NASA Technical Memorandum 88990

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NOVEMBER 1986

NASA

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**Scientific and Technical
Information Branch**

1986

SUMMARY

An investigation has been conducted in the Langley 16-Foot Transonic Tunnel to measure the flow field in and around the jet exhaust from a nonaxisymmetric nozzle configuration. The nozzle had a rectangular exit with a width-to-height ratio of 2.38. Pitot-pressure measurements were made at five longitudinal locations downstream of the nozzle exit. The maximum distance downstream of the exit was about 5 nozzle heights. These measurements were made at free-stream Mach numbers of 0.00, 0.60, and 1.20 with the nozzle operating at a ratio of nozzle total pressure to free-stream static pressure of 4.0. The jet exhaust was simulated with high-pressure air that had an exit total temperature essentially equal to the free-stream total temperature.

The pitot-pressure measurements showed that the shear layer between the jet and the external flow region was essentially rectangular in shape for at least 5 nozzle exit heights downstream of the nozzle exit, the maximum distance at which measurements were made. At free-stream Mach numbers of 0.60 and 1.20, a vortexlike flow was present in the external flow field near the corner of the exit.

INTRODUCTION

Fighter aircraft must be designed for high maneuverability over a wide range of Mach numbers and engine power settings. A propulsion exhaust-nozzle system with variable geometry enhances the aircraft performance at different power settings. Investigations conducted over many years have shown that rectangular or nonaxisymmetric nozzles cannot only meet the performance requirements but can provide many valuable options for propulsion system design (refs. 1 through 5). The nonaxisymmetric nozzle integrates well into multiengine airframe designs and results in low installed drag (refs. 6 through 8). The nonaxisymmetric nozzle also facilitates thrust-vectoring and thrust-reversing capabilities which improve the overall aircraft maneuverability and handling characteristics and reduce takeoff and landing distances (refs. 3 and 4).

To take full advantage of the options available with nonaxisymmetric nozzles requires that computational methods be developed for predicting the flow about such configurations. At the present time, a few methods are available for predicting such flows but they are severely limited in capability. For better prediction methods to be developed requires that improved solution algorithms be developed and that the theory developer have a basic understanding of the physics of the flow about these three-dimensional nozzles. To obtain this understanding, fundamental experimental studies must be made. In addition to providing insight into the flow phenomena involved, these experiments can provide the high quality, detailed experimental data needed for code verification. Many experimental investigations have been made to provide details of the pressure distributions on three-dimensional nozzle configurations. (See ref. 9, for example.) Also many fundamental experiments have been conducted to study the structure and mixing characteristics of rectangular jets. (See refs. 10 through 13, for example.) However, these experiments typically have been concerned with the far-field characteristics of the jet and with low-speed, constant-pressure parallel jet/free-stream mixing. Studies reported in reference 14 show that the near-field modeling of the jet exhaust characteristics is extremely important in

predicting the pressure distributions and drag of nozzle afterbodies. The increased development of solutions of the Navier-Stokes equations for such flows (ref. 15) also requires that detailed flow-field measurement in the near field of the jet exhaust be available.

The purpose of the present investigation is, therefore, to provide detailed flow-field measurements in and around the exhaust from a rectangular nozzle. Ideally, measurements of the velocity components of the flow, the local static pressure, and the local temperature are needed to define the mean flow. Static pressure, pitot pressure, flow angle, and stagnation temperature can be measured with a survey probe. These parameters then can be used to compute local Mach number and the mean velocity components of the flow. However, the finite size of any survey probe and the large flow-field gradients found in the mixing regions between the jet and the external field can cause large interference effects on the measurements and result in large measurement errors. (See ref. 16.) The quantity that can be measured with the smallest error is pitot pressure. The pitot pressure may be used instead of local total pressure to define some of the dominant flow-field characteristics, such as boundary-layer and shock-wave locations. The comparison of computed pitot pressures with experimental pitot data can provide a basis for evaluating computational methods.

An experiment has, therefore, been conducted in the Langley 16-Foot Transonic Tunnel to measure pitot pressures in and around a jet exhausting from a rectangular nozzle. Pitot-pressure surveys were made at five longitudinal locations downstream of the nozzle exit at free-stream Mach numbers of 0.00, 0.60, and 1.20. The jet was operated at a nozzle pressure ratio (i.e., the ratio of jet or nozzle total pressure to free-stream static pressure) of 4.0. The total temperature of the jet was held at about 530°R. The ratio of the jet total temperature to free-stream total temperature varied from about 0.98 at a Mach number of 0.00 to 0.81 at a Mach number of 1.20.

SYMBOLS

a	semimajor axis of superellipse
b	semiminor axis of superellipse
c	variable used in computation of n for internal transition section geometry (eq. (7))
M_∞	free-stream Mach number
n	exponent in equation for superellipse
NPR	ratio of jet total pressure to free-stream static pressure, $p_{t,j}/p_\infty$
p_∞	free-stream static pressure
$p_{t,j}$	average jet total pressure
$(p_{t,j})_i$	individual jet total pressure
$p_{t,p}$	pitot pressure

$p_{t,\infty}$ free-stream total pressure

$T_{t,j}$ jet total temperature

$T_{t,\infty}$ free-stream total temperature

r radial distance from center of rotation of survey probe

r' radial distance from centerline of model

t dummy variable of integration (eq. (7))

x longitudinal distance downstream of nozzle exit

x' longitudinal distance downstream of model nose

y horizontal distance from model centerline

y_o horizontal location of center of superellipse (eq. (8))

z vertical distance from model centerline

z_o vertical location of center of superellipse (eq. (8))

θ radial angle from model horizontal axis, positive counterclockwise looking upstream

ϕ roll angle of survey rake, $\phi = 0.0$ when rake is horizontal

Abbreviations:

FS fuselage station

O.D. outside diameter

APPARATUS AND TESTS

Wind Tunnel

This investigation was conducted in the Langley 16-Foot Transonic Tunnel. This facility is an atmospheric, single-return wind tunnel with continuous air exchange for cooling. The test section is octagonal with eight longitudinal slots. The tunnel is capable of operating at Mach numbers from 0.2 to 1.3. The average Reynolds number per foot ranges from 1.4×10^6 at a free-stream Mach number of 0.2 to 3.8×10^6 at a free-stream Mach number of 1.3. A detailed description of the tunnel can be found in references 17 and 18.

Model and Support System

General arrangement.- The single-engine air-powered nacelle model of reference 19 was used during this investigation. A detailed sketch of the single-engine propulsion simulation system, with the nozzle of the present investigation installed,

is presented in figure 1. A photograph of the model installed in the Langley 16-Foot Transonic Tunnel is presented as figure 2. As shown in figure 1, the model was composed of five major sections: a nose-forebody, a low-pressure plenum section, an instrumentation section, a transition section, and the nozzle.

Model support system.- The single-engine nacelle model was supported in the tunnel by a sting-strut support system. Part of this support system is shown in figures 1 and 2. The nose-forebody was attached to the top of the strut. The centerline of the model was aligned with the centerline of the wind tunnel. The centerline of the sting was 22.00 in. below the centerline of the wind tunnel. The cross section of the sting was 2.00 in. wide by 4.00 in. high. The top and bottom of the sting were capped by half-cylinders of 1.00 in. radius. The strut blade was 1.00 in. thick and had a 14.14-in. chord normal to the strut leading edge (the streamwise chord was 20.00 in.). The leading edge and trailing edge of the strut were swept 45°. The model blockage was 0.14 percent of the test-section cross-sectional area; the maximum-blockage cross section of the model and support system was 0.19 percent.

Internal air supply.- The exhaust jet flow was simulated with air from a high-pressure air system external to the model. A continuous flow of clean, dry, high-pressure air at a total temperature of approximately 540°R entered the high-pressure plenum in the nose-forebody through six supply lines in the support strut. (See fig. 1.) From the high-pressure plenum, the pressurized air is discharged perpendicular to the model axis into the low-pressure plenum through eight sonic nozzles. The sonic nozzles were equally spaced around the high-pressure plenum supply pipe. The decelerated airflow in the low-pressure plenum was diffused over the balance housing and straightened by a 79-percent open-area baffle plate. Note that for the present investigation, strain-gauge balance measurements were not made. However, the design of the single-engine nacelle requires that a strain-gauge balance or a dummy balance be present. The airflow next passes into the instrumentation section of the model, where the jet total temperature and jet total pressure are measured, and then into the transition section of the model. In the transition section, the internal geometry changes from circular to rectangular to be compatible with the internal geometry at the nonaxisymmetric nozzle connect station. Details of the internal transition geometry are discussed later. From the transition section, the airflow is exhausted through the nonaxisymmetric nozzle.

Nose-forebody-centerbody external geometry.- The nose-forebody section of the model allowed a smooth external transition from a circular cross section at the conical nose to a superelliptical cross section at fuselage station 26.50 in. that was nearly rectangular with large rounded corners. The maximum external cross-sectional area of 41.170 in^2 occurs at fuselage station 26.50 in. The cross-sectional area and the external geometry remained constant from fuselage station 26.50 in. to fuselage station 55.05 in., the nozzle connect station. The external geometry of the model up to fuselage station 55.05 in. is defined by the following equations:

$$r' = \left[\left(\frac{\cos\theta}{a}\right)^n + \left(\frac{\sin\theta}{b}\right)^n\right]^{-1/n} \tag{1}$$

$$y = r' \cos\theta \tag{2}$$

$$z = r' \sin\theta \tag{3}$$

From $x' = 0.0$ to 6.010 in.,

$$\left.\begin{aligned} n &= 2.00 \\ a &= x' \tan \frac{14\pi}{180} \\ b &= x' \tan \frac{14\pi}{180} \end{aligned}\right\} \tag{4}$$

From $x' = 6.010$ to 26.50 in.,

$$\left.\begin{aligned} n &= 3.5 \sin\left(\pi \frac{x' - 16.255}{20.490}\right) + 5.50 \\ a &= -0.363118x' - 9.924540 + \sqrt{-0.834887(x')^2(10)^{-13} + 16.665089x' + 84.948188} \\ b &= -0.209539x' - 2.196445 + \sqrt{-0.213163(x')^2(10)^{-13} + 4.546669x' - 2.781034} \end{aligned}\right\} \tag{5}$$

From $x' = 26.50$ to 55.05 in.,

$$\left.\begin{aligned} n &= 9.0000 \\ a &= 3.4000 \\ b &= 3.1000 \end{aligned}\right\} \tag{6}$$

Internal transition-section geometry.- The model low-pressure plenum internal geometry and the end of the constant-geometry instrumentation section had a circular cross section. The nonaxisymmetric nozzle used in the present investigation had a rectangular internal cross-sectional geometry at the nozzle connect station. The transition section provides a smooth constant area transition from the circular cross section at the beginning of the transition to the rectangular cross section at the nozzle connect station. The geometry change from circular to rectangular is accomplished by using superellipse cross sections. Equations (1), (2), and (3) were used to compute the cross-sectional shape at each fuselage station. The equations for the exponent of the superellipse, the semimajor axis, and the semiminor axis for the internal transition section are given as follows.

From $x' = 49.90$ to 52.87 in.,

$$\left.\begin{aligned} a &= 2.4750 \\ c &= 1.0 + 0.207107\left[\sin\left(\pi\,\frac{x' - 45.445000}{2.9700}\right) + 1\right] \\ n &= \frac{\ln 2}{\ln\left(\sqrt{2}/c\right)} \\ b &= \frac{19.2442185a}{4\displaystyle\int_0^a (a^n - t^n)^{1/n}\,dt} \end{aligned}\right\} \tag{7}$$

where the cross-sectional area of the transition is 19.2442185. From $x' = 52.87$ in. to $x' = 55.05$ in., the internal cross section of the transition section is a rectangle with semiwidth of 2.475 in. and semiheight of 1.944 in. Ahead of 49.90 in., the cross section was circular with a diameter of 2.475 in.

Nozzle geometry.- Details of the two-dimensional, convergent-divergent nozzle used in the present investigation are presented in figure 3. The nozzle had straight parallel internal sidewalls. The nozzle throat aspect ratio (i.e., the ratio of nozzle throat width to nozzle throat height) was 2.380. The ratio of nozzle exit area to throat area was 1.250. As a result, the design exit Mach number was 1.6 and the design nozzle pressure ratio was 4.25.

The external cross-sectional geometry varied from the superellipse at the nozzle connect station to essentially a rectangle with rounded corners at the nozzle exit. At each cross section, the rounded corner was a quarter of a superellipse. A sketch illustrating the shape of the cross section is shown in figure 3. The equation defining the external cross-sectional geometry is as follows:

$$\left(\frac{y - y_o}{a}\right)^n + \left(\frac{z - z_o}{b}\right)^n = 1 \tag{8}$$

where a, b, n, z_o, and y_o are given in table 1 as a function of x'.

Translating Mechanism and Survey Probe

A sketch of the translating survey mechanism is presented in figure 4(a). The translating mechanism allows a survey probe to be positioned within a cylindrical volume approximately 4 ft in length and 4 ft in diameter. The mechanism has provisions for translating the probe in the longitudinal direction and in a radial direction from the tunnel centerline. The probe may be rolled about the axis of the probe support mechanism. The actual longitudinal location of the survey region in

the tunnel test section is determined by the length of the probe support sting. The survey mechanism uses potentiometers to determine the relative longitudinal, radial, and roll positions of the probe.

A sketch of the probe used in the present investigation is shown in figure 4(b). The pitot-pressure rake had seven probes spaced 0.500 in. apart to enable seven measurements of pitot pressure to be made at one time during the test. The rake was attached to the 1.000-in-diameter support sting of the translating mechanism such that the plane of the probes was aligned with the radial translating direction of the mechanism.

Tests

Tests were made at free-stream Mach numbers of 0.00, 0.60, and 1.20. The average Reynolds number per foot was 3.21×10^6 at a Mach number of 0.60 and 3.91×10^6 at a Mach number of 1.20. At each Mach number, flow-field pitot-pressure measurements were made at a nozzle pressure ratio of approximately 4.0. The jet total temperature was held at about 530°R throughout the tests. The pitot pressures were measured at five longitudinal locations downstream of the nozzle exit: x = 0.0, 2.6, 5.2, 7.8, and 10.4 in. At each longitudinal station, the rake was translated radially at a given roll angle in increments of approximately 0.1 in. After moving 0.4 in. from the survey mechanism centerline, the rake was moved radially outward 3.0 in. and then moved in increments of about 0.1 in. for another 0.4 in. This procedure provided pitot pressures at every 0.1 in. from the centerline of the jet to about 6.5 in. from the centerline. (Note that sometimes the probe was moved radially only until the outer two or three probes measured free-stream pitot pressure. This situation occurred primarily at a Mach number of 0.00.) After completing data acquisition at a given roll angle, the survey mechanism was rolled to the next position and the same procedure repeated. Data were obtained at 11 roll angles: approximately 0.0°, 7.5°, 15.0°, 25.0°, 27.7°, 30.0°, 37.5°, 45.0°, 60.0°, 75.0°, and 90.0° from the horizontal looking upstream. Because the model was only tested at an angle of attack of 0.0°, only one fourth of the jet exhaust and external flow field was surveyed. Looking upstream, the measurements were made in the upper right-hand quadrant.

Boundary-layer transition was fixed by a 0.1-in-wide strip of No. 90 grit, which was located 1.0 in. from the model nose. The grain size and location of the transition strip were selected according to the recommendations of references 20 and 21.

INSTRUMENTATION

The pitot pressures were measured with 100-psi differential pressure transducers. The jet total pressure was averaged from 10 total pressures which were measured with rakes in the instrumentation section of the model. These 10 jet total pressures were measured with 100-psi differential pressure transducers. Free-stream static pressure was measured with a precision transducer, and free-stream total pressure was measured with a precision sonar mercury manometer. The tunnel total temperature was measured with a platinum resistance thermometer. The total temperature in the exhaust jet was measured with a thermocouple located in the model instrument section. The radial and longitudinal locations of the survey rake were measured with 100-turn potentiometers. The roll position was measured with a 10-turn potentiometer.

DATA REDUCTION AND CORRECTIONS

There was a small misalignment of the survey mechanism and the model such that the centerline of the model and the center of rotation of the survey mechanism were offset. The centerlines were parallel, however. Therefore, to calculate the y- and z-locations of a pitot-pressure probe in the body axis system of the model, the following equations were used:

$$\left.\begin{aligned} y &= (r + 0.23) \cos \phi - 0.23 \\ z &= (r + 0.23) \sin \phi - 0.10 \end{aligned}\right\} \tag{9}$$

Posttest analysis of the data indicated that the pitot-pressure contours measured at the nozzle exit (x = 0.0 in.) at Mach numbers of 0.60 and 1.20 were rolled relative to the model exit. Data measured at a Mach number of 0.00 were not rolled. The data at Mach numbers of 0.60 and 1.20 were obtained during the first tunnel run. All other data were obtained in later runs. Analysis of all available information did not provide an explanation of the discrepancy. However, the gear attached to the 10-turn potentiometer used to measure roll had 40 teeth. The most logical cause of the discrepancy is that the gear slipped when the initial aerodynamic loads were first applied. If this gear slipped by one tooth, a difference of 9° in roll angle would result. Applying this correction to the data of the first tunnel run eliminated the roll of the data relative to the nozzle exit. Therefore, the data presented in this paper at x = 0.0 in. for Mach numbers of 0.60 and 1.20 have been corrected for this 9°. To accomplish this correction, the following equations were used to calculate the y- and z-locations of the pitot-pressure probes:

$$\left.\begin{aligned} y &= (r + 0.23) \cos (\phi + 9°) - 0.23 \\ z &= (r + 0.23) \sin (\phi + 9°) - 0.10 \end{aligned}\right\} \tag{10}$$

ACCURACY OF DATA

Based on estimates of the precision of the potentiometers, transducers, thermocouples, and resistance thermometers and the observed noise in the data acquisition system, the estimated instrumentation accuracy is as follows:

x, in.	±0.1
r, in.	±0.02
ϕ, deg	±1.2
$p_{t,p}$, psi	±0.50
$p_{t,\infty}$, psi	±0.0005
p_∞, psi	±0.0005
$T_{t,\infty}$, °R	±0.5
$T_{t,j}$, °R	±2.5
$(p_{t,j})_i$, psi	±0.50

Because only seven pitot pressures could be measured simultaneously, a rather lengthy period of time and many individual data points of seven pitot-pressure measurements were required to obtain the flow-field mapping of the present investigation. To assess the repeatability of the free-stream measurements and the jet exhaust measurements an analysis of variance was made. (See ref. 22.) The results of this analysis indicated that the two-standard-deviation (sigma) repeatable band of the free-stream conditions, jet-exhaust conditions, and longitudinal probe location was as shown below:

M_∞	±0.0029
x, in.	±0.089
NPR	±0.034
$T_{t,j}/T_{t,\infty}$	±0.030

RESULTS AND DISCUSSION

Tabulated listings of the pitot-pressure data are provided in tables 2 through 16. Plots of these data are presented in figures 5 through 10. These plots are presented for each free-stream Mach number and longitudinal survey plane in two forms: the ratio of pitot pressure to free-stream total pressure ($p_{t,p}/p_{t,\infty}$) plotted as a function of radial distance from the survey mechanism centerline for each roll angle position, and contour plots of the ratio of pitot pressure to free-stream total pressure.

There is evidence of a weak shock wave located inside the jet exhaust at the nozzle exit at $M_\infty = 0.00$. (See fig. 5(a).) The shock wave is indicated by the sudden increase in pitot pressure at about $r = 0.4$ in. at $\phi = 89.6°$ to $r = 1.0$ in. at $\phi = 25.2°$. This shock is also present at $x = 2.6$ in. (fig. 5(b)) but is not present at the other downstream survey planes. The jet shear layer is rectangular in shape at the nozzle exit. (See fig. 6.) (Note that the saw-tooth structure indicated in the contour plots is caused by the contouring procedure used and not the data.) The shear layer grows with x as expected but does not change significantly from the rectangular shape. At $x = 10.4$ in., however, the shear layer begins to change from the rectangular shape near the corner flow region. This change in shape may be because of increased mixing caused by corner vortices at the nozzle exit.

At $M_\infty = 0.60$, the internal shock was present at the nozzle exit (fig. 7) but was not evident at any of the downstream survey planes. In the external flow region there is a defect in the pitot-pressure profiles resulting from the boundary layer on the external surfaces of the model. However, at $x = 0.0$ in. near the corner of the nozzle, the pressure profiles are not typical of boundary-layer flow. (See pitot-pressure data between $\phi = 33.8°$ and $38.8°$ at about $r = 2.5$ in. in fig. 7(a) and the contour plot in fig. 8(a).) This nonmonotonic variation of the pitot pressures in the external flow region near the corner indicates that a vortexlike flow is probably present. This vortexlike flow is probably caused by the difference in pressure on the top flap and the nozzle sidewall. The vortex would be formed by the air flowing from the high-pressure region to the low-pressure region. This vortex rapidly dissipates and is not evident in the data downstream of $x = 2.6$ in. The shear layer between the jet and external stream is again essentially rectangular up to $x = 5.2$ in. (fig. 8). The nonrectangular corner structure begins to show up near $x = 7.8$ in. which is upstream of where it appears at $M = 0.00$.

The internal shock wave present at the nozzle exit when the free-stream Mach number was 1.20 is very weak. This nozzle configuration has a large separated boundary-layer region on the top and bottom flaps. (See fig. 9(a).) The vortices caused by the difference in pressure between the sidewalls and the upper and bottom flaps are much stronger than at $M_\infty = 0.60$ and persist beyond the last longitudinal survey station of the present investigation. (See figs. 9 and 10.) Because of the separated boundary layer and the vortex, the mixing of the external and jet flows occurs much faster. At $x = 10.4$ in. the mixing region extends almost to the horizontal nozzle centerline (figs. 9(e) and 10(e)).

CONCLUDING REMARKS

An investigation has been conducted in the Langley 16-Foot Transonic Tunnel to measure the flow field in and around the jet exhaust from a nonaxisymmetric nozzle configuration. Pitot-pressure measurements were made at five longitudinal locations downstream of the nozzle exit with the nozzle operating at a nozzle pressure ratio of 4.0. These measurements were made at free-stream Mach numbers M_∞ of 0.00, 0.60, and 1.20. The jet exhaust was simulated with high-pressure air that had an exit total temperature essentially equal to the free-stream total temperature.

Analysis of the flow-field measurements showed that the shear layer between the jet and the external flow region was essentially rectangular in shape at all longitudinal mapping plane locations. (The maximum distance downstream of the nozzle exit at which measurements were made was approximately 5 nozzle heights.) At $M_\infty = 0.60$ and 1.20 a vortexlike flow was present in the external flow field near the corner of the nozzle exit. At $M_\infty = 0.60$, this vortex rapidly dissipated downstream of the nozzle exit. At $M_\infty = 1.20$, however, there appears to be a strong interaction between the jet exhaust mixing layer and the external flow.

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September 23, 1986

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TABLE 1.- NOZZLE EXTERNAL GEOMETRY PARAMETERS

x', in.	n	y_o, in.	a, in.	z_o, in.	b, in.
55.050000	9.000000	0.0	3.400000	0.0	3.100000
55.800000	9.000000	.0	3.400000	.0	3.100000
55.955000	8.971336	.021620	3.377273	.019712	3.079182
56.110000	8.885800	.085850	3.309725	.078265	3.017310
56.265000	8.744759	.190812	3.199229	.173926	2.916114
56.420000	8.550502	.333435	3.048852	.303860	2.778427
56.575000	8.306262	.509542	2.862770	.464213	2.608099
56.730000	8.016265	.713960	2.646147	.650215	2.409891
56.885000	7.685825	.940668	2.404996	.856320	2.189344
57.040000	7.321539	1.182966	2.146010	1.076359	1.952617
57.110255	7.147499	1.295949	2.024724	1.178869	1.841804
57.195000	6.923570	1.433990	1.876380	1.303889	1.706142
57.350000	6.459978	1.687944	1.603588	1.532708	1.456110
57.505000	5.932959	1.937487	1.335207	1.755519	1.209805
57.660000	5.351886	2.175169	1.078687	1.965047	.974486
57.815000	4.428499	2.393870	.841148	2.154417	.757011
57.970000	4.078337	2.586997	.629184	2.317381	.563611
58.125000	3.424089	2.748665	.448678	2.448520	.399683
58.280000	2.803543	2.873865	.304640	2.543429	.269612
58.435000	2.287744	2.958598	.201069	2.598861	.176621
58.590000	2.006571	2.999990	.140839	2.612835	.122664
58.719355	2.000000	3.000108	.125000	2.592250	.108007
58.745000	↓	2.996991	↓	2.585239	.107826
58.900000		2.978153		2.541479	.106672
59.055000		2.959315		2.495322	.105401
59.076861		2.956659		2.488617	.105212
59.210000		2.940478		2.447643	.104050
59.365000		2.951640		2.399957	.102680
59.520000		2.902802		2.352287	.101294
59.675000		2.883964		2.304635	.099890
59.830000		2.865126		2.257001	.098469
59.985000		2.846288		2.209385	.097029
60.140000		2.827450		2.161787	.095571
60.295000		2.808613		2.114208	.094095
60.450000		2.789775		2.066648	.092599
60.605000		2.770937		2.019108	.091084
60.760000		2.752099		1.971587	.089549
60.915000		2.733261		1.924087	.087994
61.070000		2.714423		1.876607	.086418
60.225000		2.695585		1.829148	.084821
61.380000		2.676747		1.781711	.083203
61.535000		2.657910		1.734295	.081563
61.690000		2.639072		1.686902	.079900
61.845000		2.620234		1.639532	.078215
62.000000		2.601396		1.592185	.076506
62.155000		2.582558		1.544862	.074774
62.310000		2.563720		1.497563	.073017
62.465000		2.544882		1.450289	.071236
62.620000		2.526045		1.403040	.069425
62.775000		2.507207		1.355817	.067596
62.930000		2.488369		1.308621	.065737
63.040000	2.000000	2.475000	.125000	1.275143	.064401

TABLE 2.- PITOT-PRESSURE MEASUREMENTS AT $x = 0.0$ in. FOR $M_\infty = 0.00$ WITH NPR = 4.03 AND $T_{t,j}/T_{t,\infty} = 0.98$

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
-.008	-.100	3.490	-.008	-.1
.095	-.101	3.503	.095	-.1
.187	-.101	3.506	.187	-.1
.282	-.100	3.510	.282	.0
.385	-.101	3.508	.385	-.1
.492	-.101	3.499	.492	-.1
.595	-.101	3.510	.595	-.1
.687	-.101	3.509	.687	-.1
.782	-.101	3.510	.782	.0
.885	-.101	3.507	.885	-.1
.992	-.102	3.505	.992	-.1
1.095	-.102	3.513	1.095	-.1
1.187	-.102	3.516	1.187	-.1
1.282	-.101	3.522	1.282	.0
1.385	-.102	3.524	1.385	-.1
1.492	-.102	3.515	1.492	-.1
1.595	-.103	3.528	1.595	-.1
1.687	-.102	3.526	1.687	-.1
1.782	-.101	3.528	1.782	.0
1.885	-.103	3.529	1.885	-.1
1.992	-.103	3.522	1.992	-.1
2.095	-.104	3.525	2.095	-.1
2.187	-.103	3.510	2.187	-.1
2.282	-.102	3.491	2.282	.0
2.385	-.103	3.139	2.385	-.1
2.492	-.104	.997	2.492	-.1
2.595	-.105	1.000	2.595	-.1
2.687	-.104	1.000	2.687	-.1
2.782	-.102	1.000	2.782	.0
2.885	-.104	1.000	2.885	-.1
2.992	-.104	.998	2.992	-.1
3.095	-.105	.998	3.095	-.1
3.187	-.104	.999	3.187	-.1
3.282	-.102	.999	3.282	.0
3.385	-.105	.998	3.385	-.1
-.013	-.070	3.498	-.011	7.9
.092	-.060	3.501	.095	7.0
.197	-.047	3.506	.200	7.1
.280	-.037	3.507	.284	7.1
.380	-.025	3.510	.385	7.0
.482	-.002	3.510	.489	7.9
.588	.001	3.510	.595	7.0
.693	.014	3.508	.700	7.1
.776	.025	3.507	.784	7.1
.877	.037	3.508	.885	7.0
.977	.067	3.511	.989	7.9
1.085	.062	3.511	1.095	7.0
1.189	.076	3.511	1.200	7.1
1.272	.087	3.516	1.284	7.1
1.373	.098	3.521	1.385	7.0
1.473	.135	3.527	1.489	7.9
1.581	.124	3.526	1.595	7.0
1.685	.137	3.528	1.700	7.1
1.769	.148	3.531	1.784	7.1
1.869	.159	3.532	1.885	7.0
1.968	.203	3.535	1.989	7.9
2.077	.185	3.536	2.095	7.0
2.181	.199	3.536	2.200	7.1
2.265	.210	3.519	2.284	7.1
2.365	.221	3.374	2.385	7.0
2.463	.272	1.038	2.489	7.9
2.573	.246	1.000	2.595	7.0
2.678	.260	1.000	2.700	7.1
2.761	.271	1.000	2.784	7.1
2.862	.282	1.000	2.885	7.0
2.959	.340	.999	2.989	7.9
3.070	.308	.999	3.095	7.0
3.174	.322	.999	3.200	7.1
3.257	.333	.999	3.284	7.1
3.358	.343	.998	3.385	7.0
-.019	-.042	3.499	-.011	15.3
.083	-.015	3.503	.094	15.2
.201	.017	3.509	.217	15.2
.274	.038	3.510	.292	15.3
.367	.063	3.513	.388	15.2
.463	.090	3.511	.489	15.3
.565	.116	3.513	.594	15.2
.684	.149	3.514	.717	15.2
.756	.170	3.510	.792	15.3
.849	.194	3.510	.888	15.2
.946	.222	3.508	.989	15.3
1.048	.247	3.512	1.094	15.2
1.166	.280	3.511	1.217	15.2
1.238	.302	3.509	1.292	15.3
1.331	.326	3.517	1.388	15.2
1.428	.354	3.550	1.489	15.3
1.530	.378	3.589	1.594	15.2
1.648	.411	3.616	1.717	15.2

TABLE 2.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
1.721	.434	3.621	1.792	15.3
1.814	.457	3.623	1.888	15.2
1.910	.486	3.616	1.989	15.3
2.013	.509	3.612	2.094	15.2
2.131	.543	3.604	2.217	15.2
2.203	.566	3.595	2.292	15.3
2.296	.589	3.565	2.388	15.2
2.392	.618	3.495	2.489	15.3
2.495	.640	1.034	2.594	15.2
2.613	.674	1.000	2.717	15.2
2.685	.698	1.000	2.792	15.3
2.779	.720	1.000	2.888	15.2
2.875	.750	.999	2.989	15.3
2.978	.771	.999	3.094	15.2
3.096	.805	.999	3.217	15.2
3.168	.830	1.000	3.292	15.3
3.261	.852	1.000	3.388	15.2
-.032	-.007	3.503	-.011	25.3
.062	.041	3.505	.094	25.9
.153	.082	3.508	.195	25.4
.236	.116	3.512	.283	24.8
.332	.158	3.514	.388	24.7
.420	.207	3.515	.489	25.3
.511	.260	3.517	.594	25.9
.605	.297	3.517	.695	25.4
.690	.326	3.515	.783	24.8
.786	.367	3.512	.888	24.7
.872	.420	3.600	.989	25.3
.961	.478	3.626	1.094	25.9
1.056	.512	3.632	1.195	25.4
1.143	.536	3.629	1.283	24.8
1.240	.576	3.627	1.388	24.7
1.324	.633	3.631	1.489	25.3
1.411	.696	3.634	1.594	25.9
1.508	.727	3.634	1.695	25.4
1.597	.746	3.636	1.783	24.8
1.694	.785	3.635	1.888	24.7
1.777	.847	3.628	1.989	25.3
1.861	.914	3.620	2.094	25.9
1.959	.942	3.614	2.195	25.4
2.051	.956	3.608	2.283	24.8
2.149	.994	3.583	2.388	24.7
2.229	1.060	3.366	2.489	25.3
2.311	1.132	3.039	2.594	25.9

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
2.411	1.156	2.056	2.695	25.4
2.505	1.166	1.033	2.783	24.8
2.603	1.203	1.000	2.888	24.7
2.681	1.274	1.000	2.989	25.3
2.761	1.350	1.000	3.094	25.9
2.862	1.371	.999	3.195	25.4
2.958	1.376	.999	3.283	24.8
3.057	1.412	1.000	3.388	24.7
-.035	.000	3.465	-.011	27.1
.061	.046	3.471	.095	26.6
.154	.088	3.478	.197	26.1
.231	.127	3.481	.283	26.2
.324	.173	3.487	.388	26.2
.410	.228	3.478	.489	27.1
.508	.270	3.483	.595	26.6
.603	.307	3.487	.697	26.1
.679	.347	3.485	.783	26.2
.773	.393	3.487	.888	26.2
.855	.455	3.596	.989	27.1
.955	.494	3.603	1.095	26.6
1.052	.527	3.606	1.197	26.1
1.128	.568	3.602	1.283	26.2
1.222	.614	3.604	1.388	26.2
1.300	.683	3.594	1.489	27.1
1.402	.718	3.603	1.595	26.6
1.501	.747	3.604	1.697	26.1
1.576	.789	3.603	1.783	26.2
1.670	.834	3.607	1.888	26.2
1.745	.911	3.587	1.989	27.1
1.849	.942	3.580	2.095	26.6
1.950	.967	3.568	2.197	26.1
2.025	1.010	3.548	2.283	26.2
2.119	1.055	3.495	2.388	26.2
2.190	1.139	1.736	2.489	27.1
2.296	1.166	1.014	2.595	26.6
2.399	1.186	1.000	2.697	26.1
2.474	1.230	1.000	2.783	26.2
2.568	1.276	1.000	2.888	26.2
2.635	1.367	1.000	2.989	27.1
2.743	1.390	1.001	3.095	26.6
2.848	1.406	1.001	3.197	26.1
2.922	1.451	1.001	3.283	26.2
3.017	1.496	1.001	3.388	26.2
-.041	.010	3.473	-.011	30.2

TABLE 2.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r,in.	ϕ, deg
.058	.064	3.476	.101	29.8
.143	.112	3.478	.199	29.6
.223	.157	3.480	.290	29.6
.308	.204	3.484	.388	29.5
.391	.261	3.486	.489	30.2
.492	.313	3.488	.601	29.8
.578	.358	3.488	.699	29.6
.657	.404	3.491	.790	29.6
.744	.450	3.526	.888	29.5
.824	.512	3.617	.989	30.2
.926	.561	3.616	1.101	29.8
1.013	.605	3.614	1.199	29.6
1.092	.651	3.610	1.290	29.6
1.179	.696	3.607	1.388	29.5
1.256	.764	3.604	1.489	30.2
1.360	.809	3.601	1.601	29.8
1.448	.852	3.598	1.699	29.6
1.527	.898	3.594	1.790	29.6
1.614	.942	3.591	1.888	29.5
1.688	1.015	3.547	1.989	30.2
1.794	1.057	3.459	2.101	29.8
1.883	1.098	3.175	2.199	29.6
1.962	1.145	2.309	2.290	29.6
2.050	1.188	1.093	2.388	29.5
2.121	1.266	1.000	2.489	30.2
2.228	1.305	1.000	2.601	29.8
2.318	1.345	1.000	2.699	29.6
2.396	1.392	1.000	2.790	29.6
2.485	1.434	1.000	2.888	29.5
2.553	1.517	1.001	2.989	30.2
2.662	1.553	1.001	3.101	29.8
2.753	1.592	1.001	3.199	29.6
2.831	1.639	1.001	3.290	29.6
2.920	1.680	1.001	3.388	29.5
-.057	.034	3.474	-.011	37.7
.029	.094	3.477	.094	36.9
.096	.143	3.478	.177	36.8
.176	.210	3.481	.281	37.4
.267	.268	3.485	.388	36.6
.339	.339	3.486	.489	37.7
.429	.394	3.487	.594	36.9
.496	.443	3.494	.677	36.8
.573	.514	3.589	.781	37.4
.668	.566	3.620	.888	36.6

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
.735	.645	3.622	.989	37.7
.829	.694	3.621	1.094	36.9
.897	.742	3.617	1.177	36.8
.970	.817	3.613	1.281	37.4
1.070	.864	3.603	1.388	36.6
1.131	.950	3.588	1.489	37.7
1.229	.994	3.572	1.594	36.9
1.298	1.041	3.527	1.677	36.8
1.367	1.121	3.342	1.781	37.4
1.472	1.162	1.678	1.888	36.6
1.527	1.255	1.001	1.989	37.7
1.629	1.294	1.001	2.094	36.9
1.698	1.341	1.001	2.177	36.8
1.765	1.425	1.001	2.281	37.4
1.873	1.460	1.001	2.388	36.6
1.923	1.561	1.000	2.489	37.7
2.030	1.594	1.000	2.594	36.9
2.099	1.640	1.000	2.677	36.8
2.162	1.728	1.000	2.781	37.4
2.275	1.758	1.000	2.888	36.6
2.319	1.866	1.001	2.989	37.7
2.430	1.894	1.001	3.094	36.9
2.499	1.939	1.001	3.177	36.8
2.559	2.032	1.002	3.281	37.4
2.676	2.056	1.001	3.388	36.6
-.073	.056	3.476	-.009	44.8
.003	.132	3.478	.099	44.8
.060	.188	3.479	.178	44.8
.134	.262	3.482	.283	44.8
.209	.336	3.486	.388	44.8
.282	.408	3.486	.491	44.8
.358	.484	3.555	.599	44.8
.414	.540	3.618	.678	44.8
.489	.614	3.626	.783	44.8
.564	.688	3.626	.888	44.8
.637	.761	3.625	.991	44.8
.713	.836	3.619	1.099	44.8
.769	.892	3.609	1.178	44.8
.844	.966	3.591	1.283	44.8
.919	1.040	3.533	1.388	44.8
.991	1.113	3.243	1.491	44.8
1.067	1.189	1.050	1.599	44.8
1.124	1.245	1.000	1.678	44.8
1.198	1.319	1.001	1.783	44.8

TABLE 2.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
1.274	1.392	1.001	1.888	44.8
1.346	1.465	1.001	1.991	44.8
1.422	1.541	1.001	2.099	44.8
1.479	1.597	1.001	2.178	44.8
1.553	1.671	1.001	2.283	44.8
1.629	1.744	1.001	2.388	44.8
1.701	1.818	1.000	2.491	44.8
1.777	1.893	1.000	2.599	44.8
1.833	1.949	1.000	2.678	44.8
1.908	2.023	1.000	2.783	44.8
1.984	2.096	1.000	2.888	44.8
2.056	2.170	1.001	2.991	44.8
2.132	2.246	1.002	3.099	44.8
2.188	2.302	1.002	3.178	44.8
2.263	2.376	1.002	3.283	44.8
2.339	2.448	1.002	3.388	44.8
-.114	.089	3.476	-.008	58.5
-.063	.178	3.478	.095	59.0
-.009	.268	3.475	.199	59.0
.037	.344	3.467	.289	59.0
.089	.430	3.478	.388	59.0
.147	.516	3.609	.492	58.5
.195	.607	3.619	.595	59.0
.249	.696	3.624	.699	59.0
.295	.773	3.618	.789	59.0
.347	.858	3.623	.888	59.0
.408	.942	3.614	.992	58.5
.453	1.035	3.566	1.095	59.0
.507	1.125	3.231	1.199	59.0
.553	1.201	1.067	1.289	59.0
.604	1.287	1.002	1.388	59.0
.670	1.368	1.000	1.492	58.5
.711	1.463	1.002	1.595	59.0
.765	1.553	1.002	1.699	59.0
.811	1.630	1.002	1.789	59.0
.862	1.715	1.002	1.888	59.0
.931	1.795	1.001	1.992	58.5
.968	1.892	1.001	2.095	59.0
1.022	1.981	1.001	2.199	59.0
1.068	2.058	1.001	2.289	59.0
1.120	2.144	1.001	2.388	59.0
1.192	2.221	1.000	2.492	58.5
1.226	2.320	1.000	2.595	59.0
1.280	2.410	1.000	2.699	59.0
1.326	2.486	1.000	2.789	59.0
1.378	2.572	1.000	2.888	59.0
1.453	2.647	1.002	2.992	58.5
1.484	2.748	1.002	3.094	59.0
1.538	2.838	1.002	3.199	59.0
1.584	2.915	1.002	3.289	59.0
1.635	3.000	1.002	3.388	59.0
-.171	.111	3.473	-.011	74.3
-.142	.212	3.474	.094	74.3
-.120	.293	3.473	.178	74.3
-.091	.394	3.474	.283	74.3
-.063	.495	3.507	.388	74.3
-.035	.593	3.611	.489	74.3
-.007	.693	3.615	.594	74.3
.016	.774	3.618	.678	74.3
.044	.875	3.620	.783	74.3
.073	.977	3.614	.888	74.3
.100	1.074	3.455	.989	74.3
.128	1.175	1.829	1.094	74.3
.151	1.256	1.002	1.178	74.3
.179	1.357	1.002	1.283	74.3
.208	1.458	1.002	1.388	74.3
.235	1.555	1.001	1.489	74.3
.263	1.656	1.002	1.594	74.3
.286	1.737	1.002	1.678	74.3
.315	1.838	1.001	1.783	74.3
.343	1.939	1.000	1.888	74.3
.370	2.037	1.001	1.989	74.3
.399	2.137	1.001	2.094	74.3
.421	2.218	1.001	2.178	74.3
.450	2.320	1.001	2.283	74.3
.478	2.421	1.001	2.388	74.3
.506	2.518	1.000	2.489	74.3
.534	2.619	1.000	2.594	74.3
.557	2.700	1.000	2.678	74.3
.585	2.801	1.000	2.783	74.3
.614	2.902	1.000	2.888	74.3
.641	2.999	1.002	2.989	74.3
.669	3.100	1.002	3.094	74.3
.692	3.181	1.002	3.178	74.3
.720	3.282	1.002	3.283	74.3
.749	3.384	1.002	3.388	74.3
-.229	.119	3.474	-.011	89.6

TABLE 2.- Concluded

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
-.228	.223	3.471	.093	89.6
-.227	.308	3.474	.178	89.6
-.227	.415	3.476	.285	89.6
-.226	.518	3.561	.388	89.6
-.226	.619	3.612	.489	89.6
-.225	.723	3.616	.593	89.6
-.224	.808	3.619	.678	89.6
-.224	.915	3.616	.785	89.6
-.223	1.018	3.609	.888	89.6
-.222	1.119	2.828	.989	89.6
-.222	1.223	1.002	1.093	89.6
-.221	1.308	1.002	1.178	89.6
-.221	1.415	1.002	1.285	89.6
-.220	1.518	1.002	1.388	89.6
-.219	1.619	1.002	1.489	89.6
-.219	1.723	1.002	1.593	89.6
-.218	1.808	1.002	1.678	89.6
-.218	1.915	1.002	1.785	89.6
-.217	2.018	1.000	1.888	89.6
-.216	2.119	1.001	1.989	89.6
-.216	2.223	1.001	2.093	89.6
-.215	2.308	1.001	2.178	89.6
-.214	2.415	1.001	2.285	89.6
-.214	2.518	1.001	2.388	89.6
-.213	2.619	1.000	2.489	89.6
-.213	2.723	1.000	2.593	89.6
-.212	2.808	1.000	2.678	89.6
-.211	2.915	1.000	2.785	89.6
-.211	3.018	1.000	2.888	89.6
-.210	3.119	1.002	2.989	89.6
-.210	3.223	1.002	3.093	89.6
-.209	3.308	1.002	3.178	89.6
-.208	3.415	1.002	3.285	89.6
-.208	3.518	1.002	3.388	89.6

TABLE 3.- PITOT-PRESSURE MEASUREMENTS AT $x = 2.588$ in. FOR $M_\infty = 0.00$ WITH NPR = 4.02 AND $T_{t,j}/T_{t,\infty} = 0.98$

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
-.011	-.100	3.715	-.011	-.1
.095	-.100	3.781	.095	.0
.199	-.100	3.794	.199	.0
.284	-.100	3.799	.284	.0
.388	-.100	3.798	.388	.0
.489	-.101	3.791	.489	-.1
.595	-.101	3.784	.595	.0
.699	-.101	3.777	.699	.0
.784	-.101	3.769	.784	.0
.888	-.101	3.765	.888	.0
.989	-.102	3.757	.989	-.1
1.095	-.101	3.750	1.095	.0
1.199	-.101	3.743	1.199	.0
1.284	-.101	3.736	1.284	.0
1.388	-.101	3.726	1.388	.0
1.489	-.102	3.708	1.489	-.1
1.595	-.101	3.697	1.595	.0
1.699	-.101	3.688	1.699	.0
1.784	-.101	3.679	1.784	.0
1.888	-.101	3.669	1.888	.0
1.989	-.103	3.629	1.989	-.1
2.095	-.101	3.396	2.095	.0
2.199	-.102	2.568	2.199	.0
2.284	-.102	1.816	2.284	.0
2.388	-.102	1.345	2.388	.0
2.489	-.104	1.069	2.489	-.1
2.595	-.102	1.011	2.595	.0
2.699	-.102	1.000	2.699	.0
2.784	-.102	1.000	2.784	.0
2.888	-.102	1.000	2.888	.0
2.989	-.104	1.000	2.989	-.1
3.095	-.102	1.001	3.095	.0
3.199	-.102	1.000	3.199	.0
3.284	-.102	1.000	3.284	.0
3.388	-.102	1.001	3.388	.0
-.012	-.073	3.711	-.011	7.1
.072	-.063	3.776	.074	7.0
.175	-.050	3.793	.178	7.1
.279	-.037	3.797	.283	7.1
.383	-.019	3.799	.388	7.5
.484	-.011	3.794	.489	7.1
.568	-.001	3.787	.574	7.0
.671	.012	3.780	.678	7.1
.776	.025	3.771	.783	7.1

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
.879	.046	3.763	.888	7.5
.980	.051	3.757	.989	7.1
1.064	.060	3.752	1.074	7.0
1.167	.074	3.747	1.178	7.1
1.272	.086	3.739	1.283	7.1
1.374	.112	3.730	1.388	7.5
1.476	.112	3.720	1.489	7.1
1.561	.121	3.710	1.574	7.0
1.663	.136	3.700	1.678	7.1
1.768	.148	3.689	1.783	7.1
1.870	.177	3.675	1.888	7.5
1.972	.174	3.653	1.989	7.1
2.057	.183	3.590	2.074	7.0
2.160	.198	3.155	2.178	7.1
2.264	.209	2.266	2.283	7.1
2.366	.243	1.562	2.388	7.5
2.469	.236	1.170	2.489	7.1
2.553	.244	1.060	2.574	7.0
2.656	.259	1.008	2.678	7.1
2.760	.270	1.000	2.783	7.1
2.862	.308	1.000	2.888	7.5
2.965	.298	.999	2.989	7.1
3.049	.305	1.000	3.074	7.0
3.152	.321	1.001	3.178	7.1
3.257	.332	1.000	3.283	7.1
3.357	.374	1.000	3.388	7.5
-.018	-.046	3.711	-.011	14.4
.075	-.020	3.766	.085	14.7
.267	.028	3.796	.283	14.4
.362	.060	3.798	.384	15.2
.466	.079	3.795	.489	14.4
.558	.106	3.791	.585	14.7
.751	.152	3.774	.783	14.4
.845	.191	3.766	.884	15.2
.950	.203	3.756	.989	14.4
1.042	.233	3.752	1.085	14.7
1.236	.276	3.740	1.283	14.4
1.328	.322	3.736	1.384	15.2
1.435	.328	3.723	1.489	14.4
1.526	.359	3.717	1.585	14.7
1.720	.401	3.695	1.783	14.4
1.810	.453	3.686	1.884	15.2
1.919	.453	3.671	1.989	14.4
2.009	.486	3.658	2.085	14.7
2.204	.525	3.295	2.283	14.4

TABLE 3.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
2.293	.583	2.547	2.384	15.2
2.403	.577	1.663	2.489	14.4
2.493	.612	1.312	2.585	14.7
2.689	.649	1.014	2.783	14.4
2.775	.714	1.000	2.884	15.2
2.887	.702	.999	2.989	14.4
2.977	.739	.999	3.085	14.7
3.173	.774	1.000	3.283	14.4
3.258	.845	1.001	3.384	15.2
-.026	-.006	3.743	-.005	24.7
.064	.035	3.714	.094	24.7
.141	.071	3.788	.179	24.7
.238	.115	3.796	.285	24.7
.330	.158	3.795	.387	24.7
.428	.203	3.788	.495	24.7
.519	.244	3.785	.594	24.7
.595	.280	3.780	.679	24.7
.692	.324	3.773	.785	24.7
.785	.368	3.769	.887	24.7
.882	.413	3.760	.995	24.7
.973	.453	3.756	1.094	24.7
1.049	.490	3.753	1.179	24.7
1.147	.533	3.746	1.285	24.7
1.239	.577	3.738	1.387	24.7
1.336	.622	3.697	1.495	24.7
1.427	.662	3.689	1.594	24.7
1.504	.699	3.679	1.679	24.7
1.601	.742	3.664	1.785	24.7
1.693	.786	3.649	1.887	24.7
1.790	.831	3.625	1.995	24.7
1.881	.871	3.621	2.094	24.7
1.958	.908	3.613	2.179	24.7
2.055	.951	3.603	2.285	24.7
2.147	.995	3.581	2.387	24.7
2.245	1.040	3.228	2.495	24.7
2.335	1.080	2.875	2.594	24.7
2.412	1.118	2.135	2.679	24.7
2.509	1.160	1.537	2.785	24.7
2.601	1.205	1.268	2.887	24.7
2.699	1.250	1.077	2.995	24.7
2.790	1.289	1.024	3.094	24.7
2.866	1.327	1.002	3.179	24.7
2.963	1.369	.999	3.285	24.7
3.055	1.414	1.000	3.387	24.7

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
-.039	.008	3.771	-.011	29.5
.050	.058	3.715	.091	29.4
.125	.101	3.751	.178	29.5
.216	.152	3.796	.283	29.5
.308	.204	3.795	.388	29.5
.396	.254	3.789	.489	29.5
.486	.303	3.784	.591	29.4
.561	.347	3.778	.678	29.5
.652	.398	3.770	.783	29.5
.744	.450	3.766	.888	29.5
.831	.500	3.760	.989	29.5
.922	.548	3.755	1.091	29.4
.996	.593	3.745	1.178	29.5
1.087	.644	3.730	1.283	29.5
1.179	.696	3.709	1.388	29.5
1.267	.745	3.633	1.489	29.5
1.358	.793	3.623	1.591	29.4
1.431	.839	3.614	1.678	29.5
1.522	.890	3.607	1.783	29.5
1.614	.942	3.598	1.888	29.5
1.702	.991	3.490	1.989	29.5
1.793	1.038	3.397	2.091	29.4
1.866	1.085	3.227	2.178	29.5
1.958	1.136	2.960	2.283	29.5
2.050	1.188	2.659	2.388	29.5
2.137	1.237	1.779	2.489	29.5
2.229	1.283	1.608	2.591	29.4
2.302	1.331	1.441	2.678	29.5
2.393	1.382	1.308	2.783	29.5
2.485	1.434	1.205	2.888	29.5
2.573	1.483	1.051	2.989	29.5
2.665	1.528	1.017	3.091	29.4
2.737	1.577	1.002	3.178	29.5
2.828	1.628	1.000	3.283	29.5
2.920	1.680	1.001	3.388	29.5
-.030	.003	3.763	-.005	27.2
.061	.049	3.715	.097	27.1
.152	.096	3.787	.199	27.1
.235	.138	3.796	.292	27.1
.321	.181	3.794	.388	27.1
.414	.232	3.788	.495	27.2
.506	.277	3.783	.597	27.1
.597	.324	3.778	.699	27.1
.680	.366	3.771	.792	27.1

TABLE 3.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
.766	.409	3.768	.888	27.1
.859	.460	3.758	.995	27.2
.951	.504	3.755	1.097	27.1
1.042	.552	3.751	1.199	27.1
1.125	.594	3.741	1.292	27.1
1.211	.636	3.727	1.388	27.1
1.304	.689	3.666	1.495	27.2
1.396	.732	3.658	1.597	27.1
1.487	.780	3.641	1.699	27.1
1.570	.821	3.628	1.792	27.1
1.656	.864	3.621	1.888	27.1
1.748	.918	3.594	1.995	27.2
1.841	.960	3.575	2.097	27.1
1.932	1.008	3.523	2.199	27.1
2.015	1.049	3.433	2.292	27.1
2.102	1.091	3.306	2.388	27.1
2.193	1.147	2.447	2.495	27.2
2.286	1.188	2.258	2.597	27.1
2.377	1.236	1.896	2.699	27.1
2.461	1.277	1.555	2.792	27.1
2.547	1.319	1.314	2.888	27.1
2.637	1.376	1.080	2.995	27.2
2.731	1.416	1.020	3.097	27.1
2.822	1.464	1.002	3.199	27.1
2.906	1.505	1.000	3.292	27.1
2.992	1.547	1.001	3.388	27.1
-.054	.031	3.771	-.011	36.7
.030	.093	3.731	.094	36.7
.115	.156	3.726	.199	36.6
.186	.208	3.796	.287	36.5
.267	.268	3.796	.388	36.5
.347	.329	3.793	.489	36.7
.431	.392	3.784	.594	36.7
.516	.454	3.778	.699	36.6
.587	.506	3.772	.787	36.5
.669	.566	3.767	.888	36.5
.748	.628	3.758	.989	36.7
.832	.691	3.723	1.094	36.7
.918	.752	3.668	1.199	36.6
.989	.803	3.627	1.287	36.5
1.070	.864	3.601	1.388	36.5
1.149	.927	3.498	1.489	36.7
1.233	.989	3.343	1.594	36.7
1.319	1.050	3.031	1.699	36.6
1.391	1.101	2.659	1.787	36.5
1.472	1.161	2.284	1.888	36.5
1.550	1.225	1.702	1.989	36.7
1.634	1.288	1.468	2.094	36.7
1.721	1.348	1.285	2.199	36.6
1.792	1.399	1.178	2.287	36.5
1.874	1.459	1.105	2.388	36.5
1.951	1.524	1.015	2.489	36.7
2.035	1.587	1.004	2.594	36.7
2.122	1.646	1.000	2.699	36.6
2.194	1.697	.999	2.787	36.5
2.275	1.757	1.000	2.888	36.5
2.352	1.822	1.000	2.989	36.7
2.436	1.885	1.001	3.094	36.7
2.524	1.944	1.001	3.199	36.6
2.596	1.994	1.001	3.287	36.5
2.676	2.056	1.001	3.388	36.6
2.677	2.055	1.001	3.388	36.5
-.075	.055	3.769	-.011	45.0
.000	.128	3.744	.094	44.8
.060	.188	3.714	.178	44.8
.139	.267	3.776	.290	44.8
.209	.336	3.798	.388	44.8
.279	.409	3.795	.489	45.0
.355	.481	3.788	.594	44.8
.414	.540	3.782	.678	44.8
.494	.619	3.777	.790	44.8
.564	.688	3.756	.888	44.8
.632	.763	3.707	.989	45.0
.709	.833	3.659	1.094	44.8
.769	.892	3.607	1.178	44.8
.849	.971	3.429	1.290	44.8
.918	1.040	2.952	1.388	44.8
.985	1.116	2.422	1.489	45.0
1.064	1.185	1.924	1.594	44.8
1.124	1.245	1.563	1.678	44.8
1.204	1.324	1.233	1.790	44.8
1.273	1.393	1.086	1.888	44.8
1.339	1.470	1.049	1.989	45.0
1.419	1.538	1.016	2.094	44.8
1.479	1.597	1.004	2.178	44.8
1.558	1.676	1.001	2.290	44.8
1.628	1.745	1.001	2.388	44.8
1.692	1.824	1.001	2.489	45.0

TABLE 3.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
1.774	1.890	1.000	2.594	44.8
1.833	1.949	1.000	2.678	44.8
1.913	2.029	1.000	2.790	44.8
1.983	2.098	1.000	2.888	44.8
2.045	2.178	1.001	2.989	45.0
2.128	2.242	1.001	3.094	44.8
2.188	2.302	1.002	3.178	44.8
2.268	2.381	1.002	3.290	44.8
2.337	2.450	1.002	3.388	44.8
-.118	.088	3.772	-.011	59.2
-.065	.183	3.763	.098	59.7
-.003	.282	3.720	.214	59.2
.035	.340	3.720	.284	59.0
.091	.438	3.740	.396	59.1
.138	.517	3.769	.489	59.2
.188	.615	3.784	.598	59.7
.253	.711	3.749	.714	59.2
.292	.769	3.724	.784	59.0
.348	.867	3.684	.896	59.1
.395	.947	3.535	.989	59.2
.440	1.047	2.740	1.098	59.7
.509	1.141	1.960	1.214	59.2
.550	1.197	1.573	1.284	59.0
.604	1.296	1.250	1.396	59.1
.651	1.376	1.075	1.489	59.2
.692	1.478	1.006	1.598	59.7
.765	1.570	1.002	1.714	59.2
.808	1.626	1.001	1.784	59.0
.860	1.725	1.002	1.896	59.1
.907	1.805	1.001	1.989	59.2
.944	1.910	1.001	2.098	59.7
1.021	2.000	1.001	2.214	59.2
1.065	2.054	1.001	2.284	59.0
1.117	2.155	1.001	2.396	59.1
1.163	2.235	1.000	2.489	59.2
1.197	2.342	1.000	2.598	59.7
1.277	2.430	1.000	2.714	59.2
1.323	2.483	1.000	2.784	59.0
1.373	2.584	1.000	2.896	59.1
1.420	2.664	1.002	2.989	59.2
1.449	2.773	1.002	3.098	59.7
1.532	2.859	1.002	3.214	59.2
1.581	2.911	1.002	3.284	59.0
1.630	3.013	1.002	3.396	59.1

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
-.171	.111	3.775	-.011	74.3
-.145	.201	3.774	.083	74.3
-.120	.290	3.776	.175	74.2
-.091	.394	3.776	.283	74.3
-.061	.502	3.747	.396	74.3
-.036	.592	3.720	.489	74.3
-.010	.683	3.707	.583	74.3
.016	.771	3.683	.675	74.2
.045	.875	3.639	.783	74.3
.074	.984	3.439	.896	74.3
.100	1.073	2.717	.989	74.3
.125	1.164	1.933	1.083	74.3
.152	1.252	1.457	1.175	74.2
.180	1.357	1.136	1.283	74.3
.210	1.465	1.025	1.396	74.3
.235	1.555	.999	1.489	74.3
.260	1.645	1.000	1.583	74.3
.288	1.733	1.002	1.675	74.2
.316	1.838	1.002	1.783	74.3
.345	1.946	.999	1.896	74.3
.370	2.036	1.001	1.989	74.3
.396	2.127	1.001	2.083	74.3
.423	2.214	1.001	2.175	74.2
.451	2.319	1.001	2.283	74.3
.480	2.428	1.001	2.396	74.3
.505	2.517	1.000	2.489	74.3
.531	2.608	1.000	2.583	74.3
.559	2.696	1.000	2.675	74.2
.587	2.800	1.001	2.783	74.3
.615	2.909	1.000	2.896	74.3
.641	2.999	1.002	2.989	74.3
.666	3.089	1.002	3.083	74.3
.695	3.177	1.002	3.175	74.2
.723	3.282	1.002	3.283	74.3
.751	3.390	1.002	3.396	74.3
-.229	.119	3.776	-.011	89.6
-.228	.203	3.772	.073	89.6
-.227	.329	3.768	.199	89.6
-.227	.414	3.768	.284	89.6
-.226	.518	3.770	.388	89.6
-.226	.619	3.774	.489	89.6
-.225	.703	3.757	.573	89.6
-.224	.829	3.702	.699	89.6
-.224	.914	3.616	.784	89.6

TABLE 3.- Concluded

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
-.223	1.018	3.273	.888	89.6
-.222	1.119	2.245	.989	89.6
-.222	1.203	1.647	1.073	89.6
-.221	1.329	1.162	1.199	89.6
-.221	1.414	1.044	1.284	89.6
-.220	1.518	1.005	1.388	89.6
-.219	1.619	.999	1.489	89.6
-.219	1.703	1.001	1.573	89.6
-.218	1.829	1.002	1.699	89.6
-.218	1.914	.999	1.784	89.6
-.217	2.018	1.002	1.888	89.6
-.216	2.119	1.001	1.989	89.6
-.216	2.203	1.001	2.073	89.6
-.215	2.329	1.001	2.199	89.6
-.214	2.414	1.001	2.284	89.6
-.214	2.518	1.001	2.388	89.6
-.213	2.619	1.000	2.489	89.6
-.213	2.703	1.000	2.573	89.6
-.212	2.829	1.001	2.699	89.6
-.211	2.914	1.001	2.784	89.6
-.211	3.018	1.000	2.888	89.6
-.210	3.119	1.002	2.989	89.6
-.210	3.203	1.002	3.073	89.6
-.209	3.329	1.002	3.199	89.6
-.208	3.414	1.002	3.284	89.6
-.208	3.518	1.002	3.388	89.6

TABLE 4.- PITOT-PRESSURE MEASUREMENTS AT $x = 5.218$ in. FOR $M_\infty = 0.00$ WITH NPR = 4.02 AND $T_{t,j}/T_{t,\infty} = 0.98$

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
-.011	-.101	3.420	-.011	-.1
.093	-.101	3.425	.093	-.1
.189	-.101	3.437	.189	-.1
.304	-.101	3.448	.304	-.1
.390	-.100	3.459	.390	.0
.489	-.102	3.468	.489	-.1
.593	-.102	3.477	.593	-.1
.689	-.101	3.491	.689	-.1
.804	-.101	3.500	.804	-.1
.890	-.101	3.509	.890	.0
.989	-.103	3.516	.989	-.1
1.093	-.103	3.523	1.093	-.1
1.189	-.102	3.535	1.189	-.1
1.304	-.102	3.546	1.304	-.1
1.390	-.101	3.558	1.390	.0
1.489	-.104	3.576	1.489	-.1
1.593	-.104	3.592	1.593	-.1
1.689	-.102	3.616	1.689	-.1
1.804	-.103	3.613	1.804	-.1
1.890	-.101	3.498	1.890	.0
1.989	-.106	3.055	1.989	-.1
2.093	-.104	2.574	2.093	-.1
2.189	-.103	1.980	2.189	-.1
2.304	-.103	1.592	2.304	-.1
2.390	-.102	1.351	2.390	.0
2.489	-.107	1.179	2.489	-.1
2.593	-.105	1.101	2.593	-.1
2.689	-.104	1.036	2.689	-.1
2.804	-.104	1.011	2.804	-.1
2.890	-.102	1.001	2.890	.0
2.989	-.108	.999	2.989	-.1
3.093	-.106	.999	3.093	-.1
3.189	-.104	1.000	3.189	-.1
3.304	-.105	1.000	3.304	-.1
3.390	-.102	1.000	3.390	.0
-.014	-.076	3.418	-.013	6.3
.092	-.061	3.426	.094	7.0
.196	-.049	3.436	.199	6.8
.298	-.044	3.449	.301	6.1
.384	-.024	3.458	.389	7.0
.482	-.021	3.463	.487	6.3
.588	.000	3.474	.594	7.0
.693	.010	3.487	.699	6.8

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
.795	.009	3.500	.801	6.1
.881	.037	3.507	.889	7.0
.979	.034	3.515	.987	6.3
1.084	.061	3.527	1.094	7.0
1.189	.069	3.540	1.199	6.8
1.292	.062	3.554	1.301	6.1
1.377	.097	3.564	1.389	7.0
1.476	.089	3.575	1.487	6.3
1.581	.121	3.594	1.594	7.0
1.686	.129	3.617	1.699	6.8
1.790	.115	3.624	1.801	6.1
1.873	.158	3.554	1.889	7.0
1.973	.144	3.293	1.987	6.3
2.077	.182	2.706	2.094	7.0
2.182	.188	2.095	2.199	6.8
2.287	.167	1.701	2.301	6.1
2.369	.219	1.428	2.389	7.0
2.470	.199	1.259	2.487	6.3
2.573	.243	1.125	2.594	7.0
2.679	.247	1.050	2.699	6.8
2.784	.220	1.017	2.801	6.1
2.866	.280	1.003	2.889	7.0
2.967	.254	1.000	2.987	6.3
3.069	.303	.999	3.094	7.0
3.175	.306	.999	3.199	6.8
3.281	.273	1.000	3.301	6.1
3.362	.341	1.000	3.389	7.0
-.020	-.042	3.422	-.012	15.3
.065	-.019	3.427	.076	15.2
.168	.000	3.436	.181	14.1
.267	.027	3.446	.283	14.3
.363	.049	3.457	.381	14.1
.463	.090	3.462	.488	15.3
.548	.112	3.469	.576	15.2
.653	.122	3.480	.681	14.1
.752	.150	3.489	.783	14.3
.848	.171	3.503	.881	14.1
.945	.222	3.512	.988	15.3
1.030	.244	3.522	1.076	15.2
1.138	.244	3.538	1.181	14.1
1.236	.274	3.553	1.283	14.3
1.332	.293	3.569	1.381	14.1
1.427	.353	3.578	1.488	15.3
1.513	.375	3.588	1.576	15.2

TABLE 4.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
1.623	.366	3.596	1.681	14.1
1.721	.398	3.606	1.783	14.3
1.817	.415	3.617	1.881	14.1
1.910	.485	3.576	1.988	15.3
1.995	.507	3.409	2.076	15.2
2.108	.488	2.980	2.181	14.1
2.205	.521	2.453	2.283	14.3
2.302	.537	1.963	2.381	14.1
2.392	.617	1.580	2.488	15.3
2.477	.638	1.343	2.576	15.2
2.593	.610	1.168	2.681	14.1
2.690	.645	1.078	2.783	14.3
2.787	.659	1.032	2.881	14.1
2.874	.749	1.009	2.988	15.3
2.960	.770	1.002	3.076	15.2
3.078	.732	.999	3.181	14.1
3.174	.768	.999	3.283	14.3
3.272	.781	.999	3.381	14.1
-.030	-.008	3.432	-.010	24.7
.063	.039	3.435	.094	25.4
.140	.072	3.443	.178	24.9
.236	.115	3.452	.283	24.8
.327	.169	3.459	.388	25.8
.433	.190	3.472	.494	23.7
.524	.243	3.480	.599	24.4
.594	.282	3.493	.678	24.9
.690	.325	3.500	.783	24.8
.777	.386	3.505	.888	25.8
.891	.391	3.518	.994	23.7
.966	.467	3.537	1.094	25.4
1.047	.493	3.547	1.178	24.9
1.144	.535	3.559	1.283	24.8
1.228	.603	3.569	1.388	25.8
1.349	.592	3.584	1.494	23.7
1.418	.681	3.588	1.594	25.4
1.501	.703	3.592	1.678	24.9
1.598	.744	3.592	1.783	24.8
1.678	.821	3.588	1.888	25.8
1.807	.792	3.588	1.994	23.7
1.890	.864	3.573	2.099	24.4
1.954	.914	3.512	2.178	24.9
2.051	.954	3.330	2.283	24.8
2.128	1.038	2.977	2.388	25.8
2.240	1.039	2.486	2.490	24.7
2.322	1.109	2.103	2.594	25.4
2.408	1.124	1.773	2.678	24.9
2.505	1.164	1.456	2.783	24.8
2.579	1.255	1.284	2.888	25.8
2.800	1.278	1.096	3.099	24.4
2.862	1.334	1.074	3.178	24.9
2.959	1.374	1.030	3.283	24.8
3.029	1.472	1.010	3.388	25.8
3.181	1.394	1.002	3.494	23.7
3.255	1.485	.999	3.599	24.4
-.035	.000	3.432	-.011	27.1
.062	.042	3.437	.095	25.9
.136	.081	3.443	.178	26.3
.227	.134	3.456	.283	27.1
.324	.187	3.464	.394	27.4
.413	.229	3.475	.492	27.1
.508	.278	3.487	.599	27.1
.582	.317	3.497	.683	27.2
.672	.362	3.507	.783	27.1
.768	.417	3.514	.894	27.4
.858	.457	3.523	.992	27.1
.953	.505	3.534	1.099	27.1
1.032	.524	3.552	1.178	26.3
1.117	.589	3.565	1.283	27.1
1.212	.647	3.574	1.394	27.4
1.301	.683	3.578	1.489	27.1
1.411	.698	3.577	1.595	25.9
1.481	.745	3.576	1.678	26.3
1.562	.817	3.567	1.783	27.1
1.656	.878	3.547	1.894	27.4
1.748	.912	3.519	1.992	27.1
1.843	.961	3.470	2.099	27.1
1.916	1.003	3.399	2.183	27.2
2.007	1.045	3.179	2.283	27.1
2.100	1.108	2.908	2.394	27.4
2.193	1.140	2.586	2.492	27.1
2.288	1.189	2.195	2.599	27.1
2.360	1.232	1.859	2.683	27.2
2.452	1.273	1.580	2.783	27.1
2.544	1.338	1.385	2.894	27.4
2.636	1.367	1.240	2.989	27.1
2.760	1.354	1.152	3.095	25.9
2.805	1.461	1.092	3.183	27.2
2.897	1.501	1.046	3.283	27.1

TABLE 4.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
2.988	1.568	1.016	3.394	27.4
3.083	1.596	1.006	3.492	27.1
3.178	1.644	1.002	3.599	27.1
3.250	1.689	.999	3.683	27.2
-.039	.008	3.439	-.011	29.5
.053	.059	3.441	.095	29.4
.141	.109	3.449	.196	29.4
.203	.134	3.456	.262	28.3
.311	.199	3.470	.388	28.9
.404	.247	3.482	.493	28.7
.492	.308	3.491	.599	29.5
.565	.349	3.500	.683	29.5
.643	.371	3.512	.762	28.3
.749	.441	3.522	.888	28.9
.843	.487	3.530	.993	28.7
.927	.554	3.539	1.099	29.5
1.000	.595	3.549	1.183	29.5
1.084	.608	3.566	1.262	28.3
1.187	.682	3.577	1.388	28.9
1.267	.745	3.571	1.489	29.5
1.360	.796	3.564	1.595	29.4
1.447	.846	3.546	1.696	29.4
1.524	.845	3.529	1.762	28.3
1.624	.924	3.471	1.888	28.9
1.720	.967	3.393	1.993	28.7
1.798	1.045	3.283	2.099	29.5
1.871	1.087	3.164	2.183	29.5
2.062	1.166	2.653	2.388	28.9
2.159	1.206	2.374	2.493	28.7
2.233	1.291	2.067	2.599	29.5
2.318	1.338	1.685	2.696	29.4
2.500	1.408	1.394	2.888	28.9
2.598	1.446	1.267	2.993	28.7
2.668	1.537	1.167	3.099	29.5
2.741	1.579	1.105	3.183	29.5
2.844	1.557	1.059	3.262	28.3
2.937	1.649	1.020	3.388	28.9
3.036	1.686	1.006	3.493	28.7
3.104	1.783	1.002	3.599	29.5
3.177	1.825	1.000	3.683	29.5
-.054	.030	3.438	-.011	36.5
.030	.093	3.443	.094	36.5
.098	.143	3.451	.178	36.5

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
.182	.206	3.465	.283	36.5
.251	.256	3.480	.369	36.5
.269	.270	3.481	.391	36.5
.351	.331	3.495	.494	36.5
.432	.391	3.509	.594	36.5
.500	.441	3.519	.678	36.5
.584	.503	3.529	.783	36.5
.653	.554	3.538	.869	36.5
.671	.568	3.539	.891	36.5
.749	.626	3.550	.989	36.5
.844	.696	3.557	1.107	36.5
.901	.738	3.558	1.178	36.5
.986	.801	3.554	1.283	36.5
1.054	.852	3.532	1.369	36.5
1.072	.865	3.523	1.391	36.5
1.155	.926	3.462	1.494	36.5
1.246	.994	3.319	1.607	36.5
1.303	1.036	3.064	1.678	36.5
1.387	1.099	2.831	1.783	36.5
1.456	1.150	2.598	1.869	36.5
1.474	1.163	2.547	1.891	36.5
1.556	1.224	2.267	1.994	36.5
1.647	1.291	1.980	2.107	36.5
1.705	1.334	1.801	2.178	36.5
1.789	1.397	1.612	2.283	36.5
1.858	1.447	1.460	2.369	36.5
1.958	1.522	1.304	2.494	36.5
2.039	1.582	1.154	2.594	36.5
2.106	1.632	1.120	2.678	36.5
2.191	1.694	1.096	2.783	36.5
2.277	1.758	1.077	2.891	36.5
2.356	1.817	1.037	2.989	36.5
2.440	1.879	1.027	3.094	36.5
2.508	1.929	1.020	3.178	36.5
2.593	1.992	1.010	3.283	36.5
2.661	2.043	1.003	3.369	36.5
2.679	2.056	1.003	3.391	36.5
2.761	2.117	1.000	3.494	36.5
2.852	2.184	.999	3.607	36.5
-.072	.057	3.440	-.007	44.8
.012	.140	3.449	.110	44.8
.075	.203	3.458	.200	44.8
.134	.262	3.471	.283	44.8
.211	.334	3.492	.388	44.5

TABLE 4.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
.283	.410	3.511	.494	44.8
.369	.495	3.529	.614	44.8
.430	.556	3.533	.700	44.8
.489	.614	3.540	.783	44.8
.568	.684	3.548	.888	44.5
.638	.762	3.552	.994	44.8
.723	.847	3.540	1.114	44.8
.785	.908	3.472	1.200	44.8
.844	.966	3.370	1.283	44.8
.924	1.035	3.113	1.388	44.5
.993	1.115	2.749	1.494	44.8
1.078	1.199	2.340	1.614	44.8
1.140	1.260	1.992	1.700	44.8
1.198	1.319	1.806	1.783	44.8
1.281	1.385	1.558	1.888	44.5
1.348	1.467	1.376	1.994	44.8
1.433	1.552	1.238	2.114	44.8
1.494	1.613	1.172	2.200	44.8
1.553	1.671	1.122	2.283	44.8
1.637	1.736	1.064	2.388	44.5
1.703	1.817	1.022	2.493	44.8
1.785	1.902	1.008	2.610	44.8
1.849	1.965	1.002	2.700	44.8
1.908	2.023	1.001	2.783	44.8
1.994	2.086	1.001	2.888	44.5
2.057	2.172	1.000	2.994	44.8
2.142	2.256	1.000	3.114	44.8
2.204	2.317	.999	3.200	44.8
2.263	2.376	.999	3.283	44.8
2.350	2.437	1.000	3.388	44.5
2.412	2.524	1.000	3.494	44.8
2.497	2.609	1.001	3.614	44.8
-.112	.096	3.443	-.001	59.0
-.063	.178	3.454	.094	59.0
-.018	.250	3.468	.179	58.8
.035	.341	3.486	.285	59.0
.089	.430	3.506	.388	59.0
.146	.524	3.525	.499	59.0
.195	.606	3.538	.594	59.0
.241	.677	3.540	.679	58.8
.293	.769	3.537	.785	59.0
.347	.858	3.517	.888	59.0
.403	.953	3.358	.999	59.0
.453	1.034	3.089	1.094	59.0

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
.500	1.105	2.671	1.179	58.8
.551	1.198	2.192	1.285	59.0
.604	1.287	1.828	1.388	59.0
.661	1.381	1.445	1.499	59.0
.710	1.463	1.280	1.594	59.0
.759	1.533	1.165	1.679	58.8
.809	1.626	1.087	1.785	59.0
.862	1.715	1.044	1.888	59.0
.919	1.810	1.016	1.999	59.0
.968	1.891	1.006	2.094	59.0
1.018	1.960	1.001	2.179	58.8
1.066	2.055	1.001	2.285	59.0
1.120	2.144	1.001	2.388	59.0
1.177	2.238	1.001	2.499	59.0
1.226	2.320	1.001	2.594	59.0
1.277	2.388	1.001	2.679	58.8
1.324	2.483	1.001	2.785	59.0
1.378	2.572	1.001	2.888	59.0
1.435	2.667	1.001	2.999	59.0
1.484	2.748	1.001	3.094	59.0
1.536	2.816	1.001	3.179	58.8
1.582	2.911	1.001	3.285	59.0
1.635	3.000	1.001	3.388	59.0
-.166	.127	3.450	.006	74.3
-.142	.212	3.459	.094	74.3
-.113	.315	3.478	.201	74.3
-.091	.394	3.490	.283	74.3
-.061	.495	3.509	.388	74.1
-.030	.608	3.535	.506	74.3
-.007	.693	3.537	.594	74.3
.022	.796	3.523	.701	74.3
.044	.875	3.497	.783	74.3
.076	.976	3.400	.888	74.1
.105	1.090	2.833	1.006	74.3
.128	1.175	2.368	1.094	74.3
.157	1.278	1.884	1.201	74.3
.179	1.357	1.633	1.283	74.3
.212	1.457	1.397	1.388	74.1
.241	1.571	1.142	1.506	74.3
.263	1.656	1.073	1.594	74.3
.292	1.759	1.027	1.701	74.3
.315	1.838	1.010	1.783	74.3
.349	1.938	1.002	1.888	74.1
.377	2.052	1.001	2.006	74.3

TABLE 4.- Concluded

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
.399	2.137	1.001	2.094	74.3
.428	2.240	1.001	2.201	74.3
.450	2.320	1.001	2.283	74.3
.486	2.419	1.001	2.388	74.1
.513	2.533	1.001	2.506	74.3
.534	2.619	1.001	2.594	74.3
.563	2.722	1.001	2.701	74.3
.585	2.801	1.001	2.783	74.3
.622	2.900	1.001	2.888	74.1
.648	3.014	1.001	3.006	74.3
.669	3.100	1.001	3.094	74.3
.698	3.203	1.001	3.201	74.3
.720	3.282	1.001	3.283	74.3
.759	3.381	1.001	3.388	74.1
-.229	.122	3.452	-.008	89.6
-.228	.224	3.464	.094	89.6
-.227	.308	3.474	.178	89.6
-.227	.415	3.495	.285	89.6
-.226	.518	3.509	.388	89.6
-.226	.622	3.532	.492	89.6
-.225	.724	3.533	.594	89.6
-.224	.808	3.523	.678	89.6
-.224	.915	3.470	.785	89.6
-.223	1.018	3.325	.888	89.6
-.222	1.122	2.895	.992	89.6
-.222	1.224	2.160	1.094	89.6
-.221	1.308	1.799	1.178	89.6
-.221	1.415	1.460	1.285	89.6
-.220	1.518	1.285	1.388	89.6
-.219	1.622	1.137	1.492	89.6
-.219	1.724	1.041	1.594	89.6
-.218	1.808	1.016	1.678	89.6
-.218	1.915	1.002	1.785	89.6
-.217	2.018	1.001	1.888	89.6
-.216	2.122	1.000	1.992	89.6
-.216	2.224	1.001	2.094	89.6
-.215	2.308	1.001	2.178	89.6
-.214	2.415	1.001	2.285	89.6
-.214	2.518	1.001	2.388	89.6
-.213	2.622	1.001	2.492	89.6
-.213	2.724	1.001	2.594	89.6
-.212	2.808	1.001	2.678	89.6
-.211	2.915	1.001	2.785	89.6
-.211	3.018	1.001	2.888	89.6
-.210	3.122	1.000	2.992	89.6
-.210	3.224	1.001	3.094	89.6
-.209	3.308	1.001	3.178	89.6
-.208	3.414	1.002	3.285	89.6
-.208	3.518	1.001	3.388	89.6
-.207	3.622	1.002	3.492	89.6

TABLE 5.- PITOT-PRESSURE MEASUREMENTS AT x = 7.762 in. FOR M_∞ = 0.00 WITH NPR = 4.02 AND $T_{t,j}/T_{t,\infty}$ = 0.98

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
-.009	-.100	3.692	-.009	-.1
.095	-.100	3.698	.095	.0
.199	-.100	3.717	.199	.0
.292	-.099	3.748	.292	.1
.388	-.098	3.764	.388	.1
.491	-.101	3.755	.491	-.1
.595	-.101	3.768	.595	.0
.699	-.100	3.767	.699	.0
.792	-.098	3.761	.792	.1
.888	-.097	3.759	.888	.1
.991	-.102	3.758	.991	-.1
1.095	-.101	3.752	1.095	.0
1.199	-.100	3.738	1.199	.0
1.292	-.098	3.725	1.292	.1
1.388	-.096	3.723	1.388	.1
1.491	-.102	3.715	1.491	-.1
1.595	-.101	3.653	1.595	.0
1.699	-.099	3.464	1.699	.0
1.792	-.097	3.138	1.792	.1
1.888	-.095	2.775	1.888	.1
1.991	-.103	2.273	1.991	-.1
2.095	-.101	1.930	2.095	.0
2.199	-.099	1.653	2.199	.0
2.292	-.096	1.448	2.292	.1
2.388	-.093	1.320	2.388	.1
2.491	-.104	1.191	2.491	-.1
2.595	-.102	1.118	2.595	.0
2.699	-.099	1.066	2.699	.0
2.792	-.095	1.033	2.792	.1
2.888	-.092	1.015	2.888	.1
2.991	-.104	1.006	2.991	-.1
3.095	-.102	1.001	3.095	.0
3.199	-.099	.999	3.199	.0
3.292	-.094	.999	3.292	.1
3.388	-.091	.999	3.388	.1
.090	-.061	3.696	.000	6.9
.090	-.061	3.696	.093	6.9
.177	-.052	3.717	.180	6.7
.280	-.037	3.747	.284	7.0
.385	-.024	3.768	.390	7.0
.587	-.001	3.767	.593	6.9
.674	.006	3.764	.680	6.7
.776	.024	3.759	.784	7.0
.881	.037	3.748	.890	7.0
1.083	.060	3.752	1.093	6.9
1.170	.065	3.730	1.180	6.7
1.272	.086	3.724	1.284	7.0
1.377	.099	3.709	1.390	7.0
1.579	.120	3.686	1.593	6.9
1.667	.123	3.536	1.680	6.7
1.769	.147	3.275	1.784	7.0
1.874	.160	2.871	1.890	7.0
2.076	.180	2.117	2.093	6.9
2.164	.182	1.770	2.180	6.7
2.265	.208	1.543	2.284	7.0
2.370	.221	1.369	2.390	7.0
2.572	.241	1.161	2.593	6.9
2.660	.240	1.086	2.680	6.7
2.761	.270	1.044	2.784	7.0
2.866	.283	1.021	2.890	7.0
2.976	.294	1.006	3.000	7.0
3.068	.301	1.003	3.093	6.9
3.157	.299	.999	3.180	6.7
3.257	.331	.999	3.284	7.0
3.362	.344	.999	3.390	7.0
3.472	.355	1.000	3.500	7.0
3.968	.416	1.000	4.000	7.0
4.465	.477	1.002	4.500	7.0
4.961	.538	1.002	5.000	7.0
5.457	.599	1.001	5.500	7.0
5.954	.660	1.002	6.000	7.0
-.019	-.043	3.690	-.011	15.1
.082	-.014	3.690	.094	15.3
.180	.016	3.712	.197	15.8
.265	.035	3.721	.283	15.3
.366	.063	3.760	.388	15.3
.464	.087	3.760	.489	15.1
.565	.117	3.763	.594	15.3
.661	.153	3.756	.697	15.8
.747	.167	3.763	.783	15.3
.848	.196	3.745	.888	15.3
.947	.217	3.757	.989	15.1
1.047	.249	3.734	1.094	15.3
1.142	.289	3.727	1.197	15.8
1.230	.299	3.741	1.283	15.3
1.330	.328	3.714	1.388	15.3
1.430	.347	3.722	1.489	15.1
1.529	.381	3.680	1.594	15.3

TABLE 5.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
1.623	.426	3.627	1.697	15.8	.154	.087	3.692	.197	25.9
1.712	.431	3.565	1.783	15.3	.232	.125	3.716	.284	25.9
1.812	.460	3.306	1.888	15.3	.411	.211	3.753	.483	25.9
1.912	.477	2.942	1.989	15.1	.513	.255	3.758	.594	25.5
2.012	.513	2.515	2.094	15.3	.604	.305	3.750	.697	25.9
2.104	.562	2.132	2.197	15.8	.682	.343	3.745	.784	25.9
2.194	.563	1.905	2.283	15.3	.776	.388	3.739	.888	25.9
2.294	.593	1.614	2.388	15.3	.861	.429	3.753	.983	25.9
2.395	.607	1.423	2.489	15.1	.965	.471	3.745	1.094	25.5
2.494	.645	1.263	2.594	15.3	1.054	.524	3.732	1.197	25.9
2.585	.699	1.160	2.697	15.8	1.132	.562	3.724	1.284	25.9
2.676	.695	1.109	2.783	15.3	1.226	.606	3.712	1.388	25.9
2.777	.725	1.059	2.888	15.3	1.311	.647	3.707	1.483	25.9
2.878	.738	1.037	2.989	15.1	1.416	.686	3.686	1.594	25.5
2.976	.777	1.021	3.094	15.3	1.503	.743	3.652	1.697	25.9
3.066	.835	1.013	3.197	15.8	1.581	.780	3.620	1.784	25.9
3.159	.827	1.006	3.283	15.3	1.676	.824	3.569	1.888	25.9
3.259	.857	1.003	3.388	15.3	1.761	.866	3.441	1.983	25.9
3.361	.898	1.003	3.497	15.5	1.867	.902	3.262	2.094	25.5
3.438	.930	1.001	3.580	15.7	1.953	.961	2.965	2.197	25.9
3.542	.948	1.000	3.685	15.5	2.031	.999	2.672	2.284	25.9
3.638	.960	1.000	3.780	15.3	2.126	1.042	2.368	2.388	25.9
3.843	1.032	1.000	3.997	15.5	2.211	1.084	2.032	2.483	25.9
3.920	1.066	1.000	4.080	15.7	2.318	1.117	1.790	2.594	25.5
4.024	1.082	1.000	4.185	15.5	2.403	1.180	1.562	2.697	25.9
4.120	1.092	1.000	4.280	15.3	2.481	1.218	1.423	2.784	25.9
4.325	1.165	.999	4.497	15.5	2.576	1.260	1.320	2.888	25.9
4.401	1.201	1.002	4.580	15.7	2.691	1.270	1.219	2.997	25.1
4.505	1.215	1.001	4.685	15.5	2.775	1.324	1.165	3.095	25.4
4.602	1.224	.999	4.780	15.3	2.841	1.393	1.121	3.185	25.9
4.807	1.299	1.001	4.997	15.5	2.937	1.413	1.080	3.279	25.5
4.882	1.336	1.001	5.080	15.7	3.026	1.478	1.055	3.388	25.9
4.987	1.349	1.001	5.185	15.5	3.144	1.483	1.035	3.497	25.1
5.084	1.356	1.001	5.280	15.3	3.226	1.538	1.021	3.595	25.4
5.288	1.433	1.001	5.497	15.5	3.291	1.611	1.011	3.685	25.9
5.364	1.471	1.001	5.580	15.7	3.388	1.628	1.005	3.779	25.5
5.469	1.483	1.001	5.685	15.5	3.597	1.695	.999	3.997	25.1
5.566	1.488	1.001	5.780	15.3	3.678	1.752	.999	4.095	25.4
5.770	1.567	1.002	5.997	15.5	3.741	1.830	1.000	4.185	25.9
5.845	1.607	1.002	6.080	15.7	3.839	1.844	1.000	4.279	25.5
5.951	1.617	1.002	6.185	15.5	4.049	1.907	1.002	4.497	25.1
6.049	1.620	1.002	6.280	15.3	4.130	1.966	1.002	4.595	25.4
					4.190	2.049	1.002	4.685	25.9
-.038	-.007	3.684	-.017	25.9	4.290	2.060	1.001	4.779	25.5
.062	.040	3.681	.094	25.5					

TABLE 5.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
4.502	2.120	1.001	4.997	25.1
4.582	2.180	1.002	5.095	25.4
4.640	2.267	1.002	5.185	25.9
4.741	2.275	1.001	5.279	25.5
4.955	2.332	1.001	5.497	25.1
5.034	2.394	1.001	5.595	25.4
5.090	2.486	1.001	5.685	25.9
5.192	2.491	1.001	5.779	25.5
5.407	2.544	1.002	5.997	25.1
5.486	2.608	1.002	6.095	25.4
5.539	2.704	1.002	6.185	25.9
5.643	2.706	1.002	6.279	25.5
-.038	.008	3.689	-.010	29.5
.051	.059	3.688	.093	29.5
.127	.102	3.691	.180	29.5
.215	.151	3.698	.281	29.5
.308	.204	3.713	.388	29.5
.397	.254	3.743	.490	29.5
.486	.305	3.757	.593	29.5
.562	.348	3.772	.680	29.5
.650	.397	3.778	.781	29.5
.743	.450	3.779	.888	29.5
.832	.500	3.775	.990	29.5
.922	.551	3.767	1.093	29.5
.998	.594	3.753	1.180	29.5
1.086	.643	3.738	1.281	29.5
1.179	.696	3.714	1.388	29.5
1.268	.746	3.616	1.490	29.5
1.357	.797	3.574	1.593	29.5
1.433	.840	3.505	1.680	29.5
1.521	.889	3.442	1.781	29.5
1.614	.942	3.363	1.888	29.5
1.703	.992	3.181	1.990	29.5
1.792	1.042	3.073	2.093	29.5
1.868	1.085	2.901	2.180	29.5
1.956	1.135	2.712	2.281	29.5
2.049	1.188	2.478	2.388	29.5
2.138	1.238	2.066	2.490	29.5
2.228	1.288	1.910	2.593	29.5
2.304	1.331	1.728	2.680	29.5
2.392	1.381	1.594	2.781	29.5
2.485	1.434	1.467	2.888	29.5
2.624	1.405	1.331	2.996	27.8
2.663	1.534	1.253	3.093	29.5
2.770	1.532	1.190	3.185	28.5
2.842	1.602	1.134	3.282	29.0
2.920	1.679	1.088	3.388	29.5
3.066	1.638	1.055	3.496	27.8
3.126	1.703	1.035	3.580	28.2
3.210	1.771	1.021	3.685	28.5
3.279	1.844	1.010	3.782	29.0
3.508	1.871	1.001	3.996	27.8
3.567	1.940	.999	4.080	28.2
3.649	2.010	.999	4.185	28.5
3.717	2.086	1.001	4.282	29.0
3.950	2.105	.999	4.496	27.8
4.007	2.177	1.002	4.580	28.2
4.088	2.249	1.002	4.685	28.5
4.154	2.329	.999	4.782	29.0
4.393	2.338	1.001	4.996	27.8
4.448	2.413	1.001	5.080	28.2
4.527	2.488	1.001	5.185	28.5
4.592	2.571	1.001	5.282	29.0
4.835	2.571	1.001	5.496	27.8
4.888	2.650	1.001	5.580	28.2
4.966	2.726	1.001	5.685	28.5
5.029	2.813	1.001	5.782	29.0
5.277	2.804	1.002	5.996	27.8
5.329	2.887	1.002	6.080	28.2
5.406	2.965	1.002	6.185	28.5
5.466	3.056	1.002	6.282	29.0
-.038	-.002	3.686	-.014	27.1
.058	.047	3.684	.093	27.1
.151	.095	3.692	.198	27.1
.228	.133	3.703	.283	26.9
.320	.182	3.719	.388	27.1
.407	.226	3.748	.486	27.1
.503	.275	3.763	.593	27.1
.597	.323	3.768	.698	27.1
.673	.359	3.773	.783	26.9
.766	.410	3.772	.888	27.1
.852	.454	3.765	.986	27.1
.948	.503	3.764	1.093	27.1
1.042	.551	3.760	1.198	27.1
1.119	.586	3.756	1.283	26.9
1.211	.637	3.742	1.388	27.1
1.297	.682	3.688	1.486	27.1
1.393	.731	3.663	1.593	27.1
1.487	.779	3.628	1.698	27.1

TABLE 5.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
1.565	.812	3.589	1.783	26.9
1.656	.865	3.534	1.888	27.1
1.742	.909	3.389	1.986	27.1
1.838	.959	3.247	2.093	27.1
1.932	1.006	3.021	2.198	27.1
2.011	1.039	2.793	2.283	26.9
2.101	1.093	2.522	2.388	27.1
2.187	1.137	2.119	2.486	27.1
2.283	1.186	1.885	2.593	27.1
2.377	1.234	1.672	2.698	27.1
2.456	1.265	1.537	2.783	26.9
2.546	1.321	1.410	2.888	27.1
2.632	1.365	1.295	2.986	27.1
2.728	1.414	1.217	3.093	27.1
2.817	1.459	1.141	3.193	27.1
2.902	1.492	1.109	3.283	26.9
2.991	1.549	1.073	3.388	27.1
3.088	1.598	1.044	3.497	27.1
3.160	1.635	1.028	3.578	27.1
3.262	1.687	1.013	3.693	27.1
3.340	1.727	1.007	3.780	27.1
3.533	1.826	.999	3.997	27.1
3.605	1.863	.999	4.078	27.1
3.707	1.915	.999	4.193	27.1
3.785	1.955	1.001	4.280	27.1
3.978	2.054	1.002	4.497	27.1
4.050	2.091	1.001	4.578	27.1
4.152	2.143	1.002	4.693	27.1
4.230	2.183	1.002	4.780	27.1
4.423	2.281	1.001	4.997	27.1
4.495	2.319	1.001	5.078	27.1
4.597	2.371	1.001	5.193	27.1
4.675	2.410	1.001	5.280	27.1
4.868	2.509	1.001	5.497	27.1
4.940	2.546	1.001	5.578	27.1
5.042	2.598	1.001	5.693	27.1
5.120	2.638	1.001	5.780	27.1
5.313	2.737	1.002	5.997	27.1
5.386	2.774	1.002	6.078	27.1
5.487	2.826	1.002	6.193	27.1
5.565	2.866	1.002	6.280	27.1
-.057	.033	3.691	-.011	37.6
.029	.097	3.685	.095	37.4
.111	.158	3.686	.197	37.1
.178	.213	3.694	.285	37.5
.273	.284	3.710	.402	37.4
.340	.338	3.729	.489	37.6
.426	.401	3.752	.595	37.4
.518	.459	3.769	.704	36.7
.572	.520	3.770	.783	37.7
.670	.587	3.768	.902	37.4
.741	.649	3.748	.996	37.7
.824	.709	3.711	1.099	37.5
.919	.758	3.651	1.204	36.7
.971	.822	3.466	1.285	37.5
1.067	.890	3.340	1.402	37.4
1.132	.948	3.003	1.489	37.6
1.137	.954	3.179	1.496	37.7
1.221	1.013	3.021	1.599	37.5
1.320	1.057	2.848	1.704	36.7
1.362	1.132	2.592	1.783	37.7
1.465	1.194	2.391	1.902	37.4
1.533	1.260	2.211	1.996	37.7
1.617	1.318	2.048	2.099	37.5
1.720	1.356	1.890	2.204	36.7
1.764	1.432	1.735	2.285	37.5
1.925	1.558	1.398	2.489	37.6
2.016	1.614	1.332	2.595	37.4
2.105	1.666	1.283	2.697	37.1
2.161	1.736	1.245	2.785	37.5
2.260	1.801	1.208	2.902	37.4
2.324	1.871	1.170	2.996	37.7
2.411	1.927	1.136	3.099	37.5
2.521	1.954	1.103	3.204	36.7
2.549	2.050	1.064	3.283	37.7
2.557	2.041	1.066	3.285	37.5
2.657	2.104	1.045	3.402	37.4
2.720	2.176	1.027	3.496	37.7
2.807	2.231	1.015	3.599	37.5
2.922	2.254	1.006	3.704	36.7
2.944	2.356	1.003	3.783	37.7
-.075	.054	3.692	-.011	44.8
.000	.128	3.685	.094	44.8
.061	.190	3.684	.181	44.8
.134	.261	3.690	.283	44.8
.209	.336	3.705	.388	44.8
.280	.407	3.721	.489	44.8
.358	.484	3.748	.599	44.8

TABLE 5.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
.418	.543	3.756	.683	44.8
.488	.614	3.750	.783	44.8
.564	.688	3.706	.888	44.8
.633	.758	3.638	.987	44.8
.713	.836	3.456	1.099	44.8
.772	.896	3.257	1.183	44.8
.843	.966	2.977	1.283	44.8
.918	1.040	2.691	1.388	44.8
.990	1.111	2.352	1.489	44.8
1.067	1.189	2.207	1.599	44.8
1.127	1.248	2.016	1.683	44.8
1.198	1.318	1.830	1.783	44.8
1.273	1.393	1.661	1.888	44.8
1.343	1.462	1.554	1.987	44.8
1.418	1.538	1.420	2.094	44.8
1.479	1.600	1.326	2.181	44.8
1.553	1.671	1.255	2.283	44.8
1.628	1.745	1.176	2.388	44.8
1.698	1.815	1.131	2.487	44.8
1.777	1.893	1.086	2.599	44.8
1.834	1.953	1.054	2.681	44.8
1.907	2.023	1.043	2.783	44.8
1.983	2.098	1.032	2.888	44.8
2.054	2.168	1.020	2.989	44.8
2.128	2.243	1.016	3.094	44.8
2.188	2.305	1.010	3.181	44.8
2.262	2.375	1.009	3.283	44.8
2.337	2.450	1.005	3.388	44.8
2.407	2.519	1.003	3.487	44.8
2.487	2.598	1.001	3.599	44.8
2.546	2.657	1.000	3.683	44.8
-.121	.090	3.693	-.011	60.1
-.068	.182	3.688	.095	60.1
-.016	.272	3.686	.199	60.1
.025	.345	3.690	.283	60.1
.078	.436	3.701	.388	60.1
.128	.523	3.711	.489	60.1
.181	.616	3.715	.595	60.1
.233	.706	3.675	.699	60.1
.274	.779	3.580	.783	60.1
.327	.870	3.364	.888	60.1
.377	.957	3.062	.989	60.1
.430	1.049	2.668	1.095	60.1
.481	1.139	2.319	1.199	60.1
.523	1.212	2.070	1.283	60.1
.576	1.304	1.804	1.388	60.1
.626	1.391	1.599	1.489	60.1
.679	1.483	1.414	1.595	60.1
.730	1.573	1.288	1.699	60.1
.772	1.646	1.214	1.783	60.1
.825	1.737	1.141	1.888	60.1
.875	1.824	1.102	1.989	60.1
.928	1.917	1.058	2.095	60.1
.979	2.007	1.033	2.199	60.1
1.021	2.080	1.019	2.283	60.1
1.073	2.171	1.008	2.388	60.1
1.123	2.258	1.001	2.489	60.1
1.176	2.350	1.000	2.595	60.1
1.228	2.440	1.000	2.699	60.1
1.270	2.513	1.000	2.783	60.1
1.322	2.605	1.001	2.888	60.1
1.372	2.692	.999	2.989	60.1
1.425	2.784	.999	3.095	60.1
1.477	2.874	1.000	3.199	60.1
1.519	2.947	1.000	3.283	60.1
1.571	3.038	1.000	3.388	60.1
-.171	.111	3.699	-.011	74.3
-.143	.212	3.696	.094	74.4
-.120	.292	3.695	.177	74.4
-.091	.397	3.701	.286	74.4
-.064	.496	3.707	.388	74.4
-.036	.592	3.702	.489	74.3
-.009	.694	3.670	.594	74.4
.014	.774	3.576	.677	74.4
.043	.878	3.293	.786	74.4
.070	.977	2.982	.888	74.4
.099	1.074	2.558	.989	74.3
.126	1.175	2.206	1.094	74.4
.149	1.256	1.955	1.177	74.4
.178	1.360	1.654	1.286	74.4
.205	1.459	1.478	1.388	74.4
.234	1.555	1.310	1.489	74.3
.260	1.657	1.204	1.594	74.4
.283	1.737	1.141	1.677	74.4
.312	1.842	1.073	1.786	74.4
.339	1.941	1.041	1.888	74.4
.369	2.036	1.019	1.989	74.3
.394	2.139	1.008	2.094	74.4

TABLE 5.- Concluded

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
.417	2.219	1.004	2.177	74.4
.447	2.323	1.001	2.286	74.4
.473	2.422	1.001	2.388	74.4
.504	2.518	1.001	2.489	74.3
.529	2.620	1.001	2.594	74.4
.552	2.700	1.001	2.677	74.4
.581	2.805	1.000	2.786	74.4
.608	2.904	1.001	2.888	74.4
.639	2.999	1.000	2.989	74.3
.663	3.102	1.000	3.094	74.4
.686	3.182	1.001	3.177	74.4
.716	3.286	1.000	3.286	74.4
.742	3.385	1.000	3.388	74.4
-.229	.119	3.711	-.011	89.6
-.228	.224	3.710	.094	89.6
-.227	.308	3.713	.178	89.6
-.227	.414	3.720	.284	89.6
-.226	.518	3.725	.388	89.6
-.226	.624	3.717	.494	89.6
-.225	.724	3.665	.594	89.6
-.224	.808	3.543	.678	89.6
-.224	.914	3.235	.784	89.6
-.223	1.018	2.864	.888	89.6
-.222	1.119	2.428	.989	89.6
-.222	1.224	2.064	1.094	89.6
-.221	1.308	1.831	1.178	89.6
-.221	1.414	1.568	1.284	89.6
-.220	1.518	1.394	1.388	89.6
-.219	1.619	1.239	1.489	89.6
-.219	1.724	1.148	1.594	89.6
-.218	1.808	1.098	1.678	89.6
-.218	1.914	1.048	1.784	89.6
-.217	2.018	1.024	1.888	89.6
-.216	2.119	1.008	1.989	89.6
-.216	2.224	1.002	2.094	89.6
-.215	2.308	1.001	2.178	89.6
-.214	2.414	1.001	2.284	89.6
-.214	2.518	1.001	2.388	89.6
-.213	2.619	1.001	2.489	89.6
-.213	2.724	1.000	2.594	89.6
-.212	2.808	1.001	2.678	89.6
-.211	2.914	1.001	2.784	89.6
-.211	3.018	1.000	2.888	89.6
-.210	3.124	1.001	2.994	89.6
-.209	3.229	1.001	3.099	89.6
-.209	3.308	1.001	3.178	89.6
-.208	3.414	1.000	3.284	89.6
-.208	3.518	1.001	3.388	89.6
-.207	3.624	1.001	3.494	89.6
-.206	3.729	1.001	3.599	89.6

TABLE 6.- PITOT-PRESSURE MEASUREMENTS AT $x = 10.238$ in. FOR $M_\infty = 0.00$ WITH NPR = 4.00 AND $T_{t,j}/T_{t,\infty} = 0.98$

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
.104	-.100	3.387	.104	.0	5.017	-.100	1.000	5.017	.0
.220	-.100	3.388	.220	.0	5.122	-.097	1.000	5.122	.0
.305	-.100	3.392	.305	.0	5.206	-.100	1.000	5.206	.0
.409	-.100	3.392	.409	.0	5.312	-.100	1.000	5.312	.0
.507	-.100	3.399	.507	.0	5.517	-.100	1.000	5.517	.0
.604	-.100	3.407	.604	.0	5.622	-.096	1.000	5.622	.0
.720	-.100	3.413	.720	.0	5.706	-.100	1.000	5.706	.0
.805	-.100	3.429	.805	.0	5.812	-.100	1.000	5.812	.0
.909	-.100	3.444	.909	.0					
1.007	-.100	3.467	1.007	.0	.008	-.067	3.385	.010	7.8
1.104	-.100	3.495	1.104	.0	.115	-.053	3.387	.118	7.7
1.220	-.100	3.516	1.220	.0	.216	-.040	3.390	.220	7.7
1.305	-.100	3.537	1.305	.0	.305	-.028	3.395	.310	7.7
1.409	-.099	3.538	1.409	.0	.404	-.016	3.397	.409	7.5
1.507	-.100	3.506	1.507	.0	.503	.001	3.403	.510	7.8
1.604	-.100	3.367	1.604	.0	.610	.013	3.410	.618	7.7
1.720	-.100	3.123	1.720	.0	.712	.027	3.421	.720	7.7
1.805	-.100	2.788	1.805	.0	.800	.039	3.439	.810	7.7
1.909	-.099	2.434	1.909	.0	.900	.050	3.454	.909	7.5
2.007	-.100	2.124	2.007	.0	.998	.069	3.485	1.010	7.8
2.104	-.100	1.818	2.104	.0	1.106	.080	3.506	1.118	7.7
2.220	-.100	1.606	2.220	.0	1.207	.093	3.524	1.220	7.7
2.305	-.100	1.433	2.305	.0	1.296	.106	3.538	1.310	7.7
2.409	-.099	1.309	2.409	.0	1.395	.115	3.534	1.409	7.5
2.507	-.100	1.217	2.507	.0	1.494	.137	3.437	1.510	7.8
2.604	-.100	1.138	2.604	.0	1.601	.147	3.262	1.618	7.7
2.720	-.100	1.090	2.720	.0	1.703	.160	3.013	1.720	7.7
2.805	-.100	1.053	2.805	.0	1.791	.173	2.679	1.810	7.7
2.909	-.099	1.031	2.909	.0	1.891	.181	2.389	1.909	7.5
3.017	-.100	1.012	3.017	.0	1.989	.205	1.953	2.010	7.8
3.122	-.098	1.004	3.122	.0	2.097	.214	1.728	2.118	7.7
3.206	-.100	1.001	3.206	.0	2.198	.226	1.550	2.220	7.7
3.312	-.100	.998	3.312	.0	2.287	.240	1.396	2.310	7.7
3.517	-.100	.999	3.517	.0	2.387	.247	1.296	2.409	7.5
3.622	-.098	1.000	3.622	.0	2.484	.273	1.180	2.510	7.8
3.706	-.100	.999	3.706	.0	2.592	.281	1.121	2.618	7.7
3.812	-.100	.999	3.812	.0	2.694	.293	1.081	2.720	7.7
4.017	-.100	1.000	4.017	.0	2.782	.307	1.051	2.810	7.7
4.122	-.097	1.000	4.122	.0	2.882	.312	1.034	2.909	7.5
4.206	-.100	1.000	4.206	.0	2.989	.328	1.015	3.017	7.6
4.312	-.100	1.000	4.312	.0	3.097	.318	1.008	3.123	7.2
4.517	-.100	1.000	4.517	.0	3.201	.336	1.001	3.229	7.2
4.622	-.097	1.001	4.622	.0	3.285	.336	1.001	3.312	7.1
4.706	-.100	1.001	4.706	.0	3.485	.393	.999	3.517	7.6
4.812	-.100	.999	4.812	.0	3.593	.381	.998	3.623	7.2
					3.697	.399	.998	3.729	7.2

TABLE 6.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
3.781	.398	.999	3.812	7.1
3.980	.459	1.000	4.017	7.6
4.089	.443	1.000	4.123	7.2
4.193	.462	1.000	4.229	7.2
4.277	.459	1.000	4.312	7.1
4.476	.525	1.001	4.517	7.6
4.585	.505	1.001	4.623	7.2
4.689	.525	1.001	4.729	7.2
4.773	.521	1.001	4.812	7.1
4.971	.591	1.000	5.017	7.6
5.081	.568	1.000	5.123	7.2
5.185	.588	1.000	5.229	7.2
5.269	.582	1.000	5.312	7.1
5.467	.657	1.001	5.517	7.6
5.577	.630	1.000	5.623	7.2
5.681	.651	1.000	5.729	7.2
5.766	.644	1.000	5.812	7.1
.002	-.038	3.385	.010	15.1
.100	-.011	3.386	.112	15.2
.186	.013	3.390	.201	15.2
.286	.040	3.394	.304	15.2
.387	.067	3.397	.409	15.1
.484	.092	3.404	.510	15.1
.583	.120	3.409	.612	15.2
.669	.144	3.420	.701	15.2
.768	.171	3.435	.804	15.2
.869	.197	3.451	.909	15.1
.967	.222	3.476	1.010	15.1
1.066	.251	3.490	1.112	15.2
1.151	.274	3.506	1.201	15.2
1.251	.302	3.522	1.304	15.2
1.352	.328	3.528	1.409	15.1
1.450	.352	3.493	1.510	15.1
1.548	.382	3.418	1.612	15.2
1.634	.405	3.269	1.701	15.2
1.733	.434	3.016	1.804	15.2
1.835	.458	2.734	1.909	15.1
1.933	.482	2.299	2.010	15.1
2.031	.512	2.053	2.112	15.2
2.116	.536	1.823	2.201	15.2
2.216	.565	1.612	2.304	15.2
2.317	.589	1.457	2.409	15.1
2.416	.612	1.306	2.510	15.1
2.514	.643	1.229	2.612	15.2
2.599	.667	1.167	2.701	15.2
2.698	.696	1.117	2.804	15.2
2.800	.719	1.085	2.909	15.1
2.904	.750	1.057	3.017	15.2
3.006	.776	1.040	3.122	15.2
3.088	.800	1.026	3.208	15.2
3.188	.829	1.017	3.312	15.2
3.387	.881	1.008	3.517	15.2
3.488	.907	1.005	3.622	15.2
3.571	.930	1.002	3.708	15.2
3.671	.960	1.001	3.812	15.2
3.869	1.011	1.000	4.017	15.2
3.971	1.038	1.000	4.122	15.2
4.053	1.061	1.000	4.208	15.2
4.153	1.091	1.000	4.312	15.2
4.352	1.142	1.001	4.517	15.2
4.454	1.168	1.001	4.622	15.2
4.536	1.192	1.001	4.708	15.2
4.636	1.223	1.001	4.812	15.2
4.834	1.273	1.000	5.017	15.2
4.936	1.299	1.000	5.122	15.2
5.018	1.323	1.000	5.208	15.2
5.118	1.354	1.000	5.312	15.2
5.317	1.404	1.000	5.517	15.2
5.419	1.430	1.000	5.622	15.2
5.501	1.454	1.000	5.708	15.2
5.601	1.485	1.001	5.812	15.2
-.011	.002	3.441	.012	25.0
.065	.040	3.442	.096	25.4
.158	.084	3.447	.200	25.3
.254	.128	3.452	.305	25.2
.337	.162	3.455	.394	24.8
.442	.214	3.457	.512	25.0
.516	.254	3.463	.596	25.4
.610	.298	3.471	.700	25.3
.706	.341	3.482	.805	25.2
.790	.372	3.492	.894	24.8
.895	.425	3.509	1.012	25.0
.968	.468	3.515	1.096	25.4
1.062	.512	3.525	1.200	25.3
1.159	.554	3.532	1.305	25.2
1.244	.582	3.537	1.394	24.8
1.349	.636	3.507	1.512	25.0
1.420	.682	3.495	1.596	25.4

TABLE 6.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
1.514	.726	3.475	1.700	25.3
1.611	.767	3.405	1.805	25.2
1.698	.792	3.296	1.894	24.8
1.802	.848	3.051	2.012	25.0
1.872	.897	2.879	2.096	25.4
1.966	.940	2.645	2.200	25.3
2.064	.980	2.353	2.305	25.2
2.152	1.002	2.113	2.394	24.8
2.255	1.059	1.881	2.512	25.0
2.323	1.111	1.755	2.596	25.4
2.418	1.154	1.605	2.700	25.3
2.516	1.193	1.469	2.805	25.2
2.708	1.270	1.331	3.012	25.0
2.775	1.325	1.288	3.096	25.4
2.870	1.368	1.232	3.200	25.3
2.968	1.405	1.184	3.305	25.2
3.059	1.422	1.143	3.394	24.8
3.151	1.468	1.084	3.497	24.9
3.605	1.678	1.007	3.997	24.9
4.058	1.888	1.000	4.497	24.9
4.512	2.099	1.000	4.997	24.9
4.966	2.309	1.000	5.497	24.9
5.419	2.519	1.000	5.997	24.9
-.017	.015	3.440	.012	28.4
.055	.055	3.441	.095	28.6
.150	.101	3.443	.200	27.9
.243	.149	3.447	.305	27.8
.335	.197	3.450	.408	27.7
.423	.252	3.459	.512	28.4
.494	.295	3.465	.595	28.6
.592	.335	3.471	.700	27.9
.686	.382	3.482	.805	27.8
.777	.430	3.491	.908	27.7
.863	.490	3.502	1.012	28.4
.933	.534	3.503	1.095	28.6
1.034	.569	3.503	1.200	27.9
1.128	.615	3.501	1.305	27.8
1.220	.662	3.492	1.408	27.7
1.303	.727	3.407	1.512	28.4
1.372	.774	3.378	1.595	28.6
1.476	.802	3.337	1.700	27.9
1.571	.848	3.269	1.805	27.8
1.663	.895	3.173	1.908	27.7
1.743	.965	2.919	2.012	28.4

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
1.811	1.013	2.788	2.095	28.6
1.918	1.036	2.596	2.200	27.9
2.013	1.080	2.371	2.305	27.8
2.105	1.128	2.173	2.408	27.7
2.183	1.202	1.902	2.512	28.4
2.250	1.253	1.786	2.595	28.6
2.360	1.270	1.663	2.700	27.9
2.456	1.313	1.533	2.805	27.8
2.548	1.360	1.435	2.908	27.7
2.626	1.401	1.386	2.996	27.7
2.623	1.440	1.367	3.012	28.4
2.688	1.492	1.317	3.095	28.6
2.802	1.504	1.263	3.200	27.9
2.898	1.546	1.206	3.305	27.8
2.990	1.593	1.164	3.408	27.7
3.068	1.634	1.107	3.496	27.7
3.511	1.867	1.011	3.996	27.7
3.953	2.099	1.000	4.496	27.7
4.396	2.332	1.000	4.996	27.7
4.838	2.565	1.000	5.496	27.7
5.281	2.797	1.001	5.996	27.7
-.034	.013	3.432	-.003	30.0
.051	.063	3.436	.095	30.1
.142	.115	3.440	.200	29.9
.233	.168	3.442	.305	30.1
.320	.218	3.448	.405	30.1
.400	.263	3.452	.497	30.0
.483	.313	3.461	.595	30.1
.576	.364	3.469	.700	29.9
.665	.419	3.479	.805	30.1
.753	.469	3.489	.905	30.1
.833	.513	3.490	.997	30.0
.916	.564	3.488	1.095	30.1
1.009	.614	3.481	1.200	29.9
1.098	.670	3.467	1.305	30.1
1.186	.719	3.447	1.405	30.1
1.266	.762	3.333	1.497	30.0
1.349	.815	3.278	1.595	30.1
1.442	.863	3.219	1.700	29.9
1.531	.920	3.136	1.805	30.1
1.618	.970	3.043	1.905	30.1
1.699	1.012	2.808	1.997	30.0
1.781	1.066	2.673	2.095	30.1
1.875	1.113	2.501	2.200	29.9

TABLE 6.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
1.963	1.171	2.312	2.305	30.1
2.051	1.220	2.142	2.405	30.1
2.132	1.262	1.878	2.497	30.0
2.214	1.316	1.762	2.595	30.1
2.309	1.362	1.643	2.700	29.9
2.396	1.422	1.536	2.805	30.1
2.484	1.470	1.443	2.905	30.1
2.565	1.512	1.325	2.997	30.0
2.647	1.567	1.261	3.095	30.1
2.742	1.612	1.195	3.200	29.9
2.828	1.672	1.136	3.305	30.1
2.917	1.721	1.055	3.405	30.1
3.449	1.982	1.011	3.997	29.5
3.884	2.228	1.000	4.497	29.5
4.319	2.474	1.000	4.997	29.5
4.754	2.720	1.000	5.497	29.5
5.189	2.966	1.000	5.997	29.5
-.049	.044	3.429	.001	38.4
.025	.101	3.453	.095	38.4
.107	.167	3.455	.200	38.4
.189	.232	3.458	.305	38.4
.272	.297	3.463	.410	38.4
.343	.354	3.452	.501	38.4
.417	.412	3.480	.595	38.4
.499	.477	3.487	.700	38.4
.582	.542	3.488	.805	38.4
.664	.607	3.484	.910	38.4
.736	.664	3.408	1.001	38.4
.809	.722	3.385	1.095	38.4
.891	.787	3.313	1.200	38.4
.974	.852	3.222	1.305	38.4
1.056	.918	3.108	1.410	38.4
1.128	.974	2.779	1.501	38.4
1.201	1.032	2.672	1.595	38.4
1.283	1.097	2.544	1.700	38.4
1.366	1.163	2.399	1.805	38.4
1.448	1.228	2.249	1.910	38.4
1.520	1.285	1.994	2.001	38.4
1.593	1.342	1.900	2.095	38.4
1.675	1.408	1.796	2.200	38.4
1.758	1.473	1.688	2.305	38.4
1.840	1.538	1.588	2.410	38.4
1.912	1.595	1.384	2.501	38.4
1.985	1.653	1.350	2.595	38.4
2.068	1.718	1.297	2.700	38.4
2.150	1.783	1.262	2.805	38.4
2.232	1.848	1.224	2.910	38.4
2.304	1.905	1.139	3.001	38.4
2.377	1.963	1.127	3.095	38.4
2.460	2.028	1.102	3.200	38.4
2.542	2.093	1.085	3.305	38.4
2.625	2.159	1.064	3.410	38.4
3.086	2.524	1.007	3.998	38.4
3.478	2.834	1.000	4.498	38.4
3.870	3.144	1.000	4.998	38.4
4.262	3.454	1.000	5.498	38.4
4.654	3.765	1.000	5.998	38.4
-.061	.071	3.441	.011	45.4
-.002	.132	3.444	.095	45.4
.072	.206	3.449	.200	45.4
.145	.281	3.456	.305	45.4
.220	.357	3.466	.411	45.4
.290	.428	3.464	.511	45.4
.349	.488	3.472	.595	45.4
.423	.562	3.476	.700	45.4
.496	.637	3.470	.805	45.4
.571	.713	3.441	.911	45.4
.640	.784	3.315	1.011	45.4
.700	.844	3.238	1.095	45.4
.774	.918	3.109	1.200	45.4
.847	.994	2.925	1.305	45.4
.922	1.069	2.722	1.411	45.4
.991	1.140	2.389	1.511	45.4
1.051	1.200	2.247	1.595	45.4
1.125	1.274	2.091	1.700	45.4
1.198	1.350	1.916	1.805	45.4
1.273	1.426	1.761	1.911	45.4
1.342	1.496	1.592	2.011	45.4
1.402	1.557	1.515	2.095	45.4
1.476	1.630	1.424	2.200	45.4
1.549	1.706	1.336	2.305	45.4
1.624	1.782	1.261	2.411	45.4
1.693	1.852	1.168	2.511	45.4
1.753	1.913	1.142	2.595	45.4
1.827	1.986	1.118	2.700	45.4
1.900	2.062	1.095	2.805	45.4
1.974	2.138	1.076	2.911	45.4
2.044	2.209	1.046	3.011	45.4

TABLE 6.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
2.103	2.269	1.039	3.095	45.4
2.178	2.342	1.033	3.200	45.4
2.251	2.418	1.025	3.305	45.4
2.325	2.494	1.018	3.411	45.4
2.325	2.494	1.000	4.000	45.4
-.112	.110	3.437	.011	60.7
-.070	.185	3.431	.097	60.7
-.020	.275	3.434	.200	60.7
.032	.367	3.431	.305	60.7
.082	.458	3.455	.409	60.8
.132	.546	3.458	.511	60.7
.175	.622	3.451	.597	60.7
.224	.711	3.431	.700	60.7
.276	.803	3.364	.805	60.7
.326	.894	3.256	.909	60.8
.376	.982	3.005	1.011	60.7
.419	1.058	2.814	1.097	60.7
.469	1.147	2.593	1.200	60.7
.521	1.239	2.313	1.305	60.7
.570	1.331	2.060	1.409	60.8
.621	1.418	1.784	1.511	60.7
.664	1.494	1.651	1.597	60.7
.713	1.584	1.518	1.700	60.7
.765	1.675	1.381	1.805	60.7
.815	1.767	1.278	1.909	60.8
.865	1.855	1.195	2.011	60.7
.908	1.930	1.149	2.097	60.7
.958	2.020	1.109	2.200	60.7
1.010	2.111	1.071	2.305	60.7
1.059	2.203	1.043	2.409	60.8
1.110	2.291	1.022	2.511	60.7
1.153	2.366	1.014	2.597	60.7
1.202	2.456	1.007	2.700	60.7
1.254	2.547	1.004	2.805	60.7
1.303	2.640	1.000	2.909	60.8
1.354	2.727	1.000	3.011	60.7
1.397	2.802	1.000	3.097	60.7
1.446	2.892	1.000	3.200	60.7
1.499	2.983	1.000	3.305	60.7
1.547	3.076	1.000	3.409	60.8
-.173	.130	3.437	.007	76.1
-.147	.236	3.444	.116	76.1
-.126	.318	3.451	.201	76.1
-.102	.419	3.463	.305	76.1
-.076	.521	3.472	.410	76.1
-.052	.616	3.452	.507	76.1
-.027	.721	3.437	.616	76.1
-.006	.804	3.388	.701	76.1
.018	.905	3.265	.805	76.1
.045	1.007	3.095	.910	76.1
.068	1.101	2.730	1.007	76.1
.094	1.206	2.470	1.116	76.1
.114	1.289	2.248	1.201	76.1
.138	1.390	1.979	1.305	76.1
.165	1.492	1.792	1.410	76.1
.188	1.586	1.539	1.507	76.1
.214	1.691	1.408	1.616	76.1
.235	1.774	1.319	1.701	76.1
.258	1.875	1.219	1.805	76.1
.285	1.977	1.157	1.910	76.1
.309	2.071	1.097	2.007	76.1
.334	2.177	1.061	2.116	76.1
.355	2.260	1.041	2.201	76.1
.378	2.361	1.021	2.305	76.1
.406	2.462	1.011	2.410	76.1
.429	2.557	1.004	2.507	76.1
.455	2.662	1.000	2.616	76.1
.475	2.745	1.000	2.701	76.1
.498	2.846	1.000	2.805	76.1
.526	2.948	1.000	2.910	76.1
.550	3.042	1.000	3.007	76.1
.575	3.147	1.000	3.116	76.1
.595	3.230	1.000	3.201	76.1
.618	3.332	1.001	3.305	76.1
.647	3.433	1.000	3.410	76.1
-.231	.140	3.425	.010	90.3
-.232	.244	3.419	.114	90.3
-.232	.332	3.450	.202	90.3
-.233	.434	3.448	.304	90.3
-.233	.540	3.466	.410	90.3
-.234	.640	3.444	.510	90.3
-.234	.744	3.415	.614	90.3
-.235	.832	3.358	.702	90.3
-.235	.934	3.228	.804	90.3
-.236	1.040	3.000	.910	90.3
-.236	1.140	2.676	1.010	90.3
-.237	1.244	2.400	1.114	90.3

TABLE 6.- Concluded.

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
-.237	1.332	2.124	1.202	90.3
-.237	1.434	1.916	1.304	90.3
-.238	1.540	1.691	1.410	90.3
-.239	1.640	1.484	1.510	90.3
-.240	1.744	1.359	1.614	90.3
-.239	1.832	1.252	1.702	90.3
-.240	1.934	1.185	1.804	90.3
-.240	2.040	1.120	1.910	90.3
-.242	2.140	1.075	2.010	90.3
-.242	2.244	1.046	2.114	90.3
-.242	2.332	1.025	2.202	90.3
-.242	2.434	1.014	2.304	90.3
-.243	2.540	1.004	2.410	90.3
-.244	2.640	1.000	2.510	90.3
-.245	2.744	1.000	2.614	90.3
-.244	2.832	1.000	2.702	90.3
-.245	2.934	1.000	2.804	90.3
-.245	3.040	1.000	2.910	90.3
-.247	3.140	1.000	3.010	90.3
-.247	3.244	1.000	3.114	90.3
-.247	3.332	1.000	3.202	90.3
-.247	3.434	1.000	3.304	90.3
-.248	3.540	1.000	3.410	90.3

TABLE 7.- PITOT-PRESSURE MEASUREMENTS AT $x = 0.0$ in. FOR $M_\infty = 0.60$ WITH NPR = 4.02 AND $T_{t,j}/T_{t,\infty} = 0.91$

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
-.016	-.066	2.728	-.014	9.0	4.537	.655	.997	4.597	9.0
.106	-.047	2.733	.110	9.0	4.641	.671	.995	4.701	9.0
.209	-.031	2.736	.214	9.0	4.746	.688	.996	4.808	9.0
.294	-.017	2.738	.300	9.0	4.935	.718	.999	5.000	9.0
.397	-.001	2.739	.405	9.0	5.031	.733	1.000	5.097	9.0
.477	.012	2.733	.486	9.0	5.134	.750	1.000	5.201	9.0
.599	.031	2.734	.610	9.0	5.240	.766	.999	5.308	9.0
.703	.048	2.733	.714	9.0	5.429	.796	.999	5.500	9.0
.788	.061	2.732	.800	9.0	5.525	.812	.999	5.597	9.0
.891	.078	2.731	.905	9.0	5.628	.828	.999	5.701	9.0
.971	.090	2.735	.986	9.0	5.734	.845	.999	5.808	9.0
1.093	.110	2.738	1.110	9.0	5.923	.875	.997	6.000	9.0
1.196	.126	2.736	1.214	9.0	6.019	.890	.997	6.097	9.0
1.282	.139	2.742	1.300	9.0	6.122	.906	.997	6.201	9.0
1.385	.156	2.746	1.405	9.0	6.228	.923	.997	6.308	9.0
1.465	.168	2.747	1.486	9.0					
1.587	.188	2.751	1.610	9.0	-.006	-.036	2.727	.003	16.1
1.690	.204	2.752	1.714	9.0	.096	-.006	2.729	.110	16.1
1.775	.218	2.753	1.800	9.0	.188	.021	2.731	.205	16.1
1.879	.234	2.756	1.905	9.0	.281	.047	2.734	.302	16.1
1.959	.247	2.757	1.986	9.0	.377	.075	2.737	.402	16.1
2.081	.266	2.759	2.110	9.0	.474	.103	2.732	.503	16.1
2.184	.282	2.756	2.214	9.0	.577	.133	2.732	.610	16.1
2.269	.296	2.741	2.300	9.0	.668	.159	2.733	.705	16.1
2.372	.312	2.616	2.405	9.0	.761	.186	2.731	.802	16.1
2.453	.325	1.602	2.486	9.0	.858	.214	2.730	.902	16.1
2.575	.344	.851	2.610	9.0	.954	.241	2.737	1.003	16.1
2.678	.361	.878	2.714	9.0	1.057	.271	2.743	1.110	16.1
2.763	.374	.900	2.800	9.0	1.149	.297	2.748	1.205	16.1
2.866	.390	.921	2.905	9.0	1.242	.324	2.754	1.302	16.1
2.960	.405	.940	3.000	9.0	1.338	.352	2.768	1.402	16.1
3.056	.420	.954	3.097	9.0	1.435	.380	2.817	1.503	16.1
3.159	.437	.968	3.201	9.0	1.538	.410	2.821	1.610	16.1
3.257	.452	.980	3.300	9.0	1.629	.436	2.822	1.705	16.1
3.360	.469	.991	3.405	9.0	1.722	.463	2.823	1.802	16.1
3.454	.483	.995	3.500	9.0	1.819	.491	2.822	1.902	16.1
3.550	.499	.996	3.597	9.0	1.915	.518	2.823	2.003	16.1
3.653	.515	.996	3.701	9.0	2.018	.548	2.817	2.110	16.1
3.759	.532	.996	3.808	9.0	2.110	.574	2.813	2.205	16.1
3.947	.562	.999	4.000	9.0	2.203	.601	2.804	2.302	16.1
4.044	.577	.998	4.097	9.0	2.299	.629	2.784	2.402	16.1
4.147	.593	.998	4.201	9.0	2.396	.657	2.771	2.503	16.1
4.253	.610	.998	4.308	9.0	2.499	.687	1.910	2.610	16.1
4.441	.640	.997	4.500	9.0	2.590	.713	.826	2.705	16.1
					2.683	.740	.875	2.802	16.1

TABLE 7.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
2.780	.768	.899	2.902	16.1	1.262	.575	2.829	1.407	24.3
2.876	.795	.919	3.003	16.1	1.350	.615	2.828	1.505	24.3
2.979	.825	.941	3.110	16.1	1.447	.657	2.829	1.610	24.3
3.071	.851	.956	3.205	16.1	1.522	.693	2.829	1.693	24.3
3.163	.878	.971	3.302	16.1	1.619	.736	2.832	1.799	24.3
3.260	.906	.983	3.402	16.1	1.717	.781	2.831	1.907	24.3
3.349	.932	.993	3.495	16.1	1.806	.821	2.827	2.005	24.3
3.446	.960	.996	3.596	16.1	1.902	.863	2.820	2.110	24.3
3.548	.989	.996	3.701	16.1	1.978	.899	2.816	2.193	24.3
3.650	1.019	.996	3.808	16.1	2.074	.942	2.814	2.299	24.3
3.830	1.070	.998	3.995	16.1	2.173	.987	2.803	2.407	24.3
3.927	1.098	.997	4.096	16.1	2.262	1.027	2.769	2.505	24.3
4.028	1.127	.998	4.201	16.1	2.358	1.069	2.724	2.610	24.3
4.131	1.157	.998	4.308	16.1	2.433	1.105	2.637	2.693	24.3
4.310	1.209	.996	4.495	16.1	2.530	1.148	1.264	2.799	24.3
4.407	1.237	.997	4.596	16.1	2.629	1.193	.852	2.907	24.3
4.508	1.266	.996	4.701	16.1	2.717	1.233	.863	3.005	24.3
4.611	1.296	.997	4.808	16.1	2.814	1.275	.898	3.110	24.3
4.791	1.347	1.000	4.995	16.1	2.889	1.311	.921	3.193	24.3
4.888	1.375	1.000	5.096	16.1	2.985	1.355	.948	3.299	24.3
4.989	1.404	1.000	5.201	16.1	3.084	1.399	.969	3.407	24.3
5.092	1.434	1.000	5.308	16.1	3.179	1.442	.985	3.512	24.3
5.271	1.486	.998	5.495	16.1	3.259	1.473	.992	3.597	24.3
5.368	1.514	.999	5.596	16.1	3.362	1.521	.996	3.711	24.3
5.469	1.543	.999	5.701	16.1	3.446	1.557	.996	3.802	24.3
5.572	1.573	.999	5.808	16.1	3.635	1.648	.998	4.012	24.3
5.751	1.624	.997	5.995	16.1	3.715	1.679	.998	4.097	24.3
5.849	1.652	.997	6.096	16.1	3.818	1.727	.998	4.211	24.3
5.950	1.681	.997	6.201	16.1	3.901	1.763	.998	4.302	24.3
6.053	1.711	.997	6.308	16.1	4.091	1.855	.997	4.512	24.3
					4.171	1.884	.995	4.597	24.3
-.016	-.003	2.726	.005	24.3	4.274	1.932	.998	4.711	24.3
.080	.040	2.727	.110	24.3	4.357	1.968	.998	4.802	24.3
.156	.074	2.728	.193	24.3	4.546	2.061	1.000	5.012	24.3
.252	.118	2.731	.299	24.3	4.627	2.090	1.000	5.097	24.3
.351	.163	2.736	.407	24.3	4.730	2.138	1.000	5.211	24.3
.439	.203	2.731	.505	24.3	4.813	2.174	.999	5.302	24.3
.535	.246	2.739	.610	24.3	5.002	2.267	.998	5.512	24.3
.611	.281	2.752	.693	24.3	5.083	2.295	.998	5.597	24.3
.708	.324	2.762	.799	24.3	5.185	2.344	.998	5.711	24.3
.806	.369	2.793	.907	24.3	5.269	2.379	.998	5.802	24.3
.895	.409	2.841	1.005	24.3	5.457	2.473	.998	6.012	24.3
.991	.451	2.839	1.110	24.3	5.538	2.501	.998	6.097	24.3
1.067	.487	2.836	1.193	24.3	5.641	2.549	.998	6.211	24.3
1.163	.530	2.831	1.299	24.3	5.725	2.585	.998	6.302	24.3

TABLE 7.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
-.034	.031	2.715	.006	33.8
.053	.089	2.722	.110	33.7
.122	.136	2.728	.194	33.8
.209	.194	2.729	.298	33.7
.297	.253	2.734	.404	33.8
.382	.309	2.735	.506	33.8
.468	.366	2.795	.610	33.7
.538	.414	2.828	.694	33.8
.625	.471	2.836	.798	33.7
.713	.531	2.837	.904	33.8
.797	.587	2.834	1.006	33.8
.884	.644	2.837	1.110	33.7
.953	.692	2.837	1.194	33.8
1.041	.749	2.834	1.298	33.7
1.128	.809	2.829	1.404	33.8
1.213	.865	2.807	1.506	33.8
1.300	.922	2.804	1.610	33.7
1.369	.970	2.796	1.694	33.8
1.457	1.027	2.763	1.798	33.7
1.544	1.087	2.695	1.904	33.8
1.628	1.143	1.788	2.006	33.8
1.716	1.200	.897	2.110	33.7
1.785	1.248	.846	2.194	33.8
1.872	1.305	.857	2.298	33.7
1.959	1.365	.884	2.404	33.8
2.044	1.421	.903	2.506	33.8
2.131	1.477	.913	2.610	33.7
2.200	1.526	.901	2.694	33.8
2.288	1.582	.871	2.798	33.7
2.375	1.643	.847	2.904	33.8
2.460	1.699	.855	3.006	33.8
2.547	1.755	.876	3.110	33.7
2.616	1.804	.905	3.194	33.8
2.704	1.860	.933	3.298	33.7
2.791	1.921	.955	3.404	33.8
2.862	1.969	.970	3.490	33.8
2.951	2.028	.985	3.597	33.8
3.038	2.086	.992	3.701	33.8
3.125	2.144	.995	3.806	33.8
3.278	2.247	.999	3.990	33.8
3.367	2.306	.999	4.097	33.8
3.453	2.364	.999	4.201	33.8
3.541	2.422	.998	4.306	33.8
3.693	2.525	.996	4.490	33.8
3.782	2.584	.996	4.597	33.8

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
3.869	2.642	.996	4.701	33.8
3.956	2.700	.997	4.806	33.8
4.109	2.803	1.000	4.990	33.8
4.198	2.862	.999	5.097	33.8
4.284	2.920	.999	5.201	33.8
4.372	2.978	.999	5.306	33.8
4.525	3.081	.998	5.490	33.8
4.614	3.140	.999	5.597	33.8
4.700	3.198	.998	5.701	33.8
4.787	3.256	.999	5.806	33.8
4.940	3.359	.998	5.990	33.8
5.029	3.418	.998	6.097	33.8
5.115	3.476	.997	6.201	33.8
5.203	3.535	.997	6.306	33.8
.045	.100	2.727	.110	36.1
.134	.165	2.728	.220	36.1
.199	.214	2.729	.302	36.1
.346	.321	2.739	.484	36.1
.448	.395	2.824	.610	36.1
.538	.460	2.836	.720	36.1
.603	.508	2.838	.802	36.1
.750	.616	2.845	.984	36.1
.852	.689	2.840	1.110	36.1
.942	.755	2.835	1.220	36.1
1.007	.803	2.831	1.302	36.1
1.154	.911	2.811	1.484	36.1
1.256	.984	2.795	1.610	36.1
1.346	1.049	2.759	1.720	36.1
1.411	1.098	2.708	1.802	36.1
1.558	1.206	.841	1.984	36.1
1.660	1.279	.843	2.110	36.1
1.750	1.344	.857	2.220	36.1
1.814	1.393	.873	2.302	36.1
1.961	1.500	.911	2.484	36.1
2.064	1.573	.914	2.610	36.1
2.154	1.638	.888	2.720	36.1
2.218	1.688	.860	2.802	36.1
2.365	1.795	.876	2.984	36.1
2.468	1.868	.891	3.110	36.1
2.558	1.933	.923	3.220	36.1
2.622	1.983	.943	3.302	36.1
-.048	.046	2.750	.003	38.9
.040	.115	2.752	.115	38.6
.117	.179	2.752	.215	38.8

TABLE 7.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
.341	.360	2.780	.503	38.9
.430	.428	2.856	.615	38.6
.506	.492	2.864	.715	38.8
.730	.674	2.868	1.003	38.9
.821	.740	2.862	1.115	38.6
.896	.805	2.859	1.215	38.8
1.119	.988	2.798	1.503	38.9
1.211	1.052	2.663	1.615	38.6
1.286	1.119	1.928	1.715	38.8
1.509	1.302	.843	2.003	38.9
1.602	1.364	.857	2.115	38.6
1.675	1.432	.875	2.215	38.8
1.898	1.615	.918	2.503	38.9
1.992	1.676	.925	2.615	38.6
2.065	1.745	.925	2.715	38.8
2.287	1.929	.920	3.003	38.9
2.383	1.988	.930	3.115	38.6
2.455	2.058	.940	3.215	38.8
-.069	.072	2.719	.005	46.8
.008	.153	2.721	.118	46.8
.075	.225	2.720	.216	46.8
.123	.276	2.723	.285	46.8
.204	.363	2.758	.404	46.9
.273	.436	2.824	.505	46.8
.350	.518	2.832	.618	46.8
.418	.590	2.833	.716	46.8
.465	.640	2.834	.785	46.8
.545	.728	2.831	.904	46.9
.615	.801	2.831	1.005	46.8
.692	.883	2.819	1.118	46.8
.760	.955	2.789	1.216	46.8
.807	1.005	2.737	1.285	46.8
.887	1.093	2.234	1.404	46.9
.957	1.165	.830	1.505	46.8
1.034	1.247	.834	1.618	46.8
1.102	1.319	.841	1.716	46.8
1.150	1.369	.848	1.785	46.8
1.229	1.458	.861	1.904	46.9
1.300	1.530	.880	2.005	46.8
1.377	1.612	.900	2.118	46.8
1.444	1.684	.914	2.216	46.8
1.492	1.734	.919	2.285	46.8
1.571	1.823	.931	2.404	46.9
1.642	1.895	.938	2.505	46.8

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
1.719	1.976	.948	2.618	46.8
1.786	2.048	.953	2.716	46.8
1.834	2.098	.957	2.785	46.8
1.913	2.187	.961	2.904	46.9
1.984	2.259	.970	3.005	46.8
2.063	2.339	.968	3.117	46.8
2.125	2.404	.973	3.207	46.8
2.194	2.478	.978	3.308	46.8
2.254	2.552	.987	3.404	46.9
2.362	2.657	.988	3.554	46.8
2.405	2.703	.990	3.617	46.8
2.467	2.768	.992	3.707	46.8
2.536	2.842	.995	3.808	46.8
2.705	3.021	.995	4.054	46.8
2.748	3.067	.996	4.117	46.8
2.810	3.133	.995	4.207	46.8
2.879	3.206	.996	4.308	46.8
3.047	3.385	.997	4.554	46.8
3.090	3.431	.997	4.617	46.8
3.152	3.497	.997	4.707	46.8
3.221	3.571	.997	4.808	46.8
3.390	3.750	.997	5.054	46.8
3.433	3.796	.996	5.117	46.8
3.495	3.861	.997	5.207	46.8
3.564	3.935	.997	5.308	46.8
3.732	4.114	.996	5.554	46.8
3.775	4.160	.996	5.617	46.8
3.837	4.225	.996	5.707	46.8
3.906	4.299	.996	5.808	46.8
4.075	4.478	.997	6.054	46.8
4.118	4.524	.997	6.117	46.8
4.180	4.590	.997	6.207	46.8
4.249	4.663	.997	6.308	46.8
-.093	.099	2.717	.012	55.5
-.041	.182	2.720	.109	56.1
.017	.270	2.721	.215	56.2
.037	.282	2.724	.236	55.0
.130	.412	2.820	.396	54.9
.191	.511	2.823	.512	55.5
.237	.597	2.831	.609	56.1
.296	.685	2.835	.715	56.2
.324	.691	2.837	.736	55.0
.417	.821	2.830	.896	54.9
.474	.923	2.819	1.012	55.5

TABLE 7.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
.516	1.012	2.745	1.109	56.1	3.457	5.067	.998	6.117	54.5
.574	1.101	1.973	1.215	56.2	3.502	5.137	.998	6.201	54.5
.610	1.101	1.428	1.236	55.0	3.557	5.236	.997	6.314	54.6
.704	1.230	.832	1.396	54.9					
.757	1.335	.839	1.512	55.5	-.112	.210	2.749	.102	69.2
.794	1.427	.851	1.609	56.1	-.063	.314	2.750	.216	68.1
.852	1.516	.865	1.715	56.2	-.035	.414	2.760	.319	69.2
.897	1.511	.870	1.736	55.0	.001	.508	2.848	.420	69.2
.992	1.639	.897	1.896	54.9	.031	.587	2.855	.505	69.2
1.041	1.747	.911	2.012	55.5	.066	.678	2.861	.602	69.2
1.073	1.843	.927	2.109	56.1	.124	.778	2.863	.716	68.1
1.130	1.932	.935	2.215	56.2	.143	.881	2.862	.819	69.2
1.184	1.921	.939	2.236	55.0	.179	.975	2.851	.920	69.2
1.279	2.049	.953	2.396	54.9	.209	1.054	2.749	1.005	69.2
1.324	2.159	.958	2.512	55.5	.243	1.145	1.521	1.102	69.2
1.352	2.258	.970	2.609	56.1	.310	1.241	.831	1.216	68.1
1.408	2.347	.976	2.715	56.2	.321	1.348	.835	1.319	69.2
1.470	2.330	.978	2.736	55.0	.356	1.442	.846	1.420	69.2
1.567	2.458	.988	2.896	54.9	.386	1.521	.864	1.505	69.2
1.676	2.549	.991	3.033	54.3	.421	1.612	.879	1.602	69.2
1.714	2.625	.993	3.117	54.5	.497	1.705	.900	1.716	68.1
1.761	2.694	.993	3.201	54.5	.498	1.816	.915	1.819	69.2
1.821	2.790	.994	3.314	54.6	.534	1.910	.926	1.920	69.2
1.854	2.867	.997	3.396	54.9	.564	1.989	.940	2.005	69.2
1.968	2.955	.996	3.533	54.3	.599	2.080	.950	2.102	69.2
2.005	3.032	.996	3.617	54.5	.684	2.169	.960	2.216	68.1
2.051	3.101	.996	3.701	54.5	.676	2.283	.968	2.319	69.2
2.110	3.198	.995	3.814	54.6	.712	2.377	.978	2.420	69.2
2.260	3.361	.995	4.033	54.3	.742	2.456	.986	2.505	69.2
2.295	3.439	.996	4.117	54.5	.776	2.547	.991	2.602	69.2
2.341	3.508	.996	4.201	54.5	.871	2.633	.994	2.716	68.1
2.400	3.605	.995	4.314	54.6	.854	2.750	.996	2.819	69.2
2.552	3.766	.997	4.533	54.3	.889	2.844	.996	2.920	69.2
2.586	3.846	.995	4.617	54.5	.917	2.918	.995	2.998	69.2
2.631	3.915	.997	4.701	54.5	.954	3.014	.995	3.102	69.2
2.689	4.013	.997	4.814	54.6	.990	3.108	.994	3.202	69.2
2.844	4.172	.997	5.033	54.3	1.031	3.218	.995	3.319	69.2
2.876	4.253	.997	5.117	54.5	1.067	3.312	.994	3.420	69.2
2.922	4.323	.997	5.201	54.5	1.095	3.385	.996	3.498	69.2
2.979	4.421	.997	5.314	54.6	1.138	3.497	.996	3.619	69.2
3.136	4.578	.996	5.533	54.3	1.167	3.575	.996	3.702	69.2
3.166	4.660	.996	5.617	54.5	1.205	3.674	.996	3.808	69.2
3.212	4.730	.996	5.701	54.5	1.273	3.852	.995	3.998	69.2
3.268	4.829	.996	5.814	54.6	1.315	3.965	.995	4.119	69.2
3.428	4.984	.997	6.033	54.3	1.345	4.043	.996	4.202	69.2

TABLE 7.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
1.383	4.142	.995	4.308	69.2
1.450	4.320	.994	4.498	69.2
1.493	4.432	.994	4.619	69.2
1.523	4.510	.994	4.702	69.2
1.560	4.609	.998	4.808	69.2
1.628	4.787	.997	4.998	69.2
1.671	4.899	.996	5.119	69.2
1.700	4.977	.996	5.202	69.2
1.738	5.076	.997	5.308	69.2
1.806	5.254	.996	5.498	69.2
1.848	5.367	.996	5.619	69.2
1.878	5.445	.996	5.702	69.2
1.916	5.544	.996	5.808	69.2
1.983	5.722	.995	5.998	69.2
2.026	5.834	.994	6.119	69.2
2.056	5.912	.995	6.202	69.2
2.093	6.011	.995	6.308	69.2
-.208	.132	2.751	.003	84.5
-.198	.240	2.754	.112	84.5
-.190	.330	2.754	.202	84.7
-.183	.429	2.762	.301	84.9
-.182	.535	2.857	.407	85.7
-.160	.629	2.856	.503	84.5
-.150	.738	2.864	.612	84.5
-.143	.828	2.864	.702	84.7
-.138	.927	2.860	.801	84.9
-.145	1.034	2.832	.907	85.7
-.112	1.127	2.545	1.003	84.5
-.102	1.236	.831	1.112	84.5
-.097	1.326	.833	1.202	84.7
-.094	1.425	.842	1.301	84.9
-.107	1.532	.860	1.407	85.7
-.065	1.625	.880	1.503	84.5
-.055	1.733	.902	1.612	84.5
-.050	1.823	.915	1.702	84.7
-.049	1.923	.929	1.801	84.9
-.070	2.031	.942	1.907	85.7
-.017	2.122	.954	2.003	84.5
-.007	2.231	.966	2.112	84.5
-.003	2.321	.975	2.202	84.7
-.005	2.421	.985	2.301	84.9
-.033	2.529	.991	2.407	85.7
.031	2.620	.993	2.503	84.5
.040	2.729	.996	2.612	84.5

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r,in.	ϕ, deg
.043	2.819	.996	2.702	84.7
.040	2.919	.996	2.801	84.9
.005	3.028	.997	2.907	85.7
.079	3.127	.995	3.012	84.5
.046	3.236	.995	3.117	85.3
.090	3.317	.995	3.202	84.7
.107	3.422	.995	3.308	84.5
.042	3.527	.996	3.407	85.7
.127	3.625	.997	3.512	84.5
.088	3.734	.996	3.617	85.3
.070	3.799	.996	3.681	85.6
.155	3.919	.996	3.808	84.5
.175	4.123	.997	4.012	84.5
.129	4.232	.996	4.117	85.3
.109	4.298	.996	4.181	85.6
.203	4.417	.996	4.308	84.5
.222	4.620	.996	4.512	84.5
.170	4.731	.995	4.617	85.3
.147	4.796	.994	4.681	85.6
.251	4.915	.997	4.808	84.5
.270	5.118	.998	5.012	84.5
.212	5.229	.997	5.117	85.3
.186	5.295	.997	5.181	85.6
.298	5.413	.996	5.308	84.5
.318	5.616	.997	5.512	84.5
.253	5.727	.996	5.617	85.3
.224	5.794	.996	5.681	85.6
.346	5.910	.996	5.808	84.5
.365	6.114	.996	6.012	84.5
.294	6.226	.995	6.117	85.3
.262	6.292	.995	6.181	85.6
.394	6.408	.995	6.308	84.5
-.265	.132	2.750	.005	98.7
-.279	.220	2.750	.094	98.7
-.297	.340	2.749	.216	98.7
-.310	.421	2.749	.297	98.7
-.326	.526	2.835	.404	98.7
-.341	.626	2.854	.505	98.7
-.354	.715	2.860	.594	98.7
-.373	.835	2.858	.716	98.7
-.385	.915	2.856	.797	98.7
-.401	1.021	2.851	.904	98.7
-.416	1.120	2.598	1.005	98.7
-.430	1.209	.855	1.094	98.7

TABLE 7.- Concluded

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
-.448	1.329	.832	1.216	98.7
-.461	1.410	.837	1.297	98.7
-.477	1.515	.853	1.404	98.7
-.492	1.615	.880	1.505	98.7
-.505	1.703	.900	1.594	98.7
-.524	1.823	.918	1.716	98.7
-.536	1.904	.924	1.797	98.7
-.552	2.009	.940	1.904	98.7
-.568	2.109	.958	2.005	98.7
-.581	2.197	.967	2.094	98.7
-.599	2.318	.980	2.216	98.7
-.612	2.398	.984	2.297	98.7
-.628	2.503	.992	2.404	98.7
-.643	2.603	.995	2.505	98.7
-.657	2.692	.996	2.594	98.7
-.675	2.812	.996	2.716	98.7
-.687	2.892	.997	2.797	98.7
-.703	2.998	.996	2.904	98.7
-.718	3.092	.994	2.999	98.7
-.737	3.217	.994	3.125	98.7
-.748	3.308	.995	3.217	98.7
-.765	3.417	.994	3.328	98.7
-.779	3.492	.996	3.404	98.7
-.793	3.586	.996	3.499	98.7
-.812	3.711	.996	3.625	98.7
-.824	3.802	.995	3.717	98.7
-.840	3.911	.995	3.828	98.7
-.869	4.080	.995	3.999	98.7
-.888	4.205	.996	4.125	98.7
-.899	4.297	.997	4.217	98.7
-.915	4.406	.995	4.328	98.7
-.944	4.575	.994	4.499	98.7
-.963	4.699	.994	4.625	98.7
-.974	4.791	.995	4.717	98.7
-.991	4.900	.996	4.828	98.7
-1.020	5.069	.998	4.999	98.7
-1.039	5.194	.997	5.125	98.7
-1.049	5.285	.998	5.217	98.7
-1.066	5.394	.997	5.328	98.7
-1.095	5.563	.996	5.499	98.7
-1.114	5.688	.996	5.625	98.7
-1.124	5.779	.996	5.717	98.7
-1.141	5.889	.996	5.828	98.7
-1.171	6.057	.997	5.999	98.7
-1.190	6.182	.996	6.125	98.7
-1.200	6.274	.996	6.217	98.7
-1.216	6.383	.996	6.328	98.7

TABLE 8.- PITOT-PRESSURE MEASUREMENTS AT $x = 2.572$ in. FOR $M_\infty = 0.60$ WITH NPR = 4.02 AND $T_{t,j}/T_{t,\infty} = 0.93$

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
-.004	-.093	3.067	-.004	1.8
.080	-.090	3.048	.080	1.8
.186	-.087	3.047	.187	1.8
.294	-.083	3.050	.294	1.8
.374	-.074	3.035	.375	2.5
.496	-.078	3.035	.496	1.8
.580	-.075	3.020	.580	1.8
.686	-.072	3.016	.687	1.8
.793	-.068	3.013	.794	1.8
.874	-.052	2.995	.875	2.5
.995	-.062	3.001	.996	1.8
1.080	-.059	2.988	1.080	1.8
1.186	-.056	2.983	1.187	1.8
1.293	-.052	2.979	1.294	1.8
1.373	-.031	2.960	1.375	2.5
1.495	-.047	2.958	1.496	1.8
1.579	-.044	2.941	1.580	1.8
1.686	-.041	2.935	1.687	1.8
1.793	-.036	2.930	1.794	1.8
1.873	-.009	2.906	1.875	2.5
1.995	-.031	2.759	1.996	1.8
2.079	-.028	2.312	2.080	1.8
2.186	-.025	1.618	2.187	1.8
2.293	-.020	1.197	2.294	1.8
2.372	.012	1.031	2.375	2.5
2.495	-.016	.936	2.496	1.8
2.579	-.012	.932	2.580	1.8
2.685	-.010	.945	2.687	1.8
2.792	-.005	.959	2.794	1.8
2.872	.034	.970	2.875	2.5
2.990	.066	.982	2.995	3.0
3.084	.071	.989	3.088	3.0
3.189	.076	.996	3.194	3.0
3.284	.081	.997	3.289	3.0
3.371	.055	.998	3.375	2.5
3.490	.092	.997	3.495	3.0
3.583	.096	.997	3.588	3.0
3.689	.102	.997	3.694	3.0
3.784	.107	.998	3.789	3.0
3.989	.117	.998	3.995	3.0
4.082	.122	.998	4.088	3.0
4.188	.128	.998	4.194	3.0
4.283	.133	.998	4.289	3.0
4.488	.143	.998	4.495	3.0
4.582	.148	.998	4.588	3.0
4.687	.153	.998	4.694	3.0
4.782	.158	.998	4.789	3.0
4.988	.169	1.000	4.995	3.0
5.081	.174	1.000	5.088	3.0
5.187	.179	1.000	5.194	3.0
5.282	.184	1.000	5.289	3.0
5.487	.195	.998	5.495	3.0
5.580	.199	.998	5.588	3.0
5.686	.205	.998	5.694	3.0
5.781	.210	.998	5.789	3.0
5.986	.220	.998	5.995	3.0
6.080	.225	.998	6.088	3.0
6.185	.231	.998	6.194	3.0
6.280	.236	.998	6.289	3.0
-.027	-.073	3.075	-.025	7.6
.078	-.060	3.056	.080	7.4
.182	-.047	3.053	.185	7.4
.265	-.034	3.048	.269	7.6
.370	-.019	3.043	.375	7.7
.469	-.006	3.037	.475	7.6
.573	.004	3.027	.580	7.4
.678	.018	3.020	.685	7.4
.761	.032	3.009	.769	7.6
.865	.048	3.001	.875	7.7
.964	.060	3.002	.975	7.6
1.069	.069	2.995	1.080	7.4
1.174	.082	2.989	1.185	7.4
1.256	.099	2.981	1.269	7.6
1.361	.114	2.971	1.375	7.7
1.460	.126	2.962	1.475	7.6
1.565	.133	2.952	1.580	7.4
1.670	.146	2.943	1.685	7.4
1.752	.165	2.935	1.769	7.6
1.856	.181	2.918	1.875	7.7
1.955	.193	2.840	1.975	7.6
2.061	.197	2.444	2.080	7.4
2.165	.210	1.761	2.185	7.4
2.247	.231	1.351	2.269	7.6
2.352	.248	1.069	2.375	7.7
2.451	.259	.955	2.475	7.6
2.557	.262	.933	2.580	7.4
2.661	.274	.945	2.685	7.4
2.743	.297	.955	2.769	7.6

TABLE 8.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
2.848	.314	.969	2.875	7.7	1.314	.341	2.991	1.375	15.9
2.952	.341	.982	2.983	7.9	1.411	.362	2.974	1.475	15.7
3.058	.343	.988	3.088	7.7	1.511	.397	2.971	1.580	15.9
3.142	.354	.995	3.172	7.7	1.606	.420	2.961	1.679	15.8
3.250	.370	.996	3.282	7.7	1.713	.452	2.951	1.790	15.9
3.343	.381	.998	3.375	7.7	1.794	.478	2.941	1.875	15.9
3.448	.410	.997	3.483	7.9	1.893	.497	2.920	1.975	15.7
3.554	.410	.997	3.588	7.7	1.991	.534	2.884	2.080	15.9
3.637	.421	.997	3.672	7.7	2.088	.557	2.680	2.179	15.8
3.746	.437	.997	3.782	7.7	2.194	.589	2.124	2.290	15.9
3.943	.478	.998	3.983	7.9	2.275	.615	1.599	2.375	15.9
4.049	.476	.997	4.088	7.7	2.374	.632	1.216	2.475	15.7
4.133	.488	.997	4.172	7.7	2.472	.671	1.019	2.580	15.9
4.241	.504	.997	4.282	7.7	2.569	.693	.944	2.679	15.8
4.438	.547	.998	4.483	7.9	2.675	.725	.946	2.790	15.9
4.545	.543	.997	4.588	7.7	2.756	.752	.956	2.875	15.9
4.628	.554	.997	4.672	7.7	2.860	.782	.971	2.983	15.9
4.737	.571	.997	4.782	7.7	2.961	.811	.981	3.088	15.9
4.933	.616	1.001	4.983	7.9	3.041	.834	.990	3.172	15.9
5.040	.610	1.000	5.088	7.7	3.143	.863	.996	3.278	15.9
5.124	.621	1.000	5.172	7.7	3.237	.890	.998	3.375	15.9
5.232	.637	1.000	5.282	7.7	3.341	.919	.998	3.483	15.9
5.429	.684	.998	5.483	7.9	3.441	.948	.998	3.588	15.9
5.536	.677	.997	5.588	7.7	3.522	.971	.997	3.672	15.9
5.619	.688	.997	5.672	7.7	3.624	1.000	.997	3.778	15.9
5.728	.704	.997	5.782	7.7	3.822	1.056	.997	3.983	15.9
5.924	.753	.999	5.983	7.9	3.922	1.085	.997	4.088	15.9
6.031	.743	.999	6.088	7.7	4.003	1.108	.998	4.172	15.9
6.115	.754	.999	6.172	7.7	4.105	1.137	.997	4.278	15.9
6.223	.771	.999	6.282	7.7	4.302	1.194	.997	4.483	15.9
					4.403	1.222	.997	4.588	15.9
-.033	-.044	3.082	-.025	15.7	4.484	1.245	.998	4.672	15.9
.068	-.015	3.067	.080	15.9	4.586	1.275	.997	4.778	15.9
.163	.011	3.064	.179	15.8	4.783	1.331	1.000	4.983	15.9
.270	.042	3.062	.290	15.9	4.884	1.360	1.000	5.088	15.9
.352	.066	3.056	.375	15.9	4.965	1.383	1.000	5.172	15.9
.449	.091	3.043	.475	15.7	5.066	1.412	1.000	5.278	15.9
.549	.122	3.041	.580	15.9	5.264	1.468	.997	5.483	15.9
.644	.148	3.033	.679	15.8	5.365	1.497	.997	5.588	15.9
.751	.179	3.023	.790	15.9	5.445	1.520	.997	5.672	15.9
.833	.203	3.014	.875	15.9	5.547	1.549	.997	5.778	15.9
.930	.226	3.008	.975	15.7	5.745	1.605	.999	5.983	15.9
1.030	.260	3.008	1.080	15.9	5.845	1.634	.999	6.088	15.9
1.125	.284	3.002	1.179	15.8	5.926	1.657	.999	6.172	15.9
1.232	.315	2.998	1.290	15.9	6.028	1.686	.999	6.278	15.9

TABLE 8.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
-.042	-.011	3.101	-.022	25.4	4.172	2.063	.998	4.675	26.2
.050	.033	3.075	.080	25.4	4.278	2.079	.997	4.777	25.8
.126	.069	3.059	.164	25.4	4.474	2.146	1.000	4.983	25.5
.244	.136	3.054	.299	26.5	4.538	2.257	1.000	5.089	26.3
.314	.169	3.052	.377	26.3	4.621	2.283	1.000	5.175	26.2
.409	.204	3.049	.478	25.4	4.728	2.296	1.000	5.277	25.8
.502	.248	3.047	.580	25.4	4.925	2.361	.998	5.483	25.5
.578	.284	3.043	.664	25.4	4.986	2.479	.998	5.589	26.3
.691	.359	3.029	.799	26.5	5.070	2.504	.998	5.675	26.2
.762	.391	3.018	.877	26.3	5.179	2.514	.997	5.777	25.8
.861	.419	3.007	.978	25.4	5.377	2.576	.998	5.983	25.5
.953	.462	2.995	1.080	25.4	5.434	2.701	.999	6.089	26.3
1.029	.499	2.980	1.164	25.4	5.518	2.724	.999	6.175	26.2
1.139	.582	2.962	1.299	26.5	5.629	2.732	1.000	6.277	25.8
1.210	.612	2.954	1.377	26.3					
1.312	.633	2.942	1.478	25.4	-.027	.012	3.058	.002	28.9
1.405	.677	2.935	1.580	25.4	.041	.050	3.079	.080	28.9
1.481	.713	2.925	1.664	25.4	.130	.101	3.076	.182	29.1
1.586	.805	2.893	1.799	26.5	.226	.152	3.050	.291	28.9
1.658	.834	2.835	1.877	26.3	.299	.192	3.054	.374	28.9
1.764	.848	2.811	1.978	25.4	.411	.254	3.023	.502	28.9
1.857	.891	2.718	2.080	25.4	.478	.292	3.037	.580	28.9
1.932	.928	2.554	2.164	25.4	.567	.344	3.038	.682	29.1
2.034	1.028	2.314	2.299	26.5	.664	.394	3.031	.791	28.9
2.107	1.055	2.183	2.377	26.3	.736	.434	3.022	.874	28.9
2.215	1.063	1.761	2.478	25.4	.848	.496	2.973	1.002	28.9
2.308	1.106	1.530	2.580	25.4	.916	.534	2.969	1.080	28.9
2.384	1.143	1.296	2.664	25.4	1.003	.587	2.957	1.182	29.1
2.481	1.250	1.072	2.799	26.5	1.102	.635	2.942	1.291	28.9
2.555	1.277	1.009	2.877	26.3	1.174	.676	2.928	1.374	28.9
2.667	1.277	.923	2.978	25.4	1.286	.737	2.878	1.502	28.9
2.760	1.320	.944	3.080	25.4	1.353	.776	2.789	1.580	28.9
2.836	1.357	.966	3.164	25.4	1.440	.831	2.609	1.682	29.1
2.928	1.426	.985	3.277	25.8	1.539	.877	2.398	1.791	28.9
3.003	1.499	.993	3.377	26.3	1.611	.918	2.200	1.874	28.9
3.121	1.499	.997	3.483	25.5	1.724	.979	2.098	2.002	28.9
3.193	1.593	.997	3.589	26.3	1.791	1.018	1.735	2.080	28.9
3.275	1.622	.997	3.675	26.2	1.877	1.074	1.426	2.182	29.1
3.378	1.644	.997	3.777	25.8	1.977	1.119	1.234	2.291	28.9
3.572	1.715	.998	3.983	25.5	2.049	1.160	1.110	2.374	28.9
3.641	1.814	.998	4.089	26.3	2.161	1.221	1.002	2.502	28.9
3.723	1.842	.998	4.175	26.2	2.229	1.260	.938	2.580	28.9
3.828	1.861	.997	4.277	25.8	2.314	1.318	.904	2.682	29.1
4.023	1.930	.996	4.483	25.5	2.415	1.361	.889	2.791	28.9
4.089	2.036	.997	4.589	26.3	2.487	1.401	.885	2.874	28.9

TABLE 8.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
2.559	1.496	.906	2.983	29.8
2.666	1.502	.931	3.080	28.9
2.750	1.561	.954	3.182	29.1
2.852	1.602	.975	3.291	28.9
2.924	1.643	.984	3.374	28.9
2.993	1.744	.994	3.483	29.8
3.083	1.798	.997	3.588	29.8
3.152	1.851	.997	3.674	30.0
3.247	1.893	.997	3.778	29.8
3.427	1.992	.997	3.983	29.8
3.516	2.047	.998	4.088	29.8
3.585	2.101	.998	4.174	30.0
3.681	2.141	.998	4.278	29.8
3.861	2.241	.997	4.483	29.8
3.950	2.295	.995	4.588	29.8
4.018	2.351	.997	4.674	30.0
4.115	2.390	.996	4.778	29.8
4.294	2.489	1.000	4.983	29.8
4.384	2.544	.999	5.088	29.8
4.451	2.600	1.000	5.174	30.0
4.549	2.638	1.000	5.278	29.8
4.728	2.737	.997	5.483	29.8
4.818	2.793	.998	5.588	29.8
4.884	2.850	.998	5.674	30.0
4.983	2.887	.998	5.778	29.8
5.162	2.985	.998	5.983	29.8
5.252	3.041	.997	6.088	29.8
5.317	3.100	.997	6.174	30.0
5.417	3.136	.998	6.278	29.8
-.053	.003	3.082	-.025	30.2
.038	.056	3.093	.080	30.1
.129	.108	3.067	.185	30.1
.204	.152	3.050	.271	30.1
.311	.214	3.046	.396	30.1
.379	.255	3.054	.475	30.2
.471	.306	3.049	.580	30.1
.562	.359	3.043	.685	30.1
.636	.402	3.029	.771	30.1
.744	.464	3.006	.896	30.1
.811	.507	2.992	.975	30.2
.903	.557	2.970	1.080	30.1
.995	.610	2.955	1.185	30.1
1.069	.653	2.926	1.271	30.1
1.177	.715	2.893	1.396	30.1
1.243	.758	2.772	1.475	30.2
1.336	.808	2.608	1.580	30.1
1.427	.860	2.416	1.685	30.1
1.501	.904	2.201	1.771	30.1
1.609	.966	2.001	1.896	30.1
1.675	1.010	1.670	1.975	30.2
1.768	1.059	1.417	2.080	30.1
1.860	1.111	1.235	2.185	30.1
1.934	1.155	1.128	2.271	30.1
2.042	1.216	1.033	2.396	30.1
2.107	1.261	.939	2.475	30.2
2.201	1.310	.913	2.580	30.1
2.292	1.362	.898	2.685	30.1
2.366	1.406	.892	2.771	30.1
2.474	1.467	.893	2.896	30.1
2.550	1.511	.914	2.983	30.1
2.639	1.563	.940	3.086	30.1
2.725	1.612	.962	3.185	30.1
2.799	1.657	.975	3.271	30.1
2.907	1.718	.986	3.396	30.1
2.983	1.762	.993	3.483	30.1
3.072	1.813	.997	3.586	30.1
3.165	1.869	.997	3.695	30.1
3.237	1.909	.997	3.777	30.1
3.416	2.013	.997	3.983	30.1
3.504	2.064	.998	4.086	30.1
3.598	2.120	.998	4.195	30.1
3.670	2.160	.997	4.277	30.1
3.848	2.263	.997	4.483	30.1
3.937	2.315	.995	4.586	30.1
4.031	2.371	.996	4.695	30.1
4.102	2.411	.997	4.777	30.1
4.281	2.514	1.000	4.983	30.1
4.370	2.565	.999	5.086	30.1
4.463	2.622	.999	5.195	30.1
4.535	2.661	1.000	5.277	30.1
4.713	2.765	.997	5.483	30.1
4.802	2.816	.998	5.586	30.1
4.896	2.872	.998	5.695	30.1
4.968	2.912	.997	5.777	30.1
5.146	3.015	.998	5.983	30.1
5.235	3.067	.997	6.086	30.1
5.328	3.123	.997	6.195	30.1
5.400	3.163	.998	6.277	30.1
-.068	.025	3.070	-.025	37.7

TABLE 8.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
.015	.091	3.098	.080	37.9	3.701	3.002	.998	4.777	38.3
.097	.156	3.066	.185	38.0	3.864	3.127	.999	4.983	38.2
.171	.215	3.064	.280	38.1	3.968	3.165	.998	5.089	37.9
.246	.273	3.066	.375	38.0	4.016	3.241	.999	5.173	38.2
.328	.331	3.061	.475	37.7	4.093	3.312	1.000	5.277	38.3
.409	.398	3.059	.580	37.9	4.257	3.436	.998	5.483	38.2
.491	.464	3.052	.685	38.0	4.363	3.472	.997	5.589	37.9
.565	.523	3.037	.780	38.1	4.408	3.551	.997	5.673	38.2
.640	.581	3.013	.875	38.0	4.486	3.621	.998	5.777	38.3
.724	.636	2.957	.975	37.7	4.650	3.745	.998	5.983	38.2
.804	.705	2.895	1.080	37.9	4.758	3.779	.997	6.089	37.9
.885	.772	2.811	1.185	38.0	4.801	3.860	.997	6.173	38.2
.958	.832	2.646	1.280	38.1	4.878	3.931	.998	6.277	38.3
1.034	.889	2.384	1.375	38.0					
1.120	.942	1.796	1.475	37.7	-.085	.046	3.069	-.024	45.4
1.199	1.012	1.534	1.580	37.9	-.013	.119	3.087	.078	45.3
1.279	1.080	1.362	1.685	38.0	.063	.197	3.074	.187	45.4
1.351	1.141	1.178	1.780	38.1	.137	.271	3.071	.292	45.4
1.428	1.197	1.046	1.875	38.0	.219	.350	3.072	.406	45.0
1.516	1.247	.968	1.975	37.7	.266	.402	3.057	.476	45.4
1.593	1.319	.947	2.080	37.9	.338	.475	3.066	.578	45.3
1.673	1.388	.945	2.185	38.0	.414	.552	3.040	.687	45.4
1.745	1.449	.949	2.280	38.1	.488	.627	3.003	.792	45.4
1.821	1.505	.952	2.375	38.0	.572	.704	2.930	.906	45.0
1.912	1.552	.954	2.475	37.7	.617	.758	2.784	.976	45.4
1.988	1.626	.950	2.580	37.9	.690	.830	2.583	1.078	45.3
2.067	1.696	.945	2.685	38.0	.765	.908	2.127	1.187	45.4
2.138	1.758	.945	2.780	38.1	.839	.983	1.677	1.292	45.4
2.215	1.813	.951	2.875	38.0	.926	1.057	1.323	1.406	45.0
2.293	1.889	.956	2.983	38.2	.969	1.114	1.115	1.476	45.4
2.390	1.937	.966	3.089	37.9	1.042	1.185	1.010	1.578	45.3
2.444	2.004	.973	3.173	38.2	1.116	1.264	.942	1.687	45.4
2.523	2.073	.982	3.277	38.3	1.190	1.339	.927	1.792	45.4
2.609	2.121	.990	3.375	38.0	1.279	1.411	.934	1.906	45.0
2.686	2.198	.993	3.483	38.2	1.320	1.469	.940	1.976	45.4
2.784	2.244	.996	3.589	37.9	1.394	1.541	.947	2.078	45.3
2.837	2.314	.997	3.673	38.2	1.468	1.620	.956	2.187	45.4
2.916	2.382	.997	3.777	38.3	1.541	1.695	.964	2.292	45.4
3.079	2.508	.998	3.983	38.2	1.632	1.765	.970	2.406	45.0
3.179	2.551	.997	4.089	37.9	1.671	1.825	.973	2.476	45.4
3.230	2.623	.997	4.173	38.2	1.745	1.896	.977	2.578	45.3
3.308	2.692	.998	4.277	38.3	1.819	1.976	.981	2.687	45.4
3.472	2.817	.998	4.483	38.2	1.893	2.051	.983	2.792	45.4
3.574	2.858	.996	4.589	37.9	1.985	2.119	.987	2.906	45.0
3.623	2.932	.998	4.673	38.2					

TABLE 8.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
2.024	2.190	.988	2.983	45.4
2.100	2.262	.989	3.088	45.4
2.172	2.338	.993	3.192	45.4
2.230	2.399	.993	3.277	45.4
2.339	2.473	.997	3.406	45.0
2.375	2.546	.997	3.483	45.4
2.451	2.618	.997	3.588	45.4
2.523	2.694	.998	3.692	45.4
2.581	2.756	.996	3.777	45.4
2.725	2.902	.998	3.983	45.4
2.802	2.974	.998	4.088	45.4
2.874	3.051	.997	4.192	45.4
2.932	3.112	.997	4.277	45.4
3.076	3.258	.998	4.483	45.4
3.153	3.330	.998	4.588	45.4
3.224	3.407	.998	4.692	45.4
3.283	3.468	.997	4.777	45.4
3.427	3.615	.999	4.983	45.4
3.504	3.686	.998	5.088	45.4
3.575	3.763	.998	5.192	45.4
3.634	3.825	.999	5.277	45.4
3.778	3.971	.998	5.483	45.4
3.855	4.042	.998	5.588	45.4
3.926	4.119	.998	5.692	45.4
3.984	4.181	.997	5.777	45.4
4.128	4.327	.997	5.983	45.4
4.207	4.398	.997	6.088	45.4
4.277	4.475	.998	6.192	45.4
4.335	4.537	.997	6.277	45.4
-.132	.080	3.041	-.025	61.4
-.079	.170	3.061	.079	60.8
-.027	.263	3.078	.185	60.8
.011	.337	3.087	.269	61.1
.074	.448	3.073	.397	61.0
.108	.519	3.050	.475	61.4
.165	.606	3.021	.579	60.8
.217	.699	2.929	.685	60.8
.252	.775	2.757	.769	61.1
.317	.885	2.306	.897	61.0
.347	.958	1.669	.975	61.4
.409	1.042	1.267	1.079	60.8
.461	1.135	1.042	1.185	60.8
.494	1.213	.955	1.269	61.1
.559	1.323	.919	1.397	61.0

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
.587	1.397	.923	1.475	61.4
.653	1.479	.933	1.579	60.8
.705	1.572	.944	1.685	60.8
.735	1.651	.952	1.769	61.1
.802	1.760	.960	1.897	61.0
.826	1.836	.969	1.975	61.4
.897	1.915	.979	2.079	60.8
.949	2.008	.986	2.185	60.8
.976	2.089	.991	2.269	61.1
1.045	2.197	.996	2.397	61.0
1.066	2.275	.997	2.475	61.4
1.142	2.351	.997	2.579	60.8
1.193	2.445	.998	2.685	60.8
1.218	2.527	.998	2.769	61.1
1.287	2.634	.998	2.897	61.0
1.339	2.704	.996	2.983	60.8
1.390	2.795	.995	3.087	60.8
1.432	2.870	.995	3.173	60.8
1.531	2.957	.996	3.298	60.1
1.530	3.071	.998	3.397	61.0
1.583	3.140	.997	3.483	60.8
1.634	3.231	.996	3.587	60.8
1.676	3.306	.996	3.673	60.8
1.781	3.390	.997	3.798	60.1
1.827	3.576	.997	3.983	60.8
1.878	3.668	.997	4.087	60.8
1.920	3.743	.996	4.173	60.8
2.031	3.824	.998	4.298	60.1
2.071	4.013	.996	4.483	60.8
2.122	4.104	.997	4.587	60.8
2.164	4.179	.996	4.673	60.8
2.280	4.257	.998	4.798	60.1
2.315	4.449	.998	4.983	60.8
2.366	4.540	.999	5.087	60.8
2.408	4.615	.999	5.173	60.8
2.530	4.690	.998	5.298	60.1
2.559	4.885	.997	5.483	60.8
2.611	4.977	.997	5.587	60.8
2.653	5.052	.996	5.673	60.8
2.779	5.123	.998	5.798	60.1
2.804	5.322	.998	5.983	60.8
2.855	5.413	.999	6.087	60.8
2.897	5.488	.998	6.173	60.8
3.029	5.557	.998	6.298	60.1

TABLE 8.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
-.180	.099	3.028	-.025	76.0	1.050	4.654	.998	4.693	74.9
-.155	.201	3.033	.080	76.1	1.005	4.775	.998	4.799	75.8
-.130	.303	3.043	.185	76.1	1.054	4.952	.999	4.983	75.7
-.108	.394	3.049	.279	76.1	1.136	5.040	.999	5.089	75.1
-.085	.488	3.048	.375	76.1	1.180	5.137	1.000	5.193	74.9
-.059	.584	3.035	.475	76.0	1.128	5.260	.999	5.299	75.8
-.035	.686	2.954	.580	76.1	1.177	5.437	.997	5.483	75.7
-.010	.788	2.751	.685	76.1	1.265	5.523	.997	5.589	75.1
.012	.879	2.367	.779	76.1	1.310	5.619	.997	5.693	74.9
.035	.973	1.784	.875	76.1	1.251	5.744	.998	5.799	75.8
.062	1.069	1.239	.975	76.0	1.300	5.921	.999	5.983	75.7
.086	1.172	1.002	1.080	76.1	1.393	6.007	.998	6.089	75.1
.111	1.274	.928	1.185	76.1	1.440	6.102	.999	6.193	74.9
.132	1.365	.916	1.279	76.1	1.374	6.229	.999	6.299	75.8
.155	1.458	.926	1.375	76.1					
.184	1.554	.939	1.475	76.0	-.234	.106	3.022	-.024	91.0
.206	1.657	.947	1.580	76.1	-.231	.211	3.026	.081	90.3
.231	1.759	.956	1.685	76.1	-.232	.315	3.030	.185	90.3
.252	1.850	.966	1.779	76.1	-.232	.411	3.036	.281	90.3
.275	1.944	.976	1.875	76.1	-.233	.527	3.032	.397	90.2
.305	2.039	.985	1.975	76.0	-.242	.606	3.006	.476	91.0
.327	2.142	.992	2.080	76.1	-.234	.711	2.966	.581	90.3
.351	2.244	.997	2.185	76.1	-.234	.815	2.834	.685	90.3
.372	2.335	.997	2.279	76.1	-.235	.911	2.457	.781	90.3
.395	2.429	.998	2.375	76.1	-.235	1.027	1.658	.897	90.2
.426	2.524	.997	2.475	76.0	-.251	1.106	1.174	.976	91.0
.447	2.627	.997	2.580	76.1	-.236	1.211	.996	1.081	90.3
.472	2.730	.997	2.685	76.1	-.237	1.315	.930	1.185	90.3
.492	2.821	.997	2.779	76.1	-.237	1.411	.917	1.281	90.3
.515	2.915	.998	2.875	76.1	-.237	1.527	.930	1.397	90.2
.561	3.014	.995	2.983	75.7	-.260	1.606	.944	1.476	91.0
.622	3.107	.996	3.089	75.1	-.239	1.711	.951	1.581	90.3
.660	3.205	.996	3.193	74.9	-.239	1.815	.959	1.685	90.3
.637	3.321	.996	3.299	75.8	-.240	1.911	.969	1.781	90.3
.635	3.400	.998	3.375	76.1	-.239	2.027	.981	1.897	90.2
.684	3.498	.997	3.483	75.7	-.268	2.106	.992	1.976	91.0
.751	3.590	.997	3.589	75.1	-.241	2.211	.996	2.081	90.3
.790	3.688	.997	3.693	74.9	-.241	2.315	.997	2.185	90.3
.760	3.806	.997	3.799	75.8	-.242	2.411	.999	2.281	90.3
.807	3.983	.997	3.983	75.7	-.241	2.527	.999	2.397	90.2
.879	4.074	.997	4.089	75.1	-.277	2.606	.997	2.476	91.0
.920	4.171	.997	4.193	74.9	-.243	2.711	.997	2.581	90.3
.882	4.290	.997	4.299	75.8	-.244	2.815	.997	2.685	90.3
.931	4.468	.997	4.483	75.7	-.244	2.911	.997	2.781	90.3
1.008	4.557	.996	4.589	75.1	-.243	3.027	.997	2.897	90.2
					-.302	3.112	.994	2.983	91.3

TABLE 8.- Concluded

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
-.286	3.217	.995	3.088	91.0
-.269	3.322	.995	3.192	90.7
-.273	3.407	.995	3.277	90.7
-.245	3.527	.998	3.397	90.2
-.313	3.612	.997	3.483	91.3
-.295	3.717	.996	3.588	91.0
-.275	3.822	.996	3.692	90.7
-.279	3.907	.997	3.777	90.7
-.325	4.112	.996	3.983	91.3
-.303	4.217	.997	4.088	91.0
-.281	4.322	.996	4.192	90.7
-.285	4.407	.996	4.277	90.7
-.336	4.612	.996	4.483	91.3
-.312	4.717	.997	4.588	91.0
-.287	4.822	.997	4.692	90.7
-.291	4.907	.996	4.777	90.7
-.347	5.111	.999	4.983	91.3
-.320	5.217	1.000	5.088	91.0
-.292	5.322	.999	5.192	90.7
-.297	5.407	.999	5.277	90.7
-.358	5.611	.996	5.483	91.3
-.329	5.717	.997	5.588	91.0
-.298	5.822	.998	5.692	90.7
-.303	5.907	.998	5.777	90.7
-.370	6.111	.999	5.983	91.3
-.337	6.217	.999	6.088	91.0
-.304	6.322	.999	6.192	90.7
-.309	6.407	.999	6.277	90.7

TABLE 9.- PITOT-PRESSURE MEASUREMENTS AT $x = 5.136$ in. FOR $M_\infty = 0.60$ WITH NPR = 3.98 AND $T_{t,j}/T_{t,\infty} = 0.90$

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
.000	-.100	2.653	.000	.0	4.509	-.102	1.000	4.509	.0
.125	-.100	2.657	.125	.0	4.613	-.102	1.000	4.613	.0
.225	-.100	2.660	.225	.0	4.709	-.102	1.000	4.709	.0
.316	-.100	2.662	.316	.0	4.802	-.102	1.000	4.802	.0
.400	-.100	2.663	.400	.0	5.009	-.102	1.000	5.009	.0
.500	-.100	2.665	.500	.0	5.113	-.102	.999	5.113	.0
.625	-.100	2.668	.625	.0	5.209	-.102	1.000	5.209	.0
.725	-.100	2.669	.725	.0	5.302	-.102	.999	5.302	.0
.816	-.100	2.675	.816	.0	5.509	-.102	.998	5.509	.0
.900	-.100	2.678	.900	.0	5.613	-.102	.998	5.613	.0
1.000	-.100	2.697	1.000	.0	5.709	-.102	.997	5.709	.0
1.125	-.100	2.707	1.125	.0	5.802	-.102	.998	5.802	.0
1.225	-.100	2.714	1.225	.0	6.009	-.102	1.000	6.009	.0
1.316	-.100	2.722	1.316	.0	6.113	-.102	1.000	6.113	.0
1.400	-.101	2.728	1.400	.0	6.209	-.102	1.000	6.209	.0
1.500	-.101	2.747	1.500	.0	6.302	-.102	.999	6.302	.0
1.625	-.101	2.752	1.625	.0					
1.725	-.101	2.758	1.725	.0	-.001	-.070	2.649	.001	7.4
1.816	-.101	2.762	1.816	.0	.103	-.054	2.651	.106	7.9
1.900	-.101	2.729	1.900	.0	.206	-.039	2.655	.210	7.9
2.000	-.101	2.452	2.000	.0	.307	-.028	2.662	.312	7.7
2.125	-.101	2.052	2.125	.0	.394	-.018	2.662	.400	7.4
2.225	-.101	1.687	2.225	.0	.495	-.005	2.666	.501	7.4
2.316	-.101	1.393	2.316	.0	.598	.015	2.669	.606	7.9
2.400	-.101	1.235	2.400	.0	.701	.030	2.675	.710	7.9
2.500	-.101	1.042	2.500	.0	.802	.039	2.683	.812	7.7
2.625	-.101	.972	2.625	.0	.890	.046	2.687	.900	7.4
2.725	-.101	.958	2.725	.0	.991	.060	2.701	1.001	7.4
2.816	-.101	.966	2.816	.0	1.093	.084	2.708	1.106	7.9
2.900	-.101	.972	2.900	.0	1.197	.099	2.719	1.210	7.9
3.009	-.101	.982	3.009	.0	1.298	.106	2.732	1.312	7.7
3.113	-.101	.989	3.113	.0	1.386	.111	2.740	1.400	7.4
3.209	-.101	.995	3.209	.0	1.487	.124	2.762	1.501	7.4
3.302	-.101	.996	3.302	.0	1.588	.153	2.769	1.606	7.9
3.400	-.101	.999	3.400	.0	1.692	.168	2.773	1.710	7.9
3.509	-.101	.997	3.509	.0	1.793	.172	2.766	1.812	7.7
3.613	-.101	.997	3.613	.0	1.882	.176	2.754	1.900	7.4
3.709	-.101	.997	3.709	.0	1.982	.189	2.599	2.001	7.4
3.802	-.101	.997	3.802	.0	2.083	.222	2.321	2.106	7.9
4.009	-.101	.998	4.009	.0	2.187	.237	1.962	2.210	7.9
4.113	-.101	.998	4.113	.0	2.289	.239	1.592	2.312	7.7
4.209	-.101	.998	4.209	.0	2.377	.241	1.378	2.400	7.4
4.302	-.101	.998	4.302	.0	2.478	.254	1.138	2.501	7.4
					2.579	.291	1.028	2.606	7.9
					2.682	.306	.977	2.710	7.9
					2.784	.306	.967	2.812	7.7

TABLE 9.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
2.873	.306	.970	2.900	7.4	1.341	.329	2.737	1.399	15.3
3.003	.312	.983	3.029	7.3	1.444	.357	2.753	1.505	15.3
3.067	.320	.989	3.094	7.3	1.539	.385	2.762	1.604	15.3
3.153	.340	.992	3.181	7.4	1.642	.412	2.770	1.710	15.3
3.274	.343	.995	3.302	7.2	1.745	.434	2.774	1.816	15.1
3.369	.371	.998	3.400	7.4	1.824	.461	2.770	1.899	15.3
3.499	.375	.999	3.529	7.3	1.926	.489	2.748	2.005	15.3
3.563	.384	.998	3.594	7.3	2.021	.517	2.701	2.104	15.3
3.649	.405	.997	3.681	7.4	2.124	.543	2.537	2.210	15.3
3.770	.406	.997	3.802	7.2	2.228	.564	2.150	2.316	15.1
3.995	.439	.998	4.029	7.3	2.306	.593	1.913	2.399	15.3
4.059	.447	.998	4.094	7.3	2.409	.621	1.547	2.505	15.3
4.144	.469	.998	4.181	7.4	2.503	.649	1.348	2.604	15.3
4.266	.469	.998	4.302	7.2	2.606	.675	1.174	2.710	15.3
4.491	.502	1.001	4.529	7.3	2.711	.695	1.068	2.816	15.1
4.555	.510	1.000	4.594	7.3	2.788	.725	1.038	2.899	15.3
4.640	.534	1.000	4.681	7.4	2.894	.734	.988	3.003	15.0
4.762	.532	1.000	4.802	7.2	3.000	.778	.987	3.118	15.2
4.987	.565	1.000	5.029	7.3	3.095	.802	.991	3.215	15.2
5.051	.573	1.000	5.094	7.3	3.184	.810	.993	3.303	14.9
5.136	.598	1.000	5.181	7.4	3.271	.857	.997	3.399	15.3
5.258	.594	1.000	5.302	7.2	3.377	.863	.998	3.503	15.0
5.483	.628	.997	5.529	7.3	3.483	.910	.997	3.618	15.2
5.547	.636	.998	5.594	7.3	3.577	.933	.998	3.715	15.2
5.632	.663	.997	5.681	7.4	3.667	.939	.998	3.803	14.9
5.755	.657	.997	5.802	7.2	3.860	.992	.997	4.003	15.0
5.979	.691	1.000	6.029	7.3	3.965	1.041	.997	4.118	15.2
6.043	.700	1.000	6.094	7.3	4.060	1.063	.997	4.215	15.2
6.128	.727	.999	6.181	7.4	4.150	1.068	.998	4.303	14.9
6.251	.720	1.000	6.302	7.2	4.343	1.121	1.001	4.503	15.0
					4.448	1.172	1.000	4.618	15.2
-.003	-.038	2.643	.005	15.3	4.542	1.194	.999	4.715	15.2
.092	-.012	2.647	.104	15.3	4.633	1.197	1.000	4.803	14.9
.195	.016	2.651	.210	15.3	4.826	1.250	.999	5.003	15.0
.297	.042	2.660	.316	15.1	4.930	1.303	.999	5.118	15.2
.377	.066	2.661	.399	15.3	5.025	1.325	.999	5.215	15.2
.479	.094	2.668	.505	15.3	5.116	1.326	.998	5.303	14.9
.574	.120	2.673	.604	15.3	5.309	1.379	.997	5.503	15.0
.677	.148	2.678	.710	15.3	5.413	1.434	.997	5.618	15.2
.780	.173	2.687	.816	15.1	5.508	1.456	.996	5.715	15.2
.859	.198	2.691	.899	15.3	5.599	1.455	.998	5.803	14.9
.962	.226	2.707	1.005	15.3	5.792	1.508	.999	6.003	15.0
1.056	.252	2.713	1.104	15.3	5.895	1.565	.999	6.118	15.2
1.159	.280	2.719	1.210	15.3	5.990	1.587	.999	6.215	15.2
1.263	.303	2.731	1.316	15.1	6.082	1.584	.998	6.303	14.9

TABLE 9.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
-.026	-.006	2.642	-.005	24.7	4.737	2.135	.998	5.217	24.2
.082	.043	2.645	.113	24.7	4.832	2.133	.999	5.302	23.8
.168	.083	2.651	.208	24.7	5.082	2.315	.998	5.605	24.4
.266	.128	2.661	.316	24.7	5.193	2.340	.998	5.717	24.2
.337	.161	2.668	.394	24.7	5.289	2.335	.998	5.802	23.8
.428	.203	2.678	.495	24.7	5.537	2.522	.999	6.105	24.4
.536	.252	2.687	.613	24.7	5.649	2.545	.998	6.217	24.2
.622	.292	2.696	.708	24.7	5.747	2.536	.999	6.302	23.8
.720	.337	2.708	.816	24.7					
.791	.370	2.715	.894	24.7	-.039	.001	2.640	-.014	28.0
.883	.412	2.739	.995	24.7	.068	.057	2.646	.106	27.8
.990	.461	2.744	1.113	24.7	.164	.105	2.654	.214	27.5
1.077	.501	2.751	1.208	24.7	.255	.150	2.663	.316	27.3
1.174	.546	2.756	1.316	24.7	.347	.197	2.673	.419	27.3
1.245	.579	2.757	1.394	24.7	.403	.236	2.680	.486	28.0
1.337	.621	2.708	1.495	24.7	.510	.290	2.694	.606	27.8
1.444	.670	2.673	1.613	24.7	.608	.336	2.709	.714	27.5
1.531	.710	2.637	1.708	24.7	.700	.379	2.718	.816	27.3
1.628	.755	2.562	1.816	24.7	.792	.426	2.725	.919	27.3
1.700	.789	2.505	1.894	24.7	.844	.470	2.746	.986	28.0
1.791	.830	2.250	1.995	24.7	.952	.524	2.746	1.106	27.8
1.899	.879	2.097	2.113	24.7	1.051	.567	2.736	1.214	27.5
1.985	.919	1.978	2.208	24.7	1.144	.608	2.719	1.316	27.3
2.082	.964	1.811	2.316	24.7	1.236	.655	2.701	1.419	27.3
2.154	.998	1.713	2.394	24.7	1.286	.705	2.571	1.486	28.0
2.245	1.039	1.382	2.495	24.7	1.394	.757	2.476	1.606	27.8
2.353	1.088	1.260	2.613	24.7	1.495	.797	2.321	1.714	27.5
2.439	1.128	1.184	2.708	24.7	1.589	.838	2.211	1.816	27.3
2.537	1.173	1.097	2.816	24.7	1.681	.884	2.106	1.919	27.3
2.608	1.207	1.063	2.894	24.7	1.727	.939	1.847	1.986	28.0
2.700	1.248	.988	2.995	24.7	1.836	.991	1.683	2.106	27.8
2.807	1.297	.980	3.113	24.7	1.938	1.028	1.501	2.214	27.5
2.894	1.337	.979	3.208	24.7	2.033	1.067	1.393	2.316	27.3
2.991	1.382	.988	3.316	24.7	2.125	1.113	1.311	2.419	27.3
3.062	1.416	.993	3.394	24.7	2.169	1.174	1.129	2.486	28.0
3.261	1.487	.999	3.605	24.4	2.279	1.224	1.057	2.606	27.8
3.369	1.520	.997	3.717	24.2	2.382	1.259	.997	2.714	27.5
3.459	1.527	.997	3.802	23.8	2.478	1.296	.968	2.816	27.3
3.716	1.694	.998	4.105	24.4	2.570	1.342	.956	2.919	27.3
3.825	1.725	.999	4.217	24.2	2.611	1.408	.949	2.986	28.0
3.917	1.729	.998	4.302	23.8	2.721	1.457	.962	3.106	27.8
4.171	1.901	1.002	4.605	24.4	2.825	1.490	.977	3.214	27.5
4.281	1.930	1.001	4.717	24.2	2.914	1.510	.986	3.302	27.1
4.374	1.931	1.001	4.802	23.8	3.014	1.571	.994	3.419	27.3
4.627	2.108	1.000	5.105	24.4	3.116	1.616	.997	3.530	27.2

TABLE 9.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
3.189	1.654	.997	3.613	27.2
3.282	1.703	.997	3.718	27.2
3.359	1.738	.997	3.802	27.1
3.560	1.845	.998	4.030	27.2
3.634	1.882	.999	4.113	27.2
3.727	1.932	.999	4.218	27.2
3.804	1.966	.999	4.302	27.1
4.005	2.073	1.000	4.530	27.2
4.079	2.111	1.001	4.613	27.2
4.172	2.160	1.001	4.718	27.2
4.249	2.194	1.000	4.802	27.1
4.450	2.301	.998	5.030	27.2
4.524	2.339	.998	5.113	27.2
4.617	2.388	.999	5.218	27.2
4.694	2.422	.999	5.302	27.1
4.895	2.529	.998	5.530	27.2
4.969	2.567	.998	5.613	27.2
5.061	2.617	.998	5.718	27.2
5.139	2.650	.998	5.802	27.1
5.340	2.757	.999	6.030	27.2
5.414	2.795	.998	6.113	27.2
5.506	2.845	.999	6.218	27.2
5.584	2.878	.999	6.302	27.1
-.032	.016	2.644	-.001	30.4
.075	.081	2.650	.125	30.6
.167	.134	2.660	.231	30.6
.221	.167	2.664	.294	30.6
.310	.214	2.674	.394	30.2
.399	.269	2.688	.499	30.4
.506	.335	2.703	.625	30.6
.597	.389	2.716	.731	30.6
.652	.422	2.724	.794	30.6
.742	.466	2.731	.894	30.2
.830	.523	2.748	.999	30.4
.936	.590	2.737	1.125	30.6
1.027	.643	2.708	1.231	30.6
1.082	.677	2.671	1.294	30.6
1.174	.718	2.626	1.394	30.2
1.261	.776	2.437	1.499	30.4
1.366	.844	2.277	1.625	30.6
1.458	.898	2.107	1.731	30.6
1.512	.931	1.974	1.794	30.6
1.606	.969	1.842	1.894	30.2
1.692	1.029	1.603	1.999	30.4
1.797	1.099	1.428	2.125	30.6

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
1.888	1.152	1.301	2.231	30.6
1.942	1.186	1.219	2.294	30.6
2.038	1.221	1.146	2.394	30.2
2.124	1.282	1.026	2.499	30.4
2.227	1.354	.974	2.625	30.6
2.319	1.407	.949	2.731	30.6
2.373	1.441	.941	2.794	30.6
2.470	1.473	.941	2.894	30.2
2.555	1.535	.954	2.999	30.4
2.662	1.535	.964	3.092	29.5
2.749	1.661	.979	3.231	30.6
2.803	1.695	.986	3.294	30.6
2.902	1.724	.993	3.394	30.2
3.005	1.732	.997	3.488	29.5
3.097	1.781	.996	3.592	29.5
3.238	1.877	.996	3.761	29.7
3.298	1.895	.996	3.823	29.5
3.441	1.978	.998	3.988	29.5
3.532	2.027	.998	4.092	29.5
3.672	2.124	.998	4.261	29.7
3.734	2.141	.998	4.323	29.5
3.876	2.225	1.000	4.488	29.5
3.968	2.273	1.000	4.592	29.5
4.106	2.372	1.000	4.761	29.7
4.169	2.387	1.000	4.823	29.5
4.311	2.471	.997	4.988	29.5
4.403	2.519	.997	5.092	29.5
4.541	2.620	.998	5.261	29.7
4.604	2.633	.997	5.323	29.5
4.746	2.717	.998	5.488	29.5
4.838	2.765	.997	5.592	29.5
4.975	2.867	.997	5.761	29.7
5.039	2.879	.997	5.823	29.5
5.181	2.964	.997	5.988	29.5
5.273	3.011	.997	6.092	29.5
5.410	3.115	.998	6.261	29.7
5.475	3.125	.998	6.323	29.5
-.048	.041	2.644	.001	37.7
.036	.106	2.649	.106	37.7
.111	.164	2.654	.201	37.7
.203	.236	2.669	.318	37.7
.283	.297	2.678	.419	37.7
.348	.347	2.694	.501	37.7
.431	.412	2.711	.606	37.7

TABLE 9.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
.506	.470	2.722	.701	37.7	4.388	3.475	.997	5.610	37.7
.599	.542	2.738	.818	37.7	4.449	3.522	.997	5.687	37.7
.678	.603	2.743	.919	37.7	4.585	3.605	.997	5.845	37.6
.743	.653	2.711	1.001	37.7	4.686	3.705	.997	5.987	37.7
.827	.718	2.647	1.106	37.7	4.783	3.781	.997	6.110	37.7
.902	.776	2.569	1.201	37.7	4.844	3.828	.997	6.187	37.7
.994	.848	2.417	1.318	37.7	4.981	3.910	.997	6.345	37.6
1.074	.909	2.309	1.419	37.7					
1.139	.959	1.917	1.501	37.7	-.071	.058	2.640	-.005	44.8
1.222	1.024	1.727	1.606	37.7	.024	.152	2.647	.128	44.8
1.297	1.082	1.591	1.701	37.7	.083	.211	2.657	.211	44.8
1.390	1.154	1.418	1.818	37.7	.142	.270	2.668	.294	44.8
1.469	1.215	1.327	1.919	37.7	.213	.340	2.681	.394	44.8
1.534	1.265	1.145	2.001	37.7	.284	.411	2.700	.495	44.8
1.618	1.330	1.075	2.106	37.7	.378	.504	2.724	.628	44.8
1.692	1.388	1.034	2.201	37.7	.437	.563	2.738	.711	44.8
1.785	1.460	.996	2.318	37.7	.497	.622	2.744	.794	44.8
1.865	1.521	.979	2.419	37.7	.568	.692	2.730	.894	44.8
1.929	1.571	.965	2.501	37.7	.639	.763	2.579	.995	44.8
2.013	1.636	.959	2.606	37.7	.733	.857	2.348	1.128	44.8
2.088	1.694	.958	2.701	37.7	.792	.916	2.188	1.211	44.8
2.180	1.766	.962	2.818	37.7	.851	.975	2.004	1.294	44.8
2.260	1.827	.963	2.919	37.7	.923	1.044	1.811	1.394	44.8
2.325	1.878	.974	3.001	37.7	.993	1.116	1.446	1.495	44.8
2.408	1.942	.980	3.106	37.7	1.088	1.209	1.258	1.628	44.8
2.483	2.000	.984	3.201	37.7	1.147	1.268	1.175	1.711	44.8
2.576	2.072	.992	3.318	37.7	1.206	1.327	1.102	1.794	44.8
2.655	2.133	.994	3.419	37.7	1.278	1.397	1.045	1.894	44.8
2.709	2.175	.993	3.487	37.7	1.348	1.468	.986	1.995	44.8
2.806	2.250	.996	3.610	37.7	1.442	1.562	.971	2.128	44.8
2.867	2.297	.996	3.687	37.7	1.501	1.621	.972	2.211	44.8
3.000	2.385	.996	3.845	37.6	1.561	1.680	.975	2.294	44.8
3.104	2.481	.998	3.987	37.7	1.633	1.749	.979	2.394	44.8
3.202	2.556	.998	4.110	37.7	1.703	1.821	.983	2.495	44.8
3.262	2.603	.997	4.187	37.7	1.797	1.914	.986	2.628	44.8
3.396	2.690	.998	4.345	37.6	1.856	1.973	.987	2.711	44.8
3.500	2.787	1.001	4.487	37.7	1.915	2.032	.990	2.794	44.8
3.597	2.862	.999	4.610	37.7	1.988	2.101	.990	2.894	44.8
3.658	2.909	.999	4.687	37.7	2.057	2.173	.996	2.995	44.8
3.792	2.995	1.000	4.845	37.6	2.151	2.267	.997	3.128	44.8
3.895	3.093	.997	4.987	37.7	2.211	2.326	.997	3.211	44.8
3.992	3.168	.996	5.110	37.7	2.270	2.384	.998	3.294	44.8
4.053	3.216	.997	5.187	37.7	2.342	2.453	.999	3.394	44.8
4.188	3.300	.997	5.345	37.6	2.406	2.520	.997	3.487	44.8
4.291	3.399	.998	5.487	37.7	2.483	2.596	.996	3.595	44.8

TABLE 9.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
2.555	2.668	.997	3.697	44.8
2.630	2.742	.997	3.802	44.8
2.761	2.872	.998	3.987	44.8
2.837	2.948	.998	4.095	44.8
2.910	3.021	.998	4.197	44.8
2.985	3.095	.998	4.302	44.8
3.116	3.225	1.000	4.487	44.8
3.192	3.301	1.000	4.595	44.8
3.265	3.373	1.000	4.697	44.8
3.339	3.447	1.000	4.802	44.8
3.470	3.577	.999	4.987	44.8
3.547	3.653	.999	5.095	44.8
3.619	3.726	.999	5.197	44.8
3.694	3.800	1.000	5.302	44.8
3.825	3.930	.997	5.487	44.8
3.901	4.006	.997	5.595	44.8
3.974	4.078	.997	5.697	44.8
4.049	4.152	.997	5.802	44.8
4.179	4.282	.999	5.987	44.8
4.256	4.358	.999	6.095	44.8
4.329	4.431	.999	6.197	44.8
4.403	4.505	1.000	6.302	44.8
-.116	.099	2.633	-.001	60.2
-.063	.191	2.640	.105	60.2
-.013	.278	2.652	.206	60.2
.043	.376	2.668	.318	60.2
.083	.446	2.679	.400	60.2
.133	.533	2.717	.499	60.2
.186	.624	2.733	.605	60.2
.235	.712	2.722	.706	60.2
.291	.809	2.610	.818	60.2
.332	.880	2.517	.900	60.2
.382	.966	2.035	.999	60.2
.434	1.058	1.755	1.105	60.2
.484	1.146	1.531	1.206	60.2
.540	1.243	1.281	1.318	60.2
.581	1.314	1.201	1.400	60.2
.630	1.400	1.021	1.499	60.2
.683	1.492	.980	1.605	60.2
.733	1.579	.965	1.706	60.2
.788	1.677	.963	1.818	60.2
.830	1.747	.965	1.900	60.2
.879	1.834	.975	1.999	60.2
.932	1.926	.983	2.105	60.2

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
.981	2.013	.989	2.206	60.2
1.037	2.111	.993	2.318	60.2
1.078	2.181	.996	2.400	60.2
1.128	2.268	.997	2.499	60.2
1.181	2.359	.997	2.605	60.2
1.230	2.447	.997	2.706	60.2
1.286	2.545	.997	2.818	60.2
1.327	2.615	.997	2.900	60.2
1.377	2.701	.999	2.999	60.2
1.429	2.793	1.000	3.105	60.2
1.478	2.881	.999	3.206	60.2
1.534	2.978	.999	3.318	60.2
1.576	3.049	.999	3.400	60.2
1.619	3.124	.997	3.487	60.2
1.686	3.241	.997	3.621	60.2
1.724	3.307	.997	3.697	60.2
1.798	3.404	.997	3.818	59.9
1.868	3.558	.998	3.987	60.2
1.935	3.675	.998	4.121	60.2
1.973	3.740	.998	4.197	60.2
2.048	3.836	.998	4.318	59.9
2.117	3.991	1.000	4.487	60.2
2.184	4.108	1.000	4.621	60.2
2.221	4.174	1.000	4.697	60.2
2.298	4.269	1.000	4.818	59.9
2.366	4.425	.999	4.987	60.2
2.433	4.542	.998	5.121	60.2
2.470	4.608	.999	5.197	60.2
2.549	4.702	.999	5.318	59.9
2.614	4.859	.997	5.487	60.2
2.681	4.976	.997	5.621	60.2
2.719	5.041	.997	5.697	60.2
2.799	5.135	.997	5.818	59.9
2.863	5.293	.999	5.987	60.2
2.930	5.410	.999	6.121	60.2
2.968	5.475	.999	6.197	60.2
3.050	5.567	.999	6.318	59.9
-.178	.104	2.633	-.019	75.8
-.151	.209	2.635	.089	75.7
-.125	.328	2.650	.210	76.2
-.104	.431	2.675	.316	76.6
-.077	.511	2.700	.400	75.9
-.055	.589	2.721	.481	75.8
-.028	.693	2.718	.589	75.7

TABLE 9.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
-.005	.813	2.629	.710	76.2	-.238	.121	2.633	-.009	92.0
.012	.917	2.365	.816	76.6	-.242	.232	2.635	.102	92.0
.045	.996	2.103	.900	75.9	-.246	.430	2.662	.300	91.7
.068	1.074	1.726	.981	75.8	-.242	.550	2.681	.420	91.0
.095	1.178	1.442	1.089	75.7	-.255	.621	2.725	.491	92.0
.114	1.299	1.230	1.210	76.2	-.259	.731	2.725	.602	92.0
.128	1.403	1.074	1.316	76.6	-.261	.930	2.489	.800	91.7
.166	1.481	1.010	1.400	75.9	-.251	1.050	2.242	.920	91.0
.191	1.558	.968	1.481	75.8	-.273	1.121	1.670	.991	92.0
.218	1.663	.962	1.589	75.7	-.276	1.231	1.460	1.102	92.0
.233	1.784	.968	1.710	76.2	-.277	1.430	1.110	1.300	91.7
.244	1.890	.977	1.816	76.6	-.260	1.550	1.027	1.420	91.0
.288	1.966	.982	1.900	75.9	-.291	1.620	.965	1.491	92.0
.314	2.043	.989	1.981	75.8	-.293	1.731	.965	1.602	92.0
.342	2.147	.992	2.089	75.7	-.292	1.929	.977	1.800	91.7
.353	2.270	.996	2.210	76.2	-.269	2.050	.987	1.920	91.0
.360	2.376	.996	2.316	76.6	-.308	2.120	.994	1.991	92.0
.410	2.451	.998	2.400	75.9	-.311	2.230	.997	2.102	92.0
.437	2.528	.997	2.481	75.8	-.307	2.429	.997	2.300	91.7
.465	2.632	.997	2.589	75.7	-.278	2.550	.997	2.420	91.0
.472	2.755	.997	2.710	76.2	-.326	2.620	.997	2.491	92.0
.475	2.863	.997	2.816	76.6	-.328	2.730	.998	2.602	92.0
.531	2.936	.997	2.900	75.9	-.322	2.929	.998	2.800	91.7
.516	3.050	.996	3.007	76.7	-.287	3.050	.998	2.920	91.0
.588	3.116	.999	3.089	75.7	-.344	3.119	.999	2.991	92.0
.591	3.241	.999	3.210	76.2	-.345	3.230	.999	3.102	92.0
.591	3.349	.999	3.316	76.6	-.341	3.325	.996	3.197	91.9
.653	3.421	.999	3.400	75.9	-.338	3.429	.998	3.300	91.7
.631	3.537	.998	3.507	76.7	-.295	3.549	.997	3.420	91.0
.729	3.730	.997	3.718	75.9	-.360	3.657	.997	3.529	92.0
.720	3.840	.996	3.823	76.4	-.366	3.740	.997	3.612	92.0
.746	4.023	.998	4.007	76.7	-.363	3.762	.996	3.634	92.0
.850	4.215	.998	4.218	75.9	-.357	3.825	.996	3.697	91.9
.837	4.326	.998	4.323	76.4	-.305	3.932	.998	3.803	91.1
.861	4.510	1.001	4.507	76.7	-.378	4.156	.997	4.029	92.0
.972	4.700	1.000	4.718	75.9	-.383	4.240	.998	4.112	92.0
.955	4.812	1.000	4.823	76.4	-.380	4.261	.998	4.134	92.0
.976	4.996	.999	5.007	76.7	-.373	4.325	.998	4.197	91.9
1.093	5.185	.998	5.218	75.9	-.314	4.432	.997	4.303	91.1
1.072	5.299	.999	5.323	76.4	-.395	4.656	.999	4.529	92.0
1.091	5.483	.997	5.507	76.7	-.401	4.739	1.000	4.612	92.0
1.214	5.670	.998	5.718	75.9	-.397	4.761	1.000	4.634	92.0
1.189	5.785	.997	5.823	76.4	-.390	4.824	1.000	4.697	91.9
1.207	5.969	1.000	6.007	76.7	-.324	4.932	1.002	4.803	91.1
1.336	6.155	.999	6.218	75.9	-.412	5.156	.999	5.029	92.0
1.306	6.271	.999	6.323	76.4	-.419	5.239	.997	5.112	92.0

TABLE 9.- Concluded

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
-.414	5.261	.999	5.134	92.0
-.406	5.324	.999	5.197	91.9
-.333	5.432	.998	5.303	91.1
-.430	5.655	.997	5.529	92.0
-.436	5.739	.998	5.612	92.0
-.431	5.761	.997	5.634	92.0
-.422	5.824	.997	5.697	91.9
-.342	5.932	.998	5.803	91.1
-.447	6.155	.999	6.029	92.0
-.454	6.238	.998	6.112	92.0
-.449	6.260	.999	6.134	92.0
-.438	6.324	1.000	6.197	91.9
-.351	6.432	.998	6.303	91.1

TABLE 10.- PITOT-PRESSURE MEASUREMENTS AT $x = 7.713$ in. FOR $M_\infty = 0.60$ WITH NPR = 3.98 AND $T_{t,j}/T_{t,\infty} = 0.90$

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
-.005	-.102	2.935	-.005	-.5	4.690	-.144	.998	4.691	-.5
.078	-.103	2.949	.078	-.5	4.796	-.149	.997	4.796	-.6
.183	-.104	2.968	.183	-.6	5.001	-.139	.998	5.001	-.4
.288	-.105	3.013	.289	-.6	5.085	-.127	.998	5.086	-.3
.394	-.106	3.030	.394	-.6	5.190	-.149	.999	5.191	-.5
.495	-.107	3.014	.495	-.5	5.296	-.153	.999	5.296	-.6
.578	-.108	3.027	.578	-.5	5.501	-.142	.999	5.501	-.4
.683	-.109	3.019	.683	-.6	5.585	-.130	.999	5.586	-.3
.788	-.110	3.012	.789	-.6	5.690	-.153	.999	5.691	-.5
.894	-.111	3.007	.894	-.6	5.796	-.158	.999	5.796	-.6
.995	-.111	2.988	.995	-.5					
1.077	-.112	2.994	1.078	-.5	-.027	-.073	2.942	-.026	7.7
1.183	-.114	2.984	1.183	-.6	.087	-.057	2.947	.090	7.7
1.288	-.115	2.976	1.289	-.6	.179	-.043	2.960	.183	8.0
1.394	-.116	2.967	1.394	-.6	.283	-.029	2.991	.288	7.9
1.495	-.116	2.954	1.495	-.5	.368	-.017	3.007	.373	7.9
1.577	-.117	2.955	1.578	-.5	.468	-.006	3.024	.474	7.7
1.683	-.118	2.919	1.683	-.6	.583	.010	3.021	.590	7.7
1.788	-.119	2.809	1.789	-.6	.675	.027	3.015	.683	8.0
1.894	-.121	2.562	1.894	-.6	.778	.040	3.009	.788	7.9
1.995	-.121	2.131	1.995	-.5	.863	.051	2.992	.873	7.9
2.077	-.122	1.918	2.078	-.5	.963	.062	2.994	.974	7.7
2.183	-.123	1.659	2.183	-.6	1.078	.077	2.991	1.090	7.7
2.288	-.124	1.437	2.289	-.6	1.170	.096	2.989	1.183	8.0
2.394	-.125	1.261	2.394	-.6	1.273	.108	2.985	1.288	7.9
2.495	-.125	1.109	2.495	-.5	1.358	.120	2.958	1.373	7.9
2.577	-.126	1.050	2.578	-.5	1.459	.129	2.974	1.474	7.7
2.683	-.128	1.002	2.683	-.6	1.574	.145	2.963	1.590	7.7
2.788	-.129	.981	2.789	-.6	1.665	.165	2.951	1.683	8.0
2.894	-.130	.979	2.894	-.6	1.769	.177	2.904	1.788	7.9
3.001	-.124	.985	3.001	-.4	1.853	.188	2.764	1.873	7.9
3.085	-.117	.991	3.086	-.3	1.954	.196	2.494	1.974	7.7
3.191	-.131	.995	3.191	-.5	2.069	.212	2.175	2.090	7.7
3.296	-.134	.998	3.296	-.6	2.160	.234	1.938	2.183	8.0
3.501	-.128	.997	3.501	-.4	2.264	.246	1.680	2.288	7.9
3.585	-.120	.996	3.586	-.3	2.349	.257	1.461	2.373	7.9
3.691	-.135	.997	3.691	-.5	2.450	.263	1.294	2.474	7.7
3.796	-.139	.997	3.796	-.6	2.564	.279	1.163	2.590	7.7
4.001	-.131	.994	4.001	-.4	2.655	.304	1.097	2.683	8.0
4.085	-.122	.994	4.086	-.3	2.759	.314	1.046	2.788	7.9
4.190	-.140	.995	4.191	-.5	2.844	.325	1.019	2.873	7.9
4.296	-.144	.995	4.296	-.6	2.972	.332	.996	3.001	7.7
4.501	-.135	.998	4.501	-.4	3.055	.351	.994	3.086	7.8
4.585	-.125	.998	4.586	-.3	3.158	.390	.995	3.193	8.2
					3.264	.372	.998	3.296	7.7

TABLE 10.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
3.468	.399	.997	3.501	7.7
3.550	.419	.997	3.586	7.8
3.653	.461	.997	3.693	8.2
3.760	.439	.997	3.796	7.7
3.963	.466	.994	4.001	7.7
4.045	.487	.994	4.086	7.8
4.148	.533	.995	4.193	8.2
4.255	.506	.995	4.296	7.7
4.459	.533	.998	4.501	7.7
4.541	.555	.997	4.586	7.8
4.643	.604	.998	4.693	8.2
4.751	.572	.998	4.796	7.7
4.954	.600	.999	5.001	7.7
5.036	.623	.999	5.086	7.8
5.138	.676	.999	5.193	8.2
5.246	.639	.999	5.296	7.7
5.450	.667	.999	5.501	7.7
5.531	.691	.999	5.586	7.8
5.632	.747	.999	5.693	8.2
5.742	.706	.999	5.796	7.7
-.017	-.039	2.930	-.009	16.0
.066	-.015	2.927	.078	16.0
.163	.012	2.934	.179	16.0
.269	.042	2.963	.289	16.0
.368	.071	2.992	.392	16.0
.464	.098	2.996	.491	16.0
.547	.122	2.996	.578	16.0
.644	.150	2.995	.679	16.0
.749	.180	2.992	.789	16.0
.849	.208	2.989	.892	16.0
.944	.236	2.967	.991	16.0
1.028	.259	2.958	1.078	16.0
1.125	.287	2.959	1.179	16.0
1.230	.317	2.953	1.289	16.0
1.330	.346	2.947	1.392	16.0
1.425	.373	2.920	1.491	16.0
1.509	.397	2.905	1.578	16.0
1.605	.425	2.901	1.679	16.0
1.711	.455	2.885	1.789	16.0
1.811	.483	2.867	1.892	16.0
1.906	.510	2.784	1.991	16.0
1.989	.534	2.702	2.078	16.0
2.086	.562	2.587	2.179	16.0
2.192	.592	2.375	2.289	16.0
2.291	.621	2.170	2.392	16.0
2.387	.648	1.889	2.491	16.0
2.470	.672	1.739	2.578	16.0
2.567	.699	1.600	2.679	16.0
2.672	.729	1.455	2.789	16.0
2.772	.758	1.359	2.892	16.0
2.877	.788	1.249	3.001	16.0
2.958	.809	1.200	3.086	15.9
3.064	.841	1.132	3.196	16.0
3.160	.869	1.081	3.296	16.0
3.358	.925	1.014	3.501	16.0
3.439	.946	1.005	3.586	15.9
3.545	.979	.998	3.696	16.0
3.641	1.006	.999	3.796	16.0
3.838	1.063	.995	4.001	16.0
3.920	1.083	.995	4.086	15.9
4.026	1.116	.994	4.196	16.0
4.122	1.144	.994	4.296	16.0
4.319	1.200	.997	4.501	16.0
4.401	1.220	.997	4.586	15.9
4.506	1.254	.996	4.696	16.0
4.602	1.281	.997	4.796	16.0
4.800	1.338	.998	5.001	16.0
4.882	1.357	.998	5.086	15.9
4.987	1.391	.998	5.196	16.0
5.083	1.418	.998	5.296	16.0
5.281	1.475	.999	5.501	16.0
5.363	1.494	.999	5.586	15.9
5.468	1.528	.998	5.696	16.0
5.564	1.556	.998	5.796	16.0
-.044	-.005	2.944	-.021	27.1
.042	.040	2.933	.076	27.2
.125	.082	2.944	.169	27.2
.236	.140	2.949	.294	27.2
.312	.176	2.955	.378	27.0
.401	.223	2.959	.479	27.1
.486	.268	2.953	.576	27.2
.569	.311	2.945	.669	27.2
.680	.368	2.909	.794	27.2
.757	.403	2.889	.878	27.0
.846	.452	2.812	.979	27.1
.931	.497	2.745	1.076	27.2
1.014	.540	2.679	1.169	27.2
1.125	.597	2.565	1.294	27.2

TABLE 10.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
1.203	.630	2.524	1.378	27.0	-.036	.021	2.958	-.001	31.8
1.291	.680	2.392	1.479	27.1	.023	.056	2.946	.068	31.7
1.376	.726	2.282	1.576	27.2	.125	.121	2.941	.189	31.9
1.459	.768	2.183	1.669	27.2	.197	.166	2.937	.273	31.9
1.570	.826	2.031	1.794	27.2	.284	.221	2.934	.376	31.9
1.648	.857	1.967	1.878	27.0	.389	.284	2.931	.499	31.8
1.736	.908	1.871	1.979	27.1	.449	.319	2.921	.568	31.7
1.820	.954	1.754	2.076	27.2	.550	.385	2.887	.689	31.9
1.903	.997	1.653	2.169	27.2	.622	.431	2.830	.773	31.9
2.014	1.054	1.509	2.294	27.2	.709	.485	2.762	.876	31.9
2.094	1.084	1.438	2.378	27.0	.814	.548	2.610	.999	31.8
2.181	1.136	1.289	2.479	27.1	.874	.582	2.518	1.068	31.7
2.265	1.183	1.202	2.576	27.2	.974	.650	2.375	1.189	31.9
2.348	1.226	1.133	2.669	27.2	1.046	.695	2.240	1.273	31.9
2.459	1.283	1.069	2.794	27.2	1.133	.749	2.115	1.376	31.9
2.539	1.311	1.044	2.878	27.0	1.239	.812	1.954	1.499	31.8
2.626	1.364	1.011	2.979	27.1	1.299	.845	1.850	1.568	31.7
2.710	1.412	1.001	3.076	27.2	1.399	.914	1.717	1.689	31.9
2.793	1.454	.996	3.169	27.2	1.470	.960	1.602	1.773	31.9
2.904	1.512	.996	3.294	27.2	1.557	1.014	1.511	1.876	31.9
2.985	1.538	.997	3.378	27.0	1.664	1.075	1.433	1.999	31.8
3.076	1.598	.998	3.486	27.2	1.725	1.108	1.362	2.068	31.7
3.151	1.635	.997	3.570	27.2	1.823	1.178	1.273	2.189	31.9
3.260	1.653	.997	3.676	26.7	1.894	1.224	1.196	2.273	31.9
3.366	1.723	.997	3.801	26.9	1.981	1.278	1.134	2.376	31.9
3.521	1.826	.998	3.986	27.2	2.088	1.339	1.060	2.499	31.8
3.596	1.863	.998	4.070	27.2	2.150	1.371	1.025	2.568	31.7
3.707	1.877	.998	4.176	26.7	2.248	1.442	.991	2.689	31.9
3.811	1.949	.998	4.301	26.9	2.319	1.489	.974	2.773	31.9
3.966	2.054	.999	4.486	27.2	2.406	1.543	.970	2.876	31.9
4.041	2.091	.999	4.570	27.2	2.513	1.603	.972	2.999	31.8
4.154	2.101	.999	4.676	26.7	2.587	1.656	.979	3.089	31.9
4.257	2.175	.999	4.801	26.9	2.672	1.706	.985	3.189	31.9
4.410	2.283	.998	4.986	27.2	2.743	1.753	.990	3.273	31.9
4.485	2.319	.998	5.070	27.2	2.830	1.807	.994	3.376	31.9
4.601	2.326	.998	5.176	26.7	2.917	1.862	.997	3.478	31.9
4.703	2.401	.998	5.301	26.9	3.011	1.920	.997	3.589	31.9
4.855	2.511	1.000	5.486	27.2	3.102	1.977	.997	3.696	31.9
4.930	2.548	1.000	5.570	27.2	3.168	2.018	.997	3.774	31.9
5.048	2.550	1.000	5.676	26.7	3.341	2.126	.998	3.978	31.9
5.149	2.627	1.000	5.801	26.9	3.435	2.185	.998	4.089	31.9
5.300	2.739	.999	5.986	27.2	3.526	2.241	.999	4.196	31.9
5.375	2.776	.999	6.070	27.2	3.592	2.283	.999	4.274	31.9
5.494	2.774	.998	6.176	26.7	3.766	2.391	.999	4.478	31.9
5.595	2.853	.999	6.301	26.9	3.859	2.449	.999	4.589	31.9

TABLE 10.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
3.950	2.506	.999	4.696	31.9
4.017	2.547	.998	4.774	31.9
4.190	2.655	.998	4.978	31.9
4.284	2.714	.998	5.089	31.9
4.375	2.770	.998	5.196	31.9
4.441	2.812	.998	5.274	31.9
4.614	2.920	1.000	5.478	31.9
4.708	2.978	1.000	5.589	31.9
4.799	3.035	1.000	5.696	31.9
4.865	3.076	1.000	5.774	31.9
5.039	3.184	1.000	5.978	31.9
5.132	3.243	.999	6.089	31.9
5.223	3.299	.999	6.196	31.9
5.290	3.341	.998	6.274	31.9
-.069	.031	2.958	-.022	39.0
-.012	.096	2.936	.081	39.0
.095	.164	2.931	.189	39.0
.161	.217	2.928	.273	39.0
.243	.283	2.916	.379	39.0
.320	.346	2.899	.478	39.0
.400	.410	2.866	.581	39.0
.484	.478	2.801	.689	39.0
.549	.531	2.705	.773	39.0
.631	.598	2.572	.879	39.0
.708	.660	2.367	.978	39.0
.788	.725	2.201	1.081	39.0
.872	.793	2.025	1.189	39.0
.938	.846	1.868	1.273	39.0
1.020	.913	1.722	1.379	39.0
1.097	.975	1.565	1.478	39.0
1.177	1.040	1.456	1.581	39.0
1.261	1.108	1.354	1.689	39.0
1.326	1.161	1.271	1.773	39.0
1.408	1.227	1.196	1.879	39.0
1.485	1.290	1.142	1.978	39.0
1.565	1.355	1.093	2.081	39.0
1.649	1.423	1.050	2.189	39.0
1.715	1.476	1.020	2.273	39.0
1.797	1.542	.999	2.379	39.0
1.874	1.605	.987	2.478	39.0
1.954	1.670	.982	2.581	39.0
2.038	1.737	.980	2.689	39.0
2.103	1.790	.981	2.773	39.0
2.185	1.857	.983	2.879	39.0

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
2.306	1.876	.979	2.985	37.9
2.383	1.949	.984	3.091	38.1
2.454	1.995	.988	3.175	38.0
2.538	2.059	.991	3.280	37.9
2.574	2.172	.997	3.379	39.0
2.700	2.184	.998	3.485	37.9
2.777	2.257	.997	3.591	38.1
2.849	2.302	.997	3.675	38.0
2.932	2.366	.997	3.780	37.9
3.095	2.491	.999	3.985	37.9
3.170	2.566	.999	4.091	38.1
3.243	2.610	.999	4.175	38.0
3.327	2.673	.999	4.280	37.9
3.489	2.798	1.000	4.485	37.9
3.564	2.874	.999	4.591	38.1
3.637	2.918	.999	4.675	38.0
3.721	2.981	.999	4.780	37.9
3.884	3.106	.998	4.985	37.9
3.957	3.183	.998	5.091	38.1
4.031	3.225	.998	5.175	38.0
4.115	3.288	.998	5.280	37.9
4.278	3.413	1.000	5.485	37.9
4.351	3.491	1.000	5.591	38.1
4.425	3.533	1.000	5.675	38.0
4.509	3.596	1.000	5.780	37.9
4.672	3.720	.999	5.985	37.9
4.744	3.800	.999	6.091	38.1
4.820	3.840	.999	6.175	38.0
4.904	3.903	.999	6.280	37.9
-.085	.051	2.955	-.020	46.1
-.012	.127	2.935	.085	46.1
.048	.188	2.924	.170	46.1
.120	.263	2.914	.274	46.1
.191	.338	2.902	.377	46.1
.262	.411	2.853	.480	46.1
.335	.487	2.798	.585	46.1
.394	.549	2.734	.670	46.1
.466	.623	2.582	.774	46.1
.538	.698	2.448	.877	46.1
.609	.772	2.106	.980	46.1
.682	.847	1.940	1.085	46.1
.741	.909	1.817	1.170	46.1
.813	.984	1.631	1.274	46.1
.885	1.058	1.519	1.377	46.1

TABLE 10.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
.956	1.132	1.319	1.480	46.1	-.130	.084	2.961	-.020	61.4
1.028	1.208	1.238	1.585	46.1	-.081	.174	2.939	.081	61.4
1.088	1.269	1.184	1.670	46.1	-.031	.265	2.922	.185	61.4
1.160	1.344	1.111	1.774	46.1	.011	.342	2.895	.273	61.4
1.231	1.418	1.071	1.877	46.1	.061	.434	2.837	.379	61.4
1.302	1.492	1.019	1.980	46.1	.110	.523	2.742	.480	61.4
1.375	1.568	1.002	2.085	46.1	.158	.613	2.617	.581	61.4
1.434	1.629	.992	2.170	46.1	.208	.704	2.433	.685	61.4
1.506	1.704	.987	2.274	46.1	.250	.781	2.204	.773	61.4
1.578	1.779	.987	2.377	46.1	.300	.874	1.979	.879	61.4
1.649	1.852	.990	2.480	46.1	.350	.962	1.716	.980	61.4
1.722	1.928	.993	2.585	46.1	.397	1.052	1.567	1.081	61.4
1.781	1.990	.993	2.670	46.1	.447	1.143	1.413	1.185	61.4
1.853	2.064	.996	2.774	46.1	.489	1.220	1.280	1.273	61.4
1.925	2.139	.997	2.877	46.1	.539	1.313	1.178	1.379	61.4
1.996	2.213	.997	2.980	46.1	.589	1.401	1.082	1.480	61.4
2.069	2.288	.998	3.085	46.1	.636	1.491	1.038	1.581	61.4
2.128	2.350	.998	3.170	46.1	.686	1.582	1.006	1.685	61.4
2.202	2.431	.998	3.280	46.1	.728	1.660	.988	1.773	61.4
2.271	2.499	.998	3.377	46.1	.778	1.752	.985	1.879	61.4
2.344	2.577	.997	3.484	46.1	.829	1.839	.984	1.980	61.4
2.418	2.655	.997	3.591	46.1	.875	1.930	.988	2.081	61.4
2.475	2.716	.997	3.675	46.2	.925	2.021	.992	2.185	61.4
2.549	2.791	.997	3.780	46.1	.967	2.099	.995	2.273	61.4
2.691	2.937	.998	3.984	46.1	1.017	2.191	.998	2.379	61.4
2.764	3.015	.999	4.091	46.1	1.069	2.278	1.000	2.480	61.4
2.822	3.077	.999	4.175	46.2	1.114	2.369	1.000	2.581	61.4
2.895	3.152	.999	4.280	46.1	1.164	2.461	1.000	2.685	61.4
3.038	3.297	.999	4.484	46.1	1.206	2.538	1.000	2.773	61.4
3.111	3.376	.999	4.591	46.1	1.256	2.630	1.000	2.879	61.4
3.168	3.437	.999	4.675	46.2	1.308	2.717	.999	2.980	61.4
3.242	3.512	.999	4.780	46.1	1.353	2.809	.998	3.081	61.4
3.384	3.658	.998	4.984	46.1	1.403	2.900	.999	3.185	61.4
3.457	3.736	.998	5.091	46.1	1.445	2.977	.998	3.273	61.4
3.514	3.798	.998	5.175	46.2	1.495	3.069	.998	3.379	61.4
3.588	3.873	.998	5.280	46.1	1.546	3.163	.997	3.485	61.4
3.731	4.018	1.000	5.484	46.1	1.590	3.236	.997	3.570	61.4
3.804	4.097	1.000	5.591	46.1	1.667	3.313	.997	3.675	60.9
3.861	4.159	1.000	5.675	46.2	1.731	3.398	.997	3.780	60.7
3.935	4.233	1.000	5.780	46.1	1.785	3.602	.999	3.985	61.4
4.077	4.379	1.000	5.984	46.1	1.829	3.675	.998	4.070	61.4
4.150	4.457	.999	6.091	46.1	1.910	3.750	.998	4.175	60.9
4.207	4.519	.999	6.175	46.2	1.976	3.834	.999	4.280	60.7
4.281	4.594	.999	6.280	46.1	2.024	4.041	.999	4.485	61.4
					2.069	4.114	.999	4.570	61.4

TABLE 10.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
2.152	4.188	.999	4.675	60.9
2.220	4.270	.999	4.780	60.7
2.263	4.480	.998	4.985	61.4
2.308	4.552	.998	5.070	61.4
2.395	4.625	.998	5.175	60.9
2.465	4.706	.998	5.280	60.7
2.502	4.920	1.000	5.485	61.4
2.548	4.991	.999	5.570	61.4
2.638	5.062	1.000	5.675	60.9
2.709	5.142	1.000	5.780	60.7
2.741	5.359	.999	5.985	61.4
2.787	5.430	.999	6.070	61.4
2.881	5.499	.999	6.175	60.9
2.954	5.578	.999	6.280	60.7
-.182	.101	2.973	-.024	76.5
-.156	.205	2.951	.083	76.4
-.129	.301	2.928	.183	75.9
-.106	.390	2.893	.275	75.7
-.079	.488	2.837	.377	75.6
-.065	.587	2.710	.476	76.5
-.038	.691	2.511	.583	76.4
-.007	.786	2.315	.683	75.9
.018	.874	2.060	.775	75.7
.045	.973	1.851	.877	75.6
.052	1.073	1.586	.976	76.5
.079	1.176	1.409	1.083	76.4
.114	1.271	1.295	1.183	75.9
.141	1.359	1.182	1.275	75.7
.169	1.457	1.107	1.377	75.6
.168	1.559	1.029	1.476	76.5
.197	1.662	.999	1.583	76.4
.236	1.756	.988	1.683	75.9
.264	1.844	.985	1.775	75.7
.293	1.941	.988	1.877	75.6
.285	2.045	.991	1.976	76.5
.315	2.148	.995	2.083	76.4
.358	2.241	.997	2.183	75.9
.387	2.328	.998	2.275	75.7
.418	2.426	.998	2.377	75.6
.402	2.532	1.000	2.476	76.5
.433	2.634	1.000	2.583	76.4
.480	2.726	1.000	2.683	75.9
.510	2.813	1.000	2.775	75.7
.542	2.910	1.000	2.877	75.6

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
.518	3.018	.999	2.976	76.5
.551	3.120	.999	3.083	76.4
.602	3.210	.998	3.183	75.9
.587	3.314	.998	3.280	76.5
.666	3.394	.999	3.377	75.6
.694	3.499	.997	3.486	75.6
.715	3.580	.997	3.569	75.6
.666	3.702	.997	3.676	76.7
.703	3.800	.997	3.780	76.5
.818	3.983	.998	3.986	75.6
.839	4.064	.999	4.069	75.6
.780	4.189	.999	4.176	76.7
.820	4.286	.998	4.280	76.5
.943	4.468	.999	4.486	75.6
.964	4.548	.999	4.569	75.6
.895	4.676	.999	4.676	76.7
.936	4.773	.999	4.780	76.5
1.067	4.952	.998	4.986	75.6
1.088	5.033	.998	5.069	75.6
1.010	5.162	.998	5.176	76.7
1.053	5.259	.998	5.280	76.5
1.191	5.436	1.000	5.486	75.6
1.212	5.517	1.000	5.569	75.6
1.124	5.649	1.000	5.676	76.7
1.169	5.745	1.000	5.780	76.5
1.316	5.920	.999	5.986	75.6
1.337	6.001	.999	6.069	75.6
1.239	6.136	.998	6.176	76.7
1.285	6.231	.998	6.280	76.5
-.233	.099	2.977	-.031	90.9
-.235	.211	2.960	.081	90.9
-.237	.319	2.936	.189	90.9
-.238	.403	2.904	.273	90.9
-.240	.508	2.845	.378	90.9
-.241	.599	2.709	.469	90.9
-.243	.711	2.521	.581	90.9
-.245	.818	2.261	.689	90.9
-.246	.903	2.043	.773	90.9
-.248	1.008	1.819	.878	90.9
-.250	1.099	1.561	.969	90.9
-.252	1.211	1.398	1.081	90.9
-.253	1.318	1.252	1.189	90.9
-.255	1.403	1.162	1.273	90.9
-.256	1.508	1.091	1.378	90.9

TABLE 10.- Concluded

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
-.258	1.599	1.020	1.469	90.9
-.260	1.711	.994	1.581	90.9
-.262	1.818	.985	1.689	90.9
-.263	1.902	.985	1.773	90.9
-.265	2.008	.992	1.878	90.9
-.266	2.099	.995	1.969	90.9
-.268	2.211	.998	2.081	90.9
-.270	2.318	.998	2.189	90.9
-.271	2.402	.998	2.273	90.9
-.273	2.508	.998	2.378	90.9
-.274	2.599	1.000	2.469	90.9
-.276	2.711	1.000	2.581	90.9
-.278	2.818	1.000	2.689	90.9
-.279	2.902	1.000	2.773	90.9
-.281	3.007	1.000	2.878	90.9
-.283	3.099	.999	2.969	90.9
-.284	3.211	.999	3.081	90.9
-.286	3.318	.998	3.189	90.9
-.288	3.402	.998	3.273	90.9
-.289	3.507	.997	3.378	90.9
-.291	3.596	.997	3.467	90.9
-.293	3.712	.997	3.582	90.9
-.294	3.806	.997	3.676	90.9
-.296	3.924	.997	3.795	90.9
-.299	4.096	.999	3.967	90.9
-.301	4.212	.998	4.082	90.9
-.302	4.306	.998	4.176	90.9
-.304	4.424	.999	4.295	90.9
-.307	4.596	.999	4.467	90.9
-.309	4.712	.999	4.582	90.9
-.311	4.806	.999	4.676	90.9
-.313	4.924	.999	4.795	90.9
-.315	5.096	.998	4.967	90.9
-.317	5.212	.998	5.082	90.9
-.319	5.306	.998	5.176	90.9
-.321	5.424	.998	5.295	90.9
-.324	5.596	1.000	5.467	90.9
-.325	5.712	1.000	5.582	90.9
-.327	5.806	1.000	5.676	90.9
-.329	5.924	1.000	5.795	90.9
-.332	6.096	.999	5.967	90.9
-.334	6.211	.999	6.082	90.9
-.335	6.305	.999	6.176	90.9
-.337	6.424	.997	6.295	90.9

TABLE 11.- PITOT-PRESSURE MEASUREMENTS AT $x = 10.235$ in. FOR $M_\infty = 0.60$ WITH NPR = 4.03 AND $T_{t,j}/T_{t,\infty} = 0.96$

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
.007	-.102	2.681	.007	-.5	4.623	-.150	.996	4.623	-.6
.108	-.103	2.694	.108	-.6	4.706	-.151	.997	4.706	-.6
.201	-.104	2.700	.201	-.6	4.813	-.152	.998	4.813	-.6
.305	-.106	2.707	.305	-.6	5.018	-.154	.999	5.018	-.6
.410	-.107	2.713	.410	-.6	5.123	-.155	.998	5.123	-.6
.507	-.106	2.699	.507	-.5	5.206	-.156	.998	5.206	-.6
.608	-.109	2.715	.608	-.6	5.313	-.157	.998	5.313	-.6
.701	-.110	2.724	.701	-.6	5.518	-.159	.998	5.518	-.6
.805	-.111	2.736	.805	-.6	5.623	-.160	.998	5.623	-.6
.910	-.112	2.747	.910	-.6	5.706	-.161	.997	5.706	-.6
1.007	-.111	2.747	1.007	-.5	5.813	-.162	.998	5.813	-.6
1.108	-.114	2.768	1.108	-.6	6.017	-.164	.999	6.018	-.6
1.201	-.115	2.784	1.201	-.6	6.123	-.165	.999	6.123	-.6
1.305	-.116	2.799	1.305	-.6	6.206	-.166	.998	6.206	-.6
1.410	-.117	2.813	1.410	-.6					
1.507	-.115	2.807	1.507	-.5	.008	-.068	2.764	.011	7.6
1.608	-.119	2.790	1.608	-.6	.113	-.054	2.765	.116	7.6
1.701	-.120	2.688	1.701	-.6	.217	-.040	2.766	.221	7.7
1.805	-.121	2.508	1.805	-.6	.300	-.029	2.762	.305	7.7
1.910	-.122	2.261	1.910	-.6	.404	-.015	2.768	.410	7.7
2.007	-.119	1.908	2.007	-.5	.504	-.002	2.781	.511	7.6
2.108	-.124	1.699	2.108	-.6	.609	.012	2.784	.616	7.6
2.201	-.125	1.496	2.201	-.6	.712	.027	2.789	.721	7.7
2.305	-.126	1.354	2.305	-.6	.796	.038	2.788	.805	7.7
2.410	-.127	1.231	2.410	-.6	.900	.052	2.798	.910	7.7
2.507	-.124	1.111	2.507	-.5	1.000	.064	2.821	1.011	7.6
2.608	-.129	1.054	2.608	-.6	1.104	.078	2.828	1.116	7.6
2.701	-.130	1.013	2.701	-.6	1.208	.094	2.836	1.221	7.7
2.805	-.131	.997	2.805	-.6	1.291	.105	2.838	1.305	7.7
2.910	-.132	.992	2.910	-.6	1.395	.119	2.849	1.410	7.7
3.007	-.128	.995	3.007	-.5	1.495	.131	2.867	1.511	7.6
3.108	-.134	.996	3.108	-.6	1.600	.145	2.854	1.616	7.6
3.201	-.135	.998	3.201	-.6	1.703	.160	2.795	1.721	7.7
3.305	-.136	.999	3.305	-.6	1.787	.172	2.707	1.805	7.7
3.410	-.137	.999	3.410	-.6	1.891	.186	2.516	1.910	7.7
3.518	-.139	.999	3.518	-.6	1.991	.197	2.181	2.011	7.6
3.623	-.140	.998	3.623	-.6	2.096	.211	1.916	2.116	7.6
3.706	-.141	.998	3.706	-.6	2.199	.227	1.720	2.221	7.7
3.813	-.142	.998	3.813	-.6	2.282	.238	1.579	2.305	7.7
4.018	-.144	.996	4.018	-.6	2.386	.252	1.416	2.410	7.7
4.123	-.145	.996	4.123	-.6	2.486	.263	1.266	2.511	7.6
4.206	-.146	.997	4.206	-.6	2.591	.277	1.178	2.616	7.6
4.313	-.147	.995	4.313	-.6	2.694	.294	1.147	2.721	7.7
4.518	-.149	.997	4.518	-.6	2.778	.305	1.114	2.805	7.7
					2.882	.319	1.080	2.910	7.7
					2.970	.346	1.052	3.001	7.9

TABLE 11.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
3.069	.365	1.035	3.102	8.0	1.544	.406	2.822	1.615	15.9
3.185	.378	1.019	3.218	8.0	1.626	.429	2.817	1.700	15.9
3.273	.372	1.013	3.305	7.7	1.742	.463	2.779	1.821	15.9
3.378	.386	1.004	3.410	7.7	1.828	.487	2.719	1.910	15.9
3.465	.415	1.000	3.501	7.9	1.925	.515	2.559	2.011	15.9
3.564	.435	.999	3.602	8.0	2.025	.544	2.400	2.115	15.9
3.680	.447	.998	3.718	8.0	2.107	.565	2.225	2.200	15.9
3.772	.476	.998	3.814	8.2	2.223	.600	2.026	2.321	15.9
3.960	.484	.995	4.001	7.9	2.309	.625	1.883	2.410	15.9
4.060	.504	.995	4.102	8.0	2.406	.652	1.719	2.511	15.9
4.175	.516	.996	4.218	8.0	2.506	.681	1.602	2.615	15.9
4.267	.547	.996	4.314	8.2	2.588	.702	1.499	2.700	15.9
4.456	.553	.995	4.501	7.9	2.704	.737	1.403	2.821	15.9
4.555	.574	.995	4.602	8.0	2.789	.762	1.339	2.910	15.9
4.671	.586	.995	4.718	8.0	2.887	.790	1.266	3.011	15.9
4.762	.618	.996	4.814	8.2	2.987	.818	1.208	3.115	15.9
4.951	.622	.998	5.001	7.9	3.069	.839	1.156	3.200	15.9
5.050	.644	.998	5.102	8.0	3.184	.875	1.102	3.321	15.9
5.166	.655	.998	5.218	8.0	3.270	.899	1.067	3.410	15.9
5.257	.689	.998	5.314	8.2	3.374	.929	1.045	3.518	15.9
5.446	.691	.998	5.501	7.9	3.476	.958	1.019	3.624	15.9
5.545	.714	.998	5.602	8.0	3.564	.983	1.007	3.716	15.9
5.661	.724	.998	5.718	8.0	3.657	1.010	1.000	3.812	15.9
5.752	.761	.998	5.814	8.2	3.855	1.066	.996	4.018	15.9
5.941	.759	.998	6.001	7.9	3.957	1.095	.996	4.124	15.9
6.040	.784	.998	6.102	8.0	4.045	1.120	.996	4.216	15.9
6.156	.794	.998	6.218	8.0	4.138	1.147	.996	4.312	15.9
6.247	.832	.998	6.314	8.2	4.335	1.203	.997	4.518	15.9
					4.438	1.232	.998	4.624	15.9
.002	-.034	2.768	.011	15.9	4.526	1.258	.998	4.716	15.9
.102	-.005	2.775	.115	15.9	4.619	1.284	.997	4.812	15.9
.183	.018	2.781	.200	15.9	4.816	1.340	.999	5.018	15.9
.300	.051	2.786	.321	15.9	4.919	1.370	.998	5.124	15.9
.386	.076	2.791	.410	15.9	5.006	1.395	.999	5.216	15.9
.483	.103	2.787	.511	15.9	5.099	1.421	.999	5.312	15.9
.583	.132	2.796	.615	15.9	5.297	1.478	.998	5.518	15.9
.664	.155	2.802	.700	15.9	5.399	1.507	.998	5.624	15.9
.780	.188	2.809	.821	15.9	5.487	1.532	.999	5.716	15.9
.866	.213	2.815	.910	15.9	5.580	1.559	.998	5.812	15.9
.963	.241	2.814	1.011	15.9	5.778	1.615	1.000	6.018	15.9
1.063	.269	2.821	1.115	15.9	5.880	1.644	.998	6.124	15.9
1.145	.292	2.828	1.200	15.9	5.968	1.669	.999	6.216	15.9
1.261	.326	2.831	1.321	15.9	6.061	1.696	.999	6.312	15.9
1.347	.350	2.835	1.410	15.9					
1.444	.378	2.821	1.511	15.9	-.013	.003	2.695	.011	25.4

TABLE 11.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
.078	.046	2.694	.110	25.4	4.507	2.160	.998	5.018	25.5
.177	.093	2.701	.221	25.4	4.576	2.210	.998	5.102	25.7
.255	.130	2.706	.307	25.4	4.640	2.326	.999	5.211	26.5
.349	.175	2.713	.411	25.4	4.742	2.349	.999	5.312	26.2
.439	.217	2.723	.511	25.4	4.958	2.375	.998	5.518	25.5
.529	.260	2.723	.610	25.4	5.026	2.426	.998	5.602	25.7
.629	.307	2.721	.721	25.4	5.088	2.549	.997	5.711	26.5
.707	.344	2.717	.807	25.4	5.190	2.570	.998	5.812	26.2
.801	.389	2.715	.911	25.4	5.410	2.590	.998	6.018	25.5
.891	.432	2.675	1.011	25.4	5.477	2.643	1.000	6.102	25.7
.981	.474	2.651	1.110	25.4	5.535	2.772	1.000	6.211	26.5
1.081	.522	2.603	1.221	25.4	5.639	2.791	1.000	6.312	26.2
1.159	.559	2.564	1.307	25.4					
1.252	.603	2.530	1.411	25.4	-.018	.016	2.692	.011	28.7
1.343	.646	2.395	1.511	25.4	.075	.063	2.701	.116	28.1
1.433	.689	2.327	1.610	25.4	.167	.114	2.705	.221	28.3
1.533	.736	2.229	1.721	25.4	.335	.202	2.720	.411	28.1
1.610	.773	2.146	1.807	25.4	.420	.256	2.720	.511	28.7
1.704	.817	2.072	1.911	25.4	.516	.299	2.723	.616	28.1
1.794	.860	1.951	2.011	25.4	.607	.351	2.717	.721	28.3
1.885	.903	1.859	2.110	25.4	.776	.437	2.699	.911	28.1
1.984	.950	1.738	2.221	25.4	.859	.496	2.629	1.011	28.7
2.062	.987	1.632	2.307	25.4	.957	.534	2.593	1.116	28.1
2.156	1.032	1.533	2.411	25.4	1.048	.588	2.529	1.221	28.3
2.246	1.074	1.368	2.511	25.4	1.217	.673	2.414	1.411	28.1
2.336	1.117	1.297	2.610	25.4	1.297	.736	2.234	1.511	28.7
2.436	1.164	1.218	2.721	25.4	1.398	.770	2.164	1.616	28.1
2.514	1.201	1.163	2.807	25.4	1.488	.824	2.054	1.721	28.3
2.608	1.246	1.119	2.911	25.4	1.658	.908	1.884	1.911	28.1
2.698	1.289	1.062	3.011	25.4	1.736	.976	1.746	2.011	28.7
2.788	1.331	1.046	3.110	25.4	1.839	1.006	1.670	2.116	28.1
2.888	1.379	1.030	3.221	25.4	1.928	1.061	1.560	2.221	28.3
2.966	1.416	1.024	3.307	25.4	2.099	1.144	1.393	2.411	28.1
3.060	1.460	1.012	3.411	25.4	2.175	1.216	1.252	2.511	28.7
3.224	1.560	1.011	3.602	25.7	2.280	1.241	1.189	2.616	28.1
3.298	1.657	1.004	3.711	26.5	2.368	1.298	1.122	2.721	28.3
3.396	1.686	1.000	3.812	26.2	2.540	1.379	1.054	2.911	28.1
3.605	1.729	.995	4.018	25.5	2.613	1.456	1.014	3.011	28.7
3.674	1.776	.996	4.102	25.7	2.721	1.477	1.006	3.116	28.1
3.745	1.880	.996	4.211	26.5	2.809	1.535	1.000	3.221	28.3
3.845	1.907	.996	4.312	26.2	2.982	1.615	1.000	3.411	28.1
4.056	1.944	.997	4.518	25.5	3.161	1.729	1.000	3.622	28.3
4.125	1.993	.997	4.602	25.7	3.233	1.774	.999	3.708	28.4
4.193	2.103	.997	4.711	26.5	3.322	1.840	.998	3.817	28.6
4.293	2.128	.996	4.812	26.2	3.502	1.929	.996	4.018	28.5
					3.601	1.966	.995	4.122	28.3

TABLE 11.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
3.673	2.012	.995	4.208	28.4
3.761	2.079	.996	4.317	28.6
3.941	2.167	.996	4.518	28.5
4.041	2.203	.996	4.622	28.3
4.113	2.250	.996	4.708	28.4
4.200	2.319	.996	4.817	28.6
4.381	2.406	.998	5.018	28.5
4.481	2.441	.999	5.122	28.3
4.553	2.488	.998	5.208	28.4
4.639	2.559	.999	5.317	28.6
4.820	2.645	.998	5.518	28.5
4.921	2.678	.999	5.622	28.3
4.992	2.726	.998	5.708	28.4
5.078	2.798	.998	5.817	28.6
5.259	2.884	.999	6.018	28.5
5.361	2.916	.999	6.122	28.3
5.432	2.963	.999	6.208	28.4
5.517	3.038	.999	6.317	28.6
-.027	.023	2.659	.007	31.3
.059	.075	2.664	.108	31.3
.137	.123	2.673	.199	31.3
.226	.176	2.683	.303	31.2
.320	.227	2.690	.410	30.7
.400	.283	2.688	.507	31.3
.486	.335	2.686	.608	31.3
.564	.382	2.684	.699	31.3
.653	.435	2.675	.803	31.2
.750	.482	2.660	.910	30.7
.827	.542	2.566	1.007	31.3
.913	.594	2.508	1.108	31.3
.991	.642	2.454	1.199	31.3
1.081	.695	2.387	1.303	31.2
1.180	.737	2.316	1.410	30.7
1.255	.802	2.101	1.507	31.3
1.341	.854	2.003	1.608	31.3
1.419	.901	1.922	1.699	31.3
1.509	.954	1.837	1.803	31.2
1.610	.993	1.757	1.910	30.7
1.682	1.061	1.609	2.007	31.3
1.768	1.114	1.524	2.108	31.3
1.846	1.161	1.457	2.199	31.3
1.936	1.213	1.385	2.303	31.2
2.040	1.248	1.312	2.410	30.7
2.110	1.321	1.178	2.507	31.3
2.195	1.373	1.123	2.608	31.3
2.274	1.421	1.082	2.699	31.3
2.364	1.472	1.046	2.803	31.2
2.470	1.503	1.019	2.910	30.7
2.537	1.581	.994	3.007	31.3
2.623	1.633	.992	3.108	31.3
2.701	1.680	.990	3.199	31.3
2.791	1.731	.993	3.303	31.2
2.900	1.759	.997	3.410	30.7
3.013	1.779	.999	3.518	30.1
3.117	1.839	.997	3.638	30.1
3.176	1.874	.997	3.707	30.1
3.272	1.933	.997	3.819	30.1
3.445	2.030	.996	4.018	30.1
3.549	2.090	.996	4.138	30.1
3.609	2.125	.995	4.207	30.1
3.705	2.184	.996	4.319	30.1
3.878	2.281	.996	4.518	30.1
3.982	2.341	.996	4.638	30.1
4.042	2.375	.996	4.707	30.1
4.137	2.435	.997	4.819	30.1
4.310	2.531	.998	5.018	30.1
4.415	2.592	.998	5.138	30.1
4.474	2.626	.998	5.207	30.1
4.570	2.686	.999	5.319	30.1
4.743	2.782	.998	5.518	30.1
4.847	2.842	.997	5.638	30.1
4.907	2.877	.999	5.707	30.1
5.002	2.937	.998	5.819	30.1
5.176	3.033	.999	6.018	30.1
5.280	3.093	.999	6.138	30.1
5.339	3.128	.999	6.207	30.1
5.435	3.188	1.000	6.319	30.1
-.043	.048	2.657	.009	38.3
.030	.106	2.666	.101	38.4
.107	.167	2.675	.200	38.4
.189	.232	2.684	.305	38.4
.276	.300	2.690	.415	38.3
.349	.358	2.680	.509	38.3
.422	.416	2.673	.601	38.4
.499	.477	2.658	.700	38.4
.582	.542	2.623	.805	38.4
.669	.610	2.571	.915	38.3
.742	.668	2.431	1.009	38.3

TABLE 11.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
.814	.726	2.343	1.101	38.4	4.735	3.829	.999	6.102	38.4
.891	.787	2.248	1.200	38.4	4.825	3.900	.999	6.216	38.4
.974	.852	2.117	1.305	38.4	4.902	3.956	1.000	6.312	38.3
1.061	.920	1.996	1.415	38.3					
1.134	.978	1.791	1.509	38.3	-.064	.075	2.691	.012	46.5
1.206	1.036	1.690	1.601	38.4	.010	.149	2.700	.116	46.0
1.283	1.097	1.603	1.700	38.4	.082	.226	2.707	.221	46.2
1.366	1.163	1.498	1.805	38.4	.140	.277	2.711	.298	45.5
1.454	1.230	1.414	1.915	38.3	.220	.357	2.714	.411	45.4
1.526	1.288	1.316	2.009	38.3	.281	.438	2.700	.512	46.5
1.598	1.347	1.258	2.101	38.4	.358	.508	2.684	.616	46.0
1.675	1.408	1.203	2.200	38.4	.428	.587	2.643	.721	46.2
1.758	1.473	1.144	2.305	38.4	.490	.634	2.601	.798	45.5
1.846	1.539	1.097	2.415	38.3	.571	.713	2.518	.911	45.4
1.919	1.598	1.039	2.509	38.3	.625	.801	2.299	1.012	46.5
1.990	1.657	1.017	2.601	38.4	.705	.868	2.194	1.116	46.0
2.068	1.718	1.002	2.700	38.4	.773	.948	2.053	1.221	46.2
2.150	1.783	.990	2.805	38.4	.841	.991	1.948	1.298	45.5
2.238	1.849	.988	2.915	38.3	.922	1.069	1.799	1.411	45.4
2.318	1.914	.984	3.018	38.3	.969	1.164	1.564	1.512	46.5
2.383	1.968	.986	3.102	38.4	1.052	1.227	1.476	1.616	46.0
2.472	2.038	.987	3.216	38.4	1.119	1.309	1.378	1.721	46.2
2.549	2.096	.991	3.312	38.3	1.191	1.347	1.312	1.798	45.5
2.631	2.159	.998	3.415	38.3	1.273	1.426	1.231	1.911	45.4
2.711	2.224	.996	3.518	38.3	1.313	1.526	1.139	2.012	46.5
2.775	2.278	.998	3.602	38.4	1.400	1.587	1.101	2.116	46.0
2.864	2.348	.997	3.716	38.4	1.465	1.670	1.063	2.221	46.2
2.941	2.406	.998	3.812	38.3	1.541	1.704	1.041	2.298	45.5
3.103	2.534	.995	4.018	38.3	1.624	1.782	1.018	2.411	45.4
3.167	2.588	.996	4.102	38.4	1.657	1.889	1.000	2.512	46.5
3.256	2.659	.997	4.216	38.4	1.747	1.947	.998	2.616	46.0
3.333	2.716	.996	4.312	38.3	1.811	2.031	.996	2.721	46.2
3.495	2.844	.996	4.518	38.3	1.892	2.061	.995	2.798	45.5
3.559	2.898	.997	4.602	38.4	1.974	2.138	.996	2.911	45.4
3.648	2.969	.997	4.716	38.4	2.058	2.223	.995	3.031	45.4
3.726	3.026	.997	4.812	38.3	2.123	2.289	.996	3.123	45.4
3.887	3.154	.999	5.018	38.3	2.183	2.350	.996	3.208	45.4
3.951	3.209	.998	5.102	38.4	2.254	2.424	.998	3.312	45.5
4.040	3.279	.998	5.216	38.4	2.325	2.494	.999	3.411	45.4
4.118	3.336	.999	5.312	38.3	2.409	2.579	.997	3.531	45.4
4.280	3.464	.999	5.518	38.3	2.474	2.645	.996	3.623	45.4
4.343	3.519	.998	5.602	38.4	2.534	2.706	.998	3.708	45.4
4.433	3.589	.997	5.716	38.4	2.605	2.780	.998	3.812	45.5
4.510	3.646	.998	5.812	38.3	2.760	2.936	.995	4.031	45.4
4.672	3.774	.999	6.018	38.3	2.825	3.001	.995	4.123	45.4

TABLE 11.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
2.885	3.062	.995	4.208	45.4
2.956	3.137	.996	4.312	45.5
3.111	3.292	.995	4.531	45.4
3.175	3.357	.996	4.623	45.4
3.235	3.418	.997	4.708	45.4
3.307	3.493	.998	4.812	45.5
3.462	3.648	.998	5.031	45.4
3.526	3.714	.997	5.123	45.4
3.586	3.775	.999	5.208	45.4
3.657	3.849	.997	5.312	45.5
3.813	4.004	.998	5.531	45.4
3.877	4.070	.997	5.623	45.4
3.937	4.131	.999	5.708	45.4
4.008	4.206	.998	5.812	45.5
4.163	4.361	.999	6.031	45.4
4.228	4.426	.999	6.123	45.4
4.288	4.487	.999	6.208	45.4
4.359	4.562	.998	6.312	45.5
-.114	.112	2.686	.012	61.4
-.064	.203	2.702	.115	61.3
-.012	.291	2.710	.218	60.8
.034	.373	2.718	.312	60.9
.071	.465	2.714	.410	62.0
.125	.551	2.669	.512	61.4
.176	.641	2.629	.615	61.3
.233	.727	2.558	.718	60.8
.277	.810	2.451	.812	60.9
.306	.906	2.326	.910	62.0
.364	.990	2.055	1.012	61.4
.416	1.080	1.917	1.115	61.3
.477	1.163	1.773	1.218	60.8
.520	1.247	1.626	1.312	60.9
.541	1.348	1.501	1.410	62.0
.604	1.429	1.307	1.512	61.4
.656	1.518	1.227	1.615	61.3
.721	1.600	1.158	1.718	60.8
.764	1.683	1.096	1.812	60.9
.776	1.789	1.052	1.910	62.0
.843	1.868	1.013	2.012	61.4
.896	1.957	1.003	2.115	61.3
.965	2.036	.998	2.218	60.8
1.007	2.120	.997	2.312	60.9
1.011	2.230	.999	2.410	62.0
1.082	2.307	.998	2.512	61.4

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
1.137	2.395	.998	2.615	61.3
1.209	2.472	.998	2.718	60.8
1.251	2.557	.999	2.812	60.9
1.246	2.671	.999	2.910	62.0
1.356	2.734	.997	3.018	60.8
1.407	2.826	.997	3.123	60.8
1.451	2.901	.998	3.210	60.7
1.500	2.985	.997	3.306	60.7
1.481	3.113	.999	3.410	62.0
1.600	3.171	.999	3.518	60.8
1.651	3.263	.998	3.623	60.8
1.696	3.337	.998	3.710	60.7
1.744	3.421	.998	3.806	60.7
1.844	3.607	.995	4.018	60.8
1.895	3.699	.995	4.123	60.8
1.940	3.773	.995	4.210	60.7
1.989	3.857	.995	4.306	60.7
2.088	4.044	.996	4.518	60.8
2.139	4.135	.996	4.623	60.8
2.184	4.209	.998	4.710	60.7
2.233	4.293	.995	4.806	60.7
2.332	4.480	.999	5.018	60.8
2.383	4.572	.999	5.123	60.8
2.429	4.646	.997	5.210	60.7
2.478	4.729	.998	5.306	60.7
2.576	4.916	.999	5.518	60.8
2.628	5.008	.999	5.623	60.8
2.673	5.082	.998	5.710	60.7
2.722	5.165	.998	5.806	60.7
2.820	5.353	.999	6.018	60.8
2.872	5.444	.999	6.123	60.8
2.918	5.518	.997	6.210	60.7
2.967	5.601	.998	6.306	60.7
-.172	.134	2.693	.011	76.2
-.150	.222	2.704	.102	76.1
-.124	.327	2.712	.210	76.1
-.102	.419	2.716	.305	76.1
-.076	.521	2.704	.410	76.1
-.053	.619	2.652	.511	76.2
-.030	.708	2.589	.602	76.1
-.004	.813	2.478	.710	76.1
.018	.905	2.342	.805	76.1
.044	1.007	2.164	.910	76.1
.067	1.104	1.897	1.011	76.2

TABLE 11.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
.090	1.193	1.762	1.102	76.1	1.295	6.072	.999	6.128	76.1
.116	1.298	1.612	1.210	76.1	1.317	6.159	1.000	6.217	76.1
.138	1.390	1.481	1.305	76.1	1.333	6.234	1.000	6.294	76.1
.164	1.492	1.349	1.410	76.1					
.187	1.590	1.196	1.511	76.2	-.231	.142	2.695	.012	90.3
.210	1.678	1.134	1.602	76.1	-.232	.244	2.706	.114	90.3
.236	1.784	1.077	1.710	76.1	-.241	.330	2.717	.200	91.5
.258	1.875	1.039	1.805	76.1	-.243	.426	2.719	.296	91.5
.283	1.978	1.009	1.910	76.1	-.233	.539	2.706	.409	90.3
.306	2.075	.999	2.011	76.2	-.234	.642	2.641	.512	90.3
.329	2.164	.997	2.102	76.1	-.234	.744	2.565	.614	90.3
.356	2.269	.998	2.210	76.1	-.254	.829	2.459	.700	91.5
.378	2.361	.999	2.305	76.1	-.256	.925	2.302	.796	91.5
.403	2.463	.998	2.410	76.1	-.236	1.039	2.122	.909	90.3
.426	2.561	.999	2.511	76.2	-.236	1.142	1.846	1.012	90.3
.449	2.649	.999	2.602	76.1	-.237	1.244	1.700	1.114	90.3
.475	2.754	.998	2.710	76.1	-.266	1.329	1.566	1.200	91.5
.498	2.846	.999	2.805	76.1	-.269	1.425	1.430	1.296	91.5
.523	2.948	.998	2.910	76.1	-.238	1.539	1.306	1.409	90.3
.550	3.054	.997	3.019	76.1	-.238	1.642	1.155	1.512	90.3
.576	3.159	.997	3.128	76.1	-.239	1.744	1.099	1.614	90.3
.597	3.246	.997	3.217	76.1	-.279	1.829	1.055	1.700	91.5
.614	3.321	.997	3.294	76.1	-.282	1.925	1.023	1.796	91.5
.643	3.434	.998	3.410	76.1	-.240	2.039	1.003	1.909	90.3
.670	3.540	.997	3.519	76.1	-.241	2.142	.998	2.012	90.3
.696	3.645	.996	3.628	76.1	-.241	2.244	.998	2.114	90.3
.717	3.732	.997	3.717	76.1	-.292	2.329	.999	2.200	91.5
.734	3.807	.997	3.794	76.1	-.294	2.425	.999	2.296	91.5
.789	4.025	.996	4.019	76.1	-.243	2.539	.998	2.409	90.3
.816	4.130	.996	4.128	76.1	-.243	2.642	.999	2.512	90.3
.837	4.217	.996	4.217	76.1	-.244	2.744	.999	2.614	90.3
.854	4.292	.996	4.294	76.1	-.305	2.829	.999	2.700	91.5
.909	4.510	.997	4.519	76.1	-.307	2.925	.999	2.796	91.5
.935	4.616	.996	4.628	76.1	-.245	3.039	.998	2.909	90.3
.957	4.702	.997	4.717	76.1	-.237	3.127	.996	2.997	90.1
.974	4.777	.997	4.794	76.1	-.212	3.232	.998	3.102	89.7
1.029	4.996	.998	5.019	76.1	-.245	3.338	.998	3.208	90.2
1.055	5.101	.998	5.128	76.1	-.247	3.442	.998	3.312	90.3
1.077	5.188	.999	5.217	76.1	-.248	3.539	.999	3.409	90.3
1.094	5.263	.997	5.294	76.1	-.239	3.627	.998	3.497	90.1
1.149	5.481	.997	5.519	76.1	-.209	3.732	.998	3.602	89.7
1.175	5.586	.998	5.628	76.1	-.247	3.838	.998	3.708	90.2
1.197	5.673	.999	5.717	76.1	-.250	3.942	.998	3.812	90.3
1.213	5.748	.997	5.794	76.1	-.240	4.127	.995	3.997	90.1
1.269	5.967	1.000	6.019	76.1	-.206	4.232	.995	4.102	89.7

TABLE 11.- Concluded

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
-.249	4.338	.995	4.208	90.2
-.252	4.442	.995	4.312	90.3
-.241	4.627	.996	4.497	90.1
-.204	4.732	.997	4.602	89.7
-.251	4.838	.995	4.708	90.2
-.255	4.942	.998	4.812	90.3
-.242	5.127	.999	4.997	90.1
-.201	5.232	.998	5.102	89.7
-.253	5.338	.998	5.208	90.2
-.257	5.442	.998	5.312	90.3
-.243	5.627	.999	5.497	90.1
-.198	5.732	.998	5.602	89.7
-.255	5.838	.998	5.708	90.2
-.259	5.942	.998	5.812	90.3
-.244	6.127	.999	5.997	90.1
-.196	6.232	.998	6.102	89.7
-.257	6.338	.998	6.208	90.2
-.262	6.442	.998	6.312	90.3

TABLE 12.- PITOT-PRESSURE MEASUREMENTS AT x = 0.0 in. FOR $M_\infty = 1.20$ WITH NPR = 4.00 AND $T_{t,j}/T_{t,\infty} = 0.87$

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
-.019	-.067	1.449	-.016	8.9	4.667	.470	.942	4.700	6.6
.116	-.060	1.449	.118	6.6	4.772	.482	.944	4.806	6.6
.189	-.051	1.452	.192	6.6	4.957	.504	.948	4.992	6.6
.294	-.039	1.451	.297	6.6	5.060	.516	.948	5.096	6.6
.401	-.027	1.437	.405	6.6	5.164	.528	.949	5.200	6.6
.475	.010	1.448	.484	8.9	5.269	.540	.949	5.306	6.6
.613	-.002	1.446	.618	6.6	5.453	.562	.949	5.492	6.6
.686	.007	1.447	.692	6.6	5.557	.574	.952	5.596	6.6
.790	.019	1.445	.797	6.6	5.660	.586	.952	5.700	6.6
.897	.031	1.432	.905	6.6	5.765	.598	.953	5.806	6.6
.969	.087	1.454	.984	8.9	5.950	.619	.955	5.992	6.6
1.109	.056	1.454	1.118	6.6	6.054	.631	.957	6.096	6.6
1.182	.064	1.457	1.192	6.6	6.157	.643	.958	6.200	6.6
1.287	.077	1.457	1.297	6.6	6.262	.656	.958	6.306	6.6
1.394	.089	1.446	1.405	6.6					
1.463	.164	1.461	1.484	8.9	-.005	-.035	1.435	.005	16.1
1.606	.114	1.459	1.618	6.6	.098	-.006	1.439	.111	16.1
1.679	.122	1.462	1.692	6.6	.177	.017	1.439	.194	16.1
1.783	.134	1.461	1.797	6.6	.279	.047	1.439	.300	16.1
1.891	.147	1.450	1.905	6.6	.379	.076	1.441	.404	16.1
1.957	.241	1.463	1.984	8.9	.476	.104	1.437	.505	16.1
2.103	.172	1.454	2.118	6.6	.578	.133	1.437	.611	16.1
2.176	.180	1.452	2.192	6.6	.658	.156	1.435	.694	16.1
2.280	.192	1.368	2.297	6.6	.759	.186	1.435	.800	16.1
2.387	.205	.811	2.405	6.6	.860	.215	1.435	.904	16.1
2.451	.319	.534	2.484	8.9	.956	.243	1.441	1.005	16.1
2.599	.229	.600	2.618	6.6	1.059	.271	1.445	1.111	16.1
2.672	.238	.648	2.692	6.6	1.138	.294	1.448	1.194	16.1
2.777	.250	.729	2.797	6.6	1.240	.324	1.452	1.300	16.1
2.884	.262	.787	2.905	6.6	1.340	.354	1.460	1.404	16.1
2.945	.396	.835	2.984	8.9	1.436	.382	1.473	1.505	16.1
3.074	.285	.882	3.096	6.6	1.539	.410	1.478	1.611	16.1
3.177	.297	.915	3.200	6.6	1.619	.433	1.479	1.694	16.1
3.282	.309	.938	3.306	6.6	1.720	.463	1.481	1.800	16.1
3.467	.330	.949	3.492	6.6	1.820	.493	1.482	1.904	16.1
3.571	.342	.945	3.596	6.6	1.917	.521	1.481	2.005	16.1
3.674	.354	.942	3.700	6.6	2.019	.548	1.476	2.111	16.1
3.779	.367	.942	3.806	6.6	2.099	.571	1.469	2.194	16.1
3.963	.388	.942	3.992	6.6	2.200	.601	1.436	2.300	16.1
4.067	.400	.941	4.096	6.6	2.300	.632	1.312	2.404	16.1
4.170	.412	.940	4.200	6.6	2.397	.660	1.030	2.505	16.1
4.275	.424	.941	4.306	6.6	2.500	.687	.575	2.611	16.1
4.460	.446	.941	4.492	6.6	2.579	.710	.597	2.694	16.1
4.564	.458	.940	4.596	6.6	2.681	.740	.671	2.800	16.1
					2.781	.771	.738	2.904	16.1

TABLE 12.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
2.877	.799	.798	3.005	16.1	1.360	.593	1.486	1.505	23.5
2.980	.825	.868	3.111	16.1	1.454	.640	1.488	1.609	23.7
3.060	.848	.903	3.194	16.1	1.533	.670	1.489	1.694	23.6
3.161	.879	.936	3.300	16.1	1.626	.715	1.487	1.797	23.7
3.261	.910	.957	3.404	16.1	1.729	.744	1.486	1.904	23.3
3.366	.937	.955	3.512	16.1	1.819	.793	1.485	2.005	23.5
3.547	1.009	.954	3.707	16.4	1.912	.841	1.483	2.109	23.7
3.620	1.042	.953	3.785	16.5	1.991	.871	1.481	2.194	23.6
3.644	1.033	.953	3.806	16.3	2.084	.916	1.478	2.297	23.7
3.846	1.075	.952	4.012	16.1	2.189	.942	1.470	2.404	23.3
4.027	1.149	.951	4.207	16.4	2.277	.993	1.431	2.505	23.5
4.099	1.184	.950	4.285	16.5	2.369	1.042	.981	2.609	23.7
4.124	1.173	.949	4.306	16.3	2.449	1.071	.653	2.694	23.6
4.327	1.213	.947	4.512	16.1	2.541	1.117	.544	2.797	23.7
4.507	1.290	.946	4.707	16.4	2.648	1.140	.627	2.904	23.3
4.578	1.326	.945	4.785	16.5	2.735	1.192	.743	3.005	23.5
4.604	1.314	.945	4.806	16.3	2.827	1.243	.799	3.109	23.7
4.807	1.352	.948	5.012	16.1	2.907	1.271	.840	3.194	23.6
4.987	1.431	.951	5.207	16.4	2.999	1.319	.888	3.297	23.7
5.058	1.469	.954	5.285	16.5	3.107	1.338	.929	3.404	23.3
5.084	1.454	.953	5.306	16.3	3.174	1.394	.956	3.487	23.7
5.287	1.490	.952	5.512	16.1	3.280	1.423	.963	3.596	23.5
5.466	1.572	.954	5.707	16.4	3.375	1.468	.963	3.701	23.5
5.537	1.611	.955	5.785	16.5	3.476	1.501	.960	3.806	23.4
5.564	1.594	.955	5.806	16.3	3.632	1.595	.963	3.987	23.7
5.768	1.629	.957	6.012	16.1	3.739	1.622	.959	4.096	23.5
5.946	1.713	.958	6.207	16.4	3.833	1.668	.959	4.201	23.5
6.016	1.753	.959	6.285	16.5	3.935	1.699	.959	4.306	23.4
6.044	1.735	.959	6.306	16.3	4.089	1.796	.958	4.487	23.7
					4.197	1.821	.955	4.596	23.5
-.015	-.006	1.436	.005	23.5	4.292	1.867	.954	4.701	23.5
.080	.036	1.437	.109	23.7	4.394	1.897	.952	4.806	23.4
.158	.070	1.439	.194	23.6	4.547	1.997	.956	4.987	23.7
.253	.112	1.440	.297	23.7	4.656	2.020	.953	5.096	23.5
.352	.151	1.442	.404	23.3	4.750	2.067	.953	5.201	23.5
.443	.193	1.437	.505	23.5	4.853	2.096	.953	5.306	23.4
.538	.237	1.437	.609	23.7	5.005	2.198	.953	5.487	23.7
.617	.270	1.438	.694	23.6	5.115	2.219	.954	5.596	23.5
.710	.313	1.442	.797	23.7	5.209	2.266	.955	5.701	23.5
.811	.349	1.451	.904	23.3	5.312	2.294	.956	5.806	23.4
.902	.393	1.473	1.005	23.5	5.463	2.399	.958	5.987	23.7
.996	.439	1.479	1.109	23.7	5.573	2.418	.958	6.096	23.5
1.075	.470	1.484	1.194	23.6	5.667	2.466	.959	6.201	23.5
1.168	.514	1.484	1.297	23.7	5.771	2.492	.960	6.306	23.4
1.270	.546	1.485	1.404	23.3					

TABLE 12.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
-.034	.031	1.434	.005	33.8	3.869	2.642	.965	4.701	33.8
.053	.090	1.434	.111	33.8	3.955	2.702	.962	4.806	33.8
.138	.146	1.436	.213	33.8	4.111	2.804	.964	4.992	33.8
.213	.196	1.439	.303	33.8	4.197	2.862	.963	5.096	33.8
.297	.252	1.446	.404	33.8	4.284	2.920	.963	5.201	33.8
.381	.309	1.451	.505	33.8	4.371	2.980	.959	5.306	33.8
.469	.368	1.470	.611	33.8	4.526	3.082	.955	5.492	33.8
.554	.424	1.482	.713	33.8	4.612	3.140	.956	5.596	33.8
.629	.474	1.491	.803	33.8	4.700	3.198	.955	5.701	33.8
.712	.530	1.489	.904	33.8	4.786	3.258	.956	5.806	33.8
.797	.587	1.493	1.005	33.8	4.942	3.360	.956	5.992	33.8
.885	.646	1.492	1.111	33.8	5.028	3.418	.957	6.096	33.8
.969	.702	1.491	1.213	33.8	5.115	3.476	.958	6.201	33.8
1.044	.752	1.490	1.303	33.8	5.202	3.536	.957	6.306	33.8
1.128	.808	1.488	1.404	33.8					
1.212	.865	1.482	1.505	33.8	-.063	.022	1.441	-.023	36.1
1.300	.924	1.477	1.611	33.8	.048	.095	1.440	.110	35.0
1.385	.980	1.464	1.713	33.8	.204	.203	1.446	.299	35.0
1.460	1.030	1.434	1.803	33.8	.290	.263	1.447	.404	35.0
1.543	1.086	1.320	1.904	33.8	.341	.317	1.462	.477	36.1
1.628	1.143	1.099	2.005	33.8	.458	.382	1.488	.610	35.0
1.716	1.202	.665	2.111	33.8	.613	.490	1.497	.799	35.0
1.800	1.258	.465	2.213	33.8	.700	.550	1.495	.904	35.0
1.875	1.308	.403	2.303	33.8	.745	.612	1.501	.977	36.1
1.959	1.364	.431	2.404	33.8	.867	.668	1.496	1.110	35.0
2.043	1.421	.471	2.505	33.8	1.023	.776	1.494	1.299	35.0
2.131	1.480	.566	2.611	33.8	1.109	.836	1.491	1.404	35.0
2.216	1.536	.632	2.713	33.8	1.148	.907	1.487	1.477	36.1
2.291	1.586	.632	2.803	33.8	1.277	.955	1.478	1.610	35.0
2.374	1.642	.549	2.904	33.8	1.433	1.063	1.432	1.799	35.0
2.459	1.699	.509	3.005	33.8	1.519	1.123	1.288	1.904	35.0
2.547	1.758	.558	3.111	33.8	1.552	1.202	.853	1.977	36.1
2.632	1.814	.651	3.213	33.8	1.687	1.242	.415	2.110	35.0
2.706	1.864	.768	3.303	33.8	1.843	1.349	.402	2.299	35.0
2.790	1.920	.846	3.404	33.8	1.929	1.409	.442	2.404	35.0
2.864	1.970	.915	3.492	33.8	1.956	1.497	.503	2.477	36.1
2.950	2.027	.943	3.596	33.8	2.096	1.529	.638	2.610	35.0
3.038	2.086	.962	3.701	33.8	2.252	1.636	.592	2.799	35.0
3.124	2.146	.966	3.806	33.8	2.339	1.696	.488	2.904	35.0
3.279	2.248	.968	3.992	33.8	2.360	1.791	.505	2.977	36.1
3.366	2.306	.968	4.096	33.8	2.428	1.756	.552	3.012	34.9
3.453	2.364	.966	4.201	33.8	2.473	1.874	.662	3.117	36.1
3.540	2.424	.966	4.306	33.8	2.541	1.924	.752	3.201	36.1
3.695	2.526	.965	4.492	33.8	2.626	1.986	.834	3.306	36.1
3.781	2.584	.964	4.596	33.8	2.748	1.983	.883	3.404	35.0

TABLE 12.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
2.838	2.042	.932	3.512	34.9
2.877	2.169	.952	3.617	36.1
2.945	2.219	.963	3.701	36.1
3.030	2.281	.967	3.806	36.1
3.248	2.329	.966	4.012	34.9
3.281	2.464	.967	4.117	36.1
3.349	2.514	.966	4.201	36.1
3.433	2.576	.966	4.306	36.1
3.658	2.615	.965	4.512	34.9
3.684	2.759	.966	4.617	36.1
3.752	2.808	.963	4.701	36.1
3.837	2.870	.962	4.806	36.1
4.068	2.901	.963	5.012	34.9
4.088	3.054	.964	5.117	36.1
4.156	3.103	.963	5.201	36.1
4.241	3.165	.960	5.306	36.1
4.478	3.187	.956	5.512	34.9
4.492	3.349	.955	5.617	36.1
4.560	3.398	.953	5.701	36.1
4.645	3.460	.953	5.806	36.1
4.888	3.474	.957	6.012	34.9
4.896	3.644	.956	6.117	36.1
4.964	3.693	.956	6.201	36.1
5.049	3.755	.957	6.306	36.1
-.046	.046	1.440	.005	38.5
.040	.115	1.439	.115	38.5
.118	.177	1.441	.215	38.5
.184	.229	1.446	.299	38.5
.266	.295	1.455	.404	38.5
.345	.357	1.475	.505	38.5
.431	.426	1.494	.615	38.5
.509	.488	1.499	.715	38.5
.575	.541	1.499	.799	38.5
.658	.606	1.498	.904	38.5
.736	.669	1.500	1.005	38.5
.823	.737	1.495	1.115	38.5
.901	.800	1.492	1.215	38.5
.967	.852	1.490	1.299	38.5
1.049	.917	1.486	1.404	38.5
1.127	.980	1.457	1.505	38.5
1.214	1.049	1.316	1.615	38.5
1.292	1.111	.989	1.715	38.5
1.358	1.163	.472	1.799	38.5
1.440	1.229	.390	1.904	38.5

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
1.519	1.291	.385	2.005	38.5
1.605	1.360	.397	2.115	38.5
1.683	1.422	.414	2.215	38.5
1.749	1.474	.457	2.299	38.5
1.831	1.540	.521	2.404	38.5
1.910	1.602	.583	2.505	38.5
1.996	1.671	.689	2.615	38.5
2.075	1.733	.731	2.715	38.5
2.140	1.786	.735	2.799	38.5
2.223	1.851	.706	2.904	38.5
2.297	1.933	.683	3.013	38.8
2.358	2.022	.757	3.117	39.4
2.419	2.081	.799	3.201	39.5
2.532	2.097	.838	3.299	38.5
2.614	2.162	.875	3.404	38.5
2.687	2.246	.917	3.513	38.8
2.745	2.339	.946	3.617	39.4
2.805	2.399	.957	3.701	39.5
2.886	2.467	.967	3.807	39.5
3.076	2.560	.970	4.013	38.8
3.132	2.656	.968	4.117	39.4
3.191	2.716	.966	4.201	39.5
3.272	2.785	.966	4.307	39.5
3.466	2.873	.966	4.513	38.8
3.518	2.973	.966	4.617	39.4
3.577	3.034	.966	4.701	39.5
3.658	3.103	.965	4.807	39.5
3.855	3.187	.967	5.013	38.8
3.905	3.290	.967	5.117	39.4
3.963	3.352	.964	5.201	39.5
4.044	3.421	.963	5.307	39.5
4.245	3.500	.957	5.513	38.8
4.292	3.608	.955	5.617	39.4
4.349	3.670	.953	5.701	39.5
4.430	3.738	.953	5.807	39.5
4.635	3.813	.954	6.013	38.8
4.678	3.925	.954	6.117	39.4
4.735	3.987	.954	6.201	39.5
4.816	4.056	.954	6.307	39.5
-.069	.071	1.439	.005	46.8
.002	.147	1.439	.109	46.7
.065	.214	1.442	.200	46.8
.130	.283	1.453	.296	46.7
.202	.359	1.483	.401	46.7

TABLE 12.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
.273	.435	1.494	.505	46.8	3.584	3.928	.967	5.317	46.6
.345	.511	1.498	.609	46.7	3.738	4.079	.959	5.533	46.5
.407	.578	1.499	.700	46.8	3.785	4.139	.957	5.609	46.6
.473	.647	1.499	.796	46.7	3.848	4.207	.953	5.701	46.6
.545	.723	1.496	.901	46.7	3.928	4.291	.950	5.817	46.6
.616	.799	1.496	1.005	46.8	4.082	4.442	.950	6.033	46.5
.688	.875	1.489	1.109	46.7	4.128	4.502	.951	6.109	46.6
.750	.942	1.473	1.200	46.8	4.192	4.570	.951	6.201	46.6
.816	1.011	1.411	1.296	46.7	4.272	4.654	.951	6.317	46.6
.888	1.087	1.085	1.401	46.7					
.958	1.164	.408	1.505	46.8	-.092	.093	1.439	.007	54.3
1.031	1.239	.376	1.609	46.7	-.030	.178	1.441	.112	54.2
1.092	1.306	.378	1.700	46.8	.029	.261	1.450	.214	54.3
1.159	1.375	.380	1.796	46.7	.076	.331	1.475	.298	54.6
1.231	1.451	.390	1.901	46.7	.136	.418	1.496	.404	54.7
1.301	1.528	.406	2.005	46.8	.200	.499	1.495	.507	54.3
1.373	1.603	.441	2.109	46.7	.263	.583	1.499	.612	54.2
1.435	1.671	.490	2.200	46.8	.321	.667	1.500	.714	54.3
1.501	1.739	.546	2.296	46.7	.366	.738	1.496	.798	54.6
1.573	1.816	.634	2.401	46.7	.425	.826	1.491	.904	54.7
1.643	1.892	.681	2.505	46.8	.492	.905	1.477	1.007	54.3
1.716	1.967	.743	2.609	46.7	.555	.989	1.361	1.112	54.2
1.777	2.035	.781	2.700	46.8	.612	1.073	.851	1.214	54.3
1.844	2.103	.806	2.796	46.7	.656	1.146	.452	1.298	54.6
1.916	2.180	.836	2.901	46.7	.714	1.234	.374	1.404	54.7
1.986	2.256	.865	3.005	46.8	.784	1.311	.374	1.507	54.3
2.059	2.331	.884	3.109	46.7	.847	1.395	.375	1.612	54.2
2.120	2.399	.904	3.200	46.8	.904	1.479	.379	1.714	54.3
2.187	2.467	.918	3.296	46.7	.946	1.553	.386	1.798	54.6
2.259	2.544	.938	3.401	46.7	1.003	1.642	.415	1.904	54.7
2.361	2.629	.943	3.533	46.5	1.076	1.717	.443	2.007	54.3
2.409	2.687	.957	3.609	46.6	1.140	1.800	.497	2.112	54.2
2.473	2.755	.966	3.701	46.6	1.196	1.886	.560	2.214	54.3
2.553	2.839	.970	3.817	46.6	1.235	1.960	.620	2.298	54.6
2.705	2.992	.970	4.033	46.5	1.292	2.050	.714	2.404	54.7
2.753	3.050	.971	4.109	46.6	1.368	2.122	.755	2.507	54.3
2.817	3.118	.970	4.201	46.6	1.432	2.206	.807	2.612	54.2
2.896	3.202	.970	4.317	46.6	1.487	2.292	.847	2.714	54.3
3.050	3.354	.969	4.533	46.5	1.525	2.368	.874	2.798	54.6
3.097	3.413	.969	4.609	46.6	1.581	2.458	.911	2.904	54.7
3.161	3.481	.969	4.701	46.6	1.660	2.528	.939	3.007	54.3
3.240	3.565	.967	4.817	46.6	1.698	2.641	.948	3.121	54.9
3.394	3.717	.970	5.033	46.5	1.759	2.721	.956	3.222	54.8
3.441	3.776	.971	5.109	46.6	1.815	2.775	.962	3.298	54.6
3.505	3.844	.968	5.201	46.6	1.870	2.866	.969	3.404	54.7

TABLE 12.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
1.964	2.983	.971	3.554	54.6
1.986	3.050	.970	3.621	54.9
2.047	3.130	.970	3.722	54.8
2.091	3.211	.971	3.813	55.0
2.254	3.390	.972	4.054	54.6
2.273	3.459	.971	4.121	54.9
2.335	3.539	.971	4.222	54.8
2.378	3.620	.971	4.313	55.0
2.544	3.798	.973	4.554	54.6
2.561	3.868	.971	4.621	54.9
2.623	3.947	.971	4.722	54.8
2.665	4.029	.970	4.813	55.0
2.834	4.205	.971	5.054	54.6
2.849	4.277	.970	5.121	54.9
2.911	4.356	.970	5.222	54.8
2.952	4.439	.968	5.313	55.0
3.124	4.613	.956	5.554	54.6
3.136	4.686	.951	5.621	54.9
3.199	4.765	.948	5.722	54.8
3.239	4.848	.946	5.813	55.0
3.414	5.020	.947	6.054	54.6
3.424	5.095	.947	6.121	54.9
3.487	5.173	.947	6.222	54.8
3.526	5.258	.948	6.313	55.0
-.151	.107	1.443	-.009	69.2
-.110	.216	1.444	.108	69.2
-.074	.309	1.472	.208	69.2
-.041	.396	1.493	.300	69.1
-.004	.493	1.498	.404	69.1
.026	.574	1.498	.491	69.2
.068	.683	1.499	.608	69.2
.103	.776	1.495	.708	69.2
.137	.863	1.488	.800	69.1
.174	.960	1.460	.904	69.1
.204	1.042	.897	.991	69.2
.245	1.150	.380	1.108	69.2
.281	1.244	.374	1.208	69.2
.315	1.330	.370	1.300	69.1
.352	1.427	.369	1.404	69.1
.382	1.509	.373	1.491	69.2
.423	1.618	.382	1.608	69.2
.459	1.711	.397	1.708	69.2
.493	1.797	.424	1.800	69.1
.530	1.894	.462	1.904	69.1

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
.559	1.976	.519	1.991	69.2
.601	2.085	.602	2.108	69.2
.636	2.179	.676	2.208	69.2
.671	2.264	.745	2.300	69.1
.708	2.362	.804	2.404	69.1
.737	2.444	.846	2.491	69.2
.778	2.553	.894	2.608	69.2
.814	2.646	.922	2.708	69.2
.850	2.732	.938	2.800	69.1
.886	2.829	.949	2.904	69.1
.915	2.911	.952	2.991	69.2
.956	3.020	.954	3.108	69.2
.992	3.113	.955	3.208	69.2
1.028	3.199	.954	3.300	69.1
1.064	3.296	.958	3.404	69.1
1.104	3.398	.957	3.514	69.1
1.137	3.496	.961	3.617	69.2
1.170	3.573	.964	3.701	69.1
1.209	3.671	.967	3.806	69.1
1.282	3.866	.968	4.014	69.1
1.315	3.963	.968	4.117	69.2
1.348	4.040	.970	4.201	69.1
1.388	4.138	.970	4.306	69.1
1.460	4.333	.971	4.514	69.1
1.492	4.431	.970	4.617	69.2
1.527	4.507	.971	4.701	69.1
1.566	4.605	.971	4.806	69.1
1.638	4.800	.971	5.014	69.1
1.670	4.898	.971	5.117	69.2
1.705	4.974	.968	5.201	69.1
1.744	5.073	.960	5.306	69.1
1.816	5.267	.943	5.514	69.1
1.848	5.366	.939	5.617	69.2
1.883	5.442	.939	5.701	69.1
1.922	5.540	.939	5.806	69.1
1.994	5.734	.941	6.014	69.1
2.026	5.833	.941	6.117	69.2
2.061	5.909	.943	6.201	69.1
2.101	6.007	.944	6.306	69.1
-.203	.134	1.441	.005	83.5
-.191	.236	1.439	.108	83.4
-.180	.339	1.471	.212	83.4
-.170	.426	1.492	.299	83.5
-.159	.530	1.496	.404	83.6

TABLE 12.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
-.146	.630	1.497	.505	83.5	.390	5.402	.930	5.306	83.6
-.133	.732	1.494	.608	83.4	.384	5.614	.931	5.517	83.9
-.122	.835	1.490	.712	83.4	.415	5.708	.931	5.614	83.7
-.113	.922	1.471	.799	83.5	.429	5.797	.933	5.704	83.6
-.103	1.026	1.024	.904	83.6	.446	5.898	.935	5.806	83.6
-.090	1.127	.393	1.005	83.5	.438	6.111	.940	6.017	83.9
-.075	1.229	.373	1.108	83.4	.471	6.205	.940	6.114	83.7
-.065	1.332	.366	1.212	83.4	.485	6.294	.942	6.204	83.6
-.057	1.419	.365	1.299	83.5	.502	6.395	.944	6.306	83.6
-.047	1.523	.387	1.404	83.6					
-.033	1.624	.375	1.505	83.5	-.268	.144	1.440	.017	98.8
-.018	1.725	.389	1.608	83.4	-.282	.236	1.440	.110	98.9
-.008	1.829	.412	1.712	83.4	-.297	.338	1.473	.213	98.7
.000	1.916	.450	1.799	83.5	-.299	.423	1.493	.297	97.5
.009	2.020	.546	1.904	83.6	-.314	.529	1.496	.405	97.6
.024	2.121	.586	2.005	83.5	-.345	.638	1.497	.517	98.8
.040	2.222	.663	2.108	83.4	-.360	.730	1.495	.610	98.9
.049	2.326	.742	2.212	83.4	-.372	.832	1.491	.713	98.7
.057	2.413	.805	2.299	83.5	-.365	.918	1.477	.797	97.5
.065	2.517	.883	2.404	83.6	-.380	1.025	1.066	.905	97.6
.081	2.618	.902	2.505	83.5	-.422	1.132	.373	1.017	98.8
.098	2.719	.933	2.608	83.4	-.437	1.224	.371	1.110	98.9
.106	2.822	.948	2.712	83.4	-.448	1.326	.365	1.213	98.7
.113	2.910	.952	2.799	83.5	-.430	1.414	.366	1.297	97.5
.121	3.014	.955	2.904	83.6	-.447	1.520	.372	1.405	97.6
.138	3.114	.957	3.005	83.5	-.498	1.626	.384	1.517	98.8
.156	3.215	.959	3.108	83.4	-.514	1.718	.403	1.610	98.9
.163	3.319	.961	3.212	83.4	-.523	1.821	.437	1.713	98.7
.170	3.406	.962	3.299	83.5	-.495	1.910	.480	1.797	97.5
.177	3.511	.965	3.404	83.6	-.513	2.016	.571	1.905	97.6
.171	3.625	.963	3.517	83.9	-.575	2.120	.654	2.017	98.8
.195	3.720	.966	3.614	83.7	-.591	2.212	.730	2.110	98.9
.207	3.810	.967	3.704	83.6	-.599	2.315	.798	2.213	98.7
.222	3.911	.969	3.806	83.6	-.561	2.405	.850	2.297	97.5
.224	4.122	.971	4.017	83.9	-.579	2.512	.911	2.405	97.6
.250	4.217	.971	4.114	83.7	-.652	2.614	.934	2.517	98.8
.263	4.307	.972	4.204	83.6	-.668	2.706	.947	2.610	98.9
.278	4.408	.973	4.306	83.6	-.674	2.809	.952	2.713	98.7
.278	4.619	.973	4.517	83.9	-.626	2.901	.955	2.797	97.5
.305	4.714	.973	4.614	83.7	-.646	3.007	.955	2.905	97.6
.318	4.803	.973	4.704	83.6	-.729	3.109	.958	3.017	98.8
.334	4.905	.971	4.806	83.6	-.745	3.200	.960	3.110	98.9
.331	5.117	.955	5.017	83.9	-.750	3.303	.961	3.213	98.7
.360	5.211	.943	5.114	83.7	-.692	3.397	.965	3.297	97.5
.374	5.300	.933	5.204	83.6	-.712	3.503	.968	3.405	97.6

TABLE 12.- Concluded

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
-.781	3.601	.966	3.512	98.5
-.793	3.705	.969	3.616	98.4
-.808	3.790	.969	3.703	98.4
-.818	3.897	.970	3.810	98.4
-.855	4.096	.971	4.012	98.5
-.866	4.199	.972	4.116	98.4
-.881	4.285	.972	4.203	98.4
-.891	4.391	.973	4.310	98.4
-.928	4.590	.973	4.512	98.5
-.939	4.694	.971	4.616	98.4
-.955	4.779	.968	4.703	98.4
-.964	4.886	.957	4.810	98.4
-1.002	5.085	.936	5.012	98.5
-1.012	5.188	.927	5.116	98.4
-1.028	5.274	.926	5.203	98.4
-1.037	5.381	.927	5.310	98.4
-1.075	5.579	.930	5.512	98.5
-1.085	5.683	.930	5.616	98.4
-1.102	5.768	.933	5.703	98.4
-1.110	5.875	.934	5.810	98.4
-1.149	6.074	.939	6.012	98.5
-1.158	6.178	.942	6.116	98.4
-1.175	6.263	.942	6.203	98.4
-1.182	6.370	.945	6.310	98.4

TABLE 13.- PITOT-PRESSURE MEASUREMENTS AT $x = 2.571$ in. FOR $M_\infty = 1.20$ WITH NPR = 4.00 AND $T_{t,j}/T_{t,\infty} = 0.88$

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
-.025	-.098	1.615	-.025	.6	4.588	-.053	.989	4.589	.6
.080	-.097	1.624	.080	.6	4.686	-.049	.989	4.687	.6
.185	-.096	1.630	.185	.6	4.778	-.053	.989	4.778	.5
.291	-.095	1.630	.291	.6	4.988	-.046	.991	4.988	.6
.379	-.094	1.629	.379	.5	5.088	-.049	.990	5.089	.6
.475	-.093	1.624	.475	.6	5.186	-.044	.990	5.187	.6
.580	-.092	1.622	.580	.6	5.278	-.049	.989	5.278	.5
.685	-.091	1.618	.685	.6	5.488	-.041	.986	5.488	.6
.791	-.089	1.616	.791	.6	5.588	-.044	.970	5.589	.6
.879	-.090	1.614	.879	.5	5.686	-.039	.956	5.687	.6
.975	-.088	1.614	.975	.6	5.778	-.044	.954	5.778	.5
1.080	-.087	1.613	1.080	.6	5.988	-.036	.955	5.988	.6
1.185	-.085	1.607	1.185	.6	6.088	-.039	.955	6.089	.6
1.291	-.084	1.603	1.291	.6	6.186	-.034	.955	6.187	.6
1.379	-.085	1.600	1.379	.5	6.278	-.039	.955	6.278	.5
1.475	-.084	1.595	1.475	.6					
1.580	-.081	1.592	1.580	.6	-.012	-.071	1.622	-.010	7.7
1.685	-.080	1.584	1.685	.6	.077	-.059	1.632	.080	7.7
1.791	-.079	1.557	1.791	.6	.182	-.045	1.638	.185	7.7
1.879	-.080	1.466	1.879	.5	.286	-.031	1.637	.291	7.6
1.975	-.079	1.209	1.975	.6	.369	-.019	1.637	.375	7.7
2.080	-.076	.952	2.080	.6	.484	-.004	1.634	.490	7.7
2.185	-.075	.753	2.185	.6	.573	.008	1.632	.580	7.7
2.291	-.074	.670	2.291	.6	.677	.022	1.630	.685	7.7
2.378	-.076	.670	2.379	.5	.781	.036	1.627	.791	7.6
2.475	-.074	.706	2.475	.6	.865	.047	1.625	.875	7.7
2.580	-.071	.755	2.580	.6	.979	.063	1.621	.990	7.7
2.685	-.070	.808	2.685	.6	1.068	.075	1.619	1.080	7.7
2.791	-.069	.863	2.791	.6	1.173	.089	1.616	1.185	7.7
2.878	-.071	.905	2.879	.5	1.277	.102	1.614	1.291	7.6
2.988	-.067	.954	2.988	.6	1.360	.114	1.612	1.375	7.7
3.080	-.066	.979	3.080	.6	1.475	.130	1.605	1.490	7.7
3.185	-.065	.992	3.185	.6	1.564	.142	1.602	1.580	7.7
3.278	-.067	.992	3.278	.5	1.668	.156	1.595	1.685	7.7
3.378	-.066	.994	3.379	.5	1.773	.168	1.577	1.791	7.6
3.488	-.062	.991	3.488	.6	1.856	.181	1.519	1.875	7.7
3.588	-.063	.991	3.589	.6	1.970	.196	1.277	1.990	7.7
3.686	-.060	.991	3.687	.6	2.060	.208	1.026	2.080	7.7
3.778	-.063	.991	3.778	.5	2.164	.222	.805	2.185	7.7
3.988	-.057	.992	3.988	.6	2.268	.235	.693	2.291	7.6
4.088	-.058	.992	4.089	.6	2.351	.248	.681	2.375	7.7
4.186	-.055	.991	4.187	.6	2.466	.263	.716	2.490	7.7
4.278	-.058	.990	4.278	.5	2.555	.275	.761	2.580	7.7
4.488	-.051	.989	4.488	.6	2.659	.289	.810	2.685	7.7
					2.764	.301	.863	2.791	7.6

TABLE 13.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
2.847	.314	.905	2.875	7.7	1.315	.334	1.605	1.375	15.7
2.961	.330	.957	2.990	7.7	1.412	.363	1.598	1.476	15.7
3.058	.343	.976	3.088	7.7	1.513	.385	1.593	1.580	15.6
3.162	.357	.988	3.193	7.7	1.615	.416	1.588	1.686	15.6
3.246	.368	.992	3.277	7.7	1.717	.442	1.581	1.791	15.5
3.342	.381	.995	3.375	7.7	1.796	.469	1.582	1.875	15.7
3.431	.393	.992	3.464	7.7	1.894	.498	1.567	1.976	15.7
3.554	.410	.992	3.588	7.7	1.995	.520	1.525	2.080	15.6
3.658	.424	.991	3.693	7.7	2.097	.551	1.347	2.186	15.6
3.741	.435	.991	3.777	7.7	2.199	.576	1.058	2.291	15.5
3.926	.460	.991	3.964	7.7	2.278	.604	.873	2.375	15.7
4.049	.476	.990	4.088	7.7	2.375	.634	.757	2.476	15.7
4.154	.490	.990	4.193	7.7	2.477	.654	.727	2.580	15.6
4.237	.502	.989	4.277	7.7	2.578	.686	.753	2.686	15.6
4.422	.526	.989	4.464	7.7	2.681	.710	.795	2.791	15.5
4.545	.543	.989	4.588	7.7	2.759	.740	.834	2.875	15.7
4.649	.557	.989	4.693	7.7	2.856	.769	.896	2.976	15.7
4.732	.568	.988	4.777	7.7	2.958	.788	.947	3.080	15.6
4.917	.593	.991	4.964	7.7	3.060	.821	.980	3.186	15.6
5.040	.610	.991	5.088	7.7	3.144	.861	.989	3.279	15.9
5.145	.624	.990	5.193	7.7	3.240	.875	.994	3.375	15.7
5.228	.635	.991	5.277	7.7	3.341	.915	.991	3.482	15.9
5.413	.660	.988	5.464	7.7	3.443	.941	.990	3.588	15.8
5.536	.677	.973	5.588	7.7	3.544	.972	.989	3.693	15.9
5.640	.691	.962	5.693	7.7	3.625	.998	.989	3.779	15.9
5.724	.702	.960	5.777	7.7	3.821	1.052	.989	3.982	15.9
5.908	.727	.959	5.964	7.7	3.924	1.077	.989	4.088	15.8
6.031	.743	.958	6.088	7.7	4.025	1.109	.988	4.193	15.9
6.136	.757	.955	6.193	7.7	4.106	1.135	.988	4.279	15.9
6.219	.769	.955	6.277	7.7	4.302	1.189	.989	4.482	15.9
					4.405	1.213	.989	4.588	15.8
-.031	-.044	1.624	-.024	15.7	4.506	1.245	.989	4.693	15.9
.068	-.017	1.630	.080	15.6	4.587	1.272	.989	4.779	15.9
.171	.012	1.641	.186	15.6	4.783	1.326	.990	4.982	15.9
.272	.040	1.641	.291	15.5	4.887	1.350	.989	5.088	15.8
.352	.064	1.644	.375	15.7	4.987	1.382	.988	5.193	15.9
.450	.091	1.639	.476	15.7	5.068	1.409	.988	5.279	15.9
.550	.117	1.637	.580	15.6	5.264	1.463	.980	5.482	15.9
.652	.147	1.632	.686	15.6	5.368	1.486	.970	5.588	15.8
.754	.174	1.626	.791	15.5	5.468	1.518	.967	5.693	15.9
.833	.199	1.625	.875	15.7	5.549	1.545	.967	5.779	15.9
.931	.227	1.619	.976	15.7	5.745	1.599	.965	5.982	15.9
1.032	.251	1.615	1.080	15.6	5.849	1.622	.962	6.088	15.8
1.134	.282	1.611	1.186	15.6	5.949	1.655	.961	6.193	15.9
1.236	.308	1.606	1.291	15.5	6.030	1.682	.959	6.279	15.9

TABLE 13.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
-.044	-.012	1.632	-.024	25.4	4.200	2.001	.988	4.673	25.4
.050	.033	1.636	.080	25.4	4.304	2.030	.986	4.779	25.2
.144	.077	1.645	.183	25.4	4.480	2.134	.989	4.983	25.4
.240	.123	1.650	.291	25.4	4.575	2.179	.988	5.088	25.4
.316	.159	1.650	.375	25.4	4.652	2.215	.987	5.173	25.4
.408	.202	1.651	.476	25.4	4.756	2.243	.985	5.279	25.2
.502	.247	1.644	.580	25.4	4.932	2.348	.979	5.483	25.4
.595	.291	1.639	.683	25.4	5.027	2.393	.974	5.588	25.4
.692	.337	1.628	.791	25.4	5.104	2.429	.970	5.673	25.4
.768	.373	1.624	.875	25.4	5.209	2.456	.970	5.779	25.2
.859	.417	1.612	.976	25.4	5.384	2.562	.969	5.983	25.4
.954	.461	1.606	1.080	25.4	5.479	2.607	.967	6.088	25.4
1.047	.506	1.600	1.183	25.4	5.556	2.644	.966	6.173	25.4
1.144	.552	1.585	1.291	25.4	5.661	2.668	.966	6.279	25.2
1.220	.588	1.579	1.375	25.4					
1.311	.631	1.524	1.476	25.4	-.049	-.005	1.613	-.025	27.7
1.406	.676	1.489	1.580	25.4	.045	.044	1.615	.080	27.7
1.499	.720	1.436	1.683	25.4	.138	.093	1.621	.185	27.7
1.596	.766	1.320	1.791	25.4	.229	.141	1.631	.289	27.7
1.672	.802	1.225	1.875	25.4	.317	.188	1.632	.388	27.7
1.763	.845	1.055	1.976	25.4	.394	.228	1.632	.475	27.7
1.857	.890	.964	2.080	25.4	.487	.277	1.628	.580	27.7
1.951	.934	.883	2.183	25.4	.580	.326	1.621	.685	27.7
2.047	.980	.804	2.291	25.4	.672	.374	1.614	.789	27.7
2.123	1.016	.765	2.375	25.4	.760	.420	1.600	.888	27.7
2.215	1.059	.675	2.476	25.4	.837	.461	1.580	.975	27.7
2.309	1.104	.656	2.580	25.4	.930	.510	1.573	1.080	27.7
2.402	1.148	.648	2.683	25.4	1.023	.559	1.554	1.185	27.7
2.499	1.194	.654	2.791	25.4	1.114	.607	1.537	1.289	27.7
2.575	1.230	.660	2.875	25.4	1.203	.653	1.501	1.388	27.7
2.673	1.277	.709	2.983	25.4	1.279	.693	1.415	1.475	27.7
2.768	1.322	.813	3.088	25.4	1.372	.742	1.355	1.580	27.7
2.854	1.363	.923	3.183	25.4	1.465	.791	1.248	1.685	27.7
2.946	1.392	.976	3.279	25.2	1.557	.839	1.130	1.789	27.7
3.027	1.445	.988	3.375	25.4	1.645	.886	.984	1.888	27.7
3.125	1.491	.989	3.483	25.4	1.722	.926	.884	1.975	27.7
3.220	1.536	.989	3.588	25.4	1.815	.975	.820	2.080	27.7
3.297	1.573	.988	3.673	25.4	1.908	1.024	.779	2.185	27.7
3.399	1.605	.988	3.779	25.2	1.999	1.072	.750	2.289	27.7
3.576	1.705	.989	3.983	25.4	2.088	1.118	.699	2.388	27.7
3.672	1.750	.989	4.088	25.4	2.164	1.159	.645	2.475	27.7
3.749	1.787	.989	4.173	25.4	2.257	1.208	.587	2.580	27.7
3.851	1.818	.989	4.279	25.2	2.351	1.257	.545	2.685	27.7
4.028	1.919	.987	4.483	25.4	2.442	1.305	.547	2.789	27.7
4.123	1.964	.988	4.588	25.4	2.530	1.351	.577	2.888	27.7

TABLE 13.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
2.614	1.395	.688	2.983	27.7	1.246	.756	1.296	1.476	30.1
2.707	1.444	.823	3.089	27.7	1.337	.806	1.196	1.580	30.0
2.793	1.489	.903	3.185	27.7	1.427	.860	1.065	1.685	30.1
2.884	1.537	.967	3.289	27.7	1.523	.916	.917	1.796	30.1
2.973	1.584	.990	3.388	27.7	1.591	.955	.822	1.875	30.1
3.057	1.628	.992	3.483	27.7	1.679	1.006	.779	1.976	30.1
3.150	1.677	.992	3.589	27.7	1.770	1.056	.762	2.080	30.0
3.240	1.724	.992	3.690	27.7	1.860	1.111	.767	2.185	30.1
3.317	1.765	.992	3.777	27.7	1.955	1.166	.754	2.296	30.1
3.500	1.861	.992	3.983	27.7	2.024	1.206	.720	2.375	30.1
3.593	1.910	.992	4.089	27.7	2.112	1.257	.670	2.476	30.1
3.682	1.957	.992	4.190	27.7	2.203	1.307	.615	2.580	30.0
3.760	1.997	.991	4.277	27.7	2.292	1.362	.574	2.685	30.1
3.942	2.093	.991	4.483	27.7	2.388	1.417	.575	2.796	30.1
4.035	2.142	.990	4.589	27.7	2.456	1.457	.618	2.875	30.1
4.125	2.189	.989	4.690	27.7	2.544	1.508	.766	2.976	30.1
4.202	2.230	.988	4.777	27.7	2.642	1.564	.876	3.089	30.1
4.385	2.326	.991	4.983	27.7	2.714	1.639	.941	3.189	30.6
4.478	2.375	.989	5.089	27.7	2.787	1.688	.977	3.277	30.6
4.567	2.422	.988	5.190	27.7	2.889	1.707	.990	3.375	30.1
4.645	2.463	.987	5.277	27.7	2.982	1.764	.992	3.483	30.1
4.827	2.559	.981	5.483	27.7	3.075	1.815	.993	3.589	30.1
4.920	2.608	.974	5.589	27.7	3.144	1.893	.992	3.689	30.6
5.010	2.655	.974	5.690	27.7	3.218	1.943	.992	3.777	30.6
5.087	2.695	.973	5.777	27.7	3.414	2.015	.992	3.983	30.1
5.270	2.791	.973	5.983	27.7	3.507	2.066	.991	4.089	30.1
5.363	2.840	.971	6.089	27.7	3.575	2.148	.991	4.189	30.6
5.452	2.887	.970	6.190	27.7	3.648	2.197	.992	4.277	30.6
5.530	2.928	.969	6.277	27.7	3.847	2.266	.991	4.483	30.1
					3.940	2.316	.991	4.589	30.1
-.051	.003	1.616	-.024	30.1	4.005	2.402	.988	4.689	30.6
.039	.055	1.618	.080	30.0	4.078	2.452	.989	4.777	30.6
.129	.108	1.619	.185	30.1	4.279	2.517	.991	4.983	30.1
.225	.164	1.629	.296	30.1	4.372	2.567	.988	5.089	30.1
.293	.203	1.634	.375	30.1	4.436	2.656	.987	5.189	30.6
.381	.254	1.629	.476	30.1	4.508	2.707	.986	5.277	30.6
.471	.306	1.624	.580	30.0	4.712	2.768	.981	5.483	30.1
.562	.359	1.610	.685	30.1	4.805	2.818	.976	5.589	30.1
.658	.414	1.595	.796	30.1	4.866	2.910	.973	5.689	30.6
.726	.454	1.580	.875	30.1	4.938	2.962	.974	5.777	30.6
.814	.505	1.556	.976	30.1	5.144	3.019	.973	5.983	30.1
.904	.556	1.545	1.080	30.0	5.238	3.068	.972	6.089	30.1
.995	.610	1.520	1.185	30.1	5.297	3.165	.972	6.189	30.6
1.090	.665	1.473	1.296	30.1	5.369	3.217	.972	6.277	30.6
1.158	.705	1.413	1.375	30.1					

TABLE 13.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
-.069	.028	1.615	-.024	38.4	3.627	2.945	.989	4.684	38.3
.014	.092	1.615	.080	38.3	3.704	3.006	.989	4.783	38.3
.097	.158	1.614	.187	38.3	3.870	3.120	.987	4.983	38.1
.178	.222	1.611	.290	38.3	3.948	3.192	.987	5.089	38.2
.244	.275	1.603	.375	38.4	4.019	3.255	.987	5.184	38.3
.323	.338	1.599	.476	38.4	4.096	3.316	.986	5.283	38.3
.406	.402	1.585	.580	38.3	4.263	3.429	.980	5.483	38.1
.489	.468	1.567	.687	38.3	4.341	3.502	.977	5.589	38.2
.570	.532	1.553	.790	38.3	4.411	3.565	.977	5.684	38.3
.636	.585	1.525	.875	38.4	4.489	3.626	.977	5.783	38.3
.716	.648	1.446	.976	38.4	4.656	3.738	.976	5.983	38.1
.799	.712	1.351	1.080	38.3	4.733	3.811	.976	6.089	38.2
.882	.778	1.190	1.187	38.3	4.804	3.875	.976	6.184	38.3
.963	.842	1.049	1.290	38.3	4.881	3.936	.976	6.283	38.3
1.028	.896	.894	1.375	38.4					
1.108	.958	.762	1.476	38.4	-.085	.047	1.605	-.024	45.4
1.191	1.021	.700	1.580	38.3	-.005	.128	1.607	.090	45.4
1.274	1.088	.662	1.687	38.3	.062	.197	1.601	.187	45.4
1.355	1.152	.663	1.790	38.3	.134	.269	1.587	.289	45.4
1.421	1.206	.682	1.875	38.4	.204	.340	1.562	.388	45.4
1.500	1.269	.731	1.976	38.4	.266	.403	1.564	.476	45.4
1.584	1.331	.767	2.080	38.3	.345	.484	1.554	.590	45.4
1.667	1.398	.809	2.187	38.3	.413	.553	1.529	.687	45.4
1.747	1.462	.830	2.290	38.3	.485	.626	1.475	.789	45.4
1.813	1.516	.843	2.375	38.4	.555	.696	1.327	.888	45.4
1.892	1.579	.853	2.476	38.4	.617	.759	1.165	.976	45.4
1.976	1.641	.856	2.580	38.3	.696	.841	.973	1.090	45.4
2.059	1.708	.862	2.687	38.3	.764	.909	.813	1.187	45.4
2.139	1.772	.876	2.790	38.3	.836	.982	.698	1.289	45.4
2.205	1.826	.892	2.875	38.4	.907	1.052	.616	1.388	45.4
2.297	1.885	.921	2.983	38.1	.967	1.116	.602	1.476	45.4
2.369	1.951	.940	3.080	38.3	1.047	1.197	.608	1.590	45.4
2.451	2.017	.963	3.187	38.3	1.115	1.265	.630	1.687	45.4
2.532	2.082	.979	3.290	38.3	1.187	1.338	.668	1.789	45.4
2.597	2.137	.990	3.375	38.4	1.258	1.408	.722	1.888	45.4
2.690	2.194	.990	3.483	38.1	1.318	1.472	.759	1.976	45.4
2.770	2.264	.992	3.589	38.2	1.398	1.553	.804	2.090	45.4
2.842	2.326	.992	3.684	38.3	1.466	1.622	.838	2.187	45.4
2.919	2.387	.991	3.783	38.3	1.537	1.694	.871	2.289	45.4
3.084	2.503	.991	3.983	38.1	1.609	1.764	.905	2.388	45.4
3.162	2.573	.992	4.089	38.2	1.669	1.828	.919	2.476	45.4
3.234	2.635	.991	4.184	38.3	1.748	1.910	.939	2.590	45.4
3.312	2.697	.991	4.283	38.3	1.817	1.978	.954	2.687	45.4
3.477	2.811	.989	4.483	38.1	1.888	2.050	.966	2.789	45.4
3.555	2.883	.989	4.589	38.2	1.960	2.120	.980	2.888	45.4

TABLE 13.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
2.025	2.189	.984	2.983	45.4
2.103	2.259	.990	3.088	45.3
2.175	2.337	.991	3.194	45.4
2.232	2.400	.992	3.279	45.4
2.311	2.476	.994	3.388	45.4
2.376	2.545	.993	3.483	45.4
2.455	2.615	.992	3.588	45.3
2.526	2.693	.991	3.694	45.4
2.583	2.756	.991	3.779	45.4
2.727	2.902	.991	3.983	45.4
2.806	2.970	.990	4.088	45.3
2.877	3.049	.990	4.194	45.4
2.934	3.112	.989	4.279	45.4
3.078	3.258	.988	4.483	45.4
3.158	3.326	.988	4.588	45.3
3.229	3.404	.988	4.694	45.4
3.285	3.468	.988	4.779	45.4
3.429	3.614	.987	4.983	45.4
3.509	3.681	.986	5.088	45.3
3.580	3.760	.985	5.194	45.4
3.636	3.824	.984	5.279	45.4
3.779	3.970	.980	5.483	45.4
3.861	4.037	.980	5.588	45.3
3.931	4.116	.979	5.694	45.4
3.987	4.181	.978	5.779	45.4
4.130	4.327	.979	5.983	45.4
4.212	4.392	.977	6.088	45.3
4.282	4.472	.975	6.194	45.4
4.337	4.537	.976	6.279	45.4
-.128	.083	1.600	-.020	60.8
-.079	.170	1.596	.079	60.8
-.027	.262	1.578	.185	60.8
.024	.354	1.551	.291	60.8
.065	.428	1.539	.375	60.8
.117	.519	1.521	.480	60.8
.165	.606	1.466	.579	60.8
.217	.699	1.340	.685	60.8
.268	.791	1.105	.791	60.8
.309	.864	.908	.875	60.8
.361	.956	.723	.980	60.8
.409	1.042	.633	1.079	60.8
.461	1.135	.572	1.185	60.8
.512	1.227	.546	1.291	60.8
.554	1.300	.549	1.375	60.8
.605	1.392	.569	1.480	60.8
.653	1.479	.591	1.579	60.8
.705	1.571	.627	1.685	60.8
.757	1.663	.683	1.791	60.8
.798	1.737	.732	1.875	60.8
.849	1.828	.792	1.980	60.8
.897	1.915	.837	2.079	60.8
.949	2.008	.887	2.185	60.8
1.001	2.100	.935	2.291	60.8
1.042	2.173	.958	2.375	60.8
1.093	2.265	.970	2.480	60.8
1.142	2.351	.977	2.579	60.8
1.194	2.444	.983	2.685	60.8
1.245	2.536	.986	2.791	60.8
1.286	2.609	.986	2.875	60.8
1.342	2.709	.987	2.989	60.8
1.390	2.796	.988	3.088	60.8
1.441	2.887	.988	3.192	60.8
1.483	2.961	.989	3.277	60.8
1.530	3.046	.992	3.375	60.8
1.586	3.146	.990	3.489	60.8
1.634	3.232	.990	3.588	60.8
1.685	3.323	.990	3.692	60.8
1.727	3.397	.990	3.777	60.8
1.830	3.582	.988	3.989	60.8
1.878	3.668	.988	4.088	60.8
1.929	3.759	.988	4.192	60.8
1.971	3.833	.988	4.277	60.8
2.074	4.018	.988	4.489	60.8
2.123	4.105	.986	4.588	60.8
2.174	4.196	.985	4.692	60.8
2.215	4.270	.985	4.777	60.8
2.319	4.455	.983	4.989	60.8
2.367	4.541	.983	5.088	60.8
2.418	4.632	.983	5.192	60.8
2.459	4.706	.983	5.277	60.8
2.563	4.891	.980	5.489	60.8
2.611	4.977	.980	5.588	60.8
2.662	5.068	.980	5.692	60.8
2.703	5.142	.980	5.777	60.8
2.807	5.328	.981	5.989	60.8
2.855	5.414	.980	6.088	60.8
2.906	5.505	.979	6.192	60.8
2.947	5.579	.979	6.277	60.8

TABLE 13.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
-.176	.099	1.593	-.024	74.9	1.045	4.634	.980	4.673	74.9
-.149	.200	1.586	.081	74.9	1.072	4.735	.978	4.777	74.9
-.122	.300	1.562	.185	74.9	1.125	4.934	.981	4.983	74.9
-.091	.416	1.536	.304	74.9	1.152	5.035	.980	5.088	74.9
-.068	.504	1.505	.395	74.9	1.175	5.117	.979	5.173	74.9
-.046	.582	1.476	.476	74.9	1.202	5.218	.980	5.277	74.9
-.019	.683	1.335	.581	74.9	1.255	5.416	.980	5.483	74.9
.008	.783	1.115	.685	74.9	1.282	5.518	.980	5.588	74.9
.039	.899	.805	.804	74.9	1.304	5.600	.980	5.673	74.9
.062	.986	.664	.895	74.9	1.332	5.701	.980	5.777	74.9
.084	1.065	.600	.976	74.9	1.385	5.899	.982	5.983	74.9
.111	1.166	.548	1.081	74.9	1.412	6.001	.982	6.088	74.9
.138	1.266	.533	1.185	74.9	1.434	6.083	.981	6.173	74.9
.169	1.382	.537	1.304	74.9	1.462	6.184	.983	6.277	74.9
.192	1.469	.553	1.395	74.9					
.214	1.548	.569	1.476	74.9	-.232	.104	1.605	-.026	90.7
.241	1.649	.603	1.581	74.9	-.232	.210	1.590	.080	90.4
.268	1.749	.644	1.685	74.9	-.232	.316	1.559	.186	90.3
.299	1.864	.720	1.804	74.9	-.232	.421	1.537	.291	90.3
.322	1.952	.781	1.895	74.9	-.233	.527	1.469	.397	90.2
.344	2.030	.821	1.976	74.9	-.238	.604	1.411	.474	90.7
.371	2.131	.881	2.081	74.9	-.235	.710	1.201	.580	90.4
.398	2.232	.927	2.185	74.9	-.234	.816	.936	.686	90.3
.429	2.347	.965	2.304	74.9	-.235	.921	.703	.791	90.3
.452	2.435	.977	2.395	74.9	-.235	1.027	.594	.897	90.2
.474	2.513	.980	2.476	74.9	-.244	1.104	.562	.974	90.7
.501	2.614	.981	2.581	74.9	-.238	1.210	.544	1.080	90.4
.528	2.714	.984	2.685	74.9	-.237	1.316	.546	1.186	90.3
.559	2.830	.984	2.804	74.9	-.237	1.421	.566	1.291	90.3
.582	2.918	.984	2.895	74.9	-.237	1.527	.595	1.397	90.2
.604	2.996	.986	2.976	74.9	-.250	1.604	.626	1.474	90.7
.631	3.097	.986	3.081	74.9	-.242	1.709	.672	1.580	90.4
.658	3.197	.986	3.185	74.9	-.239	1.816	.725	1.686	90.3
.689	3.313	.986	3.304	74.9	-.240	1.920	.802	1.791	90.3
.712	3.400	.987	3.395	74.9	-.239	2.027	.866	1.897	90.2
.735	3.485	.983	3.483	74.9	-.255	2.104	.903	1.974	90.7
.763	3.587	.984	3.588	74.9	-.245	2.209	.940	2.080	90.4
.785	3.669	.983	3.673	74.9	-.241	2.316	.960	2.186	90.3
.812	3.769	.983	3.777	74.9	-.242	2.420	.973	2.291	90.3
.865	3.968	.984	3.983	74.9	-.241	2.527	.977	2.397	90.2
.893	4.069	.984	4.088	74.9	-.261	2.604	.974	2.474	90.7
.915	4.151	.984	4.173	74.9	-.248	2.709	.977	2.580	90.4
.942	4.252	.984	4.277	74.9	-.244	2.816	.981	2.686	90.3
.995	4.451	.981	4.483	74.9	-.244	2.920	.981	2.791	90.3
1.022	4.552	.978	4.588	74.9	-.243	3.027	.981	2.897	90.2

TABLE 13.- Concluded

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
-.267	3.104	.983	2.974	90.7
-.251	3.209	.983	3.080	90.4
-.246	3.316	.983	3.186	90.3
-.247	3.420	.984	3.291	90.3
-.245	3.527	.984	3.397	90.2
-.180	3.612	.983	3.483	89.2
-.170	3.719	.982	3.590	89.1
-.167	3.907	.982	3.777	89.1
-.173	4.112	.981	3.983	89.2
-.162	4.219	.980	4.090	89.1
-.159	4.407	.976	4.277	89.1
-.166	4.612	.978	4.483	89.2
-.154	4.719	.976	4.590	89.1
-.151	4.907	.975	4.777	89.1
-.159	5.112	.979	4.983	89.2
-.146	5.219	.978	5.090	89.1
-.143	5.407	.978	5.277	89.1
-.152	5.612	.977	5.483	89.2
-.138	5.719	.979	5.590	89.1
-.135	5.906	.979	5.777	89.1
-.146	6.112	.979	5.983	89.2
-.130	6.219	.981	6.090	89.1
-.127	6.406	.981	6.277	89.1

TABLE 14.- PITOT-PRESSURE MEASUREMENTS AT $x = 5.172$ in. FOR $M_\infty = 1.20$ WITH NPR = 4.00 AND $T_{t,j}/T_{t,\infty} = 0.87$

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
-.021	-.100	1.492	-.021	.0	4.608	-.102	.992	4.608	.0
.105	-.100	1.493	.105	.0	4.720	-.102	.993	4.720	.0
.211	-.103	1.493	.211	-.3	4.802	-.102	.993	4.802	.0
.316	-.100	1.492	.316	.0	4.997	-.102	.990	4.997	.0
.401	-.100	1.490	.401	.0	5.108	-.102	.991	5.108	.0
.479	-.100	1.489	.479	.0	5.220	-.102	.990	5.220	.0
.605	-.100	1.483	.605	.0	5.302	-.102	.991	5.302	.0
.711	-.105	1.481	.711	-.3	5.497	-.102	.988	5.497	.0
.816	-.100	1.480	.816	.0	5.608	-.102	.988	5.608	.0
.901	-.100	1.480	.901	.0	5.720	-.102	.989	5.720	.0
.979	-.100	1.485	.979	.0	5.802	-.102	.989	5.802	.0
1.105	-.100	1.481	1.105	.0	5.997	-.102	.990	5.997	.0
1.211	-.108	1.481	1.211	-.3	6.108	-.102	.991	6.108	.0
1.316	-.100	1.476	1.316	.0	6.220	-.102	.991	6.220	.0
1.401	-.101	1.476	1.401	.0	6.302	-.102	.991	6.302	.0
1.479	-.101	1.486	1.479	.0					
1.605	-.101	1.489	1.605	.0	-.002	-.069	1.493	.000	7.7
1.711	-.111	1.492	1.711	-.3	.102	-.056	1.492	.105	7.6
1.816	-.101	1.445	1.816	.0	.207	-.038	1.492	.212	8.1
1.901	-.101	1.361	1.901	.0	.395	-.017	1.488	.400	7.6
1.979	-.101	1.208	1.979	.0	.493	-.002	1.487	.500	7.7
2.105	-.101	1.008	2.105	.0	.598	.011	1.486	.605	7.6
2.211	-.114	.856	2.211	-.3	.702	.032	1.483	.712	8.1
2.316	-.101	.759	2.316	.0	.890	.049	1.481	.900	7.6
2.401	-.101	.727	2.401	.0	.989	.065	1.483	1.000	7.7
2.479	-.101	.729	2.479	.0	1.093	.077	1.485	1.105	7.6
2.605	-.101	.770	2.605	.0	1.197	.103	1.486	1.212	8.1
2.711	-.117	.825	2.711	-.3	1.386	.116	1.487	1.400	7.6
2.816	-.101	.876	2.816	.0	1.484	.131	1.495	1.500	7.7
2.901	-.101	.911	2.901	.0	1.589	.143	1.503	1.605	7.6
2.979	-.101	.944	2.979	.0	1.692	.173	1.508	1.712	8.1
3.105	-.101	.975	3.105	.0	1.882	.182	1.462	1.900	7.6
3.211	-.120	.990	3.211	-.3	1.980	.198	1.320	2.000	7.7
3.316	-.101	.993	3.316	.0	2.085	.209	1.144	2.105	7.6
3.401	-.101	.993	3.401	.0	2.187	.243	.960	2.212	8.1
3.497	-.101	.990	3.497	.0	2.377	.248	.783	2.400	7.6
3.608	-.101	.991	3.608	.0	2.475	.265	.747	2.500	7.7
3.720	-.101	.991	3.720	.0	2.580	.276	.766	2.605	7.6
3.802	-.101	.992	3.802	.0	2.682	.313	.812	2.712	8.1
3.997	-.101	.991	3.997	.0	2.873	.314	.891	2.900	7.6
4.108	-.101	.991	4.108	.0	2.969	.354	.928	3.001	8.1
4.220	-.101	.991	4.220	.0	3.078	.376	.963	3.112	8.2
4.302	-.101	.993	4.302	.0	3.183	.392	.984	3.218	8.2
4.497	-.102	.993	4.497	.0	3.275	.340	.989	3.303	7.2
					3.368	.380	.994	3.400	7.6

TABLE 14.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
3.464	.424	.993	3.501	8.1
3.573	.447	.991	3.612	8.2
3.678	.463	.993	3.718	8.2
3.771	.402	.992	3.803	7.2
3.959	.494	.992	4.001	8.1
4.068	.518	.993	4.112	8.2
4.173	.535	.991	4.218	8.2
4.268	.464	.992	4.303	7.2
4.454	.565	.995	4.501	8.1
4.563	.590	.992	4.612	8.2
4.667	.606	.993	4.718	8.2
4.764	.527	.995	4.803	7.2
4.949	.635	.994	5.001	8.1
5.058	.661	.992	5.112	8.2
5.162	.678	.993	5.218	8.2
5.260	.589	.993	5.303	7.2
5.444	.705	.991	5.501	8.1
5.553	.732	.992	5.612	8.2
5.657	.749	.991	5.718	8.2
5.756	.651	.991	5.803	7.2
5.939	.775	.993	6.001	8.1
6.048	.803	.995	6.112	8.2
6.152	.820	.993	6.218	8.2
6.252	.714	.993	6.303	7.2
-.007	-.042	1.490	.000	14.5
.117	-.008	1.489	.129	14.8
.195	.015	1.489	.210	15.1
.296	.043	1.488	.316	15.2
.378	.062	1.487	.400	15.0
.477	.083	1.484	.500	14.5
.600	.120	1.485	.629	14.8
.678	.145	1.485	.710	15.1
.779	.174	1.482	.816	15.2
.861	.191	1.483	.900	15.0
.961	.209	1.482	1.000	14.5
1.084	.248	1.484	1.129	14.8
1.161	.275	1.486	1.210	15.1
1.261	.306	1.487	1.316	15.2
1.344	.320	1.490	1.400	15.0
1.445	.334	1.496	1.500	14.5
1.567	.376	1.501	1.629	14.8
1.643	.405	1.503	1.710	15.1
1.744	.437	1.501	1.816	15.2
1.828	.450	1.499	1.900	15.0
1.929	.459	1.476	2.000	14.5
2.050	.504	1.405	2.129	14.8
2.126	.536	1.323	2.210	15.1
2.226	.568	1.166	2.316	15.2
2.311	.579	1.051	2.400	15.0
2.413	.585	.951	2.500	14.5
2.534	.631	.833	2.629	14.8
2.609	.666	.813	2.710	15.1
2.709	.699	.828	2.816	15.2
2.794	.708	.855	2.900	15.0
2.914	.715	.896	3.018	14.5
3.003	.759	.934	3.116	14.9
3.109	.741	.964	3.213	14.1
3.233	.787	.988	3.344	14.4
3.277	.837	.994	3.400	15.0
3.398	.840	.994	3.518	14.5
3.487	.887	.994	3.616	14.9
3.593	.863	.994	3.713	14.1
3.717	.911	.994	3.844	14.4
3.882	.966	.993	4.018	14.5
3.970	1.016	.992	4.116	14.9
4.078	.985	.993	4.213	14.1
4.201	1.035	.994	4.344	14.4
4.366	1.091	.996	4.518	14.5
4.453	1.144	.996	4.616	14.9
4.563	1.108	.995	4.713	14.1
4.686	1.159	.995	4.844	14.4
4.850	1.217	.994	5.018	14.5
4.936	1.273	.994	5.116	14.9
5.048	1.230	.994	5.213	14.1
5.170	1.283	.994	5.344	14.4
5.334	1.342	.995	5.518	14.5
5.420	1.401	.995	5.616	14.9
5.533	1.352	.995	5.713	14.1
5.654	1.407	.994	5.844	14.4
5.818	1.468	.994	6.018	14.5
5.903	1.529	.994	6.116	14.9
6.018	1.474	.994	6.213	14.1
6.139	1.531	.995	6.344	14.4
-.034	-.009	1.486	-.014	24.9
.072	.041	1.489	.103	25.1
.169	.086	1.489	.210	25.1
.256	.131	1.489	.308	25.4
.339	.161	1.489	.396	24.6

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TABLE 14.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
.420	.202	1.487	.486	24.9	4.713	2.192	.995	5.219	24.9
.525	.253	1.493	.603	25.1	4.819	2.262	.994	5.344	25.1
.622	.298	1.494	.710	25.1	5.035	2.333	.995	5.570	24.8
.707	.345	1.494	.808	25.4	5.072	2.356	.995	5.613	24.9
.794	.369	1.495	.896	24.6	5.167	2.402	.994	5.719	24.9
.873	.412	1.492	.986	24.9	5.272	2.474	.995	5.844	25.1
.978	.465	1.492	1.103	25.1	5.489	2.543	.997	6.070	24.8
1.075	.510	1.489	1.210	25.1	5.525	2.566	.997	6.113	24.9
1.159	.559	1.483	1.308	25.4	5.621	2.612	.997	6.219	24.9
1.248	.578	1.471	1.396	24.6	5.725	2.686	.997	6.344	25.1
1.327	.623	1.428	1.486	24.9					
1.430	.677	1.396	1.603	25.1	-.039	.002	1.489	-.014	28.1
1.528	.722	1.338	1.710	25.1	.068	.054	1.492	.105	27.3
1.611	.774	1.256	1.808	25.4	.162	.101	1.490	.211	27.2
1.703	.786	1.169	1.896	24.6	.226	.135	1.489	.283	27.3
1.780	.833	1.055	1.986	24.9	.330	.187	1.487	.400	27.1
1.883	.889	.977	2.103	25.1	.402	.237	1.491	.486	28.1
1.981	.934	.912	2.210	25.1	.512	.284	1.494	.605	27.3
2.063	.988	.865	2.308	25.4	.607	.330	1.494	.711	27.2
2.157	.995	.834	2.396	24.6	.670	.364	1.495	.783	27.3
2.234	1.044	.789	2.486	24.9	.775	.415	1.494	.900	27.1
2.336	1.101	.769	2.603	25.1	.843	.472	1.490	.986	28.1
2.434	1.145	.763	2.710	25.1	.956	.513	1.489	1.105	27.3
2.514	1.202	.767	2.808	25.4	1.052	.558	1.476	1.211	27.2
2.612	1.203	.772	2.896	24.6	1.115	.593	1.464	1.283	27.3
2.687	1.255	.759	2.986	24.9	1.220	.643	1.436	1.400	27.1
2.789	1.313	.772	3.103	25.1	1.284	.707	1.368	1.486	28.1
2.887	1.357	.796	3.210	25.1	1.400	.743	1.326	1.605	27.3
2.966	1.417	.862	3.308	25.4	1.497	.787	1.237	1.711	27.2
3.007	1.415	.884	3.344	25.1	1.559	.822	1.161	1.783	27.3
3.066	1.411	.931	3.396	24.6	1.665	.871	1.041	1.900	27.1
3.220	1.494	.984	3.570	24.8	1.726	.943	.942	1.986	28.1
3.257	1.515	.990	3.613	24.9	1.844	.973	.889	2.105	27.3
3.352	1.561	.994	3.719	24.9	1.942	1.015	.847	2.211	27.2
3.460	1.627	.994	3.844	25.1	2.003	1.051	.824	2.283	27.3
3.674	1.704	.995	4.070	24.8	2.110	1.100	.795	2.400	27.1
3.711	1.725	.995	4.113	24.9	2.167	1.178	.762	2.486	28.1
3.806	1.771	.995	4.219	24.9	2.288	1.202	.721	2.605	27.3
3.913	1.839	.994	4.344	25.1	2.386	1.243	.697	2.711	27.2
4.128	1.913	.996	4.570	24.8	2.448	1.280	.695	2.783	27.3
4.164	1.936	.998	4.613	24.9	2.555	1.328	.711	2.900	27.1
4.260	1.981	.998	4.719	24.9	2.686	1.403	.735	3.050	27.3
4.366	2.051	.998	4.844	25.1	2.747	1.425	.747	3.115	27.1
4.581	2.123	.995	5.070	24.8	2.831	1.472	.788	3.211	27.2
4.618	2.146	.995	5.113	24.9	2.913	1.512	.835	3.302	27.2

TABLE 14.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
3.000	1.556	.939	3.400	27.1
3.130	1.632	.983	3.550	27.3
3.192	1.653	.991	3.615	27.1
3.269	1.692	.994	3.701	27.1
3.358	1.741	.994	3.802	27.2
3.575	1.861	.995	4.050	27.3
3.637	1.881	.995	4.115	27.1
3.714	1.920	.995	4.201	27.1
3.803	1.969	.995	4.302	27.2
4.019	2.090	.998	4.550	27.3
4.082	2.109	.997	4.615	27.1
4.159	2.148	.998	4.701	27.1
4.247	2.197	.998	4.802	27.2
4.464	2.319	.995	5.050	27.3
4.527	2.337	.994	5.115	27.1
4.604	2.376	.995	5.201	27.1
4.692	2.425	.995	5.302	27.2
4.908	2.548	.995	5.550	27.3
4.972	2.565	.995	5.615	27.1
5.049	2.604	.995	5.701	27.1
5.137	2.653	.994	5.802	27.2
5.352	2.778	.997	6.050	27.3
5.417	2.793	.997	6.115	27.1
5.494	2.832	.997	6.201	27.1
5.582	2.882	.996	6.302	27.2
-.030	.013	1.497	.000	29.5
.062	.067	1.490	.106	29.7
.152	.119	1.491	.210	29.8
.260	.181	1.492	.335	29.8
.333	.226	1.490	.421	30.1
.405	.259	1.497	.500	29.5
.496	.315	1.494	.606	29.7
.586	.368	1.495	.710	29.8
.693	.430	1.496	.835	29.8
.765	.477	1.495	.921	30.1
.841	.505	1.490	1.000	29.5
.930	.563	1.468	1.106	29.7
1.019	.617	1.449	1.210	29.8
1.127	.678	1.402	1.335	29.8
1.198	.728	1.371	1.421	30.1
1.276	.751	1.288	1.500	29.5
1.365	.811	1.189	1.606	29.7
1.453	.865	1.107	1.710	29.8
1.561	.927	.973	1.835	29.8
1.630	.979	.916	1.921	30.1
1.711	.998	.867	2.000	29.5
1.799	1.059	.827	2.106	29.7
1.887	1.114	.820	2.210	29.8
1.995	1.176	.806	2.335	29.8
2.063	1.230	.787	2.421	30.1
2.146	1.244	.762	2.500	29.5
2.233	1.307	.703	2.606	29.7
2.321	1.363	.670	2.710	29.8
2.428	1.425	.660	2.835	29.8
2.496	1.481	.675	2.921	30.1
2.595	1.526	.702	3.030	29.9
2.666	1.570	.731	3.113	30.0
2.741	1.613	.790	3.199	30.0
2.825	1.673	.868	3.302	30.1
2.928	1.731	.969	3.421	30.1
3.029	1.776	.984	3.530	29.9
3.099	1.819	.993	3.613	30.0
3.174	1.862	.994	3.699	30.0
3.258	1.924	.994	3.802	30.1
3.462	2.025	.995	4.030	29.9
3.533	2.069	.994	4.113	30.0
3.607	2.112	.995	4.199	30.0
3.690	2.175	.995	4.302	30.1
3.896	2.275	.998	4.530	29.9
3.966	2.319	.997	4.613	30.0
4.040	2.362	.998	4.699	30.0
4.122	2.426	.998	4.802	30.1
4.329	2.524	.995	5.030	29.9
4.399	2.568	.995	5.113	30.0
4.474	2.611	.996	5.199	30.0
4.555	2.677	.994	5.302	30.1
4.762	2.773	.994	5.530	29.9
4.832	2.818	.994	5.613	30.0
4.907	2.861	.994	5.699	30.0
4.987	2.928	.994	5.802	30.1
5.196	3.023	.997	6.030	29.9
5.265	3.068	.996	6.113	30.0
5.340	3.111	.997	6.199	30.0
5.420	3.179	.997	6.302	30.1
-.048	.041	1.491	.000	37.7
.037	.104	1.502	.106	37.4
.122	.167	1.504	.212	37.2
.204	.231	1.506	.316	37.3

TABLE 14.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
.273	.284	1.504	.403	37.4	4.133	3.129	.995	5.198	36.5
.348	.346	1.494	.500	37.7	4.237	3.199	.995	5.323	36.5
.434	.407	1.507	.606	37.4	4.379	3.353	.994	5.529	36.8
.520	.469	1.503	.712	37.2	4.483	3.390	.994	5.635	36.5
.602	.534	1.497	.816	37.3	4.535	3.427	.994	5.698	36.5
.671	.587	1.481	.903	37.4	4.639	3.497	.994	5.823	36.5
.744	.652	1.418	1.000	37.7	4.779	3.653	.997	6.029	36.8
.832	.711	1.365	1.106	37.4	4.885	3.688	.997	6.135	36.5
.918	.772	1.277	1.212	37.2	4.937	3.724	.996	6.198	36.5
.999	.837	1.193	1.316	37.3	5.041	3.794	.996	6.323	36.5
1.068	.891	1.110	1.403	37.4					
1.139	.957	.970	1.500	37.7	-.067	.062	1.485	.000	44.8
1.229	1.014	.886	1.606	37.4	.014	.142	1.485	.114	44.8
1.316	1.074	.821	1.712	37.2	.082	.210	1.486	.210	44.8
1.397	1.140	.792	1.816	37.3	.153	.281	1.485	.310	44.8
1.465	1.194	.789	1.903	37.4	.229	.355	1.485	.416	44.8
1.535	1.263	.793	2.000	37.7	.288	.414	1.485	.500	44.8
1.627	1.317	.822	2.106	37.4	.368	.495	1.475	.614	44.8
1.715	1.376	.848	2.212	37.2	.437	.563	1.456	.710	44.8
1.795	1.443	.865	2.316	37.3	.508	.633	1.411	.810	44.8
1.863	1.498	.866	2.403	37.4	.583	.707	1.328	.916	44.8
1.931	1.568	.874	2.500	37.7	.643	.766	1.217	1.000	44.8
2.024	1.621	.875	2.606	37.4	.723	.847	1.095	1.114	44.8
2.113	1.679	.874	2.712	37.2	.792	.915	.990	1.210	44.8
2.193	1.746	.886	2.816	37.3	.863	.985	.890	1.310	44.8
2.260	1.801	.899	2.903	37.4	.938	1.060	.797	1.416	44.8
2.327	1.874	.935	3.000	37.7	.998	1.118	.753	1.500	44.8
2.422	1.924	.961	3.106	37.4	1.078	1.200	.735	1.614	44.8
2.525	1.939	.974	3.198	36.5	1.146	1.268	.743	1.710	44.8
2.590	2.049	.993	3.316	37.3	1.218	1.337	.765	1.810	44.8
2.658	2.104	.994	3.403	37.4	1.293	1.412	.803	1.916	44.8
2.778	2.154	.994	3.529	36.8	1.353	1.470	.833	2.000	44.8
2.876	2.200	.994	3.635	36.5	1.432	1.552	.871	2.114	44.8
2.927	2.237	.994	3.698	36.5	1.501	1.620	.901	2.210	44.8
3.030	2.308	.993	3.823	36.5	1.573	1.689	.923	2.310	44.8
3.178	2.453	.995	4.029	36.8	1.648	1.764	.945	2.416	44.8
3.277	2.498	.995	4.135	36.5	1.708	1.823	.958	2.500	44.8
3.329	2.534	.995	4.198	36.5	1.787	1.905	.966	2.614	44.8
3.432	2.605	.995	4.323	36.5	1.856	1.973	.974	2.710	44.8
3.579	2.753	.998	4.529	36.8	1.928	2.042	.979	2.810	44.8
3.679	2.795	.996	4.635	36.5	2.003	2.116	.986	2.916	44.8
3.731	2.832	.998	4.698	36.5	2.063	2.175	.993	3.000	44.8
3.835	2.902	.997	4.823	36.5	2.202	2.317	.993	3.198	44.8
3.979	3.053	.994	5.029	36.8	2.308	2.374	.992	3.314	44.3
4.081	3.093	.994	5.135	36.5	2.358	2.468	.995	3.416	44.8

TABLE 14.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
2.453	2.526	.994	3.524	44.4
2.556	2.669	.995	3.698	44.8
2.666	2.723	.994	3.814	44.3
2.811	2.875	.995	4.024	44.4
2.911	3.022	.994	4.198	44.8
3.024	3.072	.995	4.314	44.3
3.168	3.225	.998	4.524	44.4
3.266	3.374	.997	4.698	44.8
3.382	3.421	.998	4.814	44.3
3.525	3.575	.996	5.024	44.4
3.620	3.727	.996	5.198	44.8
3.740	3.770	.994	5.314	44.3
3.883	3.925	.994	5.524	44.4
3.975	4.079	.994	5.698	44.8
4.098	4.119	.995	5.814	44.3
4.240	4.274	.996	6.024	44.4
4.330	4.431	.996	6.198	44.8
4.456	4.468	.996	6.314	44.3
-.116	.103	1.492	.003	60.6
-.059	.214	1.491	.128	61.3
-.022	.281	1.492	.204	61.3
.032	.379	1.487	.316	61.3
.079	.466	1.482	.415	61.3
.129	.539	1.466	.503	60.6
.181	.652	1.410	.628	61.3
.218	.719	1.361	.704	61.3
.271	.817	1.225	.816	61.3
.319	.905	1.118	.915	61.3
.374	.974	.969	1.003	60.6
.421	1.091	.842	1.128	61.3
.458	1.158	.789	1.204	61.3
.511	1.256	.719	1.316	61.3
.559	1.343	.695	1.415	61.3
.619	1.410	.693	1.503	60.6
.661	1.530	.720	1.628	61.3
.697	1.597	.741	1.704	61.3
.751	1.695	.789	1.816	61.3
.799	1.782	.823	1.915	61.3
.865	1.846	.871	2.003	60.6
.901	1.969	.921	2.128	61.3
.937	2.036	.943	2.204	61.3
.991	2.134	.971	2.316	61.3
1.038	2.221	.981	2.415	61.3
1.110	2.282	.987	2.503	60.6
1.140	2.407	.991	2.628	61.3
1.177	2.474	.991	2.704	61.3
1.231	2.572	.994	2.816	61.3
1.278	2.660	.994	2.915	61.3
1.355	2.717	.993	3.003	60.6
1.380	2.846	.993	3.128	61.3
1.417	2.913	.994	3.204	61.3
1.470	3.011	.995	3.316	61.3
1.518	3.098	.995	3.415	61.3
1.653	3.143	.994	3.520	59.9
1.747	3.195	.994	3.612	59.0
1.804	3.284	.993	3.718	59.0
1.844	3.357	.993	3.802	59.0
1.904	3.576	.995	4.020	59.9
2.004	3.624	.995	4.112	59.0
2.062	3.712	.995	4.218	59.0
2.101	3.786	.994	4.302	59.0
2.155	4.008	.998	4.520	59.9
2.261	4.052	.995	4.612	59.0
2.320	4.141	.998	4.718	59.0
2.359	4.215	.997	4.802	59.0
2.406	4.441	.994	5.020	59.9
2.518	4.481	.994	5.112	59.0
2.577	4.569	.995	5.218	59.0
2.616	4.643	.994	5.302	59.0
2.657	4.873	.994	5.520	59.9
2.776	4.910	.994	5.612	59.0
2.835	4.998	.994	5.718	59.0
2.873	5.072	.993	5.802	59.0
2.908	5.306	.997	6.020	59.9
3.033	5.339	.997	6.112	59.0
3.093	5.426	.996	6.218	59.0
3.130	5.501	.996	6.302	59.0
-.172	.121	1.492	-.002	75.3
-.145	.224	1.490	.105	75.3
-.118	.325	1.493	.210	75.3
-.096	.405	1.488	.292	75.2
-.062	.529	1.456	.421	75.0
-.046	.604	1.441	.498	75.3
-.019	.708	1.350	.605	75.3
.009	.809	1.237	.710	75.3
.032	.888	1.115	.792	75.2
.068	1.011	.937	.921	75.0
.081	1.088	.870	.998	75.3

TABLE 14.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
.108	1.192	.769	1.105	75.3
.136	1.292	.711	1.210	75.3
.160	1.372	.678	1.292	75.2
.197	1.494	.667	1.421	75.0
.207	1.572	.678	1.498	75.3
.235	1.675	.702	1.605	75.3
.263	1.776	.734	1.710	75.3
.288	1.855	.771	1.792	75.2
.326	1.977	.843	1.921	75.0
.334	2.055	.869	1.998	75.3
.361	2.159	.919	2.105	75.3
.391	2.259	.951	2.210	75.3
.416	2.338	.968	2.292	75.2
.456	2.460	.982	2.421	75.0
.461	2.539	.984	2.498	75.3
.488	2.643	.987	2.605	75.3
.518	2.743	.987	2.710	75.3
.544	2.822	.987	2.792	75.2
.585	2.943	.987	2.921	75.0
.592	3.032	.984	3.008	75.3
.614	3.130	.984	3.108	75.4
.645	3.227	.988	3.210	75.3
.662	3.317	.984	3.302	75.4
.715	3.426	.988	3.421	75.0
.719	3.516	.986	3.508	75.3
.740	3.614	.986	3.608	75.4
.762	3.700	.987	3.697	75.4
.788	3.801	.987	3.802	75.4
.846	4.000	.988	4.008	75.3
.867	4.097	.988	4.108	75.4
.888	4.184	.989	4.197	75.4
.914	4.285	.989	4.302	75.4
.972	4.483	.992	4.508	75.3
.993	4.581	.993	4.608	75.4
1.014	4.667	.992	4.697	75.4
1.041	4.769	.991	4.802	75.4
1.099	4.967	.992	5.008	75.3
1.120	5.065	.992	5.108	75.4
1.140	5.151	.993	5.197	75.4
1.167	5.252	.993	5.302	75.4
1.226	5.451	.991	5.508	75.3
1.246	5.549	.991	5.608	75.4
1.267	5.635	.992	5.697	75.4
1.293	5.736	.993	5.802	75.4
1.353	5.934	.993	6.008	75.3
1.372	6.032	.993	6.108	75.4
1.393	6.119	.994	6.197	75.4
1.419	6.220	.993	6.302	75.4
-.229	.130	1.493	.000	89.8
-.229	.233	1.494	.103	89.8
-.235	.340	1.495	.210	90.7
-.234	.424	1.486	.294	90.5
-.234	.531	1.458	.401	90.4
-.228	.630	1.411	.500	89.8
-.227	.733	1.309	.603	89.8
-.241	.840	1.159	.710	90.7
-.238	.924	1.013	.794	90.5
-.237	1.031	.893	.901	90.4
-.227	1.130	.796	1.000	89.8
-.226	1.233	.728	1.103	89.8
-.247	1.340	.688	1.210	90.7
-.242	1.424	.675	1.294	90.5
-.240	1.531	.683	1.401	90.4
-.225	1.630	.711	1.500	89.8
-.224	1.733	.742	1.603	89.8
-.253	1.840	.786	1.710	90.7
-.246	1.924	.836	1.794	90.5
-.244	2.031	.885	1.901	90.4
-.224	2.130	.922	2.000	89.8
-.222	2.233	.953	2.103	89.8
-.259	2.340	.971	2.210	90.7
-.250	2.424	.979	2.294	90.5
-.247	2.531	.983	2.401	90.4
-.223	2.630	.986	2.500	89.8
-.221	2.733	.987	2.603	89.8
-.265	2.839	.987	2.710	90.7
-.254	2.924	.986	2.794	90.5
-.250	3.031	.987	2.901	90.4
-.221	3.130	.987	3.000	89.8
-.219	3.233	.987	3.103	89.8
-.271	3.339	.989	3.210	90.7
-.258	3.424	.988	3.294	90.5
-.253	3.531	.988	3.401	90.4
-.208	3.660	.986	3.530	89.7
-.207	3.849	.986	3.719	89.7
-.206	3.932	.986	3.802	89.7
-.205	4.160	.987	4.030	89.7
-.204	4.349	.988	4.219	89.7
-.203	4.432	.988	4.302	89.7
-.202	4.660	.990	4.530	89.7

TABLE 14.- Concluded

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
-.201	4.849	.991	4.719	89.7
-.200	4.932	.992	4.802	89.7
-.199	5.160	.990	5.030	89.7
-.198	5.349	.990	5.219	89.7
-.197	5.432	.990	5.302	89.7
-.196	5.660	.990	5.530	89.7
-.195	5.849	.991	5.719	89.7
-.195	5.932	.990	5.802	89.7
-.193	6.160	.992	6.030	89.7
-.192	6.349	.993	6.219	89.7
-.192	6.432	.993	6.302	89.7

TABLE 15.- PITOT-PRESSURE MEASUREMENTS AT $x = 7.743$ in. FOR $M_\infty = 1.20$ WITH NPR = 3.99 AND $T_{t,j}/T_{t,\infty} = 0.87$

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
-.022	-.098	1.523	-.022	.7
.082	-.094	1.530	.082	1.1
.188	-.091	1.523	.188	1.2
.273	-.090	1.527	.273	1.2
.399	-.086	1.528	.400	1.3
.478	-.092	1.524	.478	.7
.582	-.084	1.527	.582	1.1
.688	-.081	1.522	.688	1.2
.773	-.079	1.524	.773	1.2
.899	-.075	1.525	.900	1.3
.978	-.086	1.526	.978	.7
1.082	-.074	1.530	1.082	1.1
1.188	-.070	1.525	1.188	1.2
1.272	-.069	1.528	1.273	1.2
1.399	-.064	1.529	1.400	1.3
1.478	-.080	1.528	1.478	.7
1.582	-.064	1.528	1.582	1.1
1.688	-.060	1.501	1.688	1.2
1.772	-.059	1.435	1.773	1.2
1.899	-.053	1.318	1.900	1.3
1.977	-.074	1.171	1.978	.7
2.082	-.054	1.049	2.082	1.1
2.187	-.049	.934	2.188	1.2
2.272	-.048	.842	2.273	1.2
2.399	-.042	.785	2.400	1.3
2.477	-.068	.768	2.478	.7
2.582	-.044	.778	2.582	1.1
2.687	-.039	.808	2.688	1.2
2.772	-.038	.852	2.773	1.2
2.899	-.032	.896	2.900	1.3
2.967	-.095	.918	2.967	.1
3.083	-.122	.950	3.083	-.4
3.172	-.134	.970	3.172	-.6
3.266	-.152	.985	3.266	-.8
3.399	-.021	.994	3.400	1.3
3.467	-.094	.991	3.467	.1
3.583	-.126	.991	3.583	-.4
3.672	-.139	.991	3.672	-.6
3.766	-.159	.991	3.766	-.8
3.967	-.093	.992	3.967	.1
4.083	-.129	.991	4.083	-.4
4.172	-.144	.991	4.172	-.6
4.266	-.167	.991	4.266	-.8
4.467	-.092	.990	4.467	.1
4.583	-.133	.990	4.583	-.4
4.672	-.149	.990	4.672	-.6
4.766	-.174	.990	4.766	-.8
4.967	-.092	.989	4.967	.1
5.083	-.136	.989	5.083	-.4
5.172	-.154	.989	5.172	-.6
5.266	-.181	.989	5.266	-.8
5.467	-.091	.990	5.467	.1
5.583	-.139	.990	5.583	-.4
5.672	-.159	.990	5.672	-.6
5.766	-.189	.990	5.766	-.8
5.967	-.090	.990	5.967	.1
6.083	-.143	.991	6.083	-.4
6.172	-.164	.991	6.172	-.6
6.266	-.196	.991	6.266	-.8
-.024	-.070	1.523	-.022	8.3
.080	-.055	1.523	.083	8.3
.188	-.039	1.522	.193	8.3
.290	-.024	1.522	.295	8.3
.371	-.012	1.523	.378	8.3
.471	.003	1.525	.478	8.3
.575	.018	1.524	.583	8.3
.683	.034	1.522	.693	8.3
.784	.049	1.517	.795	8.3
.866	.061	1.517	.878	8.3
.966	.075	1.519	.978	8.3
1.070	.090	1.517	1.083	8.3
1.178	.106	1.519	1.193	8.3
1.279	.121	1.517	1.295	8.3
1.361	.133	1.517	1.378	8.3
1.460	.148	1.517	1.478	8.3
1.564	.163	1.517	1.583	8.3
1.672	.179	1.514	1.693	8.3
1.774	.194	1.500	1.795	8.3
1.856	.206	1.477	1.878	8.3
1.955	.220	1.401	1.978	8.3
2.059	.235	1.302	2.083	8.3
2.167	.251	1.161	2.193	8.3
2.268	.266	1.047	2.295	8.3
2.350	.278	.982	2.378	8.3
2.450	.293	.916	2.478	8.3
2.554	.308	.858	2.583	8.3
2.662	.324	.838	2.693	8.3
2.763	.338	.848	2.795	8.3

TABLE 15.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r,in.	ϕ, deg
2.845	.350	.868	2.878	8.3
2.933	.357	.894	2.966	8.2
3.048	.380	.937	3.083	8.3
3.077	.384	.941	3.112	8.3
3.153	.396	.965	3.189	8.3
3.225	.413	.980	3.262	8.4
3.340	.423	.990	3.378	8.3
3.428	.429	.990	3.466	8.2
3.571	.457	.991	3.612	8.3
3.648	.468	.991	3.689	8.3
3.719	.486	.991	3.762	8.4
3.923	.500	.992	3.966	8.2
4.066	.529	.992	4.112	8.3
4.143	.541	.991	4.189	8.3
4.214	.560	.991	4.262	8.4
4.418	.572	.992	4.466	8.2
4.561	.602	.992	4.612	8.3
4.637	.613	.990	4.689	8.3
4.708	.633	.991	4.762	8.4
4.913	.643	.991	4.966	8.2
5.055	.674	.991	5.112	8.3
5.132	.686	.991	5.189	8.3
5.203	.707	.992	5.262	8.4
5.407	.715	.993	5.466	8.2
5.550	.747	.993	5.612	8.3
5.627	.758	.993	5.689	8.3
5.697	.780	.993	5.762	8.4
5.902	.786	.993	5.966	8.2
6.045	.819	.993	6.112	8.3
6.122	.831	.994	6.189	8.3
6.192	.853	.994	6.262	8.4
-.029	-.044	1.519	-.022	15.5
.072	-.017	1.518	.083	15.4
.174	.011	1.519	.189	15.4
.275	.040	1.516	.294	15.5
.366	.066	1.517	.389	15.5
.453	.089	1.511	.478	15.5
.554	.116	1.513	.583	15.4
.655	.144	1.513	.689	15.4
.757	.174	1.510	.794	15.5
.848	.200	1.506	.889	15.5
.935	.222	1.494	.978	15.5
1.036	.249	1.492	1.083	15.4
1.137	.278	1.489	1.189	15.4

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
1.238	.307	1.487	1.294	15.5
1.330	.333	1.481	1.389	15.5
1.416	.356	1.448	1.478	15.5
1.518	.382	1.435	1.583	15.4
1.619	.411	1.409	1.689	15.4
1.720	.441	1.387	1.794	15.5
1.812	.467	1.363	1.889	15.5
1.898	.489	1.299	1.978	15.5
2.000	.515	1.271	2.083	15.4
2.101	.544	1.230	2.189	15.4
2.202	.575	1.193	2.294	15.5
2.294	.601	1.154	2.389	15.5
2.380	.622	1.075	2.478	15.5
2.482	.648	1.042	2.583	15.4
2.583	.677	.995	2.689	15.4
2.684	.708	.940	2.794	15.5
2.775	.735	.892	2.889	15.5
2.852	.816	.855	2.985	16.6
2.964	.781	.847	3.083	15.4
3.065	.810	.860	3.189	15.4
3.165	.842	.895	3.294	15.5
3.257	.869	.937	3.389	15.5
3.331	.959	.969	3.485	16.6
3.533	1.021	.990	3.697	16.6
3.617	1.046	.991	3.784	16.6
3.810	1.101	.992	3.985	16.6
4.012	1.164	.992	4.197	16.6
4.096	1.189	.992	4.284	16.6
4.290	1.244	.993	4.485	16.6
4.491	1.307	.993	4.697	16.6
4.575	1.332	.993	4.784	16.6
4.769	1.386	.992	4.985	16.6
4.971	1.450	.992	5.197	16.6
5.054	1.475	.992	5.284	16.6
5.248	1.529	.993	5.485	16.6
5.450	1.593	.993	5.697	16.6
5.534	1.618	.993	5.784	16.6
5.727	1.671	.994	5.985	16.6
5.929	1.735	.993	6.197	16.6
6.013	1.760	.993	6.284	16.6
-.042	-.008	1.523	-.020	26.0
.052	.038	1.522	.083	26.0
.147	.084	1.516	.189	26.0
.242	.119	1.514	.290	24.9

TABLE 15.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
.322	.156	1.509	.378	24.9
.408	.211	1.498	.480	26.0
.501	.257	1.491	.583	26.0
.596	.304	1.477	.689	26.0
.696	.329	1.473	.790	24.9
.775	.366	1.457	.878	24.9
.857	.430	1.388	.980	26.0
.950	.477	1.359	1.083	26.0
1.045	.523	1.315	1.189	26.0
1.150	.539	1.311	1.290	24.9
1.229	.576	1.264	1.378	24.9
1.307	.649	1.121	1.480	26.0
1.399	.696	1.067	1.583	26.0
1.495	.742	1.005	1.689	26.0
1.603	.749	.997	1.790	24.9
1.683	.786	.951	1.878	24.9
1.756	.868	.887	1.980	26.0
1.849	.915	.871	2.083	26.0
1.944	.962	.857	2.189	26.0
2.057	.959	.853	2.290	24.9
2.136	.996	.832	2.378	24.9
2.206	1.087	.801	2.480	26.0
2.298	1.135	.765	2.583	26.0
2.393	1.181	.735	2.689	26.0
2.511	1.170	.733	2.790	24.9
2.590	1.206	.742	2.878	24.9
2.655	1.306	.738	2.980	26.0
2.747	1.354	.759	3.083	26.0
2.835	1.397	.786	3.181	26.0
2.897	1.503	.811	3.284	27.1
3.044	1.417	.855	3.378	24.9
3.161	1.471	.913	3.507	24.9
3.284	1.617	.976	3.681	26.0
3.342	1.731	.988	3.784	27.1
3.614	1.681	.991	4.007	24.9
3.733	1.836	.992	4.181	26.0
3.787	1.959	.991	4.284	27.1
4.068	1.891	.990	4.507	24.9
4.183	2.056	.993	4.681	26.0
4.232	2.187	.991	4.784	27.1
4.522	2.101	.992	5.007	24.9
4.632	2.275	.992	5.181	26.0
4.677	2.416	.992	5.284	27.1
4.975	2.311	.994	5.507	24.9
5.081	2.494	.994	5.681	26.0
5.122	2.644	.994	5.784	27.1
5.429	2.522	.994	6.007	24.9
5.530	2.714	.994	6.181	26.0
5.567	2.872	.994	6.284	27.1
-.047	.000	1.524	-.021	28.7
.043	.053	1.520	.083	29.3
.134	.106	1.516	.188	29.5
.217	.154	1.508	.285	29.6
.304	.190	1.504	.378	28.5
.392	.240	1.494	.479	28.7
.479	.297	1.481	.583	29.3
.569	.352	1.466	.688	29.5
.652	.401	1.440	.785	29.6
.743	.429	1.416	.878	28.5
.831	.480	1.348	.979	28.7
.915	.542	1.304	1.083	29.3
1.005	.597	1.253	1.188	29.5
1.087	.648	1.190	1.285	29.6
1.183	.668	1.139	1.378	28.5
1.269	.720	1.036	1.479	28.7
1.351	.786	.983	1.583	29.3
1.440	.843	.931	1.688	29.5
1.522	.895	.891	1.785	29.6
1.622	.907	.869	1.878	28.5
1.708	.960	.854	1.979	28.7
1.788	1.031	.853	2.083	29.3
1.875	1.089	.857	2.188	29.5
1.957	1.142	.856	2.285	29.6
2.061	1.145	.843	2.378	28.5
2.147	1.200	.830	2.479	28.7
2.224	1.275	.800	2.583	29.3
2.311	1.335	.764	2.688	29.5
2.391	1.389	.741	2.785	29.6
2.501	1.384	.740	2.878	28.5
2.570	1.464	.753	2.978	29.2
2.652	1.554	.783	3.093	29.9
2.746	1.581	.824	3.188	29.5
2.826	1.636	.880	3.285	29.6
2.940	1.623	.917	3.378	28.5
3.007	1.708	.942	3.478	29.2
3.086	1.803	.976	3.593	29.9
3.144	1.908	.987	3.696	30.8
3.265	1.866	.988	3.780	29.4
3.444	1.952	.991	3.978	29.2

TABLE 15.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
3.519	2.052	.991	4.093	29.9
3.574	2.163	.991	4.196	30.8
3.701	2.111	.991	4.280	29.4
3.880	2.196	.993	4.478	29.2
3.953	2.301	.990	4.593	29.9
4.003	2.419	.992	4.696	30.8
4.137	2.356	.990	4.780	29.4
4.317	2.440	.992	4.978	29.2
4.387	2.550	.991	5.093	29.9
4.433	2.675	.992	5.196	30.8
4.573	2.601	.992	5.280	29.4
4.753	2.684	.993	5.478	29.2
4.820	2.798	.993	5.593	29.9
4.863	2.930	.993	5.696	30.8
5.008	2.846	.994	5.780	29.4
5.190	2.927	.994	5.978	29.2
5.254	3.047	.994	6.093	29.9
5.292	3.186	.994	6.196	30.8
5.444	3.091	.994	6.280	29.4
-.050	.007	1.524	-.021	30.8
.025	.054	1.521	.068	31.1
.127	.119	1.521	.189	31.5
.207	.162	1.513	.280	31.0
.308	.224	1.506	.398	31.0
.379	.263	1.498	.479	30.8
.454	.312	1.486	.568	31.1
.553	.380	1.466	.689	31.5
.636	.420	1.439	.780	31.0
.737	.481	1.403	.898	31.0
.809	.518	1.343	.979	30.8
.882	.571	1.299	1.068	31.1
.980	.641	1.237	1.189	31.5
1.065	.677	1.176	1.280	31.0
1.165	.739	1.104	1.398	31.0
1.239	.774	1.022	1.479	30.8
1.310	.829	.972	1.568	31.1
1.406	.902	.915	1.689	31.5
1.493	.935	.877	1.780	31.0
1.594	.997	.855	1.898	31.0
1.668	1.030	.847	1.979	30.8
1.738	1.087	.848	2.068	31.1
1.833	1.163	.856	2.189	31.5
1.922	1.192	.859	2.280	31.0
2.023	1.254	.852	2.398	31.0

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
2.098	1.285	.849	2.479	30.8
2.166	1.346	.823	2.568	31.1
2.259	1.424	.790	2.689	31.5
2.351	1.449	.771	2.780	31.0
2.451	1.512	.762	2.898	31.0
2.503	1.595	.768	2.986	31.8
2.601	1.656	.792	3.101	31.8
2.688	1.700	.834	3.199	31.7
2.756	1.745	.867	3.280	31.7
2.880	1.769	.940	3.398	31.0
2.928	1.859	.953	3.486	31.8
3.026	1.919	.978	3.601	31.8
3.114	1.962	.988	3.699	31.7
3.181	2.008	.989	3.780	31.7
3.353	2.122	.991	3.986	31.8
3.451	2.183	.991	4.101	31.8
3.540	2.224	.990	4.199	31.7
3.607	2.271	.992	4.280	31.7
3.778	2.386	.992	4.486	31.8
3.876	2.446	.990	4.601	31.8
3.965	2.487	.990	4.699	31.7
4.032	2.534	.992	4.780	31.7
4.203	2.649	.992	4.986	31.8
4.301	2.710	.992	5.101	31.8
4.391	2.749	.992	5.199	31.7
4.457	2.797	.992	5.280	31.7
4.628	2.913	.994	5.486	31.8
4.726	2.974	.994	5.601	31.8
4.816	3.012	.994	5.699	31.7
4.883	3.060	.994	5.780	31.7
5.053	3.176	.994	5.986	31.8
5.151	3.237	.994	6.101	31.8
5.242	3.274	.994	6.199	31.7
5.308	3.322	.994	6.280	31.7
-.055	.039	1.527	-.007	38.3
.010	.090	1.530	.076	38.3
.094	.157	1.530	.183	38.4
.186	.229	1.517	.300	38.3
.255	.284	1.507	.388	38.3
.338	.349	1.489	.493	38.3
.402	.400	1.471	.576	38.3
.486	.467	1.445	.683	38.4
.578	.539	1.392	.800	38.3
.647	.594	1.353	.888	38.3

TABLE 15.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
.730	.659	1.250	.993	38.3	-.085	.047	1.526	-.024	45.5
.795	.710	1.196	1.076	38.3	-.014	.120	1.526	.078	45.6
.878	.777	1.128	1.183	38.4	.060	.195	1.525	.184	45.5
.970	.849	1.034	1.300	38.3	.134	.270	1.515	.289	45.5
1.039	.904	.978	1.388	38.3	.208	.345	1.488	.394	45.5
1.122	.969	.890	1.493	38.3	.265	.403	1.467	.476	45.5
1.187	1.020	.856	1.576	38.3	.336	.477	1.435	.578	45.6
1.270	1.088	.830	1.683	38.4	.411	.552	1.389	.684	45.5
1.363	1.159	.820	1.800	38.3	.484	.626	1.327	.789	45.5
1.432	1.214	.820	1.888	38.3	.558	.702	1.234	.894	45.5
1.514	1.279	.844	1.993	38.3	.616	.760	1.147	.976	45.5
1.579	1.330	.864	2.076	38.3	.686	.834	1.077	1.078	45.6
1.662	1.398	.888	2.183	38.4	.762	.908	1.001	1.184	45.5
1.755	1.469	.909	2.300	38.3	.835	.983	.925	1.289	45.5
1.824	1.524	.916	2.388	38.3	.909	1.058	.852	1.394	45.5
1.907	1.589	.927	2.493	38.3	.967	1.116	.813	1.476	45.5
1.971	1.641	.931	2.576	38.3	1.036	1.191	.792	1.578	45.6
2.054	1.709	.934	2.683	38.4	1.112	1.265	.788	1.684	45.5
2.147	1.780	.943	2.800	38.3	1.186	1.339	.798	1.789	45.5
2.216	1.834	.948	2.888	38.3	1.260	1.414	.830	1.894	45.5
2.289	1.890	.957	2.980	38.3	1.318	1.472	.855	1.976	45.5
2.372	1.960	.971	3.089	38.4	1.386	1.548	.885	2.078	45.6
2.453	2.022	.981	3.191	38.3	1.463	1.621	.917	2.184	45.5
2.537	2.085	.985	3.296	38.3	1.536	1.695	.944	2.289	45.5
2.681	2.200	.990	3.480	38.3	1.610	1.771	.966	2.394	45.5
2.764	2.271	.991	3.589	38.4	1.668	1.829	.976	2.476	45.5
2.845	2.332	.991	3.691	38.3	1.736	1.905	.980	2.578	45.6
2.929	2.395	.991	3.796	38.3	1.813	1.977	.985	2.684	45.5
3.073	2.510	.987	3.980	38.3	1.887	2.052	.987	2.789	45.5
3.156	2.581	.987	4.089	38.4	1.961	2.127	.990	2.894	45.5
3.238	2.642	.987	4.191	38.3	2.010	2.200	.988	2.980	45.7
3.322	2.705	.987	4.296	38.3	2.092	2.267	.990	3.086	45.5
3.466	2.820	.991	4.480	38.3	2.146	2.358	.991	3.189	46.0
3.548	2.891	.992	4.589	38.4	2.230	2.426	.992	3.296	45.8
3.630	2.952	.990	4.691	38.3	2.359	2.558	.991	3.480	45.7
3.714	3.015	.990	4.796	38.3	2.442	2.624	.991	3.586	45.5
3.858	3.130	.990	4.980	38.3	2.494	2.717	.992	3.689	46.0
3.940	3.202	.991	5.089	38.4	2.578	2.785	.991	3.796	45.8
4.022	3.262	.991	5.191	38.3	2.708	2.916	.987	3.980	45.7
4.107	3.325	.990	5.296	38.3	2.792	2.980	.987	4.086	45.5
4.250	3.440	.991	5.480	38.3	2.841	3.077	.988	4.189	46.0
4.332	3.512	.992	5.589	38.4	2.927	3.143	.987	4.296	45.8
4.414	3.572	.992	5.691	38.3	3.057	3.274	.991	4.480	45.7
4.499	3.635	.992	5.796	38.3	3.143	3.337	.990	4.586	45.5
					3.189	3.436	.991	4.689	46.0

TABLE 15.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
3.276	3.501	.991	4.796	45.8
3.406	3.632	.991	4.980	45.7
3.493	3.694	.990	5.086	45.5
3.536	3.796	.991	5.189	46.0
3.625	3.859	.991	5.296	45.8
3.755	3.990	.992	5.480	45.7
3.843	4.051	.992	5.586	45.5
3.884	4.155	.992	5.689	46.0
3.974	4.218	.992	5.796	45.8
-.122	.091	1.525	-.011	60.7
-.079	.170	1.523	.079	60.8
-.028	.261	1.520	.183	60.8
.024	.354	1.501	.290	60.8
.074	.444	1.472	.394	60.8
.122	.527	1.425	.489	60.7
.165	.606	1.370	.579	60.8
.216	.697	1.310	.683	60.8
.268	.790	1.218	.790	60.8
.318	.881	1.136	.894	60.8
.367	.963	1.029	.989	60.7
.409	1.042	.957	1.079	60.8
.460	1.133	.898	1.183	60.8
.512	1.226	.831	1.290	60.8
.562	1.317	.791	1.394	60.8
.612	1.399	.764	1.489	60.7
.654	1.478	.760	1.579	60.8
.705	1.570	.767	1.683	60.8
.757	1.662	.788	1.790	60.8
.806	1.754	.819	1.894	60.8
.857	1.835	.858	1.989	60.7
.898	1.915	.894	2.079	60.8
.949	2.006	.921	2.183	60.8
1.001	2.099	.948	2.290	60.8
1.050	2.190	.965	2.394	60.8
1.102	2.271	.976	2.489	60.7
1.142	2.351	.981	2.579	60.8
1.193	2.442	.984	2.683	60.8
1.245	2.535	.987	2.790	60.8
1.294	2.627	.987	2.894	60.8
1.342	2.708	.988	2.988	60.8
1.388	2.794	.990	3.086	60.8
1.442	2.886	.991	3.192	60.8
1.490	2.978	.990	3.296	60.8
1.586	3.144	.990	3.488	60.8
1.632	3.230	.990	3.586	60.8

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r,in.	ϕ, deg
1.686	3.322	.989	3.692	60.8
1.734	3.414	.988	3.796	60.8
1.831	3.581	.986	3.988	60.8
1.876	3.667	.987	4.086	60.8
1.930	3.758	.987	4.192	60.8
1.978	3.850	.987	4.296	60.8
2.075	4.017	.990	4.488	60.8
2.120	4.103	.990	4.586	60.8
2.174	4.195	.990	4.692	60.8
2.222	4.287	.990	4.796	60.8
2.319	4.453	.990	4.988	60.8
2.364	4.540	.991	5.086	60.8
2.419	4.631	.991	5.192	60.8
2.466	4.723	.991	5.296	60.8
2.563	4.890	.992	5.488	60.8
2.608	4.976	.993	5.586	60.8
2.663	5.067	.993	5.692	60.8
2.710	5.160	.992	5.796	60.8
-.181	.097	1.520	-.027	76.1
-.156	.199	1.519	.078	76.1
-.129	.310	1.509	.193	76.1
-.105	.405	1.481	.290	76.1
-.081	.505	1.437	.394	76.1
-.062	.583	1.391	.473	76.1
-.036	.684	1.322	.578	76.1
-.009	.796	1.222	.693	76.1
.014	.890	1.126	.790	76.1
.039	.991	1.041	.894	76.1
.058	1.068	.966	.973	76.1
.083	1.169	.899	1.078	76.1
.111	1.281	.829	1.193	76.1
.134	1.376	.782	1.290	76.1
.159	1.476	.755	1.394	76.1
.178	1.553	.745	1.473	76.1
.203	1.655	.745	1.578	76.1
.231	1.767	.763	1.693	76.1
.254	1.861	.790	1.790	76.1
.279	1.962	.822	1.894	76.1
.298	2.039	.849	1.973	76.1
.323	2.140	.888	2.078	76.1
.350	2.252	.922	2.193	76.1
.374	2.346	.945	2.290	76.1
.399	2.447	.960	2.394	76.1

TABLE 15.- Concluded

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
.418	2.524	.969	2.473	76.1
.443	2.626	.976	2.578	76.1
.470	2.737	.980	2.693	76.1
.494	2.832	.981	2.790	76.1
.518	2.933	.984	2.894	76.1
.544	3.035	.982	2.999	76.1
.565	3.120	.983	3.087	76.1
.590	3.222	.982	3.191	76.1
.615	3.323	.981	3.296	76.1
.664	3.521	.983	3.499	76.1
.685	3.606	.984	3.587	76.1
.710	3.707	.984	3.691	76.1
.735	3.809	.984	3.796	76.1
.783	4.006	.979	3.999	76.1
.804	4.091	.980	4.087	76.1
.829	4.193	.981	4.191	76.1
.854	4.294	.982	4.296	76.1
.903	4.492	.987	4.499	76.1
.924	4.576	.987	4.587	76.1
.949	4.678	.987	4.691	76.1
.974	4.779	.986	4.796	76.1
1.023	4.977	.988	4.999	76.1
1.044	5.062	.987	5.087	76.1
1.069	5.163	.987	5.191	76.1
1.094	5.265	.988	5.296	76.1
1.143	5.463	.990	5.499	76.1
1.164	5.547	.990	5.587	76.1
1.189	5.649	.990	5.691	76.1
1.214	5.750	.991	5.796	76.1
-.235	.104	1.521	-.026	91.4
-.238	.221	1.513	.091	91.4
-.240	.315	1.498	.185	91.4
-.243	.418	1.471	.288	91.5
-.246	.525	1.403	.395	91.4
-.247	.604	1.355	.474	91.4
-.250	.721	1.260	.591	91.4
-.252	.814	1.168	.685	91.4
-.256	.918	1.077	.788	91.5
-.258	1.025	.970	.895	91.4
-.260	1.104	.905	.974	91.4
-.263	1.221	.837	1.091	91.4
-.264	1.314	.793	1.185	91.4
-.269	1.417	.765	1.288	91.5
-.270	1.524	.750	1.395	91.4

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
-.272	1.604	.759	1.474	91.4
-.275	1.721	.777	1.591	91.4
-.276	1.814	.800	1.685	91.4
-.282	1.917	.833	1.788	91.5
-.283	2.024	.875	1.895	91.4
-.285	2.104	.901	1.974	91.4
-.288	2.221	.931	2.091	91.4
-.288	2.314	.948	2.185	91.4
-.295	2.417	.962	2.288	91.5
-.295	2.524	.973	2.395	91.4
-.297	2.604	.977	2.474	91.4
-.300	2.720	.980	2.591	91.4
-.300	2.814	.982	2.685	91.4
-.308	2.917	.982	2.788	91.5
-.308	3.024	.983	2.895	91.4
-.294	3.122	.981	2.992	91.1
-.292	3.215	.981	3.086	91.1
-.296	3.320	.981	3.191	91.1
-.298	3.417	.982	3.288	91.1
-.304	3.621	.982	3.492	91.1
-.301	3.715	.983	3.586	91.1
-.306	3.820	.984	3.691	91.1
-.308	3.917	.984	3.788	91.1
-.314	4.121	.976	3.992	91.1
-.311	4.215	.976	4.086	91.1
-.316	4.320	.975	4.191	91.1
-.317	4.417	.973	4.288	91.1
-.324	4.621	.986	4.492	91.1
-.320	4.715	.986	4.586	91.1
-.325	4.820	.986	4.691	91.1
-.327	4.917	.986	4.788	91.1
-.334	5.121	.986	4.992	91.1
-.329	5.215	.987	5.086	91.1
-.335	5.320	.987	5.191	91.1
-.337	5.417	.988	5.288	91.1
-.344	5.621	.988	5.492	91.1
-.339	5.714	.990	5.586	91.1
-.345	5.820	.990	5.691	91.1
-.346	5.917	.990	5.788	91.1

TABLE 16.- PITOT-PRESSURE MEASUREMENTS AT x = 10.270 in. FOR M_∞ = 1.20 WITH NPR = 4.02 AND $T_{t,j}/T_{t,\infty}$ = 0.89

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
.031	-.105	1.508	.031	-1.2	4.725	-.100	.986	4.725	.0
.116	-.101	1.519	.116	-.2	4.801	-.100	.986	4.801	.0
.221	-.102	1.520	.221	-.3	5.017	-.100	.985	5.017	.0
.325	-.101	1.520	.325	-.1	5.124	-.100	.984	5.124	.0
.430	-.100	1.507	.430	.0	5.225	-.100	.984	5.225	.0
.531	-.116	1.516	.531	-1.2	5.301	-.100	.984	5.301	.0
.616	-.103	1.524	.616	-.2	5.517	-.100	.987	5.517	.0
.721	-.105	1.524	.721	-.3	5.624	-.100	.987	5.624	.0
.825	-.102	1.526	.825	-.1	5.725	-.100	.987	5.725	.0
.930	-.101	1.530	.930	.0	5.801	-.100	.986	5.801	.0
1.031	-.126	1.524	1.031	-1.2					
1.116	-.105	1.534	1.116	-.2	.008	-.071	1.512	.010	7.0
1.221	-.108	1.537	1.221	-.3	.092	-.060	1.516	.094	7.0
1.325	-.103	1.538	1.325	-.1	.217	-.045	1.517	.221	7.0
1.430	-.101	1.540	1.430	.0	.321	-.032	1.516	.325	7.0
1.531	-.136	1.531	1.531	-1.2	.405	-.022	1.517	.410	7.0
1.616	-.106	1.537	1.616	-.2	.504	-.010	1.521	.510	7.0
1.721	-.111	1.510	1.721	-.3	.588	.001	1.523	.594	7.0
1.825	-.105	1.447	1.825	-.1	.714	.016	1.524	.721	7.0
1.930	-.101	1.363	1.930	.0	.817	.029	1.524	.825	7.0
2.030	-.146	1.183	2.031	-1.2	.902	.039	1.526	.910	7.0
2.116	-.108	1.127	2.116	-.2	1.001	.051	1.527	1.010	7.0
2.221	-.113	1.015	2.221	-.3	1.084	.062	1.530	1.094	7.0
2.325	-.106	.924	2.325	-.1	1.210	.077	1.531	1.221	7.0
2.430	-.100	.863	2.430	.0	1.314	.090	1.531	1.325	7.0
2.530	-.156	.815	2.531	-1.2	1.398	.100	1.531	1.410	7.0
2.616	-.110	.811	2.616	-.2	1.497	.113	1.533	1.510	7.0
2.721	-.116	.820	2.721	-.3	1.580	.123	1.535	1.594	7.0
2.825	-.107	.849	2.825	-.1	1.706	.138	1.527	1.721	7.0
2.930	-.100	.871	2.930	.0	1.810	.151	1.512	1.825	7.0
3.017	-.100	.894	3.017	.0	1.894	.161	1.479	1.910	7.0
3.124	-.100	.938	3.124	.0	1.993	.174	1.397	2.010	7.0
3.225	-.100	.961	3.225	.0	2.077	.184	1.325	2.094	7.0
3.301	-.100	.976	3.301	.0	2.202	.199	1.201	2.221	7.0
3.517	-.100	.988	3.517	.0	2.306	.212	1.113	2.325	7.0
3.624	-.100	.990	3.624	.0	2.390	.223	1.032	2.410	7.0
3.725	-.100	.988	3.725	.0	2.489	.235	.969	2.510	7.0
3.801	-.100	.989	3.801	.0	2.573	.245	.923	2.594	7.0
4.017	-.100	.984	4.017	.0	2.699	.261	.886	2.721	7.0
4.124	-.100	.983	4.124	.0	2.802	.273	.875	2.825	7.0
4.225	-.100	.983	4.225	.0	2.887	.284	.880	2.910	7.0
4.301	-.100	.981	4.301	.0	2.970	.294	.889	2.994	7.0
4.517	-.100	.988	4.517	.0	3.076	.307	.918	3.101	7.0
4.624	-.100	.986	4.624	.0	3.202	.322	.957	3.227	7.0
					3.268	.331	.970	3.294	7.0
					3.466	.355	.988	3.494	7.0

TABLE 16.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
3.573	.368	.991	3.601	7.0
3.698	.384	.990	3.727	7.0
3.764	.392	.989	3.794	7.0
3.963	.416	.983	3.994	7.0
4.069	.429	.982	4.101	7.0
4.194	.445	.980	4.227	7.0
4.261	.453	.981	4.294	7.0
4.459	.477	.989	4.494	7.0
4.565	.490	.989	4.601	7.0
4.690	.506	.988	4.727	7.0
4.757	.514	.988	4.794	7.0
4.955	.538	.987	4.994	7.0
5.061	.551	.986	5.101	7.0
5.187	.567	.986	5.227	7.0
5.253	.575	.986	5.294	7.0
5.451	.599	.987	5.494	7.0
5.558	.612	.986	5.601	7.0
5.683	.628	.987	5.727	7.0
5.749	.636	.986	5.794	7.0
.001	-.037	1.509	.010	15.2
.082	-.015	1.511	.093	15.2
.204	.018	1.513	.220	15.2
.286	.040	1.504	.304	15.2
.387	.068	1.503	.409	15.2
.484	.094	1.517	.510	15.2
.564	.116	1.518	.593	15.2
.687	.149	1.519	.720	15.2
.768	.171	1.507	.804	15.2
.870	.199	1.504	.909	15.2
.966	.225	1.497	1.010	15.2
1.047	.247	1.496	1.093	15.2
1.169	.280	1.490	1.220	15.2
1.251	.302	1.474	1.304	15.2
1.352	.330	1.461	1.409	15.2
1.449	.356	1.440	1.510	15.2
1.529	.378	1.427	1.593	15.2
1.652	.412	1.400	1.720	15.2
1.733	.434	1.364	1.804	15.2
1.835	.461	1.335	1.909	15.2
1.931	.487	1.309	2.010	15.2
2.012	.509	1.285	2.093	15.2
2.134	.543	1.236	2.220	15.2
2.216	.565	1.190	2.304	15.2
2.317	.592	1.150	2.409	15.2

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
2.414	.619	1.098	2.510	15.2
2.494	.641	1.075	2.593	15.2
2.617	.674	1.027	2.720	15.2
2.698	.696	.986	2.804	15.2
2.800	.723	.949	2.909	15.2
2.903	.752	.910	3.017	15.2
2.985	.772	.899	3.101	15.2
3.072	.798	.901	3.192	15.2
3.168	.821	.913	3.291	15.2
3.168	.824	.914	3.291	15.2
3.386	.883	.966	3.517	15.2
3.468	.903	.978	3.601	15.2
3.555	.929	.987	3.692	15.2
3.650	.952	.989	3.791	15.2
3.650	.955	.989	3.791	15.2
3.868	1.014	.983	4.017	15.2
3.950	1.033	.984	4.101	15.2
4.037	1.060	.984	4.192	15.2
4.133	1.083	.981	4.291	15.2
4.133	1.086	.982	4.291	15.2
4.351	1.145	.988	4.517	15.2
4.433	1.164	.987	4.601	15.2
4.520	1.191	.990	4.692	15.2
4.616	1.214	.990	4.791	15.2
4.615	1.217	.988	4.791	15.2
4.833	1.276	.989	5.017	15.2
4.916	1.295	.988	5.101	15.2
5.002	1.322	.988	5.192	15.2
5.098	1.345	.989	5.291	15.2
5.098	1.348	.989	5.291	15.2
5.316	1.407	.989	5.517	15.2
5.398	1.426	.988	5.601	15.2
5.485	1.453	.990	5.692	15.2
5.581	1.475	.989	5.791	15.2
5.580	1.479	.989	5.791	15.2
-.011	.000	1.499	.011	24.5
.086	.044	1.498	.117	24.6
.171	.083	1.498	.211	24.6
.256	.122	1.496	.304	24.6
.355	.167	1.498	.413	24.6
.444	.208	1.493	.511	24.5
.540	.252	1.486	.617	24.6
.626	.291	1.477	.711	24.6
.711	.330	1.462	.804	24.6

TABLE 16.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg	y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
.809	.375	1.444	.913	24.6	-.019	.007	1.505	.007	26.9
.899	.415	1.391	1.011	24.5	.059	.047	1.507	.094	26.9
.995	.460	1.359	1.117	24.6	.156	.096	1.508	.202	26.9
1.081	.499	1.331	1.211	24.6	.246	.142	1.494	.304	26.9
1.165	.538	1.289	1.304	24.6	.341	.190	1.502	.410	26.9
1.264	.583	1.243	1.413	24.6	.427	.233	1.496	.507	26.9
1.354	.623	1.164	1.511	24.5	.505	.273	1.490	.594	26.9
1.450	.668	1.114	1.617	24.6	.602	.322	1.476	.702	26.9
1.535	.707	1.074	1.711	24.6	.692	.368	1.447	.804	26.9
1.620	.746	1.028	1.804	24.6	.787	.416	1.430	.910	26.9
1.719	.791	.990	1.913	24.6	.873	.460	1.373	1.007	26.9
1.809	.830	.957	2.011	24.5	.951	.499	1.341	1.094	26.9
1.905	.876	.932	2.117	24.6	1.047	.548	1.291	1.202	26.9
1.990	.915	.917	2.211	24.6	1.138	.594	1.238	1.304	26.9
2.075	.953	.900	2.304	24.6	1.233	.642	1.187	1.410	26.9
2.174	.999	.880	2.413	24.6	1.319	.686	1.112	1.507	26.9
2.264	1.038	.852	2.511	24.5	1.397	.725	1.066	1.594	26.9
2.359	1.083	.825	2.617	24.6	1.493	.774	1.015	1.702	26.9
2.445	1.123	.806	2.711	24.6	1.584	.820	.969	1.804	26.9
2.530	1.161	.798	2.804	24.6	1.678	.868	.939	1.910	26.9
2.628	1.206	.801	2.913	24.6	1.765	.912	.920	2.007	26.9
2.705	1.242	.811	2.997	24.6	1.842	.952	.908	2.094	26.9
2.800	1.285	.822	3.102	24.6	1.939	1.001	.897	2.202	26.9
2.915	1.337	.827	3.227	24.6	2.030	1.047	.885	2.304	26.9
2.982	1.341	.837	3.291	24.2	2.124	1.095	.865	2.410	26.9
3.160	1.449	.861	3.497	24.6	2.210	1.138	.846	2.507	26.9
3.255	1.493	.904	3.602	24.6	2.288	1.178	.817	2.594	26.9
3.369	1.545	.952	3.727	24.6	2.385	1.227	.784	2.702	26.9
3.438	1.546	.968	3.791	24.2	2.476	1.273	.766	2.804	26.9
3.615	1.657	.977	3.997	24.6	2.570	1.321	.767	2.910	26.9
3.710	1.701	.981	4.102	24.6	2.666	1.369	.770	3.017	26.9
3.824	1.753	.982	4.227	24.6	2.761	1.417	.787	3.124	26.9
3.895	1.750	.982	4.291	24.2	2.853	1.464	.802	3.227	26.9
4.070	1.865	.991	4.497	24.6	2.929	1.503	.818	3.312	26.9
4.165	1.909	.989	4.602	24.6	3.112	1.596	.877	3.517	26.9
4.279	1.961	.989	4.727	24.6	3.207	1.644	.921	3.624	26.9
4.351	1.955	.989	4.791	24.2	3.299	1.691	.954	3.727	26.9
4.524	2.073	.989	4.997	24.6	3.375	1.729	.975	3.812	26.9
4.619	2.116	.990	5.102	24.6	3.558	1.822	.983	4.017	26.9
4.734	2.169	.990	5.227	24.6	3.652	1.870	.984	4.124	26.9
4.807	2.160	.990	5.291	24.2	3.745	1.917	.982	4.227	26.9
4.979	2.281	.990	5.497	24.6	3.821	1.955	.984	4.312	26.9
5.074	2.324	.990	5.602	24.6	4.003	2.048	.990	4.517	26.9
5.188	2.377	.990	5.727	24.6	4.098	2.096	.990	4.624	26.9
5.263	2.364	.990	5.791	24.2	4.191	2.143	.989	4.727	26.9

TABLE 16.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
4.267	2.181	.990	4.812	26.9
4.449	2.274	.989	5.017	26.9
4.544	2.322	.988	5.124	26.9
4.637	2.369	.989	5.227	26.9
4.712	2.408	.989	5.312	26.9
4.895	2.500	.989	5.517	26.9
4.990	2.549	.990	5.624	26.9
5.083	2.596	.990	5.727	26.9
5.158	2.634	.991	5.812	26.9
-.021	.018	1.495	.010	29.4
.070	.069	1.495	.114	29.4
.161	.124	1.492	.221	29.8
.237	.166	1.492	.308	29.6
.332	.221	1.485	.417	29.7
.415	.263	1.476	.510	29.4
.505	.315	1.464	.614	29.4
.595	.373	1.442	.721	29.8
.672	.413	1.424	.808	29.6
.766	.468	1.390	.917	29.7
.851	.508	1.315	1.010	29.4
.941	.561	1.271	1.114	29.4
1.028	.622	1.214	1.221	29.8
1.107	.660	1.171	1.308	29.6
1.200	.716	1.111	1.417	29.7
1.286	.753	1.030	1.510	29.4
1.376	.807	.988	1.614	29.4
1.462	.871	.946	1.721	29.8
1.542	.907	.925	1.808	29.6
1.634	.964	.905	1.917	29.7
1.722	.999	.892	2.010	29.4
1.812	1.052	.892	2.114	29.4
1.896	1.120	.891	2.221	29.8
1.976	1.154	.888	2.308	29.6
2.069	1.212	.878	2.417	29.7
2.158	1.244	.864	2.510	29.4
2.247	1.298	.832	2.614	29.4
2.329	1.368	.795	2.721	29.8
2.411	1.401	.776	2.808	29.6
2.503	1.460	.772	2.917	29.7
2.585	1.518	.782	3.017	29.9
2.678	1.564	.790	3.120	29.8
2.769	1.626	.814	3.230	29.9
2.846	1.655	.840	3.312	29.7
3.019	1.767	.910	3.517	29.9
3.112	1.812	.939	3.620	29.8
3.202	1.875	.969	3.730	29.9
3.281	1.902	.984	3.812	29.7
3.453	2.016	.984	4.017	29.9
3.546	2.060	.982	4.120	29.8
3.636	2.125	.982	4.230	29.9
3.715	2.150	.983	4.312	29.7
3.886	2.265	.990	4.517	29.9
3.980	2.308	.988	4.620	29.8
4.069	2.374	.988	4.730	29.9
4.149	2.398	.989	4.812	29.7
4.320	2.514	.990	5.017	29.9
4.414	2.557	.989	5.120	29.8
4.502	2.623	.989	5.230	29.9
4.584	2.646	.989	5.312	29.7
4.753	2.763	.991	5.517	29.9
4.848	2.805	.989	5.620	29.8
4.936	2.873	.989	5.730	29.9
5.018	2.893	.990	5.812	29.7
-.073	.018	1.491	-.034	36.8
.028	.093	1.505	.093	36.8
.080	.133	1.503	.158	36.8
.170	.199	1.495	.269	36.8
.251	.260	1.483	.371	36.8
.327	.318	1.457	.466	36.8
.428	.393	1.444	.593	36.8
.480	.432	1.419	.658	36.8
.570	.499	1.379	.769	36.8
.651	.560	1.324	.871	36.8
.727	.617	1.236	.966	36.8
.828	.693	1.169	1.093	36.8
.881	.732	1.123	1.158	36.8
.970	.799	1.060	1.269	36.8
1.051	.860	.996	1.371	36.8
1.128	.917	.932	1.466	36.8
1.229	.993	.895	1.593	36.8
1.281	1.032	.876	1.658	36.8
1.370	1.099	.867	1.769	36.8
1.451	1.160	.871	1.871	36.8
1.528	1.217	.882	1.966	36.8
1.629	1.293	.903	2.093	36.8
1.681	1.332	.913	2.158	36.8
1.770	1.399	.923	2.269	36.8
1.851	1.459	.926	2.371	36.8

TABLE 16.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
1.928	1.517	.934	2.466	36.8
2.029	1.593	.930	2.593	36.8
2.081	1.632	.931	2.658	36.8
2.170	1.699	.927	2.769	36.8
2.251	1.759	.924	2.871	36.8
2.324	1.814	.937	2.961	36.8
2.406	1.875	.948	3.064	36.8
2.485	1.935	.959	3.163	36.8
2.569	1.998	.968	3.268	36.8
2.724	2.113	.983	3.461	36.8
2.806	2.175	.988	3.564	36.8
2.885	2.234	.989	3.663	36.8
2.970	2.298	.989	3.768	36.8
3.124	2.413	.983	3.961	36.8
3.206	2.475	.981	4.064	36.8
3.286	2.534	.981	4.163	36.8
3.370	2.597	.979	4.268	36.8
3.524	2.713	.989	4.461	36.8
3.606	2.775	.988	4.564	36.8
3.686	2.834	.989	4.663	36.8
3.770	2.897	.989	4.768	36.8
3.924	3.013	.988	4.961	36.8
4.006	3.074	.988	5.064	36.8
4.086	3.134	.988	5.163	36.8
4.170	3.197	.988	5.268	36.8
4.325	3.313	.989	5.461	36.8
4.407	3.374	.989	5.564	36.8
4.486	3.434	.989	5.663	36.8
4.570	3.497	.988	5.768	36.8
-.092	.039	1.501	-.034	45.0
-.031	.099	1.496	.052	45.0
.047	.177	1.486	.162	45.0
.116	.247	1.474	.260	45.0
.192	.322	1.448	.367	45.0
.262	.392	1.432	.466	45.0
.323	.453	1.396	.552	45.0
.400	.531	1.348	.662	45.0
.470	.601	1.297	.760	45.0
.545	.676	1.215	.867	45.0
.615	.746	1.140	.966	45.0
.676	.807	1.073	1.052	45.0
.753	.885	1.007	1.162	45.0
.823	.954	.947	1.260	45.0
.898	1.030	.888	1.367	45.0

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
.968	1.100	.857	1.466	45.0
1.029	1.161	.840	1.552	45.0
1.107	1.238	.835	1.662	45.0
1.177	1.308	.839	1.760	45.0
1.252	1.383	.862	1.867	45.0
1.322	1.454	.885	1.966	45.0
1.383	1.514	.912	2.052	45.0
1.460	1.592	.937	2.162	45.0
1.530	1.662	.954	2.260	45.0
1.605	1.737	.970	2.367	45.0
1.675	1.807	.977	2.466	45.0
1.736	1.868	.982	2.552	45.0
1.814	1.946	.985	2.662	45.0
1.883	2.016	.986	2.760	45.0
1.958	2.091	.988	2.867	45.0
2.018	2.151	.986	2.951	45.0
2.100	2.233	.988	3.067	45.0
2.184	2.317	.988	3.186	45.0
2.244	2.374	.988	3.269	45.0
2.372	2.505	.989	3.451	45.0
2.453	2.586	.989	3.567	45.0
2.537	2.671	.989	3.686	45.0
2.598	2.727	.988	3.769	45.0
2.725	2.858	.976	3.951	45.0
2.807	2.940	.977	4.067	45.0
2.891	3.024	.976	4.186	45.0
2.951	3.081	.976	4.269	45.0
3.078	3.212	.988	4.451	45.0
3.160	3.294	.990	4.567	45.0
3.244	3.378	.988	4.686	45.0
3.305	3.434	.989	4.769	45.0
3.432	3.566	.990	4.951	45.0
3.513	3.648	.989	5.067	45.0
3.598	3.732	.988	5.186	45.0
3.659	3.788	.988	5.269	45.0
3.785	3.920	.989	5.451	45.0
3.867	4.002	.990	5.567	45.0
3.951	4.086	.989	5.686	45.0
4.012	4.142	.989	5.769	45.0
-.129	.069	1.500	-.034	59.1
-.086	.140	1.492	.050	59.1
-.032	.230	1.477	.155	59.1
.031	.336	1.447	.279	59.1
.076	.411	1.411	.366	59.1

TABLE 16.- Continued

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
.128	.497	1.378	.466	59.1
.171	.569	1.331	.550	59.1
.225	.659	1.267	.655	59.1
.288	.765	1.183	.779	59.1
.333	.840	1.118	.866	59.1
.385	.926	1.040	.966	59.1
.428	.998	.985	1.050	59.1
.482	1.088	.920	1.155	59.1
.545	1.194	.865	1.279	59.1
.590	1.269	.831	1.366	59.1
.642	1.355	.810	1.466	59.1
.685	1.427	.804	1.550	59.1
.739	1.517	.812	1.655	59.1
.802	1.623	.833	1.779	59.1
.847	1.698	.852	1.866	59.1
.899	1.784	.883	1.966	59.1
.942	1.856	.907	2.050	59.1
.996	1.946	.932	2.155	59.1
1.059	2.052	.954	2.279	59.1
1.104	2.127	.963	2.366	59.1
1.156	2.213	.970	2.466	59.1
1.199	2.285	.975	2.550	59.1
1.253	2.375	.980	2.655	59.1
1.316	2.481	.984	2.779	59.1
1.361	2.556	.983	2.866	59.1
1.418	2.651	.984	2.977	59.1
1.470	2.738	.984	3.078	59.1
1.471	2.738	.985	3.079	59.1
1.514	2.811	.986	3.163	59.1
1.568	2.901	.986	3.268	59.1
1.675	3.080	.989	3.477	59.1
1.727	3.167	.990	3.578	59.1
1.728	3.167	.989	3.579	59.1
1.771	3.239	.989	3.663	59.1
1.825	3.330	.991	3.768	59.1
1.932	3.509	.982	3.977	59.1
1.984	3.596	.981	4.078	59.1
1.985	3.596	.981	4.079	59.1
2.028	3.668	.981	4.163	59.1
2.082	3.758	.981	4.268	59.1
2.189	3.938	.990	4.477	59.1
2.241	4.024	.990	4.578	59.1
2.242	4.025	.989	4.579	59.1
2.285	4.097	.990	4.663	59.1
2.339	4.187	.989	4.768	59.1
2.446	4.367	.991	4.977	59.1
2.498	4.453	.990	5.078	59.1
2.499	4.454	.991	5.079	59.1
2.542	4.526	.991	5.163	59.1
2.596	4.616	.991	5.268	59.1
2.703	4.795	.991	5.477	59.1
2.756	4.882	.988	5.578	59.1
2.756	4.883	.990	5.579	59.1
2.799	4.955	.991	5.663	59.1
2.853	5.045	.990	5.768	59.1
-.180	.090	1.500	-.034	75.4
-.150	.204	1.488	.085	75.3
-.132	.273	1.470	.156	75.3
-.100	.395	1.422	.282	75.3
-.079	.479	1.365	.369	75.4
-.054	.574	1.327	.466	75.4
-.023	.688	1.256	.585	75.3
-.005	.757	1.200	.656	75.3
.026	.879	1.108	.782	75.3
.047	.963	1.035	.869	75.4
.072	1.058	.973	.966	75.4
.104	1.172	.915	1.085	75.3
.121	1.240	.874	1.156	75.3
.153	1.363	.824	1.282	75.3
.174	1.447	.802	1.369	75.4
.198	1.541	.789	1.466	75.4
.231	1.655	.794	1.585	75.3
.248	1.724	.804	1.656	75.3
.279	1.846	.826	1.782	75.3
.300	1.931	.855	1.869	75.4
.325	2.025	.876	1.966	75.4
.358	2.139	.904	2.085	75.3
.375	2.208	.921	2.156	75.3
.406	2.330	.942	2.282	75.3
.426	2.414	.957	2.369	75.4
.451	2.509	.964	2.466	75.4
.485	2.622	.973	2.585	75.3
.501	2.692	.976	2.656	75.3
.533	2.814	.979	2.782	75.3
.553	2.898	.980	2.869	75.4
.574	2.979	.979	2.952	75.4
.603	3.081	.980	3.058	75.3
.635	3.203	.982	3.185	75.3
.653	3.285	.982	3.268	75.4

TABLE 16.- Concluded

y, in.	z, in.	$p_{t,p}/p_{t,\infty}$	r, in.	ϕ, deg
.700	3.463	.985	3.452	75.4
.730	3.564	.986	3.558	75.3
.761	3.687	.985	3.685	75.3
.780	3.769	.985	3.768	75.4
.826	3.947	.979	3.952	75.4
.857	4.048	.977	4.058	75.3
.888	4.171	.980	4.185	75.3
.906	4.252	.977	4.268	75.4
.952	4.430	.988	4.452	75.4
.984	4.532	.986	4.558	75.3
1.014	4.655	.987	4.685	75.3
1.032	4.736	.987	4.768	75.4
1.079	4.914	.988	4.952	75.4
1.110	5.015	.988	5.058	75.3
1.141	5.138	.988	5.185	75.3
1.159	5.220	.988	5.268	75.4
1.205	5.398	.988	5.452	75.4
1.237	5.499	.987	5.558	75.3
1.267	5.622	.987	5.685	75.3
1.285	5.704	.987	5.768	75.4
-.232	.096	1.501	-.034	90.7
-.233	.202	1.485	.072	90.6
-.234	.286	1.464	.156	90.7
-.236	.391	1.409	.261	90.7
-.236	.496	1.348	.366	90.6
-.238	.596	1.300	.466	90.7
-.239	.702	1.226	.572	90.6
-.240	.786	1.164	.656	90.7
-.241	.891	1.068	.761	90.7
-.242	.996	.996	.866	90.6
-.244	1.096	.933	.966	90.7
-.244	1.202	.885	1.072	90.6
-.246	1.286	.850	1.156	90.7
-.247	1.391	.812	1.261	90.7
-.247	1.496	.801	1.366	90.6
-.249	1.596	.799	1.466	90.7
-.249	1.702	.814	1.572	90.6
-.251	1.786	.827	1.656	90.7
-.253	1.891	.856	1.761	90.7
-.252	1.996	.885	1.866	90.6
-.255	2.096	.901	1.966	90.7
-.255	2.202	.926	2.072	90.6
-.257	2.286	.939	2.156	90.7
-.258	2.391	.954	2.261	90.7
-.258	2.496	.966	2.366	90.6
-.261	2.596	.971	2.466	90.7
-.260	2.701	.977	2.572	90.6
-.263	2.786	.977	2.656	90.7
-.264	2.891	.980	2.761	90.7
-.263	2.996	.983	2.866	90.6
-.266	3.104	.982	2.974	90.7
-.267	3.188	.983	3.058	90.7
-.266	3.297	.981	3.168	90.6
-.270	3.398	.983	3.268	90.7
-.272	3.604	.986	3.474	90.7
-.273	3.688	.985	3.558	90.7
-.272	3.797	.985	3.668	90.6
-.275	3.898	.986	3.768	90.7
-.278	4.104	.972	3.974	90.7
-.279	4.188	.972	4.058	90.7
-.277	4.297	.971	4.168	90.6
-.281	4.398	.972	4.268	90.7
-.283	4.603	.986	4.474	90.7
-.284	4.688	.986	4.558	90.7
-.282	4.797	.986	4.668	90.6
-.287	4.898	.986	4.768	90.7
-.289	5.103	.987	4.974	90.7
-.290	5.188	.987	5.058	90.7
-.288	5.297	.987	5.168	90.6
-.292	5.398	.987	5.268	90.7
-.295	5.603	.987	5.474	90.7
-.296	5.688	.987	5.558	90.7
-.293	5.797	.985	5.668	90.6
-.298	5.898	.988	5.768	90.7

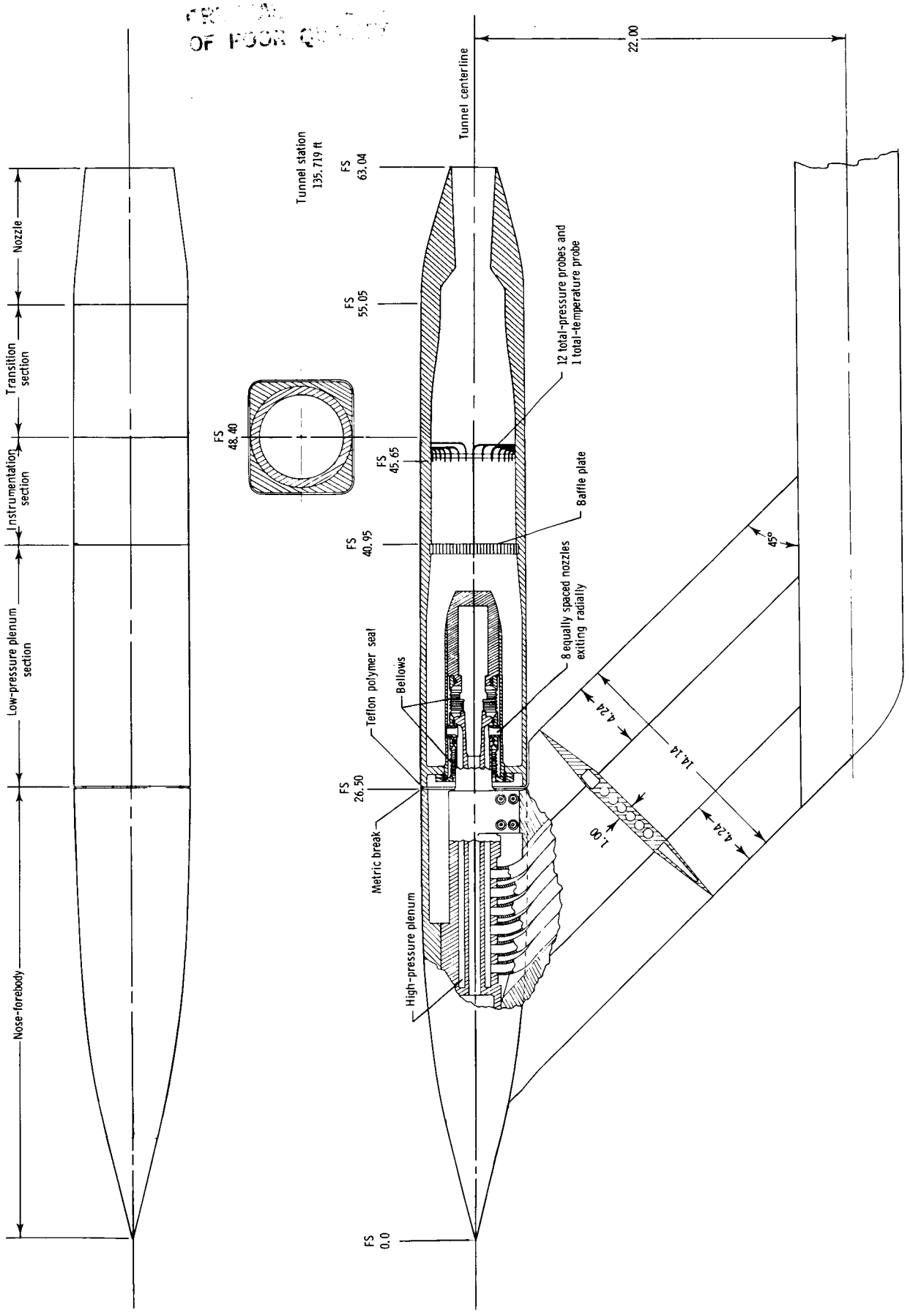
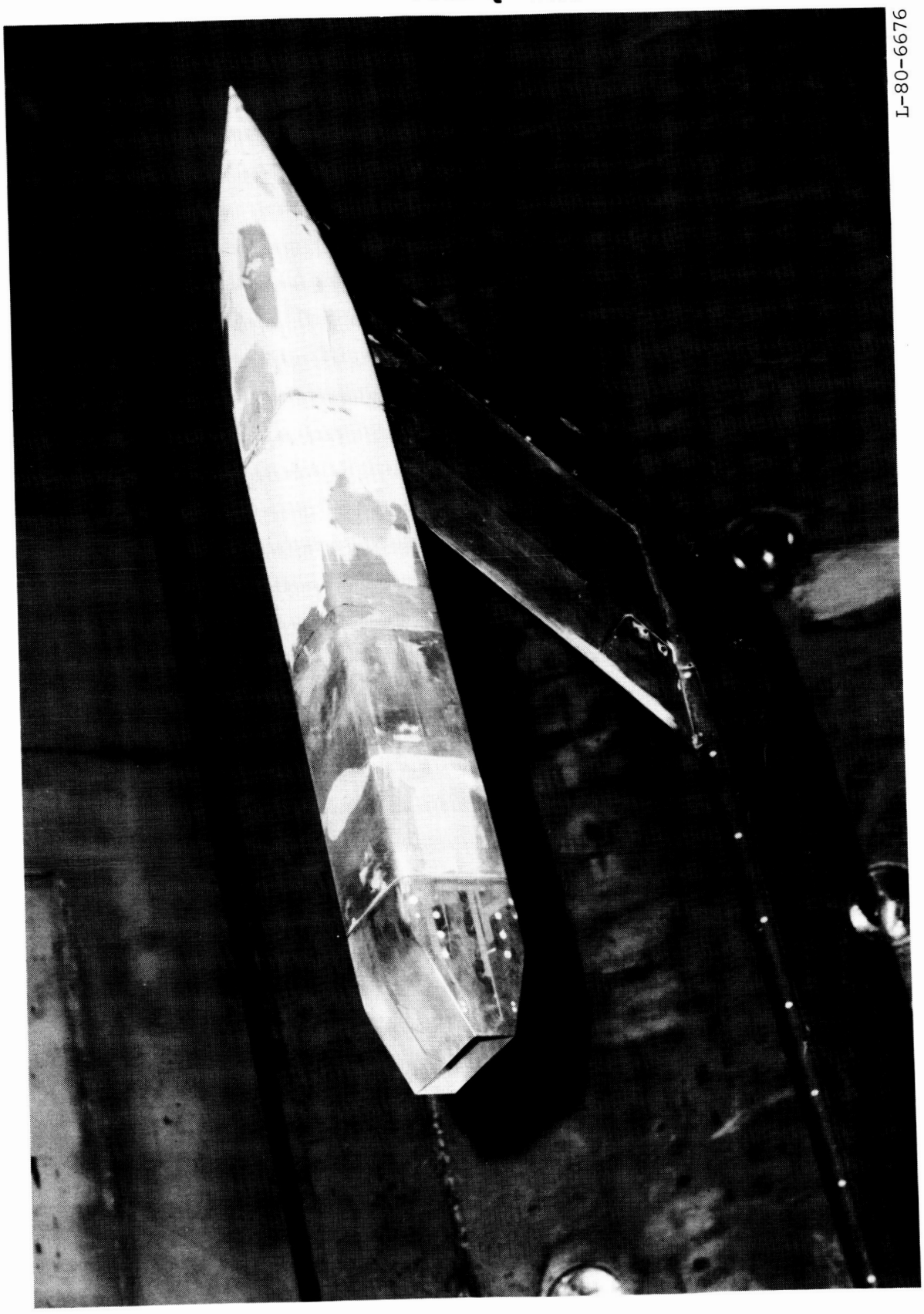
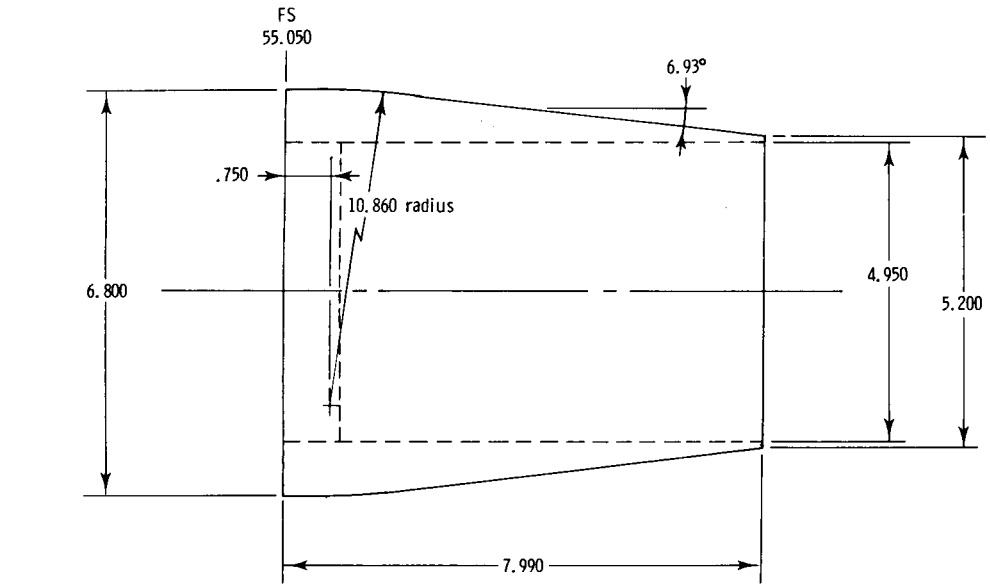


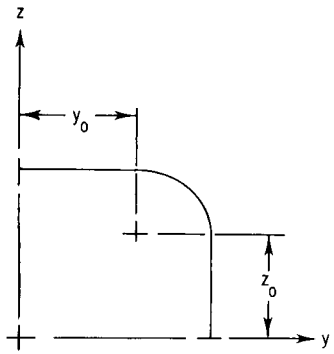
Figure 1.- Sketch of model showing internal details. All dimensions are in inches unless otherwise noted.



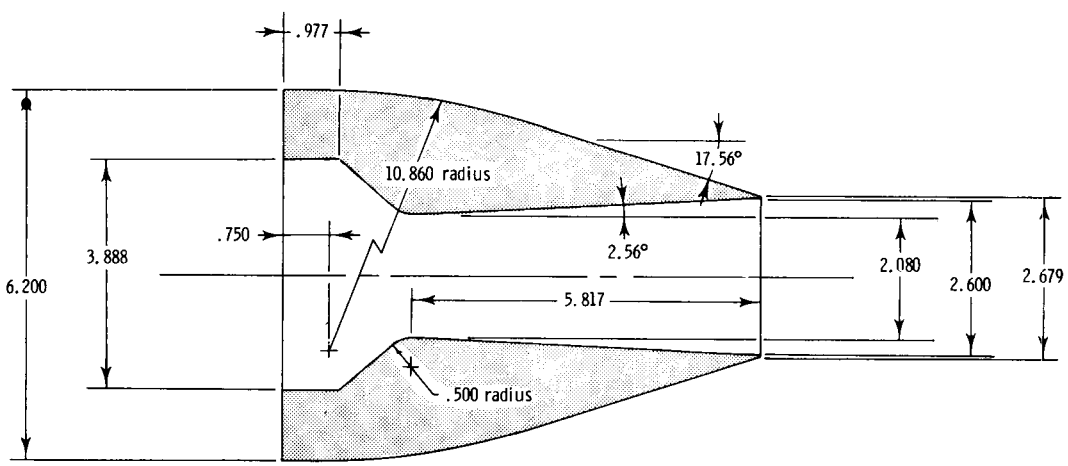
L-80-6676

Figure 2.- Photograph of model in Langley 16-Foot Transonic Tunnel.





Typical cross section



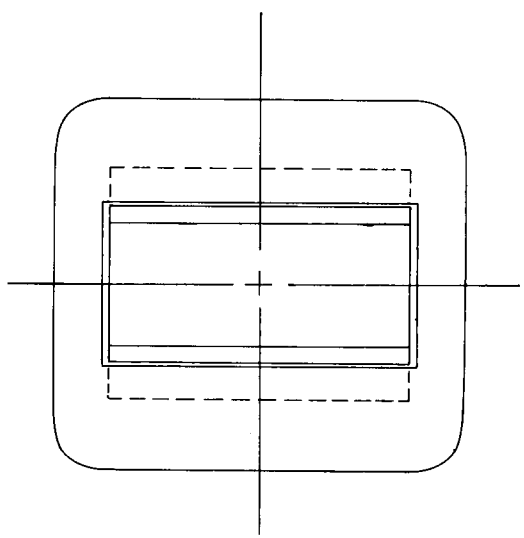
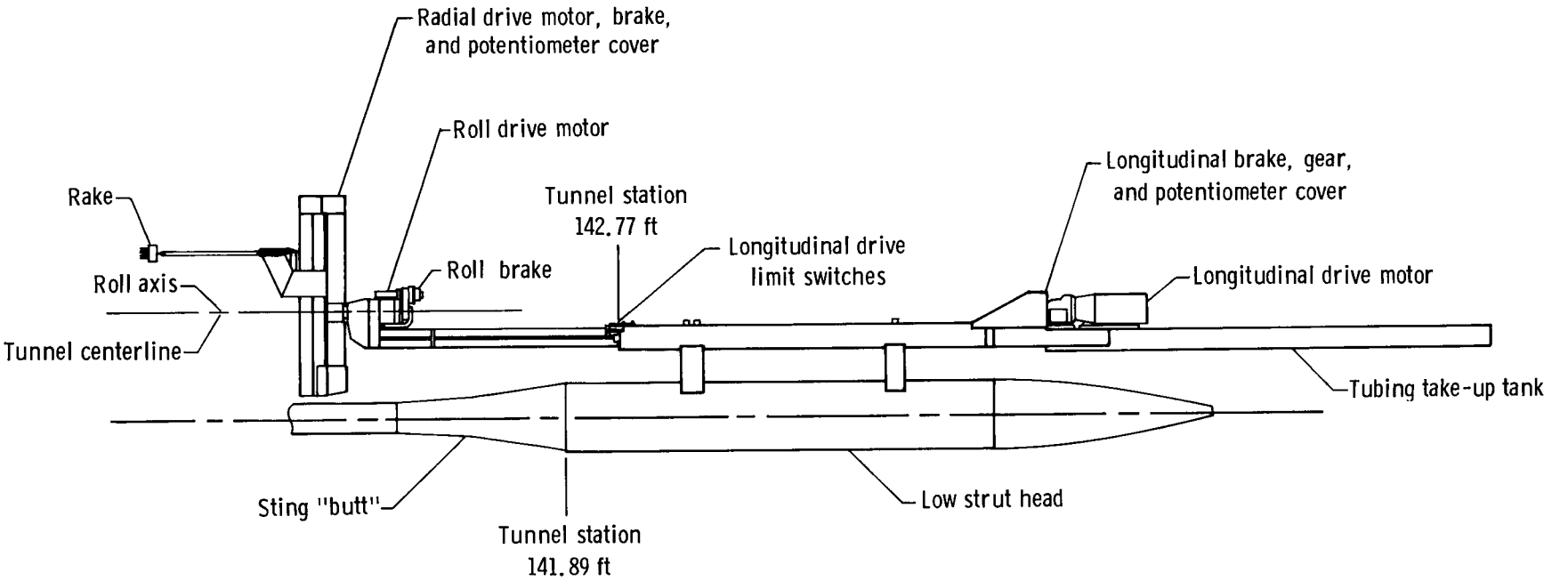
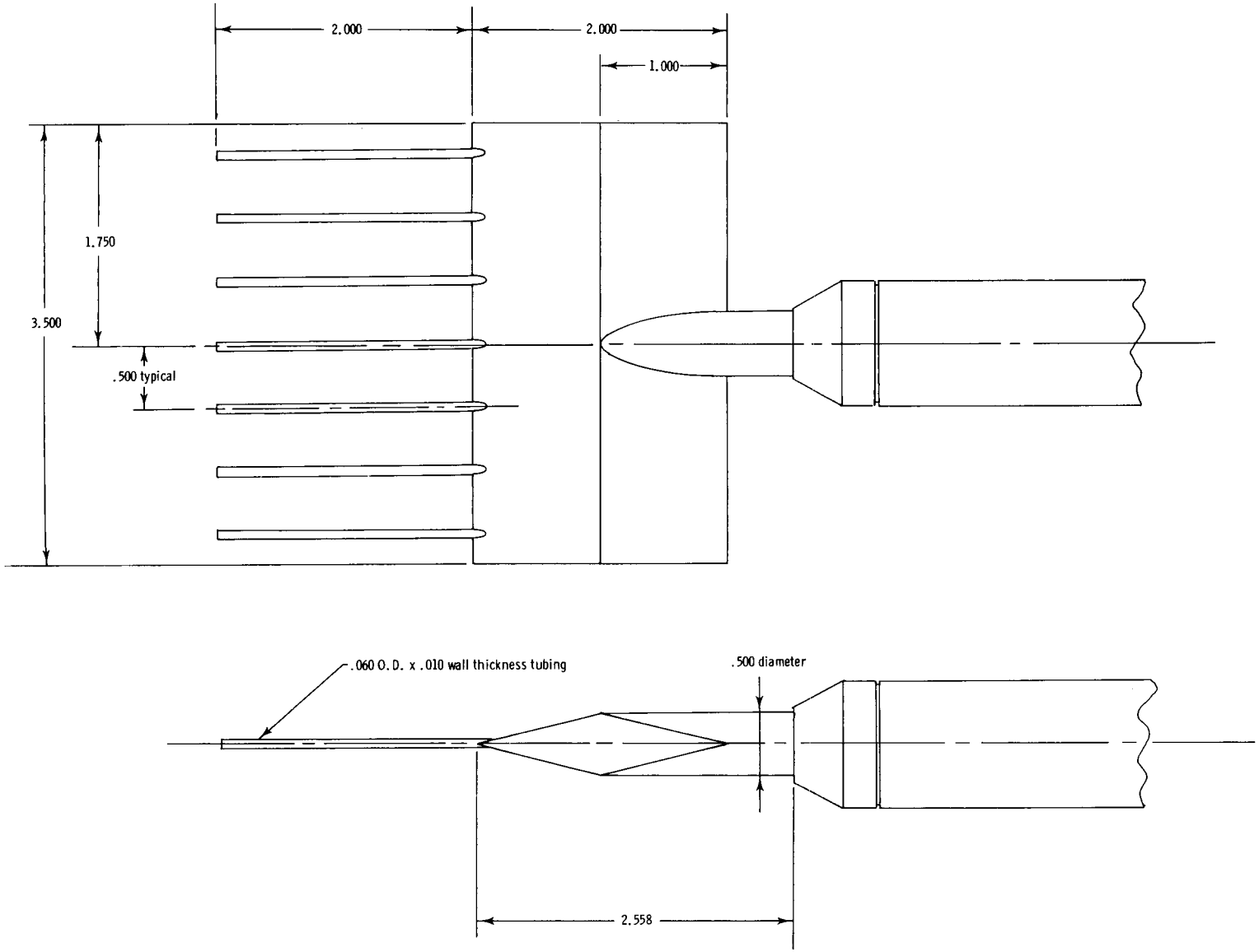


Figure 3.- Details of the nozzle. Linear dimensions are in inches.



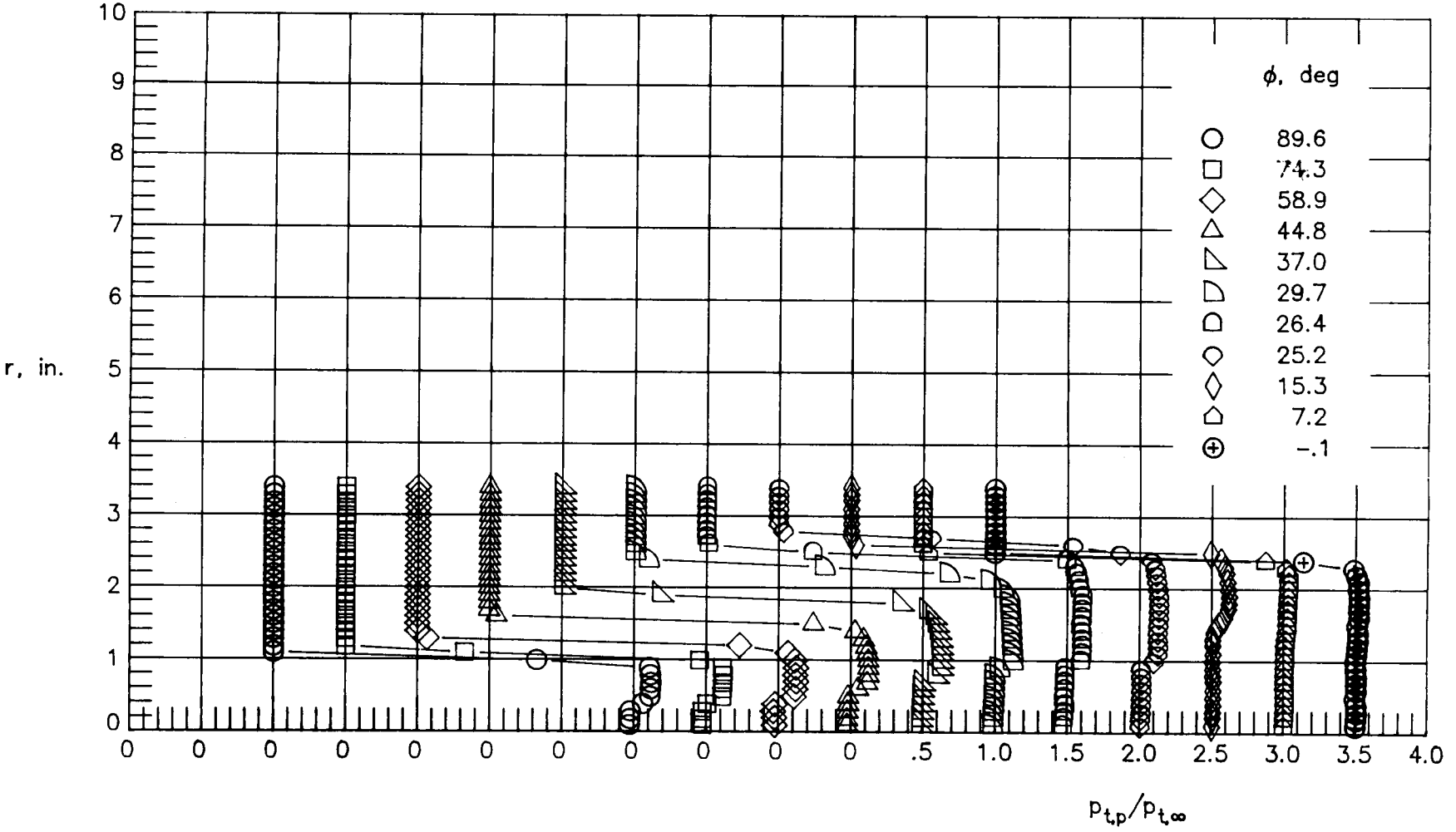
(a) Sketch of translating survey mechanism.

Figure 4.- Details of translating survey mechanism and rake.



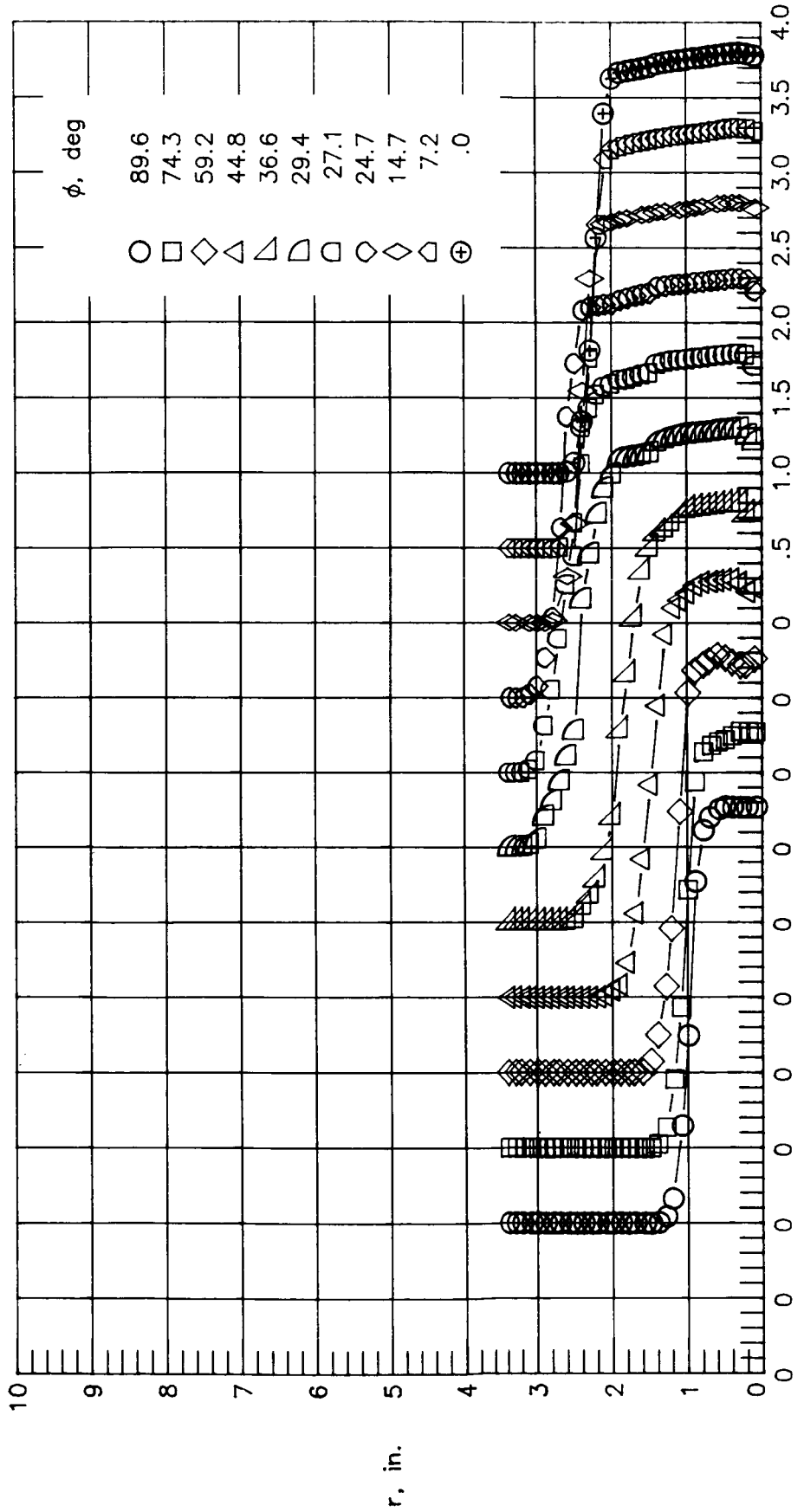
(b) Sketch of pitot-pressure rake. Linear dimensions are in inches.

Figure 4.- Concluded.



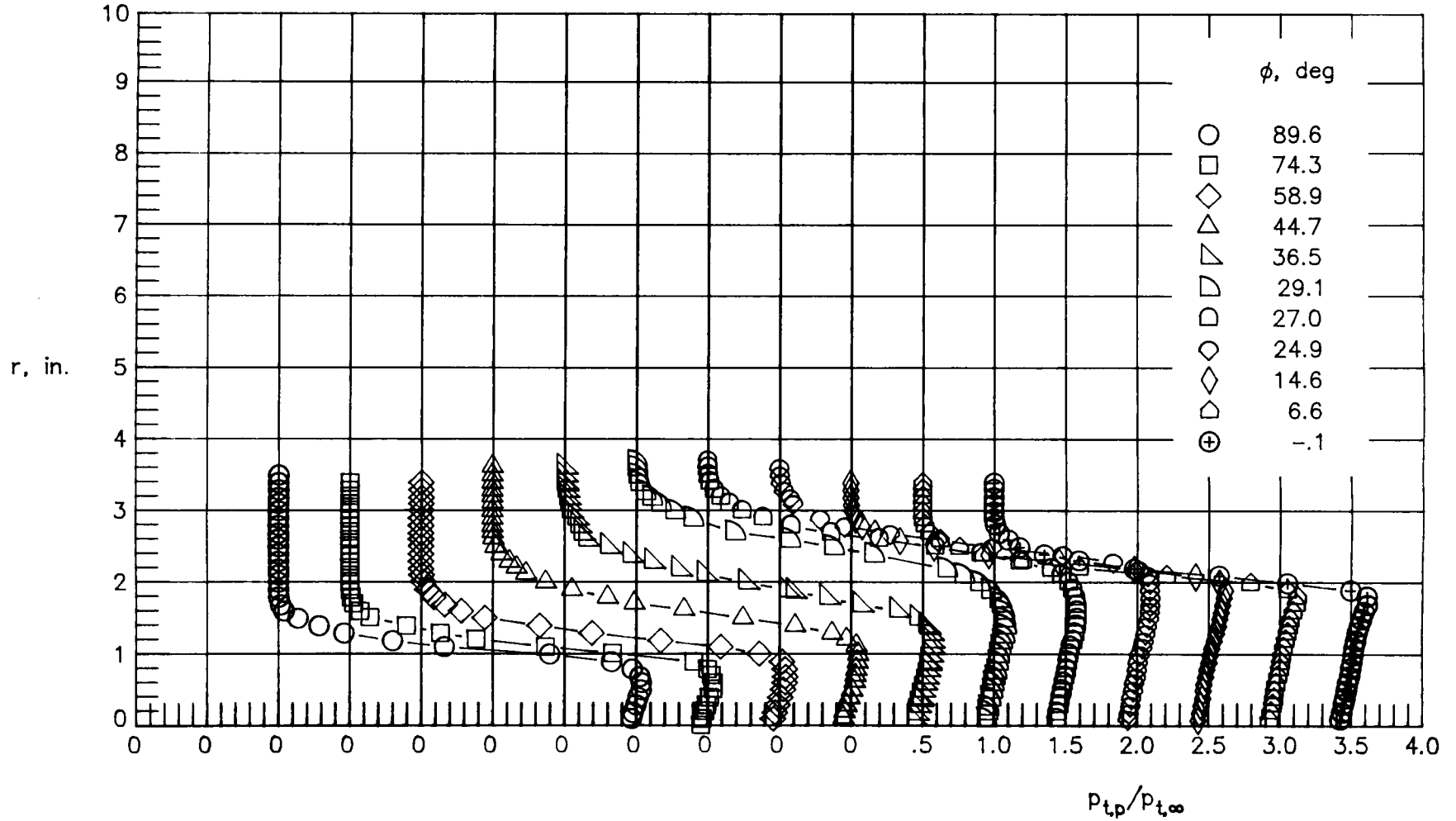
(a) x = 0.0 in.

Figure 5.- Variation of pitot pressure with r and ϕ at M_∞ = 0.00 and NPR = 4.0.



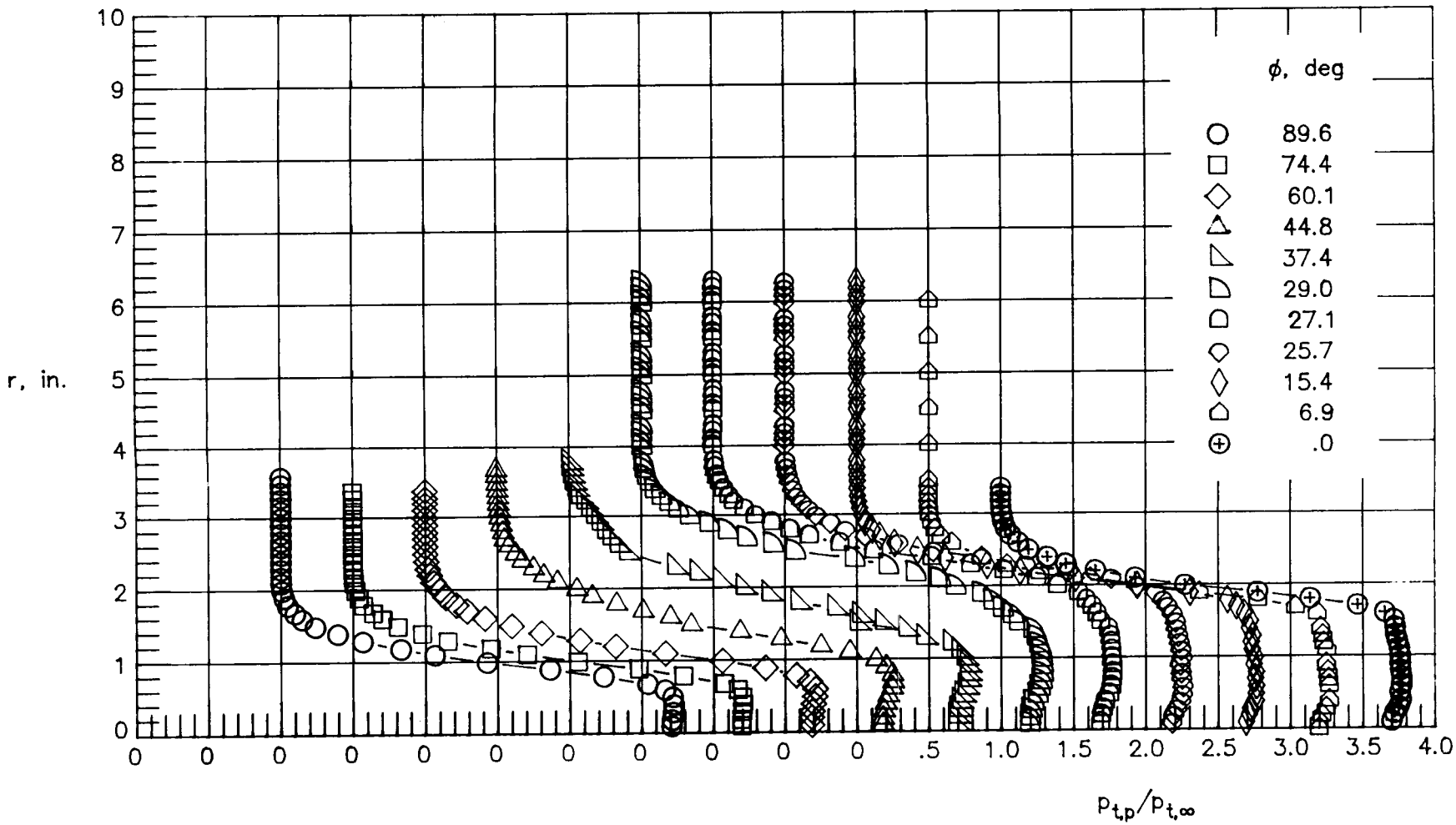
(b) x = 2.6 in.

Figure 5.- Continued.



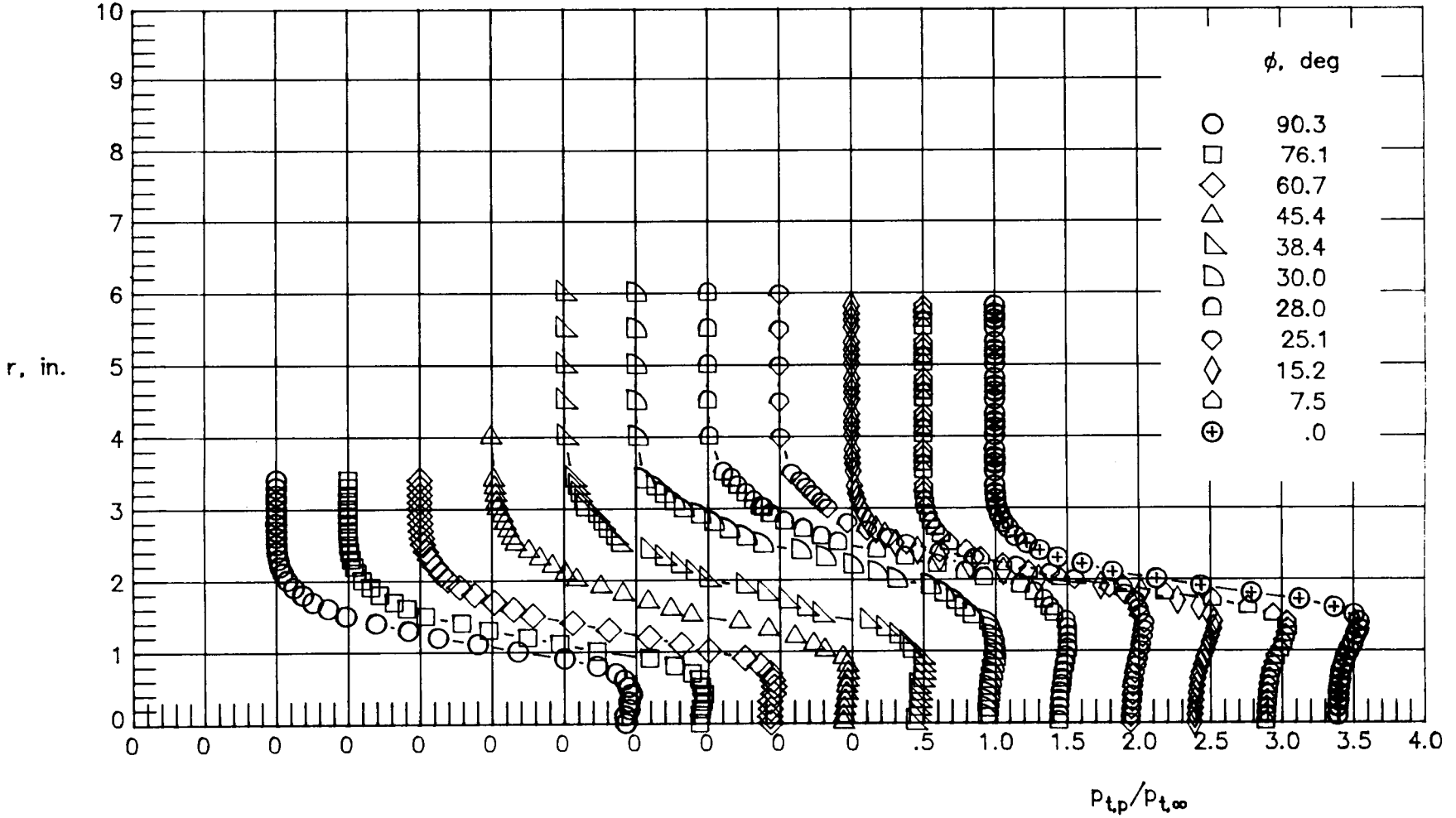
(c) x = 5.2 in.

Figure 5.- Continued.



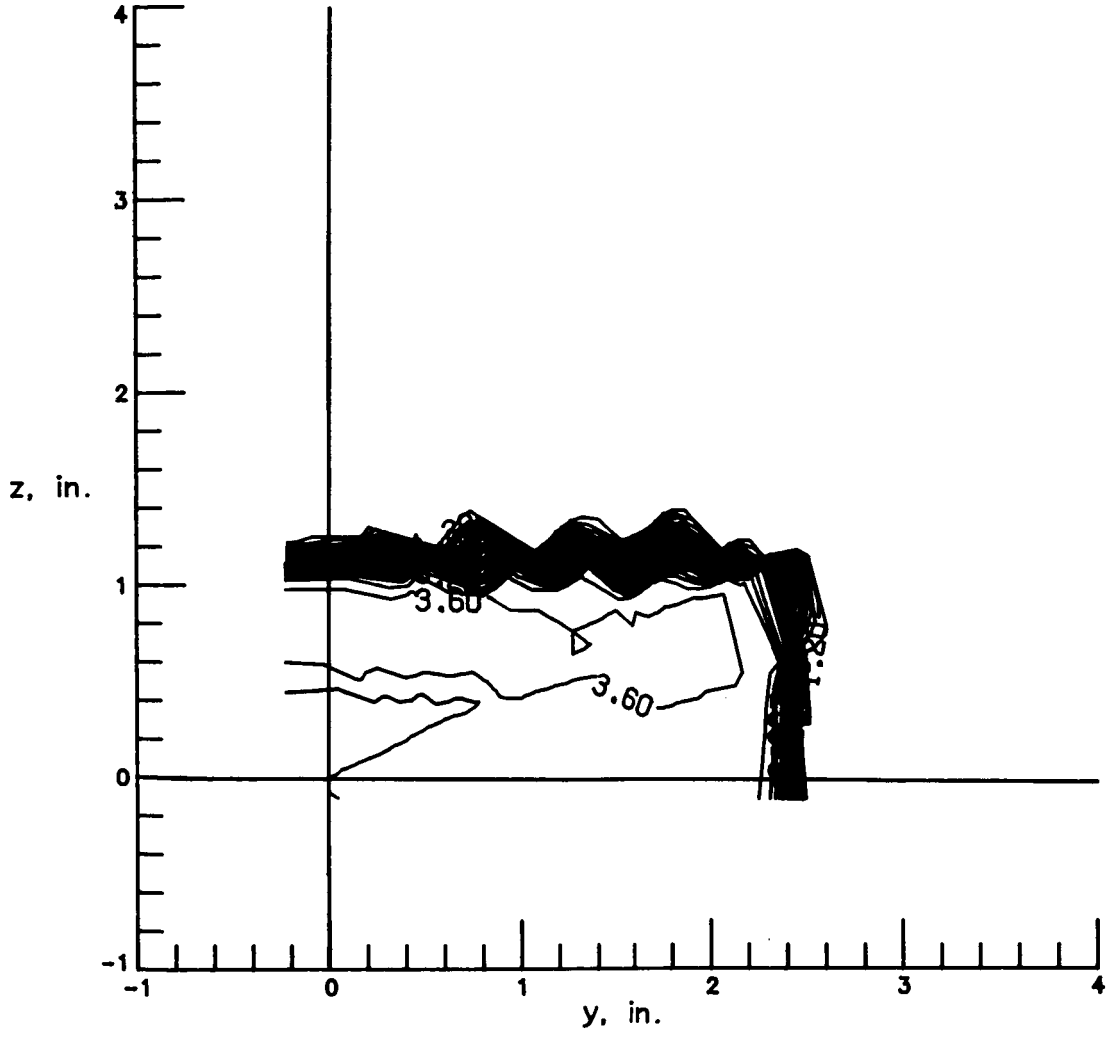
(d) x = 7.8 in.

Figure 5.- Continued.



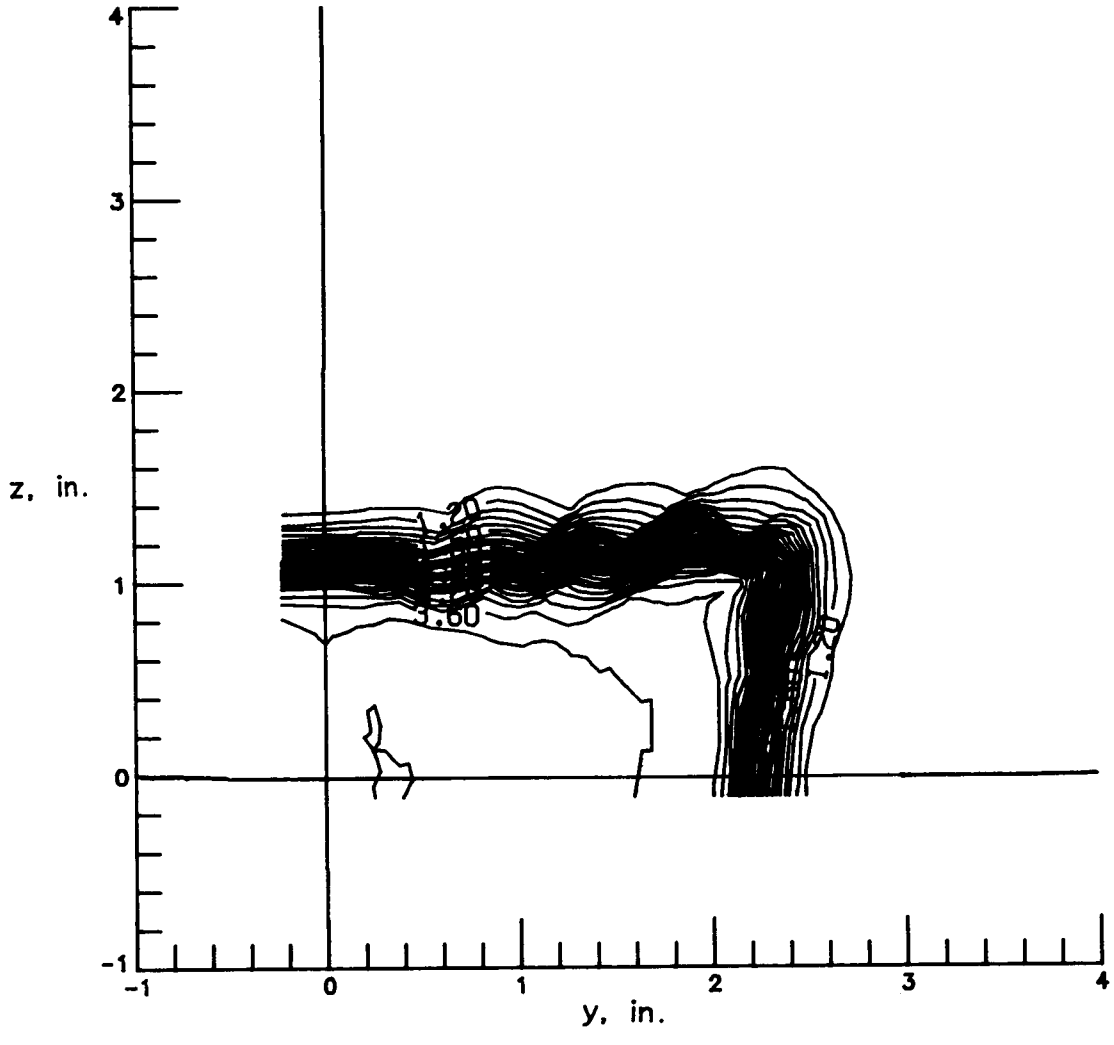
(e) x = 10.4 in.

Figure 5.- Concluded.



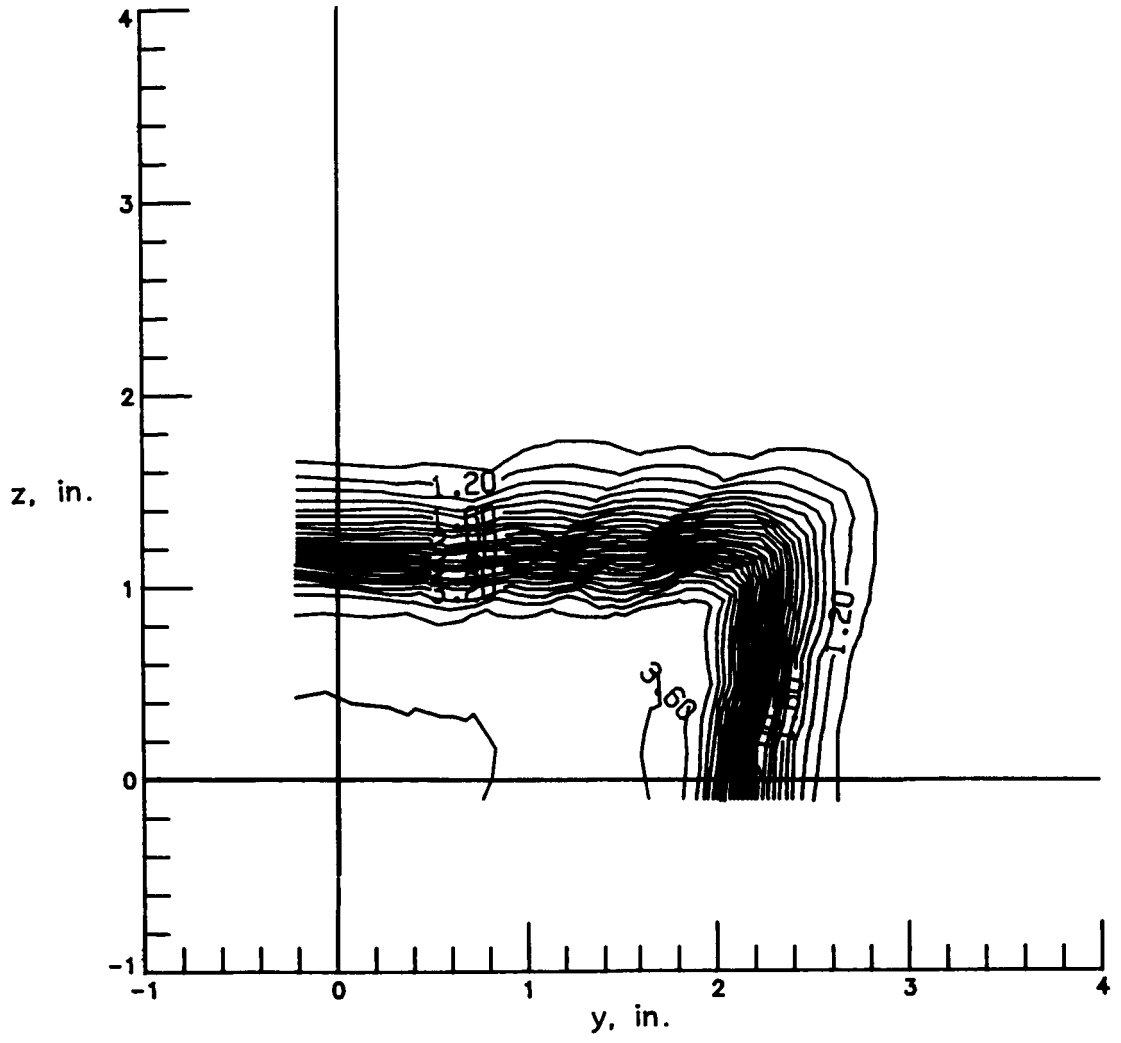
(a) x = 0.0 in.

Figure 6.- Contour plots of $p_{t,p}/p_{t,\infty}$ at $M_\infty = 0.00$ and NPR = 4.0.



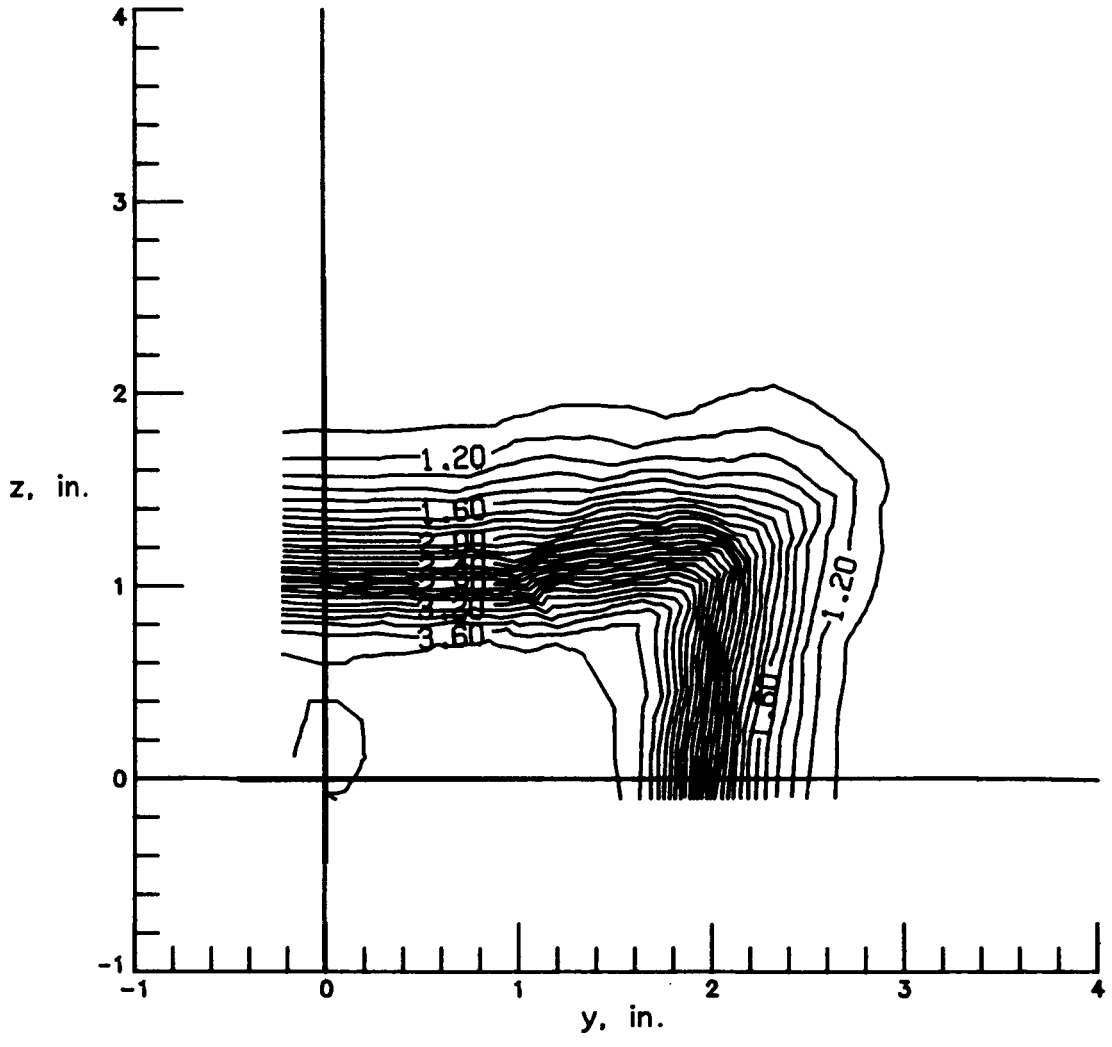
(b) x = 2.6 in.

Figure 6.- Continued.



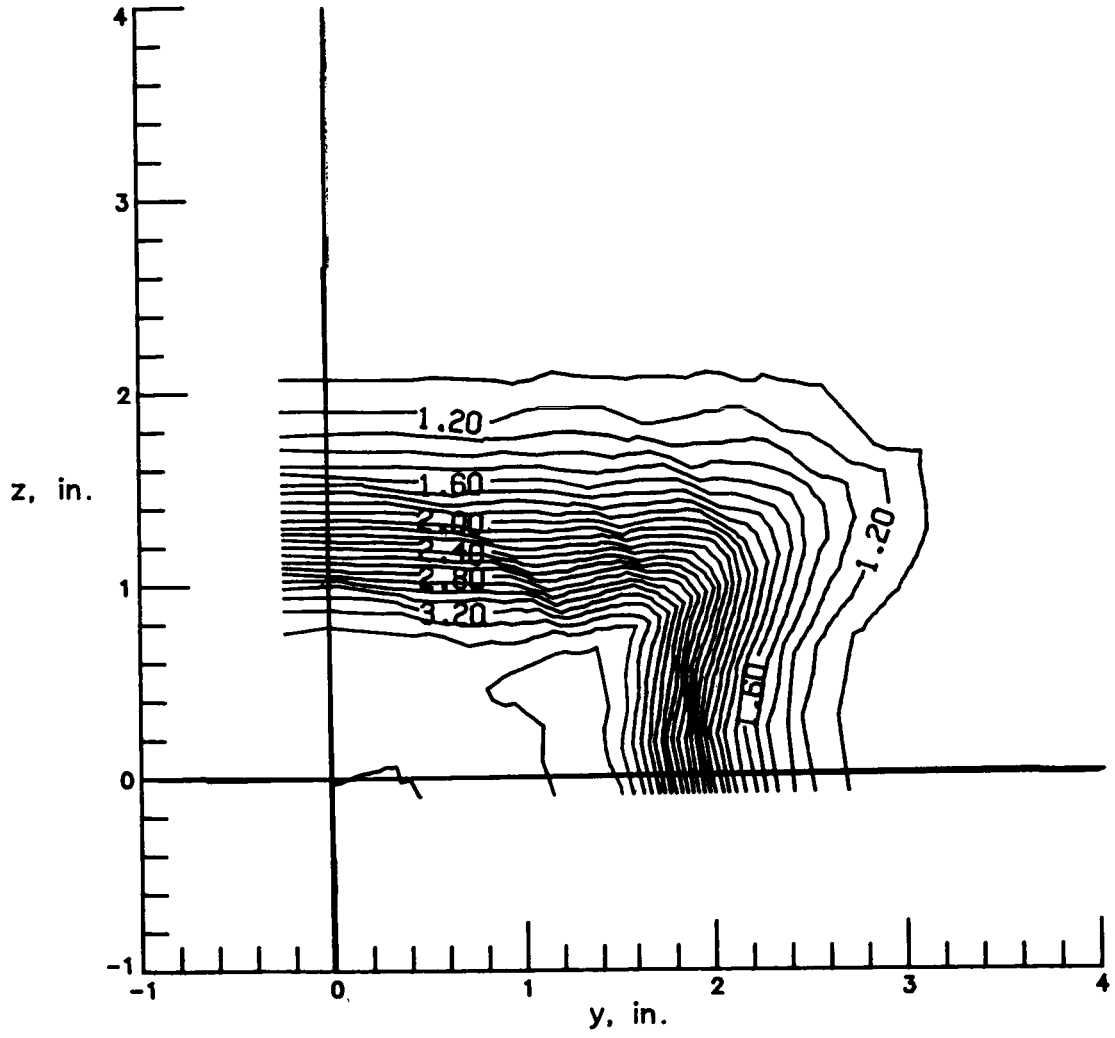
(c) x = 5.2 in.

Figure 6.- Continued.



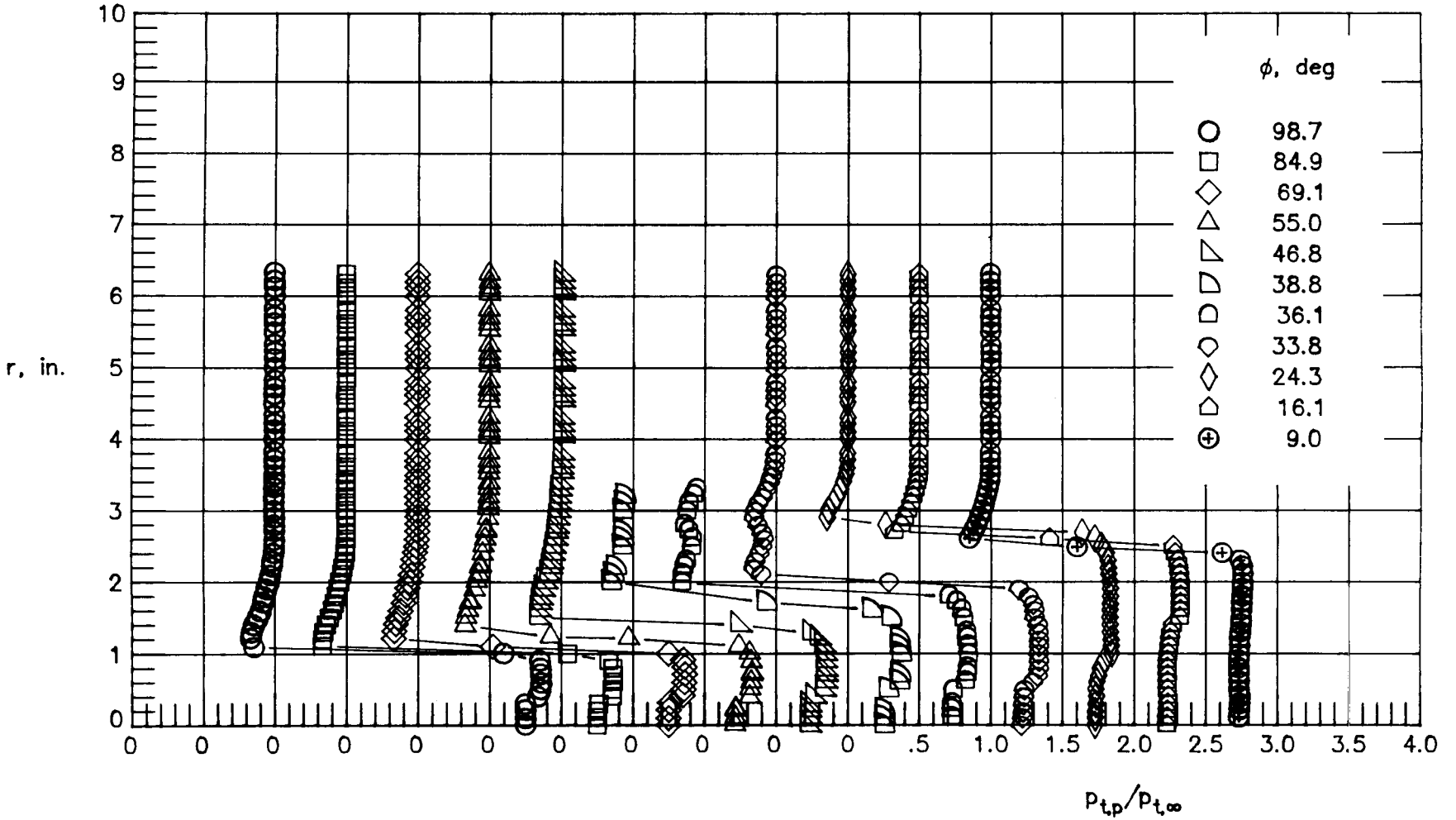
(d) x = 7.8 in.

Figure 6.- Continued.



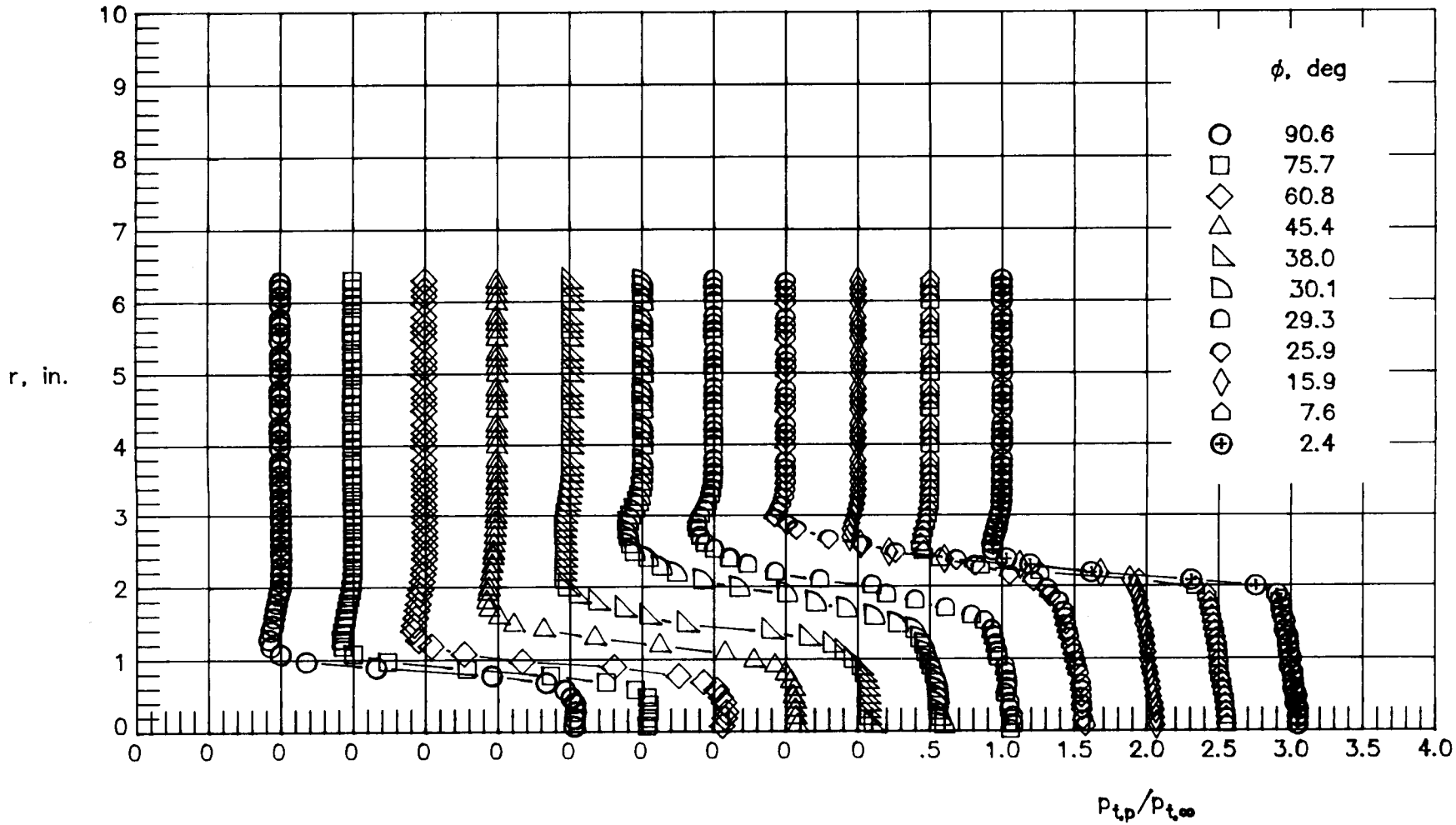
(e) x = 10.4 in.

Figure 6.- Concluded.



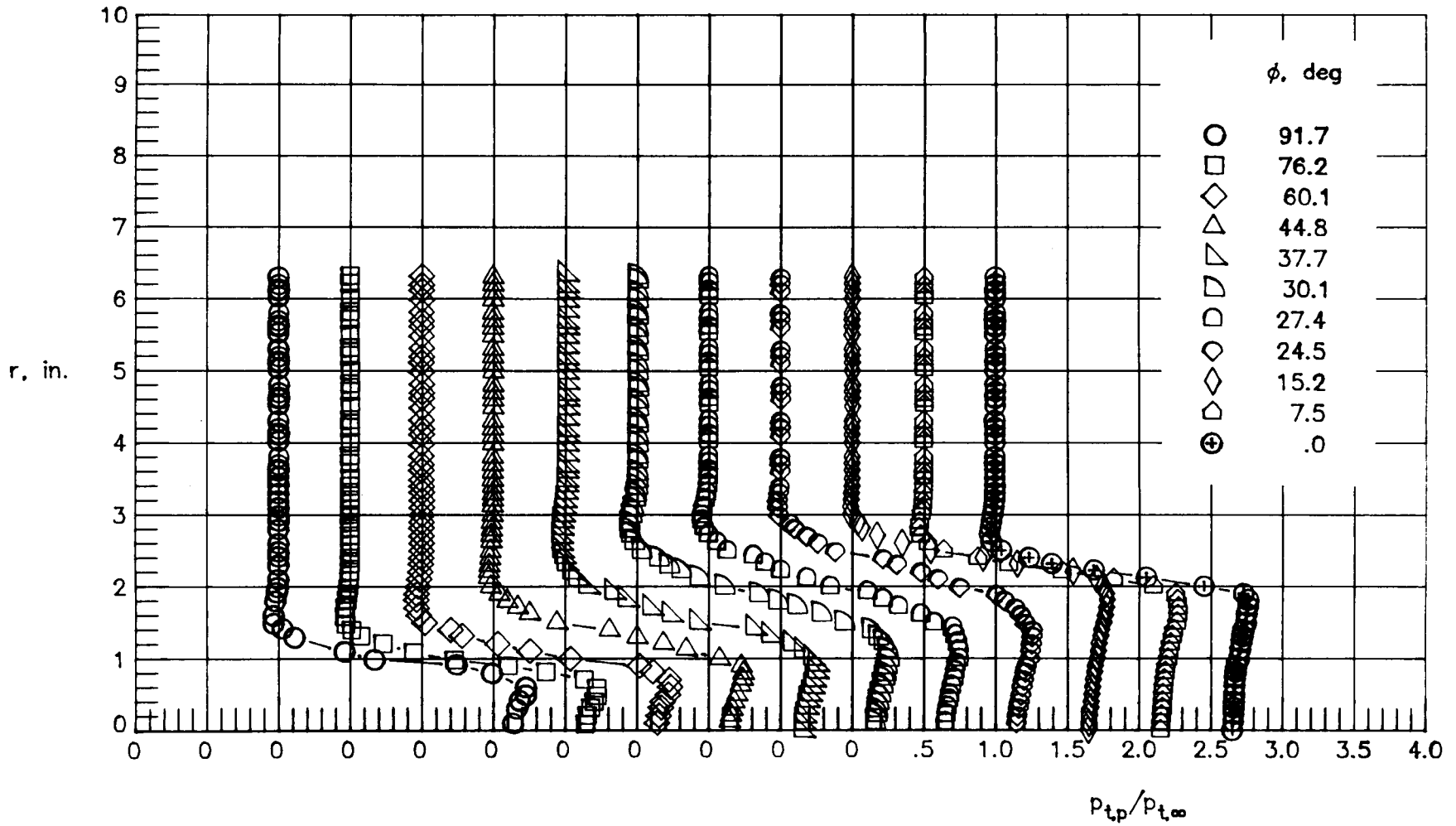
(a) x = 0.0 in.

Figure 7.- Variation of pitot pressure with r and ϕ at M_∞ = 0.60 and NPR = 4.0.



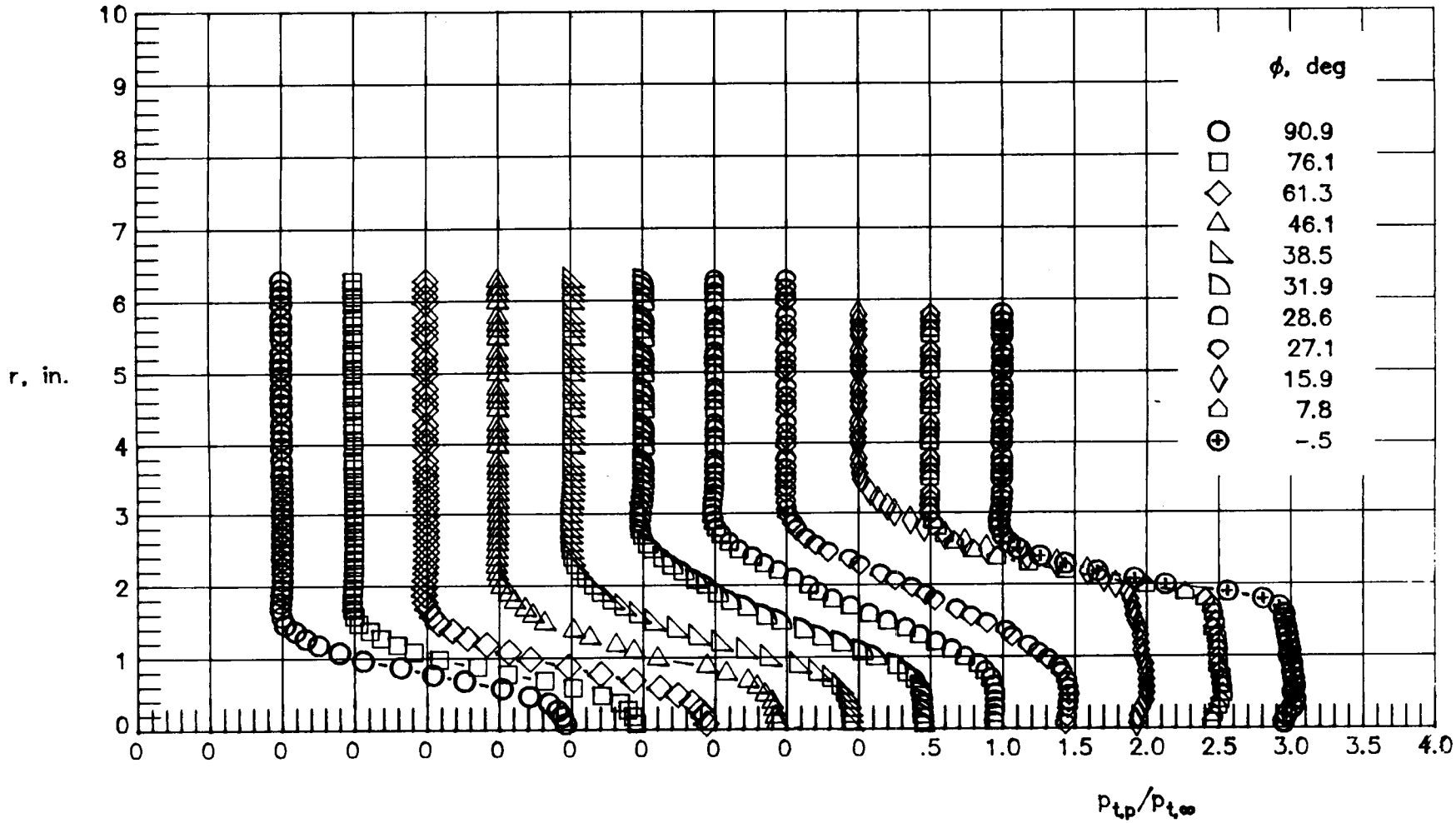
(b) x = 2.6 in.

Figure 7.- Continued.



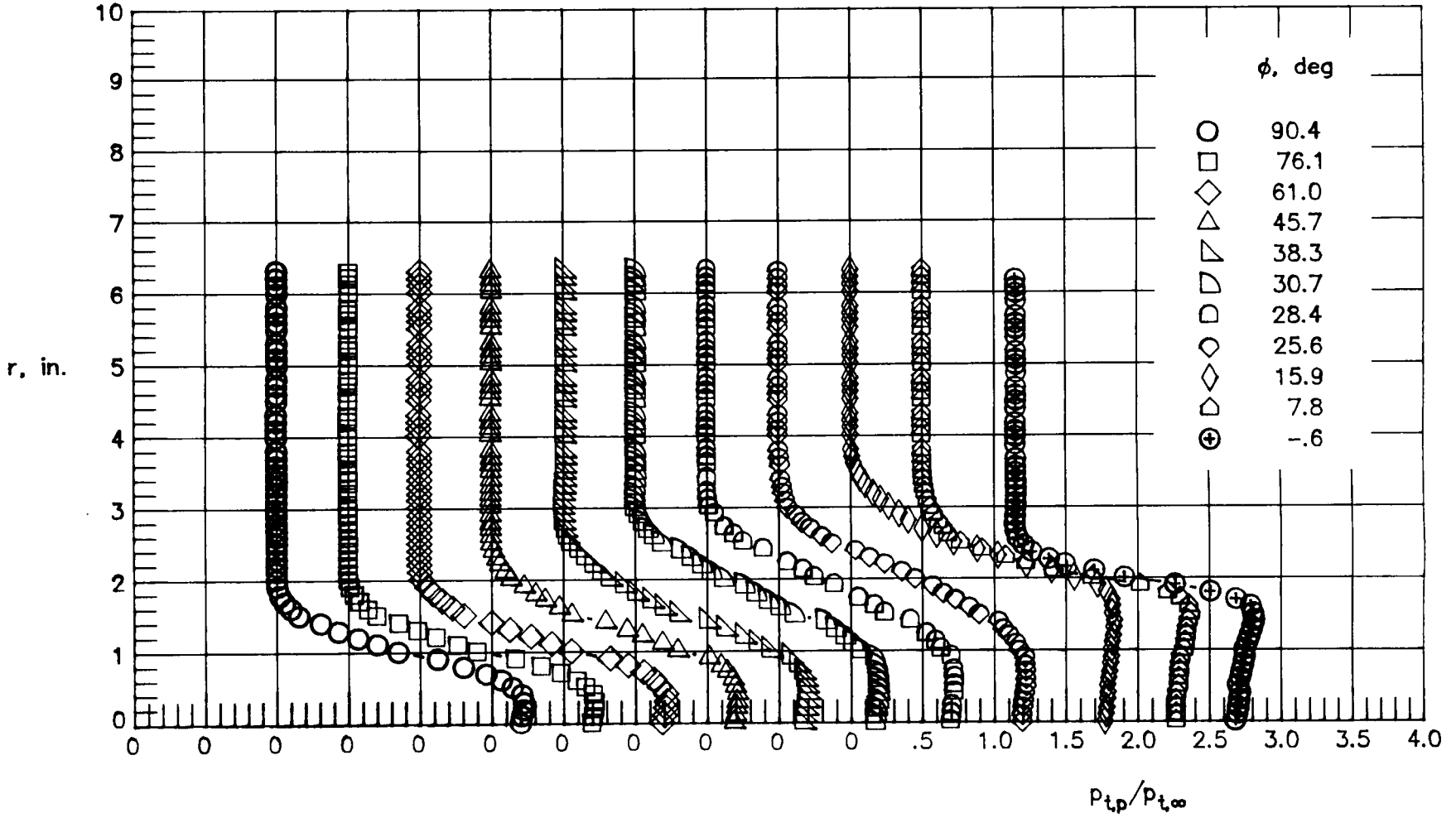
(c) x = 5.2 in.

Figure 7.- Continued.



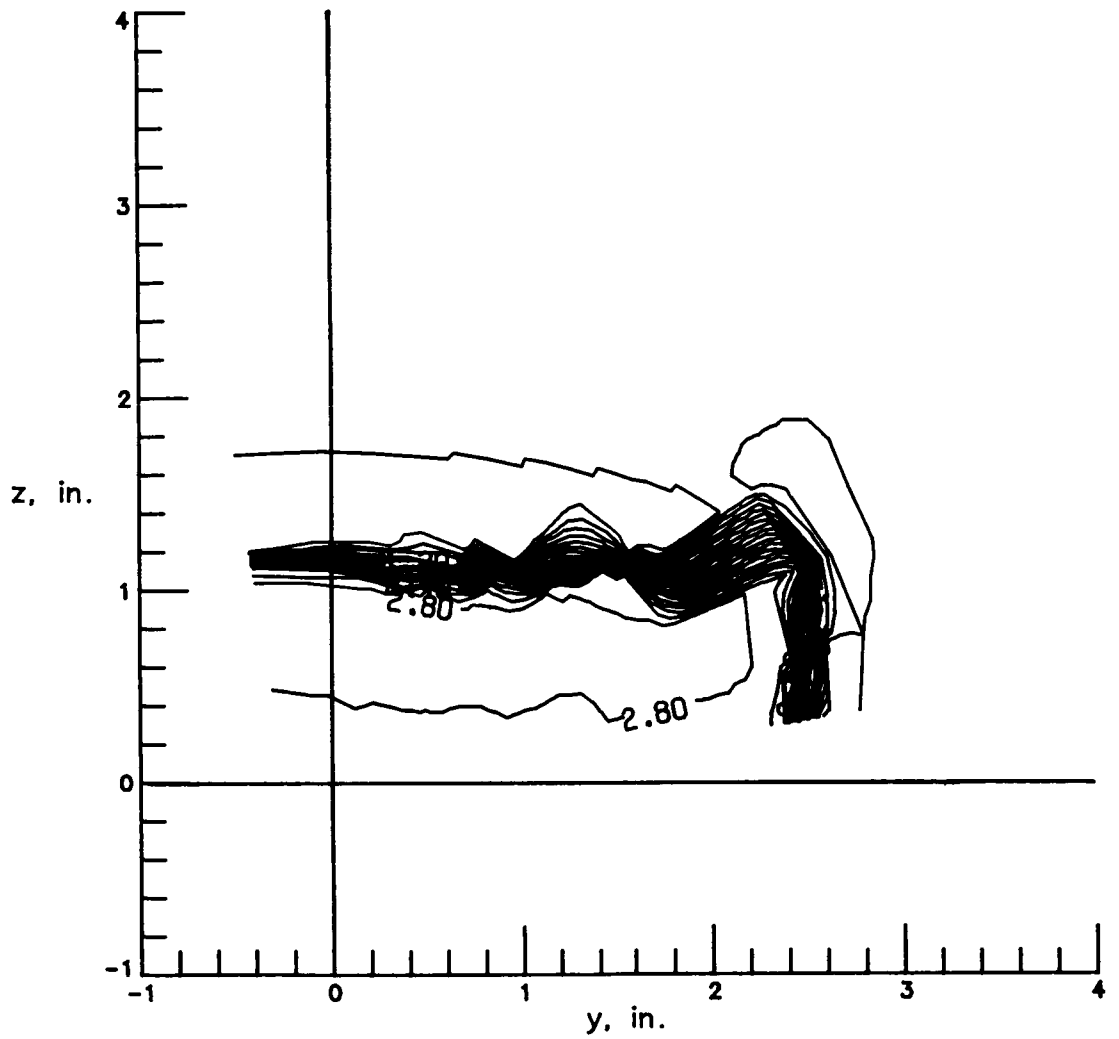
(d) x = 7.8 in.

Figure 7.- Continued.



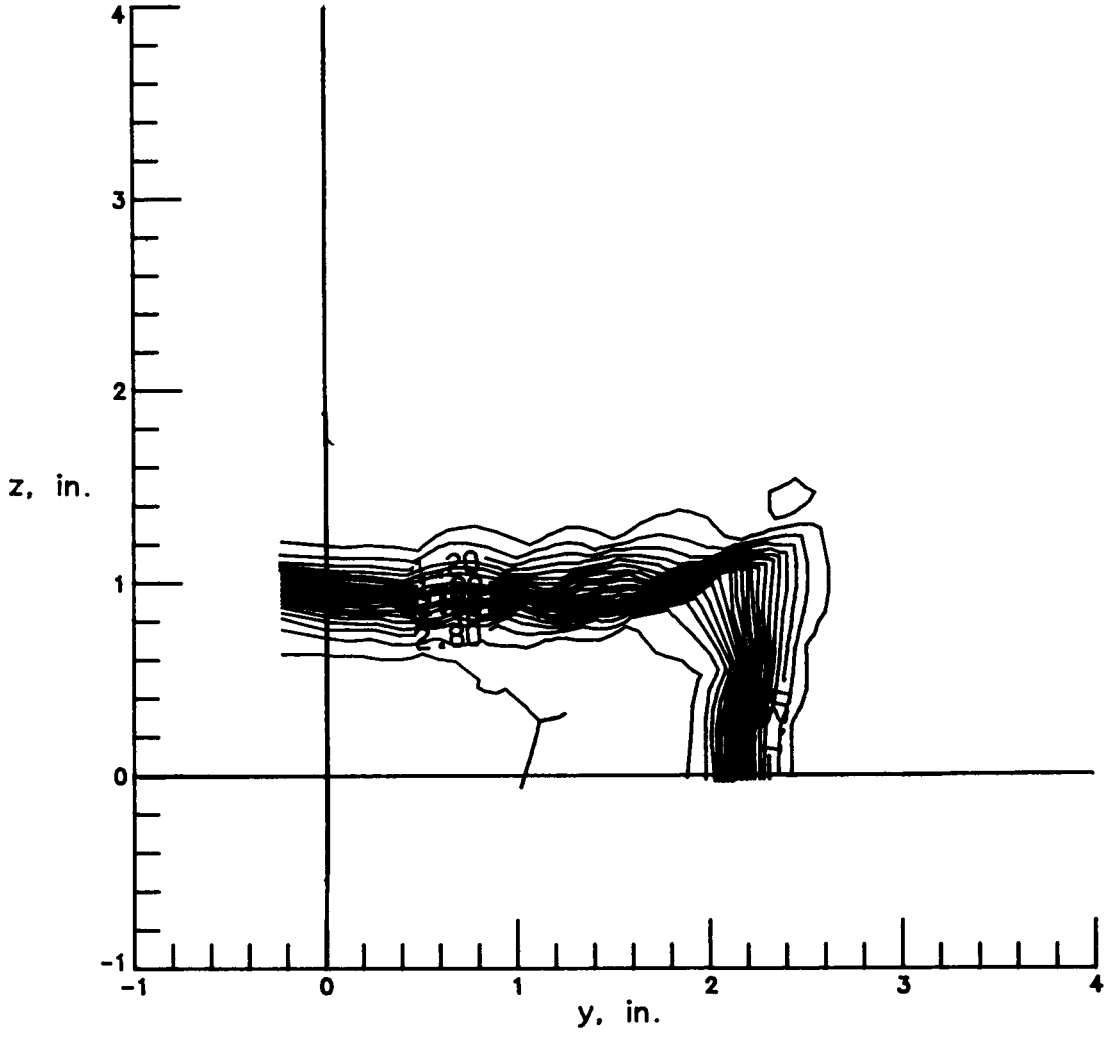
(e) x = 10.4 in.

Figure 7.- Concluded.



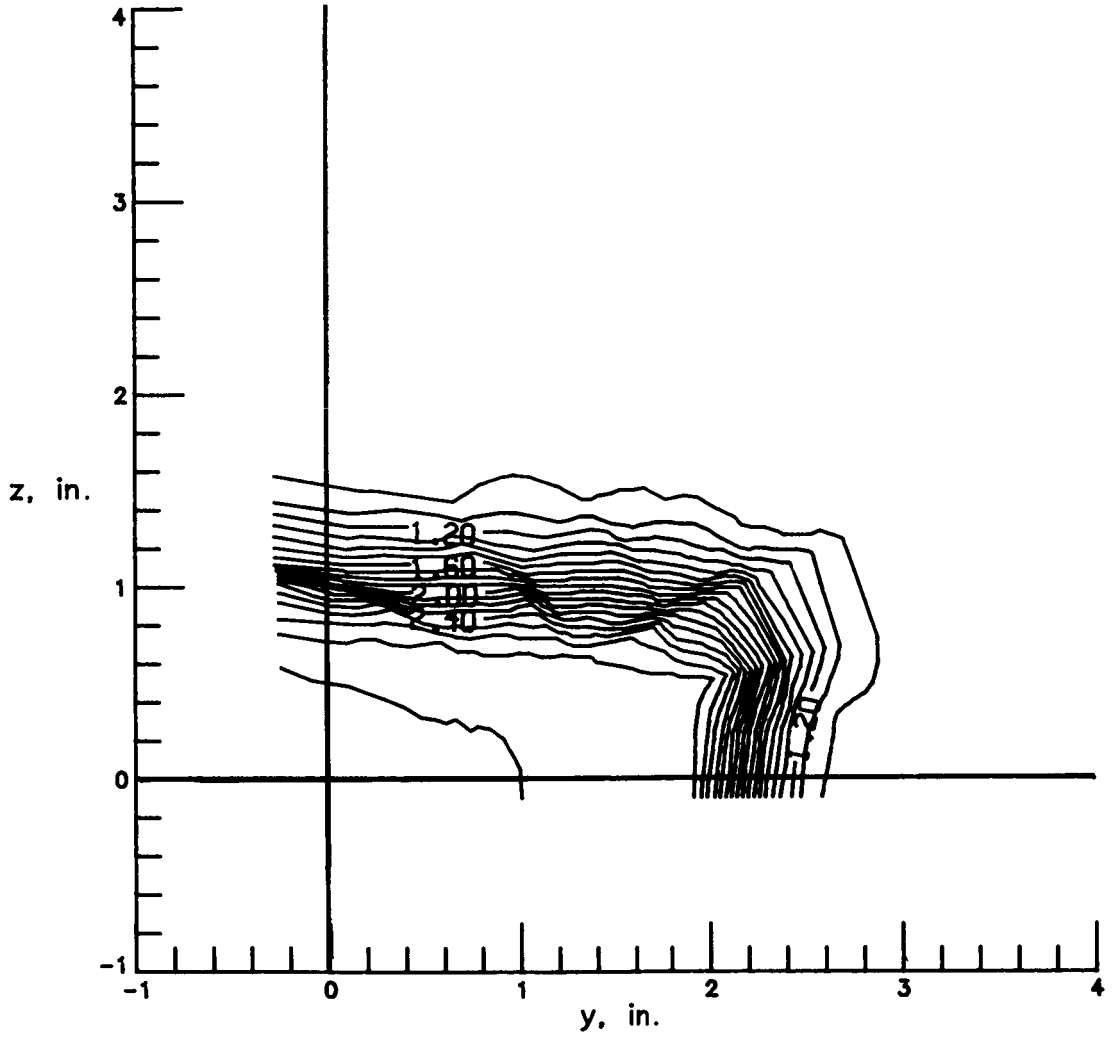
(a) x = 0.0 in.

Figure 8.- Contour plots of $p_{t,p}/p_{t,\infty}$ at $M_\infty = 0.60$ and NPR = 4.0.



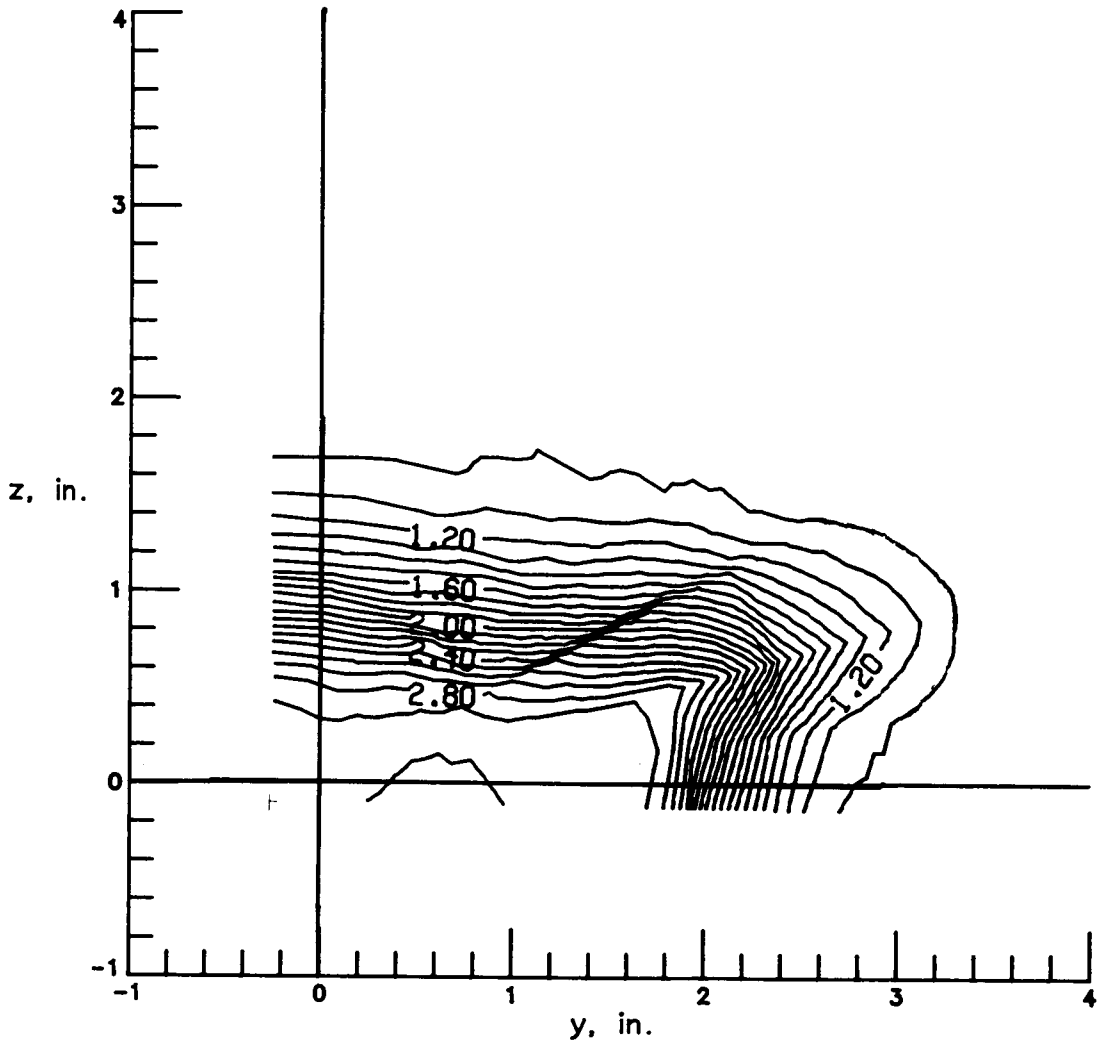
(b) x = 2.6 in.

Figure 8.- Continued.



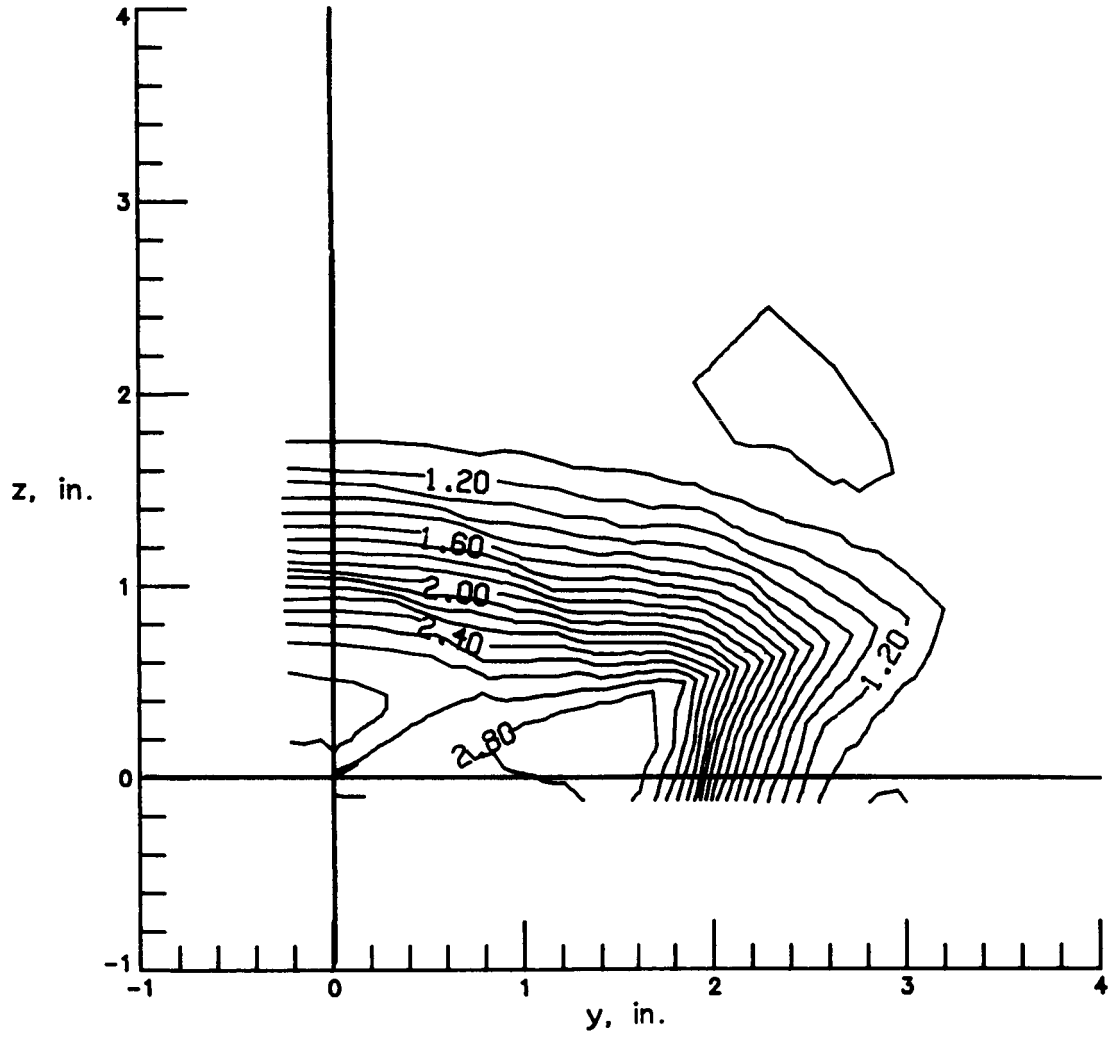
(c) x = 5.2 in.

Figure 8.- Continued.



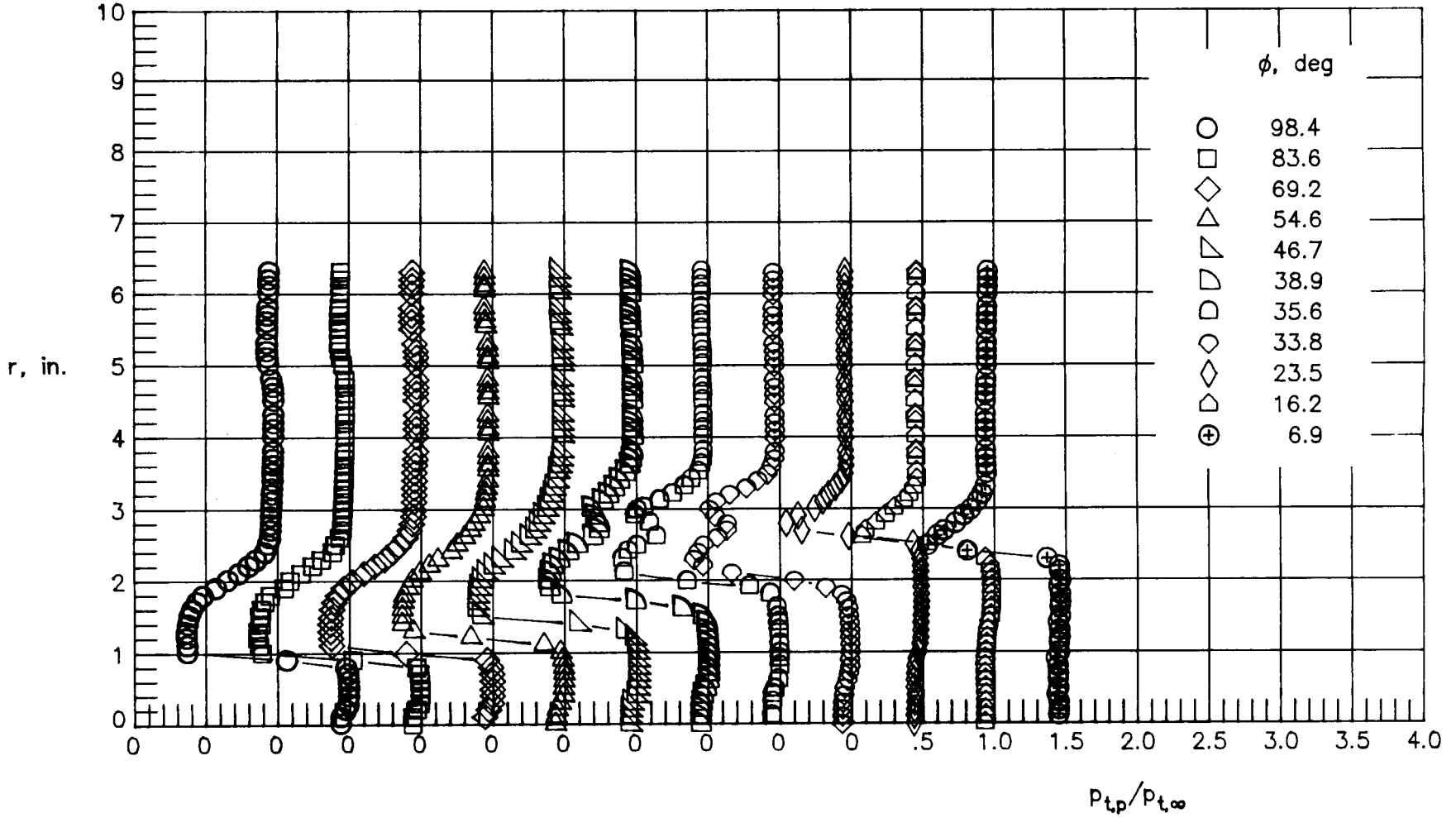
(d) x = 7.8 in.

Figure 8.- Continued.



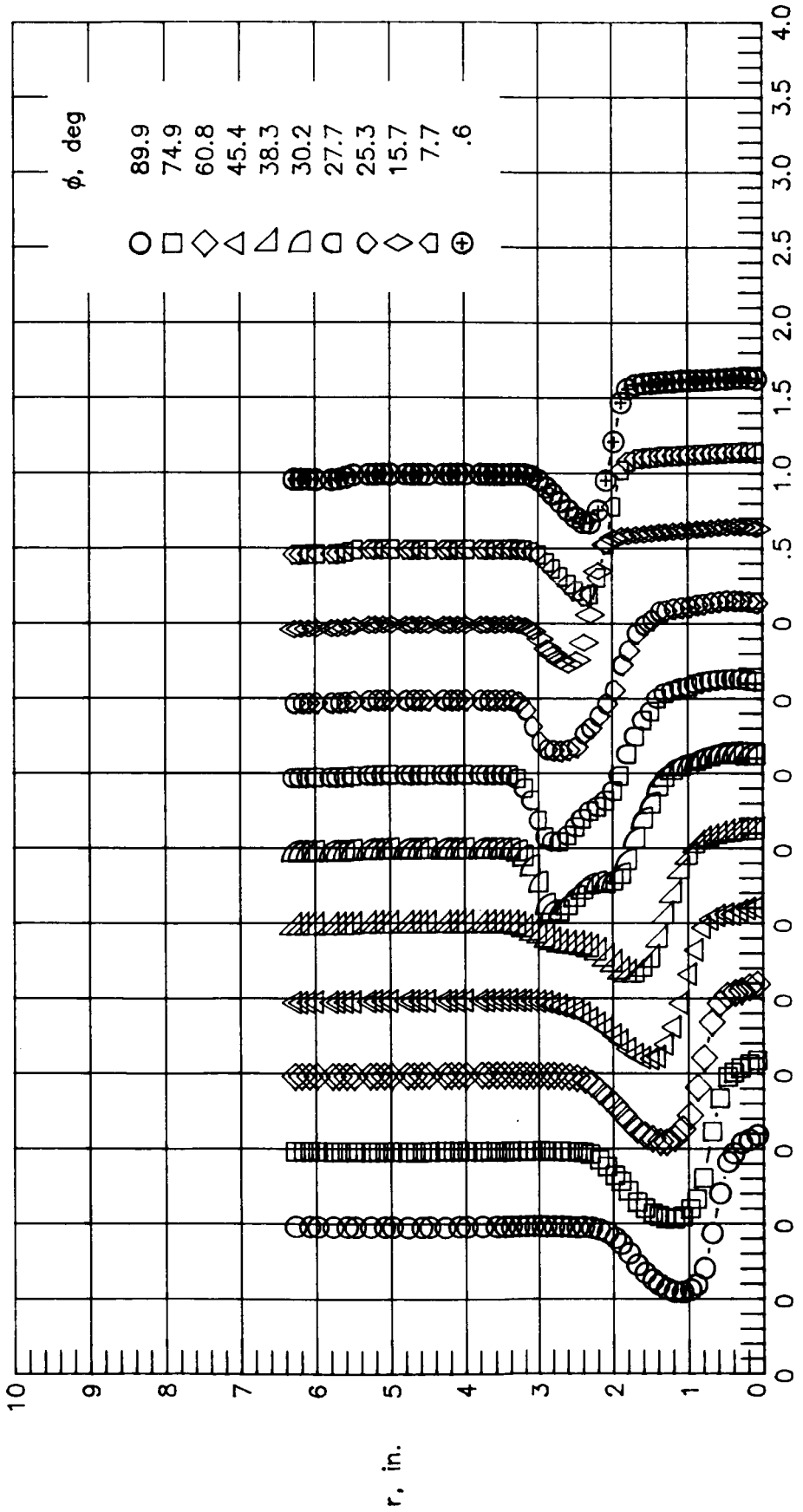
(e) x = 10.4 in.

Figure 8.- Concluded.



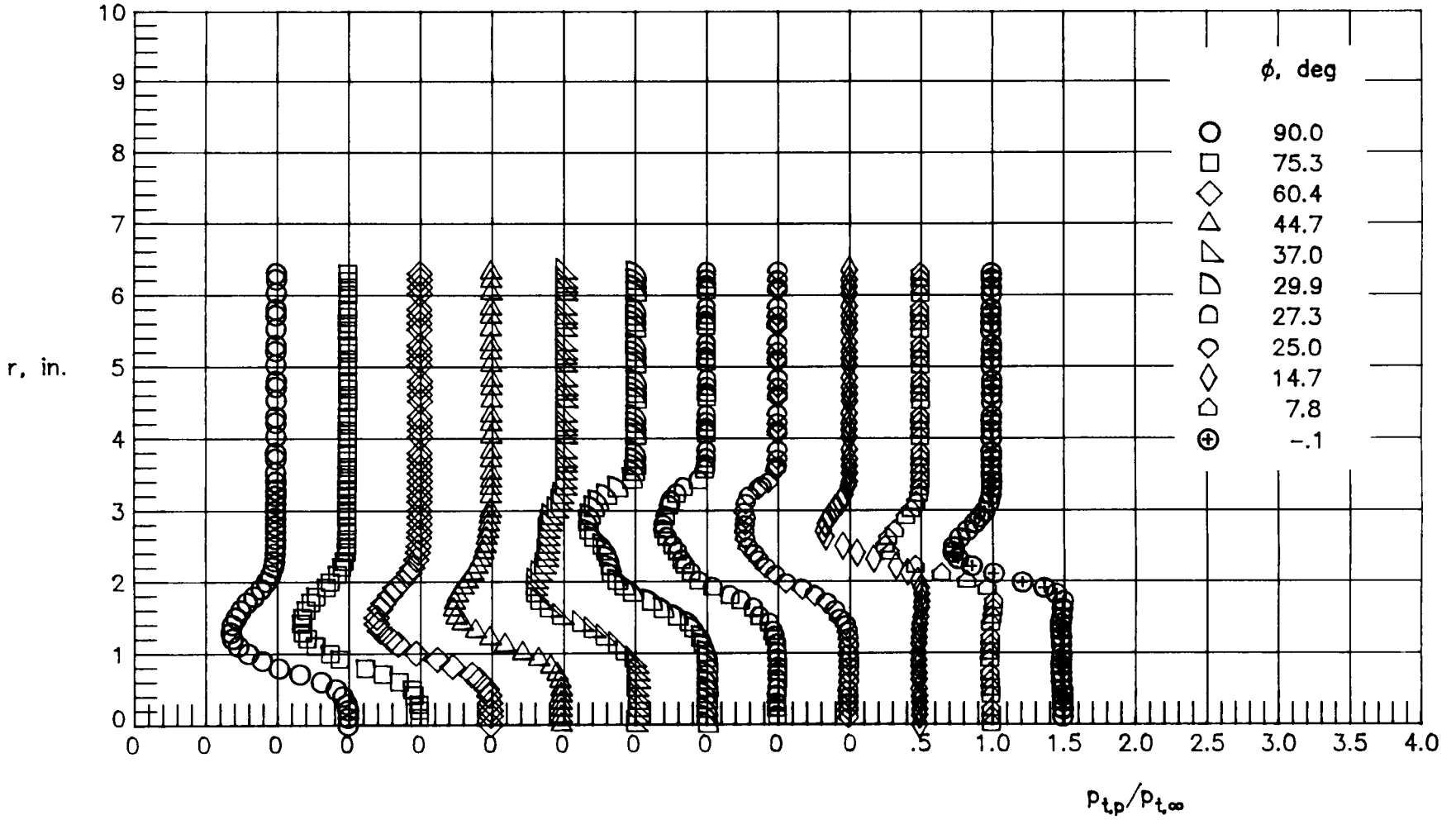
(a) x = 0.0 in.

Figure 9.- Variation of pitot pressure with r and ϕ at M_∞ = 1.20 and NPR = 4.0.



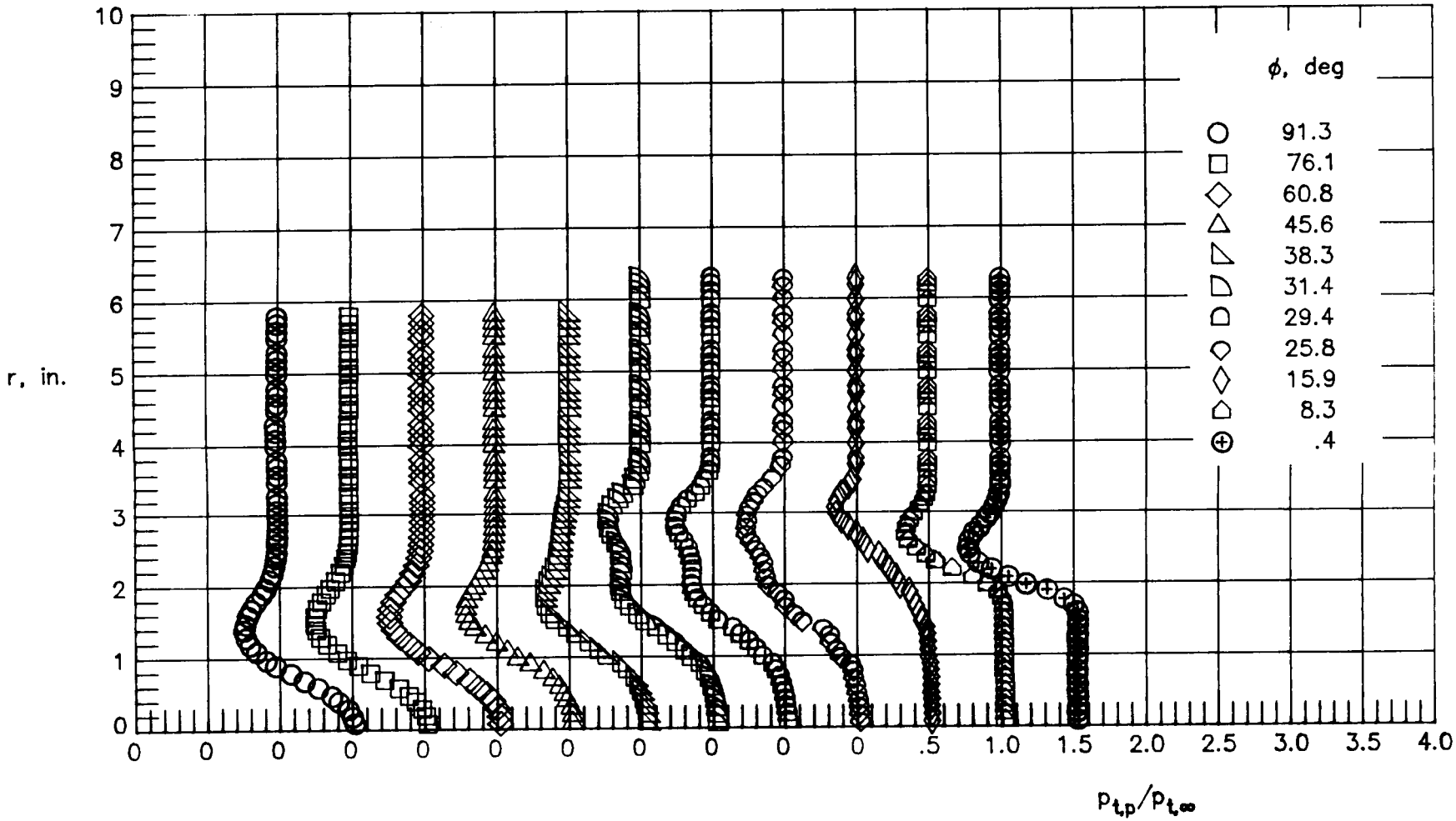
(b) x = 2.6 in.

Figure 9.- Continued.



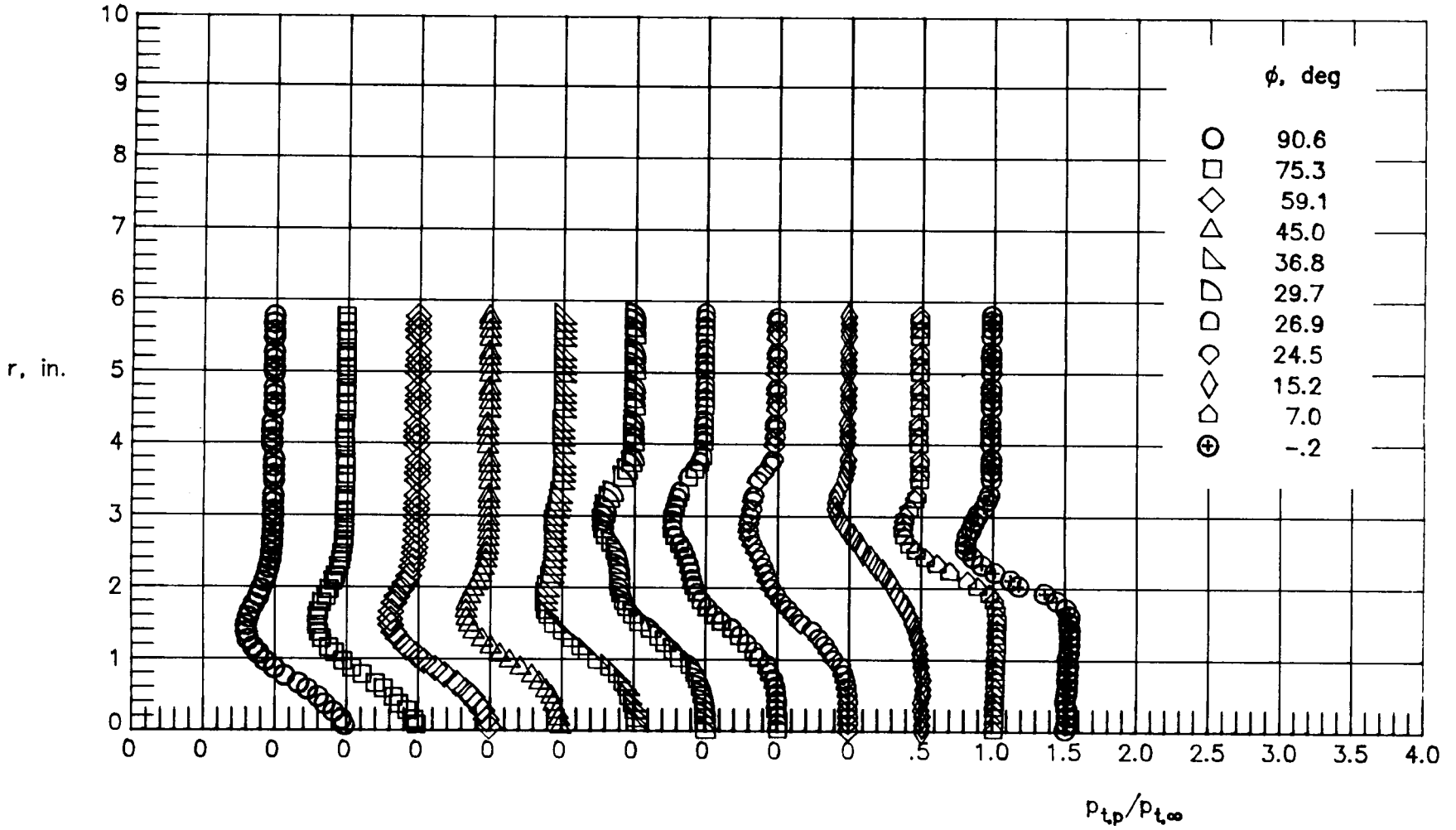
(c) x = 5.2 in.

Figure 9.- Continued.



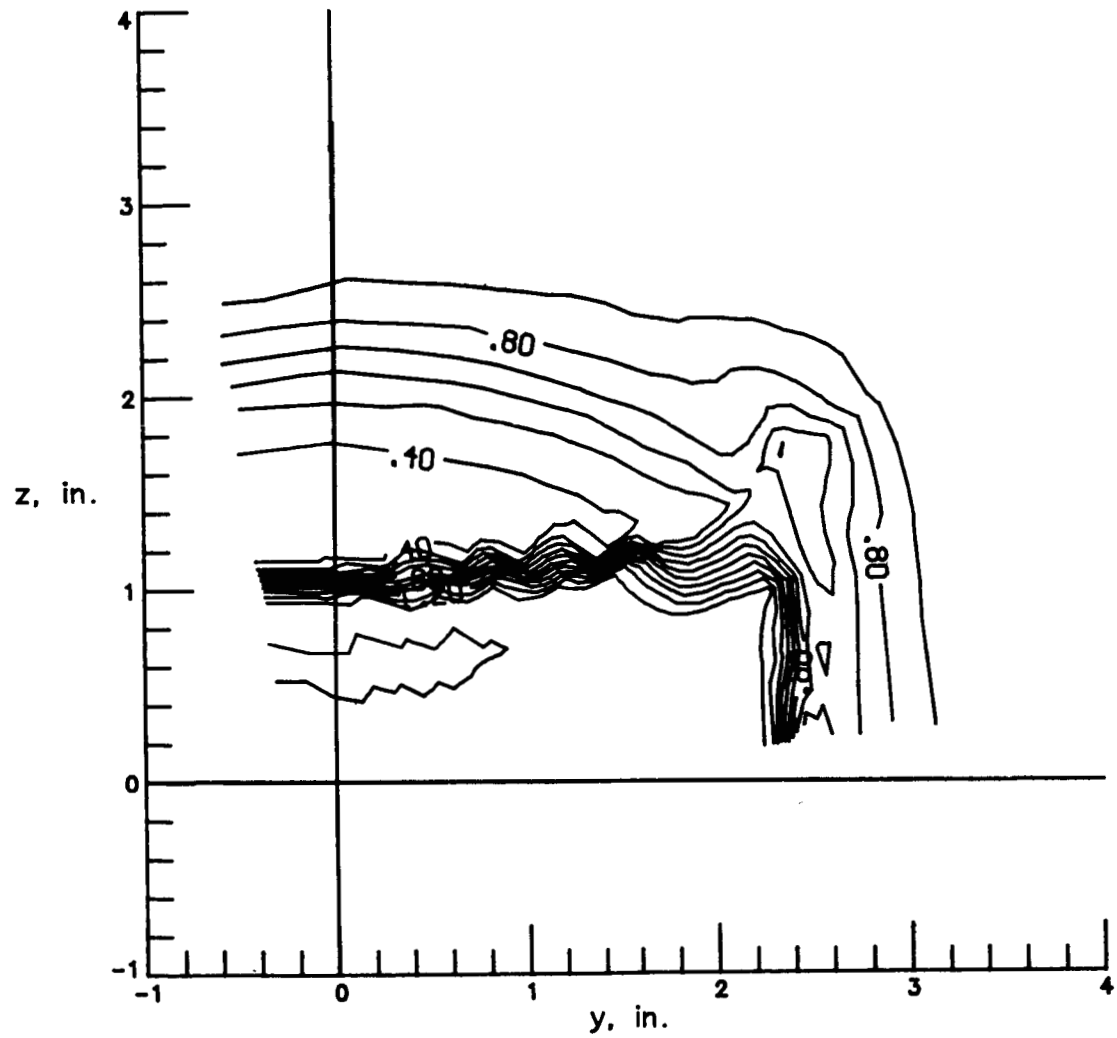
(d) x = 7.8 in.

Figure 9.- Continued.



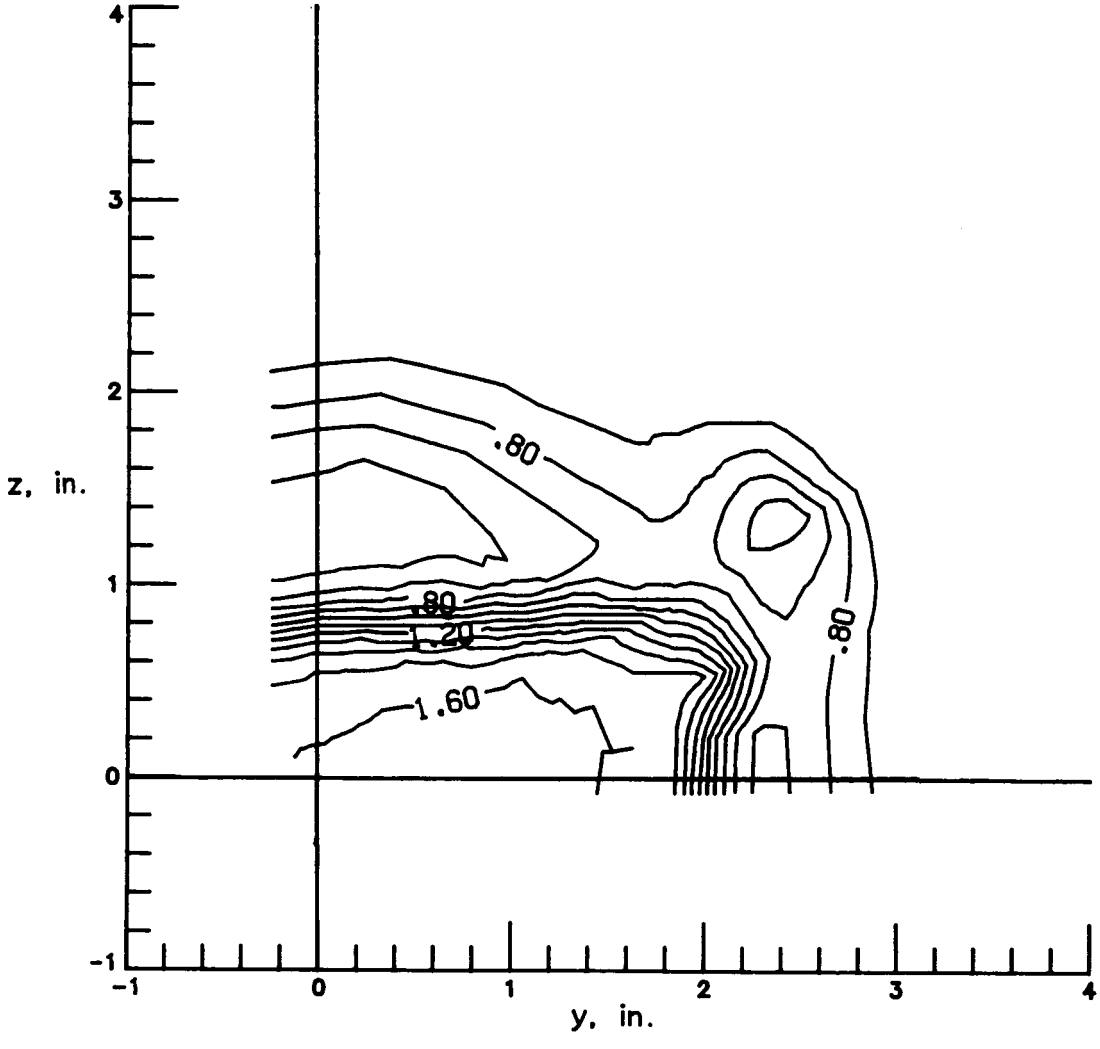
(e) x = 10.4 in.

Figure 9.- Concluded.



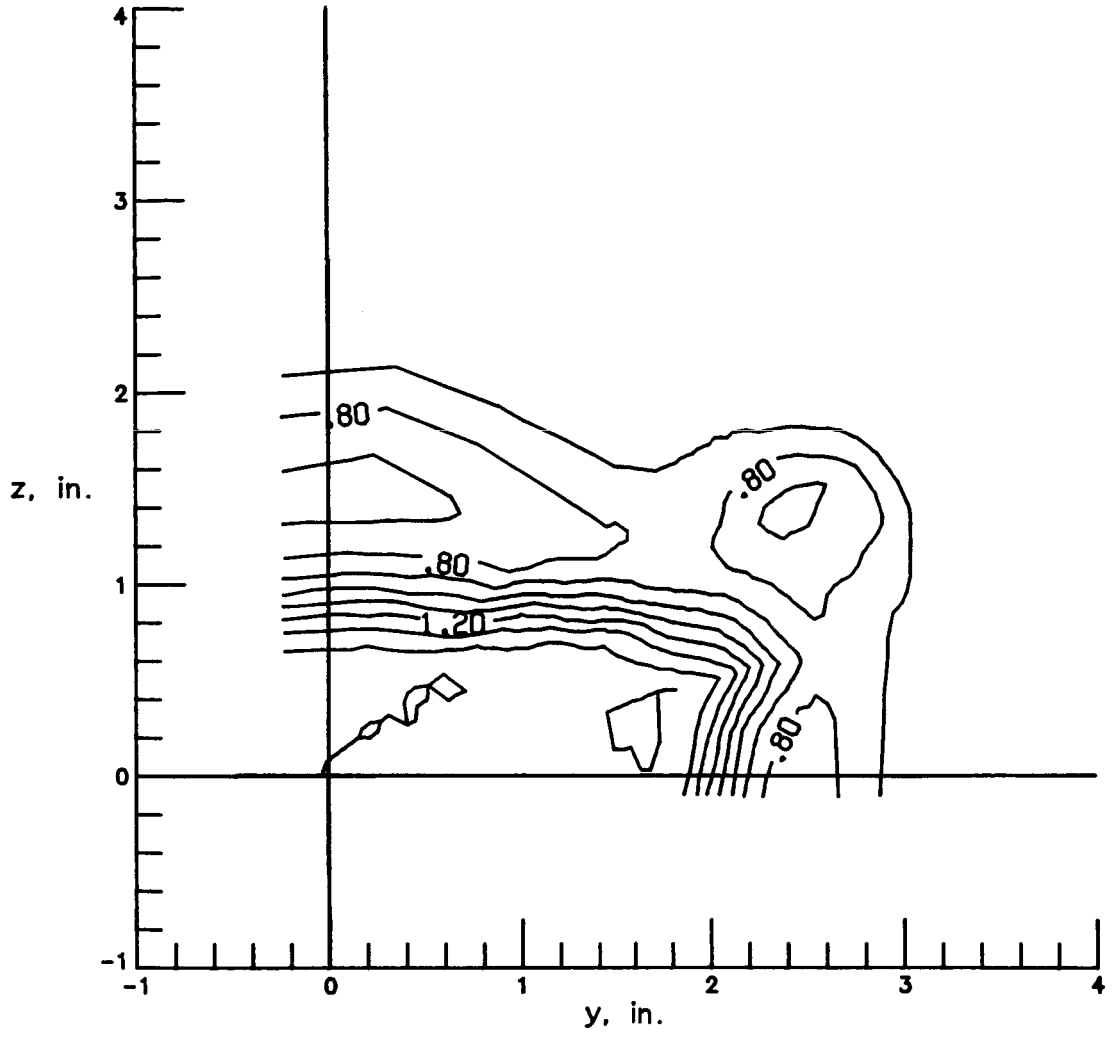
(a) x = 0.0 in.

Figure 10.- Contour plots of $p_{t,p}/p_{t,\infty}$ at $M_\infty = 1.20$ and NPR = 4.0.



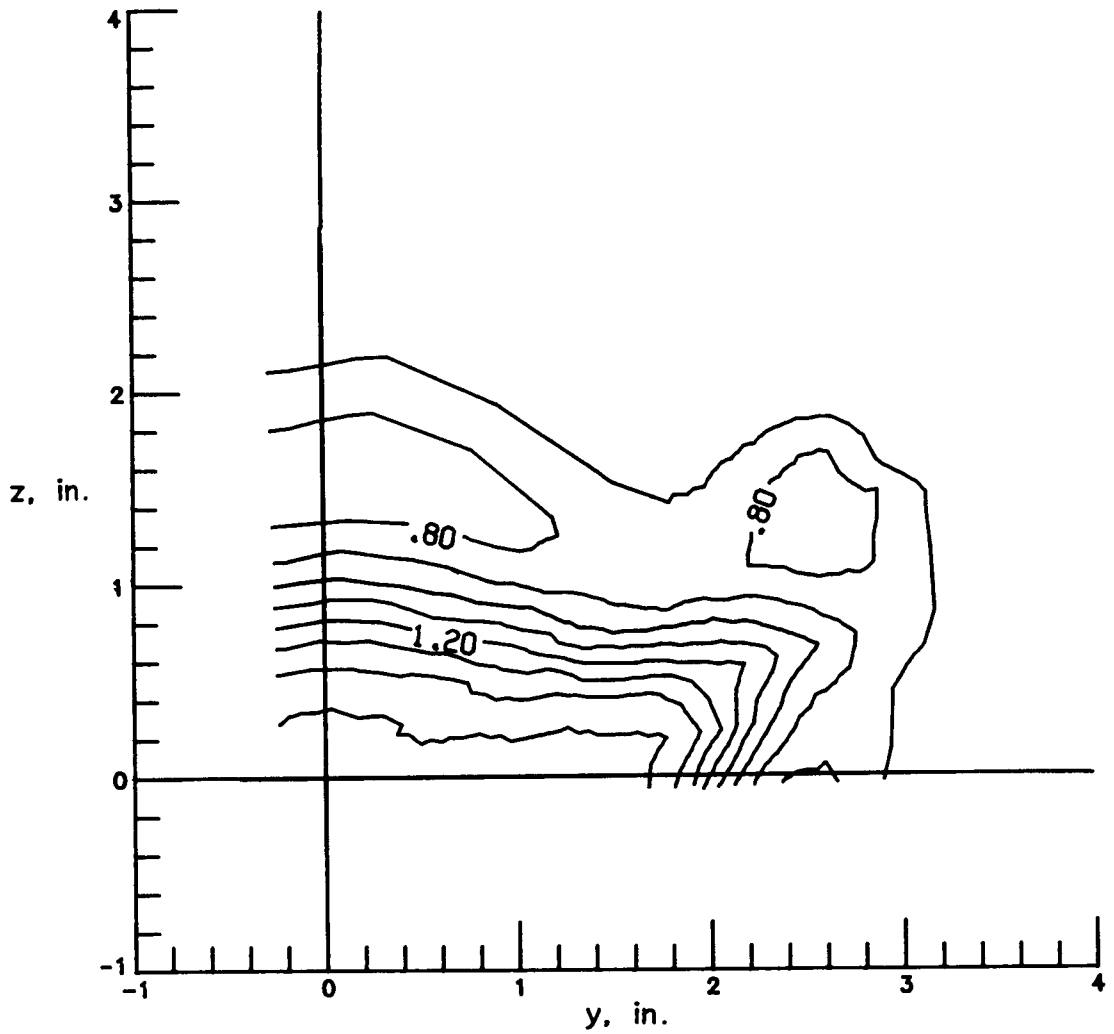
(b) x = 2.6 in.

Figure 10.- Continued.



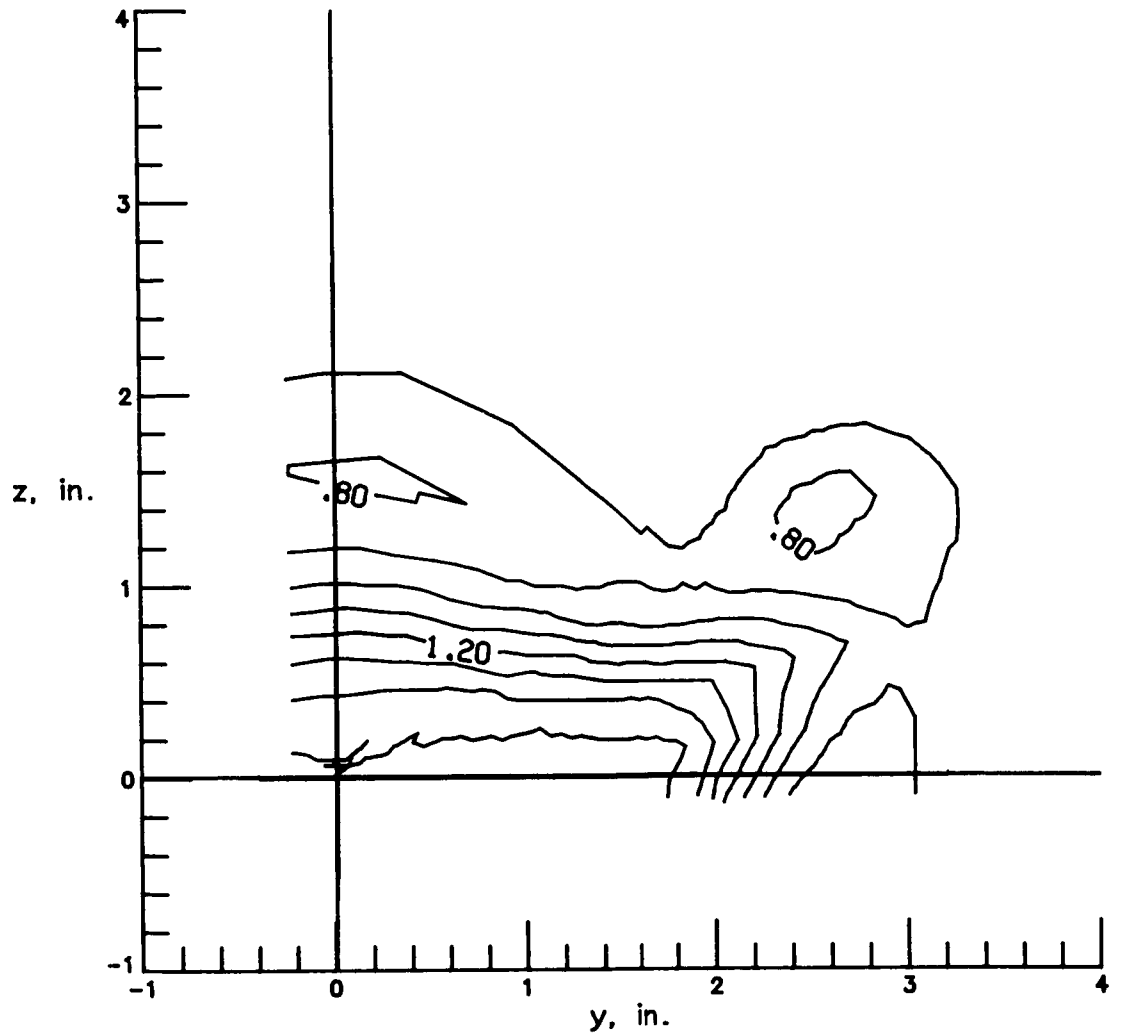
(c) x = 5.2 in.

Figure 10.- Continued.



(d) x = 7.8 in.

Figure 10.- Continued.



(e) x = 10.4 in.

Figure 10.- Concluded.

Standard Bibliographic Page

1. Report No.	2. Government Accession No.	3. Recipient's Catalog No.
NASA TM-88990		

4. Title and Subtitle	5. Report Date
Pitot-Pressure Measurements in Flow Fields Behind a Rectangular Nozzle With Exhaust Jet for Free-Stream Mach Numbers of 0.00, 0.60, and 1.20	November 1986
	6. Performing Organization Code: 505-62-91-01
7. Author(s): Lawrence E. Putnam and Charles E. Mercer	8. Performing Organization Report No.: L-16166
9. Performing Organization Name and Address: NASA Langley Research Center, Hampton, VA 23665-5225	10. Work Unit No.
	11. Contract or Grant No.
12. Sponsoring Agency Name and Address: National Aeronautics and Space Administration, Washington, DC 20546-0001	13. Type of Report and Period Covered: Technical Memorandum
	14. Sponsoring Agency Code

15. Supplementary Notes

16. Abstract

An investigation has been conducted in the Langley 16-Foot Transonic Tunnel to measure the flow field in and around the jet exhaust from a nonaxisymmetric nozzle configuration. The nozzle had a rectangular exit with a width-to-height ratio of 2.38. Pitot-pressure measurements were made at five longitudinal locations downstream of the nozzle exit. The maximum distance downstream of the exit was about 5 nozzle heights. These measurements were made at free-stream Mach numbers of 0.00, 0.60, and 1.20 with the nozzle operating at a ratio of nozzle total pressure to free-stream static pressure of 4.0. The jet exhaust was simulated with high-pressure air that had an exit total temperature essentially equal to the free-stream total temperature.

17. Key Words (Suggested by Authors(s))	18. Distribution Statement
Jet exhaust Transonic speeds Flow-field measurements Rectangular nozzles	Unclassified - Unlimited Subject Category 02

19. Security Classif.(of this report)	20. Security Classif.(of this page)	21. No. of Pages	22. Price
Unclassified	Unclassified	152	A08

For sale by the National Technical Information Service, Springfield, Virginia 22161

NASA-Langley, 1986