rotor has a 26.67-inch chord, while the 27.61-foot rotor has a 29.45-inch chord.

8.0 DISCUSSION OF THE EFFECTS OF FUSELAGE/WING/ENGINE UPWASH ON THE PERFORMANCE AND LOADS OF THE RSRA ROTOR

The effects of upwash on performance is shown in Figures 8-1 through 8-5.

Figure 8-1 displays the values of required rotor horsepower determined by B-65 for the 27 flight conditions shown in Table II. To keep from splitting hairs too finely, it was deemed necessary to consider an influence due to fuselage/wing/engine upwash which changed the rotor power by less than 400 horsepower to be questionable. Considering only consequential influences, it appears that for only Flight Conditions 2, 8, 16, and 21 does fuselage/wing/engine upwash increase the required rotor power, while for only Flight Conditions 7, 13, 14, 22, and 23 does the upwash decrease that power. From these observations one can conclude that, at least in general, fuselage/wing/engine upwash increases required rotor power at high flight velocities when the sum of rotor and wing lift is high, while auxiliary engine upwash without wing upwash decreases the required power.

Figure 8-2 displays the values of equivalent lift-to-drag ratio determined by B-65. If one considers here that differences in L/DE of less than 0.6 are not significant, one finds that fuselage/wing/engine upwash significantly increases L/DE for Flight Conditions 7, 13, 14, 22, 23, and 27 and significantly decreases L/DE for Flight Conditions 8 and 21. From these observations one can conclude that, in general, engine upwash can significantly influence L/DE in the presence of little or no wing upwash. One can conclude also that the engine upwash increases L/DE except possibly when auxiliary thrust is high.

In comparing Figures 8-1 and 8-2 and while noting that the only quantity contributing to L/DE which should change due to fuselage/wing/engine upwash is the rotor power, one should expect changes in L/DE due to fuselage/wing/engine upwash to be opposite changes in rotor horsepower. This indeed is the case, except for Flight Conditions 2 and 4, where the changes in power are slight and are offset by the changes in lift and X allowed by the convergence tolerances.

Figure 8-3 displays the vibratory component of the blade tip elastic twist deflection as calculated by B-65. If one decides that differences in $\Delta\theta_{EL}$, less than 0.016 radians are questionable one finds fuselage/wing/engine upwash significantly decreases $\Delta\theta_{EL}$ for Flight Conditions 2, 12, 14, 19, and 27 but never significantly increases $\Delta\theta_{EL}$. It is somewhat difficult to find commonality in these five flight conditions, although they all involve high flight velocities or auxiliary propulsion. None involve wing lift. Most of these conditions involve reasonably high disk loading.

Figure 8-4 displays the normalized magnitudes of the fourth and eighth harmonics of rotor thrust as determined by B-65. If one considers differences in T_4/T_0 less than 0.014 to be insignificant, one finds that fuselage/wing/engine upwash significantly increases T_4/T_0 for Flight Conditions 21 and 22 and significantly decreases it for Flight Conditions 2, 4, 6, 12, 24, and 26. These Flight Conditions are at medium and high flight velocities and usually involve disk loadings that are not high. In particular, the two flight conditions for which fuselage/wing/engine upwash increases T_4/T_0 involve a high flight velocity and reasonably low disk loadings. But these are the only flight conditions among the eight significant ones which involve auxiliary propulsion. The other six flight conditions involve no auxiliary propulsion and experience decreases in T_4/T_0 due to fuselage/wing upwash.

If one uses 0.014 as also the lower limit of significant differences in T_8/T_0 , one finds that fuselage/wing/engine upwash significantly increases T_8/T_0 for Flight Conditions 5, 8, 13, 19, 21, 22, and 23 and significantly decreases it for Flight Conditions 2, 6, 14, 16, 18, 24, and 25. These 14 flight conditions have little in common except that most of them involve the highest flight velocity. Why fuselage/wing/engine upwash increases or decreases T_8/T_0 is not clear at all.

Figure 8-5 displays the normalized magnitudes of the fourth and eighth harmonics of rotor torque as determined by B-65. A comparison of differences in Q_4/Q_0 due to fuselage/wing/upwash show little correlation with the key parameters of the flight conditions or the RSRA potential flow models, except that the largest differences occur at high flight velocity. If one considers differences in Q_8/Q_0 less than 0.022 to be insignificant, one finds that fuselage/wing/engine upwash significantly increases Q_8/Q_0 for Flight Conditions 7, 9, 13, and 17 and significantly decreases it for Flight Condition 22. The flight conditions for which Q_8/Q_0 is significantly increased are all at the lowest flight velocity and all use auxiliary propulsion. Flight condition 22, by contrast, uses the highest flight velocity and, by comparison, also uses auxiliary propulsion. However, other flight conditions using auxiliary propulsion and high flight velocity do not experience significant changes in Q_8/Q_0 due to fuselage/wing/engine upwash.

The effects of upwash on loads is shown in Figures 8-6 through 8-41. In each figure, the solid curve indicates the isolated rotor, the dashed curve the rotor influenced by upwash induced by fuselage and/or auxiliary wings and/or auxiliary engines.

The figures are grouped according to the independent variable and the constant parameters. Figures 8-6 through 8-9 show functions of flight velocity in which the upwash (if any) is caused by only the RSRA fuselage. Figures 8-10 through 8-13 are similar except that the influence of the wings has been added.

Figures 8-14 through 8-17 are like Figures 8-6 through 8-9 except that the influence of the auxiliary engines has been added. Figures 8-18 through 8-21 show functions of disk loading in which the upwash is caused by only the fuselage. Figures 8-22 through 8-25 show functions of wing lift. Figures 8-26 through 8-29 show functions of the flat plate area for the thrust from the auxiliary engines. Figures 8-30 through 8-33 are similar but with wing lift added. Figures 8-34 through 8-37 show functions of auxiliary engine flat plate area and wing lift as both increase together. Finally, Figures 8-38 through 8-41 show functions of rotor size at a constant disk loading. Table IV lists the flight conditions and potential flow models for each of the above groups of figures.

Another grouping can be considered in which the figures of each group display the same dependent, as opposed to independent, variable. Figures 8-6, 8-10, 8-14, 8-18, 8-22, 8-26, 8-30, 8-34, and 8-38 display the variation of equivalent lift-to-drag ratio with several different parameters and at many different flight conditions. Figures 8-7, 8-11, 8-15, 8-19, 8-23, 8-27, 8-31, 8-35, and 8-39 display the variation of pitch link load vibratory amplitude with the same parameters and at the same flight conditions. Figures 8-8, 8-12, 8-16, 8-20, 8-24, 8-28, 8-32, 8-36, and 8-40 display the variation of flap hinge vertical shear vibratory amplitude while Figures 8-9, 8-13, 8-17, 8-21, 8-25, 8-29, 8-33, 8-37, and 8-41 display the variation of FZF, the vertical hub force fourth harmonic amplitude.

It will be most instructive to discuss these figures according to this last grouping, beginning with the equivalent lift-to-drag ratio.

Fuselage upwash alone generally slightly increases L/DE regardless of flight velocity (Figure 8-6) or disk loading (Figure 8-18). Wing plus fuselage upwash slightly decreases L/DE regardless of flight velocity (Figure 8-10), but generally increases it at low values of wing lift (Figure 8-22). There is a significant increase in L/DE due to the upwash of the fuselage and auxiliary engines for all flight velocities (Figure 8-14) and for all values of the flat plate area opposing the auxiliary engines (Figure 8-26). The upwash of fuselage, wing, and auxiliary engines generally increases L/DE despite variation in flat plate area (Figures 8-30 and 8-34) or wing lift (Figure 8-34). There appears to be little effect due to fuselage upwash alone if the rotor size varies but disk loading remains constant (Figure 8-38).

These results are not identical to those determined by B-65. The primary reason for the differences is probably the fact that the C-60 loads analysis performs calculations considerably different from those in the B-65 performance analysis. The differences in these calculations were outlined in Sections 4.1 and 4.2.

TABLE IV

FLIGHT CONDITIONS AND POTENTIAL FLOW MODELS
FOR LOAD ANALYSIS ILLUSTRATED COMPARISONS

| FIGURES | FLIGHT CONDITIONS | | | POTENTIAL FLOW MODEL |
|-------------------|-------------------|----|----|-----------------------------|
| 8-6 through 8-9 | 1 | 2 | 25 | Fuselage only |
| 8-10 through 8-13 | 5 | 6 | 26 | Fuselage and wing |
| 8-14 through 8-13 | 7 | 8 | 27 | Fuselage and engines |
| 8-18 through 8-21 | 2 | 4 | 19 | Fuselage only |
| 8-22 through 8-25 | 4* | 6 | 20 | Fuselage and wing |
| 8-26 through 8-29 | 4* | 8 | 22 | Fuselage and engines |
| 8-30 through 8-33 | 6** | 10 | 23 | Fuselage, wing, and engines |
| 8-34 through 8-37 | 4* | 10 | 23 | Fuselage, wing, and engines |
| 8-38 through 8-41 | 2 | 12 | 24 | Fuselage only |

*Fuselage only

**Fuselage and wing only

In contrast to its effect on L/DE, fuselage upwash alone increases the pitch link load vibratory amplitude significantly at high flight velocities (Figures 8-7 and 8-19). The fuselage and engine upwash together produce the same result if the engines are providing most of the forward thrust (Figures 8-15 and 8-27). The fuselage-plus-wing upwash increases the PLL amplitude at all flight velocities (Figure 8-11), and the addition of the engines does not generally change this result (Figure 8-31). The fuselage-plus-wing upwash alone increases the PLL amplitude at all values of wing lift (Figure 8-23). The addition of engines has the same effect, generally, if the wing lift and engine thrust increase together (Figure 8-35). With the fuselage alone causing upwash, the PLL amplitude increases quickly with rotor size (Figure 8-39).

The effects of upwash on the vertical shear vibratory amplitude at the flap hinge are somewhat similar to the effects on L/DE. The fuselage upwash alone increases the vibratory amplitude at all flight velocities (Figure 8-8), all disk loadings (Figure 8-20), and all rotor sizes (Figure 8-40). The addition of upwash from the wing decreases the amplitude at all flight velocities (Figure 8-12) and all rotor if the wing lift is high, but not otherwise (Figure 8-24). The fuselage-plus-engine upwash generally increases the amplitude at high but not at low velocities (Figure 8-16) and then only when the auxiliary thrust is large (Figure 8-28). The upwash from the complete RSRA configuration generally increases the flap hinge vertical shear vibratory amplitude (Figures 8-32 and 8-36), at least at high values of auxiliary thrust.

The vertical hub force fourth harmonic amplitude (FZF) is decreased by fuselage upwash at high flight velocities (Figure 8-9). When wing upwash is added FZF is increased at all flight velocities (Figure 8-13) but not all values of wing lift (Figure 8-25). The fuselage-plus-engine upwash decreases FZF at all flight velocities (Figure 8-17) and all values of auxiliary thrust (Figure 8-29). The upwash from the fuselage alone decreases FZF for all values of disk loading (Figure 8-21) and for all rotor sizes (Figure 8-41). The upwash from the complete configuration decreases FZF at high values of auxiliary thrust when the wing lift is also high (Figures 8-33 and 8-37).

It should be noted at this point that the flight conditions labeled "LINEARITY CHECK" in Table II show that the results in Figures 8-6 through 8-41 are, in general, highly nonlinear. This nonlinearity is most prominent in the variation of flap hinge vertical shear vibratory amplitude. In fact, the vertical shear vibratory amplitude appears to be lowest at these "LINEARITY CHECK" flight conditions.

Although curve crossings have not been specifically mentioned as such, they appear in most of the figures which display loads analysis results. They are prominent in those figures which involve variations in flat plate equivalent area for auxiliary thrust. Most of these figures which display loads indicate that, in general, loads are decreased by fuselage/wing/engine upwash at low values of f_e , but are increased at high values of f_e .

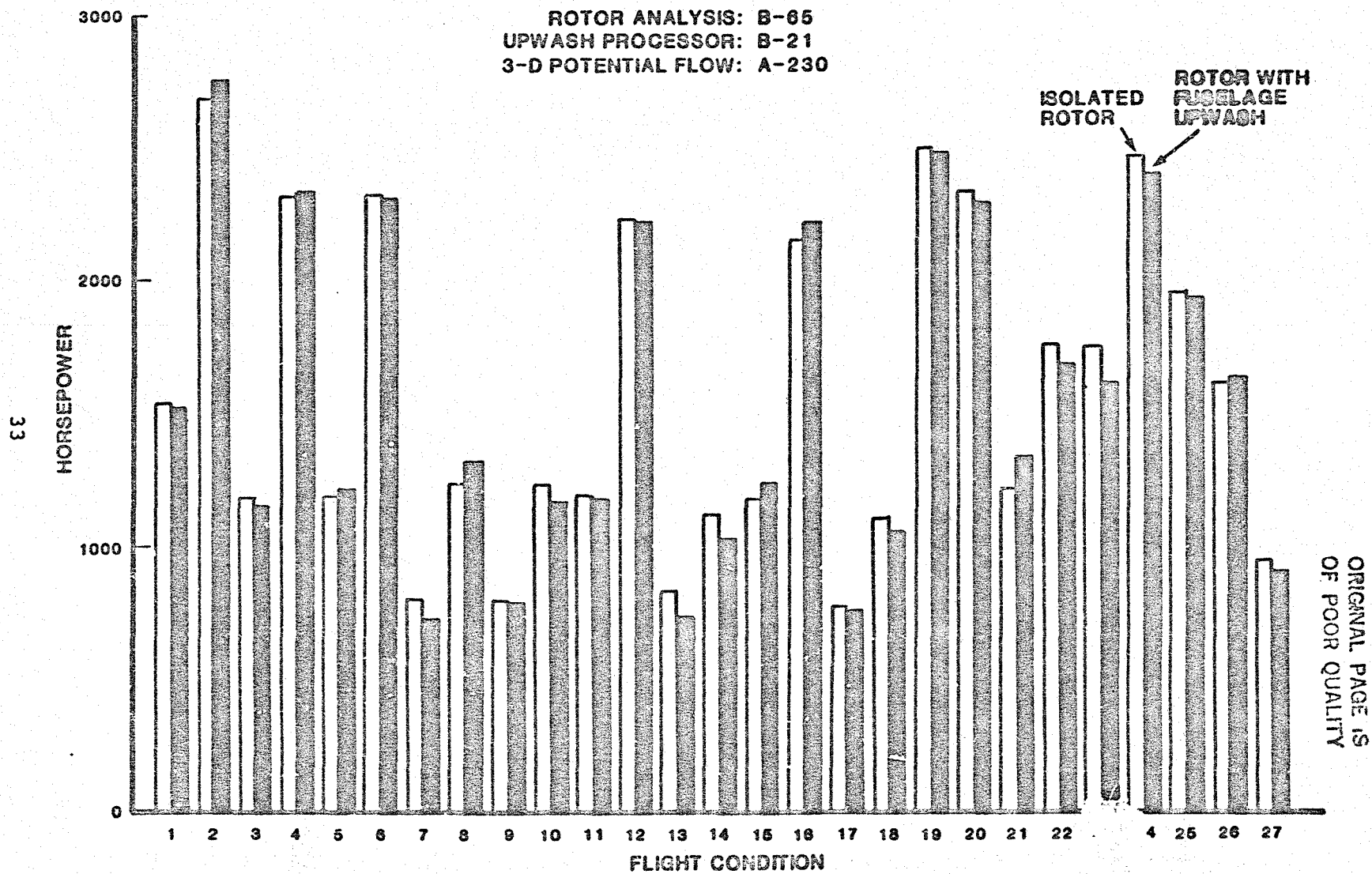


Figure 8-1. Effect of RSRA Upwash on Calculated Rotor Power

ROTOR ANALYSIS: B-85
UPWASH PROCESSOR: B-21
3-D POTENTIAL FLOW: A-230

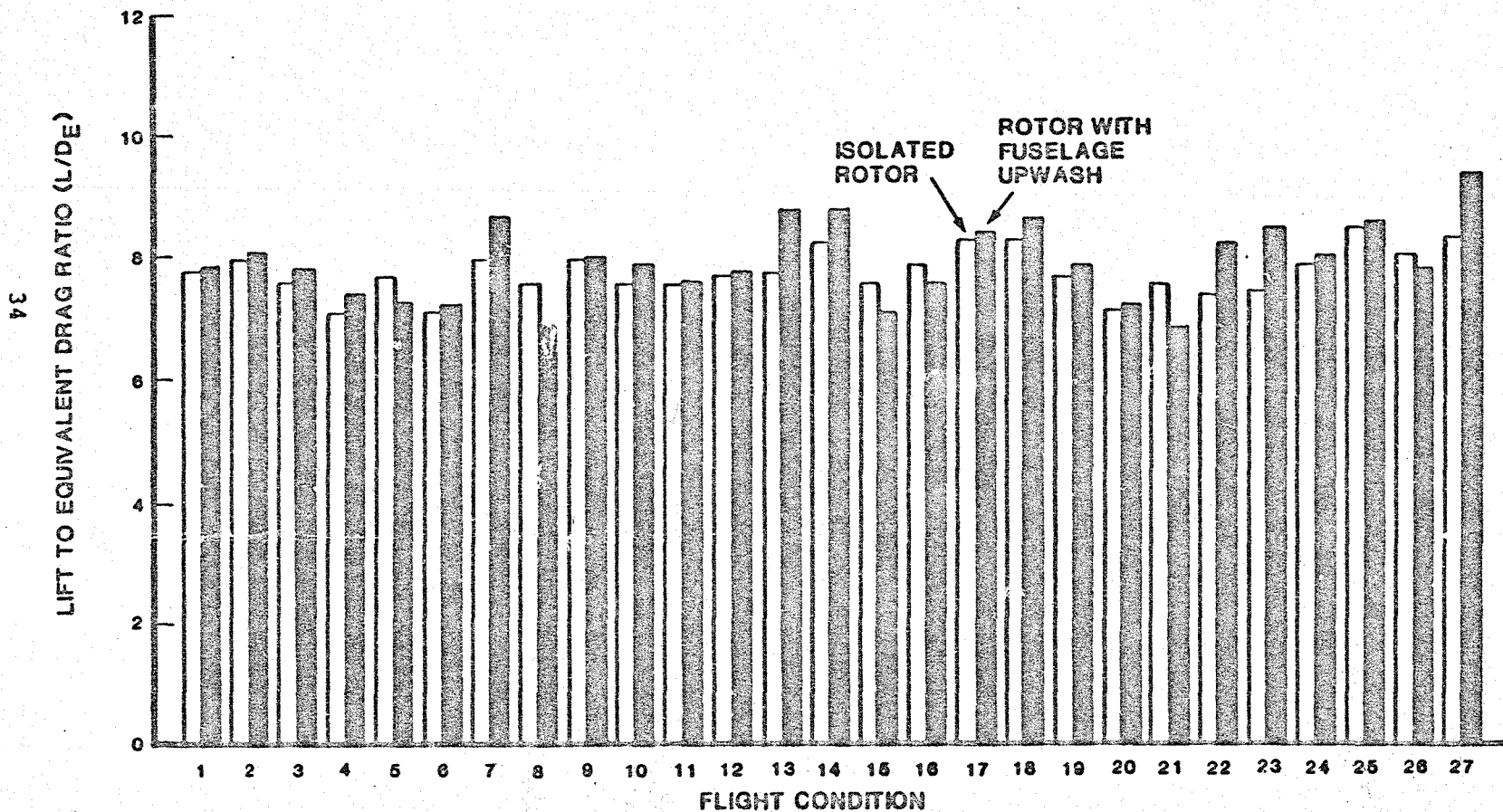


Figure 8-2. Effect of RSRA Upwash on Calculated Equivalent Lift-to-Drag Ratio

ROTOR ANALYSIS : B-65
 UPWASH PROCESSOR: B-21
 3-D POTENTIAL FLOW: A-230

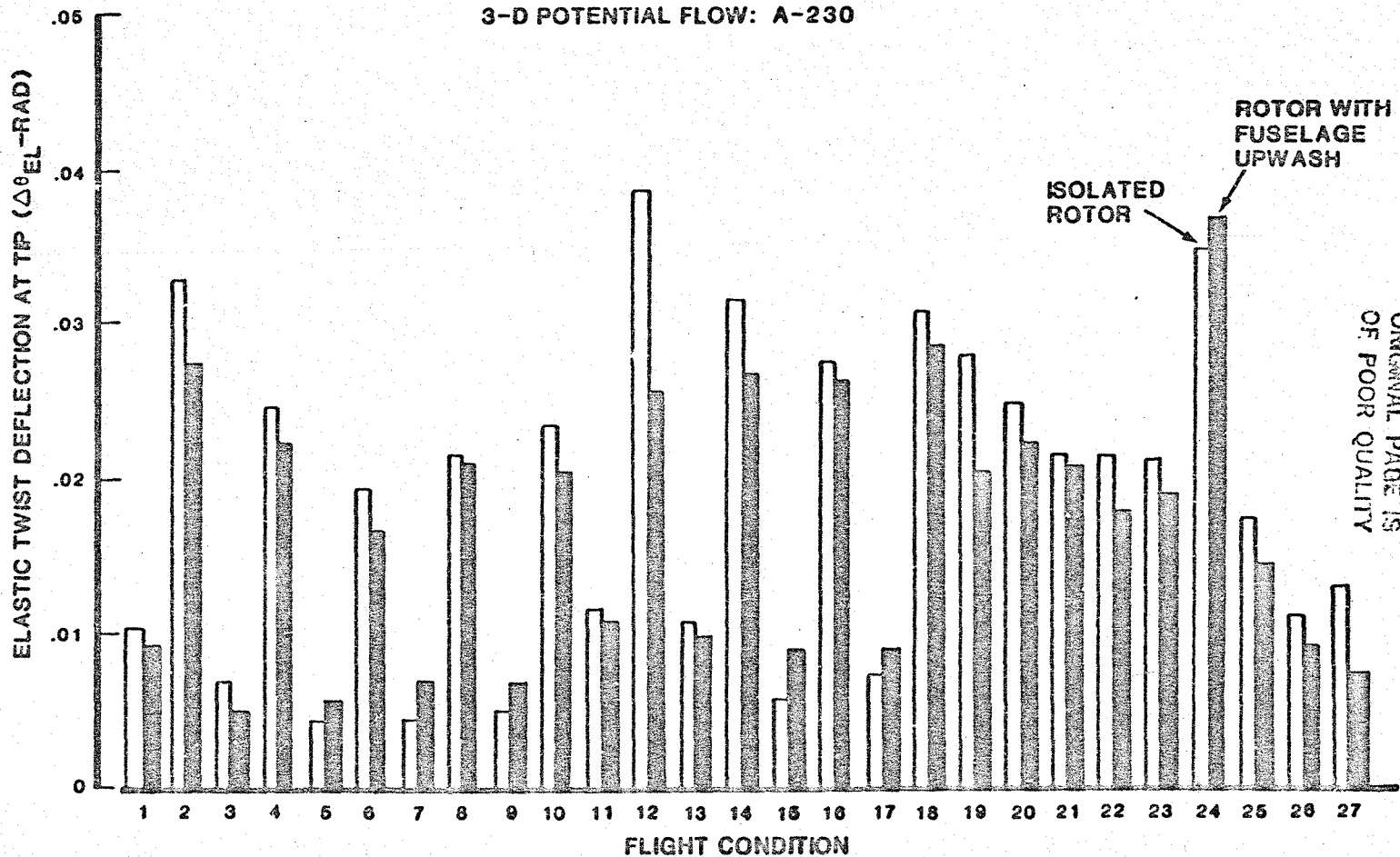


Figure 8-3. Effect of RSRA Upwash on the Calculated Elastic Twist Deflection at the Tip - Vibratory Component

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ROTOR ANALYSIS: B-65
 UPWASH PROCESSOR: B-21
 3-D POTENTIAL FLOW: A-230

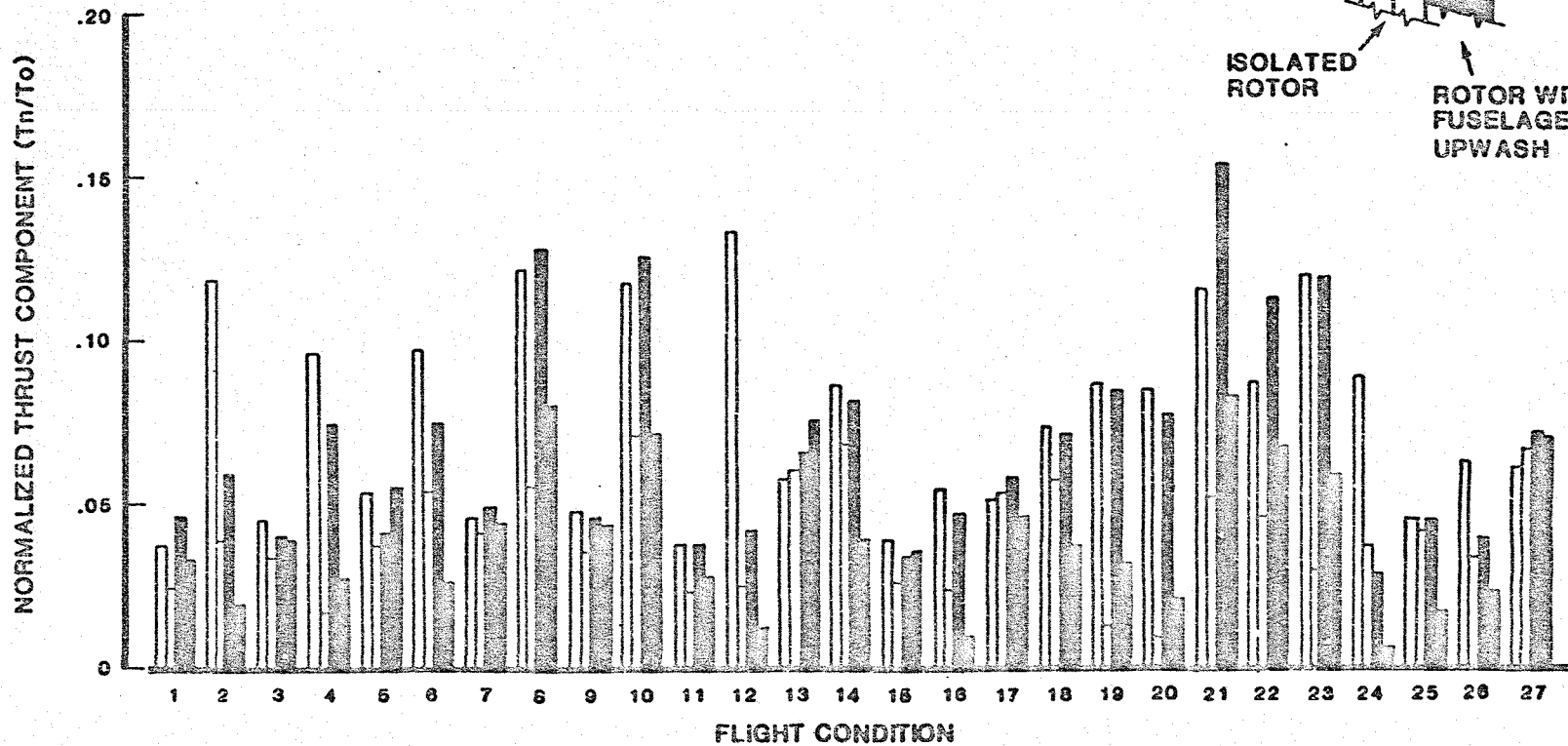
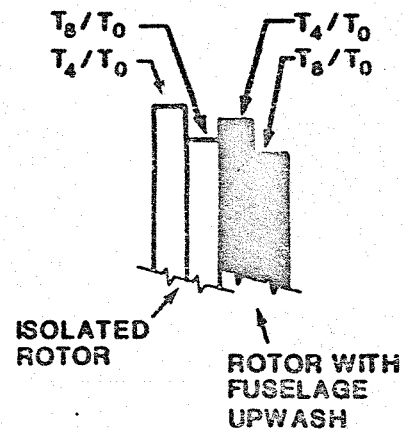


Figure 8-4. Effect of RSRA Upwash on the Calculated Fourth and Eighth Harmonics of Rotor Thrust

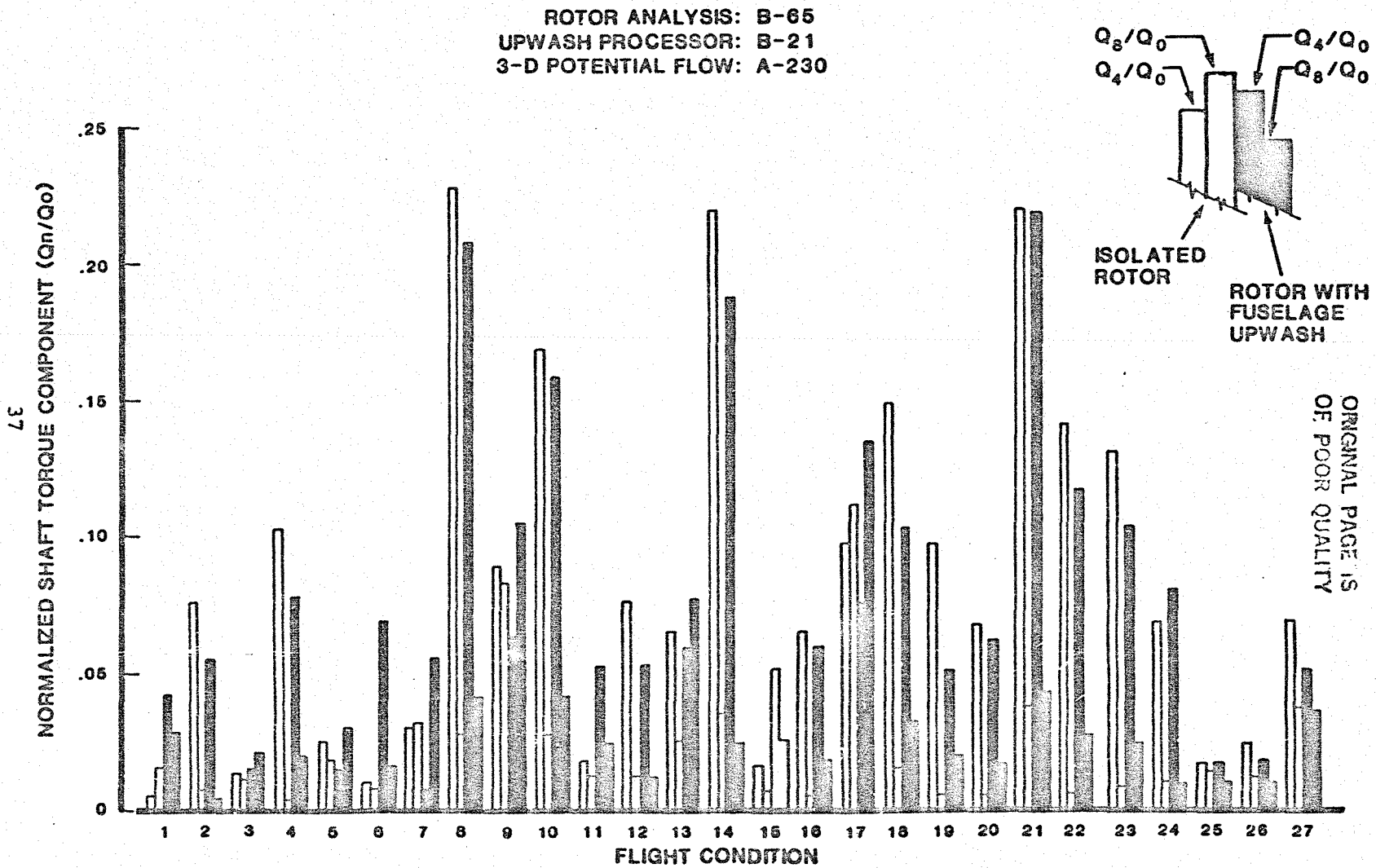


Figure 8-5. Effect of RSRA Upwash on the Calculated Fourth and Eighth Harmonics of Rotor Torque

WITHOUT UPWASH ———
WITH UPWASH - - - -

GROSS WEIGHT = 26,400 LB
ROTOR LIFT = 26,400 LB
ROTOR RADIUS = 30 FT

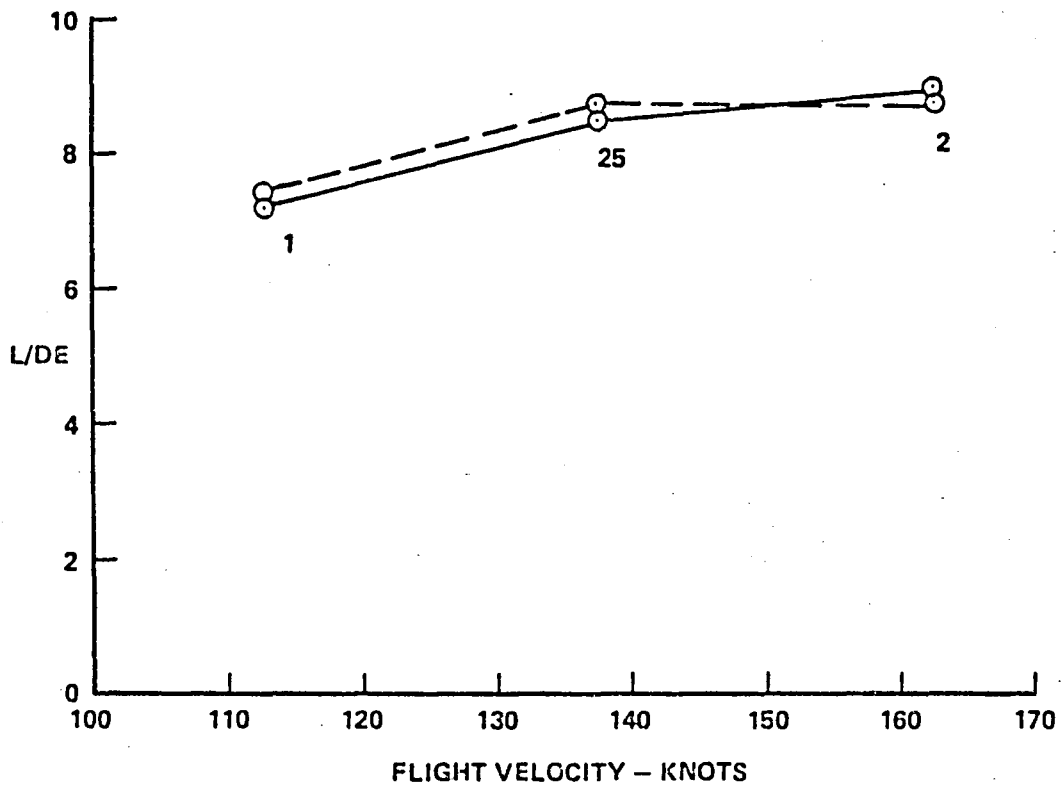


Figure 8-6. Variation of Equivalent Lift-to-Drag Ratio With Flight Velocity From Loads Analysis. Rotor Lift, Gross Weight, and Rotor Radius Are Held Constant. Numerals Near Symbols Indicate Flight Condition.

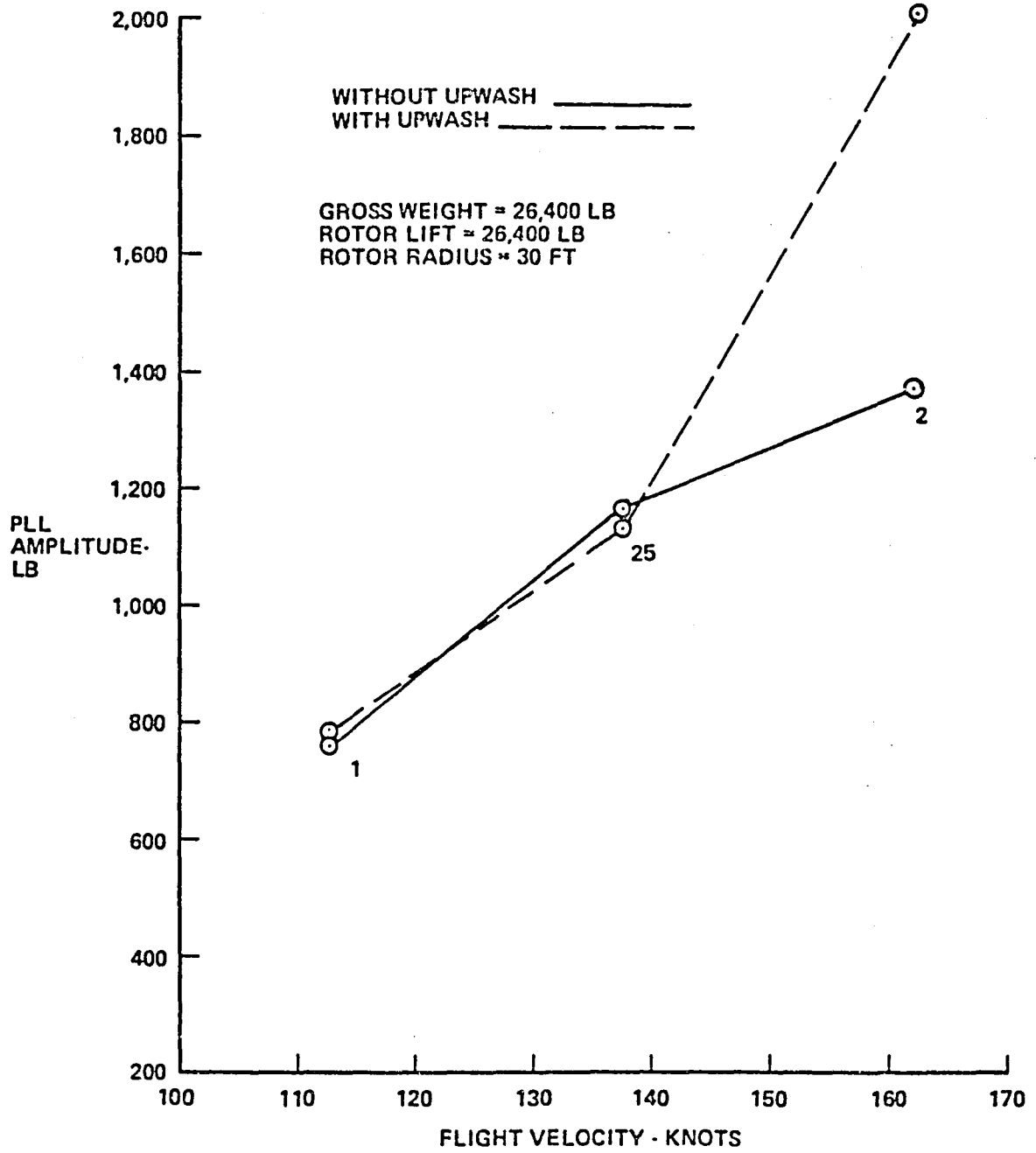


Figure 8-7 Variation of Pitch Link Load Vibratory Amplitude With Flight Velocity From Loads Analysis. Rotor Lift, Gross Weight, and Rotor Radius Are Held Constant. Numerals Near Symbols Indicate Flight Condition.

GROSS WEIGHT = 26,400 LB
ROTOR LIFT = 26,400 LB
ROTOR RADIUS = 30 FT

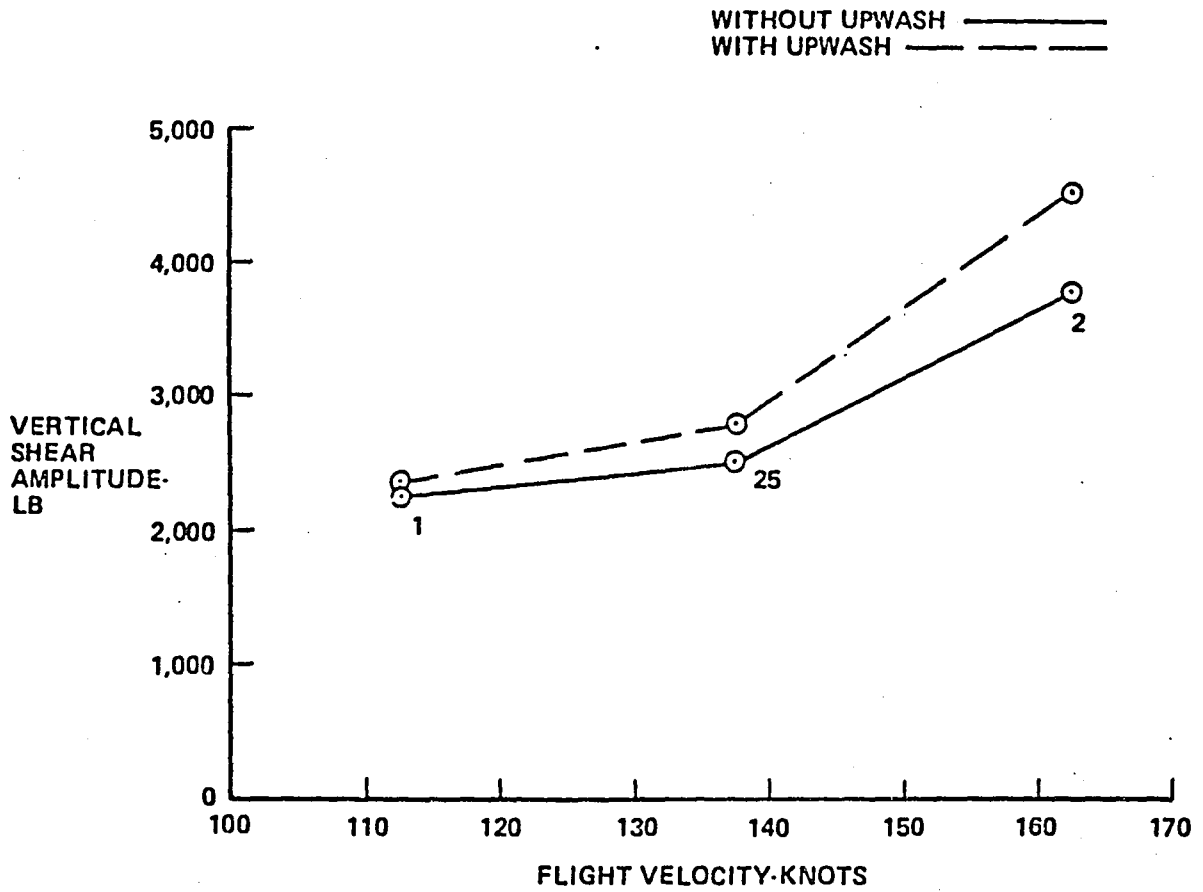


Figure 8-8. Variation of Flap Hinge Vertical Shear Vibratory Amplitude With Flight Velocity From Loads Analysis. Rotor Lift, Gross Weight, and Rotor Radius Are Held Constant. Numerals Near Symbols Indicate Flight Condition.

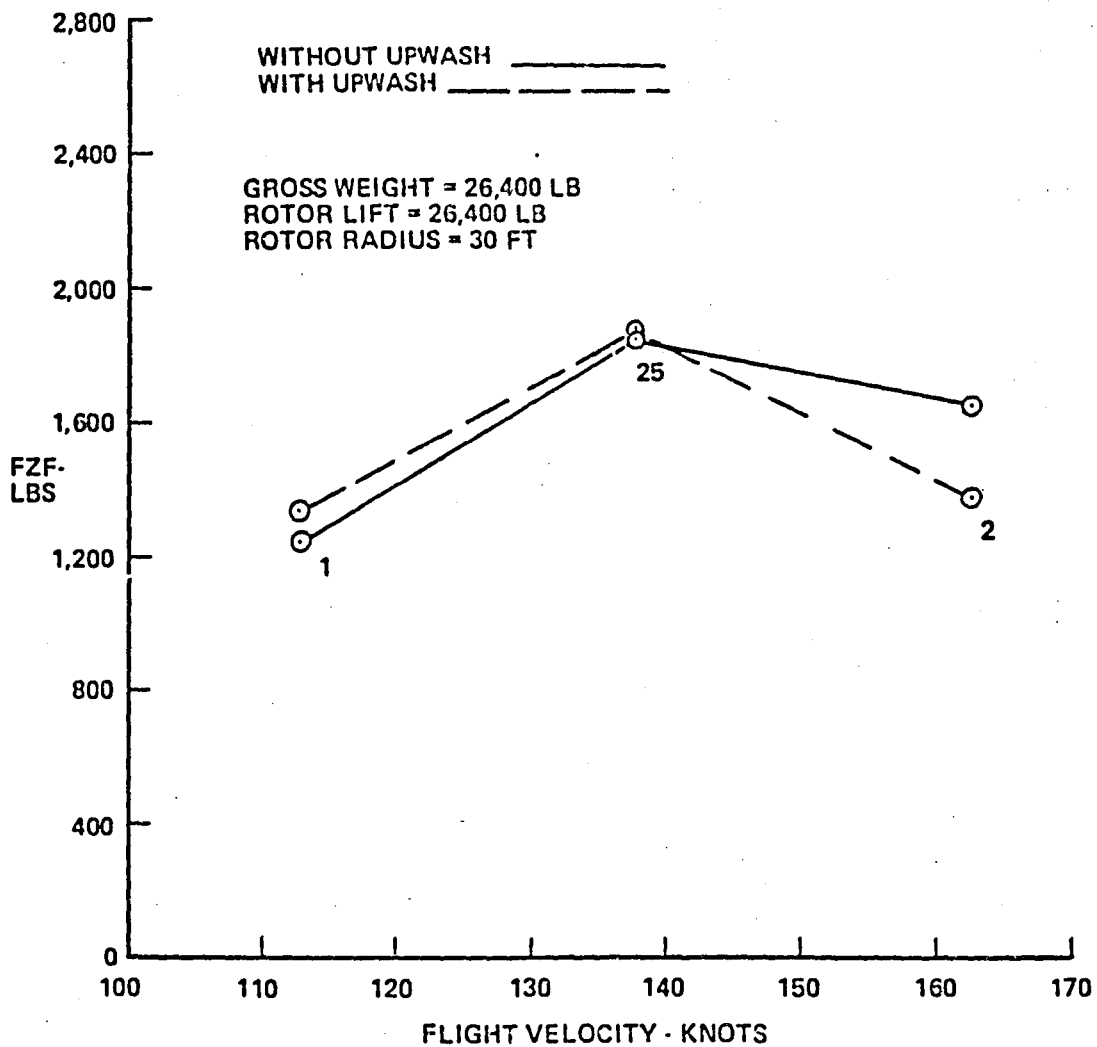


Figure 8-9. Variation of Vertical Hub Force Fourth Harmonic Amplitude With Flight Velocity From Loads Analysis. Rotor Lift, Gross Weight, and Rotor Radius Are Held Constant. Numerals Near Symbols Indicate Flight Condition.

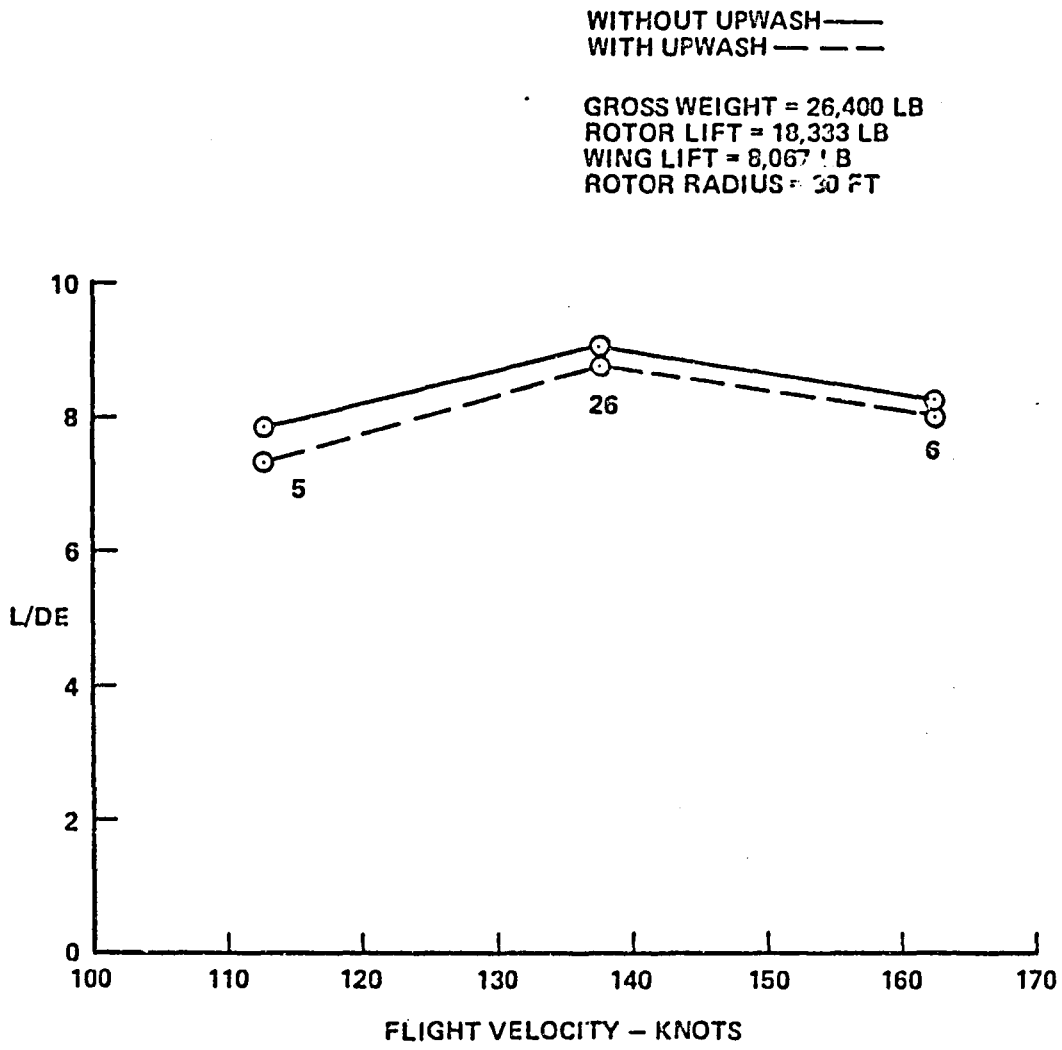


Figure 8-10. Variation of Equivalent Lift-to-Drag Ratio With Flight Velocity From Loads Analysis. Rotor Lift, Gross Weight, Wing Lift, and Rotor Radius Are Held Constant. Numerals Near Symbols Indicate Flight Condition.

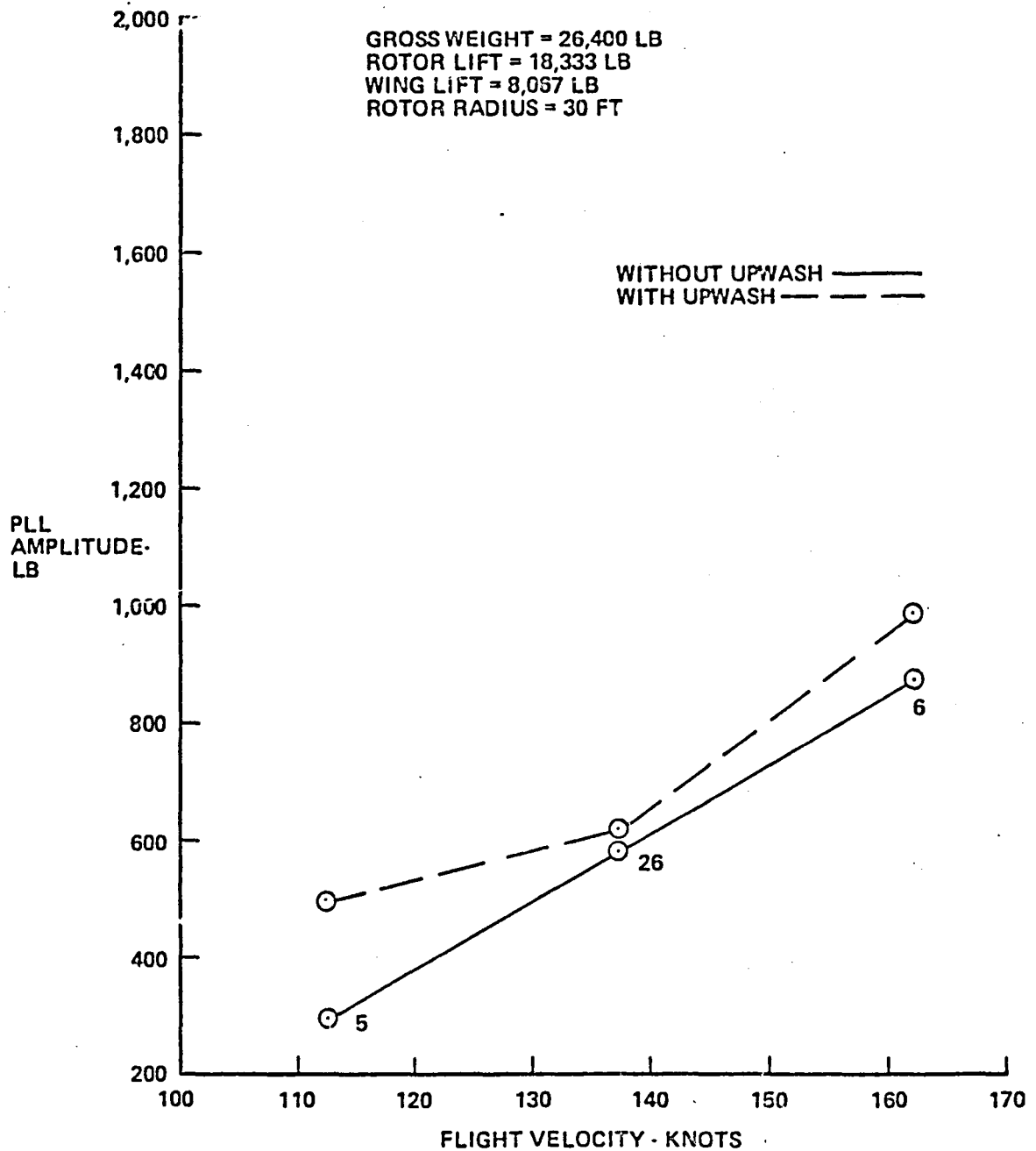


Figure 8-11. Variation of Pitch Link Load Vibratory Amplitude With Flight Velocity From Loads Analysis. Rotor Lift, Gross Weight, Wing Lift, and Rotor Radius Are Held Constant. Numerals Near Symbols Indicate Flight Condition.

GROSS WEIGHT = 26,400 LB
ROTOR LIFT = 18,333 LB
WING LIFT = 8,067 LB
ROTOR RADIUS = 30 FT

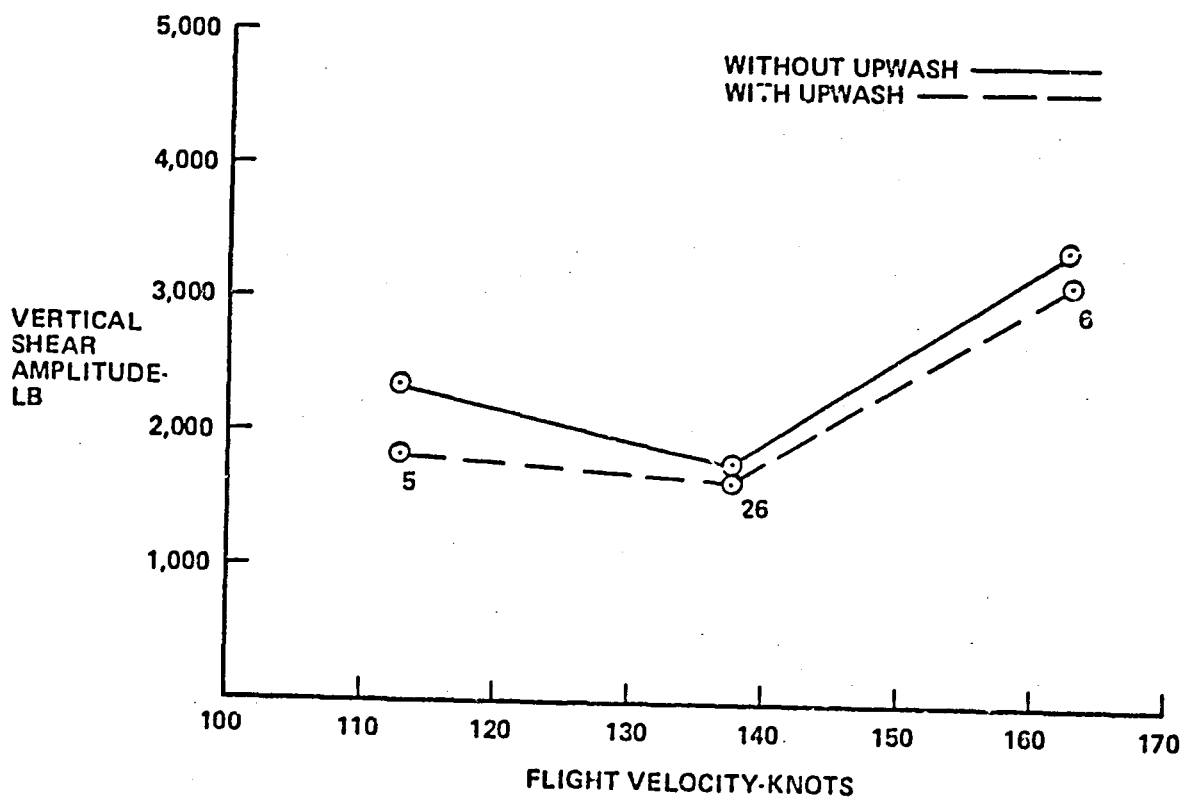


Figure 8-12. Variation of Flap Hinge Vertical Shear Vibratory Amplitude With Flight Velocity From Loads Analysis. Rotor Lift, Gross Weight, Wing Lift, and Rotor Radius Are Held Constant. Numerals Near Symbols Indicate Flight Condition.

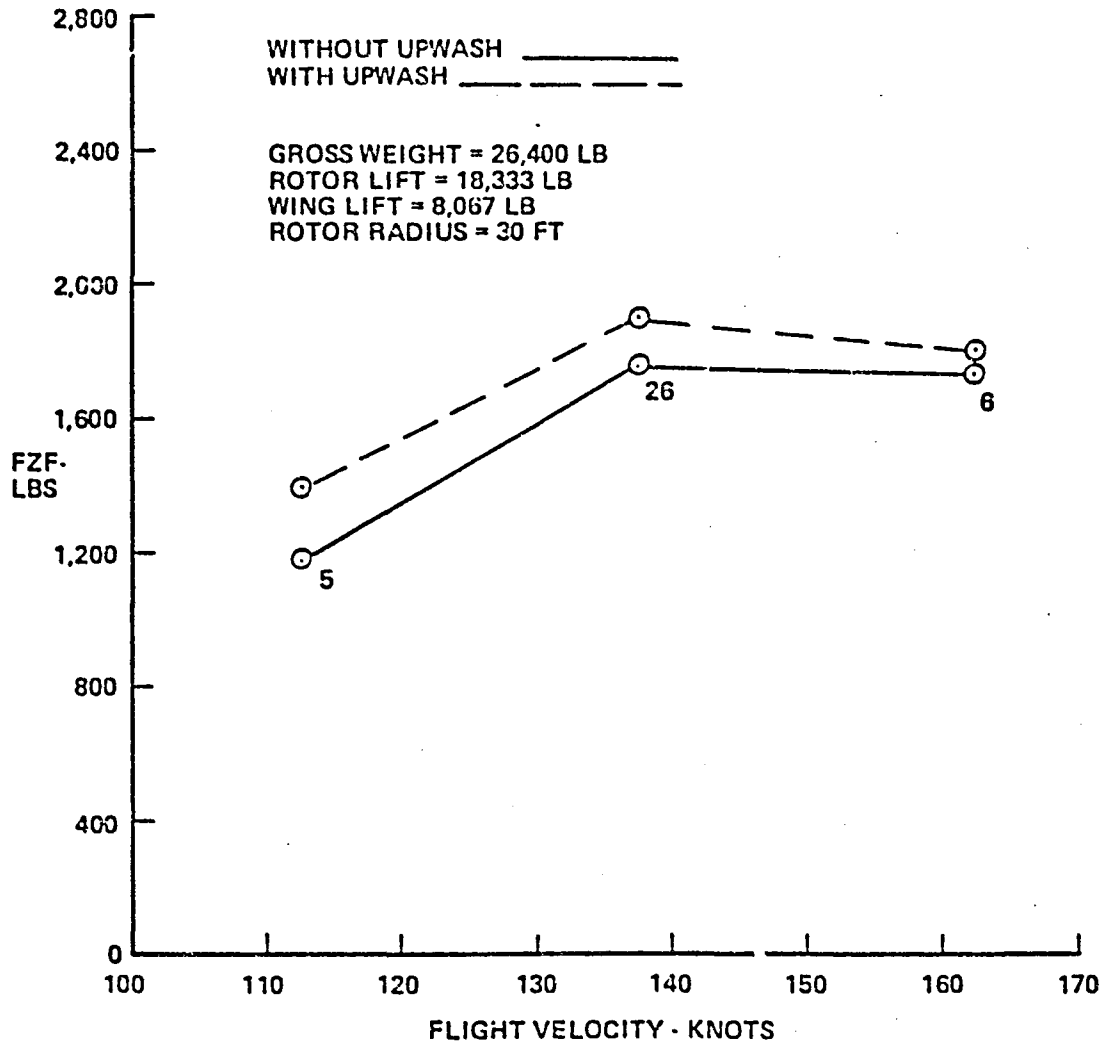


Figure 8-13. Variation of Vertical Hub Force Fourth Harmonic Amplitude With Flight Velocity From Loads Analysis. Rotor Lift, Gross Weight, Wing Lift, and Rotor Radius Are Held Constant. Numerals Near Symbols Indicate Flight Condition.

GROSS WEIGHT = 18,333 LB
ROTOR LIFT = 18,333 LB
FLAT PLATE AREA = 22.9 FT²

WITHOUT UPWASH ———
WITH UPWASH — — —

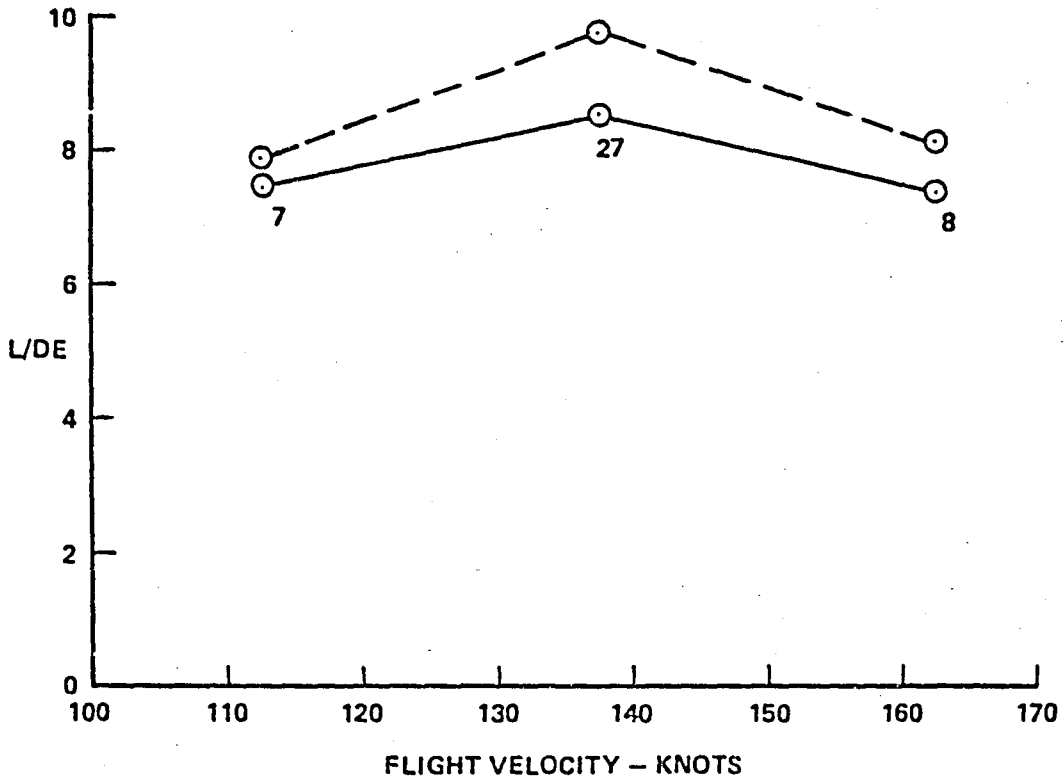


Figure 8-14. Variation of Equivalent Lift-to-Drag Ratio With Flight Velocity From Loads Analysis. Rotor Lift, Gross Weight, and Equivalent Flat Plate Area Are Held Constant. Numerals Near Symbols Indicate Flight Condition.

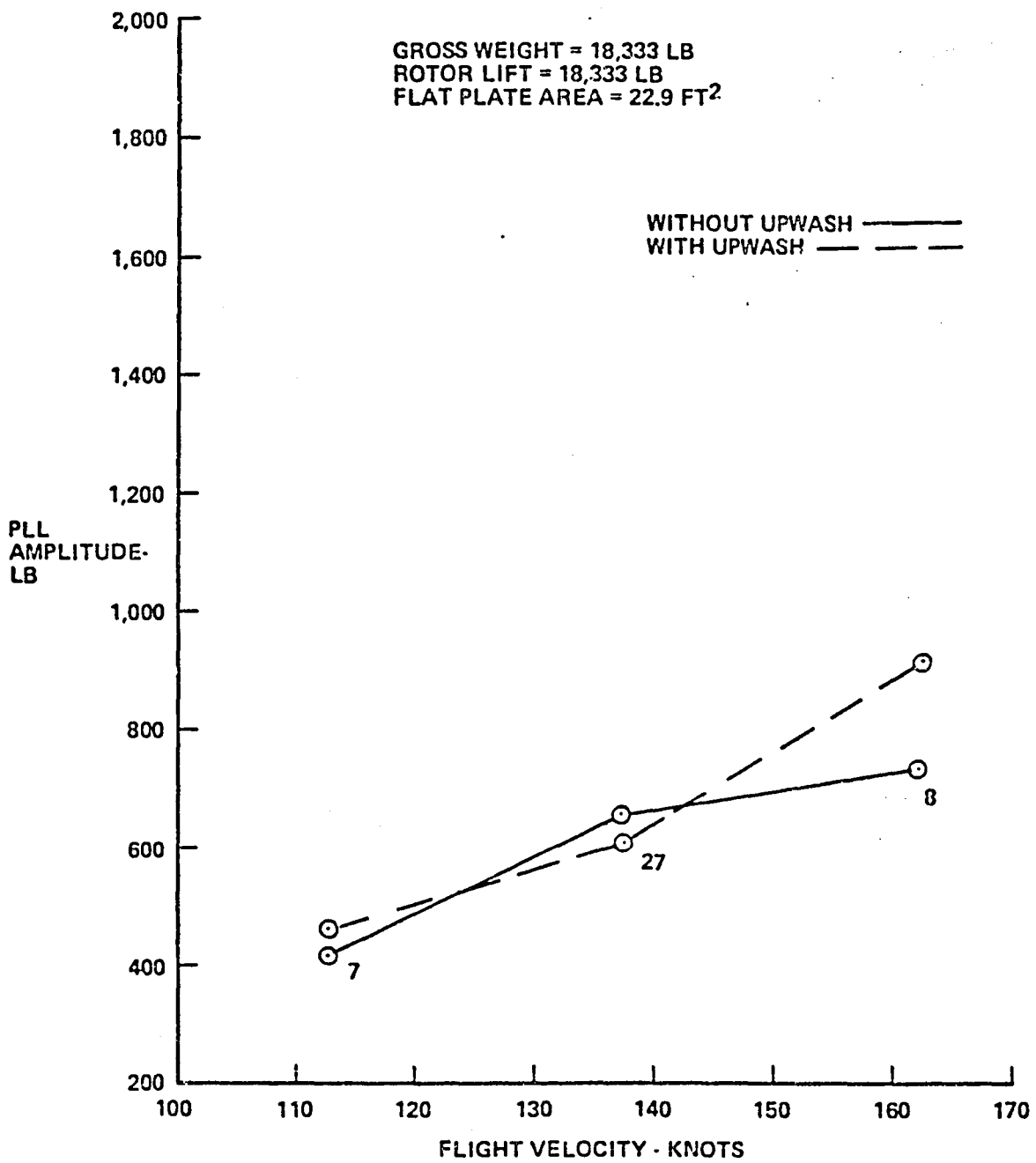


Figure 8-15. Variation of Pitch Link Load Vibratory Amplitude With Flight Velocity From Loads Analysis. Rotor Lift, Gross Weight, and Equivalent Flat Plate Area Are Held Constant. Numerals Near Symbols Indicate Flight Condition.

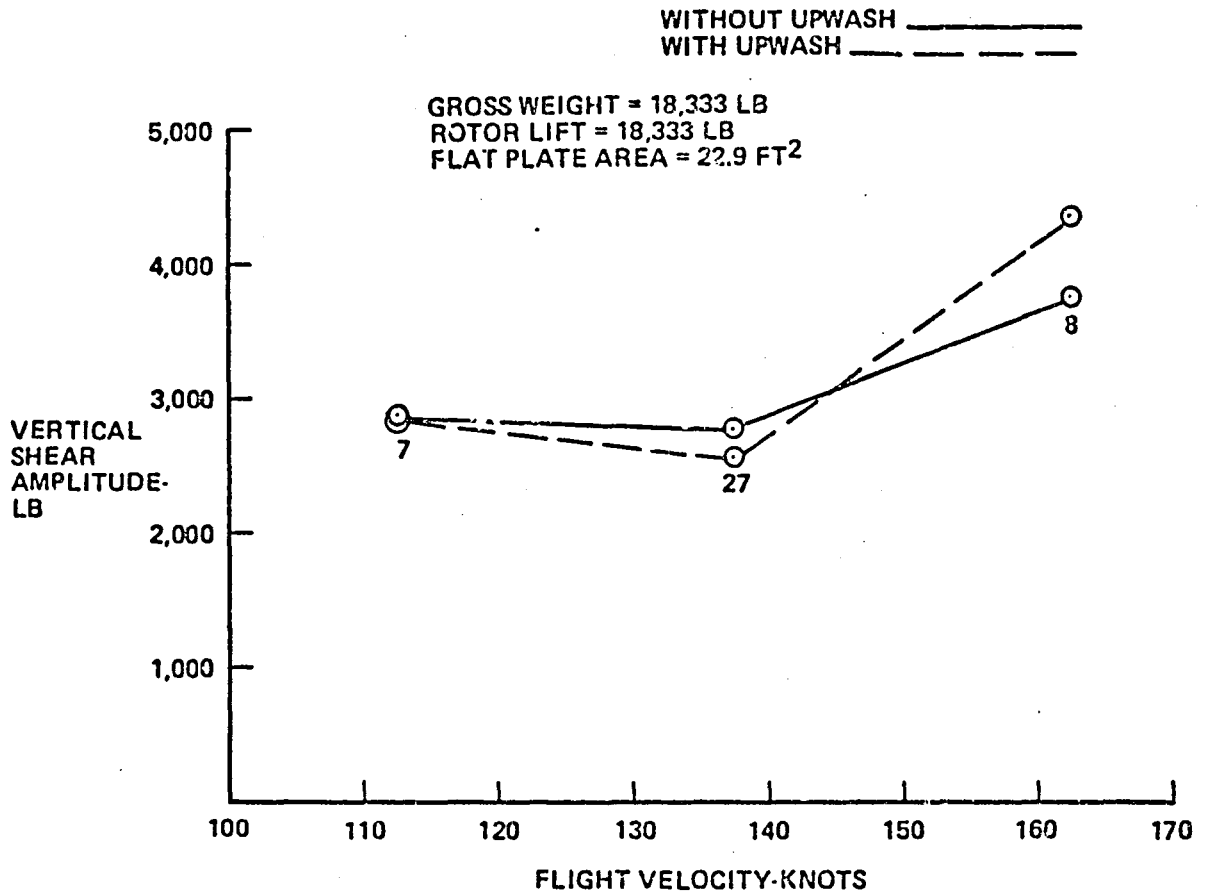


Figure 8-16. Variation of Flap Hinge Vertical Shear Vibratory Amplitude With Flight Velocity From Loads Analysis. Rotor Lift, Gross Weight, and Equivalent Flat Plate Area Are Constant. Numerals Near Symbols Indicate Flight Condition.

GROSS WEIGHT = 18,333 LB
ROTOR LIFT = 18,333 LB
FLAT PLATE AREA = 22.9 FT²

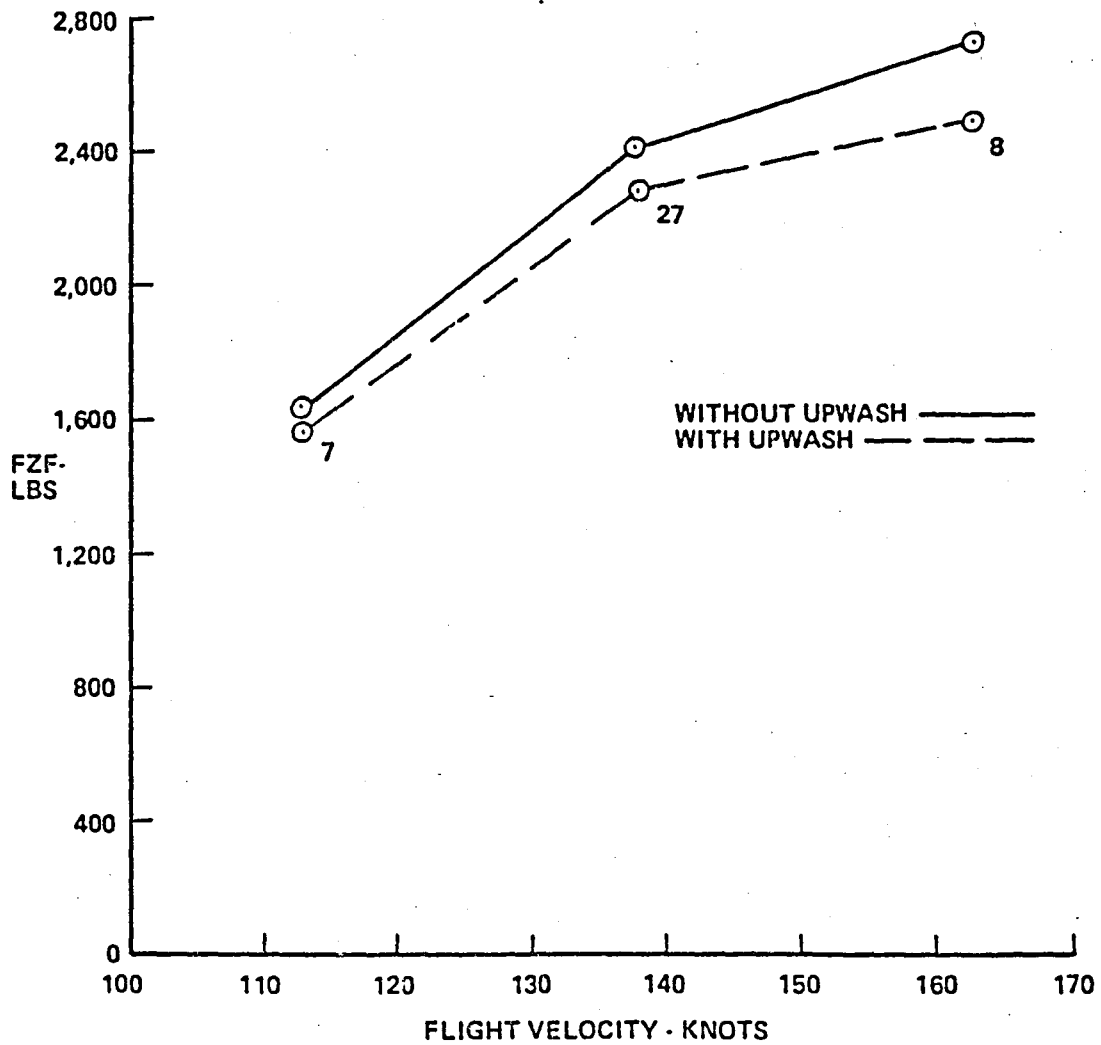


Figure 8-17. Variation of Vertical Hub Force Fourth Harmonic Amplitude With Flight Velocity From Loads Analysis. Rotor Lift, Gross Weight, and Equivalent Flat Plate Area Are Held Constant. Numerals Near Symbols Indicate Flight Condition.

WITHOUT UPWASH _____
WITH UPWASH - - - - -

FLIGHT VELOCITY = 162.5 KN
ROTOR RADIUS = 30 FT

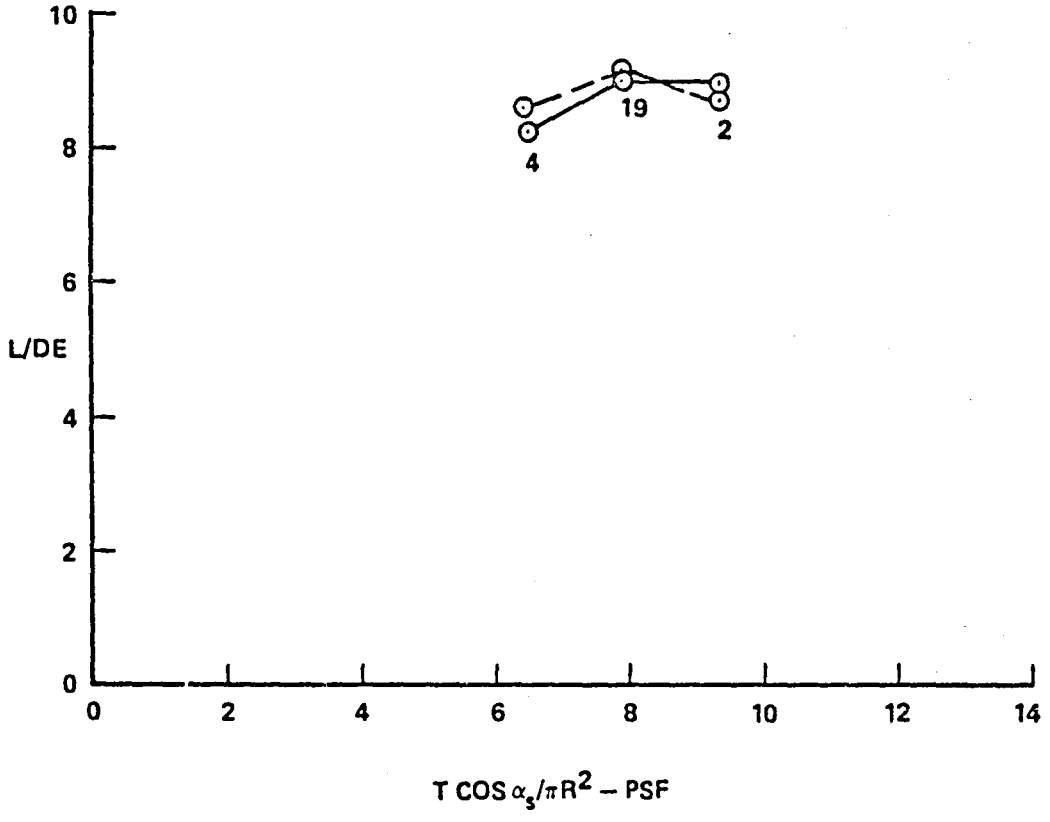


Figure 8-18. Variation of Equivalent Lift-to-Drag Ratio With Disk Loading From Loads Analysis. Flight Velocity and Rotor Radius Are Held Constant. Numerals Near Symbols Indicate Flight Condition.

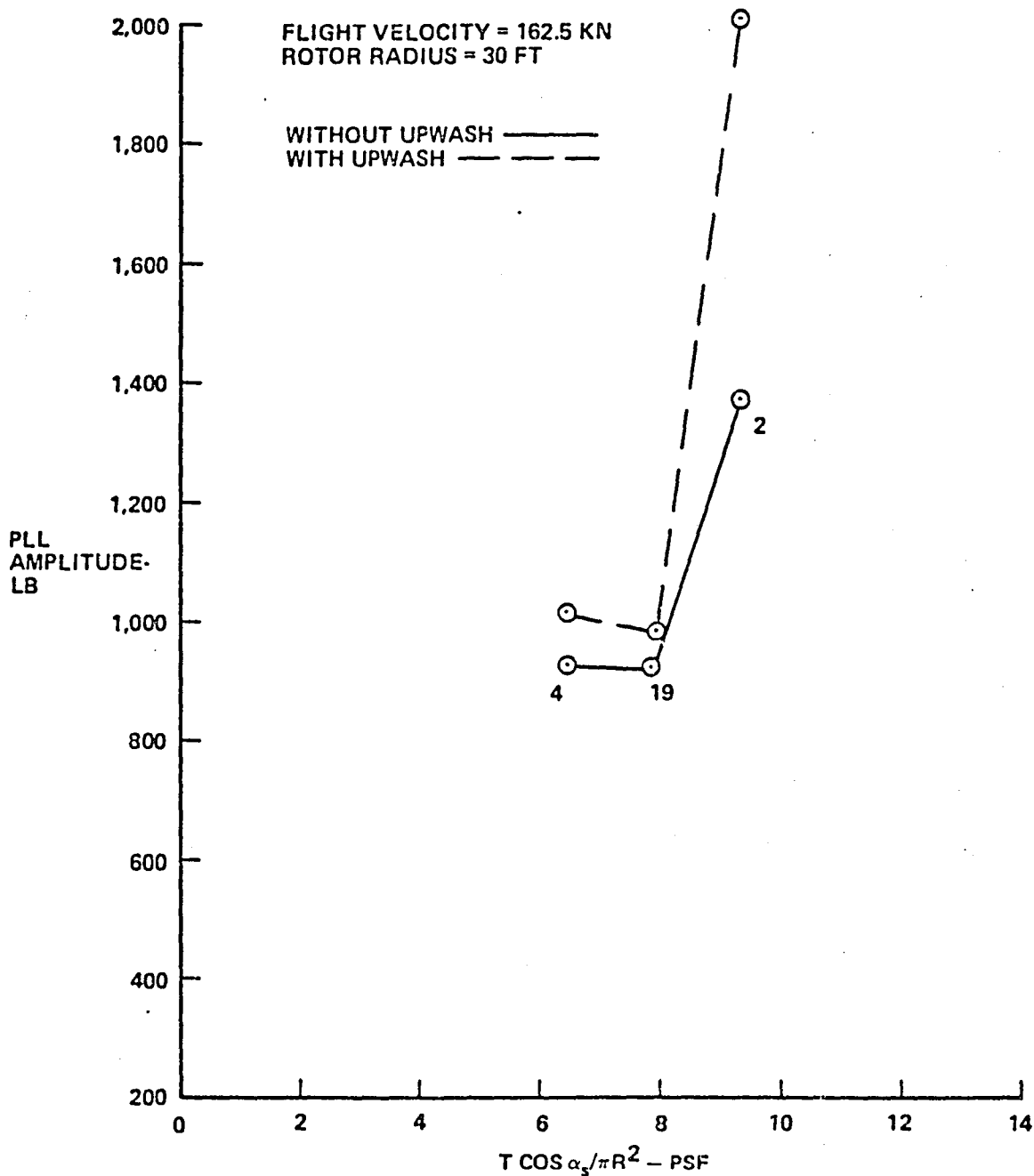


Figure 8-19. Variation of Pitch Link Load Vibratory Amplitude With Disk Loading From Loads Analysis. Flight Velocity and Rotor Radius Are Held Constant. Numerals Near Symbols Indicate Flight Condition.

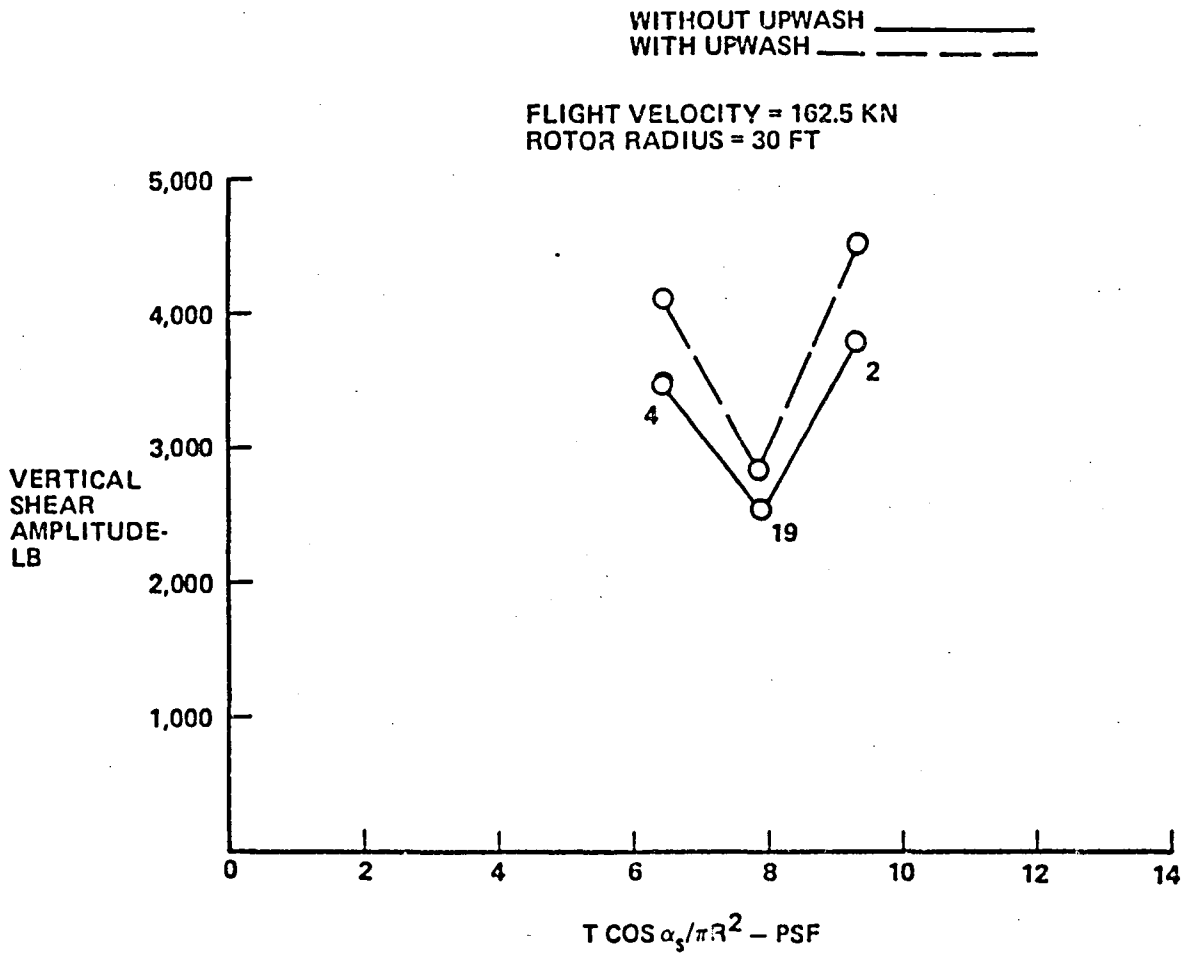


Figure 8-20. Variation of Flap Hinge Vertical Shear Vibratory Amplitude With Disk Loading From Loads Analysis. Flight Velocity and Rotor Radius Are Held Constant. Numerals Near Symbols Indicate Flight Condition.

FLIGHT VELOCITY = 162.5 KN
ROTOR RADIUS = 30 FT

WITHOUT UPWASH ———
WITH UPWASH — — —

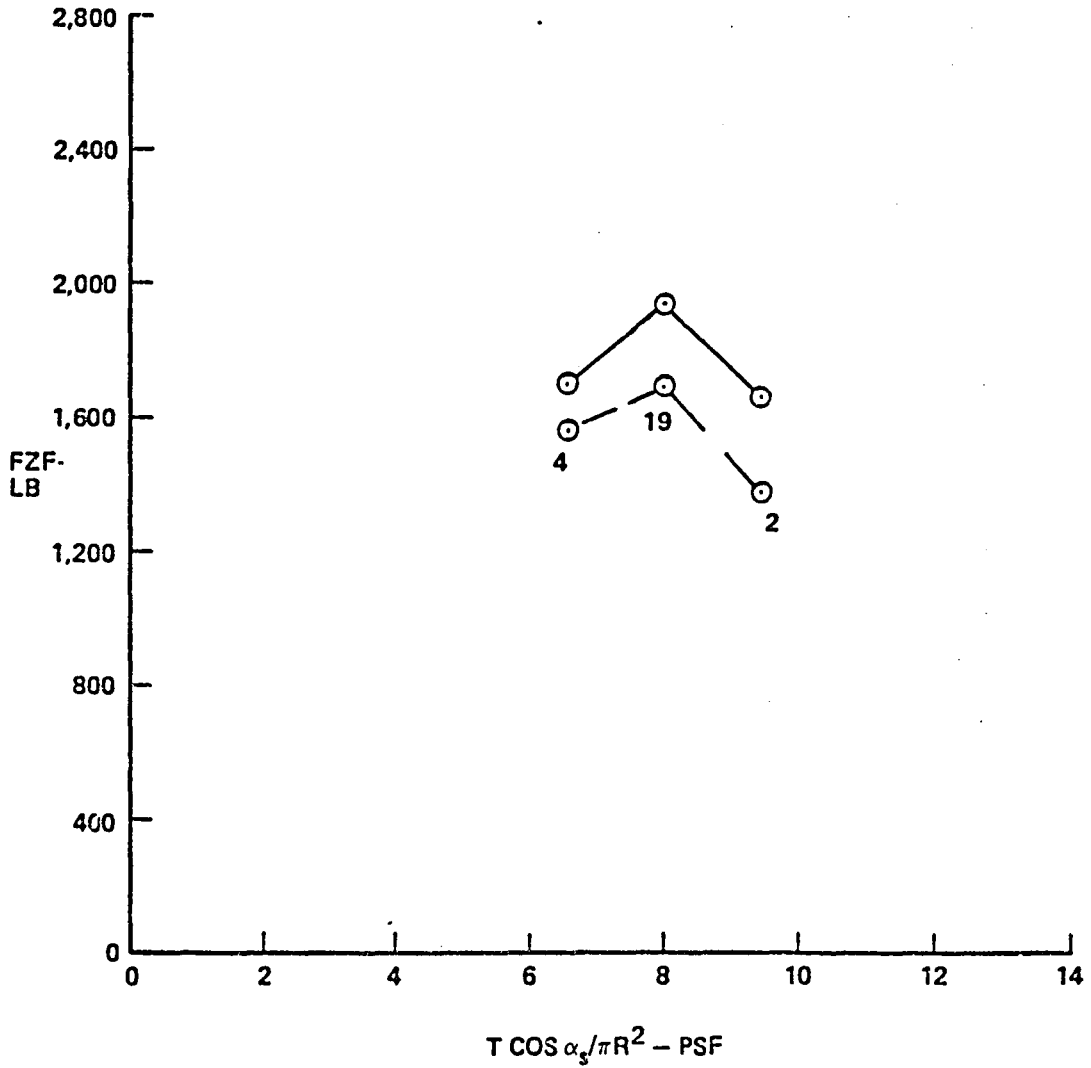


Figure 8-21. Variation of Vertical Hub Force Fourth Harmonic Amplitude With Disk Loading From Loads Analysis. Flight Velocity and Rotor Radius Are Held Constant. Numerals Near Symbols Indicate Flight Condition.

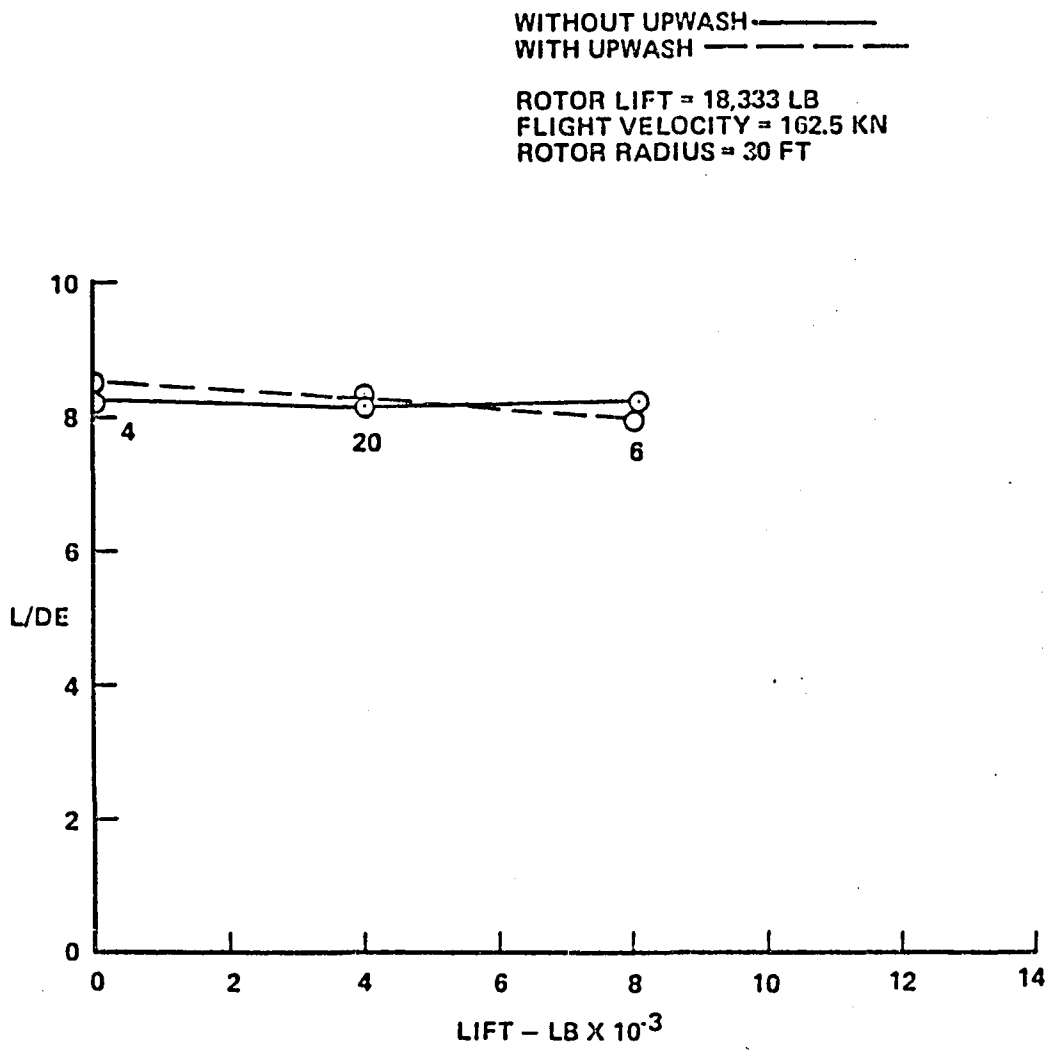


Figure 8-22. Variation of Equivalent Lift-to-Drag Ratio With Wing Lift From Loads Analysis. Rotor Lift, Flight Velocity, and Rotor Radius Are Held Constant. Numerals Near Symbols Indicate Flight Condition.

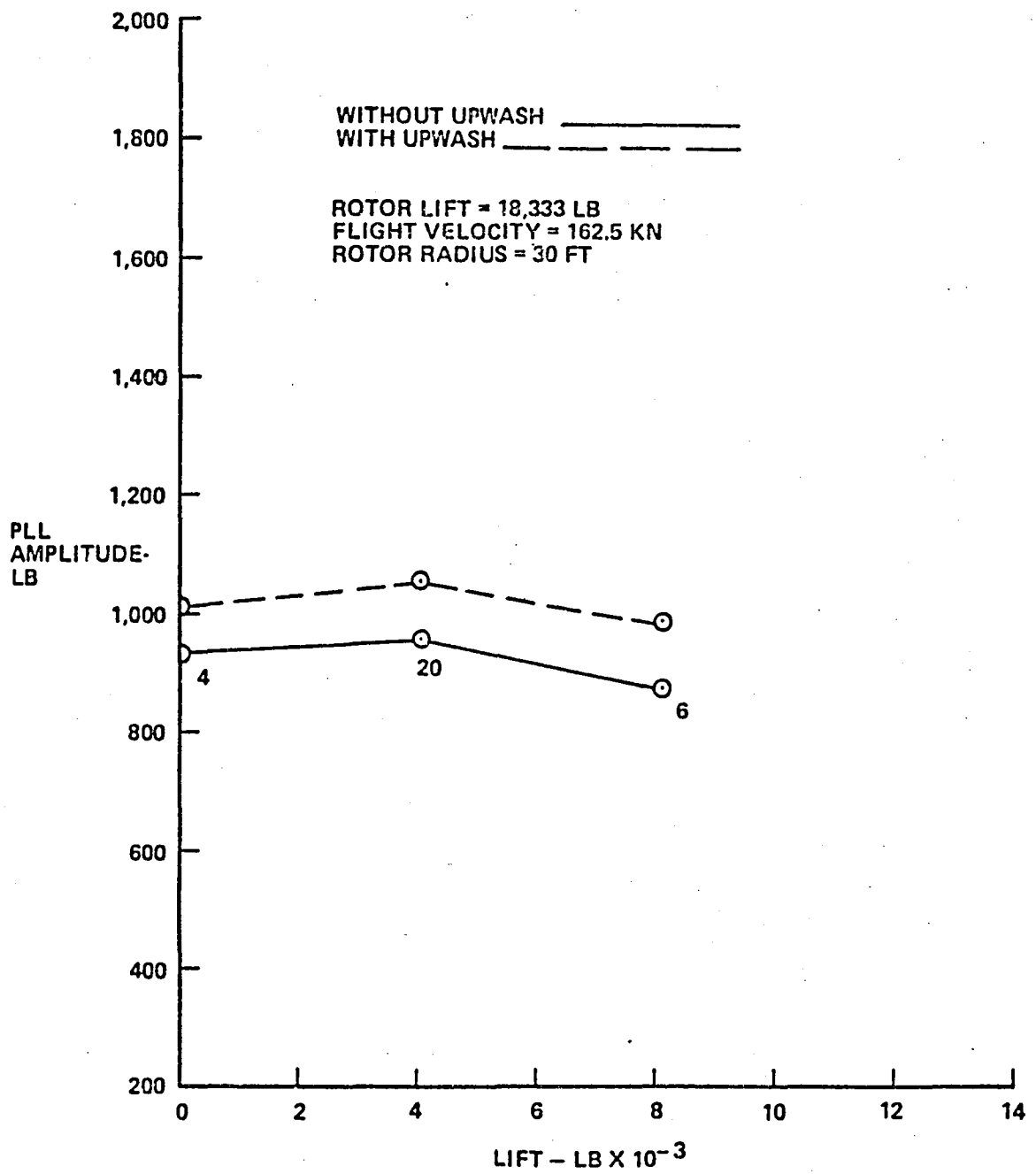


Figure 8-23. Variation of Pitch Link Load Vibratory Amplitude With Wing Lift From Loads Analysis. Rotor Lift, Flight Velocity, and Rotor Radius Are Held Constant. Numerals Near Symbols Indicate Flight Condition.

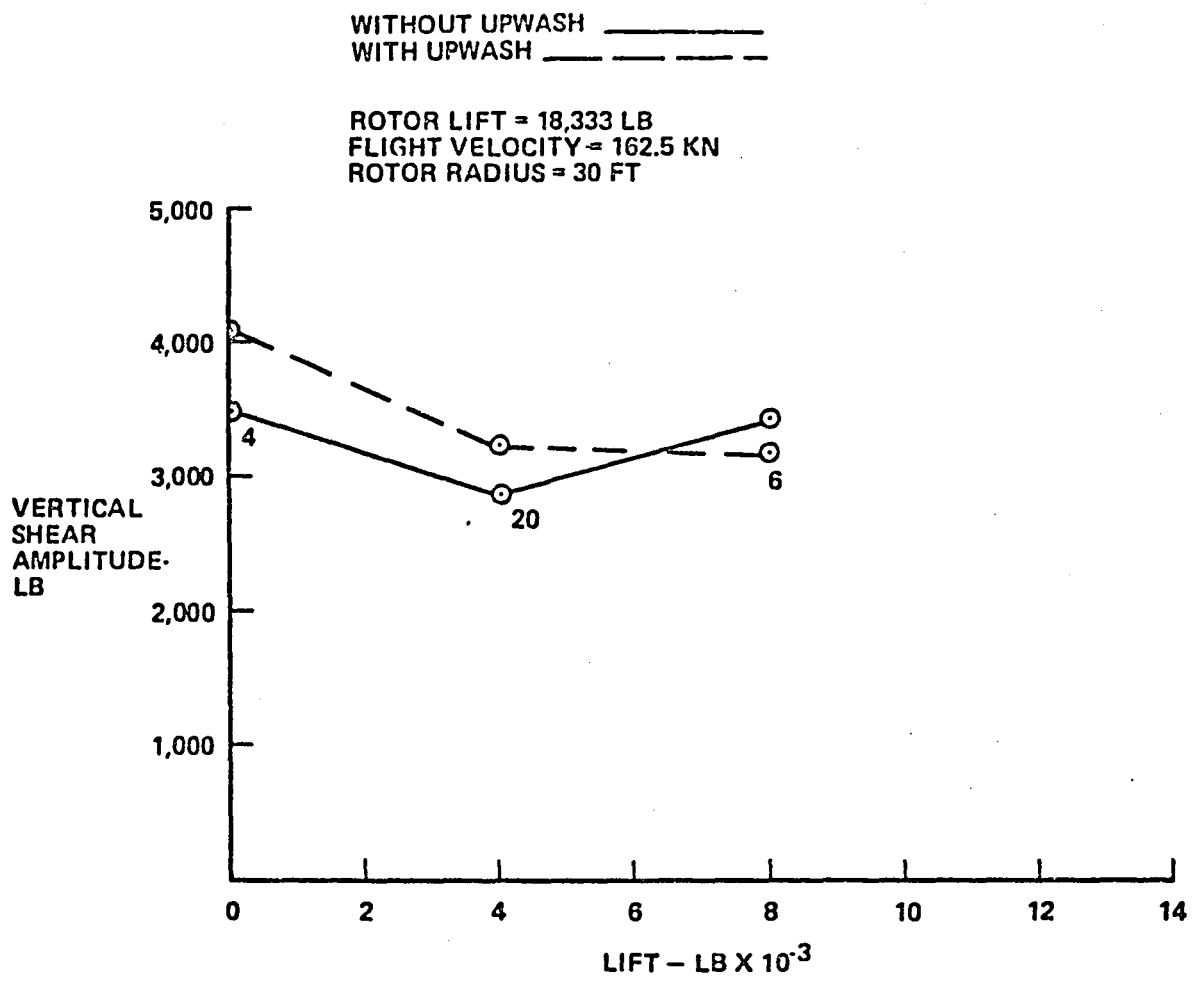


Figure 8-24. Variation of Flap Hinge Vertical Shear Vibratory Amplitude With Wing Lift From Loads Analysis. Rotor Lift, Flight Velocity, and Rotor Radius Are Held Constant. Numerals Near Symbols Indicate Flight Condition.

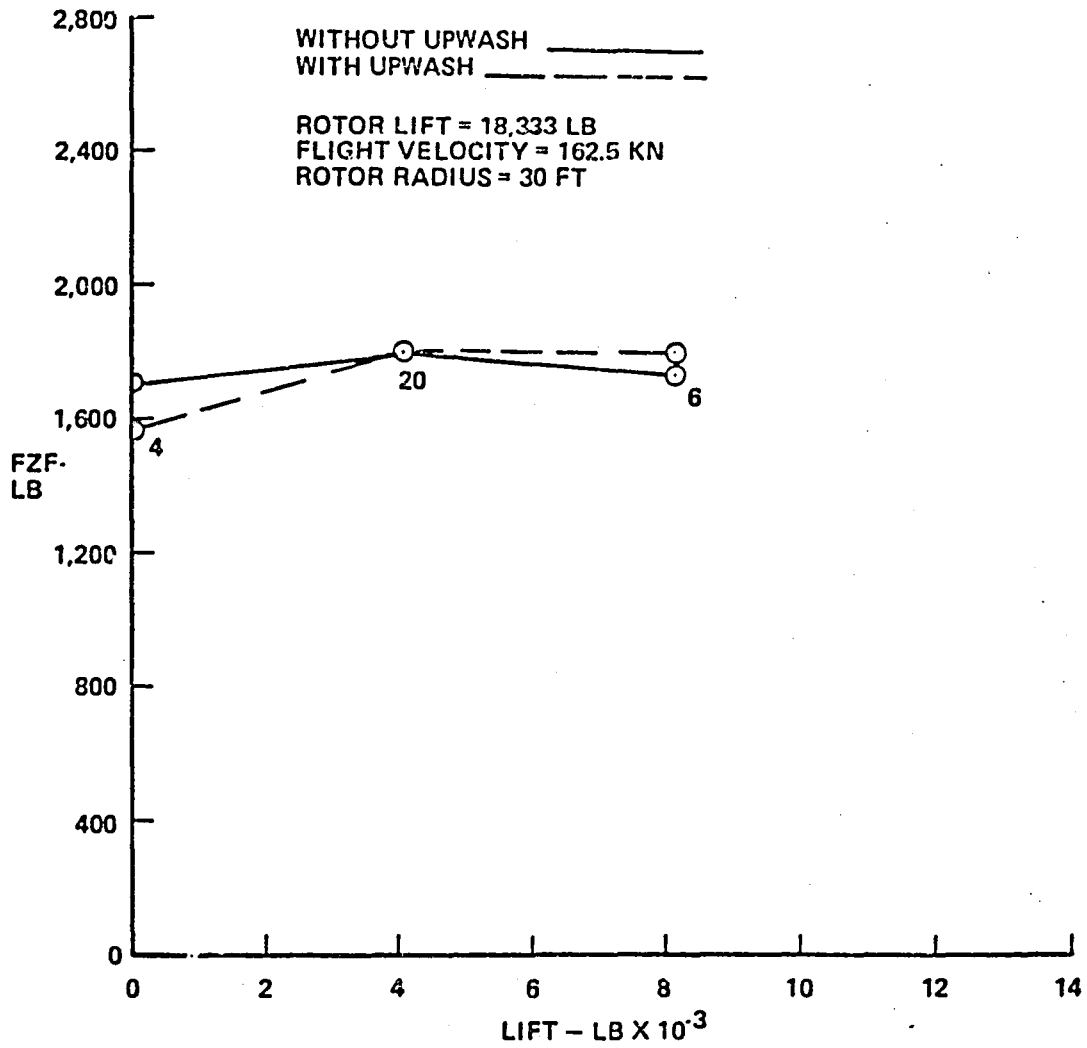


Figure 8-25. Variation of Vertical Hub Force Fourth Harmonic Amplitude With Wing Lift From Loads Analysis. Rotor Lift, Flight Velocity, and Rotor Radius Are Held Constant. Numerals Near Symbols Indicate Flight Condition.

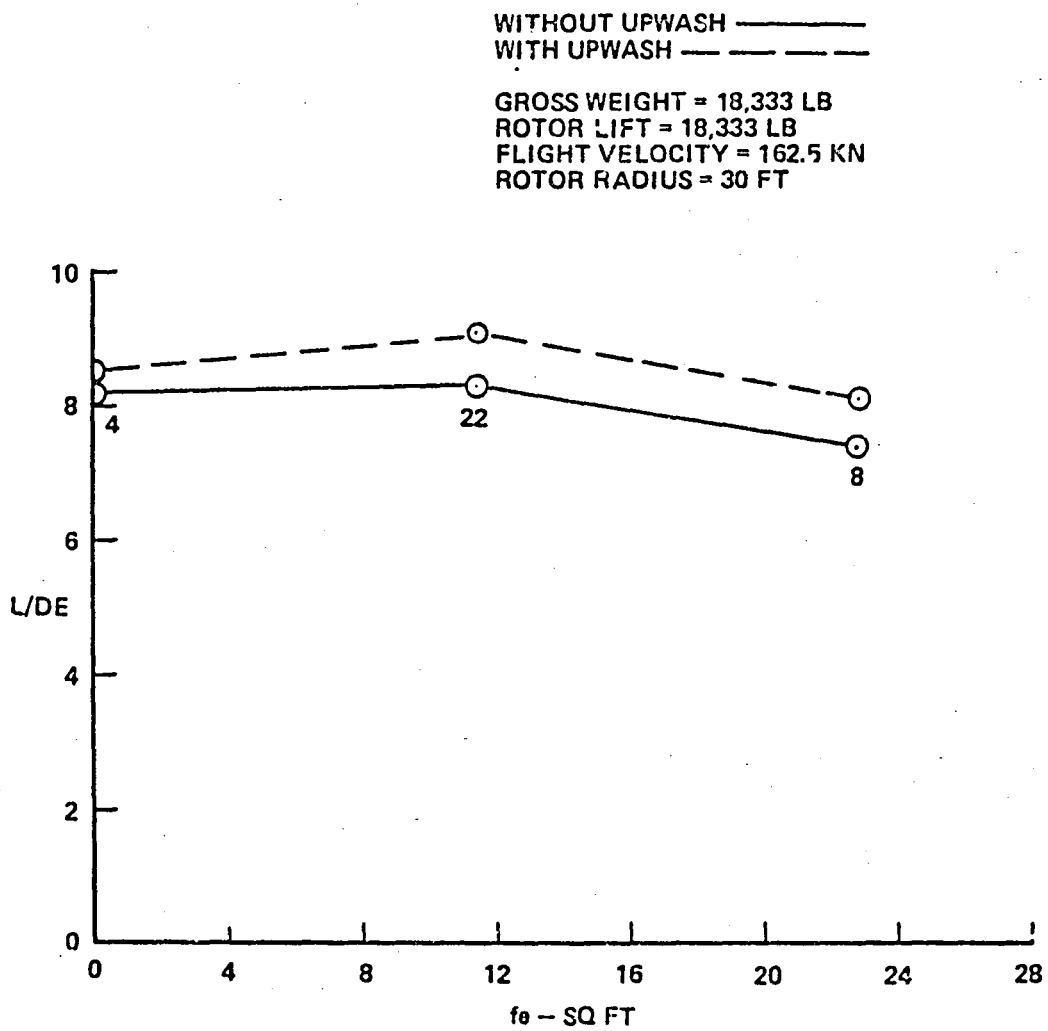


Figure 8-26. Variation of Equivalent Lift-to-Drag Ratio With Flat Plate Area for Auxiliary Thrust From Loads Analysis. Rotor Radius, Rotor Lift, Gross Weight, and Flight Velocity Are Held Constant. Numerals Near Symbols Indicate Flight Condition.

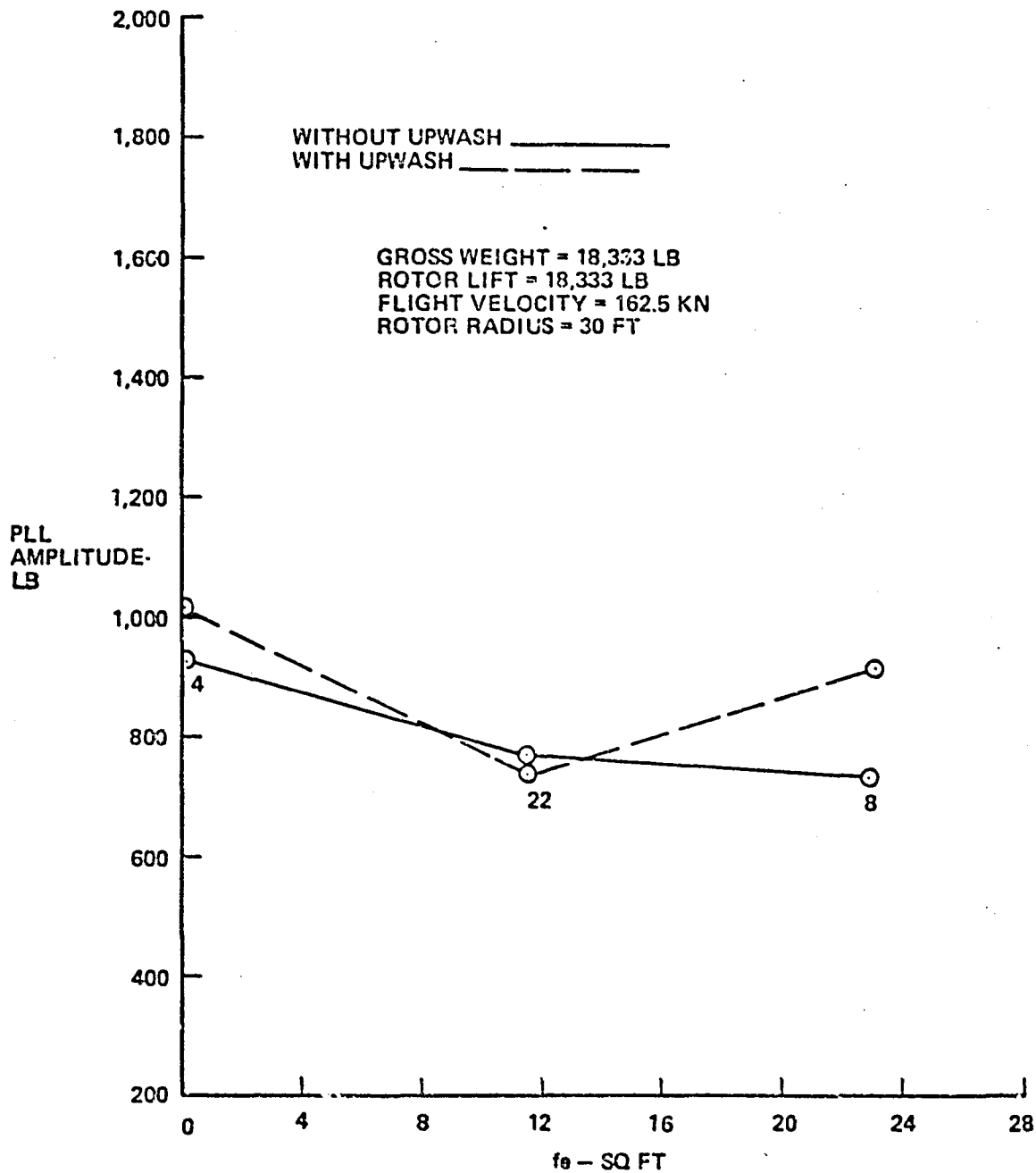


Figure 8-27. Variation of Pitch Link Load Vibratory Amplitude With Flat Plate Area for Auxiliary Thrust From Loads Analysis. Rotor Radius, Rotor Lift, Gross Weight, and Flight Velocity Are Held Constant. Numerals Near Symbols Indicate Flight Condition.

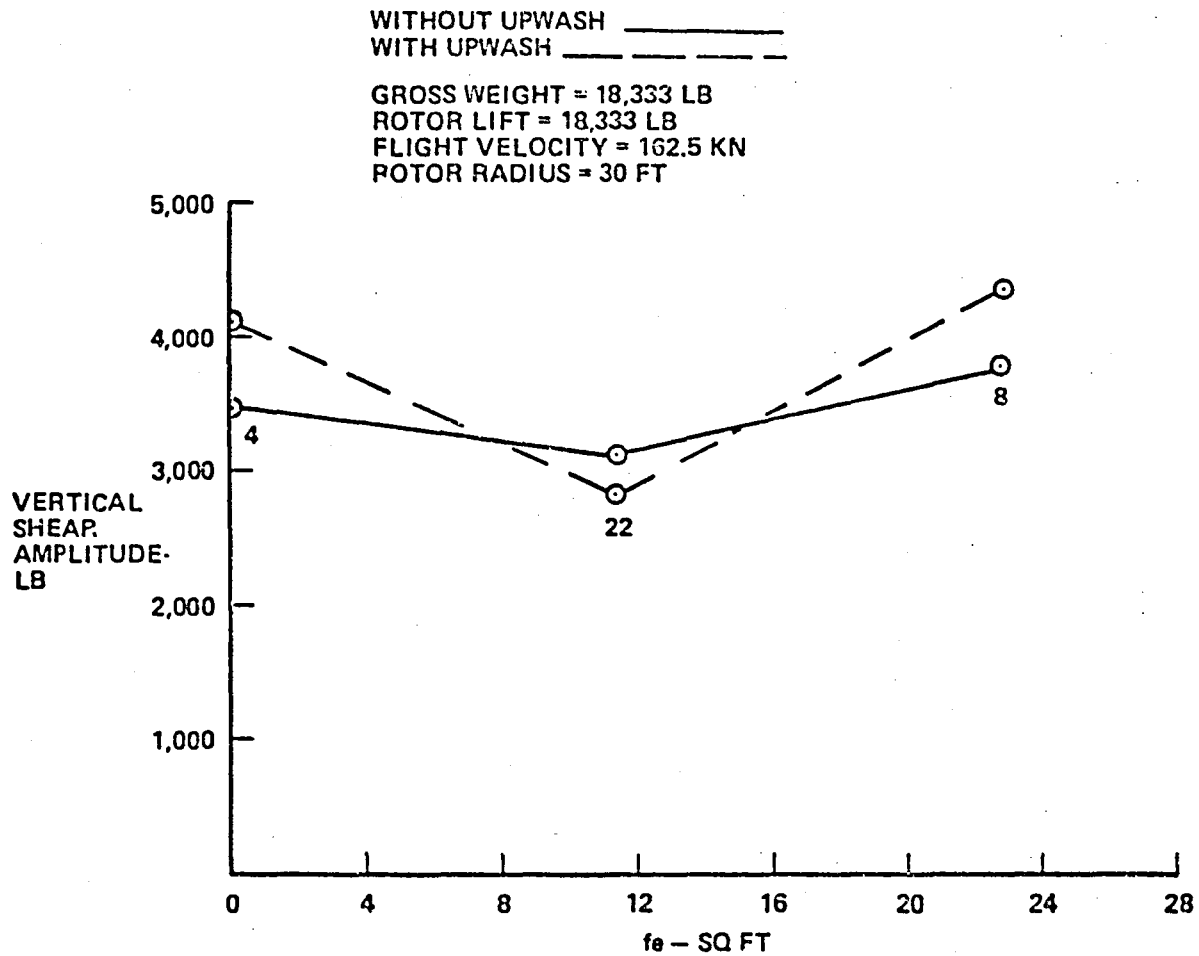


Figure 8-28. Variation of Flap Hinge Vertical Shear Vibratory Amplitude With Flat Plate Area for Auxiliary Thrust From Loads Analysis. Rotor Radius, Rotor Lift, Gross Weight, and Flight Velocity Are Held Constant. Numerals Near Symbols Indicate Flight Condition.

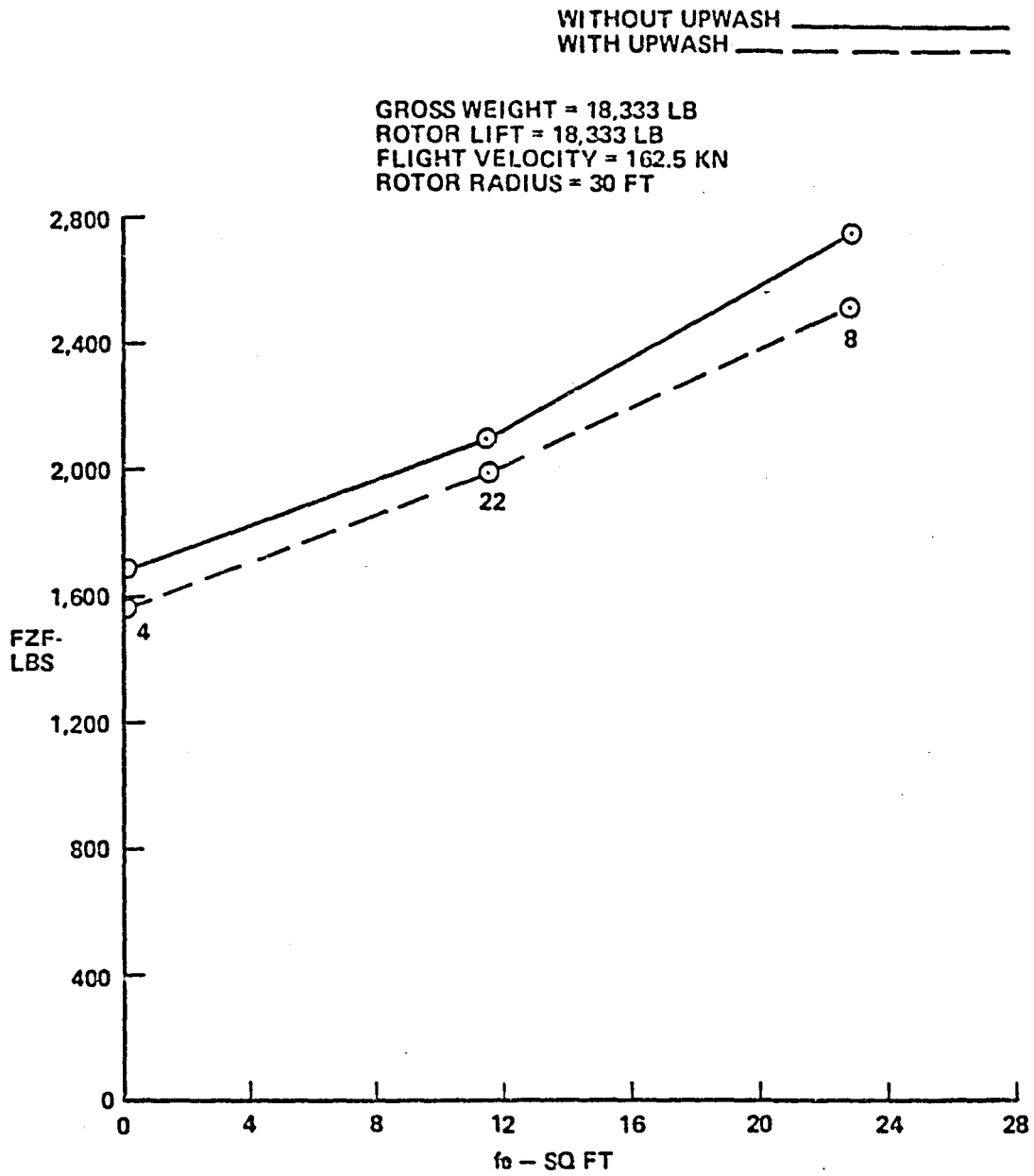


Figure 8-29. Variation of Vertical Hub Force Fourth Harmonic Amplitude With Flat Plate Area for Auxiliary Thrust From Loads Analysis. Rotor Radius, Rotor Lift, Gross Weight, and Flight Velocity Are Held Constant. Numerals Near Symbols Indicate Flight Condition.

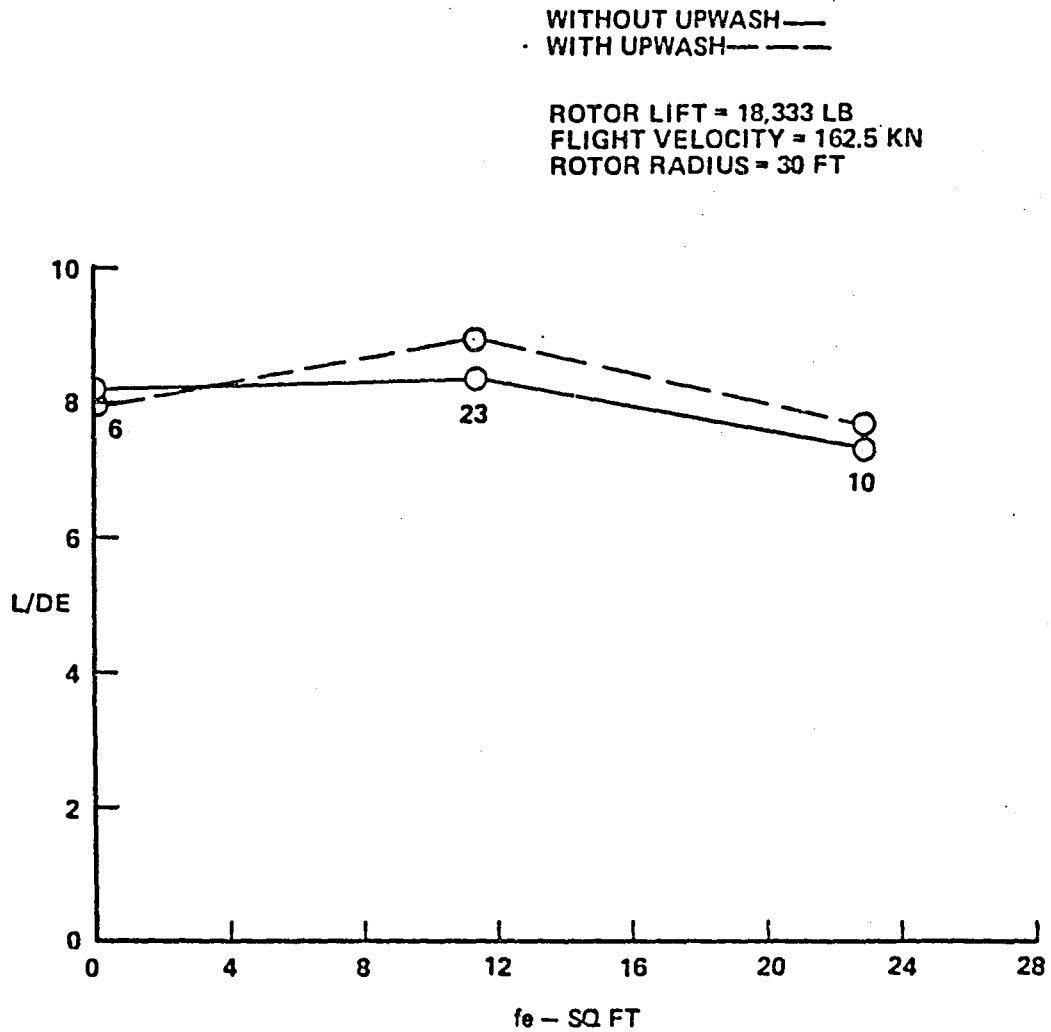


Figure 8-30. Variation of Equivalent Lift-to-Drag Ratio With Flat Plate Area for Auxiliary Thrust From Loads Analysis. Rotor Radius, Rotor Lift, and Flight Velocity Are Held Constant. Numerals Near Symbols Indicate Flight Condition.

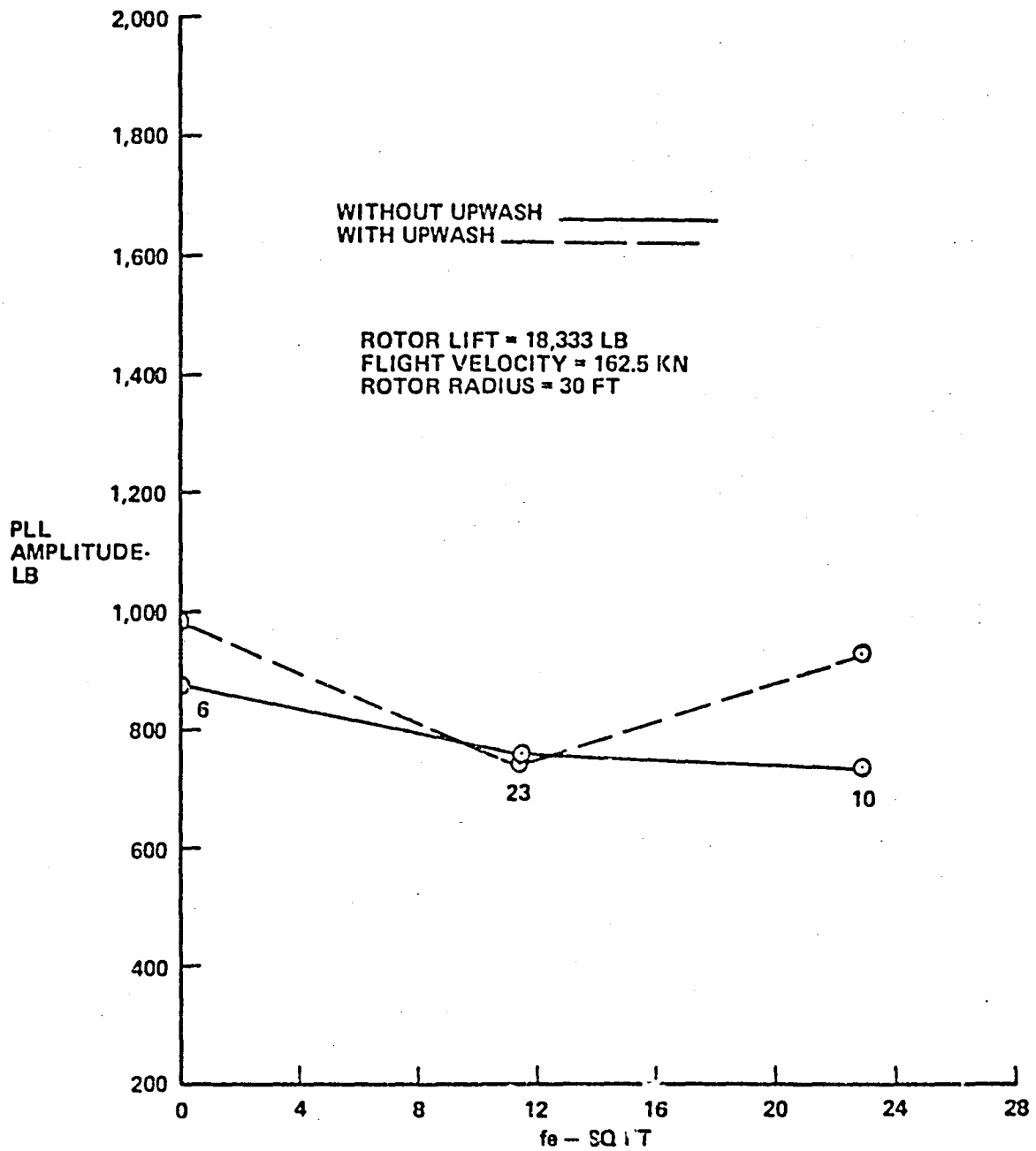


Figure 8-31. Variation of Pitch Link Load Vibratory Amplitude With Flat Plate Area for Auxiliary Thrust From Loads Analysis. Rotor Radius, Rotor Lift, and Flight Velocity Are Held Constant. Numerals Near Symbols Indicate Flight Condition.

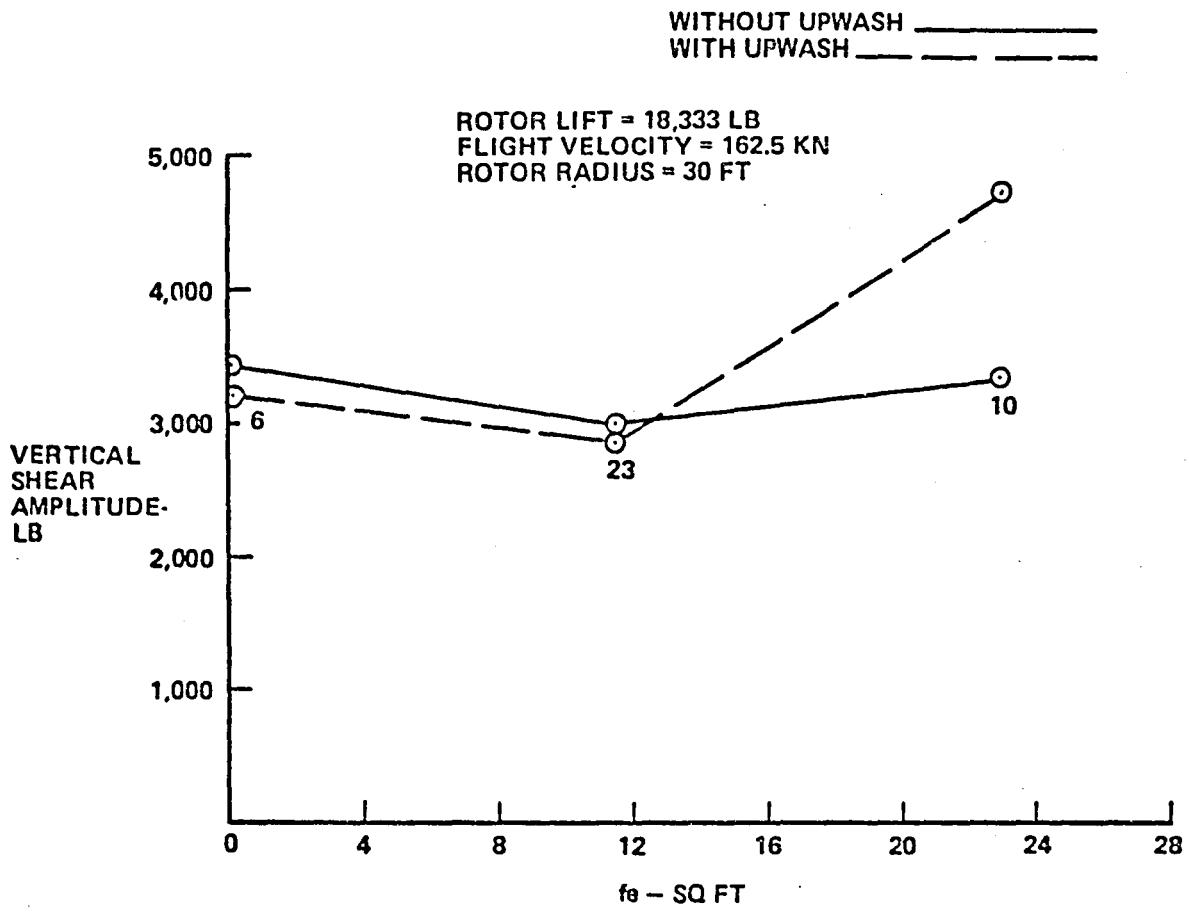


Figure 8-32. Variation of Flap Hinge Vertical Shear Vibratory Amplitude With Flat Plate Area for Auxiliary Thrust From Loads Analysis. Rotor Radius, Rotor Lift, and Flight Velocity Are Held Constant. Numerals Near Symbols Indicate Flight Condition.

ROTOR LIFT = 18,333 LB
FLIGHT VELOCITY = 162.5 KN
ROTOR RADIUS = 30 FT

WITHOUT UPWASH ———
WITH UPWASH - - - - -

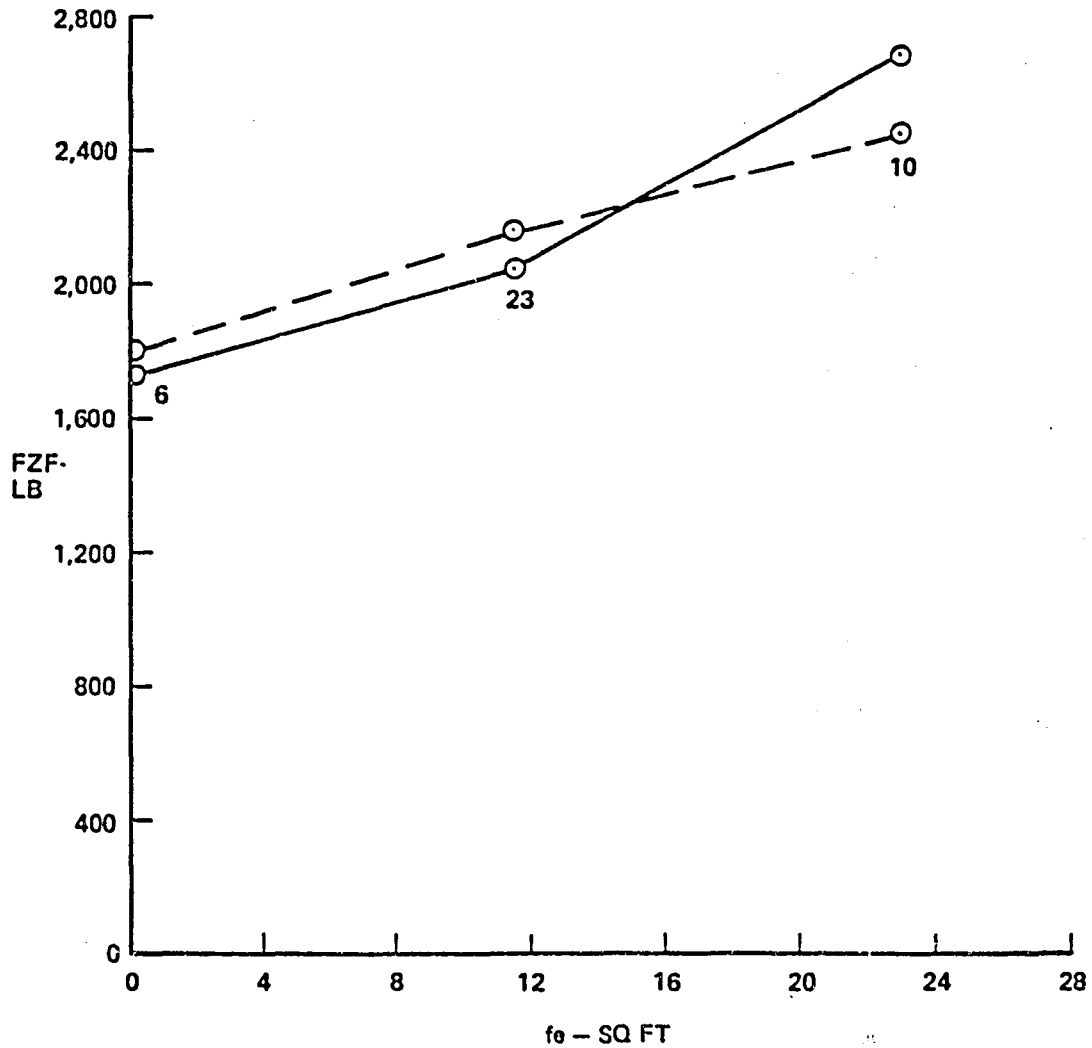


Figure 8-33. Variation of Vertical Hub Force Fourth Harmonic Amplitude With Flat Plate Area for Auxiliary Thrust From Loads Analysis. Rotor Radius, Rotor Lift, and Flight Velocity Are Held Constant. Numerals Near Symbols Indicate Flight Condition.

ROTOR LIFT = 18,333 LB
 FLIGHT VELOCITY = 162.5 KN
 ROTOR RADIUS = 30 FT

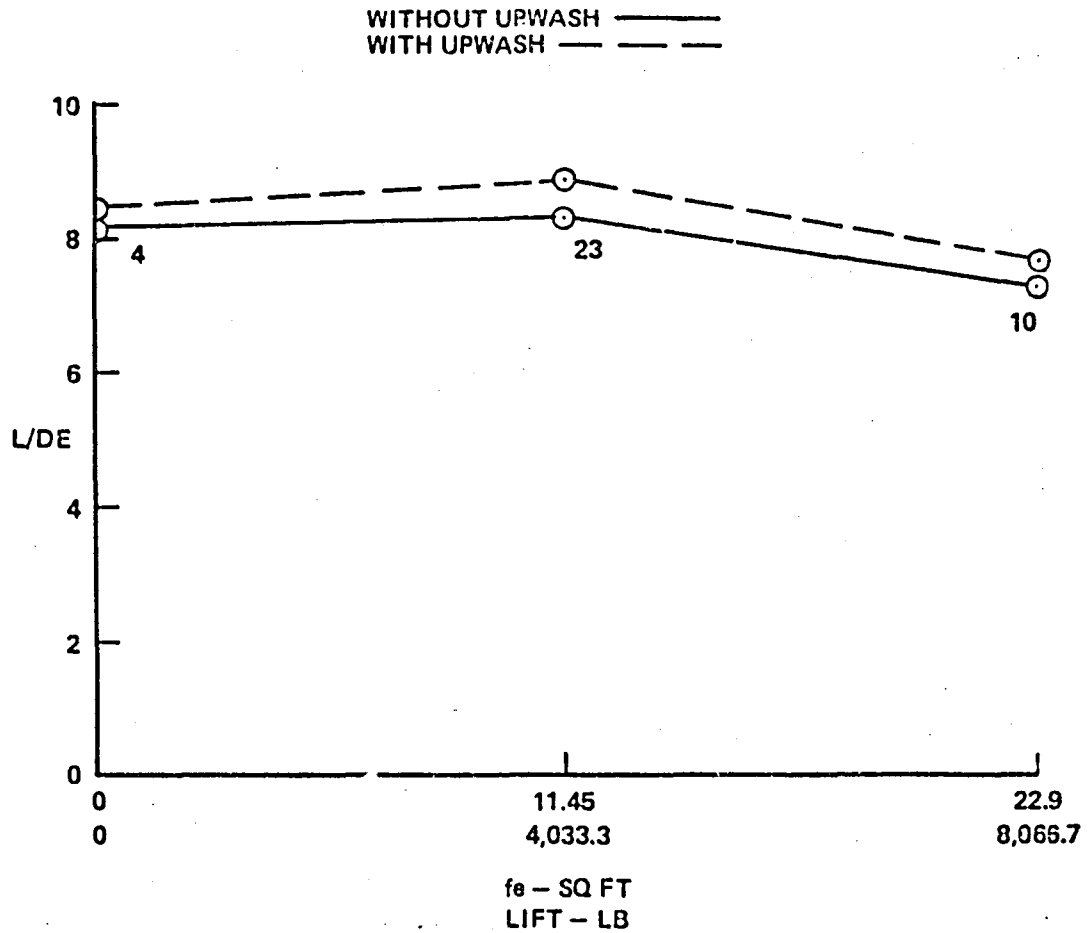


Figure 8-34. Variation of Equivalent Lift-to-Drag Ratio With Flat Plate Area for Auxiliary Thrust and Wing Lift From Loads Analysis. Rotor Lift, Flight Velocity, and Rotor Radius Are Held Constant. Numerals Near Symbols Indicate Flight Condition.

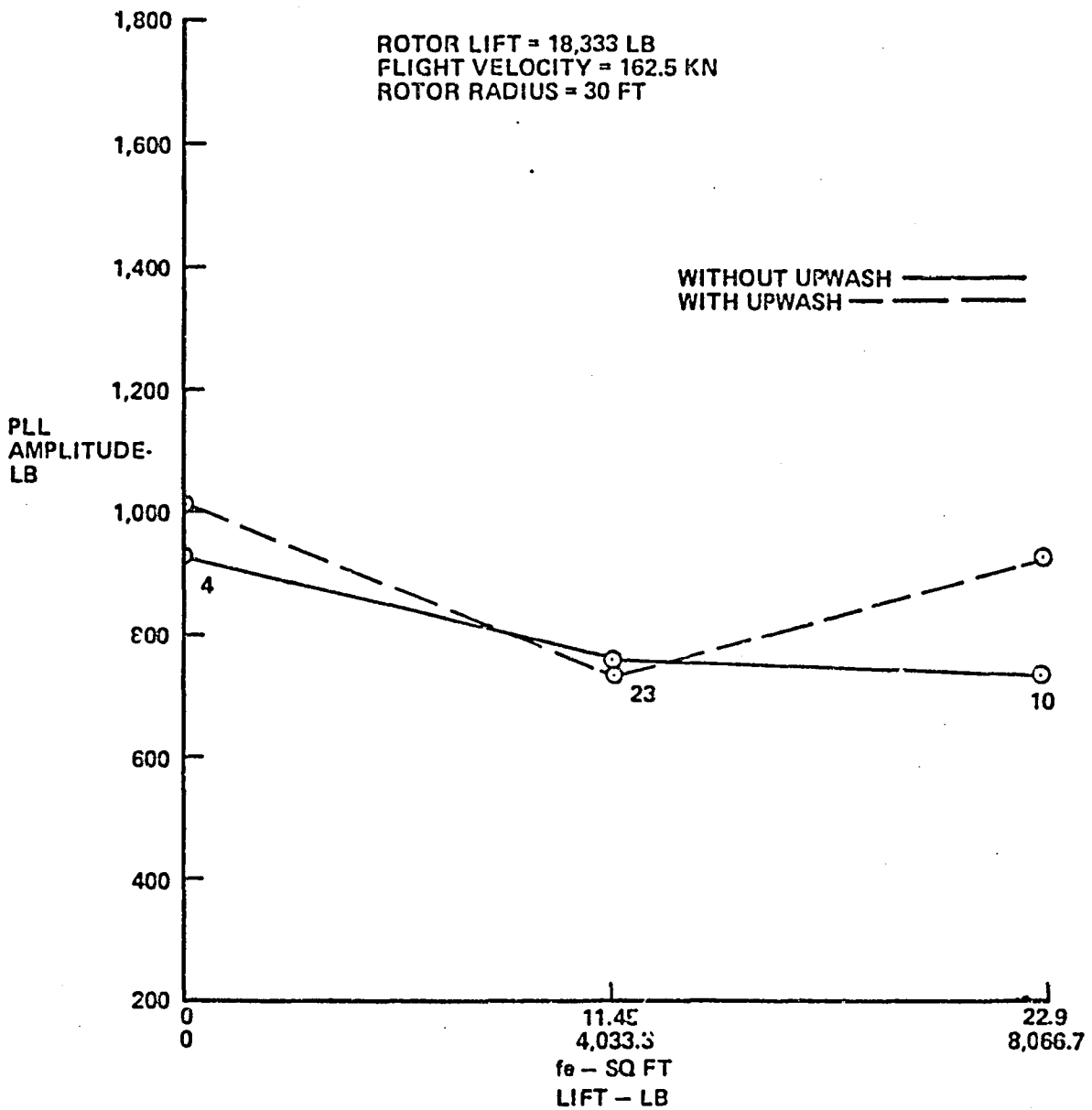


Figure 8-35. Variation of Pitch Link Load Vibratory Amplitude With Flat Plate Area for Auxiliary Thrust and Wing Lift From Loads Analysis. Rotor Lift, Flight Velocity, and Rotor Radius Are Held Constant. Numerals Near Symbols Indicate Flight Condition.

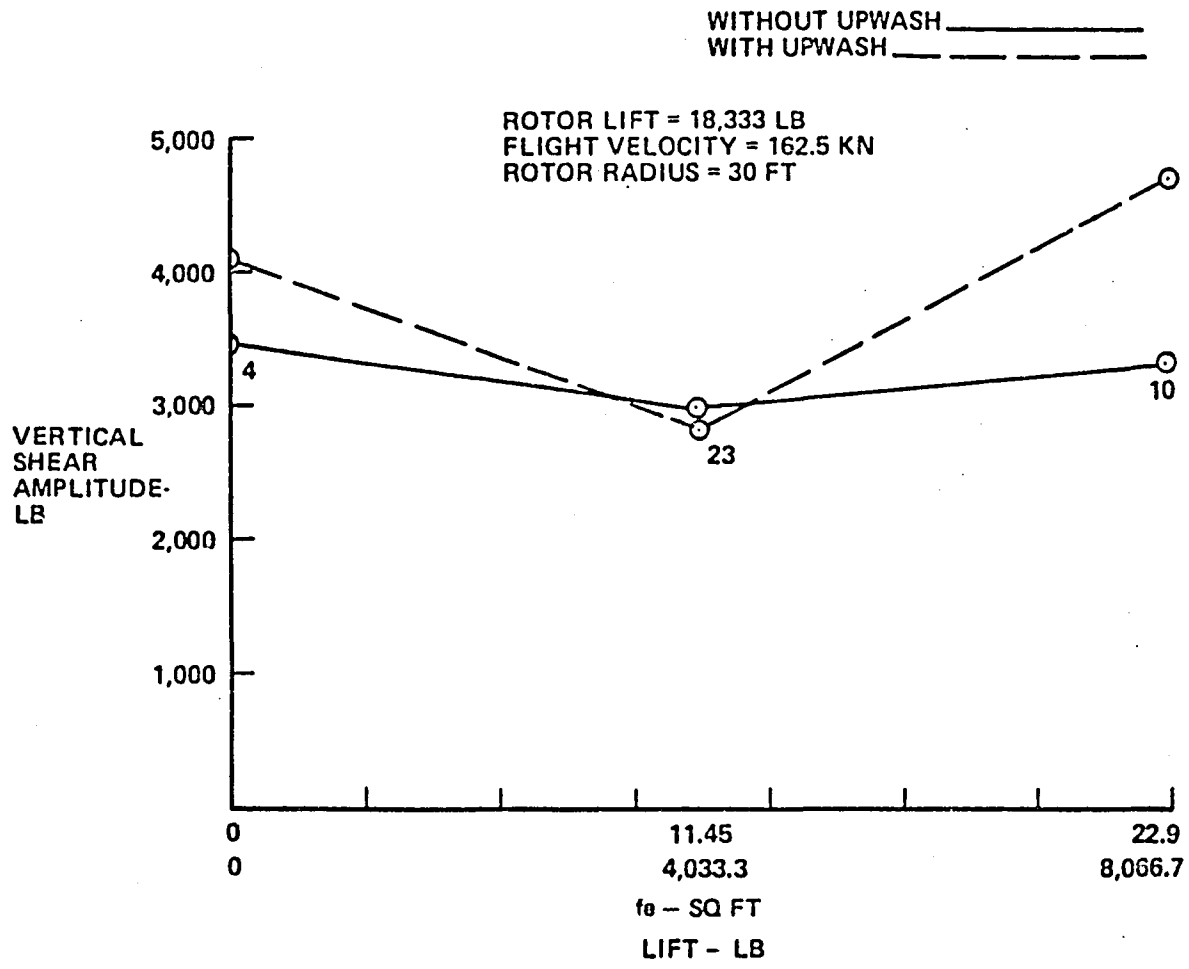


Figure 8-36. Variation of Flap Hinge Vertical Shear Vibratory Amplitude With Flat Plate Area for Auxiliary Thrust and Wing Lift From Loads Analysis. Rotor Lift, Flight Velocity, and Rotor Radius Are Held Constant. Numerals Near Symbols Indicate Flight Condition.

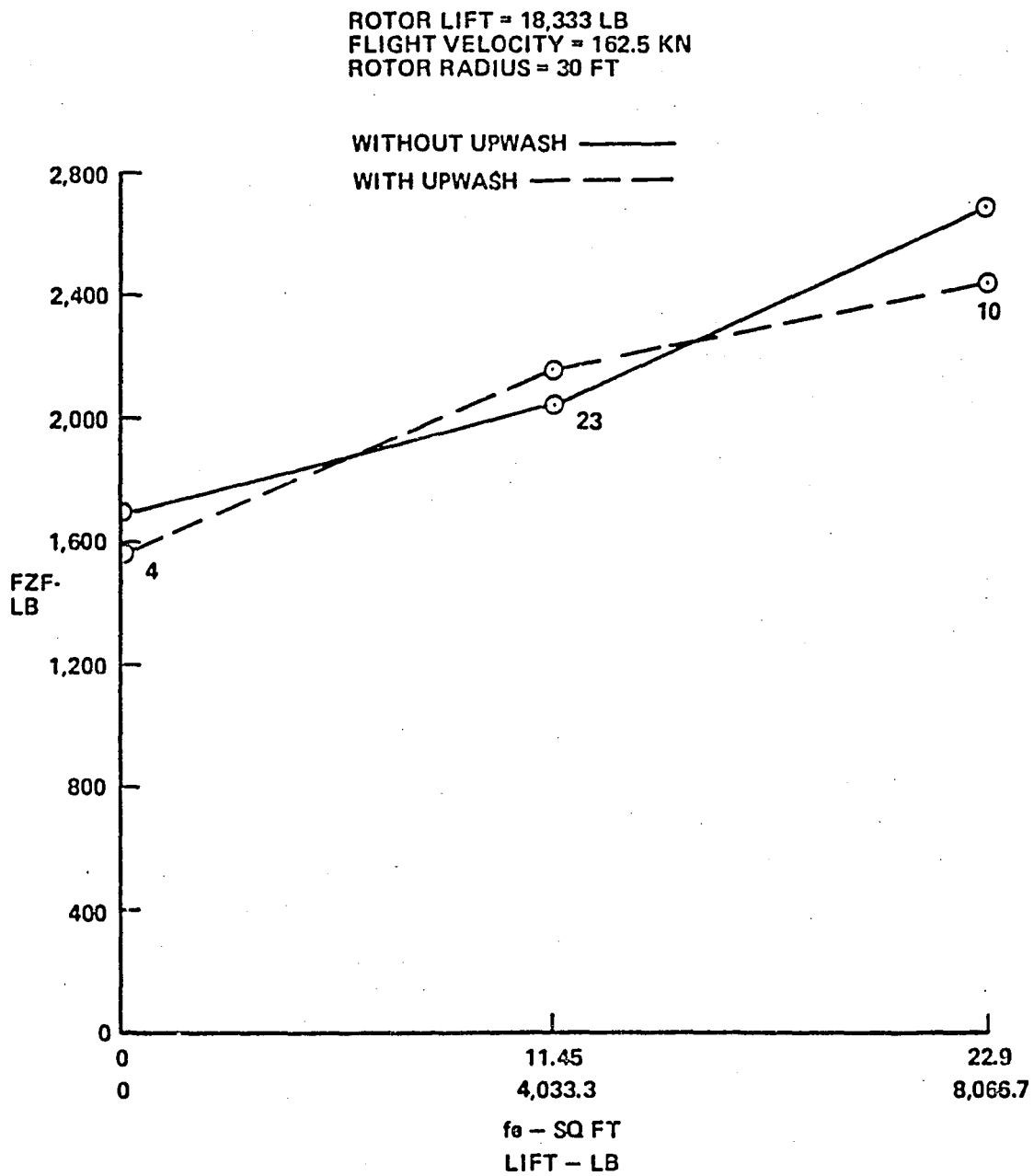


Figure 8-37. Variation of Vertical Hub Force Fourth Harmonic Amplitude With Flat Plate Area for Auxiliary Thrust and Wing Lift From Loads Analysis. Rotor Lift, Flight Velocity, and Rotor Radius Are Held Constant. Numerals Near Symbols Indicate Flight Condition.

WITHOUT UPWASH
WITH UPWASH

DISK LOAD = 9.34 LB/FT²
FLIGHT VELOCITY = 162.5 KN

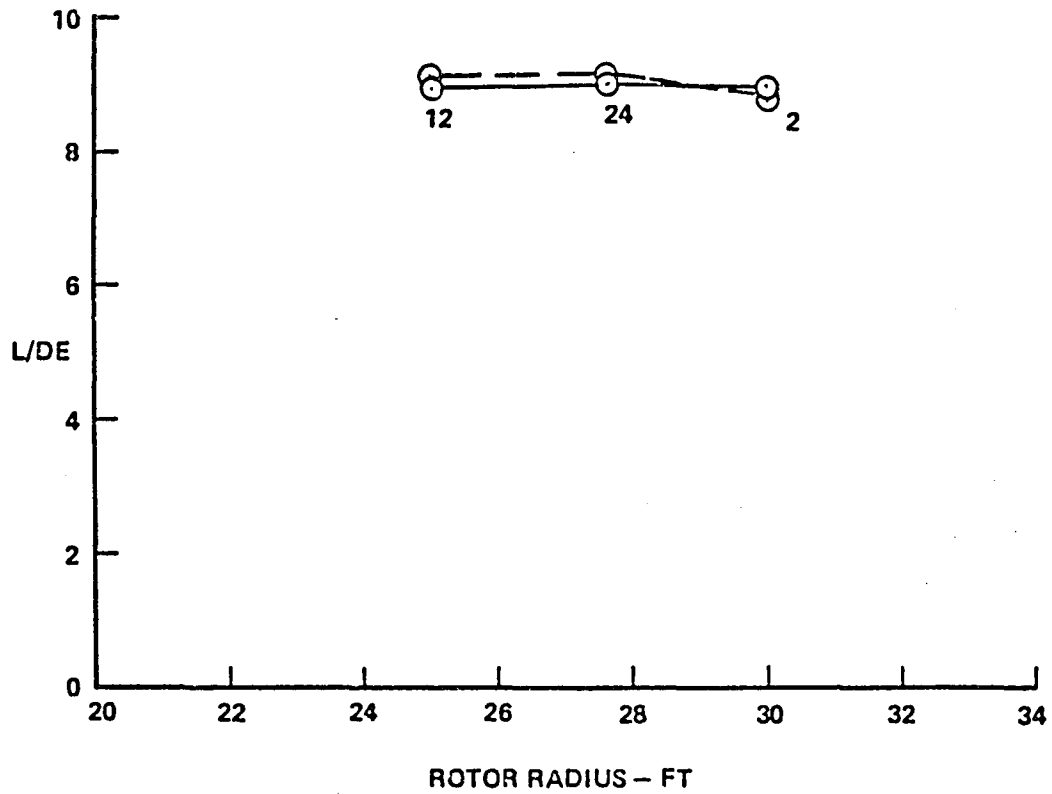


Figure 8-38. Variation of Equivalent Lift-to-Drag Ratio With Rotor Radius From Loads Analysis. Flight Velocity and Disk Loading Are Held Constant. Numerals Near Symbols Indicate Flight Condition.

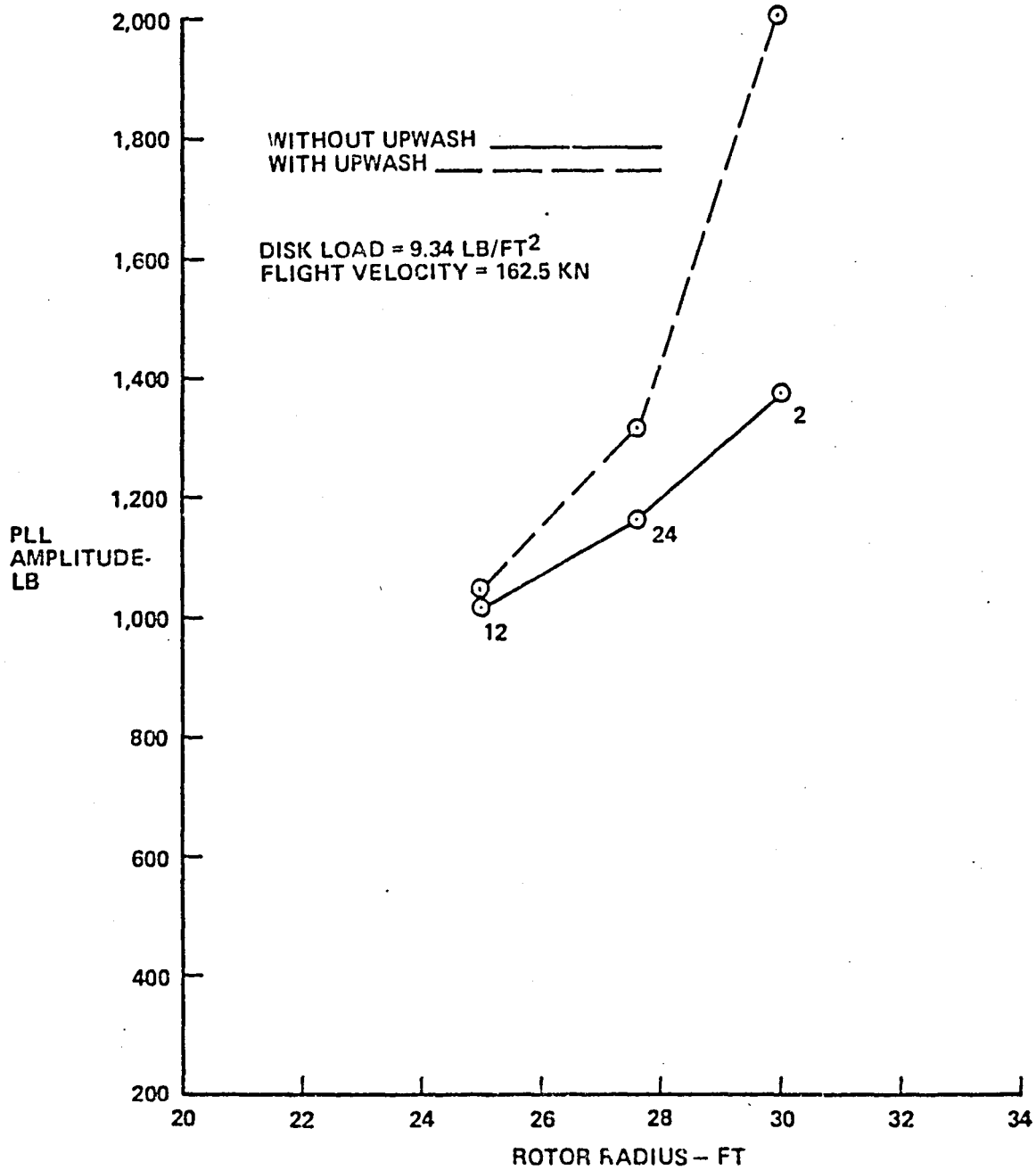


Figure 8-39. Variation of Pitch Link Load Vibratory Amplitude With Rotor Radius From Loads Analysis. Flight Velocity and Disk Loading Are Held Constant. Numerals Near Symbols Indicate Flight Condition.

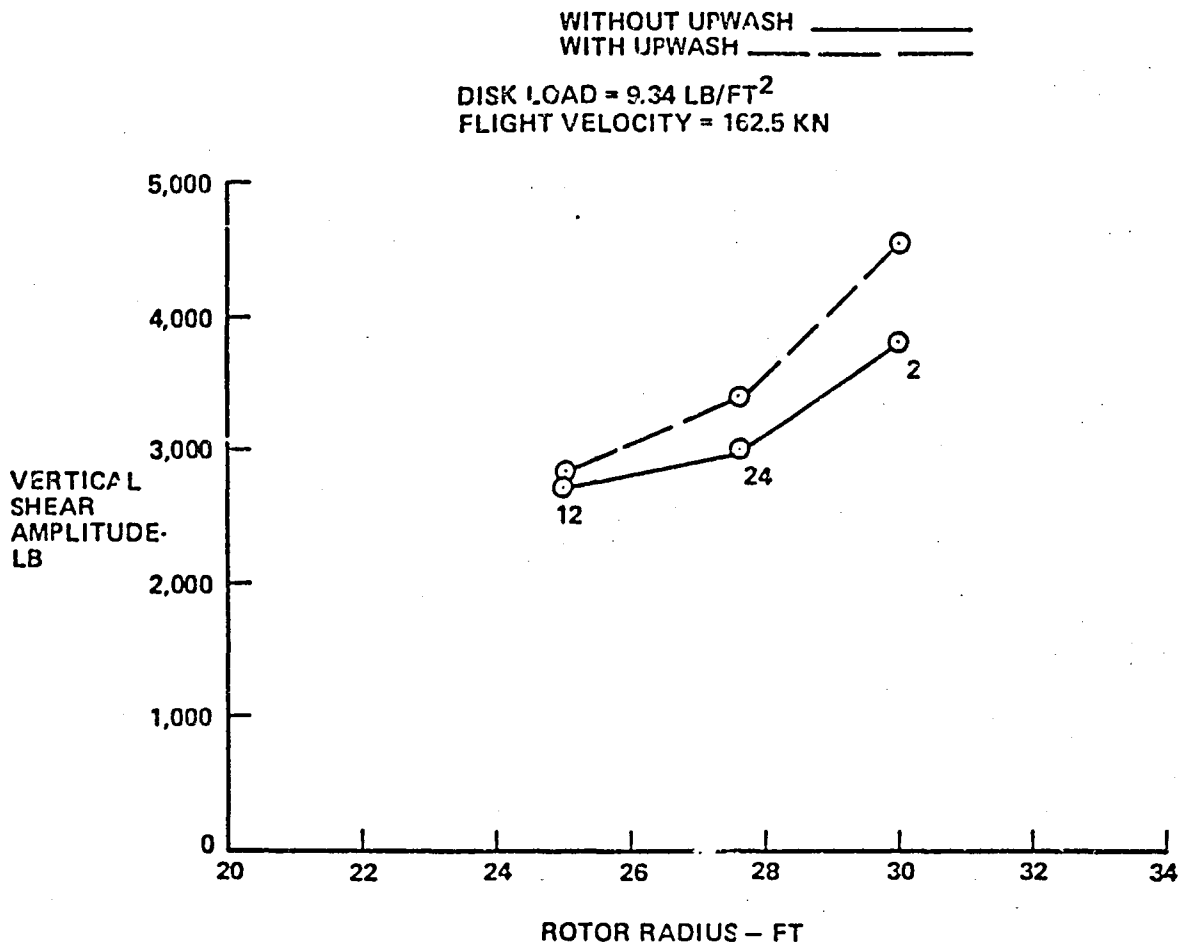


Figure 8-40. Variation of Flap Hinge Vertical Shear Vibratory Amplitude With Rotor Radius From Loads Analysis. Flight Velocity and Disk Loading Are Held Constant. Numerals Near Symbols Indicate Flight Condition.

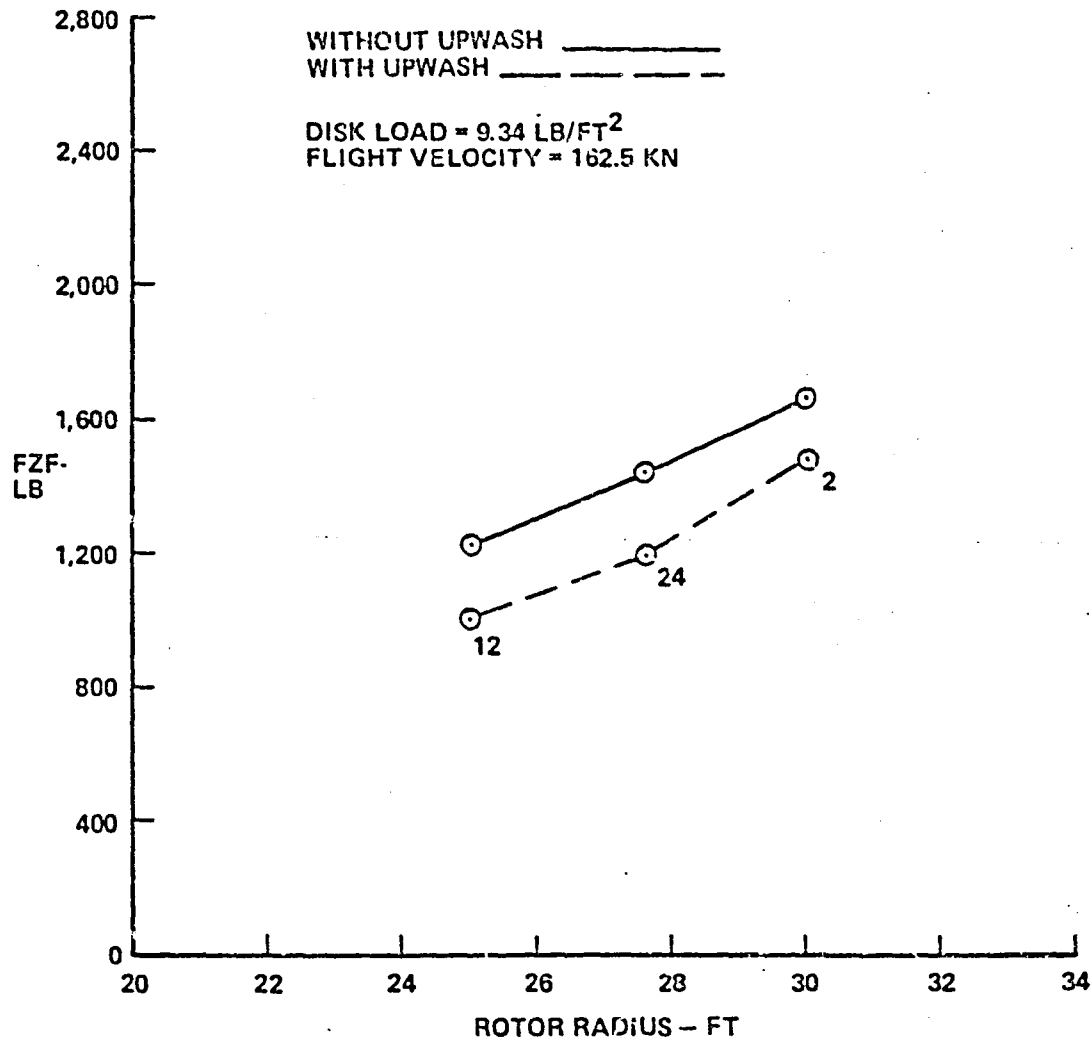


Figure 8-41. Variation of Vertical Hub Force Fourth Harmonic Amplitude With Rotor Radius From Loads Analysis. Flight Velocity and Disk Loading Are Held Constant. Numerals Near Symbols Indicate Flight Condition.

9.0 CONCLUSIONS AND RECOMMENDATIONS

It is obvious from the discussion and figures in Section 8.0 that the effects of upwash on the fuselage, wings, and/or engines of the RSRA reflect complicated flow interactions, not always lending themselves to simple or straightforward interpretation.

At any rate some generalizations can be stated. Upwash from the fuselage and auxiliary engines decreases the required rotor power and increases L/DE and the flap hinge vertical shear vibratory amplitude. The tip elastic twist deflection is most influenced by fuselage/wing/engine upwash at high as opposed to low flight velocities. Wing upwash decreases T_4/T_0 and Q_4/Q_0 . Fuselage/wing/engine upwash changes T_8/T_0 mainly at high flight velocities and decreases Q_8/Q_0 mainly at low flight velocities. The PLL amplitude is increased by fuselage/wing/engine upwash. Fuselage/wing upwash increases FZF, while fuselage or fuselage/engine upwash decreases it.

It is recommended that follow-on work focus on the interpretation of these effects.

10.0 REFERENCES

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2. Bain, L., and A. Landgrebe, "Investigation of Compound Helicopter Aerodynamic Interference Effects," USAAVLABS Technical Report 67-44, November 1967.
3. Saaris, G.R., and N.R. Vandevender, "TEA-230 Users's Manual - TEA-230 Computer Program for Solving Potential Flow About Arbitrary Configurations and Supporting Computer Programs," BCAC, Document No. D6-41081, Renton, Washington, November 1973.
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5. Tarzanin, F., and J. Ranieri, "Aeroelastic Rotor Analysis Program C-50," Boeing Report D210-10371, Philadelphia, Pa. Revised 1978.
6. Dadone, L., "U.S. Army Helicopter Design Datcom, Volume I, Airfoils," USAAMRDL CR 76-2 (NASA CR-153247), September 1976.

11.0 APPENDICES

APPENDIX A

Potential Flow Model Coordinates

This appendix contains the point coordinates which define the fuselage, wings, engines, fuselage wake, and engine exhausts as they occur in the six potential flow models used in this study. The point coordinates are contained in the input data sets used by the potential flow program, TEA-230, to determine the velocities induced by the fuselage/wings/engines at the rotor blade locations. The six input data sets, one for each potential flow model, are reproduced in this appendix.

The title in the second line of each data set identifies the potential flow model involved. Those models involving wings will have a wing incidence of 0° unless another incidence is indicated in this line.

The first line of each data set contains the word "CASE." The ninth line contains the first of the sets of point coordinates. These coordinates are, in order, station, butto line, waterline. They are all in inches and they define, for purposes of the potential flow program, the corners of quadrilaterals from which source panels are made. The product of the first two numbers in the eighth line indicates the number of sets of coordinate points that follow before another line similar to the eighth line is encountered. The number of groups indicated by lines similar to the eighth line is designated by the number in the seventh line. The totality of point coordinates defining the corners of quadrilaterals from which source panels are made is followed by another word, either "END" or "MULT." Most data following either of these words refer to vortices or reference dimensions.

CASE
 RSRA FUSELAGE ONLY
 J D COMAN BOEING VERTOL ORG 7440 X7834 M/S P32-74
 GEOM
 3.0000 288.0 1. -1.
 SOUR

| | | |
|-----------|----------|-----------|
| 6.0 | | |
| 7.00 | 4.00 | |
| 36.00000 | 0.0 | 95.89999 |
| 36.00000 | 0.0 | 95.89999 |
| 36.00000 | 0.0 | 95.89999 |
| 36.00000 | 0.0 | 95.89999 |
| 36.00000 | 0.0 | 95.89999 |
| 36.00000 | 0.0 | 95.89999 |
| 36.00000 | 0.0 | 95.89999 |
| 58.79999 | 0.0 | 110.20000 |
| 58.79999 | 16.29999 | 108.09999 |
| 58.79999 | 22.50000 | 106.00000 |
| 58.79999 | 22.50000 | 96.20000 |
| 58.79999 | 22.50000 | 86.39999 |
| 58.79999 | 16.89999 | 82.29999 |
| 58.79999 | 0.0 | 82.29999 |
| 81.50000 | 0.0 | 119.89999 |
| 81.50000 | 22.09999 | 116.39999 |
| 81.50000 | 29.50000 | 113.00000 |
| 81.50000 | 29.50000 | 99.00000 |
| 81.50000 | 29.50000 | 85.00000 |
| 81.50000 | 22.09999 | 78.09999 |
| 81.50000 | 0.0 | 78.09999 |
| 120.89999 | 0.0 | 147.59999 |
| 120.89999 | 28.39999 | 136.70000 |
| 120.89999 | 37.79999 | 125.89999 |
| 120.89999 | 37.79999 | 108.00000 |
| 120.89999 | 37.79999 | 90.70000 |
| 120.89999 | 28.39999 | 74.79999 |
| 120.89999 | 0.0 | 74.79999 |
| 7.00 | 13.00 | |
| 120.89999 | 0.0 | 147.59999 |
| 120.89999 | 28.39999 | 136.70000 |
| 120.89999 | 37.79999 | 125.89999 |
| 120.89999 | 37.79999 | 108.00000 |
| 120.89999 | 37.79999 | 90.70000 |
| 120.89999 | 28.39999 | 74.79999 |
| 120.89999 | 0.0 | 74.79999 |
| 133.00000 | 0.0 | 148.89999 |
| 133.00000 | 29.20000 | 148.89999 |
| 133.00000 | 38.89999 | 129.89999 |
| 133.00000 | 38.89999 | 110.79999 |
| 133.00000 | 38.89999 | 91.79999 |
| 133.00000 | 29.20000 | 72.79999 |
| 133.00000 | 0.0 | 72.79999 |
| 175.29999 | 12.10000 | 148.89999 |
| 175.29999 | 29.20000 | 148.89999 |
| 175.29999 | 38.89999 | 129.89999 |
| 175.29999 | 38.89999 | 110.79999 |
| 175.29999 | 38.89999 | 91.79999 |

| | | |
|-----------|----------|-----------|
| 175.29999 | 29.20000 | 72.79999 |
| 175.29999 | 0.0 | 72.79999 |
| 209.29999 | 21.89999 | 148.89999 |
| 209.29999 | 29.20000 | 148.89999 |
| 209.29999 | 38.89999 | 129.89999 |
| 209.29999 | 38.89999 | 110.79999 |
| 209.29999 | 38.89999 | 91.79999 |
| 209.29999 | 29.20000 | 72.79999 |
| 209.29999 | 0.0 | 72.79999 |
| 222.29999 | 22.70000 | 148.89999 |
| 222.29999 | 29.20000 | 148.89999 |
| 222.29999 | 38.89999 | 129.89999 |
| 222.29999 | 38.89999 | 110.79999 |
| 222.29999 | 38.89999 | 91.79999 |
| 222.29999 | 29.20000 | 72.79999 |
| 222.29999 | 0.0 | 72.79999 |
| 271.00000 | 22.70000 | 148.89999 |
| 271.00000 | 29.20000 | 148.89999 |
| 271.00000 | 38.89999 | 129.89999 |
| 271.00000 | 38.89999 | 110.79999 |
| 271.00000 | 38.89999 | 91.79999 |
| 271.00000 | 29.20000 | 72.79999 |
| 271.00000 | 0.0 | 72.79999 |
| 300.00000 | 22.70000 | 148.89999 |
| 300.00000 | 29.20000 | 148.89999 |
| 300.00000 | 38.89999 | 129.89999 |
| 300.00000 | 38.89999 | 110.79999 |
| 300.00000 | 38.89999 | 91.79999 |
| 300.00000 | 29.20000 | 72.79999 |
| 300.00000 | 0.0 | 72.79999 |
| 376.59985 | 17.79999 | 148.89999 |
| 376.59985 | 29.20000 | 148.89999 |
| 376.59985 | 38.89999 | 129.89999 |
| 376.59985 | 38.89999 | 110.79999 |
| 376.59985 | 38.89999 | 91.79999 |
| 376.59985 | 29.20000 | 72.79999 |
| 376.59985 | 0.0 | 72.79999 |
| 391.69995 | 15.70000 | 147.29999 |
| 391.69995 | 28.00000 | 147.29999 |
| 391.69995 | 37.29999 | 129.00000 |
| 391.69995 | 37.29999 | 110.79999 |
| 391.69995 | 37.29999 | 92.59999 |
| 391.69995 | 28.00000 | 74.39999 |
| 391.69995 | 0.0 | 74.39999 |
| 445.69995 | 7.87174 | 143.45999 |
| 445.69995 | 24.50000 | 143.45999 |
| 445.69995 | 32.70000 | 127.20000 |
| 445.69995 | 32.70000 | 110.79999 |
| 445.69995 | 32.70000 | 94.39999 |
| 445.69995 | 24.50000 | 77.79999 |
| 445.69995 | 0.0 | 77.79999 |
| 500.00000 | 0.0 | 139.59999 |
| 500.00000 | 21.00000 | 139.59999 |
| 500.00000 | 28.00000 | 125.39999 |
| 500.00000 | 28.00000 | 110.79999 |
| 500.00000 | 28.00000 | 96.20000 |
| 500.00000 | 21.00000 | 81.29999 |
| 500.00000 | 0.0 | 81.29999 |
| 600.00000 | 0.0 | 131.00000 |
| 600.00000 | 13.50000 | 121.00000 |

| | | |
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| 600.00000 | 18.00000 | 120.89999 |
| 600.00000 | 18.00000 | 110.79999 |
| 600.00000 | 18.00000 | 100.39999 |
| 600.00000 | 13.50000 | 89.89999 |
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| 1000.00000 | 0.0 | 131.00000 |
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| 1000.00000 | 18.00000 | 120.89999 |
| 1000.00000 | 18.00000 | 110.79999 |
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| 133.00000 | 0.0 | 148.89999 |
| 133.00000 | 0.0 | 148.89999 |
| 133.00000 | 0.0 | 148.89999 |
| 133.00000 | 0.0 | 148.89999 |
| 133.00000 | 0.0 | 148.89999 |
| 133.00000 | 0.0 | 148.89999 |
| 175.29999 | 0.0 | 165.89999 |
| 175.29999 | 8.10000 | 165.89999 |
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| 175.29999 | 12.10000 | 161.39999 |
| 175.29999 | 12.10000 | 157.39999 |
| 175.29999 | 12.10000 | 153.79999 |
| 175.29999 | 12.10000 | 148.89999 |
| 209.29999 | 0.0 | 179.70000 |
| 209.29999 | 14.60000 | 179.70000 |
| 209.29999 | 21.09999 | 175.50000 |
| 209.29999 | 22.00000 | 171.59999 |
| 209.29999 | 22.00000 | 164.29999 |
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| 209.29999 | 21.89999 | 148.89999 |
| 222.29999 | 0.0 | 181.29999 |
| 222.29999 | 19.59999 | 181.29999 |
| 222.29999 | 22.70000 | 181.29999 |
| 222.29999 | 22.70000 | 174.79999 |
| 222.29999 | 22.70000 | 166.39999 |
| 222.29999 | 22.70000 | 158.89999 |
| 222.29999 | 22.70000 | 148.89999 |
| 271.00000 | 0.0 | 189.20000 |
| 271.00000 | 19.59999 | 189.20000 |
| 271.00000 | 22.70000 | 189.20000 |
| 271.00000 | 22.70000 | 181.09999 |
| 271.00000 | 22.70000 | 173.70000 |
| 271.00000 | 22.70000 | 161.39999 |
| 271.00000 | 22.70000 | 148.89999 |
| 300.00000 | 0.0 | 193.79999 |
| 300.00000 | 19.59999 | 193.79999 |
| 300.00000 | 22.70000 | 193.79999 |
| 300.00000 | 22.70000 | 184.79999 |
| 300.00000 | 22.70000 | 173.29999 |
| 300.00000 | 22.70000 | 163.00000 |
| 300.00000 | 22.70000 | 148.89999 |
| 348.59985 | 0.0 | 196.39999 |
| 348.59985 | 16.89999 | 196.39999 |
| 348.59985 | 19.59109 | 196.39999 |
| 348.59985 | 19.59109 | 186.89999 |
| 348.59985 | 19.59109 | 174.59999 |

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| 348.59985 | 19.59109 | 163.59999 |
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| 376.59985 | 0.0 | 188.09999 |
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| 376.59985 | 17.79999 | 148.89999 |
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| 391.69995 | 15.70000 | 158.29999 |
| 391.69995 | 15.70000 | 147.29999 |
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| 120.89999 | -28.39999 | 136.70000 |
| 120.89999 | 0.0 | 147.59999 |

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| 175.29999 | -38.89999 | 91.79999 |
| 175.29999 | -38.89999 | 110.79999 |
| 175.29999 | -38.89999 | 129.89999 |
| 175.29999 | -29.20000 | 148.89999 |
| 175.29999 | -12.10000 | 148.89999 |
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| 209.29999 | -29.20000 | 72.79999 |
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| 209.29999 | -38.89999 | 110.79999 |
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| 209.29999 | -29.20000 | 148.89999 |
| 209.29999 | -21.89999 | 148.89999 |
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| 376.60010 | -38.89999 | 110.79999 |
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| 376.60010 | -29.20000 | 148.89999 |
| 376.60010 | -17.79999 | 148.89999 |
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| 391.69995 | -28.00000 | 74.39999 |
| 391.69995 | -37.29999 | 92.59999 |
| 391.69995 | -37.29999 | 110.79999 |
| 391.69995 | -37.29999 | 129.00000 |
| 391.69995 | -28.00000 | 147.29999 |
| 391.69995 | -15.70000 | 147.29999 |
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| 445.69995 | -24.50000 | 77.79999 |
| 445.69995 | -32.70000 | 94.39999 |
| 445.69995 | -32.70000 | 110.79999 |

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| 445.69995 | -32.70000 | 127.20000 |
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| 445.69995 | -7.87174 | 143.45999 |
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| 500.00000 | -28.00000 | 110.79999 |
| 500.00000 | -28.00000 | 125.39999 |
| 500.00000 | -21.00000 | 139.59999 |
| 500.00000 | 0.0 | 139.59999 |
| 600.00000 | 0.0 | 89.89999 |
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| 600.00000 | -18.00000 | 100.39999 |
| 600.00000 | -18.00000 | 110.79999 |
| 600.00000 | -18.00000 | 120.89999 |
| 600.00000 | -13.50000 | 131.00000 |
| 600.00000 | 0.0 | 131.00000 |
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| 1000.00000 | -18.00000 | 110.79999 |
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| | 7.00 | 10.00 |
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| 133.00000 | 0.0 | 148.89999 |
| 133.00000 | 0.0 | 148.39999 |
| 133.00000 | 0.0 | 148.89999 |
| 133.00000 | 0.0 | 148.39999 |
| 133.00000 | 0.0 | 148.89999 |
| 133.00000 | 0.0 | 148.89999 |
| 175.29999 | -12.10000 | 148.89999 |
| 175.29999 | -12.10000 | 153.79999 |
| 175.29999 | -12.10000 | 157.39999 |
| 175.29999 | -12.10000 | 161.39999 |
| 175.29999 | -11.70000 | 163.59999 |
| 175.29999 | -8.10000 | 165.89999 |
| 175.29999 | 0.0 | 165.89999 |
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| 209.29999 | -20.20000 | 157.79999 |
| 209.29999 | -22.00000 | 164.29999 |
| 209.29999 | -22.00000 | 171.59999 |
| 209.29999 | -21.09999 | 175.50000 |
| 209.29999 | -14.60000 | 179.70000 |
| 209.29999 | 0.0 | 179.70000 |
| 222.29999 | -22.70000 | 148.39999 |
| 222.29999 | -22.70000 | 158.89999 |
| 222.29999 | -22.70000 | 166.39999 |
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| 222.29999 | -22.70000 | 181.29999 |
| 222.29999 | -19.59999 | 181.29999 |
| 222.29999 | 0.0 | 181.29999 |
| 271.00000 | -22.70000 | 148.89999 |
| 271.00000 | -22.70000 | 161.39999 |
| 271.00000 | -22.70000 | 170.70000 |
| 271.00000 | -22.70000 | 181.09999 |
| 271.00000 | -22.70000 | 189.20000 |
| 271.00000 | -19.59999 | 189.20000 |
| 271.00000 | 0.0 | 189.20000 |

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| 300.00000 | -22.70000 | 148.89999 |
| 300.00000 | -22.70000 | 163.00000 |
| 300.00000 | -22.70000 | 173.29999 |
| 300.00000 | -22.70000 | 184.79999 |
| 300.00000 | -22.70000 | 193.79999 |
| 300.00000 | -19.59999 | 193.79999 |
| 300.00000 | 0.0 | 193.79999 |
| 348.60010 | -19.59109 | 148.89999 |
| 348.60010 | -19.59109 | 163.59999 |
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| 348.60010 | -19.59109 | 196.39999 |
| 348.60010 | -16.89999 | 196.39999 |
| 348.60010 | 0.0 | 196.39999 |
| 376.60010 | -17.79999 | 148.89999 |
| 376.60010 | -17.79999 | 161.00000 |
| 376.60010 | -17.79999 | 170.09999 |
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| 376.60010 | -17.79999 | 188.09999 |
| 376.60010 | -15.30000 | 188.09999 |
| 376.60010 | 0.0 | 188.09999 |
| 391.69995 | -15.70000 | 147.29999 |
| 391.69995 | -15.70000 | 158.29999 |
| 391.69995 | -15.70000 | 166.50000 |
| 391.69995 | -15.70000 | 175.79999 |
| 391.69995 | -15.70000 | 182.89999 |
| 391.69995 | -13.50000 | 182.89999 |
| 391.69995 | 0.0 | 182.89999 |
| 500.00000 | 0.0 | 139.59999 |
| 500.00000 | 0.0 | 139.59999 |
| 500.00000 | 0.0 | 139.59999 |
| 500.00000 | 0.0 | 139.59999 |
| 500.00000 | 0.0 | 139.59999 |
| 500.00000 | 0.0 | 139.59999 |
| 500.00000 | 0.0 | 139.59999 |

END
AERO

| | | | | | | |
|-------|----|-------|--------|------|-------|----|
| 0. | 0. | 0. | | | | |
| FORC | | | | | | |
| 307.5 | 0. | 75.52 | 52112. | 98.1 | 531.2 | 0. |
| END | | | | | | |

CASE
 RSRA FUSELAGE AND WINGS
 J D COWAN AERO RESEARCH ORGN 7440 EXT 3871

GEOM
 3. 634. 1. -1.

SOUR
 16.
 7.
 36. 0. 95.9
 36. 0. 95.9
 36. 0.0 95.9
 36. 0.0 95.9
 36. 0.0 95.9
 36. 0.0 95.9
 36. 0.0 95.9
 36. 0.0 95.9
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 58.8 16.9 108.1
 58.8 22.5 106.
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 81.5 0.0 119.9
 81.5 22.1 116.4
 81.5 29.5 113.
 81.5 29.5 99.
 81.5 29.5 85.
 81.5 22.1 78.1
 81.5 0.0 78.1
 120.9 0. 147.6
 120.9 28.4 136.7
 120.9 37.8 125.9
 120.9 37.8 108.
 120.9 37.8 90.7
 120.9 28.4 74.8
 120.9 0. 74.8
 7.
 120.9 0. 147.6
 120.9 28.4 136.7
 120.9 37.8 125.9
 120.9 37.8 108.
 120.9 37.8 90.7
 120.9 28.4 74.8
 120.9 0. 74.8
 133. 0. 148.9
 133. 12. 148.9
 133. 29.2 129.9
 133. 38.9 110.8
 133. 38.9 91.3
 133. 38.9 72.8
 133. 38.9 72.8
 175.3 12.1 148.9
 175.3 29.2 148.9
 175.3 38.9 129.9
 175.3 38.9 110.8
 175.3 38.9 91.3

ORIGINAL PAGE
OF POOR QUALITY

| | | |
|-------|----------|--------|
| 175.3 | 29.2 | 72.8 |
| 175.3 | 0. | 72.8 |
| 209.3 | 21.9 | 148.9 |
| 209.3 | 21.2 | 148.9 |
| 209.3 | 38.9 | 129.9 |
| 209.3 | 38.9 | 110.8 |
| 209.3 | 38.9 | 91.8 |
| 209.3 | 29.2 | 72.8 |
| 209.3 | 0. | 72.8 |
| 222.3 | 22.7 | 148.9 |
| 222.3 | 29.2 | 148.9 |
| 222.3 | 38.9 | 129.9 |
| 222.3 | 38.9 | 110.8 |
| 222.3 | 38.9 | 91.8 |
| 222.3 | 29.2 | 72.8 |
| 222.3 | 0. | 72.8 |
| 271. | 22.7 | 148.9 |
| 271. | 29.2 | 148.9 |
| 271. | 38.9 | 129.9 |
| 271. | 38.9 | 110.8 |
| 271. | 38.9 | 91.8 |
| 271. | 29.2 | 72.8 |
| 271. | 0. | 72.8 |
| 6. | 4. | |
| 271. | 22.7 | 148.9 |
| 271. | 29.2 | 148.9 |
| 271. | 38.9 | 129.9 |
| 271. | 38.9 | 110.8 |
| 271. | 38.9 | 91.8 |
| 271. | 29.2 | 72.8 |
| 300. | 22.7 | 148.9 |
| 300. | 29.2 | 148.9 |
| 300. | 38.9 | 129.9 |
| 300. | 38.9 | 110.8 |
| 300. | 38.9 | 91.8 |
| 300. | 38.9 | 85. |
| 376.6 | 17.8 | 148.9 |
| 376.6 | 22.2 | 148.9 |
| 376.6 | 38.9 | 129.9 |
| 376.6 | 38.9 | 110.8 |
| 376.6 | 38.9 | 91.8 |
| 376.6 | 38.9 | 85. |
| 391.7 | 15.7 | 147.3 |
| 391.7 | 28. | 147.3 |
| 391.7 | 37.3 | 129. |
| 391.7 | 37.3 | 110.8 |
| 391.7 | 37.3 | 92.6 |
| 391.7 | 28. | 74.4 |
| 7 | 5. | |
| 391.7 | 15.7 | 147.3 |
| 391.7 | 28. | 147.3 |
| 391.7 | 37.3 | 129. |
| 391.7 | 37.3 | 110.8 |
| 391.7 | 37.3 | 92.6 |
| 391.7 | 28. | 74.4 |
| 391.7 | 0. | 74.4 |
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| 445.7 | 24.5 | 143.46 |
| 445.7 | 32.7 | 121.2 |
| 445.7 | 32.7 | 110.8 |

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| 445.7 | 32.7 | 94.4 |
| 445.7 | 24.5 | 77.8 |
| 445.7 | 0. | 77.8 |
| 500. | 0. | 139.6 |
| 500. | 21. | 139.6 |
| 500. | 28. | 125.4 |
| 500. | 28. | 110.8 |
| 500. | 28. | 96.2 |
| 500. | 21. | 81.3 |
| 500. | 0. | 81.3 |
| 600. | 0. | 131. |
| 600. | 13.5 | 131. |
| 600. | 18. | 120.9 |
| 600. | 18. | 110.8 |
| 600. | 18. | 100.4 |
| 600. | 13.5 | 89.9 |
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| 1000. | 0. | 131. |
| 1000. | 13.5 | 131. |
| 1000. | 18. | 120.9 |
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| 1000. | 13.5 | 89.9 |
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| 7. | 10. | |
| 133. | 0. | 148.9 |
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| 133. | 0. | 148.9 |
| 133. | 0. | 148.9 |
| 133. | 0. | 148.9 |
| 175.3 | 0. | 165.9 |
| 175.3 | 8.1 | 165.9 |
| 175.3 | 11.7 | 163.6 |
| 175.3 | 12.1 | 161.4 |
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| 175.3 | 12.1 | 153.8 |
| 175.3 | 12.1 | 148.9 |
| 209.3 | 0. | 179.7 |
| 209.3 | 14.6 | 179.7 |
| 209.3 | 21.1 | 175.5 |
| 209.3 | 22. | 171.6 |
| 209.3 | 22. | 164.3 |
| 209.3 | 20.2 | 157.8 |
| 209.3 | 21.9 | 148.9 |
| 222.3 | 0. | 181.3 |
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| 222.3 | 22.7 | 181.3 |
| 222.3 | 22.7 | 174.8 |
| 222.3 | 22.7 | 166.4 |
| 222.3 | 22.7 | 158.9 |
| 222.3 | 22.7 | 148.9 |
| 271. | 0. | 189.2 |
| 271. | 19.6 | 189.2 |
| 271. | 22.7 | 189.2 |
| 271. | 22.7 | 181.1 |
| 271. | 22.7 | 170.7 |
| 271. | 22.7 | 161.4 |
| 271. | 22.7 | 148.9 |

| | | |
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| 300. | 19.6 | 193.8 |
| 300. | 22.7 | 193.8 |
| 300. | 22.7 | 184.8 |
| 300. | 22.7 | 173.3 |
| 300. | 22.7 | 163. |
| 300. | 22.7 | 148.9 |
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| 348.6 | 16.9 | 196.4 |
| 348.6 | 19.5911 | 196.4 |
| 348.6 | 19.5911 | 186.9 |
| 348.6 | 19.5911 | 174.6 |
| 348.6 | 19.5911 | 163.6 |
| 348.6 | 19.5911 | 148.9 |
| 376.6 | 0. | 188.1 |
| 376.6 | 15.3 | 188.1 |
| 376.6 | 17.8 | 188.1 |
| 376.6 | 17.8 | 180.3 |
| 376.6 | 17.8 | 170.1 |
| 376.6 | 17.8 | 161.0 |
| 376.6 | 17.8 | 148.9 |
| 391.7 | 0. | 182.9 |
| 391.7 | 13.5 | 182.9 |
| 391.7 | 15.7 | 182.9 |
| 391.7 | 15.7 | 175.8 |
| 391.7 | 15.7 | 166.5 |
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| 391.7 | 15.7 | 147.3 |
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| 500. | 0. | 139.6 |
| 500. | 0. | 139.6 |
| 500. | 0. | 139.6 |
| 500. | 0. | 139.6 |
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| 500. | 0. | 139.6 |

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| 36. | 0. | 95.9 | |
| 36.0000 | -0.0000 | 95.9000 | |
| 36.0000 | -0.0000 | 95.9000 | |
| 36.0000 | -0.0000 | 95.9000 | |
| 36.0000 | -0.0000 | 95.9000 | |
| 36.0000 | -0.0000 | 95.9000 | |
| 58.8000 | -0.0000 | 82.3000 | |
| 58.8 | -16.9 | 82.3 | |
| 58.8000 | -22.5000 | 86.4000 | |
| 58.8000 | -22.5000 | 96.2000 | |
| 58.8000 | -22.5000 | 106.0000 | |
| 58.8 | -16.9 | 108.1 | |
| 58.8000 | -0.0000 | 110.2000 | |
| 81.5000 | -0.0000 | 78.1000 | |
| 81.5 | -22.1 | 78.1 | |
| 81.5000 | -29.5000 | 85.0000 | |
| 81.5000 | -29.5000 | 99.0000 | |
| 81.5000 | -29.5000 | 113.0000 | |
| 81.5 | -22.1 | 116.4 | |
| 81.5000 | -0.0000 | 119.9000 | |
| 120.9000 | -0.0000 | 74.8000 | |
| 120.9 | -28.4 | 74.8 | |
| 120.9000 | -37.8000 | 90.7000 | |

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| 120.9000 | -37.8000 | 108. |
| 120.9000 | -37.8000 | 125.9000 |
| 120.9 | -28.4 | 136.7 |
| 120.9000 | -0.0000 | 147.6000 |
| 7.0 | 6. | |
| 120.9000 | -0.0000 | 74.8000 |
| 120.9000 | -28.4000 | 74.8000 |
| 120.9000 | -37.8000 | 90.7000 |
| 120.9000 | -37.8000 | 108. |
| 120.9000 | -37.3000 | 125.9000 |
| 120.9000 | -28.4000 | 136.7000 |
| 120.9000 | -0.0000 | 147.6000 |
| 133.0000 | -0.0000 | 72.8000 |
| 133.0000 | -29.2000 | 72.8000 |
| 133.0000 | -38.9000 | 91.8000 |
| 133.0000 | -38.9000 | 110.8000 |
| 133.0000 | -38.9000 | 129.9000 |
| 133.0000 | -29.2000 | 148.9000 |
| 133.0000 | -0.0000 | 148.9000 |
| 175.3000 | -0.0000 | 72.8000 |
| 175.3000 | -29.2000 | 72.8000 |
| 175.3000 | -38.9000 | 91.8000 |
| 175.3000 | -38.9000 | 110.8000 |
| 175.3000 | -38.9000 | 129.9000 |
| 175.3000 | -29.2000 | 148.9000 |
| 175.3000 | -12.1000 | 148.9000 |
| 209.3000 | -0.0000 | 72.8000 |
| 209.3000 | -29.2000 | 72.8000 |
| 209.3000 | -38.9000 | 91.8000 |
| 209.3000 | -38.9000 | 110.8000 |
| 209.3000 | -38.9000 | 129.9000 |
| 209.3000 | -29.2000 | 148.9000 |
| 209.3000 | -21.9000 | 148.9000 |
| 222.3000 | -0.0000 | 72.8000 |
| 222.3000 | -29.2000 | 72.8000 |
| 222.3000 | -38.9000 | 91.8000 |
| 222.3000 | -38.9000 | 110.8000 |
| 222.3000 | -38.9000 | 129.9000 |
| 222.3000 | -9.2000 | 148.9000 |
| 222.3000 | -22.7000 | 148.9000 |
| 271.0000 | -0.0000 | 72.8000 |
| 271.0000 | -29.2000 | 72.8000 |
| 271.0000 | -38.9000 | 91.8000 |
| 271.0000 | -38.9000 | 110.8000 |
| 271.0000 | -38.9000 | 129.9000 |
| 271.0000 | -29.2000 | 148.9000 |
| 271. | -22.7 | 148.9000 |
| 6. | 4. | |
| 271.0000 | -29.2000 | 72.8 |
| 271.0000 | -38.9000 | 91.8 |
| 271.0000 | -38.9000 | 110.8000 |
| 271.0000 | -38.9000 | 129.9000 |
| 271.0000 | -29.2000 | 148.9000 |
| 271.0000 | -22.7000 | 148.9000 |
| 300. | -38.9 | 85. |
| 300. | -38.9 | 91.8 |
| 300. | -38.9 | 110.8 |
| 300. | -38.9 | 129.9 |
| 300. | -29.2 | 148.9 |
| 300. | -22.7 | 148.9 |

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| 376.6 | -38.9 | 85. |
| 376.6 | -38.9 | 91.8 |
| 376.6 | -38.9 | 110.8 |
| 376.6 | -38.9 | 129.9 |
| 376.6 | -29.2 | 148.9 |
| 376.6 | -17.8 | 148.9 |
| 391.7 | -28. | 74.4 |
| 391.7 | -37.3 | 92.6 |
| 391.7 | -37.3 | 110.8 |
| 391.7 | -37.3 | 129. |
| 391.7 | -28. | 147.3 |
| 391.7 | -15.7 | 147.3 |
| 7. | 5. | |
| 391.7000 | -0.0000 | 74.4000 |
| 391.7000 | -28.0000 | 74.4000 |
| 391.7000 | -37.3000 | 92.6000 |
| 391.7000 | -37.3000 | 110.8000 |
| 391.7000 | -37.3000 | 129.0000 |
| 391.7000 | -28.0000 | 147.3000 |
| 391.7000 | -15.7000 | 147.3000 |
| 445.7000 | -0.0000 | 77.8000 |
| 445.7000 | -24.5000 | 77.8000 |
| 445.7000 | -32.7000 | 94.4000 |
| 445.7000 | -32.7000 | 110.8000 |
| 445.7000 | -32.7000 | 127.2000 |
| 445.7000 | -24.5000 | 143.4600 |
| 445.7000 | -7.871745 | 143.4600 |
| 500.0000 | -0.0000 | 81.3000 |
| 500.0000 | -21.0000 | 81.3000 |
| 500.0000 | -28.0000 | 96.2000 |
| 500.0000 | -28.0000 | 110.8000 |
| 500.0000 | -28.0000 | 125.4000 |
| 500.0000 | -21.0000 | 139.6000 |
| 500.0000 | -0.0000 | 139.6000 |
| 600.0000 | -0.0000 | 89.9000 |
| 600.0000 | -13.5000 | 89.9000 |
| 600.0000 | -18.0000 | 100.4000 |
| 600.0000 | -18.0000 | 110.8000 |
| 600.0000 | -18.0000 | 120.9000 |
| 600.0000 | -13.5000 | 131.0000 |
| 600.0000 | -0.0000 | 131.0000 |
| 1000.0000 | -0.0000 | 89.9000 |
| 1000.0000 | -13.5000 | 89.9000 |
| 1000.0000 | -18.0000 | 100.4000 |
| 1000.0000 | -18.0000 | 110.8000 |
| 1000.0000 | -18.0000 | 120.9000 |
| 1000.0000 | -13.5000 | 131.0000 |
| 1000.0000 | -0.0000 | 131.0000 |
| 7.0 | 10.0 | |
| 133.0000 | -0.0000 | 148.9000 |
| 133.0000 | -0.0000 | 148.9000 |
| 133.0000 | -0.0000 | 148.9000 |
| 133.0000 | -0.0000 | 148.9000 |
| 133.0000 | -0.0000 | 148.9000 |
| 133.0000 | -0.0000 | 148.9000 |
| 133.0000 | -0.3000 | 148.9000 |
| 175.3000 | -12.1000 | 148.9000 |
| 175.3000 | -12.1000 | 153.8000 |
| 175.3000 | -12.1000 | 157.4600 |
| 175.3000 | -12.1000 | 161.4000 |

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| 175.3000 | -11.7000 | 163.6000 |
| 175.3000 | -8.1000 | 165.9000 |
| 175.3000 | -0.0000 | 165.9000 |
| 209.3000 | -21.9000 | 148.9000 |
| 209.3000 | -20.2000 | 157.8000 |
| 209.3000 | -22.0000 | 164.3000 |
| 209.3000 | -22.0000 | 171.6000 |
| 209.3000 | -21.1000 | 175.5000 |
| 209.3000 | -14.6000 | 179.7000 |
| 209.3000 | -0.0000 | 179.7000 |
| 222.3000 | -22.7000 | 148.3000 |
| 222.3000 | -22.7000 | 158.9000 |
| 222.3000 | -22.7000 | 166.4000 |
| 222.3000 | -22.7000 | 174.8000 |
| 222.3000 | -22.7000 | 181.3000 |
| 222.3000 | -19.6000 | 181.3000 |
| 222.3000 | -0.0000 | 181.3000 |
| 271.0000 | -22.7000 | 148.9000 |
| 271.0000 | -22.7000 | 161.4000 |
| 271.0000 | -22.7000 | 170.7000 |
| 271.0000 | -22.7000 | 181.1000 |
| 271.0000 | -22.7000 | 189.2000 |
| 271.0000 | -19.6000 | 189.2000 |
| 271.0000 | -0.0000 | 189.2000 |
| 300.0000 | -22.7000 | 148.9000 |
| 300.0000 | -22.7000 | 163.0000 |
| 300.0000 | -22.7000 | 173.3000 |
| 300.0000 | -22.7000 | 184.8000 |
| 300.0000 | -22.7000 | 193.8000 |
| 300.0000 | -19.6000 | 193.8000 |
| 300.0000 | -0.0000 | 193.8000 |
| 348.6001 | -19.5911 | 148.9000 |
| 348.6001 | -19.5911 | 163.6000 |
| 348.6001 | -19.5911 | 174.6000 |
| 348.6001 | -19.5911 | 186.9000 |
| 348.6001 | -19.5911 | 196.4000 |
| 348.6001 | -16.9000 | 196.4000 |
| 348.6001 | -0.0000 | 196.4000 |
| 376.6001 | -17.8000 | 148.9000 |
| 376.6001 | -17.8000 | 161.0000 |
| 376.6001 | -17.8000 | 170.1000 |
| 376.6001 | -17.8000 | 180.3000 |
| 376.6001 | -17.8000 | 188.1000 |
| 376.6001 | -15.3000 | 188.1000 |
| 376.6001 | -0.0000 | 188.1000 |
| 391.7000 | -15.7000 | 147.3000 |
| 391.7000 | -15.7000 | 158.3000 |
| 391.7000 | -15.7000 | 166.5000 |
| 391.7000 | -15.7000 | 175.8000 |
| 391.7000 | -15.7000 | 182.9000 |
| 391.7000 | -13.5000 | 182.9000 |
| 391.7000 | -0.0000 | 182.9000 |
| 500. | -0.0000 | 139.6000 |
| 500. | -0.0000 | 139.6000 |
| 500. | -0.0000 | 139.6000 |
| 500. | -0.0000 | 139.6 |
| 500. | -0.0000 | 139.6 |
| 500. | -0.0000 | 139.6000 |
| 500. | -0.0000 | 139.6000 |
| 17. | 10. | |

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|--------|--------|-------|
| 391.36 | 56.65 | 71.07 |
| 369.4 | 56.17 | 75.35 |
| 347.29 | 55.71 | 79.4 |
| 325.04 | 55.47 | 81.52 |
| 308.31 | 55.55 | 80.88 |
| 297.19 | 55.74 | 79.13 |
| 288.89 | 56. | 76.84 |
| 283.43 | 56.29 | 74.32 |
| 280.98 | 56.64 | 71.21 |
| 284.09 | 56.93 | 68.64 |
| 289.67 | 56.1 | 67.16 |
| 297.92 | 57.23 | 65.97 |
| 308.87 | 57.32 | 65.2 |
| 325.25 | 57.3 | 65.32 |
| 347.14 | 57.06 | 67.44 |
| 369.18 | 56.74 | 70.29 |
| 391.36 | 56.65 | 71.07 |
| 389.72 | 79.71 | 73.68 |
| 368.48 | 79.24 | 77.81 |
| 347.11 | 78.8 | 81.73 |
| 325.59 | 78.57 | 83.78 |
| 309.41 | 78.64 | 83.16 |
| 298.65 | 78.83 | 81.47 |
| 290.63 | 79.08 | 79.26 |
| 285.35 | 79.35 | 76.82 |
| 282.98 | 79.69 | 73.81 |
| 285.99 | 79.97 | 71.32 |
| 291.38 | 80.13 | 69.9 |
| 299.36 | 80.26 | 68.74 |
| 309.95 | 80.35 | 67.99 |
| 325.79 | 80.33 | 68.12 |
| 346.96 | 80.1 | 70.17 |
| 368.27 | 79.79 | 72.92 |
| 389.72 | 79.71 | 73.68 |
| 388.08 | 102.76 | 76.28 |
| 367.57 | 102.31 | 80.28 |
| 346.92 | 101.88 | 84.06 |
| 326.13 | 101.66 | 86.04 |
| 310.51 | 101.73 | 85.44 |
| 300.12 | 101.91 | 83.81 |
| 292.37 | 102.15 | 81.67 |
| 287.27 | 102.42 | 79.32 |
| 284.98 | 102.75 | 76.41 |
| 287.89 | 103.02 | 74.01 |
| 293.09 | 103.17 | 72.63 |
| 300.8 | 103.3 | 71.51 |
| 311.03 | 103.38 | 70.79 |
| 326.33 | 103.37 | 70.91 |
| 346.78 | 103.14 | 72.89 |
| 367.36 | 102.84 | 75.55 |
| 388.08 | 102.76 | 76.28 |
| 386.44 | 125.81 | 78.89 |
| 366.65 | 125.38 | 82.74 |
| 346.73 | 124.97 | 86.39 |
| 326.68 | 124.75 | 88.3 |
| 311.61 | 124.82 | 87.72 |
| 301.59 | 124.99 | 86.15 |
| 294.11 | 125.23 | 84.09 |
| 289.19 | 125.48 | 81.82 |
| 286.98 | 125.8 | 79.01 |

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| 289.79 | 126.06 | 76.69 |
| 294.81 | 126.21 | 75.36 |
| 302.25 | 126.33 | 74.29 |
| 312.11 | 126.41 | 73.59 |
| 326.87 | 126.4 | 73.71 |
| 346.59 | 126.18 | 75.62 |
| 366.45 | 125.89 | 78.18 |
| 386.44 | 125.81 | 78.89 |
| 384.8 | 148.87 | 81.49 |
| 365.74 | 148.45 | 85.2 |
| 346.55 | 148.05 | 88.72 |
| 327.23 | 147.84 | 90.56 |
| 312.71 | 147.91 | 90. |
| 303.05 | 148.08 | 88.49 |
| 295.85 | 148.3 | 86.5 |
| 291.11 | 148.55 | 84.31 |
| 288.98 | 148.85 | 81.61 |
| 291.68 | 149.11 | 79.38 |
| 296.52 | 149.25 | 78.1 |
| 303.69 | 149.37 | 77.06 |
| 313.19 | 149.44 | 76.39 |
| 327.41 | 149.43 | 76.5 |
| 346.41 | 149.22 | 78.34 |
| 365.54 | 148.94 | 80.81 |
| 384.8 | 148.87 | 81.49 |
| 383.16 | 171.92 | 84.1 |
| 364.82 | 171.52 | 87.67 |
| 346.36 | 171.13 | 91.05 |
| 327.78 | 170.93 | 92.82 |
| 313.81 | 171. | 92.28 |
| 304.52 | 171.16 | 90.82 |
| 297.59 | 171.38 | 88.91 |
| 293.03 | 171.61 | 86.81 |
| 290.99 | 171.91 | 84.21 |
| 293.58 | 172.15 | 82.06 |
| 298.24 | 172.29 | 80.83 |
| 305.13 | 172.4 | 79.83 |
| 314.27 | 172.47 | 79.19 |
| 327.95 | 172.46 | 79.29 |
| 346.23 | 172.26 | 81.06 |
| 364.63 | 171.99 | 83.44 |
| 383.16 | 171.92 | 84.1 |
| 381.52 | 194.97 | 86.7 |
| 363.91 | 194.59 | 90.13 |
| 346.17 | 194.22 | 93.38 |
| 328.32 | 194.03 | 95.08 |
| 314.91 | 194.09 | 94.56 |
| 305.98 | 194.24 | 93.16 |
| 299.33 | 194.45 | 91.33 |
| 294.95 | 194.68 | 89.31 |
| 292.99 | 194.96 | 86.81 |
| 295.48 | 195.19 | 84.75 |
| 299.95 | 195.33 | 83.56 |
| 306.57 | 195.44 | 82.6 |
| 315.35 | 195.51 | 81.57 |
| 328.49 | 195.49 | 82.09 |
| 346.05 | 195.3 | 83.79 |
| 363.73 | 195.04 | 86.07 |
| 381.52 | 194.97 | 86.7 |
| 379.88 | 218.03 | 89.3 |

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| 362.99 | 217.66 | 92.59 |
| 345.99 | 217.3 | 95.71 |
| 328.87 | 217.12 | 97.34 |
| 316.01 | 217.18 | 96.84 |
| 307.45 | 217.33 | 95.5 |
| 301.07 | 217.53 | 93.74 |
| 296.87 | 217.74 | 91.8 |
| 294.99 | 218.02 | 89.41 |
| 297.38 | 218.24 | 87.43 |
| 301.67 | 218.37 | 86.3 |
| 308.01 | 218.47 | 85.38 |
| 316.43 | 218.54 | 84.78 |
| 329.03 | 218.53 | 84.88 |
| 345.87 | 218.34 | 86.51 |
| 362.82 | 218.10 | 88.7 |
| 379.88 | 218.03 | 89.3 |
| 378.24 | 241.08 | 91.91 |
| 362.07 | 240.72 | 95.06 |
| 345.8 | 240.39 | 98.04 |
| 329.42 | 240.21 | 99.6 |
| 317.11 | 240.27 | 99.13 |
| 308.92 | 240.41 | 97.84 |
| 302.81 | 240.6 | 96.15 |
| 298.79 | 240.81 | 94.3 |
| 296.99 | 240.07 | 92.01 |
| 299.28 | 241.28 | 90.12 |
| 303.38 | 241.41 | 89.03 |
| 309.45 | 241.5 | 88.15 |
| 317.51 | 241.57 | 87.58 |
| 329.57 | 241.56 | 87.68 |
| 345.69 | 241.38 | 89.23 |
| 361.91 | 241.15 | 91.33 |
| 378.24 | 241.08 | 91.91 |
| 376.6 | 264.13 | 94.51 |
| 361.16 | 263.79 | 97.52 |
| 345.61 | 263.47 | 100.37 |
| 329.97 | 263.3 | 101.86 |
| 318.21 | 263.35 | 101.41 |
| 310.38 | 263.49 | 100.18 |
| 304.55 | 263.68 | 98.57 |
| 300.71 | 263.88 | 96.8 |
| 298.99 | 264.12 | 94.61 |
| 301.17 | 264.33 | 92.8 |
| 305.09 | 264.44 | 91.76 |
| 310.9 | 264.54 | 90.92 |
| 318.59 | 264.6 | 90.38 |
| 330.11 | 264.59 | 90.47 |
| 345.51 | 264.42 | 91.96 |
| 361. | 264.2 | 93.96 |
| 376.6 | 264.13 | 94.51 |
| 17.0 | 10.0 | |
| 391.3601 | -56.6500 | 71.0700 |
| 369.1799 | -56.7400 | 70.2900 |
| 347.1399 | -57.0600 | 67.4400 |
| 325.2500 | -57.3000 | 65.3200 |
| 308.8701 | -57.3200 | 65.2000 |
| 297.9199 | -57.2300 | 65.9700 |
| 289.6699 | -56.1000 | 67.1600 |
| 284.0901 | -56.9300 | 68.6400 |
| 280.9800 | -56.6400 | 71.2100 |

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| 283.4299 | -56.2900 | 74.3200 |
| 288.8899 | -56.0000 | 76.8400 |
| 297.1899 | -55.7400 | 79.1300 |
| 308.3101 | -55.5500 | 80.8800 |
| 325.0400 | -55.4700 | 81.5200 |
| 347.2900 | -55.7100 | 79.4000 |
| 369.3999 | -56.1700 | 75.3500 |
| 391.3601 | -56.6500 | 71.0700 |
| 389.7200 | -79.7100 | 73.6800 |
| 368.2700 | -79.7900 | 72.9200 |
| 346.9600 | -80.1000 | 70.1700 |
| 325.7900 | -80.3300 | 68.1200 |
| 309.9500 | -80.3500 | 67.9900 |
| 299.3601 | -80.2600 | 68.7400 |
| 291.3799 | -80.1300 | 69.9000 |
| 285.9900 | -79.9700 | 71.3200 |
| 282.9800 | -79.6900 | 73.8100 |
| 285.3501 | -79.3500 | 76.8200 |
| 290.6299 | -79.0800 | 79.2600 |
| 298.6499 | -78.8300 | 81.4700 |
| 309.4099 | -78.6400 | 83.1600 |
| 325.5901 | -78.5700 | 83.7800 |
| 347.1101 | -78.8000 | 81.7300 |
| 368.4300 | -79.2400 | 77.8100 |
| 389.7200 | -79.7100 | 73.6800 |
| 388.0801 | -102.7600 | 76.2300 |
| 367.3601 | -102.8400 | 75.5500 |
| 346.7800 | -103.1400 | 72.8900 |
| 326.3301 | -103.3700 | 70.9100 |
| 311.0300 | -103.3800 | 70.7900 |
| 300.8000 | -103.3000 | 71.5100 |
| 293.0901 | -103.1700 | 72.6300 |
| 287.8899 | -103.0200 | 74.0100 |
| 284.9800 | -102.7500 | 76.4100 |
| 287.2700 | -102.4200 | 79.3200 |
| 292.3701 | -102.1500 | 81.6700 |
| 300.1201 | -101.9100 | 83.8100 |
| 310.5100 | -101.7300 | 85.4400 |
| 326.1299 | -101.6600 | 86.0400 |
| 346.9199 | -101.8800 | 84.0600 |
| 367.5701 | -102.3100 | 80.2800 |
| 388.0801 | -102.7600 | 76.2800 |
| 386.4399 | -125.8100 | 78.8900 |
| 366.4500 | -125.8900 | 78.1800 |
| 346.5901 | -126.1800 | 75.6200 |
| 326.8701 | -126.4000 | 73.7100 |
| 312.1101 | -126.4100 | 73.5900 |
| 302.2500 | -126.3300 | 74.2900 |
| 294.8101 | -126.2100 | 75.3600 |
| 289.7900 | -126.0600 | 76.6900 |
| 286.9800 | -125.8000 | 79.0100 |
| 289.1899 | -125.4800 | 81.8200 |
| 294.1101 | -125.2300 | 84.0900 |
| 301.5901 | -124.9900 | 86.1500 |
| 311.6101 | -124.8200 | 87.7200 |
| 326.6799 | -124.7500 | 88.3000 |
| 346.7300 | -124.9700 | 86.3900 |
| 366.6499 | -125.3300 | 82.7400 |
| 386.4399 | -125.8100 | 78.8900 |
| 384.8000 | -148.8700 | 81.4900 |

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| 365.5400 | -148.9400 | 80.8100 |
| 346.4099 | -149.2200 | 78.3400 |
| 327.4099 | -149.4300 | 76.5000 |
| 313.1899 | -149.4400 | 76.3900 |
| 303.6899 | -149.3700 | 77.0600 |
| 296.5200 | -149.2500 | 78.1000 |
| 291.6799 | -149.1100 | 79.3800 |
| 288.9300 | -148.8500 | 81.6100 |
| 291.1101 | -148.5500 | 84.3100 |
| 295.8501 | -148.3000 | 86.5000 |
| 303.0500 | -148.0800 | 88.4900 |
| 312.7100 | -147.9100 | 90.0000 |
| 327.2300 | -147.8400 | 90.5600 |
| 346.5500 | -148.0500 | 88.7200 |
| 365.7400 | -148.4500 | 85.2000 |
| 384.8000 | -148.8700 | 81.6900 |
| 383.1599 | -171.9200 | 84.1000 |
| 364.6299 | -171.9900 | 83.4400 |
| 346.2300 | -172.2600 | 81.0600 |
| 327.9500 | -172.4600 | 79.2900 |
| 314.2700 | -172.4700 | 79.1900 |
| 305.1099 | -172.4000 | 79.8300 |
| 298.2000 | -172.2900 | 80.8300 |
| 293.2001 | -172.1500 | 82.0600 |
| 290.9900 | -171.9100 | 84.2100 |
| 293.0300 | -171.6100 | 86.8100 |
| 297.5901 | -171.3300 | 88.9100 |
| 304.5200 | -171.1600 | 90.8200 |
| 313.8101 | -171.0000 | 92.2300 |
| 327.7800 | -170.9300 | 92.8200 |
| 346.3601 | -171.1300 | 91.0500 |
| 364.8201 | -171.5200 | 87.6700 |
| 383.1599 | -171.9200 | 84.1000 |
| 381.5200 | -194.9700 | 86.7000 |
| 363.7300 | -195.0400 | 86.0700 |
| 346.0500 | -195.3000 | 83.7900 |
| 323.4900 | -195.4900 | 82.0900 |
| 315.3501 | -195.5100 | 81.9800 |
| 306.5701 | -195.4400 | 82.6000 |
| 299.9500 | -195.3300 | 83.5600 |
| 295.4800 | -195.1900 | 84.7500 |
| 292.9900 | -194.9600 | 86.8100 |
| 294.9500 | -194.6800 | 89.3100 |
| 299.3301 | -194.4500 | 91.3300 |
| 305.9800 | -194.2400 | 93.1600 |
| 314.9099 | -194.0900 | 94.5600 |
| 328.3201 | -194.0300 | 95.0800 |
| 346.1699 | -194.2200 | 93.3800 |
| 363.9099 | -194.5900 | 90.1300 |
| 381.5200 | -194.9700 | 86.7000 |
| 379.8799 | -218.0300 | 89.3000 |
| 362.8201 | -218.1000 | 88.7000 |
| 345.8701 | -218.3400 | 86.5100 |
| 329.0300 | -218.5300 | 84.8800 |
| 316.4299 | -218.5400 | 84.7800 |
| 308.0100 | -218.4700 | 85.3800 |
| 301.6699 | -218.3700 | 86.3000 |
| 297.3799 | -218.2400 | 87.4300 |
| 294.9900 | -218.0200 | 89.4100 |
| 296.8701 | -217.7400 | 91.8000 |

ORIGINAL PAGE IS
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| 301.0701 | -217.5300 | 93.7400 |
| 307.4500 | -217.3300 | 95.5000 |
| 316.0100 | -217.1800 | 96.8400 |
| 328.8701 | -217.1200 | 97.3400 |
| 345.9900 | -217.3000 | 95.7100 |
| 362.9900 | -217.6600 | 92.5900 |
| 379.8799 | -218.0300 | 89.3000 |
| 378.2400 | -241.0800 | 91.9100 |
| 361.9099 | -241.1500 | 91.3300 |
| 345.6899 | -241.3800 | 89.2300 |
| 329.5701 | -241.5600 | 87.6800 |
| 317.5100 | -241.5700 | 87.5800 |
| 309.4500 | -241.5000 | 88.1500 |
| 303.3799 | -241.4100 | 89.0300 |
| 299.2800 | -241.2800 | 90.1200 |
| 296.9900 | -240.0700 | 92.0100 |
| 298.7900 | -240.8100 | 94.3000 |
| 302.8101 | -240.6000 | 96.1500 |
| 308.9199 | -240.4100 | 97.8400 |
| 317.1101 | -240.2700 | 99.1300 |
| 329.4199 | -240.2100 | 99.6000 |
| 345.8000 | -240.3900 | 98.0400 |
| 362.0701 | -240.7200 | 95.0600 |
| 378.2400 | -241.0800 | 91.9100 |
| 376.6001 | -264.1299 | 94.5100 |
| 361.0000 | -264.2000 | 93.9600 |
| 345.5100 | -264.4199 | 91.9600 |
| 330.1101 | -264.5901 | 90.4700 |
| 318.5901 | -264.6001 | 90.3300 |
| 310.8999 | -264.5400 | 90.9200 |
| 305.0901 | -264.4399 | 91.7600 |
| 301.1699 | -264.3301 | 92.8000 |
| 298.9900 | -264.1201 | 94.6100 |
| 300.7100 | -263.8799 | 96.8000 |
| 304.5500 | -263.6799 | 98.5700 |
| 310.3799 | -263.4900 | 100.1800 |
| 318.2100 | -263.3501 | 101.4100 |
| 329.9700 | -263.3000 | 101.8600 |
| 345.6101 | -263.4700 | 100.3700 |
| 361.1599 | -263.7900 | 97.5200 |
| 376.6001 | -264.1299 | 94.5100 |
| 8. | 2. | |
| 271. | 0. | 72.8 |
| 284.09 | 0. | 68.64 |
| 289.67 | 0. | 67.16 |
| 297.92 | 0. | 65.97 |
| 308.87 | 0. | 65.2 |
| 325.25 | 0. | 65.32 |
| 347.14 | 0. | 67.44 |
| 391.7 | 0. | 74.4 |
| 271. | 29.2 | 72.8 |
| 284.09 | 29.2 | 68.64 |
| 289.67 | 29.2 | 67.16 |
| 297.92 | 29.2 | 65.97 |
| 308.87 | 29.2 | 65.2 |
| 325.25 | 29.2 | 65.32 |
| 347.14 | 29.2 | 67.44 |
| 391.7 | 28. | 74.4 |
| | 8.0 | 2.0 |
| 391.7 | -0.0000 | 74.4 |

| | | |
|----------|----------|---------|
| 347.1399 | -0.0000 | 67.4400 |
| 325.2500 | -0.0000 | 65.3200 |
| 308.8701 | -0.0000 | 65.2000 |
| 297.9199 | -0.0000 | 65.9700 |
| 289.6699 | -0.0000 | 67.1600 |
| 284.0901 | -0.0000 | 68.6400 |
| 271.0000 | -0.0000 | 72.8000 |
| 391.7 | -28. | 74.4 |
| 347.1399 | -29.2000 | 67.4400 |
| 325.2500 | -29.2000 | 65.3200 |
| 308.8701 | -29.2000 | 65.2000 |
| 297.9199 | -29.2000 | 65.9700 |
| 289.6699 | -29.2000 | 67.1600 |
| 284.0901 | -29.2000 | 68.6400 |
| 271.0000 | -29.2000 | 72.8000 |

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|--------|----------|----------|
| 17. | 2. | |
| 391.7 | 28. | 74.4 |
| 376.6 | 38.9 | 85. |
| 347.29 | 38.9 | 85. |
| 325.04 | 38.9 | 85. |
| 308.31 | 38.9 | 85. |
| 300. | 38.9 | 85. |
| 289. | 35.22069 | 80.37241 |
| 282. | 32.87931 | 77.42759 |
| 271. | 29.2 | 72.8 |
| 284.09 | 29.2 | 68.64 |
| 289.67 | 29.2 | 67.16 |
| 297.92 | 29.2 | 65.97 |
| 308.87 | 29.2 | 65.2 |
| 325.25 | 29.2 | 65.32 |
| 347.14 | 29.2 | 67.44 |
| 369.18 | 28.60646 | 70.88251 |
| 391.7 | 28. | 74.4 |
| 391.36 | 56.65 | 71.07 |
| 369.4 | 56.17 | 75.35 |
| 347.29 | 55.71 | 79.4 |
| 325.04 | 55.47 | 81.52 |
| 308.31 | 55.55 | 80.88 |
| 297.19 | 55.74 | 79.13 |
| 288.89 | 56. | 76.84 |
| 283.43 | 56.29 | 74.32 |
| 280.98 | 56.66 | 71.21 |
| 284.09 | 56.93 | 68.64 |
| 289.67 | 56.1 | 67.16 |
| 297.92 | 57.23 | 65.97 |
| 308.87 | 57.32 | 65.2 |
| 325.25 | 57.3 | 65.32 |
| 347.14 | 57.06 | 67.44 |
| 369.18 | 56.74 | 70.29 |
| 391.36 | 56.65 | 71.07 |

| | | |
|----------|----------|---------|
| | 17.0 | 2.0 |
| 391.7000 | -28.0000 | 74.4000 |
| 369.1799 | -28.6065 | 70.8825 |
| 347.1399 | -29.2000 | 67.4400 |
| 325.2500 | -29.2000 | 65.3200 |
| 308.8701 | -29.2000 | 65.2000 |
| 297.9199 | -29.2000 | 65.9700 |
| 289.6699 | -29.2000 | 67.1600 |
| 284.0901 | -29.2000 | 68.6400 |
| 271.0000 | -29.2000 | 72.8000 |

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OF POOR QUALITY

| | | |
|----------|----------|---------|
| 282.0000 | -32.8793 | 77.4276 |
| 289.0000 | -35.2207 | 80.3724 |
| 300.0000 | -38.9000 | 85.0000 |
| 308.3101 | -38.9000 | 85.0000 |
| 325.0400 | -38.9000 | 85.0000 |
| 347.2900 | -38.9000 | 85.0000 |
| 376.6001 | -38.9000 | 85.0000 |
| 391.7000 | -28.0000 | 74.4000 |
| 391.3601 | -56.6500 | 71.0700 |
| 369.1799 | -56.7400 | 70.2900 |
| 347.1599 | -57.0600 | 67.4400 |
| 325.2500 | -57.3000 | 65.3200 |
| 308.8701 | -57.3200 | 65.2000 |
| 297.9199 | -57.2300 | 65.9700 |
| 289.6699 | -56.1000 | 57.1600 |
| 284.0901 | -56.9300 | 68.6400 |
| 280.9800 | -56.6400 | 71.2100 |
| 283.4299 | -56.2900 | 74.3200 |
| 288.8899 | -56.0000 | 76.8400 |
| 297.1899 | -55.7400 | 79.1300 |
| 308.3101 | -55.5500 | 80.8800 |
| 325.0400 | -55.4700 | 81.5200 |
| 347.2900 | -55.7100 | 79.4000 |
| 369.3999 | -56.1700 | 75.3500 |
| 391.3601 | -56.6500 | 71.0700 |

MULT

| 2. | 9. | 7. | 1. | 10. | 0. |
|--------|--------|---------|----|-----|----|
| 11. | | | | | |
| 285.35 | 79.63 | 74.34 | | | |
| 290.63 | 79.59 | 74.68 | | | |
| 298.65 | 79.54 | 75.16 | | | |
| 309.41 | 79.49 | 75.6 | | | |
| 325.59 | 79.45 | 75.95 | | | |
| 347.11 | 79.45 | 75.96 | | | |
| 368.48 | 79.52 | 74.37 | | | |
| 389.72 | 79.71 | 73.68 | | | |
| 411.29 | 79.71 | 71.98 | | | |
| 454.51 | 79.71 | 69.72 | | | |
| 9000. | 79.71 | -165.62 | | | |
| 287.27 | 102.69 | 76.92 | | | |
| 292.37 | 102.65 | 77.25 | | | |
| 300.12 | 102.6 | 77.71 | | | |
| 310.51 | 102.55 | 78.13 | | | |
| 326.13 | 102.51 | 78.48 | | | |
| 346.92 | 102.51 | 78.49 | | | |
| 367.57 | 102.53 | 77.92 | | | |
| 388.08 | 102.76 | 76.23 | | | |
| 408.92 | 102.76 | 74.64 | | | |
| 450.66 | 102.76 | 72.46 | | | |
| 9000. | 102.76 | -162.88 | | | |
| 289.19 | 125.74 | 79.5 | | | |
| 294.11 | 125.71 | 79.82 | | | |
| 301.59 | 125.66 | 80.26 | | | |
| 311.61 | 125.61 | 80.67 | | | |
| 326.68 | 125.57 | 81. | | | |
| 346.73 | 125.57 | 81.01 | | | |
| 366.65 | 125.64 | 80.46 | | | |
| 386.44 | 125.81 | 78.89 | | | |
| 406.54 | 125.81 | 77.31 | | | |
| 446.81 | 125.81 | 75.2 | | | |

| | | |
|--------|--------|---------|
| 9000. | 125.81 | -160.15 |
| 291.11 | 148.8 | 82.08 |
| 295.85 | 148.77 | 82.39 |
| 303.05 | 148.72 | 82.82 |
| 312.71 | 148.67 | 83.21 |
| 327.23 | 148.64 | 83.53 |
| 346.55 | 148.64 | 83.54 |
| 365.74 | 148.7 | 83.01 |
| 384.8 | 148.87 | 81.49 |
| 404.17 | 148.87 | 79.97 |
| 442.96 | 148.87 | 77.94 |
| 9000. | 148.87 | -157.41 |
| 293.03 | 171.86 | 84.67 |
| 297.59 | 171.82 | 84.96 |
| 304.52 | 171.78 | 85.57 |
| 313.81 | 171.73 | 85.75 |
| 327.78 | 171.7 | 86.06 |
| 346.36 | 171.7 | 86.07 |
| 364.82 | 171.76 | 85.56 |
| 383.16 | 171.92 | 84.1 |
| 401.79 | 171.92 | 82.63 |
| 439.11 | 171.92 | 80.68 |
| 9000. | 171.92 | -154.67 |
| 294.95 | 194.91 | 87.25 |
| 299.53 | 194.88 | 87.53 |
| 305.98 | 194.84 | 87.93 |
| 314.91 | 194.79 | 88.29 |
| 328.32 | 194.76 | 88.58 |
| 346.17 | 194.76 | 88.59 |
| 363.91 | 194.82 | 88.1 |
| 381.52 | 194.97 | 86.7 |
| 399.41 | 194.97 | 85.29 |
| 435.26 | 194.97 | 83.41 |
| 9000. | 194.97 | -151.93 |
| 296.87 | 217.97 | 89.83 |
| 301.07 | 217.94 | 90.1 |
| 307.45 | 217.89 | 90.48 |
| 316.01 | 217.85 | 90.83 |
| 328.87 | 217.82 | 91.11 |
| 345.99 | 217.82 | 91.12 |
| 362.99 | 217.87 | 90.65 |
| 379.88 | 218.03 | 89.3 |
| 397.04 | 218.03 | 87.95 |
| 431.41 | 218.03 | 86.15 |
| 9000. | 218.03 | -149.19 |
| 298.79 | 241.02 | 92.41 |
| 302.81 | 240.99 | 92.67 |
| 308.92 | 240.95 | 93.03 |
| 317.11 | 240.92 | 93.57 |
| 329.42 | 240.89 | 93.64 |
| 345.8 | 240.88 | 93.64 |
| 362.07 | 240.93 | 93.2 |
| 378.24 | 241.08 | 91.91 |
| 394.66 | 241.08 | 90.62 |
| 427.56 | 241.08 | 88.89 |
| 9000. | 241.08 | -146.45 |
| 300.51 | 261.77 | 94.73 |
| 304.37 | 261.75 | 94.98 |
| 310.24 | 261.71 | 95.33 |
| 318.1 | 261.67 | 95.65 |

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|---------|---------|---------|---------|---------|---------|
| 329.91 | 261.64 | 95.91 | | | |
| 345.63 | 261.64 | 95.92 | | | |
| 361.25 | 261.69 | 95.49 | | | |
| 376.76 | 261.83 | 94.25 | | | |
| 392.52 | 261.83 | 93.01 | | | |
| 424.1 | 261.83 | 91.36 | | | |
| 9000. | 261.83 | -143.98 | | | |
| .050192 | .085453 | .120618 | .172921 | .242018 | .219928 |
| .10887 | | | | | |
| 388.93 | 91.17 | 74.97 | .07889 | -.10036 | .99119 |
| 387.29 | 114.22 | 77.58 | .07889 | -.10036 | .99119 |
| 385.64 | 137.27 | 80.18 | .07889 | -.10036 | .99119 |
| 384. | 160.32 | 82.78 | .07889 | -.10036 | .99119 |
| 382.36 | 183.37 | 85.39 | .07889 | -.10036 | .99119 |
| 380.72 | 206.42 | 87.99 | .07889 | -.10036 | .99119 |
| 379.08 | 229.47 | 90.59 | .07889 | -.10036 | .99119 |
| 377.44 | 252.52 | 93.2 | .07889 | -.10036 | .99119 |
| 11. | 9. | 7. | 1. | 10. | 0. |
| 285.35 | -79.63 | 74.34 | | | |
| 290.63 | -79.59 | 74.68 | | | |
| 298.65 | -79.54 | 75.16 | | | |
| 309.41 | -79.49 | 75.6 | | | |
| 325.59 | -79.45 | 75.95 | | | |
| 347.11 | -79.45 | 75.96 | | | |
| 368.48 | -79.52 | 74.37 | | | |
| 389.72 | -79.71 | 73.68 | | | |
| 411.29 | -79.71 | 71.98 | | | |
| 454.51 | -79.71 | 69.72 | | | |
| 9000. | -79.71 | -165.62 | | | |
| 287.27 | -102.69 | 76.92 | | | |
| 292.37 | -102.65 | 77.25 | | | |
| 300.12 | -102.6 | 77.71 | | | |
| 310.51 | -102.55 | 78.13 | | | |
| 326.13 | -102.51 | 78.48 | | | |
| 346.92 | -102.51 | 78.49 | | | |
| 367.57 | -102.58 | 77.92 | | | |
| 388.08 | -102.76 | 76.28 | | | |
| 408.92 | -102.76 | 74.64 | | | |
| 450.66 | -102.76 | 72.46 | | | |
| 9000. | -102.76 | -162.88 | | | |
| 289.19 | -125.74 | 79.5 | | | |
| 294.11 | -125.71 | 79.82 | | | |
| 301.59 | -125.66 | 80.26 | | | |
| 311.61 | -125.61 | 80.67 | | | |
| 326.68 | -125.57 | 81. | | | |
| 346.73 | -125.57 | 81.01 | | | |
| 366.65 | -125.64 | 80.46 | | | |
| 386.44 | -125.81 | 78.89 | | | |
| 406.54 | -125.81 | 77.31 | | | |
| 446.81 | -125.81 | 75.2 | | | |
| 9000. | -125.81 | -160.15 | | | |
| 291.11 | -148.8 | 82.08 | | | |
| 295.85 | -148.7 | 82.39 | | | |
| 303.05 | -148.2 | 82.82 | | | |
| 312.71 | -148.67 | 83.21 | | | |
| 327.23 | -148.64 | 83.53 | | | |
| 346.55 | -148.64 | 83.54 | | | |
| 365.74 | -148.7 | 83.01 | | | |
| 384.8 | -148.87 | 81.49 | | | |
| 404.17 | -148.87 | 79.97 | | | |

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|---------|---------|---------|---------|---------|---------|
| 442.96 | -148.87 | 77.94 | | | |
| 9000. | -148.87 | -157.41 | | | |
| 293.03 | -171.86 | 84.67 | | | |
| 297.59 | -171.82 | 84.96 | | | |
| 304.52 | -171.78 | 85.37 | | | |
| 313.31 | -171.73 | 85.75 | | | |
| 327.78 | -171.7 | 86.06 | | | |
| 346.36 | -171.7 | 86.07 | | | |
| 364.82 | -171.76 | 85.56 | | | |
| 383.16 | -171.92 | 84.1 | | | |
| 401.79 | -171.92 | 82.63 | | | |
| 439.11 | -171.92 | 80.68 | | | |
| 9000. | -171.92 | -154.67 | | | |
| 294.95 | -194.91 | 87.25 | | | |
| 299.33 | -194.88 | 87.53 | | | |
| 305.98 | -194.84 | 87.93 | | | |
| 314.91 | -194.79 | 88.29 | | | |
| 328.32 | -194.76 | 88.58 | | | |
| 346.17 | -194.76 | 88.59 | | | |
| 363.91 | -194.82 | 88.1 | | | |
| 381.52 | -194.97 | 86.7 | | | |
| 399.41 | -194.97 | 85.29 | | | |
| 435.26 | -194.97 | 83.41 | | | |
| 9000. | -194.97 | -151.93 | | | |
| 296.87 | -217.97 | 89.83 | | | |
| 301.07 | -217.94 | 90.1 | | | |
| 307.45 | -217.89 | 90.48 | | | |
| 316.01 | -217.85 | 90.83 | | | |
| 328.87 | -217.82 | 91.11 | | | |
| 345.99 | -217.82 | 91.12 | | | |
| 362.99 | -217.87 | 90.65 | | | |
| 379.88 | -218.03 | 89.3 | | | |
| 397.04 | -218.03 | 87.95 | | | |
| 431.41 | -218.03 | 86.15 | | | |
| 9000. | -218.03 | -149.19 | | | |
| 298.79 | -241.02 | 92.41 | | | |
| 302.81 | -240.99 | 92.67 | | | |
| 308.92 | -240.95 | 93.03 | | | |
| 317.11 | -240.92 | 93.37 | | | |
| 329.42 | -240.89 | 93.64 | | | |
| 345.8 | -240.88 | 93.64 | | | |
| 362.07 | -240.93 | 93.2 | | | |
| 378.24 | -241.08 | 91.91 | | | |
| 394.66 | -241.08 | 90.62 | | | |
| 427.56 | -241.08 | 88.89 | | | |
| 9000. | -241.08 | -146.45 | | | |
| 300.51 | -261.77 | 94.73 | | | |
| 304.37 | -261.75 | 94.98 | | | |
| 310.24 | -261.71 | 95.33 | | | |
| 318.1 | -261.67 | 95.65 | | | |
| 329.91 | -261.64 | 95.91 | | | |
| 345.63 | -261.64 | 95.92 | | | |
| 361.25 | -261.69 | 95.49 | | | |
| 376.76 | -261.83 | 94.25 | | | |
| 392.52 | -261.83 | 93.01 | | | |
| 424.1 | -261.83 | 91.36 | | | |
| 9000. | -261.83 | -143.98 | | | |
| .050192 | .085453 | .120618 | .172921 | .242618 | .219928 |
| .10887 | | | | | |
| 388.93 | -91.17 | 74.97 | .07889 | .10636 | .99119 |

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 OF POOR QUALITY

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|----------|---------|-----------|---------|---------|---------|
| 387.29 | -114.22 | 77.58 | .07889 | .10636 | .99119 |
| 385.64 | -137.27 | 80.18 | .07889 | .10636 | .99119 |
| 334. | -160.32 | 82.78 | .07889 | .10636 | .99119 |
| 382.36 | -183.37 | 85.39 | .07889 | .10636 | .99119 |
| 380.72 | -206.42 | 87.99 | .07889 | .10636 | .99119 |
| 379.08 | -229.47 | 90.59 | .07889 | .10636 | .99119 |
| 377.44 | -252.52 | 93.2 | .07889 | .10636 | .99119 |
| B-MU | | | | | |
| 2. | | | | | |
| 11. | 3. | 7. | 1. | 10. | 0. |
| 283.43 | 0. | 71.76 | | | |
| 288.89 | 0. | 72.11 | | | |
| 297.19 | 0. | 72.6 | | | |
| 308.31 | 0. | 73.06 | | | |
| 325.04 | 0. | 73.42 | | | |
| 347.29 | 0. | 73.43 | | | |
| 369.4 | 0. | 76. | | | |
| 392.0323 | 0. | 77.65445 | | | |
| 413.67 | 0. | 100. | | | |
| 458.36 | 0. | 120. | | | |
| 9000. | 0. | -115.3426 | | | |
| 283.43 | 56.58 | 71.76 | | | |
| 288.89 | 56.54 | 72.11 | | | |
| 297.19 | 56.48 | 72.6 | | | |
| 308.31 | 56.43 | 73.06 | | | |
| 325.04 | 56.39 | 73.42 | | | |
| 347.29 | 56.39 | 73.43 | | | |
| 369.4 | 56.46 | 72.82 | | | |
| 391.36 | 56.65 | 71.07 | | | |
| 413.67 | 56.65 | 69.32 | | | |
| 458.36 | 56.65 | 66.93 | | | |
| 9000. | 56.65 | -168.36 | | | |
| 285.35 | 79.63 | 74.34 | | | |
| 290.63 | 79.59 | 74.68 | | | |
| 298.65 | 79.54 | 75.16 | | | |
| 309.41 | 79.49 | 75.6 | | | |
| 325.59 | 79.41 | 75.95 | | | |
| 347.11 | 79.45 | 75.96 | | | |
| 368.48 | 79.52 | 75.37 | | | |
| 389.72 | 79.71 | 73.68 | | | |
| 411.29 | 79.71 | 71.98 | | | |
| 454.51 | 79.71 | 69.72 | | | |
| 9000. | 79.71 | -165.62 | | | |
| .050192 | .085453 | .120618 | .172921 | .242018 | .219928 |
| .10387 | | | | | |
| 390.57 | 68.12 | 72.37 | .07889 | -.10636 | .99119 |
| 11. | 3. | 7. | 1. | 10. | 0. |
| 283.43 | 0. | 71.76 | | | |
| 288.89 | 0. | 72.11 | | | |
| 297.19 | 0. | 72.6 | | | |
| 308.31 | 0. | 73.06 | | | |
| 325.04 | 0. | 73.42 | | | |
| 347.29 | 0. | 73.43 | | | |
| 369.4 | 0. | 76. | | | |
| 392.0323 | 0. | 77.65445 | | | |
| 413.67 | 0. | 100. | | | |
| 458.36 | 0. | 120. | | | |
| 9000. | 0. | -115.3426 | | | |
| 283.43 | -56.58 | 71.76 | | | |
| 288.89 | -56.54 | 72.11 | | | |

| | | | | | |
|---------|---------|---------|---------|---------|---------|
| 297.19 | -56.48 | 72.6 | | | |
| 308.31 | -56.43 | 73.06 | | | |
| 325.04 | -56.39 | 73.42 | | | |
| 347.29 | -56.39 | 73.43 | | | |
| 369.4 | -56.46 | 72.82 | | | |
| 391.36 | -56.65 | 71.07 | | | |
| 413.67 | -56.65 | 69.32 | | | |
| 458.36 | -56.65 | 66.98 | | | |
| 9000. | -56.65 | -168.36 | | | |
| 285.35 | -79.63 | 74.34 | | | |
| 290.63 | -79.59 | 74.68 | | | |
| 298.65 | -79.54 | 75.16 | | | |
| 309.41 | -79.49 | 75.6 | | | |
| 325.59 | -79.45 | 75.95 | | | |
| 347.11 | -79.45 | 75.96 | | | |
| 368.43 | -79.52 | 75.37 | | | |
| 389.72 | -79.71 | 73.68 | | | |
| 411.29 | -79.71 | 71.98 | | | |
| 454.51 | -79.71 | 69.72 | | | |
| 9000. | -79.71 | -165.62 | | | |
| .050192 | .085453 | .120618 | .172921 | .242018 | .219928 |
| .10867 | | | | | |
| 390.57 | -68.12 | 72.37 | .07889 | .10636 | .99119 |
| END | | | | | |
| AERO | | | | | |
| 5. | 0. | 0. | | | |
| FORC | | | | | |
| 307.5 | 0. | 75.52 | 52112. | 98.1 | 531.2 |
| END | | | | | 0. |

ORIGINAL PAGE IS
OF POOR QUALITY

CASE
RSRA FUSELAGE AND ENGINES
J D COWAN BOEING VERTOL ORG 7440 X7834 M/S P32-74
GEOM
3.00000 400. 1. -1. 0.
SOUR

| | | | |
|-----------|----------|-----------|--|
| 8.0 | | | |
| 7.00 | 4.00 | | |
| 36.00000 | 0.0 | 95.89999 | |
| 36.00000 | 0.0 | 95.89999 | |
| 36.00000 | 0.0 | 95.89999 | |
| 36.00000 | 0.0 | 95.89999 | |
| 36.00000 | 0.0 | 95.89999 | |
| 36.00000 | 0.0 | 95.89999 | |
| 36.00000 | 0.0 | 95.89999 | |
| 58.79999 | 0.0 | 110.20000 | |
| 58.79999 | 16.89999 | 108.09999 | |
| 58.79999 | 22.50000 | 106.00000 | |
| 58.79999 | 22.50000 | 96.20000 | |
| 58.79999 | 22.50000 | 86.39999 | |
| 58.79999 | 16.89999 | 82.29999 | |
| 58.79999 | 0.0 | 82.29999 | |
| 81.50000 | 0.0 | 119.89999 | |
| 81.50000 | 22.09999 | 116.39999 | |
| 81.50000 | 29.50000 | 113.00000 | |
| 81.50000 | 29.50000 | 99.00000 | |
| 81.50000 | 29.50000 | 85.00000 | |
| 81.50000 | 22.09999 | 78.09999 | |
| 81.50000 | 0.0 | 78.09999 | |
| 120.89999 | 0.0 | 147.59999 | |
| 120.89999 | 28.39999 | 136.70000 | |
| 120.89999 | 37.79999 | 125.89999 | |
| 120.89999 | 37.79999 | 108.00000 | |
| 120.89999 | 37.79999 | 90.70000 | |
| 120.89999 | 28.39999 | 74.79999 | |
| 120.89999 | 0.0 | 74.79999 | |
| 7.00 | 13.00 | | |
| 120.89999 | 0.0 | 147.59999 | |
| 120.89999 | 28.39999 | 136.70000 | |
| 120.89999 | 37.79999 | 125.89999 | |
| 120.89999 | 37.79999 | 108.00000 | |
| 120.89999 | 37.79999 | 90.70000 | |
| 120.89999 | 28.39999 | 74.79999 | |
| 120.89999 | 0.0 | 74.79999 | |
| 133.00000 | 0.0 | 148.89999 | |
| 133.00000 | 29.20000 | 148.89999 | |
| 133.00000 | 38.89999 | 129.89999 | |
| 133.00000 | 38.89999 | 110.79999 | |
| 133.00000 | 38.89999 | 91.79999 | |
| 133.00000 | 29.20000 | 72.79999 | |
| 133.00000 | 0.0 | 72.79999 | |
| 175.29999 | 12.10000 | 148.89999 | |
| 175.29999 | 29.20000 | 148.89999 | |
| 175.29999 | 38.89999 | 129.89999 | |
| 175.29999 | 38.89999 | 110.79999 | |
| 175.29999 | 38.89999 | 91.79999 | |

| | | |
|-----------|----------|-----------|
| 175.29999 | 29.20000 | 72.79999 |
| 175.29999 | 0.0 | 72.79999 |
| 209.29999 | 21.89999 | 148.89999 |
| 209.29999 | 29.20000 | 148.89999 |
| 209.29999 | 38.89999 | 129.89999 |
| 209.29999 | 38.89999 | 110.79999 |
| 209.29999 | 38.89999 | 91.79999 |
| 209.29999 | 29.20000 | 72.79999 |
| 209.29999 | 0.0 | 72.79999 |
| 222.29999 | 22.70000 | 148.89999 |
| 222.29999 | 29.20000 | 148.89999 |
| 222.29999 | 38.89999 | 129.89999 |
| 222.29999 | 38.89999 | 110.79999 |
| 222.29999 | 38.89999 | 91.79999 |
| 222.29999 | 29.20000 | 72.79999 |
| 222.29999 | 0.0 | 72.79999 |
| 271.00000 | 22.70000 | 148.89999 |
| 271.00000 | 29.20000 | 148.89999 |
| 271.00000 | 38.89999 | 129.89999 |
| 271.00000 | 38.89999 | 110.79999 |
| 271.00000 | 38.89999 | 91.79999 |
| 271.00000 | 29.20000 | 72.79999 |
| 271.00000 | 0.0 | 72.79999 |
| 300.00000 | 22.70000 | 148.89999 |
| 300.00000 | 29.20000 | 148.89999 |
| 300.00000 | 38.89999 | 129.89999 |
| 300.00000 | 38.89999 | 110.79999 |
| 300.00000 | 38.89999 | 91.79999 |
| 300.00000 | 29.20000 | 72.79999 |
| 300.00000 | 0.0 | 72.79999 |
| 376.59985 | 17.79999 | 148.89999 |
| 376.59985 | 29.20000 | 148.89999 |
| 376.59985 | 38.89999 | 129.89999 |
| 376.59985 | 38.89999 | 110.79999 |
| 376.59985 | 38.89999 | 91.79999 |
| 376.59985 | 29.20000 | 72.79999 |
| 376.59985 | 0.0 | 72.79999 |
| 391.69995 | 17.70000 | 147.29999 |
| 391.69995 | 28.00000 | 147.29999 |
| 391.69995 | 37.29999 | 129.00000 |
| 391.69995 | 37.29999 | 110.79999 |
| 391.69995 | 37.29999 | 92.59999 |
| 391.69995 | 28.00000 | 74.39999 |
| 391.69995 | 0.0 | 74.39999 |
| 445.69995 | 7.87174 | 143.45999 |
| 445.69995 | 24.50000 | 143.45999 |
| 445.69995 | 32.70000 | 127.20000 |
| 445.69995 | 32.70000 | 110.79999 |
| 445.69995 | 32.70000 | 94.39999 |
| 445.69995 | 24.50000 | 77.79999 |
| 445.69995 | 0.0 | 77.79999 |
| 500.00000 | 0.0 | 139.59999 |
| 500.00000 | 21.00000 | 139.59999 |
| 500.00000 | 23.00000 | 125.39999 |
| 500.00000 | 23.00000 | 110.79999 |
| 500.00000 | 23.00000 | 96.20000 |
| 500.00000 | 21.00000 | 81.29999 |
| 500.00000 | 0.0 | 81.29999 |
| 600.00000 | 0.0 | 131.00000 |
| 600.00000 | 13.50000 | 131.00000 |

ORIGINAL TABLE
OF FOUR QUANTITIES

| | | |
|------------|----------|-----------|
| 600.00000 | 18.00000 | 120.89999 |
| 600.00000 | 18.00000 | 110.79999 |
| 600.00000 | 18.00000 | 100.39999 |
| 600.00000 | 13.50000 | 89.89999 |
| 600.00000 | 0.0 | 89.89999 |
| 1000.00000 | 0.0 | 131.00000 |
| 1000.00000 | 13.50000 | 131.00000 |
| 1000.00000 | 18.00000 | 120.89999 |
| 1000.00000 | 18.00000 | 110.79999 |
| 1000.00000 | 18.00000 | 100.39999 |
| 1000.00000 | 13.50000 | 89.89999 |
| 1000.00000 | 0.0 | 89.89999 |
| | 7.00 | 10.00 |
| 133.00000 | 0.0 | 148.89999 |
| 133.00000 | 0.0 | 148.89999 |
| 133.00000 | 0.0 | 148.89999 |
| 133.00000 | 0.0 | 148.89999 |
| 133.00000 | 0.0 | 148.89999 |
| 133.00000 | 0.0 | 148.89999 |
| 133.00000 | 0.0 | 148.89999 |
| 175.29999 | 0.0 | 165.89999 |
| 175.29999 | 8.10000 | 165.89999 |
| 175.29999 | 11.70000 | 163.59999 |
| 175.29999 | 12.10000 | 161.39999 |
| 175.29999 | 12.10000 | 157.39999 |
| 175.29999 | 12.10000 | 153.79999 |
| 175.29999 | 12.10000 | 148.89999 |
| 209.29999 | 0.0 | 179.70000 |
| 209.29999 | 14.60000 | 179.70000 |
| 209.29999 | 21.09999 | 175.50000 |
| 209.29999 | 22.00000 | 171.59999 |
| 209.29999 | 22.00000 | 164.29999 |
| 209.29999 | 20.20000 | 157.79999 |
| 209.29999 | 21.89999 | 148.89999 |
| 222.29999 | 0.0 | 181.29999 |
| 222.29999 | 19.59999 | 181.29999 |
| 222.29999 | 22.70000 | 181.29999 |
| 222.29999 | 22.70000 | 174.79999 |
| 222.29999 | 22.70000 | 166.39999 |
| 222.29999 | 22.70000 | 158.89999 |
| 222.29999 | 22.70000 | 148.89999 |
| 271.00000 | 0.0 | 189.20000 |
| 271.00000 | 19.59999 | 189.20000 |
| 271.00000 | 22.70000 | 189.20000 |
| 271.00000 | 22.70000 | 181.09999 |
| 271.00000 | 22.70000 | 170.70000 |
| 271.00000 | 22.70000 | 161.39999 |
| 271.00000 | 22.70000 | 148.89999 |
| 300.00000 | 0.0 | 193.79999 |
| 300.00000 | 19.59999 | 193.79999 |
| 300.00000 | 22.70000 | 193.79999 |
| 300.00000 | 22.70000 | 184.79999 |
| 300.00000 | 22.70000 | 173.29999 |
| 300.00000 | 22.70000 | 163.00000 |
| 300.00000 | 22.70000 | 148.89999 |
| 348.59985 | 0.0 | 196.39999 |
| 348.59985 | 16.89999 | 196.39999 |
| 348.59985 | 19.59109 | 196.39999 |
| 348.59985 | 19.59109 | 186.89999 |
| 348.59985 | 19.59109 | 174.59999 |

| | | |
|-----------|-----------|-----------|
| 348.59985 | 19.59109 | 163.59999 |
| 348.59985 | 19.59109 | 148.89999 |
| 376.59985 | 0.0 | 188.09999 |
| 376.59985 | 15.30000 | 188.09999 |
| 376.59985 | 17.79999 | 188.09999 |
| 376.59985 | 17.79999 | 180.29999 |
| 376.59985 | 17.79999 | 170.09999 |
| 376.59985 | 17.79999 | 161.00000 |
| 376.59985 | 17.79999 | 148.89999 |
| 391.69995 | 0.0 | 182.89999 |
| 391.69995 | 13.50000 | 182.89999 |
| 391.69995 | 15.70000 | 182.89999 |
| 391.69995 | 15.70000 | 175.79999 |
| 391.69995 | 15.70000 | 166.50000 |
| 391.69995 | 15.70000 | 158.29999 |
| 391.69995 | 15.70000 | 147.29999 |
| 500.00000 | 0.0 | 139.59999 |
| 500.00000 | 0.0 | 139.59999 |
| 500.00000 | 0.0 | 139.59999 |
| 500.00000 | 0.0 | 139.59999 |
| 500.00000 | 0.0 | 139.59999 |
| 500.00000 | 0.0 | 139.59999 |
| 500.00000 | 0.0 | 139.59999 |
| 7.00 | 4.00 | |
| 36.00000 | 0.0 | 95.89999 |
| 36.00000 | 0.0 | 95.89999 |
| 36.00000 | 0.0 | 95.89999 |
| 36.00000 | 0.0 | 95.89999 |
| 36.00000 | 0.0 | 95.89999 |
| 36.00000 | 0.0 | 95.89999 |
| 36.00000 | 0.0 | 95.89999 |
| 58.79999 | 0.0 | 82.29999 |
| 58.79999 | -16.89999 | 82.29999 |
| 58.79999 | -22.50000 | 86.39999 |
| 58.79999 | -22.50000 | 96.20000 |
| 58.79999 | -22.50000 | 106.00000 |
| 58.79999 | -16.89999 | 108.09999 |
| 58.79999 | 0.0 | 110.20000 |
| 81.50000 | 0.0 | 78.09999 |
| 81.50000 | -22.09999 | 78.09999 |
| 81.50000 | -29.50000 | 85.00000 |
| 81.50000 | -29.50000 | 99.00000 |
| 81.50000 | -29.50000 | 113.00000 |
| 81.50000 | -22.09999 | 116.39999 |
| 81.50000 | 0.0 | 119.89999 |
| 120.89999 | 0.0 | 74.79999 |
| 120.89999 | -28.39999 | 74.79999 |
| 120.89999 | -37.79999 | 90.70000 |
| 120.89999 | -37.79999 | 108.00000 |
| 120.89999 | -37.79999 | 125.89999 |
| 120.89999 | -28.39999 | 136.70000 |
| 120.89999 | 0.0 | 147.59999 |
| 7.00 | 13.00 | |
| 120.89999 | 0.0 | 74.79999 |
| 120.89999 | -28.39999 | 74.79999 |
| 120.89999 | -37.79999 | 90.70000 |
| 120.89999 | -37.79999 | 108.00000 |
| 120.89999 | -37.79999 | 125.89999 |
| 120.89999 | -28.39999 | 136.70000 |
| 120.89999 | 0.0 | 147.59999 |

ORIGINAL PAGE IS
OF POOR QUALITY

| | | |
|-----------|-----------|-----------|
| 133.00000 | 0.0 | 72.79999 |
| 133.00000 | -29.20000 | 72.79999 |
| 133.00000 | -38.89999 | 91.79999 |
| 133.00000 | -38.89999 | 110.79999 |
| 133.00000 | -38.89999 | 129.89999 |
| 133.00000 | -29.20000 | 148.89999 |
| 133.00000 | 0.0 | 148.89999 |
| 175.29999 | 0.0 | 72.79999 |
| 175.29999 | -29.20000 | 72.79999 |
| 175.29999 | -38.89999 | 91.79999 |
| 175.29999 | -38.89999 | 110.79999 |
| 175.29999 | -38.89999 | 129.89999 |
| 175.29999 | -29.20000 | 148.89999 |
| 175.29999 | -12.10000 | 148.89999 |
| 209.29999 | 0.0 | 72.79999 |
| 209.29999 | -29.20000 | 72.79999 |
| 209.29999 | -38.89999 | 91.79999 |
| 209.29999 | -38.89999 | 110.79999 |
| 209.29999 | -38.89999 | 129.89999 |
| 209.29999 | -29.20000 | 148.89999 |
| 209.29999 | -21.89999 | 148.89999 |
| 222.29999 | 0.0 | 72.79999 |
| 222.29999 | -29.20000 | 72.79999 |
| 222.29999 | -38.89999 | 91.79999 |
| 222.29999 | -38.89999 | 110.79999 |
| 222.29999 | -38.89999 | 129.89999 |
| 222.29999 | -29.20000 | 148.89999 |
| 222.29999 | -22.70000 | 148.89999 |
| 271.00000 | 0.0 | 72.79999 |
| 271.00000 | -29.20000 | 72.79999 |
| 271.00000 | -38.89999 | 91.79999 |
| 271.00000 | -38.89999 | 110.79999 |
| 271.00000 | -38.89999 | 129.89999 |
| 271.00000 | -29.20000 | 148.89999 |
| 271.00000 | -22.70000 | 148.89999 |
| 300.00000 | 0.0 | 72.79999 |
| 300.00000 | -29.20000 | 72.79999 |
| 300.00000 | -38.89999 | 91.79999 |
| 300.00000 | -38.89999 | 110.79999 |
| 300.00000 | -38.89999 | 129.89999 |
| 300.00000 | -29.20000 | 148.89999 |
| 300.00000 | -22.70000 | 148.89999 |
| 376.60010 | 0.0 | 72.79999 |
| 376.60010 | -29.20000 | 72.79999 |
| 376.60010 | -38.89999 | 91.79999 |
| 376.60010 | -38.89999 | 110.79999 |
| 376.60010 | -38.89999 | 129.89999 |
| 376.60010 | -29.20000 | 148.89999 |
| 376.60010 | -17.79999 | 148.89999 |
| 391.69995 | 0.0 | 74.39999 |
| 391.69995 | -22.00000 | 74.39999 |
| 391.69995 | -37.29999 | 92.59999 |
| 391.69995 | -37.29999 | 110.79999 |
| 391.69995 | -37.29999 | 129.00000 |
| 391.69995 | -23.00000 | 147.29999 |
| 391.69995 | -15.70000 | 147.29999 |
| 445.69995 | 0.0 | 77.79999 |
| 445.69995 | -24.50000 | 77.79999 |
| 445.69995 | -32.70000 | 94.39999 |
| 445.69995 | -32.70000 | 110.79999 |

| | | |
|------------|-----------|-----------|
| 445.69995 | -32.70000 | 127.20000 |
| 445.69995 | -24.50000 | 143.45999 |
| 445.69995 | -7.87174 | 143.45999 |
| 500.00000 | 0.0 | 81.29999 |
| 500.00000 | -21.00000 | 81.29999 |
| 500.00000 | -28.00000 | 96.20000 |
| 500.00000 | -28.00000 | 110.79999 |
| 500.00000 | -28.00000 | 125.39999 |
| 500.00000 | -21.00000 | 139.59999 |
| 500.00000 | 0.0 | 139.59999 |
| 600.00000 | 0.0 | 89.89999 |
| 600.00000 | -13.50000 | 89.89999 |
| 600.00000 | -18.00000 | 100.39999 |
| 600.00000 | -18.00000 | 110.79999 |
| 600.00000 | -18.00000 | 120.89999 |
| 600.00000 | -13.50000 | 131.00000 |
| 600.00000 | 0.0 | 131.00000 |
| 1000.00000 | 0.0 | 89.89999 |
| 1000.00000 | -13.50000 | 89.89999 |
| 1000.00000 | -18.00000 | 100.39999 |
| 1000.00000 | -18.00000 | 110.79999 |
| 1000.00000 | -18.00000 | 120.89999 |
| 1000.00000 | -13.50000 | 131.00000 |
| 1000.00000 | 0.0 | 131.00000 |
| | 7.00 | 10.00 |
| 133.00000 | 0.0 | 148.89999 |
| 133.00000 | 0.0 | 148.89999 |
| 133.00000 | 0.0 | 148.89999 |
| 133.00000 | 0.0 | 148.89999 |
| 133.00000 | 0.0 | 148.89999 |
| 133.00000 | 0.0 | 148.89999 |
| 133.00000 | 0.0 | 148.89999 |
| 175.29999 | -12.10000 | 148.89999 |
| 175.29999 | -12.10000 | 153.79999 |
| 175.29999 | -12.10000 | 157.39999 |
| 175.29999 | -12.10000 | 161.39999 |
| 175.29999 | -11.70000 | 163.59999 |
| 175.29999 | -8.10000 | 165.89999 |
| 175.29999 | 0.0 | 165.89999 |
| 209.29999 | -21.89999 | 148.89999 |
| 209.29999 | -20.20000 | 157.79999 |
| 209.29999 | -22.00000 | 164.29999 |
| 209.29999 | -22.00000 | 171.59999 |
| 209.29999 | -21.09999 | 175.50000 |
| 209.29999 | -14.60000 | 179.70000 |
| 209.29999 | 0.0 | 179.70000 |
| 222.29999 | -22.70000 | 148.89999 |
| 222.29999 | -22.70000 | 158.89999 |
| 222.29999 | -22.70000 | 166.39999 |
| 222.29999 | -22.70000 | 174.79999 |
| 222.29999 | -22.70000 | 181.29999 |
| 222.29999 | -19.59999 | 181.29999 |
| 222.29999 | 0.0 | 181.29999 |
| 271.00000 | -22.70000 | 148.89999 |
| 271.00000 | -22.70000 | 161.39999 |
| 271.00000 | -22.70000 | 170.70000 |
| 271.00000 | -22.70000 | 181.09999 |
| 271.00000 | -22.70000 | 189.20000 |
| 271.00000 | -19.59999 | 189.20000 |
| 271.00000 | 0.0 | 189.20000 |

ORIGINAL PARTS
OF POOR QUALITY

| | | |
|-----------|-----------|-----------|
| 300.00000 | -22.70000 | 148.89999 |
| 300.00000 | -22.70000 | 163.00000 |
| 300.00000 | -22.70000 | 173.29999 |
| 300.00000 | -22.70000 | 184.79999 |
| 300.00000 | -22.70000 | 193.79999 |
| 300.00000 | -19.59999 | 193.79999 |
| 300.00000 | 0.0 | 193.79999 |
| 348.60010 | -19.59109 | 148.89999 |
| 348.60010 | -19.59109 | 163.59999 |
| 348.60010 | -19.59109 | 174.59999 |
| 348.60010 | -19.59109 | 186.89999 |
| 348.60010 | -19.59109 | 196.39999 |
| 348.60010 | -16.89999 | 196.39999 |
| 348.60010 | 0.0 | 196.39999 |
| 376.60010 | -17.79999 | 148.89999 |
| 376.60010 | -17.79999 | 161.00000 |
| 376.60010 | -17.79999 | 170.09999 |
| 376.60010 | -17.79999 | 180.29999 |
| 376.60010 | -17.79999 | 188.09999 |
| 376.60010 | -15.30000 | 188.09999 |
| 376.60010 | 0.0 | 188.09999 |
| 391.69995 | -15.70000 | 147.29999 |
| 391.69995 | -15.70000 | 158.29999 |
| 391.69995 | -15.70000 | 166.50000 |
| 391.69995 | -15.70000 | 175.79999 |
| 391.69995 | -15.70000 | 182.89999 |
| 391.69995 | -13.50000 | 182.89999 |
| 391.69995 | 0.0 | 182.89999 |
| 500.00000 | 0.0 | 139.59999 |
| 500.00000 | 0.0 | 139.59999 |
| 500.00000 | 0.0 | 139.59999 |
| 500.00000 | 0.0 | 139.59999 |
| 500.00000 | 0.0 | 139.59999 |
| 500.00000 | 0.0 | 139.59999 |
| 500.00000 | 0.0 | 139.59999 |

| | | |
|----|-------|-------|
| 9. | 8. | |
| | 175.6 | 79.9 |
| | 175.6 | 79.9 |
| | 175.6 | 79.9 |
| | 175.6 | 79.9 |
| | 175.6 | 79.9 |
| | 175.6 | 79.9 |
| | 175.6 | 79.9 |
| | 175.6 | 79.9 |
| | 175.6 | 79.9 |
| | 175.6 | 79.9 |
| | 211.9 | 79.9 |
| | 211.5 | 64.8 |
| | 210.4 | 58.6 |
| | 207.3 | 64.8 |
| | 208.9 | 79.9 |
| | 209.3 | 95.0 |
| | 210.4 | 101.2 |
| | 211.5 | 95.0 |
| | 211.9 | 79.9 |
| | 225.9 | 79.9 |
| | 225.3 | 61.9 |
| | 224.0 | 54.4 |
| | 222.8 | 61.9 |
| | 222.2 | 79.9 |
| | 222.8 | 97.9 |
| | | 120.3 |
| | | 120.3 |
| | | 120.3 |
| | | 120.3 |
| | | 120.3 |
| | | 120.3 |
| | | 120.3 |
| | | 101.5 |
| | | 107.7 |
| | | 122.8 |
| | | 137.8 |
| | | 144.0 |
| | | 137.8 |
| | | 122.8 |
| | | 107.7 |
| | | 101.5 |
| | | 98.3 |
| | | 105.7 |
| | | 123.7 |
| | | 141.7 |
| | | 149.2 |
| | | 141.7 |

| | | |
|-------|-------|-------|
| 224.0 | 105.4 | 123.7 |
| 225.3 | 97.9 | 105.7 |
| 225.9 | 79.9 | 98.3 |
| 248.4 | 79.9 | 99.4 |
| 247.9 | 61.5 | 107.0 |
| 246.6 | 53.9 | 125.3 |
| 245.3 | 61.5 | 143.7 |
| 244.7 | 79.9 | 151.3 |
| 245.3 | 98.3 | 143.7 |
| 246.6 | 105.9 | 125.3 |
| 247.9 | 98.3 | 107.0 |
| 248.4 | 79.9 | 99.4 |
| 267.1 | 79.9 | 102.4 |
| 266.6 | 62.6 | 109.5 |
| 265.3 | 55.5 | 126.7 |
| 264.1 | 62.6 | 143.9 |
| 263.6 | 79.9 | 151.0 |
| 264.1 | 97.2 | 143.9 |
| 265.3 | 104.3 | 126.7 |
| 266.6 | 97.2 | 109.5 |
| 267.1 | 79.9 | 102.4 |
| 299.3 | 79.9 | 104.7 |
| 298.8 | 62.6 | 111.8 |
| 297.6 | 55.5 | 129.0 |
| 296.3 | 62.6 | 146.2 |
| 295.8 | 79.9 | 153.3 |
| 296.3 | 97.2 | 146.2 |
| 297.6 | 104.3 | 129.0 |
| 298.8 | 97.2 | 111.8 |
| 299.3 | 79.9 | 104.7 |
| 700.7 | 79.9 | 133.4 |
| 700.2 | 62.6 | 140.6 |
| 699.0 | 55.5 | 157.8 |
| 697.7 | 62.6 | 175.0 |
| 697.2 | 79.9 | 182.1 |
| 697.7 | 97.2 | 175.0 |
| 699.0 | 104.3 | 157.8 |
| 700.2 | 97.2 | 140.6 |
| 700.7 | 79.9 | 133.4 |
| 1000. | 79.9 | 133.4 |
| 1000. | 62.6 | 140.6 |
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| 1000. | 79.9 | 182.1 |
| 1000. | 97.2 | 175.0 |
| 1000. | 104.3 | 157.8 |
| 1000. | 97.2 | 140.6 |
| 1000. | 79.9 | 133.4 |

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| 9. | 8. | |
| 175.60 | -79.90 | 120.30 |
| 175.60 | -79.90 | 120.30 |
| 175.60 | -79.90 | 120.30 |
| 175.60 | -79.90 | 120.30 |
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| 175.60 | -79.90 | 120.30 |
| 211.90 | -79.90 | 101.50 |
| 211.50 | -95.00 | 107.70 |

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| 209.30 | -95.00 | 137.80 |
| 208.90 | -79.90 | 144.00 |
| 209.30 | -64.80 | 137.80 |
| 210.40 | -58.60 | 122.80 |
| 211.50 | -64.80 | 107.70 |
| 211.90 | -79.90 | 101.50 |
| 225.90 | -79.90 | 98.30 |
| 225.30 | -97.90 | 105.70 |
| 224.00 | -105.40 | 123.70 |
| 222.80 | -97.90 | 141.70 |
| 222.20 | -79.90 | 149.20 |
| 222.80 | -61.90 | 141.70 |
| 224.00 | -54.40 | 123.70 |
| 225.30 | -61.90 | 145.70 |
| 225.90 | -79.90 | 98.30 |
| 248.40 | -79.90 | 99.40 |
| 247.90 | -98.30 | 107.00 |
| 246.60 | -105.90 | 125.30 |
| 245.30 | -98.30 | 143.70 |
| 244.70 | -79.90 | 151.30 |
| 245.30 | -61.50 | 143.70 |
| 246.60 | -53.90 | 125.30 |
| 247.90 | -61.50 | 107.00 |
| 248.40 | -79.90 | 99.40 |
| 267.10 | -79.90 | 102.40 |
| 266.60 | -97.20 | 109.50 |
| 265.30 | -104.30 | 126.70 |
| 264.10 | -97.20 | 143.90 |
| 263.60 | -79.90 | 151.00 |
| 264.10 | -62.60 | 143.90 |
| 265.30 | -55.50 | 126.70 |
| 266.60 | -62.60 | 109.50 |
| 267.10 | -79.90 | 102.40 |
| 299.30 | -79.90 | 104.70 |
| 298.80 | -97.20 | 111.80 |
| 297.60 | -104.30 | 129.00 |
| 296.30 | -97.20 | 146.20 |
| 295.80 | -79.90 | 153.30 |
| 296.30 | -62.60 | 146.20 |
| 297.60 | -55.50 | 129.00 |
| 298.80 | -62.60 | 111.80 |
| 299.30 | -79.90 | 104.70 |
| 700.70 | -79.90 | 133.40 |
| 700.20 | -97.20 | 140.60 |
| 699.00 | -104.30 | 157.80 |
| 697.70 | -97.20 | 175.00 |
| 697.20 | -79.90 | 182.10 |
| 697.70 | -62.60 | 175.00 |
| 699.00 | -55.50 | 157.80 |
| 700.20 | -62.60 | 140.60 |
| 700.70 | -79.90 | 133.40 |
| 1000.00 | -79.90 | 133.40 |
| 1000.00 | -97.20 | 140.60 |
| 1000.00 | -104.30 | 157.80 |
| 1000.00 | -97.20 | 175.00 |
| 1000.00 | -79.90 | 182.10 |
| 1000.00 | -62.60 | 175.00 |
| 1000.00 | -55.50 | 157.80 |
| 1000.00 | -62.60 | 140.60 |

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| | 1000.00 | -79.90 | 133.40 | | | | |
| END | | | | | | | |
| AERO | | | | | | | |
| | 0. | 0.0 | 0.0 | | | | |
| FORC | | | | | | | |
| 307.5 | 0. | 75.52 | 52112. | 98.1 | 531.2 | 0. | |
| END | | | | | | | |

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CASE
RSRA FUSELAGE, WINGS AND ENGINES
J D COWAN AERO RESEARCH ORGN 7440 EXT 7834

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|-------|------|-------|-----|
| GEOM | | | |
| 3. | 746. | 1. | -1. |
| SOUR | | | |
| 18. | | | |
| 7. | 4. | | |
| 36. | 0. | 95.9 | |
| 36. | 0. | 95.9 | |
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| 36. | 0.0 | 95.9 | |
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| 36. | 0.0 | 95.9 | |
| 36. | 0.0 | 95.9 | |
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| 58.8 | 16.9 | 108.1 | |
| 58.8 | 22.5 | 106. | |
| 58.8 | 22.5 | 96.2 | |
| 58.8 | 22.5 | 86.4 | |
| 58.8 | 16.7 | 82.3 | |
| 58.8 | 0.0 | 82.3 | |
| 81.5 | 0.0 | 119.9 | |
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| 81.5 | 29.5 | 113. | |
| 81.5 | 29.5 | 99. | |
| 81.5 | 29.5 | 85. | |
| 81.5 | 22.1 | 78.1 | |
| 81.5 | 0.0 | 78.1 | |
| 120.9 | 0. | 147.6 | |
| 120.9 | 28.4 | 136.7 | |
| 120.9 | 37.8 | 125.9 | |
| 120.9 | 37.8 | 108. | |
| 120.9 | 37.8 | 90.7 | |
| 120.9 | 28.4 | 74.8 | |
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| 7. | 6. | | |
| 120.9 | 0. | 147.6 | |
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| 120.9 | 37.8 | 108. | |
| 120.9 | 37.8 | 90.7 | |
| 120.9 | 28.4 | 74.8 | |
| 120.9 | 0. | 74.8 | |
| 133. | 0. | 148.9 | |
| 133. | 29.2 | 148.9 | |
| 133. | 38.9 | 129.9 | |
| 133. | 38.9 | 110.8 | |
| 133. | 38.9 | 91.8 | |
| 133. | 29.2 | 72.8 | |
| 133. | 0. | 72.8 | |
| 175.3 | 12.1 | 148.9 | |
| 175.3 | 29.2 | 148.9 | |
| 175.3 | 38.9 | 129.9 | |
| 175.3 | 38.9 | 110.8 | |
| 175.3 | 38.9 | 91.8 | |

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| 175.3 | 29.2 | 72.8 |
| 175.3 | 0. | 72.8 |
| 209.3 | 21.9 | 148.9 |
| 209.3 | 29.2 | 148.9 |
| 209.3 | 38.9 | 129.9 |
| 209.3 | 38.9 | 110.8 |
| 209.3 | 38.9 | 91.8 |
| 209.3 | 29.2 | 72.8 |
| 209.3 | 0. | 72.8 |
| 222.3 | 22.7 | 148.9 |
| 222.3 | 29.2 | 148.9 |
| 222.3 | 38.9 | 129.9 |
| 222.3 | 38.9 | 110.8 |
| 222.3 | 38.9 | 91.8 |
| 222.3 | 29.2 | 72.8 |
| 222.3 | 0. | 72.8 |
| 271. | 22.7 | 148.9 |
| 271. | 29.2 | 148.9 |
| 271. | 38.9 | 129.9 |
| 271. | 38.9 | 110.8 |
| 271. | 38.9 | 91.8 |
| 271. | 29.2 | 72.8 |
| 271. | 0. | 72.8 |
| 6. | 4. | |
| 271. | 22.7 | 148.9 |
| 271. | 29.2 | 148.9 |
| 271. | 38.9 | 129.9 |
| 271. | 38.9 | 110.8 |
| 271. | 38.9 | 91.8 |
| 271. | 29.2 | 72.8 |
| 300. | 22.7 | 148.9 |
| 300. | 29.2 | 148.9 |
| 300. | 38.9 | 129.9 |
| 300. | 38.9 | 110.8 |
| 300. | 38.9 | 91.8 |
| 300. | 38.9 | 85. |
| 376.6 | 17.8 | 148.9 |
| 376.6 | 29.2 | 148.9 |
| 376.6 | 38.9 | 129.9 |
| 376.6 | 38.9 | 110.8 |
| 376.6 | 38.9 | 91.8 |
| 376.6 | 38.9 | 85. |
| 391.7 | 15.7 | 147.3 |
| 391.7 | 28. | 147.3 |
| 391.7 | 37.3 | 129. |
| 391.7 | 37.3 | 110.8 |
| 391.7 | 37.3 | 92.6 |
| 391.7 | 28. | 74.4 |
| 7. | 5. | |
| 391.7 | 15.7 | 147.3 |
| 391.7 | 28. | 147.3 |
| 391.7 | 37.3 | 129. |
| 391.7 | 37.3 | 110.8 |
| 391.7 | 37.3 | 92.6 |
| 391.7 | 28. | 74.4 |
| 391.7 | 0. | 74.4 |
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| 445.7 | 24.5 | 143.46 |
| 445.7 | 32.7 | 127.2 |
| 445.7 | 32.7 | 110.8 |

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| 445.7 | 24.5 | 77.8 |
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| 500. | 0. | 139.6 |
| 500. | 21. | 139.6 |
| 500. | 27. | 125.4 |
| 500. | 28. | 110.8 |
| 500. | 28. | 96.2 |
| 500. | 21. | 81.3 |
| 500. | 0. | 81.3 |
| 600. | 0. | 131. |
| 600. | 13.5 | 131. |
| 600. | 18. | 120.9 |
| 600. | 18. | 110.8 |
| 600. | 18. | 100.4 |
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| 600. | 0. | 89.9 |
| 1000. | 0. | 131. |
| 1000. | 13.5 | 131. |
| 1000. | 18. | 120.9 |
| 1000. | 18. | 110.8 |
| 1000. | 18. | 100.4 |
| 1000. | 13.5 | 89.9 |
| 1000. | 0. | 89.9 |
| 7. | 10. | |
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| 133. | 0. | 148.9 |
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| 133. | 0. | 148.9 |
| 133. | 0. | 148.9 |
| 133. | 0. | 148.9 |
| 175.3 | 0. | 165.9 |
| 175.3 | 8.1 | 165.9 |
| 175.3 | 11.7 | 163.6 |
| 175.3 | 12.1 | 161.4 |
| 175.3 | 12.1 | 157.4 |
| 175.3 | 12.1 | 153.8 |
| 175.3 | 12.1 | 148.9 |
| 209.3 | 0. | 179.7 |
| 209.3 | 14.6 | 179.7 |
| 209.3 | 21.1 | 175.5 |
| 209.3 | 22. | 171.6 |
| 209.3 | 22. | 164.3 |
| 209.3 | 20.2 | 157.8 |
| 209.3 | 21.9 | 148.9 |
| 222.3 | 0. | 181.3 |
| 222.3 | 19.6 | 181.3 |
| 222.3 | 22.7 | 181.3 |
| 222.3 | 22.7 | 174.8 |
| 222.3 | 22.7 | 166.4 |
| 222.3 | 22.7 | 158.9 |
| 222.3 | 22.7 | 148.9 |
| 271. | 0. | 189.2 |
| 271. | 19.6 | 189.2 |
| 271. | 22.7 | 189.2 |
| 271. | 22.7 | 181.1 |
| 271. | 22.7 | 170.7 |
| 271. | 22.7 | 161.4 |
| 271. | 22.7 | 148.9 |

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| 300. | 0. | 193.8 |
| 300. | 19.6 | 193.8 |
| 300. | 22.7 | 193.8 |
| 300. | 22.7 | 184.8 |
| 300. | 22.7 | 173.3 |
| 300. | 22.7 | 163. |
| 300. | 22.7 | 148.9 |
| 348.6 | 0. | 196.4 |
| 348.6 | 16.9 | 196.4 |
| 348.6 | 19.5911 | 196.4 |
| 348.6 | 19.5911 | 186.9 |
| 348.6 | 19.5911 | 174.6 |
| 348.6 | 19.5911 | 163.6 |
| 348.6 | 19.5911 | 148.9 |
| 376.6 | 0. | 188.1 |
| 376.6 | 15.3 | 188.1 |
| 376.6 | 17.8 | 188.1 |
| 376.6 | 17.8 | 180.3 |
| 376.6 | 17.8 | 170.1 |
| 376.6 | 17.8 | 161.0 |
| 376.6 | 17.8 | 148.9 |
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| 391.7 | 13.5 | 182.9 |
| 391.7 | 15.7 | 182.9 |
| 391.7 | 15.7 | 175.8 |
| 391.7 | 15.7 | 166.5 |
| 391.7 | 15.7 | 158.3 |
| 391.7 | 15.7 | 147.3 |
| 500. | 0. | 139.6 |
| 500. | 0. | 139.6 |
| 500. | 0. | 139.6 |
| 500. | 0. | 139.6 |
| 500. | 0. | 139.6 |
| 500. | 0. | 139.6 |
| 500. | 0. | 139.6 |

| | 7.0 | 4.0 | |
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| 36. | 0. | | 95.9 |
| 36. | 0. | | 95.9 |
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| 36.0000 | -0.0000 | | 95.9000 |
| 36.0000 | -0.0000 | | 95.9000 |
| 36.0000 | -0.0000 | | 95.9000 |
| 36.0000 | -0.0000 | | 95.9000 |
| 58.8000 | -0.0000 | | 82.3000 |
| 58.8 | -16.9 | | 82.3 |
| 58.8000 | -22.5000 | | 86.4000 |
| 58.8000 | -22.5000 | | 96.2000 |
| 58.8000 | -22.5000 | | 106.0000 |
| 58.8 | -16.9 | | 108.1 |
| 58.8000 | -0.0000 | | 110.2000 |
| 81.5000 | -0.0000 | | 78.1000 |
| 81.5 | -22.1 | | 78.1 |
| 81.5000 | -29.5000 | | 85.0000 |
| 81.5000 | -29.5000 | | 99.0000 |
| 81.5000 | -29.5000 | | 113.0000 |
| 81.5 | -22.1 | | 116.4 |
| 81.5000 | -0.0000 | | 119.9000 |
| 120.9000 | -0.0000 | | 74.8000 |
| 120.9 | -28.4 | | 74.8 |
| 120.9000 | -37.8000 | | 90.7000 |

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| 120.9000 | -37.8000 | 108. |
| 120.9000 | -37.8000 | 125.9000 |
| 120.9 | -28.4 | 136.7 |
| 120.9000 | -0.0000 | 147.6000 |
| 7.0 | 6. | |
| 120.9000 | -0.0000 | 74.8000 |
| 120.9000 | -28.4000 | 74.8000 |
| 120.9000 | -37.8000 | 90.7000 |
| 120.9000 | -37.8000 | 108. |
| 120.9000 | -37.8000 | 125.9000 |
| 120.9000 | -28.4000 | 136.7000 |
| 120.9000 | -0.0000 | 147.6000 |
| 133.0000 | -0.0000 | 72.8000 |
| 133.0000 | -29.2000 | 72.8000 |
| 133.0000 | -38.9000 | 91.8000 |
| 133.0000 | -38.9000 | 110.8000 |
| 133.0000 | -38.9000 | 129.9000 |
| 133.0000 | -29.2000 | 148.9000 |
| 133.0000 | -0.0000 | 148.9000 |
| 175.3000 | -0.0000 | 72.8000 |
| 175.3000 | -29.2000 | 72.8000 |
| 175.3000 | -38.9000 | 91.8000 |
| 175.3000 | -38.9000 | 110.8000 |
| 175.3000 | -38.9000 | 129.9000 |
| 175.3000 | -29.2000 | 148.9000 |
| 175.3000 | -12.1000 | 148.9000 |
| 209.3000 | -0.0000 | 72.8000 |
| 209.3000 | -29.2000 | 72.8000 |
| 209.3000 | -38.9000 | 91.8000 |
| 209.3000 | -38.9000 | 110.8000 |
| 209.3000 | -38.9000 | 129.9000 |
| 209.3000 | -29.2000 | 148.9000 |
| 209.3000 | -21.9000 | 148.9000 |
| 222.3000 | -0.0000 | 72.8000 |
| 222.3000 | -29.2000 | 72.8000 |
| 222.3000 | -38.9000 | 91.8000 |
| 222.3000 | -38.9000 | 110.8000 |
| 222.3000 | -38.9000 | 129.9000 |
| 222.3000 | -29.2000 | 148.9000 |
| 222.3000 | -22.7000 | 148.9000 |
| 271.0000 | -0.0000 | 72.8000 |
| 271.0000 | -29.2000 | 72.8000 |
| 271.0000 | -38.9000 | 91.8000 |
| 271.0000 | -38.9000 | 110.8000 |
| 271.0000 | -38.9000 | 129.9000 |
| 271.0000 | -29.2000 | 148.9000 |
| 271. | -22.7 | 148.9000 |
| 6. | 4. | |
| 271.0000 | -29.2000 | 72.8 |
| 271.0000 | -38.9000 | 91.8 |
| 271.0000 | -38.9000 | 110.8000 |
| 271.0000 | -38.9000 | 129.9000 |
| 271.0000 | -29.2000 | 148.9000 |
| 271.0000 | -22.7000 | 148.9000 |
| 300. | -38.9 | 85. |
| 300. | -38.9 | 91.8 |
| 300. | -38.9 | 110.8 |
| 300. | -38.9 | 129.9 |
| 300. | -29.2 | 148.9 |
| 300. | -22.7 | 148.9 |

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| 376.6 | -38.9 | 85. |
| 376.6 | -38.9 | 91.8 |
| 376.6 | -38.9 | 110.8 |
| 376.6 | -38.9 | 129.9 |
| 376.6 | -29.2 | 148.9 |
| 376.6 | -17.8 | 148.9 |
| 391.7 | -28. | 74.4 |
| 391.7 | -37.3 | 92.6 |
| 391.7 | -37.3 | 110.8 |
| 391.7 | -37.3 | 129. |
| 391.7 | -28. | 147.3 |
| 391.7 | -15.7 | 147.3 |
| 7. | 5. | |
| 391.7000 | -0.0000 | 74.4000 |
| 391.7000 | -28.0000 | 74.4000 |
| 391.7000 | -37.3000 | 92.6000 |
| 391.7000 | -37.3000 | 110.8000 |
| 391.7000 | -37.3000 | 129.0000 |
| 391.7000 | -28.0000 | 147.3000 |
| 391.7000 | -15.7000 | 147.3000 |
| 445.7000 | -0.0000 | 77.8000 |
| 445.7000 | -24.5000 | 77.8000 |
| 445.7000 | -32.7000 | 94.4000 |
| 445.7000 | -32.7000 | 110.8000 |
| 445.7000 | -32.7000 | 127.2000 |
| 445.7000 | -24.5000 | 143.4600 |
| 445.7000 | -7.871745 | 143.4600 |
| 500.0000 | -0.0000 | 81.3000 |
| 500.0000 | -21.0000 | 81.3000 |
| 500.0000 | -28.0000 | 96.2000 |
| 500.0000 | -28.0000 | 110.8000 |
| 500.0000 | -28.0000 | 125.4000 |
| 500.0000 | -21.0000 | 139.6000 |
| 500.0000 | -0.0000 | 139.6000 |
| 600.0000 | -0.0000 | 89.9000 |
| 600.0000 | -13.5000 | 89.9000 |
| 600.0000 | -18.0000 | 100.4000 |
| 600.0000 | -18.0000 | 110.8000 |
| 600.0000 | -18.0000 | 120.9000 |
| 600.0000 | -13.5000 | 131.0000 |
| 600.0000 | -0.0000 | 131.0000 |
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| 1000.0000 | -13.5000 | 89.9000 |
| 1000.0000 | -18.0000 | 100.4000 |
| 1000.0000 | -18.0000 | 110.8000 |
| 1000.0000 | -18.0000 | 120.9000 |
| 1000.0000 | -13.5000 | 131.0000 |
| 1000.0000 | -0.0000 | 131.0000 |
| 7.0 | 10.0 | |
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| 133.0000 | -0.0000 | 148.9000 |
| 133.0000 | -0.0000 | 148.9000 |
| 133.0000 | -0.0000 | 148.9000 |
| 133.0000 | -0.0000 | 148.9000 |
| 133.0000 | -0.0000 | 148.9000 |
| 133.0000 | -0.0000 | 148.9000 |
| 175.3000 | -12.1000 | 148.9000 |
| 175.3000 | -12.1000 | 153.8000 |
| 175.3000 | -12.1000 | 157.4000 |
| 175.3000 | -12.1000 | 161.4000 |

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| 175.3000 | -11.7000 | 163.6000 |
| 175.3000 | -8.1000 | 165.9000 |
| 175.3000 | -0.0000 | 165.9000 |
| 209.3000 | -21.9000 | 148.9000 |
| 209.3000 | -20.2000 | 157.8000 |
| 209.3000 | -22.0000 | 164.3000 |
| 209.3000 | -22.0000 | 171.6000 |
| 209.3000 | -21.1000 | 175.5000 |
| 209.3000 | -14.6000 | 179.7000 |
| 209.3000 | -0.0000 | 179.7000 |
| 222.3000 | -22.7000 | 148.9000 |
| 222.3000 | -22.7000 | 158.9000 |
| 222.3000 | -22.7000 | 166.4000 |
| 222.3000 | -22.7000 | 174.8000 |
| 222.3000 | -22.7000 | 181.3000 |
| 222.3000 | -19.6000 | 181.3000 |
| 222.3000 | -0.0000 | 181.3000 |
| 271.0000 | -22.7000 | 148.9000 |
| 271.0000 | -22.7000 | 161.4000 |
| 271.0000 | -22.7000 | 170.7000 |
| 271.0000 | -22.7000 | 181.1000 |
| 271.0000 | -22.7000 | 189.2000 |
| 271.0000 | -19.6000 | 189.2000 |
| 271.0000 | -0.0000 | 189.2000 |
| 300.0000 | -22.7000 | 148.9000 |
| 300.0000 | -22.7000 | 163.0000 |
| 300.0000 | -22.7000 | 173.3000 |
| 300.0000 | -22.7000 | 184.8000 |
| 300.0000 | -22.7000 | 193.8000 |
| 300.0000 | -19.6000 | 193.8000 |
| 300.0000 | -0.0000 | 193.8000 |
| 348.6001 | -19.5911 | 148.9000 |
| 348.6001 | -19.5911 | 163.6000 |
| 348.6001 | -19.5911 | 174.6000 |
| 348.6001 | -19.5911 | 186.9000 |
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| 348.6001 | -0.0000 | 196.4000 |
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| 376.6001 | -17.8000 | 161.0000 |
| 376.6001 | -17.8000 | 170.1000 |
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| 376.6001 | -15.3000 | 188.1000 |
| 376.6001 | -0.0000 | 188.1000 |
| 391.7000 | -15.7000 | 147.3000 |
| 391.7000 | -15.7000 | 158.3000 |
| 391.7000 | -15.7000 | 166.5000 |
| 391.7000 | -15.7000 | 175.8000 |
| 391.7000 | -15.7000 | 182.9000 |
| 391.7000 | -13.5000 | 182.9000 |
| 391.7000 | -0.0000 | 182.9000 |
| 500. | -0.0000 | 139.6000 |
| 500. | -0.0000 | 139.6000 |
| 500. | -0.0000 | 139.6000 |
| 500. | -0.0000 | 139.6 |
| 500. | -0.0000 | 139.6 |
| 500. | -0.0000 | 139.6000 |
| 500. | -0.0000 | 139.6000 |
| 17. | 10. | |

| | | |
|--------|--------|-------|
| 391.36 | 56.65 | 71.07 |
| 369.4 | 56.17 | 75.35 |
| 347.29 | 55.71 | 79.4 |
| 325.04 | 55.47 | 81.52 |
| 308.31 | 55.55 | 80.88 |
| 297.19 | 55.74 | 79.13 |
| 288.89 | 56. | 76.84 |
| 283.43 | 56.29 | 74.32 |
| 280.98 | 56.64 | 71.21 |
| 284.09 | 56.93 | 68.64 |
| 289.67 | 56.1 | 67.16 |
| 297.92 | 57.23 | 65.97 |
| 308.87 | 57.32 | 65.2 |
| 325.25 | 57.3 | 65.32 |
| 347.14 | 57.06 | 67.44 |
| 369.18 | 56.74 | 70.29 |
| 391.36 | 56.65 | 71.07 |
| 389.72 | 79.71 | 73.68 |
| 368.48 | 79.24 | 77.81 |
| 347.11 | 78.8 | 81.73 |
| 325.59 | 78.57 | 83.78 |
| 309.41 | 78.64 | 83.16 |
| 298.65 | 78.83 | 81.47 |
| 290.63 | 79.08 | 79.26 |
| 285.35 | 79.35 | 76.82 |
| 282.98 | 79.69 | 73.81 |
| 285.99 | 79.97 | 71.32 |
| 291.38 | 80.13 | 69.9 |
| 299.36 | 80.26 | 68.74 |
| 309.95 | 80.35 | 67.99 |
| 325.79 | 80.33 | 68.12 |
| 346.96 | 80.1 | 70.17 |
| 368.27 | 79.79 | 72.92 |
| 389.72 | 79.71 | 73.68 |
| 388.08 | 102.76 | 76.28 |
| 367.57 | 102.31 | 80.28 |
| 346.92 | 101.88 | 84.06 |
| 326.13 | 101.66 | 86.04 |
| 310.51 | 101.73 | 85.44 |
| 300.12 | 101.91 | 83.81 |
| 292.37 | 102.15 | 81.67 |
| 287.27 | 102.42 | 79.32 |
| 284.98 | 102.75 | 76.41 |
| 287.89 | 103.02 | 74.01 |
| 293.09 | 103.17 | 72.63 |
| 300.8 | 103.3 | 71.51 |
| 311.03 | 103.38 | 70.79 |
| 326.33 | 103.37 | 70.91 |
| 346.78 | 103.14 | 72.89 |
| 367.36 | 102.84 | 75.55 |
| 388.08 | 102.76 | 76.28 |
| 386.44 | 125.81 | 78.89 |
| 366.65 | 125.38 | 82.74 |
| 346.73 | 124.97 | 86.39 |
| 326.68 | 124.75 | 88.3 |
| 311.61 | 124.82 | 87.72 |
| 301.59 | 124.99 | 86.15 |
| 294.11 | 125.23 | 84.09 |
| 289.19 | 125.48 | 81.82 |
| 286.98 | 125.8 | 79.01 |

ORIGINAL PAGE IS
OF POOR QUALITY

| | | |
|--------|--------|-------|
| 289.79 | 126.06 | 76.69 |
| 294.81 | 126.21 | 75.36 |
| 302.25 | 126.33 | 74.29 |
| 312.11 | 126.41 | 73.59 |
| 326.87 | 126.4 | 73.71 |
| 346.59 | 126.18 | 75.62 |
| 366.45 | 125.89 | 78.18 |
| 386.44 | 125.81 | 78.89 |
| 384.8 | 148.87 | 81.49 |
| 365.74 | 148.45 | 85.2 |
| 346.55 | 148.05 | 88.72 |
| 327.23 | 147.84 | 90.56 |
| 312.71 | 147.91 | 90. |
| 303.05 | 148.08 | 88.49 |
| 295.85 | 148.3 | 86.5 |
| 291.11 | 148.55 | 84.31 |
| 288.98 | 148.85 | 81.61 |
| 291.68 | 149.11 | 79.38 |
| 296.52 | 149.25 | 78.1 |
| 303.69 | 149.37 | 77.06 |
| 313.19 | 149.44 | 76.39 |
| 327.41 | 149.43 | 76.5 |
| 346.41 | 149.22 | 78.34 |
| 365.54 | 148.94 | 80.81 |
| 384.8 | 148.87 | 81.49 |
| 383.16 | 171.92 | 84.1 |
| 364.82 | 171.52 | 87.67 |
| 346.36 | 171.13 | 91.05 |
| 327.78 | 170.93 | 92.82 |
| 313.81 | 171. | 92.28 |
| 304.52 | 171.16 | 90.82 |
| 297.59 | 171.38 | 88.91 |
| 293.03 | 171.61 | 86.81 |
| 290.99 | 171.91 | 84.21 |
| 293.58 | 172.15 | 82.06 |
| 298.24 | 172.29 | 80.83 |
| 305.13 | 172.4 | 79.83 |
| 314.27 | 172.47 | 79.19 |
| 327.95 | 172.46 | 79.29 |
| 346.23 | 172.26 | 81.86 |
| 364.63 | 171.99 | 83.44 |
| 383.16 | 171.92 | 84.1 |
| 381.52 | 194.97 | 86.7 |
| 363.91 | 194.59 | 90.13 |
| 346.17 | 194.22 | 93.38 |
| 328.32 | 194.03 | 95.03 |
| 314.91 | 194.09 | 94.56 |
| 305.98 | 194.24 | 93.16 |
| 299.33 | 194.45 | 91.33 |
| 294.95 | 194.68 | 89.31 |
| 292.99 | 194.96 | 86.81 |
| 295.48 | 195.19 | 84.75 |
| 299.95 | 195.33 | 83.56 |
| 306.57 | 195.44 | 82.6 |
| 315.35 | 195.51 | 81.98 |
| 328.49 | 195.49 | 82.09 |
| 346.05 | 195.3 | 83.79 |
| 363.73 | 195.04 | 86.07 |
| 381.52 | 194.97 | 86.7 |
| 379.88 | 218.03 | 89.3 |

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|----------|----------|---------|
| 362.99 | 217.66 | 92.59 |
| 345.99 | 217.3 | 95.71 |
| 328.87 | 217.12 | 97.34 |
| 316.01 | 217.18 | 96.84 |
| 307.45 | 217.33 | 95.5 |
| 301.07 | 217.53 | 93.74 |
| 296.87 | 217.74 | 91.8 |
| 294.99 | 218.02 | 89.41 |
| 297.38 | 218.24 | 87.43 |
| 301.67 | 218.37 | 86.3 |
| 308.01 | 218.47 | 85.38 |
| 316.43 | 218.54 | 84.78 |
| 329.03 | 218.53 | 84.83 |
| 345.87 | 218.34 | 86.51 |
| 362.82 | 218.10 | 88.7 |
| 379.88 | 218.03 | 89.3 |
| 378.24 | 241.08 | 91.91 |
| 362.07 | 240.72 | 95.06 |
| 345.8 | 240.39 | 98.04 |
| 329.42 | 240.21 | 99.6 |
| 317.11 | 240.27 | 99.13 |
| 308.92 | 240.41 | 97.84 |
| 302.81 | 240.6 | 96.15 |
| 298.79 | 240.81 | 94.3 |
| 296.99 | 240.07 | 92.01 |
| 299.28 | 241.28 | 90.12 |
| 303.38 | 241.41 | 89.03 |
| 309.45 | 241.5 | 88.15 |
| 317.51 | 241.57 | 87.58 |
| 329.57 | 241.56 | 87.68 |
| 345.69 | 241.38 | 89.23 |
| 361.91 | 241.15 | 91.33 |
| 378.24 | 241.08 | 91.91 |
| 376.6 | 264.13 | 94.51 |
| 361.16 | 263.79 | 97.52 |
| 345.61 | 263.47 | 100.37 |
| 329.97 | 263.3 | 101.86 |
| 318.21 | 263.35 | 101.41 |
| 310.38 | 263.49 | 100.18 |
| 304.55 | 263.68 | 98.57 |
| 300.71 | 263.88 | 96.8 |
| 298.99 | 264.12 | 94.61 |
| 301.17 | 264.33 | 92.8 |
| 305.09 | 264.44 | 91.76 |
| 310.9 | 264.54 | 90.92 |
| 318.59 | 264.6 | 90.38 |
| 330.11 | 264.59 | 90.47 |
| 345.51 | 264.42 | 91.96 |
| 361. | 264.2 | 93.96 |
| 376.6 | 264.13 | 94.51 |
| 17.0 | 10.0 | |
| 391.3601 | -56.6500 | 71.0700 |
| 369.1799 | -56.7400 | 70.2900 |
| 347.1399 | -57.0600 | 67.4400 |
| 325.2500 | -57.3000 | 65.3200 |
| 308.8701 | -57.3200 | 65.2000 |
| 297.9199 | -57.2300 | 65.9700 |
| 289.6699 | -56.1000 | 67.1600 |
| 284.0901 | -56.9300 | 68.6400 |
| 280.9800 | -56.6400 | 71.2100 |

ORIGINAL PAGE IS
OF POOR QUALITY

| | | |
|----------|-----------|---------|
| 283.4299 | -56.2900 | 74.3200 |
| 288.8399 | -56.0000 | 76.8400 |
| 297.1899 | -55.7400 | 79.1300 |
| 308.3101 | -55.5500 | 80.8800 |
| 325.0400 | -55.4700 | 81.5200 |
| 347.2900 | -55.7100 | 79.4000 |
| 369.3999 | -56.1700 | 75.3500 |
| 391.3601 | -56.6500 | 71.0700 |
| 389.7200 | -79.7100 | 73.6800 |
| 368.2700 | -79.7900 | 72.9200 |
| 346.9600 | -80.1000 | 70.1700 |
| 325.7900 | -80.3300 | 68.1200 |
| 309.9500 | -80.3500 | 67.9900 |
| 299.3601 | -80.2600 | 68.7400 |
| 291.3799 | -80.1300 | 69.9000 |
| 285.9900 | -79.9700 | 71.3200 |
| 282.9800 | -79.6900 | 73.8100 |
| 285.3501 | -79.3500 | 76.8200 |
| 290.6299 | -79.0800 | 79.2600 |
| 298.6499 | -78.8300 | 81.4700 |
| 309.4099 | -78.6400 | 83.1600 |
| 325.5901 | -78.5700 | 83.7800 |
| 347.1101 | -78.8000 | 81.7300 |
| 368.4800 | -79.2400 | 77.8100 |
| 389.7200 | -79.7100 | 73.6800 |
| 388.0801 | -102.7600 | 76.2800 |
| 367.3601 | -102.8400 | 75.5500 |
| 346.7800 | -103.1400 | 72.8900 |
| 326.3301 | -103.3700 | 70.9100 |
| 311.0300 | -103.3800 | 70.7900 |
| 300.8000 | -103.3000 | 71.5100 |
| 293.0901 | -103.1700 | 72.6300 |
| 287.8399 | -103.0200 | 74.0100 |
| 284.9800 | -102.7500 | 76.4100 |
| 287.2700 | -102.4200 | 79.3200 |
| 292.3701 | -102.1500 | 81.6700 |
| 300.1201 | -101.9100 | 83.8100 |
| 310.5100 | -101.7300 | 85.4400 |
| 326.1299 | -101.6600 | 86.0400 |
| 346.9199 | -101.8800 | 84.0600 |
| 367.5701 | -102.3100 | 80.2800 |
| 388.0801 | -102.7600 | 76.2800 |
| 386.4399 | -125.8100 | 78.8900 |
| 366.4500 | -125.8900 | 78.1800 |
| 346.5901 | -126.1800 | 75.6200 |
| 326.8701 | -126.4000 | 73.7100 |
| 312.1101 | -126.4100 | 73.5900 |
| 302.2500 | -126.3300 | 74.2900 |
| 294.8101 | -126.2100 | 75.5600 |
| 289.7900 | -126.0600 | 76.6900 |
| 286.9800 | -125.8000 | 79.0100 |
| 289.1899 | -125.4800 | 81.8200 |
| 294.1101 | -125.2300 | 84.9900 |
| 301.5901 | -124.9900 | 86.1500 |
| 311.6101 | -124.8200 | 87.7200 |
| 326.6799 | -124.7500 | 88.3000 |
| 346.7300 | -124.9700 | 86.3900 |
| 366.6499 | -125.3800 | 82.7400 |
| 386.4399 | -125.5100 | 78.8900 |
| 384.8000 | -148.8700 | 81.4900 |

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| 365.5400 | -148.9400 | 80.8100 |
| 346.4099 | -149.2200 | 78.3400 |
| 327.4099 | -149.4300 | 76.5000 |
| 313.1899 | -149.4400 | 76.3900 |
| 303.6899 | -149.3700 | 77.0600 |
| 296.5200 | -149.2500 | 78.1000 |
| 291.6799 | -149.1100 | 79.3800 |
| 288.9800 | -148.8500 | 81.6100 |
| 291.1101 | -148.5500 | 84.3100 |
| 295.8501 | -148.3000 | 86.5000 |
| 303.0500 | -148.0800 | 88.4900 |
| 312.7100 | -147.9100 | 90.0000 |
| 327.2300 | -147.8400 | 90.5600 |
| 346.5500 | -148.0500 | 88.7200 |
| 365.7400 | -148.4500 | 85.2000 |
| 384.8000 | -148.8700 | 81.4900 |
| 383.1599 | -171.9200 | 84.1000 |
| 364.6299 | -171.9900 | 83.4400 |
| 346.2300 | -172.2600 | 81.0600 |
| 327.9500 | -172.4600 | 79.2900 |
| 314.2700 | -172.4700 | 79.1900 |
| 305.1299 | -172.4000 | 79.8300 |
| 298.2400 | -172.2900 | 80.8300 |
| 293.5801 | -172.1500 | 82.0600 |
| 290.9900 | -171.9100 | 84.2100 |
| 293.0300 | -171.6100 | 86.8100 |
| 297.5901 | -171.3800 | 88.9100 |
| 304.5200 | -171.1600 | 90.8200 |
| 313.8101 | -171.0000 | 92.2800 |
| 327.7800 | -170.9300 | 92.8200 |
| 346.3601 | -171.1300 | 91.0500 |
| 364.8201 | -171.5200 | 87.6700 |
| 383.1599 | -171.9200 | 84.1000 |
| 381.5200 | -194.9700 | 86.7000 |
| 363.7300 | -195.0400 | 86.0700 |
| 346.0500 | -195.3000 | 83.7900 |
| 328.4900 | -195.4900 | 82.0900 |
| 315.3501 | -195.5100 | 81.9800 |
| 306.5701 | -195.4400 | 82.6000 |
| 299.9500 | -195.3300 | 83.5600 |
| 295.4800 | -195.1900 | 84.7500 |
| 292.9900 | -194.9600 | 86.8100 |
| 294.9500 | -194.6800 | 89.3100 |
| 299.3301 | -194.4500 | 91.3300 |
| 305.9800 | -194.2400 | 93.1600 |
| 314.9099 | -194.0900 | 94.5600 |
| 328.3201 | -194.0300 | 95.0800 |
| 346.1699 | -194.2200 | 93.3800 |
| 363.9699 | -194.5900 | 90.1300 |
| 381.5200 | -194.9700 | 86.7000 |
| 379.8799 | -218.0300 | 89.3000 |
| 362.8201 | -218.1300 | 88.7000 |
| 345.8701 | -218.3400 | 86.5100 |
| 329.0300 | -218.5300 | 84.8800 |
| 316.4299 | -218.5400 | 84.7800 |
| 308.0100 | -218.4700 | 85.3800 |
| 301.6699 | -218.3700 | 86.3000 |
| 297.3799 | -218.2400 | 87.4300 |
| 294.9900 | -218.0200 | 89.4100 |
| 296.8701 | -217.7400 | 91.8000 |

ORIGINAL PAGE(S)
OF POOR QUALITY

| | | |
|----------|-----------|----------|
| 301.0701 | -217.5300 | 93.7400 |
| 307.4500 | -217.3300 | 95.5000 |
| 316.0100 | -217.1800 | 96.8400 |
| 328.8701 | -217.1200 | 97.3400 |
| 345.9900 | -217.3000 | 95.7100 |
| 362.9900 | -217.6600 | 92.5900 |
| 379.8799 | -218.0300 | 99.3000 |
| 378.2400 | -241.0800 | 91.9100 |
| 361.9099 | -241.1500 | 91.3300 |
| 345.6899 | -241.3800 | 89.2300 |
| 329.5701 | -241.5600 | 87.6800 |
| 317.5100 | -241.5700 | 87.5800 |
| 309.4500 | -241.5000 | 88.1500 |
| 313.3799 | -241.4100 | 89.0300 |
| 299.2800 | -241.2800 | 90.1200 |
| 296.9900 | -240.0700 | 92.0100 |
| 298.7900 | -240.8100 | 94.3000 |
| 302.8101 | -240.6000 | 96.1500 |
| 308.9199 | -240.4100 | 97.8400 |
| 317.1101 | -240.2700 | 99.1300 |
| 329.4199 | -240.2100 | 99.6000 |
| 345.8000 | -240.3900 | 98.0400 |
| 362.0701 | -240.7200 | 95.0600 |
| 378.2400 | -241.0800 | 91.9100 |
| 376.6001 | -264.1299 | 94.5100 |
| 361.0000 | -264.2000 | 93.9600 |
| 345.5100 | -264.4199 | 91.9600 |
| 330.1101 | -264.5901 | 90.4700 |
| 318.5901 | -264.6001 | 90.3800 |
| 310.8999 | -264.5400 | 90.9200 |
| 305.0901 | -264.4399 | 91.7500 |
| 301.1699 | -264.3301 | 92.8000 |
| 298.9900 | -264.1201 | 94.6100 |
| 300.7100 | -263.8799 | 96.8000 |
| 304.5500 | -263.6799 | 98.5700 |
| 310.3799 | -263.4900 | 100.1800 |
| 318.2100 | -263.3501 | 101.4100 |
| 329.9700 | -263.3000 | 101.8600 |
| 345.6101 | -263.4700 | 100.3700 |
| 361.1599 | -263.7900 | 97.5200 |
| 376.6001 | -264.1299 | 94.5100 |

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|--------|------|---------|
| 8. | 2. | |
| 271. | 0. | 72.8 |
| 284.09 | 0. | 68.64 |
| 289.67 | 0. | 67.16 |
| 297.92 | 0. | 65.97 |
| 308.87 | 0. | 65.2 |
| 325.25 | 0. | 65.32 |
| 347.14 | 0. | 67.44 |
| 391.7 | 0. | 74.4 |
| 271. | 29.2 | 72.8 |
| 284.09 | 29.2 | 68.64 |
| 289.67 | 29.2 | 67.16 |
| 297.92 | 29.2 | 65.97 |
| 308.87 | 29.2 | 65.2 |
| 325.25 | 29.2 | 65.32 |
| 347.14 | 29.2 | 67.44 |
| 391.7 | 28. | 74.4 |
| 391.7 | 8.0 | 2 0 |
| | | -0.0000 |
| | | 74.4 |

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|----------|----------|----------|
| 347.1399 | -0.0000 | 67.4400 |
| 325.2500 | -0.0000 | 65.3200 |
| 308.8701 | -0.0000 | 65.2000 |
| 297.9199 | -0.0000 | 65.9700 |
| 289.6699 | -0.0000 | 67.1600 |
| 284.0901 | -0.0000 | 68.6400 |
| 271.0000 | -0.0000 | 72.8000 |
| 391.7 | -28. | 74.4 |
| 347.1399 | -29.2000 | 67.4400 |
| 325.2500 | -29.2000 | 65.3200 |
| 308.8701 | -29.2000 | 65.2000 |
| 297.9199 | -29.2000 | 65.9700 |
| 289.6699 | -29.2000 | 67.1600 |
| 284.0901 | -29.2000 | 68.6400 |
| 271.0000 | -29.2000 | 72.8000 |
| 17. | 2. | |
| 391.7 | 28. | 74.4 |
| 376.6 | 38.9 | 85. |
| 347.29 | 38.9 | 85. |
| 325.04 | 38.9 | 85. |
| 308.31 | 38.9 | 85. |
| 300. | 35.9 | 85. |
| 289. | 35.22069 | 80.37241 |
| 282. | 32.87931 | 77.42759 |
| 271. | 29.2 | 72.8 |
| 284.09 | 29.2 | 68.64 |
| 289.67 | 29.2 | 67.16 |
| 297.92 | 29.2 | 65.97 |
| 308.87 | 29.2 | 65.2 |
| 325.25 | 29.2 | 65.32 |
| 347.14 | 29.2 | 67.44 |
| 369.18 | 28.60646 | 70.88251 |
| 391.7 | 28. | 74.4 |
| 391.36 | 56.65 | 71.07 |
| 369.4 | 56.17 | 75.35 |
| 347.29 | 55.71 | 79.4 |
| 325.04 | 55.47 | 81.52 |
| 308.31 | 55.55 | 80.88 |
| 297.19 | 55.74 | 79.13 |
| 288.89 | 56. | 76.84 |
| 283.43 | 56.29 | 74.32 |
| 280.98 | 56.64 | 71.21 |
| 284.09 | 56.93 | 68.64 |
| 289.67 | 56.1 | 67.16 |
| 297.92 | 57.23 | 65.97 |
| 308.87 | 57.32 | 65.2 |
| 325.25 | 57.3 | 65.32 |
| 347.14 | 57.06 | 67.44 |
| 369.18 | 56.74 | 70.29 |
| 391.36 | 56.65 | 71.07 |
| 17.0 | 2.0 | |
| 391.7000 | -28.0000 | 74.4000 |
| 369.1799 | -28.6065 | 70.8825 |
| 347.1399 | -29.2000 | 67.4400 |
| 325.2500 | -29.2000 | 65.3200 |
| 308.8701 | -29.2000 | 65.2000 |
| 297.9199 | -29.2000 | 65.9700 |
| 289.6699 | -29.2000 | 67.1600 |
| 284.0901 | -29.2000 | 68.6400 |
| 271.0000 | -29.2000 | 72.8000 |

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| 282.0900 | -32.8793 | 77.4276 |
| 289.0000 | -35.2207 | 80.3724 |
| 300.0000 | -38.9000 | 85.0000 |
| 308.3101 | -38.9000 | 85.0000 |
| 325.0400 | -38.9000 | 85.0000 |
| 347.2500 | -38.9000 | 85.0000 |
| 376.6001 | -38.9000 | 85.0000 |
| 391.7000 | -28.0000 | 74.4000 |
| 391.3601 | -56.6500 | 71.0700 |
| 369.1799 | -56.7400 | 70.2900 |
| 347.1399 | -57.0600 | 67.4400 |
| 325.2500 | -57.3000 | 65.3200 |
| 308.8701 | -57.3200 | 65.2000 |
| 297.9199 | -57.2300 | 65.9700 |
| 289.6699 | -56.1000 | 67.1600 |
| 284.0901 | -56.9300 | 68.6400 |
| 280.9800 | -56.6400 | 71.2100 |
| 283.4299 | -56.2900 | 74.3200 |
| 288.8899 | -56.0000 | 76.8400 |
| 297.1899 | -55.7400 | 79.1300 |
| 308.3101 | -55.5500 | 80.8800 |
| 325.0400 | -55.4700 | 81.5200 |
| 347.2900 | -55.7100 | 79.4000 |
| 369.3999 | -56.1700 | 75.3500 |
| 391.3601 | -56.6500 | 71.0700 |

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|----|-------|-------|-------|
| 9. | 8. | | |
| | 175.6 | 79.9 | 120.3 |
| | 175.6 | 79.9 | 120.3 |
| | 175.6 | 79.9 | 120.3 |
| | 175.6 | 79.9 | 120.3 |
| | 175.6 | 79.9 | 120.3 |
| | 175.6 | 79.9 | 120.3 |
| | 175.6 | 79.9 | 120.3 |
| | 175.6 | 79.9 | 120.3 |
| | 175.6 | 79.9 | 120.3 |
| | 211.9 | 79.9 | 101.5 |
| | 211.5 | 64.8 | 107.7 |
| | 210.4 | 58.6 | 122.8 |
| | 209.3 | 64.8 | 137.8 |
| | 208.9 | 79.9 | 144.0 |
| | 209.3 | 95.0 | 137.8 |
| | 210.4 | 101.2 | 122.8 |
| | 211.5 | 95.0 | 107.7 |
| | 211.9 | 79.9 | 101.5 |
| | 225.9 | 79.9 | 98.3 |
| | 225.3 | 61.9 | 105.7 |
| | 224.0 | 54.4 | 123.7 |
| | 222.8 | 61.9 | 141.7 |
| | 222.2 | 79.9 | 149.2 |
| | 222.8 | 97.9 | 141.7 |
| | 224.0 | 105.4 | 123.7 |
| | 225.3 | 97.9 | 105.7 |
| | 225.9 | 79.9 | 98.3 |
| | 248.4 | 79.9 | 99.4 |
| | 247.9 | 61.5 | 107.0 |
| | 246.6 | 53.9 | 125.3 |
| | 245.3 | 61.5 | 143.7 |
| | 244.7 | 79.9 | 151.3 |
| | 245.3 | 98.3 | 143.7 |
| | 246.6 | 105.9 | 125.3 |

| | | |
|-------|-------|-------|
| 247.9 | 98.3 | 107.0 |
| 248.6 | 79.9 | 99.4 |
| 267.1 | 79.9 | 102.4 |
| 266.6 | 62.6 | 109.5 |
| 265.3 | 55.5 | 126.7 |
| 264.1 | 62.6 | 143.9 |
| 263.6 | 79.9 | 151.0 |
| 264.1 | 97.2 | 143.9 |
| 265.3 | 104.3 | 126.7 |
| 266.6 | 97.2 | 109.5 |
| 267.1 | 79.9 | 102.4 |
| 299.3 | 79.9 | 104.7 |
| 298.8 | 62.6 | 111.8 |
| 297.6 | 55.5 | 129.0 |
| 296.3 | 62.6 | 146.2 |
| 295.8 | 79.9 | 153.3 |
| 296.3 | 97.2 | 146.2 |
| 297.6 | 104.3 | 129.0 |
| 298.8 | 97.2 | 111.8 |
| 299.3 | 79.9 | 104.7 |
| 700.7 | 79.9 | 133.4 |
| 700.2 | 62.6 | 140.6 |
| 699.0 | 55.5 | 157.8 |
| 697.7 | 62.6 | 175.0 |
| 697.2 | 79.9 | 182.1 |
| 697.7 | 97.2 | 175.0 |
| 699.0 | 104.3 | 157.8 |
| 700.2 | 97.2 | 140.6 |
| 700.7 | 79.9 | 133.4 |
| 1000. | 79.9 | 133.4 |
| 1000. | 62.6 | 140.6 |
| 1000. | 55.5 | 157.8 |
| 1000. | 62.6 | 175.0 |
| 1000. | 79.9 | 182.1 |
| 1000. | 97.2 | 175.0 |
| 1000. | 104.3 | 157.8 |
| 1000. | 97.2 | 140.6 |
| 1000. | 79.9 | 133.4 |

| | | |
|--------|---------|--------|
| 9. | 8. | |
| 175.60 | -79.90 | 120.30 |
| 175.60 | -79.90 | 120.30 |
| 175.60 | -79.90 | 120.30 |
| 175.60 | -79.90 | 120.30 |
| 175.60 | -79.90 | 120.30 |
| 175.60 | -79.90 | 120.30 |
| 175.60 | -79.90 | 120.30 |
| 175.60 | -79.90 | 120.30 |
| 175.60 | -79.90 | 120.30 |
| 211.90 | -79.90 | 101.50 |
| 211.50 | -95.00 | 107.70 |
| 210.40 | -101.20 | 122.80 |
| 209.30 | -95.00 | 137.80 |
| 208.90 | -79.90 | 144.00 |
| 209.30 | -64.80 | 137.80 |
| 210.40 | -58.60 | 122.80 |
| 211.50 | -64.80 | 107.70 |
| 211.90 | -79.90 | 101.50 |
| 225.90 | -79.90 | 98.30 |
| 225.30 | -97.90 | 105.70 |
| 224.00 | -105.40 | 123.70 |

ORIGINAL POINTS
OF POOR QUALITY

| | | | | |
|---------|---------|--------|----|-----|
| 222.80 | -97.90 | 141.70 | | |
| 222.20 | -79.90 | 149.20 | | |
| 222.80 | -61.90 | 141.70 | | |
| 224.00 | -54.40 | 123.70 | | |
| 225.30 | -61.90 | 105.70 | | |
| 225.90 | -79.90 | 98.30 | | |
| 248.40 | -79.90 | 99.40 | | |
| 247.90 | -98.30 | 107.00 | | |
| 246.60 | -105.90 | 125.30 | | |
| 245.30 | -98.30 | 143.70 | | |
| 244.70 | -79.90 | 151.30 | | |
| 245.30 | -61.50 | 143.70 | | |
| 246.60 | -53.90 | 125.30 | | |
| 247.90 | -61.50 | 107.00 | | |
| 248.40 | -79.90 | 99.40 | | |
| 267.10 | -79.90 | 102.40 | | |
| 266.60 | -97.20 | 109.50 | | |
| 265.30 | -104.30 | 126.70 | | |
| 264.10 | -97.20 | 143.90 | | |
| 263.60 | -79.90 | 151.00 | | |
| 264.10 | -62.60 | 143.90 | | |
| 265.30 | -55.50 | 126.70 | | |
| 266.60 | -62.60 | 109.50 | | |
| 267.10 | -79.90 | 102.40 | | |
| 299.30 | -79.90 | 104.70 | | |
| 298.80 | -97.20 | 111.80 | | |
| 297.60 | -104.30 | 129.00 | | |
| 296.30 | -97.20 | 146.20 | | |
| 295.80 | -79.90 | 153.30 | | |
| 296.30 | -62.60 | 146.20 | | |
| 297.60 | -55.50 | 129.00 | | |
| 298.80 | -62.60 | 111.80 | | |
| 299.30 | -79.90 | 104.70 | | |
| 700.70 | -79.90 | 133.40 | | |
| 700.20 | -97.20 | 140.60 | | |
| 699.00 | -104.30 | 157.80 | | |
| 697.70 | -97.20 | 175.00 | | |
| 697.20 | -79.90 | 182.10 | | |
| 697.70 | -62.60 | 175.00 | | |
| 699.00 | -55.50 | 157.80 | | |
| 700.20 | -62.60 | 140.60 | | |
| 700.70 | -79.90 | 133.40 | | |
| 1000.00 | -79.90 | 133.40 | | |
| 1000.00 | -97.20 | 140.60 | | |
| 1000.00 | -104.30 | 157.80 | | |
| 1000.00 | -97.20 | 175.00 | | |
| 1000.00 | -79.90 | 182.10 | | |
| 1000.00 | -62.60 | 175.00 | | |
| 1000.00 | -55.50 | 157.80 | | |
| 1000.00 | -62.60 | 140.60 | | |
| 1000.00 | -79.90 | 133.40 | | |
| MULT | | | | |
| 2. | | | | |
| 11. | 9. | 7. | 1. | 10. |
| 285.35 | 79.63 | 74.34 | | 0. |
| 290.63 | 79.59 | 74.68 | | |
| 298.65 | 79.54 | 75.16 | | |
| 309.41 | 79.49 | 75.6 | | |
| 325.59 | 79.45 | 75.95 | | |
| 347.11 | 79.45 | 75.96 | | |

| | | |
|--------|--------|---------|
| 368.48 | 79.52 | 74.37 |
| 389.72 | 79.71 | 73.68 |
| 411.29 | 79.71 | 71.98 |
| 454.51 | 79.71 | 69.72 |
| 9010. | 79.71 | -165.62 |
| 287.27 | 102.69 | 76.92 |
| 292.37 | 102.65 | 77.25 |
| 300.12 | 102.6 | 77.71 |
| 310.51 | 102.55 | 78.13 |
| 326.13 | 102.51 | 78.48 |
| 346.92 | 102.51 | 78.49 |
| 367.57 | 102.58 | 77.92 |
| 388.08 | 102.76 | 76.28 |
| 408.92 | 102.76 | 74.64 |
| 450.66 | 102.76 | 72.46 |
| 9000. | 102.76 | -162.88 |
| 289.19 | 125.74 | 79.5 |
| 294.11 | 125.71 | 79.82 |
| 301.59 | 125.66 | 80.26 |
| 311.61 | 125.61 | 80.67 |
| 326.68 | 125.57 | 81. |
| 346.73 | 125.57 | 81.01 |
| 366.65 | 125.64 | 80.46 |
| 386.44 | 125.81 | 78.89 |
| 406.54 | 125.81 | 77.31 |
| 446.81 | 125.81 | 75.2 |
| 9000. | 125.81 | -160.15 |
| 291.11 | 148.8 | 82.08 |
| 295.85 | 148.77 | 82.39 |
| 303.05 | 148.72 | 82.82 |
| 312.71 | 148.67 | 83.21 |
| 327.23 | 148.64 | 83.53 |
| 346.55 | 148.64 | 83.54 |
| 365.74 | 148.7 | 83.01 |
| 384.8 | 148.87 | 81.49 |
| 404.17 | 148.87 | 79.97 |
| 442.96 | 148.87 | 77.94 |
| 9000. | 148.87 | -157.41 |
| 293.03 | 171.86 | 84.67 |
| 297.59 | 171.82 | 84.96 |
| 304.52 | 171.78 | 85.37 |
| 313.81 | 171.73 | 85.75 |
| 327.78 | 171.7 | 86.06 |
| 346.36 | 171.7 | 86.07 |
| 364.82 | 171.76 | 85.56 |
| 383.16 | 171.92 | 84.1 |
| 401.79 | 171.92 | 82.63 |
| 439.11 | 171.92 | 80.68 |
| 9000. | 171.92 | -154.67 |
| 294.95 | 194.91 | 87.25 |
| 299.33 | 194.88 | 87.53 |
| 305.98 | 194.84 | 87.93 |
| 314.91 | 194.79 | 88.29 |
| 328.32 | 194.76 | 88.58 |
| 346.17 | 194.76 | 88.59 |
| 363.91 | 194.82 | 88.1 |
| 381.52 | 194.97 | 86.7 |
| 399.41 | 194.97 | 85.29 |
| 435.26 | 194.97 | 83.41 |
| 9000. | 194.97 | -151.93 |

ORIGINAL PAGE
OF FOOD QUANTITY

| | | | | | |
|---------|---------|---------|---------|---------|---------|
| 296.87 | 217.97 | 89.83 | | | |
| 301.07 | 217.94 | 90.1 | | | |
| 307.45 | 217.89 | 90.48 | | | |
| 316.01 | 217.85 | 90.83 | | | |
| 328.87 | 217.82 | 91.11 | | | |
| 345.99 | 217.82 | 91.12 | | | |
| 362.99 | 217.87 | 90.65 | | | |
| 379.88 | 218.03 | 89.3 | | | |
| 397.04 | 218.03 | 87.95 | | | |
| 431.41 | 218.03 | 86.15 | | | |
| 9000. | 218.03 | -149.19 | | | |
| 298.79 | 241.02 | 92.41 | | | |
| 302.81 | 240.99 | 92.67 | | | |
| 308.92 | 240.95 | 93.03 | | | |
| 317.11 | 240.92 | 93.37 | | | |
| 329.42 | 240.89 | 93.64 | | | |
| 345.8 | 240.88 | 93.64 | | | |
| 362.07 | 240.93 | 93.2 | | | |
| 378.24 | 241.08 | 91.91 | | | |
| 394.66 | 241.08 | 90.62 | | | |
| 427.56 | 241.08 | 88.89 | | | |
| 9000. | 241.08 | -146.45 | | | |
| 300.51 | 261.77 | 94.73 | | | |
| 304.37 | 261.75 | 94.98 | | | |
| 310.24 | 261.71 | 95.33 | | | |
| 318.1 | 261.67 | 95.65 | | | |
| 329.91 | 261.64 | 95.91 | | | |
| 345.63 | 261.64 | 95.92 | | | |
| 361.25 | 261.69 | 95.49 | | | |
| 376.76 | 261.83 | 94.25 | | | |
| 392.52 | 261.83 | 93.01 | | | |
| 424.1 | 261.83 | 91.36 | | | |
| 9000. | 261.83 | -143.98 | | | |
| .050192 | .085453 | .120618 | .172921 | .242018 | .219928 |
| .10887 | | | | | |
| 388.93 | 91.17 | 74.97 | .07889 | -.10636 | .99119 |
| 387.29 | 114.22 | 77.58 | .07889 | -.10636 | .99119 |
| 385.64 | 137.27 | 80.18 | .07889 | -.10636 | .99119 |
| 384. | 160.32 | 82.78 | .07889 | -.10636 | .99119 |
| 382.36 | 183.37 | 85.39 | .07889 | -.10636 | .99119 |
| 380.72 | 206.42 | 87.99 | .07889 | -.10636 | .99119 |
| 379.08 | 229.47 | 90.59 | .07889 | -.10636 | .99119 |
| 377.44 | 252.52 | 93.2 | .07889 | -.10636 | .99119 |
| 11. | 9. | 7. | 1. | 10. | 0. |
| 285.35 | -79.63 | 74.34 | | | |
| 290.63 | -79.59 | 74.68 | | | |
| 298.65 | -79.54 | 75.16 | | | |
| 309.41 | -79.49 | 75.6 | | | |
| 325.59 | -79.45 | 75.95 | | | |
| 347.11 | -79.45 | 75.96 | | | |
| 366.48 | -79.52 | 74.37 | | | |
| 389.72 | -79.71 | 73.68 | | | |
| 411.29 | -79.71 | 71.98 | | | |
| 454.51 | -79.71 | 69.72 | | | |
| 9000. | -79.71 | -165.62 | | | |
| 287.27 | -102.69 | 76.92 | | | |
| 292.37 | -102.65 | 77.25 | | | |
| 300.12 | -102.6 | 77.71 | | | |
| 310.51 | -102.55 | 78.13 | | | |
| 326.13 | -102.51 | 78.48 | | | |

| | | |
|--------|---------|---------|
| 346.92 | -102.51 | 78.49 |
| 367.57 | -102.58 | 77.92 |
| 383.08 | -102.76 | 76.28 |
| 408.92 | -102.76 | 74.64 |
| 450.66 | -102.76 | 72.46 |
| 9000. | -102.76 | -162.88 |
| 289.19 | -125.74 | 79.5 |
| 294.11 | -125.71 | 79.82 |
| 301.59 | -125.66 | 80.26 |
| 311.61 | -125.61 | 80.67 |
| 326.68 | -125.57 | 81. |
| 346.73 | -125.57 | 81.01 |
| 366.65 | -125.64 | 80.46 |
| 386.44 | -125.81 | 78.89 |
| 406.54 | -125.81 | 77.31 |
| 446.81 | -125.81 | 75.2 |
| 9000. | -125.81 | -160.15 |
| 291.11 | -148.8 | 82.08 |
| 295.85 | -148.77 | 82.39 |
| 303.05 | -148.72 | 82.82 |
| 312.71 | -148.67 | 83.21 |
| 327.23 | -148.64 | 83.53 |
| 346.55 | -148.64 | 83.54 |
| 365.74 | -148.7 | 83.01 |
| 384.8 | -148.87 | 81.49 |
| 404.17 | -148.87 | 79.97 |
| 442.96 | -148.87 | 77.94 |
| 9000. | -148.87 | -157.41 |
| 293.03 | -171.86 | 84.67 |
| 297.59 | -171.82 | 84.96 |
| 304.52 | -171.78 | 85.37 |
| 313.81 | -171.73 | 85.75 |
| 327.78 | -171.7 | 86.06 |
| 346.36 | -171.7 | 86.07 |
| 364.82 | -171.76 | 85.56 |
| 383.16 | -171.92 | 84.1 |
| 401.79 | -171.92 | 82.63 |
| 439.11 | -171.92 | 80.68 |
| 9000. | -171.92 | -154.67 |
| 294.95 | -194.91 | 87.25 |
| 299.33 | -194.88 | 87.53 |
| 305.98 | -194.84 | 87.93 |
| 314.91 | -194.79 | 88.29 |
| 328.32 | -194.76 | 88.58 |
| 346.17 | -194.76 | 88.59 |
| 363.91 | -194.82 | 88.1 |
| 381.52 | -194.97 | 86.7 |
| 399.41 | -194.97 | 85.29 |
| 435.26 | -194.97 | 83.41 |
| 9000. | -194.97 | -151.93 |
| 296.87 | -217.97 | 89.83 |
| 301.07 | -217.94 | 90.1 |
| 307.45 | -217.89 | 90.48 |
| 316.01 | -217.85 | 90.83 |
| 328.87 | -217.82 | 91.11 |
| 345.99 | -217.82 | 91.12 |
| 362.99 | -217.87 | 90.65 |
| 379.88 | -218.03 | 89.3 |
| 397.04 | -218.03 | 87.95 |
| 431.41 | -218.03 | 86.15 |

| | | | | | |
|----------|---------|-----------|---------|---------|---------|
| 9000. | -218.03 | -149.19 | | | |
| 298.79 | -241.02 | 92.41 | | | |
| 302.81 | -240.99 | 92.67 | | | |
| 308.92 | -240.95 | 93.03 | | | |
| 317.11 | -240.92 | 93.37 | | | |
| 329.42 | -240.89 | 93.64 | | | |
| 345.8 | -240.88 | 93.64 | | | |
| 362.07 | -240.93 | 93.2 | | | |
| 378.24 | -241.08 | 91.91 | | | |
| 394.66 | -241.08 | 90.62 | | | |
| 427.56 | -241.08 | 88.89 | | | |
| 9000. | -241.08 | -146.45 | | | |
| 300.51 | -261.77 | 94.73 | | | |
| 304.37 | -261.75 | 94.98 | | | |
| 310.24 | -261.71 | 95.33 | | | |
| 318.1 | -261.67 | 95.65 | | | |
| 329.91 | -261.64 | 95.91 | | | |
| 345.63 | -261.64 | 95.92 | | | |
| 361.25 | -261.69 | 95.49 | | | |
| 376.76 | -261.83 | 94.25 | | | |
| 392.52 | -261.83 | 93.01 | | | |
| 424.1 | -261.83 | 91.36 | | | |
| 9000. | -261.83 | -143.98 | | | |
| .050192 | .025453 | .120618 | .172921 | .242018 | .219928 |
| .10887 | | | | | |
| 368.93 | -91.17 | 74.97 | .07889 | .10636 | .99119 |
| 387.29 | -114.22 | 77.58 | .07889 | .10636 | .99119 |
| 385.64 | -137.27 | 80.18 | .07889 | .10636 | .99119 |
| 384. | -160.32 | 82.78 | .07889 | .10636 | .99119 |
| 382.36 | -183.37 | 85.39 | .07889 | .10636 | .99119 |
| 380.72 | -206.42 | 87.99 | .07889 | .10636 | .99119 |
| 379.08 | -229.47 | 90.59 | .07889 | .10636 | .99119 |
| 377.44 | -252.52 | 93.2 | .07889 | .10636 | .99119 |
| B-MU | | | | | |
| 2. | | | | | |
| 11. | 3. | 7. | 1. | 10. | 0. |
| 283.43 | 0. | 71.76 | | | |
| 288.89 | 0. | 72.11 | | | |
| 297.19 | 0. | 72.6 | | | |
| 308.31 | 0. | 73.06 | | | |
| 325.04 | 0. | 73.42 | | | |
| 347.29 | 0. | 73.43 | | | |
| 369.4 | 0. | 76. | | | |
| 392.0323 | 0. | 77.65445 | | | |
| 413.67 | 0. | 100. | | | |
| 458.36 | 0. | 120. | | | |
| 9000. | 0. | -115.3426 | | | |
| 283.43 | 56.58 | 71.76 | | | |
| 288.89 | 56.54 | 72.11 | | | |
| 297.19 | 56.48 | 72.6 | | | |
| 308.31 | 56.43 | 73.06 | | | |
| 325.04 | 56.39 | 73.42 | | | |
| 347.29 | 56.39 | 73.43 | | | |
| 369.4 | 56.46 | 72.82 | | | |
| 391.36 | 56.65 | 71.07 | | | |
| 413.67 | 56.65 | 69.32 | | | |
| 458.36 | 56.65 | 66.98 | | | |
| 9000. | 56.65 | -168.36 | | | |
| 285.35 | 79.63 | 74.34 | | | |
| 290.63 | 79.59 | 74.68 | | | |

| | | | | | |
|----------|---------|-----------|---------|---------|---------|
| 298.65 | 79.54 | 75.16 | | | |
| 309.41 | 79.49 | 75.6 | | | |
| 325.59 | 79.45 | 75.95 | | | |
| 347.11 | 79.45 | 75.96 | | | |
| 368.48 | 79.52 | 75.37 | | | |
| 389.72 | 79.71 | 73.68 | | | |
| 411.29 | 79.71 | 71.98 | | | |
| 454.51 | 79.71 | 69.72 | | | |
| 9000. | 79.71 | -165.62 | | | |
| .050192 | .085453 | .120618 | .172921 | .242018 | .219928 |
| .10887 | | | | | |
| 390.57 | 68.12 | 72.37 | .07889 | -.10636 | .99119 |
| 11. | 3. | 7. | 1. | 10. | 0. |
| 283.43 | 0. | 71.76 | | | |
| 288.89 | 0. | 72.11 | | | |
| 297.19 | 0. | 72.6 | | | |
| 308.31 | 0. | 73.06 | | | |
| 325.04 | 0. | 73.42 | | | |
| 347.29 | 0. | 73.43 | | | |
| 369.4 | 0. | 76. | | | |
| 392.0323 | 0. | 77.65445 | | | |
| 413.67 | 0. | 100. | | | |
| 458.36 | 0. | 120. | | | |
| 9000. | 0. | -115.3426 | | | |
| 283.43 | -56.58 | 71.76 | | | |
| 288.89 | -56.54 | 72.11 | | | |
| 297.19 | -56.48 | 72.6 | | | |
| 308.31 | -56.43 | 73.06 | | | |
| 325.04 | -56.39 | 73.42 | | | |
| 347.29 | -56.39 | 73.43 | | | |
| 369.4 | -56.46 | 72.82 | | | |
| 391.36 | -56.65 | 71.07 | | | |
| 413.67 | -56.65 | 69.32 | | | |
| 458.36 | -56.65 | 66.98 | | | |
| 9000. | -56.65 | -168.36 | | | |
| 285.35 | -79.63 | 74.34 | | | |
| 290.63 | -79.59 | 74.68 | | | |
| 298.65 | -79.54 | 75.16 | | | |
| 309.41 | -79.49 | 75.6 | | | |
| 325.59 | -79.45 | 75.95 | | | |
| 347.11 | -79.45 | 75.96 | | | |
| 368.48 | -79.52 | 75.37 | | | |
| 389.72 | -79.71 | 73.68 | | | |
| 411.29 | -79.71 | 71.98 | | | |
| 454.51 | -79.71 | 69.72 | | | |
| 9000. | -79.71 | -165.62 | | | |
| .050192 | .085453 | .120618 | .172921 | .242018 | .219928 |
| .10887 | | | | | |
| 390.57 | -68.12 | 72.37 | .07889 | .10636 | .99119 |
| END | | | | | |
| AERO | | | | | |
| 0. | 0. | 0. | | | |
| FORC | | | | | |
| 307.5 | 0. | 75.52 | 52112. | 98.1 | 531.2 |
| END | | | | | 0. |

CASE
RSRA FUSELAGE AND WINGS. WING INCIDENCE 5.52 DEGREES
J D COWAN AERO RESEARCH ORGN 7440 EXT 7834

GEOM
3. 634. 1. -1.

SOUR

16.

7.

| | | |
|-------|------|-------|
| 36. | 4. | 95.9 |
| 36. | 0. | 95.9 |
| 36. | 0.0 | 95.9 |
| 36. | 0.0 | 95.9 |
| 36. | 0.0 | 95.9 |
| 36. | 0.0 | 95.9 |
| 36. | 0.0 | 95.9 |
| 58.8 | 0.0 | 110.2 |
| 58.8 | 16.9 | 108.1 |
| 58.8 | 22.5 | 106. |
| 58.8 | 22.5 | 96.2 |
| 58.8 | 22.5 | 86.4 |
| 58.8 | 16.9 | 82.3 |
| 58.8 | 0.0 | 82.3 |
| 81.5 | 0.0 | 119.9 |
| 81.5 | 22.1 | 116.4 |
| 81.5 | 29.5 | 113. |
| 81.5 | 29.5 | 99. |
| 81.5 | 29.5 | 85. |
| 81.5 | 22.1 | 78.1 |
| 81.5 | 0.0 | 78.1 |
| 120.9 | 0. | 147.6 |
| 120.9 | 28.4 | 136.7 |
| 120.9 | 37.8 | 125.9 |
| 120.9 | 37.8 | 108. |
| 120.9 | 37.8 | 90.7 |
| 120.9 | 28.4 | 74.8 |
| 120.9 | 0. | 74.8 |
| 7. | 6. | |
| 120.9 | 0. | 147.6 |
| 120.9 | 28.4 | 136.7 |
| 120.9 | 37.8 | 125.9 |
| 120.9 | 37.8 | 108. |
| 120.9 | 37.8 | 90.7 |
| 120.9 | 28.4 | 74.8 |
| 120.9 | 0. | 74.8 |
| 133. | 0. | 148.9 |
| 133. | 29.2 | 148.9 |
| 133. | 38.9 | 129.9 |
| 133. | 38.9 | 110.8 |
| 133. | 38.9 | 91.8 |
| 133. | 29.2 | 72.8 |
| 133. | 0. | 72.8 |
| 175.3 | 12.1 | 148.9 |
| 175.3 | 29.2 | 148.9 |
| 175.3 | 38.9 | 129.9 |
| 175.3 | 38.9 | 110.8 |
| 175.3 | 38.9 | 91.8 |

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|-------|----------|--------|
| 175.3 | 29.2 | 72.8 |
| 175.3 | 0. | 72.8 |
| 209.3 | 21.9 | 148.9 |
| 209.3 | 29.2 | 148.9 |
| 209.3 | 38.9 | 129.9 |
| 209.3 | 38.9 | 110.8 |
| 209.3 | 38.9 | 91.8 |
| 209.3 | 29.2 | 72.8 |
| 209.3 | 0. | 72.8 |
| 222.3 | 22.7 | 148.9 |
| 222.3 | 29.2 | 148.9 |
| 222.3 | 38.9 | 129.9 |
| 222.3 | 38.9 | 110.8 |
| 222.3 | 38.9 | 91.8 |
| 222.3 | 29.2 | 72.8 |
| 222.3 | 0. | 72.8 |
| 271. | 22.7 | 148.9 |
| 271. | 29.2 | 148.9 |
| 271. | 38.9 | 129.9 |
| 271. | 38.9 | 110.8 |
| 271. | 38.9 | 91.8 |
| 271. | 29.2 | 72.8 |
| 271. | 0. | 72.8 |
| 6. | 4. | |
| 271. | 22.7 | 148.9 |
| 271. | 29.2 | 148.9 |
| 271. | 38.9 | 129.9 |
| 271. | 38.9 | 110.8 |
| 271. | 38.9 | 91.8 |
| 271. | 29.2 | 72.8 |
| 300. | 22.7 | 148.9 |
| 300. | 29.2 | 148.9 |
| 300. | 38.9 | 129.9 |
| 300. | 38.9 | 110.8 |
| 300. | 38.9 | 91.8 |
| 300. | 38.9 | 85. |
| 376.6 | 17.8 | 148.9 |
| 376.6 | 29.2 | 148.9 |
| 376.6 | 38.9 | 129.9 |
| 376.6 | 38.9 | 110.8 |
| 376.6 | 38.9 | 91.8 |
| 376.6 | 38.9 | 85. |
| 391.7 | 15.7 | 147.3 |
| 391.7 | 28. | 147.3 |
| 391.7 | 37.3 | 129. |
| 391.7 | 37.3 | 110.8 |
| 391.7 | 37.3 | 92.6 |
| 391.7 | 28. | 74.4 |
| 7. | 5. | |
| 391.7 | 15.7 | 147.3 |
| 391.7 | 28. | 147.3 |
| 391.7 | 37.3 | 129. |
| 391.7 | 37.3 | 110.8 |
| 391.7 | 37.3 | 92.6 |
| 391.7 | 28. | 74.4 |
| 391.7 | 0. | 74.4 |
| 445.7 | 7.871745 | 143.46 |
| 445.7 | 24.5 | 143.46 |
| 445.7 | 32.7 | 127.2 |
| 445.7 | 32.7 | 110.8 |

ORIGINAL PLUGS
OF POOR QUALITY

| | | |
|-------|------|-------|
| 445.7 | 32.7 | 94.4 |
| 445.7 | 24.5 | 77.8 |
| 445.7 | 0. | 77.8 |
| 500. | 0. | 139.6 |
| 500. | 21. | 139.6 |
| 500. | 28. | 125.4 |
| 500. | 28. | 110.8 |
| 500. | 28. | 96.2 |
| 500. | 21. | 81.3 |
| 500. | 0. | 81.3 |
| 600. | 0. | 131. |
| 600. | 13.5 | 131. |
| 600. | 18. | 120.9 |
| 600. | 18. | 110.8 |
| 600. | 18. | 100.4 |
| 600. | 13.5 | 89.9 |
| 600. | 0. | 89.9 |
| 1000. | 0. | 131. |
| 1000. | 13.5 | 131. |
| 1000. | 18. | 120.9 |
| 1000. | 18. | 110.8 |
| 1000. | 18. | 100.4 |
| 1000. | 13.5 | 89.9 |
| 1000. | 0. | 89.9 |
| 7. | 10. | |
| 133. | 0. | 148.9 |
| 133. | 0. | 148.9 |
| 133. | 0. | 148.9 |
| 133. | 0. | 148.9 |
| 133. | 0. | 148.9 |
| 133. | 0. | 148.9 |
| 133. | 0. | 148.9 |
| 175.3 | 0. | 165.9 |
| 175.3 | 8.1 | 165.9 |
| 175.3 | 11.7 | 163.6 |
| 175.3 | 12.1 | 161.4 |
| 175.3 | 12.1 | 157.4 |
| 175.3 | 12.1 | 153.8 |
| 175.3 | 12.1 | 148.9 |
| 209.3 | 0. | 179.7 |
| 209.3 | 14.6 | 179.7 |
| 209.3 | 21.1 | 175.5 |
| 209.3 | 22. | 171.6 |
| 209.3 | 22. | 164.3 |
| 209.3 | 20.2 | 157.8 |
| 209.3 | 21.9 | 148.9 |
| 222.3 | 0. | 181.3 |
| 222.3 | 19.6 | 181.3 |
| 222.3 | 22.7 | 181.3 |
| 222.3 | 22.7 | 174.8 |
| 222.3 | 22.7 | 166.4 |
| 222.3 | 22.7 | 158.9 |
| 222.3 | 22.7 | 148.9 |
| 271. | 0. | 189.2 |
| 271. | 19.6 | 189.2 |
| 271. | 22.7 | 189.2 |
| 271. | 22.7 | 181.1 |
| 271. | 22.7 | 170.7 |
| 271. | 22.7 | 161.4 |
| 271. | 22.7 | 148.9 |

| | | |
|-------|---------|-------|
| 300. | 0. | 193.8 |
| 300. | 19.6 | 193.8 |
| 300. | 22.7 | 193.8 |
| 300. | 22.7 | 184.8 |
| 300. | 22.7 | 173.3 |
| 300. | 22.7 | 163. |
| 300. | 22.7 | 148.9 |
| 348.6 | 0. | 196.4 |
| 348.6 | 16.9 | 196.4 |
| 348.6 | 19.5911 | 196.4 |
| 348.6 | 19.5911 | 186.9 |
| 348.6 | 19.5911 | 174.6 |
| 348.6 | 19.5911 | 163.6 |
| 348.6 | 19.5911 | 148.9 |
| 376.6 | 0. | 188.1 |
| 376.6 | 15.3 | 188.1 |
| 376.6 | 17.8 | 188.1 |
| 376.6 | 17.8 | 180.3 |
| 376.6 | 17.8 | 170.1 |
| 376.6 | 17.8 | 161.0 |
| 376.6 | 17.8 | 148.9 |
| 391.7 | 0. | 182.9 |
| 391.7 | 13.5 | 182.9 |
| 391.7 | 15.7 | 182.9 |
| 391.7 | 15.7 | 175.8 |
| 391.7 | 15.7 | 166.5 |
| 391.7 | 15.7 | 158.3 |
| 391.7 | 15.7 | 147.3 |
| 500. | 0. | 139.6 |
| 500. | 0. | 139.6 |
| 500. | 0. | 139.6 |
| 500. | 0. | 139.6 |
| 500. | 0. | 139.6 |
| 500. | 0. | 139.6 |
| 500. | 0. | 139.6 |

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| 7.0 | 4.0 |
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| 36. | 0. | 95.9 |
| 36. | 0. | 95.9 |
| 36.0000 | -0.0000 | 95.9000 |
| 36.0000 | -0.0000 | 95.9000 |
| 36.0000 | -0.0000 | 95.9000 |
| 36.0000 | -0.0000 | 95.9000 |
| 36.0000 | -0.0000 | 95.9000 |
| 58.8000 | -0.0000 | 82.3000 |
| 58.8 | -16.9 | 82.3 |
| 58.8000 | -22.5000 | 86.4000 |
| 58.8000 | -22.5000 | 96.2000 |
| 58.8000 | -22.5000 | 106.0000 |
| 58.8 | -16.9 | 108.1 |
| 58.8000 | -0.0000 | 110.2000 |
| 81.5000 | -0.0000 | 78.1000 |
| 81.5 | -22.1 | 78.1 |
| 81.5000 | -29.5000 | 85.0000 |
| 81.5000 | -29.5000 | 99.0000 |
| 81.5000 | -29.5000 | 113.0000 |
| 81.5 | -22.1 | 116.4 |
| 81.5000 | -0.0000 | 119.9000 |
| 120.9000 | -0.0000 | 74.8000 |
| 120.9 | -28.4 | 74.8 |
| 120.9000 | -37.8000 | 90.7000 |

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| 120.9000 | -37.8000 | 108. |
| 120.9000 | -37.8000 | 125.9000 |
| 120.9 | -28.4 | 136.7 |
| 120.9000 | -0.0000 | 147.6000 |
| | 7.0 | 6. |
| 120.9000 | -0.0000 | 74.8000 |
| 120.9000 | -28.4000 | 74.8000 |
| 120.9000 | -37.8000 | 90.7000 |
| 120.9000 | -37.8000 | 108. |
| 120.9000 | -37.8000 | 125.9000 |
| 120.9000 | -28.4000 | 136.7000 |
| 120.9000 | -0.0000 | 147.6000 |
| 133.0000 | -0.0000 | 72.8000 |
| 133.0000 | -29.2000 | 72.8000 |
| 133.0000 | -38.9000 | 91.8000 |
| 133.0000 | -38.9000 | 110.8000 |
| 133.0000 | -38.9000 | 129.9000 |
| 133.0000 | -29.2000 | 148.9000 |
| 133.0000 | -0.0000 | 148.9000 |
| 175.3000 | -0.0000 | 72.8000 |
| 175.3000 | -29.2000 | 72.8000 |
| 175.3000 | -38.9000 | 91.8000 |
| 175.3000 | -38.9000 | 110.8000 |
| 175.3000 | -38.9000 | 129.9000 |
| 175.3000 | -29.2000 | 148.9000 |
| 175.3000 | -12.1000 | 148.9000 |
| 209.3000 | -0.0000 | 72.8000 |
| 209.3000 | -29.2000 | 72.8000 |
| 209.3000 | -38.9000 | 91.8000 |
| 209.3000 | -38.9000 | 110.8000 |
| 209.3000 | -38.9000 | 129.9000 |
| 209.3000 | -29.2000 | 148.9000 |
| 209.3000 | -21.9000 | 148.9000 |
| 222.3000 | -0.0000 | 72.8000 |
| 222.3000 | -29.2000 | 72.8000 |
| 222.3000 | -38.9000 | 91.8000 |
| 222.3000 | -38.9000 | 110.8000 |
| 222.3000 | -38.9000 | 129.9000 |
| 222.3000 | -29.2000 | 148.9000 |
| 222.3000 | -22.7000 | 148.9000 |
| 271.0000 | -0.0000 | 72.8000 |
| 271.0000 | -29.2000 | 72.8000 |
| 271.0000 | -38.9000 | 91.8000 |
| 271.0000 | -38.9000 | 110.8000 |
| 271.0000 | -38.9000 | 129.9000 |
| 271.0000 | -29.2000 | 148.9000 |
| 271. | -22.7 | 148.9000 |
| 6. | 4. | |
| 271.0000 | -29.2000 | 72.8 |
| 271.0000 | -38.9000 | 91.8 |
| 271.0000 | -38.9000 | 110.8000 |
| 271.0000 | -38.9000 | 129.9000 |
| 271.0000 | -29.2000 | 148.9000 |
| 271.0000 | -22.7000 | 148.9000 |
| 300. | -38.9 | 85. |
| 300. | -38.9 | 91.8 |
| 300. | -38.9 | 110.8 |
| 300. | -38.9 | 129.9 |
| 300. | -29.2 | 148.9 |
| 300. | -22.7 | 148.9 |

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| 376.6 | -38.9 | 85. |
| 376.6 | -38.9 | 91.8 |
| 376.6 | -38.9 | 110.8 |
| 376.6 | -38.9 | 129.9 |
| 376.6 | -29.2 | 148.9 |
| 376.6 | -17.8 | 148.9 |
| 391.7 | -28. | 74.4 |
| 391.7 | -37.3 | 92.6 |
| 391.7 | -37.3 | 110.8 |
| 391.7 | -37.3 | 129. |
| 391.7 | -28. | 147.3 |
| 391.7 | -15.7 | 147.3 |
| 7. | 5. | |
| 391.7000 | -0.0000 | 74.4000 |
| 391.7000 | -28.0000 | 74.4000 |
| 391.7000 | -37.3000 | 92.6000 |
| 391.7000 | -37.3000 | 110.8000 |
| 391.7000 | -37.3000 | 129.0000 |
| 391.7000 | -28.0000 | 147.3000 |
| 391.7000 | -15.7000 | 147.3000 |
| 445.7000 | -0.0000 | 77.8000 |
| 445.7000 | -24.5000 | 77.8000 |
| 445.7000 | -32.7000 | 94.4000 |
| 445.7000 | -32.7000 | 110.8000 |
| 445.7000 | -32.7000 | 127.2000 |
| 445.7000 | -24.5000 | 143.4600 |
| 445.7000 | -7.871745 | 143.4600 |
| 500.0000 | -0.0000 | 81.3000 |
| 500.0000 | -21.0000 | 81.3000 |
| 500.0000 | -28.0000 | 96.2000 |
| 500.0000 | -28.0000 | 110.8000 |
| 500.0000 | -28.0000 | 125.4000 |
| 500.0000 | -21.0000 | 139.6000 |
| 500.0000 | -0.0000 | 139.6000 |
| 600.0000 | -0.0000 | 89.9000 |
| 600.0000 | -13.5000 | 89.9000 |
| 600.0000 | -18.0000 | 100.4000 |
| 600.0000 | -18.0000 | 110.8000 |
| 600.0000 | -18.0000 | 120.9000 |
| 600.0000 | -13.5000 | 131.0000 |
| 600.0000 | -0.0000 | 131.0000 |
| 1000.0000 | -0.0000 | 89.9000 |
| 1000.0000 | -13.5000 | 89.9000 |
| 1000.0000 | -18.0000 | 100.4000 |
| 1000.0000 | -18.0000 | 110.8000 |
| 1000.0000 | -18.0000 | 120.9000 |
| 1000.0000 | -13.5000 | 131.0000 |
| 1000.0000 | -0.0000 | 131.0000 |
| 7.0 | 10.0 | |
| 133.0000 | -0.0000 | 148.9000 |
| 133.0000 | -0.0000 | 148.9000 |
| 133.0000 | -0.0000 | 148.9000 |
| 133.0000 | -0.0000 | 148.9000 |
| 133.0000 | -0.0000 | 148.9000 |
| 133.0000 | -0.0000 | 148.9000 |
| 175.3000 | -12.1000 | 148.9000 |
| 175.3000 | -12.1000 | 153.8000 |
| 175.3000 | -12.1000 | 157.4000 |
| 175.3000 | -12.1000 | 161.4000 |

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| 175.3000 | -11.7000 | 163.6000 |
| 175.3000 | -8.1000 | 165.9000 |
| 175.3000 | -0.0000 | 165.9000 |
| 209.3000 | -21.9000 | 148.9000 |
| 209.3030 | -20.2000 | 157.8000 |
| 209.3000 | -22.0000 | 164.3000 |
| 209.3000 | -22.0000 | 171.6000 |
| 209.3000 | -21.1000 | 175.5000 |
| 209.3000 | -14.6000 | 179.7000 |
| 209.3000 | -0.0000 | 179.7000 |
| 222.3000 | -22.7000 | 148.9000 |
| 222.3000 | -22.7000 | 158.9000 |
| 222.3000 | -22.7000 | 166.4000 |
| 222.3000 | -22.7000 | 174.8000 |
| 222.3000 | -22.7000 | 181.3000 |
| 222.3000 | -19.6000 | 181.3000 |
| 222.3000 | -0.0000 | 181.3000 |
| 271.0000 | -22.7000 | 148.9000 |
| 271.0000 | -22.7000 | 161.4000 |
| 271.0000 | -22.7000 | 170.7000 |
| 271.0000 | -22.7000 | 181.1000 |
| 271.0000 | -22.7000 | 189.2000 |
| 271.0000 | -19.6000 | 189.2000 |
| 271.0000 | -0.0000 | 189.2000 |
| 300.0000 | -22.7000 | 148.9000 |
| 300.0000 | -22.7000 | 163.0000 |
| 300.0000 | -22.7000 | 173.3000 |
| 300.0000 | -22.7000 | 184.8000 |
| 300.0000 | -22.7000 | 193.8000 |
| 300.0000 | -19.6000 | 193.3000 |
| 300.0000 | -0.0000 | 193.8000 |
| 348.6001 | -19.5911 | 148.9000 |
| 348.6001 | -19.5911 | 163.6000 |
| 348.6001 | -19.5911 | 174.6000 |
| 348.6001 | -19.5911 | 186.9000 |
| 348.6001 | -19.5911 | 196.4000 |
| 348.6001 | -16.9000 | 196.4000 |
| 348.6001 | -0.0000 | 196.4000 |
| 376.6001 | -17.8000 | 148.9000 |
| 376.6001 | -17.8000 | 161.0000 |
| 376.6001 | -17.8000 | 170.1000 |
| 376.6001 | -17.8000 | 180.3000 |
| 376.6001 | -17.8000 | 188.1000 |
| 376.6001 | -15.3000 | 188.1000 |
| 376.6001 | -0.0000 | 188.1000 |
| 391.7000 | -15.7000 | 147.3000 |
| 391.7000 | -15.7000 | 158.3000 |
| 391.7000 | -15.7000 | 166.5000 |
| 391.7000 | -15.7000 | 175.8000 |
| 391.7000 | -15.7000 | 182.9000 |
| 391.7000 | -13.5000 | 182.9000 |
| 391.7000 | -0.0000 | 182.9000 |
| 500. | -0.0000 | 139.6000 |
| 500. | -0.0000 | 139.6000 |
| 500. | -0.0000 | 139.6000 |
| 500. | -0.0000 | 139.6 |
| 500. | -0.0000 | 139.6 |
| 500. | -0.0000 | 139.6000 |
| 500. | -0.0000 | 139.6000 |

17.

10.

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| 391.17400 | 57.08647 | 67.24026 |
| 369.73042 | 56.36848 | 73.59626 |
| 348.11788 | 55.67416 | 79.74264 |
| 326.17208 | 55.19565 | 83.97866 |
| 309.46237 | 55.08731 | 84.93768 |
| 298.21946 | 55.16361 | 84.26228 |
| 289.73513 | 55.33131 | 82.77772 |
| 284.05489 | 55.55556 | 80.79251 |
| 281.32157 | 55.87912 | 77.92827 |
| 284.16805 | 56.20197 | 75.07025 |
| 289.57370 | 56.42300 | 73.06931 |
| 297.67233 | 56.65164 | 71.08961 |
| 302.49333 | 56.85676 | 69.27374 |
| 324.81283 | 57.01911 | 67.83657 |
| 346.80632 | 57.01725 | 67.85307 |
| 369.01630 | 56.93522 | 68.57924 |
| 391.17400 | 57.08647 | 67.24026 |
| 389.54160 | 80.12214 | 70.00121 |
| 368.80529 | 79.42783 | 76.14757 |
| 347.90560 | 78.75641 | 82.09122 |
| 326.68364 | 78.29368 | 86.18752 |
| 310.52507 | 78.18892 | 87.11492 |
| 299.65298 | 78.26270 | 86.46179 |
| 291.44849 | 78.42487 | 85.02619 |
| 285.95560 | 78.64173 | 83.10646 |
| 283.31244 | 78.95461 | 80.33670 |
| 286.66502 | 79.26681 | 77.57294 |
| 291.29238 | 79.48539 | 75.63800 |
| 299.12390 | 79.70165 | 73.72359 |
| 309.58799 | 79.90001 | 71.96761 |
| 325.34922 | 80.05700 | 70.57785 |
| 346.63730 | 80.05520 | 70.59381 |
| 368.11473 | 79.97587 | 71.29602 |
| 389.54160 | 80.12214 | 70.00121 |
| 387.90921 | 103.15781 | 72.76215 |
| 367.88017 | 102.48718 | 78.69888 |
| 347.69332 | 101.83866 | 84.43980 |
| 327.19520 | 101.39171 | 88.39638 |
| 311.58777 | 101.29053 | 89.29215 |
| 301.08651 | 101.36179 | 88.66130 |
| 293.16185 | 101.51843 | 87.27467 |
| 287.85631 | 101.72789 | 85.42042 |
| 285.30330 | 102.03010 | 82.74512 |
| 287.96200 | 102.33165 | 80.07563 |
| 293.01107 | 102.54278 | 78.20669 |
| 300.57546 | 102.75166 | 76.35757 |
| 310.68265 | 102.94325 | 74.66149 |
| 325.92561 | 103.09489 | 73.31912 |
| 346.46829 | 103.09315 | 73.33454 |
| 367.21316 | 103.01653 | 74.01280 |
| 387.90921 | 103.15781 | 72.76215 |
| 386.27681 | 126.19348 | 75.52310 |
| 366.95505 | 125.54653 | 81.25018 |
| 347.48105 | 124.92092 | 86.78838 |
| 327.70676 | 124.48975 | 90.60525 |
| 312.65046 | 124.39213 | 91.46938 |
| 302.52063 | 124.46088 | 90.86081 |
| 294.87521 | 124.61199 | 89.52314 |
| 289.75702 | 124.81405 | 87.73437 |
| 287.29416 | 125.10559 | 85.15354 |

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| 289.85898 | 125.39650 | 82.57832 |
| 294.72975 | 125.60016 | 80.77537 |
| 302.02703 | 125.80167 | 78.99155 |
| 311.77731 | 125.98650 | 77.35536 |
| 326.46201 | 126.13270 | 76.06040 |
| 346.29927 | 126.13110 | 76.07527 |
| 366.31159 | 126.05719 | 76.72958 |
| 386.27681 | 126.19340 | 75.52310 |
| 384.64442 | 149.22915 | 78.28404 |
| 366.02993 | 148.60588 | 83.80149 |
| 347.26877 | 148.00317 | 89.13696 |
| 328.21833 | 147.58778 | 92.81411 |
| 313.71316 | 147.49374 | 93.64661 |
| 303.95355 | 147.55997 | 93.06032 |
| 296.58857 | 147.70555 | 91.77162 |
| 291.65773 | 147.90022 | 90.04832 |
| 289.28503 | 148.10108 | 87.56196 |
| 291.75596 | 148.46134 | 85.08101 |
| 296.44843 | 148.65755 | 83.34406 |
| 303.47860 | 148.85168 | 81.62554 |
| 312.87197 | 149.02975 | 80.04924 |
| 327.03840 | 149.17067 | 78.80168 |
| 346.13025 | 149.16906 | 78.81601 |
| 365.41002 | 149.09785 | 79.44636 |
| 384.64442 | 149.22915 | 78.28404 |
| 383.01202 | 172.26482 | 81.04499 |
| 365.10481 | 171.66523 | 86.35279 |
| 347.05650 | 171.08542 | 91.48554 |
| 328.72989 | 170.68582 | 95.02297 |
| 314.77586 | 170.59535 | 95.82384 |
| 305.38707 | 170.65906 | 95.25983 |
| 298.30193 | 170.79911 | 94.02009 |
| 293.55844 | 170.98638 | 92.36227 |
| 291.27589 | 171.25657 | 89.97033 |
| 293.65294 | 171.52618 | 87.58370 |
| 298.16712 | 171.71494 | 85.91274 |
| 304.93017 | 171.90169 | 84.25952 |
| 313.96662 | 172.07299 | 82.74311 |
| 327.59479 | 172.20857 | 81.54296 |
| 345.96123 | 172.20701 | 81.55674 |
| 364.50846 | 172.13851 | 82.16315 |
| 383.01202 | 172.26482 | 81.04499 |
| 381.37963 | 195.30049 | 83.80593 |
| 364.17968 | 194.72458 | 88.90410 |
| 346.84422 | 194.16767 | 93.83412 |
| 329.24145 | 193.78385 | 97.23184 |
| 315.83855 | 193.69696 | 98.00108 |
| 306.82059 | 193.75815 | 97.45934 |
| 300.01529 | 193.89267 | 96.26856 |
| 295.45916 | 194.07254 | 94.67622 |
| 293.26676 | 194.33207 | 92.37881 |
| 295.54992 | 194.59103 | 90.08639 |
| 299.88580 | 194.77233 | 88.48143 |
| 306.38173 | 194.95171 | 86.89350 |
| 315.06120 | 195.11624 | 85.43699 |
| 328.15119 | 195.24646 | 84.28423 |
| 345.79222 | 195.24496 | 84.29747 |
| 363.60687 | 195.17917 | 84.87993 |
| 381.37963 | 195.30049 | 83.80593 |
| 379.74723 | 218.33616 | 86.56688 |

| | | |
|-----------|-----------|-----------|
| 363.25456 | 217.78393 | 91.45540 |
| 346.63194 | 217.24992 | 96.18270 |
| 329.75301 | 216.88189 | 99.44070 |
| 316.90125 | 216.79856 | 100.17831 |
| 308.25411 | 216.85724 | 99.65885 |
| 301.72865 | 216.98623 | 98.51704 |
| 297.35987 | 217.15871 | 96.99018 |
| 295.25762 | 217.40756 | 94.78723 |
| 297.44690 | 217.65587 | 92.58908 |
| 301.60449 | 217.82972 | 91.05012 |
| 307.83330 | 218.00172 | 89.52748 |
| 316.15594 | 218.15948 | 88.13086 |
| 328.70758 | 218.20435 | 87.02551 |
| 345.62320 | 218.28291 | 87.03820 |
| 362.70532 | 218.21982 | 87.59671 |
| 379.74723 | 218.33616 | 86.56688 |
| 378.11484 | 241.37183 | 89.32783 |
| 362.32944 | 240.84328 | 94.00671 |
| 346.41967 | 240.33217 | 98.53128 |
| 330.26457 | 239.97992 | 101.64957 |
| 317.96395 | 239.90017 | 102.35554 |
| 309.68763 | 239.95634 | 101.85835 |
| 303.44201 | 240.07979 | 100.75551 |
| 299.26058 | 240.24487 | 99.30413 |
| 297.24846 | 240.48305 | 97.19566 |
| 299.34388 | 240.72071 | 95.09177 |
| 303.32317 | 240.88710 | 93.61880 |
| 309.28487 | 241.05173 | 92.16147 |
| 317.25060 | 241.20273 | 90.82474 |
| 329.26397 | 241.32224 | 89.76679 |
| 345.45418 | 241.32087 | 89.77894 |
| 361.80375 | 241.26048 | 90.31349 |
| 378.11484 | 241.37183 | 89.32783 |
| 376.48244 | 264.40750 | 92.08877 |
| 361.40432 | 263.90263 | 96.55802 |
| 346.20739 | 263.41443 | 100.87986 |
| 330.77613 | 263.07796 | 103.85843 |
| 319.02664 | 263.00178 | 104.53277 |
| 311.12115 | 263.05543 | 104.05786 |
| 305.15537 | 263.17335 | 103.01399 |
| 301.16129 | 263.33103 | 101.61808 |
| 299.23935 | 263.55854 | 99.60408 |
| 301.24085 | 263.78555 | 97.59446 |
| 305.04186 | 263.94449 | 96.18749 |
| 310.73643 | 264.10174 | 96.79545 |
| 318.34526 | 264.24598 | 93.51862 |
| 329.82037 | 264.36013 | 92.50807 |
| 345.28517 | 264.35882 | 92.51967 |
| 360.90218 | 264.30114 | 93.03028 |
| 376.48244 | 264.40750 | 92.08877 |
| 17.0 | 10.0 | |
| 391.17 | -57.09 | 67.24 |
| 369.02 | -56.94 | 68.58 |
| 346.81 | -57.02 | 67.85 |
| 324.81 | -57.02 | 67.84 |
| 308.49 | -56.86 | 69.27 |
| 297.67 | -56.65 | 71.09 |
| 289.57 | -56.43 | 73.07 |
| 284.17 | -56.20 | 75.07 |
| 281.32 | -55.88 | 77.93 |

ORIGINAL PAGES
OF POOR QUALITY

| | | |
|--------|---------|-------|
| 284.05 | -55.56 | 80.79 |
| 289.74 | -55.33 | 82.78 |
| 298.22 | -55.16 | 84.26 |
| 309.46 | -55.09 | 84.94 |
| 326.17 | -55.20 | 83.98 |
| 348.12 | -55.67 | 79.74 |
| 369.73 | -56.37 | 73.60 |
| 391.17 | -57.09 | 67.24 |
| 389.54 | -80.12 | 70.00 |
| 368.11 | -79.98 | 71.30 |
| 346.64 | -80.06 | 70.59 |
| 325.37 | -80.06 | 70.58 |
| 309.59 | -79.90 | 71.97 |
| 299.12 | -79.70 | 73.72 |
| 291.29 | -79.49 | 75.64 |
| 286.06 | -79.27 | 77.57 |
| 283.31 | -78.95 | 80.34 |
| 285.96 | -78.64 | 83.11 |
| 291.45 | -78.42 | 85.03 |
| 299.65 | -78.26 | 86.46 |
| 310.53 | -78.19 | 87.11 |
| 326.68 | -78.29 | 86.19 |
| 347.91 | -78.76 | 82.09 |
| 368.81 | -79.43 | 76.15 |
| 389.54 | -80.12 | 70.00 |
| 387.91 | -103.16 | 72.76 |
| 367.21 | -103.02 | 74.01 |
| 346.47 | -103.09 | 73.33 |
| 325.93 | -103.09 | 73.32 |
| 310.68 | -102.94 | 74.66 |
| 300.58 | -102.75 | 76.36 |
| 293.01 | -102.54 | 78.21 |
| 287.96 | -102.33 | 80.08 |
| 285.30 | -102.03 | 82.75 |
| 287.86 | -101.73 | 85.42 |
| 293.16 | -101.52 | 87.27 |
| 301.09 | -101.36 | 88.66 |
| 311.59 | -101.29 | 89.29 |
| 327.20 | -101.39 | 88.40 |
| 347.69 | -101.84 | 84.44 |
| 367.88 | -102.49 | 78.70 |
| 387.91 | -103.16 | 72.76 |
| 386.28 | -126.19 | 75.52 |
| 366.31 | -126.06 | 76.73 |
| 346.30 | -126.13 | 76.08 |
| 326.48 | -126.13 | 76.06 |
| 311.78 | -125.99 | 77.36 |
| 302.03 | -125.80 | 78.99 |
| 294.73 | -125.60 | 80.78 |
| 289.86 | -125.40 | 82.58 |
| 287.29 | -125.11 | 85.15 |
| 289.76 | -124.81 | 87.73 |
| 294.88 | -124.61 | 89.52 |
| 302.52 | -124.46 | 90.86 |
| 312.65 | -124.39 | 91.47 |
| 327.71 | -124.49 | 90.61 |
| 347.48 | -124.92 | 86.79 |
| 366.96 | -125.55 | 81.25 |
| 386.28 | -126.19 | 75.52 |
| 384.64 | -149.23 | 78.28 |

| | | |
|--------|---------|-------|
| 365.41 | -149.10 | 79.45 |
| 346.13 | -149.17 | 78.82 |
| 327.04 | -149.17 | 78.80 |
| 312.87 | -149.03 | 80.05 |
| 303.48 | -148.85 | 81.63 |
| 296.45 | -148.66 | 83.34 |
| 291.76 | -148.46 | 85.08 |
| 289.28 | -148.18 | 87.56 |
| 291.66 | -147.90 | 90.05 |
| 296.59 | -147.71 | 91.77 |
| 303.95 | -147.56 | 93.06 |
| 313.71 | -147.49 | 93.65 |
| 328.22 | -147.59 | 92.81 |
| 347.27 | -148.00 | 89.14 |
| 366.03 | -148.61 | 83.80 |
| 384.64 | -149.23 | 73.28 |
| 383.01 | -172.26 | 81.04 |
| 364.51 | -172.14 | 82.16 |
| 345.96 | -172.21 | 81.56 |
| 327.59 | -172.21 | 81.54 |
| 313.97 | -172.07 | 82.74 |
| 304.93 | -171.90 | 84.26 |
| 298.17 | -171.71 | 85.91 |
| 293.65 | -171.53 | 87.58 |
| 291.28 | -171.26 | 89.97 |
| 293.56 | -170.99 | 92.36 |
| 298.30 | -170.80 | 94.02 |
| 305.39 | -170.66 | 95.26 |
| 314.78 | -170.60 | 95.82 |
| 328.73 | -170.69 | 95.02 |
| 347.06 | -171.09 | 91.49 |
| 365.10 | -171.67 | 86.35 |
| 383.01 | -172.26 | 81.04 |
| 381.38 | -195.30 | 83.81 |
| 363.61 | -195.18 | 84.88 |
| 345.79 | -195.24 | 84.30 |
| 328.15 | -195.25 | 84.28 |
| 315.06 | -195.12 | 85.44 |
| 306.38 | -194.95 | 86.89 |
| 299.89 | -194.77 | 88.48 |
| 295.55 | -194.59 | 90.09 |
| 293.27 | -194.33 | 92.38 |
| 295.46 | -194.07 | 94.68 |
| 300.02 | -193.89 | 96.27 |
| 306.82 | -193.76 | 97.46 |
| 315.84 | -193.70 | 98.00 |
| 329.24 | -193.78 | 97.23 |
| 346.84 | -194.17 | 93.83 |
| 364.18 | -194.72 | 88.90 |
| 381.38 | -195.30 | 83.81 |
| 379.75 | -218.34 | 86.57 |
| 362.71 | -218.22 | 87.60 |
| 345.62 | -218.28 | 87.04 |
| 328.71 | -218.28 | 87.03 |
| 316.16 | -218.16 | 88.13 |
| 307.83 | -218.00 | 89.53 |
| 301.60 | -217.83 | 91.05 |
| 297.45 | -217.66 | 92.59 |
| 295.26 | -217.41 | 94.79 |
| 297.36 | -217.16 | 96.99 |

| | | |
|--------|---------|--------|
| 301.73 | -216.99 | 98.52 |
| 308.25 | -216.86 | 99.66 |
| 316.90 | -216.80 | 100.18 |
| 329.75 | -216.88 | 99.44 |
| 346.63 | -217.25 | 96.18 |
| 363.25 | -217.78 | 91.46 |
| 379.75 | -218.34 | 86.57 |
| 378.11 | -241.37 | 89.33 |
| 361.60 | -241.26 | 90.31 |
| 345.45 | -241.32 | 89.78 |
| 329.26 | -241.32 | 89.77 |
| 317.25 | -241.20 | 90.82 |
| 309.28 | -241.05 | 92.16 |
| 303.32 | -240.89 | 93.62 |
| 299.34 | -240.72 | 95.09 |
| 297.25 | -240.48 | 97.20 |
| 299.26 | -240.24 | 99.30 |
| 303.44 | -240.08 | 100.77 |
| 309.69 | -239.96 | 101.86 |
| 317.96 | -239.90 | 102.36 |
| 330.26 | -239.98 | 101.65 |
| 346.42 | -240.33 | 98.53 |
| 362.33 | -240.84 | 94.01 |
| 378.11 | -241.37 | 89.33 |
| 376.48 | -264.41 | 92.39 |
| 360.90 | -264.30 | 93.03 |
| 345.29 | -264.36 | 92.52 |
| 329.82 | -264.36 | 92.51 |
| 318.35 | -264.25 | 93.52 |
| 310.74 | -264.10 | 94.80 |
| 305.04 | -263.94 | 96.19 |
| 301.24 | -263.79 | 97.59 |
| 299.24 | -263.56 | 99.60 |
| 301.16 | -263.33 | 101.62 |
| 305.16 | -263.17 | 103.01 |
| 311.12 | -263.06 | 104.06 |
| 319.03 | -263.00 | 104.53 |
| 330.78 | -263.08 | 103.86 |
| 346.21 | -263.41 | 100.88 |
| 361.40 | -263.90 | 96.56 |
| 376.48 | -264.41 | 92.09 |

| | | |
|--------|---------|-------|
| 8. | 2. | |
| 271. | 0. | 72.8 |
| 284.09 | 0. | 68.64 |
| 289.67 | 0. | 67.16 |
| 297.92 | 0. | 65.97 |
| 308.87 | 0. | 65.2 |
| 325.25 | 0. | 65.32 |
| 347.14 | 0. | 67.44 |
| 391.7 | 0. | 74.4 |
| 271. | 29.2 | 72.8 |
| 284.09 | 29.2 | 68.64 |
| 289.67 | 29.2 | 67.16 |
| 297.92 | 29.2 | 65.97 |
| 308.87 | 29.2 | 65.2 |
| 325.25 | 29.2 | 65.32 |
| 347.14 | 29.2 | 67.44 |
| 391.7 | 28. | 74.4 |
| | 8.0 | 2.0 |
| 391.7 | -0.0000 | 74.4 |

UP VALUES FROM FOOT TO TIP AT ALL AZIMUTH STATIONS

| PSI | X/R 0.240 | 0.301 | 0.362 | 0.423 | 0.483 | 0.544 | 0.605 | 0.666 | 0.727 | 0.787 | 0.848 | 0.909 | 0.970 |
|-------|-----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 0.0 | 0.0001 | 0.0001 | 0.0001 | 0.0001 | 0.0001 | 0.0001 | 0.0001 | 0.0001 | 0.0001 | 0.0001 | 0.0001 | 0.0001 | 0.0001 |
| 15.0 | 0.0256 | 0.0263 | 0.0270 | 0.0277 | 0.0284 | 0.0291 | 0.0298 | 0.0305 | 0.0312 | 0.0319 | 0.0326 | 0.0333 | 0.0340 |
| 30.0 | 0.0473 | 0.0480 | 0.0487 | 0.0494 | 0.0501 | 0.0508 | 0.0515 | 0.0522 | 0.0529 | 0.0536 | 0.0543 | 0.0550 | 0.0557 |
| 45.0 | 0.0580 | 0.0587 | 0.0594 | 0.0601 | 0.0608 | 0.0615 | 0.0622 | 0.0629 | 0.0636 | 0.0643 | 0.0650 | 0.0657 | 0.0664 |
| 60.0 | 0.0687 | 0.0694 | 0.0701 | 0.0708 | 0.0715 | 0.0722 | 0.0729 | 0.0736 | 0.0743 | 0.0750 | 0.0757 | 0.0764 | 0.0771 |
| 75.0 | 0.0794 | 0.0801 | 0.0808 | 0.0815 | 0.0822 | 0.0829 | 0.0836 | 0.0843 | 0.0850 | 0.0857 | 0.0864 | 0.0871 | 0.0878 |
| 90.0 | 0.0901 | 0.0908 | 0.0915 | 0.0922 | 0.0929 | 0.0936 | 0.0943 | 0.0950 | 0.0957 | 0.0964 | 0.0971 | 0.0978 | 0.0985 |
| 105.0 | 0.0908 | 0.0915 | 0.0922 | 0.0929 | 0.0936 | 0.0943 | 0.0950 | 0.0957 | 0.0964 | 0.0971 | 0.0978 | 0.0985 | 0.0992 |
| 120.0 | 0.0915 | 0.0922 | 0.0929 | 0.0936 | 0.0943 | 0.0950 | 0.0957 | 0.0964 | 0.0971 | 0.0978 | 0.0985 | 0.0992 | 0.0999 |
| 135.0 | 0.0922 | 0.0929 | 0.0936 | 0.0943 | 0.0950 | 0.0957 | 0.0964 | 0.0971 | 0.0978 | 0.0985 | 0.0992 | 0.0999 | 0.1006 |
| 150.0 | 0.0929 | 0.0936 | 0.0943 | 0.0950 | 0.0957 | 0.0964 | 0.0971 | 0.0978 | 0.0985 | 0.0992 | 0.0999 | 0.1006 | 0.1013 |
| 165.0 | 0.0936 | 0.0943 | 0.0950 | 0.0957 | 0.0964 | 0.0971 | 0.0978 | 0.0985 | 0.0992 | 0.0999 | 0.1006 | 0.1013 | 0.1020 |
| 180.0 | 0.0943 | 0.0950 | 0.0957 | 0.0964 | 0.0971 | 0.0978 | 0.0985 | 0.0992 | 0.0999 | 0.1006 | 0.1013 | 0.1020 | 0.1027 |
| 195.0 | 0.0950 | 0.0957 | 0.0964 | 0.0971 | 0.0978 | 0.0985 | 0.0992 | 0.0999 | 0.1006 | 0.1013 | 0.1020 | 0.1027 | 0.1034 |
| 210.0 | 0.0957 | 0.0964 | 0.0971 | 0.0978 | 0.0985 | 0.0992 | 0.0999 | 0.1006 | 0.1013 | 0.1020 | 0.1027 | 0.1034 | 0.1041 |
| 225.0 | 0.0964 | 0.0971 | 0.0978 | 0.0985 | 0.0992 | 0.0999 | 0.1006 | 0.1013 | 0.1020 | 0.1027 | 0.1034 | 0.1041 | 0.1048 |
| 240.0 | 0.0971 | 0.0978 | 0.0985 | 0.0992 | 0.0999 | 0.1006 | 0.1013 | 0.1020 | 0.1027 | 0.1034 | 0.1041 | 0.1048 | 0.1055 |
| 255.0 | 0.0978 | 0.0985 | 0.0992 | 0.0999 | 0.1006 | 0.1013 | 0.1020 | 0.1027 | 0.1034 | 0.1041 | 0.1048 | 0.1055 | 0.1062 |
| 270.0 | 0.0985 | 0.0992 | 0.0999 | 0.1006 | 0.1013 | 0.1020 | 0.1027 | 0.1034 | 0.1041 | 0.1048 | 0.1055 | 0.1062 | 0.1069 |
| 285.0 | 0.0992 | 0.0999 | 0.1006 | 0.1013 | 0.1020 | 0.1027 | 0.1034 | 0.1041 | 0.1048 | 0.1055 | 0.1062 | 0.1069 | 0.1076 |
| 300.0 | 0.0999 | 0.1006 | 0.1013 | 0.1020 | 0.1027 | 0.1034 | 0.1041 | 0.1048 | 0.1055 | 0.1062 | 0.1069 | 0.1076 | 0.1083 |
| 315.0 | 0.1006 | 0.1013 | 0.1020 | 0.1027 | 0.1034 | 0.1041 | 0.1048 | 0.1055 | 0.1062 | 0.1069 | 0.1076 | 0.1083 | 0.1090 |
| 330.0 | 0.1013 | 0.1020 | 0.1027 | 0.1034 | 0.1041 | 0.1048 | 0.1055 | 0.1062 | 0.1069 | 0.1076 | 0.1083 | 0.1090 | 0.1097 |
| 345.0 | 0.1020 | 0.1027 | 0.1034 | 0.1041 | 0.1048 | 0.1055 | 0.1062 | 0.1069 | 0.1076 | 0.1083 | 0.1090 | 0.1097 | 0.1104 |

Flight Condition 5

UP VALUES FROM ROOT TO TIP AT ALL AZIMUTH STATIONS

| PSI | X/R | 0.240 | 0.301 | 0.362 | 0.423 | 0.483 | 0.544 | 0.605 | 0.666 | 0.727 | 0.787 | 0.848 | 0.909 | 0.970 |
|-----|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 51 | 0.017 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 50 | 0.017 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 45 | 0.017 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 40 | 0.017 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 35 | 0.017 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 30 | 0.017 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 25 | 0.017 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 20 | 0.017 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 15 | 0.017 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 10 | 0.017 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 5 | 0.017 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 0 | 0.017 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |

Flight Condition 6

UP VALUES FROM ROOT TO TIP AT ALL AZIMUTH STATIONS

| X/R | 0.248 | 0.301 | 0.362 | 0.423 | 0.483 | 0.544 | 0.605 | 0.666 | 0.727 | 0.787 | 0.848 | 0.909 | 0.970 |
|-------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
| P51 | -0.01466 | -0.02515 | -0.01931 | -0.01483 | -0.01172 | -0.00997 | -0.00784 | -0.00658 | -0.00550 | -0.00454 | -0.00364 | -0.00281 | -0.00209 |
| 150 | -0.01332 | -0.01801 | -0.01371 | -0.01043 | -0.00823 | -0.00653 | -0.00490 | -0.00394 | -0.00317 | -0.00252 | -0.00193 | -0.00141 | -0.00094 |
| 100 | -0.01099 | -0.01522 | -0.01137 | -0.00862 | -0.00683 | -0.00546 | -0.00428 | -0.00332 | -0.00267 | -0.00215 | -0.00167 | -0.00125 | -0.00085 |
| 50 | -0.00866 | -0.01220 | -0.00879 | -0.00647 | -0.00507 | -0.00402 | -0.00325 | -0.00269 | -0.00224 | -0.00182 | -0.00142 | -0.00104 | -0.00070 |
| 25 | -0.00618 | -0.00918 | -0.00671 | -0.00502 | -0.00392 | -0.00316 | -0.00259 | -0.00214 | -0.00172 | -0.00133 | -0.00096 | -0.00062 | -0.00036 |
| 12.5 | -0.00468 | -0.00718 | -0.00517 | -0.00392 | -0.00305 | -0.00248 | -0.00202 | -0.00167 | -0.00135 | -0.00105 | -0.00077 | -0.00051 | -0.00028 |
| 6.25 | -0.00368 | -0.00568 | -0.00418 | -0.00322 | -0.00258 | -0.00212 | -0.00176 | -0.00142 | -0.00112 | -0.00084 | -0.00059 | -0.00036 | -0.00018 |
| 3.125 | -0.00298 | -0.00478 | -0.00358 | -0.00272 | -0.00218 | -0.00182 | -0.00146 | -0.00112 | -0.00082 | -0.00057 | -0.00034 | -0.00018 | -0.00008 |
| 1.562 | -0.00248 | -0.00408 | -0.00308 | -0.00232 | -0.00178 | -0.00142 | -0.00106 | -0.00072 | -0.00047 | -0.00027 | -0.00014 | -0.00006 | -0.00002 |
| 0.781 | -0.00208 | -0.00348 | -0.00268 | -0.00202 | -0.00148 | -0.00112 | -0.00076 | -0.00042 | -0.00022 | -0.00011 | -0.00005 | -0.00002 | -0.00000 |
| 0.390 | -0.00168 | -0.00288 | -0.00218 | -0.00162 | -0.00118 | -0.00082 | -0.00046 | -0.00022 | -0.00011 | -0.00005 | -0.00002 | -0.00000 | -0.00000 |
| 0.195 | -0.00128 | -0.00228 | -0.00168 | -0.00122 | -0.00086 | -0.00050 | -0.00024 | -0.00012 | -0.00005 | -0.00002 | -0.00000 | -0.00000 | -0.00000 |
| 0.097 | -0.00088 | -0.00168 | -0.00128 | -0.00092 | -0.00066 | -0.00040 | -0.00014 | -0.00007 | -0.00003 | -0.00001 | -0.00000 | -0.00000 | -0.00000 |
| 0.048 | -0.00048 | -0.00098 | -0.00078 | -0.00052 | -0.00036 | -0.00020 | -0.00004 | -0.00001 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 |
| 0.024 | -0.00028 | -0.00058 | -0.00048 | -0.00032 | -0.00022 | -0.00012 | -0.00004 | -0.00001 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 |
| 0.012 | -0.00018 | -0.00038 | -0.00028 | -0.00018 | -0.00012 | -0.00006 | -0.00002 | -0.00001 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 |
| 0.006 | -0.00008 | -0.00018 | -0.00012 | -0.00008 | -0.00004 | -0.00002 | -0.00001 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 |
| 0.003 | -0.00004 | -0.00008 | -0.00004 | -0.00002 | -0.00001 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 |
| 0.001 | -0.00002 | -0.00004 | -0.00002 | -0.00001 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 |

Flight Condition 7

ORIGINAL DATA
OF FOOT STATIONS

UP VALUES FROM ROOT TO TIP AT ALL AZIMUTH STATIONS

| X/R | 0.260 | 0.301 | 0.362 | 0.423 | 0.483 | 0.544 | 0.605 | 0.666 | 0.727 | 0.787 | 0.848 | 0.909 | 0.970 |
|-------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| PSI | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 15.0 | 0.04553 | 0.03654 | 0.02751 | 0.02133 | 0.01649 | 0.01348 | 0.01114 | 0.00933 | 0.00778 | 0.00648 | 0.00516 | 0.00409 | 0.00322 |
| 30.0 | 0.04532 | 0.02997 | 0.01774 | 0.01142 | 0.00719 | 0.00457 | 0.00279 | 0.00172 | 0.00097 | 0.00059 | 0.00041 | 0.00032 | 0.00026 |
| 45.0 | 0.04588 | 0.03186 | 0.01919 | 0.01197 | 0.00719 | 0.00457 | 0.00279 | 0.00172 | 0.00097 | 0.00059 | 0.00041 | 0.00032 | 0.00026 |
| 60.0 | 0.04329 | 0.02865 | 0.01666 | 0.00978 | 0.00616 | 0.00371 | 0.00221 | 0.00145 | 0.00082 | 0.00053 | 0.00035 | 0.00027 | 0.00023 |
| 75.0 | 0.04167 | 0.02677 | 0.01577 | 0.00922 | 0.00581 | 0.00349 | 0.00217 | 0.00142 | 0.00082 | 0.00053 | 0.00035 | 0.00027 | 0.00023 |
| 90.0 | 0.03722 | 0.02465 | 0.01471 | 0.00871 | 0.00549 | 0.00331 | 0.00212 | 0.00137 | 0.00082 | 0.00053 | 0.00035 | 0.00027 | 0.00023 |
| 105.0 | 0.03502 | 0.02357 | 0.01404 | 0.00829 | 0.00529 | 0.00321 | 0.00202 | 0.00127 | 0.00077 | 0.00048 | 0.00030 | 0.00022 | 0.00018 |
| 120.0 | 0.03279 | 0.02193 | 0.01281 | 0.00769 | 0.00493 | 0.00291 | 0.00172 | 0.00107 | 0.00067 | 0.00040 | 0.00024 | 0.00017 | 0.00013 |
| 135.0 | 0.02777 | 0.02095 | 0.01203 | 0.00727 | 0.00461 | 0.00269 | 0.00150 | 0.00095 | 0.00057 | 0.00031 | 0.00018 | 0.00012 | 0.00009 |
| 150.0 | 0.02586 | 0.02095 | 0.01169 | 0.00686 | 0.00427 | 0.00242 | 0.00131 | 0.00080 | 0.00049 | 0.00025 | 0.00014 | 0.00009 | 0.00006 |
| 165.0 | 0.02386 | 0.02095 | 0.01137 | 0.00647 | 0.00392 | 0.00213 | 0.00102 | 0.00059 | 0.00032 | 0.00016 | 0.00008 | 0.00005 | 0.00003 |
| 180.0 | 0.02304 | 0.02095 | 0.01108 | 0.00612 | 0.00367 | 0.00188 | 0.00077 | 0.00044 | 0.00022 | 0.00011 | 0.00005 | 0.00003 | 0.00002 |
| 200.0 | 0.01982 | 0.01708 | 0.01021 | 0.00532 | 0.00319 | 0.00172 | 0.00062 | 0.00036 | 0.00017 | 0.00008 | 0.00004 | 0.00002 | 0.00001 |
| 220.0 | 0.01609 | 0.01564 | 0.00925 | 0.00419 | 0.00254 | 0.00132 | 0.00043 | 0.00021 | 0.00010 | 0.00005 | 0.00002 | 0.00001 | 0.00000 |
| 240.0 | 0.01427 | 0.01289 | 0.00819 | 0.00317 | 0.00181 | 0.00092 | 0.00036 | 0.00017 | 0.00008 | 0.00004 | 0.00002 | 0.00001 | 0.00000 |
| 260.0 | 0.01225 | 0.01126 | 0.00758 | 0.00238 | 0.00136 | 0.00065 | 0.00026 | 0.00013 | 0.00006 | 0.00003 | 0.00001 | 0.00000 | 0.00000 |
| 280.0 | 0.01165 | 0.01056 | 0.00703 | 0.00187 | 0.00106 | 0.00051 | 0.00021 | 0.00010 | 0.00005 | 0.00002 | 0.00001 | 0.00000 | 0.00000 |
| 300.0 | 0.01063 | 0.00957 | 0.00651 | 0.00148 | 0.00087 | 0.00046 | 0.00019 | 0.00009 | 0.00004 | 0.00002 | 0.00001 | 0.00000 | 0.00000 |
| 315.0 | 0.01078 | 0.00972 | 0.00666 | 0.00156 | 0.00093 | 0.00050 | 0.00022 | 0.00010 | 0.00005 | 0.00002 | 0.00001 | 0.00000 | 0.00000 |
| 330.0 | 0.01078 | 0.00972 | 0.00666 | 0.00156 | 0.00093 | 0.00050 | 0.00022 | 0.00010 | 0.00005 | 0.00002 | 0.00001 | 0.00000 | 0.00000 |
| 345.0 | 0.01078 | 0.00972 | 0.00666 | 0.00156 | 0.00093 | 0.00050 | 0.00022 | 0.00010 | 0.00005 | 0.00002 | 0.00001 | 0.00000 | 0.00000 |

Flight Condition 8

UP VALUES FROM ROOT TO TIP AT ALL AZIMUTH STATIONS

| X/R | 0.240 | 0.301 | 0.362 | 0.423 | 0.483 | 0.544 | 0.605 | 0.666 | 0.727 | 0.787 | 0.848 | 0.909 | 0.970 |
|-------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| PSI | | | | | | | | | | | | | |
| 0.0 | 0.01644 | 0.03188 | 0.04731 | 0.06274 | 0.07817 | 0.09360 | 0.10903 | 0.12446 | 0.13989 | 0.15532 | 0.17075 | 0.18618 | 0.20161 |
| 10.0 | 0.01728 | 0.03185 | 0.04730 | 0.06274 | 0.07817 | 0.09360 | 0.10903 | 0.12446 | 0.13989 | 0.15532 | 0.17075 | 0.18618 | 0.20161 |
| 20.0 | 0.01774 | 0.03182 | 0.04726 | 0.06270 | 0.07814 | 0.09358 | 0.10902 | 0.12446 | 0.13989 | 0.15532 | 0.17075 | 0.18618 | 0.20161 |
| 30.0 | 0.01791 | 0.03177 | 0.04721 | 0.06265 | 0.07809 | 0.09353 | 0.10897 | 0.12441 | 0.13985 | 0.15529 | 0.17073 | 0.18617 | 0.20161 |
| 40.0 | 0.01783 | 0.03171 | 0.04715 | 0.06259 | 0.07803 | 0.09347 | 0.10891 | 0.12435 | 0.13979 | 0.15523 | 0.17067 | 0.18611 | 0.20155 |
| 50.0 | 0.01761 | 0.03155 | 0.04699 | 0.06243 | 0.07787 | 0.09331 | 0.10875 | 0.12419 | 0.13963 | 0.15507 | 0.17051 | 0.18595 | 0.20139 |
| 60.0 | 0.01726 | 0.03129 | 0.04673 | 0.06217 | 0.07761 | 0.09305 | 0.10849 | 0.12393 | 0.13937 | 0.15481 | 0.17025 | 0.18569 | 0.20113 |
| 70.0 | 0.01679 | 0.03093 | 0.04637 | 0.06181 | 0.07725 | 0.09269 | 0.10813 | 0.12357 | 0.13891 | 0.15445 | 0.16989 | 0.18533 | 0.20077 |
| 80.0 | 0.01622 | 0.03057 | 0.04601 | 0.06145 | 0.07689 | 0.09233 | 0.10777 | 0.12321 | 0.13855 | 0.15409 | 0.16953 | 0.18497 | 0.20041 |
| 90.0 | 0.01556 | 0.03021 | 0.04565 | 0.06109 | 0.07653 | 0.09197 | 0.10741 | 0.12285 | 0.13819 | 0.15373 | 0.16917 | 0.18461 | 0.20005 |
| 100.0 | 0.01480 | 0.02985 | 0.04529 | 0.06073 | 0.07617 | 0.09161 | 0.10705 | 0.12249 | 0.13783 | 0.15337 | 0.16881 | 0.18425 | 0.19969 |
| 110.0 | 0.01394 | 0.02949 | 0.04493 | 0.06037 | 0.07581 | 0.09125 | 0.10669 | 0.12213 | 0.13747 | 0.15301 | 0.16845 | 0.18389 | 0.19933 |
| 120.0 | 0.01308 | 0.02913 | 0.04457 | 0.06001 | 0.07545 | 0.09089 | 0.10633 | 0.12177 | 0.13711 | 0.15265 | 0.16809 | 0.18353 | 0.19897 |
| 130.0 | 0.01222 | 0.02877 | 0.04421 | 0.05965 | 0.07509 | 0.09053 | 0.10597 | 0.12141 | 0.13675 | 0.15229 | 0.16773 | 0.18317 | 0.19861 |
| 140.0 | 0.01136 | 0.02841 | 0.04385 | 0.05929 | 0.07473 | 0.09017 | 0.10561 | 0.12105 | 0.13639 | 0.15193 | 0.16737 | 0.18281 | 0.19825 |
| 150.0 | 0.01050 | 0.02805 | 0.04349 | 0.05893 | 0.07437 | 0.08981 | 0.10525 | 0.12069 | 0.13603 | 0.15157 | 0.16701 | 0.18245 | 0.19789 |
| 160.0 | 0.00964 | 0.02769 | 0.04313 | 0.05857 | 0.07401 | 0.08945 | 0.10489 | 0.12033 | 0.13567 | 0.15121 | 0.16665 | 0.18209 | 0.19753 |
| 170.0 | 0.00878 | 0.02733 | 0.04277 | 0.05821 | 0.07365 | 0.08909 | 0.10453 | 0.12000 | 0.13531 | 0.15085 | 0.16629 | 0.18173 | 0.19717 |
| 180.0 | 0.00792 | 0.02697 | 0.04241 | 0.05785 | 0.07329 | 0.08873 | 0.10417 | 0.11964 | 0.13495 | 0.15049 | 0.16593 | 0.18137 | 0.19681 |
| 190.0 | 0.00706 | 0.02661 | 0.04205 | 0.05749 | 0.07293 | 0.08837 | 0.10381 | 0.11928 | 0.13459 | 0.15013 | 0.16557 | 0.18101 | 0.19645 |
| 200.0 | 0.00620 | 0.02625 | 0.04169 | 0.05713 | 0.07257 | 0.08801 | 0.10345 | 0.11892 | 0.13423 | 0.14977 | 0.16521 | 0.18065 | 0.19609 |
| 210.0 | 0.00534 | 0.02589 | 0.04133 | 0.05677 | 0.07221 | 0.08765 | 0.10309 | 0.11856 | 0.13387 | 0.14941 | 0.16485 | 0.18029 | 0.19573 |
| 220.0 | 0.00448 | 0.02553 | 0.04097 | 0.05641 | 0.07185 | 0.08729 | 0.10273 | 0.11820 | 0.13351 | 0.14905 | 0.16449 | 0.17993 | 0.19537 |
| 230.0 | 0.00362 | 0.02517 | 0.04061 | 0.05605 | 0.07149 | 0.08693 | 0.10237 | 0.11784 | 0.13315 | 0.14869 | 0.16413 | 0.17957 | 0.19501 |
| 240.0 | 0.00276 | 0.02481 | 0.04025 | 0.05569 | 0.07113 | 0.08657 | 0.10201 | 0.11748 | 0.13279 | 0.14833 | 0.16377 | 0.17921 | 0.19465 |
| 250.0 | 0.00190 | 0.02445 | 0.03989 | 0.05533 | 0.07077 | 0.08621 | 0.10165 | 0.11712 | 0.13243 | 0.14797 | 0.16341 | 0.17885 | 0.19429 |
| 260.0 | 0.00104 | 0.02409 | 0.03953 | 0.05497 | 0.07041 | 0.08585 | 0.10129 | 0.11676 | 0.13207 | 0.14761 | 0.16305 | 0.17849 | 0.19393 |
| 270.0 | 0.00018 | 0.02373 | 0.03917 | 0.05461 | 0.07005 | 0.08549 | 0.10093 | 0.11640 | 0.13171 | 0.14725 | 0.16269 | 0.17813 | 0.19357 |
| 280.0 | 0.00000 | 0.02337 | 0.03881 | 0.05425 | 0.06969 | 0.08513 | 0.10057 | 0.11604 | 0.13135 | 0.14689 | 0.16233 | 0.17777 | 0.19321 |
| 290.0 | 0.00000 | 0.02301 | 0.03845 | 0.05389 | 0.06933 | 0.08477 | 0.10021 | 0.11568 | 0.13099 | 0.14653 | 0.16197 | 0.17741 | 0.19285 |
| 300.0 | 0.00000 | 0.02265 | 0.03809 | 0.05353 | 0.06901 | 0.08441 | 0.09985 | 0.11532 | 0.13063 | 0.14617 | 0.16161 | 0.17705 | 0.19249 |
| 310.0 | 0.00000 | 0.02229 | 0.03773 | 0.05317 | 0.06865 | 0.08405 | 0.09949 | 0.11496 | 0.13027 | 0.14581 | 0.16125 | 0.17669 | 0.19213 |
| 320.0 | 0.00000 | 0.02193 | 0.03737 | 0.05281 | 0.06829 | 0.08369 | 0.09913 | 0.11460 | 0.12991 | 0.14545 | 0.16089 | 0.17633 | 0.19177 |
| 330.0 | 0.00000 | 0.02157 | 0.03701 | 0.05245 | 0.06793 | 0.08333 | 0.09877 | 0.11424 | 0.12955 | 0.14509 | 0.16053 | 0.17597 | 0.19141 |
| 340.0 | 0.00000 | 0.02121 | 0.03665 | 0.05209 | 0.06757 | 0.08297 | 0.09841 | 0.11388 | 0.12919 | 0.14473 | 0.16017 | 0.17561 | 0.19105 |
| 350.0 | 0.00000 | 0.02085 | 0.03629 | 0.05173 | 0.06721 | 0.08261 | 0.09805 | 0.11352 | 0.12883 | 0.14437 | 0.15981 | 0.17525 | 0.19069 |

Flight Condition 9

UP VALUES FROM ROOT TO TIP AT ALL AZIMUTH STATIONS

| X/R | 0.240 | 0.301 | 0.362 | 0.423 | 0.483 | 0.544 | 0.605 | 0.666 | 0.727 | 0.787 | 0.848 | 0.909 | 0.970 |
|-------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
| PSI | | | | | | | | | | | | | |
| 10.0 | -0.01681 | -0.02358 | -0.02943 | -0.03731 | -0.04385 | -0.05106 | -0.06098 | -0.06771 | -0.08628 | -0.09524 | -0.09442 | -0.08668 | -0.00221 |
| 15.0 | -0.04133 | -0.05992 | -0.07160 | -0.08134 | -0.09468 | -0.09613 | -0.08122 | -0.06551 | -0.06495 | -0.04177 | -0.03358 | -0.00022 | -0.00211 |
| 20.0 | -0.07332 | -0.09111 | -0.09918 | -0.09755 | -0.06222 | -0.05113 | -0.04025 | -0.03314 | -0.01148 | -0.01441 | -0.01118 | -0.00073 | -0.00015 |
| 25.0 | -0.06566 | -0.00611 | -0.00077 | -0.00205 | -0.00205 | -0.01666 | -0.00359 | -0.00116 | -0.00097 | -0.00082 | -0.00069 | -0.00059 | -0.00008 |
| 30.0 | -0.02274 | -0.00114 | -0.00072 | -0.00115 | -0.00095 | -0.00095 | -0.00076 | -0.00058 | -0.00023 | -0.00016 | -0.00013 | -0.00011 | -0.00002 |
| 35.0 | -0.01151 | -0.00117 | -0.00005 | -0.00002 | -0.00001 | -0.00002 | -0.00018 | -0.00008 | -0.00002 | -0.00001 | -0.00001 | -0.00001 | -0.00001 |
| 40.0 | -0.00099 | -0.00005 | -0.00003 | -0.00001 | -0.00001 | -0.00001 | -0.00018 | -0.00008 | -0.00001 | -0.00001 | -0.00001 | -0.00001 | -0.00001 |
| 45.0 | -0.01338 | -0.00005 | -0.00003 | -0.00002 | -0.00001 | -0.00001 | -0.00018 | -0.00007 | -0.00001 | -0.00001 | -0.00001 | -0.00001 | -0.00001 |
| 50.0 | -0.01000 | -0.00005 | -0.00003 | -0.00002 | -0.00001 | -0.00001 | -0.00018 | -0.00007 | -0.00001 | -0.00001 | -0.00001 | -0.00001 | -0.00001 |
| 55.0 | -0.00732 | -0.00005 | -0.00003 | -0.00002 | -0.00001 | -0.00001 | -0.00018 | -0.00007 | -0.00001 | -0.00001 | -0.00001 | -0.00001 | -0.00001 |
| 60.0 | -0.00474 | -0.00005 | -0.00003 | -0.00002 | -0.00001 | -0.00001 | -0.00018 | -0.00007 | -0.00001 | -0.00001 | -0.00001 | -0.00001 | -0.00001 |
| 65.0 | -0.00224 | -0.00005 | -0.00003 | -0.00002 | -0.00001 | -0.00001 | -0.00018 | -0.00007 | -0.00001 | -0.00001 | -0.00001 | -0.00001 | -0.00001 |
| 70.0 | -0.00074 | -0.00005 | -0.00003 | -0.00002 | -0.00001 | -0.00001 | -0.00018 | -0.00007 | -0.00001 | -0.00001 | -0.00001 | -0.00001 | -0.00001 |
| 75.0 | -0.00024 | -0.00005 | -0.00003 | -0.00002 | -0.00001 | -0.00001 | -0.00018 | -0.00007 | -0.00001 | -0.00001 | -0.00001 | -0.00001 | -0.00001 |
| 80.0 | -0.00074 | -0.00005 | -0.00003 | -0.00002 | -0.00001 | -0.00001 | -0.00018 | -0.00007 | -0.00001 | -0.00001 | -0.00001 | -0.00001 | -0.00001 |
| 85.0 | -0.00124 | -0.00005 | -0.00003 | -0.00002 | -0.00001 | -0.00001 | -0.00018 | -0.00007 | -0.00001 | -0.00001 | -0.00001 | -0.00001 | -0.00001 |
| 90.0 | -0.00174 | -0.00005 | -0.00003 | -0.00002 | -0.00001 | -0.00001 | -0.00018 | -0.00007 | -0.00001 | -0.00001 | -0.00001 | -0.00001 | -0.00001 |
| 95.0 | -0.00224 | -0.00005 | -0.00003 | -0.00002 | -0.00001 | -0.00001 | -0.00018 | -0.00007 | -0.00001 | -0.00001 | -0.00001 | -0.00001 | -0.00001 |
| 100.0 | -0.00274 | -0.00005 | -0.00003 | -0.00002 | -0.00001 | -0.00001 | -0.00018 | -0.00007 | -0.00001 | -0.00001 | -0.00001 | -0.00001 | -0.00001 |
| 105.0 | -0.00324 | -0.00005 | -0.00003 | -0.00002 | -0.00001 | -0.00001 | -0.00018 | -0.00007 | -0.00001 | -0.00001 | -0.00001 | -0.00001 | -0.00001 |
| 110.0 | -0.00374 | -0.00005 | -0.00003 | -0.00002 | -0.00001 | -0.00001 | -0.00018 | -0.00007 | -0.00001 | -0.00001 | -0.00001 | -0.00001 | -0.00001 |
| 115.0 | -0.00424 | -0.00005 | -0.00003 | -0.00002 | -0.00001 | -0.00001 | -0.00018 | -0.00007 | -0.00001 | -0.00001 | -0.00001 | -0.00001 | -0.00001 |
| 120.0 | -0.00474 | -0.00005 | -0.00003 | -0.00002 | -0.00001 | -0.00001 | -0.00018 | -0.00007 | -0.00001 | -0.00001 | -0.00001 | -0.00001 | -0.00001 |
| 125.0 | -0.00524 | -0.00005 | -0.00003 | -0.00002 | -0.00001 | -0.00001 | -0.00018 | -0.00007 | -0.00001 | -0.00001 | -0.00001 | -0.00001 | -0.00001 |
| 130.0 | -0.00574 | -0.00005 | -0.00003 | -0.00002 | -0.00001 | -0.00001 | -0.00018 | -0.00007 | -0.00001 | -0.00001 | -0.00001 | -0.00001 | -0.00001 |
| 135.0 | -0.00624 | -0.00005 | -0.00003 | -0.00002 | -0.00001 | -0.00001 | -0.00018 | -0.00007 | -0.00001 | -0.00001 | -0.00001 | -0.00001 | -0.00001 |

Flight Condition 11



UP VALUES FROM ROOT TO TIP AT ALL AZIMUTH STATIONS

| X/R | 0.240 | 0.301 | 0.362 | 0.423 | 0.483 | 0.544 | 0.605 | 0.666 | 0.727 | 0.787 | 0.848 | 0.909 | 0.970 |
|-------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| PSI | | | | | | | | | | | | | |
| 0.0 | 0.04877 | 0.03393 | 0.02559 | 0.02048 | 0.01651 | 0.01348 | 0.01119 | 0.00944 | 0.00806 | 0.00694 | 0.00596 | 0.00509 | 0.00431 |
| 10.0 | 0.04839 | 0.03297 | 0.02463 | 0.01952 | 0.01555 | 0.01252 | 0.01023 | 0.00848 | 0.00710 | 0.00600 | 0.00502 | 0.00415 | 0.00337 |
| 20.0 | 0.04762 | 0.03204 | 0.02370 | 0.01859 | 0.01462 | 0.01159 | 0.00930 | 0.00755 | 0.00617 | 0.00507 | 0.00409 | 0.00322 | 0.00244 |
| 30.0 | 0.04640 | 0.03064 | 0.02230 | 0.01719 | 0.01322 | 0.01019 | 0.00790 | 0.00615 | 0.00477 | 0.00367 | 0.00269 | 0.00182 | 0.00104 |
| 40.0 | 0.04466 | 0.02890 | 0.02056 | 0.01515 | 0.01118 | 0.00815 | 0.00586 | 0.00411 | 0.00273 | 0.00163 | 0.00065 | 0.00001 | 0.00000 |
| 50.0 | 0.04244 | 0.02668 | 0.01834 | 0.01293 | 0.00896 | 0.00593 | 0.00364 | 0.00189 | 0.00051 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| 60.0 | 0.03977 | 0.02391 | 0.01557 | 0.01016 | 0.00619 | 0.00316 | 0.00087 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| 70.0 | 0.03664 | 0.02165 | 0.01331 | 0.00790 | 0.00393 | 0.00090 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| 80.0 | 0.03309 | 0.01899 | 0.01065 | 0.00524 | 0.00127 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| 90.0 | 0.02904 | 0.01594 | 0.00760 | 0.00219 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| 100.0 | 0.02459 | 0.01294 | 0.00460 | 0.00110 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| 110.0 | 0.02064 | 0.00994 | 0.00315 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| 120.0 | 0.01719 | 0.00694 | 0.00165 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| 130.0 | 0.01424 | 0.00394 | 0.00015 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| 140.0 | 0.01179 | 0.00194 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| 150.0 | 0.00979 | 0.00094 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| 160.0 | 0.00779 | 0.00044 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| 170.0 | 0.00579 | 0.00014 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| 180.0 | 0.00379 | 0.00004 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| 190.0 | 0.00179 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| 200.0 | 0.00079 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| 210.0 | 0.00029 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| 220.0 | 0.00019 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| 230.0 | 0.00009 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| 240.0 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |

Flight Condition 13

UP VALUES FROM ROOT TO TIP AT ALL AZIMUTH STATIONS

| | X/R | 0.240 | 0.301 | 0.362 | 0.423 | 0.483 | 0.544 | 0.605 | 0.666 | 0.727 | 0.787 | 0.848 | 0.909 | 0.970 |
|-------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|-------|
| PSI | | | | | | | | | | | | | | |
| 0.0 | -0.35984 | -0.04840 | -0.03803 | -0.03008 | -0.02424 | -0.01980 | -0.01644 | -0.01388 | -0.01186 | -0.01023 | -0.00880 | -0.00752 | -0.00638 | |
| 15.0 | -0.04452 | -0.03517 | -0.02797 | -0.02243 | -0.01816 | -0.01471 | -0.01193 | -0.00967 | -0.00779 | -0.00621 | -0.00481 | -0.00360 | -0.00256 | |
| 30.0 | -0.02110 | -0.01744 | -0.01399 | -0.01086 | -0.00821 | -0.00602 | -0.00436 | -0.00317 | -0.00235 | -0.00181 | -0.00142 | -0.00115 | -0.00095 | |
| 45.0 | -0.01066 | -0.00801 | -0.00586 | -0.00387 | -0.00273 | -0.00206 | -0.00170 | -0.00147 | -0.00130 | -0.00115 | -0.00101 | -0.00088 | -0.00076 | |
| 60.0 | -0.00498 | -0.00282 | -0.00147 | -0.00087 | -0.00072 | -0.00071 | -0.00070 | -0.00067 | -0.00062 | -0.00056 | -0.00049 | -0.00042 | -0.00037 | |
| 75.0 | -0.00136 | 0.00015 | 0.00070 | 0.00065 | 0.00043 | 0.00024 | 0.00011 | 0.00004 | 0.00000 | -0.00001 | -0.00002 | -0.00002 | -0.00002 | |
| 90.0 | 0.00128 | 0.00227 | 0.00236 | 0.00203 | 0.00164 | 0.00130 | 0.00104 | 0.00084 | 0.00068 | 0.00054 | 0.00047 | 0.00039 | 0.00033 | |
| 105.0 | 0.00377 | 0.00463 | 0.00468 | 0.00426 | 0.00369 | 0.00309 | 0.00251 | 0.00206 | 0.00167 | 0.00137 | 0.00112 | 0.00093 | 0.00078 | |
| 120.0 | 0.00692 | 0.00846 | 0.00920 | 0.00900 | 0.00804 | 0.00668 | 0.00535 | 0.00421 | 0.00332 | 0.00265 | 0.00213 | 0.00173 | 0.00142 | |
| 135.0 | 0.01123 | 0.01405 | 0.01606 | 0.01630 | 0.01472 | 0.01215 | 0.00959 | 0.00747 | 0.00584 | 0.00463 | 0.00369 | 0.00298 | 0.00243 | |
| 150.0 | 0.01809 | 0.02125 | 0.02285 | 0.02223 | 0.02010 | 0.01730 | 0.01453 | 0.01204 | 0.00989 | 0.00810 | 0.00658 | 0.00532 | 0.00431 | |
| 165.0 | 0.03179 | 0.03604 | 0.03609 | 0.03205 | 0.02846 | 0.02633 | 0.02465 | 0.02231 | 0.01928 | 0.01609 | 0.01303 | 0.01035 | 0.00814 | |
| 180.0 | 0.03894 | 0.04407 | 0.04824 | 0.04252 | 0.03746 | 0.03534 | 0.03420 | 0.03165 | 0.02754 | 0.02293 | 0.01841 | 0.01442 | 0.01111 | |
| 195.0 | 0.03132 | 0.03489 | 0.03467 | 0.03097 | 0.02761 | 0.02537 | 0.02346 | 0.02107 | 0.01817 | 0.01519 | 0.01235 | 0.00987 | 0.00781 | |
| 210.0 | 0.01894 | 0.02125 | 0.02205 | 0.02101 | 0.01888 | 0.01630 | 0.01379 | 0.01151 | 0.00952 | 0.00765 | 0.00641 | 0.00522 | 0.00426 | |
| 225.0 | 0.01209 | 0.01403 | 0.01506 | 0.01467 | 0.01308 | 0.01092 | 0.00881 | 0.00703 | 0.00561 | 0.00452 | 0.00366 | 0.00299 | 0.00246 | |
| 240.0 | 0.00752 | 0.00856 | 0.00885 | 0.00838 | 0.00739 | 0.00617 | 0.00501 | 0.00402 | 0.00323 | 0.00261 | 0.00213 | 0.00175 | 0.00145 | |
| 255.0 | 0.00410 | 0.00468 | 0.00461 | 0.00417 | 0.00360 | 0.00301 | 0.00248 | 0.00203 | 0.00166 | 0.00137 | 0.00113 | 0.00094 | 0.00079 | |
| 270.0 | 0.00134 | 0.00209 | 0.00215 | 0.00188 | 0.00156 | 0.00127 | 0.00102 | 0.00083 | 0.00068 | 0.00056 | 0.00047 | 0.00039 | 0.00033 | |
| 285.0 | -0.00146 | -0.00019 | 0.00030 | 0.00035 | 0.00024 | 0.00013 | 0.00004 | 0.00001 | -0.00002 | -0.00003 | -0.00003 | -0.00003 | -0.00003 | |
| 300.0 | -0.00514 | -0.00319 | -0.00196 | -0.00133 | -0.00105 | -0.00092 | -0.00082 | -0.00074 | -0.00066 | -0.00058 | -0.00051 | -0.00044 | -0.00038 | |
| 315.0 | -0.01082 | -0.00818 | -0.00596 | -0.00429 | -0.00317 | -0.00245 | -0.00197 | -0.00165 | -0.00140 | -0.00121 | -0.00104 | -0.00090 | -0.00077 | |
| 330.0 | -0.02106 | -0.01716 | -0.01365 | -0.01061 | -0.00814 | -0.00614 | -0.00462 | -0.00349 | -0.00267 | -0.00209 | -0.00165 | -0.00133 | -0.00108 | |
| 345.0 | -0.04253 | -0.03371 | -0.02677 | -0.02142 | -0.01730 | -0.01399 | -0.01134 | -0.00919 | -0.00742 | -0.00595 | -0.00467 | -0.00357 | -0.00266 | |

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Flight Condition 14

UP VALUES FROM ROOT TO TIP AT ALL AZIMUTH STATIONS

| X/R | 0.240 | 0.301 | 0.362 | 0.423 | 0.483 | 0.544 | 0.605 | 0.666 | 0.727 | 0.787 | 0.848 | 0.909 | 0.970 |
|-------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
| PSI | -0.04616 | -0.01113 | -0.03465 | -0.02889 | -0.02435 | -0.02074 | -0.01798 | -0.01588 | -0.01472 | -0.01297 | -0.01153 | -0.00979 | -0.00822 |
| 15.0 | -0.03702 | -0.02336 | -0.02110 | -0.02332 | -0.02150 | -0.02074 | -0.01677 | -0.01314 | -0.01132 | -0.01297 | -0.01153 | -0.00979 | -0.00822 |
| 30.0 | -0.02167 | -0.01325 | -0.01123 | -0.01191 | -0.01400 | -0.01521 | -0.01407 | -0.01169 | -0.01132 | -0.01167 | -0.00982 | -0.00768 | -0.00577 |
| 45.0 | -0.00893 | -0.00508 | -0.00427 | -0.00414 | -0.00457 | -0.00496 | -0.00522 | -0.00522 | -0.00477 | -0.00477 | -0.00441 | -0.00399 | -0.00347 |
| 60.0 | -0.00469 | -0.00271 | -0.00279 | -0.00287 | -0.00343 | -0.00444 | -0.00522 | -0.00577 | -0.00577 | -0.00522 | -0.00477 | -0.00419 | -0.00354 |
| 75.0 | -0.00004 | -0.00271 | -0.00355 | -0.00387 | -0.00429 | -0.00484 | -0.00522 | -0.00522 | -0.00477 | -0.00477 | -0.00441 | -0.00399 | -0.00347 |
| 90.0 | 0.00559 | 0.00544 | 0.00521 | 0.00581 | 0.00649 | 0.00728 | 0.00785 | 0.00822 | 0.00822 | 0.00777 | 0.00729 | 0.00681 | 0.00633 |
| 105.0 | 0.00982 | 0.00911 | 0.00858 | 0.00871 | 0.00943 | 0.01021 | 0.01085 | 0.01122 | 0.01122 | 0.01077 | 0.01029 | 0.00981 | 0.00933 |
| 120.0 | 0.01392 | 0.01323 | 0.01254 | 0.01273 | 0.01358 | 0.01447 | 0.01508 | 0.01544 | 0.01544 | 0.01499 | 0.01451 | 0.01403 | 0.01355 |
| 135.0 | 0.01745 | 0.01686 | 0.01617 | 0.01643 | 0.01738 | 0.01837 | 0.01908 | 0.01944 | 0.01944 | 0.01899 | 0.01851 | 0.01803 | 0.01755 |
| 150.0 | 0.02057 | 0.02008 | 0.01939 | 0.01974 | 0.02079 | 0.02188 | 0.02259 | 0.02294 | 0.02294 | 0.02249 | 0.02201 | 0.02153 | 0.02105 |
| 165.0 | 0.02320 | 0.02281 | 0.02212 | 0.02257 | 0.02372 | 0.02497 | 0.02582 | 0.02618 | 0.02618 | 0.02573 | 0.02525 | 0.02477 | 0.02429 |
| 180.0 | 0.02537 | 0.02511 | 0.02442 | 0.02497 | 0.02632 | 0.02777 | 0.02832 | 0.02868 | 0.02868 | 0.02823 | 0.02775 | 0.02727 | 0.02679 |
| 195.0 | 0.02700 | 0.02684 | 0.02615 | 0.02670 | 0.02815 | 0.02970 | 0.03025 | 0.03061 | 0.03061 | 0.03016 | 0.02968 | 0.02920 | 0.02872 |
| 210.0 | 0.02817 | 0.02811 | 0.02742 | 0.02797 | 0.02952 | 0.03117 | 0.03172 | 0.03208 | 0.03208 | 0.03163 | 0.03115 | 0.03067 | 0.03019 |
| 225.0 | 0.02880 | 0.02884 | 0.02815 | 0.02870 | 0.03025 | 0.03190 | 0.03245 | 0.03281 | 0.03281 | 0.03236 | 0.03188 | 0.03140 | 0.03092 |
| 240.0 | 0.02900 | 0.02914 | 0.02845 | 0.02900 | 0.03055 | 0.03220 | 0.03275 | 0.03311 | 0.03311 | 0.03266 | 0.03218 | 0.03170 | 0.03122 |
| 255.0 | 0.02880 | 0.02894 | 0.02825 | 0.02880 | 0.03035 | 0.03200 | 0.03255 | 0.03291 | 0.03291 | 0.03246 | 0.03198 | 0.03150 | 0.03102 |
| 270.0 | 0.02820 | 0.02834 | 0.02769 | 0.02824 | 0.02979 | 0.03144 | 0.03200 | 0.03236 | 0.03236 | 0.03191 | 0.03143 | 0.03095 | 0.03047 |
| 285.0 | 0.02720 | 0.02734 | 0.02669 | 0.02724 | 0.02879 | 0.03044 | 0.03100 | 0.03136 | 0.03136 | 0.03091 | 0.03043 | 0.02995 | 0.02947 |
| 300.0 | 0.02580 | 0.02594 | 0.02529 | 0.02584 | 0.02739 | 0.02904 | 0.02960 | 0.02996 | 0.02996 | 0.02951 | 0.02903 | 0.02855 | 0.02807 |
| 315.0 | 0.02400 | 0.02414 | 0.02349 | 0.02404 | 0.02559 | 0.02724 | 0.02780 | 0.02816 | 0.02816 | 0.02771 | 0.02723 | 0.02675 | 0.02627 |
| 330.0 | 0.02180 | 0.02194 | 0.02129 | 0.02184 | 0.02339 | 0.02504 | 0.02560 | 0.02596 | 0.02596 | 0.02551 | 0.02503 | 0.02455 | 0.02407 |
| 345.0 | 0.01920 | 0.01934 | 0.01869 | 0.01924 | 0.02079 | 0.02244 | 0.02300 | 0.02336 | 0.02336 | 0.02291 | 0.02243 | 0.02195 | 0.02147 |

Flight Condition 16

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OF POOR QUALITY

UP VALUES FROM ROOT TO TIP AT ALL AZIMUTH STATIONS

| X/R | 0.200 | 0.300 | 0.362 | 0.425 | 0.485 | 0.544 | 0.605 | 0.666 | 0.727 | 0.787 | 0.848 | 0.909 | 0.970 |
|-----|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| 0.0 | 0.04542 | 0.05588 | 0.06457 | 0.07229 | 0.07914 | 0.08514 | 0.09037 | 0.09494 | 0.09894 | 0.10246 | 0.10559 | 0.10834 | 0.11071 |
| 10 | 0.04496 | 0.05536 | 0.06404 | 0.07176 | 0.07861 | 0.08461 | 0.08984 | 0.09441 | 0.09841 | 0.10193 | 0.10506 | 0.10781 | 0.11018 |
| 20 | 0.04450 | 0.05485 | 0.06353 | 0.07125 | 0.07810 | 0.08410 | 0.08933 | 0.09390 | 0.09790 | 0.10142 | 0.10455 | 0.10730 | 0.10967 |
| 30 | 0.04404 | 0.05439 | 0.06307 | 0.07079 | 0.07764 | 0.08364 | 0.08887 | 0.09344 | 0.09744 | 0.10096 | 0.10409 | 0.10684 | 0.10921 |
| 40 | 0.04358 | 0.05393 | 0.06261 | 0.07063 | 0.07748 | 0.08348 | 0.08871 | 0.09328 | 0.09728 | 0.10080 | 0.10393 | 0.10668 | 0.10905 |
| 50 | 0.04312 | 0.05347 | 0.06215 | 0.07017 | 0.07702 | 0.08302 | 0.08825 | 0.09282 | 0.09682 | 0.10034 | 0.10347 | 0.10622 | 0.10859 |
| 60 | 0.04266 | 0.05301 | 0.06169 | 0.06971 | 0.07656 | 0.08256 | 0.08779 | 0.09236 | 0.09636 | 0.09988 | 0.10301 | 0.10576 | 0.10813 |
| 70 | 0.04220 | 0.05255 | 0.06123 | 0.06925 | 0.07610 | 0.08210 | 0.08733 | 0.09190 | 0.09590 | 0.09942 | 0.10255 | 0.10530 | 0.10767 |
| 80 | 0.04174 | 0.05209 | 0.06077 | 0.06879 | 0.07564 | 0.08164 | 0.08687 | 0.09144 | 0.09544 | 0.09896 | 0.10209 | 0.10484 | 0.10721 |
| 90 | 0.04128 | 0.05163 | 0.06031 | 0.06833 | 0.07518 | 0.08118 | 0.08641 | 0.09098 | 0.09498 | 0.09850 | 0.10163 | 0.10438 | 0.10675 |
| 100 | 0.04082 | 0.05117 | 0.05985 | 0.06787 | 0.07472 | 0.08072 | 0.08595 | 0.09052 | 0.09452 | 0.09804 | 0.10117 | 0.10392 | 0.10629 |
| 110 | 0.04036 | 0.05071 | 0.05939 | 0.06741 | 0.07426 | 0.08026 | 0.08549 | 0.09006 | 0.09406 | 0.09758 | 0.10071 | 0.10346 | 0.10583 |
| 120 | 0.03990 | 0.05025 | 0.05893 | 0.06695 | 0.07380 | 0.07980 | 0.08503 | 0.08960 | 0.09360 | 0.09712 | 0.10025 | 0.10300 | 0.10537 |
| 130 | 0.03944 | 0.04979 | 0.05847 | 0.06649 | 0.07334 | 0.07934 | 0.08457 | 0.08914 | 0.09314 | 0.09666 | 0.09979 | 0.10254 | 0.10491 |
| 140 | 0.03898 | 0.04933 | 0.05801 | 0.06603 | 0.07288 | 0.07888 | 0.08411 | 0.08868 | 0.09268 | 0.09620 | 0.09933 | 0.10208 | 0.10445 |
| 150 | 0.03852 | 0.04887 | 0.05755 | 0.06557 | 0.07242 | 0.07842 | 0.08365 | 0.08822 | 0.09222 | 0.09574 | 0.09887 | 0.10162 | 0.10399 |
| 160 | 0.03806 | 0.04841 | 0.05709 | 0.06511 | 0.07196 | 0.07796 | 0.08319 | 0.08776 | 0.09176 | 0.09528 | 0.09841 | 0.10116 | 0.10353 |
| 170 | 0.03760 | 0.04795 | 0.05663 | 0.06465 | 0.07150 | 0.07750 | 0.08273 | 0.08730 | 0.09130 | 0.09482 | 0.09795 | 0.10070 | 0.10307 |
| 180 | 0.03714 | 0.04749 | 0.05617 | 0.06419 | 0.07104 | 0.07704 | 0.08227 | 0.08684 | 0.09084 | 0.09436 | 0.09749 | 0.10024 | 0.10261 |
| 190 | 0.03668 | 0.04703 | 0.05571 | 0.06373 | 0.07068 | 0.07668 | 0.08191 | 0.08648 | 0.09048 | 0.09400 | 0.09713 | 0.09988 | 0.10225 |
| 200 | 0.03622 | 0.04657 | 0.05525 | 0.06327 | 0.07022 | 0.07622 | 0.08145 | 0.08602 | 0.09002 | 0.09354 | 0.09667 | 0.09942 | 0.10179 |
| 210 | 0.03576 | 0.04611 | 0.05479 | 0.06281 | 0.06976 | 0.07576 | 0.08099 | 0.08556 | 0.08956 | 0.09308 | 0.09621 | 0.09896 | 0.10133 |
| 220 | 0.03530 | 0.04565 | 0.05433 | 0.06235 | 0.06930 | 0.07530 | 0.08053 | 0.08510 | 0.08910 | 0.09262 | 0.09575 | 0.09850 | 0.10087 |
| 230 | 0.03484 | 0.04519 | 0.05387 | 0.06189 | 0.06884 | 0.07484 | 0.08007 | 0.08464 | 0.08864 | 0.09216 | 0.09529 | 0.09804 | 0.10041 |
| 240 | 0.03438 | 0.04473 | 0.05341 | 0.06143 | 0.06838 | 0.07438 | 0.07961 | 0.08418 | 0.08818 | 0.09170 | 0.09483 | 0.09758 | 0.10005 |
| 250 | 0.03392 | 0.04427 | 0.05295 | 0.06097 | 0.06792 | 0.07392 | 0.07915 | 0.08372 | 0.08772 | 0.09124 | 0.09437 | 0.09712 | 0.09949 |
| 260 | 0.03346 | 0.04381 | 0.05249 | 0.06051 | 0.06746 | 0.07346 | 0.07869 | 0.08326 | 0.08726 | 0.09078 | 0.09391 | 0.09666 | 0.09903 |
| 270 | 0.03300 | 0.04335 | 0.05203 | 0.06005 | 0.06700 | 0.07300 | 0.07823 | 0.08280 | 0.08680 | 0.09032 | 0.09345 | 0.09620 | 0.09857 |
| 280 | 0.03254 | 0.04289 | 0.05157 | 0.05959 | 0.06654 | 0.07254 | 0.07777 | 0.08234 | 0.08634 | 0.08986 | 0.09299 | 0.09574 | 0.09811 |
| 290 | 0.03208 | 0.04243 | 0.05111 | 0.05913 | 0.06608 | 0.07208 | 0.07731 | 0.08188 | 0.08588 | 0.08940 | 0.09253 | 0.09528 | 0.09765 |
| 300 | 0.03162 | 0.04197 | 0.05065 | 0.05867 | 0.06562 | 0.07162 | 0.07685 | 0.08142 | 0.08542 | 0.08894 | 0.09207 | 0.09482 | 0.09719 |

Flight Condition 18

UP VALUES FROM ROOT TO TIP AT ALL AZIMUTH STATIONS

| X/R | 0.248 | 0.301 | 0.362 | 0.423 | 0.483 | 0.544 | 0.605 | 0.666 | 0.727 | 0.787 | 0.848 | 0.909 | 0.970 |
|-------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
| P.51 | -0.04699 | -0.03588 | -0.02605 | -0.01968 | -0.01326 | -0.01294 | -0.00975 | -0.00797 | -0.00448 | -0.00329 | -0.00407 | -0.00213 | -0.00238 |
| 10.0 | -0.03334 | -0.02544 | -0.01882 | -0.01510 | -0.01187 | -0.00944 | -0.00740 | -0.00545 | -0.00345 | -0.00249 | -0.00312 | -0.00143 | -0.00169 |
| 15.0 | -0.01777 | -0.01348 | -0.01082 | -0.00853 | -0.00677 | -0.00528 | -0.00429 | -0.00347 | -0.00275 | -0.00221 | -0.00177 | -0.00142 | -0.00114 |
| 45.0 | -0.00935 | -0.00735 | -0.00590 | -0.00466 | -0.00369 | -0.00293 | -0.00235 | -0.00187 | -0.00151 | -0.00122 | -0.00099 | -0.00081 | -0.00066 |
| 60.0 | -0.00558 | -0.00421 | -0.00329 | -0.00258 | -0.00204 | -0.00162 | -0.00129 | -0.00094 | -0.00074 | -0.00059 | -0.00056 | -0.00047 | -0.00039 |
| 75.0 | -0.00318 | -0.00236 | -0.00179 | -0.00138 | -0.00108 | -0.00083 | -0.00067 | -0.00054 | -0.00044 | -0.00035 | -0.00029 | -0.00024 | -0.00020 |
| 105.0 | -0.00113 | -0.00077 | -0.00057 | -0.00044 | -0.00034 | -0.00027 | -0.00022 | -0.00016 | -0.00012 | -0.00008 | -0.00005 | -0.00003 | -0.00002 |
| 120.0 | -0.00049 | -0.00031 | -0.00021 | -0.00016 | -0.00012 | -0.00009 | -0.00007 | -0.00005 | -0.00004 | -0.00003 | -0.00002 | -0.00001 | -0.00001 |
| 135.0 | -0.00028 | -0.00019 | -0.00014 | -0.00011 | -0.00008 | -0.00006 | -0.00004 | -0.00003 | -0.00002 | -0.00001 | -0.00001 | -0.00000 | -0.00000 |
| 150.0 | -0.00015 | -0.00010 | -0.00007 | -0.00005 | -0.00004 | -0.00003 | -0.00002 | -0.00001 | -0.00001 | -0.00000 | -0.00000 | -0.00000 | -0.00000 |
| 165.0 | -0.00008 | -0.00005 | -0.00004 | -0.00003 | -0.00002 | -0.00001 | -0.00001 | -0.00001 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 |
| 180.0 | -0.00004 | -0.00003 | -0.00002 | -0.00001 | -0.00001 | -0.00001 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 |
| 210.0 | -0.00002 | -0.00001 | -0.00001 | -0.00001 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 |
| 225.0 | -0.00001 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 |
| 240.0 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 |
| 255.0 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 |
| 270.0 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 |
| 285.0 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 |
| 300.0 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 |
| 315.0 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 |
| 330.0 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 |
| 345.0 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 |

Flight Condition 19

TABLE 11
OF POOR QUALITY

UP VALUES FROM ROOT TO TIP AT ALL AZIMUTH STATIONS

| X/R | 0.248 | 0.301 | 0.362 | 0.423 | 0.483 | 0.544 | 0.605 | 0.666 | 0.727 | 0.787 | 0.848 | 0.909 | 0.970 |
|------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 100 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 150 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 200 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 250 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 300 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 350 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 400 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 450 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 500 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 550 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 600 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 650 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 700 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 750 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 800 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 850 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 900 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 950 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 1000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |

Flight Condition 20

UP VALUES FROM ROOT TO TIP AT ALL AZIMUTH STATIONS

| X/R | 0.240 | 0.301 | 0.362 | 0.423 | 0.483 | 0.544 | 0.605 | 0.666 | 0.727 | 0.787 | 0.848 | 0.909 | 0.970 |
|-------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
| 9.0 | 0.04573 | -0.02659 | -0.05619 | -0.08491 | -0.11286 | -0.14009 | -0.16659 | -0.19237 | -0.21742 | -0.24178 | -0.26548 | -0.28856 | -0.31102 |
| 10.0 | 0.03429 | -0.01962 | -0.04273 | -0.06378 | -0.08274 | -0.10060 | -0.11737 | -0.13304 | -0.14762 | -0.16114 | -0.17364 | -0.18515 | -0.19568 |
| 15.0 | 0.01794 | -0.00919 | -0.01971 | -0.02951 | -0.03860 | -0.04701 | -0.05472 | -0.06187 | -0.06847 | -0.07451 | -0.08009 | -0.08521 | -0.09001 |
| 20.0 | 0.01223 | -0.00641 | -0.01367 | -0.02079 | -0.02778 | -0.03464 | -0.04137 | -0.04798 | -0.05446 | -0.06081 | -0.06704 | -0.07315 | -0.07912 |
| 25.0 | 0.00893 | -0.00474 | -0.00962 | -0.01448 | -0.01930 | -0.02408 | -0.02881 | -0.03349 | -0.03811 | -0.04267 | -0.04718 | -0.05164 | -0.05605 |
| 30.0 | 0.00775 | -0.00418 | -0.00796 | -0.01166 | -0.01533 | -0.01896 | -0.02254 | -0.02607 | -0.02955 | -0.03298 | -0.03636 | -0.03969 | -0.04296 |
| 102.0 | 0.01653 | -0.00789 | -0.01238 | -0.01686 | -0.02134 | -0.02581 | -0.03028 | -0.03474 | -0.03920 | -0.04366 | -0.04812 | -0.05258 | -0.05704 |
| 125.0 | 0.01822 | -0.01234 | -0.01724 | -0.02214 | -0.02704 | -0.03194 | -0.03684 | -0.04174 | -0.04664 | -0.05154 | -0.05644 | -0.06134 | -0.06624 |
| 150.0 | 0.02317 | -0.01928 | -0.02538 | -0.03148 | -0.03758 | -0.04368 | -0.04978 | -0.05588 | -0.06198 | -0.06808 | -0.07418 | -0.08028 | -0.08638 |
| 180.0 | 0.03221 | -0.03191 | -0.04221 | -0.05251 | -0.06281 | -0.07311 | -0.08341 | -0.09371 | -0.10401 | -0.11431 | -0.12461 | -0.13491 | -0.14521 |
| 188.0 | 0.04266 | -0.05391 | -0.06521 | -0.07651 | -0.08781 | -0.09911 | -0.11041 | -0.12171 | -0.13301 | -0.14431 | -0.15561 | -0.16691 | -0.17821 |
| 195.0 | 0.03756 | -0.05853 | -0.07342 | -0.08831 | -0.10320 | -0.11809 | -0.13298 | -0.14787 | -0.16276 | -0.17765 | -0.19254 | -0.20743 | -0.22232 |
| 210.0 | 0.02554 | -0.06254 | -0.08243 | -0.10232 | -0.12221 | -0.14210 | -0.16199 | -0.18188 | -0.20177 | -0.22166 | -0.24155 | -0.26144 | -0.28133 |
| 225.0 | 0.01849 | -0.07181 | -0.09569 | -0.11957 | -0.14345 | -0.16733 | -0.19121 | -0.21509 | -0.23897 | -0.26285 | -0.28673 | -0.31061 | -0.33449 |
| 240.0 | 0.01105 | -0.08196 | -0.10983 | -0.13770 | -0.16557 | -0.19344 | -0.22131 | -0.24918 | -0.27705 | -0.30492 | -0.33279 | -0.36066 | -0.38853 |
| 255.0 | 0.00696 | -0.09771 | -0.12958 | -0.16145 | -0.19332 | -0.22519 | -0.25706 | -0.28893 | -0.32080 | -0.35267 | -0.38454 | -0.41641 | -0.44828 |
| 270.0 | 0.00000 | -0.10000 | -0.13500 | -0.17000 | -0.20500 | -0.24000 | -0.27500 | -0.31000 | -0.34500 | -0.38000 | -0.41500 | -0.45000 | -0.48500 |
| 285.0 | -0.00002 | -0.09442 | -0.12630 | -0.15818 | -0.19006 | -0.22194 | -0.25382 | -0.28570 | -0.31758 | -0.34946 | -0.38134 | -0.41322 | -0.44510 |
| 300.0 | -0.00556 | -0.09442 | -0.12630 | -0.15818 | -0.19006 | -0.22194 | -0.25382 | -0.28570 | -0.31758 | -0.34946 | -0.38134 | -0.41322 | -0.44510 |
| 315.0 | -0.01211 | -0.09195 | -0.12383 | -0.15571 | -0.18759 | -0.21947 | -0.25135 | -0.28323 | -0.31511 | -0.34699 | -0.37887 | -0.41075 | -0.44263 |
| 330.0 | -0.02121 | -0.08115 | -0.11303 | -0.14491 | -0.17679 | -0.20867 | -0.24055 | -0.27243 | -0.30431 | -0.33619 | -0.36807 | -0.40000 | -0.43200 |
| 345.0 | -0.04488 | -0.03370 | -0.02753 | -0.02136 | -0.01519 | -0.00902 | -0.00285 | 0.00332 | 0.00949 | 0.01566 | 0.02183 | 0.02800 | 0.03417 |

Flight Condition 21

UP VALUES FROM ROOT TO TIP AT ALL AZIMUTH STATIONS

| PSI | X/R | 0.246 | 0.301 | 0.362 | 0.423 | 0.483 | 0.544 | 0.605 | 0.666 | 0.727 | 0.787 | 0.848 | 0.909 | 0.970 |
|-------|-----|-----------|------------|------------|------------|------------|------------|-------------|--------|--------|--------|--------|--------|--------|
| 0.0 | 0.0 | 0.0014 | 0.0029 | 0.0072 | 0.0155 | 0.0315 | 0.0613 | 0.1103 | 0.0222 | 0.0768 | 0.0832 | 0.0593 | 0.0093 | 0.0017 |
| 15.0 | 0.0 | 0.0119 | 0.0238 | 0.0366 | 0.0525 | 0.0756 | 0.1089 | 0.1548 | 0.0424 | 0.1240 | 0.0829 | 0.0503 | 0.0097 | 0.0011 |
| 30.0 | 0.0 | 0.0153 | 0.0316 | 0.0482 | 0.0695 | 0.0989 | 0.1402 | 0.1971 | 0.0519 | 0.1412 | 0.0929 | 0.0573 | 0.0099 | 0.0012 |
| 45.0 | 0.0 | 0.0164 | 0.0336 | 0.0517 | 0.0758 | 0.1085 | 0.1548 | 0.2145 | 0.0538 | 0.1452 | 0.0980 | 0.0631 | 0.0099 | 0.0013 |
| 60.0 | 0.0 | 0.0124 | 0.0250 | 0.0376 | 0.0542 | 0.0775 | 0.1119 | 0.1515 | 0.0497 | 0.1392 | 0.0937 | 0.0602 | 0.0099 | 0.0013 |
| 75.0 | 0.0 | 0.0166 | 0.0316 | 0.0476 | 0.0682 | 0.0962 | 0.1369 | 0.1881 | 0.0512 | 0.1367 | 0.0917 | 0.0582 | 0.0099 | 0.0013 |
| 90.0 | 0.0 | 0.0377 | 0.0731 | 0.1097 | 0.1592 | 0.2235 | 0.3045 | 0.4082 | 0.0521 | 0.1367 | 0.0917 | 0.0582 | 0.0099 | 0.0013 |
| 105.0 | 0.0 | 0.0622 | 0.1246 | 0.1891 | 0.2701 | 0.3806 | 0.5245 | 0.7082 | 0.0521 | 0.1367 | 0.0917 | 0.0582 | 0.0099 | 0.0013 |
| 120.0 | 0.0 | 0.1133 | 0.2250 | 0.3377 | 0.4960 | 0.7192 | 1.0070 | 1.3852 | 0.0521 | 0.1367 | 0.0917 | 0.0582 | 0.0099 | 0.0013 |
| 135.0 | 0.0 | 0.2270 | 0.4504 | 0.6774 | 1.0160 | 1.5020 | 2.1266 | 2.9322 | 0.0521 | 0.1367 | 0.0917 | 0.0582 | 0.0099 | 0.0013 |
| 150.0 | 0.0 | 0.4509 | 0.9118 | 1.3671 | 2.0257 | 2.9478 | 4.1256 | 5.7322 | 0.0521 | 0.1367 | 0.0917 | 0.0582 | 0.0099 | 0.0013 |
| 165.0 | 0.0 | 0.9118 | 1.8237 | 2.7342 | 4.0257 | 5.8235 | 8.2392 | 11.5320 | 0.0521 | 0.1367 | 0.0917 | 0.0582 | 0.0099 | 0.0013 |
| 180.0 | 0.0 | 1.8237 | 3.6474 | 5.4686 | 8.0514 | 11.6570 | 16.4744 | 23.0643 | 0.0521 | 0.1367 | 0.0917 | 0.0582 | 0.0099 | 0.0013 |
| 195.0 | 0.0 | 3.6474 | 7.2948 | 10.9372 | 16.1028 | 23.3141 | 33.3922 | 46.1280 | 0.0521 | 0.1367 | 0.0917 | 0.0582 | 0.0099 | 0.0013 |
| 210.0 | 0.0 | 7.2948 | 14.5896 | 21.8744 | 32.2056 | 46.6282 | 66.7844 | 96.2560 | 0.0521 | 0.1367 | 0.0917 | 0.0582 | 0.0099 | 0.0013 |
| 225.0 | 0.0 | 14.5896 | 29.1792 | 43.7488 | 64.4112 | 93.2564 | 133.5688 | 192.5120 | 0.0521 | 0.1367 | 0.0917 | 0.0582 | 0.0099 | 0.0013 |
| 240.0 | 0.0 | 29.1792 | 58.3584 | 87.4976 | 128.8224 | 186.5128 | 267.1376 | 385.0240 | 0.0521 | 0.1367 | 0.0917 | 0.0582 | 0.0099 | 0.0013 |
| 255.0 | 0.0 | 58.3584 | 116.7168 | 174.9952 | 257.6448 | 373.0256 | 534.2752 | 770.0480 | 0.0521 | 0.1367 | 0.0917 | 0.0582 | 0.0099 | 0.0013 |
| 270.0 | 0.0 | 116.7168 | 233.4336 | 349.9904 | 515.2896 | 746.0512 | 1068.5504 | 1540.0960 | 0.0521 | 0.1367 | 0.0917 | 0.0582 | 0.0099 | 0.0013 |
| 285.0 | 0.0 | 233.4336 | 466.8672 | 699.9808 | 1030.5792 | 1492.1024 | 2137.1008 | 3080.1920 | 0.0521 | 0.1367 | 0.0917 | 0.0582 | 0.0099 | 0.0013 |
| 300.0 | 0.0 | 466.8672 | 933.7344 | 1399.9616 | 2061.1584 | 2984.2048 | 4274.2016 | 6160.3840 | 0.0521 | 0.1367 | 0.0917 | 0.0582 | 0.0099 | 0.0013 |
| 315.0 | 0.0 | 933.7344 | 1867.4688 | 2799.9232 | 4122.3168 | 5968.4096 | 8548.4032 | 12320.7680 | 0.0521 | 0.1367 | 0.0917 | 0.0582 | 0.0099 | 0.0013 |
| 330.0 | 0.0 | 1867.4688 | 3734.9376 | 5599.8464 | 8244.6336 | 11936.8192 | 17096.8064 | 24641.5360 | 0.0521 | 0.1367 | 0.0917 | 0.0582 | 0.0099 | 0.0013 |
| 345.0 | 0.0 | 3734.9376 | 7469.8752 | 11199.6928 | 16489.2672 | 23873.6384 | 34193.6128 | 49283.0720 | 0.0521 | 0.1367 | 0.0917 | 0.0582 | 0.0099 | 0.0013 |
| 360.0 | 0.0 | 7469.8752 | 14939.7504 | 22399.3856 | 32978.5344 | 47747.2768 | 68387.2256 | 100566.1440 | 0.0521 | 0.1367 | 0.0917 | 0.0582 | 0.0099 | 0.0013 |

Flight Condition 22

UP VALUES FROM ROOT TO TIP AT ALL AZIMUTH STATIONS

| X/R | 0.240 | 0.301 | 0.362 | 0.423 | 0.483 | 0.544 | 0.605 | 0.666 | 0.727 | 0.787 | 0.848 | 0.909 | 0.970 |
|-------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
| PSI | | | | | | | | | | | | | |
| 0.0 | -0.00943 | -0.03926 | -0.03132 | -0.02550 | -0.02132 | -0.01823 | -0.01595 | -0.01413 | -0.01256 | -0.01114 | -0.00982 | -0.00866 | -0.00769 |
| 15.0 | -0.01674 | -0.02970 | -0.02413 | -0.01982 | -0.01597 | -0.01287 | -0.01024 | -0.00796 | -0.00598 | -0.00431 | -0.00295 | -0.00195 | -0.00138 |
| 30.0 | -0.01895 | -0.01568 | -0.01239 | -0.00937 | -0.00730 | -0.00608 | -0.00552 | -0.00510 | -0.00516 | -0.00497 | -0.00470 | -0.00437 | -0.00398 |
| 45.0 | -0.00839 | -0.00645 | -0.00564 | -0.00589 | -0.00641 | -0.00665 | -0.00667 | -0.00596 | -0.00527 | -0.00453 | -0.00376 | -0.00303 | -0.00237 |
| 60.0 | -0.00153 | -0.00144 | -0.00214 | -0.00451 | -0.00536 | -0.00550 | -0.00514 | -0.00452 | -0.00374 | -0.00294 | -0.00217 | -0.00151 | -0.00097 |
| 75.0 | 0.00322 | 0.00224 | 0.00024 | -0.00125 | -0.00200 | -0.00225 | -0.00220 | -0.00195 | -0.00157 | -0.00115 | -0.00073 | -0.00038 | -0.00012 |
| 90.0 | 0.00688 | 0.00579 | 0.00412 | 0.00301 | 0.00242 | 0.00211 | 0.00188 | 0.00167 | 0.00144 | 0.00121 | 0.00101 | 0.00085 | 0.00073 |
| 105.0 | 0.01021 | 0.00944 | 0.00795 | 0.00663 | 0.00561 | 0.00475 | 0.00401 | 0.00334 | 0.00274 | 0.00222 | 0.00179 | 0.00144 | 0.00118 |
| 120.0 | 0.01435 | 0.01475 | 0.01341 | 0.01107 | 0.00870 | 0.00671 | 0.00519 | 0.00405 | 0.00319 | 0.00255 | 0.00205 | 0.00167 | 0.00137 |
| 135.0 | 0.01975 | 0.02212 | 0.02136 | 0.01765 | 0.01335 | 0.00970 | 0.00724 | 0.00547 | 0.00421 | 0.00331 | 0.00263 | 0.00211 | 0.00172 |
| 150.0 | 0.02711 | 0.02900 | 0.02719 | 0.02296 | 0.01842 | 0.01444 | 0.01123 | 0.00871 | 0.00673 | 0.00522 | 0.00406 | 0.00317 | 0.00250 |
| 165.0 | 0.04621 | 0.04564 | 0.03864 | 0.03346 | 0.03074 | 0.02748 | 0.02287 | 0.01797 | 0.01359 | 0.01011 | 0.00741 | 0.00544 | 0.00403 |
| 180.0 | 0.05985 | 0.05424 | 0.05385 | 0.04669 | 0.04501 | 0.04197 | 0.03532 | 0.02757 | 0.02048 | 0.01477 | 0.01040 | 0.00730 | 0.00519 |
| 195.0 | 0.04532 | 0.04447 | 0.03787 | 0.03282 | 0.02987 | 0.02647 | 0.02199 | 0.01732 | 0.01317 | 0.00986 | 0.00728 | 0.00539 | 0.00402 |
| 210.0 | 0.02736 | 0.02836 | 0.02614 | 0.02207 | 0.01785 | 0.01411 | 0.01107 | 0.00863 | 0.00671 | 0.00524 | 0.00409 | 0.00322 | 0.00255 |
| 225.0 | 0.01971 | 0.02103 | 0.01970 | 0.01627 | 0.01252 | 0.00940 | 0.00722 | 0.00542 | 0.00422 | 0.00334 | 0.00267 | 0.00216 | 0.00176 |
| 240.0 | 0.01413 | 0.01406 | 0.01257 | 0.01036 | 0.00821 | 0.00639 | 0.00499 | 0.00392 | 0.00312 | 0.00251 | 0.00203 | 0.00166 | 0.00137 |
| 255.0 | 0.00978 | 0.00892 | 0.00750 | 0.00622 | 0.00519 | 0.00433 | 0.00362 | 0.00300 | 0.00246 | 0.00202 | 0.00164 | 0.00134 | 0.00111 |
| 270.0 | 0.00619 | 0.00515 | 0.00374 | 0.00273 | 0.00216 | 0.00180 | 0.00155 | 0.00134 | 0.00115 | 0.00098 | 0.00084 | 0.00073 | 0.00064 |
| 285.0 | 0.00241 | 0.00156 | 0.00003 | -0.00111 | -0.00115 | -0.00186 | -0.00179 | -0.00156 | -0.00125 | -0.00093 | -0.00061 | -0.00035 | -0.00014 |
| 300.0 | -0.00224 | -0.00214 | -0.00317 | -0.00421 | -0.00474 | -0.00496 | -0.00461 | -0.00386 | -0.00321 | -0.00256 | -0.00194 | -0.00141 | -0.00097 |
| 315.0 | -0.00872 | -0.00694 | -0.00411 | -0.00294 | -0.00216 | -0.00142 | -0.00082 | -0.00031 | -0.00048 | -0.00043 | -0.00037 | -0.00026 | -0.00020 |
| 330.0 | -0.01878 | -0.01543 | -0.01222 | -0.00956 | -0.00766 | -0.00643 | -0.00570 | -0.00525 | -0.00491 | -0.00460 | -0.00426 | -0.00391 | -0.00356 |
| 345.0 | -0.03562 | -0.02875 | -0.02330 | -0.01891 | -0.01539 | -0.01244 | -0.00998 | -0.00789 | -0.00610 | -0.00463 | -0.00343 | -0.00256 | -0.00204 |

Flight Condition 23

UP VALUES FROM ROOT TO TIP AT ALL AZIMUTH STATIONS

| PSI | X/R | 0.240 | 0.301 | 0.362 | 0.423 | 0.483 | 0.544 | 0.605 | 0.666 | 0.727 | 0.787 | 0.848 | 0.909 | 0.970 |
|-------|-----|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
| 0.0 | | -0.05239 | -0.03373 | -0.02598 | -0.01959 | -0.01510 | -0.01193 | -0.00999 | -0.00787 | -0.00652 | -0.00539 | -0.00448 | -0.00374 | -0.00296 |
| 15.0 | | -0.03185 | -0.02088 | -0.01493 | -0.01051 | -0.00752 | -0.00502 | -0.00372 | -0.00297 | -0.00254 | -0.00219 | -0.00194 | -0.00177 | -0.00164 |
| 30.0 | | -0.01635 | -0.01138 | -0.00742 | -0.00513 | -0.00351 | -0.00233 | -0.00160 | -0.00118 | -0.00094 | -0.00079 | -0.00069 | -0.00062 | -0.00056 |
| 45.0 | | -0.00923 | -0.00578 | -0.00378 | -0.00257 | -0.00173 | -0.00114 | -0.00074 | -0.00055 | -0.00043 | -0.00036 | -0.00031 | -0.00028 | -0.00025 |
| 60.0 | | -0.00516 | -0.00329 | -0.00209 | -0.00146 | -0.00093 | -0.00057 | -0.00037 | -0.00026 | -0.00019 | -0.00014 | -0.00010 | -0.00008 | -0.00006 |
| 75.0 | | -0.00264 | -0.00169 | -0.00116 | -0.00072 | -0.00045 | -0.00027 | -0.00017 | -0.00011 | -0.00007 | -0.00005 | -0.00003 | -0.00002 | -0.00001 |
| 90.0 | | -0.00148 | -0.00093 | -0.00055 | -0.00034 | -0.00022 | -0.00014 | -0.00009 | -0.00006 | -0.00004 | -0.00003 | -0.00002 | -0.00001 | -0.00000 |
| 105.0 | | -0.00094 | -0.00057 | -0.00035 | -0.00022 | -0.00014 | -0.00009 | -0.00006 | -0.00004 | -0.00003 | -0.00002 | -0.00001 | -0.00000 | -0.00000 |
| 120.0 | | -0.00068 | -0.00042 | -0.00026 | -0.00017 | -0.00011 | -0.00007 | -0.00005 | -0.00003 | -0.00002 | -0.00001 | -0.00000 | -0.00000 | -0.00000 |
| 135.0 | | -0.00048 | -0.00031 | -0.00019 | -0.00012 | -0.00008 | -0.00005 | -0.00003 | -0.00002 | -0.00001 | -0.00000 | -0.00000 | -0.00000 | -0.00000 |
| 150.0 | | -0.00032 | -0.00021 | -0.00013 | -0.00008 | -0.00005 | -0.00003 | -0.00002 | -0.00001 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 |
| 165.0 | | -0.00020 | -0.00013 | -0.00008 | -0.00005 | -0.00003 | -0.00002 | -0.00001 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 |
| 180.0 | | -0.00012 | -0.00007 | -0.00004 | -0.00002 | -0.00001 | -0.00001 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 |
| 195.0 | | -0.00007 | -0.00004 | -0.00002 | -0.00001 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 |
| 210.0 | | -0.00004 | -0.00002 | -0.00001 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 |
| 225.0 | | -0.00002 | -0.00001 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 |
| 240.0 | | -0.00001 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 |
| 255.0 | | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 |
| 270.0 | | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 |
| 285.0 | | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 |
| 300.0 | | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 |
| 315.0 | | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 |
| 330.0 | | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 |
| 345.0 | | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 | -0.00000 |

UP VALUES FROM ROOT TO TIP AT ALL AZIMUTH STATIONS

Flight Condition 24

UP VALUES FROM ROOT TO TIP AT ALL AZIMUTH STATIONS

| X/R | 0.248 | 0.301 | 0.352 | 0.423 | 0.483 | 0.544 | 0.605 | 0.666 | 0.727 | 0.787 | 0.848 | 0.909 | 0.970 |
|-------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| PSI | 0.0436 | 0.0452 | 0.0289 | 0.0289 | 0.02127 | 0.01860 | 0.01667 | 0.01515 | 0.01385 | 0.01266 | 0.01155 | 0.01055 | 0.00971 |
| 15.0 | 0.0450 | 0.02932 | 0.02932 | 0.02936 | 0.01983 | 0.01749 | 0.01588 | 0.01433 | 0.01332 | 0.01224 | 0.01126 | 0.01038 | 0.00962 |
| 30.0 | 0.02173 | 0.02954 | 0.01919 | 0.01777 | 0.01637 | 0.01499 | 0.01367 | 0.01242 | 0.01126 | 0.01019 | 0.00917 | 0.00827 | 0.00733 |
| 45.0 | 0.02517 | 0.03227 | 0.01903 | 0.01845 | 0.01369 | 0.01253 | 0.01133 | 0.01035 | 0.00933 | 0.00842 | 0.00742 | 0.00647 | 0.00571 |
| 60.0 | 0.02517 | 0.03227 | 0.01903 | 0.01845 | 0.01369 | 0.01253 | 0.01133 | 0.01035 | 0.00933 | 0.00842 | 0.00742 | 0.00647 | 0.00571 |
| 75.0 | 0.02102 | 0.02624 | 0.00933 | 0.00928 | 0.00604 | 0.00562 | 0.00493 | 0.00378 | 0.00268 | 0.00177 | 0.00079 | 0.00049 | 0.00049 |
| 90.0 | 0.02102 | 0.0167 | 0.00933 | 0.00928 | 0.00604 | 0.00562 | 0.00493 | 0.00378 | 0.00268 | 0.00177 | 0.00079 | 0.00049 | 0.00049 |
| 105.0 | 0.02148 | 0.0193 | 0.00935 | 0.00927 | 0.0054 | 0.0051 | 0.0043 | 0.00299 | 0.00198 | 0.00121 | 0.00058 | 0.00014 | 0.00117 |
| 120.0 | 0.0235 | 0.0450 | 0.00935 | 0.00940 | 0.0045 | 0.00484 | 0.0046 | 0.00299 | 0.00271 | 0.00238 | 0.00208 | 0.0014 | 0.00168 |
| 135.0 | 0.0235 | 0.0376 | 0.00937 | 0.00921 | 0.00558 | 0.00594 | 0.0051 | 0.00371 | 0.00319 | 0.00273 | 0.00236 | 0.00172 | 0.00168 |
| 150.0 | 0.03225 | 0.03687 | 0.00937 | 0.00908 | 0.00558 | 0.00594 | 0.0051 | 0.00371 | 0.00319 | 0.00273 | 0.00236 | 0.00172 | 0.00168 |
| 165.0 | 0.03225 | 0.03687 | 0.00937 | 0.00908 | 0.00558 | 0.00594 | 0.0051 | 0.00371 | 0.00319 | 0.00273 | 0.00236 | 0.00172 | 0.00168 |
| 180.0 | 0.03226 | 0.03687 | 0.00937 | 0.00908 | 0.00558 | 0.00594 | 0.0051 | 0.00371 | 0.00319 | 0.00273 | 0.00236 | 0.00172 | 0.00168 |
| 195.0 | 0.03226 | 0.03687 | 0.00937 | 0.00908 | 0.00558 | 0.00594 | 0.0051 | 0.00371 | 0.00319 | 0.00273 | 0.00236 | 0.00172 | 0.00168 |
| 210.0 | 0.03226 | 0.03687 | 0.00937 | 0.00908 | 0.00558 | 0.00594 | 0.0051 | 0.00371 | 0.00319 | 0.00273 | 0.00236 | 0.00172 | 0.00168 |
| 225.0 | 0.03226 | 0.03687 | 0.00937 | 0.00908 | 0.00558 | 0.00594 | 0.0051 | 0.00371 | 0.00319 | 0.00273 | 0.00236 | 0.00172 | 0.00168 |
| 240.0 | 0.03226 | 0.03687 | 0.00937 | 0.00908 | 0.00558 | 0.00594 | 0.0051 | 0.00371 | 0.00319 | 0.00273 | 0.00236 | 0.00172 | 0.00168 |
| 255.0 | 0.03226 | 0.03687 | 0.00937 | 0.00908 | 0.00558 | 0.00594 | 0.0051 | 0.00371 | 0.00319 | 0.00273 | 0.00236 | 0.00172 | 0.00168 |
| 270.0 | 0.03226 | 0.03687 | 0.00937 | 0.00908 | 0.00558 | 0.00594 | 0.0051 | 0.00371 | 0.00319 | 0.00273 | 0.00236 | 0.00172 | 0.00168 |
| 285.0 | 0.03226 | 0.03687 | 0.00937 | 0.00908 | 0.00558 | 0.00594 | 0.0051 | 0.00371 | 0.00319 | 0.00273 | 0.00236 | 0.00172 | 0.00168 |
| 300.0 | 0.03226 | 0.03687 | 0.00937 | 0.00908 | 0.00558 | 0.00594 | 0.0051 | 0.00371 | 0.00319 | 0.00273 | 0.00236 | 0.00172 | 0.00168 |
| 315.0 | 0.03226 | 0.03687 | 0.00937 | 0.00908 | 0.00558 | 0.00594 | 0.0051 | 0.00371 | 0.00319 | 0.00273 | 0.00236 | 0.00172 | 0.00168 |
| 330.0 | 0.03226 | 0.03687 | 0.00937 | 0.00908 | 0.00558 | 0.00594 | 0.0051 | 0.00371 | 0.00319 | 0.00273 | 0.00236 | 0.00172 | 0.00168 |
| 345.0 | 0.03226 | 0.03687 | 0.00937 | 0.00908 | 0.00558 | 0.00594 | 0.0051 | 0.00371 | 0.00319 | 0.00273 | 0.00236 | 0.00172 | 0.00168 |
| 360.0 | 0.03226 | 0.03687 | 0.00937 | 0.00908 | 0.00558 | 0.00594 | 0.0051 | 0.00371 | 0.00319 | 0.00273 | 0.00236 | 0.00172 | 0.00168 |

Flight Condition 26

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UP VALUES FROM ROOT TO TIP AT ALL AZIMUTH STATIONS

| X/R | 0.240 | 0.301 | 0.362 | 0.423 | 0.483 | 0.544 | 0.605 | 0.666 | 0.727 | 0.787 | 0.848 | 0.909 | 0.970 |
|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| PSI | 0.8947 | 0.8741 | 0.8282 | 0.7259 | 0.6178 | 0.5136 | 0.4180 | 0.3199 | 0.2679 | 0.2718 | 0.2628 | 0.2504 | 0.2407 |
| 8.0 | 0.8365 | 0.8205 | 0.8149 | 0.8121 | 0.8108 | 0.8102 | 0.8097 | 0.8093 | 0.8091 | 0.8091 | 0.8091 | 0.8091 | 0.8091 |
| 10.0 | 0.8141 | 0.8016 | 0.8083 | 0.8099 | 0.8105 | 0.8111 | 0.8116 | 0.8121 | 0.8126 | 0.8131 | 0.8136 | 0.8141 | 0.8146 |
| 15.0 | 0.8070 | 0.8047 | 0.8020 | 0.8000 | 0.8000 | 0.8000 | 0.8000 | 0.8000 | 0.8000 | 0.8000 | 0.8000 | 0.8000 | 0.8000 |
| 20.0 | 0.8077 | 0.8074 | 0.8079 | 0.8082 | 0.8085 | 0.8087 | 0.8089 | 0.8091 | 0.8093 | 0.8095 | 0.8097 | 0.8099 | 0.8101 |
| 25.0 | 0.8034 | 0.8023 | 0.8017 | 0.8010 | 0.8007 | 0.8005 | 0.8003 | 0.8002 | 0.8001 | 0.8000 | 0.8000 | 0.8000 | 0.8000 |
| 30.0 | 0.8033 | 0.8048 | 0.8065 | 0.8081 | 0.8094 | 0.8103 | 0.8110 | 0.8116 | 0.8121 | 0.8126 | 0.8131 | 0.8136 | 0.8141 |
| 35.0 | 0.8046 | 0.8069 | 0.8099 | 0.8135 | 0.8171 | 0.8207 | 0.8242 | 0.8277 | 0.8311 | 0.8345 | 0.8378 | 0.8411 | 0.8444 |
| 40.0 | 0.8129 | 0.8154 | 0.8182 | 0.8212 | 0.8242 | 0.8271 | 0.8300 | 0.8328 | 0.8355 | 0.8381 | 0.8407 | 0.8432 | 0.8457 |
| 45.0 | 0.8199 | 0.8221 | 0.8247 | 0.8274 | 0.8301 | 0.8327 | 0.8353 | 0.8378 | 0.8403 | 0.8427 | 0.8451 | 0.8474 | 0.8497 |
| 50.0 | 0.8270 | 0.8289 | 0.8309 | 0.8328 | 0.8346 | 0.8363 | 0.8380 | 0.8396 | 0.8411 | 0.8425 | 0.8439 | 0.8452 | 0.8465 |
| 55.0 | 0.8348 | 0.8364 | 0.8379 | 0.8393 | 0.8406 | 0.8418 | 0.8429 | 0.8439 | 0.8448 | 0.8456 | 0.8463 | 0.8470 | 0.8476 |
| 60.0 | 0.8424 | 0.8438 | 0.8451 | 0.8462 | 0.8471 | 0.8478 | 0.8484 | 0.8489 | 0.8493 | 0.8496 | 0.8498 | 0.8500 | 0.8501 |
| 65.0 | 0.8498 | 0.8511 | 0.8523 | 0.8533 | 0.8542 | 0.8549 | 0.8555 | 0.8560 | 0.8564 | 0.8567 | 0.8570 | 0.8572 | 0.8574 |
| 70.0 | 0.8570 | 0.8581 | 0.8591 | 0.8599 | 0.8606 | 0.8612 | 0.8617 | 0.8621 | 0.8624 | 0.8627 | 0.8629 | 0.8631 | 0.8632 |
| 75.0 | 0.8660 | 0.8670 | 0.8679 | 0.8687 | 0.8694 | 0.8700 | 0.8705 | 0.8709 | 0.8712 | 0.8715 | 0.8717 | 0.8719 | 0.8720 |
| 80.0 | 0.8670 | 0.8680 | 0.8689 | 0.8696 | 0.8702 | 0.8707 | 0.8711 | 0.8714 | 0.8717 | 0.8719 | 0.8721 | 0.8722 | 0.8723 |
| 85.0 | 0.8670 | 0.8680 | 0.8689 | 0.8696 | 0.8702 | 0.8707 | 0.8711 | 0.8714 | 0.8717 | 0.8719 | 0.8721 | 0.8722 | 0.8723 |
| 90.0 | 0.8670 | 0.8680 | 0.8689 | 0.8696 | 0.8702 | 0.8707 | 0.8711 | 0.8714 | 0.8717 | 0.8719 | 0.8721 | 0.8722 | 0.8723 |
| 95.0 | 0.8670 | 0.8680 | 0.8689 | 0.8696 | 0.8702 | 0.8707 | 0.8711 | 0.8714 | 0.8717 | 0.8719 | 0.8721 | 0.8722 | 0.8723 |
| 100.0 | 0.8670 | 0.8680 | 0.8689 | 0.8696 | 0.8702 | 0.8707 | 0.8711 | 0.8714 | 0.8717 | 0.8719 | 0.8721 | 0.8722 | 0.8723 |

Flight Condition 27

APPENDIX C

Supplementary Loads Analysis Comparisons

To supplement the loads analysis results shown in Figures 8-6 through 8-41, this appendix contains several additional comparisons in tabular form.

| | | |
|---|-------|-------|
| Flight Velocity - Knots | 112.5 | 162.5 |
| L/DE (without upwash) | 7.80 | 8.21 |
| L/DE (with upwash) | 7.91 | 8.53 |
| PLL Amplitude-lbs (without upwash) | 305 | 929 |
| PLL Amplitude-lbs (with upwash) | 435 | 1014 |
| Vertical Shear Amplitude-lbs (without upwash) | 1897 | 3476 |
| Vertical Shear Amplitude-lbs (with upwash) | 1410 | 4106 |
| FZF-lbs (without upwash) | 1182 | 1686 |
| FZF-lbs (with upwash) | 1219 | 1557 |
| Flight Condition | 3 | 4 |

Variation of Equivalent Lift-to-Drag Ratio, Flap Hinge Vertical Shear Vibratory Amplitude, Pitch Link Load Vibratory Amplitude, and Vertical Hub Force Fourth Harmonic Amplitude with Flight Velocity from Loads Analysis. Rotor Lift, Gross Weight, and Rotor Radius Are Held Constant.

| | | |
|---|-------|-------|
| Flight Velocity - Knots | 112.5 | 162.5 |
| L/DE (without upwash) | 7.45 | 7.29 |
| L/DE (with upwash) | 7.26 | 7.65 |
| PLL Amplitude-lbs (without upwash) | 407 | 735 |
| PLL Amplitude-lbs (with upwash) | 546 | 927 |
| Vertical Shear Amplitude-lbs (without upwash) | 5386 | 3306 |
| Vertical Shear Amplitude-lbs (with upwash) | 5220 | 4694 |
| FZF-lbs (without upwash) | 1733 | 2685 |
| FZF-lbs (with upwash) | 1594 | 2444 |
| Flight Condition | 9 | 10 |

Variation of Equivalent Lift-to-Drag Ratio, Flap Hinge Vertical Shear Vibratory Amplitude, Pitch Link Load Vibratory Amplitude, and Vertical Hub Force Fourth Harmonic Amplitude with Flight Velocity from Loads Analysis. Rotor Lift, Wing Lift, Gross Weight, Flat Plate Area for Auxiliary Thrust, and Rotor Radius Are Held Constant.

| | | |
|---|-------|-------|
| Flight Velocity - Knots | 112.5 | 162.5 |
| L/DE (without upwash) | 6.96 | 8.94 |
| L/DE (with upwash) | 7.10 | 9.06 |
| PLL Amplitude-lbs (without upwash) | 551 | 1019 |
| PLL Amplitude-lbs (with upwash) | 519 | 1044 |
| Vertical Shear Amplitude-lbs (without upwash) | 1102 | 2270 |
| Vertical Shear Amplitude-lbs (with upwash) | 1288 | 2815 |
| FZF-lbs (without upwash) | 682 | 1223 |
| FZF-lbs (with upwash) | 706 | 1005 |
| Flight Condition | 11 | 12 |

Variation of Equivalent Lift-to-Drag Ratio, Flap Hinge Vertical Shear Vibratory Amplitude, Pitch Link Load Vibratory Amplitude, and Vertical Hub Force Fourth Harmonic Amplitude with Flight Velocity from Loads Analysis. Rotor Lift, Gross Weight, and Rotor Radius Are Held Constant.

| | | |
|---|-------|-------|
| Flight Velocity - Knots | 112.5 | 162.5 |
| L/DE (without upwash) | 7.23 | 8.06 |
| L/DE (with upwash) | 7.66 | 8.99 |
| PLL Amplitude-lbs (without upwash) | 321 | 825 |
| PLL Amplitude-lbs (with upwash) | 485 | 1154 |
| Vertical Shear Amplitude-lbs (without upwash) | 1449 | 2598 |
| Vertical Shear Amplitude-lbs (with upwash) | 1912 | 3449 |
| FZF-lbs (without upwash) | 754 | 1446 |
| FZF-lbs (with upwash) | 682 | 1503 |
| Flight Condition | 13 | 14 |

Variation of Equivalent Lift-to-Drag Ratio, Flap Hinge Vertical Shear Vibratory Amplitude, Pitch Link Load Vibratory Amplitude, and Vertical Hub Force Fourth Harmonic Amplitude with Flight Velocity from Loads Analysis. Rotor Lift, Gross Weight, Flat Plate Area for Auxiliary Thrust, and Rotor Radius Are Held Constant.

| | | |
|---|-------|-------|
| Flight Velocity - Knots | 112.5 | 162.5 |
| L/DE (without upwash) | 7.09 | 8.93 |
| L/DE (with upwash) | 6.63 | 8.72 |
| PLL Amplitude-lbs (without upwash) | 483 | 1025 |
| PLL Amplitude-lbs (with upwash) | 532 | 1052 |
| Vertical Shear Amplitude-lbs (without upwash) | 897 | 2556 |
| Vertical Shear Amplitude-lbs (with upwash) | 1431 | 3436 |
| FZF-lbs (without upwash) | 720 | 1362 |
| FZF-lbs (with upwash) | 795 | 1194 |
| Flight Condition | 15 | 16 |

Variation of Equivalent Lift-to-Drag Ratio, Flap Hinge Vertical Shear Vibratory Amplitude, Pitch Link Load Vibratory Amplitude, and Vertical Hub Force Fourth Harmonic Amplitude with Flight Velocity from Loads Analysis. Rotor Lift, Wing Lift, Gross Weight, and Rotor Radius Are Held Constant.

| | | |
|---|-------|-------|
| Flight Velocity - Knots | 112.5 | 162.5 |
| L/DE (without upwash) | 7.27 | 8.04 |
| L/DE (with upwash) | 7.18 | 8.57 |
| PLL Amplitude-lbs (without upwash) | 261 | 869 |
| PLL Amplitude-lbs (with upwash) | 429 | 905 |
| Vertical Shear Amplitude-lbs (without upwash) | 3124 | 3234 |
| Vertical Shear Amplitude-lbs (with upwash) | 3138 | 4630 |
| FZF-lbs (without upwash) | 765 | 1559 |
| FZF-lbs (with upwash) | 655 | 1521 |
| Flight Condition | 17 | 18 |

Variation of Equivalent Lift-to-Drag Ratio, Flap Hinge Vertical Shear Vibratory Amplitude, Pitch Link Load Vibratory Amplitude, and Vertical Hub Force Fourth Harmonic Amplitude with Flight Velocity from Loads Analysis. Rotor Lift, Wing Lift, Gross Weight, Flat Plate Area for Auxiliary Thrust, and Rotor Radius Are Held Constant.

| | | |
|---|------|------|
| $T \cos \alpha_g / \pi R^2 - \text{psf}$ | 6.48 | 9.34 |
| L/DE (without upwash) | 7.80 | 7.21 |
| L/DE (with upwash) | 7.91 | 7.38 |
| PLL Amplitude-lbs (without upwash) | 305 | 756 |
| PLL Amplitude-lbs (with upwash) | 435 | 776 |
| Vertical Shear Amplitude-lbs (without upwash) | 1897 | 2270 |
| Vertical Shear Amplitude-lbs (with upwash) | 1410 | 2360 |
| FZF-lbs (without upwash) | 1182 | 1253 |
| FZF-lbs (with upwash) | 1219 | 1344 |
| Flight Condition | 3 | 1 |

Variation of Equivalent Lift-to-Drag Ratio, Flap Hinge Vertical Shear Vibratory Amplitude, Pitch Link Load Vibratory Amplitude, and Vertical Hub Force Fourth Harmonic Amplitude with Vertical Component of Disk Loading from Loads Analysis. Flight Velocity and Rotor Radius Are Held Constant.

| | | |
|---|------|--------|
| Lift-lbs | 0 | 8066.7 |
| L/DE (without upwash) | 7.80 | 7.83 |
| L/DE (with upwash) | 7.91 | 7.30 |
| PLL Amplitude-lbs (without upwash) | 305 | 293 |
| PLL Amplitude-lbs (with upwash) | 435 | 493 |
| Vertical Shear Amplitude-lbs (without upwash) | 1897 | 2336 |
| Vertical Shear Amplitude-lbs (with upwash) | 1410 | 1820 |
| FZF-lbs (without upwash) | 1182 | 1173 |
| FZF-lbs (with upwash) | 1219 | 1386 |
| Flight Condition | 3 | 5 |

Variation of Equivalent Lift-to-Drag Ratio, Flap Hinge Vertical Shear Vibratory Amplitude, Pitch Link Load Vibratory Amplitude, and Vertical Hub Force Fourth Harmonic Amplitude with Wing Lift from Loads Analysis. Rotor Lift, Flight Velocity, and Rotor Radius Are Held Constant.

| | | |
|---|------|--------|
| Lift-lbs | 0 | 8066.7 |
| L/DE (without upwash) | 6.96 | 7.09 |
| L/DE (with upwash) | 7.10 | 6.63 |
| PLL Amplitude-lbs (without upwash) | 551 | 483 |
| PLL Amplitude-lbs (with upwash) | 519 | 532 |
| Vertical Shear Amplitude-lbs (without upwash) | 1102 | 897 |
| Vertical Shear Amplitude-lbs (with upwash) | 1288 | 1431 |
| FZF-lbs (without upwash) | 682 | 720 |
| FZF-lbs (with upwash) | 706 | 795 |
| Flight Condition | 11 | 15 |

Variation of Equivalent Lift-to-Drag Ratio, Flap Hinge Vertical Shear Vibratory Amplitude, Pitch Link Load Vibratory Amplitude, and Vertical Hub Force Fourth Harmonic Amplitude with Wing Lift from Loads Analysis. Rotor Lift, Flight Velocity, and Rotor Radius Are Held Constant.

| | | |
|---|------|--------|
| Lift-lbs | 0 | 8066.7 |
| L/DE (without upwash) | 8.94 | 8.93 |
| L/DE (with upwash) | 9.06 | 8.72 |
| PLL Amplitude-lbs (without upwash) | 1019 | 1025 |
| PLL Amplitude-lbs (with upwash) | 1044 | 1052 |
| Vertical Shear Amplitude-lbs (without upwash) | 2270 | 2556 |
| Vertical Shear Amplitude-lbs (with upwash) | 2815 | 3436 |
| FZF-lbs (without upwash) | 1223 | 1362 |
| FZF-lbs (with upwash) | 1005 | 1194 |
| Flight Condition | 12 | 16 |

Variation of Equivalent Lift-to-Drag Ratio, Flap Hinge Vertical Shear Vibratory Amplitude, Pitch Link Load Vibratory Amplitude, and Vertical Hub Force Fourth Harmonic Amplitude with Wing Lift from Loads Analysis. Rotor Lift, Flight Velocity, and Rotor Radius Are Held Constant.

| | | |
|---|------|--------|
| Lift-lbs | 0 | 8066.7 |
| L/DE (without upwash) | 7.44 | 7.45 |
| L/DE (with upwash) | 7.85 | 7.26 |
| PLL Amplitude-lbs (without upwash) | 419 | 407 |
| PLL Amplitude-lbs (with upwash) | 460 | 546 |
| Vertical Shear Amplitude-lbs (without upwash) | 2905 | 5386 |
| Vertical Shear Amplitude-lbs (with upwash) | 2877 | 5220 |
| FZF-lbs (without upwash) | 1629 | 1733 |
| FZF-lbs (with upwash) | 1561 | 1594 |
| Flight Condition | 7 | 9 |

Variation of Equivalent Lift-to-Drag Ratio, Flap Hinge Vertical Shear Vibratory Amplitude, Pitch Link Load Vibratory Amplitude, and Vertical Hub Force Fourth Harmonic Amplitude with Wing Lift from Loads Analysis. Rotor Lift, Flight Velocity, Flat Plate Area for Auxiliary Thrust, and Rotor Radius Are Held Constant.

| | | | |
|---|------|--------|--------|
| Lift-lbs | 0 | 4033.3 | 8066.7 |
| L/DE (without upwash) | 7.40 | 7.34 | 7.29 |
| L/DE (with upwash) | 8.14 | 7.80 | 7.65 |
| PLL Amplitude-lbs (without upwash) | 734 | 688 | 735 |
| PLL Amplitude-lbs (with upwash) | 916 | 882 | 927 |
| Vertical Shear Amplitude-lbs (without upwash) | 3766 | 3873 | 3306 |
| Vertical Shear Amplitude-lbs (with upwash) | 4359 | 4830 | 4694 |
| FZF-lbs (without upwash) | 2736 | 2693 | 2685 |
| FZF-lbs (with upwash) | 2507 | 2402 | 2444 |
| Flight Condition | 8 | 21 | 10 |

Variation of Equivalent Lift-to-Drag Ratio, Flap Hinge Vertical Shear Vibratory Amplitude, Pitch Link Load Vibratory Amplitude, and Vertical Hub Force Fourth Harmonic Amplitude with Wing Lift from Loads Analysis. Rotor Lift, Flight Velocity, Flat Plate Area for Auxiliary Thrust, and Rotor Radius Are Held Constant.

| | | |
|---|------|--------|
| Lift-lbs | 0 | 8066.7 |
| L/DE (without upwash) | 7.23 | 7.27 |
| L/DE (with upwash) | 7.66 | 7.18 |
| PLL Amplitude-lbs (without upwash) | 321 | 261 |
| PLL Amplitude-lbs (with upwash) | 485 | 429 |
| Vertical Shear Amplitude-lbs (without upwash) | 1449 | 3124 |
| Vertical Shear Amplitude-lbs (with upwash) | 1912 | 3138 |
| FZF-lbs (without upwash) | 754 | 765 |
| FZF-lbs (with upwash) | 682 | 655 |
| Flight Condition | 13 | 17 |

Variation of Equivalent Lift-to-Drag Ratio, Flap Hinge Vertical Shear Vibratory Amplitude, Pitch Link Load Vibratory Amplitude, and Vertical Hub Force Fourth Harmonic Amplitude with Wing Lift from Loads Analysis. Rotor Lift, Flight Velocity, Flat Plate Area for Auxiliary Thrust, and Rotor Radius Are Held Constant.

| | | |
|---|------|--------|
| Lift-lbs | 0 | 8066.7 |
| L/DE (without upwash) | 8.06 | 8.04 |
| L/DE (with upwash) | 8.99 | 8.57 |
| PLL Amplitude-lbs (without upwash) | 825 | 869 |
| PLL Amplitude-lbs (with upwash) | 1154 | 905 |
| Vertical Shear Amplitude-lbs (without upwash) | 2598 | 3234 |
| Vertical Shear Amplitude-lbs (with upwash) | 3449 | 4630 |
| FZF-lbs (without upwash) | 1446 | 1559 |
| FZF-lbs (with upwash) | 1503 | 1521 |
| Flight Condition | 14 | 18 |

Variation of Equivalent Lift-to-Drag Ratio, Flap Hinge Vertical Shear Vibratory Amplitude, Pitch Link Load Vibratory Amplitude, and Vertical Hub Force Fourth Harmonic Amplitude with Wing Lift from Loads Analysis. Rotor Lift, Flight Velocity, Flat Plate Area for Auxiliary Thrust, and Rotor Radius Are Held Constant.

| | | |
|---|------|------|
| fe-sq ft | 0 | 22.9 |
| L/DE (without upwash) | 7.80 | 7.44 |
| L/DE (with upwash) | 7.91 | 7.85 |
| PLL Amplitude-lbs (without upwash) | 305 | 419 |
| PLL Amplitude-lbs (with upwash) | 435 | 460 |
| Vertical Shear Amplitude-lbs (without upwash) | 1897 | 2905 |
| Vertical Shear Amplitude-lbs (with upwash) | 1410 | 2877 |
| FZF-lbs (without upwash) | 1182 | 1629 |
| FZF-lbs (with upwash) | 1219 | 1561 |
| Flight Condition | 3 | 7 |

Variation of Equivalent Lift-to-Drag Ratio, Flap Hinge Vertical Shear Vibratory Amplitude, Pitch Link Load Vibratory Amplitude, and Vertical Hub Force Fourth Harmonic Amplitude with Flat Plate Area for Auxiliary Thrust from Loads Analysis. Rotor Radius, Rotor Lift, Gross Weight, and Flight Velocity Are Held Constant.

| | | |
|---|------|------|
| fe-sq ft | 0 | 22.9 |
| L/DE (without upwash) | 6.96 | 7.23 |
| L/DE (with upwash) | 7.10 | 7.66 |
| PLL Amplitude-lbs (without upwash) | 551 | 321 |
| PLL Amplitude-lbs (with upwash) | 519 | 485 |
| Vertical Shear Amplitude-lbs (without upwash) | 1102 | 1449 |
| Vertical Shear Amplitude-lbs (with upwash) | 1288 | 1912 |
| FZF-lbs (without upwash) | 682 | 754 |
| FZF-lbs (with upwash) | 706 | 682 |
| Flight Condition | 11 | 13 |

Variation of Equivalent Lift-to-Drag Ratio, Flap Hinge Vertical Shear Vibratory Amplitude, Pitch Link Load Vibratory Amplitude, and Vertical Hub Force Fourth Harmonic Amplitude with Flat Plate Area for Auxiliary Thrust from Loads Analysis. Rotor Radius, Rotor Lift, Gross Weight, and Flight Velocity Are Held Constant.

| | | |
|---|------|------|
| fe-sq ft | 0 | 22.9 |
| L/DE (without upwash) | 8.94 | 8.06 |
| L/DE (with upwash) | 9.06 | 8.99 |
| PLL Amplitude-lbs (without upwash) | 1019 | 825 |
| PLL Amplitude-lbs (with upwash) | 1044 | 1154 |
| Vertical Shear Amplitude-lbs (without upwash) | 2270 | 2598 |
| Vertical Shear Amplitude-lbs (with upwash) | 2815 | 3449 |
| FZF-lbs (without upwash) | 1223 | 1446 |
| FZF-lbs (with upwash) | 1005 | 1503 |
| Flight Condition | 12 | 14 |

Variation of Equivalent Lift-to-Drag Ratio, Flap Hinge Vertical Shear Vibratory Amplitude, Pitch Link Load Vibratory Amplitude, and Vertical Hub Force Fourth Harmonic Amplitude with Flat Plate Area for Auxiliary Thrust from Loads Analysis. Rotor Lift, Gross Weight, Flight Velocity, and Rotor Radius Are Held Constant.

| | | |
|---|------|------|
| fe-sq ft | 0 | 22.9 |
| L/DE (without upwash) | 7.83 | 7.45 |
| L/DE (with upwash) | 7.30 | 7.26 |
| PLL Amplitude-lbs (without upwash) | 293 | 407 |
| PLL Amplitude-lbs (with upwash) | 493 | 546 |
| Vertical Shear Amplitude-lbs (without upwash) | 2336 | 5386 |
| Vertical Shear Amplitude-lbs (with upwash) | 1820 | 5220 |
| FZF-lbs (without upwash) | 1173 | 1733 |
| FZF-lbs (with upwash) | 1386 | 1594 |
| Flight Condition | 5 | 9 |

Variation of Equivalent Lift-to-Drag Ratio, Flap Hinge Vertical Shear Vibratory Amplitude, Pitch Link Load Vibratory Amplitude, and Vertical Hub Force Fourth Harmonic Amplitude with Flat Plate Area for Auxiliary Thrust from Loads Analysis. Rotor Lift, Gross Weight, Flight Velocity, Wing Lift, and Rotor Radius Are Held Constant.

| | | |
|---|------|------|
| fe-sq ft | 0 | 22.9 |
| L/DE (without upwash) | 7.09 | 7.27 |
| L/DE (with upwash) | 6.63 | 7.18 |
| PLL Amplitude-lbs (without upwash) | 483 | 261 |
| PLL Amplitude-lbs (with upwash) | 532 | 429 |
| Vertical Shear Amplitude-lbs (without upwash) | 897 | 3124 |
| Vertical Shear Amplitude-lbs (with upwash) | 1431 | 3138 |
| FZF-lbs (without upwash) | 720 | 765 |
| FZF-lbs (with upwash) | 795 | 655 |
| Flight Condition | 15 | 17 |

Variation of Equivalent Lift-to-Drag Ratio, Flap Hinge Vertical Shear Vibratory Amplitude, Pitch Link Load Vibratory Amplitude, and Vertical Hub Force Fourth Harmonic Amplitude with Flat Plate Area for Auxiliary Thrust from Loads Analysis. Rotor Lift, Gross Weight, Flight Velocity, Wing Lift, and Rotor Radius Are Held Constant.

| | | |
|---|------|------|
| fe-sq ft | 0 | 22.9 |
| L/DE (without upwash) | 8.93 | 8.04 |
| L/DE (with upwash) | 8.72 | 8.57 |
| PLL Amplitude-lbs (without upwash) | 1025 | 869 |
| PLL Amplitude-lbs (with upwash) | 1052 | 905 |
| Vertical Shear Amplitude-lbs (without upwash) | 2556 | 3234 |
| Vertical Shear Amplitude-lbs (with upwash) | 3436 | 4630 |
| FZF-lbs (without upwash) | 1362 | 1559 |
| FZF-lbs (with upwash) | 1194 | 1521 |
| Flight Condition | 16 | 18 |

Variation of Equivalent Lift-to-Drag Ratio, Flap Hinge Vertical Shear Vibratory Amplitude, Pitch Link Load Vibratory Amplitude, and Vertical Hub Force Fourth Harmonic Amplitude with Flat Plate Area for Auxiliary Thrust from Leads Analysis. Rotor Lift, Gross Weight, Flight Velocity, Wing Lift, and Rotor Radius Are Held Constant.

| | | |
|---|------|--------|
| fe-sq ft | 0 | 22.9 |
| Lift-lbs | 0 | 8066.7 |
| L/DE (without upwash) | 7.80 | 7.45 |
| L/DE (with upwash) | 7.91 | 7.26 |
| PLL Amplitude-lbs (without upwash) | 305 | 407 |
| PLL Amplitude-lbs (with upwash) | 435 | 546 |
| Vertical Shear Amplitude-lbs (without upwash) | 1897 | 5386 |
| Vertical Shear Amplitude-lbs (with upwash) | 1410 | 5220 |
| FZF-lbs (without upwash) | 1182 | 1733 |
| FZF-lbs (with upwash) | 1219 | 1594 |
| Flight Condition | 3 | 9 |

Variation of Equivalent Lift-to-Drag Ratio, Flap Hinge Vertical Shear Vibratory Amplitude, Pitch Link Load Vibratory Amplitude, and Vertical Hub Force Fourth Harmonic Amplitude with Flat Plate Area for Auxiliary Thrust and Wing Lift from Loads Analysis. Rotor Lift, Flight Velocity, and Rotor Radius Are Held Constant.

| | | |
|---|------|--------|
| fe-sq ft | 0 | 22.9 |
| Lift-lbs | 0 | 8066.7 |
| L/DE (without upwash) | 6.96 | 7.27 |
| L/DE (with upwash) | 7.10 | 7.18 |
| PLL Amplitude-lbs (without upwash) | 551 | 261 |
| PLL Amplitude-lbs (with upwash) | 519 | 429 |
| Vertical Shear Amplitude-lbs (without upwash) | 1102 | 3124 |
| Vertical Shear Amplitude-lbs (with upwash) | 1288 | 3138 |
| FZF-lbs (without upwash) | 682 | 765 |
| FZF-lbs (with upwash) | 706 | 655 |
| Flight Condition | 11 | 17 |

Variation of Equivalent Lift-to-Drag Ratio, Flap Hinge Vertical Shear Vibratory Amplitude, Pitch Link Load Vibratory Amplitude, and Vertical Hub Force Fourth Harmonic Amplitude with Flat Plate Area for Auxiliary Thrust from Loads Analysis. Rotor Lift, Flight Velocity, and Rotor Radius Are Held Constant.

| | | |
|---|------|--------|
| fe-sq ft | 0 | 22.9 |
| Lift-lbs | 0 | 8066.7 |
| L/DE (without upwash) | 8.94 | 8.04 |
| L/DE (with upwash) | 9.06 | 8.57 |
| PLL Amplitude-lbs (without upwash) | 1019 | 869 |
| PLL Amplitude-lbs (with upwash) | 1044 | 905 |
| Vertical Shear Amplitude-lbs (without upwash) | 2270 | 3234 |
| Vertical Shear Amplitude-lbs (with upwash) | 2815 | 4630 |
| FZF-lbs (without upwash) | 1223 | 1559 |
| FZF-lbs (with upwash) | 1005 | 1521 |
| Flight Condition | 12 | 18 |

Variation of Equivalent Lift-to-Drag Ratio, Flap Hinge Vertical Shear Vibratory Amplitude, Pitch Link Load Vibratory Amplitude, and Vertical Hub Force Fourth Harmonic Amplitude with Flat Plate Area for Auxiliary Thrust from Loads Analysis. Rotor Lift, Flight Velocity, and Rotor Radius Are Held Constant.

| | | |
|---|------|------|
| Rotor Radius-ft | 25 | 30 |
| L/DE (without upwash) | 6.96 | 7.21 |
| L/DE (with upwash) | 7.10 | 7.38 |
| PLL Amplitude-lbs (without upwash) | 551 | 756 |
| PLL Amplitude-lbs (with upwash) | 519 | 776 |
| Vertical Shear Amplitude-lbs (without upwash) | 1102 | 2270 |
| Vertical Shear Amplitude-lbs (with upwash) | 1288 | 2360 |
| FZF-lbs (without upwash) | 682 | 1253 |
| FZF-lbs (with upwash) | 706 | 1344 |
| Flight Condition | 11 | 1 |

Variation of Equivalent Lift-to-Drag Ratio, Flap Hinge Vertical Shear Vibratory Amplitude, Pitch Link Load Vibratory Amplitude, and Vertical Hub Force Fourth Harmonic Amplitude with Rotor Radius from Loads Analysis. Flight Velocity and Disk Loading Are Held Constant.

| | | |
|---|------|------|
| Rotor Radius-ft | 25 | 30 |
| L/DE (without upwash) | 6.96 | 7.80 |
| L/DE (with upwash) | 7.10 | 7.91 |
| PLL Amplitude-lbs (without upwash) | 551 | 305 |
| PLL Amplitude-lbs (with upwash) | 519 | 435 |
| Vertical Shear Amplitude-lbs (without upwash) | 1102 | 1897 |
| Vertical Shear Amplitude-lbs (with upwash) | 1288 | 1410 |
| FZF-lbs (without upwash) | 682 | 1182 |
| FZF-lbs (with upwash) | 706 | 1219 |
| Flight Condition | 11 | 3 |

Variation of Equivalent Lift-to-Drag Ratio, Flap Hinge Vertical Shear Vibratory Amplitude, Pitch Link Load Vibratory Amplitude, and Vertical Hub Force Fourth Harmonic Amplitude with Rotor Radius from Loads Analysis. Flight Velocity, Rotor Lift, and Gross Weight Are Held Constant.

| | | |
|---|------|------|
| Rotor Radius-ft | 25 | 30 |
| L/DE (without upwash) | 8.94 | 8.21 |
| L/DE (with upwash) | 9.06 | 8.53 |
| PLL Amplitude-lbs (without upwash) | 1019 | 929 |
| PLL Amplitude-lbs (with upwash) | 1044 | 1014 |
| Vertical Shear Amplitude-lbs (without upwash) | 2270 | 3476 |
| Vertical Shear Amplitude-lbs (with upwash) | 2815 | 4106 |
| FZF-lbs (without upwash) | 1223 | 1686 |
| FZF-lbs (with upwash) | 1005 | 1557 |
| Flight Condition | 12 | 4 |

Variation of Equivalent Lift-to-Drag Ratio, Flap Hinge Vertical Shear Vibratory Amplitude, Pitch Link Load Vibratory Amplitude, and Vertical Hub Force Fourth Harmonic Amplitude with Rotor Radius from Loads Analysis. Flight Velocity, Rotor Lift, and Gross Weight Are Held Constant.

| | | |
|---|------|------|
| Rotor Radius-ft | 25 | 30 |
| L/DE (without upwash) | 7.23 | 7.44 |
| L/DE (with upwash) | 7.66 | 7.85 |
| PLL Amplitude-lbs (without upwash) | 321 | 419 |
| PLL Amplitude-lbs (with upwash) | 485 | 460 |
| Vertical Shear Amplitude-lbs (without upwash) | 1449 | 2905 |
| Vertical Shear Amplitude-lbs (with upwash) | 1912 | 2877 |
| FZF-lbs (without upwash) | 754 | 1629 |
| FZF-lbs (with upwash) | 682 | 1561 |
| Flight Condition | 13 | 7 |

Variation of Equivalent Lift-to-Drag Ratio, Flap Hinge Vertical Shear Vibratory Amplitude, Pitch Link Load Vibratory Amplitude, and Vertical Hub Force Fourth Harmonic Amplitude with Rotor Radius from Loads Analysis. Flight Velocity, Rotor Lift, Gross Weight, and Flat Plate Area for Auxiliary Thrust Are Held Constant.

| | | |
|---|------|------|
| Rotor Radius-ft | 25 | 30 |
| L/DE (without upwash) | 8.06 | 7.40 |
| L/DE (with upwash) | 8.99 | 8.14 |
| PLL Amplitude-lbs (without upwash) | 825 | 734 |
| PLL Amplitude-lbs (with upwash) | 1154 | 916 |
| Vertical Shear Amplitude-lbs (without upwash) | 2598 | 3766 |
| Vertical Shear Amplitude-lbs (with upwash) | 3449 | 4359 |
| FZF-lbs (without upwash) | 1446 | 2736 |
| FZF-lbs (with upwash) | 1503 | 2507 |
| Flight Condition | 14 | 8 |

Variation of Equivalent Lift-to-Drag Ratio, Flap Hinge Vertical Shear Vibratory Amplitude, Pitch Link Load Vibratory Amplitude, and Vertical Hub Force Fourth Harmonic Amplitude with Rotor Radius from Loads Analysis. Flight Velocity, Rotor Lift, Gross Weight, and Flat Plate Area for Auxiliary Thrust Are Held Constant.

| | | |
|---|------|------|
| Rotor Radius-ft | 25 | 30 |
| L/DE (without upwash) | 7.09 | 7.83 |
| L/DE (with upwash) | 6.63 | 7.30 |
| PLL Amplitude-lbs (without upwash) | 483 | 293 |
| PLL Amplitude-lbs (with upwash) | 532 | 493 |
| Vertical Shear Amplitude-lbs (without upwash) | 897 | 2336 |
| Vertical Shear Amplitude-lbs (with upwash) | 1431 | 1820 |
| FZF-lbs (without upwash) | 720 | 1173 |
| FZF-lbs (with upwash) | 795 | 1386 |
| Flight Condition | 15 | 5 |

Variation of Equivalent Lift-to-Drag Ratio, Flap Hinge Vertical Shear Vibratory Amplitude, Pitch Link Load Vibratory Amplitude, and Vertical Hub Force Fourth Harmonic Amplitude with Rotor Radius from Loads Analysis. Flight Velocity, Rotor Lift, Wing Lift, and Gross Weight Are Held Constant.

| | | |
|---|------|------|
| Rotor Radius-ft | 25 | 30 |
| L/DE (without upwash) | 8.93 | 8.21 |
| L/DE (with upwash) | 8.72 | 8.01 |
| PLL Amplitude-lbs (without upwash) | 1025 | 873 |
| PLL Amplitude-lbs (with upwash) | 1052 | 987 |
| Vertical Shear Amplitude-lbs (without upwash) | 2556 | 3431 |
| Vertical Shear Amplitude-lbs (with upwash) | 3436 | 3188 |
| FZF-lbs (without upwash) | 1362 | 1730 |
| FZF-lbs (with upwash) | 1194 | 1795 |
| Flight Condition | 16 | 6 |

Variation of Equivalent Lift-to-Drag Ratio, Flap Hinge Vertical Shear Vibratory Amplitude, Pitch Link Load Vibratory Amplitude, and Vertical Hub Force Fourth Harmonic Amplitude with Rotor Radius from Loads Analysis. Flight Velocity, Rotor Lift, Wing Lift, and Gross Weight Are Held Constant.

| | | |
|---|------|------|
| Rotor Radius-ft | 25 | 30 |
| L/DE (without upwash) | 7.27 | 7.45 |
| L/DE (with upwash) | 7.18 | 7.26 |
| PLL Amplitude-lbs (without upwash) | 261 | 407 |
| PLL Amplitude-lbs (with upwash) | 429 | 546 |
| Vertical Shear Amplitude-lbs (without upwash) | 3124 | 5386 |
| Vertical Shear Amplitude-lbs (with upwash) | 3138 | 5220 |
| FZF-lbs (without upwash) | 765 | 1733 |
| FZF-lbs (with upwash) | 655 | 1594 |
| Flight Condition | 17 | 9 |

Variation of Equivalent Lift-to-Drag Ratio, Flap Hinge Vertical Shear Vibratory Amplitude, Pitch Link Load Vibratory Amplitude, and Vertical Hub Force Fourth Harmonic Amplitude with Rotor Radius from Loads Analysis. Flight Velocity, Rotor Lift, Wing Lift, Gross Weight, and Flat Plate Area for Auxiliary Thrust Are Held Constant.

| | | |
|---|------|------|
| Rotor Radius-ft | 25 | 30 |
| L/DE (without upwash) | 8.04 | 7.29 |
| L/DE (with upwash) | 8.57 | 7.65 |
| PLL Amplitude-lbs (without upwash) | 869 | 735 |
| PLL Amplitude-lbs (with upwash) | 905 | 927 |
| Vertical Shear Amplitude-lbs (without upwash) | 3234 | 3306 |
| Vertical Shear Amplitude-lbs (with upwash) | 4630 | 4694 |
| FZF-lbs (without upwash) | 1559 | 2685 |
| FZF-lbs (with upwash) | 1521 | 2444 |
| Flight Condition | 18 | 10 |

Variation of Equivalent Lift-to-Drag Ratio, Flap Hinge Vertical Shear Vibratory Amplitude, Pitch Link Load Vibratory Amplitude, and Vertical Hub Force Fourth Harmonic Amplitude with Rotor Radius from Loads Analysis. Flight Velocity, Rotor Lift, Wing Lift, Gross Weight, and Flat Plate Area for Auxiliary Thrust Are Held Constant.

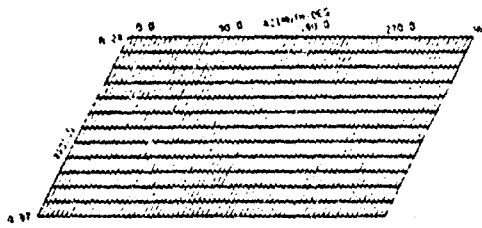
APPENDIX D

Surface Plots

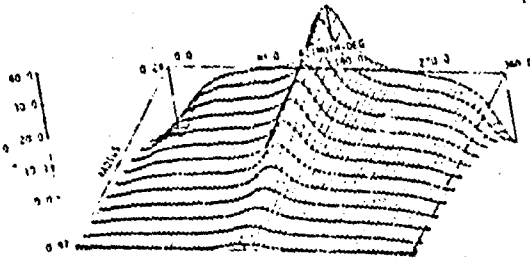
This appendix contains a few surface plots of upwash values, UP, the steady value and first ten harmonics of the blade loading, and the same blade loading with the steady value and first two harmonics removed. The blade loading is from B-65. The upwash values in this appendix are not nondimensionalized by rotor tip speed. They have units of ft/sec. The blade loading is in lb/in. These surface plots are examples only. They show that the effects of fuselage/wing/engine upwash on blade loading distribution is not dramatic.

ORIGINAL DRAWING
OF POOR QUALITY.

ISOLATED ROTOR

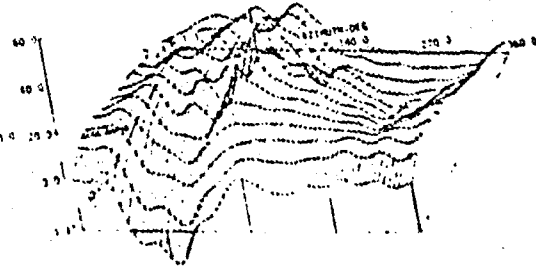
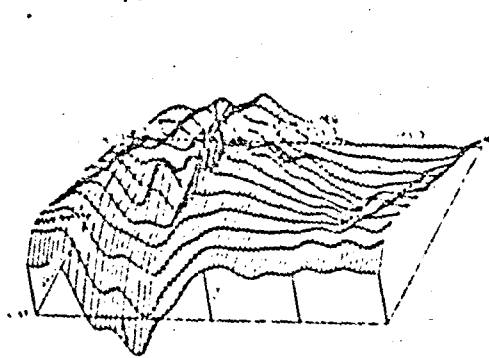


FUSELAGE UPWASH



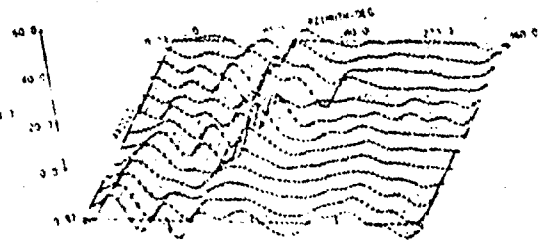
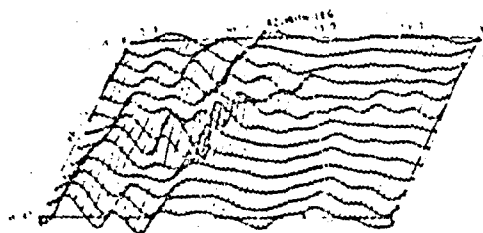
UPWASH VELOCITY, NORMAL COMPONENT,
 Δu_p FUSELAGE (ft/sec)

UPWASH VELOCITY, NORMAL COMPONENT,
 Δu_p FUSELAGE (ft/sec)



BLADE LOADING (lb/in)
HARMONICS 0 TO 10

BLADE LOADING (lb/in)
HARMONICS 0 TO 10



BLADE LOADING (lb/in)
HARMONICS 3 TO 10

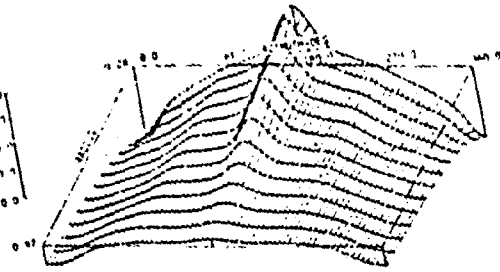
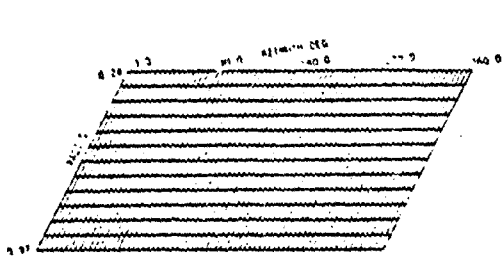
BLADE LOADING (lb/in)
HARMONICS 3 TO 10

Flight Condition 3

ISOLATED ROTOR

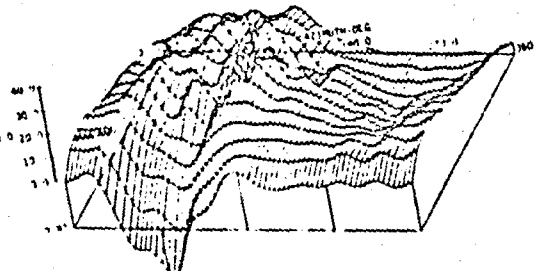
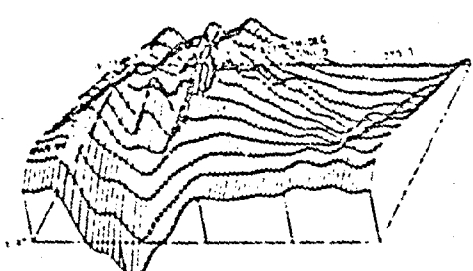
ORIGINAL PAGE IS
OF POOR QUALITY

FUSELAGE UPWASH



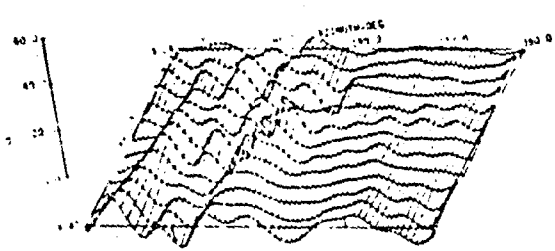
UPWASH VELOCITY, NORMAL COMPONENT,
 ΔU_p FUSELAGE (ft/sec)

UPWASH VELOCITY, NORMAL COMPONENT,
 ΔU_p FUSELAGE (ft/sec)



BLADE LOADING (lb/in)
HARMONICS 0 TO 10

BLADE LOADING (lb/in)
HARMONICS 0 TO 10



BLADE LOADING (lb/in)
HARMONICS 3 TO 10

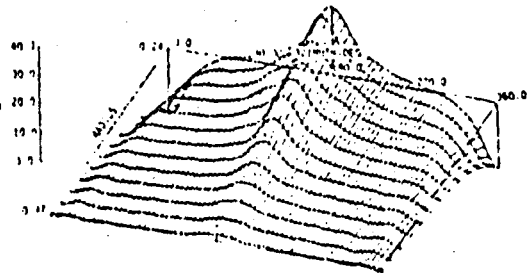
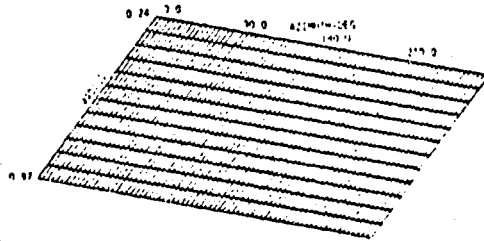
BLADE LOADING (lb/in)
HARMONICS 3 TO 10

Flight Condition 5

ORIGINAL PAIR IS
OF POOR QUALITY

ISOLATED ROTOR

FUSELAGE UPWASH

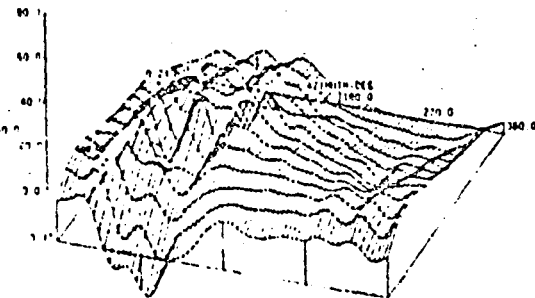
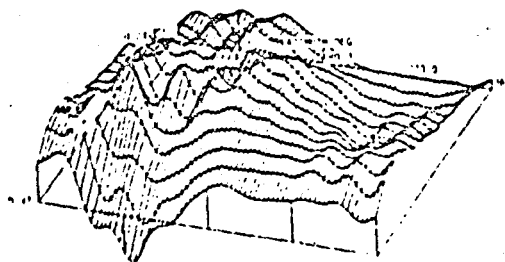


UPWASH VELOCITY, NORMAL COMPONENT,

UPWASH VELOCITY, NORMAL COMPONENT,

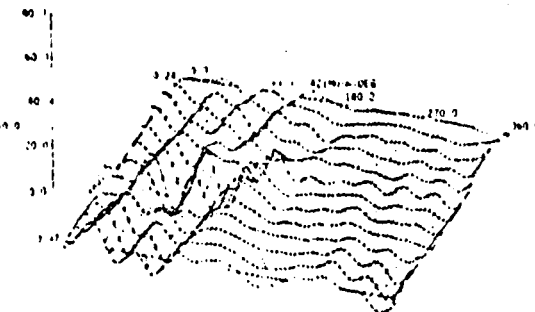
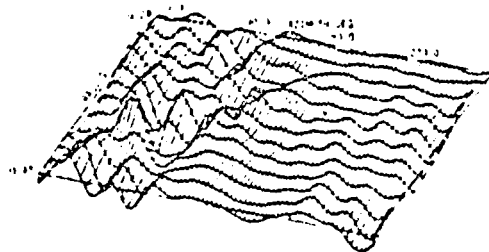
ΔU_p FUSELAGE (ft/sec)

ΔU_p FUSELAGE (ft/sec)



BLADE LOADING (lb/in)
HARMONICS 0 TO 10

BLADE LOADING (lb/in)
HARMONICS 0 TO 10



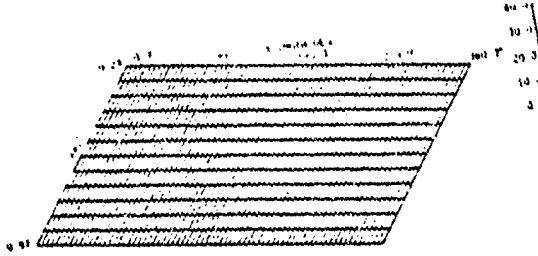
BLADE LOADING (lb/in)
HARMONICS 3 TO 10

BLADE LOADING (lb/in)
HARMONICS 3 TO 10

Flight Condition 7

ORIGINAL PAGE IS
OF POOR QUALITY.

ISOLATED ROTOR

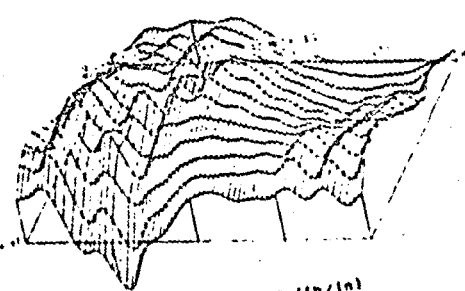


UPWASH VELOCITY, NORMAL COMPONENT,
 Δ_{UP} FUSELAGE (ft/sec)

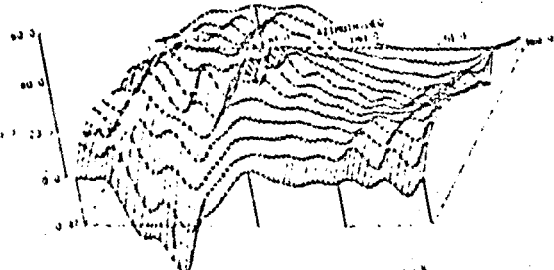
FUSELAGE UPWASH



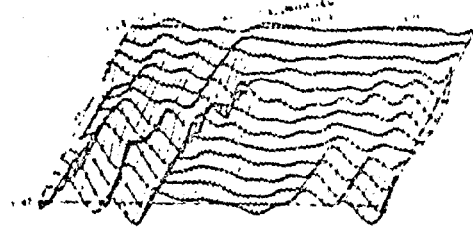
UPWASH VELOCITY, NORMAL COMPONENT,
 Δ_{UP} FUSELAGE (ft/sec)



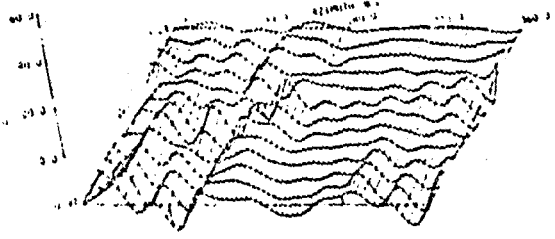
BLADE LOADING (lb/in)
HARMONICS 0 TO 10



BLADE LOADING (lb/in)
HARMONICS 3 TO 10



BLADE LOADING (lb/in)
HARMONICS 5 TO 10



BLADE LOADING (lb/in)
HARMONICS 3 TO 10

Flight Condition 9

| | | | | | |
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| 16. Abstract The effects of RSRA fuselage configurations on rotor performance and loads have been quantified analytically by means of currently available potential flow and rotor analysis. Four configurations of the Rotor Systems Research Aircraft (RSRA) were considered in this study. They were: <ol style="list-style-type: none"> (1) Fuselage alone (conventional helicopter) (2) Fuselage with auxiliary propulsion (3) Fuselage with wings (auxiliary lift) (4) Fuselage with both auxiliary lift and propulsion The rotor system investigated was identical to a CH-47D front rotor except that it had four instead of three blades. Two scaled-down versions of the same rotor were also analyzed to determine the effect of rotor scale on the fuselage upwash effects. The flight conditions considered for the upwash study are discussed. The potential flow models for the RSRA configuration, with and without the wings and the auxiliary propulsion system, are presented. The results of fuselage/wing/propulsion system upwash on performance and loads are also presented. The plethora of data resulting from this study reflected the existence of complicated flow interactions and did not lend itself to straightforward interpretation in all cases. More often than not though, neglecting fuselage upwash causes an underestimation of performance and an underestimation of loads. | | | | | |
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