THEORETICAL AND EXPERIMENTAL FLOW CELL STUDIES OF A HYDROGEN-BROMINE FUEL CELL

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Final Report, Part I

Prepared for

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Note:

Part I of the Final Report represents the M. S. Thesis of Ms. Sharon D. Fritts "Equilibrium Studies on the Hydrogen-Bromine Fuel Cell," University of Akron, 1986.

ABSTRACT

There is increasing interest in hydrogen-bromine fuel cells as both primary and regenerative energy storage systems. One promising design for a hydrogen-bromine fuel cell is a negative half cell having only a gas phase, which is separated by a cationic exchange membrane from a positive half cell having an aqueous electrolyte. The hydrogen gas and the aqueous bromide solution are stored external to the cell.

In order to calculate the energy storage capacity and to predict and assess the performance of a single cell, the open circuit potential (OCV) must be estimated for different states of charge, under various conditions.

Theoretical expressions were derived to estimate the OCV of a hydrogen-bromine fuel cell. In these expressions temperature, hydrogen pressure, bromine and hydrobromic acid concentrations were taken into consideration. Also included are the effects of the Nafion membrane separator and the various bromide complex species. Activity coefficients were taken into account in one of the expressions. The sensitivity of these parameters on the calculated OCV was studied.

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Experiments were completed to measure the OCV of a hydrogen-bromine fuel cell at various states of charge of a cell with initial charge capacities of 35% HBr and 48% HBr. Rates of membrane and solution equilibrium were also studied.

The theoretical expressions were useful in assessing the effects of various parameters on the OCV. The variables which were found to have a significant effect on the OCV through either experimental or theoretical study were: hydrogen pressure, temperature, hydrobromic acid and bromine concentrations. The type of Nafion membrane separator had an insignificant influence on the OCV. The agreement between the predicted and the actual OCV might be improved with knowledge of the activity coefficients, and of the chemistry of bromide species in concentrated solutions.

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NOMENCLATURE

والمنازر

ai	<pre>= activity of species i, moles/liter</pre>
aiθ	<pre>= property expressing secondary reference state, liter/mole</pre>
a _l	<pre>= mole fraction tribromide formed from elemental bromine</pre>
b ₁	<pre>= mole fraction pentabromide formed from elemental bromine</pre>
c _l	= mole fraction of free bromine
Ci	= initial concentration of species i, moles/liter
c ₁	= equilibrium concentration of species i, moles/liter
Co	= concentration of solvent, moles/liter
c _R	= fixed anion concentration of membrane, moles/liter
de	= density of electrolyte absorbed by membrane, g/cc
F	= Faraday's constant, 96,487 c/equiv.
fe	= weight fraction of electrolyte absorbed by membrane
fi	= fraction of membrane ion groups in ion clusters
fw	= fraction of membrane electrolyte in ion clusters
K	= equilibrium constant
mi	= molality of species i, moles/kg
Mo	= molecular weight of solvent, g/mole
r ²	= parameter which represents goodness of a linear regression
R.	= universal gas constant, 8.314 J/gmole-K
т	= temperature, K

хv

= open circuit potential, volts U υ^θ = open circuit potential at standard state, volts Wi = weight of species i in solution, g = weight fraction of species i in solution X_i = molal activity coefficient of species i Υi = absolute activity of species i λi λ_i^{θ} = property expressing secondary reference state, kg/mole = electric potential, (or quasielectrostatic potential), φ. volts μ_i = electrochemical potential of species i, J/mole * = chemical potential of hydrogen referred to ideal gas μ

, state, J/mole

Superscripts

a = hydrogen electrode phase

a' = bromine electrode current collector

 β = membrane phase

 δ = solution phase

 θ = standard state

Subscripts

n = reference ion, hydrogen ion

s = supporting electrolyte

e = electron

CHAPTER I

INTRODUCTION AND BACKGROUND

There has been increasing interest in recent years in hydrogen-halogen rechargeable fuel cells as both primary and regenerative energy storage systems. They can be coupled with solar cell systems to provide the power necessary to charge the hydrogen-halogen battery [1]. This, along with the high energy densities of these, systems, make them candidates for space power applications.

The types of hydrogen-halogen batteries that have been studied are the hydrogen-chlorine, hydrogen-bromine, and hydrogen-iodine. The hydrogen-chlorine and hydrogenbromine systems are comparable in terms of efficiency and heat rejection, but the hydrogen-iodine is less efficient [2]. The advantage the hydrogen-bromine system has over the hydrogen-chlorine system is the high solubility of bromine in hydrobromic acid, whereas chlorine has a low solubility in hydrochloric acid.

The electrochemical reactions for the hydrogenbromine system are reversible, and the use of polymer electrolytes has eliminated cell gaps. Consequently, good energy storage efficiencies can be obtained even at high current density operation.

A high power density system, where there is a high rate of energy delivery, is important because it is useful for situations requiring either high or low power. The power density of a system is directly proportional to its current density, so high current density operation is desirable.

Operation at high current densities requires reactor designs which enhance mass transfer rates. A flow system is necessary to improve mass transfer performance and aid in thermal management.

1.1 Hydrogen-Bromine Fuel Cells

The flow system design for a hydrogen-bromine cell is a negative half-cell having only a gas phase which is separated by a solid polymer ionic conducting membrane from a positive half-cell having a flowing aqueous electrolyte. Figure 1 shows a schematic of the hydrogen-bromine energy storage system. The hydrogen and bromine formed are stored external to the cell, the hydrogen stored in the form of a metal hydride.

1.1.1 Reactions and Battery Operation

The overall reaction taking place in the cell during charge can be written as:

HBr(aq.) + electrical energy + $1/2H_2(g) + 1/2Br_2(1)$

The energy is stored in the form of bromine in the

Bra

ΒY

FLOW

ELECTRODE

AQUEOUS

HBr/Br2

STORAGE





Н₂

STORAGE

Чz

ELECTRODE

H₂ FLOW

CONDUCTIVE

FIELD



Figure 1. Schematic of a hydrogen-bromine energy storage system.

₽

electrolyte reservoir and as hydrogen gas in the hydrogen reservoir. Because of this, the total energy storage as watt-hours depends primarily on the reservoir size, rather than on the size of the cells [3].

The use of solid polymer electrolytes combined with electrodes promoting good mass transfer make it possible to operate the cell with current densities in the range of 300 mA/cm^2 [4]. In practice, the configuration for a multicell battery is bipolar construction, with the electrodes in direct contact with the solid polymer electrolyte, which is a proton conducting membrane.

1.1.2 Advantages and Disadvantages of Hydrogen-Bromine Fuel Cells

The major advantage that the hydrogen-bromine battery has over other fuel cell systems is that the positive electrode overpotential during the charge reaction is negligible, as is its polarization during the discharge reaction. Therefore, the reaction

 $Br^- \ddagger 1/2 Br_2 + e$

approaches thermodynamic reversibility [3].

Other advantages the hydrogen-bromine system possesses are:

 fast electrode kinetics cause a high electric to electric efficiency [5];

2. the cells can be operated at high current densities;

 a flow system improves mass transfer performance and aids in thermal management;

4. because of the high solubility of bromine in hydrobromic acid, there is less concern regarding mass transfer limitations; and

5. the fuel cell can be operated with shallow discharges, and can tolerate both over charge and under discharge [5].

Another advantage is that the use of a solid polymer electrolyte (SPE) allows the anode and the cathode to be operated at different pressures. This means that hydrogen can be produced at a pressure high enough for storage as a metal hydride or as a compressed gas without further compression.

A major disadvantage to any flow cell system is the external pumping energy necessary for operation and the associated efficiency loss.

There are also some disadvantages specific to the hydrogen-bromine system. They are:

 the weight of the aqueous phase containing bromine, and its solubilizer;

the high corrosivity of bromine and hydrobromic acid; and

3. the open circuit voltage is dependent on the state of charge of the bromine reservoir [3].

Another disadvantage to the system is the complexities inherent to the lack of knowledge regarding the mechanism of charge transport within the cation exchange membrane used as the solid polymer electrolyte.

1.2 Background on the Development of the Hydrogen-Bromine Fuel Cell

The major components of a hydrogen-bromine fuel cell were studied for the development of a reliable, longlived system. The areas studied include electrodes, materials of construction, electrolytes, and membranes.

Long-lived electrodes with high current density operation are desired. Teflon-bonded platinum black gas diffusion anodes and porous carbon or graphite cathodes have been found to be capable of long term, high current density operation with no significant degradation [7].

Because of the corrosive behavior of bromine and hydrobromic acid, materials that could be used for cell construction were determined by soaking samples in aqueous concentrated HBr / Br_2 solutions [6]. It was found that the acceptable metals include platinum, platinum-iridium, titanium-palladium, tantalum, and niobium. The tri- or tetra-fluoroethylene polymers, Teflon, Kynar, and Halon, were also found to be bromine resistant.

Besides being resistant to the corrosive properties of bromine, the SPE used must permit transport of hydrogen ions and prevent the transport of the bromine containing

species. The transport of bromine species would cause the discharge reactions to occur without electrochemical benefit, and also causes the degradation of the hydrogen electrode due to bromine attack. Perfluorinated sulfonic acid membranes, Nafion, have been used since they are chemically inert, highly permeable to cations, and preclude passage of anions [4].

Because the electrode kinetics of a hydrogenbromine fuel cell are fast, the voltage and coulombic efficiencies are primarily determined by the voltage drop across the membrane. This means that the efficiency is strongly related to the membrane conductivity and reactant permeation across the membrane. Good conductivity can be achieved by boiling the membrane in water to swell the polymer matrix, but the effects of this do not last if the membrane is allowed to dry [5].

Bromine has a very low solubility in water, so a solubilizer must be present in the system. The bromine needs to be dissolved in as little unreacting solvent as possible due to the weight considerations for aerospace applications.

A study showed that the cell resistance was three to eight times higher in the charged state for a cell with a salt solubilizer, (e.g., NaBr, KBr, LiBr, NH₄Br, CsBr, NaCl or SrBr₂), than for a cell with an HBr solubilizer [6]. This was believed to be due to fewer available

7.

hydrogen ions within the membrane for charge transport. For cells that were substantially discharged, the salt solubilizers had little impact on the cell resistance. For these reasons, HBr is the preferred solubilizer for bromine.

1.3 Goal of this Research

Since the open circuit voltage is dependent on the state of charge of the electrolyte, multicell systems use switches to control the number of cells being used to meet the requirements at any given time. Therefore, the open circuit potential must be known as a function of the state of charge of the bromine solution reservoir.

This research was done to develop a theoretical expression capable of finding the open circuit potential of the hydrogen-bromine cell for a given hydrogen partial pressure, hydrobromic acid and bromine concentrations, operating temperature, and type of membrane separator.

Experimental work was done to confirm the theoretical development. The rates of membrane and solution equilibrium were measured to determine the length of time required for the membrane to come into equilibrium with the solution.

CHAPTER II

LITERATURE REVIEW

2.1 Reported Values of the Open Circuit Potential

Work had been done previously to determine the open circuit potential of a hydrogen-bromine fuel cell. The details of this work were either not thoroughly reported, or the system was significantly different, causing the reported values to be unusable for the system presently being studied.

Yeo and Chin [5] reported an empirical equation which can be used to calculate the open circuit cell voltage. The open circuit voltage, E_0 , is expressed as:

$$E_{O} = \pm \left\{ \phi - (T-298) \left[4.3 \pm 1.86 \ln \frac{12.36X}{1-X_{HBr}} \right] \times 10^{-4} + 4.31 \times 10^{-5} T \left(\ln f_{H_{2}} + \ln a_{Br_{2}} \right) \right\}$$
(2-1)

where

$$b = \begin{bmatrix} 1.073 - 0.0567 \ln \frac{12.36X}{1-X_{HBr}} & (0.016 < X_{HBr} < 0.11) \\ 1.095 - 0.1042 \ln \frac{12.36X}{1-X_{HBr}} & (0.11 < X_{HBr} < 0.28) & (2-2) \\ 1.336 - 0.2581 \ln \frac{12.36X}{1-X_{HBr}} & (0.28 < X_{HBr} < 0.58) \end{bmatrix}$$

where

T - temperature in ${}^{O}K$ X_{HBr} - weight fraction of hydrobromic acid f_{H_2} - fugacity of hydrogen gas ${}^{a}Br_2$ - activity of Br_2 in the electrolyte

This equation was determined through experiments where the electrolyte was aqueous HBr, rather than an aqueous solution of bromine and hydrobromic acid. The hydrogen and bromine terms used in this expression are the theoretical Nernst-type terms added to approximate the effects these values would have on the open circuit voltage [8]. Note that the expression

$$\frac{R}{2F} = 4.31 \times 10^{-5}$$
 (2-3)

follows the Nernst expression form. They state that the activity of the bromine can be taken as unity for bromine present as a liquid phase. It seems that these expressions assume that bromine is saturated in the hydrobromic acid solution for all states of charge. However, this is only true for high states of charge. Therefore, this equation does not accurately reflect the open circuit potentials where the bromine content is below its solubility limit in the hydrobromic acid solution.

Analysis of the term $12.36X_{HBr}/(1-X_{HBr})$ reveals that it is a conversion of the weight fraction of HBR to its molality. This means that expressions (2-1) and (2-2) are Nernst-type expressions in terms of hydrobromic acid concentration. The first and second terms of (2-1) contain numerical values found through a regression of data, and are assumed to represent the activity coefficient effects on the activity of hydrobromic acid, as would be found in a theoretical Nernst expression.

This correlation was determined using temperature studies, but not through experiments of hydrogen pressures. A Nafion 115 membrane was used as the solid polymer electrolyte for these experiments. A computer program that calculates the open circuit voltage using this correlation is given in Appendix A.

Some General Electric open circuit voltage data were given [9]. That report provides the temperature and pressure used in the experiments and the measured open circuit potential at four different states of charge. The initial and final HBr concentrations were given. The concentrations were reported in weight percentages, and it is unclear whether these values include the weight of the bromine present in the solution. Furthermore, no information on the membrane was provided.

Experimental work to measure the open circuit potential of a hydrogen-bromine cell was done by Glass and Boyle [3,6] using the system shown in Figure 2. A hydrobromic acid solution was prepared, and half was placed in the hydrogen half cell, compartment C. Bromine was



A = BROMINE HALF CELL G = STIRRER B = WICK

H = HYDROGEN ELECTRODES

- C = HYDROGEN HALF CELL
- I = PLATINUM ELECTRODES (BROMINE)
- Schematic of experimental cell used by Glass and Boyle [3,6] to measure open circuit voltage of a hydrogen- bromine fuel cell. Figure 2.

mixed with the remaining acid, and placed in the bromine half cell, compartment A. The hydrogen electrodes were platinized platinum, and the bromine electrode was shiny platinum. The values reported for the open circuit voltage were referenced against a hydrogen electrode. It is not clear whether the reported potentials were corrected to standard conditions of a normal hydrogen reference electrode, i.e., 1 atm. hydrogen pressure, and unit activity of hydrogen ions. Also, no membrane was used in their system, therefore the values found in these experiments may not adequately represent those of the flow cell SPE system considered in this research.

2.2 Nafion Membranes as Solid Polymer Electrolytes

The Nafion membrane is an ion containing polymer. Nafion has a perfluorinated ethylene backbone with side chains of the form

> $-(0-CF_2-CF)_{x}OCF_2CF_2SO_3H$ i CF_3

where x is usually one [4, 24].

The hypothesis that the ions in Nafion are clustered is generally accepted, but has not been verified, especially in acidic electrolytes [4].

Yeo [10] states that the structure of the membrane can be described as a microphase-separated system in which a matrix of low ion content is interspersed with ion

clusters. Part of the water contained in the membrane is associated with the sulfonic acid groups, part with the organic matrix, and the remainder forms hydrophilic ion clusters.

Yeo and McBreen [4] found that the membrane resistivity is permanently reduced after it has been heated once, so the membrane should be preheated to at least 70° C before it is used. This is apparently due to an increase in the water content of the membrane. They also found that the membrane conductivity is about one order of magnitude less than the conductivity of the free electrolyte.

Yeo and McBreen [4] also studied the permeation of bromine through Nafion. They found that the bromine diffusivity in the membrane decreased with increasing acid concentration. This is due to the decrease of the water content of the membrane with high acid concentrations. The rates of bromine permeation were lower than they expected, and this is believed to be due to the complexing of bromine to form tribromide and pentabromide ions.

2.3 Equilibria of Aqueous Bromine and Hydrobromic Acid Solutions

The equilibria present in aqueous solutions of hydrobromic acid and bromine were studied by Jones and Baeckstrom [11]. The equilibrium constants of the reactions

.14 .

 $Br_2 + H_2O \ddagger H^+ + Br^- + HBrO$

 $Br_2 + Br^- \neq Br_3$

 $2Br_2 + Br^- \ddagger Br_5$

were determined from conductance measurements. The equilibrium constant for the hydrolysis reaction was found to be 5.8 x 10^{-9} . For the complexing reactions forming tribromide and pentabromide, the equilibrium constants were found to be 16 and 40, respectively. These values were determined at the solubility of bromine in water at 25° C, which is equivalent to 0.2141 molar, of which 0.2098 mole is present as Br₂.

Work was done by Will [12] to determine the tribromide concentrations in aqueous solutions made using high concentrations of bromide ions and bromine. He found that essentially all of the bromine originally added reacted to form tribromide.

CHAPTER III

THEORY

The open circuit potential of a fuel cell is the potential of the cell at equilibrium, where no current is flowing through the cell. The properties a fuel cell possesses at the open circuit condition can be determined theoretically through thermodynamic relationships and material properties.

3.1 Derivation of the Open Circuit Potential Expression

A theoretical expression was derived to determine the open circuit potential for the SPE hydrogen-bromine fuel cell depicted in Figure 3. The open circuit potential for this hydrogen-bromine cell can be expressed as:

$$FU = -F(\phi^{\alpha} - \phi^{\alpha'}) = \mu^{\alpha} - \mu^{\alpha'} \qquad (3-1)$$

The symbol μ_i represents the electrochemical potential of species i.

In the α phase, the reaction is

so

$$1/2 H_{2} + H^{+} + e$$

$$a^{\alpha} = 1/2 \mu^{\alpha} - \mu^{\alpha}_{H} + \mu^{\alpha}_{H}$$

(3-2)

α′ δ α Pt (s) C (s) Membrane Solution н+ н+ н+ H₂ s + s + R Br⁻ Br₃ Br⁻ Br₃ Br5 Brs Br₂ Br₂ H₂0 H_{2}^{0}

Figure 3. Diagram of species present in each phase of the SPE hydrogen-bromine fuel cell.

At equilibrium, the electrochemical potentials of the hydrogen ion in the α and β phases are equal, therefore

$$\mu_{H^{+}}^{\alpha} = \mu_{H^{+}}^{\beta}$$
 (3-3)

The reactions taking place at the a' electrode are:

 $\frac{1}{2} \operatorname{Br}_{2} + e^{-} \neq \operatorname{Br}_{3}^{-}$ $\frac{3}{2} \operatorname{Br}_{2} + e^{-} \neq \operatorname{Br}_{3}^{-}$ $\frac{5}{2} \operatorname{Br}_{2} + e^{-} \neq \operatorname{Br}_{5}^{-}$ $\frac{1}{2} \operatorname{Br}_{3} + e^{-} \neq 3/2 \operatorname{Br}_{3}^{-}$ $\frac{1}{4} \operatorname{Br}_{5} + e^{-} \neq 5/4 \operatorname{Br}_{3}^{-}$ $\frac{3}{2} \operatorname{Br}_{5} + e^{-} \neq 5/2 \operatorname{Br}_{3}^{-}$

The hydrolysis reaction of bromine is neglected due to its extremely low equilibrium constant [11].

By combining the equations in such a way as to eliminate dependent reactions, three independent reactions are found. They are:

 $Br_{2} + Br^{-} \ddagger Br_{3}$ $2Br_{2} + Br^{-} \ddagger Br_{5}$ $1/2 Br_{2} + e^{-} \ddagger Br^{-}$

These equations describe the solution phase chemistry of the δ phase.

The electrochemical potentials of the electrons in the α' and δ phases are equal.

$$\begin{array}{ccc}
\alpha & \delta \\
\mu &= \mu \\
e & e
\end{array} \tag{3-4}$$

The bromine oxidation reaction can then be described by

$$\mu_{e}^{\delta} = \mu_{Br}^{\delta} - \frac{1}{2} \mu_{Br}^{\delta}$$
(3-5)

Because some of the bromine reacts to form tribromide and pentabromide, the electrochemical potential of bromine can be written as

$$\mu_{Br_{2}}^{\delta} = a_{1}(\mu_{Br_{3}}^{\delta} - \mu_{Br_{2}}^{\delta}) + 1/2b_{1}(\mu_{Br_{5}}^{\delta} - \mu_{Br_{2}}^{\delta}) + c_{1}\mu_{Br_{2}}^{\delta} (3-6)$$

following the stoichiometry of the reactions, where a_1 , b_1 , and c_1 are the mole fractions of the Br_3^- , Br_5^- , and Br_2 formed in their respective orders. Also, by definition,

$$a_1 + b_1 + c_1 = 1$$
 (3-7)

where

С

$$a_{1} = \frac{\overline{c}_{Br_{3}}^{\delta}}{\overline{c}_{Br_{2}}^{\delta} + \overline{c}_{Br_{3}}^{\delta} + \overline{c}_{Br_{5}}^{\delta}}$$
(3-8)
$$b_{1} = \frac{\overline{c}_{Br_{2}}^{\delta}}{\overline{c}_{Br_{2}}^{\delta} + \overline{c}_{Br_{3}}^{\delta} + \overline{c}_{Br_{5}}^{\delta}}$$
(3-9)
$$\overline{c}_{Br_{2}}^{\delta} + \overline{c}_{Br_{3}}^{\delta} + \overline{c}_{Br_{5}}^{\delta}$$

$$I = \frac{\overline{C}\delta^{2}}{\overline{C}Br_{2}} + \overline{C}\delta^{2} + \overline{C}\delta}$$
(3-10)
The open circuit potential becomes

$$FU = 1/2 \mu_{H_{2}}^{\alpha} - \mu_{H^{+}}^{\beta} - \mu_{Br^{-}}^{\delta} + 1/2[a_{1}(\mu_{Br_{3}}^{\delta} - \mu_{Br^{-}}^{\delta}) + 1/2[a_{1}(\mu_{Br^{-}}^{\delta} - \mu_{Br^{-}}^{\delta}) + 1/2[a_$$

Using the definitions given by Newman [13],

$$\mu_{H}^{\alpha} = \mu_{H}^{\star} + RT \ln \rho_{H}^{\alpha}$$
(3-12)

2 2 2 2

$$\mu_{H+}^{\beta} = RTln(\lambda_{H+}^{\beta}) + RTln(m_{H+Y}^{\beta})$$
(3-13)

$$\mu_{Br}^{\delta} = RTln(\lambda_{Br-}^{\delta}) = RTln(\lambda_{Br-}^{\theta}) + RTln(m_{Br-}^{\delta}\gamma_{Br-}^{\delta}) \quad (3-15)$$

$$\mu_{Br_{5}}^{\delta} = RT1n(\lambda_{Br_{5}}^{\delta})$$
(3-16)

$$\mu_{\text{Br}_{2}}^{\delta} = \text{RTln}(\lambda_{\text{Br}_{2}}^{\delta}) = \text{RTln}(\lambda_{\text{Br}_{2}}^{\theta}) + \text{RTln}(m_{\text{Br}_{2}}^{\delta} \sigma_{\text{Br}_{2}}^{\delta})$$
(3-17)

Substituting these expressions into the equation for the open circuit potential gives

$$FU = 1/2 \mu_{H_2}^{*} - RTln\lambda_{H^+}^{\theta} - RTln\lambda_{Br^-}^{\theta} + RTln(\frac{P_{H_2}^{\alpha}}{m_{H^+}^{\beta} \gamma_{H^+}^{\beta} m_{Br^-}^{\delta} \gamma_{Br^-}^{\delta}})$$

+
$$1/2[a_1RTln(\frac{\lambda_{Br_3}^{\delta}}{\lambda_{Br-}^{\delta}\lambda_{Br_2}^{\delta}}) + 1/2b_1RTln(\frac{\lambda_{Br_3}^{\delta}}{\lambda_{Br-}^{\delta}\lambda_{Br_2}^{\delta}})$$

+ $a_1RTln\lambda_{Br_2}^{\delta} + b_1RTln\lambda_{Br_2}^{\delta} + c_1RTln\lambda_{Br_2}^{\delta}]$ (3-18)

By definition [13] there is the relationship

$$m_{j} \gamma = a_{j}$$
 (3-19)

The equilibrium relationships also exist [11]:

2

$$\frac{\lambda_{Br_3}^{\delta}}{\lambda_{Br-}^{\delta}\lambda_{Br_2}^{\delta}} = K_1 = 16$$
(3-20)

$$\frac{\lambda_{Br5}^{\delta}}{\lambda_{Br}^{\delta} - \lambda_{Br2}^{\delta}} = K_2 = 40 \qquad (3-21)$$

By combining the above equations, the open circuit potential expression becomes:

$$\begin{aligned} FU &= 1/2 \ \mu_{H_{2}}^{*} - RT \ln \lambda_{H^{+}}^{\theta} - RT \ln \lambda_{Br^{-}}^{\theta} + 1/2 \ RT \ln \lambda_{Br_{2}}^{\theta} \\ &+ RT \ln \frac{\frac{p_{H_{2}}^{\alpha} - a_{B}\delta_{R}}{a_{H^{+}}^{\beta} - a_{B}r^{-}}}{a_{H^{+}}^{\beta} - a_{B}r^{-}} + 1/2 [a_{I} \ RT \ln K_{I} + 1/2 \ b_{I} RT \ln K_{2}] \end{aligned}$$

The standard potential is defined to be

$$FU^{\theta} = 1/2 \mu^{\star} - RT \ln \lambda^{\theta} - RT \ln \lambda^{\theta} + 1/2 RT \ln \lambda^{\theta} (3-23)$$

$$H_{2}^{\theta} = H_{1}^{\theta} - RT \ln \lambda^{\theta} + 1/2 RT \ln \lambda^{\theta} RT^{\theta}$$

so the open circuit potential expression now becomes:

$$FU = FU^{\theta} + RTIn \frac{p_{H_2}^{\alpha} a_{Br_2}^{\delta}}{a_{H^+}^{\beta} a_{Br^-}^{\delta}} + 1/2[a_1RTInK_1 + 1/2b_1RTInK_2]$$
(3-24)

Neglecting activity coefficients of the ions gives the following expression:

$$FU = FU^{\theta} + RTIn \frac{P_{H_2}^{\alpha^{1/2}} a_{Br_2}^{\delta^{1/2}}}{m_{H^+}^{\beta} n_{Br^-}^{\delta}} + \frac{1}{2[a_1RT]nK_1} + \frac{1}{2b_1RT]nK_2]}$$

The molalities can be expressed in terms of molarity units by the relationship

$$n_i = \frac{C_i}{C_0 M_0}$$
(3-26)

where C_0 and M_0 are the concentration and molecular weight of the solvent, respectively.

The concentrations of the bromide species in the solution and of the hydrogen ion concentration in the membrane must be determined in order to calculate the open circuit voltage of the system.

3.2 Calculation of Equilibrium Bromide Concentrations

The equilibrium concentrations of the bromide compounds for the solution or & -phase are calculated using the symbols \overline{C}_{i} = concentration at equilibrium of species i

 $C_i \equiv initial$ concentration of species i

where the subscript s refers to a uni-univalent supporting electrolyte (e.g. NaBr, LiBr).

The principle of electroneutrality requires that:

$$\overline{C}_{H^{+}} + \overline{C}_{s} = \overline{C}_{Br_{-}} + \overline{C}_{Br_{-}} + \overline{C}_{Br_{-}}$$
(3-27)

It is assumed that the cation concentration in the δ -phase is unchanging and known.

$$\overline{C}_{H^+} = C_{H^+}$$
 (3-28)

$$\overline{C} = C \qquad (3-29)$$

The various anion concentrations change during equilibration, but are subject to the condition that bromine atoms in unit volume are conserved.

$$C_{s} + C_{H^{+}} + 2C_{Br_{2}} = \overline{C}_{Br_{-}} + 2\overline{C}_{Br_{2}} + 3\overline{C}_{Br_{-}} + 5\overline{C}_{Br_{-}} (3-30)$$

These changes are due to the complexing reactions

$$Br_2 + Br_{\pm} Br_3$$

 $2Br_2 + Br^- \downarrow Br_5$

where the equilibrium constants are simplified from (3-20) and (3-21) to be:

$$\frac{\overline{C}_{Br_{3}}}{\overline{C}_{Br_{-}} \overline{C}_{Br_{2}}} = K_{1} = 16 \qquad (3-31)$$

$$\frac{\overline{C}_{Br_{3}}}{\overline{C}_{Br_{-}} \overline{C}_{Br_{2}}} = K_{2} = 40 \qquad (3-32)$$

Combining equations (3-27) through (3-32) gives a cubic equation which can be used to solve for the equilibrium bromine concentration:

$$0 = 2C_{\text{Br}_{2}} + (32C_{\text{Br}_{2}} - 32C_{\text{S}} - 32C_{\text{H}} + -2)\overline{C}_{\text{Br}_{2}} + (80C_{\text{Br}_{2}} - 160C_{\text{H}} - 160C_{\text{S}} - 32)\overline{C}_{\text{Br}_{2}}^{2} - 80\overline{C}_{\text{Br}_{2}}^{3}$$
(3-33)

The root of this equation can be found using the bisection technique, as this method will insure a reasonable value to the root calculated. After the equilibrium bromine concentration is known, the bromide, tribromide, and pentabromide concentrations are found as follows:

$$\overline{C}_{Br^{-}} = \frac{C_{s} + C_{H^{+}}}{1 + 16\overline{C}_{Br_{2}} + 40\overline{C}_{Br_{2}}^{2}}$$
(3-34)

$$\overline{C}_{Br_{\overline{3}}} = 16\overline{C}_{Br_2} \overline{C}_{Br_{\overline{3}}}$$
(3-35)

$$\overline{C}_{Br5} = 40\overline{C}_{Br2}^2 \overline{C}_{Br}$$
 (3-36)

For the high states of charge, where two liquid phases are present in the δ -phase, the equilibrium concentrations are found by assuming the second liquid phase is pure bromine with unit activity [5]. This reduces equations (3-20) and (3-21) to be

$$\frac{C_{Br_{3}}}{\overline{C}_{Br_{1}}^{2} - a_{Br_{2}}^{2}} = K_{1} = 16$$
 (3-37)

$$\frac{-3}{\overline{C}_{Br-}}^{2} = K_{2} = 40$$
 (3-38)

thus allowing the concentrations of bromide, tribromide, and pentabromide to be readily calculated.

3.3 Derivation of Expression to Estimate Hydrogen Ion Concentration in Membrane

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A potential difference develops between two phases of adjoining electrolytes at equilibrium if the phase boundary is not permeable to all ions [14]. The hydrogenbromine fuel cell has a cation exchange membrane, which restricts the passage of anions. This potential difference is expressed in terms of concentrations in the derivation of the open circuit potential expression where

This inequality is accounted for by use of Donnan principles, and is derived as follows.

The concentration of the hydrogen ion in the membrane was found using the conditions of electroneutrality in the β and δ -phases, and the fact that the electrochemical potentials of an ion in the β and δ -phases are equal at equilibrium.

Following the definitions of equilibrium in Newman [13], the electrochemical potential of a reference ion in solution can be written as

$$n = RT \ln C + z F \Phi \qquad (3-40)$$

and for all other ions present,

= RTIn
$$\overline{C}_i$$
 + $z_i F \Phi$ + RT(Inf_i - $\frac{z_i}{z_n}$ Inf_n)
+ RT(Ina $\frac{\theta}{i}$ - $\frac{z_i}{z_n}$ Ina $\frac{\theta}{n}$) (3-41)

Since the electrochemical potentials of an ion at the phase boundary are equal, the term $RT(\ln a_{i}^{\theta} - \frac{z_{i}}{z_{n}} \ln a_{n}^{\theta})$ cancels out, because it is independent of phase. The approximation that the $RT(\ln f_{i} - \frac{z_{i}}{z_{n}} \ln f_{n})$ terms are equal for the β and δ -phases is made. Therefore, for the hydrogen ion,

RTIn
$$C_{H+}^{\delta}$$
 + F ϕ = RTIn C_{H+} + F ϕ (3-42)

RTIn
$$\overline{C}^{\delta} - F\phi = RTIn \overline{C}^{\beta} - F\phi$$
 (3-43)
Br₃ Br₃ Br₃

Similar equations were written for all ions in the system. Combination of these equations leads to the relationships

$$\frac{C_{H+}^{\delta}}{C_{H+}^{\beta}} = \frac{\overline{C}_{Br\bar{3}}^{\beta}}{\overline{C}_{Br\bar{3}}^{\delta}} = \frac{C_{S}^{\delta}}{C_{S}^{\beta}} = \frac{\overline{C}_{Br\bar{5}}^{\beta}}{\overline{C}_{Br\bar{5}}^{\delta}} = \frac{\overline{C}_{Br-}^{\beta}}{\overline{C}_{Br-}^{\delta}}$$
(3-44)

The conditions of electroneutrality are:

with the assumption that the amount of solution absorbed by the membrane is negligible.

Combining equations (3-44), (3-45), and (3-46) leads to the equation

$$c_{H+}^{\beta} = \frac{c_{R}^{+} + c_{R}^{2} + 4(c_{H+}^{\delta} + c_{s}^{\delta})^{2}}{2} \qquad \frac{c_{H+}^{\delta}}{c_{H+}^{\delta} + c_{s}^{\delta}} \quad (3-47)$$

where C_R is the fixed anion concentration of the membrane.

CHAPTER IV

EXPERIMENTAL SYSTEM AND PROCEDURE

An experimental system was designed and built to measure the open circuit potential of a hydrogen-bromine fuel cell. The variables to be studied were HBr and Br₂ concentration, hydrogen partial pressure, and type of Nafion membrane. Estimated rates of membrane and solution equilibrium were also measured with this system.

4.1 Equipment

4.1.1 Experimental System

Figure 4 is a schematic of the system used for experimental measurements. A listing of the equipment used is given in Appendix C. All parts were constructed of Teflon or glass due to the high corrosivity of hydrobromic acid and bromine.

The hydrobromic acid solution was sparged with nitrogen to remove oxygen from the system to obtain more reproducible results. The solution was mixed in a storage tank that was immersed in a water bath. The solution was pumped through the cell, using a Teflon piston pump chosen because of the low flow rates. A standard calomel reference electrode was inserted into this line. A



Figure 4. Diagram of experimental system for measuring open circuit voltage.

thermistor at the cell entrance measures the solution temperature to determine as closely as possible the actual cell temperature. There are pressure gages at the cell outlets, followed by needle valves to maintain equal pressure in each half cell.

Detailed diagrams of the half cells are shown in Figures 5 and 6. Both half cells were machined of TFE Teflon blocks. The cell was designed around the constraint of the size of the catalytically active region of the SPE membrane electrode assembly. A drawing of the membrane electrode assembly is shown in Figure 7. The electrode materials bonded to the membrane are a platinum black catalyst on the hydrogen side and a proprietary catalyst of Electrochem. Inc. bonded to the Nafion 120 membrane on the bromine side [15].

For some experiments, the Nafion 120 SPE membrane electrode assembly was replaced by a Nafion 117 film (equivalent weight 1100, thickness 0.178 cm. [12]). The Nafion 117 film does not have an electrode bonded to it. In either case, a 52 mesh platinized platinum screen was pressed against the membrane on the gas side, with a 52 mesh shiny platinum screen placed behind it, which was spot welded to a platinum lead wire.

The hydrogen flow field was designed to provide the most support for the platinum screens and membrane with minimal contact area. This was done by cutting v-shaped

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PLATINUM CURRENT COLLECTOR

HYDROGEN FLOW FIELD VITON 0-RING BOLT HOLES

Diagram of hydrogen half cell. The dimensions of drawing are inches, and the drawing is to 75% of scale. Figure 5.



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Figure 6. Diagram of bromine half cell. The dimensions of drawing are inches, and the drawing is to 75% of scale.

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NOBLE

METAL



Figure 7. Diagram of Nafion 120 membrane electrode assembly. Dimensions are given in inches, and drawing is to 75% of scale.

ယ ယ grooves perpendicular to each other across the surface of the cell. This creates pyramids which were subsequently machined down 0.012" to allow placement of the platinum screens.

The bromine half cell contains a carbon felt electrode and a graphite block current collector. The geometry of the carbon felt electrode is as shown in Figure 6. This design allows for open regions at the chamber entrance and exit, to prevent solution hold up in the cell, and thus maintain constant and uniform concentration throughout the electrode.

4.1.2 Electrometer and Data Acquisition System

Voltage measurements were taken with a Keithley 617 Programmable Electrometer which was controlled by an IBM PC. The software used for this was the Keithley DAS Plus 500. This electrometer was chosen for these measurements because of its high impedance (> 200 x 10^{12} ohms) and its high accuracy (about 0.05%) [16]. In order to measure the cell voltage and the voltage from the reference electrode to a half cell, a relay was built. A schematic of the relay circuit is shown in Appendix C.

A program was written using Keithley DAS Plus 500 software to measure the required voltage readings. A flowchart of the program is shown in Figure 8 and the Basic code of the program is listed in Appendix E.

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Figure 8. Flowchart of data acquisition program.

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4.2 Experimental Procedure

All solutions used in this study were prepared from Fisher Scientific analytical grade chemicals and from deionized and distilled water. Ultra-high purity hydrogen and nitrogen from Linde Co. were used.

The hydrobromic acid solution was placed in the storage reservoir, then nitrogen sparged for at least two hours. Then, the acid solution was drawn into the reference electrode holder, and a sample of the HBr solution was taken for titration. (See Appendix F.) Bromine was added to the storage tank, and then the experiment could be started. Before each experiment, the solution was titrated to insure that the bromine concentration was unchanged. (See Appendix F.) The same solution could be used for all experiments involving the same concentrations of hydrobromic acid and bromine.

The complete experimental start up procedure is outlined in Appendix D. The solution was mixed throughout each experiment. During each experiment, voltage measurements were taken across the cell and between the bromine and reference electrodes.

The cell voltage was measured by the electrometer with the hydrogen electrode was common. In the bromine electrode measurements, the bromine electrode was held as common and the potential was measured with respect to a reference electrode. (See wiring diagram in Appendix C.) This procedure allowed correct readings of the magnitude of the potential although the sign convention must carefully be interpreted.

Voltage measurements were taken every second. During the first hour of each experiment, the average value of these measurements was recorded every fifteen seconds. For the remainder of the experiment, the average voltages were recorded every minute. The median time between the reported measurements was also recorded.

4.2.1 Determination of Equilibrium Conditions

Equilibrium was considered to be reached when the recorded cell voltages differed by less than 0.0002V over the past ten minutes. Because of the way in which the program was written, this condition could be met for more than ten minutes before equilibrium was considered to be reached. (See Figure 8.)

After the equilibrium condition was met, the temperature at the cell entrance was placed into the data file by the operator, and a titration was done to verify that the bromine concentration had not changed during the experiment. This was necessary because of the high vapor pressure of bromine.

4.2.2 Measurement of Rates of Solution and Membrane Equilibrium

In order to measure the rates of solution and membrane equilibrium, the hydrobromic acid and bromine

solution in the storage reservoir was spiked with bromine after the equilibrium condition had been met for at least seven minutes. This was done by pouring bromine into the storage flask. The system was then allowed to equilibrate. The transient voltages after the addition of bromine provide information on the rates at which the system reaches equilibrium after the solution concentration is altered.

CHAPTER V

RESULTS AND DISCUSSION

The open circuit voltage of a hydrogen-bromine fuel cell was determined both theoretically and experimentally. These studies were done to determine the effects of electrolyte concentration, type of Nafion membrane, operating temperature, and pressure.

5.1 Computation of Open Circuit Voltage

5.1.1 Calculation Procedure

Computer programs were written to calculate the open circuit potential of a hydrogen-bromine fuel cell using the theoretical expression derived in Chapter III. The algorithm used in these programs is shown in Figure 9, and their FORTRAN listings are given in Appendix B.

These programs, OCV1 and OCVACT, calculate the open circuit voltage of the hydrogen-bromine cell for a given temperature, hydrogen pressure, bromine and hydrobromic acid concentrations. These concentrations can be given in terms of weight percentages or molalities. The programs can calculate the open circuit voltage with or without a Nafion membrane present. If a uni-univalent supporting

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Figure 9. Flowchart of method used to calculate the open circuit voltage of a hydrogen-bromine fuel cell.

electrolyte (e.g., NaBr, KBr) is present in the system, its concentration and molecular weight must also be provided.

If the concentrations are given in weight percentages, the molal concentrations are calculated. Then, the density of the solution-phase electrolyte is determined from a curve fit of the milliequivalents of bromine atoms per gram of water versus solution density data of Glass and Boyle [3]. The equation is

 $\rho = 1.017686873 + 0.04488363995EQ - 0.0004914449546EQ^2 (5-1)$

where

 ρ - solution density (g/cc)

EQ - equivalents of bromide ions, defined by

$$EQ = m_{Br-} + 2m_{Br2} + 3m_{Br3-} + 5m_{Br5-}$$
 (5-2)

where the concentration terms are the molal bromide, bromine, tribromide and pentabromide concentrations. For this correlation it does not matter if the bromine is present as Br^- , Br_3^- , Br_5^- , or Br_2 . For calculation of solution density with a supporting electrolyte present, the assumption is made that the size of the cation is small compared to the size of the bromide ion. This allows the bromide ion of the supporting electrolyte to be included in the solution density calculation.

For systems with a membrane, the fixed anion concentration of the membrane can be calculated using the ion cluster model of Nafion, discussed in Chapter II. Using this model, the fixed ion concentration of the membrane, C_R , is given by [10]

$$C_{R} = \frac{1000d}{EW f_{e}} \frac{f}{f_{w}}$$

where

EW - equivalent weight of the membrane

d_ - density of electrolyte absorbed by the membrane

- f_i fraction of ionic groups in ion clusters
- f_w fraction of electrolyte in ion clusters

Due to the hydrophilic nature of the ionic groups the ratio of f_i/f_w is assumed to be one [10].

For calculation of the fixed anion concentration of the membrane, the density of the electrolyte absorbed in the membrane is assumed to be the same as the density of the solution phase. The weight fraction of the electrolyte absorbed can be determined by an empirical expression given by Yeo and Chin [5]

$$f_{e} = \frac{0.323}{1 + 0.068C_{HBr}}$$
(5-4)

where C_{HBr} is the molarity of the charged bromide species in the solution phase, or the molarity of the hydrobromic

(5-3)

acid given as input to the program. This equation was determined for a system using a Nafion 115 membrane, with an equivalent weight of 1200, and was assumed to be valid for any type of Nafion membrane.

After calculating the fixed ion concentration of the membrane, the hydrogen ion concentration of the membrane can be found using equation (3-47). If no membrane is present in the system, the hydrogen ion concentration used in equation (3-25) is that of the solution phase.

A curve fit of the data of Glass [6] is used to determine whether the bromine concentration in the solution is above the solubility limit. The second order polynomial used to describe this data is

$$CURVE = 0.2526794598 + 1.057577737C_{H+} + 0.0487321524C_{H+}^2$$
 (5-5)

where

CURVE - solubility limit of bromine (molar concentration) C_{H+} - molar hydrogen ion concentration of solution phase

Two liquid phases are present when

$$C_{\rm Bro}$$
 > CURVE (5-6)

If two liquid phases are present, the second phase is considered to be pure bromine, with unit activity, and the equilibrium distribution of the bromide species is found directly from equations (3-37) and (3-38).

If the bromine concentration is below the solubility limit, the bisection method is used to determine the equilibrium bromine concentration from the cubic equation (3-33). This method insures that the root calculated is of a reasonable value. Once the equilibrium bromine concentration is known, the others are easily calculated.

The program OCV1 determines the open circuit potential of a hydrogen-bromine fuel cell using equation (3-25), which neglects activity coefficients of all species. The program OCVACT determines the open circuit voltage of the fuel cell using equation (3-24) using the approximation that

$$\gamma_{HBr}^{\delta} = \gamma_{Br-}^{\delta} = \gamma_{H+}^{\beta}$$
 (5-7)

where γ_{HBr}^{δ} is evaluated at the concentration of charged bromide species in the solution phase. The polynomial used to calculate the hydrobromic acid activity coefficient was determined through a third order curve fit of the activity coefficients given by Balko [2]

$$\gamma_{HBr} = 0.9418152476 - 0.03224218452m_{H+} + 0.045343504m_{H+}^2 + 0.015525929m_{H+}^3$$
 (5-8)

5.1.2 Comparison of Calculations with Literature Data The values calculated from the open circuit voltage equations (3-24) and (3-25) were compared to the values given by G.E. [9]. For these cases, the weight percentages of HBr and Br₂ were calculated two ways. First, it was assumed that the weight of Br₂ was not used in the determination of the given initial and final values of the weight percentages of hydrobromic acid. Second, it was assumed that the weight of bromine was included in the given weight percentages.

The equilibrium voltage was also calculated using the empirical correlation (2-1) and (2-2) of Yeo and Chin [5]. The concentrations used in the calculations were found by the same two methods as described earlier, for comparison of these values to the data of G.E. and the values found by the theoretical expressions, (3-24) and (3-25). The results are tabulated in Table 1 and in Figures 10 through 12, where the 45 degree line signifies where perfect agreement with the reported data would lie.

In general, the values calculated by OCV1 are greater than the data of G.E. or of the correlation of Yeo and Chin. This result was attributed to the fact that OCV1 neglects the activity coefficients, which seems plausible, since this system is of concentrated solutions. For the lower states of charge, the values calculated by OCVACT are lower than the values calculated by OCV1, but larger than

Table 1. Comparison of values calculated from open circuit potential equation to those given by G. E. [9] and values calculated from empirical correlation of R.S. Yeo and D-T. Chin [5]. The temperature is 23 C, pressure is 1 bar for all cases. In the calculations, U^{θ} is taken to be 1.088V according to [17]. Voltages in parantheses include estimated activity coefficients.

Case	Method 1	Method 2	Yeo & Chir	G. E.
Start at 48% HBr	0.976V	0.955V	0.793V (1	L) 0.74V
40% HBr at eq.	(0.876V)	(0.827V)	0.749V (2	2)
Start at 48% HBr	1.157V	1.043V	0.978V (1	L) 0.96V
20% HBr at eq.	(1.151V)	(1.015V)	0.946V (2	2)
Start at 48% HBr	1.183V	1.167V	1.056V (1) 1.20V
10% HBr at eq.	(1.186V)	(1.166V)	1.006V (2	2)
7% HBr 7% Br ₂		1.066V (1.068V)	1.094V	1.02V

(1)
$$X_{HBr} = \frac{W_{HBr}}{W_{HBr} + W_{H}}$$

 $\frac{\text{HBr}}{+ W_{\text{H}_2\text{O}}}$ (2)

(2) $X_{HBr} = \frac{W_{HBr}}{W_{HBr} + W_{Br2} + W_{H2O}}$



Figure 10. Comparison of theoretically determined open circuit voltages using OCV1 and OCVACT to data of G. E. [9], assuming weight of bromine was excluded from given weight fractions.



Figure 11.

Comparison of theoretically determined open circuit voltages using OCV1 and OCVACT to data of G. E. [9], assuming weight of bromine was included in given weight fractions.



Theoretical Expression (volts)

Figure 12. Comparison of theoretically determined open circuit voltages calculated by OCV1 and OCVACT to empirical correlation of Yeo and Chin [5].

the data of G. E. At the higher states of charge, there is little effect from the activity correction. For the highest state of charge, the open circuit voltages calculated by OCV1 and OCVACT are somewhat lower than those measured by G.E.

Figure 12 is a comparison of the open circuit voltages calculated by OCV1 and OCVACT to those calculated by the correlation of Yeo and Chin [5]. At the lowest state of charge, the voltages calculated by OCVACT were lower than the voltages calculated by OCV1, but larger than the values calculated from the correlation of Yeo and Chin. At the high states of charge, where two solution phases are present, the open circuit voltages calculated by OCVACT and OCV1 are nearly equal.

The calculated results of OCVACT provide reasonable estimates considering the fact that the true activity coefficients of bromide ions in this ternary solution are not known, nor are the activity coefficients of hydrogen ion in the Nafion membrane. At high concentrations of hydrobromic acid, the activity coefficients of HBr are large, and might be larger in a solution with bromine present. Also, the activity coefficient of protons in the membrane is unknown. At higher states of charge, the activity coefficient of aqueous hydrobromic acid decreases. At concentrations less than one molal, the activity coefficient of hydrobromic acid is less than unity [18]. In the case of comparing the calculated values with the G.E. data at the high bromine concentration, the calculated values are less than the experimental value of G.E. This may be due to the fact that the equilibrium constants for the bromine complexing reactions are for dilute solutions, and may not be valid in solutions of high bromine concentrations.

The effects of these equilibrium constants were studied through use of the computer program OCKEFF, listed in Appendix B. It allows the open circuit voltage to be calculated using equilibrium constants of the complexing reactions other than those in equations (3-31) and (3-32). The results of this program are shown in Figures 13 and 14. They show that the effects of the equilibrium constants are negligible at low states of charge, where the bromine concentration is small, and increase with increasing bromine concentration. The magnitude of the effect of multiplying or dividing the equilibrium constants by five at 79.2% of charge was about one hundred millivolts.

The open circuit voltages of a hydrogen-bromine fuel cell with no solid polymer electrolyte were calculated for comparison to the values of Glass and Boyle [3] using programs OCV1 and OCVACT. The results are shown in Table 2 and Figure 15. For solutions with high HBr concentrations, the voltages calculated by OCV1 are significantly higher than the data of Glass and Boyle. However, the values



Figure 13. Effects of larger equilibrium constants of complexing reactions on the calculated open circuit voltage using OCV1.

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Figure 14. Effects of smaller equilibrium constants of complexing reactions on the calculated open circuit voltage using OCV1.

უ თ Table 2. Comparison of values calculated from theoretical open circuit potential expression to those found by Glass and Boyle [3] at 30 C, 1 atm. U^{θ} is taken to be 1.084V according to [17]. Voltages in parentheses include estimated activities.

		Calculated from	Glass and
Case		Theory	Boyle
^m HBr	= 11.19	0.940V	0.692V
^m Br2	= 0.478	(0.766V)	
m _{HBr}	= 8.95	0.949V	0.748V
m _{Br} 2	= 0.499	(0.810V)	
^m HBr	= 5.74	0.978V	0.884V
^m Br2	= 0.538	(0.892V)	
^m HBr	= 1.60	1.108V	1.076V
^m Br2	= 2.04	(1.104V)	
^m HBr	= 11.20	0.978V	0.704V
^{mBr} 2	= 3.53	(0.803V)	
^m HBr	= 5.67	1.019V	0.880V
^m Br2	= 3.59	(0.935V)	
^m HBr	= 2.64	1.084V	1.032V
^m Br2	= 3.57	(1.065V)	
^m HBr	= 11.25	0.990V	0.729V
^m Br2	= 6.73	(0.815V)	
m _{HBr}	= 5.68	1.038V	0.895V
m _{Br2}	= 6.97	(0.953V)	
^m HBr	= 6.67	1.032V	0.888V
^m Br2	= 9.01	(0.928V)	



Figure 15. Comparison of open circuit voltages calculated by OCV1 and OCVACT to the data of Glass [3,6].
calculated by OCVACT are much closer to the experimental data. At intermediate bromine concentrations, the results are similar, but the calculated values are in better agreement with the reported data. At high bromine concentrations, the values calculated by both programs approach measured values. This comparison at different states of charge shows that the activity coefficients have a significant effect on the open circuit potential, especially at high HBr concentrations. Also, the agreement between OCVACT estimates and reported data is surprisingly good considering that activity coefficient data for this system are not accurately known.

5.1.3 Effects of Parameters on Open Circuit Voltage

The effects of several parameters on the open circuit voltage of the hydrogen-bromine fuel cell were studied using the program OCV1. The results of these calculations were to help identify which parameters produce a significant effect which could then be experimentally observed using the system described in chapter 4.

The open circuit voltages were calculated for 25, 45, and 75^oC. From equation (3-25) the temperature dependence of the U^{θ} term is given by the equation

 $U^{\theta} = 1.0873 - (T - 298.15) \times 541 \times 10^{-6}$ (5-9)

where

 U^{θ} - standard potential

T - Kelvin temperature

The other terms of (3-25) are also dependent on the temperature. The results of these calculations are shown in Figure 16. The temperature effect is greatest at low states of charge. At high states of charge, the second term of equation (3-25) increases, causing a lesser temperature dependence. An increase in temperature causes a decrease in the open circuit voltage, as predicted by equation (5-9).

The effects of membrane equivalent weight on the open circuit voltage were examined. The results are shown in Figure 17. Membrane equivalent weights of 1100, 1200 and 1500 were studied, using the assumption that equation (5-4) is valid for any type of Nafion membrane. The equivalent weight of the membrane was determined to have little effect on the open circuit voltage.

Also, the effects of varying the hydrobromic acid and bromine concentrations were calculated using OCV1. The results of these studies are shown in Figures 18 and 19. In Figure 18, open circuit voltage is plotted against the bromine concentration with constant hydrobromic acid concentration. For a given hydrobromic acid concentration, the open circuit voltage increases with increasing bromine concentration. Also, the voltages are lower for the



State-of-Charge (%)

Figure 16.

Open Circuit Voltage (volts)

16. Effects of temperature on the open circuit voltage calculated by OCV1 for various statesof-charge.









Figure 18. Semilog plot of effects of bromine concentration on the open circuit voltage calculated by OCV1.





Figure 19. Semilog plot of effects of hydrobromic acid concentration on the open circuit voltage calculated by OCV1.

solutions with higher hydrobromic acid concentrations. The curve for a solution with 10% HBr (1.37 molal HBr) shows that at higher bromine concentrations, the solution forms two phases, causing the bromine concentration to have no effect on the open circuit voltage, since the activity of the bromine is constant with a value of unity.

The step change in the 1.37 molal HBr curve of Figure 18 indicates the presence of a two phase solution, and is an artifact of the method used to define the activity of bromine. Prior to the presence of a second, pure bromine phase in the solution, the majority of the bromine complexed to form tribromide and pentabromide. Therefore, the molality of the bromine after equilibration was significantly less than unity, and was defined to be equal to the bromine activity. When two liquid solution phases where present, the bromine activity was assumed to be unity in calculation of the open circuit voltage, causing the discontinuity in the calculated open circuit voltages.

Figure 19 shows the open circuit voltage as a function of hydrobromic acid concentration for constant bromine concentrations. The open circuit voltage decreases with increasing HBr concentrations. Higher voltages were calculated for the solutions with higher bromine concentrations. Both Figures 18 and 19 reflect the trends expected from the first two terms of (3-25). If complexing of the bromine to form tribromide and pentabromide ions did not occur, these would be the only two terms needed to describe the open circuit voltage. To determine the effects of the complexing reactions on the open circuit voltage, a relationship between the open circuit voltage and the molal hydrobromic acid concentration for a constant bromine concentration was examined. This result should be a line with a slope of -59 mV at 23°C if the effects of the complexing reactions on the open circuit voltage are insignificant.

Table 3 shows the results of a linear regression and r^2 , which represents the goodness of fit of the line, where perfect fit is represented by r^2 equal to one, and a poor fit by r^2 of zero. The results indicate that the complexing reactions are less significant for lower bromine concentrations, and more significant when the bromine concentrations are high. The linearly regressed lines are shown in Figure 19.

The effects of the complexing reactions on the open circuit voltage can also be seen in Figure 18. If complexing reactions of the bromine species do not occur, a plot of the open circuit voltage versus the bromine concentration would give a line with a slope of -30 mV. Table 4 shows the results of a linear regression on the

Table 3. Results of a linear regression of ln(m_{HBr}) versus the open circuit voltage calculated by OCV1 for constant bromine concentrations.

Bromine Concentration	Linear Equation that Describes OCV	r ² Goodness of Fit
7.95%	1.06511-0.052557 ln(m _{HBr}) 0.993450
17.88%	1.09757-0.060954 ln(m _{HBr}) 0.993030
27.82%	1.18477-0.103431 ln(m _{HBr}) 0.944587
37.76%	1.18729-0.098084 ln(m _{HBr}) 0.967060

Table 4. Results of a linear regression of ln(m_{Br2}) versus the open circuit voltage calculated by OCV1 for constant hydrobromic acid concentrations.

Hydrobromic Acid Concentration	Linear Equation that Describes OCV	r ² Goodness of Fit
10% *	1.07171+0.039961 ln(m _{Br2})	0.98124
20%	1.02017+0.027412 ln(m _{Br2})	0.98961
- 3O€	0.98935+0.021273 ln(m _{Br2})	0.99565
40%	0.96601+0.018838 ln(m _{Br2})	0.99717

Regression only includes points prior to the solubility limit of bromine in 10% HBr. calculated open circuit voltages, at concentrations below the solubility limit of bromine in solution, and the goodness of fit parameter, r^2 . These regressions show that due to the complexing reactions, the slope is near 30 mV in the first two cases, however the line fit is not as good, thus indicating that a significant quantity of the bromine complexes to form tribromide and pentabromide.

5.2 Experimentally Determined Open Circuit Voltages

Open circuit voltage measurements were made for four states of charge of solutions with initial charge capacities of 48% and 35% HBr. The effects of pressure and membrane equivalent weights were also studied. Experimental results are tabulated in Appendix H, along with samples of experimental data.

The effects of the membrane types on the open circuit voltage of a hydrogen-bromine fuel cell were determined experimentally. A comparison was made of two type of membranes. They were a Nafion 117 membrane with an equivalent weight of 1100, and a catalyzed Nafion 120 membrane with an equivalent weight of 1200. These membranes were chosen for comparison because, although Nafion 120 is no longer commercially available and has been replaced by Nafion 117, Nafion 120 was the type that was purchased from General Electric with electrodes bonded to it; platinized platinum on the hydrogen side, and a

proprietary noble metal catalyst of Electrochem Inc. on the bromine side.

Figure 20 shows experimental results for the two membrane types at concentrations corresponding to 58.5% state of charge for an electrolyte capacity of 48% HBr. It shows reproducibility within the limits of experimental error. Similar equilibrium voltages for the two systems are predicted. This is because the ratio of the equivalent weights is close to unity in equation (5-3), so the fixed ion concentrations of the membranes are about the same. This means that the difference in the hydrogen ion concentrations of the membrane will be small, having little effect on the open circuit voltage.

Table 5 shows the open circuit voltages determined for a system with a Nafion 117 membrane, a pressure of 2 psig, and room temperature operation. These experiments were done for a 16.7% state of charge of a solution with a capacity of 48% HBr. The open circuit voltages found in these experiments have an average value of 0.733V, with a standard deviation of 0.034V.

Table 5 also shows the results of four experiments done for the same conditions of concentration, temperature and pressure, except the Nafion 120 membrane electrode assembly was used. The average open circuit voltage of these experiments is 0.737V, with a standard deviation of 0.006V. Thus, the effects of different Nafion membranes



Figure 20.

Cell Potential (valts)

 Comparison of experimental results obtained using Nafion 117 membrane (T=26.1C) to those of catalyzed Nafion 120 catalyzed membrane (T=25.5C). The experiments were conducted at 2 p.s.i. and concentrations of 20% HBr and 27.82% Br₂.

Table 5. Open circuit voltages for 16.7% state of charge of solution with an initial charge capacity of 48% HBr. All experiments conducted at room temperature, and pressure of 2 p.s.i. The SPE used in these studies was either a Nafion 117 membrane, or a Nafion 120 membrane electrode assembly.

Membrane	Open Circuit Voltage (V)
Nafion 117	0.745
Nafion 117	0.780
Nafion 117	0.688
Nafion 117	0.719
Nafion 120 MEA	0.744
Nafion 120 MEA	0.740
Nafion 120 MEA	0.732
Nafion 120 MEA	0.731

are negligible, although these experiments appear to be more reproducible than those with the Nafion 117 membrane.

The reason for less reproducible data with the Nafion 117 system could be related to slow deactivation of the platinized platinum electrode in that system. (e.g., caused by the dry environment). The high surface area platinum catalyst on the Nafion 120 membrane is less likely to deactivate. Also, the precious metal catalyst on the bromine side of the Nafion 120 membrane may keep bromine species from diffusing across the separator. Therefore, deactivation of the platinum hydrogen electrode in the Nafion 120 system is less likely.

Experiments were also done to determine the magnitude of the effects of the hydrogen pressure and the bromide solution pressure on the open circuit voltage. This was accomplished by altering the hydrogen or bromine pressure during an experiment; 2 psig to 4 psig. The effects of altering the hydrogen pressure are shown in Figure 21. The results show that for pressure increases, the voltage sharply rises a couple of millivolts, then falls to a value higher than that prior to the change. When the pressure is reduced to 2 psig, the voltage drops a few millivolts, then rises rapidly to a value less than that before the change.

The effect of pressure changes in the aqueous electrolyte for one experiment is shown in Figure 22.



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Figure 21. Effects of altering hydrogen pressure during an experiment conducted at 27C, solution pressure of 2 p.s.i. and concentrations of 10% HBr and 7.95% Br₂.

Potential Across Celi (volts)

1.028



Figure 22. Effects of altering solution pressure during an experiment conducted at 27C, hydrogen pressure of 2 p.s.i. and concentrations of 10% HBr and 7.95% Br₂.

The effects of liquid pressure changes are not as pronounced as for those of the hydrogen. When the solution pressure is increased, the voltage increases slightly, then oscillates to a value close to that prior to the change. For a decrease in the pressure, the voltage decreases slightly, then oscillates to a value close to that prior to the change. In one of the experiments, equilibrium was reached, even though the solution pressure was being altered.

A detailed analysis of the effects of altering the half cell pressures during operation is beyond the scope of this research. However, the theoretical expression (3-24) does not depend on the bromine pressure, so the effect of changing the solution pressure value is expected to be negligible, as was shown. Since the hydrogen pressure is a term in the expression, the effect of altering this value is expected to be more significant, and this was shown to be true.

The effect of the hydrogen pressure on the open circuit potential of the hydrogen-bromine cell at 16.7% state of charge was determined for three pressures. The open circuit voltage of the cell was plotted against the log of the square root of the pressure. The resulting graph should be a line with a positive slope of 30 mV/atm. This plot is shown in Figure 23, which shows that a regression would be meaningless. Because the experimental



Figure 23.

 Semilog plot of effects of hydrogen pressure on the open circuit potential. Experiments were conducted at room temperature, concentrations of 40% HBr and 7.95% Br₂. inaccuracies involved in measuring the open circuit potential of this system, are on the order of the differences expected due to the pressures studied, this trend could not be detected. However, due to safety considerations, operation at higher pressures was not attempted. Therefore, the remainder of the experiments were conducted at a pressure of 2 psig. Also, due to safety considerations, all experiments were conducted at room temperature.

The experimentally determined open circuit voltages of hydrogen bromine fuel cells with initial charge capacities of 48% and 35% are given in Tables 6 and 7. Although the experiments were not completed at the same temperature, the expected effect of the temperature difference on the open circuit voltage is less than 3 mV., and was considered to be insignificant.

The mean experimental values and the error incurred in the estimation of the mean within a 95% confidence interval [19] are shown in Figure 24. Note that the results of the experiments with a charge capacity of 35% HBr are much more reproducible than those with an electrolyte capacity of 48% HBr.

For both the 35% HBr and 48% HBr electrolyte capacity solutions, the 79.2% state of charge electrolyte was a two phase liquid, where the second phase is considered to be pure bromine. For these experiments at

Table 6. Open circuit potentials determined experimentally for an electrolyte capacity of 35% HBr, Nafion 120 membrane electrode assembly, room temperature, 2 p.s.i. Reported error is that in estimation of mean within a 95% confidence level.

State-of-Charge (१)	N	Mean (V)	Error (V)
16.7	· · · · · · · · · · · · · · · · · · ·	0.854	0.001
37.5	2	0.916	0.000
58.5	3	0.988	0.001
79.2	2	1.107	0.013
•			

N = number of experimental values

All experiments were done at a pressure of 2 psig, and temperatures between 23.7 and 25.4 C.

Table 7. Open circuit voltages determined experimentally for an electrolyte capacity of 48% HBr, room temperature, and 2 p.s.i. Reported error is the error incurred in estimation of the mean within a 95% confidence interval.

State-of-Charge (१)	Membrane (Nafion)	N	Mean (V)	Error (V)
16.7	120 MEA	4	0.737	0.009
16.7	117	· · 4 · ·	0.733	0.054
37.5	120 MEA	3	0.802	0.023
58.5	120 MEA	2	0.897	0.022
58.5	117	1	0.898	
79.2	120 MEA	2	1.068	0.000

For all experiments, the pressures were 2 psig, and the temperatures were 24.4 C to 27.4 C.



Open Circuit Voltage (volts)

Figure 24. Estimated means of experimental results for experiments with Nafion 120 catalyzed membrane. Error incurred in estimation of mean is in the 95% confidence interval [19].

the 48% capacity electrolyte, equilibrium was not reached, although the voltage stayed fairly constant at 1.068V, but then began to decline. See Figure 25. In one experiment for the 79.2% state of charge determined from a 35% HBr solution, equilibrium appeared to be reached at 1.108V. However, in the other experiment, the voltage stayed constant for several minutes at 1.106V, then began to decline.

Because this is the only state of charge where equilibrium was not achieved, the cause may be related to the presence of a two phase electrolyte, or perhaps catalyst deactivation due to the high bromine concentration. These experiments suggest that the more concentrated solutions are not as stable as the less concentrated solutions.

5.3 Comparison of Experimental Data to Previously Reported and Theoretical Open Circuit Voltages

The open circuit voltages predicted by others and the theoretical expression were compared to the results measured experimentally in this research.

Figure 26 is a comparison between the experimentally measured open circuit voltage of this work and the open circuit voltage reported by G.E. [9]. This comparison is made assuming that the weight fractions of HBr that correspond to the reported open circuit voltages included the weight of bromine in the solution. The 45 degree line



Figure 25. Results of an experiment to determine open circuit voltage of a solution of 10% HBr, 37.76% Br₂, pressure of 2 p.s.i., and Nafion 120 catalyzed membrane.

Cell Potential (volts)



Figure 26.

 $\left(-\frac{1}{2}\right)$

G.E. OCV (volts)

Comparison of experimental results to the open circuit voltages reported by G. E. [9]. represents perfect agreement between the data of G.E. and the open circuit voltages measured here. The values reported by G.E. are greater than those determined experimentally. This could be due to the reported HBr fractions not including the weight of bromine.

Figures 27 and 28 are comparisons of the open circuit voltages measured experimentally to those calculated from the semi-empirical correlation of Yeo and Chin [5] for solutions with initial charge capacities of 35% HBr and 48% HBr. The correlation predicts somewhat greater open circuit voltages than those found experimentally at the lower states of charge. At the highest state of charge, the open circuit voltage predicted by Yeo and Chin was less than that found experimentally. These differences are thought to be due to the absence of bromine in the experiments performed by Yeo and Chin [8] when developing their correlation (2-1); they treated the bromine effects theoretically. Their correlation also neglected the effects of tribromide and pentabromide formation.

Figures 29 and 30 show a comparison of the experimentally measured open circuit voltages to the calculated values for cells with initial charge capacities of 35% and 48% HBr. The voltages calculated by neglecting the activity coefficients (program OCV1) are greater than the measured values. At the lower states of charge



Figure 27.

Comparison of experimental results for solutions with charge capacity of 35% HBr to open circuit voltages determined by correlation of Yeo and Chin [5].



Figure 28. Comparison of experimental results for solutions with charge capacity of 48% HBr to open circuit voltages determined by correlation of Yeo and Chin [5].



Figure 29. Comparison of open circuit voltages calculated by OCV1 and OCVACT to those found experimentally for solutions with a charge capacity of 35% HBr.



Figure 30.

Calculated OCV (volts)

Comparison of open circuit voltages calculated by OCV1 and OCVACT to those found experimentally for solutions with a charge capacity of 48% HBr.

program OCVACT, with estimated HBr activity coefficients, calculates voltages closer to those found experimentally. However, the agreement is not as good as shown earlier in comparison to the data of Glass, (section 5.1.2). This indicates that the uncertainty of accounting for activity of protons in the membrane may be the cause of the discrepancy. As the state of charge increases, the effects of the activity coefficients decrease, so at the highest state of charge, the voltages calculated by OCVACT are actually greater than those found experimentally.

These comparisons accentuate the fact that knowledge of the actual bromine, hydrogen ion, and bromide ion activity coefficients are necessary for a theoretical expression to accurately predict the open circuit voltages of a hydrogen bromine fuel cell.

5.4 Rates of Solution and Membrane Equilibrium

To qualitatively determine the rates of solution and membrane equilibrium, experiments were done where additional bromine was added to the solution after equilibrium was practically reached. The resulting transient voltages across the cell and of the bromine electrode relative to a reference electrode were analyzed. The cell voltages during these experiments are shown in Figure 31. These experiments were conducted for 16.7% state of charge for a solution with a capacity of 35% HBr.



Figure 31.

 Results of experiments where bromine was added to solution near equilibrium for initial solution concentration of 29.17% HBr, 5.78% Br₂. Final solution concentration was 27.58% HBr, 10.93% Br₂.

For about the first minute after the bromine addition, the increases in the voltage across the cell and the voltage of the bromine electrode relative to the reference electrode were equal. Figure 32 is a plot of the transient voltages (potential minus the potential prior to bromine addition). The short-time transient may be due to mixing effects and kinetic effects of formation of bromide complexes.

Then, the transient potential difference of the bromine electrode began to increase faster than the transient potential difference across the cell. After several minutes, the transient potential difference of the bromine electrode was two millivolts higher than the transient potential difference across the cell. This difference is believed to be due to the liquid junction between the solution and the membrane.

The junction potential is caused by the difference of electrochemical potentials for an ionic species between the solution phase and the membrane phase. This is caused by the diffusion of ions in the membrane. The cause, magnitude and time dependence of this effect cannot be verified theoretically without knowledge of the transport properties in the membrane [20].

Figure 33 is a plot of the rate of the voltage changes after the addition of the bromine. It shows that the rate of cell and bromine electrode transient potentials



Figure 32. Transient voltages after addition of bromine.





Céll Voltage





Slopes of transient voltages after addition of bromine. Figure 33.

Time (minutes)
are equal during the first minute. This suggests that the membrane does not act as a capacitor, otherwise there would be evidence of a time delay in the cell potential.

CHAPTER VI

SUMMARY

6.1 Conclusions

The following conclusions based on this research can be made:

1. An expression was derived for predicting the open circuit voltage of a hydrogen-bromine fuel cell and is useful for assessing the effects of various parameters.

2. Analysis of the literature data and this data suggests that proton activity in the membrane may have a significant influence on the open circuit voltage.

3. Knowledge of the actual activity coefficients, especially of protons in the membrane, should improve the agreement between the predicted and actual open circuit voltages.

4. The effects of the complexing reactions, in which tribromide and pentabromide ions are formed from the bromide ions and bromine, are significant at high states of charge, so that knowledge of the equilibrium constants of these reactions may improve the prediction of the open circuit voltage at higher states of charge.

5. The effect of membrane type was determined experimentally using Nafion 117 and Nafion 120, the latter

having electrode materials bonded to it. Although the mean open circuit voltages found using these two systems were similar (0.733V and 0.737V, respectively), the error in the measurements taken with the Nafion 120 membrane electrode was considerably less (\pm 0.054V for Nafion 117 vs. \pm 0.009V for Nafion 120, respectively).

6. The effect of fluctuations in hydrogen pressure on the open circuit voltage was found to be significant. The effects of pressure on the bromide solution were found to be negligible.

7. The open circuit voltages for solutions with a charge capacity of 48% HBr have a lower open circuit voltage (order of 100 mV) than those found for solutions with a charge capacity of 35% HBr. This means that there is a trade off between the open circuit voltage and the charge capacity.

8. The effect of operating temperature was determined theoretically. The open circuit voltage decreases with increasing temperature. The magnitude of this temperature effect is greatest at low states of charge, and is considerably less at high states of charge.

9. The variables which were found to have a significant effect on the open circuit voltage through either experimental or theoretical study are: hydrogen pressure, temperature, hydrobromic acid and bromine concentrations.

6.2 Recommendations

The following recommendations can be made:

1. Experimental work should be done to measure the activity of protons in Nafion membranes in contact with concentrated aqueous hydrobromic acid and bromine solutions.

2. Experimental work should be done to measure the activity coefficients of bromide ion and bromine in aqueous hydrobromic acid and bromine solutions within the concentration ranges of interest for this energy storage system.

3. The equilibrium constants of the complexing reactions of bromide ions and bromine to form tribromide and pentabromide ions should be experimentally measured in these concentrated solutions.

4. After acquiring necessary experimental thermodynamic data of this system, the expression for predicting the open circuit potential of the hydrogen-bromine fuel cell should be tested rigorously and refined to account for concentrated solution behavior.

5. Experimental work should be done to measure the effects of larger hydrogen pressures and higher operating temperatures on the hydrogen-bromine fuel cell.

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APPENDICES

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APPENDIX A

<u>COMPUTER PROGRAM TO CALCULATE OCV FROM EMPIRICAL</u> <u>CORRELATION OF YEO AND CHIN [5]</u>

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list 10 C PROGRAM YEO AND CHIN 20 C 30 C PROGRAMMER: SHARON FRITTS 40 C 50 C THIS PROGRAM CALCULATES THE OCV OF THE H2-BR2 BATTERY USING THE CORRELATION OF R.S. YEO AND D-T. CHIN. THE INPUTS TO THIS PROGRAM 60 C ARE THE TEMPERATURE, H2 PRESSURE AND WIEGHT PERCENTAGES OF HBR AND 70 C 71 C BR2 72 C REAL MBR2, MHBR 80 90 WRITE (6.100) 100 FORMAT(5X, 'WEIGHT PERCENTAGE OF HBR') 100 READ (5,*) XHBR 110 120 WRITE (6,101) 101 FORMAT(5X, 'WEIGHT PERCENTAGE OF BR2') 130 READ (5,*) XBR2 140 150 WRITE (6,102) 160 102 FORMAT(5X, 'TEMPERATURE, CENTIGRADE') READ (5,*) T 170 180 WRITE (6,103) 190 103 FORMAT(5X, 'HYDROGEN PRESSURE') READ (5,*) PH2 200 210 C 22Ø C CALCULATE HBR AND BR2 MOLALITIES TO CALCULATE DENSITY THEN CALCULATE MOLARITIES 230 C 240 C 25Ø MBR2=1000*XBR2/(159.818*(100-XBR2)) 260 MHBR=1000*XHBR/(80.917*(100-XHBR)) 27Ø EQ=2*MBR2+MHBR CENS=1 -0 04983275934*EQ+0 08197743373*EQ**2-0.02473400994*EQ**3 28Ø &+0.003635063042*EQ**4-0 0002914127657*EQ**5+0 00001296501373*EQ 290 &**6-3.001481576E-7*EQ**7+2.817081558E-9*EQ**8 300 31Ø CHBR=1000*DENS*MHBR/(1000+80.917*MHBR) CBR2=1000*DENS*MBR2/(1000+159 818*MBR2) 320 33Ø R=8.3143 340 T=T+273 35Ø F=96487 36Ø C 37Ø C CHECK TO SEE JF BR2 IS SEPARATE PHASE 38Ø C 39Ø CURVE=0.08733789318+2.394484059*CHBR-4.445906568*CHBR**2+ 400 \$7.722716276*CHBR**3-7 ØØ1672287*CHBR**4+3.348377237*CHBR**5-&0.7771662813*CHBR**6+0.05887092684*CHBR**7+.002968743831*CHBR**8 410 420 JF((CBR2-CURVE).GE.Ø) ABR2=1 430 IF ((CBR2-CURVE).LT.0) ABR2=CBR2*1000/(1000*DENS-159.8*CBR2) 431 C 432 C THIS CORRELATION USES WEIGHT FRACTIONS OF HBR EXCLUDING THE WEIGHT OF BROMINE, SO A NEW WEIGHT FRACTION OF HBR IS CALCULATED. 433 C 434 C 435 XH2O=100-XHBR-XBR2 XHBR=100*XHBR/(XH2O+XHBR) 436 VAL=ALOG(12 36*XHBR/100/(1-XHBR/100)) 440 45Ø IF((XHBR/100) LT 0 11) PHJ=1.073-0 0567*VAL **46**Ø IF((XHBR/100).GE.0.11.AND.(XHBR/100).LT.0.28) PHI=1.095-.1042*VAL IF((XHBR/10C) GE 0 28) PHI=1.336-0.2581*VAL 47Ø OCV=PHJ-(T-298)*(4.3+1 86*VAL)*1E-4+4.31E-5*T*ALOG(PH2*ABR2) 480 49Ø WRITE (6.105) ABR2 105 FORMAT(5X, 'BROMINE ACTIVITY', F6 3) 500 510 WRITE (6.106) OCV 52Ø 106 FORMAT(5X, 'OPEN CIRCUIT VOLTAGE IS', F8.4) 530 END

Example Output of YEO

run YEO Ø1/Ø2/86 13:27 42 WEIGHT PERCENTAGE OF HBR 74Ø WEIGHT PERCENTAGE OF BR2 77.95 TEMPERATURE, CENTIGRADE 723 HYDROGEN PRESSURE 71 BROMINE ACTIVITY Ø 54Ø OPEN CIRCUIT VOLTAGE IS Ø 8543 STOP TIME Ø.1 SECS

APPENDIX B

FORTRAN LISTINGS OF OCV1, OCVACT AND OCKEFF

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list
  10 C
            OCV1
  20 C
  30 C
            PROGRAMMER:
                         SHARON FRITTS
  40 C
            THIS PROGRAM CALCULATES THE OPEN CIRCUIT POTENTIAL OF THE HYDROGEN-
  50 C
  60 C
            BROMINE CELL FOR A GIVEN TEMPERATURE, HYDROGEN PRESSURE,
                                                            IT ALSO INCLUDES THE
  70 C
            BROMINE AND HYDROGEN BROMIDE CONCENTRATION.
            EFFECTS OF A SUPPORTING ELECTROLYTE, IF PRESENT. IF A MEMBRANE
  80 C
  90 C
             IS PRESENT. THE DONNAN EFFECTS ON THE HYDROGEN ION CON-
 100 C
            CENTRATION IS USED IN THE EXPRESSION.
 110 C
 120
            REAL MBR2, MHBR, HBR, NERNST, MSE
            WRITE (6,99)
 130
        99 FORMAT(2X, 'TEMPERATURE, C')
READ (5,*) T
 140
 150
 160
            WRITE (6,100)
       100 FORMAT(2X,'HYDROGEN PRESSURE, ATM')
    READ (5,*) PH2
 170
 180
 190
            WRITE (6,101)
 200
        101 FORMAT(2X,'IF THE CONCENTRATIONS OF BR2 AND HBR ARE GIVEN IN')
            WRITE (6,102)
 210
 220
        102 FORMAT(2X, WEIGHT PERCENT, INPUT 1; IF THEY ARE IN MOLALITY, ')
            WRITE (6,103)
 2 3Ø
        103 FORMAT(2X, 'INPUT 2.')
 240
 25Ø
            READ (5,*) I
        WRITE (6,104)
104 FORMAT(2X,'BROMINE CONCENTRATION')
 26Ø
 270
 280
            READ (5,*) BR2
       WRITE (6,105)
105 FORMAT(2X, 'HYDROGEN BROMIDE CONCENTRATION')
 29Ø
 300
            READ (5,*) HER
 310
            WRITE (6,122)
 320
        122 FORMAT(2X, 'JS MEMBRANE PRESENT? (1 FOR YES, Ø FOR NO)')
 33Ø
 340
            READ (5,*) J
            JF (J.EQ.0) GO TO 11
 350
 36Ø
            WRITE (6,123)
        123 FORMAT (2X, 'MEMBRANE EQUIVALENT WEIGHT')
 37Ø
            READ (5,*) EW
 38Ø
        11 WRITE (6,115)
 390
 400
        115 FORMAT(2X, 'CONCENTRATION OF SUPPORTING ELECTROLYTE, MOLARITY')
            READ (5,*) SE
 410
 420
            IF (SE.EC.Ø.) GO TO 10
 430
            WRITE (6,120)
        120 FORMAT(2X 'SUPPORTING ELECTROLYTE')
 440
            READ (5,121)
 450
 46Ø
        121 FORMAT(A5)
 470
            WRJTE (6,116)
        116 FORMAT(2X, 'MOLECULAR WEIGHT OF SUPPORTING ELECTROLYTE')
 480
 490
            READ (5,*) WT
 500 C
 510 C
            THE CONSTANTS ARE DEFINED
 520 C
 53Ø
         10 R=8.3143
            T = 273.15 + T
 540
            F = 96487.
 55Ø
 560
            JF (J.EQ.1) GO TO 1
            JF (J.EQ.2) GO TO 2
 570
 580 C
            FOR THE COMCENTRATIONS GIVEN IN WEIGHT PERCENTAGES. THE
 590 C
            MOLALITIES OF HER AND BR2 ARE FOUND FOR USE IN LATER CALCULATIONS
 600 C
 610 C
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62Ø 1 XBR2=BR2 XHBR=HBR 63Ø 640 XSE=SE MBR2=1000*XBR2/(159.818*(100.-XBR2)) 650 MHBR=1000*XHBR/(80.917*(100.-XHBR)) 66Ø 67Ø IF(XSE.EQ.Ø) GO TO 3 MSE=1000*XSE/(WT*(100.-XSE)) 68Ø 69Ø GO TO 3 700 C 710 C FOR THE CONCENTRATIONS GIVEN IN MOLALITIES, THE CONCENTRATIONS 72Ø C ARE FOUND IN WEIGHT PERCENTAGES FOR USE IN LATER CALCULATIONS 73Ø C 74Ø 2 MBR2=BR2 MHBR=HBR 75Ø 76Ø MSE=SE 77Ø XHBR=100.*80.917/(1000.+MHBR*80.917) 78Ø C 79Ø C THE EQUIVALENTS OF BROMINE ATOMS PER KG SOLUTION ARE FOUND FOR USE IN CALCULATION OF THE SOLUTION DENSITY USING A SECOND 800 C 81Ø C ORDER POLYNOMIAL CURVE FIT OF THE DATA OF GLASS AND BOYLE, "PERFORMANCE OF HYDROGEN BROMINE FUEL CELLS", FUFL CELL SYSTEMS, 82Ø C ACS ADVANCES IN CHEMISTRY SERIES #47, P.203, (1965). 830 C 840 C 850 3 EQ=2*MBR2+MHBR+MSE 86Ø DENS=1.017686873+0.04488363995*EQ-4.914449546E-4*EQ**2 870 C 880 C THE MOLAR CONCENTRATIONS OF THE SOLUTION ARE CALCULATED AFTER. 890 C THE DENSITY OF THE SOLUTION IS KNOWN 900 C 910 CHBR=1000.*DENS*MHBR/(1000.+80.917*MHBR) CBR2=1000.*DENS*HBR2/(1000.+159.818*NBR2) 920 930 CSE=1000.*DENS*MSE/(1000.+WT*MSE) 940 CH=CHBR 950 C IF A MEMBRANE IS PRESENT IN THIS CELL, SOME EXTRA CALCULATIONS 960 С REQUIRED. THEY ARE, THE WEIGHT FRACTION OF ELECTROLYTE ABSORBED 97Ø C 980 C BY THE MEMBRANE, THE FIXED ANION CONCENTRATION OF THE MEMBRANE, 990 C THE HYDROGEN ION CONCENTRATION IN THE MEMBRANE, AND ITS ACTIVITY 1000 C IF NO MEMBFANE IS PRESENT, THESE CALCULATIONS ARE SKIPPED. 1010 C 1020 IF (J.EQ.8) GO TO 6 1030 C 1040 C THE WEIGHT FRACTION OF THE ELECTROLYTE ABSORBED BY THE MEMBRANE WAS EMPJRICALLY DETERMINED AS A FUNCTION OF THE MOLAR CONCENTRATION 1050 C BY R.S. YEO AND D-T. CHIN IN "A HYDROGEN-BROMINE CELL FOR ENERGY 1060 C STORAGE APPLICATIONS," J. ELECTROCHEM. SOC., 127, P. 549 (1980) 1070 C 1080 C 1090 WTF=0.323/(1+0.068*CHBR) 1100 C THE FIXED ANION CONCENTRATION OF THE MEMBRANE IS CALCULATED BY 1110 C AN EQUATION REPORTED BY R.S. YEO, "JON CLUSTERING AND PROTON TRANSPORT IN NAFION MEMBRANES ..." J. ELECTROCHEM. SOC., 130, 1120 C 1130 C P.533, (1983) 1140 C 1150 C 1160 CR=1000.*LENS/WTF/EW 1170 C 1180 C THE HYDPOGEN JON CONCENTRATION IN THE MEMBRANE JS CALCULATED FROM AN EQUATION DERIVED THROUGH USE OF DONNAN PRINCIPLES, AND THE 1190 C ACTIVITY OF THE HYDROGEN ION IS FOUND FOR USE IN THE NERNST 1200 C EXPRESSION 1210 C 1220 C

CHM=(CR+SQRT(CR**2+4*(CH+CSE)**2))/2*CH/(CH+CSE) 1230 AHM=CHM*1000/(1000*DENS-1.008*CHM) 1240 1250 WRITE (6,112) CHM 112 FORMAT (/2X, 'MEMBRANE PROTON CONCENTRATION', F8.4, ' MOLES/LITER') 1260 1270 GO TO 7 128Ø C 129Ø C IF NO MEMBRANE IS PRESENT. THE ACTIVITY OF THE HYDROGEN ION IN THE 1300 C SOLUTION PHASE IS FOUND FOR USE IN THE NERNST EXPRESSION 131Ø C 6 AHM=CH*1000/(1000*DENS-1.008*CH) 132Ø 1330 C 1340 C THESE CALCULATIONS DETERMINE WHETHER THE BROMINE CONCENTRATION IS ABOVE THE SOLUBILITY LIMIT, USING A CURVE FIT OF THE DATA OF GLASS, "HYDROGEN-BROMINE FUEL CELL", IONICS, INC., CAMBRIDGE, MASS., 135Ø C 136Ø C 137Ø C CONTRACT NO. AF19(604)-8508, (1964) 138Ø C 7 CURVE=0.2526794598+1.057577737*CH+0.0487321524*CH**2 1390 1400 С IF THE DATA IS BELOW THE SOLUBILITY LIMIT, THE EQUILIBRIUM BROMIDE 1410 C COMPOUND CONCENTRATIONS MUST BE DETERMINED BY THE BISECTION METHOD 1420 C 1430 C WHICH SOLVES THE CUBIC EQUATION FOUND THROUGH COMBINATION OF THE REACTION EQUILIBRIUM CONSTANTS AND ELECTRONEUTRALITY CONDITIONS. 1440 C 145Ø C THE EQUILIBRIUM CONCENTRATIONS CAN BE EASILY FOUND IF THE BROMINE CONCENTRATION IS ABOVE THE SOLUBILITY LIMIT. THROUGH USE OF THE 1460 C EQUILIBRIUM CONSTANTS OF THE COMPLEXING REACTIONS. 1470 C 1480 C 1490 IF((CBR2-CURVE).LT.0) GO TO 4 1500 ABR2=11510 WRITE (6,200) 200 FORMAT(2X/2X, 'BROMINE IS IN SEPARATE PHASE') 1520 153Ø CBREQ=(CH+CSE)/57 1540 CBR3EC=16*CBREO155Ø CBR5EQ=40*CBREQ 1560 CBR2EQ=CURVE 1570 GO TO 5 1580 4 CALL BISECT(CBR2, CH, CBR2EQ, CSE) CBREQ=(CH+CSE)/(1.0+16.*CBR2EQ+40.*CBR2EQ*CBR2EQ)1590 1600 CBR3EQ=16.*CER2EQ*CBREQ CBR5EC=40.*CBREQ*CBR2EQ*CBR2EQ 1610 ABR2=CBR2EQ*1000/(1000*DENS-159.818*CBR2EQ) 1620 1630 C THE POTENTIAL EVE TO COMPLEXING OF THE BROMIDE IONS AND BROMINE 1640 C 1650 C TO FORM TRIBROMIDE AND PENTABROMIDE LONS IS FOUND 1660 C 1670 5 SUM=CBR2E0+CBR3E0+CBR5EC 1680 COMP=0.5*(CDR3EO/SUM*R*T/F*(ALOG(16.))+0.5*CBR5EQ/SUM*R*T/F*(ALOG(1690 £4Ø.))) 1700 C 1710 C THE ACTIVITY OF THE BROMIDE ION IS FOUND, AND THE NERNST POTENTIAL 1720 C IS CALCULATED, USING THE STANDARD POTENTIAL OF 1.0873-541E-6*(T-298.15) GIVEN BY MILAZZO AND CAROLI, TABLES OF STANDARD ELECTRODE 1730 C 1740 C POTENTIALS, WILEY, NY, 1977, P.284-5. 1750 C ABR=CBREO*1000/(1000*DENS-79.909*CBREC) 1760 NERNST=1.0873+ALOG(SCRT(2H2)*SQRT(ABR2)/AHM/ABR)*R*T/F+(T-298.15)* 1770 1780 &(-541E-6) 1790 C THE OUTPUT OF THE PROGRAM IS GIVEN . 1800 C 1810 C 1820 WRITE (6,106) DENS 106 FORMAT(2X/2X, 'DENSITY OF DELTA PHASE', F10,6, ' G/ML') 1830

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1840 WRITE(6,107) CBR2EQ 1850 107 FORMAT(2X, 'EQUILIBRIUM BROMINE CONCENTRATION', F9.6, ' MOLES/LITER') WRITE (6,108) CBREQ 1860 187Ø 108 FORMAT(2X, 'EQUILIBRIUM BROMIDE CONCENTRATION', F9.6, ' MOLES/LITER') 1880 WRITE(6,109) CBR3EQ 109 FORMAT(2X, 'EQUILIBRIUM TRIBROMIDE CONCENTRATION', FIG.6, ' MOLES/LIT) 1890 &ER') 1900 1910 WRITE (6,110) CBR5EQ 110 FORMAT(2X, 'EQUILIBRIUM PENTABROMIDE CONCENTRATION', FI0.6,' MOLES/L) 192Ø &ITER') 1930 WRITE (6,111) NERNST 1940 1950 111 FORMAT(2X, 'NERNST POTENTIAL', F10.6, ' VOLTS') WRITE(6,113) COMP 1960 113 FORMAT(2X, 'POTENTIAL DUE TO COMPLEX FORMATION', F10.6, ' VOLTS') 1970 1980 TOTAL=NERNST+COMP 1990 WRITE (6,114) TOTAL 114 FORMAT(2X, 'TOTAL POTENTIAL', F10.6.' VOLTS'/) 2000 2010 END 2020 C 2Ø3Ø C THIS SUBROUTINE USES THE BISECTION METHOD TO DETERMINE THE EQUILIBRIUM BROMINE CONCETRATION WHICH IS THE ROOT OF A CUBIC 2040 C 2050 C EXPRESSION 2060 C SUBROUTINE BISECT (CBP2, CH, CBR2EQ, CSE) 2070 2080 REAL MID 2090 A=0. 2100 B=2. FA=2*CBR2 -2110 2120 1 MID=(A+B)/2.FM=2.*CBR2+(32.*CBR2-32.*CH-32.*CSE-2.)*MJD+(80.*CBR2-160.*CH-32. 2130 C-160.*CSE)*MID**2-80*MID**3 2140 2150 JF (FA*FM.LE.U.) GO TO 2 2160 A=MJ.D 2170 FA=FM 2180 GC TO 3 2190 2 B=MJD 3 IF (AES(E-A).LE.0.000001) GO TO 4 2200 2210 GO TO 1 2220 4 CBR2EQ= $(\Lambda + E)/2$ RETURN 2230 2240

END

Example Output of OCV1

run OCV1 Ø1/02/86 13:07:41 TEMPERATURE, C 223 HYDROGEN PRESSURE. ATM 71 IF THE CONCENTRATIONS OF BR2 AND HBR ARE GIVEN IN WEIGHT PERCENT. INPUT 1. IF THEY ARE IN MOLALITY INPUT 2. 71 BROMINE CONCENTRATION 27 95 HYDROGEN BROMIDE CONCENTRATION 240 IS MEMBRANE PRESENT? (1 FOR YES Ø FOR NO) 71 MEMBRANE EQUIVALENT WEIGHT ?1200 CONCENTRATION OF SUPPORTING ELECTROLYTE MOLARITY 20 MEMBRANE PROTON CONCENTRATION 10 0001 MOLES/LITER DENSITY OF DELTA PHASE 1 391439 G/ML EQUILIBRIUM BROMINE CONCENTRATION Ø ØØ6682 MOLES/LITER EQUILIBRIUM BROMIDE CONCENTRATION 6 204001 MOLES/LITER EQUILIBRIUM TRIBROMIDE CONCENTRATION Ø 663274 MOLES/LITER EQUILIBRIUM PENTABROMIDE CONCENTRATION 0 011080 MOLES/LITER NERNST POTENTIAL Ø.920367 VOLTS POTENTIAL DUE TO COMPLEX FORMATION 0 034837 VOLTS TOTAL POTENTIAL Ø 955205 VOLTS

STOP TIME Ø 2 SECS

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list 10 C OCVACT 20 C PROGRAMMER: SHARON FRITTS 3Ø C 40 C THIS PROGRAM CALCULATES THE OPEN CIRCUIT POTENTIAL OF THE HYDROGEN-50 C BROMINE CELL FOR A GIVEN TEMPERATURE, HYDROGEN PRESSURE, 60 C BROMINE AND HYDROGEN BROMIDE CONCENTRATION. IT ALSO INCLUDES THE 7Ø C 80 C EFFECTS OF A SUPPORTING ELECTROLYTE, IF PRESENT. IF A MEMBRANE IS PRESENT THE DONNAN EFFECTS ON THE HYDROGEN LON CONCENTRATION 90 C 100 C IS USED IN THE EXPRESSION. ESTIMATES OF ACTIVITY COEFFICIENTS 110 C OF HBR ARE INCLUDED. 120 C 130 IMPLICIT REAL (A-H,O-Z) DOUBLE PRECISION MBR2, MHBR, MBR, NERNST, MSE 140 WRITE (6,99) 150 99 FORMAT(2X, 'TEMPERATURE, C') 160 READ (5,*) T 170 WRITE (6,100) 180 190 100 FORMAT(2X, 'HYDROGEN PRESSURE, ATM') 200 READ (5,*) PH2 210 WRITE (6,101) 101 FORMAT(2X, 'IF THE CONCENTRATIONS OF BR2 AND HBR ARE GIVEN IN') 220 230 WRJTE (6,102) 240 102 FORMAT(2X, WEIGHT PERCENT, INPUT 1; IF THEY ARE IN MOLALITY, ') 25Ø WRITE (6,103) 26Ø 103 FORMAT(2X, 'JNPUT 2.') READ (5,*) I 27Ø WRITE (6,104) 280 290 104 FORMAT(2X, 'BROMINE CONCENTRATION') 300 READ (5,*) ER2 31Ø WRITE (6,105) 105 FORMAT(2X, 'HYDROGEN BROMIDE CONCENTRATION') 320 3 3Ø READ (5,*) HER WRITE (6,122) 340 122 FORMAT(2X, 'IS MEMBRANE PRESENT? (1 FOR YES, Ø FOR NO)') 35Ø READ (5,*) J 36Ø 370 IF (J.EQ.U) GO TO 11 380 WRITE (6,123) 123 FORMAT (2X, 'MEMERANE EQUIVALENT WEIGHT') 390 400 READ (5,*) EW 11 WRITE (6,115) 410 115 FOPMAT(2X, 'CONCENTRATION OF SUPPORTING ELECTROLYTE, MOLARITY') 420 4 3Ø READ (5,*) SE 440 IF (SE.EQ.C.) GO TO 19 WRITE (6,120) 120 FORMAT(2X,'SUPPORTING FLECTROLYTE') 450 460 470 READ (5,121) 48Ø 121 FORMAT(A5) 490 WRITE (6,116) 116 FORMAT(2X, 'MOLCCULAR WEIGHT OF SUPPORTING ELECTROLYTE') 500 READ (5,*) UT 510 520 C 53Ø C THE CONSTANTS ARE DEFINED 540 C 10 R=8.3143 550 560 T=273.15+T F=96487. 570 IF (I.EQ.1) GO TO 1 58Ø IF (I.EQ.2) GC TO 2 590 600 C

610 C FOR THE CONCENTRATIONS GIVEN IN WEIGHT PERCENTAGES, THE 62Ø C MOLALITIES OF HBR AND BR2 ARE FOUND FOR USE IN LATER CALCULATIONS 63Ø C 640 1 XBR2=BR265Ø XHBR=HBR 660 XSE=SE 670 MBR2=1000*XBR2/(159.818*(100.-XBR2)) MHBR=1000*XHBR/(80.917*(100.-XHBR)) 68Ø IF(XSE.EO.Ø) GO TO 3 690 700 MSE=1000*XSE/(WT*(100.-XSE)) 710 GO TO 3 720 C FOR THE CONCENTRATIONS GIVEN IN MOLALITIES, THE CONCENTRATIONS 730 C 740 C ARE FOUND IN WEIGHT PERCENTAGES FOR USE IN LATER CALCULATIONS 750 С 760 2 MBR2=BR2 770 MHBR=HBR 780 MSE=SE XHER=100.*80.917/(1000.+MHBR*80.917) 790 800 C 810 C THE EQUIVALENTS OF BROMINE ATOMS PER KG SOLUTION ARE FOUND FOR 82Ø C CALCULATION OF THE DENSITY OF THE SOLUTION USING A SECOND ORDER 83Ø C CURVE FIT OF THE DATA OF GLASS AND BOLYLE IN THE ARTICLE "PERFORMANCE OF HYDROGEN BROMINE FUEL CELLS", FUEL CELL SYSTEMS, 840 C 850 C ACS ADVANCES IN CHEMISTRY SERIES #47, P.203, (1965). 860 C 870 3 EQ=2*MBR2+MHBR+MSE 880 CENS=1.017686873+0.04488363995*EC-4.914449546E-4*EQ**2 890 C 900 C THE MOLAR CONCENTRATIONS OF THE SOLUTION ARE CALCULATED AFTER 910 C THE DENSITY OF THE SOLUTION IS KNOWN 920 C CHBR=1000.*DENS*MHBR/(1000.+80.917*MHER) 930 CBR2=1000.*DENS*MBR2/(1000.+159.818*MBR2) 940 950 CSE=1000.*DENS*MSE/(1000.+WT*MSE) 96Ø CH≏CHBR 970 C 980 C IF A MEMBRANE IS PRESENT IN THIS CELL, SOME EXT-F CALCULATIONS 990 C REQUIRED. THEY ARE, THE WEIGHT FPACTION OF ELECTROLYTE ABSORBED 1000 C BY THE NEMERANE, THE FIXED ANION CONCENTRATION OF THE MEMBRANE, THE HYDROGEN ION CONCENTRATION IN THE MEMBRANE, AND ITS ACTIVITY. 1010 C 1020 C IF NO MEMBRANE JS PRESENT, THESE CALCULATIONS ARE SKIPPED. 1030 C 1040 IF (J.EO.0) GO TO 6 1050 C THE WEIGHT FRACTION OF THE ELECTROLYTE ABSORBED BY THF MEMBRANE 1060 C WAS EMPIRICALLY DETERMINED AS A FUNCTION OF THE MOLAR CONCENTRATION BY R.S. YEO AND D-T. CHIN IN "A HYDROGEN-BROMINE CELL FOR ENERGY 1070 C 1080 C STORAGE APPLICATIONS, " J. ELECTROCHEM. SOC., 127, P. 549 (1980) 1090 C 1100 C WTF=0.323/(1+0.068*CHBR) 1110 1120 C 1130 C THE FIXED ANJON CONCENTRATION OF THE MEMBRANE IS CALCULATED BY AN EQUATION REPORTED BY R.S. YEO, "ION CLUSTERING AND PROTON TRANSPORT IN NAFION MEMBRANES ..." J. ELECTROCHEM. SOC., 130, 1140 C 1150 C 116Ø C P.533, (1983) 1170 C 1180 CR=1000.*PENS/WTF/EW 1190 C 1200 C THE HYDROGEN TON CONCENTRATION IN THE MEMBRANE IS CALCULATED FROM

1210 C AN EQUATION DERIVED THROUGH USE OF DONNAN PRINCIPLES, AND THE ACTIVITY OF THE HYDROGEN ION IS FOUND FOR USE IN THE NERNST 1220 C 1230 C EXPRESSION 1240 C CHM=(CR+SQRT(CR**2+4*(CH+CSE)**2))/2*CH/(CH+CSE) 1250 1260 AHM=CHM*1000/(1000*DENS-1.008*CHM) 1270 GO TO 7 128Ø C 1290 C IF NO MEMBRANE IS PRESENT, THE ACTIVITY OF THE HYDROGEN ION IN THE SOLUTION PHASE IS FOUND FOR USE IN THE NERNST EXPRESSION 1300 C 1310 C 1320 6 AHM=CH*1000/(1000*DENS-1.008*CH) 1330 C 134Ø C THESE CALCULATIONS DETERMINE WHETHER THE BROMINE CONCENTRATION IS ABOVE THE SOLUBILITY LIMIT, USING A CURVE FIT OF THE DATA OF GLASS, "HYDROGEN-BROMINE FUEL CELL", IONICS, INC., CAMBRIDGE, MASS., CONTRACT NO. AF19(604)-8508, (1964) 1350 C 136Ø C 1370 C 1380 C 1390 7 CURVE=0.2526794598+1.057577737*CH+0.0487321524*CH**2 1400 C IF THE DATA IS BELOW THE SOLUBILITY LIMIT, THE EQUILIBRIUM BROMIDE 1410 C 1420 C COMPOUND CONCENTRATIONS MUST BE DETERMINED BY THE BISECTION METHOD 1430 C WHICH SOLVES THE CUBIC EQUATION FOUND THROUGH COMBINATION OF THE 1440 C REACTION EQUILIBRIUM CONSTANTS AND ELECTRONEUTRALITY CONDITIONS. 1450 C THE EQUILIBRIUM CONCENTRATIONS CAN BE EASILY FOUND IF THE BROMINE 1460 C CONCENTRATION IS ABOVE THE SOLUBILITY LIMIT. THROUGH USE OF THE 1470 C EQUILIBRIUM CONSTANTS OF THE COMPLEXING REACTIONS. 1480 C 1490 IF((CBR2-CURVE).LT.0) GO TO 4 1500 ABR2=11510 WRITE (6,200) 200 FORMAT(2X/2X, 'BROMINE IS IN SEPARATE PHASE') 1520 1530 CBREO = (CH+CSE)/57154Ø CBR3E0=16*CBRE0CBR5EQ=40*CBREO 1550 CBR2EQ=CURVE 1560 1570 GO TO 5 1580 4 CALL BISECT(CBR2, CH, CBR2EQ, CSE) 1590 CBREC = (CH+CSE) / (1.0+16.*CBR2EQ+40.*CBR2EQ*CBR2EQ)CBR3EC=16.*CBR2EQ*CBREQ 1666 CBR5EQ=40.*CBREQ*CBR2EQ*CBR2EQ 1610 ABR2=CBP2EQ*1000/(1000*DENS-159.818*CBR2EQ) 1620 1630 C THE POTENTIAL DUE TO COMPLEXING OF THE BROMIDE JONS AND BROMINE 1640 C 1650 C TO FORM TRIBROMIDE AND PENTABROMIDE LONS IS FOUND 1660 C 167Ø 5 SUM=CBR2EQ+CBR3EQ+CBR5EQ 1680 COMP=0.5*(CBR3EQ/SUM*R*T/F*(ALCG(16.))+0.5*CBR5EQ/SUM*R*T/F*(ALCG(1690 &4Ø.))) 1700 C THIS SECTION DETERMINES THE ACTIVITY COEFFICENT OF HBR FOR THE 1710 C 1720 C CONCENTRATION OF BROMIDE JONS DETERMINED TO BE PRESENT AFTER 1730 C SOLUTION EQUILIBRATION FROM A CUBIC CURVE FIT OF THE DATA REPORTED 1740 C BY E.N. BALKO 1750 C 1760 MBR=MHBR GANMA=0.9418152476-0.03224218452*MBR+0.045343504*MBR*MBR 1770 &+0.015525929*MBR**3 1780 1790 C THE ACTIVITY OF THE BROMICE ION IS FOUND, AND THE NERNST POTENTIAL 1800 C

1810 C IS CALCULATED USING THE STANDARD POTENTIAL OF 1.0873-541E-6*(T-182Ø C 298.15) GIVEN BY MILAZZO AND CAROLI, TABLES OF STANDARD ELECTRODE 1830 C POTENTIALS, WILEY, NY, 1977, P.284-5. 1840 C ABR=1000*CBREQ/(1000*DENS-CBREQ*79.909)*GAMMA 185Ø 1860 AHM=AHM*GAMMA 1870 NERNST=1.0873+ALOG(SQRT(PH2)*SQRT(ABR2)/AHM/ABR)*R*T/F+(T-298.15)* 188ø &(-541E-6)1890 C THE OUTPUT OF THE PROGRAM IS GIVEN 1900 C 1910 C 1920 WRITE (6,106) DENS 106 FORMAT(2X/2X, 'DENSITY OF DELTA PHASE', F10.6, ' G/ML') 1930 WRITE(6,107) CBR2EQ 1940 1950 107 FORMAT(2X, 'EQUILIBRIUM BROMINE CONCENTRATION', F9.6, ' MOLES/LITER') 1960 WRITE (6,108) CBREQ 197Ø 108 FORMAT(2X, 'EQUILIBRIUN BROMIDE CONCENTRATION', F9.6, ' MOLES/LITER') 1980 WRITE(6,109) CBR3EQ 1990 109 FORMAT(2X, 'EQUILIBRIUM TRIBROMIDE CONCENTRATION', F10.6, ' MOLES/LIT &ER') 2000 2010 WRITE (6,110) CBR5EQ 2020 110 FORMAT(2X, 'EQUILIBRIUM PENTABROMICE CONCENTRATION' F10.6, ' MOLES/L 2030 &ITER') 2040 WRITE (6,111) NEENST 2050 111 FORMAT(2X, 'NERNST POTENTIAL', F10.6, ' VOLTS') 2060 WRITE(6,113) COMP 2070 113 FORMAT(2X, 'POTENTIAL DUE TO COMPLEX FORMATION' F10.6,' VOLTS') 2080 TOTAL=NERNST+COMP 2090 WRITE (6,114) TOTAL 2100 114 FORMAT(2X, 'TOTAL POTENTIAL', F10.6, ' VOLTS'/) 2110 END 2120 C 2130 C THIS SUBROUTINE USES THE BISECTION METHOD TO DETERMINE THE 2140 C EQUILIBRIUM BROMINE CONCETRATION WHICH IS THE FOOT OF A CUBIC 2150 C EXPRESSION 216Ø C SUBROUTINE LISECT (CBR2, CH, CBR2EC, CSE) 2170 218Ø REAL MID 2190 **Λ=0**. 2200 B=2. 2210 FA=2*CBR2 2220 1 MID=(A+B)/2.2230 FM=2.*CBR2+(32.*CBR2-32.*CH-32.*CSE-2.)*MID+(80.*CBR2-160.*CH-32. C-160.*CSE)*MID**2-80*MID**3 2240 2250 IF (FA*FM.LE.0.) GO TO 2 2260 A≈HJ.D 227Ø FA=FM 2280 GO TO 3 2290 2 B=MID 2300 3 IF (ABS(B-A).LE.0.000001) GO TO 4 2310 CO TO 1 2320 CBR2EQ=(A+D)/22330 RETURN 2340 END

Example Output of OCVACT

```
run
OCVACT Ø1/15/86 13:58:53
TEMPERATURE, C
223
HYDROGEN PRESSURE, ATM
71
 IF THE CONCENTRATIONS OF BR2 AND HBR ARE GIVEN IN
 WEIGHT PERCENT, INPUT 1; IF THEY ARE IN MOLALITY,
 INPUT 2.
?1
BROMINE CONCENTRATION
27.95
HYDROGEN BROMIDE CONCENTRATION
24Ø
IS MEMBRANE PRESENT? (1 FOR YES, Ø FOR NO)
21
MEMBRANE EQUIVALENT WEIGHT
21200
 CONCENTRATION OF SUPPORTING ELECTROLYTE, MOLARITY
?Ø
```

DENSITY OF DELTA PHASE 1.393303 G/ML EQUILIBRIUM BRONINE CONCENTRATION 0.006683 MOLES/LITER EQUILIBRIUM BROMIDE CONCENTRATION 6.212220 MOLES/LITER EQUILIBRIUM TRIBROMIDE CONCENTRATION 0.664248 MOLES/LITER EQUILIBRIUM PENTABROMIDE CONCENTRATION 0.611098 MOLES/LITER NERNST POTENTIAL 0.791697 VCLTS POTENTIAL DUE TO COMPLEX FORMATION 0.034838 VOLTS TOTAL POTENTIAL 0.826535 VOLTS

STOP TIME Ø.2 SECS

ORIGINAL PAGE IS OF POOR OUALITY

2Ø C PROGRAMMER: SHARON FRITTS 30 C 40 C 50 C THIS PROGRAM CALCULATES THE OPEN CIRCUIT POTENTIAL OF THE HYDROGEN-BROMINE CELL FOR A GIVEN TEMPERATURE, HYDROGEN PRESSURE, 6Ø C 70 C BROMINE AND HYDROGEN BROMIDE CONCENTRATION. IT ALSO INCLUDES THE EFFECTS OF A SUPPORTING ELECTROLYTE, IF PRESENT. IF A MEMBRANE IS PRESENT, THE CONNAN EFFECTS ON THE HYDROGEN ION CONCENTRATION 80 C 90 C 100 C IS USED IN THE EXPRESSION. THE K VALUES FOR THE COMPLEXING REACTIONS ARE VARIED. 110 C 120 C REAL MBR2, MHBR, HBR, NERNST WRITE (6,99) 99 FORMAT(2X,'TEMPERATURE, C') READ (5,*) T WRITE (6,100) 100 FORMAT(2X, 'HYDROGEN PRESSURE, ATM') READ (5,*) PH2 WRITE (6,101) 101 FORMAT(2X, 'IF THE CONCENTRATIONS OF BR2 AND HBR ARE GIVEN IN') WRITE (6,102) 102 FORMAT(2X, WEIGHT PERCENT, INPUT 1; IF THEY ARE IN MOLALITY, ') WRITE (6,103) 103 FORMAT(2X, 'INPUT 2.') READ (5,*) J WRITE (6,104) 104 FORMAT(2X, 'BROMINE CONCENTRATION') READ (5,*) BR2 WRITE (6,105) 105 FORMAT(2X, 'HYDROGEN BROMIDE CONCENTRATION') READ (5,*) HBR WRITE (6,122) 122 FORMAT(2X, 'IS MEMBFANE PRESENT? (1 FOR YES, Ø FOR NO)') READ (5,*) J IF (J.EQ.C) GO TO 11 WRITE (6,123) 123 FORMAT (2X, 'MFMBRANE EQUIVALENT WEIGHT')
READ (5,*) EW 11 WRITE (6,127) 127 FORMAT (2X, 'FACTOR TO MULTIPLY K FOR TRIBROMIDE REACTION BY') READ (5,*) TRI WRITE (6,128) 128 FORMAT (2X, 'FACTOR TO MULTIPLY K FOR PENTAPROMIDE REACTION BY') READ (5,*) PENTA 460 C 470 C THE CONSTANTS ARE DEFINED 480 C R=8.3143 T = 273.15 + TF=96487. LF (J.EQ.1) GO TO 1 IF (I.EC.2) GO TO 2 540 C 550 C FOR THE CONCENTRATIONS GIVEN IN WEIGHT PERCENTAGES, THE 56Ø C MOLALITIES OF HER AND BR2 ARE FOUND FOR USE IN LATER CALCULATIONS 570 C 1 XBR2=BR2

58Ø XIIBR=HBP 590 600

list 10 C

1 3Ø

140 150

160

170

180 190

200

210

220

230

240

25Ø

260 270

28Ø

290 300

310

32Ø 330

340

35Ø

360 370

380 390

400

410 420 430

440

450

49Ø

500

510 52Ø

5 3Ø

OCKEFF

MBR2=1000*MER2/(159.818*(100.-XER2))

ORIGINAL PÂGE[÷]TS OF POOR QUALITY

610 620 640 650 660 670 700 7100 7300 740 750 770 780			MHBR=1000*XHBR/(80.917*(100XHBR)) GO TO 3
			FOR THE CONCENTRATIONS GIVEN IN MOLALITIES, THE CONCENTRATIONS ARE FOUND IN WEIGHT PERCENTAGES FOR USE IN LATER CALCULATIONS
		2	NBR2=BR2 MHBR=HBR XHBR=100.*80.917/(1000.+MHBR*80.917)
	000000		THE EQUIVALENTS OF BROMINE ATOMS PER KG SOLUTION ARE FOUND FOR USE IN CALCULATION OF THE SOLUTION DENSITY USING A SECOND ORDER POLYNOMIAL CURVE FIT OF THE DATA OF GLASS AND BOYLE, "PERFORMANCE OF HYDROGEN BROMINE FUEL CELLS", FUEL CELL SYSTEMS, ACS ADVANCES IN CHEMISTRY SERIES #47, P.203, (1965).
	c	3	EQ=2*MBR2+MIER DENS=1.017686873+0.C4488363995*EQ-4.914449546E-4*EQ**2
790 800 810	000		THE MOLAR CONCENTRATIONS OF THE SOLUTION ARE CALCULATED AFTER THE DENSITY OF THE SOLUTION IS KNOWN
820 830 840 850 860 870 880 890 900 910	C		CHBR=1000.*DENS*MHBR/(1000.+80.917*MHBR) CBR2=1000.*DENS*MBR2/(1000.+159.818*MBR2) CH=CHBR
	000000		IF A MEMBRANE IS PRESENT IN THIS CELL, SOME EXTRA CALCULATIONS REQUIRED. THEY ARE, THE WEIGHT FRACTION OF ELECTROLYTE ABSORBED BY THE MEMBRANE, THE FIXED ANION CONCENTRATION OF THE MEMBRANE, THE HYDROGEN ION CONCENTRATION IN THE MEMBRANE, AND ITS ACTIVITY. IF NO MEMBRANE IS PRESENT, THESE CALCULATIONS ARE SKIPPED.
92Ø 93Ø	c		IF (J.EQ.0) GO TO 6
950 960 970 980	00000		THE WEJGHT FRACTION OF THE ELECTROLYTE ABSORBED BY THE MEMBRANE WAS EMPIRICALLY DETERMINED AS A FUNCTION OF THE MOLAR CONCENTRATION BY R.S. YEO AND D-T. CHIN IN "A HYDROGEN-BROMINE CELL FOR ENERGY STORAGE APPLICATIONS," J. ELECTROCHEM. SOC., 127, P. 549 (1980)
1000	с ~		WTF=0.323/(1+0.068*CHBR)
1020 1030 1040 1050	00000		THE FIXED ANION CONCENTRATION OF THE MEMBRANE IS CALCULATED BY AN EQUATION REPORTED BY R.S. YEO, "ION CLUSTERING AND PROTON TRANSPORT IN NAFION MEMBRANES" J. ELECTROCHEM. SOC., 130, P.533, (1983)
1060 1070 1080	c c		CR=1000.*DENS/WTF/EW
1090 1100 1110 1110	00000		THE HYDROGEN ION CONCENTRATION IN THE MEMBRANE IS CALCULATED FROM AN EQUATION DERIVED THPOUGH USE OF DONNAM PRINCIPLES, AND THE ACTIVITY OF THE HYDROGEN ION IS FOUND FOR USE IN THE NERNST EXPRESSION
1140 1150 1160	C		CHM=(CR+SQRT(CR**2+4*(CH)**2))/2*CH/(CH) AHM=CHM*1000/(1000*DENS-1.008*CHM) WRITE (6,112) CHM
1170 1180	c	112	FORMAT (/2X, 'MEMBRANE PROTON CONCENTRATION', F8.4, ' MOLES/ LITER') GO TO 7
1200	č		IF NO MEMOPANE IS PRESENT, THE ACTIVITY OF THE HYDROGEN ION IN THE

ORIGINAL PAGE IS OF POOR QUALITY

121Ø C SOLUTION PHASE IS FOUND FOR USE IN THE NERNST EXPRESSION 1220 C 6 AHM=CH*1000/(1000*DENS-1.008*CH) 1230 1240 C 125Ø C THESE CALCULATIONS DETERMINE WHETHER THE BROMINE CONCENTRATION IS ABOVE THE SOLUBILITY LIMIT, USING A CURVE FIT OF THE DATA OF GLASS, "HYDROGEN-BROMINE FUEL CELL", IONICS, INC., CAMBRIDGE, MASS., 126Ø C 1270 C 1280 C CONTRACT NO. AF19(6C4)-8508, (1964) 1290 C 1300 7 CURVE=0.2526794598+1.057577737*CH+0.0487321524*CH**2 1310 C IF THE DATA IS BELOW THE SOLUBILITY LIMIT, THE EQUILIBRIUM BROMIDE 132Ø C 1330 C COMPOUND CONCENTRATIONS MUST BE DETERMINED BY THE BISECTION METHOD WHICH SOLVES THE CUBIC EQUATION FOUND THROUGH COMBINATION OF THE 134Ø C REACTION EQUILIBRIUM CONSTANTS AND ELECTRONEUTRALITY CONDITIONS. 135Ø C THE EQUILIBRIUM CONCENTRATIONS CAN BE EASILY FOUND IF THE BROMINE CONCENTRATION IS ABOVE THE SOLUBILITY LIMIT, THROUGH USE OF THE 1360 C 137Ø C EQUILIBRIUM CONSTANTS OF THE COMPLEXING REACTIONS. 1380 C 1390 C 1400 JF((CBR2-CURVE).LT.0) GO TO 4 1410 ABR2=1 1420 WRITE (6,200) 200 FORMAT(2X/2X, 'BROMINE IS IN SEPARATE PHASE') 1430 CBREQ=(CH)/(1+16*TRI+40*PENTA)1440 1450 CBR3EQ=16*CBREQ*TRL CBR5EQ=40*CBREQ*PENTA 1460 CBR2EQ=CURVE 1470 1480 GO TO 5 4 CALL BISECT(CBR2, CH, CBR2EQ, TRI, PENTA) 1490 1500 CBREQ=(CH)/(1.0+16.*CBR2EQ*TRI+40.*CBR2EQ*CBR2EQ*PENTA)CBR3EQ=16.*CBR2EC*CEREC*TRI 1510 CBR5EQ=40.*CBREQ*CBR2EC*CBR2EC*PENTA 1520 ABR2=CBR2EQ*1000/(1000*DENS-159.818*CBR2EQ) 1530 1540 C 1550 C THE POTENTIAL DUE TO COMPLEXING OF THE BROMIDE JONS AND BROMINE TO FORM TRIBROMIDE AND PENTABROMIDE LONS IS FOUND 1560 C 1570 C 1580 5 SUM=CBR2EC+CBR3EC+CBR5EQ 1590 COMP=0.5*(CBR3EQ/SUM*R*T/F*(ALOG(16.*TRI))+0.5*CBR5EQ/SUM*R*T/F* &(ALOG(40.*PENTA))) 1600 1610 C 1620 C THE ACTIVITY OF THE BROMIDE ION IS FOUND, AND THE NERNST POTENTIAL IS CALCULATED, USING THE STANDARD POTENTIAL OF 1.0873-541E-6*(T-1630 C 298.15) GIVEN BY MILAZZO AND CAROLI, TABLES OF STANDARD ELECTRODE 1640 C 1650 C POTENTIALS, WILEY, NY, 1977, P.284-5. 1660 C 1670 ABR=CBREO*1000/(1000*DENS-79.909*CBREO) NERNST=1.0873+ALOG(SCRT(PH2)*SCRT(AER2)/AHM/ABR)*R*T/F+(T-298.15)* 1680 1690 &(-541E-6)1700 C THE OUTPUT OF THE PROGRAM IS GIVEN 1710 C 1720 C 1730 WRITE (6,106) DENS 106 FORMAT(2X/2X, 'DENSITY OF DELTA PHASE', F10.6, ' G/ML') 1740 1750 WRITE(6,107) CBR2EQ 1760 107 FORMAT(2X, 'EQUILIBRIUM BROMINE CONCENTRATION', F9.6, ' MOLES/LITER') WRITE (6,108) CBREQ 1770 1780 108 FORMAT(2X, 'ECUILIBRIUN BRONIDE CONCENTRATION', F9.6, ' MOLES/LITER') 1790 WRJTE(6,109) CBR3EQ 109 FORMAT(2X, 'EQUILIBRIUM TRIBRONIDE CONCENTRATION', FI0.6, ' MOLES/LIT 1800 181Ø &ER')

1820 WRITE (6,110) CBR5EQ 110 FORMAT(2X, 'EQUILIBRIUM PENTABROMIDE CONCENTRATION', F10.6, ' MOLES/L 183Ø 1840 &ITER') WRITE (6,111) NERNST 185Ø 1860 111 FORMAT(2X, 'NERNST POTENTIAL', F10.6, ' VOLTS') WRITE(6,113) COMP 1870 1880 113 FORMAT(2X, 'POTENTIAL DUE TO COMPLEX FORMATION', F10.6, ' VOLTS') 1890 TOTAL=NERNST+COMP 1900 WRITE (6,114) TOTAL 1910 114 FORMAT(2X, 'TOTAL POTENTIAL', F10.6, ' VOLTS'/) 1920 END 1930 C 1940 C THIS SUBROUTINE USES THE BISECTION METHOD TO DETERMINE THE EQUILIBRIUM BRONINE CONCETRATION WHICH IS THE ROOT OF A CUBIC 195Ø C 196Ø C EXPRESSION 1970 C SUBROUTINE BISECT (CBR2, CH, CBR2EQ, TRI, PENTA) 198Ø 1990 REAL MID A=Ø. 2000 2010 B=2.2020 FA=2*CBR2 1 MID=(A+B)/22030 FM=2*CBR2+(32*CBR2*TRI-32*CH*TRI-2)*MID+(80*CBR2*PENTA-160*PENTA 2Ø4Ø 2050 &*CH-32*TRI)*MID**2-80*PENTA*MID**3 2060 IF (FA*FM.LE.Ø.) GO TO 2 2Ø7Ø A=MJ.D FA=FM 2080 2090 GO TO 3 2100 2 B=MID 2110 3 IF (ABS(B-A).LE.0.000001) GO TO 4 2120 GO TO 1 2130 4 CBR2EQ=(A+B)/22140 RETURN 2150 END

Example Output of OCKEFF

```
run
OCKEFF 01/02/86 13:24:18
 TEMPERATURE, C
223
HYDROGEN PRESSURE, ATM
71
IF THE CONCENTRATIONS OF BR2 AND HBR ARE GIVEN IN
 WEIGHT PERCENT, INPUT 1; IF THEY ARE IN MOLALITY.
 INPUT 2.
21
 BROMINE CONCENTRATION
27.95
HYDROGEN BROMIDE CONCENTRATION
240
IS MEMBRANE PRESENT? (I FOR YES, Ø FOR NO)
71
MEMBRANE EQUIVALENT WEIGHT
71200
 FACTOR TO MULTIPLY K FOR TRIBROMIDE REACTION BY
25
FACTOR TO MULTIPLY K FOR PENTABROMIDE REACTION BY
25
MEMBRANE PROTON CONCENTRATION 10 0001 MOLES/ LITER
 DENSITY OF DELTA PHASE 1.391439 G/ML
 EQUILIBRIUM BROMINE CONCENTRATION Ø ØØ1385 MOLES/LITER
```

EQUILIBRIUM BROMIDE CONCENTRATION 6 190020 MOLES/LITER EQUILIBRIUM TRIBROMIDE CONCENTRATION 0 685959 MOLES/LITER EQUILIBRIUM PENTABROMIDE CONCENTRATION 0 002375 MOLES/LITER NERNST POTENTIAL 0.900371 VOLTS POTENTIAL DUE TO COMPLEX FORMATION 0.055725 VOLTS TOTAL POTENTIAL 0.956096 VOLTS

STOP TIME Ø 2 SECS

APPENDIX C

EXPERIMENTAL EQUIPMENT

A listing of the experimental equipment is given in Table 8. It specifies the manufacturer and catalog number of all major pieces of equipment. The types of tubing used were FEP Teflon flexible tubing, and machined TFE Teflon tubing. The fittings were either injection molded PFA Teflon or machined TFE Teflon.

Figure 34 shows the wiring diagram for experimental data acquisition. The relay circuit shown in Figure 35 was constructed for this research.

Bromide Solution Storage Flask: 6954-77 Ace Glass, 1000 ml. Flask, Flask, Four Necks, One Threaded, Thermometer neck internally threaded, Teflon bushing to hold 7mm thermometer, and Viton Orings. Side Necks T 20/40 fitted with 5031-10 Twin Ace-Thread adapators, T 24/25 joint, Teflon bushing and Viton O-rings to hold 7 mm tubing. Center neck, T 20'40, fitted with stirrer.

Bromide Solution Stirrer:

Constant Temperature Bath:

Thermistor Thermometer:

Thermistor Probe:

Bromine Solution Pump:

Needle Valves:

Pressure Gages:

Reference Electrode:

stirrer, R-4335-00 with speed range of 500-7500 rpm, up to 5 gal. bath. Neslab Instruments Co., T 9/10 W,

system stirrer with T 24/40 joint.

Has glass shaft, Teflon blades and seal assembly, Viton O-ring. Used with Cole Parmer's variable-speed

Closed

Cole Parmer R-4740-00.

heats to 100 C.

Cole-Parmer R-8110-20 digital thermistor thermometer. Resolution to 0.1 degree in both Celsius and Fahrenheit with accuracy of $\pm 0.1\%$ of reading. For 0 to 50° C operating temperature.

Cole-Parmer Liquid Immersion Probe R-8110-20. 5" Pyrex Glass probe with time constant of 4.2 sec.

All-Teflon piston pump, model no. 7149-10 Cole Parmer 0.0-2.4 1/min., pressure to 14.9 psi, -40 to 150 C.

Teflon TFE Needle valves, Cole Parmer R-6393-60. 0.2 gpm maximum flow at 1 psig. 75 psig. maximum pressure.

0 to 30 psigage with Fluorocarbon Co. GPO-42 all Teflon body protector.

Standard Calomel Reference Electrode, Fisher Scientific 13-639-52. Prefilled with saturated KCl solution.



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Figure 34. Schematic of wiring for experimental data acquisition.







APPENDIX D

EXPERIMENTAL PROCEDURE

The steps taken to begin an experiment after the solutions are prepared as described in Chapter IV are listed below:

1. Turn electrometer on three hours before experiment is to begin.

2. Turn on water bath one hour before experiment is to begin.

3. Activate the platinized platinum screen by the method described in Appendix F. (When necessary, strip the platinum screen and platinize it again.)

4. Place platinized platinum screen in the hydrogen half cell, then place platinized side of membrane (when catalyzed Nafion 120 separator is used) between half cells, and bolt the cell together.

5. Connect cell to line, and connect leads.

6. Turn on stirrer, and collect solution sample for titration to determine bromine content. See Appendix F.

7. Enter storage solution temperature, pressure, and solution concentration into computer program.

8. Set the hydrogen flow to the desired pressure.

9. Prime the pump, then begin pumping solution.

10. Wait fifteen seconds for the solution to flow through cell, then begin data acquisition.

At the completion of an experiment:

1. Turn off the hydrogen.

2. Turn off the pump. Disconnect the cell, rinse the membrane and platinized platinum with distilled deionized water, then place both in a beaker of distilled deionized water.

3. Cap tubing at cell entrance and exit to prevent evaporation of bromine from storage.

4. Take a solution sample for titration, then turn off the stirrer and electrometer.

APPENDIX E

BASIC CODE OF DATA ACQUISITION PROGRAM FOR KEITHLEY PLUS 500 DATA ACQUISITION SYSTEM

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10 REM Program used in data acquisition of hydrogen-bromine cell open circuit 20 REM voltage and rates of solution and membrane equilibrium data. 30 REM 40 REM Programmers: Sharon Fritts, Doug Smith and Gail Lance 50 REM 80 REM Note: An uncommented version of this program was used to collect 70 REM experimental data since comments slow running time considerably. 80 REM 90 PRINT "IF CONTROL UP IS PRESSED THE PROGRAM IS TO STOP" 100 REM 110 REM These lines initialize the Plus500 software system. 120 REM ,63000! 130 CLEAR ' GPIB-PC Rev. B.1 ' BASICA Declaration File IBINIT1 = 63000! 140 IBINIT2 = IBINIT1 + 3 15Ò BLOAD "bib.m", IBINIT1 180 CALL IBINIT1 (IBFIND, IBTRG, IBCLR, IBPCT, IBSIC, IBLOC, IBPPC, IBBNA, IBONL, IB 170 RSC, IBSRE, IBRSV, IBPAD, IBSAD, IBIST, IBDMA, IBEOS, IBTMO, IBEOT) CALL IBINIT2 (IBGTS, IBCAC, IBWAIT, IBPOKE, IBWRT, IBWRTA, IBCMD, IBCMDA, IBRD, 180 IBRDA, IBSTOP, IBRPP, IBRSP, IBDIAG, IBXTRC, IBSTAX, IBERRX, IBCNTX) 190 NAS="gpib0": CALL IBFIND(NAS, INTERFIX) 200 NAS="dev15": CALL IBFIND(NAS, ELECTRX) 210 V%=&H102: CALL IBFOKE(BRD0X, V%) 220 VX=27:CALL IBPAD(ELECTRX,VX) 230 VX=1:CALL IBSRE(INTERF1X,VX) 240 REM 250 REM This command locks out the front panel of the electrometer. 260 REM 270 CMDs=CHRs(&H11):CALL IBCMD(INTERF1%, CMDs) 280 CLS 290 REM 300 REM Initialize pressure, temperature and concentration arrays. 310 REM 320 DIM PT(5) 330 REM 340 REM Initialize the voltage and time storing arrays. 350 REM 360 DIM VOLT1(2048) 370 DIM VOLT2(2048) 380 DIM TIME(2048) 390 INPUT "WHAT IS THE PRESSURE"; PT(1) 400 INPUT "WHAT IS THE TEMPERATURE"; PT(2) 410 INPUT "WHAT IS CONCENTRATION OF HBr"; PT(3) 420 INPUT "WHAT IS CONCENTRATION OF Br2"; PT(4) 430 REM 440 REM Sets the clock to zero. 450 REM 460 X\$="00" 470 TIME\$=X\$ 480 REM 490 REM Initialize time buffer, number of voltages read. 500 REM 510 TBUF=0:D=0 520 REM 530 REM Clears the electrometer 540 REM 550 CALL IBCLR(ELECTR%) 560 REM 570 REM Command that sets the function and range for measuring VOLT1 580 REM 590 CMDs="R2F0C0T5X"

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600 REM 810 REM Sets voltage source to be used to trip the relay, and then 620 REM command string that sets function and range for measuring VOLT2 630 REM 640 V\$="D1V+10201X" 650 CME\$="R2FOCOT501X" 660 REM 670 REM Command string that turns off voltage source. 680 REM 690 V1\$="OOX" 700 REM 710 REM Intialize the checks to be used throughout the program. 720 REM 730 X=0:SCOUNT=0:LCOUNT=0:CHK=59 740 REM If cursor up key is pressed, go to routine that saves data 750 REM 760 ON KEY(11) GOSUB 2550:KEY(11) ON 770 REM 780 REM Turn off voltage source, then insert a time delay of 130msec. 790 REM read voltage to be used to find VOLT1 with electrometer, then convert 800 REM it to a numerical value. If this voltage is about 0V then beep. 810 REM 820 CALL IBWRT(ELECTR%, V1\$) 830 CALL IBWRT (ELECTR%, CMD\$) 840 V%=9:CALL IBTMO(BRDO%, V%) 850 **V%=8** 860 CALL IBTMO(BRD0%, V%) 870 RD\$=SPACE\$(50) 880 CALL IBRD(ELECTR%, RD\$) 890 RD=VAL(MID\$(RD\$,5,16)) 900 IF ABS(RD)<6.000001E-04 THEN BEEP 910 REM 920 REM Turn on voltage source to trip the relay, then insert a time delay 930 REM of 130msec, read voltage used to find VOLT2, then convert reading 940 REM to a numerical value. If this voltage is about 0V then beep. 950 REM 960 CALL IBWRT(ELECTR%,V\$) 970 CALL IBWRT (ELECTR%, CME\$) 980 V%=9 990 CALL IBTMO(BRD0%,V%) 1000 V%=8 1010 CALL IBTMO(BRD0%, V%) 1020 RE\$=SPACE\$(50) 1030 CALL IBRD(ELECTR%, RE\$) 1040 RE=VAL(MID\$(RE\$,5,16)) 1050 IF ABS(RE)<6.000001E-04 THEN BEEP 1060 REM 1070 REM Reads the time into minutes, and calls it SBUF 1080 REM 1090 T\$=TIME\$ 1100 A=VAL(MID\$(T\$,1,2))*60 1110 B=VAL(MID\$(T\$,4,2)) 1120 C=VAL(MID\$(T\$,7,2))/60 1130 SBUF=A+B+C 1140 REM 1150 REM Increment number of voltages read, and sum voltages to find VOLT1 and 1160 REM VOLT2 into V1BUF and V2BUF as they are being read for averaging later. 1170 REM 1180 D=D+1 1190 V1BUF=V1BUF+RD

1200 V2BUF=V2BUF+RE 1210 REM 1220 REM If the time since the last time a voltage has been averaged and 1230 REM recorded is less than 15 seconds, go to 740 for more voltage readings 1240 REM 1250 IF(SBUF-TBUF)<=.25 GOTO 760 1260 REM 1270 REM Find median time between sets of recorded voltages, and average the 1271 REM during this time and store them in arrays Volt1 and Volt2 1280 RÉM 1290 TIME(X+1)=(SBUF+TBUF)/2 1300 TBUF=SBUF 1310 VOLT1(X+1)=V1BUF/D 1320 VOLT2(X+1)=V2BUF/D 1330 REM 1340 REM Reset number of voltages used in averaging to zero, print recorded 1350 REM voltages on screen 1360 REM 1370 D=0 1380 PRINT "THE VOLTAGES AND TIME ARE", VOLT1(X+1), VOLT2(X+1), TIME(X+1),X ,SCOU NT 1390 REM 1400 REM If number of times equilibrium condition has been met is zero, set 1410 REM last recorded voltage to be that used for determining equilibrium 1420 REM criteria 1430 REM 1440 IF SCOUNT =0 THEN VOLT=VOLT1(X) 1450 REM 1460 REM If equilibrium condition is met, increment SCOUNT, otherwise, set 1470 REM SCOUNT to be zero 1460 REM 1490 IF ABS(VOLT1(X+1)-VOLT)<.0002 THEN SCOUNT=SCOUNT+1 ELSE SCOUNT=0 1500 REM 1510 REM Increment space number in storage array, and check to see if equil. 1520 REM condition has been met for ten minutes. If so, go to data storage. 1530 REM 1540 X=X+1 1550 IF SCOUNT=40 THEN GOTO 2550 1560 REM 1570 REM Reset voltage buffers, and if experiment has been running less than one 1580 REM hour, return to line 740 to read more data. 1590 REM 1600 V1BUF=0:V2BUF=0 1610 IF (SBUF<60) THEN GOTO 760 1620 REM 1630 REM Calculate the number of minutes the equilibrium criteria has been met. 1640 REM Check to see if the cursor up key has been hit to stop the program and 1650 REM store the data. 1660 REM 1670 LCOUNT=SCOUNT\4 1680 ON KEY(11) GOSUB 2550: KEY(11) ON 1690 REM 1700 REM Turn off voltage source, then insert a time dalay of 130 msec. Read 1710 REM voltage to be used in determining VOLT1 with electrometer, then 1720 REM convert voltage to a numerical value. Make sure voltage is not zero. 1730 REM 1740 CALL IBWRT(ELECTR%, V1\$) 1750 CALL IBWRT(ELECTR%, CMD\$) 1760 V%=9:CALL IBTMO(BRD0%, V%)
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1770 V%=8 1780 CALL IBTMO(BRDO%, V%) 1790 RD\$=SPACE\$(50) 1800 CALL IBRD(ELECTR%, RD\$) 1810 RD=VAL(MID\$(RD\$,5,18)) 1820 IF ABS(RD)<6.000001E-04 THEN BEEP 1830 REM 1840 REM Turn on voltage source to trip the relay, then insert a time delay 1850 REM of 130 msec, read voltage to be used to find VOLT2, then convert it 1860 REM to a numerical value. Make sure this voltage is not zero. 1870 REM 1880 CALL IBWRT(ELECTR%, V\$) 1890 CALL IBWRT(ELECTR%, CME\$) 1900 V%=9 1910 CALL IBTMO(BRD0%, V%) 1920 V%=8 1930 CALL IBTMO(BRDO%, V%) 1940 RE\$=SPACE\$(50) 1950 CALL IBRD(ELECTR%, RE\$) 1960 RE=VAL(MID\$(RE\$,5,16)) 1970 IF ABS(RE)<6.000001E-04 THEN BEEP 1980 REM 1990 REM Reads the time into minutes, and call it SBUF 2000 REM 2010 T\$=TIME\$ 2020 A=VAL(MID\$(T\$,1,2))*60 2030 B=VAL(MID\$(T\$,4,2)) 2040 C=VAL(MID\$(T\$,7,2))/60 2050 SBUF=A+B+C 2060 REM 2070 REM Increment number of voltages read, and sum voltages to be used to 2080 REM determine VOLT1 and VOLT2 into V1BUF and V2BUF as they are being read 2090 REM for averaging later. 2100 REM 2110 D=D+1 2120 V1BUF=V1BUF+RD 2130 V2BUF=V2BUF+RE 2140 REM 2150 REM If it has been a minute since the last time a voltage has been 2160 REM recorded or averaged, go to 1860 2170 REM 2180 IF(SBUF-TBUF)<1 THEN GOTO 1680 2190 REM 2200 REM Find median time between recorded voltages, and average voltage during 2210 REM this time and store in VOLT1 and VOLT2 arrays. Reset voltage counter 2220 REM to zero, and put recorded voltages and time on the screen. 2230 REM 2240 TIME(X+1)=(TBUF+SBUF)/2 2250 TBUF=SBUF 2260 VOLT1(X+1)=V1BUF/D 2270 VOLT2(X+1)=V2BUF/D 2280 D=0 2290 PRINT"THE VOLTAGES AND TIME ARE", VOLT1(X+1), VOLT2(X+1), TIME(X+1), X, LCOUNT 2300 IF LCOUNT =0 THEN VOLT=VOLT1(X) 2310 REM 2320 REM If number of times equilibrium condition has been met is zero, set 2330 REM last recorded voltage to be that used for determining equilibrium 2340 REM criteria in the next reading 2350 REM 2360 REM If equilibrium condition is met increment LCOUNT, otherwise, set it to

2370 REM be zero.

2380 REM 2390 IF ABS(VOLT1(X+1)-VOLT)<.0002 THEN LCOUNT=LCOUNT+1 ELSE LCOUNT=0 2400 X=X+1 2410 REM 2420 REM If equilibrium condition has been met for ten minutes, go to data 2430 REM storage section of program. 2440 REM 2450 IF LCOUNT=10 THEN GOTO 2550 2460 V1BUF=0:V2BUF=0 2470 REM 2480 REM If it has been one hour since the electrometer was zeroed, rezero the 2490 REM electrometer, otherwise continue reading data. 2500 REM 2510 IF CHK<59 THEN CHK=CHK+1 ELSE CHK=0 2520 IF CHK>0 GOTO 2540 2530 CHK\$="20XC1X21XC0X": CALL IBWRT(ELECTR%,CHK\$) 2540 GOTO 1680 2550 V%=0:CALL IBONL(INTERF1%,V%) 2560 CALL IBONL(ELECTR%,V%) 2570 REM 2580 REM Store data in file. 2590 REM 2600 CMD\$=CHR\$(&H14):CALL IBCMD(INTERF1%,CMD\$) 2610 INPUT WHAT DO YOU WANT TO NAME THIS RUN"; A\$ 2620 INPUT WHAT IS THE FINAL TEMPERATURE"; PT(5) 2630 B\$=".prn' 2640 C\$=A\$+B\$ 2650 Y1\$=" VOLT1" 2660 Y2\$=" VOLT2" 2670 Z\$="MINUTES" 2680 OPEN "o",#1,C\$ 2690 PRINT #1, Y1\$, Y2\$, Z\$ 2700 CLOSE #1 2710 OPEN CS FOR APPEND AS #1 2720 FOR Y=1 TO X+1 2730 PRINT #1, VOLT1(Y), VOLT2(Y), TIME(Y) 2740 NEXT Y 2750 CLOSE #1 2760 OPEN C\$ FOR APPEND AS #1 2770 PRINT #1,PT(1),PT(2),PT(3),PT(4),PT(5) 2780 CLOSE #1 2790 END

APPENDIX F

TITRATIONS AND OTHER EXPERIMENTAL PROCEDURES

A. Mohr Titration for Hydrobromic Acid Concentration

The hydrobromic acid concentration was determined after sparging the aqueous hydrobromic acid solution in the storage tank with nitrogen, to insure that the correct concentration was still present in the solution. The Mohr titration method was used [21]. This method involves titration with silver nitrate, with a sodium chromate indicator.

B. Titration for Bromine

The bromine concentration was measured before and after each experiment to determine whether any bromine had evaporated from the aqueous hydrobromic acid and bromine solution. This was done through titrations with sodium thiosulfate and a potassium iodide indicator. The method used is the same as the method used by LaHurd [22] for determination of chlorine concentration, except the sodium thiosulfate concentration for titration was 0.1 molar and 0.2 ml solution samples were used.

C. Platinizing the Platinum Screen

The platinum hydrogen electrode was platinized and activated using the electrochemical method of Gileadi [23]. The electrode was activated by polarizing anodically and cathodically dilute sulfuric acid prior to each experiment.

APPENDIX G

SAMPLE CALCULATIONS

I. Bromide Solution Concentrations

The bromide species concentrations were calculated for a 48% HBr charge capacity solution in the following manner.

The basis used in these calculations was 100 g. of solution. This initial solution is composed of 48 g. HBr, and 52 g. water. The solution was then hypothetically charged to form bromine, with the assumption that all of the hydrogen ions released in the reaction

HBr $\ddagger 1/2 H_2 + 1/2 Br_2$

had been transported through the membrane and were no longer present in the solution. It was also assumed that the amount of water in the solution is unchanging. The concentrations were determined for solutions where the reported weight fractions excluded the weight of bromine, and for solutions where the reported weight fraction included the weight of bromine.

The molecular weights used in the calculations are 80.917 for HBr and 159.818 for bromine.

1.1 Reported Concentrations Excluding Bromine Weight

Because computer programs OCV1, OCVACT, and OCKEFF require the weight fraction of bromine as input to the program, reported concentrations which excluded the weight of bromine were treated in the following manner.

The initial solution was found to have 0.593 moles of HBr. The weight of HBr in the solution was found through iteration by

$$W_{\rm HBr} = X/(X+52)$$
 (G-1)

where X is the reported weight fraction of HBr [9]. The quantity of bromine in the reported solution was found through conservation of bromide ions in the equation

 $1/2(0.593 \text{ moles Br} - W_{HBr}/80.917) 159.818 = W_{Br2}$ (G-2)

where W_i = weight of species i.

Then, the weight fraction of HBr in a solution which includes the weight of Br_2 must be found, so both the HBr and Br_2 concentrations input to the program are defined by the same method. The weight percentage of HBr input to the program was given by

$$X_{HBr} = W_{HBr} / (W_{HBr} + W_{Br2} + W_{H2O})$$
 (G-3)

where X_i is the weight fraction of species i. The weight

fraction of Br₂ is found in the same manner. The solution concentrations found by this method are listed in Table 9.

1.2 Reported Concentrations Including Bromine Weight

Open circuit voltages were calculated for comparison to the data of G. E. [9], using the assumption that the reported weight fractions of HBr included the weight of bromine. These were also the concentrations used in the experimental measurement of the open circuit voltage for various states of charge of a system with a charge capacity of 48% HBr.

The weights of bromine and HBr were calculated from a solution with a known weight percentage of HBr, through the equation

$$X_{HBr} = \frac{W_{HBr}}{1/2(48 - W_{HBr}) 159.818/80.917 + W_{HBr} + 52}$$
(G-4)

which combines the definition of weight fraction with conservation of bromide ions and the first term of the denominator is $W_{\rm Br2}$. Because $X_{\rm HBr}$ was reported, $W_{\rm HBr}$ was found by iteration. The total solution weight is then calculated, along with $X_{\rm Br2}$. The solution concentrations calculated by this method are listed in Table 10.

The solution concentrations used in determining the open circuit voltage of a cell with a charge capacity of 35% HBr were calculated using an equation similar to (G-4). The solution concentrations are given in Table 11.

Table 9. Solution concentrations calculated from weight fractions of HBr that exclude weight of bromine for comparison to data of G. E. [9].

			x _{HBr}	x _{Br2}
Start with 40% HBr at	48% eq.	HBr	34.7	13.2
Start with 20% HBr at	48% eq.	HBr	13.1	34.7
Start with 10% HBr at	48% eq.	HBr	5.8	41.9

State of Charge	x _{HBr}	x _{Br2}
16.7	40	7.95
37.5	30	17.88
58.5	20	27.82
79.2	10	37.76

Table 10. Solution concentrations for various states of charge from 48% HBr charge capacity.

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Table 11. Solution concentrations for various states of charge from 35% HBr charge capacity.

State of Charge	X _{HBr}	X _{Br2}
16.7	29.17	5.78
37.5	21.88	13.02
58.5	14.54	20.21
79.2	7.29	27.49

II. State-of-Charge

The states-of-charge reported in Tables 10 and 11 are calculated from the weight fractions of HBr in solutions which include the weight of Br_2 . The equation used for this calculation is

S.O.C. =
$$100(1-X_{HBr}/X_{HBr}^{O})$$
 (G-5)

where X_{HBr}^{O} is the charge capacity of the solution.

III. Curve fits of Data

Polynomials were estimated from regression of the data of Glass and Boyle [3], and of Glass [6] and Balko [2] to estimate the solution density, bromine solubility limit and activity coefficients of hydrobromic acid. These curve fits were done in APL, and are attached. The vectors given as output are the polynomial coefficients for the equation with the dependent variable to the zeroth, first, second, and, when necessary, third power. DENS 1.017686873 0.04488363995 -4.914449546E-4

DENS + RHO = MEQBR + . * 0 1 2

RHO + 1 1.108 1.25 1.42 1.5 1.57 1.7 1.82 1.9

MEQBE + 0 2 5 10 12 15 20 25 27.5

OF BROMIDE SPECIES OF GLASS AND BOYLE [3]

CURVE FIT OF SOLUTION DENSITY TO MOLAL CONCENTRATION

CURVE FIT OF-GLASS' [6] SOLUBILITY DATA

OF BROMINE IN AQUEOUS HBR

CHBR + 0.2 0.4 0.6 0.8 1.0 1.5 2.0 2.5 3.0

CBR2 + 0.44 0.68 0.91 1.15 1.39 1.95 2.55 3.15 3.90

CURVE + CBR2 E CHBR • . * 0 1 2

CURVE

0,2526794598 1.057577737 0.0487321524

CURVE FIT OF BALKO [2] ACTIVITY COEFFICIENT DATA

IN AQUEOUS HBR

MHBR + 0 1 2 3 5 6 7 8 9

LOGGAM + 0 0.055 0.073 0.229 0.565 0.788 0.915 1.049 1.199

GAMMA + 10 + LOGGAM

Gamma

1 0.881048873 1.183041556 1.6943378 3.672823005 6.137620052 8.222426499 11.19437883 15.81248039

GAMHBR \leftarrow GAMMA \boxminus MHBR \bullet . \star 0 1 2 3

GAMHBR

0.9418152476 0.03224218452 0.045343504 0.015525929

APPENDIX H

EXPERIMENTAL DATA

The results of the experiments to measure the equilibrium of the hydrogen-bromine fuel cell with a charge capacity of 48% HBr are listed in Table 12. They are listed in the order of descending states of charge. The results of the studies to determine the effect of pressure on the open circuit voltage are also included. This Table combines the results obtained using the Nafion 120 membrane electrode assembly and the Nafion 117 membrane.

The results of the experiments to measure the open circuit voltages at various states of charge of a solution with a charge capacity of 35% HBr are listed in Table 13 in the order of descending states of charge. The experiments SPIKE3 and SPIKE4 are included here with the open circuit voltages measured before the addition of bromine.

Experiments SPIKE3 and SPIKE4 were conducted to measure the rates of solution and membrane equilibrium, and the results are given in Table 14. The voltage-time output of the data acquisition program is also given in Table 15. The first column of data is the cell voltage, the second column is the reference to bromine electrodes voltage, and the third column is the time in minutes. The last row of

each data set reported here records the pressure (psig), solution storage temperature (C), weight fractions of HBr and Br_2 , and the temperature at the cell inlet at the completion of the experiment.

The output of experiments PRESCHG, BRPCHG, BRPCHGl, and BRPCHG2 are given in Table 16. In PRESCHG, the hydrogen pressures were changed during operation. In BRPCHG, BRPCHG1, and BRPCHG2 the solution pressures were changed during operation. Equilibrium was reached in experiment BRPCHG1.

The outputs of the experiments LLMMM1 and LLMMS1 are given in Table 17. These experiments compare the effects of a Nafion 120 catalyzed membrane to a Nafion 117 membrane for experiments conducted at 59.2% state of charge of a solution with a charge capacity of 48% HBr.

The data of experiments LLLHM1 and NLHM2 are given in Table 18. LLLHM1 is an experiment for a solution at 79.2% state of charge from a solution with charge capacity of 48% HBr. Equilibrium was not reached during this experiment. NLHM2 is an experiment representing 79.2% state of charge of a solution with a charge capacity of 35% HBr. This was the only experiment conducted at 79.2% state of charge (two liquid phases are present) where equilibrium was reached. The data of experiments LLHLS, MLHLS3, and HLHLS are given in Table 19. These experiments are for a Nafion 117 membrane, solutions with 40% HBr and 7.95% Br₂. The experiments were conducted at hydrogen pressures of 2 psig, 8 psig, and 12 psig.

Table 12. Results of experiments to measure OCV of hydrogen-bromine fuel cell with charge capacity of 48% HBr.

Name	Nafion	Р	Т	X HBr	X Br2	OCV	.Ref.	Time
	(1	osi)	(C)	(%)	(%)	(V)	(V)	(min.)
LLLHM1 .	120	2 ·	24.4	10	37.76	1.062	1.032	175
LLLHM2	120	2	24.4	10	37.76	1.064	1.032	90
LLLLS	117	2	26.5	10	7.95	1.014	0,788	93.5
LLLLS2	117	2	27.2	10	7.95	1.017	0.789	80.5
LLMMM 1	120	2	25.5	20	27.82	0.899	0.898	81.8
LLMMM2	120	2	26.2	20	27.82	0.894	0.889	144.2
LLMMS 1	117	2	26.1	20	27.82	0.898	0.895	82.7
LLNNM1	120	2	24.2	30	17.88	0.815	0.818	31.1
LLNNM2	120	2	24.7	.30	17.88	0.795	0.816	135.2
LLNNM3	120	2	25.4	. 30	17.88	0.796	0.825	150.9
LLHLM	120	2	27.4	40	7.95	0.744	0.611	57.4
LLHLM4	120	2	26.8	÷ 40	7.95	0.74	0.628	117.8
LLHLM5	120	2	26.2	40	7.95	0.732	0.666	90.7
llhlm7	120	2	25.6	40	7.95	0.731	0.75	53.4
LLHLS	117	2	26.5	40	7.95	0.745	0.55	28.5
LLHLS1	117	2	26.8	40	7.95	0.78	0.642	149.7
LLHLS4	117	2	26.2	40	7.95	0.688	0.641	194.9
LLHLS7	117	2	25.5	40	7.95	0.719	0.752	125.9
MLHLM	120	8	27.8	40	7.95	0.741	0.611	210
MLHLS	117	8	26.8	40	7.95			
MLHLS2	117	8	26.6	40	7.95			
MLHLS3	117	8	25.4	40	7.95	0.703	0.615	81.5
HLHLS	117	12	25.6	40	7.95	0.738	0.615	76.5

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Table 13.	Results of experiments to measure	OCV of
	hydrogen-bromine fuel cell with	charge
	capacity of 35% HBr.	

Name	Nafior	I P	T.	X HBr	X Br2	OCV	Ref.	Time
	(psi)	(C)	(%)	(%)	(V)	(V)	(min.)
NLHM 1	yes	2	25	7.29	27.49	1.105	1.051	40
NLHM2	yes	2	24.6	7.29	27.49	1.108	1.045	40.8
NMMM 1	yes	2	24.2	14.54	20.21	0.963	0.95	24.1
NMMM 4	yes	2	24.6	14.54	20.21	0.988	0.939	15.6
NMMM6	yes	2	24.7	14.54	20.21	0.988	0.937	39.7
NMMS1	no	2	25.4	14.54	20.21	0.978	0.94	25.4
NNNM1	yes	2	24.2	21.84	13	0.916	0.876	12.7
NNNM2	yes	2	23.9	21.88	13.02	0.916	0.878	47.4
NHLM1	yes	2	23.7	29.17	5.78	0.854	2.003	57
NHLM2	yes	2	22.9	29.17	5.78	0.855	0.835	12.1
SPIKE3	yes	2	24.2	29.17	5.78	0.853	0.837	53.5
SPIKE4	yes	2	24.4	29.17	5.78	0.854	0.826	36.5

Table 14. Results of rates of solution and membrane equilibrium experiments.

	SPIKE3	SPIKE4
Before Bromine Addition		
X HBr	29.17	29.17
X Br2	5.78	5.78
OCV (V)	0.853	0.854
Ref. (V)	0.837	0.826
Time at Br2 Spike	53.5	36.5
After Bromine Addition		
X HBr	27.58	27.58
X Br2	10.93	10.93
OCV (V)	0.862	0.864
Ref. (V)	0.849	0.837
Time at Equilibrium	84.7	88.7
Temperature (C)	24.6	. 25
Pressure (psi)	2	2

Voltage-time data of experiments SPIKE3 and SPIKE4.

SPIKE 3

VOLTI	VOLT2	MINUTES
0.597283	-0.83569	0.133333
0.649222	-0.83603	0.4
0.697559	-0.83622	0.666666
0.735564	-0.83640	0.933333
0.760565	-0.83657	1.2
0.777463	-0.83677	1.466667
0.784835	-0.83692	1.733333
0.788857	-0.83702	. 2
0.79168	-0.83709	2.266667
0.793963	-0.83713	2.533333
0.795773	-0.83715	2.8
0./9/3/1	-0.83/18	3.066667
0.000/7	~0.83/18	3.333334
0.000947	-0.83/18	3.0
0.802410	-0.03/10	2.00000/
0.804752	-0.83716	4.133333
0.80573	-0.83716	4 666667
0.806640	-0.83713	4.933334
0.807466	-0.83712	5.2
0.808245	-0.83710	5.466667
0.808967	-0.83708	5.733334
0.809636	-0.83706	6
0.810305	-0.83704	6.275
0.810929	-0.837.03	6.55
0.811518	-0.83701	6.816667
0.812101	-0.83699	7.091666
0.812683	-0.83697	7.366667
0.813423	-0.83696	7.633333
0.814227	-0.83695	7.9
0.814967	-0.83693	8.166667
0.815644	-0.83693	8.433333
0.8162/2	-0.83693	8./
0.816843	-0.83692	8.90000/
0.81/303	-0.83689	9.233334
0.01/042	-0.03009	0 766666
0.010330	-0.93690	9./00000
0.010/92	-0.83690	10.00000
0.819751	-0.83690	10.56667
0.820225	-0.83690	10.83333
0.820732	-0.83689	11.1
0.821227	-0.83687	11.36667
0.821733	-0.83687	11.63333
0.822263	-0.83687	11.9
0.822808	-0.83686	12.16667
0.823353	-0.83689	12.43333
0.823959	-0.83688	12.7
0.824563	-0.83688	12.96667
0.825208	-0.83689	13.23333
0.825846	-0.83690	13.5
0.826538	-0.83692	13.76667
0.827266	-0.83692	14.03333
0.828000	-0.83692	14.3
0.828/20	-0.83692	14.5666/
0.829441	-0.03091	14.83333
0.0301/5	-0.03090	15 2667
0.030912	-0.83697	12 43333
0.832396	-0.83685	15.9
	0.00000	× J • J

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0 833132	-0.83685	16 16667
0.833857	-0.83684	16.43333
0.834572	-0.83683	16.7
0.835935	-0.83684	17.23333
0.8365//	-0.83685	17.76667
0.837835	-0.83686	18.03333
0.839034	-0.83689	18.56667
0.839612	-0.83690 -0.83691	18.83333
0.840694	-0.83693	19.36667
0.841710	-0.83697	19.03333
0.842169	-0.83698	20.16667
0.84306	-0.83701	20.7
0.843874	-0.83704	21.23333
0.844243	-0.83705	21.5
0.844942	-0.83708	22.03333
0.845584	-0.83709	22.56667
0.846169	-0.83710	22.83334
0.846437 0.846701	-0.83710 -0.83711	23.36667
0.846954	-0.83709	23.9
0.847449	-0.83708	24.43334
0.84/6/4 0.847875	-0.83706	24./ 24.96667
0.848067	-0.83706	25.23333
0.848430	-0.83705	25.76667
0.848593	-0.83704 -0.83703	26.03333
0.848912	-0.83705 -0.83705	26.56667
0.849225	-0.83705	27.1
0.849487	-0.83704	27.63333
0.84960/	-0.83702 -0.83702	27.9
0.849821	-0.83703	28.43334
0.850003	-0.83703	28.96667
0.850106	-0.83705	29.23333
0.850295	-0.83708	29.76667
0.850442	-0.83708	30.3
0.850513	-0.83709	30.83334
0.850632	-0.83709	31.10833
0.850751	-0.83709	31.65
0.850806	-0.83709	32.18334
0.850909	-0.83708	32.45 32.71667
0.851008	-0.837.09	32.98333
0.8510/2	-0.837 09	33.51667

$\begin{array}{c} 0.851176\\ 0.851217\\ 0.851249\\ 0.851249\\ 0.851249\\ 0.851306\\ 0.851367\\ 0.851444\\ 0.851479\\ 0.851519\\ 0.851594\\ 0.851594\\ 0.851594\\ 0.851743\\ 0.851743\\ 0.851743\\ 0.851743\\ 0.851942\\ 0.851942\\ 0.851942\\ 0.851942\\ 0.851942\\ 0.851942\\ 0.851942\\ 0.851942\\ 0.851942\\ 0.851942\\ 0.851942\\ 0.851942\\ 0.851942\\ 0.852232\\ 0.852235\\ 0.8522333\\ 0.8522333\\ 0.8522333\\ 0.8522333\\ 0.8522333\\ 0.8522333\\ 0.8522333\\ 0.8522333\\ 0.8522333\\ 0.8522333\\ 0.8522333\\ 0.8522333\\ 0.8522333\\ 0.8522333\\ 0.8522333\\ 0.8522333\\ 0.85223377\\ 0.8522333\\ 0.8522333\\ 0.8522335\\ 0.8522333\\ 0.8522333\\ 0.8522333\\ 0.8522333\\ 0.8522333\\ 0.8522333\\ 0.8522333\\ 0.8522333\\ 0.8522333\\ 0.8522333\\ 0.8522333\\ 0.852258\\ 0.852258\\ 0.852258\\ 0.8522578\\ 0.852258\\ 0.852258\\ 0.8522578\\ 0.852258\\ 0.8522578\\ 0.8525258\\ 0.852525$	$\begin{array}{c} - 0.83709\\ - 0.83709\\ - 0.83710\\ - 0.83710\\ - 0.83710\\ - 0.83711\\ - 0.83712\\ - 0.83713\\ - 0.83714\\ - 0.83716\\ - 0.83716\\ - 0.83716\\ - 0.83716\\ - 0.83716\\ - 0.83716\\ - 0.83716\\ - 0.83716\\ - 0.83716\\ - 0.83716\\ - 0.83716\\ - 0.83716\\ - 0.83716\\ - 0.83716\\ - 0.83716\\ - 0.83721\\ - 0.83722\\ - 0.83723\\ - 0.83723\\ - 0.83723\\ - 0.83723\\ - 0.83725\\ - 0.83725\\ - 0.83725\\ - 0.83725\\ - 0.83725\\ - 0.83725\\ - 0.83725\\ - 0.83726\\ - 0.83723\\ - 0.83723\\ - 0.83733\\$	33.78333 34.31667 34.58334 34.85 35.11667 35.38333 35.65 35.91667 36.455 36.71667 36.98333 37.255 37.51667 37.78333 38.057 38.38.057 38.38.057 38.38.057 38.38.057 38.38.057 38.38.057 38.38.057 38.38.057 38.38.057 38.38.057 38.38.057 38.38.057 38.38.057 38.38.057 38.38.057 38.38.057 38.38.333 39.91667 40.183345 40.71667 40.983333 42.55001 42.58334 43.657 43.38333 43.657 43.38333 43.657 44.18334 43.657 44.18334 43.657 44.18333 43.657 44.18333 43.91667 44.18333 43.91667 44.18333 43.657 45.578334 45.578334 45.657 45.578334 45.657 45.578334 45.657 45.578334 45.657 45.578334 45.657 45.578334 45.657 45.78334 45.657 45.578334 45.657 45.578334 45.657 45.578334 45.657 45.578334 45.657 45.578334 45.657 45.578334 45.657 45.578334 45.657 45.578334 45.657 45.78334 45.657 45.78334 45.657 45.78334 45.657 45.78334 45.657 45.78334 45.657 45.78334 45.657 45.78334 45.657 45.78334 45.657 45.78334 45.657 45.78334 45.657 45.78334 45.657 45.78334 45.657 45.78334 45.657 45.78334 45.657 45.78334 45.657 45.78334 45.677 45.787 45.787 45.787 45.787 45.787 45.787 45.787 45.787 45.787 45.787 45.787
0.852528 0.852547 0.852571 0.852588 0.852595 0.852607 0.852617 0.852660 0.852660 0.852660 0.852673 0.852673 0.852797 0.852797 0.852740 0.852784 0.852784 0.852784 0.852784 0.852784 0.852802 0.852847 0.852837 0.852847	$\begin{array}{c} -0.83736\\ -0.83737\\ -0.83737\\ -0.83738\\ -0.83738\\ -0.83738\\ -0.83739\\ -0.83739\\ -0.83739\\ -0.83740\\ -0.83740\\ -0.83740\\ -0.83740\\ -0.83741\\ -0.83741\\ -0.83743\\ -0.83743\\ -0.83743\\ -0.83743\\ -0.83743\\ -0.83743\\ -0.83744\\ -0.83744\\ -0.83745\\ -0.8576\\ -0.8576\\ -0.8576\\ -0.8576\\ -0.8576\\ -0.8576\\ -0.85$	45.25 45.51667 45.78334 46.05001 46.31667 46.58334 46.85 47.11667 47.38334 47.65 47.91667 48.18334 48.45 48.71667 48.98333 49.25 49.51667 49.78334 50.05001 50.31667 50.58334 50.85 51.11667

$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} \textbf{0}, \textbf{0},$
	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$

5.78

24.2

SPIKE4

VOLT1 0.87 0997 0.867 330 0.866 037 0.867 330 0.866 037 0.864 981 0.863 939 0.862 799 0.861615 0.859249 0.859249 0.859249 0.859249 0.853722 0.8532781 0.8522 02 0.8532781 0.8522 02 0.851277 0.851407 0.851407 0.851331 0.851331 0.851331 0.851331 0.851331 0.851331 0.851331 0.851331 0.851409 0.851555 0.851547 0.851555 0.851547 0.851622 0.851622 0.851622 0.851696 0.851775 0.851622 0.851696 0.851775 0.851622 0.851696 0.851775 0.851622 0.851696 0.851817 0.851817 0.851899 0.851914 0.85191	$\begin{array}{c} VOLT2\\ -0.82174\\ -0.82195\\ -0.82235\\ -0.82242\\ -0.82245\\ -0.82245\\ -0.82252\\ -0.82255\\ -0.82255\\ -0.82255\\ -0.82255\\ -0.82255\\ -0.82255\\ -0.82255\\ -0.82255\\ -0.82255\\ -0.82256\\ -0.82256\\ -0.82268\\ -0.822787\\ -0.822308\\ -0.822308\\ -0.822308\\ -0.822308\\ -0.823351\\ -0.823357\\ -0.823396\\ -0.823396\\ -0.82400\\ -0.82410\\ -0.82413\\ -0.82413\\ -0.82416\\ -0.82417\\ -0.82418\end{array}$	MINUTES 0.133333 0.666666 0.933333 1.2 1.466667 1.733333 2.266667 2.533333 3.066667 3.33334 3.866667 4.141667 4.416667 4.416667 4.416667 4.416667 5.225001 5.766667 6.033334 6.5666667 6.033333 6.566667 6.833333 8.455 7.916667 8.183333 8.455 7.916667 8.183333 8.455 7.916667 8.183333 8.455 7.916667 8.183333 8.455 7.916667 8.183333 8.455 7.916667 8.183333 8.455 7.916667 1.7375 7.957 9.916667 8.183333 8.455 7.916667 1.73333 1.06667 1.13333 1.0.6 1.0.86667 1.1.13333 1.2.2 1.2.46667 1.2.73333 1.3 1.2.1 1.2.7 1.3.33 1.3 1.3 1.3 1.3 1.3 1.3
0.851696 0.851748 0.851765 0.851817 0.851809 0.85189 0.851914 0.852030 0.852050 0.852154 0.852196	-0.82413 -0.82414 -0.82415 -0.82416 -0.82416 -0.82416 -0.82417 -0.82417 -0.82418 -0.82419 -0.82420 -0.82419	11.13333 11.4 11.66667 11.93333 12.2 12.46667 12.73333 13.26667 13.53333 13.53333
0.852252 0.852381 0.852466 0.852532 0.852532 0.852587 0.852620 0.852653 0.852714 0.852784 0.852784 0.852899 0.852930	-0.82421 -0.82423 -0.82423 -0.82423 -0.82422 -0.82422 -0.82424 -0.82426 -0.82426 -0.82426 -0.82427 -0.82427 -0.82429	$14.06667 \\ 14.33333 \\ 14.6 \\ 14.86667 \\ 15.13333 \\ 15.4 \\ 15.66667 \\ 15.93333 \\ 16.2 \\ 16.46667 \\ 16.73333 \\ 16.73333 \\ 16.73333 \\ 16.2 \\ 16.733333 \\ 16.733333 \\ 16.73333 \\ 16.73333 \\ 16.73333 \\ 16.73333 \\ 16.733$

	0.852994 -0.82429 17 0.853059 -0.82431 17.26667	7	
	$\begin{array}{c} 0.853100 - 0.82433 & 17.53333\\ 0.853148 - 0.82434 & 17.8\\ 0.853141 - 0.82437 & 18.06667\\ 0.853141 - 0.82437 & 18.06667\\ \end{array}$	3	
	0.853161 -0.82439 18.3333 0.853246 -0.82439 18.6 0.853261 -0.82440 18.86667	3 5 7	
	$\begin{array}{r} 0.853314 & -0.82442 & 19.13333 \\ 0.853360 & -0.82445 & 19.4 \\ 0.853400 & -0.82448 & 19.66667 \end{array}$	3 4 7	· · ·
	0.853445 -0.82448 19.9333 0.853481 -0.82449 20.2 0.853513 -0.82451 20.46667	3	
· · · · · ·	$\begin{array}{c} 0.853541 & -0.82453 & 20.7333 \\ 0.853595 & -0.82454 & 21 \\ 0.853622 & -0.82454 & 21.26667 \end{array}$	3 1 7	
	$\begin{array}{c} 0.853644 & -0.82455 & 21.53333 \\ 0.853660 & -0.82456 & 21.8 \\ 0.853657 & -0.82458 & 22.06667 \\ 0.853657 & -0.82458 & -0.82458 \\ 0.85767 & -0.82458 & -0.82458 \\ 0.85767 & -0.82458 & -0.82458 \\ 0.85777 & -0.82458 & -0.82458$	3 B 7	
	0.853705 - 0.82460 22.8667 0.853735 - 0.82460 22.8667 0.853735 - 0.82460 22.86667 0.853743 - 0.82460 23.1333	+ 6 7 3	
·	0.853768 - 0.82463 23.40 0.853797 - 0.82464 23.66667 0.853816 - 0.82465 23.93334	5 4 7 4	
	0.853839 - 0.82464 24.2 0.853715 - 0.82456 24.46667 0.853715 - 0.82456 24.46667 0.853852 - 0.82465 24.7333 0.853852 - 0.82465 24.7333 0.853852 - 0.855852 - 0.85585852 - 0.85585852 - 0.855858585852 - 0.85585858585858585858585858585858585858	273	
	0.853876 -0.82466 2 0.853883 -0.82468 25.26667 0.85391 -0.82471 25.5333	5 7 3	
	0.853918 -0.82472 25.8 0.853932 -0.82473 26.0667 0.853946 -0.82474 26.33334	3 7 4	
	0.853930 -0.82476 26.6 0.853955 -0.82478 26.86667 0.853973 -0.82480 27.1333	6 7 3	
	0.853984 -0.82483 27.4 0.853978 -0.82485 27.66667 0.853984 -0.82487 27.93334	4 7 4	
	0.853991 -0.82489 28.2 0.854027 -0.82492 28.46667 0.854057 -0.82496 28.7333	2 7 3	
	0.854047 -0.82497 29 0.854060 -0.82501 29.26667 0.854067 -0.82504 29.5333	9 7 、 3	
	$\begin{array}{c} 0.854083 - 0.82508 & 29.8 \\ 0.854093 - 0.82511 & 30.06667 \\ 0.854112 - 0.82514 & 30.33334 \end{array}$	5 7 4	
	$\begin{array}{c} 0.854115 - 0.82517 & 30.6\\ 0.854118 - 0.82520 & 30.86667\\ 0.854127 - 0.82522 & 31.1333\end{array}$	b . 7 3	
	0.63413 - 0.82525 31.66667 0.854139 - 0.82526 31.66667 0.854145 - 0.82530 31.9333	4 7 3	
	$\begin{array}{c} 0.854140 & -0.82532 \\ 0.854150 & -0.82536 \\ 0.85417 & -0.82538 \\ 0.85417 & -0.82538 \\ 0.85416 & -0.82540 \\ $	2 7 3	· .
	0.854107 - 0.82540 33.26667 0.854146 - 0.82543 33.53333 0.854146 - 0.82543 33.53333 0.854146 - 0.82544 333.53333 0.854154 - 0.82544 333.53333 0.854154 - 0.82544 333.53333 0.854154 - 0.82544 - 0.	3	
	$\begin{array}{r} 0.854184 & -0.82547 & 34.06667 \\ 0.854175 & -0.82549 & 34.33334 \end{array}$	5 7 4	

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		<u> </u>
0.854187	-0.82551	34.6
0.8542.02	-0.82552	34.86667
0 854211	-0.82551	35 13333
0.034211	-0.02551	77.17777
0.854191	-0.82553	35.4
0.854175	-0.82555	35.66667
0.854212	-0.82557	35.93334
0 0 5 / 10	0.02555	22072224
0.03419	-0.02555	30.2
0.854202	-0.8255/	30.4666/
0.854196	-0.82559	36.73333
0 858/02	-0.82979	37
0.061022	0.02111	27 26667
0.001000	-0.03303	3/ • 2000/
0.862390	-0.83389	3/ • 53333
0.862575	-0.83443	37.8
0 862633	-0.83478	38 06667
0.002033	0.03470	20.00007
0.802/2/	-0.83208	38.33334
0.862725	-0.83536	38.6
0.862737	-0.83556	38.86667
0 062704	_0.03572	20 1 2 2 2 2
0.002/04	~0.03372	72+17777
0.862830	-0.83286	39.4
0.862901	÷0.83596	39.66667
0.862968	-0.836.01	39.93334
0.002000	- 0 0 2 6 1 5	
0.002010	-0.03013	40.4
0.863047	-0.83623	40.4666/
0.863155	-0.83630	40.73333
0.863227	-0.83637	41
0.0000227	0.03037	11 26667
0.003292	-0.03043	41.2000/
0.86337/	-0.83655	41.53333
0.863452	-0.83661	41.8
0 863514	-0.83664	12 06667
0.0000014	-0.03004	42.00007
0.803334		42.33334
0.863580	-0.83673	42.6
0.863615	-0.83681	42.86667
0 96 36 6 5	-0.83686	12 12222
0.000000	0.00000	
0.863706	-0.83689	43.4
0.863752	-0.83692	43.66667
0.863777	-0.83694	43.93334
0 06 20 16	- 0 93600	10000000 11100
0.000010	-0.03033	11 12227
0.803830	-0.83699	44.4000/
0.863842	-0.83701	44.73333
0 863842	-0.837.06	45
0.0000042	0.037.00	15 96667
0.803890	-0.83708	42.2000/
0.863907	-0.837.09	45.53334
0.863924	-0.83710	45.80001
0 863061		16 06667
0.000000	0.03716	16 22226
0.803903	-0.03/10	40.33334
0.863985	-0.83/15	46.6
0.863998	-0.83717	46.86667
0 864 011	-0 83717	47 13333
0.004011	0.03715	17 10001
0.004000	-0.03/13	47.400.34
0.86402	-0.83/19	4/.68334
0.864029	-0.83723	47.95
0 864 046	-0 83723	48 21667
0.004040	-0.03723	40 40 21007
0.864061	-0.83/24	48.48333
0.864081	-0.83725	48.75
0.864078	-0.83727	49.01667
0 861 001	-0.83727	10 28 221
0.004074	0.03/2/	40 5500
0.004110	-0.03/24	47.33001
0.864124	-0.83729	49.81667
0.864132	-0.83727	50.08334
0 06/100	-0 22720	50.30
0.004132	~ 0.03/23	50 (1(1)
0.004141	-0.03/34	70.0100/
0.864152	-0.83734	50.88333
0.864138	-0.83729	51.15
ñ 86/ n77	-0 83774	51 11667
0.0040/7	-0.03/20	51 (000/
0.864132	11 12 4 1 4 1	
	-0.02124	21.00224

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5.78

24.4

Table 16.

Voltage-time data of experiments PRESCHG, BRPCHG1, BRPCHG2 and BRPCHG.

PRESCHG

1.026392 - 0.78603 0.133333	
1 027309 -0 79536 0 4	
$1 \cdot 027 J 00 - 0 \cdot 70 J J 4 0 \cdot 4$	
$1 \cdot 027814 - 0.78508 0.6666666$	
1.027563 - 0.78494 0.933333	
$1 \cdot 027407 = 0.78485$ $1 \cdot 2$	
$1 \cdot 02/307 = 0 \cdot 78465 + 733333$	
1.027373 - 0.78453 2	
1.027277 -0.78445 2.266667	
1.027406 -0.78424 2.533333	
1.027309 -0.78414 2.8	
$1 \cdot 02/256 = 0.78411 3 \cdot 066667$	
$1 \cdot 02/194 = 0 \cdot /8392 \cdot 3 \cdot 333334$	
$1 \cdot 02/129 = 0 \cdot 78366 = 3.866667$	
1.026626 - 0.78355 4.133333	
1.026408 - 0.78341 4.4	
1.026095 -0.78328 4.666667	
1.025664 - 0.78313 4.933334	
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1.020161 - 0.78241 6.533334	
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1.018149 -0.78280 7.333333	
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1.018091 - 0.78292 7.866667	
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1.019005 - 2.00229 - 10.055555	
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1.015506 -2.00230 11.63333	
1.015203 -2.00229 11.9	
1.017225 - 2.00226 12.16667	
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$1 \cdot 017800 = 2 \cdot 00230 12 \cdot 90007$ 1 017834 = 2 00230 13 23333	
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$\begin{array}{c} 1.018074 - 2.00226 & 14.3067 \\ 1.018002 - 0.75460 & 14.83333 \\ 1.017962 - 0.78301 & 15.1 \\ 1.017786 - 0.78299 & 15.36667 \end{array}$	

1.017722 -0.78298 15.91667 $\begin{array}{c} 1. 017721 & -0.78299 & 16.18333 \\ 1. 017727 & -0.78299 & 16.71667 \\ 1. 017698 & -0.78300 & 17.25 \\ 1. 017694 & -0.78300 & 17.25 \\ 1. 017717 & -0.78300 & 17.51667 \\ 1. 018917 & -0.78300 & 17.51667 \\ 1. 018917 & -0.78303 & 17.78333 \\ 1. 018482 & -0.78311 & 18.31667 \\ 1. 018223 & -0.78311 & 18.58333 \\ 1. 018207 & -0.78314 & 19.11667 \\ 1. 018207 & -0.78314 & 19.11667 \\ 1. 018207 & -0.78315 & 19.91667 \\ 1. 01817 & -0.78316 & 20.18333 \\ 1. 018146 & -0.78315 & 19.91667 \\ 1. 018096 & -0.78316 & 20.18333 \\ 1. 018166 & -0.78316 & 20.71667 \\ 1. 018019 & -0.78316 & 20.71667 \\ 1. 018019 & -0.78316 & 20.71667 \\ 1. 017922 & -0.78317 & 21.25 \\ 1. 017925 & -0.78318 & 21.51667 \\ 1. 017925 & -0.78318 & 21.51667 \\ 1. 017925 & -0.78318 & 21.51667 \\ 1. 01785 & -0.78319 & 22.33334 \\ 1. 017764 & -0.78319 & 22.36667 \\ 1. 017779 & -0.78320 & 23.13333 \\ 1. 017764 & -0.78320 & 23.93334 \\ 1. 017764 & -0.78320 & 23.93334 \\ 1. 017764 & -0.78320 & 23.93334 \\ 1. 017764 & -0.78320 & 23.93334 \\ 1. 017764 & -0.78320 & 24.73333 \\ 1. 017654 & -0.78320 & 25.53333 \\ 1. 017651 & -0.78320 & 25.53333 \\ 1. 017651 & -0.78320 & 25.6667 \\ 1. 017574 & -0.78320 & 25.6667 \\ 1. 017574 & -0.78320 & 25.6667 \\ 1. 017574 & -0.78320 & 25.6667 \\ 1. 017599 & -0.78319 & 27.45 \\ 1. 017439 & -0.78319 & 27.45 \\ 1. 017439 & -0.78319 & 27.45 \\ 1. 017447 & -0.78319 & 27.45 \\ 1. 017447 & -0.78319 & 27.45 \\ 1. 017447 & -0.78319 & 27.45 \\ 1. 017244 & -0.78319 & 27.45 \\ 1. 017244 & -0.78319 & 27.45 \\ 1. 017244 & -0.78319 & 27.45 \\ 1. 017244 & -0.78319 & 27.45 \\ 1. 017244 & -0.78319 & 27.45 \\ 1. 017244 & -0.78319 & 27.45 \\ 1. 017244 & -0.78319 & 27.45 \\ 1. 017244 & -0.78319 & 27.45 \\ 1. 017244 & -0.78319 & 27.45 \\ 1. 016365 & -0.78307 & 31.4667 \\ 1. 015298 & -0.78307 & 31.4667 \\ 1. 016477 & -0.78317 & 32.75 \\ 1. 016501 & -0.78314 & 33.28333 \\ 1. 016677 & -0.78314 & 33.28333 \\ 1. 016677 & -0.78314 & 33.28333 \\ 1. 016571 & -0.78314 & 33.28333 \\ 1. 016571 & -0.78314 & 33.28333 \\ 1. 016571 & -0.78314 & 33.28333 \\ 1. 016571 & -0.78314 & 33.28333 \\ 1. 016571 & -0.78314 & 33.2833$

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$\begin{array}{c} 1 \cdot 014289 \\ 1 \cdot 014238 \\ 1 \cdot 013796 \\ 1 \cdot 013809 \\ 1 \cdot 01387 \\ 1 \cdot 014083 \\ 1 \cdot 01446 \\ 1 \cdot 015062 \\ 1 \cdot 01553 \\ 1 \cdot 01553 \\ 1 \cdot 015047 \\ 1 \cdot 014673 \\ 1 \cdot 015251 \\ 1 \cdot 015251 \\ \end{array}$	$\begin{array}{c} -0.78006\\ -0.78003\\ -0.78003\\ -0.78003\\ -0.78003\\ -0.78003\\ -0.78003\\ -0.78003\\ -0.78003\\ -0.78005\\ -0.78005\\ -0.78005\\ -0.78007\\ -0.7$	23.05 23.91667 24.18334 24.45 24.71667 24.98333 25.25 25.51667 25.78333 26.05 26.325 26.6 26.8667
$\begin{array}{c} 1 \cdot 014262 \\ 1 \cdot 014303 \\ 1 \cdot 013443 \\ 1 \cdot 013551 \\ 1 \cdot 013501 \\ 1 \cdot 013931 \\ 1 \cdot 014311 \\ 1 \cdot 013771 \\ 1 \cdot 013394 \\ 1 \cdot 013377 \\ 1 \cdot 013435 \\ 1 \cdot 013435 \\ 1 \cdot 013815 \end{array}$	$\begin{array}{c} -0.78008\\ -0.78009\\ -0.78009\\ -0.78009\\ -0.78010\\ -0.78010\\ -0.78010\\ -0.78011\\ -0.78013\\ -0.78013\\ -0.78017\\ -0.78011\\ \end{array}$	27.13333 27.4 27.66667 27.93334 28.2 28.46667 28.73333 29.26667 29.53333 29.26667 29.53333 29.3333 29.3334
$\begin{array}{c} 1 \cdot 01 3696 \\ 1 \cdot 01 3601 \\ 1 \cdot 014727 \\ 1 \cdot 015285 \\ 1 \cdot 01 3364 \\ 1 \cdot 01 3241 \\ 1 \cdot 01 3241 \\ 1 \cdot 01 3287 \\ 1 \cdot 01 3428 \\ 1 \cdot 014239 \\ 1 \cdot 014239 \\ 1 \cdot 016074 \\ 1 \cdot 015146 \\ 1 \cdot 015146 \\ 1 \cdot 013601 \\ \end{array}$	$\begin{array}{c} -0.78013\\ -0.78015\\ -0.78015\\ -0.78015\\ -0.78016\\ -0.78016\\ -0.78016\\ -0.78016\\ -0.78015\\ -0.78015\\ -0.78015\\ -0.78016\\ -0.78016\\ -0.78016\\ -0.78016\\ -0.78016\\ -0.78014\end{array}$	$\begin{array}{c} 30.6\\ 30.86667\\ 31.13333\\ 31.4\\ 31.66667\\ 31.93333\\ 32.2\\ 32.475\\ 32.75\\ 32.75\\ 33.01667\\ 33.28333\\ 33.55\\ 33.81667\\ 34.08334 \end{array}$

original páge is of poor quality

1. $01 36 38$ 1. $01 3427$ 1. $01 4136$ 1. $01 3427$ 1. $01 4136$ 1. $01 3892$ 1. $01 37 08$ 1. $01 391$ 1. $01 3596$ 1. $01 3218$ 1. $01 3131$ 1. $01 3059$ 1. $01 3078$ 1. $01 3078$ 1. $01 3144$ 1. $01 3078$ 1. $01 3144$ 1. $01 302$ 1. $01 3238$ 1. $01 3144$ 1. $01 3255$ 1. $01 3144$ 1. $01 3255$ 1. $01 3144$ 1. $01 3238$ 1. $01 3238$ 1. $01 3238$ 1. $01 3238$ 1. $01 3238$ 1. $01 2924$ 1. $01 2931$ 1. $01 2951$ 1. $01 2953$ 1. $01 2954$ 1. $01 3034$ 1. $01 3059$ 1. $01 3034$ 1. $01 3059$ 1. $01 2977$ 1. $01 2977$ 1. $01 2977$ 1. $01 2944$ 1. $01 2931$ 1. $01 2931$ 1. $01 2931$ 1. $01 2911$ 1. $01 2931$ 1. $01 2931$ 1. $01 2991$ 1. $01 2931$ 1. $01 2991$ 1. $01 2931$ 1. $01 2931$ 1. $01 2931$ 1. $01 29291$ 1. $01 2931$ 1. $01 2931$	$\begin{array}{c} - 0.78 015 \\ - 0.78 016 \\ - 0.78 016 \\ - 0.78 016 \\ - 0.78 016 \\ - 0.78 016 \\ - 0.78 016 \\ - 0.78 016 \\ - 0.78 016 \\ - 0.78 015 \\ - 0.78 016 \\ - 0.78 017 \\ - 0.78 018 \\ - 0.78 021 \\ - 0.78 021 \\ - 0.78 021 \\ - 0.78 033 \\ - 0.78 035 \\ - 0.78 035 \\ - 0.78 035 \\ - 0.78 035 \\ - 0.78 035 \\ - 0.78 035 \\ - 0.78 035 \\ - 0.78 035 \\ - 0.78 036 \\ - 0.78 036 \\ - 0.78 037 \\ - 0.78 038 \\ - 0.78 038 \\ - 0.78 038 \\ - 0.78 039 \\ - 0.78 034 \\ - 0.78 042 \\ - 0.78 042 \\ - 0.78 042 \\ - 0.78 042 \\ - 0.78 042 \\ - 0.78 042 \\ - 0.78 042 \\ - 0.78 042 \\ - 0.78 042 \\ - 0.78 042 \\ - 0.78 042 \\ - 0.78 042 \\ - 0.78 042 \\ - 0.78 042 \\ - 0.78 041 \\ - 0.78 038 \\ - 0.78 038 \\ - 0.78 038 \\ - 0.78 038 \\ - 0.78 038 \\ - 0.78 038 \\ - 0.78 038 \\ - 0.78 038 \\ - 0.78 038 \\ - 0.78 038 \\ - 0.78 041 $	34.61667 34.88333 35.15 35.41667 35.68334 35.95 36.21667 36.48333 36.75 37.01667 37.28333 37.55 37.81667 38.36667 38.3339 9.166677 38.36667 39.39.43334 40.76667 40.23333 40.76667 40.23333 40.76667 41.033334 42.63333 42.63333 42.6667 42.63333 42.99 43.16667 42.63333 44.25 42.6667 42.63333 44.25 45.51667 45.3334 45.657 45.3334 45.657 45.677 45.677 45.677 45.677 45.677 45.677 45.677 45.677 45.677 45
1.012937 1.012919 1.012911 1.012931 1.012909 1.012899 1.012899 1.012896 1.012922 1.012665 1.012295 1.012295 1.012295 1.012199 1.0122024	$\begin{array}{c} -0.78041 \\ -0.78041 \\ -0.78041 \\ -0.78041 \\ -0.78040 \\ -0.78040 \\ -0.78040 \\ -0.78040 \\ -0.78030 \\ -0.78030 \\ -0.78030 \\ -0.78007 \\ -0.78007 \\ -0.78007 \\ -0.78008 \\ -0.7$	$\begin{array}{r} 48.25\\ 48.51667\\ 48.78334\\ 49.05834\\ 49.33334\\ 49.86667\\ 50.13333\\ 50.4\\ 50.66667\\ 50.93334\\ 51.2\\ 51.2\\ 51.46667\end{array}$
1.01205	-0.78007	52.2666
--	----------------------------------	--------------------
1.011984 1.011975	-0.78013 -0.78014	52.5333 52.8000
1.011974 1.011929	-0.78013 -0.78014 -0.78014	53.0666
1.011955	-0.78014 -0.78014 -0.78016	53.8666
1.011886	-0.78014 -0.78012 -0.78002	54.6666
1.011691 1.011639	-0.78008 -0.78008 -0.78007	55.2166
1.011672 1.011605	-0.78008 -0.78008 -0.78008	55.7 56.0166
1.011629	-0.78008 -0.78008 -0.78008	56.5500
1.011578	-0.78008 -0.78007	57.0833
1.011793 1.011741	-0.78012 -0.78021 -0.78023	57.8833
1.011746	-0.78025 -0.78026	58.4166 58.6833
$1 \cdot 011724$ $1 \cdot 011724$ $1 \cdot 011747$	-0.78023 -0.78024 -0.78024	59.2166 59.4833
1.011728 1.011819	-0.78024 -0.78027	59.7 60.3916
1.011974 1.012295 1.011999	-0.78036 -0.78035 -0.78035	61 62 63
1.011987 1.011982	-0.78032 -0.78028	64.4083
1.0121	-0.78030 -0.78033 -0.78044	68.4333
1.012236	-0.78040 -0.78033	69.4333
1.011979 1.011984 1.011736	-0.78032 -0.78033 -0.78021	72.4
1.011331 1.011355	-0.78022 -0.78027	74.2
$1 \cdot 011621$ $1 \cdot 011566$ $1 \cdot 011547$	-0.78041 -0.78045 -0.78046	77.4
1.011581 1.01169	-0.78047 -0.78047	79.4666
$1 \cdot 011317$ $1 \cdot 01145$ $1 \cdot 011432$	-0.78051 -0.78051 -0.78051	81.4666
1.011381	-0.78052 -0.78053	84.4666
$1 \cdot 011315$ $1 \cdot 011324$	-0.78054 -0.78055 -0.78057	86.47
1.011301 1.011355	-0.78057 -0.78058 -0.78057	89.4833 90.4833
1.011353	-0.78059 -0.78060	91.4916 92.
1.011411 1.011474 1.011535	-0.78062	93. 94. 95.
1.011551	-0.78063	96.5083

ORIGINAL PACETIS OF POOR QUALITY



BRPCHG2

VOLT1 1.006635	VOLT2 -0.78051	MINUTES 0.133333
1.011531 1.011434 1.011061	-0.78073 -0.78085 -0.78093	0.4 0.666666 0.933333
1.010758 1.010516 1.010364	-0.78097 -0.78101 -0.78105	1.2 1.466667 1.733333
1.010228 1.010101 1.009986	-0.78102 -0.78098 -0.78097	2.266667 2.533333
1.009894 1.009859 1.009783	-0.78097 -0.78100 -0.78102	2.8 3.066667 3.333334
1.009776 1.009776 1.00975	-0.78103 -0.78104 -0.78104	3.866667 4.133333
1.009787 1.009838 1.00985	-0.78104 -0.78104 -0.78103	4.6666667 4.933334
1.009888	-0.78103 -0.78103 -0.78103	5.466667 5.733334
1.010091 1.010114 1.010146 1.010183	-0.78100 -0.78100 -0.78100 -0.78100	6.266667 6.533334
1.010226 1.010161	-0.78099 -0.78100 -0.78099	7.066667
1.010073 1.010124	-0.78099 -0.78101 -0.78101	7.866667 8.133333 8.408333
1.010228	-0.78099	8.683333

1.01033	-0.78097	8.95
1.010/29 1.010329	-0.78086	9.216667
1.010258	-0.78085	9.75
1.010261	-0.78085	10.28333
1.010283	-0.78083	10.55
1.010325	-0.78082	11.08333
1.010385	-0.78082 -0.78081	11.35
1.010387	-0.78081	11.88333
1.010403	-0.78078	12.41667
1.010417	-0.78075	12.68333
1.010475	-0.78074	13.21667
1.010444	-0.78068	13.75
1.010467	-0.78063	14.025
1.010536	-0.78062	14.56667
1.010672	-0.78060	15.1
1.010683	-0.78058	15.63333
1.010263	-0.78058	15.9 16.16667
1.011047	-0.78062	16.43333
1.011092	-0.78055	16.96667
1.010771	-0.78047 -0.78043	17.25555
1.010759	-0.78043	1/./666/ 18.03333
1.010757	-0.78039 -0.78036	18.3 18.56667
1.01079	-0.78032	18.83333
1.010939	-0.78033	19.36667
1.011046	-0.78029 -0.78029	19.64167
1.011195	-0.78026 -0.78022	20.18333
1.010826	-0.78023	20.71667
1.01087	-0.78021	20.98535
1.011068	-0.78027 -0.78034	21.78333
1.011361	-0.78036 -0.78036	22.05 22.31667
1.011424	-0.78036	22.58334
1.011479	-0.78034	23.11667
1.011522	-0.78035	23.38333
1.010583	-0.78007 -0.78020	23.93334
1.01161	-0.78032	24.46667
1.011701	-0.78039	24.73333
1.011135	-0.78039 -0.78048	25.26667 25.53333
1.01177	-0.78047 -0.78046	25.8
1.011816	-0.78046	26.33334

1.011832	-0.78045	26.0
1.011864	-0.78044	26.8666
1.011872	-0.78049	27 • 1 5 5 5
1.011842	-0.78049	27.6666
1.011869	-0.78047	28.2083
1.011899	-0.78045	28.4833
1.012004	-0.78044	29.0166
1.012081	-0.78041	29.2833
1.012196	-0.78042	29.8166
1.012109	-0.78050	30.0833
1.01205	-0.78048	30.6166
1.01213	-0.78047	30.8833
1.012154	-0.78045	31.4166
1.012138	-0.78043 -0.78042	31.6833
1.012172	-0.78040	32.2166
1.012199	-0.78038	32.4833
1.012156	-0.78035	33.0333
1.012179	-0.78030	33.5666
1.012166	-0.78031	33.8333
1.012182	-0.78029	34.3666
1.012213 1.012229	-0.78028	34.6333
1.012207	-0.78026	35.1666
1.012449	-0.78021 -0.78019	35.4333
1.012318	-0.78026	35.9666
1.012186	-0.78023	36.5083
1.01214	-0.78019	36.7833
1.012159	-0.78017	37.3166
1.012164	-0.78015 -0.78014	37.5833
1.01224	-0.78013	38.1166
1.012249	-0.78012	38.3833
1.01226	-0.78008	38.9166
1.012289	-0.78009 -0.78008	39.1833
1.012196	-0.78007	39.7166
1.012207	-0.78006	40.2
1.0122	-0.78005	40.5166
1.012129	-0.77999	41.0666
1.012193	-0.78000	41.3333
1.012193	-0.77998	41.8666
1.012183	-0.77997	42.1333
1.012234	-0.77994	42.6666
1.012204	-0.77995	42.9333
1.012219	-0.77994	43.4666
1.012208	-0.77994	44.0083

$\begin{array}{c} 012218 & -0.77992 & 44.5500.\\ 012285 & -0.77993 & 44.8166\\ 012331 & -0.77991 & 45.0833\\ 012098 & -0.77992 & 45.3\\ 012381 & -0.77992 & 45.3\\ 012381 & -0.77994 & 45.8833\\ 012381 & -0.77994 & 45.8833\\ 012474 & -0.77990 & 46.4166\\ 012611 & -0.77992 & 46.6833\\ 012631 & -0.77994 & 47.22\\ 012687 & -0.77994 & 47.22\\ 012689 & -0.77994 & 47.22\\ 012654 & -0.77991 & 47.7666\\ 012644 & -0.77990 & 48.0333\\ 012609 & -0.77981 & 48.56666\\ 012644 & -0.77981 & 48.56666\\ 012297 & -0.77973 & 48.8333\\ 1.01235 & -0.77978 & 48.333\\ 1.01235 & -0.77978 & 49.36666\\ 012401 & -0.77979 & 49.6333\\ 1.01235 & -0.77980 & 50.16666\\ 012443 & -0.77980 & 50.16666\\ 012443 & -0.77981 & 50.4466\\ 1.01244 & -0.77981 & 50.4466\\ 1.012424 & -0.77981 & 50.4466\\ 1.012424 & -0.77972 & 51.5166\\ 1.01243 & -0.77972 & 51.5166\\ 1.012031 & -0.77972 & 51.5166\\ 1.012039 & -0.77974 & 52.3506\\ 1.012039 & -0.77974 & 52.3506\\ 1.012106 & -0.77974 & 52.3506\\ 1.012106 & -0.77974 & 52.3506\\ 1.01213 & -0.77973 & 53.1166\\ 1.012234 & -0.77973 & 53.1166\\ 1.012234 & -0.77973 & 53.3833\\ 1.012 - 0.77973 & 53.6583\\ 1.012 - 0.77974 & 52.3506\\ 1.012234 & -0.77973 & 55.2666\\ 1.012234 & -0.77973 & 55.2666\\ 1.012234 & -0.77973 & 55.2666\\ 1.012234 & -0.77973 & 55.2666\\ 1.012234 & -0.77973 & 55.2666\\ 1.012234 & -0.77973 & 55.2666\\ 1.012234 & -0.77973 & 55.2666\\ 1.012234 & -0.77973 & 55.2666\\ 1.012234 & -0.77973 & 55.2666\\ 1.012234 & -0.77993 & 57.146\\ 1.012274 & -0.77993 & 57.146\\ 1.012274 & -0.77993 & 57.146\\ 1.012363 & -0.77993 & 57.146\\ 1.012263 & -0.77993 & 57.146\\ 1.012264 & -0.77993 & 57.146\\ 1.012264 & -0.77993 & 57.333\\ 1.012264 & -0.77993 & 57.4633\\ 1.012264 & -0.77993 & 57.4633\\ 1.012264 & -0.77993 & 57.4663\\ 1.012264 & -0.77993 & 57.4663\\ 1.012264 & -0.77993 & 57.4666\\ 1.012268 & -0.77993 & 59.2833\\ 1.012264 & -0.77993 & 59.2833\\ 1.012264 & -0.77993 & 59.2833\\ 1.012264 & -0.77993 & 59.2833\\ 1.012264 & -0.77993 & 59.2833\\ 1.012264 & -0.77993 & 59.2833\\ 1.012263 & -0.77993 & 59.2833\\ 1.012263 & -0.77993 & 59.2833\\ 1.012263 & -0.77993 & 59.2833\\ 1.012264 & -0.77993 & 59.2833\\$
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7.95

26.8

BRPCHG

VOLT1 1.035629 1.031636 1.029017 1.027204 1.025317 1.024494 1.0236933 1.022933 1.022137 1.0222933 1.022137 1.0220289 1.019267 1.017564 1.017564 1.017564 1.0176887 1.016887 1.016793 1.016755 1.016655	VOLT2 -0.77984 -0.78057 -0.7807 -0.78087 -0.78104 -0.78106 -0.78101 -0.78097 -0.78091 -0.78078 -0.78050 -0.78057 -0.78050 -0.78050 -0.78051 -0.78054 -0.78051 -0.7805	MINUTES 0.133333 0.4 0.666666 0.933333 1.2 1.466667 1.733333 2.266667 2.533333 3.066667 3.33334 3.6 3.866667 4.133333 4.4 4.666667 4.93334 5.2 5.466667 5.733334
$\begin{array}{c} 1.01604\\ 1.015997\\ 1.015956\\ 1.015943\\ 1.015915\\ 1.015915\\ 1.015905\\ 1.015905\\ 1.015846\\ 1.015782\\ 1.015782\\ 1.015782\\ 1.015756\\ 1.015756\\ 1.015528\\ 1.015528\\ 1.015544\\ 1.015528\\ 1.015528\\ 1.015523\\ $	$\begin{array}{c} -0.77985 \\ -0.77982 \\ -0.77979 \\ -0.77979 \\ -0.77976 \\ -0.77967 \\ -0.77967 \\ -0.77966 \\ -0.77966 \\ -0.77966 \\ -0.77966 \\ -0.77955 \\ -0.77955 \\ -0.77955 \\ -0.77955 \\ -0.77947 \\ -0.77946 \\ -0.77946 \\ -0.77946 \\ -0.77944 \\ -0.77944 \\ -0.77944 \\ -0.77944 \\ -0.77944 \\ -0.77944 \\ -0.77944 \\ -0.77944 \\ -0.77944 \\ -0.77944 \\ -0.77944 \\ -0.77944 \\ -0.77944 \\ -0.77944 \\ -0.77937 \\ -0.77937 \\ -0.77937 \\ -0.77936 \\ -0.7$	$\begin{array}{c} 8.416667\\ 8.683333\\ 8.95\\ 9.216667\\ 9.483334\\ 9.75\\ 10.01667\\ 10.28333\\ 10.55\\ 10.81667\\ 11.08333\\ 11.35\\ 11.61667\\ 11.08333\\ 11.35\\ 12.15\\ 12.425\\ 12.7\\ 12.96667\\ 13.23333\\ 13.5\\ 13.76667\\ 14.03333\\ 13.5\\ 13.76667\\ 14.83333\\ 15.1\\ 15.36667\\ 15.63333\\ 15.1\\ 15.36667\\ 15.63333\\ 15.90833\\ 16.45\\ 16.71667\\ \end{array}$

1.015438	-0.77936	16.983
1.015269	-0.77935 -0.77936	17.516
1.015355	-0.77936 -0.77936	18.316
1.01533 1.015367	-0.77936 -0.77936	18.583 18.
1.015497 1.015699	-0.77936 -0.77936	19.116
1.01591	-0.77936 -0.77937	19.666
1.014947 1.014952	-0.77934 -0.77931	20 20.466
1.014956	-0.77931	20.733
1.014887	-0.77934	21.266
1.015001 1.015119	-0.77936 -0.77936	21 22.066
1.015255	-0.77937 -0.77937	22.333
1.015094 1.015209	-0.77937	23.133
1.015218 1.015249	-0.77934	23.683
1.015294	-0.77933 -0.77936	24.216
1.015467 1.015205	-0.77939 -0.77937	24. 25.016
1.015297 1.015244	-0.77937 -0.77936	25.283
1.015622 1.015528	-0.77940 -0.77941	25.816 26.083
1.015181	-0.77941 -0.77939	26. 26.6
1.015292	-0.77940	26 27•166
1.016075 1.015382	-0.77944 -0.77945	27.433
1.014951	-0.77951 -0.77953	27.966
1.014829	-0.77955	28.766
1.014764 1.014731	-0.77955 -0.77955	29.033
$1 \cdot 014832$ $1 \cdot 014838$ $1 \cdot 014758$	-0.77955	29.833
1.0147	-0.77959	30.366
1.014892	-0.77970	30.908
1.014771	-0.77970 -0.77969	31. 31.716
1.01474 1.014766	-0.77973	31.983 32.
1.014718 1.01469	-0.77970 -0.77971	32.516 32.783
1.014726 1.014731	-0.77969 -0.77973	33. 33.316
1.014719 1.014646	-0.77975 -0.77974	33.583 33.
1.014632 1.014658	-0.77978 -0.77973	34.1 34

$\begin{array}{c} 1.014609\\ 1.014617\\ 1.014624\\ 1.014663\\ 1.014652\\ 1.014651\\ 1.014595\\ 1.014595\\ 1.014576\\ 1.014576\\ 1.014576\\ 1.014576\\ 1.014556\\ 1.014463\\ 1.014443\\ 1.014449\\ 1.014409\\ 1.014405\\ 1.014348\\ 1.014441\\ 1.014441\end{array}$	-0.77975 -0.77978 -0.77981 -0.77982 -0.77979 -0.77982 -0.77982 -0.77982 -0.77982 -0.77980 -0.77980 -0.77980 -0.77980 -0.77980 -0.77980 -0.77983 -0.77983 -0.77983 -0.77983 -0.77983 -0.77983 -0.77983 -0.77983 -0.77983 -0.77983 -0.77983 -0.77983 -0.77983 -0.77983 -0.77983 -0.77983 -0.77983 -0.77983	$\begin{array}{c} 34.66667\\ 34.9334\\ 35.2\\ 35.46667\\ 35.73333\\ 36.26667\\ 36.53333\\ 36.8\\ 37.06667\\ 37.33334\\ 37.60833\\ 37.88333\\ 38.15\\ 38.41667\\ 38.68334\\ 38.95\\ 39.21667\\ 39.48333\\ \end{array}$	
1.014544	~0.77982	39.75	-7
Z	20	10	/

7.95 26.7

Voltage-time data of experiments LLMMM1 and LLMMS1.

LLMMM1

VOLT1	VOLT2	MINUTES
0.915172	-0.89539	0.133333
0.914685	-0.89610	0.4
0.913502	-0.89628	0.666666
0.912181	-0.89635	0.933333
0.910914	-0.89639	1.2
0.909819	-0.89642	1.466667
0.909042	-0.89644	1.733333
0.908435 0.907962	-0.89645 -0.89646 -0.89650	2 • 2666667
0.907137	-0.89651	2.555555 2.8 3.066667
0.906410	-0.89656	3.866667 3.866667
0.906135	-0.89656	4.133333
0.905910	-0.89656	4.4
0.905796	-0.89656	4.6666667
0.905656	-0.89656	4.933334
0.905941	-0.89654	5.2
0.905442	-0.89654	5.475001
0.905310	-0.89657	5.75
0.90513	-0.89660	6.016667
0.905034	-0.89665	6.283334
0.905008	-0.89669 -0.89672 -0.89676	6.55 6.816667 7.091666
0.904921 0.904858	-0.89679	7.366667
0.904813	-0.89681 -0.89682 -0.89684	8.166667 8.441667
0.904805	-0.89686	8.716667
0.904747	-0.89687	8.983334
0.904763	-0.89689	9.25
0.904792	-0.89691	9.516666
0.904735	-0.89695	9.783333
0.904689	-0.89696	10.05
0.904692	-0.89697	10.31667
0.904599	-0.89700	10.58333
0.904610	-0.89701	10.85
0.904692 0.904691 0.904732	-0.89699 -0.89698 -0.89698	11.11667 11.38333
0.904862	-0.89700 -0.89700 -0.89700	11.91667 12.18333
0.904825	-0.89705	12.725
0.904917	-0.89708	13.53333
0.904953	-0.89709	13.8
0.905032	-0.89710 -0.89712 -0.89715	14.00007
0.905057	-0.89/16	14.86667
0.905202	-0.89715	15.13333
0.905344	-0.89715	15.4
0.905332	-0.89716 -0.89716	15.66667

Table 17.

0.90266 0.902561 0.902464 0.902302 0.9022302 0.902036 0.901930 0.901745 0.901635 0.901433 0.901291 0.901291 0.90295 0.900731 0.900509	$\begin{array}{c} - \ 0.89747 \\ - \ 0.89745 \\ - \ 0.89746 \\ - \ 0.89747 \\ - \ 0.89747 \\ - \ 0.89747 \\ - \ 0.89747 \\ - \ 0.89746 \\ - \ 0.89746 \\ - \ 0.89746 \\ - \ 0.89744 \\ - \ 0.897$	$\begin{array}{c} 33.81667\\ 34.08334\\ 34.35\\ 34.61667\\ 34.88333\\ 35.15\\ 35.41667\\ 35.68334\\ 35.95\\ 36.225\\ 36.5\\ 36.76667\\ 37.03333\\ 37.3\\ 37.56667\\ \end{array}$
0.899990 0.899822 0.899643 0.899643 0.899775 0.899570 0.899316 0.899316 0.899215 0.891774 0.895972 0.898412 0.898412 0.898046 0.897639 0.897639	-0.89749 -0.89749 -0.89751 -0.89750 -0.89755 -0.89755 -0.89755 -0.89756 -0.89767 -0.89761 -0.89762 -0.89765 -0.89766 -0.89766 -0.89766	$\begin{array}{c} 38.1\\ 38.36667\\ 38.663333\\ 38.9\\ 39.16667\\ 39.44167\\ 39.71667\\ 39.98333\\ 40.25\\ 40.51667\\ 40.78333\\ 41.05\\ 41.31667\\ 41.58334\\ \end{array}$
$\begin{array}{c} 0.896904\\ 0.896485\\ 0.896485\\ 0.895889\\ 0.895855\\ 0.895557\\ 0.895312\\ 0.895312\\ 0.895344\\ 0.895329\\ 0.895229\\ 0.8955320\\ 0.895525\\ 0.8955525\\ 0.895525\\ 0.895525\\ 0.895525\\ 0.895525\\ 0.895525\\ 0.89$	-0.89768 -0.89767 -0.89765 -0.89765 -0.89764 -0.89764 -0.89765 -0.89765 -0.89765 -0.89776 -0.89773 -0.89774 -0.89774	$\begin{array}{r} 41.85\\ 42.11667\\ 42.38333\\ 42.65\\ 42.91667\\ 43.18334\\ 43.45\\ 43.71667\\ 43.98333\\ 44.25\\ 44.51667\\ 44.78334\\ 45.05001\\ 45.31667\\ 45.58334 \end{array}$
0.895800 0.895800 0.896148 0.896148 0.896308 0.896432 0.896432 0.897098 0.897320 0.897240 0.897240 0.897242 0.897484 0.897522 0.897577 0.897664 0.8976852	-0.89774 -0.89773 -0.89773 -0.89773 -0.89776 -0.89776 -0.89776 -0.89777 -0.89777 -0.89777 -0.89777 -0.89777 -0.89777 -0.89777 -0.89777 -0.89773 -0.89774	43.05 46.11667 46.38333 46.65 46.91667 47.18334 47.45 47.71667 47.98333 48.25 48.51667 48.78334 49.05001 49.31667 49.58334 49.65 50.11667 50.38333
0.897875 0.897902 0.897909	-0.89775 -0.89776 -0.89776	50.01 50.91667 51.18334

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27.82

25.5

LLMMS1

VOLT1 0.937486 0.933187 0.927827 0.922100 0.916769 0.914635 0.909874 0.904217 0.900339 0.897878 0.896297 0.895114 0.895114 0.894202	VOLT2 -0.89026 -0.89044 -0.89079 -0.89126 -0.89204 -0.89260 -0.89281 -0.89317 -0.89362 -0.89399 -0.89426 -0.89444 -0.89461	MINUTES 0.133333 0.4 0.6666666 0.933333 1.2 1.466667 1.733333 2.266667 2.533333 2.8 3.066667 3.333334
0.893431 0.892973 0.892652 0.892470 0.892380 0.8922881 0.892265 0.892273 0.892273 0.89225 0.89225 0.89229 0.892412 0.892412 0.892462 0.892472 0.892472 0.892478 0.892478	-0.89497 -0.89502 -0.89509 -0.89509 -0.89509 -0.89518 -0.89531 -0.89532 -0.89532 -0.89536 -0.89539 -0.895555 -0.895555 -0.895555 -0.895555555 -0.89555555555555555555555555555555555555	$\begin{array}{r} 3.875 \\ 4.15 \\ 4.416667 \\ 4.683334 \\ 4.95 \\ 5.216667 \\ 5.483334 \\ 5.75 \\ 6.025 \\ 6.3 \\ 6.566667 \\ 6.833333 \\ 7.1 \\ 7.366667 \\ 7.633333 \\ 7.9 \\ 8.175 \end{array}$
0.892392 0.892345 0.892402 0.892293 0.892375 0.892412 0.892610 0.892610 0.892507 0.892507 0.892505 0.892515 0.892515 0.892719 0.892735 0.892749 0.892749	$\begin{array}{c} - 0.89557 \\ - 0.89557 \\ - 0.89562 \\ - 0.89560 \\ - 0.89561 \\ - 0.89562 \\ - 0.89562 \\ - 0.89562 \\ - 0.89564 \\ - 0.89564 \\ - 0.89569 \\ - 0.89570 \\ - 0.89570 \\ - 0.89577 \\$	8.45 8.716667 9.983334 9.25 9.516666 9.783333 10.05 10.31667 10.58333 10.85 11.11667 11.38333 11.65 11.91667 12.18333 12.45 12.71667
0.892836 0.892881 0.892931 0.893006 0.893209 0.893016 0.893213 0.893117 0.893169 0.893169 0.893149 0.893214 0.893361 0.893390 0.893284	-0.89577 -0.89579 -0.89580 -0.89586 -0.89586 -0.89586 -0.89586 -0.89585 -0.89585 -0.89583 -0.89584 -0.89584 -0.89584 -0.89584 -0.89584 -0.89584 -0.89584 -0.89585	$\begin{array}{c} 12.98333\\ 13.25\\ 13.51667\\ 13.78333\\ 14.05\\ 14.31667\\ 14.58333\\ 14.85\\ 15.11667\\ 15.38333\\ 15.65\\ 15.91667\\ 16.18333\\ 16.45\\ 16.71667\\ \end{array}$

0.893216 0.893194 0.893214 0.893246 0.893257 0.893286 0.893304 0.893304 0.893343 0.893437 0.893437 0.893483 0.893483 0.893570 0.893651 0.893656	$\begin{array}{c} -0.89587\\ -0.89588\\ -0.89588\\ -0.89588\\ -0.89588\\ -0.89589\\ -0.89589\\ -0.89590\\ -0.89590\\ -0.89590\\ -0.89590\\ -0.89590\\ -0.89588\\ -0.89588\\ -0.89588\\ -0.89588\\ -0.89588\\ -0.89588\\ -0.89592\\ -0.89594\end{array}$	16.9833317.2517.5166717.7833318.0518.3166718.5833318.8519.1166719.3833319.6519.9166720.1833320.4520.7166720.9833321.2521.5166721.78333
0.893688 0.893867 0.893796 0.893796 0.893657 0.893657 0.893676 0.893676 0.893676 0.893676 0.893676 0.893676 0.893676 0.893749 0.893749 0.893747 0.893772	$\begin{array}{c} -0.89595 \\ -0.89596 \\ -0.89595 \\ -0.89595 \\ -0.89595 \\ -0.89595 \\ -0.89594 \\ -0.89594 \\ -0.89594 \\ -0.89591 \\ -0.8$	22.03 22.31667 22.58334 22.85 23.11667 23.38333 23.65 23.91667 24.18334 24.45 24.71667 24.98333 25.25 25.51667 25.78333 26.05 26.31667
0.893789 0.893797 0.893795 0.893830 0.893872 0.893808 0.893904 0.893904 0.893904 0.894088 0.894109 0.894118 0.894115 0.894115 0.894165 0.894110	-0.89591 -0.89590 -0.89590 -0.89591 -0.89590 -0.89590 -0.89590 -0.89589 -0.89588 -0.89588 -0.89588 -0.89586 -0.89585 -0.89585 -0.89585 -0.89585 -0.89582 -0.89582	26.58334 26.85 27.11667 27.38333 27.65 27.91667 28.18334 28.45 28.71667 28.98333 29.25 29.51667 29.78333 30.05 30.31667 30.38334
0.894110 0.894137 0.894131 0.894131 0.894111 0.894113 0.894164 0.894163 0.894163 0.894163 0.894147 0.894173 0.894139 0.894614	-0.89582 -0.89581 -0.89581 -0.89581 -0.89580 -0.89578 -0.89578 -0.89578 -0.89578 -0.89577 -0.89577 -0.89577 -0.89577 -0.89576 -0.89565	30.85 31.11667 31.38333 31.65 31.91667 32.18334 32.45 32.71667 32.98333 33.25 33.51667 33.78333 34.05 34.31667

0.896773 0.897249 0.897255 0.897255 0.897142 0.897255 0.897142 0.895250 0.8957170 0.895980 0.8959170 0.895980 0.8958450 0.89584500 0.8955400 0.8955400 0.8955400 0.8955400 0.8955400 0.8955400 0.8955400 0.8955400 0.8955400 0.8955400 0.8955400 0.8955400 0.8955400 0.8955400 0.89550910 0.8955097 0.89551010 0.8955138 0.895138 0.895138 0.895140 0.895138 0.895140 0.895104 0.89510500 0.89510500 0.895107 0.8951040 0.8951040 0.8955050 0.895107 0.895107 0.8951040 0.895107	$\begin{array}{c} - \ 0.89516 \\ - \ 0.89516 \\ - \ 0.89516 \\ - \ 0.89516 \\ - \ 0.89516 \\ - \ 0.89516 \\ - \ 0.89516 \\ - \ 0.89516 \\ - \ 0.89536 \\ - \ 0.89536 \\ - \ 0.89536 \\ - \ 0.895536 \\ - \ 0.895536 \\ - \ 0.895536 \\ - \ 0.895536 \\ - \ 0.895552 \\ - \ 0.895552 \\ - \ 0.895552 \\ - \ 0.8895552 \\ - \ 0.8895552 \\ - \ 0.8895552 \\ - \ 0.8895552 \\ - \ 0.8895556 \\ - \ 0.889556 \\ - \ 0$	34.58334 34.85 35.11667 35.38333 35.65 35.91667 36.18334 36.45 36.45 36.71667 37.78333 37.657 37.78333 38.31667 39.39667 39.39.667 39.39.667 39.39.667 40.21667 40.21667 40.21667 40.21667 40.21667 40.21667 41.01667 41.28333 41.55 42.61667 42.88334 43.15 43.41667 42.61667 43.435 43.41667 42.61667 43.435 43.41667 43.435 43.41667 45.28334 45.550067 46.88334 45.55007 46.61667 45.28334 45.55007 46.61667 46.88334 47.15 47.41667 47.4167 47.4167 47.4167 47.4167 47.4167
0.891883 0.893792 0.894827 0.895683 0.896168 0.896168	-0.89500 -0.89584 -0.89575 -0.89568 -0.89566 -0.89566	47.41007 47.68334 47.95 48.21667 48.48333 48.75
0.896427 0.896427 0.896470 0.896411 0.896376 0.896667	-0.89569 -0.89569 -0.89568 -0.89570 -0.89571 -0.89571	49.01667 49.28334 49.55001 49.81667 50.08334
0.896693 0.896442 0.896243 0.896367 0.896532	-0.89571 -0.89571 -0.89573 -0.89573 -0.89575 -0.89575	50.35 50.61667 50.88333 51.15 51.41667
0.896395 0.896657	-0.89575 -0.89572	51.68334

c - 3

0.000000000000000000000000000000000000	6777777777777777777777777777777777777		395766311 395766313339956611 395766313339956611 395766313339956611 395766313339956611 39556116100 395556110000 39555561100000 39555556100000000000000000000000000000000	3 52 3 52 5 52 5 53 5 55 5	6376376633663166376637663766376316336366666666	735741745735745735741745735741573574533344747777777777
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27.82

26.1

Voltage-time data of experiments LLLHM1 and NLHM2.

LLLHM1

VOLTI	VOLT2	MINUTES
1.070117	-1.02576	0.133333
$1 \cdot 0/1407$ 1 071317	-1.02764	0.4
1.070323	-1.02937	0.933333
1.069035	-1.02981	1.2
1.065995	-1.03002	1.466667
1.064391	-1.03007	2
1.062597	-1.03007	2.266667
1.059599	-1.03013	2.955555
1.058268	-1.03018	3.066667
1.055319	-1.03021	3.333334
1.053785	-1.03019	3.866667
1.051224	-1.03020	4.133333
1.050381	-1.03022	4.666667
1.049301	-1.03021	4.933334
1.049002	-1.03025	5.466667
1.048993	-1.03025	5.733334
1.048364	-1.03022	6.266667
1.047549	-1.03019	6.533334
1.047431	-1.03022	7.066667
1.046851	-1.03026	7.333333
1.045878	-1.03021	7.866667
1.045509	-1.03019	8.133333
1.046014	-1.03022	8.399999
1.045546	-1.03028	8.933333
1.044734	-1.03030	9.2
1.044724	-1.03028	9.733334
1.045112	-1.03011	10
1.045691	-1.03005	10.26667
1.046286	-1.03006	10.8
1.046517	-1.03004	11.06667
1.051166	-1.03009	11.6
1.051109	-1.03007	11.86667
1.050919	-1.03004	12.13555
1.050954	-1.03003	12.66667
1.050813	-1.03002	12.93335
1.050604	-1.02998	13.46667
1.050574	-1.02998	13./3333
1.050797	-1.03000	14.26667
1.050686	-1.03000	14.53333
1.050285	-1.02998	15.06667
1.049904	-1.02998	15.33333
1.049214	-1.02997	15.86667

1.048976	-1.02998	16.13333
1.048918	-1.02998	16.4
1.048895	-1.02999	16.66667
1.049397	-1.02998	16.93333
1.050067	-1.03001	17.2
1.049252	-1.03007	17.46667
1.049182	-1.03008	17.73333
1.048486 1.04747 1.047751	-1.03008 -1.03010 -1.03012	18.26667 18.53333
1.047734	-1.03014	18.80833
1.047529	-1.03015	19.08333
1.047391	-1.03017	19.35
1.047667	-1.03021	19.61667
1.047641	-1.03022	19.88333
1.047629	-1.03023 -1.03024	20.15
1.047306	-1.03023	20.68333
1.047318	-1.03023	20.95
1.047111	-1.03024	21.21667
1.047976	-1.03025	21.48333
1.047903	-1.03024	21.75
1.047881 1.047682	-1.03025 -1.03025 -1.03027	22.28333 22.55
1.047469 1.047419	-1.03027 -1.03028 -1.03030	22.81667 23.08334
1.047715 1.047998	-1.03030 -1.03030 -1.03036	23.61667 23.88333
1.048085 1.048034	-1.03041 -1.03039 -1.03020	24.15 24.41667 24.68334
1.048793	-1.03014	24.95
1.048889	-1.03013	25.21667
1.049017	-1.03007	25.48333
1.048624	-1.03012	25.75
1.048753	-1.03014	26.01667
1.048695 1.048576	-1.03016 -1.03017	26.28333
1.048676	-1.03002	26.825
1.048684	-1.02999	27.1
1.04847	-1.03000	27.36667
1.048155	-1.03000 -1.03001	27.63333
1.048116	-1.03003	28.16667
1.048594	-1.03003	28.43334
1.048431	-1.03004	28.7
1.048184	-1.03002	28.96667
1.049408	-1.03000	29.23333
1.04936	-1.03003	29.76667
1.049543	-1.03003	30.03333
1.049006 1.048357	-1.03002 -1.03000 -1.03000	30.3 30.56667 30.83334
1.048824	-1.02999	31.1
1.04836	-1.02999	31.36667
1.047266	-1.02998	31.63333
1.047266	-1.02997	31.9
1.046273	-1.03009	32.16667
1.046026	-1.03009 -1.03007	32.43334
1.046386 1.046386 1.045883	-1.03009 -1.03008 -1.03006	33.23333 33.5

$\begin{array}{c} 1 \cdot 045774 \\ 1 \cdot 045718 \\ 1 \cdot 045718 \\ 1 \cdot 046878 \\ 1 \cdot 046986 \\ 1 \cdot 047059 \\ 1 \cdot 047059 \\ 1 \cdot 047059 \\ 1 \cdot 047044 \\ 1 \cdot 047623 \\ 1 \cdot 048102 \\ 1 \cdot 048102 \\ 1 \cdot 048102 \\ 1 \cdot 048154 \\ 1 \cdot 048158 \\ 1 \cdot 048264 \\ 1 \cdot 048158 \\ 1 \cdot 048264 \\ 1 \cdot 048158 \\ 1 \cdot 048254 \\ 1 \cdot 048257 \\ 1 \cdot 048264 \\ 1 \cdot 048257 \\ 1 \cdot 048258 \\ 1 \cdot 048251 \\ 1 \cdot 0505285 \\ 1 \cdot 0520766 \\ 1 \cdot 052219 \\ 1 \cdot 05050412 \\ 1 \cdot 0505041 \\ 1 $	$\begin{array}{c} -1 \cdot 03007\\ -1 \cdot 03006\\ -1 \cdot 03006\\ -1 \cdot 03006\\ -1 \cdot 03007\\ -1 \cdot 03006\\ -1 \cdot 03007\\ -1 \cdot 03010\\ -1 \cdot 03014\\ -1 \cdot 03014\\ -1 \cdot 03014\\ -1 \cdot 03016\\ -1 \cdot 03014\\ -1 \cdot 03016\\ -1 \cdot 02999\\ -1 \cdot 02999\\ -1 \cdot 02994\\ -1 \cdot 02992\\ -1 \cdot 02994\\ -1 \cdot 02992\\ -1 \cdot 02994\\ -1 \cdot 02992\\ -1 \cdot 02991\\ -1 \cdot 02991\\ -1 \cdot 02991\\ -1 \cdot 02991\\ -1 \cdot 02992\\ -1 \cdot 02910\\ -1 \cdot 02914\\ -1 \cdot 02907\\ -1 \cdot 02907$	33.76667 34.03333 34.56667 34.83334 35.36667 35.36667 35.63333 35.63333 36.16667 36.43334 37.23333 37.537 76667 38.333 38.55 39.11667 39.38333 39.65 39.91667 40.18334 40.45 39.91667 40.98333 41.25 41.51667 40.98333 41.25 41.51667 41.78333 42.05001 42.31667 42.38334 43.657 43.38333 43.657 42.38334 43.657 43.38333 43.657 43.38333 43.657 44.18334 43.657 45.255 45.51667 45.78334 45.255 45.51667 45.78334 45.255 45.51667 45.78334 45.255 45.51667 45.78334 45.255 45.51667 45.78334 45.255 45.51667 45.78334 45.255 45.51667 45.78334 45.255 45.51667 45.78334 45.255 45.51667 45.78334 45.255 45.51667 45.78334 45.255 45.51667 45.78334 45.255 45.51667 45.78334 45.255 45.51667 45.78334 45.255 45.51667 45.78334 45.255 45.51667 45.78334 45.255 45.51667 45.78334 45.255 45.51667 45.78334 45.255 45.78334 45.255 45.51667 45.78334 45.255 45.78334 45.255 45.78334 45.255 45.78334 45.255 45.78334 45.255 45.78334 45.255 45.78334 45.255 45.78334 45.255 45.78334 45.255 45.78334 45.255 45.78334 45.255 45.78334 45.255 45.78334 45.255 45.78334 45.255 45.78334 45.255 45.78334 45.255 45.78334 45.255 45.78334 45.255 45.78334 45.255 45.78334 45.657 45.78334 45.657 45.78334 45.657 45.78334 45.657 45.78334 45.657 45.78334 45.657 45.78334 45.657 45.78334 45.657 45.78334 45.657 45.78334 45.657 45.78334 45.657 45.78334 45.657 45.78334 45.657 45.7857 45.7857 45.7857 45.7857 45.7857 45.7857 45.7857 45.7857 45.7857 45.7857 45.7857 45.7857 45.7857 45.7857 45.7857 45.7857 45.78577 45.78577 45.78577 45.78577 45.78577
$\begin{array}{c} 1.034841\\ 1.037377\\ 1.041146\\ 1.044544\\ 1.046229\\ 1.04725\\ 1.04725\\ 1.048304\\ 1.049297\\ 1.049622\\ 1.050778\\ 1.052408\\ 1.051683\\ 1.051683\\ 1.051683\\ 1.050733\\ 1.050696\\ 1.050696\\ 1.050695\\ 1.050649\\ 1.050862\\ 1.051042\\ 1.051042\\ 1.051129\end{array}$	$\begin{array}{c} -1.02898\\ -1.02900\\ -1.02914\\ -1.02914\\ -1.02918\\ -1.02918\\ -1.02918\\ -1.02914\\ -1.02914\\ -1.02907\\ -1.02907\\ -1.02895\\ -1.02895\\ -1.02895\\ -1.02898\\ -1.02898\\ -1.02898\\ -1.02898\\ -1.02896\\$	$\begin{array}{r} 45.51667\\ 45.78334\\ 46.05001\\ 46.31667\\ 46.88334\\ 46.85\\ 47.11667\\ 47.38333\\ 47.65\\ 47.91667\\ 48.19167\\ 48.19167\\ 48.46667\\ 48.73333\\ 49.26667\\ 49.53334\\ 49.80001\\ 50.06667\\ 50.33334\\ 50.6\\ 50.86667\\ 51.13333\end{array}$

1.051285 1.051244 1.051283 1.051215 1.051104	-1.02895 -1.02895 -1.02894 -1.02895 -1.02895 -1.02895	51.4 51.66667 51.93334 52.2 52.46667
1.050786 1.050788 1.050739 1.050736 1.050774 1.050786	-1.02897 -1.02896 -1.02897 -1.02895 -1.02894 -1.02893 -1.02893	52.73333 53.26667 53.53334 53.80001 54.06667 54.33334
1.051667 1.051683 1.051064 1.050939 1.050764 1.051144	-1.02887 -1.02879 -1.02879 -1.02879 -1.02883 -1.02886 -1.02886	54.86667 55.13333 55.4 55.66667 55.93334
1.050999 1.050844 1.050354 1.050096 1.050231 1.050299	-1.02888 -1.02888 -1.02891 -1.02891 -1.02890 -1.02891	56.2 56.46667 56.73333 57.26667 57.53334
1.05033/ 1.05048 1.050714 1.050584 1.05063 1.050574	-1.02891 -1.02891 -1.02891 -1.02891 -1.02891 -1.02891 -1.02891 -1.02891	57.80834 58.09167 58.36667 58.63333 58.9 59.16667 59.43334
1.050736 1.051586 1.051955 1.051112 1.051435 1.051155	-1.02888 -1.02885 -1.02885 -1.02888 -1.02871 -1.02867 -1.02864	59.96667 59.96667 60.6 61.6 62.6 63.6
1.051482 1.051725 1.052016 1.051706 1.05097 1.05102	-1.02862 -1.02858 -1.02856 -1.02851 -1.02845 -1.02845 -1.02840	64.6 65.6 66.6 67.6 68.6 69.6
1.051127 1.051189 1.051162 1.051286 1.051343 1.051548	-1.02835 -1.02830 -1.02826 -1.02824 -1.02821 -1.02818	70.6 71.6 72.6 73.6 74.6 75.6
1.051446 1.051551 1.051589 1.051774 0.65258 0.829189	-1.02816 -1.02815 -1.02813 -1.02814 -1.03085 -1.03375	76.6 77.6 78.6 79.6 80.6 81.6
1.038101 1.058923 1.065687 1.06707 1.067918	-1.03372 -1.02928 -1.02949 -1.02974 -1.02983 -1.02997	82.0 83.6 84.6 85.6 86.6 87.6
1.069025 1.068168 1.068772 1.069227	-1.03010 -1.03030 -1.03035 -1.03043 -1.03055	89.61667 90.61667 91.625 92.63333

1.06878	-1.03071	93.6333
1.06877	-1.03088 -1.03104	95.6333
1.068204 1.068069 1.068611	-1.03122 -1.03130 -1.03118	97.6333 98.6333 99.6333
1.068617	-1.03118 -1.03133	100.633
1.0683/3 1.067849 1.067932	-1.03142 -1.03163 -1.03158	102.633
1.068206 1.068338	-1.03148 -1.03141 -1.03147	105.633
1.067469	-1.03147 -1.03159 -1.03168	108.633
1.067505 1.068459	-1.03164 -1.03133 -1.03156	110.633
1.066994	-1.03179 -1.03178	113.633
1.06/5/5 1.06724	-1.031/5 -1.03188 -1.03218	115.633 116.633 117.633
1.066804 1.066686	-1.03222 -1.03230	118.633
1.066511 1.066812 1.066902	-1.03230 -1.03205 -1.03186	120.641 121.6 122.6
1.066772	-1.03179 -1.03165 -1.03165	123.6
1.068242	-1.03130 -1.03115 -1.03103	126.6
1.068443 1.068598	-1.03103 -1.03090 -1.03089	128.666
1.068574	-1.03086 -1.03086	131.683
1.068508 1.068427	-1.03083 -1.03082 -1.03082	133. 134. 135.708
1.067651	-1.03107 -1.03100	136.716
1.067643	-1.031 -1.03108 -1.03098	138.733 139.741 140.7
1.06776	-1.03105 -1.03101	141.758
1.067588	-1.03092 -1.03085 -1.03083	143.783 144.783 145.791
1.067379 1.067225	-1.03083 -1.03092	146.
1.066766 1.06658 1.066346	-1.03111 -1.03120 -1.03123	149.82
1.066217 1.066305	-1.03132 -1.03125	151.833
1.065905	-1.03163 -1.03163 -1.03175	154.833
1.065649 1.065268	-1.03189 -1.03190 -1.03186	156.833 157.833 158.833

1.065207	-1.03185	159.8333
1.065215	-1.03175	160.8333
1.065084	-1.03181	161.8417
1.064853	-1.03192	162.85
1.064404	-1.03186	164 85
1.064297	-1.03179	165.85
1.064252	-1.03188	166.8583
1.064512	-1.03186	167.8667
1.064496	-1.03187	168.8667
1.064257	-1.03195	170 875
1.063666	-1.03204	171.8833
1.062898	-1.03210	172.8917
1.062567	-1.03219	173.9
1.062602	-1.03215	174.9
1.062004	-1.03213	176 9 083
1.061924	-1.03243	177.9167
1.06212	-1.03243	178.9167
1.062252	-1.03240	179.925
1.061564	-1.03240	180.9333
1.061889	-1.03225	182.9333
0	0	0
2	27.5	10

NLHM2

VOLT1	VOLT2	MINUTES
0	0	0.183333
1.114178	-1.03988	0.833333
1.113501	-1.04034	1.35
1.113023	-1.04114 -1.04152	1.61666/
1,11237	-1.04191	2.15
1.111426	-1.04254	2.683334
1.110895	-1.04281 -1.04301	2.95 3.216667
1.1101	-1.04323	3.4833333
1.109739	-1.04341	4.016667
1.109203	-1.04371 -1.04381	4.283334
1.108802	-1.04391	4.816667
1.108034	-1.04401	5.35
1.108352	-1.04418 -1.04423	5.608334 5.866667
1.108189	-1.04426	6.133333
1.108134	-1.04430	6.666667
1.108049	-1.04437	6.933334 7.2
1.107934	-1.04441	7.466667
1.107878	-1.04445	8
1.107856	-1.04447 -1.04449	8.266666
1.10782	-1.04452	8.8

37.76

24.4

1 107793	-1 04/152	9 066667
1.107791	-1.04454	9.333333
1.107768	-1.04455	9.600001
1.107785	-1.04455	9.866667
1.107787	-1.04452	10.4
1.107811	-1.04451	10.66667
1.107813	-1.04449	11.2
1.107833	-1.04447	11.46667
1.107858	-1.04440	11.75555
1.107863	-1.04444	12.26667
1.107377	-1.04469	12.55555
1.06942	-1.04875	13.06667
1.107625	-1.04923	13.33333
1,107706	-1.04482	13.86667
1.107787	-1.04471	14.13535
1.107821	-1.04466	14.66667
1.107903	-1.04450	14.95555
1.107934	-1.04447	15.46667
1.108104	-1.04442	16.01667
1.108139	-1.04437	16.28333
1.107976	-1.04439	16.81667
1.107951	-1.04441	17.08333
1.107904	-1.04441	17.61667
1.107853	-1.04443	17.88333
1.107802	-1.04444	18.41667
1.107797	-1.04443	18.68333
1.107747	-1.04445	19.21667
1.107749	-1.04446	19.48333
1.107771	-1.04443	20.01667
1.10773	-1.04445	20.28333
1.107726	-1.04448	20.81667
1.107763	-1.04448	21.08334
1.107752	-1.04462	21.61667
1.107711	-1.04467	21.88333
1.107761	-1.04467	22.41667
1.107765	-1.04469	22.68334
1.107761	-1.04467	23.21667
1.107699 1.107717	-1.04479	23.48333
1.107777	-1.04472	24.03333
1.107662	-1.044/5 -1.04491	24.3
1.107414	-1.04529	24.83334
1.107435	-1.04532 -1.04521	25.1
1,107473	-1.04395	25.63333
1.107535	-1.04503 -1.04510	25.9
1.107644	-1.04504	26.43334

$\begin{array}{c} 1 \cdot 1 07746 \\ 1 \cdot 1 07712 \\ 1 \cdot 1 07726 \\ 1 \cdot 1 07726 \\ 1 \cdot 1 07772 \\ 1 \cdot 1 0777 \\ 1 \cdot 1 07772 \\ 1 \cdot 1 0776 \\ 1 \cdot 1 07953 \\ 1 \cdot 1 08212 \\ 1 \cdot 1 08306 \\ 1 \cdot 1 08293 \\ 1 \cdot 1 08306 \\ 1 \cdot 1 08498 \\ 1 \cdot 1 08487 \\ 1 \cdot 1 08599 \\ 1 \cdot 1 08567 \\ 1 \cdot 1 08488 \\ 1 \cdot 1 084478 \\ 1 \cdot 1 08447 \\ 1 \cdot 1 08447 \\ 1 \cdot 1 08447 \\ 1 \cdot 1 08394 \\ 1 \cdot 1 08348 \\ 1 \cdot 1 08478 \\ 1 \cdot 1 08391 \\ 1 \cdot 1 08379 \\ 1 \cdot 1 08379 \\ 1 \cdot 1 08379 \\ 1 \cdot 1 08377 \\ 1 \cdot 1 08464 \\ 1 \cdot 08477 \\ 1 \cdot 1 08464 \\ 1 \cdot 1 08379 \\ 1 \cdot 1 08467 \\ 1 \cdot 1 08379 \\ 1 \cdot 1 08467 \\ 1 \cdot 1 08467 \\ 1 \cdot 1 08379 \\ 1 \cdot 1 08467 \\ 1 \cdot 1 08477 \\ 1 \cdot 1 08466 \\ 1 \cdot 1 08379 \\ 1 \cdot 1 08467 \\ 1 \cdot 1 08466 \\ 1 \cdot 1 08478 \\ 1 \cdot 1 08466 \\ 1 \cdot 1 08477 \\ 1 \cdot 1 08466 \\ 1 \cdot 1 08478 \\ 1 \cdot 1 08466 \\ 1 \cdot 1 08379 \\ 1 \cdot 1 08466 \\ 1 \cdot 1 08477 \\ 1 \cdot 1 08466 \\ 1 \cdot 1 08478 \\ 1 \cdot 1 08466 \\ 1 \cdot 1 08478 \\ 1 \cdot 1 08466 \\ 1 \cdot 1 08478 \\ 1 \cdot 1 08466 \\ 1 \cdot 1 08478 \\ 1 \cdot 1 08466 \\ 1 \cdot 1 08478 \\ 1 \cdot 1 08466 \\ 1 \cdot 1 08478 \\ 1 \cdot 1 08466 \\ 1 \cdot 1 08478 \\ 1 \cdot 1 08466 \\ 1 \cdot 1 08478 \\ 1 \cdot 1 08466 \\ 1 \cdot 1 08466 \\ 1 \cdot 1 08478 \\ 1 \cdot 1 08466 \\ 1 \cdot 1 08478 \\ 1 \cdot 1 08466 \\ 1 \cdot 1 0846 \\ 1 $	$\begin{array}{c} -1 & 04497 \\ -1 & 04508 \\ -1 & 04506 \\ -1 & 04506 \\ -1 & 04501 \\ -1 & 04498 \\ -1 & 04494 \\ -1 & 04494 \\ -1 & 04467 \\ -1 & 04467 \\ -1 & 04465 \\ -1 & 04465 \\ -1 & 04468 \\ -1 & 04466 \\ -1 & 04467 \\ -1 & 04468 \\ -1 & 04468 \\ -1 & 04468 \\ -1 & 04468 \\ -1 & 04468 \\ -1 & 04468 \\ -1 & 04468 \\ -1 & 04468 \\ -1 & 04468 \\ -1 & 04468 \\ -1 & 04468 \\ -1 & 04468 \\ -1 & 04468 \\ -1 & 04466 \\ -1 & 04468 $	$\begin{array}{c} 26.7\\ 26.96667\\ 27.23333\\ 27.5\\ 27.76667\\ 28.03333\\ 28.3\\ 28.3\\ 28.3\\ 28.3\\ 28.3\\ 29.1\\ 29.36667\\ 29.63333\\ 29.9\\ 30.16667\\ 30.43334\\ 30.7\\ 30.96667\\ 31.23333\\ 31.5\\ 31.76667\\ 32.025\\ 32.28333\\ 32.55\\ 32.81667\\ 33.08334\\ 33.35\\ 32.655\\ 32.81667\\ 33.08334\\ 33.35\\ 33.61667\\ 33.88333\\ 34.15\\ 33.61667\\ 33.88333\\ 34.15\\ 33.61667\\ 33.88333\\ 34.15\\ 35.5\\ 35.76667\\ 35.23333\\ 35.5\\ 35.76667\\ 35.3333\\ 36.56667\\ 37.63333\\ 37.9\\ 38.16667\\ 38.43334\\ 38.7\\ 38.9667\\ 39.23333\\ 39.5\\ 39.76667\\ 40.03333\\ 50.5\\ 40.028\\ 4$
1.108356 1.108379 1.108437 1.108464 1.108491 1.108433	-1.04470 -1.04469 -1.04463 -1.04465 -1.04462 -1.04467	39.23333 39.5 39.76667 40.03333 40.56667 40.83334
0	24 4	0 7 29

27.49

24.6

. 187

Table 19.

Voltage-time data of experiments LLHLS, MLHLS3 and HLHLS.

LLHLS

VOLT1	VOLT2	MINUTES
0.811803	-1.73595	0.133333
0.803872	-0.98662	0.666666
0.793659	-0.95230	0.933333
0.789584	-0.92579	1.2
0.785684	-1.08882	1.466667
0.778240	-0.54860	2
0.774435	-0.54924	2.266667
0.767.028	-0.55000	2.533333
0.763878	-0.55027	3.066667
0.761187	-0.55060	3.333334
0.757228	-0.86787	3.866667
0.755792	-0.95755	4.133333
0.687455	-0.55114	4.4
0.752886	-0.91059	4.933334
0.752280	-0.55123	5.2
0.751354	-0.95379	5.733334
0.750987	-0.55113	6
0.750680	-0.55109	6.533334
0.750172	-0.55103	6.8
0,74992	-0.55102	7.066667
0.748690	-0.6996	7.600001
0.748023	-1.10979	7.866667
0.750935	-1.13066	8.416667
0.754592	-1.00772	8.683333
0.754086	-1.12188	8.95
0.710437	-0.96209	9.483334
0.763462	-1.23558	9.75
0.766901	-1.138/1	10.0166/
0.769040	-1.26299	10.55
0.772940	-1.28776	10.81667
0.772417	-1.20634	11.00333
0.776025	-0.95915	11.61667
0.776200	-1.14358	11.88333
0.782823	-0.75161	12.41667
0.783650	-0.54638	12.69167
0.781225	-0.54579	13.23333
0.783468	-0.54843	13.5
0.780995	-0.54888	13.76667
0.7175	-0.54924	14.3
0.718464	-0.54930	14.56667
0.720300) -0.3493/) -0.54961	14.83333
0.752120	<u> - 0.54978</u>	15.36667
0.788781	-0.54983	15.63333

0.776460 0.745286 0.745286 0.745286 0.745174 0.745065 0.744910 0.744910 0.744862 0.7447891 0.7447891 0.744769 0.744769 0.744779 0.744779 0.744770 0.7447730 0.7447730 0.744731 0.744730 0.744731 0.744733 0.744733 0.744733 0.744733 0.744733 0.744735 0.744735 0.744735 0.744735 0.744738 0.744738 0.744755	$\begin{array}{c} - 0.54986 \\ - 0.54985 \\ - 0.54982 \\ - 0.54981 \\ - 0.54981 \\ - 0.54981 \\ - 0.54963 \\ - 0.54963 \\ - 0.54933 \\ - 0.54929 \\ - 0.54929 \\ - 0.54929 \\ - 0.54929 \\ - 0.54929 \\ - 0.54929 \\ - 0.54929 \\ - 0.54926 \\ - 0.54955 \\ - 0.54956 \\ - 0.54956 \\ - 0.54956 \\ - 0.54956 \\ - 0.54956 \\ - 0.54956 \\ - 0.54956 \\ - 0.54966 \\$	$\begin{array}{c} 15.9\\ 16.16667\\ 16.43333\\ 16.7\\ 16.96667\\ 17.23333\\ 17.5\\ 17.775\\ 18.05\\ 18.31667\\ 18.58333\\ 18.85\\ 19.11667\\ 19.38333\\ 19.65\\ 19.91667\\ 20.18333\\ 20.45\\ 20$
2	26.5	40

7.95

26.5

MLHLS3

VOLT1 0.768033	VOLT2 -0.61781	MINUTES 0.133333
0.768873	-0.61732 -0.61696	0.4
0.727802 0.695912	-0.61676 -0.61665 -0.61659	1.2 1.466667
0.663237 0.624117	-0.61656 -0.61655	1.733333
0.555775	-0.61656 -0.61660	2.533333 2.8
0.525135	-0.61660 -0.61661	3.066667 3.333334
0.525266 0.537083	-0.61668 -0.61671	3.866667 4.133333
0.543705 0.551175 0.55869	-0.61672 -0.61673 -0.61676	4.4 4.666667 4.933334
0.566124 0.57392	-0.61678	5.2 5.466667
0.581697 0.589772 0.595322	-0.61678 -0.61678 -0.61677	5.741667 6.025
0.600370	-0.61678 -0.61676	6.566667 6.833 <u>3</u> 33
0.610824 0.613812 0.618863	-0.61674 -0.61672 -0.61671	/.1 7.366667 7.633333
0.624402 0.625852	-0.61670	7.9 8.166667
0.631407	-0.61667 -0.61665 -0.61663	8.433333 8.7 8.966667
0.637081 0.639188	-0.61661	9.233334
0.632628	-0.61658 -0.61656 -0.61653	10.03333
0.637723 0.640181	-0.61652	10.56667 10.83333
0.644498 0.646953	-0.61649 -0.61647 -0.61646	11.36667 11.63333
0.648816 0.651541	-0.61644 -0.61642	11.9 12.175 12.45
0.654778	-0.61638 -0.61635	12.71667 12.98333
0.657980	-0.61633 -0.61631 -0.61630	13.25 13.51667
0.661240	-0.61628 -0.61626	14.05 14.31667
0.663347 0.66443	-0.61625 -0.61623 -0.61621	14.58333 14.85 15.11667
0.666722	-0.61620 -0.61619	15.38333 15.65
0.668306 0.668847	-0.61617 -0.61615	15.91667 16.18333

0.669	43 -	0.6	1615	16.4	58	22
0.000	-5 67 -	0.6	1613	16.7	33	33
0.6719	12 -	0.6	1611	10		í7
0.6723	74 -	0.6	1610	17.2	666	57
)•6/2/).6738	60 - 67 -	0.6	1610	1/.5	33.	33
0,6748	05 -	0.6	1607	18.0	666	57
0.6756	51 -	0.6	1606	18.3	33:	33
J•6/63 J•677(1// - 1/49 -	0.6	1605	18:8	18.	• 0 5 7
0.6776	82 -	0.6	1604	19.1	33	33
0.6783	47 -	0.6	1605	10 6	$\frac{19}{666}$	4
0.6795	39 -	0.6	1603	19.9	33	33
2.6800	67 -	0.6	1602	201	20	2
)•6811	$\frac{12}{43} =$	0.6	1602	20.4	33	33
0.6816	15 -	0.6	1600	21 0		ŽĮ
J•681/ J•6823	85 - 67 -	0.6	1 599	21.2	33)/ 33
0.68	29 -	Ŏ. Ŏ	1598		21	.8
0•6833 1.6837	86 -	0.6	1598	22.0	666 416	57
68 44	04 -	0.6	1597	22.6	166	57
0.6846	45 -	0.6	1596	22.8	83	33
0.685	79 -	0.6	1595	23.4	166	57
0.6862	43 -	0.6	1595	23.6	83	34
J•6866 J•687(00 -	0.6	1 594 s 1 594	24.2	3.1	13 57
0.6873	80 -	Ŏ. Ŏ	1593	24.4	83.	33
)•68/6 1.6881	95 -	0.6	1593	25 0	4.	15
0.688	42 -	ŏ.ĕ	1591	25.2	83	33
)•6887	87 -	0.6	1591	25 8	5.	55
0.6891	82 -	0.6	1589	26.0	83	34
2.6893	64 -	0.6	1589	26 6	6.	35
)•6894	.65 -	0.6	1588	26.8	916	57
0.6896	55 -	0.6	1588	27.1	666	57
J•6897 J•6898	84 - 37 -	0.6	1587	2/.4	27	34
0.6898	<u>87</u> –	0.6	1586	27.9	66	57
)•6900 16899)0/ -	0.6	1586	28.2	33.	33
5. 6898	92 -	0.6	1585	28.7	660	57
0.6900)79 -	0.6	1585	29.0)33:	33
).6902).6909	- 07 - 07	0.6	1583	29.5	666	• 3 57
0.6912	32 -	0.6	1583	29.8	33	34
J•6915 J•6916	29 -	0.6	1583	30.3	30 1661	• 1 57
0.6917	75 -	Ŏ.ĕ	1582	30.6	33	33
0.6919	004 -	0.6	1582	31 1	30	•9 57
0.6924		0.6	1581	31.4	33	34
0.6927	15 -	0.6	1580	21	31	.7
0.0928 0.6931	19 -	0.6	1579	10	2.	25
0.6933	36 -	0.6	1580	32.5	īģ	57
0.6935 0.6936	037 - 74 -	0.6	1579	32.7	83.	33 05
0.69	38 -	0.6	1578	33.3	16	67

 $\begin{array}{c} 0.694020 - 0.61578 & 33.58334 \\ 0.693972 - 0.61578 & 33.85 \\ 0.694138 - 0.61577 & 34.11667 \\ 0.69431 - 0.61575 & 34.91667 \\ 0.69431 - 0.61575 & 34.91667 \\ 0.694761 - 0.61575 & 35.18334 \\ 0.694817 - 0.61575 & 35.71667 \\ 0.695061 - 0.61575 & 35.71667 \\ 0.695125 - 0.61575 & 35.71667 \\ 0.695125 - 0.61574 & 35.98333 \\ 0.695125 - 0.61574 & 36.51667 \\ 0.695298 - 0.61574 & 36.79167 \\ 0.695298 - 0.61573 & 37.33334 \\ 0.695552 - 0.61573 & 37.33334 \\ 0.695552 - 0.61573 & 37.86667 \\ 0.695666 - 0.61573 & 37.38.46667 \\ 0.695967 - 0.61572 & 38.93334 \\ 0.695995 - 0.61572 & 38.93334 \\ 0.695995 - 0.61572 & 38.93334 \\ 0.696076 - 0.61572 & 39.46667 \\ 0.696178 - 0.61572 & 39.46667 \\ 0.696633 - 0.61570 & 40.8333 \\ 0.696633 - 0.61570 & 40.8333 \\ 0.696633 - 0.61570 & 40.8333 \\ 0.696663 - 0.61570 & 41.34167 \\ 0.696685 - 0.61570 & 41.34167 \\ 0.696685 - 0.61570 & 41.38333 \\ 0.697057 - 0.61570 & 41.88333 \\ 0.697057 - 0.61569 & 42.41667 \\ 0.697221 - 0.61569 & 42.41667 \\ 0.697221 - 0.61569 & 42.41667 \\ 0.697553 - 0.61567 & 41.88333 \\ 0.697652 - 0.61567 & 41.61667 \\ 0.697592 - 0.61567 & 42.68334 \\ 0.697592 - 0.61567 & 42.68334 \\ 0.697652 - 0.61567 & 42.68334 \\ 0.697652 - 0.61567 & 44.28334 \\ 0.697652 - 0.61567 & 44.28334 \\ 0.697652 - 0.61567 & 44.28334 \\ 0.697892 - 0.61567 & 44.28334 \\ 0.697892 - 0.61567 & 44.28334 \\ 0.698667 - 0.61567 & 44.28334 \\ 0.698667 - 0.61567 & 44.28334 \\ 0.698667 - 0.61567 & 44.28334 \\ 0.698667 - 0.61567 & 44.28334 \\ 0.698627 - 0.61566 & 44.55001 \\ 0.698647 - 0.61565 & 45.63333 \\ 0.698627 - 0.61566 & 44.81667 \\ 0.698625 - 0.61566 & 44.81667 \\ 0.698625 - 0.61566 & 44.81667 \\ 0.698625 - 0.61566 & 44.81667 \\ 0.698625 - 0.61566 & 44.81667 \\ 0.698625 - 0.61566 & 45.98334 \\ 0.698667 - 0.61565 & 45.63333 \\ 0.698607 - 0.61565 & 45.63333 \\ 0.698607 - 0.61565 & 45.63333 \\ 0.698607 - 0.61565 & 45.63333 \\ 0.698607 - 0.61565 & 45.63333 \\ 0.698607 - 0.61566 & 48.8334 \\ 0.698667 - 0.61562 & 48.3334 \\ 0.698667 - 0.61562 & 48.3334 \\ 0.699695 - 0.61561 & 49.375 \\ 0.699695 - 0.61561 & 49.375 \\ 0.699695 - 0.61561 & 49.657 \\ 0.699$ 0.699814 -0.61560 49.91667 0.700002 -0.61560 50.18334 0.700099 -0.61560 50.45

 $\begin{array}{c} 0.700098 & -0.61560 & 50.71667 \\ 0.700083 & -0.61559 & 50.98333 \\ 0.699992 & -0.61559 & 51.25 \\ 0.700140 & -0.61558 & 51.51667 \\ 0.700210 & -0.61558 & 51.78334 \\ 0.700326 & -0.61558 & 52.05001 \\ 0.700405 & -0.61558 & 52.31667 \\ 0.70053 & -0.61557 & 52.58334 \\ 0.700663 & -0.61557 & 53.11667 \\ 0.700672 & -0.61557 & 53.38333 \\ 0.700798 & -0.61557 & 53.38333 \\ 0.700798 & -0.61557 & 53.38333 \\ 0.700798 & -0.61555 & 53.91667 \\ 0.700827 & -0.61555 & 54.91667 \\ 0.700827 & -0.61555 & 54.98333 \\ 0.700967 & -0.61555 & 54.98333 \\ 0.700967 & -0.61555 & 54.98333 \\ 0.701055 & -0.61555 & 54.98333 \\ 0.701055 & -0.61555 & 55.255 \\ 0.701101 & -0.61555 & 55.255 \\ 0.701220 & -0.61554 & 56.06667 \\ 0.701220 & -0.61554 & 56.33344 \\ 0.70129 & -0.61553 & 57.13333 \\ 0.701427 & -0.61553 & 57.66667 \\ 0.701588 & -0.61552 & 57.66667 \\ 0.701588 & -0.61552 & 57.93334 \\ 0.701807 & -0.61551 & 58.46667 \\ 0.701752 & -0.61551 & 58.46667 \\ 0.701807 & -0.61551 & 58.46667 \\ 0.701775 & -0.61551 & 58.73333 \\ 0.$ 54.45 54.71667 54.98333 55.25 55.80001 56.06667 56.33334 56.6 56.86667 57.13333 57.6667 57.13333 57.6667 57.93334 57.66667 57.93334 57.6667 58.73333 0.701807 - 0.61551 0.701775 - 0.61551 0.701775 - 0.61551 0.701787 - 0.61551 0.701876 - 0.61551 0.701929 - 0.61551 0.701897 - 0.6155159.26667 59.53334 59.80001 $\begin{array}{c} 0.7\,01897 & -0.61551 & 59.80001\\ 0.688594 & -0.60389 & 60.43334\\ 0.7\,01579 & -0.61539 & 61.43334\\ 0.7\,01589 & -0.61539 & 62.43334\\ 0.7\,01783 & -0.61538 & 63.43334\\ 0.7\,01942 & -0.61538 & 63.43334\\ 0.7\,02174 & -0.61537 & 65.45\\ 0.7\,02268 & -0.61537 & 66.45\\ 0.7\,02256 & -0.61537 & 66.45\\ 0.7\,02246 & -0.61537 & 68.45\\ 0.7\,02502 & -0.61533 & 69.45833\\ 0.7\,02502 & -0.61531 & 70.46667\\ 0.7\,02815 & -0.61532 & 71.46667\\ 0.7\,02663 & -0.61532 & 72.46667\\ \end{array}$ 0.702815 - 0.61532 0.702663 - 0.61532 0.702777 - 0.61531 0.702881 - 0.61530 0.702817 - 0.61530 0.702817 - 0.61529 0.702675 - 0.6152972.46667 74.46667 76.46667 77.46667 $\begin{array}{c} 0.702675 - 0.61529 \\ 0.702674 - 0.61529 \\ 0.702754 - 0.61529 \\ 0.702811 - 0.61529 \\ 0.70285 - 0.615$ 78.46667 80.46667 81.475 0 8 26.4 4 Ŏ

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VOLT1 0.821977 0.792875 0.778423 0.794778 0.795601 0.796472 0.796735 0.796735 0.77674 0.7660217 0.764906 0.762087 0.7660217 0.769032 0.757882 0.7575938 0.757538 0.757538 0.757538 0.757258 0.757257 0.757258 0.757263 0.757163 0.757163 0.757163 0.757163 0.757163 0.757163 0.757163 0.757163 0.757163 0.757163 0.757163 0.757258 0.755925 0.755925 0.755925 0.755925 0.755925 0.755925 0.755926 0.755026 0.755026 0.755026 0.755028 0.755008 0.755028 0.75500800000000000000	$\begin{array}{c} VOLT2\\ -0.62402\\ -0.59219\\ -0.58229\\ -0.60208\\ -0.60500\\ -0.60949\\ -0.61850\\ -0.61850\\ -0.61858\\ -0.61826\\ -0.61826\\ -0.61848\\ -0.61848\\ -0.61833\\ -0.61848\\ -0.61848\\ -0.61848\\ -0.61848\\ -0.61848\\ -0.61755\\ -0.61771\\ -0.61773\\ -0.61773\\ -0.61755\\ -0.61755\\ -0.61759\\ -0.61759\\ -0.61759\\ -0.61759\\ -0.61755\\ -0.61755\\ -0.61755\\ -0.61755\\ -0.61755\\ -0.61682\\ -0.61662\\ -0.61652\\ -0.61644\\ -0.61635\end{array}$	MINUTES 0.133333 0.4 0.666666 0.933333 1.2 1.466667 1.733333 2.266667 2.533333 3.066667 3.33334 3.666667 4.133333 4.666667 4.133333 4.666667 5.733334 5.2 5.466667 5.733334 6.266667 6.541667 6.541667 6.541667 6.541667 7.083333 7.35 7.608334 7.8666667 8.133333 8.399999 8.666667 8.933333 9.22 9.466667 8.933333 9.22 9.466667 1.0.253333 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2
0.757258 0.757257 0.757253 0.757163 0.757066 0.757082	-0.61771 -0.61773 -0.61768 -0.61755 -0.61739 -0.61731	5.466667 5.733334 6.266667 6.541667 6.816667
0.757093 0.757123 0.757163 0.757107 0.756696 0.755925	-0.61720 -0.61711 -0.61705 -0.61705 -0.61693 -0.61682	7.083333 7.35 7.608334 7.866667 8.133333 8.399999
0.755006 0.754094 0.753258 0.752528 0.751890	-0.61671 -0.61667 -0.61662 -0.61656 -0.61652 -0.61652	8.666667 8.933333 9.2 9.4666667 9.733334
0.750688 0.750688 0.750176 0.749573 0.748984 0.748418	-0.61644 -0.61635 -0.61632 -0.61632 -0.61626	10.26667 10.53333 10.8 11.06667 11.33333
0.747904 0.747372 0.746802 0.746482 0.746083 0.745667	-0.61623 -0.61618 -0.61613 -0.61607 -0.61600 -0.61598	11.6 11.86667 12.13333 12.4 12.66667 12.93333
0.745299 0.744915 0.744074 0.742691 0.739164 0.734637	-0.61593 -0.61576 -0.61505 -0.61392 -0.61048 -0.60617	$13.2 \\ 13.46667 \\ 13.74167 \\ 14.01667 \\ 14.28333 \\ 14.55$
0.676015 0.703404 0.709102 0.732343 0.738805 0.742090	-0.55428 -0.57701 -0.57984 -0.60486 -0.61049 -0.61358	14.81667 15.08333 15.35 15.61667 15.88333 16.15
0.74224 0.742130	-0.61377 -0.61386	16.41667 16.68333

0.742136 0.742649	-0.61 -0.61 -0.61	398 466 490	16.95 17.21667 17.48333
0.742923	-0.61	499	17.75
0.742772	-0.61	502	18.01667
0.74278	-0.61	518	18.28333
0.742788 0.742884 0.742884	-0.61	536	18.81667 19.08333 19.35833
0.743204	-0.61	547	19.63333
0.743100	-0.61	553	19.9
0.743010	-0.61	557	20.16667
0.743024 0.743088 0.74315	-0.61	1557 1558 1558 1559	20.43333 20.7 20.96667 21.23333
0.738932	-0.61	561	21.5
0.738542	-0.61	560	21.76667
0.738556	-0.61	560	22.03333
0.738526 0.738857 0.739255	-0.61 -0.61 -0.61	L 56 0 L 56 0 L 56 0	22.3 22.56667 22.83334 23.1
0.738875 0.739171 0.739055	-0.61 -0.61	561 562 561	23.36667 23.64167 23.91667
0.739097	-0.6]	L 561	24.18334
0.738812		L 560	24.45
0.738509		L 561	24.71667
0.738616	-0.6	1562	25.25
0.738985	-0.6	1561	25.51667
0.739245	-0.6	1561	25.78333
0.739191	-0.6	L 561	26.05
0.739144		L 560	26.31667
0.739360		L 561	26.58334
0.739374	-0.6	L 56 0	27.11667
0.739535		L 56 0	27.38333
0.739845		L 56 0	27.65833
0.739731	-0.6	1560	27.93334
0.739582	-0.6	1561	28.2
0.739384	-0.6	1561	28.46667
0.739275 0.739197 0.739097 0.739167	-0.6	1560 1560 1560	28./3333 29 29.26667 29.53333
0.739285	-0.6	1560	29.8
0.73924	-0.6	1560	30.06667
0.739335	-0.6	1560	30.33334
0.739786 0.740077 0.74015	-0.6	1559 1558 1557 1556	30.6 30.86667 31.13333
0.740302	-0.6	1556	31.66667
0.740256		1557	31.93333
0.740442		1557	32.2
0.740396	-0.6	1557	32.46667
0.740242		1558	32.74167
0.740078		1559	33.01667
0.740347	-0.6	1558	33.55
0.740435		1558	33.81667
0.740572		1559	34.08334
0.740674	-0.6	1559	34.35

$\begin{array}{c} 0.61560 & 34.61667 \\ 0.61559 & 34.88333 \\ 0.61560 & 35.41667 \\ 0.61560 & 35.68334 \\ 0.61560 & 35.955 \\ 0.61560 & 36.21667 \\ 0.61560 & 36.21667 \\ 0.61559 & 37.01667 \\ 0.61559 & 37.01667 \\ 0.61559 & 37.28333 \\ 0.61559 & 37.81667 \\ 0.61559 & 37.81667 \\ 0.61559 & 38.625 \\ 0.61559 & 38.625 \\ 0.61559 & 38.625 \\ 0.61559 & 38.99 \\ 0.61559 & 38.99 \\ 0.61559 & 39.16667 \\ 0.61559 & 39.43334 \\ 0.61559 & 39.43334 \\ 0.61559 & 40.76667 \\ 0.61559 & 40.76667 \\ 0.61559 & 41.3333 \\ 0.61559 & 41.3333 \\ 0.61557 & 42.36667 \\ 0.61557 & 42.36667 \\ 0.61557 & 43.4667 \\ 0.61557 & 43.4667 \\ 0.61557 & 43.6667 \\ 0.61557 & 43.6667 \\ 0.61557 & 43.6667 \\ 0.61557 & 43.6667 \\ 0.61557 & 43.6667 \\ 0.61557 & 43.6667 \\ 0.61557 & 43.6667 \\ 0.61557 & 43.71667 \\ 0.61557 & 43.71667 \\ 0.61557 & 43.71667 \\ 0.61556 & 44.78334 \\ 0.61556 & 44.78333 \\ 0.61559 & 46.9667 \\ 0.61559 & 46.9667 \\ 0.61559 & 46.9667 \\ 0.61559 & 46.9667 \\ 0.61559 & 46.9667 \\ 0.61559 & 46.9667 \\ 0.61557 & 50.93334 \\ 0.61557 & 50.96667 \\ 0.61557 & 50$
0.740572 0.740575 0.740637 0.740637 0.740575 0.740397 0.740397 0.740397 0.740397 0.740326 0.740326 0.740326 0.740326 0.740326 0.740326 0.740326 0.740326 0.740326 0.740326 0.740326 0.7395831 0.739587 0.7356527 0.736162 0.735846 0.735846 0.735846 0.735846 0.735846 0.735942 0.735846 0.735942 0.735846 0.735942 0.735846 0.735942 0.735942 0.735736 0.735736 0.735736 0.735736 0.735736 0.735736 0.735736 0.735736 0.735736 0.735745 0.735745 0.736031 0.736031 0.736169 0.736169 0.736169 0.736169 0.736169 0.736253 0.736255 0.736255 0.736255 0.736265 0.736255 0.736555 0.736555 0.736555 0.736555 0.736555 0.736555 0.736555 0.736555 0.736555 0.736555 0.736555 0.736555 0.736555 0.736555 0.736555 0.736555 0.7365555 0.7365555 0.7365555 0.7365555 0.7365555 0.7365555 0.7365555 0.7365555 0.73655555 0.73655555 0.73655555 0.73655555 0.7365555555555555

0 736539	-0.61556	52 2
0 7 3 6 5 7 3	0 61556	52.52
0./303/3	-0.01000	24.2
0.73654/	-0.61556	-52.8
0.736535	-0.61557	53.0
0.736528	-0.61556	5
0 7 2 6 5 9 5	-0 61556	52 6
0.730303	-0.01000	22.0
0./36/18	-0.01227	22.8
0.736835	-0.61556	5
0.73685	-0.61556	54.4
0 73680	-0 61556	5/ 6
0.737009	0.01556	54.0
0.737090	-0.01000	24.9
0.737135	-0.61557	55.2
0.737153	-0.61556	
0.737151	-0.61556	55.7
0 7 2 7 1 0 7	-0 61555	56 0
0.13/10/	-0.01333	70.7
0.73/250	-0.61555	20.3
0.737352	-0.61555	56.5
0.737400	-0.61554	56.8
0 737623	-0.61554	2010
0 7 27 500	0 61556	57 3
0.131309	-0.01334	24.2
0./3/461	-0.61554	5/.6
0.737517	-0.61554	
0.737512	-0.61554	58.1
0.737539	-0.61553	58.4
0 7 2 7 6 7 0	-0.61556	50 7
0.757070	-0.01554	10.1
0./3/5/8	-0.01003	28.7
0.737636	-0.61553	- 5
0.737618	-0.61553	59.5
0.737705	-0.61553	59.7
0 724 057	-0.60.13	601
0.727000	0.00413	00.4
0.737880	-0.01532	01.4
0./3/823	-0.61532	62.4
0.737575	-0.61532	63.4
0.737791	-0.61532	64.4
0 73770	-0.61532	651
0 7 2 7 7 5 0	0.61522	66 1
0.737730	-0.01332	00.4
0./3//49	-0.61532	6/.4
0.737755	-0.61532	68.4
0.737745	-0.61532	69.4
0 737740	-0.61532	701
0 7 2 7 7 5 6	0 61 522	71 7
0.13/130	-0.01002	41.4
0./3/842	-0.61531	12.4
0.738048	-0.61531	73.4
0.738034	-0.61531	74.4
0 7 3 8 1 2 0	-0 61530	7
0.730120	0.01000	7617
0.738248	-0.01230	10.4
0	0	
12	26.4	

7.95

25.6